SPECIAL PUBLICATION ARCCB-SP-96020

INDEX TO BENET LABORATORIES TECHNICAL REPORTS - 1995

R. D. NEIFELD

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JULY 1996



US ARMY ARMAMENT RESEARCH, DEVELOPMENT AND ENGINEERING CENTER close combat armaments center benét laboratories watervliet, n.y. 12189-4050



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	CUMENTATION PA		Form Approved OMB No. 0704-0188
Public reporting burden for this collection of inform gathering and maintaining the data needed, and con collection of information, including suggestions for Dawn Michawa, Suite 1204, Arlington, VA 22202-430	ation is estimated to average 1 hour per r mpleting and reviewing the collection of in reducing this burden, to Washington Heat 2, and to the Office of Management and B	esponse, including the time for re iformation. Send comments regar dquarters Services, Directorate for Budget, Paperwork Reduction Proje	viewing instructions, searching existing data sources, ding this burden estimate or any other aspect of this information Operations and Reports, 1215 Jefferson ect (0704-0188), Washington, DC 20503.
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE July 1996	3. REPORT TYPE AND Final	D DATES COVERED
4. TITLE AND SUBTITLE INDEX TO BENET LABORATORIES TECHNICAL REPORTS - 1995			5. FUNDING NUMBERS N/A
5. AUTHOR(S) R.D. Neifeld			
7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-SP-96020
9. SPONSORING / MONITORING AGENO U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	CY NAME(S) AND ADDRESS(ES)	10. SPONSORING/MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES			
12a. DISTRIBUTION / AVAILABILITY ST Approved for public release; distribution			12b. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words) This is a compilation of technical repo	orts published by Benet Laborat	ories during 1995.	
14. SUBJECT TERMS Benet Laboratories, Technical Publica	ations, Bibliographies, Abstracts	, Document Control Data	15. NUMBER OF PAGES 64 16. PRICE CODE
			ICATION 20. LIMITATION OF ABSTRAC

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ARCCB-TR-95029	A302 173
ARCCB-TR-95030	A301 050
ARCCB-TR-95031	A302 276
ARCCB-TR-95032	B205 258L
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ARCCB-TR-95034	B206 811L
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ARCCB-TR-95040	A304 948
ARCCB-TR-95041	A305 399
ARCCB-TR-95042	A305 688
ARCCB-TR-95043	A306 485

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	January 1995	Final	5. FUNDING NUMBERS
. TITLE AND SUBTITLE A SIMPLE AND ACCURATE T CRACK GROWTH BEHAVIOR			AMCMS: 611.02.H611.1
. AUTHOR(S) D. Eric Leighton and Ronald T. A	Abbott	<u></u>	
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11. SUPPLEMENTARY NOTES			126 DISTRIBUTION CODE
2a. DISTRIBUTION AVAILABILITY STA	TEMENT		
Approved for public release; distr	ibution unlimited		
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I. AGENCY USE ONLY (Leave I		3. REPORT TYPE AND Final	
I. TITLE AND SUBTITLE FATIGUE LIFE AND FRACTU FOR THE M185/M284 BREEC	5. FUNDING NUMBERS AMCMS No. 6126.24.H180.0 PRON No. LT3A3FUS1ABJ		
. AUTHOR(S) .H. Underwood, E. Troiano, an	d A.A. Kapusta		
V. PERFORMING ORGANIZATION U.S. Army ARDEC Benet Laboratories, AMSTA-AH Watervliet, NY 12189-4050	N NAME(S) AND ADDRESS(ES) R-CCB-O		8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95002
SPONSORING / MONITORING J.S. Army ARDEC Close Combat Armaments Cente Vicatinny Arsenal, NJ 07806-500		S(ES)	10. SPONSORING / MONITORING AGENCY: REPORT NUMBER
1. SUPPLEMENTARY NOTES		I	,,,,,,, .
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1. AGENCY USE ONLY (Leave blank		3. REPORT TYPE AND	DATES COVERED
	January 1995	Final	5. FUNDING NUMBERS
TITLE AND SUBTILLE			AMCMS No. 6126.24.H180.0 PRON No. F14XCCF6M11A
6. AUTHOR(S) J.H. Underwood, D.E. Leighton, R.T	. Abbott, and E. Troiano		
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7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050			REPORT NUMBER ARCCB-TR-95003
9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS(ES	}	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
12a. DISTRIBUTION / AVAILABILITY S Distribution limited to Department of because of critical technology; Januar referred to Commander, U.S. Army Center, ATTN: Benet Laboratories,	of Defense and Department of Det ary 1995. Other requests for this Armament Research, Developmen	document must be nt, and Engineering	126. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 word) Fracture mechanics testing and analy property and inspection results from	s) ysis were performed for the long re the manufacturer of the tungsten e performed from each of the five nt Research. Development, and E	od penetrator of the 105-mi alloy penetrator were revi production lots for the pe ingineering Center's test re	m C76A1 kinetic energy round. Material ewed. Fracture toughness was measured netrator. Analysis of the manufacturer's soults failed to identify any defect in the round during firing tests.
A penetrator was fatigue tested so a this cracked penetrator was measure	as to produce a 1.6-mm deep crac ad to be about one-eighth of that of	k in the root of its rearmos of an uncracked penetrator.	st groove. The bend energy-to-failure of
Results of the tests and analyses inc that failed in firing tests. A recomm tungsten alloy penetrator.	licate that a crack of about the same nendation was given to use an edd	me size as that in the fatigu ly-current inspection metho	te test had been present in the penetrator of in future manufacturing of this type of
14. SUBJECT TERMS			15. NUMBER OF PAGES
Fracture Mechanics, Tungsten Allo Nondestructive Inspection, Fracture			13 16. PRICE CODE
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIF OF ABSTRACT UNCLASSIFIED	ՄԼ
NSN 7540-01-280-5500		23	Standard Form 298 (Rev. 2-8) Prescribed by 445 Std. 239-18

REPORT DO	Form Approved OMB No. 0704-0188		
Public reporting burden for this collection of inform gathering and maintaining the data needed, and con collection of information, including suggestions for i Davis hichwar, Suite 1264, Arlington, VA 22202430	npleting and reviewing the collection of reducing this burden, to Washington Hea	information – Send comments rec adquarters Services, Directorate	reviewing instructions searching existing data sources, garding this burden estimate or any other aspect of this (or information Operations and Reports, 1215 Jefferson roject (0724.0138) Washington, DC 20503.
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE January 1995		ND DATES COVERED
4. TITLE AND SUBTITLE CONTACTLESS CHARACTER USING LASER-INDUCED SUR VOLTAGE MEASUREMENTS 6. AUTHOR(S)	5. FUNDING NUMBERS AMCMS: 6126.24.H180.0 PRON: LT4B4FVQ1ABJ		
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7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benét Laboratories, AMSTA-AR- Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95004
 SPONSORING / MONITORING AGENC U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000 	r	;)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES Presented at the 1st Internationa Germany. Published in the Symp		ctor Processing and C	haracterization with Lasers, Stuttgard,
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(SPCV) measurements is presente light whose photon energy exceeds thus SPCV measurements do not re the SPCV is measured as a function spectrum is associated with the den with experimental results performe	d. SPCV measures the chan s the band gap energy of the s equire the fabrication of metal n of the energy of a sub-band sity of surface states. A quali- ed on gallium arsenide sample pletely contactless, and it ca	ge in the surface electri emiconductor sample. contacts. In photo-char gap monochromatic stea tative analysis of the pro is passivated with a thin an be used as an in-li	ices using surface photo-charge voltage ical charge induced by a chopped laser This charge is measured capacitatively, rge voltage spectroscopy measurements, ady-state illumination, and its derivative posed measurement is presented along zinc selenide film of variable thickness. ne nondestructive characterization of
14. SUBJECT TERMS Semiconductor Characterization, S Zinc Selenide, Spectroscopy	Surface Charge, Surface State	 es,	15. NUMBER OF PAGES 10 16. PRICE CODE
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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE January 1995	3. REPORT TYPE A Final	AND DATES COVERED
4. TITLE AND SUBTITLE ADAPTIVE FINITE ELEMENT MESH REFINEMENT	5. FUNDING NUMBERS AMCMS: 612624H191.0		
6. AUTHOR(S) J.M. Coyle and J.E. Flaherty	<u></u>		
7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benét Laboratories, AMSTA-AR Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95005
 SPONSORING / MONITORING AGENO U.S. Army ARDEC Close Combat Armaments Cente Picatinny Arsenal, NJ 07806-5000 	r	ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES	ATEMENT		120 DISTRIELTICH CUEL
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14. SUBJECT TERMS Parabolic Differential Equations Superconvergence, Error Estima	, Adaptive Finite Elements, tion, Error Decomposition,	Finite Differences, Mesh Refinement	15. NUMBER OF PAGES 19 16. PRICE CODE
17. SECURITY CLASSIFICATION 18 OF REPORT UNCLASSIFIED	SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLAS OF ABSTRACT UNCLASSIFIE	
NSN 7540-01-280-5500		25	Standard Form 1950 Rev 2-89 Prescibed by ANS Stoll 200 re 295/00

