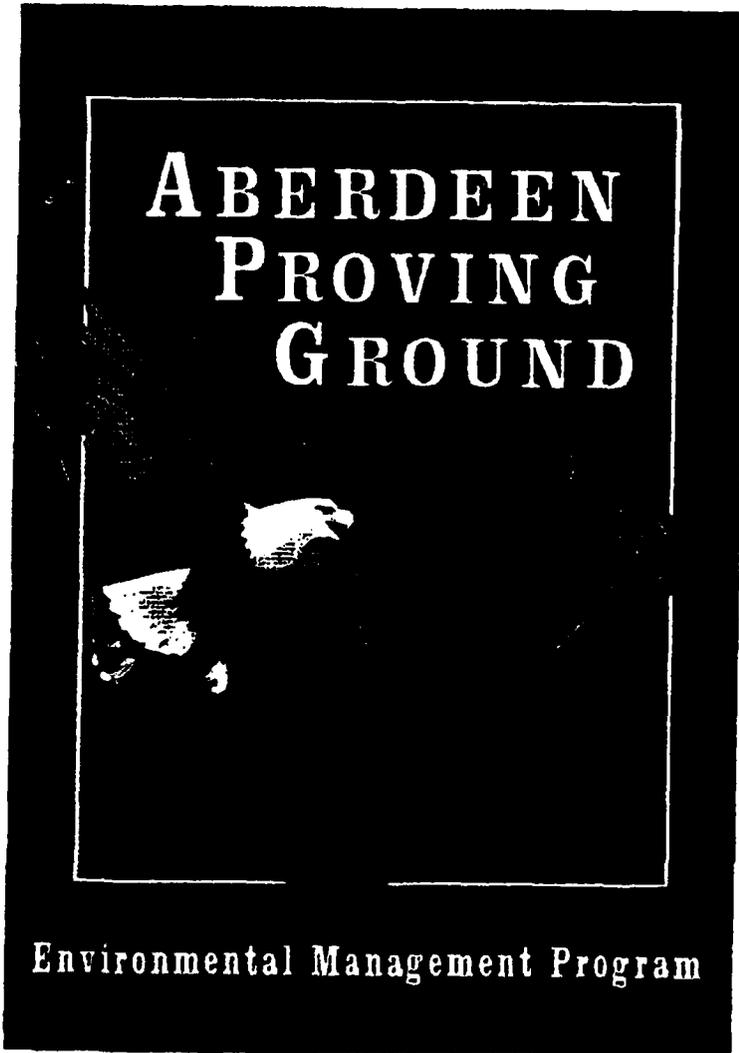




*Canal Creek Study Area
Aberdeen Proving Ground - Edgewood Area, Maryland*

APPENDIX A

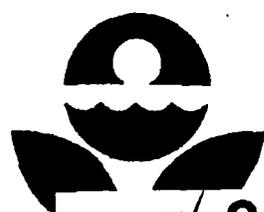
**GROUNDWATER MONITORING PLAN
FINAL QUALITY ASSURANCE PROJECT PLAN
STANDARD OPERATING PROCEDURES (SOPs)**



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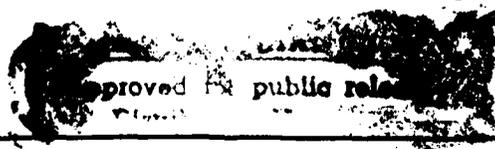


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U.S. EPA. 1980, Interim Guidelines and Specifications for Preparing Quality Assurance Project Plans, QAMS-005/80

STANDARD OPERATING PROCEDURE 003
FIELD LOGBOOK

1.0 Scope and Application

The purpose of this standard operating procedure is to delineate protocols for recording field survey and sampling information in the Field Logbook.

2.0 Material

- a. Field Logbook (Teledyne 415 Level Book, or equivalent)¹
- b. Indelible ink pen

3.0 Procedure

All information pertinent to a field survey or sampling effort will be recorded in a bound logbook. Each page/form will be consecutively numbered, dated, and signed. All entries will be made in indelible ink and all corrections will consist of line-out deletions that are initialed and dated. The person making the correction will provide a brief explanation for the change. There should be no blank lines on a page. A single blank line or a partial blank line (such as at the end of a paragraph) should be lined to the end of the page. If only part of a page is used, the remainder of the page should have an "X" drawn across it. At a minimum, entries in the logbook will include but not be limited to the following:

- a. Project number.
- b. Unique, sequential field sample number.
- c. Purpose of sampling.
- d. Location, description, and log of photographs of each sampling point.
- e. Details of the sample site (for example, the elevation of the casing, casing diameter and depth, integrity of the casing, etc.)
- f. Name and address of field contact.
- g. Documentation of procedures for preparation of reagents or supplies which become an integral part of the sample (e.g., filters and absorbing reagents).

¹ Pre-printed, bound forms are approved as well. See SOP 016 for recommended content and format.

**STANDARD OPERATING PROCEDURE 004
SAMPLE PACKING AND SHIPPING**

1.0 Scope and Application

The purpose of this Standard Operating Procedure (SOP) is to delineate protocols for the packing and shipping of samples to the laboratory for analysis.

2.0 Material

- a. Waterproof coolers (hard plastic or metal)
- b. Metal cans with friction-seal lids (e.g. paint cans)
- c. Custody seals
- d. ~~Non-absorbent~~ Packing material²
- e. Sample Documentation
- f. Ice
- g. Plastic Garbage Bags
- h. Clear Tape
- i. ~~Bubble wrap or closed cell foam packing sheets~~
- j. Zip seal plastic bags

3.0 Procedure

- 3.1 Check cap tightness and verify that clear tape covers label and encircles container.
- 3.2 Wrap sample container in bubble wrap or closed cell foam sheets.
- 3.3 Enclose each sample in a clear zip-seal plastic bag.
- 3.4 Place several layers of bubble wrap, or at least 1" of vermiculite on the bottom of the cooler. Line cooler with open garbage bag, place all the samples upright inside a garbage bag and tie the bag.
- 3.5 Double bag and seal loose ice to prevent melting ice from soaking the packing material. Place the ice outside the garbage bags containing the samples.

² Permissible packing materials are: a) (non-absorbent) bubble wrap or closed cell foam packing sheets; b) (absorbent) vermiculite. Organic materials such as paper, wood shavings (excelsior), and cornstarch packing "peanuts" will not be used.

- a. Wipe tape with a clean cloth or laboratory wipe which has been soaked with non-phosphate laboratory detergent solution to remove gross contamination. Rinse cloth in the solution and continue wiping until tape is clean.
- b. Wipe tape with a second clean, wet cloth (or lab wipe) to remove soap residues.
- c. Dry tape with a third cloth (or lab wipe) and rewind into case, or re-coil tape.

3.3.4 Drilling Rigs

All drilling rigs and associated equipment such as augers, drill casing, rods, samplers, tools, recirculation tank, and water tank (inside and out) will be decontaminated prior to site entry after over-the-road mobilization and immediately upon departure from a site after drilling a hole. Supplementary cleaning will be performed prior to site entry there is a likelihood that contamination has accumulated on tires and as spatter or dust enroute from one site to the next (see also Field Investigation Plan, § 6.3.7).

- a. Place contaminated equipment in an enclosure designed to contain all decontamination residues (water, sludge, etc.).
- b. Steam clean equipment until all dirt, mud, grease, asphaltic, bituminous, or other encrusting coating materials (with the exception of manufacturer-applied paint) have been removed.
- c. Water used will be taken from an approved source.
- d. Containerize, sample, characterize, and dispose of all decontamination residues properly.

3.3.5 HPLC-grade water Storage

Dedicated glass storage containers will be used solely for dispensing HPLC-grade water. New HPLC-grade water containers will be decontaminated as follows:

- a. Clean with hot tapwater from approved source and non-phosphate laboratory detergent while scrubbing the exterior and interior of the container with a stiff-bristled brush.
- b. Rinse thoroughly with approved water.
- c. Rinse with 0.01N Nitric acid.
- d. Rinse with approved water.
- e. Rinse thoroughly with HPLC-grade water.

Blot excess.

Analysis of Water and Wastes, March, 1983.

1 swirl gently, keeping the probes in the

Standard Methods for the Examination of Water and
Public Health Assn., American Water Works Assn., and Water

re after stabilization. Note any problems such

Blot excess.

additional samples.

er's specifications.

ection 3.3.1.4 "labware".

meter
id.

1 adjusted to pH 4 when the meter is not in
1 with deionized water and the protective cap
o not blot the electrode dry prior to putting

matter that can impair electrode response by
distilled water rinsing.

is may not apply to alternate manufacturers'

7.00 and one end point (pH 4.00 or 11.00)
two end points only.

pH Meter, .™ 11 pH meter, and .™ 12 -

- 3.1.4 Keep all equipment and supplies protected from gross contamination; use clean plastic sheeting. Keep the water level indicator probe in its protective case when not in use.

3.2 Operation

- 3.2.1 Sample the air in the well head for gross organic vapors by lifting the well cap only high enough for an organic vapor meter (PID or FID) probe to be entered into the well casing. This will indicate the presence of gross volatile contaminants as well as indicating potential sampler exposure.

Remove cap. Allow well to vent for 60 to 90 seconds. Resample headspace. Record both readings. If the second reading is lower than the first, use the second reading to determining whether respiratory protection will be required during subsequent water level and well depth determinations, and sampling. Note that all headspace sampling must be performed at arm's length and from the upwind side of the well if possible.

3.2.1.1 Refer to SOP 011, 023, or 024 as appropriate.

- 3.2.2 If non-aqueous phase liquid (NAPL) contamination is suspected ⁶, use an interface probe to determine the existence and thickness of NAPLs.

3.2.2.1 Open the probe housing, turn the probe on, and test the alarm. Slowly lower the probe into the well until the alarm sounds. A continuous alarm indicates a NAPL while an intermittent alarm indicates water. If a NAPL is detected, record the initial level (first alarm). Mark the spot by grasping the cable with the thumb and forefingers at the top of the casing. If a mark is present on the casing, use the mark as the reference point. If no mark is present, use the highest point on the casing as the reference point. Withdraw the cable sufficiently to record the depth.

3.2.2.2 Continue to slowly lower the probe until it passes into the water phase. Slowly retract the probe until the NAPL alarm sounds and record that level in the manner as described above.

3.2.2.3 Record the thickness of the LNAPL (see section 3.3.1).

~~3.2.2.4 Continue to slowly lower the interface probe through the water column to check for the presence of DNAPL.~~

⁶ Interface probes will be used in all wells for first round sampling, regardless of site history. If no NAPLs are detected during the first round of sampling, this step may be omitted during subsequent sampling events unless conditions such as site history or headspace vapors would indicate otherwise.

3.4 Calibration to a Gas Other Than Isobutylene

The HNu may be calibrated to any certified calibration gas. However, after calibration all subsequent instrument readings will be relative to the calibration gas used.

3.4.1 Calibrate according to procedure 3.3

3.4.2 Partially fill and flush to two times a gas bag (Tedlar recommended) with the certified National Institute of Standards and Technology (NIST) (formerly NBS) traceable calibration gas. Then fill the bag with one to three liters of the calibration gas. If the gas is toxic, this must be done in a fume hood.

3.4.3 Feed the calibration gas into the probe with the range set for the value of the gas. After five seconds, adjust the span control until the meter reads the value of the calibration gas.

3.4.4 Record the results of the calibration on the calibration/maintenance log and attach a new calibration sticker (if available) or correct the existing sticker to reflect the new calibration data. All subsequent readings will be relative to the new calibration gas.

3.5 Operation

3.5.1 Follow the start up procedure, operational check and calibration check (refer to 3.1).

3.5.2 Set the function switch to the appropriate range. If the concentration of gases or vapors is unknown, set the function switch to 0-20 ppm range. Adjust if necessary.

3.5.3 While taking care not to permit the HNu to be exposed to excessive moisture, dirt, or contaminants, monitor the work activity as specified in the Site Health and Safety Plan.

3.5.4 When the activity is completed or at the end of the day, carefully clean the outside of the HNu with a damp disposable towel to remove all visible dirt. Return the HNu to a secure area and place on charge. Place the instrument on charge after each use; the lead acid batteries cannot be ruined by over charging.

3.5.5 With the exception of the probe's inlet and exhaust, the HNu can be wrapped in clear plastic to prevent it from becoming contaminated and to prevent water from getting inside in the event of precipitation. If the instrument becomes contaminated, make sure to take necessary steps to decontaminate it. Call the Equipment Administrator if necessary; under no circumstances should and instrument be returned from the field in a contaminated condition.

3.6 Refer to SOP 3 and 16.

Check for this condition regularly to insure that the HNu is functioning properly. If the instrument is malfunctioning, call your respective equipment manager to arrange to have a fresh replacement.

4.1.2 Lamp eV Change

If different applications for the analyzer would require different eV lamps, separate probes, each with its own eV lamp, must be used. A single readout assembly will serve for any of the probes (9.5, 10.2 and 11.7 eV). A change in probe will require resetting of the zero control and recalibrating the instrument. The 11.7 eV lamp will detect more compounds than either of the two lower eV lamps. However, the 11.7 eV probe needs more frequent calibration, it burns out much faster than the lower eV lamps.

5.0 Precautions

- 5.1 The HNu PI-101 and HW-101 are designed to sample air or vapors only. DO NOT allow any liquids or low boiling vapors to get into the probe or meter assembly.
- 5.2 High concentrations of any gas can cause erroneous readings. High humidity can also cause the instrument readings to vary significantly from the actual concentration of gases or vapors present. This is true even through the HNu cannot react to water vapor.
- 5.3 High humidity, dust, and exposure to concentrations of low boiling vapors will contaminate the ion chamber, causing a steady decrease in sensitivity.
- 5.4 Continued exposure to ultraviolet light generated by the light source can be harmful to eyesight. If a visual check of the UV lamp is performed: Do not look at the light source from a distance closer than 6 inches with unprotected eyes. Use eye protection (UV-blocking sunglasses or safety glasses). Only look briefly - never more than about 2 seconds.
- 5.5 Place the instrument on charge after each use; the lead batteries cannot be ruined by over charging.
- 5.6 If at any time the instrument does not check out or calibrate properly in the field, the equipment manager is to be notified immediately and a replacement provided for the malfunctioning instrument. Under no circumstances should field work requiring continuous air monitoring for organic vapors and/or gases be done with a malfunctioning HNu, without a HNu or an approved comparable instrument.

6.0 References

Manufacturer's Equipment Manual(s).

- 3.5.2 Peristaltic, gas-lift, and centrifugal pumps can cause volatilization, produce high pressure differentials, and can result in variability in the analysis of some analytes of interest. These types of pumps shall not be used to purge or sample wells.
- 3.5.3 To prevent ground-water from cascading down the sides of the screen in to an open hole, thereby aerating the sample, purge rates will closely match recharge rates. If the static water level is within the casing, the initial purge rates may be set high enough to lower the water level to the top of the screen, then reduced to maintain that level.
- 3.5.4 Purging will be accomplished with either a submersible pump, a low-flow (submersible or bladder) pump, or bailer. The choice of bailer or pump will be based on depth to water table, volume to be purged, and permeability of the aquifer. If the well recharges rapidly and/or has greater than 20 gallons (estimated EV) to be purged, water may be removed with a submersible pump or a low-flow pump. If the well recharges slowly and/or has less than 20 gallons to be purged, water will be removed with a bailer or a low-flow pump.
- 3.5.5 Purging will be accomplished with as minimal disturbance to the surrounding formation as possible.
- 3.5.6 Purge water will be containerized¹² on site until analysis of samples is completed. At that time, if the samples are non-hazardous, the water may be disposed of through the waste water treatment plant on-post. If the purge water is found to be hazardous, it will be disposed of as hazardous waste in a licensed TSDF.
- 3.5.7 If the water level is within the screened interval and the well recharge rate is less than 0.1 L/min purge the well using a low-flow pump as follows:
- 3.5.7.1 Draw the water down to within 1 foot of the top of the pump.
 - 3.5.7.2 Allow the well to recover.
 - 3.5.7.3 Check and record field parameters (§ 3.7.3).

