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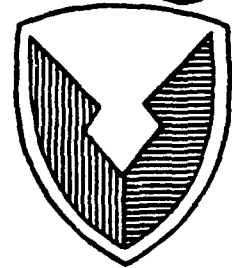


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MATERIEL COMMAND

METEOROLOGICAL INFLUENCES ON SMOKE/OBSCURANT
EFFECTIVENESS PHASE I I

Volume II

by

Steven R. Hanna, David G. Strimaitis
Joseph C. Chang and Sharon M. McCarthy

Sigma Research Corporation
234 Littleton Road, Suite 2E
Westford, Massachusetts 01886

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TABLE OF CONTENTS

- Appendix A: Representativeness of Wind Measurements on a Mesoscale Grid with Station Separations of 312 m to 10000 m
- Appendix B1: Uncertainty Associated with Emission Rate Estimation
- Appendix B2: Analysis of Fog-Oil Smoke Emissions
- Appendix C: Uncertainties in Source Emission Rate Estimates using Dispersion Models
- Appendix D: Display of Relations among Data using Box Plots
- Appendix E: User's Guide for the Sigplot Plotting Package
- Appendix F1: Listings of the Dugway Data Archives - Historical Datasets
- Appendix F2: Listings of the Dugway Data Archives - Smoke/Obscurant Datasets

APPENDIX A

REPRESENTATIVENESS OF WIND MEASUREMENTS ON A
MESOSCALE GRID WITH STATION SEPARATIONS OF 312m TO 10000m

To Appear in Boundary Layer Meteorology

Appendix A

Table of Contents

Abstract	A-1
1. Objective	A-2
2. Previous Studies of Mesoscale Wind Variability	A-2
Empirical Studies of St. Louis Data	A-3
Theoretical Analysis of Spatial Structure	A-4
3. Proposed Formula	A-6
4. Field Experiment at Hereford, Colorado	A-8
5. Analysis of Hereford Data	A-11
5.1 Single Station Variances as a Function of Averaging Time	A-11
5.2 Statistics of Pairs of Observing Stations	A-14
6. Recommended Empirical Formula for Variances	A-19
7. Test of General Equation with Independent Data	A-20
Acknowledgement	A-23
References	A-23

Appendix A

List of Tables

Table	Page
A-1 Steady-State Periods from the Herford Dataset Selected for Analysis.	A-12
A-2 Ratios of Variances $\sigma^2(T_a)/\sigma^2(1 \text{ min})$ for Averaging Times, T_a , of 10 and 60 min., for Wind Speed and Wind Direction at the Herford Site. Results are Given for Each Run. The Median of the Ratios for the Thirteen Stations is Given. The Scatter of the Ratios for the Thirteen Stations about any Median has a Standard Deviation of about 0.05 to 0.10. Medians over all Dates are Given at the Bottom.	A-15
A-3 Observations and Model Predictions for Dugway Proving Ground Wind Data, with Tower Separation of 500m, for All Levels Combined, and Wind Speed and Direction Combined. Medians are Listed for the Observed Values. Model Parameters are given in the Footnotes.	A-22

Appendix A

Table of Figures

Figure	Page
A-1 Schematic diagram of wind station locations at the Hereford site. Terrain sloped slightly downward from west to east with an average slope of 1%. North is towards the tip of the figure and there is 10 km spacing between stations 1 and 7 or stations 7 and 13.	A-10
A-2 Time series of five-minute averaged wind speed (u) and wind direction (θ) for Station 3 for 31 March 1990 at the Hereford site. Thick lines indicate steady-state periods selected for analysis.	A-13
A-3 Spatial correlation coefficient, R , as a function of station separation for E-W and N-S legs of Hereford monitoring network. Wind speed (u) correlations are on the left, and wind direction (θ) correlations are on the right. Medians over all eleven runs are shown for averaging times of 1 min. (Long Dashes), 10 min. (Short Dashes), and 60 min. (Solid Line). The standard deviation of the scatter of the 11 points about each line is about 0.2.	A-17
A-4 Spatial correlation coefficients, R , for various spatial separations, Δx , and averaging times, T_a (1 min; * 10 min; + 60 min) from Hereford site. Plotted are the medians over eleven runs, E-W and N-S legs, and wind speed and wind direction observations. Typical scatter of all the data about each line is about 0.2 at a correlation of 0.5. Empirical curves from Equation (A-17) are drawn (dotted, $T_a = 1$ min.; dashed, $T_a = 10$ min.; solid, $T_a = 60$ min.).	A-18

Appendix A

Representativeness of Wind Measurements on a
Mesoscale Grid with Station Separations of 312m to 10000m

by

Steven R. Hanna and Joseph C. Chang

Sigma Research Corp., 234 Littleton Road, Suite 2E, Westford, MA 01886

Abstract

A field experiment was carried out in which wind speed and direction were measured over flat terrain at a height of 10 m using 13 identical instruments spaced logarithmically along two perpendicular 10 km lines. Station separations ranged from 312 m to 1000 m. One-minute data from 11 sampling periods of duration 6 to 10 hours were studied.

The statistics showed little dependence on whether the line of instruments was oriented along the wind or across the wind, or whether wind speeds or wind directions were being analyzed. The integral time scale derived from the variation of the single station variances with averaging time was found to equal several minutes. The correlation coefficients between two stations separated by distance Δx were found to vary exponentially with Δx , with an integral distance scale on the order of 1 km. At a station separation of 10 km, the correlation coefficient equals 0.24, 0.37, and 0.47 for averaging times of 1, 10, and 60 minutes respectively. These correlation coefficients correspond to root-mean-square differences in wind speed at the two stations of about 1.2, 1.1, and 1.0 m/s respectively.

Empirical equations based on dimensional analysis are suggested for fitting these observations. It is found that the observations are best fit if two independent integral time scales are used - a boundary-layer time scale about 300s that best applies to small averaging times or small separations and a mesoscale time scale of about 1800s that applies to larger averaging times or large separations.

1. Objectives

In order to solve most atmospheric transport and dispersion problems, it is necessary to assume that the wind measurements at one site represent the wind flow at a nearby site. The separation between these two sites can range from 10 m to 100 km. This assumption is sometimes quite good, but situations often occur where wind direction observations differ by 180° between two towers in the same mesoscale network. There are a few limited studies of wind variability over mesoscale distances (e.g. Perry et al. (1978), Lockhart and Irwin (1980), Hanna (1982), and Panofsky and Dutton (1984)), but there is much more theoretical and observational work needed.

This study is part of a comprehensive research program in which the contributions of meteorological uncertainties to errors in air quality modeling and source emission estimation are being investigated. A cooperative two week field experiment was conducted in which 13 wind instruments were set up along an "L-shaped" pattern with maximum station separation of 10 km. Variances and spatial correlations of wind speeds and directions are calculated, with the objective being the development of simplified empirical/theoretical formulas. The accuracy of these simplified formulas is calculated and suggestions made for using these formulas in more generalized mesoscale settings. Finally, the formulas were tested with independent data from a wind study at Dugway Proving Ground.

2. Previous Studies of Mesoscale Wind Variability

The literature contains two types of studies of mesoscale wind variability. Both employ near-surface wind observations made by two or more wind monitors with separations of 10 m to 100 km. In the first type of study, the variances for a variety of wind monitor separations are calculated and presented, and a very simple empirical formula is suggested (e.g., Lockhart and Irwin (1980) and Hanna (1982)). In the second type of study, theoretical formulas based on spectral analyses are applied to the problem (e.g., Pielke and Panofsky (1970), Perry et al. (1978) and Panofsky and Dutton (1984)). Reviews of these two types of studies are given below.

Empirical Studies of St. Louis Data. During the St. Louis Regional Air Pollution Study (RAPS), hourly-averaged wind observations were recorded for one year from a network of twenty-five wind monitors. The separation of the wind monitors ranged from 3 km to 80 km. Lockhart and Irwin (1980) and Hanna (1982) report calculations of the standard deviation, σ , of the difference in wind speed, u , and wind direction, θ , for concurrent measurements between each pair of stations. For example, the following procedure is used to calculate $\sigma_{(u_a - u_b)}$ for any pair of stations, a and b, over the entire sampling period:

$$\sigma^2_{(u_a - u_b)} = \frac{\sum_{i=1}^N (u'_a - u'_b)^2}{N} \quad (\text{A-1})$$

where the primes indicate deviations from the average speed at each station and N is the total number of time periods being analyzed. As the separation distance between the stations decreases, this standard deviation should asymptotically approach the standard deviation due to instrument errors for two co-located wind monitors. Lockhart and Irwin (1980) suggested the regression formulas:

$$\sigma_{(\theta_a - \theta_b)} = 15 + 5.7 \ln x \quad (\text{A-2})$$

$$\sigma_{(u_a - u_b)} = 0.47 + 0.24 \ln x \quad (\text{A-3})$$

where x is in km, θ is in degrees, and u is in m/s. The median value of $\sigma_{(\theta_a - \theta_b)}$ is about 33° and $\sigma_{(u_a - u_b)}$ is about 1.2 m/s, at a median separation distance of about 20 km. The standard deviations of the points scattered about equations (A-2) and (A-3) are 0.16 m/s and 4° , respectively.

Hanna (1982) reported an analysis by Nappo of the same set of RAPS wind data, emphasizing the dependence of the standard deviations of the wind differences upon wind speed. Nappo defined the spatial standard deviations, $\sigma_{\Delta u}$ and $\sigma_{\Delta \theta}$ using the set of concurrent measurements at the 25 monitoring stations. For example, the following procedure is used to calculate $\sigma_{\Delta u}^2$ for any given hour:

$$\sigma_{\Delta u}^2 = \frac{\sum_{i=1}^{24} \sum_{n=i+1}^{25} (u'_i - u'_n)^2}{24!} \quad (\text{A-4})$$

where the prime indicates a deviation from the overall average speed for the 25 stations. The magnitude of the spatial standard deviation, $\sigma_{\Delta u}$ is expected to be somewhat larger than that calculated from equation (A-2), since the differences in the means among the stations are included in equation (A-4). It was found that the differences in wind speed and direction among the stations increase by a factor of three or four as wind speed decreases from 5.0 m/s to about 1.5 m/s. At higher wind speeds (~10 m/s), asymptotic limits of about 5° for σ_θ and about 0.15 for σ_u/u are evident. The following empirical formulas fit these data:

$$\sigma_{\Delta\theta} = (5^\circ)^2 + (60^\circ/u)^2 \quad (\text{A-5})$$

$$(\sigma_{\Delta u}/u)^2 = (0.15)^2 + (0.6/u)^2 \quad (\text{A-6})$$

where u is in m/s and σ_θ is in degrees.

Theoretical Analyses of Spatial Structure

Panofsky and Dutton (1984, Chapter 9) discuss the technical issues related to the differences in wind velocities measured at two points. They look at the problem from the point of view of the spectrum of sizes of turbulent eddies. They make a distinction between vertical separations, Δz , lateral (cross-wind) separations, Δy , and longitudinal (along-wind) separations, Δx , between the locations of the measurements. Because turbulent eddies tend to maintain their identities as they travel with the wind, at a given separation the along-wind correlations in wind velocities between the measurement stations should be larger than the vertical or cross-wind correlations.

These authors also point out that most of the correlation between wind velocities at two points is due to larger turbulent eddies, with dimensions approximately equal to or larger than the separation between the points. By the same argument, the wind fluctuations in small eddies at one point are uncorrelated with the wind fluctuations in the same size of eddies at a distant point.

Because of the fact that the larger eddies move with the wind flow and slowly change with time, the maximum correlation between two time series of wind velocities at two points separated by an along-wind distance, Δx , may occur at a time lag of about $\Delta x/\bar{u}$, where \bar{u} is the mean wind speed. This is the approximate time required for an air parcel to travel from the first point to the second point.

The issues raised in the previous three paragraphs have led Panofsky and Dutton (1984) and others to the hypothesis that the spatial correlations are functions of the eddy size, the wind speed, and the separation between the wind observation points. They use a mathematical expression known as the coherence, which "is a measure of the square of the correlation between the Fourier component of two time series with their phases adjusted to obtain maximum correlation." The coherence is a function of eddy frequency, n , and is given by:

$$\text{coh}(n) = \frac{[\text{Co}^2(n) + Q^2(n)]}{S_1(n) S_2(n)} \quad (\text{A-7})$$

where $S_1(n)$ and $S_2(n)$ are estimates of the spectral density of the two time series at points 1 and 2, $\text{Co}(n)$ is the cospectrum, and $Q(n)$ the quadrature spectrum. The frequency, n , can have units of cycles per second or radians per second. The cospectrum refers to the correlation due to in-phase fluctuations and the quadrature spectrum refers to the correlation due to fluctuations that are 90° out of phase. The coherence ranges from zero, for no correlation, to one for perfect correlation. In order to calculate $\text{coh}(n)$ for two long time series, specialized computer software for carrying out time series analysis is needed.

Pielke and Panofsky (1970) generalized an empirical expression for the coherence, $\text{coh}(n)$, based on a suggestion by Davenport (1961):

$$\text{coh}(n) = \exp(-a_i n \Delta x_i / u) \quad (\text{A-8})$$

where the subscript i refers to the direction component and the dimensionless "constant", a_i , is called the "decay parameter." Observations show that " a_i " is typically in the range from 1 to 10. The dimensionless variable, $n \Delta x_i / u$, is often referred to as the reduced frequency. It is found that the "constant," a_i , is in fact a function of station separation, Δx . Other investigators have found a_i to be a function of the ambient stability, the turbulence intensity, and the integral time or distance scale of the turbulence. For example, Perry et al (1978) propose the following formula for horizontal station separations, Δx :

$$a = (65\sigma_w / u) + (6.3\sigma_v \Delta x / u L_y) \quad (\text{A-9})$$

where σ_w and σ_v are the standard deviations of turbulent velocity fluctuations in the vertical and cross-wind directions, and L_y is the lateral integral distance scale of the lateral turbulence.

3. Proposed Formula

The relation between wind speed, u , or wind direction, θ , observed at two stations at positions 1 and 2 can be expressed in terms of a variance or a correlation. The relationship between the two quantities can be derived by beginning with the identity:

$$\sigma_{\Delta u}^2 = \overline{(u_2' - u_1')^2} = \overline{u_2'^2} + \overline{u_1'^2} - 2 \overline{u_1' u_2'} \quad (\text{A-10})$$

where the primes refer to fluctuations (i.e., the means have been already subtracted) and the overbar refers to a time average. If the two variances $\overline{u_2'^2}$ and $\overline{u_1'^2}$ are equal, then equation (A-10) can be written in the form:

$$\sigma_{\Delta u}^2 / 2\sigma_u^2 = 1 - R_{12} \quad (\text{A-11})$$

where $\sigma_u^2 = \overline{u'^2}$ and the correlation coefficient $R_{12} = \overline{u_1' u_2'} / \sigma_u^2$. Thus if the correlation equals 1, 0, or -1, the ratio $\sigma_{\Delta u}^2 / 2\sigma_u^2$ will equal 0, 1, or 2, respectively. For two stations that are separated by such a large distance that the correlation equals zero, then Equation (A-11) states that $\sigma_{\Delta u}^2 = 2\sigma_u^2$.

After investigating the semi-theoretical formulas (A-8) and (A-9), it was decided that there was so much adjustment of "constants" taking place that it was best to begin with a simpler formula based on dimensional analysis. This simpler formula does not explicitly include the frequency, n , but does account for frequency effects through the implicit assumption that wind speed autocorrelograms are exponential (i.e., $R = \exp(-\Delta t/T_I)$, implying that a so-called Markov-energy spectrum is valid) and are completely determined once an integral time scale, T_I , or space scale, Λ_I , is specified. The following dimensionless relationship can then be postulated:

$$\sigma_{\Delta u}^2 / 2\sigma_u^2 = f(\Delta x, T_I, \Lambda_I, T_a) \quad (\text{A-12})$$

where f is a universal dimensionless function, and variables and parameters are defined in the following way:

$$\sigma_{\Delta u}^2 = \overline{(u_2' - u_1')^2}, \quad \text{where } u_1' \text{ and } u_2' \text{ are wind speed fluctuations at positions 1 and 2.}$$

$$\sigma_u^2 = (\sigma_{u_1}^2 + \sigma_{u_2}^2) / 2 \quad \text{is the average turbulent energy at positions 1 and 2.}$$

Δx is the horizontal separation between positions 1 and 2.

T_I is the integral time scale of the time series of wind speed fluctuations measured at position 1 or position 2.

Λ_I is the integral space scale of the correlogram of wind fluctuation differences ($u_i' - u_1'$) measured between positions 1 and i for several positions.

T_a is the averaging time.

The averaging time, T_a , is very important because it is typically of the same order of magnitude as the integral time scale (i.e., within the range from 1 min to 1 hr). As T_a approaches zero, the ratio $\sigma_{\Delta u}^2/2\sigma_u^2$ reaches a maximum at any given station separation, since there are poor correlations between wind fluctuations in smaller eddies at two positions.

Exponential shapes are proposed for all correlation functions:

$$R(\Delta x/\Lambda_I) = \exp(-\Delta x/\Lambda_I) \quad (A-13a)$$

$$R(\Delta t/T_I) = \exp(-\Delta t/T_I) \quad (A-13b)$$

The following approximation to Taylor's equation is used to account for the effects of averaging time on variances:

$$\sigma^2(T_a)/\sigma^2(0) = (1 + T_a/2T_I)^{-1} \quad (A-14)$$

For a given separation, Δx , the spatial correlation $R(\Delta x/\Lambda_I)$ is also going to depend on averaging time, T_a , since the effects of the fluctuations due to small eddies will drop to zero at large averaging times. Consequently, $R(\Delta x/\Lambda_I)$ should approach unity as T_a increases, and the second term in the following empirical formula is proposed to account for this effect:

$$\begin{aligned} R(T_a, \Delta x) &= \overline{u_2' u_1'} / \sigma_{u_1} \sigma_{u_2} (T_a, \Delta x) \\ &= \exp(-\Delta x/\Lambda_I) + (1 - \exp(-\Delta x/\Lambda_I)) g(T_a u/\Lambda_I) \end{aligned} \quad (A-15)$$

where the dimensionless function $g(T_a u/\Lambda_I)$ approaches zero as T_a approaches zero and approaches unity as T_a becomes very large.

4. Field Experiment at Hereford, Colorado

The research programs summarized in Section 2 all took advantage of wind observations made at two or more locations. However, none of these wind observations satisfied all of the following desired characteristics of a study

in which differences in wind observations are being calculated.

- Flat terrain with few obstructions.
- All wind instruments alike, with relatively fast response and adequate calibration procedures.
- Five or more wind stations along a line with spacings ranging from a few hundred meters to 10000 meters.
- Two perpendicular lines of wind stations.
- Several days or more of one-minute averaged wind observations.

A field experiment was designed to satisfy these characteristics, using instruments and technicians from the National Center for Atmospheric Research (NCAR). Thirteen identical wind stations from NCAR's Portable Automated Mesonet (PAM) were set up in flat, open farmland (mostly covered by short, winter-weathered grass) near Hereford, Colorado, and operated for the two week period between 30 March 1990 and 14 April 1990. The instruments were installed, maintained and calibrated by experienced NCAR technicians. The anemometers were located at an elevation of 10 m above the ground. A schematic diagram of the relative instrument locations is given in Figure A-1. The slope of the terrain is less than about 1% over the entire network. It is seen that logarithmic spacings (312.5m, 625m, 1250m, 2500m, 5000m, 10000m) are used for the instruments along each leg of the "L"-shaped network. The perpendicular axes were used in order to determine if there was a significant difference between the along-wind and cross-wind statistics.

The resulting "Hereford" dataset contained values of N-S and E-W components of the wind velocity at one minute resolution. First, these wind components were converted to wind speed, u , and wind direction, θ , for each minute. Because the threshold of these instruments was about 0.5m/s, periods with reported wind speeds less than 0.5m/s were flagged and not used in the analysis. 5-minute averages of u and θ were made and the resulting time series for each station plotted for the entire 16 day duration of the study (see Figure A-2 for an example of the time series plots for 31 March 1990 Station 6). Visual inspection of the 15 days of time series in the figure revealed that, most of the time, the wind speed and direction are quite variable and unsteady in time. For example, during the afternoon on 1 April and 10 April, the wind speed went through a cycle in which it increased from

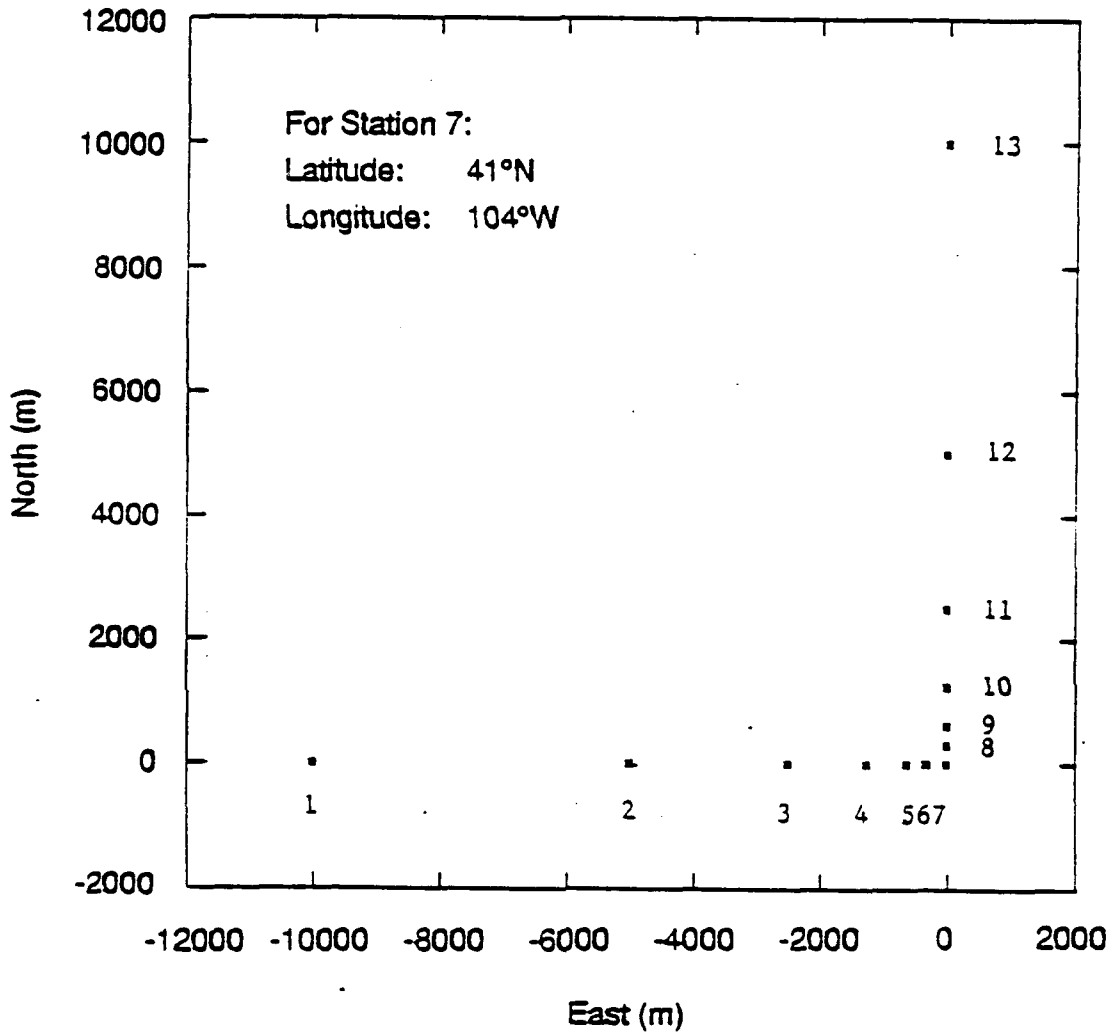


Figure A-1. Schematic diagram of wind station locations at the Hereford site. Terrain sloped slightly downward from west to east with an average slope of 1%. North is towards the top of the figure and there is 10 km spacing between stations 1 and 7 or stations 7 and 13.

nearly zero to about 10 m/s and decreases back down to zero again. This large half-sine-wave would totally dominate any statistical analysis of these wind data.

Because it became clear that any time series analysis of the 16 days would be overly influenced by diurnal changes and synoptic effects, it was decided to confine the analysis to time periods on the order of 6 to 10 hours, when the wind speed and direction appeared to be relatively steady. The eleven steady-state periods that were chosen are listed in Table A-1. Two of these periods are indicated by thick lines in Figure A-2. Median values of wind speed, u , wind direction, θ , standard deviation of wind speed, σ_u , and standard deviation of wind direction, σ_θ , are also listed on the table. These eleven periods are seen to cover a wide range of wind speeds (2.5 to 10.5 m/s), wind directions (170° to 330°) and times of the day.

5. Analysis of Hereford Data

This section presents the results of the analysis of the Hereford data and the next section presents some empirical formulas that fit this dataset. As a first step, variances and time and space correlations were calculated for averaging times of 1, 10, and 60 minutes. A linear trend (estimated from the data from all 13 stations) was removed from the data from each run. Because steady-state periods have been selected and linear trends have been removed, much of the influence of larger mesoscale and regional eddies has been removed there statistics. As will be shown, mesoscale eddies with time scales less than the sampling time are still strongly reflected in the statistics.

5.1 Single Station Variances as a Function of Averaging Time

The variances in the wind speed and wind direction time series were calculated for each of the eleven "steady-state" runs, for each of the thirteen stations, for averaging times of 1, 10, and 60 min. The data are presented in a Table A-2, in the form of ratios of the variance for 10 or 60 minute time periods to the variance for the one minute time period. The medians over the thirteen stations are listed. The overall medians at the

Table A-1

Steady-State Periods from the Hereford Dataset Selected for Analysis.
 Meteorological Parameters Represent Medians over 13 Stations

Date/Run	Time	Wind Speed u(m/s)	Wind Direction $\theta(^{\circ})$	σ_u (m/s)	σ_{θ} ($^{\circ}$)
0330	00-10	2.5	130	0.7	17
0330	14-24	3.0	215	0.8	17
0331	00-08	3.5	200	0.45	10
0331	16-24	7.5	325	1.2	13
0404	06-12	5.5	90	1.2	13
0404	12-20	7.5	135	1.2	10
0406	18-24	4.0	215	0.9	14
0409	14-24	10.5	10	1.3	8
0411	06-16	3.0	170	0.9	13
0412	00-08	5.5	140	1.1	11
0413	14-20	7.5	330	1.1	10

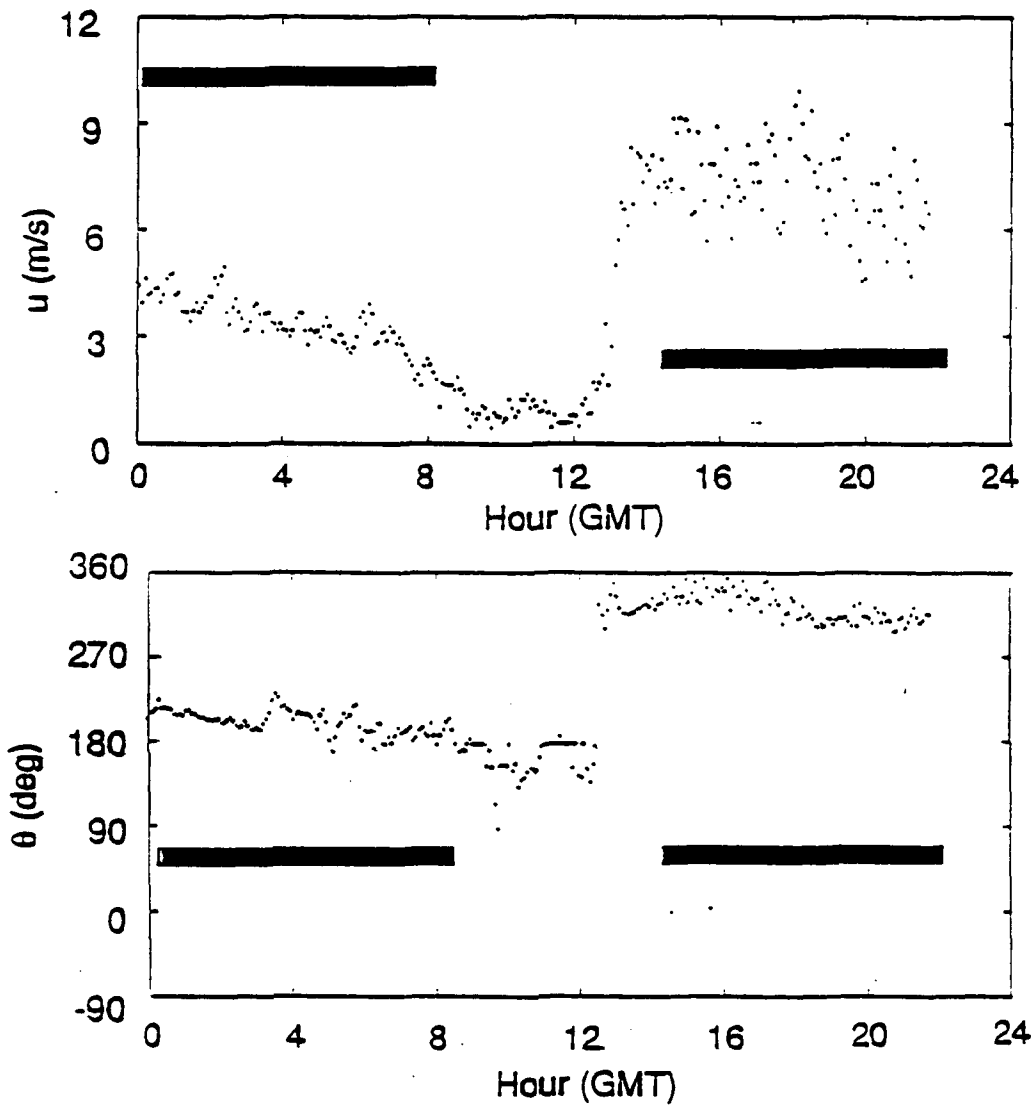


Figure A-2. Time series of five-minute averaged wind speed (u) and wind direction (θ) for Station 3 for 31 March 1990 at the Hereford site. Thick lines indicate steady-state periods selected for analysis.

bottom of the table suggest that there is little difference between the statistics for wind speed and wind direction, with medians of the variance ratios of about 0.68 for $\sigma^2(10 \text{ min})/\sigma^2(1 \text{ min})$ and about 0.39 for $\sigma^2(60 \text{ min})/\sigma^2(1 \text{ min})$. The run-to-run variability in the median variance ratios is about ± 0.20 , with no dependence on wind speed, wind direction, σ_u , σ_θ , or time of day. For a given day, the station-to-station variability in the variance ratios is typically about ± 0.05 to 0.10.

Table A-2 suggests that observed median values of $\sigma^2(10 \text{ min})/\sigma^2(1 \text{ min})$ and $\sigma^2(60 \text{ min})/\sigma^2(1 \text{ min})$ are 0.68 and 0.37, respectively. Solving Equation (14) for the integral time scale T_I , we obtain $T_I \approx 9 \text{ min}$ for $T_a = 10 \text{ min}$ and $T_I \approx 15 \text{ min}$ for $T_a = 60 \text{ min}$. This trend is duplicated in all types of calculations in this analysis, i.e., the derived time and distance integral scales increase as the averaging time, T_a , or station separation, Δx , increase. Persistent mesoscale eddies are associated with turbulence at time scales of several hours and distance scales of several tens of kilometers. Superimposed on these "baseline mesoscale eddies" are the smaller turbulent eddies normally thought to be associated with the atmospheric boundary layer. Consequently it is assumed that the turbulent velocity field is described by two time scales, one (T_{I1}) associated with boundary layer turbulence, and another (T_{I2}) associated with mesoscale eddies. These two time scales are assumed to contribute equally to $\sigma^2(T_a)$, leading to the following modification to Equation (A-14):

$$\frac{\sigma^2(T_a)}{\sigma^2(0)} = \frac{0.5}{1 + T_a/2T_{I1}} + \frac{0.5}{1 + T_a/2T_{I2}} \quad (\text{A-16})$$

The Hereford dataset is best-fit by $T_{I1} \approx 300\text{s}$ and $T_{I2} \approx 1800\text{s}$, which yield $\sigma^2(10)/\sigma^2(1) = 0.71$ (slightly above the median observation of 0.68) and $\sigma^2(60)/\sigma^2(1) = 0.35$ (slightly below the median observation of 0.37).

5.2 Statistics for Pairs of Observing Stations

The spatial statistics to be presented are all keyed to wind station (7) at the corner of the "L" of the network shown in Figure A-1. The results in this section are given for the spatial correlation coefficient,

Table A-2

Ratios of Variances $\sigma^2(T_a)/\sigma^2(1 \text{ min})$ for Averaging Times, T_a , of 10 and 60 min., for Wind Speed and Wind Direction at the Hereford Site. Results are Given for Each of Eleven Runs. The Median of the Ratios for the Thirteen Stations is Given. The Scatter of the Ratios for the Thirteen Stations about any Median has a Standard Deviation of about 0.05 to 0.10. Medians over all Dates are Given at the Bottom.

Run Date/Time	$\sigma_u^2(T_a)/\sigma_u^2(1 \text{ min})$		$\sigma_\theta^2(T_a)/\sigma_\theta^2(1 \text{ min})$	
	Wind Speed		Wind Direction	
	10 Minute	60 Minute	10 Minute	60 Minute
0330/00-10	.88	.61	.93	.58
0330/14-24	.71	.58	.69	.50
0331/00-08	.74	.39	.77	.36
0331/16-24	.41	.21	.64	.25
0404/06-12	.55	.19	.81	.50
0404/12-20	.51	.37	.42	.17
0406/18-24	.31	.13	.40	.10
0409/14-24	.68	.58	.63	.34
0411/06-16	.81	.51	.76	.38
0412/00-08	.80	.56	.92	.52
0413/14-20	.38	.15	.50	.20
Overall Median	0.68	0.39	0.69	0.36

$R(\Delta x, T_a) = \overline{u_i' u_7'} / \sigma_{u_i} \sigma_{u_7}$, which are functions of the separation, Δx , of stations 1 and 7, the averaging time, T_a and the integral scale of the turbulence. Averaging times of 1, 10 and 60 min are used. Results are presented separately for the E-W and N-S legs of the "L". Rather than showing the correlation for all eleven time periods or runs, we present the median of the 11 periods. These correlations, are plotted in Figure A-3. There does not appear to be a strong dependence on E-W or N-S leg, or on whether wind speed or wind direction is being plotted.

As expected, the calculated correlations are lowest for the shorter averaging times and the largest station separations, due to the fact that the dominant turbulent eddies are characterized by space scales of a few hundred meters and time scales on the order of a few minutes.

At the 10 km separation distance, the correlations average about 0.5. Because of the relation between spatial correlation, R_{12} , spatial variance, $\sigma_{\Delta u}^2$, and variance, σ_u^2 , indicated by Equation (A-11), it follows that, at 10 km separation, $\sigma_{\Delta u}^2 = \sigma_u^2$. Knowing that $\sigma_u^2(T_a = 1 \text{ min}) \approx 1.2 \text{ m}^2/\text{s}^2$, and using the median values of $\sigma_u^2(T_a)/\sigma_u^2(1 \text{ min})$ in Table A-2, it can be concluded that $\sigma_{\Delta u}^2 \sim 1.1 \text{ m}^2/\text{s}^2$ for $T_a = 1 \text{ min}$, $\sigma_{\Delta u}^2 \sim 0.8 \text{ m}^2/\text{s}^2$ for $T_a = 10 \text{ min}$, and $\sigma_{\Delta u}^2 \sim 0.4 \text{ m}^2/\text{s}^2$ for $T_a = 60 \text{ min}$ at the 10 km separation distance. This value of $\sigma_{\Delta u} \sim 0.7 \text{ m/s}$ for one-hour averages is close to that found with the St. Louis RAPS data, as discussed in Section 2.

At small averaging times, T_a , Equation (A-15) suggests that the correlation coefficient for wind speed fluctuations at two points separated by a distance, Δx , should be an exponential function of Δx . Therefore, if $\ln R$ is plotted against Δx , a straight line should be seen. Observations of R from this wind network are plotted in Figure A-4, for the six Δx values (312.5, 625, 1250, 2500, 5000, and 10000 m) and three averaging times (1, 10, and 60 min) of interest. Because the correlations in Figure A-3 did not indicate much dependence on E-W or N-S direction, and were similar for wind speed and wind direction, all runs, legs, and variables are combined in this table and figure.

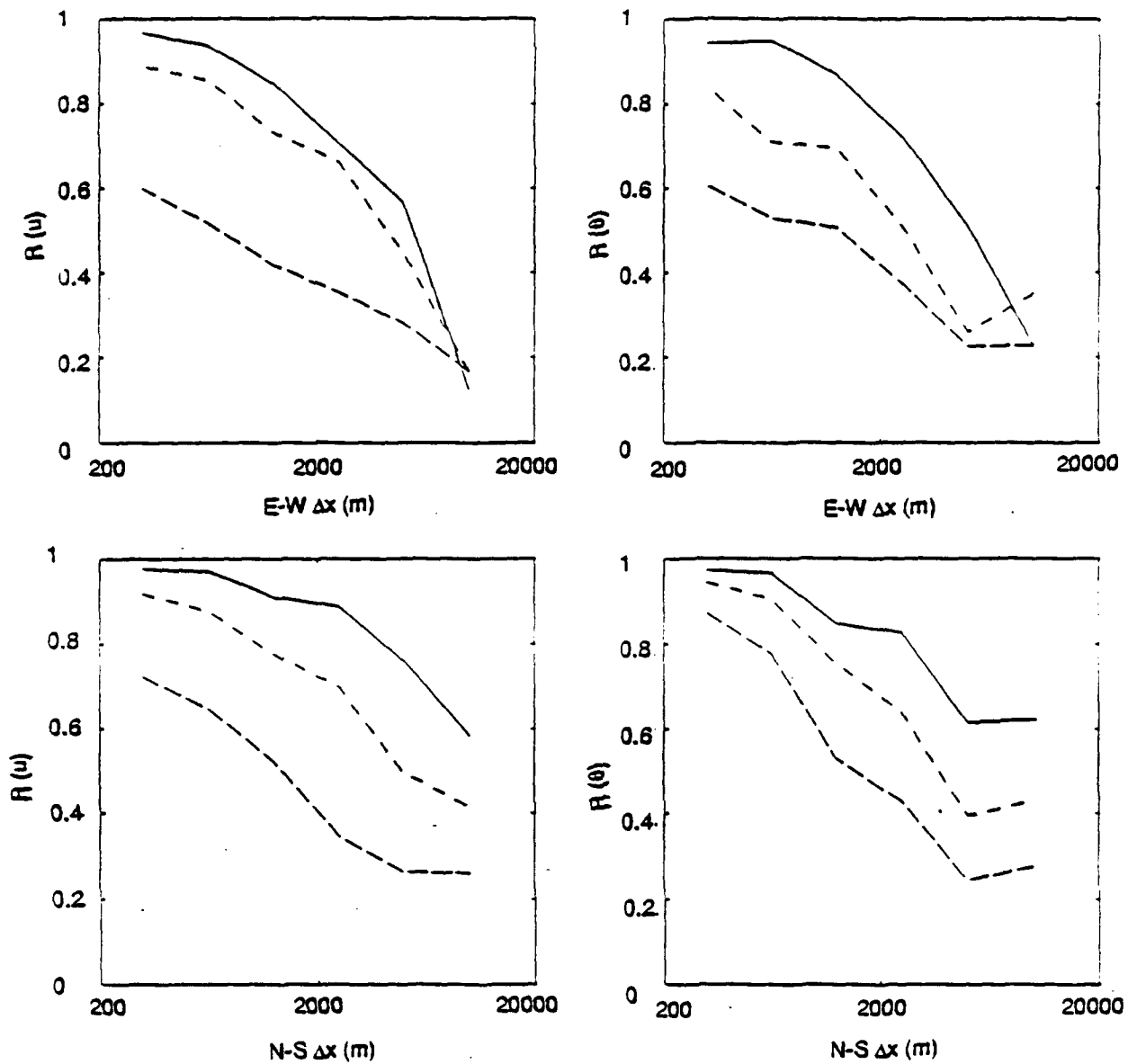


Figure A-3. Spatial correlation coefficient, R , as a function of station separation for E-W and N-S legs of Hereford monitoring network. Wind speed (u) correlations are on the left, and wind direction (θ) correlations are on the right. Medians over all eleven runs are shown for averaging times of 1 min. (Long Dashes), 10 min. (Short Dashes), and 60 Min. (Solid Line). The standard deviation of the scatter of the 11 points about each line is about 0.2.

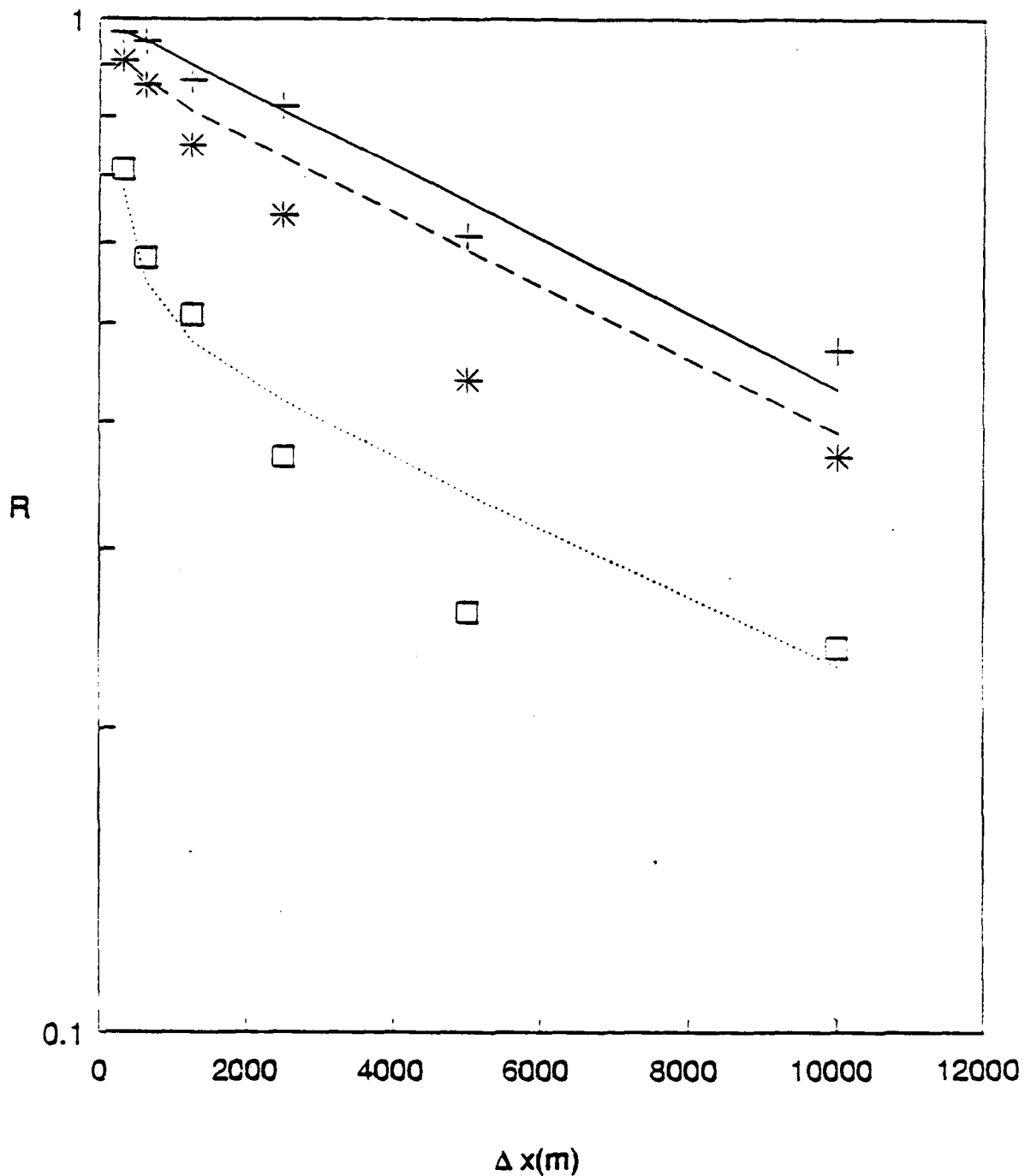


Figure A-4. Spatial correlation coefficients, R , for various spatial separations, Δx , and averaging times, T_a (\square 1 min; $*$ 10 min; $+$ 60 min), from Hereford site. Plotted are the medians over eleven runs. E-W and N-S legs, and wind speed and wind direction observations. Typical scatter of all the data about each line is about 0.2 at a correlation of 0.5. Empirical curves from Equation (A-17) are drawn (dotted, $T_a = 1$ min.; dashed, $T_a = 10$ min.; solid, $T_a = 60$ min.).

The points in the figure follow a straight line only for the largest averaging time (60 min). For the smallest averaging time (1 min), there is a much more rapid drop-off in correlation at small separation distances. This behavior can be explained by the same two-scale phenomenon discussed under Section 5.1 in the analysis of the effects of averaging time; i.e., the results are influenced by a smaller eddy scale, Λ_1 , representative of boundary layer processes, and a larger eddy scale, Λ_2 , representative of mesoscale fluctuations. However, the effects of the smaller scales tend to disappear at large averaging times, T_a , when the condition $T_a > \Lambda_1/u$ is satisfied. Thus, equation (A-15) appears to be satisfied, with the limits:

$$R(\Delta x, T_a \rightarrow 60 \text{ min}) = e^{-\Delta x/\Lambda_2}$$

$$R(\Delta x, T_a \rightarrow 1 \text{ min}) = 0.5e^{-\Delta x/\Lambda_1} + 0.5e^{-\Delta x/\Lambda_2}$$

The following empirical equation fits these data and has the proper asymptotic behavior:

$$R(\Delta x, T_a) = e^{-\Delta x/\Lambda_2} - 0.5 \left(e^{-\Delta x/\Lambda_2} - e^{-\Delta x/\Lambda_1} \right) / \left(1 + (T_a u/a\Lambda_1)^2 \right) \quad (\text{A-17})$$

where $\Lambda_1 = 300$ m, $\Lambda_2 = 12000$ m, and $a = 5$ when $u \approx 5$ m/s. The predicted curves are drawn on Figure A-4. The value of $a = 5$ is consistent with "Pasquill's Beta" = 4, which is the known proportionality factor between Lagrangian and Eulerian scales. Because the actual eddy diameters are equal to about five times the integral scales Λ , the smaller eddy diameters would be about 1500 m and the larger eddy diameters would be about 60 km. Of course the confidence limits on the data (\pm about 0.2) are so broad that a much wider range of scales, Λ_1 and Λ_2 , is possible. Furthermore, these results are limited to this particular site and time of year, and to the ranges of Δx , T_a , and meteorological conditions that we have considered. The sampling time (a maximum of 10 hours) also imposes a maximum limit on integral scales.

6. Recommended Empirical Formula for Variances

Our analysis of the Hereford data has suggested that the variances and correlations for wind speed and wind direction are similar. In addition, we

have found that, despite the theoretical prediction that along-wind correlations will be larger than cross-wind correlations, there is no clear dependency of the correlations on wind direction (or any other meteorological variable). This apparent lack of dependency may be due to the fact that this effect is overwhelmed by the natural variability in the observations.

The similarity relations in Equation (A-8) have been shown to be valid, resulting in Equation (A-16) for the effects of averaging time and Equation (A-17) for the effects of station separation. These equations can be combined into the following general equation:

$$\frac{\sigma_{\Delta u}^2(\Delta x, T_a)}{2\sigma_u^2(T_a = 0)} = \left[\frac{0.5}{1 + T_a/2T_{I1}} + \frac{0.5}{1 + T_a/2T_{I2}} \right] \cdot \left[1 - e^{-\Delta x/\Lambda_2} + 0.5 \frac{(e^{-\Delta x/\Lambda_2} - e^{-\Delta x/\Lambda_1})}{(1 + (T_a u/a\Lambda_1)^2)} \right] \quad (A-18)$$

where $T_{I1} \sim 300$ s $T_{I2} \sim 1800$ s
 $\Lambda_1 \sim 300$ m $\Lambda_2 \sim 1200$ m
 a (Lagrangian-Eulerian scale) ~ 5

This equation should be tested with independent data from a different site. Slightly different values of the time and distance scales may be appropriate at a different site. For any given time and place, the confidence limits on the results would be expected to be in the same range (about 20% to 30%) has been found here.

7. Test of General Equation with Independent Data

A set of independent wind data from the so-called XM21 field study at Dugway Proving Ground, Utah, were provided by C. Biltoft. Data were available from two towers, separated by 500m, on a relatively flat test range. Instruments were located at heights of 2, 4, 8, 16, and 32m, and measurements were made at a frequency of one per second. Because the towers were constructed of scaffolding, it was necessary to disregard periods when the

wind blew through one of the towers. Two periods of valid data were analyzed--from 1110 to 1651 on 11 April 1989, and from 0937 to 2059 on 2 May 1989. Both periods were marked by wind speeds of about 3.5 m/s and relatively strong turbulence intensities ($\sigma_u/\bar{u} \sim 0.3$ and $\sigma_\theta \sim 30^\circ$).

Because the integral scales of the horizontal components of turbulence are not strongly dependent on height, the results from all five levels are combined in our analysis. This assumption will cause a slight error, since the various ratios $\sigma^2(T_a)/\sigma^2(1\text{sec})$ and correlations are observed to increase by about 10% to 20% between heights of 2m and 32m. In addition, the wind speed and direction results appear similar and are combined in our analysis. The combined data results (two variables, two days, five levels) are presented in Table A-3.

The predictions of $\sigma^2(T_a)/\sigma^2(1\text{sec})$ in the table have been made using Equation (A-16), with the same time scales derived from the NCAR wind network ($T_1 = 300\text{s}$ and $T_2 = 1800\text{s}$). There is a $\pm 10\%$ agreement between the predictions and the observed medians, and the predictions are within the \pm standard deviation error bounds of the observations. It can be concluded that the variances $\sigma^2(T_a)$ show similar behavior at the two sites, and that Equation (A-16) can adequately simulate this behavior.

Equation (A-17) (for spatial correlations) does not transfer as well to the new site. Its predictions are shown under column (2), assuming the parameters ($\Lambda_1 = 300\text{m}$, $\Lambda_2 = 12000\text{m}$, and $a = 5$) derived from the NCAR wind network. Clearly the predictions of $R_{\Delta u}(T_a)$ are too low by about 10 to 30%. If the Λ_1 , Λ_2 , and "a" parameters are "tuned" with these new data, the predictions under column (3) are all within $\pm 4\%$ of the observations. However, the smaller of the length scales, Λ_1 , has to be increased from 300m to 1000m, and the Lagrangian-Eulerian parameter "a" has to be reduced from 5 to 0.2. It appears that the weakest part of Equation (A-17) is the correction term, $(1 + (uT_a/a\Lambda_1)^2)^{-1}$, for averaging time, T_a . This term is intended to cause an increase in the spatial correlation as averaging time increases. However, the functional form for this correction term is not obvious and more thought is clearly needed.

