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# Statistics of Sampled Rician Fading

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February 1993

**Technical Report** 

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# **CONVERSION TABLE**

Conversion factors for U.S. Customary to metric (SI) units of measurement

AULTIPLY	BY		TO GET		
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angetrom	1.000000 x E -10	meters (m)	、		
atmosphere (normal)	1.01325 x E +2	kilo pascal (kPa			
	$1.000000 \times E + 2$	kilo pascal (kPa	.)		
Darn	$1.000000 \times E - 28$	meter <sup>2</sup> (m <sup>2</sup> )			
British thermal unit (thermochemical)	1.054350 x E +3	joule (J)			
calorie (thermochemical)	4.184000	joule (J)			
cal (thermochemical) / cm <sup>2</sup>	4.184000 × E -2	mega joule/m <sup>2</sup>			
arie (1997)	3.700000 × E +1	"giga becquerel	(GBq)		
degree (angle)	1.745329 x E -2	radian (rad)			
legree Farenheit	$t_{\kappa} = (t_{P} + 459.67)/1.8$	degree kelvin (i	()		
electron volt	1.60219 x F -19	joule (J)			
nî.	$1.000000 \times E -7$	joule (J)			
rg/second	1.000060 x E -7	watt (W)			
oot	3.048000 x E -1	meter (m)			
oot-pound-force	1.355818	joule (J)			
rallon (U.S. liquid)	3.785412 x E -3	meter <sup>3</sup> (m <sup>3</sup> )			
nch	2.540000 x E -2	meter (m)			
erk	1.000000 x E +9				
	••••	joule (J)			
oule/kilogram (J/kg) (radiation dose absorbed)	1.000000	Gray (Gy)			
	4.183	terajoules			
tip (1000 lbf)	4.448222 x E +3	newton (N)			
tip/inch <sup>2</sup> (ksi)	6.894757 x E +3	kilo pascal (kPa			
ttap	$1.000000 \times E +2$	newton-second/	$m^2 (N-s/m^2)$		
micron	$1.000000 \times E -6$	mete: (m)			
nil	2.540000 x E -5	meter (m)			
nile (international)	$1.609344 \times E + 3$	meter (m)			
Dunce	2.834952 × E -2	kilogram (kg)			
pound-force (lbs avoirdupois)	4.448222	newton (N)			
pound-force inch	1.129848 x E -1	newton-mater (	im)		
pound-force/inch	1.751268 x E +2	newton/matr.			
pound-force/foot <sup>2</sup>	4.788026 x E -2	kilo pascal (kPa			
pound-force/inch <sup>2</sup> (psi)	6.894757	kilo pascal (kPa	· ·		
pound-mass (lbm avoirdupois)	4.535924 x E -1	kilogram (kg)	•)		
pound-mass-foot <sup>2</sup> (moment of inertia)	4.214011 x E -2	kilogram-meter	3 (1		
pound-mass/foot <sup>3</sup>	$1.601846 \times E + 1$	kilogram/meter			
			- ( <b>kg</b> /m-)		
rad (radiation dose absorbed)	$1.000000 \times E^{-2}$	**Gray (Gy)			
roentgen	2.579760 x E -4	coulomb/kilogr:	am (C/kg)		
shake	$1.000000 \times E - B$	second (s)			
slug	$1.459390 \times E + 1$	kilogram (kg)			
torr (mm Hg, 0° C)	1.333220 x E -1	kilo pascal (kPs	The second secon		
The becquerel (Bq) 1: the SI unit of radioactivi	ity; $1 \text{ Bq} = 1 \text{ event/s}$ .		Accesion For		
**The Gray (Gy) is the SI unit of absorbed rad	lation.		NITIC ODIAL		
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# SECTION 1 INTRODUCTION

Design, evaluation, and testing of trans-ionospheric radio frequency (RF) communication systems require high fidelity channel models and detailed knowledge of fading channel statistics. Such models can be used to construct realizations of the received signal for use in digital simulations or hardware channel simulators. During the design process, knowledge of channel fading statistics is used to develop power requirements, size interleavers, and assess performance, for example.

The design goal for a truly robust trans-ionospheric communications system is to achieve performance that is acceptable over the entire range of possible fading conditions from fast, frequency selective, Rayleigh fading to slow, flat fading including the regime between Rayleigh fading and a non-fading channel. While considerable effort has been expended in the nuclear effects community over the past three decades to characterize the Rayleigh fading channel and to develop Rayleigh fading mitigation techniques, somewhat less effort has been directed at robust design and performance in non-Rayleigh fading. One reason for this is that if a system is properly designed to successfully operate over the full range of Rayleigh fading, then it is generally assumed that it will also perform well in non-Rayleigh fading.

There are situations, however, where this assumption may not be valid. For example, the performance of many systems is degraded in slow Rayleigh fading where long, deep fades can cause tracking loops to loose lock on the received signal. A natural question to ask is the following: What happens to receiver performance in slightly non-Rayleigh fading where the channel coherence time may be longer than under Rayleigh fading? Does performance degrade further because the fades may be longer or does it improve because the fades are generally not as deep?

Effects of non-Rayleigh fading are also important in determining the performance of systans that have not been designed to operate under highly disturbed ionospheric conditions. An obvious question is: Will these systems perform adequately under weakly disturbed (either man-made or naturally occurring) ionospheric conditions? This question should be addressed before effort is spent to needlessly upgrade communications systems that may already perform adequately in weak scintillation or before fragile communications systems unexpectedly fail.

The purpose of this report and a companion report [Dana, 1992b] is to extend existing Defense Nuclear Agency (DNA) channel models to include the non-Rayleigh fading regime. Ideally these models will then cover all possible fading conditions, from fast, frequency selective fading caused by a highly disturbed ionosphere to naturally occurring slow, non-Rayleigh fading. Such models are needed for the design, analysis, and testing of existing and new communications systems.

The problem with a general-purpose channel model is that the statistics of non-Rayleigh fading are not described by any single mathematical expression, as is the case for Rayleigh fading. Thus it is the intent of the companion report, *Temporal Statistics* of Non-Rayleigh Fading, to demonstrate that Rician statistics provide a reasonable worst case channel model in this regime. In this report, temporal statistics (i.e., mean fade duration and separation) of Rician fading are derived. These statistics are then used to demonstrate that realizations of sampled Rician fading can be generated with the desired statistics. In Dana [1992b] the temporal statistics of non-Rayleigh fading are analyzed, and it is shown that Rician statistics may provide a reasonable worst case for the cumulative distribution, mean fade duration, and mean fade separation.

#### **1.1 RICIAN STATISTICS.**

Realizations of the channel impulse response function generated with Rician amplitude statistics [*Rice*, 1948] have been used for many years to evaluate system performance in the regime between full Rayleigh fading and ambient non-fading conditions. This approach is often used because it is easy to generate a realization of Rician fading from a realization of Rayleigh fading by simply adding a constant component to the complex impulse response function, appropriately re-normalized to maintain constant power.

However researchers in the area of ionospheric physics (see, for example, *Fremouw*, *Livingston*, and *Miller* [1980]; *Rino and Fremouw* [1973]; *Rino, Livingston*, and Whitney [1976]; and Whitney, et al. [1972]) have suggested that Nakagami-m, generalized Gaussian, or log-normal distributions may more accurately describe the observed amplitude distribution of RF scintillation caused by the ambient ionosphere.

None of these distributions or the Rician distribution adequately describe the observed phase fluctuations of non-Rayleigh fading. Indeed, the Nakagami-m and lognormal distributions only describe amplitude fluctuations. Often two-component models, one for amplitude and another for phase, are used to described the statistics of observed trans-ionospheric signals (see, for example, *Wittwer* [1930]). However, such two-component models may not accurately reproduce observed amplitude-phase correlation of non-Rayleigh fading [Fremouw, Livingston, and Miller, 1980].

Two important points should be noted about proper design of robust transionospheric communications systems. First, performance should be insensitive to the random phase fluctuations encountered on a the link. Second, it is important that the performance is insensitive to the differences between the various fading distributions. All are possible, so the system should be designed to perform against the reasonable worst case. If phase fluctuations are important, then separate Total Electron Content (TEC) dynamics models are available to stress the system [Wittwer, 1980; Frasier, 1988].

Recently *De Raad and Grover* [1990] undertook a theoretical study of the amplitude statistics of non-Rayleigh fading for a wide range of ionospheric conditions. They conclude that (1) *none* of these models is reliable in general; (2) the actual amplitude distribution has a strong dependence on the power spectrum of the scattering

ionospheric structure as well as the Fresnel length; and (3) Rician amplitude statistics provide a useful "worst case" description of the occurrence of deep fades.

Multiple phase screen (MPS) techniques (e.g., Knepp [1983]; De Raad and Grover [1990]) can be used to generate realizations of the channel impulse response function that represent direct solutions to Maxwell's equations. These higher fidelity realizations exhibit a large range of amplitude and phase fluctuations under non-Rayleigh fading conditions. However De Raad and Grover [1990] correctly observe that the uncertainty in the validity of MPS realizations has been shifted from the amplitude: and phase distributions to the statistical desc. pain of the scattering medium.

Still, the temptation persists to use Rician fading realizations for non-Rayleigh fading. They are easy to generate from Rayleigh fading realizations, and they contain phase fluctuations (albeit fluctuations that differ significantly fluctuations). By comparison with MPS realizations of non-Rayleigh fading, *De Raad and Grover* [1996] show that Rician amplitude statistics represent a reasonable worst case for the observed cumulative distribution of fades, and *Dana* [1992b] shows that Rician temporal statistics also represent a reasonable worst case for the observed mean fade duration and separation.