¹² If, after two rounds of quarterly samples, the water has proven to be uncontaminated, and the purge volume does not exceed 10,000 Gal/day, the purge water may be discharged on the surface, at least 50 ft downhill from the well. If the water is contaminated but does not exceed 100 ppm total VOC, and other contaminants are non toxic to aquatic life as defined in COMAR 26.08.02.03-2, Table 1, MDE may be petitioned on a case-by case basis for a waiver for surface discharge. This letter will be drafted by the contractor for DSHE signature.

- 3.5.7.4 Repeat steps 3.5.7.1 through 3.5.7.3 then collect samples for metals analysis only¹³.
- 3.5.7.5 Note the event in the field log book, and report the problem to the APG project manager. If this extremely low recharge problem consistently occurs in a given well, the well may be considered for re-development and/or replacement.
- 3.5.7.6 If adjacent wells have elevated VOC levels, additional soil gas surveys will be considered in the vicinity of the low recharge well to help determine the need for replacement.

3.6 Purging and Sampling With Bailers

- 3.6.1 Bailers may be used for both purging and sampling wells if: a) the well recharge rate is less than 4 L/min, b) depth to the water table is less than 50 ft, and c) less than 20 gal are to be purged (5 EV < 20 gal)¹⁴.
- 3.6.2 When purging with a bailer, either a PVC, PTFE, or stainless steel bailer may be used. The bailer will be attached to either a spool of PTFE-coated stainless steel cable or polypropylene rope. If using cable, attach it to the bailer using stainless steel cable clamps. Thoroughly decon the cable after each use, prior to rewinding cable onto spool. Cable clamps and raw cable ends may serve to trap contamination. Exercise particular caution in deconning these areas. If using rope, attach the rope to the bailer using a bowline knot, dispense the needed length (a few feet more than the well depth) and cut the remainder away, then, at the end opposite the bailer, make a slip knot and place it around the well casing or protective posts to prevent losing the bailer and rope down the well. The polypropylene rope will be not reused, it will be properly disposed of. Either type of bailer will be repeatedly lowered gently into the well until it fills with water, removed, and the water will be discharged into an appropriate container until purging is complete. Care must be taken not to unduly agitate the water, as this tends to aerate the sample, increase turbidity, makes stabilization of required parameters (3.6.3) difficult to achieve, and generally prolongs purging.

¹³ Analyte losses due to volatilization in a drained well are too high for valid VOC sampling (McAlary and Barker, 1987).

¹⁴ These numbers are based on the following assumptions: 1) In purging, it is preferable to remove water at approximately the recharge rate. 2) Four L/min is estimated as the approximate maximum rate at which water can be removed with a bailer from depths of 20-50 feet. 3) Twenty gallons is estimated to be at the limit of the sampler's endurance, at which point fatigue and sloppiness of technique begin.

3.6.3 After purging 2 EV, obtain a sample of groundwater and measure the following stabilization parameters: temperature (SOP 009), conductivity (SOP 012), pH (SOP 008), turbidity (SOP 036), redox potential (Eh) (SOP 038), and dissolved oxygen level (SOP 037) at each successive half-well volume. When three of these stabilization parameters are in agreement within approximately 10% in three consecutive half-well volume samples, sufficient water has been purged from the well. The results of these tests should be recorded in the sampling logbook. Should these parameters not reach agreement, no more than five well volumes will be purged.

3.6.4 Immediately upon completion of purging, collect samples for laboratory analysis using a PTFE bailer on a PTFE-coated stainless steel cable. The bailer will be equipped with double check valve top and controlled flow bottom discharge attachments for VOC sampling (40-mL vials), and top discharge attachment for collecting larger samples (1-L bottles).

3.6.5 Slowly, so as not to agitate the water, lower the bailer into the well, using a spool of PTFE-coated cable. Allow bailer to fill, withdraw smoothly. Refill bailer as needed.

3.6.5.1 Please see footnote 2. If the controlled flow bottom discharge attachment is used for VOC sampling, attach it to the bottom of the bailer. Using the stopcock valve on the bailer to control the flow, fill sample vials as described above in § 3.3.8.

3.6.5.2 Remove check valve top and pour unfiltered sample into inorganics sample bottles.

3.6.5.3 Collect filtered samples as described in § 3.3.9(above).

3.6.6 Decon bailer and cable in accordance with SOP 005 § 3.3.1.1

3.7 Purging With Pump, Sampling With Bailer

3.7.1 If the recharge rate of the well is greater than 30 L/min, or the water level is deeper than 50 ft, or more than 20 gal or purge water will be generated (5 EV > 20 gal), then purging and sampling may be accomplished using a submersible pump / bailer combination.

3.7.2 When purging with a pump, gradually lower the intake until it is submerged within the screened interval. Lower an electronic water level probe to the top of the screen (as determined from completion records) to the monitor water level, start pump, and slowly lower the pump as the water level continues to fall. Care should

be exercised to lower the water column to the top of the screened interval (water level probe will stop beeping) but not below the top of the screen if possible. This will ensure that the stagnant layer has been removed, but should minimize the detrimental effects of over pumping the well. Secure hose(s) and/or power cord to casing and place discharge hose into the proper container, downhill and as far away from the well as possible. Determine and record the discharge rate.

Discharge rate = volume of container/time to fill container

The discharge rate will be established at approximately equal to or just greater than the well's recharge rate (determined from well development). If well development records are incomplete, recharge rate can be determined by monitoring the rise/fall of the water level within the casing as one purges the well. If the water level is static at a given pumping rate, but fluctuates up or down as pumping rate is decreased or increased, the pumping rate at which the water level is static is the recharge rate.

- 3.7.3 After purging 2 EV, obtain a sample of groundwater and measure the following stabilization parameters: temperature, conductivity, pH, turbidity, redox potential (Eh), and dissolved oxygen level at each successive half-well volume. When three of these stabilization parameters are in agreement within approximately 10% in three consecutive half-well volume samples, sufficient water has been purged from the well. The results of these tests should be recorded in the sampling logbook. Should these parameters not reach agreement, no more than five well volumes will be purged.
- 3.7.4 Immediately upon completion of purging, collect samples for laboratory analysis using a PTFE bailer on a PTFE-coated stainless steel cable. The bailer will be equipped with double check valve top and controlled flow bottom discharge attachments for VOC sampling (40-mL vials), and top discharge attachment for collecting larger samples (1-L bottles). Filtration of metals samples will be accomplished using either an in-line filter attached to the bottom of the bailer, or a funnel and appropriate filter (see § 3.3.9 above).
- 3.7.5 Slowly, so as not to agitate the water, lower the bailer into the well, using a spool of PTFE-coated cable. Allow bailer to fill, withdraw smoothly, fill sample containers as described above in § 3.6.5
- 3.7.6 Decon bailer and cable in accordance with SOP 005 § 3.3.1.1. Decon pump in accordance with SOP 005 § 3.3.1.2.

3.8 Purging and Sampling With Low-Flow Pump

To obtain representative samples, subsurface disturbances should be kept to a minimum, thereby preventing sample alteration due to sampling actions. The reasoning behind the use

August, 1993

of low-flow pumps to purge and sample monitoring wells is that these pumps minimize physical disturbance (turbulence) at the sampling point and chemical changes (aeration) in the medium. For these reasons, the low-flow pump is the preferred method for both purging and sampling in most cases. For the purposes of this SOP, "low-flow pumps" are defined as either dedicated bladder pumps or variable speed submersible pumps. Practical operational flow rates for these sampling devices range from 0.1 L/min to 30 L/min.

3.8.1 Low-flow pumps may be used for purging and sampling any well having recharge greater than 0.1 L/min, which is the practical lower limit of pump performance. Below that pumping rate, pump inefficiencies and/or overheating may alter the physical and chemical properties of the sample. If the pump is continuously operated at sampling rates higher than the well recharge rate, the water level will be lowered in the well, possibly allowing aeration of the sample which is unacceptable sampling procedure. Low-flow pumps are suitable for sampling wells with recharge rates lower than 0.1 L/min if precautions are taken to avoid aeration of the sample.

3.8.2 Low flow submersible pumps will be used as follows:

3.8.2.1 Lower the pump into the well, slowly so as not to agitate the water, until the pump is at the mid-point of the screened interval or the mid-point of the water column if the static water table lies below the top of the screen¹⁵

3.8.2.2 Attach the pump's umbilical cord (which will consist of power cord and sampling tubing) to the protective casing, or lock the cord spool so that the pump cannot move vertically in the well during sampling.

3.8.2.3 Lower the water level probe into the well behind the pump until it just touches water. This will allow the sampler to monitor the water level while purging and sampling, and prevent the inadvertent drying of the well.

¹⁵ This assumes a 10-ft. screened interval. If the screened interval is greater than 10-ft., multiple samples should be taken as follows:

L If the screen is 10 - 12 ft., sample the center of the water column, as outlined above.

L If the screen is longer than 12-ft., and the water column is 10-ft or less, sample the center of the water column.

L If the screen is longer than 12-ft., and the water column fills the screen, or extends above the screen, sample at 1/3 and 2/3 the height of the water column, or about every 6-ft.

- 3.8.2.4 Begin purging at the pump's lowest setting, then gradually increase rate ¹⁶ until the pumping rate matches the aquifer recharge rate. If the water level is above the top of the screen, the pumping rate may be allowed to slightly exceed recharge rate, lowering the water level to no less than 1 foot above the screen, then reduced until it matches recharge rate and purging continued. If the water level is below the top of the screen, always keep the purge rate lower than well's recharge rate.
 - 3.8.2.5 Monitor stabilization parameters listed in § 3.6.3 beginning immediately, using an in-line monitoring system. Record parameters regularly, at a rate of one set of parameters per each 1-3 liters of water removed from the well. When these parameters stabilize to within 10% over 3 consecutive readings, reduce ¹⁷ flow rate to 0.1 L/min (if needed) and begin collecting VOC samples directly from the discharge line.
 - 3.8.2.6 If the well recharges at a rate less than 0.1 L/min, purge until the water level is even with the top of the screen, allow the well to recover and sample immediately.
 - 3.8.2.7 Remove and decon water level probe (SOP 005 § 3.3.1.5) and pump (SOP 005 § 3.3.1.2).
- 3.8.3 The length of tubing used in conjunction with the low-flow pump will be appropriate to the depth of the well (*i.e.* A 100 ft roll of tubing may not be used in sampling a 30 ft well. A 50 ft roll would be used instead, thereby generating less decon solution, and providing less opportunity for physical and chemical changes in the sample due to contact with the spooled tubing (see § 3.8.4)). This means that the contractor will have on hand: a) spools of varying length (*e.g.* 25, 50, 75, and 100 ft spools) or b) several short *e.g.* 10 ft lengths of tubing with a secure means of connecting them end-to-end.
- 3.8.4 When a sampling event occurs during summer months, in full sun, shade will be provided for the spooled tubing. Otherwise the tubing will be an effective water heater, warming the ground-water sample, creating the potential for volatilization of organics.

¹⁶ Some sources indicate that the pumping rate should not exceed 1 L/min, with 0.5 L/min being preferable. The optimal purge rate is highly aquifer dependent, and may range from less than 0.5 L/min to greater than 10 L/min. The purge rate for a given well will, therefore, be a field decision, based on well development, purge, and sampling records rather than SOP mandate.

¹⁷ Sampling should occur at the same rate as purging as long as aeration of sample does not occur.

- 3.8.5 Spooled tubing will be monitored to ensure that no air bubbles are trapped at the top of a coil. Trapped air bubbles can enhance volatilization of organics.
- 3.8.6 If a dedicated bladder pump is used, follow steps 3.8.2.3 through 3.8.2.5 for purging and sampling.

4.0 Maintenance

Refer to manufacturer's requirements for maintenance of pumps and generators.

5.0 Precautions

Refer to the HASP for appropriate PPE.

6.0 References

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**STANDARD OPERATING PROCEDURE 014
COLLECTION OF PRODUCTION WELL SAMPLES**

1.0 Scope and Application

The purpose of this standard operating procedure is to delineate protocols for the collection of groundwater samples from production wells. This protocol will allow for collection of samples from both active production wells (§ 3.4) and inactive production wells (§ 3.10).

2.0 Material

- a. Conductivity meter
- b. Temperature meter
- c. pH meter
- d. Turbidity meter
- e. ORD probe
- f. Dissolved oxygen meter
- g. Sample bottles and labels
- h. Logbook or field parameter form

3.0 Procedure

- 3.1 Upon arrival at the well site, immediately set up and organize the sampling and ancillary equipment. If needed, due to muddy or contaminated ground and/or remoteness from sampling vehicle place plastic sheeting at, or around the sampling location as conditions warrant. Exercise caution not to step on and contaminate the sheeting.
- 3.2 If the well is remote from the sampling vehicle set up the filtration equipment and place sample containers on the plastic sheet, uphill of the sampling location.
- 3.3 If a pump is to be used for filtration, situate the portable generator on level ground approximately 15 feet away from and downwind from the sampling location. All generator maintenance (oil and fueling) is to be preformed off site.
- 3.4 If the well is currently in use. As close as possible to the well, open a tap to a high flow rate and allow the well to purge.
- 3.5 Obtain a sample of groundwater for temperature, conductivity, ORD, DO, turbidity, and pH measurements. Record values in sampling logbook.
- 3.6 Take samples for physical stabilization (water quality) parameters every 5 minutes during the well purging process.

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- 3.7 Allow the well to purge until the water quality parameters of pH, temperature, conductivity, turbidity, oxidation-reduction potential, and dissolved oxygen measurements stabilize within 10% in three consecutive 5-minute sampling periods, purging will be considered complete and sampling may proceed.
- 3.8 Slow water flow rate to a trickle.
- 3.9 For procedures for collecting samples, with the exception of the sample source being a bailer: Refer to SOP 013 3.2.1;3.5.1 and 3.5.3 through 3.5.8.
- 3.10 If the well is not currently in use. Use a pump and bailer, or low-flow pump for sampling. Refer to SOP 013 for purging and sampling protocol.
- 3.11 decontaminate equipment
- 3.12 Refer to SOP 1-5, 13, and 16.

4.0 Maintenance

Not applicable.

5.0 Precautions

Not applicable.

6.0 References

USATHAMA. 1990. Installation Restoration Quality Assurance Program, December 1985, 1st edition, March 1987, 2nd edition).

**STANDARD OPERATING PROCEDURE 015
DOCUMENT CONTROL SYSTEM**

1.0 Scope and Application

The purpose of this standard operating procedure is to delineate protocols for identifying and storing a complete set of documents relating to project tasks. Each document will receive a unique identification number made up of elements describing the document.

2.0 Materials

Not applicable.

3.0 Procedure

3.1 Each project-related document will be given to the Document Control Officer.

3.2 The Document Control Officer will record information for each document on a Document Control Sheet which will be retained as a backup record.

3.3 The information from each Document Control Sheet will be maintained in a computer database.

3.4 The individual Document Control Number will be entered on the Document Log Sheet and will be written on the document.

3.5 The storage location for each document will be recorded on the Document Control Logsheet and the documents will be stored in the recorded location.

3.6 The database file will be backed up on a regular basis to prevent accidental loss of the data.

4.0 Maintenance

Not Applicable.

5.0 Precautions

None.

6.0 References

None.

