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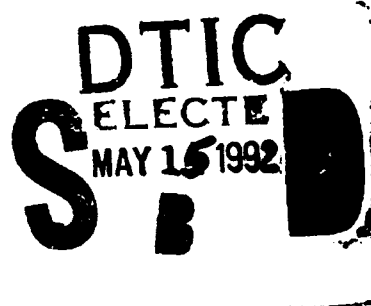
# THE GEBODIII PROGRAM USER'S GUIDE AND DESCRIPTION

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FOR THE COMMANDER



PETER A. LURKER, Lt Col, USAF BSC  
Acting Director  
Biodynamics and Biocommunications Division

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## PREFACE

This manual is written in two parts. Part 1 is the user's guide which describes how to install, run, and use GEBODIII. Part 2 is the program description which explains the program modifications and computations. This manual should be used in conjunction with the report Development of an Interactive Computer Program to Produce Body Description Data, L. Douglas Baughman, July 1983, AFAMRL-TR-83-058.



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PART 1  
USER'S GUIDE

1.1 INTRODUCTION

Program GEBODIII is the latest version of GEBOD (Generator of Body Data). GEBOD is a program which is used to automate the process for generating the body description portion of the Articulated Total Body (ATB) model (Obergefell, et al., 1988) input data set. GEBOD was originally developed and documented by Baughman (1983). GEBODII was released in 1988, but was not documented. This manual documents the changes made for GEBODII as well as those made for GEBODIII. GEBODIII is similar in operation to GEBOD, although the output may be quite different. The changes apparent to the user while running the program are the prompting for output filenames and the addition of the option to output data for either 15 or 17 body segments. Otherwise, the program appears unaltered. Major changes to the program include the addition of dummy data sets and the use of human stereophotometric data to calculate segment inertial properties and joint locations for adult human data sets. Refer to the introduction to Part 2, Program Description, for a brief summary of all modifications.

GEBODIII provides body data for several human subject types. They are: child (2-19 years), adult human female, adult human male, and a human based on user-supplied body dimensions. Also available are the following manikin data sets: Hybrid III dummy with seated pelvis (50th percentile), Hybrid III dummy with standing pelvis (50th percentile), and Hybrid II dummy (50th percentile). For all of the above subject types, GEBODIII provides segment data for mass, center of gravity location, contact surface dimensions, principal moments of inertia and their associated directions. Further, for the adult human female, the adult human male, and the manikin data sets, the program outputs elastic, viscous, and joint stop properties for



each joint. All calculations are done in English units, but output is also available in metric units.

GEBODIII accesses up to seven files or input/output (I/O) devices. Prompts for the user are written to the console, I/O unit 6. Interactive user input is received through the console, I/O unit 5. Body description data produced by GEBODIII is written to both I/O units 3 and 9. Data written to unit I/O 3 is formatted for the ATB model input data set, and the data written to I/O unit 9 is a tabular presentation of the data. If the user selects the User-Defined Body Dimensions option, the body description data is input using an external data file through I/O unit 1. GEBOD.DAT is an external file containing data that is needed by GEBODIII, such as the subject type option titles and selected ATB input data sets available to the user. The GEBOD.DAT file is distributed with the GEBODIII program and is always assigned to I/O unit 2. GEBOD.DAT should not be changed by the user.

The user is prompted for the filenames to be assigned to I/O units 1, 3, and 9. The first time through the program, the filenames assigned to I/O units 3 and 9 must be new names. An error will occur if a file with the chosen filename already exists in the computer directory. However, on subsequent runs through the program (when the user responds "y" to the prompt asking if it is desired to produce another body description data set), the user may enter the same filenames for I/O units 3 and 9. When this is done, the output is appended to the end of the existing file rather than overwriting the file.

To install GEBODIII, the source code and GEBOD.DAT files must be copied onto the user's computer. The source code must then be compiled using the Fortran compiler available to the user. To run the program, type "GEBODIII". The user is then prompted for output file names and other required program inputs.

## 1.2 PROGRAM FLOW

The interactive program flow is depicted in Figure 1. After the program is started, GEBOD prompts the user for a description of the subject that is less than 60 characters long. This description can be left blank by hitting <ENTER>. The user is then prompted to provide a filename for the tabular body description output.

Next, the user is asked to choose the desired subject type from the option menu. The possible choices are:

1. Child (2-19 years)
2. Adult Human Female (based on female stereophotometric and Air Force personnel data)
3. Adult Human Male (based on male stereophotometric and Air Force flying personnel data)
4. User-Supplied Body Dimensions
5. Sitting Hybrid III Dummy (50%)
6. Standing Hybrid III Dummy (50%)
7. Hybrid II Dummy (50%)

If option 1, Child (2-19 years), is chosen, the user is asked to select the parameters which will be used to generate the subject data set. The user can select age, weight, standing height, or all of the above. If age is selected, the user is asked to specify months or years as the units in which age will be given. Then the user is asked to provide the age. A range for the possible values of age is displayed on the screen to assist the user in providing an appropriate age. Similar procedures are followed for weight and standing height, if they were selected by the user. For weight, the possible units of input are pounds or newtons. For standing height, possible units of input are inches or meters.

