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# Derivation of the Generalized, Average Euclidean Distance Function for the PDI Model

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## **PREFACE**

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13. ABSTRACT (Maximum 200 words)

This report derives distance functions that form the basis for the Population Density Index (PDI) model, which is a three-parameter square-root model for measuring discrete spatial density in finite populations. The PDI and its methods have been applied to facilities layout methodologies in submarine environments at the Naval Undersea Warfare Center Division, Newport, RI, resulting in several U.S. patent applications. The emphasis here is on the "micro-population" model in which the linear units are "feet." The derivations relate Cartesian rectangular coordinate systems to uniform unit and nonunit lattices, as well as to the nonlattice distribution. Other proofs relate to the bounds of the calculated density measure and the density rate index called "effective distance." Alternative distance functions are discussed, and examples of the numerical calculations are provided. Also derived is the algorithm for selecting a rectangular lattice conformal to a quadrilateral area and for calculating interpoint distance in a PDI lattice. A table of computer-generated unit lattice average Euclidean distances for up to 10,000 density points is included.

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# DERIVATION OF THE GENERALIZED, AVERAGE EUCLIDEAN DISTANCE FUNCTION FOR THE PDI MODEL

## INTRODUCTION

Research has demonstrated spatial density (or crowding) to be a significant stressor in animal and human populations (Galle, Grove, and McPherson, 1972; Baum and Epstein, 1975). In previous papers, the author formulated and tested a mathematical model and methodology for measuring discrete spatial density in human populations (O'Brien (1989, 1990a, 1990b)). The model, called the population density index (PDI) model, was demonstrated to provide a more accurate and flexible approach for discrete spatial density measurement than the conventional formulation. The traditional approach to measuring human physical density involves two parameters: the number of persons ( $n$ ) and the geometric area ( $A$ ) in which the persons dwell. The equation  $D = n/A$  serves as the conceptual and computational definition for "density," "congestion," "population density," or "physical crowding," each term used interchangeably. In contrast, the PDI model is based on three parameters:  $n$ ,  $A$ , and inter-object distance. The derivation of the PDI model metrics is patterned on the "square-root law" of average distances used in the physical sciences. The capability to model inter-object distance within a defined geometric plane is a significant enhancement to discrete spatial density measurement. In O'Brien (1991a), the PDI model was generalized to any finite number of density points (i.e., people).

The motivation for developing the PDI formula and model was the need to be able to measure crowding among people from variable spatial configurations such as in a typical dynamic workplace environment. The conventional density model assumes that a static description is adequate without taking into account the way in which people use an environment over time.

The PDI model has been used at the Naval Undersea Warfare Center (NUWC) Division, Newport, for density measurement (O'Brien and Kanter, 1988; Kanter and O'Brien, 1989a; 1989b) in submarine attack center concept of operations experiments (Wallin, 1987). Practical applications of the PDI model resulting from research at NUWC have been documented for a variety of disciplines in several U.S. patent applications (O'Brien, 1991c, 1991d, 1991e, 1991f).

The purpose of this report is to provide a more rigorous derivation of the PDI model than currently exists. The basis of the PDI model is the distance function in Euclidean space. All of

the measures in the model are related to distance. Thus, an attempt is made to characterize the PDI distance function in  $R^2$  (two-dimensional Euclidean space).

## DERIVATION OF THE DISTANCE FUNCTION

### GENERAL CASE LATTICES

The notation and structure of this section is patterned on Morrey (1962, Chapter 8, "The Definite Integral"), where the theory of area and concept of functional uniform continuity are developed in detail. Also, the ideas of inner and outer areas of bounded sets and the idea of a planar figure developed in Morrey are germane to the present development.

In the X-Y Euclidean plane (quadrant I) of figure 1, any two consecutive abscissa (horizontal) or ordinate (vertical) points (denoted by a large dot  $\bullet$ ) are assumed to be equidistant with interpoint spacing parameter  $\delta$ . That is, the directed distances of the collinear point pairs  $(P_1P_2) = [(x_k, y_l), (x_{k+1}, y_l)]$  and  $(P_3P_4) = [(x_m, y_j), (x_m, y_{j+1})]$  are

$$\overline{P_1P_2} = |x_{k+1} - x_k| = \delta, \tag{1}$$

$$\overline{P_3P_4} = |y_{j+1} - y_j| = \delta,$$

where  $x_k$  is a representative abscissa and  $y_j$  is a representative ordinate;  $(x_k, y_j) > 0$ . Generally,  $x_k, y_j$  will not be lattice (integer) points. In this report the units of the interpoint distance parameter  $\delta$  for human populations are assumed to be feet ( $\delta \geq 1$ ).

The interior rectangular lattice shown in figure 1 consists of  $n$  (a nonprime number) finite points arranged uniformly with  $R$  row (horizontal) and  $C$  column (vertical) points such that  $n = RC$  ( $n \geq 2$ ). The selection of an  $RC$  configuration and the computation of  $\delta$  are explained in appendix A.

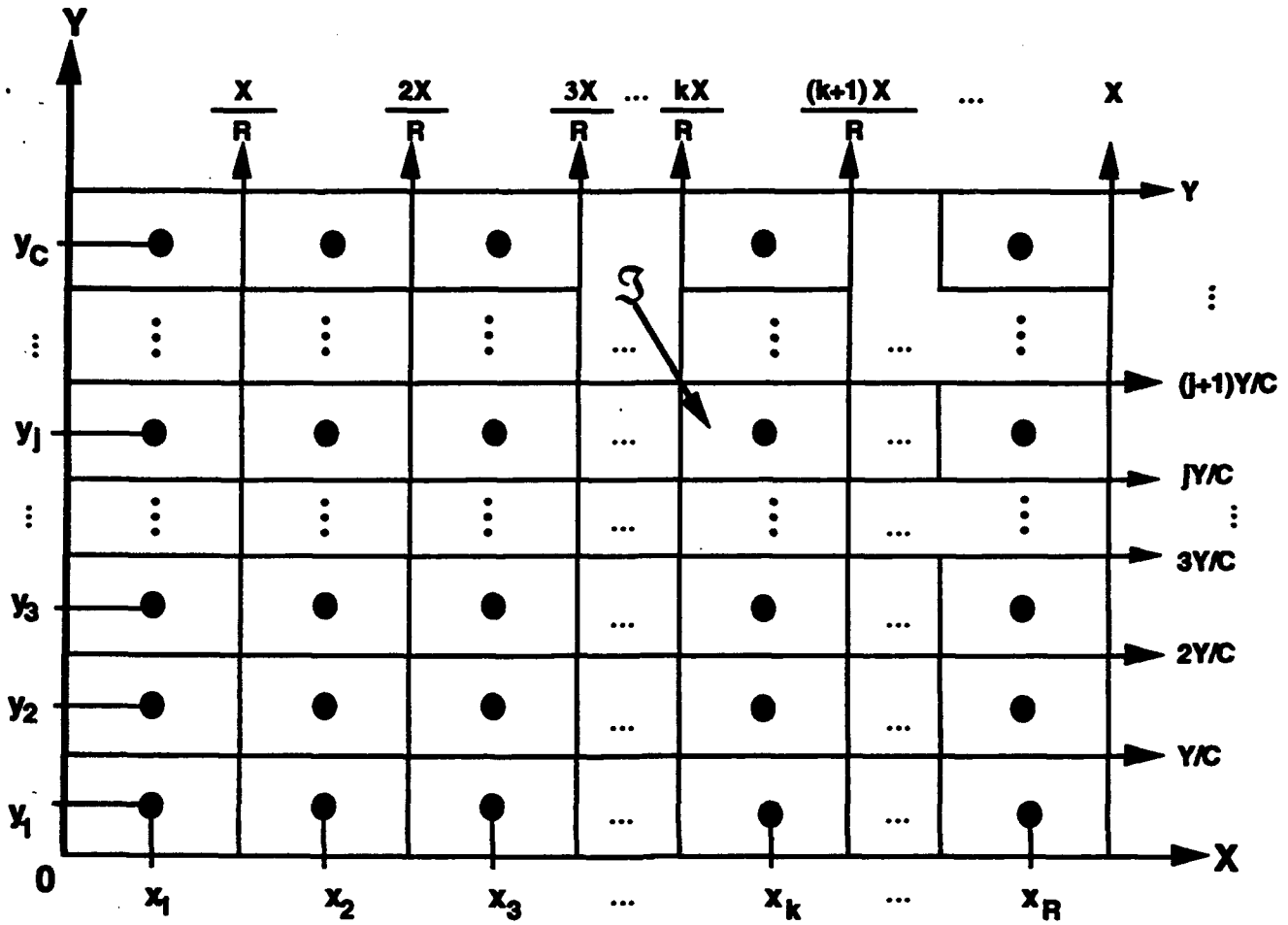


Figure 1. General Case Lattice

For a representative region  $S$  bounded by the nonnegative curves (see figure 1)

$$f_A(x) = (j+1)Y/C \tag{2}$$

$$g_A(x) = jY/C, \quad g_A(x) < f_A(x),$$

$$kX/R \leq x \leq (k+1)X/R, \quad 0 \leq k \leq R-1, 0 \leq j \leq C-1,$$

the area  $A(S)$  is defined as

$$A(S) = \int_{kX/R}^{(k+1)X/R} [f_A(x) - g_A(x)] dx, \tag{3}$$

$$= XY/RC = A/n,$$



which is seen to be a rectangle. For human populations with feet as the linear units, the restriction will be placed on the value of  $A/n$ ; viz.,  $A \geq n$ . When  $A = n$ , the RC rectangular or square uniform discrete distribution is referred to as a "unit lattice"; otherwise, the homogeneous distribution of points is called a "nonunit lattice." The distinction will be understood in context. Each such rectangle will be obtained by dividing the total study area  $n[A(S)]$  into  $n = RC$  partitioned rectangles each, with area given by equation (3).