- h. **SITE TYPE:** record the abbreviation appropriate for where the sample was taken. Correct abbreviations can be found on pages 18-21 of the IRDMS User's Guide for chemical data entry. This entry must match the Site Type on the map file form.
- i. **SITE ID:** record a code up to 10 characters or numbers which is unique to the site.
- j. **FIELD SAMPLE NUMBER:** record a code specific for the sample.
- k. **DATE:** enter the date the sample was taken.
- l. **TIME:** enter the time (12 hour or 24 hour clock acceptable as long as internally consistent) the sample was taken.
- m. **AM PM:** circle "AM" or "PM" to designate morning or afternoon (12 hour clock).
- n. **SAMPLE PROG:** record "GQA" (Groundwater Quality Assessment) or other appropriate sample program.
- o. **DEPTH (TOP):** record the total depth sampled.
- p. **DEPTH INTERVAL:** record the intervals at which the plug will be sampled.
- q. **UNITS:** record the units of depth (feet, meters)
- r. **SAMPLE MEASUREMENTS:** check the appropriate sampling method.
- s. **CHK:** check off each container released to a laboratory.
- t. **ANALYSIS:** record the type of analysis to be performed on each sample container.
- u. **SAMPLE CONTAINER:** record the sample container type and size.
- v. **NO.:** record the number of containers.
- w. **REMARKS:** record any remarks about the sample
- x. **TOTAL NUMBER OF CONTAINERS FOR SAMPLE:** record the total number of containers.
- y. **SITE DESCRIPTION:** describe the location where the sample was collected.

- z. **SAMPLE FORM:** record the form of the sample (i.e., clay, loam, etc.) using The Unified Soil Classification System (USCS).
 - aa. **COLOR:** record the color of the sample as determined from standard Munsell Color Charts.
 - bb. **ODOR:** record the odor of the sample or "none". See SOP 001 § 5.0 "Precautions".
 - cc. **PID (HNu):** record the measured PID(HNu) values.
 - dd. **UNUSUAL FEATURES:** record anything unusual about the site or sample.
 - ee. **WEATHER/TEMPERATURE:** record the weather and temperature.
 - ff. **SAMPLER:** record your name.
2. **Map File Form (refer to form 16-c)**
- a. The mapfile logbook form will be located on the reverse of the field parameter logbook form, or on an adjoining page of the field logbook (if level book is used)
 - b. **SITE ID:** record the Site ID from the field parameter form.
 - c. **POINTER:** record the field sample number for the sample being pointed to.
 - d. **DESCRIPTION/MEASUREMENTS:** describe the location where the sample was taken, along with distances to landmarks.
 - e. **SKETCH/DIMENSIONS:** diagram the surroundings and record the distances to landmarks.
 - f. **MAP REFERENCE:** record which U.S.G.S. Quad Map references the site.
 - g. **COORDINATE DEFINITION:** write the compass directions the X- and Y-Coordinates of the map run.
 - h. **COORDINATE SYSTEM:** write "UTM" (Universal Transverse Mercator).
 - i. **SOURCE:** record the 1 digit code representing the Map Reference.
 - j. **ACCURACY:** give units (*e.g* write "1-M" for 1 meter).

- k. X-COORDINATE: record the X-Coordinate of the sample site location.
- l. Y-COORDINATE: record the Y-Coordinate of the sample site location.
- m. UNITS: record the units map sections are measured in.
- n. ELEVATION REFERENCE: record whether topography was determined from a map or a topographical survey.
- o. ELEVATION SOURCE: record the 1 digit code representing the elevation reference.
- p. ACCURACY: record the accuracy of the map or survey providing the topographical information.
- q. ELEVATION: record the elevation of the sampling site.
- r. UNITS: write the units in which the elevation is recorded.
- s. SAMPLER: write your name.

B. Surface Water Logbook (refer to form 16-b and c)

1. Field Parameter Logbook

- a. CAL REF: record the calibration reference for the pH meter.
- b. pH: record the pH of the sample.
- c. TEMP: record the temperature of the sample in degrees Celsius.
- d. COND: record the conductivity of the water.
- e. For all other sections, see 3.B.1.

2. Map File Form - See 3.A.2.

C. Groundwater Logbook (refer to form 16-b and d)

1. Field Parameter form - See 3.B.1.

2. Map File form (refer to form 16-c)

- a. WELL NO. OR ID: record the abbreviation appropriate for where the sample was taken. Correct abbreviations can be found on pages 18-21 of the IRDMS User's Guide for chemical data entry.

- b. SAMPLE NO.: record the reference number of the sample.
- c. WELL/SITE DESCRIPTION: describe the location where the sample was taken, along with distances to landmarks.
- d. X-COORD and Y-COORD: record the survey coordinates for the sampling site.
- e. ELEV: record the elevation where the sample was taken.
- f. UNITS: record the units the elevation was recorded in.
- g. DATE: record the date in the form MM/DD/YY.
- h. TIME: record the time, including a designation of AM or PM.
- i. AIR TEMP.: record the air temperature, including a designation of C or F (Celsius or Fahrenheit).
- j. WELL DEPTH: record the depth of the well in feet and inches.
- k. CASING HT.: record the height of the casing in feet and inches.
- l. WATER DEPTH: record the depth (underground) of the water in feet and inches.
- m. WELL DIAMETER: record the diameter of the well in inches.
- n. WATER COLUMN HEIGHT: record the height of the water column in feet and inches.
- o. SANDPACK DIAM.: record the diameter of the sandpack. Generally, this will be the same as the bore diameter.
- p. EQUIVALENT VOLUME OF STANDING WATER: use one of the following equations, to determine one equivalent volume (EV):

1 EV = volume in casing + volume in saturated sand pack. Or to restate:

$$1 \text{ EV} = (\pi R_w h_w + 0.30\pi(R_s^2 - R_w^2)h_s) * (0.0043)$$

where: R_s = radius of sandpack in inches
 R_w = radius of well casing in inches
 h_s = height of sandpack in inches
 h_w = water depth in inches

$$0.0043 = \text{gal/in}^3$$

and filter pack porosity is assumed as 30%

– OR –

$$\text{Volume in casing} = (0.0043 \text{ gal/in}^3)(P)(12 \text{ in/ft})(R_c^2)(W_h)$$

where R_c = radius of casing in inches, and
 W_h = water column height in feet

$$\text{Vol. in sandpack} = (0.0043 \text{ gal/in}^3)(P)(12 \text{ in/ft})(R_b^2 - R_c^2)(W_h)(0.30)$$

(if W_h is less than the length of the sandpack),

– PLUS –

$$\text{Vol. in sandpack} = (0.0043 \text{ gal/in}^3)(P)(12 \text{ in/ft})(R_b^2 - R_c^2)(S_h)(0.30)$$

(if W_h is greater than the length of the sandpack).

where R_b = radius of the borehole, and
 S_h = length of the sandpack.

Show this calculation in the comments section.

- q. VOLUME OF BAILER OR PUMP RATE: record bailer volume or pump rate.
- r. TOTAL NUMBER OF BAILERS OR PUMP TIME: record the number of bailers required to remove 3 equivalent volumes (EV) of water from the well or the total purge time and volume as applicable.
- s. WELL WENT DRY? write "YES" OR "NO."
- t. NUMBER OF BAILERS OR PUMP TIME: record the number of bailers or pump time which made the well go dry.
- u. VOLUME REMOVED: record the volume of water (gal) removed before the well went dry.
- v. RECOVERY TIME: record the time required for the well to refill.
- w. PURGE AGAIN?: answer "YES" or "NO."
- x. TOTAL VOL. REMOVED: record the total volume of water (in gallons) removed from the well.
- y. CAL REF.: record the calibration reference for the pH meter.

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- z. TIME: record time started (INITIAL T(0)), 2 times DURING the sampling and the time sampling ended (FINAL).
- aa. pH: record the pH at start of sampling (INITIAL), twice DURING the sampling and at the end of sampling (FINAL).
- bb. TEMP: record the water temperature (Celsius) at the start of sampling, twice DURING the sampling and at the end of sampling (FINAL).
- cc. COND: record the conductivity of the water at the start of sampling, twice DURING the sampling and at the end of sampling (FINAL).
- dd. D.O.: record the dissolved oxygen level in the water at the start of sampling, twice DURING the sampling and at the end of sampling (FINAL).
- ee. TURBIDITY: record the readings from the turbidity meter (nephelometer) and units at the start of sampling, twice DURING the sampling and at the end of sampling (FINAL).
- ff. ORD: record the oxidation/reduction (RedOx) potential of the water sample at the start of sampling, twice DURING the sampling and at the end of sampling (FINAL).
- gg. HEAD SPACE: record any positive readings from organic vapor meter reading taken in well headspace prior to sampling.
- hh. NAPL: Record the presence and thickness of any non aqueous phase liquids (LNAPL and DNAPL)
- ii. COMMENTS: record any pertinent information not already covered in the form.
- jj. SIGNATURE: sign the form.

D. Field Calibration Forms (refer to form 16-e)

- a. Record time and date of calibration.
- b. Record calibration standard reference number.
- c. Record meter I.D. number
- d. Record initial instrument reading, recalibration reading (if necessary), and final calibration reading on appropriate line.
- e. Record value of reference standard (as required).

f. **COMMENTS:** Record any pertinent information not already covered on form.

g. **SIGNATURE:** sign form.

4.0 MAINTENANCE

Not Applicable.

5.0 PRECAUTIONS

None.

6.0 REFERENCES

User's Guide to the Contract Laboratory Program, USEPA, July, 1984.

FIELD PARAMETER/LOGBOOK FORM 16-a
 SOIL AND SEDIMENT SAMPLES

HIGH CONCENTRATION EXPECTED? _____ HIGH HAZARD? _____

INSTALLATION/SITE _____ AREA _____

INST CODE _____ FILE NAME _____

SITE TYPE _____ SITE ID _____

FIELD SAMPLE NUMBER _____

DATE (MM/DD/YY) ____/____/____ TIME _____ AM PM SAMPLE PROG. _____

DEPTH (TOP) _____ DEPTH INTERVAL _____ UNIT _____

SAMPLING METHOD:
 SPLIT SPOON _____ AUGER _____ SHELBY TUBE _____ SCOOP _____ OTHER _____

CHK	ANALYSIS	SAMPLE CONTAINER	NO.	REMARKS
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____

TOTAL NUMBER OF CONTAINERS FOR SAMPLE _____

DESCRIPTION OF SITE AND SAMPLE CONDITIONS

SITE DESCRIPTION : _____

SAMPLE FORM _____ COLOR _____ ODOR _____

PID (HNU) _____ UNUSUAL FEATURES _____

WEATHER/TEMPERATURE _____

SAMPLER _____

MAP FILE LOGBOOK FORM 16-c
SURFACE WATER, SOIL, AND SEDIMENT SAMPLES

SITE ID _____ POINTER _____

DESCRIPTION/MEASUREMENTS _____

SKETCH/DIMENSIONS :

MAP REFERENCE _____

COORDINATE DEFINITION (X is _____ Y is _____)

COORDINATE SYSTEM _____ SOURCE _____

ACCURACY _____

X-COORDINATE _____ Y-COORDINATE _____ UNITS _____

ELEVATION REFERENCE _____

ELEVATION SOURCE _____ ACCURACY _____

ELEVATION _____ UNITS _____

SAMPLER _____

MAP FILE AND PURGING LOGBOOK FORM 16-d
GROUNDWATER SAMPLES

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WELL COORD. OR ID _____ SAMPLE NO. _____

WELL/SITE DESCRIPTION _____

X-COORD. _____ Y-COORD. _____ ELEV. _____ UNITS _____

DATE ____ / ____ / ____ TIME _____ AIR TEMP. _____

WELL DEPTH _____ FT. _____ IN. CASING HT. _____ FT. _____ IN.

WATER DEPTH _____ FT. _____ IN. WELL DIAMETER _____ IN.

WATER COLUMN HEIGHT _____ FT. _____ IN. SANDPACK DIAM. _____ IN.

EQUIVALENT VOLUME OF STANDING WATER _____ (GAL) (L)

VOLUME OF BAILER _____ (GAL) (L) or PUMP RATE _____ (GPM) (LPM)

TOTAL NO. OF BAILERS (5 EV) _____ or PUMP TIME _____ MIN.

WELL WENT DRY? [Yes] [No] NUM. OF BAILERS _____ or PUMP TIME _____

VOL. REMOVED _____ (GAL) (L) RECOVERY TIME _____

PURGE AGAIN? [Yes] [No] TOTAL VOL. REMOVED _____ (GAL) (L)

DATE & TIME	QUANTITY REMOVED	TIME REQ'D	pH	Cond	Temp	ORD	Turb	DO	Character of water (color / clarity / odor / partic.)
(before)									
(during)									
(during)									
(during)									
(after)									

COMMENTS _____

SIGNATURE _____

EXAMPLE
 FIELD CALIBRATION FORM 16-e
 FOR
 pH, CONDUCTIVITY, TEMPERATURE, TURBIDITY,
 ORD, AND DISSOLVED OXYGEN METERS

INITIAL CALIBRATION	FINAL CALIBRATION
DATE:	DATE:
TIME:	TIME:

pH METER CALIBRATION

CALIBRATION STANDARD REFERENCE NO: _____

METER ID

pH STANDARD	INITIAL READING	RECALIB. READING	FINAL READING
7.0			
10.0			
4.0			

CONDUCTIVITY METER CALIBRATION

CALIBRATION STANDARD REFERENCE NO: _____

METER ID

COND. STANDARD	INITIAL READING	RECALIB. READING	FINAL READING

TEMPERATURE METER CALIBRATION

METER ID

TEMP. STANDARD	INITIAL READING	RECALIB. READING	FINAL READING
ICE WATER			
BOILING WATER			
OTHER			

EXAMPLE
FIELD CALIBRATION FORM 16-e
FOR
pH, CONDUCTIVITY, TEMPERATURE, TURBIDITY,
ORD, AND DISSOLVED OXYGEN METERS

TURBIDITY METER CALIBRATION

CALIBRATION STANDARD REFERENCE NO: _____

METER ID _____

STANDARD	INITIAL READING	RECALIB. READING	FINAL READING

ORD METER CALIBRATION

CALIBRATION STANDARD REFERENCE NO: _____

METER ID _____

STANDARD	INITIAL READING	RECALIB. READING	FINAL READING

DISSOLVED OXYGEN METER CALIBRATION

CALIBRATION STANDARD REFERENCE NO: _____

METER ID _____

STANDARD	INITIAL READING	RECALIB. READING	FINAL READING

COMMENTS _____

SIGNATURE _____

STANDARD OPERATING PROCEDURE 017 GROUND PENETRATING RADAR SURVEY

1.0 PURPOSE

This guideline provides a description of, and technical management guidance on the use of Ground Penetrating Radar surveys during hazardous waste site investigations at U.S. Army installations.

2.0 SCOPE

This guideline provides a description of and the principles of operation, instrumentation, applicability, and implementation of ground penetrating radar (GPR) geophysical surveys. GPR surveys can be used to map subsurface stratigraphy; to rapidly locate buried metallic objects, such as pipes, drums, ordnance, and tanks; to locate buried waste disposal structures; to locate voids within the subsurface; and in some cases can directly detect contaminants.

The document is intended to be used by a site manager to develop an understanding of the method sufficient to permit work planning and scheduling, resource planning, subcontractor procurement and evaluation, and manipulation and use of the technical data during remedial investigations and feasibility studies. This guidance is not intended to provide a detailed description of methodology and operation, which will vary between sites, between target depths and characteristics, and between instruments. The description focuses on methods and equipment that are readily available and typically applied; it is not intended to provide a complete discussion of the state of the art. Specialized expertise is required during both planning and execution of geophysical surveys to develop a target-specific, site-specific, and instrument-specific scope of work, with detailed operating procedures, which will best achieve the goals of the survey.

