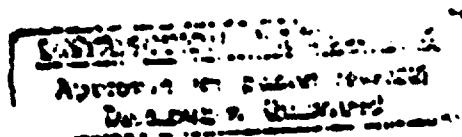


ENERGY ENGINEERING ANALYSIS PROGRAM  
STUDY REPORT

EXECUTIVE SUMMARY  
FINAL REPORT

ANNISTON ARMY DEPOT  
ANNISTON, ALABAMA



MOBILE DISTRICT  
CORPS OF ENGINEERS

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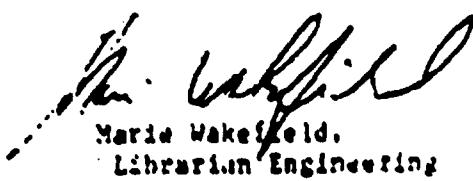


DEPARTMENT OF THE ARMY  
CONSTRUCTION ENGINEERING RESEARCH LABORATORY, CHAMPAIGN, ILLINOIS  
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A handwritten signature in black ink, appearing to read "Marie Wakefield".

Marie Wakefield,  
Librarian Engineering

## EXECUTIVE SUMMARY

This is a summary of the Energy Engineering Analysis performed for the Anniston Army Depot (AAD) in Anniston, Alabama. It includes recommendations to be considered in the development of a Basewide Energy Plan, consisting of energy conservation projects and other recommendations for reduction of the installation's 1983 source energy consumption.

Anniston Army Depot is located in Northeastern Alabama, approximately 10 miles west of the City of Anniston. The Depot is the largest combat vehicle rebuilding facility in the free world. The eastern part of the property is gently rolling land, while the western part is hilly with some steep slopes. The Coosa River Storage Annex is operated as part of the Depot, with land ranging from gently rolling to mountainous.

This summary presents data on:

- Historical and predicted energy consumption
- Energy conservation procedures for distribution systems
- Energy conservation procedures for buildings and processes
- Utilization of energy monitoring and control systems (EMCS)
- Utilization of wood biomass and waste fuels
- Cogeneration and Replacement Boilers

The conservation of energy in existing facilities can be accomplished in the following two ways:

- Reduce the basic system energy requirements and source energy use
- Recover energy discharged from one user and utilize this waste energy for other purposes

A reduction in system energy requirements is represented by such activities as lowering equipment operating temperatures, reduction of transmission losses by better insulation, and night/weekend setback or shutdown of energy users and associated distribution systems.

Recovery of energy discharged by one user and utilization of this waste energy for other purposes is demonstrated by such activities as returning condensate to boiler systems and recovery of heat from process exhaust air systems to preheat replacement air. Examples of energy below the level of practical utilization are exhaust flue gases from boilers (cooled to near the dew point), and air exhausted from buildings near ambient temperature conditions.

This study has been directed towards identifying means of energy conservation conforming to those two methods identified as reduction in overall use and recovery of waste energy. Although the above discussion may appear to be confined to heat energy, investigations covered electrical usage, water usage, compressed air, wood biomass and solar energy.

The number and type of viable ECIP funded projects has been restricted by direction of the COR, Mobile to those which qualify at an Energy/Cost ratio of 1.0 or greater for fiscal year 1985, and which exceed a Capital Cost Value of \$100,000. The total energy savings presented in this report can be obtained only upon full implementation of the viable ECIP projects, compliance with the recommended conservation measures requiring capital investments less than \$100,000, and those measures requiring policy changes at the management level.

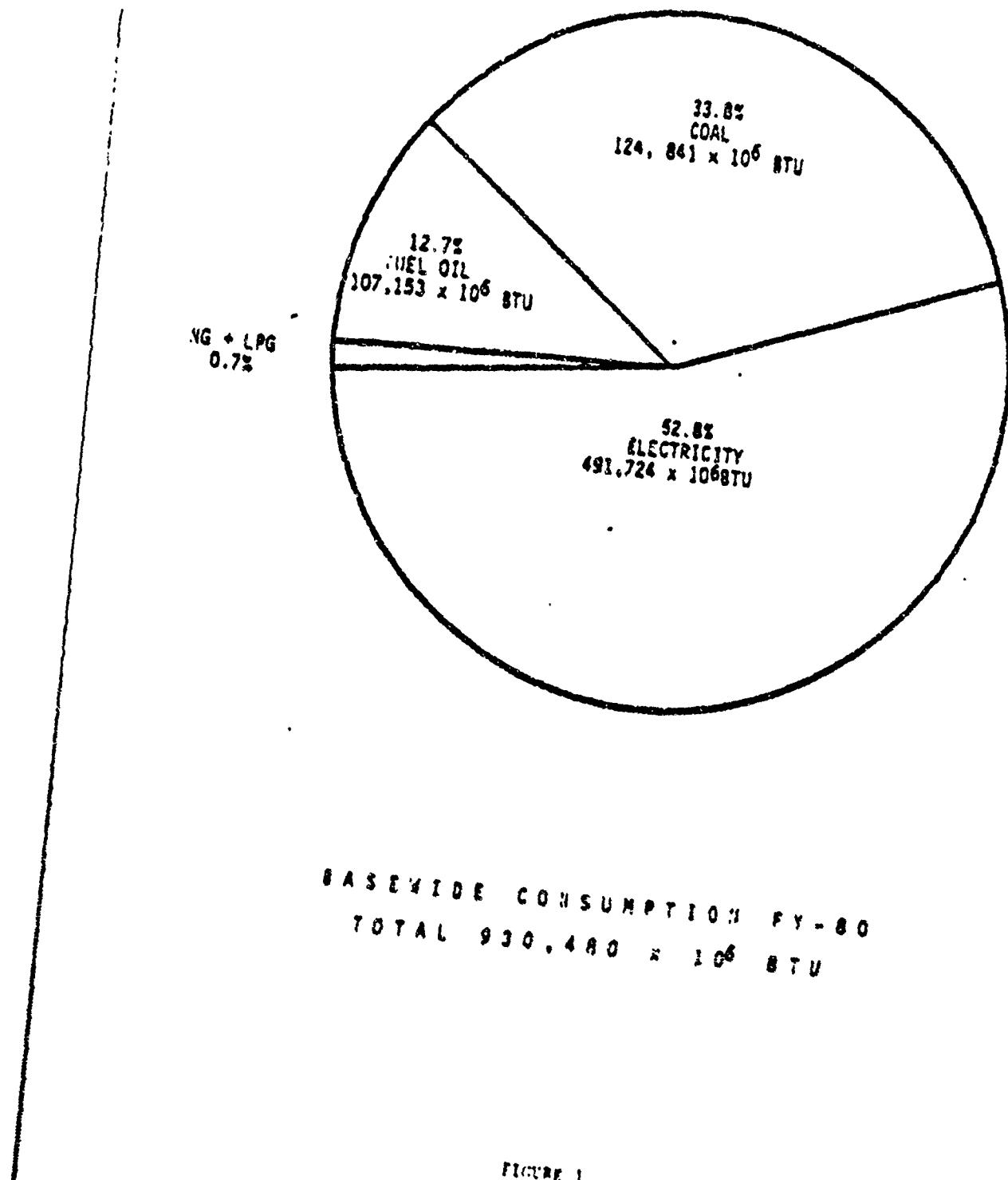
Computer simulations of building energy use were modeled using the DOE-2.1 program. Computer simulations for energy utilization were performed on typical building types. Categorizing and prototyping methodology followed procedures outlined in the Black & Veatch Study "Engineering Instructions for Preparation of a Basewide Energy Systems Plan", dated January 1980. After careful examination of the ANAD facilities during field surveys, taking into consideration the building construction, building functions, and plant operating procedures, a total of 13 typical buildings were computer modeled to determine their energy use, both thermal and electrical, and to verify recorded historical energy consumption figures during the base year 1979. The final analysis resulted in a correlation which was within 2 percent of recorded consumption figures.

Energy conservation projects were generated from the energy model for conservation measures involving building insulation, reduction in fenestration area, temperature controls installation, re-lighting with energy-efficient fixtures, and a basewide EMCSS. A detailed analysis is provided in the main report.

The following is a tabulation of the ANAD source energy consumption for the fiscal year ending September 1980.

|                |                           |
|----------------|---------------------------|
| Electricity    | $691,726 \times 10^6$ BTU |
| Fuel Oil No. 2 | $118,363 \times 10^6$ BTU |
| Coal           | $314,658 \times 10^6$ BTU |
| Natural Gas    | $78.6 \times 10^6$ BTU    |
| LPG            | $6,275.8 \times 10^6$ BTU |
| Total          | 130,480 Mera BTU          |

... .



This yields a total of 930,480 Megn BTU's for FY-80 (see Figure 1).

It is reported that operations during this period were at the normal production level for this facility.

Figure 2 shows the historical and predicted annual energy consumption for a ten-year period through fiscal year 1986, reflecting the effect of proposed conservation measures.

It was determined that the fuel consumption rate for this facility is partially weather-dependent. Since about 43% of the steam generated in the boilers is consumed in process operations, the remainder is therefore consumed in building heating and transmission line losses getting the steam to the buildings. Figure 3 shows the monthly fuel consumption for fiscal year 1980. Note the peaks during the cold winter months.

Figure 4 shows the baseline electrical consumption for the past three fiscal years. Recent annual consumption shows a slight decline due to the shaving of peaks in cold winter months, while the average yearly consumption remains relatively constant between 42 and 43 million kilowatt hours. It is apparent the peaks have been reduced as a result of an Executive Order prohibiting supplemental electrical heating units where a building already contains a main source of heat.

Production levels in the near future can be expected to remain the same as for fiscal year 1980. Therefore, assuming similar weather conditions for the Anniston Area, future fuel consumption on a short term basis should remain relatively constant.