Options 2 and 3, Adult Human Female and Adult Human Male,

Figure 1. Interactive Flow Chart

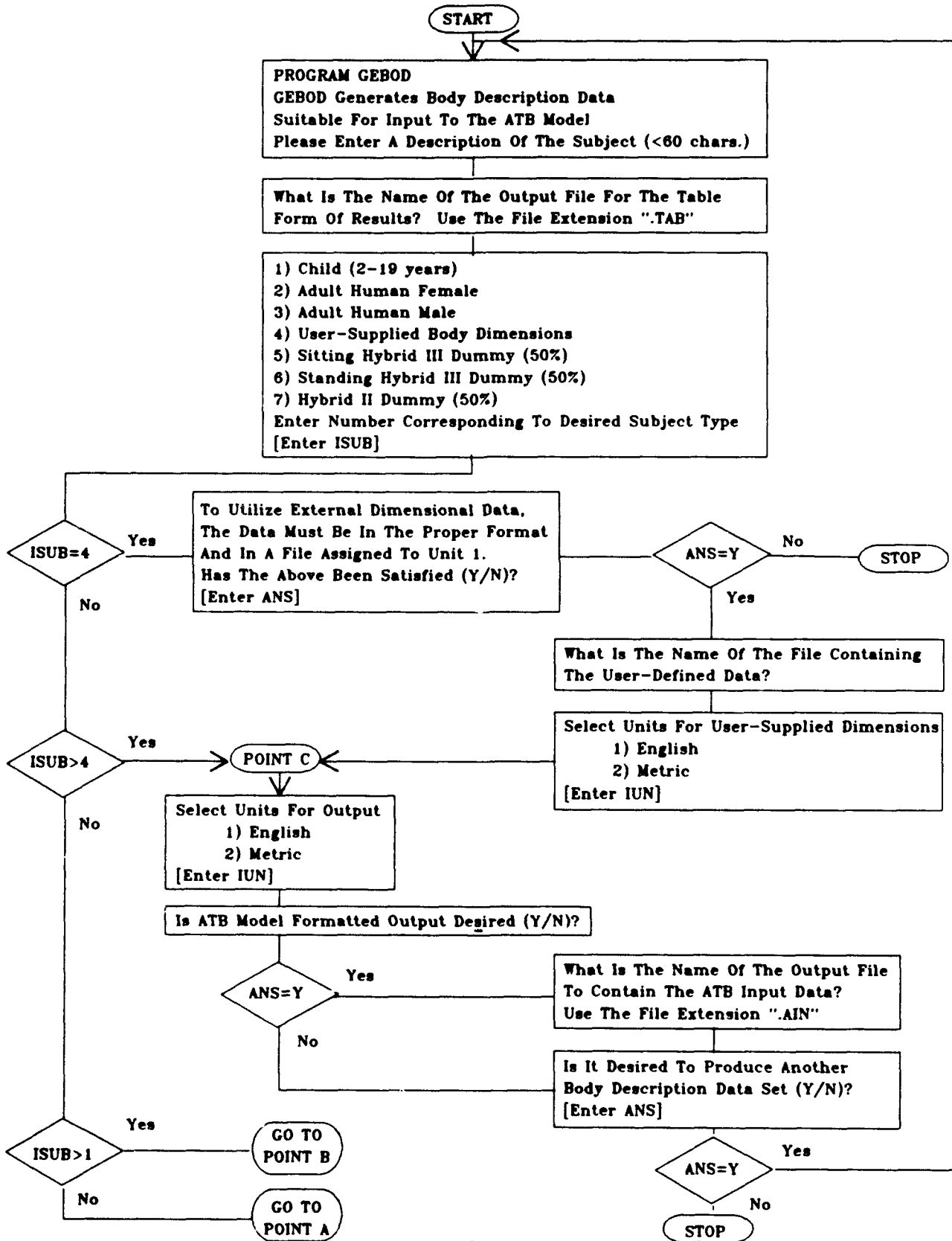


Figure 1. Interactive Flow Chart

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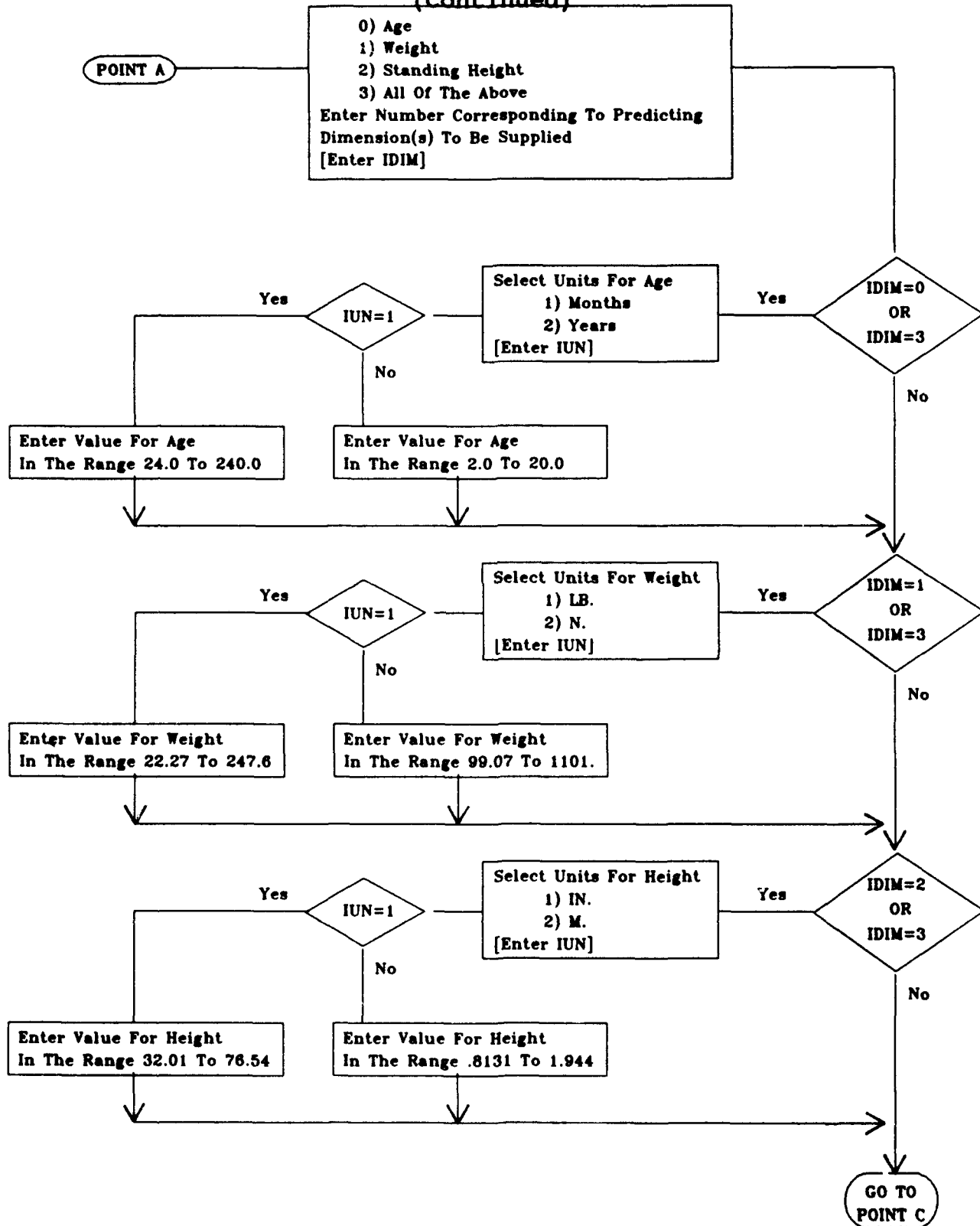


