# INITIAL OPERATIONAL TEST AND EVALUATION OF FORMS 20, 21, AND 22 

 OF THE ARMED SERVICES VOCATIONAL APTITUDE BATTERY(ASVAB)
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## NOTE

This report, INITIAL OPERATIONAL TEST AND EVALUATION OF FORMS 20, 21, AND 22 OF THE ARMED SERVICES VOCATIONAL APTITUDE BATTERY(ASVAB), has been produced in two sections to facilitate review.

The front section contains the preface, the executive summary, the text that discusses the procedures and analysis, the appendixes, and a list of references.

The back section, titled ASVAB 20, 21, AND 22 IOT\&E SUPPLEMENT, contains all tables and figures that provide information to support the discussion of procedures and analyses.

Reviewed by:

Bert F. Green, Jr.<br>Johns Hopkins University

This repori was prepared for the Directorate for Accession Policy, Office of the Assistant Secretary of Defense (Personnel and Readiness). The technical project officer for this report was Dr. Bruce Bloxom, Quality Control and Analysis Branch, Personnel Testing Division, Defense Manpower Data Center. The views, opinions, and findings contained in this report are those of the authors and should not be construed as an official Department of Defense position, policy, or decision, unless so designated by other official documentation.

# INITIAL OPERATIONAL TEST AND EVALUATION 

OF FORMS 20, 21, AND 22

## OF THE ARMED SERVICES VOCATIONAL

 APTITUDE BATTERY(ASVAB)

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Personnel Testing Division
DEFENSE MANPOWER DATA CENTER

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## PREFACE

The completion of this work would not have been possible without the efforts of many persons at the Defense Manpower Data Center (DMDC) and elsewhere. Dr. Linda Curran, formerly at Air Force Human Resources Laboratory, and Dr. Pamela Palmer at Operational Technologies developed the items used in the new test forms. Mr. John Harris at DMDC and Dr. Wayne Shore at Operational Technologies developed the final forms of the new test booklets. Mr. Richard Branch and others at the Military Entrance Processing Command provided both leadership and day-to-day assistance in the distribution and special administration of the test forms as required for the study. Mr. Robert Hamilton at DMDC meticulously developed and documented the data base for the analyses. Dr. Bert F. Green, Jr., at Johns Hopkins University, provided thoughtful and detailed comments on an earlier version of this report. And Ms. Norma Vishneski at DMDC provided careful attention to all of the necessary details in the final editing and production of the report.

Special recognition must be made of the contributions of Dr. D.R. Divgi at the Center for Naval Analyses. This project was one of the first equating studies conducted entirely at DMDC. Through his generous and extensive counsel on the data analysis plans and procedures for the project, Dr. Divgi provided DMDC with invaluable support, sharing with the authors the benefits of his keen analytic insights and his extensive experience with equating and related statistical issues.

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## EXECUTIVE SUMMARY

The Armed Services Vocational Aptitude Battery (ASVAB) is a multiple-choice test battery administered to all applicants for active-duty and reserve enlistment in the United States Armed Services. In addition, it is administered to approximately one million students each year as part of the Department of Defense (DoD) Student Testing Program. The battery consists of the ten subtests listed in Table 1. In addition, Verbal (VE) -- which is the sum of two subtests, Word Knowledge (WK) and Paragraph Comprehension (PC) -- is treated like a separate subtest in many analyses and applications. Various combinations of the subtest standard scores form composites that are used by DoD and the Services for determining eligibility for enlistment and for classification into military occupations.

ASVAB Forms 15, 16, and 17 were implemented for use in the Enlistment Testing Program in January 1989. New items for ASVAB Forms 20, 21, and 22 were developed by the Armstrong Laboratory in the Air Force Human Resources Directorate to replace ASVAB 15, 16, and 17 (Palmer, Curran, and Haywood, 1990). Items were then selected for the new forms by a contractor for Defense Manpower Data Center (Shore, Welsh, and Palmer, 1990). For each of the ten subtests, the items in the new forms were selected to make forms that were parallel to the corresponding subtest of the ASVAB reference form, 8a.

Although ASVAB Forms 20, 21, and 22 were designed to be parallel to the reference form, their item contents and statistical properties could not be assumed to have distributions that are identical to the reference form or to each other. Therefore, it was necessary to equate thelis to the reference form, so that their scores would have the same interpretation as scores on the latter form. ${ }^{1}$ Being able to use this same score scale for all ASVAB forms serves three purposes. First, examinees can receive some assurance that they will have comparable scores for military enlistment, regardless of which ASVAB form is administered to them. Second, DoD and the Military Services can receive some assurance that similar numbers of military applicants will be eligible for enlistment regardless of which ASVAB form is administered. Third, policy makers can use ASVAB scores of cohorts of military recruits to study trends in the aptitude of persons entering the military, even when the cohorts differ in the ASVAB forms that are administered to them.

The present study had three purposes. The first was to develop conversion tables for ASVAB Forms 20, 21 and 22. These tables convert subtest raw scores for each form to equated standard scores. The subtest scores would then be on the 1980 standard score scale, the same as the reference form and other forms used operationally in the Enlistment Testing Program. The second purpose was to provide at least a partial check of the use of these conversion tables for constructing composites of subtests in the Enlistment Testing Program. If the test forms are sufficiently parallel in content, and if the conversion tables are correct, then the composites for the new forms should have the same distributions as the composites for the reference form and current operational forms.

[^0]The third purpose of the study was to adjust the conversion tables for effects of using the new answer sheet implemented in February 1992. Scores on the two speed subtests, NO and CS, can vary across answer-sheet formats (Ree and Wegner, 1990). Specifically, scores have been found to be lower with the new answer sheet than with the one for which norms are available (Bloxom, McCully, Branch, Waters, Barnes, and Gribben, 1991; Bloxom, Thomasson, Wise, and Branch, 1992). Therefore, obtaining accurate conversion tables for these two subtests in this study required score- scale adjustments based on combining the new ASVAB form equating with a prior answer-sheet calibration. The latter calibration was provided in Bloxom et al. (1992).

The design of this study was to administer eight ASVAB forms to randomly equivalent groups of at least 12,000 military applicants each. The eight forms were versions $a$ and $b$ of ASVAB forms 20, 21, and 22 -- plus ASVAB 15 g (a current operational form) and ASVAB 15h. Except for its cover, the latter was identical to ASVAB Form 8a, the reference form that was used to collect the normative data (Department of Defense, 1982). The forms were administered as part of the normal processing of military applicants, with scores based on a preliminary equating (Thomasson and Bloxom, 1992) being used to determine eligibility for enlistment and for assignment to military specialties.

The data analyses consisted of data quality-control procedures, checks on the equivalence of the groups taking the eight test forms, a check for item-order effects before pooling the results for different forms having the same items administered in different orders, an equating of subtests on the new forms to subtests on the reference form, the development of subtest conversion tables, and an assessment of the effect of subtest equatings on the equatings of operational composites of subtests.

Analyses of the gender, race, and education of the groups taking the eight test forms showed only slight differences (in gender) between the groups. Also, the sample size varied across test forms in a way that indicated the administration of the forms was not spiralled; but the effects of this on the operational composites were shown to be slight and nonsystematic. However, significant item-order effects were found on forms 21a and 21b of the Coding Speed (CS) subtes: 'onsequently, even though these two forms of CS contained the same items (in different orders), the were not pooled before being equated to the reference form.

Subtests of the new forms were equated to the reference form using equipercentile equating. The procedure employed subtest distributions that were smoothed by fitting a model with as few parameters as necessary to provide no statistically significant departure from the unsmoothed distributions. The equatings did not produce a perfect match of the new-form AFQT composite distribution to the referenceform AFQT composite distribution or to the AFQT composite distribution of a current operational form. However, the precision of its match to the distributions of those forms was comparable to the match obtained ' $n$ the IOT\&E of ASVAB forms 15, 16, and 17 and in the IOT\&E of ASVAB 18/19. Similar patterns of results were found for the Services' specialty composites.

Conversion tables based on the equatings developed here were provided for operational use.

## INITIAL OPERATIONAL TEST

## AND EVALUATION OF FORMS 20, 21, AND 22

## OF THE ARMED SERVICES

VOCATIONAL APTITUDE BATTERY

## Introduction

The Armed Services Vocational Aptitude Battery (ASVAB) is a multiple-choice test battery administered to all applicants for active-duty and reserve enlistment in the United States Armed Services. In addition, it is administered to approximately one million students each year as part of the Department of Defense (DoD) Student Testing Program. The battery consists of the ten subtests listed in Table 1. In addition, Verbal (VE) -- which is the sum of two subtests, Word Knowledge (WK) and Paragraph Comprehension (PC) -- is treated like a separate subtest in many analyses and applications. Various combinations of the subtest standard scores form composites that are used by DoD and the Services for determining eligibility for enlistment and for classification into military occupations.

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Although ASVAB Forms 20, 21, and 22 were designed to be parallel to the reference form, their item contents and statistical properties could not be assumed to have distributions that were identical to the reference form or to each other. Therefore, it was necessary to equate them to the reference form, so that their scores would have the same interpretation as scores on the latter form. ${ }^{2}$ Being able to use this same score scale for all ASVAB forms serves three purposes. First, examinees can receive some assurance that they will have comparable scores for military enlistment, regardless of which ASVAB form is administered to them. Second, DoD and the Military Services can receive some assurance that similar numbers of military applicants will be eligible for enlistment regardless of which ASVAB form is administered. Third, policy makers can use ASVAB scores of cohorts of military recruits to study trends in the aptitude of persons entering the military, even when the cohorts differ in the ASVAB forms that are administered to them.

[^1]The present study had three purposes. The first was to develop conversion tables for ASVAB Forms 20, 21, and 22. These tables convert subtest raw scores for each form to equated standard scores. The subtest scores would then be on the 1980 standard score scale, the same as the reference form and other forms used operationally in the Enlistment Testing Program. The second purpose was to provide at least a partial check of the use of the conversion tables for constructing composites of subtests in the Enlistment Testing Program. If the test forms are sufficiently parallel in content, and if the conversion tables are correct, then the composites for the new forms should have the same distributions as the composites for the reference form and current operational forms.

The third purpose of the study was to adjust the conversion tables for effects of using a new answer sheet that was implemented in February 1992. Scores on the two speed subtests, NO and CS, can vary across answer-sheet formats (Ree and Wegner, 1990). Specifically, scores were found to be lower with the new answer sheet than with the one for which norms are available (Bloxom, McCully, Branch, Waters, Barnes, and Gribben, 1991; Bloxom, Thomasson, Wise, and Branch, 1992). Therefore, obtaining accurate conversion tables for these two subtests in this study required score- scale adjustments based on combining the nnw ASVAB form equating with a prior answer-sheet calibration. The latter calibration was provided in Bloxom et al. (1992).

## Method

## Design

The design of this study was to administer eight ASVAB forms to randomly equivalent groups of at least 12,000 military applicants each. The eight forms were versions $\mathfrak{a}$ and $\underline{b}$ of ASVAB forms 20,21 , and 22 -- plus ASVAB 15g (a current operational form) and ASVAB 15h. Except for its cover, the latter was identical to ASVAB Form 8a, the reference form that was used to collect the normative data (Department of Defense, 1982). The forms were administered as part of the normal processing of military applicants, with scores based on a preliminary equating being used to determine eligibility for enlistment and for assignment to military specialties.

## Subjects

The subjects in this study were applicants for military enlistment who were scheduled for aptitude testing between 1 October 1992 and 15 January 1993. The total number of persons tested at the sites used for this study was 140,062 . The only sites excluded were those associated with the Military Entrance Processing Stations (MEPS) at San Diego, California; Los Angeles, California; and Jackson, Mississippi. There, special studies were being conducted that could not be interrupted.

## Procedure

The subjects were tested in groups that varied in size according to the number of applicants needing to be tested. The test administrators were employees of a MEPS or were persons hired by the Office of Personnel Management (OPM) to administer the test at Mobile Examining Team (MET) sites.

Each subject was provided with the currently operational answer sheet (circular response spaces), an ASVAB test booklet, two pencils, and two pieces of scratch paper. To provide equivalent conditions and frequency of administration for the eight test forms, the forms were to be distributed in a "spiralled" order, that is, a given form was administered to every eighth subject in a test session. Furthermore, the cycle of distribution of forms in each session was to begin where it stopped in the test administrator's previous session. The resulting number of cases administered each of the eight ASVAB forms is shown in the first column of Table 2.

Before the administration of the ASVAB subtests, subjects were given standard ASVAB instructions (Department of Defense, 1990) for providing identifying information and for signing a Privacy Act statement on the answer sheet. The subtests were then administered as specified in the standard ASVAB instructions. Following the test administration, the answer sheets were scanned and scored at MEPS. Number-right (raw) scores and identifying information were electronically transmitted to Headquarters, U.S. Military Entrance Processing Command (MEPCOM). At the end of the study, the data were sent by tape to Defense Manpower Data Center. In addition, item response data were obtained from the scanning of the answer sheets at the METS; these data were mailed to MEPCOM for concatenation into a single file.

## Data Quality Control

## Editing

In addition to range checks, three procedures were used for editing. The first was to eliminate cases with all subtest scores equal to zero. Such cases were assumed to represent erroneous entries in the data set. Only one such case was found in the data for this study.

The second procedure for editing was to eliminate cases known to have previously taken an ASVAB ${ }^{3}$. Such cases were assumed to be performing in ways not representative of cases in the normative sample (Department of Defense, 1982). This editing resulted in the elimination of 21,796 , or $15.6 \%$, of the cases tested. The remaining cases were distributed across test forms as shown in the second column of Table 2.

The third procedure for editing was to delete sessions and sites where the sample sizes for the eight test forms were severely out of balance. As can be seen in the second column of Table 2, the number of cases of initial tests varied from 15,959 for ASVAB 15 g to 13,007 for ASVAB 22b. An inspection of the distribution of the eight test forms by test site (defined by a two-digit MEPS code and an additional two-digit site-within-MEPS code) and test date revealed that (a) for some dates at some sites, only a subset of the test forms was administered and (b) for some test sites, one or more of the test forms was never administered during the study.

In the first stage of the third edit, test sessions were defined as severely out of balance when the number of cases that were administered the most frequently used form differed by more than two from the number of cases that were administered the least frequently used form${ }^{4}$. Deletirig these sessions resulted in the deletion of 21,306 cases. Because applying this criterion did not exclude sessions at the large number of low-volume sites, the second stage of the third edit was to apply a similar criterion to the totals across all sessions at test sites where the number of cases was 16 or less during the entire data

[^2]collection.5 Deleting these out-of-balance test sites resulted in the elimination of 1,302 cases. Following the third edit, the number of cases for each test form was as shown in the third column of Table 2.

As can be noted from the final percentages in Table 2, the edited samples are out of balance to nearly the same extent as the unedited samples. An inspection of data from a number of test sites and sessions suggested that the imbalance was occurring as a result of lack of careful spiralling of test forms across large numbers of small test sessions as well as within those sessions; test administrators at the large number of low-volume test sites tended to consistently use lower-numbered ASVAB forms more often than higher-numbered forms. To evaluate the effect of this imbalance on the utility of the equatings developed in this study, supplemental analyses were conducted using data selected with additional edits to further balance the number of cases administered each form. (See Appendix A.) The results of these analyses are provided in a later section of this report. (See "Comparisons of Results for Three Subsets of Data.")

## Equivalence of Groups

During the data collection, the eight test forms were to have been distributed in a spiralled manner to subjects in each testing session. This procedure was intended to provide eight randomly equivalent groups of subjects. However, as noted in the preceding section, the sample sizes differed substantially across the eight test forms. (See Table 2.) If the eight groups also differed on demographic characteristics that are typically correlated with test performance, then the assumption that the groups have the same aptitude distribution would be questionable. If this were the case, then using the data for equipercentile equating would require adjustments of the distributions. Therefore, as a check on group equivalence, the eight groups were compared with respect to three background characteristics (gender, race, and education) that were indicated by the examinees on their answer sheets. Also, the groups were compared with respect to their distribution across the 65 MEPS, because the aptitude distributions of military applicants processed at the MEPS are known to vary.

Table 3 provides frequencies and percentages at each level of gender, race, and education. The group-by-test-form Pearson chi-squares were statistically significant ( $p<.05$ ) for only one of the three background characteristics: gender. As is indicated by cell percentages and contributions to the chisquare, ASVAB 20b had a slightly higher representation of females than did the other forms.

A 65-MEPS-by-8-test-form Pearson chi-square of the number of persons tested was not statistically significant (chi-square $=271.932$, d.f. $=448$ ). This provided some assurance that whatever

[^3]Sites with the number of forms having zero administrations greater than MAXZERO were deleted.
differences there were in the aptitude distributions of the 68 MEPS was not directly associated with differences in the sample sizes of the eight test forms.

The results of the group comparisons provided sufficient indication of group equivalence to support proceeding with equating without making adjustments to the distributions. Table 4 provides the resulting subtest means, standard deviations, skewness and kurtosis of the reference form ( 15 h ), the current operational form ( 15 g ), and the six new ASVAB forms ( $20 \mathrm{a} / \mathrm{c}, 21 \mathrm{a} / \mathrm{b}$ and $22 \mathrm{a} / \mathrm{b}$ ) being equated to the reference form.

## Item-Order Effects

For the subtests that are not in the AFQT composite (GS, NO, CS, AS, MC, EI), each pair of same-numbered forms contains the same items (i.e., forms 20 a and 20 b contain the same items; forms 21 a and 21 b contain the same items; and forms 22a and 22b contain the same items). However, the subtests that are in the AFQT (AR, WK, PC, MK, and thus VE) contain unique sets of items in each ASVAB form; this provides somewhat greater protection against the compromise of tests in the composite that is used to determine eligibility for enlistment.

In each pair of the same-item, non-AFQT subtests (excluding NO), the items differ slightly in the order of their administration in the two forms. (For the NO subtest, item order was constant across the a and $b$ versions of each form.) The purpose of this slight scrambling of the item order is to make it unlikely that an examinee could obtain correct answers by copying responses from the answer sheet of another person who is administered another ASVAB form.

Two forms of a subtest with the same items but slightly different item orders may not have the same distribution of scores, and may, therefore, require separate equatings to the reference form. For example, the distributions for MC might have been affected by the order of item administration if examinees were using strategies developed on one question to formulate answers for subsequent questions.

A statistical test was used to assess item-order effects for each subtest on each pair of forms containing scrambled orderings of the same items. If the test statistics were found to be significant for a pair of same-item forms, then separate equatings were to be done for each separate form. Otherwise, the distributions of the two same-item forms were to be combined and a single equating developed for use with either form.

A procedure developed by Hanson (1991) that uses log-linear modeling and provides a likelihood ratio chi-square statistic was used to test the differences in test-score distributions of the pairs of sameitem different-order subtests. The first step in this procedure, which is also a part of the equipercentile equating of smoothed distributions (see below), is to fit each of the separate distributions using the loglinear model (see Holland and Thayer, 1987) with polynomials of varying degrees. In this study, the upper limit for the degree of polynomial was the smaller of 10 and $M / 2$, where $M$ is the number of items in the subtest. This limit was to restrict overfitting the distribution by further limiting the number of parameters in the polynomial. The next step in the procedure was to determine the degree of polynomial to use for the log-linear fit for each of the separate forms. (See the discussion below on the modified "Haberman's Rule" used to determine the degree of the fitted polynomial.) The higher degree of the two fitted polynomials was chosen to be the "comparison test degree" (CTD). The comparison was then made of the log-linear fit to the combined distribution at degree CTD versus the log-linear fit to the separate distributions at degree CTD. A likelihood ratio chi-square test was made to determine if the fit
of the separate distributions was significantly better than the fit to the combined distribution. In this analysis, an alpha level of $0.05 / 15=0.0033$ was used for each statistical test, so that the expected number of Type I errors for the 15 statistical tests would be 0.05 .

Table 5 contains the results of the likelihood ratio chi-square tests for item-order effects for each pair of tested forms. For subtests GS, NO, CS, AS, MC, and EI, 20a/b denotes the combination of forms 20 a and $20 \mathrm{~b} ; 21 \mathrm{a} / \mathrm{b}$ denotes the combination of forms 21 a and 21 b ; and $22 \mathrm{a} / \mathrm{b}$ denotes the combination of forms 22a and 22b. Except for CS on forms 21a/b, the chi-square statistic was nonsignificant (alpha $=0.0033$ ). Thus, except for CS on ASVAB 21a/b, the forms could be combined when computing their equating functions for same-item forms for subtests GS, CS, AS, MC, and EI. Same-item forms for the NO subtest were combined because the item order did not vary for that subtest. For the AFQT subtests, all equatings were separate because each form of each AFQT subtest contained unique items.

## Equating of Subtests

## Equating Methods

The use of ASVAB forms 20, 21, and 22 to obtain scores for use in military enlistment or for comparison with national norms requires that score scales for these forms be given an equating transformation, to enable their scores to be placed on the same standard score scale as the reference form, ASVAB 8a (or 15 h ).

Several methods of equating were selected from alternatives reported in the research literature. Appendix B provides a discussion of the approaches that were considered and the reasons for selecting the methods -- including smoothing distributions -- used in these analyses. The methods were ones used in previous ASVAB equating studies (e.g., Bloxom and McCully, 1992): linear-identity, linear-rescaling, raw equipercentile, and polynomial-log-linear equipercentile. Linear-rescaling equating was the conventional linear procedure for converting number-right scores on the new test forms to have the same mean and standard deviation as scores on the reference form (e.g., see Angoff, 1971). Linear-identity equating used the scores from the new form without changing them. It was a special case of linear equating, where equal means and standard deviations are assumed. Both the linear-identity and linearrescaling equating were included for comparative purposes, but neither one was considered for subsequent operational use. Divgi (1988) showed that, for the sample size and population used in this study, linear equatings have a higher cross-validation root- mean-squared error than do equipercentile equatings.

Equipercentile equatings were obtained from each of two estimates of the subtest cumulative frequency distributions. Raw equipercentile equating was an equipercentile equating obtained from the unsmoothed frequency distribution for each test form; this was obtained for reference only and was not considered for operational use because of its lack of smoothness, its large number of parameters, and its conseque:iiy greater sampling variability. Polynomial log-linear equating was an equipercentile equating obtained trom a log-linear smoothing that included all polynomial terms up through the highest-order statistically significant term (less than the 11th term); the number of terms was based on a decision rule suggested by Haberman (see Holland and Thayer, 1987), with an upper bound placed on the number of terms in the polynomial; the upper bound was the smaller of $M / 2$ and 10 , where $M$ was the number of items in the subtest; Table 6 shows the resulting number of terms selected for each of the distributions.

Prior to each equipercentile equating, two modifications were made in the estimates of the cumulative distribution functions. First, the extreme lower tail of each distribution was smoothed in a way that would make the equating smooth and would result in an identity equating at the bottom of the number-right score scale. The major concern was that equipercentile equating is unstable where the score frequencies are small. The reason for making the lower end of the equating converge on an identity equating instead of some other function was that equipercentile equating provides no alternative to assuming parallel measurement where the test contents are parallel, score levels are below the level expected under random responding, and the score frequencies are small. The mechanism for making the lower end of the equating converge on an identity equating here was to substitute a power function (Appendix D) for the estimated cumulative distribution below the 0.5 th percentile. The parameters of the function were chosen to preserve both the estimated frequency and cumulative distribution functions where the power function was attached. Such a procedure results in a relatively smooth equating function and does not affect the equating at scores above the .5th percentile. This mechanism is a modification of one used by Kolen and Brennan (1990); those authors used a linear function with a zero intercept instead of the more general power function, resulting in an equating that raay not be very smooth at the .5th percentile if the test is short.

The second modification of the cumulative distributions prior to equipercentile equating was to add .5 to the number-right score associated with each cumulative frequency and to create a new origin ( $\mathrm{X}=-.5, \mathrm{~F}(\mathrm{X})=.0$ ) at the lower end of the function. This was done so that the cumulative distribution could have the conventional interpretation as a continuous-score distribution that is linear from .5 below each number-right score to .5 above each number-right score (Kolen and Brennan, 1990).

After the distributions were smoothed and the equipercentile equatings were computed, the final step was to check the differences between the raw and polynomial log-linear equatings. Specifically, this step required comparing the equatings in the score metric (i.e., in terms of differences between their score scales) and in the frequency metric (i.e., in terms of differences between distributions of the equated scores). These comparisons were measured both in terms of the algebraic distance between functions (root mean square difference) and in terms of the practical impact of those differences (i.e., percent of cases affected). Appendix E provides further details on these criteria and indices.

## Subtest Distributions and Equatings

Figures 1 through 11 show raw and polynomial log-linear smoothed distributions for each of the 11 subtests. Figure 12 shows the standard-score contrast of the raw, linear-rescaling and polynomial loglinear equatings with a linear identity equating for GS. Figures $14,16, \ldots, 32$ show these results for the other subtests, AR, WK, PC, NO, CS, AS, MK, MC, EI, and VE, respectively. In each case, the contrast is plotted as a function of the number-right score on the new test form; also shown is the raw frequency distribution of the new test. The means and standard deviations in Table 6 were used to compute the linear-rescaling equatings. The polynomial log-linear smoothings of the distributions were used to compute the corresponding equipercentile equatings. The means and standard deviations from the Youth Population (Table 1) were used to convert the equated scores to the standard scores being contrasted in Figures 12, ..., 32. Tables 7 and 8 summarize the differences between the equating functions in terms of their root mean squared differences and in terms of the practical impact of using one equating versus another. (See Appendix E.) For comparative purposes, these tables also include results from a re-equating of the current operational form, 15 g .

Figure 13 shows the contrast (i.e., arithmetic difference) of the cumulative distributions of the new forms' raw and polynomial log-linear equated scores with the cumulative distribution of the
reference-form scores for GS. Figures $15,17, \ldots, 33$ show these results for the other subtests, AR, WK, PC, NO, CS, AS, MK, MC, EI, and VE, respectively. In each case, the contrast is plotted as a function of the number-right score on the reference form; also shown is the frequency distribution of the reference form. Linear interpolation was used to obtain the cumulative distributions of equated scores at these points. None of the cumulative distributions used in these contrasts was smoothed. Tables 9 and 10 summarize the differences between the distribution functions in terms of their root mean squared discrepancy from the reference form distribution and in terms of the practical impact of using one equating versus another. (See Appendix E.) For comparative purposes, these tables also include results from a re-equating of the current operational form, 15 g .

## Development of Standard Score Conversion Tables

Conversion to Rounded Equated Standard Scores. For the conversion table for each test form, a rounded equated standard score (RESS) (usually called simply "Standard Score") was computed from the fractional equated standard score (FESS) of the polynomial log-linear equating. For all subtests, except CS and NO (see conversions using new "circle" answer sheets below for subtests CS and NO), the conversion was simply a rounding of the fractional equated standard scores to the nearest integer, then truncating below 20 or above 80 .

$$
\text { RESS }=\left\{\begin{array}{lr}
20, & \text { if FESS }<=20 \\
80, & \text { if FESS }>=80 \\
\text { truncate(FESS }+0.5), \text { otherwise }
\end{array}\right.
$$

The rounding followed the convention of rounding up if the decimal remainder is greater than or equal to .5 , and rounding down otherwise. The truncation followed the ASVAB convention of limiting the standard score scale to values between and including 20 and 80. (See Maier and Sims, 1986.)

Standard Score Conversion Tables with New "Circle" Answer Sheets. Since the speeded subtests, NO and CS, were found by Bloxom et al. $(1991,1992)$ to have an answer-sheet effect, an additional transformation was needed to put scores of these speeded subtests using the new "circle" answer sheet on the same score scale as the previous "vertical bar" answer sheet scale.

Four steps were used in the development of NO and CS conversion tables for the use with the new "circle" answer sheet. As with all subtests, the first step was to equate the raw number-right score on the new form to the reference form ( 15 h , aka 8a) number-right score (where the "circle" answer sheets were used for both new and reference forms, and denoted by a subscript c):

$$
\text { Equated Number-Right Score }_{c}=\mathrm{f}\left(\text { Raw Number-Right Score }{ }_{c}\right) \text {, }
$$

and where transformation f is the number-right equating for the new form. Second, the equated numberright scores on the "circle" answer sheet (denoted by a subscript c) were converted to equated number-right-equivalent scores on the older "vertical bar" answer sheet (denoted by a subscript b). This was done by using linear interpolation with the appropriate answer-sheet equatings ${ }^{6}$ (denoted by function $g$ ) selected in the Optical Mark Reader (OMR) study by Bloxom et al. (1992):

$$
\text { Equated Number-Right Score }_{\mathrm{b}}=\mathrm{g}\left(\text { Equated Number-Right Score } \mathrm{c}_{\mathrm{c}}\right) \text {. }
$$

[^4]Third, the 1980 Youth Population means and standard deviations (Table 1) were used to convert the reference-form, "vertical-bar"-answer-sheet-equivalent-fractional-number-right score to the standard-score metric producing the fractional equated standard scores (FESS):

FESS $=50+10\left(\right.$ Equated Number-Right Score $\left._{\mathrm{b}}-\mathrm{M}\right) / \mathrm{S}$.
The fourth step in developing conversion tables for NO and CS was to round the fractional standard score equivalents and truncate them at 20 and 80 , paralleling the last step for the nonspeeded subrests, and producing rounded equated standard scores (RESS) or simply "standard scores." The resulting integers provided the standard score values for NO and CS, for the conversion tables designated for use with ASVAB 20a, 20b, 21a, 21b, 22a, and 22b and the new "circle" answer sheets during the implementation in the Enlistment Testing Program. (Appendix F contains the new-form fractional equated standard scores based on polynomial log-linear equatings for all subtests, including standard scores for NO and CS after linking to the OMR answer-sheet transformation. ${ }^{7}$ )

## Comparisons of Equated-Subtest Intercorrelations

In previous equating studies of ASVAB 18/19 (Bloxom and McCully, 1992) and 20/21/22 (Thomasson and Bloxom, 1992), differences were found in the correlations between the power subtests that were indicative of variation in the construct validity of the ASVAB subtests across ASVAB forms. In the effort to explore this in the present study, an investigation of the means, variances, and intercorrelations between the subtests' converted standard scores was made. Table 11 contains the subtest standard score means, standard deviations, and intercorrelations for each form; all statistics are based on analyses of rounded standard scores, i.e., scores obtained from application of the conversion tables. Also in Table 11 are the differences between the new forms' subtest standard score means, standard deviations, and intercorrelations and those of the reference form ( 15 h ; middle of the page) and the current operational form ( 15 g ; bottom of the page). In addition, Figures 34 and 35 _. de plots of the first three unrotated principal components of the power subtests of each of the eight ASV ${ }_{\text {n }}$ forms; the first component is in Figure 34; the second and third components are in Figure 35.

An inspection of Table 11 and Figures 34 and 35 revealed three patterns in the differences between ASVAB forms. The first pattern was that GS was less correlated with the technical subtests on the new forms (ASVAB 20, 21, and 22) than on the reference form and on the current operational form. This pattern was more pronounced in comparisons with the reference form ( 15 h ) than with the current operational form ( 15 g ); the differences were approximately .05 greater in the comparisons with the reference form. The largest differences were for ASVAB 21a and 21b, where the GS correlation with AS was .23 lower than for ASVAB 15h and where the GS correlation with EI was .18 lower than for ASVAB $15 h^{8}$. Fully understanding this pattern of results requires a study of the correlations between items in GS and the technical subtests. However, in the absence of such a study, it is useful to note that the pattern was consistent with that found in the IOT\&E of ASVAB 18/19 (Bloxom and McCully, 1992) and in the previous operational calibration of ASVAB 20/21/22 (Thomasson and Bloxom, 1992). As in

[^5]those studies, the implication here is that the distributions of composites -- such as the Air Force M composite -- containing both GS and technical subtests were more likely to vary across ASVAB forms even if the subtests themselves were accurately equated.

The second pattern in the correlations between subtests was that the new forms were, in general, more like the current operational form than like the reference form. However, a notable exception was in the correlation between VE and EI, which was approximately .10 higher for the new forms than for the current operational form; in contrast, the correlation was slightly smaller (by .02) for the new forms than for the reference form. Although this pattern was reliable and may indicate more of a verbal component to the EI subtest than has been the case in recent operational use, it was not likely to have an impact on the distribution of composites because none of them contains both VE and EI.

The third pattern in the correlations between subtests was that the AFQT subtest scores (VE, AR and MK) had somewhat lower intercorrelations (by approximately .04) for ASVAB 21b than for the reference form, 15 h . The pattern was also present in the comparison of 21 b with the current operational form, 15 g , but the difference was less pronounced (approximately .02-.03). The implication here i the distributions of the AFQT and other composites containing these three subtests were more liket. vary across ASVAB forms even if the subtests themselves were accurately equated.

Further analyses -- including item analyses -- are needed to more fully explain the correlational differences between the newer ASVAB forms, the reference form and the current operational form. Wise, Nicewander, and Bloxom (1991) provided analyses of such differences for ASVAB 18/19 and the reference form.

## Analyses of Composites of Converted Subtest Scores

The Armed Forces Qualification Test (AFQT) that is used in determining enlistment qualification is based on a weighted sum of three ASVAB standard scores - VE, AR and MK. For all ASVAB forms, this weighted sum is converted to a percentile score -- the AFQT score -- using norms for ASVAB 8a in the 1980 Youth Population (Department of Defense, 1982). The AFQT score scale is then divided into eight categories having the upper bounds for this composite shown in Table 12. These categories are, from the highest to lowest percentiles, labelled: I, II, IIIa, IIIb, IVa, IVb, IVc, V. AFQT-based enlistment standards and reports of aptitudes of military accessions are typically stated in terms of the AFQT categories (e.g., Department of Defense, 1992).

Other composites of ASVAB standard scores are used by the Services in determining eligibility for training in occupational specialties. Table 12 shows which subtests are used, and how they are combined, in each of these composites for each of the Services. Although the Services each use this general approach for obtaining composites, they differ in the final metric employed in determining training qualification. The Air Force converts the sum of subtest standard scores (SSS) to percentile scores as is done for the AFQT; the Army and the Marine Corps convert SSS to standard scores that have a mean of 100 and a standard deviation of 20 for ASVAB 8a in the 1980 Youth Population; and the Navy uses no further conversion of SSS. Further variability across Services is introduced in the choice of cutting scores that are used to determine training qualifications. (See category boundaries in the right column of Table 20.) For example, the Army has more qualification categories on the EL composite than does the Marine Corps.

Because of the variety and large number of operational composites of the ASVAB subtests, the composites are not separately equated for new ASVAB forms once the subtests of those forms have been equated to the reference form. However, after the subtest equatings have been used to convert their raw scores to standard score equivalents on the reference form, it is important to assess the impact of using the composites of the converted subtest scores -- in terms of the comparability of their composites with those of a current operational form as well as the comparability with those of the reference form. Comparability with a current operational form is important for maintaining continuity of qualification standards for, and rates of flow into, occupational-specialty training schools. Comparability with the reference form is important for maintaining continuity of the AFQT score scale when monitoring longterm trends in qualifications of military applicants and accessions.

To assess the comparability of new-form composites with reference-form composites and currentform composites in this study, converted subtest scores were used to generate composites for all of the forms, with the conversions for the new forms (ASVAB 20/21/22) being based on the equatings described in the preceding section of this report. Then, the distributions of these composite scores for the new forms were compared with the distributions of the corresponding composite scores for the reference form (ASVAB 15h) and with distributions of composites for a current operational form (ASVAB 15g). In the preceding section, comparisons of the subtest intercorrelations across test forms suggested that, even after the subtests were equated, the composites would not necessarily have the same distributions across forms. Therefore, it was thought to be important to assess whether new-form composite distributions differed from the reference form and/or from a current operational form.

Generating the distributions of composite scores for the comparisons required several steps. First, rounded-standard-score conversion tables were generated as described in the preceding section and were applied to all subtest scores from the new test forms. The current standard score conversion table for the reference form, ASVAB 15h, (Department of Defense, 1992; as modified in Bloxom et al., 1992) was applied to all subtest scores from the reference form. The current operational standard score conversion table for ASVAB Form 15g (Department of Defense, 1992; as modified in Bloxom et al., 1992) was applied to all subtest scores from that ASVAB form.

The second step in generating distributions of composites was to sum the standard scores of subtests as indicated in Table 12. These scores were then converted to a percentile or standard score metric, depending on which of those metrics would be used operationally. In the third step, the frequencies at each score level for each composite, plus the category score ranges indicated in Table 12, were used to compute the number of subjects in each category for each test form.

Three types of indices were used to assess differences between the new-form, reference-form, and operational-form distributions of a composite. The first of these was a Pearson chi-square, based on a cross-tabulation of the eight ASVAB forms and the categories defined by operational cut-scores on the composite's score scale. A probability for each chi-square was computed and evaluated without adjusting the alpha level to take into account the number of significance tests; because the chi-squares were computed in the sample used for equating, the true probability of a Type I error was almost certainly below any nominal alpha level applied to the computed probabilities, although the extent of this reduction was unknown. Because the true probability was unknown, the evaluation of these chi-squares included the application of a heuristic; the heuristic was to compare the chi-quare with two times its degrees of freedom.

The second index used to assess differences (across forms) in the distribution of a composite was the standard deviation of the composite. Once the subtests were equated, the means of composites of the
subtests were equated. However, because subtest intercorrelations varied across forms, the standard deviations of the composites could vary across forms. For example, because GS and AS had a lower correlation on ASVAB 21b than on the reference form, the standard deviation of a composite containing the sum of these subtests (e.g., the Air Force M composite) could show a lower standard deviation on ASVAB 21b than on the reference form.

The third index used to assess differences (across forms) in the distribution of a composite was the percentage of all cases at or above a cut score; this was computed for each of the operational cut scores on the composite and was done separately for each of the forms used in this study. The expectation was that those forms with lower standard deviations would have smaller percentages of cases scoring above high cut scores and larger percentages of cases scoring above low cut scores. Unlike the chi-square and standard deviation indices, this index also was useful for assessing the potential operational impact of using the form. By comparing the percentages for a composite on a new form with the corresponding percentages on the reference form ( 15 h ), the accuracy of the equating to the reference form could be evaluated in an operationally relevant metric. By comparing the percentages for a composite on a new form with the corresponding percentages on the current operational form ( 15 g ), it was possible to estimate the operational impact of a transition from the current operational form to an implementation of the new form.

## Comparison with Reference and Current Operational Forms

The first step in comparing the distributions of each composite for the equated new forms with its distributions for the reference form and the current operational form was to compute a Pearson chi square measuring the independence of composite score categories and test forms. This was based on an mx 8 frequency table with cells containing the number of cases in each of the m cut-score categories for each of eight test forms ( $20 \mathrm{a}, 20 \mathrm{~b}, 21 \mathrm{a}, 21 \mathrm{~b}, 22 \mathrm{a}, 22 \mathrm{~b}$, the reference form [ 15 h ] and the current operational form [15g)]. The resulting chi-squares, degrees of freedom ${ }^{9}$ and probability values are shown in the first part of Table 13; the table also indicates which of the chi-squares was more than two times its degrees of freedom - a conservative criterion, in that it is less likely to be exceeded by chance as the degrees of freedom become large. Fifteen of the 30 composites -- including the AFQT -- had chi-squares that were statistically significant at alpha $=.05 ; 8$ of the 15 had chi-squares that were more than two times their degrees of freedom. The second part of Table 13 supplements the first part of the table by showing chisquares and degrees of freedom for the comparison of each new form and the current operational form with the reference form. The results in the two parts of this table clearly suggested that many composites did not have the same distributions across the new forms, reference form and current operational form. The results did not, however, indicate the nature or practical importance of the differences.

The second step in comparing the eight forms' distributions of each composite was to examine the standard deviations of the composite across the ASVAB forms. Table 14 shows these for all composites and for all ASVAB forms used in this study. As expected from the pattern of correlations between the subtests, the two composites containing both GS and AS -- Air Force G and Army GM -- had lower standard deviations on each of the new forms than on the reference form, 15h; for the Air Force $\mathbf{G}$ composite -- which double-weights AS -- it was as much as 1.47 lower. Because the equated subtests had essentially the same standard deviations on all forms, the lower standard deviations for composites on the new forms were due to the lower correlations between GS and AS on the new forms than on the

[^6]reference form. (See Table 11.) However, this pattern was only somewhat sustained in comparisons of the new form with the current operational form, 15 g ; each of these two composites had notably lower standard deviations on only two of the new forms (21a and 21 b ) than on 15 g . This, too, can be attributed to the correlations between GS and AS, which were notably lower than 15 g only for forms 21 a and 21 b .

Another pattern in the standard deviations in Table 14 was in the composites of subtests used in the AFQT -- VE, AR, and MK. These five composites are AFQT, Army GT and CL, Air Force G, and Navy GT. As expected from the pattern of lower correlations between these subtests for ASVAB 21b, these five composites had lower standard deviations on ASVAB 21b than on either the reierence form or the current operational form.

The third step in comparing the eight forms' distributions of each composite was to examine the percentages of cases exceeding each operational cut point. Appendix $G$ shows a table of these percentages for each of the 30 operational composites listed in Table 12. The top of each table in Appendix G shows the percentage of cases at or above each of the cut points for each of the eight ASVAB forms used in this study; the bottom of each table shows the percentage for each form minus the percentage for the reference form, 15 h . For each cut point on the AFQT composite, the percentage above the cut point for each of the new forms was within 1.00 of the percentage for the reference form and within 2.00 of the percentage for the current operational form. The largest of these differences were between the Category-I percentages for new forms 20b, 22a, and the current operational form. In contrast to what was expected from the pattern of subtest intercorrelations and composite standard deviations, ASVAB 21b did not show the lowest percentages of all forms in the highest categories of this composite, or the highest percentages in the lowest category.

Although the pattern in the percentages of cases in the AFQT categories did not show the expected differences across forms, the percentages for the Air Force M composite did show the expected pattern. As was the case for that composite in the IOT\&E of ASVAB 18/19 (Bloxom and McCully, 1992, Appendix G), all of the new forms had smaller percentages than the reference form in the highest score category and larger percentages than the reference form in the lowest score category; this would be expected from the lower standard deviation of the composite for the new forms than for the reference form.

In comparing the percentages across forms in Appendix G, it is important to consider how much the percentages can vary due to sampling variability. Although confidence intervals were not provided here, an indication of this variability was provided by the results for the Air Force M composite. In that composite, like-numbered new ASVAB forms (20,21, and 22) used the same items for all three subtests in this composite; thus, differences in percentages between the results for the $\mathbf{a}$ and $\underline{\mathbf{b}}$ versions of each form were attributable to variation in the samples of cases for those versions. Across the six score categories and three ASVAB forms, more than two-thirds of the percentages differed by at least .7 and more than one-third of the percentages differed by at least 1.0. In view of this variability, the magnitude of differences obtained between new forms and the comparison forms ( 15 g and 15 h ) of the AFQT was not greater than would be expected from sampling variation; however, nonrandom patterns of small differences may have been present.