The connected density points in each of the horizontal and vertical intervals are defined by relations (or multiple-valued discrete constant functions):

$$\begin{aligned} f(R) = X &= (R - 1)\delta + p, \quad p > 0, \\ f(C) = Y &= (C - 1)\delta + q, \quad q > 0. \end{aligned} \tag{4}$$

Equations (4) indicate that each X or Y interval consists of two components: the length of the density points segment  $[(R - 1)\delta$  or  $(C - 1)\delta]$  and an excess factor ( $p$  or  $q$ ). The region outside the perimeter of the uniform point arrangement [equal to  $A - (R - 1)(C - 1)\delta^2$ ] is required to accommodate environmental objects (furniture, equipment, displays, etc.). Each of the CX intervals and RY intervals is defined by the constant functions in equations (4). The interval X will be partitioned into R subintervals, each subpartition of which will have the length shown in figure 1, and Y will be similarly divided and have the length shown in figure 1.

The derivation of the coordinate system for the general-case lattice will allow a precise graph to be drawn of any uniform rectangular distribution on a rectangular Cartesian X-Y coordinate system such that the interior RC lattice is contained within the XY exterior region. The coordinates of the density points derived from equation (4) will be generated by

$$\begin{aligned} x_k &= p/2 + (k - 1)\delta, \quad 1 \leq k \leq R, \\ y_j &= q/2 + (j - 1)\delta, \quad 1 \leq j \leq C. \end{aligned} \tag{5}$$

Then, the coordinate system for the general case will be defined as

$$\begin{aligned} (x_k, y_j) &= [(x_1, y_1), (x_2, y_1), \dots, (x_k, y_j), \dots, (x_R, y_C)] \\ &= \left[ \left( \frac{p}{2}, \frac{q}{2} \right), \left( \frac{p}{2} + \delta, \frac{q}{2} \right), \dots, \left( \frac{p}{2} + (k - 1)\delta, \frac{q}{2} + (j - 1)\delta \right), \dots, \right. \\ &\quad \left. \left( \frac{p}{2} + (R - 1)\delta, \frac{q}{2} + (C - 1)\delta \right) \right]. \end{aligned} \tag{6}$$

The coordinate system of equation (6) applies to either a unit or nonunit lattice because it is derived from the general case. An example of the use of equation (6) is depicted in figure 2. The coordinates were generated from the following assumptions:  $n = 6$ ;  $R = 3$ ,  $C = 2$  (from equation (A-4) in appendix A);  $A = X \times Y = 16 \times 6$ ;  $p/2 = 4$ ,  $q/2 = 1$  (from (4));  $\delta = 4$  (from equation (A-5) in appendix A). Then the coordinate points are generated by  $x_k = 4 + 4(k - 1)$ ;  $y_j = 1 + 4(j - 1)$ . The plot points are obtained from all  $k \times j$  combinations ( $k = 1, 2, 3$ ;  $j = 1, 2$ ).

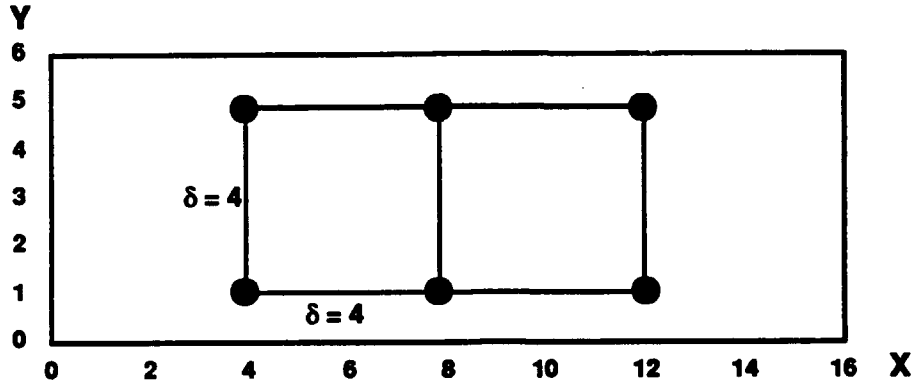


Figure 2. Example of General Case PDI Graph

### SPECIAL CASE LATTICES

Each density point ( $\bullet$ ) is now assumed to be the centroid (center of mass) bounded by its respective planar region (see figure 3). Let a representative region be called  $S$ . The area of  $S$  can be determined by first defining the nonnegative curves as the boundaries of  $S$ :

$$f_B(x) = (j + 1)\delta, \tag{7}$$

$$g_B(x) = j\delta, \quad g_B(x) < f_B(x),$$

$$k\delta \leq x \leq (k + 1)\delta, \quad 0 \leq k \leq R - 1, \quad 0 \leq j \leq C - 1.$$

The special case of equation (7) can be derived from equation (2) by assuming that  $\delta = p = q = X/R = Y/C$  in equation (4) of the general case (i.e., proportionate commensurability between the dimensions of the outer and inner rectangular areas).

The area of  $S$  is then found by integrating between the curves  $f_B(x)$  and  $g_B(x)$  in the  $x$  interval, and applying the Fundamental Theorem of Calculus:

$$A(S) = \int_{k\delta}^{(k+1)\delta} [f_B(x) - g_B(x)] dx = \delta^2, \quad \delta^2 \geq 1. \quad (8)$$

This is intuitively the area of a square figure. The figure will be obtained by dividing the total area  $n[A(S)]$  into  $n = RC$  partitions after determining which lattice configuration will accommodate best the  $n$  points into a rectangular configuration with associated interpoint spacing parameter  $\delta$  (see appendix A). Note that for commensurate (unit or nonunit) lattices, the interpoint spacing parameter is related to the region in equation (8).

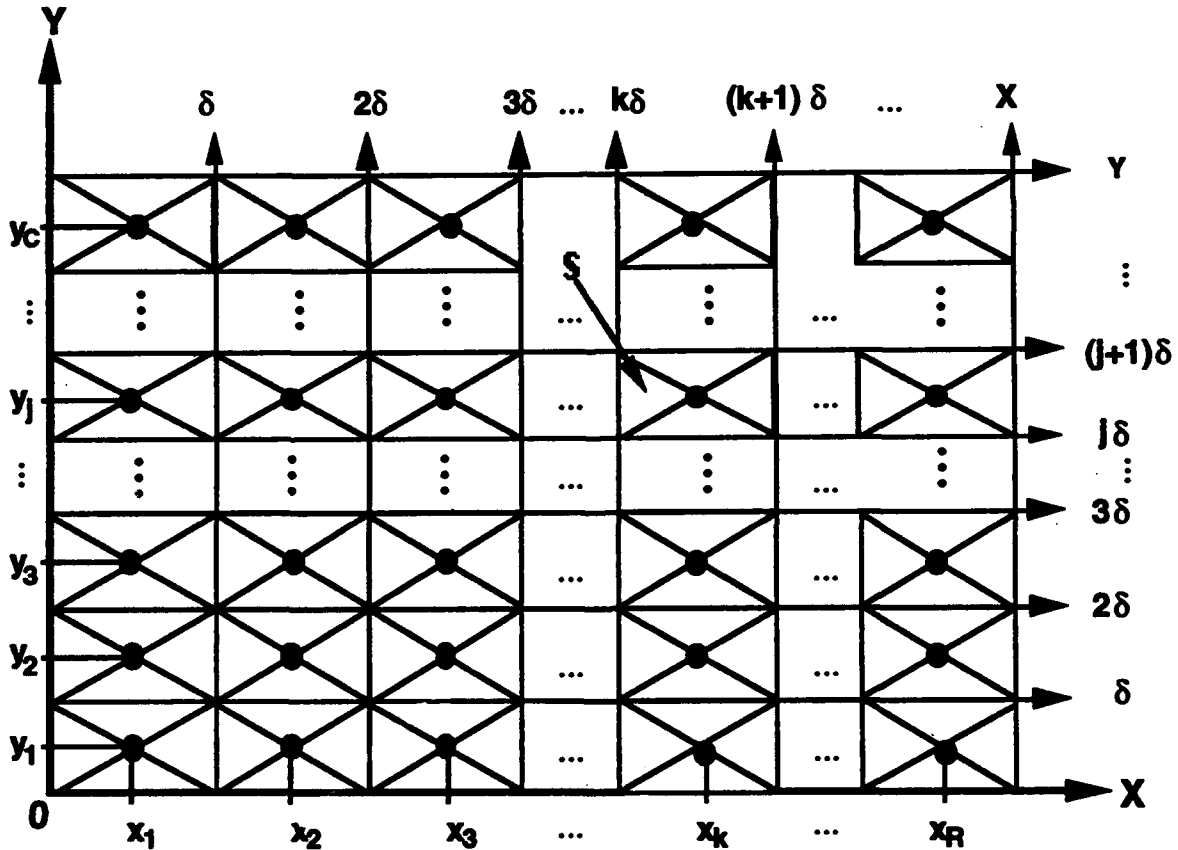


Figure 3. Special Case Lattice

Bers (1969, Vol. II, chapter 8, section 8, "Centroids of Plane Regions and Curves") gives the following definitional formulas for determining the coordinate points  $(x_k, y_j)$  of the centroid in region S:

$$(x_k, y_j): x_k = \frac{\int_{k\delta}^{(k+1)\delta} x [f_B(x) - g_B(x)] dx}{\int_{k\delta}^{(k+1)\delta} [f_B(x) - g_B(x)] dx} = \frac{\delta(2k+1)}{2} \quad (9)$$

$$(x_k, y_j): y_j = \frac{\int_{k\delta}^{(k+1)\delta} 1/2 [f_B(x)^2 - g_B(x)^2] dx}{\int_{k\delta}^{(k+1)\delta} [f_B(x) - g_B(x)] dx} = \frac{\delta(2j+1)}{2}$$