Table A-3

Observations and Model Predictions for Dugway Proving Ground Wind Data,
with Tower Separation of 500m, for All Levels Combined,
and Wind Speed and Direction Combined. Medians are Listed for the
Observed Values. Model Parameters are given in the
Footnotes.

Averaging Time T_a	$\frac{\sigma^2(T_a)}{\sigma^2(1\text{sec})}$	$\frac{\sigma^2(T_a)}{\sigma^2(1\text{sec})}$	$R_{\Delta u}(T_a)$	$R_{\Delta u}(T_a)$	
	Observed	Predicted (1)	Observed	Predicted (2)	(3)
1 sec			0.78	0.57	0.77
60 sec	0.87	0.95	0.83	0.58	0.86
600 sec	0.68	0.65	0.94	0.83	0.95

- Footnotes: (1) Equation (A-16) is used, with the same values for the parameters as derived from the NCAR data ($T_1 = 300\text{s}$ and $T_2 = 1800\text{s}$)
- (2) Equation (A-17) is used, with the same values for the parameters as derived from the NCAR data ($\Lambda_1 = 300\text{m}$, $\Lambda_2 = 12000\text{m}$, and $a = 5$)
- (3) Equation (A-17) is used, with $\Lambda_1 = 1000\text{m}$, $\Lambda_2 = 12000\text{m}$, and $a = 0.2$.

Acknowledgements:

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References:

Davenport, A.G., :1961, "The Spectrum of Horizontal Gustiness near the Ground in High Winds," *Quart. J. Roy. Meteorol. Soc.* 87, 194-211.

Hanna, S.R. :1982, "Applications in Air Pollution Modeling," Ch. 7 in *Atmospheric Turbulence and Air Pollution Modelling*. (Eds: F.T.M. Nieuwstadt and H. van Dop), 275-310.

Lockhart, T.J. and Irwin J.S., :1980, "Methods for Calculating the Representativeness of Data," *Proceedings, DOE Symposium on Intermediate Range Atmospheric Transport Processes and Technology Assessment*, CONF801064, NTIS, 169-176.

Panofsky, H.A. and Dutton J.A., :1984, "*Atmospheric Turbulence*," John Wiley and Sons, New York, Chapter 9.

Perry, S.G., Norman J.M., Panofsky H.A. and Martsolf J.D., :1978, "Horizontal Coherence Decay near Large Mesoscale Variations in Topography," *J. Atmos. Sci.* 35, 1884-1889.

Pielke, R.A. and Panofsky H.A., :1970, "Turbulence Characteristics along Several Towers," *Bound. Lay. Meteorol.* 1, 115-130.

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APPENDIX B-1

UNCERTAINTY ASSOCIATED WITH EMISSION RATE ESTIMATION

Appendix B-1

Table of Contents

Uncertainty Associated with Emission Rate Estimation

	Page
1. Introduction	B-1
2. Measurement of Smoke Munition Emissions	B-2
2.1 Wind Tunnel Experiments	B-2
2.2 Field Experiments	B-4
3. The Emission Rate Expression	B-6
3.1 Input Parameters	B-6
3.2 Approach to Estimating Uncertainty in the Emission Rate	B-10
3.3 Uncertainty Analysis Results	B-16
4. Conclusions and Recommendations	B-19
References	B-21

Definition of Terms

A, B, C, D	coefficients which are determined by fitting the observed wind tunnel experiments to a curve
COV_{xy}	covariance of xy
CV_x^2	squared coefficient of variation of x, $\frac{s_x^2}{\bar{x}^2}$
CV_y^2	squared coefficient of variation of y, $\frac{s_y^2}{\bar{y}^2}$
h	relative humidity
M_o	initial mass
M_x	mass of zinc or phosphorus aerosolized, as measured in the wind tunnel experiments
MYF	munition yield factor, the ratio $\frac{M_x}{M_o}$
Q_t	mass emission rate
q	$\frac{Q_t}{M_o}$
\bar{x}	mean of x
\bar{y}	mean of y
YF	yield factor, theoretical adjustment to mass of aerosol based on the ability of the active ingredient to absorb water vapor
ΔM	mass lost during burn, initial mass less final mass, as measured by the load cell
σ_{xy}^2	variance of the product xy
σ_x^2	variance of x
σ_y^2	variance of y

UNCERTAINTY ASSOCIATED WITH EMISSION RATE ESTIMATION

1. Introduction

To estimate the uncertainty of an entire model it is necessary to evaluate the uncertainty of its components. The input data for atmospheric dispersion models consists of emission rate data and meteorological data. In this discussion we address the issue of uncertainty associated with the estimation of emission rates of aerosols from smoke munitions. Emission rates are generally expressed in terms of weight per unit time; in this case they are expressed as grams of active ingredient, (e.g., phosphorus) per second.

The issue of estimating the emission rate of obscurant munitions is complex, aside from the issue of estimating the associated uncertainty. There are several reasons for this. First, the critical property which provides the obscurant effect is not directly emitted by the munition; it results from an interaction of the active ingredient, e.g., red phosphorus, and moisture in the ambient atmosphere to form a dense smoke cloud. Second, munitions contain other materials which burn simultaneously but do not contribute directly to the obscurant effect; thus measuring total weight loss over burn time only indirectly measures the amount of active ingredient which has been released. Third, to experimentally determine the amount of active ingredient released, the mass of the active ingredient in the entire smoke cloud must be determined and this measurement can only be carried out in a wind tunnel. Thus, data from the wind tunnel experiments are extrapolated to the field setting. These issues affect emission rate estimation as well as contribute to the associated uncertainty.

This discussion covers the following topics: how emissions are measured in both wind tunnel and field experiments, the model used for estimating emission rates, a technique for estimating uncertainty (using existing data as an example), and conclusions and recommendations for the collection of additional data which would enhance the uncertainty analysis. Several reports were reviewed for this analysis, but the information on the method of measuring and modeling emission rates is based on two reports: *Basic*

Smoke Characterization Test (DPG-FR-77-311) (DPG, 1978) and *Methodology Investigation Final Report Validation of a Transport and Dispersion Model for Smoke* (DPG-FR-702) (Carter et al., 1979). These reports contain data on three different types of smoke obscurant munitions: white phosphorus, red phosphorus, and zinc oxide-hexachloroethane-aluminum. Because only limited amounts of appropriate data are available for the uncertainty analysis, the conclusions drawn from this analysis must be considered tentative.

2. Measurement of Smoke Munition Emissions

2.1 Wind Tunnel Experiments

The most detailed measurement of emission rates of submunitions were conducted in wind tunnel experiments. Although field measurements have been collected, these data are not adequate for developing a model. Thus, the model used to predict emission rates is based on the wind tunnel experiments. The experiments and the data described in this section are summarized from DPG (1978).

The wind tunnel experiments were conducted at the Dugway wind tunnel. In the experiments, single submunitions (e.g., an individual component which contains the smoke producing compound) of zinc and white phosphorus were burned. In actual field use of smoke munitions, multiple submunitions are loaded into a canister and burn simultaneously. For red phosphorus, three submunitions (wedges) were burned simultaneously. The wind tunnel tests were conducted at a wind speed of 2 m/s and the ambient temperature, relative humidity, (%RH), and barometric pressures were recorded. Pre-weighed submunitions were placed on a load cell in the center line of the tunnel and fired remotely. The load cell recorded the elapsed time and weight loss of the submunition as it burned. The end of the tunnel had a barrier that contained a grid of holes through which the air in the tunnel passed. The air passed into sampling lines and through collection devices, impingers. (See Figure B-1.) The impingers were then analyzed for zinc or phosphorus, the appropriate active ingredient. The concentrations in all impingers were summed to determine the total amount of active ingredient which had been aerosolized during the burn. Data collected on each test included: weight loss with burn time, total zinc or phosphorus, tunnel wind speed, temperature, and relative humidity.

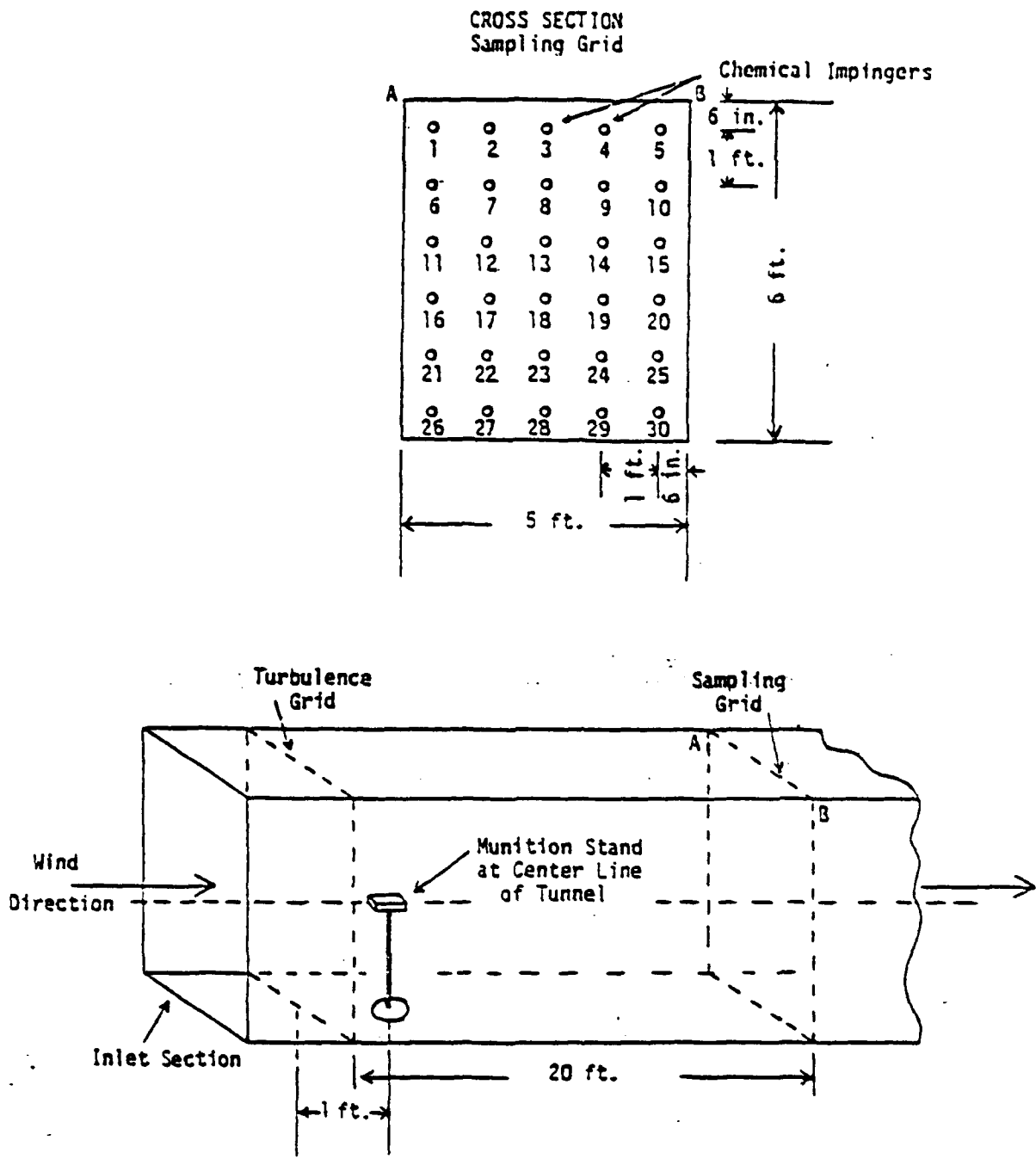


Figure B-1. Diagram of Wind Tunnel.

Source: DPG, 1978

Transmittance, which is routinely measured in the field, cannot be measured in the wind tunnel because the concentrations are too high. The types of submunitions tested (as reported in DPG (1978)) were:

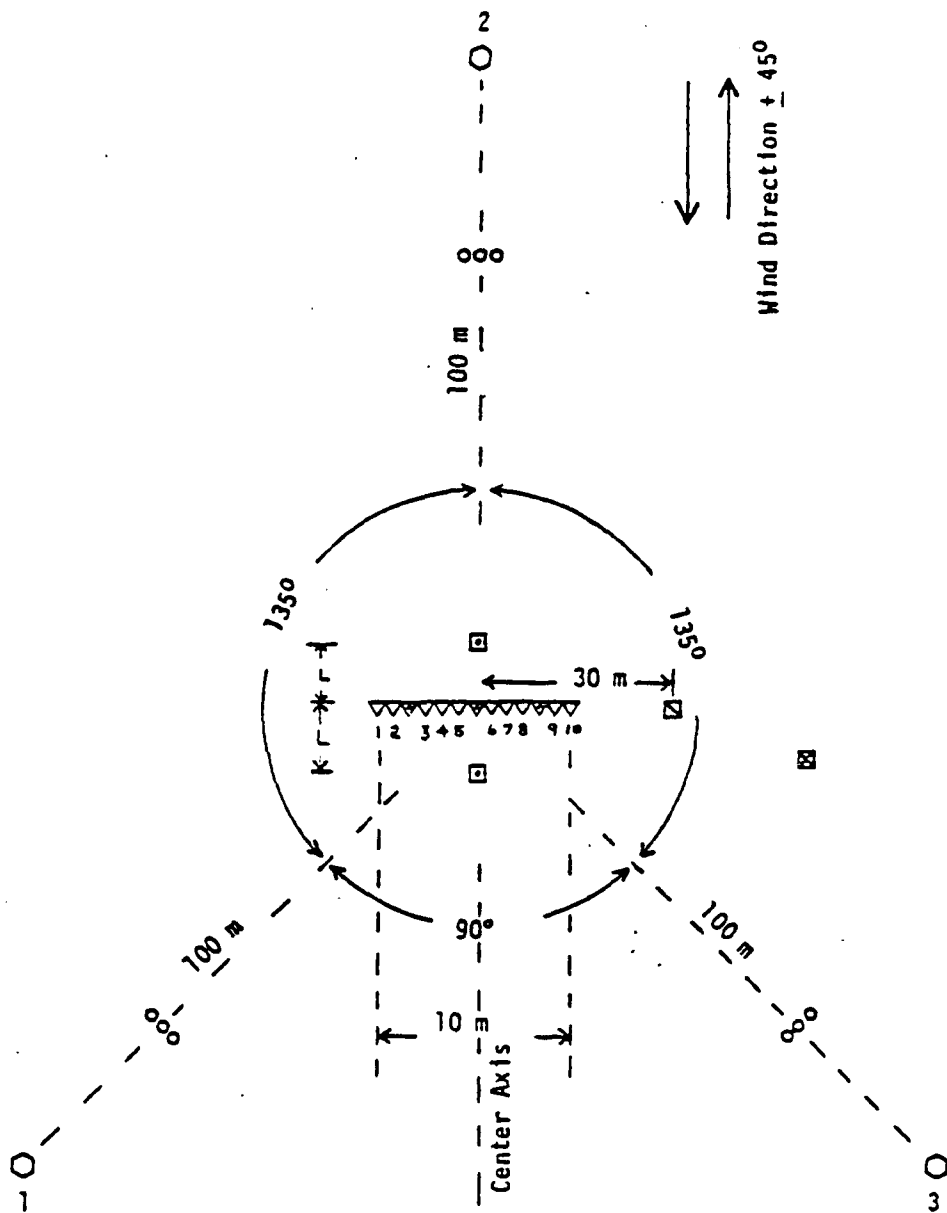
- 155mm HC M1 Canister (zinc)
- 155mm HC M2 Canister (zinc)
- 105mm HC M1 Canister (zinc)
- 6 inch WP Wick (white phosphorus)
- 2.75 inch Rocket WP Wick (white phosphorus)
- 81mm Navy RP Wedge (red phosphorus)
- 155mm Navy RP Wedge (red phosphorus)
- 81mm German RP Wedge (red phosphorus).

For each type of submunition, two burns were conducted.

2.2 Field Experiments

The field experiments were conducted at the Horizontal Grid, Dugway Proving Ground, Utah. The experiments described in this section are summarized from DPG (1978). The data were collected by means of photography, aerosol sampling with aerosol photometers, particle size analyzers, and impingers. Samplers were located 1.22 meters above the ground. Motion pictures recorded the size and shape of the smoke cloud; aerosol photometers recorded total particle concentration; particle size analyzers recorded size distributions; and impingers measured zinc or phosphorus concentrations. The mass of zinc or phosphorus from these impingers cannot be summed to calculate total zinc or phosphorus aerosolized as was done in the wind tunnel experiments because the total smoke cloud is not collected by the impingers.

Figure B-2 (DPG, 1978) shows the layout of the instruments for these experiments. The sampling line was always oriented perpendicular ($\pm 45^\circ$) to the prevailing wind direction. The impingers were located halfway between the aerosol photometers. As in the wind tunnel experiments, the munitions were placed in a load cell so that data on weight loss with burn time were recorded. The types of submunitions tested were the same as those used in the wind tunnel experiments. For each type of submunition, two burns were conducted.



- Camera Positions
- Stadia Markers
- Submunition Position
- ▼ Particle Size Analyzer
- ▼ Aerosol Photometer+2 CIs at each location
- Recorders
- 2-Meter Mast
- L Sampling Distance (L varies with submunition)

Figure B-2. Grid for munition cloud characterization. Source: DPG, 1978

The meteorological data recorded in these experiments included: wind speed and direction, temperature, and relative humidity.

3. The Emission Rate Expression

The critical parameter to be derived from these experiments is the amount of smoke generated per second of burn time. In its simplest form, this would be calculated by dividing the mass lost by the burn time to derive a value in units of grams per second. However, the amount of smoke generated is more than a function of the mass burned; it is also a function of the interaction of the zinc or phosphorus with water vapor to create the smoke. Zinc and phosphorus are hygroscopic, absorbing upwards of four times their mass in water vapor. Thus, the actual emission rate of interest is total amount of hydrated smoke generated per second. To add one further complexity to the equation, the burn rate of the munitions is not constant with time. There is an initial growth period, followed by a plateau of relatively constant rate of emissions, followed by a rapid decline. In field tests, there are data which indicate munitions can burn unevenly; this is characterized as "flashing" toward the end of the burn time by the observers.

The following discussion covers two topics. The first topic presents the parameters in the emission rate expression and the second discusses the uncertainty associated with those parameters and presents a technique for computing the uncertainty in the overall emission rate value.

3.1 Input Parameters

The emission rate of hydrated smoke is a function of the initial mass of the munition, the fraction of this mass which is the aerosolized zinc or phosphorus, the increase in mass of the aerosol due to hydration, and burn time. The expression which was developed from the wind tunnel experiments to estimate the emission rate is as follows (DPG, 1978):

$$Q_s = M_o MYF YF(A/t_b + 2Bt/t_b^2 + 3Ct^2/t_b^3 + 4Dt^3/t_b^4) \quad (B-1)$$

where: Q_t = mass emission rate

M_o = initial mass

MYF = munition yield factor

YF = yield factor

A,B,C,D = coefficients which are determined by fitting the observed data in the wind tunnel experiments to a curve.

They are constrained to sum to unity.

The munition yield factor, MYF, is the ratio of the mass of zinc or phosphorus burned, M_x , to the initial mass of the munition, M_o . M_x is determined from the wind tunnel experiments and is calculated by summing the mass of zinc or phosphorus collected by all the impingers. These wind tunnel values of M_x are used to predict the emission rate, Q_t , for field experiments, as M_x cannot be measured in the field setting.

The yield factor takes into account the hygroscopic growth of the aerosolized zinc or phosphorus and is a function of ambient relative humidity. For the three different types of smoke munitions, yield factors are based on theoretical calculations or experimental data. The conceptual definition of the yield factor is:

$$YF = \frac{\text{mass of smoke (including aerosol)}}{\text{mass of starting material}}$$

In the case of phosphorus, the final material is primarily hydrated orthophosphoric acid, ($H_3PO_4 + nH_2O$). According to DPG (1977), it is assumed that the hydration of the droplets of H_3PO_4 proceeds until their aqueous vapor pressure equals the partial pressure of H_2O in the atmosphere. The mass of hydrated H_3PO_4 is then constant (assuming no other environmental changes occur) and the yield factor can be expressed as:

$$YF = \frac{\text{mass } H_3PO_4 + nH_2O}{\text{mass P}}$$

DPG (1977) contains the following example of how a yield factor is calculated. Yield factors for phosphorus can be readily computed from tables correlating aqueous vapor pressures with the composition of various mixtures

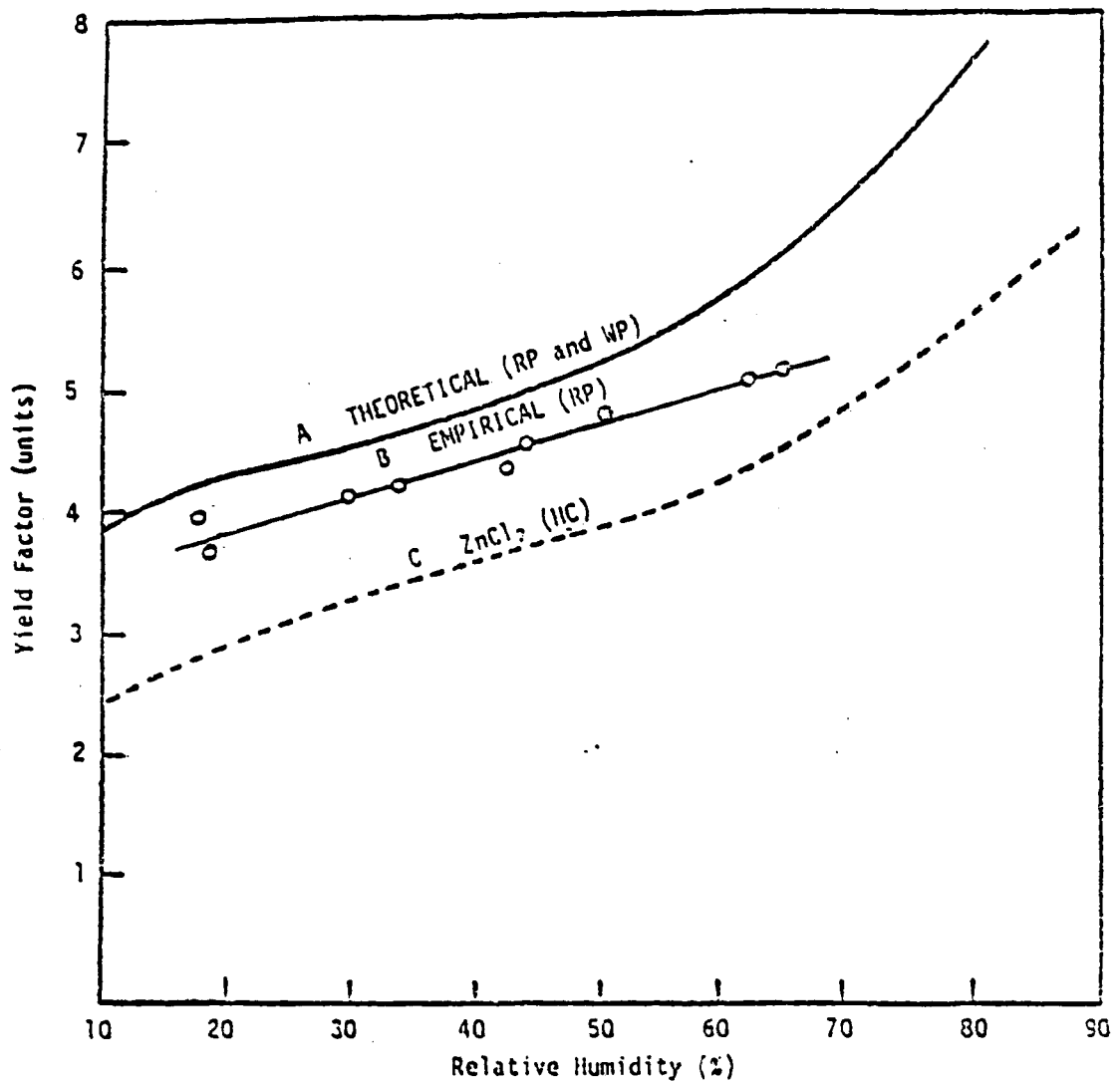
of H_3PO_4 , when the concentration of H_3PO_4 in the solution is expressed as weight %, (i.e., $\text{mass } (H_3PO_4) \times 100 / \text{mass } (H_3PO_4 + nH_2O)$). For a specified aqueous vapor pressure, the ratio of the molecular weight of H_3PO_4 to the atomic weight of P is 3.16:

$$YF = \frac{100 \times 3.16}{H_3PO_4 \text{ (wt \%)}} = \frac{316}{H_3PO_4 \text{ (wt \%)}}$$

Taking, as an example, the burning of 1 gram of P in the air at 25°C and containing moisture at a partial pressure of 22.39 mmHg, the oxidation to phosphoric oxide and hydrolysis of phosphoric oxide will result in 1 x 98/31 gram or 3.16 gram H_3PO_4 . H_3PO_4 will then hydrate until the aqueous vapor pressure of the diluted H_3PO_4 ($H_3PO_4 + nH_2O$) equals the ambient vapor pressure. At 22.39 mmHg and 25°C, the equilibrium composition of the mixture is found to be 20.07 weight % H_3PO_4 . The YF is then $316/20.07 = 15.7$, (i.e., under these conditions, the mass of smoke is 15.7 gram for every gram of P burned). An additional correction will be necessary if the munition efficiency is not 100%.

DPG (1978) notes that the theoretical curve for phosphorus assumes that orthophosphoric acid is produced immediately during combustion. If this assumption does not hold, the yield factor may overestimate the effective dosage. DPG (1977) also presents a derivation which proves that YF's are insensitive to temperature up to 100°C.

Figure B-3 (DPG, 1978) presents yield factor curves based on theoretical calculations for P as well as empirical data for red phosphorus and theoretical calculations for zinc oxide-hexachloroethane-aluminum (HC). It can be seen from these figures that the slope of the lines for all three materials, white phosphorus, red phosphorus, and the zinc based munition, is relatively shallow over the range of relative humidity from approximately 20% to 65%. For example, over the range of 20% to 65% RH, the yield factor for red phosphorus increases by a factor of 1.4. However, the theoretical curves rise sharply at humidities greater than 65%. Between humidity levels of 65% to 80% red and white phosphorus increase by a factor of approximately 1.3 and hydrated zinc chloride by a factor of 1.7. For field tests conducted on one day, the relative humidity would not be expected to vary over this wide a range, so that



Curve A: Yield factors for the conversion of P to hydrated H_3PO_4 (ref. 8).
 Curve B: Yield factors empirically determined for RP.
 Curve C: Yield factors for the conversion of Zn to hydrated $ZnCl_2$ (ref. 5).

Figure B-3. Yield factors as a function of relative humidity for various smoke producing agents. Source: DPG, 1978.

the yield factor between burns should not vary substantially. For example, an increase from 40% to 50% RH only produces a difference in the yield factor of 1.04 for red phosphorus. During the field experiments, which took place on several different days, the relative humidity varied from 40% to 80%, but within a given day the RH only varied by 2%-4%.

3.2 Approach to Estimating Uncertainty in the Emission Rate

A direct method for determining uncertainty values would be to compare modeled emission rates with actual emission rates; however, emission rate measurements from the field experiments are not available. In the absence of actual data, uncertainty values can be modeled based on estimated uncertainty values for the input parameters and on the uncertainty inherent in the emissions rate model. To estimate uncertainty values for the variables, there should be sufficient data available to calculate the probability density functions (i.e., measures of variability) of the input variables. To model the uncertainty in the emission rate model, an assumption must be made regarding the independence or dependence of the variables in the model, as there are different approaches for each case.

The following discussion presents both a qualitative and quantitative assessment of the emission rate uncertainty of the various smoke munitions. The qualitative assessment highlights the sources of uncertainty of the input parameters to the emission rate model and the limitations imposed by the amount of data (for each type of munition) available for the analysis. The quantitative assessment presents a model for estimating the emission rate uncertainty and an example application for several munitions.

Two factors limit the uncertainty analysis of the smoke munitions data. First, too few experiments were conducted for each type of munition to determine robust probability density functions for the various parameters. For both wind tunnel and field experiments only two burns were conducted for each type of submunition, thus means or variances will not be stable or robust. Confidence intervals are large when $n = 2$. Therefore the quantitative uncertainty analysis presented subsequently is neither a precise nor an accurate measure of uncertainty, but the method is valid with sufficient data.

Second, the data from the wind tunnel experiment are suspect. For five of the nine munitions tested in the wind tunnel, the mass of aerosolized active ingredient, M_x , as measured by the bubblers exceeded the mass burned, ΔM , as measured by the load cell on which the munition was placed. This clearly violates the law of conservation of mass. There are two plausible hypotheses for these results. First, the design of the wind tunnel is suspect. It has been observed that there may have been insufficient downwind distance from the load cell to establish laminar flow at the sampling point (Carter, (1991), personal communication). Second, the wind speed was measured at only one location and the assumption of constant velocity may not be correct (Bowers, (1991), personal communication). Either or both of these situations could have led to an overestimation of air velocity at the point of sampling. Although this condition most likely existed for all tests, it was not evident in the data from the three types of zinc oxide-hexachloroethane-aluminum (HC) smoke munitions (155mm M1 and M2 and the 105mm canisters) and one red phosphorus (RP) munition (81mm Navy wedge). (This observation is based on data reported in DPG, 1978.) The reason for the differences between munitions is not readily evident, and it is not possible to ascertain given the age of the data. The error associated with the inaccuracy of the bubbler data will affect all field experiment data because of the fundamental assumption in the emission rate model. Namely, the MYF relationship (the ratio of the mass of active ingredient aerosolized, M_x , to the initial mass of the munition, M_0), as measured in the wind tunnel experiments, is assumed to apply to the field experiments. As the wind tunnel tests overestimated the MYF, the emission rate, Q_t , would also be overestimated.

A simple analysis was performed to (1) determine if there was a consistent bias in the data which could be used to adjust the mass aerosolized, M_x , and the MYF for those munitions where M_x was greater than the mass burned, ΔM , and (2) evaluate the within munition variability for M_x and ΔM . The computation performed was:

$$\text{bias} = 1 - M_x / \Delta M$$

where a negative value indicates the mass of Zn or P aerosolized is greater than the mass burned and a positive value indicates this relationship is reversed.

The data were taken from DPG (1978) and the results are shown in Table B-1. The first five entries in the table are for the munitions where M_x , the mass of Zn or P aerosolized, exceeds ΔM mass burned; the next four entries are for munitions where M_x is less than ΔM . For one munition, the 155mm RP Navy Wedge, in one test result M_x was less than ΔM and for the second test M_x was greater than ΔM . The reason for this anomaly within a munition type is not clearly evident. It can be observed from this table that for munitions where the mass of Zn or P is less than the mass burned, the within munition variability is relatively small, less than 20%. However, for the munitions where the mass of Zn or P is greater than the mass burned, the within variability was much larger, ranging from approximately 45%-88%. Because the within munition variability is so large for those cases when M_x is greater than ΔM , it is not appropriate to adjust M_x or MYF for these munitions.

Three conclusions can be made based on this analysis. First, those munitions for which the mass of Zn or P aerosolized exceeds the mass burned will be dropped from further analysis because the data violate the law of conservation of mass and the large within munition variability precludes adjusting the original data. Second, the results indicate that there may be another source of error affecting the data in addition to the wind tunnel design. One would anticipate that the design error would affect all munitions equally, however, this is clearly not the case. There could appear to be other sources of variation related to the type of munition (e.g., mass aerosolized is less than mass burned is for all of the zinc canister munitions). Or there may have been some other source of experimental error associated with the operation of the wind tunnel or in the analyses of the bubblers. These additional sources of error cannot be evaluated further due to the age of the data. Third, if one assumes that the affect of the wind tunnel design on the munitions is constant across all experiments, then it must be concluded that M_x , the mass of Zn or P aerosolized, is overestimated for all munitions even if M_x is less than ΔM , the mass burned. It follows then that the MYF, which is the ratio of mass aerosolized to mass burned, is overestimated for all munitions.

To estimate the uncertainty in the emission rate model the issue of independence or dependence of the variables must be considered. The

Table B-1
Evaluating Wind Tunnel Bias

		Initial Mass (M _o)	Mass burned (ΔM)	Mass ¹ Aerosolized (M _x)	Bias ²
2.75" WP Wedge	A9	217	125	150	-.20
	A10	203	116	129	-.11
6" WP Wick	A5	102	59	64	-.09
	A6	101	51	77	-.51
3" WP Wick	A7	63	40	45	-.13
	A8	52	36	Void	
155mm RP Navy Wedge	A15	114	78	72	+.08
	A16	117	69	79	-.15
81mm RP German Wedge	A11	30	15	24	-.60
	A14	35	14	15	-.07
155mm HC M1 Canister	A1	3450	2330	425	+.82
	A2	3572	2412	382	+.84
155mm HC M2 Canister	A12	2055	1162	369	+.68
	A13	1987	1182	391	+.67
105mm HC Canister	A3	1178	646	154	+.76
	A4	1177	633	234	+.63
81mm Navy RP Wedge	A17	117	73	64	+.12
	A18	116	68	61	+.10

¹ Zn or P

² Bias = $1 - \frac{M_x}{\Delta M}$

assumption of independence allows one to use a relatively simple expression to calculate overall model uncertainty as the covariance terms can be neglected. However, if this assumption is incorrect and the variables are dependent, the estimated uncertainty will be unrealistically low.

In the case where the variables can be assumed to be independent, Goodman (1960) presents the expression:

$$\sigma_{xy}^2 = \bar{x}^2 \sigma_y^2 + \bar{y}^2 \sigma_x^2 = (\bar{xy})^2 [CV_x^2 + CV_y^2] \quad (B-2)$$

where σ_{xy}^2 = variance of the product xy

\bar{x} = mean of x

σ_x^2 = variance of X = $\frac{\sum(x - \bar{x})^2}{n - 1}$

\bar{y} = mean of Y

σ_y^2 = variance of Y

CV_x^2 = squared coefficient of variation of x, $\frac{\sigma_x^2}{\bar{x}^2}$

CV_y^2 = squared coefficient of variation of y, $\frac{\sigma_y^2}{\bar{y}^2}$

The variables in the emission rate model (see equation B-1) are not independent, both the munition yield fraction, MYF, and the yield fraction, YF, depend on the type of active ingredient. The variance of the product of two or more variables, which are not independent, is given as (Goodman, 1960):

$$\sigma_{xy}^2 = \bar{x}^2 \sigma_y^2 + \bar{y}^2 \sigma_x^2 + 2\bar{x}\bar{y}(\text{COV}_{xy})$$

where the variables are defined as above and COV_{xy} , the covariance of xy, is expressed as:

$$\text{COV}_{xy} = \sigma_x \sigma_y = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})(y_i - \bar{y}) = \frac{1}{N} \sum_{i=1}^N (x_i y_i) - \bar{x} \bar{y} \quad (B-3)$$

To apply Equation (B-2) to the model for Q_t , the emission rate, integrating over the total burn time, it is written as:

$$Q = \int_0^{t_b} dt Q_t = M_0 \cdot MYF \cdot YF \quad (B-4)$$

Let $E = MYF$ and $Y = YF$. Assuming the uncertainty associated with the initial mass, M_0 , is small (i.e., the load cell is accurate), Q_t can be divided by M_0 and expressed as q

$$q = \frac{Q_t}{M_0} = E \cdot Y \quad (B-5)$$

The variance of q (σ_q^2) is

$$\sigma_q^2 = \bar{Y}^2 \sigma_E^2 + \bar{E}^2 \sigma_Y^2 + 2\bar{E} \bar{Y} \text{COV}_{EY} \quad (B-6)$$

where COV_{EY} is the covariance of the munition yield fraction, now expressed as E , with the yield factor, now expressed as Y . Since the yield factor is a function of the relative humidity ($Y = Y(h)$ where h is fractional relative humidity), this value can be incorporated into the expression for σ_q^2 as follows:

$$\sigma_q^2 = \bar{Y}^2 \sigma_E^2 + \bar{E}^2 Y'^2 \sigma_h^2 + 2\bar{E} \bar{Y} Y' \text{COV}_{Eh} \quad (B-7)$$

The fractional relative humidity, h , is = 0 at zero humidity and 1 at 100% humidity and Y' is defined as:

$$Y' = \left. \frac{\Delta y}{\Delta h} \right|_{h = \bar{h}} \quad (B-8)$$

As there are only two values for each munition, Y' is simply the slope of the straight line between the two points. The term COV_{Eh} is the covariance of the munition yield fraction (E) with relative humidity (h).

3.3 Results of Uncertainty Analysis

Table B-2 presents a sample set of data taken from DPG (1978) and used to calculate the variance of the quantity Q_t/M_o , expressed as σ_q^2 . The munitions included in this analysis were only those where the mass of Zn or P aerosolized, M_x , was less than mass burned, ΔM , as discussed previously. An example of how the variance of Q_t/M_o (or σ_q^2) is calculated is given below for the zinc munition 155mm HC M1 canister.

Step 1. Calculate the covariance of the munition yield fraction (E) and relative humidity (h) for trials B1R1 and B2R1. The values for E and h are given in Table B-2. Equation B-3 is the definitional formula for covariance; the computation formula is:

$$\text{COV}_{E,h} = \frac{N(\sum E \cdot h) - (\sum E)(\sum h)}{N^2}$$

$$\begin{aligned}\text{COV}_{E,h} &= \frac{2([0.12 \times 0.76] + [0.11 \times 0.72]) - ([0.12 + 0.11][0.76 + 0.72])}{2^2} \\ &= \frac{0.3408 - 0.3404}{4} \\ &= 1 \times 10^{-4}\end{aligned}$$

Step 2. Calculate Y' according to Equation B-8 where y , the yield factors (YF), are 5.2 and 5.0, and h , the fractional relative humidity, is 0.76 and 0.72.

$$\begin{aligned}Y' &= \frac{\Delta y}{\Delta h} \\ &= \frac{5.2 - 5.0}{0.76 - 0.72} \\ &= 5\end{aligned}$$

Table B-2^a

Variance of the Ratio of the Emission Rate to the Initial
Mass, (Q_t/M_o) for Selected Munitions

Munition	Trial	Munition ^b Yield Fraction	Relative Humidity	Yield ^c Factor	Variance of $\frac{Q_t}{M_o}$
155mm HC M1 Canister	B1R1	.12	76	5.2	2.15×10^{-3}
	B2R1	.11	72	5.0	
155mm HC M2 Canister	B3R1	.18	75	5.2	5.41×10^{-3}
	B4R1	.20	75	5.2	
105mm HC Canister	B15	.13	73	5.1	4.68×10^{-2}
	B16	.19	73	5.1	
81mm Navy RP Wedge	B11	.55	70	6.6	0.160
	B12	.52	80	7.8	

- a. Data taken from Tables III and IV in DPG (1978) for the field experiments conducted at the horizontal grid.
- b. MYF values are from the wind tunnel data for the particular munitions.
- c. Estimated values from Figure B-3 for $ZnCl_2$ (Curve C) and for the theoretical curve for white phosphorus and red phosphorus (Curve A).

Step 3. Calculate σ_q^2 according to Equation B-7. The variance of E, the munition yield fraction, is

$$\sigma_E^2 = 2 \times 10^{-4}. \text{ Equation B-7 is as follows:}$$

$$\sigma_q^2 = \bar{Y}^2 \sigma_E^2 + \bar{E}^2 Y'^2 \sigma_h^2 + 2\bar{E} \bar{Y} Y' \text{COV}_{Eh}$$

and by making the following substitutions:

$$\begin{aligned} \sigma_q^2 &= (5.1)^2 (5 \times 10^{-5}) + (0.115)^2 (5)^2 (8 \times 10^{-4}) + 2(0.115)(5.1) \\ &\quad (5)(1 \times 10^{-4}) \\ &= 2.15 \times 10^{-3} \end{aligned}$$

Interpretation of the variance estimates is limited by the potential error in the munition yield fraction (MYF) values and the limited amount of data (n = 2) for each type of munition. However, some summary comments can be made about these data and this approach to calculating variance. The variance of the 81mm Navy red phosphorus wedge is larger than the three zinc based munitions (zinc oxide-hexachloroethane-aluminum). The cause of this difference could be due to the type of munition. For example, the red phosphorus MYF is larger than the MYF for zinc munitions. Further, for phosphorus munitions the relative humidity on the two days of red phosphorus tests differed by 10% where as for two of the zinc munition tests it was constant. If there is no variation in relative humidity the variance of q is the product of the mean of the yield factor and the variance of the MYF (see Equation B-7).

Bevington (1969) defines the standard deviation, σ , as the estimated error or uncertainty of a parameter. When a parameter, e.g., x, is a function of two or more other variables ($x = ab$) the standard deviations of a and b, when combined, give the uncertainty of x. To put the standard deviation values for each munition in perspective, Table B-3 presents the mean emission rates integrated over time, the standard deviation, σ , (as calculated according to Equation B-7), and the standard deviation expressed as a percentage of the mean. This table shows that the emission rates of the two 155mm HC (zinc) canisters (M1 and M2) have the least uncertainty and the 105mm HC (zinc) wedge has the greatest uncertainty. The uncertainty of the 81mm Navy RP wedge is only slightly greater than the 155mm HC canisters.

Table B-3

Comparison of the Mean and Standard Deviation
of the Ratio of the Emission Rate to the Initial Mass $\left(\frac{Q_t}{M_o}\right)$ *

Munition	Mean $\frac{Q_t}{M_o}$	Standard Deviation of $\frac{Q_t}{M_o}$	Standard Deviation as a % of the mean
155mm HC M1 Canister	0.587	0.046	7.8
155mm HC M2 Canister	0.962	0.074	7.7
105mm HC Canister	0.817	0.216	26.6
81mm Navy RP Wedge	3.844	0.40	10.4

- * Q_t is integrated over the burn time, thus the quantity $\frac{Q_t}{M_o}$ is actually

$$\frac{Q_t}{M_b} \cdot t_b$$

An approach to evaluating emission test results from future experiments would be to compute the 95% confidence interval (95% CI = $\bar{x} \pm 1.96\sigma$) of the quantity $\frac{Q_t}{M_o}$ for each munition. If a subsequent experiment produced a $\frac{Q_t}{M_o}$ value outside of the confidence interval, then it could be concluded that the munition was significantly different from the original sample of munitions. Ideally, a larger dataset than that currently available would be necessary to assure that the standard deviations were stable.

An interesting comparison can be made between these results and the findings presented in *Methodology Investigation Final Report, Validation of Transport and Dispersion Model for Smoke* (DPG, 1979). In DPG, (1979), modeled concentrations along the line of sight (CL) were compared to field measurements as well as comparisons between measured and modeled concentration line integrated dosage (CLID). DPG (1979) reports that the CLID were consistently underpredicted for the zinc based munitions (HC) by a factor of 1.4-1.5 and overpredicted by a factor of 2 for the red and white phosphorus munitions. A comparison of these air dispersion modeling results to standard deviations of the source term (presented in Table B-3) shows a similar relationship among munitions. The zinc based munitions exhibited less variability than the red phosphorus munition. One hypothesis which could partially explain the discrepancies in the modeled versus measured comparisons in DPG (1979) is uncertainty in source terms. The red phosphorus has the largest uncertainty (as measured by the standard deviation) and it also shows the greatest difference between measured and modeled values. The large uncertainty in the red phosphorus source term may account for a portion of the uncertainty in the modeled red phosphorus concentrations.

4. Conclusions and Recommendations

The smoke munitions data from DPG (1978) have been reviewed and a method for estimating uncertainty, as expressed as the standard deviation, in the emission rates has been presented. Available data for the present analysis is limited, but the approach to variance estimation is applicable to larger data sets. The quality of the smoke munitions data is suspect due to design problems with the wind tunnel. The number of tests conducted on each munition, $n = 2$, means the variance computations are not stable. The uncertainty

analysis of the source terms indicated that the 105mm HC munition has the largest uncertainty, being slightly more than 3 times the uncertainty of the 155mm HC munitions and 2.6 times the 81mm Navy RP wedge. For the two 155mm HC canisters, the relative humidity was constant for the M2 test runs and varied for the M1 test runs. However, when uncertainty is expressed by the standard deviation as a percent of the mean, the two munitions have almost the same uncertainty.

Two recommendations can be made based on the preceding analysis. First, the munition yield factor should be determined in an accurate and precise manner. This variable is critical, as it is applied to all the field test data. Second, to assess meaningfully the uncertainty in the emission rate values, more than two sets of data must be available for the results to be more stable, and thus reliable.

To use this technique of computing variance to evaluate munition variability, the following plan is suggested. Assuming the wind tunnel design issue has been resolved and accurate MYF's determined, field data from numerous test burns should be collected. This should be done at the horizontal grid, but without simultaneous aerosol and meteorological monitoring. This is because to compute uncertainty for the emission rate value, the only parameters needed are initial weight, M_0 , munition yield fraction, and yield factor (as computed based on relative humidity); thus only M_0 and %RH would need to be recorded. Numerous burns for each type of munition should be conducted, e.g., $N = 30$. Tests should be conducted under as wide a range of humidities as possible. Such a database could then be used to compute robust variance and 95% confidence intervals. Subsequent test results would be compared to this confidence interval to determine if the emission rate is statistically different. Further, with sufficient data to compute stable variances, these values could be incorporated into an expression with meteorological variances to compute overall model uncertainty.

References

- Bevington, P.R., 1969: *Data Reduction and Error Analysis for the Physical Sciences*, McGraw-Hill Book Co., NY.
- Carter, F.L., R.K. Dumbauld and J.E. Rafferty, 1979: Methodology Investigation, Final Report, Validation of Transport and Dispersion Model for Smoke, TECOM Project No. 7-CO-PB8-DP1-004, U.S. Army Dugway Proving Ground, Dugway, UT.
- DPG, 1977: Methodology Investigation for Testing Effectiveness of Smoke/Aerosol Munitions Pilot Study, Final Report, TECOM Project No. CO-RD6-DPI-005, U.S. Army Dugway Proving Ground, Dugway, UT.
- DPG, 1978: Basic Smoke Characterization Test, Final Report, TECOM Project No. 7-CO-RD7-DPI-001, U.S. Army Dugway Proving Ground, Dugway, UT.
- Goodman, L.A., 1960: On the exact variance of products, *J. of the American Statistical Assoc.*, 55, 708-713.

APPENDIX B-2

ANALYSIS OF FOG-OIL SMOKE EMISSIONS

Appendix B-2

Table of Contents

Analysis of Fog-Oil Smoke Emissions

	Page
1. Introduction	B-25
2. Method	B-25
3. Results	B-35
4. Conclusions	B-36

Appendix B-2
Analysis of Fog-Oil Smoke Emissions

1. Introduction

This analysis focuses on the fog-oil smoke generator emission rates as tested at the Dugway Proving Ground in March and April, 1985 (Liljegren et al., 1988). Liljegren et al. (1988) reported the details of how the experiment was conducted. Only the method of computing the emission rate will be addressed here. The objectives of this analysis are threefold: (1) to assess the variability in the emission rate from the fog-oil smoke generator, (2) to compare two methods of computing the emission rate, and (3) to evaluate the influence of averaging time on emission rate variability.

2. Method

The fog-oil smoke emission data were taken from Liljegren et al. (1988). The configuration of the smoke test provided for the "instantaneous" measurement of the emission rate based on the weight loss of the oil drum and the exit velocity of the generator. Due to mechanical difficulties, the weight loss values are actually 1-minute averages, as opposed to "instantaneous" values. Plots of these data (and exit temperature) versus time for seven experiments were reported in Figures 3.2 through 3.8 in Liljegren et al. (1988). (For reference, copies of those figures are included, with the original figure numbers.) These data were digitized and the means, \bar{x} , and standard deviations, σ , were computed for each experiment. These values and the coefficient of variation (σ/\bar{x}) for each test are presented in Table B-1. Some experiments were screened to remove values which were approximately zero at the end of the test. Otherwise, the data reflect the actual emissions for the duration of the experiment.

Liljegren et al. (1988) computed a time integrated emission rate based on the total mass of oil burned divided by the duration of operation of the smoke generator. These values, taken from Table 3.1, are shown in Table B-2.

To evaluate the influence of averaging time on the variability in the emission rate, the emission rates were re-calculated based on averaging times up to 510 seconds. To do this the data were processed through a program which

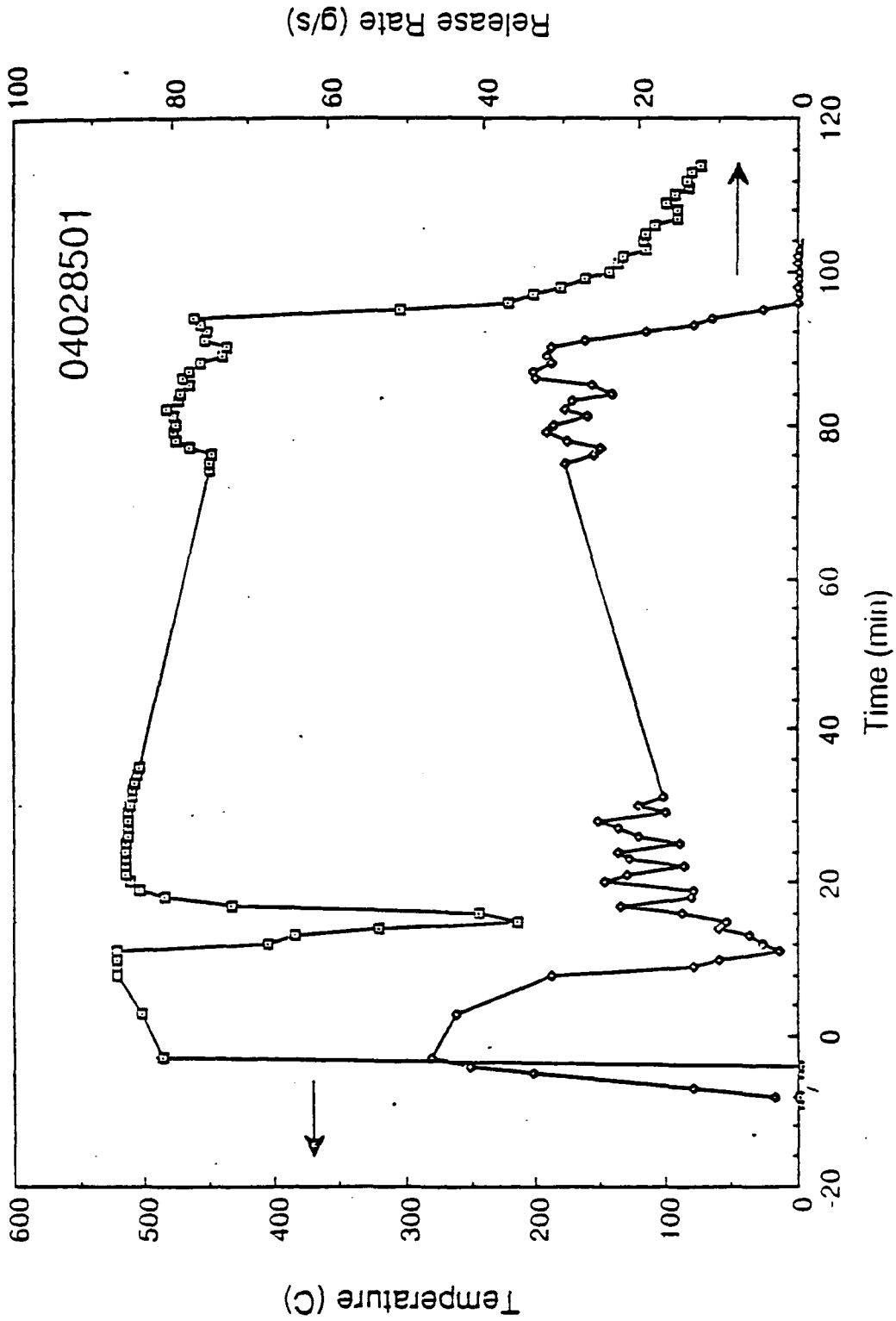


Figure 3.2. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test 10003 (2 April 85).
 Missing data due to equipment failure (tape jam) "Taken from L.I. Jegren et al., (1988)".