The purpose of this report is to provide further information on the temporal statistics (mean fade duration and separation) of Rician fading and to define sampling requirements of Rician realizations of the channel impulse response function. These analytic results are compared to measured values from a representative set of MPS realizations in *Dana* [1992b] where utility of Rician temporal statistics in bounding the observed range of fade durations and separations in MPS realizations is demonstrated.

#### **1.2 SAMPLING STATISTICS.**

The original version of this report [Dana 1988] was intended to address three questions that arise during simulation or hardware testing activities of communications links under Rayleigh fading conditions: (1) How many decorrelation times ( $\tau_0$ ) per realization of the channel impulse response function are necessary? (2) How many samples per decorrelation time are necessary? (3) How should interpolation be done between samples? This report re-addresses these questions for the more general case of Rician fading, and more completely addresses an additional question: (4) What is the expected variation in measured parameters [] a realization?

The fourth question can arise in at least two situations. The efficacy of a realization of the channel impulse response function may be in question, or it may be necessary to validate a realization for use in hardware testing. An approach used by the author to validate realizations is to measure key parameters, such as mean power, amplitude moments, decorrelation time, and number of samples per decorrelation time. These measured parameters should agree with ensemble values to within some tolerance. The question is: What tolerance? Dana [1991] partially addresses this question. This report incorporates some recent findings on the expected tolerance of measured realization parameters.

The first three questions are answered in part in the DNA signal specification for nuclear scintillation [*Wittwer*, 1980] which requires a minimum of 100 decorrelation times per realization and 10 samples per decorrelation time. However considerable statistical variation in receiver performance is seen when the minimum realization length is used. This is particularly true of links that have large power margins and are susceptible to only the deepest fades. Of course the best answer to these questions is to measure link performance with realizations of increasing length and resolution until the statistical variation in the results from one realization to the next is acceptable. Unfortunately the luxury of doing this analysis ordinarily does not erist.

The next higher level of analysis of these questions is to look at the statistics of the realizations. This is the approach that will be taken in this report. The first order statistics of realizations are measured by calculating amplitude moments and the cumulative distribution and comparing these to ensemble values for Rayleigh fading. The second order statistics of the realizations are measured by calculating the mean duration and separation of fades.

In general, the received signal may be written as the convolution of the channel impulse response function  $h(t,\tau)$  with the transmitted modulation m(t):

$$u(t) = \int_{0}^{\infty} h(t,\tau) m(t-\tau) d\tau . \qquad (1.1)$$

In either software link simulations or in hardware channel simulator, Equation 1.1 can be implemented as a tapped delay line:

$$u(t) = \sum_{j=0}^{N_{\tau}-1} h(t, j\Delta\tau) m(t-j\Delta\tau) \Delta\tau \qquad (1.2)$$

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where  $N_{\tau}$  is number of taps on the delay line;  $\Delta \tau$  is the delay spacing of the delay line; and  $h(t,j\Delta \tau)$  is the time varying complex weight of the  $j^{th}$  tap. In a software simulation of link performance time will also be discretely sampled (i.e.,  $t = k\Delta t$ ).

Under Rayleigh fading conditions  $h(t,\tau)$  is a complex, zero mean, normally distributed random variable and thus has a Rayleigh amplitude distribution. It then follows from Equation 1.2 that u(t) is also a complex, zero mean, normally distributed random variable with a Rayleigh amplitude distribution.

A complete analysis of the first three questions would consider the sampling requirements for each delay of the discrete impulse response function  $h(k\Delta t, j\Delta \tau)$ . However this is beyond the scope of this report. Therefore sampling requirements on the flat fading impulse response function  $h(k\Delta t)$ , where will be addressed in this report. The sampling requirements for  $h(k\Delta t)$  will give some indication of the sampling requirements for the free new selective impulse response function  $h(k\Delta t, j\Delta \tau)$ . Perhaps this should be state, another way: Sampling that is inadequate for  $h(k\Delta t)$  will surely '... inadequate for  $h(k\Delta t, j\Delta \tau)$ . Thus it is the intent of this report to define adequate sampling for  $h(k\Delta t)$  and to infer adequate sampling requirements for each delay of  $h(k\Delta t, j\Delta \tau)$ .

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# SECTION 2 TEMPORAL STATISTICS OF RICIAN FADING

This section is a generalization of well-known results from the classical work of *Rice* [1948, 1954, 1958] on the first and second order statistics of Rayleigh fading. To the author's knowledge, the extension of Rice's results on temporal statistics to non-Rayleigh fading is new.

## 2.1 FIRST ORDER STATISTICS.

Under strong scattering conditions, the electric field incident on the plane of the receiver is the summation of many waves propagating in slightly different directions about the line-of-sight. Under the central limit theorem of statistics, the two orthogonal components of the electric field must then be zero-mean, normally distributed random variables. It is assumed that the two orthogonal components are also independent. The complex narrow-band envelope of the electric field undergoing Rayleigh fading may be then represented as

$$E(t) = x(t) + i y(t)$$

where x and y are independent and normally distributed with zero mean and standard deviation  $\sigma$ . The carrier frequency term, exp (*icot*), has been neglected in this expression. Thus E(t) may be thought of as the output voltage of a down-converter where x(t) is the in-phase component and y(t) is the quadrature-phase component.

Under mild to weak scattering conditions, a *model* of the electric field is a specular component plus a normally distributed random component. The electric field is then written as

$$E(t) = [x(t) + r \cos \vartheta] + i [y(t) + r \sin \vartheta]$$

where r is the constant component and  $\vartheta$  is a constant phase. Clearly Rayleigh fading corresponds to the case where r is zero.

*Rice* [1948] was the first to show that the probability density function of the amplitude of E(t),

$$a(t) = \sqrt{E(t)E^*(t)}$$

has the probability density function:

$$f(a) = \frac{a}{\sigma^2} \exp\left[-\frac{a^2 + r^2}{2\sigma^2}\right] I_0\left[\frac{ar}{\sigma^2}\right]$$
(2.1)

where  $I_0(\cdot)$  is the modified Bessel function.

For the mean power of of the electric field,

$$P_0 = \langle a^2 \rangle = 2\sigma^2 + r^2 ,$$

to be constant, the power of the fluctuating component,  $2\sigma^2$ , must be reduced as the power of the specular component,  $r^2$ , is increased. To keep track of this in a consistent manner both are written in terms of the scintillation index  $S_4$ , where

$$S_4 = \left[\frac{\langle a^4 \rangle - \langle a^2 \rangle^2}{\langle a^2 \rangle^2}\right]^{\frac{1}{2}} .$$

The powers of the two components are then:

$$2\sigma^2 = P_0(1-R)$$
$$r^2 = P_0R$$

where the "Rician" index R is

$$R = \sqrt{1-S_4^2}.$$

The Rician index is the fraction of the total power that is in the constant component.

Upon writing  $\sigma$  and r in terms of R, Equation 2.1 becomes

$$f(a) = \frac{2a}{P_0(1-R)} \exp\left[-\frac{a^2/P_0+R}{1-R}\right] I_0\left[\frac{2\sqrt{Ra^2/P_0}}{1-R}\right]$$

The corresponding phase  $\theta$  if the electric field is

$$\theta = \tan^{-1}\left[\frac{x(t) + r\cos\vartheta}{y(t) + r\sin\vartheta}\right].$$

The probability density function of the phase is

$$f(\theta) = \frac{1}{2\pi} \exp\left[-\frac{R}{1-R}\right] + \frac{1}{2} \left[\frac{R}{\pi(1-R)}\right]^{\frac{1}{2}} \cos\left(\theta - \vartheta\right) \times \\ \exp\left\{-\frac{R\left[1-\cos\left(\theta - \vartheta\right)\right]}{1-R}\right\} \left\{1 + \exp\left[\left(\frac{R}{1-R}\right)^{\frac{1}{2}} \cos\left(\theta - \vartheta\right)\right]\right\}$$

where erf (·) is the error function. The probability density function of phase is just  $1/2\pi$  when the scintillation index is unity (R=0), as it should be for Rayleigh fading.

These two probability density functions are plotted in Figures 1 and 2 for several values of the scintillation index. Amplitude in Figure 1 is  $a/\sqrt{P_0}$ , and phase in Figure 2 is the quantity  $\theta - \vartheta$ . The solid line curves in both figures are the Rayleigh limits. As expected, both functions approach delta functions as the scintillation index approaches zero.



Figure 1. Rician amplitude probability density function.



Figure 2. Rician phase probability density function.

The cumulative distribution of the power  $P(P = a^2)$ , which is equal to the probability that the instantaneous power is less than or equal to P, is given by

$$F(P) = \int_{0}^{\sqrt{P}} f(a)da = \exp\left[-\frac{R}{1-R}\right] \sum_{n=0}^{\infty} \frac{1}{\Gamma^{2}(n+1)} \left[\frac{R}{1-R}\right]^{n} \gamma\left[n+1, \frac{P/P_{0}}{1-R}\right]$$
(2.2)

where  $\gamma(n,x)$  is the incomplete gamma function and  $\Gamma(n+1) = n!$  is the gamma function. The summation is obtained by expanding the Bessel function in a power series and then performing the integration term-by-term. This form of Marcum's Q function [Marcum, 1948] is easily evaluated for values of R that are not too close to unity. In particular Equation 2.2 converges slowly for values of  $S_4$  less than 0.25, corresponding to R values greater than 0.96.

For the Rayleigh case the cumulative distribution is exponential:

$$F(P) = 1 - \exp\left[-\frac{P}{P_0}\right]$$
.  $(S_4 = 1)$ 

The Rician cumulative distribution function is plotted in Figure 3 versus the ratio  $P/P_0$  for several values of the scintillation index. For values of the scintillation index between 0.75 and unity the Rician cumulative distribution is close to the Rayleigh curve. As the scintillation index is reduced from about 0.75 to 0.5, the probability of deep fades is significantly reduced. It is noteworthy that case where the power of the specular and fluctuating components are equal corresponds to an  $S_4$  value of  $\sqrt{3/4}$  ( $S_4 = 0.866$ ). Thus a Rician cumulative distribution does not deviate significantly from a Rayleigh distribution until more than half of the power is in the constant component. Of course the performance a receiver may be quite sensitive to the existence of a specular component.