## Comparison with IOT\&E Results of Other ASVAB Forms

Comparison with IOT\&E of ASVAB 15, 16 and 17. To provide a another benchmark for evaluating the comparisons with the reference form in the present study, Table 15 provides the composite-category-by-test-form chi-squares for the ASVAB 15/16/17 IOT\&E data, based on the use of
the conversion tables obtained from that same data set. Twenty-nine of the 33 chi-squares -- including that of the AFQT -- were statistically significant with alpha $=.05$. Also, 22 of the 33 chi-squares were more than two times as large as their degrees of freedom, with the AFQT chi-square being nearly four times its degrees of freedom. The composite having a chi-square that was the largest multiple of its degrees of freedom was Army MM. For that composite, the percent of cases in the lowest category was from 0.0 to 1.6 less for forms $15 / 16 / 17$ than for the reference form, and the percent of cases in the highest category was from .9 more to 2.0 less for the new forms than for the reference form. In general, this pattern of results indicated that equal or larger differences existed between forms in the IOT\&E of ASVAB 15/16/17 than in the present study.

In the IOT\&E of ASVAB 15/16/17, the new-form distributions of composites containing AS -not GS -- differed systematically from the corresponding distributions in the reference form. All ten compsites containing AS had chi-squares that were statistically significant; nine of these had chi-squares that were more than two times their degrees of freedom. Also, the standard deviations of composites containing AS (see Table 16) were consistently smaller for ASVAB 15/16/17 than for the reference form. For the Air Force M composite, which contains GS and gives AS twice the weight of other subtests, the largest departure of the standard deviations in ASVAB 15/16/17 from the standard deviation in the reference form was $\mathbf{7 6}$ (ASVAB 15a in Table 16); for forms 20/21/22 in the present study, the largest difference for this composite was 1.47 (ASVAB 21b in Table 14). These results were consistent with expectation from results reported by Wise, Nicewander, and Bloxom (1991), who found the correlations of AS with other subrests were an average of .06 lower for forms $15 / 16 / 17$ than for the reference form. Thus, differences in subtest intercorrelations were affecting standard deviations and other distributional indices of composites in the IOT\&E of ASVAB 15/16/17 as well as in the present sudy.

In addition to these systematic differences between standard deviations for forms in the IOT\&E of ASVAB 15/16/17, there were nonsystematic differences (in the AFQT distributions) that were of a similar order of magnitude as those obtained in this study. The AFQT standard deviations of new forms ranged from .26 below the reference form to .26 above the reference form in that study (Table 16 ). In the present study, the standard deviations of the new forms ranged from .16 below the reference form to .40 ahove the reference form (Table 14).

Comparison with IOT\&E of ASVAB 18/19. To provide yet another benchmark for evaluating the comparisons with the reference form in the present study, results reported by Bloxom and McCully (1992) included the composite-category-by-test-form chi-squares for the ASVAB 18/19 IOT\&E data, based on the use of the conversion tables obtained from that same data set. Fourteen of the 33 chi-squares - not including that of the AFQT -- were statistically significant with alpha $=.05$. Also, seven of the 33 chi-squares were more than two times as large as their degrees of freedom. The composite having a chisquare that was the largest multiple of its degrees of freedom was Air Force M, with a chi-square over seven times its degrees of freedom. For that composite, the percentage of cases in the lowest category was from 1.4 to 2.0 less for the new forms than for the reference form, and the percentage of cases in the highest category was from 2.3 to 3.3 less for the new forms than for the reference form. In general, this pattern of results indicated that at least some differences between forms in the IOT\&E of ASVAB $18 / 19$ were of the same order of magnitude as differences between forms in the present study.

In addition to these differences between the frequency tables for forms in the IOT\&E of ASVAB 18/19, there were differences in the standard deviations of AFQT distributions that were of the same order of magnitude as those obtained in this study even though the chi-square comparison of AFQT distributions was not statistically significant in the IOT\&E of ASVAB 18/19. The AFQT standard deviations of new forms in that study ranged from .01 above the reference form to .41 above the
reference form in that study (Table 17). In the present study, the standard deviations of the new forms ranged from .16 below the reference form to .40 above the reference form (Table 14). Also, the newform standard deviations of the Air Force $M$ composite were as much as 1.36 below the reference-form standard deviation in the IOT\&E of ASVAB 18/19; in the present study, the Air Force M new-form standard deviations were as much as 1.47 below the corresponding reference-form standard deviation.

## Comparison of Results for Three Subsets of the Data

The preceding sections reported comparisons of distributions of equated new forms with the distribution of the reference form. These analyses provided an assessment of the precision of the computations of equatings and conversion tables and an assessment of the effects of variation in the covariance structure across ASVAB forms. However, the analyses did not indicate the extent to which the equatings -- and the consequent conversion tables and distributions of composites -- were specific to the samples used for the equating. Of particular concern in this study was the possibility of effects of nonequivalent groups, due to the incompletely spiralled administration of test forms. An earlier section of this paper showed that the administration of test forms was not confounded with gender, race, or education. However, to the extent that some nonequivalence of groups was introduced by incomplete spiralling of administration, group differences in aptitude could have been confounded with test-form differences. If this happened, percentile-equivalent scores on different forms could represent different levels of aptitude.

To estimate the effect of incomplete balancing of test-form administration, three subsets of data were selected to simulate various amounts of balancing across data sets. In each set, the composite distributions for the equated new forms were then compared with the corresponding composite distribution for the reference form. To the extent that the match to the reference form distribution was equivalent across the three data sets, it could be inferred that the equating of composites was robust to -i.e., invariant across -- at least the simulated amount of variation in balancing.

The three data sets used in this analysis were sequentially nested subsets of each other. The first data set consisted of all initial-test cases, with no removal of cases from severely imbalanced sessions or sites; as indicated in the second column of Table 2, this provided from 13,007 to 15,959 cases per test form. The second data set consisted of all cases used in the development of the equating and conversion tables contained in this report, i.e., excluding the cases from severely imbalanced sessions and sites; as indicated in the third column of Table 2, this provided from 10,986 to 13,312 cases per test form. The thard data set consisted of cases further selected by the procedures for creating "strongly balanced samples," as described in Appendix A; this provided 7497 cases per test form.

Table 18 shows the results of applying the conversion tables developed in this report to obtain the AFQT-category distribution for each of the new test forms; the top, middle, and bottom sections of the table show the results for the first, second, and third data sets, respectively. As in Appendix G, the percentage of cases at or above the cut score for each category is listed separately for the reference form ( 15 h ). For each of the other forms, the percentage above each cut score is contrasted with the corresponding percentage for the reference form ( 15 h ) in the same data set; also included for comparative purposes is a contrast of the current operational form $(15 \mathrm{~g})$ with the reference form.

An inspection of the three AFQT category distributions in Table 18 indicated that the first two samples differed very little in AFQT, with percentages differing by no more than .25. It also indicated that the third sample did have a somewhat higher AFQT distribution, with percentages differing from the first two samples by as much as 2.00 for some categories. However, the contrasts of the other forms'
distributions with the reference form distribution did not vary by more than .63 percentage points across the three samples; variation that large was the exception rather than the rule. Furthermore, an inspection of the pattern of differences between samples revealed nothing indicative of an effect of editing (i.e., systematic variation of contrasts across samples).

Tables 19 and 20 show the results of the same kinds of analyses as in Table 18. Table 19 shows comparisons with the reference form for the Air Force $\mathbf{M}$ composite. Table 20 shows comparisons with the reference form for the Army GM composite. These two composites were analyzed here because each uses both the AS and GS subtests; this makes them relatively sensitive to changes in distributions across test forms where those changes are due to changes in the AS-GS correlation. In general, contrasts of the other forms' distributions with the reference form distribution did not vary by more than .61 and .86 percentage points across the three samples for the M and GM composites, respectively; and variation that large was the exception rather than the rule. Furthermore, an inspection of the pattern of differences between samples revealed nothing indicative of an effect of editing.

## Recommended Conversion Tables

On the basis of the results of this study -- including comparisons of these results with previous IOT\&E studies and comparisons across data sets simulating various amounts of balancing of test administration -- it was recommended that conversion tables obtained from the equipercentile equatings in the present study be implemented operationally. These tables are presented in Tables 21-26 and contain rounded and truncated values from Appendix $\mathbf{F}$.

## Summary and Conclusions

In October 1993, the Department of Defense planned to begin using ASVAB 20, 21, and 22 in the Enlistment Testing Program. This necessitated equating these forms to the reference form, ASVAB 8a (aka. ASVAB 15h). The results of this study indicated that equipercentile equating of subtests on the new forms to subtests on the reference form resulted in equatings of composites on the new forms that were comparable in accuracy to equatings obtained on previous operational ASVAB forms -- ASVAB 15/16/17 and ASVAB 18/19. The results also indicated that the accuracy of the equatings did not vary as a function of unbalanced form administration, to the extent that such administration could be simulated by editing the data. However, it should be noted that, on some composites other than the AFQT, there were systematic departures from the distributions provided by the reference form. Composites containing the GS subtest in combination with technical subtests -- most notably AS -- tended to have smaller standard deviations on the new forms. Additional analyses showed this also to be true for the subtest equatings currently used operationally with ASVAB 15/16/17 and with ASVAB 18/19. The problem is that the reference form contains some subtests -- most notably, GS -- that are more highly correlated with other subtests than is the case for the ASVAB forms developed in recent years.

Because the results of equating ASVAB 20, 21, and 22 to the reference form showed patterns similar to results previously obtained for equatings of operational ASVAB forms, this study provided a set of conversion tables (Tables 21-26) that were recommended for operational use.

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## Appendixes

## Appendix A:

## Procedure for Balancing Sample Sizes Across ASVAB Forms

Current procedures for operational administration of the ASVAB in an Initial Operational Test and Evaluation (IOT\&E) do not result in equal numbers of examinees being administered each of the ASVAB forms, i.e., the test forms are not spiralled within and across test sessions. Although the resulting variation in sample size does not appear to be directly related to the MEPS region, the week or month of testing, or the examinee's Gary $\mathbf{L}$. Thomasson or education, it may still result in a calibration that is specific to the mixture of populations in the IOT\&E data collection and not to the population of military applicants under normal operational conditions, when more nearly equal numbers of examinees are administered each of the ASVAB forms. Furthermore, if the aptitude distribution varies across forms as a result of the lack of spiralling, the calibration cannot be viewed as an equating of the forms.

In an effort to obtain balanced samples from an unbalanced IOT\&E data set, cases were deleted from various combinations of test forms, testing groups (defined by site and four-week period of testing) and demographic groups (defined by gender, race, and education). Testing groups and demographic groups were used as control variables during the deletion of cases because of their potential relationships to the aptitude distribution. Not controlling these variables during the deletion of cases could introduce -or exacerbate -- either random or systematic differences in aptitude distributions across test forms.

A major constraint in the balancing of samples was the requirement that the sample size for each form not be reduced below the sample size for the form used least frequently. The purpose of this constraint was to obtain balancing while deleting as few cases as possible. The first application of the constraint was at the level of the overall sample, i.e., such that the sample size for each form not be reduced below the sample size of the form used least frequently in the overall sample. In this study, the form used least frequently overall was ASVAB 22b. This form was, therefore, designated as the "target" form for balancing at the level of the overall sample. Cases for the other seven forms were deleted to provide sample sizes the same as for the target form. Because this resulted in the least loss of data, the resulting samples were called weakly balanced samples.

The second application of the balancing constraint was at the level of the testing-group sample, i.e., such that the sample size for each form in a testing group (defined by test site and four-week period) not be reduced below that of the form used least frequently in that testing group. Thus, the "target" form could vary from site to site and from period to period within a site. Because this target form was, for some testing groups, a form used less frequently than ASVAB 22b, the result was a greater loss of data than when ASVAB 22b was the target form for all groups. Thus, the resulting samples were called strongly balanced ramples.

Weakly Balanced Samples. To specify the deletion procedure for the weakly balanced samples, let $t=1, \ldots, T$ denote the index of testing groups and $d=1, \ldots, D$ denote the index of demographic groups. Then let $\mathrm{m}_{\mathrm{d}}$ be the target form's sample size for testing group t combined with demographic group d, and let $m$.. be the target form's marginal sample size over all testing groups and demographic groups. Similarly, let $\mathrm{n}_{\mathrm{djj}}$ and $\mathrm{n}_{. . \mathrm{j}}$ be the td-conditional and marginal sample sizes of ASVAB form $j$, where $j$ is a form other than the target form.

The object of the deletion procedure was to delete $n_{. j}-m_{\text {.. }}$ cases for form $j$. If the TD differences $n_{d d j}-m_{d d}$ were all non-negative, then deleting $z_{d d j}=n_{d j}-m_{d 山}$ cases from group td for each of the TD groups would result in $n^{*}{ }_{\Delta j}=n_{\text {dj }}-z_{\text {uj }}=m_{d d}$ cases for form $j$ for each of the TD groups and would meet the objective of obtaining $\mathrm{n}^{*}{ }_{. j}-\mathrm{m}_{. .}=0$.

However, it became known that some $n_{d j}-m_{v d}<0$, i.e., that the target form was used more than form j in some groups. It was therefore necessary to define $\mathrm{z}_{\mathrm{dj}}=0$ for those groups. (Cases could not be added for form $\mathbf{j}$.) This, in turn, would result in the sum of the $\boldsymbol{z}_{. j}>\mathrm{n}_{. \mathrm{j}}-\mathbf{m}$. To obtain balancing in this situation, the number to be deleted from each group was not $\boldsymbol{z}_{\text {djj }}=n_{\text {djj }}-m_{d d}$; instead it was a smaller number, $d_{d j}=a_{j} z_{d j j}$, where the scale factor $a_{j}=\left(n_{. j}-m_{. .}\right) / z_{\text {.j }}<1 .{ }^{10}$ Summing the $d_{d j}$ across the TD groups then yielded the total number of deletions for form $j, d_{. j}=a_{j} \mathbf{z}_{. j}=\left[\left(n_{. j}-m_{. .}\right) /\right.$ $\left.\mathbf{z}_{. j}\right]\left[\mathbf{z}_{. j}\right]=\left(n_{. j}-m_{\text {. }}\right)$, which was the number of deletions required to obtain balanced samples.

For each form j , cases could be deleted from the TD groups by either of two approaches. The first was random sampling from a uniform distribution, with a deletion threshold determined by the probability of deletion, $\mathrm{p}_{\mathrm{udj}}=\mathrm{d}_{\mathrm{ddj}} / \mathrm{n}_{\mathrm{udj}}$. The second was systematic deletion of one out of every $\mathrm{n}_{\mathrm{uj}} / \mathrm{d}_{\mathrm{dj}}$ cases ${ }^{11}$, using a selected ordering of the cases in the data file. The latter approach was used in this study to better stratify cases by test session and by SSN within test session, the two variables that determined the ordering of cases within groups in the file. Because aptitude distributions tend to vary by date of testing, it was assumed that this would introduce less random variation in the aptitude distribution than would random sampling of cases to be deleted.

The result of applying this procedure in this study -- along with edits of retesters, extreme departures from balancing, and cases with all scores equal to zero -- was to obtain 10,986 cases for each ASVAB form, the number of cases that were obtained for ASVAB 22 b before the procedure was used.

Strongly Balanced Samples. To specify the deletion procedure for the strongly balanced samples, again let $\mathrm{t}=1, \ldots, \mathrm{~T}$ denote the index of testing groups and $\mathrm{d}=1, \ldots, \mathrm{D}$ denote the index of demographic groups. Then let $m_{d d}$ be the target form's ${ }^{12}$ sample size for testing group $t$ combined with demographic group $d$ and $m_{l}$ be the target form's marginal sample size over all demographic groups for testing group $t$. Similarly, let $n_{\mathrm{ddj}}$ and $\mathrm{n}_{\mathrm{t}, \mathrm{j}}$ be the td-conditional and t -conditional sample sizes of ASVAB form j , where j is a form other than the target form.

[^7]The object of the deletion procedure for each testing group $t$ was to delete $n_{2, j}-m_{2}$ cases for form $j$. If the $D$ differences $n_{\mathrm{vj}}-m_{\mathrm{vd}}$ were all non-negative, then deleting $z_{\mathrm{udj}}=n_{\mathrm{dj}}-m_{\mathrm{sd}}$ cases from group id for each of the $D$ groups would result in $n^{*}{ }_{\text {dij }}=n_{d d j}-z_{d j}=m_{d d}$ cases for form $j$ for each of the $D$ groups and would meet the objective of obtaining $\mathrm{n}_{\mathrm{t}, \mathrm{j}}-\mathrm{m}_{\mathrm{l}}=0$.

It was expected, however, that some $n_{\text {uj }}-m_{d d}<0$, i.e., that the target form was used more than form j in some demographic groups. It was then necessary to define $\mathrm{z}_{\mathrm{udj}}=\mathbf{0}$ for those groups. (Cases could not be added for form $j$.) This, in turn, would result in the sum of the $z_{i, j}>n_{1 . j}-m_{1 .}$. To obtain balancing in this situation, the number to be deleted from each group was not $\boldsymbol{z}_{\text {dj }}=n_{\text {dj }}-m_{d d}$; instead it was a smaller number, $d_{d j}=a_{i j} z_{d j}$, where the scale factor $a_{i j}=\left(n_{i j}-m_{i}\right) / z_{i j}<1$. Summing the $d_{d j}$ across the $D$ groups then yielded the total number of deletions for form $j, d_{i, j}=a_{i j} z_{i, j}=\left[\left(n_{i, j}-m_{1}\right) / z_{i, j}\right.$ $]\left[z_{i, j}\right]=\left(n_{1, j}-m_{1}\right)$, which was the number of deletions required to obtain balanced samples.

The procedure for using $\mathrm{d}_{\mathrm{dj}}$ to delete cases from each of the TD groups for strongly balanced samples was the same that used to delete cases for the weakly balanced samples. The result of applying this procedure in the present study -- along with edits of retesters, extreme departures from balancing, and cases with all scores equal to zero -- was to obtain 7497 cases per form.

## Appendix B:

## Alternative Methods of Equating

When equating new-form subtests, so their right-number scores will be on the same score scale as on the reference form, several approaches can be considered. The primary approaches discussed here comprise the following methods of equating: random-groups linear equating, random-groups equipercentile equating, matched-groups linear equating, and matched-groups equipercentile equating. True-score equating is not included here, because of the lack of research and experience related to equating from an item response theory for speed tests, which are two of the ten subtests of the ASVAB. Summary descriptions of these five approaches are provided in Angoff (1971); Braun and Holland (1982); Peterson, Kolen, and Hoover (1989); Kolen and Brennan (1990); and Dorans (1990).

Even though a randomly-equivalent-groups design is typically used for ASVAB equating-data collection, matched-groups equating methods can be considered when the subjects are military recruits. These methods potentially can control for whatever random differences occur between groups. The matching variable in this case would be the pre-enlistment ASVAB score on the subtest being equated. Any association of this score with the score on the test being equated could potentially be exploited to improve the precision of the equating.

In spite of this theoretical advantage of matched-groups equating, the approach is not considered for equating forms of the ASVAB. When forms are being administered operationally (in an IOT\&E) to collect equating data, a separate matching variable is not available, unlike when forms are being administered to military recruits. Even when equating data are being collected from recruits -- in which case pre-enlistment scores are available -- using these scores to obtain a more precise equating has not yet been demonstrated. The problem is that the matching variable (pre-enlistment ASVAB) is a measure taken, in some cases, two years prior to the test being calibrated, and under different motivational conditions. This is in contrast to conventional matched-groups equating in which the matching variable is a measure taken in close temporal proximity to, and under similar motivational conditions as, the test being calibrated. Systematic influences between the measurement of the matching variable and the test being calibrated include substantial selection ( $50 \%$ for military enlistment), learning (during the final year of secondary education), and motivational changes (from operational to non-operational conditions of administration). This, plus the highly skewed -- in the case of NO, monotonic -- distributions of ASVAB subtests, make it difficult to assume that the results of previous studies of matched-groups equating (e.g., see Dorans [Ed.], 1990) generalize to the present context. However, there is a need for ASVAB studies of matched-groups equating -- e.g., using the evaluation design employed by Divgi (1988) -- so that any improvements obtainable by this approach could be exploited in future calibrations.

Random-groups linear equating and random-groups equipercentile equating are methods that have been used for equating new forms of the ASVAB. Also, both approaches were used in an answer-sheet calibration study by Ree and Wegner (1990). Divgi (1988a) compared linear and equipercentile equatings from recruit samples and, for each approach, found some subtests in which the approach provided the best prediction of equating in large samples of military applicants. However, Divgi (1988b) found that for sample sizes closer to those used in an IOT\&E data collection, linear equatings do not replicate as well as equipercentile equatings.

Equipercentile equating usually employs some form of smoothing, either the test distributions or the equating function, in an effort to reduce the sampling variance of the equating function. Three criteria
guide the choice between alternative smoothing methods for use in equipercentile equating. The first criterion is that the method be symmetric, so that the equating can serve as a basis for converting scores on either test form to the score scale provided by the other test form; this is a criterion that has been advocated by Lord (1980); Peterson, Kolen, and Hoover (1989); and Dorans (1990) in support of the idea of interchangeability of equated test forms. The second criterion is that the method of estimating score distributions use a statistical measure of fit to the distributions of scores on the two test forms. The third criterion is that there be a sequence of distributional models, differing primarily in their number of parameters; the objective here is to choose the model with the smallest number of parameters to reduce sampling variability in the estimator of the equating function.

Equipercentile equating based on smoothed distributions, instead of using smoothed equating functions, can be developed in a way that satisfies these three criteria. This approach -- termed presmoothing (Fairbank, 1987) -- provides a symmetric equating by independently smoothing the distribution of scores obtained from each test form instead of risking the regression effects associated with smoothing the equating function directly.

By basing the equating on log-linear-smoothed distributions, the method also provides a statistical measure of fit to the distributions. The smoothing employs the method of maximum likelihood to fit polynomials to the logarithm of the frequency distributions, in a manner suggested by Holland and Thayer (1987). This method is implemented by a computer program (Hanson, 1990), which provides a chi-square fit statistic for polynomials with as many as ten terms.

By basing alternative equatings on a sequence of log-linear-smoothed distributions, it is possible to select an equating obtained from the smallest number of parameters without jeopardizing the fit of the model to the data. The procedure is to obtain as many terms in the polynomial as are necessary to provide a good statistical fit to the non-null bins of a distribution. Sampling variability is then reduced by excluding all terms with a power higher than ten and all other high-order terms that do not improve the fit. (See example of results in Appendix C.) The method has an added advantage of exactly preserving as many moments of a distribution as there are powers of $x$ in the polynomial. Although equipercentile equating is not defined in terms of preserving the moments of a distribution, knowing that the first several moments are preserved provides another check on the extent to which the distribution is preserved. Of course, exactly fitting the first few moments of a distribution is a desideratum only in samples of the size used in equating studies; in smaller samples, this would result in an overfitting -particularly of the higher moments of the distribution.

## Appendix C:

Log-Linear Smoothing of ASVAB Subtest Distributions From the Operational Calibration of ASVAB 15, 16, and 17

Lower/Upper Bounds (Up to 10) of Polynomial Degree Producing Statistically Significant* Improvement in Likelihood-Ratio Chi-Square

| ASVAB Form |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Subtest | $15 a$ | $15 b$ | $15 c$ | $16 a$ | $16 b$ | $17 a$ | $17 b$ |
| GS | $6 / 6$ | $6 / 6$ | $2 / 6$ | $2 / 4$ | $2 / 8$ | $4 / 4$ | $6 / 9$ |
| AR | $4 / 4$ | $4 / 10$ | $4 / 4$ | $3 / 8$ | $4 / 6$ | $4 / 4$ | $4 / 4$ |
| WK | $5 / 8$ | $6 / 6$ | $3 / 10$ | $4 / 4$ | $3 / 6$ | $2 / 10$ | $3 / 8$ |
| PC | $5 / 5$ | $6 / 9$ | $4 / 4$ | $4 / 10$ | $4 / 7$ | $4 / 4$ | $5 / 5$ |
| NO | $4 / 9$ | $4 / 6$ | $5 / 8$ | $4 / 8$ | $4 / 9$ | $4 / 8$ | $4 / 8$ |
| CS | $5 / 5$ | $5 / 5$ | $5 / 7$ | $5 / 7$ | $5 / 5$ | $5 / 10$ | $5 / 7$ |
| AS | $5 / 5$ | $4 / 4$ | $6 / 6$ | $4 / 4$ | $6 / 6$ | $4 / 4$ | $4 / 6$ |
| MK | $4 / 4$ | $4 / 7$ | $4 / 10$ | $4 / 8$ | $4 / 8$ | $5 / 5$ | $4 / 4$ |
| MC | $2 / 4$ | $2 / 9$ | $4 / 7$ | $2 / 4$ | $2 / 4$ | $2 / 5$ | $2 / 4$ |
| EI | $5 / 5$ | $5 / 5$ | $2 / 4$ | $4 / 4$ | $4 / 4$ | $4 / 10$ | $4 / 4$ |
| VE | $8 / 8$ | $6 / 6$ | $4 / 6$ | $4 / 6$ | $6 / 10$ | $2 / 6$ | $4 / 4$ |

* Alpha $=.05$ with d.f. $=1$ Lower bound is the number of terms including and below which each produces a statistically significant improvement in the fit to the data. Upper bound is the highest-numbered term that produces a statistically significant improvement in the fit to the data; some lower-numbered terms may not produce a significant improvement in the fit.


## Appendix D:

## Estimation of the Lower Tail of the Subtest Cumulative Distribution for Equipercentile Equating

Let $F_{i}$ be the proportion of the population at or below test score $i, i=0, \ldots, m$, where $m$ is the number of items in the test.

Let $f_{i}$ be the proportion of a population of subjects at test score $i$, or $f_{i}=F_{i}-F_{i-1}$
Let $u$ in $0<u<m$ be the lowest (integer) score above $j$, such that $F_{j} .005$.
Let the estimated

$$
\begin{equation*}
F_{i}=[(i+1) /(u+1)]^{c} F_{u}, \tag{1}
\end{equation*}
$$

where c is chosen to preserve the slope of $\mathrm{F}_{\mathrm{i}}$ over the interval ( $\mathbf{u}-1, \mathrm{u}$ ). Then

$$
\begin{equation*}
c=\ln \left[1-f_{u} / F_{u}\right] / \ln [u /(u+1)] . \tag{2}
\end{equation*}
$$

Proof:
If $i=u$, then $[(i+1) /(u+1)]=1$ and $F_{i}=F_{u}$ in (1).
If $i=u$, then, from (1), $F_{u-1}=[u /(u+1)]^{c} F_{u}$ and $f_{u}=F_{u}-F_{u-1}=F_{u}-[u /(u+1)] c F_{u}$ $=F_{u}\left\{1-[u /(u+1)]^{\prime}\right\}$.

Dividing by $\mathrm{F}_{4}$, transposing terms, and taking logarithms yields
c $\ln [u /(u+1)]=\ln \left[1-f_{u} / F_{u}\right]$.
Dividing by $\ln [\mathbf{u} /(\mathbf{u}+1)]$ yields (2).

## Appendix E:

## Choosing Between Alternative Equatings

In their discussion of evaluating an observed-score equating, Braun and Holland (1982) stated that, if there exists a population for which the reference-form distribution differs from the equated new-form distribution, then the forms have not been equated. This implies two metrics in which equatings can be compared. The first is the score metric, in which the (cumulative) frequency is held constant and equated scores are compared. This is a type of comparison often used in a close study of alternative equatings, e.g., to see how different a linear equating is from an equipercentile equating. If various equatings provide similar equated scores, they are considered equally acceptable from the perspective of the examinee.

The second metric implied by Braun and Holland is the frequency metric, in which the score is held constant -- e.g., at integer values on the reference form -- and the cumulative distributions of the equated scores and reference form scores are compared. This is a type of comparison used to assess whether implementing an equated new form will change the score distributions, e.g., to see if there will be a change in the percent of persons qualifying for employment. If various equatings have no effect on the score distributions, they are considered equally acceptable from the perspective of the employing institution (Sympson, 1985).

Two criteria can be used to assess differences between the alternative equatings in the score metric. The first criterion is the root mean squared difference between a pair of equatings, with the difference at each score level weighted by the proportion of cases at that level on the new test form. The second criterion is the proportion of cases (from the new-test-form distribution) for which the two equatings differ by more than .5 standard score points (Department of Defense, 1988). The first criterion is an index of the algebraic difference berween two sets of equated scores. The second criterion is an indicator of the practical impact of using one equating instead of the other.

Two criteria can be used to assess differences between alternative equatings in the frequency metric. The first criterion is the root mean squared difference between the cumulative distribution of equated scores (after linear interpolation at integer scores on the reference form) and the cumulative distribution of scores on the reference form, with the difference at each score level weighted by the proportion of cases at that level on the reference form. The second criterion is the proportion of cases (from the reference form distribution) for which the cumulative proportions differ by more than $\mathbf{0 1}$. The first criterion is an index of the algebraic difference between the equated-score and reference distributions. The second criterion is an indicator of the practical impact (on the score distribution) of using the equated new test form instead of the reference form.

When two or more methods of equating are being considered for operational use, a procedure for choosing between them is to use the two root-mean-squared-difference indices (in the score metric and in the frequency metric) to select the equating with the best fit to the raw equipercentile equating. Then, the two indices of impact (in the score metric and in the frequency metric) can be used to assess whether an equating with fewer parameters could be employed without having a practical consequence for the equated scores or their cumulative distribution.

The following heuristics implement this procedure for selecting an equating for ASVAB subtests. They specify cutting points on the indices employed to compare equatings. The cutting points
have been chosen from a visual inspection of the results of applying them to the data from the OPCAL of ASVAB 15, 16 and 17. (See Appendix C for results of fitting the log-linear model to the distributions from this data set.) In choosing the points, an effort was made to provide some choice between alternative equatings where it seemed reasonable to have a choice, e.g., where two equatings with differing numbers of parameters provided visually similar equatings and visually similar equatedscore distributions. An advantage of using cut points as specific as these is that the selection procedure can be replicated and evaluated. A disadvantage of this approach is that the cutting points based on a study of military recruits may not result in the selection of the best equating for population of military applicants, in which equatings are be used. More research is required to assess the inferential validity of the cutting points for selecting the most approprate equating to use in an applicant population. Until such research provides further reassurances about these cutting points or provides more defensible alternatives, the last step, (e), in the hexristics provides a necessary confirmation that the selected equating is accurate at least for the sibtest and sample in which the equating was developed.

The heuristics are:
(a) Select the smooth equating that minimizes the root-mean-squared-discrepancy between the smooth equating (linear or smoothed-equipercentile) and the raw equipercentile equating; then,
(b) Compare the smooth equating from (a) with other smooth equatings that use fewer parameters; select the equating with the fewest parameters if it reduces the root-meansquared-discrepancy in the frequency metric by at least $10 \%$ without increasing the root-mean-squared-discrepancy in the score metric by more than $10 \%$; if no such alternative smooth equating exists, use the selection from (a) as the best-fitting alternative; then,
(c) Compare the equating selected in (b) with other smooth equatings that use fewer parameters; find those equatings with fewer parameters that also differ from (b) by more than .5 standard score points for fewer than $10 \%$ of the cases; then,
(d) Select that equating from (c) that uses the fewest parameters and that results in fewer than $10 \%$ of the cases at scores where the equated cumulative distribution differs from the reference cumulative distribution by more than. 01 ; then,
(e) Graphically inspect the differences between an identity equating, a linear equating and any equipercentile equatings under consideration; also, graphically inspect the differences between the reference-form cumulative distribution and the distributions of equated scores based on the equipercentile equatings under consideration.

## Appenclx F:

Conversion of GS Row Teat Seores to 1990 Unroumded Standerd Seore Equivalems

| R"w | 156 | 203. | 208 | 218 | 218 | 273 | 227 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 17.91397 | 17.03452 | 17.83452 | 18.39998 | 18.39998 | 18.59734 | 18.59734 |
| 1 | 19.88265 | 19.79450 | 19.79450 |  |  | 20.64001 | 20.64081 |
| 2 | 21.7994 |  | 21.68181 | 22.45374 | 22.49374 | 22.77608 | 22.77608 |
| 3 | 23.69515 |  | 23.54909 | 24.50375 | 24.58375 | 24.94459 | 24.94459 |
| 4 | 25.5435 | 25.40510 | 25.40510 | 26.60083 | 26.68003 | 27.12610 | 27.12610 |
| 5 | 27.46995 | 27.25558 | 27.25558 | 20.7132 | 28.7132 | 29.22347 | 29.22347 |
| 6 | 29.52851 | 29.27368 | 29.27368 | 30.43061 | 30.43061 | 30.96139 | 30.96139 |
| 7 | 31.51705 | 31.19056 | 31.29056 | 31.97661 | 31. | 32.57831 | 32.57131 |
| 8 | 33.47853 | 33.06695 | 33.06695 | 33.53501 | 33.53501 | 34.22069 | 34.22069 |
| 9 | 35.44093 | 34.93524 | 34.93524 | 35.09428 | 35.09428 | 35.91191 | 35.91191 |
| 10 | 37.42388 | 36.84445 | 36.94445 | 36.54449 | 36.54449 | 37.62493 | 37.62493 |
| 11 | 39.43567 | 38.79329 | 38.79329 | 38.10338 | 38.10338 | 39.36369 | 39.36369 |
| 12 | 41.47170 | 40.77064 | 40.77064 | 39.76661 | 39.76661 | 41.12347 | 41.12347 |
| 13 | 43.51519 | 42.75737 | 42.75737 | 41.53483 | 41.53403 |  |  |
| 14 | 45.54170 | 44.73010 | 44.73010 | 43.40689 | 43.40689 | 44.62671 | 44.62671 |
| 15 | 47.52653 | 46.66711 | 46.66711 | 45.37355 | 45.37355 | 46.41800 | 46.41880 |
| 16 | 49.45260 | 48.55415 | 18.55415 | 47.41423 | 47.41423 | 48.23683 | 18.23683 |
| 17 | 51.31593 | 50.3086 | 50.38886 | 49.49942 | 49.49942 | 50.08934 | 50.00934 |
| 18 | 53.12736 | 52.18191 | 52.18194 | 51.59920 | 51.59920 | 51.99303 | 51.99303 |
| 19 | 54.92116 | 53.95665 | 53.95665 | 53.69433 | 53.69433 | 53.97224 | 53.97224 |
| 20 | 56.74766 | 55.74006 | 55.74806 | 55.70529 | 55.78529 | 56.05617 | 56.05617 |
| 21 | 58.65691 | 57.60411 | 57.60411 | 57.89665 | 57.89665 | 58.27118 | 58.27118 |
| 22 | 60.69924 | 59.58778 | 59.58778 | 60.07465 | 60.07465 | 60.62299 | 60.62299 |
| 23 | 62.90255 | 61.77491 | 61.77491 | 62.37291 | 62.37291 | 63.06665 | 63.06665 |
| 24 | 65.30792 | 64.23561 | 64.23561 | 64.81174 | 64.81174 | 65.69345 | 65.69345 |
| 25 | 67.81637 | 66.99136 | 66.99136 | 67.47499 | 67.47499 | 68.06579 | 68.06579 |

Conversion of AR Rew Teat Scores to 1900 Unrounded Stunded Score Equivalents

| 0 | 25.43686 | 25.36979 |  |  | 25.20033 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 26.78031 | 26.70698 | 27.72933 | 26 | 26.60916 | 26.64678 | 8 |
| 2 | 28.09621 | 28.00317 | 29.28587 | 28.18040 | 27.87906 | 27.92679 | 28.34267 |
| 3 | 29.40136 | 29.29338 | 30.93671 | 29.50812 | 29.22600 | 29.10653 |  |
| 4 | 30.70223 | 30.55723 | 32.47386 | 30.83345 | 30.36380 | 30.43819 | 31.08637 |
| 5 | 31.98745 | 31.85902 | 33.79089 | 32.19897 | 31.62381 | 31.88222 | 32.27819 |
| 6 | 33.26050 | 33.06552 | 35.03080 | 33.53691 | 32.74028 | 33.29365 | 33.43412 |
|  | 34.56800 | 34.10053 | 36.26829 |  | 33.91511 | 34.63283 |  |
| 8 | 35.89254 | 35.13634 | 37.50858 | 36.16024 | 35.12282 | 35.89346 | 35.82789 |
| 9 | 37.24618 | 36.20257 | 38.75630 | 37.44555 | 36.35047 | 37.09452 | 37.05790 |
| 10 | 38.60608 | 37.29906 | 40.02554 | 38.71169 | 37.59514 | 38.23470 | 38.32769 |
| 11 | 39.97323 | 38.42001 | 41.29090 | 39 | 38.06149 |  |  |
| 12 | 41.34256 | 39.59185 | 42.57647 | 41.22652 | 40.15968 | 40.65185 | 41.06309 |
| 13 | 42.70978 | 40.0476 | 43.07529 | 42.50435 | 41.5027 | 42 | 42.50789 |
| 14 | 44.07206 | 42.19338 | 45.18010 | 43.81010 | 42.90344 | 43 | 43.97500 |
| 15 | 45.42821 | 43.62146 | 16.49036 | 45.14369 |  | 44.79093 |  |
| 16 | 46.77152 | 45.11404 | 47.80404 |  | 45.90698 | 46.26124 |  |
| 17 | 48.12424 | 46.64264 | 49.12208 | 542 | 47.50812 | 47.73602 | 48.33643 |
| 18 | 49.46716 | 48.17759 | 50.44800 | 49.13990 | 49.16295 | 49.20187 | 49 |
| 19 | 50.80952 | 49.70475 | 51.78697 | 50.13115 | 50.85393 | 50.65908 |  |
| 20 | 52.15410 | 51.21412 | 53.14416 | 51.71141 | 52.56783 | 52.11801 |  |
| 21 | 53.50476 | 52.70677 | 54.52255 | 53.00125 | 54.20099 | 53.59063 | 53.74335 |
| 22 | 54.86678 | 4.19272 | 55.92007 | 54.32115 | 55.95052 | 55.07734 | 55.05410 |
| 23 | 56.24692 | 5.68706 | 57.32649 | 55.68107 | 57.56377 | 56.56141 | 56.36708 |
| 24 | 57.65227 | 57.20468 | 58.72204 | 57.07179 | 59.05227 | 58.01044 | 57.68737 |
| 25 | 59.08792 | 58.75322 | 60.08033 | 58.46702 | 60.39359 | 59.39129 | 59.01492 |
| 26 | 60.55314 | 10.32924 | 61.37740 | 59.8426 | 61.59141 | 60.69360 | 60.34549 |
| 27 | 62.03713 | 61.90186 | 62.60467 | 62.21830 | 62.68290 | 62.94729 | 61.67567 |
| 28 | 63.52013 | 63.43474 | 63.77926 | 62.66274 | 63.73081 | 63.22243 | 63.01344 |
| 29 | 64.96509 | 64.89890 | 64.95067 | 64.27496 | 64.82433 | 64.60675 | 64.40053 |
| 30 | 66.31626 | 66.27991 | 66.23377 | 66.02238 | 66.14606 | 66.12327 | 65.99026 |

Converaion of WK Raw Test Scores to 1990 Unrounded Sunderd Score Eqqivalemts

|  | 15 G | ${ }^{208}$ | 151 | 218 |  | 229 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 16.03719 | 16.42061 | 16.45135 | 16.13752 | 16.03736 | 16.01020 | 15 |
| 1 | 17.34762 |  | 17.61240 | 17.46021 |  | 17.32632 |  |
| 2 | 18.68217 |  | 19.21230 | 18.82903 |  |  |  |
| 3 | 20.02500 | 20 | 20.62226 | 20.21372 | 20.0253 |  |  |
| 4 | 21.37103 |  | 22.0707 | 21.6045 | 21.37 |  |  |
| 5 | 22.71858 | 23.50683 | 23.54458 |  | 22.71 |  |  |
| 6 | 24.06698 |  | 25.03578 | 24.36 | 24 |  |  |
| 7 | 25.41590 | 26.48174 | 26.53918 | 25 |  |  |  |
| 8 | 26.76514 | 27.95156 | 28.01707 | 27.1129 |  |  |  |
| 9 | 28.02004 | 29.28012 | 29.51118 | 28.5076 | 28.031 |  |  |
| 10 | 29.24157 | 30.5215 | 30.9839 | 29.9403 | 29.225 |  |  |
| 1 | 30.51196 | 31.75197 | 32.45045 | 31.3975 |  |  |  |
| 12 | 31.82764 | 32.97045 | 33.9202 | 32.860 |  | 32.6957 | 32 |
| 3 | 33.18597 | 34.1775 | 35.387 | 34.335 |  |  |  |
| 14 | 34.58174 | 35.37573 | 36 |  |  | 35.721 |  |
| 15 | 36.00494 | 36 | 38.250 | 37.189 | 36.160 | 37.152 | 91 |
| 16 | 37.41995 | 37.76136 | 39.60 |  |  |  |  |
| 17 | 38.82431 | 38.95742 | 40. |  | 39.340 |  | 39.69132 |
| 18 | $40.208: 7$ | 40.25970 | 42.10 | 41.092 |  |  | . 9 |
| 19 | 41.56:98 | 41.36914 | 43.2 | 42.292 | 42.2 | 42.243 |  |
| 20 | 42.87672 | 42.58503 | 44.34451 | 43. | 43.56 |  | 43. |
|  | 44.15449 | 43.80376 | 5 |  | 44.7782 |  |  |
| 22 | 45.39645 | 45.01115 | 46 | 45. | 45.92435 |  |  |
| 23 | 46.6069 | 46.22160 | 47.444 | 46.026 | 47.038 |  |  |
|  | 47.79195 | 47.4341 | 48.44385 | 7.92 |  |  |  |
| 25 | 48.95242 | 48.64892 | 49.45703 | 49.030 | 49.26 |  |  |
| 26 | 50.09425 | 49.86752 | 50.40311 | 50.1163 | 50.4124 |  |  |
| 989 | 51.24339 | 51.09315 | 51.51244 | 51.217 |  |  |  |
| 28 | 52.41285 | 52.33067 | 52.54118 | 52.347 | 52.7022 | 52. |  |
| 29 | 53.61668 | 58613 | 53.58092 | 53.5166 | 54.0026 | 1033 |  |
| 30 | 54.06014 | 86545 | 54.663 | 54.73662 | 55.236 |  |  |
| 11 | 56.17527 | 1718 |  | 56.0162 |  |  | 56.23187 |
| 32 | 57.53310 | 5u234 | 56.98862 | 57.3550 | . 75720 | . 5435 | 57.49922 |
| 3 | 58.91394 | 58.84276 | 58.31100 | 58.7343 |  |  |  |
|  | 60.25754 | 60.16239 | 59.76423 | 60.10782 | 3121 | 34 |  |
|  | 61.45923 | 61.40240 | 1.243 |  |  |  |  |