Here,  $(x_k, y_j)$  represents the rule for locating all and every density point (centroid) in the entire XY area, given concisely as

$$\begin{aligned} (x_k, y_j) &= \left[ \left( \frac{\delta}{2} + (k-1)\delta \right), \left( \frac{\delta}{2} + (j-1)\delta \right) \right] \\ &= [(x_1, y_1), (x_2, y_1), (x_3, y_1), \dots, (x_k, y_1), \\ &\quad (x_1, y_2), \dots, (x_k, y_2), \dots, (x_k, y_j), \dots, (x_R, y_C)] \\ &= \left[ \left[ \frac{\delta}{2}, \frac{\delta}{2} \right], \left[ \frac{3\delta}{2}, \frac{\delta}{2} \right], \left[ \frac{5\delta}{2}, \frac{\delta}{2} \right], \dots, \left[ \frac{\delta(2R-1)}{2}, \frac{\delta}{2} \right], \right. \\ &\quad \left. \left[ \frac{\delta}{2}, \frac{3\delta}{2} \right], \dots, \left[ \frac{\delta(2R-1)}{2}, \frac{3\delta}{2} \right], \dots, \right. \\ &\quad \left. \left[ \frac{\delta}{2} + (k-1)\delta, \frac{\delta}{2} + (j-1)\delta \right], \dots, \left[ \frac{\delta(2R-1)}{2}, \frac{\delta(2C-1)}{2} \right] \right], \\ &1 \leq k \leq R, \quad 1 \leq j \leq C. \end{aligned} \quad (10)$$

The coordinate system of equation (10) applies to unit lattices and commensurate nonunit lattices. Figure 4 is an example of equation (10) applied to a 3 x 2 unit lattice ( $\delta = 1$  from equation (A-5) in appendix A). Note that  $X/R = Y/C = p = q = \delta = \sqrt{XY/RC} = 1$  because all unit lattices are commensurate. The graph is plotted from equation (10) by  $x_k = k - 0.5$ ;  $y_j = j - 0.5$  ( $k = 1,2,3$ ;  $j = 1,2$ ).

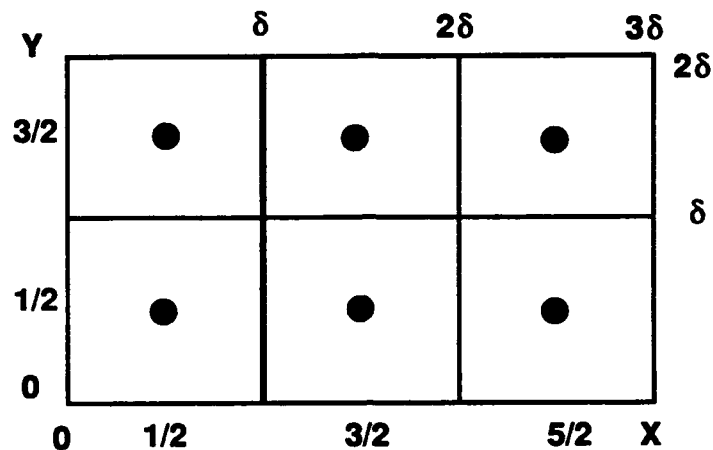


Figure 4. Example of Special Case PDI Graph (Unit Lattice)

Figure 5 is an example of a graph for a nonunit commensurate lattice with  $n = 15$  points within area of 40 ft x 24 ft. Note that  $X/R = Y/C = p = q = \delta = \sqrt{XY/RC} = 8$ . Plot points are generated from equation (10):  $x_k = 4 + 8(k - 1)$ ;  $y_j = 4 + 8(j - 1)$ .

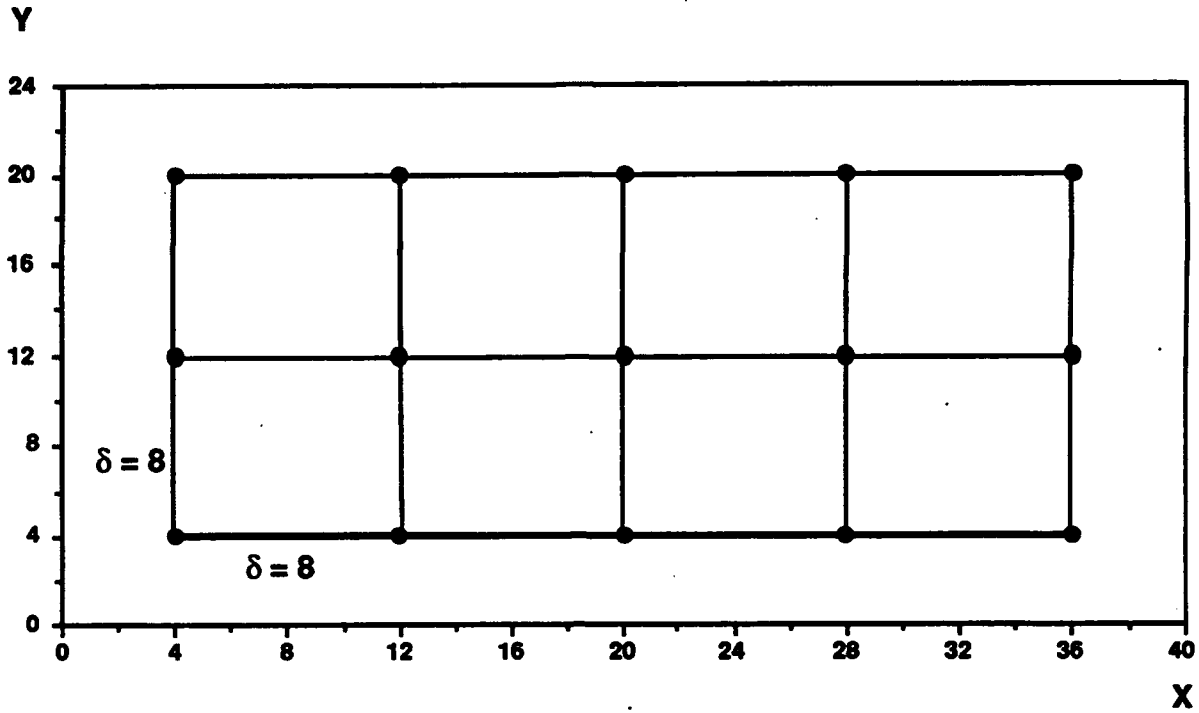


Figure 5. Example of Special Case PDI Graph (Commensurate Nonunit Lattice)

### GENERALIZED DISTANCE FUNCTION IN A LATTICE

Since the coordinate points in the PDI lattice can now be specified completely, the PDI “exact” and “approximate” distance formulas can be derived (O’Brien, 1990b, 1991b). Here is derived the generalized, Euclidean distance formula for any PDI lattice (nonunit lattice and thereby the unit lattice as a special case) and any nonuniform distribution. First shown is the derivation for a lattice using the general case notation system. The derivation applies equally to the special case by assuming commensurability.

Let any density point in the X-Y plane be called  $(x_k, y_j)$  and let a second distinct point be called  $(x_{k+i}, y_{j+l})$ . Then, from equation (6),

$$(x_k, y_j) = (p/2 + (k - 1)\delta, q/2 + (j - 1)\delta), \quad (11)$$

$$(x_{k+i}, y_{j+l}) = (p/2 + (k + i - 1)\delta, q/2 + (j + l - 1)\delta),$$

$$1 \leq k \leq R - 1, \quad 1 \leq j \leq C - 1,$$

$$2 \leq k+i \leq R, \quad 2 \leq j+l \leq C.$$

Bers (1969, Vol. I) shows that the classical Pythagorean distance formula for any two points in a Cartesian plane can generally be derived from the integral calculus arc length formula, given for our notation as

$$L = \int_{x_k}^{x_{k+i}} \sqrt{1 + [f'(x)]^2} dx. \quad (12)$$

The quantity  $f'(x)$  is the first derivative of the function  $f(x)$ , taken to be a generalized single-valued relation for two points in a Euclidean X-Y plane specified by the first degree equation  $f(x) = a + bx$ , for the slope intercept  $a$  and linear slope  $b$ .