#### 2.2 DBPSK EXAMPLE.

An easily calculated example of the effects of Rician fading is the differentially coherent binary phase-shift keying (DBPSK) symbol error rate. The well known DBPSK symbol error rate for an additive white Gaussian noise (AWGN) channel is

$$P_{SE} = \frac{1}{2} e^{-\gamma P} \qquad (AWGN \text{ Channel}) \tag{2.3}$$

where  $\gamma$  is the symbol energy-to-noise density ratio and P is unity for this channel. In a Rician fading channel this error rate must be averaged over the probability density function of the fading power  $P = a^2$ :

$$\langle P_{SE} \rangle = \int_{0}^{\infty} \frac{1}{2} \exp[-\gamma a^{2}] f(a) da$$
.



Figure 3. Cumulative distribution of Rician fading.

This equation is easily evaluated using Equation 2.1 with the result:

$$\langle P_{SE} \rangle = \frac{1}{2[1+(1-R)\gamma]} \exp \left[\frac{-R\gamma}{1+(1-R)\gamma}\right]$$
 (Rician Channel)

When R is unity, corresponding to the non-fading case, this expression reduces to Equation 2.3. When R is zero, corresponding to full Rayleigh fading, it 1. Juces to the well-known form:

$$\langle P_{SE} \rangle = \frac{1}{2[1+\gamma]}$$
 (Rayleigh Channel).

Plots of the Rician channel DBPSK error rates for several values of the scintillation index are in Figure 4. As one might expect from examining the cumulative distribution, the DBFSK symbol error rate for a Rician fading channel is close to the full Rayleigh fading channel error rate when the scintillation index is larger that about 0.75, and is close to the AWGN error rate when the scintillation index is less that about 0.25. Thus for DBPSK the most interesting values of scintillation index, excluding 1 and 0, are between 0.75 and 0.25.





## 2.3 SECOND ORDER STATISTICS.

The fading rate is determined by the second order statistics of the fluctuating p at of the electric field. The autocovarience of the electric field is, in general,

$$\langle [E(t) - E_0] [E^*(t+\tau) - E_0^*] \rangle = \langle x(t)x(t+\tau) \rangle + \langle y(t)y(t+\tau) \rangle = 2\sigma^2 \rho(\tau)$$

where

$$E_0 = r \cos \vartheta + ir \sin \vartheta$$
.

There are two limiting forms for the correlation function  $\rho(\tau)$ . Under strongly disturbed scattering conditions that occur at early times or at the center of the disturbed region,  $\rho(\tau)$  has the Gaussian form

$$\rho(\tau) = \exp\left[-\frac{\tau^2}{\tau_0^2}\right]$$

where  $\tau_0$ , the decorrelation time of the electric field, is defined as the e folding point of the autocorrelation function  $[\rho(\tau_0) = e^{-1}]$ . The corresponding Doppler spectrum of the temporal fluctuations is

$$S(\omega_D) = \int_{-\infty}^{\infty} \exp(-i\omega_D \tau) \rho(\tau) d\tau = \sqrt{\pi}\tau_0 \exp\left[-\frac{\tau_0^2 \omega_D^2}{4}\right]$$

which also has the Gaussian form. Under less disturbed conditions, the correlation function is usually assumed to have the form

$$\rho(\tau) = \left[1 + \frac{\alpha_4 |\tau|}{\tau_0}\right] \exp\left[-\frac{\alpha_4 |\tau|}{\tau_0}\right]$$

where the parameter  $\alpha_4$  ( $\alpha_4 = 2.146193$ ) is determined by the condition that  $\rho(\tau_0) = e^{-1}$ . The corresponding Doppler spectrum has the form commonly referred to as an  $f^{-4}$  spectrum:

$$S(\omega_D) = \frac{4\tau_0}{\alpha_4} \frac{1}{[1 + (\tau_0 \omega_D / \alpha_4)^2]^2} .$$

A third Doppler spectrum is used for real-time frequency selective channel models [Dana 1992a]. This  $f^{-5}$  spectrum has the functional form

$$S(\omega_D) = \frac{16\tau_0}{3\alpha_6} \frac{1}{[1 + (\tau_0 \omega_D / \alpha_6)^2]^3}$$

where the normalization of  $S(\omega_D)$  is chosen so that  $\rho(0)$  is unity. The corresponding correlation function is

$$\rho(\tau) = \left[1 + \frac{\alpha_6 |\tau|}{\tau_0} + \frac{(\alpha_6 \tau)^2}{3\tau_0^2}\right] \exp\left[-\frac{\alpha_6 |\tau|}{\tau_0}\right]$$

where  $\alpha_6 = 2.904630$  results from setting  $\rho(\tau_0) = e^{-1}$ .

A comparison of Rayleigh fading realizations  $(S_4 = 1)$  of the impulse response function with  $f^{-4}$ ,  $f^{-6}$ , and Gaussian Doppler spectra is shown in Figure 5 where realization power in decibels (dB) is plotted versus time/ $\tau_0$ . These realizations were generated from the same set of random numbers, as described in Appendix A, so there is correlation in the features seen in the three frames. The  $f^{-4}$  realization in the bottom frame has the most spiky appearance because it has more energy at high Doppler frequencies. The three realizations have similar low frequency behavior, and fades in the realizations follow each other quite closely. The difference between the realizations is the high frequency jitter of the  $f^{-4}$  and  $f^{-5}$  realizations about the more smoothly varying Gaussian one. The significance of this on the temporal statistics of the fades will become apparent later.



1.2.2.

Figure 5. Realizations of Rayleigh fading with Gaussian,  $f^{-6}$ , and  $f^{-4}$ Doppler spectra.

A comparison of Rician fading realizations of the impulse response function with  $f^{-4}$  Doppler spectra and scintillation indices of 1.0, 0.75, 0.5 and 0.25 is shown in Figure 6. Again these realizations were generated from the same set of random numbers, so there is correlation in the features seen in all four plots. As expected, the Rayleigh fading realization in the top frame (reproduced from the bottom frame of Figure 3) has the deepest fades and the largest flares. As the scintillation index is reduced, the deep fades fill in and the power in flares above 0 dB is reduced. It is interesting that as the scintillation index decreases, fades at a given level appear to get longer. This phenomenon is shown theoretically for Rician fading in the developments below.

## 2.4 TEMPORAL STATISTICS.

The mean duration and separation of fades below an arbitrary power level P and that of flares above P, are calculated from the mean number  $\langle N(P,T) \rangle$  of crossings of the level P in the time interval T.

The probability that the amplitude *a* crosses the level  $l = \sqrt{P}$  in the time interval *t* to *t*+*dt* with a positive derivative is equal to the probability that a' > 0 and that l - a'dt < a < l. This probability is given by the expression

$$\int_{0}^{\infty} da' \int_{l-a}^{l} dt \, daf(a,a') = dt \int_{0}^{\infty} da' a' f(l,a')$$

where f(a,a') is the joint probability density function of the amplitude a and its time derivative a' = da/dt. The probability that a will cross the level l in the time interval t to t+dt with a derivative of either sign is then

$$dt\int_{-\infty}^{\infty}|a'|\,f(l,a')\,da'$$

For stationary processes, the mean number of level crossings of P in the interval t to t+T then becomes

$$\langle N(P,T)\rangle = T \int_{-\infty}^{\infty} |a'| f(\sqrt{P},a') da'$$
.

The joint probability density function of the Rician distributed amplitude a and its time derivative a' is derived in Appendix B. This function is:



Figure 6. Realizations of Rician fading with  $f^{-4}$  Doppler spectra and scintillation indices of 1.0, 0.75, 0.5 and 0.25.

$$f(a,a') = \frac{2a}{P_0(1-R)} \exp\left[-\frac{a^2/P_0 + R}{1-R}\right] I_0\left[\frac{2a\sqrt{R/P_0}}{1-R}\right] \\ \times \left[\frac{\tau_0}{\Delta\sqrt{2\pi P_0(1-R)}}\right] \exp\left[-\frac{(\tau_0 a')^2}{2\Delta^2 P_0(1-R)}\right] .$$

$$(0 < a < \infty, -\infty < a' < \infty)$$

It can be seen from the form of this equation that the probability density function of a is Rician; the probability density function of a' is Gaussian with zero mean and variance of  $\Delta^2 P_0(1-R)/\tau_0^2$ ; and a and a' are independent. Also the functional form of f(a,a') is independent of the functional form of the Doppler spectrum. Only the parameter  $\Delta$  varies with the Doppler spectrum ( $\Delta = 1$  for the Gaussian spectrum,  $\Delta = 1.1858$  for the  $f^{-6}$  spectrum, and  $\Delta = 1.518$  for the  $f^{-4}$  spectrum).

The mean number of level crossings can now be easily evaluated with the result

$$\langle N(P,T) \rangle = \Delta \left( \frac{T}{\tau_0} \right) \left[ \frac{8P/P_0}{\pi(1-R)} \right]^{\frac{1}{2}} \exp \left[ -\frac{P/P_0+R}{1-R} \right] I_0 \left[ \frac{2\sqrt{RP/P_0}}{1-R} \right]$$

The effect of different Doppler spectra is to scale the mean number of level crossings by the quantity  $\Delta$ . This fact was shown qualitatively by comparing the realizations with different spectra in Figure 5.

