

**INSTALLATION RESTORATION PROGRAM**

**AD-A277 739**

**FINAL**

2



**Site Investigation Report**

**Volume 2**

**Appendices A Through G**

**November 1992**

161st AIR REFUELING GROUP  
ARIZONA AIR NATIONAL GUARD  
SKY HARBOR INTERNATIONAL AIRPORT  
PHOENIX, ARIZONA



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THIS QUANTITY REFLECTS 3

Hazardous Waste Remedial Actions Program  
Oak Ridge K-25 Site  
Oak Ridge, Tennessee 37831-7606  
Managed by MARTIN MARIETTA ENERGY SYSTEMS, INC  
For the U.S. DEPARTMENT OF ENERGY under contract DE-AC05-84OR21400

1. Agency Use Only (Leave Blank)		2. Report Date	3. Report Type and Dates Covered	
		NOV. 1997	SITE INVESTIGATION REPORT	
4. Title and Subtitle			5. Funding Numbers	
SLY HARBOR HAS EXIST, PROCEED, MS VOL. 2				
6. Author(s)				
7. Performing Organization Name(s) and Address(es)			8. Performing Organization Report number	
IT CORPORATION 312 DUNNONS BLVD KNOXVILLE, TN 37422				
9. Sponsoring/Monitoring Agency Name(s) and Address(es)			10. Sponsoring/Monitoring Agency Report Number	
Hazardous Waste Remedial Action Program Oak Ridge TN  Air National Guard Readiness Center Andrews Air Force Base, Maryland 20331				
11. Supplemental Notes				
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Approved for public release; distribution is unlimited				
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SITE INVESTIGATION OF HAS (S) HAS SITE AT SLY HARBOR FOR NATIONAL GUARD BASE AND ONE (1) HAS AT FORTY SEVEN RESERVATION. THIS REPORT CONTAINS				
14. Subject Terms			15. Number of Pages	
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FINAL  
SITE INVESTIGATION REPORT  
161ST AIR REFUELING GROUP  
ARIZONA AIR NATIONAL GUARD  
SKY HARBOR INTERNATIONAL AIRPORT  
AND PAPAGO MILITARY RESERVATION  
PHOENIX, ARIZONA

VOLUME 2  
APPENDICES  
A THROUGH G

Submitted To:

AIR NATIONAL GUARD READINESS CENTER  
ANDREWS AIR FORCE BASE, MARYLAND

Submitted By:

HAZARDOUS WASTE REMEDIAL ACTIONS PROGRAM  
Oak Ridge K-25 Site  
Oak Ridge, Tennessee 37831-7606  
managed by  
MARTIN MARIETTA ENERGY SYSTEMS, INC.  
for the  
U.S. DEPARTMENT OF ENERGY  
under contract DE-AC05-84OR21400

Prepared By:

IT CORPORATION  
312 DIRECTORS DRIVE  
KNOXVILLE, TENNESSEE 37923

NOVEMBER 1992

RECEIVED

Accession For	
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Unannounced	<input type="checkbox"/>
Justification	<input type="checkbox"/>
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A-1	

## List of Appendices

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### Appendix

### Title

#### VOLUME 2

- A Variance and Nonconformance Reports
- B Preliminary Review of Hydrogeologic Data for Facilities Adjacent to Sky Harbor Air National Guard Base
- C Geophysical Survey Report
- D SOV Survey Report
- E Soil Boring Logs
- F Piezometer and Monitoring Well Completion Diagrams
- G Piezometer and Monitoring Well Development Records

#### VOLUME 3

- H Sample Collection Logs
- I Slug Tests and Analysis
- J Potentiometric Measurements
- K Results of Screening Analyses
- L Tabulation of Soil Analytical Results
- M Tabulation of Water Analytical Results

**APPENDIX A**  
**VARIANCE AND NONCONFORMANCE REPORTS**



# VARIANCE LOG

## CHRONOLOGIC LIST OF PROJECT VARIANCES

PROJECT NUMBER 409721 PAGE 1 OF 1

PROJECT NAME SKY HARBOR

DATE <small>VAR. # APPROVED BY</small>	VARIANCE GRANTED AND APPLICABLE DOCUMENT	RESPONSIBLE INDIVIDUAL
11/29/90	VAR. #1 USE OF DIFFERENT GC INSTRUMENT; FIELD SAMPLING PLAN (FSP)	S. SARES
11/29/90	VAR. #2 USE OF EVACUATED GLASS VIALS FOR SOV; FSP	S. SARES
12/11/90	VAR. #3 MODIFICATION OF SITE #3 SAMPLING POINTS	S. SARES / J. WILSON
12/12/90	VAR. #4 CHANGE IN ANALYTICAL PROCEDURES & EQUIPMENT FOR ON-SITE FIELD SCREENING OF SOIL BORINGS/SAMPLES	DOUG PERRY
1/11/91	VAR. #5 CHANGE IN PIEZO. / WELL SAND PACK	S. SARES
1/11/91	VAR. #6 CHANGE IN SOIL CLASSIFICATION AND SAMPLING FORMS	S. SARES
1/16/91	VAR. #7 SAMPLE COLLECTION/SUBMIT	S. SARES
1/17/91	VAR. #8 CHANGE IN ANALYTE TESTS	ORRALL FERGUSON
1/24/91	VAR. #9 SITE A, DELETION OF <sup>SOL</sup> BORING SAMPLES	S. SARES
2/13/91	VAR. #10 GROUNDWATER SAMPLING PURGE PROCEDURE	S. SARES
4/9/91	VAR. #11 GROUNDWATER SAMPLING OF 2 IN. PIEZOMETER	S. SARES



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# VARIANCE FORM

VARIANCE NO. 1

PROJECT NO. 409721.02 PAGE 1 OF 1

PROJECT NAME SKY HARBOR ANG BASE SI DATE 29 Nov 90

## VARIANCE (INCLUDE JUSTIFICATION)

THE SKY HARBOR WORK PLANS WERE PREPARED SPECIFYING A PHOTOVAC 10550 GC/PD FOR ANALYSIS OF SOV SAMPLES FOR AROMATIC AND HALOGENATED VOLATILE ORGANIC COMPOUNDS. DETECTION LIMITS FOR THIS EQUIPMENT ARE TYPICALLY 20-100 PPB (UG/L) FOR SOV AROMATIC SAMPLES AND 50 PPB FOR HALOGENATED. THE SUBCONTRACTOR SELECTED FOR SOV ANALYSIS PROPOSES TO UTILIZE A "SHIMADZU 14A" GAS CHROMATOGRAPH WITH FID AND ECD RATHER THAN THE PHOTOVAC. THE SHIMADZU EQUIPMENT IS "LABORATORY QUALITY" AS OPPOSED TO A "FIELD" SCREENING INSTRUMENT LIKE THE PHOTOVAC 10550. USE OF THE SHIMADZU SHOULD PROVIDE MORE EFFICIENT LABORATORY OPERATION AND LOWER DETECTION LIMITS. DETECTION LIMITS FOR THE SHIMADZU ~~WHICH~~<sup>SOP</sup> ~~11-29-90~~ ARE EXPECTED TO BE APPROXIMATELY 0.1 TO 1 PPB FOR HALOGENATED COMPOUNDS AND 1 PPB FOR AROMATIC COMPOUNDS.

## APPLICABLE DOCUMENT:

SECTION 5.2  
FINAL SITE INVESTIGATION FIELD SAMPLING PLAN, 161ST AIR REFUELING GROUP, AE, AIR NATIONAL GUARD, SKY HARBOR INTERNATIONAL AIRPORT, PHOENIX, ARIZONA, SEPTEMBER 1990.

CC: B. Stanley (MIMS)

REQUESTED BY

*[Signature]*

DATE 11-29-90

APPROVED BY

*[Signature]*  
Project Manager

DATE 11/29/90

*[Signature]*  
Quality Assurance Officer

DATE 30 NOV 90

*[Signature]*  
INTERIM PROJECT MGR.

DATE 1/21/91



# VARIANCE FORM

VARIANCE NO. 2

PROJECT NO. 409721.02 PAGE 1 OF 1

PROJECT NAME SKY HARBOR AND BASE SI DATE 29 NOV 90

## VARIANCE (INCLUDE JUSTIFICATION)

SOV SAMPLE CONTAINER CHANGE FROM TEDLAR BAG TO EVACUATED GLASS VIAL.  
CONTAINER FILL METHOD CHANGE FROM DESSICATOR DEFLETION TO ACTIVE PLACEMENT.

SKY HARBOR WORK PLANS WERE PREPARED USING IT'S NORMAL PROCEDURE FOR SAMPLE COLLECTION. RFPs WERE LET TO TWO QUALIFIED FIRMS FOR EXECUTION OF SOV SURVEY. EACH FIRM RESPONDED WITH MINOR CHANGES TO SAMPLE COLLECTION AND HANDLING PROCEDURES. THE VENDOR WITH PROCEDURES MOST CLOSELY FOLLOWING IT'S WAS SELECTED. THE METHOD OF COLLECTION IS DESCRIBED BELOW.

SAMPLE CONTAINERS ARE EVACUATED GLASS VIALS RATHER THAN TEDLAR BAGS. THE VIALS WILL BE FILLED BY ACTIVE SYSTEM RATHER THAN DESSICATOR DEFLETION. VIALS MEET EPA CLEANING CRITERIA FOR ORGANIC COMPOUNDS. SAMPLES ARE PUMPED INTO VIALS AT 15 PSIG.

THE USE OF "EPA CLEAN" GLASS VIALS INSTEAD OF TEDLAR BAGS <sup>WILL</sup> ~~WILL NOT CAUSE~~ AND THE ACTIVE PLACEMENT METHOD WILL NOT <sup>CHANGE</sup> ~~CHANGE~~ DATA QUALITY; RATHER, PLACEMENT OF SAMPLES INTO CONTAINERS AT HIGHER THAN ATMOSPHERIC PRESSURE SHOULD DECREASE POTENTIAL FOR SAMPLE CONTAMINATION DUE TO CONTAINER LEAKS AS ANY LEAKS WOULD BE FROM THE CONTAINER TO THE ATMOSPHERE. THE PROPOSED SAMPLE COLLECTION METHOD WILL BE CONSISTANT WITH P90 LEVEL B.

## APPLICABLE DOCUMENT:

FIELD SECTION 5.2  
FINAL SITE INVESTIGATION/SAMPLING PLAN, A 161ST AIR REFUELING GROUP, AZ, AIR NATIONAL GUARD,  
SKY HARBOR INTERNATIONAL AIRPORT, PHOENIX, AZ, SEPTEMBER 1990.

CC: J. S. Tomlin (MME)

REQUESTED BY

*[Signature]*

DATE 11-29-90

APPROVED BY

*[Signature]*  
Project Manager

DATE 11/29/90

*[Signature]*  
Quality Assurance Officer

DATE 30 NOV 90

*[Signature]*  
HARDWARE PROJECT MANAGER

DATE 1/21/91





# VARIANCE FORM

VARIANCE NO. 3

PROJECT NO. 409721 PAGE 1 OF 1

PROJECT NAME SKY HARBOR AND CASE SITE DATE 12/11/90

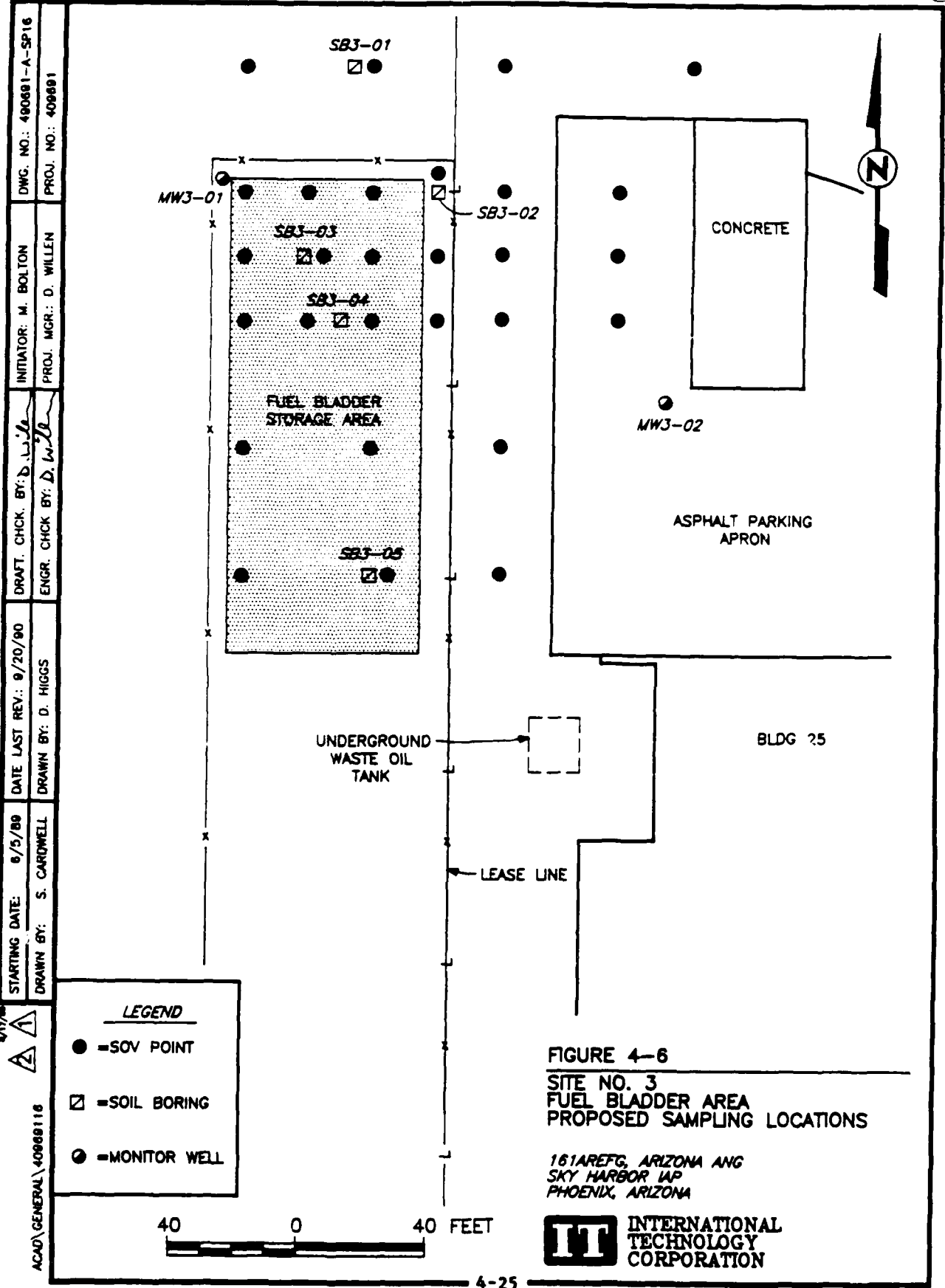
### VARIANCE (INCLUDE JUSTIFICATION)

TIRE FIELD SAMPLING PLAN WAS PREPARED UTILIZING "EXISTING" BLUE LINE DRAWINGS FROM TIRE BASE. IN PARTICULAR, SITE 3 WAS A FUEL STORAGE AREA BELIEVED TO HAVE BEEN WITHIN A CYCLONE FENCED AREA (ATTACHMENT 1). RECENT UTILITY CLEARANCE ACTIVITIES DISCLOSED A 1972 MAP SHOWING THE FUEL STORAGE AREA ABOUT 150 FT. WEST OF LEASE LINE. THE PURPOSE OF THIS VARIANCE IS TO REQUEST MODIFICATION OF SAMPLING AREAS TO THOSE SHOWN ON ATTACHMENT 2. NO SCOPE CHANGE IS ENVISIONED. THE SAME SAMPLING POINTS OCCUR BUT IN SLIGHTLY DIFFERENT LOCATION TO ADEQUATELY CHARACTERIZE THE SITE.

### APPLICABLE DOCUMENT:

FINAL FIELD SAMPLING PLAN, ~~APP~~ SECTION 4.6, SITE 3, FUEL BLADDER STORAGE AREA; A-B A.R. NATIONAL GUARD, SKY HARBOR INTERNATIONAL

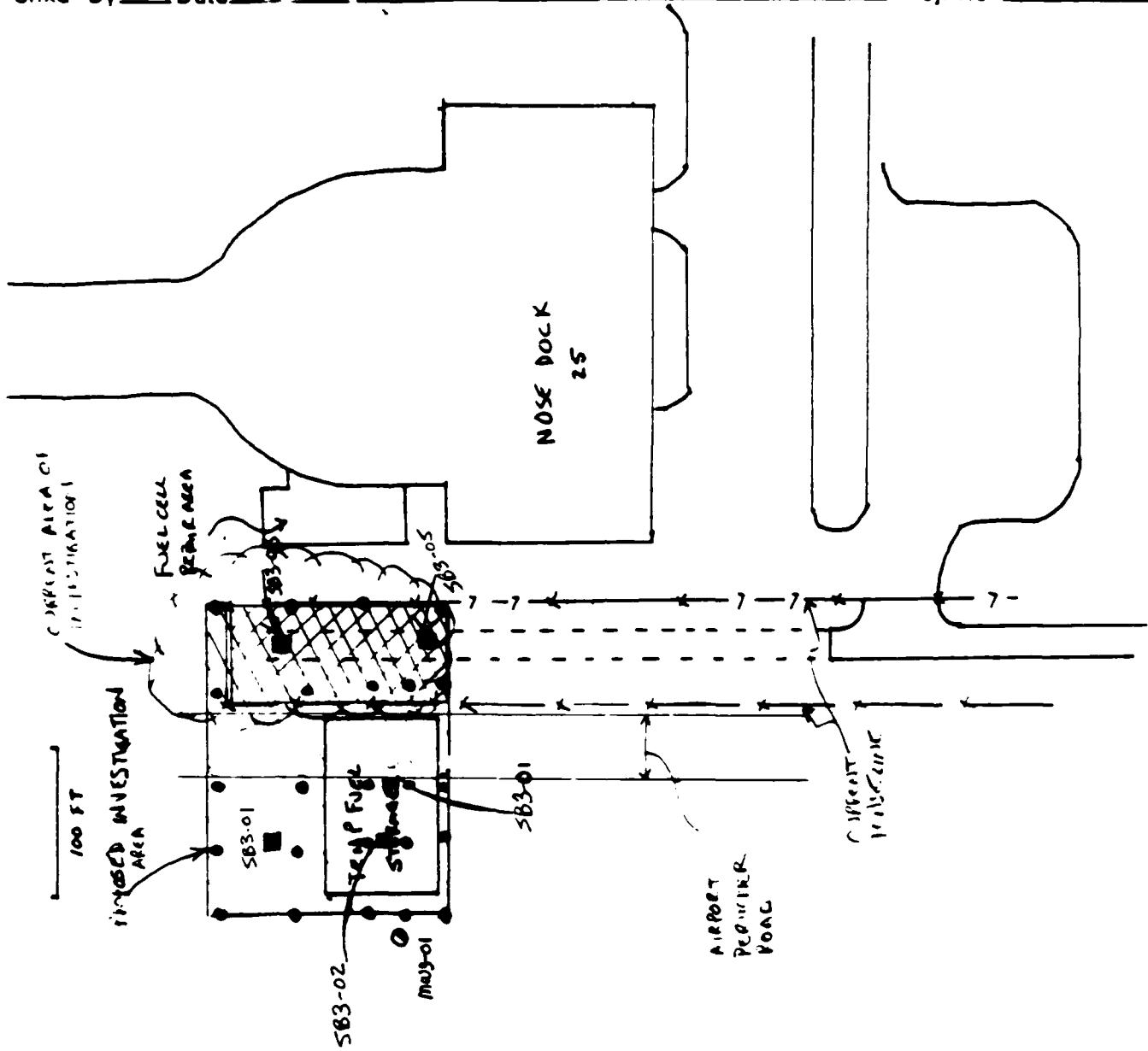
CC: David Bunn <sup>EB</sup>	REQUESTED BY <u>D. Wilson</u>	DATE <u>12/11/90</u>
HAZWRAP Files-0449	APPROVED BY <u>D. Wilson</u>	DATE <u>12/11/90</u>
	Project Manager	
	<u>John W. Meek</u>	DATE <u>11/26/90</u>
	Quality Assurance Officer	
	<u>John W. Meek</u>	DATE <u>4/15/91</u>



STARTING DATE: 6/5/89	DATE LAST REV.: 9/20/90	DRAFT. CHCK. BY: D. W. J.	INITIATOR: M. BOLTON	DWG. NO.: 490881-A-SP16
DRAWN BY: S. CARDWELL	DRAWN BY: D. HIGGS	ENGR. CHCK BY: D. W. J.	PROJ. MGR.: D. WILLEN	PROJ. NO.: 408891

ACAD\GENERAL\40888116

By SWS Date 11 DEC 90 Subject SKETCH MAP OF AREA AROUND Sheet No 1 of       
Chkd By      Date      SITE NO 3 ADAPTED FROM BASE ENG. DRAWING Proj. No 409321





### VARIANCE LOG

PROJECT NO. 409721 PAGE 1 OF 2  
PROJECT NAME AIR NATIONAL GUARD SKY HARBOR DATE: 12/11/90

VARIANCE (INCLUDE JUSTIFICATION)

**PURPOSE:**

The purpose of this variance is to document a change in the analytical procedure and equipment for on-site field screening analysis of soil boring samples at Sky Harbor National Guard. This change does not affect the target compounds or the intended use of the resulting data, but allows a more accurate qualification and quantification of the target compounds.

**CHANGE:**

Originally as stated in the SAP, a Photovac 10S50 portable gas chromatograph (GC) using headspace technique was to be used to determine relative concentrations of the target compounds.

The change will be to replace the 10S50 GC with a SRI model 8610 GC equipped with an PID and FID detector in series, purge and trap, and Peaksimple data system. The onboard integrator of the 10S50 will be replaced with a laptop computer and printer.

APPLICABLE DOCUMENT:

*FIELD SAMPLING PLAN, SECTION 5.2, SOV SURVEY / FIELD SCREENING*

CC: *B. Stanley (MMES)*

REQUESTED BY *[Signature]* DATE: 12/14/90

APPROVED BY *[Signature]* DATE: 12/12/90

*[Signature]* DATE: 12 DEC 90  
Quality Assurance Officer

*[Signature]* DATE: 1/21/91

HAZWOPER Project Mgr.



### VARIANCE LOG

PROJECT NO. 409721 PAGE 2 OF 3  
PROJECT NAME AIR NATIONAL GUARD SKY HARBOR DATE: 12/11/90

VARIANCE (INCLUDE JUSTIFICATION)

**JUSTIFICATION:**

1. The headspace procedure is an indirect method for determining the concentration of compounds. The use of the SRI with the purge and trap allows direct measurement of the compounds. Because of the direct measurement:
  - lower detection limits are obtainable
  - there will be less variability of measurement therefore the data will be more accurate
  - less sample prep equipment is required causing a reduction in cost, time, and potential biasing and errors
  - more accurate simulation of standard laboratory procedures
  
2. Because the SRI utilizes the FID and PID in series it is easier to more accurately identify and quantify the target compounds in a complex chromatograph by comparing the results of the two detectors. The 10S50 only utilizes the PID thus relying more on the operators interpretation.

APPLICABLE DOCUMENT:

CC:

REQUESTED BY: [Signature] DATE: 12/12/90

APPROVED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Project Manager

Quality Assurance Officer

DATE: \_\_\_\_\_

DATE: \_\_\_\_\_



# VARIANCE LOG

PROJECT NO. 409721 PAGE 3 OF 3  
PROJECT NAME AIR NATIONAL GUARD SKY HARBOR DATE: 12/11/90

## VARIANCE (INCLUDE JUSTIFICATION)

### JUSTIFICATION (continued):

3. The interfacing and utilization of a laptop computer by the SRI allows chromatographic data to be stored on floppy disk in a format that permits the data to be easily stored and recalled at any future time for reexamination, integration and manipulation. The 10S50 does not allow this without the addition of extra peripheral support.
4. The higher level of technology in the SRI allows the operator to easily and more accurately control the GC operational parameters thus allowing for more accurate qualification and quantification of the target compounds

## APPLICABLE DOCUMENT:

CC:

REQUESTED BY: *Dave Eay* DATE: 12/11/90

APPROVED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Project Manager

Quality Assurance Officer

DATE: \_\_\_\_\_

DATE: \_\_\_\_\_



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# VARIANCE FORM

VARIANCE NO. 5

PROJECT NO. 409721.02.06 PAGE 1 OF 3

PROJECT NAME SKY HARBOR ANG-SI DATE 11 JAN 91

**VARIANCE (INCLUDE JUSTIFICATION)** CHANGE IN PIEZO/WELL SAND PACK.

Drillers requested substitution of silica sand specification for piezometers and monitoring well sand pack from 30-60-40 mesh (current work plan) to 20/40 mix. 30-40 mesh sand is not a readily available product and obtaining special mix will cause delay and added expense. 20/40 mesh is similar gradation and is commonly used with screen size to be used (0.010 in slot).

The 20/40 Sand is suitable for use with 0.010 slot screen and should not cause data quality to be effected. The 20/40 sand with the 0.010 screen size is recommended in HAZWRAP position paper T4, pg. 12.

**APPLICABLE DOCUMENT:**

Final Site Investigation Field Sampling Plan, 161st Air Refueling Group, Az Air National Guard, Sky Harbor International Airport, Phoenix Arizona, Sept. 1990, Section 5.5.3.1, Pg 5-20

CC: WILLEN  
DYBURSKI  
D. MACK  
B. Standley (MMES)

REQUESTED BY [Signature]

DATE 11 JAN 91

APPROVED BY [Signature]  
Project Manager

DATE 1/16/91

[Signature]  
Quality Assurance Officer

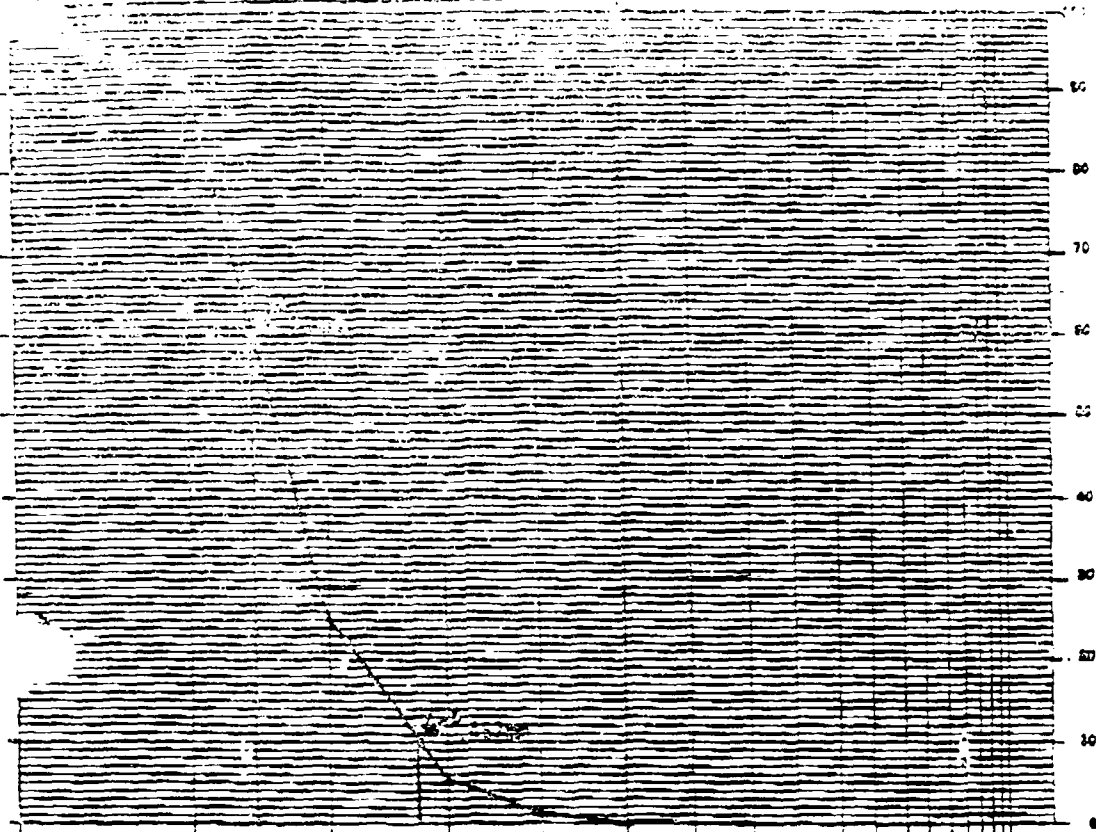
DATE 11 JAN 91

[Signature]

DATE 1/18/91

Form 100 of Two Series for Close Sizing

Cumulative Direct Diagram of Particle Analysis on Sample of \_\_\_\_\_  
 Effective Size  $\mu_{50}$  = 1.55 Date \_\_\_\_\_

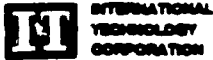


16 20 30 40 50 60 70 80 90 100  
 1.12 1.41 1.75 2.24 2.82 3.55 4.45 5.62 7.07 8.81 11.0

Screens		Tyler No.	U. S. No.	Sample Weights	Per Cent	Per Cent Cumulative Weights	Sample Weights	Per Cent	Per Cent Cumulative Weights	Sample Weights	Per Cent	Per Cent Cumulative Weights
Inches	Milli- meters											
			16			100						
			20		93.2							
			30		75.2							
			40		5.2							
			60		1.2							
			100		0							







# VARIANCE FORM

VARIANCE NO. 6

PROJECT NO. 409721.02.06 PAGE 1 OF 7

PROJECT NAME SKY HARBOR ANG. BASE SI DATE 11 Jan 91

## VARIANCE (INCLUDE JUSTIFICATION) CHANGE IN SOIL CLASS. & SAMPLING FORMS

Substitute the following field description forms for forms described in work Plans. The "new" forms are specified in HAZWOP Guidance documents as preferred to maintain program consistency. The replacement forms contain the same or more information as the work plan forms.

Current WP Form      Replacement

- |                                             |                                                                                                                                  |
|---------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------|
| ① Visual Classification of Soils<br>Fig 5-3 | Boring Log - Rev Date May 1990 (Figure 5-3a)                                                                                     |
| ② No Form                                   | Monitoring Well Construction Log - Rev Date May 1990 - Standard and Flush Work. Fig. 5-4a & 5-4b                                 |
| ③ No Form                                   | Monitoring Well Development Log - Rev Date May 1990, Including Post Development Water Level Recovery Graph (Figures 5-4c & 5-4d) |
| ④ Sampling Information Form<br>Fig 5-6      | Monitoring Well Purging Log - Rev Date May 1990 (Fig. 5-6a)<br>Monitoring Well Sampling Log - Rev Date May 1990 (Fig. 5-6b)      |

THE FSP IS MODIFIED AS FOLLOWS: PG. 5-17, SECT. 5.5.2, 2ND SENTENCE IS MODIFIED TO READ, "THE INFORMATION RECORDED ON THE BORING LOG FORM (FIGURE 5-3a) WILL ALSO INCLUDE ----"; PG. 5-24, SECT. 5.5.3.2, LAST SENTENCE, REPLACE REFERENCE TO "FIGURE 5-4" WITH "FIGURES 5-4a AND 5-4b"; PG. 5-25, SECT. 5.5.4, LAST PARA., 2ND SENTENCE, IS MODIFIED AS FOLLOWS: "FIELD TURBIDITY AND OTHER DEVELOPMENT RESULTS WILL BE REPORTED ON FIGURES 5-4c AND 5-4d FOR EACH WRM." PG. 5-30, SECT. 5.7.4.2, LAST SENTENCE, IS MODIFIED BY REPLACING, "FIGURE 5-6" WITH "FIGURES 5-6a AND 5-6b."

### APPLICABLE DOCUMENT:

Final Site Investigation Field Sampling Plan, 161st Air Refueling Group, AZ Air National Guard, Sky Harbor International Airport, Phoenix, AZ, Sept 1990, Section 5.5.3.2, 5.7.4.2, 5.5.2

CC: WILLIAM TYBURSKI  
D. MACK  
B. Stanley (MMES)

REQUESTED BY [Signature]

DATE 11 Jan 91

APPROVED BY [Signature]

DATE 1/11/91

[Signature]  
Project Manager

DATE 4 JAN 91

[Signature]  
Quality Assurance Officer

DATE 1/18/91

FIGURE S-3a

BORING LOGS	BORING WELL NO.		
DATA BISON <b>Sky Harbor</b>	<b>Coordinates:</b>		Site
Project No.	Client/Project:		
HAZWRAP Contractor	Drill Contractor	Driller	
Drill Started	_____ m'	Drill Ended	_____ m' End of data
Drill Method/Rig Type			
Logged by	E-Log ( Y / N ) From _____ to _____		Protection Level

Depth (m)  
 Sample No.  
 Sample No.  
 Recovery (%)

USCS  
 Blows 16 inch  
 Graphic Log  
 Well Logs  
 Water Levels  
 Remarks  
 E. ex

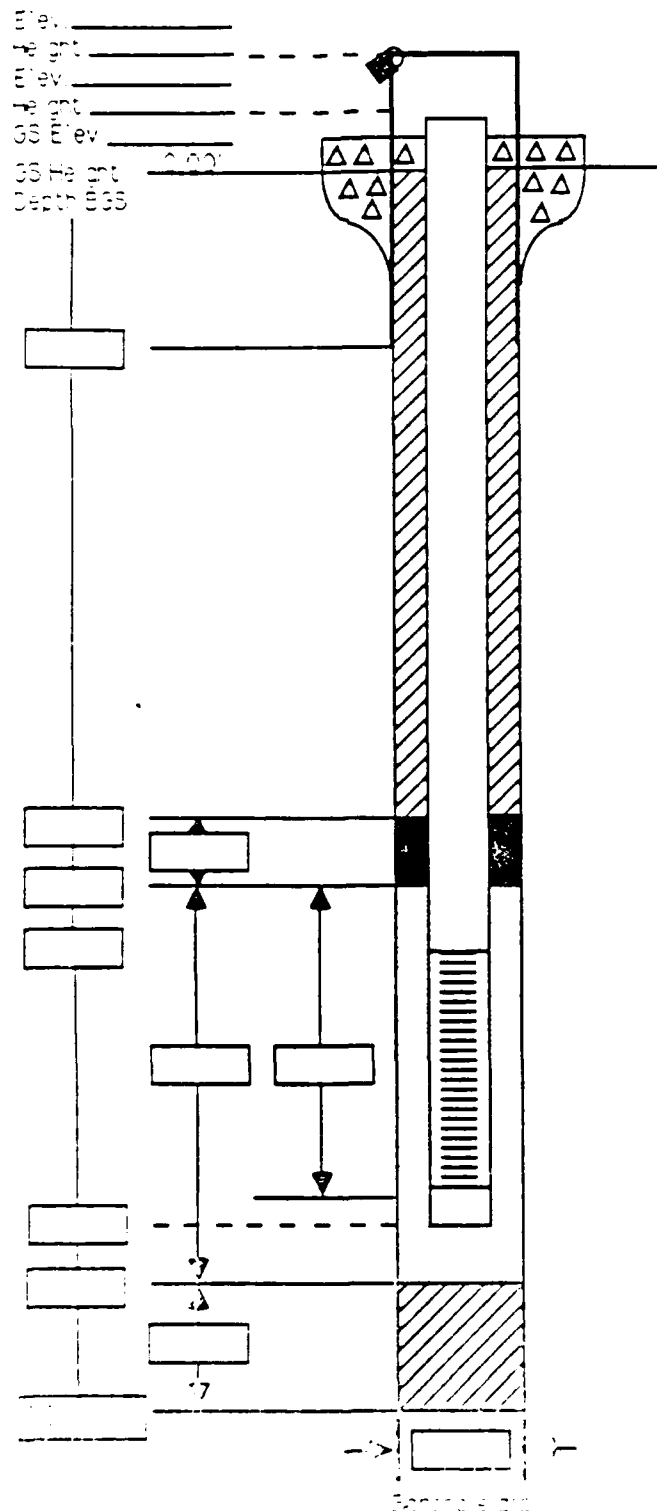
Lithologic Description


Use this Well Tube	Risk Coring _____	Field G/C (Make/Model) _____
Use this Log Label	Or Other _____	G/C Open _____
Drill Core	Notes	

FIGURE 5-4a

REV. DATE MAY 1997

MONITORING WELL CONSTRUCTION LOG -- Standard		
WELL NO. _____	Installation: <b>Sky Harbor</b>	Coordinates: _____
Project No. _____	Client/Project: _____	
HAZWRAP Contractor: _____	Drill Contractor: _____	
Comp. Start: _____ ( _____ m)	Comp. End: _____ m	
Built By: _____	Well Coord.: _____	



PROTECTIVE CSG  
 Material / Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_ Weep Hole (Y / N) \_\_\_\_\_

GUARD POSTS (Y / N) \_\_\_\_\_  
 No. \_\_\_\_\_ Type \_\_\_\_\_

SURFACE PAD  
 Composition & Size \_\_\_\_\_

RISER PIPE  
 Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Total Length (TOC to TOS) \_\_\_\_\_  
 Ventilated Cap (Y / N) \_\_\_\_\_

GROUT  
 Composition & Proportions \_\_\_\_\_  
 Tremied (Y / N) \_\_\_\_\_  
 Interval BGS \_\_\_\_\_

CENTRALIZERS (Y / N) \_\_\_\_\_  
 Depth(s) \_\_\_\_\_

SEAL  
 Type \_\_\_\_\_  
 Source \_\_\_\_\_  
 Setup/Hydratation time \_\_\_\_\_ Vol. Fluid Added \_\_\_\_\_  
 Tremied (Y / N) \_\_\_\_\_

FILTER PACK  
 Type \_\_\_\_\_  
 Amt. Used \_\_\_\_\_  
 Tremied (Y / N) \_\_\_\_\_  
 Source \_\_\_\_\_  
 Gr. Size Dist. \_\_\_\_\_

SCREEN  
 Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Slot Size & Type \_\_\_\_\_  
 Interval BGS \_\_\_\_\_

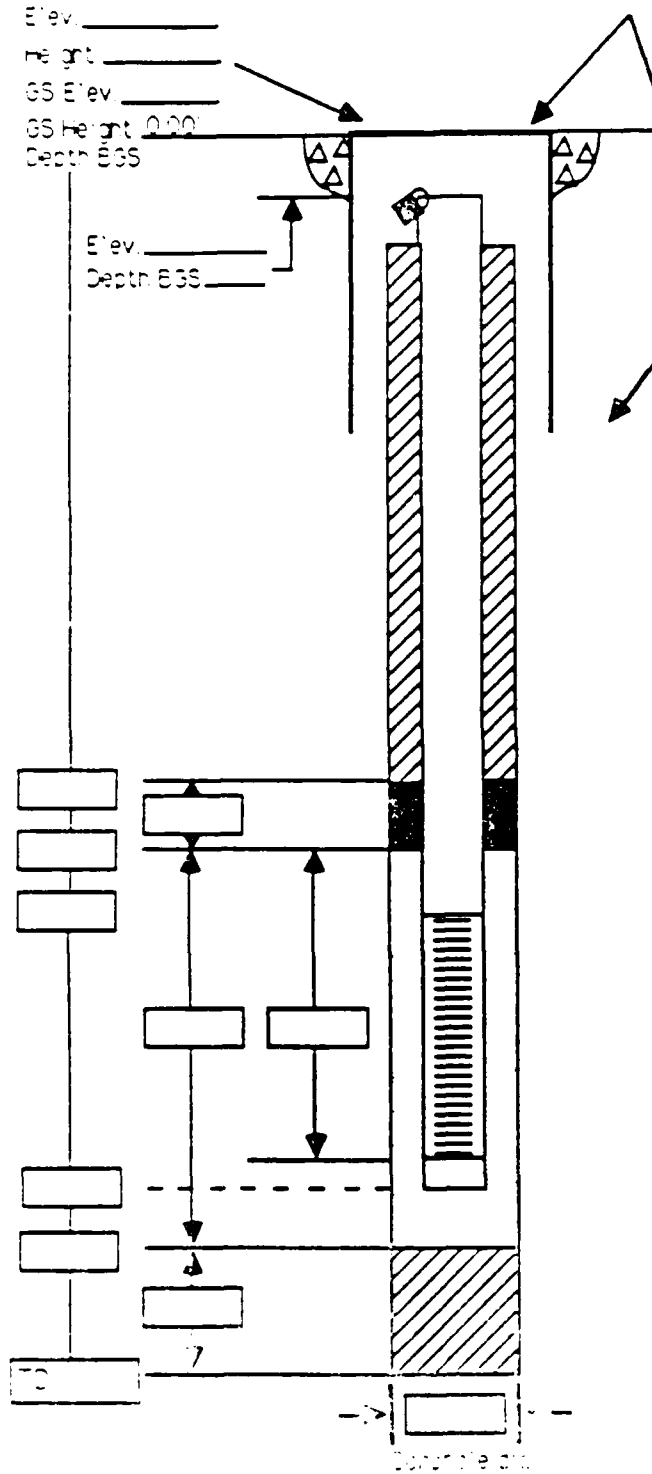
SUMP (Y / N) \_\_\_\_\_  
 Interval BGS \_\_\_\_\_ Length \_\_\_\_\_  
 Bottom Cap (Y / N) \_\_\_\_\_

BACKFILL PLUG  
 Material \_\_\_\_\_  
 Setup/Hydratation time \_\_\_\_\_  
 Tremied (Y / N) \_\_\_\_\_

FIGURE 5-4b

REV DATE MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO:	Installation: <b>Sky Harbor</b>	Coordinates:
Project No:	Client/Project:	
HADWRAP Contractor:	Drill Contractor:	
Comp. Start: ( _____ )	Comp. End: ( _____ )	
Built By:	Well Coord.:	



**PROTECTIVE CSG**  
 Material / Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_  
 Watertight O-Ring (Y/N) \_\_\_\_\_

**SURFACE PAD**  
 Composition & Size \_\_\_\_\_  
 Breathes With Vadose Zone (Y/N) \_\_\_\_\_

**RISER PIPE**  
 Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Total Length (TOC to TOS) \_\_\_\_\_  
 Ventilated Cap (Y/N) \_\_\_\_\_

**GROUT**  
 Composition & Proportions \_\_\_\_\_  
 Tremied (Y/N) \_\_\_\_\_  
 Interval BGS \_\_\_\_\_

**CENTRALIZERS (Y/N)**  
 Depth(s) \_\_\_\_\_

**SEAL**  
 Type \_\_\_\_\_  
 Source \_\_\_\_\_  
 Setup/Hydration time \_\_\_\_\_ Vol. Fluid Added \_\_\_\_\_  
 Tremied (Y/N) \_\_\_\_\_

**FILTER PACK**  
 Type \_\_\_\_\_  
 Amt. Used \_\_\_\_\_  
 Tremied (Y/N) \_\_\_\_\_  
 Source \_\_\_\_\_  
 Gr. Size Dist. \_\_\_\_\_

**SCREEN**  
 Type \_\_\_\_\_  
 Diameter \_\_\_\_\_  
 Slot Size & Type \_\_\_\_\_  
 Interval BGS \_\_\_\_\_

**SUMP (Y/N)**  
 Interval BGS \_\_\_\_\_ Length \_\_\_\_\_  
 Bottom Cap (Y/N) \_\_\_\_\_

**BACKFILL PLUG**  
 Material \_\_\_\_\_  
 Setup/Hydration time \_\_\_\_\_  
 Tremied (Y/N) \_\_\_\_\_



POST DEVELOPMENT WATER LEVEL RECOVERY GRAPH

REV DATE MAY 1999

Well Recording Instrument

Start Recovery ( ) ( m) End Recovery ( ) ( m) Total Recovery Time

Beginning WL Final SWL Project Name No.

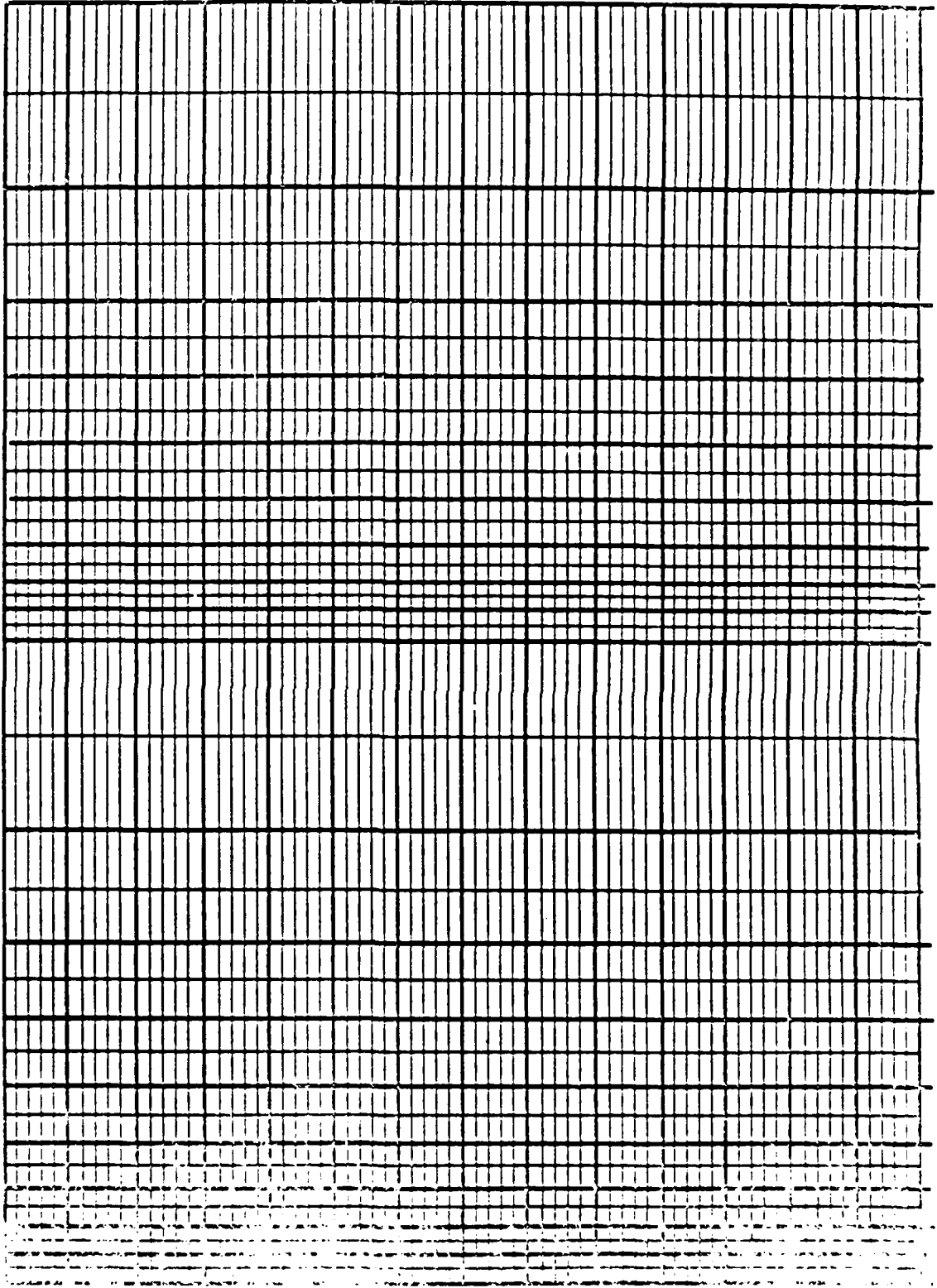


FIGURE 5-42

BRAND

MONITORING WELL PURGING LOG		Sample ID No
Installation Sky Harbor Coordinates		WELL NO
HADRAP Contractor		Project No
Purge Start (Date)	(Time)	Purge End (Date) (Time)
Purged by		

Depth Measurement Ref. Point\* \_\_\_\_\_ Well Csg ID 2" 4" 6" Other \_\_\_\_\_  
 Well Haspace/Odor \_\_\_\_\_ LNAPL Check (Y/N) DNAPL Check (Y/N)  
 Equipment Used To Measure Thickness and Sample Free Product (Make, Model, etc) \_\_\_\_\_

Depth to Top and Bottom of Screen Interval \_\_\_\_\_  
 Depth to LNAPL \_\_\_\_\_ Depth to DNPL \_\_\_\_\_ Orig DTW \_\_\_\_\_ Final DTW \_\_\_\_\_  
 LNAPL/DNAPL Thickness \_\_\_\_\_ LNAPL/DNAPL Sample and Volume \_\_\_\_\_  
 Measured Well TD \_\_\_\_\_  
 (H) Orig DTW \_\_\_\_\_

	2" - 0.16					
(H) Wtr Col. Thick. (x)	4" - 0.65	Gals/ft (=)	Gals/Csg Vol. (x)	Csg Vol' (=)	Total	
	6" - 1.47				Purge	
					Gas	

Purge Method  
 Submersible Pump  Dedicated Bladder Pump  Bladder Pump  Baller   SS   
 Centrifugal Pump   Tef   
 PVC   
 Peristaltic Pump  Hand Pump  Gas Lift/ Displacement Pump  Other \_\_\_\_\_  
 Purging Equipment (Make, Model, etc.) \_\_\_\_\_ Purge Equipment Decont? (Y/N)

Purge Wtr Containerized? (Y/N) Avge Purge Rate \_\_\_\_\_ gpm  
 weather \_\_\_\_\_ ( °F)

Actual Time	Elapsed Time	Vol. Purged (Gals)	Depth To Wtr (ft)	Depth Of Pump Intake (ft)	Temp (°C)	pH (s.a)	Cond. (µmhos/m)	Turbidity (NTa)	Other	Comment

Depth of first discharge point \_\_\_\_\_ Distance To Top of Casing TCC \_\_\_\_\_  
 DNAPL Sample and Volume \_\_\_\_\_



FIGURE 5-6 b

MONITORING WELL SAMPLING LOG		Sample D No
Installation: <b>Sky Harbor</b> Coordinates		WELL NO
HAZWRAP Contractor:		Site
Sample Start (Date)	(Time)	Sample End (Date)
Sampled by		Project No

Orig. SWL \_\_\_\_\_ ft. BTOC\* Final SWL \_\_\_\_\_ ft. BTOC  
 Screen Interval: \_\_\_\_\_ - \_\_\_\_\_ ft. BTOC

Temp	pH	Cond	Turbidity

Are parameters 20%  
of purge values? Y / N

Repurge Y / N

No. repurge volumes \_\_\_\_\_

Sampling Method

Submersible Pump  Dedicated Bladder Pump  Bladder Pump  Bailor  SS   
 Tef  Centrifugal Pump   
 PVC

Peristaltic Pump  Hand Pump  Gas Lift/ Displacement Pump  Other \_\_\_\_\_

Sampling Equipment (Make, Model, etc.) \_\_\_\_\_

Sample Equipment Decont'd? Y / N

If pump or discrete bailer, Depth(s) where pump set: \_\_\_\_\_ ft. BTOC

weather \_\_\_\_\_ ( °F)

Lab Analyses (Circle)

VOA      SVOA      METALS      PEST/PCBS      TPH      CATIONS      ANIONS      TDS

Others \_\_\_\_\_

Metals (Circle) Filtered      Unfiltered      Both

Field Dups.      Y / N      Referee Dups      Y / N

Comments

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

BTOC is Below Top of Casing (for other measurement reference point)  
 SWL is Static Water Level

Figure 6-1

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# VARIANCE FORM

VARIANCE NO. 7

PROJECT NO. 409721 PAGE 1 OF     

PROJECT NAME SKY HARBOR AND BASE SI DATE 16 Jan 91

**VARIANCE (INCLUDE JUSTIFICATION) SAMPLE COLLECTION/SHIPMENT**

Section 6.2 of the Field Sampling Plan specifies that samples will be packaged and shipped... within 24 hours of collection, and coolers containing samples will be shipped by next-day delivery service. Field work for the SI is on a 4 day off-10 day on schedule for cost efficiency. ~~So~~ Because of the schedule ~~it~~ samples will be collected on Saturday and Sunday, periodically. ~~Given~~ <sup>S/S</sup> Samples collected on Sunday cannot be shipped overnight because delivery services typically do not work on Sunday. This variance allows for samples collected on Sunday to be shipped on Monday for Tuesday delivery at the laboratory.

Samples collected on Saturday could be shipped for Monday delivery; however this would require them to sit in a warehouse on Sunday. This variance allows for soil samples collected on Saturday to be shipped ~~for~~ <sup>sub</sup> Monday for Tuesday delivery. Using this schedule a sample collected Saturday would be 3 days old upon arrival at the laboratory. The shortest soil-holding time for analytes to be tested is 14 days. This variance allows the lab 11 days to meet holding time.

Water samples will not be collected on weekends, with the exception of rinseate blanks. Rinseate blanks which must be collected on weekends will be specially scheduled with the laboratory to meet holding times.

**APPLICABLE DOCUMENT:**

Final Field Sampling Plan, 161st Air Refueling Group, Arizona Air National Guard, Sky Harbor International Airport, Phoenix, AZ. SECTION 6.2 (PS 6-1)

CC: D. MACK

J. TYBURSKI

P. Gunn (HAZWAP)

HAZWAP Files-0449

REQUESTED BY [Signature]

DATE 1-6-91

APPROVED BY [Signature]

DATE 1/16/91

Project Manager

[Signature]  
 Quality Assurance Officer

DATE 1/21/91

[Signature]

DATE 4/16/91



# VARIANCE FORM

VARIANCE NO. 8PROJECT NO. 409721 PAGE 1 OF 1PROJECT NAME Sky Harbor AUG DATE 1/16/91VARIANCE (INCLUDE JUSTIFICATION) CHANGE IN ANALYTE TESTS

The current CLP Statement of Work covers the Target Compound List (TCL) which replaces the Hazardous Substance List (HSL) as in older Statements of Work. Four (4) organic compounds which were on the HSL are not on the TCL

(Volatiles: 2-chloroethyl vinyl ether;  
Semivolatiles: N-nitrosodimethylamine, aniline, benzidine)

ITAS/Cerritos requests a variance to the Sky Harbor OAPP to omit these compounds from the analytical testing program (Table 9-3: Analyte # 26, # 36, # 38, # 39C)

APPLICABLE DOCUMENT: field Sampling Plan - Appendix A (OAPP) TABLE 9-3

CC: C. FERGUSON~~S. BARRIS~~J. DYBURSKID. MACKD. BURN HAZWRAPHAZWRAP Files -0449REQUESTED BY Cheryl Ingham/ITAS DATE 1/16/91APPROVED BY [Signature] DATE 4/17/91

Project Manager

[Signature]  
Quality Assurance OfficerDATE 17 JAN 91DATE 4/8/91

# VARIANCE FORM

VARIANCE NO. 9

PROJECT NO. 402721 PAGE 1 OF 1

PROJECT NAME SKY HARBOR ANG BASE SI DATE 22 JAN 91

**VARIANCE (INCLUDE JUSTIFICATION) SITE 4, DELETION OF SOIL BORING SAMPLES**

The Field Sampling Plan (FSP) Section 4.7.2 specifies that a minimum of 2 soil borings are to be completed at Site 4. Section 4.7.6 specifies that the borings will be 20-45 feet deep, depending on the depth to water. Soil samples are to be collected at 5-foot-depth intervals and three from each boring are to be submitted for laboratory analysis.

During the initial hydrogeologic characterization, the hammer rig penetration rate was approximately 1 ft per hour. The soil materials are ~~fine~~ sand, gravel, weathered breccia to approximately 10' below this is caliche and volcanic bedrock. The conditions will not allow collection of split spoon samples due to penetration difficulties.

In lieu of installing soil borings this variance will allow collection of surficial soil samples to assess soil contamination from site 4. Six samples will be collected, 3 at the current drum storage area, 2 at the PA-drum storage area, and one background sample located east of PB-01. Samples will be collected from the ground surface, below any gravel cover, using a slide hammer with brass sample rings. If no sample recovery is obtained after three attempts, samples may be collected with a stainless-steel trowel and placed in a 250 ml glass jar and 2-40 ml vial vials.

Samples are also to be collected from monitoring well boreholes, as specified in section 4.7.7. Due to adverse subsurface conditions ~~soils~~ (e.g. bedrock) soil samples will not be able to be installed ~~and~~ collected from monitoring wells at Papego.

**APPLICABLE DOCUMENT:**

Final Site Investigation Field Sampling Plan, 161st Air Refueling Group, Sky Harbor Air National Guard, Sky Harbor International Airport, Phoenix Arizona, Sept. 1990. Sections 4.7.2, 4.7.6, 4.7.7.

CC: David Bunn  
HAZWRAP Files -0449

REQUESTED BY [Signature]

DATE 24 Jan 91

APPROVED BY [Signature]

DATE 1/24/91

Project Manager

[Signature]  
Quality Assurance Officer

DATE 24 JAN 91

DATE 4/15/91

[Handwritten initials]

RECEIVED

FEB 10 3 00 PM '91 Figure 6-1

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# VARIANCE FORM

VARIANCE NO. 10

PROJECT NO. 409721 PAGE 1 OF 2

PROJECT NAME SKY HARBOR ANAB SI DATE 13 Feb 91

## VARIANCE (INCLUDE JUSTIFICATION)

GROUNDWATER SAMPLING PURGE PROCEDURE (FSP Sec 5, 3.4.1)

The calculated purge volume for monitoring wells at the Sky Harbor site is approximately 145 gallons (3 well volumes) assuming 90% porosity in the casing - borehole annulus.

The sampling plan specifies the wells will be purged using bailers or bladder pumps. Using a 3 inch diameter - 3 foot long bailer will require ~130 trips to purge a well, using a bladder pump against 100' head requires a 2-stage pump to achieve flow rates greater than 1 gallon per minute (GPM). Such pumping systems are over \$2000 cost. This variance is to allow use of a piston-pump (expensive) to purge wells at Sky Harbor sites. The piston pump will produce flow rates of ~1.5 GPM and allow wells to be purged in 1 1/2 - 2 hrs. This is viewed as preferable to bailer purge which is likely to agitate water in the more costly bladder - 2 stage pump.

After completion of purging, wells will be sampled using Teflon bailers in accordance to the sampling plan. <sup>and through SOP # 57 SEC ATTACHED</sup> All down-hole wetted equipment will be decontaminated before and after introduction to a well in accordance with the sampling plan.

Wells at the Papago Military Reservation are likely to be "low yielding wells."

**APPLICABLE DOCUMENT:**  
 Final SI Field Sampling Plan, 161st Air Refueling Group, Arizona ANG, Sky Harbor International Airport, Phoenix, Arizona - September 1990.

CC: J. Bunn (HAZWRAP) REQUESTED BY [Signature] DATE 13 Feb 91  
 HAZWRAP Files-0449 APPROVED BY [Signature] DATE 2/13/91  
[Signature] Project Manager  
[Signature] Quality Assurance Officer DATE 14 FEB 91  
[Signature] DATE 2/20/91  
 HAZWRAP PROJECT MGR.

Figure 6-1

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# VARIANCE FORM

VARIANCE NO. 10

PROJECT NO. 40972 PAGE 2 OF 2

PROJECT NAME SKY HARBOR ANGB SI DATE 13 FEB 91

**VARIANCE (INCLUDE JUSTIFICATION)**

*Such wells will be purged and sampled in accordance with the wrap position paper No. 2 "Development and Sampling of Long Recharge Wells" (SEE ATTACHED)*

*No Purging or Sampling of Wells will be fully documented in the Sampling Log. Purging will be accomplished using a pump down of 0.5 gpm or less. After one hour or more has been purged, samples will be collected as soon as sufficient water returns to the well to collect a sample. A bailer will be used to collect samples.*

**APPLICABLE DOCUMENT:**

CC: REQUESTED BY \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY \_\_\_\_\_ DATE \_\_\_\_\_

Project Manager

Quality Assurance Officer \_\_\_\_\_ DATE \_\_\_\_\_

\_\_\_\_\_ DATE \_\_\_\_\_

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**HAZARDOUS WASTE REMEDIAL ACTIONS PROGRAM  
STANDARD OPERATING PROCEDURE 5  
GROUNDWATER SAMPLING WITH BAILERS**

**1. OBJECTIVE**

The purpose of this procedure is to define requirements for the collection of groundwater samples.

**2. BACKGROUND**

Methods used for the collection of groundwater samples include bailing and a variety of pumping techniques. Bailers are hollow cylinders with unidirectional (open up) check valves at the bottom end. Some bailers may also be closed or valved at the upper end. Bailers used in environmental applications are typically constructed of stainless steel, disposable nylon string, disposable monofilament polypropylene, Teflon-coated stainless steel wire, or Teflon, with stainless steel or Teflon being preferred. The bailer is lowered into the well on an acceptable line or coated wire line until submerged. The bailer is then retrieved to the surface for sample collection. This procedure describes groundwater sampling with bailers. For the best results, the sequence of sampling is from least to most contaminated wells. It is preferable for most sampling events using bailers to have dedicated bailers or enough bailers to last for 1 day's worth of sampling (normally 6 to 8/d).

**3. RESPONSIBILITIES**

**Site Manager:** The Site Manager is responsible for ensuring that field personnel are trained in the use of this procedure and for verifying that groundwater samples are collected in accordance with this procedure.

**Project Field Geologist:** The Project Field Geologist is responsible for complying with this procedure, including sample collection, packaging, and documentation.

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#### 4. REQUIRED EQUIPMENT

- For surface sample - bailer types.
- For specific depths - bailer types.
- Bottom-filling, bottom-emptying bailer (with bottom release, if needed) of the appropriate material.
- Clean rope or wire line of sufficient length for conditions.
- Appropriate sample containers with labels and preservatives, as required.
- Hard plastic or steel cooler with cold packs (or ice).
- Water-level meter and/or other water-level measuring device.
- Temperature, conductivity, pH, dissolved oxygen, and organic vapor meters, if required.
- Plastic sheeting.
- Decontamination supplies, as required
- Personnel protective clothing and equipment, if required by the site-specific health and safety plan.
- Latex or polyvinyl chloride (PVC) gloves.

#### 5. PROCEDURE

The following steps must be followed when sampling groundwater with bailers:

1. Put on protective clothing and equipment as specified in the site-specific health and safety plan.
2. Prepare the site for sample acquisition by covering the ground surface around the wellhead with plastic sheeting. Arrange the required sampling equipment for convenient use. If on-site decontamination is required, arrange the necessary supplies in a nearby but separate location, away from the wellhead.
3. Open the well and note the condition of the casing and cap. Check for vapors using vapor analyzing equipment. Using a water-level meter, determine the static water level and depth to well bottom. Record this information in the field logbook or on the water sampling form.
4. Purge the well according to Hazardous Waste Remedial Actions Program (HAZWRAP) Standard Operating Procedure (SOP) 4, if not already accomplished. Allow the water level to recover to a depth at least sufficient for the complete submergence of the bailer without contacting the well bottom.
5. While the well is recovering from purging, decontaminate the bailer. If the bailer was decontaminated before arrival at the site, remove the protective wrappings. Securely attach the bailer to the line. The end of the line should also be secured.



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6. Arrange the sample containers in the order of use. Volatile organic analyte (VOA) samples, if required, will be obtained first, followed in order by semivolatiles (SVOA) and other samples.
7. Lower the bailer into the well. Do not allow the bailer to touch the casing. The bailer should enter the water slowly to prevent aeration, particularly when VOA and SVOA samples are being collected. Do not permit the bailer to contact the well bottom.
8. Retrieve the filled bailer to the surface. Do not allow the line to contact the ground. Hang the bailer from a bailer stand or other support, if available, or have an assistant hold it off the ground. The first bailer of water should be used as a rinse and then discarded. Immediately obtain any required VOA and SVOA samples by using the release valve to gently transfer water to the sample bottle. The sample bottle should be tilted when filling to prevent aeration. Check the filled vial for bubbles. The first volume of sample should be used as a rinse and then discarded, unless the sample bottles contain preservative. If sample filtration is required, it should be done as soon as possible, or after sample retrieval. If, after collecting VOA and SVOA samples, the total required sample volume is greater than the water remaining in the bailer, decant the water into a clean compositing container. The compositing container must have adequate volume to contain the entire volume necessary for collection. Again lower the bailer to collect water for additional sample volume, if needed.
9. When the composited sample volume is sufficient, decant water into the remaining sample containers. Add preservative (if needed), cap, seal, and properly label all containers. Place the filled containers in the cooler(s) immediately.
10. Record sample types and amounts collected, and time and date of collection in the field logbook and on the groundwater sampling form per HAZWRAP SOP 1, Parts A and B, respectively. Prepare chain-of-custody and analytic request documents as required by the project quality assurance plan.
11. Decontaminate sampling equipment according to HAZWRAP SOP 14.
12. Clean up the area and place disposable materials (plastic sheeting, gloves, Tyvek) in the designated receptacle. Close and lock the well cover.

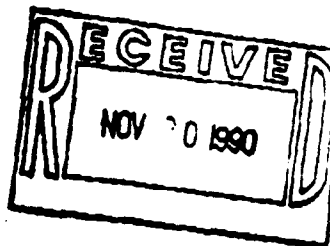
## 6. RESTRICTIONS/LIMITATIONS

Obtain on-site data such as temperature conductivity, pH, or dissolved oxygen measurements after samples have been collected. This may require additional time for well recovery.

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## 7. REFERENCES

- Driscoll, F. G., *Groundwater and Wells*, Second Edition, St. Paul, Minnesota, Johnson Division, 1986.
- U.S. Environmental Protection Agency, *A Compendium of Superfund Field Operations Methods*, EPA/540/P-87/001, 1987.
- U.S. Environmental Protection Agency, *Manual of Water Well Construction Practices*, EPA/570/9-75-001, 1975.



## POSITION PAPER NO. 2

## DEVELOPMENT AND SAMPLING OF LOW RECHARGE WELLS

Hydrogeology Support Group  
Hazardous Waste Remedial Actions Program\*  
Martin Marietta Energy Systems, Inc.  
Oak Ridge, Tennessee 37831-7106

## 1. INTRODUCTION

A low recharge well can be defined as a well that does not recover to 90% of its static water level within 6 to 8 h after being purged. There are many other definitions for low recharge formations; however, this is the one that the Hazardous Waste Remedial Actions Program (HAZWRAP) will use in its discussion of this issue. Low recharge formations can be found in most of the following environmental scenarios: fine-grained, unconsolidated material such as clay, silt, shale, or clay in the interstices of larger-grained material; or igneous and metamorphic rocks. Under the above conditions, four problem areas surface when it is the task of the hydrogeologist to obtain a representative sample of the groundwater from these types of aquifers. They are: how do you reduce siltation within the well, how do you develop a low recharge well, how do you purge a low recharge well, and when do you sample for volatile organics after purging a low recharge well?

In the following document, we will discuss these issues and present the most recent discussions with regard to these issues. It is the intent of this position paper to make the hydrogeologist aware of the problems associated with low recharge wells and to provide some guidance on the above issues. For the purpose of this position paper, only low recharge aquifers composed of fine-grained, unconsolidated materials will be discussed.

## 2. SILTATION AND DEVELOPMENT

## 2.1 STATEMENT OF THE PROBLEM

Siltation and development problems are usually relegated to unconsolidated sediment aquifers. These are generally not problems associated with slow recharge in consolidated sedimentary, igneous, or metamorphic environments. Both of these issues (i.e., siltation and development) will be

\*Operated by Martin Marietta Energy Systems, Inc., for the U.S. Department of Energy under contract DE-AC05-84OR21400.

discussed concurrently since, in general, they are related issues (i.e., siltation is largely a problem of ineffective development procedures and/or well construction techniques).

Siltation is the process whereby, during well construction and/or development, small-sized aquifer material (generally smaller than that retained on a #50 US standard sieve) can be found within the well casing, making the water sample turbid. It is of note that this same grain size range (i.e., less than #50 standard sieve size) makes up over 30% of the aquifer material, which is the principal reason why the formation is a slow recharger. This material ends up in the well casing usually by two methods. In the first, the fine-grained materials are introduced into the well casing directly during well installation. This usually occurs at the same time as the well screen, filter pack, and riser pipe are placed at the bottom of the borehole. From the time the borehole drilling is complete and the well is placed, groundwater will move up into the auger flights, carrying with it an associated amount of aquifer material due to hydrostatic pressure. The screen, casing, and filter pack are introduced directly into this "soup", thereby introducing the fine-grained material directly into the casing. Also during placement, the aquifer material may become integrated with the filter pack material during placement of the filter pack.

The second siltation problem area occurs during development. In monitoring well construction, the purpose of the design of the filter pack is to retain 95 to 100% of the aquifer material. In general, this is not always accomplished because all too often the well screen size and filter pack size are selected before the field investigation (i.e., during the work plan development stage). During this stage, when they suspect slow recharge aquifers, 10-slot screens with Ottawa #1, Morie #1, or equivalent filter pack material are selected in advance of actual field information. The development procedure, therefore, must clean out the residual materials in the well casing and must also pull the fine material out of the filter pack since it was placed and commingled with aquifer material during placement. Therefore, due to poor construction design, new aquifer fine-grained material is pulled into the casing during development because the filter pack material cannot retain 95 to 100% of the aquifer material.

This represents a synopsis of the siltation and development problems associated with monitoring well construction techniques. The following section will discuss some of the more recent published articles relevant to these issues.

**2.2 PUBLISHED APPROACHES TO SILTATION AND DEVELOPMENT**

**2.2.1 Well Construction Methods**

The key question to be answered in assessing well construction methods in low-yield aquifers is, "Can well-designed construction techniques improve the quality and quantity of groundwater samples from a low recharge aquifer?". In review of the literature, the following information is submitted for evaluation:

- o In a study conducted by Paul, Palmer, and Cherkauer (1988), a series of ten wells were placed in glacial tills. Of these wells some had been installed wet (the well was not cleaned out of excess loose material before well placement) because of delays in setting the screens, and some had been installed dry (the loose materials had been removed from the borehole). Of the wells installed wet, the wet wells exhibited 50 to 200 times greater turbidity than wells installed dry.
- o In an article in Groundwater Age (Wehrmann, 1983), a method that can be used in clayey environments, where an open borehole can be sustained, is to pump water down the inside of the monitoring well casing, out the screen, and up the annulus of the borehole. This should be done both before and after the gravel pack is emplaced to free fine-grained material from the surface of the borehole and the gravel pack materials. Circulation should be continued until the water coming up the annulus looks clear (Wehrmann, 1983).
- o According to Nielson (1988), the continuous-slot, wire-wound screen is more effective in preventing formation materials from becoming clogged in the openings. It allows particles slightly smaller than the openings to pass freely into the well without wedging in the opening, making these intakes nonclogging.
- o In an article by Gass (1989), drilling methods and well construction techniques must be adapted to minimize borehole damage before the installation of a well screen (commonly referred to as "skin effect") and a filter pack, or at least to correct borehole damage before installation of the well screen and filter pack. In addition, it must be understood that the effectiveness of well development is going to be extremely limited in alleviating this effect. To reduce this effect, he suggests several techniques: (1) boring the zone representing the screened interval with a 3- to 5-in. Shelby tube, (2) scratching the sides of the borehole with an oversized brush or wire to eliminate the smear effect, and/or (3) developing the low-recharge well with a bailer or small-diameter surge block to achieve gentle agitation of the filter pack so that any residual fine material that may have been incorporated into the filter pack during its emplacement can be removed.

### 2.2.2 Well Construction Materials

In assessing well construction materials, the following information is submitted for evaluation:

- o In an article by Gass (1988), Gass states that the filter pack should be graded, fine to medium sand. Because of the gradation, the effective size of the filter pack will be quite small and yet will still be orders of magnitude more permeable than the formation and will not restrict well yield. In almost all cases, a 10-slot screen will retain 80% to 90% of the filter pack.

- o In an article by Nielson (1988), the use of an artificial filter pack in a fine-grained material allows the screen slot size to be considerably larger than if the screen were placed in without the filter pack. This is particularly true where fine slot sizes, which are designed to hold out formation materials, are either impractical or not commercially available. The larger screen slot size afforded by the filter pack allows for the collection of adequate volume of sediment-free samples (Nielson, 1988).
- o Paul, et al. (1988), states that the function of the filter pack is to stabilize the borehole and to prevent formation materials from entering the well. They recommend that the proper size of filter pack and screen can be chosen from the grain size distribution curve of the formation by applying the method outlined by Driscoll (1986). In addition, he states that commonly available well screens and sand packs were not capable of filtering out clay-sized particles found in fine-grained glacial tills. The optimal well design would require a silt-sized sand pack and a very fine-meshed screen (<0.05 mm). In addition, the wells within his study were constructed of different types of screens (slotted and continuous). From this condition he observed in his glacial till study that surging of the wells that had standard factory slot screens pulled more formation material through the sand pack and into the screen than wells that had continuous-slot screens. There were no substantial differences in the turbidity measurements between the three types of well screens that had been bailed.

From the information collected, several issues were not discussed. One of these issues is the use of sumps in well construction in low-yield unconsolidated aquifers. It has been a standing practice during the past 5 years that sumps be used in well construction in low-yield aquifers. A sump is a piece of blank casing placed below the screen and is designed to retain and separate the siltation materials (accumulated fine-grained material settling out of suspension) from the screened interval. This device is used primarily to keep the entire surface area of the screened interval open to receive groundwater.

Another issue that has become a standard practice is to ensure an appropriate filter pack thickness. All too often, particularly in shallow groundwater wells (i.e., those less than 50 ft), a 2-in. well is placed in a nominal 4-in. borehole. It is generally agreed that the filter pack thickness should equal the well diameter and that it should be tremied into place. The reasoning behind this position is that an insufficiently large filter pack thickness will not retain the large volume of fine-grained material trying to enter the well screen and that a sufficient volume is needed to effectively retain or retard this condition.

In addition to the above, Johnson Screens has developed a new screen specifically designed for low-yield aquifers. This new well screen is called Channel Pack and is basically two continuously wrapped screens separated by a glass bead filter pack. This screen has not been extensively field tested, so its advantages and disadvantages have not been well established.

**2.2.3 Recommendations**

Based on the above information, the following construction methods and material specifications are recommended:

- o Filter pack thickness around the well screen should be at least the same thickness as the diameter of the casing/riser.
- o Sumps should be placed below the well screens to act as a sediment trap for all low-yield aquifer wells.
- o Well screens should be of the continuous slot variety.
- o Well screens, casing, and filter pack material should be placed in dry wells (i.e., the loose "soupy" material within the drill casing should be cleaned out or removed before materials placement).
- o For optimum design, the filter pack should be graded according to the aquifer particle size distribution to ensure that the largest percentage of the aquifer material will be retained by the filter pack.
- o Well screen slot size should be sized to the filter pack. In most instances, the filter pack should be sized to retain 95 to 100% of the aquifer material.

**3. DEVELOPMENT**

The main purpose for the development of a well, any well, is to produce a turbid-free sample (i.e., to rid the filter pack, screen, and well casing of the small particles that remain that are the direct result of the installation procedure or design). Beyond this, the goal for wells in the water well industry differs significantly from the hazardous waste industry. In the water well industry, the purpose of well development is to obtain maximum yield with the least turbidity for the purpose of water consumption. In the hazardous waste industry, the purpose of development is to obtain a turbid-free sample for the purposes of chemical analysis in the parts per billion range. Wells designed for pump testing are the exception since increasing well efficiency may improve the quality of the pump test data. There is a significant difference between these two goals. In the hazardous waste industry, constructing wells for the purpose of high yields tends to be a secondary requirement.

Common methods of well development in fine-grained materials are pumping, surging, bailing, and the use of compressed air to "blow out" the well. All of these, or combinations thereof, are acceptable methods within the water well industry; however, all do not carry the same level of confidence within the hazardous waste industry. The following is a

presentation of recent information from literature addressing this issue.

### 3.1 PUBLISHED INFORMATION ON DEVELOPMENT

- o In the development of wells in glacial tills (Harman, 1988), a stainless steel submersible pump was used. The pump was lowered by hand to decrease the turbidity of the water. The pumping rate was slow and continuous, with a low volume of water being pumped. This pulled the fine-grained material from the sand pack. The silt settled to the bottom, and water samples could be taken from the top of the water column. Bailing could be used instead of pumping to develop the well.
- o In tight formations, well development must be sufficiently vigorous to remove fine-grained particles without damaging the well (Marbury and Brazie, 1988). The turbidity of the water needs to be reduced.
- o According to Giddings (1985), the steep hydraulic gradient caused by dewatering the well during pumping causes turbulent flow in the aquifer and in the gravel and sand pack, and this results in a very turbid sample. A surge and block bailer has been successfully used in developing low recharge wells.
- o According to Gass (1988), when an attempt is made to develop a silt or clay formation, the formation will not bridge, and greater amounts of the formation will be pulled into the well. The same type of surge energy reaches the formation when a well is purged and sampled with a bailer that fits snugly within the well or when a pump that just fits in a well is rapidly inserted or removed from the well. The key to achieving clean samples then is to reduce or eliminate surge energy from reaching the formation.
- o The following study was performed by Paul, Palmer, and Cherkauer (1988). In this case, some wells installed in fine-grained glacial tills were surged for 10 min and then bailed along with wells that were bailed only. Water was collected from the screened intervals for turbidity analysis. The hydraulic conductivity of the formation was sufficiently low that no significant well recovery occurred between the time the well was bailed and the sample was taken. Many of the samples contained a considerable amount of sediment. Bailings of two wells indicated a large amount of clay sediment at the bottom, which was easily agitated, especially when the bailer touched bottom. The wells were then pumped dry to reduce the amount of sediment and were allowed to recover. When samples were taken 4 months later, the turbidity had been reduced in all but one well.
- o Surging of the wells increased the turbidity. The turbidity was 50 to 100 times greater than that in wells that were bailed. Sand pack and screens had little effect on the amount of turbidity. In surged wells, the average turbidity stayed the same between the two sampling periods. In the bailed wells the turbidity decreased fourfold (Paul, Palmer, and Cherkauer, 1988).



- o In the restoration of clogged wells installed in glacial tills, jetting was used, and fine sand, silt, and clay are washed out of the water-bearing formation. The turbulence created by the jet brings these fine materials back into the well through screen openings above and below the point of operation (Gass, 1985).