Since  $f'(x) = \frac{d[f(x)]}{dx} = D_x(a + bx) = b$ , the constant slope of the points in equation (11)

can be defined as  $b = \frac{y_{j+l} - y_j}{x_{k+i} - x_k} = \frac{\delta l}{\delta i}$ . Then,

$$\begin{aligned} L &= \int_{x_k}^{x_{k+i}} \sqrt{1 + \left(\frac{\delta l}{\delta i}\right)^2} dx, \\ &= \delta \sqrt{i^2 + l^2}, \end{aligned} \quad (13)$$

which is seen to be of the form for the standard bivariate Pythagorean theorem scaled by a constant:

$$L = \delta \sqrt{(x_{k+i} - x_k)^2 + (y_{j+l} - y_j)^2}. \quad (14)$$

Bers (1969, Vol. I, p. 279) terms equation (12) the "length formula." It may also be viewed as an average -- the average length of one pair of points. The length (distance) between any one pair of points in the uniform RC lattice can be generalized to an average among all possible pairs of RC points since each point pair defines a simple linear function each of which possesses a piecewise continuous first derivative. The average pair-to-pair distance, summed over all pairs of points, will be the average of all the line-to-line curves (total length), since the connected graph defines a multiple-valued relation (Bers, 1969, Vol. I, page 279). That is, the uniform average distance in the total lattice is

$$\bar{d} = \frac{\sum_{k=j=1}^n L_{kj}}{C(n,2)}, \quad (15)$$

where

$$C(n,2) = \frac{(RC)!}{2!(RC-2)!} = \frac{n(n-1)}{2}, \quad (n \geq 2), \quad (16)$$

is the combinatorial expression specifying the total number of nonredundant pairwise-connected lines from  $n$  nodes and the exact summation index limits are given in equation (11). The uniform lattice distance equation (15) can be further expressed in a more computational convenient form as

$$\bar{d} = \delta \bar{\Delta}, \quad (17)$$

where  $\delta$  is given in appendix A and  $\bar{\Delta}$  is the unit lattice average distance, which has been derived in O'Brien (1991a) as

$$\bar{\Delta} = \frac{12 \sum_{i=1}^{R-1} \sum_{j=1}^{C-1} (R-i)(C-j) \sqrt{i^2 + j^2} + RC(R^2 + C^2 - 2)}{3(RC)(RC-1)}, \quad (18)$$

where  $R$  is the number of horizontal points in each row of the unit lattice,  $C$  is the number of vertical points in each column of the unit lattice, and  $RC$  is the total number of density points in the unit lattice.

An accurate approximation to equation (18) exists when  $n$  is not small. This relation is derived under the assumption that there is a continuous uniform distribution within a rectangular plane. The objective is to find the average distance between any two randomly selected points of a convex set. The approximation formula\* (Santalo, 1976, formula 4.18, page 49) is as follows:

$$\bar{\Delta}' = \frac{1}{15} \left\{ \frac{R^3}{C^2} + \frac{C^3}{R^2} + d \left( 3 - \frac{R^2}{C^2} - \frac{C^2}{R^2} \right) + \frac{5}{2} \left[ \frac{C^2}{R} \ln \left( \frac{R+d}{C} \right) + \frac{R^2}{C} \ln \left( \frac{C+d}{R} \right) \right] \right\}, \quad (19)$$

---

\* The author gratefully acknowledges an anonymous referee of *The American Mathematical Monthly* for suggesting equation (19) (in correspondence related to O'Brien, 1990c).



where  $d = \sqrt{R^2 + C^2}$  and  $\ln$  is the natural logarithm operator.

Calculations have shown equation (19) to be a good approximation to equation (18). For example, for  $n$  under 100, the maximum discrepancy is less than 10 percent. Equation (19) is an interesting example where a continuous distribution relation is applied to a discrete distribution to obtain an approximation to the latter. In the limiting case, as  $RC$  approaches infinity, the difference between equations (18) and (19) approaches zero.

In conclusion, for any finite, discrete, uniform distribution with distance between any two points  $\delta$ , the generalized average Euclidean distance in any PDI lattice among all possible pairs of  $RC$  points will be  $\bar{d} = \delta \bar{\Delta}$  or  $\delta \bar{\Delta}' \approx \bar{d}$ . If a unit lattice ( $\delta = 1$ ), then  $\bar{d} = \bar{\Delta}$  or  $\bar{\Delta}' \approx \bar{d}$ . Selected values of  $\bar{\Delta}$  calculated from equation (18) are given in appendix B for all  $RC$  configurations from  $R \times C = 2 \times 2$  to  $R \times C = 100 \times 100$  ( $n = 10,000$  density points).

## GENERALIZED DISTANCE FUNCTION IN A NONLATTICE

Here, density points can fall anywhere within the  $X$ - $Y$  geometric area, subject to restrictions specified earlier. The average Euclidean distance is calculated by equation (15) from known coordinate points as

$$\bar{d} = \frac{\sum_{i < j} \sqrt{(x_i - x_j)^2 + (y_i - y_j)^2}}{C(n,2)}, \quad (20)$$

where  $(x_i, y_i)$ ,  $(x_j, y_j)$  ( $i = 1, 2, \dots, n$ ;  $j = 1, 2, \dots, n$ ) denote the coordinate locations for the density points ( $n > 1$ ) within the rectangular study area  $X \times Y$  with arbitrary origin  $O$ . Equation (20) is the form used for calculating the population density measure of observed density points (i.e.,  $PDI_{act}$ , defined below in equation (29)).

An approximation to equation (20) is useful because exact  $(x_i, y_i)$ ,  $(x_j, y_j)$  coordinates cannot always be obtained. Recently, O'Brien (1991b) derived an approximation PDI method by assuming knowledge of the relative location of the density objects when  $(x_i, y_i)$ ,  $(x_j, y_j)$  data were unavailable.

If one assumes that the study area  $A = X \times Y$  has been partitioned into  $n = RC$  rectangles, each with subarea given by equation (3), then the following abbreviated calculation routines can be derived.

Define a cell density measure,

$$D_{jk} = n_{jk} / A_{jk}, \quad (21)$$

where  $n_{jk}$  is the number of objects observed to be within each of the subareas  $A_{jk} = A/n$  ( $j = 1, 2, \dots, R$ ;  $k = 1, 2, \dots, C$ ),  $0 \leq n_{jk} \leq A_{jk}$ ,  $0 \leq D_{jk} \leq 1$ . Then, define a cell indicator variable I:

$$I_{jk} = \begin{cases} 1 & \text{if } D_{jk} \neq 0, \\ 0 & \text{if } D_{jk} = 0. \end{cases} \quad (22)$$

Let

$$m = \sum_{k=1}^R \sum_{j=1}^C I_{jk}, \quad nD \leq m \leq n, \quad (23)$$

where  $D = n/A$  is obtained from equation (21) as an average cell density with weights spread over all cells; i.e.,  $D = \sum_{k=1}^R \sum_{j=1}^C D_{jk} n^{-1}$ . The measure  $m$  represents the total number of RC partitions occupied by at least one object. In practice,  $n_{jk}$  is taken as the smallest integer value. Likewise,  $m$  is taken to be the largest integer value.

Hence, equation (17) can be redefined to give the following approximation to equation (20):

$$\bar{d}' = \delta'_{\text{eff}} \bar{\Delta}, \quad (24)$$

where

$$\delta'_{\text{eff}} = \left( \frac{\sum_{k=1}^R \sum_{j=1}^C D_{jk}}{m} \right)^{-1/2} = \left( \frac{mA_{jk}}{n} \right)^{1/2}, \quad 1 \leq \delta'_{\text{eff}} \leq D^{-1/2}. \quad (25)$$

$\delta'_{\text{eff}}$  is obtained from equation (21) as an average cell density with weights spread over only the  $m$  occupied cells. The limits of equation (24) follow immediately by substituting the lower and upper limits of  $m$  given in equation (23); viz.,  $\bar{\Delta} \leq \bar{d}' \leq \bar{\Delta} \sqrt{A/n}$ . Noting that  $1 \leq \delta \leq \sqrt{A/n}$  (see appendix A) and assuming, in practice, that  $1 \leq \delta'_{\text{eff}} \leq \delta$ , it then follows that

$$\bar{d}_{\text{max}} \leq \bar{d}' \leq \bar{d}_{\text{min}}, \quad (26)$$

where  $\bar{d}_{\min}$  and  $\bar{d}_{\max}$  are, respectively, the lower and upper distance measures in the exact PDI model (O'Brien, 1990b). The relationship of (26) translates directly into a proof of the bounds of the approximate PDI measure ( $PDI'_{act} = \sqrt{D/\bar{d}} = [D\sqrt{n/m}] / \bar{\Delta}$ ; i.e.,  $PDI'_{act}$ ) is bounded by the  $PDI_{\min}$  and  $PDI_{\max}$  relations defined in O'Brien (1990b) and in equations (27) and (28) below.

## ALTERNATIVE DISTANCE MODELS

Thus far, the distance function has been derived for a rectangular configuration of points by assuming a rectangular exterior region. Mathematically, there is good reason for doing this because a square or rectangle can be drawn around any closed curve (Steinhaus, 1969).

Occasionally, the environment of interest may be modeled by curved configurations such as ellipses or circles, the latter being the easier to work with. Circular distributions have two advantages. First, for regions nearly square, a circle offers a more compact concentration of points, which may provide more realistic bounds on the density measure for highly cluttered environments. Second, any number  $n$  of points (including prime numbers) can be placed uniformly on a circle of radius  $r$  with linear point-to-point distance  $d = 2r \sin(180/n)$ . Based on this chord length measure, the author recently constructed a PDI model for discrete spatial density for circular distributions (O'Brien, 1992).