Figure 7 shows plots of the mean number of crossings of P in one decorrelation time versus the ratio  $P/P_0$  for a Gaussian Doppler spectrum and several values of the scintillation index. For the Rayleigh case the maximum value of  $\langle N(P,T) \rangle$  occurs at  $P/P_0 = 1/2$  or -3 dB. As the scintillation index decreases the maximum value of  $\langle N(P,T) \rangle$  approaches 0 dB.

By noting that two level crossings are required to define the beginning and end of a fade, the number of fades per unit time below the level P is  $\eta = \langle N(P, \tau_0) \rangle / 2\tau_0$ . The mean separation  $\langle T_{sep}(P) \rangle$  of fades below P is then obtained from the mean number of fades per unit time. For any long time interval T the mean number of fades is  $\eta T$ , and the mean separation is just  $T/\eta T$  or  $1/\eta$ . Thus the mean separation of fades below P is

$$\langle T_{Sep}(P) \rangle = \frac{2\tau_0}{\langle N(P,\tau_0) \rangle}$$

The mean separation of fades below P is equal to the average time between crossings of P with either a negative value of a' (which defines the start of the fade) or with positive value of a' (which defines the end of the fade). Thus the mean separation of fades below P is also equal to the mean separation of flares above P.



# Figure 7. Mean number of level crossings per $\tau_0$ for several scintillation indices.

The mean duration  $\langle T_{Dur}(P) \rangle$  of fades below P is obtained as follows: During a long time interval T the total time that the power will be below P is F(P)T where F(P) is the cumulative distribution given in Equation 2.2. The mean duration is then the sum of all durations F(P)T divided by the number of fades  $\eta T$ . The result is

$$\langle T_{Dur}(P) \rangle = \frac{2\tau_0 F(P)}{\langle N(P,\tau_0) \rangle}$$
.

The mean duration  $\langle T_{Flare}(P) \rangle$  of a flare above P is the mean time that the power stays above P. Using the arguments given above, the mean separation of a fade or a flare is equal to the mean time that the signal is above P plus the mean time that it is below P,  $\langle T_{Dur}(P) \rangle + \langle T_{Flare}(P) \rangle = \langle T_{Sep}(P) \rangle$ . The mean duration of a flare is then

$$\langle T_{Flare}(P) \rangle = \frac{2\tau_0[1-F(P)]}{\langle N(P,\tau_0) \rangle}$$

The mean duration and separation of fades are shown in Figures 8 and 9, respectively, for a Gaussian Doppler spectrum and several values of the scintillation index. For other Doppler spectra, the curves in Figures 8 and 9 scale by  $1/\Delta$ .

The curves in Figure 8 show, for some power levels, that the duration of fades increases as the scintillation index is reduced. The mean duration of fades for  $S_4$  equal to 0.75 exceeds that of Rayleigh fading at all power levels: the mean fade duration for  $S_4$  equal to 0.5 exceeds that of Rayleigh fading except for  $P/P_0$  values between -4 and -2 dB; and the mean fade duration for  $S_4$  equal to 0.25 exceeds that of Rayleigh fading except for  $P/P_0$  values between -4 and -2 dB; and the mean fade duration for  $S_4$  equal to 0.25 exceeds that of Rayleigh fading except for  $P/P_0$  values between -13 and -1 dB. Note, however, that when  $S_4$  is equal to 0.25 the probability of a 13 dB fade is  $3.7 \times 10^{-10}$ , and the mean separation of 13 dB fades is  $7.4 \times 10^8 \tau_0$ . Thus for  $S_4$  values greater than about 0.25, it is possible to have fades that are longe: than occur at the same level with full Rayleigh amplitude statistics.



Figure 8. Mean duration of Rician distributed fades.

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Figure 9. Mean separation of Rician distributed fades.

## SECTION 3 SAMPLED RICIAN FADING

The requirements on the sampling of fading realizations are given in the DNA signal specification for nuclear scintillation [*Wittwer*, 1980] which requires a minimum of 100 decorrelation times per realization and 10 samples per decorrelation time. The questions that arise from this requirement can be summarized as: How close are such realizations to Rician fading? To address this question, random realizations of Rician fading are generated; moments of the amplitude, cumulative distribution, and mean fade duration and separation are measured; and these measured values are compared with their ensemble values.

Dana [1988] showed that  $100\tau_0$  realizations of Rayleigh fading are adequate for fade depths of 20 dB or less, and that  $400\tau_0$  realizations are necessary to simulate fades down to 30 dB. It was also shown in Dana [1988] that 10 samples per decorrelation time are sufficient when linear interpolation of the complex impulse response function is used to sample  $h(k\Delta t_{sam})$  40 times per decorrelation time.

Thus results in this section are, for the most part, limited to  $400\tau_0$  realizations sampled at  $\Delta t_{Sam} = \tau_0/40$ . Only the  $f^{-4}$  Doppler frequency PSD is considered for non-Rayleigh fading because this is the PSD recommended by DNA for slow, flat fading cases where the scintillation index is most likely to be less than unity.

Because of the finite number of samples in each realization, each measurement of realization statistics is a random variable with some mean and standard deviation. Variations in statistics from realization-to-realization are measured by generating a large number of realizations (1024 to be exact). Each parameter is measured by averaging over the entire realization. Average and standard deviation values of the 1024 measurements are computed. Thus the standard deviations below represent the realization-to-realization variation in the measurements of amplitude moments, cumulative distribution, and temporal statistics.

The measurement variation of the mean power of realizations can be calculated analytically, as discussed in Appendix C. It may be possible to compute measurement variances for other amplitude moments in the general case of Rician fading. Such a tedious exercise, however, is left to the determined reader. Power measurement variances below agree quite well with the analytic results given in Appendix C.

Three cases will be considered. The number of samples per realization N is 1024, 2048, or 4096, and the number of samples per decorrelation time  $N_0$  is 10. Here  $N_0$  is the number of samples per decorrelation time used to generate the realizations. Methods of generating such realizations are outlined in Appendix A. To measure the statistics of the realizations, linear interpolation of the real and imaginary parts of the impulse response function is used to obtain a sampling period  $\Delta t_{Sam}$  of  $\tau_0/40$ .

The objectives of this section are to present the means and standard deviations of amplitude moment, cumulative distribution, and temporal statistics, and to attempt to

answer the above question based on these results. This section is limited to flat fading realizations with varying values of the scintillation index and Doppler frequency power spectral density.

## 3.1 MEASURED FIRST ORDER STATISTICS.

One criterion for deciding that a realization has the proper Rician amplitude statistics is that measured moments of the amplitude should agree with Rician values within some tolerance. Ensemble values for the moments of the amplitude are obtained from Equation 2.1:

$$\begin{aligned} \langle a \rangle &= \frac{1}{2} \left[ \frac{\pi P_0}{1-R} \right]^{\frac{1}{2}} \exp \left[ -\frac{R}{2(1-R)} \right] \left\{ I_0 \left[ \frac{R}{2(1-R)} \right] + R I_1 \left[ \frac{R}{2(1-R)} \right] \right\} \\ \langle a^2 \rangle &= P_0 \\ \langle a^3 \rangle &= \frac{1}{4} \left[ \frac{\pi P_0^3}{1-R} \right]^{\frac{1}{2}} \exp \left[ -\frac{R}{2(1-R)} \right] \left\{ (3-R^2) I_0 \left[ \frac{R}{2(1-R)} \right] + 2R (2-R) I_1 \left[ \frac{R}{2(1-R)} \right] \right\} \\ \langle a^4 \rangle &= P_0^2 (2-R^2) \end{aligned}$$

where  $I_0(\cdot)$  and  $I_1(\cdot)$  are modified Bessel function.

These moments are plotted in Figure 10 versus the scintillation index for unity mean power. However, amplitude moments are easily obtained for other values of the mean power by noting that  $\langle a^n \rangle$  scales as  $P_0^{n/2}$ .

The scintillation index  $S_4$  is the standard deviation of the power. It is necessary but not sufficient that  $S_4$  equal unity for Rayleigh fading. The scintillation index is a good measure of the statistics of flares but not of fades.

Statistics that are sensitive to the distribution of fades are moments of the log amplitude. Using Equation 2.1 and a little algebra, these moments are found to be:

$$\langle \chi \rangle = \langle \ln a \rangle = \frac{1}{2} \ln \left[ P_0(1-R) \right] + \frac{1}{2} \exp \left[ -\frac{R}{1-R} \right] \sum_{n=0}^{\infty} \left[ \frac{R}{1-R} \right]^n \frac{\psi(n+1)}{\Gamma(n+1)}$$





$$\langle \chi^2 \rangle = \langle \ln^2 a \rangle = \ln \left[ \mathsf{P}_0(1-R) \right] \langle \chi \rangle - \frac{1}{4} \ln^2 \left[ \mathsf{P}_0(1-R) \right] \\ + \frac{1}{4} \exp \left[ -\frac{R}{1-R} \right] \sum_{n=0}^{\infty} \left[ \frac{R}{1-R} \right]^n \frac{\psi^2(n+1) + \zeta(2,n+1)}{\Gamma(n+1)}$$

The  $\psi$  and  $\zeta$  functions are:

$$\Psi(n+1) = -\gamma + \sum_{k=1}^{n} \frac{1}{k} = \Psi(n) + \frac{1}{n}$$

$$\zeta(2,n+1) = \sum_{k=n+1}^{\infty} \frac{1}{k^2} = \zeta(2,n) - \frac{1}{n^2}, \qquad \zeta(2,1) = \frac{\pi^2}{6}$$

where  $\gamma$  is Euler's constant ( $\gamma = 0.5772157...$ ).

The first two moments of log amplitude are plotted in Figure 11 versus the scintillation index for unity mean power.