Figure 1. Interactive Flow Chart  
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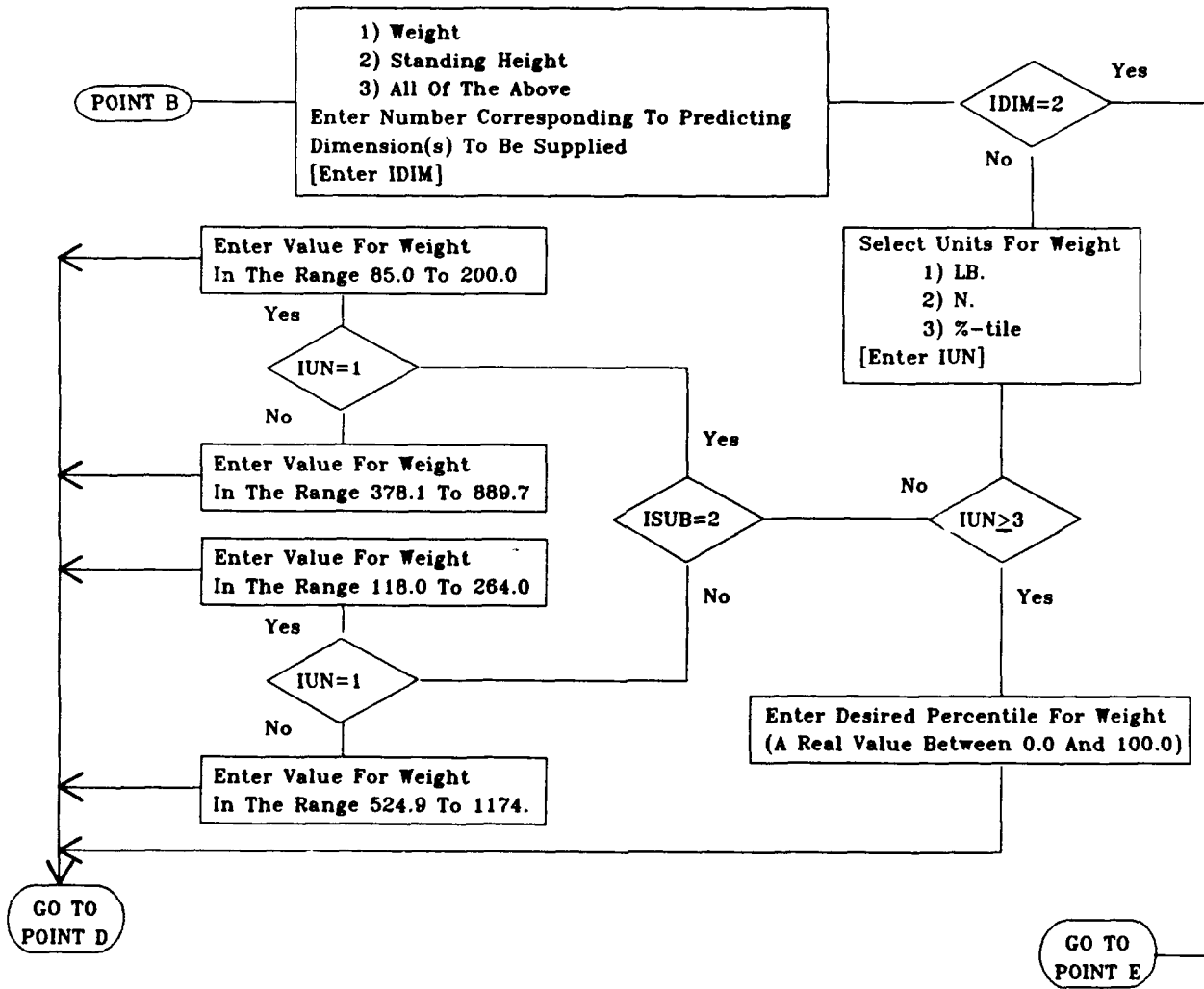
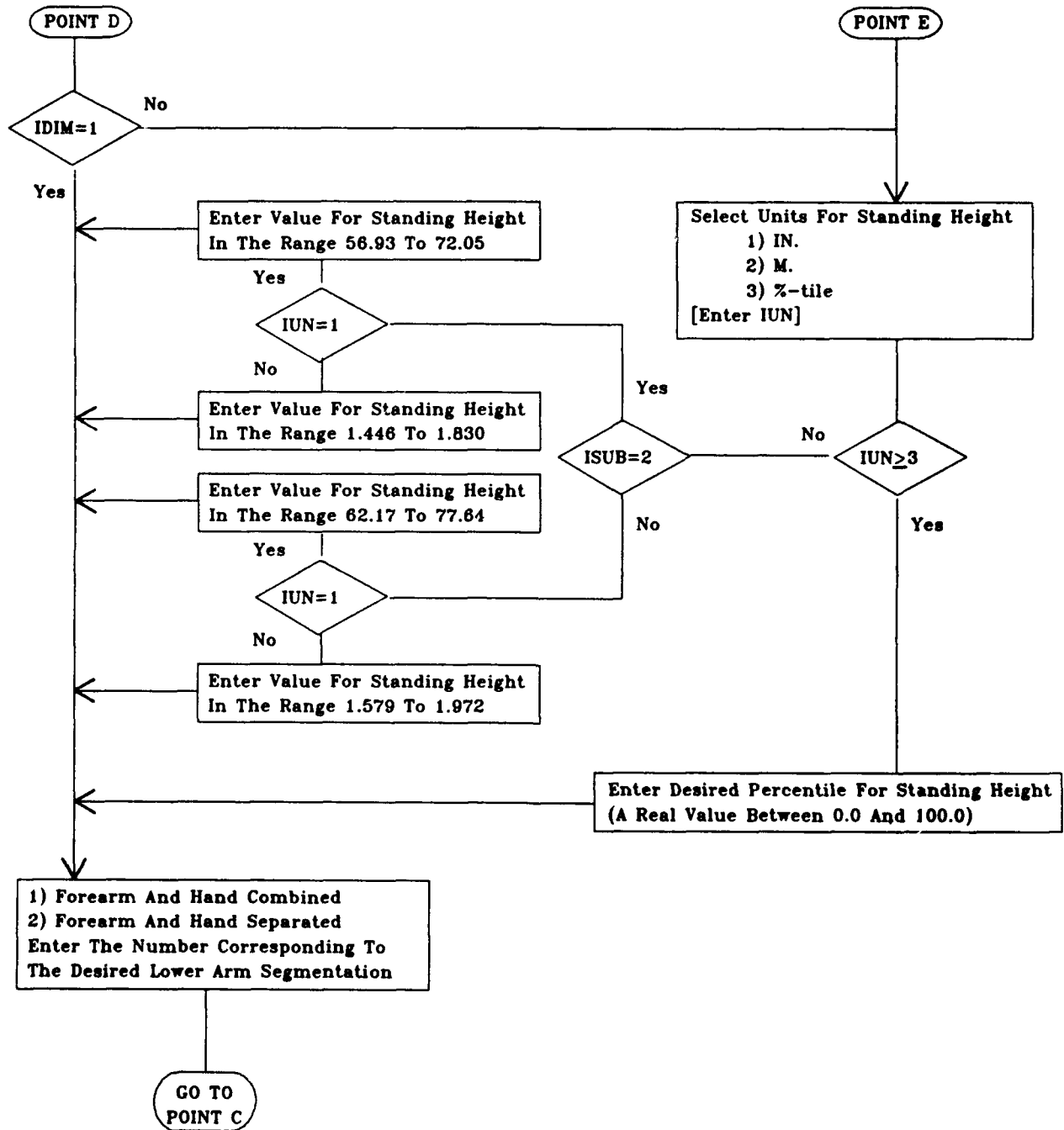


Figure 1. Interactive Flow Chart  
(Continued)



respectively, use the same procedure as option 1, except that the option to input age is omitted. After the specified data have been entered for these options, the program asks the user to select the desired lower arm segmentation scheme: forearm and hand combined resulting in output for 15 segments and 14 joints, or forearm and hand separated resulting in output for 17 segments and 16 joints.

If option 4, User-Supplied Body Dimensions, is selected, the user is asked to select the units in which the user-supplied body dimensions are to be provided. The choices are English (inches and pounds) or metric (meters and newtons). (See Appendix A of Baughman (1983) for more details on the use of option 4.)

The manikin options 5 through 7 refer to specific data sets stored in GEBOD.DAT; they do not require any user-supplied description of the subject.

When all user input for the description of the subject has been completed, the user is asked to select the units for output, either English (inches and pounds) or metric (meters and newtons). Next, the user is asked if ATB model formatted output is desired. If the user does not intend to use the output from this program as input to the ATB model, the user should specify "n" and the program output will consist solely of a tabular presentation of the data. If "y" is specified, the user is asked to supply the name of the file to contain this data and the program output will provide both a tabular presentation of the data and an ATB model formatted presentation of the data.

After the calculations and output are completed, the user is asked if another body description data set is to be generated. If not, execution stops. If another data set is desired, the program loops back to the beginning of the program and the input process is repeated.

### 1.3 REGRESSION EQUATIONS AND THEIR USE

Regression analysis is a method widely used in anthropometry for predicting various body measurements from known body measurements. All regression equations for the Adult Human Female and the Adult Human Male options used by GEBODIII are based on weight, standing height, or both. The goal was to use this limited description to achieve the best possible prediction of other body measurements for a subject. The coefficient of determination or R-square ( $R^2$ ) value is an indicator of the predictive ability of a regression equation. The  $R^2$  value associated with each regression equation is given in the appendices containing these regression equations. For example, the following regression equations to predict shoulder height can be found in Appendix D of Baughman (1983).

$$\begin{aligned} \text{Shoulder Height} &= .7182\text{E-}01 * \text{Weight} + 42.77 & R^2 &= .3049 \\ \text{Shoulder Height} &= .8751 * \text{Standing} - 3.936 & R^2 &= .9194 \\ \text{Shoulder Height} &= .7555\text{E-}02 * \text{Weight} + .8469 * \text{Standing} - 3.096 & R^2 &= .9218 \end{aligned}$$

where Shoulder Height, generally referred to as  $\hat{Y}$ , is the predicted dependent variable. Predictor or independent variables are generally referred to as  $X_i$  and in the above example are Weight and Standing Height.

$R^2$  is calculated according to the following four steps:

1. The prediction error that would result without the use of the regression equation is calculated. This prediction error is the sum of the squared differences between the observed value of  $Y$  at each observed value of  $X_1$  (and  $X_2$ ) and the mean value of  $Y$ .

$$\Sigma(Y_i - \bar{Y})^2, i=1, \dots, n$$



2. The prediction error that would result from using the regression equation to predict the behavior of the dependent variable is calculated. This prediction error is the sum of the squared differences between the observed value of Y and the predicted value of Y at each observed value of X<sub>1</sub> (and X<sub>2</sub>).

$$\Sigma(Y_i - \hat{Y}_i)^2, i=1, \dots, n$$

3. The resulting prediction error from step 2 is subtracted from the resulting prediction error from step 1. This difference represents the reduction in the prediction error achieved by using the regression equation predictions rather than the mean.