## SELECTED PROOFS

### PROOF THAT $PDI_{\min} \leq PDI_{\text{act}} \leq PDI_{\max}$

First, a statement of the relationships involved in this proof is given as follows:

$$\text{Lower bound: } PDI_{\min} = \frac{1}{\delta \bar{\Delta}} \sqrt{\frac{n}{A}}, \quad (27)$$

$$\text{Upper bound: } PDI_{\max} = \frac{1}{\bar{\Delta}} \sqrt{\frac{n}{A}}, \quad (28)$$

$$\text{Actual PDI: } PDI_{\text{act}} = \frac{1}{\bar{d}_{\text{act}}} \sqrt{\frac{n}{A}}. \quad (29)$$

The terms  $n$ ,  $A$ ,  $\bar{\Delta}$ , and  $\bar{d}_{\text{act}}$  (equivalent to equation (20)) are used here as defined in this report;  $\delta$  is defined in appendix A.

Now, to the proof. From the relationships of equations (27), (28), and (29), a formal statement of the relationship to be proven is as follows:

$$\frac{1}{\delta \bar{\Delta}} \sqrt{\frac{n}{A}} \leq \frac{1}{\bar{d}_{\text{act}}} \sqrt{\frac{n}{A}} \leq \frac{1}{\bar{\Delta}} \sqrt{\frac{n}{A}}. \quad (30)$$

To prove that equation (30) is a true statement, three assumptions are required:

$$\bar{d}_{\text{act}}, \delta, \text{ and } \bar{\Delta} \text{ are measured in linear units of feet,} \quad (31)$$

$$\delta \geq 1, \quad (32)$$

$$\bar{d}_{\text{act}} \leq \delta \bar{\Delta}. \quad (33)$$

The first assumption (31) is self-explanatory. The second assumption (32) is deemed reasonable because it amounts to saying that if persons are positioned uniformly the head-to-head distance ( $\delta$ ) is about 1 foot. Although (32) would not be a reasonable assumption for areal units of, say, square miles, (32) is reasonable when the areal units are square feet. (See O'Brien, 1991f, for the finite "macro" PDI model when areal units are square miles.)

The third assumption (33) states that, for a given geometric area to be studied in a density analysis, the actual clustering of the density points (i.e., people) in that area (with associated density  $\bar{d}_{\text{act}}$ ) will not be greater than the maximum theoretical dispersion provided by the

relation  $\delta\bar{\Delta}$  (equation (17)). The region outside  $\delta\bar{\Delta}$  is assumed to contain physical objects such as furniture, equipment, etc., making it unlikely that density points will be observed in that region. Empirical evidence from Monte Carlo simulations in O'Brien (1989) is cited in support of (33). In effect, (33) assumes that the persons are maximally dispersed in accord with the relation  $\delta\bar{\Delta}$ . Figure 6 describes the essential meaning of (33).

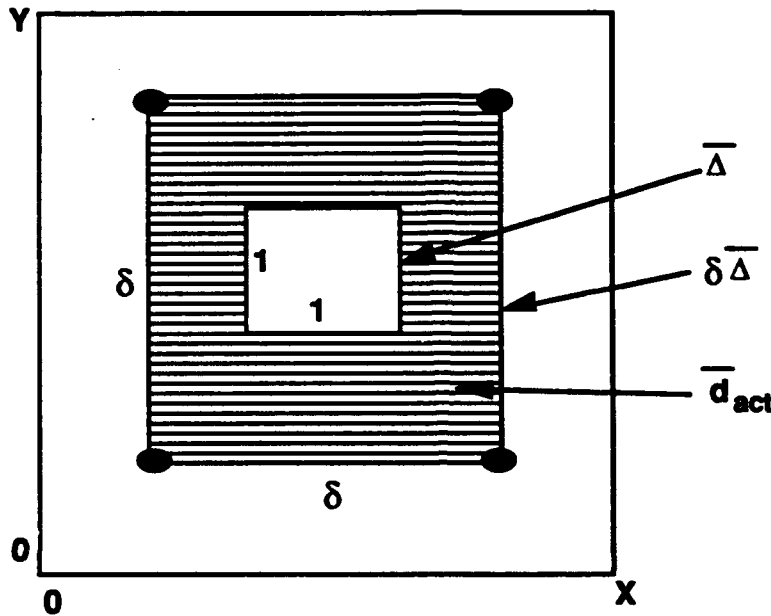


Figure 6. Intuitive Justification for Third Assumption

The formal proof of equation (30) can now be given in detail. The proof is presented in three parts. The first part states

$$\frac{1}{\delta\bar{\Delta}} \sqrt{\frac{\pi}{A}} \leq \frac{1}{\bar{d}_{act}} \sqrt{\frac{\pi}{A}}. \quad (34)$$

Simplifying and rearranging the terms of equation (34) gives the following relationship:

$$\bar{d}_{act} \leq \delta\bar{\Delta}, \quad (35)$$

which follows directly from (33).

The second part of the proof states that

$$\frac{1}{\bar{d}_{act}} \sqrt{\frac{\bar{n}}{A}} \leq \frac{1}{\bar{\Delta}} \sqrt{\frac{\bar{n}}{A}}. \quad (36)$$

Simplifying and rearranging the terms of equation (36) gives the following relationship:

$$\bar{\Delta} \leq \bar{d}_{act}. \quad (37)$$

From (33) the following relationship can be established:

$$\frac{\bar{d}_{act}}{\bar{\Delta}} \leq \delta, \quad (38)$$

from which it can be deduced that

$$\frac{\bar{\Delta}}{\bar{d}_{act}} \leq \frac{1}{\delta}. \quad (39)$$

Since, by (32), it follows that  $1/\delta \leq 1$ , then it can be deduced that  $\bar{\Delta}/\bar{d}_{act} \leq 1$ , from which it follows that  $\bar{\Delta} \leq \bar{d}_{act}$ .

The third part of the proof asserts that

$$\frac{1}{\delta \bar{\Delta}} \sqrt{\frac{\bar{n}}{A}} \leq \frac{1}{\bar{\Delta}} \sqrt{\frac{\bar{n}}{A}}. \quad (40)$$

The relationship between the lower and upper limits of equation (40) follows necessarily from the proofs given for equations (34) and (36) by the transitivity property of relations. It can be readily seen that equation (40) reduces algebraically to  $\delta \geq 1$ , which follows directly from (32). Thus, the statement of equation (30) has been shown to be true as derived from the stated definitions and assumptions.

The proof that the approximate PDI formula is bounded by the minimum and maximum bounds given in equations (27) and (28) follows from equation (26) and from the definition of the approximate PDI measure.

## PROOFS FOR $\delta_{\text{eff}}$

From O'Brien (1990b, equation(9)),  $\delta_{\text{eff}}$  is defined as

$$\delta_{\text{eff}} = \frac{\bar{d}_{\text{act}}}{\Delta}. \quad (41)$$

The objective is to show that  $\delta_{\text{eff}} \geq 1$ . Since  $\frac{\bar{d}_{\text{act}}}{\Delta} \geq 1$ , as proven from equation (36), equation (41) follows.

The proof that  $\delta/\delta_{\text{eff}} \geq 1$  is as follows:

By definition,  $\delta_{\text{eff}} = \frac{\bar{d}_{\text{act}}}{\Delta}$ ; then,  $\delta/\delta_{\text{eff}} = \frac{\delta\bar{\Delta}}{\bar{d}_{\text{act}}} \geq 1$ , which follows because it reduces to  $\delta\bar{\Delta} \geq \bar{d}_{\text{act}}$ , which was established previously in (33).

Because the quantity  $\delta_{\text{eff}}$  is a "pure number" (i.e., it has no dimensions because they cancel out as in the above definition), it provides a pure measure of relative change in population density.

The reader may also note that in the approximation model  $\delta'_{\text{eff}} \geq 1$  and  $\delta/\delta'_{\text{eff}} \geq 1$  follows from the derived limits given in equation (25) and the relationship given in equation (26).

## SUMMARY

This report has presented derivations of various distance functions that relate to the author's three-parameter square-root model for measuring discrete spatial density in finite populations. The model, called the Population Density Index (PDI) model, was developed to capture dynamic density relations among persons within a naturalistic environment. An "exact" model and an "approximate" model were presented.

The derivations related a generalized Euclidean distance function to the fundamental measures in the model ( $PDI_{act}$ , the approximation measure  $PDI'_{act}$ , their lower and upper bounds, and the density rate indices  $\delta_{eff}$  and  $\delta'_{eff}$ ). Coordinate systems were derived for plotting graphs of the PDI lattices and calculating the distance measures.

Also derived was the algorithm required to select a conformal lattice and the average uniform distance among the lattice points based on the number of density points to be analyzed within the reference quadrilateral area.

Average Euclidean distance values ( $\bar{\Delta}$ ) were presented for unit lattices up to a 100 x 100 matrix. Using these values, researchers will be able to compute lower and upper bounds of the PDI measures for up to 10,000 density objects.



## APPENDIX A SELECTING A UNIT LATTICE AND INTERPOINT DISTANCE PARAMETER

### DERIVATION OF THE ALGORITHM

In this appendix, the algorithm is presented for (1) determining a unique finite, discrete, conformal RC lattice and (2) computing the average interpoint distance among the RC points.

To begin, it is assumed that  $n$  (sample size) and  $A = X \times Y$  (the outer rectangular geometric area) are known. If  $n$  is a prime number (like 5 or 13 or 29), augment  $n$  by 1 before determining the rectangular/square dimensions of the unit lattice. The derivation of the algorithm for selecting an RC lattice is developed from concepts of number theory (Ore, 1967). In particular, interest is centered on sets and subsets of composite numbers that can be expressed as rectangular or square integers; i.e., positive (nonprime) integers that are two-integer products.