REPORT DO	Form Approved OME No: 0704-0183		
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6. AUTHOR(S) J.M. Coyle and J.E. Flaherty			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050	PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95006		
 SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Cem Picatinny Arsenal, NJ 07806-500 	ter	5} 10.	SPONSORING / MONITORING AGENCY REPORT NUMBER
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14, SUBJECT TERMS Parabolic Differential Equation Linear Stability, Mesh Moveme	s, Adaptive Finite Elements, E nt	quidistribution,	15. NUMBER OF PAGES 31 16. PRICE CODE
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		Budget Paperwork Reduction Project	ing this burden escharted by the solution information Operations and Reports (1215 Jefferson et (0704-0185) Washington, Dro 20503	
. AGENCY USE ONLY (Leave blank)	2. REPORT DATE 3. REPORT TYPE AN		D DATES COVERED	
	February 1995	Final	5. FUNDING NUMBERS	
4. TITLE AND SUBTITLE FRACTURE TOUGHNESS ASSESSMENT OF PRESENT AND FUTURE PRESSURE VESSEL MATERIALS BASED ON CHARPY IMPACT ENERGY AND YIELD STRENGTH			AMCMS No. 6111.02.H611.1	
			PRON No. 1A11Z1CANMBJ	
AUTHOR(S)				
Edward Troiano and Gregory Vigilan	te			
PERFORMING ORGANIZATION NAM	AE(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER	
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050			ARCCB-TR-95007	
. SPONSORING / MONITORING AGEN	CY NAME(S) AND ADDRESS(ES	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000				
12. DISTRIBUTION AVAILABILITY ST			126 DISTRIBUTION COL:	
Approved for public release; distribut	ion unlimited.			
13. ABSTRACT (Maximum 200 words) Several medium and high strength allo	bys, including AF1410, Inconel	718, PH 13-8 Mo stainless s	teel, and ASTM A723 high strength low	
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1. AGENCY USE ONLY (Leave bla		3. REPORT TYPE AND Final		
4. TITLE AND SUBTITLE RESIDUAL STRESS EFFECTS AT A NOTCH ROOT IN A723 STEEL TO EXTEND FATIGUE LIFE			5. FUNDING NUMBERS AMCMS: 6111.02.H611.1	
6. AUTHOR(5) J.H. Underwood				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benét Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95008	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000			10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES Published in <i>Experimental Me</i>	chanics, March 1995.	<u> </u>		
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treatments and resulting residu different depths and surface v notch root surface value of co both the deepest and the high life agreed well with measure growth properties of the mat magnitude of the residual stre life plot, where the ΔK is for a relationship between ΔK and the	rmed with notched bend specin ual stress: shot peening, hole swag values of residual stress near the compressive residual stress. The l hest surface value residual stress ements. The calculations account erial; the shallow surface-crack ss distribution. A consistent desc shallow crack near the notch roof fatigue life agreed well with the r	ing, and tensile overload. T notch root and different fa highest life was measured f distribution. Fracture me need for the following factor configuration; the applied cription of fatigue life was co to and in the region of comp esults from both the untrea	with three types of residual stress he three treatments produced widely atigue lives depending mainly on the rom overload specimens, which had chanics-based calculations of fatigue ors that affect fatigue life: the crack loading; and the depth and surface obtained from a ΔK versus calculated pressive residual stress. A power-law ted notches and those with the three confidence for tests under generally	
14. SUBJECT TERMS Residual Stress, Fatigue Life, Crack Growth, Notch Root, Shot Peening, Tensile Overload, Hole Swaging, Notched Bend Specimens		ot Peening,	15. NUMBER OF PAGES 16 16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFIC OF ABSTRACT	ATION 20. LIMITATION OF ABSTRACT	
UNCLASSIFIED NSN 7540-01-280-5500	UNCLASSIFIED	UNCLASSIFIED	TIT. Standard Form (296)(Fey, 2469) Elegated bill 413 Stal (296)(F	