4. This reduction is expressed as a percentage by dividing the difference from step 3 by the result from step 1 to obtain a percentage reduction in the amount of the prediction error and is equal to R<sup>2</sup>.

The values of R<sup>2</sup> are always between zero and one, or equivalently, a percentage between 0 and 100 percent. A value of 0 implies that the regression equation is useless in reducing the prediction error and, therefore, has little or no predictive ability beyond that provided by using the mean value. A value of 50 percent implies that the prediction error has been reduced by 50 percent, or cut in half, by using the regression equation. Finally, a value of 100 percent indicates that no prediction error occurs when the regression equation is used.

In some instances, the regression equations used by GEBODIII may yield questionable results. This is true when one or more subjects in the regression analysis sample have extreme values for standing height and/or weight. In this case, due to the use of the least squares method, the regression line may have been disproportionately skewed toward the extreme. A user running the program may input a value for standing height and/or weight that

is within the specified range of reasonable values, but end up with an unreasonable value for a predicted variable.

While  $R^2$  is a measure of the relationship between the dependent and independent variables, it can not be used as the sole indicator of the effectiveness of the regression equation. If there is an extreme value pulling the regression line toward that value, the  $R^2$  value may be quite high, while the regression equation may not best represent the data.

If the regression results from using GEBODIII appear to be unsatisfactory, the user should first check the measurement description and summary statistics to determine whether the predicted value is reasonable. It is important to check these descriptions, especially when comparing regression results between males and females, since the method of measurement may vary somewhat.

The following example demonstrates the importance of referring to the measurement descriptions and summary statistics to determine the usefulness of predicted body measurements. The regression equation for the ankle height of an adult male of 179.84 pounds (800 newtons) and 72.05 inches (1.83 meters) results in a predicted value of 5.6 inches (.1422 meters). The equation for an adult female of equal standing height and weight results in a predicted value of 3.01 inches (.0723 meters). These values seem to be quite different and raise suspicion regarding their validity. However, the female dimension was measured from the standing surface to the lateral malleolus landmark, while the male dimension was measured from the standing surface to the level of minimum ankle circumference, which is found above the lateral malleolus landmark. The female ankle height is, therefore, expected to be noticeably shorter than that of the male. The mean value of these measurements confirms that the predicted values are reasonable.

If the predicted value is found to be unreasonable after checking the measurement description and summary statistics, it is safe to assume that the regression line is affected by an extreme value. In this case, the mean value of that measurement instead of the predicted value generated by GEBODIII should be used.

The user should examine the tabular output of GEBODIII to determine that the predicted body measurement values are reasonable. If the user decides to change some of the body measurements predicted by the program, the User-Supplied Body Dimensions option can be used. In this case, the user must create an input file that will be read through unit 1, containing all 32 body measurements. Refer to Appendix A of Baughman (1983), for specifics on the format of the file. The user can supply the body measurements from GEBODIII and substitute alternate values in place of those predicted values which are unreasonable. The body measurements provided by running GEBODIII with this user-defined data file will reflect the new values.

The measurement descriptions and summary statistics for adult male and adult female anthropometry are provided in Appendix F of this manual. An explanation of anthropometric terms used is presented in Appendix E. The actual regression equations used for predicting anthropometry (except for the hand) are given in Appendix D of Baughman (1983). These equations have remained unchanged. The regression equations for the hand dimensions of the Adult Human Female and Adult Human Male options have been added to GEBODIII and are given in Appendix A of this manual. Also, regression equations for joint center location, principal moments of inertia, and segment volume for the Adult Human Female and Adult Human Male options have been incorporated into the program and are given in Appendix B, C, and D of this manual, respectively.

## 1.4 SEGMENT ELLIPSOID ALIGNMENT

The segment ellipsoid positions were obtained by using regression equations to locate the joint center with respect to the center of gravity for each segment. Using the ATB model, the ellipsoids were then visually aligned by adjusting each ellipsoid center with respect to the segment center of gravity, so that as the segments moved, the ellipsoid alignment was maintained.

Currently, there is no anthropometric data available upon which to directly predict the location of the ellipsoid center with respect to the segment center of gravity; therefore, the expressions used to calculate these locations were derived by trial-and-error and are, in most cases, based on joint center locations or segment semiaxes. Section 2.3.1.3 in Part 2 of this manual describes this process in more detail.

### 1.4.1 ADJUSTING THE SEGMENT ELLIPSOID ALIGNMENT

There may be some instances where the user is not completely satisfied with the segment ellipsoid alignment as shown in a plot of the program output. This may occur when the subject is extremely tall and skinny or extremely short and fat. Ellipsoid alignment is easily changed by altering the ellipsoid center with respect to segment center of mass data in the B.2 cards in the ATB input data set. By adjusting the X, Y, and Z values in the local coordinate system, the user should be able to align the ellipsoids as desired.

Most ellipsoid alignments provided by GEBODIII are reasonable, and the ellipsoid centers should not be altered unless a graphic plot of the body indicates such action.

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PART 2  
PROGRAM DESCRIPTION  
2.1 INTRODUCTION

This part describes in more detail the modifications and improvements that were made to create GEBODIII. These changes are as follows:

- 1) The option to output data for the Sitting Hybrid III, Standing Hybrid III, and the Hybrid II manikin data sets was added.
- 2) Human stereophotometric data (McConville, et al., 1980; Young, et al., 1983) were incorporated into the program in the form of regression equations used to calculate segment mass properties and joint center locations for the adult human options.
- 3) Joint characteristics for the adult human options were added.
- 4) The option to output data for either combined or separated forearm and hand segments for the adult human options was added.
- 5) Since kilograms is a metric unit of mass, not weight, all weight data is now output in metric units of newtons. Also the use of meters and centimeters was inconsistent for metric output in GEBOD. GEBODIII makes use of meters only.
- 6) The user is prompted for filenames to be used by the program.
- 7) Alterations to make the program more portable to other computers were made.

Changes 1, 2, 3, and 4 are described more thoroughly in the following sections.

## 2.2 CHILD AND USER-DEFINED BODY DIMENSIONS OPTIONS

The methods of calculating body data for subject type options 1 and 4, the Child and the User-Defined Body Dimensions options, respectively, have not been altered with this version of GEBOD. Refer to Baughman (1983) for details describing these calculations.

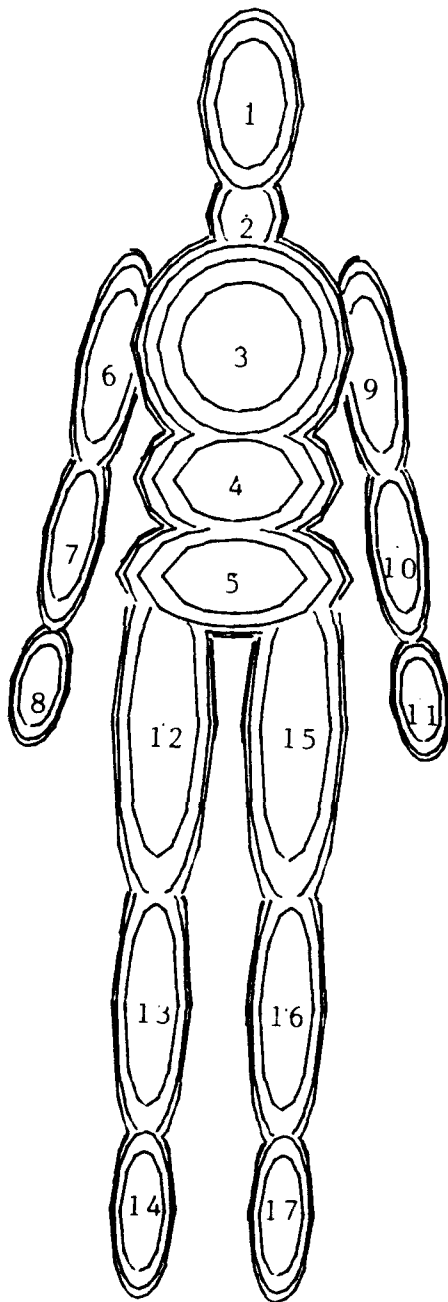
## 2.3 ADULT HUMAN FEMALE AND ADULT HUMAN MALE OPTIONS

The methods of calculating body data for subject type options 2 and 3 have been changed significantly. Previously, the methods used by GEBOD to calculate the segment mass properties were based on the segment ellipsoids, not directly measured body geometry or mass properties. This method was replaced with calculations from stereophotometrically generated body surface data obtained from both male and female sample populations (McConville, et al., 1980; Young, et al., 1983). Joint center locations were based on three-dimensional surface landmark data also available in the stereophotometric data sets.