The value of  $n$  can be expressed in terms of the prime factors of the whole number:

$$n = \prod_{j=1}^r P_j^{\alpha_j}, \quad (\text{A-1})$$

where  $P_j$  represents the  $j$ th prime number and  $\alpha_j$  is the number of occurrences of the  $j$ th prime number of  $n$ . For example, composite 60 can be decomposed into  $P_1^{\alpha_1} P_2^{\alpha_2} P_3^{\alpha_3} = 2^2 \times 3 \times 5$ . Next, it is desired to derive the total number of possible RC ( $n = R \times C$ ) product configurations of  $n$  in order to create the set of RC configurations; the latter will be a subset of the former. This number can be derived as follows.

Let  $\tau(n)$  represent the number of all possible configurations of a composite integer  $n$ . Then it can be shown that this quantity is obtained from equation (A-1) by

$$\tau(n) = \prod_{j=1}^r (\alpha_j + 1). \quad (\text{A-2})$$

For example, 60 can be partitioned into  $(2+1)(1+1)^2 = 12$  two-integer products.

Next, the set of the  $\tau(n)$  configurations is examined to select only those nontrivial and/or nonredundant configurations. Let  $\Phi(\text{RC})$  represent the total number of nonredundant and nontrivial  $R \times C$  configurations for composite  $n$ ,  $\tau(n) \supset \Phi(\text{RC})$ . The trivial configurations are those for which  $n = n \times 1$  or  $1 \times n$ , and the redundant configurations are the multiplicative, commutative equivalents of  $R \times C$ ; i.e.,  $R \times C = C \times R$  ( $R \geq C$ ) (e.g.,  $10 \times 4 = 4 \times 10$ ). Then,

$$\Phi(RC) = \frac{\tau(n) - 2 + S}{2}, \quad (A-3)$$

where  $S = 0$  when  $n$  is a rectangular number, and  $S = 1$  when  $n$  is a square number.\* The set of all such specified configurations is denoted  $P$  of size  $\Phi(RC) = m$ ;  $P = \{R_1C_1, R_2C_2, \dots, R_iC_i, \dots, R_mC_m\}$ , ( $R_i \geq C_i$ ). For example, if  $n = 60$ , then  $\Phi(RC) = [(3 \times 2 \times 2) - 2 + 0]/2 = 5$ ;  $P = \{30 \times 2, 20 \times 3, 15 \times 4, 12 \times 5, 10 \times 6\}$ . Note that the trivial ( $60 \times 1, 1 \times 60$ ) and redundant commutative equivalent configurations ( $2 \times 30, 3 \times 20, 4 \times 15, 5 \times 12, 6 \times 10$ ) have been eliminated from  $P$ . Likewise, for  $n = 100$ ,  $\Phi(100) = \Phi(2^2 \times 5^2) = [(3 \times 3) - 2 + 1]/2 = 4$ ;  $P = \{50 \times 2, 25 \times 4, 20 \times 5, 10 \times 10\}$ .

Selection of a unique RC lattice with interpoint distance parameter  $\delta$  is accomplished by the following guidelines.

Select the  $R \times C$  lattice configuration (usually one) with dimensions most commensurate with the exterior  $X \times Y$  dimensions; i.e., the one for which  $X/Y - R/C$  is a minimum absolute difference ( $X \geq Y, R \geq C$ ). Determine the uniform interpoint spacing parameter  $\delta = \sqrt{A/n} = \sqrt{XY/RC}$  as defined in O'Brien (1990b, equation (3)). Next, test for conformity of the dimensions of the selected lattice to the study area dimensions by the quantities  $(R - 1)\delta$  and  $(C - 1)\delta$ . If either of the  $R, C$  dimensions is nonconformal (i.e.,  $(R - 1)\delta \geq X$  or  $(C - 1)\delta \geq Y$ ), then conform the lattice dimensions by adjusting  $\delta$  by the relation  $\delta = \min[X/(R - 1), Y/(C - 1)] - 0.1$ . Finally, in the rarest of instances, when commensurability is achieved simultaneously by more than one lattice configuration, the researcher should approximate  $\delta$  as above for each configuration, and then the  $R \times C$  configuration will be that associated with the maximum  $\delta$  value. If plural maxima  $\delta$  occur, select the  $R \times C$  configuration associated with the smallest value of  $\bar{\Delta}$ , given in appendix B.

The symbolic specification of the above guidelines can be stated as follows. Because the desired discrete  $R \times C$  lattice must be unique, the selection mechanism requires a complex

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\* Equation (A-3) is not proven nor could a proof be found in the mathematical literature. Its correctness seems intuitively obvious. For example, for a number to be square, it is necessary and sufficient that all exponents in the prime factorization (equation (A-1)) be even (Ore, p. 42), which implies that  $\tau(n)$  is odd, as is  $\tau(n) - 2$ , but adding 1 ( $S$ ) makes  $\Phi(RC)$  even. Finally, dividing by 2 eliminates the rectangular duplicates in  $\tau(n) + S - 2$ . The same logic applies to rectangular numbers, thus completing the proof outline.

two-step procedure. First, the following commensurability relation is determined from the dimensions of A and each element of the set P:

$$R_k C_k = \min_{1 \leq i \leq m} \left| \frac{\max(X, Y)}{\min(X, Y)} - \frac{\max(R_i, C_i)}{\min(R_i, C_i)} \right| \quad (1 \leq k \leq m). \quad (\text{A-4})$$

Then, based on equation (A-4) above and equation (4) in the main body of the text,  $\delta$  is determined from one of the following four mutually exclusive and exhaustive conditions:

$$\delta = \begin{cases} \sqrt{\frac{\bar{\Delta}}{n}} & \text{if } k = 1 \text{ and } p > 0 \text{ and } q > 0 \quad (\text{A-5}) \\ \min \left[ \left( \frac{X}{R-1}, \frac{Y}{C-1} \right) - 0.1 \right] & \text{if } k = 1 \text{ and } p \leq 0 \text{ or } q \leq 0 \quad (\text{A-6}) \\ \max_{1 \leq l \leq k} \left\{ \min_{2 \leq k \leq m} \left[ \left( \frac{X}{R_k-1}, \frac{Y}{C_k-1} \right) - 0.1 \right] \right\} & \text{if } k > 1 \text{ and } l = 1 \quad (\text{A-7}) \\ \min_{2 \leq l \leq k} [\bar{\Delta} (R_l C_l)] & \text{if } k > 1 \text{ and } l > 1 \quad (\text{A-8}) \end{cases}$$

where  $p, q$  are defined in equation (4). In (A-5) through (A-8),  $\delta \geq 1$  by definition. Also, it may be proven that  $\delta \leq \sqrt{A/n}$  based on equation (4) where it can be deduced that  $(R-1)\delta < X$ ,  $(C-1)\delta < Y$ , and for commensurate lattices ( $\delta \leq \sqrt{A/n}$ ),  $\delta = X/R = Y/C$ . This relationship places an upper bound on  $\delta$  that is important in the proofs and derivations of the text.

Figure A-1 summarizes the algorithm for the RC lattice selection and computation of  $\delta$ . In summary, if  $k = 1$ ,  $R_k C_k$  is the lattice selected from equation (A-4) and  $\delta$  is selected from equation (A-5) or equation (A-6). If  $k > 1$ ,  $\delta$  is selected from equation (A-7) and  $R \times C$  is selected as the lattice associated with the maximum  $\delta$  in equation (A-7). Finally, if (A-7) provides a plurality of  $\delta$  values, then (A-8) is used, which selects the  $R_l C_l$  ( $2 \leq l \leq k$ ) lattice associated with the smallest  $\bar{\Delta}$  value. Appendix B contains the required  $\bar{\Delta}$  values computed to five decimal places. Note that for a unit lattice, or commensurate nonunit lattice,  $k = 1$  and equation (A-5) computes the correct  $\delta$ . Hansen et al. (1953, Vol. I) provides an interesting discussion of commensurate nonunit lattices related to a square-root law for distances in the field of discrete finite-population sampling theory when equation (A-5) applies.

Thus, equations (A-4) through (A-8) provide a unique, conforming lattice with associated interpoint distance parameter  $\delta$ . A table of prime numbers and factorizations of composite numbers is an indispensable tool for implementing equation (A-4). See Lehmer (1941, 1961) for extensive tables and Abramowitz and Stegun (1964) for abbreviated tables.

These calculations assure that the lengths of the R and C line segments of the nonunit lattice,  $(R - 1)\delta$  and  $(C - 1)\delta$ , containing human density points do not exceed the dimensions of the study area. The utility of adjusting  $\delta$  (when so required) as recommended resides in plotting minimum/maximum dispersions of the RC density points in the study area as given in equations (6) and (10).