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TITLE AND SUBTITLE WINDABLE QUASI-GEODESIC PATHS ON SURFACES OF REVOLUTION		5. FUNDING NUMBERS AMCMS: 6111.02.H611.100	
AUTHOR(S) Royce W. Soanes			
Royce W. Solaites			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benét Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050		8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95009	
SPONSORING / MONITORING AGENC U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000		ES)	10. SPONSORING MONITORING AGENCY REPORT NUMBER
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1. AGENCY USE ONLY (Leave blan			ND DATES COVERED
I. TITLE AND SUBTITLE CHEMICAL ANALYSIS OF GUN STEEL BY OPTIMIZED EMISSION SPECTROSCOPY		5. FUNDING NUMBERS AMCMS No. 6126.24.H180	
5. AUTHOR(S) Samuel Sopok and Jay Hoessle			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050		8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95010	
9. SPONSORING/MONITORING AG U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	ENCY NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES 12a. DISTRIBUTION AVAILABILITY Distribution limited to Department February 1995. Other requests for	of Defense only because of critics		12b. DISTRIBUTION CODE
U.S. Army Armament Research, De Benet Laboratories, AMSTA-AR-C	evelopment, and Engineering Cent	ter, ATTN:	
the Angstrom model V-70 direct rea- of gun steel materials. The develops and system operating condition com- chemically characterize critical serv- respective required concentration ra- precisions at 95 percent confidence = 2.00 to 3.50, ± 0.05 , ± 0.10 ; phosp 1.20, ± 0.05 , ± 0.10 ; manganese = 0.5 ± 0.030 ; silicon = 0.15 to 0.30, ± 0.0 Optimized emission spectroscopy in	lequately screen noncritical standar ading vacuum emission spectromet nent of multi-element calibration d rections are discussed. Unfortunat vice intensive metals, such as gun anges (weight percent), required p (weight percent, optimized emiss horus = 0.001 to 0.014, ± 0.001 , ± 1000 , ± 0.001 , to 0.014, ± 0.001 , ± 0.001 , to 0.001 horus = 0.001 to 0.014, ± 0.001 , ± 1000 , ± 0.001 to 0.00 horus = 0.001 to 0.014, ± 0.001 to 0.00 hadequately characterizes gun steps sma and carbon/sulfur analyzer be	ter was used to perform c lata, spectral interference of tely, even fully optimized a steel, with their narrow precisions at 95 percent of tion spectroscopy) are: c 0.002; sulfur = 0.001 to 0 um = 0.40 to 0.60, ± 0.02 , 0.001 , ± 0.001 , ± 0.005 ; and el to the desired level of	wide constituent tolerances. For this work, omputer-assisted chemical characterization corrections, matrix interference corrections, emission spectroscopy completely fails to constituent tolerances. For gun steel, the confidence (weight percent), and achieved arbon = 0.30 to 0.38, ± 0.01 , ± 0.02 ; nickel 0.012, ± 0.001 , ± 0.003 ; chromium = 0.80 to ± 0.03 ; vanadium = 0.080 to 0.120, ± 0.005 , titanium = 0.001 to 0.015, ± 0.001 , ± 0.017 . precision. Although they are more time- ongly recommended for all future gun steel
14. SUBJECT TERMS Chemical Analysis, Gun Steel, Opti	mized Emission Spectroscopy		15. NUMBER OF PAGES 28 16. PRICE CODE
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	February 1995	Final		
TITLE AND SUBTITLE RIFLING TWIST DESIGN			5. FUNDING NUMBERS	
AUTHOR(S) Royce W. Soanes		<u></u>		
			8. PERFORMING ORGA	ANIZATION
. PERFORMING ORGANIZATION NAMI U.S. Army ARDEC Benét Laboratories, AMSTA-AR- Watervliet, NY 12189-4050			REPORT NUMBER ARCCB-TR-95	
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1. AGENCY USE ONLY (Leave bla	ank) 2. REPORT DATE February 1995	3. REPORT TYPE AN Final	D DATES COVERED
4. TITLE AND SUBTITLE AMMUNITION TEMPERA INVESTIGATION FOR TH	TURE EMULATOR		5. FUNDING NUMBERS AMCMS: 6126.24.H180.0 PRON: 473GEV08471A
6. AUTHOR(S) Philip C. Wheeler			
7. PERFORMING ORGANIZATION	NAME(S) AND ADDRESS(ES)	···· · · · · · · · · · · · · · · · · ·	8. PERFORMING ORGANIZATION
U.S. Army ARDEC Benét Laboratories, AMSTA Watervliet, NY 12189-4050	-AR-CCB-O		REPORT NUMBER ARCCB-TR-95012
 SPONSORING / MONITORING AG U.S. Army ARDEC Close Combat Armaments C Picatinny Arsenal, NJ 07806- 		5)	10. SPONSORING, MONITORING AGENCY REPORT NUMBER
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the trajectory of the projectil increases projectile velocity, t deflections during firing are r is necessary to establish a mo- minimize muzzle deflection.	e propellant temperature of a role. As the propellant temperature hus affecting range, accuracy, and elated to projectile velocities, while ore accurate estimate of the prop	e varies, its burn rate als d penetrating capability is ich in turn relate to the p bellant temperature at th approach that can be use	ts the dynamics of a cannon and thus o varies. A faster burning propellant for kinetic energy projectiles. Muzzle propellant temperature. Therefore, it e time of ignition to account for and ed to develop an emulator design. An
14. SUBJECT TERMS Thermal Emulator, Temperat	ture Gage		15. NUMBER OF PAGES 11 16. PRICE CODE
17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFI OF ABSTRACT	CATION 20. LIMITATION OF ABSTRACT
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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE	3. REPORT TYPE AN	
	February 1995	Final	
4. TITLE AND SUBTITLE TRANSLAMINAR FRACTURE TOU FROM INTERLABORATORY TEST	GHNESS TEST METHODS A S OF CARBON/EPOXY LAM	ND RESULTS INATES	5. FUNDING NUMBERS AMCMS No. 6111.02.H611.1
6. AUTHOR(S) John H. Underwood, Mark T. Kortsch Natl. Engineering Lab), Harvey L. Eid	inoff (Northrup-Grumman Cor	p., Bethpage, NY),	
Dale A. Wilson (Tennessee Tech. U.). 7. PERFORMING ORGANIZATION NAM	and Noel Ashbaugh (U. of Da	vion)	8. PERFORMING ORGANIZATION
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB Watervliet, NY 12189-4050			REPORT NUMBER ARCCB-TR-95013
9. SPONSORING / MONITORING AGENO U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	Y NAME(S) AND ADDRESS(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES Presented at the 26th ASTM National Published in Proceedings of the Confe 12a. DISTRIBUTION AVAILABILITY ST. Approved for public release; distribution	ATEMENT	anics, Idaho Falls, ID, 27	29 June 1994.
test and analysis procedures. Notcher two carbon fiber/epoxy materials, a rel 2-mm and 4-mm; and three specimen specimen with arm height-to-specime specimen, including those for stress ir and for a/W in terms of V. Relationsl specimen were also derived. Damage was characterized in the test damage in the bend specimen. Two to the notch in predominantly 0° fiber K at maximum load, K _{max} , determined as a measure of fracture toughness. measurements of fracture toughness. toughness measurement, including the resistance to crack growth for quasi- 14. SUBJECT TERMS Fracture Toughness, Laminated Com	d specimens were tested on tw latively brittle T300 fiber/976 ep configurations, the standard than n width ratio of 1.9. Stress an itensity factor, K, and crack-mo- hips for the bending stresses that its, including that associated we types of notch-tip damage were layups, and that which occurs a d in a way that took account of For deviations from the lim This criterion also excluded test arm breakage and load-point dis sotropic layups and constant re- posites, Carbon/Epoxy, Notch-	to types of symmetrical la boxy and a tougher AS4 fi ee-point bend and compace d displacement expression buth opening displacement at control self-similar and ith arm breakage in the s e characterized using radii head of the notch in quasi the effective crack growt car P-V plot corresponding the with damage of the type mage noted in the tests. P sistance to crack growth for Fip Damage,	developing translaminar fracture toughness yups, quasi-isotropic [0/45/90] and [0/90]; ber/977-2 epoxy; two laminate thicknesses, ct configurations, and an extended compact is were obtained for the extended compact swere obtained for the extended compact , V, in terms of relative notch length, a/W, off-axis cracking for the extended compact tandard compact specimen and load-point ography, that which extends perpendicular -isotropic and 90° fiber layups. The applied h up to the maximum load point, was used ing to $\Delta a/W \leq 0.04$, K_{max} gave consistent to that violates the basic concept of fracture for predominantly 90° fiber layups.
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1. AGENCY USE ONLY (Leave blan	k) 2. REPORT DATE March 1995	3. REPORT TYPE AND Final	DATES COVERED
4. TITLE AND SUBTITLE PREDICTION OF SHOT IM ANALYSIS AND FIRING RE	PACT USING DYNAMIC ESULTS FOR THE M1A1 TA		5. FUNDING NUMBERS AMCMS: 6126.24.H180.0 PRON: M147A074M11A
6. AUTHOR(S) Ronald G. Gast			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050		8	ARCCB-TR-95014
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12a. DISTRIBUTION AVAILABILITY S Approved for public release; di		1	26. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words Conventional tank battles are a weaponry is extremely accurate, can should embrace the mindset zero' concept brought about by entire fleet using only a few ta determined. Therefore, for the that contributes to accuracy) mu a comprehensive study into the their effect upon dynamics at the in the early 1990s. Modelling is The overall goal is to provide an jump offset for a specific round randomly drawn from an expecte of output responses having its distribution. For the test data u	in important aspect of current we should not embrace the mir t that the best in tank gun accura- the downsizing trend in today' inks and gun tubes. The contri- concept to work, variability in ist be minimized or accounted for relationship among the charact e muzzle and shot accuracy. The performed using Benét's gun v ming point correction factors be and ballistic load. In this type of ed statistical distribution. There own characteristics. The likeli ised and the analysis run, fifty p prediction. Further study includ cross the full family of rounds for un Accuracy, Modal Analysis,	adset that the best in tank gu acy has been achieved. We a s army means that zeroing ribution of individual tubes tube-to-tube manufacture (or through the use of compu- eristics of gun tubes, project and the use of compu- eristics of gun tubes, project assed upon system dynamics of analysis, the values of unc- fore, a given distribution of hood that a response occu- percent of the samples show ing more rounds and gun tu- for the M1A1 tank.	ues. Even though our mechanized in accuracy has been achieved. We can and should do more! The 'fleet exercises will be conducted for the is to a tank's accuracy is no longer for more importantly the variability ter simulation. This report presents tiles, gun mounts, and ballistics and dynamic index tube test conducted and an empirically determined exit certain or unknown parameters are input values results in a distribution rs is cast in terms of a probability w promise for the use of this semi- bes is recommended with the intent 15. NUMBER OF PAGES 94 16. PRICE CODE
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1. AGENCY USE ONLY (Leave blank	2. REPORT DATE	3. REPORT TYPE AND L	DATES COVERED
4. TITLE AND SUBTITLE FATIGUE LIFE MEASUREMENTS OVERSTRAINED TUBES WITH F	March 1995 S AND ANALYSIS FOR EVACUATOR HOLES	Final 5.	FUNDING NUMBERS AMCMS No. 6111.02.H611.1
6. AUTHOR(S) John H. Underwood, Anthony P. Pa at Newcastle, UK), Daniel J. Corrig	rker (University of Northumbria an, and Michael J. Audino		
7. PERFORMING ORGANIZATION NA	ME(S) AND ADDRESS(ES)	8	PERFORMING ORGANIZATION REPORT NUMBER
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9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS(ES)	1	O. SPONSORING / MONITORING AGENCY, REPORT NUMBER
11. SUPPLEMENTARY NOTES To be presented at ASME Pressure To be published in Proceedings of	Vessels and Piping Conference, Hohe Conference.		
12a. DISTRIBUTION AVAILABILITY	STATEMENT	1	20. DISTRIBUTION COL:
Approved for public release; distrib	ution unlimited.		
fatigue failure occurred. The failur purpose of evacuating combustion a including 0, 30, 50, and 100 percent hole and the measured fatigue life. wall position and significantly incre Fracture mechanics and solid mech calculations gave a good description concentration of the hole, crack siz the grack surfaces. As with measure	r radius of 53, 60, and 78 mm wer e locations were along 2-mm holes gases from the cannon after firing. The amount of overstrain affected Increasing the amount of overstrain eased fatigue life. anics-based calculations of fatigue of the measured life, taking account te and shape, material fatigue crack red fatigue life, the calculated life y	cut through the cannon wal The cannons had various and both the initiation position moved the crack initiation f life were performed for con- t of tube configuration, appli- c rate behavior and yield st was significantly affected by	100 to 300 MPa internal pressure until 1 at a 30° angle to the tube axis, for the nounts of autofrettage by overstraining, of the fatigue crack along the evacuator from the tube inner radius toward a mid- mparison with the measured lives. The ied pressure, amount of overstrain, stress rength, and pressure in the hole and on the amount of autofrettage of the tube. had substantial effects on the calculated
14. SUBJECT TERMS Fatigue Life, Thick-Wall Cylinder,	Residual Stress, Pressure Vessel.	Stress Concentration	15. NUMBER OF PAGES
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17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFIC OF ABSTRACT UNCLASSIFIED	ATION 20. LIMITATION OF ABSTRAC
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1. AGENCY USE ONLY (Leave bla		3. REPORT TYPE AN Final	
4. TITLE AND SUBTITLE A MATHEMATICA FORM GEOMETRIC ALGEBRA I			5. FUNDING NUMBERS AMCMS: 6111.02.H611.1
5. AUTHOR(5) L.V. Meisel			
7. PERFORMING ORGANIZATION N U.S. Army ARDEC Benét Laboratories, AMSTA Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95016
 SPONSORING / MONITORING AG U.S. Army ARDEC Close Combat Armaments Co Picatinny Arsenal, NJ 07806-3 		;)	10. SPONSORING / MONITORIA 2 AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES Published in: American Journa	al of Physics		<u> </u> .
2a. DISTRIBUTION AVAILABILITY	STATEMENT		126. DISTRIBUTION CODE
Approved for public release;	distribution unlimited		
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A. SUBJECT TERMS Mathematica, Geometric Alge	ebra, Multivector Algebra		15. NUMBER OF PAGES 36 16. PRICE CODE
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4. TITLE AND SUBTITLE NEURAL NETWORKS IN SEIZURE	DIAGNOSIS		JNDING NUMBERS AMCMS No. 6111.02.H611.1 PRON No. 1A13Z1CANMBJ
5. AUTHOR(S) M.A. Johnson, G. Kendall, P.J. Cote,	and L.V. Meisel		
7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCH Watervliet, NY 12189-4050		R	ERFORMING ORGANIZATION EPORT NUMBER ARCCB-TR-95017
9. SPONSORING / MONITORING AGENO U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	TY NAME(S) AND ADDRESS(ES)) 10. <u>5</u>	PONSORING MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES Presented at Artificial Neural Network Published in Proceedings of ANNIE 12a. DISTRIBUTION AVAILABILITY ST. Approved for public release; distribut	94. ATEMENT		DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words) A monitor has been designed to detect technology was developed to detect th sensor data and activates a remote teth seizure activity, therefore, false alarm differentiating seizure activity from ca a feature set. Our results indicate this currently employed.	e minor, barely perceptible tren terless alarm when a seizure is o as do occur. Neural networks asual motion. The network uses	nors characteristic of partial seize letected. However, the sensor re have been studied as a means o s elements of the normalized pow	Ires. A microcontroller analyzes the sponse is similar for both casual and f analyzing the sensor response and wer spectrum of the response data as
14. SUBJECT TERMS Epilepsy, Neural Networks, Seizures,	Monitor, Status Epilepticus		15. NUMBER OF PAGES 11 16. PRICE CODE
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1. SUPPLEMENTARY NOTES Published in: Computers in Phys.	ics		
2a. DISTRIBUTION AVAILABILITY S	TATEMEN		126. DISTRIBUTION CODE
Approved for public release; dis	tribution unlimited		
modules by straightforward trans	ensor analysis, such as Christ cription of their defining equa	ations. The built-in fun	vature tensors, are coded as <i>Mathematica</i> actions can then be used to perform tensor lustrated by examples from Schwarzchild
4, SUBJECT TERMS Mathematica, Tensor Analysis			15. NUMBER OF PAGES 13 16. PRICE CODE
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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE March 1995	3. REPORT TYPE AN Final	D DATES COVER	ID
4. TITLE AND SUBTITLE AN EXPERIMENTAL INVEST PERFORMANCE OF GUN BC ON 155-MM SELF-PROPELLE	IGATION OF THE GASDY DRE EVACUATORS MOUN	NAMIC ITED	5. FUNDING NU Contract	IMBERS DAAA-C-1149
 AUTHOR(5) H.T. Nagamatsu, L.N. Myrabo, I C. Ekonomidis, M. Greenman, F 	D.G. Messitt, P. Yagle			
7. PERFORMING ORGANIZATION NAN Rensselaer Polytechnic Institute Troy, NY 12180-3590	IE(S) AND ADDRESS(ES)		8. PERFORMING REPORT NUI	S ORGANIZATION MBER
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11. SUPPLEMENTARY NOTES Charles A. Andrade: Benét Lab 12a. DISTRIBUTION / AVAILABILITY ST			12b. DISTRIBUT	NON COD
Approved for public release; dis	tribution unlimited			
13. ABSTRACT (Maximum 200 words) The charge and discharge cycle: Institute (RPI) High Pressure She pressure shock tube, a 65 percen- diaphragms are placed over the e is 91 psia, and the flow Mach nur to-bore pressure up to 2300. The restriction at the exit of the charal discharge ports varies from 0.51 across the evacuator ports, shock coefficient for the ejector ports model of the 155-mm gun bore with six staggered ejector ports is of approximately 20 percent in coefficients for the baseline and than 26 psig, and the coefficient	s of the 155-mm gun bore evolved to the scale model of the the sca	w Facilities. To test the acuator is installed on the acuator is installed on the ports. The pressure bet essure is varied to obtain a charge ports in the bant is approximately 0.40. /P. of 1570. During the s behind the waves are procuator pressure range PI Steady-State Flow Family figuration. The staggered a ratio over test pressure constant at approximately $(1, 1)^{10}$	the end of the sho ind the Mach 1.1 ratios of the init seline configurat The charge coor charge phase wi resent in the eva of 50 to 195 psi cility, and the pe d ejector configures from 1 to 84	arge phases in the high ock tube. Thin plastic 39 incident shock wave ial evacuator pressure- tion is 0.29. With no efficient for the angled th high pressure ratios cuator. The discharge ia. A 33 percent scale erformance of a model iration results in a gain psig. The discharge
14. SUBJECT TERMS 155-mm Self-Propelled Howitze	r, Gas Dynamics, Model Bor	e Evacuator Performanc	e,	NUMBER OF PAGES
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1. AGENCY USE ONLY (Leave b)		3. REPORT TYPE AND Final	
4. TITLE AND SUBTITLE INVESTIGATION INTO ANAL' FILAMENT WOUND COMPOS	YSIS AND DESIGN OF		FUNDING NUMBERS Contract No: DAAA-2192-C-0079
Technology), Preston Bates, Geor	a U.), Kurt Gramoll (Georgia Inst. gia Tech Research Inst.), David Ko d Stephen Hiamang (Clark Atlanta	okan	
7. PERFORMING ORGANIZATION Clark Atlanta University Atlanta, Georgia 30314	NAME(S) AND ADDRESS(ES)		PERFORMING ORGANIZATION REPORT NUMBER
9. SPONSORING / MONITORING A U.S. Army ARDEC Benet Laboratories, AMSTA-AR-	GENCY NAME(S) AND ADDRESS(E	5) 1	0. SPONSORING / MONITORING AGENCY REPORT NUMBER ARCCB-CR-95020
Watervliet, NY 12189-4050 1. SUPPLEMENTARY NOTES Kevin Miner - Benet Laboratories	Project Engineer		
2a. DISTRIBUTION / AVAILABILITY Distribution limited to Departmen March 1995. Other requests for t	A STATEMENT t of Defense only because of critica his document must be referred to C	al technology; commander,	26. DISTRIBUTION CODE
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Experimental and theoretical investigation of the second s	stigations into filament would comp sult of gun barrel manufacture and ant residual stress state will exist be cycle, large localized stresses can be ented. A simple technique for mea	field use is presented. Nume ecause of the filament winding generated which could cause suring the tension during filar e employed successfully in th	med. A technique for calculating the rical results were obtained for several g processing technique. Furthermore defects such as longitudinal wrinkles nent winding was developed and used a experiments. The use of such high
4. SUBJECT TERMS ilament Winding, Composites, G esidual Stress, Epoxy, Wrinkles	un Barrels, Elastic Strains,		15. NUMBER OF PAGES 44 16. PRICE CODE
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4. TITLE AND SUBTITLE FRACTURE MECHANICS CHARA FATIGUE LIFE ANALYSIS OF NO J _L FRACTURE TOUGHNESS TEST	CTERIZATION OF WELDS: DTCHES AT WELDS;	5	FUNDING NUMBERS AMCMS No. 6111.02.H611.1
6. AUTHOR(S) John H. Underwood			
7. PERFORMING ORGANIZATION NA	ME(S) AND ADDRESS(ES)	8	PERFORMING ORGANIZATION
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CC Watervliet, NY 12189-4050			REPORT NUMBER ARCCB-TR-95021
9. SPONSORING/MONITORING AGEI U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS(E	5) 1	0. SPONSORING / MONITORING AGENCY REPORT NUMBER
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13. ABSTRACT (Maximum 200 words)		
In this report two methods of fracture welds, and the other addressing the fracture. These fatigue and fracture : Army Armament Research, Develop investigations. A brief general sum structures. Specific fatigue crack init box beam of a cannon carriage.	e analysis of welds will be empl final fracture of the welded co methods will be described by re oment, and Engineering Center, mary will be given of fatigue iation tests and analysis methods Recent improvements and simp	mponent and the fracture tou ferring to recent work from th primarily fracture case study and fracture methods and con will be presented, using exam- ilifications in J-integral fractu	e life testing and analysis of notches at ighness tests used to characterize final e technical literature and from the U.S. and fracture test method development neepts that have application to welded ple results from a welded stainless steel ure toughness tests will be described, eld metals and heat treatments will also
14. SUBJECT TERMS Fracture Mechanics, Welds, Fatigue	Life, J-Integral Fracture Tough	ness, Notch Stresses	15. NUMBER OF PAGES 23 16. PRICE CODE
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6. AUTHOR(S) J.H. Underwood			
7. PERFORMING ORGANIZATION N U.S. Army ARDEC Benét Laboratories, AMSTA Watervliet, NY 12189-4050		. 8	PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95022
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 11. SUPPLEMENTARY NOTES Presented at the Australian Fr Published in the Conference F 12a. DISTRIBUTION : AVAILABILITY 	_		ember 1994. 25. DISTRIBUTION CODE
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	March 1995	Final	
N TITLE AND SUBTITLE NONDESTRUCTIVE EVALUA TANTALUM CARBIDE REFR		-	AMCMS: 6111.02.H611.1
. AUTHOR(S) S.L. Lee, W.J. Heffernan, J. Wal	den		
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U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-500	er	1	O. SPONSORING MONITORING AGENCY REPORT NUMBER
Published in the Conference Pro 2a DISTRIEUTION AVAILABILITY ST	ceedings.		erials, Oahu, Hawaii, 7-11 July 1993. 2b. DISTRIBUTION CODI
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3. ABSTRACT (Maximum 200 words) Desirable characteristics of refract hardness, electrical conductivity, and tantalum compounds, such a high pressure, high temperature, a were reactively sputtered-depose determined that body-centered-cc cubic (fcc) tantalum carbide was de carbide was deposited at the trans	tory coatings for future project good adhesion, thermal stability is tantalum nitride and tantalum and aggressive chemical environ ited from argon plasmas cont ubic (<i>bcc</i>) tantalum was deposite leposited at methane concentrat sitional 22 percent methane con-	y, and high plasma resista carbide are being conside ment of the bore. In this v aining methane. Nonde d at methane concentrations above 25 percent, and centration. Coating comp d temperature coefficient	nce properties. Sputtered tantalum red as future coatings to endure the work, tantalum and tantalum carbide estructive x-ray diffraction analysis ons below 20 percent, face-centered- l a mixture of tantalum and tantalum osition, crystalline structure, particle
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A. TITLE AND SUBTITLE MULTIFRACTAL ANALYSIS BADII-POLITI AND CORRE	S OF IMPRECISE DATA:	DACHES	5. FUNDING NUMBERS AMCMS: 6111.02.H611.1
i. AUTHOR(S) L.V. Meisel and M.A. Johnson			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95024
D. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Cen Picatinny Arsenal, NJ 07806-50	ter	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
1. SUPPLEMENTARY NOTES Submitted to: Physical Review I	2		L
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described and applied to maching good results for machine preci- algorithm did not yield satisfact	entations of the correlation in ne precision and imprecise mod sion data and for data with 1 ory results for data with 0.05 p ation of the Badii-Politi approa	lel multifractal data. The percent random errors. ercent or larger random	ti multifractal analysis algorithms are e correlation integral technique yields The standard numerical Badii-Politi errors. However, the present results sted by Kostelich and Swinney can be
14, SUBJECT TERMS Fractal, Multifractal, Correlatio	n Integral, Imprecise Data		15. NUMBER OF PAGES 17 16. PRICE CODE
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4. TITLE AND SUBTITLE EFFECTS OF ION IMPLANTATIO ELECTROPLATED CHROMIUM	April 1995	I Final	5. FUNDING NUMBERS AMCMS No. 6126.24.H180.0 PRON No. 470TEV64471A
6. AUTHOR(S) Kathryn E. Noll			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CC Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95025
9. SPONSORING / MONITORING AGEI U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
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contraction chromium were plated of	lantation on two kinds of electron nto samples of 4340 grade steel $x = 10^{15}$ to 3.1 x 10 ¹⁸ atoms/cm ² a	and subsequently implante nd the implantations were	en studied. Both hard chromium and ed with N_2^+ or Ar^+ at atom energies of e conducted at both room temperature ed to study the effects of ion implante
on the surface properties of the chro The greatest improvement in the properties improved with an increase in the coefficient of friction and a m with nitrogen at elevated temperatur at the same condition. The elevated temperature nitrogen implantations.	mium plating. coperties was observed for the ni ing nitrogen dose. For both kinds leasurable decrease in the wear ra e showed improved friction and w temperature implantations also ap the hardness was increased three contraction chromium. At the	trogen implantations. In of chromium, the nitroger te. At the intermediate do year properties compared to peared to decrease the hard times that of the unimpla- highest dose tested, the r	general, the hardness, wear, and frid n implantation resulted in a 50% reduc oses tested, some of the samples impla to the room temperature samples impla dness of the bulk chromium. For the r inted hard chromium and slightly less maximum nitrogen concentration rea
14. SUBJECT TERMS Ion Implantation, Chromium, Electr Nitrogen, Friction, Wear Properties			15. NUMBER OF PAGES 75 16. PRICE CODE
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4. TITLE AND SUBTITLE LOW CYCLE NOTCHED FATIGU PREDICTIONS OF A723 HIGH ST	E BEHAVIOR AND LIFE		5. FUNDING NUMBERS AMCMS No. 6126.24.H180.0 PRON No. 4A2B2FYE1ABJ
6. AUTHOR(S) E. Troiano, J.H. Underwood, D. Cra	yon, and R.T. Abbott		
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CC Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95026
9. SPONSORING / MONITORING AGEI U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS(ES	;)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
 11. SUPPLEMENTARY NOTES To be presented at 1995 ASME/JSM To be published in proceedings of the 12a. DISTRIBUTION AVAILABILITY S Approved for public release; distribution 	TATEMENT	Conference, 23-27 July 199	5, Honolulu, Hawaii. 125. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words)			
were tested in four-point bending, bo Neuber notch analysis (classic and c Comparison of measured and predict as much as 67 percent at large strains also underpredicts the measured fatig	oth with and without notches, and elastic/plastic remote applied lost ted lives indicates that the elastic s, and becomes a better predictor gue lives by 45 percent at large a re mechanics approach assumes e	the measured fatigue live ding), and standard fractur plastic Neuber analysis up of life as the applied strain pplied strains, but seems t	ss than 10 ⁴ cycles to failure). Specimens s were compared with those predicted by re mechanics life prediction techniques. inderpredicts the measured fatigue life by ns decrease. The elastic Neuber analysis to accurately predict lives at reversals-to- tip, and predicts lives within 30 percent
fracture mechanics life prediction tech times more conservative than those en	hunique. As the life cycles-to-failu xperimentally measured. Since the include that for this class of steels	ire decreases, the Neuber a he fracture mechanics appr	fatigue behavior of A723 steels as is the nalysis predicts lives that are two to three oach and the elastic Neuber approach are ictions technique works even through we
14. SUBJECT TERMS Low Cycle Fatigue, Life Predictions, A723 Steel, Fracture Mechanics Life			15. NUMBER OF PAGES 19 16. PRICE CODE