### 3.2 DEVELOPMENT RECOMMENDATIONS

Based on the above information and in consideration of the procedures previously recommended for well design and installation, the following development procedures are recommended:

- o Remove any sediment that may exist within the well casing. This may be accomplished by using a sand bailer (which most drill rig operators are familiar with for larger diameter wells), by using pump and surge, or by using air lift techniques to remove the sediment in the sediment trap.
- o Ideally, the first attempt should be to develop a low yield well by pumping and/or removing water at a rate equal to or less than the recharge rate of the aquifer. This may be accomplished using peristaltic pumps, bailers, or bladder pumps for some aquifers. The object of this methodology is to induce water into the well at a very low but constant rate until the water is relatively clear. (NOTE: If bladder pumps are to be used, removing the silt from the well is critical because of the potential damage to the bladder.)
- o If the above techniques cannot be accomplished and the wells are pumped to near dryness even with slow rates of water removal, the next recommended option is to use a closed-bottom bailer in a pump-and-surge-type scenario. Under this scenario, as the bailer enters the well, the bailer itself acts as a surge block and forces water out through the screen, dislodging silt and clay size particles from the screen and the filter pack with the intention of the particles returning through the screen to be removed during the bailing operation. The surging activity, however, should not be so vigorous as to extend the surging action into the aquifer material itself. If during this process the well is pumped to dryness, the above procedure may have to be repeated one to two additional times to obtain a sample that is relatively sediment free. A specific application of this approach is to develop the well in stages (2 to 3 ft at a time, from the bottom up). In this the surge stroke should not exceed the surged interval.
- o At the completion of the development of a well, a well recovery test should be performed. This test is similar to a rising head slug test. These data will assist the field hydrogeologist in the development of other wells and in the scheduling and planning of

purge and sample activities. It is not implied, however, that well recovery tests should be conducted on every well. The discretion of the use of this test is held within the purview of the field hydrogeologist and the HAZWRAP project team.

#### 4. PURGING AND SAMPLING

##### 4.1 PURGING

Perhaps the most critical component of collecting a representative sample of the aquifer water occurs during the purging process. The main purpose of purging a well is to remove the stagnant water from the well casing and borehole and to replace it with groundwater that more accurately reflects chemical conditions within the aquifer. A lot of discussion has focused on this issue. The rationale for purging is to help remove fine-grained particles in the well and sand pack that may potentially enter the well screen and the sample (Paul, Palmer, and Cherkauer, 1988). (NOTE: All operations need to be performed with materials and equipment that have been thoroughly cleaned to avoid introducing contamination into the well. This is especially critical in low-yield wells because even a minute amount of contaminant may result in relatively high concentrations in samples.)

The following is a presentation of discussions on this issue that have occurred in technical publications over the past several years:

- o According to the Wisconsin Department of Natural Resources Guidance (Lindorf, Feld, Connelly, 1987), the most straightforward method for removing all of the stagnant water from wells screened in low permeability formations is to pump or bail the well dry. This procedure may be the best way to ensure that all of the stagnant water in the well has been exchanged with water from the aquifer. After purging, the well should be allowed to fully recover and can be purged a second time if needed.
- o The Environmental Protection Agency (EPA) Technical Enforcement Guidance Document (1986) is similar to this. It states that when low-yield wells are being developed, they should be pumped to dryness once. If the recharge rate of the well causes the formation water to vigorously cascade down the intake screen and accelerate the loss of volatiles, the well should not be pumped dry. If this is anticipated, three casing volumes should be purged from the well at a rate that does not cause the recharge water to be excessively agitated.
- o If a monitoring well is drained completely during purging, the formation water will be exposed to the atmosphere as it enters the well. This may cause a 10% loss of volatiles within 5 min and a 70% loss within 1 h. Protocols should avoid draining the well and any unnecessary exposure of the sample to the atmosphere, especially when combined with turbulence (McAlary and Barker, 1987).

- o If the sand pack around screens is drained during purging or flushing, the formation water will flow into the well by cascading through the headspace in the dewatered sand filter pack. Some volatilization can be expected to affect the groundwater even before a sample can be collected (McAlary and Barker, 1987).
- o The amount of recharge may limit the amount of sample that can be collected. Frequent purging will likely dewater the saturated zone, causing the well to go dry for a period of time. In wells that require a very long period of time to recharge, the interval between sampling events may not be sufficient to allow full recovery to static water-level conditions. In such cases, an annual or semiannual sampling event may be more appropriate than quarterly events (Marbury and Brazie, 1988).
- o The results of a laboratory standing-column volatilization test by McAlary and Barker (1987) showed that losses will reach 10% within 1 h and 99% in 1 month. The standing water should therefore be thoroughly purged before sampling. In the context of a sampling event, it may be acceptable in moderately low permeability materials to return for sampling of volatile organics several hours after purging, provided that the calm surface of the water in the casing was the only exposure of the sample to headspace.

#### 4.2 SAMPLING

The problems of purging and sampling low recharge wells are mutually related events. The type of purging a field team performs may affect the sampling effort. In addition, within the literature, it is not clear as to the best time to sample for volatile organics. The following are submitted for evaluation and review:

- o In low-yielding bedrock aquifers, wells may be pumped dry by removing only one bore volume of water. If the water-bearing fractures are located just below the static water table level, the well will refill by cascading water entering the bore and falling to the bottom. This alters the dissolved gases in the water and increases the dissolved oxygen content. Many monitoring parameters are sensitive to this alteration, and it can lead to misrepresentative sampling (Giddings, 1985).
- o A water-level monitoring period of several hours or days may be required to determine whether the well bore is making water or to determine if the water level will return to static water-level conditions. In these instances, it may be possible to remove only one casing volume before sampling (Marbury and Brazie, 1988).

- o Samples should be collected as soon as there is a sufficient amount of water in the well bore in order to get a sample that is representative of the formation water (Lindorf, Feld, Connelly, 1987).
- o According to the EPA Guidance, as soon as the well recovers, the order of sampling should be pH, volatiles, oxidation-reduction, semivolatiles, pesticides/polychlorinated biphenyls (PCBs), metals, and inorganic compounds. For wells with a recovery time of greater than 3 h, samples should be taken in order of their volatility as soon as there is a sufficient volume of water available for a sample for each parameter. Parameters that are not pH sensitive or subject to volatilization should be taken last.
- o In the sampling of naturally purged wells (Robin and Gillham, 1987), results indicated that a representative sample could be obtained from the screened interval through the use of dedicated sampling device, such as a syringe sampler. The intake would need to be located near the bottom of the screened interval. The volume of the sample would have to be significantly less than the volume of the screened interval. Some contamination could result from displacement of water by the sampling device. In this study, as screen lengths became shorter (screen lengths of 1, 2, and 5 ft), the first samples were progressively more contaminated.
- o In a recent article by Herzon et al. (1988) eleven 2-in. OD stainless steel wells were developed using bailers and a diaphragm pump. Bailers were used to extract water and to act as surge blocks to draw in fine materials. This procedure was repeated four times for each well. The diaphragm pumps were used to pump the wells to dryness so that a rising-head test could be performed on each well. Samples were retrieved at several different times after purging. The final conclusions were that wells in low-yield aquifers should be purged before sampling and that concentrations of volatile organics in the sample collected 4 h after purging contained the highest volatile organic concentrations.

#### 5. EQUIPMENT FOR DEVELOPMENT, PURGING, AND SAMPLING

To minimize the introduction of contamination into the well, positive gas displacement Teflon bladder pumps are recommended for purging wells. Teflon or stainless steel bailers are also recommended purging equipment. Where these devices can't be used, peristaltic pumps, gas-lift pumps, centrifugal pumps, and venturi pumps may be used. Where a sampling device requires an intake line, or discharge line, the composition of the line should be Teflon, polyethylene lined with Teflon, or polyethylene. Where a sampling device requires a support line to the surface (as in bailers), the support line should be single-strand, stainless steel wire, Teflon-coated stainless steel wire (single strand or braided), or a stainless steel leader attached to monofilament polyethylene line.

Pumping rates for peristaltic pumps are typically less than 1500 mL/min. Other types of pumps produce volatilization and high-pressure differentials, causing variability in the analysis of pH, specific conductance, metals, and volatile organic samples. They are, however, acceptable for purging wells (EPA Guidance, 1986).

The equipment required for jet development includes a jetting tool with two or more nozzles, a high-pressure pump, a high-pressure hose, and a supply of water. The nozzles should be evenly spaced on the jetting tool (Gass, 1985).

The valve-type plunger could be used in tight formations because it has a lighter surging action. A bailer can be used along with the plunger (Gass, 1985).

In Paul, Palmer, and Cherkauer, the surging process (in fine-grained glacial tills) was performed with a length of polyvinyl chloride (PVC) electrical conduit fitted with an oversized rubber stopper. The rubber stopper was small enough to allow passage through the well but large enough to force water before it. A peristaltic sampling pump was used to remove the bottom sediment from the monitoring wells.

In a study by Griffin et al. (1988) on the collection of volatile organics from fine-grained materials, samples were collected using a double-check valve, Teflon bailer with a bottom-draining device. For shallow, small-diameter wells with low yields, evacuation of the well by a bailer is feasible. Syringes can also be used to sample water from low hydrostatic head aquifers because they only remove a small volume of water from the well (Nielsen, 1985).

## 6. RECOMMENDED PROCEDURES FOR PURGING AND SAMPLING

The following purge and sample procedures are based on a review of the information provided above, known characteristics of monitoring well recharge and well dynamics, and the best available technology. The succeeding information is provided to act as a starting point with regard to planning and execution of sampling activities within low recharge environments. It is understood that as field activities commence, minor revisions to the purge and sample activities may be required based on site-specific information; however, the following scenario should be used and planned for during the early stages of field activity development.

The following procedures are recommended for purging and sampling of low recharge aquifers:

- o As a general rule, under low recharge conditions, purge and sample activities should not occur for a minimum of 7 d after well development. This period may be extended, dependent upon very low recharge conditions and varying site conditions.

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- o Purging and sampling are considered by HAZWRAP to be mutually inclusive activities (i.e., they are not separate events). Therefore, the common field activity of purging all wells first then sampling is not considered to be the best available procedure. Purging and sampling should be considered, in terms of schedule, as one event.
- o Purging begins with placing the pump or purge device at the top of the water column to remove the water from the well casing and borehole from the top down.
- o Purge rates should be at a value less than that indicated from the well development recharge rate recorded at the conclusion of well development. Under low recharge conditions, this rate will rarely exceed 0.5 gal/min. This low purge rate will permit the water within the casing and borehole to exchange without pumping the well to dryness or appreciably depressing the static water level.
- o If the above condition cannot be met, the entire volume of water within the well casing and borehole should be removed at the rate determined above. If it is already known that the well can be pumped down without appreciable recharge, the rate specified above should not be exceeded. Excessive pumping will only cause turbidity problems when eventual recharge and sampling begin. (NOTE: As a reminder, under the well construction recommendations, each well will exhibit a 2- to 5-ft sediment trap to be located below the screen. Therefore, the sediment trap should be removed of built-up sediment before actual purging and sampling).
- o If the well does not recover to 90% of its static water level within 6 to 8 h, only one borehole volume need be removed. If the well recovers in less time, purge activities should be repeated at least one more time. At the conclusion of the initial purge activities, if significant fines have accumulated in the sediment trap, these fines should be removed before the second purge activity.
- o Sampling from wells in which the static water level was not appreciably depressed is to occur immediately after purge activities are completed (within 3 h as a general rule). Sampling from wells, in which the water was completely removed from the well or the recovery time exceeds 3 h, will occur (for volatiles and pH and oxidation-reduction sensitive analytes) when the water level has reached a point above the bottom of the screen such that a sufficient sample can be retrieved. Sampling for other nonsensitive analytes may occur at some point later as the well has had time to more completely recover and provide sufficient sample. If sufficient sample has not become available within 24 h, the HAZWRAP Project Manager should be immediately informed so that a decision can be made as to the disposition of this condition.

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- Lindorf, D., Feld, J., and Connelly, J., Groundwater Sampling Procedure Guidelines, Wisconsin Department of Natural Resources Publication PUBL-WR-153 87, February 1987.
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Robin, M. J. L. and Gillham, R. W., "Field Evaluation of Well Purging Procedures," pp. 85-93, Groundwater Monitoring Review, Fall 1987.

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U.S. EPA, RCRA Ground Water Monitoring Technical Enforcement Guidance Document (TEGD), printed by National Water Well Association, Dublin, Ohio, p.208. 1986.

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# VARIANCE FORM

VARIANCE NO. 11

PROJECT NO. 409721.02.05 PAGE 1 OF     

PROJECT NAME SKY HARBOR DATE 9 APR 91

### VARIANCE (INCLUDE JUSTIFICATION)

The purge requirements for sampling groundwater in the Sky Harbor FSP require 3 well volumes be removed prior to sampling monitoring wells, FSP Section 5.7.4.1. Following HAZWRAP SOP #4 <sup>to calculate the well volume,</sup> this amounts to approximately 150 gallons per well. A piezometer (2-inch diameter) is being sampled for additional GW quality information. Because of the smaller diameter, the sampling pump will not fit into the piezometer screen. This variance requests the use of HAZWRAP SOP #4 - INDICATOR PARAMETER METHOD OF WELL PURGING (Section 5.3) <sup>(SEE ATTACHMENT)</sup> Be used in place of the 3 volume requirement. The variance is requested because of the length of time that will be required to remove 150 gallons from a 2-inch piezometer using a 1-inch I.D. Bailor.

Monitoring wells sampled to date indicate parameter (PH, etc) stabilization is achieved within 1 well volume, thus, the need for purging beyond 1 well volume is not indicated. 1 well volume will be removed from the subject piezometer and parameter stabilization will be used prior to sampling. The indicator parameters to be measured are those discussed in Sect. 5.7.4.2. No adverse effects on data quantity or quality are expected to result from this variance.

This variance applies only to the sampling of 2-inch piezometers.

### APPLICABLE DOCUMENT:

Final Site Investigation Field Sampling Plan 141st Air Refueling Group, Arizona Air National Guard, Sky Harbor International Airport, Phoenix, Arizona. Sept 1990 Section 5.7.4.1

CC: David Bunn *DB*  
HAZWRAP Files - 0449

REQUESTED BY *Steve Jones* DATE 4-9-91

APPROVED BY *David Bunn* DATE 4/9/91  
Project Manager

*Don Mack* DATE 10 APR 91  
Quality Assurance Officer

*Robert W. Jones* DATE 4/15/91  
HAZWRAP Project Manager

HAZARDOUS WASTE REMEDIAL ACTIONS PROGRAM  
STANDARD OPERATING PROCEDURE 4  
WELL DEVELOPMENT AND PURGING

1. OBJECTIVE

The objective of this procedure is to define the procedural requirements for well development and purging.

2. BACKGROUND

Monitor wells are developed to remove skin (i.e., near-well-bore formation damage) and to settle and remove fines from the filter pack. Wells should not be developed for 24 h after completion when a cement bentonite grout is used to seal the annular space. However, wells may be developed before grouting if conditions warrant. Wells are purged immediately before groundwater sampling to remove stagnant water and a sample representative of groundwater conditions. Wells should be sampled within 3 h of purging (optimum) to 24 h after purging (maximum, for low recharge conditions).

3. RESPONSIBILITIES

Site Manager: The Site Manager is responsible for ensuring that field personnel are trained in the use of this procedure and for verifying that development and purging are carried out in accordance with this procedure.

Project Field Geologist: The Project Field Geologist is responsible for complying with this procedure.

4. REQUIRED EQUIPMENT

- Pump, pump tubing, or bailer and rope or wire line.
- Power source (e.g., generator), if required.
- Water-level meter or weighted surveyor's tape.
- Temperature, conductivity, pH, and/or dissolved oxygen meters (for Sect. 5.2 below).
- Personnel protective equipment as specified in the site-specific health and safety plan.

- Decontamination supplies, if required on-site.
- Disposal drums, if required.

## 5. PROCEDURES

### 5.1 WELL DEVELOPMENT

The following steps must be followed when developing wells:

1. Put on personnel protective clothing and equipment as specified in the site-specific health and safety plan.
2. Open and check the condition of the wellhead, including the condition of the surveyed reference mark, if any.
3. Determine the depth to static water level and depth to bottom of the casing.
4. Prepare the necessary equipment for developing the well. There are a number of techniques that can be used to develop a well. Some of the more common methods are bailing, overpumping, backwashing, mechanical surging, surge and pump, and high-velocity jetting. All of these procedures are acceptable; however, final approval of the development method rests with the appropriateness of a specific method to the site and the Hazardous Waste Remedial Actions Program (HAZWRAP) project manager.
5. For screened intervals longer than 10 ft, develop the well in 2- to 3-ft intervals from bottom to top. This will ensure proper packaging in the filter pack. Note: It is good practice to develop all screened and filter-packed wells in stages.
6. Continue well development until produced water is clear and free of suspended solids. Record pertinent data in the field logbook and on appropriate well development forms per HAZWRAP SOP 1, Parts A and B, respectively.
7. Remove the pump assembly or bailers from the well, decontaminate (if required), and clean up the site. Lock the well cover before leaving. Dispose of produced water as required by the project work plan.

### 5.2 VOLUMETRIC METHOD OF WELL PURGING

The following steps should be followed when purging a well by the volumetric method:

1. Put on personnel protective clothing and equipment as specified in the site-specific health and safety plan.
2. Open the well cover and check the condition of the wellhead, including the condition of the surveyed reference mark, if any.
3. Determine the depth to static water level and depth to bottom of well string. Calculate the well volume (volume of water within the well bore) using the following formula (or equivalent):

$$7.4805 \left( \frac{D^2 \pi}{4} \right) dH = \text{volume (in gallons)},$$

where

D = casing diameter in feet. (NOTE: This equation is used for grouted wells with short screens. For wells with long screens and/or ungrouted wells, then D = borehole diameter in feet.)

dH = the distance from well bottom to static water level in feet.

Note these data and calculations in the field logbook.

4. Prepare the pump and tubing, or bailer, and lower it into the casing.
5. Remove the number of well volumes specified in the project plans. Generally, three to five well volumes will be required. In low-recharge aquifers, the well will commonly pump or bail to dryness before three well volumes of water are removed. If this is the case, there is no need to continue with purging operations (HAZWRAP Position Paper No. 2). Record pertinent data (e.g., water volume) in the field logbook.
6. Remove the pump assembly or bailer from the well, decontaminate it (if required), and clean up the site. Lock the well cover before leaving. Dispose of produced water as required by the project work plan.

### 5.3 INDICATOR PARAMETER METHOD OF WELL PURGING

1. Put on personnel protective clothing and equipment as specified in the site-specific health and safety plan.
2. Open the well cover and check the condition of the wellhead, including the condition of the surveyed reference mark, if any.
3. Determine the depth to static water level and depth to bottom. Lower the probe(s) of the indicator meters (e.g., temperature, conductivity) into the water to a point near (but not at) the well bottom or use the flow-through system for indicator parameter measurement. Alternatively, set up surface probe(s) (e.g., pH, dissolved oxygen) at the discharge orifice or dedicated probe port of the pump assembly or within the flow-through chamber. Allow subsurface probe(s) to equilibrate according to manufacturer's specifications. Record the equilibrated readings in the field logbook together with the time.
4. Assemble the pump and tubing, or bailer, and lower into the casing.
5. Begin pumping or bailing the well. Record indicator parameter readings at predetermined intervals. Maintain a record of the approximate volumes of water produced.
6. Continue pumping or bailing until indicator parameter readings remain stable within  $\pm 10\%$  for three consecutive recording intervals. Purging should continue until the discharge stream is clear. In low-recharge aquifers the well may pump or bail to

- dryness before indicator parameters stabilize. In this case, there is no need to continue purging. Record pertinent data (e.g., water volume) in the field logbook.
7. Remove the pump assembly or bailer from the well, decontaminate (if required), and clean up the site. Lock the well cover before leaving. Dispose of produced water as required by the project work plan.

## 6. RESTRICTIONS/LIMITATIONS

Where flammable free or emulsified product is expected or known to exist on or in groundwater, use only intrinsically safe electrical devices and place portable power sources (e.g., generators) 50 ft or more from the wellhead and disposal drums.

## 7. REFERENCES

- Driscoll, F. G., *Groundwater and Wells*, Second Edition, St. Paul, Minnesota, Johnson Division, 1986.
- U.S. Environmental Protection Agency, *A Compendium of Superfund Field Operations Methods*, EPA/540/P-87/001, 1987.
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# NONCONFORMANCE REPORT

PROJECT AZANG Sky Harbor

NR NO. 1

PROJECT NO. 409721

PAGE 1 OF 1

DATE: 01/18/91

## 1. NONCONFORMANCE DESCRIPTION

**Problem:** Poor recovery of some peaks or completed loss of peaks for start of day standard analysis.

**Criteria:** Per SOP, start of day calibration will be ran and acceptable recovery occur for all compounds.

**Impact:** Has no impact on previous analytical data, but will have significant impact on any future data if not corrected.

IDENTIFIED BY: D. Peary DATE: 01/17/91

## 2. PROPOSED CORRECTIVE ACTION, INCLUDING INITIATION AND COMPLETION DATES

Cleaning of lamp and detector head 01/17, 01/18, 01/19 and recalibrate.

TO BE PERFORMED BY: D. PEERY

## 3. APPROVAL FOR PROPOSED CORRECTIVE ACTION

[Signature] 1/17/91  
Project Manager Date  
[Signature] 1/24/91  
Quality Assurance Manager Date

## 4. CORRECTIVE ACTION TAKEN (IF DIFFERENT FROM THAT PROPOSED)

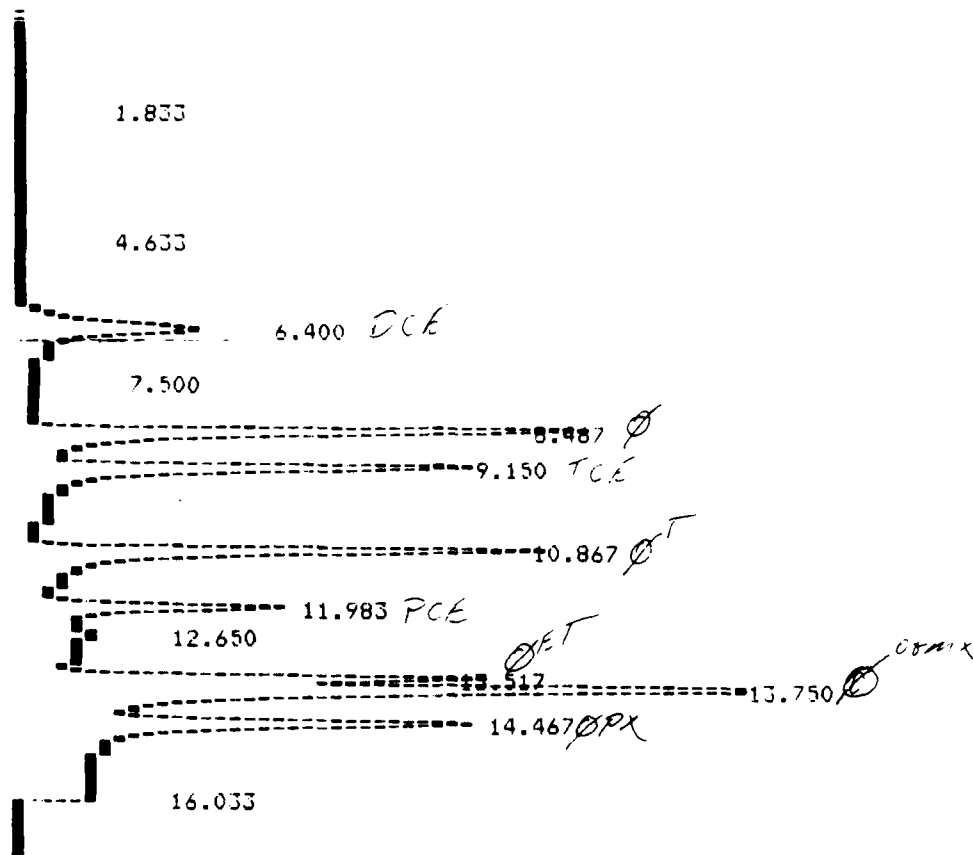
GC was replaced 01/19/91 with a new instrument from a different vendor.

## 5. CORRECTIVE ACTION COMPLETE

PERFORMED BY: D. Peary DATE: 01/19/91  
VERIFIED BY: [Signature] DATE: 1/19/91

CC: PROGRAM MANAGER  
PROJECT MANAGER  
QUALITY ASSURANCE MANAGER  
QUALITY ASSURANCE COORDINATOR  
CENTRAL FILES \_\_\_\_\_  
OTHER: \_\_\_\_\_

FULLSCALE MILLIVOLTS 256



SKYHARBOR PHOENIX AZ, PROJECT E 409721  
 DATA FILENAME C:\STSTD4.PRN  
 16:24:23 01-19-1991  
 START STANDARD DAY 4 @ JUL 5 + 3UL BTEX

RET.TIME	PEAK AREA	HEIGHT	AREA%	NORM%	EXT.STD	INT.STD.	PEAKNAME	RET
6.400	1401.95	64.45	8.3007	9.61	1401.95	1401.9501		6.40
8.467	2602.07	222.35	15.4064	17.84	2602.07	2602.0691		8.47
9.150	2059.98	174.75	12.1968	14.12	2059.98	2059.9827		9.15
10.867	2580.66	204.55	15.2796	1.89	275.12	275.1227	BENZENE	10.87
11.983	1057.73	99.75	6.2626	7.25	1057.73	1057.7277		11.98
12.650	280.54	26.10	1.6611	1.92	280.54	280.5441		12.65
13.517	1550.76	177.85	9.1818	10.63	1550.76	1550.7592		13.51
13.750	3431.59	323.75	20.3179	23.53	3431.59	3431.5930		13.75
14.467	1667.60	172.85	9.8736	11.43	1667.60	1667.6001		14.47
16.033	153.81	27.90	0.9107	1.05	153.81	153.8100		16.03

DILUTION FACTOR = 1  
 TOTAL NUMBER OF PEAKS DETECTED 14 AREA REJECT= 75  
 TOTAL NUMBER OF IDENTIFIED PEAKS 1 USING SKYHARB.CFT .LFT  
 TOTAL UN-CORRECTED PEAK AREA 16889.5  
 TOTAL NORMALIZED PEAK AREA 14583.97  
 INTERNAL STANDARD CORRECTION FACTOR 1  
 INTERNAL STANDARD PEAK NAME AT TIME 1

TOTAL HYDROCARBONS (total peak area using TPH cal.curve) 31979 NANOGRAMS





INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# NONCONFORMANCE REPORT

PROJECT AZANG Sky Harbor NR NO. 2  
 PROJECT NO. 409721 PAGE 1 OF 1  
 DATE: 01/30/91

## 1. NONCONFORMANCE DESCRIPTION

**Problem:** Significant shifting of retention time and loss of resolution for ethylbenzene and xylenes.

**Criteria:** Per SOP, calibration should show consistent retention time and separation of peaks.

**Impact:** Samples ran during time GC was out of control, some tentative identification and quantification of compounds based upon information from retention time data obtained from extra standard runs daily. Samples will be rerun when back on line.

IDENTIFIED BY: Cara Huston DATE: 01/17/91

## 2. PROPOSED CORRECTIVE ACTION, INCLUDING INITIATION AND COMPLETION DATES

Check temperature program, carrier gas flow rate, carrier gas pressures, connectors for leaks, cycle through program shooting standards monitoring standards data 01/29 through 02/01/91.

TO BE PERFORMED BY: Cara Huston

## 3. APPROVAL FOR PROPOSED CORRECTIVE ACTION

<u>[Signature]</u>	<u>1/18/91</u>
Project Manager	Date
<u>[Signature]</u>	<u>01/20/91</u>
Quality Assurance Manager	Date

## 4. CORRECTIVE ACTION TAKEN (IF DIFFERENT FROM THAT PROPOSED)

Same as above.

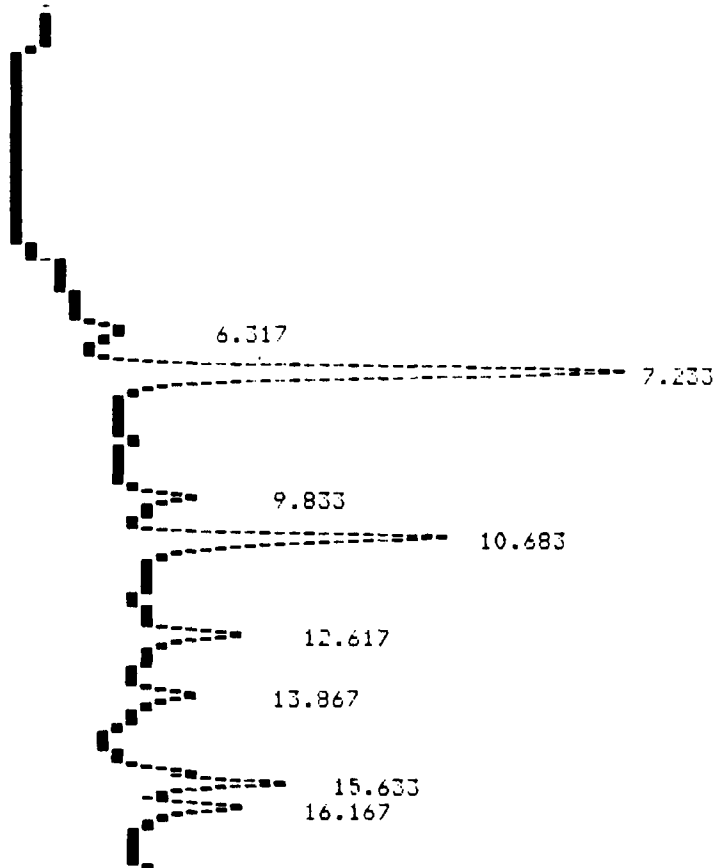
## 5. CORRECTIVE ACTION COMPLETE

PERFORMED BY: Cara Huston DATE: 01/29/91-02/01/91  
 VERIFIED BY: [Signature] DATE: 01/20/91

CC: PROGRAM MANAGER  
 PROJECT MANAGER  
 QUALITY ASSURANCE MANAGER  
 QUALITY ASSURANCE COORDINATOR  
 CENTRAL FILES \_\_\_\_\_  
 OTHER: \_\_\_\_\_

**CHROMATOGRAM PLOT**  
**DATA FILE C:STSD11.PRN**  
**13:19:07 01-30-1991**

FULLSCALE MILLIVOLTS 64



*Handwritten notes:*  
 2000  
 20000  
 RT 5.834  
 Peak 10.683

**SKYHARBOR PHOENIX AZ, PROJECT E 409721**  
**DATA FILENAME C:STSD11.PRN**  
**13:19:07 01-30-1991**  
**START OF DAY 11 STANDARD *3ul Low***

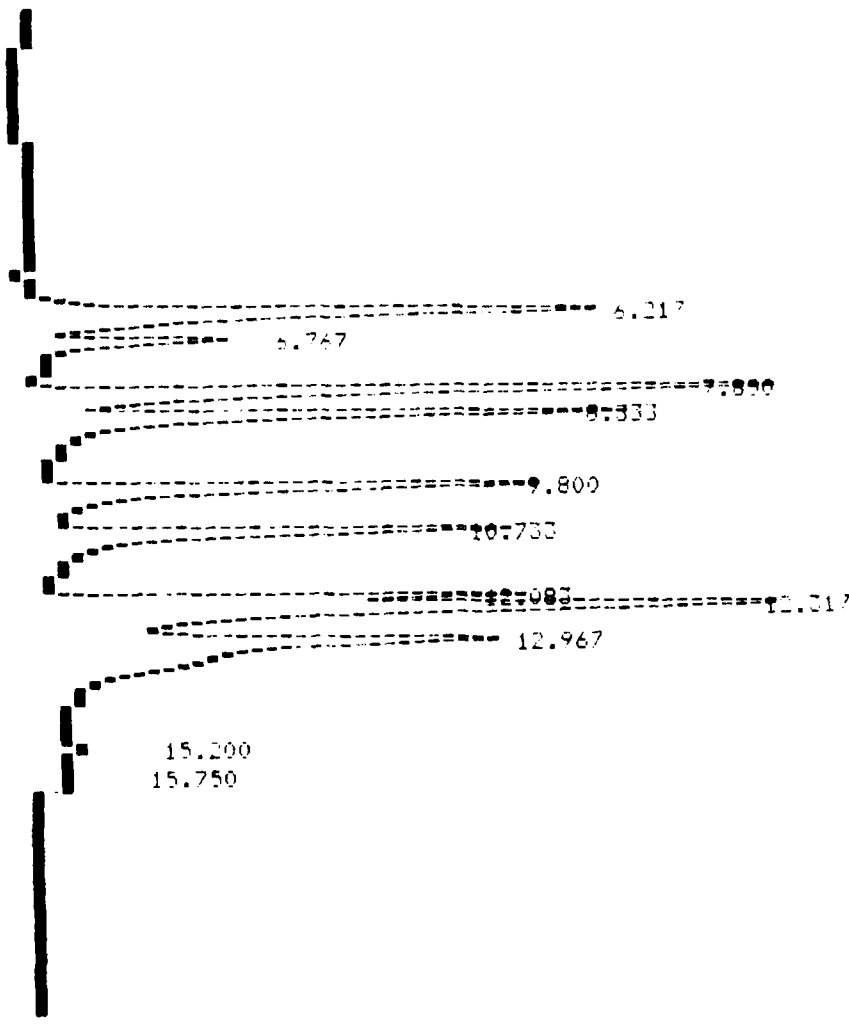
RET.TIME	PEAK AREA	HEIGHT	AREA%	NORM%	EXT.STD	INT.STD.	PEAKNAME	REF
7.233	316.85	53.46	39.8579	37.87	161.95	161.9519	TCASDCE	7.233
9.833	81.76	13.61	3.9892	1.37	5.87	5.8719	BENZENE	9.833
10.683	462.07	38.52	22.5467	16.75	71.64	71.5403	TCE	10.683
12.617	142.23	17.93	6.9401	2.19	9.34	9.3440	TOLUENE	12.617
13.867	117.06	13.56	5.7119	14.71	62.90	62.8953	PCE	13.867
15.633	252.61	22.74	12.3261	5.84	24.98	24.9766	D&MXYL	15.633
16.167	95.20	18.04	4.6941	2.41	10.32	10.3249	PXYL	16.167

DILUTION FACTOR = 1  
 TOTAL NUMBER OF PEAKS DETECTED 8 AREA REJECT= 50  
 TOTAL NUMBER OF IDENTIFIED PEAKS 7 USING SKYHARBOR FT 1000  
 ONLY IDENTIFIED PEAKS WERE REPORTED-OTHER PEAKS MAY HAVE BEEN DETECTED  
 TOTAL UN-CORRECTED PEAK AREA 2049.394  
 TOTAL NORMALIZED PEAK AREA 427.6283  
 INTERNAL STANDARD CORRECTION FACTOR 1  
 INTERNAL STANDARD PEAK NAME AT TIME 1

TOTAL HYDROCARBONS (total peak area using TPH cal. curve) 2298.797 (nanograms)

CHROMATOGRAM PLOT  
 DATA FILE C:EDSD13.PRN  
 21:54:33 02-01-1991

FULLSCALE MILLIVOLTS 128



*IN CONTROL  
 AT BACK - 0.1MVA  
 GOOD ANALYSIS*

SKYHARBOR PHOENIX AZ, PROJECT # 409721  
 DATA FILENAME C:EDSD13.PRN  
 21:54:33 02-01-1991  
 END OF DAY STD.@ 2uL 100 + 2uL HI BX

RET. TIME	PEAK AREA	HEIGHT	AREA%	NORM%	EXT. STD	INT. STD.	PEAK NAME	REF
6.217	1800.21	108.30	15.5782	29.41	874.74	874.7409	TCAPDCE	5120
7.850	1705.73	144.70	14.7312	6.46	198.87	198.8682	BENZENE	5120
8.333	1381.09	111.70	11.9206	9.90	274.12	274.1245	TCE	5120
9.800	1192.63	94.80	10.2939	4.82	148.54	148.5386	TOLUENE	5120
10.733	1192.36	88.50	10.2916	12.70	390.90	390.8995	PCB	5120
12.083	857.19	94.10	7.3986	5.19	159.66	159.5612	ETHBENT	1000
12.317	1655.05	142.70	14.2854	8.30	255.57	255.5690	OSMOL	5120
12.967	1262.56	88.50	10.8975	7.75	238.56	238.5624	PAH	5120

DILUTION FACTOR = 1  
 TOTAL NUMBER OF PEAKS DETECTED 11 AREA REJECT= 50  
 TOTAL NUMBER OF IDENTIFIED PEAKS 8 USING SKYHARBOR LIT  
 ONLY IDENTIFIED PEAKS WERE REPORTED-OTHER PEAKS MAY HAVE BEEN DETECTED  
 TOTAL UN-CORRECTED PEAK AREA 11585.74  
 TOTAL NORMALIZED PEAK AREA 1078.892  
 INTERNAL STANDARD CORRECTION FACTOR 1



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# NONCONFORMANCE REPORT

NR NO. 3

PROJECT SKY HARBOR SI

PAGE 1 OF 1

PROJECT NO. 409721

DATE: 22 FEB 91

## 1. NONCONFORMANCE DESCRIPTION

SAMPLES ARE SENT TO THE LABORATORY DAILY AND HELD PENDING PHONED-IN INSTRUCTIONS FOR WHICH SAMPLES TO ANALYZE BASED ON FIELD SCREENING. TWO CASES ARE IDENTIFIED IN WHICH MISCOMMUNICATION HAS RESULTED IN SAMPLES NOT BEING SCHEDULED FOR ANALYSIS. SAMPLES SBI-02-5-7 AND SBI-02-25-27 WERE NOT SCHEDULED FOR ANALYSIS; ONLY 1 SAMPLE FROM THIS BORING WAS ANALYZED. ALSO, SAMPLE SB2-01-50-52 WAS NOT ANALYZED; 2 SAMPLES FROM THIS BORING WERE ANALYZED. THE WORK PLANS CALL FOR THREE SAMPLES TO BE ANALYZED FROM EACH BORING.

SW 5  
3-14-91

LOSS OF THE VOA AND SVOA WILL NOT CAUSE SIGNIFICANT IMPACTS TO THE PROJECT RESULTS. EACH BORING HAS LABORATORY LEVEL C DATA FROM AT LEAST ONE DEPTH. FIELD-LEVEL B ANALYSES WERE CONDUCTED ON ALL SAMPLES AND CAN BE USED AS INDICATORS OF THE PRESENCE OR ABSENCE OF CROSS CONTAMINATION. ALSO, TPH ANALYSES WILL PROVIDE SOME LEVEL C INDICATIONS OF CONTAMINATION FOR ALL SAMPLES. THE LOSS OF DATA WILL LOWER THE "COMPLETENESS" OBJECTIVE BUT WILL HAVE MINIMAL INTERPRETATIVE SIGNIFICANCE

IDENTIFIED BY: S. SARGO DATE: 22 FEB 91

## 2. PROPOSED CORRECTIVE ACTION, INCLUDING INITIATION AND COMPLETION DATES

1. SAMPLES FROM SBI-02 HAVE EXCEEDED HOLDING TIME FOR VOA AND SVOA AND DATA CANNOT BE RECOVERED
2. SAMPLES FROM SBI-02 CAN BE SCHEDULED FOR TPH WITHIN HOLDING TIME.
3. SAMPLE SB2-01-50-52 HAVE EXCEEDED HOLDING TIME FOR SOA AND SIOA AND DATA CANNOT BE RECOVERED
4. SAMPLE SB2-01-50-52 TO BE SCHEDULED FOR TPH AND TAL ANALYSIS
5. FUTURE INSTRUCTION FOR SAMPLES TO BE ANALYZED TO BE WRITTEN AND FOLLOWED BY PHONE VERIFICATION

TO BE PERFORMED BY: S. SARGO/LAB #1-4; FIELD SUPER #5

## 3. APPROVAL FOR PROPOSED CORRECTIVE ACTION

[Signature] 2/25/91  
Project Manager / Date

[Signature] 15 MAR 91  
Quality Assurance Manager / Date

## 4. CORRECTIVE ACTION TAKEN (IF DIFFERENT FROM THAT PROPOSED)

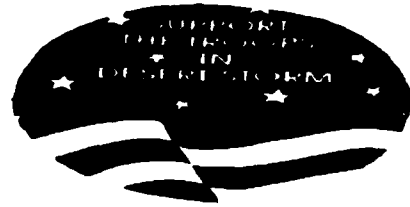
## 5. CORRECTIVE ACTION COMPLETE

PERFORMED BY: [Signature] DATE: 2-22-91

VERIFIED BY: [Signature] DATE: 3-25-91

- CC: PROGRAM MANAGER  
PROJECT MANAGER  
QUALITY ASSURANCE MANAGER  
QUALITY ASSURANCE COORDINATOR  
CENTRAL FILES \_\_\_\_\_  
OTHER: \_\_\_\_\_

TELECOPY REQUEST



TELECOPY NUMBER: IT-Abingogoe-Carrizos  
 TO: Marla Miller  
 FROM: Steve Savelle  
 DATE: 22 Feb 91  
 NUMBER OF PAGES: 3 (INCLUDING COVER SHEET)  
 REMARKS:

IT CORPORATION  
 312 DIRECTORS DRIVE  
 KNOXVILLE, TN 37923  
 (615) 690-3211

DISCARD WHEN SENT  
 PLEASE RETURN

IF ALL PAGES ARE NOT RECEIVED, PLEASE ASK FOR EXTENSION 2223 AT THE ABOVE NUMBER. THANK YOU.

IF KNOXVILLE FAX NO. 615/690-3626 OR 615/690-4682

TRANSMISSION REPORT

THIS DOCUMENT WAS CONFIRMED  
 (REDUCED SAMPLE ABOVE - SEE DETAILS BELOW)

**\*\* COUNT \*\***

TOTAL PAGES SCANNED : 3  
 TOTAL PAGES CONFIRMED : 3

RESULT OF LAST BATCH SENT  
 \*\*\* SEND \*\*\*

NO.	REMOTE STATION	START TIME	DURATION	#PAGES	MODE	RESULTS
1	CERRITOS	2-22-91 11:41AM	2 00"	3/ 3		COMPLETED 9600

TOTAL 01:02 00" 3

NOTE:

NO. : OPERATION NUMBER 48 : 4800BPS SELECTED EC : ERROR CORRECT G2 : G2 COMMUNICATION  
 PD : POLLED BY REMOTE SF : STORE & FORWARD RI : RELAY INITIATE RS : RELAY STATION  
 MB : SEND TO MAILBOX PG : POLLING A REMOTE MP : MULTI-POLLING RM : RECEIVE TO MEMORY



# RECORD OF

TELECON  
 MEETING

Project Name	Number	Phase	Task	Subtask
--------------	--------	-------	------	---------

SKY HARBOR	409721			
------------	--------	--	--	--

Date 22 FEB 91

Time 11:05 EST

CALL FROM  NAME: Steve Sares  
CALL TO

Other Participants - Name/Location/Representing:

NONE

CALL FROM  NAME:  
CALL TO  Marla Miller

Telephone Number:

Company Name: ITAS-CERRITOS

Address:

Topic

SKY HARBOR ANALYSES.

City

State

Zip Code

Summary (Decisions & Specific Actions Required by Named Persons):

1. I've reviewed her fax from 21 FEB with respect to sample nos. and analyses - action items for lab are:

A. Sample no. recorded as SB1-01-0-2-01 - Lab# C1-01-317 01A received 1/30/91 on CofC # 163132 should be SB2-01-0-2-01/-02 SB1-01 was not drilled.

B. Sample SB1-02-5-7-01, Lab# C1-02-071 01A received 2/6/91 should be analyzed for TPH. - Note close holding time.

C. Sample SB1-02-25-27-01, Lab# C1-02-071 02A received 2/6/91 should be analyzed for TPH. - Note close holding time.

D. Sample SB2-01-50-52-01, Lab# C1-01-317 06A received 1/30/91 should be analyzed for TPH and TAC Metals. - Note close holding time on TPH.

Required Action: A. LAB to schedule analyses indicated above  
B. Sares to fax phone record for confirmation  
C. LAB to include RFA with sample login letter  
D. Marla to send copy of tracking spreadsheet regularly.

Prepared by (Signature)

Distribution:  
Original to Project File  
Copy to Project Manager  
Copy to Preparer

Other Distribution (By Preparer)

J. Tybuski, M. Miller

PAGE 1 OF 2



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# RECORD OF

TELECON  
 MEETING

Project Name	Number	Phase	Task	Subtask
SKY HARBOR	409721			

Date: 22 FEB 91 Time: 1105 EST

CALL FROM  NAME: Steve Sares  
CALL TO

Other Participants - Name/Location/Representing:

NONE

CALL FROM  NAME:  
CALL TO  Marla Miller

Telephone Number:

Company Name: ITAS-Ceritos

Address:

Topic

SKY HARBOR ANALYSES

City

State

Zip Code

Summary (Decisions & Specific Actions Required by Named Persons):

2. GROUND water Sampling will be delayed, probably will do ~ 5-6 Soil Borings x 3 Samples each in 2 to 3 weeks. Gwl Sampling will be after soil borings. Schedule not certain yet. Tybuski will coordinate field schedule as soon as we know more.

3. Lab to send RFA with sample logs in receipts  
\* Tybuski to fax revised RFAs to Lab to indicate changes in analytical program and follow up with unusual phone call.

Required Action:

E. Tybuski to fax revised RFA to Lab to indicate changes from original RFA.

Prepared by (Signature)

*Steve Sares*

Distribution  
Original to Project File  
Copy to Project Manager  
Copy to Preparer

Other Distribution (By Preparer)

J. Tybuski, M. Miller

PAGE 2 OF 2



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

REQUEST FOR ANALYSIS

R/A Control No. 203062  
C/C Control No. 163151

PROJECT NAME Sky Harbor ANG DATE SAMPLES SHIPPED 3/21/91  
 PROJECT NUMBER 40972(02.06) LAB DESTINATION ITAS - CERRITOS, CA  
 PROFIT CENTER NUMBER 3521 LABORATORY CONTACT MARLA MILLER  
 PROJECT MANAGER DON WILLEN SEND LAB REPORT TO DON WILLEN  
 BILL TO IT - KNOXVILLE  
312 DIRECTORS DR.  
KNOXVILLE, TN  
 PURCHASE ORDER NO. See Don Willem DATE REPORT REQUIRED 3 WEEKS  
 PROJECT CONTACT JOE TYBURSKI PROJECT CONTACT PHONE NO. 602/275-1325

Sample No	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
M83-04-01-2-01	SOIL	6-INCH GRASS SCRIBE	ICE	TPH, TOPB, VOA, SEMVOA	
M83-04-15-16 1/2-01 & 02	↓	2 X 6-INCH GRASS SCRIBES	↓	TPH, TOPB, VOA, SEMVOA	
M83-04-99-01	SOIL	400 ML	ICE	HOLD FOR INSTRUCTIONS	←

TURNAROUND TIME REQUIRED: (Rush must be approved by the Laboratory Project Manager) OC LEVEL: (Levels II and III subject to surcharge; project-specific requirements must be submitted to lab before beginning work.)  
 Normal  Rush \_\_\_\_\_ (Subject to rush surcharge.) I \_\_\_\_\_ II \_\_\_\_\_ III \_\_\_\_\_ Project Specific   
 POSSIBLE HAZARD IDENTIFICATION (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances.)  
 Non-hazard \_\_\_\_\_ Flammable  Skin Irritant  Highly Toxic \_\_\_\_\_  
 SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, archive and disposal.)  
 Return to Client \_\_\_\_\_ Disposal by Lab  Archive \_\_\_\_\_ (Indicate number of months.)  
 FOR LAB USE ONLY Received by Marla Miller Date/Time \_\_\_\_\_  
 \* Lab instructed to analyze for TPH, TCPB, VOA, SWOA. JET 3-22-91  
 POSSIBLE HAZARD IDENTIFICATION: OTHER SOLVENTS (Please Specify)





**REQUEST FOR ANALYSIS**

R/A Control No. **208057**  
 C/C Control No. **163146**

PROJECT NAME SKY HARBOUR ASHG DATE SAMPLES SHIPPED \_\_\_\_\_  
 PROJECT NUMBER 409221.02.06 LAB DESTINATION \_\_\_\_\_  
 PROFIT CENTER NUMBER 3521 LABORATORY CONTACT \_\_\_\_\_  
 PROJECT MANAGER Don Wilton SEND LAB REPORT TO \_\_\_\_\_  
 BILL TO IT - Knoxville

PURCHASE ORDER NO. 312 DICKENS DR.,  
KNOXVILLE, TN  
SEA DON WILTON  
 DATE REPORT REQUIRED 3 WEEKS  
 PROJECT CONTACT FOR TY BURMAN  
 PROJECT CONTACT PHONE NO. 602/275-1325

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
MIS-01-0- 2-01-02-03	SOIL	3 X 6-INCH BRASS SLEEVES	ICE TO 4°C	TPH, VOA, SWA, TAL, TOP	
MIS-01-0- 3-01-04	↓	2 X 6-INCH BRASS SLEEVES	↓	HOLD FOR INSTRUCTIONS	
MIS-01-0- 10-32	SOIL	1 X 6-INCH BRASS SLEEVE	ICE TO 4°C	TPH, VOA, SWA, TAL, TOP, B, ULTRAVIOLET/NITRATE	IF SAME AMOUNT IS IN EXCELLENT CONTACT PLEASE CONTACT FOR ORDER OF PRIORITY
MIS-01-TB	WATER	2 X 40 ML	HCL, ICE TO 4°C	VOA	
MIS-01-60-62- 01	SOIL	LAST 2 PART 1500 1 X 6-INCH BRASS SLEEVE	ICE TO 4°C	HOLD FOR INSTRUCTIONS	
		LAST LINE			

TURNAROUND TIME REQUIRED: (Rush must be approved by the Laboratory Project Manager) OC LEVEL: (Levels II and III subject to surcharge; project-specific requirements must be submitted to lab before beginning work)

Normal  Rush \_\_\_\_\_ (Subject to rush surcharge) I \_\_\_\_\_ II \_\_\_\_\_ III \_\_\_\_\_ Project Specific

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Non-hazardous \_\_\_\_\_ Flammable \_\_\_\_\_ Skin Irritant  Highly Toxic \_\_\_\_\_

SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, archive and disposal)

Return to Client \_\_\_\_\_ Disposal by Lab  Archive \_\_\_\_\_ (Indicate number of months.)

FOR LAB USE ONLY

Received by \_\_\_\_\_ Date/Time \_\_\_\_\_

Other POSSIBLE PRIORITY AMOUNT  
OTHER SEE VOA/TAL CONTACT NUMBER  
 (Please Specify)

WHITE - Original, to accompany samples  
 YELLOW - Field copy

\* Notified lab to add sample to analysis group. JRT 2-8-91

128A 10 85



**INTERNATIONAL  
TECHNOLOGY  
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**REQUEST FOR ANALYSIS**

R/A Control No. **208055**  
C/C Control No. **163141**

PROJECT NAME SKY HARBOR ANG DATE SAMPLES SHIPPED 6 FEBRUARY 91  
 PROJECT NUMBER 409721 LAB DESTINATION ITAS - CARROLLTON, CA  
 PROFIT CENTER NUMBER 3521 LABORATORY CONTACT MRS MARIA MILLER  
 PROJECT MANAGER DON WILSON SEND LAB REPORT TO DON WILSON  
 BILL TO IT - KNOXVILLE  
312 DIRECTORS DR.  
KNOXVILLE, TN  
 PURCHASE ORDER NO. SKC Don Wilson DATE REPORT REQUIRED 2 WEEKS  
 PROJECT CONTACT FOR TIBURSI  
 PROJECT CONTACT PHONE NO. 602/295-1325

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
M02-02-0-2-01-01-03	SOIL	3 X 6-INCH BARRIS SCANS W/ 15 MIN SWEEPERS	ICE TO 4°C	TPH, VOA, SVOA, TAL	
M02-02-0-3-01-01	↓	2 X 6-INCH BARRIS SCANS	↓	HOLD FOR INSTRUMENTS	
M02-02-0-30-01-01	↓	1 X 6-INCH BARRIS SCANS	↓	HOLD FOR INSTRUMENTS	
M02-02-0-30-01-02	SOIL	2 X 6-INCH BARRIS SCANS	ICE TO 4°C	TAL, VOA, SVOA, TAL	
M02-02-0-30-01-03	WATER	2 X 40-ML VOA	ICE TO 4°C, HCl	VOA	

TURNAROUND TIME REQUIRED: (Rush must be approved by the Laboratory Project Manager.) QC LEVEL: (Levels II and III subject to surcharge; project-specific requirements must be submitted to lab before beginning work.)  
 Normal  Rush  (Subject to rush surcharge) I  II  III  Project Specific   
 POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)  
 Non-hazard  Flammable  Skin Irritant  Highly Toxic  Other SOLVENT CONTAINERS (Please Specify) None  
 SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, archive and disposal)  
 Return to Client  Disposal by Lab  Archive  (Indicate number of months.)  
 FOR LAB USE ONLY Received by \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original, to accompany samples  
YELLOW - Field copy  
 \* Lab directed to run analyses 2/7/91 JRT



**INTERNATIONAL  
TECHNOLOGY  
CORPORATION**

**REQUEST FOR ANALYSIS**

PROJECT NAME SKY HARBOUR ANG DATE SAMPLES SHIPPED 5 FEBRUARY 91  
 PROJECT NUMBER 409721-02-06 LAB DESTINATION ITAS-CAROLINA  
 PROJECT MANAGER DON WILLIAMS LABORATORY CONTACT CHEVEL FORGANO  
 BILL TO IT-KNOXVILLE SEND LAB REPORT TO DON WILLIAMS  
312 DUNSTON RD  
KNOXVILLE, TN  
 PURCHASE ORDER NO. SEE DON WILLIAMS DATE REPORT REQUIRED 3 FEBRUARY  
 PROJECT CONTACT JOE TYRUSKI PROJECT CONTACT PHONE NO. 602/295-1925

R/A Control No. **B** 87028  
 C/C Control No. 163157

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
S81-02-05-3-01	SOIL	6-gram Plastic Sieve	Ice to 4°C	HOLD FOR INSTRUCTIONS	
S81-02-25-29-01	SOIL	6-gram Brass Sieve	Ice to 4°C	HOLD FOR INSTRUCTIONS	
S81-02-TR2	WATER/FILTRATE	2 x 40ml GALS	Ice to 4°C, HCl	VOA	

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager )  
 Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)  
 Nonhazard  Flammable  Skin Irritant  Highly Toxic

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis Lab will charge for packing, shipping, and disposal)  
 Return to Client  Disposal by Lab

FOR LAB USE ONLY  
 Received By \_\_\_\_\_ Date/Time \_\_\_\_\_  
 WHITE - Original, to accompany samples  
 YELLOW - Field copy  
 \* S. Series intended for analysis for TPH 2/22/91 Tele con.

Residue Present?   
 Other Solvents Classified? (Please Specify)



REQUEST FOR ANALYSIS

R/A Control No. B 87927  
C/C Control No. 163141

PROJECT NAME: Sky Harbor ANG  
PROJECT NUMBER: 409221  
PROJECT MANAGER: Don Wilmer  
BILL TO: IT - Knoxville  
312 DIXON DR.  
KNOXVILLE, TN  
PURCHASE ORDER NO.: See Don Wilmer  
DATE SAMPLES SHIPPED: 4 FEBRUARY 91  
LAB DESTINATION: ITAS - CHARLOTTE  
LABORATORY CONTACT: CHRIS FERGUSON  
SEND LAB REPORT TO: AT - Don Wilmer  
IT - Knoxville  
DATE REPORT REQUIRED: 3 WEEKS  
PROJECT CONTACT: Tom Tykewski  
PROJECT CONTACT PHONE NO.: 602/275-1725

Sample No	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
QC-FB5	WATER	1-LITER GLASS	HCl; 1CS 42	TPH	
		1-LITER GLASS		SVOA	
		1-LITER GLASS		TOTAL ORGANIC Ph	
		2x 40ml GLASS	HCl;	VOA	
		2x 40ml GLASS	HCl;	VINYL CHLORIDE	
		1-LITER POLY	HNO <sub>3</sub> ;	METALS (EXCEPT MERCURY)	
		1-LITER POLY	HNO <sub>3</sub> ;	MERCURY	
		1-500ml POLY	H <sub>2</sub> SO <sub>4</sub> ;	ALIBRATS/NITRATE	
QC-FB5-TB	↓	2 40ml GLASS	HCl;	VOA	
QC-FB5-TB	WATER	2-40ml GLASS	HCl;	VINYL CHLORIDE	

TURNAROUND TIME REQUIRED: (Rush must be approved by the Project Manager.)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazardous  Flammable  Skin Irritant  Highly Toxic  Other (Please Specify)

SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)

Return to Client  Disposal by Lab

FOR LAB USE ONLY Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original to accompany samples  
YELLOW - Field copy



**INTERNATIONAL  
TECHNOLOGY  
CORPORATION**

**REQUEST FOR ANALYSIS**

PROJECT NAME Sky Harbor A116  
 PROJECT NUMBER 409921.02.06  
 PROJECT MANAGER Don Wilson  
 BILL TO IT - Knoxville  
312 Diabene Dr.  
Knoxville, TN

DATE SAMPLES SHIPPED \_\_\_\_\_  
 LAB DESTINATION \_\_\_\_\_  
 LABORATORY CONTACT \_\_\_\_\_  
 SEND LAB REPORT TO \_\_\_\_\_

PURCHASE ORDER NO. See Don Wilson  
 DATE REPORT REQUIRED \_\_\_\_\_  
 PROJECT CONTACT \_\_\_\_\_  
 PROJECT CONTACT PHONE NO. 602/235-1325

R/A Control No. **B 87022**  
 C/C Control No. 163136  
30 January 91  
ITAS - CHESTER  
CHESTER BRANSON  
Don Wilson  
IT - Knoxville

3 Weeks  
Don Wilson

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
M35-03-0- L-01-02	SOIL	2x6-inch Beas Seives	ICE TO 4°C	TPH, VOA, SVOA, TAL, TOPG ALLIGATE/AUTATE	
M35-03-5- 7-01	SOIL	1x6-inch Beas Seives	ICE TO 4°C	Hold for Institutional	
M35-03-TO	WATER/TRIP BEAS	2X 40 mL	ICE TO 4°C, HCl	VOA	
		LAST LINE			

TURNAROUND TIME REQUIRED: (Rush must be approved by the Project Manager )  
 Normal  Rush \_\_\_\_\_ (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)  
 Nonhazard \_\_\_\_\_ Flammable \_\_\_\_\_ Skin Irritant  Highly Toxic \_\_\_\_\_

SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis Lab will charge for packing, shipping, and disposal)  
 Return to Client \_\_\_\_\_ Disposal by Lab

FOR LAB USE ONLY Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original, to accompany samples  
 YELLOW - Field copy

\* Continued Check Figure 2-1-41 to add sample for analysis.



**INTERNATIONAL  
TECHNOLOGY  
CORPORATION**

**REQUEST FOR ANALYSIS**

R/A Control No **B 27018**  
C/C Control No **163132**

PROJECT NAME Sky Hazine Auk  
PROJECT NUMBER 409321  
PROJECT MANAGER Bill Wilson  
BILL TO ITT-Knoxville  
312 Dabney Dr  
Knoxville, TN  
PURCHASE ORDER NO. See Bill Wilson

DATE SAMPLES SHIPPED  
LAB DESTINATION  
LABORATORY CONTACT  
SEND LAB REPORT TO  
DATE REPORT REQUIRED  
PROJECT CONTACT  
PROJECT CONTACT PHONE NO.

29 January 91  
ITAS - CHARLES  
Charles Williams  
Bill Wilson  
ITT-Knoxville  
3 weeks  
Joe T. Jensen  
602/275-1325

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
S17-01-0-2-01-02	SOIL	2 X 6-INCH BRASS SIEVES	ICE TO 4°C	TPH, VOA, SVOA, TAL	
S17-01-5-2-01		1 X 6-INCH BRASS SIEVE		HOLD FOR INSTRUCTIONS	
S17-01-10-12-01				HOLD FOR INSTRUCTIONS	
S17-01-15-13-01				HOLD FOR INSTRUCTIONS	
S17-01-50-12-01				HOLD FOR INSTRUCTIONS	
S17-01-55-52-01		1 X 6-INCH BRASS SIEVE		TPH, VOA, SVOA, TAL	SEE MASTER CONTACT IF SAMPLE VOLUME IS INSUFFICIENT
M15-01-0-2-01-02		3 X 6-INCH BRASS SIEVES		TPH, VOA, SVOA, TAL, TOPb, AARATE/AUTATE	
M15-01-60-62-01	SOIL	1 X 6-INCH BRASS SIEVE	ICE TO 4°C	TPH, VOA, SVOA, TAL, TOPb, AARATE/AUTATE	SEE MASTER CONTACT IF SAMPLE VOLUME IS INSUFFICIENT
M15-01-TB	WASTE (TRIP BURN)	2 X 40 ML	HCL; Ice to 4°C	VOA	

TURNAROUND TIME REQUIRED: (Rush must be approved by the Project Manager.)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazard  Flammable  Skin Irritant  Highly Toxic  Other POSSIBLE PERMANENT RESIDUAL CONTAMINATION (Please Specify)

SAMPLE DISPOSAL: (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)

Return to Client  Disposal by Lab

FOR LAB USE ONLY

Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original to accompany samples \* Cheryl Ferguson told toxic sample for analysis.  
YELLOW - Field copy 1/30 JET



INTERNATIONAL  
TECHNOLOGY  
CORPORATION

REQUEST FOR ANALYSIS

PROJECT NAME Sky Harbor A16 DATE SAMPLES SHIPPED 28 JANUARY 91  
 PROJECT NUMBER 409721 LAB DESTINATION ITAS - CERRITOS  
 PROJECT MANAGER Bill Winters LABORATORY CONTACT Cheryl Ferguson  
 BILL TO IT - Knoxville SEND LAB REPORT TO Bill Winters  
312 DUBLIN DR  
KNOXVILLE, TN  
See Bill Winters

PURCHASE ORDER NO. THREE WEEKS DATE REPORT REQUIRED  
 PROJECT CONTACT Joe Tysowski PROJECT CONTACT PHONE NO. 602/275-1325

R/A Control No. B 87017  
 C/C Control No. 163131

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
MDI-02-0-2-01	SOIL	6" BESS SAMPLE	ICS to 40c	TPH, VOA, SVOA	
MDI-02-0-2-02				TPH, VOA, SVOA	
MDI-02-35-33-01					HOLD FOR INSTRUCTIONS
MDI-02-60-42-01					HOLD FOR INSTRUCTIONS
MDI-02-75-72-01	SOIL	6" BESS SAMPLE		TPH, VOA, SVOA	See Project Contact for Special Instructions
MDI-02-73	WATER	2X 40ML	HCl, ICS to 40c	TPH, VOA, SVOA	

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION. (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazardous  Flammable  Skin Irritant  Highly Toxic  Other  (Please Specify)

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)

Return to Client  Disposal by Lab

FOR LAB USE ONLY Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original to accompany samples  
 YELLOW - Field copy

\* Cheryl Ferguson indicated to analyze sample  
 1/30 JFR



# REQUEST FOR ANALYSIS

R/A Control No. **179885**  
C/C Control No. \_\_\_\_\_

PROJECT NAME SKY HARBOR ANG  
PROJECT NUMBER 409771  
PROJECT MANAGER DON WILLEN  
BILL TO IT CORPORATION  
312 ~~BRIDGE~~ DIRECTORS DR.  
KNOXVILLE, TN 37901  
PURCHASE ORDER NO Site Don Willess

DATE SAMPLES SHIPPED \_\_\_\_\_  
LAB DESTINATION \_\_\_\_\_  
LABORATORY CONTACT \_\_\_\_\_  
SEND LAB REPORT TO \_\_\_\_\_  
DATE REPORT REQUIRED 3 WEEKS  
PROJECT CONTACT J. TY BURSKI  
PROJECT CONTACT PHONE NO. 602/275-1325

Sample No	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
S81-03-55-57-01	SOIL	6" Brass Sleeve	Ice to 4°C	TPH, VOA, SVOA	
S01-03-55-58-02				↓	
S03-02-55-57-03				TPH, VOA, SVOA	MATRIX SPIKE & MATRICES
S82-02-0-2-01				TPH, VOA, SVOA, TAL	
S02-02-8-4-01				HOLD FOR INSTRUCTIONS	←
S02-02-10-12-01				HOLD FOR INSTRUCTIONS	←
S02-02-40-41-01				HOLD FOR INSTRUCTIONS	←
S02-02-50-52-01				HOLD FOR INSTRUCTIONS	←
S02-02-55-58-01				HOLD FOR INSTRUCTIONS	←
S02-02-60-72-01	SOIL	6" Brass Sleeve	Ice to 4°C	TPH, VOA, SVOA, TAL	

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazardous  Flammable  Skin Irritant  Highly Toxic  Other  (Please Specify)

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis Lab will charge for packing, shipping and disposal)

Return to Client  Disposal by Lab

FOR LAB USE ONLY Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original, to accompany samples  
YELLOW - Field copy

\* Directed by (Jones Martin) to analyze 1-23-41





**INTERNATIONAL  
TECHNOLOGY  
CORPORATION**

**REQUEST FOR ANALYSIS**

R/A Control No. **B 37010**  
C/C Control No. **143034**

PROJECT NAME Sty Huber ANG  
PROJECT NUMBER 409721  
PROJECT MANAGER Don Willey  
BILL TO ITT Corp  
312 Directors Drive  
Knoxville, TN  
See Don Willey

DATE SAMPLES SHIPPED  
LAB DESTINATION Cerritos, CA  
LABORATORY CONTACT Cheryl Ferguson  
SEND LAB REPORT TO Don Willey

PURCHASE ORDER NO. \_\_\_\_\_  
DATE REPORT REQUIRED 2-11-91  
PROJECT CONTACT J. Tyburski  
PROJECT CONTACT PHONE NO. 602-235-1325

Sample No	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
SBI-03-15-13-01	SOIL	6" BRASS SLEEVE	ICE TO 40%	TPH, <del>SO4</del> VOA, SVOA	HOLD FOR INSTRUCTIONS
SBI-03-20-22-01					HOLD FOR INSTRUCTIONS
SBI-03-35-33-01					
SBI-03-35-34-01	SOIL	6" BRASS SLEEVE	ICE TO 40%	TPH, UOA, SVOA	
SBI-04-TB	WATER	2 x 40 ml	HCl, Ice to 40%	VOA	

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager)  
Normal  Rush \_\_\_\_\_ (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)  
Non-hazardous \_\_\_\_\_ Flammable \_\_\_\_\_ Highly Toxic \_\_\_\_\_  
Skin Irritant

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)  
Return to Client \_\_\_\_\_ Disposal by Lab

FOR LAB USE ONLY  
Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original, to accompany samples  
YELLOW - Field copy

\* Directed Lab (Same, Marti) to analyze 1-23-91.



**INTERNATIONAL  
TECHNOLOGY  
CORPORATION**

**REQUEST FOR ANALYSIS**

R/A Control No. **179883**  
C/C Control No. **105473**

PROJECT NAME SKY HAWK AVE ANG  
PROJECT NUMBER 409721-02.06  
PROJECT MANAGER DON WILSON  
BILL TO IT - KNOXVILLE  
312 DUFFORDS RD.  
KNOXVILLE, TN 37901  
PURCHASE ORDER NO. SEE DON WILSON

DATE SAMPLES SHIPPED 1/18/91  
LAB DESTINATION ITAS - CERRITOS, CA  
LABORATORY CONTACT CHRISTY FEAGAN  
SEND LAB REPORT TO DON WILSON  
IT - KNOXVILLE  
↓  
STANDARD  
PROJECT CONTACT JOE TRIGUASIL  
PROJECT CONTACT PHONE NO. 602/295-1325

Sample No	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
SD1-05-01-01	SOIL	6 INCH BATHS SIEVE	ICE TO 4°C	TPH, VOA, SVOA	Hold for instructions
SD1-05-01-02					Hold for instructions
SD1-05-01-03					Hold for instructions
SD1-05-01-04					Hold for instructions
SD1-05-01-05					Hold for instructions
SD1-05-01-06					Hold for instructions
SD1-05-01-07					Hold for instructions
SD1-05-01-08					Hold for instructions
SD1-05-01-09					Hold for instructions
SD1-05-01-10					Hold for instructions
SD1-05-01-11					Hold for instructions
SD1-05-01-12					Hold for instructions
SD1-05-01-13					Hold for instructions
SD1-05-01-14					Hold for instructions
SD1-05-01-15					Hold for instructions
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SD1-05-01-94					Hold for instructions
SD1-05-01-95					Hold for instructions
SD1-05-01-96					Hold for instructions
SD1-05-01-97					Hold for instructions
SD1-05-01-98					Hold for instructions
SD1-05-01-99					Hold for instructions
SD1-05-01-100					Hold for instructions

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazardous  Flammable  Skin Irritant  Highly Toxic

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)

Return to Client  Disposal by Lab

FOR LAB USE ONLY

Received By \_\_\_\_\_ Date/Time \_\_\_\_\_  
WHITE - Original, to accompany samples  
YELLOW - Field copy  
\* Analyze for indicated (i.e., Lab notified 1-21-91 JRT



REQUEST FOR ANALYSIS

R/A Control No. 1798880  
C/C Control No. 105428

PROJECT NAME: Sky Harbor ANG  
PROJECT NUMBER: 409721  
PROJECT MANAGER: Don Willen  
BILL TO: IT Corp  
312 Purcellville Drive  
Purcellville, VA 90701  
PURCHASE ORDER NO.: Contract D.Willen  
DATE REPORT REQUIRED: J. Tyburst  
PROJECT CONTACT: J. Tyburst  
PROJECT CONTACT PHONE NO.: 602-275-1325

DATE SAMPLES SHIPPED: 1/18/91  
LAB DESTINATION: Carsonville, CA  
LABORATORY CONTACT: Cheryl Ferguson  
SEND LAB REPORT TO: Don Willen

Sample No.	Sample Type	Sample Volume	Preservative	Requested Testing Program	Special Instructions
01-FBI	Water	1-liter amber	NA / 4°C	Organic Lead	
02-FBI	Water	2-40ml glass	HCL / 4°C	VOA	
03-FBI		2-40ml glass	HCL / 4°C	Vinyl chloride	
04-FBI		1-liter amber	4°C	Flammable Organics	
05-FBI		1-liter poly	HNO3 / 4°C	Metals (except Arsenic)	
06-FBI		1-liter poly	HNO3 / 4°C	Mercury	
07-FBI		1-liter amber	HCL / 4°C	TPH	
08-FBI		1-40ml glass	HCL / 4°C	DTX, PCN, ILI, DTE	
09-FBI		1-500ml poly	H2SO4 / 4°C	Nitrates / Nitrites	
10-FBI-TB		2-40ml glass	HCL / 4°C	Triphenyltin VOA	

TURNAROUND TIME REQUIRED (Rush must be approved by the Project Manager)

Normal  Rush  (Subject to rush surcharge)

POSSIBLE HAZARD IDENTIFICATION: (Please indicate if sample(s) are hazardous materials and/or suspected to contain high levels of hazardous substances)

Nonhazardous  Flammable  Skin Irritant  Highly Toxic  Other (Please Specify)

SAMPLE DISPOSAL (Please indicate disposition of sample following analysis. Lab will charge for packing, shipping, and disposal.)

Return to Client  Disposal by Lab

FOR LAB USE ONLY  
Received By \_\_\_\_\_ Date/Time \_\_\_\_\_

WHITE - Original, to accompany samples  
YELLOW - Field copy  
\*Cancelled SPT 1-21-91, Lab note field.

Fr.  
3-22-91

Weather: Clearing today 50°F cal - in AM. Afternoon  
partly cloudy, 65°F, cal -

IT Personnel: M. Gardiner, D. Schapp, B. Wilkins, J. Tyburati

Visitors: MMES - D. Bunn, F. Lebow

Layne - P. Peterson, B. Shrum, W. Williams, M. Phillips

- Arrive at Base at 0630. MMES visitors arrive at  
0715. Tailgate Safety Mtg. held w/ IT & MMES.

• Contacted Marla Miller (Cerritos) to verify receipt  
of samples shipped 3-21-91. Directed Marla to  
analyze MBS-04-99-01 for TPH, TORB, VOA, & SVOC.

• Drilled and sampled well MW3-01. Sampled well to  
70ft, drilled to total depth of 100ft, set  
screen and well casing.

• Collected three samples of spoils, one each  
from well PS-1, PS-2, and PS-3. Samples shipped  
on Fed Ex waybill no. 0144320120.

• Collected equipment rinsewater sample no. QC-ER14 from  
sampler at well MW3-01. Sample shipped on above  
waybill.

Mon  
3-25-91

Weather: Overcast 55°F in AM; PM clearing, 75°F

IT Personnel: M. Gardner, B. Williams, D. Schamp,  
J. Tyburst.

Visitors: Layne - D. Peterson, W. Williams, M. Phillips  
MMES - D. Bunn

Arrive at Base at ~~07~~ 0630.

• Contacted Marla Miller (Cerritos) to verify receipt of samples shipped Friday. Instructed Marla to run sample MB3-01-50-51½-01 for VOA, SVOA, TOPb, & TPH.

• Notified Lab to expect large number of samples collected Sat, Sun, & Mon for Tues delivery.

• Completed drilling and sampling soil boring SB3-04 to approx. 74 ft. Completed drilling and sampling SB3-03 to approx. 73 ft.

• Spoke with Steve Sines about various sampling issues at site:

- Third soil boring at site 3 will be last one
- Five poly tanks on site will be sampled for VOC & TPH for disposition of water.
- Piezometer PS-2 will be sampled and analyzed for Site 3 parameters.

Tues  
3-26-91

Weather: AM 5-10 mph, intermittent heavy rain;  
clearing PM intermittent drizzle 60°F

IT Personnel: M. Gardiner, B. Wilkins, D. Schamp, J. Tybuck

Visitors: W. Williams, D. Peterson, M. Phillips, Sugg,  
O. DeLaughter.

· Arrive at Base at 0630.

· Verified receipt of large sample shipment with  
Marla Miller (IT-Cerritos). Directed Marla to  
analyze sample SB3-03-10-11½-01,02 for VOA, SVOA,  
TOP6 and TPH.

· Notified Marla Miller (IT-Cerritos) of error in samples  
shipped yesterday. Sample SB3-04-15-16½-01 was  
included in shipment but was not noted in RFA or  
Chain of Custody. Sample will be analyzed for  
VOA, SVOA, TOP6, & TPH. (Reference - Telecom - JRT  
to Marla Miller 3/26/91).

· Developed monitor well MWS-04 by surging,  
bailing, and pumping. Purged approx 210 gallons  
from well. Well developed strong hydrocarbon odor,  
suspect approx 0.01 ft of PSH in well.

· Terminated well development due to weather  
conditions; will resume Wednesday.

Depart Base at 1815 for Fed Ex. Boyd &  
Gardiner depart Base at 1900.

Thurs  
4-4-91

Weather - AM - clear, high clouds 65°F, PM - slight  
breeze, 94°F.

IT Personnel - J. Boyd, M. Gardiner, J. Tyburski

- Arrive at Base at 0630. Prep materials and truck for sampling at Site 4 (Papago).
- Arrived at Site 4 at 0830 and set-up at well MW4-01. Well was bailed dry within approx. 1 hr. Returned Shrs later and were able to pull an additional  $\frac{1}{2}$  gallon. Total volume purged approx. 13 gallons, one well volume for current water level. Will discuss with IT Knoxville as to procedure for sampling this very slow producing well.
- Purged and sampled well MW4-02. This sample and samples identified 43-91 were shipped Fed Ex on waybill no. 0098749770.
- Collected bailer equipment rinsate no. QC-ER20 and shipped on above waybill no.

Notified Kim Laisy - IT - Middlebrook Lab of samples to expect Friday.

Replaced air compressor. Installed in-line filter to help reduce clogging of pump piston.

Notified by Middlebrook Lab that Friday samples received Saturday were at 10-17°C. Procedure will be changed to use an ice bath in coolers to help chill samples before refrigeration.

Depart site at 1700.

Tues  
4-9-91

Weather: AM - Clear, calm 62°F PM - 92°F

IT Personnel: J. Boyd, M. Gardiner, J. Tyburski

Arrive at Base at 0630. Prep equipment for purging by bailer and sampling PS-2. One well volume will be removed from well based on discussion of S. Sares and B. Stanley (Hazwup).

Telex from S Sares - Notified that all previous samples (except for samples shipped Mon 4-8) were 6-8°C above specified 4°C. Hazwup has directed all previous wells to be resampled. If samples cannot be chilled adequately they will be held overnight in refrigerator. Measured refrigerator with electronic temp probe, at 4.6°C which is fairly close. Turn refrigerator down slightly.





INTERNATIONAL  
TECHNOLOGY  
CORPORATION

# NONCONFORMANCE REPORT

NR NO. 4

PROJECT AZANG Sky Harbor

PAGE      OF     

PROJECT NO. 409721

DATE: 03/04/91

## 1. NONCONFORMANCE DESCRIPTION

**Problem:** No sensitivity of PID detector for TCA, after finding that TCA and DCE are not co-eluding as originally thought.

**Criteria:** Scope of work required analysis of samples and reporting contamination concentration for TCA.

**Impact:** Reported concentration for DCE will change along with detection limits; will not be able to report confident TCA values.

IDENTIFIED BY: D. Pray DATE: 02/02/91

## 2. PROPOSED CORRECTIVE ACTION, INCLUDING INITIATION AND COMPLETION DATES

Continue program on present course, at end of project re-integrate DCE values. review FID response for TCA and see if its possible to determine TCA concentration from FID.

TO BE PERFORMED BY: D. Pray 02/21/91 - 03/04/91

## 3. APPROVAL FOR PROPOSED CORRECTIVE ACTION

[Signature] 2/21/91  
Project Manager / Date  
[Signature] 2/29/91  
Quality Assurance Manager / Date

## 4. CORRECTIVE ACTION TAKEN (IF DIFFERENT FROM THAT PROPOSED)

Same as above. DCE values were reintegrated and corrected values reported, TCA detection limit for FID was high and resulting curve was poor and inconsistent. Results reported with unique qualifier.