3.0 DEFINITIONS

Dielectric Constant. The measure of the ability of a material to store a charge when an electromagnetic field is applied. This is the measure of the property which determines the reflection, adsorption, and transmission characteristics of the radar signal in the subsurface. Dielectric constants for common materials are listed in Table 017-1.

Ground Penetrating Radar (GPR) Survey. A geophysical survey technique where an (electromagnetic) radar pulse is transmitted into the subsurface and the reflected pulse is measured and recorded.

Penetration or Exploration Depth. The maximum depth at which an object of interest can be detected using a given GPR configuration. The penetration depth is a function of the electrical properties of the subsurface materials and of the GPR signal strength and antenna design.

Radar Trace. The display of reflected signal strength on a graph of lateral distance along the ground-vs-travel time.

Transceiver. Antenna design consisting of a transmitter mounted on or within the antenna - also known as a monostatic configuration. A bistatic antenna configuration consists of the transmitter in a separate housing from the antenna.

Travel Time. The time required for a radar signal to travel from the antenna to a target, reflect, and return to the antenna. Travel time is a function of the depth of the target and the electromagnetic characteristics of the subsurface.

4.0 RESPONSIBILITIES

Site Manager. Responsible for the scoping of geophysical surveys during development of the work plan, with the help of the RI leader, site geologist, and site geophysicist.

Site Geophysicist. As a specialist in this field, the site geophysicist plays a central role in determining the appropriateness of these techniques for providing necessary data. Field work for these surveys is supervised by the site geophysicist, with support from geophysical technical specialists and other personnel as needed. Data reduction and interpretation are performed by the site geophysicist or technical specialists.

Field Operations. Leader responsible for the overall management and coordination of the field work and enforcement of proper work and Health and Safety practices - including coordination, observation, or supervision of Explosive Ordnance Disposal (EOD) or military personnel, subcontractors, or co-contractors as required.

5.0 THEORY AND PRINCIPLES OF OPERATION

5.1 Description of the Ground Penetrating Radar (GPR) Method

Commercially-available GPR units operate on the principle of time-domain reflectometry, in which the difference in strength and the time delay between a transmitted electromagnetic pulse and its reflection from an object are measured. The time delay, t , is directly related to the propagation velocity of the electromagnetic waves, v , and to the distance between the transmitter and the subsurface object or reflector, D , as follows:

$$t = \frac{2D}{v}$$

Because GPR antenna are generally placed near the ground surface, the distance, D , corresponds to the depth of buried targets that reflect the radar signals.

The strength of a radar signal is a complex function of the distance traveled through the medium and the dielectric constant, the magnetic permeability, and the electrical conductivity of the medium. Radar signals are attenuated rapidly in materials with high dielectric constants. The attenuation of radar signals in subsurface media is dependent on their mineralogy and the water content. Thus, materials such as dry sands and gravels are least absorptive of radar signals, whereas wet clays are highly absorptive. The absorptive properties of the medium limits the penetration depth, i.e., the depth at which targets may be detected. The strength of a radar reflection is also a function of the composition, size shape, and depth of the target. Reflections are strong not only from objects exhibiting large difference in dielectric constant from the surrounding medium, but also which are large in size compared to the radar signal wave length.

The GPR repetitively transmits very short-duration (typically 5 to 10 nanosecond) pulses of high-frequency (typically 80 MHz to 1 GHz) electromagnetic energy through an antenna

that is moved along the ground surface at a constant speed. Reflected pulses are detected by the same antenna at a location corresponding to the distance traveled by the antenna during the transmission and reflection of the pulse, at which point another pulse is transmitted. At a typical antenna speed of 2 miles per hour (3 feet per second), a complete pulse transmit/receive cycle occurs about every 2 inches along the path of the antenna. GPR antenna may have either a monostatic or bistatic configuration. In the monostatic configuration, the antenna is a transceiver that utilizes a fast acting switch changing it to a receiving antenna immediately following pulse transmission and back to transmitting antenna for generation of the next pulse. The bistatic configuration utilizes separate transmitter and receiver antennas. The received signal is transmitted to the central control unit where the initial signal processing takes place and the pulse is typically recorded with digital tape recorders and displayed on an oscilloscope and/or graphic recorder. The reflected data may also be run through a video display units for real-time viewing. Recording enables the geophysicist to play back data later for further processing or analysis.

Common radar antennas operate at approximate center frequencies of between 80 and 1000 MHz. The higher frequencies provide the best resolution for smaller targets, however, the penetration depth is roughly inversely proportional to frequency. Thus, the design of any GPR survey requires an analysis of the trade-off between target resolution and depth of penetration so that the optimal antenna frequency may be selected.

5.2 Applicability

The antenna frequency and equipment configuration used for ground penetrating radar (GPR) surveys, as well as the survey methodology, is dependent upon site-specific conditions and the particular objectives of the survey. In addition, analysis of data requires interpretive skills developed through extensive training in the geosciences/geophysics and exposure to the application of GPR to a variety of field problems. The supervising geophysicist should have experience applying the technique at sites presenting a wide range of soil conditions and where the objectives of surveys have involved identification of subsurface features that include distinct targets such as buried metal objects and more subtle features such as back-filled excavations. Because of the highly interpretative nature of the GPR work it is difficult, therefore, to establish a standard operating procedure that would apply to all site surveys. The following material, however, offers some general guidelines for the conduct of GPR surveys, including information on the principles of operation, instrumentation, application and interpretation associated with standard GPR methods.

Because the GPR method utilizes high-frequency radio waves that are of higher frequency than the wave frequencies associated with seismic surveys or resistivity soundings, target resolution is better than that provided by these other two techniques. However high frequencies are more susceptible to signal attenuation. In typical clay materials, for example, the useful penetration depth is about 3 feet using a 100 megahertz (MHz) antenna. The same antenna used to survey over an area of dry sand soils (< 20 percent moisture); however, will allow for a penetration depth of about 30 feet.

Ground penetrating radar (GPR) is typically useful in detecting three classes of subsurface anomalies - metallic objects, layers/areas/objects of differing electrical properties, and disruptions in the layering of the subsurface materials. Buried metallic objects, such as pipes, barrels, bomb casings, and underground storage tanks, typically show prominent hyperbolic signatures due to the high contrast in electrical conductivity between metals and soil materials. Buried materials of differing electrical properties, such as concrete or brick walls, or water or air-filled pvc pipes, can also be detected. In some cases, contamination in

the soils or floating on the water table can be directly detected using GPR. For example, free petroleum product strongly attenuates the radar signal and can often be detected floating on the water table. GPR is also useful for delineating disruptions in the natural soil layering, due to excavations, disposal trenches, or voids.

Characterization of the subsurface with GPR involves the generation of plots of distance along a survey line vs. reflected wave travel time and signal strength (amplitude) for return pulses from subsurface reflectors. The "reflective" property of subsurface materials or objects is associated with strong contrasts in the electrical properties between materials or objects that are in contact. These strong contrasts may be associated with naturally occurring stratigraphic or structural boundaries or from the disruption of natural materials and/or the presence of man-made materials (i.e., buried drums or contaminants). The dielectric constants for natural and man-made materials provide a parameter for quantifying and comparing electrical properties of subsurface materials. Disruptions of natural earth materials (e.g., excavation of and back-filling of trenches or formation of voids through subsidence) change the materials bulk physical and chemical properties, and, consequently, their electrical properties. These contrasts make GPR an effective means for identifying the boundaries of abandoned landfills or locating drums or subsurface contaminant plumes. Depending on the depth of penetration that may be achieved, the method may be used to map the interface between the saturated and unsaturated zones, map the depth to bedrock, locate sinkholes, or map fracture systems more efficiently than may be accomplished with other conventional methods such as soil boring programs.

A major limitation of GPR is subjective process involved in data interpretive. Weak reflections from objects of interest may be indistinguishable from noise in the radar record or masked by stronger reflections from other objects. However, special computerized signal processing and enhancing routines originally developed for seismic processing now enable the geophysicist to enhance weaker signals, but the success of the data interpretative process ultimately depends heavily on the experience of the geophysicist.

6.0 INSTRUMENTATION

The standard array of GPR instrumentation consists of a transmitter/antenna unit(s), a DC power supply, a control unit and the signal processing circuitry connected to the antenna by a cable; an oscillograph or video display unit, and a plotter or an analog or digital recording device. The field equipment may be vehicle mounted but is small enough that it may be hand carried into areas not having vehicle access. Examples of GPR units are Geophysical Survey Systems, Incorporated's (GSSI) SIR System 8 and System 10 ground-penetrating radar systems. Both GSSI systems utilize impulse radar technology to sense and record continuous, high resolution profiles of subsurface materials.

The primary variable in GPR instruments is the antenna configuration. Antennas are currently available in both monostatic (one-piece) and bistatic (two-piece) configurations and are generally designed to detect radar signals ranging from about 80 to 1000 MHz.

7.0 DATA ACQUISITION

7.1 Field Procedures

7.1.1 Planning. The planning phase of a GPR survey requires the development of information pertaining to the geophysical characteristics of the site and how they

might vary across the area to be surveyed. The type and structure of soils, geologic formations, and the approximate elevation of the water table are critical factors that should be established. In addition to developing information about the characteristics of earth materials that are present at the site, the geophysicist needs to develop information about the targets of interest and factors that may interfere with execution of the survey or cause excessive noise in the acquired data. If possible, it is useful to know the depth, size and shape, and type of potential targets to be detected. The depth and size of the objects are very important such that the appropriate antenna configuration and spacing between survey lines may be selected. Surveys over known objects on site are useful to cross-check the survey detection limit and depth calculations; however, they are not absolutely necessary. Other specifications include accuracy of locational resolution desired, probable weather conditions during site activities, and the type and sophistication of data processing required for data interpretation and presentation.

The time and effort required to perform GPR field surveys depends on several factors including the sophistication of the equipment used, the type of target, and logistical considerations. Additional time and effort are required to process and interpret data. Sophisticated data processing, detailed interpretations, and high-quality displays require considerable computer usage and may require more time to complete than the actual field survey.

- 7.1.2 Site Layout. GPR surveys are performed by establishing a grid of parallel survey lines across the site and moving the radar antenna along each of these lines. The spacing between the lines is dependent upon the size and depth of the targets of interest and the objectives of the survey (i.e. reconnaissance or detailed survey). GSSI systems employ an electronic marking device that records a mark on direct field graphic records or within digital radar files. Generally, double marks or clicks are made at the beginning and end of the survey lines and single clicks are recorded as the antenna passes over predetermined distance intervals. Following acquisition of data in the field the data is downloaded from digital tape to PC storage for subsequent processing and analysis in the office.
- 7.1.3 Depth Determination. To determine the depth of anomalies noted on radar profiles, it is necessary to convert the data from recorded travel times, to depths. This is done by determining the transmission velocity(ies) associated with the earth materials. The velocity of electromagnetic waves within the subsurface at the site may be determined through excavation of observed targets to determine their depth of burial. Several excavations may be made and an average or range of transmission velocities for materials at a given site may be determined. Once velocity values are determined, interpretations or determinations concerning the depths of other signatures or anomalies may be made. Two other simpler methods, discussed in the following section, provide a simple means of determining the radar-wave velocities through subsurface materials and, therefore a means for converting travel-times to depths. These are two graphical approaches, one involving examination of hyperbolic signatures and the other involving the examination of changes in the travel-time within a given subsurface section as the transmitter and receiver antenna (bistatic configuration) are moved away from each other. The later is referred to as wide angle radar reflection (WARR) measurements.
- 7.1.4 GPR Survey Measurements. Once an optimal GPR survey configuration has been decided upon, The survey itself is straightforward, barring changes in the subsurface

electrical characteristics. The unit is activated and the antenna is towed along one of the prearranged grid lines. An electronic mark is placed on the data at the beginning and end of each survey line, and every 10 or 20 feet along the line, so that the position of the data and anomalies on each radar line is readily apparent. The locations of surface metal, utilities, walkways, etc. should be noted on the field logs during the survey.

7.2 Data Format

Although much of the data obtained in GPR surveys are automatically recorded by the instrumentation, additional information to unambiguously identify and to interpret each trace should be recorded in the field logbook. At a minimum, the field logbook should contain the following information:

- Project name, number and location
- Company or organization
- Date and time of day
- Operator's name
- Line and trace designation (also recorded directly on the signal recording medium)
- Equipment serial numbers
- Antenna frequency
- Direction and speed of antenna movement
- Weather and temperature
- Site map coordinates at the beginning and end of the trace
- Other pertinent notes, remarks or comments
- Electromagnetic velocity in the subsurface medium at the nearest calibration point.
- Map of grid and survey lines referenced to permanent features (wells, buildings, etc.)
- Data acquisition parameters (gain, range, filters used)

8.0 DATA PROCESSING AND INTERPRETATION

8.1 General

Reflected radar signals are electronically processed and displayed as an intensity-modulated time spectrum, where the time corresponds to target depth as described above. The series of signals corresponding to the reflected pulses as the antenna moves along a path forms a three-dimensional data set containing distance of traverse, depth, and intensity information.

Typically, the data are recorded on magnetic tape and/or displayed on a graphic recorder with distance displayed along the X-axis, time (i.e., depth) displayed along the Y-axis, and the intensity given by the degree of darkness of the trace. In a typical survey, a series of parallel traverses are made with the GPR, and the series of graphical traces provide X-Y-Z locational, as well as intensity of reflection information for targets of interest. Interpretation of anomalies in GPR traces requires considerable subjective evaluation by a trained geophysicist. Extensive experience is essential to distinguishing target reflections from inherent system noise and interferences. In many cases, the anomalies due to targets of interest are small compared to varying reflections from the antenna system, the ground surface, geologic perturbations, and other interferences. Similarly, an acceptable

interpretation of target depth from travel-time data requires knowledge of the varying geophysical characteristics across the site area surveyed.

A radar antenna transmits a "cone" rather than a thin beam of electromagnetic energy. The result is that reflections are obtained from objects not directly below the antenna. As the antenna moves across the plane of an object, reflections are obtained for a considerable distance along the antenna path. The radar reflections will generate a hyperbolic signature pattern. The size and shape of this hyperbolic signature varies as a function of the wave velocity within the subsurface materials, the size and the orientation of the object relative to the radar wave pulse, and the rate, t , at which the antenna configuration is moved along the surveyed line. The signal travel times will vary corresponding to the distance between the antenna and the object.

8.2 Hyperbolic reflectors

A discrete spherical target, therefore, will generate a hyperbolic reflection patterns with the apex of the hyperbola corresponding to the location and depth of the object. Multiple or odd-shaped targets or targets of considerable size in comparison to the radar wavelength) will generate complex reflection patterns consisting of overlapping hyperbolas. Thus, a true "picture" of subsurface objects is not obtained, and experience is necessary to translate the complex tracings into information concerning target depths, size, or shape.

8.3 Depth Determination

The calculation of the depth of exploration for a particular GPR configuration may be accomplished by knowing the dielectric constant of the earth materials or the depth to a particular reflector that is clearly visible on the radar record. In addition, the depth may be calculated through identification and graphical measurement of hyperbolic signatures or through the development wide angle refraction and reflection (WARR) data. The values for resistivity (inverse of conductivity), dielectric constant, and wave velocity in Table 017-1 are typical values; however, the real values for subsurface materials may change significantly over short lateral distances. The use of the published values exclusively may not yield depth calculations of sufficient precision.