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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE April 1995	3. REPORT TYPE A Final		
4. TITLE AND SUBTITLE ULTRASONIC CULVERT THI				CMS: 6126.24.H180.0 DN: LT4B4FVQ1ABJ
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 13. ABSTRACT (Maximum 200 words) This work describes a response to established at the New York Sta evaluate the remaining safe lives commercial off-the-shelf ultrasoni of the 25DL precision thickness gather user has to add a small wata application of the bubbler to the 14. SUBJECT TERMS Ultrasonics, Squirter Technology 	te Department of Transporta s of the culverts. The technic ic equipment and piezoelectric age and the B120 bubbler with er pump to provide continuou culvert surface.	tion. The proposed que developed uses to transducers in a bubbl V316-B, 0.75-inch PTI is stream of water and	nethod will pr he ultrasonic p er configuration 7, 20 MHz trans d a hollowed-o	5. NUMBER OF PAGES 30
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1. AGENCY USE ONLY (Leave blank		3. REPORT TYPE AND Final	
4. TITLE AND SUBTITLE CONVERGENCE OF NUME CORRELATION INTEGRAL TECHNIQUES	RICAL BOX-COUNTING AN		5. FUNDING NUMBERS AMCMS: 6111.02.H611.1
6. AUTHOR(S) L.V. Meisel and M.A. Johnson			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95028
9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Cen Picatinny Arsenal, NJ 07806-50	ter	}	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES Submitted to: Computers in Phy	nics		
12a. DISTRIBUTION AVAILABILITY	STATEMENT		12b. DISTRIBUTION CODE
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applied to Euclidean point sets, required for 5 percent converge for the fractal sets studied is of	of convergence for a numerical . Koch constructions, and a symmetric symmetry for $0 \le 1$ determined by the generalized by points are required for 1 percent	metric chaotic mapping is $q \le 25$) and correlation dimension $D(q)$ and is cent convergence. The b	nerical correlation integral algorithm s described. The number of points N ₅ integral (for $-25 \le q \le 25$) algorithms given by $\log_{10}(N_5) \approx 2.54$ D(q)-0.11. box-based correlation integral (BBCI) data sets, is also described.
14. SUBJECT TERMS Fractal, Multifractal, Correlation	n Integral, Box-Counting		15. NUMBER OF PAGES 13 16. PRICE CODE
17. SECURITY CLASSIFICATION 1 OF REPORT	8. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFIC OF ABSTRACT	CATION 20. LIMITATION OF ABSTRACT
UNCLASSIFIED NSN 7540-01-280-5500	UNCLASSIFIED 4	UNCLASSIFIED 8	UL Standard Form 298 (Ré. 2-89) Prescribed by ANSI Sta 239-19