PROJECTED ENERGY CONSUMPTION  
ATMISTON ARMY SEPT  
BASEMIDE FUEL & ELECTRIC

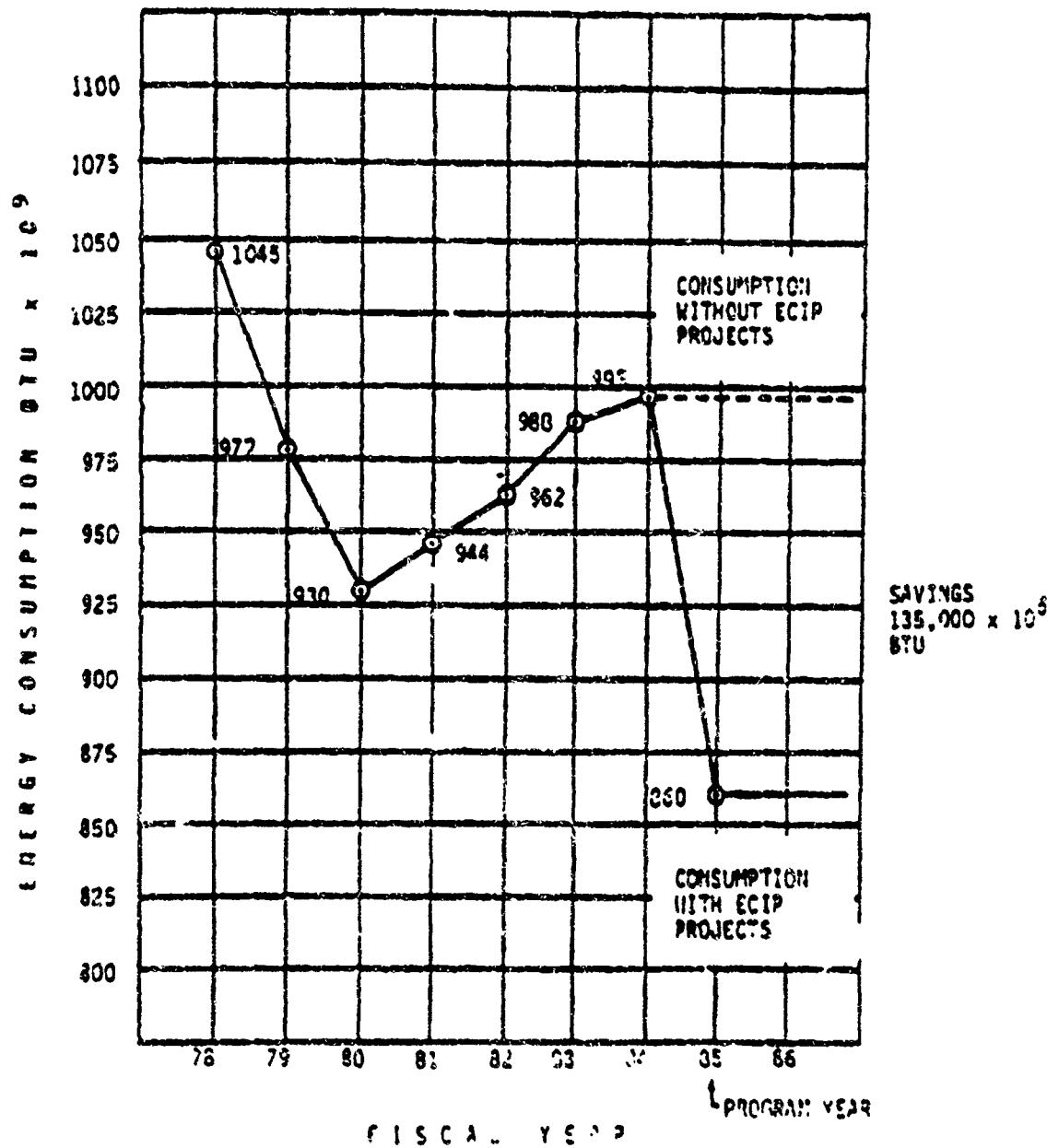


FIGURE 2  
ES-6

BASEWIDE FUEL CONSUMPTION  
ANNISTON ARMY DEPOT FY-80

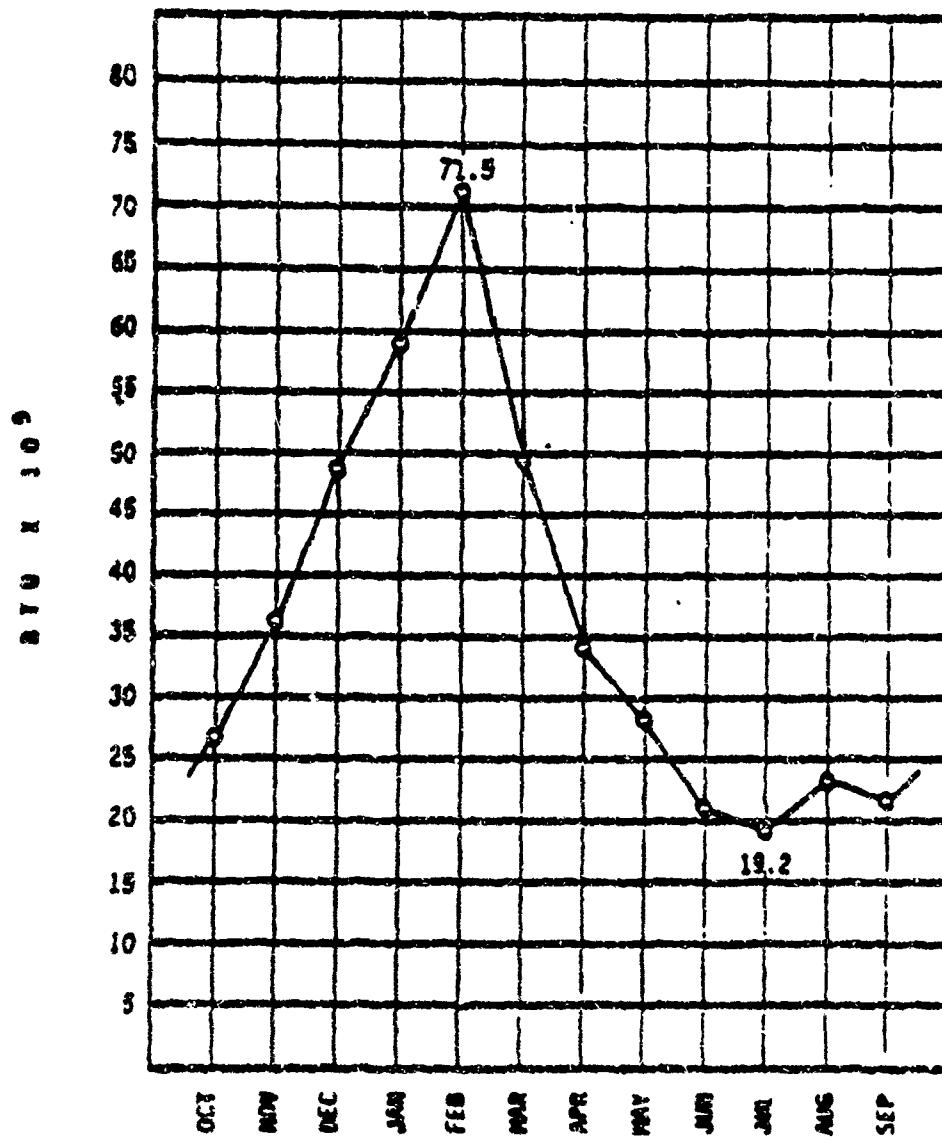
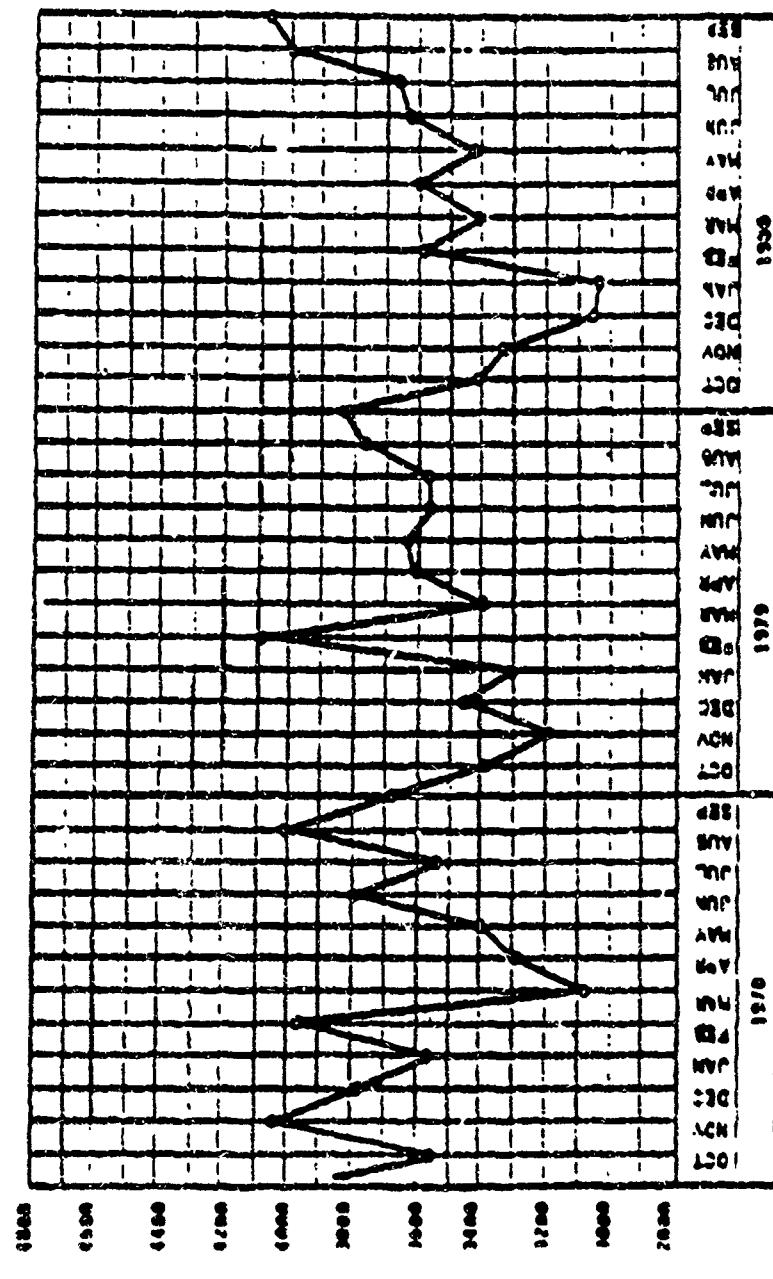