8.3.1 WARR Method. The WARR measurement requires the use of actual data from the surveys conducted at each of the areas, are used to determine the velocities of the pulse, depth to significant reflectors, and the total depth of penetration. WARR measurements are performed with a bistatic (separate transmitter and receiver) antenna configuration. The two antennae are moved away from each other at a constant rate as a record is developed. By knowing the distance between the transmitter and receiver at a given time during the development of the record, the geophysicist may calculate the electromagnetic wave velocity(ies) using a t^2-x^2 plot. The recorded reflections are graphically plotted with the square of the distance between transmitter and receiver on the x-axis and the square of the time period on the y-axis. The inverse of the slope of the line of the reflection is the velocity of propagation. A simple calculation relating distance versus time will yield a velocity of the propagated pulse. Once the transmission velocity is known, depths to reflectors may be determined. The WARR measurements require the presence of good horizontal reflectors.

8.3.2 Hyperbola Geometry Method. The second method, the identification and measurement of hyperbolas, also provides good estimates of GPR penetration depth. The shape and position of the hyperbolic signatures, caused by cylindrical

objects (e.g. pipes or drums), is a function of the wave velocity within the subsurface, the size of the object, and the rate at which the antenna is moved. This type of calculation is possible because the GPR pulse has a broad cone-shaped radiation pattern and cylindrical objects have numerous surfaces that are normal to the pulse as the antenna is moved along a survey line: first approaching, directly over, and then away from the buried object.

The cone-shaped radiation pattern has an included angle of approximately 90 degrees. For flat or horizontal reflectors, only the vertical component of the pulse is reflected back to the receiver and the other sub-vertical components of the pulse are reflected or refracted away from the antenna not producing a record. Therefore, the two-way reflection sensitivity, or field of view, for flat surfaces is small. For cylindrical objects in the subsurface the sub-vertical components of the pulse may also be reflected back to the receiver as the antenna approaches the object. Because the round trip travel-time for the reflected pulse decreases as the antenna approaches the object, reaches a minimum directly over the object, and then increases again as the antenna moves away from the object, the record that is produced has a hyperbolic (inverted horse shoe) signature or pattern. The hyperbolic pattern generated on a radar record, distance (x) vs time (y), is a representation of the maximum round trip travel for the pulse when it first intersects the pipe, decreasing as the antenna approaches the axis of the pipe, and then increasing to a maximum again as it moves away from the pipe. Therefore, the position and shape of the hyperbola in the radar record are directly related to the wave transmission characteristics of the subsurface materials. Utilizing this simple geometric relationship the geophysicist may calculate transmission velocities for the various areas and the depths of penetration for the pulse and the depth to significant anomalies. Essentially, this results in a conversion of time on the y-axis of the GPR records to depth.

(T₁) represents the time of travel (or distance once velocity is known) for the "first" or "last" reflection that is produced when the center axis of the antenna is 45 degrees from the curved object (e.g. pipe). This reflection is recorded in the GPR record as the ends of the limbs of the parabola. This value is also referred to as the slant range or distance between the target and the antenna. The distance represented by (T₁) is greater than the actual depth of the target. As the antenna approaches the object the radar signature (top of the hyperbola) approaches the actual depth of the object. (T₀) represents the time of travel (or distance once the velocity is known) when the antenna is directly over the reflector.

If it is assumed that the subsurface materials over path distance (Z) have on average the same electrical properties as those for path distance (Y) and the dimensions of the pipe are considered insignificant relative to the other dimensions, then following geometric relations are true:

$$X^2 + Y^2 = Z^2$$

and

$$\frac{T_1}{T_0} = \frac{Y}{Z}$$

Combining these equations and solving for Y (the actual depth of the pipe), the following equation may be derived:

$$Y = X * (1/((T_x/T_y)^2 - 1)^{0.5})$$

X = distance along the ground in any convenient unit.

Y = depth of pipe in distance units.

T_x = travel time or "slant range" to pipe in any units.

T_y = travel time when the antenna is directly over the pipe.

The distance along the surface and the lengths of the T_x and T_y, scaled directly from the record are all that are needed to calculate the depth to the object causing the hyperbola. While these graphical measurements and calculations are relatively simple, they may become tedious when performed on all of the hyperbolae. This process has been automated with RADAN software available from GSSI.

9.0 SURVEY DESIGN

9.1 Prerequisites

Appropriate planning of GPR surveys requires a basic understanding of the site subsurface and hydrogeologic features, including the probable lateral variability. A statement of work should be generated that describes, in as much detail as possible, the known site conditions that may affect the subsurface electrical properties and the objectives of the proposed survey efforts, and allows for changing the survey parameters if the subsurface conditions change or are not found to be as described. The type and degree of data interpretation and the desired format for data presentation should also be specified if possible.

9.2 Instrument Selection

The important instrument selection decision for the survey lies in the determination of the optimal antenna. Generally, the higher the antenna frequency, the smaller the object that it can resolve, and the smaller its depth of penetration. The optimal antenna is the one with the highest resolution that will have sufficient depth of exploration. However, the depth of penetration for a given antenna will vary widely between sites, primarily due to soil moisture content and the amount of clay/sand ratio of the soils. Overnight rainfall can often elevate the soil moisture content such that an antenna's depth of penetration can be degraded by 30% in a few hours. No one antenna configuration is suitable for all cases, even at the same site. Ideally, the survey crew should carry multiple antennas to the site for the survey so that an optimal configuration will always be available.

9.3 Grid Design

The survey grid should be designed such that the GPR measurements are spaced to adequately define the distribution and extent of the exploration targets. For convenience, an orthogonal survey grid, located relative to a known location, is usually established over the survey area and the GPR measurements and anomalies are located by their grid coordinates (x,y). This is a convenient method for recording the data in an organized manner, for graphically displaying the data, and for ease of locating the anomalies detected. For determination of geologic features or to detect large targets, reconnaissance-type, low-resolution surveys are typically performed with a track spacing of 5 to 20 feet. Surveys to detect small discrete targets or to resolve target details require a track spacing of 1 to 5 feet.

- For surveys requiring reasonable resolution of target depth, the travel time to targets of known depths must be determined at each site. As the radar trace is made over the known targets, the reflection patterns provide direct depth-calibration points on the trace. Sites with uniform lithology may require only a few depth calibrations, but generally it is necessary to perform these calibrations at several locations and at several depths throughout the area of interest. Each radar trace should be referenced to the calibration most representative of the trace coordinates at the site. The preferred method is to use buried objects of known depth as calibration targets, or to excavate to detected objects and measure their depth below ground surface. A less desirable (but often necessary) procedure is to bury standard targets at various depths within the area of interest.
- In addition, WARR measurements may be conducted at several locations over the entire area of the site to determine how the transmission velocities change. If necessary specific transmission velocities may be determined for each subarea within the surveyed area.

10.3 Daily Quality Control

All radar traces and interpreted data sets should be accompanied by quality control data that indicate the level of quality of the data. Periodic replicate measurements should be made so that measurement precision may be established. Time and/or depth calibrations should be performed on a daily basis.

A calibration that yields significant changes in instrument parameters or travel time may indicate the need for repetition of data or increased density of travel time calibrations in the area of interest. Graphical data should be reviewed during the field activities to determine that data quality is adequate, and whether the survey results appear to be consistent with conceptual models.

11.0 HEALTH AND SAFETY CONSIDERATIONS

11.1 General

All procedures for hazardous waste site entrance, traverse, and egress that apply to general field operations established in the Site Health and Safety Plan also apply to conduct of geophysical surveys. Because GPR surveys are non-intrusive, the potential for exposure to chemicals of concern is generally low. Conducting GPR surveys consists of traversing the site on foot or in vehicles, and there are extended periods during which personnel are subject to adverse environments at the site. Geophysics survey personnel will adhere to the guidelines of the Site Health and Safety Plan for field activities.

Towing the GPR antenna by hand may involve considerable physical activity or hazards, especially on sloping or rough terrain. The geophysical methods discussed herein do not require extremely strenuous activity, and exposure to heat or cold is similar to that during other field activities. Extreme weather conditions will have adverse effects on the time required to obtain validated data, there by increasing the duration of personal exposure to the elements and to hazardous site influences.

11.2 Explosive Ordnance Disposal (EOD)

For surveys in areas where ordnance disposal or the presence of ordnance is suspected, EOD personnel will clear site access and survey areas prior to survey activities as per the Health and Safety Plan. The GPR methods described here involve the transmission of a weak electromagnetic radar signal whose characteristics vary between antenna transceivers. These transceivers generally emit a total electromagnetic signal of 0.1-4.0milliwatts over a frequency spectrum ranging from 80-1000 MHz. These signal strengths are total output strengths measured at the transceiver. The signal strength at any given frequency is measured in microwatts and falls off rapidly with depth in the subsurface. It is possible that this signal may not be safely broadcast in the vicinity of certain types of (live) ordnance, particularly those which may have active radar proximity detonators. The individual GPR instruments proposed for the survey(s) will be cleared for use, for each site where ordnance may be present, by the facility Health and Safety officer.

12.0 POTENTIAL PROBLEMS

GPR surveys are subject to a wide variety of potential problems that may impact conduct of the survey and/or proper interpretation of the survey results. The two most significant problems include:

- Noise and Interferences. GPR measurements may be affected severely both by natural and by man-made sources of electromagnetic interference. Sources of system noise that degrade the quality of radar traces include improper spacing of antennas above ground, improper cable placement, location of antennas too close to other system components, and facility instrument operation. Because reflections are obtained from any object with a dielectric constant differing from the surroundings, large masses or a high density of buried or surface rocks, metal, debris, wet soil, or structures can mask targets of interest. Some antennas are not shielded on their top surface and, as a result, are subject to interfering reflections obtained from overhead objects such as trees, power lines, and buildings. Topographic and geologic features can also interfere with acquisition of high-quality target detection data. Small depressions in the ground surface, the presence of boulders, clay lenses and moist soil zones affect both the capability to detect the target and determine its depth. Sources of electromagnetic energy in the vicinity, such as radio or television transmitters, or navigational radar antennas may result in spurious signals in the radar traces. In some cases, these problems may be minimized by judicious selection of radar and/or data communications frequency, and by scheduling the surveys during period of transmission inactivity.
- Rebar. The presence of steel reinforcing mesh or concrete rods in concrete (rebar) is a common problem for GPR surveys. The rebar generates regularly spaced hyperbolas in the data. If the rebar is thick and closely spaced, the reflections from the rebar can completely obscure the underlying material.
- Weather Conditions. Because water absorbs radar signals, wet weather has a very serious effect on the ability to perform GPR surveys. Physical difficulties in executing a survey over wet terrain also may be expected. Therefore, survey activities should be planned, if at all possible, during periods when dry weather can be expected. The survey schedule should also account for moist soil conditions and changes in these conditions.

TABLE 017-1

	<u>Resistivity (ohm/meter)</u>	<u>Relative Dielectric Constant</u>	<u>Electromagnetic Wave Vel. (cm/ns)</u>
Air	-----	1	30
Asphalt	~10	2.5-3.5	16-19
Concrete	~10	3-9	10-17
Conglomeratic soil	100-1000	9-14	8-10
Sandy soil	50-400	11-18	7-9
Silty soil	20-200	14-36	5-8
Clayey soil	1-30	25-56	4-6
Sandstone	200-1000	9-14	8-10
Limestone	2000-10000	6-11	9-12
Ice	-----	3.2	17
Water	-----	81	3.3
Sea Water	5x10-2	81	3.3

*Reference: 1987, Operation Manual, Model 2441 GeoRadar-I, OYO Corporation.

STANDARD OPERATING PROCEDURE 018 ELECTROMAGNETIC INDUCTION (TERRAIN CONDUCTIVITY) SURVEYS

1.0 PURPOSE

The purpose of this standard operating procedure is to provide a general description and technical management guidance on the use of electromagnetic induction (terrain conductivity) surveys during hazardous waste site investigations at U.S. Army installations.

2.0 SCOPE

This guideline provides a description of the principles of operation, instrumentation, applicability, and implementation of electromagnetic induction methods used during hazardous waste site investigations to determine subsurface conductivity. Measurements of subsurface conductivity can be used to determine the presence and approximate extent of subsurface contaminants, buried drums, and metal containers, along with depth to the water table and structural characteristics of the subsurface environment.

The document is intended to be used by a site manager to develop an understanding of the method sufficient to permit work planning and scheduling, resource planning, subcontractor procurement and evaluation, and manipulation and use of the technical data during remedial investigations and feasibility studies. This guidance is not intended to provide a detailed description of methodology and operation, which will vary between sites, between target depths and characteristics, and between instruments. The description focuses on methods and equipment that readily available and typically applied; it is not intended to provide a complete discussion of the state of the art. Specialized expertise is required during both planning and execution of geophysical surveys to develop a target-specific, site-specific, and instrument-specific scope of work, with detailed operating procedures, which will best achieve the goals of the survey.

3.0 DEFINITIONS

Apparent Conductivity. The quantity measured during an electromagnetic induction survey; proportional to the actual conductivities of subsurface materials.

Conductivity. The property of a material to conduct an electric current, roughly equal to the reciprocal of resistivity.

Current. The quantity of charge transmitted per unit time.

Electromagnetic Induction (EMI). The process of transmitting a primary electromagnetic field which induces a secondary magnetic field in magnetic or paramagnetic objects or volume.

Electromagnetic Induction Survey. A geophysical exploration method whereby secondary electromagnetic fields are induced in the subsurface and whose strength is a measure of ground conductivity.

Horizontal Dipole Coil Orientation. The horizontal dipole coil orientation induces a field response which is greatest in the near-surface and falls off monotonically with depth.

EMI instruments are calibrated to read subsurface conductivity directly in units of millimhos per meter, where

$$1000 \text{ millimho per meter} = 1 / \text{ohm-meter}$$

This relation indicates that the conductivity obtained from EMI measurements varies inversely with the resistivity measured using a resistivity survey. However, because the subsurface sections associated with the two methods are generally of different depth or cross-sectional area, there is not an exactly inverse relationship between conductivity and resistivity surveys.

The conductivity value obtained by an EMI instrument depends on the combined effects of the number of soil and rock layers, their thicknesses and depths, and the inherent conductivities of the materials. The quantity actually measured is an apparent conductivity of the earth volume between the ground surface and an effective penetration depth, which is defined as the depth at which variations in conductivity no longer have a significant effect on the measurement. The sampling depth is related to the spacing between the transmitter and receiver coils of the instrument, approximately as follows:

$$\text{Sampling depth} = 1.5 (\text{coil spacing})$$

Vertical profiling can be accomplished by multiple measurements about a point, with varying coil spacings. Horizontal profiling is performed by making measurements along traverses with a fixed coil spacing.

5.2 Applicability

The measurement of subsurface conductivity at a hazardous waste site provides a valuable contribution to site characterization for the following reasons:

- Conductivity is a function of the geohydrologic section and is overwhelmingly influenced by the presence of water (where buried metal is not present). Therefore, conductivity can provide indirect evidence on the porosity and permeability of subsurface materials and the degree of saturation. These parameters, in turn, are directly related to subsurface lithology and to the potential for infiltration/migration of contaminants from a source area.
- Conductivity is influenced by the presence of dissolved electrolytes in soil or rock pore fluids. Contaminant plumes in the vadose (unsaturated) and saturated zones can be mapped if there is sufficient change in conductivity to be detected by EMI measurements. In general, contaminant plumes of inorganic wastes are most easily detected because conductivity may be increased by one to three orders of magnitude above background values. The limit of detection is a change from a background of 10% - 20%. Plumes of non-polar organic constituents from spills or leaking containers may be detected if sufficient soil moisture has been displaced to affect the ground conductivity to a measurable degree.
- Conductivity can be used to detect the presence of buried wastes if the degree of saturation, containerization, or inherent electrical properties of the wastes produce sufficient variation from the soil matrix. Practically, only large sources, such as a buried disposal trench or a group of buried drums, can be detected by these methods. The degree of detail provided by typical surveys cannot distinguish the size, shape, or mass of sources except in a qualitative manner.