With past versions of GEBOD, output was limited to body data for 15 segments where the forearm and hand were considered as one segment. Because of the many applications involving hand movement, the need arose to consider the forearm and hand segments separately, connected by the wrist joint. This option was incorporated into GEBODIII, making available body data for 17 segments. Figure 2 depicts the 17 segment configuration. Regression equations to calculate hand length, hand breadth, and hand thickness were added to GEBODIII. These equations are given in Appendix A.

### 2.3.1 Body Geometry

The body geometry includes the contact ellipsoid semiaxes and



1. Head
2. Neck
3. Thorax
4. Abdomen
5. Pelvis
6. Right Upper Arm
7. Right Lower Arm
8. Right Hand
9. Left Upper Arm
10. Left Lower Arm
11. Left Hand
12. Right Thigh
13. Right Calf
14. Right Foot
15. Left Thigh
16. Left Calf
17. Left Foot

**Figure 2. Seventeen Segment Configuration**



joint locations for each segment in the local reference axis system.

#### 2.3.1.1 Reference axis systems

All data output by GEBODIII are described with respect to the segment local reference axis systems. Each segment's local axis system is defined such that its origin is at the segment center of mass and, when the body is in a standing position with the toes pointing down, the local axis systems' positive Z-axes point down, positive X-axes point forward, and positive Y-axes point to the right of the body.

The stereophotometric data was collected in a global axis system defined with the body in the standard anatomical position with the origin on the floor centrally located between the subject's feet and directly underneath the body. The axes are defined so that the positive X-axis points forward, positive Y-axis points to the left of the body, and positive Z-axis points upward from the origin. The hands of the female subjects were positioned with the palms facing anteriorly; the hands of the male subjects were positioned with the palms facing posteriorly.

In segmenting the data, McConville and Young defined the standard anatomical axis systems for each segment based on body surface landmarks. In general, anatomical axis systems are defined so that the positive X-axes point forward, positive Y-axes point to the body's left, and positive Z-axes point distal to proximal. Complete definitions of the anatomical axis systems are given in McConville, et al. (1980) for males and Young, et al. (1983) for females.

Based on the above definitions, the transformation from the segment anatomical axis system to the local axis system consists of a translation to the segment center of mass and a 180 degree rotation about the anatomical X-axis for all the segments except

the neck and pelvis. The landmarks used to define the anatomical axis systems for these two segments result in X-axes that are not horizontal in the standing position. Therefore, the transformation from the segment anatomical axis system to the local axis system for these two segments includes a rotation about the Y-axis after the X-axis rotation. For the neck, this Y-axis rotation is +30 degrees and for the pelvis, -12 degrees. The transformation cosine matrix from the neck anatomical axis system to the neck local axis system is:

$$\begin{bmatrix} \cos(30^\circ) & 0 & \sin(30^\circ) \\ 0 & -1 & 0 \\ \sin(30^\circ) & 0 & -\cos(30^\circ) \end{bmatrix}$$

The transformation cosine matrix from the pelvis anatomical axis system to the pelvis local axis system is:

$$\begin{bmatrix} \cos(12^\circ) & 0 & -\sin(12^\circ) \\ 0 & -1 & 0 \\ -\sin(12^\circ) & 0 & -\cos(12^\circ) \end{bmatrix}$$

The transformation cosine matrix from the anatomical axis system to the local axis system for all other segments is:

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

In the stereophotometric data for the adult human female forearms, the anatomical Z-axis is represented as a vector from the ulnar styloid landmark to the radiale landmark. This vector crosses the forearm diagonally from lateral to medial which did not conform to the desired vertical alignment of the segment axes. Therefore, the anatomical axes were redefined as follows:

### RIGHT FOREARM

Z axis - vector from radial styloid to radiale

Y axis - normal from Z axis to ulnar styloid

X axis -  $\underline{Y} \times \underline{Z}$

Origin - at radiale

### LEFT FOREARM

Z axis - vector from radial styloid to radiale

Y axis - normal from ulnar styloid to Z axis

X axis -  $\underline{Y} \times \underline{Z}$

Origin - at radiale

The local reference axes for the right and left forearm segments were obtained by rotating the above anatomical axes 180 degrees about the X axis and translating the origin to the center of mass.

#### 2.3.1.2 Segment ellipsoid semiaxes

Segment ellipsoid semiaxes are based on anthropometric dimensions. Expressions to calculate ellipsoid semiaxes for the right and left forearm and right and left hand segments are given in Table I where references to the  $i^{\text{th}}$  body measurement are made by  $DD_i$ . The body measurements are in Appendix F. The

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TABLE I  
EXPRESSIONS FOR FOREARM AND HAND SEMIAXES (IN)

| <u>SEGMENT</u> | <u>X</u>        | <u>Y</u>        | <u>Z</u>   |
|----------------|-----------------|-----------------|--|
| Forearms       | $DD_{21}/2\pi$  | $DD_{21}/2\pi$  | Females: $(DD_{18} - DD_{33}) * 0.5$<br>Males: $(DD_{18} - DD_{33}) * 0.6$ |
| Hands          | $DD_{34} * 0.5$ | $DD_{34} * 0.5$ | $DD_{33} * 0.5$  |

---

expressions to calculate ellipsoid semiaxes for all other

segments have not changed from previous versions of GEBOD (Baughman, 1983).

#### 2.3.1.3 Segment ellipsoid centers

Previous versions of GEBOD made the assumption that the segment ellipsoid center was located at the segment center of mass (CM) for most segments. For the pelvis, abdomen, thorax, and feet segments, GEBOD calculated the global location of the ellipsoid center in the Z direction based on predicted body description data and numerical integration was used to calculate the segment CM in the Z direction. Then the segment ellipsoid center Z location was subtracted from the Z location of the segment CM to give the segment ellipsoid center in the local reference axis system on the B.2 card of the ATB input data set.

No such assumptions are made in GEBODIII, since it is known that the segment CM is not, in most cases, actually located at the segment ellipsoid center. However, the exact location of the ellipsoid center with respect to segment CM is not known either. Therefore, the ellipsoid center in each local axis system was arrived at by visually aligning the segment ellipsoids with respect to each other.

Ellipsoids were aligned for an average size adult human male subject by adjusting ellipsoid centers segment-by-segment, beginning with the feet and working up to the head. The arm segments were aligned with each other and then with the rest of the body. The alignment was validated for a small and a large male subject. The ellipsoids of the adult human female were similarly aligned.

The 15 and 17 segment ellipsoid configurations align well for the adult human male. For the adult human female, the 15 segment ellipsoid configuration aligns well; however, in the 17 segment ellipsoid configuration, all segments are well aligned, except

the hands. The user may wish to adjust ellipsoid locations for some subjects, as described in section 1.4.1 of Part 1, so that the hand alignment is more reasonable.

