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Petu (1. Jurken PETER A. LURKER, Lt Col, USAF, BSC Acting Director Biodynamics and Biocommunications Division Armstrong Laboratory

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PREFACE

This report was prepared by the Noise Effects Branch, Armstrong Laboratory in conjunction with a vulnerability assessment test of the F-15A crew station conducted by the Sulvivability Enhancement Branch, WL/FIST.

The author gratefully acknowledges Capt Denise West, AL/CFBA for her assistance in preparing the hearing assessment chapter, and Mr Henry T. Mohlman for his assistance in the graphic display of the data. The author is also thankful to Ms Jackie Brennaman and Ms Bea Heflin for the preparation of this report for publishing and to Mr Jerry Speakman for his editorial comments.

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INTRODUCTION

A live fire test was conducted to evaluate the vulnerability of a F-15 pilot to the impact of ballistic projectiles striking the F-15 crew station. The primary emphasis of this test program was the evaluation of pilot shielding, premature initiation of the emergency escape system and the possible disabling of the mechanical and electrical flight control system. As part of this test program the blast overpressure was measured from 21 different projectiles/velocities/directions striking a section of the F-15 fuselage (Fuselage Station FS 250.5 to FS 415) to assess potencial crew hazards. A manikin placed in the cockpit was instrumented with four pressure transducers to measure the overpressure at the right and left ear and at the upper and lower Time histories for each recording and the sound exposure torso. spectrum levels as a function of frequency are presented. A hearing damage risk assessment is made in the context of the Air Force hearing damage risk criteria (AFR 161-35)³, and laboratory data⁴ regarding the effects of intense blast overpressures on man.

TEST CONDITIONS AND PROCEDURES

During this program tests were conducted using 21 different projectiles aimed and fired at the F-15 fuselage section, installed at Range 2 of the Aircraft Survivability Research Facility (ASRF), WPAFB,OH. The F-15 cockpit with manikin was installed in a fixture, to allow a rotation in place to achieve shotlines from above, below and either side. The projectiles used for each test with the different charges, velocities and directions are listed in Table 1 TEST MATRIX. The tests were typically conducted every two days to allow time for repair of damages to the fuselage section caused by the different projectile strikes and for removal and examination of the manikin.

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The gun, firing the differenc projectiles, was placed for most tests at a distance of 15 feet from the crew station. The velocity of the fired projectiles ranged from 1500 ft/sec to 5000 ft/sec and by computing and comparing the traveling times of the projectiles and the speed of sound, in most cases the actual overpressure from the impact of the projectile was recorded. Although at the lower projectile velocities contamination of the recorded signal from the gun fire noise may have occurred due to the small difference in the velocity of the projectile and the speed of sound.

Instrumentation

The cockpit with the manikin in place was instrumented with four pressure transducers. One each transducer was mounted at the seat approximately 4 inches away from the helmet of the manikin next to the area of the right and left ear. One transducer was placed near the midline of the upper torso and the fourth transducer was positioned near the midline of the lower torso. The placement of the transducers with a dimension of 0.7 inches in diameter and 1.6 inches long did not interfere with the positioning of the ballistic projectile strikes to the manikin. The transducers were piezo-electric microphones with a frequency response from 0.5 Hz - 10000 Hz and a measurement range from 0.005 psf to 1200 psf (80 dB to 190 dB SPL sound pressure level). They are totally sealed and the extreme environments experienced during these tests did not affect the accuracy.

The signal from each transducer was recorded by the BOOM EVENT ANALYZER RECORDER (BEAR).¹ Four such devices were employed since this unit is a single channel instrument specially developed for recording impulsive type overpressures. This instrument is based on a 16 bit microprocessor that continuously samples the background noise and captures and stores the waveforms of any intense impulsive noise. The BEAR digitizes the signal from the microphone at a sampling rate of 8 kHz and has a frequency range

from 0.5 Hz to 2500 Hz with a dynamic range of 80 dB. The data from the BEAR is stored in removable RAM modules with a memory of 512 kbytes. The data on the modules are transferred via a Data Retrieval Unit (DRU) and then interfaced with a computer and existing software for processing. The unit is selfcontained and can operate for up to seven days without replacing the batteries.