FIGURE 3

FIGURE 6



WATER FLOW DURING ANNUAL POSITION  
1970 - 1971

The projected basewide energy costs through fiscal year 1986 are shown on Figure 5. Projections are made for the facility if operated in its 1980 mode plus projected stream load increases. Predicted costs resulting from the anticipated energy savings from implementation of all energy conservation projects and recommendations in FY-83 are shown by the solid line graph. The following escalation rates were used for calculation purposes:

|              |            |
|--------------|------------|
| Fuel Oil:    | 1.14 (14%) |
| Coal:        | 1.10 (10%) |
| Electricity: | 1.13 (13%) |

A total of 13.6% or 135,000 Mega BTU can be saved annually upon implementation of all viable ECIP projects and energy conservation recommendations determined by this study. Figure 6 shows the total source energy reduction. Further breakdown of the total savings yields the following:

|              |                                |
|--------------|--------------------------------|
| Fuel Oil:    | $5,290 \times 10^6$ BTU saved  |
| Coal:        | $30,290 \times 10^6$ BTU saved |
| Electricity: | $99,200 \times 10^6$ BTU saved |

Projects for source energy reduction are listed in Table 1 with their corresponding E/C ratio. Table A-1 contains projects not qualifying for ECIP funding, requiring less than \$100,000 capital expenditure, but which are considered to be good energy saving measures. (See Appendix A of this summary.)

PROJECTED ENERGY COSTS  
FUEL & ELECTRICITY  
ANNISTON ARMY DEPOT

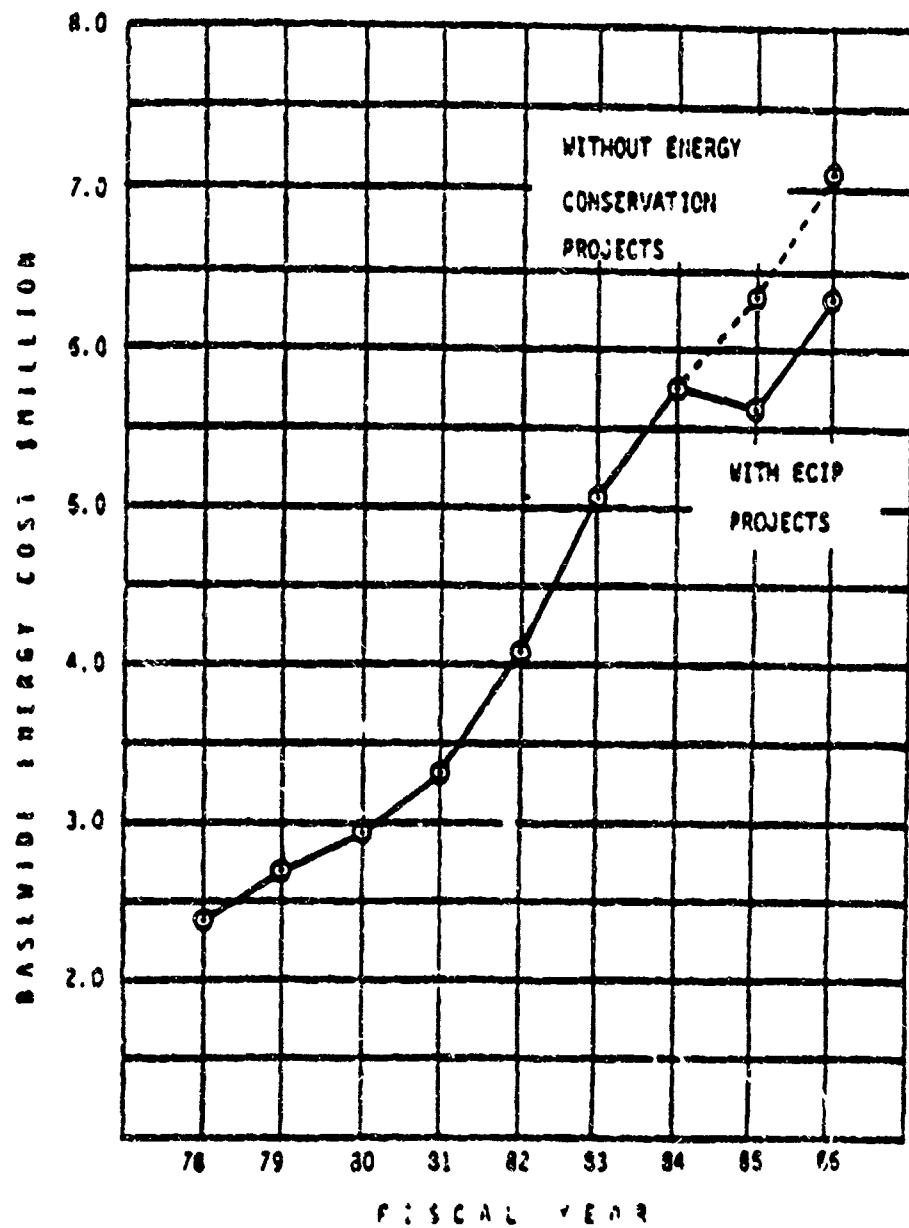
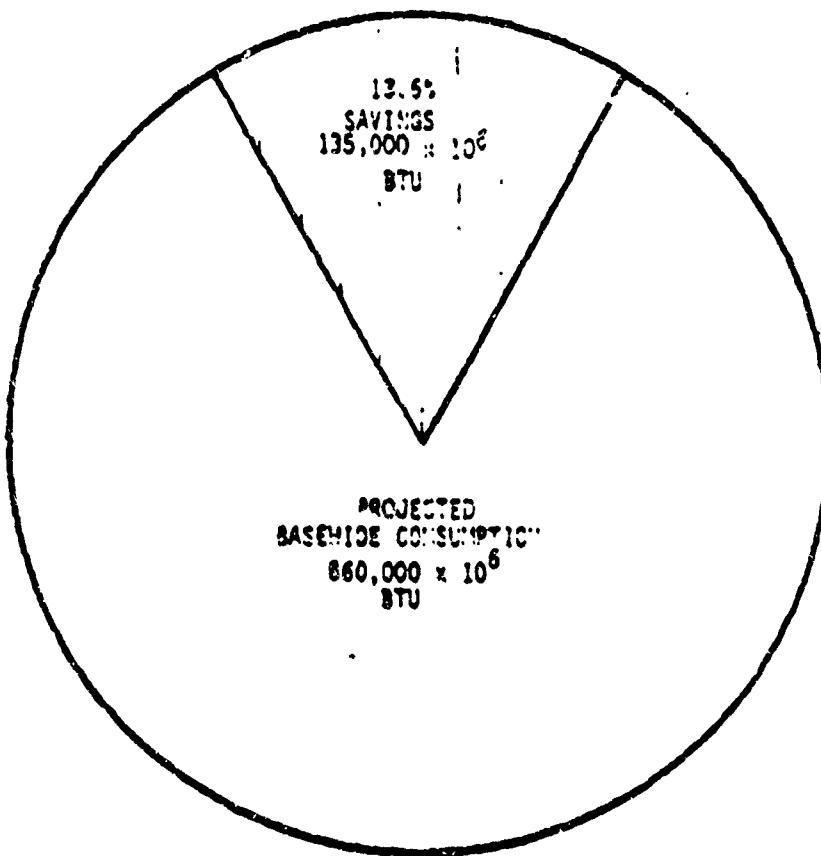


FIGURE 3



BASELINE ENERGY CONSUMPTION  
FY-35  
AFTER ECIP PROJECTS

FIGURE 6

LS-11

Further explanation of the historical energy consumption, basewide energy model, and energy conservation analysis can be found in the Energy Use Survey. The analysis for control schemes and basewide EMCS applications is included in the report on Energy Monitoring and Control Systems.

The composite total in energy reduction for building improvement projects is not a simple algebraic summation of individual project's energy savings. Due to synergistic effects, the composite total savings are approximately 85% of the simple sum. Consideration must be given to those synergistic effects when arriving at energy savings using different combinations of energy conservation projects.

The addition of simple temperature controls or the installation of a basewide EMCS essentially accounts for the same block of energy to be saved. One or the other must be chosen, and thus the energy savings can only be taken credit for one time. Although the initial cost is greater to install the EMCS, it does have a decided advantage over the simpler temperature controls arrangement due to its inherent ability to monitor and report out of state operating conditions. This discourages tampering by personnel and ultimately guarantees energy savings, provided the system is properly installed and maintained.