#### 2.3.1.4 Joint center locations

The three-dimensional joint center locations were calculated in the global axis system for each male and female stereophotometric subject based on three-dimensional landmark locations. Table II contains a list of landmarks used in the expressions to define joint center locations. Table III contains a list of the expressions. The expression used to locate the hip joint center is from Andriacchi and Strickland (1985). All other expressions were obtained by experimentation. These global joint center locations were transformed to the local reference axis systems. The resulting joint center locations were then used to calculate regression equations to estimate joint center locations in the local reference axis system for adult human female and male subject type options. These regression equations are in Appendix B.

#### 2.3.2 Inertial Properties

##### 2.3.2.1 Segment centers of mass

The segment centers of mass are indirectly located by defining the origins of the segment local reference axis systems to be at the segment centers of mass and specifying the remaining data, such as the joint and ellipsoid center locations in the local reference axis systems.

##### 2.3.2.2 Moments of inertia

The principal moments of inertia were calculated from the stereophotometric data for each female and male subject. These data were used to calculate regression equations to predict each segment's principal moments of inertia for the adult human female and male subject type options. These regression equations are in

TABLE II  
 LANDMARKS USED IN EXPRESSIONS TO DEFINE  
 JOINT CENTER LOCATIONS

| <u>Landmark Number</u> | <u>Landmark Name</u>                |
|------------------------|-------------------------------------|
| 1X, 1Y, 1Z             | Left Tragion                        |
| 2X, 2Y, 2Z             | Right Tragion                       |
| 3X, 3Y, 3Z             | Cervicale                           |
| 4X, 4Y, 4Z             | Tenth Rib Midspine                  |
| 5X, 5Y, 5Z             | Posterior Superior Iliac Midspine   |
| 6X, 6Y, 6Z             | Right Acromion                      |
| 7X, 7Y, 7Z             | Right Medial Humeral Epicondyle     |
| 8X, 8Y, 8Z             | Right Lateral Humeral Epicondyle    |
| 9X, 9Y, 9Z             | Right Radial Styloid                |
| 10X, 10Y, 10Z          | Right Ulnar Styloid                 |
| 11X, 11Y, 11Z          | Left Acromion                       |
| 12X, 12Y, 12Z          | Left Medial Humeral Epicondyle      |
| 13X, 13Y, 13Z          | Left Lateral Humeral Epicondyle     |
| 14X, 14Y, 14Z          | Left Radial Styloid                 |
| 15X, 15Y, 15Z          | Left Ulnar Styloid                  |
| 16X, 16Y, 16Z          | Right Trochanterion                 |
| 17X, 17Y, 17Z          | Right Anterior Superior Iliac Spine |
| 18X, 18Y, 18Z          | Symphysion                          |
| 19X, 19Y, 19Z          | Right Lateral Femoral Epicondyle    |
| 20X, 20Y, 20Z          | Right Medial Femoral Epicondyle     |
| 21X, 21Y, 21Z          | Right Medial Malleolus              |
| 22X, 22Y, 22Z          | Right Lateral Malleolus             |
| 23X, 23Y, 23Z          | Left Trochanterion                  |
| 24X, 24Y, 24Z          | Left Anterior Superior Iliac Spine  |
| 25X, 25Y, 25Z          | Left Lateral Femoral Epicondyle     |
| 26X, 26Y, 26Z          | Left Medial Femoral Epicondyle      |
| 27X, 27Y, 27Z          | Left Medial Malleolus               |
| 28X, 28Y, 28Z          | Left Lateral Malleolus              |

TABLE III  
 EXPRESSIONS FOR JOINT CENTER LOCATIONS  
 IN GLOBAL AXES (IN)

| <u>Joint Name</u> | <u>Location</u> | <u>Expression</u>             |
|-------------------|-----------------|-------------------------------|
| Head-Neck         | X               | $(1X + 2X) / 2.$              |
|                   | Y               | $(1Y + 2Y) / 2.$              |
|                   | Z               | $((1Z + 3Z) / 2.) - 1.1811$   |
| Neck-Thorax       | X               | $3X + 2.0079$                 |
|                   | Y               | $3Y$                          |
|                   | Z               | $3Z - 0.9843$                 |
| Thorax-Abdomen    | X               | $4X + 2.0079$                 |
|                   | Y               | $4Y$                          |
|                   | Z               | $4Z$                          |
| Abdomen-Pelvis    | X               | $5X + 2.0079$                 |
|                   | Y               | $5Y$                          |
|                   | Z               | $5Z$                          |
| Right Shoulder    | X               | $6X$                          |
|                   | Y               | $6Y + 1.4961$                 |
|                   | Z               | $6Z - 1.4961$                 |
| Right Elbow       | X               | $(7X + 8X) / 2.$              |
|                   | Y               | $(7Y + 8Y) / 2.$              |
|                   | Z               | $(7Z + 8Z) / 2.$              |
| Right Wrist       | X               | $(9X + 10X) / 2.$             |
|                   | Y               | $(9Y + 10Y) / 2.$             |
|                   | Z               | $(9Z + 10Z) / 2.$             |
| Left Shoulder     | X               | $11X$                         |
|                   | Y               | $11Y - 1.4961$                |
|                   | Z               | $11Z - 1.4961$                |
| Left Elbow        | X               | $(12X + 13X) / 2.$            |
|                   | Y               | $(12Y + 13Y) / 2.$            |
|                   | Z               | $(12Z + 13Z) / 2.$            |
| Left Wrist        | X               | $(14X + 15X) / 2.$            |
|                   | Y               | $(14Y + 15Y) / 2.$            |
|                   | Z               | $(14Z + 15Z) / 2.$            |
| Right Hip         | X               | $16X$                         |
|                   | Y               | $(17Y + 18Y) / 2.$            |
|                   | Z               | $((17Z + 18Z) / 2.) - 0.5906$ |
| Right Knee        | X               | $(19X + 20X) / 2.$            |
|                   | Y               | $(19Y + 20Y) / 2.$            |
|                   | Z               | $(19Z + 20Z) / 2.$            |
| Right Ankle       | X               | $(21X + 22X) / 2.$            |
|                   | Y               | $(21Y + 22Y) / 2.$            |
|                   | Z               | $(21Z + 22Z) / 2.$            |
| Left Hip          | X               | $23X$                         |
|                   | Y               | $(18Y + 24Y) / 2.$            |
|                   | Z               | $((18Z + 24Z) / 2.) - 0.5906$ |

---

TABLE III (Continued)

|            |   |                  |
|------------|---|------------------|
| Left Knee  | X | (25X + 26X) / 2. |
|            | Y | (25Y + 26Y) / 2. |
|            | Z | (25Z + 26Z) / 2. |
| Left Ankle | X | (27X + 28X) / 2. |
|            | Y | (27Y + 28Y) / 2. |
|            | Z | (27Z + 28Z) / 2. |

---

Appendix C. Mean principal axes orientations for both the adult male and female subject type options were determined with respect to the local axes and used for all subjects.

#### 2.3.2.3 Segment weights

The stereophotometric data were used to calculate the volume of each segment for each female and male subject. The volumes were used to calculate regression equations to predict segment volumes for the adult human female and male subject type options. These regression equations are in Appendix D. The estimated volumes are transformed to weights using the relationship, weight (slugs) = volume (in<sup>3</sup>) \* density (slugs/in<sup>3</sup>), where density is a constant 1.12287E-3. The segment weights are then converted to pounds and adjusted so that their sum equals the total body weight.

#### 2.3.3 Joint Characteristics

Most of the joints' elastic, viscous, and joint stop characteristics were obtained from a number of sources, including Engin and Chen (1987), and adjusted to provide physically realistic ATB model results. For the joints that did not have a complete set of properties available, the characteristics were estimated based on data from the other joints. These characteristics have been used in ATB simulations by Armstrong Laboratory (AL) with good results for several years.