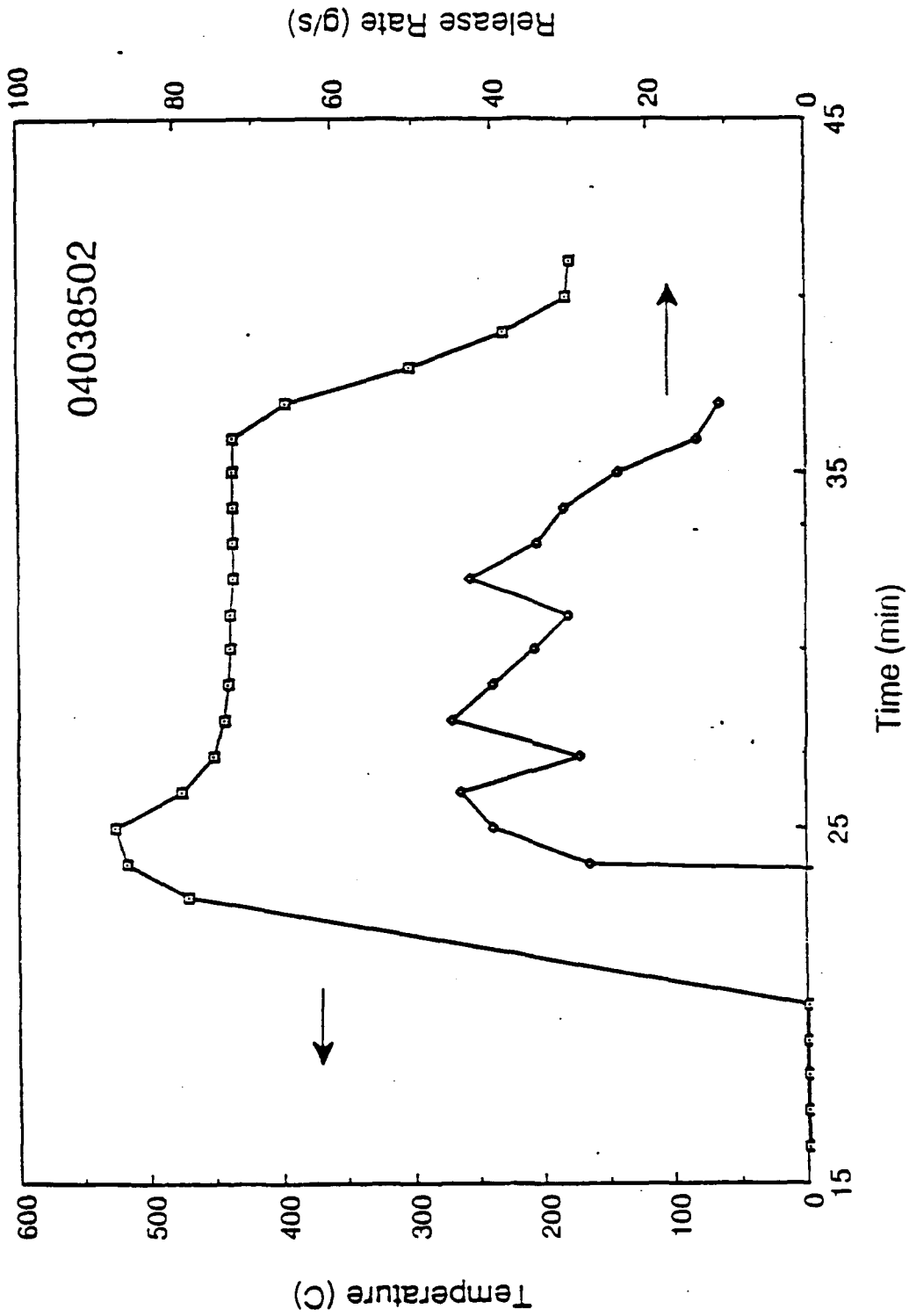


Figure 3.3. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test T0004 (3 April 1985).
 "Taken from Lilljegen et al., (1988)".

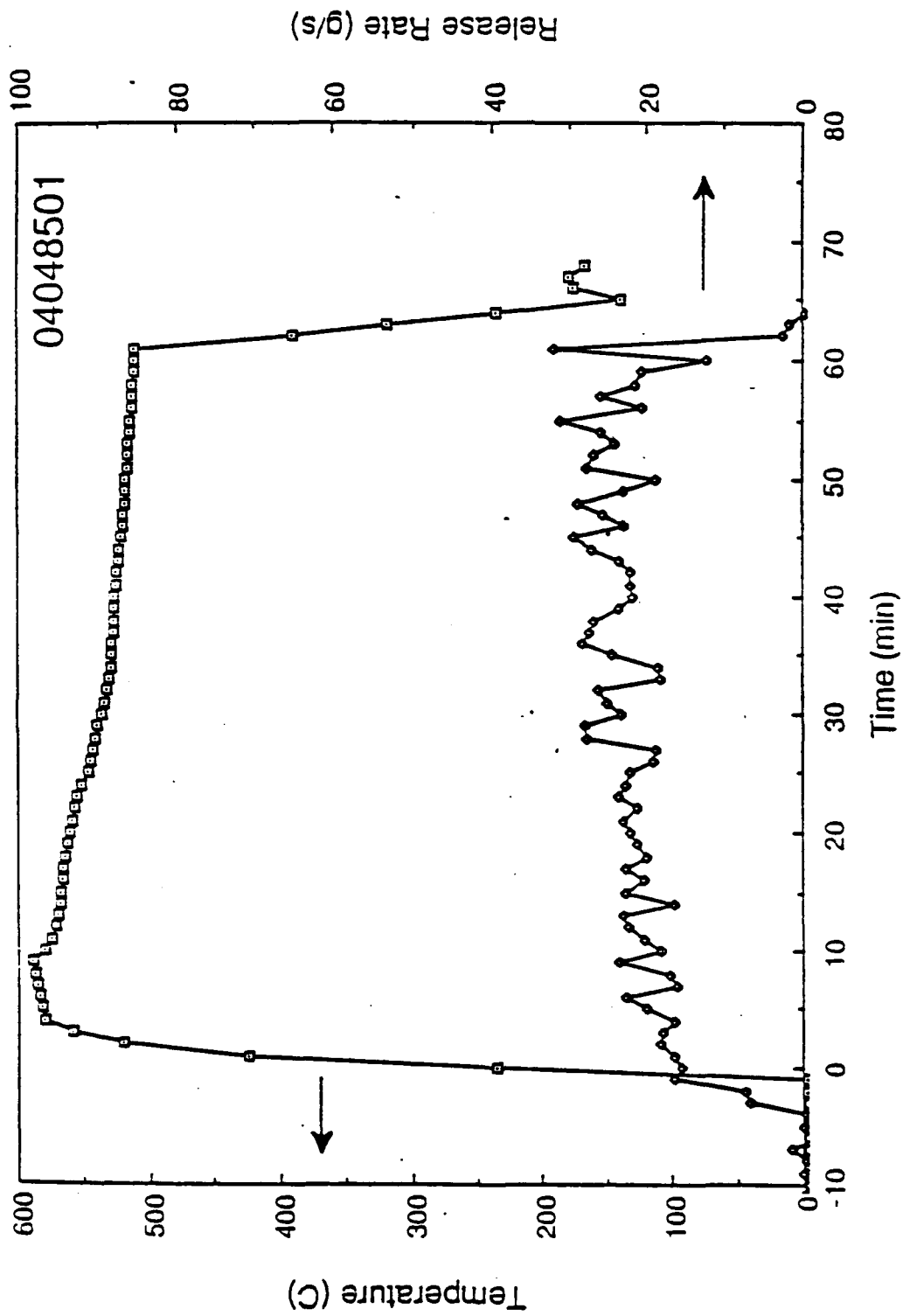


Figure 3.4. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test T0005 (4 April 1985).
 "Taken from Liljegren et al., (1988)".

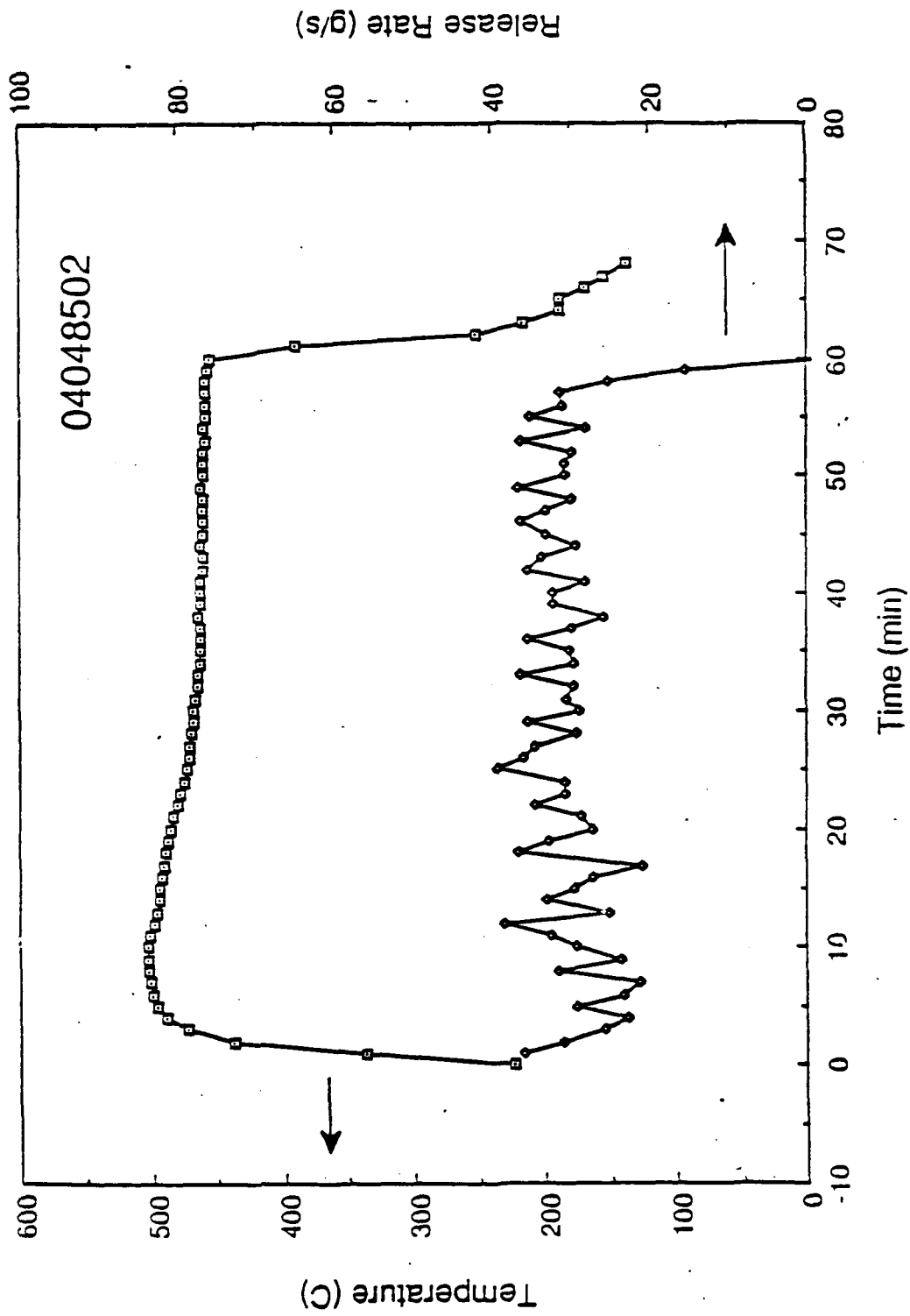


Figure 3.5. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test T0006 (4 April 1985).
 "Taken from L.L. Jørgen et al., (1988)".

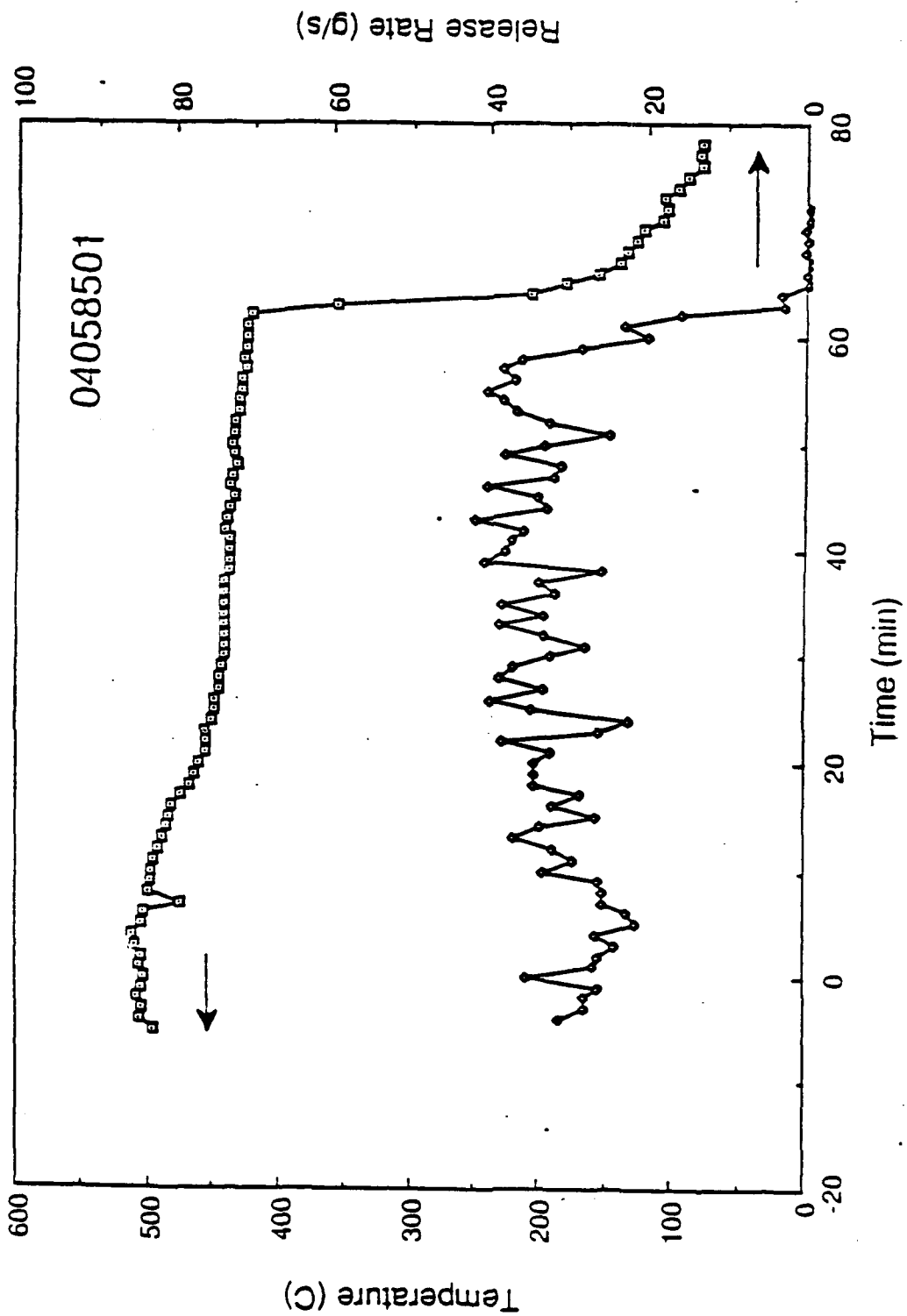


Figure 3.6. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test T0007 (5 April 1985).
 "Taken from Lilljegen et al., (1988)".

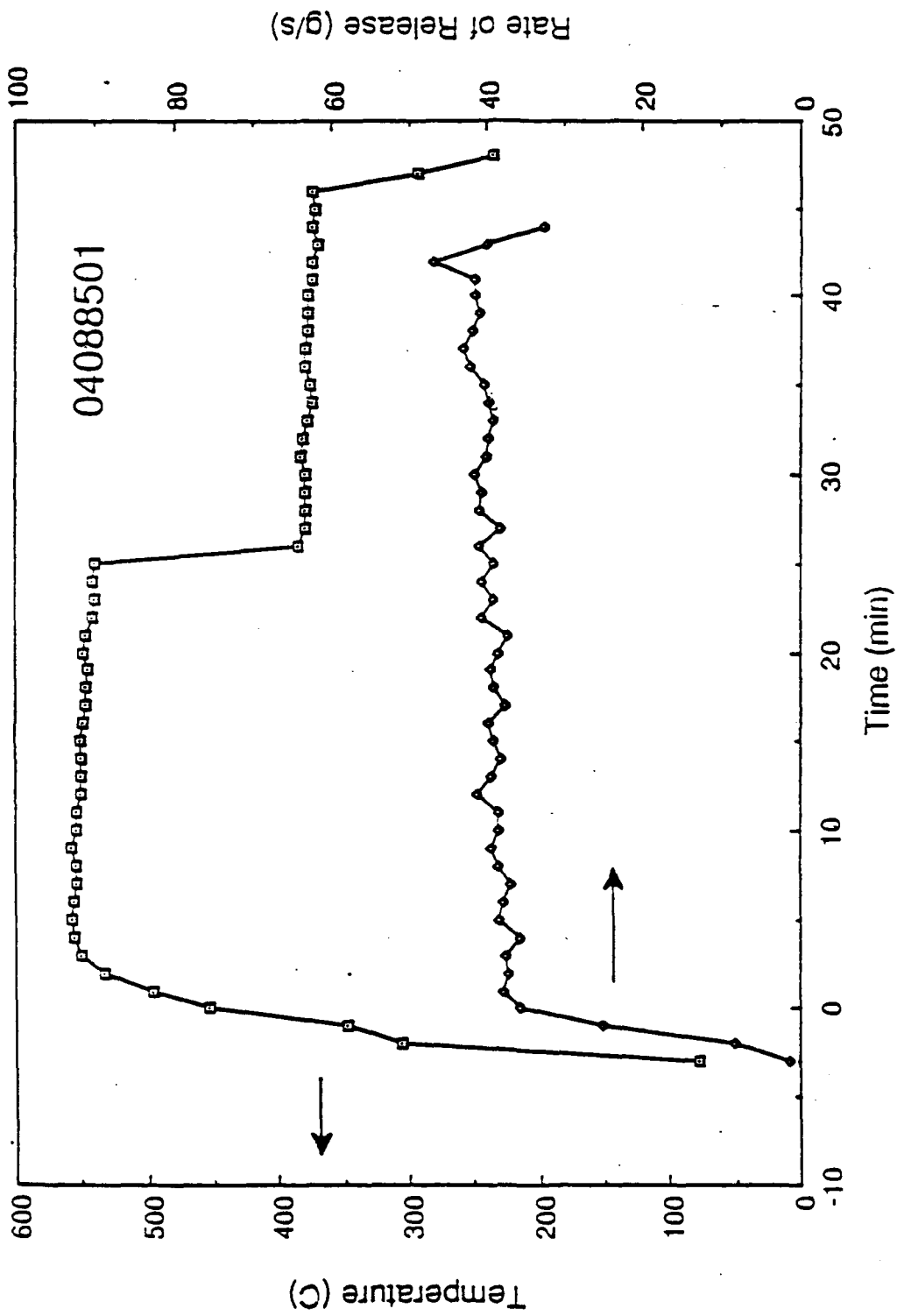


Figure 3.7. Exit Temperature (°C) and Release Rate (g/s) as a function of time for test T0008 (8 April 1985).
 "Taken from Lilljegen et al., (1988)".

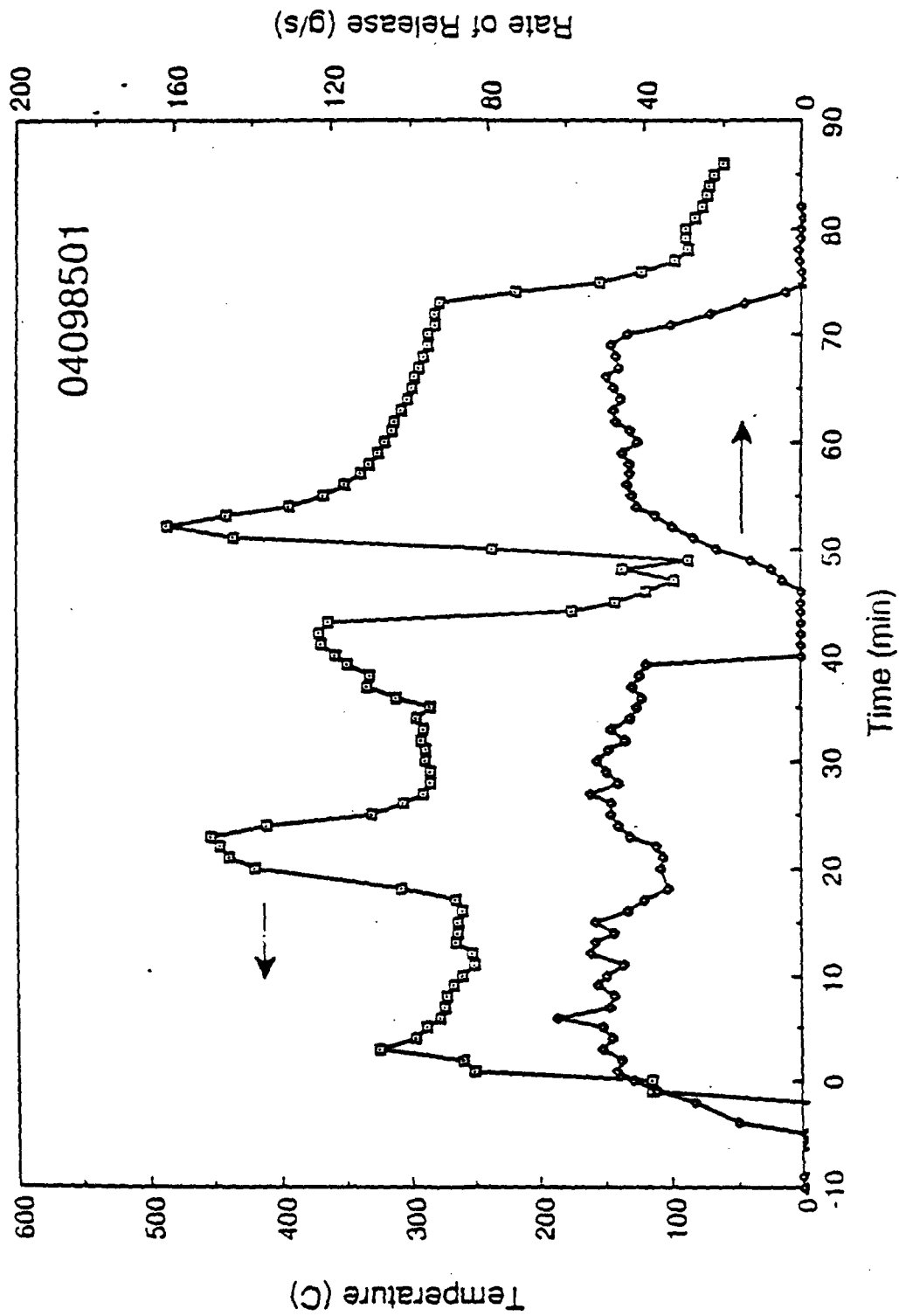


Figure 3.8. Exit Temperature ($^{\circ}\text{C}$) and Release Rate (g/s) as a function of time for test T0009 (9 April 1985).
 "Taken from Liljegren et al., (1988)".

Table B-1

Variation in Instantaneous (i.e., one-minute averaged)
Fog-Oil Smoke Emission Rates

Figure No.	Test No.	Average Instantaneous Emission Rate (g/s)	Standard Deviation	Coefficient of Variation
3.2	T0003	21.7	10.9	0.5
3.3	T0004	33.8	8.9	0.3
3.4	T0005	21.5	5.9	0.3
3.5	T0006	31.1	4.2	0.1
3.6	T0007	30.9	7.5	0.2
3.7	T0008	37.9	7.5	0.2
3.8	T0009	37.9	16.8	0.4

Table B-2

Comparison of Integrated and Averaged Instantaneous Methods
of Calculating Emission Rates

Figure No.	Test No.	Integrated Emission Rate (g/s)	Average Instantaneous Emission Rate (g/s)	Percent Difference
3.2	T0003	24.3	21.7	-12
3.3	T0004	22.5	33.8	+33
3.4	T0005	22.4	21.5	-4
3.5	T0006	28.7	31.1	+8
3.6	T0007	30.7	30.9	-0.1
3.7	T0008	36.3	37.9	+6
3.8	T0009	43.2	37.9	-12

* Taken from Liljegren et al., (1988), Table 3.1

interpolated the emission rate at 30 second intervals from the existing data which are at approximately one minute intervals. From this processed data, means and standard deviations were computed by grouping the data at 30 sec, 60 sec, 90 sec, etc. increments up to 510 seconds (8.5 minutes). To evaluate how the variability changed with averaging time, the following equation was used

$$R' = \left(\frac{\sigma_{i \text{ sec}}}{\sigma_{30 \text{ sec}}} \right) \quad (\text{B-1})$$

where $\sigma_{i \text{ sec}}$ is the standard deviation for the i-th averaging time (i = 60 sec, 90 sec, 120 sec, 510 sec) and $\sigma_{30 \text{ sec}}$ is the standard deviation from the 30 second averaging time.

3. Results

The first objective of this analysis is to evaluate the variance in the fog-oil generator emissions. Table B-1 shows that the variation in the emission rate, expressed as the standard deviation, can be large. The coefficient of variation (CV) normalizes the standard deviation by the mean. Test T0006 has the smallest CV - 0.1. Tests T0003 and T0009 have the largest CV's, 0.5 and 0.4 respectively. During these tests the smoke generator malfunctioned and the emissions were particularly erratic (see Figures 3.2 and 3.8).

The second objective of this analysis is to compare the methods for calculating the average emission rate. Table B-2 shows a comparison of the two methods of computing the mean emission rate. Liljegren et al. (1988) calculated the time integrated average by dividing the mass of oil burned by the duration of operation of the smoke generator. Our approach averaged the "instantaneous" 1 minute emission rates, as digitized from plots. The percent difference between the two methods ranges from -12% to +33%. The largest difference in the computed emission rates is for experiment T0004. A review of Figure 3.3 and the digitizing indicates that there were no errors in that step and that the mean rate of 33.8 g/sec accurately reflects the data in the plot. It is hypothesized that there may be an error in the field data relating to oil burned or duration of operation of the smoke generator, which may have caused Liljegren et al. to compute a lower emission rate. (In addition, Liljegren et al. note that the data for this experiment were divided into two groups based on a shift in wind direction. It is not clear

how this was done or if this would affect the emission rate calculation. The smallest difference was for T0007, an experiment when the smoke generator functioned in a very consistent mode (see Figure 3.6). There does not appear to be a bias in the Liljegren et al. method, with their approach producing a higher mean rate four times and a lower rate three times. The r^2 for the two methods of computing the emission rate is 0.56. This means the time integrated method of computing emissions can only account for 56% of the variance in the method based on averaging the "instantaneous" values.

The third objective of this analysis is to evaluate how the variability in the emission rate changes with averaging time. The data from five experiments, T0005 (Figure 3.4) through T0009 (Figure 3.8), were analyzed using equation (B-1). Two experiments, T0003 and T0004 (Figures 3.2 and 3.3, respectively), were excluded from this analysis due to insufficient data. Table B-3 presents the squared standard deviation ratios by averaging time for the five experiments as well as the median ratio for each averaging interval. These data are plotted in Figure B-1, with the solid line representing the median value and the minimum and maximums represented by the boxes.

A theoretical curve is also plotted in Figure B-1, representing the equation:

$$\frac{\sigma^2(T_a)}{\sigma^2(30s)} = \frac{1 + 30_s/2T_I}{1 + T_a/2T_I} \quad (B-2)$$

where T_I is the integral time scale of the physical process. This equation is based on work by G. I. Taylor in the 1920's and is further discussed in Section VIII of the main text. This theory assumes that the time scales of the fluctuations cover a wide range of values, and the time series data in the figures verify that this is the case. An integral scale, T_I , of 150 seconds provides the best fit to the data in Table B-1.

4. Conclusions

This analysis shows that the variation in the one-minute averaged emission rate from the fog-oil smoke generator can vary from 10% to 50% of the mean rate, based on the coefficient of variation. From the comparison of the two methods of computing the emission rate, it appears that when the smoke

Table B-3

Variations in Emission Rate with Averaging Time

Averaging Times (s)	Squared Standard Deviation Ratios*					Median Ratio
	T0005	T0006	T0007	T0008	T0009	
30.	1.000	1.000	1.000	1.000	1.000	1.000
60.	0.879	0.848	0.934	0.922	0.950	0.9220
90.	0.858	0.746	0.837	0.806	0.932	0.8370
120.	0.738	0.605	0.745	0.774	0.872	0.7450
150.	0.639	0.465	0.695	0.823	0.823	0.6950
180.	0.649	0.473	0.696	0.697	0.818	0.6960
210.	0.609	0.415	0.574	0.716	0.804	0.6090
240.	0.652	0.388	0.537	0.551	0.752	0.5510
270.	0.627	0.460	0.574	0.560	0.747	0.5740
300.	0.554	0.356	0.534	0.524	0.636	0.5340
330.	0.544	0.319	0.506	0.483	0.666	0.5060
360.	0.523	0.267	0.518	0.670	0.742	0.5230
390.	0.529	0.300	0.484	0.426	0.498	0.4840
420.	0.557	0.334	0.537	0.680	0.391	0.5370
450.	0.481	0.303	0.484	0.411	0.384	0.4110
480.	0.510	0.278	0.436	0.469	0.573	0.4690
510.	0.492	0.318	0.444	0.700	0.650	0.4920

$$R' = \left(\frac{\sigma_{1 \text{ sec}}}{\sigma_{30 \text{ sec}}} \right)^2$$

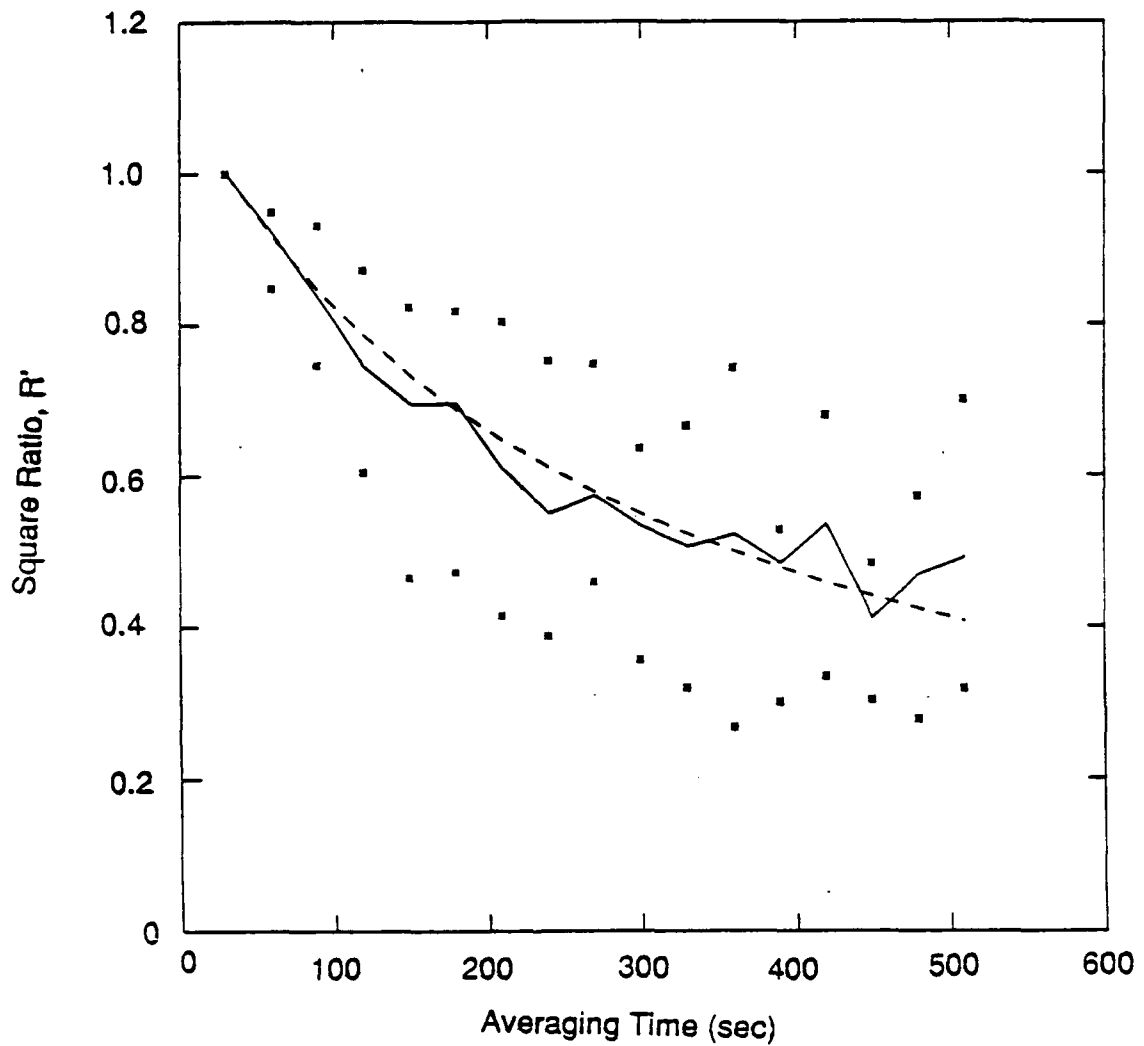


Figure B-1. Variation of emission rate fluctuation variance with averaging time. The solid line represents the median of the five experiments and the stars represent the range at that averaging time. The dashed line represents the theoretical curve given by Equation (B-2).

generator is operating in a consistent manner, both computational methods produce the same result (e.g., T0007, Figure 3.6). However, when the smoke generator malfunctions (e.g., T0003 and T0009, Figures 3.2 and 3.8, respectively), emissions can be highly variable, and the method of Liljegren et al. will over-estimate emissions relative to our method of averaging "instantaneous" emissions. An analysis of the emission rate variability with different averaging time showed that a time interval of 150 seconds best represented the experimental data.

5. References

Liljegren, J.C., W.E. Dunn, G.E. DeVaul, A.J. Policastro, Field Study of Fog-Oil Smokes, Supported by U.S. Army Medical Research and Development Command, Fort Detrick, MD, January, 1988.

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APPENDIX C

UNCERTAINTIES IN SOURCE EMISSION RATE ESTIMATES
USING DISPERSION MODELS

Reprint from Atmospheric Environment, 24A 2971-2980 (1990)

UNCERTAINTIES IN SOURCE EMISSION RATE ESTIMATES USING DISPERSION MODELS

STEVEN R. HANNA, JOSEPH S. CHANG and DAVID G. STRIMAITIS
Sigma Research Corp., 234 Littleton Rd., Suite 2E, Westford, MA 01886, U.S.A.

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Abstract—The source emission rates during the Prairie Grass dispersion experiments were carefully observed and were adjusted by the experimentalists so that they were about twice as high during unstable conditions as during stable conditions. The question was asked whether observed concentrations and meteorological conditions could be used in dispersion models in order to predict source emission rates and verify this factor of two difference. Three types of simple dispersion models were applied to this problem, with the result that for the model based on Monin-Obukhov similarity theory, the uncertainties in predictions of source emission rates for individual runs were at best about ± 10 –20% when observed cross-wind integrated concentrations from the 50 m arc were used. Consequently this model could discern the factor of two difference in average source emission rates for the two sets of field trials which consisted of about 20 runs each. However, some models, such as the Gaussian plume model, exhibit uncertainties of about ± 70 % to a factor of two in predictions for individual runs, and hence could not discern the difference in average source emission rates when concentration observations at downwind distances of 100–300 m are used. It is found that the use of observed cross-wind integrated concentrations produces more accurate conclusions than the use of observed point concentrations, for the uncertainties in predictions of source emission rates are about a factor of two larger when the observed point concentrations are used.

Key word index: Dispersion models, uncertainties in models, source emission estimates.

OBJECTIVE AND METHODS

As source emission rates for air pollutants are seldom well-known, air pollution control decisions must often be made based on observations of air pollution concentrations on monitoring networks. Observed concentrations can be combined with meteorological observations (e.g. wind speed and direction, stability, and mixing depth) and used in so-called hybrid source-receptor models in order to estimate source emission rates (Watson, 1989). These models are based on the concept that atmospheric transport and dispersion models are a mathematical link between observed concentrations and predicted source emission rates.

The specific objective of this research, funded by the U.S. Army, is to develop methods for estimating whether there is a significant difference in the source emission rate of similar types of sources from one experiment to another. For example, a typical source might be a fog oil generator (used for smoke obscuration purposes), and the question may be whether the source characteristics of the fog oil generator have significantly changed between 1980 and 1990. It is assumed that the source emission rate is not directly measured, but that several field trials are carried out at the same site in 1980 and in 1990. In each field trial, cross-wind integrated concentrations are observed at a distance 100 m downwind of the source, and wind velocities, turbulence, and vertical temperature gradients are observed on a tower near the source. The source position and orientation is not varied. Some

data of this type exist, and the procedures will eventually be tested with these data; however, first we have chosen to apply the source emission rate estimation methods to a simpler data set.

The Prairie Grass dispersion experiments produced a high-quality database (Barad, 1958) that has been used extensively in the development and testing of dispersion models. The experiments were simple, with near-ground-level continuous point sources, and extensive concentration and meteorological observations were made over the flat, homogeneous terrain. Source emission rates were also reported, and were deliberately varied so that they were twice as high during the day as during the night. Because of the care with which the Prairie Grass experiments were conducted, this database serves as an excellent test bed for study of the uncertainty in source emission rate estimation procedures. If the procedures cannot discern the known factor of two difference in average source emission rates in this highly controlled set of experiments, it would be of little use at more complicated sites, where the terrain may be more complex and the observations are likely to contain more errors.

Three representative dispersion models are used to relate observed concentrations and meteorological conditions to source emission rates. The three models include a statistical regression model, a Monin-Obukhov similarity model, and a Gaussian plume model. The Student-*t* test is used to determine whether the models can discern a factor of two difference, at the 95% confidence level, between average night and day

source emission rates. Another output of this procedure is an estimate of the typical error or uncertainty in the source emission rate estimate.

DESCRIPTION OF PRAIRIE GRASS DATABASE

Barad (1958) discusses the Prairie Grass database in great detail. SO_2 tracer gas was released over periods of about 10 min from a point source located at an elevation of 0.45 m. Ten minute averaged tracer concentrations were obtained from measurements observed at an elevation of 1.5 m along arcs at distances of 50, 100, 200, 400 and 800 m from the source. Supporting meteorological observations were made from a nearby tower, located in a flat area, representative of the site, where the average surface roughness, z_0 , was determined to be 0.6 cm. Data from 44 experiments were used in our analysis, covering a wide range of meteorological conditions. The data are approximately equally divided into unstable and stable periods.

The Prairie Grass data are listed in Table 1, based on information in the report by Barad (1958) and in papers by van Ulden (1978), Nieuwstadt (1980), and Briggs (1982). The 2 m wind speed, u , the 2 m standard deviation of wind direction fluctuations σ_d , and the 16 m to 2 m temperature difference, DT , were given in Barad's (1958) report, and the friction velocity, u_* , and the Monin-Obukhov length, L , were estimated by van Ulden (1978). The mixing depth and convective scaling velocity, w_* , were calculated for most unstable experiments by Nieuwstadt (1980). The stability class, SC , is estimated using observations of surface roughness, z_0 , Monin-Obukhov length, L , and Golder's (1972) nomogram. Briggs (1982) carefully reviewed all of the data and suggested that certain arcs for some experiments be removed from the data set because of problems with those particular data. At each downwind distance, the table lists observations of C/Q , C^*/Q , and σ_y , where C is the maximum concentration on that arc, C^* is the cross-wind integrated concentration and σ_y is the standard deviation of the lateral concentration distribution. The C^* and σ_y data were given by Nieuwstadt (1980) for most of the unstable periods. The standard deviation of vertical wind direction fluctuations, σ_{θ} , has been estimated using boundary layer similarity theory.

DISPERSION MODELS

Data from the Prairie Grass experiments (Barad, 1958) were used extensively by Pasquill (1961) and others in the development and testing of a Gaussian diffusion model now known as the Pasquill-Gifford-Turner model (Gifford, 1962, 1968, 1976; Turner, 1967), which is the basis for most decisions regarding air pollution control in the U.S. The data were also part of the database used by Nou (1963) in the

development of the empirical OB-DG model, which is the basis of the U.S. Air Force procedures for calculating toxic gas impacts. Because the early data analyses did not make use of Monin-Obukhov similarity modeling or convective scaling concepts, there was a flurry of activity with reanalyses of the Prairie Grass data from this new point of view in the late 1970s (e.g. van Ulden, 1978; Horst, 1979; Nieuwstadt, 1980; Venkatram, 1981; Briggs, 1982). In several of these papers, the new scaling parameters (e.g. the mixing depth, h , the friction velocity, u_* , and the Monin-Obukhov length, L) were derived by reanalyzing the original field data.

The variety of dispersion models in the references listed above can be grouped into three classes.

- Class 1. Empirical or statistical regression models (e.g. Nou, 1963).
- Class 2. Similarity models (e.g. Briggs, 1982).
- Class 3. Gaussian plume models (e.g. Gifford, 1976).

Because Nou's (1963) empirical or statistical regression formula was based on several other databases besides the Prairie Grass database, and he did not suggest a formula for the cross-wind integrated concentration, we decided not to use his formula directly, but instead we applied a multivariate linear regression procedure to the data in Table 1 in order to derive the following best-fit power-law formulas:

$$C/Q = 0.000137x^{-1.91}(DT + 10^\circ\text{F})^{4.72} \quad (1)$$

$$C^*/Q = 0.00666x^{-1.03}(DT + 10^\circ\text{F})^{2.34} \quad (2)$$

where C/Q and C^*/Q are in units of s m^{-3} and s m^{-2} , respectively, x is in units of m and DT is in units of $^\circ\text{F}$. This is the same statistical procedure applied by Nou (1963), and the units for all variables are consistent with those that he used. Nou (1963) also used the 10°F additive factor, which is necessary to prevent negative values of the temperature term. These formulas explain 91 and 84%, respectively, of the variance in the C/Q and C^*/Q observations, where most of the variance is explained by the x term. Note that these formulas are not based at all on physical insights, but are based on least-square fits of linear relationships to the data.

The group of similarity models proposed by van Ulden (1978), Horst (1979), Nieuwstadt (1980), Venkatram (1981) and Briggs (1982) is based on applications of Monin-Obukhov similarity theory and convective scaling similarity theory. According to Monin-Obukhov similarity theory, the following functional relations can be postulated for dispersion from continuous ground-level point sources in the surface boundary layer (Briggs, 1982):

$$Cu_*x^2/Q = f_1(x/L) \quad (3)$$

$$C^*u_*x/Q = f_2(x/L) \quad (4)$$

where f_1 and f_2 are non-dimensional universal functions. The friction velocity, u_* , and the Monin-

Obukhov length, L , are the fundamental scaling velocity and scaling length in the surface boundary layer, according to Monin-Obukhov similarity theory. The Prairie Grass data are plotted in Fig. 1 in the dimensionless forms suggested by Equations (2) and (3), illustrating that the data are ordered quite well by these similarity relations.

Because the data in the four parts of Fig. 1 appear to approach a constant as x/L approaches zero, the following functional relation is proposed:

$$f(x/L) = a(1 + bx/L)^f \quad (5)$$

A least-squares algorithm was applied to each figure, with the following results:

$$f_1(x/L) = 3.37(1 - 0.019x/L)^{-1.36} \quad x/L < 0 \quad (6)$$

$$f_1(x/L) = 3.01(1 - 2.20x/L)^{0.57} \quad x/L > 0 \quad (7)$$

$$f_2(x/L) = 1.06(1 - 0.021x/L)^{-1.74} \quad x/L < 0 \quad (8)$$

$$f_2(x/L) = 1.07(1 + 0.10x/L)^{0.68} \quad x/L > 0 \quad (9)$$

These curves are drawn on the figures and appear to

provide a good fit at all values of x/L . However, they have been derived with no requirements that certain physically-based asymptotic functional relationships be satisfied. For example, Briggs (1982) points out that $f_2(x/L)$ should be proportional to $(-x/L)^{1/2}$ in the limit of free convection ($-x/L \rightarrow \infty$). Consequently, Briggs' (1982) suggests a third term in Equation (5), which he claims to better account for "convective sweep-out" of the plume at large $|x/L|$. The similarity model is represented by Equations (6)-(9) in our analysis rather than the equations proposed in any of the above references because the other equations are based on a slightly different subset of the Prairie Grass database.

The Gaussian plume models comprise the third class of models in our analysis. The Gaussian model is based on the formulas (Gifford, 1976)

$$C/Q = (\pi u \sigma_y \sigma_z)^{-1} \exp(-(z - z_r)^2 / 2\sigma_z^2) \quad (10)$$

$$C^*/Q = (2/\pi)^{1/2} (u \sigma_z)^{-1} \exp(-(z - z_r)^2 / 2\sigma_z^2) \quad (11)$$

The source height, z_r , and receptor height, z_r , equal

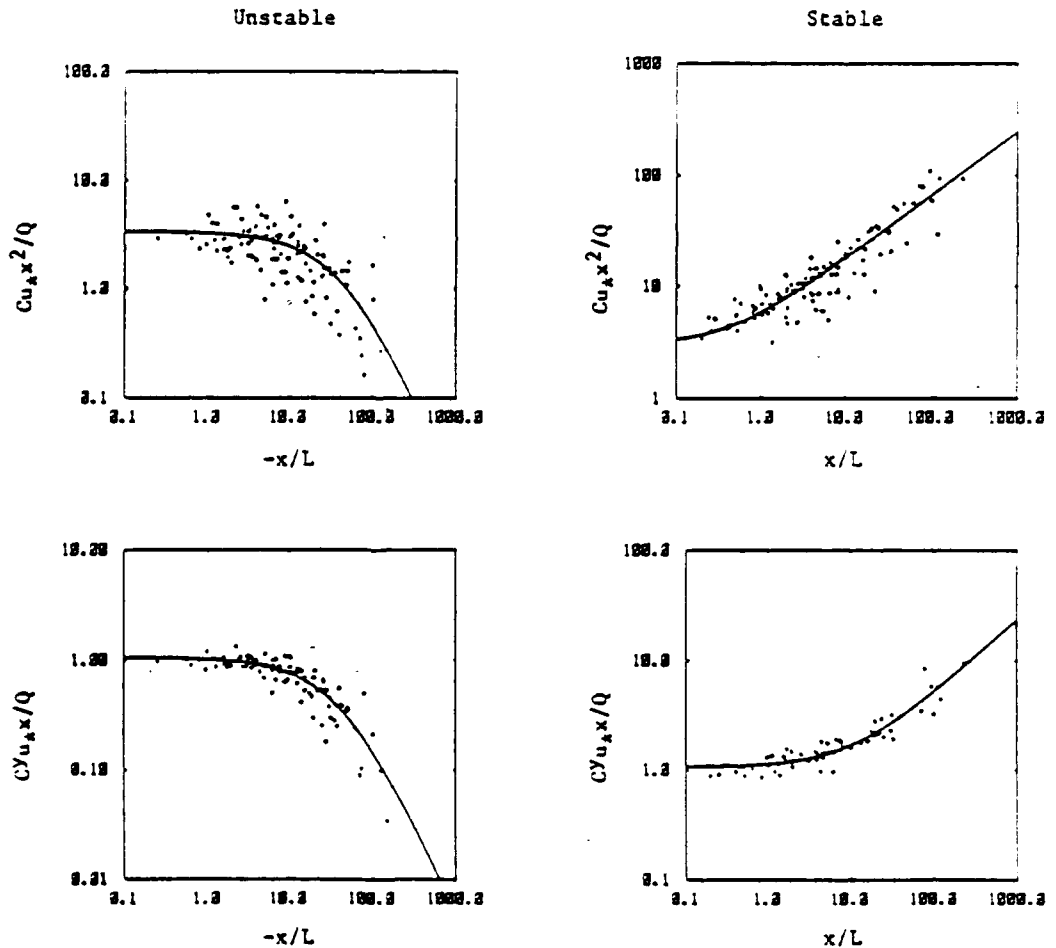


Fig. 1. Prairie Grass data plotted in the dimensionless form suggested by Equations (3) and (4). Best-fit lines of the form $a(1 + bx/L)^f$ are drawn on each figure (see Equations (6)-(9)).

0.45 m and 1.5 m, respectively, in the Prairie Grass experiments. The wind speed, u , is assumed to be that measured at a height of 2 m (see Table 1). The values for lateral and vertical dispersion coefficients, σ_y and σ_z , that are substituted into Equations (10) and (11) are based on suggestions by Briggs (1973), who used the Prairie Grass experiments, along with many other field experiments, in their derivation. These σ_y and σ_z formulas are given in Table 2. The required stability class is found in Table 1 for each Prairie Grass test.

Note that the empirical and similarity classes of dispersion models have been best-fit to the exact same data (Table 1) that will be used for further testing. The Gaussian plume model has not been subjected to these same best-fit procedures, but has been based on data from many experiments. Because of these differences in databases used to derive the models, it is expected that the Gaussian plume model will have the least success in any comparisons with field data from the Prairie Grass database.

The dispersion models in Equations (3) and (4) and (6)–(10) are inverted in order to predict source emission rates:

$$Q_p = C_o(C'/Q)_p \quad (12)$$

$$Q_p = C'_o(C'/Q)_p \quad (13)$$

where subscripts o and p represent observed and predicted variables, respectively. Because of the characteristics of the multiple linear regression or least-squares statistical procedures, an equation that produces a best-fit for C'/Q or C''/Q may not necessarily produce a best-fit for Q . These statistical procedures attempt to minimize the mean-square error and to force the mean of the observed variable to equal the mean of the predicted variable. We should therefore not be surprised if an equation which produces zero mean bias in C'/Q is discovered to produce a mean bias of 20–30% or more in Q .