Measured values of the mean and standard deviation of the amplitude moments,  $S_4$ ,  $\langle \chi \rangle$ , and  $\langle \chi^2 \rangle$  for Rician fading realizations are in Table 1 for eight cases including  $100\tau_0$ ,  $200\tau_0$ , and  $400\tau_0$  long realizations, three different Doppler frequency power spectral densities (PSDs), and four values of the scintillation index. Measured values for a single realization should equal the ensemble value plus or minus one or two standard deviations. It can be seen from the table that the average values are close to the ensemble values but the standard deviations of the higher amplitude moments can be as large as 20 percent of the measured values.

It is noteworthy that the measurement variation of  $\langle \chi \rangle$  increases dramatically as the scintillation index is reduced while that of  $\langle \chi^2 \rangle$  is relatively insensitive to  $S_4$ . An explanation for this curious behavior has not been discovered.



Figure 11. Log amplitude moments of the Rician distribution.

	[	Case							
	_	1	2	3	4	5	6	7	δ
	Ensemble Values								
N		1024	2048	4096	4096	4096	4096	4096	4096
N <sub>0</sub>		10	10	10	10	10	10	10	10
PSD		Gauss	Gauss	Gauss	f <sup>-6</sup>	f-4	f-4	f	f-4
$S_4$		1.0	1.0	1.0	1.0	1.0	0.75	0.5	0.25
		M	easured V	alues* (N	ormalized	to Ensen	nble Valu	es)	
$\langle a \rangle$	μ	0.999	0.998	0.999	0.997	0.996	0.998	0.999	1.000
	σ	0.054	0.040	0.029	0.028	0.027	0.027	0.018	0.009
$\langle a^2 \rangle$	μ	0.998	0.996	0.998	0.994	0.991	0.996	0.998	0.999
	σ	0.105	0.077	0.056	0.054	C 053	0.049	0.034	0.017
$\langle a^3 \rangle$	μ	0.995	0.993	<b>U.997</b>	0.991	0.986	0.994	0.997	0.999
	σ	0.161	0.0117	0.085	0.081	0.080	0.071	0.049	0.026
$\langle a^4 \rangle$	μ	0.991	0.988	0.995	0.989	0.984	0.991	0.995	0.998
	σ	0.226	0.164	0.119	0.113	0.111	0.094	0.065	0.034
S4	μ	0.982	0.989	0.996	0.998	0.997	0.995	0.994	0.993
	σ	0.084	0.061	0.046	0.044	0.042	0.043	0.040	0.038
$\langle \chi \rangle$	μ	1.000	1.005	1.004	1.013	1.017	1.004	1.003	1.009
	σ	0.213	0.155	0.114	0.109	0.105	0.180	0.273	0.548
$\langle \chi^2 \rangle$	μ	0.996	1.000	1.001	1.007	1.009	0.993	0.991	0.990
	σ	0.153	0.111	0.081	0.075	0.072	0.121	0.124	0.085
No	μ	1.018	1.011	1.004	0.998	0.999	0.999	0.999	0.999
	σ	0.083	0.056	0.038	0.048	0.055	0.055	0.055	0.054

 Table 1.

 Statistics of sampled Rician fading realizations.

\*  $\mu$  = Measured average value

10.

 $\sigma$  = Measured standard deviation

Perhaps a better criterion for the validity first order statistics is close agreement between the Rician and the measured cumulative distributions. Measured cumulative distributions (dots plus or minus one-sigma error bars) are plotted in Figures 12-16 for cases 5-8 in Table 1, respectively, along with the ensemble curves (Eqn. 2.2). A level of 0 dB corresponds to the mean power  $P_0$ . It can be seen from the figures that  $400\tau_0$  realizations do indeed have, on the average, a Rician distribution of fades.

#### 3.2 MEASURED SECOND ORDER STATISTICS.

Table 1 also contains the mean and standard deviation of the measured number of samples per decorrelation time. The measured value of  $N_0$  is obtained by performing an autocorrelation of the complex impulse response function and finding the  $e^{-1}$  point. Close agreement of this parameter with its ensemble value ensures that the realization will indeed have the desired decorrelation time in a simulation or hardware test.

The fidelity of the realizations in reproducing the second order statistics of Rician fading will be demonstrated by considering the mean fade duration and separation. The mean fade duration is a good statistic to examine for communications applications because errors often occur in bursts during deep fades. If the fades, on the average, are too long or too short, error bursts will not have the proper durations and the resulting receiver performance may be misleading.

Fade duration and separation measurements (dots plus or minus one-sigma error bars) and ensemble curves (solid lines) for the  $f^{-4}$  Doppler PSD are shown in Figures 16-19 for cases 5-8 respectively. Figure 16 shows the these measurements for full Rayleigh fading. Good agreement between the measure and ensemble values is seen, except for 30 dB fades. At this level the ensemble fade duration is  $0.026\tau_0$ , which is quite close to the sample duration of  $0.025\tau_0$ . As the scintillation index is reduced, measured mean fade durations are generally close to, if not right on, the ensemble curves. However, large variations are seen in the measured mean fade separations.

Two effects contribute to the low mean fade separation measurements seen for scintillation indices less than unity. Because separation measurements require two fades, some realizations do not contribute to the realization-to-realization fade separation statistics, thereby reducing the measured average. Also, it is not possible in these realizations to measure fade separations larger than about  $400\tau_0$ . Thus measured mean separations are biased to lower values because large random samples are absent.

In Figure 19, for a scintillation index of 0.25, a large discrepancy in the measured mean fade duration and separation is seen at fade level of +3 dB. Here the mean fade duration is about  $800\tau_0$ , which clearly cannot be accurately measured in  $400\tau_0$  realizations. Because the measured mean fade separation and measurer int variance at this level are *not* zero, at least two realizations must have had two +3 dB flares even though the probability of such an event is less than  $5 \times 10^{-4}$ . The measured mean duration of 5 dB fades (which occur with a probability of approximately  $3 \times 10^{-4}$ ) is close to the ensemble value of  $0.31\tau_0$ , but the measured mean fade separation is only ten percent of the ensemble value of  $1042\tau_0$ .

Except for low probability events with large durations or separations, these results demonstrate that  $400\tau_0$  Rician fading realizations sampled at  $\tau_0/40$  do indeed have the proper temporal statistics.



Figure 12. Measured cumulative distribution for  $S_4 = 1.0$ .



Figure 13. Measured cumulative distribution for  $S_4 = 0.75$ .


Figure 14. Measured cumulative distribution for  $S_4 = 0.5$ .



Figure 15. Measured cumulative distribution for  $S_4 = 0.25$ .



Figure 16a. Measured mean fade duration for  $S_4 = 1.0$ .



Figure 16b. Measured mean fade separation for  $S_4 = 1.0$ .



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Figure 17a. Measured mean fade duration for  $S_4 = 0.75$ .



Figure 17b. Measured mean fade separation for  $S_4 = 0.75$ .



Figure 18a. Measured mean fade duration for  $S_4 = 0.5$ .



Figure 18b. Measured mean fade separation for  $S_4 = 0.5$ .



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Figure 19a. Measured mean fade duration for  $S_4 = 0.25$ .



Figure 19b. Measured mean fade separation for  $S_4 = 0.25$ .

# SECTION 4 LIST OF REFERENCES

Bogusch, R. L., Digital Communications in Fading Channels: Modulation and Coding, AFWL-TR-87-52, MRC-R-1043, Mission Research Corporation, 1989.

Dana, R. A., Statistics of Sampled Rayleigh Fading, DNA-TR-89-5, MRC-R-1203, Mission Research Corporation, April 1988.

Dana, R. A., ACIRF User's Guide for the General Model (Version 3.5), DNA-TR-91-162, MRC-R-1358, Mission Research Corporation, June 1991.

Dana, R. A., A Non-Stationary Model for Frequency Selective Channels, MRC-R-1403, Mission Research Corporation, April 1992a.

Dana, R. A., Temporal Statistics of Non-Rayleigh Fading, MRC-R-1429, Mission Research Corporation, December 1992b.

De Raad, Jr., L. L., and M. K. Grover, First-Order Intensity Statistics for Non-Rayleigh Fading, DNA-TR-89-150, R&D Associates, February 1990.

Frasier, S. M., TEC Doppler and Delay Rate Realizations, MRC-N-780, Mission Research Corporation, March 1988.

Fremouw, E. J., R. C. Livingston, and D. A. Miller, "On the Statistics of Scintillating Signals," J. Aimos. Terr. Phys., Vol. 42, pp. 717-731, 1980.

Knepp, D. L., Propagation of Wide Bandwidth Signals Through Strongly Turbulent Ionized Media, DNA-TR-81-78, MRC-R-671, Mission Research Corporation, March 1982. Knepp, D. L., "Multiple Phase-Screen Calculation of the Temporal Behavior of Stochastic Waves," *Proc. IEEE*, Vol. 71, No. 6, pp. 722-737, June 1983.

Knepp, D. L., and L. A. Wittwer, "Simulation of Wide Bandwidth Signals That Have Propagated Through Random Media," *Radio Science*, Vol. 19, No. 1, pp. 303-318, January-February 1984.

Marcum, J. L., A Statistical Theory of Target Detection by Pulsed Radar: Mathematical Appendix, RM-753, RAND Corporation, July 1948.

Rice, S. O., "Statistical Properties of a Sine Wave Plus Random Noise," Bell System Technical Journal, Vol. 27, pp. 109-157, Janu 2ry 1948.

Rice, S. O., "Mathematical Analysis of Random Noise," in N. Wax (editor), Selected Papers on Noise and Stochastic Processes, Dover Publications, Inc., New York, 1954.

Rice, S. O., "Distribution of the Duration of Fades in Radio Transmission: Gaussian Noise Model," *Bell System Technical Journal*, Vol. 37, pp. 581-635, May 1958.

Rino, C. L., and E. J. Fremouw, "Statistics for Ionospherically Diffracted VHF/UHF Signals," *Radio Science*, Vol. 8, No. 3, pp. 223-233, March 1973.