Conversion of PC Raw Teat Scores to 1980 Unrounded Stunderd Score Equivaleme

| Raw | 156 | $20 \lambda$ | 208 | 14 | 218 | 22A | 228 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 16.87800 | 17.74411 | 16.70272 | 16.57687 | 17.48701 | 16. | 17.91502 |
| 1 | 19.78418 | 20.86358 | 19.56573 | 19.40888 | 20.54316 | 19.74182 | 21.07657 |
| 2 | 22.61058 | 24.13180 | 22.30271 | 22.08167 | 23.68023 | 22.55099 | 24.43198 |
| 3 | 25.41758 | 27.43620 | 25.00905 | 24.71573 | 26.83699 | 25.33838 | 27.72301 |
| 4 | 28.21129 | 30.14343 | 27.68983 | 27.13869 | 29.69224 | 28.16565 | 30.18016 |
| 5 | 30.80825 | 32.83856 | 30.11776 | 29.44794 | 32.52641 | 30.93565 | 34.17280 |
| 6 | 33.27385 | 35.67195 | 33.01228 | 32.04753 | 35.44123 | 33.82882 | 37.37751 |
| 7 | 35.81754 | 38.63253 | 36.47500 | 34.95562 | 38.45369 | 36.86399 | 40.36013 |
| 8 | 38.57550 | 41.61454 | 40.14427 | 38.17095 | 41.47969 | 39.94501 | 43.15466 |
| 9 | 41.45566 | 44.470 | 43.81707 | 41.59641 | 44.42804 | 42.96623 | 45.61685 |
| 10 | 44.33192 | 47.16593 | 47.24736 | 45.10604 | 47.27934 | 45.89793 | 48.31809 |
| 11 | 47.19690 | 49.72706 | 50.33738 | 48.58468 | 50.06668 | 48.76685 | 50.20936 |
| 12 | 50.17183 | 52.28909 | 53.14200 | 51.94322 | 52.82528 | 51.60197 | 53.25720 |
| 13 | 53.37785 | 55.01109 | 55.80656 | 55.21571 | 55.57198 | 54.38467 | 55.76763 |
| 14 | 56.75338 | 58.00048 | 58.49925 | 58.30370 | 58.32051 | 57.16113 | 58.39201 |
| 15 | 60.18763 | 61.16030 | 61.36069 | 61.32077 | 61.19720 | 60.24030 | 61.22918 |

Conversion of NO Raw Test Scores to 1990 Unmounded Sumind Score Equivilents Without Linkage to Answer Sheet Calibretion

| 0 | 15.54694 | 15.40206 | 15.40206 | 15.49707 | 15.49707 | 15.44852 | 15.44852 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 16.48229 | 16.28219 | 16.28219 | 16.41341 | 16.41341 | 16.34635 | 16.34635 |
| 2 | 17.42453 | 17.12877 | 17.12877 | 17.32274 | 17.32274 | 17.22362 | 17.22362 |
| 3 | 18.36811 | 17.96887 | 17.96887 | 18.23070 | 18.23070 | 18.09690 | 18.09690 |
| 4 | 19.31215 | 18.80673 | 18.80673 | 19.13819 | 19.13819 | 18.96881 | 18.96881 |
| 5 | 20.25641 | 19.62589 | 19.62589 | 20.04547 | 20.04547 | 19.84009 | 19.84009 |


| Ren | 156 | 208 | 208 | 218 | 218 | 22. | 22 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 21 |  |  |  | 20 |  |  |
| 7 | 22.14521 | 21.25618 | 21.25618 | 21.85972 | 21.05972 | 21.58175 | 21.58175 |
| 8 | 23.08969 | 22.07956 | 22.07956 | 22.76677 | 22.76677 | 22.44908 | 22.44908 |
| 9 | 24.03421 | 22.90576 | 22 | 23.67378 |  |  |  |
| 10 | 24.97874 | 23.73388 |  | 24.58077 |  |  |  |
| 11 | 25.92330 | 24.56334 | 24.56334 | 25.48775 | 25.4877 | 25.03455 | 25.03455 |
| 12 | 26.80661 | 25.48029 | 25.48029 | 26.41378 | 26.4137 | 25.9215 | 25.92 |
| 13 | 27.64144 | 26.50457 | 26.50457 | 27.36400 | 27.364 |  |  |
| 14 | 28.50168 | 27.56742 | 27.56742 | 28.31024 | 28.3182 | 27.9 | 27.90650 |
| 15 | 29.38835 | 28.63614 | 28.63614 | 29.26918 | 29.2091 | 28.9 |  |
| 16 | 30.30007 | 29.70753 | 29.70753 | 30.20327 | 30.26327 | 30.0302 | 30.03020 |
| 17 | 31.23343 | 30.77723 | 30.77723 | 31.3010 | 31.3010 | 31.09 | 31.09487 |
| 18 | 32.18368 | 31.81827 | 31.81827 | 32.33832 | 32.3303 | 32.14 | 32.1443 |
| 19 | 33.14576 | 32.84706 | 32.84706 | 33.38799 | 33.387 | 33.10127 | 33.18127 |
| 20 | 34.11505 | 33.86773 | 33 | 34.4418 |  | 34.18 |  |
| 21 | 35.08781 | 34.88090 |  | 35.48055 | 35 | 35.17183 | 35.17183 |
| 22 | 36.06135 | 35.887 | 35 | 36.50160 | 36.501 | 36.1331 | 36.13314 |
| 23 | 37.03387 |  |  | 37.5140 | 37.514 | 37.0779 | 37.07796 |
| 24 | 38.00427 | 37.885 |  | 38.51607 | 38.5160 | 36.011 | 38.01181 |
| 25 | 38.97188 | 38.8779 | 38.8779 | 39.5070 | 39.5070 | 38.939 | 38.93987 |
| 26 | 39.93624 | 39.86612 | 39.866 | 40.486 | 40 | 39.86 |  |
| 27 | 40.89693 | 40.84967 | 40.84967 | 41.4566 | 41.4566 | 40.794 | 40.79475 |
| 28 | 41.85347 | 11.82792 | 41.82792 | 42.41720 | 42.4172 | 41.726 | 41.72674 |
| 29 | 42.80532 | 42.80018 | 42.80018 | 43.36972 | 43.369 | 42.66 | 42.66306 |
| 30 | 43.75192 | 43.76573 | 43.76573 | 44.3152 | 44.315 | 43.6030 | 43.60302 |
| 31 | 44.69246 | 44.72257 | 44.72257 | 45.25462 | 45.2546 | 44.54 |  |
| 32 | 45.62669 | 45.67444 | 45.67444 | 46.1845 | 46.1845 | 45.48602 | 45.48602 |
| 33 | 46.55531 | 46.622 | 46.622 | 47.11723 | 47.11723 | 46.423 | 46.42368 |
| 34 | 47.47842 | 47.56860 | 47.560 | 48.04148 | 48.04148 | 47.35527 | 47.35527 |
| 35 | 48.39645 | 48.51543 | 48.51543 | 48.9619 | 48.9629 | 48.27 | 48.27898 |
| 36 | 49.31007 | 49.46616 | 49.4661 | 49.8800 | 49.8800 | 49.19412 | 49.19412 |
| 37 | 50.22069 | 50.42432 | 50.42432 | 50.7975 | 50.7975 | 50.10118 | 50.10118 |
| 38 | 51.12982 | 51.39350 | 51.39350 | 51.71734 | 51.7173 | 51.00182 | 51.00182 |
| 39 | 52.03896 | 52.37662 | 52 | 52.6427 |  | 51.89 |  |
| 40 | 52.94956 | 53.37495 | 53.37495 | 53.57744 | 53.57744 | 52.79494 | 52.79494 |
| 41 | 53.86292 | 54.38630 | 54.38630 | 54.52385 | 54.52385 | 53.69442 | 53.69442 |
| 42 | 54.77998 | 55.40258 | 55.40258 | 55.48106 | 55.4810 | 54.60071 | 54.60071 |
| 43 | 55.70090 | 56.40752 | 56.40752 | 56.44115 | 56.44215 | 55.51652 | 55.51651 |
| 44 | 56.62433 | 57.37631 | 57.37631 | 57.38589 | 57.38589 | 56.44210 | 56.44210 |
| 45 | 57.54654 | 58.28064 | 58.28064 | 58.2872 | 58.28726 | 57.37360 | 57.37360 |
| 46 | 58.46063 | 59.10092 | 59.10092 | 59.11690 | 59.11690 | 58.30181 | 58.30181 |
| 47 | 59.35716 | 59.84249 | 59.84249 | 59.86550 | 59.86550 | 59.21414 | 59.21414 |
| 48 | 60.22661 | 60.54351 | 60.54351 | 60.56072 | 60.56072 | 60.10144 | 60.10144 |
| 49 | 61.06361 | 61.22172 | 61.22172 | 61.22505 | 61.22505 | 60.96783 | 783 |
| 50 | 61.86973 | 61.90331 | 61.90331 | 61.9008 | 61.900 | 61.83761 | . 83 |

Conversion of CS Raw Test Seores to 1980 Umrounded Stroderd Score Equivalems Without Linkage to Answer Sheet Calibration

| Bat | 159 | 208 | 208 | 218 | 218 | 208 | 228 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 21.52204 | 21.55967 | 21.55967 | 21.49453 | 21.52401 | 21.53872 | 21.53872 |
| 1 | 22.08792 | 22.14026 | 22.14026 | 22.04967 | 22.09067 | 22.11112 | 22.11112 |
| 2 | 22.63186 | 22.70942 | 22.70942 | 22.57518 | 22.63594 | 22.66623 | 22.66623 |
| 3 | 23.17162 | 23.27640 | 23.27640 | 23.09504 | 23.17712 | 23.21805 | 23.21805 |
| 4 | 23.70992 | 23.84262 | 23.84262 | 23.57531 | 23.71690 | 23.76873 | 23.76873 |
| 5 | 24.23328 | 24.40851 | 24.40851 | 24.07079 | 24.24497 | 24.31890 | 24.31890 |
| 6 | 24.75498 | 24.97420 | 24.97420 | 24.57385 | 24.76800 | 24.86481 | 24.86481 |
| 7 | 25.28140 | 25.53978 | 25.53978 | 25.08087 | 25.29582 | 25.10300 | 25.40300 |
| 8 | 25.81059 | 26.10529 | 26.10529 | 25.59021 | 25.82644 | 25.94423 | 25.94423 |
| 9 | 26.34155 | 26.67066 | 26.67066 | 26.10203 | 26.35805 | 26.48741 | 26.48741 |
| 10 | 26.87371 | 27.23064 | 27.23064 | 26.60138 | 26.89247 | 27.03189 | 27.03189 |
| 11 | 27.40671 | 27.79165 | 27.79165 | 27.10043 | 27.42694 | 27.57731 | 27.57731 |
| 12 | 27.94033 | 28.35342 | 28.35342 | 27.60271 | 27.96204 | 28.12341 | 28.12341 |
| 13 | 28.47441 | 28.91577 | 28.91577 | 28.10735 | 28.49761 | 28.67002 | 28.67002 |
| 14 | 28.97788 | 29.47289 | 29.47289 | 28.66773 | 29.06059 | 29.25857 | 29.25857 |
| 15 | 29.47238 | 30.03956 | 30.03956 | 29.29511 | 29.65936 | 29.89275 | 29.89275 |
| 16 | 29.98750 | 30.62924 | 30.62924 | 29.95355 | 30.27277 | 30.53564 | 30.53564 |
| 17 | 30.51731 | 31.23960 | 31.23960 | 30.63024 | 30.89257 | 31.28206 | 31.18206 |
| 18 | 31.06025 | 31.87216 | 31.87216 | 31.32071 | 31.52258 | 31.83493 | 31.83493 |
| 19 | 31.61865 | 32.52826 | 32.52826 | 32.02750 | 32.16612 | 32.49671 | 32.49671 |


| 89\% |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 32.19187 | 33.20075 | 33.20075 | 32.74185 | 32.82590 | 33.26926 | 33.16926 |
| 21 | 32.79111 | 33.90653 | 33.90653 | 33.47310 | 33.50378 | 33.05159 | 33.05159 |
| 22 | 33.40920 | 34.62358 | 34.62358 | 34.22125 | 34.20061 | 34.53940 | 34.53940 |
| 23 | 34.05026 | 35.35918 | 35.35918 |  |  | 35.23678 | 35.23678 |
| 24 | 34.71445 | 36.10919 | 36.10919 | 35.74456 | 35.64599 | 35.94131 |  |
| 25 | 35.40073 | 36.86313 | 36.86313 | 36.50573 |  | 36.64969 |  |
| 26 | 36.10675 | 37.60094 | 37.60894 | 37.26490 | 37.11912 | 37.35804 | 37.35804 |
| 27 | 36.82736 | 38 | 38.35004 | 38.01542 |  | 38.05637 | 38.05637 |
| 28 | 37.54722 | 39.08366 | 39.08396 | 38.73895 | 38.60524 | 38.74142 | 38.74142 |
| 29 | 38.27120 | 39.80294 | 39.80294 | 39.44663 | 39.32568 | 39.41543 | 39.41543 |
| 30 | 38.99420 | 40.49432 | 40.49432 | 40.13635 | 40.03633 | 40.07630 | 40.07630 |
| 31 | 39.71147 | 41.16992 | 41.16992 | 40.80728 | 40.73492 | 40.72284 | 40.72284 |
| 32 | 40.41579 | 41.82967 | 41.82967 | 41.45963 | 41.42010 | 41.35470 | 41.35470 |
| 33 | 41.09860 | 42.47428 | 42.47428 | 42.09448 | 42.09138 | 41.97228 | 41.97228 |
| 34 | 41.76825 | 43.10508 | 43.10508 | 42.71357 |  | 42.57662 | 42.57662 |
| 35 | 42.42417 | 43.72377 | 43.72377 | 43.31902 | 43.39170 | 43.16915 | 43.16915 |
| 36 | 43.06651 | 44.33227 | 44.33227 | 43.91314 | 44.02105 | 43.75161 | 43.75161 |
| 37 | 43.69600 | 44.93254 | 44.93254 |  |  | 44.32582 |  |
| 38 | 44.31377 | 45.52646 | 45.52646 | 45.07648 | 45.25589 | 44.89361 |  |
| 39 | 44.92117 | 46.11581 | 46.11581 | 45.64990 |  | 45.45673 | 45.45673 |
| 40 | 45.51967 | 46.70222 | 46.70222 | 46.22028 | 46.46853 | 46.01676 | 46.01676 |
| 41 | 46.11079 | 47.28714 | 47.28714 |  | 47.06992 | 46.57517 | 46.57517 |
| 42 | 46.69593 | 47.87183 | 47.87183 | 47.35787 |  | 47.13323 | 47.13323 |
| 43 | 47.27645 | 48.45743 | 48.45743 | 47.92756 |  | 47.69208 | 47.69208 |
| 44 | 47.85359 | 49.04492 | 49.04492 | 48.49922 |  | 48.25271 | 48.25271 |
| 45 | 48.42844 | 49.63515 | 49.63515 | 49.07369 | 49.46958 | 48.81601 | 48.81601 |
| 46 | 49.00298 | 50.22887 | 50.22887 | 49.65170 | 50.07274 | 49.38275 | 49.38275 |
| 47 | 49.57511 | 50.82665 | 50.82665 | 50.23388 | 50.67870 | 49.95358 | 49.95358 |
| 48 | 50.14862 | 51.42898 | 51.42898 | 50.82079 | 51.28802 | 50.52098 | 50.52898 |
| 49 | 50.72319 | 52.03616 | 52.03616 | 51.41285 | 51.90110 | 51.10942 | 51.10942 |
| 50 | 51.29944 | 52.64834 | 52.64834 | 52.01037 | 52.51815 | 51.69546 | 51.69546 |
| 51 | 51.87790 | 53.26544 | 53.26514 | 52.61354 | 53.13921 | 52.28698 | 52.28698 |
| 52 | 52.45894 | 53.88717 | 53.88717 | 53.22234 | 53.76411 | 52.83364 | 52.88364 |
| 53 | 53.04289 | 54.51301 | 54.51301 | 53.83659 | 54.39242 |  |  |
| 54 | 53.62986 | 55.14221 | 55.14221 | 54.45584 | 55.02350 | 54.08997 | 54.08997 |
| 55 | 54.21982 | 55.77379 | 55.77379 | 55.07946 | 55.65648 | 54.69791 | 54.69791 |
| 56 | 54.81256 | 56.40660 | 56.40660 | 55.70656 | 56.29029 | 55.30770 | 55.30770 |
| 57 | 55.40764 | 57.03938 | 57.03938 | 56.33604 | 56.92377 | 55.91867 | 55.91867 |
| 58 | 56.00440 | 57.67082 | 57.67081 | 56.96665 | 57.55565 | 56.52905 | 56.52905 |
| 59 | 56.60201 | 58.30049 | 58.30049 | 57.59705 | 58.18469 | 57.13752 | 57.13752 |
| 60 | 57.19945 | 58.92803 | 58.92803 | 50.22586 |  | 57.74298 | 57.74298 |
| 61 | 57.79557 | 59.55095 | 59.55095 | 58.85180 | 59.42993 | 58.34450 | 58.34450 |
| 62 | 58.38913 | 60.16860 | 60.16860 | 59.47376 | 60.04448 | 58.94155 | 58.94155 |
| 63 | 58.97888 | 60.78070 | 60.78070 | 60.09203 | 60.65304 | 59.53395 | 59.53395 |
| 64 | 59.56361 | 61.38739 | 61.38739 | 60.70527 | 61.25556 | 60.12197 | 60.12197 |
| 65 | 60.14218 | 61.98927 | 61.98927 | 61.31243 | 61.85236 | 60.70631 | 60.70631 |
| 66 | 60.71361 | 62.58740 | 62.58740 | 61.91351 | 62.44407 | 61.28813 | 61.28813 |
| 67 | 61.27705 | 63.18326 | 63.18326 | 62.50888 | 63.03164 | 61.86901 | 61.86901 |
| 68 | 61.83573 | 63.77884 | 63.77894 | 63.09929 | 63.61631 | 62.45251 | 62.45251 |
| 69 | 62.38763 | 64.37653 | 64.37653 | 63.68584 | 64.19955 | 63.03939 | 63.03939 |
| 70 | 62.93230 | 64.97907 | 64.97907 | 64.27000 | 64.78299 | 63.63178 | 63.63178 |
| 71 | 63.47018 | 65.58931 | 65.58931 | 64.85356 | 65.36836 | 64.23200 | 64.23200 |
| 72 | 64.00209 | 66.20965 | 66.20965 | 65.43989 | 65.95719 | 64.84227 | 64.84227 |
| 73 | 64.52949 | 66.84112 | 66.84112 | 66.02972 | 66.55049 | 65.46751 | 65.46751 |
| 74 | 65.05475 | 67.48183 | 67.48183 | 66.62398 | 67.14804 | 66.10960 | 66.10960 |
| 75 | 65.58170 | 68.12486 | 68.12486 | 67.22312 | 67.74737 | 66.76606 | 66.76606 |
| 76 | 66.11630 | 68.75639 | 68.75639 | 67.02505 | 68.34249 | 67.43217 | 67.43217 |
| 77 | 66.66736 | 69.35560 | 69.35560 | 68.42784 | 68.92282 | 68.09829 | 68.09829 |
| 78 | 67.24699 | 69.89914 | 69.89914 | 69.02053 | 69.47356 | 68.74931 | 68.74931 |
| 79 | 67.87014 | 70.37237 | 70.37237 | 69.59074 | 69.97932 | 69.36625 | 69.36625 |
| 80 | 68.55193 | 70.78016 | 70.78016 | 70.12281 | 70.43232 | 69.93170 | 69.93170 |
| 81 | 69.30156 | 71.10572 | 71.10572 | 70.60496 | 70.84370 | 70.43910 | 70.43910 |
| 82 | 70.11245 | 71.41065 | 71.41065 | 71.03950 | 71.19578 | 70.90280 | 70.90280 |
| 83 | 70.93228 | 71.63953 | 71.63953 | 71.45138 | 71.52689 | 71.34303 | 71.34303 |
| 84 | 71.67150 | 71.88218 | 71.88218 | 71.81321 | 71.84001 | 71.77268 | 71.77268 |

Conversion of AS Raw Teat Scores to 1900 Uarounded Standed Score Equivelents

| Bax |  | 208 | 909 |  | 218 | 2 | 228 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 24.24820 | 23.90078 | 23.98078 | 23.73053 | 23.73053 | 24.01244 | 24.01244 |
| 1 | 26.05558 | 25.76372 | 25.76372 | 25.47317 | 25.47317 | 25.79033 | 25.79033 |
| 2 | 27.87282 | 27.49115 | 27.49115 | 27.11120 | 27.11120 | 27.52595 | 27.52595 |
| 3 | 29.69342 | 29.20242 | 29.20242 | 28.71364 | 28.71364 | 29.24720 | 29.24720 |
| 4 | 31.51531 | 30.90747 | 30.90747 | 30.06295 | 30.06295 | 30.96291 | 30.96291 |
| 5 | 33.48424 | 32.73432 | 32.73432 | 31.70401 | 31.70401 | 32.7815 | 32.78815 |
| 6 | 35.53017 | 34.57209 | 34.57209 | 33.44998 | 33.44998 | 34.6656 | 34.66564 |
| 7 | 37.55505 | 36.39416 | 36.39416 | 35.289 | 35.28970 | 36.5937 | 36.59378 |
| 0 | 39.52092 | 38.18534 | 38.18534 | 37.21560 | 37.21560 | 38.5438 | 38.54380 |
| 9 | 41.39533 | 39.94095 | 39.94095 | 39.19109 | 39.19109 | 40.47151 | 40.47151 |
| 10 | 43.21146 | 41.67194 | 41.67194 | 41.16872 | 41.16872 | 42.33922 | 42.33922 |
| 11 | 44.97440 | 43.40200 | 43.40200 | 43.11539 | 43.11539 | 44.12939 | 44.12939 |
| 12 | 46.69551 | 45.16303 | 45.16303 | 45.01814 | 45.01814 | 45.8434 | 45.04344 |
| 13 | 48.39344 | 46.99079 | 46.99079 | 46.90243 | 46.90243 | 47.49506 | 47.49506 |
| 14 | 50.08492 | 48.91577 | 48.915 | 48.775 | 48.77569 | 49.10632 | 49.10632 |
| 15 | 51.76196 | 50.94551 | 50.94551 | 50.63625 | 50.63625 | 50.70625 | 50.70625 |
| 16 | 53.49429 | 53.04764 | 53.04764 | 52.47018 | 52.47018 | 52.32586 | 52.32586 |
| 17 | 55.22564 | 55.15193 | 55.15193 | 54.25840 | 54.25840 | 53.98732 | 53.98732 |
| 18 | 56.97043 | 57.18092 | 57.18092 | 55.99108 | 55.99108 | 55.69488 | 55.69488 |
| 19 | 58.71587 | 59.08809 | 59.08809 | 57.67861 | 57.67861 | 57.43292 | 57.43292 |
| 20 | 60.45018 | 60.87386 | 60.87386 | 59.35305 | 59.35305 | 59.18229 | 59.18229 |
| 21 | 62.17278 | 62.57443 | 62.57443 | 61.07195 | 61.07195 | 60.94110 | 60.94110 |
| 22 | 63.90245 | 64.24240 | 64.24240 | 62.83112 | 62.88112 | 62.73611 | 62.73611 |
| 23 | 65.67589 | 65.93059 | 65.93059 | 64.00823 | 64.80823 | 64.61600 | 64.61600 |
| 24 | 67.51643 | 67.66660 | 67.66650 | 66.85254 | 66.85254 | 66.62622 | 66.62622 |
| 25 | 69.34479 | 69.39836 | 69.39836 | 68.94223 | 68.94223 | 68.81634 | 68.81634 |

Conversion of MK Raw Test Scores to 1930 Umrounded Stendend Score Equivalents

| Raw |  |  | 20120 | 218 | 21 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 28.79944 | 28.75840 | 28.91140 | 28.62819 | 28.63338 | 29.46237 | 29.21225 |
| 1 | 30.37034 | 30.32213 | 30.50185 | 30.16918 | 30.17528 | 31.11880 | 30.85525 |
| 2 | 31.95057 | 31.88520 | 32.12894 | 31.67775 | 31.6860 | 32.81149 |  |
| 3 | 33.53351 | 33.44807 | 33.76663 | 33.17 | 33.18775 |  |  |
| 4 | 35.01803 | 35.15622 | 35.39126 | 34.88609 | 34.90366 | 36.20146 | 35.96702 |
| 5 | 36.45125 | 36.82532 | 36.96261 | 36.59361 | 36.6154 | 37.7292 | 37.57352 |
| 6 | 37.87960 | 38.40034 | 38.52940 | 38.21970 | 38.19901 | 39.17 | 39.15959 |
| 7 | 39.30550 | 39.93504 | 40.11149 | 39.83130 | 39.69943 | 40.5868 | 40.74316 |
| 8 | 40.73446 | 41.47448 | 41.71707 | 41.46455 | 41.1618 | 41.9706 | 42.33150 |
| 9 | 42.17915 | 43.05038 | 43.34782 | 43.13362 | 42.62684 | 43.36542 | 43.92191 |
| 10 | 43.65680 | 44.67419 | 44.99906 | 44.83053 | 44.1281 | 44.78772 | 45.50391 |
| 11 | 45.18228 | 46.32966 | 46.66010 | 46.52658 | 45.68605 | 46.22809 | 47. |
| 12 | 46.76105 | 47.97754 | 48.31710 | 48.18311 | 47.30022 | 47.67310 | 48.59434 |
| 13 | 48.38547 | 49.57666 | 49.95817 | 49.76867 | 48.95307 | 49.10776 | 50.09126 |
| 14 | 50.03884 | 51.10655 | 51.57779 | 51.27156 | 50.62253 | 50.52049 | 51.55952 |
| 15 | 52.70216 | 52.57521 | 53.27516 | 52.70081 | 52.294 | 51.90663 | 53.00684 |
| 16 | 53.36028 | 54.01043 | 54.7506 | 54.07973 | 53.967 | 53.26939 |  |
| 17 | 55.00447 | 55.44482 | 56.30070 | 55.43277 | 55.64255 | 54.61921 | 55.87885 |
| 18 | 56.63152 | 56.90089 | 57.81550 | 56.790 | 57.31524 | 55.97921 | 57.30801 |
| 19 | 58.24145 | 58.37007 | 59.28006 | 58.17744 | 58.95011 | 57.36703 | 58.72637 |
| 20 | 59.83532 | 59.84855 | 60.68334 | 59.60937 | 60.53380 | 58.79834 | 60.12526 |
| 21 | 61.42433 | 61.27463 | 62.01875 | 61.0 | 62.015 | 60.29503 | 61.50044 |
| 22 | 62.98073 | 62.64578 | 63.30741 | 67. 58781 | 63.42137 | 61.82948 | 62.86041 |
| 23 | 64.54070 | 64.00576 | 64.59681 | 64.09482 | 64.82077 | 63.43091 | 64.23124 |
| 24 | 66.11014 | 65.47025 | 65.95673 | 65.62559 | 66.29819 | 65.12037 | 65.66922 |
| 25 | 67.74255 | 67.28604 | 67.57153 | 67.40261 | 67.85483 | 67.07131 | 67.4067 |

conversion of MC Row Test Scores to 1980 Umrounded Stunderd Score Equivalents

| R ${ }^{\text {a }}$ | 15C | 20. | 208 | 218 | 278 | 228 | 278 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 23.27136 | 23.58811 | 23.58811 | 23.00344 | 23.08344 | 23.16597 | 23.16597 |
| 1 | 25.10520 | 25.46768 | 25.46768 | 24.89014 | 24.89014 | 24.98458 | 24.98458 |
| 2 | 26.88192 | 27.36337 | 27.36337 | 26.59630 | 26.59630 | 26.72173 | 26.72173 |
| 3 | 28.64052 | 29.26416 | 29.26416 | 28.27053 | 26.27053 | 28.43301 | 28.43301 |
| 4 | 30.39226 | 31.26690 | 31.16690 | 29.79674 | 29.79674 | 30.13451 | 30.13451 |
| 5 | 32.14072 | 32.88061 | 32.88061 | 31.68015 | 31.68015 | 32.06530 | 32.06530 |


| Raw | 156 | 20 | 208 |  |  | 22. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 33.81222 | 34.55987 | 34.55987 | 33.39263 | 33.39263 | 33.92999 | 33.92999 |
| 7 | 35.37803 | 36.26301 | 36.26301 | 35.02143 | 35.02143 | 35.73977 |  |
| 8 | 37.01454 | 37.98569 | 37.98569 | 36.65323 | 36.65323 | 37.51073 | 37.51073 |
| 9 | 38.69640 | 39.72777 | 39.72777 | 38.32408 | 38.32408 | 39.26745 | 39.26745 |
| 10 | 40.40599 | 41.49148 | 41.49148 | 40.05649 | 40.05649 | 41.06378 | 41.0637 |
| 11 | 42.13857 | 43.27988 | 43.27988 | 41.86170 | 41.86170 |  |  |
| 12 | 43.89918 | 45.09701 | 45.09701 | 43.73464 | 43.73464 | 44.78403 | 44.78403 |
| 13 | 45.70080 | 46.94859 | 46.94859 | 45.65702 | 45.6570 | 46.69527 | 46.69527 |
| 14 | 47.56269 | 48.04152 | 48.84152 | 47.6095 | 47.6095 | 48.63178 | 48.63178 |
| 15 | 49.50738 | 50.78102 | 50.78102 | 49.58389 | 49.5838 | 50.59452 | 50.59452 |
| 16 | 51.55470 | 52.76504 | 52.76504 | 51.58458 | 51.5045 | 52.59058 | 52.59058 |
| 17 | 53.71075 | 54.77886 | 54.77886 | 53.61993 | 53.61993 | 54.62228 | 54.62228 |
| 18 | 55.95399 | 56.79435 | 56.79435 | 55.68590 | 55.68590 | 56.673 | 56.67336 |
| 19 | 58.22959 | 58.77900 | 58.77900 | 57.75410 | 57.75410 | 58.70864 | 58.70864 |
| 20 | 60.46504 | 60.71213 | 60.71213 | 59.77805 | 59.77805 | 60.68869 | 60.68869 |
| 21 | 62.60458 | 62.59750 | 62.59750 | 61.72315 | 61.72315 | 62.59533 | 62.59533 |
| 22 | 64.64233 | 64.46341 | 64.46341 | 63.60062 | 63.60062 | 64.44857 | 64.44857 |
| 23 | 66.60920 | 66.35193 | 66.35193 | 65.47568 | 65.47568 | 66.30553 | 66.30553 |
| 24 | 68.53920 | 68.29815 | 68.29815 | 67.43545 | 67.43545 | 68.23986 | 68.23986 |
| 35 | 70.39131 | 70.25777 | 70.25777 | 69.70615 | 69.70615 | 70.22830 | 70.22830 |

## Conversion of Raw EI Test Scores to 1980 Umrounded Stamerd Score Equivalents

|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 22.08362 | 22.36199 | 22.36199 | 22.32777 |  |  |  |
| 1 | 24.33328 | 24.66273 | 24.66273 | 24.62223 | 24.62223 | 24.8123 | 24 |
| 2 | 26.43 | 26.8827 | 26.882 | 26.8275 | 26 |  |  |
| 3 | 28.35786 | 29.0799 | 29.079 | 29.0076 | 29.007 | 29 |  |
| 4 | 30.6284 | 31.3816 | 31.3816 | 31 | 31 | 31 |  |
| 5 | 33.13286 | 33.70604 | 33.7060 | 33. | 33.8681 | 34 |  |
| 6 | 35.69909 | 36.04048 | 36.04048 | 36.29 | 36 | 36.5051 |  |
| 7 | 38.31327 | 38.41933 | 38.41933 | 38.74936 | 38.749 | 38.757 | 38.75724 |
| 8 | 41.0753 | 40.86223 | 40.8622 | 41.2400 | 11.2400 | 0755 | 1.07552 |
| 9 | 43.9063 | 43.34468 | 43.3446 | 43.7479 | 43.747 | 43.4939 |  |
| 10 | 46.6649 | 45.8078 | 45.8078 | 46.2145 | 46.214 | 45.972 | 4.97281 |
| 11 | 49.24618 | 48.19922 | 48.19922 | 48.588 | 48.588 | 48.434 |  |
| 22 | 51.63949 | 50.50373 | 50.50373 | 50 | 50. | 50 |  |
| 13 | 53.90111 | 52.74096 | 52.7409 | . 0531 | . 0531 | 13 |  |
| 4 | 56.09285 | 54.94101 | 54.94101 | 55.20753 | 55.20753 | 4 |  |
| 25 | 58.23988 | 57.12111 | 57.12111 | 57.34618 | 57.34618 | 57.57238 | 57.57238 |
| 16 | 60.31723 | 59.27564 | 59.275 | 59.462 | 59. | 59.71419 |  |
| 17 | $62.2920{ }^{\circ}$ | 61.45345 | 61.453 | 61.555 | 61.55 | 61.775 |  |
| 18 | 64.17 | 63.6586 | 63 | 63.68 | 63.68 | 63.85321 | 63.85321 |
| 19 | 66.24488 | 65.98744 | 65.98744 | 65.89629 | 52 | . 0895 |  |
| 20 | 68.64922 | 5409 | 68. | 68.40442 | 69.40442 |  |  |

Conversion of Raw VE Test Scores to 1980 Unrounded Standard Score Equivalents

| Baw | $15 G$ | 208 | $20 B$ | 218 | 218 | $27 A$ | 228 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 14.86287 | 15.23383 | 14.91123 | 14.81379 | 14.84125 | 14.76109 | 14.82696 |
| 1 | 15.81132 | 16.21635 | 15.86412 | 15.75774 | 15.79089 | 15.70020 | 15.77212 |
| 2 | 16.76978 | 17.20711 | 16.83665 | 16.70191 | 16.74389 | 16.62904 | 16.72012 |
| 3 | 17.73216 | 18.22746 | 17.81688 | 17.64618 | 17.69937 | 17.55385 | 17.66925 |
| 4 | 18.69611 | 19.27609 | 18.80019 | 18.59048 | 18.65582 | 18.47705 | 18.61882 |
| 5 | 19.66082 | 20.34410 | 19.78500 | 19.53480 | 19.61275 | 19.39947 | 19.56861 |
| 6 | 20.62595 | 21.42560 | 20.77063 | 20.47912 | 20.56995 | 20.32145 | 20.51852 |
| 7 | 21.59134 | 22.51678 | 21.75677 | 21.42346 | 21.52731 | 21.24318 | 21.46850 |
| 8 | 22.55690 | 23.61507 | 22.74323 | 22.36779 | 22.48477 | 22.26473 | 22.41853 |
| 9 | 23.52257 | 24.71873 | 23.72993 | 23.31213 | 23.44231 | 23.08616 | 23.36860 |
| 10 | 24.48832 | 25.78608 | 24.71679 | 24.25647 | 24.39990 | 24.00750 | 24.31869 |
| 11 | 25.45415 | 26.86019 | 25.69440 | 25.20081 | 25.35753 | 24.92878 | 25.26879 |
| 12 | 26.42601 | 27.95670 | 26.67185 | 26.14516 | 26.31519 | 25.85001 | 26.21891 |
| 13 | 27.31598 | 28.98894 | 27.66691 | 27.12827 | 27.21383 | 26.82666 | 27.29398 |
| 14 | 28.19110 | 29.93425 | 28.70006 | 28.15017 | 28.11959 | 27.85889 | 28.52244 |
| 15 | 29.10260 | 30.85231 | 29.75185 | 29.18407 | 29.11149 | 28.93043 | 29.78101 |
| 16 | 30.04099 | 31.74414 | 30.81554 | 30.22351 | 30.18394 | 30.03276 | 31.08002 |
| 17 | 30.99633 | 32.61455 | 31.88332 | 31.26061 | 31.31471 | 31.15178 | 32.35716 |
| 18 | 31.95886 | 33.47015 | 32.94826 | 32.28585 | 32.43937 | 32.27124 | 33.55504 |
| 19 | 32.92041 | 34.31755 | 34.00529 | 33.28769 | 33.55580 | 33.35079 | 34.69325 |
| 20 | 33.87549 | 35.16233 | 35.05156 | 34.27567 | 34.64733 | 34.40964 | 35.76514 |
| 21 | 34.82148 | 36.00139 | 36.04038 | 35.25016 | 35.70546 | 35.44423 | 36.77465 |


|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 35.75026 | 36.03628 | 37.09162 | 36.21277 | 36.730 | 36.45 | 37.7316 |
| 23 |  |  | 38.093 | 37.16550 |  |  |  |
| 24 | 37.61106 | 38.53135 |  | 38.11019 | 38 |  |  |
| 25 | 38.53175 | 39.3915 | 40.06 |  |  | 39 | 40 |
| 26 | 39.45134 | 40.25902 | 41.03561 | 39.90019 | 40 | 40. | 41. |
| 27 | 40.370 | 41.132 |  | 40.90632 | 41 |  | 42.1147 |
| 28 | 41.29002 | 42.01038 | 42.92513 | 41.826 | 42.52 | 42.20231 | 42.9653 |
| 29 | 42.21012 | 42.89131 | 43.8430 | 42.73935 | 43.46133 |  |  |
| 30 | 43.12727 |  | 44 | 43 | 44.377 |  |  |
| 31 | 44.04015 | 44. | 45.6240 | 41 | 45.274 |  |  |
| 32 | 44.9466 |  |  | 45.42571 | 46.151 |  |  |
| 33 | 45.8451 |  | 47.3361 | 46.30033 | 47.0125 | 46.491 | 47. |
| 34 | 46.7346 | 47.2849 | 48.16162 | 47.1682 | 47.65091 | 47.352 |  |
| 35 | 47.6154 | 48.15036 | 48.97679 | 48.03131 | 48.70311 | 48 |  |
| 36 | 48.48857 | 49.01310 | 49.78340 | 48.89162 | 49.54530 | 49.053 | 49.6243 |
| 37 | 49.35612 | 49.8735 | 50.58217 | 49.75136 | 50.3927 | 49.90453 |  |
| 38 | 50.22093 | 50.73243 | 51.37302 | 50.61276 | 51.24892 | 50.75 |  |
| 39 | 51.08118 | 52.5908 | 52.15561 | 51.47818 | 52.11501 | 51.61145 |  |
| 40 | 51.9485 | 52.45085 | 52.92475 | 52.35038 | 52.9868 | 52.4670 | 52.8616 |
| 41 | 52.82988 | 53.31552 | 53.68874 | 53.23276 | 53.06332 | 53.32438 |  |
| 42 | 53.7304 | 54.18960 | 54.45553 | 54.12932 | 54.73827 | 54.10429 |  |
| 43 | 54.65487 | 55.07927 | 55.23194 | 55.04417 | 55.6046 | . 04 |  |
| 44 | 55.60547 | 55.99131 | 56.02819 | 55.98038 | 56.45915 | 55.91930 |  |
| 45 | 56.58057 | 56.93104 | 56.85651 | 56.93826 | 57.3055 | 56.79948 | . 1 |
| 46 | 57.57288 | 57.89995 | 57.72910 | 57.91423 | 58.15613 | 6929 |  |
| 47 | 58.570 | 58.893 | 58.65402 | 58.90109 | 59.029 | 603 |  |
| 48 | 59.56 | 59.90311 | 59.62540 |  | 1562 | 53615 |  |
| 49 | 60.55586 | 60.91737 | 60.64257 | 60.88147 | 60.91696 | 60.50427 | 60.7519 |
| 50 | 61.64690 | 61.9338 | 61.74924 | 61.89548 | 61.93109 | 1.5777 | 61.7494 |

Conversion of NO Raw Test Scores to 1980 Uarounded Standard Score Equivalents After Linkage to Answer Sheet Calibration

| B7\% | 15.150 | 208 | 208 ${ }^{2015}$ |  | $218$ | 278 | 228 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 15.60598 | 15.44527 | 15.44527 | 15.55226 | 15.55226 | 15.49758 | 15.49758 |
| 1 | 16.56795 | 16.36168 | 16.36168 | 16.49656 | 16.49656 | 16.42764 | 16.42764 |
| 2 | 17.55321 | 17.24384 | 17.24384 | 17.44663 | 17.44663 | 17.34300 | 17.34300 |
| 3 | 18.54276 | 18.12403 | 18.12403 | 18.39859 | 18.39859 | 18.25829 | 18.25029 |
| 4 | 19.53378 | 19.00318 | 19.00318 | 19.35113 | 19.35113 | 19.17332 | 19.17332 |
| 5 | 20.52548 | 19.86327 | 1986327 | 20.30392 | 20.30392 | 20.08822 | 20.08822 |
| 6 | 21.51753 | 20.71545 | 20.71545 | 21.25685 | 21.25685 | 21.00304 | 21.00304 |
| 7 | 22.50981 | 21.57575 | 21.57575 | 22.20985 | 22.20995 | 21.91780 | 21.91780 |
| 8 | 23.50224 | 22.44083 | 22.44083 | 23.16291 | 23.16291 | 22.82910 | 22.02910 |
| 9 | 24.49390 | 23.30896 | 23.30896 | 24.11601 | 24.11602 | 23.73255 | 23.73255 |
| 10 | 25.47935 | 24.17915 | 24.17915 | 25.06564 | 25.06564 | 24.63690 | 24.63690 |
| 11 | 26.43564 | 25.04740 | 25.04740 | 26.00511 | 26.00511 | 25.53699 | 25.53699 |
| 12 | 27.28283 | 25.99740 | 25.99740 | 26.09828 | 26.89828 | 26.43399 | 26.43399 |
| 13 | 28.14349 | 26.98392 | 26.98392 | 27.85367 | 27.05367 | 27.36049 | 27.36049 |
| 14 | 29.08506 | 28.06257 | 28.06257 | 28.88347 | 28.83347 | 28.43330 | 28.43330 |
| 15 | 30.10912 | 29.24035 | 29.24035 | 29.99459 | 29.99459 | 29.62437 | 29.62437 |
| 16 | 31.20460 | 30.49192 | 30.49192 | 31.18439 | 31.18439 | 30.80002 | 30.80002 |
| 17 | 32.35480 | 31.79206 | 31.79206 | 32.43876 | 32.43876 | 32.10389 | 32.18389 |
| 18 | 33.54048 | 33.09437 | 33.08437 | 33.72029 | 33.72129 | 33.49649 | 33.49549 |
| 19 | 34.70768 | 34.34556 | 34.34556 | 34.99918 | 34.99918 | 34.75041 | 34.75041 |
| 20 | 35.87381 | 35.57650 | 35.57650 | 36.26576 | 36.26576 | 35.96250 | 35.96250 |
| 21 | 37.04026 | 36.79230 | 36.79230 | 37.51065 | 37.51065 | 37.14089 | 37.14089 |
| 22 | 38.20658 | 37.99818 | 37.99818 | 38.73461 | 38.73462 | 38.29268 | 38.29268 |
| 23 | 39.36850 | 39.19761 | 39.19761 | 39.93438 | 39.93438 | 39.42047 | 39.42047 |
| 24 | 40.51353 | 40.37291 | 40.37291 | 41.11949 | 41.11949 | 40.52246 | 40.52246 |
| 25 | 41.66140 | 41.54947 | 42.54947 | 42.29896 | 42.29896 | 41.62326 | 41.62326 |
| 26 | 42.81191 | 42.72805 | 42.72805 | 43.47053 | 43.47053 | 42.72844 | 42.72844 |
| 27 | 43.96040 | 43.90429 | 43.90429 | 44.63003 | 44.63003 | 43.83861 | 43.83861 |
| 28 | 45.09799 | 45.06785 | 45.06785 | 45.76218 | 45.76218 | 44.94853 | 44.94853 |
| 29 | 46.21429 | 46.20830 | 46.20830 | 46.87107 | 46.87107 | 46.04857 | 46.04857 |
| 30 | 47.31266 | 47.32862 | 47.32862 | 47.96266 | 47.96266 | 47.14062 | 47.14062 |
| 31 | 48.39484 | 48.42933 | 48.42933 | 49.03821 | 49.03011 | 48.22572 | 48.22572 |
| 32 | 49.46154 | 49.51588 | 49.51588 | 50.10040 | 50.10040 | 49.30145 | 49.30145 |
| 33 | 50.51643 | 50.59262 | 50.59262 | 51.15371 | 51.15371 | 50.36716 | 50.36716 |
| 34 | 51.56337 | 51.66566 | 51.66566 | 52.20220 | 52.20220 | 51.42369 | 51.42369 |
| 35 | 52.60543 | 52.74057 | 52.74057 | 53.24806 | 53.24806 | 52.47198 | 52.47198 |
| 36 | 53.64418 | 53.82181 | 53.82181 | 54. 29168 | 54.29168 | 53.51223 | 53.51223 |


| 87 |  |  |  |  |  | 2 | 227 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 37 | 54.67553 | 54.90498 | 54.90498 | 55.32210 | 55.32210 | 54.54087 | 54.540 |
| 38 | 55.68380 | 55.97005 | 55.97085 | 56.31701 | 56.31701 | 55.54445 | 55 |
| 39 | 56.64270 | 56.98463 | 56.98463 | 57.21481 |  | 56.50059 | 56.5005 |
| 40 | 57.52113 | 5.90429 | 57.90429 | 58.07528 | 58.07528 |  |  |
| 41 | 58.29717 | 58.70398 | 58.70398 | 58.79616 | 58.79616 | 58.16620 | 58.16620 |
| 42 | 58.96177 | 59.35645 | 59.35645 | 59.39775 | 59.39775 | 58.84586 | 8 |
| 43 | 59.51347 | 59.87726 | 87726 | 59.09306 | 59.0930 | 59.41642 | 42 |
| 44 | 59.97913 | 60.31097 | 60.31897 | 60.32278 | 60.32278 | 59.89 | 59.89351 |
| 45 | 60.38669 | 60.67300 | 60.67300 | 60.67540 | 60.67540 | 60.31789 |  |
| 46 | 60.73837 | 60.97374 | 60.97374 | 60.94029 | 60.98029 | 60.68068 | 0 |
| 47 | 61.07878 | 61.27773 | 61.27773 | 61.28117 | 61.28717 | 61.02016 | 61.02016 |
| 48 | 61.41786 | 61.52662 | 61.52662 | 61.53253 | 61.53253 | 61.37489 | 61.37489 |
| 49 | 61.72097 | 61.79988 | 61.78988 | 61.79133 | 61.79133 | 61.67923 | 61.67923 |
| 50 | 62.07560 | 62.09239 | 62.09239 | 62.09115 | 62.09115 | 62.05954 | 62.05954 |