An acoustical calibration signal was applied to each system shortly before each test to assure proper operation. Any change in signal level was adjusted to obtain an accuracy of +/- 1 dB for all test data.

Four additional pressure transducers were installed alongside the BEAR microphones. The output of these transducers were connected to the ASRF on-site data aquisition system and provided an instantaneous readout of the overpressures generated during the impact of projectiles. This additional capability complimented the BEAR instrumentation. It extended the measthement range of up to 50 psi (7200 psf) or 204 dB sound pressure level.

Data Analysis

In these tests, the BEAR recorder was triggered by the overpressure generated from the projectile impact and/or explosion inside the crew station and the captured acoustical signal was stored in the RAM modules. The data stored in these modules were transferred through the Data Retrieval Unit (DRU) to a Z-100 computer which processed and displayed each recorded event, time of occurrence and summary information for all data This analysis was performed the same day after each stored. test, to ensure proper operation of the systems and allow for any adjustments necessary for the next test. The overpressures were analyzed in terms of maximum overpressure in pounds/sqft, max sound pressure level in dB re 20 µPa and sound exposure spectrum level (1Hz bandwidth) as a function of frequency. In addition a time history was plotted for each recorded firing. Reviewing the analyzed data of the blast overpressures with such sharp rise times, one would expect significant energy at higher frequencies. However the frequency spectrum analysis of the data showed that the levels at 2500 Hz were significantly reduced. Therefore the peak noise levels should not be affected since they are only partly influenced by the high frequency content of the spectrum.

The data are plotted in Fig.1 through Fig.50. The lowest overpressure which was recorded was 7 psf or 145 dB and the highest level recorded was 1875 psf or 193 dB sound pressure level. Table 2 COCKPIT MAX OVERPRESSURE (PSF) and MAX SPL (dB) summarizes the data for each test and location. During some tests a signal was not recorded due to electro-magnetic interference which rendered the system inoperable or the threshold levels were set too high and the BEAR did not record the event. However, it can be seen that the sound pressure levels recorded in the cockpit are fairly uniformly distributed, although the projectiles were fired from different elevations and azimuths.

In Table 3 COMPARISON OF MAX OVERPRESSURE a comparison was made between overpressures as recorded by the BEARs and as measured by the ASRF on-site data acquisition system. The levels as recorded by the on-site system are listed in italics. Agreement between the two recorded overpressures is reasonable since one can expect a difference in level due to the placement and mounting of the microphone.

Transducers were also installed at the upper torso and lower torso. The data were analyzed and are presented in the same format as the data recorded at earlevel. Analysis for nonauditory damage such as injury to the lung or other internal organs was not performed. In the literature the estimated threshold for lung damage is reported to occur at overpressures of 2160 PSF or 194 dB SPL².

HEARING DAMAGE RISK ASSESSMENT

The AFR 161-35³ is used for the assessment of Hazardous Noise Exposure of Air Force personnel exposed to continuous noise environs and impulse noise such as gun fire and similiar phenomena. For impulse noise it requires that the waveform of the impulse be analyzed for the peak overpressure and for two different durations, the pressure-wave (A) duration and the pressure-envelope (B) duration of the impulse signal. The limiting exposures for a 100 msec impulse without reflection ("A" duration) is 152 dB SPL and 140 dB SPL for impulses with reflected wave components ("B" duration). These values are valid for an exposure of 100 pulses/day over a period not less than 4 min per day. This criteria cannot be applied to the Live Fire In a real world scenario a pilot would experience only one Test. or two exposure during a day with a much higher peak overpressure level. For this reason the AFR 161-35 was not used for this study in the hearing risk assessment.

However, data obtained from a recent US Army study⁴ can be compared with the Live Fire blast overpressure measurements. In that study human subjects were exposed to the noise from explosive charges and the temporary hearing loss was measured. The subjects wore muff type hearing protection and were exposed to a series of 50 blasts on the same day with a peak level of 193 dB sound pressure level (SPL). For these subjects a temporary change in hearing of less than 15 dB was observed which is a mild temporary hearing loss and should not result in any loss of auditory function.