#### 2.3.4 Comparison of Stereophotometric Data Distributions with Air Force Distributions

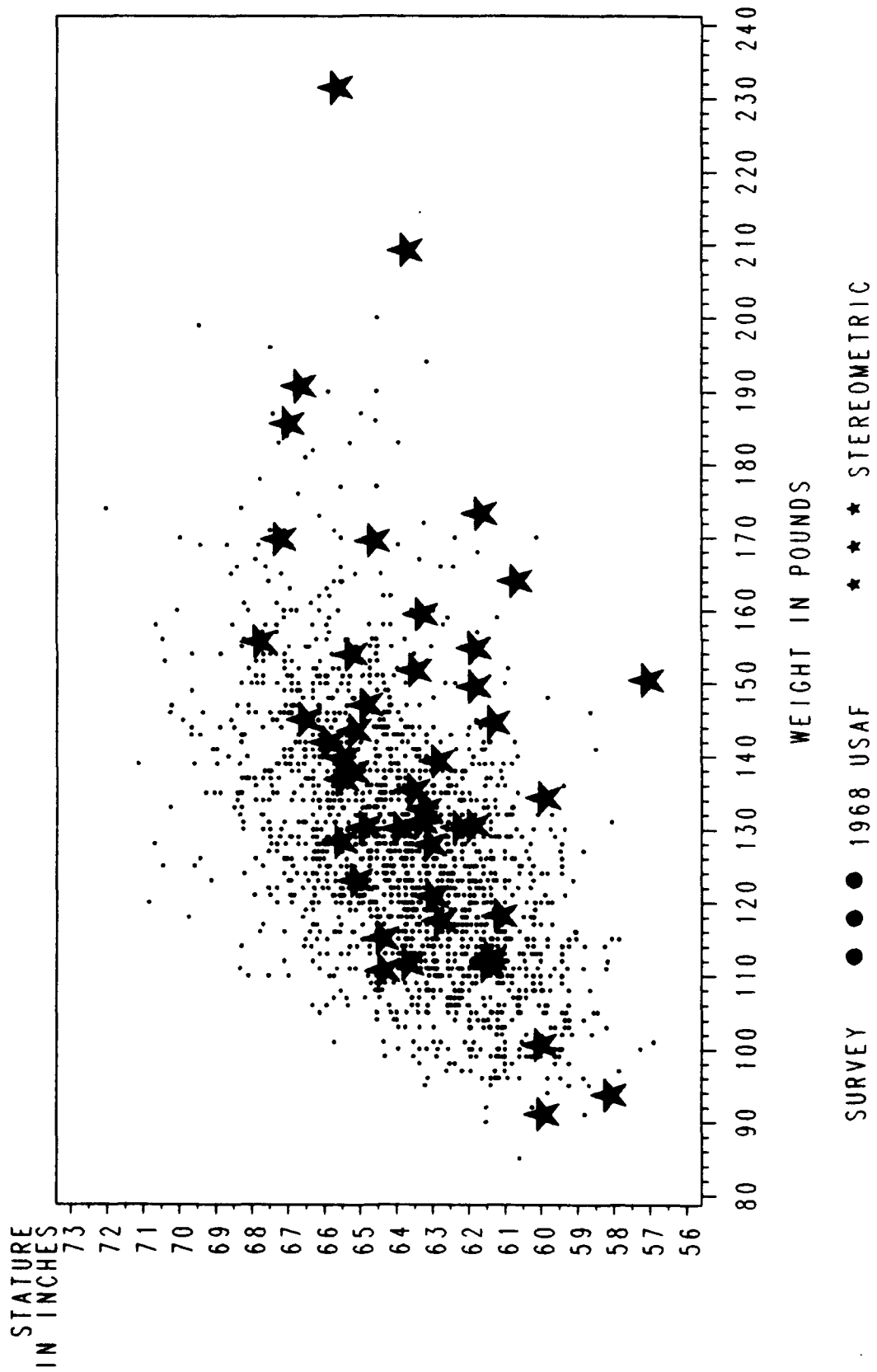
Originally, the only actual human data used by GEBOD was from the 1967 and 1968 USAF anthropometric surveys. When the idea was conceived to incorporate into GEBODIII the inertial property data provided by the stereophotometric surveys, it became necessary to compare the USAF and stereophotometric surveys to determine the compatibility of the data.

Selection of the male stereophotometric data subjects was based on the 1967 USAF survey stature and weight distribution. Figure 3 is a bivariate plot of the 1967 USAF stature and weight distribution overlaid with the male stereophotometric stature and weight distribution. The slope of the two data distributions show that the relationship between stature and weight for the two survey distributions is similar, as expected. This demonstrates the soundness of using the male stereophotometric data to obtain inertial properties in GEBODIII.

Selection of the female stereophotometric data subjects was based on a civilian female stature and weight distribution. Figure 4 is a bivariate plot of the 1968 USAF stature and weight distribution overlaid with the female stereophotometric stature and weight distribution. It shows that the stereophotometric females are shorter and heavier than the USAF females; therefore, the relationship between stature and weight is different for the two surveys. In spite of this difference, comparisons of GEBODII and GEBODIII to the actual data of several stereophotometric subjects have shown a vast improvement by using the stereophotometric data to produce inertial property output, over using the geometric approximations.



FIGURE 4  
BIVARIATE PLOT FOR STATURE AND WEIGHT  
1968 USAF AND STEREOMETRIC FEMALES



## 2.4 DUMMY DATA SETS

Output is available for the following dummy data sets: Hybrid III with seated pelvis (50<sup>th</sup> percentile), Hybrid III with standing pelvis (50<sup>th</sup> percentile), and Hybrid II (50<sup>th</sup> percentile). The data set for the Hybrid II dummy, also known as the Part 572 dummy, was developed by Fleck, Butler, and DeLeys (1982), to be used in validating the Crash Victim Simulator (CVS), an earlier version of the ATB model. The development of the Hybrid III dummy data sets is fully documented in Kaleps, et al. (1988). The user can choose input and output in English (pounds, inches) or metric (newtons, meters) units, and the output format can be in ATB input format, tabular format, or both. Since these data sets were compiled under different efforts, the amount of data varies somewhat. For example, the Hybrid III data sets include surface deformation properties, whereas the Hybrid II data set does not.

Because the dummy data sets do not change, they are stored in the GEBOD.DAT file which is read by GEBODIII. The ATB formatted input data set for each dummy is stored in English and metric units, in the GEBOD.DAT data file. In the file, each data set is preceded by a line which indicates how many lines are in the following data set and provides a data set title. This title is used to find the data set to be used. When a title match is found, GEBODIII simply reads the appropriate English or metric data from GEBOD.DAT and writes it to the appropriate output units.

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APPENDIX A  
HAND DIMENSION REGRESSION EQUATIONS

This appendix contains a complete listing of the hand dimension regression equations developed for the adult human female and the adult human male options. The regression equations for the adult human female are based on the 1968 U.S. Air Force survey (Clauser, et al., 1972) and the equations for the adult human male are based on the 1967 U.S. Air Force survey (Grunhofer and Kroh, 1975). The predicting variables are weight (lb) and standing height (in). The predicted hand dimensions are in inches. At the top of each set of regression equations are listed the range of values, mean, and standard deviation of the predicting variables within that subject type option. For each hand dimension, a separate regression equation is given against each of the predicting variables. The last regression equation is a multiple regression equation based on both predicting variables. With each regression equation, the coefficient of determination ( $R^2$ ) is given. Since hand depth was not measured in the 1968 U.S. Air Force survey, the regression equations given for female hand depth are based on the 1967 U.S. Air Force survey and, therefore, are the same as the equations given for the males. The regression equations are based on 1905 female subjects and 2420 male subjects.