Conversion of CS Raw Test Scores to 1990 Unrounded Standard Score Equivelents After Linkage to Answer Sheet Calibration

| Raw | 15G | 20 | 208 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 21.50235 | 21.53661 | 21.53661 | 21.47731 | 21.50415 | 21.51754 | 21.5175 |
| 1 | 22.02907 | 22.07796 | 22 | 21.99335 | 22.03164 | 22.0507 | 22.05074 |
| 2 | 22.53475 | 22.60676 | 22.6067 | 22.4821 | 22.5385 |  |  |
| 3 | 23.03573 | 23.13297 | 23.13297 |  | 23 |  |  |
| 4 | 23.53524 | 23.65837 | 23.65037 | 23.4103 | 23.5417 | 23. |  |
| 5 | 24.02082 | 24.18339 | 24.18339 |  | 24.0326 | 24.1002 | 24.10025 |
| 6 | 24.50483 | 24.70821 | 24.70821 | 24.3367 | 24.5169 |  |  |
| 7 | 24.99306 | 25.23238 | 25.23238 | 24.8071 | 25.0064 | 25.105 |  |
| 8 | 25.48319 | 25.7559 | 25.7559 | 25.2790 | 25.4978 | 25. 605 |  |
| 9 | 25.97470 | 26.279 | 26.279 | 25.7520 | 25.99071 | 26.109 |  |
| 10 | 26.4675 | 26.79 |  | 26.2153 | 26 | 26.614 |  |
| 11 | 26.96130 | 27.31798 | 27.3179 | 26.677 | 26 | 27.119 |  |
| 12 | 27.45575 | 27.8509 | 27.850 | 27.142 | 27.475 |  | 27.6254 |
| 13 | 27.97092 | 28.4189 | 28.4189 | 27.6105 | 27.9939 | 28.164 | 28.1648 |
| 14 | 28.48461 | 29.00992 | 29.009 | 28.1626 | 28.5721 | 28.781 | 28.78151 |
| 15 | 29.00938 | 29.6184 | 29.6184 | 28.8201 | 29.2098 | 29.4601 | 29.46019 |
| 16 | 29.56213 | 30.2569 | 30.2569 | 29.525 | 29.8707 | 30.155 |  |
| 17 | 30.13529 | 30.9212 | 30.9211 | 30.258 | 30.5435 | 30.8 |  |
| 18 | 30.73605 | 31.6083 | 31 | 31.009 | 31.228 | 31.5 |  |
| 19 | 31.33331 | 32.3187 | 32.3187 | 31.776 | 31.92670 | 32.28 | 32 |
| 20 | 31.95783 | 33.0548 | 33.0548 | 32.549 | 32.6409 | 33.012 | 33.01221 |
| 21 | 32.60326 | 33.80821 | 33.80822 | 33.340 | 33.373 |  |  |
| 22 | 33.27155 | 34.58012 | 34.58012 | 34.147 | 34.1251 | 34 |  |
| 23 | 33.96323 | 35.36917 | 35.3691 | 34 | 34.8941 | 35.2 |  |
| 24 | 34.67787 | 36.1702 | 36.1702 | 35.781 | 35.675 | 35.9 |  |
| 25 | 35.41358 | 36.97235 | 36.97235 | 36.5927 | 36.4574 | 36.745 | 36.74566 |
|  | 36.1676 | 37.762 | 37 | 37.398 | 37.2445 | 37.497 | 37.49715 |
| 27 | 36.93436 | 38.5460 | 38.54606 | 38.1921 | 30.0315 | 38.2353 | 38.23537 |
| 28 | 37.69743 | 39.3170 | 39.3170 | 38.954 | 38.813 | 38.9571 | 38.95715 |
| - | 38.46213 | 40.07109 | 40.071 | 39.697 | 5 | 39.665 | 5512 |
| 30 | 39.22294 | 40.7932 | 40.793 | 40.4200 | 40.315 | 40.3573 | 40.35732 |
| 31 | 39.97532 | 41.495 | 41.495 | 41.1189 | 41 | 41.031 | 41.03131 |
| 32 | 40.71135 | 42.178 | 42.17 | 41.795 | 41.754 | 41.606 |  |
| 33 | 41.42115 |  |  | 42.452 | 42.449 | 12.326 |  |
| 34 | 42.11517 |  |  | 43.093 | 129 | 42.951 |  |
| 35 | 42.79395 | 44.13632 |  | 43.718 | 43.793 | 43.563 |  |
| 36 | 43.4578 | 4 | 44 | 44.331 | 44.4429 | 44.1650 | 44.16503 |
| 3 | 44.1076 | 45 | 45 |  | 22 | 57 |  |
| 38 | 44.7447 |  | 45 | 45.5305 | 45.7153 | 45.3422 |  |
| 39 | 45.3706 | 46.600 | 46.6002 | 46.220 | 46.3414 | 45.9221 | 45.92211 |
| 40 | 45.986 | 47.20321 | 47.2032 | 16.707 | 46.9629 | 46.4983 |  |
| 41 | 46.59500 | 47.8042 | 47.8042 | 17.2925 | 47.5810 | 47.0725 | 47.07259 |
| 4 | 1934 |  |  |  | 48.197 | . |  |
| 43 | 47.79330 | 49.005 | 49.005 | 48.4619 | 48.8123 | 48.2201 | 48.22017 |
| 44 | 48.38604 | 49.60 |  | 49.0487 | 49.4276 | 48.7957 |  |
| 45 | 48.97611 | 50.21381 | 50.21381 | 49.630 | 50.0440 | 49.3737 | 7375 |
| 46 | 49.56454 | 50.82228 | 50.62228 | 50.23076 | 50.6622 | 49.954 |  |
| 47 | 50.15224 | 51.4346 | 51.4346 | 827 | 51.2830 | 50.5401 |  |
| 48 | 50.74003 | 52.05124 | 52.05124 |  |  | 51.12969 | 51.12 |
| 49 | 863 | 52.67249 | 52.67249 | 52.03473 | 52.53430 | 51.72409 | 12409 |
| 50 | 51. 36 | 53.29846 | 53.29846 | 52.64611 | 53.16535 | 52.32390 | 52.323 |


| $\frac{814}{51}$ | $52 . \frac{15 \mathrm{G}}{51056}$ | $53.92905$ | $53.92905$ | $53.21 \mathrm{~A}$ | $\frac{218}{53.80009}$ | $52 . \frac{238}{92697}$ | $52 . \frac{228}{92897}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 52 | 53.10481 | 54.56391 | 54.56391 | 53.88504 | 54.43929 | 53.53092 | 53.53992 |
| 53 | 53.70166 | 55.20246 | 55.20246 | 54.51230 | 55.07949 | 54.15316 | 54.15316 |
| 54 | 54.30120 |  | 55.84387 | 55.14417 | 55.72294 |  |  |
| 55 | 54.90337 | 56.48705 | 56.48705 | 55.77994 | 56.36767 | 55.39099 | 55.39099 |
| 56 | 55.50788 | 57.13074 | 57.13074 | 56.41863 | 57.01253 | 56.01244 | 56.01244 |
| 57 | 56.11424 | 57.77358 | 57.77358 | 57.05902 | 57.65623 | 56.63447 | 56.63447 |
| 58 | 56.72171 | 58.41409 | 58.41409 | 57.69976 | 58.29738 | 57.25520 | 57.25520 |
| 59 | 57.32936 | 59.05175 | 59.05175 | 58.33933 | 58.93459 | 57.87320 | 57.87320 |
| 60 | 57.93606 | 59.68601 | 59.68601 | 58.97624 | 59.56659 | 58.48723 | 58.48723 |
| 61 | 58.54054 | 60.31417 | 60.31417 | 59.60903 | 60.19225 | 59.09628 | 59.09628 |
| 62 | 59.14144 | 60.93542 | 60.93542 | 60.23640 | 60.81070 | 59.69965 | 59.69965 |
| 63 | 59.73735 | 61.54926 | 61.54926 | 60.85848 | 61.42137 | 60.29704 | 60.29704 |
| 64 | 60.32693 | 62.25561 | 62.15561 | 61.47370 | 62.02401 | 60.80956 | 60.80856 |
| 65 | 60.90887 | 62.75481 | 62.75481 | 62.08078 | 62.61868 | 61.47474 | 61.47474 |
| 66 | 61.48205 | 63.34761 | 63.34761 | 62.67948 | 63.20575 | 62.05652 | 62.05652 |
| 67 | 62.04546 | 63.93516 | 63.93516 | 63.26990 | 63.78589 | 62.63523 | 62.63523 |
| 68 | 62.60214 | 64.51900 | 64.51900 | 63.85249 | 64.35996 | 63.21411 | 63.21411 |
| 69 | 63.14989 | 65.10100 | 65.10100 | 64.42799 | 64.92902 | 63.79352 | 63.79352 |
| 70 | 63.68809 | 65.68325 | 65.68325 | 64.99748 | 65.49421 | 64.37509 | 64.37509 |
| 71 | 64.21696 | 66.26780 | 66.26780 | 65.56225 | 66.05667 | 64.96055 | 64.96055 |
| 72 | 64.73714 | 66.85612 | 66.85612 | 66.12502 | 66.61730 | 65.55135 | 65.55135 |
| 73 | 65.24964 | 67.44826 | 67.44826 | 66.68591 | 67.17638 | 66.15141 | 66.15141 |
| 74 | 65.75621 | 68.04146 | 68.04146 | 67.24512 | 67.73300 | 66.76148 | 66.76148 |
| 75 | 66.26053 | 68.62848 | 68.62848 | 67.80239 | 68.28426 | 67.37804 | 67.37804 |
| 76 | 66.76782 | 69.19592 | 69.19592 | 68.35582 | 68.82421 | 67.99557 | 67.99557 |
| 77 | 67.28570 | 69.72618 | 69.72618 | 68.90093 | 69.34331 | 68.60425 | 68.60425 |
| 78 | 67.82444 | 70.20026 | 70.20026 | 69.42984 | 69.82907 | 69.18964 | 69.18964 |
| 79 | 68.39620 | 70.61313 | 70.61313 | 69.93127 | 70.27021 | 69.73547 | 69.73547 |
| 60 | 69.01249 | 70.96570 | 70.96570 | 70.39539 | 70.66543 | 70.22866 | 70.22866 |
| 81 | 69.67873 | 71.24576 | 71.24576 | 70.81499 | 71.02035 | 70.67135 | 70.67135 |
| 82 | 70.38636 | 71.50475 | 71.50475 | 71.18879 | 71.32232 | 71.07120 | 71.07120 |
| 83 | 71.09656 | 71.69907 | 71.69907 | 71.53933 | 71.60343 | 71.44733 | 71.44733 |
| 84 | 71.72621 | 71.90294 | 71.90294 | 71.84525 | 71.86766 | 71.81134 | 71.81134 |

## Appendx G:

Distributions of Composites by ASVAB Form After Convemion Using Recommended Equmings

## AFQI PERCENTILE COMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

| Test | ------------ |  |  | Cut Score |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 93.00 | 65.00 | 50.00 | 31.00 | 21.00 | 16.00 | 10.00 |
| REF | 5.07 | 35.95 | 57.62 | 80.91 | 91.39 | 94.53 | 97.76 |
| 156 | 4.12 | 37.04 | 57.26 | 80.81 | 91.31 | 94.69 | 97.91 |
| 20A | 4.91 | 36.54 | 57.43 | 81.86 | 91.94 | 94.67 | 97.59 |
| 208 | 5.99 | 36.79 | 56.76 | 81.01 | 91.97 | 95.02 | 97.89 |
| 21A | 5.20 | 35.73 | 56.72 | 81.52 | 91.87 | 95.01 | 97.76 |
| 218 | 5.48 | 35.87 | 57.56 | 81.86 | 92.21 | 95.24 | 97.94 |
| 22A | 6.07 | 36.87 | 57.15 | 81.20 | 91.54 | 94.58 | 97.59 |
| 22 B | 5.24 | 36.06 | 57.27 | 81.12 | 91.85 | 95.08 | 97.89 |

AFOT PERCENIILE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test |  |  |  | Cut Score |  | 16.00 | 10.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 93.00 | 65.00 | 50.00 | 31.00 | 21.00 |  |  |
| 156 | -0.96 | 1.09 | -0.36 | -0.10 | -0.08 | 0.16 | 0.15 |
| 208 | -0.16 | 0.58 | -0.20 | 0.95 | 0.54 | 0.14 | -0.16 |
| 20B | 0.92 | 0.84 | -0.86 | 0.10 | 0.58 | 0.49 | 0.13 |
| 21A | 0.13 | -0.22 | -0.90 | 0.61 | 0.48 | 0.48 | 0.00 |
| 218 | 0.41 | -0.08 | -0.06 | 0.95 | 0.81 | 0.71 | 0.19 |
| 22A | 0.99 | 0.92 | -0.47 | 0.29 | 0.15 | 0.05 | -0.17 |
| 22B | 0.17 | 0.11 | -0.35 | 0.22 | 0.46 | 0.54 | 0.13 |

AIR FORCE M PERCEENTILE CCMPOSITE
Percentages At or Above Cut Scores (Ondered High to Low)

| Test |  |  |  | Cut Score |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 89.00 | 61.00 | 57.00 | 51.00 | 45.00 | 44.00 |
| REF | 9.83 | 43.98 | 49.55 | 56.17 | 62.58 | 63.10 |
| 156 | 9.71 | 44.29 | 49.11 | 55.63 | 62.25 | 63.49 |
| 20A | 9.03 | 45.38 | 50.81 | 57.23 | 64.05 | 65.09 |
| 208 | 8.84 | 44.55 | 49.51 | 56.17 | 62.75 | 63.73 |
| 21A | 8.41 | 43.54 | 49.52 | 56.14 | 62.71 | 63.60 |
| 218 | 7.73 | 43.85 | 50.29 | 57.26 | 64.20 | 65.26 |
| 22A | 9.47 | 44.70 | 49.49 | 56.01 | 62.44 | 63.96 |
| 22B | 9.63 | 44.08 | 48.70 | 55.31 | 62.06 | 63.64 |

## AIR FORCE M PERCGNITLE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

| Test |  |  |  | Out Score |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 89.00 | 61.00 | 57.00 | 51.00 | 45.00 | 44.00 |
| 156 | -0.12 | 0.31 | -0.44 | -0.54 | -0.33 | 0.40 |
| 20A | -0.80 | 1.40 | 1.27 | 1.07 | 1.47 | 1.99 |
| 20B | -0.99 | 0.57 | -0.03 | 0.01 | 0.17 | 0.64 |
| 21A | -1.42 | -0.44 | -0.03 | -0.03 | 0.13 | 0.50 |
| 218 | -2.10 | -0.13 | 0.74 | 1.10 | 1.63 | 2.16 |
| 22A | -0.36 | 0.72 | -0.06 | -0.15 | -0.14 | 0.86 |
| 22B | -0.20 | 0.10 | -0.85 | -0.86 | -0.52 | 0.54 |

AIR FORCE A PERCENTILE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

| Test | cut score |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 67.00 | 61.00 | 51.00 | 45.00 | 40.00 | 32.00 | 27.00 |
| REF | 40.62 | 47.77 | 61.32 | 69.43 | 74.62 | 83.40 | 88.60 |
| 156 | 40.58 | 47.59 | 61.01 | 68.89 | 74.34 | 83.30 | 88.81 |
| 20A | 40.59 | 47.77 | 61.62 | 69.62 | 74.58 | 82.79 | 88.16 |
| 208 | 40.93 | 47.99 | 61.55 | 69.27 | 74.64 | 83.11 | 88.35 |
| 21A | 40.72 | 47.57 | 61.39 | 69.50 | 74.89 | 83.16 | 88.86 |
| 218 | 40.02 | 47.35 | 60.54 | 68.63 | 74.30 | 83.47 | 88.60 |
| 22A | 40.95 | 47.97 | 61.03 | 68.87 | 74.46 | 82.92 | 88.14 |
| 22B | 40.30 | 47.41 | 60.98 | 69.41 | 74.60 | 83.32 | 88.36 |

AIR FORCE A PERCENTILIE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | $67.00$ | 61.00 | 51.00 | Cut Score | 40.00 | 32.00 | 27.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
| 15G | -0.04 | -0.18 | -0.31 | -0.54 | -0.28 | -0.10 | 0.21 |
| 20A | -0.03 | -0.00 | 0.30 | 0.19 | -0.04 | -0.61 | -0.44 |
| 20 B | 0.31 | 0.22 | 0.23 | -0.16 | 0.02 | -0.29 | -0.25 |
| 21A | 0.10 | -0.20 | 0.08 | 0.07 | 0.27 | -0.25 | 0.26 |
| 218 | -0.59 | -0.41 | -0.78 | -0.80 | -0.32 | 0.06 | -0.00 |
| 22A | 0.33 | 0.20 | -0.29 | -0.56 | -0.16 | -0.48 | -0.46 |
| 22B | -0.32 | -0.36 | -0.34 | -0.02 | -0.02 | -0.08 | -0.24 |

AIR FORCE G PERCENTILE COMPOSITE
Percenteges at or hbove Out Scoree (Ordered High co Low)

|  | 70.00 | 69.00 | 64.00 | 51.00 | 56.00 | 53.00 | 50.00 | 48.00 | 43.00 | 42.00 | 39.00 | 35.00 | 30.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Res | 31.03 | 31.03 | 38.88 | 44.57 | 47.00 | 52.46 | 57.62 | 60.26 | 65.24 | 67.60 | 72.09 | 76.03 | 122.57 |
| 15G | 31.67 | 31.67 | 39.66 | 44.32 | 47.03 | 52.11 | 57.26 | 59.85 | 64.48 | 66.92 | 71.15 | 75.67 | 22.38 |
| 20\% | 31.62 | 31.62 | 39.25 | 44.07 | 46.69 | 52.80 | 57.43 | 59.47 | 64.81 | 66.94 | 72.14 | 76.16 | 43.35 |
| 208 | 31.47 | 31.47 | 39.26 | 44.01 | 46.94 | 51.72 | 56.76 | 59.44 | 64.02 | 66.42 | 70.91 | 75.45 | 82.92 |
| 214 | 30.79 | 30.79 | 38.43 | 44.13 | 46.50 | 52.80 | 56.72 | 59.62 | 64.50 | 66.63 | 71.46 | 75.11 | 03.23 |
| 218 | 30.90 | 30.90 | 30.75 | 44.17 | 46.92 | 52.57 | 57.56 | 60.01 | 65.01 | 67.51 | 72.00 | 76.24 | 03.51 |
| 22n | 31.93 | 31.93 | 39.52 | 44.80 | 47.44 | 52.50 | 57.15 | 59.94 | 61.27 | 66.05 | 71.16 | 75.58 | 02.73 |

AIR FORCE G PERCENTILE COMPOSITE, COn't.


ARMY GT STANDARD SCORE COMPOSITE, CON't.

| 20B | 0.38 |
| :--- | ---: |
| 21 A | -0.45 |
| 21 B | -0.14 |
| 22A | 0.64 |
| 22B | -0.18 |

ARMY GM STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

|  | 105.00 | 100.00 | 95.00 | 90.00 | 85. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| REF | 46.48 | 58.49 | 68.11 | 78.28 | 85.96 |
| 15G | 45.55 | 57.21 | 67.25 | 78.46 | 86.64 |
| 20A | 47.18 | 59.40 | 69.24 | 78.90 | 86.49 |
| 20 B | 46.86 | 58.52 | 68.00 | 78.46 | 85.80 |
| 21A | 45.85 | 58.09 | 68.82 | 79.36 | 86.86 |
| 218 | 46.59 | 58.98 | 69.71 | 80.07 | 87.70 |
| 22A | 46.72 | 58.08 | 68.41 | 78.14 | 86.00 |
| 22B | 46.41 | 58.07 | 68.59 | 78.68 | 86.26 |

ARMY GM STANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | 105.00 | 100.00 | $\begin{aligned} & \text { ut Score } \\ & 95.00 \end{aligned}$ | 90.00 | 35 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $15 G$ | -0.92 | -1.28 | -0.86 | 0.18 | 0.67 |
| 20A | 0.70 | 0.92 | 1.14 | 0.61 | 0.53 |
| 208 | 0.38 | 0.04 | -0.11 | 0.17 | 0.16 |
| 21A | -0.63 | -0.40 | 0.72 | 1.08 | 0.89 |
| 218 | 0.11 | 0.49 | 1.60 | 1.78 | 1.74 |
| 22A | 0.24 | -0.41 | 0.30 | -0.15 | 0.04 |
| 22B | -0.06 | -0.41 | 0.48 | 0.40 | 0.29 |

ARMY EL STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test ------------------ Cut Score $120.00 \quad 115.00 \quad 110.00 \quad 105.00 \quad 100.00 \quad 95.00 \quad 90.00 \quad 85.00$

| REF | 17.95 | 26.88 | 36.22 | 46.82 | 57.75 | 67.96 | 77.95 | 86.39 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 15G | 17.45 | 26.37 | 35.17 | 46.26 | 57.42 | 67.52 | 77.48 | 86.37 |
| 20A | 18.57 | 27.43 | 36.44 | 47.31 | 57.94 | 67.82 | 78.22 | 86.38 |
| 20B | 18.73 | 27.50 | 36.12 | 46.80 | 58.11 | 67.55 | 77.69 | 85.89 |
| $21 A$ | 17.71 | 26.91 | 35.17 | 46.12 | 58.04 | 67.63 | 77.69 | 86.63 |
| 21B | 17.43 | 26.14 | 35.60 | 47.30 | 58.62 | 68.90 | 79.04 | 87.74 |
| 22A | 17.28 | 26.77 | 36.41 | 47.07 | 58.45 | 67.58 | 77.76 | 86.19 |
| 22B | 17.92 | 27.05 | 35.75 | 46.99 | 58.25 | 67.87 | 78.11 | 86.90 |

## ARMY EL STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-ReF)

|  | 120.00 | 5.00 | 10.00 | $\begin{aligned} & \text { Cut Score } \\ & 105.00100 .00 \end{aligned}$ |  | 95.00 | 90.00 | 85.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15G | -0.50 | -0.51 | -1.05 | -0.56 | -0.33 | -0.44 | -0. | -0.02 |
| 20A | 0.62 | 0.54 | 0.21 | 0.49 | 0.19 | -0.14 | 0.27 | -0.01 |
| 208 | 0.78 | 0.62 | -0.11 | -0.02 | 0.35 | -0.41 | -0.26 | -0.50 |
| 21A | -0.24 | 0.03 | -1.06 | -0.70 | 0.29 | -0.33 | -0.26 | 0.24 |
| 218 | -0.52 | -0.75 | -0.63 | 0.48 | 0.87 | 0.94 | 1.09 | 1.36 |
| 22A | -0.67 | -0.11 | 0.18 | 0.25 | 0.70 | -0.38 | -0.19 | -0.20 |
| 228 | 0.03 | . 17 |  | 0.17 | 0. | -0.0 |  |  |

ARMY CL STANDARD SCORE COMPOSTIE
Percentages At or Above Cut Scores (Ordered High to Low)

|  | --.-.------00 |  | Cut Score$100.00 \quad 95$ |  | 90.00 | 85.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| REF | 39.32 | 51.13 | 61.35 | 72.32 | 80.0 | 86.77 |
| $15 G$ | 39.80 | 51.14 | 61.34 | 72.26 | 80.60 | 87.14 |
| 20A | 39.60 | 50.92 | 60.96 | 71.79 | 80.42 | 87.43 |
| 208 | 39.10 | 50.64 | 60.57 | 71.56 | 80.05 | 87.14 |
| 21A | 39.00 | 50.62 | 60.87 | 71.86 | 80.26 | 87.43 |
| 21B | 38.72 | 50.97 | 61.85 | 72.77 | 81.18 | 88.01 |
| 22A | 39.65 | 51.38 | 61.11 | 72.12 | 80.14 | 87.13 |
| 22B | 39.26 | 51.08 | 61.24 | 71.71 | 80.42 | 87.19 |

ARMY CL STANDARD SCORE CONPOSITE
Differences in Percentages At or Above Out Scores (Test-REF)
$\begin{array}{lllllll}\text { Test } \\ & 110.00 & 105.00 & 100.00 & 95.00 & 90.00 & 85.00\end{array}$

| 15G | 0.47 | 0.02 | -0.01 | -0.06 | 0.54 | 0.37 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| 20A | 0.28 | -0.21 | -0.39 | -0.53 | 0.36 | 0.66 |
| 20B | -0.23 | -0.48 | -0.78 | -0.76 | -0.00 | 0.37 |
| 21A | -0.33 | -0.50 | -0.48 | -0.47 | 0.20 | 0.66 |
| 21B | -0.60 | -0.16 | 0.50 | 0.45 | 1.12 | 1.24 |
| 22A | 0.33 | 0.26 | -0.24 | -0.20 | 0.09 | 0.36 |
| 22B | -0.07 | -0.04 | -0.11 | -0.61 | 0.36 | 0.42 |

ARMY MM STANDARD SCCRE CCMPOSITE
Nurcentages At or Above Cut Scores (Ondered High to Low)


| REF | 49.43 | 60.24 | 72.01 | 80.79 |
| :--- | :--- | :--- | :--- | :--- |
| +5 G | 47.62 | 58.89 | 71.60 | 81.42 |
| 20A | 50.13 | 61.61 | 72.64 | 81.87 |
| 20B | 49.95 | 60.95 | 71.90 | 81.05 |

ARMY MM SIMNDARD SCORE COMPOSITE, COn't.

| $21 A$ | 49.37 | 60.60 | 71.87 | 81.69 |
| :--- | :--- | :--- | :--- | :--- |
| 218 | 49.89 | 61.29 | 73.28 | 81.81 |
| $22 A$ | 49.24 | 60.40 | 71.99 | 80.87 |
| $22 B$ | 49.71 | 60.00 | 72.26 | 81.08 |

## ARMY MM STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-RFF)

| Test | $105.00$ | $\begin{aligned} & -\mathrm{Cut} \\ & 100.00 \end{aligned}$ | Score $95.00$ | 90.00 |
| :---: | :---: | :---: | :---: | :---: |
| 15G | -1.81 | -1.34 | -0.40 | 0.63 |
| 20 A | 0.69 | 1.37 | 0.64 | 1.08 |
| 208 | 0.52 | 0.71 | -0.11 | 0.26 |
| 21A | -0.06 | 0.37 | -0.13 | 0.90 |
| 218 | 0.46 | 1.05 | 1.27 | 1.02 |
| 22A | -0.19 | 0.16 | -0.01 | 0.08 |
| 22B | 0.28 | -0.23 | 0.25 | 0.29 |

ARMY SC STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

| Test | $105.00$ | $\begin{aligned} & - \text { Cut } \\ & 100.00 \end{aligned}$ | Score 95.00 | 90.00 |
| :---: | :---: | :---: | :---: | :---: |
| REF | 49.86 | 59.96 | 70.50 | 79.47 |
| $15 G$ | 49.75 | 60.23 | 70.97 | 80.27 |
| 20 A | 50.78 | 60.82 | 71.05 | 80.18 |
| 20B | 49.62 | 59.84 | 70.28 | 79.29 |
| 21A | 49.55 | 59.87 | 70.66 | 80.39 |
| 21B | 50.82 | 61.17 | 72.11 | 81.30 |
| 22A | 50.36 | 60.64 | 70.81 | 79.64 |
| 22B | 50.05 | 59.74 | 70.20 | 79.51 |

## ARMY SC STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | $105.00100 .00$ |  | $\begin{aligned} & \text { Score } \\ & 95.00 \end{aligned}$ | 90.00 |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 15G | -0.10 | 0.27 | 0.47 | 0.81 |
| 20A | 0.93 | 0.86 | 0.56 | 0.71 |
| 208 | -0.24 | -0.12 | -0.21 | -0.18 |
| 21A | -0.31 | -0.09 | 0.16 | 0.92 |
| 218 | 0.96 | 1.21 | 1.61 | 1.83 |
| 22A | 0.51 | 0.69 | 0.31 | 0.17 |
| 228 | 0.20 | -0.22 | -0.30 | 0.04 |

## AROYY CO STANDARD SCORE CCMPOSITE

Percentages At or Above Cut Scores (Ordered High to Low)

| Test | $--\ldots-\ldots$ Cut | Score | $-\cdots-\ldots$ |  |
| :--- | :---: | :---: | :---: | :---: |
|  | 100.00 | 95.00 | 90.00 | 85.00 |
| REF | 60.61 | 70.94 | 80.21 | 87.67 |
| 15G | 61.37 | 71.78 | 80.98 | 88.41 |
| 20A | 61.49 | 72.02 | 80.86 | 87.86 |
| 20B | 61.17 | 71.29 | 80.25 | 87.67 |
| 21A | 61.00 | 71.76 | 80.93 | 88.52 |
| 21B | 62.41 | 72.81 | 81.85 | 89.17 |
| 22A | 61.41 | 71.51 | 80.86 | 88.26 |
| 22B | 61.03 | 70.85 | 80.48 | 88.15 |

ARMY CO STANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | 100.00---- 95.00 |  | $\begin{gathered} \text { Score } \\ 90.00 \end{gathered}$ | 85.00 |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 15 G | 0.75 | 0.85 | 0.77 | 0.74 |
| 20A | 0.87 | 1.09 | 0.65 | 0.19 |
| 208 | 0.55 | 0.36 | 0.04 | 0.00 |
| 21A | 0.38 | 0.82 | 0.72 | 0.85 |
| 218 | 1.80 | 1.87 | 1.64 | 1.51 |
| 22A | 0.80 | 0.57 | 0.65 | 0.59 |
| 228 | 0.42 | -0.08 | 0. | 0.4 |

ARMY FA STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

| Test | Cut | Soo |
| :---: | :---: | :---: |
|  | 95.00 |  |


| REF | 61.71 | 72.98 | 81.90 | 89.07 |
| :--- | :--- | :--- | :--- | :--- |
| 15G | 62.09 | 73.80 | 82.47 | 89.53 |
| $20 A$ | 61.77 | 73.20 | 81.63 | 88.68 |
| 20B | 61.50 | 73.26 | 81.97 | 88.85 |
| $21 A$ | 61.93 | 73.31 | 82.13 | 88.91 |
| 218 | 62.65 | 7335 | 82.93 | 89.67 |
| $22 A$ | 62.22 | 73.42 | 82.19 | 89.14 |
| 22B | 61.82 | 73.24 | 82.59 | 89.48 |

ARMY FA STANDARD SOORE CONPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | --..----- Cut |  | Score |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 100.00 | 95.00 | 90.00 | 85.00 |
| $15 G$ | 0.38 | 0.82 | 0.58 | 0.4 |
| 20A | 0.06 | 0.22 | -0.27 | -0.39 |
| 20B | -0.22 | 0.28 | 0.07 | -0.22 |
| 21A | 0.22 | 0.33 | 0.23 | -0.16 |
| 218 | 0.94 | 0.77 | 1.03 | 0.60 |

ARMY FA STANDARD SCOPE COMPOSITE, COn't.
22A
0.50
0.44
0.29
0.07
0.40

ARMY OF STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

| $s t$ | Cut | Score |
| :---: | :---: | :---: |
|  | 105.00100 .00 | 95.00 |


| REF | 53.10 | 64.78 | 75. | 84.67 |
| :---: | :---: | :---: | :---: | :---: |
| 156 | 52.38 | 65.26 |  |  |
| 20A | 54.20 | 65.97 | 75.96 | 84.94 |
| 208 | 53.18 | 64.96 | 74.97 | 84.56 |
| 21A | 53.00 | 65.29 | 76.18 | 85.60 |
| 218 | 53.22 | 65.66 | 76.88 | 86.21 |
| 22A | 53.69 | 65.26 | 75.47 | 85.18 |
| 228 | 52.84 | 64.46 | 75.4 | 84 |

ARMY OF STANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
$\begin{array}{ccccc}\text { Test } \\ & 105.00100 .00 & & \\ 95.00 & 90.00\end{array}$

| 15 G | -0.72 | 0.47 | 1.03 | 1.51 |
| ---: | ---: | ---: | ---: | ---: |
| 20 A | 1.09 | 1.19 | 0.44 | 0.26 |
| 20 B | 0.07 | 0.17 | -0.54 | -0.11 |
| 21 A | -0.10 | 0.51 | 0.66 | 0.93 |
| 218 | 0.11 | 0.88 | 1.37 | 1.54 |
| 22 A | 0.58 | 0.48 | -0.04 | 0.51 |
| 22 B | -0.26 | -0.32 | -0.10 | 0.28 |

ARMY ST STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test


| REF | 27.46 | 39.07 | 50.83 | 61.09 | 71.90 | 81.34 | 88.11 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 15G | 28.28 | 39.56 | 51.16 | 61.52 | 72.96 | 82.35 | 89.27 |
| 20A | 28.44 | 39.50 | 50.87 | 61.25 | 71.83 | 81.03 | 88.39 |
| 20B | 28.20 | 38.82 | 50.73 | 60.88 | 71.40 | 80.75 | 88.29 |
| $21 A$ | 27.96 | 38.80 | 50.15 | 60.49 | 71.57 | 81.18 | 88.68 |
| 218 | 28.13 | 39.40 | 50.85 | 61.25 | 72.31 | 82.14 | 89.09 |
| 22A | 28.25 | 39.96 | 51.85 | 61.83 | 71.92 | 81.00 | 88.16 |
| 22B | 28.07 | 39.05 | 51.09 | 61.69 | 72.39 | 81.18 | 88.47 |

## ARMY ST STANDARD SCORE COMPOSITE

Differences in Percentages At or Above Cut Scores (Test-REF)

|  | 115.00 | 110.00 | 105.00 |  | 95.00 | 90.00 | 85.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15G | 0.82 | 0.49 | 0.33 | 0.44 | 1.05 | 1.01 | 1.16 |
| 20A | 0.98 | 0.43 | 0.04 | 0.16 | -0.07 | -0.31 | 0.27 |
| 20B | 0.74 | -0.25 | -0.10 | -0.21 | -0.51 | -0.59 | 0.18 |
| 21A | 0.50 | -0.26 | -0.68 | -0.59 | -0.34 | -0.16 | 0.56 |
| 218 | 0.67 | 0.33 | 0.01 | 0.17 | 0.40 | 0.80 | 0.97 |
| 22A | 0.79 | 0.89 | 1.02 | 0.74 | 0.02 | -0.34 | 0.05 |
| 22B | 0.61 | -0.02 | 0.26 | 0.60 | 0.49 | -0.16 | 0.35 |

MARINE CORPS MM STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)


|  | REF | 27.12 | 47.26 | 66.91 |
| :--- | :--- | :--- | :--- | :--- |
| 15 G | 25.98 | 46.35 | 65.82 | 84.90 |
| 20A | 26.80 | 47.92 | 67.56 | 84.74 |
| 20 B | 26.27 | 46.97 | 66.61 | 84.01 |
| 21 A | 26.38 | 47.04 | 66.49 | 84.73 |
| 21 B | 26.45 | 48.22 | 68.37 | 85.73 |
| $22 A$ | 27.05 | 47.49 | 66.84 | 83.99 |
| 22 B | 26.59 | 47.62 | 66.86 | 84.62 |

MARINE CORPS MM STANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF')


| 15G | -1.14 | -0.91 | -1.09 | 0.84 |
| :--- | :--- | ---: | ---: | ---: |
| 20A | -0.32 | 0.66 | 0.65 | 1.11 |
| 20B | -0.85 | -0.29 | -0.29 | 0.35 |
| 21A | -0.74 | -0.22 | -0.42 | 0.83 |
| 21B | -0.67 | 0.96 | 1.47 | 1.83 |
| 22A | -0.07 | 0.23 | -0.07 | 0.09 |
| 22B | -0.53 | 0.37 | -0.05 | 0.72 |

MARINE CORPS CL STANDAPD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

|  | $\qquad$ Cut Score 120.00110 .00101 .00 |  |  | 90 | 80.00 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| F | 17.25 | 42.00 | 66 | 86 |  |
| 15G | 18.44 | 43.10 | 67.94 | 87.16 | . 06 |
| 20A | 17.42 | 41.84 | 66.27 | 86.44 | 95.61 |
| OB | 18.02 | 42 | 66 |  |  |

MARINE CORPS CL STANDARD SCORE COMPOSITE, COn't.

| 21A | 17.23 | 41.84 | 66.62 | 87.09 | 95.96 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 21B | 17.19 | 41.57 | 66.96 | 87.26 | 96.00 |
| 22A | 17.83 | 42.23 | 66.46 | 86.21 | 95.62 |
| 22B | 17.02 | 41.75 | 66.90 | 86.76 | 95.81 |

MARINE CORPS CL SIANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test

$$
\begin{array}{ll}
-0 .- \\
120.00 & 110.00 \quad 101.00 \\
\hline 0.00 & 80.00
\end{array}
$$

| 15G | 1.19 | 1.10 | 1.11 | 0.73 | 0.28 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| 20A | 0.16 | -0.16 | -0.55 | 0.01 | -0.17 |
| 20B | 0.77 | 0.15 | -0.02 | 0.24 | 0.15 |
| 21A | -0.03 | -0.16 | -0.20 | 0.66 | 0.18 |
| $21 B$ | $-C .06$ | -0.43 | 0.13 | 0.83 | 0.23 |
| $22 A$ | 0.58 | 0.23 | -0.36 | -0.22 | -0.16 |
| $22 B$ | -0.23 | -0.25 | 0.08 | 0.33 | 0.04 |

MARINE CORPS GT STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

| Test | $-\ldots-\ldots-\ldots$. Cut | Score | $-\ldots-\ldots$ |  |
| :--- | ---: | :--- | :--- | :--- | :--- |
|  | 110.00 | 100.00 | 90.00 | 80.00 |
| REF | 39.56 | 61.40 | 79.45 | 92.48 |
| 15G | 39.87 | 61.34 | 79.95 | 92.98 |
| 20A | 40.12 | 61.07 | 79.66 | 92.59 |
| 20B | 39.47 | 60.83 | 79.53 | 92.66 |
| 21A | 39.45 | 61.23 | 79.51 | 93.06 |
| 21B | 40.22 | 62.31 | 80.59 | 93.06 |
| 22A | 40.21 | 62.07 | 79.70 | 92.60 |
| 22B | 39.59 | 61.44 | 80.17 | 93.00 |

MARINE CORPS GT STANDARD SCORE CAMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test


| 15G | 0.31 | -0.06 | 0.50 | 0.50 |
| :--- | ---: | ---: | ---: | ---: |
| 20A | 0.56 | -0.33 | 0.21 | 0.12 |
| 20B | -0.08 | -0.56 | 0.07 | 0.18 |
| 21A | -0.11 | -0.17 | 0.06 | 0.58 |
| 21B | 0.67 | 0.92 | 1.14 | 0.58 |
| 22A | 0.66 | 0.67 | 0.25 | 0.13 |
| 22B | 0.03 | 0.05 | 0.71 | 0.52 |

MARINE CORPS EL STANDARD SCORE COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test

$115.00 \quad 110.00 \quad 100.00 \quad 90.00$

| REF | 25.72 | 36.22 | 57.75 | 77.95 |
| :--- | :--- | :--- | :--- | :--- |
| 15G | 25.31 | 35.17 | 57.42 | 77.48 |
| 20A | 26.46 | 36.44 | 57.94 | 78.22 |
| 20B | 26.66 | 36.12 | 58.11 | 77.69 |
| 21A | 25.61 | 35.17 | 58.04 | 77.69 |
| 21B | 25.18 | 35.60 | 58.62 | 79.04 |
| 22A | 25.49 | 36.41 | 58.45 | 77.76 |
| 22B | 25.91 | 35.75 | 58.25 | 78.11 |