The Live Fire Tests were conducted under similiar conditions. However the numbers of exposures as reported in the US Army study far exceed the single exposures analyzed for the Joint Live Fire Tests. The highest level measured was 193 dB (Test Nr. 26) and the crew member (manikin) was wearing the standard Air Force flight helmet type HGU 55/P which provides hearing protection in the frequency range from 125 Hz to 8 kHz and to some degree in the lower frequencies. In these tests only one projectile was fired per day which represents a real live scenario during a air-to-air combat engagement. Comparing the measured levels recorded during the live fire test with the finding of the US Army study⁴, the impact on the hearing and communication of the pilot or crew member during the Live Fire Test can be estimated. From these Live Fire exposures crew members could experience a mild reduction in hearing but these hearing changes would not be sufficient to impair communication capability.

CONCLUSION

The maximum blast overpressure (193 dB) measured during this test was higher than an individual would normally experience. Comparing the findings of the US Army study⁴ with the data of the Live Fire Test, only mild temporary hearing losses can be expected by the F-15 pilots and crewmembers and it should not affect their ability to communicate with ground stations and/or other aircraft.

Little information in the literature is available on the response of humans to impulse or blast overpressure levels of this magnitude, except for subjective reports from voluntary subjects exposed to higher than normal overpressure levels. These observations and some predictions have been tabulated in Table 4 AUDITORY RESPONSE TO BLAST OVERPRESSURE².

F-15A LIVE FIRE TEST TEST MATRIX

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TEST NR.	IMPACT AREA	THREAT	AZ/EL	VELOCITY
5	Left Side Fuselage	12.7mm API	90/0 deg	1500 ft/s
6	Left Side Fuselage	12.7mm API	90/30 deg	1500 ft/a
8	Left Side Rear	12.7mm API	120/30 deg	1500 ft/s
9	Right Side Rear Avionic Bay	23 mm HEI/MG-25	225/45 deg	2200 ft/s
10	Left Center Fuselage	110 gr fragm.	60/60 deg	5000 ft/s
11	Left Center Fuselage	12.7 mm API	60/60 deg	1500 ft/s
12	Left Rear Fuselage	12.7mm API	150/45 deg	1500 ft/s
14	Right Front Fuselage	23 mm API	345/45 deg	2200 ft/s
15	Ctr Front Fuselage	23 mm API	0/15 deg	2200 ft/s
16	Right Front Fuselage	23 mm HEI/MG-25	315/45 deg	2200 ft/s
17	Left Front Fuselage	30 mm HEI/A-30	15/45 deg	2000 ft/s
18	Left Ctr Fuselage	110 gr fragm,	60/30 deg	6000 ft/s
19	Canopy from Rear	110 gr fragm.	160/30 deg	5000 ft/s
20	Canopy from Rear	12.7 mm API	150/30 deg	1500 ft/s
22	Left through Canopy	23 mm HEI/MG-25	45/0 deg	2200 ft/s

F-15A LIVE FIRE TEST TEST MATRIX

TEST NR.	IMPACT AREA	THREAT	AZ/EL	VELOCITY
23.	Right Side Fuselage	23 mm HEI/MG-25	270/0 deg	2200 ft/s
24	Right Side Fuselage	12.7 mm API	270/0 deg	1600 ft/a
25	Left Side Fuselage	30 mm HEI/A-30	135/0 deg	2000 ft/s
26	Bottom Landiong Gear	23mm HEI/MG-25	180/60 deg	2200 ft/s
27		unknown		
		:	ľ	
	1			

Table l

F-15A LIVE FIRE TEST COCKPIT MAX OVERPRESSURE (PSF) - MAX SPL (dB)

TEST NR.	RIGHT	EAR	LEFT	EAR	UPPER	TORSO	LOWER -	rorso
	PSF	SPL	PSF	SPL	PSF	SPL	PSF	SPL
5	83	166	65	164	-	-	53	162
6	-	-	-	-	-	-	-	- 1
8	-	-	-	-	-	-	-	-
9	396	179	212	174	148	171	128	170
10	-		21	154	25	155	-	-
11		-	43	160	50	161	67	164
12	-	-	10	148	-	-	7	145
14	-	-	-	. - '	-	-	45	161
15	-	-	-	· _ ·	77	165	70	164
16	l	-	í -	· • i	-	-	-	-
17	115	169	100	168	-	-	123	169
18	-	-	-		77	165	77	165
19	89	167	91	167	73	165	37	159
20	368	179	295	177	117	169	130	170
22	872	186	-	' _	-	-	1285	190
23	595	183	653	184	744	185	700	185
24	98	167	88	166	73	165	98	167
25	444	181	-	-	399	180	335	178