Rino, C. L., R. C. Livingston, and H. E. Whitney, "Some New Rest its on the Statistics of Radio Wave Scintillation, 1. Empirical Evidence for Gaus an Statistics," J. Geophys. Res., Vol. 81, No. 13, pp. 2051-2057, 1976.

Whitney, H. E., J. Aarons, R. S. Allen, and D. R. Seeman, "Estimation of the Cumulative Amplitude Probability Distribution Function of Ionospheric Scintillations," *Radio Science*, Vol. 7, No. 12, pp. 1095-1104, December 1972.

Wittwer, L. A., A Trans-Ionospheric Signal Specification for Satellite  $C^3$  Applications, DNA 5662D, Defense Nuclear Agency, December 1980.

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# APPENDIX A REALIZATIONS OF RICIAN FADING

The methods of generating flat fading realizations of the impulse response function for Rician fading channels are simple extensions of Rayleigh fading methods discussed in detail elsewhere [e.g., Knepp, 1982; Knepp and Wittwer, 1984; Dana, 1991; Dana 1992a]. Only a brief review is presented this appendix.

The methods fall into two classes: Fourier transform and real-time digital filter techniques. The  $f^{-4}$  and  $f^{-6}$  Doppler Power Spectral Density (PSD) realizations are particularly simple to g serate using digital filters. Realizations with a Gaussian Doppler PSD are more easily generated using Fourier transforms. These methods will be reviewed in subsections of this appendix.

### A.1 FOURIER TRANSFORM TECHNIQUE FOR GAUSSIAN PSDs.

The starting point of the Fourier transform method of generating a realization of flat Rician fading is the Doppler frequency PSD function,  $S(\omega_D)$ . The Gaussian form of this function is:

$$S(\omega_D) = \sqrt{\pi} \tau_0 P_0(1-R) \exp\left[-\frac{\tau_0^2 \omega_D^2}{4}\right]$$
 (Gaussian PSD)

where  $P_0$  is the mean power of the realization, and 1-R is the fraction of power in the random component. The "Rician" index R is

$$R = \sqrt{1 - S_4^2}$$

where  $S_4$  is the scintillation index. The quantity  $S(\omega_D)d\omega_D/2\pi$  is the mean power in the Doppler radian frequency interval  $\omega_D/2\pi$  to  $(\omega_D + d\omega_D)/2\pi$ .

Discrete realizations of the charnel impulse response function will contain N time samples and  $N_0$  samples per decorrelation time. Thus the time spacing of the discrete samples is

$$\Delta t = \frac{\tau_0}{N_0} \; .$$

and the total time duration of the realization is  $N\Delta t$ . In the Doppler radian frequency domain the spacing of the discrete samples is

$$\Delta\omega_D = \frac{2\pi}{N\Delta t} \; .$$

Note that the quantity  $\Delta \omega_D \Delta t$ , which will appear later in a Fourier transform, is just  $2\pi/N$ .

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The samples in the frequency domain are generated by first calculating the fraction o signal power in each Doppler frequency bin,  $S_j = S(j\Delta\omega_D)\Delta\omega_D/2\pi$ . For the Gaussian PSD,

$$S_j = \frac{\sqrt{\pi}P_0(1-R)N_0}{N} \exp\left[-\frac{j^2\pi^2N_0^2}{N^2}\right], \quad (j = -N/2, \dots, N/2-1) .$$

Next the random Doppler frequency spectrum  $H(j\Delta\omega_D)$  of the impulse response function is generated:

$$H(j\Delta\omega_D) = \frac{2\pi}{\Delta\omega_D} \left[ \sqrt{S_j} \xi_j + \left( \sqrt{P_0 R} e^{i\varphi} \right) \delta_{j,0} \right] .$$

where R is the fraction of the total power in the constant component and  $\varphi$  is the constant phase of the Rician component. The quantity  $\delta_{j,k}$  is the Kronecker delta symbol:

$$\delta_{j,k} = \begin{cases} 1 & j = k \\ 0 & \text{otherwise} \end{cases}$$

The leading factor  $2\pi/\Delta\omega_D$  has been included in  $H(j\Delta\omega_D)$  so that the discrete Fourier transform of  $H(j\Delta\omega_D)$  will be dimensionless. Random components of the spectrum,  $\xi_j$ , are complex, normally disturbed random variables with the properties:

$$\langle \xi_j \xi_k^* \rangle = \delta_{j,k}$$
  
 $\langle \xi_j \xi_k \rangle = 0$ .

Thus the mean power of the  $\xi$  samples is unity. Random samples of  $\xi_j$  may be easily generated using

$$\xi_j = \sqrt{-\ln(u_{1,j})} \exp\left(2\pi i u_{2,j}\right)$$

where  $u_{1,j}$  and  $u_{2,j}$  are independent random variables uniformly distributed on the interval [0,1).

Finally the random Doppler spectrum of the channel impulse response function is Fourier transformed to the time domain. In continuous notation this Fourier transform is

$$h(t) = \int_{-\infty}^{\infty} H(\omega_D) \exp(i\omega_D t) \frac{d\omega_D}{2\pi} ,$$

and in discrete notation,

$$h(k\Delta t) = \sum_{j=-N/2}^{N/2-1} H(j\Delta\omega_D) \exp\left[i(j\Delta\omega_D)(k\Delta t)\right] \frac{\Delta\omega_D}{2\pi}$$
$$= \sum_{j=-N/2}^{N/2-1} \left[\sqrt{S_j} \xi_j + \left(\sqrt{P_0R}e^{i\varphi}\right)\delta_{j,0}\right] \exp\left[2\pi i(jk/N)\right]$$

where  $k = 0, 1, \dots, N-1$ .

# A.2 DIGITAL FILTER TECHNIQUE FOR $f^{-4}$ AND $f^{-6}$ PSDs.

An  $f^{4}$  or  $f^{4}$  realization can be generated by passing white Gaussian noise through cascaded single-pole filters, as described in *Dana* [1992a].

An  $f^{-4}$  filter can be created by cascading two single-pole filters:

$$y_k = ay_{k-1} + bx_{k-1}$$
 (A.1)  
 $x_k = ax_{k-1} + bv_{k-1}$ .

The coefficients a and b are<sup>1</sup>:

$$a = \exp(-\alpha_4 \Delta t / \tau_0) = \exp(-\alpha_4 / N_0)$$
$$b = \sqrt{1 - a^2}$$

where  $\alpha_4 = 2.146193$ . Discrete samples of the additive white Gaussian noise random process  $v_k$  are generated using the equation:

$$v_k = \left[\frac{(1-a^2)P_0(1-R)}{1+a^2}\right]^{\frac{1}{2}} \xi_k \; .$$

The  $v_k$  samples must have mean power given by the quantity in the square brackets so that the mean power of the filter output samples,  $y_k$ , will have mean power of  $P_0(1-R)$ . The discrete channel impulse response function in this case is

$$h(k\Delta t) = y_k + \sqrt{P_0 R e^{i\varphi}} .$$

To minimize the transient response at start-up it is necessary to initialize the filter. This is done by setting

<sup>&</sup>lt;sup>1</sup> Some authors prefer to include the gain of the filter in *b* coefficients. For example, see *Bogusch* [1989] Equation 2-40. Wittwer [1980] writes the  $f^{-4}$  filter equations as shown here but he combines the exponential in the *a* coefficient with the expression for the mean power of the input white Gaussian noise to obtain a hyperbolic tangent function.

$$y_0 = \sqrt{P_0(1-R)} u_0$$
$$x_0 = \left[\frac{(1-a^2)P_0(1-R)}{1+a^2}\right]^{\frac{1}{2}} u_1$$

where  $u_0$  and  $u_1$  are independent samples of the random process  $\xi$  uncorrelated with the  $v_k$  samples. The  $y_1$  and  $x_1$  samples are obtained from Equation A.1 and the first  $v_k$ sample,  $v_0$ . Even with this initialization there is a transient response because  $y_0$  and  $x_0$ do not have a "history" as they do after steady state is achieved. It is therefore suggested that the filter be "warmed up" for at least one decorrelation time before using the output.

An  $f^{-6}$  filter can be created by cascading three  $f^{-2}$  filters. The filter equations are therefore given by:

$$z_{k} = az_{k-1} + by_{k-1}$$

$$y_{k} = ay_{k-1} + bx_{k-1}$$

$$(A.2)$$

$$x_{k} = ax_{k-1} + by_{k-1}$$

The coefficients a and b are:

$$a = \exp(-\alpha_6 \Delta t / c_0) = \exp(-\alpha_6 / N_0)$$
$$b = \sqrt{1 - a^2}$$

where  $\alpha_6 = 2.904630$ . Discrete samples of the additive white Gaussian noise random process  $v_k$  are generated using the equation:

$$v_k = \left[\frac{(1-a^2)^2 P_0(1-R)}{1+4a^2+a^4}\right]^{\frac{1}{2}} \xi_k$$
.

Again the  $v_k$  samples must have mean power given by the quantity in the square brackets so that the mean power of the filter output samples,  $z_k$ , will have mean power of  $P_0(1-R)$ . The discrete channel impulse response function is

$$h(k\Delta t) = z_k + \sqrt{P_0 R} e^{i\varphi} .$$

Again, to minimize the transient response at start-up the initial filter values are:

$$z_0 = \sqrt{P_0(1-R)} u_0$$
$$y_0 = \left[\frac{(1-a^4)P_0(1-R)}{1+4a^2+a^4}\right]^{\frac{1}{2}} u_1$$

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$$x_0 = \left[\frac{(1-a^2)^2 P_0(1-R)}{1+4a^2+a^4}\right]^{\frac{1}{2}} u_2$$

where  $u_0, u_1$ , and  $u_2$  are independent samples of complex AWGN uncorrelated with the  $v_k$  samples. The filter should be "warmed up" for at least one decorrelation time before the output is used.