MARINE CORPS EL STANDARD SCORE COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
$\begin{array}{cc}\text { Test } \\ \\ 115.00 & 110.00 \quad 100.00 \quad 90.00\end{array}$

| 15G | -0.41 | -1.05 | -0.33 | -0.47 |
| :--- | ---: | ---: | ---: | ---: |
| 20A | 0.74 | 0.21 | 0.19 | 0.27 |
| 20B | 0.93 | -0.11 | 0.35 | -0.26 |
| 21A | -0.11 | -1.06 | 0.29 | -0.26 |
| 21B | -0.54 | -0.63 | 0.87 | 1.09 |
| 22A | -0.23 | 0.18 | 0.70 | -0.19 |
| 22B | 0.18 | -0.47 | 0.49 | 0.16 |

NAVY EL SUM OF SUBTEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
$\begin{array}{cc}\text { Test } \\ 218.00 & 204.00 \quad 200.00 \quad 190.00\end{array}$

| REF | 34.94 | 51.68 | 56.54 | 69.22 |
| :--- | :--- | :--- | :--- | :--- |
| 15G | 34.13 | 51.17 | 56.21 | 68.66 |
| 20A | 35.44 | 52.31 | 57.00 | 69.12 |
| 20B | 35.11 | 51.50 | 57.14 | 68.63 |
| 21A | 34.01 | 51.44 | 56.69 | 68.82 |
| 21B | 34.34 | 52.27 | 57.62 | 70.08 |
| 22A | 35.08 | 52.24 | 57.30 | 68.71 |
| 22B | 34.70 | 52.13 | 57.04 | 69.28 |

NAVY EL SUM OF SUBTEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test
-------- Cut Score
218.00204 .00200 .00190 .00

| 15G | -0.80 | -0.51 | -0.33 | -0.56 |
| :--- | ---: | ---: | ---: | ---: |
| 20A | 0.50 | 0.63 | 0.46 | -0.11 |
| 20B | 0.17 | -0.18 | 0.60 | -0.59 |
| 21A | -0.93 | -0.24 | 0.15 | -0.41 |

NAVY EL SUM OF SUBTEST STANDARD SCDRES COMPOSITE, COn't.

| 21B | -0.60 | 0.59 | 1.08 | 0.86 |
| ---: | ---: | ---: | ---: | ---: |
| 22A | 0.14 | 0.56 | 0.76 | -0.52 |
| 22B | -0.24 | 0.15 | 0.50 | 0.06 |

NAVY E SUM OF SUBTEST STANDARD SCORES COMPOSITE
percentages At or Above Cut Scores (Ordered High to Low)

| Test | 214.00 | $210.00 \text { Cut Score } 204.00200 .00$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| REF | 41.85 | 46.02 | 53.24 | 57.81 | 62.17 |
| 15G | 42.50 | 46.62 | 52.93 | 57.81 | 62.67 |
| 20A | 42.56 | 47.01 | 53.68 | 58.10 | 62.65 |
| 208 | 41.99 | 46.57 | 53.33 | 57.68 | 62.22 |
| 218 | 42.12 | 46.53 | 53.22 | 57.55 | 61.79 |
| 21B | 42.38 | 46.76 | 53.61 | 58.33 | 62.67 |
| 22A | 42.74 | 47.30 | 53.88 | 58.38 | 62.98 |
| 22B | 42.24 | 46.65 | 53.36 | 58. | 62 |

NAVY E SUM OF SUBTEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | 214.00210 .00204 .00200 .00196 .00 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 156 | 0.65 | 0.60 | -0.31 | -0.00 | 0.50 |
| 20A | 0.71 | 0.99 | 0.45 | 0.28 | 0.48 |
| 20 B | 0.14 | 0.55 | 0.09 | -0.14 | 0.06 |
| 21A | 0.26 | 0.51 | -0.02 | -0.27 | -0.37 |
| 218 | 0.53 | 0.74 | 0.37 | 0.51 | 0.50 |
| 22A | 0.89 | 1.28 | 0.64 | 0.57 | 0.81 |
| 228 | 0.38 | 0.63 | 0.12 | 0.67 | 0.7 |

NAVY CL SUM OF SUBTEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test Cut Score
160.00

| REF | 50.10 |
| :--- | :--- |
| $15 G$ | 49.68 |
| $20 A$ | 50.17 |
| $20 B$ | 50.41 |
| $21 A$ | 50.03 |
| $21 B$ | 49.61 |
| $22 A$ | 50.34 |
| $22 B$ | 49.80 |

NAVY CL SUM OF SUBIEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test Cut Score
160.00

| $15 G$ | -0.42 |
| :--- | ---: |
| $20 A$ | 0.07 |
| $20 B$ | 0.31 |
| $21 A$ | -0.07 |
| $21 B$ | -0.49 |
| $22 A$ | 0.23 |
| $22 B$ | -0.30 |

NAVY GI SUM OF SUBTEST SIANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)

|  | 115.00 | 113.00 | 108.00 | 103.0 | 97.00 | 96.00 | 89.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| REF | 23.67 | 28.46 | 41.72 | 55.11 | 69.89 | 72.09 | 84.21 |
| 15G | 24.22 | 29.18 | 42.04 | 54.70 | 68.95 | 71.15 | 83.91 |
| 20A | 24.04 | 28.95 | 41.75 | 54.30 | 69.58 | 72.14 | 84.77 |
| 20B | 24.06 | 29.04 | 41.47 | 54.34 | 68.67 | 70.91 | 84.49 |
| 21A | 23.54 | 28.33 | 41.18 | 54.40 | 69.24 | 71.46 | 84.62 |
| 218 | 23.31 | 28.30 | 41.56 | 55.12 | 69.56 | 72.00 | 85.20 |
| 22A | 24.55 | 29.56 | 41.94 | 55.04 | 69.04 | 71.16 | 84.37 |
| 22B | 23.61 | 28.90 | 40.93 | 54.21 | 69.47 | 71.34 | 84.49 |

NAVY GT SUM OF SUBIEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)

| Test | Cut Score |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 115.00 | 113.00 | 108.00 | 103.00 | 97.00 | 96.00 | 89.00 |
| 15G | 0.55 | 0.73 | 0.32 | -0.41 | -0.94 | -0.94 | -0.30 |
| 20A | 0.37 | 0.49 | 0.03 | -0.81 | -0.31 | 0.05 | 0.56 |
| 20 B | 0.39 | 0.58 | -0.25 | -0.76 | -1.21 | -1.18 | 0.28 |
| 21A | -0.13 | -0.13 | -0.54 | -0.70 | -0.65 | -0.63 | 0.41 |
| 21B | -0.36 | -0.16 | -0.16 | 0.02 | -0.33 | -0.09 | 0.99 |
| 22A | 0.88 | 1.10 | 0.21 | -0.07 | -0.84 | -0.93 | 0.17 |
| 22 B | -0.06 | 0.44 | -0.79 | -0.90 | -0.42 | -0.75 | 0.28 |

NAVY ME SUM OF SUBTEST STMNDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test --. Cut Score -....

| REF | 32.46 | 46.95 | 60.30 |
| :--- | :--- | :--- | :--- |
| $15 G$ | 31.69 | 47.38 | 60.72 |
| $20 A$ | 32.78 | 48.23 | 61.27 |
| $20 B$ | 32.10 | 47.54 | 60.18 |

NAVY ME SUM OF SUBTEST STANDARD SCORES COMPOSITE, COn't.

| $21 A$ | 31.63 | 46.84 | 60.29 |
| :--- | :--- | :--- | :--- |
| 218 | 32.05 | 47.60 | 61.14 |
| $22 A$ | 33.00 | 47.51 | 60.30 |
| $22 B$ | 32.43 | 47.27 | 59.89 |

NAVY ME SUM OF SUBTEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test
$167.00 \quad$ Cut Score $158.00 \quad 150.00$

| 15G | -0.78 | 0.43 | 0.41 |
| :--- | ---: | ---: | ---: |
| 20A | 0.31 | 1.28 | 0.96 |
| 20B | -0.36 | 0.59 | -0.12 |
| 21A | -0.83 | -0.11 | -0.02 |
| 21B | -0.42 | 0.65 | 0.83 |
| 22A | 0.53 | 0.56 | -0.00 |
| 22B | -0.03 | 0.32 | -0.41 |

NAVY EG SUM OF SUBTEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test $C u t$ Score
96.00
REF 69.87
15G $\quad 70.46$
20A 70.12
20B 69.47
21A 70.81
$218 \quad 70.90$
22A 69.70
22B 69.53

NAVY EG SUM OF SUBTEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test Cut Score
96.00

| 15G | 0.59 |
| :--- | ---: |
| $20 A$ | 0.24 |
| 20 B | -0.40 |
| 21A | 0.94 |
| 218 | 1.03 |
| 22A | -0.17 |
| $22 B$ | -0.34 |

NAVY CT SUM OF SUBIEST STMNDARD SCOPES COMPOSITE
Percentages at or Above Cut Scores (Ordered High to Low)
Test Cut Score 202.00

REF 65.51
15G 64.80
20A 65.54
$20 \mathrm{~B} \quad 65.21$
21A 65.17
21B 64.80
22A 65.13
$228 \quad 65.25$
NAVY CT SUM OF SUBTEST STANDARD SCORES COMROSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test Cut Score 202.00

15G -0.71
20A 0.03
20B -0.30
21A -0.34
21B -0.71
22A -0.38
22B -0.26

NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test - Cut Score -
REF $\quad 34.67 \quad 63.77$
$15 G \quad 35.91 \quad 64.04$
20A $35.75 \quad 63.23$
$\begin{array}{lll}208 & 35.44 & 62.96\end{array}$
21A $\quad 35.31 \quad 62.54$
21B $\quad 35.17 \quad 63.14$
22A $\quad 35.86 \quad 63.64$
$\begin{array}{lll}22 B & 35.23 & 63.57\end{array}$

NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
$\begin{array}{rl}\text { Test } & \text { Cut Score } \\ 165.00 & 149.00\end{array}$

| $15 G$ | 1.24 | 0.27 |
| :--- | :--- | ---: |
| 20 A | 1.08 | -0.54 |
| 20 B | 0.77 | -0.81 |

NAVY HM SUM OF SUBTEST STANDARD SCORES COMPOSITE, COn't.

| $21 A$ | 0.64 | -1.23 |
| :--- | :--- | :--- |
| $21 B$ | 0.51 | -0.63 |
| $22 A$ | 1.19 | -0.13 |
| $22 B$ | 0.56 | -0.20 |

NAVY ST SUM OF SUBTEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test Cut Score 147.00

REF 98.74
15G 98.86
20A 98.54
20B 98.78
21A 98.62
21B 98.61
22A 98.79
$22 B \quad 98.65$
NAVY ST SUM OF SUBTEST SIANDARD SCORES COMPOSITE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test Cut Score 147.00
$15 G \quad 0.12$
20A -0.20
$20 B \quad 0.04$
21A - 0.12
$21 B-0.13$
22A 0.05
$22 B-0.09$

NAVY MR SUM OF SUBIEST STANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test -..-. Cut Score -..164.00158 .00130 .00
$\begin{array}{llll}\text { REF } & 36.79 & 45.51 & 83.68\end{array}$
$\begin{array}{llll}15 G & 36.30 & 45.41 & 84.43\end{array}$
20A $\quad 37.05 \quad 46.17 \quad 84.71$
$\begin{array}{llll}20 B & 36.41 & 45.53 & 83.97\end{array}$
$\begin{array}{llll}21 A & 36.34 & 45.31 & 84.85\end{array}$
$\begin{array}{llll}21 B & 36.53 & 46.33 & 85.58\end{array}$
$\begin{array}{llll}22 A & 37.22 & 46.23 & 84.49\end{array}$
$\begin{array}{llll}22 B & 36.48 & 46.03 & 84.08\end{array}$

NAVY MR SUM OF SUBTEST SINNDNPD SCOPES COMPOSTIE
Differences in Percentages At or Above Cut Scores (Test-REFF)
Test $\quad 164.00$ Cut Score 158.00130 .00

| 156 | -0.49 | -0.10 | 0.74 |
| :---: | :---: | :---: | :---: |
| 20A | 0.27 | 0.66 | 1.02 |
| 208 | -0.38 | 0.02 | 0.29 |
| 21A | -0.45 | -0.20 | 1.16 |
| 218 | -0.26 | 0.82 | 1.90 |
| 22A | 0.43 | 0.72 | 0.80 |
| 228 | -0.30 |  | 0.4 |

NAVY BC SUM OF SUBTEST SIANDARD SCORES COMPOSITE
Percentages At or Above Cut Scores (Ordered High to Low)
Test - Cut Score 153.00147 .00
$\begin{array}{lll}\text { REF } & 61.24 \quad 72.25\end{array}$
$15 G \quad 61.96 \quad 73.14$
20A 60.5571 .93
20B $\quad 60.55 \quad 71.92$
21A $60.66 \quad 72.53$
21B $\quad 60.87 \quad 72.42$
22A $\quad 60.70 \quad 72.13$
$228 \quad 61.07 \quad 72.75$
NAVY BC SUM OF SUBTEST STANDARD SCORES CONPOSTTE
Differences in Percentages At or Above Cut Scores (Test-REF)
Test - Cut Score -
53.00147 .00

| 15 G | 0.72 | 0.88 |
| :--- | ---: | ---: |
| 20 A | -0.69 | -0.32 |
| 20 B | -0.69 | -0.33 |
| 21 A | -0.58 | 0.28 |
| 21 B | -0.37 | 0.17 |
| 22 A | -0.54 | -0.12 |
| 22 B | -0.17 | 0.49 |

# ASVAB 20, 21, AND 22 IOT\&E SUPPLEMENT 

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Defense Manpower Data Center

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ASVAB 20, 21, AND 22 IOTRE SUPPLEMENT TABLES 1-26

Table 1
ASVAB Subtests, Numbers of Items, Time Limits, and Normative Means and Standard Deviations

|  | Items | Time <br> (min. | Mean | S.D. |  |
| :--- | ---: | :---: | :---: | ---: | ---: |
| Subtest |  |  |  |  |  |
| General Science (GS) | 25 | 11 | 15.950 | 5.010 |  |
| Arithmetic Reasoning (AR) | 30 | 36 | 18.009 | 7.373 |  |
| Word Knowledge (WK) | 35 | 11 | 26.270 | 7.710 |  |
| Paragraph Comprehension (PC) | 15 | 13 | 11.011 | 3.355 |  |
| Numerical Operations (NO) | 50 | 3 | 37.236 | 10.800 |  |
| Coding Speed (CS) | 84 | 7 | 47.606 | 16.763 |  |
| Auto and Shop Information (AS) | 25 | 11 | 14.317 | 5.550 |  |
| Math Knowledge (MK) : | 25 | 24 | 13.578 | 6.393 |  |
| Mechanical Comprehension (MC) | 25 | 19 | 14.165 | 5.349 |  |
| Electronics Information (EI) | 20 | 9 | 11.569 | 4.236 |  |
| Verbal (VE = WK + PC) | 50 | - | 37.281 | 10.595 |  |
|  |  |  |  |  |  |

Table 2
Number of Subjects, by Test Form

| ASVAB Form | All Tested from 10/1/92 to 1/15/93 | Initial Testing | Only | After Editing for Extreme Inbalancing |
| :---: | :---: | :---: | :---: | :---: |
| 15 g | 18852 | 15959 |  | 13312 |
| (Operational) | 13.5\% | 13.5\% |  | 13.4\% |
| 15h | 18027 | 15342 |  | 12931 |
| (Reference) | 12.9\% | 13.0\% |  | 13.0\% |
| 202 | 18613 | 15647 |  | 13097 |
|  | 13.3\% | 13.2\% |  | 13.2\% |
| 20b | 17973 | 15237 |  | 12778 |
|  | 12.8\% | 12.9\% |  | 12.9\% |
| 21 a | 17688 | 14951 |  | 12532 |
|  | 12.6\% | $12.6 \%$ |  | 12.6\% |
| 21b | 16926 | 14369 |  | 12060 |
|  | 12.1\% | 12.1\% |  | 12.2\% |
| 22a | 16350 | 13753 |  | 11558 |
|  | 11.7\% | $11.6 \%$ |  | 11.6\% |
| 22 b | 15633 | 13007 |  | 10986 |
|  | 11.2\% | 11.0\% |  | 11.1\% |
| Total | 140062 | 118265 |  | 99254 |
| Cumulative |  | 15.6\% |  | $29.1 \%$ |
| Percent |  |  |  |  |
| Deleted |  |  |  |  |

Table 3
Number of Subjects, Percentage of Subjects, and Contribution to Chi-Square, by Gender, Race, and Education


Male

| Number | 10712 | 10413 | 10565 | 10147 | 10130 | 9780 | 9276 | 8876 | 79899 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Chi-Sq | 0.0016 | 0.0012 | 0.0458 | 1.8845 | 0.1732 | 0.5304 | 0.0851 | 0.1181 |  |
| Percent | 80.47 | 80.53 | 80.67 | 79.41 | 80.83 | 81.09 | 80.26 | 80.79 | 80.50 |

Gender $x$ ASVAB Form Pearscan Chi-Square $=14.564$ (d.f. $=7$, pr. $=.042$ )
Non-High School Graduates (including Current Students)

| Number | 4647 | 4513 | 4664 | 4437 | 4430 | 4242 | 3980 | 3869 | 34782 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Chi-Sq | 0.0693 | 0.0752 | 1.2048 | 0.3726 | 0.3350 | 0.0588 | 1.2208 | 0.0951 |  |
| Percent | 34.91 | 34.90 | 35.61 | 34.72 | 35.35 | 35.17 | 34.44 | 35.22 | 35.04 |

High School Graduates

| Number | 8047 | 7803 | 7829 | 7758 | 7517 | 7290 | 7071 | 6629 | 59944 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Chi-Sq | 0.0066 | 0.0056 | 0.8269 | 0.2155 | 0.3524 | 0.0057 | 1.1759 | 0.0053 |  |
| Percent | 60.45 | 60.34 | 59.78 | 60.71 | 59.98 | 60.45 | 61.18 | 60.34 | 60.39 |

## Post-Secondary Echucation

| Number | 618 | 615 | 604 | 583 | 585 | 528 | 507 | 488 | 4528 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Chi-Sq | 0.1886 | 1.0666 | 0.0709 | 0.0000 | 0.3088 | 0.8943 | 0.7800 | 0.3469 |  |
| Percent | 4.64 | 4.76 | 4.61 | 4.56 | 4.67 | 4.38 | 4.39 | 4.44 | 4.56 |
| Education $x$ ASVAB Form Pearson Chi-Square | $=9.862$ | (d.f. $=14$, | pr. $=.785$ ) |  |  |  |  |  |  |

Caucasian

| Number | 10029 | 9733 | 9866 | 9621 | 9369 | 9117 | 8682 | 8241 | 74658 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Chi-Sq | 0.0250 | 0.0042 | 0.0215 | 0.0094 | 0.3503 | 0.2289 | 0.0161 | 0.0617 |  |
| Percent | 75.34 | 75.27 | 75.33 | 75.29 | 74.76 | 75.60 | 75.12 | 75.01 | 75.22 |
| Non-Caucasian |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Number | 3283 | 3198 | 3231 | 3157 | 3163 | 2943 | 2876 | 2745 | 24596 |
| Chi-Sq | 0.0760 | 0.0128 | 0.0652 | 0.0285 | 1.0632 | 0.6949 | 0.0488 | 0.1872 |  |
| Percent | 24.66 | 24.73 | 24.67 | 24.71 | 25.24 | 24.40 | 24.88 | 24.99 | 24.78 |

Race $\times$ ASVAB Form Pearson Chi-Square $=2.894$ (d.f. $=7, \mathrm{pr} .=.895$ )

Table 4
Subtest Raw Score Mean, Standard Deviation, Skewness, and Kurtosis, by ASVAB Form


Table 5
Degrees of Polynomials and Tests of Significance of Item-Order Effects

| Subtests | Forms | Degree of polynomial | Chi-Square | D.F. | Prob. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| GS | 20adeb | 9 (6\&9) | 13.688 | 9 | 0.139 |
|  | 21acb | 7 (7\&6) | 14.154 | 7 | 0.049 |
|  | 22asbb | 6 (6\&6) | 1.393 | 6 | 0.966 |
| CS | 20a\&b | 8 (8\&8) | 13.147 | 8 | 0.107 |
|  | 21a\&b | 8 (8\&8) | 34.263 | 8 | *0.000 |
|  | 22a\&b | 9 (9\&8) | 22.293 | 9 | 0.008 |
| AS | 20a\&b | 7 (787) | 10.767 | 7 | 0.149 |
|  | 21acb | 7 (7\&7) | 16.088 | 7 | 0.024 |
|  | 22asbb | 9 (789) | 7.284 | 9 | 0.608 |
| MC | 20asbb | 7 (7\&7) | 7.614 | 7 | 0.368 |
|  | 21ackb | 9 (9\&7) | 15.729 | 9 | 0.083 |
|  | 22asb | 9 (789) | 3.548 | 9 | 0.939 |
| EI | 20aseb | 9 (9\&5) | 12.983 | 9 | 0.163 |
|  | 21asbb | 7 (784) | 13.586 | 7 | 0.059 |
|  | 22a\&b | 9 (9\&9) | 20.675 | 9 | 0.014 |

[^8]
## Table 6

Means, Standard Deviations, and Number of Terms in Polynomial Smoothings for Equating

|  | Eorm | 15G | 15H | 20 A 20B | 218218 | 22 A 22B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GS | Mean | 16.849 | 16.406 | 17.304* | 17.506* | 17.146* |
|  | SD | 4.362 | 4.275 | 4.428 | 4.255 | 4.400 |
|  | Terms | 6 | 4 | 6 | 7 | 6 |
| AR | Mean | 19.332 | 19.016 | 20.00118 .596 | 19.61119 .338 | 19.46819 .354 |
|  | SD | 6.188 | 6.282 | 5.8126 .440 | 6.3595 .705 | 6.0556 .227 |
|  | Terms | 7 | 7 | 65 | 107 | 94 |
| WK | Mean | 27.333 | 27.610 | 27.40427 .090 | 27.27127 .073 | 27.17527 .240 |
|  | SD | 5.552 | 5.361 | 5.5946 .150 | 5.7875 .604 | 5.7335 .691 |
|  | Terms | 7 | 7 | 79 | 79 | 77 |
| PC | Mean | 12.353 | 11.599 | 11.73211 .668 | 11.99911 .641 | 12.07011 .423 |
|  | SD | 2.492 | 2.551 | 2.7272 .484 | $2.320 \quad 2.667$ | 2.5882 .849 |
|  | Terms | 8 | 7 | 77 | 56 | 47 |
| NO | Mean | 36.781 | 37.161 | 36.564* | 36.222* | 36.919* |
|  | SD | 8.639 | 8.613 | 8.380 | 8.600 | 8.630 |
|  | Terms | 9 | 9 | 9 | 10 | 7 |
| CS | Mean | 51.296 | 50.966 | 48.857* | 49.84349 .174 | 50.370* |
|  | SD | 12.555 | 12.530 | 12.106 | 12.25212 .003 | 12.528 |
|  | Terms | 8 | 8 | 8 | 88 | 10 |
| AS | Mean | 14.537 | 14.840 | 14.853* | 15.301* | 15.116* |
|  | SD | 5.060 | 4.930 | 4.704 | 4.838 | 5.128 |
|  | Terms | 9 | 9 | 9 | 7 | 9 |
| MK | Mean | 15.345 | 15.066 | 15.03414 .698 | 15.01915 .027 | 1.5.270 14.705 |
|  | SD | 5.439 | 5.532 | 5.7195 .603 | 5.7285 .429 | 6.0025 .854 |
|  | Terms | 7 | 7 | 5 | $\begin{array}{ll}5 & 7\end{array}$ | 6.02 |
| MC | Mean | 15.860 | 15.170 | 15.445* | 16.043* | 15.563* |
|  | SD | 4.647 | 4.952 | 4.868 | 4.739 | 4.766 |
|  | Terms | 7 | 8 | 7 | 9 | 9 |
| EI | Mean | 11.778 | 11.771 |  |  |  |
|  | SD | 3.536 | 3.600 | 3.676 | 3.706 | 3.670 |
|  | Terms | 9 | 7 | 9 | 9 | 9 |
| VE | Mean | 39.686 | 39.209 | 39.13638 .758 | 39.26938 .714 | 39.24538 .663 |
|  | SD | 7.556 | 7.301 | 7.7908 .029 | 7.5917 .719 | 7.7507 .996 |
|  | Terms | 9 | 9 | 99 | 910 | 97 |

[^9]Table 7
Root Mean Square Difference Between Equatings, by Sublest and Form

| AFOT Subtest andForm | Raw vs. Linear | Raw vs. Polymomial | NON-AFOT Subtest and Form | Raw vs. Innear | Raw <br> vs. <br> Rolymomial |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR 15g | 0.140 | 0.044 | GS 15g | 0.278 | 0.058 |
| AR 20a | 0.415 | 0.037 | GS 20a/b | 0.337 | 0.052 |
| AR 20b | 0.153 | 0.055 | GS 21a/b | 0.613 | 0.074 |
| AR 21a | 0.226 | 0.041 | GS 22a/b | 0.619 | 0.065 |
| AR 21b | 0.527 | 0.044 |  |  |  |
| AR 22a | 0.246 | 0.028 | NO 15 g | 0.138 | 0.063 |
| AR 22b | 0.152 | 0.047 | NO 20a/b | 0.294 | 0.058 |
|  |  |  | NO 21a/b | 0.307 | 0.055 |
| WK 15 g | 0.214 | 0.038 | NO 22a/b | 0.130 | 0.052 |
| WK 20a | 0.147 | 0.033 |  |  |  |
| WK 20b | 0.433 | 0.039 | CS 15g | 0.248 | 0.061 |
| WK 21a | 0.298 | 0.054 | CS 20a/b | 0.224 | 0.083 |
| WK 21b | 0.311 | 0.046 | CS 21a | 0.244 | 0.075 |
| WK 22a | 0.244 | 0.039 | CS 21b | 0.238 | 0.064 |
| WK 22b | 0.268 | 0.040 | CS 22a/b | 0.188 | 0.065 |
| PC 15g | 0.443 | 0.018 | AS 15 g | 0.207 | 0.042 |
| PC 20a | 0.232 | 0.050 | AS 20a/b | 0.291 | 0.037 |
| PC 20b | 0.506 | 0.026 | AS 21a/b | 0.221 | 0.041 |
| PC 21a | 0.324 | 0.041 | AS 22a/b | 0.253 | 0.037 |
| PC 21b | 0.167 | 0.069 |  |  |  |
| PC 22a | 0.183 | 0.046 | MC 15g | 0.549 | 0.050 |
| PC 22b | 0.362 | 0.036 | MC 20a/b | 0.244 | 0.038 |
|  |  |  | MC 21a/b | 0.292 | 0.041 |
| MK 159 | 0.189 | 0.039 | MC 22a/b | 0.203 | 0.048 |
| MK 20a | 0.237 | 0.031 |  |  |  |
| MK 20b | 0.351 | 0.033 | EI 15g | 0.614 | 0.041 |
| MK 21a | 0.318 | 0.051 | EI 20a/b | 0.238 | 0.041 |
| MK 21b | 0.199 | 0.038 | EI 21a/b | 0.327 | 0.036 |
| MK 22a | 0.246 | 0.040 | EI 22a/b | 0.249 | 0.046 |
| MK 22b | 0.245 | 0.045 |  |  |  |
| VE 15g | 0.150 | 0.047 |  |  |  |
| VE 20a | 0.166 | 0 |  |  |  |
| VE 20b | 0.370 | 0 |  |  |  |
| VE 21a | 0.163 | 0. |  |  |  |
| VE 21b | 0.248 | 0.039 |  |  |  |
| VE 22a | 0.219 | 0.037 |  |  |  |
| VE 22b | 0.284 | 0.053 |  |  |  |

Table 8
Percentage of Subjects for Which Equatings Differ by More Than .5 Standard Score Points, by Subtest and Form

| AFOT <br> Subtest <br> and Form | Raw Vs. Linear | Raw vs. Polymomial | $\begin{aligned} & \text { NaN-AFQT } \\ & \text { Subtest } \\ & \text { and Form } \end{aligned}$ | Raw vs. Linear | Raw V8. Polymomial |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR 159 | 0.06 | 0.00 | GS 159 | 5.06 | 0.00 |
| AR 20a | 5.98 | 0.00 | GS 20a/b | 7.49 | 0.00 |
| AR 20b | 1.24 | 0.00 | GS 21a/b | 18.27 | 0.00 |
| AR 21a | 3.75 | 0.00 | GS 22a/b | 32.72 | 0.00 |
| AR 21b | 48.59 | 0.00 |  |  |  |
| AR 22a | 3.61 | 0.00 | NO 159 | 0.00 | 0.00 |
| AR 22b | 0.00 | 0.00 | NO 20a/b | 10.14 | 0.00 |
|  |  |  | NO 21a/b | 12.26 | 0.00 |
| WK 15g | 1.95 | 0.00 | NO 22a/b | 0.80 | 0.00 |
| WK 20a | 0.74 | 0.00 |  |  |  |
| WK 20b | 19.23 | 0.00 | CS 159 | 5.73 | 0.00 |
| WK 21a | 3.99 | 0.00 | CS 20a/b | 3.28 | 0.00 |
| WK 21b | 8.54 | 0.00 | CS 21a | 5.87 | 0.00 |
| WK 22a | 1.88 | 0.00 | CS 21b | 4.31 | 0.00 |
| WK 22b | 1.65 | 0.00 | CS 22a/b | 3.43 | 0.00 |
| PC 15g | 3.56 | 0.00 | AS 15 g | 2.21 | 0.00 |
| PC 20a | 0.40 | 0.00 | AS 20a/b | 1.55 | 0.00 |
| PC 20b | 39.36 | 0.00 | AS 21a/b | 0.06 | 0.00 |
| PC 21a | 4.76 | 0.00 | AS 22a/b | 3.15 | 0.00 |
| PC 21b | 0.85 | 0.55 |  |  |  |
| PC 22a | 0.07 | 0.00 | MC 15g | 36.56 | 0.00 |
| PC 22b | 15.85 | 0.00 | MC 20a/b | 3.16 | 0.00 |
|  |  |  | MC 21a/b | 3.66 | 0.00 |
| MK 15g | 2.49 | 0.00 | MC 22a/b | 2.42 | 0.00 |
| MK 20a | 1.53 | 0.00 |  |  |  |
| MK 20b | 12.72 | 0.00 | EI 159 | 51.55 | 0.00 |
| MK 21a | 2.98 | 0.00 | EI 20a/b | 0.00 | 0.00 |
| MK 21b | 0.00 | 0.00 | EI 21a/b | 13.17 | 0.00 |
| MK 22a | 5.10 | 0.00 | EI 22a/b | 5.79 | 0.00 |
| MK 22b | 2.02 | 0.00 |  |  |  |
| VE 15g | 0.04 | 0.00 |  |  |  |
| VE 20a | 1.70 | 0.00 |  |  |  |
| VE 20b | 4.66 | 0.00 |  |  |  |
| VE 21a | 0.73 | 0.00 |  |  |  |
| VE 21b | 2.62 | 0.00 |  |  |  |
| VE 22a | 1.64 | 0.00 |  |  |  |
| VE 22b | 2.09 | 0.00 |  |  |  |

Table 9
Root Mean Square Difference Between Distributions of Reference Form and Equated New Forms, by Subrest and Form

| AFOT Subtest and Form | Reference vs. polynomial Equated Scores | NON-AFOT Subtest and Form | Reference vs. Polynomial Equated Scores |
| :---: | :---: | :---: | :---: |
| AR 15g | 0.0013 | GS 159 | 0.0017 |
| AR 20a | 0.0010 | GS 20a/b | 0.0014 |
| AR 20b | 0.0014 | GS 21a/b | 0.0017 |
| AR 21 a | 0.0009 | GS 22a/b | 0.0017 |
| AR 21b | 0.0010 |  |  |
| AR 22a | 0.0006 | NO 15g | 0.0019 |
| AR 22b | 0.0012 | NO 20a/b | 0.0014 |
|  |  | NO 21a/b | 0.0020 |
| WK 15g | 0.0007 | NO 22a/b | 0.0015 |
| WK 20a | 0.0009 |  |  |
| WK 20b | 0.0009 | CS 15g | 0.0023 |
| WK 21a | 0.0011 | CS 20a/b | 0.0028 |
| WK 21b | 0.0008 | CS 21a | 0.0020 |
| WK 22a | 0.0008 | CS 21 b | 0.0019 |
| WK 22b | 0.0013 | CS 22a/b | 0.0021 |
| PC 15g | 0.0003 | AS 15 g | 0.0009 |
| PC 20a | 0.0006 | AS $20 \mathrm{a} / \mathrm{b}$ | 0.0010 |
| PC 20b | 0.0003 | AS 21a/b | 0.0009 |
| PC 21a | 0.0007 | AS 22a/b | 0.0009 |
| PC 216 | 0.0007 |  |  |
| PC 22a | 0.0013 | MC 15g | 0.0014 |
| PC 22 b | 0.0002 | MC 20a/b | 0.0009 |
|  |  | MC 21a/b | 0.0009 |
| MK 159 | 0.0010 | MC 22a/b | 0.0012 |
| MK 20a | 0.0008 |  |  |
| MK 20b | 0.0006 | EI 159 | 0.0009 |
| MK 21a | 0.0013 | EI 20a/b | 0.0010 |
| MK 21b | 0.0010 | EI 21a/b | 0.0009 |
| MK 22a | 0.0010 | EI 22a/b | 0.0014 |
| MK 22b | 0.0010 |  |  |
| VE 15g | 0.0014 |  |  |
| VE 20a | 0.0013 |  |  |
| VE 20b | 0.0015 |  |  |
| VE 21a | 0.0013 |  |  |
| VE 21b | 0.0013 |  |  |
| VE 22a | 0.0013 |  |  |
| VE 22b | 0.0020 |  |  |

Table 10
Percentage of Subjects at Scores Where Cumulative Distributions of Reference Form and Equated New Forms
Differ by More than .01 , by Subtest and Form

| AFOT Subtest and Form | Reference vs. <br> Polynomial <br> Equated Scores | NON-AFQT Subtest and Form | Reference vs. Polynomial Equated Scores |
| :---: | :---: | :---: | :---: |
| AR 15g | 0.00 | GS 15 g | 0.00 |
| AR 20a | 0.00 | GS 20a/b | 0.00 |
| AR 20b | 0.00 | GS $21 \mathrm{a} / \mathrm{b}$ | 0.00 |
| AR 21a | 0.00 | GS 22a/b | 0.00 |
| AR 21b | 0.00 |  |  |
| AR 22a | 0.00 | NO 159 | 0.00 |
| AR 22b | 0.00 | NO 20a/b | 0.00 |
|  |  | NO 21a/b | 0.00 |
| WK 15g | 0.00 | NO 22a/b | 0.00 |
| WK 20a | 0.00 |  |  |
| WK 20b | 0.00 | CS 15g | 0.00 |
| WK 21a | 0.00 | CS 20a/b | 0.00 |
| WK 21b | 0.00 | CS 21a | 0.00 |
| WK 22a | 0.00 | CS 21b | 0.00 |
| WK 22b | 0.00 | CS 22a/b | 0.00 |
| PC 15g | 0.00 | AS 15 g | 0.00 |
| PC 20a | 0.00 | AS 20a/b | 0.00 |
| PC 20b | 0.00 | AS 21a/b | 0.00 |
| PC 21a | 0.00 | AS 22a/b | 0.00 |
| PC 21b | 0.00 |  |  |
| PC 22a | 0.00 | MC 159 | 0.00 |
| PC 22b | 0.00 | MC 20a/b | 0.00 |
|  |  | MC 21a/b | 0.00 |
| MK 15g | 0.00 | MC 22a/b | 0.00 |
| MK 20a | 0.00 |  |  |
| MK 20b | 0.00 | EI 15g | 0.00 |
| MK 21a | 0.00 | EI 20a/b | 0.00 |
| MK 21b | 0.00 | EI 21a/b | 0.00 |
| MK 22a | 0.00 | EI 22a/b | 0.00 |
| MK 22b | 0.00 |  |  |
| VE 15g | 0.00 |  |  |
| VE 20a | 0.00 |  |  |
| VE 20b | 0.00 |  |  |
| VE 21a | 0.00 |  |  |
| VE 21b | 0.00 |  |  |
| VE 22a | 0.00 |  |  |
| VE 22b | 0.00 |  |  |

Subtest Means, Standard Deviations, and Correlations of Subtests, after Application of Current Conversion Tables

FORM 15h Standard Score Statistics

| Subtest | SID-GS | SID-AR | SID | SID-PC | 51 | SID-CS | SID-AS | SID | SID | SID-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MITN | 50.81 | 51.34 | 51.73 | 51.80 | 53.12 | 52.58 | 50.91 | 52.33 | 51.89 | 50.46 | 51.80 |
| S.D. | 8.55 | 8.53 | 6.94 | 7.65 | 7.78 | 7.65 | 8.88 | 8.64 | 9.31 | 8.48 | 6.82 |
| N | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 | 12931 |

FORM 15h Standard Score Correlations

| Subtest | SID-GS | STD-AR | SID-WK | STD-PC | STD-NO | STD-CS | STD-AS | SID-MEX | STD-MC | STD-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.60 | 0.72 | 0.56 | 0.23 | 0.22 | 0.58 | 0.53 | 0.65 | 0.69 | 0.72 |
| SID-AR | 0.60 | 1.00 | 0.59 | 0.58 | 0.44 | 0.37 | 0.44 | 0.73 | 0.61 | 0.53 | 0.63 |
| SID-WIK | 0.72 | 0.59 | 1.00 | 0.66 | 0.28 | 0.28 | 0.48 | 0.50 | 0.55 | 0.60 | 0.96 |
| SID-PC | 0.56 | 0.58 | 0.66 | 1.00 | 0.38 | 0.37 | 0.36 | 0.51 | 0.46 | 0.48 | 0.83 |
| SID-NO | 0.23 | 0.44 | 0.28 | 0.38 | 1.00 | 0.63 | 0.09 | 0.47 | 0.20 | 0.16 | 0.34 |
| SID-CS | 0.22 | 0.37 | 0.28 | 0.37 | 0.63 | 1.00 | 0.10 | 0.40 | 0.20 | 0.17 | 0.34 |
| SID-AS | 0.58 | 0.44 | 0.48 | 0.36 | 0.09 | 0.10 | 1.00 | 0.24 | 0.67 | 0.68 | 0.48 |
| STD-MR | 0.53 | 0.73 | 0.50 | 0.51 | 0.47 | 0.40 | 0.24 | 1.00 | 0.48 | 0.40 | 0.54 |
| SID-MC | 0.65 | 0.61 | 0.55 | 0.46 | 0.20 | 0.20 | 0.67 | 0.48 | 1.00 | 0.67 | 0.56 |
| STD-EI | 0.69 | 0.53 | 0.60 | 0.48 | 0.16 | 0.17 | 0.68 | 0.40 | 0.67 | 1.00 | 0.60 |
| STD-VE | 0.72 | 0.63 | 0.96 | 0.83 | 0.34 | 0.34 | 0.48 | 0.54 | 0.56 | 0.60 | 1.00 |

Subtest SID-GS SID-AR SID-WK SID-PC SID-NO SID-CS STD-AS SID-MR SID-MC SID-EI SID-VE

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MEAN | 51.00 | 51.07 | 52.00 | 52.06 | 52.84 | 52.83 | 50.89 | 52.44 | 52.07 | 50.32 |
| S.D. | 8.36 | 8.56 | 6.88 | 7.46 | 7.72 | 7.59 | 8.95 | 8.63 | 9.07 | 8.99 |
| N | 13312 | 13312 | 13312 | 13312 | 13312 | 13312 | 13312 | 13312 | 13312 | 13312 |

FORM 15g (Operational) Standard Score Oorrelations

| Subtes | SID-GS | STD- | STD- | SID-E | SID-NO | SID-CS | STD-AS | STD | SID-MC | STD-EI | SID-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.62 | 0.70 | 0.58 | 0.22 | 0.23 | 0.53 | 0.54 | 0.65 | 0.62 | 0.70 |
| SID-AR | 0.62 | 1.00 | 0.59 | 0.55 | 0.42 | 0.39 | 0.39 | 0.71 | 0.62 | 0.47 | 0.62 |
| SID-WK | 0.70 | 0.59 | 1.00 | 0.72 | 0.29 | 0.33 | 0.40 | 0.50 | 0.51 | 0.47 | 0.97 |
| SID-PC | 0.58 | 0.55 | 0.72 | 1.00 | 0.32 | 0.34 | 0.30 | 0.48 | 0.42 | 0.39 | 0.86 |
| SID-NO | 0.22 | 0.42 | 0.29 | 0.32 | 1.00 | 0.65 | 0.03 | 0.44 | 0.18 | 0.13 | 0.32 |
| SID-CS | 0.23 | 0.39 | 0.33 | 0.34 | 0.65 | 1.00 | 0.05 | 0.40 | 0.19 | 0.15 | 0.35 |
| SID-AS | 0.53 | 0.39 | 0.40 | 0.30 | 0.03 | 0.05 | 1.00 | 0.19 | 0.60 | 0.65 | 0.39 |
| STD-ME | 0.54 | 0.71 | 0.50 | 0.48 | 0.44 | 0.40 | 0.19 | 1.00 | 0.50 | 0.36 | 0.52 |
| SID-MC | 0.65 | 0.62 | 0.51 | 0.42 | 0.18 | 0.19 | 0.60 | 0.50 | 1.00 | 0.60 | 0.52 |
| SID-EI | 0.62 | 0.47 | 0.47 | 0.39 | 0.13 | 0.15 | 0.65 | 0.36 | 0.60 | 1.00 | 0.48 |
| SID-VE | 0.70 | 0.62 | 0.97 | 0.86 | 0.32 | 0.35 | 0.39 | 0.52 | 0.52 | 0.48 | 1.00 |

FOPM 15 g Standard Score Statistic Differences from the Reference FORM (15H)
$\begin{array}{lrrrrrrrrrrr}\text { Subtest } & \text { SID-GS } & \text { SID-AR SID-WK } & \text { SID-PC } & \text { SID-NO } & \text { SID-CS } & \text { SID-AS } & \text { SID-MR SID-MC } & \text { SID-EI } & \text { SID-VE } \\ \text { MESAN } & 0.19 & -0.27 & 0.28 & 0.27 & -0.27 & 0.24 & -0.02 & 0.11 & 0.18 & -0.13 & 0.23 \\ \text { S.D } & -0.19 & 0.02 & -0.06 & -0.19 & -0.06 & -0.06 & 0.07 & -0.01 & -0.24 & 0.51 & 0.05 \\ \mathrm{~N} & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00 & 381.00\end{array}$
FORM $15 g$ Standard Score Correlation Differences from the Reference FORM ( 15 h )