STATISTICAL PROCEDURES

A primary objective of this research is the development of methods for estimating whether there is a significant difference in the source emission rate of similar types of sources from one experiment to another, as determined by observations of meteorological conditions and of point concentrations or

cross-wind integrated concentrations. Dispersion models, such as the three presented above, can be used to remove the effects on the concentration observations of variations in meteorological parameters and down-wind position of the concentration monitor.

A listing of the observed source emissions, Q , during the Prairie Grass experiment is given in Table 1, and the data are plotted in Fig. 2 as a function of the stability parameter $1/L$ (the point for run 46 has been excluded, since it was an evening transition period when Q was still high although $1/L$ had just become positive). During the Prairie Grass experiment the night-time emissions, Q , of tracer gas were controlled so that Q averaged 45.2 gs^{-1} with a range from about 38 to 58 gs^{-1} and a standard deviation of 5.91 gs^{-1} , and the daytime emissions were controlled so that Q averaged 98.25 gs^{-1} with a range from about 90 to 105 gs^{-1} and a standard deviation of 4.48 gs^{-1} . The experimentalists deliberately maintained this factor of 2 difference in day-night Q s so that the magnitude of concentrations at the monitors would not vary much from day to night. With 19 stable (night) runs and 20 unstable (day) runs, the Student- t parameter (Panofsky and Brier, 1968, p. 63) can be calculated in order to determine if the daytime \bar{Q} is significantly different from the night-time \bar{Q} :

$$t = (\bar{Q}_d - \bar{Q}_n) \left(\frac{N_d \sigma_d^2 + N_n \sigma_n^2}{N_d + N_n - 2} \left(\frac{1}{N_d} + \frac{1}{N_n} \right) \right)^{-1/2} \quad (14)$$

where subscripts d and n indicate day and night. If $|t|$ is less than 2.04, then the difference ($\bar{Q}_d - \bar{Q}_n$) is not significantly different from zero, at the 95% confidence level. In fact, using the observed \bar{Q} and σ_Q

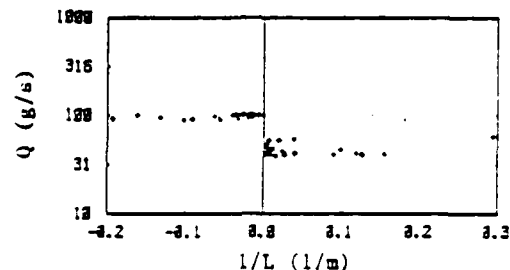


Fig. 2. Observed tracer gas source emission rates, Q , as a function of inverse Monin-Obukhov length, $1/L$, for the Prairie Grass data (run 46 excluded).

Table 2. Formulas recommended by Briggs (1973) for σ_y and σ_z , for rural conditions

Stability class	σ_y (m)	σ_z (m)
A	$0.22x(1 - 0.0001x)^{-1/2}$	0.20x
B	$0.16x(1 - 0.0001x)^{-1/2}$	0.12x
C	$0.11x(1 - 0.0001x)^{-1/2}$	$0.08x(1 - 0.0002x)^{-1/2}$
D	$0.08x(1 - 0.0001x)^{-1/2}$	$0.06x(1 - 0.0015x)^{-1/2}$
E	$0.06x(1 - 0.0001x)^{-1/2}$	$0.03x(1 + 0.0003x)^{-1}$
F	$0.04x(1 - 0.0001x)^{-1/2}$	$0.016x(1 - 0.0003x)^{-1}$

figures quoted above, the calculated Student-*t* parameter is 30.86 for the difference between the mean night-time and daytime emission rates, which implies that the difference is significant at far greater than the 95% confidence level.

Because there is such a clear difference in the observed day and night tracer gas source emission rates, Q , at the Prairie Grass site, it is interesting to ask whether the dispersion models would be able to predict this significant difference in the mean emission rates, based on observed concentrations and meteorological variables. The three types of models described earlier were used to prepare predictions of source emission rate, Q_p (one set of predictions using C_p and another set using C_p^*). This calculation of Q_p was made individually using data from each of five monitoring arcs (50, 100, 200, 400 and 800 m) for C_p , and each of three monitoring arcs (50, 200 and 800 m) for C_p^* . For each set of predictions, values of night-time and daytime \bar{Q}_p and σ_{Qp} were calculated. Then Equation (14) was used to calculate the Student-*t* parameter. If the resulting *t* value exceeds 2.04, it is concluded that the model successfully simulated the difference in source emission rates. If *t* is less than 2.04, then it is concluded that the model has failed to simulate the difference.

Besides investigating the day-night difference in mean source emission rate predictions, it is also of interest to investigate the ability of the models to predict emission rates for all Prairie Grass runs taken as a group. For this purpose, the following performance measures are calculated (where an overbar represents an average over all the database).

$$\text{Relative bias: } (\bar{Q}_p - \bar{Q}_o) / \bar{Q}_o$$

$$\text{Correlation: } r = (Q_p - \bar{Q}_p)(Q_o - \bar{Q}_o) / \sigma_{Qp} \sigma_{Qo}$$

Fractions of predictions, Q_p , within a factor of two of observations, Q_o .

$$\text{Normalized mean square error: } \overline{(Q_p - Q_o)^2} / \bar{Q}_o \bar{Q}_o$$

These performance measures are tabulated for each model and for C_p and C_p^* on each monitoring arc. In addition, the individual residuals ($Q_p - Q_o$) are plotted as a function of downwind distance for each model.

RESULTS AND CONCLUSIONS

Predictions of average daytime and night-time source emission rates

The procedures for estimating the daytime and night-time average source emission rates reviewed above were applied to the Prairie Grass database, with the results given in Tables 3 and 4, for C_p and C_p^* , respectively. By comparing the numbers in the two tables, it is evident that use of the observed cross-wind integrated concentration, C_p^* , produced better results than use of the observed point concentration, C_p . The standard deviations, σ_{Qp} , of the predicted source emission rates are about 50% larger during the night, and a factor of 2 or 3 larger during the day, for C_p than for C_p^* . Consequently the calculated Student-*t* parameters are about twice as large for C_p^* than for C_p , implying that there is more confidence in the conclusions for C_p^* . We expected that there would be a difference, because

Table 3. Predictions of source emission rate, Q_p (g s^{-1}), for night-time and daytime Prairie Grass runs, using observed maximum concentrations, C_p , on monitoring arcs at distances of 50, 100, 200, 400 and 800 m. Three different models are used to calculate $Q_p = C_p(C/Q)_p$. The average, \bar{Q}_p , and standard deviation, σ_{Qp} , for night-time and daytime conditions is listed. Student-*t* is calculated using Equation (14)

Model	Monitoring distance (m)	Student <i>t</i>	Night (<i>N</i> = 19)		Day (<i>N</i> = 20)	
			\bar{Q}_p (g s^{-1})	σ_{Qp} (g s^{-1})	\bar{Q}_p (g s^{-1})	σ_{Qp} (g s^{-1})
Observed Q		30.86	45.2	5.9	98.2	4.5
Regression	50	7.40	30.1	12.0	144.6	64.7
	100	5.47	43.8	19.4	139.1	71.6
	200	4.27	52.0	23.0	128.3	72.5
	400	2.20	61.2	27.3	93.4	56.2
	800	-1.19	84.2	51.6	64.5	48.9
Similarity	50	5.68	39.9	14.1	70.8	18.5
	100	4.62	49.2	16.2	84.0	37.1
	200	5.51	48.7	16.2	101.1	37.1
	400	5.52	45.8	15.6	105.4	43.2
	300	4.30	46.3	14.6	116.2	60.1
Gaussian	50	2.40	55.2	45.5	115.5	96.9
	100	1.07	76.3	94.9	109.2	92.2
	200	0.05	98.1	150.9	100.2	70.1
	400	-0.88	118.8	196.3	76.8	62.7
	300	-1.67	150.1	264.1	48.0	30.1

Table 4. Predictions of source emission rate, Q_p (g s^{-1}), for night-time and daytime Prairie Grass runs, using observed cross-wind integrated concentrations, C_p^* , on monitoring arcs at distances of 50, 200 and 300 m. Three different models are used to calculate $Q_p = C_p^* / (C^* Q_p)$. The average, \bar{Q}_p , and standard deviation, σ_{Q_p} , for night-time and daytime conditions listed. Student- t is calculated using Equation (14)

Model	Monitoring distance (m)	Student t	Night ($N = 19$)		Day ($N = 20$)	
			\bar{Q}_p (g s^{-1})	σ_{Q_p} (g s^{-1})	\bar{Q}_p (g s^{-1})	σ_{Q_p} (g s^{-1})
Observed Q		27.27	45.2	5.9	97.8	4.7
Regression	50	17.19	29.7	9.8	140.1	24.8
	200	7.43	46.9	16.9	124.8	40.1
	300	-0.58	69.4	34.3	62.1	36.4
Similarity	50	16.24	39.7	8.3	89.6	9.0
	200	9.54	49.0	9.0	100.1	20.3
	300	4.38	45.2	13.8	99.6	50.2
Gaussian	50	6.18	61.7	30.9	161.0	58.4
	200	2.83	65.5	60.3	116.6	34.9
	300	-0.99	85.5	145.1	46.9	20.3

σ_p is another complicating factor included in C_p that would act to increase the uncertainty, but did not expect that the difference would be this large.

The ability of the models to arrive at the proper answer (i.e. that the daytime \bar{Q} is significantly larger than the night-time \bar{Q} , with at least 95% confidence) can be seen by identifying cases where $t \geq 2.04$ in Tables 3 and 4. It is seen that most models are able to reproduce this conclusion at most arc distances. However, false conclusions ($t < 2.04$) are reached for the following arcs and models.

C_p : 100 m arc:	Gaussian
200 m arc:	Gaussian
400 m arc:	Gaussian
800 m arc:	Regression and Gaussian.
C_p^* : 800 m arc:	Regression and Gaussian.

It is seen that the use of C_p and C_p^* from the closest arc (50 m) leads to the correct conclusion for all three models, with a value for Student- t ranging from 2.4 to 7.4 for C_p , and 5.2 to 17.2 for C_p^* . The regression and similarity models are seen to be better able to simulate the difference in observed Q (i.e. they yield a higher t) than the Gaussian model. However, the number of false conclusions increases as downwind distance increases. At the 300 m arc in both tables, only the similarity model yields the proper conclusion. Figs 3 and 4 contain extreme examples of plots of predicted source emission rates, Q_p , as a function of $1/L$, in the same format as the observations in Fig. 2. The similarity model predictions in Fig. 3, using observations of C_p^* on the 50 m arc, produce patterns similar to the observed data, but with slightly more scatter. However, the Gaussian plume model predictions in Fig. 4, using observations of C_p on the 300 m arc, obviously miss the overall trend of the observations of Q_p , as well as containing much more scatter.

The failure of the regression model and the Gaussian model to estimate \bar{Q} using C_p and C_p^* observations

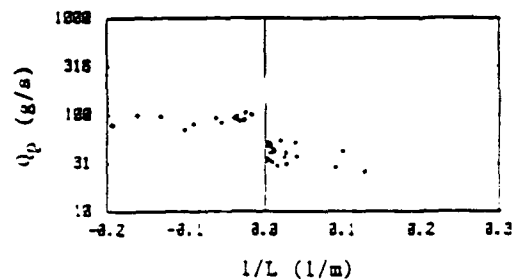


Fig. 3. Tracer gas source emission rates, Q_p , predicted by the similarity model as a function of inverse Monin-Obukhov length, $1/L$, for the Prairie Grass data (run 46 excluded). Observed cross-wind integrated concentrations on the 50 m arc are used.

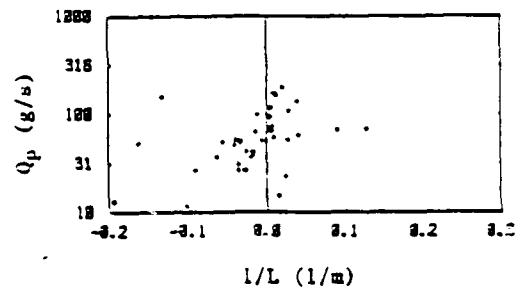


Fig. 4. Gas source emissions rate predicted by the Gaussian plume model, Q_p , as a function of inverse Monin-Obukhov length, $1/L$, for the Prairie Grass data (run 46 excluded). Observed concentrations on the 300 m arc are used.

at the largest distances may be seen by investigating the variation of the ratio C_p/C_p^* with distance for the three models for stable and unstable conditions (Figs 5 and 6). The C_p/C_p^* values for the similarity model have very little trend with distance and are always centered

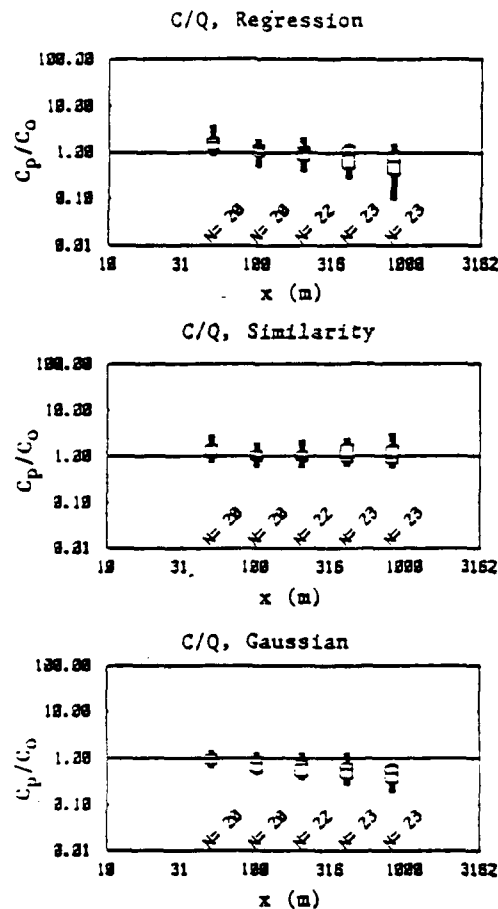


Fig. 5. Ratios of predicted to observed concentrations (C/Q) for the Prairie Grass dataset, as a function of downwind distance, for three models (regression, similarity, and Gaussian) for stable conditions. N is the number of data points at each distance. The midline of each box plot is the median, and the other lines represent \pm one and two standard deviations.

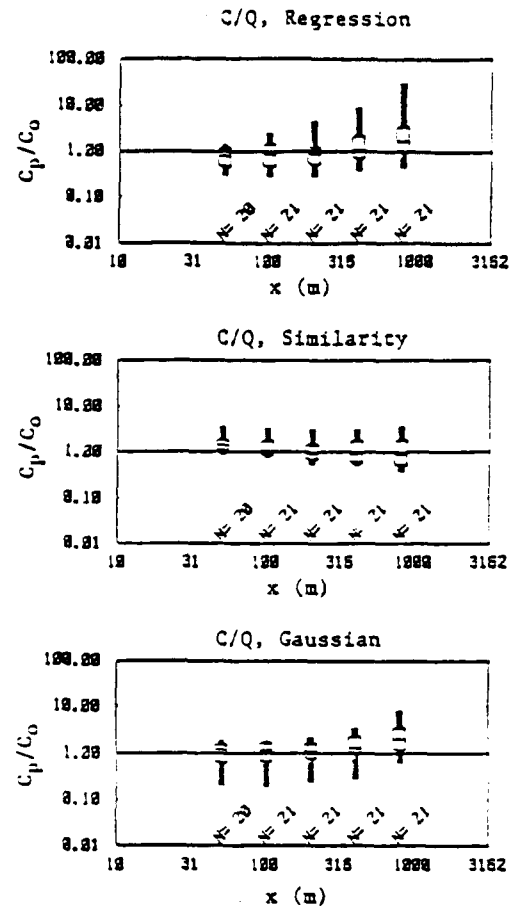


Fig. 6. Ratios of predicted to observed concentrations (C/Q) for the Prairie Grass dataset, as a function of downwind distance, for three models (regression, similarity, and Gaussian) for unstable conditions. N is the number of data points at each distance. The midline of each box plot is the median, and the other lines represent \pm one and two standard deviations.

on 1.0. In contrast, at large distances, the regression and Gaussian models tend to underpredict ($C_p/C_o < 1$) during stable conditions (Fig. 3) and overpredict ($C_p/C_o > 1$) during unstable conditions. It is important to note that a model which overpredicts the concentration, C , will underpredict the source emission rate, Q . Consequently, at large distances, the regression and Gaussian models can be expected to overpredict the source emission rate, Q , during stable conditions, and underpredict it during unstable conditions. But since the observed stable \bar{Q} is about 45 gs^{-1} and the unstable \bar{Q} is about 98 gs^{-1} , the \bar{Q} s predicted by these two models will tend to be either nearly the same, or their relative magnitudes may even be switched. This problem is seen to occur for the Gaussian model on the 800 m arc, using the C_o data, where the following discrepancy is found in Table 3 and can be seen in Figs 2 and 4

Thus the Gaussian model leads to the opposite conclusion regarding daytime and night-time \bar{Q} differences if the 300 m C_o data are used. Note that if the experimentalists had controlled the emissions in the opposite way, such that the night-time Q exceeded the daytime Q , then these trends in the errors in the regression and Gaussian models would have led to a correct conclusion regarding the differences in Q .

	Night	Day
Observed \bar{Q}_o	45.2	98.2
Gaussian predicted \bar{Q}_o	150.1	48.0

Consider the best-performing model in Table 6, where C_o^* data from the 50 m arc are used in the similarity model to predict the average source emission rate, \bar{Q} (see Fig. 3). The calculated Student- t value

Table 5. Evaluations of predictions of source emission rate, Q_o ($g s^{-1}$), for all Prairie Grass runs, using observed maximum point concentrations, C_o , on monitoring arcs at distances of 50, 200 and 300 m. Three different models are used to calculate $Q_o = C_o (C/Q)_o$.

Distance to C_o observation	Model	\bar{Q}_o ($g s^{-1}$)	$\frac{\bar{Q}_o - Q_o}{Q_o}$	Correlation r	Fraction within factor of 2	$\frac{Q_o - Q_o^2}{\bar{Q}_o \bar{Q}_o}$
	Observed	72.4				
50 m	Regression	88.8	0.23	0.77	0.82	0.53
	Similarity	55.7	-0.23	0.74	0.90	0.15
	Gaussian	86.1	0.19	0.36	0.80	0.97
200 m	Regression	91.2	0.26	0.59	0.85	0.51
	Similarity	75.6	0.04	0.71	0.92	0.14
	Gaussian	99.2	0.37	0.02	0.74	2.08
300 m	Regression	74.1	0.02	-0.15	0.54	0.70
	Similarity	82.1	0.13	0.65	0.90	0.34
	Gaussian	97.6	0.35	-0.25	0.49	5.75

Table 6. Evaluation of predictions of source emission rate, Q_o ($g s^{-1}$), for all Prairie Grass runs, using observed cross-wind integrated concentrations, C_o^i , on monitoring arcs at distances of 50, 200 and 300 m. Three different models are used to calculate $Q_o = C_o^i / (C^i/Q)_o$.

Distance to C_o observation	Model	\bar{Q}_o ($g s^{-1}$)	$\frac{\bar{Q}_o - Q_o}{Q_o}$	Correlation r	Fraction within factor of 2	$\frac{Q_o - Q_o^2}{\bar{Q}_o \bar{Q}_o}$
	Observed	68.4				
50 m	Regression	78.4	0.14	0.94	0.91	0.23
	Similarity	61.7	-0.10	0.98	1.00	0.02
	Gaussian	106.0	0.55	0.74	0.88	0.55
200 m	Regression	81.2	0.19	0.80	0.94	0.21
	Similarity	71.6	0.05	0.89	1.00	0.04
	Gaussian	88.1	0.29	0.46	0.88	0.48
300 m	Regression	66.1	-0.03	-0.07	0.74	0.46
	Similarity	69.2	0.01	0.60	0.88	0.26
	Gaussian	68.4	0.00	-0.15	0.65	2.98

in this case is 16.2. Since $\bar{Q}_o(\text{day}) - \bar{Q}_o(\text{night}) \cong 53 g s^{-1}$, it is concluded that a significant difference in \bar{Q} values could be discerned by this model if $\Delta\bar{Q}_o = \bar{Q}_o(\text{day}) - \bar{Q}_o(\text{night})$ drops as low as $53 \times (2.04/16.2) = 6.7 g s^{-1}$; that is, if $\Delta\bar{Q}_o$ is about 15% of \bar{Q}_o . Therefore, in these best of research-grade experiments, where there are about 20 daytime and 20 night-time tests, and where a dispersion model is fit to these same data, a day-night difference in \bar{Q} of less than 15% of the mean would not be estimated to be significant by this procedure.

Predictions of source emission rates for all cases

Putting aside the question of differences in daytime and night-time averages in \bar{Q} , it is possible to use the complete database to estimate the overall ability of the models to estimate the 39 individual source emission rates. The relative bias, the correlation, the fraction of predictions within a factor of two of observations, and the normalized mean square error for the three models are listed in Table 5 and 6, for maximum point concentrations and cross-wind integrated concentra-

tions, respectively. These performance measures are calculated using data from the 50 m, 200 m and 300 m arcs.

In most cases, the similarity model shows the most accuracy and the Gaussian model shows the least accuracy. Also, the use of observed cross-wind integrated concentrations, C_o^i , leads to better results than the use of observed point maximum concentrations. The deterioration of model performance as distance increases can also be seen. Focusing on Table 6, for cross-wind integrated concentrations, it is seen that the most accurate model, the similarity model, produces a mean relative bias with a magnitude of 0.10 or less on all three distance arcs. The correlation drops from 0.98 to 0.60 as distance increases from 50 to 300 m, and the fraction within a factor of two drops from 1.00 to 0.88 over the same distance. The normalized mean-square-error increases from 0.02 to 0.26 over those distances, implying that the root-mean-square-error (rmse) increases from about 15% to 50% of the mean. In contrast, the Gaussian model yields a

much larger rmse that increases from about 70% to 300% of the mean.

The factor of 5 or 6 difference in rmse between the similarity and Gaussian models implies that the similarity model can discern differences in source emission rates that are a factor of 5 or 6 less than the minimum differences in source emission rates discerned by the Gaussian model. By comparing these numbers between Tables 5 and 6, it is seen that the relative rmses using C_0 observations are about 50% to 100% larger than the relative rmses using C_0^2 observations. Consequently the use of C_0^2 data permits one to discern differences in source emission rate that are 50% to 100% smaller than the minimum differences in source emission rates discerned by C_0 data.

IMPLICATIONS FOR FUTURE RESEARCH

The uncertainties in estimating source emission rates were first investigated using the Prairie Grass database, since the source conditions were simplified (a single continuous non-buoyant point source near the ground), the source emission rate was closely monitored, the site was flat and uniform, comprehensive meteorological data were taken, and observations of ground-level concentrations were taken at many points along monitoring arcs at five downwind distances. This experiment represents the optimum database of its type, and has been used in numerous research programs on atmospheric turbulence and dispersion. For this reason, the uncertainties in any analysis procedure should be *minimized* at this site. Conversely, if these procedures were to be applied to other experiments at other sites, where conditions are not so steady, smooth, or carefully-observed, the uncertainties would be expected to be larger.

In the future, we will test these procedures using less ideal observations from other field experiments. These will include U.S. Army field tests of fog oil generators, which are used for smoke obscuration purposes. The plumes from fog oil generators are more complicated than those in the Prairie Grass experiments, since the fog oil plumes are characterized by significant momentum and buoyancy fluxes. Furthermore, the supporting meteorological data are not as complete as at Prairie Grass. Future tests will also include experimental data obtained for plumes from tall power plant stacks, where plume rise and mixing depth are complicating factors. From each set of experiments, the relative uncertainty of the procedures for estimating source emission rate will be assessed. It is expected that the uncertainty will increase as source conditions become more complex or as input data are less complete.

This study has demonstrated that models that do well (in a least squares sense) in estimating point concentrations do not necessarily do well when they are 'turned around' to estimate source emission rate. The reason for this difference is the strong variation

with distance of the plume centerline concentration. Consequently it is possible that a model which has zero mean bias in its concentration estimates, will have a 50% mean bias in its source emission rate estimates. For the same reason, if a variable is first made non-dimensional and the model is 'tuned' with the data (e.g. the similarity model described above), the predictions of the non-dimensional variable (e.g. Cu_0x^2/Q) may have zero bias, while the predictions of the concentration, C , may have significant bias. For optimum results, any tuning or regression analysis should be done with the variable that is of ultimate interest.

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REFERENCES

- Barad M. L. (ed.) (1958) Project Prairie Grass. A field program in diffusion. *Geophys. Res. Paper No. 59*, Vols. I and II, AF-CRF-TR-58-235, Air Force Cambridge Research Center, Bedford, MA.
- Briggs G. A. (1973) Diffusion estimation for small emissions. ATDL Cont. File No. 79, ATDL, Oak Ridge, TN.
- Briggs G. A. (1982) Similarity forms for ground source surface layer diffusion. *Boundary-Layer Met.* 23, 489-502.
- Draxler R. R. (1984) Diffusion and transport experiments. Chapter 9 In *Atmospheric Science and Power Production*, Chapter 9 (edited by D. Randerson), pp. 367-422. DOE/TIC-27601, USDOE.
- Gifford F. A. (1961) Use of routine meteorological observations for estimating atmospheric dispersion. *Nucl. Saf.* 2, 47-57.
- Gifford F. A. (1968) An outline of theories of diffusion in the lower layers of the atmosphere. In *Meteorology and Atomic Energy—1968* (edited by D. H. Slade), pp. 66-116. USAEC Report TID-24190, NTIS, 66-116.
- Gifford F. A. (1976) Turbulent diffusion typing schemes. A review. *Nucl. Saf.* 17, 68-86.
- Golder D. (1972) Relations among stability parameters in the surface layer. *Boundary-Layer Met.* 3, 47-58.
- Horst T. W. (1979) Lagrangian similarity modeling of vertical diffusion from a ground-level source. *J. appl. Met.* 18, 733-740.
- Nieuwstadt F. T. M. (1980) Application of mixed-layer similarity to the observed dispersion from a ground-level source. *J. appl. Met.* 19, 157-162.
- Nou J. V. (1963) The Ocean Breeze and Dry Guich diffusion programs. AF-CRL, Hanscom AFB, MA.
- Pasquill F. (1961) The estimation of dispersion of windborne material. *Met. Mag.* 90, 33-49.
- Turner D. B. (1967) Workbook of atmospheric dispersion estimates. Public Health Service, Pub. No. 999-AP-26, Robert A. Taft Sanitary Engineering Center, Cincinnati, OH.
- van Ulden A. P. (1973) Simple estimates for vertical diffusion from sources near the ground. *Atmospheric Environment* 12, 2125-2129.
- Venkatram A. (1981) A semi-empirical method to compute concentrations associated with surface releases in the stable boundary layer. *Atmospheric Environment* 15.
- Watson J. G. (ed.) (1989) Receptor models in air resources management. *Transactions of an International Specialty Conference*. Air and Waste Management Association, Pittsburgh, PA.

APPENDIX D

DISPLAY OF RELATIONS AMONG DATA USING BOX PLOTS

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DISPLAY OF RELATIONS AMONG DATA USING BOX PLOTS

One way of displaying large numbers of data is through the use of box plots, where the cumulative distribution function (cdf) of the dependent variables within a group of data is represented by a set of significant percentile values. For example, the 2th, 16th, 50th, 84th, and 98th percentiles are used in our analyses. These five significant points in the cdf are plotted by the SIGPLOT program using a "box" pattern as seen in the examples below. Variations of one type of data with another can be seen by breaking up the first type of data into groups defined by ranges of the second type of data.

The SIGPLOT plotting package (see Appendix E) is used to generate the box plots. The ANADISTR program, described below, is used to generate the special input file required by SIGPLOT from a file containing multiple columns of data, representing concurrent values of variables such as observations of concentrations, wind speed, or stability. In the ANADISTR program, the user defines certain ranges of the primary variables in the input file to be used for grouping the dependent variables and plotting them by means of box plots. The ANADISTR program requires one input file and generates one output file. The output file then serves as the input file to the SIGPLOT plotting package. There are no default names associated with these files, and the user is prompted for the file names during the execution of the program. The ANADISTR program is written in FORTRAN 77.

The input data file of the ANADISTR program could contain multiple columns of dependent variables (such as concurrent values of concentration observation) and other primary variables such as wind speed and stability. The ranges of the primary variables are also defined in the input file, to be used for grouping the data prior to generating the box plots. Table D-1 describes the format of the input file. Figure D-1 shows an example of an input file. Note that the ANADISTR program makes no corrections or substitutions for missing data; it is the responsibility of the user to provide valid data at each position.

The output file of the ANADISTR program contains distributions (the 2th, 16th, 50th, 84th, and 98th percentiles of the cdf) of the first variable as a function of the second variable. The information stored in this output file can then be plotted using the SIGPLOT plotting package (see Figure D-2 for an example).

During the execution of the ANADISTR program, the following questions will be asked:

- Name of the input file:

The user must specify the name of the input data file here. There is no default answer.

- Name of the output file:

The user must specify the name of the output file. There is no default answer.

- An input file typically contains several columns of dependent and independent data. The ANADISTR program handles one such column or the ratio of any two columns of dependent data, specified by the user, at a time. This is accomplished by asking the user to select any two columns between 0 and MM, (see Table D-2). The distribution of the ratio of the numbers in these columns will be analyzed. Note that column "0" is simply all 1's, and is not part of the input data file. Therefore, if the user wants to investigate the distribution of the dependent data in column 2, then two integers, 2 and 0 should be entered. If the user wants to investigate the distribution of the ratio of the dependent data in column 2 to the data in column 1, then 2 and 1 should be entered.

- Implement a lower threshold for the dependent variable? (y/n):

The user has the option of specifying a lower threshold for the one dependent variable or the ratio of the two dependent variables chosen above. This is sometimes necessary if the logarithmic scale is to be used and there are zero or minute values in the data whose distribution is to be analyzed. The default (i.e., hitting the RETURN key) answer is "y".

TABLE D-1. FORMAT OF THE MANDATORY INPUT DATA FILE OF THE ANADISTR PROGRAM.
 THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE
 FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL.

LINE NO.	FORMAT	DESCRIPTION
1	FF/I	There are four integer constants in this line, representing the total number of observations (NN, < 501), the total number of dependent variable (MM, < 16), the total number of blocks (KK), and the total number of primary variables (NVAR, < 11). Note that KK is not used by ANADISTR since the blocking of data is performed internally according to the defined ranges of the primary variables. The limits on NN, MM, and NVAR are assigned in the program using the PARAMETER statements, and can be easily changed.
2	FF/I	There are KK integer constants in this line, representing the number of pieces in each block. The sum of all these integers should equal NN. Note that the information in this line is currently not used by the ANADISTR program.
3	FF/I	There are MM character constants in this line; each one can be at most eight characters long, containing the name of each of the dependent variables. All character constants must be enclosed in apostrophes.
4	FF/I	There should be KK character constants in this line. Each one can be at most 20 characters long, containing the name of each of the blocks. All character constants must be enclosed in apostrophes. Note that the information in this line is not used by the ANADISTR program.

LINE NO. FORMAT

DESCRIPTION

Next NN lines:

FF/R

There are MM+NVAR real numbers in each line, with the first MM numbers representing the dependent variables, and the following NVAR numbers representing of the primary variables.

Next NVAR lines:

FF/

I,C,R

Each line describes the way each of the NVAR primary variables is to be blocked. The first parameter is an integer (IXR, < 21), representing the number of ranges for the primary variable. The second parameter is a character constant, at most 40 characters long, enclosed in apostrophes, representing the name of the primary variable. The next IXR+1 real numbers, in numerical ascending order, define the boundaries of the ranges. For example, the following line:

4 'u (m/s)' 0. 2. 5. 10. 20.

means that wind speeds should be divided into four groups where the distribution of the dependent variables within each group is to be calculated. The first group is for those data when wind speeds are between 0. and 2. m/s, the second group is for wind speeds between 2. and 5. m/s, etc.

The limits on IXR are assigned in the program using the PARAMETER statement, and can be easily changed. Note that the sequence of the NVAR lines must be consistent with that of the last NVAR columns described in the previous section. As an example, if the MM+1th column in the previous section contains information for wind speeds, then the first line in this section should also contain grouping information for wind speeds.

```

79 4 2 4
39 40
'DEPVAR-A' 'DEPVAR-B' 'DEPVAR-C' 'DEPVAR-D'
'SUBSET1' 'SUBSET2'
616.0 708.7 594.7 516.5 11 3.0 800. 2
604.1 689.2 585.8 496.7 12 3.4 1000. 2
868.0 674.8 580.3 516.8 13 3.5 1100. 2
498.6 668.8 652.1 548.3 14 3.8 1200. 2
393.1 560.2 704.7 581.9 15 4.7 1300. 2
409.0 740.9 570.1 621.4 16 5.2 1000. 3
640.2 249.6 510.1 553.5 17 5.4 1100. 3
265.3 259.6 463.4 446.0 18 4.9 1100. 4
192.7 91.6 131.0 485.0 19 4.2 1100. 5
1149.1 1217.5 1116.1 520.6 10 2.6 1600. 2
972.8 1275.8 1175.1 536.9 11 3.2 1900. 2
1137.5 1225.7 1081.7 617.4 12 3.8 1600. 2
669.5 1052.8 905.1 637.3 13 4.5 1600. 2
595.5 862.0 862.0 664.1 14 5.0 1500. 2
741.2 589.5 767.0 665.3 15 5.1 1500. 2
612.6 602.4 728.2 672.4 16 5.0 1500. 3
312.0 398.9 637.5 659.5 17 5.2 1500. 3
400.2 340.2 412.3 586.0 18 5.1 1500. 4
264.7 612.1 774.2 705.9 16 5.7 1400. 3
290.0 428.4 757.3 708.8 17 5.1 1800. 3
459.5 355.0 512.3 602.4 18 5.1 2000. 4
444.0 216.0 441.4 681.1 19 4.4 2000. 5
175.1 216.6 456.1 825.4 20 4.6 2000. 6
102.3 126.1 255.6 522.9 21 4.9 2000. 6
128.8 16.5 0.5 834.9 22 4.6 0. 6
200.2 301.9 208.9 728.0 23 5.4 0. 6
358.3 481.8 354.0 742.4 24 5.4 0. 6
611.1 1010.2 987.1 679.0 14 4.4 1500. 2
499.3 752.5 921.6 725.7 15 5.0 1500. 2
537.8 724.0 826.8 675.9 16 4.7 1500. 3
220.0 523.3 908.2 640.8 17 3.9 1800. 3
479.2 357.5 788.6 544.7 18 4.2 2000. 4
133.2 195.3 383.1 738.5 19 3.1 1800. 5
98.2 167.3 213.5 1064.9 20 3.2 1500. 6
92.5 104.6 142.2 741.2 21 3.1 1200. 6
21.0 127.4 176.3 805.2 22 3.3 1200. 6
353.0 307.8 167.1 576.9 20 3.8 2000. 5
358.0 280.9 188.4 225.3 21 2.3 2000. 4
233.3 355.3 234.9 719.1 22 2.4 2000. 5
198.3 12.7 184.0 745.2 23 3.6 2000. 6
507.2 0.0 126.3 564.9 24 3.5 2000. 6
313.7 0.0 0.0 667.1 1 4.2 0. 6
165.1 0.0 0.0 703.9 2 3.6 0. 6
295.6 329.9 454.6 695.3 4 5.2 0. 6
527.7 308.0 295.9 775.0 5 4.7 0. 6
454.1 301.0 1.0 995.6 6 2.9 0. 6
240.3 417.5 361.1 933.8 7 3.4 0. 6
590.8 579.3 144.2 666.5 8 3.1 1500. 5
638.3 756.6 608.9 400.1 9 3.4 1500. 4
949.8 1004.2 805.4 528.9 10 3.4 1500. 3
886.8 855.6 706.2 517.4 11 3.0 1300. 2
635.5 761.0 670.9 596.6 12 4.5 1200. 2
359.3 412.6 232.5 937.6 1 2.3 1200. 6
484.7 360.7 226.8 979.0 2 2.5 1200. 6
529.7 332.0 202.5 980.0 3 2.4 1200. 6
585.8 291.4 186.1 1100.1 4 2.1 1200. 6
367.7 368.0 260.2 1005.6 5 2.1 1200. 6
324.7 270.9 72.7 1058.6 6 2.0 1200. 6
489.0 274.6 208.5 942.2 7 2.6 1200. 6
570.8 337.1 218.0 646.5 8 2.8 1200. 5
419.7 254.4 206.1 344.0 9 4.3 1200. 4
532.8 414.2 197.9 477.0 9 4.8 1800. 3
425.2 365.7 198.7 469.5 10 7.1 1700. 4
467.5 411.5 228.5 455.3 11 7.5 2000. 4
362.2 306.4 147.6 405.2 12 5.1 2000. 4
429.2 287.4 139.2 450.6 13 5.4 2000. 4
446.0 338.1 169.5 461.2 14 5.7 2000. 4
192.9 253.8 145.6 460.7 15 5.8 2400. 4
630.3 322.5 257.2 460.5 16 7.3 2700. 4
364.9 326.7 251.1 510.6 17 7.8 3000. 4
111.4 196.4 248.5 0.0 23 1.9 250. 4
89.8 146.5 254.9 0.0 24 1.9 250. 4
82.5 248.0 160.9 0.0 1 2.9 250. 4
296.5 253.2 193.2 0.0 2 2.8 250. 4
215.4 299.7 165.0 0.0 3 2.9 250. 4
454.5 274.2 154.0 0.0 4 3.5 250. 4
384.7 324.6 163.2 0.0 5 3.5 250. 4
253.2 488.3 175.6 0.0 6 3.5 250. 4
289.5 304.1 193.1 0.0 7 3.1 250. 4
6 'hour of day' -0.01, 4., 8., 12., 16., 20., 24.01
10 'u (m/s)' 0.5, 1.5, 2.5, 3.5, 4.5, 5.5, 6.5, 7.5, 8.5, 9.5, 10.5
6 'h (m)' -0.01, 200., 600., 1000., 1500., 2000., 3000.1
3 'pg class' 0.5 1.5 4.5 6.5

```

Figure D-1. An example of the input data file for the ANADISTR program.

DEMONSTRATION OF THE RESULTS GENERATED BY THE ANADISTR PROGRAM.

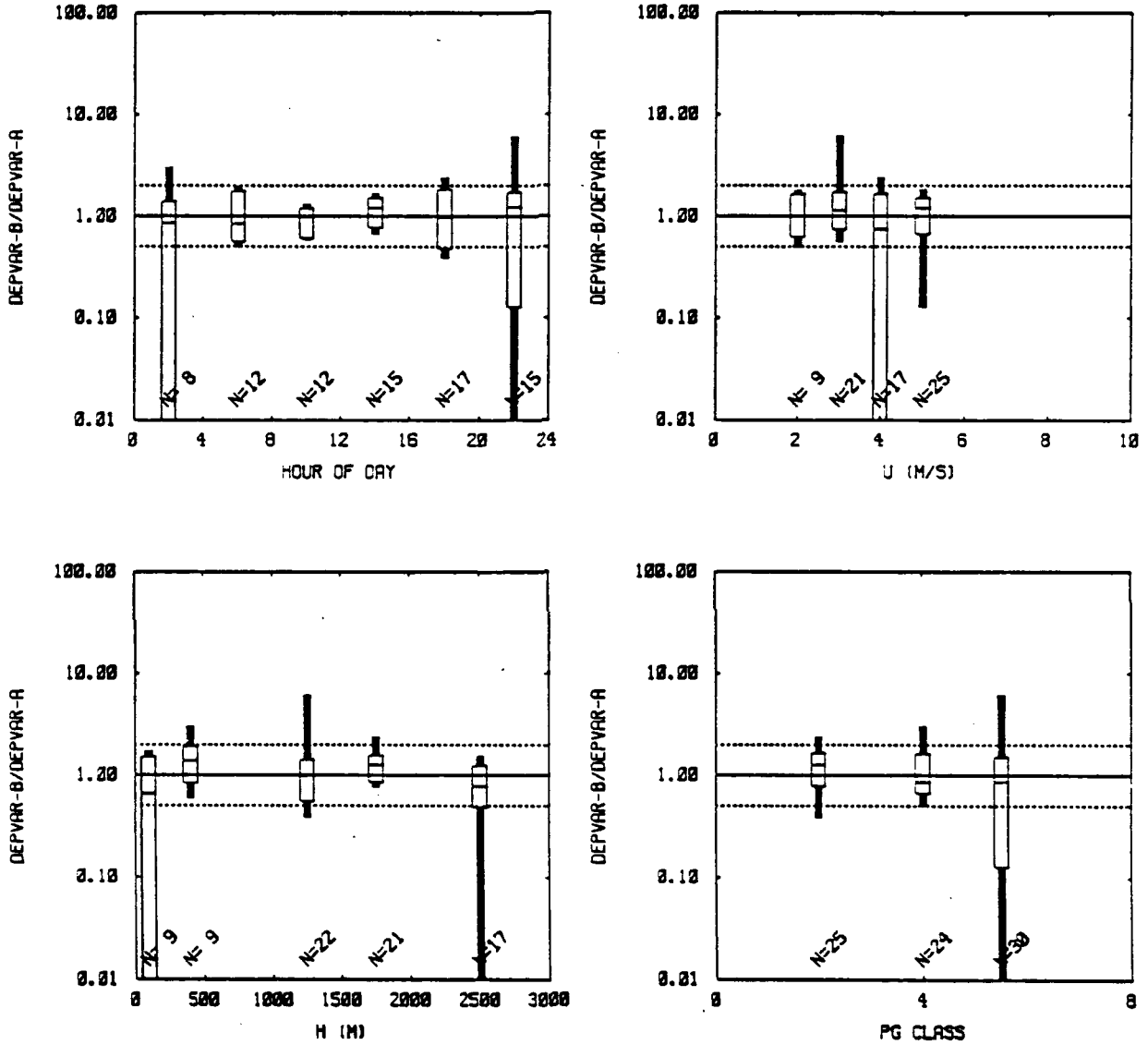


Figure D-2. An example of the results generated by the ANADISTR program and plotted using SIGPLOT. Significant points on each box represent the 2nd, 16th, 50th, 84th, and 98th percentiles. The dashed lines represent the factor of two lines.

The next question will be asked only if the user answers "y" to the above question.

- Enter the lower threshold (e.g. 0.01):

There is no default answer, but 0.01 has proven to be a good choice for the ratio of two dependent variables in our tests.

- Implement an upper threshold for the dependent variable? (y/n):

This is sometimes necessary if the logarithmic scale is to be used and there are very large values in the data whose distribution is to be analyzed. The default (i.e., hitting the RETURN key) answer is "y".

The following question will be asked only if the user answers "y" to the above question.

- Enter the upper threshold of the ratio (e.g. 100.):

There is no default answer, but 100 has proven to be a good choice for the ratio of two dependent variables in our tests.

Intentionally Blank

APPENDIX E

USER'S GUIDE FOR THE SIGPLOT PLOTTING PACKAGE

APPENDIX E

A. USER'S GUIDE FOR THE SIGPLOT PLOTTING PACKAGE

The SIGPLOT plotting package developed at Sigma Research Corporation is a versatile tool for producing different kinds of two-dimensional plots, such as scatter plots, graphs, box plots (sometimes called residual or whisker plots), or error bar plots. The user can specify many parameters including the number of frames per page, the aspect ratio of the frame, and the mapping of the coordinates. The graphics library routines used by SIGPLOT, together with the screen and printer drivers (described later) were originally developed by Dr. Arlindo daSilva of the University of Wisconsin at Milwaukee.

SIGPLOT requires two input files: 1) the template file that contains the control parameters which influence the appearance of the plots, and 2) the input data file that contains the data to be plotted. Tables E-1 and E-2 describe the formats of the template file and the input data file, respectively. Examples of the template file are shown in Figures E-1 and E-2. Examples of the input data file are shown in Figures E-3 and E-4.

SIGPLOT creates a Tektronix picture file that can be viewed directly on any kind of the PC graphics environments (e.g., Hercules, CGA, EGA, and VGA) using the screen driver, TEKPC. Hard copy output can also be generated from the Tektronix picture file with a printer driver. There are three printer drives, TEKEPS, TEKELQ, and PS, that are currently available. The first two drivers are used to drive an EPSON-compatible dot matrix printer, with TEKEPS for low resolution and TEKELQ for high resolution. The PS program is used to drive a PostScript printer, such as Apple LaserWriter, NEC LC-890, or TI MicroLaser PS35. It is recommended that the user have access to a PostScript printer to obtain the best results in the shortest time.

SIGPLOT requires about 200KB of memory. The other screen and printer drivers require less than 100KB of memory, except for TEKELQ, where 450KB of memory is required due to the high resolution and the use of the bitmap approach in the driver program. The SIGPLOT plotting package and the graphics library routines were written in FORTRAN. The screen and printer drivers were written in C.

TABLE E-1. THE FORMAT OF THE TEMPLATE FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL.

The global control parameters are specified in the first section of the template file, lines 1 through 16.

LINE NO.	FORMAT	DESCRIPTION
1-3		Reserved for comments
4	FF/C	Name of the input data file, currently not used
5	FF/C	Name of the output Tektronix picture file, currently not used
6	FF/I	Flag for the frame aspect ratio, 1-5, 1: x:y = 1:1 2: x:y = 1:2 3: x:y = 2:1 4: x:y = 1:3 5: x:y = 3:1
7	FF/I	Number of frames per page, 1-4
8-9	A80	Title for the page (no title will be drawn if "0" appears as the first character of the line)
10	FF/C	Flag (PAXIS) for the axis along which the first column, representing the independent variable, of the data in the input data file (see Table E-2) will be plotted (x or y). PAXIS must = x if IPATTN (described below) = 4, and PAXIS must = y if IPATTN = 6
11	FF/I	Flag for mapping, 1-4, 1: linear in x, linear in y 2: linear in x, logarithmic in y 3: logarithmic in x, linear in y 4: logarithmic in x, logarithmic in y

TABLE E-1. THE FORMAT OF THE TEMPLATE FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL. Continued.

LINE NO.	FORMAT	DESCRIPTION
12	FF/I	Flag (IPATTN) for plot pattern, 1-6, 1: scatter plot 2: line graph 3: scatter plot except line graph for the last variable 4: box plot 5: error bar plot 6: same as 5 but with extra labelling
13	FF/I	Flag for background, 0 or 2, 0: no background 2: gridded background
14	FF/C	Flag for system time, y or n, if y: system time will be printed out on the upper right corner of each page
15	SA1	Five point patterns for the 'scatter plot
16	FF/I	Flag (IEXTRA) for the plotting of extra lines, 1: $x=0$ will be plotted 2: $y=0$ will be plotted 3: $x=0$ and $y=0$ will be plotted 4: $x=1$ will be plotted 5: $y=1$ will be plotted 6: $x=1$ and $y=1$ will be plotted 7: diagonal line will be plotted 8: $y=0.5$ and $y=2$ (factor of two) will be plotted 9: $x=-0.667$, 0 , and 0.667 , and $y=4x^2/(4-x^2)$. (see text) will be plotted. else: no extra lines will be plotted. Note that IEXTRA = 9 is effective only if IPATTN = 6

TABLE E-1. THE FORMAT OF THE TEMPLATE FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL. Continued.

The next section of the template file (lines 17 through 29) contains the parameters that are applicable to a frame. This section can be repeated if there are multiple frames to be plotted in a print job. However, the user can prepare just one such section if the same information is to be used repeatedly by all frames.

LINE NO.	FORMAT	DESCRIPTION
17-19		Reserved for comments
20	FF/R	Constants, a and b, for the linear transformation of the independent variable, where $x_{\text{new}} = a \cdot x_{\text{old}} + b,$ a=1 and b=0 means no transformation is needed
21	FF/R	Constants, a and b, for the linear transformation of the first dependent variable, where $y_{1,\text{new}} = a \cdot y_{1,\text{old}} + b,$ a=1 and b=0 means no transformation is needed
22	FF/R	Same as above, but for the second dependent variable
23	FF/R	Same as above, but for the third dependent variable
24	FF/R	Same as above, but for the fourth dependent variable

TABLE E-1. THE FORMAT OF THE TEMPLATE FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL. Concluded.

LINE NO.	FORMAT	DESCRIPTION
25	FF/R	Same as above, but for the fifth dependent variable. Note that lines 22 through 25 cannot be omitted even if only one group of data were to be plotted
26	FF/R	xmin, xmax, and dx of the x-axis
27	FF/R	ymin, ymax, and dy of the y-axis
28	FF/C	Format specifier for the numerical labels of the x-axis. If "!" appears as the first character of the line, the appropriate format will be determined internally by the program; otherwise, the user should supply a simple FORTRAN I-, F-, or E-format specifier, enclosed in parentheses, e.g., (I5), (F6.3), and (E8.1) are accepted, but (3I5), (I5,f6.3), (1P,E8.1), and (G9.1) are not accepted
29	FF/C	Format specifier for the numerical labels of the y-axis

TABLE E-2. THE FORMAT OF THE INPUT DATA FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL.

LINE NO.	FORMAT	DESCRIPTION
1	A40	Title for the frame (no title will be drawn if "0" appears as the first character of the line)
2	A40	Label for the x-axis (no label will be drawn if "0" appears as the first character of the line)
3	A40	Label for the y-axis (no label will be drawn if "0" appears as the first character of the line)
4	FF/I	Two integers specifying the number of points (NPTS) and the number of groups of data (MANY) to be plotted. MANY cannot be > 5 for IPATTN = 1, 2, 3, and 5, and MANY must be = 1 for IPATTN = 4 and 6. NPTS cannot be > 700 for IPATTN = 1, 2, and 3. NPTS cannot be > 50 for IPATTN = 4, 5, and 6 (see text).

Next NPTS lines:

For IPATTN = 1, 2, and 3,

FF/R There are 1+MANY real numbers in each line. The first number represents the independent variable, which can be plotted either along the x- or the y-axis depending the value of PAXIS (see Table E-1). The next MANY numbers represent the dependent variables. For example, if three curves (MANY=3), $f_1(x)$, $f_2(x)$, and $f_3(x)$ were to be plotted, then each line here should contain four real numbers, x_i , $f_{1,i}$, $f_{2,i}$, and $f_{3,i}$, where $i=1, \dots, \text{NPTS}$. If PAXIS = "x", the x will be plotted along the abscissa, and f_1 , f_2 , and f_3 will be plotted along the ordinate; vice versa PAXIS = "y".

TABLE E-2. THE FORMAT OF THE INPUT DATA FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL. Continued.

LINE NO.	FORMAT	DESCRIPTION
		For IPATTN = 4,
	FF/R,I	There are six real numbers and one integer in each line. The first real number represents the independent variable. The next five real numbers represent the values of the dependent variable at the 2th, 16th, 50th, 84th, and 98th percentiles, respectively. Note that the value of the independent variable listed here frequently represents a range of the independent variable; for example, a wind speed of 7 m/s actually represents wind speeds in the range of 6 to 8 m/s. The integer represents the number of data points based on which the distribution of the dependent variable is derived. No box will be plotted if the number of data points is less than five since not enough information is available to define a distribution.
		For IPATTN = 5,
	FF/R	There are 1+3*MANY real numbers in each line. The first number represents the independent variable. The remaining numbers for the dependent variables are in MANY groups of three numbers. The three numbers, which must be in order, represent the distribution of a dependent variable. This distribution can be 1) $\mu - \sigma$, μ , and $\mu + \sigma$, where μ is the mean, and σ is the standard deviation, or 2) lower c.l., nominal value, and upper c.l., where c.l. is the confidence limit.