## 5. CORRECTIVE ACTION COMPLETE

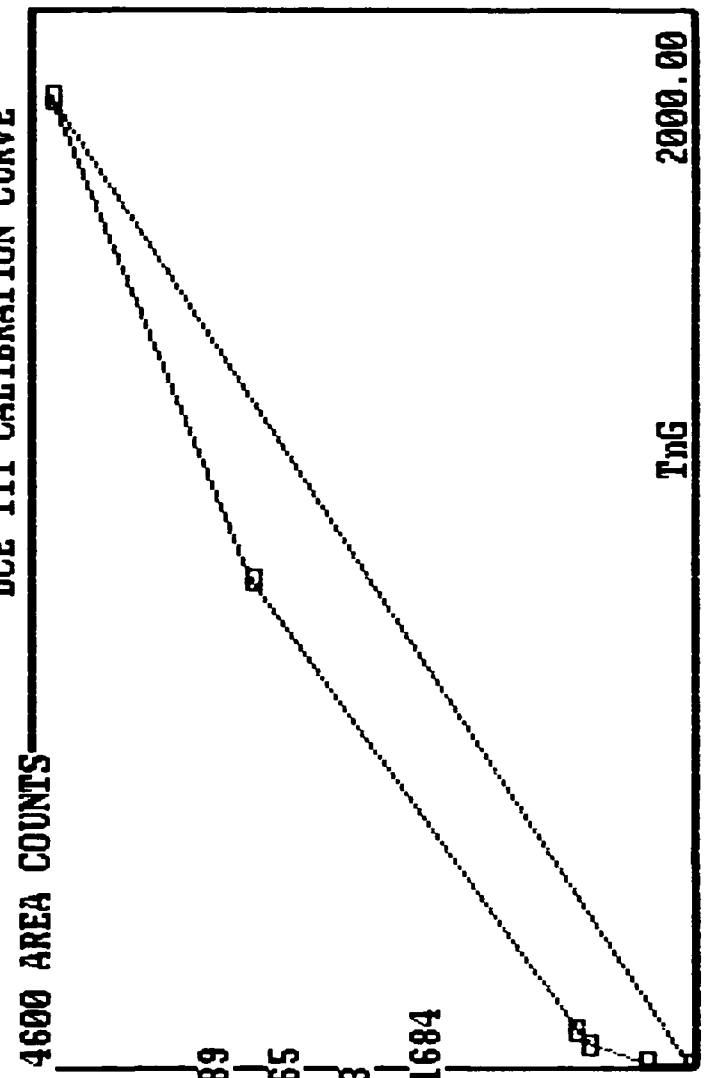
PERFORMED BY: D. Pray DATE: 03/04/91  
VERIFIED BY: [Signature] DATE: 3/1/91

- CC: PROGRAM MANAGER
- PROJECT MANAGER
- QUALITY ASSURANCE MANAGER
- QUALITY ASSURANCE COORDINATOR
- CENTRAL FILES \_\_\_\_\_
- OTHER: \_\_\_\_\_

LOCATION HISTORY FOR PEAK IDENTIFIED AS DCE III  
 #01 CAL.PMT.CAL.AREA DUF.PMT.CUR.AREA EXP.MAT.PCT.MAT.#01

*03/04/91  
 cur.ck  
 DCE only*

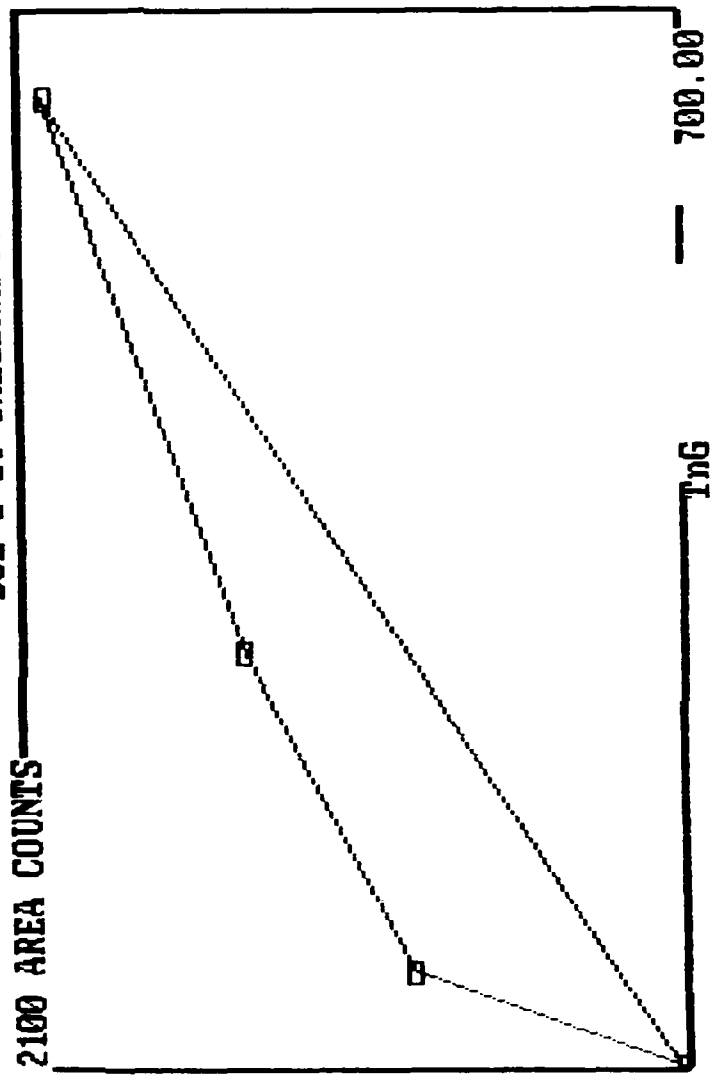
DCE III CALIBRATION CURVE



AMOUNT	AREA	SLOPE	Y-INT
1 ) 1	300	%300.00	0
2 ) 36.8	691.47	10.9289	
3 ) 64.4	786.56	3.4565	
4 ) 920	3087.6	2.7613	
5 ) 1840	4491.47	1.51684	
6 ) 0	0	2.4	0
7 ) 0	0	2.4	0
8 ) 0	0	2.4	0

08/14 CAPOK + PCA  
DCE

DCE 1-19 CALIBRATION CURVE



1 )	64.4	862.79
2 )	276	1401.95
3 )	644	2037.09
4 )	0	0
5 )	0	0
6 )	0	0
7 )	0	0
8 )	0	0

**APPENDIX B**

**PRELIMINARY REVIEW OF HYDROGEOLOGIC  
DATA FOR FACILITIES ADJACENT TO  
SKY HARBOR AIR NATIONAL GUARD BASE**

To Don Willen, Project Manager Date September 18, 1990

From Steve <sup>SUB</sup>Sares, Principal Hydrogeologist

Subject Preliminary Review of Hydrogeologic Data for Facilities  
Adjacent to Sky Harbor Air National Guard Base

## I. INTRODUCTION

In accordance with your request, I have prepared a brief summary of data collection activities and analysis of hydrogeologic data for facilities adjacent to the Sky Harbor Air National Guard facilities at the Phoenix, Arizona Airport (the Base). These activities and preliminary conclusions regarding the hydrogeology of the vicinity are presented below.

The goal of this data collection and review effort is to aid in determining appropriate monitoring-well placement and design specifications for wells to be installed during the Base Site Investigation (SI). As you are aware, there has been much discussion of appropriate depth, screen interval, and location for the SI monitoring wells.

Data collection activities for this task were conducted between July 9 and 11, 1990 and consisted of locating and obtaining available potentiometric records for facilities generally within one and one-half miles of the Base. Field activities such as verification of well locations or measurement of water levels were not conducted during data collection activities. All findings presented below are based on the assumption that data collection, reduction, calculation, and presentation contained in the records are accurate and complete. Records were obtained from the following agencies:

City of Phoenix Environmental Services Department

Arizona Department of Environmental Quality (ADEQ)

Arizona Department of Water Resources (ADWR)

In addition, a Remedial Investigation report was located at a public library which contained hydrogeologic information relevant to the Air National Guard facilities at the Papago Military Reservation (Papago). The sources of information and relevant hydrogeologic information are further discussed below.

## II. DATA SOURCE BIBLIOGRAPHY

Six primary sources of information were identified and evaluated in this effort. Selected pages of reports and files were extracted and copied from the sources listed below:

- A. Summary of the Phase II Site Investigation for the City of Phoenix at the West Sky Harbor Fuel Storage Facility and Vicinity, Phoenix Sky Harbor International Airport, Phoenix, Arizona. (May 31, 1990), Groundwater Technology, Inc. Received from Mr. Donn Stoltzfus, City of Phoenix.
- B. ADEQ files for Avis Sky Harbor, ADEQ File No. 4715.122. Received from Mr. Douglas Jamison, ADEQ.
- C. ADEQ files for Garrett General Aviation Services Division, ADEQ File No. 4715.355. Received from Mr. Douglas Jamison, ADEQ.
- D. Draft Remedial Action Plan for Del Rio Landfill, City of Phoenix, Arizona (February 23, 1990), Dames and Moore. Received from Mr. Donn Stoltzfus, City of Phoenix.
- E. Estes Landfill Hydrogeology. Received from Mr. Donn Stoltzfus, City of Phoenix.
- F. Remedial Investigation Report, 52nd Street RI/FS, Phoenix, Arizona for Motorola, Inc. (June 1987), Dames and Moore. Copy at Saguaro Library, Phoenix, Arizona.

In addition to the above referenced documents, several others were reviewed and received from the agencies listed above. Information in the additional documents either duplicated information presented below or are for facilities remote from the Base. Mr. David Annis of the ADWR also provided much valuable discussion regarding facilities and history of hydrogeologic investigations in the area adjacent to the Base.

## II. FINDINGS

Results of the hydrogeologic investigation at the Sky Harbor fuel facilities (Reference A) are likely to be directly applicable to the SI as the fuel facilities are located approximately 4,300 feet (0.8 miles) from the center of the Base on a bearing of fifty degrees west of north (N 50 W). These findings are summarized below.

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Five monitoring wells, 90 feet deep, were installed at the site in March and April 1990. The water level in each well is approximately 71 feet below grade or at an elevation of 1,038 to 1,036 feet above Mean Sea Level (feet MSL).

Detailed casing elevations and depth to water were not included in the information provided, however, a site gradient map indicates a due westerly groundwater flow direction at a gradient of approximately 0.002 or 10.9 ft per mile.

Lithologic logs indicate mixed, unindurated alluvium at the site consisting generally of sand to silt in the 0-5 foot depth interval, sand to pebbles in the 5-15 foot interval, and sand to cobbles below 15 feet.

Avis Car Rental facility at Sky Harbor is conducting an investigation for a fuel release (Reference B). The Avis facility is located approximately 7,600 feet (1.4 miles) from the center of the Base on a bearing of N 82 W. Findings from these files are summarized below.

The depth to water, measured on 24 Nov 87 ranges from 61.26 to 64.51 feet below the surface, this corresponds to an approximate elevation of 1,035 to 1,039 feet MSL.

The groundwater flow direction at the site is generally west with the flow direction diverging to northwest and southwest west of the Avis site. Reports suggest that the divergence may be caused by an Arizona Department of Transportation (ADOT) dewatering project located in line with 21st Street between Buckeye Road and the Salt River.

The ADOT project was in operation at the time the material in the files was prepared (1987). At that time the dewatering system consisted of 11 wells each pumping at approximately 1,500 gallons per minute.

The U.S. Geological Survey (USGS) conducted a pump test during the dewatering project and determined the aquifer transmissivity (T) to be 194,000 GPD/ft, and hydraulic conductivity (K) to be 1,200 GPD/ft, using a saturated thickness of 150 feet.

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Garrett General Aviation Services Division operates a facility located approximately 6,300 feet (1.2 miles) southwest of the center of the Base on a bearing of S 73 W. This facility is conducting an investigation for fuel and solvent release (Reference C). Findings from the Garrett files are summarized below.

The depth to groundwater was measured to be approximately 55.5 to 57.9 feet below grade or at an elevation of 1,044 to 1,042 feet MSL on 5 Dec 88.

Garrett has presented the groundwater flow direction to be northwesterly (N 36 W). The ADEQ disagrees with this interpretation and states that the ground water flow direction at Garrett is North 80 East. This direction is inconsistent with the regional flow direction as indicated by all other references from the area. I have reviewed the available potentiometric data at Garrett and the flow direction, based on three-point solutions ranges from N 15 W to S 36 E depending on the combination of wells used. Thus the data from Garrett appears inconsistent and should not be relied upon for the Base SI.

The City of Phoenix owns a landfill located approximately 14,600 feet (2.8 miles) southwest of the Base on a bearing of S 74 W. This landfill is called the Del Rio or 16th Street landfill and it is located on the south edge of the Salt River (Reference D). Findings from the files are presented below.

Depth to groundwater is typically 35 to 40 feet below ground level or at an elevation of 1,045 to 1,040 feet MSL.

Water levels in wells have demonstrated fluctuation of up to 28.7 feet in a single well over a period of ten years. The peak water level (all wells) was 1,055.6 feet MSL (approximately 24 feet below ground level). The minimum water level over the same period was 1,020.51 feet MSL (approximately 59.5 feet below ground level).

Hydrographs for monitoring wells over the period from 1979 to 1990 indicate that water elevations in wells in the period 1986 to 1990 are at the lower end of the range (1,025 to 1,045) while during the period 1983 to 1986 they were in peak ranges (1,055 to 1,045). In general, water levels in these wells have declined approximately 20 feet from the 1983 peaks to the 1990 lows or an average of 2.8 feet per year. Prior to the 1983 peak levels, water levels were in the 1,030 foot range as late



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as 1982. Water levels in monitoring wells demonstrate a strong correlation to flows in the Salt River, thus a continued decline in water levels cannot be projected.

Reference D provided several potentiometric maps for the Del Rio Landfill. These maps were prepared by the authors of the report by unknown means. Based on the maps presented, the groundwater flow direction averages a bearing of N 60 W (300 degrees azimuth) for nine maps presented in the report under dry river conditions. One potentiometric map representing conditions of flow in the river was also presented, the groundwater flow direction in this case was S 57 W (213 degrees azimuth).

The City of Phoenix also owns another landfill southeast of the Base. The Estes Landfill is located approximately 6,500 feet (1.2 miles) from the Base on a bearing of S 82 E (Reference E).

Depth to water at the Estes Landfill is typically 40 to 60 feet below ground level or at an elevation of 1,080 to 1,060 feet MSL.

Water levels in monitoring wells also fluctuate in association with flow in the River at the Estes Landfill. The maximum fluctuation observed in a single well over a period of seven years is 43.77 feet. The peak groundwater elevation in all wells is 1,111.5 feet MSL (approximately 20 feet below ground level). The minimum water level in all wells was 1,038.63 feet MSL (84 feet below ground level).

Potentiometric data from shallow and deep wells suggest a downward vertical gradient at the Estes Landfill, however, lack of well specifications in the information presented prohibits analysis of the vertical gradient conditions.

The groundwater flow direction from prepared maps reviewed averages S 83 W during dry conditions in the river. One map presented for streamflow conditions depicts a groundwater flow direction of S 51 W.

The Motorola facility is located approximately 3000 feet (0.6 miles) on a bearing of S 15 W from ANG facilities at the Papago Military Reservation. Findings from review of Reference F are presented below.

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Depth to water at the Motorola facility is approximately 22 feet below the ground level or at an elevation of 1,198 feet MSL.

Hydrograph records for well DM101 (nearest to Papago) indicate a maximum fluctuation of five feet, primarily in response to precipitation. The peak water level in this well was 17.5 feet below the top of casing and the minimum measured was 23 feet below the top of casing.

Groundwater flow direction in the shallow portions of the aquifer is approximately S 70 W.

Alluvium overlies volcanic bedrock to a depth of approximately 26 feet. The alluvium thins to the north and west and may be thinner at ANG facilities at Papago.

### III. DISCUSSION AND CONCLUSIONS

#### A. MONITORING WELL SCREEN INTERVAL

##### Sky Harbor

The Base is located in an area with ground elevation of approximately 1,110 feet MSL. The current monitoring well design calls for 50 feet of screen to be placed 30 feet below the ambient water table and 20 feet above the water table.

Data from the Sky Harbor fuel facility investigation and other sites in the area suggest that the water table will be encountered at a depth of approximately 70 feet below the surface or at an elevation of 1,040 feet MSL. This configuration will require soil borings to be extended to approximately 100 feet below the ground surface for well construction. The well bottom will be located at an elevation of approximately 1,010 feet MSL and the top of the screen interval will be approximately 50 feet below ground or 1,060 feet MSL.

Using data from the Del Rio Landfill (Reference D) during periods of prolonged flow in the Salt River, water levels may be expected to rise as much as 20 to 25 feet. Assuming a 20 foot rise in the water table due to flow in the river, the water table elevation at the Base would be approximately 1,060 feet MSL. This is at the level of the top of screen in proposed monitoring wells. Based on this scenario, it may be prudent to set the top of screen at an elevation of 1,065 or 25 feet above the expected water table.

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A screen length of 50 feet would place the bottom of the well at 1,015 feet or 25 feet below the expected water table. Assuming five feet of saturated well are required for representative samples to be collected, the water table could go as low as 1,020 feet and the wells would remain useful. This is approximately the lowest level recorded at any of the surrounding areas, the 1,020 level also represents over seven years of useful life at an average water table decline rate of 2.8 feet per year. The 50-foot-long screen proposed should be adequate for the objectives of the SI and future use.

#### Papago

The current proposed monitoring well design for Papago wells is the same as the wells designed for the Base; thirty feet of screen to be placed within the water table. Given the information presented in Reference F, above, it is likely that upon completion of piezometers at Papago and measurement of water levels, it will be desirable to modify the screened interval to allow 15 feet below and five to ten feet above the water table. This interval should be sufficient to accommodate anticipated water-level fluctuations.

#### B. MONITORING WELL PLACEMENT

##### Sky Harbor

Proposed monitoring well locations for the Base SI were developed assuming a westerly (N 90 W) groundwater flow direction. The possibility of significant deviation from this direction motivated the collection of existing data to verify the assumption of westerly groundwater flow.

Because the potentiometric data obtained during this effort were not collected from a single point in time, they cannot be used in preparation of an area potentiometric map, therefore accurate prediction of groundwater flow direction for the base cannot be made.

Generally, published groundwater flow directions are in a westerly (S 83 W) to northwesterly (N 60 W) direction during no-flow conditions in the Salt River. The exceptions to this condition are during flow in the river and one combination of water levels at the Garrett Aviation facility. Groundwater flow direction during river flow is discussed below. The Garrett data are inconsistent, using the same four data points groundwater flow direction variation of

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140 degrees can be obtained. It is advisable not to utilize this data in placement of SI wells unless separate conformation of easterly flow directions can be made.

The available data indicate that during periods of river flow, the groundwater gradient on the south side of the river is in a southwesterly direction (S 57 W to S 51 W). It follows, assuming flow in the river creates a mound in the water table coincident with the axis of the river, that the groundwater flow direction north of the river would be in a northwest (N 57 W to N 51 W) direction during periods of river flow.

Using the above discussion it is reasonable to assume that groundwater flow direction around the Base is primarily westerly, with a maximum northerly component of 30 degrees north of west during no-flow in the river and a maximum northerly component of 39 degrees during periods of flow in the river. Given this analysis it is recommended that the initial plan of piezometer installation and flow direction determination prior to well placement be adhered to for the SI. It may be prudent to periodically measure water levels in elevation-surveyed wells from surrounding facilities to develop an area potentiometric map during the SI. Any offsite monitoring should be limited to facilities within a one and one-half to two mile radius of the Base.

#### Papago

Proposed monitoring well locations for Papago were developed assuming a westerly groundwater flow direction. Should piezometric information agree with the data contained in Reference F, indicating a southwesterly flow direction, it may be desirable to relocate well MW4-03 to the west side of Building 112. However this determination should be postponed until site-specific potentiometric data are available.

**APPENDIX C**  
**GEOPHYSICAL SURVEY REPORT**

**GEOPHYSICAL INVESTIGATION**

**161 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA**

**PROJECT NO. 409721**

**PREPARED BY:**

**IT CORPORATION  
17461 DERIAN AVENUE, SUITE 190  
IRVINE, CALIFORNIA 92714**

**SEPTEMBER 1991**

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2.2 Geophysical Survey: Site 5 - Ammunition Disposal Area	2
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4.0 Discussion and Results	4
5.0 Conclusions	5
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Appendix B - Electromagnetic Induction Profiles	
Appendix C - Sample Ground Penetrating Radar Records	

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1	Geophysical Survey Area
2	Geophysical Interpretation Map



# GEOPHYSICAL SURVEY

## **1.0 Introduction**

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A geophysical survey was conducted from December 13 to 23, 1990 at Sky Harbor International Airport (IAP) in Phoenix, Arizona. The survey was conducted in two phases. The first phase involved the geophysical clearance of all proposed soil organic vapor (SOV) sampling points and soil boring and monitoring well locations of underground pipelines and utilities at Site 1 (JP-4 Hydrant Area), Site 2 (Hazardous Waste Storage Area), Site 3 (Fuel Bladder Area), Site 4 (107TCS Hazardous Waste Collection Area), and Site 5 (Ammunition Disposal Area). Electromagnetic (EM) utility locators and ground penetrating radar (GPR) methods were used during this phase of the investigation.

During the second phase of the geophysical investigation, EM and GPR surveys were conducted at Site 5 to locate buried ammunition. In 1980, live 50-caliber ammunition was discovered in excavations during installation of a closed circuit television (CCT) system (AZANG, 1990). Ammunition was found in two areas shown in Figure 1. The Preliminary Assessment (PA) reported that ammunition was found at depths ranging from 6 to 8 feet at a location approximately 50 feet south of the CCT trench locations (HMTC, 1988).

The locations of the Site 5 EM and GPR surveys are shown in Figure 1. Several modifications to the original survey design were necessary based on unanticipated field conditions. As originally planned, magnetic and EM surveys were to be the primary means of locating buried ammunition with the use of GPR restricted to problem areas or areas requiring additional data. However, due to the abundance of surface structures, vehicles, and underground utilities, EM surveying was conducted only in areas relatively uncongested with metallic material. The magnetic survey was not performed because of interference from unwanted sources over much of the area of the site. As a consequence, GPR was used as the primary exploration tool. In addition, the EM survey was extended 130 feet to the west to include a more open area approximating background soil conductivity conditions.

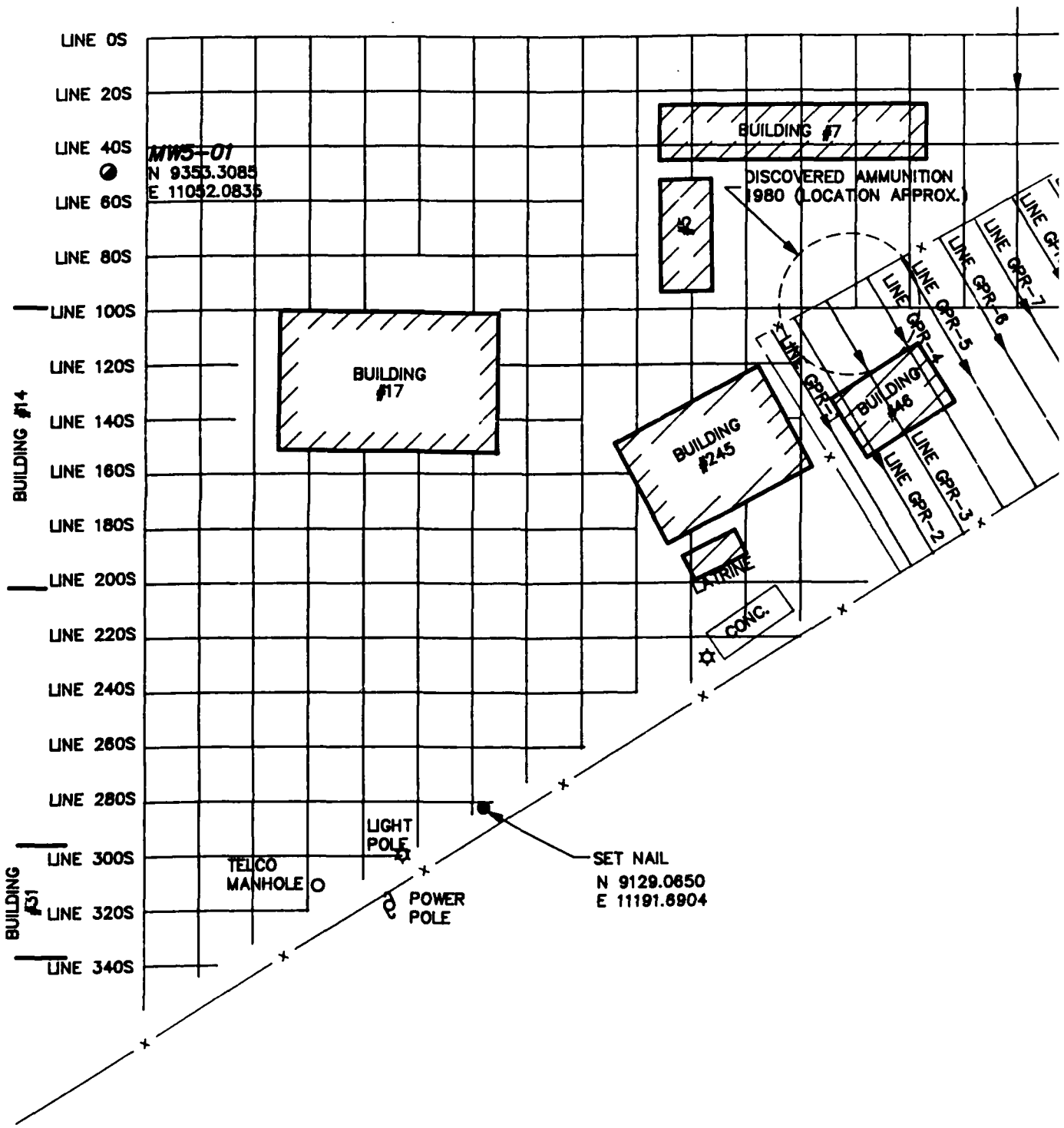
## **2.0 Field Procedures**

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This section describes the field procedures used for the geophysical clearance and the

AIRCRAFT PARKING AREA

- LINE 0E
- LINE 20E
- LINE 40E
- LINE 60E
- LINE 80E
- LINE 100E
- LINE 120E
- LINE 140E
- LINE 160E
- LINE 180E
- LINE 200E
- LINE 220E
- LINE 240E
- LINE 260E
- LINE 280E
- LINE 300E
- LINE 320E



LINE 0S  
 LINE 20S  
 LINE 40S  
 LINE 60S  
 LINE 80S  
 LINE 100S  
 LINE 120S  
 LINE 140S  
 LINE 160S  
 LINE 180S  
 LINE 200S  
 LINE 220S  
 LINE 240S  
 LINE 260S  
 LINE 280S  
 LINE 300S  
 LINE 320S  
 LINE 340S

BUILDING #14  
 BUILDING #31

MWS-01  
 N 9353.3085  
 E 11052.0835

BUILDING #7

DISCOVERED AMMUNITION  
 1980 (LOCATION APPROX.)

BUILDING #17

BUILDING #245

BUILDING #48

EXTRINE

CONC.

SET NAIL  
 N 9129.0650  
 E 11191.6904

TELCO  
 MANHOLE

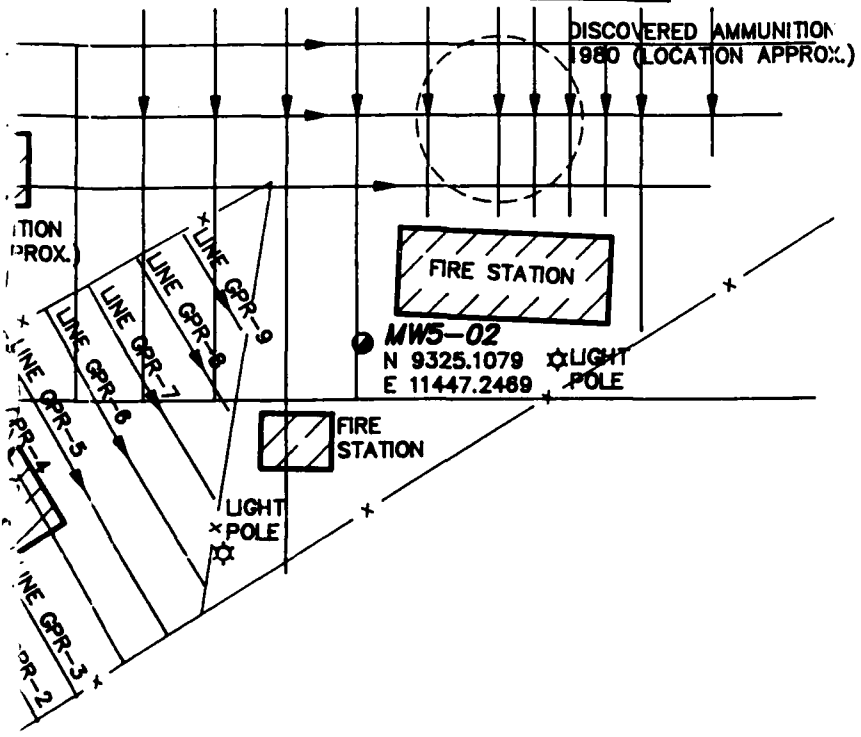
LIGHT  
 POLE

POWER  
 POLE

LINE GPR-1  
 LINE GPR-2  
 LINE GPR-3  
 LINE GPR-4  
 LINE GPR-5  
 LINE GPR-6  
 LINE GPR-7

LINE 300E  
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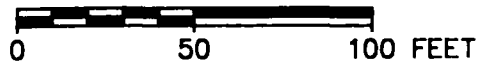
SET CONCRETE  
 NAIL & SHINER  
 N 9405.9349  
 E 11659.5025



**LEGEND:**

- ☆ LIGHT
- MANHOLE
- MONITORING WELL
- ➔ GPR SURVEY LINE WITH TRAVERSE DIRECTION
- GEONICS EM-31 SURVEY LINE

**SCALE:**



**FIGURE 1**  
**SITE 5-AMMUNITION DISPOSAL AREA**  
**GEOPHYSICAL SURVEY AREA**

161 AREFG, ARIZONA ANG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



SI REPORT

DRAWING NO.: H3971B-B-C22  
PROJ. NO.: H3971B

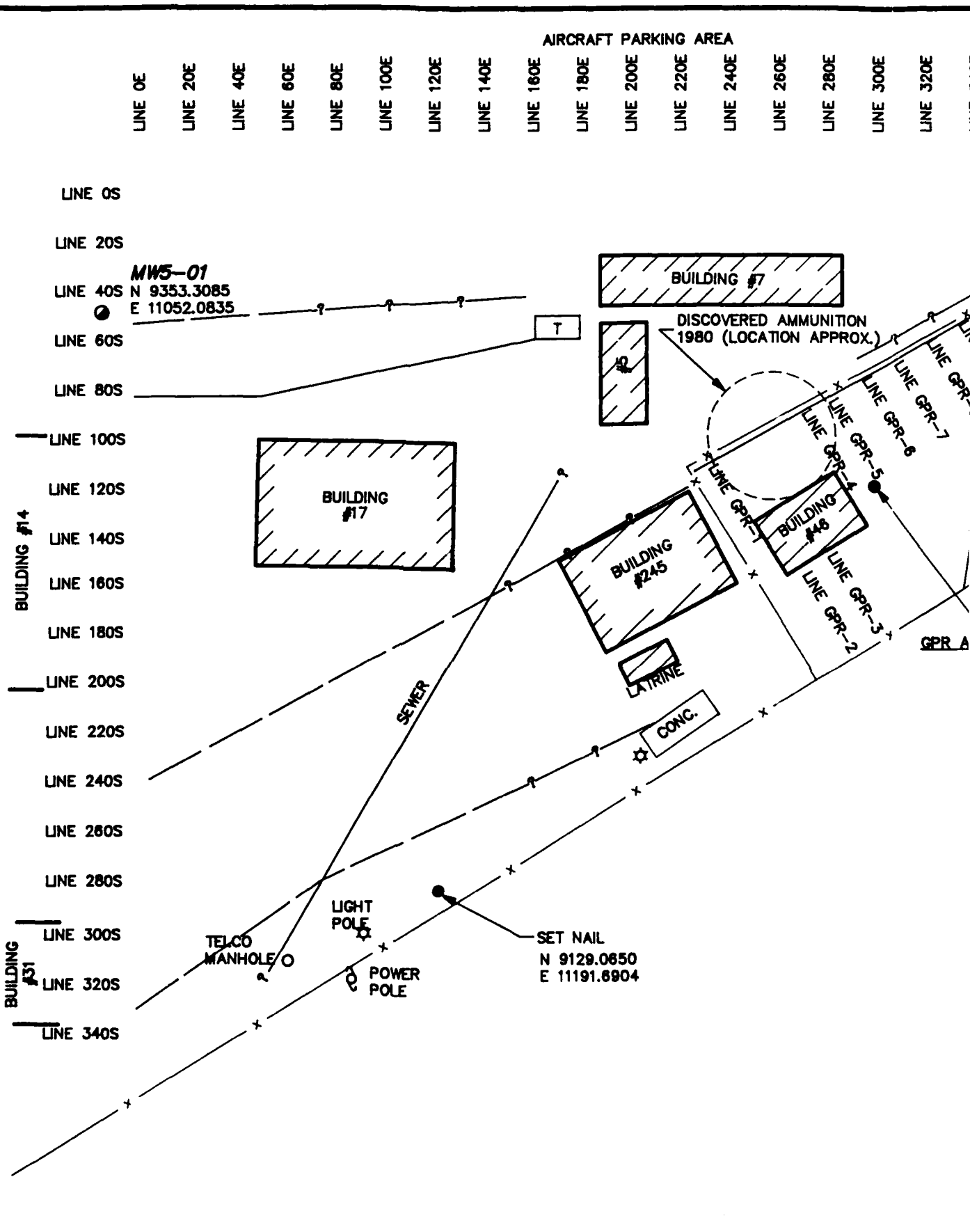
INITIATOR: S. SARES  
PROJ. MGR.: D. WILLEN

DRAFT. CHK. BY: J. HUBBARD  
ENGR. CHK. BY: S. SARES

DATE LAST REV.:  
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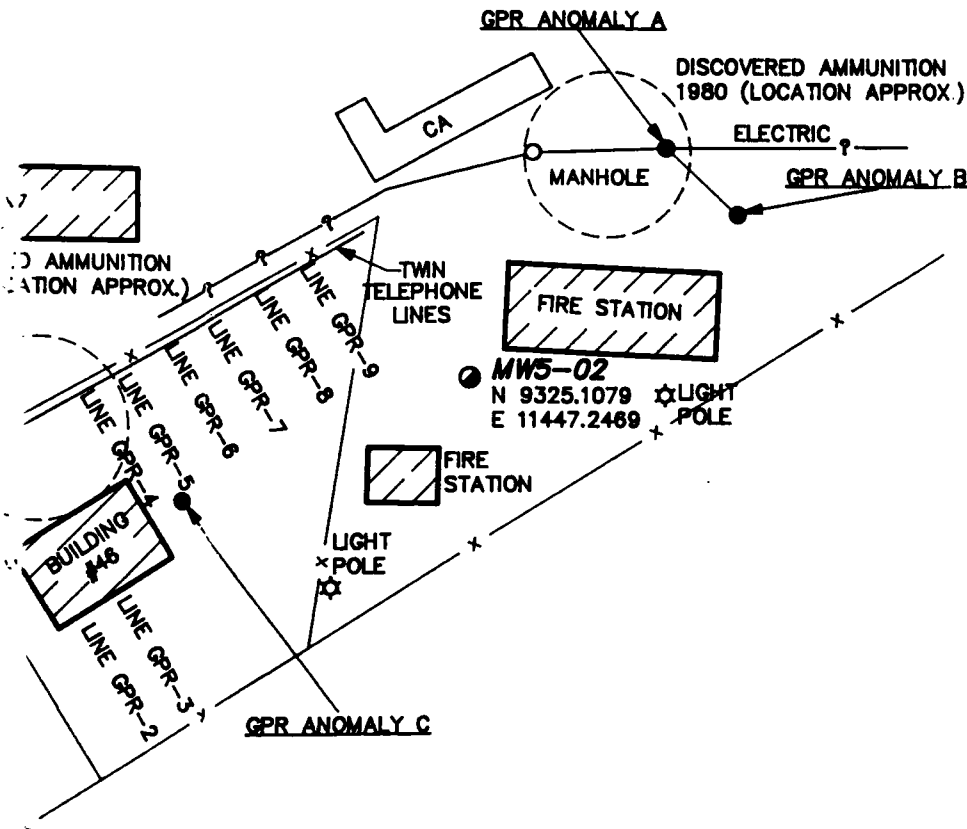
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DRAWN BY: G. PACHECO

H3971B02 08/17/91 3:32pm SAT



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 LINE 280E  
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 LINE 340E  
 LINE 360E  
 LINE 380E  
 LINE 400E  
 LINE 420E  
 LINE 430E  
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 LINE 460E

SET CONCRETE  
 NAIL & SHINER  
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 E 11659.5025



**LEGEND:**

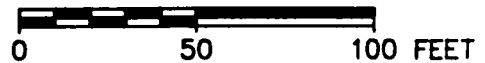
- ☆ LIGHT
- MANHOLE
- MONITORING WELL

CA CUT IN ASPHALT

UTILITY DASHED WHERE APPROXIMATE,  
 QUERIED WHERE UNCERTAIN

T TRANSFORMER

**SCALE:**



**FIGURE 2**

**SITE 5-AMMUNITION DISPOSAL AREA  
 GEOPHYSICAL INTERPRETATION MAP**

151 AREFG, ARIZONA ANG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



geophysical survey at Site 5 (Ammunitions Disposal Area). A Geophysical Survey Systems, Inc. (GSSI) Subsurface Interface Radar System 10, which was equipped with 120-, 300-, and 500-MHz monostatic antennae, a Radio Detection Model RD-400 electromagnetic cable locator, and a Metrotech Model 810 pipe and cable detector were used during the geophysical clearance phase. The GPR unit and a Geonics EM-31DL (EM-31) with a digital data logger were used during the geophysical surveys at Site 5. Detailed equipment descriptions and supporting theory are included in Appendix A.

### **2.1 Geophysical Clearance**

Geophysical field procedures used to clear drilling locations of subsurface obstructions are described in this section. First, all utilities near the drilling point evident from utility maps and visual observation were traced by placing the Metrotech or RD-400 transmitter on the line, delineating the line using the receiver, and marking it on the ground surface using orange surveyor's paint. Individual drilling locations were then cleared by holding the transmitter on the line and circling with the receiver at a radius of approximately 40 feet. When a line was located using the receiver, the transmitter was relocated to that point and the line was traced and marked in the vicinity of the drill point. If a utility was found within approximately 3 feet of the drilling location, it was moved and the entire procedure repeated. Finally, in areas where nonmetallic pipes or large numbers of utilities were present, two perpendicular GPR profiles were conducted over the drilling point using the 120-, 300-, and/or 500-MHz antennae. If additional utilities were located within 3 feet of the drilling location, the boring was moved and the clearance procedures repeated.

### **2.2 Geophysical Survey: Site 5 - Ammunition Disposal Area**

EM and GPR surveys were conducted at Site 5 to determine the possible location of buried ammunition disposed of during the 1950s.

To provide spatial control, a 20- by 20-foot grid was marked with surveyors paint in the area of interest. The location of the base grid relative to permanent site features is shown in Figure 1.

Readings of conductivity and in-phase component field strength, as measured by the EM-31, were collected at 5-foot intervals along both north-south and east-west lines spaced 20 feet apart. The locations of the EM survey lines are shown in Figure 1. Data were stored in a digital data logger and downloaded to a laptop computer at the completion of the survey. Many of the EM survey lines were conducted in segments due to buildings and other

obstructions. For example, data were not collected in the Liquid Oxygen Storage Area (Building No. 46 and its perimeter) because of the adverse effects of the oxygen tanks and surrounding fences.

The GPR survey was concentrated in the vicinity of the Ammunition Dump and in the areas where ammunition was discovered during trench excavations in 1980. The locations of the GPR profiles are shown in Figure 1. All GPR profiles within the Liquid Oxygen Storage Area (Lines GPR-1 through GPR-9) were conducted with both the 300- and 120-MHz antennae. All other GPR profiles were conducted with only the 300-MHz antenna. All GPR data were stored on digital tape for later processing.

To allow an accurate interpretation of the geophysical data, the locations of all surface metallic objects were accurately plotted relative to the base grid as shown in Figure 2.

### ***3.0 Data Processing and Interpretation***

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Computer-generated plots of the EM profiles are included in Appendix B. In-phase and conductivity anomalies were tracked from line to line when possible, or noted as single anomalies. Some portions of the data severely affected by buildings and vehicles were deleted before plotting.

Field mapping of surface metallic objects made it possible to distinguish anomalies caused by known sources from those caused by buried pipelines and other conductive objects. Contour maps of the EM data were not generated because a significant portion of the data was affected by buried objects and surface features.

Color plots of the GPR sections were made for interpretation, with a color scale proportional to the amplitude of the reflected signal. Two-way travel times were converted to depths using an assumed relative dielectric constant of five. Anomalies due to known sources, such as surface objects or buried pipes, are noted on the profiles. Examples of interpreted GPR sections are included in Appendix C.

## 4.0 Discussion and Results

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The first phase of geophysical surveying involving geophysical clearance of subsurface obstructions to drilling resulted in the successful installation of all SOV probes, soil borings, and monitoring wells.

In the second phase of geophysical surveying, EM and GPR were used to assess the likelihood of additional buried ammunition at Site 5. The results of the EM survey are presented graphically in Appendix B and are summarized in Figure 2. After discarding in-phase and conductivity anomalies due to known sources, significant remaining anomalies were observed to exhibit continuity between parallel survey lines, and because of their linear character are interpreted to be caused by underground utilities.

GPR profiles are presented in Appendix C. Assuming a relative dielectric constant of five for geologic materials at Site 5, effective depth of penetration was approximately 5 feet for the 300 MHz antenna and approximately 12 feet for the 120 MHz antenna. Although the penetration depth of the 120 MHz antenna was significantly greater, its resolution was correspondingly lower than the 300 MHz model. In addition, the 120 MHz antenna was not shielded, and therefore was subject to signal interference from aboveground sources. An example of this can be seen in Figure C-4, in which a fence is responsible for a hyperbolic reflection between 75 and 90 feet. Because of these shortcomings, it is not likely that the 120 MHz antenna was capable of resolving containerized ammunition.

The anomalies observed on GPR profiles north of monitoring well MW5-02 were compared with known surface and subsurface features as shown in Figure 2. Two significant anomalies could not be related to known features. Anomaly A, shown in Figures 2 and C-2, is located at approximately 19 feet south on Line 440 east. This anomaly is traceable through several parallel survey lines, and its trace intersects a manhole located at the intersection of Lines 400 east and 20 south. Further, the depth of the anomaly is less than approximately 3 feet. There is little doubt that the source of the anomaly is an underground utility. Anomaly B (Figures 2 and C-2) is characteristic of a metal object very near the ground surface. A similar anomaly was caused by an iron manhole at the intersection of Lines 400 east and 20 south.



GPR surveys in the area north of monitoring well MW5-02 were apparently capable of resolving underground utilities down to several inches in diameter. Therefore, assuming that ammunition was containerized or buried in some other bulk fashion, it is likely its presence would be indicated in the GPR data to a depth of roughly 5 feet. The lack of unaccounted-for GPR anomalies is an indication that large concentrations of ammunition are not present in this location.

GPR profiles in the vicinity of Building 46, labelled GPR-1 through GPR-9 in Figure 1, were compared with known surface and subsurface features. Anomalies traceable across several records can be explained by the presence of features shown in Figure 2. For example, comparison of Figures 2 and C-4 demonstrates the hyperbolic signature of several underground utilities and the masking effect of the concrete-slab floor of Building 46.

No anomalies were found that strongly indicated the presence of buried ammunition near Building 46. However, as shown in Figure C-4, geologic layering below a depth of approximately 2 feet is apparently indistinct to nonexistent. This leads to two possibilities: (1) layering does not exist; this may be a natural condition or layering may be disturbed, (2) layering exists but was not resolved with GPR due to poor penetration or interference from known features. In considering the latter case, Figures C-1, C-2, and C-3 should be compared to Figure C-4. Figures C-1, C-2, and C-3 are radar profiles obtained along survey lines located approximately 150 feet northeast of Building 46 (Figure 1). Geologic layering in this area appears much more distinct than in the vicinity of Building 46; thereby lending support to the former possibility.

## ***5.0 Conclusions***

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Two phases of geophysical surveying were conducted at Sky Harbor IAP using GPR and EM methods. The first phase of surveying involved geophysical clearance of drilling and SOV locations of subsurface obstructions. In the second phase of the survey, subsurface conditions were assessed for the presence of buried ammunition.

The geophysical clearance phase of work resulted in the successful installation of all borings, monitoring wells, and SOV sample points.

The results and conclusions of the second phase of the investigation are based primarily on GPR data. The EM data were of limited use because of the adverse effects of abundant

surface and subsurface electrically conducting material not related to previous disposal operations.

Radar data in the vicinity of Building 46, the Liquid Oxygen Storage Area, did not provide direct evidence of buried ammunition. However, the apparent lack of layering in geologic materials within this area may be due to excavation and disruption during disposal operations.

Geologic layering appears more distinct in the survey area northwest of Building 46. This may be an indication that disposal has not occurred in this area. Further, no anomalous materials were apparent in the radar data to its approximately 5-foot depth limit, although underground utilities were clearly resolved in this same interval. This implies that buried ammunition, if present and of approximately the dimensions of a typical underground utility diameter, would be detected to a depth of approximately 5 feet.

Direct confirmation of the presence or absence of buried ammunition at Site 5 is not possible based solely on nonintrusive methods. Individual cartridges smaller than the minimum dimensions resolved by GPR may be present at any of the locations surveyed. Ammunition in any form may be present at depths greater than effectively sensed by radar. Finally, ammunition disposal occurring in discrete zones of dimensions smaller than the geophysical grid spacing of 20 feet may not have been crossed by a geophysical survey line and therefore could remain undetected.

## ***References***

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**APPENDIX A**  
**THEORETICAL BACKGROUND**

## APPENDIX A

### THEORETICAL BACKGROUND

#### ***A.1.0 Electromagnetic Induction***

---

Electromagnetic (EM) induction equipment used during this investigation consisted of a Geonics EM-31DL terrain conductivity meter (EM-31) with an Omni digital data logger, a Metrotech Model 810 pipe and cable detector (Metrotech), and a Radio Detection Model RD-400 electromagnetic cable locator (RD-400).

The EM-31 has a transmitter and receiver coil mounted at each end of a 12-foot-long plastic boom. An audio-frequency alternating current is applied to the transmitter coil, causing the coil to radiate a primary EM field with a magnetic field vector parallel to the axis of the coils. This time varying magnetic field induces eddy currents in any conducting material in the subsurface as described by Faraday's Law on induction. These eddy currents have an associated (secondary) magnetic field with a strength and phase shift relative to the primary field that is dependent on the conductivity of the medium. The receiver coil measures the resultant effect of both primary and secondary fields. By comparing the signal at the receiver to that at the transmitter, the instrument is able to record the in-phase component (in-phase) and the component 90 degrees out of phase (quadrature) with the primary field.

Most geological materials are poor conductors, and the flow of current through the material takes place in the pore fluids (Keller and Frischknecht, 1966). Conductivity is predominantly a function of soil type, porosity, permeability, pore fluid ion content, and degree of saturation. The EM-31 is calibrated so that the out-of-phase component is converted to electrical conductivity in units of millisiemens per meter (mS/m) (McNeill, 1980). The in-phase component is read in parts per thousand (ppt) of the primary EM field and is generally adjusted in the field to read zero response over background materials.

The depth of penetration for EM induction instruments is dependent on the transmitter-receiver separation and coil orientation (McNeill, 1980). The EM-31 has an effective exploration depth of about 18 feet when operating in the vertical dipole mode (horizontal coils). In the absence of large metallic features such as tanks, drums, pipes, and reinforced concrete, the maximum instrument response results from materials at about 3 to 5 feet below ground surface. A single buried drum typically can be located to depths of about 5 feet whereas clusters of drums can be located to significantly greater depths depending on

background noise. The EM-31 generally must pass over or very near to a buried metallic object to detect it. Both the out-of-phase (conductivity) and in-phase components exhibit a characteristic anomaly over near-surface metallic conductors. This anomaly consists of a narrow zone having strong negative amplitude centered over the target and a broader lobe of weaker, positive amplitude on either side of the target. For long, linear conductors such as pipelines, the characteristic anomaly is as described above when the axis of the coils (instrument boom) is at an angle to the conductor; however, when the instrument boom is oriented parallel to the conductor, a positive amplitude anomaly is obtained.

EM-31 applications include the delineation of soil contamination, oil brine pits, buried metallic and nonmetallic debris, landfill boundaries, buried pipes and cables, and buried drums and tanks.

The RD-400 and Metrotech are specifically designed to accurately locate and delineate underground pipes and utilities. A transmitter emits a radio-frequency signal that induces a secondary EM field in nearby utilities. A receiver unit measures the signal strength of this secondary field and emits an audible response to allow the precise location of the pipe, cable, or other conductor in which a signal is induced. If the utility is accessible anywhere, the source signal can be directly applied to it, making the secondary field much larger and readily measurable.

## ***A.2.0 Ground Penetrating Radar***

---

Ground penetrating radar (GPR) equipment used during this investigation consisted of a Geophysical Survey Systems, Inc. (GSSI) Subsurface Interface Radar System 10 equipped with 120-MHz, 300-MHz, and 500-MHz monostatic antennae.

In conducting a GPR survey, a transmitter antenna that emits a high frequency (center frequencies in the range of 80 to 900 MHz) EM wave into the subsurface is pulled along the survey line. This wave propagates at the speed of light in a vacuum scaled by the square root of the relative dielectric constant of the medium and reflects at boundaries where the relative dielectric constant (and therefore the propagation velocity) changes. The contrast in velocity between the two media can be quantified as a reflection coefficient at the boundary. The magnitude of the reflection coefficient increases as the contrast in velocities increases, and its sign is positive or negative depending on whether the velocity increases or decreases, respectively, at the boundary.

The reflected signal is detected at a receiver antenna, often as a characteristic triplet that is the result of the receiving antenna response and multiples generated along the propagation path. The signal is transmitted to a control unit, displayed on a color monitor, and saved on digital tape (if necessary).

As predicted by Maxwell's equations for a propagating EM wave, two kinds of charge flow are caused by the alternating electric (E) and magnetic (H) fields associated with it (Ulriksen, 1982). These are conduction currents and displacement currents. The conduction current term is predominant at lower frequencies and it is these that are used in the EM induction method. At the higher frequencies used in the GPR method, the displacement current term becomes predominant. The high frequencies will set bound charges in motion causing polarization.

The material physical properties that describe the movement of charges by conduction currents and displacement currents are the conductivity and the dielectric constant of the medium, respectively. The conductivity is a measure of the ease with which charges and charged particles move freely through the medium when subjected to an external electric field. The dielectric constant, or its value normalized by the dielectric constant of free space, called the relative dielectric constant, is a measure of how easily a medium polarizes to accommodate the EM fields of propagating wave (Keller and Frischknecht, 1966).

Although conductivity has a lesser effect on the transmission of EM waves emitted from a GPR unit, it does have an important effect on the attenuation of the waves (Ulriksen, 1982). Highly conductive media will attenuate the EM signal rapidly, restricting depth penetration of the first several feet. Highly resistive (poorly conductive) media will allow much deeper depth of penetration. The frequency of the transmitted waves also affects the depth of penetration. Lower frequencies penetrate deeper, but have low resolution, whereas the higher frequencies can resolve smaller objects and layers at the expense of decreased effective depth penetration.

In unconsolidated materials, conduction takes place mostly through the pore fluids (Keller and Frischknecht, 1966). Changes in pore fluid content, porosity, permeability, and degree of saturation will therefore affect reflected and refracted EM signals. This is how trenches, in which there may be different compaction relative to the surrounding area, can be identified. When the target of a GPR survey is a metallic conductor such as metal pipes and cables, drums, tanks, ammunition shells, etc., the mechanism is somewhat different. An EM wave

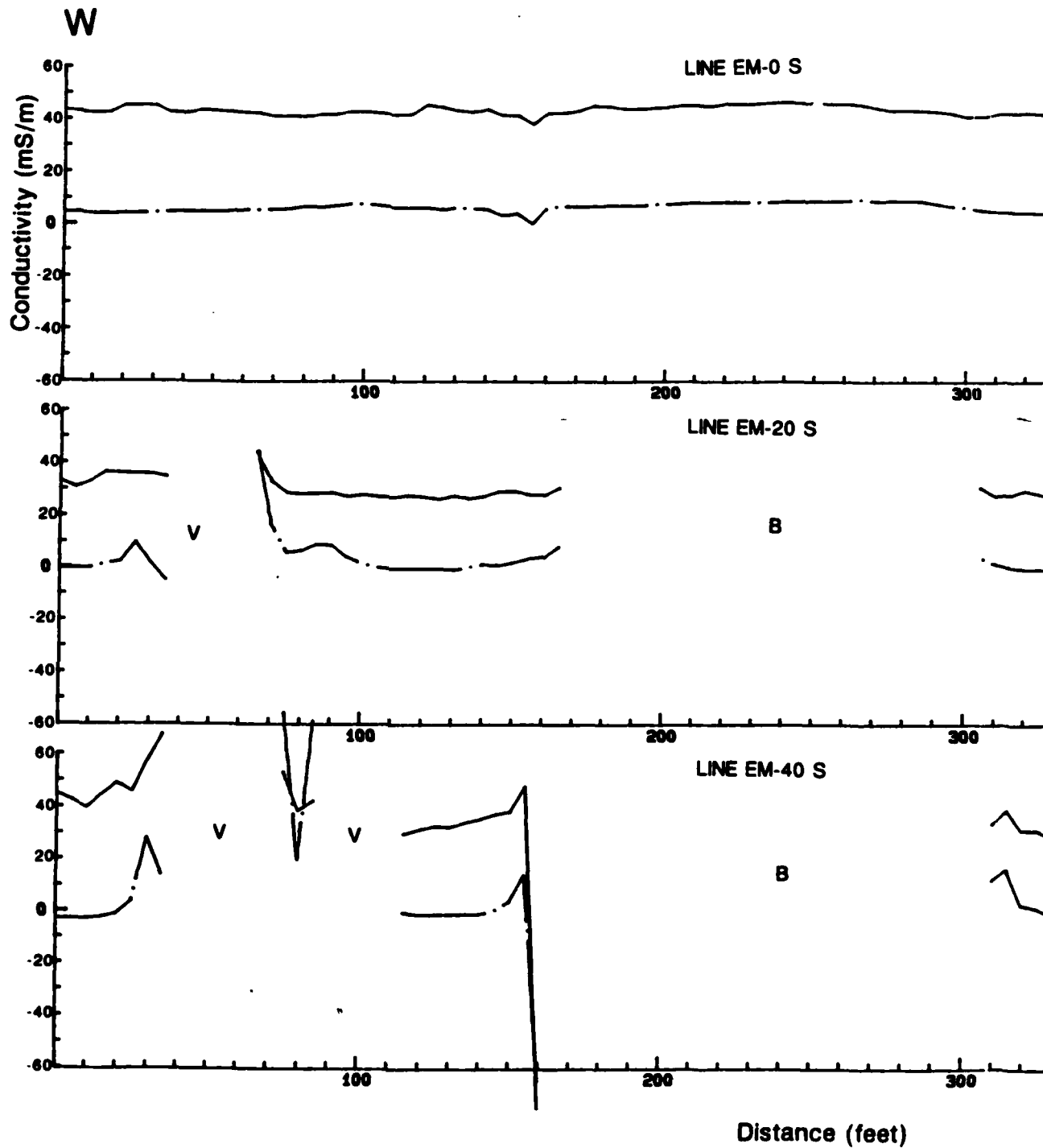
will completely reflect when reaching a metallic conductor. This total reflection makes metallic targets well suited for the GPR method when they are within the depth of penetration range of the instrument. There will be no reflections from below the metallic conductor, although there generally will be multiples. The edges of the metallic reflector will have diffraction patterns that are a result of the fact that both the transmitting and the receiving antennae are not focused, but emit and receive from a 45 degree cone. This cone allows the radar to see objects that are ahead of it, placing them deeper in time. As the radar approaches the object, the reflection becomes shallower, with the shallowest reflection taking place when the radar is right above it. The same pattern will be seen as the antenna moves away from the object.

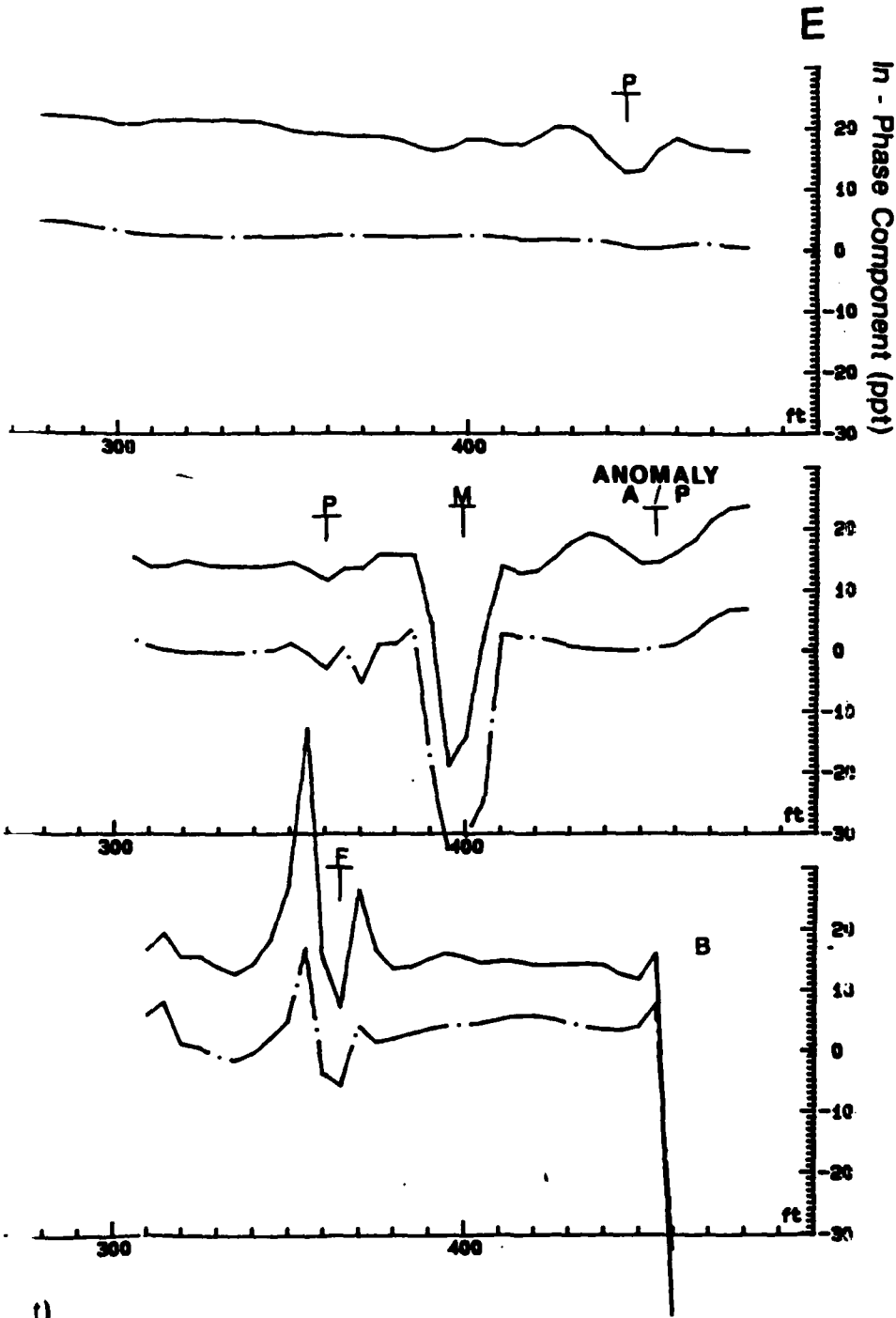
Applications of GPR include delineation of pits and trenches containing metallic and nonmetallic debris; location of buried pipes, drums, and tanks; mapping of landfill boundaries; and mapping of near-surface geology. Near-surface metallic objects such as pipes and tanks exhibit a characteristic high-amplitude hyperbolic anomaly and generally are relatively easy to recognize.



**APPENDIX B**  
**ELECTROMAGNETIC INDUCTION PROFILES**

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 CHECKED BY L.C.  
 APPROVED BY L.C.  
 DATE 4-24-91  
 DRAWING NUMBER 409721-B13  
 DATE 4/30/91  
 DATE 4/18/91





**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

**FIGURE B-1  
ELECTROMAGNETIC INDUCTION PROFILES**

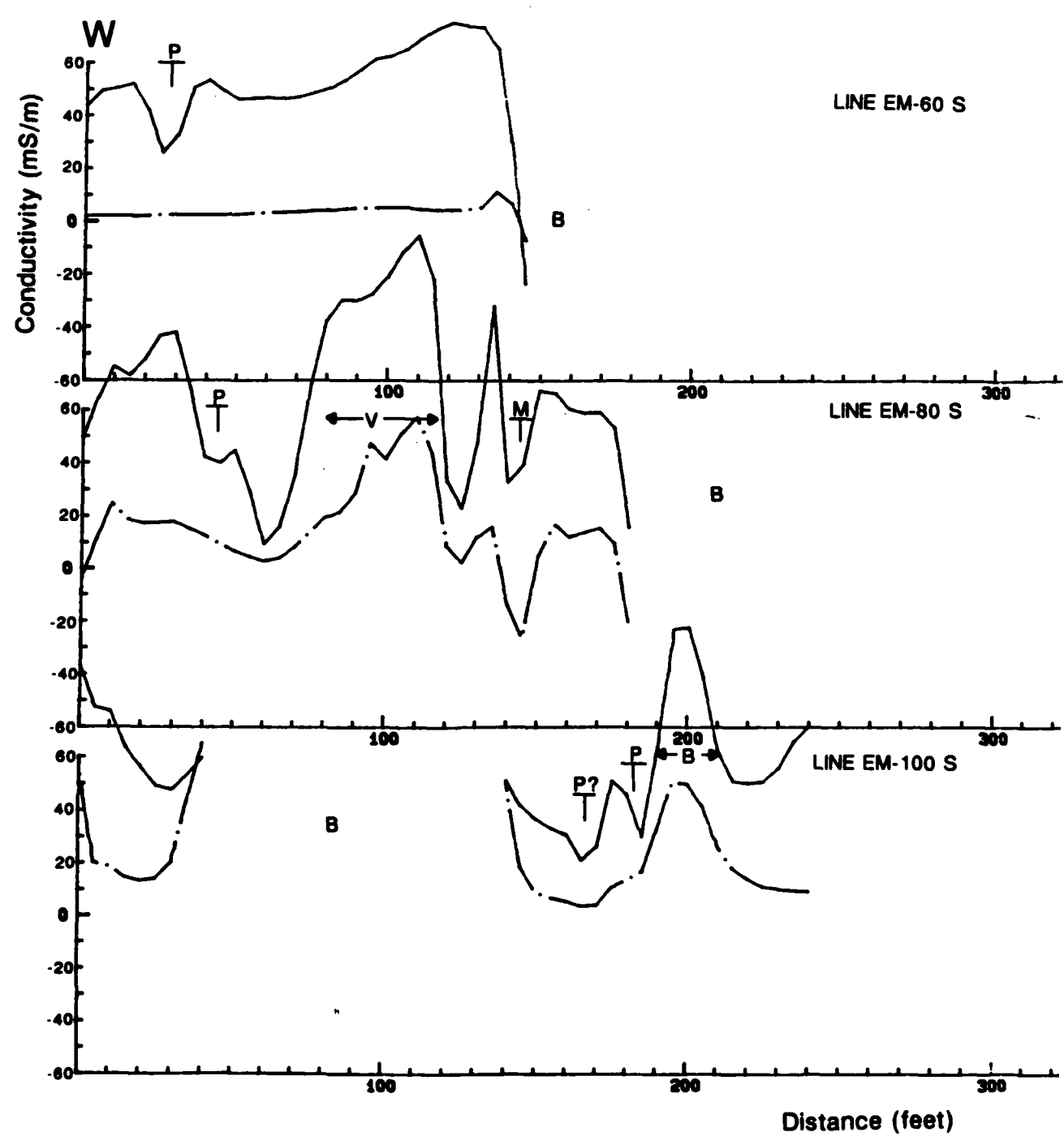
**SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG**

**SKY HARBOR IAP  
PHOENIX, ARIZONA**



t)

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 CHECKED BY L.C.  
 APPROVED BY L.C.  
 DRAWING NUMBER 409721-B14  
 DATE 4/24/91  
 DATE 4/24/91



0 S

0 S

0 S

et)

In - Phase Component (ppt)

In - Phase Component (ppt)

In - Phase Component (ppt)

**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

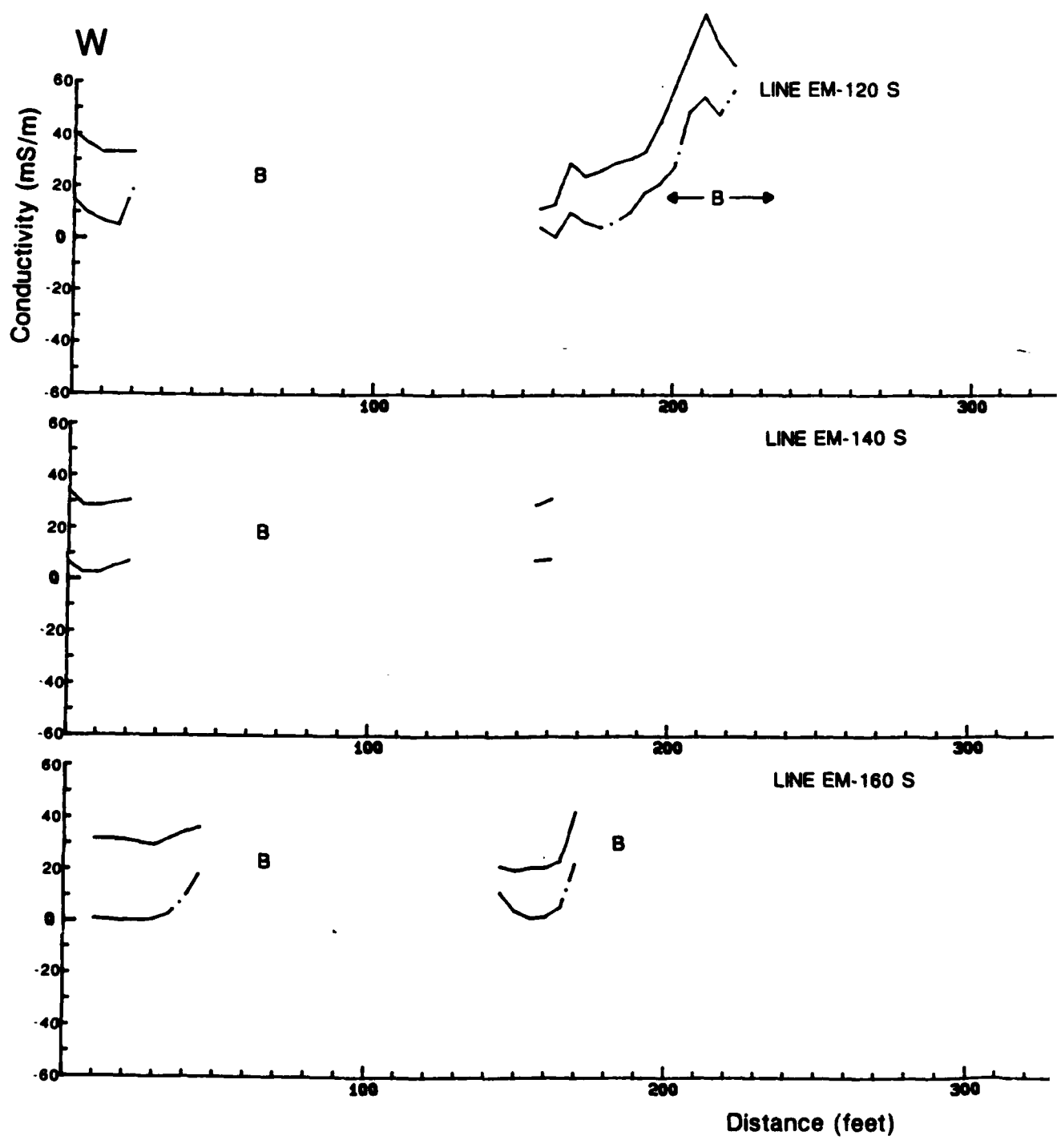
FIGURE B-2

**ELECTROMAGNETIC INDUCTION PROFILES**

SITE 5 - AMMUNITION DISPOSAL AREA  
 161 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



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 APPROVED BY: [Signature]  
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 DATE: 4/30/91  
 DATE: 4/30/91  
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**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

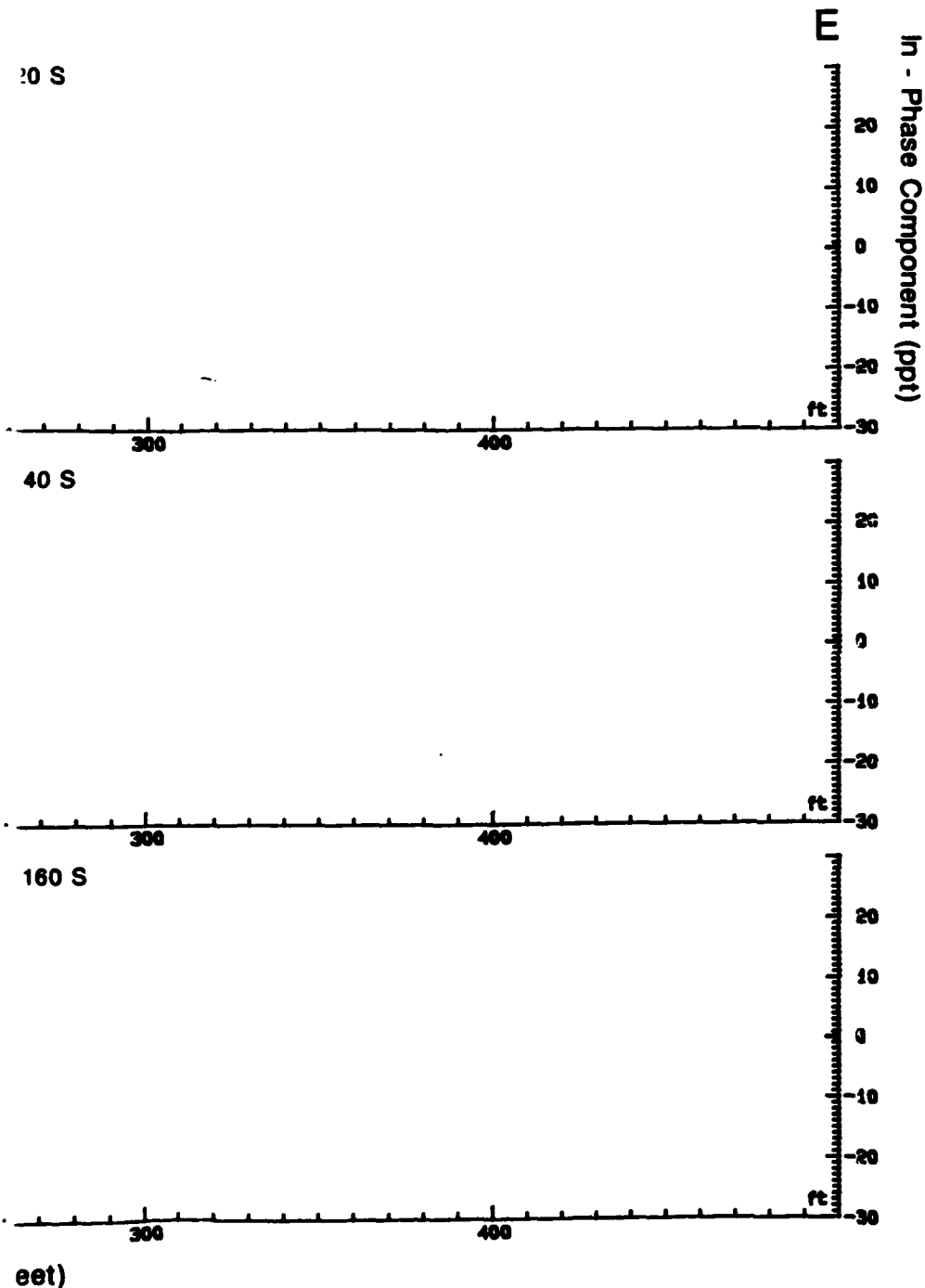
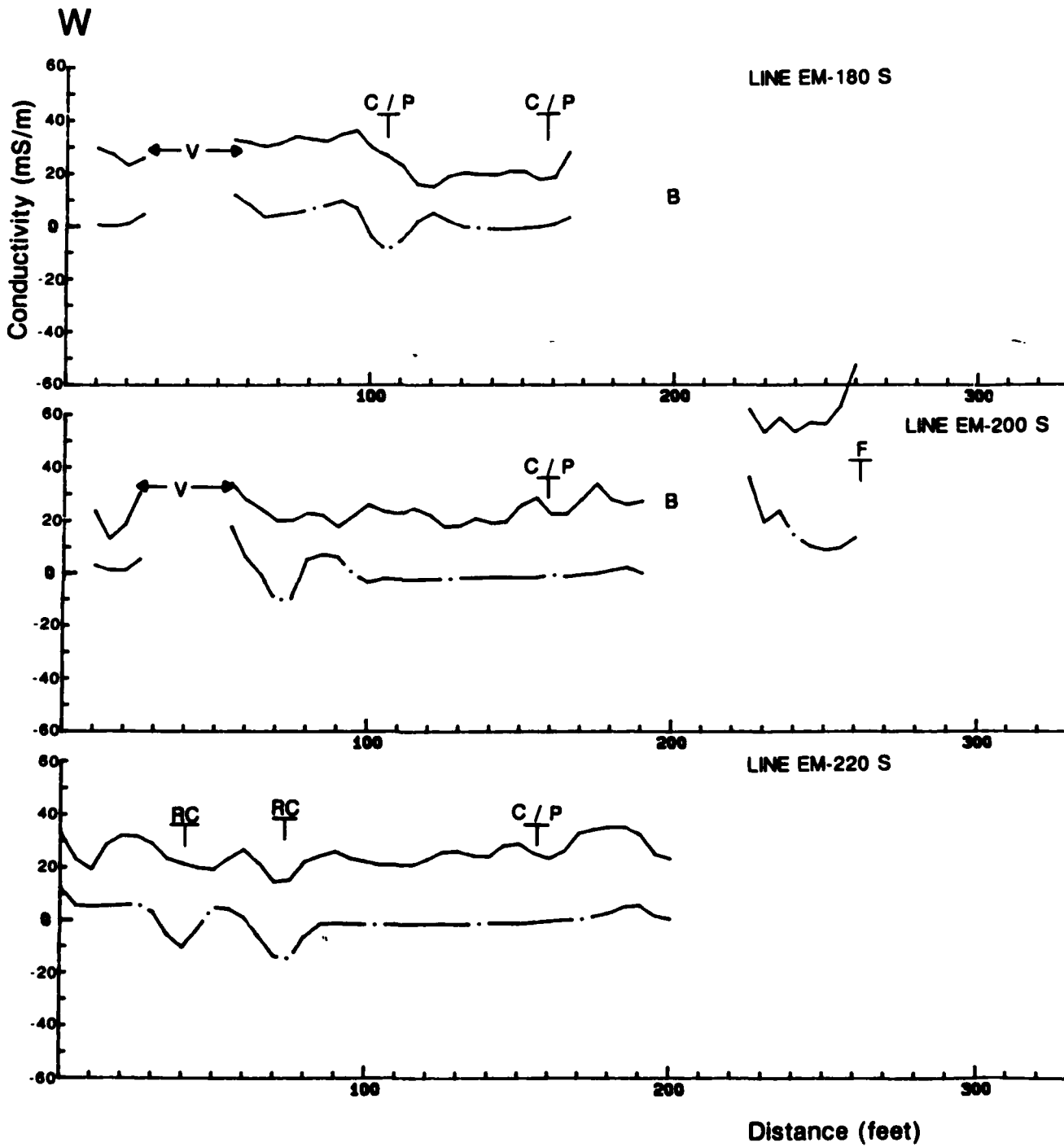