# A.3 WHAT ABOUT $f^{-2}$ PSDs?

An obvious question is: Why not discuss generation of realizations with an  $f^{-2}$ Doppler PSD? Indeed the expressions for  $x_k$  in Equations A.1 and A.2 are single-pole filters that produce realizations with  $f^{-2}$  Doppler PSDs:

$$x_k = a x_{k-1} + b v_{k-1} .$$

For this simple case, the coefficients a and b are:

$$a = \exp(-\Delta t/\tau_0) = \exp(-1/N_0)$$
  
 $b = \sqrt{1-a^2}$ .

The problem with this Markov process is that the temporal statistics are, strictly speaking, undefined. This is because the scale factor  $\Delta$  in the expression for the mean number of level crossings in Section 2.4 is

$$\Delta^2 = \frac{1}{2} \int_{-\infty}^{\infty} (\tau_0 \omega_D)^2 S(\omega_D) \frac{d\omega_D}{2\pi} . \qquad (A.3)$$

For the  $f^{-2}$  Doppler PSD,

$$S(\omega_D) = \frac{2\tau_0}{1+\tau_0^2\omega_D^2} .$$

and the expression for  $\Delta$  yields infinity.

Fortuna'ely, for a discrete realization there is a maximum Doppler frequency determined by the sample spacing. The highest Doppler frequency component in the sampled realizations has a period  $2\Delta t$ , corresponding to a maximum frequency of:

$$\omega_{D,max} = \frac{\pi N_0}{\tau_0} .$$

The value of  $\Delta$  for a sampled realization is then:

$$\Delta^2 = N_0 - \frac{\tan^{-1}(\pi N_0)}{\pi} .$$

For integer values of  $N_0$  this expression reduces to  $N_0$ .

Thus the mean number of level crossing is finite and the mean duration and separation of fades are non-zero. Unfortunately these quantities depend on  $N_0$ . As the number of samples per decorrelation time is increased, the mean number of level crossing increases and the mean fade duration decreases.

The dependence of the temporal statistics of the  $f^{-2}$  Doppler PSD realization on  $N_0$  is likely to be unacceptable in most applications. Thus only Doppler PSDs with a frequency roll-off greater than  $f^{-3}$  (so Eqn. A.3 is finite) should be used to generate realizations of Rician fading. This will ensure that the realization temporal statistics are well-behaved.

## APPENDIX B JOINT PROBABILITY DENSITY FUNCTION f(a,a')

The purpose of this appendix is to derive the joint probability density function of the Rician amplitude a and its time derivative a' = da/dt. This function is required to calculate the temporal statistics of Rician fading. A less general form of this derivation was first published by *Rice* [1948].

The starting point for this calculation is the determination of the joint probability density function of the random in-phase and quadrature components x and y of the complex envelope of the electric field. It is assumed that x and y are independent, have zero mean, and that they are normally distributed. Thus the joint probability density function of x and y is

$$f(x,y) = \frac{1}{2\pi\sigma^2} \exp\left[-\frac{x^2 + y^2}{2\sigma^2}\right] .$$
 (B.1)

Now the joint probability density function of the time derivatives x' = dx/dt and y' = dy/dt must be calculated. It will be shown that x and x' are independent, as are y and y'. It will be assumed that x, x', y, and y' are jointly independent. Thus the joint probability density function of x' and y' is all that is needed in addition to Equation B.1 to write down the joint probability density function f(x,x',y,y'). Once this function has been obtained, a simple change of variables from x, x', y, and y' to a and a' will yield the desired function.

In order to determine the distribution of x' (or y'), consider the random function x(t) written as a Fourier stochastic integral

$$x(t) = \int_{-\infty}^{\infty} z(\omega_D) \exp(i\omega_D t) \frac{d\omega_D}{2\pi} .$$
 (B.2)

The quantity  $z(\omega_D)$  is a random function in the Doppler frequency domain. It is useful to assume that  $z(\omega_D)$  is a zero-mean, normally distributed random process, although this is not necessary because the central limit theorem will make x(t) normally distributed for almost any reasonable distribution of  $z(\omega_D)$ . However, with the normal assumption for  $z(\omega_D)$ , x(t) is the sum of many independent, normally distributed random variables, and is necessarily a zero-mean, normally distributed random variable.

Before continuing, it is interesting to show the relationship between the random spectral components  $z(\omega_D)$  and the Doppler spectrum  $S(\omega_D)$ . The correlation function of the stationary process x(t) may be written as

$$\rho(t_2 - t_1) = \frac{\langle x(t_1)x(t_2) \rangle}{\sigma^2}$$
(B.3)

$$= \int_{-\infty}^{\infty} \frac{d\omega_{D_1}}{2\pi} \int_{-\infty}^{\infty} \frac{d\omega_{D_2}}{2\pi} \frac{\langle z(\omega_{D_1})z^*(\omega_{D_2})\rangle}{\sigma^2} \exp(i\omega_{D_1}t_1 - i\omega_{D_2}t_2) .$$

However the correlation function  $\rho(\tau)$  may also be written in terms of  $S(\omega_D)$ :

$$\rho(\tau) = \int_{-\infty}^{\infty} S(\omega_D) \exp(i\omega_D \tau) \frac{d\omega_D}{2\pi} . \qquad (\text{Fi.4})$$

The spectrum  $S(\omega_D)$  must be an even function if the correlation function  $\rho(\tau)$  is to be real.

To ensure the integral in Equation B.3 is only a function of time difference  $\tau = t_1 - t_2$ , the integrand must contain a factor  $2\pi\delta(\omega_{D_1} - \omega_{D_2})$ . Using the Dirac delta function to collapse the double integral in Equation B.3 and comparing the result with Equation B.4 gives

$$\langle z(\omega_{D_1})z^*(\omega_{D_2})\rangle = 2\pi\sigma^2 \,\delta(\omega_{D_1}-\omega_{D_2})\,S(\omega_{D_1}) \quad . \tag{B.5}$$

This equation also demonstrates that the random Doppler spectral components of  $z(\omega_D)$  are uncorrelated, which is a consequence of the assumption that the random process x(t) is stationary.

The time derivative of x(t) is given by differentiating Equation B.2, with a similar expression holding for y':

$$x'(t) = \int_{-\infty}^{\infty} (i\omega_D) z(\omega_D) \exp(i\omega_D t) \frac{d\omega_D}{2\pi} .$$

Because  $z(\omega_D)$  is normally distributed with zero mean, x'(t) will also be normally distributed with zero mean. The variance of x'(t) is

$$\langle x'(t)x'(t)\rangle = \int_{-\infty}^{\infty} \frac{d\omega_{D1}}{2\pi} \int_{-\infty}^{\infty} \frac{d\omega_{D2}}{2\pi} \omega_{D1} \omega_{D2} \langle z(\omega_{D1})z^*(\omega_{D2})\rangle \exp\left[i(\omega_{D1}-\omega_{D2})t\right]$$
$$= \sigma^2 \int_{-\infty}^{\infty} \omega_D^2 S(\omega_D) \frac{d\omega_D}{2\pi} = -\sigma^2 \frac{d^2 \rho(\tau)}{d\tau^2} \Big|_{\tau=0} .$$
(B.6)

The variance of x'(t) may be written in the general form:

$$\langle x'(t)x'(t)\rangle = \frac{2\sigma^2\Delta^2}{\tau_0^2}$$

where

$$\Delta = \begin{cases} 1 & \text{Gaussian Doppler PSD} \\ \alpha_6/\sqrt{6} = 1.1858 & f^{-6} \text{ Doppler PSD} \\ \alpha_4/\sqrt{2} = 1.5176 & f^{-4} \text{ Doppler PSD} \end{cases}$$

and where the parameters  $\alpha_4$  and  $\alpha_6$  were determined in Section 2.2.

The cross correlation of x'(t) and x(t) is

$$\langle x'(t)x(t)\rangle = \int_{-\infty}^{\infty} \frac{d\omega_{D1}}{2\pi} (i\omega_{D1}) \int_{-\infty}^{\infty} \frac{d\omega_{D2}}{2\pi} \langle z(\omega_{D1})z^*(\omega_{D2})\rangle \exp\left[i(\omega_{D1}-\omega_{D2})t\right]$$
$$= -i\sigma^2 \int_{-\infty}^{\infty} \omega_D S(\omega_D) \frac{d\omega_D}{2\pi} = 0 \quad . \tag{B.7}$$

Equation B.5 and the fact that  $S(\omega_D)$  is an even function have been used in reducing Equations B.6 and B.7. Because x(t) and x'(t) are uncorrelated and normally distributed, they are also independent. Identical results hold for the variance of y' and the cross correlation of y and y'.