For these reasons, conductivity surveys should be investigated as potentially appropriate site characterization tools when any of the following information is desirable:

- Detection and mapping of contaminant plumes; the rate of plume movement may also be deduced from measurements made over time.
- Estimates of depth, thickness and resistivity of subsurface layers, depth to the water table, or probable geologic composition of a layer.
- Detection, mapping and depths of burial pits, landfills, clay caps or lenses, or deposits of buried waste.
- Determination of locations for drilling to intercept contamination or to investigate aquifer properties.
- Corroboration of limited chemical and geohydrologic data at a site.

6.0 INSTRUMENTATION

EMI instruments are available in two forms:

6.1 Fixed Coil

Single-piece models operable by one person, with fixed coil spacings of 1, 4, and 12 feet; these provide sampling depths on the order of 1.5, 6, and 15 feet, respectively. The Geonics EM-38 (1 foot coil spacing) and EM-31 (12 foot coil spacing) are examples of this type of instrument.

6.2 Variable-coil

Dual-coil models, operable by two persons, with variable coil spacing up to about 40 feet (sampling depth up to about 60 feet). The Geonics EM-34 is an example of this type of instrument.

The 12-foot fixed coil and the dual-coil apparatus are most commonly used in hazardous wastes site investigations. In either case, an additional person to record data and identify measurement locations is highly desirable and more time efficient. The instruments are calibrated to read directly in conductivity units, and values are typically read and recorded on a data sheet. Some units have been modified to provide direct digital recording on magnetic tape.

7.0 DATA ACQUISITION

7.1 Field Procedures

7.1.1 Planning. Known or assumed geohydrologic features of the site, potential source locations and migration characteristics of hazardous constituents, are used to select specific techniques and equipment to establish appropriate locations and depths for geophysical measurements. The level of detail necessary (data quality objectives) determines the amount of effort and, in simple terms, the required number and

density of data points. The data quality will depend on the method and specific equipment selected, the supporting hardware and software capabilities, and site-specific conditions.

Most of the details can be planned prior to site activities; however, some leeway must be accorded to the field procedures to account for variable site conditions and weather.

7.1.2 **Site Layout.** One of the most labor-intensive and time-consuming aspects of the field work involves layout of grids, and surveying or careful measurement of locations to allow geophysical surveys to be accomplished in a systematic, documentable manner. Every data point must be uniquely identified by locational coordinates of sufficient resolution to accomplish the objectives of the survey. Where possible, a cartesian (X,Y) grid should be established to provide these coordinates.

7.1.3 **Electromagnetic Induction Measurements.** At a given site grid location, the specified orientation of the apparatus is established, i.e., with the axis of the coils either parallel or perpendicular to the direction of the survey line. The meter reading is recorded and the apparatus moved to the next site grid location.

For the dual-coil method, both the intercoil spacing and coplanarity of the coils must be established prior to recording the data. Surveys are normally conducted with the coil axes horizontal and at right angles to the survey direction.

EMI profiles can be accomplished in a continuous manner using vehicle-mounted equipment and strip chart or digital recorders. Location information must be appended by tic marks or voice-over and some means provided to reference written field logs in a consistent manner.

7.2 Data Format

7.2.1 **General.** Information obtained during an EMI survey should be presented according to a standard data format, using standardized data sheets with original field entries. As a minimum, this should include the following information:

- Project, task, site, and location identification;
- Company or organization;
- Date (and time, if applicable);
- Operator's name and signature;
- Method/technique identification;
- Instrument make, model, serial number, and calibration date/frequency (if applicable);
- Coil type and configuration;
- Line or site grid location(s);

- Weather and site conditions and temperatures;
- Identification of relevant calibration and QC data; and
- Data for each sounding or profile should be recorded on a single sheet, if possible.
- Presence and location of cultural or topographic features which could affect the data.

7.2.2 Survey data. Survey data should include, in a tabular format, the following information:

- Coil location, per the survey plan;
- Coil spacing and configuration (unless specified in the heading); and
- Meter reading in millimhos per meter (quadrature phase) or parts per thousand (in-phase).

Special precautions to systematize and preserve data will be required for data that are recorded continuously on strip charts, magnetic tape, or in the memory of a recording device (such as an Omnidata Polycorder). Identifying header information must be recorded directly on the chart, tape, or file. Strip charts should be permanently affixed to the field logbook. Magnetic tapes or memory devices should be downloaded at least daily and hardcopy obtained. The original hard copy of output should be similarly secured/stored.

8.0 DATA INTERPRETATION

Corrections may be applied to EMI data for accuracy and drift, variation in location from pre-established coordinates, changes in scale, and nonlinearities associated with high conductivity values. In all cases, such corrections must be fully supported by data originally recorded or annotated in the field. Profile data along traverses are obtained as plots of conductivity versus distance. Parallel traverse data may be combined to provide conductivity contour maps of a site. Two or more profiles at different sampling depths, as well as sounding data at a given location, provide information on the relative conductivities of shallow and deeper layers. Contour plots can provide valuable information on the extent and direction of groundwater flow and contaminant transport.

Detailed comparison of EMI sounding measurements with layer models of the site can be made. This type of interpretation has been used at sites with relatively simple, uniform geohydrology to determine overburden-bedrock spatial and depth relationships. In some cases, very detailed interpretations, including aquifer flow properties, location of permeable zones, and interaquifer transfer, are possible.

9.0 SURVEY DESIGN

9.1 Prerequisites

10.0 QUALITY CONTROL

10.1 General

Geophysical surveys are subject to misapplication, erroneous interpretations, and use of incomplete or inadequate data. All of these avoidable errors can severely impact both the cost of subsequent site investigations and the validity of the site characterization. This susceptibility to misuse and potential for negative impact demands in assurance that appropriate quality control measures have been implemented. Quality control aspects common to most types of geophysical field programs are as follows:

- Program management personnel with technical expertise in preparing of statements of work, reviewing of proposals, work plans and reports, and technical supervision of subcontracts and field-related programs.
- Insistence on a defined scope of work, clear specifications, and data validation procedures.
- Requirement of a field quality control program.
- Appropriate justification before rejection of data points from a data set. Field data sheets should contain all observed data and the conditions that could impact data validity.
- Field data should be recorded in permanent ink in a bound logbook and each page signed and dated by the operator. Original unaltered logbooks should be retained in the site file.
- Proper calibration of instrumentation. In general, the objectives of geophysical surveys can be met by relative measurements across an area or with depth and, therefore, absolute calibration is of lesser importance than precision of measurements. However, a properly calibrated instrument provides an added measure of data validity. Furthermore, proper calibration permits correlation and comparison of the associated data with site features and geohydrologic characteristics not evident at the time of the field effort.
- An evaluation should be made of noise, interferences, and obstructions at a site. Such measurements, inferences, and explanations should be recorded in the field. These real-time quality control procedures aid field personnel in correction of noise sources over which they have control, in validating suspected external sources, and in early detection of problems that may jeopardize the survey objectives.

10.2 Instrument Quality Control

10.2.1 Calibration. EMI instruments are calibrated by the manufacturer over massive rock outcrops of known characteristic that are used as a geologic standard to measure the absolute conductivity over a uniform section of earth. The EMI apparatus should be maintained in calibration by the user, by noting drift in the readings at a stable "secondary standard" site. A secondary standard site is a location established in the field that is used to check the accuracy (calibration of the instrument and the

Ward, Stanley H., ed., 1990. Volume II - Environmental and Groundwater, Geotechnical and Environmental Geophysics, Society of Exploration Geophysicists Investigations in Geophysics No. 5.; SEG, Tulsa, OK.

Anticipated depths of wells are given in well specific work plans (e.g. Appendix D). In case the previously defined criteria have not been met before the depth range for a given hole is reached, the geologist will stop the drilling and confer with her/his supervisor. The current boring conditions (depth, nature of the stratigraphic unit, and water-table depth) will be compared to those of other wells nearby to decide to continue drilling or to terminate and complete the well.

- 3.2.7 If the well is to be installed in the surficial aquifer:** Drilling will be terminated before penetrating the basal aquitard. The basal aquitard is defined as the first 2 foot-thick clay below the water table, or below 5 feet in the case of a shallow aquifer (Field Investigation Plan, § 6.7.3)
- 3.2.8 If the well is to be installed in a lower, confined aquifer:**
- 3.2.8.1** Penetrations of aquifers located lower than the watertable aquifer will be limited to avoid cross-contamination.
- 3.2.8.2** Placement of new upper confined aquifer wells will be initially limited to those areas where contamination has been confirmed.
- 3.2.8.3** The location of upper confined aquifer wells will be based upon the findings of the water-table aquifer investigation. Areas of known contamination will be targeted for installing upper confined aquifer wells for the purposes of delineating vertical contamination.
- 3.2.8.4** Where possible, upper-confined aquifer wells will be located such that they afford triangulation with other wells within the same aquifer to allow for a determination of ground-water flow direction.
- 3.2.8.5** Some upper-confined aquifer wells will be installed approximately 10-15 ft from water-table wells to enable the accurate assessment of vertical hydraulic gradients. If the direction of ground-water flow is known, wells within a group will be located sidegradient of each other.
- 3.2.8.6** The boring will be advanced until the base of the surficial aquifer is reached (see § 3.2.7).
- 3.2.8.7** An outer, surface casing will be set 2 to 5 ft into the confining layer to minimize the potential for cross-contamination from the unconfined aquifer during drilling activities.
- 3.2.8.8** The surface casing will be driven into the confining bed and grouted into place. A grout plug at least 2 feet thick will be tremied into the bottom of the surface casing. The grout will be permitted to cure for 24 hours. All drilling fluids within the surface casing will then be removed, and the casing will be flushed with clean potable water.
- 3.2.8.9** The drilling equipment will be decontaminated, a smaller bit or auger selected, and the hole will be continued through the grout plug into the confined aquifer.

- k. Depositional Environment and Formation
- l. Incidental odors
- m. OVA reading(s)
- n. Staining

3.3.3 Material description for rock samples must include:

- a. Classification
- b. Lithologic Characteristics
- c. Bedding/Banding Characteristics
- d. Color
- e. Hardness
- f. Degree of Cementation
- g. Texture
- h. Structure and Orientation
- i. Degree of Weathering
- i. Solution or Void Conditions
- k. Primary and Secondary Permeability
- l. Sample Recovery
- m. Incidental odors
- n. OVA reading(s)
- o. Staining

See also SOP003 and SOP016 for details on logbook entries.

3.4 Well Construction and Installation

After the hole is drilled and logged, backfill hole as required for proper screen placement. The integrity of the aquitard will be restored by placing a bentonite plug of an appropriate thickness, either to the top of the aquitard (normal well installation) or to within 0.3 ft. of the top of the aquitard (DNAPL well). Aquifer fill will be clean filter pack.

Normal screen placement for the water table (surficial) aquifer will be with 2 ft. of the screen extending above the static water level. The bottom of the screen will rest no more than 6 in. from the bottom of the hole or backfill material, whichever is applicable.

Note: the end cap in DNAPL wells will rest on the bottom of the bottom of the hole, or bentonite backfill if applicable. (see § 3.2.9.2above)

Screen placement for a confined aquifer well will normally be at the top of the confined aquifer.

3.4.1 Screen lengths will not normally exceed 10 feet. If it appears advantageous in a given situation (e.a. to screen an entire aquifer which is thicker than 10 feet, approval must be sought on a case-by-case basis from MDE and EPA. Otherwise, wells will be screened as follows:

Thickness of Aquifer:	Action:
-----------------------	---------

< 10'	Screen entire aquifer
> 10' < 30'	screen top 10' consider vertically nested well cluster
> 30'	install vertically nested well cluster

3.4.2 The installation of monitoring wells in uncased or partially cased holes will begin within 12 hours of completion of drilling, or if the hole is to be logged, within 12 hours of well logging, and within 48 hours for holes fully cased with temporary drill casings. Once installation has begun, work will continue until the well has been grouted and the drill casing has been removed. Exceptions MUST be requested in writing by the contractor to the Contracting officer's Representative prior to drilling. Unscheduled delays attributable to unforeseeable site occurrences will not require advance approval.

3.4.3 Well screens, casings, and fittings will conform to National Sanitation Foundation Standard 14 or American Society for Testing and Materials (ASTM) equivalent for potable water usage. These materials will bear the appropriate rating logo. If the logos are not present, a written statement from the manufacturer/supplier stating that the materials contain the appropriate rating must be obtained. Material used will be new and essentially chemically inert to the site environment.

3.4.3.1 Well screen and casing should be inert with respect to the ground water; therefore, the selection of screen and casing material will be based on select field tests of aquifer chemistry and potential contaminants. The screen will be capped without sediment trap or DNAPL sampling cup, and lowered into the hole. The well casing will be pre-cut to extend 2 to 2.5 ft above the ground surface. Prior to placement of the last piece of well casing, a notch or other permanent reference point will be cut, filed, or scribed into the top edge of the casing.

3.4.3.2 Screen slot size will be appropriately sized to retain 90 to 100% of the filter pack material, the size of which will be determined by sieve analysis of formation material (See § 3.4.3.2).

3.4.3.3 The tops of all well casing will be capped with covers composed of materials compatible with the products used in the well installation. Caps may either be vented, or a telescopic fit, constructed to preclude binding to the well casing caused by tightness of fit, unclean surfaces, or weather conditions. In either case it should be secure enough to preclude the introduction of foreign material into the well, yet allow pressure equalization between the well and the atmosphere.

3.4.4 Filter pack material will be tremied into place, and lightly tamped and leveled. Filter pack will extend from the bottom of the hole to a height of 1-2 ft above the top of the screen. The filter pack will be capped with 1 ft of fine (Ottawa) sand to prevent the bentonite seal from infiltrating the filter pack.

3.4.4.1 Granular filter packs will be chemically and texturally clean, inert, and siliceous.

3.4.4.2 Filter pack grain size will be based on formation grain-size analysis. The D30 (70% retained) sieve size multiplied by a factor of not less than 3 nor greater than 6 will be used to determine the appropriate grain size.

3.4.4.3 Calculations regarding filter pack volumes will be entered into the Field Logbook along with any discrepancies between calculated and actual volumes used. If a discrepancy of greater than 10% exists between calculated and actual volumes exists, an explanation for the discrepancy will also be entered in the Logbook.

3.4.5 Bentonite seals will be no less than two feet nor more than five feet thick as measured immediately after placement. The normal installation will include a five foot seal. Thinner seals may be used in special cases as defined in Section 3.12 of Appendix A. The final depth to the top of the bentonite seal will be measured and recorded.

3.4.6 GROUT

Grout used in construction will be composed by weight of:

- 20 parts cement (Portland cement, type II)(see footnote)
- 0.4 to 1 part (max.)(2-5%) bentonite
- 8-gallons (max.) approved water per 94-lb bag of cement.

Neither additives nor borehole cuttings will be mixed with the grout. Bentonite will be added after the required amount of cement is mixed with the water.

3.4.6.1 All grout material will be combined in an above-ground container and mechanically blended to produce a thick, lump-free mixture. The mixed grout will be recirculated through the grout pump prior to placement.

3.4.6.2 Grout placement will be performed using a commercially available grout pump and a rigid, side discharge tremie pipe.

3.4.6.3 The following will be noted in the Field Logbook: 1) calculations of predicted grout volumes, 2) exact amounts of cement, bentonite, and water used in mixing grout, c) actual volume of grout placed in the hole, d) any discrepancies between calculated and actual volumes used. If a discrepancy of greater than 10% exists between calculated and actual volumes exists, an explanation for the discrepancy will also be entered in the Logbook.

3.4.7 Well protective casings will be installed around all monitoring wells on the same day as the initial grout placement around the well. Any annulus formed between the outside of the protective casing and the borehole will be filled to ground surface with cement.