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Public reporting burden for this collection of info gathering and maintaining the data needed, and collecticn of information, including suggestions f Daris mgn way, Suite 1204, Arlington, VA 22202-	rmation is estimated to average 1 hour per res completing and reviewing the collection of info reducing this burden. To Washington Headd 4302, and to the Office of Management and Bu	uarters Services, Directorate for Infor dget. Paperwork Reduction Project (0)	mation Operations and Reports 1215 Jefferson (C4-0188), Washington, DC 20503
1. AGENCY USE ONLY (Leave blank		3. REPORT TYPE AND DA Final	ATES COVERED
	EEN RESIDUAL STRESS ANI ET OF PLASTIC DEFORMATI)	FUNDING NUMBERS AMCMS: 6126.24.H180.0 PRON: LT4B4FVQ1ABJ
 AUTHOR(S) S.C. Schroeder (Benét Laborate J. Frankel, A. Abbate 	ories and RPI, Troy, NY),		
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050			PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95029
9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Cen Picatinny Arsenal, NJ 07806-50	ter	10.	SPONSORING / MONITORING AGENCY REPORT NUMBER
12a. DISTRIBUTION / AVAILABILITY 9 Approved for public release; di			DISTRIBUTION CODE
diameter to tensile at the outsid treated previously. In order to measured as a function of radia load to indent the sample surfa- techniques. From a model prop of plastic deformation was deriv- we saw that the effect of res deformation: plastic deformation is enhanced for a tensile residu is detectable for the tests using (i.e., less total plastic deformation hardness dependence on residu be done with an awareness that used to obtain residual stress of	all of a hollow steel cylinder that le diameter. The question of how of generalize the previously devel al position using various hardness. The posed by Frankel, Abbate, and Schwed, and the experimental dependitual stress on measured hardness is increated stress, therefore the measured larger loads, R_c and Rockwell-D on). The Rockwell-A (R_A) and the tresidual stress can affect the resultstribution.	the Rockwell-C (R_c) hardin loped concepts, in this rep testers. Each of the hardne residual stress of the samp olz, the relationship betwee ence of R_c on residual stress ess stems from the effect ased for a compressive resid hardness is decreased. From (R_D), and becomes washed e Microdur@ testers using v ockwell-C and Rockwell-D ults, and (b) careful Rockwe	ties from compressive at the inside ness varies with residual stress was oort the hardness in the wall was ess testers used a different applied ole was measured using ultrasonic in the residual stress and the onset is was shown. From previous work of stress on the onset of plastic tual stress, and plastic deformation in this work, we see that the effect out for the tests using lower loads Vickers indenters did not show the hardness tests on gun steel should ell-C and Rockwell-D tests can be
14, SUBJECT TERMS, Residual Stress, Hardness, Pla	stic Deformation, Yield Criteria,	Ultrasonic Inspection	15. NUMBER OF PAGES 28 16. PRICE CODE
17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFICA OF ABSTRACT	TION 20. LIMITATION OF ABSTRACT
UNCLASSIFIED NSN 7540-01-280-5500	UNCLASSIFIED 4	UNCLASSIFIED	UL Standard Form 198 (Rev. 2-89) Prescibed b. 245 Stal 339-15