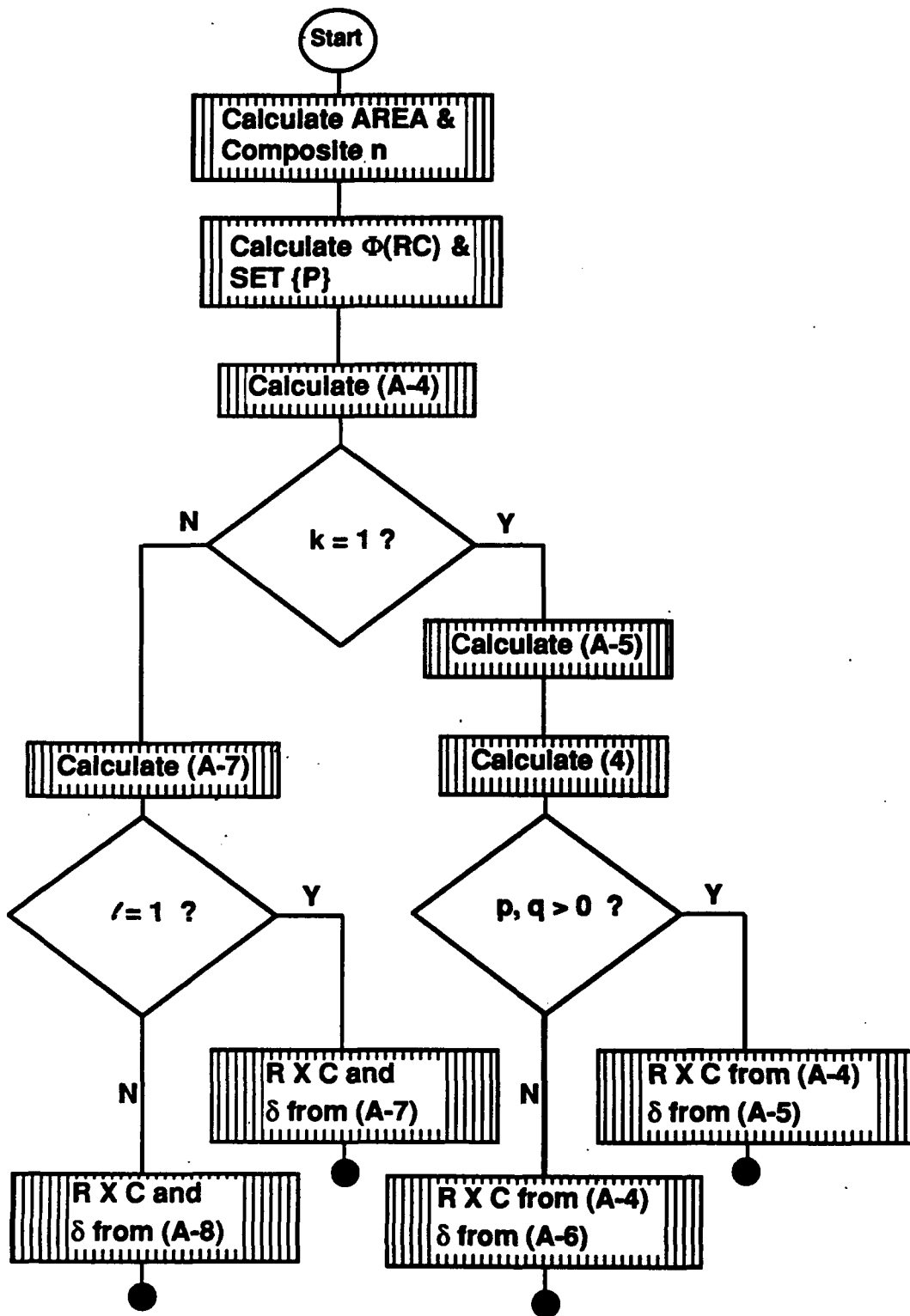


Figure A-1. Flowchart for Determining R X C Unit Lattice and Interpoint Distance Parameter  $\delta$

## NUMERICAL EXAMPLES

Three artificial examples are selected to demonstrate the procedures. A complete setup is provided. The flowchart in figure A-1 is useful in tracing the decision logic.

In the first example, the data are as follows:  $n = 12$ ,  $A = 25 \times 25 \text{ ft}^2$ . It is obvious that  $n = 12$  provides two nontrivial, nonredundant choices ( $\Phi(12) = 2$ ); viz.,  $R_1C_1 = 6 \times 2$  or  $R_2C_2 = 4 \times 3$ . Because  $X/Y = 1$ ,  $R_2C_2 = 4 \times 3$  comes closest to satisfying equation (A-4). Because  $k = 1$ , first compute  $\delta = 7.22$  (from equation (A-5)); R,C is found to be conformal (each row/column "fits" inside the outside  $25 \text{ ft}^2$  area in accord with equation (4)). Thus,  $R = 4$ ,  $C = 3$ , and  $\delta = 7.22$ .

In the second example,  $n = 64$  and  $A = 50 \times 5 \text{ ft}^2$ . This example is one of those rare possibilities. For  $n = 64$ ,  $\tau(64) = 7$ ;  $\Phi(RC) = [7 + 1 - 2]/2 = 3$ , and  $P = \{32 \times 2, 16 \times 4, 8 \times 8\}$ . Applying equation (A-4) shows that  $32 \times 2$  and  $16 \times 4$  are equally commensurate ( $k > 1$ ); i.e.,  $|10 - 16| = |10 - 4|$ . Thus, because  $k = 2$  and  $l$  is undetermined, apply equation (A-7), giving  $\delta = \max(1.57, 1.51) = 1.57 (l = 1)$ . The configuration associated with the largest  $\delta$  value is  $16 \times 4$ . Thus,  $R = 16$ ,  $C = 4$ , and  $\delta = 1.57$  for this data distribution.

As an example requiring equation (A-8) for determining  $R \times C$  and  $\delta$ , consider the data:  $A = 80 \times 16 \text{ ft}^2$ ,  $n = 32$ ,  $P = \{16 \times 2, 8 \times 4\}$ . Here, applying (A-4) to the above data distributions produces  $|5 - 8| = |5 - 2|$  (i.e.,  $k = 2$ ), and (A-7) produces  $\delta = \max\{(5.23, 5.23)\} (l > 1)$ , which is clearly ambiguous. But  $\min[\bar{\Delta}(16 \times 2), \bar{\Delta}(8 \times 4)] = \min(5.59, 3.27) = \bar{\Delta}(8 \times 4)$ . Thus,  $R \times C = 8 \times 4$ , and  $\delta = 5.23$ .

In general, the reader will note that (A-7) or (A-8) will be required for determining  $\delta$  whenever the study area ratio  $X/Y$  is equal to the average of the ratios of two equally commensurate lattices. The above examples bear out this relationship.