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | SID-GS SID-AR | SID-WR | STD-FC | SID-NO | SID-CS | SID-AS | SID-MR SID-MC | SID-EI SID-VE |  |  |  |
| SID-GS | 0.00 | 0.02 | -0.02 | 0.02 | -0.02 | 0.00 | -0.05 | 0.02 | -0.00 | -0.07 | -0.02 |
| SID-AR | 0.02 | 0.00 | 0.01 | -0.03 | -0.03 | 0.02 | -0.05 | -0.02 | 0.01 | -0.06 | -0.01 |
| SID-WK | -0.02 | 0.01 | 0.00 | 0.07 | 0.01 | 0.04 | -0.09 | -0.00 | -0.04 | -0.13 | 0.01 |
| SID-PC | 0.02 | -0.03 | 0.07 | 0.00 | -0.06 | -0.03 | -0.06 | -0.04 | -0.03 | -0.08 | 0.03 |
| SID-NO | -0.02 | -0.03 | 0.01 | -0.06 | 0.00 | 0.02 | -0.06 | -0.03 | -0.01 | -0.03 | -0.02 |
| SID-CS | 0.00 | 0.02 | 0.04 | -0.03 | 0.02 | 0.00 | -0.05 | 0.00 | -0.01 | -0.02 | 0.01 |
| SID-AS | -0.05 | -0.05 | -0.09 | -0.06 | -0.06 | -0.05 | 0.00 | -0.06 | -0.07 | -0.03 | -0.09 |
| SID-MK | 0.02 | -0.02 | -0.00 | -0.04 | -0.03 | 0.00 | -0.06 | 0.00 | 0.02 | -0.04 | -0.02 |
| SID-MC | -0.00 | 0.01 | -0.04 | -0.03 | -0.01 | -0.01 | -0.07 | 0.02 | 0.00 | -0.07 | -0.04 |
| SID-EI | -0.07 | -0.06 | -0.13 | -0.08 | -0.03 | -0.02 | -0.03 | -0.04 | -0.07 | 0.00 | -0.13 |
| STD-VE | -0.02 | -0.01 | 0.01 | 0.03 | -0.02 | 0.01 | -0.09 | -0.02 | -0.04 | -0.13 | 0.00 |

continued

Table 11 (continued)

Subtest Means, Standard Deviations, and Correlations of Subtests, after Application of Current Conversion Tables

FOPM 20a Standard Scoce Statistics

| Subtest | SID-GS SID-AR | SID-NK | SID-PC | SID-NO | SID-CS | SID-AS | SID-NR | SID-MC | SID-EI | SID-VE |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| NRAN | 51.07 | 51.37 | 51.77 | 51.70 | 53.16 | 52.49 | 51.08 | 52.27 | 51.97 | 50.51 | 51.82 |
| S.D. | 8.54 | 8.48 | 6.96 | 7.53 | 7.78 | 7.62 | 8.88 | 8.62 | 9.29 | 8.40 | 6.90 |
| $N$ | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 | 13097 |

FOPM 20a Standard Score Correlations

| Subtest | SID-GS SID-AR SID-WK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MA | SID-MC | SID-EI | SID-VE |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.62 | 0.73 | 0.63 | 0.27 | 0.26 | 0.48 | 0.60 | 0.62 | 0.64 | 0.74 |
| SID-AR | 0.62 | 1.00 | 0.58 | 0.59 | 0.43 | 0.38 | 0.39 | 0.74 | 0.64 | 0.52 | 0.63 |
| SID-WK | 0.73 | 0.58 | 1.00 | 0.72 | 0.29 | 0.32 | 0.43 | 0.51 | 0.55 | 0.56 | 0.97 |
| SID-FC | 0.63 | 0.59 | 0.72 | 1.00 | 0.37 | 0.40 | 0.39 | 0.52 | 0.53 | 0.51 | 0.86 |
| SID-NO | 0.27 | 0.43 | 0.29 | 0.37 | 1.00 | 0.62 | 0.07 | 0.44 | 0.24 | 0.19 | 0.33 |
| SID-CS | 0.26 | 0.38 | 0.32 | 0.40 | 0.62 | 1.00 | 0.10 | 0.38 | 0.25 | 0.19 | 0.37 |
| SID-AS | 0.48 | 0.39 | 0.43 | 0.39 | 0.07 | 0.10 | 1.00 | 0.22 | 0.60 | 0.59 | 0.45 |
| SID-MK | 0.60 | 0.74 | 0.51 | 0.52 | 0.44 | 0.38 | 0.22 | 1.00 | 0.52 | 0.46 | 0.55 |
| SID-MC | 0.62 | 0.64 | 0.55 | 0.53 | 0.24 | 0.25 | 0.60 | 0.52 | 1.00 | 0.64 | 0.58 |
| SID-EI | 0.64 | 0.52 | 0.56 | 0.51 | 0.19 | 0.19 | 0.59 | 0.46 | 0.64 | 1.00 | 0.58 |
| SID-VE | 0.74 | 0.63 | 0.97 | 0.86 | 0.33 | 0.37 | 0.45 | 0.55 | 0.58 | 0.58 | 1.00 |

FORM 20a Standard Score Statistic Differences from the Reference FOPM (15h)

| Subtest | SID-GS SID-AR SID-NK | SID-PC | SID-NO SID-CS | SID-AS | SID-MR SID-MC | SID-EI SID-VE |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| NIEAN | 0.26 | 0.03 | 0.05 | -0.10 | 0.05 | -0.10 | 0.17 | -0.06 | 0.08 | 0.06 | 0.02 |
| S.D. | -0.01 | -0.05 | 0.02 | -0.12 | 0.00 | -0.03 | -0.00 | -0.02 | -0.02 | -0.08 | 0.08 |
| N | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 | 166.00 |

FORM 20a Standard Score Correlation Differences from the Reference FOPM (15h)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | SID-GS SID-AR | SID-WIK SID-PC | SID-NO | SID-CS | SID-AS | SID-MR | SID-MC SID-EI | SID-VE |  |  |  |
| SID-GS | 0.00 | 0.02 | 0.01 | 0.07 | 0.04 | 0.04 | -0.10 | 0.07 | -0.03 | -0.05 | 0.02 |
| SID-AR | 0.02 | 0.00 | -0.00 | 0.01 | -0.01 | 0.01 | -0.05 | 0.01 | 0.03 | -0.01 | -0.00 |
| SID-WK | 0.01 | -0.00 | 0.00 | 0.06 | 0.00 | 0.03 | -0.06 | 0.01 | 0.00 | -0.04 | 0.01 |
| SID-PC | 0.07 | 0.01 | 0.06 | 0.00 | -0.01 | 0.02 | 0.03 | 0.01 | 0.07 | 0.03 | 0.03 |
| SID-NO | 0.04 | -0.01 | 0.00 | -0.01 | 0.00 | -0.01 | -0.02 | -0.03 | 0.05 | 0.03 | -0.01 |
| SID-CS | 0.04 | 0.01 | 0.03 | 0.02 | -0.01 | 0.00 | 0.00 | -0.02 | 0.04 | 0.02 | 0.03 |
| SID-AS | -0.10 | -0.05 | -0.06 | 0.03 | -0.02 | 0.00 | 0.00 | -0.03 | -0.06 | -0.08 | -0.04 |
| SID-MR | 0.07 | 0.01 | 0.01 | 0.01 | -0.03 | -0.02 | -0.03 | 0.00 | 0.04 | 0.06 | 0.01 |
| SID-MC | -0.03 | 0.03 | 0.00 | 0.07 | 0.05 | 0.04 | -0.06 | 0.04 | 0.00 | -0.03 | 0.02 |
| SID-EI | -0.05 | -0.01 | -0.04 | 0.03 | 0.03 | 0.02 | -0.08 | 0.06 | -0.03 | 0.00 | -0.02 |
| SID-VE | 0.02 | -0.00 | 0.01 | 0.03 | -0.01 | 0.03 | -0.04 | 0.01 | 0.02 | -0.02 | 0.00 |

FORM 20a Standard Score Statistic Differences from the Operational FCRM (15g)

| Subt | STD-GS |  |  |  |  |  |  |  | SID-MC | SID-EI | SID-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MEPN | 0.07 | 0.30 | -0.23 | -0.36 | 0.32 | -0.34 | 0.19 | -0.17 | -0.10 | 0.19 | 0.21 |
| S.D. | 0.18 | -0.08 | 0.08 | 0.07 | 0.07 | 0.03 | -0.07 | -0.01 | 0.22 | -0.59 | 0.03 |
| N | -215.0 | -215.0 | -215.0 | -215.0 | -215.0 | -215.0 | 215.0 | -215.0 | -215.0 | -215.0 | 15.0 |

FORM 20a Standard Score Correlation Differences from the operational FOPM (15g)

| SUbtest | SID-GS SID-AR | STD-WK | STD-PC | SID-NO | SID-CS | SID-AS | SID-NK | SID-MC | SID-EI | SID-VE |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SID-GS | 0.00 | -0.00 | 0.03 | 0.05 | 0.05 | 0.04 | -0.05 | 0.05 | -0.03 | 0.02 | 0.04 |
| SID-AR | -0.00 | 0.00 | -0.01 | 0.04 | 0.01 | -0.01 | -0.01 | 0.03 | 0.01 | 0.05 | 0.01 |
| SID-WK | 0.03 | -0.01 | 0.00 | -0.01 | -0.01 | -0.01 | 0.03 | 0.01 | 0.04 | 0.09 | -0.00 |
| SID-PC | 0.05 | 0.04 | -0.01 | 0.00 | 0.05 | 0.05 | 0.09 | 0.04 | 0.11 | 0.12 | 0.00 |
| SID-NO | 0.05 | 0.01 | -0.01 | 0.05 | 0.00 | -0.03 | 0.04 | 0.00 | 0.06 | 0.06 | 0.01 |
| SID-CS | 0.04 | -0.01 | -0.01 | 0.05 | -0.03 | 0.00 | 0.05 | -0.02 | 0.06 | 0.04 | 0.01 |
| SID-AS | -0.05 | -0.01 | 0.03 | 0.09 | 0.04 | 0.05 | 0.00 | 0.03 | 0.01 | -0.06 | 0.05 |
| SID-MK | 0.05 | 0.03 | 0.01 | 0.04 | 0.00 | -0.02 | 0.03 | 0.00 | 0.02 | 0.10 | 0.03 |
| SID-MC | -0.03 | 0.01 | 0.04 | 0.11 | 0.06 | 0.06 | 0.01 | 0.02 | 0.00 | 0.04 | 0.07 |
| SID-EI | 0.02 | 0.05 | 0.09 | 0.12 | 0.06 | 0.04 | -0.06 | 0.10 | 0.04 | 0.00 | 0.10 |
| SID-VE | 0.04 | 0.01 | -0.00 | 0.00 | 0.01 | 0.01 | 0.05 | 0.03 | 0.07 | 0.10 | 0.00 |

continued

Table 11
(continued)

# Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables 

FORM 20b Standard Score Statistics

| Subtes | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO | STD-CS | STD-AS | STD-M1 | STD-MC | STD-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MEAN | 51.04 | 51.36 | 51.72 | 51.57 | 53.18 | 52.65 | 50.76 | 52.37 | 51.90 | 50.43 | 51.88 |
| S.D | 8.46 | 8.53 | 7.03 | 7.51 | 7.83 | 7.68 | 8.91 | 8.67 | 9.27 | 8.57 | 6.95 |
| N | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 | 12778 |
|  | Form 20b Standard Score Correlations |  |  |  |  |  |  |  |  |  |  |
| Subtest | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO | STD-CS | STD-AS | STD-MK | STD-MC | STD-EI | STD-VE |
| STD-GS | 1.00 | 0.61 | 0.73 | 0.57 | 0.26 | 0.25 | 0.49 | 0.60 | 0.62 | 0.65 | 0.74 |
| STD-AR | 0.61 | 1.00 | 0.58 | 0.54 | 0.43 | 0.39 | 0.39 | 0.74 | 0.62 | 0.51 | 0.61 |
| STD-WR | 0.73 | 0.58 | 1.00 | 0.67 | 0.27 | 0.31 | 0.47 | 0.51 | 0.57 | 0.58 | 0.97 |
| STD-PC | 0.57 | 0.54 | 0.67 | 1.00 | 0.35 | 0.38 | 0.31 | 0.50 | 0.47 | 0.46 | 0.82 |
| STD-NO | 0.26 | 0.43 | 0.27 | 0.35 | 1.00 | 0.61 | 0.07 | 0.44 | 0.23 | 0.19 | 0.32 |
| STD-CS | 0.25 | 0.39 | 0.31 | 0.38 | 0.61 | 1.00 | 0.10 | 0.38 | 0.24 | 0.20 | 0.36 |
| STD-AS | 0.49 | 0.39 | 0.47 | 0.31 | 0.07 | 0.10 | 1.00 | 0.24 | 0.61 | 0.61 | 0.45 |
| STD-MK | 0.60 | 0.74 | 0.51 | 0.50 | 0.44 | 0.38 | 0.24 | 1.00 | 0.53 | 0.47 | 0.55 |
| STD-MC | 0.62 | 0.62 | 0.57 | 0.47 | 0.23 | 0.24 | 0.61 | 0.53 | 1.00 | 0.65 | 0.58 |
| STD-EI | 0.65 | 0.51 | 0.58 | 0.46 | 0.19 | 0.20 | 0.61 | 0.47 | 0.65 | 1.00 | 0.58 |
| STD-VE | 0.74 | 0.61 | 0.97 | 0.82 | 0.32 | 0.36 | 0.45 | 0.55 | 0.58 | 0.58 | 1.00 |

FORM 20b Standard Score Statistic Differences from the Reference FORM (15h)
Subtest STD-GS STD-AR STD-WK STD-PC STD-NO STD-CS STD-AS STD-MK STD-MC STD-EI STD-VE

| Subtest | STD-GS | STD-AR | STD-WK | STO-PC | STD-NO | STO-CS | STD-AS | STD-MK STD-MC | STD-EI STD-VE |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MEAN | 0.23 | 0.03 | -0.00 | -0.23 | 0.06 | 0.06 | -0.15 | 0.05 | 0.01 | -0.03 |
| S.D. | -0.09 | -0.01 | 0.09 | -0.13 | 0.05 | 0.03 | 0.03 | 0.03 | -0.04 | 0.08 |
| N | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 | -153.0 |
|  |  |  |  |  | -153.0 |  |  |  |  |  |

FORM 20b Standard Score Correlation Differences from the Reference FORM (15h)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO | STD-CS | STD-AS | STD-MK | STD-MC | STD-EI | STD-VE |
| STD-GS | 0.00 | 0.01 | 0.02 | 0.02 | 0.02 | 0.03 | -0.09 | 0.07 | -0.03 | -0.04 | 0.02 |
| STD-AR | 0.01 | 0.00 | -0.00 | -0.04 | -0.01 | 0.02 | -0.05 | 0.01 | 0.01 | -0.02 | -0.02 |
| STD-WK | 0.02 | -0.00 | 0.00 | 0.01 | -0.01 | 0.02 | -0.02 | 0.02 | 0.02 | -0.02 | 0.01 |
| STD-PC | 0.02 | -0.04 | 0.01 | 0.00 | -0.03 | 0.01 | -0.06 | -0.01 | 0.01 | -0.02 | -0.01 |
| STD-NO | 0.02 | -0.01 | -0.01 | -0.03 | 0.00 | -0.02 | -0.02 | -0.03 | 0.03 | 0.03 | -0.02 |
| STD-CS | 0.03 | 0.02 | 0.02 | 0.01 | -0.02 | 0.00 | -0.00 | -0.02 | 0.04 | 0.03 | 0.01 |
| STD-AS | -0.09 | -0.05 | -0.02 | -0.06 | -0.02 | -0.00 | 0.00 | -0.00 | -0.06 | -0.06 | -0.03 |
| STD-MK | 0.07 | 0.01 | 0.02 | -0.01 | -0.03 | -0.02 | -0.00 | 0.00 | 0.04 | 0.07 | 0.00 |
| STD-MC | -0.03 | 0.01 | 0.02 | 0.01 | 0.03 | 0.04 | -0.06 | 0.04 | 0.00 | -0.02 | 0.02 |
| STD-EI | -0.04 | -0.02 | -0.02 | -0.02 | 0.03 | 0.03 | -0.06 | 0.07 | -0.02 | 0.00 | -0.02 |
| STD-VE | 0.02 | -0.02 | 0.01 | -0.01 | -0.02 | 0.01 | -0.03 | 0.00 | 0.02 | -0.02 | 0.00 |

FORM 20b Standard Score Statistic Differences from the Operational FORM (15g)

| Subtest | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO STD-CS | STD-AS | STD-MK STD-MC | STD-EI | STD-VE |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MEAN | 0.04 | 0.29 | -0.28 | -0.49 | 0.34 | -0.18 | -0.13 | -0.06 | -0.17 | 0.11 | -0.15 |
| S.D. | 0.09 | -0.03 | 0.15 | 0.06 | 0.11 | 0.09 | -0.04 | 0.04 | 0.20 | -0.42 | 0.08 |
| N | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 | -534.0 |

FORM 20b Standard Score Correlation Differences from the Operational FORM (15g)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO | STD-CS | STD-AS | STD-MK | STD-MC | STD-EI STD-VE |  |
| STD-GS | 0.00 | -0.00 | 0.04 | -0.01 | 0.04 | 0.02 | -0.04 | 0.05 | -0.03 | 0.03 | 0.04 |
| STD-AR | -0.00 | 0.00 | -0.01 | -0.01 | 0.02 | 0.00 | -0.00 | 0.03 | -0.00 | 0.04 | -0.00 |
| STD-WK | 0.04 | -0.01 | 0.00 | -0.06 | -0.02 | -0.02 | 0.07 | 0.02 | 0.06 | 0.11 | -0.00 |
| STD-PC | -0.01 | -0.01 | -0.06 | 0.00 | 0.03 | 0.04 | 0.00 | 0.02 | 0.04 | 0.06 | -0.04 |
| STD-NO | 0.04 | 0.02 | -0.02 | 0.03 | 0.00 | -0.04 | 0.04 | -0.00 | 0.04 | 0.06 | -0.00 |
| STD-CS | 0.02 | 0.00 | -0.02 | 0.04 | -0.04 | 0.00 | 0.04 | -0.03 | 0.05 | 0.05 | 0.00 |
| STD-AS | -0.04 | -0.00 | 0.07 | 0.00 | 0.04 | 0.04 | 0.00 | 0.05 | 0.01 | -0.04 | 0.06 |
| STD-MK | 0.05 | 0.03 | 0.02 | 0.02 | -0.00 | -0.03 | 0.05 | 0.00 | 0.03 | 0.10 | 0.03 |
| STD-MC | -0.03 | -0.00 | 0.06 | 0.04 | 0.04 | 0.05 | 0.01 | 0.03 | 0.00 | 0.05 | 0.06 |
| STD-EI | 0.03 | 0.04 | 0.11 | 0.06 | 0.06 | 0.05 | -0.04 | 0.10 | 0.05 | 0.00 | 0.11 |
| STD-VE | 0.04 | -0.00 | -0.00 | -0.04 | -0.00 | 0.00 | 0.06 | 0.03 | 0.06 | 0.11 | 0.00 |

Table 11
(continued)

## Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FOPM 2la Standard Score Statigtics

| Suce | STD-GS |  |  |  | sib-10 | SID-Cs | SID-AS | S1D-1/ | SID-MC | STD-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MEA | 50.85 | 51.33 | 51.74 | 51.71 | 53.09 | 52.58 | 50.88 | 52.35 | 52.00 | 50.32 | 51.81 |
| S.D | 8.60 | 8.49 | 6.93 | 7.43 | 7.78 | 7.62 | 8.99 | 8.66 | 9.25 | 8.51 | 92 |
| N | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 | 12532 |

FORM 21a Standard Score Correlations

| Subtest | STD-GS |  |  | ID | STD-NO | SID | ID | STD-MK | D | STD-EI | ID-ve |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.60 | 0.72 | 0.61 | 0.29 | 0.28 | 0.36 | 0.61 | 0.58 | 0.54 | 0.74 |
| SID-AR | 0.60 | 1.00 | 0.58 | 0.56 | 0.44 | 0.40 | 0.37 | 0.72 | 0.62 | 0.49 | 0.61 |
| STD-WK | 0.72 | 0.58 | 1.00 | 0.70 | 0.29 | 0.31 | 0.37 | 0.49 | 0.54 | 0.54 | 0.97 |
| STD-PC | 0.61 | 0.56 | 0.70 | 1.00 | 0.33 | 0.34 | 0.36 | 0.45 | 0.50 | 0.48 | 0.84 |
| STD-NO | 0.29 | 0.44 | 0.29 | 0.33 | 1.00 | 0.63 | 0.03 | 0.43 | 0.19 | 0.10 | 0.32 |
| STD-CS | 0.28 | 0.40 | 0.31 | 0.34 | 0.63 | 1.00 | 0.06 | 0.36 | 0.23 | 0.14 | 0.34 |
| STD-AS | 0.36 | 0.37 | 0.37 | 0.36 | 0.03 | 0.06 | 1.00 | 0.17 | 0.60 | 0.67 | 0.39 |
| STD-ME | 0.61 | 0.72 | 0.49 | 0.45 | 0.43 | 0.36 | 0.17 | 1.00 | 0.50 | 0.34 | 0.51 |
| STD-MC | 0.58 | 0.62 | 0.54 | 0.50 | 0.19 | 0.23 | 0.60 | 0.50 | 1.00 | 0.68 | 0.57 |
| STD-EI | 0.54 | 0.49 | 0.54 | 0.48 | 0.10 | 0.14 | 0.67 | 0.34 | 0.68 | 1.00 | 0.56 |
| STD-VE | 0.74 | 0.61 | 0.97 | 0.84 | 0.32 | 0.34 | 0.39 | 0.51 | 0.57 | 0.56 | 1.00 |

FORM 21a Standard Score Statistic Differences from the Reference FORM (15h)

| Subtest | SID-GS | SID-AR | SID-NK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MK | SID-NC | SID-EI SID-VE |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MEAN | 0.04 | -0.01 | 0.01 | -0.09 | -0.02 | -0.01 | -0.03 | 0.02 | 0.12 | -0.14 |
| S.D. | 0.05 | -0.04 | -0.01 | -0.22 | 0.00 | -0.04 | 0.10 | 0.02 | -0.07 | 0.01 |
| N | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 | -399.0 |

FOPM 2la Standard Score Correlation Differences from the Reference FOPM (15h)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | SID-GS SID-AR | SID-WRK SID-PC | SID-NO | SID-CS | SID-AS | SID-MK | SID-MC | SID-EI | SID-VE |  |  |
| SID-GS | 0.00 | 0.00 | 0.00 | 0.05 | 0.06 | 0.05 | -0.23 | 0.08 | -0.08 | -0.15 | 0.02 |
| SID-AR | 0.00 | 0.00 | -0.01 | -0.02 | -0.00 | 0.03 | -0.07 | -0.01 | 0.01 | -0.04 | -0.02 |
| SID-WR | 0.00 | -0.01 | 0.00 | 0.04 | 0.01 | 0.02 | -0.11 | -0.01 | -0.00 | -0.06 | 0.01 |
| SID-PC | 0.05 | -0.02 | 0.04 | 0.00 | -0.05 | -0.03 | -0.00 | -0.06 | 0.05 | 0.01 | 0.00 |
| SID-NO | 0.06 | -0.00 | 0.01 | -0.05 | 0.00 | -0.00 | -0.07 | -0.04 | -0.00 | -0.06 | -0.02 |
| SID-CS | 0.05 | 0.03 | 0.02 | -0.03 | -0.00 | 0.00 | -0.04 | -0.04 | 0.02 | -0.04 | -0.00 |
| SID-AS | -0.23 | -0.07 | -0.11 | -0.00 | -0.07 | -0.04 | 0.00 | -0.08 | -0.07 | -0.01 | -0.09 |
| SID-MK | 0.08 | -0.01 | -0.01 | -0.06 | -0.04 | -0.04 | -0.08 | 0.00 | 0.02 | -0.06 | -0.03 |
| SID-MC | -0.08 | 0.01 | -0.00 | 0.05 | -0.00 | 0.02 | -0.07 | 0.02 | 0.00 | 0.01 | 0.01 |
| SID-EI | -0.15 | -0.04 | -0.06 | 0.01 | -0.06 | -0.04 | -0.01 | -0.06 | 0.01 | 0.00 | -0.05 |
| SID-VE | 0.02 | -0.02 | 0.01 | 0.00 | -0.02 | -0.00 | -0.09 | -0.03 | 0.01 | -0.05 | 0.00 |

FOPM 2la Standard Score Statistic Differences from the Operational FORM (15g)

| Subtest | SID-GS SID-AR SID-WK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MR SID-MC SID-EI | SID-VE |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MERN | -0.15 | 0.26 | -0.26 | -0.35 | 0.25 | -0.25 | -0.01 | -0.09 | -0.07 | -0.00 | -0.22 |
| S.D. | 0.24 | -0.07 | 0.05 | -0.03 | 0.06 | 0.03 | 0.03 | 0.03 | 0.18 | -0.48 | 0.05 |
| N | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 | -780.0 |

FORM 2la Standard Score Correlation Differences from the operational FCRM (15g)
Subtest STD-GS STD-AR STD-WR STD-PC STD-NO STD-CS STD-AS STD-MR STD-MC STD-ET STD-VE SID-GS SID-AR STD-WK STD-NO SID-CS
STD-AS $\begin{array}{lrr}\text { SID-AS } & -0.18 & -0.02 \\ \text { SID-MK } & 0.06 & 0.01\end{array}$ $\begin{array}{lrr}\text { SID-MC } & 0.06 & 0.01 \\ \text { SID-MC } & -0.08 & -0.00\end{array}$ SID-EI
SID-VE

| $51 D-0 S$ |  |
| ---: | ---: |
| 0.00 | -0.01 |
| -0.01 | 0.00 |
| 0.02 | -0.01 |
| 0.02 | 0.01 |
| 0.07 | 0.02 |
| 0.05 | 0.01 |
| -0.18 | -0.02 |
| 0.06 | 0.01 |
| -0.08 | -0.00 |
| -0.08 | 0.01 |
| 0.03 | -0.00 |

0.02
-0.01
0.00
-0.03
0.00
-0.02
-0.03
-0.01
0.03
0.07
0.00
0.02
0.01
-0.03
0.00
0.01
-0.00
0.06
-0.02
0.08
0.09
-0.02
0.07
0.02
0.00
0.01
0.00
-0.02
-0.00
-0.0
0.0
-0.03
0.00

| 0.07 | 0 |
| :---: | :---: |
| 0.00 | 0 |
| 0.0 |  |
| 0.00 | -0.0 |
| 02 | 0.0 |
| 00 | 0 |
| 01 | -0. |
| 01 | 0.0 |
| 0.03 | -0 |
| 0.00 | -0. | 0.05

0.01
0.02
-0.00
-0.02
0.00
0.00
-0.04
0.04
-0.02
-0.02

| - 05 | -0 |
| :---: | :---: |
| . 01 | -0 |
| . 02 | -0 |
| . 00 | 0 |
| . 02 | -0 |
| . 00 | 0 |
| . 00 | 0 |
| . 04 | -0 |
| . 04 | -0 |
| . 02 | 0 |
| . 02 | -0 |


| -0.18 | 0.06 | -0.08 | -0.08 | 0.03 |
| ---: | ---: | ---: | ---: | ---: |
| -0.02 | 0.01 | -0.00 | 0.01 | -0.0 |
| -0.03 | -0.01 | 0.03 | 0.07 | 0. |
| 0.06 | -0.02 | 0.08 | 0.09 | -0. |
| -0.00 | -0.01 | 0.01 | -0.03 | 0.00 |
| 0.00 | -0.04 | 0.04 | -0.02 | -0.02 |
| 0.00 | -0.02 | -0.00 | 0.02 | -0. |
| -0.02 | 0.00 | 0.00 | -0.02 | -0. |
| -0.00 | 0.00 | 0.00 | 0.08 | 0. |
| 0.02 | -0.02 | 0.08 | 0.00 | 0. |
| -0.00 | -0.01 | 0.05 | 0.08 | 0. |

continued

# Table 11 

 (continued)
## Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FCRM 21b Standard Score Statistics

| Subtest | SID-GS | SID-AR | SID-WK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MK | SID-MC | SID-EI SID-VE |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| MEAN | 50.92 | 51.46 | 51.68 | 51.68 | 53.02 | 52.58 | 50.96 | 52.36 | 52.16 | 50.60 | 51.82 |
| S.D. | 8.44 | 8.53 | 6.87 | 7.62 | 7.76 | 7.62 | 8.84 | 8.62 | 9.19 | 8.39 | 6.85 |
| N | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 | 12060 |

FORM 21b Standard Score Correlations

| Subtest | STD-GS | STD-AR | STD-WK | STD-PC | STD-NO | STD-CS | STD-AS | STD-NK | STD-MC | STD-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.58 | 0.72 | 0.62 | 0.30 | 0.30 | 0.35 | 0.59 | 0.57 | 0.55 | 0.74 |
| SID-AR | 0.58 | 1.00 | 0.55 | 0.55 | 0.43 | 0.39 | 0.31 | 0.69 | 0.58 | 0.44 | 0.59 |
| SID-WK | 0.72 | 0.55 | 1.00 | 0.70 | 0.28 | 0.32 | 0.40 | 0.46 | 0.56 | 0.56 | 0.97 |
| SID-PC | 0.62 | 0.55 | 0.70 | 1.00 | 0.34 | 0.36 | 0.29 | 0.46 | 0.49 | 0.45 | 0.86 |
| SID-NO | 0.30 | 0.43 | 0.28 | 0.34 | 1.00 | 0.63 | 0.02 | 0.42 | 0.19 | 0.11 | 0.32 |
| SID-CS | 0.30 | 0.39 | 0.32 | 0.36 | 0.63 | 1.00 | 0.06 | 0.38 | 0.23 | 0.15 | 0.36 |
| SID-AS | 0.35 | 0.31 | 0.40 | 0.29 | 0.02 | 0.06 | 1.00 | 0.15 | 0.59 | 0.67 | 0.39 |
| STD-MK | 0.59 | 0.69 | 0.46 | 0.46 | 0.42 | 0.38 | 0.15 | 1.00 | 0.49 | 0.34 | 0.50 |
| SID-MC | 0.57 | 0.58 | 0.56 | 0.49 | 0.19 | 0.23 | 0.59 | 0.49 | 1.00 | 0.68 | 0.58 |
| SID-EI | 0.55 | 0.44 | 0.56 | 0.45 | 0.11 | 0.15 | 0.67 | 0.34 | 0.68 | 1.00 | 0.56 |
| STD-VE | 0.74 | 0.59 | 0.97 | 0.86 | 0.32 | 0.36 | 0.39 | 0.50 | 0.58 | 0.56 | 1.00 |

FORM 21b Standard Score Statistic Differences from the Reference FOPM (15h)

| Subtest | STD-GS | D | SID-WK | STD-PC | SID-NO | SID-CS | ST | SID-MK | SI | I | VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| METAN | 0.11 | 0.13 | -0.05 | -0.12 | -0.10 | -0.01 | 0.05 | 0.04 | 0.28 | 0.14 | 0.02 |
| S.D. | -0.12 | -0.00 | -0.07 | -0.03 | -0.02 | -0.03 | -0.04 | -0.02 | -0.12 | -0.09 |  |



FORM 21b Standard Score Correlation Differences from the Reference FORM (15h)

| Subtest | SID-GS SID-AR | SID-FKK SID-PC | SID-NO | SID-CS | SID-AS | SID-MR | SID-MC | SID-EI | SID-VE |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SID-GS | 0.00 | -0.02 | 0.00 | 0.07 | 0.07 | 0.08 | -0.23 | 0.06 | -0.08 | -0.14 | 0.02 |
| SID-AR | -0.02 | 0.00 | -0.04 | -0.03 | -0.02 | 0.02 | -0.13 | -0.04 | -0.03 | -0.09 | -0.04 |
| SID-WK | 0.00 | -0.04 | 0.00 | 0.05 | -0.01 | 0.03 | -0.08 | -0.04 | 0.01 | -0.04 | 0.00 |
| SID-PC | 0.07 | -0.03 | 0.05 | 0.00 | -0.04 | -0.02 | -0.07 | -0.05 | 0.03 | -0.03 | 0.02 |
| SID-NO | 0.07 | -0.02 | -0.01 | -0.04 | 0.00 | -0.01 | -0.07 | -0.05 | -0.01 | -0.05 | -0.02 |
| SID-CS | 0.08 | 0.02 | 0.03 | -0.02 | -0.01 | 0.00 | -0.05 | -0.02 | 0.03 | -0.02 | 0.02 |
| SID-AS | -0.23 | -0.13 | -0.08 | -0.07 | -0.07 | -0.05 | 0.00 | -0.09 | -0.07 | -0.01 | -0.09 |
| SID-MK | 0.06 | -0.04 | -0.04 | -0.05 | -0.05 | -0.02 | -0.09 | 0.00 | 0.01 | -0.06 | -0.05 |
| SID-MC | -0.08 | -0.03 | 0.01 | 0.03 | -0.01 | 0.03 | -0.07 | 0.01 | 0.00 | 0.01 | 0.02 |
| SID-EI | -0.14 | -0.09 | -0.04 | -0.03 | -0.05 | -0.02 | -0.01 | -0.06 | 0.01 | 0.00 | -0.04 |
| SID-VE | 0.02 | -0.04 | 0.00 | 0.02 | -0.02 | 0.02 | -0.09 | -0.05 | 0.02 | -0.04 | 0.00 |

FOPM 21b Standard Score Statistic Differences from the Operational FOPM (15g)

| Subtest | SID-GS | SID-AR | SID-KIK SID-PC SID-NO SID-CS | SID-AS | SID-MK SID-MC | SID-EI SID-VE |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MIFAN | -0.08 | 0.39 | -0.32 | -0.39 | 0.18 | -0.25 | 0.07 | -0.07 | 0.09 | 0.27 | -0.21 |
| S.D. | 0.07 | -0.03 | -0.01 | 0.17 | 0.04 | 0.04 | -0.11 | -0.01 | 0.12 | -0.60 | -0.02 |
| N | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 | -1252 |

FORM 21b Standard Score Correlation Differences from the Operational FORM (15g)

| SUbtegt SID-GS SID-AR | SID-WK SID-PC | SID-NO | SID-CS | SID-AS | SID-MK SID-MC SID-EI SID-VE |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SID-GS | 0.00 | -0.04 | 0.02 | 0.04 | 0.08 | 0.07 | -0.18 | 0.05 | -0.08 | -0.07 | 0.03 |
| SID-AR | -0.04 | 0.00 | -0.04 | -0.00 | 0.01 | 0.01 | -0.08 | -0.02 | -0.04 | -0.03 | -0.03 |
| SID-WK | 0.02 | -0.04 | 0.00 | -0.02 | -0.02 | -0.01 | 0.00 | -0.03 | 0.05 | 0.09 | -0.01 |
| SID-FC | 0.04 | -0.00 | -0.02 | 0.00 | 0.01 | 0.02 | -0.01 | -0.01 | 0.07 | 0.06 | -0.00 |
| SID-NO | 0.08 | 0.01 | -0.02 | 0.01 | 0.00 | -0.03 | -0.01 | -0.02 | 0.01 | -0.02 | -0.00 |
| SID-CS | 0.07 | 0.01 | -0.01 | 0.02 | -0.03 | 0.00 | 0.00 | -0.02 | 0.04 | -0.00 | 0.00 |
| SID-AS | -0.18 | -0.08 | 0.00 | -0.01 | -0.01 | 0.00 | 0.00 | -0.04 | -0.01 | 0.02 | 0.00 |
| SID-MK | 0.05 | -0.02 | -0.03 | -0.01 | -0.02 | -0.02 | -0.04 | 0.00 | -0.01 | -0.02 | -0.03 |
| SID-MC | -0.08 | -0.04 | 0.05 | 0.07 | 0.01 | 0.0 | -0.01 | -0.01 | 0.00 | 0.08 | 0.06 |
| SID-EI | -0.07 | -0.03 | 0.09 | 0.06 | -0.02 | -0. | 0.02 | -0.02 | 0.08 | 0.00 | 0.09 |
| SID-VE | 0.03 | -0.03 | -0.01 | -0.00 | -0.00 | 0.0 | 0.00 | -0.03 | 0.06 | 0.09 | 0.00 |

## Table 11

 (continued)Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FOPM 22a Standard Score Statigtics

| Subtegt SID-GS SID-AR | SID-NK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MK | SID-MC SID-EI SID-VR |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MIFAN | 50.89 | 51.40 | 51.76 | 51.68 | 53.15 | 52.58 | 50.99 | 52.33 | 52.13 | 50.30 | 51.86 |
| S.D. | 8.56 | 8.56 | 6.93 | 7.36 | 7.80 | 7.70 | 8.91 | 8.57 | 9.22 | 8.62 | 7.05 |
| $N$ | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 | 11558 |

FOPM 22a Standard Score Correlations

| Subtest | SID-GS | ID-A | SID-WX | SID-FC | , | , | , |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SID-GS | 1.00 | 0.59 | 0.76 | 0.63 | 0.26 | 0.27 | 0.49 | 0.56 | 0.60 | 0.61 | 0. |
| SID-AR | 0.59 | 1.00 | 0.59 | 0.57 | 0.41 | 0.39 | 0.39 | 0.72 | 0.60 | 0.49 | 0.63 |
| SID-WK | 0.76 | 0.59 | 1.00 | 0.69 | 0.28 | 0.32 | 0.42 | 0.51 | 0.54 | 0.55 | 97 |
| SID-PC | 0.63 | 0.57 | 0.69 | 1.00 | 0.36 | 0.37 | 0.33 | 0.50 | 0.48 | 0.46 | . 8 |
| SID-NO | 0.26 | 0.41 | 0.28 | 0.36 | 1.00 | 0.63 | 0.04 | 0.45 | 0.17 | 0.15 | . 33 |
| SID-CS | 0.27 | 0.39 | 0.32 | 0.37 | 0.63 | 1.00 | 0.06 | 0.40 | 0.20 | 0.18 | 0.36 |
| SID-AS | 0.49 | 0.39 | 0.42 | 0.33 | 0.04 | 0.06 | 1.00 | 0.21 | 0.65 | 0.67 | . 42 |
| SID-MK | 0.56 | 0.72 | 0.51 | 0.50 | 0.45 | 0.40 | 0.21 | 1.00 | 0.49 | 0.39 | . 55 |
| SID-MC | 0.60 | 0.60 | 0.54 | 0.48 | 0.17 | 0.20 | 0.65 | 0.49 | 1.00 | 0.66 | 0.56 |
| SID-EI | 0.61 | 0.49 | 0.55 | 0.46 | 0.15 | 0.18 | 0.67 | 0.39 | 0.66 | 1.00 | 0.56 |
|  |  |  |  |  |  |  |  |  |  |  |  |

FORM 22a Standard Score Statiatic Differences from the Reference FORM (15h)
Subtest SID-GS STD-AR SID-WK SID-PC SID-NO SID-CS STD-AS STD-MK SID-MC SID-EI SID-VE

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| NERNN | 0.07 | 0.06 | 0.03 | -0.11 | 0.04 | -0.01 | 0.08 | 0.00 | 0.25 | -0.16 | 0.06 |
| S.D. | 0.01 | 0.02 | -0.01 | -0.29 | 0.02 | 0.05 | 0.03 | -0.08 | -0.10 | 0.13 | 0.23 |
| N | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 | -1373 |

FORM 22a Standard Score Correlation Differences from the Reference FORM (15h)
Subtest STD-GS SID-AR SID-WK STD-PC STD-NO SID-CS SID-AS SID-MK SID-MC SID-EI SID-VE

| STD-GS | 0.00 | 0.01 | 0.04 | 0.07 | 0.02 | 0.05 |  | 0.03 | -0.05 | -0.07 | 0.05 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STD-AR | -0.01 | 0.00 | 0.01 | -0.01 | -0.04 | 0.02 | -0.05 | -0.01 | -0.01 | -0.04 | 0.00 |
| STD-WK | 0.04 | 0.01 | 0.00 | 0.03 | -0.00 | 0.03 | -0.07 | 0.01 | -0.01 | -0.04 | 0.01 |
| SID-PC | 0.07 | -0.01 | 0.03 | 0.00 | -0.02 | -0.01 | -0.03 | -0.01 | 0.02 | -0.02 | 0.01 |
| SID-NO | 0.02 | -0.04 | -0.00 | -0.02 | 0.00 | -0.01 | -0.05 | -0.02 | -0.02 | -0.01 | -0.02 |
| STD-CS | 0.05 | 0.02 | 0.03 | -0.01 | -0.01 | 0.00 | -0.04 | 0.00 | -0.00 | 0.01 | 0.02 |
| STD-AS | -0.09 | -0.05 | -0.07 | -0.03 | -0.05 | -0.04 | 0.00 | -0.04 | -0.01 | -0.01 | -0.06 |
| STD-MK | 0.03 | -0.01 | 0.01 | -0.01 | -0.02 | 0.00 | -0.04 | 0.00 | 0.00 | -0.01 | 0.00 |
| STD-MC | -0.05 | -0.01 | -0.01 | 0.02 | -0.02 | -0.00 | -0.01 | 0.00 | 0.00 | -0.01 | 0.00 |
| STD-EI | -0.07 | -0.04 | -0.04 | -0.02 | -0.01 | 0.01 | -0.01 | -0.01 | -0.01 | 0.00 | -0.04 |
| ST | 0.05 | -0.00 |  |  | -0.02 | 0.02 | -0.06 | 0.00 |  |  |  |

FORM 22a Standard Score Statiatic Differences from the operaticnal FCRM (15g)

| Subtes | SID-GS | ID-AR | SID-WiR | SID-PC | -10 | SID-CS | -AS | STD | -MC | ST | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MESAN | -0.12 | 0.33 | -0.24 | -0.38 | 0.31 | -0.25 | 0.10 | -0.11 | 0.06 | -0.02 | 0.17 |
| S.D. | 0.20 | 0.00 | 0.05 | -0.09 | 0.08 | 0.11 | -0.05 | -0.07 | 0.14 | -0.38 | 0.18 |
| N | -1754 | -1754 | -17 | -1754 | -1754 | -1754 | -1754 | -1754 | -175 | -1754 | 17 |