ECI PROJECT SUMMARY  
AMMINGTON ARMY DEPOT

| PROJECT TITLE                                   | PROJECT NUMBER | COST \$1000 | ENERGY SAVED MEGA BTU | \$/C   | E/C     | YEARS |
|---|----------------|-------------|-----------------------|--------|---------|-------|
|   |                | MSEC.       | OIL                   | COAL   |         |       |
| Temperature Controls -<br>S1 Buildings          | H-204          | 325.9       | 8000.1                | 3790.2 | 15276.1 | 5.34  |
| Upgrade District Steam<br>Insulation - East End | A-10           | 209.0       | -                     | -      | 11600   | 1.1   |
| Slight G1 Buildings                             | H-206          | 2079.2      | 7726.1                | 6      | -       | 2.9   |
| Recreational Windows<br>S1 Buildings            | H-201          | 374.1       | 4652.1                | 2617.7 | 60008.6 | 3.65  |
| Ameside EACCS -<br>S1 Buildings                 | H-205          | 1185.1      | 8000.1                | 3790.2 | 15276.1 | 1.20  |
| Total (2) Regenerative<br>Dynamometers          | A-3            | 851.1       | 11207                 | -      | -       | 1.01  |
|   |                |             |                       |        |         | 16.5  |
|   |                |             |                       |        |         | 10.7  |

TABLE I

A detailed study of the utilization of biomass material from the 14,000 acre Anniston Site as an energy source was conducted. This study indicated that it would take 20 to 25 years to develop woodlands capable of maintaining a reasonably uniform level of biomass material. However, there is opposition to increasing the amount of woodlands at ANAD for security reasons which prevents production of enough wood capable of generating the steam required by this facility.

At present, wood biomass would be a more expensive fuel than coal or oil at Anniston Army Depot. Due to the high moisture content of wood and handling expenses, the cost of burning wood grown on site would be about 1.7 times that of coal per BTU equivalent.

However, since there already exists a Forestry Program which involves the regular removal of timber, any wood which is not of sawtimber quality may be utilized in the following ways:

- used as a fuel at ANAD
- sold to pulp mills
- separated, using the low quality wood for fuel at Anniston and selling the high quality wood to pulp mills.

A complete analysis on the burning of wood materials is presented in the Biomass Survey section of the report.

An analysis was performed for the application of central boiler plants as a method of meeting the projected growth in steam demand as established in the ANAD Master Plan. It was determined that under present levels of nuclear steam demand, the installation of

cogeneration equipment was not economical, making a life cycle cost analysis (LCC) of this alternative a meaningless calculation. The final recommendations suggest the installation of new coal fired steam generators at a location in the east end of the depot. We recommend the installation of (3) - 30,000 lbs./hr. boilers, one at a time, at convenient intervals based on anticipated steam demand increases from the present time through the year 1988. Details of the study are presented in the section on Central Boiler Plants.

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APPENDIX A  
POTENTIAL CONSERVATION MEASURES

TABLE A-1  
POTENTIAL CONSERVATION MEASURES REQUIRING CAPITAL INVESTMENT

| Project Studied   | Comments  |
|---|---|
| 1. Insulate walls of chemical cleaning tanks  | Good Project  |
| 2. Install retractable covers on chemical cleaning tanks  | Good Project  |
| 3. Install boiler economizers, oxygen trim controls, blowdown heat reclaim devices, etc.                | Viable for process loads; short heating season does not justify capital cost of retrofit                      |
| 4. Reset outside air dampers to minimum requirements of ASHRAE 62-73                                    | Good project; very limited application  |
| 5. Add floor, ceiling, and wall insulation  | This is a viable project for specific buildings only  |
| 6. Install storm windows  | Limited applications to non-industrial structures   |
| 7. Install solar shading devices:<br>- Solar window film<br>- Solar screens<br>- Overhangs<br>- Awnings | Solar energy currently provides assistance to building heating in some buildings with significant window area |
| 8. Weatherstrip doors   | Limited applications to non-industrial structures   |
| 9. Install vestibules around high traffic doors   | This project has limited application due to size of vehicles  |
| 10. Install setback temperature controls  | Good Project  |
| 11. Install regenerative engine   | Good Project  |
| 12. Reduce glass area by adding insulated panels  | Good Project  |

**POTENTIAL CONSERVATION MEASURES REQUIRING CAPITAL INVESTMENT**  
 (Continued)

| <u>Project Studied</u>  | <u>Comments</u>   |
|---|---|
| 13. Install flue dampers, smaller jets, dual burners, electronic ignition, etc. in small furnaces   | Short heating season does not justify capital cost of retrofit  |
| 14. Replace manual control valves or install temperature regulators in cast-iron radiators  | Not cost effective where central controls are recommended   |
| 15. Replace existing coal boilers with gas/oil conversion kits with modern packaged boilers   | This project does not meet the criteria   |
| 16. Replace incandescent lighting with higher efficiency lighting systems   | Good Project  |
| 17. Install photocell lighting controls   | This project has limited application  |
| 18. Replace existing motors with motors of the high efficiency type   | There is an engineering disagreement concerning this project particularly where large older motors are involved |
| 19. Reduce lighting levels to minimum standards   | Limited application - many facilities are below minimum standards   |
| 20. Install water closet tank inserts, flow reducing shower heads, or other water conserving devices to reduce pumping energy consumption | Limited Application   |
| 21. Insulate existing steam lines   | Good Project  |
| 22. Revise existing chilled water/hot water pumping schemes to more efficient methods   | N/A   |
| 23. Deactivate individual room thermostats in barracks and install temperature reset controls on chilled and hot water                    | N/A   |
| 24. Shut down steam plants in the summer and set up propane steam needs with electric boilers   | N/A   |

**POTENTIAL CONSERVATION MEASURES REQUIRING CAPITAL INVESTMENT**  
 (Continued)

| Project Studied   | Comments   |
|---|--|
| 25. Install infrared heating in warehouses, hangars, and shops                                | This project does not meet the criteria due to short heating duty cycles |
| 26. Install economizer systems for "free cooling" in intermediate seasons                     | This project does not meet the criteria in retrofit applications         |
| 27. Modify multizone systems to include hot/cold deck reset                                   | N/A  |
| 28. Modify cooling tower systems to cycle fan with load and/or install bypass valving         | N/A  |
| 29. Install load-shedding system to minimize demand charges                                   | N/A  |
| 30. Correct power factor  | This project does not meet the criteria                                  |
| 31. Install chilled and hot water reset controls  | N/A  |
| 32. Install FM radio control system   | N/A  |
| 33. Replace existing windows with insulating panels   | Very limited application   |
| 34. Insulate temporary buildings  | N/A  |
| 35. Upgrade electrical distribution voltage   | N/A  |
| 36. Install total or selective energy plants  | This project does not meet the criteria                                  |
| 37. Install energy monitoring and control system (EMCS)                                       | Good Project   |
| 38. Install heat reclaim devices on air-cooled condensers                                     | Limited Application  |
| 39. Replace remotely located absorption chillers with more efficient electric-driven chillers | N/A  |
| 40. Install solid waste-burning boilers   | This project does not meet the criteria                                  |

POTENTIAL CONSERVATION MEASURES REQUIRING CAPITAL INVESTMENT  
(Continued)

| Project Studied  | Comments  |
|--|---|
| 41. Install trailer enclosing devices at loading docks                                       | This project has limited additional application |
| 42. Install solar energy systems where feasible  | This project does not meet the criteria         |
| 43. Install air-to-air heat reclaim devices in high exhaust areas, such as messhall kitchens | This project does not meet the criteria         |

TABLE A-2  
**POTENTIAL CONSERVATION MEASURES REQUIRING POLICY CHANGES  
 AT INSTALLATION LEVEL**

| Project Studied   | Comments  |
|---|---|
| 1. Replace domestic water heaters with higher efficiency models as replacement is required. | Good Project  |
| 2. Shut down steam boilers and branch lines in number                                       | Currently Practiced   |
| 3. Reduce domestic hot water temperatures from 140°F to 110-120°F                           | Good Project  |
| 4. Replace electric motors with motors of the high efficiency type on replacement basis     | Good project, limited application due to motor frame sizes of older equipment |
| 5. Use task lighting  | • Currently Practiced   |
| 6. Install temporary 4-mil plastic storm windows  | Good Project  |
| 7. Shut down HVAC and DHW systems in unoccupied buildings                                   | Currently Practiced   |
| 8. Calk cracks on self-help basis   | Good Project  |
| 9. Install high-efficiency transformers on replacement basis                                | Good project - recommend replacement of all oversized transformers            |
| 10. Enforce indoor space temperature regulations  | Good Project  |
| 11. Repair steam and condensate leaks   | Good Project  |
| 12. Repair air leakage in ducts   | N/A   |
| 13. Turn pilot lights for heating equipment off for the summer                              | Good project  |
| 14. Replace air-conditioning units with high efficiency models as replacement is required   | Good project  |

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APPENDIX 3  
BUILDING DATA

INDEX

APPENDIX B

PAGE NO.