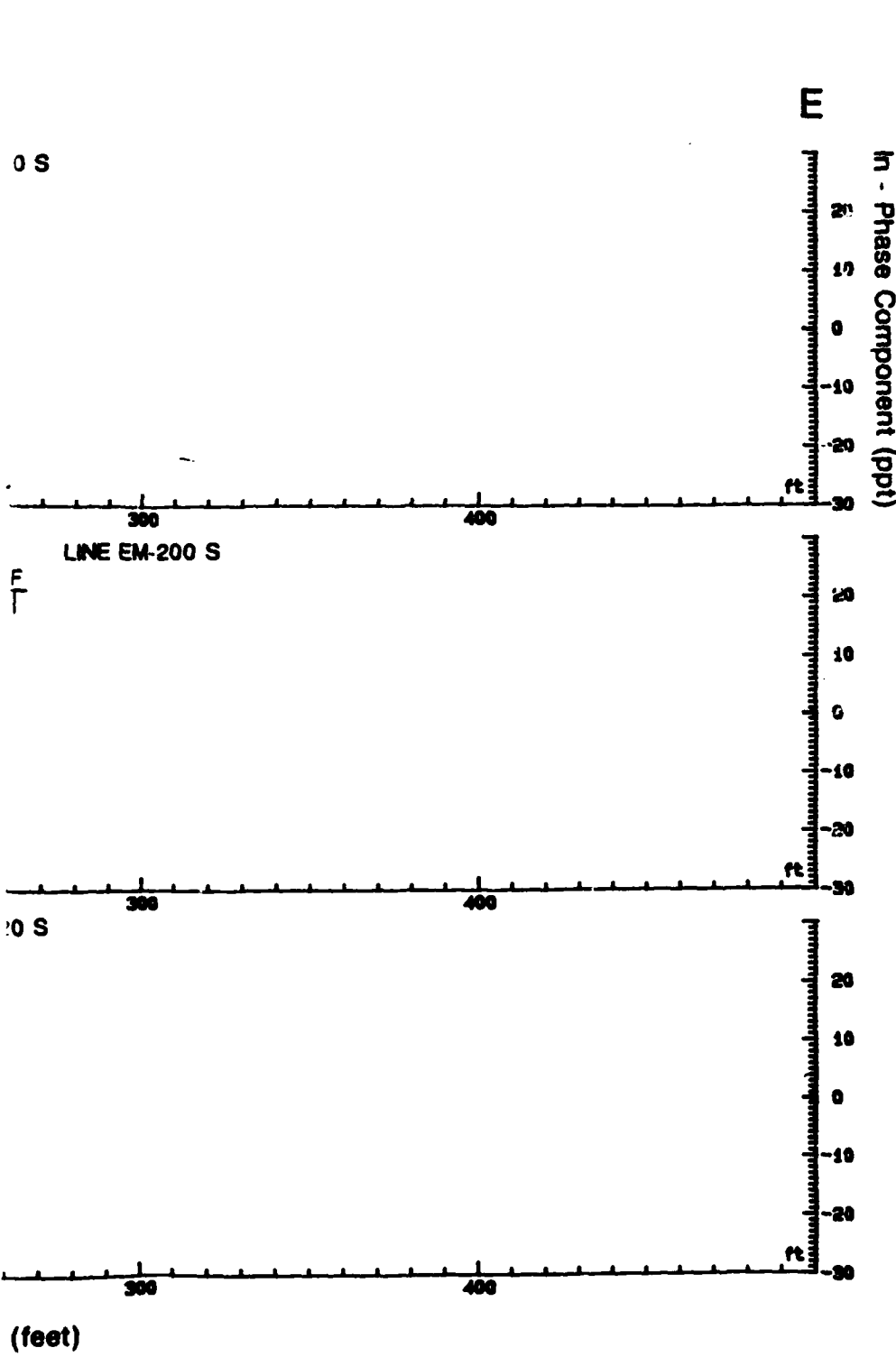
FIGURE B-3  
ELECTROMAGNETIC INDUCTION PROFILES  
SITE 5 - AMMUNITION DISPOSAL AREA  
181 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA



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**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- C - CURB
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

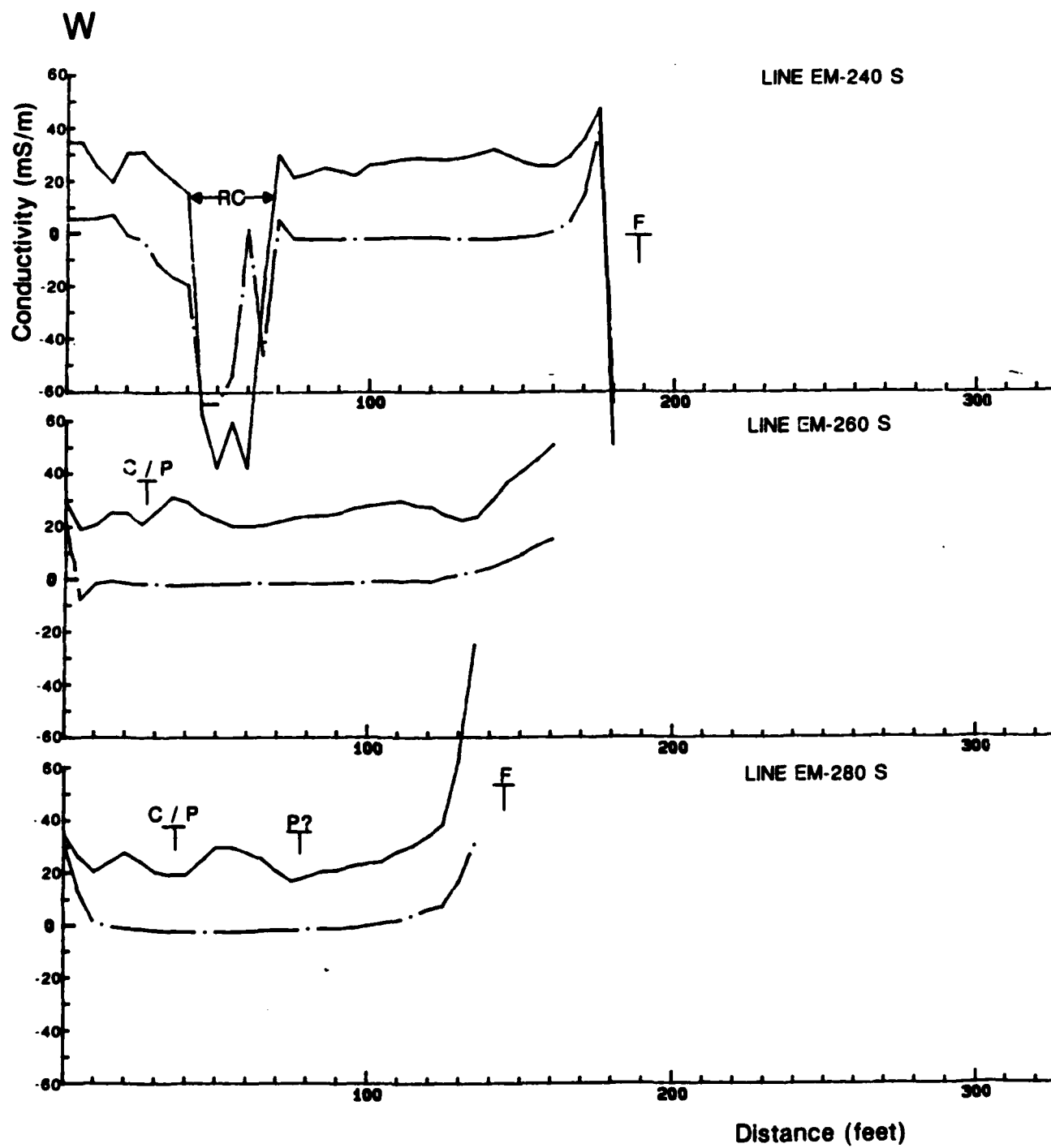
**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

FIGURE B-4  
 ELECTROMAGNETIC INDUCTION PROFILES  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 181 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



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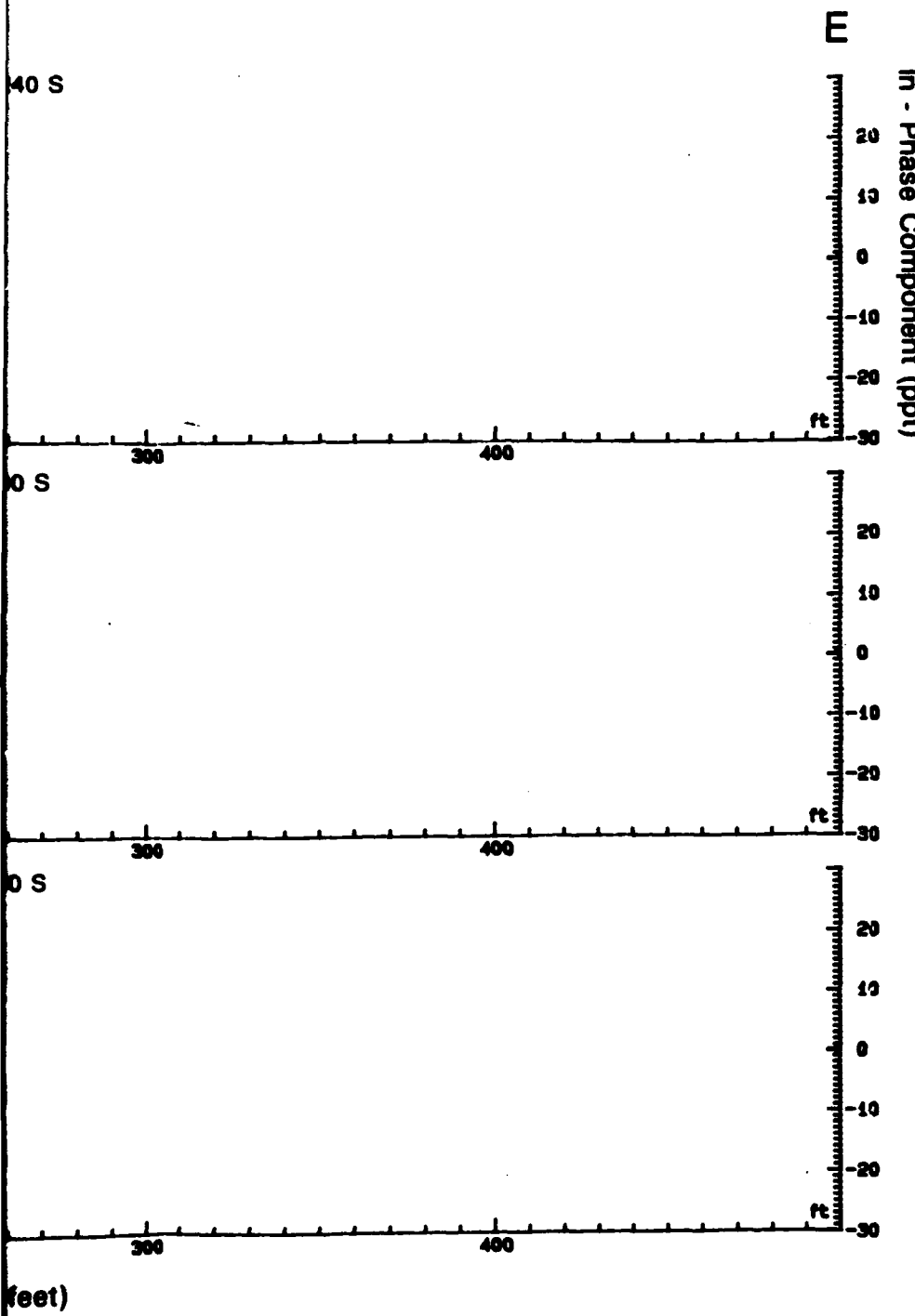
**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- C - CURB
- V - VEHICLE

- CONDUCTIVITY -  
MILLISIEMENS/METER (mS/m)
- · — · — IN-PHASE COMPONENT -  
PARTS PER THOUSAND OF PRIMARY  
ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES



**FIGURE B-5  
ELECTROMAGNETIC INDUCTION PROFILES**

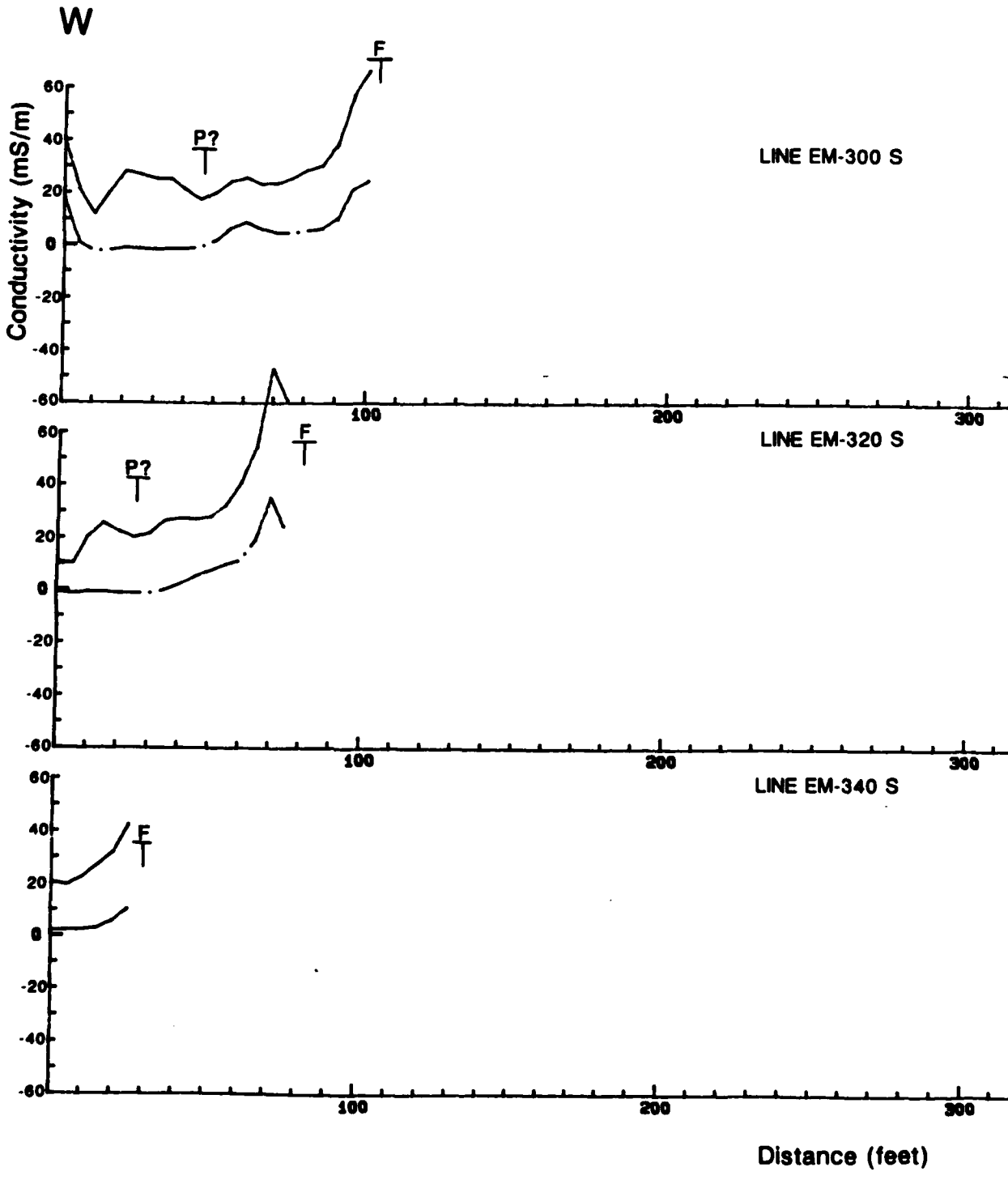
**SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG**

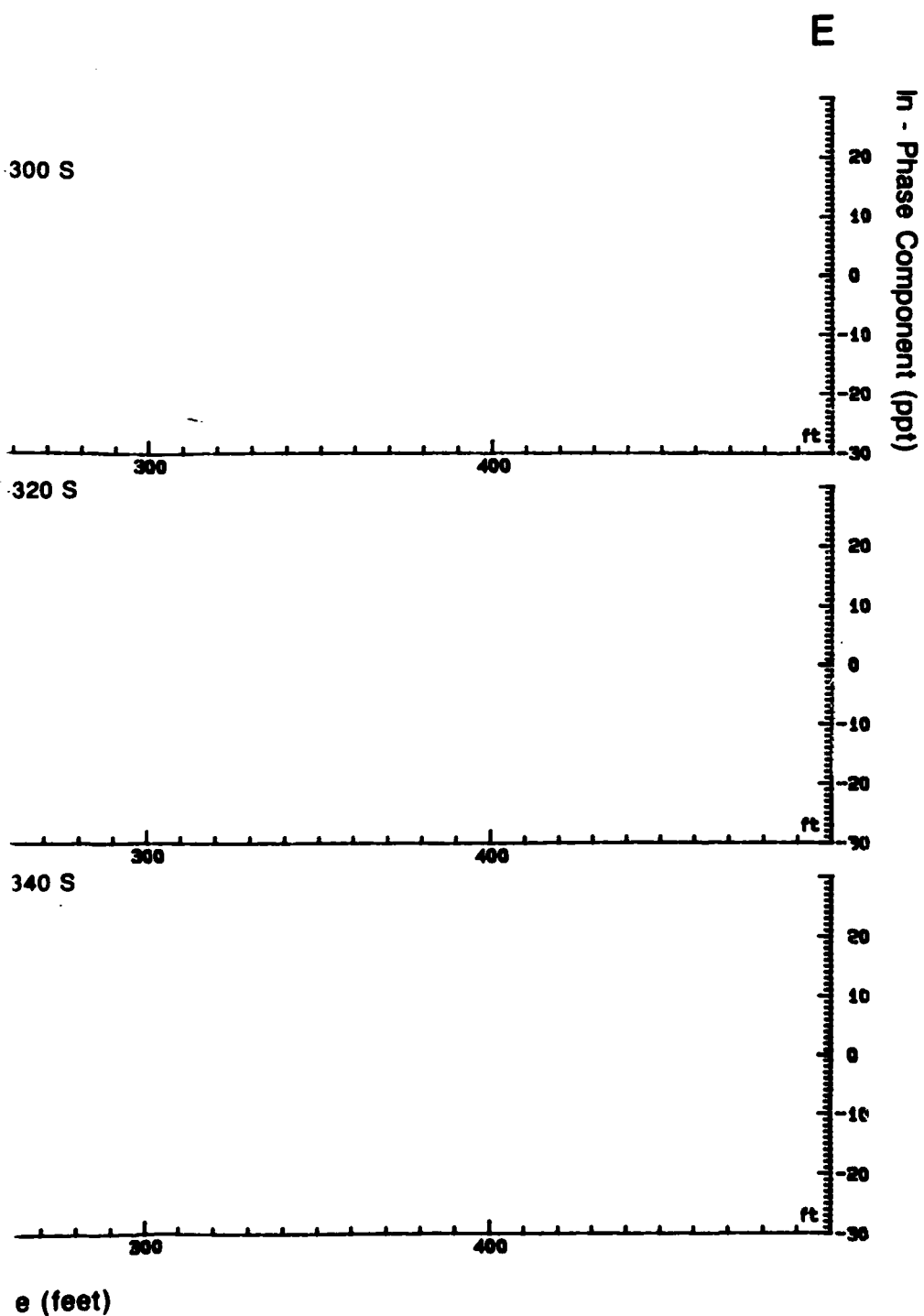
**SKY HARBOR IAP  
PHOENIX, ARIZONA**



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**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

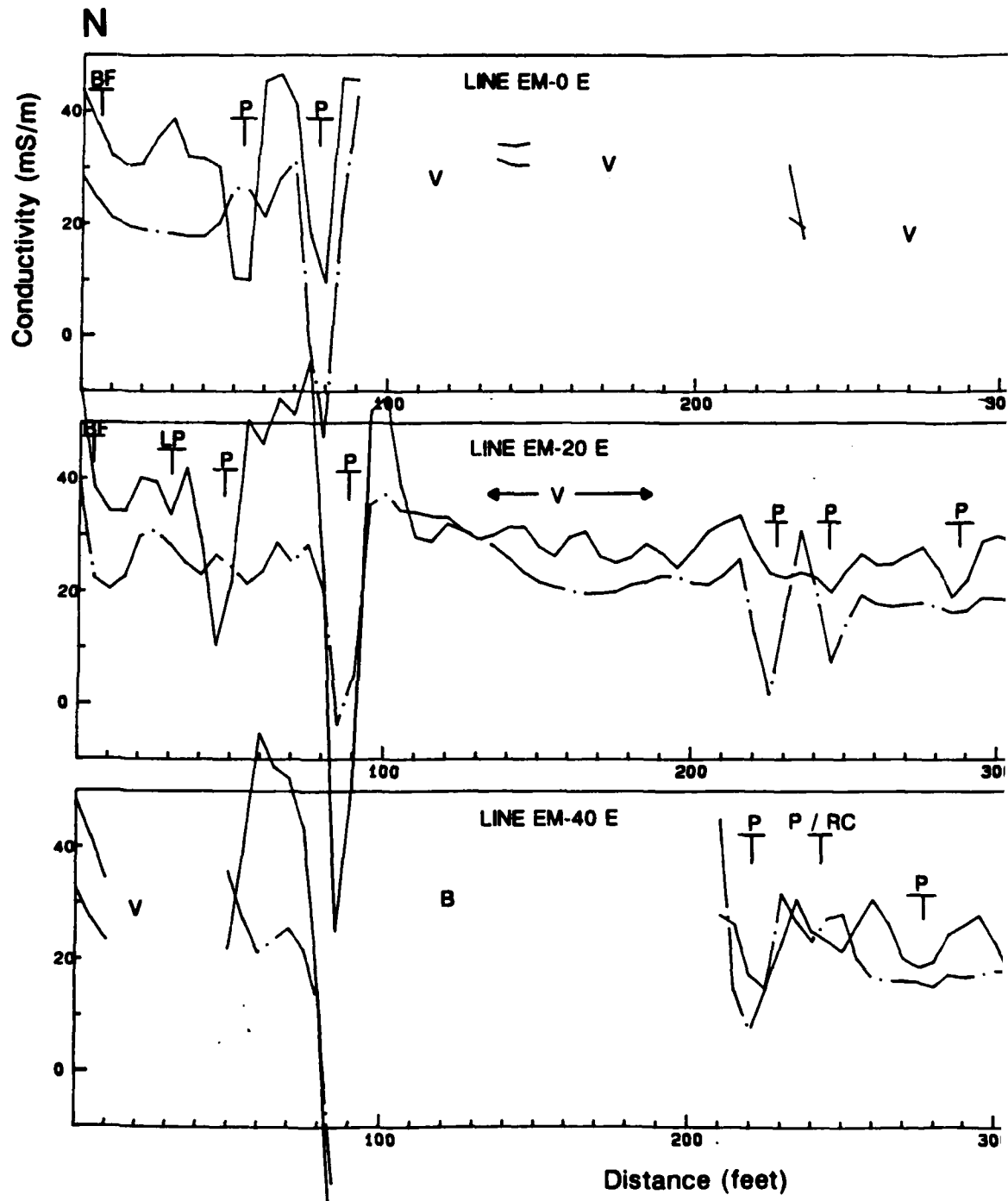
REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

**FIGURE B-6  
ELECTROMAGNETIC INDUCTION PROFILES**

**SITE 5 - AMMUNITION DISPOSAL AREA  
181 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA**



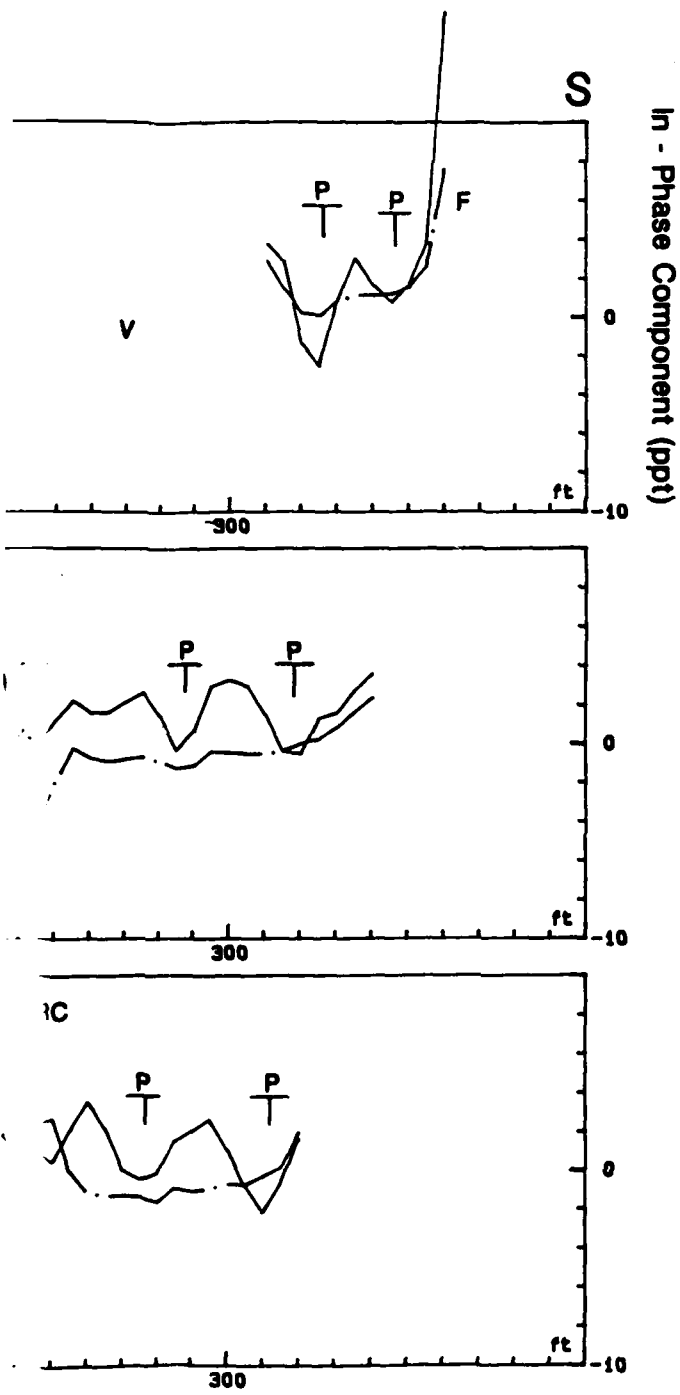
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- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE(S)

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

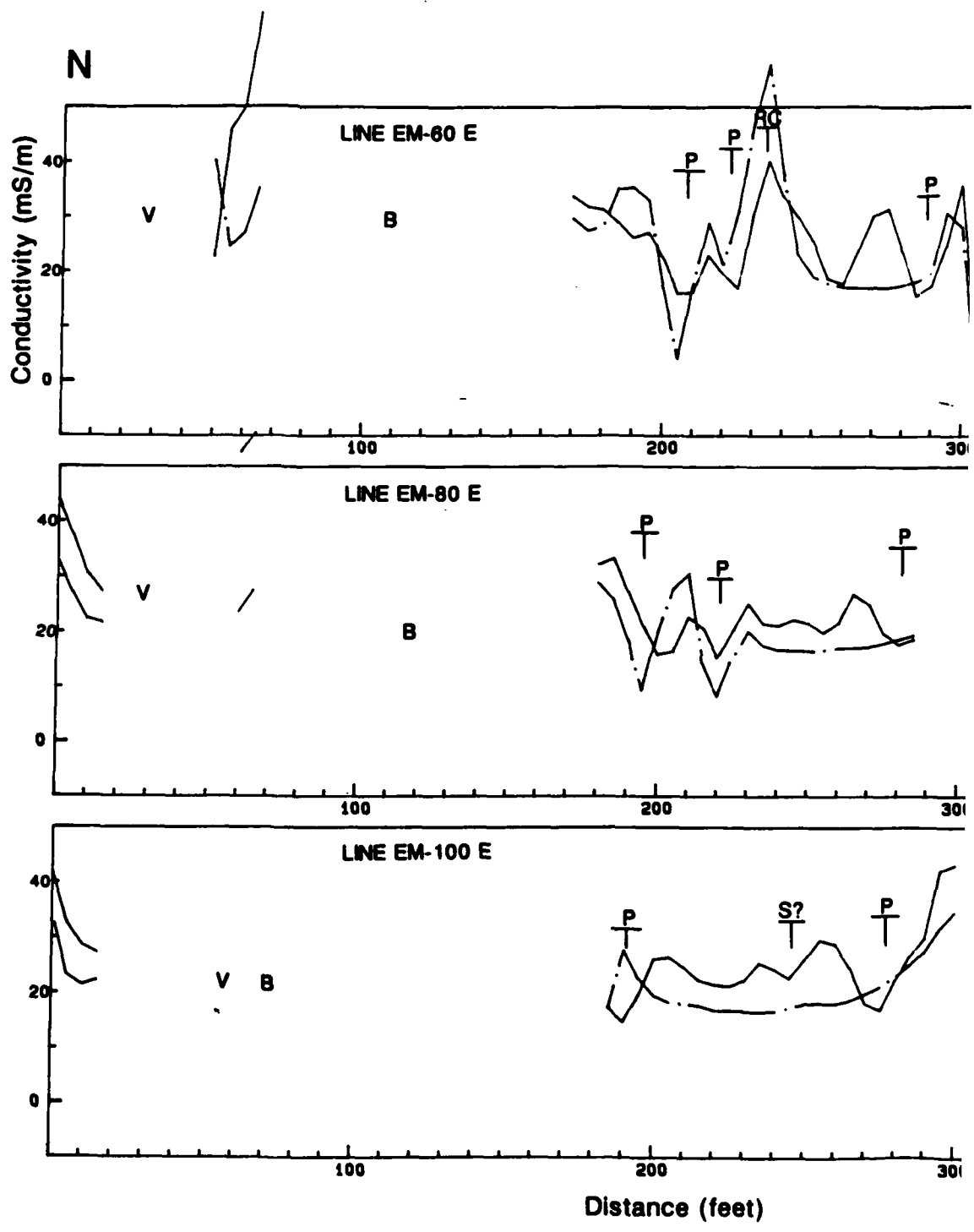
**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

FIGURE B-7  
 ELECTROMAGNETIC INDUCTION PROFILES  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 181 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



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 4/30/91  
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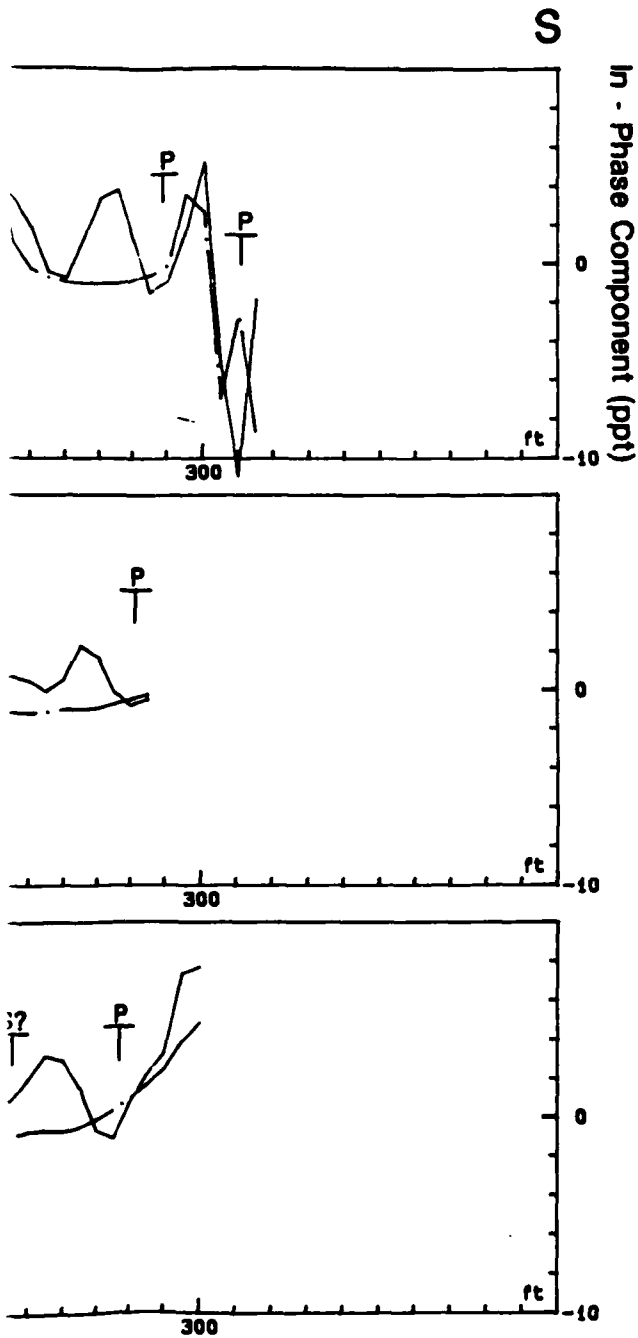
**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES



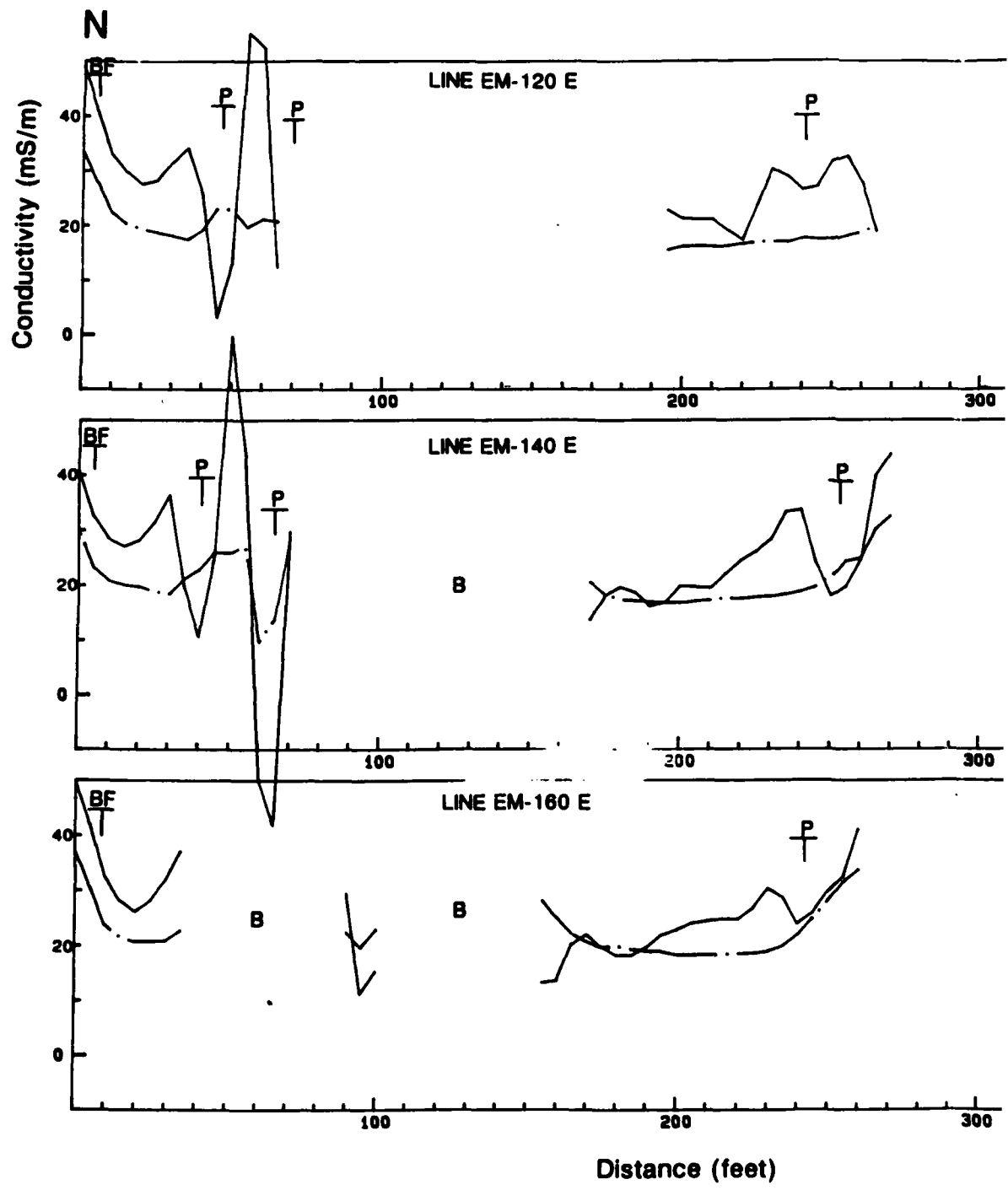
**FIGURE B-8  
ELECTROMAGNETIC INDUCTION PROFILES**

**SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG**

**SKY HARBOR IAP  
PHOENIX, ARIZONA**

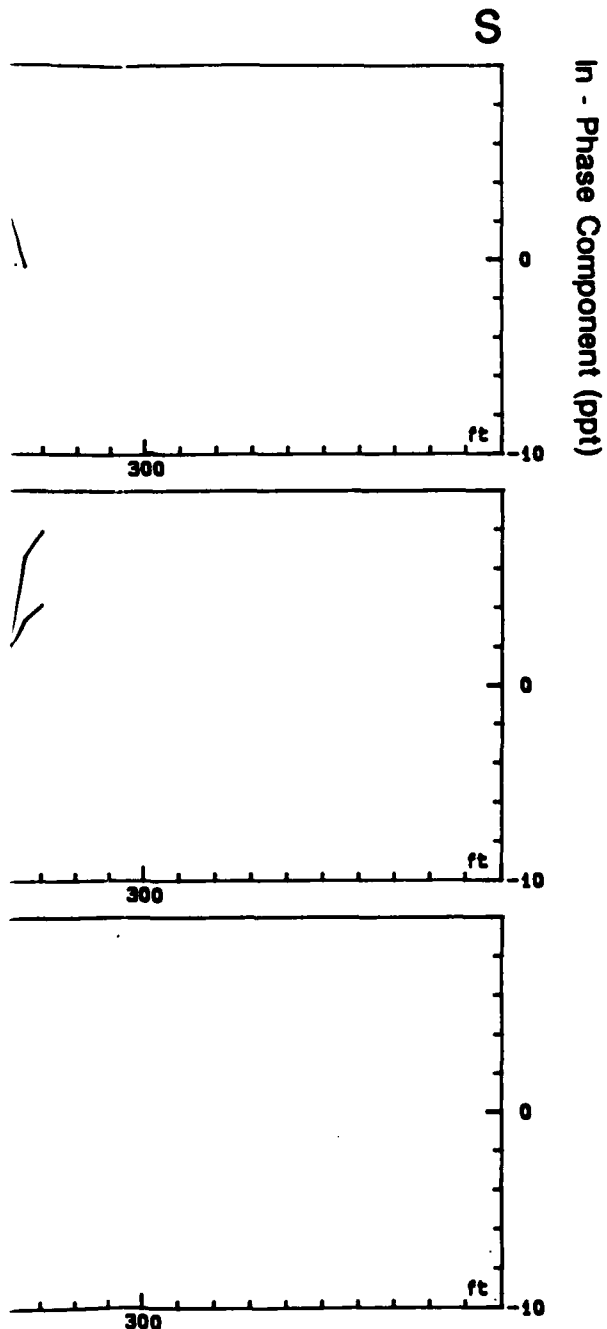


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**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

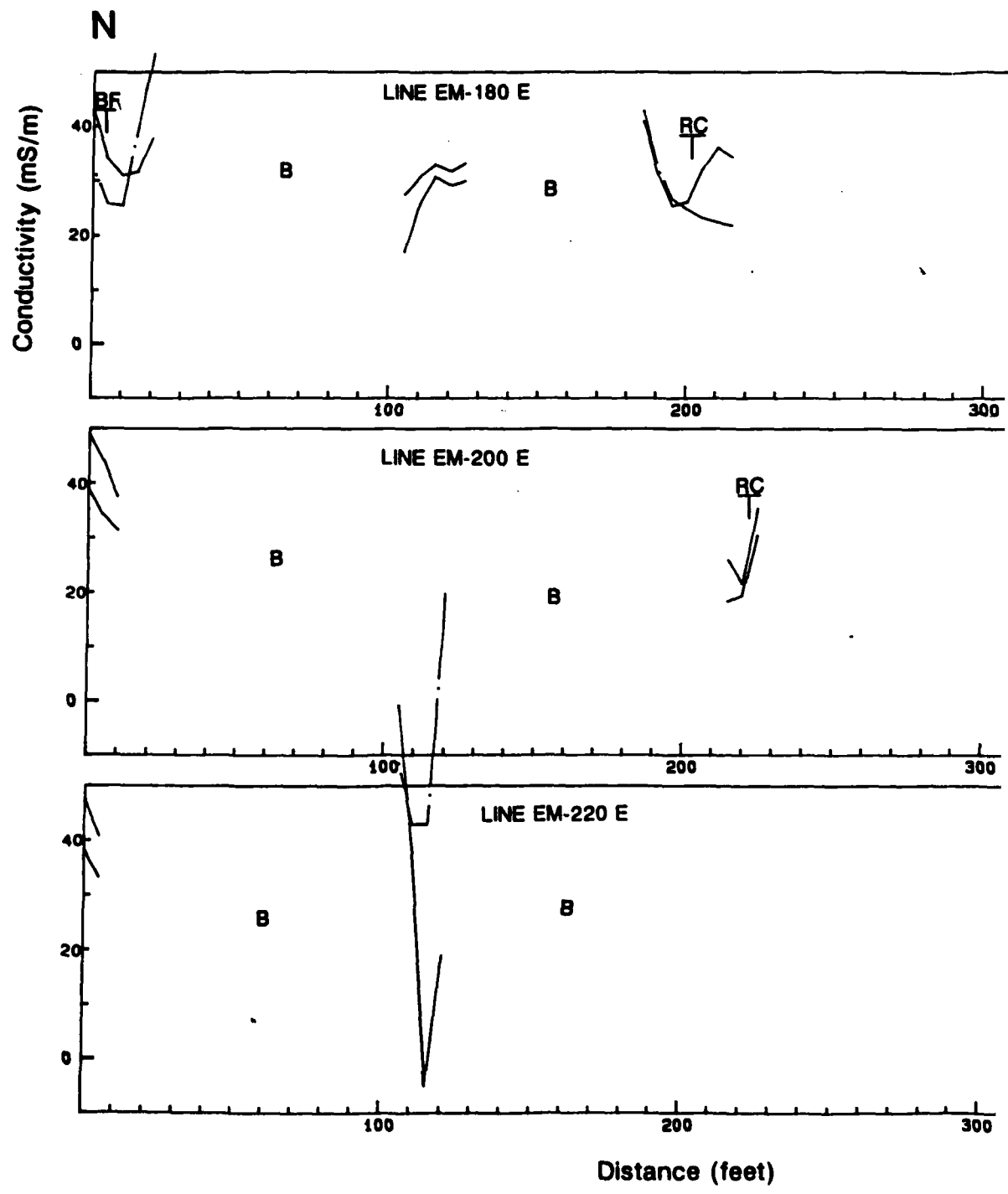
**NOTE:**

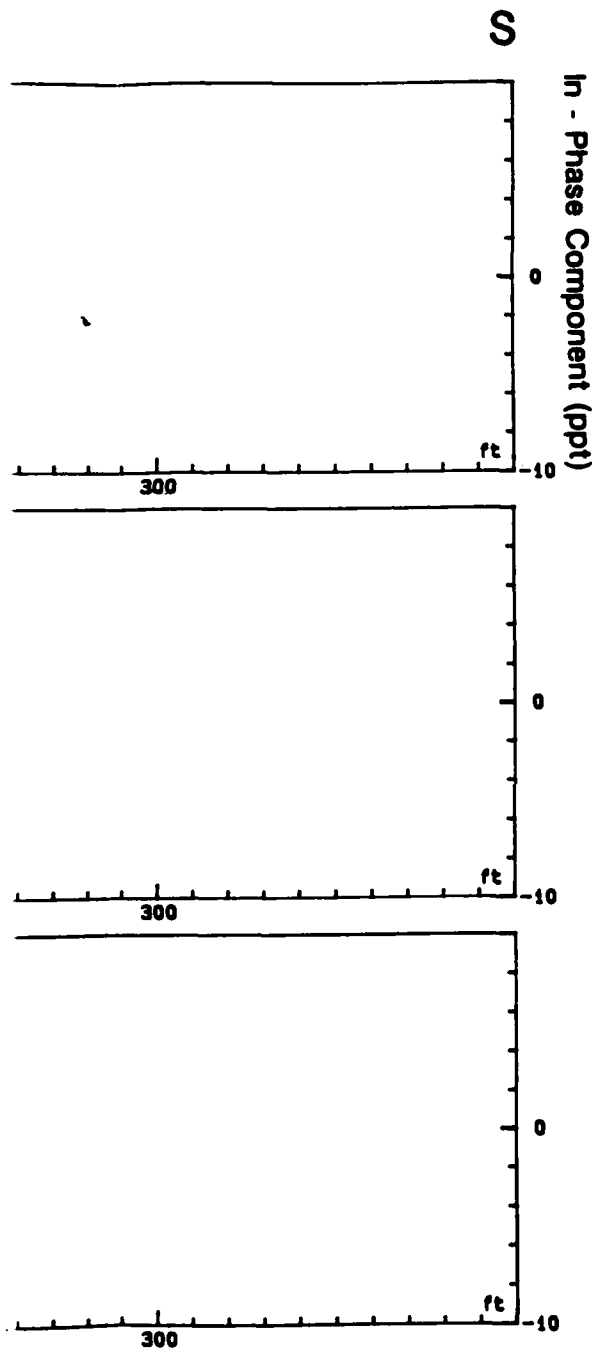
REFER TO FIGURE 1 FOR LOCATION OF SURVEY LINES

FIGURE B-9  
 ELECTROMAGNETIC INDUCTION PROFILES  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 181 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



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 APPROVED BY [Signature]  
 DATE 4-24-91  
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**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

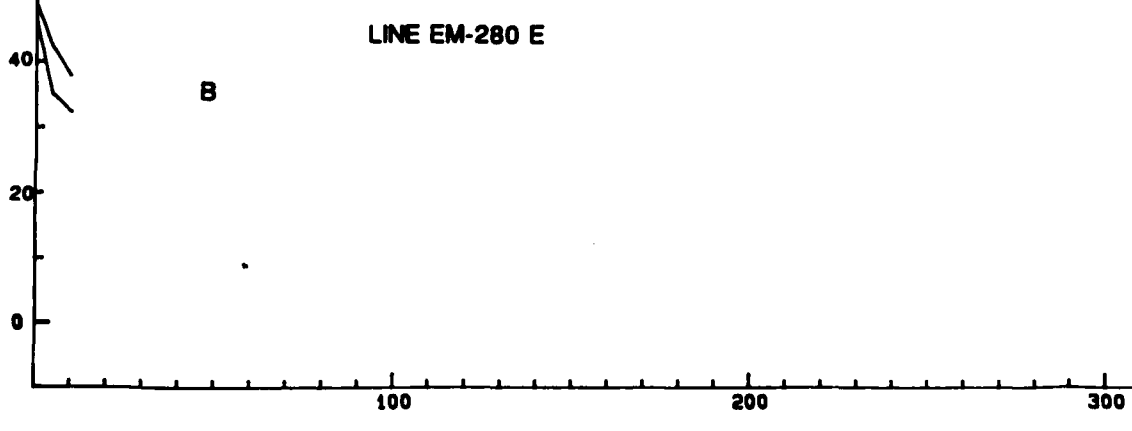
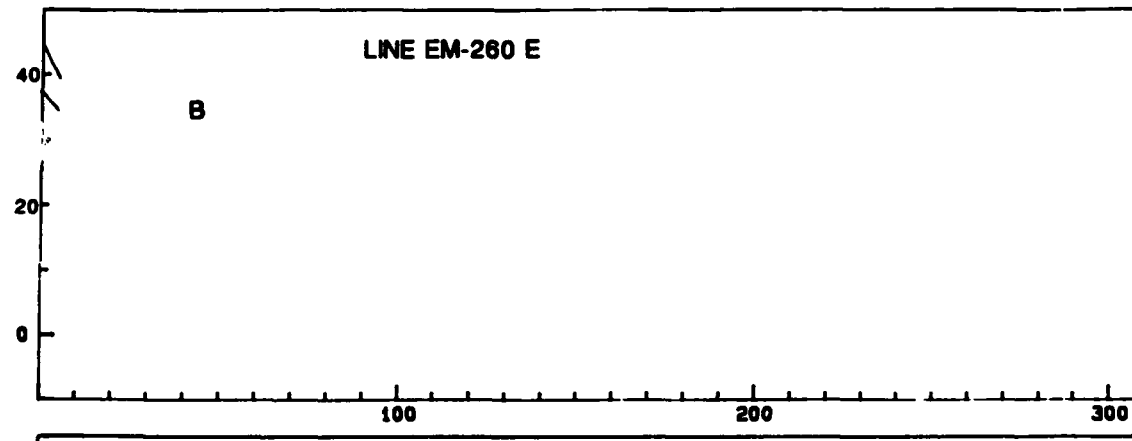
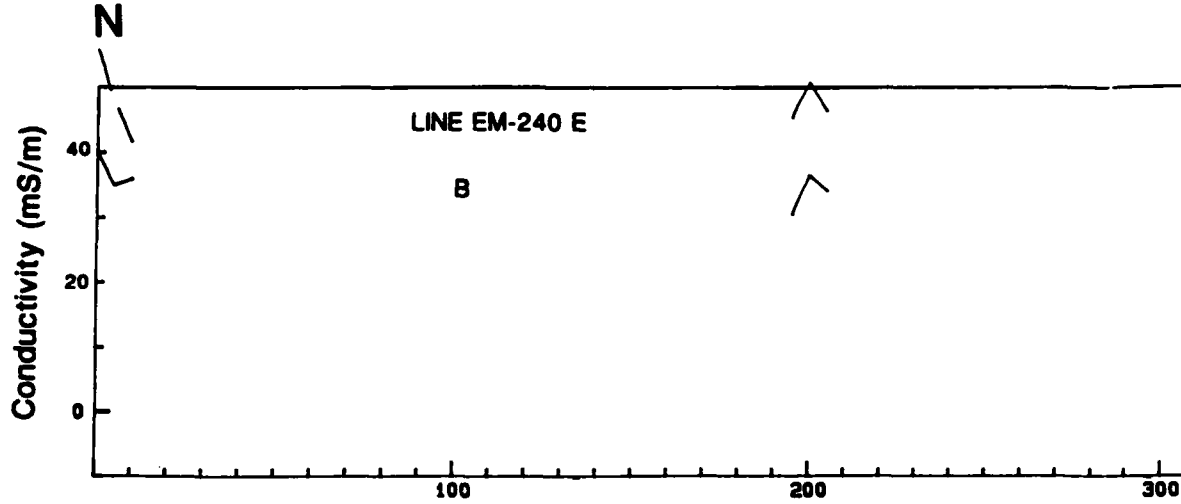
**NOTE:**

REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES

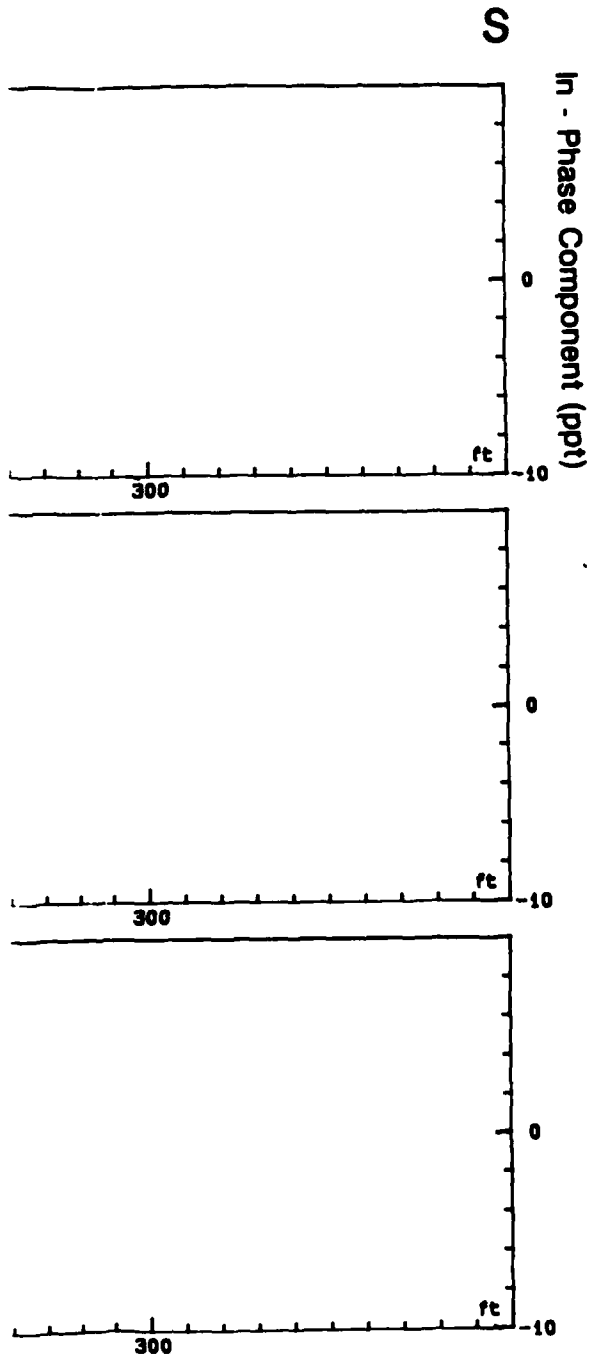
FIGURE B-10  
ELECTROMAGNETIC INDUCTION PROFILES  
SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA



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				4-24-81		



Distance (feet)



**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY -  
MILLISEMENS/METER (mS/m)
- IN-PHASE COMPONENT -  
PARTS PER THOUSAND OF PRIMARY  
ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

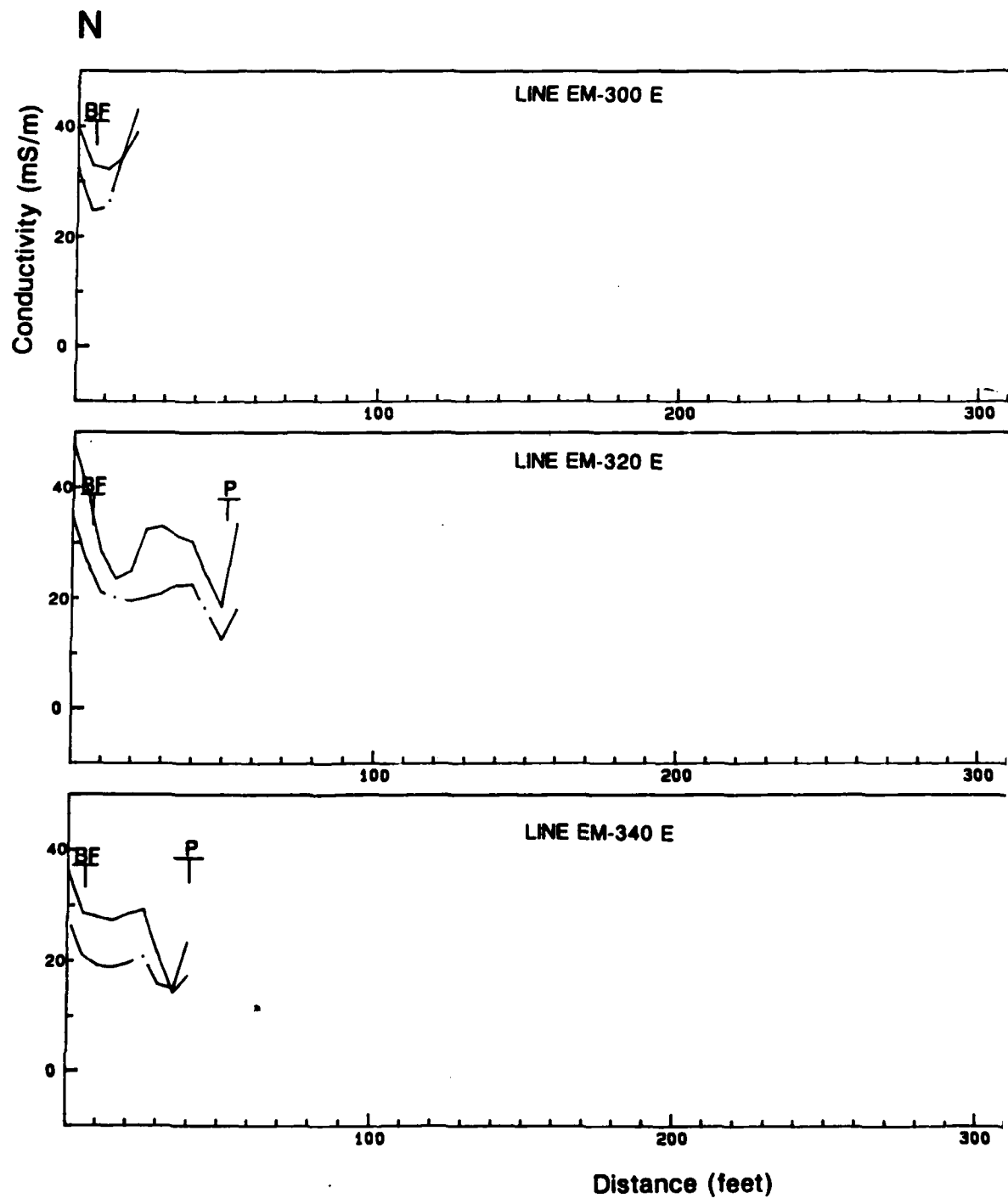
REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES

FIGURE B-11  
ELECTROMAGNETIC INDUCTION PROFILES  
SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA



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		4/30/97	
BY	APPROVED BY	4/30/97	
		4/30/97	





**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY -  
MILLISEMENS/METER (mS/m)
- · — · — IN-PHASE COMPONENT -  
PARTS PER THOUSAND OF PRIMARY  
ELECTROMAGNETIC FIELD (PPT)

**NOTE:**

REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES

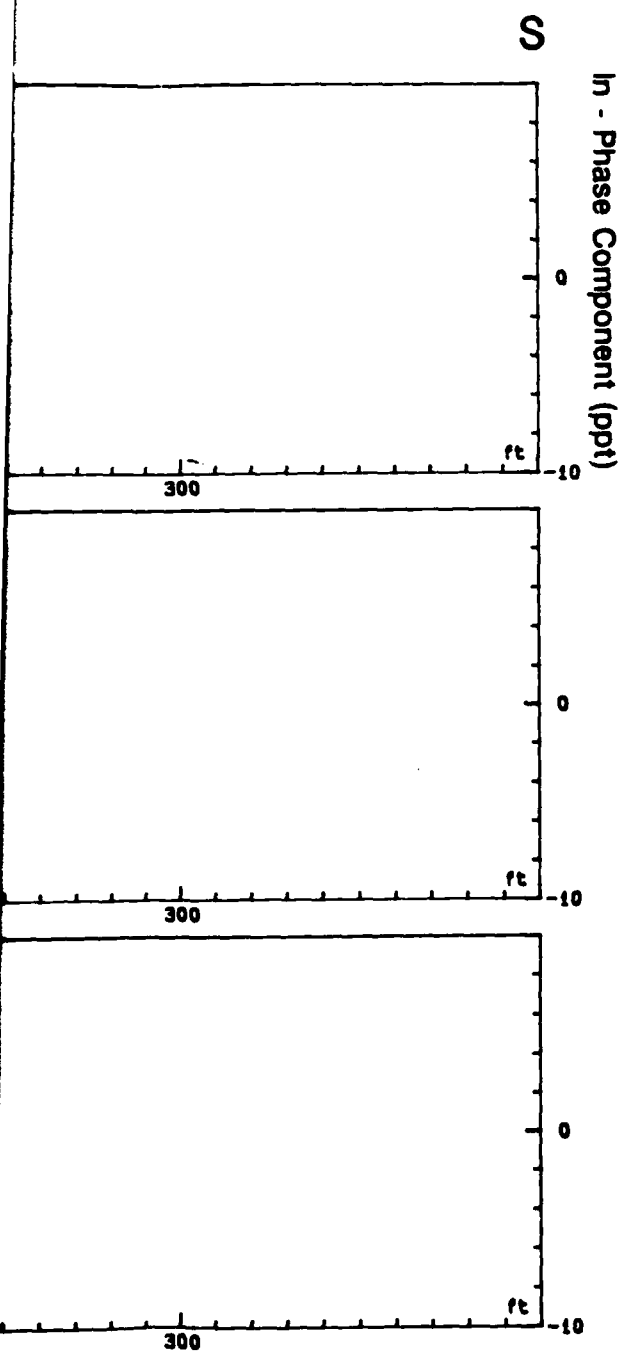


FIGURE B-12

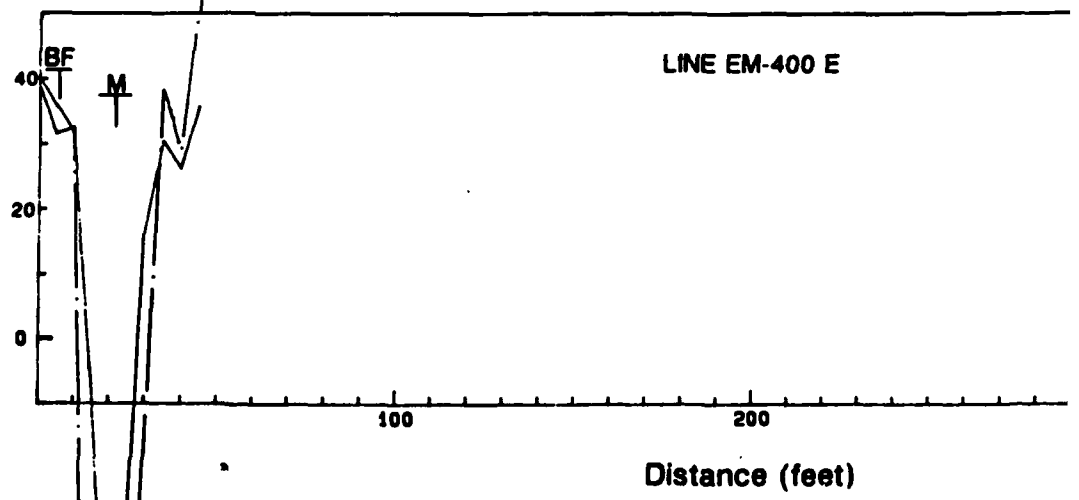
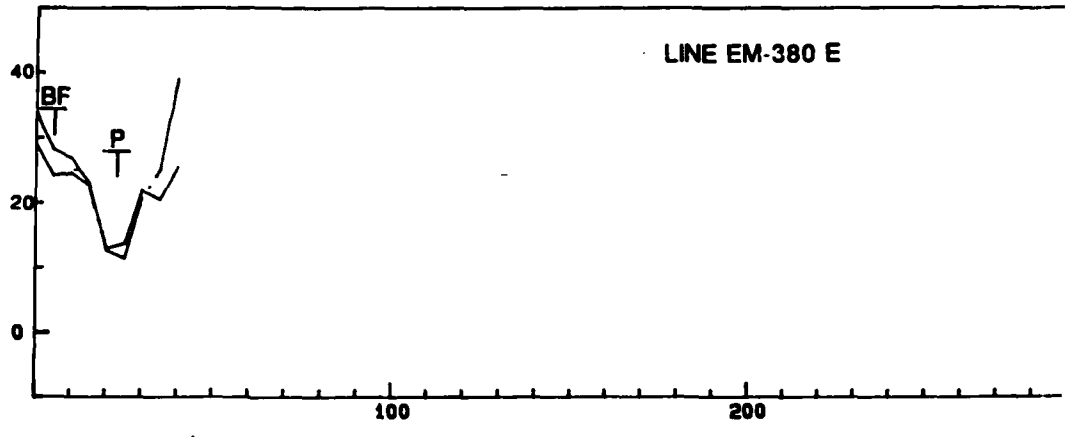
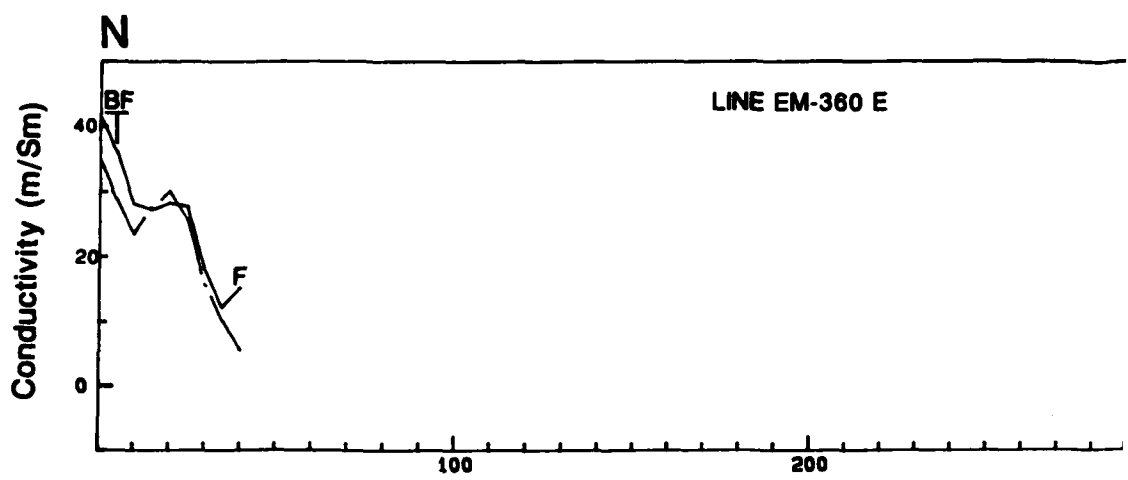
**ELECTROMAGNETIC INDUCTION PROFILES**

SITE 5 - AMMUNITION DISPOSAL AREA  
181 AREFG

SKY HARBOR IAP  
PHOENIX, ARIZONA

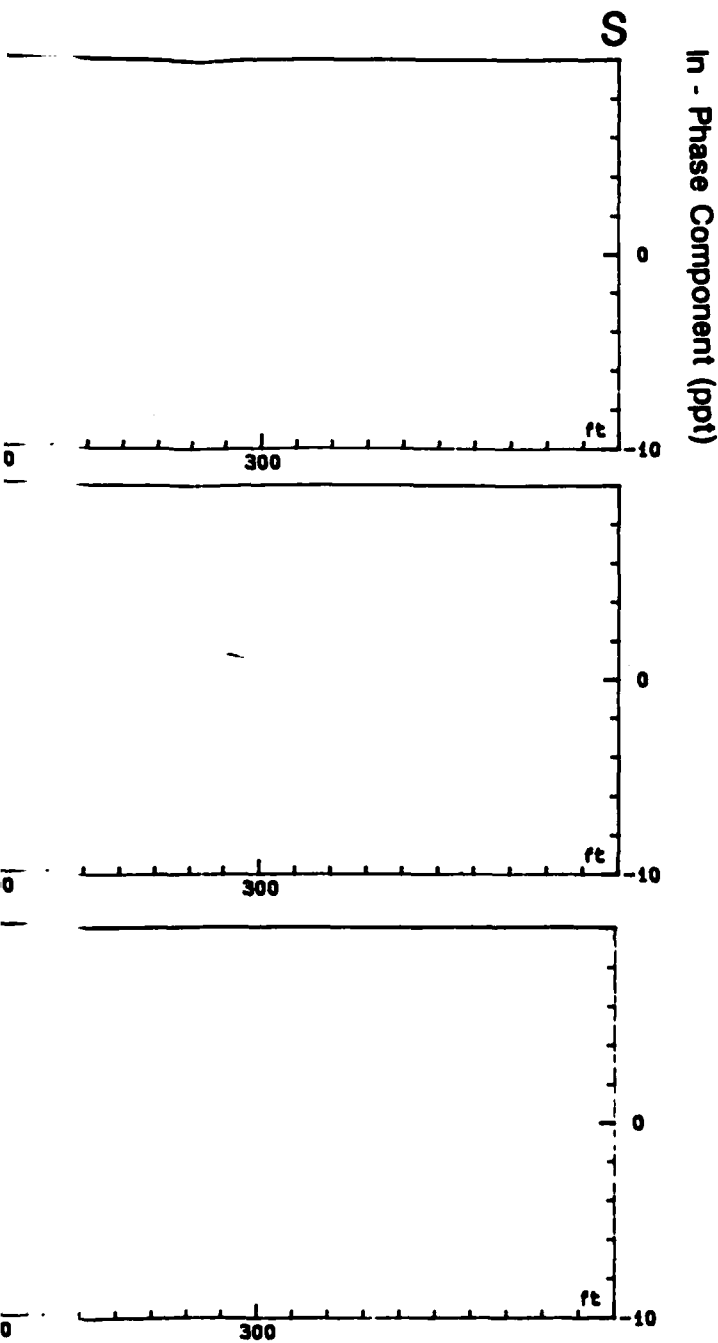


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	4-24-91	APPROVED BY	[Signature]	7/3/91	NUMBER	



047400

Do Not Scale This Drawing



**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

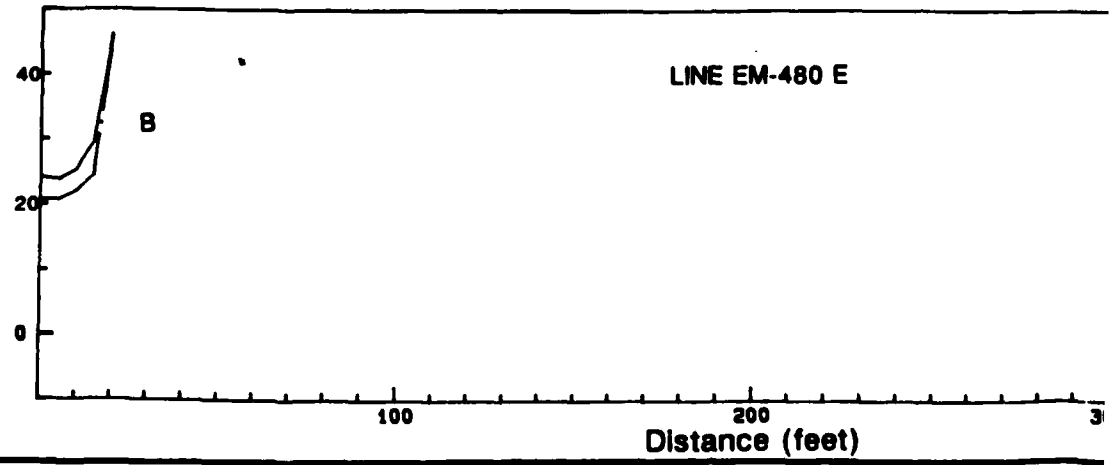
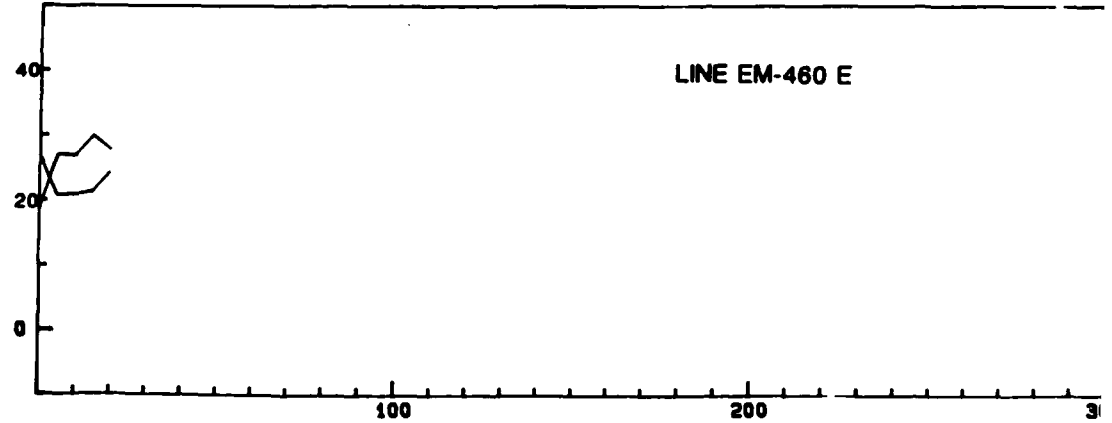
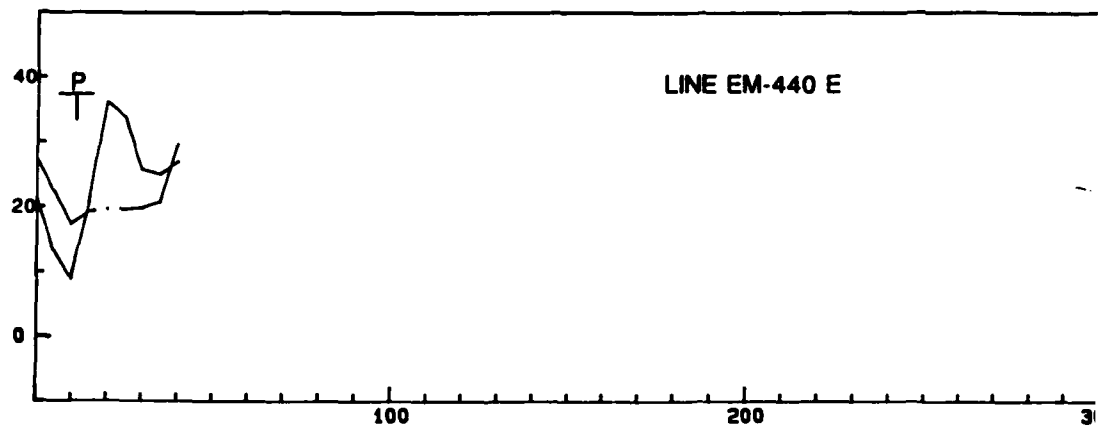
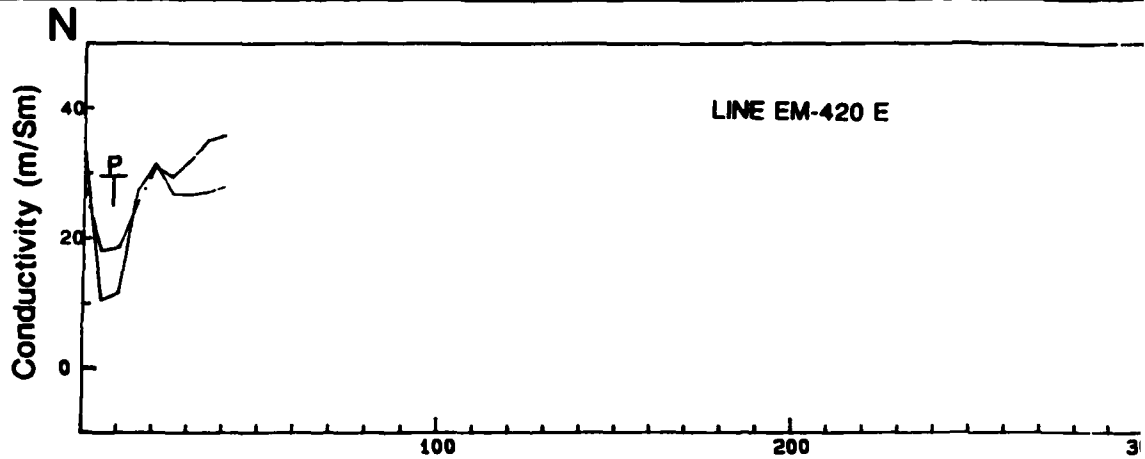
**NOTE:**

REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES

FIGURE B-13  
ELECTROMAGNETIC INDUCTION PROFILES  
SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA

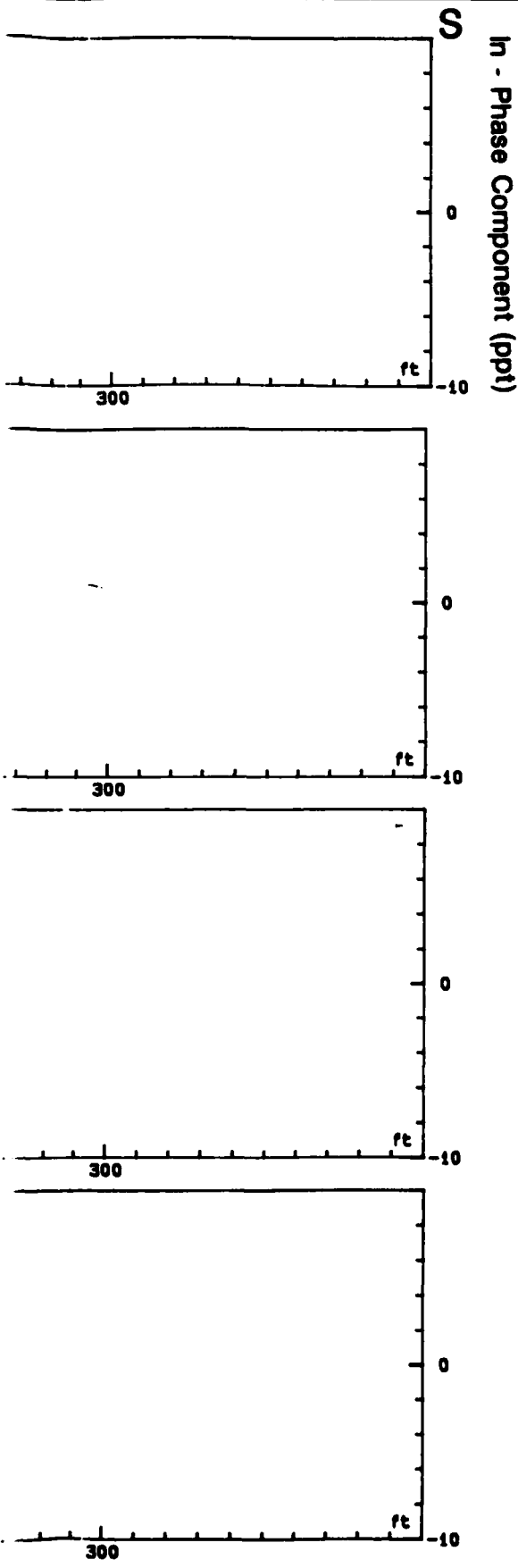


DRAWN BY	J. WALL	CHECKED BY	L.C.	4/30/91	DRAWING NUMBER	409721-B10
	4-24-91	APPROVED BY	SP	4/30/91		



047588

Do Not Scale This Drawing



**LEGEND:**

- B - BUILDING
- BF - BLAST FENCE
- F - FENCE
- FH - FIRE HYDRANT
- LP - LIGHT POLE
- M - MANHOLE
- P - UTILITY
- RC - REINFORCED CONCRETE
- S - SEWER
- V - VEHICLE

- CONDUCTIVITY - MILLISIEMENS/METER (mS/m)
- - - - IN-PHASE COMPONENT - PARTS PER THOUSAND OF PRIMARY ELECTROMAGNETIC FIELD (PPT)