TABLE E-2. THE FORMAT OF THE INPUT DATA FILE OF SIGPLOT. THE FOLLOWING KEY LETTERS ARE USED IN THE FORMAT COLUMN - FF: FREE FORMAT, C: CHARACTER, I: INTEGER, AND R: REAL. Concluded

LINE NO.	FORMAT	DESCRIPTION
----------	--------	-------------

For IPATTN = 6,

FF/R,C	There are four real numbers and one character constant (no more than 17 characters long) in each line. The definition of the first four real numbers is identical to that when IPATTN = 5, except now MANY must = 1. The character constant, enclosed in apostrophes, is used to label each data point.
--------	---

The above 4+NPTS lines provide enough information to plot a frame. Additional data, similar in structure, can be appended here if the plotting of more than one frames in a print job is desired.


```

-----
!
!      Main switches for plotting.
-----
!-----0-----0-----0-----0-----
urrs.1  Name of input data file.
tekl.pic Name of output tektronix file.
1      Aspect ratio (integer, 1 - 5).
1      Number of plots per page (integer, 1 - 4).
demo of ipattn=5
0
x      Which axis serves as independent variable (x or y).
3      Flag indicating log or linear mapping (1 - 4).
5      Pattern.
0      Background specification. (0 or 2)
n      Print out system time on the upper right hand corner (y or n).
+o.##  Patterns of scatter plots (5al)
0      Extra line,1:x=0,2:y=0,3:x,y=0,4:x=1,5:y=1,6:x,y=1,7:diag,8:y=fac. 2.,9:fb-nmse, else:nothing.
-----
!      Parameters for plot 1.
-----
1. 0.  ascale, bscale for the independent variable axis.
1. 0.  ascale, bscale for curve 1.
1. 0.  ascale, bscale for curve 2.
1. 0.  ascale, bscale for curve 3.
1. 0.  ascale, bscale for curve 4.
1. 0.  ascale, bscale for curve 5.
200. 20000. 10. xmin, xmax, and dx for the x axis.
-1.5 1.5 0.5 ymin, ymax, and dy for the y axis.
(15)
(f4.1)

```

Figure E-2. An example of the template file of SIGPLOT. Refer to Figure E-9 for the results.

0
x
y

	50	5				
-6.03186	0.248690	-0.368124	-0.844328	-0.998027	-0.770514	
-5.78053	0.481754	-0.125333	-0.684547	-0.982287	-0.904827	
-5.52920	0.684547	0.125333	-0.481753	-0.904827	-0.982287	
-5.27788	0.844328	0.368125	-0.248690	-0.770513	-0.998027	
-5.02655	0.951057	0.587786	0.397359E-06	-0.587785	-0.951056	
-4.77522	0.998027	0.770513	0.248690	-0.368125	-0.844328	
-4.52389	0.982287	0.904827	0.481754	-0.125333	-0.684547	
-4.27257	0.904827	0.982287	0.684547	0.125333	-0.481753	
-4.02124	0.770513	0.998027	0.844328	0.368125	-0.248690	
-3.76991	0.587785	0.951056	0.951057	0.587785	0.254308E-06	
-3.51858	0.368125	0.844328	0.998027	0.770513	0.248690	
-3.26726	0.125333	0.684547	0.982287	0.904827	0.481754	
-3.01593	-0.125333	0.481753	0.904827	0.982287	0.684547	
-2.76460	-0.368125	0.248690	0.770513	0.998027	0.844328	
-2.51327	-0.587785	0.397391E-07	0.587785	0.951056	0.951057	
-2.26195	-0.770513	-0.248690	0.368124	0.844328	0.998027	
-2.01062	-0.904827	-0.481754	0.125333	0.684547	0.982287	
-1.75929	-0.982287	-0.684547	-0.125334	0.481753	0.904827	
-1.50796	-0.998027	-0.844328	-0.368124	0.248690	0.770513	
-1.25664	-0.951057	-0.951057	-0.587785	-0.556284E-07	0.587785	
-1.00531	-0.844328	-0.998027	-0.770513	-0.248690	0.368124	
-0.753983	-0.684547	-0.982287	-0.904827	-0.481753	0.125333	
-0.502655	-0.481754	-0.904827	-0.982287	-0.684547	-0.125333	
-0.251328	-0.248690	-0.770513	-0.998027	-0.844328	-0.368125	
0.000000	0.000000	-0.587785	-0.951056	-0.951057	-0.587785	
0.251328	0.248690	-0.368124	-0.844328	-0.998027	-0.770513	
0.502655	0.481753	-0.125333	-0.684547	-0.982287	-0.904827	
0.753982	0.684547	0.125333	-0.481754	-0.904827	-0.982287	
1.00531	0.844328	0.368125	-0.248690	-0.770513	-0.998027	
1.25664	0.951056	0.587785	-0.381470E-06	-0.587786	-0.951057	
1.50796	0.998027	0.770513	0.248690	-0.368125	-0.844328	
1.75929	0.982287	0.904827	0.481754	-0.125333	-0.684547	
2.01062	0.904827	0.982287	0.684547	0.125333	-0.481754	
2.26195	0.770513	0.998027	0.844328	0.368125	-0.248690	
2.51327	0.587785	0.951056	0.951057	0.587785	0.190735E-06	
2.76460	0.368124	0.844328	0.998027	0.770513	0.248690	
3.01593	0.125334	0.684548	0.982287	0.904827	0.481753	
3.26726	-0.125333	0.481754	0.904827	0.982287	0.684547	
3.51858	-0.368124	0.248690	0.770514	0.998027	0.844328	
3.76991	-0.587785	0.341731E-06	0.587785	0.951057	0.951056	
4.02124	-0.770513	-0.248690	0.368125	0.844328	0.998027	
4.27257	-0.904827	-0.481754	0.125333	0.684547	0.982287	
4.52389	-0.982287	-0.684547	-0.125333	0.481754	0.904827	
4.77522	-0.998027	-0.844327	-0.368124	0.248691	0.770514	
5.02655	-0.951057	-0.951056	-0.587785	0.723200E-06	0.587786	
5.27787	-0.844328	-0.998027	-0.770513	-0.248689	0.368125	
5.52920	-0.684548	-0.982287	-0.904827	-0.481753	0.125334	
5.78053	-0.481754	-0.904827	-0.982287	-0.684547	-0.125333	
6.03186	-0.248690	-0.770513	-0.998027	-0.844328	-0.368124	
6.28319	-0.301992E-06	-0.587785	-0.951057	-0.951056	-0.587785	

Figure E-3. An example of the input data file of SIGPLOT. Refer to Figure E-6 for the results.

```

all periods
n-s distance (m)
var(dws) / median l-min var(ws) / 2
6 3
312.5 -0.029 0.002 0.034 -0.027 0.043 0.112 0.166 0.275 0.383
625.0 -0.009 0.005 0.019 0.011 0.048 0.085 0.209 0.361 0.513
1250.0 -0.035 0.012 0.059 -0.007 0.070 0.148 0.330 0.480 0.630
2500.0 -0.155 0.015 0.185 -0.126 0.100 0.325 0.359 0.565 0.771
5000.0 -0.033 0.170 0.373 0.013 0.323 0.633 0.440 0.751 1.062
10000.0 -0.417 0.061 0.539 -0.137 0.369 0.876 0.406 0.873 1.339

```

Figure E-4. An example of the input data file of SIGPLOT. Refer to Figure E-9 for the results.

As one can see from Table E-1, SIGPLOT is capable of creating the following kinds of plots:

- IPATTN = 1: scatter plot (e.g., Fig. E-5)
- IPATTN = 2: line graph (e.g., Fig. E-6)
- IPATTN = 3: scatter plot except line graph for the last variable (e.g., Fig. E-7)
- IPATTN = 4: box plot (e.g., Fig. E-8)
- IPATTN = 5: error bar plot (e.g., Fig. E-9)
- IPATTN = 6: same as IPATTN = 5 but with extra labelling (e.g., Fig. E-10)

The usage of each option is described below.

For IPATTN = 1, groups of data are represented by different dot patterns that are defined in the template file (see Table E-1). At most, five groups of data (MANY = 5) can be plotted, with a maximum of 700 points for each group.

IPATTN = 2 is similar to IPATTN = 1 except that points are now connected. The following line patterns are used to represent different curves: solid, short-dashed, long-dashed, dot-dashed, and dotted. At most, five curves (MANY = 5) can be plotted, with a maximum of 700 points for each group. No user customization of the line patterns is allowed. It is important that the data points in the input file are sorted according to the independent variable.

IPATTN = 3, a combination of IPATTN = 1 and 2, is useful when the user wants to see how well a theoretical curve fits the observed data. Although the order of the data points does not matter for a scatter plot, in this case it is important that the data points in the input file are sorted according to the independent variable. At most, five groups of data (MANY = 5) can be plotted, with a maximum of 700 points for each group.

The IPATTN = 4 option is an alternative to the scatter plot when the number of data points is large. In preparing the input data file for SIGPLOT,

the user first defines certain ranges of the independent variable to be used for grouping the dependent variable. The distribution of the dependent variables within each group is then determined and represented by five significant points in the cumulative distribution function (cdf). These five values could be the 2th, 16th, 50th, 84th, and 98th percentiles of the cdf, or the mean and mean \pm one and two standard deviations. SIGPLOT then uses a box pattern to represent the distribution of the dependent variable within each grouping or range of the independent variable. Only one set of data (i.e., MANY = 1, even though five points are needed to define a box) is accepted for this option, with a maximum of 50 boxes.

IPATTN = 5 is similar to IPATTN = 4 except that three values (vs. five) are needed to define an error bar (vs. a box). These three values can be the mean and mean \pm one standard deviation of a dependent variable, or the nominal value of a dependent variable and its 95% confidence limits. At most, five groups (MANY = 5) of data can be plotted, with a maximum of 50 error bars for each group. The following error bar patterns are used: filled square, empty square, filled triangle, empty triangle, and cross.

IPATTN = 6 is similar to IPATTN = 5 except that the user can label each data point. Because of the additional information to be plotted, only one group of data (MANY = 1) is accepted, with a maximum of 50 error bars. This option is designed primarily to plot the FB (fractional bias), together with its confidence limits, against the NMSE (normalized mean square error), where

$$FB = \frac{(\bar{C}_o - \bar{C}_p)}{(0.5(\bar{C}_o + \bar{C}_p))} \quad (E-1)$$

$$NMSE = \frac{(\bar{C}_o - \bar{C}_p)^2}{\bar{C}_o \bar{C}_p} \quad (E-2)$$

If IEXTRA = 9 (see Table E-1), SIGPLOT will plot the additional $x = -0.667$, 0 , and 0.667 lines, representing the factor of two and zero FB lines, together with the $y = 4x^2/(4-x^2)$ line, representing the "minimum" NMSE (due only to the mean bias) as a function of FB.

The information concerning the usage of the driver programs, TEKPC, TEKELQ, TEKEPS, and PS, can be obtained by simply executing the programs without providing any arguments, and will not be repeated here.

Finally, an example is given below of the procedures followed to use the graphics package.

Step 1: The user prepares the template file (DEMO.INQ) and the input data file (DEMO.DAT) according to the formats described in Tables E-1 and E-2. The user can create his own template file by editing the sample template file. The input data file is usually generated by some other programs.

Step 2: After the execution of SIGPLOT, a Tektronix picture file (DEMO.PIC) is generated.

Step 3: The user can view the results on screen by typing:
TEKPC DEMO.PIC
if a Hercules graphics card is installed, or
TEKPC DEMO.PIC 16
if an EGA (with a resolution of 640x350 pixels) graphics card is installed.

Step 4: A high resolution hard copy output can be generated on an EPSON-compatible dot matrix printer by typing:
TEKELQ DEMO.PIC.

Step 5: Or if the user has access to a PostScript printer, a PostScript file (DEMO.PS) will be created by typing:
PS DEMO.PIC,
and this file can be printed out by typing:
PRINT DEMO.PS

DEMO OF IPATTN=1

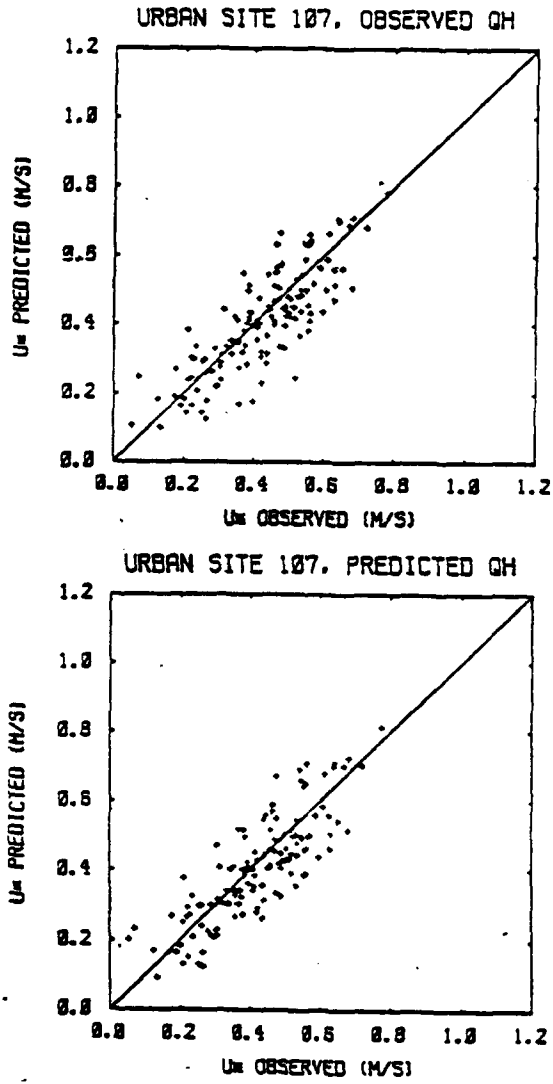


Figure E-5. A sample scatter plot (IPATTN = 1) generated by SIGPLOT.

DEMO OF IPATTN=2

03/25/91

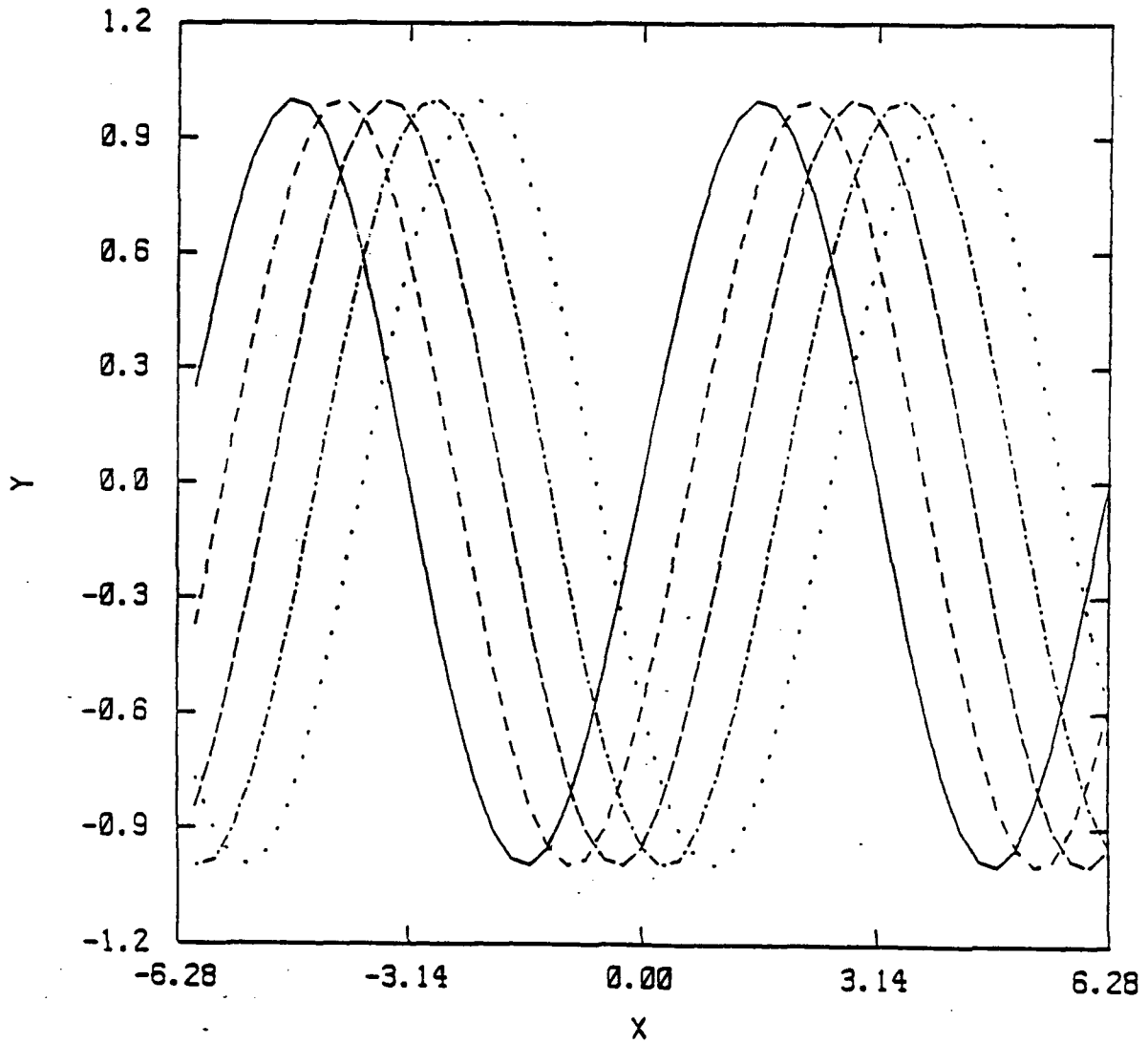


Figure E-6. A sample line graph (IPATTN = 2) generated by SIGPLOT. Refer to Figures E-1 and E-3 for the template and data files used for this figure.

DEMO OF IPATTN=3

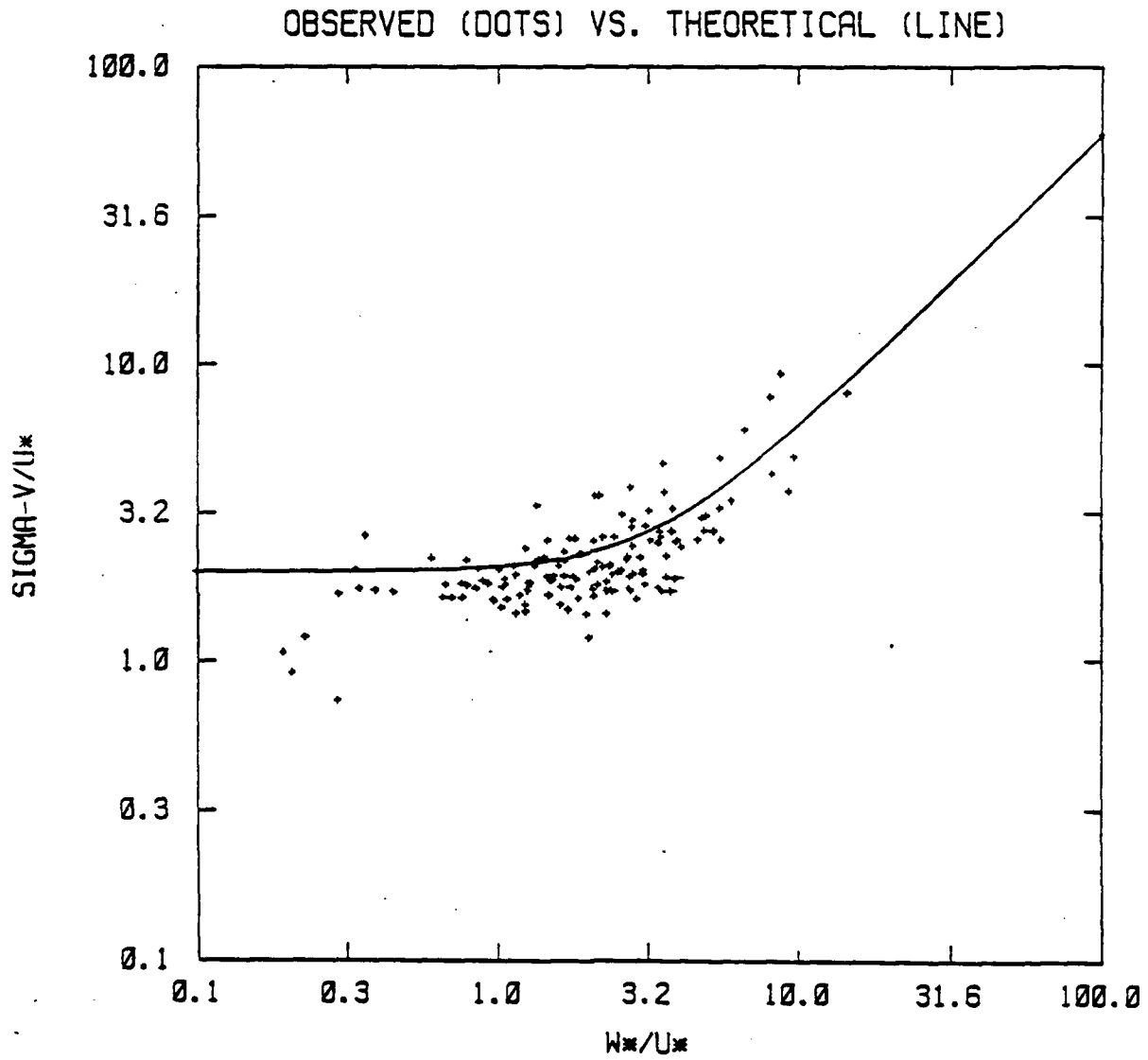


Figure E-7. A sample scatter plot and line graph (IPATTN = 3) generated by SIGPLOT.

DEMO OF IPATTN=4

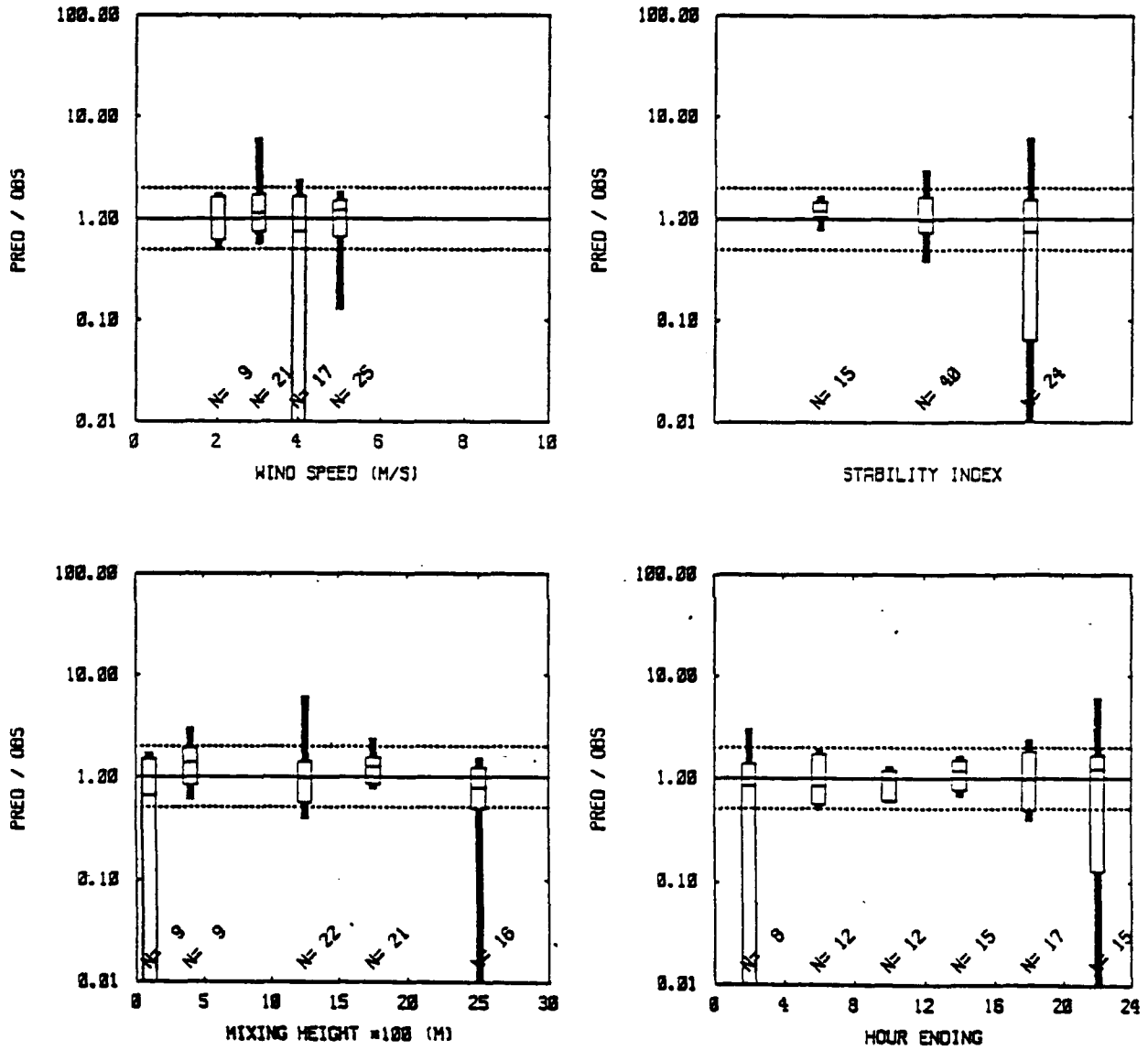


Figure E-8. A sample box plot (IPATTN = 4) generated by SIGPLOT.

DEMO OF IPATTN=5

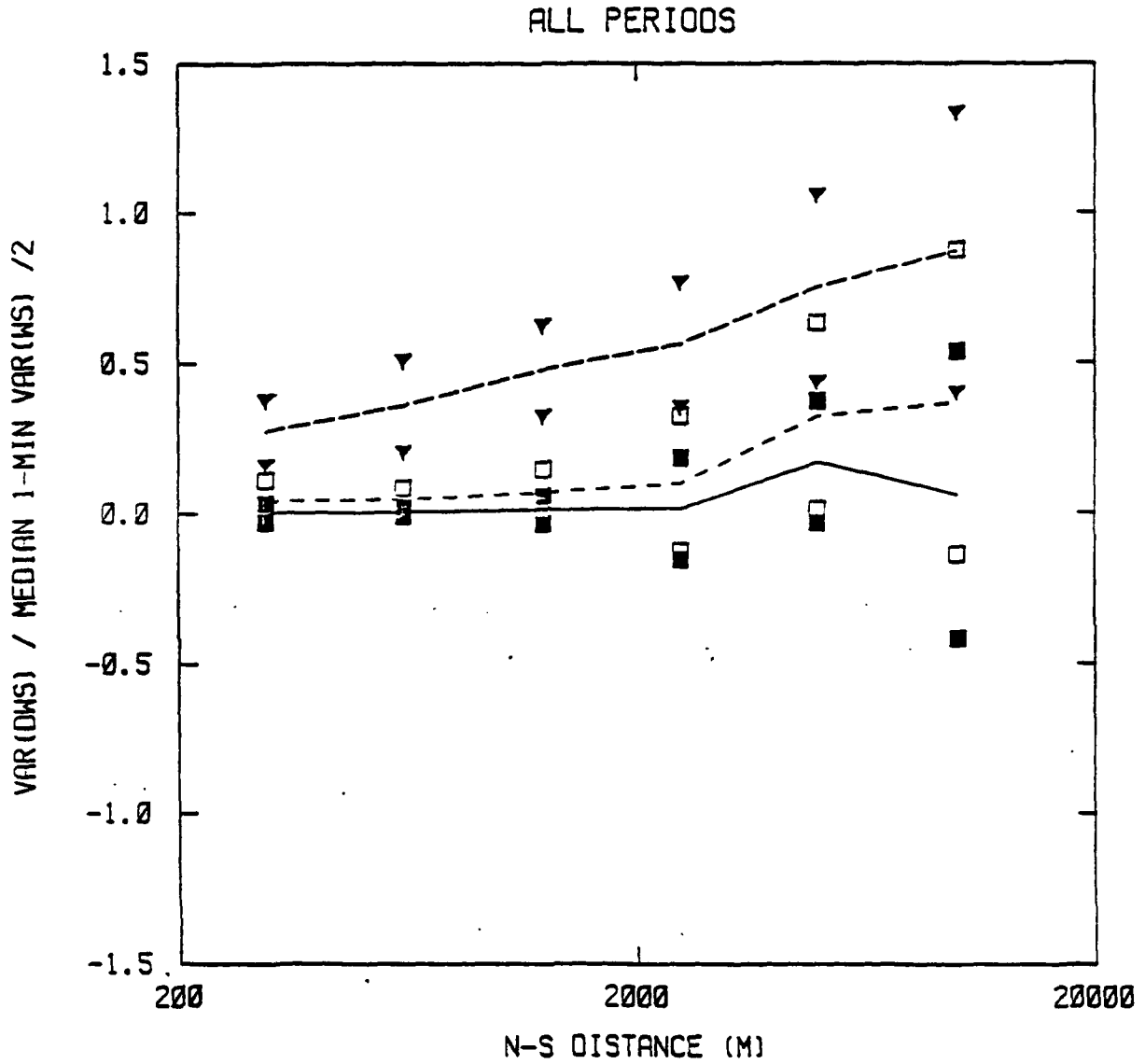


Figure E-9. A sample error bar plot (IPATTN = 5) generated by SIGPLOT. Refer to Figures E-2 and E-4 for the template and data files used for this figure.

DEMO OF IPATTN=6

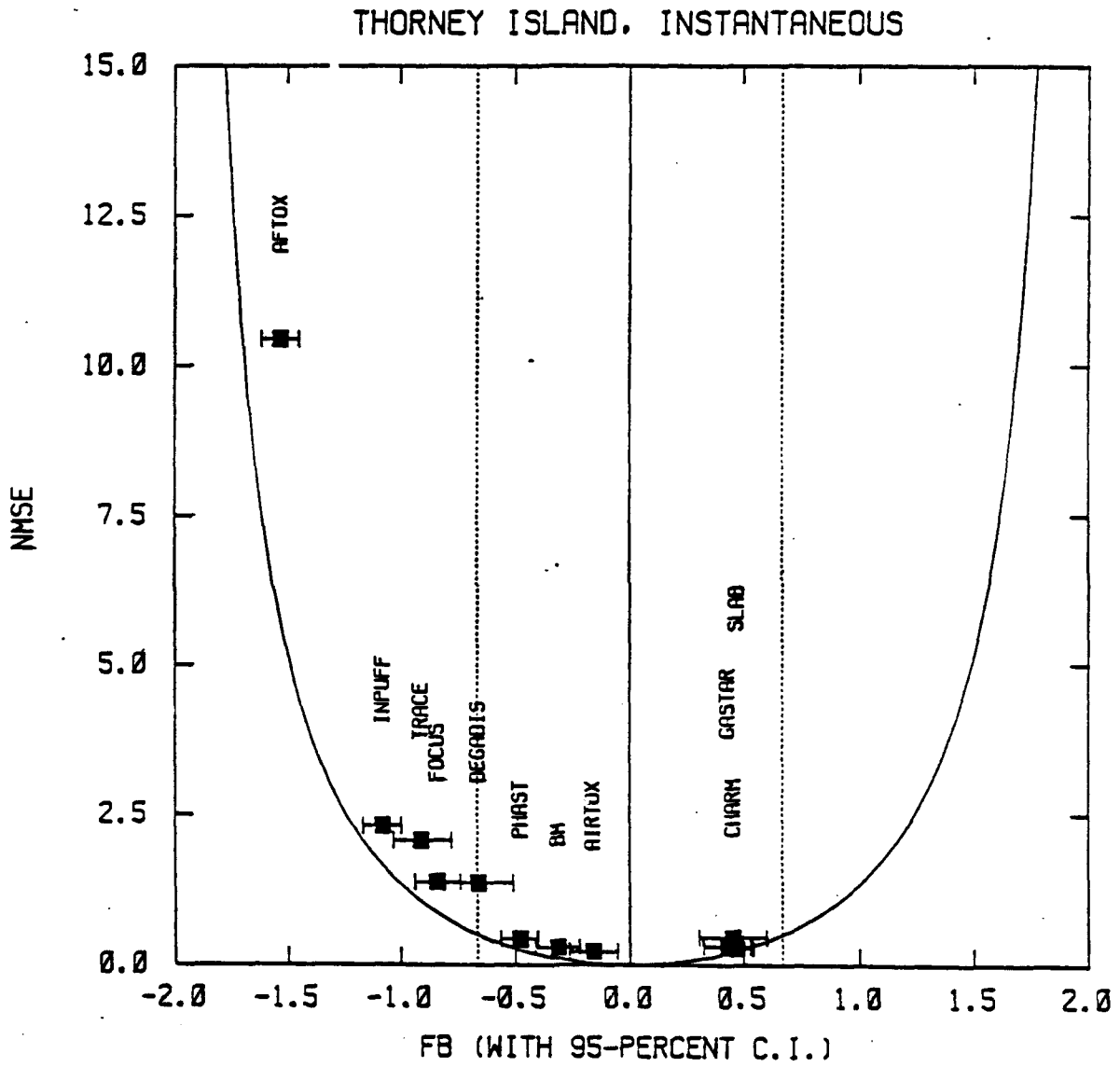


Figure E-10. A sample error bar plot with labelling (IPATTN = 6) generated by SIGPLOT.

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APPENDIX F-1

LISTINGS OF THE DUGWAY DATA ARCHIVES - HISTORICAL DATASETS

Dry Gulch, Course B

12 : number of trials included in DDA

3 : time zone designation

14.50 : latitude (deg)

120.50 : longitude (deg)

1 : trial ID

6 : month

23 : day

1961 : year

18 : hour

15 : minute

5 : no. of sources

1 : x-coord. of source (m)

0.0 : y-coord. of source (m)

2.50 : source elevation (m)

0.656 : emission rate (g/s)

1800.0 : total mass emitted (kg)

0.000 : alpha0 at the source (m)

0.000 : alpha0 at the source (m)

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Dry Gulch, Course B

12 : number of trials included in DDA
 # : time zone designation
 34.50 : latitude (deg)
 120.50 : longitude (deg)

Year	Month	Day	Hour	Minute	no. of sources	x-coord. of source (m)	y-coord. of source (m)	source elevation (m)	emission rate (g/s)	emission duration (s)	total mass emitted (kg)	sig0 at the source (m)	sig0 at the source (m)	ambient pressure (atm)	relative humidity (%)	temperature at level #1 (K)	measuring height for temperature #1 (m)	temperature at level #2 (K)	measuring height for temperature #2 (m)	wind speed (m/s) at a tower	measuring height for wind data (m)	domain-averaged wind speed (m/s)	domain-averaged wind direction (deg)	domain-averaged sigma-u (m/s)	domain-averaged sigma-theta (deg)	measuring ht for domain-avg wind speed (m)	averaging time for domain-avg wind speed (s)	wind speed power law exponent	surface roughness (m)	friction velocity (m)	inverse Monin-Obukhov length (1/m)	Albedo	moisture availability	Power ratio	Mixing height (m)	Cloud cover (%)	P-C stability class	averaging time for concentration (s)	suggested receptor height (m)	no. of distances downwind	distances downwind (m)	concentration (ug/m**3)	cross-wind integrated conc. (ug/m**2)	sigma-y (m)	distances downwind (m)	concentration (ug/m**3)	cross-wind integrated conc. (ug/m**2)	sigma-y (m)	
1961	1961	1961	1961	1961	1961	0.0	0.0	0.0	2.50	1.172	1.489	0.000	0.000	0.000	0.000	285.15	285.15	284.85	284.85	3.70	3.70	3.70	3.70	3.70	3.70	2820.0	2820.0	0.20	0.20	0.20	5.00	100.0	99.9	4.57	4.57	2	2301.0	3.520E-03	1.710E-03	5.990E+01	5.990E+01	5665.0	5665.0	5.230E-04	5.230E-04	5.990E+01	5.990E+01	5665.0	5665.0
1962	1962	1962	1962	1962	1962	0.0	0.0	0.0	2.50	1.172	1.489	0.000	0.000	0.000	285.15	285.15	284.85	284.85	3.70	3.70	3.70	3.70	3.70	3.70	2820.0	2820.0	0.20	0.20	0.20	5.00	100.0	99.9	4.57	4.57	2	2301.0	3.520E-03	1.710E-03	5.990E+01	5.990E+01	5665.0	5665.0	5.230E-04	5.230E-04	5.990E+01	5.990E+01	5665.0	5665.0	
1963	1963	1963	1963	1963	1963	0.0	0.0	0.0	2.50	1.172	1.489	0.000	0.000	0.000	285.15	285.15	284.85	284.85	3.70	3.70	3.70	3.70	3.70	3.70	2820.0	2820.0	0.20	0.20	0.20	5.00	100.0	99.9	4.57	4.57	2	2301.0	3.520E-03	1.710E-03	5.990E+01	5.990E+01	5665.0	5665.0	5.230E-04	5.230E-04	5.990E+01	5.990E+01	5665.0	5665.0	

Dry Gulch, Course D

12 : number of trials included in DOA

8 : time zone designation

34.50 : latitude (deg)

120.50 : longitude (deg)

dgdl : trial ID

6 : month

14 : day

1961 : year

10 : hour

45 : minute

1 : no. of sources

0.0 : y-coord. of source (m)

0.0 : x-coord. of source (m)

2.50 : source elevation (m)

1.400 : emission rate (g/s)

1800.0 : total mass emitted (kg)

-99.9 : emission duration (s)

0.000 : sig0 at the source (m)

0.000 : sig0 at the source (m)

0.000 : sig0 at the source (m)

-99.9 : ambient pressure (atm)

-99.9 : relative humidity (%)

283.15 : temperature at level #1 (K)

1.80 : measuring height for temperature #1 (m)

283.25 : temperature at level #2 (K)

16.50 : measuring height for temperature #2 (m)

1.80 : wind speed (m/s) at a tower

3.70 : measuring height for wind data (m)

2.90 : domain-averaged wind speed (m/s)

283.0 : domain-averaged wind direction (deg)

-99.90 : domain-averaged sigma-u (m/s)

18.40 : domain-averaged sigma-theta (deg)

-99.90 : domain-averaged sigma-phi (deg)

3.70 : measuring ht for domain-avg wind speed (m)

2820.0 : averaging time for domain-avg wind speed (s)

0.5000 : surface roughness (m)

-99.9000 : friction velocity (m)

-99.9000 : inverse Monin-Obukhov length (1/m)

0.30 : albedo

0.20 : moisture availability

5.00 : Bowen ratio

-99.9 : mixing height (m)

0.0 : cloud cover (%)

-99 : P-G stability class

2820.0 : suggested time for concentration (s)

4.57 : suggested receptor height (m)

853.0 : no. of distances downwind

1.340E-02 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

1500.0 : distances downwind (m)

8.360E-03 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

4715.0 : distances downwind (m)

5.080E-04 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

0 : no. of lines-of-sight

dgdl	6	14	1961	10	45	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl1	7	7	7	7	7	7	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl2	7	7	7	7	7	7	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl3	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl4	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl5	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl6	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl7	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl8	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl9	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl10	7	7	7	7	7	7	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl11	6	27	1961	19	15	1	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0
dgdl12	7	7	7	7	7	7	0.0	0.0	2.50	1.400	1800.0	-99.9	0.000	0.000	0.000	-99.9	-99.9	283.15	1.80	283.25	16.50	1.80	3.70	2.90	283.0	18.40	-99.90	3.70	2820.0	0.5000	-99.9000	-99.9000	0.30	0.20	5.00	-99.9	0.0	-99	2820.0	4.57	853.0	1.340E-02	-9.990E+01	1500.0	8.360E-03	-9.990E+01	4715.0	5.080E-04	-9.990E+01	-99.90	0

Dry Gulch, Course D

12 : number of trials included in DOA
 8 : time zone designation
 34.50 : latitude (deg)
 120.50 : longitude (deg)

ddq13	ddq14	ddq15	ddq16	ddq17	ddq18	ddq19	ddq20	ddq21	ddq22	ddq23	ddq24
1961	1961	1961	1961	1961	1961	1961	1961	1961	1961	1961	1961
17	35	1	1	1	1	1	1	1	1	1	1
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
0.970	1.090	1.010	1.010	1.010	1.010	1.040	1.030	0.680	1.300	0.710	0.710
1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
284.15	287.15	289.15	292.15	290.15	290.15	290.15	287.15	286.15	289.15	286.15	285.15
1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80
283.35	284.35	287.35	291.35	288.35	288.35	288.35	285.35	285.35	287.35	285.35	284.35
16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50
3.00	2.40	3.20	3.20	3.20	3.20	3.40	3.20	3.10	4.50	2.70	3.60
3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70
3.00	2.40	3.20	3.20	3.20	3.20	3.60	4.20	3.10	4.60	2.70	3.60
283.0	283.0	287.0	290.0	289.0	289.0	289.0	282.0	327.0	304.0	321.0	321.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
15.30	21.00	13.80	14.50	13.20	13.20	10.60	10.60	12.40	11.20	11.70	9.70
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30
0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57
853.0	853.0	853.0	853.0	853.0	853.0	853.0	853.0	853.0	853.0	853.0	853.0
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0	1500.0
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0	4715.0
7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04	7.190E-04
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90

Dry Gulch, Course D

12 : number of trials included in DDA

M : time zone designation

34.50 : latitude (deg)

120.50 : longitude (deg)

dgdl1 : longitude (deg)

dgdl2 : longitude (deg)

dgdl3 : longitude (deg)

dgdl4 : longitude (deg)

dgdl5 : longitude (deg)

dgdl6 : longitude (deg)

dgdl7 : longitude (deg)

dgdl8 : longitude (deg)

dgdl9 : longitude (deg)

dgdl10 : longitude (deg)

dgdl11 : longitude (deg)

dgdl12 : longitude (deg)

dgdl13 : longitude (deg)

dgdl14 : longitude (deg)

dgdl15 : longitude (deg)

dgdl16 : longitude (deg)

dgdl17 : longitude (deg)

dgdl18 : longitude (deg)

dgdl19 : longitude (deg)

dgdl20 : longitude (deg)

dgdl21 : longitude (deg)

dgdl22 : longitude (deg)

dgdl23 : longitude (deg)

dgdl24 : longitude (deg)

dgdl25 : longitude (deg)

dgdl26 : longitude (deg)

dgdl27 : longitude (deg)

dgdl28 : longitude (deg)

dgdl29 : longitude (deg)

dgdl30 : longitude (deg)

dgdl31 : longitude (deg)

dgdl32 : longitude (deg)

dgdl33 : longitude (deg)

dgdl34 : longitude (deg)

dgdl35 : longitude (deg)

dgdl36 : longitude (deg)

dgdl37 : longitude (deg)

dgdl38 : longitude (deg)

dgdl39 : longitude (deg)

dgdl40 : longitude (deg)

dgdl41 : longitude (deg)

dgdl42 : longitude (deg)

dgdl43 : longitude (deg)

dgdl44 : longitude (deg)

dgdl45 : longitude (deg)

dgdl46 : longitude (deg)

dgdl47 : longitude (deg)

dgdl48 : longitude (deg)

dgdl49 : longitude (deg)

dgdl50 : longitude (deg)

dgdl51 : longitude (deg)

dgdl52 : longitude (deg)

dgdl53 : longitude (deg)

dgdl54 : longitude (deg)

dgdl55 : longitude (deg)

dgdl56 : longitude (deg)

dgdl57 : longitude (deg)

dgdl58 : longitude (deg)

dgdl59 : longitude (deg)

dgdl60 : longitude (deg)

dgdl61 : longitude (deg)

dgdl62 : longitude (deg)

dgdl63 : longitude (deg)

dgdl64 : longitude (deg)

dgdl65 : longitude (deg)

dgdl66 : longitude (deg)

dgdl67 : longitude (deg)

dgdl68 : longitude (deg)

dgdl69 : longitude (deg)

dgdl70 : longitude (deg)

dgdl71 : longitude (deg)

dgdl72 : longitude (deg)

dgdl73 : longitude (deg)

dgdl74 : longitude (deg)

dgdl75 : longitude (deg)

dgdl76 : longitude (deg)

dgdl77 : longitude (deg)

dgdl78 : longitude (deg)

dgdl79 : longitude (deg)

dgdl80 : longitude (deg)

dgdl81 : longitude (deg)

dgdl82 : longitude (deg)

dgdl83 : longitude (deg)

dgdl84 : longitude (deg)

dgdl85 : longitude (deg)

dgdl86 : longitude (deg)

dgdl87 : longitude (deg)

Dry Gulch, Course D

j : number of trials included in DOA
 k : time zone designation
 34.50 : latitude (deg)
 120.50 : longitude (deg)
 dgd49 : trial ID
 dgd50 : trial ID
 6 : month
 26 : day
 1962 : year
 17 : hour
 45 : minute
 1 : no. of sources
 0.0 : x-coord. of source (m)
 0.0 : y-coord. of source (m)
 2.50 : source elevation (m)
 1.140 : emission rate (g/s)
 1800.0 : emission duration (s)
 -99.9 : total mass emitted (kg)
 0.000 : sign0 at the source (m)
 0.000 : sign0 at the source (m)
 -99.9 : ambient pressure (atm)
 -99.9 : relative humidity (%)
 283.15 : temperature at level #1 (K)
 1.80 : measuring height for temperature #1 (m)
 283.95 : temperature at level #2 (K)
 16.50 : measuring height for temperature #2 (m)
 16.50 : wind speed (m/s) at a tower
 3.20 : measuring height for wind data (m)
 3.20 : domain-averaged wind speed (m/s)
 317.0 : domain-averaged wind direction (deg)
 -99.90 : domain-averaged sigma-u (m/s)
 17.70 : domain-averaged sigma-theta (deg)
 -99.90 : domain-averaged sigma-phi (deg)
 1.70 : measuring ht for domain-avg wind speed (m)
 2820.0 : averaging time for domain-avg data (s)
 -99.900 : wind speed power law exponent
 0.5000 : surface roughness (m)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.30 : albedo
 0.20 : moisture availability
 5.00 : Bowen ratio
 -99.9 : mixing height (m)
 0.0 : cloud cover (%)
 -99 : P-G stability class
 2820.0 : averaging time for concentration (s)
 4.57 : suggested receptor height (m)
 3 : no. of distances downwind
 853.0 : distance downwind (m)
 3.520E-03 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)
 1500.0 : distance downwind (m)
 3.610E-03 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)
 4715.0 : distance downwind (m)
 1.030E-03 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)

Ocean Breeze

12 : number of trials included in DDA

5 : time zone designation

28.40 : latitude (deg)

80.73 : longitude (deg)

tbl : trial ID

tbl2 : trial ID

tbl3 : trial ID

tbl4 : trial ID

tbl5 : trial ID

tbl6 : trial ID

tbl7 : trial ID

tbl8 : trial ID

tbl9 : trial ID

tbl10 : trial ID

tbl11 : trial ID

tbl12 : trial ID

tbl13 : trial ID

tbl14 : trial ID

tbl15 : trial ID

tbl16 : trial ID

tbl17 : trial ID

tbl18 : trial ID

tbl19 : trial ID

tbl20 : trial ID

tbl21 : trial ID

tbl22 : trial ID

tbl23 : trial ID

tbl24 : trial ID

tbl25 : trial ID

tbl26 : trial ID

tbl27 : trial ID

tbl28 : trial ID

tbl29 : trial ID

tbl30 : trial ID

tbl31 : trial ID

tbl32 : trial ID

tbl33 : trial ID

tbl34 : trial ID

tbl35 : trial ID

tbl36 : trial ID

tbl37 : trial ID

tbl38 : trial ID

tbl39 : trial ID

tbl40 : trial ID

tbl41 : trial ID

tbl42 : trial ID

tbl43 : trial ID

tbl44 : trial ID

tbl45 : trial ID

tbl46 : trial ID

tbl47 : trial ID

tbl48 : trial ID

tbl49 : trial ID

tbl50 : trial ID

tbl51 : trial ID

tbl52 : trial ID

tbl53 : trial ID

tbl54 : trial ID

tbl55 : trial ID

tbl56 : trial ID

tbl57 : trial ID

tbl58 : trial ID

tbl59 : trial ID

tbl60 : trial ID

tbl61 : trial ID

tbl62 : trial ID

tbl63 : trial ID

tbl64 : trial ID

tbl65 : trial ID

tbl66 : trial ID

tbl67 : trial ID

tbl68 : trial ID

tbl69 : trial ID

tbl70 : trial ID

tbl71 : trial ID

tbl72 : trial ID

tbl73 : trial ID

tbl74 : trial ID

tbl75 : trial ID

tbl76 : trial ID

tbl77 : trial ID

tbl78 : trial ID

tbl79 : trial ID

tbl80 : trial ID

tbl81 : trial ID

tbl82 : trial ID

tbl83 : trial ID

tbl84 : trial ID

tbl85 : trial ID

tbl86 : trial ID

tbl87 : trial ID

Ocean Breeze

12 : number of trials included in DOA

5 : time zone designation

28.40 : latitude (deg)

80.70 : longitude (deg)

ob41 : ob42 ob43 ob44 ob45 ob46 ob47 ob48 ob49 ob50 ob51 ob52

ob41	ob42	ob43	ob44	ob45	ob46	ob47	ob48	ob49	ob50	ob51	ob52
1	1	1	1	1	1	1	1	1	1	1	1
29	30	31	31	31	31	31	31	31	31	31	31
1962	1962	1962	1962	1962	1962	1962	1962	1962	1962	1962	1962
13	13	13	13	13	13	13	13	13	13	13	13
15	14	15	15	14	14	14	16	13	15	13	15
30	5	54	42	47	48	2	19	35	15	37	7
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
1.600	1.600	1.600	1.600	1.600	1.600	1.600	1.611	1.600	1.628	1.600	1.617
1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
293.15	293.15	293.15	293.15	290.35	287.55	294.45	292.25	293.55	291.75	299.35	299.35
1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80
293.15	293.15	293.15	293.15	290.35	287.55	294.45	292.25	293.55	291.75	299.35	299.35
16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50
4.70	3.50	3.00	3.00	3.70	2.60	2.90	1.90	3.60	2.80	3.20	3.00
3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70
4.70	3.50	3.00	3.00	3.70	2.60	2.90	1.90	3.60	2.80	3.20	3.00
2.0	48.0	42.0	56.0	35.0	60.0	57.0	100.0	45.0	60.0	85.0	97.0
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
4.40	17.30	10.10	14.50	10.60	12.40	12.80	13.60	13.80	14.00	15.10	15.90
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000
0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0
4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57
1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0
3.910E-03	2.640E-03	2.640E-03	4.710E-02	6.820E-03	4.710E-02	1.120E-02	5.150E-02	6.540E-03	2.310E-02	1.180E-02	1.200E-02
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0
1.050E-01	2.110E-04	2.660E-03	2.270E-03	1.510E-03	1.430E-02	3.850E-03	9.270E-03	2.860E-03	1.370E-03	2.950E-03	3.850E-03
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0
2.710E-03	1.300E-04	1.400E-04	1.180E-03	8.370E-04	3.790E-03	1.110E-03	9.990E+01	8.600E-04	1.940E-03	9.990E+01	9.990E+01
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
0	0	0	0	0	0	0	0	0	0	0	0