3.4.8 The construction of each well will be depicted as built in a well construction diagram. The diagram will be attached to the boring log and will graphically denote:

- a. Screen location, length
- b. Joint location
- c. Granular filter pack

- d. Seal
- e. Grout
- f. Cave-in
- g. Centralizers
- h. Height of riser
- i. Protective casing detail

3.5 Monitoring well completion

- 3.5.1** Assemble appropriate decontaminated lengths of pipe and screen. Make sure these are clean and free of grease, soil, and residue.
- 3.5.2** Lower each section of pipe and screen into the borehole, one at a time, screwing each section securely into the section below it. No grease, lubricant, polytetrafluoroethylene (PTFE) tape or glue, may be used in joining the pipe and screen sections.
- 3.5.3** Centralizers will be used every 50 ft below the top 50 ft. (except within screened interval and bentonite seal). Centralizer material will be PVC, PTFE, or stainless steel. Determination of centralizer material will be based on the same criteria as screen and calling selection (see Field Investigation Plan, Section 6.8)
- 3.5.4** Prior to installation, cut the riser so that it will extend approximately 2-2.5 ft. above grade. Notch, file, or otherwise permanently mark a reference point on the top of the casing. All pipe cuts **MUST** be square to ensure that the elevation between the highest and lowest point of the well casing is less than or equal to 0.02 ft.
- 3.5.5** When the well is set to the bottom of the hole, temporarily place a cap on top of the pipe to keep the well interior clean.
- 3.5.6** Place the appropriate filter pack into using a tremie pipe. Monitor the rise annulus with a weighted tape to assure that bridging is not occurring.
- 3.5.7** After the pack is in place, wait three to five minutes for the material to settle, tamp and level a capped PVC pipe, and check its depth weighted steel tape.
- 3.5.8** Add a 1-2 foot cap of fine-grained (Ottawa) sand to prevent infiltration of the filterpack by overlying bentonite seal.
- 3.5.9** Install the bentonite seal by dropping bentonite pellets into the hole gradually. If the well is deeper than 30 feet, a tremie pipe will be used to place the pellets. Tamp and level the pellets with a capped PVC pipe, and check depth with a weighted tape as above.
- 3.5.10** Wait a for the pellets to hydrate and swell. Hydration times will be determined by field test or by manufacturer's instructions. Normally this will be 30 to 60 minutes. Document the hydration time in the field notebook. If the pellets are above the water level in the hole, add several buckets of clean water to the boring. Document the amount of water added to the hole.
- 3.5.11** Mix an appropriate cement-bentonite slurry (§ 3.4.6). Be sure the mixture is thoroughly mixed and as thick as is practicable.

- 3.5.12 Lower a side discharge tremie pipe into the annulus to the level of the pellet seal.
- 3.5.13 Pump the grout slurry into the annulus while withdrawing the tremie pipe and temporary casing.
- 3.4.14 Stop the grout fill at 5 feet below the ground surface. Allow to cure for not less than 12 hours. If grout settles more than 6-in., add grout to bring level back up to within 5-ft. of ground surface. Place approximately 2 ft. of bentonite pellets (minimum 0.5 ft) in annulus. Seat the protective casing in the bentonite seal, allowing no more than 0.2 ft between the top of the well casing and the bottom of the protective casing cap. Fill inner annulus (between well casing and protective casing) with bentonite pellets to the level of the ground surface. Cover bentonite pellets with 1 ft. of clean granular material (coarse sand or pea gravel filter pack). Fill the outer annulus (between the protective casing and the borehole) with neat cement. Allow the cement to mound above ground level and finish to slope away from the casing. Lock the cap.

-or-

- 3.5.15 Continue the grout fill to the ground surface. Seat the protective casing in the grout, allowing no more than 0.2 - ft between the top of the well casing and the bottom of the protective casing cap. Lock the cap.

-and-

- 3.5.16 Allow the grout slurry to set overnight.
- 3.5.17 Fill the outer annulus (between the casing and the borehole) with neat cement. Allow the cement to mound above ground level and finish to slope away from the casing.
- 3.5.18 Slope the ground surface away from the casing for a distance of two feet, at a rate of no less than 1 inch in two feet. Surface this sloping pad with a geotextile mat covered by 3 in. of coarse gravel.
- 3.5.19 Set pre-painted protective steel pickets (3 or 4) evenly around and 4 feet out from well.

3.6 Well Development

- 3.6.1 Well development is the process by which drilling fluids, solids, and other mobile particulates within the vicinity of the newly installed monitoring well have been removed while restoring the aquifer hydraulic conductivity. Development corrects any damage to or clogging of the aquifer caused by drilling, increases the porosity of the aquifer in the vicinity of the well, and stabilizes the formation and filter pack sands around the well screen.
- 3.6.2 Well development will be initiated after 48 consecutive hours but no longer than 7 calendar days following grouting and/or placement of surface protection. The record of well development will be submitted to the Contracting Officer's Representative within three working days after well development is completed.

3.6.3 Two well development techniques - over pumping and surging will be employed in tandem. over pumping is simply pumping the well at a rate higher than recharge. Surging is the operation of a plunger up and down within the well casing similar to a piston in a cylinder.

3.6.4 Materials Required

- a. Well Development Form
- b. Boring Log and Well Completion Diagram for the well
- c. Submersible pump or bailer of appropriate capacity, and surge block
- d. Conductivity, pH, ORD, turbidity, dissolved oxygen, and temperature meters
- e. Electric well sounder and measuring tape.
- f. Containers for purged water, if required.

3.6.5 Summary of Procedures and Data Requirements.

3.6.5.1 Pump or bail the well to ensure that water flows into it, and to remove some of the fine materials from the well. Removal of a minimum of one equivalent volume (EV) is recommended at this point. The rate of removal should be high enough to stress the well by lowering the water level to approximately 1/2 its original level.

3.6.5.2 Slowly lower a close-fitting surge block into the well until it rests below the static water level, but above the screened interval. (Note: this latter is not required in the case of an LNAPL well.)

3.6.5.3 Begin a gentle surging motion which will allow any material blocking the screen to break up, go into suspension, and move into the well. Continue surging for 5-10 minutes, remove surge block, and pump or bail the well, rapidly removing at least one EV.

3.6.5.4 Repeat previous step at successively lower levels within the well screen until the bottom of the well is reached. Note that development should always begin above, or at the top of, the screen and move progressively downward to prevent the surge block from becoming sand locked in the well casing. As development progresses, successive surging can be more vigorous and of longer duration as long as the amount of sediment in the screen is kept to a minimum.

3.6.5.5 Development is expected to take at least 2 hours in a small well installed in a clean sand, and may last several days in large wells, or in wells set in silts with low permeabilities.

3.6.5.6 Development will continue until little or no sediment can be pulled into the well, and target values for parameters listed in 3.6.4.9(e.) (below) are met.

3.6.5.7 At a minimum, development will remove 3 to 5 EV, plus 3 to 5 times the amount of fluid lost during drilling, and 3 to 5 times the volume used in filter pack placement.

3.6.5.8 All water removed must be disposed of as directed by the Sampling Design Plan.

3.6.5.9 Record all data as required on a Well Development Record Form (see example), which is made a part of the complete Well Record. These data include:

- a. Depths and dimensions of the well, the casing, and the screen, obtained from the Well Diagram.
- b. Water losses and uses during drilling, obtained from the boring log for the well.
- c. Water contained in the well, obtained from calculations using the depth of the water column and the well radius, plus the radius and height of the filter pack and an assumed 30% porosity.
- d. Measurements of the following indicator parameters: turbidity, pH, conductivity, oxidation-reduction (ORD, Redox) potential, dissolved oxygen, and temperature before, twice during, and after development.
- e. Target values for the indicator parameters listed above are as follows: pH - stabilize, conductivity - stabilize, ORD - stabilize, DO stabilize, temperature - stabilize, turbidity - NTU 5 or stabilize
- f. Notes on characteristics of the development water.
- g. Data on the equipment and technique Used for development.
- h. Estimated recharge rate and rate/quantity of water removal during development. (See SOP 013 section 3.2.)

3.7 Refer to SOP003 (Field Logbook), 005 (Decontamination), 008 - 012 and 036 038 (Instrumentation for Groundwater Parameters).

4.0 Maintenance

Not Applicable.

5.0 Precautions

Refer to the site-specific Health and Safety Plan for discussion of hazards and preventive measures during well development activities.

6.0 References

Aller, Linda, *et al.*, 1989. Handbook of Suggested Practices for the Design and Installation of Ground-Water Monitoring Wells, National Water Well Association

Cohen, Robert M., and Mercer, James W. 1993. DNAPL Site Evaluation, CRC Press, Inc.

COMAR 26.04.04 Well Construction

EPA Groundwater Handbook 1989

Nielsen, David M., 1993. Correct Well Design Improves Monitoring, in "Environmental Protection", Vol.4, No.7, July, 1993.

USATHAMA. 1987. Geotechnical Requirements for Drilling, Monitoring Wells, Data Acquisition, and Reports, March 1987.

WELL DESIGNATION: _____ DATE(S) OF INSTALLATION: ____/____/____

SITE GEOLOGIST: _____ DEVELOPMENT DATE(S): ____/____/____

STATIC WATER LEVELS BEFORE AND AFTER DEVELOPMENT * :

BEFORE _____ DATE _____ 24 HR. AFTER _____ DATE _____

DEPTH TO SEDIMENT BEFORE AND AFTER DEVELOPMENT * :

BEFORE _____ DATE _____ 24 HR. AFTER _____ DATE _____

DEPTH TO WELL BOTTOM * : _____ SCREEN LENGTH _____

HEIGHT OF WELL CASING ABOVE GROUND SURFACE: _____

QUANTITY OF MUD/WATER:

- LOST DURING DRILLING (+) _____ gallons
- REMOVED PRIOR TO WELL INSERTION (-) _____ gallons
- LOST DURING THICK FLUID DISPLACEMENT (+) _____ gallons
- ADDED DURING FILTER PACK PLACEMENT (+) _____ gallons
- TOTAL LOSSES _____ gallons

- (a) Water column ht. (ft.) _____
- (b) Well radius (in.) _____
- (c) Screen length (ft.) _____
- (d) Borehole radius (in.) _____

(e) QUANTITY OF FLUID STANDING IN WELL

$(12 * a * \pi * b^2 * 0.0043) =$ _____ gallons
 (Show Calculation)

(f) QUANTITY OF FLUID IN ANNULUS

$[12 * c * \pi * 8(d^2 - b^2) * 0.0043 * 0.30]$ _____ gallons
 (Show Calculation)

DEVELOPMENT VOLUME = $(5 * \text{TOTAL LOSSES}) + [5 * (e + f)] =$ _____ gallons
 (Show Calculation)

* ALL DEPTHS MEASURED FROM TOP OF WELL CASING

EXAMPLE WELL DEVELOPMENT RECORD
(PAGE 2 OF 2)

WELL DESIGNATION _____
____/____/____

DATE(S) OF DEVELOPMENT: _____

TYPE AND SIZE OF PUMP: _____

TYPE AND SIZE OF BAILER: _____

DESCRIPTION OF SURGE TECHNIQUE:

RECORD OF DEVELOPMENT

DATE & TIME	QUANTITY REMOVED	TIME REQ'D	pH	Cond	Temp	ORD	Turb	DO	Character of water (color / clarity / odor / partic.)
(before)									
(during)									
(during)									
(during)									
(after)									

TYPICAL PUMPING RATE _____ GAL./HR. EST. RECHARGE RATE _____

TOTAL QUANTITY OF WATER REMOVED _____ TIME REQUIRED _____

REMARKS _____

SIGNATURE OF SITE GEOLOGIST _____

DRILLING LOG		Division	Hole No.			SHEET
						OF SHEETS
1. PROJECT		10. SIZE AND TYPE OF BIT			11. STATUS FOR ELEVATION IDENTIFICATION (if any)	
2. LOCATION (Coordinates or Street)		12. MANUFACTURER'S DESIGNATION OF DRILL				
3. DRILLING AGENCY		13. TOTAL NO. OF OVER-BOROSN SAMPLES TAKEN		14. RETURNED	UNRETURNED	
4. HOLE NO. (to whom or issuing office and its number)		15. TOTAL NUMBER CORE GOES				
5. NAME OF DRILLER		16. ELEVATION GROUND WATER				
6. DIRECTION OF HOLE		18. DATE HOLE		STARTED	COMPLETED	
<input type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.		17. ELEVATION TOP OF HOLE				
7. THICKNESS OF OVERBURDEN		18. TOTAL CORE RECOVERY FOR BOROSN				
8. DEPTH DRILLED INTO ROCK		19. SIGNATURE OF INSPECTOR				
9. TOTAL DEPTH OF HOLE						
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Designation) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling fluid, water level, depth of penetration, etc., if significant) g
						

ENG FORM 18 36 PREVIOUS EDITIONS ARE OBSOLETE.
MAY 71

PROJECT

HOLE NO.

**STANDARD OPERATING PROCEDURE 020
ACTIVESOIL GAS SAMPLING**

1.0 Scope and Application

This standard operating procedure is applicable when conducting soil gas sampling. A soil gas survey is an effective screening tool in locating areas contaminated with volatile organic compounds.

2.0 Material

- a. Probe set, including probe jack
- b. Rotary hammer with 1" x 3/8" drill bit
- c. Disposable shield points
- d. 3/16" o.d. polyethylene tubing
- e. Extension cord
- f. Portable generator or other power source
- g. 1L Tedlar bags ²⁵
- h. Sample labels
- i. Vacuum box and vacuum pump
- j. Tygon tubing for vacuum box
- k. Clean sand
- l. Powdered bentonite
- m. Two measuring cups
- n. Tools: vise grips, 3/4" and 5/8" wrenches, scissors

3.0 Procedure

3.1 Soil Gas Point Installation

- 3.1.1 Assemble clean probe sections to the desired sampling depth.
- 3.1.2 Cut polyethylene tubing to at least 1' longer than the depth of the hole.
- 3.1.3 Insert one end of the tubing approximately 1/4" inside of aluminum shield point. Crimp the shield point tightly around the tubing with vise grips and insert the tube and shield point inside of the clean KV probe.
- 3.1.4 Using rotary drill and 3/8" drill bit, bore down 30" at the location desired for sampling. Be sure to clear the hole well so that soil does not fall back into hole.
- 3.1.5 Drive stainless steel probe and attached shield point and polyethylene tubing down the hole with a rotary hammer to about 4', or above the saturation zone. (It is desired to obtain a sample of the soil gas, not the ground water.) If samples are needed from greater than 4', drive the steel probe with a solid tip to the desired depth; extract, and insert a probe fitted with a disposable shield point and tubing.

²⁵ Tedlar bags and on-site analysis is preferred. Glass vials and offsite analysis will be acceptable. An equivalent SOP for glass vials and offsite analysis will be submitted by the contractor prior to sampling. Holding times for either sample container will be kept to a minimum.

- 3.1.6 Extract the probe by hand or with the jack. Be sure that shield point and tubing stays in the ground and attached to the shield point.
- 3.1.7 Pour ½ cup of sand down sampling hole. Gently shake the tubing to ensure that the sand settles and no bridged spaces remain.
- 3.1.8 Pour ½ cup bentonite down sampling hole, add ¼ cup distilled water, add another ½ cup bentonite down hole and another ¼ cup water. Continue until bentonite seal reaches the surface.
- 3.1.9 Allow at least 20 minutes before extracting sample.
- 3.1.10 Take sample (see 3.2 below)
- 3.1.11 Remove probe and backfill hole with bentonite.