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| TABLE 3 | Air Change Rates Used for Infiltration                               | ES-27          |
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| TABLE 6 | Tabulation of Energy Requirements By Building Number and Area        | ES-43 to ES-52 |

TABLE 1

| Prototype/Computer Simulated |              |                     |  |
|------------------------------|--------------|---------------------|--|
| Category Code                | AD Bldg. No. | Function            | Similar Buildings  |
| A-1-2                        | 7            | Headquarters        | None   |
| A-1-2                        | 93           | Security            | None   |
| A-1-2<br>W-1-2               | 162          | Office<br>Warehouse | None   |
| A-1-4                        | 1            | Office              | 2, 73, 220, 221, 3-13, 3-18, 3-47,<br>3-48, 3-49, 3-574  |
| A-1-0                        | 103          | General Purpose     | 106, 363 (Air Condition area only)   |
| A-1-0                        | 140          | Administration      | 100, 141, 302  |
| M-1-3                        | 901          | Tank Repair Shop    | None   |
| M-1-8                        | 21           | Shop                | 3, 4, 5, 8, 9, 10, 13, 22, 27, 38<br>46, 53  |
| M-2-8                        | 94           | Shipping            | 38, 59, 68, 87, 88, 171, 172, 320,<br>381, 600, 632, 634, 638, 669, 670,<br>673, 678, 676, 677, 680, 688, 8-64 |
| M-1-0                        | 129          | Small Arms Shop     | 104, 111-113; 127, 128, 130  |
| M-1-0                        | 143          | Tank Repair Shop    | 107, 108, 117, 144, 146, 147, 402,<br>411, 431, 303, 3-142   |
| M-1-0                        | 400          | Tank Repair Shop    | None   |
| M-1-0                        | 409          | Vehicle Maint. Shop | 410, 433   |

TABLE 1LEGEND

| <u>Category</u> | <u>Code</u> | <u>Building Type</u>   | <u>VAV System</u>   |
|-----------------|-------------|------------------------|---|
|                 | 4-1-8       | Administration         | <ul style="list-style-type: none"> <li>- Permanent Air Condition - Oil-fired individual heating plant</li> </ul>            |
|                 | 4-1-9       | Office                 | <ul style="list-style-type: none"> <li>- Permanent Air Condition - Coal-fired individual heating plant</li> </ul>           |
|                 | 4-1-0       | Administration         | <ul style="list-style-type: none"> <li>- Permanent Air condition - Coal-fired central boiler plant</li> </ul>               |
|                 | 5-1-2       | Maintenance/Production | <ul style="list-style-type: none"> <li>- Permanent In-air condition - Oil-fired individual heating plant</li> </ul>         |
|                 | 5-1-7       | Maintenance/Production | <ul style="list-style-type: none"> <li>- Permanent In-air condition - Coal-fired individual heating plant</li> </ul>        |
| (C)             | 5-2-5       | Maintenance/Production | <ul style="list-style-type: none"> <li>- Permanent Partially air Condition - Coal-fired individual heating plant</li> </ul> |
|                 | 5-1-0       | Maintenance/Production | <ul style="list-style-type: none"> <li>- Permanent V-air condition - Coal-fired central boiler plant</li> </ul>             |
|                 | 5-1-8       | Storage                | <ul style="list-style-type: none"> <li>- Permanent V-air condition - Oil-fired individual heating plant</li> </ul>          |

TABLE 2  
TECHNICAL BUILDING ENERGY CONSUMPTION DATA  
AND

| Group<br>No. | Bldg.<br>No. | Building<br>Description | Annual Energy Scarspe<br>Consumption (Btu x 10 <sup>6</sup> ) |        |          | KWh<br>Year | KWh<br>Peak | Btu x 10 <sup>6</sup><br>Eq. Ft. |
|--------------|--------------|-------------------------|---|--------|----------|-------------|-------------|----------------------------------|
|              |              |                         | Fuel  | Gas    | Oil      |             |             |                                  |
| A-1-E        | 7            | Headquarters            | -   | 2066.0 | 9,910.4  | 11,985.4    | 206.4       | 1,931,224                        |
| A-1-E        | 51           | Recruit City            | -   | 548.3  | 7,146.0  | 7,695.1     | 262.9       | 663,374                          |
| A-1-E        | 362          | Office                  | -   | 8861.6 | 14,987.0 | 21,849.4    | 489.7       | 2,055,983                        |
| B-1-E        | 1            | Warehouse               | -   | 507.1  | -        | 1,625.1     | 2,132.2     | 41.4                             |
| A-1-N        | 1            | Office                  | -   | 507.1  | -        | 1,625.1     | 2,132.2     | 41.4                             |
| A-1-O        | 102          | General Purpose         | 688.9   | -      | -        | 11,515.4    | 12,196.3    | 268.6                            |
| A-1-O        | 140          | Administration          | 270.5   | -      | -        | 1,875.6     | 1,946.1     | 79.3                             |
| B-1-S        | 501          | Tank Repair Shop        | -   | 3124.3 | 2,730.3  | 5,866.0     | 101.7       | 595,586                          |
| C-1          | 21           | Shop                    | 896.1   | -      | 0,385.3  | 5,201.8     | 621.3       | 435,253                          |
| H-2-M        | 54           | Shipping                | 247.3   | -      | -        | 715.0       | 961.4       | 31.4                             |
| H-1-O        | 129          | Small Arms Shop         | 2132.5  | -      | 6,651.0  | 10,781.5    | 173.4       | 929,612                          |
| H-1-O        | 161          | Tank Repair Shop        | 3122.3  | -      | 3,398.7  | 6,520.9     | 118.7       | 562,147                          |
| H-1-O        | 600          | Tank Repair Shop        | 7694.3  | -      | 13,813.4 | 20,987.7    | 496.5       | 1,783,767                        |
| H-1-O        | 489          | Vehicle Maint.          | 916.9   | -      | 2,454.3  | 3,378.1     | 55.1        | 395,695                          |
|              |              | Shop                    |   |        |          |             |             | 0.043                            |

TABLE 3  
ARMISTON AD  
AIR CHANGE RATES USED FOR INTEGRATION

| STRUCT. NO.     | AS IS | INSUL. ROOF | INSUL. WALLS | REDUCE GLASS |
|-----------------|-------|-------------|--------------|--------------|
| 1               | 3     | -           | -            | 2            |
| 7               | 2.5   | -           | -            | -            |
| 21              | 4     | 3.3         | 3.3          | -            |
| 53              | 2     | -           | -            | -            |
| 84              | 4     | -           | 3.3          | -            |
| 106             | 4     | -           | 3.3          | -            |
| 109             | 1.5   | -           | 3.3          | -            |
| 129             | 2.5   | 2.5         | 2.5          | -            |
| 140             | 2.5   | -           | -            | -            |
| 143             | 2.5   | 4.3         | 6.3          | -            |
| 362 (Office)    | 3     | -           | -            | -            |
| 362 (Warehouse) | 5     | 4.3         | 4.3          | -            |
| 400             | 7     | 6.3         | 6.3          | -            |
| 409             | 5     | -           | -            | -            |
| 501             | 2.5   | -           | -            | -            |

**TABLE 1**  
**ABD**  
**EMULATION - MONTHLY THERMAL COMPUTER ANALYSIS OUTPUT (MBTU)**  
**AS IN CONDITION**

| Bldg. No.<br>Bldg. End   | J       | M       | A       | M     | J | J | A | S | O     | N       | D       | Total    |
|--------------------------|---------|---------|---------|-------|---|---|---|---|-------|---------|---------|----------|
| 104                      | 218.1   | 217.2   | 265.4   | 5.5   | 6 | 6 | 6 | 6 | 11.2  | 33.5    | 127.6   | 718.5    |
| 105                      | 165.5   | 177.4   | 124.5   | 19.1  | 2 | 2 | 2 | 2 | 21.5  | 61.9    | 116.6   | 680.9    |
| 129                      | 597.7   | 597.4   | 453.1   | 15.0  | 6 | 6 | 6 | 6 | 36.7  | 91.6    | 149.0   | 2,132.5  |
| 140                      | 70.4    | 67.1    | 57.7    | 5.5   | 5 | 5 | 5 | 5 | 7.0   | 16.8    | 46.0    | 270.5    |
| 143                      | 837.9   | 812.2   | 613.1   | 29.2  | 0 | 0 | 0 | 0 | 70.6  | 162.0   | 589.7   | 3,122.3  |
| 400                      | 2,124.6 | 2,068.3 | 1,564.5 | 62.4  | 0 | 0 | 0 | 0 | 152.9 | 361.1   | 1,380.5 | 7,694.1  |
| 409                      | 261.7   | 254.8   | 195.5   | 2.4   | 0 | 0 | 0 | 0 | 8.9   | 29.7    | 161.8   | 924.8    |
| Other Bldg.<br>End Bldg. |         |         |         |       |   |   |   |   |       |         |         |          |
| 00.106.107.108.          | 6,918.3 | 4,867.0 | 3,715.3 | 159.1 |   |   |   |   | 337.9 | 853.7   | 3,148.5 | 17,990.6 |
| 11-115.117.127.          |         |         |         |       |   |   |   |   |       |         |         |          |
| 20.130.141.144.          |         |         |         |       |   |   |   |   |       |         |         |          |
| 06.147.402.410.          |         |         |         |       |   |   |   |   |       |         |         |          |
| 11.421.433.502.          |         |         |         |       |   |   |   |   |       |         |         |          |
| .03.5-142                |         |         |         |       |   |   |   |   |       |         |         |          |
| TOTAL MBTU               | 9,218.6 | 9,040.1 | 6,999.1 | 297.9 | 0 | 0 | 0 | 0 | 648.7 | 1,600.3 | 5,889.7 | 13,594.4 |
| oller/Bldg. Err.         | 65      | 60      | 55      | 50    | - | - | - | - | 50    | 60      | 65      | Avg-60.6 |
| RTU & Boiler             | 14,163  | 15,067  | 12,544  | 596   | 0 | 0 | 0 | 0 | 1,297 | 2,667   | 9,061   | 55,415   |
| % Dev.                   | -19     | -10     | +274    | -41   | 0 | 0 | 0 | 0 | -29   | -22     | -17     | 13       |
| Boiler MBTU              | 17,411  | 16,689  | 4,568   | 1,010 | 0 | 0 | 0 | 0 | 1,632 | 3,435   | 7,734   | 52,669   |

AVG. 6 YEAR AVERAGE - RECORDED DATA (FROM EXHIBIT 1)

TABLE 5









WES200455: a indicates location for 1992 sites and is not included in Project N-245.