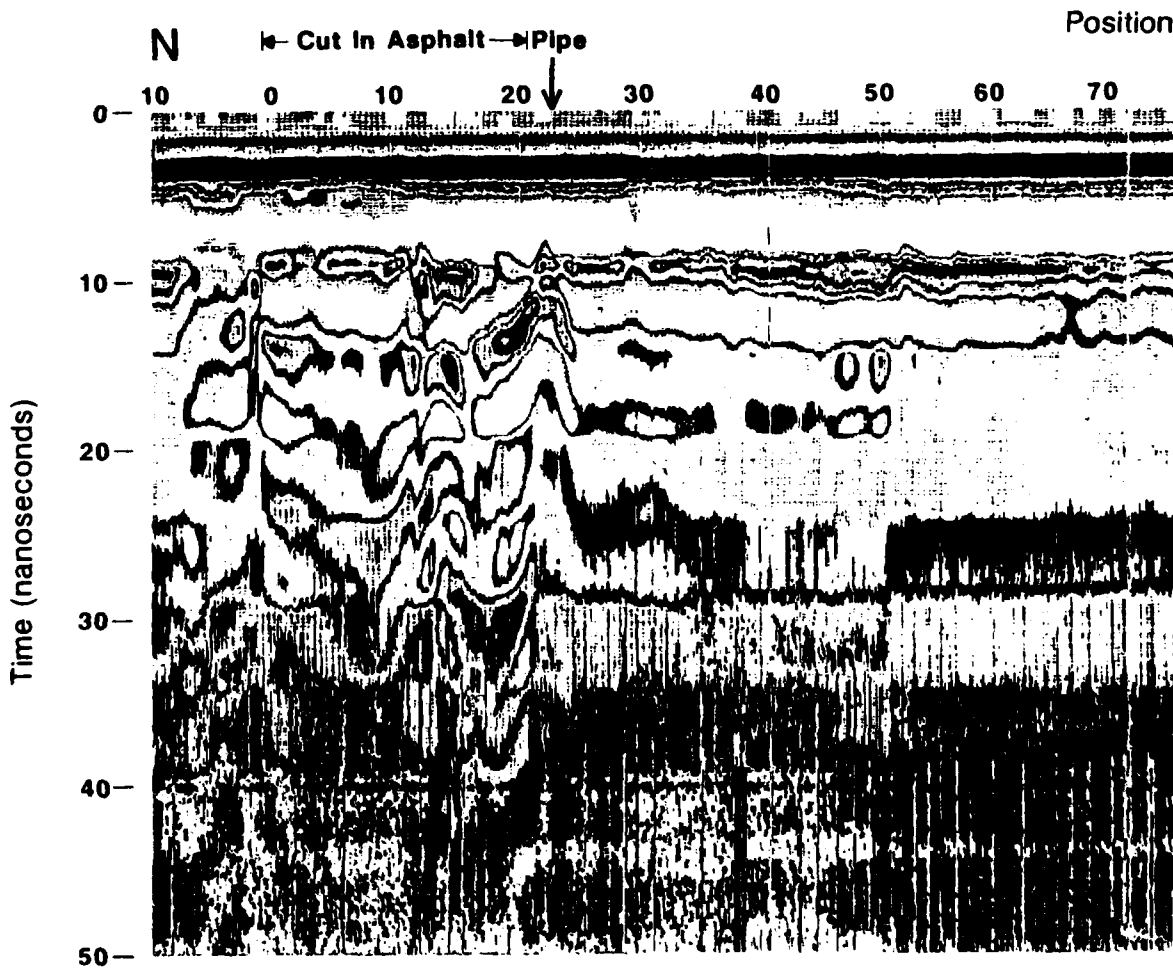
**NOTE:**  
REFER TO FIGURE 1  
FOR LOCATION OF SURVEY LINES

FIGURE B-14  
ELECTROMAGNETIC INDUCTION PROFILES  
SITE 5 - AMMUNITION DISPOSAL AREA  
161 AREFG  
SKY HARBOR IAP  
PHOENIX, ARIZONA



**APPENDIX C**  
**SELECTED GROUND PENETRATING RADAR RECORDS**

DRAWN BY	J. WALL	CHECKED BY	L. C.	DATE	4/30/91	DRAWING NUMBER	409721-B4
BY	4-24-91	APPROVED BY	CGM		4/30/91		



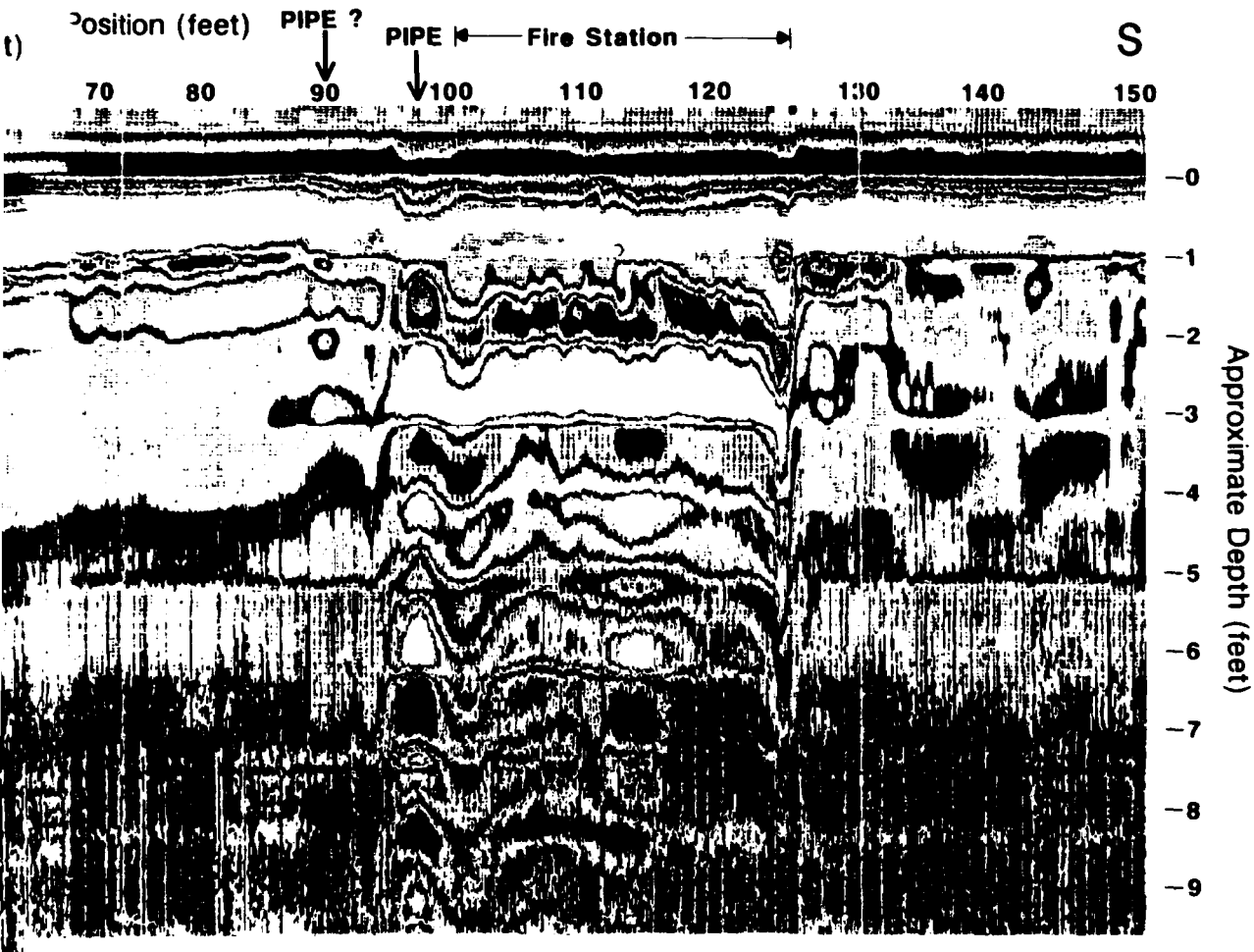


FIGURE C-1

GROUND PENETRATING RADAR

LINE 360 E, 300 MHz ANTENNA  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 161 AREFG

SKY HARBOR IAP  
 PHOENIX, ARIZONA



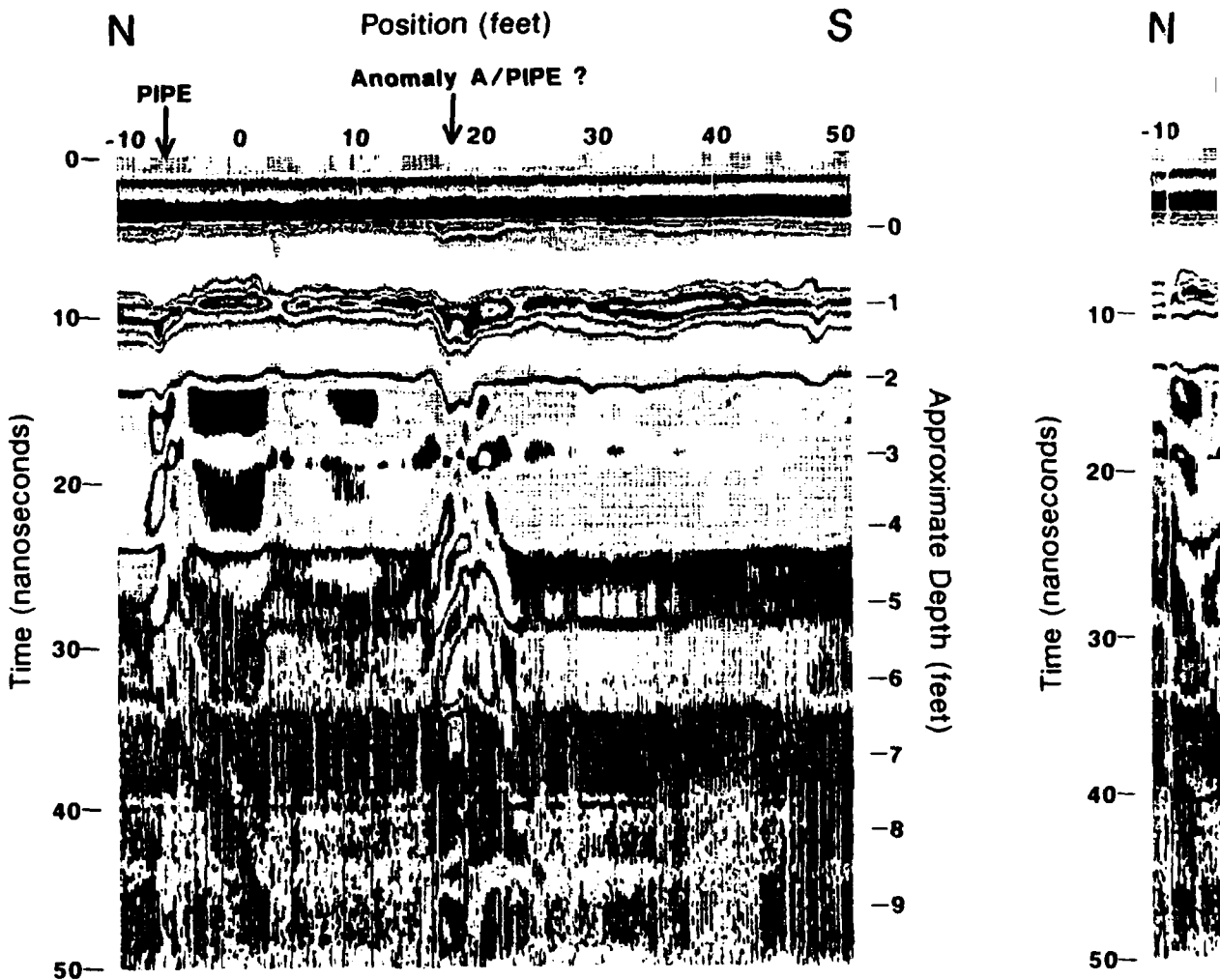


DRAWING NUMBER 409721-B3

4/30/91  
7/31/91

CHECKED BY J.L.  
APPROVED BY [Signature]

DRAWN BY J. WALL  
4-24-91

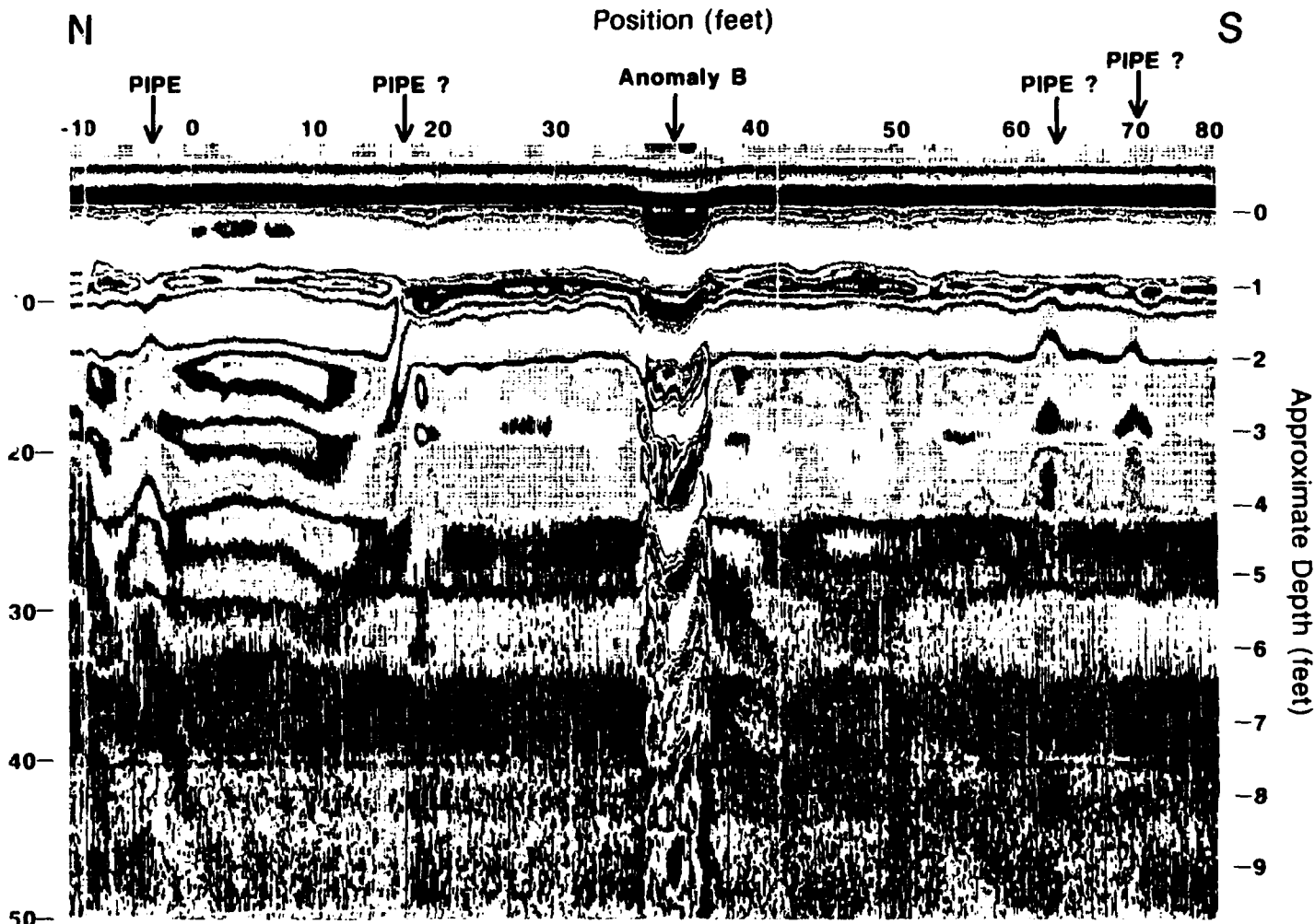


LINE 440 E

06/7/90

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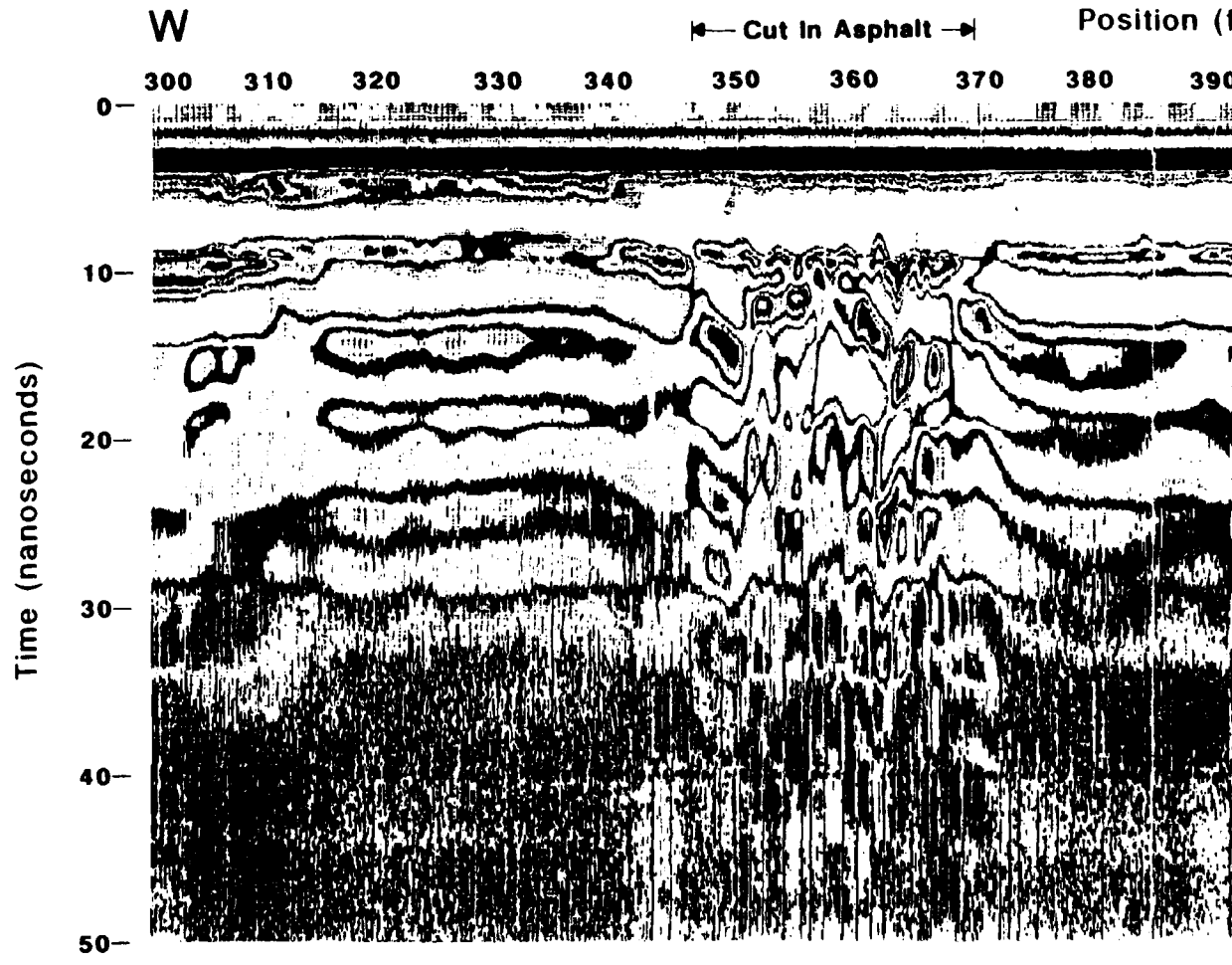
LINE 460 E

FIGURE C-2

GROUND PENETRATING RADAR  
 LINES 440 E & 460 E  
 300 MHz ANTENNA  
 SITE 5 AMMUNITION DISPOSAL AREA  
 161 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA



DRAWN BY	J. WALL	CHECKED BY	J.C.	DRAWING NUMBER	409721-B2
BY	4-24-91	APPROVED BY	29m		
				4/20/91	
				4/30/91	



067400

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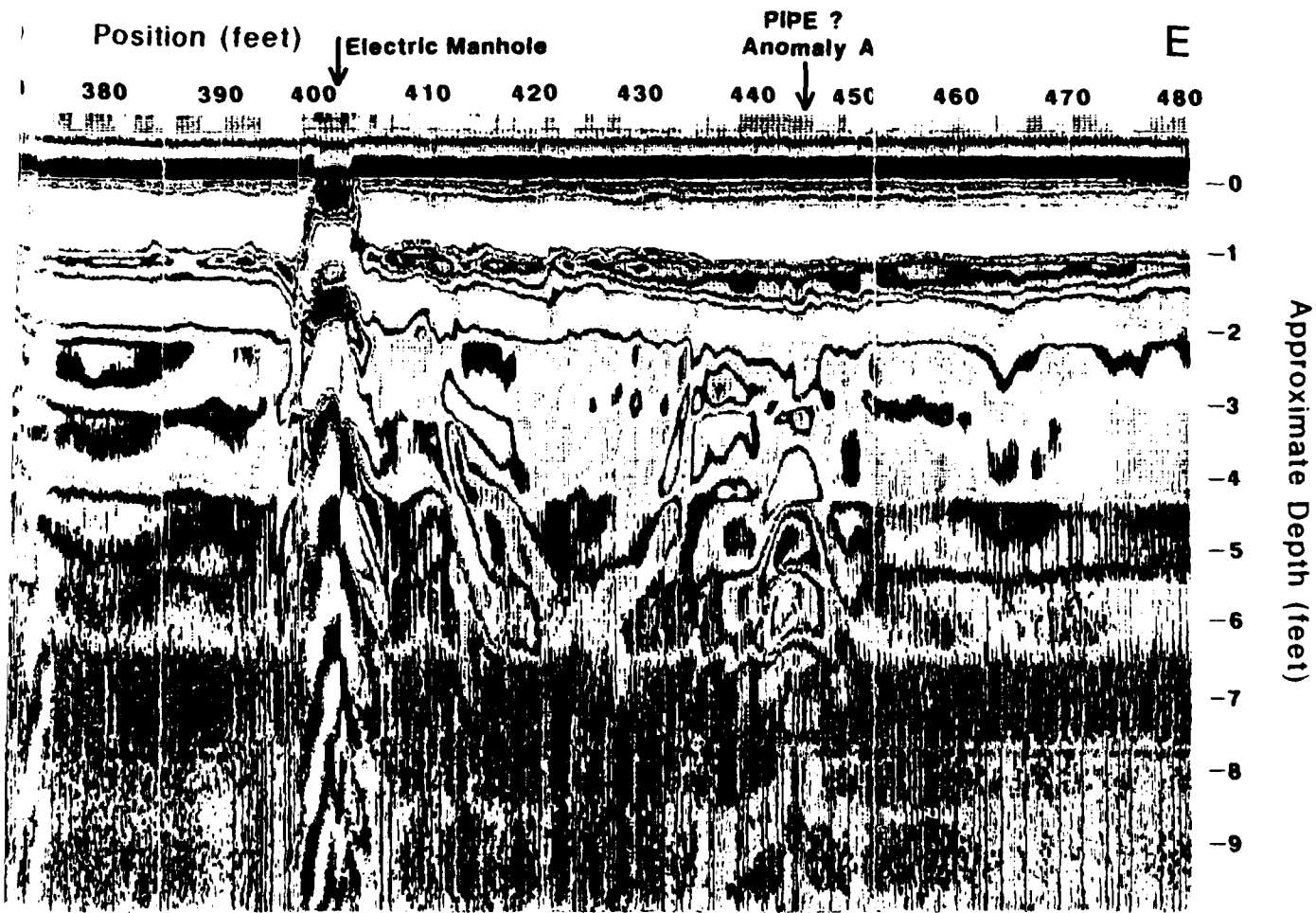


FIGURE C-3

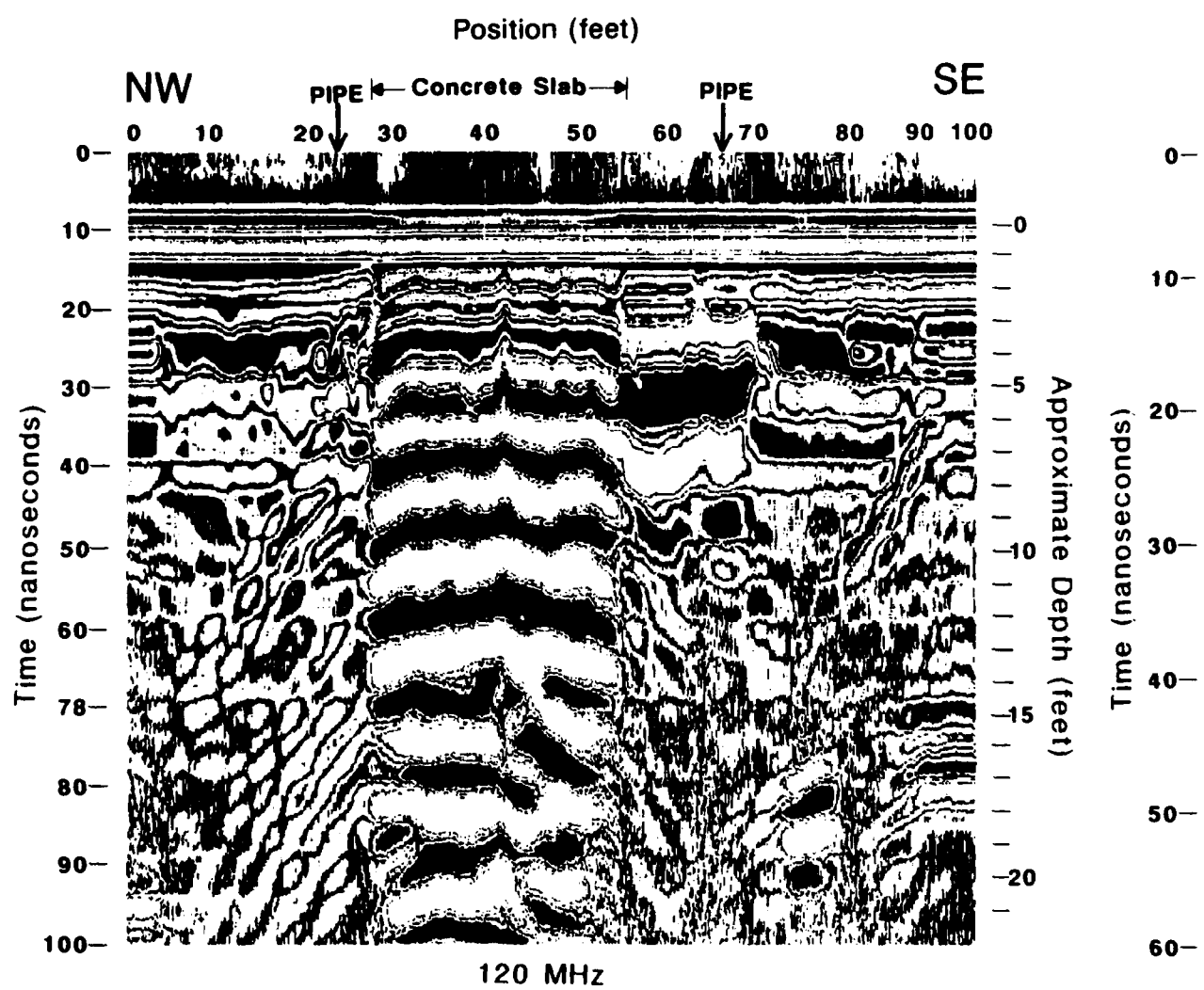
GROUND PENETRATING RADAR

LINE 20 S, 300 MHz ANTENNA  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 161 AREFG

SKY HARBOR IAP  
 PHOENIX, ARIZONA



DRAWING NUMBER	409721-B1
CHECKED BY	L.C.C.
APPROVED BY	[Signature]
DRAWN BY	J. WALL
	4-24-91
	4/30/91
	4/30/91



08/2/00

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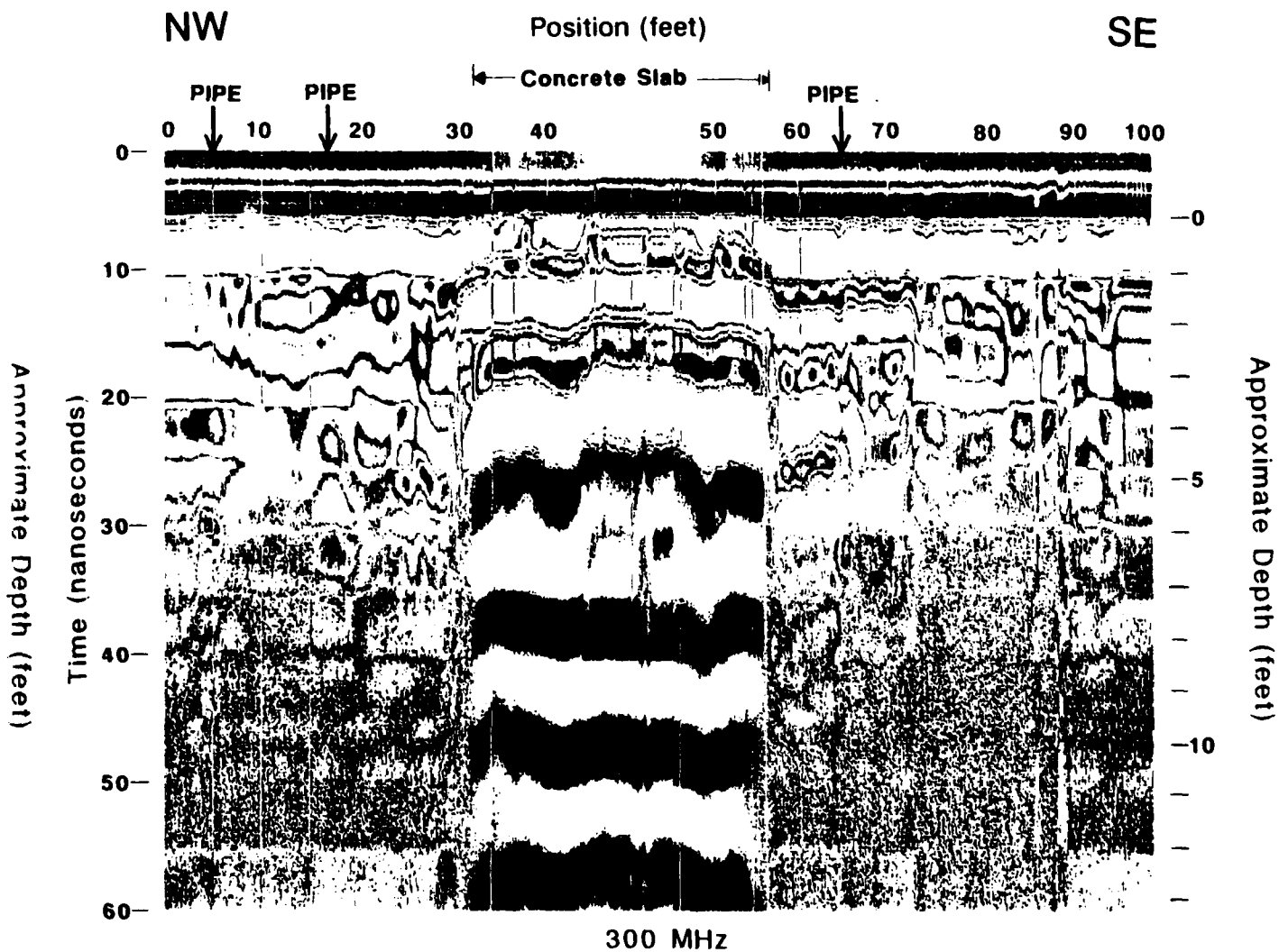


FIGURE C-4  
 GROUND PENETRATING RADAR  
 LINE GPR-4  
 120 AND 300 MHz ANTENNAE  
 SITE 5 - AMMUNITION DISPOSAL AREA  
 161 AREFG  
 SKY HARBOR IAP  
 PHOENIX, ARIZONA

**APPENDIX D**  
**SOV SURVEY REPORT**

**SOIL GAS SURVEY**  
**SKY HARBOR AIR NATIONAL BASE**  
**& PAPAGO MILITARY RESERVATION**  
**PHOENIX, ARIZONA**



**TARGET ENVIRONMENTAL SERVICES, INC.**



SOIL GAS SURVEY  
SKY HARBOR AIR NATIONAL BASE  
& PAPAGO MILITARY RESERVATION  
PHOENIX, ARIZONA

PREPARED FOR

IT CORPORATION  
312 DIRECTORS DRIVE  
KNOXVILLE, TENNESSEE

PREPARED BY

TARGET ENVIRONMENTAL SERVICES, INC.

9180 RUMSEY ROAD  
COLUMBIA, MARYLAND 21045  
(301) 992-6622

FEBRUARY 1991

## EXECUTIVE SUMMARY

From January 15-17, 1991, TARGET Environmental Services, Inc. (TARGET) conducted a soil gas survey at the Sky Harbor Air National Guard Base and at the Papago Military Reservation, Phoenix, Arizona, as part of a site investigation. Samples were analyzed by GC/FID for petroleum hydrocarbons and by GC/ECD for chlorinated hydrocarbons.

Very low levels of FID Total Volatiles occurred in several locations in the JP-4 Hydrant Area and the Hazardous Waste Storage Area at the Sky Harbor Air National Guard Base and at the Papago Military Reservation. None of the standardized FID analytes were present above their 1  $\mu\text{g}/\text{l}$  detection limit in any of the areas at either site.

GC/ECD analysis indicated that relatively low levels of 1,1-dichloroethene (1,1-DCE) were present in samples collected from the JP-4 Hydrant Area and the Hazardous Waste Storage Area at the Sky Harbor Air National Guard Base. Tetrachloroethene (PCE) was observed in all field samples. However, since comparable levels were also observed in all Field Control Samples (indicating persistent carryover in the sampling equipment), it is questionable whether the concentrations present in the field samples accurately reflect conditions in the soil gas at the sampling locations. None of the other standardized halogenated hydrocarbons were present above their respective detection limit in any soil gas samples from either site.

## Introduction

IT Corporation contracted Target Environmental Services, Inc. (TARGET) to perform a soil gas survey at three locations on the Sky Harbor National Guard Base and at one location on the Papago Military Reservation, both in Phoenix, Arizona, as part of a site investigation. The field and analytical phases of the work were performed from January 15-17, 1991.

## Field Procedures

Soil gas samples were collected at a total of 32 locations at the three sites. Fourteen (14) samples were collected at Site 1 (JP-4 Hydrant Area), 11 with the hydraulic probe and 3 with the drive rod. Twelve (12) samples were collected in Site 2 (Hazardous Waste Storage Area), all using the hydraulic probe. Sampling was attempted but was unsuccessful in three locations in Site 3 (Fuel Bladder Area). Six (6) samples were collected at the hazardous waste collection area on the Papago Military Reservation, all with the drive rod. Sampling order is included in Table 1 and sampling depths are shown in Table 2.

To collect samples with the van-mounted hydraulic probe, the probe was used to advance connected 3' sections of 1" diameter threaded steel casing down to the sampling depth. Although the proposed sampling depth was 10', some samples were collected at shallower depths due to probe refusal. The entire sampling system was purged with ambient air drawn through an organic vapor filter cartridge. A teflon line was inserted into the casing to the bottom of the hole, and the bottom-hole line perforations were

isolated from the up-hole annulus by an inflatable packer.

To collect samples with the drive rod, a 1/2 inch hole was produced to the sampling depth. Where pavement was present, an electric hammer drill was employed for penetration prior to using the drive rod. The entire sampling system was purged with ambient air drawn through an organic vapor filter cartridge, and a stainless steel probe was inserted to the full depth of the hole and sealed off from the atmosphere.

Whether using the hydraulic probe or the drive rod, a sample of in-situ soil gas was then withdrawn through the probe and used to purge atmospheric air from the sampling system. A second sample of soil gas was withdrawn through the probe and encapsulated in a pre-evacuated glass vial at two atmospheres of pressure (15 psig). The self-sealing vial was detached from the sampling system, packaged, labeled, and transported to the laboratory for analysis.

Prior to the day's field activities all sampling equipment, drive rods, and probes were decontaminated by washing with soapy water and rinsing thoroughly. Internal surfaces were flushed dry using pre-purified nitrogen, and external surfaces were wiped clean using clean paper towels.

Field control samples were collected at the beginning and end of each day's field activities and after finishing a day's sampling in an area. These QA/QC samples were obtained by inserting the probe tip into a tube flushed by a 20 psi flow of pre-purified nitrogen and collecting in the same manner as described above.

### Laboratory Procedures

All of the samples collected during the field phase of the survey were subjected to dual analyses in the field in TARGET's climate-controlled mobile laboratory using a Shimadzu 14-A gas chromatograph.

The first analysis was conducted according to EPA Method 601 (modified) on a gas chromatograph equipped with an electron capture detector (ECD), but using direct injection instead of purge and trap. Specific analytes standardized for this analysis were:

1,1-dichloroethene (1,1-DCE)  
1,1,1-trichloroethane (1,1,1-TCA)  
tetrachloroethene (PCE)

Ten other halogenated hydrocarbons are also included in TARGET's standard gas mixture and are standardized in every analytical batch. These compounds (and their respective detection limits, in  $\mu\text{g}/\text{l}$ ) are trichlorofluoromethane (0.05), methylene chloride (1.0), trans-1,2-dichloroethene (1.0), 1,1-dichloroethane (1.0), cis-1,2-dichloroethene (1.0), chloroform (0.10), carbon tetrachloride (0.05), trichloroethene (0.10), 1,1,2-trichloroethane (0.10), and 1,1,2,2-tetrachloroethane (0.1).

The second analysis was conducted according to EPA Method 602 (modified) on a gas chromatograph equipped with a flame ionization detector (FID), but using direct injection instead of purge and trap. The analytes selected for standardization in this analysis were:

benzene  
toluene  
ethylbenzene  
meta- and para- xylene  
ortho-xylene

These compounds were chosen because of their utility in evaluating the presence of fuel products, or petroleum based solvents.

The FID Total Volatiles values were generated by summing the areas of all chromatogram peaks and calculated using the instrument response factor for toluene. Injection peaks, which also contain the light hydrocarbon methane, were excluded to avoid the skewing of the Total Volatiles (Totals) values due to injection disturbances and biogenic methane. For samples with low hydrocarbon concentrations, the calculated Total Volatiles concentration is occasionally lower than the sum of the individual analytes. This is because the response factor used for the Total Volatiles calculation is a constant, whereas the individual analyte response factors vary with concentration. It is important to understand that the Total Volatiles levels reported are relative, not absolute, values.

The analytical equipment was calibrated using an instrument-response curve and injection of known concentrations of the above standards. Retention times of the standards were used to identify the peaks in the chromatograms of the field samples and their response factors were used to calculate the analyte concentrations. The tabulated results of the laboratory analyses of the soil gas samples are reported in micrograms per liter ( $\mu\text{g}/\text{l}$ ) in Tables 3 through 5. Although "micrograms per liter" is equivalent to "parts per billion (v/v)" in water analyses, they are not equivalent in gas analyses, due to the difference in the mass of equal volumes of water and gas matrices.

For QA/QC purposes, a duplicate analysis was performed on

every tenth field sample. Laboratory blanks of nitrogen gas (99.999%) were also analyzed after every tenth field sample.

#### Quality Assurance Samples

All laboratory blanks were free of detectable levels of the standardized analytes.

All Field Control Samples contained tetrachloroethene (PCE) ranging from 0.08 to 4.0  $\mu\text{g}/\text{l}$ , indicating persistent carryover in the sampling equipment. The PCE observed in the field samples (0.60 to 6.7  $\mu\text{g}/\text{l}$ ) may not accurately reflect conditions in the soil gas at the sampling locations. Unsuccessful attempts were made to remove the contamination from the sampling equipment. Instead of immediately outflushing the nitrogen drawn into the sampling system during the purging step, the nitrogen was allowed to set in the sampling box for 5 minutes prior to flushing. In addition, sampling boxes were evacuated for 1/2 hour at the end of each day.

Analyte concentrations in duplicate sample pairs were within acceptable limits.

TABLE 1

SAMPLING ORDER

JANUARY 15, 1991

SITE 2  
SAMPLE

1\*  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13\*\*

SITE 1  
SAMPLE

1  
2  
3  
4  
5\*\*\*

JANUARY 16, 1991

SITE 1  
SAMPLE

6\*  
7  
8  
9  
10  
11  
12  
13\*\*

SITE 2  
SAMPLE

14  
15\*\*\*

JANUARY 17, 1991

SITE 4  
SAMPLE

1\*  
2  
3  
4  
5  
6  
7  
8\*\*

SITE 1  
SAMPLE

14  
15  
16  
17  
18\*\*\*

\* Beginning of Day, Field Control Sample

\*\* Field Control Sample

\*\*\*End of Day, Field Control Sample



TABLE 2

SAMPLING DEPTH SITE 1

<u>SAMPLE</u>	<u>FEET</u>
1	10
2	9
3	10
4	10
7	10
8	10
9	10
10	10
11	7
12	7
14	10
15	4
16	4
17	4

SAMPLING DEPTH SITE 2

<u>SAMPLE</u>	<u>FEET</u>
2	10
3	10
4	10
5	10
6	10
7	9
8	10
9	10
10	9
11	9
12	10
14	10

SAMPLING DEPTH SITE 4

<u>SAMPLE</u>	<u>FEET</u>
2	2
3	2
4	4
5	3
6	2
7	2

**TABLE 3**

\*LABORATORY RESULTS FOR SITE 1  
CONCENTRATIONS IN MICROGRAMS PER LITER

SAMPLE	BENZENE	TOLUENE	ETHYL- BENZENE	m- & p- XYLENE	o- XYLENE	FID TOTAL VOLATILES <sup>1</sup>	11DCE	111TCA	PCE
1	<1.0	<1.0	<1.0	<1.0	<1.0	1.5	<1.0	<0.10	6.0
2	1.3	<1.0	<1.0	<1.0	<1.0	12	<1.0	<0.10	5.2
3	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.4	<0.10	6.0
4	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	2.2	<0.10	4.2
7	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.62
8	<1.0	<1.0	<1.0	<1.0	<1.0	1.1	<1.0	<0.10	6.7
9	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	5.7
10	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.1
11	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.6
12	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.1
14	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	4.8
15	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.8
16	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.75
17	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.83

\* BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

11DCE = 1,1-dichloroethene  
111TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

TABLE 3 (cont)

\*LABORATORY RESULTS FOR SITE 1  
CONCENTRATIONS IN MICROGRAMS PER LITER

SAMPLE	BENZENE	TOLUENE	ETHYL- BENZENE	m- & p- XYLENE	o- XYLENE	FID TOTAL VOLATILES <sup>1</sup>	11DCE	111TCA	PCE
<u>FIELD CONTROL SAMPLES</u>									
5	<1.0	<1.0	<1.0	<1.0	<1.0	7.7	<1.0	<0.10	0.42
6	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.08
13	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.11
18	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.38
<u>LABORATORY DUPLICATE ANALYSES</u>									
15	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.8
15R	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.9
<u>LABORATORY BLANKS</u>									
BCITP-1	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	<0.05

\* = BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

11DCE = 1,1-dichloroethene  
111TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

**TABLE 4**

**\*LABORATORY RESULTS FOR SITE 2  
CONCENTRATIONS IN MICROGRAMS PER LITER**

SAMPLE	BENZENE	TOLUENE	ETHYL- BENZENE	m- & p- XYLENE	o- XYLENE	FID TOTAL, XYLENE VOLATILES <sup>1</sup>	1,1DCE	1,1,1TCA	PCE
2	<1.0	<1.0	<1.0	<1.0	<1.0	1.0	1.3	<0.10	5.6
3	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.6	<0.10	4.5
4	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.7	<0.10	3.2
5	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.6	<0.10	4.0
6	<1.0	<1.0	<1.0	<1.0	<1.0	1.1	1.2	<0.10	1.9
7	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.5	<0.10	2.1
8	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.2	<0.10	1.5
9	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.6
10	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.4
11	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	3.3
12	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.5	<0.10	2.6
14	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.7

\* = BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

1,1DC = 1,1-dichloroethene  
1,1,1TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

TABLE 4 (cont)

\*LABORATORY RESULTS FOR SITE 2  
CONCENTRATIONS IN MICROGRAMS PER LITER

SAMPLE	BENZENE	TOLUENE	ETHYL- BENZENE	m- & p- XYLENE	o- XYLENE	FID TOTAL VOLATILES <sup>1</sup>	11DCE	111TCA	PCE
<u>FIELD CONTROL SAMPLES</u>									
1	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	4.0
13	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.3
15	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.45
<u>LABORATORY DUPLICATE ANALYSES</u>									
10	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.4
10R	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.4
14	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.7
14R	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	2.5

\* = BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

11DCE = 1,1-dichloroethene  
111TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

TABLE 4 (cont)

\*LABORATORY RESULTS FOR SITE 2  
CONCENTRATIONS IN MICROGRAMS PER LITER

SAMPLE	BENZENE	TOLUENE	ETHYL- BENZENE	m- & p- XYLENE	o- XYLENE	FID TOTAL, XYLENE VOLATILES <sup>1</sup>	11DCE	111TCA	PCE
<u>LABORATORY BLANKS</u>									
BCITP-1	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	<0.05
BCITP-2	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	<0.05

\* = BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

11DCE = 1,1-dichloroethene  
111TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM  
PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

**TABLE 5**

**\*LABORATORY RESULTS FOR SITE 4  
CONCENTRATIONS IN MICROGRAMS PER LITER**

<u>SAMPLE</u>	<u>BENZENE</u>	<u>TOLUENE</u>	<u>ETHYL- BENZENE</u>	<u>m- &amp; p- XYLENE</u>	<u>o- XYLENE</u>	<u>FID TOTAL, VOLATILES<sup>1</sup></u>	<u>11DCE</u>	<u>111TCA</u>	<u>PCE</u>
2	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	4.2
3	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.3
4	<1.0	<1.0	<1.0	<1.0	<1.0	1.2	<1.0	<0.10	0.60
5	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.3
6	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	1.9
7	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.75

FIELD CONTROL SAMPLES

1	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.46
8	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	0.17

LABORATORY BLANKS

BCITP-1	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.10	<0.05
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\* = BTEX WERE ANALYZED VIA GC/FID AND HALOCARBONS WERE ANALYZED VIA GC/ECD.

11DCE = 1,1-dichloroethene  
111TCA = 1,1,1-trichloroethane  
PCE = tetrachloroethene

<sup>1</sup>CALCULATED USING THE SUM OF THE AREAS OF ALL INTEGRATED CHROMATOGRAM PEAKS AND THE INSTRUMENT RESPONSE FACTOR FOR TOLUENE

**APPENDIX E**  
**SOIL BORING LOGS**



BORING LOG	BORING/WELL NO.: SKY PIEZOMETER #1 (PS-1)	Page 1 of 1
Installation: SKY HAZWOP ANG	Site: JRT 1/14/91	
Project No. 40721.02.06	Client/Project: HAZWRAP / SKY HAZWOP ANG	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	Driller: DWIGHT PETERSON
Drig Started: 1/15/91 (0950 AM)	Drig Ended: 1/15/91 (1335 AM)	Borehole dia(s): 9 3/4"
Drig Method/Rig Type: AIR Hammer Casing		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (MODIFIED)

Depth (ft)	Sample No	Sample Lab	Anal. (Y/N)	Recovery (%)	Lithologic Description	Mudbit Coring USES	Blows/6 inch	Graphic Log	Well data	Water depth & Remarks	Elev (ft)
0-9 ft					SAND: <sup>RED</sup> Brown, med. grad at top; transition to border. 1A. Contains w/sand. 70-80% w/sand.	10R					1120.08
9-19 ft					SAND. Brown, med grad; grad of some sand at ~ 16 ft.	3/8					
19-29 ft					SAND - Brown, med grad, med. to coarse grad. Some grad at 25 & 26 ft. Same as above, etc.	2 3/4					
29-34 ft					Same. Note: At ~ 34 ft Dark Brown DUNE MATERIAL SAND out of casing.	4/4					
34-49 ft					HAZ. Runny 5 ft at top. DUNE. Casing NO RUNNING. (Shattering 20-30 ft).						
49-59 ft					Same as above. Back to DRY SAND. <sup>MOIST</sup> Wet at 50 ft. (No ID readings).						
59-70 ft					Same as above. (No ID readings) DRY, NO ID readings. Some sorted brown sand; coarse w/ gravel. Coarse air at 60 ft.						
70-80 ft					Wet. HIT WATER ca. 73-74 ft. Brown sand, poorly sorted, coarse grad. Occasional gravel; one COBBLE LATITE at ca. 76 ft.	2.5				73-74 ft. WATER	
80-90 ft					Same as above. Some fine water.	4R					
90-100 ft					Same as above.	5/4					

BORING DEPTH = 100.5 ft.

NOTE: NO SAMPLER IN USE; OBSERVATIONS ARE FROM CUTTINGS AS COLLECTED AT THE CYCLONE. SOME STRIKE SLIPS ARE NOTED, WHERE POSSIBLE.

U = Thin wall Tube	R = Rock Coring	_____ NA	Field G/C (Make/Mod.)	_____ NA
S = Split spoon (tube)	O = Other	_____ NA	G/C Oper.:	_____ NA
C = Cuttings	Notes: <u>NO SAMPLER IN USE</u>			

BORING LOG	BORING/WELL NO.: PS-2	Page 1 of 1
Installation: Sky Harbor ANG	Site:	
Project No. 40921.02.05	Client/Project: HAZWRAP / Sky Harbor ANG	
HAZWRAP Contractor: IT Corporation	Drill Contractor: LAYNE Environmental	Driller: DAVID PETERSON
Drill Started: 12/20/89 (10:15 a.m.)	Drill Ended: 1/16/91 (10:15 a.m.)	Borehole dia(s): 9 3/4 inches
Drill Method/Rig Type: Air Hammer Casing		
Logged by: GARDNER	E-Log (Y/N) (N)	From _____ to _____
		Protection Level: D (non-rad)

DEPTH (ft)	Sample No	Lab Anal (Y/N)	RECOVERY (%)	Lithologic Description	Muswell Coring USCS	Blows/6 inch	Graphic Log	Well Data	Water Depth & Remains	Elevation
0				0-10ft: SAND, DAMP, POORLY SORTED, medium to coarse grained. COBBLES at 6 ft. LT. BRN.	SP					114.16
10				10-20 ft: (COBBLES at 15ft, 18ft.) SAME	GP					
20				20-30ft: (COBBLES at 21): SAND, POORLY SORTED coarse to very coarse. some large occas. grav. GRAVEL; 13 rows down at 29ft.	SP					
30				30-40 ft: SAND AS 20-30ft. except some gravel w/ COBBLES & is very angular	GP					
40				40-50ft: SAND; <del>very</del> very coarse grained DARK BROWN, angular, poorly sorted. Gravel, occasional COBBLES DAMP.	SP					
50				50-60ft: SAND; POORLY SORTED very coarse grained SAND to small gravel. Occasional small COBBLES. DAMP. DARK BROWN	SP					
60				60-70ft: Same as above, except no small angular gravel DAMP (water c. 75')	SP					
70				70-80ft: Same as 60-70ft. DAMP to wet (Water c. 75').	SP				Water at approx 75'	
80				80-90ft: Same to ca. 88ft 88-90ft: MOSTLY GRAVEL & COBBLES w/ FINE TO MEDIUM GRAINED SILTY SANDS stick to them. STICKY, wet, DARK BROWN	GP					
90				90-100ft: Blow water. Same as 80-90ft section coarse gravel & sand w/ SILT.	GM					

BOREHOLE DEPTH = ~ 100' 8"

NOTE: NO SAMPLER IN USE; OBSERVATIONS ARE FROM CUTTINGS AS COLLECTED AT THE CYCLONE. SOME SPECIFIC DEPTHS ARE NOTED, NUMBER POSSIBLE.

U = Thin Wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	NA	G/C Oper.:	NA
C = Cuttings	Notes:	No sampler in use		

BORING LOG	BORING/WELL NO.: PS-3	Page 1 of 1
Installation: Sky Harbor ANG Base	Site:	
Project No.: 40972.02.00	Client/Project: HAZWRAP/Sky Harbor ANG	
HAZWRAP Contractor: IT Corporation	Drig Contractor: Lane Environmental	Driller: Dwight Peterson
Drig Started: 1/16/91 (12.55 P.M.)	Drig Ended: 1/17/91 (9.10 A.M.)	Borehole dia(s): 9 3/4 inches
Drig Method/Rig Type: Air Percussion Hammer		
Logged by: Gardner	E-Log (Y/N) <input checked="" type="checkbox"/>	From _____ to _____ Protection Level: D (MODIFIED)

Depth (ft)	Sample No	Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks
0-10ft				SAND; medium grained, mostly well sorted (SYR hue 4/3), reddish brown. Sub rounded to slightly angular.	SP					1114.13
10-20ft				STONE; Gravel at ~18 ft coarse less red (4.5 SYR; 5/4) - red brown	SP					
20-30ft				SAND, medium to coarse sorted, light brown (7.5 SYR 6/4) small gravel at 29 ft & small cobbles at 30 ft; sub angular	SP					
30-40ft				SAND; medium grained (7.5 SYR 6/3); large to small angular gravel & small rounded cobbles.	SP GP					
40-50ft				SAND (DRAIN FROM 46 and down) same as 30-40 sample	SP GP					
50-60ft				SAND; medium to coarse grained, poorly sorted, angular to sub angular; angular gravel & rounded cobbles; DRAIN? (7.5 SYR 4/3)	SP					
60-70ft				SAND, same as before, DRAIN (7.5 SYR 3/3) (DARK BROWN)	SP					
70-80ft				SAND same as 60-70ft. DRAIN TO wet. Estimate water at 75 ft.						
80-90ft				SAND, wet. (SYR 3/2) (when wet) coarse gravel, poorly sorted, angular to sub ang.; rounded gravel & cobbles marking water at 93 ft.	SP GP					
90-100ft				SAND, gravel, water. Large cobbles coarse to medium sand. Rounded gravel & cobbles, sub angular sand	GP					

STEP 100  
JTS-BH

JET 200  
TDB

U = Thin Wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	NA	G/C Oper.:	NA
C = Cuttings	Notes: _____			

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO: <b>MWS-01</b>	Page <b>1</b> of <b>3</b>
Installation: <b>Sky Harbor</b>	Coordinates:	Site: <b>Sky Harbor Backwash Well</b>
Project No. <b>4092202.06</b>	Client/Project: <b>HAZWRAT/Sky Harbor ANJL</b>	
HAZWRAT Contractor: <b>ITC Corporation</b>	Drill Contractor: <b>LAYNE Environmental</b>	Driller: <b>DEARY LODGE</b>
Drill Started: <b>1/24/91 (17:40 P.M.)</b>	Drill Ended: <b>1/30/91 (11:45 A.M.)</b>	Borehole dia(s): <b>9 3/4"</b>
Drill Method/Rig Type: <b>Air Hammer Casings</b>		
Logged by: <b>GARDINER</b>	E-Log (Y/N) <b>(N)</b>	From _____ to _____ Protection Level <b>D (Modified)</b>

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks	Etc
0	X	Y	0 2/100	MED TO FINE, ROUNDED, W/IL SORTED, SAND DARK BROWN (7.5TK 3/3). SLIGHTLY MOIST	S TO SW	4 10 12				1118.30	
5	X		0 10	90%, MED TO COARSE GRAINED, ANGLULAR, MOD. W/IL SORTED, BUT W/ GRAVEL, 10%, COURSE, ROUNDED. LIGHT BROWN (7.5TK 4/3)	SP	10 50					
10	X		0 10	80%, MED TO COARSE, ROUNDED, W/ SAND, 20%, LIGHT BROWN (7.5TK 6/2), med, ROUNDED.	GP	8 10 50					
15	X		0	NO RECOVERY	-	50					
20	X		0	NO RECOVERY; FROM CYCLONE AT 21 FT: 60% COURSE TO MED, ANGLULAR, POORLY SORTED SANDS LIGHT BROWN (7.5TK 6/4), W/ GRAVEL, 40%, ROUNDED TO ANGLULAR, MED TO COARSE W/ OCCASIONAL COBBLES	SP	50 -					
25	X		0	NO RECOVERY	-	50					
30	X		0	NO RECOVERY; FROM CYCLONE AT 31 FT: 50% FINE TO COARSE, ROUNDED & ANGLULAR, VEG POORLY SORTED W/ SILT (LIGHT BROWN 7.5TK 6/4) W/ GRAVEL, 50%, ROUNDED TO ANGLULAR TO MED TO COARSE W/ COBBLES (ROUNDED).	SP TO GP	50 -					

U = Trip wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
S = Sp. (Spoon) Tube	O = Other	CA S	G/C Oper.	NA
C = Casing	Notes	NA		

FIGURE 5-3a

REV. DATE: MAY 1990

BORING LOG	BORING/WELL NO.: MWS-01	Page 2 of 3
Installation: Sky Harbor	Coordinates:	Site: Sky Harbor Break Ground Well
Project No.: 408721.02.06	Client/Project: HAZWRAP/Sky Harbor Air	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	Driller: DEERY LADDER
Drig Started: 1/21/91 (12:00 p.m.)	Drig Ended: 1/30/91 (11:45 a.m.)	Borehole dia(s): 9 3/4"
Drig Method/Rig Type: Air Hammer Casing		
Logged by: GARDNER	E-Log (Y/N): (N)	From ___ to ___ Protection Level: D (MODIFIED)

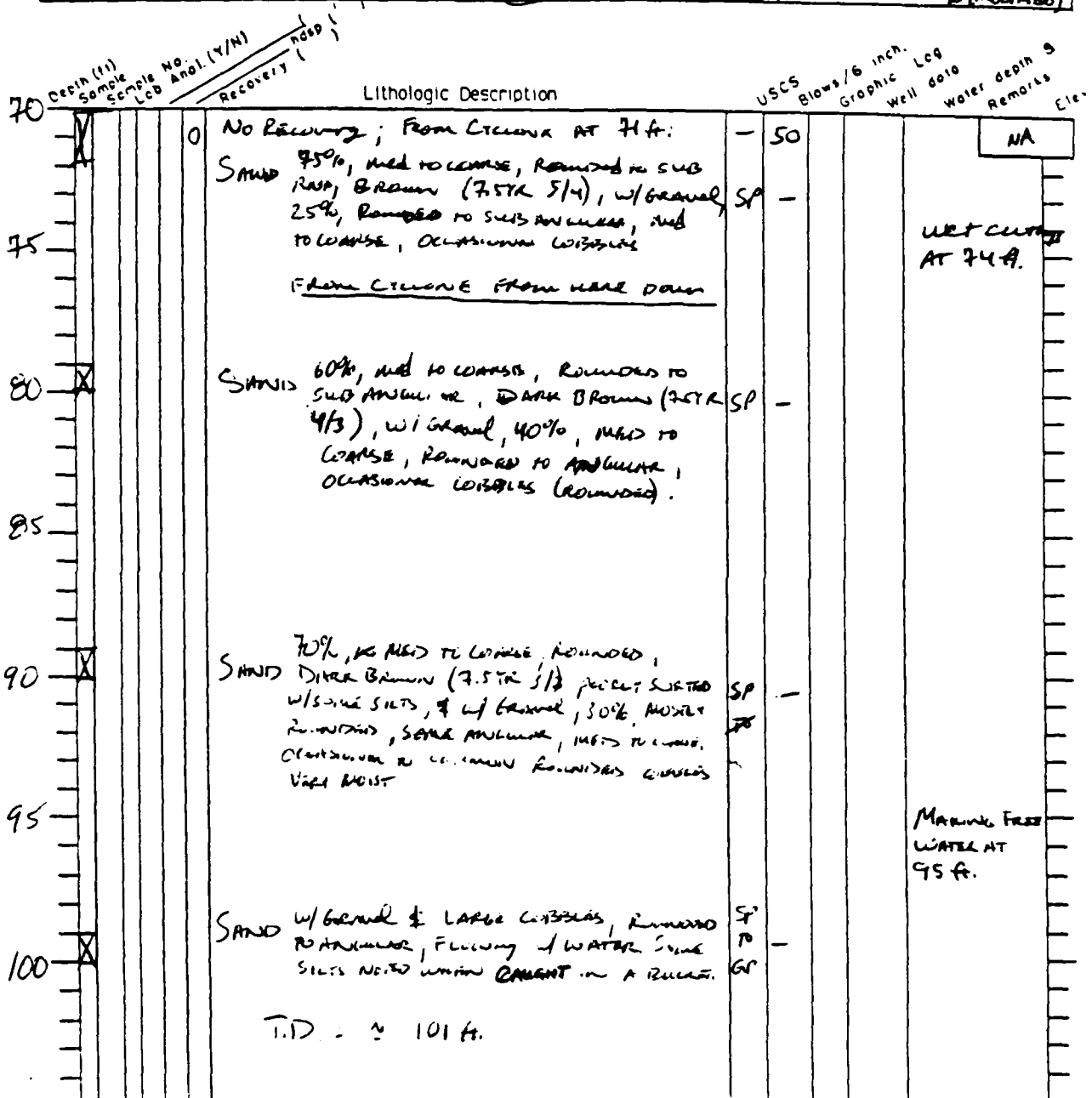
DEPTH (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth	Remarks	Etc.
35				No Recovery		50				NA	
40				No Recovery; From CYCLONE AT ≈ 41 ft. SANDS 70%, MED TO COARSE, ROUNDED TO SUB ANG, MED. BROWN (7.5YR 5/3), POORLY SORTED w/ GRAVEL, 30%, MOSTLY ROUNDED TO SUB ROUNDED, MED. Very Silty moist	SP						
45				No Recovery		50					
50				No Recovery; From CYCLONE AT ≈ 51 ft. 70%, MEDS, ROUNDED TO SUB ROUNDED SANDS (BROWN, 7.5YR 5/3), POORLY SORTED w/ GRAVEL, MED TO COARSE, ROUNDED & ABUNDANT w/ OCCASIONAL CUBICLES (ROUNDED)	SP						
55				No Recovery		50					
60				60% w/ SOME SILT, MED, ROUNDED, SAND DARK BROWN (7.5YR 3/3), POORLY SORTED w/ GRAVEL, 40% w/ SOME SILT, MED TO COARSE, ROUNDED <u>VERY MOIST</u>	SP TO SM	50 22 22 25					
65				No Recovery		50					

U = Tap wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Spill spoon (tube)	O = Other	CA S	G/C Oper:	NA
C = Cuttings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: MLWS-01	Page 3 of 3
Installation: Sky Harbor	Coordinates:	Site: Sky Harbor Background Well
Project No. 401321.07.06	Client/Project: HAZWRAP / Sky Harbor ANG	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LANE ENVIRONMENTAL	Driller: Davey Linder
Drig Started 1/22/91 6:30 P.M.	Drig Ended: 1/30/91 (11:45 A.M.)	Borehole dia(s): 9 3/4"
Drig Method/Rig Type: Air Hammer Casings		
Logged by: GARDINER	E-Log (Y/N): (N)	From _____ to _____
		Protection Level: D (MODIFIED)



U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Spill spoon (tube)	O = Other	CA S	G/C Oper:	NA
C = Cuttings	Notes:	NA		

FIGURE S-3 a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: MWS-02	Page 1 of 3
Installation Sky Harbor	Coordinates:	Site Sky Harbor Bunker 4254
PROJECT NO. 401921-01-01	Client/Project: HAZWAP / FORTER Sky Harbor AN36	
HAZWAP Contractor: IT Corporation	Drig Contractor: LAYNE Environmental	Driller: DEAN LUDERS
Drig Started 1/31/91 (14:15 P.M.)	Drig Ended: 2/6/91 (10:00 A.M.)	Borehole dia(s) 9 3/4"
Drig Method/Rig Type: AIR Hammer Casings		
Logged by: GARDNER	E-Log (Y/N) (N)	From _____ to _____
Protection Level D (MODIFIED)		

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	water depth	Remarks
0	X	Y	0	75%, MED TO COARSE, ROUNDED TO SAND SUB ROUNDED, PEAS SIZE GRAIN, 25%, ROUNDED, MED TO COARSE. SOME ANGIOSPERM PEBBLES. (2.5YR 5/4)	SP	16				1115.91
5	X	Y	0	50%, MED TO COARSE, ROUNDED, MIXED SANDS W/ ANGIOSPERM & CONCRETE FILL. MANY BEAD FILL.	SP	10				
10	X	Y	0	90%, MED TO FINE, ROUNDED TO SAND SUB ROUNDED, MOSTLY WELL SORTED, BUT W/ OCCASIONAL GRAVEL, 10%, ROUNDED MED. (7.5YR 5/4)	SP	10				
15	X	Y	0	SAND 80% MED TO COARSE, ANGIOSPERM, PEAS SIZE GRAIN W/ GRAVEL, 20% MED TO FINE, ROUNDED. (2.5YR 7/4)	SP	50				
20	X	Y	0	No Recovery		50				
25	X	Y	0	(20% Recovery) SAND 55% VEG COARSE, ANGIOSPERM, PEAS SIZE GRAIN W/ GRAVEL 4%, ROUNDED TO SAND SUB ROUNDED, MED. Slightly moist, Brown (7.5YR 5/4)	SP	50				
30	X	Y	0	No Recovery		50				

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (Tube)	O = Other	CAS	G/C Oper.:	NA
C = Castings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: MWS-02	Page 2 of 3
Installation: Sky Harbor	Coordinates:	Site: Sky Harbor Runway 4 Well
Project No. 70721.01.06	Client/Project: HAZWOP / Sky Harbor ARIG	
HAZWOP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	Driller: DERRY LADDER
Drig Started: 1/31/91 (14:15 m)	Drig Ended: 2/6/91 (10:00 A m)	Borehole dia(s) 9 3/4"
Drig Method/Rig Type: Air Hammer Casing		
Logged by: GARDINER	E-Log (Y/N): (Y)	From _____ to _____ Protection Level D (MAGNIFIED)

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch. Graphic Log	Well data	Water depth	Remarks
35			0	NO RECOVERY		50			NA
40	10		10	SAND 70%, MOSTLY ROUNDED, MED TO COARSE, POORLY SORTED, BROWN (7.5YR 5/4) w/ GRAVEL, 30%, MED TO COARSE, MOSTLY ROUNDED TO SUB-RND. w/ GRAVEL ROUNDED COBBLES	SP	50			
45	10		10	SAND 80%, MOSTLY ROUNDED, MED. TO COARSE, BROWN (7.5YR 5/4), POORLY SORTED w/ SOME SILT OR SILTY CLAY, 5%, BROWN (7.5YR 5/4), MOIST, & w/ GRAVEL, 30%, ROUNDED, MED.	SP TO SM	50			
50	10		10	SAND 70%, MED TO COARSE, ROUNDED TO SUB-RND., BROWN (7.5YR 5/4), MOIST, POORLY SORTED w/ SOME SILT/CLAY (BROWN & MOIST) & GRAVEL, med, ROUNDED (30%).	SP TO SM	50			
55			0	NO RECOVERY		50			
60			0	NO RECOVERY; FROM CIRCUMST. AT ± 61 ft: SAND 60%, MED, ROUNDED TO SUB-RND., BROWN (7.5YR 5/4), MOIST, w/ GRAVEL 40%, MED TO COARSE, ROUNDED w/ OCCASIONAL COBBLES.	SP	-			
65			0	NO RECOVERY		50			

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	CAS	G/C Oper.:	NA
C = Casing	Notes:	NA		



FIGURE 5-3a

REV DATE MAY 1993

BORING LOG	BORING/WELL NO.: MWJ-02	Page 3 of 5
Installation Sky Harbor	Coordinates:	Site: Sky Harbor Background Well
Project No. 401721-02-01	Client/Project: HAWAII / EBY HAWAII ANX	
HAWAII Contractor IT Corporation	Drill Contractor: LANE ENVIRONMENTAL	Driller: DERRY LODDER
Drill Started 1/21/91 (14:15 P.M.)	Drill Ended 2/6/91 (10:00 A.M.)	Borehole dia(s) 9 3/4"
Drill Method/Rig Type: AIR HAMMER CASING		
Logged by: GARDNER	E-Log (Y/N) (D)	From _____ to _____
Protection Level 1 (Modified)		

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth & Remarks
70	X		0	No RECOVER		50			NA
75	X			No RECOVERY; From Casing at 78ft. 65% COARSE, medium to sub angular SAND MOIST, Brown (7.5TR 5A), poorly sorted w/ gravel; 30% med to coarse rounded & cobbles, 5% med to coarse, rounded	SP to GP	50			▲ Veg mat at ca. 78ft. Free water at 82ft.
80									
85									
90	X			SAND WATER MIXTURE, APPROX 60% SAND, w/ 40% gravel & cobbles, rounded to sub rounded & minor angular. Some small silt fraction, dark brown (7.5TR 4/4). FREE WATER.					
95									
100				SAND/WATER MIXTURE, w/ 20-40% gravel & cobbles, rounded to sub-rounded, dark brown (7.5TR 4/4).	SP to GP				

T.D. = 1101 ft.

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
S = Split spoon (tube)	O = Other	CA S	G/C Oper.:	NA
C = Casing	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1990

LOG NO	BORING/WELL NO	MWS-03	Page	1	of	3
Installation	Sky Harbor	Coordinates:	Site Sky Harbor Base Ground			
Project No	401220006	Client/Project	HAWAIIAN / Sky Harbor Air			
Contractor	FLORIAN	Drill Contractor	WATER ENGINEERING	Driller	FRANK LUDWIG	
Drill Started	11/30/91 (13:30 P.M.)	Drill Ended	1/31/92 (13:20 P.M.)	Borehole dia(s)	9 1/4"	
Drill Method/Rig Type	Air Hammer Casing					
Used by	WALDINGER	E-Log (Y/N)	(Y)	From	to	Protection Level D (MODIFIED)

DEPTH (ft)	Sample No	Depth (ft)	Recovery (%)	Lithologic Description	USCS	Flow	1/6 inch	Graphic Log	Well	0010	Water	Depth	Remarks
0	X	0 to 5	0	95% MED, ROUNDED TO SUB-ROUNDED, SAND DARK BROWN (3.5 to 4/3), MOSTLY WELL SORTED BUT W/ OCCASIONAL GRAVEL, 10% 5"b, ROUNDED, med to fine.	SW	20							1116.14
5	X	5 to 10	0	75% med, round to ANGLULAR, DARK GRAY (3.5 to 4/3), POORLY SORTED W/ GRAVEL, 25% med, rounded. Pieces of CONCRETE in TOP 4 inches	SP	6							
10	X	10 to 15	0	CONCRETE		4							
15	X	15 to 20	0	NO RECOVERY, CONCRETE RUBBLE		10							
20	X	20 to 25	0	NO RECOVERY, FROM CEMENT AT ~ 21 ft: 60% very coarse, ANGLULAR, LIGHT SAND DROWN (7.5 to 5/4 to 6/4), POORLY SORTED W/ SOME FINES & GRAVEL, 40% med to coarse & OCCASIONAL COBBLES, ROUNDED	SP TO GP	-							
25	X	25 to 30	0	NO RECOVERY		50							
30	X	30 to 35	0	NO RECOVERY; FROM CEMENT AT ~ 31 ft: 55% coarse, ANGLULAR, LIGHT BROWN (3.5 to 6/4), POORLY SORTED W/ GRAVEL, 40% rounded to ANGLULAR, FINE TO COARSE w/ COBBLES, 5% rounded.	SP TO GP	-							

= Filtered Well Tube      R = Rock Spring      NA      Field or Other Mod      NA  
 \* Sp. (open tube)      O = Other      CA S      R = Other      NA  
 Notes      NA

FIGURE 5-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO MW3-C3	Page 2 of 3
Installation Sky Harbor	Coordinates:	Site Sky Harbor
Project No 408226.04	Client/Project: HAZARDOUS / Sky Harbor Area	
HAZWRAP Contractor ITC Environmental	Drill Contractor Lantz Environmental	Driller: D. [unclear]
Drill Started 1/30/91 (13 20 p.m.)	Drill Ended 1/31/91 (13 20 p.m.)	Borehole dia(s) 9 3/4"
Drill Method/Rig Type: Air Hammer (Casing)		
Logged by [unclear]	E-Log (Y/N) (Y)	From _____ to _____ Protection Level: D (Medium)

Depth (ft)	Sample No	Lab Anal (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch	Graphic Log	Well data	Water depth	Remarks
35			0	No Recovery		50				NA
40			0	No Recovery, from Casing at 41 ft. 60% Angular, coarse to very coarse, SAND RED BROWN (2.5 YR 4/4), poorly sorted w/ gravel, 40% fine to coarse, rounded to angular w/ rare but large cobbles	SP TD GP	50				
45			0	No Recovery		50				
50			0	Very Low Recovery (10%) SAND 70% very coarse, angular, brown (7.5 YR 5/4), poorly sorted w/ some fines & gravel, 30% rounded, med to coarse w/ rare large cobbles	SP	50				
55			0	No Recovery		50				
60			0	No Recovery, from Casing at 61 ft. SAND 55% coarse, angular, brown (7.5 YR 5/4), poorly sorted w/ gravel, 40% rounded to angular, med to coarse, w/ cobbles, 5% coarse, rounded, med	SP TD GP	50				
65			0	No Recovery		50				

□ = Thin wall tube	□ = Rock Coring	NA	File # 37C(Maker/Mod)	NA
○ = Sp. (3000) tube	○ = Other	CA S	3-D Open	NA
□ = Casing	Notes	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: <u>MWS-03</u>	Page <u>3</u> of <u>3</u>
Installation: <u>Sky Harbor</u>	Coordinates:	Site: <u>Set Hazards - Bunker 2nd Well</u>
Project No.: <u>40121.000</u>	Client/Project: <u>Hickory Hill / Set Hazards - Area 5</u>	
MAZWP22 Contractor: <u>ITC Operations</u>	Drill Contractor: <u>LITTON Environmental</u>	Driller: <u>Dean Ludwig</u>
Drill Started: <u>1/2/91 (13:32 L.M.)</u>	Drill Ended: <u>1/31/91 (13:20 P.M.)</u>	Borehole dia(s): <u>9 3/4"</u>
Drill Method/Rig Type: <u>Air Hammer (L.M.)</u>		
Logged by: <u>Ward Jones</u>	E-Log (Y/N): <u>Y</u>	From _____ to _____
		Protection Level: <u>D (MODIFIED)</u>

Depth (ft) Sample So. Log	Sample No. Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch. Graphic Log	Well data	Water depth	Remarks	Other
70		0	NO RECOVERY		50			NA	
75	Y	10	SAND 60% MID TO COARSE, ANGULAR, BROWN (7.5YR 4/3) TO DARK BROWN, POORLY SORTED w/ SOME SILT (50%) & GRAVEL, 35% MID TO COARSE, REMAINS & REMAINS MO. ST FROM CEMENT FILL HOLE TO T.D.:	SP	40 50			Very moist cutting water at 275 ft.	
90	X		SAND 55% Angular to sub angular, coarse, dark brown (7.5YR 3/3), poorly sorted w/ gravel, 40% MID TO COARSE, rounded to sub angular w/ lumps, 5% MID TO COARSE, rounded. <u>VERY MOIST</u>	SP R G	-				
95			WATER SAND MATURE:						
100	X		SAND 65% rounded to sub angular, dark brown (7.5YR 3/3), poorly sorted w/ some silt, 5% & gravel, 25% rounded to angular, mid to coarse, & lumps, 5% rounded, coarse. T.D. = ~ 101 ft.	SP R G	-				

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Sp. spoon (tube)	O = Other	CA S	G/C Oper.	NA
C = Cuttings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 199

BORING LOG	BORING/WELL NO. <b>ABS-04 MWS-04</b>	Page <b>1</b> of <b>3</b>
Installation: <b>Sky Harbor</b>	Coordinates:	Site: <b>SH BARRACADE, WASH MWS-04</b>
Project No: <b>40131.0126</b>	Client/Project: <b>HAZWRAP / Sky Harbor ANA Base</b>	
HAZWRAP Contractor: <b>IT Corporation</b>	Drig Contractor: <b>LANGE ENVIRONMENTAL</b>	Driller: <b>Duane Peterson</b>
Drig Started: <b>3/21/91 (9:45 A.M.)</b>	Drig Ended: <b>3/21/91 (4:30 P.M.)</b>	Borehole dia(s) <b>4 10 3/4"</b>
Drig Method/Rig Type: <b>Airt Drill Tube Percussion</b>		
Logged by: <b>GARDNER</b>	E-Log (Y/N) <b>(N)</b>	From _____ to _____ Protection Level <b>D (Mod.)</b>

Depth (ft)	Sample No.	Sample Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks
0				<b>SAND</b> 70%, med to coarse, angular, poorly sorted, brown (7.5YR 4/2) w/ some gravel, 20%, med, and some silt, 10%, fine, brown, moist. <b>SP</b>		7				
5				<b>No Recovery</b>		50				
10				<b>No Recovery</b> : from CYCLONE AT ~ 10ft:		50				
15				<b>SAND</b> 70%, med to coarse, and to sub ang, dark brown (7.5YR 3/2), poorly sorted w/ minor silt & gravel, 30%, med to sub ang, med to coarse, rare cobbles. moist	<b>SP</b>					
20				<b>SAND</b> 95%, med to coarse, angular, <del>poorly sorted</del> lt brown (7.5YR 6/4), mostly well sorted but w/ occasional gravel, 5%, fine, and. moist	<b>SW</b>	25				
25				<b>SAND</b> 75%, med to coarse, angular, lt. tan, (7.5YR 6/4), <del>poorly sorted</del> poorly sorted w/ gravel, 20%, med, and. moist	<b>SP</b>	50				
30				<b>SAND</b> 90%, med to coarse, angular to sub ang., tan (7.5YR 5/4), mostly well sorted on the sand, but w/ gravel, 20%, med, and. moist	<b>SP to SW</b>	50				
35				<b>No Recovery</b>		50				

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod)

S = Sp. spoon (tube)      O = Other      G/C Oper.