PSF in Ibs/sqft

. *

SPL in dB re .00002 N/sqm

F-15A LIVE FIRE TEST COCKPIT MAX OVERPRESSURE (PSF) - MAX SPL (dB)

TEST NR.	RIGHT	EAR	LEFT	EAR	UPPER	TORSO	LOWER	TORSO
	PSF	SPL	PSF	SPL	PSF	SPL	PSF	SPL
28 27	1875 1016	193 188	1866 1062	193 188	1830 1183	193 189	1481 1050	191 188
			1					
			2 1 1	Į				
			,					
ł	PSF in 빈	s/sqft				SPL	in dB re .0	0002 N/sqm

F-15A LIVE FIRE TEST COMPARISON OF MAX OVERPRESSURE

EST N	R .	RIGHT	EAR	LEFT	EAR	UPPER	TORSO	LOWER	rorso
		PSF	SPL	PSF	SPL	PSF	SPL	PSF	SPL
5	B K	83 174	166 <i>172</i>	65 114	164 169	- 133	- 170	53 108	162 168
9	B K	396 146	179 171	212 258	174 176	148 <i>141</i>	171 <i>171</i>	128 <i>174</i>	170 <i>172</i>
16	B K	- 259	- 176	- 262	- 176	- 229	- 175	- 259	- 176
17	B K	115	169 <i>169</i>	100 104	168 <i>168</i>	- 94	- 167	123 <i>94</i>	169 <i>167</i>
18	B	- 165	172	- 187	- 173	- 288	- 177	- 396	- 180
19	В <i>К</i>	89 115	167 <i>169</i>	91 <i>139</i>	167 <i>170</i>	73 84	165 <i>166</i>	37 50	159 <i>161</i>
20	B K	368	179 -	295	177 -	117 203	169 <i>174</i>	130 <i>194</i>	170 <i>173</i>
	8	- Bear	Transdu	Cer			PSF I	n Ibs/sqft	

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K - Kistler Transducer

SPL in dB re .00002 N/sqm

F-15A LIVE FIRE TEST COMPARISON OF MAX OVERPRESSURE

TEST N	IR.	RIGHT	EAR	LEFT	EAR	UPPER	TORSO	LOWER	rorso
		PSF	SPL	PSF	SPL	PSF	SPL	PSF	SPL
22	в	872	186	-	-	-	-	1285	190
6 , 6,	K	1267	189	-	-	-	-	626	184
23	B	595	183	653	184	744	185	700	185
20	κ	662	184	720	185	691	184	669	184
25	В	444	181	-	-	399	180	335	178
	K	720	185	864	186	360	179	353	179
26	В	1875	193	1866	193	1830	193	1491	191
20	К	3168	198	1958	193	2232	195	2232	195
27	в	1016	188	1062	188	1183	189	1050	188
	κ	-	-	1339	190	1440	191	1037	18 8
						1			
				-		ł			
	в	- Bear T	'ra-sdu	cer			PSF ir	l ibs/soft	
	ĸ	- Kistlei	Transe	ducer			SPLI	n dB re .00	002 N/sqm

Table 3

Auditory Response to Blast Overpressure

Nature of Auditory Response	Blast Overpressure Experience or Prediction
Rupture of the Tympanic Membrane	None Expected Below 720 PSF None Observed up to 144 PSF
Aural Pain	None Observed up to 144 PSF
Shori Temporary Fullness, Tinnitus	Reported Above 95 PSF
Hearing Loss: Permanent	None Expected from Frequency and Intensity of Blast Overpressure Occurrence
Hearing Loss: Temporary	Mild Temporary Hearing Loss Measured at Exposure of 1875 PSF

TABLE 4















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