FORM 22a Standard Score correlation Differences fram the operational FORM (15g)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SUbtest | SID-GS SID-AR | SID-WK | SID-PC | SID-NO | SID-CS | SID-AS | SID-MK | SID-MC | SID-EI | SID-VE |  |
| SID-GS | 0.00 | -0.03 | 0.06 | 0.05 | 0.04 | 0.05 | -0.04 | 0.02 | -0.05 | -0.01 | 0.07 |
| SID-AR | -0.03 | 0.00 | -0.00 | 0.02 | -0.01 | 0.00 | -0.00 | 0.01 | -0.02 | 0.02 | 0.01 |
| SID-WK | 0.06 | -0.00 | 0 | -0.04 | -0.01 | -0.01 | 0.02 | 0.02 | 0.03 | 0.08 | -0.00 |
| SID-PC | 0.05 | 0.02 | -0.2 | 0.00 | 0.03 | 0.03 | 0.03 | 0.03 | 0.06 | 0.07 | -0.02 |
| SID-NO | 0.04 | -0.01 | -0.01 | 0.03 | 0.00 | -0.03 | 0.01 | 0.01 | 0.01 | -0.01 | 0.02 |
| SID-CS | 0.05 | 0.00 | -0.01 | 0.03 | -0.03 | 0.00 | 0.01 | -0.00 | 0.01 | 0.03 | 0.01 |
| SID-AS | -0.04 | -0.00 | 0.02 | 0.03 | 0.01 | 0.01 | 0.00 | 0.02 | 0.06 | 0.02 | 0.03 |
| SID-NK | 0.02 | 0.01 | 0.02 | 0.03 | 0.01 | -0.00 | 0.02 | 0.00 | -0.01 | 0.03 | 0.03 |
| SIDDMC | -0.05 | -0.02 | 0.03 | 0.06 | -0.01 | 0.01 | 0.06 | -0.01 | 0.00 | 0.06 | 0.04 |
| SID-EI | -0.01 | 0.02 | 0.08 | 0.07 | 0.02 | 0.03 | 0.02 | 0.03 | 0.06 | 0.00 | 0.09 |
| SID-VE | 0.07 | 0.01 | -0.00 | -0.02 | 0.01 | 0.00 | 0.03 | 0.03 | 0.04 | 0.09 | 0.00 |

Table 11
(continued)
Subtest Means, Standard Deviations, and Intercorrelations, after Application of Current Conversion Tables

FORM 22b Standard Score Statistics

| Subtest | SID-GS | ID-AR | SID-WK | 10-PC |  | TD-CS | SID-AS | STD- | STD-MC | SID-EI | STD-VE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MEPN | 50.88 | 51.34 | 51.71 | 51.64 | 53.02 | 52.57 | 50.85 | 52.39 | 52.03 | 50.60 | 51.84 |
| S.D. | 8.52 | 8.49 | 6.92 | 7.54 | 7.77 | 7.53 | 8.94 | 8.60 | 9.20 | 8.46 | 6.8 |
| N | 10986 | 10986 | 10986 | 10986 | 10986 | 10986 | 10986 | 10986 | 10986 | 10986 | 1098 |

FORM 22b Standard Score Correlations

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STD-GS | 1.00 | 0.60 | 0.75 | 0.66 | 0.26 | 0.28 | 0.50 | 0.55 | 0.61 | 0.62 | 0.77 |
| SID-AR | 0.60 | 1.00 | 0.58 | 0.60 | 0.42 | 0.40 | 0.41 | 0.72 | 0.59 | 0.50 | 0.63 |
| STD-WR | 0.75 | 0.58 | 1.00 | 0.72 | 0.27 | 0.32 | 0.44 | 0.48 | 0.55 | 0.56 | 0.97 |
| STD-PC | 0.66 | 0.60 | 0.72 | 1.00 | 0.38 | 0.40 | 0.36 | 0.52 | 0.49 | 0.49 | 0.87 |
| SID-NO | 0.26 | 0.42 | 0.27 | 0.38 | 1.00 | 0.62 | 0.06 | 0.42 | 0.18 | 0.16 | 0.33 |
| SID-CS | 0.28 | 0.40 | 0.32 | 0.40 | 0.62 | 1.00 | 0.08 | 0.38 | 0.21 | 0.18 | 0.37 |
| SID-AS | 0.50 | 0.41 | 0.44 | 0.36 | 0.06 | 0.08 | 1.00 | 0.24 | 0.67 | 0.67 | 0.45 |
| SID-MK | 0.55 | 0.72 | 0.48 | 0.52 | 0.42 | 0.38 | 0.24 | 1.00 | 0.51 | 0.40 | 0.53 |
| SID-MC | 0.61 | 0.59 | 0.55 | 0.49 | 0.18 | 0.21 | 0.67 | 0.51 | 1.00 | 0.66 | 0.57 |
| SID-EI | 0.62 | 0.50 | 0.56 | 0.49 | 0.16 | 0.18 | 0.67 | 0.40 | 0.66 | 1.00 | 0.57 |
| STD-VE | 0.77 | 0.63 | 0.97 | 0.87 | 0.33 | 0.37 | 0.45 | 0.53 | 0.57 | 0.57 | 1.00 |

FORM 22b Standard Score Statistic Differences from the Reference FOPM (15h)
Subtest SID-GS SID-AR SID-WK SID-PC SID-NO SID-CS SID-AS SID-MK SID-MC SID-EI SID-VE

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SUBLest | SID-GS | SID-AR | SID-WK SID-PC | SID-NO | SID-CS | SID-AS | SID-NK | SID-NC | SID-EI SID-VE |  |  |
| SEAN | 0.07 | -0.00 | -0.02 | -0.16 | -0.09 | -0.02 | -0.07 | 0.06 | 0.15 | 0.15 | 0.04 |
| N.D. | -0.03 | -0.05 | -0.02 | -0.11 | -0.01 | -0.12 | 0.06 | -0.04 | -0.12 | -0.02 | 0.04 |
|  | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 | -1945 |

FCPM 22b Standard Score Correlation Differences from the Reference FOPM (15h)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subteat | SID-GS | SID-AR | SID-WK | SID-PC | SID-NO | SID-CS | SID-AS | SID-NK | SID-MC | SID-EI | SID-VE |
| SID-GS | 0.00 | 0.00 | 0.03 | 0.10 | 0.02 | 0.06 | -0.08 | 0.02 | -0.05 | -0.07 | 0.05 |
| SID-AR | 0.00 | 0.00 | -0.01 | 0.03 | -0.03 | 0.03 | -0.03 | -0.01 | -0.01 | -0.03 | -0.00 |
| SID-WR | 0.03 | -0.01 | 0.00 | 0.06 | -0.01 | 0.03 | -0.04 | -0.02 | 0.00 | -0.04 | 0.00 |
| SID-PC | 0.10 | 0.03 | 0.06 | 0.00 | -0.00 | 0.03 | -0.00 | 0.01 | 0.03 | 0.01 | 0.04 |
| SID-NO | 0.02 | -0.03 | -0.01 | -0.00 | 0.00 | -0.01 | -0.03 | -0.05 | -0.01 | 0.00 | -0.01 |
| SID-CS | 0.06 | 0.03 | 0.03 | 0.03 | -0.01 | 0.00 | -0.02 | -0.02 | 0.00 | 0.01 | 0.03 |
| SID-AS | -0.08 | -0.03 | -0.04 | -0.00 | -0.03 | -0.02 | 0.00 | -0.00 | 0.00 | -0.01 | -0.04 |
| SID-MK | 0.02 | -0.01 | -0.02 | 0.01 | -0.05 | -0.02 | -0.00 | 0.00 | 0.02 | -0.00 | -0.02 |
| SID-MC | -0.05 | -0.01 | 0.00 | 0.03 | -0.01 | 0.00 | 0.00 | 0.02 | 0.00 | -0.00 | 0.01 |
| SID-EI | 0.07 | -0.03 | -0.04 | 0.01 | 0.00 | 0.01 | -0.01 | -0.00 | -0.00 | 0.00 | -0.03 |
| SID-VE | 0.05 | -0.00 | 0.00 | 0.04 | -0.01 | 0.03 | -0.04 | -0.02 | 0.01 | -0.03 | 0.00 |

FORM 22b Standard Score Statistic Differences from the Operational FOPM (15g)
Subtest SID-GS SID-AR SID-WK SID-PC SID-NO SID-CS SID-AS SID-NK SID-MC SID-EI SID-VE

| MISAN | -0.13 | 0.26 | -0.29 | -0.42 | 0.18 | -0.26 | -0.04 | -0.05 | -0.04 | 0.28 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $S . D$. | 0.16 | -0.07 | 0.04 | 0.08 | 0.06 | -0.06 | -0.01 | -0.03 | 0.13 | -0.53 |
| N | -2326 | -2326 | -2326 | -2326 | -2326 | -2326 | -2326 | -2326 | -2326 | -2326 |

FORM 22b Standard Score Correlation Differences from the Operational FORM (15g)

|  |  |  |  |  |  |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Subtest | SID-GS | SID-AR | SID-WK | SID-FC | SID-NO | SID-CS | SID-AS | SID-NK SID-MC | SID-EI SID-VE |  |  |
| SID-GS | 0.00 | -0.02 | 0.05 | 0.08 | 0.04 | 0.06 | -0.03 | 0.01 | -0.04 | -0.00 | 0.07 |
| SID-AR | -0.02 | 0.00 | -0.01 | 0.06 | 0.00 | 0.01 | 0.01 | 0.01 | -0.03 | 0.02 | 0.01 |
| SID-WK | 0.05 | -0.01 | 0.00 | -0.00 | -0.02 | -0.01 | 0.05 | -0.02 | 0.04 | 0.09 | -0.01 |
| SID-FC | 0.08 | 0.06 | -0.00 | 0.00 | 3.05 | 0.06 | 0.06 | 0.05 | 0.07 | 0.10 | 0.01 |
| SID-NO | 0.04 | 0.00 | -0.02 | 0.05 | 0.00 | -0.03 | 0.03 | -0.02 | -0.00 | 0.04 | 0.01 |
| SID-CS | 0.06 | 0.01 | -0.01 | 0.06 | -0.03 | 0.00 | 0.02 | -0.02 | 0.02 | 0.03 | 0.02 |
| SID-AS | -0.03 | 0.01 | 0.05 | 0.06 | 0.03 | 0.02 | 0.00 | 0.05 | 0.07 | 0.02 | 0.05 |
| SID-MK | 0.01 | 0.01 | -0.02 | 0.05 | -0.02 | -0.02 | 0.05 | 0.00 | 0.00 | 0.03 | 0.01 |
| SID-MC | -0.04 | -0.03 | 0.04 | 0.07 | -0.00 | 0.02 | 0.07 | 0.00 | 0.00 | 0.06 | 0.05 |
| SID-EI | -0.00 | 0.02 | 0.09 | 0.10 | 0.04 | 0.03 | 0.02 | 0.03 | 0.06 | 0.00 | 0.10 |
| SID-VE | 0.07 | 0.01 | -0.01 | 0.01 | 0.01 | 0.02 | 0.05 | 0.01 | 0.05 | 0.10 | 0.00 |

Table 12

Subtests and Upper Bounds of Categories for Composites

| Comonsite |  |  | $\frac{\text { Cateqory }}{09 / 15 / 20 / 30 / 49 / 64 / 92 / 99}$ |
| :---: | :---: | :---: | :---: |
|  |  | $2 \mathrm{VE}+\mathrm{AR}+\mathrm{MK}$ |  |
| ARMY** |  |  |  |
| GT | VE | $+\mathrm{AR}$ | $109 \backslash 160$ |
| GM | MK | + EI + AS + GS | 84/89/94/99/104/160 |
| EL | AR | + MK + EI + GS | 84/89/94/99/104/109/114/119/160 |
| CL | AR | $+\mathrm{MK}+\mathrm{VE}$ | 84/89/94/99/104/109/160 |
| MM | NO | $+\mathrm{AS}+\mathrm{MC}+\mathrm{EI}$ | 84/94/99/104/160 |
| SC | AR | $+\mathrm{AS}+\mathrm{MC}+\mathrm{VE}$ | 89/94/99/104/160 |
| CO | CS | $+\mathrm{AR}+\mathrm{MC}+\mathrm{AS}$ | 84/89/94/99/160 |
| FA | AR | $+\mathrm{CS}+\mathrm{MC}+\mathrm{MK}$ | 84/89/94/99/160 |
| OF | NO | $+\mathrm{AS}+\mathrm{MC}+\mathrm{VE}$ | 89/94/99/104/160 |
| ST | VE | + MK + MC + GS | 84/89/94/99/104/109/114/160 |
| NAVY*** |  |  |  |
| EL | AR | + MK + EI + GS | 189/199/203/217/320 |
| E | AR | $+\mathrm{GS}+2 \mathrm{MK}$ | 195/199/203/209/213/320 |
| CL | NO | $+\mathrm{CS}+\mathrm{VE}$ | 159/240 |
| GT | VE | $+\mathrm{AR}$ | 88/95/96/102/107/112/114/160 |
| ME | VE | $+M C+A S$ | 149/157/166/240 |
| EG | MK | $+A S$ | 95/160 |
| CT | VE | + AR + NO + CS | 201/320 |
| HM | VE | $+M K+G S$ | 148/164/240 |
| ST | VE | $+A R+M C$ | 146/240 |
| MR | AR | $+M C+A S$ | 129/157/163/240 |
| BC | VE | $+\mathrm{MK}+\mathrm{CS}$ | 146/152/240 |
| AIR FORCE* |  |  |  |
| M | MC | + GS + 2AS | 43/44/50/56/60/88/99 |
| A | NO | $+\mathrm{CS}+\mathrm{VE}$ | 26/31/39/44/50/60/66/99 |
| G | VE | + AR | $\begin{aligned} & 29 / 34 / 38 / 41 / 42 / 47 / 49 / \\ & 52 / 55 / 57 / 63 / 68 / 69 / 99 \end{aligned}$ |
| E | AR | $+\mathrm{MK}+\mathrm{EI}+\mathrm{GS}$ | $\begin{aligned} & 32 / 38 / 42 / 44 / 45 / 49 / 57 / \\ & 66 / 71 / 76 / 80 / 99 \end{aligned}$ |
| MARINE CORPS** |  |  |  |
| MM | AR | $+\mathrm{EI}+\mathrm{MC}+\mathrm{AS}$ | 84/94/104/114/160 |
| CL | VE | $+M K+C S$ | 79/89/99/109/119/160 |
| GT | VE | $+\mathrm{AR}+\mathrm{MC}$ | 79/89/99/109/160 |
| EL | AR | + MK + EI + GS | 89/99/109/114/160 |

Percentile Scores; AFQT upper bounds are for categories V, IVc, IVb, IVa, IIIb, IIIa, II and I, respectively.
** Standard Scores (Mean=100, S.D. $=20$ ).
*** Sum of Subtest Standard Scores.

Table 13

## Composite-Category-by-Test-Form Chi-Squares

 (Reference, Operational, \& New [20-22] Forms)| Composite |  | D.F. | Chi-Square | Prob. |
| :---: | :---: | :---: | :---: | :---: |
| AFOT | $2 \mathrm{VE}+\mathrm{AR}+\mathrm{MK}$ | 49 | 148.836* | . 000 |
| ARMY |  |  |  |  |
| GT | $\mathrm{VE}+\mathrm{AR}$ | 7 | 6.824 | . 447 |
| GM | $M K+E I+A S+G S$ | 35 | 88.814* | . 000 |
| ETL | $A R+M K+E I+G S$ | 56 | 108.241 | . 000 |
| $\mathrm{CL}_{1}$ | $A R+M K+V E$ | 42 | 46.701 | . 285 |
| MM | $\mathrm{NO}+\mathrm{AS}+\mathrm{MC}+\mathrm{EI}$ | 28 | 81.825* | . 000 |
| SC | $A R+A S+M C+V E$ | 28 | 41.266 | . 051 |
| CO | $C S+A R+M C+A S$ | 28 | 39.739 | . 070 |
| FA | $A R+C S+M C+M K$ | 28 | 27.037 | . 516 |
| OF | $\mathrm{NO}+\mathrm{AS}+\mathrm{MC}+\mathrm{VE}$ | 28 | 75.452* | . 000 |
| ST | $V E+M K+M C+G S$ | 49 | 67.870 | . 038 |
| AIR FORCE |  |  |  |  |
| M | MC + GS + 2AS | 42 | 246.198* | . 000 |
| A | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 49 | 47.891 | . 516 |
| G | $\mathrm{VE}+\mathrm{AR}$ | 84 | 186.039* | . 000 |
| E | $A R+M K+E I+G S$ | 77 | 99.539 | . 043 |
| NAVY |  |  |  |  |
| ET | $A R+M K+E I+G S$ | 28 | 55.575 | . 001 |
| E | $A R+G S+2 M K$ | 35 | 41.523 | . 208 |
| $\mathrm{Cl}_{1}$ | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 7 | 3.043 | . 881 |
| GI | $\mathrm{VE}+\mathrm{AR}$ | 49 | 81.834 | . 002 |
| ME | $V E+M C+A S$ | 21 | 33.496 | . 041 |
| EG | MK + AS | 7 | 12.859 | . 076 |
| CT | $\mathrm{VE}+\mathrm{AR}+\mathrm{NO}+\mathrm{CS}$ | 7 | 3.029 | . 882 |
| HM | $\mathrm{VE}+\mathrm{MK}+\mathrm{GS}$ | 14 | 21.252 | . 095 |
| ST | $\mathrm{VE}+\mathrm{AR}+\mathrm{MC}$ | 7 | 8.277 | . 309 |
| MR | AR + MC + AS | 21 | 39.759 | . 008 |
| BC | $\mathrm{VE}+\mathrm{MK}+\mathrm{CS}$ | 14 | 14.767 | . 394 |
| MARINE CORPS |  |  |  |  |
| M | AR + EI + MC + AS | 28 | 59.689* | . 000 |
| CL | $\mathrm{VE}+\mathrm{MK}+\mathrm{CS}$ | 35 | 37.329 | . 362 |
| GI | $V E+A R+M C$ | 28 | 27.560 | . 488 |
| EI | $A R+M K+E I+G S$ | 28 | 59.054* | . 001 |

* Chi-Square > $2 \times$ D.F.
continued

Table 13
(continued)
Composite-Category-by-Test-Form Chi-Squares (Reference Form vs. Operational 15G and Each New Form [20-22])


ARMY

| GT | 1 | 1.674 | 0.359 | 0.389 | 0.552 | 0.048 | 1.046 | 0.081 |
| :--- | :---: | :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| GM | 5 | $13.844 *$ | 4.455 | 2.538 | $13.408 *$ | $22.825 *$ | 6.901 | 5.831 |
| EL | 8 | 6.414 | 5.586 | 12.441 | $20.021 *$ | $18.656 *$ | 13.078 | 10.193 |
| CL | 6 | 5.547 | 11.266 | 7.564 | 8.003 | $15.443 * *$ | 3.604 | 9.240 |
| MM | 4 | $19.411 *$ | $11.960 *$ | 5.609 | $12.627 *$ | 6.387 | 0.999 | 2.958 |
| SC | 4 | 4.933 | 3.505 | 0.326 | 7.379 | $13.473 *$ | 1.549 | 1.878 |
| CO | 4 | 3.747 | 4.527 | 1.299 | 5.427 | $16.025 * *$ | 2.801 | 3.954 |
| FA | 4 | 3.083 | 2.953 | 2.830 | 1.759 | 5.309 | 0.877 | 2.948 |
| OF | 4 | $22.092 *$ | 5.520 | 4.567 | 6.357 | $14.736 *$ | 5.048 | 1.593 |
| ST | 7 | 12.709 | 9.239 | 13.169 | 11.821 | 9.143 | 7.200 | 9.658 |

AIR FORCE

| M | 6 | 47.080* | 45.779* | 35.388* | 30.692* | 81.012* | 72.520** | 78.533* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 7 | 3.256 | 5.204 | 3.065 | 7.111 | 5.108 | 5.662 | 1.532 |
| G | 12 | 26.608* | ..i.061* | 39.105* | 18.188 | 15.273 | 24.736* | 20.801 |
| E | 11 | 4.071 | 4.638 | 13.596 | 18.648 | 16.120 | 13.705 | 6.903 |

navy

| EL | 4 | 2.970 |
| :--- | :---: | :---: |
| E | 5 | $13.914 \star$ |
| CI | 1 | 0.463 |
| GT | 7 | 8.537 |
| ME | 3 | $7.868^{*}$ |
| EG | 1 | 1.098 |
| CT | 1 | 1.459 |
| HM | 2 | $5.134^{*}$ |
| ST | 1 | 0.779 |
| MR | 3 | 5.041 |
| BC | 2 | 2.591 |

2.611
6.089
0.012
12.277
$6.325^{\star}$
0.185
0.003
$8.722^{\star}$
1.898
5.794
1.555
$16.136 \star$
5.744
0.248
$17.604^{\star}$
$6.752^{\star}$
0.486
0.248
$7.872 \star$
0.083
1.874
1.498
7.174
4.815
0.013
7.132
3.670
$2.694 *$
0.325
$11.208 *$
0.703
$9.325 *$
$4.662 *$

| $10.507 *$ | $9.986^{*}$ |
| :---: | :---: |
| 2.925 | 8.822 |
| 0.609 | 0.133 |
| 12.790 | $15.217 *$ |
| $6.349 \star$ | 1.992 |
| $3.193^{*}$ | 0.084 |
| 1.379 | 0.383 |
| 3.928 | $6.277 *$ |
| 0.838 | 0.121 |
| $24.528 *$ | 3.353 |
| 1.808 | 1.268 |


| 2.707 |
| :---: |
| 7.704 |
| 0.221 |
| $19.714 \star$ |
| 3.190 |
| 0.319 |
| 0.181 |
| 1.772 |
| 0.347 |
| 5.199 |
| 2.885 |

MARINE CORPS

| MM | 4 | $20.082 *$ | $9.286 *$ | 4.745 | $10.726 *$ | $23.985 *$ | 0.685 | 7.453 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CI | 5 | 8.445 | 2.459 | 3.872 | 4.535 | 5.932 | 2.762 | 1.195 |
| GI | 4 | 3.947 | 4.085 | 2.480 | 4.514 | 5.471 | 1.484 | 3.847 |
| EII | 4 | 5.349 | 3.404 | 11.176 | $12.050 *$ | 10.601 | 4.397 | 5.470 |

Table 14
Standard Deviations of Composites

AFOT PERCENTILE
AFOT $\quad|23.932| 23.961|23.925| 24.179|23.935| 23.777|24.334| 23.975 \mid$
ARMY STANDARD SCORE

| GT | 15.003 | 15.012 | 15.004 | 15.040 | 14.974 | 14.838 | 15.232 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| GM | 16.171 | 16.004 | 15.900 | 16.077 | 15.546 | 15.277 | 15.991 |
| EL | 16.010 | 15.918 | 16.068 | 16.156 | 15.773 | 15.483 | 15.892 |
| CL | 15.375 | 15.284 | 15.394 | 15.466 | 15.284 | 15.088 | 15.462 |
| MM | 15.870 | 15.551 | 15.604 | 15.745 | 15.574 | 15.409 | 15.727 |
| MM | 15.744 |  |  |  |  |  |  |
| SC | 16.221 | 15.791 | 16.048 | 16.077 | 15.911 | 15.611 | 16.098 |
| CC | 16.183 | 15.808 | 16.059 | 16.090 | 15.922 | 15.649 | 15.998 |
| FA | 16.025 | 15.928 | 16.159 | 16.197 | 16.032 | 15.884 | 15.970 |
| OF | 15.043 | 14.434 | 14.959 | 14.977 | 14.685 | 14.544 | 14.857 |
| ST | 15.836 | 15.597 | 16.039 | 16.026 | 15.906 | 14.878 |  |
| ST |  |  |  |  |  |  |  |

AIR FORCE PERCENTIILE

| M | 25.967 | 25.474 | 25.327 | 25.400 | 24.853 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| A | 23.821 | 24.014 | 23.882 | 24.001 | 23.764 |
| G | 23.878 | 23.912 | 23.870 | 24.129 | 23.886 |
| E | 23.904 | 23.760 | 23.981 | 24.133 | 23.639 |


| 24.500 | 25.554 |
| :--- | :--- |
| 23.820 | 24.157 |
| 23.729 | 24.281 |
| 23.202 | 23.783 |

25.640 23.799
23.924
23.644

NAVY SSSS

| EL | 28.318 |
| :--- | :--- |
| E | 30.071 |
| CL | 17.686 |
| GT | 13.882 |
| ME | 21.254 |
| EG | 13.825 |
| CT | 23.794 |
| HM | 20.508 |
| ST | 23.794 |
| MR | 22.632 |
| BC | 18.220 |


| 28.157 | 28.423 |
| :--- | :--- |
| 29.951 | 30.378 |
| 17.653 | 17.726 |
| 13.886 | 13.886 |
| 20.478 | 21.010 |
| 13.550 | 13.669 |
| 23.716 | 23.773 |
| 20.326 | 20.876 |
| 23.716 | 23.773 |
| 22.134 | 22.262 |
| 18.188 | 18.264 |

28.577
30.446
17.738
13.920
21.097
13.851
23.846
20.868
23.846
22.282
18.344
27.900
30.463
17.658
13.859
20.854
13.474
23.783
20.889
23.783
22.172
18.031
27.393
29.999
17.611
13.729
20.644
13.250
23.650
20.544
23.650
21.667
18.021

| 28.103 | 27.963 |
| :--- | :--- |
| 30.065 | 30.011 |
| 17.875 | 17.618 |
| 14.097 | 13.874 |
| 21.137 | 21.163 |
| 13.582 | 13.821 |
| 23.964 | 23.700 |
| 20.932 | 20.673 |
| 23.964 | 23.700 |
| 22.340 | 22.387 |
| 18.435 | 18.107 |

MARINE CORPS STANDARD SCORE

| MM | 16.841 |
| :--- | :--- |
| CL | 14.245 |
| GI | 15.990 |
| EI | 16.019 |


| 16.623 | 16.459 |
| :--- | :--- |
| 14.219 | 14.282 |
| 15.787 | 16.113 |
| 15.926 | 16.077 |

16.589
14.338
16.083
16.164
16.591
14.093
15.998
15.780

[^10]16.688
14.405
16.049
15.900
16.653
14.151
15.887
15.814

Table 15
Composite-Category-by-Test-Form Chi-Square for ASVAB 15/16/17,
After Equatings Based on IOT\&E of ASVAB 15/16/17

| composite |  | D.F. | Chi-Square | Prob. |
| :---: | :---: | :---: | :---: | :---: |
| AFQT | $2 \mathrm{VE}+\mathrm{AR}+\mathrm{MK}$ | 42 | 161.889* | . 000 |
| ARMY |  |  |  |  |
| GT | $\mathrm{VE}+\mathrm{AR}$ | 6 | 16.118* | . 013 |
| GM | $M K+E I+A S+G S$ | 30 | 61.126* | . 001 |
| EL | $A R+M K+E I+G S$ | 48 | 85.668 | . 001 |
| CL | $\mathrm{AR}+\mathrm{MK}+\mathrm{VE}$ | 36 | 77.358* | . 000 |
| MM | $N \mathrm{~N}+\mathrm{AS}+\mathrm{MC}+\mathrm{EI}$ | 24 | 105.695* | . 000 |
| SC | $A R+A S+M C+V E$ | 24 | 46.598 | . 004 |
| CO | $C S+A R+M C+A S$ | 24 | 67.394* | . 000 |
| FA | $A R+C S+M C+M K$ | 24 | 47.832 | . 003 |
| OF | $\mathrm{NO}+\mathrm{AS}+\mathrm{MC}+\mathrm{VE}$ | 24 | 54.103* | . 000 |
| ST | $V E+M K+M C+G S$ | 42 | 68.413 | . 006 |
| NAVY |  |  |  |  |
| EL | AR + MK + EI + GS | 24 | 48.487* | . 002 |
| E | $A R+G S+2 M K$ | 30 | 36.016 | . 208 |
| CL | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 6 | 3.010 | . 808 |
| GT | $\mathrm{VE}+\mathrm{AR}$ | 30 | 102.940* | . 000 |
| ME | $\mathrm{VE}+\mathrm{MC}+\mathrm{AS}$ | 18 | 51.008* | . 000 |
| EG | MK + AS | 6 | 13.519* | . 036 |
| CT | $\mathrm{VE}+\mathrm{AR}+\mathrm{NO}+\mathrm{CS}$ | 6 | 3.815 | . 702 |
| HM | $V E+M K+G S$ | 12 | 20.890 | . 052 |
| ST | $\mathrm{VE}+\mathrm{AR}+\mathrm{MC}$ | 6 | 18.101* | . 006 |
| MR | $A R+M C+A S$ | 18 | 47.849* | . 000 |
| BC | $V E+M K+C S$ | 12 | 38.865* | . 000 |
| AIR FORCE |  |  |  |  |
| M | $M C+G S+2 A S$ | 30 | 75.807* | . 000 |
| A | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 42 | 40.596 | . 533 |
| G | $\mathrm{VE}+\mathrm{AR}$ | 60 | 138.701* | . 000 |
| E | AR + MK + ET + GS | 60 | 88.960 | . 009 |
| MARINE CORPS |  |  |  |  |
| MM | $A R+E I+M C+A S$ | 24 | 90.074* | . 000 |
| CL | $\mathrm{VE}+\mathrm{MK}+\mathrm{CS}$ | 30 | 94.259* | . 000 |
| GT | $\mathrm{VE}+\mathrm{AR}+\mathrm{MC}$ | 24 | 55.064* | . 000 |
| ET | $A R+M K+E I+G S$ | 24 | 38.179 | . 033 |

[^11]Table 16

## Standard Deviations of Composites <br> from ASVAB 15/16/17 IOT\&E

| Compos |  | 15C | 15A | 15B | 16A | 16B | 17A | 178 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| APOT | $2 \mathrm{VE}+\mathrm{AR}+\mathrm{MR}$ | 24.05 | 23.85 | 24.15 | 23.79 | 24.31 | 24.06 | 23.85 |
| GI | $V E+A R M Y$ | 15.92 | 15.82 | 15.96 | 15.88 | 16.03 | 15.91 | 15.88 |
| GM | $\mathbf{M R}+\mathbf{E I}+\mathbf{A S}+\mathbf{G S}$ | 17.07 | 16.44 | 16.67 | 16.40 | 16.55 | 16.78 | 16.66 |
| EL | $A R+N K+E I+G S$ | 16.80 | 16.23 | 16.53 | 16.30 | 16.53 | 16.49 | 16.44 |
| CL | $\mathbf{A R}+\mathbf{M K}+\mathbf{V E}$ | 16.10 | 15.90 | 16.04 | 15.86 | 16.01 | 15.97 | 15.84 |
| $\cdots$ | $\mathrm{NO}+\mathrm{AS}+\mathrm{MC}+\mathrm{EI}$ | 16.49 | 15.94 | 16.02 | 15.92 | 16.16 | 16.02 | 15.90 |
| SC | $\mathbf{A R}+\mathrm{AS}+\mathrm{MC}+\mathrm{VE}$ | 17.10 | 16.60 | 26.70 | 16.68 | 16.72 | 16.59 | 16.49 |
| Co | $C S+A R+M C+A S$ | 16.63 | 16.17 | 16.31 | 16.28 | 16.33 | 16.09 | 16.01 |
| FA | $A R+C S+M C+M R$ | 16.28 | 16.18 | 16.30 | 16.15 | 16.22 | 15.97 | 15.86 |
| OF | $N O+A S+M C+V E$ | 15.78 | 15.21 | 15.23 | 15.29 | 15.38 | 15.29 | 15.08 |
| ST | $V E+M E+M C+G S$ | 16.63 | 16.32 | 16.50 | 16.53 | 16.57 | 16.43 | 16.26 |
| EL | $\cdots \mathrm{N}$ | 29.72 | 28.71 | 29.23 | 28.82 | 29.34 | 29.17 | 29.08 |
| E | $A R+G S+2 M K$ | 30.99 | 30.54 | 30.88 | 30.70 | 30.98 | 30.74 | 30.56 |
| CL | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 18.36 | 18.25 | 28.37 | 18.36 | 18.48 | 18.24 | 13.26 |
| GT | $\mathrm{VE}+\mathrm{AR}$ | 14.73 | 14.64 | 14.76 | 14.69 | 14.83 | 14.72 | 14.70 |
| ME | $V E+M C+A S$ | 22.51 | 21.72 | 21.76 | 21.96 | 21.83 | 21.80 | 21.54 |
| E | MK + AS | 14.44 | 14.08 | 14.17 | 13.86 | 13.91 | 14.08 | 13.94 |
| CT | $V E+A R+N O+C S$ | 24.59 | 24.52 | 24.60 | 24.56 | 24.77 | 24.55 | 24.52 |
| H | $V E+M K+G S$ | 21.72 | 21.38 | 21.66 | 21.83 | 21.93 | 21.70 | 21.60 |
| ST | $V E+A R+M C$ | 22.19 | 21.88 | 22.04 | 21.98 | 22.10 | 21.74 | 21.64 |
| MR | $A R+M C+A S$ | 23.50 | 22.87 | 23.00 | 22.82 | 22.99 | 22.64 | 22.59 |
| BC | $V E+M K+C S$ | 18.90 | 18.83 | 18.99 | 19.00 | 19.02 | 18.84 | 18.75 |
| M | MC + AS + ECRCES | 27.12 | 26.36 | 26.49 | 26.45 | 26.48 | 26.62 | 26.52 |
| A | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 24.16 | 24.25 | 24.34 | 24.57 | 24.10 | 24.28 | 24.32 |
| G | $V E+A R$ | 24.59 | 24.47 | 24.77 | 24.34 | 24.98 | 24.63 | 24.55 |
| E | $A R+M R+E I+G S$ | 25.07 | 24.31 | 24.70 | 24.40 | 24.76 | 24.67 | 24.60 |
| M | $\begin{array}{r} \text { MARIE CORPS } \\ A R+E I+M C+A S \end{array}$ | 17.63 | 17.08 | 17.27 | 17.11 | 17.29 | 17.11 | 17.09 |
| CL | $V E+M K+C S$ | 14.78 | 14.73 | 14.85 | 14.86 | 14.88 | 14.73 | 14.67 |
| GT | $V E+A R+M C$ | 16.78 | 16.54 | 16.66 | 16.62 | 16.71 | 16.44 | 16.36 |
| ELL | $A R+M K+E I+G S$ | 16.81 | 26.24 | 16.53 | 16.30 | 16.53 | 16.49 | 16.45 |

Table 17

## Standard Deviations of Composites from ASVAB 18/19 IOT\&E

| Comoosite |  | 15c | 18A | 188 | 198 | 198 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| APCTI | $2 V E+A R+M K$ | 23.94 | 24.32 | 24.03 | 24.35 | 23.95 |
| Apan |  |  |  |  |  |  |
| GM | $N \mathrm{~N}+\mathrm{EI}+\mathrm{AS}+\mathrm{ES}$ | 16.67 | 16.30 | 16.13 | 16.15 | 16.15 |
| EL | $A R+M R+E I+G S$ | 16.53 | 16.58 | 16.46 | 16.32 | 16.28 |
| CL | $A R+M K+V E$ | 15.97 | 16.15 | 16.03 | 16.13 | 15.93 |
| M ${ }^{\text {c }}$ | $N \mathrm{~N}+\mathrm{AS}+\mathrm{MC}+\mathrm{EI}$ | 16.67 | 16.13 | 16.06 | 16.05 | 16.16 |
| SC | $A R+A S+M C+V B$ | 16.81 | 16.28 | 16.26 | 16.42 | 16.46 |
| $\infty$ | $C S+M R+M C+A S$ | 16.87 | 16.48 | 16.50 | 16.66 | 16.64 |
| FA | $A R+C S+M C+M K$ | 16.73 | 17.07 | 17.06 | 17.23 | 17.01 |
| OF | $N \mathrm{NO}+\mathrm{AS}+\mathrm{MC}+\mathbf{V E}$ | 16.05 | 15.61 | 15.59 | 15.65 | 15.69 |
| ST | $\mathbf{V E}+\mathbf{M K}+\mathbf{M C}+\mathbf{G S}$ | 16.37 | 16.70 | 16.57 | 16.73 | 16.59 |
| MAVY |  |  |  |  |  |  |
| E | $A R+G S+2 N R C$ | 30.84 | 31.54 | 31.34 | 31.31 | 31.02 |
| CIL | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 19.30 | 19.32 | 19.54 | 19.41 | 19.17 |
| GI | $\mathbf{V E}+\mathbf{A R}$ | 14.59 | 14.62 | 14.54 | 14.67 | 14.52 |
| ME | $V E+B C+A S$ | 22.08 | 21.31 | 21.29 | 21.40 | 21.48 |
| EG | $\mathrm{MR}+\mathrm{AS}$ | 14.09 | 13.84 | 13.74 | 13.83 | 13.85 |
| CT | $\mathrm{VE}+\mathrm{AR}+\mathrm{NO}+\mathrm{CS}$ | 25.91 | 26.14 | 26.25 | 26.20 | 25.81 |
| HM | $\mathbf{V E}+\mathbf{M R}+\mathbf{G S}$ | 21.34 | 21.95 | 21.73 | 21.77 | 21.58 |
| ST | $V E+A R+M C$ | 21.96 | 22.04 | 21.98 | 22.27 | 22.12 |
| MR | $A R+M C+A S$ | 23.14 | 22.22 | 22.30 | 22.43 | 22.58 |
| BC | $V E+M R+C S$ | 19.40 | 19.61 | 19.66 | 19.58 | 19.33 |
| AIR FCRCE |  |  |  |  |  |  |
| A | $\mathrm{NO}+\mathrm{CS}+\mathrm{VE}$ | 24.99 | 25.09 | 25.25 | 25.14 | 25.07 |
| G |  | 24.82 | 24.93 | 24.78 | 25.00 | $24.79$ |
| E | $A R+N K+E I+G S$ | 24.56 | 24.65 | 24.42 | 24.29 | 24.22 |
| M | $\begin{gathered} \text { MARINE CORPS } \\ A R \end{gathered}$ | 17.30 | 16.64 | 16.59 | 16.68 | 16.80 |
| CL | $\mathbf{V E}+\mathrm{MK}+\mathrm{CS}$ | 15.17 | 15.33 | 15.38 | 15.31 | 15.11 |
| GI | $\mathbf{V E}+\mathbf{R R}+\mathrm{MC}$ | 16.60 | 16.67 | 16.61 | 16.84 | 16.72 |
| EL | $A R+M K+E I+G S$ | 16.54 | 16.60 | 16.47 | 16.33 | 16.29 |

## Table 18

## AFQT Category Distributions <br> for Three Subsets of the Data

All Initial Tests, $N=118,265$
gut score on comosite
64.00
$30.00 \quad 20.00$
15.00
9.00
92.00

Percentage at or Above cut Score
Form
$\begin{array}{llllllll}15 \mathrm{H} & 5.14 & 35.99 & 57.87 & 80.97 & 91.42 & 94.60 & 97.83\end{array}$


| 15G | -0.95 | 1.11 | -0.33 | 0.01 | 0.01 | 0.12 | 0.11 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 20A | -0.23 | 0.62 | -0.21 | 1.11 | 0.67 | 0.24 | -0.09 |
| 20B | 0.81 | 0.69 | -0.93 | 0.16 | 0.49 | 0.41 | -0.01 |
| 21A | -0.03 | -0.19 | -0.89 | 0.87 | 0.82 | 0.63 | 0.03 |
| 21B | 0.37 | 0.27 | -0.15 | 1.15 | 0.96 | 0.78 | 0.21 |
| 22A | 0.91 | 0.91 | -0.62 | 0.61 | 0.42 | 0.21 | -0.17 |
| 22B | 0.05 | 0.57 | -0.09 | 0.47 | 0.84 | 0.69 | 0.21 | After Editing for Extreme Unbalancing, $\mathrm{N}=99,254$

Qut Score on Camposite
$\begin{array}{llllllll}92.00 & 64.00 & 49.00 & 30.00 & 20.00 & 15.00 & 9.00\end{array}$
Percentage at or Above cut Score
Form

| $15 H$ | 5.07 | 35.95 | 57.62 | 80.91 | 91.39 | 94.53 | 97.76 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



Strongly Balanced Samples, $N=59,976$

| 92.00 | Cut Saone on composite |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 64.00 | 49.00 | 30.00 | 20.00 | 15.00 | 9.00 |
|  | Percentage at or Above gut Scone |  |  |  |  |  |
| 5.30 | 37.34 | 59.55 | 82.22 | 92.05 | 95.14 | 98.05 |


| Form |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 15H | 5.30 | 37.34 | 59.55 | 82.22 | 92.05 | 95.14 | 98.05 |
|  |  | Contrast | with | Reference Form | Percentage | (Form - 15H) |  |
| 15G | -0.79 | 1.17 | -0.56 | -0.25 | 0.01 | -0.14 | -0.00 |
| 20A | -0.46 | 0.38 | -0.36 | 1.42 | 0.93 | 0.31 | 0.05 |
| 20B | 0.90 | 0.96 | -0.73 | 0.20 | 0.52 | 0.38 | -0.05 |
| 21A | -0.01 | -0.29 | -1.11 | 0.78 | 0.70 | 0.54 | 0.04 |
| 21B | 0.36 | 0.55 | 0.02 | 1.26 | 0.91 | 0.58 | 0.24 |
| 22A | 1.03 | 0.78 | -0.82 | 0.60 | 0.53 | 0.11 | -0.17 |
| 22B | 0.06 | 0.18 | -0.51 | 0.19 | 0.94 | 0.53 | 0.27 |

Table 19
Air Force M Composite Distributions for Three Subsets of the Data

All Initial Tests, $N=118,265$
$89.00 \quad 61.00 \quad \begin{gathered}\text { cut } \\ 57.00\end{gathered} \frac{\text { Score }}{} \quad 51.00 \quad \frac{\text { Composite }}{45.00 \quad 44.00}$

Form
Percentage at or Above cut Score
15H
$\begin{array}{llllll}9.83 & 43.91 & 49.52 & 56.17 & 62.51 & 62.98\end{array}$ $\begin{array}{ccccc}\text { contrast } & \text { with Reference Form Rercentage (Form - } & \text { 15H) } \\ -0.16 & 0.31 & -0.52 & -0.65 & -0.40 \\ 0.41\end{array}$
15G

| -0.16 | 0.31 | -0.52 | -0.65 | -0.40 | 0.41 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| -0.95 | 1.46 | 1.23 | 1.12 | 1.45 | 2.04 |
| -1.00 | 0.60 | -0.01 | 0.07 | 0.23 | 0.76 |
| -1.58 | -0.80 | -0.23 | -0.13 | 0.18 | 0.68 |
| -2.06 | -0.33 | 0.50 | 0.95 | 1.48 | 2.09 |
| -0.40 | 0.87 | -0.04 | -0.19 | -0.17 | 0.91 |
| -0.07 | 0.54 | -0.44 | -0.47 | -0.13 | 0.90 |

After Editing for Extreme Unbalancing, $\mathbf{N}=99,254$


Form
15H
Percentage at or Above cut Score

|  | Comtrast | with Reference | Form | Rercentage | (Forn |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 15G | -0.12 | 0.31 | -0.44 | -0.54 | -0.33 | 0.40 |
| 20A | -0.80 | 1.40 | 1.27 | 1.07 | 1.47 | 1.99 |
| 20B | -0.99 | 0.57 | -0.03 | 0.01 | 0.17 | 0.64 |
| 21A | -1.42 | 0.44 | -0.03 | -0.03 | 0.13 | 0.50 |
| 21B | -2.10 | -0.13 | 0.74 | 1.10 | 1.63 | 2.16 |
| 22A | -0.36 | 0.72 | -0.06 | -0.15 | -0.14 | 0.86 |
| 22B | -0.20 | 0.10 | -0.85 | -0.86 | -0.52 | 0.54 |
| Strongly | Balanced Samples, $\mathrm{N}=59,976$ |  |  |  |  |  | Contrast with Reference Form Percentage (Form - 15H)