REPORT D	Form Approved OME No 0704-0185		
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1. AGENCY USE ONLY (Leave blan			AND DATES COVERED
4. TITLE AND SUBTITLE UNIFIED COMPUTER MODEL F THERMOCHEMICAL EROSION I	OR PREDICTING		5. FUNDING NUMBERS AMCMS No. 6126.24.H180.0 PRON No. F10XB065M11A
6. AUTHOR(S) Stuart Dunn*, Samuel Sopok, Doug Peter O'Hara, Gary Nickerson*, and	l George Pflegl		
* Software and Engineering Association of the software and Engineering Association of the software and the software of the sof	AME(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95030
9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NCY NAME(S) AND ADDRESS	(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES To be presented at the 31st AIAA/A To be published in proceedings of the		sion Conference, San Die	go, CA, July 1995.
12a. DISTRIBUTION / AVAILABILITY S Approved for public release; distribu			126. DISTRIBUTION CODE
element needed for developing a ge unattainable by experiment alone. A wall material for different rounds or scientific thermochemical erosion co forty years. The 155-mm M203 Uni materials for the same round. The fi gas thermochemical equilibrium (BL community mass addition boundary (MACE) codes. These five module and axial position. In addition, this shot thermochemical wall erosion sh	chemical erosion modeling cod- neralized gun barrel erosion m it the current stage of code devi- different gun wall materials for nsiderations that have been vali- cannon system example is used irst two modules include the st AKE) codes. The last three mod- layer (TDK/MABL), gas-wall- analyses provide recession, term output can be coupled to FEA (owed uncracked gun steel erod- ith its associated crack profile	odeling code that can pro- elopment, single-shot corr the same round. This con- idated in the reentry noset to illustrate the five mode andard gun community in dules, significantly modifi- chemistry (TDK/ODE), a uperature, and heat flux pro- cracking codes. At the pro- ed by a factor of one humo- t, it appears that gun sta-	deling code provides the necessary missing ovide analysis and design information that is parisons can be made of either the same gun mplex computer analysis is based on rigorous ip and rocket nozzle community over the last ule analyses for chromium and gun steel wall terior ballistics (XNOVAKTC) and nonideal ed for gun barrels, include the standard rocket nd wall material ablation conduction erosion ofiles for each material as a function of time tak heat load axial position, predicted single- tred million more than uncracked chromium. tel ablation at the chromium cracks leaves
14. SUBJECT TERMS Unified Computer Model, Thermoch Thermochemical Ablation, Mechanic Speed Reacting Chemical Flow, 155	al Erosion, High Pressure and	Temperature, High-	15. NUMBER OF PAGES 63 16. PRICE CODE
17. SECURITY CLASSIFICATION 1 OF REPORT	8. SECURITY CLASSIFICATION OF THIS PAGE INCLASSIFIED		SIFICATION 20. LIMITATION OF ABSTRACT UL
NSN 7540-01-280-5500		50	Standard Form 298 2-89

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AGENCY USE ONLY (Leave blank)	2. REPORT DATE May 1995	3. REPORT TYPE AND Final	D DATES COVERED
N TITLE AND SUBTITLE WAVELET TRANSFORM SIGN, APPLIED TO ULTRASONICS			5. FUNDING NUMBERS AMCMS: 6111.01.91A1.1
AUTHOR(S) A. Abbate			
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U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07801-5000			10. SPONSORING / MONITORING AGENCY REPORT NUMBER
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In instances where the mother wave windowing. Peak detection of ultr when large white noise was added wave velocity is also described. The it particularly suitable for dispersion transform signal processor.	elet is well defined, the wavelet asonic pulses using the wavelet . The use of the wavelet transi e two-dimensional wavelet tran n studies. Experimental and n	transform is described form to extract the freq sform allows for both tin umerical results show th	23 16 PRICE CODE