Ocean Breeze

29.40 : latitude (deg)	30.70 : longitude (deg)	ob54	ob55	ob56	ob57	ob58	ob60	ob62	ob63	ob64	ob65	ob66 : trial ID
10	13	13	13	13	14	14	16	16	17	17	20	3 : month
162	1962	1962	1962	1962	1962	1962	1962	1962	1962	1962	1962	22 : day
18	44	44	44	44	46	46	53	53	53	51	40	15 : hour
1	1	1	1	1	1	1	1	1	1	1	1	51 : minute
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1 : no. of sources
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 : x-coord. of source (m)
2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	0.0 : y-coord. of source (m)
1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661	1.661 : source elevation (m)
1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1.661 : emission rate (g/s)
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	-99.9 : total mass emitted (kg)
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000 : sigma at the source (m)
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000 : sigma at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	0.000 : ambient pressure (atm)
294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65	294.65 : relative humidity (%)
1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80 : temperature at level #1 (K)
294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05	294.05 : measuring height for temperature #1 (m)
16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50	16.50 : temperature at level #2 (K)
3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20 : measuring height for temperature #2 (m)
3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20 : wind speed (m/s) at a tower
3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20 : measuring height for wind data (m)
24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0	24.0 : domain-averaged wind speed (m/s)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90 : domain-averaged wind direction (deg)
10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70	10.70 : domain-averaged sigma-u (m/s)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90 : domain-averaged sigma-theta (deg)
3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70	3.70 : domain-averaged sigma-phi (deg)
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0 : averaging ht for domain-avg wind speed (m)
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900 : wind speed power law exponent
0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000 : surface roughness (m)
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900 : friction velocity (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000 : inverse Moain-Obukhov length (1/m)
0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18 : albedo
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50 : moisture availability
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50 : Bowen ratio
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9 : mixing height (m)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	100.0 : cloud cover (%)
2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	2820.0	-99 : P-G stability class
4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57	4.57 : suggested receptor height (m)
1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	1200.0	3 : no. of distances downwind
4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02	4.670E-02 : distances downwind (m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	2.640E-02 : concentration (mg/m**3)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-9.990E+01 : cross-wind integrated conc. (mg/m**2)
2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	2400.0	-99.90 : sigma-y (m)
7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	7.950E-03	2400.0 : distances downwind (m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	5.120E-03 : concentration (mg/m**3)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-9.990E+01 : cross-wind integrated conc. (mg/m**2)
4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	4800.0	-99.90 : sigma-y (m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	4800.0 : distances downwind (m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	1.290E-03 : concentration (mg/m**3)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-9.990E+01 : cross-wind integrated conc. (mg/m**2)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90 : sigma-y (m)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	0 : no. of lines-of-sight

Ocean breeze

9 : number of trials included in DDA

5 : time zone designation

40 : latitude (deg)

80 : longitude (deg)

ob71 : ob69

ob72 : ob70

ob73 : ob71

ob74 : ob72

ob75 : ob73

ob76 : ob74

ob77 : ob75

ob78 : ob76

ob79 : ob77

ob80 : ob78

ob81 : ob79

ob82 : ob80

ob83 : ob81

ob84 : ob82

ob85 : ob83

ob86 : ob84

ob87 : ob85

ob88 : ob86

ob89 : ob87

ob90 : ob88

ob91 : ob89

ob92 : ob90

ob93 : ob91

ob94 : ob92

ob95 : ob93

ob96 : ob94

ob97 : ob95

ob98 : ob96

ob99 : ob97

ob100 : ob98

ob101 : ob99

ob102 : ob100

ob103 : ob101

ob104 : ob102

ob105 : ob103

ob106 : ob104

ob107 : ob105

ob108 : ob106

ob109 : ob107

ob110 : ob108

ob111 : ob109

ob112 : ob110

ob113 : ob111

ob114 : ob112

ob115 : ob113

ob116 : ob114

ob117 : ob115

ob118 : ob116

ob119 : ob117

ob120 : ob118

ob121 : ob119

ob122 : ob120

ob123 : ob121

ob124 : ob122

ob125 : ob123

ob126 : ob124

ob127 : ob125

ob128 : ob126

ob129 : ob127

ob130 : ob128

ob131 : ob129

ob132 : ob130

ob133 : ob131

ob134 : ob132

ob135 : ob133

ob136 : ob134

ob75 : trial ID
 3 : month
 30 : day
 1962 : year
 18 : hour
 48 : minute
 1 : no. of sources
 0.0 : x-coord. of source (m)
 0.0 : y-coord. of source (m)
 2.50 : source elevation (m)
 1.244 : emission rate (g/s)
 1800.0 : emission duration (s)
 -99.9 : total mass emitted (kg)
 0.000 : sig0 at the source (m)
 0.000 : sig70 at the source (m)
 0.000 : sig0 at the source (m)
 -99.9 : ambient pressure (atm)
 -99.9 : relative humidity (%)
 298.15 : temperature at level #1 (K)
 1.80 : measuring height for temperature #1 (m)
 298.15 : temperature at level #2 (K)
 16.50 : measuring height for temperature #2 (m)
 3.30 : wind speed (m/s) at a tower
 3.70 : measuring height for wind data (m)
 155.0 : domain-averaged wind speed (m/s)
 -99.90 : domain-averaged wind direction (deg)
 10.60 : domain-averaged sigma-u (m/s)
 -99.90 : domain-averaged sigma-theta (deg)
 3.70 : measuring time for domain-avg wind speed (m)
 2820.0 : averaging time for domain-avg data (s)
 -99.9000 : wind speed power law exponent
 0.1000 : surface roughness (m)
 -99.9000 : friction velocity (m)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.18 : albedo
 0.50 : moisture availability
 0.50 : Bowen ratio
 -99.9 : mixing height (m)
 37.5 : cloud cover (%)
 -99 : P-G stability class
 2820.0 : averaging time for concentration (s)
 4.57 : suggested receptor height (m)
 3 : no. of distances downwind
 1200.0 : distance downwind (m)
 2.000E-02 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)
 2400.0 : distance downwind (m)
 5.000E-03 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)
 4800.0 : distance downwind (m)
 -9.990E+01 : concentration (mg/m**3)
 -9.990E+01 : cross-wind integrated conc. (mg/m**2)
 -99.90 : sigma-y (m)
 0 : no. of lines-of-sight

Green Glow

12	11	10	9	8	7	6	5	4	3	2	1	0
number of trials included in DDA	time zone designation	latitude (deg)	longitude (deg)	9918	9919	9920	9921	9922	9923	9924	9925	9926
46.40	1959	1959	1959	1959	1959	1959	1959	1959	1959	1959	1959	1959
119.20	0	0	0	0	0	0	0	0	0	0	0	0
9919	9918	9917	9916	9915	9914	9913	9912	9911	9910	9909	9908	9907
1	1	1	1	1	1	1	1	1	1	1	1	1
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
1.289	1.761	1.750	2.017	1.983	2.000	2.000	2.000	1.983	2.050	1.900	1.983	1.983
1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0	1800.0
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
289.15	297.15	300.15	299.15	295.15	298.15	298.15	298.15	291.15	292.15	288.15	296.15	291.15
0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
292.35	300.85	300.55	299.55	295.25	298.95	298.95	292.25	291.45	292.25	292.95	296.35	291.45
15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20	15.20
1.70	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
1.70	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
279.0	300.0	319.0	322.0	309.0	316.0	316.0	313.0	313.0	315.0	313.0	316.0	325.0
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900	99.900
0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000
99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000
0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30
0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
7.720E-01	6.510E-01	5.790E-01	4.450E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01	6.490E-01
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
5.620E-02	5.040E-02	8.780E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02	2.880E-02
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0	1600.0
2.290E-02	1.400E-02	8.220E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03	5.960E-03
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0	3200.0
7.010E-03	3.450E-03	1.030E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03	1.860E-03
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0	12800.0
9.470E-04	3.780E-04	3.110E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04	3.210E-04
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0	25600.0
7.790E-05	1.620E-04	1.820E-04	7.340E-05	2.830E-04	1.730E-04	3.430E-04	3.430E-04	3.430E-04	3.430E-04	3.430E-04	3.430E-04	3.430E-04
9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01	9.990E-01
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90

Profile Grass
 12 : number of trials included in DWA

pg7	pg8	pg9	pg10	pg13	pg15	pg16	pg17	pg18	pg19	pg20	pg21
42.30 : latitude (deg)	98.30 : longitude (deg)	6 : time designation	12 : number of trials included in DWA	6 : time designation	6 : time designation	6 : time designation	6 : time designation	6 : time designation	6 : time designation	6 : time designation	6 : time designation
pg7	pg8	pg9	pg10	pg13	pg15	pg16	pg17	pg18	pg19	pg20	pg21
7	7	7	7	7	7	7	7	7	7	7	7
10	11	11	22	23	23	23	23	23	25	25	25
1956	1956	1956	1956	1956	1956	1956	1956	1956	1956	1956	1956
14	17	16	20	20	20	20	20	22	11	14	14
0	0	0	0	0	0	0	0	0	0	0	0
1	1	1	1	1	1	1	1	1	1	1	1
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
89.900	91.100	92.000	92.100	95.500	93.000	93.000	93.000	93.000	101.800	101.800	101.800
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
305.15	305.15	305.15	304.15	293.15	301.15	301.15	301.15	297.15	302.15	307.15	307.15
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
303.55	303.95	299.55	302.15	295.05	300.15	300.15	300.65	298.75	300.85	304.85	304.85
16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00
4.20	4.90	6.90	4.60	3.40	3.20	3.20	3.30	3.50	5.80	8.60	8.60
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
4.20	4.90	6.90	4.60	3.40	3.20	3.20	3.30	3.50	5.80	8.60	8.60
186.0	184.0	204.0	225.0	209.0	192.0	192.0	184.0	187.0	166.0	178.0	178.0
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
25.60	10.20	10.20	15.80	12.80	18.50	18.50	5.60	11.30	11.60	8.20	8.20
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900
0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060
0.310	0.310	0.460	0.320	0.390	0.240	0.240	0.210	0.200	0.0660	0.0060	0.0060
-0.1020	-0.0556	-0.0323	-0.0909	0.2911	-0.1316	-0.1923	0.0208	0.0400	-0.0357	-0.0161	-0.0161
0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
1539.0	1580.0	626.0	1090.0	99.9	86.0	1259.0	99.9	745.0	745.0	813.0	813.0
0.0	0.0	30.0	30.0	20.0	0.0	0.0	70.0	10.0	30.0	20.0	20.0
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
5	5	5	5	5	5	5	5	5	5	5	5
9.260E+01	3.963E+02	1.858E+02	1.704E+02	3.887E+02	1.748E+02	1.748E+02	6.102E+02	6.044E+02	2.024E+02	1.569E+02	1.569E+02
4.001E+03	5.102E+03	3.698E+03	4.504E+03	7.096E+03	5.003E+03	5.003E+03	6.221E+03	6.221E+03	4.500E+03	3.400E+03	3.400E+03
100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
2.167E+01	1.066E+02	5.272E+01	4.052E+01	1.031E+02	3.301E+01	3.301E+01	2.554E+02	2.494E+02	5.100E+01	4.858E+01	4.858E+01
2.203E+03	2.596E+03	2.199E+03	1.796E+03	3.400E+03	1.795E+03	1.795E+03	-9.990E+01	-9.990E+01	2.199E+01	1.801E+01	1.801E+01
200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
4.225E+00	2.378E+01	1.306E+01	1.050E+01	2.063E+01	6.008E+00	6.008E+00	8.023E+01	9.216E+01	1.222E+01	1.417E+01	1.417E+01
9.975E+02	1.102E+03	1.003E+03	7.101E+02	1.347E+03	4.799E+02	4.799E+02	1.921E+03	2.650E+03	8.602E+02	8.501E+02	8.501E+02
22.00	200.0	31.00	35.00	26.00	49.00	49.00	27.00	27.00	32.00	37.00	37.00
400.0	400.0	400.0	400.0	400.0	400.0	400.0	400.0	400.0	400.0	400.0	400.0
6.841E-01	3.781E+00	2.696E+00	2.487E+00	4.545E+00	5.924E-01	5.924E-01	3.100E+01	3.100E+01	1.914E+00	3.008E+00	3.008E+00
4.001E+02	3.899E+02	4.103E+02	1.999E+02	3.698E+02	1.074E+02	1.074E+02	-9.990E+01	-9.990E+01	2.698E+02	3.400E+02	3.400E+02
39.00	800.0	61.00	61.00	45.00	72.00	72.00	55.00	55.00	49.00	49.00	49.00
800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0
7.363E-02	6.714E-01	4.839E-01	1.584E-01	5.186E-01	4.752E-02	4.752E-02	1.390E+01	1.390E+01	3.370E-01	7.124E-01	7.124E-01
1.798E+02	1.403E+02	1.297E+02	3.223E+01	1.098E+02	1.674E+01	1.674E+01	6.215E+02	1.152E+03	5.803E+01	1.295E+02	1.295E+02
71.00	86.00	116.00	97.00	92.00	116.00	116.00	85.00	85.00	85.00	90.00	90.00

Prairie Grass

12 : number of trials included in DDA

16 : time zone designation

98.30 : latitude (deg)

98.30 : longitude (deg)

pg22 : pg23

pg24 : pg25

pg26 : pg27

pg28 : pg29

pg30 : pg31

pg32 : pg33

pg34 : pg35

pg36 : pg37

pg38 : trial ID

8 : month

12 : day

1956 : year

5 : hour

0 : minute

1 : no. of sources

0.0 : x-coord. of source (m)

0.0 : y-coord. of source (m)

0.45 : source elevation (m)

45.400 : emission rate (g/s)

600.0 : emission duration (s)

-99.9 : total mass emitted (kg)

0.000 : sign0 at the source (m)

0.000 : sign0 at the source (m)

0.000 : sign0 at the source (m)

-99.9 : relative humidity (%)

-99.9 : relative humidity (%)

294.15 : temperature at level #1 (K)

2.00 : measuring height for temperature #1 (m)

294.35 : temperature at level #2 (K)

2.00 : measuring height for temperature #2 (m)

16.00 : measuring height for temperature #2 (m)

4.10 : wind speed (m/s) at a tower

2.00 : measuring height for wind data (m)

4.10 : domain-averaged wind speed (m/s)

170.0 : domain-averaged wind direction (deg)

-99.90 : domain-averaged wind direction (deg)

5.00 : domain-averaged sigma-phi (deg)

-99.90 : domain-averaged sigma-phi (deg)

2.00 : measuring ht for domain-avg wind speed (m)

600.0 : averaging time for domain-avg data (s)

-99.900 : wind speed power law exponent

0.0060 : surface roughness (m)

0.0060 : friction velocity (m/s)

0.010 : inverse Monin-Obukhov length (1/m)

0.20 : albedo

0.30 : moisture availability

2.00 : Bowen ratio

-99.9 : mixing height (m)

80.0 : cloud cover (%)

4 : P-G stability class

600.0 : averaging time for concentration (s)

1.50 : suggested receptor height (m)

5 : no. of distances downwind

30.0 : distances downwind (m)

3.528E+02 : concentration (mg/m**3)

3.541E+03 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

100.0 : distances downwind (m)

7.738E+01 : concentration (mg/m**3)

1.516E+02 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

200.0 : distances downwind (m)

5.039E+01 : concentration (mg/m**3)

1.180E+03 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

400.0 : distances downwind (m)

1.834E+01 : concentration (mg/m**3)

9.990E+01 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

800.0 : distances downwind (m)

6.311E+00 : concentration (mg/m**3)

3.832E+02 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

0 : no. of lines-of-sight

Prairie Grass

11 : number of trials included in DDA
 12 : time zone designation
 42.30 : latitude (deg)
 98.30 : longitude (deg)

PG41	PG42	PG43	PG44	PG45	PG48	PG49	PG50	PG51	PG53	PG54
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
39.900	56.400	98.600	100.700	100.800	104.100	102.800	102.800	102.400	45.200	43.400
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
294.15	296.15	308.15	310.15	309.15	293.15	297.15	304.15	305.15	290.15	292.15
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
293.55	306.55	308.55	308.55	308.75	291.95	295.35	302.55	303.75	294.05	293.05
16.00	18.00	18.00	18.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00
5.80	5.80	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
4.00	4.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
190.0	212.0	170.0	158.0	163.0	214.0	199.0	215.0	245.0	132.0	140.0
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
5.00	6.60	12.20	12.20	6.90	8.10	11.90	10.80	10.80	3.90	5.90
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900
0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060	0.0060
0.370	0.370	0.350	0.400	0.390	0.510	0.450	0.450	0.450	0.170	0.0660
0.0286	0.0286	-0.0625	-0.0400	-0.0115	-0.0120	-0.0357	-0.0385	-0.0250	0.1000	0.0250
0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
-99.9	-99.9	683.0	683.0	-99.9	638.0	638.0	638.0	2136.0	-99.9	-99.9
0.0	0.0	100.0	100.0	90.0	10.0	10.0	10.0	10.0	0.0	0.0
0.0	0.0	3	3	4	4	3	3	4	6	4
600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0	600.0
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
5	5	5	5	5	5	5	5	5	5	5
4.349E+02	2.651E+02	2.268E+02	1.742E+02	3.326E+02	2.155E+02	2.030E+02	2.231E+02	2.560E+02	9.130E+02	4.136E+02
3.152E+03	2.933E+03	4.999E+03	4.501E+03	5.242E+03	4.997E+03	4.304E+03	4.205E+03	4.700E+03	6.961E+03	3.515E+03
100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
1.831E+02	9.701E+01	5.236E+01	4.582E+01	1.048E+02	6.298E+01	6.344E+01	7.165E+01	6.748E+01	5.198E+02	1.641E+02
-9.990E+01	-9.990E+01	2.395E+03	2.295E+03	-9.990E+01	-9.990E+01	2.397E+03	2.330E+03	2.395E+03	-9.990E+01	-9.990E+01
200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
6.504E+01	3.023E+01	1.469E+01	1.309E+01	3.539E+01	1.624E+01	1.754E+01	1.708E+01	1.710E+01	2.237E+02	5.946E+01
1.277E+03	9.588E+02	1.085E+03	1.088E+03	1.714E+03	6.246E+02	1.193E+03	9.099E+02	1.000E+03	3.752E+03	1.302E+03
-99.90	-99.90	400.0	400.0	-99.90	-99.90	35.00	28.00	32.00	-99.90	-99.90
2.374E+01	7.558E+00	2.288E+00	2.648E+00	7.772E+00	4.497E+00	3.091E+00	3.526E+00	2.703E+00	400.0	400.0
-9.990E+01	-9.990E+01	3.699E+02	4.300E+02	-9.990E+01	-9.990E+01	4.498E+02	3.899E+02	3.799E+02	-9.990E+01	-9.990E+01
800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0	800.0
9.546E+00	2.044E+00	4.693E-01	5.367E-01	2.591E+00	1.260E+00	5.355E-01	5.520E-01	4.055E-01	9.244E+00	9.244E+00
4.788E+02	2.820E+02	1.203E+02	1.400E+02	3.528E+02	-9.990E+01	1.499E+02	1.100E+02	8.397E+01	2.802E+03	4.774E+02
-99.90	-99.90	126.00	126.00	-99.90	-99.90	118.00	115.00	11.00	-99.90	-99.90

Prairie Grass

8 : number of trials included in DDA

6 : time zone designation

98.30 : latitude (deg)

99.30 : longitude (deg)

p955 : p956

p957

p958

p959

p960

p961

p962 : trial ID

0 : month

26 : day

1956 : year

14 : hour

0 : minute

1 : no. of sources

0.0 : x-coord. of source (m)

0.0 : y-coord. of source (m)

0.45 : source elevation (m)

102.100 : source elevation (m)

600.0 : emission rate (g/s)

-99.9 : total mass emitted (kg)

0.000 : sign0 at the source (m)

0.000 : sign0 at the source (m)

0.000 : sign0 at the source (m)

-99.9 : ambient pressure (atm)

-99.9 : relative humidity (%)

305.15 : temperature at level #1 (K)

2.00 : measuring height for temperature #1 (m)

304.15 : temperature at level #2 (K)

16.00 : measuring height for temperature #2 (m)

5.20 : wind speed (m/s) at a tower

2.00 : measuring height for wind data (m)

5.20 : domain-averaged wind speed (m/s)

212.0 : domain-averaged wind direction (deg)

-99.90 : domain-averaged sigma-u (m/s)

8.80 : domain-averaged sigma-theta (deg)

-99.90 : domain-averaged sigma-phi (deg)

2.00 : measuring ht for domain-avg wind speed (m)

600.0 : averaging time for domain-avg wind speed (s)

-99.900 : wind speed power law exponent

0.0060 : surface roughness (m)

0.340 : friction velocity (m/s)

-0.0333 : inverse Monin-Obukhov length (1/m)

0.20 : albedo

0.50 : moisture availability

2.00 : Bowen ratio

-99.9 : mixing height (m)

80.0 : cloud cover (%)

3 : P-G stability class

600.0 : averaging time for concentration (s)

1.50 : suggested receptor height (m)

5 : no. of distances downwind

50.0 : distances downwind (m)

-9.990E+01 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

100.0 : sigma-y (m)

100.0 : distances downwind (m)

1.041E+02 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

19.00 : sigma-y (m)

200.0 : distances downwind (m)

2.940E+01 : concentration (mg/m**3)

1.327E+03 : cross-wind integrated conc. (mg/m**2)

35.00 : sigma-y (m)

400.0 : distances downwind (m)

7.105E+01 : concentration (mg/m**3)

-9.990E+01 : cross-wind integrated conc. (mg/m**2)

65.00 : sigma-y (m)

800.0 : distances downwind (m)

1.848E+00 : concentration (mg/m**3)

2.348E+02 : cross-wind integrated conc. (mg/m**2)

-99.90 : sigma-y (m)

0 : no. of lines-of-sight

0

0

0

0

0

0

0

0

0

APPENDIX F-2

LISTINGS OF THE DUGWAY DATA ARCHIVES - SMOKE/OBSCURANT DATASETS

The Development Test 1 of Mile (M), M0003 (M) and M0023 (M) Granules (M0003 M) only, (M) (M)

4 : Time zone designation		5 : Number of trials included in DOB		6 : Latitude (deg)		7 : Longitude (deg)		8 : Time zone designation		9 : Number of trials included in DOB		10 : Latitude (deg)		11 : Longitude (deg)		12 : Time zone designation		13 : Number of trials included in DOB		14 : Latitude (deg)		15 : Longitude (deg)		16 : Time zone designation		17 : Number of trials included in DOB		18 : Latitude (deg)		19 : Longitude (deg)		20 : Time zone designation																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																									
G181	G201	G211	G221	G231	G241	G251	G261	G271	G281	G291	G301	G311	G321	G331	G341	G351	G361	G371	G381	G391	G401	G411	G421	G431	G441	G451	G461	G471	G481	G491	G501	G511	G521	G531	G541	G551	G561	G571	G581	G591	G601	G611	G621	G631	G641	G651	G661	G671	G681	G691	G701	G711	G721	G731	G741	G751	G761	G771	G781	G791	G801	G811	G821	G831	G841	G851	G861	G871	G881	G891	G901	G911	G921	G931	G941	G951	G961	G971	G981	G991	G1001	G1011	G1021	G1031	G1041	G1051	G1061	G1071	G1081	G1091	G1101	G1111	G1121	G1131	G1141	G1151	G1161	G1171	G1181	G1191	G1201	G1211	G1221	G1231	G1241	G1251	G1261	G1271	G1281	G1291	G1301	G1311	G1321	G1331	G1341	G1351	G1361	G1371	G1381	G1391	G1401	G1411	G1421	G1431	G1441	G1451	G1461	G1471	G1481	G1491	G1501	G1511	G1521	G1531	G1541	G1551	G1561	G1571	G1581	G1591	G1601	G1611	G1621	G1631	G1641	G1651	G1661	G1671	G1681	G1691	G1701	G1711	G1721	G1731	G1741	G1751	G1761	G1771	G1781	G1791	G1801	G1811	G1821	G1831	G1841	G1851	G1861	G1871	G1881	G1891	G1901	G1911	G1921	G1931	G1941	G1951	G1961	G1971	G1981	G1991	G2001	G2011	G2021	G2031	G2041	G2051	G2061	G2071	G2081	G2091	G2101	G2111	G2121	G2131	G2141	G2151	G2161	G2171	G2181	G2191	G2201	G2211	G2221	G2231	G2241	G2251	G2261	G2271	G2281	G2291	G2301	G2311	G2321	G2331	G2341	G2351	G2361	G2371	G2381	G2391	G2401	G2411	G2421	G2431	G2441	G2451	G2461	G2471	G2481	G2491	G2501	G2511	G2521	G2531	G2541	G2551	G2561	G2571	G2581	G2591	G2601	G2611	G2621	G2631	G2641	G2651	G2661	G2671	G2681	G2691	G2701	G2711	G2721	G2731	G2741	G2751	G2761	G2771	G2781	G2791	G2801	G2811	G2821	G2831	G2841	G2851	G2861	G2871	G2881	G2891	G2901	G2911	G2921	G2931	G2941	G2951	G2961	G2971	G2981	G2991	G3001	G3011	G3021	G3031	G3041	G3051	G3061	G3071	G3081	G3091	G3101	G3111	G3121	G3131	G3141	G3151	G3161	G3171	G3181	G3191	G3201	G3211	G3221	G3231	G3241	G3251	G3261	G3271	G3281	G3291	G3301	G3311	G3321	G3331	G3341	G3351	G3361	G3371	G3381	G3391	G3401	G3411	G3421	G3431	G3441	G3451	G3461	G3471	G3481	G3491	G3501	G3511	G3521	G3531	G3541	G3551	G3561	G3571	G3581	G3591	G3601	G3611	G3621	G3631	G3641	G3651	G3661	G3671	G3681	G3691	G3701	G3711	G3721	G3731	G3741	G3751	G3761	G3771	G3781	G3791	G3801	G3811	G3821	G3831	G3841	G3851	G3861	G3871	G3881	G3891	G3901	G3911	G3921	G3931	G3941	G3951	G3961	G3971	G3981	G3991	G4001	G4011	G4021	G4031	G4041	G4051	G4061	G4071	G4081	G4091	G4101	G4111	G4121	G4131	G4141	G4151	G4161	G4171	G4181	G4191	G4201	G4211	G4221	G4231	G4241	G4251	G4261	G4271	G4281	G4291	G4301	G4311	G4321	G4331	G4341	G4351	G4361	G4371	G4381	G4391	G4401	G4411	G4421	G4431	G4441	G4451	G4461	G4471	G4481	G4491	G4501	G4511	G4521	G4531	G4541	G4551	G4561	G4571	G4581	G4591	G4601	G4611	G4621	G4631	G4641	G4651	G4661	G4671	G4681	G4691	G4701	G4711	G4721	G4731	G4741	G4751	G4761	G4771	G4781	G4791	G4801	G4811	G4821	G4831	G4841	G4851	G4861	G4871	G4881	G4891	G4901	G4911	G4921	G4931	G4941	G4951	G4961	G4971	G4981	G4991	G5001	G5011	G5021	G5031	G5041	G5051	G5061	G5071	G5081	G5091	G5101	G5111	G5121	G5131	G5141	G5151	G5161	G5171	G5181	G5191	G5201	G5211	G5221	G5231	G5241	G5251	G5261	G5271	G5281	G5291	G5301	G5311	G5321	G5331	G5341	G5351	G5361	G5371	G5381	G5391	G5401	G5411	G5421	G5431	G5441	G5451	G5461	G5471	G5481	G5491	G5501	G5511	G5521	G5531	G5541	G5551	G5561	G5571	G5581	G5591	G5601	G5611	G5621	G5631	G5641	G5651	G5661	G5671	G5681	G5691	G5701	G5711	G5721	G5731	G5741	G5751	G5761	G5771	G5781	G5791	G5801	G5811	G5821	G5831	G5841	G5851	G5861	G5871	G5881	G5891	G5901	G5911	G5921	G5931	G5941	G5951	G5961	G5971	G5981	G5991	G6001	G6011	G6021	G6031	G6041	G6051	G6061	G6071	G6081	G6091	G6101	G6111	G6121	G6131	G6141	G6151	G6161	G6171	G6181	G6191	G6201	G6211	G6221	G6231	G6241	G6251	G6261	G6271	G6281	G6291	G6301	G6311	G6321	G6331	G6341	G6351	G6361	G6371	G6381	G6391	G6401	G6411	G6421	G6431	G6441	G6451	G6461	G6471	G6481	G6491	G6501	G6511	G6521	G6531	G6541	G6551	G6561	G6571	G6581	G6591	G6601	G6611	G6621	G6631	G6641	G6651	G6661	G6671	G6681	G6691	G6701	G6711	G6721	G6731	G6741	G6751	G6761	G6771	G6781	G6791	G6801	G6811	G6821	G6831	G6841	G6851	G6861	G6871	G6881	G6891	G6901	G6911	G6921	G6931	G6941	G6951	G6961	G6971	G6981	G6991	G7001	G7011	G7021	G7031	G7041	G7051	G7061	G7071	G7081	G7091	G7101	G7111	G7121	G7131	G7141	G7151	G7161	G7171	G7181	G7191	G7201	G7211	G7221	G7231	G7241	G7251	G7261	G7271	G7281	G7291	G7301	G7311	G7321	G7331	G7341	G7351	G7361	G7371	G7381	G7391	G7401	G7411	G7421	G7431	G7441	G7451	G7461	G7471	G7481	G7491	G7501	G7511	G7521	G7531	G7541	G7551	G7561	G7571	G7581	G7591	G7601	G7611	G7621	G7631	G7641	G7651	G7661	G7671	G7681	G7691	G7701	G7711	G7721	G7731	G7741	G7751	G7761	G7771	G7781	G7791	G7801	G7811	G7821	G7831	G7841	G7851	G7861	G7871	G7881	G7891	G7901	G7911	G7921	G7931	G7941	G7951	G7961	G7971	G7981	G7991	G8001	G8011	G8021	G8031	G8041	G8051	G8061	G8071	G8081	G8091	G8101	G8111	G8121	G8131	G8141	G8151	G8161	G8171	G8181	G8191	G8201	G8211	G8221	G8231	G8241	G8251	G8261	G8271	G8281	G8291	G8301	G8311	G8321	G8331	G8341	G8351	G8361	G8371	G8381	G8391	G8401	G8411	G8421	G8431	G8441	G8451	G8461	G8471	G8481	G8491	G8501	G8511	G8521	G8531	G8541	G8551	G8561	G8571	G8581	G8591	G8601	G8611	G8621	G8631	G8641	G8651	G8661	G8671	G8681	G8691	G8701	G8711	G8721	G8731	G8741	G8751	G8761	G8771	G8781	G8791	G8801	G8811	G8821	G8831	G8841	G8851	G8861	G8871	G8881	G8891	G8901	G8911	G8921	G8931	G8941	G8951	G8961	G8971	G8981	G8991	G9001	G9011	G9021	G9031	G9041	G9051	G9061	G9071	G9081	G9091	G9101	G9111	G9121	G9131	G9141	G9151	G9161	G9171	G9181	G9191	G9201	G9211	G9221	G9231	G9241	G9251	G9261	G9271	G9281	G9291	G9301	G9311	G9321	G9331	G9341	G9351	G9361	G9371	G9381	G9391	G9401	G9411	G9421	G9431	G9441	G9451	G9461	G9471	G9481	G9491	G9501	G9511	G9521	G9531	G9541	G9551	G9561	G9571	G9581	G9591	G9601	G9611	G9621	G9631	G9641	G9651	G9661	G9671	G9681	G9691	G9701	G9711	G9721	G9731	G9741	G9751	G9761	G9771	G9781	G9791	G9801	G9811	G9821	G9831	G9841	G9851	G9861	G9871	G9881	G9891	G9901	G9911	G9921	G9931	G9941	G9951	G9961	G9971	G9981	G9991	G10001	G10011	G10021	G10031	G10041	G10051	G10061	G10071	G10081	G10091	G10101	G10111	G10121	G10131	G10141	G10151	G10161	G10171	G10181	G10191	G10201	G10211	G10221	G10231	G10241	G10251	G10261	G10271	G10281	G10291	G10301	G10311	G10321	G10331	G10341	G10351	G10361	G10371	G10381	G10391	G10401	G10411	G10421	G10431	G10441	G10451	G10461	G10471	G10481	G10491	G10501	G10511	G10521	G10531	G10541	G10551	G10561	G10571	G10581	G10591	G10601	G10611	G10621	G10631	G10641	G10651	G10661	G10671	G10681	G10691	G10701	G10711	G10721	G10731	G10741	G10751	G10761	G10771	G10781	G10791	G10801	G10811	G10821	G10831	G10841	G10851	G10861	G10871	G10881	G10891	G10901	G10911	G10921	G10931	G10941	G10951	G10961	G10971	G10981	G10991	G11001	G11011	G11021	G11031	G11041	G11051	G11061	G11071	G11081	G11091	G11101	G11111	G11121	G11131	G11141	G11151	G11161	G11171	G11181	G11191	G11201	G11211	G11221	G11231	G11241	G11251	G11261	G11271	G11281	G11291	G11301	G11311	G11321	G11331	G11341	G11351	G11361	G11371	G11381	G11391	G11401	G11411	G11421	G11431	G11441	G11451	G11461	G11471	G11481	G11491	G11501	G11511	G11521	G11531	G11541	G11551	G11561	G11571	G11581	G11591	G11601	G11611	G11621	G11631	G11641	G11651	G11661	G11671	G11681	G11691	G11701	G11711	G11721	G11731	G11741	G11751	G11761	G11771	G11781	G11791	G11801	G11811	G11821	G11831	G11841	G11851	G11861	G11871	G11881	G11891	G11901	G11911	G11921	G11931	G11941	G11951	G11961	G11971	G11981	G11991	G12001	G12011	G12021	G12031	G12041	G12051	G12061	G12071	G12081	G12091	G12101	G12111	G12121	G12131	G12141	G12151	G12161	G12171	G12181	G12191	G12201	G12211	G12221	G12231	G12241	G12251	G12261	G12271	G12281	G12291	G12301	G12311	G12321	G12331	G12341	G12351	G12361	G12371	G12381	G12391	G12401	G12411	G12421	G12431	G12441	G12451	G12461	G12471	G12481	G12491	G12501	G12511	G12521	G12531	G12541	G12551	G12561	G12571	G12581	G12591	G12601	G12611	G12621	G12631	G12641	G12651	G12661	G12671	G12681	G12691	G12701	G12711	G12721	G12731	G12741	G12751	G12761	G12771	G12781	G12791	G12801	G12811	G12821	G12831	G12841	G12851	G12861	G12871	G12881	G12891	G12901	G12911	G12921	G12931	G12941	G12951	G12961	G12971	G12981	G12991	G13001	G13011	G13021	G13031	G13041	G13051	G13061	G13071	G13081	G13091	G13101	G13111	G13121	G13131	G13141	G13151	G13161	G13171	G13181	G13191	G13201	G13211	G13221	G13231	G1

-131.6	0.00	-113.7	-183.5	-113.7	-128.2	-38.3	-58.3	-32.1	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
0.145	1.584	3.737	1.377	1.507	1.595	1.263	0.271	0.271	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
93.1	104.8	37.8	-26.4	37.8	11.5	-14.7	-67.2	-81.7	x-coord. of source (m)
-137.0	-95.3	-99.1	-169.0	-99.1	-128.2	-157.3	-157.3	-131.0	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
0.145	1.584	3.737	1.377	1.507	1.595	1.263	0.271	0.271	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
119.4	119.4	64.0	-84.0	64.0	-113.7	-40.9	-142.7	-55.5	x-coord. of source (m)
-122.5	-81.7	-84.6	-154.4	-84.6	-113.7	-142.7	-142.7	-116.5	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
2.610	1.267	2.180	1.989	3.164	1.885	1.684	0.947	0.406	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
145.8	145.8	64.0	-84.0	64.0	-113.7	-40.9	-142.7	-55.5	x-coord. of source (m)
-108.0	-168.1	-168.0	-139.9	-168.0	-128.2	-157.3	-157.3	-102.0	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
1.450	0.317	4.438	0.334	0.151	1.450	2.947	1.082	1.353	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
11.8	66.9	11.8	-52.3	11.8	-113.7	-40.9	-142.7	-3.0	x-coord. of source (m)
-91.4	-151.6	-151.4	-125.3	-151.4	-128.2	-157.3	-157.3	-87.4	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
2.175	1.712	3.060	0.680	0.452	0.145	0.842	1.624	1.353	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
107.7	93.1	28.1	78.6	26.1	116.5	37.8	-67.2	-3.0	x-coord. of source (m)
-163.3	-137.0	-139.9	-110.8	-139.9	-99.9	-70.0	-84.6	-87.4	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
0.870	3.326	1.868	0.980	0.836	0.140	0.140	2.842	0.812	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
119.4	119.4	64.0	-84.0	64.0	-113.7	-40.9	-142.7	-49.5	x-coord. of source (m)
-148.7	-122.5	-125.3	-104.8	-125.3	-110.8	-139.9	-139.9	-58.3	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
3.335	4.434	2.024	0.153	2.582	1.740	0.421	0.541	1.082	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
160.1	140.6	78.6	-11.8	78.6	-113.7	-40.9	-142.7	-40.9	x-coord. of source (m)
-134.2	-108.0	-110.8	-119.5	-110.8	-128.2	-157.3	-157.3	-142.7	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
2.175	2.651	2.180	0.459	2.110	1.885	1.544	0.135	0.135	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
186.4	186.4	55.2	-11.8	55.2	-113.7	-40.9	-142.7	-18.7	x-coord. of source (m)
-119.6	-182.4	-180.7	-180.7	-180.7	-128.2	-157.3	-157.3	-18.7	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)
2.465	0.158	0.156	0.165	0.151	1.740	2.806	0.812	2.571	total mass emitted (kg)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	6.980	sigm0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120	sigm0 at the source (m)
212.6	81.4	40.6	14.4	40.6	104.8	78.6	26.1	11.5	x-coord. of source (m)
-105.1	-171.8	-180.7	-166.1	-166.1	-96.3	-110.8	-139.9	-113.7	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	904.0	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	904.0	emission duration (s)

-99.9	-99.9	-99.9	-99.9	relative humidity (%)
300.00	300.00	300.00	300.00	temperature at level #1 (K)
2.00	2.00	2.00	2.00	measuring height for temperature #1 (m)
-99.90	-99.90	-99.90	-99.90	temperature at level #2 (K)
-99.90	-99.90	-99.90	-99.90	measuring height for temperature #2 (m)
5.00	5.00	5.00	5.00	wind speed (m/s) at a tower
2.00	2.00	2.00	2.00	measuring height for wind data (m)
5.40	5.40	5.40	5.40	domain-averaged wind speed (m/s)
160.0	160.0	160.0	160.0	domain-averaged wind direction (deg)
3.70	3.70	3.70	3.70	domain-averaged sigma-u (m/s)
-99.90	-99.90	-99.90	-99.90	domain-averaged sigma-theta (deg)
2.00	2.00	2.00	2.00	measuring ht for domain-avg wind speed (m)
160.0	160.0	160.0	160.0	averaging time for domain-avg data (s)
0.076	0.076	0.076	0.076	wind speed power law exponent
0.0300	0.0300	0.0300	0.0300	surface roughness (m)
-99.9000	-99.9000	-99.9000	-99.9000	friction velocity (m)
-99.9000	-99.9000	-99.9000	-99.9000	inverse Monin-Obukhov length (l/m)
0.18	0.18	0.18	0.18	albedo
0.50	0.50	0.50	0.50	moisture availability
0.50	0.50	0.50	0.50	Bowen ratio
-99.9	-99.9	-99.9	-99.9	mixing height (m)
-99.9	-99.9	-99.9	-99.9	cloud cover (%)
-99.9	-99.9	-99.9	-99.9	P-G stability class
360.0	360.0	360.0	360.0	averaging time for concentration (s)
1.50	1.50	1.50	1.50	suggested receptor height (m)
0	0	0	0	no. of distances downwind
3	3	3	3	no. of lines-of-sight
-199.3	-199.3	-199.3	-199.3	x-coord. of 1st end-point for LOS1 (m)
-156.2	-156.2	-156.2	-156.2	y-coord. of 1st end-point for LOS1 (m)
587.9	587.9	587.9	587.9	x-coord. of 2nd end-point for LOS1 (m)
280.1	280.1	280.1	280.1	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (ug/m**2)
-9.990E+01	1.000E+03	-9.990E+01	-9.990E+01	LOS integrated dosage (ug-s/m**2)
-238.0	-238.0	-238.0	-238.0	x-coord. of 1st end-point for LOS1 (m)
-86.2	-86.2	-86.2	-86.2	y-coord. of 1st end-point for LOS1 (m)
549.1	549.1	549.1	549.1	x-coord. of 2nd end-point for LOS1 (m)
350.1	350.1	350.1	350.1	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (ug/m**2)
1.920E+05	7.500E+04	1.530E+05	9.300E+04	LOS integrated dosage (ug-s/m**2)
-276.8	-276.8	-276.8	-276.8	x-coord. of 1st end-point for LOS1 (m)
-16.2	-16.2	-16.2	-16.2	y-coord. of 1st end-point for LOS1 (m)
510.3	510.3	510.3	510.3	x-coord. of 2nd end-point for LOS1 (m)
420.1	420.1	420.1	420.1	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (ug/m**2)
1.650E+05	3.800E+04	1.070E+05	5.200E+04	LOS integrated dosage (ug-s/m**2)

The Development Test 1 of 8mm Smoke Cartridge (M0010, 3 Projectile, DTIR1)

15 : number of trials included in DCA		16 : time zone designation		17 : latitude (deg)		18 : longitude (deg)		19 : trial ID		20 : trial ID		21 : trial ID		22 : trial ID		23 : trial ID		24 : trial ID		25 : trial ID		26 : trial ID		27 : trial ID		28 : trial ID		29 : trial ID		30 : trial ID		31 : trial ID		32 : trial ID		33 : trial ID		34 : trial ID		35 : trial ID		36 : trial ID		37 : trial ID		38 : trial ID		39 : trial ID		40 : trial ID		41 : trial ID		42 : trial ID		43 : trial ID		44 : trial ID		45 : trial ID		46 : trial ID		47 : trial ID		48 : trial ID		49 : trial ID		50 : trial ID		51 : trial ID		52 : trial ID		53 : trial ID		54 : trial ID		55 : trial ID		56 : trial ID		57 : trial ID		58 : trial ID		59 : trial ID		60 : trial ID		61 : trial ID		62 : trial ID		63 : trial ID		64 : trial ID		65 : trial ID		66 : trial ID		67 : trial ID		68 : trial ID		69 : trial ID		70 : trial ID		71 : trial ID		72 : trial ID		73 : trial ID		74 : trial ID		75 : trial ID		76 : trial ID		77 : trial ID		78 : trial ID		79 : trial ID		80 : trial ID		81 : trial ID		82 : trial ID		83 : trial ID		84 : trial ID		85 : trial ID		86 : trial ID		87 : trial ID		88 : trial ID		89 : trial ID		90 : trial ID		91 : trial ID		92 : trial ID		93 : trial ID		94 : trial ID		95 : trial ID		96 : trial ID		97 : trial ID		98 : trial ID		99 : trial ID		100 : trial ID																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
102A	102B	102C	102D	102E	102F	102G	102H	102I	102J	102K	102L	102M	102N	102O	102P	102Q	102R	102S	102T	102U	102V	102W	102X	102Y	102Z	102AA	102AB	102AC	102AD	102AE	102AF	102AG	102AH	102AI	102AJ	102AK	102AL	102AM	102AN	102AO	102AP	102AQ	102AR	102AS	102AT	102AU	102AV	102AW	102AX	102AY	102AZ	102BA	102BB	102BC	102BD	102BE	102BF	102BG	102BH	102BI	102BJ	102BK	102BL	102BM	102BN	102BO	102BP	102BQ	102BR	102BS	102BT	102BU	102BV	102BW	102BX	102BY	102BZ	102CA	102CB	102CC	102CD	102CE	102CF	102CG	102CH	102CI	102CJ	102CK	102CL	102CM	102CN	102CO	102CP	102CQ	102CR	102CS	102CT	102CU	102CV	102CW	102CX	102CY	102CZ	102DA	102DB	102DC	102DD	102DE	102DF	102DG	102DH	102DI	102DJ	102DK	102DL	102DM	102DN	102DO	102DP	102DQ	102DR	102DS	102DT	102DU	102DV	102DW	102DX	102DY	102DZ	102EA	102EB	102EC	102ED	102EE	102EF	102EG	102EH	102EI	102EJ	102EK	102EL	102EM	102EN	102EO	102EP	102EQ	102ER	102ES	102ET	102EU	102EV	102EW	102EX	102EY	102EZ	102FA	102FB	102FC	102FD	102FE	102FF	102FG	102FH	102FI	102FJ	102FK	102FL	102FM	102FN	102FO	102FP	102FQ	102FR	102FS	102FT	102FU	102FV	102FW	102FX	102FY	102FZ	102GA	102GB	102GC	102GD	102GE	102GF	102GG	102GH	102GI	102GJ	102GK	102GL	102GM	102GN	102GO	102GP	102GQ	102GR	102GS	102GT	102GU	102GV	102GW	102GX	102GY	102GZ	102HA	102HB	102HC	102HD	102HE	102HF	102HG	102HH	102HI	102HJ	102HK	102HL	102HM	102HN	102HO	102HP	102HQ	102HR	102HS	102HT	102HU	102HV	102HW	102HX	102HY	102HZ	102IA	102IB	102IC	102ID	102IE	102IF	102IG	102IH	102II	102IJ	102IK	102IL	102IM	102IN	102IO	102IP	102IQ	102IR	102IS	102IT	102IU	102IV	102IW	102IX	102IY	102IZ	102JA	102JB	102JC	102JD	102JE	102JF	102JG	102JH	102JI	102JJ	102JK	102JL	102JM	102JN	102JO	102JP	102JQ	102JR	102JS	102JT	102JU	102JV	102JW	102JX	102JY	102JZ	102KA	102KB	102KC	102KD	102KE	102KF	102KG	102KH	102KI	102KJ	102KK	102KL	102KM	102KN	102KO	102KP	102KQ	102KR	102KS	102KT	102KU	102KV	102KW	102KX	102KY	102KZ	102LA	102LB	102LC	102LD	102LE	102LF	102LG	102LH	102LI	102LJ	102LK	102LM	102LN	102LO	102LP	102LQ	102LR	102LS	102LT	102LU	102LV	102LW	102LX	102LY	102LZ	102MA	102MB	102MC	102MD	102ME	102MF	102MG	102MH	102MI	102MJ	102MK	102ML	102MN	102MO	102MP	102MQ	102MR	102MS	102MT	102MU	102MV	102MW	102MX	102MY	102MZ	102NA	102NB	102NC	102ND	102NE	102NF	102NG	102NH	102NI	102NJ	102NK	102NL	102NM	102NO	102NP	102NQ	102NR	102NS	102NT	102NU	102NV	102NW	102NX	102NY	102NZ	102OA	102OB	102OC	102OD	102OE	102OF	102OG	102OH	102OI	102OJ	102OK	102OL	102OM	102ON	102OO	102OP	102OQ	102OR	102OS	102OT	102OU	102OV	102OW	102OX	102OY	102OZ	102PA	102PB	102PC	102PD	102PE	102PF	102PG	102PH	102PI	102PJ	102PK	102PL	102PM	102PN	102PO	102PP	102PQ	102PR	102PS	102PT	102PU	102PV	102PW	102PX	102PY	102PZ	102QA	102QB	102QC	102QD	102QE	102QF	102QG	102QH	102QI	102QJ	102QK	102QL	102QM	102QN	102QO	102QP	102QQ	102QR	102QS	102QT	102QU	102QV	102QW	102QX	102QY	102QZ	102RA	102RB	102RC	102RD	102RE	102RF	102RG	102RH	102RI	102RJ	102RK	102RL	102RM	102RN	102RO	102RP	102RQ	102RR	102RS	102RT	102RU	102RV	102RW	102RX	102RY	102RZ	102SA	102SB	102SC	102SD	102SE	102SF	102SG	102SH	102SI	102SJ	102SK	102SL	102SM	102SN	102SO	102SP	102SQ	102SR	102SS	102ST	102SU	102SV	102SW	102SX	102SY	102SZ	102TA	102TB	102TC	102TD	102TE	102TF	102TG	102TH	102TI	102TJ	102TK	102TL	102TM	102TN	102TO	102TP	102TQ	102TR	102TS	102TT	102TU	102TV	102TW	102TX	102TY	102TZ	102UA	102UB	102UC	102UD	102UE	102UF	102UG	102UH	102UI	102UJ	102UK	102UL	102UM	102UN	102UO	102UP	102UQ	102UR	102US	102UT	102UU	102UV	102UW	102UX	102UY	102UZ	102VA	102VB	102VC	102VD	102VE	102VF	102VG	102VH	102VI	102VJ	102VK	102VL	102VM	102VN	102VO	102VP	102VQ	102VR	102VS	102VT	102VU	102VV	102VW	102VX	102VY	102VZ	102WA	102WB	102WC	102WD	102WE	102WF	102WG	102WH	102WI	102WJ	102WK	102WL	102WM	102WN	102WO	102WP	102WQ	102WR	102WS	102WT	102WU	102WV	102WW	102WX	102WY	102WZ	102XA	102XB	102XC	102XD	102XE	102XF	102XG	102XH	102XI	102XJ	102XK	102XL	102XM	102XN	102XO	102XP	102XQ	102XR	102XS	102XT	102XU	102XV	102XW	102XX	102XY	102XZ	102YA	102YB	102YC	102YD	102YE	102YF	102YG	102YH	102YI	102YJ	102YK	102YL	102YM	102YN	102YO	102YP	102YQ	102YR	102YS	102YT	102YU	102YV	102YW	102YX	102YY	102YZ	102ZA	102ZB	102ZC	102ZD	102ZE	102ZF	102ZG	102ZH	102ZI	102ZJ	102ZK	102ZL	102ZM	102ZN	102ZO	102ZP	102ZQ	102ZR	102ZS	102ZT	102ZU	102ZV	102ZW	102ZX	102ZY	102ZZ

The Development Test 1 of 81mm Smoke Cartridges (XM819, 3 projectiles, DT1X3)

7 : number of trials included in DOA

6 : time zone designation

5 : latitude (deg)

4 : longitude (deg)