□ = Blow logs      Notes \_\_\_\_\_

FIGURE 5-3a

REV. DATE MAY 1990

BORING LOG	BORING/WELL NO. <u>MWS-04</u>	Page <u>2</u> of <u>3</u>
Installation: <u>Sky Harbor</u>	Coordinates:	Site: <u>SH BANGOR WALK MWS-04</u>
Project No.: <u>40921</u>	Client/Project: <u>HAZWRAP / SKY HARBOR ANG BASE</u>	
HAZWRAP Contractor: <u>IT CORPORATION</u>	Drig Contractor: <u>LAYNE ENVIRONMENTAL</u>	Driller:
Drig Started: <u>3/1/91 (9:45 A.M.)</u>	Drig Ended: <u>3/1/91 (4:30 P.M.)</u>	Borehole dia(s): <u>N 10 3/4"</u>
Drig Method/Rig Type: <u>DUAL TUBE PERCUSSION</u>		
Logged by: <u>GARDNER</u>	E-Log (Y/N) <u>(N)</u>	From _____ to _____ Protection Level <u>D (MODIFIED)</u>

Depth (ft)	Sample No.	Sample Lab	Anol. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth & Remarks
35				0	No Recovery		50			
40	160	10		10	SAND 75%, med to coarse, ANG to sub ANG, DARK BROWN (7.5YR 3/2), POORLY SORTED w/ GRAVEL, 25%, med to coarse, RND to sub ANG. MOST. SILT VISIBLE. CARBON ODR.	SP	50			
45	170	10		10	SAND 30%, med to coarse, ANG to sub ANG, DARK BROWN (7.5YR 3/2), POORLY SORTED w/ GRAVEL, 20%, med to coarse, RND to sub ANG. MOST. HYDRATION ODR.	SP	50			
50	220	10		10	SAND 60%, med to coarse, ANG, DARK BROWN (7.5YR 3/2), POORLY SORTED w/ GRAVEL, 40%, med to coarse, ANG to sub ANG. MOST. HYDRATION ODR. SLIGHT VISIBLE GRAY STAIN.	SP	50			
55				0	No Recovery		50			
60				0	No Recovery		50			
65	300	20		20	SAND 75%, med to coarse, ANG to sub ANG, BROWN (7.5YR 3/2), POORLY SORTED w/ SOME SILT & GRAVEL, 25%, med to coarse, RND to sub ANG. MOST. HYDRATION ODR.	SP	28 50			

U = Thin wall Tube      R = Rock Coring      \_\_\_\_\_ Field G/C (Make/Mod.)  
 S = Sp. spoon (Use)      O = Other      \_\_\_\_\_ G/C Oper.  
 \_\_\_\_\_ Notes \_\_\_\_\_

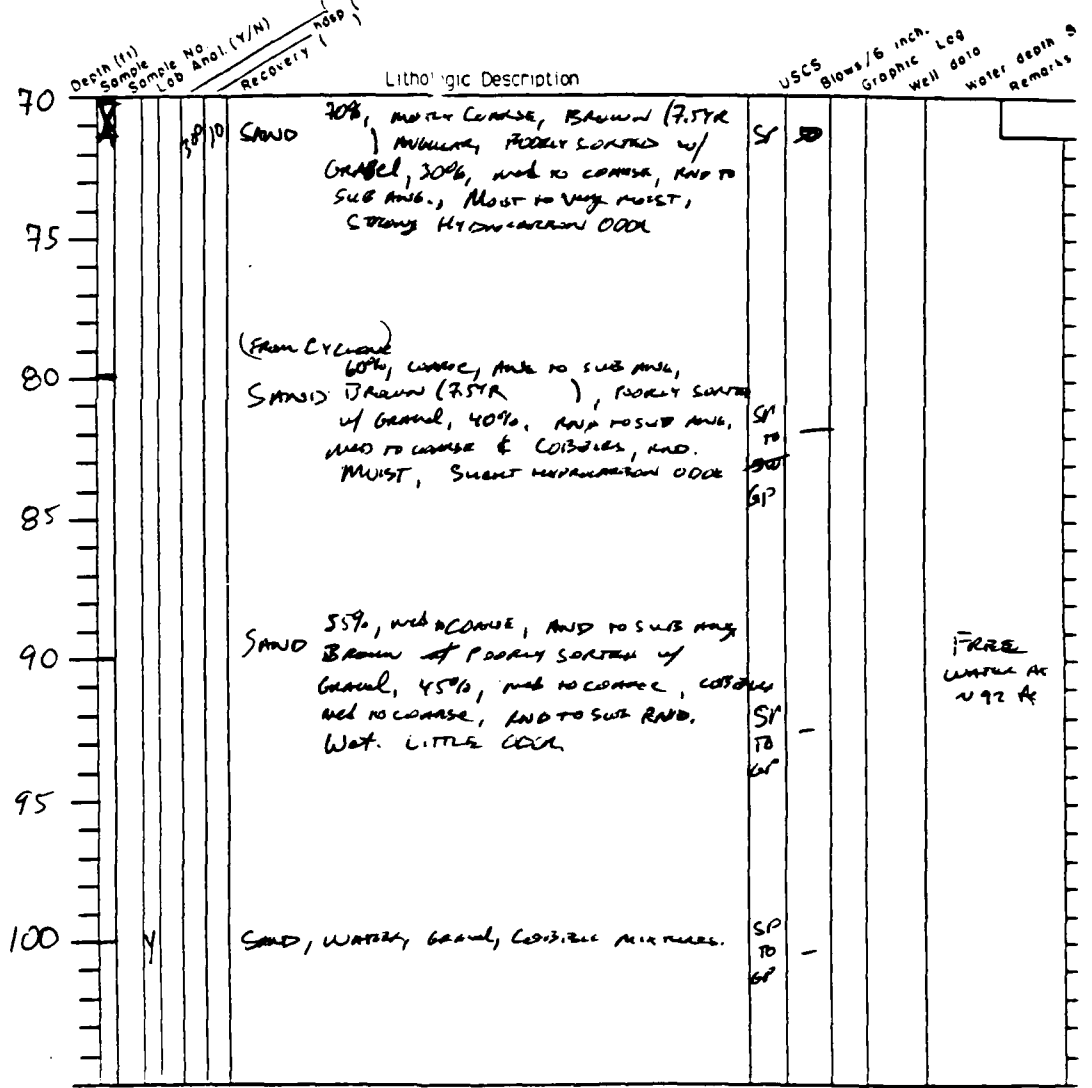
ARE NOTED, WHERE POSSIBLE.

U = Thin Wall Tube	R = Rock Coring	Field G/C (Make/Mod.)
S = Split spoon (tube)	O = Other	G/C Oper.:
C = Cuttings	Notes: <u>NO SAMPLES IN USE</u>	

FIGURE 5-3 a

REV DATE MAY 199  
Page 3 of 5

BORING LOG	BORING/WELL NO: <u>MWS-04</u>	Site: <u>SH Backcountry Well MWS-04</u>
Installation: <u>Sky Harbor</u>	Coordinates:	
Project No.: <u>40133</u>	Client/Project: <u>HAZWRAP/Sky Harbor AX6 Base</u>	
HAZWRAP Contractor: <u>IT Construction</u>	Drig Contractor: <u>Lewis Environmental</u>	Driller:
Drig Started: <u>3/21/91 (9:45 A.M.)</u>	Drig Ended: <u>3/21/91 (4:30 P.M.)</u>	Borehole dia(s): <u>4.1274"</u>
Drig Method/Rig Type: <u>Dual Tube Pressions</u>		
Logged by: <u>GARDNER</u>	E-Log (Y/N) <u>(N)</u>	From _____ to _____
		Protection Level: <u>D (Modified)</u>



U = Thin wall Tube	R = Rock Coring	Field G/C (Make/Mod.)
S = Split spoon (tube)	O = Other	G/C Oper.:
C = Cuttings	Notes:	

FIGURE 5-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO. M011-02	Page 1 of 3
Installation: Sky Harbor	Coordinates:	Site:
Project No. 40721.0200	Client/Project: HARVEST / Sky Harbor Area	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LYNNE Environmental	Driller: Darryl Lopez
Drig Started: 01/28/01 (08:45 a.m.)	Drig Ended: 1/28/01 (15:00 p.m.)	Borehole dia(s): 9 3/4"
Drig Method/Rig Type: Air Hammer Casing		
Logged by: CARDINAL	E-Log (Y/N): (N)	From _____ to _____
		Protection Level: D (Lowest)

Depth (ft)	Sample No	Lab Anal (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows: 16 inch	Graphic Log	Well data	Water depth	Remarks
0				MEETS TO RISE, BROWN (7.5% S&S), SAND SORTED w/ GLASS in ground (10%), MEETS TO FINE, rounded, MOIST.	SP	12 17 20				1116.34
5				NO RECOVERY	-	50				
10				NO RECOVERY. FROM CYCLING AT 11 ft SAND 70%, FINELY SORTED, MEETS TO COARSE, BROWN (7.5% S&S), w/ GRAVEL (30%), MEETS TO COARSE, ROUNDED w/ OILSOAK CUBES.	SP	-				
15				40% COARSE, ANGLER, BROWN (7.5% S&S), SAND W/ SORTED BUT w/ GRAVEL, 10%, ROUNDED, MOIST.	SP	50				
20				NO RECOVERY	-	50				
25				NO RECOVERY; FROM CYCLING AT ~ 20 ft.: 60% COARSE, ANGLER, BROWN (7.5% S&S), SAND SORTED w/ GRAVEL, 40%. ROUNDED w/ ANGLER, MEETS TO COARSE w/ RARE CUBES.	SP	-				
30				NO RECOVERY	-	50				

J = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
S = Split spoon tube	O = Other	CAS	G/C Oper	NA
Q = Casing	Notes	NA		



FIGURE 5-3a

REV. DATE MAY 1990

BORING LOG	BORING/WELL NO. MW1-02	Page 2 of 3
Installation: Sky Harbor	Coordinates:	Site: 1
Project No. 404221.02.06	Client/Project: HAZWRA/SH: Harbor Area	
HAZWRA Contractor: IT Corporation	Drig Contractor: Larry Hutchinson	Driller: Jeff Liddle
Drig Started: 1/28/91 (8:45 A.M.)	Drig Ended: 1/28/91 (1:00 P.M.)	Borehole dia(s): 9 3/4"
Drig Method/Rig Type: Air Hammer Case		
Logged by: Gardner	E-Log (Y/N) From _____ to _____	Protection Level: D (Moist)

Depth (ft)	Sample No	Sample Lab	Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks	Etc
35	X			0	75% MED to coarse, angular, brown (7.5R 5/3), poorly sorted w/ gravel, 25% med, rounded. moist.	SP	10 15 20				NA	
40	X			0	No Recovery		50					
45	X			0	No Recovery; From cylinder at 44 ft: 60% med to coarse, angular to sub-angular, brown (7.5R 5/3), poorly sorted w/ gravel, 40% med to coarse, angular & rounded, w/ occasional cobbles	SP SP	50					
50	X			0	75% very coarse, angular, brown (7.5R 5/3), w/ gravel, 25% rounded to sub-angular, med to fine. moist. Gravel has minor red brown silt sand sticking to it.	SP	50					
55	X			0	60% coarse to med, angular, brown (7.5R 5/2), poorly sorted w/ very minor silt, & gravel, 40% rounded, med moist.	SP	50					
60	X			0	55% coarse to med, angular, brown (7.5R 5/2), poorly sorted w/ minor silt, & gravel, 45% med, rounded. moist.	SP SP	50					
65	X			0	No Recovery		50					

U = Thin wall Tube	R = Rock Core	NA	Field G/C (Make/Mod)	NA
S = Sp. spoon (tube)	O = Other	CA S	G/C Oper	NA
C = Casing	Notes	NA		

FIGURE 5-3a

REV. DATE MAY 1990

BORING LOG	BORING/WELL NO. <b>MM-02</b>	Page <b>3</b> of <b>3</b>
Installation: <b>Sky Harbor</b>	Coordinates:	Site: <b>Site 1</b>
Project No: <b>401721.02.01</b>	Client/Project: <b>HAZWAP / Sky Harbor AN6</b>	
HAZWPAP Contractor: <b>IT Corporation</b>	Drig Contractor: <b>LAWRE FINE ENVIRONMENTAL</b>	Driller: <b>DEAN LORING</b>
Drig Started: <b>1/25/91 (08:45 A.M.)</b>	Drig Ended: <b>1/26/91 (12:00 P.M.)</b>	Borehole dia(s): <b>4 1/4"</b>
Drig Method/Rig Type: <b>Air Hammer Casing</b>		
Logged by: <b>GREENBERG</b>	E-Log (Y/N): <b>(N)</b>	From _____ to _____
Protection Level: <b>D (MODIFIED)</b>		

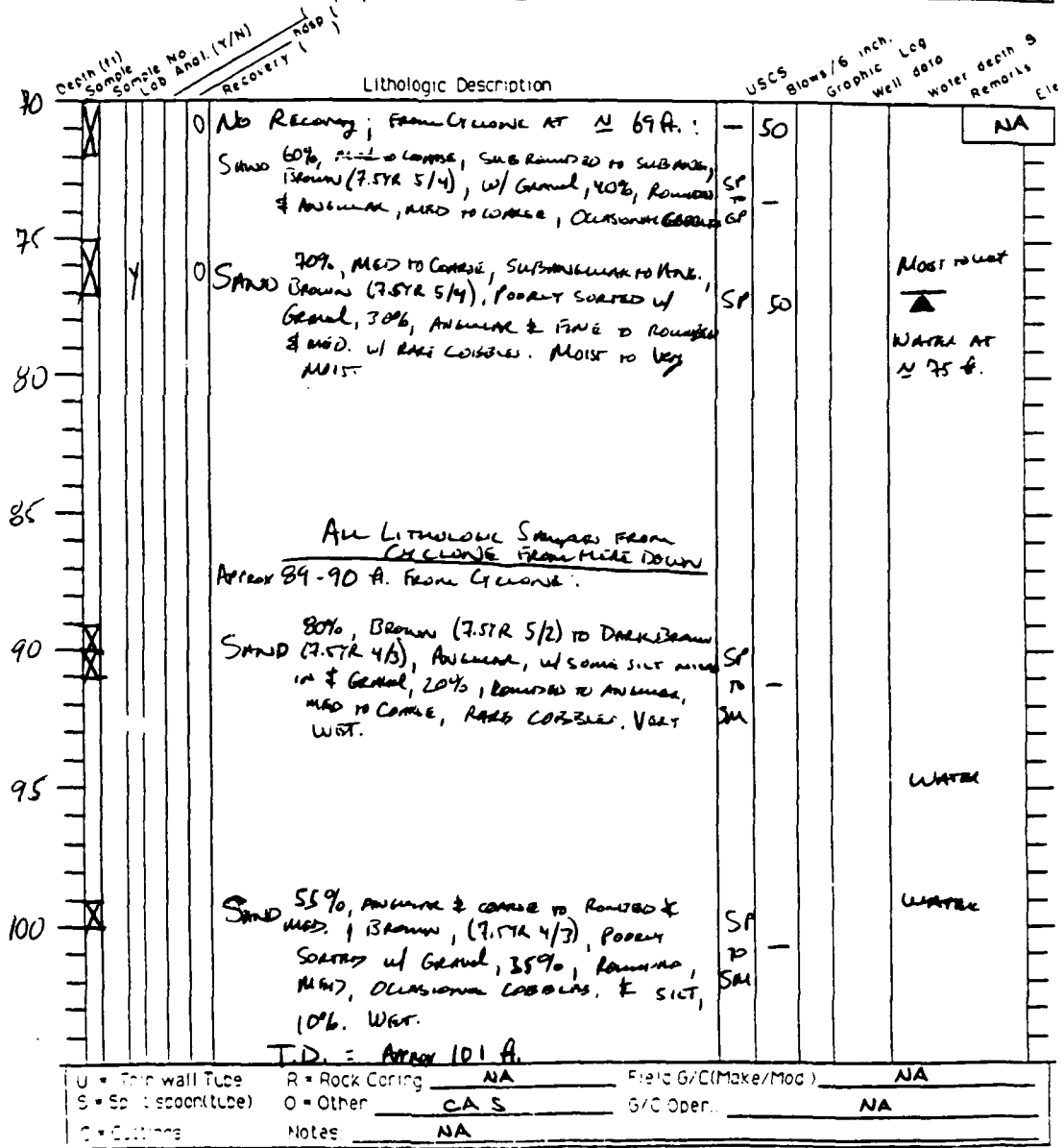


FIGURE 5-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO	SBL-02	Page	1 of 2
Installation	Sky Harbor	Coordinates:	Site	1
Project No	40921-03	Client/Project	HAZWOP/Sky Harbor ANG	
HAZWOP Contractor	IT Corporation	Drig Contractor	AT&T Environmental	Driller
Drig Started	2/4/91 (1000 ft)	Drig Ended	2/5/91 (1300 ft)	Borehole dia(s)
Drig Method/Rig Type	AIR Hammer CASING			
Logged by	GARDNER	E-Log	(N)	From _____ to _____
				Protection Level
				D (MODIFIED)

Depth (ft)	Sample No	Sample Anal (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well dia	Water depth	Remarks
0										1115.81
5				45% med to fine GRAINSD, DARK SANDS (BROWN) (7.5YR 4/4), SLIGHTLY MOIST. POORLY SORTED w/ OCCASIONAL GRAVEL, 5% med, rounded	SP	5				
						11				
						16				
10				90% med, ROUNDED TO SUB ROUNDED, SLIGHTLY MOIST BROWN (7.5YR 4/3), POORLY SORTED w/ GRAVEL, 10% med TO FINE, ROUNDED.	SP	9				
						12				
						14				
15				NO RECOVERY						
						50				
20				70% med to coarse, MEDIUM, LIGHT SAND (BROWN) (7.5YR 5/4 TO 6/4), POORLY SORTED w/ GRAVEL, med to coarse, ROUNDED, 20% w/ OCCASIONAL GRAVEL.	SP	50				
25				NO RECOVERY						
						50				
30				60% coarse, MEDIUM, MOIST, SAND BROWN (7.5YR 5/4). w/ GRAVEL, 40% med coarse, rounded	SP	7				
						15				
						50				
35				NO RECOVERY						
				60% coarse, MEDIUM, MOIST, BROWN TO LIGHT BROWN (7.5YR 5/4 TO 6/4) w/ GRAVEL, 40% med to coarse, rounded, w/ RARE COBBLES.	SP	10				
						50				

U = Thin wall Tube    R = Rock Coring    NA  
 O = Sp. (scoop) tube    C = Other    CA S    File & G. (Maker/Mod)    NA  
 G = G. (type)    Notes    NA    G-C Open    NA

FIGURE 5-3 a

REV DATE MAY 99

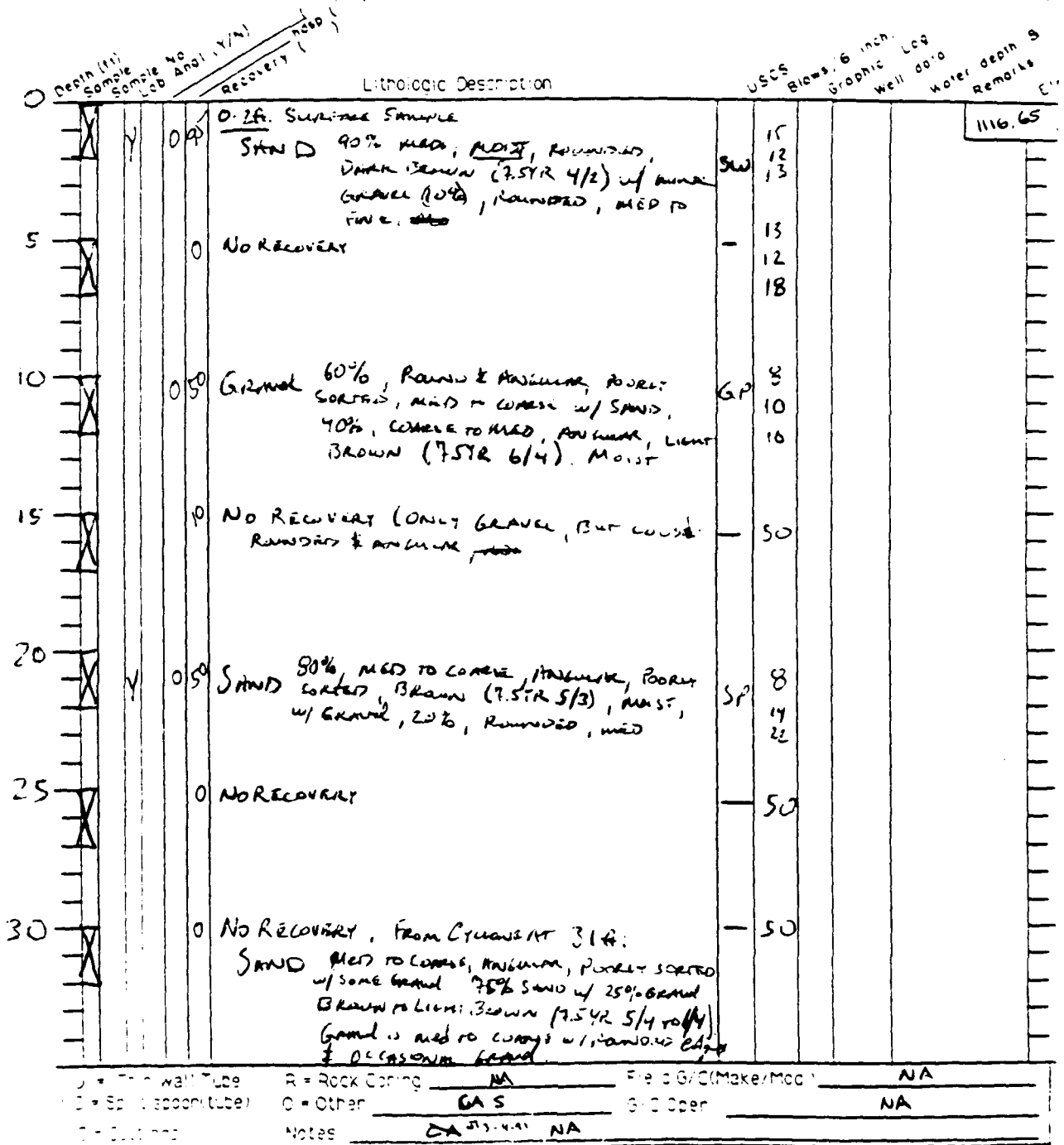
BORING LOG	BORING WELL NO	SB1-02		Page	2 of 2
Installation	Sky Harbor	Coordinates:	Site 1		
Project No	405221-01	Client/Project:	HAZOPRA / Sky Harbor AVE		
HAZWPAP Contractor	IT Corporation	Drill Contractor	LISSA Environmental	Driller	DENN LOOPER
Drill Started	2/4/91 (0900 ± mi)	Drill Ended	2/5/91 (1300 ± mi)	Borehole dia:	9 3/4"
Drill Method/Rig Type:	AIR Hammer Casing				
Logged by	GARDINER	E-Log	(initials)	From	to
				Protection Level	D (Modified)

Depth (ft)	Sample No	Sample Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch Graphic Log	Well dia	Water depth	Remarks
35				0 No Recovery		50			NA
40				0 NO RECOVERY; From Casing at 39 ft. 55% coarse, angular, light brown sand (2.5YR 6/4), poorly sorted w/ gravel, 30% rounded to angular, med to coarse & cobbles, 15% rounded, med to coarse.	SP TO G1	50			
45				0 No Recovery		50			
50				0 SAND 60% med to coarse, <sup>Dark</sup> light brown, (2.5YR 3/2) w/ some silt or silt clay, 10% black to very dark gray, (2.5YR N3/0), moist, sticky, w/ gravel, 30% med to coarse, rounded.	SP TO SM	50			
55				0 <del>NO RE</del> No Recovery		50			
60				0 NO RECOVERY; <del>From Casing</del>		50			
65				0 NO RECOVERY; From Casing at 66 ft. 60% coarse, angular to sub angular, brown sand (2.5YR 5/4), moist, poorly sorted w/ gravel, 30% med, rounded & cobbles, 10% med to coarse, rounded.	SP TO GP	50			
70				0 No Recovery		50			
72				Thin wall Tube	NA				NA
				Rock Casing	CA S				NA
				Other	NA				NA
				Notes	NA				

FIGURE 5-3a

REV DATE MAY 990

BORING LOG	BORING WELL NO	581-03	Page	1	of	2
Installation	Sky Harbor	Coordinates:	Site 1			
Project No	40134.000	Client/Project	HAZWRAP / SKY HARBOR AREA			
HAZWRAP Contractor	IT Corporation	Drill Contractor	Layne Environmental	Driller		
Drill Started	1/21/91 (1300 ± m)	Drill Ended	1/22/91 (0930 ± m)	Borehole dia(s)		
Drill Method/Rig Type:				Air Hammer Casing (Permeation)		
Logged by		G.M.H. [unclear]	E-Log	(N)	From	to
						Protection Level
						D (Monitoring)



J = Thin wall Tube      R = Rock Coring      NA  
 S = Sp. Spoon (tube)      O = Other      G.S.  
 C = Casing      Notes      DA 5/5/91      NA

FIGURE S-3a

REV DATE MAY 99C  
Page 2 of 2

BORING LOG	BORING/WELL NO	SR1-03	Site	1			
Installation	Sky Harbor	Coordinates:					
Project No.	457216-1	Client/Project	HAZWRAP/Sky Harbor ANG				
HAZWRAP Contractor	IT Corporation	Drill Contractor	Long Environmental	Driller	Dwight Peterson		
Drill Started	1/21/91	(3:00 P.M.)	Drill Ended	1/22/91	(9:30 A.M.)		
Drill Method/Rig Type:			Aug Hammer Casing	(1 casing)	Borehole dia(s)	9 1/4"	
Logged by	GARDNER	Entered	(N)	From	to	Protection Level	D (MOD. MED)

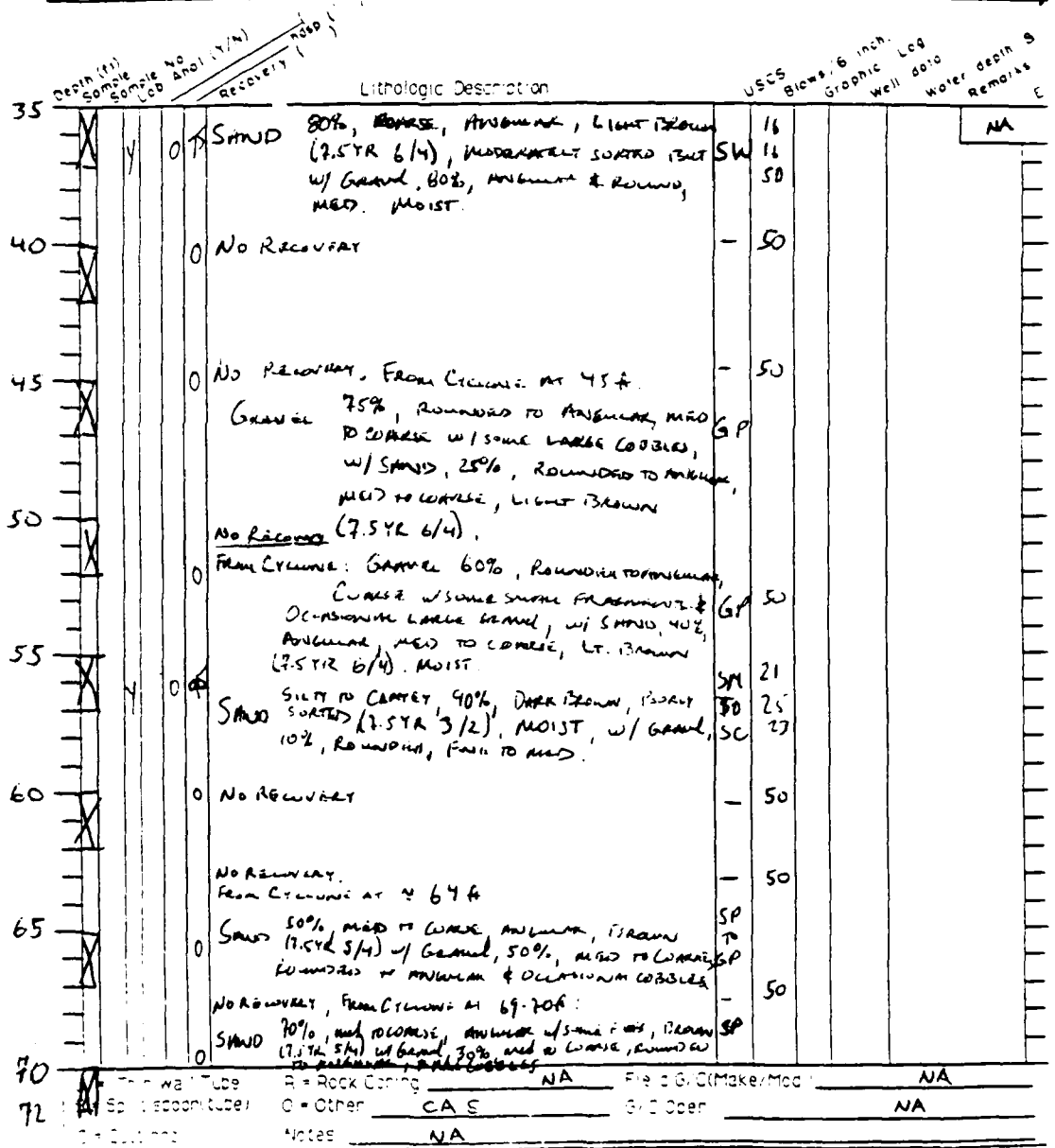


FIGURE 5-3a

REV DATE MAR 1990

BORING LOG	BORING/WELL NO	S31-04 (MODIFIED)		Page	1 of 2
Installation	Sky Harbor	Coordinates:	Site 1		
Project No	407721.02	Client/Project	HAZWOP / Sky Harbor AN6		
HAZWOP Contractor	IT CORPORATION	Drill Contractor	LARSEN ENVIRONMENTAL	Driller	DUNCAN PERKINS
Drill Started	1/21/91 08:30 a.m.	Drill Ended	1/21/91 4:20 p.m.	Borehole dia(s)	9 3/4"
Drill Method/Rig Type:	AIR HAMMER CASING (PRECISION)				
Logged by	GARDNER	E-Log	Y (P)	From	to
				Protection Level	D (Medium)

Depth (ft)	Sample No	Lab Anal (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows	6 inch. Graphic Log	Well dia	Water depth	Remarks
0	0-3 ft			Surface Sample from vertical HX POINT SANDS 80%, medium to fine, brown (7.5 YR 4/3), DRY MOIST, ANGLE of GRAIN (20%), rounded, medium	SP	12 20 24				1117.08
5	0-4 ft			SAND MED TO FINE (85%) w/ some silt DARK BROWN (7.5 YR 4/4) w/ GRAVEL (10-15%), rounded, medium to fine	SP	10 16 34				
10	0-4 ft			SAND MED GRAIN (90%); WELL SORTED SAND, BUT w/ GRAVEL (10%). Brown (7.5 YR 5/3)	SP	18 19 20				
15				Str No Recovery						
20	0-10			SAND 60%, med to coarse poorly sorted, brown (7.5 YR 5/3) MOIST w/ GRAVEL (40%), medium to coarse, rounded	SP	50				
25	0			No Recovery from casing - SANDS (60%) med to coarse, poorly sorted, brown to light brown (7.5 YR 6/3) w/ GRAVEL 2% to 4% (40%), med to coarse, rounded, MOIST	SP	6				
30	0-10			SAND 50% med to coarse, brown, (7.5 YR 5/3) w/ GRAVEL (50%), rounded, coarse, poorly sorted, moist	SP	10 90				

J = Thin wall Tube    R = Rock Coring    NA    Field G/C (Make/Mod)    NA  
 B = Split spoon Tube    O = Other    CAS    G/C Oper    NA  
 G = Other    Notes    NA

FIGURE S-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO	SB1-04 (Modified)	Page 2 of 2
Installation	Sky Harbor	Coordinates:	Site
Project No.	409221-02-00	Client/Project	HAZWRAP / Sky Harbor ANGL
HAZWRAP Contractor	IT Corporation	Drill Contractor	Lewis Engineering
Drill Method/Rig Type	Air Hammer Casing (Percussion)	Driller	Dennis Peterson
Drill Started	1/21/91 (08:30 A.M.)	Drill Ended	1/21/91 (12:00 P.M.)
Borehole d/a(s)	9 3/4"		
Logged by	GARDNER	E-Log	(N) From _____ to _____
Protection Level	D (Modified)		

DEPTH (ft)	Sample No	Anal. (Y/N)	RECOVERY (%)	Lithologic Description	USCS	Blows/6 inch. Graphic Log	Well d/a's	Water depth & Remarks
35			0	No Recovery		50		NA
40			0	Little Recovery (5%) Gravel, med to coarse, 100%. Roundish Moist.	Gr	50		
45			0	From CYCLONE AT N 42 ft: SAND (50%), med to coarse, LIGHT BROWN (7.5YR 6/4), Angular w/ gravel, 100% coarse, 50%, angular & rounded.	SP	-		
45-47 ft			0	No Recovery		50		
50			0	No Recovery		50		
55			0	SAND 80%, MED TO COARSE, DARK BROWN (7.5YR 3/3), MOIST w/ Gravel (20%), ROUNDED MED TO FINE, SAND SILT IN SAND NEAR TOP	SP	13 23 21		WET CUTTING AT 55 ft
60			0	No RECOVERY: CYCLONE HAS WET SAND MAY BE NEAR WATER		50		
65			0	No Recovery		50		
70			0	No Recovery. From CYCLONE: SAND & SILT SAND w/ SOME GRAVEL. 75% SAND w/ 25% GRAVEL. MED TO COARSE, BROWN (5.5YR 5/3). GRAVEL IS MED TO COARSE, ROUNDED & ANGULAR. MOIST TO WET.	SP	50		Near water Wet cuttings

R = Rock Coreing NA Field 3 (Maker/Mod) NA  
 O = Other CA S 3 (C) Open NA  
 Notes NA



FIGURE S-3a

REV DATE MAY 1990

BORING LOG	BORING WELL NO	SBI-05	Page	1	of	2
Installation	Sky Harbor	Coordinates:	Site 1			
Project No.	407321-02-06	Client/Project:	HAZWRAP / SKY HARBOR ANV			
HAZWRAP Contractor	IT Corporation	Drill Contractor	LATHE ENGINEERING	Driller	ART RODRIGUEZ	
Drill Started	11/8/91 (10:20 a.m)	Drill Ended	11/8/91 (6:35 p.m)	Borehole dia(s)	9 3/4"	
Drill Method/Rig Type:	AIR PERCUSSION HAMMER					
Logged by	GARDNER	E-Log	(N)	From	to	
			Protection Level	D (MODIFIED)		

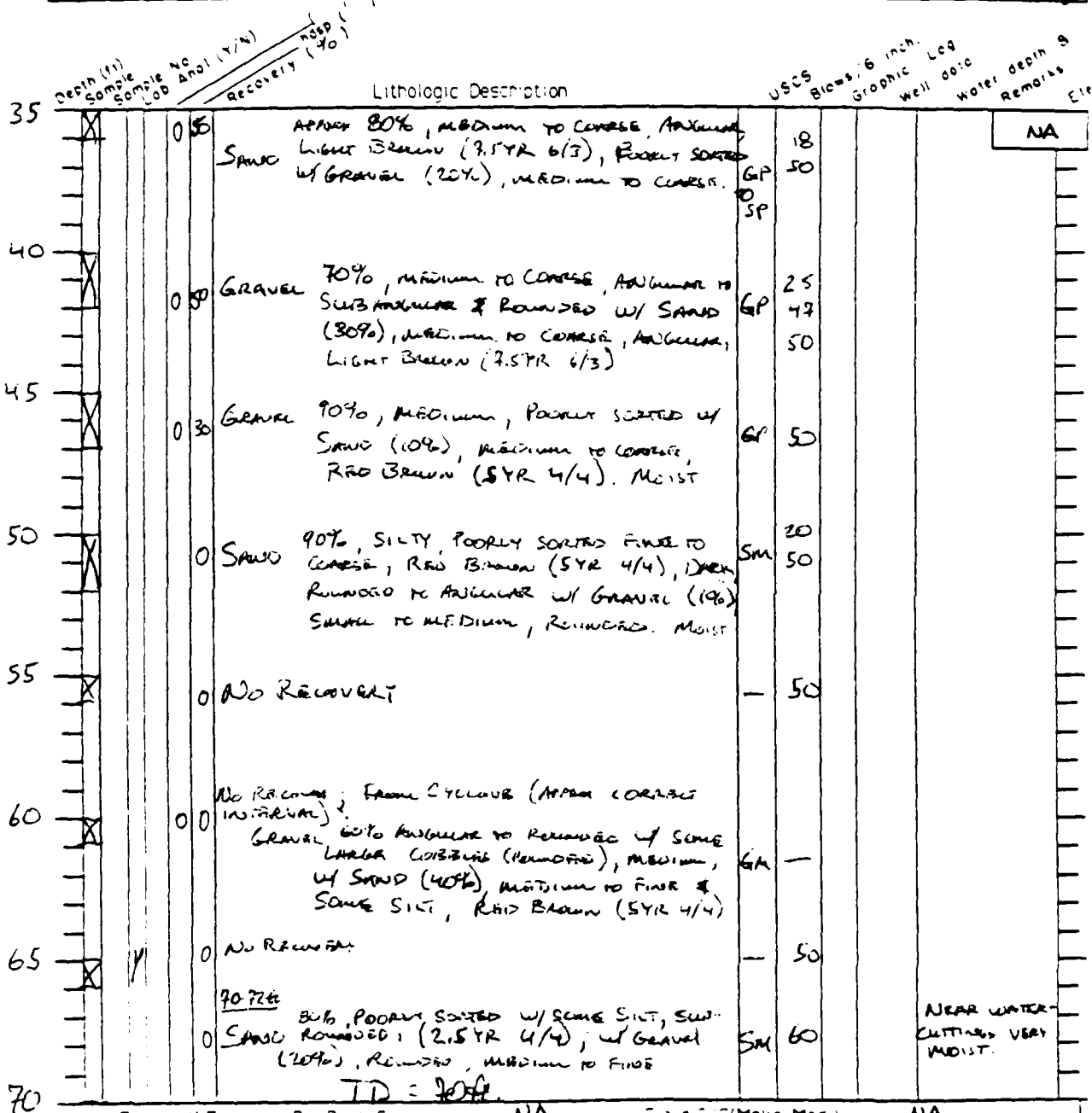
Depth (ft)	Sample No	Anal (1/4)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch		Remarks
						Graphic Log	Well logs	
0								
0	0100			SAND MEDIUM TO FINE GRAINED (80%) WITH GRAVEL, MEDIUM (20%). DARK BROWN (7.5YR 3/3), MOSTLY WELL SORTED FOR THE SAND. POORLY GRAINED.	Sw	13		1115.86
5						13		
5	0200			SAND MEDIUM GRAINED, DARK BROWN (80%) (7.5YR 4/3); w/ GRAVEL (20%), WELL ROUNDED, MEDIUM.	Sp	14		
10						18		
10	1000			SAND MEDIUM GRAINED, DARK BROWN (80%) (7.5YR 4/3), w/ GRAVEL (20%), WELL ROUNDED, MEDIUM.	Sp	14		
15						20		
15	1000			SAND MEDIUM GRAINED (80%) DARK BROWN (7.5YR 4/3), POORLY SORTED w/ GRAVEL (20%), MEDIUM & WELL ROUNDED	Sp	8		
20						19		
20				No Recovery		23		
25						50		
25				No Recovery		50		
30								
30				FROM CYCLONE (NOT NECESSARILY FROM CORRECT INSTALLED); GRAVEL (90%) ROUNDED & LARGE UP TO LOBBIES w/ SAND (10%) ROUNDED, MEDIUM TO COARSE LIGHT BROWN (7.5YR 6/4)	GP	NA		
						21		
						24		
				SAND MED TO COARSE (60%) LIGHT BROWN (7.5YR 6/4) SOFTLY SORTED, GRAVEL TO SILT SANDS (7.5YR 6/4) w/ SAND, MEDIUM, ROUNDED (40%)	Sp	32		

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
S = Split spoon Tube	O = Other	CAS	G/C Oper	NA
Q = Soil Probe	Notes	NA		

FIGURE S-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO	SBI-05		Page	2	of	2
Installation	Sky Harbor	Coordinates:	Site		1		
Project No	401221.07.02	Client/Project	HAZWAN / SMT MARZEN ANIG				
HAZWPAD Contractor	IT Corporation	Drill Contractor	LAWSON ENVIRONMENTAL				
Drill Method/Rig Type	Air Percussion Hammer		Driller	ART RODRIGUEZ			
Drill Started	11/18/91	(10:20 A.M.)	Drill Ended	11/18/91	(4:25 A.M.)	Borehole dia(s)	9 3/4"
Logged by	GARDNER	E-Log	Y	From	to	Protection Level	D (MODIFIED)



1 = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
2 = Split spoon tube	O = Other	CA S	G/C Open	NA
3 = Castings	Notes	NA		

FIGURE 5-3 a

REV. DATE MAY 990

BORING LOG	BORING WELL NO	ML02-07	Page	1	of	3	
Installation	Sky Harbor	Coordinates:	Site	A 2			
Project No.	40722602.06	Client/Project	HAZWRAP / Sky Harbor ANJG				
HAZWRAP Contractor	IT Corporation	Drill Contractor	LANGE Environmental	Driller	Derek Lopez		
Drill Started	2/6/91	10 55 P.M.	Drill Ended	2/6/91	16 20 P.M.	Borehole dia(s)	9 3/4"
Drill Method/Rig Type: Air Hammer Casing							
Logged by	GARDNER	E-Log	(N)	From	to	Protection Level: (MDFR)	

Depth (ft)	Sample No	Sample Lab	Anal (L/A)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch Graphic Log	Well depth	Water depth	Remarks
0					90% MED TO COARSE, ROUND, DARK BROWN (7.5YR 4/3), MOIST, w/ GRAND, 10% FINE TO MED, ROUND	SP NA				1114.50
5					90% COARSE, ANGULAR, BROWN (7.5YR 5/4) POORLY SORTED w/ GRAND, 10% med, ROUNDED, MOIST.	SP	6	13	14	
10					95% COARSE, ANGULAR, LIGHT BROWN (7.5YR 6/4), POORLY SORTED w/ GRAND, 25% MED TO COARSE, ANGULAR TO ROUND, SLIGHTLY MOIST.	SP	6	26	50	
15					No Recovery				50	
20					No Recovery				50	
25					No Recovery; From Casing at 25 ft:				50	
					60% COARSE, ANGULAR TO SUB ANG, LIGHT BROWN (7.5YR 6/4), POORLY SORTED w/ GRAND, 30% ROUNDED TO ANGULAR, MED TO COARSE & CUBIC, 10% ROUNDED	SP				
30					80% COARSE, ANGULAR, MOSTLY LIGHT BROWN (7.5YR 6/4), MOSTLY WELL SORTED w/ GRAND, 20% ROUNDED TO ANGULAR, MED & w/ RARE COBBLES. SLIGHTLY MOIST.	SP	30	25	50	

J = Thin wall Tube	R = Rock Casing	NA	Field S.C. (Make/Model)	NA
S = Split spoon Label	O = Other	CA S	S.C. Open	NA
Z = Casing	Notes	NA		

FIGURE 5-3 a

REV DATE MAR 1990

BORING LOG	BORING WELL NO	MW2-02	Page	2	of	3		
Installation	Sky Harbor	Coordinates:	Site	2				
Project No	40221-82	Client/Project	HAZWRAP / Sky Harbor ANJ6					
HAZWRAP Contractor	ITC Corporation	Drill Contractor	LAYNE Environmental	Driller	Darryl LODGE			
Drill Started	2/6/91	(10 55 A m)	Drill Ended	2/6/91	8 20 P m)	Borehole dia(s)	9 3/4"	
Drill Method/Rig Type: Air Hammer Casing								
Logged by	GARDNER	E-Log	(N) From			to	Protection Level	D (Modified)

Depth (ft)	Sample No	Sample Lab	No Anal (1/4)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well dia	Water depth	Remarks
35					No Recovery		50				NA
40					No Recovery; From Cyclone at ~ 41 ft: SAND 60% coarse, angular, Brown (7.5YR 5/4) poorly sorted w/ gravel, 20%, rounded to angular, med to coarse, & cobble, 20%, med to coarse, rounded. <u>MOIST</u>	SP GP	50				
45					SAND 70% coarse, angular, dark brown (7.5YR 3/3), <u>MOIST</u> , poorly sorted w/ very fine silts, & gravel, 30%, med, rounded to sub-ang.	SP GP	50				
50					SAND 51% coarse, angular, brown (7.5YR 5/4), moist w/ gravel, 49% angular, med to coarse & occasional cobbles	SP GP	50				
55					No Recovery		50				
60					No Recovery		50				
65					SAND 70% coarse, angular, brown (7.5YR 5/4), poorly sorted w/ gravel, 30%, med to coarse, coarse to ang., w/ occasional gravel	SP	50				

J = Thin wall Tube      R = Rock Coring      NA = Not Available      Field # (Make/Mod)      NA  
 S = Split spoon tube      O = Other      CAS      S-D Oper      NA  
 T = Test tube      Notes      NA

FIGURE 5-3a

REV DATE MAY 99

BORING LOG	BORING WELL NO MW2-02	Page 3 of 3
Installation Sky Harbor	Coordinates:	Site 2
Project No. 40921.02	Client/Project HAZWRAP/SKY HARBOR ANA	
HAZWRAP Contractor IT Corporation	Drill Contractor Landa Engineering	Driller Darryl Locke
Drill Started 2/6/91 (10 55 A.M.)	Drill Ended 2/6/91 (16 20 P.M.)	Borehole dia (1) 9 3/4"
Drill Method/Rig Type: Air Hammer Casing		
Logged by GARDNER	E-Log (N)	From _____ to _____ Protection Level D (MODIFIED)

Depth (ft)	Sample No	Sample Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch. Graphic Log	Well data	Water depth	Remarks
70				90% coarse angular, brown sand (7.5R 5/4), med well sorted but w/ gravel, 10% rounded, med to coarse, very moist.	SW TO SP	17 TO 30			NA
75				From Casing from here to T.D.					
80				75% coarse, angular brown to dark brown (7.5R 4/4), poorly sorted w/ gravel, 20% med to coarse rounded to angular, & cobbles, 5% rounded, med to coarse	SP	-			Very moist clumps.
85									
90				65% coarse, angular to sub ang, dark brown (7.5R 4/4), poorly sorted w/ gravel, 35% med to coarse, med to sub rounded & occasional very coarse cobbles (AND)	SP TO GP	-			
95									Free water at 95 ft.
100				Sand/water/cobble & coarse angular, brown water, brown (7.5R 5/4). Rounded to angular med to coarse gravel & cobbles.					
				T.D. = 101 ft.					

W = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
L = Sp. (spon) Label	O = Other	CAS	G/C Oper.	NA
Q = Casing	Notes	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: SB2-01	Page 1 of 2
Installation Sky Harbor	Coordinates:	Site 2
Project No. 409721.02-06	Client/Project: HAZWRAP / Sky Harbor Area	
HAZWRAP Contractor: IT Corporation	Drill Contractor: LARSEN ENGINEERING	Driller: DEAN LUDGER
Drill Started: 1/21/91 (0805 A.M.)	Drill Ended: 1/29/91 (1140 A.M.)	Borehole dia(s): 9 3/4"
Drill Method/Rig Type: Air Hammer Casings		
Loaded by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (MODIFIED)

Depth (ft)	Sample No.	Sample No. Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch. Graphic Log	Well data	water depth	Remarks	Etc
0										
0				MED TO FINE, 90% w/ coarse sand, rounded, SAND Dark Brown (7.5R 3/2), poorly sorted w/ gravel, 10%, rounded, fine. MOIST	SP	7 7 9				1115.38
5				70% med coarse, angular, brown to light SAND Brown (7.5R 5/4 to 6/4), poorly sorted w/ gravel, 30%, rounded, med. MOIST.	SP	4 7 8				
10				65% coarse, angular, brown to light brown, SAND (7.5R 3/4 to 6/4), poorly sorted w/ gravel, 35%, rounded, med to coarse, moist.	SP	10 14 13				
15				65% coarse, angular, brown to light brown, SAND (7.5R 5/4 to 6/4), poorly sorted w/ gravel, 35%, rounded, med.	SP	50				
20				No Recovery		- 50				
25				No Recovery, from casing at 26 ft. : 60% med to coarse, angular, brown SAND (7.5R 5/4), poorly sorted w/ gravel, 40%, rounded and angular, med to coarse w/ round cobbles	SP	-				
30				No Recovery		- 50				

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	CAS	G/C Oper:	NA
C = Castings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO.: SB2-01	Page 2 of 2
Installation: Sky Harbor	Coordinates:	Site: 2
Project No. 409221.02.00	Client/Project: HAZWOP / Sky Harbor AMG	
H2WFP Contractor: IT Corporation	Drig Contractor: LAMT Environmental	Drillier: Denny Lodge
Drig Started 1/24/91 (12:05 A.M.)	Drig Ended 1/24/91 (11:40 A.M.)	Borehole dia(s) 93A"
Drig Method/Rig Type: Air Hammer Casing		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level D (Modified)

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks	Elev.
35				0 NO RECOVERY; FROM CLONES AT N 36 ft: SAND 20% coarse, angular, light brown (7.5R 6M), poorly sorted w/ gravel, 30%, rounded to angular, med to fine, moist.	SP	50					NA
40				0 NO RECOVERY		50					
45				0 NO RECOVERY; FROM CLONES AT N 46 ft: 65% angular med, light brown SAND (7.5R 6/4), poorly sorted w/ gravel, 35%, rounded to sub angular, med to coarse, rare cobbles.	SP	50					
50				0 99% coarse, angular, light brown SAND (7.5R 5/4), mostly well sorted but w/ 1-5% gravel, med, rounded, moist	SW TO SP	50					
55				0 55% coarse, angular to sub ang, brown SAND (7.5R 5/4), poorly sorted w/ gravel, 45%, rounded to sub rounded, med. moist	SP	50					
60				0 50% coarse, angular, brown SAND (7.5R 5/4), poorly sorted w/ gravel, 50%, rounded to sub angular, med. moist. Very poor Recovery.	SP TO SP	50					
65				0 NO RECOVERY		50					
70				0 NO RECOVERY, FROM CLONES AT N 70 ft: 50% angular to sub ang, med to coarse, brown SAND (7.5R 5/4), poorly sorted w/ gravel, 50%, rounded to angular, med to coarse of angular cobbles	SP TO SP	50				Very moist, N 70 ft	
72											

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	CAS	G/C Oper.:	NA
C = Castings	Notes:	NA		

T.D = N 70 ft.

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO. <b>SR2-02 (02)</b>	Page <b>1</b> of <b>2</b>
Installation <b>Sky Harbor</b>	Coordinates:	Site <b>Site 2</b>
Project No. <b>409721.02.02</b>	Client/Project <b>HAZWRAP / Sky Harbor ANJ</b>	
HAZWRAP Contractor <b>IT Corporation</b>	Drig Contractor <b>LIVAK Environmental</b>	Driller <b>Dennis Johnson</b>
Drig Started <b>1/22/91</b> ( <b>41.00</b> m)	Drig Ended <b>1/22/91</b> ( <b>49.30</b> m)	Borehole dia(s) <b>9 3/4"</b>
Drig Method/Rig Type: <b>Air Percussion Hammer Coring</b>		
Logged by <b>Cosium</b>	E-Log by <b>CS</b>	From <b>0</b> to <b>0</b> Protection Level <b>D (Modified)</b>

Depth (ft)	Sample No	Sample Log	Anal (Y/N)	RECOVERY (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well logs	Water depth	Remarks
0					SAND SILTY, FINE TO MEDIUM GRAINED, DARK BROWN, (7.5YR 4/2) MOIST.	SM	8 9 5				1115.59
5					SAND SILTY, FINE TO MEDIUM, DARK BROWN (7.5YR 4/2), MOIST	SM	6 7 10				
10					SAND SLIGHTLY SILTY, FINE TO MEDIUM, BROWN (7.5YR 5/4), SLIGHTLY MOIST w/ MINOR SILT.	SM	8 10 16				
15					No RECOVERY		50				
20					No RECOVERY		50				
25					FRAM CYCLING AT 26 FT. SAND 60%, med to coarse, angular, LIGHT BROWN SAND BROWN (7.5YR 6/4) w/ gravel, 40%, med to coarse of some COBBLUS, rounded. Dry	SP	50				
30					No RECOVERY FRAM CYCLING AT 29 FT. SAND 75%, med to coarse, angular, LIGHT BROWN (7.5YR 6/4) w/ gravel, 25%, coarse, rounded & angular, occasional COBBLUS	SP	50				

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Model)	NA
S = Sp. Spoon Tube	O = Other	CA S	G/C Oper	NA
Q = Other	Notes	NA		



FIGURE 5-3a

REV DATE MAY 1990  
Page 2 of 2

BORING LOG	BORING/ WELL NO	SB2-02	Site	2
Installation	Sky Harbor Coordinates:			
Project No	402R12020	Client/Project:	HAWAIIAN / SKY HARBOUR / 1/26	
H2O/WPAP Contractor	IT Corporation	Drill Contractor	LAME Environmental	
Drill Method/Rig Type:	Air Percussion Hammer	Driller	Dariusz Roman	
Drill Started	1/22/91 (11:00 A.M.)	Drill Ended	1/22/91 (1:30 P.M.)	Borehole dia(s) 9 7/8"
Logged by	GARDNER	Entered by	(N)	From _____ to _____ Protection Level D (Medium)

Depth (ft)	Sample No	Sample Lab	NO Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch. Graphic Log	Well logs	Water depth	Remarks
35					0 No Recovery		50			NA
40	075				SAND 90% Coarse grained, Angular, Poorly sorted, Brown (2.5R 5/3) w/ gravel, 10% Angular, fragmented, fine to med. Moist	SP	46 50	40 50		
45					0 No Recovery		50			
50	077				90% med to coarse, Angular, Brown (2.5R 5/3), poorly sorted w/ some silt & gravel, 10% rounded to angular, med. Moist	SP	13 50			
55	080				SAND 60% Coarse, Angular, Brown (2.5R 5/3) poorly sorted w/ gravel, 40% rounded, fine to med. Some dark, smooth, clay? smeared on sand. Moist	SP	50			
60					0 No Recovery		50			
65					0 No Recovery		50			
65	080				10-12 ft SAND 90% Coarse, Angular, Brown (2.5R 5/3), poorly sorted w/ gravel (10%), rounded, fine to med. Moist	SP	19 26			
70					Thin wall Tube R = Rock Coring NA Field G/C (Make) NA					NA
70					Sp. Spoon Tube O = Other CAS G/C Open NA					NA
72					Notes: NA					

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING WELL NO 382-04	Page 1 of 2
Installation Sky Harbor	Coordinates:	Site 2
Project No 409221-01-06	Client/Project HAZWRAP / Sky Harbor Area	
HAZWRAP Contractor IT Corporation	Drill Contractor LAYNE ENVIRONMENTAL	Driller Dwight Peterson
Drill Started 1/22/91 (15 OF 2 MI)	Drill Ended 1/22/91 (10 TO 1 MI)	Screened (dials) 93/4"
Drill Method/Rig Type: AIR Percussion Hammer Casing		
Logged by GARDNER	E-Log (N) From _____ to _____	Protection Level: D (Modified)

Depth (ft)	Sample No	Sample Lab	Anal (Y/N)	Recovery	Lithologic Description	USCS	Blow 16 inch	Graphic Log	Well Data	Water Depth	Remarks
0	0-2				95% MED. TO COARSE, ANGLULAR, SAND W/ SOME SILT; DARK BROWN (7.5R 4/8) MOIST, w/ GRAVEL, 5%, ROUNDED, FINE.	SP TO SP	5 4 4				114.67
5	0-10				95% MED TO COARSE, ANGLULAR, BROWN (7.5R 5/3), MOIST, w/ OCCASIONAL FINE ROUNDED GRAVEL	SP	5 8 16				
10	0				NO RECOVERY		50				
15	0-15				75% MED TO COARSE, ANGLULAR, SAND POORLY SORTED, BROWN (7.5R 9/3), MOIST, w/ GRAVEL, 25%, ROUNDED FINE TO MED. MOIST	SP	29 41 50				
20	0				NO RECOVERY		50				
25	0				NO RECOVERY FROM CUTTINGS AT ≈ 26 FT		50				
25	0-25				SAND 70% COARSE; ANGLULAR, LIGHT BROWN (7.5R 6/4), w/ GRAVEL, 30%, MED TO COARSE, ROUNDED TO ANGLULAR, RARE COBBLES	SP					
30	0				NO RECOVERY		50				

U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod)	NA
S = Sp. Spoon Tube	O = Other	CAS	G-C Oper	NA
Q = Sp. Spoon	Notes	NA		

FIGURE S-3 a

REV. DATE MAY 99

BORING LOG	BORING WELL NO S32-04	Page 2 of 2
Hosta Bldg Sky Harbor	Coordinates:	Site 2
Project No 4097112.06	Client/Project HAZWRAP / Sky Harbor ANG	
HAZWRAP Contractor IT (International)	Drill Contractor LAYNE ENVIRONMENTAL	Driller Duane Peterson
Drill Start 1/22/01 1505 P.M.	Drill Ended 1/22/01 1030 A.M.	Borehole dia: 93/4"
Drill Method/Rig Type Air Percussion Hammer Casing		
Logged by GARDNER	Enclog (N)	From _____ to _____ Protection Level D (Quarried)

DEPTH (ft)	RECOVERY (%)	Lithologic Description	USCS	Blow 6 inch Sphonic Log	Water Depth	Remarks
35	0	NO RECOVERY		50		NA
40	0	NO RECOVERY FROM CLOGGING AT APPROX 40 FT: SAND 60%, COARSE, BROWN (7.5YR 5/3), SUB-ANGULAR, W/ GRAVEL 40%, ROUNDED & SUB-ANGULAR, MED, PUT UP WITH LOBBLES	SP	50		MOIST CUTTING AT 43-44 FT
45	0	NO RECOVERY		50		
50	0	80% MED TO COARSE, BROWN (7.5YR 5/3), SAND ANGLULAR W/ GRAVEL 20%, ROUNDED, MED MOIST	SP	50		
55	0	90% MED PUT UP SOME SILT, POORLY SORTED, DARK BROWN (7.5YR 4/3) (MOIST) W/ RAIR GRAVEL (5-10%), FINE TO MED, ROUNDED.	SP TO SW	50		
60	0	NO RECOVERY DRY CUTTING.		50		
65	0	NO RECOVERY FROM CLOGGING AT APPROX 66 FT: 70% COARSE ANGLULAR TO SUB-ANGULAR, BROWN (7.5YR 5/3) (MOIST), W/ GRAVEL 30%, MED TO COARSE W/ RAIR LOBBLES, ROUNDED	SP	7		
70	0	90% MED TO COARSE, ROUNDED TO SUB-ANGULAR, BROWN (7.5YR 5/3) (VERY MOIST) QUARTZ GRAVEL 10%, ROUNDED, FINE TO MED	S TO SW	16		VERY MOIST CUTTING - AHEAD WATER
72						

Test well Tube	P = Rock Coring	NA	File # G (Make/Mod)	NA
Seal/Stopper Label	O = Other	CAS	G (Open)	NA
Notes	NA			

FIGURE 5-3a

REV DATE MAY 199

BORING LOG	BORING/WELL NO	MW3-01	Page	1 of 2	
Installation	Sky Harbor	Coordinates:	Site	3	
Project No.	401331-06	Client/Project	HAZWRAP / Sky Harbor AN6		
HAZWRAP Contractor	IT CORPORATION	Drig Contractor	LAYNE Environmental	Driller	Dwight Peterson
Drig Started	3/22/91 (6 30 A.M.)	Drig Ended	3/22/91 (3 30 P.M.)	Borehole dia(s)	10 3/4"
Drig Method/Rig Type: DUAL TUBE PERCUSSION					
Lodged by	GARDNER	E-Log (Y/N)	(N)	From	to
				Protection Level	D (MODIFIED)

DEPTH (ft)	Sample No	Anal (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks
0										
0-7.5				90% FINE, SAND, DARK BROWN (7.5YR 3/3), MOIST, MOSTLY WELL SORTED BUT w/ OCCASIONAL GRAVEL, 10% FINE, SAND. MOIST	SW	12 10 11				
7.5-10				100% MED TO COARSE, SAND TO SUB SAND, BROWN (7.5YR 5/3), MOIST, WELL SORTED w/ FINE GRAVEL, FINE, SAND. MOIST	SW	5 6 8				
10-15				70% MED TO COARSE, SAND TO SUB SAND, BROWN (7.5YR 5/3), POORLY SORTED w/ GRAVEL, 30% SAND TO SUB SAND, MED TO COARSE. SLURRY MOIST	SP	30 27 50				
15-20				NO RECOVERY		50				
20-25				NO RECOVERY		50				
25-30				NO RECOVERY; FROM CYCLONE AT 24 FT: 75% MED TO FINE, SAND TO SUB SAND, LT. BROWN (7.5YR 6/4), POORLY SORTED w/ GRAVEL, 25% MED TO COARSE, SAND TO SUB SAND. NOTE: very HARD (Boulders?) AT 24 FT, then SAND UNDERMINATION w/ GRAVEL, THEN BACK TO HARD MATERIAL. DRY	SP	50				
30-35				NO RECOVERY		50				

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod.)  
 S = Spoon tube      O = Other      G/C Oper  
 T = Test pits      Notes

FIGURE 5-3a

REV DATE MAY 199

BORING LOG	BORING/WELL NO	MWJ-01	Page	2	of	3
Installation	Sky Harbor	Coordinates:	Site:	3		
Project No.	40741-06	Client/Project	HAZWRAP / Sky Harbor ANG			
HAZWRAP Contractor	IT Corporation	Drig Contractor	LAYNE ENGINEERING	Driller	DUNCAN PERKINS	
Drig Started	3/22/91 @ 30 ft	Drig Ended	3/22/91 @ 30 ft	Borehole dia(s)	10 1/2"	
Drig Method/Rig Type	DUAL TUBE PRESSURE					
Logged by	GARDNER	E-Log	Y / (N)	From	to	Protection Level D (Modified)

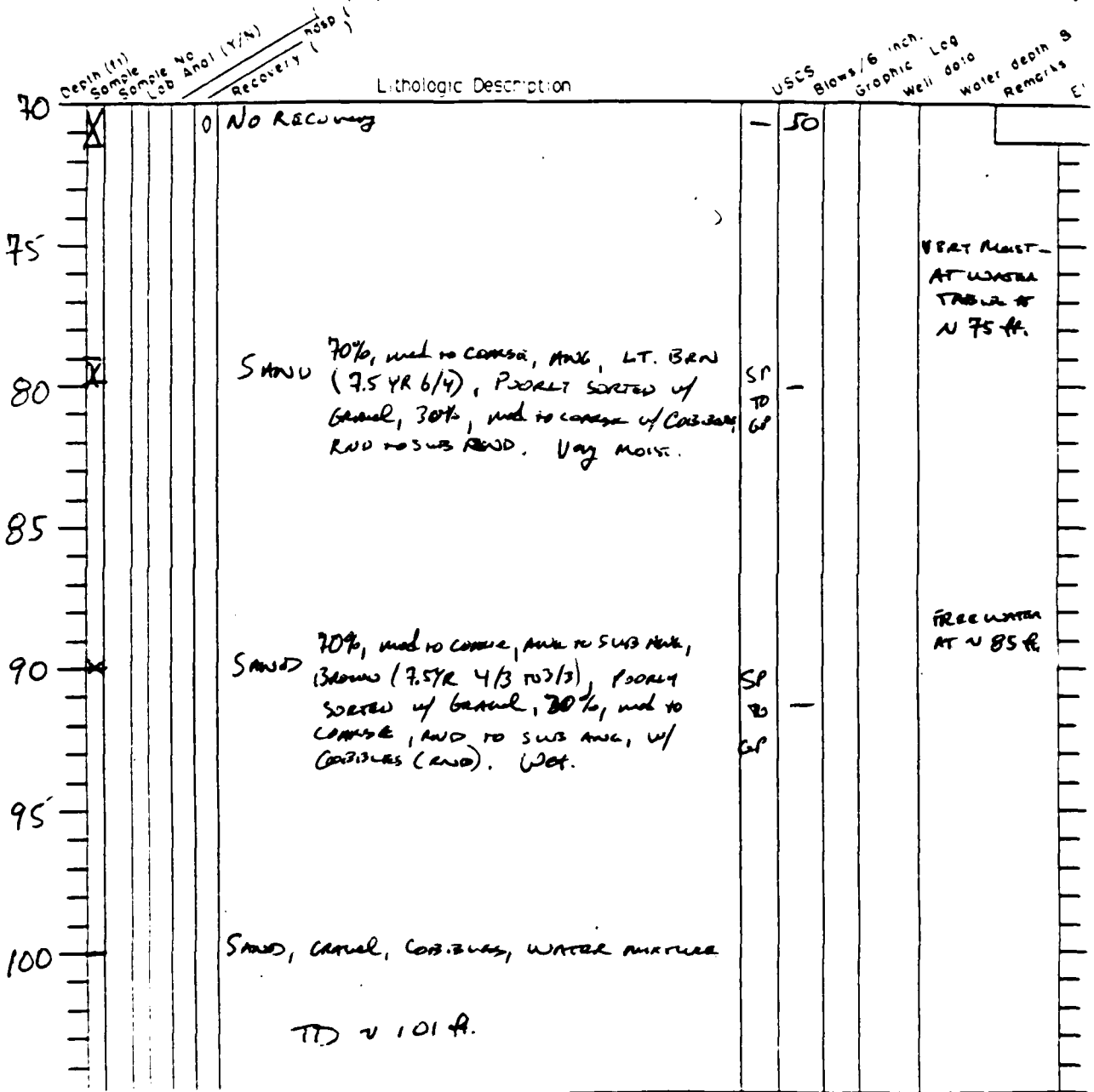
Depth (ft)	Sample No	Sample Lab	Anal (Y/N)	RECOVERY	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks
35	015				80% med to coarse, med to sub ang SAND BROWN (7.5YR 5/3 to 4/3), POORLY SORTED w/ med silt & gravel, 20% med to fine, med. Very MOIST.	SP	50				
40	020				70% med to coarse, med, Brown SAND (7.5YR 4/3), POORLY SORTED w/ silt, 10% fine, Brown, & gravel, 20% med to coarse, med to sub ang. Very MOIST.	SP	50				
45	0				55% med to coarse, med, Brown SAND (7.5YR 4/3), POORLY SORTED w/ gravel, 45% med to coarse, med to sub ang. MOIST. NOT enough sample to analyze.	SP TO GP	50				
50	010				75% med to coarse, med to sub ang SAND BROWN (7.5YR 4/3), POORLY SORTED w/ silt, 30% fine, Brown, & gravel. 20% med to coarse, med to sub ang. MOIST.	SP	50				
55	010				80% med to coarse, angular, Brown SAND (7.5YR 4/3), POORLY SORTED w/ gravel, 20% med to coarse, med to sub ang. MOIST	SP	36 50				
60	030				40% med to coarse, angular, Brown SAND (7.5YR 4/3), mostly well sorted but w/ occasional gravel, 10% fine, med, & med silt. MOIST	SW TO SP	32 50				
65	0				No Recovery	-	50				

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod) \_\_\_\_\_  
 S = Sp. Spoon (tube)      O = Other      G/C Oper. \_\_\_\_\_  
 C = Closures      Notes \_\_\_\_\_

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO. <u>MU3-01</u>	Page <u>3</u> of <u>3</u>
Installation: <u>Sky Harbor</u>	Coordinates:	Site <u>3</u>
Project No. <u>40721-06</u>	Client/Project: <u>HARBOR / Sky Harbor ANV</u>	
HAZWOP Contractor: <u>IT (CANTON)</u>	Drill Contractor: <u>LAWSON ENVIRONMENTAL</u>	Driller: <u>DWIGHT PETERSON</u>
Drill Started: <u>3/22/91 (8:30 A.M.)</u>	Drill Ended: <u>3/22/91 (3:30 P.M.)</u>	Borehole dia(s): <u>10 3/4"</u>
Drill Method/Rig Type: <u>DUAL TUBE PERCUSSION</u>		
Logged by: <u>GARDNER</u>	E-Log: <u>(N)</u> From _____ to _____	Protection Level: <u>D (MODIFIED)</u>

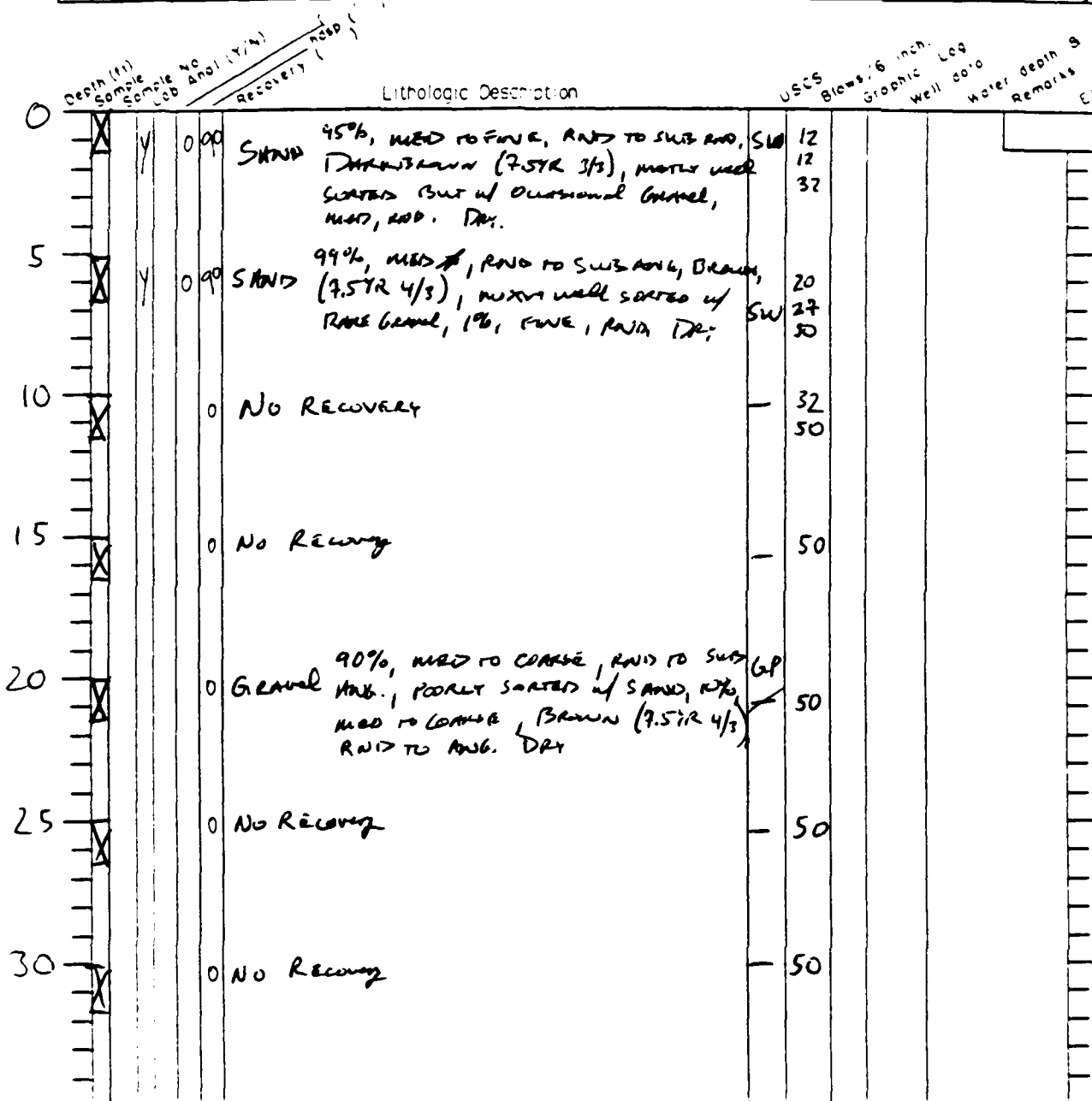


U = Thin wall Tube      R = Rock Core      Field G/C (Make/Mod.)  
 S = Split spoon tube      O = Other      G/O Open  
 T = Test      Notes

FIGURE S-3a

REV DATE MAY 99

BORING LOG	BORING/WELL NO	MW3-02	Page	1	of	3	
Installation	Sky Harbor	Coordinates:	Site	3			
Project No	4072602	Client/Project:	HAWAIIAN / AT SEA HARBOR AN6				
HAZWRAP Contractor	IT Corporation	Drill Contractor	LAMAR ENVIRONMENTAL	Driller	GABBY RODRIGUEZ		
Drill Started	3/23/91	(0.25 m)	Drill Ended	3/24/91	(4.30 m)	Borehole dia(s)	10 3/4"
Drill Method/Rig Type:	Dual Tube Percussion						
Logged by	GARDIN	E-Log	Y	From		to	
						Protection Level:	D (MODIFIED)

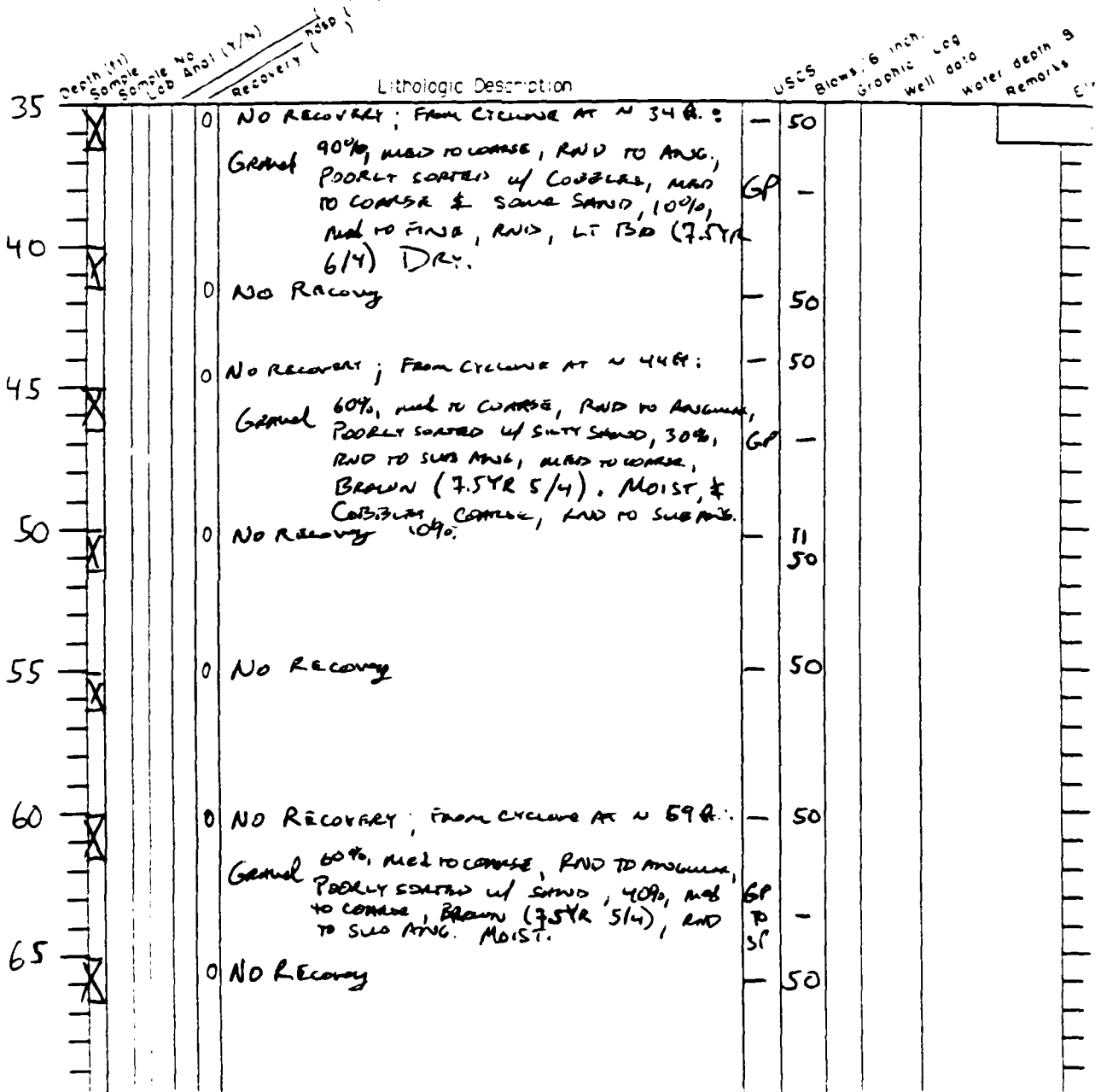


J = Trip wall Tube      R = Rock Coring      Field G.C. (Make/Mod) \_\_\_\_\_  
 S = Soil Spoon Tube      O = Other      G.C. Seen \_\_\_\_\_  
 Notes \_\_\_\_\_

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO	MW3-02	Page	2	of	5
Installation	Sky Harbor	Coordinates:	Site	3		
Project No.	40771-03-06	Client/Project:	HAZWRAP / Sky Harbor AWG			
HAZWRAP Contractor:	IT Corporation	Drill Contractor:	LARRY ENGLISH	Driller:	GABBY RODRIGUEZ	
Drill Started:	3/23/91 (8 25 A.M.)	Drill Ended:	3/23/91 (4 30 P.M.)	Borehole dia(s)	10 7/8"	
Drill Method/Rig Type:	Dual Tube Percussion					
Logged by:	GARDIN	E-Log:	Y (N)	From	to	
				Protection Level:	D (MODIFIED)	



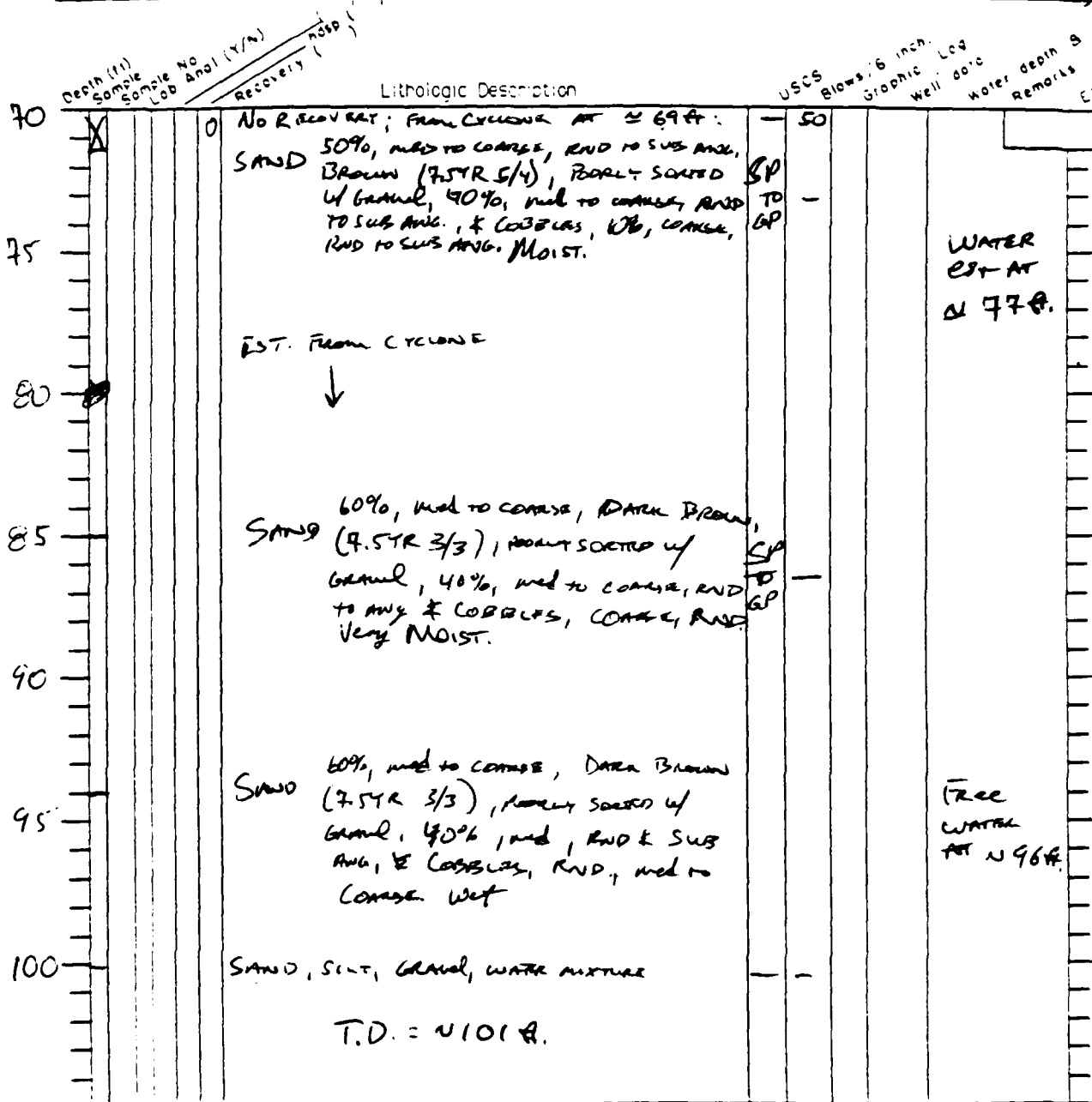
U = Thin wall Tube      R = Rock Coring      File # G/C (Maker/Mod) \_\_\_\_\_  
 S = Split spoon tube      O = Other      G/C Oper \_\_\_\_\_  
 C = Casing      Notes \_\_\_\_\_



FIGURE S-3a

REV DATE MAY 990

BORING LOG	BORING/WELL NO MW3-02	Page 3 of 3
Installation Sky Harbor	Coordinates:	Site 3
Project No: 40921-02-06	Client/Project: HAZURAT / Sky Harbor ANG	
HAZWRAP Contractor: IT Corporation	Drill Contractor: LAYNE Environmental	Driller: GARY RODRIGUEZ
Drill Started: 7/23/91 (8 25 A. m)	Drill Ended: 3/27/91 (4 30 P. m)	Borehole dia(s) 10 7/8"
Drill Method/Rig Type: Dual Tube Percussion		
Logged by: GARDIN	E-Log: Y (N) From _____ to _____	Protection Level: D (MODIFIED)



U = Thin wall Tube	R = Rock Coring	File # G/C (Make/Mod)
S = Split spoon tube	O = Other	G/C Open
Q = Other	Notes	

FIGURE 5-3 a

REV DATE MAY 19C

BORING LOG	BORING/WELL NO.: SB3-01	Page 1 of 2
Installation: Sky Harbor	Coordinates:	Site: 3
Project No.: 40772-06	Client/Project: HAZWAP / Sky Harbor ANJG	
HAZWPAP Contractor: ITC	Drig Contractor: LARSE ENVIRONMENTAL	Driller: DUNN PETERSON
Drig Started: 3/24/91 (8:40 a.m)	Drig Ended: 3/24/91 (1:00 p.m)	Borehole dia(s): 10 3/4"
Drig Method/Rig Type: Dual Tube Percussion		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (Additional)

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (Y/N)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth	Remarks
0				SAND 99% FINE, RND TO SUB ANG, BROWN (7.5YR 5/4 TO 4/4), MOSTLY WELL SORTED BUT w/ < 1% G LT & FINE, RND GRANUL.	SW	32				
5				No Recovery		50				
10				No Recovery		50				
15				No Recovery; FROM CYCLONE AT 14-15 FT.		50				
20				SAND 55% med to coarse, sub ang to ang, LT Brown (7.5YR 6/4), POORLY SORTED w/ GRANUL, 30% med to coarse, RND TO ANGULAR, & COBBLES, COARSE, RND TO SUB ANGULAR. DRY	SP TO GP					
25				No Recovery		50				
30				No Recovery		50				

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod.) \_\_\_\_\_  
 S = Spinspoon (tube)    O = Other      G/C Oper.: \_\_\_\_\_  
 C = Casing      Notes: \_\_\_\_\_

FIGURE 5-3a

REV DATE MAY 199

BORING LOG	BORING/WELL NO.: <u>MSB3-01</u>	Page <u>2</u> of <u>2</u>
Installation: <u>Sky Harbor</u>	Coordinates:	Site: <u>3</u>
Project No.: <u>407821-02-02</u>	Client/Project: <u>HAZWRAP/Sky Harbor ANG</u>	
HAZWRAP Contractor: <u>IT Corporation</u>	Drig Contractor: <u>Layne Environmental</u>	Driller: <u>Donner Peterson</u>
Drig Started: <u>3/24/91</u> (8:40 a.m)	Drig Ended: <u>3/24/91</u> (1:00 p.m)	Borehole dia(s): <u>10 3/4"</u>
Drig Method/Rig Type: <u>Down Tube Percussion</u>		
Logged by: <u>Gardner</u>	E-Log (Y/N) From <u>    </u> to <u>    </u>	Protection Level <u>D (MODIFIED)</u>

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well logs	Water depth	Remarks
35	X			No Recovery; From Cyclone at ~ 34 ft: SAND 60%, med to coarse, rnd to angular, lt. brown (7.5 YR 6/4), poorly sorted w/ gravel, 30%, med to coarse, rnd to sub ang, & cobbles, 10%, rnd to sub ang. DRY.		50				
40	X			No Recovery		50				
45	X			No Recovery; From Cyclone at ~ 44 ft: SAND 51%, coarse, med to coarse, dark brown (7.5 YR 3/3), poorly sorted w/ some silt, 5%, & gravel, 30%, med to coarse, rnd to sub ang, & cobbles, 15%, rnd, coarse. MOIST. ODDOR	SP TO GP	50				
50	X			SAND 60%, med to coarse, ang to sub rnd, dark brown (7.5 YR 3/3), poorly sorted w/ silt, 3%, & gravel, 30%, rnd, med to coarse, & cobbles, 5%, rnd, coarse. MOIST. Very sulfur odor	SP	27 50				
55	X			No Recovery		29 50				
60	X			No Recovery		50				
65	X			No Recovery No Recovery At 70 ft. = From cyclone at 67-20: SAND 63%, med to coarse, rnd to sub ang, dark brown (7.5 YR 3/3 to 4/3), poorly sorted w/ gravel, 30%, med to coarse, rnd to sub ang, & cobbles, 5%, coarse, rnd	SP TO GP	50				
70	X			Thin wall Tube Spoon (tube) C = Cuttings	R = Rock Coring O = Other	Notes: <u>TP = 20 ft</u>	Field G/C (Make/Mod.)	G/C Oper.		Very moist & muddy shale odor of solvent.