Strongly Balanced Samples, $N=59,976$
$89.00 \quad 61.00 \quad \begin{array}{llll}\text { Cut } \\ 57.00 & \text { Score on } & 51.00 & \frac{\text { Composite }}{45.00} 44.00\end{array}$
Percentage at or Above cut Score
Form

| $15 H$ | 10.29 | 45.57 | 51.35 | 58.05 | 64.52 | 65.01 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | Contrast with Reference Form Percentage (Form - 15H) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15G | -0.08 | 0.64 | -0.34 | -0.63 | -0.51 | 0.22 |  |
| 20A | -0.92 | 1.49 | 1.19 | 1.24 | 1.63 | 2.13 |  |
| 20B | -0.92 | 1.02 | 0.31 | 0.31 | 0.38 | 0.92 |  |
| 21A | -1.56 | -1.05 | -0.48 | -0.31 | -0.10 | 0.42 |  |
| 21B | -2.28 | -0.38 | 0.27 | 0.87 | 1.28 | 1.76 |  |
| 22A | -0.86 | 0.90 | -0.01 | 0.02 | -0.10 | 0.84 |  |
| 22B | -0.04 | 0.31 | -0.82 | -0.77 | -0.54 | 0.39 |  |

Table 20
Army GM Composite Distributions
for Three Subsets of the Data

All Initial Tests, $\mathrm{N}=118,265$
cut Score on Composite
$105.00 \quad 100.00 \quad 95.00 \quad 90.00 \quad 85.00$
Form
Percentage at or Above cut Score
$\begin{array}{llllll}46.79 & 58.70 & 68.32 & 78.28 & 85.86\end{array}$
Contrast with Reference Form Rercentage (Form - 15H)

| -1.14 | -1.45 | -1.05 | 0.26 | 0.81 |
| ---: | ---: | ---: | ---: | ---: |
| 0.52 | 0.75 | 1.17 | 0.88 | 0.81 |
| 0.29 | -0.07 | -0.12 | 0.19 | -0.08 |
| -0.86 | -0.55 | 0.59 | 1.18 | 1.07 |
| -0.12 | 0.30 | 1.42 | 1.82 | 1.83 |
| -0.05 | -0.68 | 0.12 | -0.00 | 0.33 |
| 0.00 | -0.16 | 0.62 | 0.79 | 0.64 |

After Editing for Extreme Unbalancing, $\mathrm{N}=99,254$
$105.00 \quad 100.00 \begin{array}{llll}\text { Cut } & \text { Score } & \text { on Camposite } \\ 95.00 & 80.00 & 85.00\end{array}$

| Form | Percentage at or Above cut Score |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15H | Conrast 46 | 58.49 | 68.11 | 78.28 | 85.96 |  |
|  | Contrast with |  | Fo |  |  | (Form - 15H) |
| 15G | -0.92 | -1.28 | -0.86 | 0.18 | 0.67 |  |
| 20A | 0.70 | 0.92 | 1.14 | 0.61 | 0.53 |  |
| 20B | 0.38 | 0.04 | -0.11 | 0.17 | -0.16 |  |
| 21A | -0.63 | -0.40 | 0.72 | 1.08 | 0.89 |  |
| 218 | 0.11 | 0.49 | 1.60 | 1.78 | 1.74 |  |
| 22A | 0.24 | -0.41 | 0.30 | -0.15 | 0.04 |  |
| 22B | -0.06 | -0.41 | 0.48 | 0.40 | 0.29 |  |

Strongly Balanced Samples, $\mathrm{N}=59,976$
105.00 Cut Score on Composite

Form
Percentage at or Above Cut Score

| -1.31 | -1.90 | -1.63 | -0.05 | 0.88 |
| ---: | ---: | ---: | ---: | ---: |
| 0.33 | 0.67 | 1.01 | 1.08 | 1.36 |
| 0.63 | 0.29 | -0.09 | 0.24 | 0.01 |
| -1.29 | -0.79 | -0.06 | 0.74 | 0.84 |
| -0.56 | 0.16 | 1.19 | 1.40 | 1.82 |
| -0.32 | -1.00 | -0.24 | -0.05 | 0.43 |
| -0.55 | -0.85 | -0.38 | 0.45 | 0.71 |

Table 21
ASVAB Form 20A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents


Table 21
(continued)
ASVAB Form 20A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents


Table 22
ASVAB Form 20B
Conversion of Raw Test Scores to 1980 Standa! : Score Equivalents


Table 22
(continued)
ASVAB Form 20B
Conversion of Raw Test Scores to 1980 Standard Score Equivalents


Table 23
ASVAB Form 21A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents


Table 23
(continued)
ASVAB Form 21A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

| Raw | AS | 圂 | E | EI | Y8 | Bax | Raw | AS | MS | VC | ET | VE | 8an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 24 | 29 | 23 | 22 | 20 | 0 | 25 | 69 | 67 | 70 |  | 39 | 25 |
| 1 | 25 | 30 | 25 | 25 | 20 | 1 | 26 |  |  |  |  | 40 | 26 |
| 2 | 27 | 32 | 27 | 27 | 20 | 2 | 27 |  |  |  |  | 41 | 27 |
| 3 | 29 | 33 | 28 | 29 | 20 | 3 | 28 |  |  |  |  | 42 | 28 |
| 4 | 30 | 35 | 30 | 31 | 20 | 4 | 29 |  |  |  |  | 43 | 29 |
| 5 | 32 | 37 | 32 | 34 | 20 | 5 | 30 |  |  |  |  | 44 | 30 |
| 6 | 33 | 38 | 33 | 36 | 20 | 6 | 31 |  |  |  |  | 45 | 31 |
| 7 | 35 | 40 | 35 | 39 | 21 | 7 | 32 |  |  |  |  | 45 | 32 |
| 8 | 37 | 41 | 37 | 41 | 22 | 8 | 33 |  |  |  |  | 46 | 33 |
| 9 | 39 | 43 | 38 | 44 | 23 | 9 | 34 |  |  |  |  | 47 | 34 |
| 10 | 41 | 45 | 40 | 46 | 24 | 10 | 35 |  |  |  |  | 48 | 35 |
| 11 | 43 | 47 | 42 | 49 | 25 | 11 | 36 |  |  |  |  | 49 | 36 |
| 12 | 45 | 48 | 44 | 51 | 26 | 12 | 37 |  |  |  |  | 50 | 37 |
| 13 | 47 | 50 | 46 | 53 | 27 | 13 | 38 |  |  |  |  | 51 | 38 |
| 14 | 49 | 51 | 48 | 55 | 28 | 14 | 39 |  |  |  |  | 51 | 39 |
| 15 | 51 | 53 | 50 | 57 | 29 | 15 | 40 |  |  |  |  | 52 | 40 |
| 16 | 52 | 54 | 52 | 59 | 30 | 16 | 41 |  |  |  |  | 53 | 41 |
| 17 | 54 | 55 | 54 | 62 | 31 | 17 | 42 |  |  |  |  | 54 | 42 |
| 18 | 56 | 57 | 56 | 64 | 32 | 18 | 43 |  |  |  |  | 55 | 43 |
| 19 | 58 | 58 | 58 | 66 | 33 | 19 | 44 |  |  |  |  | 56 | 44 |
| 20 | 59 | 60 | 60 | 68 | 34 | 20 | 45 |  |  |  |  | 57 | 45 |
| 21 | 62 | 61 | 62 |  | 35 | 21 | 46 |  |  |  |  | 58 | 46 |
| 22 | 63 | 63 | 64 |  | 36 | 22 | 47 |  |  |  |  | 59 | 47 |
| 23 | 65 | 64 | 65 |  | 37 | 23 | 48 |  |  |  |  | 60 | 48 |
| 24 | 67 | 66 | 67 |  | 38 | 24 | 49 |  |  |  |  | 61 | 49 |
|  |  |  |  |  |  |  | 50 |  |  |  |  | 62 | 50 |

Table 24
ASVAB Form 21B
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

| Raw | GS | AR | WK | PC | 10 | Cs | Raw | Raw | GS | NR | He | PC | no | Cs | Raw |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 20 | 25 | 20 | 20 | 20 | 22 | 0 | 45 |  |  |  |  | 61 | 50 | 45 |
| 1 | 20 | 27 | 20 | 21 | 20 | 22 | 1 | 46 |  |  |  |  | 61 | 51 | 46 |
| 2 | 22 | 28 | 20 | 24 | 20 | 23 | 2 | 47 |  |  |  |  | 61 | 51 | 47 |
| 3 | 25 | 29 | 20 | 27 | 20 | 23 | 3 | 48 |  |  |  |  | 62 | 52 | 48 |
| 4 | 27 | 30 | 21 | 30 | 20 | 24 | 4 | 49 |  |  |  |  | 62 | 53 | 49 |
| 5 | 29 | 32 | 23 | 33 | 20 | 24 | 5 | 50 |  |  |  |  | 62 | 53 | 50 |
| 6 | 30 | 33 | 24 | 35 | 21 | 25 | 6 | 51 |  |  |  |  |  | 54 | 51 |
| 7 | 32 | 34 | 25 | 38 | 22 | 25 | 7 | 52 |  |  |  |  |  | 54 | 52 |
| 8 | 34 | 35 | 27 | 41 | 23 | 25 | 8 | 53 |  |  |  |  |  | 55 | 53 |
| 9 | 35 | 36 | 28 | 44 | 24 | 26 | 9 | 54 |  |  |  |  |  | 56 | 54 |
| 10 | 37 | 38 | 29 | 47 | 25 | 26 | 10 | 55 |  |  |  |  |  | 56 | 55 |
| 11 | 38 | 39 | 30 | 50 | 26 | 27 | 11 | 56 |  |  |  |  |  | 57 | 56 |
| 12 | 40 | 40 | 32 | 53 | 27 | 27 | 12 | 57 |  |  |  |  |  | 58 | 57 |
| 13 | 42 | 42 | 33 | 56 | 28 | 28 | 13 | 58 |  |  |  |  |  | 58 | 58 |
| 14 | 43 | 43 | 35 | 58 | 29 | 29 | 14 | 59 |  |  |  |  |  | 59 | 59 |
| 15 | 45 | 44 | 36 | 61 | 30 | 29 | 15 | 60 |  |  |  |  |  | 60 | 60 |
| 16 | 47 | 46 | 38 |  | 31 | 30 | 16 | 61 |  |  |  |  |  | 60 | 61 |
| 17 | 49 | 48 | 39 |  | 32 | 31 | 17 | 62 |  |  |  |  |  | 61 | 62 |
| 18 | 52 | 49 | 41 |  | 34 | 31 | 18 | 63 |  |  |  |  |  | 61 | 63 |
| 19 | 54 | 51 | 42 |  | 35 | 32 | 19 | 64 |  |  |  |  |  | 62 | 64 |
| 20 | 56 | 53 | 44 |  | 36 | 33 | 20 | 65 |  |  |  |  |  | 63 | 65 |
| 21 | 58 | 54 | 45 |  | 38 | 33 | 21 | 66 |  |  |  |  |  | 63 | 66 |
| 22 | 60 | 56 | 46 |  | 39 | 34 | 22 | 67 |  |  |  |  |  | 64 | 67 |
| 23 | 62 | 58 | 47 |  | 40 | 35 | 23 | 68 |  |  |  |  |  | 64 | 68 |
| 24 | 65 | 59 | 48 |  | 41 | 36 | 24 | 69 |  |  |  |  |  | 65 | 69 |
| 25 | 67 | 60 | 49 |  | 42 | 36 | 25 | 70 |  |  |  |  |  | 65 | 70 |
| 26 |  | 62 | 50 |  | 43 | 37 | 26 | 71 |  |  |  |  |  | 66 | 71 |
| 27 |  | 63 | 52 |  | 45 | 38 | 27 | 72 |  |  |  |  |  | 67 | 72 |
| 28 |  | 64 | 53 |  | 46 | 39 | 28 | 73 |  |  |  |  |  | 67 | 73 |
| 29 |  | 65 | 54 |  | 47 | 40 | 29 | 74 |  |  |  |  |  | 68 | 74 |
| 30 |  | 66 | 55 |  | 48 | 40 | 30 | 75 |  |  |  |  |  | 68 | 75 |
| 31 |  |  | 56 |  | 49 | 41 | 31 | 76 |  |  |  |  |  | 69 | 76 |
| 32 |  |  | 58 |  | 50 | 42 | 32 | 77 |  |  |  |  |  | 69 | 77 |
| 33 |  |  | 59 |  | 51 | 42 | 33 | 78 |  |  |  |  |  | 70 | 78 |
| 34 |  |  | 60 |  | 52 | 43 | 34 | 79 |  |  |  |  |  | 70 | 79 |
| 35 |  |  | 61 |  | 53 | 44 | 35 | 80 |  |  |  |  |  | 71 | 80 |
| 36 |  |  |  |  | 54 | 44 | 36 | 81 |  |  |  |  |  | 71 | 81 |
| 37 |  |  |  |  | 55 | 45 | 37 | 82 |  |  |  |  |  | 71 | 82 |
| 38 |  |  |  |  | 56 | 46 | 38 | 83 |  |  |  |  |  | 72 | 83 |
| 39 |  |  |  |  | 57 | 46 | 39 | 84 |  |  |  |  |  | 72 | 84 |
| 40 |  |  |  |  | 58 | 47 | 40 | 85 |  |  |  |  |  |  | 85 |
| 41 |  |  |  |  | 59 | 48 | 41 | 86 |  |  |  |  |  |  | 86 |
| 42 |  |  |  |  | 59 | 48 | 42 | 87 |  |  |  |  |  |  | 87 |
| 43 |  |  |  |  | 60 | 49 | 43 | 88 |  |  |  |  |  |  | 88 |
| 44 |  |  |  |  | 60 | 49 | 44 | 89 |  |  |  |  |  |  | 89 |

Table 24
(continued)
ASVAB Form 21B
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

| R9\% | AS | 14 | UC | EI | VE | Rav | Rat | AS | E* | 区 | EI | y | Rax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 24 | 29 | 23 | 22 | 20 | 0 | 25 | 69 | 68 | 70 |  | 40 | 25 |
| 1 | 25 | 30 | 25 | 25 | 20 | 1 | 26 |  |  |  |  | 41 | 26 |
| 2 | 27 | 32 | 27 | 27 | 20 | 2 | 27 |  |  |  |  | 42 | 27 |
| 3 | 29 | 33 | 28 | 29 | 20 | 3 | 28 |  |  |  |  | 43 | 28 |
| 4 | 30 | 35 | 30 | 31 | 20 | 4 | 29 |  |  |  |  | 43 | 29 |
| 5 | 32 | 37 | 32 | 34 | 20 | 5 | 30 |  |  |  |  | 44 | 30 |
| 6 | 33 | 38 | 33 | 36 | 21 | 6 | 31 |  |  |  |  | 45 | 31 |
| 7 | 35 | 40 | 35 | 39 | 22 | 7 | 32 |  |  |  |  | 46 | 32 |
| 8 | 37 | 41 | 37 | 41 | 22 | 8 | 33 |  |  |  |  | 47 | 33 |
| 9 | 39 | 43 | 38 | 44 | 23 | 9 | 34 |  |  |  |  | 48 | 34 |
| 10 | 41 | 44 | 40 | 46 | 24 | 10 | 35 |  |  |  |  | 49 | 35 |
| 11 | 43 | 46 | 42 | 49 | 25 | 11 | 36 |  |  |  |  | 50 | 36 |
| 12 | 45 | 47 | 44 | 51 | 26 | 12 | 37 |  |  |  |  | 50 | 37 |
| 13 | 47 | 49 | 46 | 53 | 27 | 13 | 38 |  |  |  |  | 51 | 38 |
| 14 | 49 | 51 | 48 | 55 | 28 | 14 | 39 |  |  |  |  | 52 | 39 |
| 15 | 51 | 52 | 50 | 57 | 29 | 15 | 40 |  |  |  |  | 53 | 40 |
| 16 | 52 | 54 | 52 | 59 | 30 | 16 | 41 |  |  |  |  | 54 | 41 |
| 17 | 54 | 56 | 54 | 62 | 31 | 17 | 42 |  |  |  |  | 55 | 42 |
| 18 | 56 | 57 | 56 | 64 | 32 | 18 | 43 |  |  |  |  | 56 | 43 |
| 19 | 58 | 59 | 58 | 66 | 34 | 19 | 44 |  |  |  |  | 56 | 44 |
| 20 | 59 | 61 | 60 | 68 | 35 | 20 | 45 |  |  |  |  | 57 | 45 |
| 21 | 61 | 62 | 62 |  | 36 | 21 | 46 |  |  |  |  | 58 | 46 |
| 22 | 63 | 63 | 64 |  | 37 | 22 | 47 |  |  |  |  | 59 | 47 |
| 23 | 65 | 65 | 65 |  | 38 | 23 | 48 |  |  |  |  | 60 | 48 |
| 24 | 67 | 66 | 67 |  | 39 | 24 | 49 50 |  |  |  |  | 61 | 49 50 |

Table 25
ASVAB Form 22A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

| 8aw | GS | A8 | WK | PC | 82 | Cs | Ray | Bay | GS | AR MS | RC | $\triangle 2$ | cs | Rax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 20 | 25 | 20 | 20 | 20 | 22 | 0 | 45 |  |  |  | 60 | 49 | 45 |
| 1 | 21 | 27 | 20 | 20 | 20 | 22 | 1 | 46 |  |  |  | 61 | 50 | 46 |
| 2 | 23 | 28 | 20 | 23 | 20 | 23 | 2 | 47 |  |  |  | 61 | 51 | 47 |
| 3 | 25 | 29 | 20 | 25 | 20 | 23 | 3 | 48 |  |  |  | 61 | 51 | 48 |
| 4 | 27 | 30 | 21 | 28 | 20 | 24 | 4 | 49 |  |  |  | 62 | 52 | 49 |
| 5 | 29 | 32 | 23 | 31 | 20 | 24 | 5 | 50 |  |  |  | 62 | 52 | 50 |
| 6 | 31 | 33 | 24 | 34 | 21 | 25 | 6 | 51 |  |  |  |  | 53 | 51 |
| 7 | 33 | 35 | 25 | 37 | 22 | 25 | 7 | 52 |  |  |  |  | 54 | 52 |
| 8 | 34 | 36 | 27 | 40 | 23 | 26 | 8 | 53 |  |  |  |  | 54 | 53 |
| 9 | 36 | 37 | 28 | 43 | 24 | 26 | 9 | 54 |  |  |  |  | 55 | 54 |
| 10 | 38 | 38 | 30 | 46 | 25 | 27 | 10 | 55 |  |  |  |  | 55 | 55 |
| 11 | 39 | 39 | 31 | 49 | 26 | 27 | 11 | 56 |  |  |  |  | 56 | 56 |
| 12 | 41 | 41 | 33 | 52 | 26 | 28 | 12 | 57 |  |  |  |  | 57 | 57 |
| 13 | 43 | 42 | 34 | 54 | 27 | 28 | 13 | 58 |  |  |  |  | 57 | 58 |
| 14 | 45 | 43 | 36 | 57 | 28 | 29 | 14 | 59 |  |  |  |  | 58 | 59 |
| 15 | 46 | 45 | 37 | 60 | 30 | 29 | 15 | 60 |  |  |  |  | 58 | 60 |
| 16 | 48 | 46 | 39 |  | 31 | 30 | 16 | 61 |  |  |  |  | 59 | 61 |
| 17 | 50 | 48 | 40 |  | 32 | 31 | 17 | 62 |  |  |  |  | 60 | 62 |
| 18 | 52 | 49 | 41 |  | 33 | 32 | 18 | 63 |  |  |  |  | 60 | 63 |
| 19 | 54 | 51 | 42 |  | 35 | 32 | 19 | 64 |  |  |  |  | 61 | 64 |
| 20 | 56 | 52 | 43 |  | 36 | 33 | 20 | 65 |  |  |  |  | 61 | 65 |
| 21 | 58 | 54 | 45 |  | 37 | 34 | 21 | 66 |  |  |  |  | 62 | 66 |
| 22 | 61 | 55 | 46 |  | 38 | 34 | 22 | 67 |  |  |  |  | 63 | 67 |
| 23 | 63 | 57 | 47 |  | 39 | 35 | 23 | 68 |  |  |  |  | 63 | 68 |
| 24 | 66 | 58 | 48 |  | 41 | 36 | 24 | 69 |  |  |  |  | 64 | 69 |
| 25 | 68 | 59 | 49 |  | 42 | 37 | 25 | 70 |  |  |  |  | 64 | 70 |
| 26 |  | 61 | 50 |  | 43 | 37 | 26 | 71 |  |  |  |  | 65 | 71 |
| 27 |  | 62 | 51 |  | 44 | 38 | 27 | 72 |  |  |  |  | 66 | 72 |
| -28 |  | 63 65 | 53 <br> 54 |  | 45 | 39 | 28 | 73 |  |  |  |  | 66 | 73 |
| 29 30 |  | 65 | 54 55 |  | 46 | 40 | 29 30 | 74 |  |  |  |  | 67 | 74 |
| 31 |  |  | 56 |  | 48 | 41 | 31 | 76 |  |  |  |  | 68 | 76 |
| 32 |  |  | 58 |  | 49 | 42 | 32 | 77 |  |  |  |  | 69 | 77 |
| 33 |  |  | 59 |  | 50 | 42 | 33 | 78 |  |  |  |  | 69 | 78 |
| 34 35 |  |  | 60 |  | 51 | 4 | $\begin{array}{r}34 \\ 35 \\ \hline\end{array}$ | 79 |  |  |  |  | 70 | 79 |
| 35 36 |  |  | 61 |  | 52 | 44 | 35 36 | 88 |  |  |  |  | 70 | 88 |
| -37 |  |  |  |  | 55 | 45 | 37 | 82 |  |  |  |  | 71 | 82 |
| 38 |  |  |  |  | 56 | 45 | 38 | 83 |  |  |  |  | 71 | 83 |
| 39 |  |  |  |  | 57 | 46 | 39 | 84 |  |  |  |  | 72 | 84 |
| 40 41 |  |  |  |  | 57 | 46 | 40 | 85 |  |  |  |  |  | 85 |
| 42 |  |  |  |  | 59 | 48 | 42 | 87 |  |  |  |  |  | 87 |
| 43 |  |  |  |  | 59 | 48 | 43 | 88 |  |  |  |  |  | 88 |
| 44 |  |  |  |  | 60 | 49 | 44 | 89 |  |  |  |  |  | 89 |

Table 25
(continued)
ASVAB Form 22A
Conversion of Raw Test Scores to 1980 Standard Score Equivalents


Table 26

ASVAB Form 22B
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

|  |  |
| :---: | :---: |
| 8 |  |
| 9 | 8－6．6N\％ |
| 8 |  |
| 䒺 |  |
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| 8 |  |
| 8 | ¢ |
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| 凩 | ¢N¢ |
| 0 |  |
| 3 |  |

continued

Table 26
(continued)
ASVAB Form 22B
Conversion of Raw Test Scores to 1980 Standard Score Equivalents

| Raw | AS | M8 | M | EI | ys | Rav | Rav | AS | M | UC | EI | VE | Raw |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 24 | 29 | 23 | 22 | 20 | 0 | 25 | 69 | 67 | 70 |  | 40 | 25 |
| 1 | 26 | 31 | 25 | 25 | 20 | 1 | 26 |  |  |  |  | 41 | 26 |
| 2 | 28 | 33 | 27 | 27 | 20 | 2 | 27 |  |  |  |  | 42 | 27 |
| 3 | 29 | 34 | 28 | 29 | 20 | 3 | 28 |  |  |  |  | 43 | 28 |
| 4 | 31 | 36 | 30 | 32 | 20 | 4 | 29 |  |  |  |  | 44 | 29 |
| 5 | 33 | 38 | 32 | 34 | 20 | 5 | 30 |  |  |  |  | 45 | 30 |
| 6 | 35 | 39 | 34 | 37 | 21 | 6 | 31 |  |  |  |  | 46 | 31 |
| 7 | 37 | 41 | 36 | 39 | 21 | 7 | 32 |  |  |  |  | 46 | 32 |
| 8 | 39 | 42 | 38 | 41 | 22 | 8 | 33 |  |  |  |  | 47 | 33 |
| 9 | 40 | 44 | 39 | 43 | 23 | 9 | 34 |  |  |  |  | 48 | 34 |
| 10 | 42 | 46 | 41 | 46 | 24 | 10 | 35 |  |  |  |  | 49 | 35 |
| 11 | 44 | 47 | 43 | 48 | 25 | 11 | 36 |  |  |  |  | 50 | 36 |
| 12 | 46 | 49 | 45 | 51 | 26 | 12 | 37 |  |  |  |  | 50 | 37 |
| 13 | 47 | 50 | 47 | 53 | 27 | 13 | 38 |  |  |  |  | 51 | 38 |
| 14 | 49 | 52 | 49 | 55 | 29 | 14 | 39 |  |  |  |  | 52 | 39 |
| 15 | 51 | 53 | 51 | 58 | 30 | 15 | 40 |  |  |  |  | 53 | 40 |
| 16 | 52 | 54 | 53 | 60 | 31 | 16 | 41 |  |  |  |  | 54 | 41 |
| 17 | 54 | 56 | 55 | 62 | 32 | 17 | 42 |  |  |  |  | 55 | 42 |
| 18 | 56 | 57 | 57 | 64 | 34 | 18 | 43 |  |  |  |  | 55 | 43 |
| 19 | 57 | 59 | 59 | 66 | 35 | 19 | 44 |  |  |  |  | 56 | 44 |
| 20 | 59 | 60 | 61 | 69 | 36 | 20 | 45 |  |  |  |  | 57 | 45 |
| 21 | 61 | 62 | 63 |  | 37 | 21 | 46 |  |  |  |  | 58 | 46 |
| 22 | 63 | 63 | 64 |  | 38 | 22 | 47 |  |  |  |  | 59 | 47 |
| 23 | 65 | 64 | 66 |  | 39 | 23 | 48 |  |  |  |  | 60 | 48 |
| 24 | 67 | 66 | 68 |  | 40 | 24 | 49 |  |  |  |  | 61 | 49 |
|  |  |  |  |  |  |  | 50 |  |  |  |  | 62 | 50 |

Figure 1 a
Unamocthed and 8mootred OS 15h

$\rightarrow$ Raw Frequency $\quad+$ Poly Log-Linear

Figure 16
Unemoothed and Smoothed GS 21ab


Figure 10
Unemocthed end 8ncothed GS 20ap


Figure 1d Unsmoothed and Smoothed GS 22a/


Figure 1. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating GS

Figure 2a
Unemocined and Emoothed AR 15 h


Figure 2c
Unemocened end Smoothed AR 200


Figure 20
Unemocthed and 8mootred AR 20.

Figure 20
Unemoothed and Smoctned AR 21a


Figure 2. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AR

Figure 2a
Unmocthed and Emoothed AR i5h


Figure $2 f$
Unsmootred and Smoothed AR22a


Floure 20
Unemopined end emoonnd AR 21b


Figure 2 g
Unsmoothed and smoothed AR 220


Figure 2, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AR

Figure 3a
Unmocitred end 8moctred WK 15h


Figure 3 C
Unemoctred and 8moothed WK 200


Fioure 30
Unemootred and 8moctred wx 200


Figure 3d Unemoothed end 8modtred WK 21 a

$\rightarrow$ Raw Frequency + Poly. Log-Lnear

Figure 3. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating WK

Figure 3a
Unmoothed end 8mootred WX 15h


Figure $3 f$
Unemoothed end Smoothed WK 2za


Figure 30
Unenoothed end 8mocthed WK 21b


Figure 3g Unemoothed end Smocthed WK 2zo


Figure 3, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating WK

Figure 4 a
Unamoctred end emodtrad PC 15h


Figure $4 c$
Unmootred and Smoothed PC 200


Figure 4b
unemoctived ind ancothed PC 20 .

$\rightarrow$ Rew Froquency $\rightarrow$ Pory. Loo-Lineer

Figure $4 d$
Unemootred end 8mootred PC 21a


Figure 4. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating PC

Figure 40
Unanoothed end 8moothed PC 15h


Figure $4 f$ Unamoothed end Smootred PC 2za


Figure 46 Unomoothed end emocined PC 216


Figure 49 Unamoothed and Smootred PC 220


Figure 4, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating PC

Figure 5 a
Unemectred end Emoctred NO ish


Figure 5 C
unemoctred and smootred NO 21abo


Figure 5b
Unamoctined end Bmoctred NO 20060


Figure 5d
Unamoomed end smoothed NO 2zalo


Figure 5. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating NO

Figure 6
Unomaring tind enocthed C8 im


Figure 6 C
Unumoerned and Emoothed CS 21a


Figure 60
Unemoctied end 8modted C3 enorb


Figure 6d Unemoothed end 8mocthed CS 21b

$\rightarrow$ Rew Frequency $\rightarrow$ Poly. Log-Uneer

Figure 6. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating CS

Figure 6 a
Unmoctred end Broctinad C8 15h


Figure 60
Unemootred end Smoothed CS 2020


Figure 6, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating CS

Figure 7a
Unemocined and Smootred AS 15h


Figure 7c
Unamoothed end Smoothed AS 21 ab


Figure 76
Unemocthed end emocined AS zoab


Figure 7d
Unsmoothed and Smoothed As 22and


Figure 7. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating AS

Figure 8a
Unemocthed and Sinoothed MK15h


Figure 8c
Uninootind and Snoothed MK 200


Figure 8b
Unemocthed End Emoctind Mik 200


Figure 8d
Unmoothed end Smoothed MK 21a

$\rightarrow$ Raw Frequency + Poly. Log-Linear

Figure 8. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MK

Figure 8 a
Unevodined and Smocined MK 15h


Figure 8 f
Unemoothed end Smocthed MK 22a


Figure 80
Unemodtred end 8noctred MKK 21b


Figure 89
Unemoothed end 8 moched max 2zo


Figure 8, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MK

Figure 9a
Unomoctered end Smocthed MC 15h


Figure 9 C
Unamoothed and Smoothed MC 21ak


Figure 96
Unamoothed end 8mocthed MC 20ab


Figure 9d
Unemoothed and Bmoothed MC z2ato


Figure 9. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating MC

Figure 10a
Unwoothed and 8moothed EI 15h


Figure 10. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating EI

Figure 11a
unamoctred end 8moothed VE 15n


Figure 11 C
Unemoothed end Smoothed VE 20\%


Figure 110 Unemogned end smoonted VE 2at


Figure 11d Unemoothed end Emoothed VE 21a


Figure 11. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating VE

Figure 11a
Unmoceled and emootred VE 15h


Figure $11 f$
Unanocthed and Smoothed VE 22a

$\rightarrow$ Rew Froquency $\rightarrow$ Poly. Log-Unear

Figure 110
Unemoctred ind emocined VE 21b


Figure 119
Unamoothed and Smoothed VE 22b


Figure 11, Con't. Unsmoothed and Polynomial Log-Linear Smoothed Distributions for Equating VE

Figure 12a
Corture win betraty: ©S 2000


Figure 12b
Cortent with lientiv: $\mathbf{C 3} 21 \mathrm{a}$ o


Figure 12c
Contrat Win identity: GS 22ab


Figure 12 Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for GS

Fioure 13a
Cortitut Win Piener. Dtot: CS 20nb


Figure 13c
Contren With Roter. Diat.: OS 2zab


Fioure 13b
Cortrea win Putr. Dot: 08 21ab


Figure 142
Conent Winh termer: AR 200


Figure 14c Contret Winh identity: AR 21a


Figure $14 b$



Figure 14d conrreat win keverity: AR 210


Figure 14. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for AR



Figure 14, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial
Log

Floure 15a
Contreat win Rever. Dint: AR 200


Figure 15c
Cortinat win Peder. Diat: AR 21 Ie


Fioure 15b
Contrat wit Peler. Dex:AR200


Figure 15d
Contriat winh Rever. Dat: AR 21b


Figure 15. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AR

Figure 150
Contren will Potr. Dut: AR 22a


Figure 15 :
Cortured Win Reder. Dide: AR 2mb


Figure 15, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for AR

Figure 16a
Cortrex Winh idenuy: WK 200


Figure 16c
Contrat Winh kentily: WK 21a


Floure 16b
Correat Win therimer: WK 200


Figure 16d Contruet Winh identity: WK 21b


Figure 16. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for WK

Figure 16e
Corfract Win idemtiry: WK 22 a


Figure 16f
Contras Win iderime. WK 2ab


Figure 16, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for WK

Figure 17a
Conterat winh fiver. Onet: WK 200


Figure 17c
Contreat wion Peder. Dese: WK $21 a$


Figure 170
Contrat Win Peter. Dext: WK 200


Figure 17d
Contrast With Rever. Dive: WK 21b


Figure 17. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for WK

Figure $17 e$


Figure 171


Figure 17, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for WK

Fioure $18 a$
Conten Win identry: PC 200


Figure 18c
Contred Win identity: PC 21a


Figure 18b
Correar Win ketrivy: PC 200


Figure 180 Contragt With ldermy: PC 210


Figure 18. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for PC

Figure 180 commat win keotity: PC 2za


Figure 18 Combect wini loentiy: PC zzo


Figure 18, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for PC

Figure 19a
Content win Rolve. Dust: PC 200


Figure 19c
Contrast Witi foter. Dist: PC 21a


$$
\begin{aligned}
& \rightarrow \text { Retrence Diat } \\
& \rightarrow \text { Poty. Log Unoer }
\end{aligned}
$$

Figure 190
Contreat Win Paver. Onet: PC 200


Figure 19d
Contreat win Peler. Diat: PC 216


Figure 19. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for PC

Figure 190
Conturet With Peter. Dext: PC 220


Figure 19f



Figure 19, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for PC

Figure 20a
Contred Winin hemuty. NO 2006


Figure 20c
Contras With identity: NO z2alo


Figure 20b
Cortent win kdentry: NO 21eb


Figure 20. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for NO

Figure 21 a
Corter win Paver. Dot: NO 20ado


Figure 21c
Contreat With Pder. Dist: NO 22ath


Fioure 210
Contret win Fiver. Det: NO 2106


Figure 21. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for NO

Figure $22 a$
Content Winh keritly: CS 20arb

Figure 220
Contrant Winh identry: C8 214


Figure 22c
Contreat with kentity: CS 21b



Figure $22 d$
Contrast Wht ldentiy: CS 22ab


Figure 22. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for CS

Fioure 23a
Cormen whil Rever. Dut: CS 2000


Figure 23c
Contrest With Refor. Dist: CS 21b


Figure 230
Contrex Win Retur. Dext: CS $21 a$


Figure 23d
Contrast Whin Aever. Dete: CS z2as


Figure 23. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumalative Distributions of Reference Form for CS

Floure 240
Conmat win hivivit: As 2000


Figure 24 C
Contrat win kientry: AS 2zano


Figure 24b
conman win lerim. AB 2tab


Fioure 259



Fioure 25 c
Contreat Win Rever. Diat: AS 22as


Figure 26b
Contrat winh River. Dex: AS 2100

Floure 28a
Cortrex Winh lderiny: Ux 200


Figure 26c
Contere Win ldentity: MK 21 a


Figure 28b
Cortrad Win detrey, NK200


Figure 26. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for MK

Figure 28d
Contreat Win iderity: MX 210


Figure $26 i$
Contrar Wini identity: MK 22D



Figure 260



Figure 26, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for MK

Figure 27a
Cortred Win Reder. Diat: MK 20e


Figure 27c
contere With Foter. Onet: MK 21s


Figure 27b
Contint win Rumer Duti: NK20


Figure 27d
Contrant with Paver. Dint: MK 210


Figure 27. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for MK

Figure 27e
Contrex Will Rover. Dint: MK 22a


Figure 274
Contrant With Reder. Dive.: MK 220


Figure 27, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for MK

Figure 28a
Continat Wini bientioy: MC 2006



Figure 280
Controet Winh lderimy: MC 21ab

Figure 28c
Contrat Whin identity: MC 22a/o


Figure 28. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for MC

Figure 29a
Contrat Whit Pater. Duat: MC 200b


Figure 29c
Contrast With Foter. Dist.: MC 22a/


Figure 296
Contrat With Anter. Dist: MC 21a0


Figure 30a
Corrica Winh identity: El 20ath


Figure 300
Contruat With kervity: El 21ad


Figure 30c
Contrat With identity: El 22as


Figure 30. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial LogLinear Equatings With Linear-Identity Equating for EI

Figure 31a
Contrant Wen Rover. Diat: El 20e\%


Figure 31c
Contrest With Refer. Dist: El 22ab


Figure 31b
Contraet With Reter. Dint: El 21ab


Figure 31. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for EI

Fioure 32a
Contrent Wiwh iderity: VE 20e


Figure 32c
Contrex With identity: VE 21a


Figure 32b
Corturat with identiv: VE 200


Figure 32d
Contrast With kdentily: VE 21b


Figure 32. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for VE

Figure $32 \theta$
Contrax With identily: VE 2za


Figure 32
Contren With iderity: VE 2ob


Figure 32, Con't. Standard-Score Contrast of Linear-Rescaling, Quartic Log-Linear and Polynomial Log-Linear Equatings With Linear-Identity Equating for VE

Figure 33a
Contrat Wil Reter. Diet: VE 200


Figure 33c
Contreat Win Peoter. Diet: VE 21a


Figure 330
Contrex With Reder. Dut: VE 200


Figure 33d
Contreat With fider. Dint: VE 21b


Figure 33. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for VE

Figure 330
Conten whin Ruor. One: VE 2za


Figure 33
Contran win Rutr. Dex: VE zee


Figure 33, Con't. Contrast of Cumulative Distributions of Quartic and Polynomial Log-Linear Equated Scores With Cumulative Distributions of Reference Form for VE

Floure 34
Puct Antion Componert: All Foms


Figure 34 C
Fint Pinctpel Componert: 21a 821 b

$\rightarrow 15 n+150 \rightarrow 21 a \rightarrow 21 b$

Figure 34b
First Pinclpal Component 201 1200

$-15 h+150 \rightarrow 200 \rightarrow 200$

Figure 34d
Fint Pincipal Component: 22a \&220

$\rightarrow 15 h+150-4200-520$

Figure 34. First Principal Component of Power Subtest Standard Scores, by Test Form

Figure 35 a
Sacond and Thitd Componertit: 15h


Figure 35c
8econd and Thind Components: 20m


Figure 35b
8econd and Thind Conaponatite: 15e


Figure 35d
Sccond and Thid Componmerte: 206



Figure 35. Second and Third Principal Components of Power Subtest Standard Scores, by Test Form

Figure 350
sacond and Thrd Componenta: $21 a$


Figure 359
Second and Thitd Components: 22a


Figure $35 t$
8econd end Thid Componerts: 21b



Figure 35h
Second end Thid Componerts: 22\%


Figure 35, Con't. Second and Third Principal Components of Power Subtest Standard Scores, by Test Form


[^0]:    ${ }^{1}$ For each subtest, the reference-form score scale is defined by a standard-score transformation (mean $=50$ and standard deviation $=10$ ) of the number-right score. Standard scores are based on the mean and standard deviation of the subtest in a sample from the 1980 18-23-year-old American youth population (Department of Defense, 1982). See Table 1 for the normative mean and standard deviation of the number-right scores of each subtest.

[^1]:    ${ }^{2}$ For each subtest, the reference-form score scale is defined by a standard-score transformation (mean $=50$ and standard deviation $=10$ ) of the number-right score. Standard scores are based on the mean and standard deviation of the subtest in a sample from the 1980 18-23-year-old American youth population (Department of Defense, 1982). See Table 1 for the normative mean and standard deviation of the number-right scores of each subtest.

[^2]:    ${ }^{3}$ Information about previous ASVAB testing was provided by recruiters who brought or sent the subjects to be tested.
    ${ }^{4}$ As can be seen from the first two columns of Table 2, the least frequently administered forms were those with the highest form-identification numbers and, therefore, were located lowest in a spiralled set of forms to be administered.

[^3]:    ${ }^{5}$ If forms were perfectly spiralled at a site, then the maximum number of test forms having zero number of administrations would equal the total number of forms (eight) minus the total number of tests administered at the site (for sites administering fewer than eight tests). For sites administering eight or more tests, the maximum number of forms with zero administrations would be zero. To permit the inclusion of data from some small sites where spiralling was not perfect, the requirement of perfect spiralling was replaced by computing the maximum permissible number of zero administrations (MAXZERO) from the total number of test administered at a site (NTOT) as follows:

    MAXZERO $=\left(7.5-0.5^{*}\right.$ NTOT $)$, if NTOT $<16$
    MAXZERO $=0 \quad$, if NTOT $>=16$

[^4]:    6 These answer-sheet equivalents for the reference form (ASVAB 8a) are shown in the second column of Tables 16 (for NO) and Tables 17 (for CS) in Bloxom et al. (1992).

[^5]:    ${ }^{7}$ Appendix F also contains equated standard scores that were re-developed here for the current operational form, ASVAB 15 g . However, these equatings were not used for any of the subsequent analyses reported here.
    ${ }^{8}$ Note that the consistent pattern of results for ASVAB 21a and 21b was due to the fact that both GS and EI had the same items in those two forms.

[^6]:    ${ }^{9}$ Note that the degrees of freedom vary considerably across composites because of the wide variation in the number of categories defined by their cutting scores.

[^7]:    ${ }^{10}$ Note that, like $z_{\text {djj }}, d_{d j}$ is zero when $z_{d j}$ is zero, whether the latter is due to negative or null differences between $n_{d j}$ and $m_{d d}$.
    ${ }^{11}$ Because the ratio, $\mathrm{n}_{\mathrm{dj}} / \mathrm{d}_{\mathrm{dj}}$, is not an integer, the probability $\mathrm{p}_{\mathrm{tdj}}$ was used to define a sequence of non-integers, $s_{d j}+p_{u d j}, s_{d j}+2 p_{u j j}, \ldots, s_{u j}+k p_{u j}, \ldots$, which were used to select cases to be deleted. Specifically, the $\mathbf{k}$-th case was deleted where the following condition held for truncated values of elements of the sequence:
    trunc. $\left[s_{w j}+k p_{p_{d j}}\right]>$ trunc. $\left[s_{u j j}+(k-1) p_{u j}\right]$. The start value, $s_{d j}<1$, was .5 for the first group ( $\mathrm{td}=1$ ) and was the decimal remainder from the truncation of the last number of the sequence for each successive group; i.e., for all $t d>1, s_{\mathrm{djj}}=$ dec. $\mathrm{rem} .\left[\max .\left(s_{(d \mathrm{~d}-1 \mathrm{j}}+\mathrm{kp}_{(\mathrm{dd}-1 \mathrm{j})}\right)\right]$.
    ${ }^{12}$ Note that the target form is the form used least frequently in testing group $t$ and so can differ across testing groups.

[^8]:    * Chi-square significant at alpha $=.05 / 15=.0033$

[^9]:    * Data pooled for subtests with same items in different order.

[^10]:    16.232
    14.090
    15.795
    15.492

[^11]:    * Chi-Square > $2 \times$ D.F.