3 : trial ID

2 : day

1 : month

0 : year

9 : hour

8 : minute

7 : second

6 : millisecond

5 : microsecond

4 : nanosecond

3 : picosecond

2 : femtosecond

1 : attosecond

0 : zeptosecond

9 : yoctosecond

8 : rontosecond

7 : quectosecond

6 : sextosecond

5 : septosecond

4 : octosecond

3 : nonasecond

2 : decasecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

9 : centisecond

8 : decimisecond

7 : centisecond

6 : decimisecond

5 : centisecond

4 : decimisecond

3 : centisecond

2 : decimisecond

1 : centisecond

0 : decimisecond

40.20	113.00	602A	702A	901A	902A	1101A	1102A
12	2	3	3	3	3	3	3
22	12	4	4	4	4	4	4
80	81	81	81	81	81	81	81
12	10	12	10	12	10	12	10
0	27	59	20	16	16	45	45
1	1	1	1	1	1	2	2
-81.4	16.5	-2.7	86.1	-61.8	-61.8	-61.8	-61.8
74.4	-62.9	-46.0	63.4	64.1	64.1	64.1	64.1
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0
18.881	18.330	18.030	4.237	11.378	11.378	11.378	11.378
13.600	17.800	22.400	8.000	16.400	16.400	16.400	16.400
13.600	17.800	22.400	8.000	16.400	16.400	16.400	16.400
0.120	0.120	0.120	54.4	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-69.3	69.3	69.3	69.3	69.3
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0
-99.900	8.961	-99.900	6.161	-99.900	-99.900	-99.900	-99.900
-99.900	-99.900	-99.900	9.700	-99.900	-99.900	-99.900	-99.900
-99.900	-99.900	-99.900	9.700	-99.900	-99.900	-99.900	-99.900
0.120	0.120	0.120	10.6	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-81.0	81.0	81.0	81.0	81.0
-99.9	-99.9	-99.9	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0
-99.900	-99.900	-99.900	5.579	-99.900	-99.900	-99.900	-99.900
-99.900	-99.900	-99.900	12.600	-99.900	-99.900	-99.900	-99.900
-99.900	-99.900	-99.900	0.120	-99.9	-99.9	-99.9	-99.9
0.120	0.120	0.120	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	300.00	300.00	300.00	300.00	300.00
300.00	300.00	300.00	2.00	2.00	2.00	2.00	2.00
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
329.0	133.0	179.0	155.0	359.0	359.0	359.0	359.0
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
12.70	16.80	27.60	8.10	17.20	17.20	17.20	17.20
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
690.0	639.0	502.0	614.0	585.0	585.0	585.0	585.0
0.068	0.068	0.079	0.088	0.074	0.074	0.074	0.074
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900	-99.900
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000
0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
0	0	0	0	0	0	0	0
5	5	5	5	5	5	5	5
-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7
-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7
1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2
658.5	658.5	658.5	658.5	658.5	658.5	658.5	658.5
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
9.900E+01	9.900E+01	9.900E+01	1.840E+05	-9.900E+01	-9.900E+01	-9.900E+01	-9.900E+01
-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6
173.7	173.7	173.7	173.7	173.7	173.7	173.7	173.7
1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4
553.5	553.5	553.5	553.5	553.5	553.5	553.5	553.5
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
2.160E+05	-9.900E+01	-9.900E+01	-9.900E+01	-9.900E+04	-9.900E+04	-9.900E+04	-9.900E+04
-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9
421.8	421.8	421.8	421.8	421.8	421.8	421.8	421.8
-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9

-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	9.000E+04	LOS integrated dosage (mg-s/m ³ -2)	(m)
-21.7	-21.7	-21.7	-21.7	-21.7	-21.7	-21.7	121.7	x-coord. of 1st end-point for LOS1	(m)
142.3	142.3	142.3	142.3	142.3	142.3	142.3	408.7	y-coord. of 1st end-point for LOS1	(m)
408.7	408.7	408.7	408.7	408.7	408.7	408.7	768.2	x-coord. of 2nd end-point for LOS1	(m)
-768.2	-768.2	-768.2	-768.2	-768.2	-768.2	-768.2	-99.9	y-coord. of 2nd end-point for LOS1	(m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (mg/m ³ -2)	(m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	LOS integrated dosage (mg-s/m ³ -2)	(m)
-78.6	-78.6	-78.6	-78.6	-78.6	-78.6	-78.6	-78.6	x-coord. of 1st end-point for LOS1	(m)
110.8	110.8	110.8	110.8	110.8	110.8	110.8	395.5	y-coord. of 1st end-point for LOS1	(m)
395.5	395.5	395.5	395.5	395.5	395.5	395.5	775.5	x-coord. of 2nd end-point for LOS1	(m)
-775.5	-775.5	-775.5	-775.5	-775.5	-775.5	-775.5	-99.9	y-coord. of 2nd end-point for LOS1	(m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (mg/m ³ -2)	(m)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	LOS integrated dosage (mg-s/m ³ -2)	(m)

The Development Test 1 of 8mm Smoke Cartridges (M33A2, 1 Proj, 11.0, DT1H)

1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150
1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150
1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150
1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150

The Development Test I of Bluss Smoke Cartridges (M375A2, 3 projectiles, DTIM3)

10 : number of trials included in DOA
 6 : time zone designation
 40.20 : latitude (deg)
 113.00 : longitude (deg)

6018	6028	6048	6058	7018	7028	8018	8028	11018	11028	trial ID
12	12	12	12	2	2	3	3	3	3	month
17	22	23	23	5	12	12	4	5	5	day
80	80	80	80	81	81	81	81	81	81	year
15	15	15	15	15	12	11	13	12	12	hour
37	34	42	34	9	9	46	10	35	45	minute
3	3	3	3	3	3	3	3	3	3	no. of sources
-48.8	-58.7	-80.8	-13.0	-77.9	-46.1	-12.2	17.1	-88.0	-101.1	x-coord. of source (m)
32.4	23.5	26.1	-30.1	-94.6	-104.5	-114.2	-36.6	37.0	29.7	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	emission rate (g/s)
7.180	8.100	6.800	6.080	5.110	5.510	5.510	5.300	4.660	4.380	total mass emitted (kg)
1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	sigm0 at the source (m)
0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	sigm0 at the source (m)
1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	sigm0 at the source (m)
-64.6	-47.2	-35.3	-31.4	-35.3	-31.4	-18.3	-25.9	-59.6	-33.1	x-coord. of source (m)
13.4	25.3	17.7	-22.3	-107.6	-94.0	-89.3	-71.4	23.1	31.8	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	emission duration (s)
7.180	8.100	6.800	6.080	5.110	5.510	5.510	5.300	4.660	4.380	total mass emitted (kg)
1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	sigm0 at the source (m)
0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	sigm0 at the source (m)
1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	sigm0 at the source (m)
-41.3	-13.4	-16.3	-101.4	-88.7	-46.7	-10.9	-25.6	-102.8	-89.2	x-coord. of source (m)
22.9	13.4	18.1	-16.3	-21.7	-46.7	-10.9	-25.6	49.3	24.9	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	emission rate (g/s)
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	emission duration (s)
7.180	8.100	6.800	6.080	5.110	5.510	5.510	5.300	4.660	4.380	total mass emitted (kg)
1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	1.630	sigm0 at the source (m)
0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	0.930	sigm0 at the source (m)
1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	sigm0 at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	ambient pressure (atm)
300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00	relative humidity (%)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	temperature at level #1 (K)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	temperature at level #2 (K)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	measuring height for temperature #1 (m)
1.60	1.60	1.60	1.60	1.60	1.60	1.60	1.60	1.60	1.60	measuring height for temperature #2 (m)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	wind speed (m/s) at a tower
1.40	1.80	1.60	2.00	2.00	2.00	2.00	2.00	2.00	2.60	measuring height for wind data (m)
319.0	19.0	350.0	205.0	14.0	126.0	157.0	180.0	1.0	8.0	domain-averaged wind speed (m/s)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	domain-averaged wind direction (deg)
11.40	5.40	6.80	3.40	3.30	27.80	3.30	13.90	10.90	7.70	domain-averaged sigma-u
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	domain-averaged sigma-theta (deg)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	measuring ht for domain-avg phi (deg)
308.0	123.0	149.0	88.0	296.0	172.0	165.0	187.0	134.0	164.0	averaging time for domain-avg wind speed (m)
0.045	0.092	0.271	0.147	0.080	0.076	0.050	0.101	0.084	0.048	wind speed power law exponent
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	surface roughness (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	friction velocity (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	inverse Monin-Obukhov length (1/m)
0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	albedo
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	moisture availability
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	Poussin ratio
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	mixing height (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	cloud cover (%)
120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	P-G stability class
1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	averaging time for concentration (s)
0	0	0	0	0	0	0	0	0	0	suggested receptor height (m)
5	5	5	5	5	5	5	5	5	5	no. of distances downwind
-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	x-coord. of 1st end-point for LOS1 (m)
-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	y-coord. of 1st end-point for LOS1 (m)
1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	1064.2	x-coord. of 2nd end-point for LOS1 (m)
658.5	658.5	658.5	658.5	658.5	658.5	658.5	658.5	658.5	658.5	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)
-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	LOS integrated dosage (mg-s/m**2)
-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	x-coord. of 1st end-point for LOS1 (m)
-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	y-coord. of 1st end-point for LOS1 (m)
1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	1122.4	x-coord. of 2nd end-point for LOS1 (m)
553.5	553.5	553.5	553.5	553.5	553.5	553.5	553.5	553.5	553.5	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)
9.500E+04	1.500E+04	2.300E+04	-9.990E+01	-9.990E+01	-9.990E+01	1.150E+05	2.040E+05	1.900E+04	4.500E+04	LOS integrated dosage (mg-s/m**2)
-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	-152.9	x-coord. of 1st end-point for LOS1 (m)
69.6	69.6	69.6	69.6	69.6	69.6	69.6	69.6	69.6	69.6	y-coord. of 1st end-point for LOS1 (m)
421.8	421.8	421.8	421.8	421.8	421.8	421.8	421.8	421.8	421.8	x-coord. of 2nd end-point for LOS1 (m)
-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	-760.9	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)

-9.990E+01 3.800E+04 1.530E+05 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01
 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7
 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3
 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7
 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2
 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9
 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01
 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6
 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8
 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5
 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5
 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9
 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01
 1.660E+05 1.310E+05 1.660E+05 1.310E+05 1.660E+05 1.310E+05 1.660E+05 1.310E+05 1.660E+05 1.310E+05 1.660E+05 1.310E+05
 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7 -21.7
 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3 142.3
 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7 408.7
 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2 -768.2
 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9
 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01
 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6 -78.6
 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8 110.8
 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5 395.5
 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5 -775.5
 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9 -99.9
 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01
 LOS integrated dosage (mg/m³·2) x-coord. of 1st end-point for LOS1 (m) y-coord. of 1st end-point for LOS1 (m) x-coord. of 2nd end-point for LOS1 (m) y-coord. of 2nd end-point for LOS1 (m) LOS integrated dosage (mg/m³·2) x-coord. of 1st end-point for LOS1 (m) y-coord. of 1st end-point for LOS1 (m) x-coord. of 2nd end-point for LOS1 (m) y-coord. of 2nd end-point for LOS1 (m) LOS integrated dosage (mg/m³·2)

The Evaluation of the I8 Series Grenades (E81A1)

7 : number of trials included in DUA

6 : time zone designation

5 : latitude (deg)

4 : longitude (deg)

BB1 : trial ID

BB2 : month

BB3 : day

BB4 : year

BB5 : hour

BB6 : minute

BB7 : no. of sources

BB8 : x-coord. of source (m)

BB9 : y-coord. of source (m)

BB10 : source elevation (m)

BB11 : emission rate (g/s)

BB12 : emission duration (s)

BB13 : total mass emitted (kg)

BB14 : sigm0 at the source (m)

BB15 : sigm1 at the source (m)

BB16 : sigm2 at the source (m)

BB17 : ambient pressure (atm)

BB18 : relative humidity (%)

BB19 : temperature at level #1 (K)

BB20 : measuring height for temperature #1 (m)

BB21 : temperature at level #2 (K)

BB22 : measuring height for temperature #2 (m)

BB23 : wind speed (m/s) at a tower

BB24 : measuring height for wind data (m)

BB25 : domain-averaged wind speed (m/s)

BB26 : domain-averaged wind direction (deg)

BB27 : domain-averaged sigma-u (m/s)

BB28 : domain-averaged sigma-theta (deg)

BB29 : domain-averaged sigma-phi (deg)

BB30 : measuring ht for domain-avg wind speed (m)

BB31 : averaging time for domain-avg data (s)

BB32 : wind speed power law exponent

BB33 : surface roughness (m)

BB34 : friction velocity (m)

BB35 : inverse Monin-Obukhov length (1/m)

BB36 : albedo

BB37 : moisture availability

BB38 : Bowen ratio

BB39 : mixing height (m)

BB40 : P-G cloud cover (%)

BB41 : P-G stability class

BB42 : averaging time for concentration (s)

BB43 : suggested receptor height (m)

BB44 : no. of distances downwind

BB45 : no. of lines-of-sight

BB46 : x-coord. of 1st end-point for LOS1 (m)

BB47 : y-coord. of 1st end-point for LOS1 (m)

BB48 : x-coord. of 2nd end-point for LOS1 (m)

BB49 : y-coord. of 2nd end-point for LOS1 (m)

BB50 : LOS integrated conc. (mg/m**2)

BB51 : LOS integrated dosage (mg-s/m**2)

BB52 : x-coord. of 1st end-point for LOS1 (m)

BB53 : y-coord. of 1st end-point for LOS1 (m)

BB54 : x-coord. of 2nd end-point for LOS1 (m)

BB55 : y-coord. of 2nd end-point for LOS1 (m)

BB56 : LOS integrated conc. (mg/m**2)

BB57 : LOS integrated dosage (mg-s/m**2)

BB58 : x-coord. of 1st end-point for LOS1 (m)

BB59 : y-coord. of 1st end-point for LOS1 (m)

BB60 : x-coord. of 2nd end-point for LOS1 (m)

BB61 : y-coord. of 2nd end-point for LOS1 (m)

BB62 : LOS integrated conc. (mg/m**2)

BB63 : LOS integrated dosage (mg-s/m**2)

BB64 : x-coord. of 1st end-point for LOS1 (m)

BB65 : y-coord. of 1st end-point for LOS1 (m)

BB66 : x-coord. of 2nd end-point for LOS1 (m)

BB67 : y-coord. of 2nd end-point for LOS1 (m)

BB68 : LOS integrated conc. (mg/m**2)

BB69 : LOS integrated dosage (mg-s/m**2)

BB70 : x-coord. of 1st end-point for LOS1 (m)

BB71 : y-coord. of 1st end-point for LOS1 (m)

BB72 : x-coord. of 2nd end-point for LOS1 (m)

BB73 : y-coord. of 2nd end-point for LOS1 (m)

BB74 : LOS integrated conc. (mg/m**2)

BB75 : LOS integrated dosage (mg-s/m**2)

BB76 : x-coord. of 1st end-point for LOS1 (m)

BB77 : y-coord. of 1st end-point for LOS1 (m)

BB78 : x-coord. of 2nd end-point for LOS1 (m)

BB79 : y-coord. of 2nd end-point for LOS1 (m)

BB80 : LOS integrated conc. (mg/m**2)

BB81 : LOS integrated dosage (mg-s/m**2)

BB82 : x-coord. of 1st end-point for LOS1 (m)

BB83 : y-coord. of 1st end-point for LOS1 (m)

BB84 : x-coord. of 2nd end-point for LOS1 (m)

BB85 : y-coord. of 2nd end-point for LOS1 (m)

BB86 : LOS integrated conc. (mg/m**2)

BB87 : LOS integrated dosage (mg-s/m**2)

The Evaluation of the 18 Series Grenades (L81B1)

6 : number of trials included in DUA

6 : time zone designation

6 : latitude (deg)

6 : longitude (deg)

BB11	BB12	BB13	BB14	BB15	BB16	BB18	trial ID
40.20	113.00	8811	6	6	6	16	month
81	10	81	10	10	81	11	day
11	8	11	8	8	11	1	year
1	1	1	1	1	1	1	hour
39.2	-56.4	39.2	-30.4	39.2	-30.4	39.2	no. of sources
-81.2	71.4	-81.2	86.0	-81.2	86.0	-81.2	x-coord. of source (m)
-99.9	0.00	-99.9	0.00	-99.9	0.00	-99.9	y-coord. of source (m)
0.840	0.887	0.840	0.859	0.840	0.840	0.840	source elevation (m)
7.544	3.468	7.544	9.161	7.544	9.161	7.544	emission rate (g/s)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	total mass emitted (kg)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	sig0 at the source (m)
300.00	300.00	300.00	300.00	300.00	300.00	300.00	sig0 at the source (m)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	ambient pressure (atm)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	relative humidity (%)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	temperature at level #1 (K)
3.10	2.70	3.10	3.80	3.10	3.80	3.10	measuring height for temperature #1 (m)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	temperature at level #2 (K)
171.0	171.0	171.0	171.0	171.0	171.0	171.0	measuring height for temperature #2 (m)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	wind speed (m/s) at a tower
21.50	16.70	21.50	26.00	21.50	26.00	21.50	measuring height for wind data (m)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	domain-averaged wind speed (m/s)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	domain-averaged wind direction (deg)
361.0	275.0	361.0	281.0	361.0	281.0	361.0	domain-averaged sigma-u (m/s)
0.102	0.102	0.102	0.067	0.102	0.067	0.102	domain-averaged sigma-theta (deg)
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	domain-averaged sigma-phi (deg)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	measuring ht for domain-avg wind speed (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	averaging time for domain-avg data (s)
0.18	0.18	0.18	0.18	0.18	0.18	0.18	wind speed power law exponent
0.50	0.50	0.50	0.50	0.50	0.50	0.50	surface roughness (m)
0.50	0.50	0.50	0.50	0.50	0.50	0.50	inverse Monin-Obukhov length (1/m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	albedo
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	moisture availability
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	Bowen ratio
199.0	199.0	199.0	199.0	199.0	199.0	199.0	mixing height (m)
1.00	1.00	1.00	1.00	1.00	1.00	1.00	cloud cover (%)
0	0	0	0	0	0	0	P-G stability class
2	2	2	2	2	2	2	averaging time for concentration (s)
-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	-247.7	suggested receptor height (m)
-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	-68.7	no. of distances downwind
189.6	189.6	189.6	189.6	189.6	189.6	189.6	no. of lines-of-sight
173.7	173.7	173.7	173.7	173.7	173.7	173.7	x-coord. of 1st end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	y-coord. of 1st end-point for LOS1 (m)
1.530E+04	4.190E+04	3.000E+04	3.590E+04	3.520E+04	1.890E+04	1.890E+04	x-coord. of 2nd end-point for LOS1 (m)
-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	-189.6	y-coord. of 2nd end-point for LOS1 (m)
-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	-173.7	LOS integrated dosage (mg/m**2)
247.7	247.7	247.7	247.7	247.7	247.7	247.7	x-coord. of 1st end-point for LOS1 (m)
68.7	68.7	68.7	68.7	68.7	68.7	68.7	y-coord. of 1st end-point for LOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	x-coord. of 2nd end-point for LOS1 (m)
-9.990E+01	-9.990E+01	1.720E+04	1.200E+04	9.700E+03	3.190E+04	3.190E+04	y-coord. of 2nd end-point for LOS1 (m)
							LOS integrated dosage (mg/m**2)

The Evaluation of the 19 Series Grenades (L81C1)

6 : number of trials included in DUA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

8821	8822	8825	8826	8828	8830
6	6	6	6	6	6
8	10	10	10	16	17
81	81	81	81	81	17
13	10	13	14	11	17
25	37	37	56	22	12
1	1	1	1	1	5
34.0	-25.3	-25.3	34.0	-20.9	1
-84.0	88.9	88.9	-84.0	91.3	1
0.00	0.00	0.00	0.00	0.00	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
126.0	126.0	126.0	126.0	126.0	1
0.820	0.897	0.840	0.859	0.859	1
4.144	5.326	7.128	5.557	4.384	1
13.734	13.320	12.449	13.225	13.859	1
0.120	0.120	0.120	0.120	0.120	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
300.00	300.00	300.00	300.00	300.00	1
2.00	2.00	2.00	2.00	2.00	1
-99.90	-99.90	-99.90	-99.90	-99.90	1
-99.90	-99.90	-99.90	-99.90	-99.90	1
3.90	3.60	4.00	5.10	7.30	1
2.00	2.00	2.00	2.00	2.00	1
3.90	3.60	4.00	5.10	7.30	1
175.0	350.0	342.0	349.0	354.0	1
-99.90	-99.90	-99.90	-99.90	-99.90	1
16.00	17.90	11.50	6.50	6.70	1
-99.90	-99.90	-99.90	-99.90	-99.90	1
2.00	2.00	2.00	2.00	2.00	1
236.0	600.0	223.0	223.0	230.0	1
0.080	0.020	0.067	0.075	0.116	1
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	1
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	1
0.18	0.18	0.18	0.18	0.18	1
0.50	0.50	0.50	0.50	0.50	1
0.50	0.50	0.50	0.50	0.50	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
126.0	126.0	126.0	126.0	126.0	1
1.00	1.00	1.00	1.00	1.00	1
2	2	2	2	2	1
-247.7	-247.7	-247.7	-247.7	-247.7	1
-68.7	-68.7	-68.7	-68.7	-68.7	1
189.6	189.6	189.6	189.6	189.6	1
173.7	173.7	173.7	173.7	173.7	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
3.670E+03	3.660E+04	2.850E+04	4.650E+04	1.820E+04	1
-189.6	-189.6	-189.6	-189.6	-189.6	1
-173.7	-173.7	-173.7	-173.7	-173.7	1
247.7	247.7	247.7	247.7	247.7	1
68.7	68.7	68.7	68.7	68.7	1
-99.9	-99.9	-99.9	-99.9	-99.9	1
1.870E+04	1.770E+04	1.100E+04	2.230E+04	3.170E+04	1

BB30 : trial ID
 6 : month
 17 : day
 81 : year
 12 : hour
 5 : minute
 1 : no. of sources
 -20.9 : x-coord. of source (m)
 91.3 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 126.0 : emission duration (s)
 0.859 : total mass emitted (kg)
 4.384 : alpha at the source (m)
 13.859 : alpha at the source (m)
 0.120 : alpha at the source (m)
 -99.9 : relative humidity (%)
 300.00 : temperature at level #1 (K)
 2.00 : measuring height for temperature #1 (m)
 -99.90 : temperature at level #2 (K)
 -99.90 : measuring height for temperature #2 (m)
 3.30 : wind speed (m/s) at a tower
 2.00 : measuring height for wind data (m)
 3.30 : domain-averaged wind speed (m/s)
 354.0 : domain-averaged wind direction (deg)
 -99.90 : domain-averaged sigma-u (m/s)
 11.20 : domain-averaged sigma-theta (deg)
 -99.90 : domain-averaged sigma-phi (deg)
 2.00 : measuring ht for domain-avg wind speed (m)
 230.0 : averaging time for domain-avg wind speed (s)
 0.116 : wind speed power law exponent
 0.0300 : surface roughness (m)
 -99.9000 : friction velocity (m)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.18 : albedo
 0.50 : moisture availability
 0.50 : Bowen ratio
 -99.9 : mixing height (m)
 -99.9 : cloud cover (%)
 -99.9 : P-G stability class
 126.0 : averaging time for concentration (s)
 1.00 : suggested receptor height (m)
 0 : no. of distances downwind
 2 : no. of lines-of-sight
 -247.7 : x-coord. of 1st end-point for LOS1 (m)
 -68.7 : y-coord. of 1st end-point for LOS1 (m)
 189.6 : x-coord. of 2nd end-point for LOS1 (m)
 173.7 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 3.670E+04 : LOS integrated dosage (mg-s/m**2)
 -189.6 : x-coord. of 1st end-point for LOS1 (m)
 -173.7 : y-coord. of 1st end-point for LOS1 (m)
 247.7 : x-coord. of 2nd end-point for LOS1 (m)
 68.7 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 1.110E+04 : LOS integrated dosage (mg-s/m**2)

The Evaluation of the LA Series Grenades (L81D1)

2 : number of trials included in DWA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

BB32 : latitude (deg)

BB33 : longitude (deg)

BB34 : trial ID

BB35 : month

BB36 : day

BB37 : year

BB38 : hour

BB39 : minute

BB40 : no. of sources

BB41 : x-coord. of source (m)

BB42 : y-coord. of source (m)

BB43 : source elevation (m)

BB44 : emission rate (g/s)

BB45 : emission duration (s)

BB46 : total mass emitted (kg)

BB47 : sign0 at the source (m)

BB48 : sign1 at the source (m)

BB49 : sign2 at the source (m)

BB50 : ambient pressure (kpa)

BB51 : relative humidity (%)

BB52 : temperature at level #1 (K)

BB53 : measuring height for temperature #1 (m)

BB54 : temperature at level #2 (K)

BB55 : measuring height for temperature #2 (m)

BB56 : wind speed (m/s) at a tower

BB57 : measuring height for wind data (m)

BB58 : domain-averaged wind speed (m/s)

BB59 : domain-averaged wind direction (deg)

BB60 : domain-averaged sigma-u (m/s)

BB61 : domain-averaged sigma-theta (deg)

BB62 : domain-averaged sigma-phi (deg)

BB63 : measuring ht for domain-avg wind speed (m)

BB64 : averaging time for domain-avg data (s)

BB65 : wind speed power law exponent

BB66 : surface roughness (m)

BB67 : friction velocity (m)

BB68 : inverse Monin-Obukhov length (1/m)

BB69 : albedo

BB70 : moisture availability

BB71 : Bowen ratio

BB72 : mixing height (m)

BB73 : cloud cover (%)

BB74 : P-G stability class

BB75 : averaging time for concentration (s)

BB76 : suggested receptor height (m)

BB77 : no. of distances downwind

BB78 : no. of lines-of-sight

BB79 : x-coord. of lat end-point for LOS1 (m)

BB80 : y-coord. of lat end-point for LOS1 (m)

BB81 : x-coord. of 2nd end-point for LOS1 (m)

BB82 : y-coord. of 2nd end-point for LOS1 (m)

BB83 : LOS integrated dosage (mg/m**2)

BB84 : x-coord. of lat end-point for LOS1 (m)

BB85 : y-coord. of lat end-point for LOS1 (m)

BB86 : x-coord. of 2nd end-point for LOS1 (m)

BB87 : y-coord. of 2nd end-point for LOS1 (m)

BB88 : LOS integrated dosage (mg/m**2)

BB89 : x-coord. of lat end-point for LOS1 (m)

BB90 : y-coord. of lat end-point for LOS1 (m)

BB91 : x-coord. of 2nd end-point for LOS1 (m)

BB92 : y-coord. of 2nd end-point for LOS1 (m)

BB93 : LOS integrated dosage (mg/m**2)

BB94 : x-coord. of lat end-point for LOS1 (m)

BB95 : y-coord. of lat end-point for LOS1 (m)

BB96 : x-coord. of 2nd end-point for LOS1 (m)

BB97 : y-coord. of 2nd end-point for LOS1 (m)

BB98 : LOS integrated dosage (mg/m**2)

BB99 : x-coord. of lat end-point for LOS1 (m)

BB100 : y-coord. of lat end-point for LOS1 (m)

BB101 : x-coord. of 2nd end-point for LOS1 (m)

BB102 : y-coord. of 2nd end-point for LOS1 (m)

BB103 : LOS integrated dosage (mg/m**2)

BB104 : x-coord. of lat end-point for LOS1 (m)

BB105 : y-coord. of lat end-point for LOS1 (m)

BB106 : x-coord. of 2nd end-point for LOS1 (m)

BB107 : y-coord. of 2nd end-point for LOS1 (m)

BB108 : LOS integrated dosage (mg/m**2)

The Evaluation of the 18 Series Grenades (L8112)

6 : number of trials included in DDA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

BB41	BB42	BB43	BB44	BB45	BB46
6	6	6	6	6	6
16	16	16	16	16	16
81	81	81	81	81	81
8	8	10	10	8	8
4	56	52	21	30	10
12	12	12	12	12	12
67.7	64.2	57.3	70.2	62.4	62.4
-118.0	-119.9	-123.7	-116.6	-120.9	-120.9
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
6.053	3.942	3.468	3.468	3.420	3.420
15.518	16.183	19.992	19.992	13.932	13.932
97.6	34.2	90.8	38.7	92.9	92.9
-14.0	-93.9	-152.9	-87.4	-147.4	-147.4
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
0.381	9.239	3.579	3.579	1.551	1.551
16.652	13.859	19.972	19.972	14.251	14.251
0.120	0.120	0.120	0.120	0.120	0.120
-126.4	73.3	58.5	-133.1	-129.4	-129.4
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
6.656	8.656	6.887	6.887	5.787	5.787
14.231	16.622	19.086	19.086	13.126	13.126
0.120	0.120	0.120	0.120	0.120	0.120
107.3	24.5	101.7	25.8	102.8	102.8
-146.8	-91.1	-156.0	-84.3	-150.2	-150.2
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
2.517	11.506	6.993	6.993	4.004	4.004
16.465	12.044	19.047	19.047	13.775	13.775
0.120	0.120	0.120	0.120	0.120	0.120
88.5	43.3	80.6	48.9	83.7	83.7
-139.6	-88.3	-147.9	-92.4	-142.9	-142.9
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
3.267	6.692	3.267	0.056	0.949	0.949
16.333	15.253	20.290	20.290	14.314	14.314
0.120	0.120	0.120	0.120	0.120	0.120
67.7	64.2	57.3	70.2	62.4	62.4
-118.0	-119.9	-123.7	-116.6	-120.9	-120.9
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
10.995	1.831	10.096	10.096	7.933	7.933
12.511	16.556	17.600	17.600	11.922	11.922
0.120	0.120	0.120	0.120	0.120	0.120
61.1	70.7	49.9	77.6	55.8	55.8
-98.9	-139.0	-102.4	-137.9	-101.5	-101.5
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	251.0	251.0	251.0	251.0
0.820	0.801	0.820	0.801	0.813	0.813
14.612	7.383	15.507	15.507	11.575	11.575
7.986	14.931	13.085	13.085	8.474	8.474
0.120	0.120	0.120	0.120	0.120	0.120
61.5	70.4	50.3	77.2	56.1	56.1

BB48	trial ID
6	6
16	16
81	81
9	9
10	10
12	12
62.4	x-coord. of source (m)
-120.9	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
1.397	sigx0 at the source (m)
13.432	sigy0 at the source (m)
0.120	sigz0 at the source (m)
92.9	x-coord. of source (m)
-147.4	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
3.282	sigx0 at the source (m)
13.100	sigy0 at the source (m)
0.120	sigz0 at the source (m)
98.2	x-coord. of source (m)
-129.4	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
3.708	sigx0 at the source (m)
12.586	sigy0 at the source (m)
0.120	sigz0 at the source (m)
102.8	x-coord. of source (m)
-150.2	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
5.507	sigx0 at the source (m)
12.331	sigy0 at the source (m)
0.120	sigz0 at the source (m)
83.7	x-coord. of source (m)
-142.9	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
0.957	sigx0 at the source (m)
13.471	sigy0 at the source (m)
0.120	sigz0 at the source (m)
62.4	x-coord. of source (m)
-120.9	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
5.906	sigx0 at the source (m)
12.145	sigy0 at the source (m)
0.120	sigz0 at the source (m)
55.8	x-coord. of source (m)
-101.5	y-coord. of source (m)
0.00	source elevation (m)
-99.9	emission rate (g/s)
115.0	emission duration (s)
0.781	total mass emitted (kg)
9.704	sigx0 at the source (m)
9.392	sigy0 at the source (m)
0.120	sigz0 at the source (m)
56.1	x-coord. of source (m)

-78.8	-159.1	-79.9	-160.4	-81.0	-81.0
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	199.0	199.0	115.0	115.0
0.820	0.801	0.820	0.801	0.781	0.781
16.465	12.044	19.047	19.047	12.331	12.331
2.517	11.506	6.993	6.993	5.507	5.507
0.120	0.120	0.120	0.120	0.120	0.120
48.9	48.9	52.7	74.8	58.3	58.3
-108.7	-129.2	-115.4	-126.9	-111.5	-111.5
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	199.0	199.0	115.0	115.0
0.820	0.801	0.820	0.801	0.781	0.781
13.001	4.678	12.999	12.999	7.926	7.926
10.412	15.986	15.579	15.579	10.934	10.934
0.120	0.120	0.120	0.120	0.120	0.120
64.3	64.3	53.4	74.0	59.0	59.0
-168.8	-168.8	-69.0	-171.3	-71.1	-71.1
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	199.0	199.0	115.0	115.0
0.820	0.801	0.820	0.801	0.781	0.781
16.552	13.859	19.972	19.972	13.100	13.100
0.381	3.239	3.239	3.239	3.292	3.292
0.120	0.120	0.120	0.120	0.120	0.120
60.4	60.4	49.1	78.3	55.0	55.0
-88.8	-149.0	-91.2	-149.2	-91.3	-91.3
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	199.0	199.0	115.0	115.0
0.820	0.801	0.820	0.801	0.781	0.781
15.778	9.863	17.544	17.544	11.187	11.187
5.338	13.422	10.194	10.194	7.564	7.564
0.120	0.120	0.120	0.120	0.120	0.120
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
300.00	300.00	300.00	300.00	300.00	300.00
2.00	2.00	2.00	2.00	2.00	2.00
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
6.40	4.30	5.50	5.80	5.80	5.80
2.00	2.00	2.00	2.00	2.00	2.00
148.0	183.0	163.0	163.0	163.0	163.0
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
12.50	10.80	10.80	9.10	6.90	6.90
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
2.00	2.00	2.00	2.00	2.00	2.00
391.0	391.0	386.0	351.0	256.0	192.0
0.087	0.070	0.072	0.075	0.073	0.073
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300
-99.900	-99.900	-99.900	-99.900	-99.900	-99.900
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000
0.18	0.18	0.18	0.18	0.18	0.18
0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
251.0	251.0	199.0	199.0	126.0	115.0
1.00	1.00	1.00	1.00	1.00	1.00
0	0	0	0	0	0
2	2	2	2	2	2
-247.7	-247.7	-247.7	-247.7	-247.7	-247.7
-68.7	-68.7	-68.7	-68.7	-68.7	-68.7
189.6	189.6	189.6	189.6	189.6	189.6
173.7	173.7	173.7	173.7	173.7	173.7
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
1.934E+03	9.990E+01	1.838E+05	1.506E+05	1.237E+02	1.237E+02
-185.6	-185.6	-185.6	-185.6	-185.6	-185.6
247.7	247.7	247.7	247.7	247.7	247.7
68.7	68.7	68.7	68.7	68.7	68.7
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
2.978E+05	2.086E+05	3.166E+05	2.660E+05	4.909E+05	2.118E+05

The Evaluation of the 18 Series Grenades (L8A1, 8 Grenades, L8128)

6 : number of trials included in DDA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

87b : trial ID

6 : month

7 : day

82 : year

21 : hour

51 : minute

8 : no. of sources

62.6 : x-coord. of source (m)

-73.5 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

1.848 : sigx0 at the source (m)

16.883 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

51.4 : x-coord. of source (m)

-60.4 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

2.579 : sigx0 at the source (m)

16.767 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

37.2 : x-coord. of source (m)

-50.6 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

8.831 : sigx0 at the source (m)

15.528 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

20.9 : x-coord. of source (m)

-44.9 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

16.017 : sigx0 at the source (m)

13.231 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

68.0 : x-coord. of source (m)

-83.6 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

4.748 : sigx0 at the source (m)

16.286 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

72.6 : x-coord. of source (m)

-100.2 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

8.602 : sigx0 at the source (m)

14.502 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

12.2 : x-coord. of source (m)

-117.5 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

12.255 : sigx0 at the source (m)

11.730 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

68.4 : x-coord. of source (m)

-134.1 : y-coord. of source (m)

0.00 : source elevation (m)

-99.9 : emission rate (g/s)

101.0 : emission duration (s)

0.763 : total mass emitted (kg)

14.873 : sigx0 at the source (m)

8.158 : sigy0 at the source (m)

0.120 : sigz0 at the source (m)

-99.9 : ambient pressure (atm)

87b	88b	89b	810b	811b	812b
6	6	6	6	6	6
7	7	7	7	7	7
82	82	82	82	82	82
21	21	21	21	21	21
51	51	51	51	51	51
8	8	8	8	8	8
62.6	62.6	62.6	62.6	62.6	62.6
-73.5	-73.5	-73.5	-73.5	-73.5	-73.5
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
1.848	1.848	1.848	1.848	1.848	1.848
16.883	16.883	16.883	16.883	16.883	16.883
0.120	0.120	0.120	0.120	0.120	0.120
51.4	51.4	51.4	51.4	51.4	51.4
-60.4	-60.4	-60.4	-60.4	-60.4	-60.4
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
2.579	2.579	2.579	2.579	2.579	2.579
16.767	16.767	16.767	16.767	16.767	16.767
0.120	0.120	0.120	0.120	0.120	0.120
37.2	37.2	37.2	37.2	37.2	37.2
-50.6	-50.6	-50.6	-50.6	-50.6	-50.6
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
8.831	8.831	8.831	8.831	8.831	8.831
15.528	15.528	15.528	15.528	15.528	15.528
0.120	0.120	0.120	0.120	0.120	0.120
20.9	20.9	20.9	20.9	20.9	20.9
-44.9	-44.9	-44.9	-44.9	-44.9	-44.9
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
16.017	16.017	16.017	16.017	16.017	16.017
13.231	13.231	13.231	13.231	13.231	13.231
0.120	0.120	0.120	0.120	0.120	0.120
68.0	68.0	68.0	68.0	68.0	68.0
-83.6	-83.6	-83.6	-83.6	-83.6	-83.6
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
4.748	4.748	4.748	4.748	4.748	4.748
16.286	16.286	16.286	16.286	16.286	16.286
0.120	0.120	0.120	0.120	0.120	0.120
72.6	72.6	72.6	72.6	72.6	72.6
-100.2	-100.2	-100.2	-100.2	-100.2	-100.2
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
8.602	8.602	8.602	8.602	8.602	8.602
14.502	14.502	14.502	14.502	14.502	14.502
0.120	0.120	0.120	0.120	0.120	0.120
12.2	12.2	12.2	12.2	12.2	12.2
-117.5	-117.5	-117.5	-117.5	-117.5	-117.5
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
12.255	12.255	12.255	12.255	12.255	12.255
11.730	11.730	11.730	11.730	11.730	11.730
0.120	0.120	0.120	0.120	0.120	0.120
68.4	68.4	68.4	68.4	68.4	68.4
-134.1	-134.1	-134.1	-134.1	-134.1	-134.1
0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
101.0	101.0	101.0	101.0	101.0	101.0
0.763	0.763	0.763	0.763	0.763	0.763
14.873	14.873	14.873	14.873	14.873	14.873
8.158	8.158	8.158	8.158	8.158	8.158
0.120	0.120	0.120	0.120	0.120	0.120
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9

-128.7 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.859 : total mass emitted (kg)
 16.157 : sig0 at the source (m)
 5.170 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 71.5 : x-coord. of source (m)
 -94.6 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.859 : total mass emitted (kg)
 11.407 : sig0 at the source (m)
 12.556 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 66.0 : x-coord. of source (m)
 -113.4 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.859 : total mass emitted (kg)
 16.809 : sig0 at the source (m)
 2.286 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -117.5 : y-coord. of source (m)
 56.8 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.859 : total mass emitted (kg)
 15.014 : sig0 at the source (m)
 4.031 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -99.9 : ambient pressure (atm)
 -99.9 : relative humidity (%)
 300.00 : temperature at level #1 (K)
 -99.90 : temperature at level #2 (K)
 -99.90 : measuring height for temperature #1 (m)
 4.00 : wind speed (m/s) at a tower
 2.00 : measuring height for wind data (m)
 158.0 : domain-averaged wind speed (m/s)
 -99.90 : domain-averaged wind direction (deg)
 16.60 : domain-averaged sigma-u (m/s)
 2.00 : domain-averaged sigma-theta (deg)
 2.00 : domain-averaged sigma-phi (deg)
 2.00 : measuring ht for domain-avg wind speed (m)
 300.0 : averaging time for domain-avg wind speed (s)
 0.140 : wind speed power law exponent
 0.0300 : surface roughness (m)
 -99.900 : friction velocity (m/s)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.18 : albedo
 0.50 : moisture availability
 0.50 : Bowen ratio
 -99.9 : mixing height (m)
 -99.9 : cloud cover (%)
 -99 : P-G stability class
 300.0 : averaging time for concentration (s)
 2.00 : suggested receptor height (m)
 0 : no. of distances downwind
 5 : no. of lines-of-sight
 -173.8 : x-coord. of 1st end-point for LOS1 (m)
 -205.7 : y-coord. of 1st end-point for LOS1 (m)
 356.0 : x-coord. of 2nd end-point for LOS1 (m)
 76.0 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 -9.990E+01 : LOS integrated dosage (mg-s/m**2)
 -197.3 : x-coord. of 1st end-point for LOS1 (m)
 -161.5 : y-coord. of 1st end-point for LOS1 (m)
 332.5 : x-coord. of 2nd end-point for LOS1 (m)
 120.2 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 -9.990E+01 : LOS integrated dosage (mg-s/m**2)
 -220.7 : x-coord. of 1st end-point for LOS1 (m)
 -117.4 : y-coord. of 1st end-point for LOS1 (m)
 309.0 : x-coord. of 2nd end-point for LOS1 (m)
 164.3 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 3.580E+05 : LOS integrated dosage (mg-s/m**2)
 -244.2 : x-coord. of 1st end-point for LOS1 (m)
 -73.2 : y-coord. of 1st end-point for LOS1 (m)
 205.6 : x-coord. of 2nd end-point for LOS1 (m)

45.5 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.840 : total mass emitted (kg)
 16.328 : sig0 at the source (m)
 1.108 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -26.8 : x-coord. of source (m)
 78.7 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.840 : total mass emitted (kg)
 14.106 : sig0 at the source (m)
 6.424 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -32.3 : x-coord. of source (m)
 34.3 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.840 : total mass emitted (kg)
 16.863 : sig0 at the source (m)
 1.848 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -25.6 : x-coord. of source (m)
 56.8 : y-coord. of source (m)
 0.00 : source elevation (m)
 -99.9 : emission rate (g/s)
 101.0 : emission duration (s)
 0.840 : total mass emitted (kg)
 15.014 : sig0 at the source (m)
 4.031 : sig0 at the source (m)
 0.120 : sig0 at the source (m)
 -99.9 : ambient pressure (atm)
 -99.9 : relative humidity (%)
 300.00 : temperature at level #1 (K)
 -99.90 : temperature at level #2 (K)
 -99.90 : measuring height for temperature #1 (m)
 4.00 : wind speed (m/s) at a tower
 2.00 : measuring height for wind data (m)
 324.0 : domain-averaged wind speed (m/s)
 -99.90 : domain-averaged wind direction (deg)
 16.60 : domain-averaged sigma-u (m/s)
 2.00 : domain-averaged sigma-theta (deg)
 2.00 : domain-averaged sigma-phi (deg)
 2.00 : measuring ht for domain-avg wind speed (m)
 300.0 : averaging time for domain-avg wind speed (s)
 0.140 : wind speed power law exponent
 0.0300 : surface roughness (m)
 -99.900 : friction velocity (m/s)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.18 : albedo
 0.50 : moisture availability
 0.50 : Bowen ratio
 -99.9 : mixing height (m)
 -99.9 : cloud cover (%)
 -99 : P-G stability class
 300.0 : averaging time for concentration (s)
 2.00 : suggested receptor height (m)
 0 : no. of distances downwind
 5 : no. of lines-of-sight
 -173.8 : x-coord. of 1st end-point for LOS1 (m)
 -205.7 : y-coord. of 1st end-point for LOS1 (m)
 356.0 : x-coord. of 2nd end-point for LOS1 (m)
 76.0 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 7.700E+04 : LOS integrated dosage (mg-s/m**2)
 -197.3 : x-coord. of 1st end-point for LOS1 (m)
 -161.5 : y-coord. of 1st end-point for LOS1 (m)
 332.5 : x-coord. of 2nd end-point for LOS1 (m)
 120.2 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 1.230E+05 : LOS integrated dosage (mg-s/m**2)
 -220.7 : x-coord. of 1st end-point for LOS1 (m)
 -117.4 : y-coord. of 1st end-point for LOS1 (m)
 309.0 : x-coord. of 2nd end-point for LOS1 (m)
 164.3 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 2.560E+05 : LOS integrated dosage (mg-s/m**2)
 -244.2 : x-coord. of 1st end-point for LOS1 (m)
 -73.2 : y-coord. of 1st end-point for LOS1 (m)
 205.6 : x-coord. of 2nd end-point for LOS1 (m)

208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9	208.5 -99.9 -267.7 -29.1 262.1 252.6 -99.9
-9.990E+01	2.400E+04	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01	-9.990E+01
2.370E+05	2.370E+05	2.370E+05	2.370E+05	2.370E+05	2.370E+05	2.370E+05	2.370E+05
208.5	208.5	208.5	208.5	208.5	208.5	208.5	208.5
Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)	Y-coord. of 2nd end-point for LOS1 (m)
LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)	LOS integrated conc. (mg/m ³ *2)
X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)	X-coord. of 1st end-point for LOS1 (m)
Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)	Y-coord. of 1st end-point for LOS1 (m)

The Evaluation of the 18 Series Grenades (Reworked 18A1, 6 grenades, L&L6)

6 : number of trials included in DOA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

819b : B21b

5 : B22b

25 : B23b

82 : B24b

15 : trial ID

28 : month

4 : day

4 : year

17 : hour

31 : minute

27 : no. of sources

6 : x-coord. of source (m)

4 : y-coord. of source (m)

99.7 : source elevation (m)

0.00 : emission rate (g/s)

0.00 : emission duration (s)

118.0 : total mass emitted (kg)

0.916 : sig0 at the source (m)

2.576 : sig0 at the source (m)

18.137 : sig0 at the source (m)

0.120 : sig0 at the source (m)

128.3 : x-coord. of source (m)

83.3 : y-coord. of source (m)

0.00 : source elevation (m)

99.9 : emission rate (g/s)

99.9 : emission duration (s)

118.0 : total mass emitted (kg)

0.916 : sig0 at the source (m)

10.221 : sig0 at the source (m)

6.817 : sig0 at the source (m)

16.995 : sig0 at the source (m)

0.120 : sig0 at the source (m)

28.7 : x-coord. of source (m)

46.1 : y-coord. of source (m)

0.00 : source elevation (m)

99.9 : emission rate (g/s)

99.9 : emission duration (s)

118.0 : total mass emitted (kg)

0.859 : sig0 at the source (m)

13.612 : sig0 at the source (m)

12.218 : sig0 at the source (m)

0.120 : sig0 at the source (m)

99.9 : x-coord. of source (m)

79.2 : y-coord. of source (m)

0.00 : source elevation (m)

99.9 : emission rate (g/s)

99.9 : emission duration (s)

118.0 : total mass emitted (kg)

0.916 : sig0 at the source (m)

10.780 : sig0 at the source (m)

93.900 : sig0 at the source (m)

14.804 : sig0 at the source (m)

0.120 : sig0 at the source (m)

27.6 : x-coord. of source (m)

57.0 : y-coord. of source (m)

0.00 : source elevation (m)

99.9 : emission rate (g/s)

99.9 : emission duration (s)

118.0 : total mass emitted (kg)

0.859 : sig0 at the source (m)

15.202 : sig0 at the source (m)

99.900 : sig0 at the source (m)

10.221 : sig0 at the source (m)

0.120 : sig0 at the source (m)

99.9 : x-coord. of source (m)

99.9 : y-coord. of source (m)

300.00 : source elevation (m)

2.00 : measuring height for temperature #1 (m)

2.00 : measuring height for temperature #2 (m)

99.90 : measuring height for temperature #3 (m)

99.90 : measuring height for temperature #4 (m)

2.80 : wind speed (m/s) at a tower

2.00 : measuring height for wind data (m)

2.00 : domain-averaged wind speed (m/s)

332.0 : domain-averaged wind direction (deg)

99.90 : domain-averaged sigma-u (m/s)

16.90 : domain-averaged sigma-theta (deg)

4.00 : domain-averaged sigma-phi (deg)

2.00 : measuring ht for domain-avg wind speed (m)

300.0 : averaging time for domain-avg data (s)

0.098 : wind speed power law exponent

0.0300 : surface roughness (m)

99.900 : friction velocity (m)

99.9000 : inverse Monin-Obukhov length (1/m)

The Evaluation of the 18 Series Grenades (Renowned LHA1, 8 Grenades, L81H87)

6 : number of trials included in DUA		B25b		B28b		B29b		B30b : trial ID	
6	7	6	7	6	7	6	7	6	7
40.20	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
113.00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
B25b	6	60.9	60.9	60.9	60.9	60.9	60.9	60.9	60.9
B26b	7	-74.6	-74.6	-74.6	-74.6	-74.6	-74.6	-74.6	-74.6
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	10	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	11	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	12	6.837	7.426	4.094	4.094	4.094	4.094	7.426	7.426
	13	16.995	16.746	17.856	18.276	18.276	18.276	16.746	16.746
	14	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	15	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
	16	-61.9	-61.9	-61.9	-61.9	-61.9	-61.9	-61.9	-61.9
	17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	18	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	19	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	20	11.003	11.507	8.516	8.516	8.516	8.516	11.507	11.507
	21	14.647	15.978	14.254	14.254	14.254	14.254	14.254	14.254
	22	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	23	36.3	36.3	36.3	36.3	36.3	36.3	36.3	36.3
	24	-46.8	-46.8	-46.8	-46.8	-46.8	-46.8	-46.8	-46.8
	25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	26	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	27	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	28	7.183	7.808	4.521	4.521	4.521	4.521	7.808	7.808
	29	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	30	100.5	100.5	100.5	100.5	100.5	100.5	100.5	100.5
	31	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2
	32	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	33	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	34	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	35	11.796	12.408	8.347	8.347	8.347	8.347	12.408	12.408
	36	18.292	18.316	17.093	17.093	17.093	17.093	18.316	18.316
	37	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	38	70.7	70.7	70.7	70.7	70.7	70.7	70.7	70.7
	39	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2	-117.2
	40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	41	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	42	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	43	5.687	5.075	5.075	5.075	5.075	5.075	5.687	5.687
	44	17.414	17.414	17.414	17.414	17.414	17.414	17.414	17.414
	45	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	46	66.6	66.6	66.6	66.6	66.6	66.6	66.6	66.6
	47	-133.4	-133.4	-133.4	-133.4	-133.4	-133.4	-133.4	-133.4
	48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	49	118.0	118.0	118.0	118.0	118.0	118.0	118.0	118.0
	50	0.801	0.763	0.763	0.763	0.763	0.763	0.744	0.744
	51	10.000	9.900	9.900	9.900	9.900	9.900	10.000	10.000
	52	15.349	15.349	15.349	15.349	15.349	15.349	15.349	15.349
	53	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.120
	54	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9