ଅନୁଷ୍ଠାନିକ ପରିମାଣ ଏବଂ ଗ୍ରହଣ - ଶ୍ରୀ କୃତ୍ତବ୍ୟ

四庫全書

ପ୍ରକାଶକ ପତ୍ର

1

प्राणी उत्तम - विनाशक विद्युति विद्युति

गुरु गुरु गुरु

卷之三

प्राचीन इतिहास का अध्ययन सर्वोच्च - शिक्षण संस्कृति

卷之二十一

POLÍTICA EPIFICIAIS: 699



| BOILER EFFICIENCY - 60%                              |                                   |                             |                              |                             |                             |                             |                             |                             |
|--|-----------------------------------|-----------------------------|------------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| WATER TEMPERATURE<br>BOILER FEED WATER<br>WATER COOL |                                   |                             | BOILER EFFICIENCY IN PERCENT |                             |                             | TEMPERATURE CONTROL         |                             |                             |
| SOLID INSULATION                                     |                                   |                             | WATER INSULATION             |                             |                             | WATER BYPS                  |                             |                             |
| SELOC.<br>WATER<br>LEVEL<br>INCHES                   | WATER<br>AREA<br>INCHES<br>SQUARE | WATER<br>TEMP.<br>DEG.<br>F | WATER<br>TEMP.<br>DEG.<br>F  | WATER<br>TEMP.<br>DEG.<br>F | WATER<br>TEMP.<br>DEG.<br>F | WATER<br>TEMP.<br>DEG.<br>F | WATER<br>TEMP.<br>DEG.<br>F | WATER<br>TEMP.<br>DEG.<br>F |
| -  | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 1  | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 2  | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 15   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 22.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 22.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 34.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 34.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 34.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 34.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 34.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 35.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 36.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 37.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 38.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 39.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 40.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 41.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 42.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 43.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 44.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 45.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 46.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 47.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 48.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 49.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 50.9   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.0   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.1   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.2   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.3   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.4   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.5   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.6   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.7   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.8   | -                                 | -                           | -                            | -                           | -                           | -                           | -                           | -                           |
| 51.9   | -                                 | -                           | -</td                        |                             |                             |                             |                             |                             |

## ADMINISTRATIVE REPORT - Searched Areas

(Reg. Coal)

BOILER EFFICIENCY: 60%

| WATER<br>TEMP.<br>DEG.<br>F.      | WATER<br>TEMP.<br>DEG.<br>C. | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>LEVEL<br>IN<br>TANK | WATER LEVEL                  |                              |                              |                              | WATER LEVEL                  |                              |                              |                              | WATER LEVEL                  |                              |                              |                              |
|-----------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
|                                   |                              |                              |                              | WATER<br>TEMP.<br>DEG.<br>F. | WATER<br>TEMP.<br>DEG.<br>C. | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>TEMP.<br>DEG.<br>F. | WATER<br>TEMP.<br>DEG.<br>C. | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>TEMP.<br>DEG.<br>F. | WATER<br>TEMP.<br>DEG.<br>C. | WATER<br>LEVEL<br>IN<br>TANK | WATER<br>LEVEL<br>IN<br>TANK |
| <b>TEMPERATURES SURVEYED 9/28</b> |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |                              |
| 24.152                            | 70.0                         | 24.1                         | 70.0                         | 15.71                        | 60.0                         | 12.1                         | -0.357                       | 575                          | 67.3                         | 25.2                         | 11525                        | 7434                         | 69.5                         | 32.2                         | -0.111                       |
| 24.153                            | 70.0                         | 24.1                         | 70.0                         | 60.0                         | 12.0                         | -0.238                       | 893                          | 117.0                        | 45.5                         | 11525                        | 12296                        | 118.0                        | 32.0                         | -0.116                       |                              |
| 24.154                            | 70.0                         | 24.1                         | 70.0                         | 32.0                         | 0.0                          | -0.236                       | 2738                         | 115.0                        | 115.0                        | 11525                        | 115632                       | 116.0                        | 32.0                         | -0.116                       |                              |
| 24.155                            | 70.0                         | 24.1                         | 70.0                         | 25.0                         | 1.1                          | -0.234                       | 268                          | 92.3                         | 16.3                         | 11514                        | 0713                         | 58.0                         | 16.2                         | -0.116                       |                              |
| 24.156                            | 70.0                         | 24.1                         | 70.0                         | 52.0                         | 12.2                         | -0.256                       | 279                          | 31.6                         | 32.2                         | 11525                        | 15226                        | 38.0                         | 19.0                         | -0.116                       |                              |
| 24.157                            | 70.0                         | 24.1                         | 70.0                         | 26.0                         | 5.5                          | -0.236                       | 379                          | 44.7                         | 12.4                         | 11530                        | 4966                         | 31.0                         | 19.0                         | -0.116                       |                              |
| 24.158                            | 70.0                         | 24.1                         | 70.0                         | 30.0                         | 5.5                          | -0.237                       | 132                          | 16.3                         | 9.6                          | 11531                        | 1660                         | 17.0                         | 9.0                          | -0.116                       |                              |
| 24.159                            | 70.0                         | 24.1                         | 70.0                         | 21.0                         | 5.5                          | -0.234                       | 631                          | 55.0                         | 26.7                         | 11514                        | 9295                         | 61.0                         | 13.2                         | -0.116                       |                              |
| 24.160                            | 70.0                         | 24.1                         | 70.0                         | 49.0                         | 10.0                         | -0.236                       | 639                          | 92.3                         | 37.0                         | 11511                        | 9178                         | 97.0                         | 27.0                         | -0.116                       |                              |
| 24.161                            | 70.0                         | 24.1                         | 70.0                         | 77.0                         | 20.0                         | -0.234                       | 1312                         | 131.2                        | 21.0                         | 11516                        | 16216                        | 155.0                        | 43.0                         | -0.116                       |                              |
| 24.162                            | 70.0                         | 24.1                         | 70.0                         | 52.0                         | 11.0                         | -0.236                       | 646                          | 59.5                         | 20.0                         | 11533                        | 13639                        | 817.0                        | 91.0                         | -0.116                       |                              |
| 24.163                            | 70.0                         | 24.1                         | 70.0                         | 53.0                         | 11.0                         | -0.236                       | 768                          | 90.0                         | 25.0                         | 11533                        | 16600                        | 106.0                        | 10.0                         | -0.116                       |                              |
| 24.164                            | 70.0                         | 24.1                         | 70.0                         | 41.0                         | 10.0                         | -0.236                       | 687                          | 156.0                        | 68.0                         | 11562                        | 11562                        | 121.0                        | 16.2                         | -0.116                       |                              |
| 24.165                            | 70.0                         | 24.1                         | 70.0                         | 13.0                         | 2.0                          | -0.235                       | 103                          | 23.0                         | 9.0                          | 11515                        | 2293                         | 26.0                         | 2.0                          | -0.116                       |                              |
| 24.166                            | 70.0                         | 24.1                         | 70.0                         | 26.0                         | 5.5                          | -0.235                       | 171                          | 28.1                         | 7.0                          | 11531                        | 2216                         | 21.0                         | 6.0                          | -0.116                       |                              |
| 24.167                            | 70.0                         | 24.1                         | 70.0                         | 53.0                         | 12.0                         | -0.237                       | 337                          | 42.1                         | 16.0                         | 11528                        | 4672                         | 69.0                         | 14.0                         | -0.116                       |                              |
| 24.168                            | 70.0                         | 24.1                         | 70.0                         | 43.0                         | 10.0                         | -0.236                       | 666                          | 66.0                         | 7.0                          | 11516                        | 766                          | 0.0                          | 2.0                          | -0.116                       |                              |
| 24.169                            | 70.0                         | 24.1                         | 70.0                         | 28.0                         | 6.0                          | -0.235                       | 92                           | 3.0                          | 1.0                          | 11507                        | 267                          | 5.0                          | 1.0                          | -0.116                       |                              |
| 24.170                            | 70.0                         | 24.1                         | 70.0                         | 76.0                         | 20.0                         | -0.236                       | 1012                         | 1203.0                       | 23.0                         | 11511                        | 12242                        | 1224.0                       | N/A                          | -0.116                       |                              |

Continued on Next Page

N/A

ANNUAL AREA REPORT - Restricted Areas Contaminated Areas

ARMED FORCES ARMY DEPOT - Restricted Area Contained Within Con-

ARMED FORCES ARMY DEPOT - Restricted Area Contained Within Con-

## ANNISTON ARMY AMMUNITION DEPOT - (EAST END)

|                |                  | BLDG. THERMAL ENERGY CONSUMED |       |       | BLDG. ELECTRICAL ENERGY CONSUMED |         |        |
|----------------|------------------|-------------------------------|-------|-------|----------------------------------|---------|--------|
|                |                  | NET/1000 KWHLY TOTAL          |       |       | NET/1000 KWHLY TOTAL             |         |        |
|                | BLDG.<br>SQ. FT. | 1                             | 2     | 3     | 4                                | 5       | 6      |
| 0              | 7,543            | 236.8                         | -     | 150.2 | 195.5                            | 1453.2  | -      |
|                |                  | .0311                         | -     | .0252 | .0269                            | .1925   | -      |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 6              | 35,227           | 770.5                         | 535.5 | 670.4 | 764.5                            | 3163.4  | 3161.4 |
|                |                  | .0221                         | .0152 | .0196 | .0269                            | .0898   | .0898  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 5              | 29,732           | 650.2                         | -     | -     | 327.1                            | 11515.4 | -      |
|                |                  | .0229                         | -     | -     | .0110                            | .3673   | -      |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 6              | 29,317           | 671.4                         | -     | -     | 322.5                            | 11354.5 | -      |
|                |                  | .0229                         | -     | -     | .0110                            | .3673   | -      |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 7              | 4,291            | 145.5                         | 99.2  | 122.3 | 147.2                            | 110.9   | 150.8  |
|                |                  | .0319                         | .0208 | .0265 | .0242                            | .0271   | .0270  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 8              | 10,232           | 620.9                         | 620.2 | 961.6 | 1037.0                           | 637.4   | 1110.6 |
|                |                  | .0319                         | .0208 | .0265 | .0343                            | .0277   | .0370  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 1              | 13,782           | 380.6                         | 209.3 | 276.1 | -                                | 275.6   | 1237.6 |
|                |                  | .0221                         | .0152 | .0196 | -                                | .0188   | .0898  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 7              | 34,053           | 752.5                         | 517.6 | 657.4 | -                                | 481.1   | 3650.6 |
|                |                  | .0221                         | .0152 | .0196 | -                                | .0269   | .0898  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 1              | 24,023           | 752.6                         | 517.6 | 657.4 | -                                | 481.1   | 3650.6 |
|                |                  | .0221                         | .0152 | .0196 | -                                | .0269   | .0898  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |
| 7              | 38,260           | 1066.5                        | 713.6 | 965.9 | -                                | 920.9   | 9029   |
|                |                  | .0221                         | .0152 | .0196 | -                                | .0269   | .0898  |
| 1. TOTALS/ [ ] |                  |                               |       |       |                                  |         |        |