7	47	14.17982	0	20	7.47843
7	48	14.26684	0	21	7.28636
7	49	14.33394	0	22	6.23861
7	50	17.14126	0	23	6.88644
7	51	17.48877	0	24	6.21873
7	52	17.81643	0	25	9.23184
7	53	18.14426	0	26	9.84634
7	54	18.47226	0	27	9.86149
7	55	18.80036	0	28	10.17763
7	56	19.12846	0	29	10.48439
7	57	19.45677	0	30	10.53231
7	58	19.78522	0	31	11.13974
7	59	20.11429	0	32	11.44982
7	60	20.44380	0	33	11.76982
7	61	20.77289	0	34	12.08979
7	62	21.10246	0	35	12.41009
7	63	21.43215	0	36	12.73189
7	64	21.76234	0	37	13.05366
7	65	22.09271	0	38	13.37587
7	66	22.42315	0	39	13.69849
7	67	22.75385	0	40	14.02156
7	68	23.08476	0	41	14.34488
7	69	23.41586	0	42	14.66861
7	70	23.74722	0	43	14.99267
7	71	24.07887	0	44	15.31704
7	72	24.41086	0	45	15.64171
7	73	24.74329	0	46	15.96668
7	74	25.07617	0	47	16.29186
7	75	25.40952	0	48	16.61723
7	76	25.74338	0	49	16.94289
7	77	26.07778	0	50	17.26886
7	78	26.41274	0	51	17.59511
7	79	26.74828	0	52	17.92167
7	80	27.08443	0	53	18.24843
7	81	27.42121	0	54	18.57549
7	82	27.75867	0	55	18.90286
7	83	28.09685	0	56	19.23052
7	84	28.43576	0	57	19.55849
7	85	28.77544	0	58	19.88672
7	86	29.11592	0	59	20.21531
7	87	29.45723	0	60	20.54423
7	88	29.79939	0	61	20.87349
7	89	30.14244	0	62	21.20311
7	90	30.48640	0	63	21.53309
7	91	30.83129	0	64	21.86344
7	92	31.17714	0	65	22.19416
7	93	31.52400	0	66	22.52526
7	94	31.87189	0	67	22.85674
7	95	32.22085	0	68	23.18862
7	96	32.57092	0	69	23.52090
7	97	32.92214	0	70	23.85358
7	98	33.27454	0	71	24.18666
7	99	33.62816	0	72	24.52014
7	100	33.98294	0	73	24.85402
0	0	4.28824	0	74	25.18830
0	0	4.48341	0	75	25.52297
0	10	4.72626	0	76	25.85803
0	11	4.91341	0	77	26.19349
0	12	5.22689	0	78	26.52934
0	13	5.52821	0	79	26.86559
0	14	5.87245	0	80	27.20224
0	15	6.16429	0	81	27.53929
0	16	6.49833	0	82	27.87664
0	17	6.78384	0	83	28.21439
0	18	7.06796	0	84	28.55254
0	19	7.37219	0	85	28.89109
0	06	29.86787	0	86	29.23004
0	07	29.42729	0	87	29.57066
0	08	29.78784	0	88	21.29789
0	09	30.06788	0	89	21.62469
0	10	30.41822	0	90	21.95183
0	11	30.74683	0	91	22.27931
0	12	31.07912	0	92	22.60644
0	13	31.40944	0	93	22.93449
0	14	31.74821	0	94	23.26229
0	15	32.07679	0	95	23.59016
0	16	32.40549	0	96	23.91821
0	17	32.73219	0	97	24.24636
0	18	33.06294	0	98	24.57469
0	19	33.39372	0	99	24.90329
0	100	33.72454	0	100	25.23214
0	0	4.72842	0	00	25.56099
0	0	4.94331	0	01	25.88983
0	11	5.25336	0	02	26.21871
0	12	5.52982	0	03	26.54762
0	13	5.80982	0	04	26.87655
0	14	6.09459	0	05	27.20551
0	15	6.38314	0	06	27.53451
0	16	6.67586	0	07	27.86356
0	17	6.97196	0	08	28.19266
0	18	7.27142	0	09	28.52181
0	19	7.57422	0	10	28.85101
0	20	7.88032	0	11	29.18026
0	21	8.17922	0	12	29.50956
0	22	8.47842	0	13	29.83891
0	23	8.78036	0	14	30.16831
0	24	9.08490	0	15	30.49776
0	25	9.40241	0	16	30.82726
0	26	9.71482	0	17	31.15681
0	27	10.02932	0	18	31.48641
0	28	10.34686	0	19	31.81606
0	29	10.66413	0	20	32.14576
0	30	10.98304	0	21	32.47551
0	31	11.29484	0	22	32.80531
0	32	11.60124	0	23	33.13516
0	33	11.91124	0	24	33.46506
0	34	12.22447	0	25	33.79501
0	35	12.54097	10	10	3.23926
0	36	12.87486	10	11	3.56829
0	37	13.19896	10	12	3.77229
0	38	13.51322	10	13	6.04866
0	39	13.82445	10	14	6.22469
0	40	14.13282	10	15	6.99777
0	41	14.47783	10	16	6.88443
0	42	14.79694	10	17	7.18429
0	43	15.12122	10	18	7.47786
0	44	15.44389	10	19	7.77227
0	45	15.76499	10	20	8.06985
0	46	16.09229	10	21	8.26933
0	47	16.41586	10	22	8.67111
0	48	16.73782	10	23	8.87443
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0	50	17.36824	10	25	9.58879
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0	52	18.03329	10	27	10.20329
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13	32	12.29028	13	96	23.29000
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13	34	12.29028	13	100	24.14175
13	35	13.23021	14	14	7.21010
13	36	13.23004	14	15	7.20000
13	37	13.23070	14	16	7.07754
13	38	14.13011	14	17	6.13000
13	39	14.04135	14	18	6.20015
13	40	14.77725	14	19	6.77100
13	41	15.00000	14	20	6.00000
13	42	15.00000	14	21	6.20077
13	43	15.71904	14	22	6.20000
13	44	16.00000	14	23	6.01002
13	45	16.20115	14	24	10.10136
13	46	16.00700	14	25	10.20000
13	47	16.00454	14	26	10.00000
13	48	17.20100	14	27	10.00000
13	49	17.01000	14	28	11.20000
13	50	17.20011	14	29	11.00000
13	51	18.20000	14	30	11.00000
13	52	18.07000	14	31	12.10001
13	53	18.00000	14	32	12.00000
13	54	19.21004	14	33	15.70072
13	55	19.20040	14	34	13.00000
13	56	19.00000	14	35	13.00070
13	57	20.17070	14	36	13.71000
13	58	20.00704	14	37	14.00000
13	59	20.01000	14	38	14.20000
13	60	21.14111	14	39	14.00004
13	61	21.00011	14	40	14.00004
13	62	21.70000	14	41	15.20010
13	63	22.10700	14	42	15.07100
13	64	22.00000	14	43	15.00725
13	65	22.70000	14	44	16.20074
13	66	23.07000	14	45	16.31000
13	67	23.00000	14	46	16.00000
13	68	23.70000	14	47	17.10000
13	69	24.00707	14	48	17.00000
13	70	24.27100	14	49	17.77000
13	71	24.00010	14	50	18.00000
13	72	25.00000	14	51	18.01007
13	73	25.20000	14	52	18.70000
13	74	25.07000	14	53	19.00000
13	75	25.00001	14	54	19.20000
13	76	26.20014	14	55	19.00000
13	77	26.00000	14	56	20.00010
13	78	26.07000	14	57	20.20000
13	79	27.00000	14	58	20.00000
13	80	27.00010	14	59	20.00000
13	81	27.00000	14	60	21.00000
13	82	28.27007	14	61	21.00000
13	83	28.00000	14	62	21.00000
13	84	28.00000	14	63	22.20000
13	85	29.20000	14	64	22.00000
13	86	29.07000	14	65	22.00000
13	87	29.00000	14	66	23.21000
13	88	30.20070	14	67	23.00000
13	89	30.00000	14	68	23.00000
13	90	30.00000	14	69	24.17010
13	91	31.21070	14	70	24.00010
13	92	31.00000	14	71	24.00000
13	93	31.00000	14	72	25.10770
13	94	32.10000	14	73	25.07000
13	95	32.20000	14	74	25.70015
13	96	32.00000	14	75	26.11015
13	97	33.17000	14	76	26.00000
14	77	26.70707	15	57	20.07010
14	78	27.00000	15	58	20.70000
14	79	27.01000	15	59	21.00000
14	80	27.74170	15	60	21.00000
14	81	28.00000	15	61	21.70700
14	82	28.20000	15	62	22.00700
14	83	28.70000	15	63	22.00700
14	84	29.00000	15	64	22.70000
14	85	29.20010	15	65	23.00000
14	86	29.00000	15	66	23.00000
14	87	30.01070	15	67	23.07077
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14	89	30.07000	15	69	24.21000
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14	91	31.00000	15	71	24.00700
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14	94	32.00000	15	74	25.00071
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14	96	32.00700	15	76	26.07000
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14	98	33.01070	15	78	27.00000
14	99	33.00000	15	79	27.50000
14	100	34.20010	15	80	27.00000
15	15	7.00000	15	81	28.10000
15	16	8.10070	15	82	28.21000
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15	18	8.00771	15	84	29.10000
15	19	8.01100	15	85	29.00000
15	20	9.10000	15	86	29.01000
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15	22	9.70000	15	88	30.00000
15	23	10.00000	15	89	30.70011
15	24	10.20000	15	90	31.11000
15	25	10.01070	15	91	31.00011
15	26	10.00010	15	92	31.70000
15	27	11.10000	15	93	32.00000
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15	29	11.70000	15	95	32.70000
15	30	12.00000	15	96	33.00070
15	31	12.20000	15	97	33.00000
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15	42	15.70000	16	23	10.00000
15	43	16.00000	16	24	10.00000
15	44	16.27000	16	25	10.00700
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15	54	19.01010	16	35	13.70000
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16	41	15.42200	17	23	10.50226
16	42	15.53099	17	24	10.70344
16	43	16.23998	17	25	11.04034
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16	45	16.68994	17	27	11.63646
16	46	17.17100	17	28	11.82734
16	47	17.48208	17	29	12.21044
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16	49	18.18771	17	31	12.84331
16	50	18.42147	17	32	13.09946
16	51	18.79497	17	33	13.30439
16	52	19.04834	17	34	13.68439
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16	54	19.67969	17	36	14.29402
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16	56	20.31159	17	38	14.89904
16	57	20.62822	17	39	15.28188
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16	61	21.89885	17	43	16.42440
16	62	22.21782	17	44	16.73234
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16	64	22.84113	17	46	17.34921
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16	66	23.49480	17	48	17.97826
16	67	23.81489	17	49	18.28137
16	68	24.13497	17	50	18.58997
16	69	24.45482	17	51	18.90832
16	70	24.77374	17	52	19.21612
16	71	25.09080	17	53	19.53143
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16	74	26.06342	17	56	20.47428
16	75	26.38341	17	57	20.78947
16	76	26.70802	17	58	21.10889
16	77	27.02804	17	59	21.42111
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16	80	27.98647	17	62	22.37139
16	81	28.21946	17	63	22.68902
16	82	28.64303	17	64	22.98809
16	83	28.96804	17	65	23.32800
16	84	29.29830	17	66	23.64346
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16	87	30.28242	17	69	24.60899
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16	89	30.91127	17	71	25.26960
16	90	31.23892	17	72	25.56863
16	91	31.56679	17	73	25.88121
16	92	31.89843	17	74	26.20880
16	93	32.23199	17	75	26.53289
16	94	32.58807	17	76	26.84419
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16	96	33.18643	17	78	27.48728
16	97	33.51219	17	79	27.80811
16	98	33.83737	17	80	28.12114
16	99	34.16307	17	81	28.48342
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17	17	9.47922	17	83	29.09432
17	18	9.14147	17	84	29.42136
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17	89	31.03966	18	72	25.70834
17	90	31.36122	18	73	26.02874
17	91	31.68004	18	74	26.34721
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17	93	32.33432	18	76	26.98740
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18	20	9.52779	18	86	30.20134
18	21	10.19683	18	87	30.52822
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18	23	10.74334	18	89	31.18833
18	24	11.02066	18	90	31.48234
18	25	11.30036	18	91	31.81831
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18	28	12.18244	18	94	32.78890
18	29	12.46830	18	95	33.10977
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97	99	51.10180			
97	100	51.36458			
98	98	51.10050			
98	99	51.36153			
98	100	51.62323			

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Chief of Naval Research (OCNR-1271—J. Smith, OCNR-23—A. Faulstich, OCNR-232—D. Houser)	3
Naval Sea Systems Command (SEA-06U)	1
Commander, Submarine Force Atlantic Fleet	1
Commander, Submarine Force Pacific Fleet	1
Commander, Submarine Development Squadron 12	1
Defense Advanced Research Projects Agency	1
Navy Personnel Research and Development Center (Code 412—J. Grossman)	1
Defense Technical Information Center	2
Center for Naval Analyses	1