-99.9	0.00	46.1	Y-coord. of source (m)
0.00	0.00	0.00	source elevation (m)
-99.9	0.00	-99.9	emission rate (g/s)
118.0	0.897	118.0	emission duration (s)
0.973	0.763	0.820	total mass emitted (kg)
-99.900	14.647	14.647	sigx0 at the source (m)
-99.900	11.003	11.003	sigy0 at the source (m)
0.120	0.120	0.120	sigz0 at the source (m)
-99.9	-28.7	-28.7	x-coord. of source (m)
-99.9	79.2	79.2	y-coord. of source (m)
0.00	0.00	0.00	source elevation (m)
-99.9	0.00	-99.9	emission rate (g/s)
118.0	0.897	118.0	emission duration (s)
0.973	0.763	0.820	total mass emitted (kg)
-99.900	16.335	16.335	sigx0 at the source (m)
-99.900	8.292	8.292	sigy0 at the source (m)
0.120	0.120	0.120	sigz0 at the source (m)
-99.9	-27.6	-27.6	x-coord. of source (m)
-99.9	57.0	57.0	y-coord. of source (m)
0.00	0.00	0.00	source elevation (m)
-99.9	0.00	-99.9	emission rate (g/s)
118.0	0.897	118.0	emission duration (s)
0.973	0.763	0.820	total mass emitted (kg)
-99.900	12.513	12.513	sigx0 at the source (m)
-99.900	13.379	13.379	sigy0 at the source (m)
0.120	0.120	0.120	sigz0 at the source (m)
-99.9	-99.9	-99.9	ambient pressure (atm)
-99.9	-99.9	-99.9	relative humidity (%)
300.00	300.00	300.00	temperature at level #1 (K)
2.00	2.00	2.00	measuring height for temperature #1 (m)
-99.90	-99.90	-99.90	temperature at level #2 (K)
-99.90	-99.90	-99.90	measuring height for temperature #2 (m)
4.20	4.20	4.20	wind speed (m/s) at a tower
2.00	2.00	2.00	measuring height for wind data (m)
336.0	3.0	357.0	domain-averaged wind speed (m/s)
-99.90	14.10	-99.90	domain-averaged wind direction (deg)
2.00	2.00	16.20	domain-averaged sigma-u (m/s)
3.00	3.00	3.10	domain-averaged sigma-theta (deg)
300.0	300.0	300.0	measuring ht for domain-avg wind speed (m)
0.084	0.107	0.060	wind speed power law exponent
0.0300	0.0300	0.0300	surface roughness (m)
-99.900	-99.900	-99.900	friction velocity (m)
-99.9000	-99.9000	-99.9000	inverse Monin-Obukhov length (1/m)
0.18	0.18	0.18	albedo
0.50	0.50	0.50	moisture availability
0.50	0.50	0.50	Bowen ratio
-99.9	-99.9	-99.9	mixing height (m)
-99.9	-99.9	-99.9	cloud cover (%)
-99.9	-99.9	-99.9	P-G stability class
300.0	300.0	300.0	averaging time for concentration (s)
2.00	2.00	2.00	sugated receptor height (m)
0	0	0	no. of distances downwind
4	4	4	no. of lines-of-sight
-173.8	-173.8	-173.8	x-coord. of 1st end-point for LOS1 (m)
-205.7	-205.7	-205.7	y-coord. of 1st end-point for LOS1 (m)
356.0	356.0	356.0	x-coord. of 2nd end-point for LOS1 (m)
76.0	76.0	76.0	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)
1.030E+05	1.030E+05	1.030E+05	LOS integrated dosage (mg-y/m**2)
-197.3	-197.3	-197.3	x-coord. of 1st end-point for LOS1 (m)
-161.5	-161.5	-161.5	y-coord. of 1st end-point for LOS1 (m)
332.5	332.5	332.5	x-coord. of 2nd end-point for LOS1 (m)
120.2	120.2	120.2	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)
1.530E+05	1.530E+05	1.530E+05	LOS integrated dosage (mg-y/m**2)
-220.7	-220.7	-220.7	x-coord. of 1st end-point for LOS1 (m)
-117.4	-117.4	-117.4	y-coord. of 1st end-point for LOS1 (m)
309.0	309.0	309.0	x-coord. of 2nd end-point for LOS1 (m)
164.3	164.3	164.3	y-coord. of 2nd end-point for LOS1 (m)
-99.9	-99.9	-99.9	LOS integrated conc. (mg/m**2)
2.470E+05	2.470E+05	2.470E+05	LOS integrated dosage (mg-y/m**2)
-244.2	-244.2	-244.2	x-coord. of 1st end-point for LOS1 (m)
-73.2	-73.2	-73.2	y-coord. of 1st end-point for LOS1 (m)
285.6	285.6	285.6	x-coord. of 2nd end-point for LOS1 (m)

208.5 208.5 208.5 208.5 208.5 : Y-coord. of 2nd end-point for LOS1 (m)
-99.9 -99.9 -99.9 -99.9 -99.9 : LOS integrated conc. (mg/m³*2)
-9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 : LOS integrated dosage (mg-s/m³*2)

208.5 208.5 208.5 208.5 208.5 : y-coord. of 2nd end-point for IOS1 (m)
-99.9 -99.9 -99.9 -99.9 -99.9 : LOS integrated conc. (mg/m**2)
-9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 : LOS integrated dosage (mg-m**2)
-267.7 -267.7 -267.7 -267.7 -267.7 : x-coord. of 1st end-point for IOS1 (m)
279.1 279.1 279.1 279.1 279.1 : y-coord. of 1st end-point for IOS1 (m)
262.1 262.1 262.1 262.1 262.1 : x-coord. of 2nd end-point for IOS1 (m)
252.6 252.6 252.6 252.6 252.6 : y-coord. of 2nd end-point for IOS1 (m)
-99.9 -99.9 -99.9 -99.9 -99.9 : LOS integrated conc. (mg/m**2)
-9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 -9.990E+01 : LOS integrated dosage (mg-m**2)

-99.9 : relative humidity (%)
 300.00 : temperature at level #1 (K)
 2.00 : measuring height for temperature #1 (m)
 -99.90 : temperature at level #2 (K)
 -99.90 : measuring height for temperature #2 (m)
 -99.90 : wind speed (m/s) at a tower
 3.10 : measuring height for wind data (m)
 3.10 : domain-averaged wind speed (m/s)
 201.0 : domain-averaged wind direction (deg)
 -99.90 : domain-averaged sigma-u (m/s)
 9.10 : domain-averaged sigma-theta (deg)
 3.80 : domain-averaged sigma-phi (deg)
 2.00 : measuring ht for domain-avg wind speed (m)
 300.0 : averaging time for domain-avg wind speed (s)
 0.108 : wind speed power law exponent
 0.0300 : surface roughness (m)
 -99.900 : friction velocity (m)
 -99.9000 : inverse Monin-Obukhov length (1/m)
 0.18 : albedo
 0.50 : moisture availability
 0.50 : Bowen ratio
 -99.9 : mixing height (m)
 -99.9 : cloud cover (%)
 -99.9 : P-G stability class
 300.0 : averaging time for concentration (s)
 2.00 : suggested receptor height (m)
 0 : no. of distances downwind
 3 : no. of lines-of-sight
 -220.7 : x-coord. of 1st end-point for LOS1 (m)
 -117.4 : y-coord. of 1st end-point for LOS1 (m)
 309.0 : x-coord. of 2nd end-point for LOS1 (m)
 164.3 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 1.320E+05 : LOS integrated dosage (mg-s/m**2)
 -244.2 : x-coord. of 1st end-point for LOS1 (m)
 -71.2 : y-coord. of 1st end-point for LOS1 (m)
 285.6 : x-coord. of 2nd end-point for LOS1 (m)
 208.5 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 8.300E+04 : LOS integrated dosage (mg-s/m**2)
 -257.7 : x-coord. of 1st end-point for LOS1 (m)
 -79.1 : y-coord. of 1st end-point for LOS1 (m)
 282.1 : x-coord. of 2nd end-point for LOS1 (m)
 252.6 : y-coord. of 2nd end-point for LOS1 (m)
 -99.9 : LOS integrated conc. (mg/m**2)
 -9.990E+01 : LOS integrated dosage (mg-s/m**2)

The Evaluation of the L8 Series Grenades (L8A3, L2 Grenades, L8J2)

6 : number of trials included in DOA
 6 : time zone designation
 40.20 : latitude (deg)
 113.00 : longitude (deg)

B49b	B50b	B51b	B52b	B53b	B54b	B55b
5	5	6	6	6	6	6
25	26	1	1	1	1	1
22	22	22	22	22	22	22
18	18	18	18	18	18	18
14	14	14	14	14	14	14
10	10	10	10	10	10	10
12	12	12	12	12	12	12
46.6	51.7	-66.3	-66.3	-66.3	-66.3	-66.3
93.7	93.7	-80.6	-80.6	-80.6	-80.6	-80.6
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
5.368	6.257	2.801	2.801	2.801	2.801	2.801
12.834	12.834	13.721	13.721	13.721	13.721	13.721
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-59.2	-59.2	39.1	39.1	39.1	39.1	39.1
107.1	107.1	-67.1	-67.1	-67.1	-67.1	-67.1
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
0.820	1.594	2.061	2.061	2.061	2.061	2.061
13.930	13.931	13.851	13.851	13.851	13.851	13.851
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-75.6	-75.6	22.7	22.7	22.7	22.7	22.7
115.5	115.5	-58.1	-58.1	-58.1	-58.1	-58.1
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
4.202	3.260	3.260	3.260	3.260	3.260	3.260
13.358	13.358	13.311	13.311	13.311	13.311	13.311
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-52.3	-52.3	46.0	46.0	46.0	46.0	46.0
101.0	101.0	-73.3	-73.3	-73.3	-73.3	-73.3
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
3.040	3.986	4.335	4.335	4.335	4.335	4.335
13.870	13.424	13.995	13.995	13.995	13.995	13.995
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-84.6	-84.6	13.7	13.7	13.7	13.7	13.7
117.4	117.4	-56.8	-56.8	-56.8	-56.8	-56.8
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
1.819	1.819	1.819	1.819	1.819	1.819	1.819
13.885	13.938	13.283	13.283	13.283	13.283	13.283
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-42.3	-42.3	56.0	56.0	56.0	56.0	56.0
85.5	85.5	-88.7	-88.7	-88.7	-88.7	-88.7
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
6.458	5.716	8.710	8.710	8.710	8.710	8.710
12.426	12.846	10.965	10.965	10.965	10.965	10.965
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-67.0	-67.0	31.3	31.3	31.3	31.3	31.3
112.0	112.0	-62.2	-62.2	-62.2	-62.2	-62.2
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
5.799	5.799	5.799	5.799	5.799	5.799	5.799
12.747	12.747	12.747	12.747	12.747	12.747	12.747
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-67.0	-67.0	67.0	67.0	67.0	67.0	67.0
112.0	112.0	-67.0	-67.0	-67.0	-67.0	-67.0
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
13.951	13.951	13.951	13.951	13.951	13.951	13.951
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-42.3	-42.3	85.3	85.3	85.3	85.3	85.3
85.3	85.3	-42.3	-42.3	-42.3	-42.3	-42.3
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
11.395	11.395	11.395	11.395	11.395	11.395	11.395
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-38.2	-38.2	60.1	60.1	60.1	60.1	60.1
67.6	67.6	-106.6	-106.6	-106.6	-106.6	-106.6
0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
105.0	105.0	105.0	105.0	105.0	105.0	105.0
0.840	0.840	0.840	0.840	0.840	0.840	0.840
11.116	11.116	11.683	11.683	11.683	11.683	11.683
8.518	8.518	7.722	7.722	7.722	7.722	7.722
0.120	0.120	0.120	0.120	0.120	0.120	0.120
-40.4	-40.4	57.9	57.9	57.9	57.9	57.9

The Evaluation of the 18 Series Grenades (L8A), low condition temp., L83L

5 : number of trials included in DDA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

817A : trial ID

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-99.9	0.00	-99.9	0.00	-99.9	49.3	-124.9	y-coord. of source (m)
-99.9	0.00	-99.9	0.00	-99.9	0.00	0.00	source elevation (m)
-99.9	0.00	-99.9	0.00	-99.9	0.00	-99.9	emission rate (g/s)
105.0	105.0	105.0	105.0	105.0	105.0	105.0	emission duration (s)
0.973	0.763	0.973	0.763	0.973	0.897	0.916	total mass emitted (kg)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	12.311	13.913	sig0 at the source (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	6.674	1.594	sig0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	sig0 at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	39.5	58.9	x-coord. of source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	76.7	-97.5	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	-99.9	-99.9	-99.9	-99.9	0.00	-99.9	emission rate (g/s)
105.0	105.0	105.0	105.0	105.0	105.0	105.0	emission duration (s)
0.973	0.763	0.973	0.763	0.973	7.325	0.916	total mass emitted (kg)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	11.935	3.576	sig0 at the source (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	0.120	0.120	sig0 at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-43.9	34.4	x-coord. of source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	40.8	-133.5	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	-99.9	-99.9	-99.9	-99.9	0.00	-99.9	emission rate (g/s)
105.0	105.0	105.0	105.0	105.0	105.0	105.0	emission duration (s)
0.973	0.763	0.973	0.763	0.973	0.897	0.916	total mass emitted (kg)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	13.283	13.424	sig0 at the source (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	4.435	3.986	sig0 at the source (m)
0.120	0.120	0.120	0.120	0.120	0.120	0.120	sig0 at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	38.5	59.8	x-coord. of source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	58.4	-115.9	y-coord. of source (m)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	source elevation (m)
-99.9	-99.9	-99.9	-99.9	-99.9	0.00	-99.9	emission rate (g/s)
105.0	105.0	105.0	105.0	105.0	105.0	105.0	emission duration (s)
0.973	0.763	0.973	0.763	0.973	0.897	0.916	total mass emitted (kg)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	8.710	0.846	sig0 at the source (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	0.120	0.120	sig0 at the source (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	ambient pressure (atm)
-99.9	-99.9	-99.9	-99.9	-99.9	300.00	300.00	relative humidity (%)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	measuring height for temperature #1 (m)
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	-99.90	temperature at level #2 (K)
-99.90	-99.90	-99.90	-99.90	-99.90	4.20	-99.90	measuring height for temperature #2 (m)
4.50	4.50	4.50	4.50	4.50	2.00	2.00	wind speed (m/s) at a tower
2.00	2.00	2.00	2.00	2.00	2.00	2.00	measuring height for wind data (m)
4.50	4.50	4.50	4.50	4.50	351.0	136.0	domain-averaged wind speed (m/s)
349.0	349.0	349.0	349.0	349.0	-99.90	-99.90	domain-averaged wind direction (deg)
-99.90	-99.90	-99.90	-99.90	-99.90	25.90	11.90	domain-averaged sigma-u (m/s)
7.00	7.00	7.00	7.00	7.00	2.40	4.30	domain-averaged sigma-theta (deg)
2.00	2.00	2.00	2.00	2.00	2.00	2.00	measuring ht for domain-avg wind speed (m)
0.078	0.078	0.078	0.078	0.078	0.087	0.087	wind speed power law exponent
0.300	0.300	0.300	0.300	0.300	0.0300	0.0300	surface roughness (m)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	friction velocity (m/s)
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	0.18	0.18	Inverse Monin-Obukhov length (1/m)
0.50	0.50	0.50	0.50	0.50	0.50	0.50	albedo
0.50	0.50	0.50	0.50	0.50	0.50	0.50	moisture availability
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	Bowen ratio
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	mixing height (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	cloud cover (%)
300.0	300.0	300.0	300.0	300.0	300.0	300.0	P-G stability class
2.00	2.00	2.00	2.00	2.00	2.00	2.00	averaging time for concentration (s)
0	0	0	0	0	0	0	suggested receptor height (m)
0	0	0	0	0	0	0	no. of distances downwind
5	5	5	5	5	5	5	no. of lines-of-sight
-173.8	-173.8	-173.8	-173.8	-173.8	-173.8	-173.8	x-coord. of 1st end-point for IOS1 (m)
-205.7	-205.7	-205.7	-205.7	-205.7	-205.7	-205.7	y-coord. of 1st end-point for IOS1 (m)
356.0	356.0	356.0	356.0	356.0	356.0	356.0	x-coord. of 2nd end-point for IOS1 (m)
76.0	76.0	76.0	76.0	76.0	76.0	76.0	y-coord. of 2nd end-point for IOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	IOS integrated conc. (mg/m**2)
4.500E+04	4.500E+04	4.500E+04	4.500E+04	4.500E+04	-9.990E+01	-9.990E+01	IOS integrated dosage (mg-3/m**2)
-187.3	-187.3	-187.3	-187.3	-187.3	-197.3	-197.3	x-coord. of 1st end-point for IOS1 (m)
-161.5	-161.5	-161.5	-161.5	-161.5	161.5	161.5	y-coord. of 1st end-point for IOS1 (m)
332.5	332.5	332.5	332.5	332.5	332.5	332.5	x-coord. of 2nd end-point for IOS1 (m)
120.2	120.2	120.2	120.2	120.2	120.2	120.2	y-coord. of 2nd end-point for IOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	IOS integrated conc. (mg/m**2)
6.600E+04	6.600E+04	6.600E+04	6.600E+04	6.600E+04	-9.990E+01	-9.990E+01	IOS integrated dosage (mg-3/m**2)
-220.7	-220.7	-220.7	-220.7	-220.7	-220.7	-220.7	x-coord. of 1st end-point for IOS1 (m)
309.0	309.0	309.0	309.0	309.0	309.0	309.0	y-coord. of 1st end-point for IOS1 (m)
164.3	164.3	164.3	164.3	164.3	164.3	164.3	x-coord. of 2nd end-point for IOS1 (m)
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	IOS integrated conc. (mg/m**2)
1.340E+05	1.340E+05	1.340E+05	1.340E+05	1.340E+05	3.260E+05	3.260E+05	IOS integrated dosage (mg-3/m**2)
-244.2	-244.2	-244.2	-244.2	-244.2	-244.2	-244.2	x-coord. of 1st end-point for IOS1 (m)
-71.2	-71.2	-71.2	-71.2	-71.2	-71.2	-71.2	y-coord. of 1st end-point for IOS1 (m)
285.6	285.6	285.6	285.6	285.6	285.6	285.6	x-coord. of 2nd end-point for IOS1 (m)

The Evaluation of the L8 Series Grenades (L8A3, high condition temp., L83M)

5 : number of trials included in DUA

6 : time zone designation

40.20 : latitude (deg)

113.00 : longitude (deg)

841a : trial ID

842a : month

843a : day

844a : year

845a : hour

846a : minute

847a : no. of sources

848a : x-coord. of source (m)

849a : y-coord. of source (m)

850a : source elevation (m)

851a : emission rate (g/s)

852a : emission duration (s)

853a : total mass emitted (kg)

854a : sig0 at the source (m)

855a : sig0 at the source (m)

856a : sig0 at the source (m)

857a : x-coord. of source (m)

858a : y-coord. of source (m)

859a : source elevation (m)

860a : emission rate (g/s)

861a : emission duration (s)

862a : total mass emitted (kg)

863a : sig0 at the source (m)

864a : sig0 at the source (m)

865a : sig0 at the source (m)

866a : x-coord. of source (m)

867a : y-coord. of source (m)

868a : source elevation (m)

869a : emission rate (g/s)

870a : emission duration (s)

871a : total mass emitted (kg)

872a : sig0 at the source (m)

873a : sig0 at the source (m)

874a : sig0 at the source (m)

875a : x-coord. of source (m)

876a : y-coord. of source (m)

877a : source elevation (m)

878a : emission rate (g/s)

879a : emission duration (s)

880a : total mass emitted (kg)

881a : sig0 at the source (m)

882a : sig0 at the source (m)

883a : sig0 at the source (m)

884a : x-coord. of source (m)

885a : y-coord. of source (m)

886a : source elevation (m)

887a : emission rate (g/s)

888a : emission duration (s)

889a : total mass emitted (kg)

890a : sig0 at the source (m)

891a : sig0 at the source (m)

892a : sig0 at the source (m)

893a : x-coord. of source (m)

894a : y-coord. of source (m)

895a : source elevation (m)

896a : emission rate (g/s)

897a : emission duration (s)

898a : total mass emitted (kg)

899a : sig0 at the source (m)

900a : sig0 at the source (m)

901a : sig0 at the source (m)

902a : x-coord. of source (m)

903a : y-coord. of source (m)

904a : source elevation (m)

905a : emission rate (g/s)

906a : emission duration (s)

907a : total mass emitted (kg)

908a : sig0 at the source (m)

909a : sig0 at the source (m)

910a : sig0 at the source (m)

911a : x-coord. of source (m)

912a : y-coord. of source (m)

913a : source elevation (m)

914a : emission rate (g/s)

915a : emission duration (s)

916a : total mass emitted (kg)

917a : sig0 at the source (m)

918a : sig0 at the source (m)

919a : sig0 at the source (m)

920a : x-coord. of source (m)

921a : y-coord. of source (m)

922a : source elevation (m)

923a : emission rate (g/s)

924a : emission duration (s)

925a : total mass emitted (kg)

926a : sig0 at the source (m)

927a : sig0 at the source (m)

928a : sig0 at the source (m)

929a : x-coord. of source (m)

930a : y-coord. of source (m)

The Tests of Foreign Smoke Pots/Generators (Japanese 3-00, INTJA)

7 : number of trials included in DOA

6 : time zone designation

40 : latitude (deg)

113.00 : longitude (deg)

J602	J604	J609	J610	J620	J622
3	3	11	11	11	11
14	15	17	17	21	21
81	81	81	81	81	81
20	21	16	18	15	20
17	42	9	9	22	46
1	1	1	1	1	1
-29.1	19.4	19.4	19.4	19.4	19.4
52.5	-35.0	-35.0	-35.0	-35.0	-35.0
0.25	0.25	0.25	0.25	0.25	0.25
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
1345.8	1426.2	1266.0	1381.2	1330.8	1330.8
14.113	15.146	14.715	14.326	20.368	15.146
0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
300.00	300.00	300.00	300.00	300.00	300.00
2.00	2.00	2.00	2.00	2.00	2.00
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
3.50	3.10	4.50	4.80	3.20	3.60
2.00	2.00	2.00	2.00	2.00	2.00
3.50	3.10	4.50	4.80	3.20	3.60
346.0	136.0	160.0	140.0	134.0	148.0
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
4.80	4.00	3.80	4.70	11.60	8.20
-99.90	-99.90	-99.90	-99.90	-99.90	-99.90
2.00	2.00	2.00	2.00	2.00	2.00
1345.8	1387.2	1266.0	1111.2	1381.2	1330.8
0.056	0.098	0.193	0.115	0.142	0.111
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000
-99.9000	-99.9000	-99.9000	-99.9000	-99.9000	-99.9000
0.18	0.18	0.18	0.18	0.18	0.18
0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
1345.8	1387.2	1266.0	1111.2	1381.2	1330.8
2.00	2.00	2.00	2.00	2.00	2.00
0	0	0	0	0	0
-218.7	-218.7	-218.7	-218.7	-218.7	-218.7
-121.2	-121.2	-121.2	-121.2	-121.2	-121.2
568.5	568.5	568.5	568.5	568.5	568.5
315.1	315.1	315.1	315.1	315.1	315.1
-99.9	-99.9	-99.9	-99.9	-99.9	-99.9
8.500E+05	3.590E+05	9.610E+05	5.780E+05	1.156E+06	7.080E+05

Development Test I of the Man-Portable Smoke Generators (MJA3, fog oil only, POMEF)

6 : number of trials included in DDA
 6 : time zone designation

40.20 : latitude (deg)
 113.00 : longitude (deg)

FO02	FO06	FO07	FO09	FO11	FO19
4	4	4	4	4	4
5	13	13	13	14	22
81	81	81	81	81	22
17	19	20	21	20	81
24	22	21	40	26	22
1	1	1	1	1	47
-240.1	-323.5	-308.9	-294.4	-338.1	1 : no. of sources
-412.5	-24.9	-51.2	-77.4	-101.7	-294.4 : x-coord. of source (m)
0.30	0.30	0.30	0.30	0.30	-77.4 : y-coord. of source (m)
99.9	99.9	99.9	99.9	99.9	0.30 : source elevation (m)
300.0	300.0	300.0	300.0	300.0	99.9 : emission rate (g/s)
8.117	10.818	14.548	10.054	8.188	300.0 : total mass emitted (kg)
0.230	0.230	0.230	0.230	0.230	8.188 : emission duration (s)
0.230	0.230	0.230	0.230	0.230	0.230 : sigm0 at the source (m)
0.230	0.230	0.230	0.230	0.230	0.230 : sigm0 at the source (m)
99.9	99.9	99.9	99.9	99.9	0.230 : ambient pressure (atm)
99.9	99.9	99.9	99.9	99.9	99.9 : relative humidity (%)
300.00	300.00	300.00	300.00	300.00	300.00 : temperature at level #1 (K)
2.00	2.00	2.00	2.00	2.00	2.00 : measuring height for temperature #1 (m)
99.90	99.90	99.90	99.90	99.90	99.90 : temperature at level #2 (K)
99.90	99.90	99.90	99.90	99.90	99.90 : measuring height for temperature #2 (m)
3.50	4.80	5.50	6.10	2.30	6.00 : wind speed (m/s) at a tower
2.00	2.00	2.00	2.00	2.00	2.00 : measuring height for wind data (m)
3.50	4.80	5.50	6.10	2.30	6.00 : domain-averaged wind speed (m/s)
181.0	336.0	347.0	352.0	311.0	346.0 : domain-averaged wind direction (deg)
99.90	99.90	99.90	99.90	99.90	99.90 : domain-averaged sigma-u (m/s)
13.20	13.20	12.10	11.80	30.60	13.20 : domain-averaged sigma-theta (deg)
99.90	99.90	99.90	99.90	99.90	99.90 : domain-averaged sigma-phi (deg)
2.00	2.00	2.00	2.00	2.00	2.00 : measuring ht for domain-avg wind speed (m)
530.0	420.0	435.0	450.0	485.0	450.0 : averaging time for domain-avg data (s)
0.082	0.066	0.065	0.069	0.057	0.075 : wind speed power law exponent
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300 : surface roughness (m)
99.9000	99.9000	99.9000	99.9000	99.9000	99.9000 : friction velocity (m)
99.9000	99.9000	99.9000	99.9000	99.9000	99.9000 : inverse Monin-Obukhov length (1/m)
0.18	0.18	0.18	0.18	0.18	0.18 : albedo
0.50	0.50	0.50	0.50	0.50	0.50 : moisture availability
0.50	0.50	0.50	0.50	0.50	0.50 : Bowen ratio
99.9	99.9	99.9	99.9	99.9	99.9 : mixing height (m)
99.9	99.9	99.9	99.9	99.9	99.9 : cloud cover (%)
99.9	99.9	99.9	99.9	99.9	99.9 : P-G stability class
300.0	300.0	300.0	300.0	300.0	300.0 : averaging time for concentration (s)
2.44	2.44	2.44	2.44	2.44	2.44 : suggested receptor height (m)
0	0	0	0	0	0 : no. of distances downwind
3	3	3	3	3	3 : no. of lines-of-sight
-779.9	-779.9	-779.9	-779.9	-779.9	-779.9 : x-coord. of 1st end-point for LOS1 (m)
-449.4	-449.4	-449.4	-449.4	-449.4	-449.4 : y-coord. of 1st end-point for LOS1 (m)
532.0	532.0	532.0	532.0	532.0	532.0 : x-coord. of 2nd end-point for LOS1 (m)
277.8	277.8	277.8	277.8	277.8	277.8 : y-coord. of 2nd end-point for LOS1 (m)
99.9	99.9	99.9	99.9	99.9	99.9 : LOS integrated conc. (mg/m**2)
5.700E+04	7.300E+04	1.610E+05	2.660E+05	1.650E+05	2.130E+05 : LOS integrated conc. (mg/m**2)
-750.8	-750.8	-750.8	-750.8	-750.8	-750.8 : x-coord. of 1st end-point for LOS1 (m)
-501.9	-501.9	-501.9	-501.9	-501.9	-501.9 : y-coord. of 1st end-point for LOS1 (m)
561.1	561.1	561.1	561.1	561.1	561.1 : x-coord. of 2nd end-point for LOS1 (m)
225.3	225.3	225.3	225.3	225.3	225.3 : y-coord. of 2nd end-point for LOS1 (m)
99.9	99.9	99.9	99.9	99.9	99.9 : LOS integrated conc. (mg/m**2)
1.080E+05	3.700E+04	7.600E+04	1.640E+05	7.300E+04	1.160E+05 : LOS integrated conc. (mg/m**2)
-721.7	-721.7	-721.7	-721.7	-721.7	-721.7 : x-coord. of 1st end-point for LOS1 (m)
-554.4	-554.4	-554.4	-554.4	-554.4	-554.4 : y-coord. of 1st end-point for LOS1 (m)
590.2	590.2	590.2	590.2	590.2	590.2 : x-coord. of 2nd end-point for LOS1 (m)
172.8	172.8	172.8	172.8	172.8	172.8 : y-coord. of 2nd end-point for LOS1 (m)
99.9	99.9	99.9	99.9	99.9	99.9 : LOS integrated conc. (mg/m**2)
2.480E+05	3.100E+04	4.500E+04	1.180E+05	3.400E+04	7.000E+04 : LOS integrated conc. (mg/m**2)

Development Test I of the Man-Portable Smoke Generators (KM49, diesel only and diesel part of diesel+IB, FOXD)

6 : number of trials included in DDA

6 : time zone designation

113.00 : latitude (deg)

DO20 : longitude (deg)

DO21 : DO22

DO23 : DO24

DO25 : DO26

DO27 : DO28

DO29 : DO30

DO31 : DO32

DO33 : DO34

DO35 : DO36

DO37 : DO38

DO39 : DO40

DO41 : DO42

DO43 : DO44

DO45 : DO46

DO47 : DO48

DO49 : DO50

DO51 : DO52

DO53 : DO54

DO55 : DO56

DO57 : DO58

DO59 : DO60

DO61 : DO62

DO63 : DO64

DO65 : DO66

DO67 : DO68

DO69 : DO70

DO71 : DO72

DO73 : DO74

DO75 : DO76

DO77 : DO78

DO79 : DO80

DO81 : DO82

DO83 : DO84

DO85 : DO86

DO87 : DO88

DO89 : DO90

DO91 : DO92

DO93 : DO94

DO95 : DO96

DO97 : DO98

DO99 : DO100

DO101 : DO102

DO103 : DO104

DO105 : DO106

DO107 : DO108

DO109 : DO110

DO111 : DO112

DO113 : DO114

DO115 : DO116

DO117 : DO118

DO119 : DO120

DO121 : DO122

DO123 : DO124

DO125 : DO126

DO127 : DO128

DO129 : DO130

DO131 : DO132

DE364 : DE365

DE366 : DE367

DE368 : DE369

DE371 : DE372

DE373 : DE374

DE375 : DE376

DE377 : DE378

DE379 : DE380

DE381 : DE382

DE383 : DE384

DE385 : DE386

DE387 : DE388

DE389 : DE390

DE391 : DE392

DE393 : DE394

DE395 : DE396

DE397 : DE398

DE399 : DE400

DE401 : DE402

DE403 : DE404

DE405 : DE406

DE407 : DE408

DE409 : DE410

DE411 : DE412

DE413 : DE414

DE415 : DE416

DE417 : DE418

DE419 : DE420

DE421 : DE422

DE423 : DE424

DE425 : DE426

DE427 : DE428

DE429 : DE430

DE431 : DE432

DE433 : DE434

DE435 : DE436

DE437 : DE438

DE439 : DE440

DE441 : DE442

DE443 : DE444

DE445 : DE446

DE447 : DE448

DE449 : DE450

DE451 : DE452

DE453 : DE454

DE455 : DE456

DE457 : DE458

DE459 : DE460

DE461 : DE462

DE463 : DE464

DE465 : DE466

DE467 : DE468

DE469 : DE470

DE471 : DE472

DE473 : DE474

DE475 : DE476

DE477 : DE478

DE479 : DE480

DE481 : DE482

DE483 : DE484

DO39 : trial ID

6 : month

3 : day

81 : year

22 : hour

1 : minute

1 : no. of sources

1 : x-coord. of source (m)

1 : y-coord. of source (m)

1 : source elevation (m)

1 : emission rate (g/s)

1 : emission duration (s)

1 : total mass emitted (kg)

1 : sign0 at the source (m)

1 : sign0 at the source (m)

1 : sign0 at the source (m)

1 : ambient pressure (atm)

1 : relative humidity (%)

1 : temperature at level #1 (K)

1 : measuring height for temperature #1 (m)

1 : temperature at level #2 (K)

1 : measuring height for temperature #2 (m)

1 : wind speed (m/s) at a tower

1 : measuring height for wind data (m)

1 : domain-averaged wind speed (m/s)

1 : domain-averaged wind direction (deg)

1 : domain-averaged sigma-u (m/s)

1 : domain-averaged sigma-theta (deg)

1 : domain-averaged sigma-phi (deg)

1 : measuring ht for domain-avg wind speed (m)

1 : averaging time for domain-avg data (s)

1 : wind speed power law exponent

1 : surface roughness (m)

1 : friction velocity (m/s)

1 : inverse Monin-Obukhov length (1/m)

1 : albedo

1 : moisture availability

1 : Bowen ratio

1 : mixing height (m)

1 : cloud cover (%)

1 : P-G stability class

1 : averaging time for concentration (s)

1 : suggested receptor height (m)

1 : no. of distances downwind

1 : no. of lines-of-sight

1 : x-coord. of 1st end-point for LOS1 (m)

1 : x-coord. of 1st end-point for LOS1 (m)

1 : x-coord. of 2nd end-point for LOS1 (m)

1 : y-coord. of 2nd end-point for LOS1 (m)

1 : LOS integrated conc. (mg/m**2)

1 : LOS integrated dosage (mg-3/m**2)

1 : x-coord. of 1st end-point for LOS1 (m)

1 : y-coord. of 1st end-point for LOS1 (m)

1 : x-coord. of 2nd end-point for LOS1 (m)

1 : y-coord. of 2nd end-point for LOS1 (m)

1 : LOS integrated conc. (mg/m**2)

1 : LOS integrated dosage (mg-3/m**2)

1 : x-coord. of 1st end-point for LOS1 (m)

1 : y-coord. of 1st end-point for LOS1 (m)

1 : x-coord. of 2nd end-point for LOS1 (m)

Development Test 1 of the Man-Portable Smoke Generators (MX49, Fogroll part of fogroll-IR, FORFC)

10 : number of trials included in DDA
 6 : time zone designation

40.20 : latitude (deg)
 113.00 : longitude (deg)

FE26a	FE27a	FE28a	FE29a	FE30a	FE31a	FE32a	FE33a	FE34a	FE37a
5	5	5	5	5	5	5	6	6	6
28	29	29	29	29	29	29	31	31	31
81	81	81	81	81	81	81	81	81	81
15	15	15	15	15	15	15	15	15	15
34	34	34	34	34	34	34	34	34	34
1	1	1	1	1	1	1	1	1	1
-296.6	-296.6	-296.6	-296.6	-296.6	-296.6	-296.6	-290.0	-342.5	-255.0
-78.6	-78.6	-78.6	-78.6	-78.6	-78.6	-78.6	-15.0	-104.1	-55.6
0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38
240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0
13.483	13.483	13.483	13.483	13.483	13.483	13.483	13.568	11.244	13.591
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230
300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00	300.00
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
3.30	3.30	3.30	3.30	3.30	3.30	3.30	3.70	3.60	5.40
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.70	3.60	5.40
332.0	332.0	332.0	332.0	332.0	332.0	332.0	354.0	328.0	351.0
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.20	13.20	16.50
99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90	99.90
2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
420.0	420.0	420.0	420.0	420.0	420.0	420.0	420.0	420.0	420.0
0.088	0.088	0.088	0.088	0.088	0.088	0.088	0.075	0.075	0.088
0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300	0.0300
99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000
99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000	99.9000
0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0	240.0
2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44
0	0	0	0	0	0	0	0	0	0
3	3	3	3	3	3	3	3	3	3
-517.5	-517.5	-517.5	-517.5	-517.5	-517.5	-517.5	-517.5	-517.5	-517.5
-304.0	-304.0	-304.0	-304.0	-304.0	-304.0	-304.0	-304.0	-304.0	-304.0
-80.2	-80.2	-80.2	-80.2	-80.2	-80.2	-80.2	-80.2	-80.2	-80.2
-61.6	-61.6	-61.6	-61.6	-61.6	-61.6	-61.6	-61.6	-61.6	-61.6
9.400E+04	2.570E+05	2.460E+05	1.800E+05	1.410E+05	1.300E+05	1.500E+05	1.190E+05	1.660E+05	1.400E+05
-488.4	-488.4	-488.4	-488.4	-488.4	-488.4	-488.4	-488.4	-488.4	-488.4
-356.5	-356.5	-356.5	-356.5	-356.5	-356.5	-356.5	-356.5	-356.5	-356.5
-51.1	-51.1	-51.1	-51.1	-51.1	-51.1	-51.1	-51.1	-51.1	-51.1
-114.1	-114.1	-114.1	-114.1	-114.1	-114.1	-114.1	-114.1	-114.1	-114.1
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
4.700E+04	2.530E+05	2.180E+05	9.500E+04	5.200E+04	8.300E+04	8.900E+04	7.200E+04	1.210E+05	1.230E+05
-459.3	-459.3	-459.3	-459.3	-459.3	-459.3	-459.3	-459.3	-459.3	-459.3
-409.0	-409.0	-409.0	-409.0	-409.0	-409.0	-409.0	-409.0	-409.0	-409.0
-22.0	-22.0	-22.0	-22.0	-22.0	-22.0	-22.0	-22.0	-22.0	-22.0
-166.6	-166.6	-166.6	-166.6	-166.6	-166.6	-166.6	-166.6	-166.6	-166.6
99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9	99.9
-9.990E+01	2.190E+05	1.210E+05	5.100E+04	2.400E+04	5.600E+04	5.100E+04	3.700E+04	9.200E+04	8.100E+04

Atterbury-87

4 : number of trials included in DDA
 6 : time zone designation (CDT)
 39.20 : latitude (deg)
 85.90 : longitude (deg)

at1	at2	at3	at4	trial ID
11	11	11	11	month
3	4	4	4	day
87	87	87	87	year
10	9	15	15	hour
31	36	25	25	minute
1	1	1	1	no. of sources
0.0	0.0	0.0	0.0	x-coord. of source (m)
0.0	0.0	0.0	0.0	y-coord. of source (m)
1.00	1.00	1.00	1.00	source elevation (m)
34.600	26.700	40.700	42.200	emission rate (g/s)
3354.0	1650.0	2892.0	4572.0	total mass emitted (kg)
115.9	44.0	117.8	193.0	sigma-0 at the source (m)
0.000	0.000	0.000	0.000	sigma-1 at the source (m)
0.000	0.000	0.000	0.000	sigma-2 at the source (m)
0.000	0.000	0.000	0.000	sigma-3 at the source (m)
-99.9	-99.9	-99.9	-99.9	ambient pressure (atm)
43.0	25.0	43.0	40.0	relative humidity (%)
298.35	293.15	298.45	281.15	temperature at level #1 (K)
2.00	2.00	2.00	2.00	measuring height for temperature #1 (m)
296.14	193.25	300.34	280.26	temperature at level #2 (K)
10.00	10.00	10.00	10.00	measuring height for temperature #2 (m)
5.50	5.10	4.70	1.60	wind speed (m/s) at a tower
5.50	5.10	4.70	1.60	measuring height for wind data (m)
239.0	249.0	261.0	240.0	domain-averaged wind speed (m/s)
1.52	1.17	1.26	0.70	domain-averaged wind direction (deg)
16.20	11.00	18.60	35.40	domain-averaged sigma-u (deg)
8.00	6.20	8.20	14.90	domain-averaged sigma-theta (deg)
10.00	10.00	10.00	10.00	measuring ht for domain-avg wind speed (m)
4554.0	2450.0	4092.0	5772.0	averaging time for domain-avg data (s)
0.113	0.119	0.181	0.103	wind speed power law exponent
0.2000	0.2000	0.2000	0.2000	surface roughness (m)
0.610	0.590	0.440	0.280	friction velocity (m)
-0.0139	-0.0196	-0.0041	-0.0831	Inverse Monin-Obukhov length (1/m)
0.20	0.20	0.20	0.20	albedo
1.00	1.00	1.00	1.00	moisture availability
2.00	2.00	2.00	2.00	Bowen ratio
668.0	305.0	1135.0	557.0	mixing height (m)
-99.9	-99.9	-99.9	-99.9	cloud cover (%)
3	3	4	2	P-G stability class
3354.0	1450.0	2892.0	4572.0	averaging time for concentration (s)
1.00	1.00	1.00	1.00	suggested receptor height (m)
0	0	0	0	no. of distances downwind
5	5	5	5	no. of lines-of-sight
-14.7	-14.7	35.7	35.7	x-coord. of 1st end-point for LOS1 (m)
85.6	85.6	33.5	33.5	y-coord. of 1st end-point for LOS1 (m)
76.3	76.3	127.3	127.3	x-coord. of 2nd end-point for LOS1 (m)
-6.8	-6.8	-58.9	-58.9	y-coord. of 2nd end-point for LOS1 (m)
1.148E+03	1.916E+03	1.604E+03	2.658E+03	LOS integrated conc. (mg/m**2)
3.838E+06	3.161E+06	4.638E+06	1.215E+07	LOS integrated dosage (mg-s/m**2)
193.4	193.4	141.3	141.3	x-coord. of 1st end-point for LOS1 (m)
175.0	175.0	225.4	225.4	x-coord. of 2nd end-point for LOS1 (m)
-44.3	-44.3	-96.4	-96.4	y-coord. of 1st end-point for LOS1 (m)
8.410E+02	4.705E+02	1.683E+03	1.912E+03	LOS integrated conc. (mg/m**2)
2.821E+06	7.764E+05	4.866E+06	8.740E+06	LOS integrated dosage (mg-s/m**2)
-2.7	-2.7	47.7	47.7	x-coord. of 1st end-point for LOS1 (m)
352.9	352.9	300.8	300.8	y-coord. of 1st end-point for LOS1 (m)
314.1	314.1	384.5	384.5	x-coord. of 2nd end-point for LOS1 (m)
16.1	16.1	-36.0	-36.0	y-coord. of 2nd end-point for LOS1 (m)
2.138E+02	1.150E+02	4.318E+02	3.252E+02	LOS integrated conc. (mg/m**2)
7.165E+05	1.899E+05	1.249E+06	1.487E+06	LOS integrated dosage (mg-s/m**2)
548.3	548.3	496.2	496.2	x-coord. of 1st end-point for LOS1 (m)
523.3	523.3	573.7	573.7	x-coord. of 2nd end-point for LOS1 (m)
99.9	99.9	47.8	47.8	y-coord. of 1st end-point for LOS1 (m)
3.619E+01	3.825E+01	8.229E+01	9.440E+01	LOS integrated conc. (mg/m**2)
1.214E+05	6.311E+04	2.380E+05	4.316E+05	LOS integrated dosage (mg-s/m**2)
332.6	332.6	303.0	303.0	x-coord. of 1st end-point for LOS1 (m)
625.4	625.4	573.3	573.3	x-coord. of 2nd end-point for LOS1 (m)
555.5	555.5	605.9	605.9	y-coord. of 1st end-point for LOS1 (m)
403.2	403.2	351.1	351.1	y-coord. of 2nd end-point for LOS1 (m)
2.034E+01	2.891E+01	1.122E+01	1.680E+01	LOS integrated conc. (mg/m**2)
8.821E+04	4.771E+04	3.246E+04	7.881E+04	LOS integrated dosage (mg-s/m**2)

Atterbury-87

5 : number of trials included in DDA
 6 : time zone designation (CDT)
 7 : latitude (deg)
 8 : longitude (deg)

39.20 : latitude (deg)
 05.30 : longitude (deg)

atc : trial ID
 11 : month
 12 : day
 07 : year
 10 : hour
 21 : minute

0.0 : x-coord. of source (m)
 0.0 : y-coord. of source (m)
 1.50 : source elevation (m)
 78.300 : emission rate (g/s)
 2580.0 : emission duration (s)
 202.0 : total mass emitted (kg)
 0.000 : sign0 at the source (m)
 0.000 : sign0 at the source (m)
 -99.9 : ambient pressure (atm)
 45.0 : relative humidity (%)
 266.05 : temperature at level #1 (K)
 2.00 : measuring height for temperature #1 (m)
 265.31 : temperature at level #2 (K)
 10.00 : measuring height for temperature #2 (m)
 4.30 : wind speed (m/s) at a tower
 4.30 : domain-averaged wind speed (m/s)
 4.30 : domain-averaged wind direction (deg)
 1.08 : domain-averaged sigma-u (m/s)
 15.50 : domain-averaged sigma-theta (deg)
 9.90 : domain-averaged sigma-phi (deg)
 3780.0 : averaging time for domain-avg wind speed (m)
 0.137 : wind speed power law exponent
 0.2000 : surface roughness (m)
 0.570 : inverse Monin-Obukhov length (1/m)
 -0.0159 : albedo
 1.00 : moisture availability
 2.00 : Bowen ratio
 560.0 : mixing height (m)
 -99.9 : cloud cover (%)

3 : P-G stability class
 2580.0 : averaging time for concentration (s)
 1.00 : suggested receptor height (m)
 0 : no. of distances downwind
 4 : no. of lines-of-sight
 9.4 : x-coord. of 1st end-point for LOS1 (m)
 59.8 : y-coord. of 1st end-point for LOS1 (m)
 101.0 : x-coord. of 2nd end-point for LOS1 (m)
 -32.6 : y-coord. of 2nd end-point for LOS1 (m)
 3.365E+03 : LOS integrated conc. (ug/m**2)
 4.681E+05 : LOS integrated dosage (mg-s/m**2)
 -20.4 : x-coord. of 1st end-point for LOS1 (m)
 157.6 : y-coord. of 1st end-point for LOS1 (m)
 189.1 : x-coord. of 2nd end-point for LOS1 (m)
 -70.1 : y-coord. of 2nd end-point for LOS1 (m)
 1.249E+03 : LOS integrated conc. (ug/m**2)
 3.275E+06 : LOS integrated dosage (mg-s/m**2)
 21.4 : x-coord. of 1st end-point for LOS1 (m)
 327.1 : y-coord. of 1st end-point for LOS1 (m)
 358.2 : x-coord. of 2nd end-point for LOS1 (m)
 -9.7 : y-coord. of 2nd end-point for LOS1 (m)
 5.046E+02 : LOS integrated conc. (ug/m**2)
 1.302E+06 : LOS integrated dosage (mg-s/m**2)
 95.8 : x-coord. of 1st end-point for LOS1 (m)
 522.5 : y-coord. of 1st end-point for LOS1 (m)
 547.4 : x-coord. of 2nd end-point for LOS1 (m)
 74.1 : y-coord. of 2nd end-point for LOS1 (m)
 1.274E+02 : LOS integrated conc. (ug/m**2)
 3.287E+05 : LOS integrated dosage (mg-s/m**2)
 -99.9 : x-coord. of 1st end-point for LOS1 (m)
 -99.9 : y-coord. of 1st end-point for LOS1 (m)
 -99.9 : x-coord. of 2nd end-point for LOS1 (m)
 -99.9 : y-coord. of 2nd end-point for LOS1 (m)
 -9.990E+01 : LOS integrated conc. (ug/m**2)
 -9.990E+01 : LOS integrated dosage (mg-s/m**2)

atc : trial ID
 11 : month
 12 : day
 07 : year
 10 : hour
 21 : minute

0.0 : x-coord. of source (m)
 0.0 : y-coord. of source (m)
 1.50 : source elevation (m)
 79.700 : emission rate (g/s)
 2742.0 : emission duration (s)
 218.5 : total mass emitted (kg)
 0.000 : sign0 at the source (m)
 0.000 : sign0 at the source (m)
 -99.9 : ambient pressure (atm)
 49.0 : relative humidity (%)
 266.45 : temperature at level #1 (K)
 2.00 : measuring height for temperature #1 (m)
 275.45 : temperature at level #2 (K)
 10.00 : measuring height for temperature #2 (m)
 4.30 : wind speed (m/s) at a tower
 4.30 : domain-averaged wind speed (m/s)
 4.30 : domain-averaged wind direction (deg)
 1.28 : domain-averaged sigma-u (m/s)
 13.20 : domain-averaged sigma-theta (deg)
 9.30 : domain-averaged sigma-phi (deg)
 10.00 : averaging time for domain-avg wind speed (m)
 0.132 : wind speed power law exponent
 0.2000 : surface roughness (m)
 0.570 : inverse Monin-Obukhov length (1/m)
 -0.0147 : albedo
 1.00 : moisture availability
 2.00 : Bowen ratio
 434.0 : mixing height (m)
 -99.9 : cloud cover (%)

4 : P-G stability class
 2190.0 : averaging time for concentration (s)
 1.00 : suggested receptor height (m)
 0 : no. of distances downwind
 4 : no. of lines-of-sight
 -282.0 : x-coord. of 1st end-point for LOS1 (m)
 -389.9 : y-coord. of 1st end-point for LOS1 (m)
 -190.4 : x-coord. of 2nd end-point for LOS1 (m)
 -482.3 : y-coord. of 2nd end-point for LOS1 (m)
 3.336E+01 : LOS integrated conc. (ug/m**2)
 3.468E+04 : LOS integrated dosage (mg-s/m**2)
 -311.8 : x-coord. of 1st end-point for LOS1 (m)
 -282.1 : y-coord. of 1st end-point for LOS1 (m)
 -92.3 : x-coord. of 2nd end-point for LOS1 (m)
 -519.8 : y-coord. of 2nd end-point for LOS1 (m)
 1.216E+05 : LOS integrated conc. (ug/m**2)
 2.118E+05 : LOS integrated dosage (mg-s/m**2)
 -270.0 : x-coord. of 1st end-point for LOS1 (m)
 -122.6 : y-coord. of 1st end-point for LOS1 (m)
 66.8 : x-coord. of 2nd end-point for LOS1 (m)
 -459.4 : y-coord. of 2nd end-point for LOS1 (m)
 5.690E+01 : LOS integrated conc. (ug/m**2)
 1.246E+05 : LOS integrated dosage (mg-s/m**2)
 -195.6 : x-coord. of 1st end-point for LOS1 (m)
 72.8 : y-coord. of 1st end-point for LOS1 (m)
 256.0 : x-coord. of 2nd end-point for LOS1 (m)
 -375.6 : y-coord. of 2nd end-point for LOS1 (m)
 8.213E+02 : LOS integrated conc. (ug/m**2)
 1.795E+06 : LOS integrated dosage (mg-s/m**2)
 -99.9 : x-coord. of 1st end-point for LOS1 (m)
 -99.9 : y-coord. of 1st end-point for LOS1 (m)
 -99.9 : x-coord. of 2nd end-point for LOS1 (m)
 -99.9 : y-coord. of 2nd end-point for LOS1 (m)
 -9.990E+01 : LOS integrated conc. (ug/m**2)
 -9.990E+01 : LOS integrated dosage (mg-s/m**2)