The joint probability density function of x, x', y, and y' may now be written down:

$$f(x,x',y,y') = \left(\frac{1}{2\pi\sigma^2}\right) \exp\left[-\frac{x^2+y^2}{2\sigma^2}\right] \left(\frac{\tau_0^2}{4\pi\sigma^2\Delta^2}\right) \exp\left[-\frac{\tau_0^2(x'^2+y'^2)}{4\sigma^2\Delta^2}\right] .$$

This function may be transform to the desired function of a and a' by making the change of variables

$$x + r \cos \vartheta = a \cos \theta$$
$$y + r \sin \vartheta = a \sin \theta$$

where r is the constant component of Rician fading and  $\vartheta$  is the constant phase. The time derivatives of x and y are

$$x' = a' \cos \theta - a\theta' \sin \theta$$
$$y' = a' \sin \theta + a\theta' \cos \theta$$

which gives the polar coordinate equations

$$x^{2} + y^{2} = a^{2} + r^{2} - 2ar\cos(\theta - \vartheta)$$
$$x^{2} + y^{2} = a^{2} + a^{2}\theta^{2}.$$

The probability density function coordinate transformation is

$$(x,x',y,y') dx dx' dy dy' = f(a,a',\theta,\theta') |\det(J)| da da' d\theta d\theta'$$

where the determinate of the Jacobian of the transformation is

$$\det (J) = \det \begin{bmatrix} \frac{\partial x}{\partial a} & \frac{\partial x'}{\partial a} & \frac{\partial y}{\partial a} & \frac{\partial y'}{\partial a} \\ \frac{\partial x}{\partial a'} & \frac{\partial x'}{\partial a'} & \frac{\partial y}{\partial a'} & \frac{\partial y'}{\partial a'} \\ \frac{\partial x}{\partial \theta} & \frac{\partial x'}{\partial \theta} & \frac{\partial y}{\partial \theta} & \frac{\partial y'}{\partial \theta'} \end{bmatrix}$$
$$= \det \begin{bmatrix} \cos\theta & -\theta'\sin\theta & \sin\theta & \theta'\cos\theta \\ 0 & \cos\theta & 0 & \sin\theta \\ -a\sin\theta & -a'\sin\theta - a\theta'\cos\theta & a\cos\theta & a'\cos\theta - a\theta'\sin\theta \\ 0 & -a\sin\theta & 0 & a\cos\theta \end{bmatrix}$$
$$= a^{2},$$

The joint probability density function  $f(a,a',\theta,\theta')$  is

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$$f(a,a',\theta,\theta') = \left(\frac{a^2}{2\pi\sigma^2}\right) \exp\left[-\frac{a^2 + r^2 - 2ar\cos(\theta - \vartheta)}{2\sigma^2}\right] \\ \times \left(\frac{\tau_0^2}{4\pi^2\Delta^2\sigma^2}\right) \exp\left[-\frac{\tau_0^2(a'^2 + a\theta'^2)}{4\Delta^2\sigma^2}\right] .$$

. .

The joint probability density function of a and a' is obtained by integrating this equation over  $\theta$  and  $\theta'$ :

$$f(a,a') = \int_{0}^{2\pi} d\theta \int_{-\infty}^{\infty} d\theta' f(a,a',\theta,\theta') ,$$

with the result

$$f(a,a') = \left(\frac{a}{\sigma^2}\right) \exp\left[-\frac{a^2 + r^2}{2\sigma^2}\right] I_0\left[\frac{ar}{\sigma^2}\right] \left(\frac{\tau_0}{2\sqrt{\pi}\Delta\sigma}\right) \exp\left[-\frac{\tau_0^2 a'^2}{4\Delta^2 \sigma^2}\right] \quad . \tag{B.8}$$

 $I_0$  is the modified Bessel function that results from performing the integral:

$$I_0(z) = \frac{1}{2\pi} \int_0^{2\pi} \exp(z\cos\theta) d\theta \quad .$$

Thus it is apparent from Equation B.8 that the probability density function of a is Rician; the probability density function of a' is normal with zero mean and variance of  $2\Delta^2 \sigma^2/\tau_0^2$ ; and a and a' are independent because their joint probability density function is separable into a function of a times a function of a'.

# APPENDIX C VARIATION IN THE MEASUREMENT OF MEAN POWER

The  $n^{th}$  moment of the amplitude  $a_k$  of an impulse response function realization with N samples is measured using the formula

$$\mu_n = \frac{1}{N} \sum_{k=1}^N a_k^n$$

Because of the finite length of a realization,  $\mu_n$  is a random variable. The purpose of this appendix is to develop general expressions for the mean and variance of  $\mu_n$ , and then to apply those expressions to compute the expected variation,  $\sigma_2^2$ , in the measured mean power of a realization:

$$\sigma_{\mu}^2 = \langle \mu_2^2 \rangle - \langle \mu_2 \rangle^2 \ .$$

This variation depends primarily on the number of decorrelation times in the realization,  $N/N_0$ , where  $N_0$  is the number of samples per decorrelation time. It is weakly dependent on the Doppler frequency power spectral density (PSD) and on the values of N and  $N_0$ .

The mean value of  $\mu_n$  is easy to compute:

$$\langle \mu_n \rangle = \frac{1}{N} \sum_{k=1}^N \langle a_k^n \rangle = \langle a^n \rangle$$

where  $\langle a^n \rangle$  is the ensemble mean value of the  $n^{th}$  moment of amplitude. The second moment of  $\mu_n$  is a little more of a challenge to compute:

$$\langle \mu_n^2 \rangle = \frac{1}{N^2} \sum_{k=1}^N \sum_{l=1}^N \langle a_k^n a_l^n \rangle = \frac{\langle a^{2n} \rangle}{N} + \frac{2}{N} \sum_{k=1}^{N-1} (1 - k/N) R_n(k)$$

where  $R_n(k)$  is the correlation of the  $n^{th}$  moment of amplitude:

$$R_n(k) = \langle a_l^n a_{l+k}^n \rangle .$$

For the general case of Rician fading and arbitrary n, the joint probability density function of the mplitude at two times,  $f(a_1,a_2)$ , is needed to compute the correlation function. However in the special case of mean power where n is two, the correlation function is easily computed from the statistics of the underlying complex voltage.

The power in a sample of the impulse response function with a Rician amplitude distribution is

$$a_k^2 = [x_k + r\cos\vartheta]^2 + [y_k + r\sin\vartheta]^2$$
(C.1)

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where  $x_k$  and  $y_k$  are uncorrelated, normally-distributed random processes with zeromean and variance  $\sigma^2$ . The "Rician" components  $r \cos \vartheta$  and  $r \sin \vartheta$  are constant. It is assumed that the random processes x at two times is jointly normal:

$$f(x_1,x_2) = \frac{1}{2\pi\sigma^{2}\sqrt{1-\rho^2}} \exp\left[-\frac{x_1^2 - 2\rho x_1 x_2 + x_2^2}{2\sigma^2(1-\rho^2)}\right]$$

Values of the two-point correla on  $\rho$  are determined by the functional form of the Doppler PSD and the time difference between the samples  $x_1$  and  $x_2$ . A similar expression holds for the joint probability density function of  $y_1$  and  $y_2$ .

To compute the variance of the mean power measurement, the quantity  $\langle a_1^2 a_2^2 \rangle$  is required. Using Equation C.1 this quantity involves terms of the form

$$\langle x_1 \rangle = \langle x_2 \rangle = \langle y_1 \rangle = \langle y_2 \rangle = 0 \langle x_1^2 \rangle = \langle x_2^2 \rangle = \langle y_1^2 \rangle = \langle y_2^2 \rangle = \sigma^2 \langle x_1 x_2 \rangle = \langle y_1 y_2 \rangle = \sigma^2 \rho \langle x_1 x_2^2 \rangle = \langle x_1^2 x_2 \rangle = \langle y_1 y_2^2 \rangle = \langle y_1^2 y_2 \rangle = 0 \langle x_1^2 x_2^2 \rangle = \langle y_1^2 y_2^2 \rangle = \sigma^4 (1 + 2\rho^2) .$$

The cross correlation  $\langle a_1^2 a_2^2 \rangle$  is then

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$$\langle a_1^2 a_2^2 \rangle \; = \; 4 \sigma^4 (1 + \rho^2) + 4 r^2 \sigma^2 (1 + \rho) + r^4 \;\; . \label{eq:alpha2}$$

The Rician amplitude r and the variance  $\sigma^2$  are written in terms of the scintillation index  $S_4$  so that the mean power  $\langle a^2 \rangle$  is constant and equal to  $P_0$ :

$$r^2 = P_0 R$$
$$2\sigma^2 = P_0 (1-R)$$

where the "Rician" index is

$$R = \sqrt{1 - S_4^2} \, .$$

Combining these results gives the following expression for the variance in the measured mean power:

$$\frac{\sigma_{\mu}^2}{P_0^2} = \frac{1 - NR^2}{N} + \frac{2}{N} \sum_{k=1}^{N-1} (1 - k/N) [R + (1 - R)\rho(k)]^2 .$$
(C.2)

The two-point correlation  $\rho(k)$  is

C--2

	$\left[\exp\left[-(k/N_0)^2\right]\right]$	Gaussian Doppler PSD
$\rho(k) = \langle$	$[1 + \alpha_6 k/N_0 + (\alpha_6 k/N_0)^2/3] \exp[-\alpha_6 k/N_0]$	f <sup>-6</sup> Doppler PSD
	$\left[1 + \alpha_4 k N_0\right] \exp\left[-\alpha_4 k N_0\right]$	f <sup>-4</sup> Doppler PSD

where the coefficients  $\alpha_4$  ( $\alpha_4$ =2.146139) and  $\alpha_6$  ( $\alpha_6$ =2.904630) are determined by the requirement that  $\rho(N_0)=e^{-1}$ .

Plots of the power measurement standard deviation are shown in Figure 20 for N equal to 1024, 2048, and 4096. The value of  $N_0$  is 10 for each case, so the curves correspond to realizations of length  $102.4\tau_0$ ,  $204.8\tau_0$ , and  $409.6\tau_0$ , respectively. Solid lines in the figure are for a Gaussian Doppler frequency PSD, and solid circles are for an  $f^{-4}$  Doppler PSD.

As expected, the mean power measurement variation is larger for realizations with fewer decorrelation times. The measurement variation decreases with decreasing scintillation index because the fluctuating part of the impulse response contributes less and less to the total power. For a given value of N there is little difference between the results for the two PSDs. This is because the three correlation functions above differ little for values of k less than  $N_0$  where  $\rho(k)$  is close to unity, but vary significantly for larger values of k where  $\rho(k)$  is small. Thus the differences in  $\rho(k)$  for differing Doppler frequency PSDs occur in Equation C.2 at values of k that contribute little to the sum.





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