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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE May 1995	3. REPORT TYPE AND Final	
4. TITLE AND SUBTITLE ONLINE CHARACTERIZATION OF CONSTITUENTS IN CHROMIUM PL		RATION	5. FUNDING NUMBERS AMCMS: 6226.24.H191.1
6. AUTHOR(S) Samuel Sopok and Rachael Brooks (Br Instruments, Inc., Westbury, NY)	inkmann		
7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB- Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95032
9. SPONSORING / MONITORING AGENC U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	Y NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY: REPORT NUMBER
11. SUPPLEMENTARY NOTES			<u>.</u>
12a. DISTRIBUTION AVAILABILITY STA Distribution limited to U.S. Governmen critical technology; May 1995. Other r to Commander, U.S. Army Armament J ATTN: Benet Laboratories, AMSTA-A	at Agencies and their contractor equests for this document mus Research, Development, and E	ors because of st be referred angineering Center,	126. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words) The metal plating industry is constantly quality and efficiency. The advantages of hazardous waste monitoring, chemical n downtime, and improve quality. Three n acid, Cr(III), and Fe(III) in chromium pl for the monitoring of Fe(II) in electro Brinkmann Instruments, Inc. (Westbury selective potentiometric, direct colorime The optimum operating tolerances of n respectively. The first chemical constit by-products. Chromium plating solutio g/L phosphoric acid and 795 to 895 g/L are rapidly monitored using these online procedures. The precision, bias, and re adoption. These new online procedures process solutions.	of online monitoring include di reclamation monitoring, and con- new online titration procedures ating solutions. Likewise, one polishing solutions. These m v, NY). In general, these four tric, Cr(VI) reduction then com these four chemical species a usent is purposely added, while ms also contain 230 to 270 g/I sulfuric acid. Critical low of e titration procedures. These liability of these new procedure	rect sampling, process control hemical additions. These additions. These additions. These additions. These additions were developed, tested, and new online titration procedures from plex-formation colorimetric, re 2.5 to 3.5 g/L, 0 to 7.5 all other constituents are un chromic acid. Electropolition concentration chemical constituents new procedures nearly equatives should be further tested a	ol, bath quality control, data processing, livantages reduce costs, manpower, and evaluated for the monitoring of sulfuric re was developed, tested, and evaluated Benet Laboratories and were tested at a above are Cr(VI) reduction then ion- and direct redox titrations, respectively. g/L, 0 to 7.5 g/L , and 0 to 7.5 g/L , newanted low alloy steel plating process thing solutions also contain 640 to 730 tuents in the chromium plating process I precision and bias of previous offline and evaluated for at least a year before
14. SUBJECT TERMS Online Chemical Characterization, Onlin Solutions, Critical Low Concentration C Acid, Trivalent Chromium, Trivalent In	Constituents, Chromium Plating	g Solutions, Sulfuric	15. NUMBER OF PAGES 23 16. PRICE CODE
17. SECURITY CLASSIFICATION 18. OF REPORT UNCLASSIFIED UNC	SECURITY CLASSIFICATION OF THIS PAGE CLASSIFIED	19. SECURITY CLASSIFIC OF ABSTRACT UNCLASSIFIED	UL
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4. TITLE AND SUBTITLE 5. FUND FATIGUE LIFE CALCULATIONS FOR AM			5. FUNDING NUMBERS AMCMS No. 6226.24.H180.0 PRON No. TU5A5F361ABJ
6. AUTHOR(S)			
J.H. Underwood, M.J. Audino, and J	.W. Haas		
7. PERFORMING ORGANIZATION NA	ME(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CC Watervliet, NY 12189-4050			REPORT NUMBER ARCCB-TR-95033
9. SPONSORING / MONITORING AGE	NCY NAME(S) AND ADDRESS(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000			
12a. DISTRIBUTION / AVAILABILITY S	TATEMENT	10	126. DISTRIBUTION CODE
Distribution limited to Department of because of critical technology; June referred to Commander, U.S. Army Center, ATTN: Benet Laboratories,	1995. Other requests for this of Armament Research, Developm	locument must be aent, and Engineering	
13. ABSTRACT (Maximum 200 words)		
155-mm XM297 cannon tube are d properties of two types of ASTM A72 the evacuator and mount interface nor radius. Effects of pressure, autofret calculations. Comparisons are made similar cannon tubes. Environmental with mean life from tests, two sets of	escribed. Yield-before-break 23 steel. The mean fatigue life otches, the coolant channels, the tage residual stress, local resid e with measured mean fatigue cracking in areas of coolant ac of notches on the tube outer dis	calculations are based on calculations are performed coolant entry ports, the the hual stress, and notch deput lives from recent hydraulic ccess is also assessed. Base meter and the coolant char	nean fatigue life at various locations of the the fracture toughness and yield strength for muzzle brake and bore evacuator holes, read sector notches, and the chamber inner h and root radius are accounted for in the c pressure safe service fatigue life tests of ed on the life calculations and comparisons nuels at midwall are identified as locations accomplish an increase in mean fatigue life
14. SUBJECT TERMS Fatigue Life, Fracture, Stress Conce	ntration, Cannon Tubes, Residu	ual Stress	15. NUMBER OF PAGES 16 16
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	July 1995	Final	
4. TITLE AND SUBTITLE AN EXPERIMENTAL INVESTIG PROBLEM RELATIVE TO THE :		ING	5. FUNDING NUMBERS AMCMS No. 6126.24.H180.0 PRON No. C0401029AFP
5. AUTHOR(5) Carlos I. Gutierrez and Mario P. R	ivera		
7. PERFORMING ORGANIZATION N U.S. Army ARDEC Benet Laboratories, AMSTA-AR-C Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95034
9. SPONSORING/MONITORING AG U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07809-5000	ENCY NAME(S) AND ADDRESS(ES	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
12a. DISTRIBUTION AVAILABILITY Distribution limited to U.S. Govern evaluation; July 1995. Other reque Commander, U.S. Army Armameni	ment Agencies only because of te ests for this document must be refe t Research, Development, and Eng	rred to incering Center,	126. DISTRIBUTION CODE
ATTN: Benet Laboratories, AMST 13. ABSTRACT (Maximum 200 word		12189-4050.	
Traditionally, this problem is solver these traditional measures were four	d by using some combination of p ad inadequate for the problem at has	ressure washers and especial and (the 120-mm M285 system	excessive vibration and shock loading lly designed bolts. In the present work m), and the problem was solved by using re of the bolt-loosening mechanism.
14. SUBJECT TERMS Bolt Loosening, Shock and Vibratic Bolt Loosening Due to Shock, Bolt			15. NUMBER OF PAGES 12 16. PRICE CODE
OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFIC OF ABSTRACT UNCLASSIFIED	ATION 20. LIMITATION OF ABSTRA
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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE	3. REPORT TYPE AND	DATES COVERED
4. TITLE AND SUBTITLE	August 1995	Final	5. FUNDING NUMBERS
4. TITLE AND SUBTILE EVALUATION OF HIGH STRENGTI REGENERATIVE LIQUID PROPELL			AMCMS No. 6226.24.H180.0 PRON No. TU5B5F261A
6. AUTHOR(S) Gregory N. Vigilante and Daniel R. Fu	ISCO		
7. PERFORMING ORGANIZATION NAM U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95035
9. SPONSORING / MONITORING AGENC U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	Y NAME(S) AND ADDRESS(ES)		10. SPONSORING / MONITORING AGENCY-REPORT NUMBER
12a. DISTRIBUTION / AVAILABILITY ST/ Distribution limited to U.S. Governme specific authority; August 1995. Othe to Commander, U.S. Army Armament ATTN: Benet Laboratories, AMSTA-	nt Agencies and their contractors r requests for this document mus Research, Development, and En	st be referred gineering Center,	126. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words)	723, PH 13-8 Mo, AF 1410, and	Inconel 718, were evaluate	
as part of this investigation.		ty tests, and environmenta	lly-assisted cracking tests were conducted
as part of this investigation. Environmentally-assisted cracking tests propellant (LP) at both ambient and	s were conducted with constant-d slightly elevated temperatures (1	ty tests, and environmenta isplacement bolt-load mod (75°F). The duration of	lified compact specimens in XM46 liquid testing was six months and five hours, a the solution unchanged for the duration
as part of this investigation. Environmentally-assisted cracking tests propellant (LP) at both ambient and a respectively. Tests were conducted with of testing. Environmentally-assisted cracking test both ambient and slightly elevated term not be determined. Hence, none of the	s were conducted with constant-d slightly elevated temperatures (1 ith the solution refreshed at regu results indicated that no macros perature (175°F) XM46 LP. Bec materials tested were highly sus tests conducted on A723 and	ty tests, and environmenta isplacement bolt-load mod (75°F). The duration of lar intervals and also with copic crack extension too ause no macroscopic crack ceptible to XM46 LP for t an experimental heat tree	liy-assisted cracking tests were conducted lifted compact specimens in XM46 liquid testing was six months and five hours, a the solution unchanged for the duration of the materials tested in king took place, a valid K_{EAC} value could he given test conditions. However, some atment of AF 1410 showed evidence of
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AUTHOR(S) S.L. Lee, M.J. Glennon, A. G	abriele		
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SPONSORING/MONITORING AG U.S. Army ARDEC Close Combat Armaments Ce Picatinny Arsenal, NJ 07806-5		5) 1	0. SPONSORING / MONITORING AGENCY REPORT NUMBER
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redistributes the applied load to residual stresses from shot peer diffraction residual stress mapp breech ring that was fatigue to block/ring assembly was perform stresses and finite element and distribution, especially in the	-lug breech block/ring assembly w to several surfaces rather than or ning and overload processes impr bing was performed in the lugs o ested to failure. Finite element ned using ABAQUS codes on a C halysis (FEA) predictions showe	ne surface in conventional rove fatigue life of the syster f the unaffected portion of modelling of a two-dimen Convex C-220 computer. Co ed good agreement in the ed the general characteristi	ectile launchers. The new geometry breech to react the load. Induced n. In this work, experimental x-ray a 50 percent overloaded multi-lug sional cross section of the breech mparisons of experimental residual major features of residual stress ics of experimental residual stress
SUBJECT TERMS Multi-Lug Breech, Breech Mec Finite Element Analysis	chanism, Overload Process, EX3	5, Residual Stress,	15. NUMBER OF PAGES 21 16. PRICE CODE
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AGENCY USE ONLY (Leave blar		3. REPORT TYPE AN	
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TITLE AND SUBTITLE NDEX TO BENET LABORATOR ECHNICAL REPORTS - 1994	RIES		5. FUNDING NUMBERS N/A
AUTHOR(S) . D. Neifeld			
PERFORMING ORGANIZATION N J.S. Army ARDEC Senet Laboratories, AMSTA-AR-C Vatervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-SP-95037
. SPONSORING / MONITORING AC J.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	SENCY NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
1. SUPPLEMENTARY NOTES			126. DISTRIBUTION CODE
2a. DISTRIBUTION / AVAILABILITY Approved for public release; distri			126. DISTRIBUTION CODE
Approved for public release; distri 3. ABSTRACT (Maximum 200 wo	bution unlimited.	atories during 1994.	
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Approved for public release; distri	bution unlimited. rds)		15. NUMBER OF PAGES 74
Approved for public release; distri	bution unlimited. rds) reports published by Benet Labora		15. NUMBER OF PAGES