## ARMED FORCES AMMUNITION DEPOT - (EAST END)

| SAC.         | SAC. #2. | BUDG. ACTUAL ENERGY CONSUMED |        |        |        |         | SLDG. ACTUAL ENERGY CONSUMED |         |         |         |         |
|--------------|----------|------------------------------|--------|--------|--------|---------|------------------------------|---------|---------|---------|---------|
|              |          | 1                            | 2      | 3      | 4      | 5       | 1                            | 2       | 3       | 4       | 5       |
| 16,620       | 262.4    | 553.7                        | 758.7  | 913.1  | 737.4  | 984.9   | 984.9                        | 984.9   | 984.9   | 984.9   | 984.9   |
| TOTALS / [ ] | .0139    | .0208                        | .0205  | .0163  | .0277  | .0370   | .0370                        | .0370   | .0370   | .0370   | .0370   |
| 14,919       | 476.9    | 291.3                        | 399.3  | 490.5  | 368.1  | 516.4   | 516.4                        | 516.4   | 516.4   | 516.4   | 516.4   |
| TOTALS / [ ] | .0139    | .0208                        | .0205  | .0163  | .0277  | .0370   | .0370                        | .0370   | .0370   | .0370   | .0370   |
| 255,667      | 7694.3   | 6063.2                       | 6804.2 | 7881.4 | 6302.4 | 13111.4 | 13111.4                      | 13111.4 | 13111.4 | 13111.4 | 13111.4 |
| TOTALS / [ ] | .0141    | .0216                        | .0205  | .0169  | .0279  | .0391   | .0391                        | .0391   | .0391   | .0391   | .0391   |
| 5,193        | 176.9    | 108.0                        | 149.0  | 172.1  | 163.8  | 192.1   | 192.1                        | 192.1   | 192.1   | 192.1   | 192.1   |
| TOTALS / [ ] | .0139    | .0208                        | .0205  | .0163  | .0277  | .0370   | .0370                        | .0370   | .0370   | .0370   | .0370   |
| 55,060       | 924.8    | -                            | -      | -      | 846.8  | 1454.3  | -                            | -       | -       | -       | 1454.3  |
| TOTALS / [ ] | .0169    | -                            | -      | -      | .0154  | .0264   | -                            | -       | -       | -       | .0264   |
| 27,588       | 463.5    | -                            | -      | -      | 924.9  | 728.3   | -                            | -       | -       | -       | 728.3   |
| TOTALS / [ ] | .0159    | -                            | -      | -      | .0154  | .0264   | -                            | -       | -       | -       | .0264   |
| 10,077       | 361.6    | 209.6                        | 287.2  | 345.6  | 279.1  | 372.0   | 372.0                        | 372.0   | 372.0   | 372.0   | 372.0   |
| TOTALS / [ ] | .0139    | .0208                        | .0205  | .0163  | .0277  | .0370   | .0370                        | .0370   | .0370   | .0370   | .0370   |
| 10,400       | 488.2    | 299.3                        | 410.4  | 493.9  | 398.9  | 532.8   | 532.8                        | 532.8   | 532.8   | 532.8   | 532.8   |
| TOTALS / [ ] | .0139    | .0208                        | .0205  | .0163  | .0277  | .0370   | .0370                        | .0370   | .0370   | .0370   | .0370   |
| 61,208       | 325.0    | -                            | -      | -      | 665.3  | 1146.5  | -                            | -       | -       | -       | 1140.5  |
| TOTALS / [ ] | .0169    | -                            | -      | -      | .0154  | .0266   | -                            | -       | -       | -       | .0266   |
| 61,606       | 3125.5   | -                            | -      | -      | 2402.6 | 2739.3  | -                            | -       | -       | -       | 2739.3  |
| TOTALS / [ ] | .0212    | -                            | -      | -      | .0407  | .0449   | -                            | -       | -       | -       | .0449   |

PRACTICAL NEW INVENTION GUIDE - 1951 EDITION

## ARMED FORCES AMMUNITION DEPOT - (WEST END)

BLDG. SQ. FT. BLDG. THERMAL ENERGY CONSUMED  
MTRS. YEARLY TOTAL

TAB.D. ELECTRICAL, ENERGY CONSUMED  
MTRS. YEARLY TOTAL (FESTU - KWH X 0.016)

|           |        | 1       | 2     | 3     | 4     | 5      | 1       | 2      | 3      | 4       | 5       |
|-----------|--------|---------|-------|-------|-------|--------|---------|--------|--------|---------|---------|
|           | 12,600 | 5,071   | -     | -     | 408.8 | 416.6  | 1,625.1 | -      | -      | 1,541.0 | 1,433.0 |
| TOTALS/() | -      | -       | -     | -     | .0324 | .0329  | .1289   | -      | -      | .1064   | .1137   |
|           | 10,526 | 4,213.5 | -     | -     | 361.4 | 346.6  | 1,359.1 | -      | -      | 1,121.0 | 1,197.2 |
| TOTALS/() | -      | -       | -     | -     | .0324 | .0329  | .1289   | -      | -      | .1064   | .1137   |
|           | 952    | 46.6    | 319.3 | -     | 36.0  | 37.5   | 37.4    | 228.2  | 228.1  | 229.1   | 229.1   |
| TOTALS/() | -      | -       | -     | -     | .0449 | .0439  | .2677   | .2677  | .2677  | .2677   | .2677   |
|           | 14,732 | 862.8   | 576.0 | 621.7 | 649.2 | 646.7  | 3943.0  | 3943.0 | 3943.0 | 3943.0  | 3943.0  |
| TOTALS/() | -      | -       | -     | -     | .0422 | .0449  | .2677   | .2677  | .2677  | .2677   | .2677   |
|           | 17,974 | 981.2   | 762.8 | 758.5 | 796.9 | 789.1  | 4811.6  | 4811.6 | 4811.6 | 4811.6  | 4811.6  |
| TOTALS/() | -      | -       | -     | -     | .0422 | .0449  | .2677   | .2677  | .2677  | .2677   | .2677   |
|           | 56,332 | 2066.0  | -     | -     | -     | 1501.7 | 9919.4  | -      | -      | -       | 8788.0  |
| TOTALS/() | -      | -       | -     | -     | -     | .0269  | .1026   | -      | -      | -       | .1618   |
|           | 1,892  | 103.5   | 74.0  | 79.8  | 83.1  | 83.1   | 506.5   | 506.5  | 506.5  | 506.5   | 506.5   |
| TOTALS/() | -      | -       | -     | -     | -     | .0449  | .2677   | .2677  | .2677  | .2677   | .2677   |
|           | 1,392  | 103.5   | 74.0  | 79.8  | 83.2  | 83.1   | 506.5   | 506.5  | 506.5  | 506.5   | 506.5   |
| TOTALS/() | -      | -       | -     | -     | -     | .0449  | .2677   | .2677  | .2677  | .2677   | .2677   |
|           | 6,440  | 152.3   | 251.0 | 271.0 | 283.4 | 282.7  | 1724.0  | 1724.0 | 1724.0 | 1724.0  | 1724.0  |
| TOTALS/() | -      | -       | -     | -     | -     | .0449  | .0419   | .2677  | .2677  | .2677   | .2677   |
|           | 1,708  | 93.0    | 66.5  | 73.7  | 74.0  | 74.6   | 455.1   | 455.1  | 455.1  | 455.1   | 455.1   |
| TOTALS/() | -      | -       | -     | -     | -     | .0449  | .0439   | .2677  | .2677  | .2677   | .2677   |

AQUARIUM AQUARIUM AQUARIUM AQUARIUM AQUARIUM - (WEST END)

| STATE.   | BUDG. FEDERAL ENERGY CONSUMED<br>BUDG. ELECTRICAL ENERGY CONSUMED<br>MARCH YEARLY TOTAL. (MAY = 100% OF JUNE) |
|----------|---|
| MISSOURI | 1,000,000   |

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16.364 896.1 661.0 : 691.3 : 721.2 720.0 : 4365.3 - 4365.3 : 4365.3 ; 4365.3

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40,367 2219.6 1506.2 1781.3 1780.9 1685.8 1695.3 1685.8 1685.8

**RESULTS** - .9597 - .9391 - .9623 ! - .9446 - .9816 - .9677 - .9677 - .9677 : - .26 -

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THE JOURNAL OF CLIMATE

60.567 2219.6 1585.2 1704.3 1704.3 10859.8 10859.8

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| <b>TOTALS /</b> | <b>-65.97</b> | <b>-63.91</b> | <b>-6.622</b> | <b>-64.49</b> | <b>-64.39</b> | <b>-26.77</b> | <b>-26.77</b> | <b>-26.77</b> |
|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|