22 SX Cement  
3 SX Mud

FIGURE 5-3a

REV. DATE MAY 199

BORING LOG	BORING/WELL NO: SB3-03	Page 1 of 2
Installation: Sky Harbor	Coordinates:	Site: 3
Project No: 401421-06	Client/Project: HAZWRAP / Sky Harbor ANG	
HAZWRAP Contractor: IT Concessions	Drig Contractor: LAYNE Environmental	Driller: DUNCAN PATTERSON
Drig Started: 3/25/91 (11:45 A.M)	Drig Ended: 3/25/91 (4:30 P.M)	Borehole dia(s): (0.75)
Drig Method/Rig Type: DUAL TUBE PERCUSSION		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (Modified)

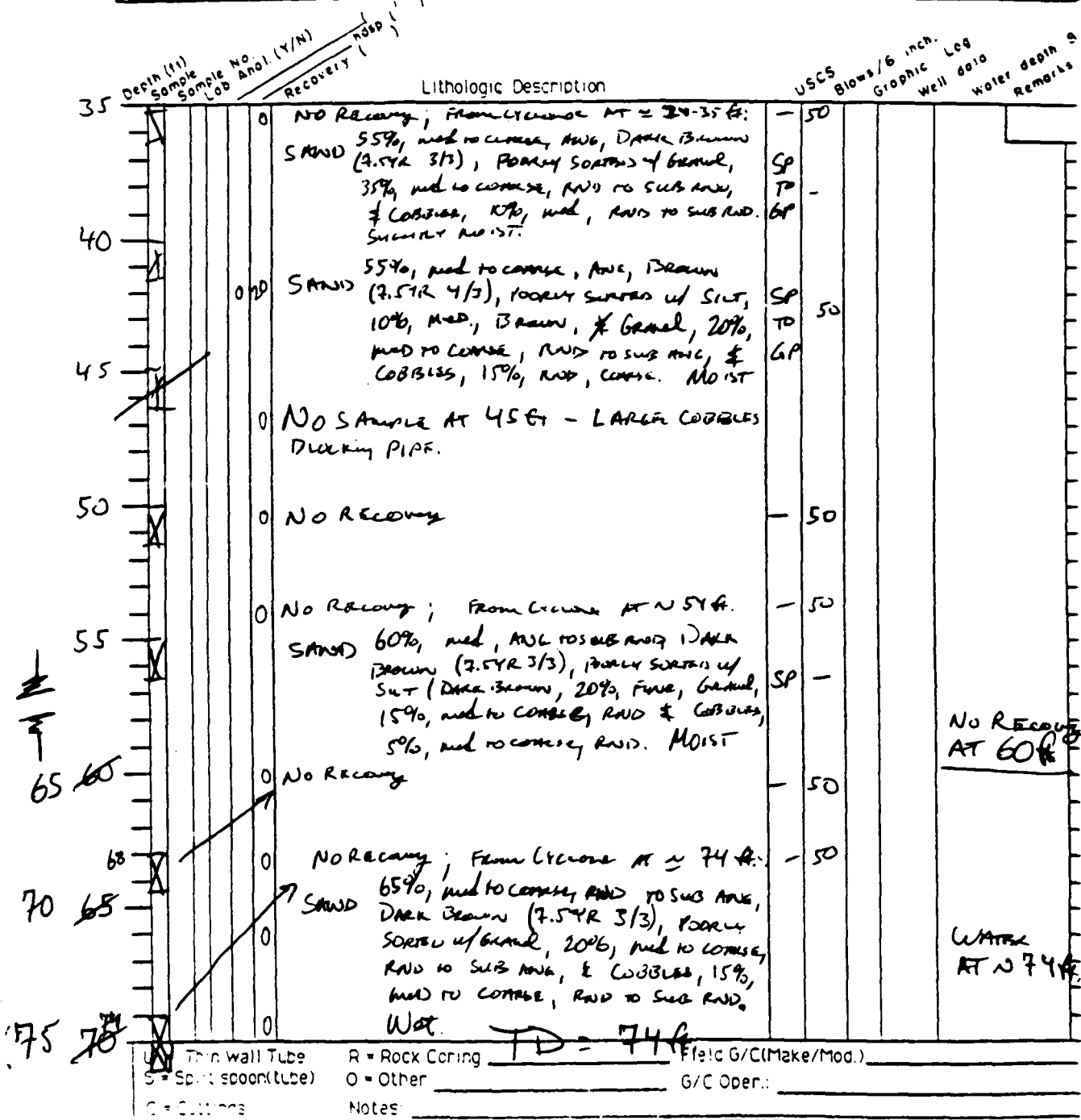
Depth (ft)	Sample No	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch	Graphic Log	Well data	Water depth	Remarks
0										
0.50				SAND 80%, med to coarse, RND to SUB ANG, Brown (7.5R 5/4), poorly sorted w/ gravel, 20%, med to fine RND. Slightly moist.	SP	22 25 34				
5				SAND 70%, med to coarse, RND to SUB ANG, Brown (7.5R 5/4), poorly sorted w/ gravel, 20%, med to coarse, med to coarse, 10%, med to coarse, RND	SP	25 50				
10				SAND 80%, med to coarse, RND to SUB ANG, Dark brown (7.5R 3/3), poorly sorted w/ gravel, 20%, med to coarse, RND to SUB RND. Slightly moist	SP	22 32 50				
15				No Recovery		50				
20				SAND 70%, med to coarse, RND to SUB ANG, Brown (7.5R 4/3), poorly sorted w/ gravel, 20%, med to coarse, ANG to SUB RND, 2 coarse, 10%, RND, coarse	SP	18 24 38				
25				No Recovery		50				
30				No Recovery		50				

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod.)  
 S = Spill spoon (tube)      O = Other      G/C Oper.:  
 C = Cuttings      Notes:

FIGURE 5-3a

REV DATE MAY 19C

BORING LOG	BORING/WELL NO.: SB3-03	Page 2 of 2
Installation: Sky Harbor	Coordinates:	Site: 3
Project No.: 409721.02	Client/Project: HAZWRAP / SKY HARBOR ANX	
HAZWRAP Contractor: ITC Corporation	Drig Contractor: LAME ENVIRONMENTAL	Driller: DWIGHT PETERSON
Drig Started: 3/25/91 (11:45 A.M.)	Drig Ended: 3/25/91 (4:30 P.M.)	Borehole dia(s): 10 1/4"
Drig Method/Rig Type: DIRT TUBE PROCESSOR		
Logged by: GARDNER	E-Log (Y/N): (N)	From _____ to _____ Protection Level: D (MODIFIED)



26 SK Cement

4 SK Bentonite Powder

FIGURE S-3a

REV. DATE MAY 199

BORING LOG	BORING/WELL NO.: SB3-04	Page 1 of 2
Installation: Sky Harbor	Coordinates:	Site: 3
Project No.: 40311-02	Client/Project: HAZWRAP / Sky Harbor ANG	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	Driller: DUNCAN PATRICKSON
Drig Started: 3/24/91 (2:00 P.M.)	Drig Ended: 3/25/91 (11:00 A.M.)	Borehole dia(s): 10 3/4"
Drig Method/Rig Type: DEEP TUBE PERCUSSION		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (MODIFIED)

Depth (ft)	Sample	Sample No.	Lab Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch.		Water Depth	Remarks
							Graphic Log	Well logs		
0	X									
0-1	Y	0180			97% FINE, RND, DARK BROWN (7.5YR 3/3 to 4/3), mostly well sorted w/ minor silt & rare gravel, fine, rnd. Slight moist	SW	10	19	14	
5	Y	0180			100% med to coarse, RND to sub ang, brown (7.5YR 5/3), well sorted. Slight moist.	SW	14	25	29	
10	X	0170			75% med to coarse, RND to sub ang, brown (7.5YR 5/2), poorly sorted w/ gravel, 20% med to coarse, RND to sub ang & gravel, 5% med to coarse, RND. DRY.	SP	50			
15	Y	0170			80% med, RND to sub ang, brown to dark brown (7.5YR 4/3), poorly sorted w/ gravel, 20% med to coarse RND to sub ang, & occasional cobbles, coarse, RND. DRY	SP	50			
20	X	0120			60% med to coarse, sub RND to ang, brown (7.5YR 5/3), poorly sorted w/ gravel, 30% med to coarse, RND to sub ang & cobbles, 10% med to coarse, RND to sub ang. DRY	SP TB 6P	50			
25	X	0			No Recovery			50		
30	Y	0			No Recovery			50		

U = Thin wall Tube      R = Rock Coring      Field G/C (Make/Mod.)  
 S = Spoon (tube)      O = Other      G/C Oper.:  
 C = Casing      Notes:

FIGURE 5-3a

REV DATE MAY 199

BORING LOG	BORING/WELL NO.: SB3-04	Page 2 of 2
Installation: Sky Harbor	Coordinates:	Site: 3
Project No.: 404921-02.06	Client/Project: HAZWRAP / Sky Harbor AN6	
HAZWRAP Contractor: [unclear]	Drig Contractor: L&E Environmental	Driller: Duane Peterson
Drig Started: 3/24/91 (2:00 P.M.)	Drig Ended: 3/25/91 (11:00 A.M.)	Borehole dia(s) 10 3/4"
Drig Method/Rig Type: Dual Tube Percussion		
Logged by: Garroun	E-Log (Y/N) From _____ to _____	Protection Level: D (Modified)

Depth (ft)	Sample No.	Sample Lab	Anal. (Y/N)	Recovery	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth	Remarks
35											
	010				SAND 30%, med to coarse, AND to sub ang, Brown to Dark Brown (7.5TR 4 1/2 to 3/3), Poorly sorted w/ minor silt & gravel, 30%, med to coarse & cobbles, med to coarse, AND to sub and. MOIST.	SP	50				
40											
	010				SAND 60%, med to coarse, AND to sub and, Brown (7.5TR 5 1/2), Poorly sorted w/ gravel, 30%, med to coarse and, & cobbles, 10%, med to coarse, AND to sub and. MOIST.	SP to GP	50				
45					No Recovery		50				3/25/91
					No Recovery; From cyclone at ~ 49 ft.		50				
50											
					SAND 70%, med to coarse, AND to sub ang, Dark Brown (7.5TR 7/3 to 4/3), Poorly sorted w/ gravel, 20%, med to coarse, AND to sub ang, & cobbles, med to coarse, AND. MOIST.	SP					No Recovery at 55 ft.
65											No Recovery at 60 ft.
68					Gravel 75%, med to coarse, AND to sub ang, Poorly sorted w/ sand, 25%, med to coarse, AND to sub ang, Brown (7.5TR 4/3). MOIST.	GF	50				
70					No Recovery at 74 ft. ; From cyclone:						
					SAND 60%, med to coarse, AND to sub ang, Brown (7.5TR 4/3), Poorly sorted w/ gravel, 30%, med to coarse, AND to sub ang, & cobbles, 10%, coarse, AND to sub and. Very MOIST.						Water at 74 ft.
75											
70											
					TD = 74 ft.						
U = Thin wall Tube		R = Rock Coring		Field G/C (Make/Mod.)							
S = Split spoon tube		O = Other		G/C Oper.:							
C = Cuttings		Notes:									

22 SK Count  
3 SK UND

FIGURE 5-3a

REV. DATE MAY 1990

BORING LOG	BORING WELL NO	MW5-01	Page	1	of	3
Installation	Sky Harbor	Coordinates:	Site	5		
Project No	40771-82	Client/Project	HAZWRAP/Sky Harbor AN6			
HAZWRAP Contractor	IT Corporation	Drill Contractor	Layne Environmental	Driller	Darryl Laddie	
Drill Started	2/2/91	(0830 a.m.)	Drill Ended	2/2/91	(1400 p.m.)	Borehole dia: 9 3/4"
Drill Method/Rig Type: Air Hammer Casing						
Logged by		GARDNER	E-Log	(N)	From	to
Protection Level: D (MODIFIED)						

Depth (ft)	Sample No	Sample No Lab	Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows	6 inch Graphic Log	Well logs	Water depth	Remarks
0	X	Y	0 90		90% DARK BROWN (7.5TR 313), MED SAND TO FINE, ROUNDED, POORLY SORTED w/ SOME SILT, 5%, & OCCASIONAL GRAD, 5%, KAWAIA, MED. MOST	SM TO SP	6 TO 8				1117.10
5	X	Y	0 80		95% COARSE, MIXED w/ SILT, LIGHT BROWN (7.5TR 614), ROUNDED TO ANHULAR, w/ OCCASIONAL GRAD, 5%, ROUNDED, FINE. SILTY MUD.	SW	8 TO 10				
10	X		0		50% COARSE, ANHULAR, LIGHT BROWN (7.5TR 614), POORLY SORTED w/ GRAD, 45%, ROUNDED TO ANHULAR, MED TO COARSE & COARSE, 5%, ROUNDED, COARSE	SP TO GP	15 TO 50				
15	X		0		No Recovery	-	50				
20	X		0 5		60% COARSE, ANHULAR, <sup>med</sup> LIGHT BROWN (7.5TR 614), POORLY SORTED w/ GRAD, 40%, MED TO COARSE, ROUNDED TO ANHULAR w/ OCCASIONAL COARSE, SAND, MED TO COARSE	SP	50				
25	X		0 5		60% COARSE TO VERY COARSE, ANHULAR, LIGHT BROWN (7.5TR 614), POORLY SORTED w/ GRAD, 35%, MED TO COARSE, ROUNDED TO ANHULAR, & COARSE, 5%, MED TO COARSE, ROUNDED.	SP TO GP	50				
30	X		0		No Recovery	-	50				

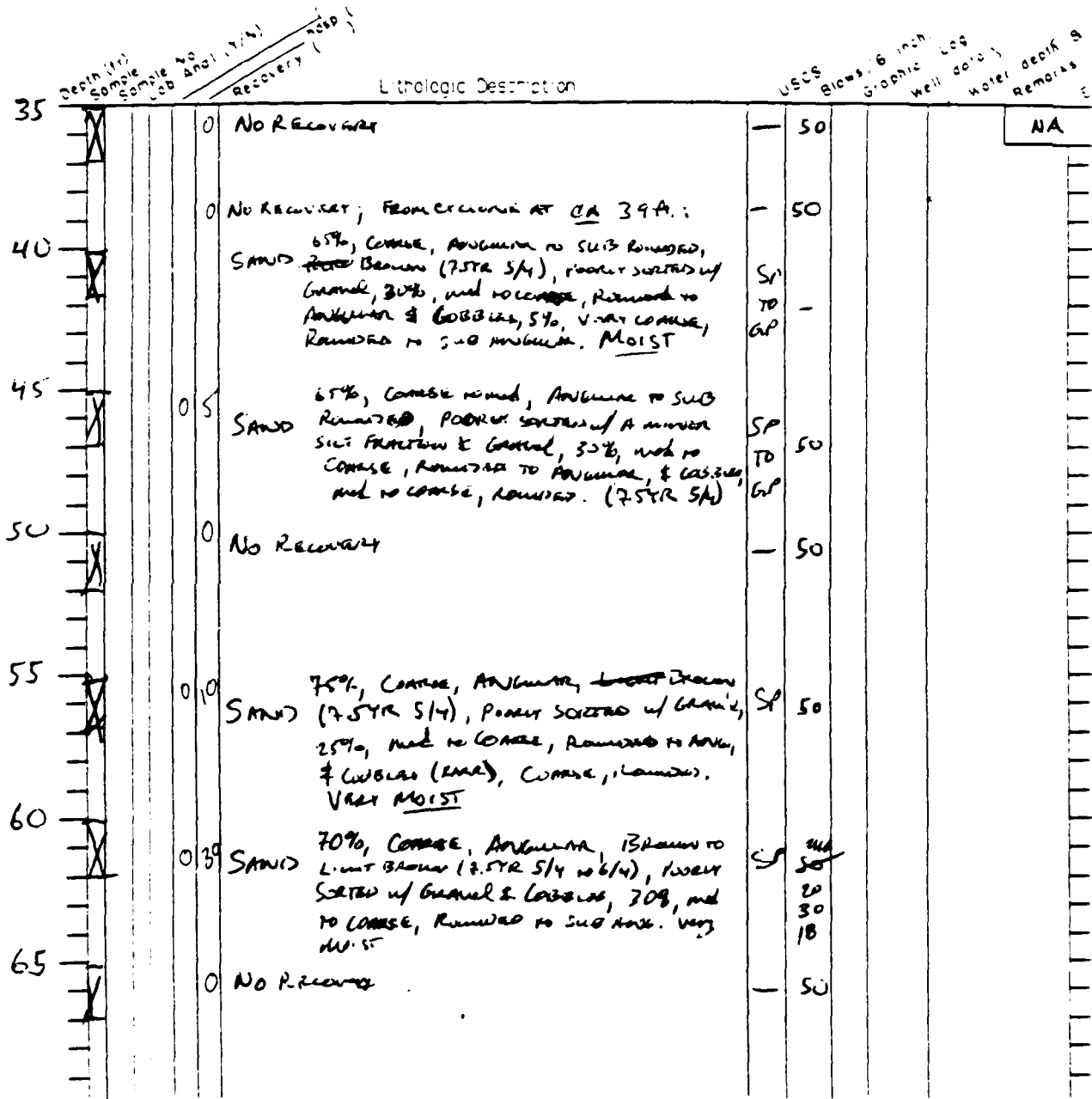
U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Maker/Mod)	NA
D = Sp. Label	O = Other	CAS	G/C Oper	NA
Notes	NA			



FIGURE S-3a

REV. DATE MAY 1997

BORING LOG	BORING WELL NO	MUS-01	Page	2	of	3
Site at	Sky Harbor	Coordinates:	Site	5		
Project No.	40974.02	Client/Project	HAZWRAP / Sky Harbor Amph			
HAZWRAP Contractor	IT Corporation	Drill Contractor	LORING ENVIRONMENTAL Driller DARY LINDA			
Drill Started	2/2/91	(0830 A.M.)	Drill Ended	2/14/91	(1400 A.M.)	Equivalent (drill) 9 3/4"
Drill Method/Rig Type:	AIR Hammer Casings					
Logged by	GARDNER	E-Log	(N)	From	to	Protection Level D (MODIFIED)



□ = Thin wall tube	□ = Rock casing	NA	Field C/Make Mod	NA
○ = Solid copper label	○ = Other	CAS	Field Oper	NA
□ = Other	Notes	NA		

FIGURE 5-3a

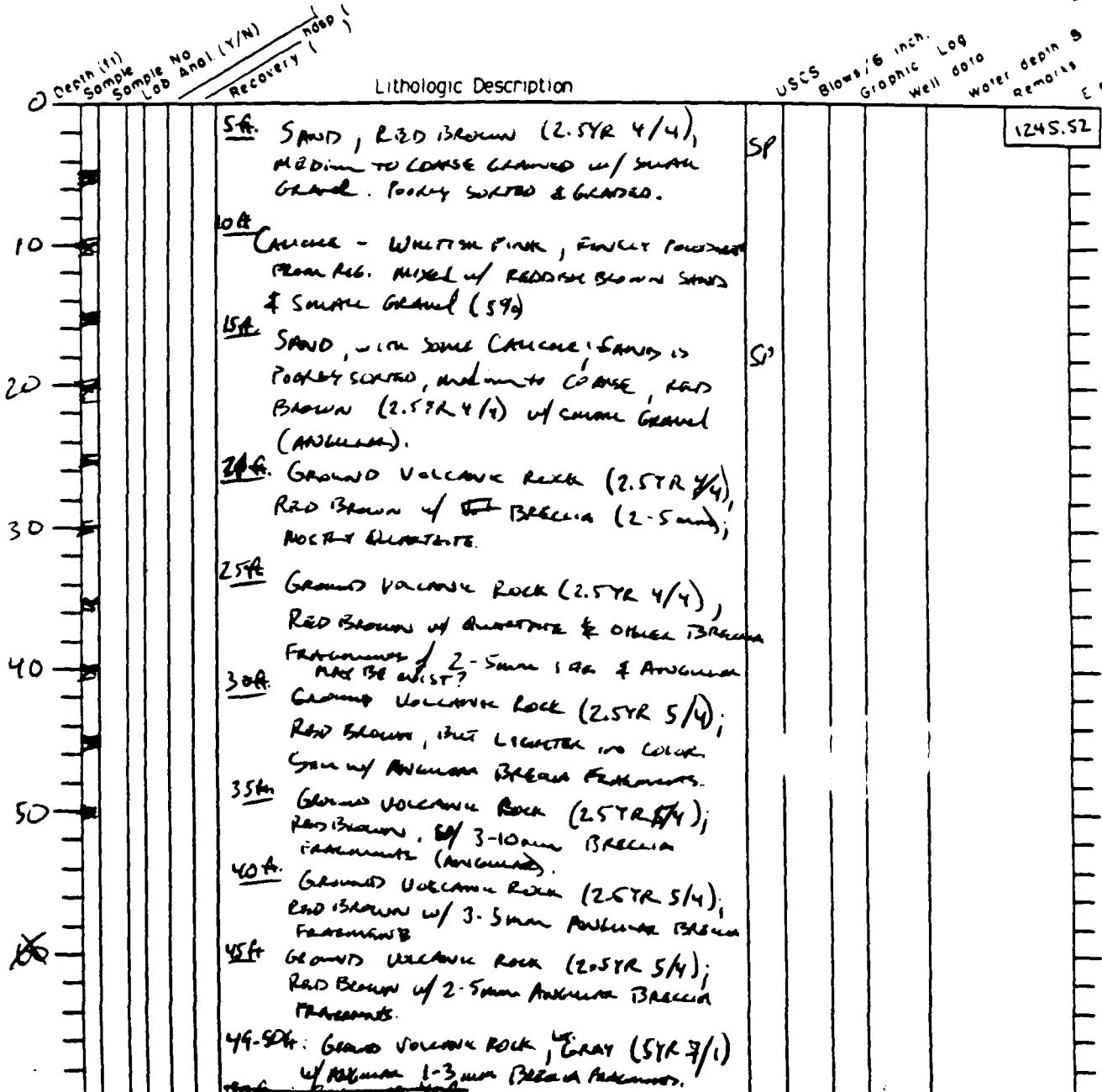
REV DATE MAY 1990

BORING LOG	BORING/WELL NO	MWS-01	Page	2 of 3	
Installation	Sky Harbor	Coordinates:	Site	5	
Project No	409771.02.06	Client/Project	HAPWRAP / Sky Harbor ANJG		
HAPWRAP Contractor	IT Construction	Dr's Contractor	LYNNE ENGINEERING	Driller	DREARY LODGE
Drig Started	2/7/91	0830 A.M.	Drig Ended	2/7/91	1400 P.M.
Drig Method/Rig Type:		AIR Hammer Casing		Borehole dia(s)	9 3/4"
Logged by	Gardner	E-Log	(N)	From	to
				Protection Level	D(MODIFIED)

Depth (ft)	Sample No	Lab Anal (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows / 6 inch	Graphic Log	Well dia	Water depth	Remarks
70	0130			70% coarse, angular brown (F.S.Y.R 5/4), poorly sorted w/ minor silt fraction (reddish brown & gravel, 30%, med to coarse, rounded to angular, w/ minor cobbles, rounded, med. silty. <u>VERY MOIST</u>	SP	50				NA
75	0120			65% coarse to med, angular, brown (F.S.Y.R 5/4), poorly sorted w/ same silt & gravel, 30%, med to coarse, rounded to sub angular, & cobbles med to coarse, rounded. <u>VERY MOIST</u>	SP	50				Δ? WATER AT ~ 70 ft?
				<u>From Cyclone to T.D..</u>						
90				70% med to coarse, rounded to angular, some silt, w/ gravel, 30%, med to coarse, rounded to angular, & cobbles, rounded, coarse. FREE WATER	SP TO GP	-				FREE WATER AT ~ 86 ft.
100				SAND/WATER mixture of med to coarse, rounded to angular gravel, 35%, & med to coarse, rounded to sub rounded cobbles, 25%.	SP TO GP	-				
				T.D. : N/01 ft.						

□ = Thin wall Tube	□ = Rock Coring	NA	Field S/C (Make/Mod)	NA
○ = 3/4" spoon tuber	○ = Other	CA S	S/C Oper	NA
Notes	NA			

BORING LOG	BORING/WELL NO.: PP-01	Page 1 of 2
Installation: PAPAJO Military Reservation, Pinal Co, AZ	Site: PAPAJO	
Project No. 409221.02	Client/Project: HAZWRAP/SURFACE ANAL	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LORAIN Environmental	Driller: GARY LYONS
Drig Started: 1/19/91 ( ) m	Drig Ended: ( ) m	Borehole dia(s): 6" TO START 10" TO FINISH
Drig Method/Rig Type: AIR ROTARY HAMMER		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level D (REQUIRED)



U = Thin Wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	CA S	G/C Oper.:	NA
C = Cuttings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1996

BORING LOG	BORING/WELL NO. PP-01	Page 2 of 2
Installation: Sky Harbor	Coordinates:	Site: PAPAGO (SMP#5)
Project No. 40974-02.00	Client/Project: HAZWOP/Sky Harbor Arks	
HAZWOP Contractor: IT Corporation	Drill Contractor: Lowe Environmental	Driller: G. [unclear]
Drill Started: 1/20/91 (10 05 A.M.)	Drill Ended: 1/20/91 (11 30 P.M.)	Borehole dia(s): 10"
Drill Method/Rig Type: Air Rotary Hammer		
Logged by: G. [unclear]	E-Log (Y/N) (N)	From _____ to _____
		Protection Level: D (modified)

Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well dia	Water depth	Remarks
50				<p><u>50A.</u> Returns to Ground Red Brown Volcanic Rock (2.5 YR 5/4) w/ 2-5 mm Angular Breccia Fragments (10%)</p>						NA
60				<p><u>55A.</u> Ground Volcanic Rock, Very Dark Red (10 YR 3/6) w/ 2-5 mm Angular Breccia Fragments (10-15%)</p>						
65				<p><u>59A.</u> Ground Volcanic Rock, Red Brown (2.5 YR 4/4) w/ 2-5 mm Angular Breccia Fragments (10-15%) TD = 59' 4" TO BE FURTHER ADVANCED - 1/20/91</p>						
				<p><u>65A.</u> Red Brown Volcanic Rock with 2-10 mm Angular Volcanic Breccia Fragments (20-25%) TD = 65' 0"</p>						

U = Thin wall Tube	R = Rock Core	NA	Field G/C (Make/Mod.)	NA
S = Soil Spoon (Label)	O = Other	CA S	G/C Oper	NA
Notes	Notes	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO	PP-02	Page 1 of 1
Installation: Sky Harbor	Coordinates:	Site: PAPA (4)	
Project No. 40174.02	Client/Project:	HAZWRAP / Sky Harbor AVB	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LATWA	Driller: Gary Lyons	
Drig Started: 1/19/91 (0842 m)	Drig Ended: 1/19/91 (630 R m)	Borehole dia(s) 10"	
Drig Method/Rig Type: Air Rotary Hammer			
Logged by: Gordon	E-Log (Y/N) (Y)	From: _____ to: _____	Protection Level: D (Maximal)

Depth (ft) Sample No Sample Lab	Recovery (Y/N)	Lithologic Description	USCS	Blows / 6 inch Graphic Log	Well data	Water depth & Remarks
0		0-3 Gravel of some sand (U 10%). Coarse, angular, light reddish brown (5YR 6/4).	GP			1251.37
10		3-5 Gravel, w/ 20% sand, light brown (7.5YR 6/4).	GP			
20		10ft Calcic; yellow to buff w/ some quartzite & other angular pieces. Fine gravel with crushes.				
30		20ft Buff to gray, calcic or other powder: mix of small (1-3mm) angular fragments of basalt. (2.5Y 7/4) Some gravel - well rounded.				
40		30ft Stone buff ground rock. Hard (possibly not calcic). Suggests pink hue, (4.5YR 7/4). Small angular fragments				
50		31ft Thinly red. 40ft Ground volcanic rock, (5YR 6/4) Light reddish brown, softer at 30ft. Small angular 2-5mm basaltic fragments making water				Water at 38 to 40ft
60		50ft Ground volcanic rock reddish brown (2.5YR 5/4); small 2-5mm angular basaltic fragments (ca. 10%). 55ft Ground volcanic rock, reddish brown (2.5YR 5/4); w/ small 2-5mm angular basaltic fragments (ca. 10%). TD: 55ft.				

U = Thin wall tube	R = Rock Coring	NA	File # G/C (Make/Mod)	NA
S = Sp. (scoop tube)	O = Other	NA	G-C Oper.	NA
Q = Quilted	Notes	NA		

BORING LOG	BORING/WELL NO.: PP-3	Page 1 of 2
Installation: <del>SKY</del> PAPAGO MILITARY RESERVATION	Site: PAPAGO	
Project No.: 401821.02.01	Client/Project: MARTIN MARISTA / SKY HANGER BANG	
HAZWRAP Contractor: IT CORPORATION	Drig Contractor: LAYNE ENVIRONMENTAL	Driller: DWIGHT PERKINS
Drig Started: 1/17/91 (12:55 P.M.)	Drig Ended: 1/19/91 (07:30 A.M.)	Borehole dia(s): 10" 6 INCHES
Drig Method/Rig Type: AIR PERCUSSION / AIR ROTARY		
Logged by: GARDNER	E-Log (Y/N) From _____ to _____	Protection Level: D (MODIFIED)

Depth (ft)	Sample No	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth & Remarks	Etc.
0-10				0-10 ft: SAND, POORLY SORTED, POORLY GRADED w/ GRAND & FINES. HUE 7.5YR 6/3 LIGHT BROWN & DRY. AT 10ft IN VERY FINE POWDERED ROCK - PROBABLY CALICHE. - FROM SIX FEET ON. 5YR	SP					1239.72
10-20				10ft: CALICHE. (FINE POWDER & COARSE FRAGMENTS - WHITE TO BUFF, IN ON CRYSTALLINE) 10-20ft. (N 12-14ft - WTD SAND & GRAVEL; 10ft: WTD FINE GRAINED SAND w/ SMALL GRAVEL, DARK REDDISH BROWN, 2.5 YR 3/3						
20-30				RUN IN w/ ROTARY RIG: 1/19/91/0845 VOLCANIC ISRAELI - RED BROWN (2.5YR 4/4); <del>GRAVEL</del> <del>FROM</del> <del>SUMMIT</del> GRAVEL COMPONENTS ARE MOSTLY QUARTZITE.						
30-40				SUGGY DARKER - VERY SLIGHTLY MIXED						
40-50				40ft RED BROWN (2.5YR 4/4) VOLCANIC ISRAELI w/ 2-5mm SIZED QUARTZITE & OTHER BRICKS CUTS.						
50-55				55ft: RED BROWN (2.5YR 4/4) VOLCANIC ISRAELI w/ 2-5mm SIZED QUARTZITE & OTHER BRICKS CUTS. SAMPLE AT 54-55ft						
				<del>FD = 55 ft. 3 inches</del>						

U = Thin Wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split spoon (tube)	O = Other	ST-2-91 NA CAS	G/C Oper.:	NA
C = Cuttings	Notes:	NA		

FIGURE 5-3a

REV DATE MAY 1990

BORING LOG	BORING/WELL NO. PP-03	Page 2 of 2
Installation: Sky Harbor	Coordinates:	Site: Papeete
Project No.: 409721	Client/Project: Martin Marietta / Sky Harbor ANG	
HAZWRAP Contractor: IT Corp	Drig Contractor: Layne Env.	Driller: Dwight Peterson
Drig Started: See 1 of 2 ( ___ m)	Drig Ended: See 1 of 2 ( ___ m)	Borehole dia(s):
Drig Method/Rig Type: See 1 of 2		
Logged by: Gardner	E-Log (Y/N) (N)	From ___ to ___ Protection Level: D (Mod. Fed)

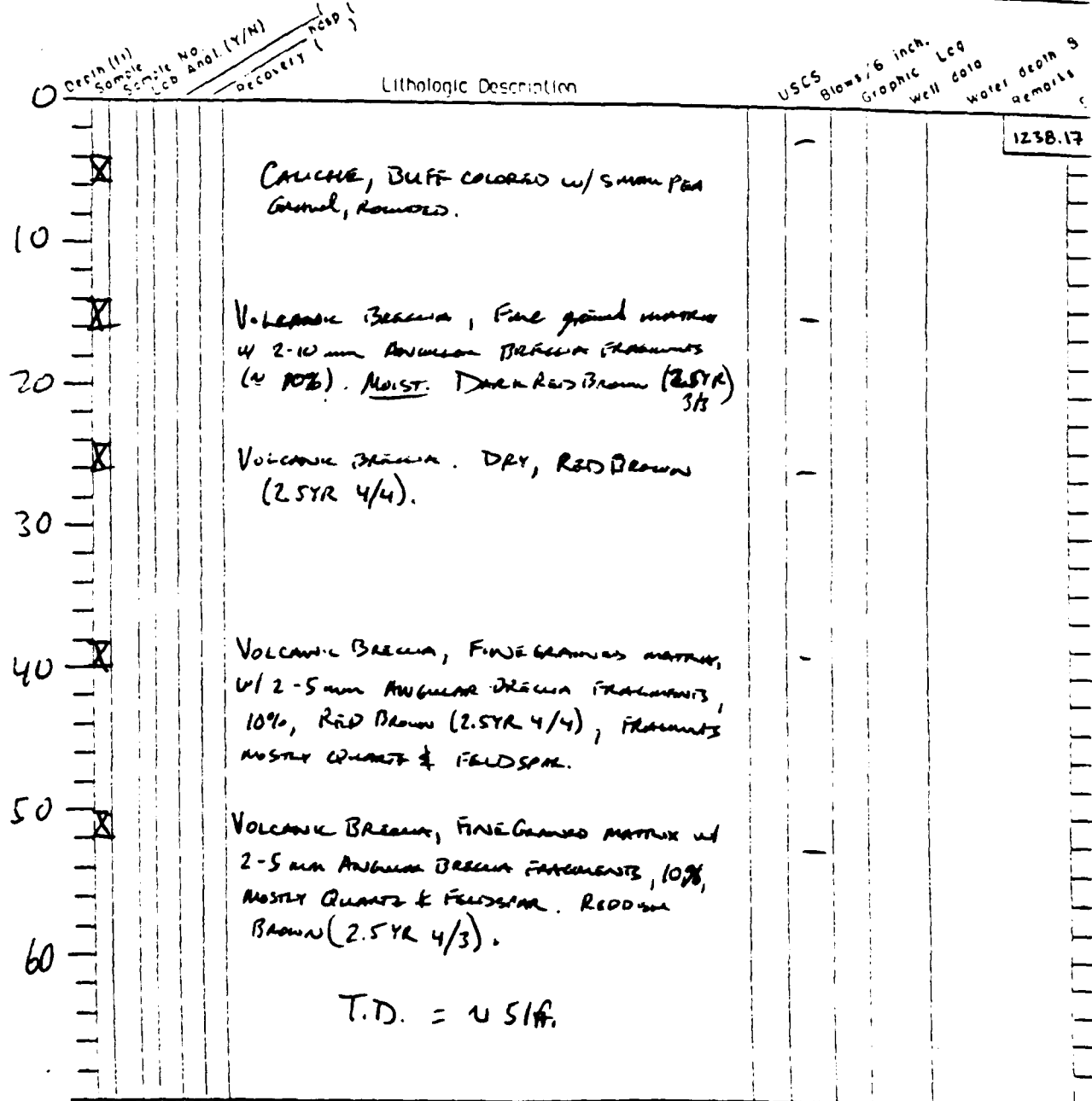
Depth (ft)	Sample No.	Lab Anal. (Y/N)	Recovery (%)	Lithologic Description	USCS	Blows/6 inch.	Graphic Log	Well data	Water depth	Remarks	
50				CONTINUE FROM 55 ft. CUTTINGS coming down from wire hole. No evidence of TRACONS BIT.						NA	
60				RED BROWN Ground Volcanic Rock (2.5R 4/4), w/ small 2-5 mm Angular BRACIA FRAGMENTS. MOIST							
70				RED BROWN Ground Volcanic Rock (2.5R 4/4) w/ small 2-5 mm Angular BRACIA FRAGMENTS. DRY.							
				TD = <del>70</del> <sup>71.2</sup> ft. 71 ft. 8 in. <sup>23</sup> / <sub>6</sub>							

J = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Soil spoon (tube)	O = Other	NA	G/C Oper.	NA
C = Casing	Notes	NA		

FIGURE S-32

REV. DATE MAY 1996

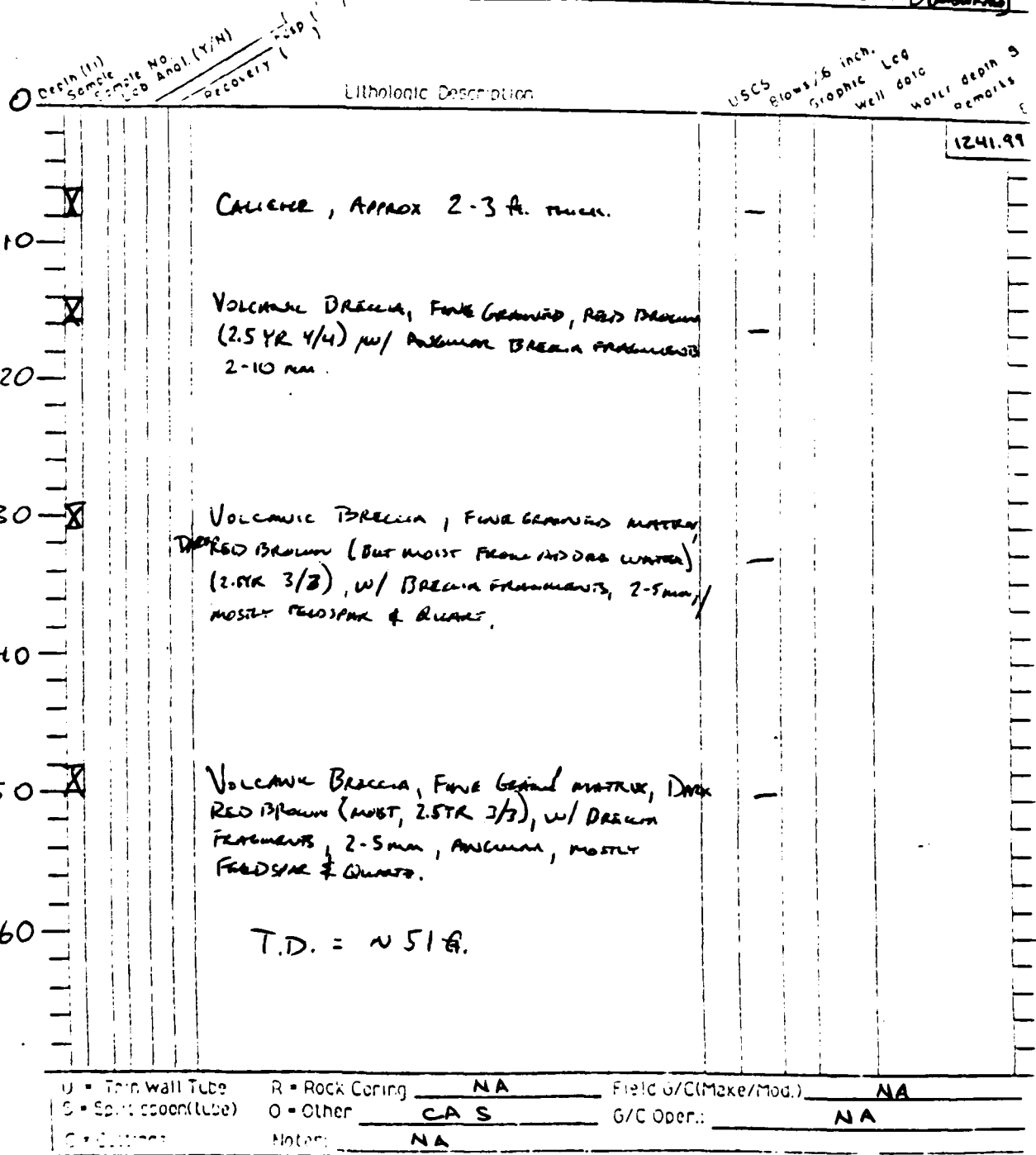
BORING LOG	BORING/WELL ID	MW 4-01	REV. DATE	MAY 1996
Project No.	Client/Project	HAZWRAP / Sky Harbor Arty	Sheet	4 (Pages)
HAZWRAP Contractor	Drill Contractor	LORRAE ENVIRONMENTAL	Driller	GARY LYONS
Drill Started	43:15 P.M.	Drill Ended	2/1/91	(15:30 P.M.) Borehole dia(s)
Drill Method/Rig Type:	AIR ROTARY HAMMER CASING			
Logged by:	GARDIN	E-Log (Y/N)	From	to
			Protection Level	D (Medium)



U = Thin wall Tube	R = Rock Coring	NA	Field G/C (Make/Mod.)	NA
S = Split count (tube)	O = Other	CAS	G/C Oper.:	NA
C = Castings	Notes:	NA		



BOHINC LOG	BOHINC/WELL NO	MUY-02		Page	1 of 1
Project No	40921.02.06	Client/Project	HAZWRAP / SET HAZWRAP AN4		
HAZWRAP Contractor	IT Corporation	Drill Contractor	Lowell Environmental	Driller	Gary Lyons
Drill Started	2/1/91 01:00 AM	Drill Ended	2/1/91 12:00 PM	Borehole dia(s)	10"
Drill Method/Rig Type	Air Rotary Hammer Core				
Logged by	Gardner	E-Log (Y/N)	(Y)	from	to
				Protection Level	D (unknown)



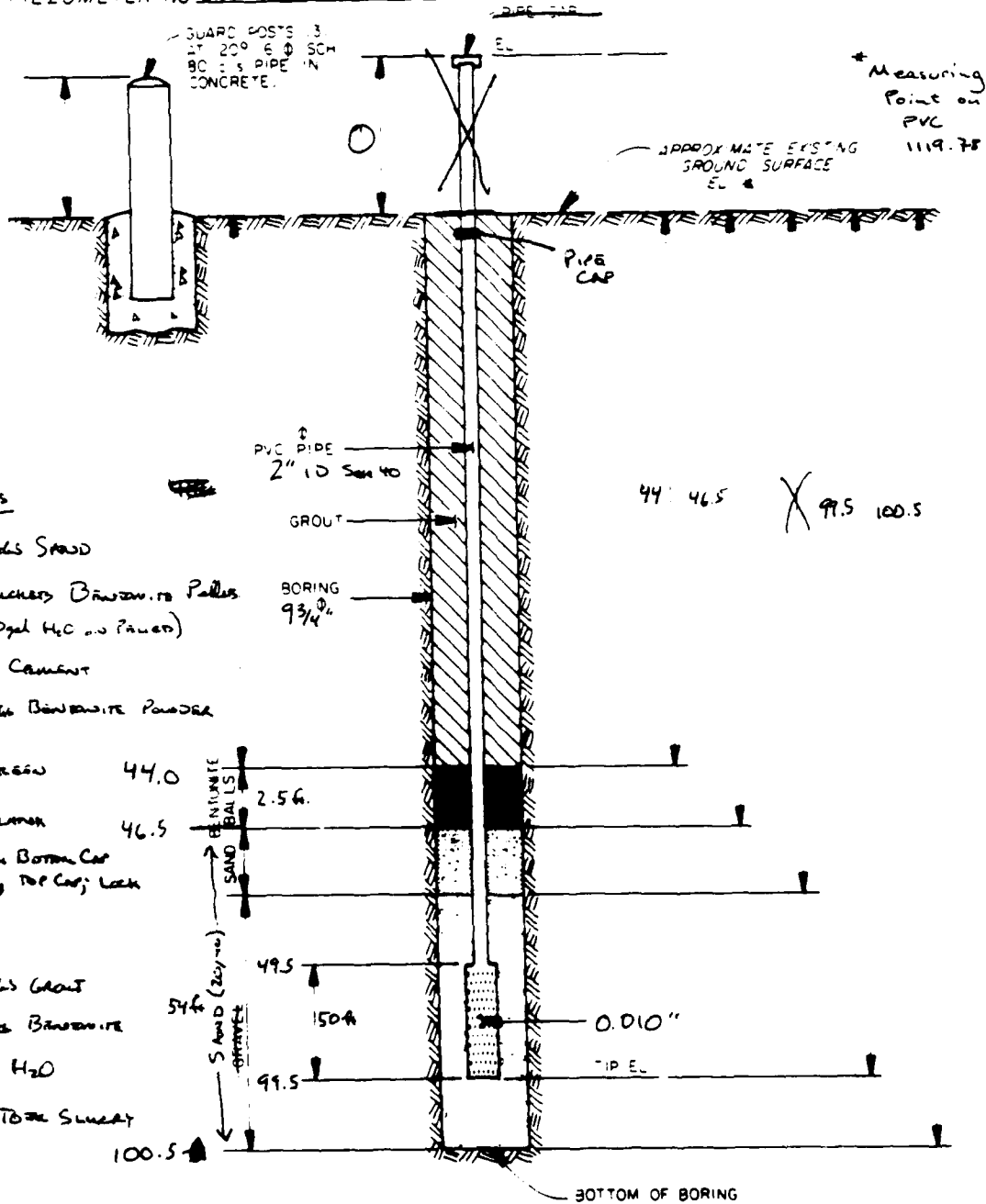
**APPENDIX F**

**PIEZOMETER AND MONITORING WELL  
COMPLETION DIAGRAMS**



# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME Sky Harbor A-16 INSTALLED BY Gardner DATE 1/15/91  
 PROJECT NO 409721.02.06 CHECKED BY NA DATE NA  
 BORING NO NA  
 PIEZOMETER NO SH #1 (PS-1)



### Materials

24 1/2 BAGS SAND

1 1/2 Buckets Bentonite Pills (10 gal H<sub>2</sub>O in Pail)

15 BAGS CEMENT

1 1/2 BAGS BLENDED POWDER

50 ft Screen 44.0

50 ft. Blower 46.5

1 3-inch Bottom Cap  
1 Locking Top Cap; Lock

### Summary

N 4 BAGS GROUT

N 1/3 BAGS BLENDED

N 40 gal H<sub>2</sub>O

180 gal TOP SOIL

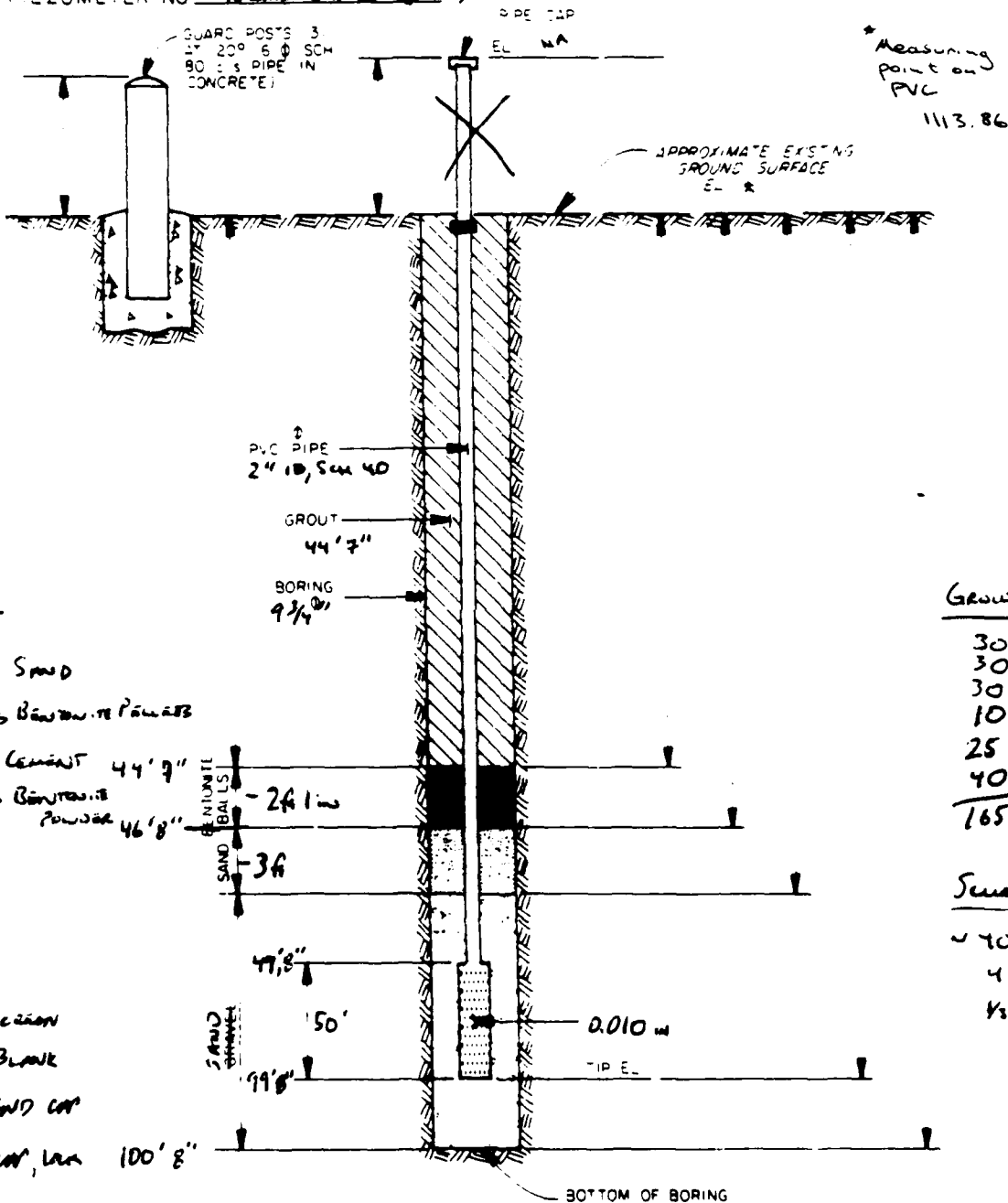
100.5'

NOT TO SCALE



# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME SH ANJG INSTALLED BY GARDNER DATE 1/16/91  
 PROJECT NO 409721.02.06 CHECKED BY NA DATE NA  
 BORING NO SH P-2  
 PIEZOMETER NO PIEZOMETER # 2 (PS-2)



### MATERIALS

- 2 1/2 Bags Sand
- 1 1/2 Bags Bentonite Powder
- 12 Bags Cement 44' 9"
- 1 1/2 Bags Bentonite Powder 46' 8"

### CASING

- 50 ft Section
- 50 ft. Blank
- 1 - 4 in END CAP
- 1 - TOP CAP, Len 100' 8"

Grout	Len
30	
30	
30	
10	
25	
40	
<hr/>	
165	gal

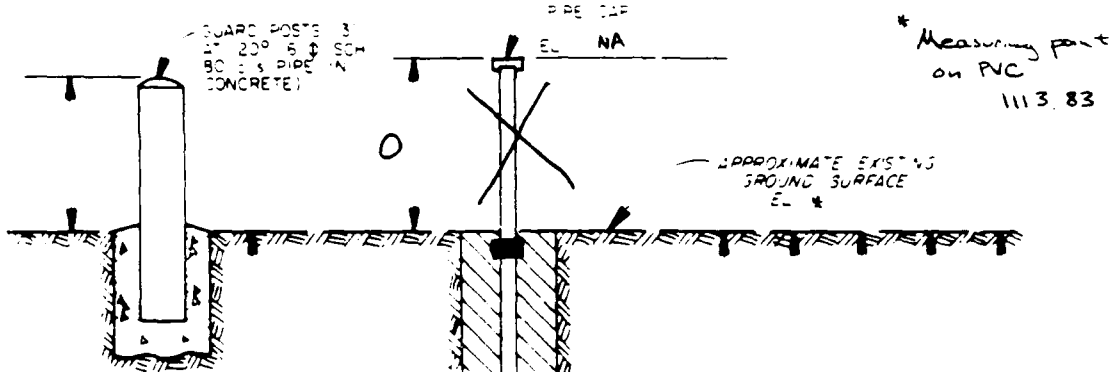
### Summary

~ 70 gal  
 40 gal  
 1/2 gal



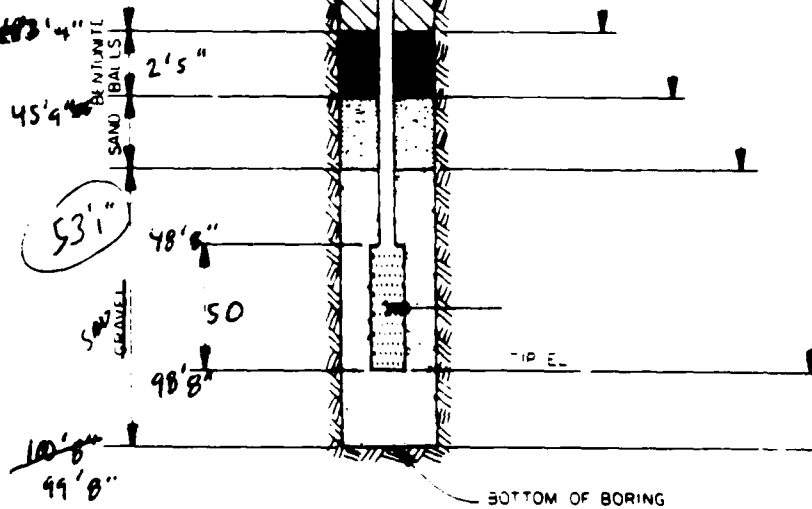
# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME Sky Harbor ANG INSTALLED BY Greenlee DATE 1/16/91/11/91  
 PROJECT NO 401721.0206 CHECKED BY MA DATE MA  
 BORING NO PS-3  
 PIEZOMETER NO #3



### MATERIALS

SAND. 23 1/2 bags  
 Bentonite: 2 Bags  
 Water: 10 gal  
 33 # Bags Cement  
 4 # Bags Bentonite



Top of  
 Pipe in  
 morning.  
 42' 2"

(Soil:  
 Swelling?)

### Summary Vol

30
30
30
35
30
30
35
35
35
<u>290</u>
+ 40 gal H <sub>2</sub> O
320
4.5 gal Cement
1/2" Bentonite

### Casing

50ft. Screen  
 50ft. Blank  
 1- 4 in FWD CAT  
 1- 1 Long TO CAT, LOCK

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: <u>MWS-01</u>	Installation: <u>SKY HARDEN Borehole Wash</u>	Site: <u>Brockton, MA 01929</u>
Project No.: <u>40924</u>	Client/Project: <u>HAZWRAP / SKY HARDEN AN16</u>	
HAZWRAP Contractor: <u>TCI</u>	Drig Contractor: <u>WALSH ENVIRONMENTAL</u>	
Comp. Start: <u>1/20/91</u> ( <u>09:00</u> A.M.)	Comp. End: <u>1/20/91</u> ( <u>11:50</u> A.M.)	
Built By: <u>GARDNER</u>	Well Coord.: <u>N 9484.29</u> <u>E 11768.37</u>	

Elev. 1118.70  
 Height 0  
 GS Elev. 1118.70  
 GS Height 0.00'  
 Depth BGS \_\_\_\_\_

Elev. 1118.40  
 Depth BGS 0.3

Gravel Screen

40  
 20  
 20  
 20  
 20  
 20  
 140pl

Base course: 20  
 " Basecourse: 2  
 " Basecourse: 1

44.5  
 46.5  
 50.0

54.5

55.0

100'

101'

NA

TD: 101'

9 3/4

Borehole dia.

**PROTECTIVE CSG**

Material / Type STEEL TUB W/ SWEET METAL JOINTS  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_  
 Watertight O-Ring (Y/N) \_\_\_\_\_

**SURFACE PAD**

Composition & Size CONCRETE / 36" x 36" x 12"  
 Breathes With Vadose Zone (Y/N) (N)

**RISER PIPE**

Type SMOOTH WALL PVC  
 Diameter 4" MIN. I.D.  
 Total Length (TOC to TOS) \_\_\_\_\_  
 Ventilated Cap (Y/N) (N)

**GROUT**

Composition & Proportions 7 Parts Type I Portland Cement + 1 Part Bentonite Grout + 35-40pl H<sub>2</sub>O  
 Tremied (Y/N) \_\_\_\_\_  
 Interval BGS \_\_\_\_\_

**CENTRALIZERS (Y/N)**

Depth(s) \_\_\_\_\_

**SEAL**

Type 1/4" thick Urethane Bitumen with Fibers  
 Source \_\_\_\_\_  
 Setup/Hydration time 15 min. Vol. Fluid Added 10pl H<sub>2</sub>O  
 Tremied (Y/N) (N) 20

**FILTER PACK**

Type 20/40 Crushed Screen Wash / 60 Silicon Sand  
 Amt. Used 19 1/2 bags, 1/2 bag  
 Tremied (Y/N) \_\_\_\_\_  
 Source \_\_\_\_\_  
 Gr. Size Dist. 20/40 for filter pack + 60 for sand

**SCREEN**

Type Smooth Wall 4" PVC  
 Diameter 4" MIN. I.D.  
 Slot Size & Type 1/2" I.D.  
 Interval BGS \_\_\_\_\_

**SUMP (Y/N)**

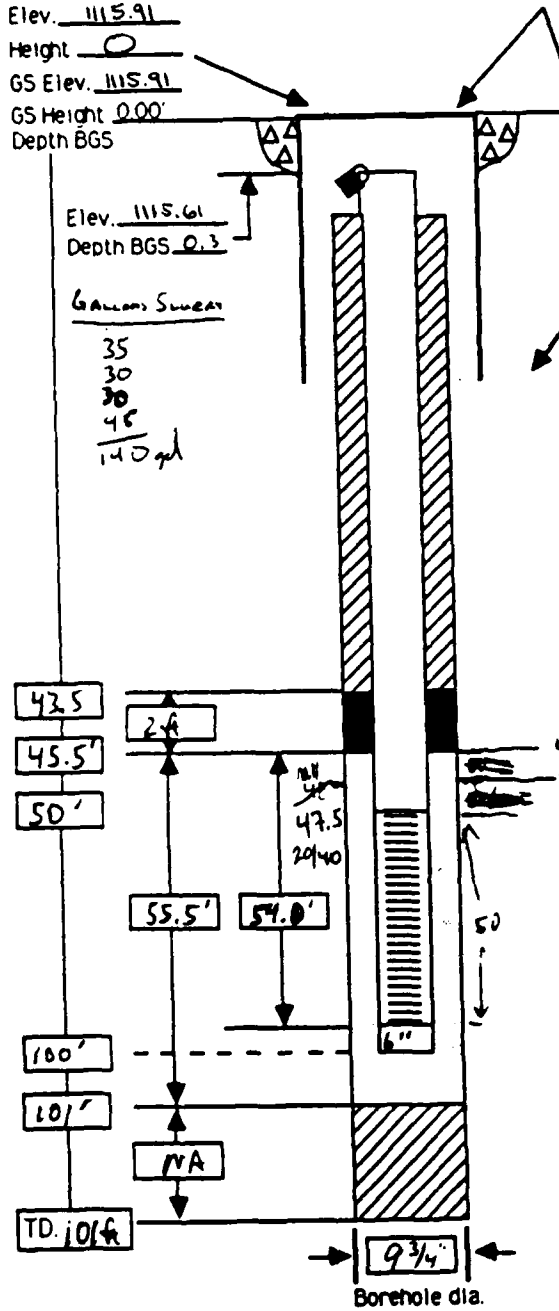
Interval BSG \_\_\_\_\_ Length \_\_\_\_\_  
 Bottom Cap (Y/N) (N)

**BACKFILL PLUG**

Material NA  
 Setup/Hydration time NA  
 Tremied (Y/N) (N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: <u>MUS-02</u>	Installation: <u>SKY HARBOR</u>	Site: <u>BALTIMORE WELLS</u>
Project No.: <u>HAZWRAP</u>	Client/Project: <u>HAZWRAP/SKY HARBOR AKA</u>	
HAZWRAP Contractor: <u>TP CORPORATION</u>	Drig Contractor: <u>LATAGE ENVIRONMENTAL</u>	
Comp. Start: <u>2/6/91</u> (08:05 A.m)	Comp. End: <u>2/6/91</u> (10:00 A.m)	
Built By: <u>GARDNER</u>	Well Coord.: N 8941.36 E 10847.55	



**PROTECTIVE CSG**  
Material / Type STEEL TOP / SWEET METAL BOTTOM  
Diameter \_\_\_\_\_  
Depth BGS \_\_\_\_\_  
Watertight O-Ring (Y/N) JT 2-4-91

**SURFACE PAD**  
Composition & Size 3 ft. x 3 ft. x 1 ft. CONCRETE  
Breathes With Vadose Zone (Y/N)

**RISER PIPE**  
Type SCH. 40 PVC  
Diameter 4 inch I.D.  
Total Length (TOC to TOS) 50 ft.  
Ventilated Cap (Y/N)

**GROUT**  
Composition & Proportions 4 BAGS TYPE I/II CEMENT  
TO 1/2 BAG BENTONITE + ~ 25-40 GAL H<sub>2</sub>O  
Tremied (Y/N) 15 SX CEMENT, 1 SX BENTONITE  
Interval BGS \_\_\_\_\_

**CENTRALIZERS** (Y/N) NA  
Depth(s) \_\_\_\_\_

**SEAL**  
Type 1/4" WYMON BENTONITE PELLETS 1 BAG  
Source \_\_\_\_\_  
Setup/Hydration time 20 min Vol. Fluid Added 10 gal  
Tremied (Y/N)

**FILTER PACK**  
Type 20/40 CRUSHED SILICA SAND + 60 GRAMS BENTONITE  
Amt. Used 10 SX 20/40; 1/2 SX 60  
Tremied (Y/N)  
Source \_\_\_\_\_  
Gr. Size Dist. 20/40 FILTER PACK; 60 GRS TOP.

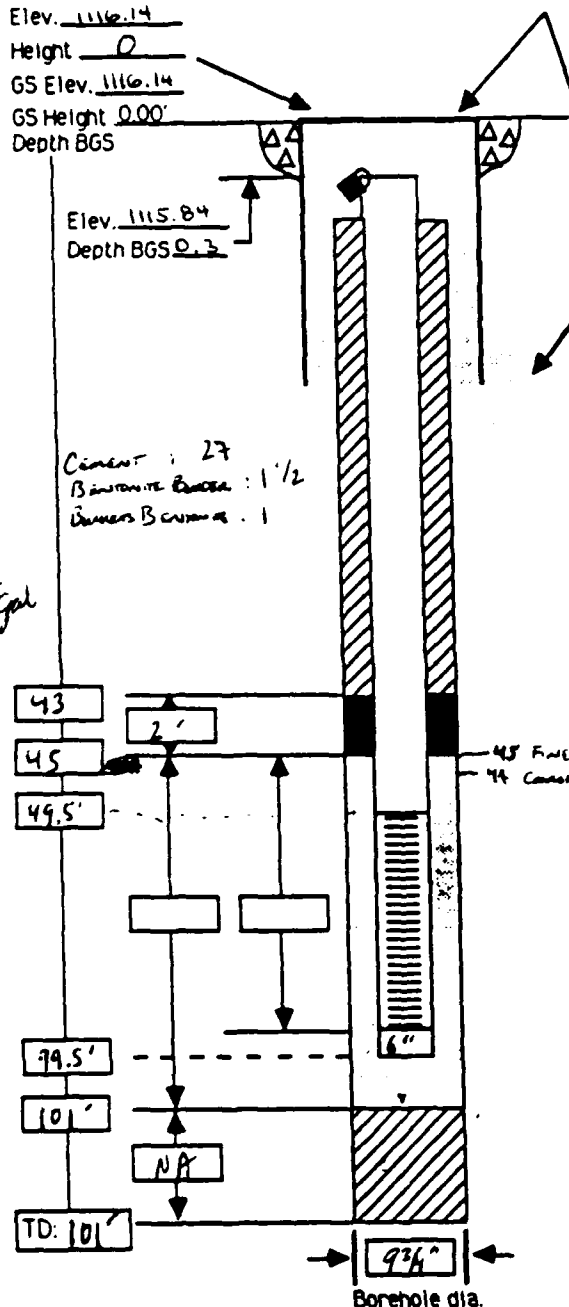
**SCREEN**  
Type SCH. 40 PVC  
Diameter 4 inch I.D.  
Slot Size & Type 0.010 mm  
Interval BGS 450-100 ft.

**SLUMP** (Y/N)  
Interval BGS \_\_\_\_\_ Length 2 ft.  
Bottom Cap (Y/N)

**BACKFILL PLUG**  
Material NA  
Setup/Hydration time NA  
Tremied (Y/N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: <u>MW-03</u>	Installation: <u>Sky Harbor</u>	Site: <u>Green Canyon Well</u>
Project No.: <u>40121-02</u>	Client/Project: <u>HAZWRAP / Sky Harbor AWW</u>	
HAZWRAP Contractor: <u>IT Corporation</u>	Drig Contractor: <u>Layne Env. Construction</u>	
Comp. Start: <u>11/3/91</u> ( <u>10:25 A.M.</u> )	Comp. End: <u>1/7/91</u> ( <u>13:20 P.M.</u> )	
Built By: <u>GARDNER</u>	Well Coord.: <u>N 8620.48</u> <u>E 10430.88</u>	



**PROTECTIVE CSG**  
 Material / Type STEEL TP, SMOOTH METAL SIDING  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_  
 Watertight O-Ring  (Y) /  (N)

**SURFACE PAD**  
 Composition & Size 3' x 3' x 1 1/2' CONCRETE  
 Breathes With Vadose Zone  (Y) /  (N)

**RISER PIPE**  
 Type SCHEDULE 40 PVC  
 Diameter 4 INCH I.D.  
 Total Length (TOC TO TOS) \_\_\_\_\_  
 Ventilated Cap  (Y) /  (N)

**GROUT**  
 Composition & Proportions 4 Bags Type I-III PORTLAND + 1/2 BAG BINDERITE + 2 3/4 WGT H<sub>2</sub>O  
 Tremied  (Y) /  (N)  
 Interval BGS \_\_\_\_\_

**CENTRALIZERS**  (Y) /  (N)  
 Depth(s) \_\_\_\_\_

**SEAL**  
 Type 4 1/2" W. BINDERITE PLUG  
 Source \_\_\_\_\_  
 Setup/Hydration time 20 MIN. Vol. Fluid Added 10 GAL H<sub>2</sub>O  
 Tremied  (Y) /  (N) 40

**FILTER PACK**  
 Type 20/40 COARSE SILICA SAND; 60 MESH  
 Amt. Used 22 2/3 GAL, 1/2 LB  
 Tremied  (Y) /  (N)  
 Source \_\_\_\_\_  
 Gr. Size Dist. 20/40 COARSE SILICA SAND, 60 MESH

**SCREEN**  
 Type SCHEDULE 40 PVC  
 Diameter 4 INCH I.D.  
 Slot Size & Type 0.010 MESH  
 Interval BGS \_\_\_\_\_

**SUMP**  (Y) /  (N)  
 Interval BSG NA Length NA  
 Bottom Cap  (Y) /  (N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied  (Y) /  (N)

Cement Slurry  
 40  
 35  
 35  
 30  
 30  
 20  
 10  
 23.5 gal

Cement: 27  
 Binderite Binder: 1 1/2  
 Baggers Binderite: 1

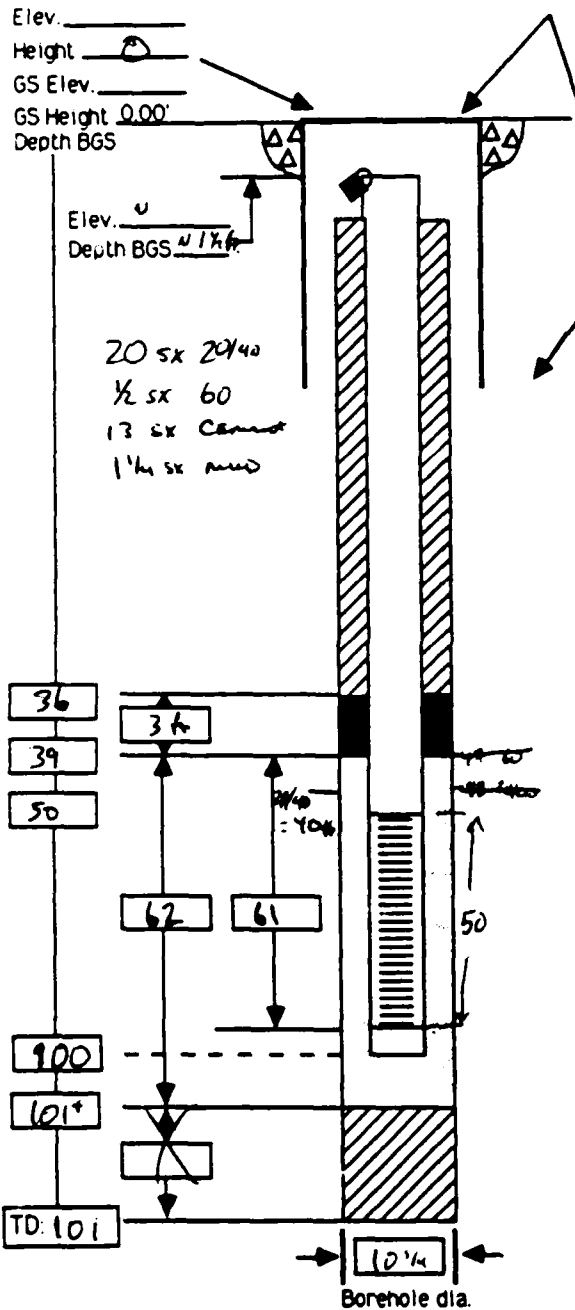
43  
 45  
 49.5'  
 79.5'  
 101'  
 TD: 101'  
 2'  
 4 1/2" FINE  
 4" COARSE  
 6"  
 9 3/4" Borehole dia.



REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount

WELL NO.: MWS-04	Installation: Sky Harbor ANK Base	Site: Back Ground Well
Project No.: 40721	Client/Project: HAZWRAP/Sky Harbor ANK	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	
Comp. Start: 3/21/91 (2:25 P.M.)	Comp. End: 3/21/91 (4:30 P.M.)	
Built By: GARDINER	Well Coord.: _____	



**PROTECTIVE CSG**  
 Material / Type STEEL TOP, ALUMINUM BOTTOM  
 Diameter 12"  
 Depth BGS 1 ft  
 Watertight O-Ring (Y) N

**SURFACE PAD**  
 Composition & Size FLUID RESISTANT ASPHALT  
 Breathes with Vadose Zone (Y/N)

**RISER PIPE**  
 Type SCHEDULE 40 PVC  
 Diameter 4 in. I.D.  
 Total Length (TOC to TOS) 50'  
 Ventilated Cap (Y) (N)

**GROUT**  
 Composition & Proportions 5% BENTONITE / TYPE III PORTLAND CEMENT GROUT  
 Tremied (Y) (N)  
 Interval BGS 0-36 ft.

**CENTRALIZERS** (Y) (N)  
 Depth(s) \_\_\_\_\_

**SEAL**  
 Type 1/4" WRAYM BENTONITE PUTTY  
 Source ENVIRONMENTAL  
 Setup/Hydration time 10 min. Vol. Fluid Added 1 qt  
 Tremied (Y) (N)

**FILTER PACK**  
 Type 20/40 COARSE SILVER SAND / 60 MESH  
 Amt. Used \_\_\_\_\_  
 Tremied (Y) (N)  
 Source \_\_\_\_\_  
 Gr. Size Dist. 20/40 P.S., 60 MESH

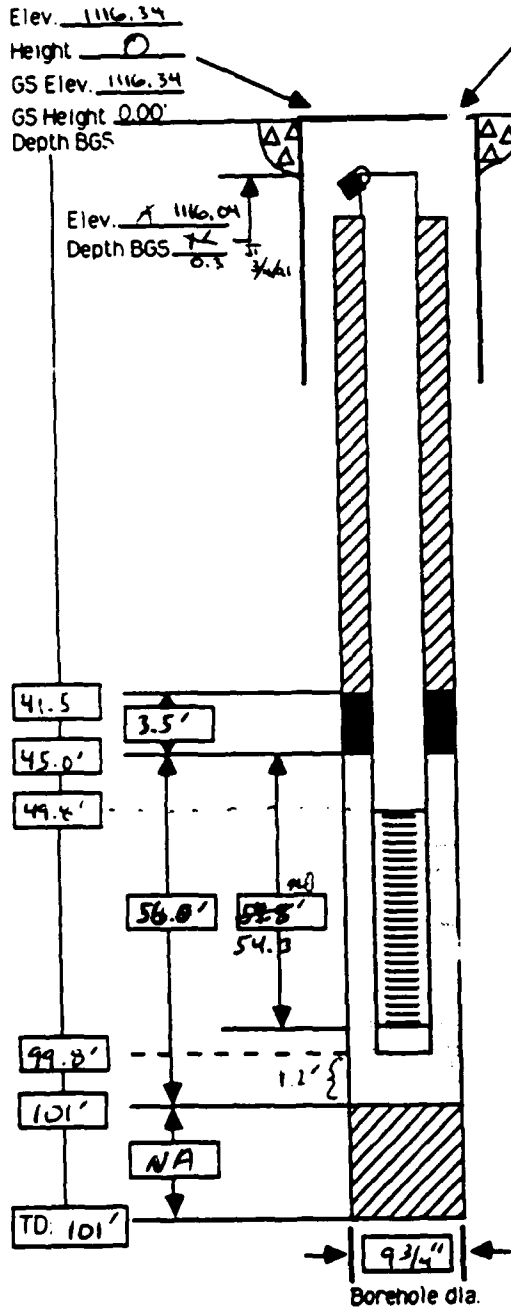
**SCREEN**  
 Type SCHEDULE 40 PVC  
 Diameter 4 in. I.D.  
 Slot Size & Type 0.010 in  
 Interval BGS 50-100

**SUMP** (Y) (N)  
 Interval BGS 100-101 ft. Length 1 ft.  
 Bottom Cap (Y) (N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y) (N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: MW1-02	Installation: Sky Harbor	Site: 1
Project No.: 01231	Client/Project: HAZWRAP / Sky Harbor Air	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE ENVIRONMENTAL	
Comp. Start: 1/29/91 (12:45 P.M.)	Comp. End: 1/29/91 (15:00 P.M.)	
Built By: GARDNER	Well Coord.: N 992.28 E 10606.30	



**PROTECTIVE CSG**  
Material / Type: STEEL TOP, SHEET PILING SIDES  
Diameter: \_\_\_\_\_  
Depth BGS: \_\_\_\_\_  
Watertight O-Ring: (Y/N)

**SURFACE PAD**  
Composition & Size: CONCRETE / 3' x 3'  
Breathes With Vadose Zone: (Y/N)

**RISER PIPE**  
Type: SCHEDULE 40 PVC  
Diameter: 4 INCH I.D.  
Total Length (TOC to TOS): 49'  
Ventilated Cap: (Y/N)

**GROUT**  
Composition & Proportions: Approx 4 parts Type I & II Cement + 1/2 Bag Bentonite per 100 lbs 95-400# H<sub>2</sub>O  
Tremied: (Y/N)  
Interval BGS: \_\_\_\_\_

**CENTRALIZERS** (Y/N)  
Depth(s): \_\_\_\_\_

**SEAL**  
Type: 1/4" WYOMING GASTROITE PELLETS  
Source: \_\_\_\_\_  
Setup/Hydration time: 15 min Vol Fluid Added 10 gal  
Tremied: (Y/N)

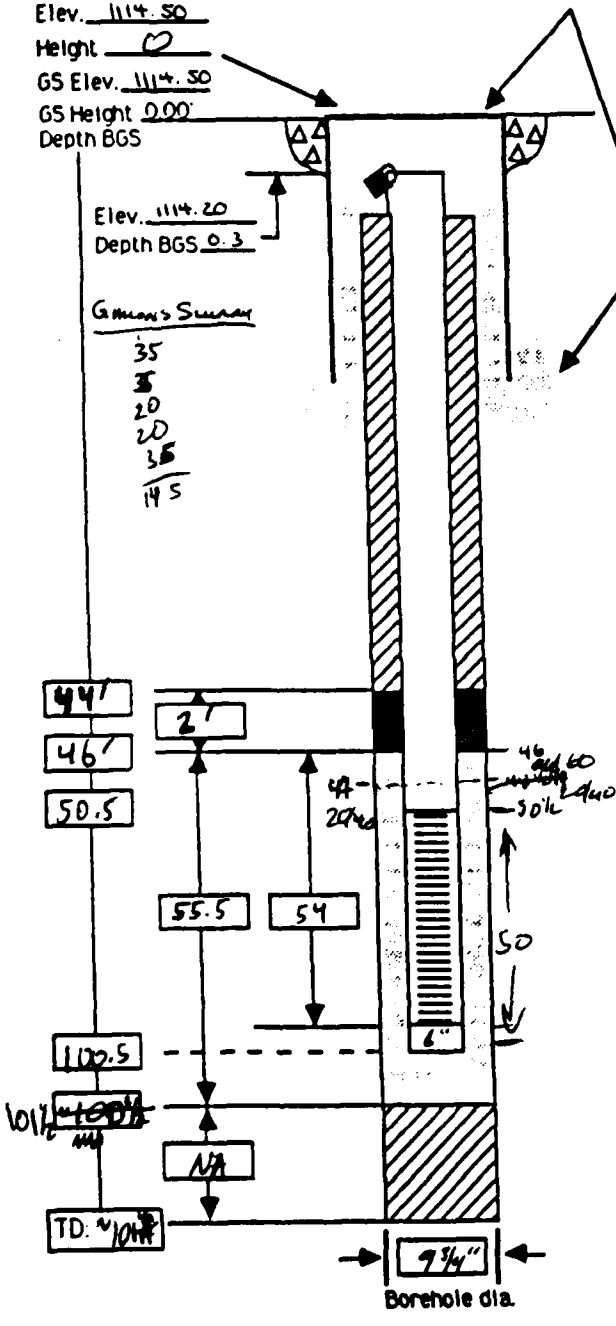
**FILTER PACK**  
Type: 20/40 COLORADO SILICA SAND  
Amt. Used: 19 1/2 BAGS 20/40 + 1/2 BAG 60  
Tremied: (Y/N)  
Source: \_\_\_\_\_  
Gr. Size Dist.: 20/40 FOR SAND PACK, 60 FOR TD OF PACK (44)

**SCREEN**  
Type: SCHEDULE 40 PVC  
Diameter: 4 INCH I.D.  
Slot Size & Type: 0.010  
Interval BGS: 50' of SCREEN

**SUMP** (Y/N)  
Interval BSG: \_\_\_\_\_ Length: \_\_\_\_\_  
Bottom Cap: (Y/N)

**BACKFILL PLUG**  
Material: NA  
Setup/Hydration time: NA  
Tremied: (Y/N)

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL ID: MW2-02	Installation: Sky Harbor	Site: 2
Project No: <del>W1722</del>	Client/Project: HAZWRAP / Sky Harbor A116	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LORIAN Environmental	
Comp. Start: 2/6/91 (14:50 P.M.)	Comp. End: 2/6/91 (16:20 P.M.)	
Built By: Gardner	Well Coord.: N 9801.70 E 10386.43	



**PROTECTIVE CSG**  
 Material / Type Steel Top / Sheet Metal Bottom  
 Diameter 4" I.D.  
 Depth BGS 3-4'  
 Watertight O-Ring (Y) (N) 3-4'

**SURFACE PAD**  
 Composition & Size 3 ft x 3 ft x 1 ft Concrete  
 Breathes With Vadose Zone (Y / N)

**RISER PIPE**  
 Type Sch. 40 PVC  
 Diameter 4" I.D.  
 Total Length (TOC to TOS) 50'  
 Ventilated Cap (Y) (N)

**GROUT**  
 Composition & Proportions 4 Bags Type III Cement, 1/2 Bag Bentonite per Sack + 2.75' 40# H<sub>2</sub>O  
 Tremied (Y) (N)  
 Interval BGS 2.75'

**CENTRALIZERS** (Y) (N)  
 Depth(s)

**SEAL**  
 Type 1/4" Dimpled Rings  
 Source   
 Setup/Hydration time  Vol. Fluid Added 12 gal 420  
 Tremied (Y) (N)

**FILTER PACK**  
 Type 20/40 Concrete Screen Sand + 60 Gravel  
 Amt. Used 19 Bags 20/40, 1/2 Sack 60  
 Tremied (Y) (N)  
 Source   
 Gr. Size Dist. 20/40 Filter Pack + 1/2 60 on top

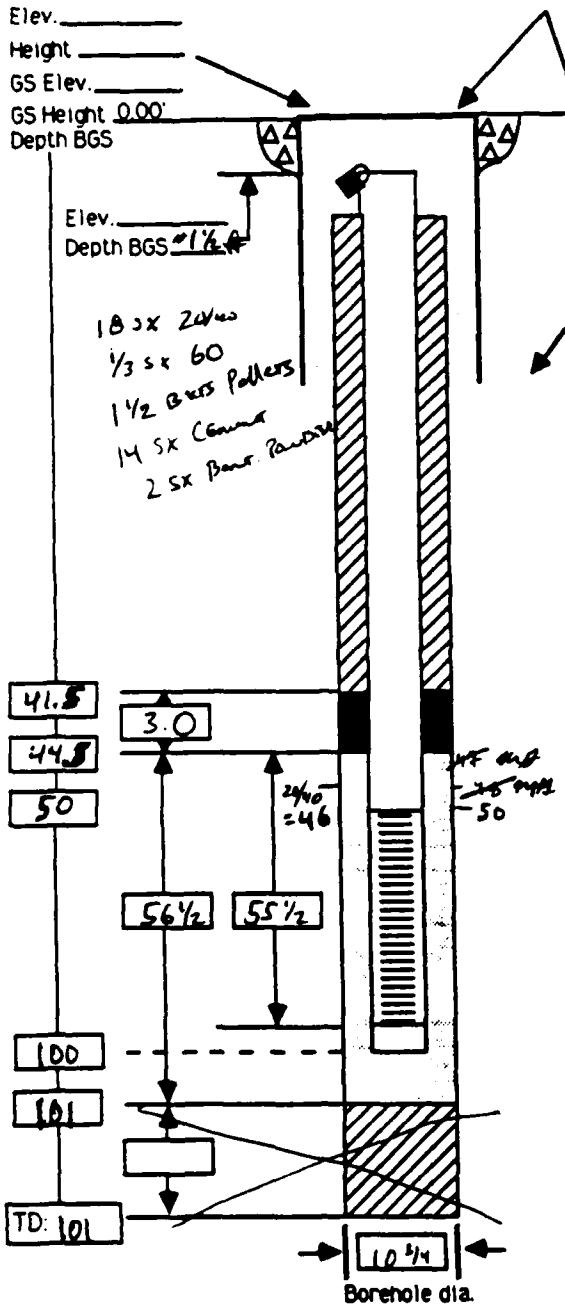
**SCREEN**  
 Type Sch. 40 PVC  
 Diameter 4" I.D.  
 Slot Size & Type 0.010" 50'  
 Interval BGS 50'

**SUMP** (Y) (N)  
 Interval BGS 100 1/2" to 101 1/2" Length  
 Bottom Cap (Y) (N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y) (N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG - Standard Flush Mount		
WELL NO.: MW3-01	Installation: Sky Harbor ANV Base	Site: 3
Project No.: 40182	Client/Project: HAZWRAP / Sky Harbor ANV	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAYNE Environmental	
Comp. Start: 3/22/91 (12:45 PM)	Comp. End: 3/22/91 (15:10 PM)	
Built By: GARDNER	Well Coord.: _____	



**PROTECTIVE CSG**  
 Material / Type STEEL TOP, ANNULAR BOTTOM  
 Diameter 12"  
 Depth BGS 0-1 1/2'  
 Watertight O-Ring (Y/N)

**SURFACE PAD**  
 Composition & Size CONCRETE UNDER ASPHALT  
 Breathes With Vadose Zone (Y/N)

**RISER PIPE**  
 Type SCHEDULE 40 PVC  
 Diameter 4" INCH ID  
 Total Length (TOC to TOS) 50 FT.  
 Ventilated Cap (Y/N)

**GROUT**  
 Composition & Proportions 5% BENTONITE/TREMIE  
PARTIAL CEMENT GROUT  
 Tremied (Y/N)  
 Interval BGS 0-41 1/2'

**CENTRALIZERS** (Y/N)  
 Depth(s) \_\_\_\_\_

**SEAL**  
 Type 3/4" WRAPPING BANDSAID PAPER  
 Source FADV. CO. INC.  
 Setup/Hydration time 20 Days Vol. Fluid Added 1 Gal  
 Tremied (Y/N) H<sub>2</sub>O

**FILTER PACK**  
 Type 20/40 COARSE SILICA SAND, 60 GLASS  
 Amt. Used 18 SX  
 Tremied (Y/N)  
 Source Colorado Silica Sand  
 Gr. Size Dist. 20/40 Mesh, 60 on top

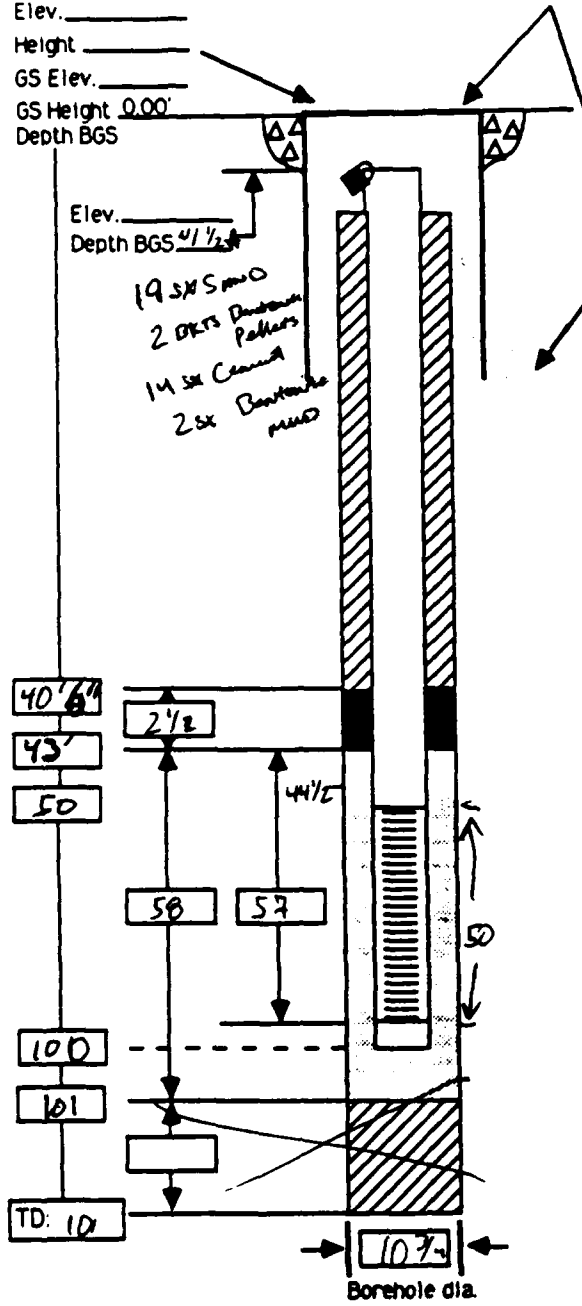
**SCREEN**  
 Type SCHEDULE 40 PVC  
 Diameter 4" INCH ID  
 Slot Size & Type 0.010  
 Interval BGS 50-100'

**SUMP** (Y/N)  
 Interval BGS 100-101' Length 1'  
 Bottom Cap (Y/N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y/N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: MW3-02	Installation: Sky Harbor Air Base	Site: 3
Project No.: 40831	Client/Project: HAZWRAP / Sky Harbor Air Base	
HAZWRAP Contractor: IT Corporation	Drig Contractor: LAMAR Environmental Services	
Comp. Start: 3/23/91 (1:45 P.M.)	Comp. End: 3/23/91 (4:30 P.M.)	
Built By: GARDIN	Well Coord.: _____	



**PROTECTIVE CSG**  
 Material / Type Steel Top / Aluminum Bottom  
 Diameter 12"  
 Depth BGS 0-1 1/2'  
 Watertight O-Ring (Y) (N)

**SURFACE PAD**  
 Composition & Size 3x3x1 Concrete  
 Breathes With Vadose Zone (Y) (N)

**RISER PIPE**  
 Type Schedule 40 PVC  
 Diameter 4" in ID  
 Total Length (TOC to TOS) 0' 0 1/2'  
 Ventilated Cap (Y) (N)

**GROUT**  
 Composition & Proportions 5% Bentonite / Tire Fill  
 Portland Cement Grout  
 Tremied (Y) (N)  
 Interval BGS 0-40 1/2' ft

**CENTRALIZERS** (Y) (N)  
 Depth(s) \_\_\_\_\_

**SEAL**  
 Type 1/2 inch Wyoming Bentonite Rollers  
 Source Environment  
 Setup/Hydration time 15 min Vol. Fluid Added 1 gal  
 Tremied (Y) (N) - 2

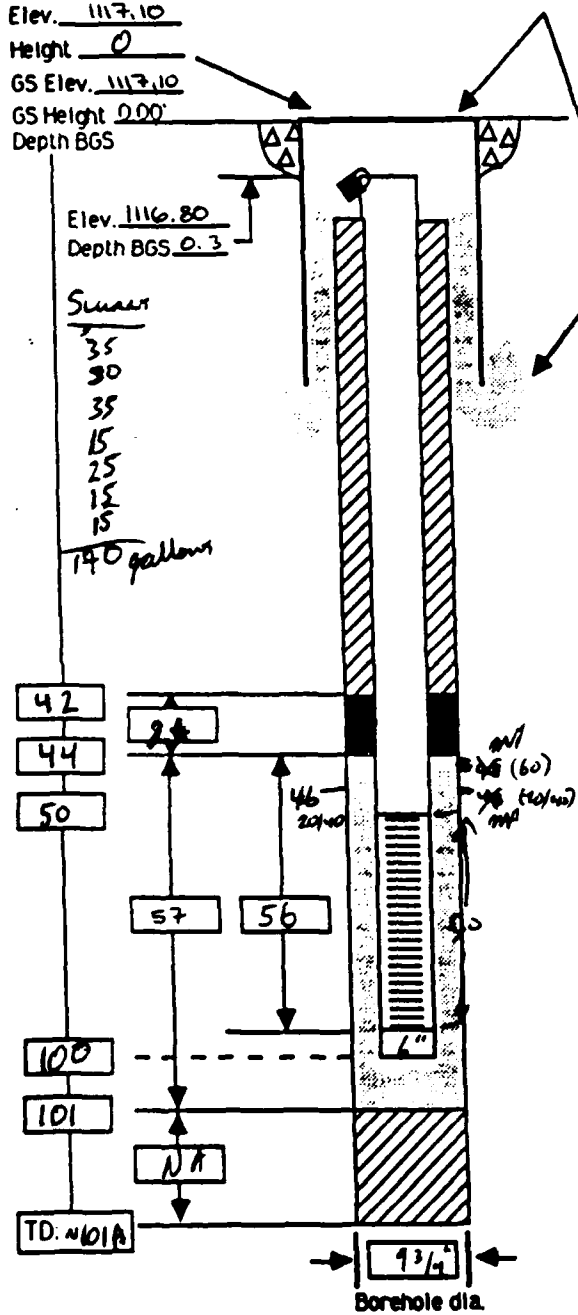
**FILTER PACK**  
 Type 20/40 Coarse Silica Sand, 60 Coarse Silica  
 Amt. Used 19.5X  
 Tremied (Y) (N)  
 Source Colorado Silica  
 Gr. Size Dist. 20/40 Pass, 60 on top

**SCREEN**  
 Type Schedule 40 PVC  
 Diameter 4" in ID  
 Slot Size & Type 0.010 inches  
 Interval BGS 50-100 ft

**SUMP** (Y) (N)  
 Interval BGS 100-101 ft Length 1 ft  
 Bottom Cap (Y) (N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y) (N)

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: <u>MWS-01</u>	Installation: <u>Sky Haz-000</u>	Site: <u>5</u>
Project No.: <u>40302.02</u>	Client/Project: <u>HAZWRAP / Sky Haz-000 ANV</u>	
HAZWRAP Contractor: <u>IT Construction</u>	Drig Contractor:	
Comp. Start: <u>2/2/91</u> ( <u>12:00 P.M.</u> )	Comp. End: <u>2/2/91</u> ( <u>14:00 P.M.</u> )	
Built By: <u>GARON</u>	Well Coord.: <u>N 9345.98</u> <u>E 11050.01</u>	



**PROTECTIVE CSG**  
Material / Type Steel Top / Smoothed Bottom  
Diameter \_\_\_\_\_  
Depth BGS \_\_\_\_\_  
Watertight O-Ring (Y) (N) IT 3-4-91

**SURFACE PAD**  
Composition & Size 3' x 3' x 1' Concrete  
Breathes With Vadose Zone (Y/N)

**RISER PIPE**  
Type 40 PVC  
Diameter 4" I.D.  
Total Length (TOC to TOS) 50'  
Ventilated Cap (Y/N)

**GROUT**  
Composition & Proportions 4 Part Type I Portland Cement + 1 Part 1/2" Bentonite to 35-40% H<sub>2</sub>O; 15 Gallons per 100 lbs  
Tremied (Y/N) (Y) (N)  
Interval BGS 0-42'

**CENTRALIZERS** (Y/N) NA  
Depth(s) \_\_\_\_\_

**SEAL**  
Type 1/2" Wiping Bentonite Pallet  
Source \_\_\_\_\_  
Setup/Hydration time 10 min Vol. Fluid Added 10 gal  
Tremied (Y/N) (Y) (N)

**FILTER PACK**  
Type Colorado Screen Sand & Gravel  
Amt. Used 28 5/8 x 20/40 1/2 5/8 x 60  
Tremied (Y/N) \_\_\_\_\_  
Source \_\_\_\_\_  
Gr. Size Dist. 20/40 Fine to 60 10/100

**SCREEN**  
Type 40 PVC  
Diameter 4" I.D.  
Slot Size & Type 0.010 mm  
Interval BGS (0-42') + 100' = 50'

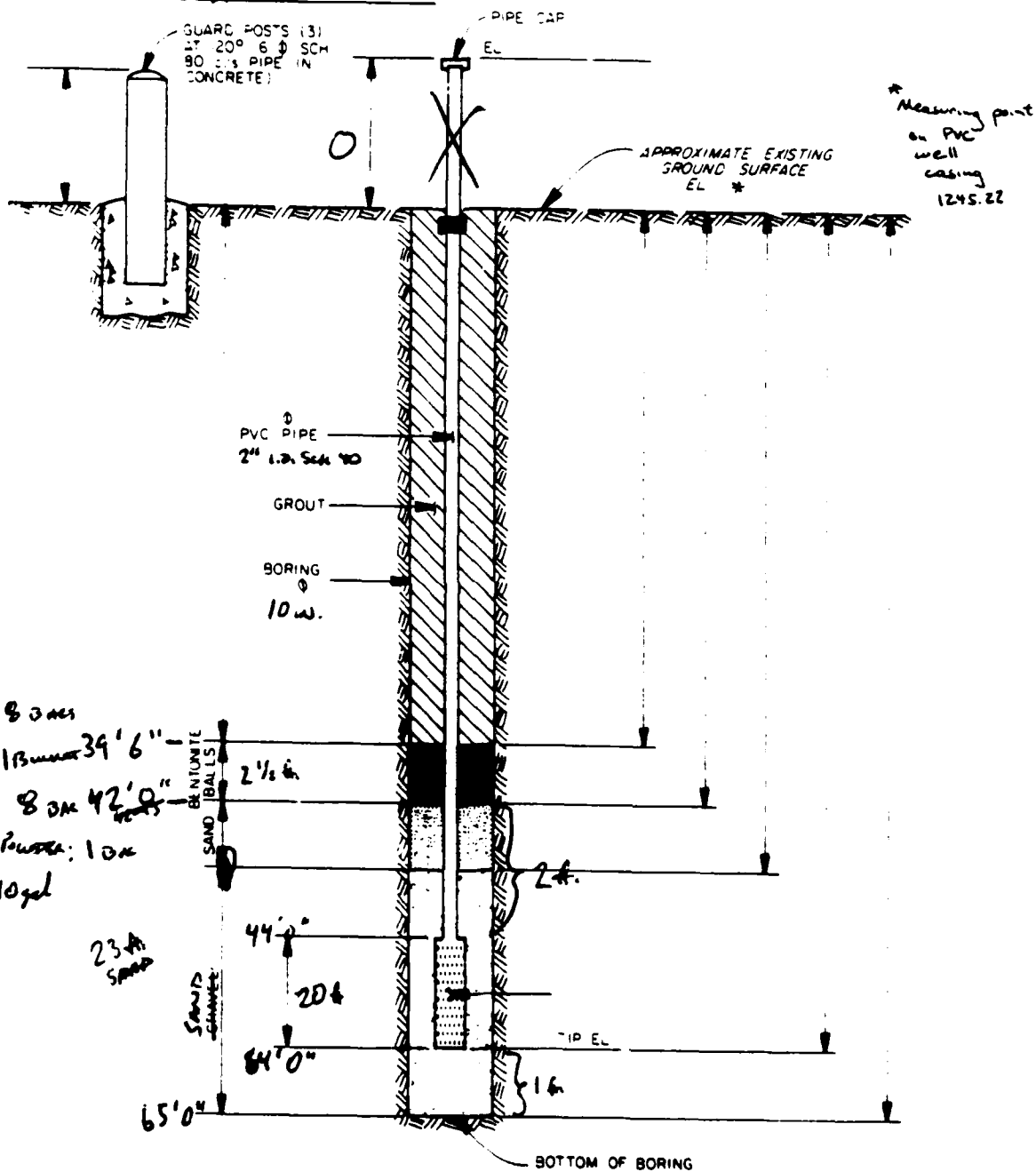
**SUMP** (Y/N) (Y) (N)  
Interval BGS 101 to 100 Length 1'  
Bottom Cap (Y/N) (Y) (N)

**BACKFILL PLUG**  
Material NA  
Setup/Hydration time NA  
Tremied (Y/N) (Y) (N)



# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME Sky Harbor Ave INSTALLED BY Greenlee DATE 1/20/61  
 PROJECT NO 40921.02.06 CHECKED BY NA DATE NA  
 BORING NO \_\_\_\_\_  
 PIEZOMETER NO PP-01



### MATERIALS

- SAND: 8 bags
- PELLETS: 13 bags 39' 6" -
- CEMENT: 8 bags 42' 0" -
- BENTONITE PASTE: 1 bag
- WATER: 10 gal

### Slurry

- 35
- 35
- 15
- 85 gal

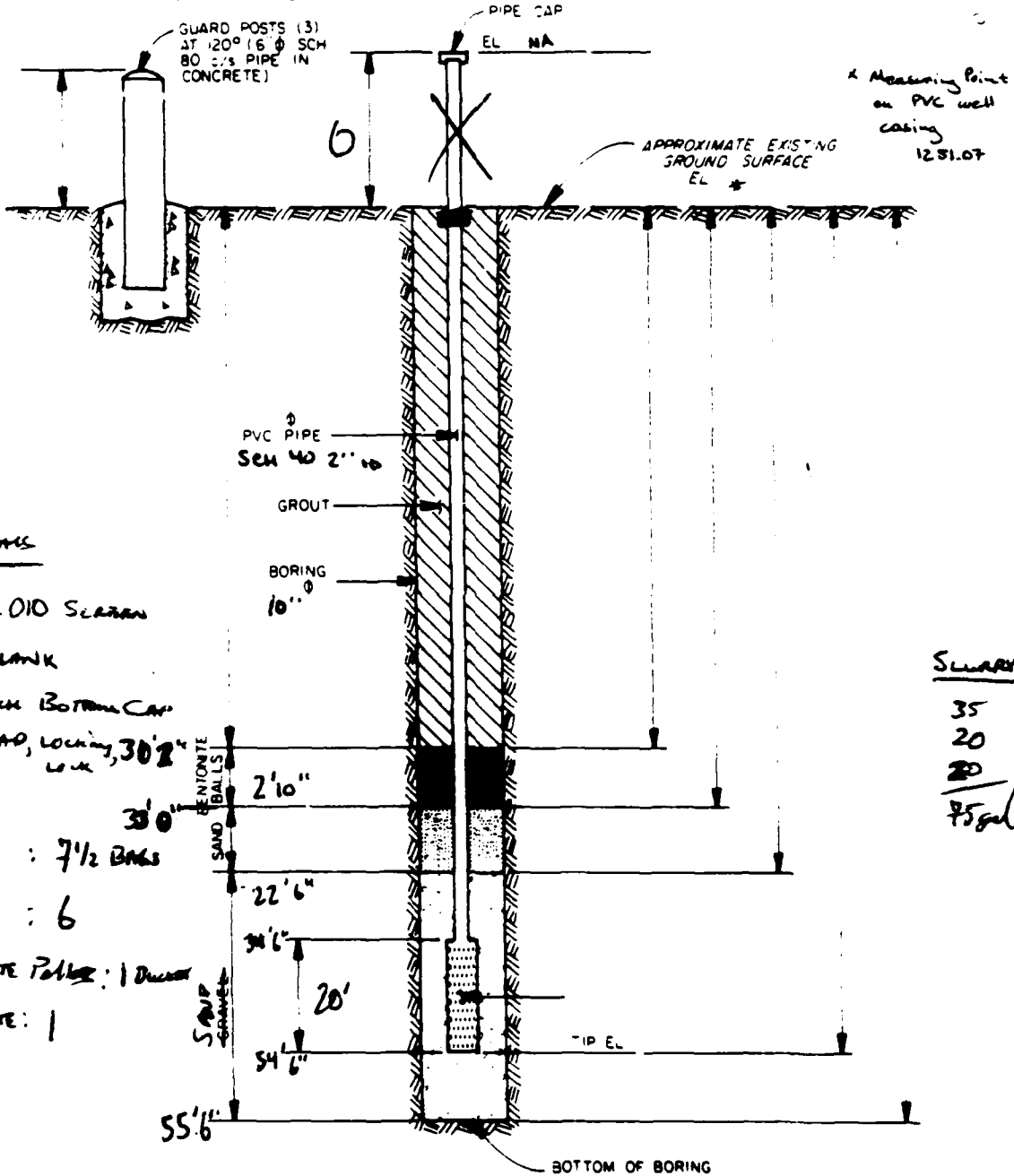
23 bags SAND

SAND FILTER



# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME SHARK INSTALLED BY Guadalupe DATE 1/19/91  
 PROJECT NO 40721.0206 CHECKED BY NA DATE NA  
 BORING NO PP-02  
 PIEZOMETER NO PP-02



### MATERIALS

20 ft. 0.010 Screen

40 ft. Blank

1 - 4 inch Bottom Cap

1 - TOP CAP, Locking, 30" 2"

SAND : 7 1/2 Bags

Cement : 6

BENTONITE PELLETS : 1 Drum

BENTONITE : 1

### Summary

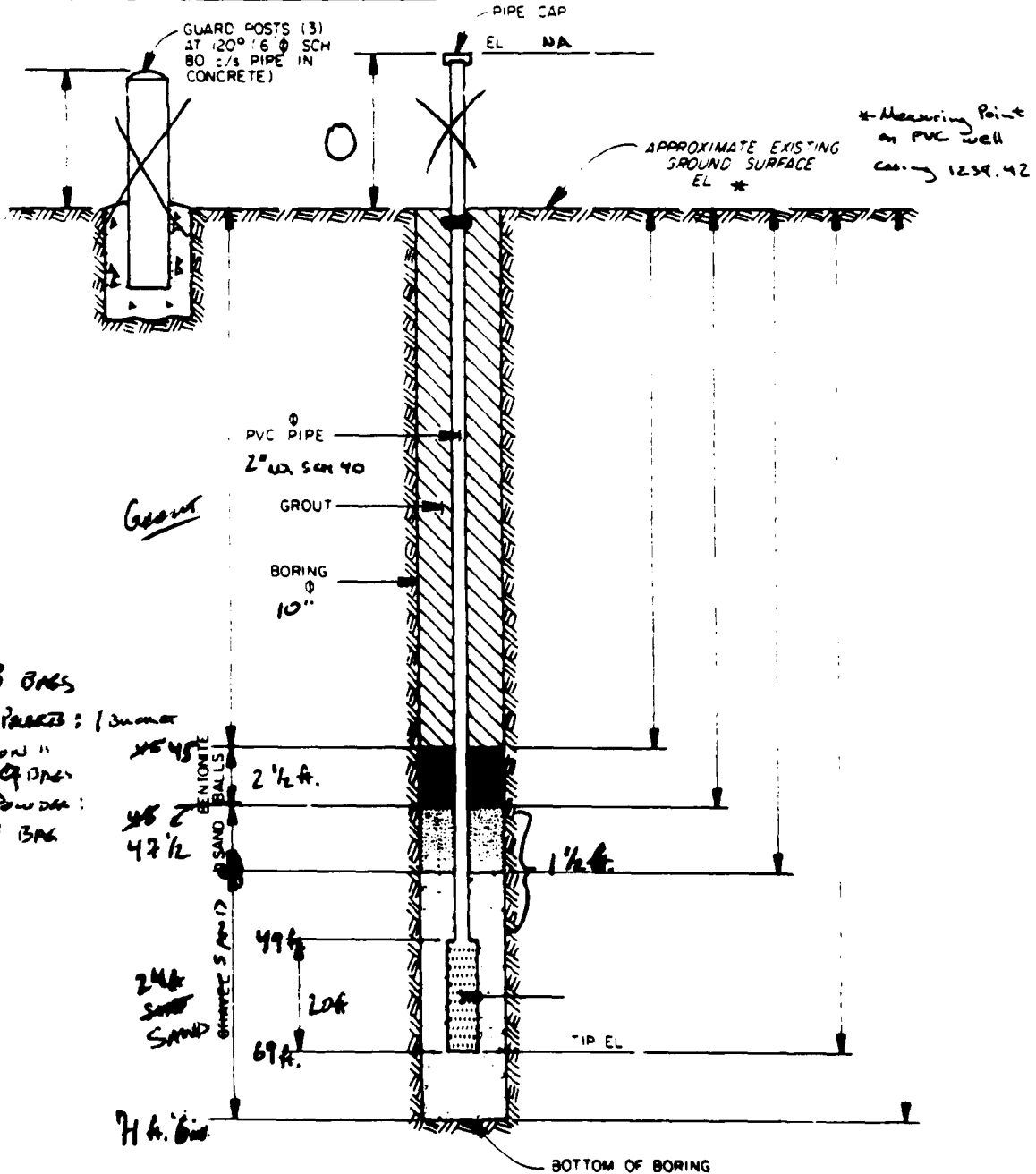
35  
 20  
 20  
 -----  
 75 gal





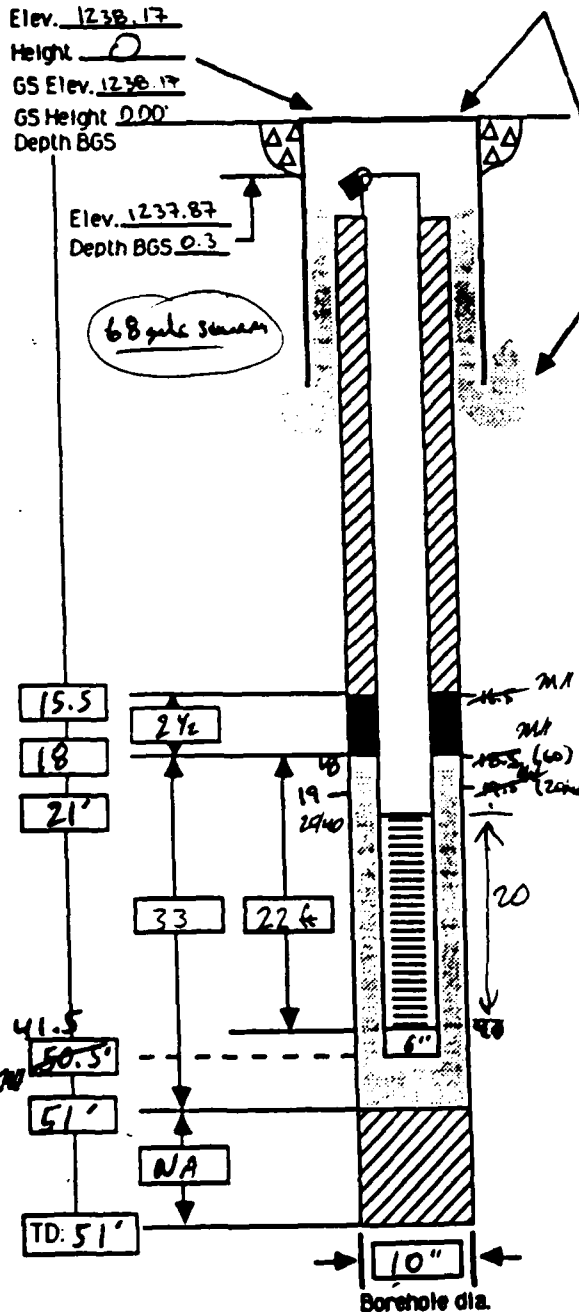
# PIEZOMETER INSTALLATION SKETCH

PROJECT NAME Sky Meadow ANG INSTALLED BY GARDNER DATE 1/20/91  
 PROJECT NO 40922102.06 CHECKED BY NA DATE NA  
 BORING NO NA  
 PIEZOMETER NO PP-03



REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: MW4-01	Installation: <u>Palms Mountain Reservation</u>	Site: <u>4</u>
Project No.: <u>40134</u>	Client/Project: <u>HAZWRAP / Sky Harbor AAK</u>	
HAZWRAP Contractor: <u>IT Corporation</u>	Drig Contractor: <u>Layne Construction</u>	
Comp. Start: <u>2/1/91</u> (15:30 P.M.)	Comp. End: <u>2/8/91</u> (12:40 P.M.)	
Built By: <u>GARDNER</u>	Well Coord.: <u>N 12733.39</u> <u>E 5749.74</u>	



**PROTECTIVE CSG**  
 Material / Type STEEL TOP / STAINLESS STEEL BOTTOM  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_  
 Watertight O-Ring  3-4-91

**SURFACE PAD**  
 Composition & Size 3 ft. x 3 ft. x 1 ft. CONCRETE  
 Breathes With Vadose Zone (Y/N) \_\_\_\_\_

**RISER PIPE**  
 Type 4" SCH 40 PVC  
 Diameter 4" I.D.  
 Total Length (TOC to TOS) 22 ft.  
 Ventilated Cap (Y/N)

**GROUT**  
 Composition & Proportions 4 PARTS TYPE I & II CEMENT  
1 PART BASE SAND  
 Tremied (Y/N)   
 Interval BGS 0-15.5 75% CEMENT 25% SAND

**CENTRALIZERS**  (Y/N)  
 Depth(s) 22 ft. ; 4 ft.

**SEAL**  
 Type 1/4" WYOMING BENTONITE PLUG  
 Source \_\_\_\_\_  
 Setup/Hydration time 1/2 HR Vol. Fluid Added 10 gal 10 gal  
 Tremied (Y/N)

**FILTER PACK**  
 Type COLORADO SILICA SAND  
 Amt. Used 8 5x 20/40 ; 1/2 5x 40  
 Tremied (Y/N)   
 Source \_\_\_\_\_  
 Gr. Size Dist. 20/40 FILTER SAND ; 60 ON 100

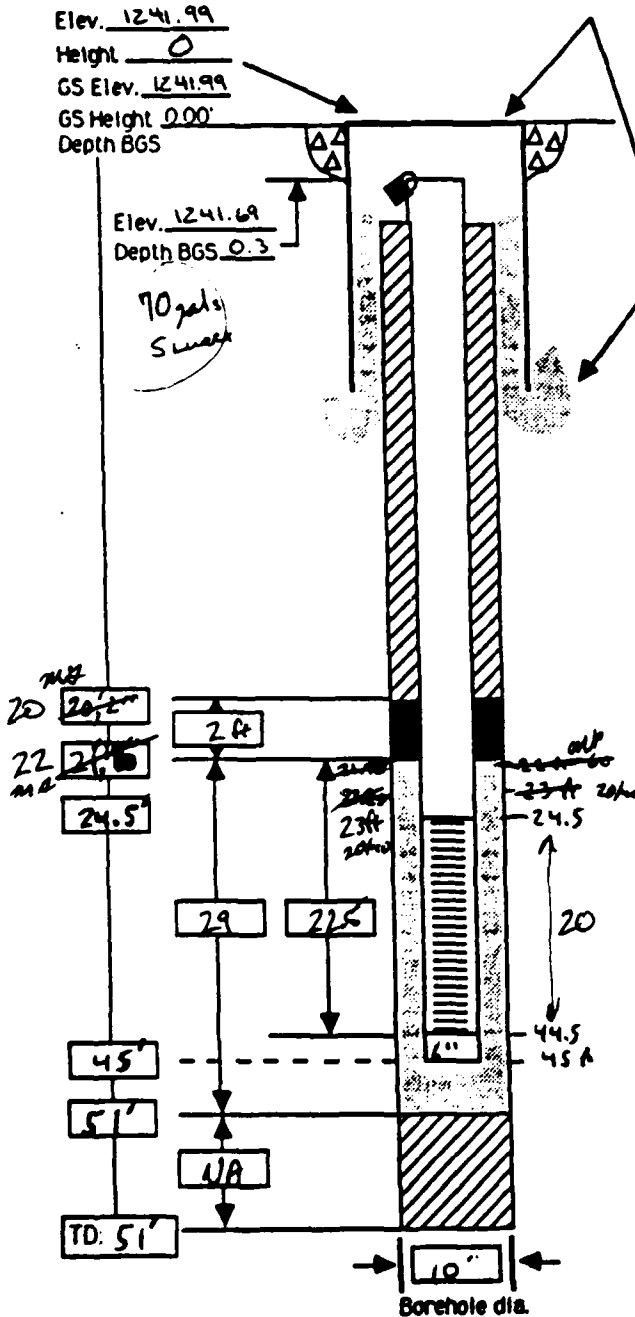
**SCREEN**  
 Type 4" SCH 40 PVC  
 Diameter 4" I.D.  
 Slot Size & Type 0.018 mm  
 Interval BGS 21-41 ft.

**SUMP**  (Y/N)  
 Interval BGS 41.5-51 Length 9.5 ft.  
 Bottom Cap  (Y/N)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y/N)

REV. DATE: MAY 1990

MONITORING WELL CONSTRUCTION LOG -- Standard Flush Mount		
WELL NO.: MW4-02	Installation: PAPPO MOUNTAIN RESERVOIR	Site: 4
Project No.: 40121.00	Client/Project: HAZWRAP / SIX HAZARDOUS	
HAZWRAP Contractor: IT CORPORATION	Drig Contractor: LARIVE ENVIRONMENTAL	
Comp. Start: 2/1/91 (09:30 AM EST)	Comp. End: 2/18/91 (12:15 PM EST)	
Built By: GARDINER	Well Coord.: N 13732.21 E 5959.36	



**PROTECTIVE CSG**  
 Material / Type STEEL TOP / STAINLESS STEEL BOTTOM  
 Diameter \_\_\_\_\_  
 Depth BGS \_\_\_\_\_  
 Watertight O-Ring 1/2" 3-4-91

**SURFACE PAD**  
 Composition & Size 3' x 3' x 1" CONCRETE  
 Breathes With Vadose Zone (Y/N) \_\_\_\_\_

**RISER PIPE**  
 Type SCH. 40 PVC  
 Diameter 4" I.D.  
 Total Length (TOC TO TOS) 24.5'  
 Ventilated Cap (Y/N) (Y)

**GROUT**  
 Composition & Proportions 4 PART TYPE III CONCRETE + 1/2 PART BENTONITE + 35-40 PART SAND  
 Tremied (Y/N) (N)  
 Interval BGS 0-20' (1/2" FILTER SAND & 1/2" SAND)

**CENTRALIZERS** (Y/N) \_\_\_\_\_  
 Depth(s) 24.5'; 50.5'

**SEAL**  
 Type 1/4" BENTONITE SEALANT  
 Source \_\_\_\_\_  
 Setup/Hydration time 1 HR Vol. Fluor. Added 10 gal H<sub>2</sub>O  
 Tremied (Y/N) (N)

**FILTER PACK**  
 Type COARSE SAND / GRAVEL  
 Amt. Used 9.5' x 20/40; 1/2' x 60  
 Tremied (Y/N) (Y)  
 Source \_\_\_\_\_  
 Gr. Size Dist. 20/40 FILTER SAND; 60 on TOP

**SCREEN**  
 Type SCH. 40 PVC  
 Diameter 4" I.D.  
 Slot Size & Type 0.010"  
 Interval BGS 44.5-45.5 (70.6)

**SUMP** (Y/N) \_\_\_\_\_  
 Interval BGS 45-51 Length 6'  
 Bottom Cap (Y/N) (Y)

**BACKFILL PLUG**  
 Material NA  
 Setup/Hydration time NA  
 Tremied (Y/N) (N)

**APPENDIX G**  
**PIEZOMETER AND MONITORING WELL**  
**DEVELOPMENT RECORDS**

WELL DEVELOPMENT LOG PS-1		Well No.: PS-1	Page 1 of 1
Installation:		Site: General	
Project No.: 40972	Client/Project: MMS / Sky Harbor ANG		
HAZWRAP Contractor:	Dev. Contractor: <del>Con</del> Environmental		
Dev. Start ( : m)	Dev. End: ( : m)	Csg Dia.: 2 inch	
Developed by: NA		Dev. Rig (Y/N)	

Dev. Method Surge with bailer and extract 10-20 well volumes with Bailer

Equipment Smeal T-5

Pre-Dev. SWL \_\_\_\_\_ Maximum drawdown during pumping \_\_\_\_\_ ft at 0.5 gpm

Range and Average Discharge rate 0.5 over gpm

Total quantity of material bailed \_\_\_\_\_

Total quantity of water discharged by pumping NA

Disposition of discharge water To be determined

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
			NA					Well could not be developed with 9ft bailer on hand. Blocked at 55ft will attempt with shorter bailer at later date. IRT 4/22/91



INTERNATIONAL  
TECHNOLOGY  
CORPORATION



By JRT Date 1-20-91 Subject Calc. Well PS-1 Sheet No. 1 of 1  
Chkd. By    Date    Casing Volume Proj. No. 409721

Total Depth : 98.42 ft  
Water Depth : 76.12 ft  
Water Column : 22.30 ft

$$\text{Vol} = \left( 2.0 \times \frac{1 \text{ ft}}{12.0} \right)^2 \div 4 \times \pi \times 22.30 = 0.48 \text{ ft}^3$$

or  
3.6 gals

$\therefore$  Bail 36 to 72 gals

WELL DEVELOPMENT LOG		Well No. <u>PS1</u>	Page <u>1</u> of <u>1</u>
Installation <u>Sky Harbor</u>	Coordinates		Site <u>1</u>
Project No: <u>409721.02.06</u>		Client/Project <u>Sky Harbor ANQ Base</u>	
HAZWRAP Contractor: <u>IT Corp</u>		Dev Contractor	
Dev Start: <u>(15-46 m)</u>	Dev End: <u>(17-00 m)</u>	Csg Dia: <u>4" ID</u>	Dev Rig: <u>(Y/N)</u>
Developed by: <u>Layne Environmental</u>			

Dev Method Bailer; surging in water

Equipment 1.5" x 10' PVC Bottom loading Bailer

Pre-Dev. SWL 97.53ft Maximum drawdown during pumping NA ft at NA gpm

Range and Average Discharge rate N/A gpm

Total quantity of material bailed 27 gallons

Total quantity of water discharged by pumping N/A gallons

Disposition of discharge water Held in poly tanks for analysis

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1546			Muddy	Muddy	24.8	7.27	1000µS	
1557	5		Muddy	Muddy	23.5	6.96	980µS	
1606	10		Muddy	Muddy	23.0	7.07	970µS	
1620	13				<del>22</del> 23.0	7.09	960µS	
1630	15				23.1	7.02	950µS	
1640	<del>18</del>				22.3	6.93	950µS	
1655	248ft				22.5	6.96	970µS	
1700	278				22.4	6.8	940µS	
						6.93		

WELL DEVELOPMENT LOG <u>P5-2</u>		Well No.: <u>P5-2</u>	Page <u>1</u> of <u>1</u>
Installation:		Site: <u>General</u>	
Project No.: <u>409721</u>	Client/Project: <u>M.M.E.S / Sky Harbor ANG</u>		
HAZWRAP Contractor:	Dev. Contractor: <u>Layne Edwin</u>		
Dev. Start (12:10 <u>m</u> )	Dev. End: (13:52 <u>m</u> )	Csg Dia.: <u>2 inch</u>	
Developed by: <u>Layne Edwin</u>		<u>Southwest Well Services</u>	Dev. Rig (Y/N)

Developed 1-20-91

Dev. Method Surge with bailer and extract 10-20 well volumes with bailer

Equipment Smel T-5

Pre-Dev. SWL 74.95 Maximum drawdown during pumping ~74.95 ft at ~0.5 gpm

Range and Average Discharge rate .05 over 1 hr 43 min gpm

Total quantity of material bailed 45 gals

Total quantity of water discharged by pumping NA

Disposition of discharge water To be determined

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1210	10		NA ↓	cloudy	20.5	7.15	1170	Fine Sand silt
1229	15			cloudy/brown	20.3	7.49	1080	Fine sand silt
1243	16			cloudy/brown	21.0	7.40	1110	Silty (w/ fine) settles
1248	20			cloudy/brown	21.0	7.42	1120	silty / settling clarity
1309	23			cloudy/brown	20.8	7.34	1130	silty / settling to clear
1329	26			cloudy/brown	20.3	7.34	1150	silty / settling to clear
1333	27			cloudy/brown	20.2	7.22	1110	Silty / and settling
1345	30			cloudy	20.4	7.43	1190	Silty and settling
1348	31			cloudy	20.9	7.30	1110	silty
1353	32			cloudy	21.1	7.37	1080	silty (Qarts Sample) for P10





By JRT Date 1-20-91 Subject Calc Well PS-2 Sheet No. 1 of 1  
Chkd. By          Date          Casing Volume Proj. No. 409721

Total Depth : 99.86  
Water Depth : 81.82  
Water Column : 18.04

$$\text{Vol} = \left( 2.12 \times \frac{1 \text{ ft}}{12 \text{ in}} \right)^2 \times 4 \times \pi \times 18.04 = 0.39 \text{ ft}^3$$

or  
~ 3 gals

∴ Bail 30 to 60 gals

WELL DEVELOPMENT LOG		Well No.: <u>SHP-2</u>	Page <u>1</u> of <u>1</u>
Installation: <u>Sky Harbor</u>	Coordinates	Site: <u>NA</u>	
Project No.: <u>40721.02.06</u>	Client/Project <u>Sky Harbor ANG</u>		
HAZWRAP Contractor: <u>IT Corp</u>	Dev. Contractor		
Dev Start ( <u>13:35</u> m)	Dev. End. ( <u>14:38</u> m)	Csd Dia. <u>2" ID</u>	
Developed by: <u>Layne Environmental</u>		Dev Rig <u>(Y/N)</u>	

2nd Development 2-4-91

Dev Method Bailing

Equipment 1.5" Bottom loading PVC bailer

Pre-Dev. SWL 76.41 Maximum drawdown during pumping NA ft at NA

Range and Average Discharge rate NA

Total quantity of material bailed ~32 gal

Total quantity of water discharged by pumping NA

Disposition of discharge water Held in 55 gal drums for analysis

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1335	2		---	muddy	21.9	7.19	1130	Slight Odor (petroleum) ↓
1353	10		---	muddy	21.8	7.22	1160	
1406	16		---	muddy	21.7	7.28	1080	
1417	21		---	muddy	21.8	7.15	1140	
1438	32		---	muddy	21.8	7.17	1170	

WELL DEVELOPMENT LOG PS-3		Well No.: PS-3	Page <u>1</u> of <u>1</u>
Installation:		Site: <u>General</u>	
Project No.: <u>409721</u>	Client/Project: <u>MMS / Sky Harbor ANG</u>		
HAZWRAP Contractor:		Dev. Contractor: <u>Layne Env.</u>	
Dev. Start ( <u>09:45</u> m)	Dev. End: ( <u>11:10</u> m)	Csg Dia.: <u>2 inch</u>	
Developed by: <u>Southwest Env. Well Services</u>		Dev. Rig (Y/N)	

Developed 1-20-91

Dev. Method Surge with bailer and extract 10-20 well volumes  
with bailer

Equipment Small T-5

Pre-Dev. SWL 75.50 Maximum drawdown during pumping ~85 ft at ~0.5 gpm

Range and Average Discharge rate 0.5 gpm over 1 hr 20 mins gpm

Total quantity of material bailed 55 gals

Total quantity of water discharged by pumping NA

Disposition of discharge water To be determined

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity $\mu$ hos	Remarks
0945			NA					
1008	15			Cloudy Brown	19.6	7.11	1080	Fine sand, silt
1026	18			Cloudy Brown	19.9	7.41	1060	Silty, sand
1037	24			Cloudy Brown	20.2	7.35	1050	Silty, fine sand
1046	30			Cloudy	20.4	7.28	1010	Silty
1050	35			Cloudy	20.5	7.31	1060	Silty
1055	42			Cloudy gray	20.8	7.40	1070	Silty
1100	50			Cloudy brown	21.3	7.31	1050	Silty, very fine
1108	55			Cloudy	20.5	7.32	1070	No visible fines
1110	55			Cloudy	20.9	7.36	1050	Clear enough for piezo



By JRT Date 1-20-91 Subject Calc. Well PS-3 Sheet No. 1 of 1  
 Chkd. By      Date      Casing Volume Proj. No. 409721

Total Depth : 98.42 ft  
 Water Depth : ~~76.12 ft~~ 83.48 ft  
 Water Column : ~~22.30 ft~~ 16.42 ft

$$Vol = \left( 2 \text{ in} \times \frac{1 \text{ ft}}{12 \text{ in}} \right)^2 \div 4 \times \pi \times 16.42 = 0.36 \text{ ft}^3$$

or  
 ~ 2 3/4 gals

∴ Bail 26 to 52 gals

WELL DEVELOPMENT LOG		Well No.: MW28-01	Page 1 of 1
Installation: Sky Harbor	Coordinates	Site: Background Well	
Project No.: 409721.02.00	Client/Project: Sky Harbor ANG		
HAZWRAP Contractor: IT Corp	Dev. Contractor:		
Dev Start (08:23 m)	Dev End: (09:28 m)	Csd Dia: 4" ID	
Developed by: Layne Environmental		Dev. Rig (RYN)	

Dev. Method Swab surge, bailer, submersible pump

Equipment 3 5/8" x 10' Bottom loading steel bailer, 1.5 HP Franklin submersible pump

Pre-Dev. SWL 77.14 ft Maximum drawdown during pumping NA ft at NA gpm

Range and Average Discharge rate 5-20 gpm <sup>10 gpm nominal</sup>

Total quantity of material bailed ~18 gals

Total quantity of water discharged by pumping 200-180 gals

Disposition of discharge water Held in poly tanks for analysis

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
0823	5		Muddy	Muddy	20.7	6.80	1090	
0904	60		1	1	22.1	6.83	1100	
0910	115		<del>Cloudy</del> 159.1	Cloudy		6.75	1090	
0915	170		27.8	Slightly Cloudy	22.3	6.72	1110	
0920	185		17.6	Clean	22.4	6.78	1100	
0928	200		13.9	Clean	21.7	6.65	1070	

WELL DEVELOPMENT LOG		Well No.: MWS-02	Page 1 of 1
Installation: Sky Harbor	Coordinates:	Site: Background	
Project No.: 409721	Client/Project: MMES / Sky Harbor ANG		
HAZWRAP Contractor: IT Corp	Dev. Contractor: Layne Env.		
Dev Start (11:15 AM)	Dev. End: (12:40 PM)		Csg Dia: 4 inch
Developed by: Tyburki / Layne Env.		Dev. Rig (Y/N)	

Developed MWS-02

Dev. Method Surge saturated screen interval; bail sediment as required; pump to visibly clear or 5 NTU's if possible

Equipment Smeal development rig.

Pre-Dev. SWL 75.25 Maximum drawdown during pumping \_\_\_\_\_ ft at \_\_\_\_\_ 5 \_\_\_\_\_ gpm

Range and Average Discharge rate 3-6 gpm avg approx 5 \_\_\_\_\_ gpm

Total quantity of material bailed 20 gals

Total quantity of water discharged by pumping 180 gals

Disposition of discharge water To be determined

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
11:15	-	75.25	-	-	-	-	-	Start Surging
11:45	-							start bailing
12:10	20			Brown	23.3	7.43	1130	Start pumping
12:15	35			lt. br	23.7	7.23	1110	
12:23	60			Cloudy	23.3	7.40	1150	
12:32	140			Cloudy	23.5	7.26	1120	
12:35	170		41.1	Slightly Cloudy	23.4	7.40	1140	
12:40	200		21.5	Clear	23.6	7.23	1140	Stop. Clarity good



WELL DEVELOPMENT LOG		Well No. <u>MWS-04</u>	Page <u>1</u> of <u>1</u>
Installation <u>Sky Harbor</u>	Coordinates	Site <u>Sky Harbor Background Well</u>	
Project No. <u>40721.02.06</u>	Client/Project <u>HAZWRAP / Sky Harbor Army</u>		
HAZWRAP Contractor <u>IT Corporation</u>	Dev. Contractor <u>Lowe Environmental</u>		
Dev Start <u>(9:30 a.m) 3/24/91</u>	Dev End <u>(2:02 p.m) 3/26/91</u>	Csd Dia. <u>4 in. I.D.</u>	Dev Rig <u>(Y) N</u>
Developed by: <u>Gardner / Winkler</u>			

Dev Method Surge w/ 4 in. Surge for 15-20 minutes, Bail for approximately 30-40 gal, then pump until water clarity & turbidity are < 20 NTU

Equipment Development Rig, pH Meter, Conductivity Meter, Temp. Probe

Pre-Dev. SWL 74.92 Maximum drawdown during pumping NA ft at NA gal

Range and Average Discharge rate 3-55 GPM / Average Rate Approx 5 gpm

Total quantity of material bailed 55 gal

Total quantity of water discharged by pumping 165 gal

Disposition of discharge water Considered on site pending water quality analysis

Time	Volume Removed (gals)	Water Level ft BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
0935	20	74.92	NA	Cloudy	20.8	7.03	1170	Very small amt (0.01 ft.?) of BSH in well
1120	35		"	"	20.5	6.67	1140	
1123	50		"	"	22.5	6.74	1170	
1125	60		"	"	21.8	6.82	1170	
1129	70		"	"	22.1	6.85	1140	
1132	80		"	"	22.5	6.80	1150	
1137	90		77	"	23.2	6.82	1140	
1141			71	Slightly Cloudy	23.3	6.79	1160	
1145	150		100	"	22.9	6.81	1020	
1147	165		54.5	"	23.1	6.83	996	
1151	190		40.7	Very Slightly Cloudy	23.2	6.81	1190	
1154	200		31.8	"	22.8	6.83	1190	
1159	220	75.06	25.2	"	23.1	6.78	1050	

NOTE: NA = NOT ANALYZED FOR.



WELL DEVELOPMENT LOG		Well No.: MW1-02	Page 1 of 1
Installation:		Site: 1	
Project No.: 409721.02.06		Client/Project: Sky Harbor ANG Base	
HAZWRAP Contractor: IT Corp		Dev. Contractor: Hayne Environmental	
Dev. Start (10:50 AM)	Dev. End: (12:51 PM)	Csg Dia.: 4" ID	
Developed by: Hayne Environmental		Dev. Rig (Y/N)	

Developed 2-4-91

Dev. Method 3 5/8" OD x 10' Steel Bailer Bailer, followed by swab, finished with pump

Equipment 3 5/8" OD x 10' Steel Bailer, 4" OD Swabs, Franklin 1.5HP Submersible pump

Pre-Dev. SWL 77.32 ft maximum drawdown during pumping \_\_\_\_\_ ft at \_\_\_\_\_ gpm

Range and Average Discharge rate 5-20 gpm (6 gpm nominal) gpm

Total quantity of material bailed 15 gallons

Total quantity of water discharged by pumping ~425 gallons

Disposition of discharge water Hold in poly tanks for analysis

Time	Volume Removed (gals)	Water Level (ft BTOC)	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
<del>1047</del>			N/A	Cloudy Brown	22.4	7.36	1080 μS	
1050	15							
1200	60		7200	Slightly Cloudy	25.0	7.10	1100 μS	Clearing quickly
1213	80		155.2	Clear	Low Battery	7.01	1090 μS	Clearer
1222	<del>165</del> 220		36.6	Clear	—	7.03	1070 μS	Fairly Clean
1235	240		63.2	Clear	—	6.84	1070 μS	pH & Conductivity Stable
1242	295		78.9	Clear	—	—	—	
1245	330		31.3	Clear	—	—	—	
1247	360		27.7	Clear	—	—	—	
1250	585		26.0	Clear	—	—	—	
1252	410		17.5	Clear	—	—	—	
1254	440		14.2	Clear	—	—	—	

Shut pump down

WELL DEVELOPMENT LOG		Well No.: MW2-02	Page 1 of 1
Installation:	50 ft. of screen Top at 50 bgs.	Site: Site Z	
Project No.:	409721	Client/Project: MMEs / Sky Harbor ANG	
HAZWRAP Contractor:	IT Corp	Dev. Contractor: Layne Env.	
Dev. Start	(8:15 AM)	Dev. End:	(10:15 AM) Csg Dia.: 4 inch
Developed by: Bailing, Surging, Pumping (Tybirk)		Dev. Rig (Y/N)	

Dev. Method Surging saturated screen interval, bail, pump to  
visibly clear or SNTU's.

Equipment Small development rig.

Pre-Dev. SWL 75.59 Maximum drawdown during pumping 99.74 ft at ~ 6 gpm gpm

Range and Average Discharge rate approx 6 gpm while pumping gpm

Total quantity of material bailed 20 gals

Total quantity of water discharged by pumping 180 gals

Disposition of discharge water To be determined

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
0815	-	75.59	-	-	-	-	-	Start surging
0845	-	-	-	-	-	-	-	Run bailer in well
0855	20 gals	-	-	Brown	20.1	6.84	1150	Begin to set pump
0935	60 gals	-	-	Light Br.	21.7	6.35	1250	Began pumping 0930
0940	70 gals	-	-	Light Br	21.8	6.28	1130	Stop pump temporarily
0945	80 gals	-	-	Cloudy	22.1	6.40	1120	
0950	110 gals	-	-	Cloudy	22.1	6.98	1130	
1000	130 gals	-	-	sl. cloudy	21.9	7.04	1170	
1001	135 gals	-	58.2	sl. cloudy	22.3	7.15	1140	
1005	160 gals	-	47.5	sl. cloudy	22.5	7.11	1190	
1008	180 gals	-	31.5	Clear	22.3	7.21	1150	
1015	200 gals	99.74	25.8	Clear	-	-	-	Considered clear enough.

WELL DEVELOPMENT LOG		Well No.: MW3-01	Page 1 of 1
Installation: Sky Harbor	Coordinates	Site: 3	
Project No.: 401221-02-06	Client/Project: HAZWRAP/Sky Harbor ANK		
HAZWRAP Contractor: IT Corporation	Dev. Contractor: LAYNE Environmental		
Dev. Start ( ) ( ) m) 3/14/91	Dev. End: ( ) ( ) m)	Csq Dia. 4.0 in. I.D.	Dev. Rig (Y/N)
Developed by: GARDNER/WOLKIN			

Dev Method SURGE  
Surge w/ 4 in Surges FOR 15-20 minutes, Bail for APPROX  
30-40 gal, THEN PUMP UNTIL WATER CLARITY/15 X ≤ 20 NTU  
TURBIDITY

Equipment Development Rig, pH meter, Conductivity meter, Turb Probe

Pre-Dev. SWL 75.82 Maximum drawdown during pumping \_\_\_\_\_ ft at \_\_\_\_\_ gpm

Range and Average Discharge rate 3-5 GPM \_\_\_\_\_ gpm

Total quantity of material bailed 55 Gallons

Total quantity of water discharged by pumping 155

Disposition of discharge water CONTAINED AND SITE PERIODIC WATER QUALITY ANALYSIS

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1120	0	75.28	-	-	-	-	-	Strong odor from well
1140	15	-	-	very cloudy	20.6	6.93	970	
1145	40	-	-	"	21.0	7.02	1070	
1148	55	-	-	"	21.4	7.01	1050	
1210	80	-	-	"	20.9	6.88	1110	
1213	95	-	-	cloudy	22.0	6.83	1020	
1216	105	-	-	"	23.1	6.79	1060	
1220	120	-	-	slightly clear	23.3	6.78	1060	
1225	140	-	-	"	22.7	6.79	1050	
1230	160	-	137.6	"	22.4	6.75	1050	
1235	175	-	102.3	"	23.7	6.77	1050	
1239	190	-	92.1	"	23.6	6.76	1000	
1243	205	-	64.0	"	24.0	6.75	1010	
1245	215	75.3	41.1	"	23.7 23	6.77	1000	

WELL DEVELOPMENT LOG		Well No. <u>WU 3-02</u>	Page <u>1</u> of <u>1</u>
Installation: <u>Sky Harbor</u>	Coordinates	Site: <u>3</u>	
Project No.: <u>40921.02.06</u>	Client/Project: <u>HAZWRAP / Sky Harbor ASX</u>		
HAZWRAP Contractor: <u>ITC</u>	Dev. Contractor: <u>LAMAR ENVIRONMENTAL</u>		
Dev. Start ( <u>    </u> m)	Dev. End: ( <u>    </u> m)		Csg Dia. <u>4 in. I.D.</u>
Developed by: <u>GARDNER / WILSON</u>		Dev Ric <u>(Y/N)</u>	

Dev Method Swirl w/ 4 in. Swirl for 15-20 minutes, Bail for approximately 30-40 gals, then pump until water clarity & turbidity is  $\leq 20$  NTU

Equipment Development Rig, pH meter, Conductivity meter, Temp. Probe

Pre-Dev. SWL 76.23 Maximum drawdown during pumping \_\_\_\_\_ ft at \_\_\_\_\_ gpd

Range and Average Discharge rate 3-5 GPM \_\_\_\_\_ gpd

Total quantity of material bailed 55 gals.

Total quantity of water discharged by pumping 155 gals

Disposition of discharge water CONTAINED ON SITE PENDING WATER QUALITY ANALYSIS

Time	Volume Removed (gals)	Water Level! ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
0830	15	76.23	NA	cloudy	19	6.73	1150	
0833	45		NA		19.2	6.76	1140	
0900	60		NA		19.7	6.77	1130	
0904	75				21.5	6.83	1010	
0908	80				22.0	6.75	1030	
0912	95				22.7	6.73	1080	
0915	110				22.9	6.83	980	
0920	130				23.1	6.74	1070	
0923	145				22.7	6.77	960	
0925	175		513	slightly cloudy	23.1	6.74	1010	
0930	180		50.0		23.0	6.78	980	
0935	200		45.6	clear	23.0	6.72	1010	
0940	210		18.1	clear	22.2	6.83	1110	
		* 73.64						

\* Finishing crew cut off several inches of well casing when finishing well.



WELL DEVELOPMENT LOG		Well No.: PP-01	Page 1 of 1
Installation:		Site: PARAGO ANG	
Project No.: 40974-02-06	Client/Project: MARES / AZ ANG		
HAZWRAP Contractor:	Dev. Contractor: SOUTHWEST ENVIRONMENTAL WELL SERVICE CO.		
Dev. Start (11:47 m)	Dev. End: (12:22 m)	Csg Dia.: 2"	
Developed by: SOUTHWEST ENVIRONMENTAL WELL SERVICES CO. J.S. FL. CORP.		Dev. Rig (Y/N)	

Developed 1-29-91

Dev. Method 1.25 O.D. x 9.90 PVC BOTTOM LOADING BAULER w/ DEDICATED ROPE

Equipment SMALL RG USING HOIST + HAND PULLING.

Pre-Dev. SWL 30.84 Maximum drawdown during pumping N/A ft at N/A gpm

Range and Average Discharge rate N/A gpm

Total quantity of material bailed 17 Gallons

Total quantity of water discharged by pumping N/A

Disposition of discharge water ROPED IN 6 SS gal DRS + LABELED BY PILOMETER NUMBER

Time	Volume Removed (gals)	Water Level ft BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1118	1			RAWISH	22.6	7.02	1740	MEASUREMENTS BEFORE INSERT FIRST BAULER. VOLUME REMOVED FROM WELL.
1134	3			RAWISH	22.9	7.20	1610	WATER HAS A SLIGHT OOR. IT CAN NOT DESCRIBE SLIGHTLY.
1145	6			RAWISH	23.0	7.20	1560	SLIGHT OOR. MEASURED WATER LEVEL LEVEL DROPPED 16" AFTER REMOVAL 6 GALLONS.
1200	9			RAWISH	22.8	7.29	1510	SLIGHT OOR. CLOUDY.
1209	12			RAWISH	22.9	7.24	1500	SIGHT OOR. CLOUDY.
1216	16			RAWISH	22.8	7.20	1620	SLIGHT OOR, CLOUDY, SIFTY.

WELL DEVELOPMENT LOG		Well No.: PP-02	Page 1 of 1
Installation:		Site: PARGO ANG	
Project No.: 409721-02-06	Client/Project: MMS / A2 ANG		
HAZWRAP Contractor:	Dev. Contractor: SOUTHWEST ENVIRONMENTAL WELL SERVICES CO.		
Dev. Start (12:52 m)	Dev. End: (14:25 m)	Csg Dia: 2"	
Developed by: SOUTHWEST ENVIRONMENTAL WELL SERVICES CO. J.S. III. (P) Dev. Rig (D/N)		Developed 1-29-91	

Dev. Method 1.25<sup>ad</sup> x 9.76 PVC BOTTOM LEADING BAILER w/ DEDICATED ROPE.

Equipment SMALL RIG w/ HOIST USING ROPE + HAND PULLING

Pre-Dev. SWL 37.45 Maximum drawdown during pumping N/A ft at N/A gpm

Range and Average Discharge rate \_\_\_\_\_ gpm

Total quantity of material bailed 42 GALLONS

Total quantity of water discharged by pumping N/A

Disposition of discharge water POURED INTO SS AND DMS + LABELED BY PNEUMETER NUMBER

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1303	43			Brown	24.0	7.22	1980	MUDDY, NO ODR, HAD TO BAL 4 GALS OF WATER COMING OUT MUDDY.
1309	6			Brown	22.7	7.37	1990	MUDDY, NO ODR
1321	9			Brown	23.8	7.37	1950	MUDDY, NO ODR
1328	12			Brown	24.4	7.40	1920	MUDDY, NO ODR
1331	15			Brown	24.7	7.30	1990	SLIGHTLY MUDDY, NO ODR
1347	21			Brown	24.8	7.29	1990	SLIGHTLY MUDDY, NO ODR
1400	20			Brown	24.4	7.29	2000	
1413	41			Almost clear	24.5	7.34	2020	ALMOST CLEAR, NO ODR

WELL DEVELOPMENT LOG		Well No.: PP-03	Page 1 of 1
Installation:		Site: PABAGO ANG	
Project No.: 409721	Client/Project: MMES / A.E. ANG		
HAZWRAP Contractor:	Dev. Contractor: SOUTHWEST ENVIRONMENTAL WELL SERVICES		
Dev. Start (0.921m)	Dev. End: 40 (10.39 m)	Csg Dia.: 2"	
Developed by: SOUTHWEST ENVIRONMENTAL WELL SERVICES CO.		Dev. Rig (Y/N)	

Developed 1-29-91

Dev. Method 1.25 O.D. X 9.90 PVC BOTTOM LOADING BAILER W/ DEDICATED POLY ROPE.

Equipment SMEAL RIG. W/ HOIST. POLLING BAILER BY HAND.

Pre-Dev. SWL 32.30 Maximum drawdown during pumping N/A ft at N/A gpm

Range and Average Discharge rate \_\_\_\_\_ gpm

Total quantity of material bailed 11 GALLONS

Total quantity of water discharged by pumping N/A

Disposition of discharge water POURED INTO 55 GNL DRUM + LABELED BY PERIMETER NUMBER

Time	Volume Removed (gals)	Water Level ft BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
0935	~1			SLIGHTLY CLAYY, NO ODOOR	23.7	7.08	1330	MEASUREMENT REPRESENT FIRST BAILER VOLUME.
0944	~2			BROWNISH	23.8	7.18	1360	SINK 37.83. STOPPING WELL FOR ~10 MIN. N/BETWEEN FOLD PERIMETER WATER SLIGHTLY CLAYY. NO ODOOR
0954	~2.5			BROWNISH	24.5	7.26	1320	WATER SLIGHTLY CLAYY. NO ODOOR
1006	3.5			BROWNISH	23.3	7.30	1320	WATER SLIGHTLY CLAYY. NO ODOOR
1018	4.5			BROWNISH	23.9	7.32	1310	SLIGHTLY CLAYY, NO ODOOR
1035	10			BROWNISH	23.6	7.32	1330	SLIGHTLY CLAYY, NO ODOOR REMOVED SIGALS IN BAILER + WATER LEVEL DECREASED FROM 48.96 TO 59.45



WELL DEVELOPMENT LOG		Well No.: <u>W4-02</u>	Page <u>1</u> of <u>2</u>
Installation: <u>Sky Harbor</u>	Coordinates	Site: <u>4 (Paradise)</u>	
Project No.: <u>40121.02.06</u>	Client/Project: <u>HAZWRAP / Sky Harbor Park</u>		
HAZWRAP Contractor: <u>ITC</u>		Dev. Contractor: <u>Lovely Environ.</u>	
Dev. Start: <u>(10:45 A.M.) 2/1/91</u>	Dev. End: <u>(16:00 P.M.) 2/1/91</u>	Csg Dia: <u>4-in I.D.</u>	Dev. Rig: <u>(N)</u>
Developed by: <u>Gardner</u>			

Dev. Method Soils w/ 4 well swags for 30 minutes; Bar w/ 10 ft (5 gal. brace) to standard Turbidity, pH, Temp, Conductivity

Equipment Development Rig, pH/Conductivity Meter, Turbidity meter.

Pre-Dev. SWL 27.41 ft Maximum drawdown during pumping Barred ft at \_\_\_\_\_ gpm

Range and Average Discharge rate \_\_\_\_\_ gpm

Total quantity of material bailed N 50 gal w/ 1 bag of sand/silt; w/ 45 gal water

Total quantity of water discharged by pumping 0

Disposition of discharge water Drummed and site near debris area at Paradise

Time	Volume Removed (gals)	Water Level ft. BTOC	Turbidity	Clarity/Color	Temp °C	pH	Conductivity	Remarks
1045	0	27.41						Initial
1125	10		194	Beau	26.2	7.02	930	
1128	20		192	↓	26.2	7.33	940	
1130	27 1/2		—	↓	26.1	7.25	970	Turbidity meter now functioning
1132	31 1/2		—	LT. Beau	25.8	7.15	940	
1227	35		—	↓	26.7	7.56	980	
1305	37		—	↓	26.5	7.31	990	
1340	39		—	Very LT. Beau	26.6	7.40	890	11
1435	42		—	"	26.4	7.38	910	11
1505	43 1/2		—	"	26.5	7.43	960	11
1600	45		—	Slightly cloudy	26.3	7.43	950	11
1602	45 1/2		—	"	26.2	7.45	960	11

Based on color & amount of opaqueness, turbidity was probably reduced by about 1/2 of starting value.