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188
Public reporting burgen for this collection of informa gathering and maintaining the data needed, and com collection of information, including suggestions for ri Davis High way, Suite 1224, Arlington, VA 222024302	pleting and reviewing the collection of during this burgen, to Washington He	information. Send comments rec	reviewing instructions, searching existing data sources parding this burden estimate or any other aspect of this for information Operations and Report, 1215 Jefferson opect (0704-0188), Washington, 2012020
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE September 1995		ND DATES COVERED
4. TITLE AND SUBTITLE THRICE DIFFERENTIABLE AF CONIC SPLINE INTERPOLATIO	FINE		5. FUNDING NUMBERS AMCMS: 6126.24.H180.0 PRON: 4A4A4FYB1ABJ
6. AUTHOR(5) Royce W. Soanes			
7. PERFORMING ORGANIZATION NAME U.S. Army ARDEC Benét Laboratories, AMSTA-AR-6 Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95038
9. SPONSORING / MONITORING AGENCY U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES 12a. DISTRIBUTION : AVAILABILITY STA Approved for public release; distri			126. DISTRIBUTION CODE
13. ABSTRACT (Maximum 200 words) We present interpolating functions are defined as piecewise conics and "affine" refers to the fact that we m of numerical differentiation using of system solved by Newton iteration. Newton iteration are obtained by the based on conic splines is also include of the mathematical machinery behing applicable than global C ³ conic splipointwise sense. This apparent includes the set of the set o	which have three orders of are therefore guaranteed to ake no use of Euclidean dis conics. The nodal derivative each iteration involving the he aforementioned conic nu led, as well as a discussion of ind conic differentiation and ines are, as well as being co crease of smoothness beyon etched interpolants reproduc	to be convex in the case of tance or angle in the dis- ss for the conic splines s e solution of a pentadia merical differentiation. If what we refer to as "ske local C ³ conic splines. Si- mputationally simpler, if d C ³ is obtained through the conics with or without	(convex) data point. These functions of (strictly) convex data. The modifier scussion. We also include a discussion atisfy a locally quadrivariate quadratic gonal linear system. Initial values for A discussion of numerical quadrature etched" interpolation, which makes use ketched interpolation is more generally more flexible, and smoother in a local h a process of re-sketching during the t re-sketching. This is to say that if the t that conic.
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avis Highway, Suite 1204 Anington, VH 22202-30	2, and to the Office of Management and 2. REPORT DATE	•	ND DATES COVERED
. AGENCY USE ONLY (Leave blank)		Final	
TITLE AND SUBTITLE	October 1995		5. FUNDING NUMBERS
RACTURE MECHANICS TESTS AL FOR THE 120-MM M121 MORTAR			AMCMS No. 6111.02.H611.1
. AUTHOR(S)			
I.H. Underwood, E. Troiano, and D. C	rayon		
PERFORMING ORGANIZATION NAM	E(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER
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. SPONSORING / MONITORING AGENC	Y NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
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1. SUPPLEMENTARY NOTES			
2a. DISTRIBUTION / AVAILABILITY STA	ATEMENT		12b. DISTRIBUTION CODE
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13. ABSTRACT (Maximum 200 words)			
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4. TITLE AND SUBTITLE COMMON TIME REFERENCE FOR I	NTERIOR BALLISTIC I	DATA	5. FUNDING NUMBERS AMCMS No. 6226.24.H180.0 PRON No. TU5B5F261ABJ
5. AUTHOR(S) G. Peter O'Hara			
7. PERFORMING ORGANIZATION NAME U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB- Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95040
9. SPONSORING / MONITORING AGENCY U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	Y NAME(S) AND ADDRES	S(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES			126. DISTRIBUTION COD:
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14. SUBJECT TERMS Interior Ballistics, Time Constant, Zero	Time, Pressure, Time De	lay	15. NUMBER OF PAGES 17 16. PRICE CODE

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1. AGENCT OSE ONET (SECTO SIGNA	October 1995	Final	
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6. AUTHOR(5) Royce W. Soanes			
7. PERFORMING ORGANIZATION NA U.S. Army ARDEC Benét Laboratories, AMSTA-A Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-95041
 SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Cen Picatinny Arsenal, NJ 07801-50 	ter		10. SPONSORING/MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES	STATEMENT		126. DISTRIBUTION CODE
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17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIF OF ABSTRACT	ICATION 20. LIMITATION OF ABSTRAC
UNCLASSIFIED	UNCLASSIFIED	UNCLASSIFIED	UL
NSN 7540-01-280-5500	6	51	Standard Form 298 (Rev. 2-89) Prescribed by ANS Std. 239-16

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	November 1995	Final	
4. TITLE AND SUBTITLE STRESS DISTRIBUTION IN CON WALLED TUBES SUBJECTED T		HICK-	5. FUNDING NUMBERS AMCMS No. 6111.02.H611.1
6. AUTHOR(S)			
Boaz Avitzur			
7. PERFORMING ORGANIZATION N	AME(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-C Watervliet, NY 12189-4050	СВ-О		ARCCB-TR-95042
9. SPONSORING / MONITORING AGE U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000	ENCY NAME(S) AND ADDRESS(E	5)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES			
12a. DISTRIBUTION / AVAILABILITY	STATEMENT		126. DISTRIBUTION CODE
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thickness undergoes plastic deformation, Autofrettage is a process whereby a thick while an outer sleeve remains elastic. A stress distribution of the tubes under pre- general, when uniformly distributed rad (throughout the tube's wall thickness) he surface of the same tube, the tangential magnitude of the tangential stress compo- surface, as well as with increasing magn- the magnitude of the tangential compon- wall thickness tubes it might reverse its a as that of the imposed radial component. of other related processes and/or produc uniformly distributed radial stresses at i components, the cooled annulus imposes of the elastic-plastic interface diameter a the plastically deformed inner sleeve of	whereby thick-walled tubes are subject while the rest of it remains elastic. The k-walled tube is subjected to internal p ulthough the investigators of this proce- ssure and the corresponding pressure l tial stresses are acting on the outer (d as the same sign as the radial compone- and the radial stress components will when increases towards the inner surfa- titude of the imposed radial stress. How ent decreases (from a maximum at the rign (at some intermediary radius between In a more generalized form, the comp ts. A press-fitted concentric liner in a its bore, the liner is subjected to the s a uniformly distributed radial stress on and the stresses on that surface and the the tube are presented in this report.	e most widely known and intensivessurization until, hopefully, and ressurization until, hopefully, and ress are seeking to determine the have to be determined in order to tiametrical) surface of a thick- unt. If, however, uniformly dist be of the opposite sign to each ce regardless of whether the impo- wever, if loaded at the tube's in e elastic-plastic interface towar even the elastic-plastic interface a utational method used in autofur thick-walled tube is such an ex- ame radial stresses at its outer the uncooled sleeve or liner and e equations for the stress distrib The calculations of the impos-	ial stresses in which part of the tube's wall ely studied of these processes is autofrettage. In inner sleeve undergoes plastic deformation, stress distribution after depressurization, the o arrive at the retained stress distribution. In walled tube, the tangential stress component ributed radial stresses are acting on the inner o ther. In an elastically deformed tube, the posed radial stress is at the outer or the inner interior after plastic deformation commences, ds the tube's inner surface and in very large and the inner surface) assuming the same sign ettage analysis can be utilized in the analysis sample. While the outer tube is subjected to diameter. During heat treatment of tubular vice versa. The equations for the calculation ution thereof in both the outer sleeve and in ed radial stress(es) (internal and/or external) tion that the material is nonstrain-hardening
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17. SECURITY CLASSIFICATION	18. SECURITY CLASSIFICATION	19. SECURITY CLASSIFIC	
OF REPORT UNCLASSIFIED	OF THIS PAGE UNCLASSIFIED	OF ABSTRACT UNCLASSIFIED	UL
NSN 7540-01-280-5500	6	2	Standard Form 295 (Rev. 2-85) Prescribed by 245: Std. 239-15 298-102

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I. MULINCI USE UNEI (LEUTE LIGHA)	December 1995	Finel	
4. TITLE AND SUBTITLE			5. FUNDING NUMBERS
THERMAL STABILITY OF EPOXY	Y COMPOSITE MATERIALS		AMCMS: 6111.01.91A1.100
5. AUTHOR(S)			-
Mark F. Fleszar			
7. PERFORMING ORGANIZATION NA	ME(S) AND ADDRESS(ES)	······································	8. PERFORMING ORGANIZATION REPORT NUMBER
U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CC Watervliet, NY 12189-4050	В-О		ARCCB-TR-95043
9. SPONSORING/MONITORING AGE	NCY NAME(S) AND ADDRESS	(ES)	10. SPONSORING / MONITORING AGENCY REPORT NUMBER
U.S. Army ARDEC			
Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000			
11. SUPPLEMENTARY NOTES Presented at the 24th Annual North .		onference, San Francisco	o, CA, 10-13 September 1995.
Presented at the 24th Annual North A Published in Proceedings of the Con 12a. DISTRIBUTION / AVAILABILITY S Approved for public release; distribution	ference.	onference, San Francisco	D, CA, 10-13 September 1995.
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