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|               |               |                |                |                |                |            |            |               |               |
|---------------|---------------|----------------|----------------|----------------|----------------|------------|------------|---------------|---------------|
| <b>TOTALS</b> | <b>(\$11)</b> | <b>(\$161)</b> | <b>(\$137)</b> | <b>(\$150)</b> | <b>(\$162)</b> | <b>(-)</b> | <b>(-)</b> | <b>(-219)</b> | <b>(-223)</b> |
|---------------|---------------|----------------|----------------|----------------|----------------|------------|------------|---------------|---------------|

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| 6.367 | 2e-4 | 0 | - | - | 212.8 | 215.1 | 216.5 | - | - | 690.7 | 705. |
|-------|------|---|---|---|-------|-------|-------|---|---|-------|------|

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## ARMED FORCES AIR FORCE AMMUNITION DEPOT - (WEST END)

|              | BLDG.<br>SQ. FT. | BLDG. THERMAL ENERGY CONSUMED |         |          |          |          | BLDG. ELECTRICAL ENERGY CONSUMED |          |          |         |         |
|--------------|------------------|-------------------------------|---------|----------|----------|----------|----------------------------------|----------|----------|---------|---------|
|              |                  | 1                             | 2       | 3        | 4        | 5        | 1                                | 2        | 3        | 4       | 5       |
| 243,760      | 8861.6           | -                             | 7535.8  | 7654.1   | 14987.8  | -        | -                                | -        | -        | 14172.4 | 14151.2 |
| TOTALS / [ ] | .0366            | -                             | .0109   | .0322    | .0613    | -        | -                                | -        | -        | .0581   | .0589   |
| 13,860       | 293.1            | -                             | -       | -        | 4957.4   | -        | -                                | -        | -        | -       | -       |
| TOTALS / [ ] | .0229            | -                             | -       | -        | .3873    | -        | -                                | -        | -        | -       | -       |
| 4,500        | 180.9            | -                             | 105.8   | 149.1    | 580.1    | -        | -                                | -        | 470.8    | 511.7   | -       |
| TOTALS / [ ] | .0462            | -                             | .0324   | .0329    | .1263    | -        | -                                | -        | .1064    | .1137   | -       |
| 4,500        | 180.9            | -                             | 145.8   | 149.1    | 580.1    | -        | -                                | -        | 470.8    | 511.7   | -       |
| TOTALS / [ ] | .0462            | -                             | .0324   | .0329    | .1263    | -        | -                                | -        | .1064    | .1137   | -       |
| 15,422       | 429.0            | -                             | 499.7   | 507.4    | 1227.9   | -        | -                                | -        | 1640.1   | 1753.5  | -       |
| TOTALS / [ ] | .0462            | -                             | .0324   | .0329    | .1263    | -        | -                                | -        | .1064    | .1137   | -       |
| 2,860        | 112.6            | -                             | 90.7    | 92.1     | 360.9    | -        | -                                | -        | 227.9    | 310.4   | -       |
| TOTALS / [ ] | .0462            | -                             | .0324   | .0329    | .1263    | -        | -                                | -        | .1064    | .1137   | -       |
| 5,720        | 229.9            | -                             | 185.3   | 188.2    | 737.3    | -        | -                                | -        | 608.6    | 653.4   | -       |
| TOTALS / [ ] | .0462            | -                             | .0324   | .0329    | .1263    | -        | -                                | -        | .1064    | .1137   | -       |
| 4,519        | 101.6            | -                             | -       | 146.8    | 148.6    | 582.4    | -                                | -        | 400.7    | 513.7   | -       |
| TOTALS / [ ] | .0462            | -                             | -       | .0324    | .0329    | .1263    | -                                | -        | .1064    | .1137   | -       |
| TOTAL / [ ]  | .2264297         | 202,762                       | 202,762 | 512,773  | 614,187  | 526,907  | 292,769                          | 559,775  | 614,107  |         |         |
| TOTALS / [ ] | 26,446.2         | 7,922.8                       | 8,056.6 | 13,571.2 | 21,651.2 | 20,222.6 | 54,289.7                         | 91,080.1 | 91,605.1 |         |         |
| TOTALS / [ ] | 0.032            | 0.019                         | 0.0422  | 0.015    | 0.015    | 0.163    | 0.268                            | 0.268    | 0.150    | 0.152   |         |

## ARMED FORCES AIRPORTS AND DEPOTS - (RESTRICTED AREA)

| 1. BLDG.<br>SQ. FT. | BLDG. FLOOR<br>YEARLY TOTAL |   |       |       |       | BLDG. ELECTRICAL ENERGY CONSUMED<br>YEARLY TOTAL (BTU'S - KW x 0.0161) |   |        |        |        |
|---------------------|-----------------------------|---|-------|-------|-------|--|---|--------|--------|--------|
|                     | 1                           | 2 | 3     | 4     | 5     | 1  | 2 | 3      | 4      | 5      |
| 4. 7,496            | 367.5                       | - | 193.3 | 267.1 | 199.5 | 715.9  | - | 703.8  | 689.7  | 691.2  |
| TOTALS/11           | .0730                       | - | .0735 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 5. 12,398           | 428.9                       | - | 315.3 | 358.7 | 345.7 | 1261.3   | - | 1220.5 | 1195.0 | 1202.3 |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 6. 35,659           | 4176.7                      | - | 916.6 | 964.2 | 948.5 | 3485.6   | - | 3348.4 | 3280.6 | 3298.5 |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 7. 4,718            | 153.7                       | - | 121.7 | 130.2 | 125.5 | 450.6  | - | 443.0  | 434.1  | 436.4  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 8. 35,520           | 116.4                       | - | 92.6  | 97.4  | 93.8  | 336.9  | - | 331.3  | 324.6  | 326.3  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 9. 6,960            | 163.7                       | - | 128.0 | 136.9 | 131.9 | 475.7  | - | 463.7  | 456.3  | 458.6  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 10. 1,600           | 52.6                        | - | 62.3  | 46.2  | 42.6  | 152.8  | - | 150.2  | 147.2  | 149.0  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 11. 3,895           | 194.5                       | - | 152.1 | 162.7 | 156.8 | 562.0  | - | 551.3  | 542.1  | 545.1  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 12. 9,130           | 201.4                       | - | 225.7 | 232.1 | 243.0 | 872.3  | - | 857.7  | 840.3  | 844.9  |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |
| 13. 14,578          | 481.1                       | - | 376.2 | 402.4 | 387.8 | 1392.2   | - | 1368.9 | 1341.2 | 1348.5 |
| TOTALS/11           | .0730                       | - | .0258 | .0276 | .0266 | .0955  | - | .0919  | .0920  | .0925  |

— (ESTATE PLANNING AREA) —

FIG. 2. THE PEARL MUSSELS OF THE LAKE OF THE  
WOODS. (See Fig. 1 for locality.)

NETU WRAAT TUTAAL, SEERTU = KWH X 0.0161

| SD. F. NO. |        | SLAB NO. |   | MATERIALS CONSUMED |        | MATERIALS PURCHASED |        | MATERIALS PURCHASED (NET) = MAM X 0.01161 |                      |
|------------|--------|----------|---|--------------------|--------|---------------------|--------|---|----------------------|
| 1          |        | 2        |   | 3                  |        | 4                   |        | 5   |                      |
| 11.055     | 364.9  | -        | - | 258.6              | -      | 275.6               | 365.9  | 655.0                                     | -                    |
| TOTALS/()  | 0310   | -        | - | 265.3              | 305.2  | 294.2               | 1056.1 | -   | 1039.4 1017.4 1021.0 |
| TOTALS/()  | 0310   | -        | - | 0.0250             | 0.0276 | 0.0256              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 10.342 | 311.5    | - | 238.3              | 318.1  | 307.5               | 1106.2 | -   | 1085.7 1061.7 1064.5 |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 2.500  | 82.0     | - | 64.1               | 69.2   | 66.7                | 232.5  | -   | 235.5 230.7 232.0    |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 2.236  | 73.9     | - | 57.7               | 61.7   | 59.5                | 211.5  | -   | 210.0 205.7 206.0    |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 4.672  | 154.2    | - | 120.5              | 120.9  | 124.3               | 446.2  | -   | 438.7 429.8 432.2    |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 781    | 25.8     | - | 20.1               | 21.6   | 20.8                | 76.6   | -   | 71.3 71.9 72.2       |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 567    | 18.1     | - | 16.1               | 15.1   | 14.6                | 52.2   | -   | 51.6 50.3 50.6       |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 781    | 25.6     | - | 20.1               | 21.6   | 20.8                | 74.6   | -   | 73.3 71.9 72.2       |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |
| TOTALS/()  | 932    | 32.7     | - | 25.6               | 27.1   | 27.4                | 94.7   | -   | 93.1 91.1 91.6       |
| TOTALS/()  | 0310   | -        | - | 0.0258             | 0.0276 | 0.0266              | 0.0555 | -   | .0919 .0920 .0923    |

ESTATE PLANNING AND INVESTMENT - (ESTATE PLANNING)

**APPENDIX C**  
**LIST OF REPORTS**

LIST OF REPORTS

ENERGY USE SURVEY

Narrative - Volume I, Section 3

Supporting Data - Volume II & III

ENERGY MONITORING AND CONTROL SYSTEMS

Narrative - Volume I, Section 4

Supporting Data - Volume II

BIOMASS SURVEY

Narrative - Volume I, Section 5

Supporting Data - Volume III

CENTRAL BOILER PLANTS

Narrative - Volume I, Section 6

Supporting Data - Volume III

BASEWIDE ENERGY PLAN RECOMMENDATIONS

Narrative - Volume I, Section 7

SCIP PROJECT PROCEDURES

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