3.2 Soil Gas Sample Collection Using Tedlar Bags

- 3.2.1 Cut at least 1" off the end of the tubing to ensure a clean sample.
- 3.2.2 Attach tubing to the vacuum box and pump.
- 3.2.3 Open valve on a clean, dry Tedlar bag and attach inside the vacuum box.
- 3.2.4 Close the vacuum box, close stopcock (3-way valve) between vacuum box and pump and then turn the pump on.
- 3.2.5 Allow Tedlar bag to fill 90% (do not overfill bag), shut off, crimp Tygon tubing (to prevent release of sample back down hole), open stopcock, and remove Tedlar bag from box.
 - 3.2.5.1 If the bag is filled with air only, squeeze the air out completely to purge air that was in the tubing and sand and reattach inside the box. Repeat steps 3.2.4 and 3.2.5. Close the valve on the Tedlar bag upon removal, label it accordingly, and put it in a cool, dark area. Note: not so cool as to cause condensation.
 - 3.2.5.2 If Tedlar bag is filled with water and air, be sure to close valve on Tedlar bag before removing it, label the bag accordingly, and put it in a cool, dark area. Note: not so cool as to cause condensation.
 - 3.2.5.3 If water is pulled into the Tedlar bag, Tygon tubing inside the vacuum box must be replaced.

3.2.6 Remove and decon probes.

- 3.2.7 Repeat the above procedures for each additional soil gas point.

3.3 Sampling with glass vials.

4.0 Maintenance

None

5.0 Field Quality Control Measures

5.1 To ensure that the equipment is free of volatile contaminants, collect at least two QC samples per day by drawing uncontaminated air through an unused representative sampling apparatus (assembled shield point and tubing). One sample should be taken at the beginning of the day, prior to collecting any samples, the other at the end of the day, after decontaminating the equipment. Ambient air may usually be assumed to be uncontaminated. If site ambient air is assumed to be contaminated, it should be sampled for contaminant levels.

5.2 To ensure that the analyzed samples are representative of the collected samples, and that the Tedlar bags are not losing volatile samples, spiked samples of known volatile concentration will be prepared. These samples will be stored and handled in the same manner as other field samples. Spiked samples will be the first collected and last analyzed.

Selected low level samples should also be duplicated at a different time and analyzed immediately to verify that analyte loss is not occurring.

Alternatively, samples may be analyzed in the field, using either Tedlar bags or syringe samplers to collect and transport the samples to the gas chromatograph.

5.3 Note sampling times for each sample in field notebook and on sample bag (if bags are used).

5.4 No more than 4 hours should elapse between sampling and analysis 15 minutes is preferable.

6.0 References

None

**STANDARD OPERATING PROCEDURE 021
SEDIMENT SAMPLING**

1.0 SCOPE AND APPLICATION

The purpose of this standard operating procedure is to delineate protocols for sampling sediments. Sediments include solid matter derived from rocks or biological materials which are suspended in, or settled from, water. This procedure can be applied to the collection of sediment samples from areas of deposition such as streams, rivers, ditches, lakes, ponds and lagoons. Sediment samples indicate the amount of contamination adsorbed on sediment particles and/or the amount of wastes transported from the site. It is therefore important to collect a representative sample.

2.0 MATERIAL

- a. Stainless steel, Polytetrafluoroethylene (PTFE), or PTFE-lined sampling tray or bowl
- b. Stainless steel or PTFE dip sampler, scoops, trowels, spoons, ladles
- c. PVC pipe, 2 in. diameter
- d. Hand core sediment sampler, liners (optional) and extensions
- e. Pipe dredge sampler
- f. Jaw type sampler
- g. Sample bottles
- h. Rubber boots/waders
- i. Plastic sheeting
- j. Utility knife
- k. Rope
- l. Boat
- m. PPE
- n. Personal flotation devices (PFDs)

3.0 PROCEDURE

The water content of the sediment may vary greatly. Likewise, the sediments themselves may range from very soft to dense. It may be necessary to use a variety of equipment to obtain the required samples, even at a single site.

- 3.1 Upon arrival at the site, immediately set up and organize the equipment downstream (where applicable) from sampling point.
 - 3.1.1 Cut a section of plastic sheet approximately 6 ft. x 6 ft. Place plastic on ground to use as a clean staging area for sampling equipment.
 - 3.1.2 Arrange sample containers, samplers, preservatives, and decon equipment on the plastic sheet. Exercise caution not to step on, or otherwise contaminate this clean working surface.

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**STANDARD OPERATING PROCEDURE 032
DRIVE-POINT PIEZOMETER INSTALLATION**

SOP being drafted

July, 1993

5.0 Precautions and Limitations

- 5.1 If for any reason a hazardous or unsafe condition presents itself for which there is no clear procedure or guideline, work shall cease until Program Safety Management can be notified and the condition rectified.
- 5.2 No person shall enter a confined space without an emergency response spotter outside the confined space.
- 5.3 A ladder shall be provide for any trench which is deeper than 4 ft. or when appropriate in other confined spaces.

6.0 Performance Steps

- 6.1 Evaluate the work area against the definition of a confined space.
- 6.2 Notify the Project Manager or Program Safety Management of any work spaces not previously identified that are suspected of meeting the definition of a confined space.
- 6.3 Contact the APG designated confined space attendant prior to entry and verify APG requirements for entry.
- 6.4 Obtain positive identification of the materials that are (or have been) present in the space.
 - a. Evaluate the hazards presented by the materials and byproducts.
 - b. Determine if any atmospheric monitoring will be required.
- 6.5 Determine the necessary safety precautions and protective clothing required for the particular space, based on the classification of the confined space.
 - a. If the space meets the definition of a class A confined space, then proceed to step 6.6.
 - b. If the space meets the definition of a class B confined space, then proceed to step 6.7.
 - c. If the space meets the definition of a class C confined space, then proceed to step 6.8.
- 6.6 Enter class A confined space.
 - a. Prepare a confined space entry permit. Include the following as a minimum:
 - 1) Identity of the space

- 2) Purpose of the entry
 - 3) Date of authorized entry
 - 4) Authorized entrants
 - 5) Eligible attendants
 - 6) Personnel eligible to be in charge of entry
 - 7) Substances stored in the confined space
 - 8) Potential hazards
 - 9) Permitted work
 - 10) PPE requirements
 - 11) Safety equipment requirements
 - 12) Signature and printed name of authorizing person
-
- b. Ensure that any line, except for a fire suppressant or extinguishing system, that enters the space and carries a harmful agent is physically disconnected from the space or blocked by a device capable of ensuring complete closure.
 - c. Render inoperable by disconnection any fixed mechanical device or equipment which, if operated, might endanger personnel.
 - d. Except for lighting, padlock or tag out-of-service electrical service equipment.
 - e. Select a suitable entrance point that will be safe for the entrant to pass through. Open the entrance.
 - f. Survey the entrance to the confined space for oxygen levels, combustible vapors, and other hazards.
 - g. Verify, based on levels obtained from step f. above, that all precautions are sufficient to permit entry. Ensure entrant is properly suited in required personal protective equipment. Allow entrant to enter the confined space.
 - h. Conduct atmospheric monitoring inside the confined space to determine the presence of combustible, toxic gases, or an oxygen deficient atmosphere.
 - 1) Determine oxygen levels prior to any other testing.
 - 2) Draw test air from lowest to highest elevations of the confined space: 12-18 inches off of floor, mid-levels, and within 12-18 inches of the top (if possible).
 - 3) For spaces greater than 500 cubic feet, draw test air from additional sample points in sufficient number to categorize the atmosphere in the confined space.
 - i. Once inside, verify any communication equipment used is properly working.

- j. Monitor for oxygen levels, combustible vapors, and any other identified hazards on a continuous basis while working in class A confined spaces. Continuous monitoring shall include all instruments on with the alarms functioning and set, or a second attendant whose only purpose is to monitor the work environment for the identified hazards.
- k. Proceed to Step 6.9.

6.7 Enter class B confined space.

- a. Ensure that any line, except for a fire suppressant or extinguishing system, that enters the space and carries a harmful agent is physically disconnected from the space or blocked by a device capable of ensuring complete closure.
- b. Render inoperable by disconnection any fixed mechanical device or equipment which, if operated, might endanger personnel.
- c. Except for lighting, padlock or tag out-of-service electrical service equipment.
- d. Select a suitable entrance point that will be safe for the entrant to pass through. Open the entrance.
- e. Survey the entrance to the confined space for oxygen levels, combustible vapors, and other hazards.
- f. Verify, based on levels obtained from step e. above, that all precautions are sufficient to permit entry. Ensure entrant is properly suited in the required personal protective equipment. Allow entrant to enter the confined space.
- g. Conduct atmospheric monitoring inside the confined space to determine the presence of combustible, toxic gases, or an oxygen deficient atmosphere.
 - 1) Determine oxygen levels prior to any other testing.
 - 2) Draw test air from lowest to highest elevations of the confined space: 12-18 inches off of floor, mid-levels, and within 12-18 inches of the top (if possible).
 - 3) For spaces greater than 500 cubic feet, draw test air from additional sample points in sufficient number to categorize the atmosphere in the confined space.
- h. Once inside, verify any communication equipment used is properly working.
- i. Monitor for oxygen levels, combustible vapors, and any other identified hazards on a continuous basis while working in class B confined spaces. Continuous

monitoring shall include all instruments on with the alarms functioning and set or a second attendant whose only purpose is to monitor the work environment for the identified hazards.

- j. Proceed to Step 6.9.

6.8 Enter class C confined space.

- a. Select a suitable entrance point that will be safe for the entrant to pass through. Open the entrance.
- b. Survey the entrance to the confined space for oxygen levels, combustible vapors, and other hazards.
- c. Verify based on levels obtained from step f. above that all precautions are sufficient to permit entry. Allow entrant to enter the confined space.
- d. Conduct atmospheric monitoring inside the confined space to determine the presence of combustible, toxic gases, or an oxygen deficient atmosphere.
 - 1) Determine oxygen levels prior to any other testing.
 - 2) Draw test air from lowest to highest elevations of the confined space: 12-18 inches off of floor, mid-levels, and within 12-18 inches of the top (if possible).
 - 3) For spaces greater than 500 cubic feet, draw test air from additional sample points in sufficient number to categorize the atmosphere in the confined space.
- e. Monitor for oxygen levels, combustible vapors, and any other identified hazards on an intermittent basis while working in class C confined spaces. Intermittent monitoring shall include a complete set of readings for all initial parameters on a specified basis. The frequency of the monitoring shall be determined prior to entrance by Safety Program Management.

6.9 Exit confined space.

6.10 Close off confined space to prevent unauthorized access.

6.11 Cancel confined space permit (if appropriate).

7.0 Documentation

Document the entry and results of all atmospheric monitoring in the field logbook. Maintain a copy of the confined space entry permit (if appropriate) in the project files.

8.0 References

COMAR 09.12.35, Maryland Occupational Safety and Health Standards for Confined Spaces

**STANDARD OPERATING PROCEDURE 041
SLUDGE SAMPLING PROCEDURES**

1.0 Scope and Application

The purpose of this standard operating procedure is to delineate protocols for sampling sludges. Sludges include solid matter derived from waste materials that are suspended in or settled from a liquid. This procedure can be applied to the collection of sludge samples from areas of deposition such as: tanks, sumps, landfills, ditches, ponds and lagoons. It is important to collect a representative sample of the waste material.

2.0 Material

- a. Stainless steel or Teflon tray
- b. Stainless steel hand core sludge sampler and extensions
- c. Stainless steel dip sampler, spoons, trowels, spoons, and ladles
- d. Sample bottles
- e. Plastic sheeting
- f. Utility knife
- g. Polypropylene rope

3.0 Procedure

The liquid content of the sludge sample may vary from nearly all liquid to a dense, nearly liquid-free material. It may be necessary to use a variety of equipment to obtain the required samples, even at a single site.

3.1 General Procedure:

- 3.1.1 Upon arrival at the site, immediately set up and organize the equipment.
- 3.1.2 Establish background levels of airborne organic compounds using a photoionization detector (PID) or a flame ionization detector (FID).
- 3.1.3 Cut a section of 6 mil plastic sheeting of approximately 6 ft x 6 ft. Place the sheeting on the upgradient side of the sample area.
- 3.1.4 Arrange the sample containers, sampler(s), and decontamination equipment on the plastic sheeting.
- 3.1.5 Don PPE in accordance with the site health and safety plan.

- 3.1.6 Collect the sample(s). The preferred method of collecting sludge samples will be by hand corer, refer to Section 3.2. If using a scoop, trowel, spoon, or ladle, refer to Section 3.3.

3.2 Hand Corer

- 3.2.1 Ensure that the corers and liners are properly decontaminated prior to use.
- 3.2.2 Force the corer into the sludge with a smooth continuous motion to a depth of 9 to 12 inches.
- 3.2.3 Twist the corer to detach the sample; then withdraw the corer in a single smooth motion.
- 3.2.4 Remove the top of the corer and, if excess liquid is present, decant the liquid into a sample bottle. This liquid will be labeled and analyzed.
- 3.2.5 Remove the nosepiece of the corer and deposit the sample into a stainless steel or Teflon tray.
- 3.2.6 Transfer the sample into sample bottles using a stainless steel laboratory spoon or equivalent object.
- 3.2.7 If possible, the top 6 inches of the core will be sampled into 3 separate sample bottles. 2 inches per bottle, to ensure that an accurate chronology of contamination can be determined.
- 3.2.8 Ensure that each sample bottle is properly labeled, noted on the chain-of-custody form, and placed in the sample cooler with ice packs.
- 3.2.9 Decontaminate sampling equipment according to SOP 005.
- 3.2.10 Dispose of all sampling wastes in properly labeled containers

3.3 Scoop, Trowel, Spoon, or Ladle

- 3.3.1 Ensure that the sampling equipment is properly decontaminated prior to use.
- 3.3.2 Insert the sampling device into the material at the selected point and slowly remove the sample. Care should be taken to retain as much of the solid component as possible.
- 3.3.3 Transfer the sample into the appropriate sample bottles.

3.3.4 Ensure that each sample bottle is properly labeled, noted on the chain-of-custody form, and placed in the sample cooler with ice packs.

3.3.5 Decontaminate sampling equipment according to SOP 005

3.3.6 Dispose of all sampling wastes in properly labeled containers.

3.4 Sampling Location

For all samples mark the sampling location on a site map. Photograph (optional, recommended) the sampling site. Describe each sampling location in the field logbook. Establish the sampling coordinates using the Global Positioning System and record the coordinates for each sample in the field logbook.

4.0 Maintenance

Not applicable.

5.0 Precautions

Sludges may contain high levels of contaminants.

It is extremely important to continually monitor the levels of contaminants, using the appropriate survey instruments (e.g., PID, indicator tubes) in the breathing zone of the sampler(s) and other field team members.

Refer to the HASP for appropriate PPE.

Field team members should consult with the Site Health and Safety Coordinator for all health and safety questions or concerns relating to sampling activities.

6.0 References

EPA/54/P-87/001, A Compendium of Superfund Field Operations Methods.

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**STANDARD OPERATING PROCEDURE 042
DISPOSAL OF ENVIRONMENTAL WELL DEVELOPMENT/PURGE WATER**

SOP being drafted

July, 1993

**STANDARD OPERATING PROCEDURE 043
HYDROLABMULTIPARAMETERWATERQUALITYMONITORING INSTRUMENT**

1.0 Purpose and Scope

Use of brand names in this SOP is in nowise intended as endorsement or mandate that a given brand be used. Alternate equivalent brands of detectors, sensors, meters, etc. are acceptable. If alternate equipment is to be used, the contractor shall provide applicable and comparable SOPs for the maintenance and calibration of same.

SOP being drafted

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**STANDARD OPERATING PROCEDURE 044
ASSESSMENT OF EXISTING WELLS USING DOWNHOLE GEOPHYSICS**

SOP being drafted

July, 1993

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Revision: 0
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**STANDARD OPERATING PROCEDURE 045
ASSESSMENT OF TIDAL EFFECTS ON GROUND-WATER**

SOP being drafted

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