REGRESSION EQUATIONS FOR ADULT FEMALE HAND DIMENSIONS

PREDICTING VARIABLES

WEIGHT RANGE: 85.00 200.00 MEAN: 127.30 S.D.: 16.590  
 STANDING HEIGHT RANGE: 56.93 72.05 MEAN: 63.82 S.D.: 2.364

REGRESSION EQUATIONS FOR HAND BREADTH

HAND BREADTH = 0.003847 \*WEIGHT +2.480278 R\*\*2 = 0.1736  
 HAND BREADTH = 0.024549 \*STANDING +1.403283 R\*\*2 = 0.1436  
 HAND BREADTH = 0.002769 \*WEIGHT +0.014202 \*STANDING +1.711157 R\*\*2 = 0.2080

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REGRESSION EQUATIONS FOR HAND LENGTH

HAND LENGTH = 0.008718 \*WEIGHT +6.122934 R\*\*2 = 0.1466  
 HAND LENGTH = 0.096038 \*STANDING +1.103882 R\*\*2 = 0.3614  
 HAND LENGTH = 0.001995 \*WEIGHT +0.088582 \*STANDING +1.325739 R\*\*2 = 0.3669

REGRESSION EQUATIONS FOR HAND DEPTH (BASED ON MALE DATA)

HAND DEPTH = 0.000996 \*WEIGHT +0.912979 R\*\*2 = 0.0667  
 HAND DEPTH = 0.006630 \*STANDING +0.623029 R\*\*2 = 0.0381  
 HAND DEPTH = 0.000828 \*WEIGHT +0.002881 \*STANDING +0.741114 R\*\*2 = 0.0720

REGRESSION EQUATIONS FOR ADULT MALE HAND DIMENSIONS

PREDICTING VARIABLES

WEIGHT RANGE: 118.00 264.00 MEAN: 173.60 S.D.: 21.440  
 STANDING HEIGHT RANGE: 62.17 77.64 MEAN: 69.82 S.D.: 2.437

REGRESSION EQUATIONS FOR HAND BREADTH

HAND BREADTH = 0.003424 \*WEIGHT +2.906047 R\*\*2 = 0.1995  
 HAND BREADTH = 0.027691 \*STANDING +1.567278 R\*\*2 = 0.1685  
 HAND BREADTH = 0.002455 \*WEIGHT +0.016569 \*STANDING +1.917571 R\*\*2 = 0.2439

REGRESSION EQUATIONS FOR HAND LENGTH

HAND LENGTH = 0.005839 \*WEIGHT +6.504896 R\*\*2 = 0.1503  
 HAND LENGTH = 0.086296 \*STANDING +1.493816 R\*\*2 = 0.4239  
 HAND LENGTH = 0.001076 \*WEIGHT +0.061423 \*STANDING +1.647298 R\*\*2 = 0.4276

REGRESSION EQUATIONS FOR HAND DEPTH

HAND DEPTH = 0.000996 \*WEIGHT +0.912979 R\*\*2 = 0.0667  
 HAND DEPTH = 0.006630 \*STANDING +0.623029 R\*\*2 = 0.0381  
 HAND DEPTH = 0.000828 \*WEIGHT +0.002881 \*STANDING +0.741114 R\*\*2 = 0.0720



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APPENDIX B  
JOINT CENTER LOCATION REGRESSION EQUATIONS

This appendix contains a complete listing of the regression equations for the joint center locations in the local axis system developed for the adult human female and the adult human male options. The regression equations are based on human stereophotometric surface landmark location data (McConville, et al., 1980; Young, et al., 1983). The predicting variables are weight (lb) and standing height (in). The predicted joint center locations are in inches. At the top of each set of regression equations are listed the range of values, mean, and standard deviation of the predicting variables within that subject type option. A joint center location is described by a three-dimensional location in each adjoining segment in that segment's local reference axis system. For the X, Y, and Z location of each joint location, a separate regression equation is given against each of the predicting variables. The last regression equation is a multiple regression equation based on both predicting variables. With each regression equation, the coefficient of determination ( $R^2$ ) is given. The regression equations are based on 46 female subjects and 31 male subjects.

REGRESSION EQUATIONS FOR ADULT FEMALE JOINT CENTER LOCATIONS

PREDICTING VARIABLES

|                 |              |        |              |              |
|-----------------|--------------|--------|--------------|--------------|
| WEIGHT          | RANGE: 85.00 | 200.00 | MEAN: 127.30 | S.D.: 16.590 |
| STANDING HEIGHT | RANGE: 56.93 | 72.05  | MEAN: 63.82  | S.D.: 2.364  |

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS X COORDINATE

|                           |   |           |           |           |               |
|---------------------------|---|-----------|-----------|-----------|---------------|
| ABDOMEN-PELVIS WRT PELVIS | = | -0.011939 | *WEIGHT   | -0.084100 | R**2 = 0.3959 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.006868 | *STANDING | -1.330381 | R**2 = 0.0009 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.014132 | *WEIGHT   | +0.062264 | R**2 = 0.4601 |
|                           |   |           | *STANDING | -3.727573 |               |

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REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS Y COORDINATE

|                           |   |           |           |           |               |
|---------------------------|---|-----------|-----------|-----------|---------------|
| ABDOMEN-PELVIS WRT PELVIS | = | -0.002634 | *WEIGHT   | +0.343410 | R**2 = 0.1700 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.021026 | *STANDING | +1.306908 | R**2 = 0.0780 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.002288 | *WEIGHT   | -0.009832 | R**2 = 0.1842 |
|                           |   |           | *STANDING | +0.918761 |               |

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS Z COORDINATE

|                           |   |           |           |           |               |
|---------------------------|---|-----------|-----------|-----------|---------------|
| ABDOMEN-PELVIS WRT PELVIS | = | -0.015625 | *WEIGHT   | +0.553757 | R**2 = 0.5264 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.025001 | *STANDING | -0.060794 | R**2 = 0.0097 |
| ABDOMEN-PELVIS WRT PELVIS | = | -0.017813 | *WEIGHT   | +0.062141 | R**2 = 0.5760 |
|                           |   |           | *STANDING | -3.082532 |               |

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN X COORDINATE

|                            |   |           |           |           |               |
|----------------------------|---|-----------|-----------|-----------|---------------|
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.016965 | *WEIGHT   | +0.758479 | R**2 = 0.6359 |
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.022146 | *STANDING | -0.226130 | R**2 = 0.0078 |
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.019554 | *WEIGHT   | +0.073510 | R**2 = 0.7070 |
|                            |   |           | *STANDING | -3.543103 |               |

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN Y COORDINATE

|                            |   |           |           |           |               |
|----------------------------|---|-----------|-----------|-----------|---------------|
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.001232 | *WEIGHT   | +0.152484 | R**2 = 0.0547 |
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.006846 | *STANDING | +0.413536 | R**2 = 0.0122 |
| THORAX-ABDOMEN WRT ABDOMEN | = | -0.001197 | *WEIGHT   | -0.000992 | R**2 = 0.0549 |
|                            |   |           | *STANDING | +0.210518 |               |

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN Z COORDINATE

|                            |   |          |           |           |               |
|----------------------------|---|----------|-----------|-----------|---------------|
| THORAX-ABDOMEN WRT ABDOMEN | = | 0.001250 | *WEIGHT   | -1.282322 | R**2 = 0.0119 |
| THORAX-ABDOMEN WRT ABDOMEN | = | 0.016781 | *STANDING | -2.171454 | R**2 = 0.0154 |
| THORAX-ABDOMEN WRT ABDOMEN | = | 0.000796 | *WEIGHT   | +0.012887 | R**2 = 0.0194 |
|                            |   |          | *STANDING | -2.036457 |               |

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX X COORDINATE

|                        |   |           |           |           |               |
|------------------------|---|-----------|-----------|-----------|---------------|
| NECK-THORAX WRT THORAX | = | -0.009617 | *WEIGHT   | +0.994733 | R**2 = 0.3981 |
| NECK-THORAX WRT THORAX | = | 0.001555  | *STANDING | -0.458953 | R**2 = 0.0001 |
| NECK-THORAX WRT THORAX | = | -0.011684 | *WEIGHT   | +0.058713 | R**2 = 0.4865 |
|                        |   |           | *STANDING | -2.440950 |               |

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX Y COORDINATE

NECK-THORAX WRT THORAX = -0.001619 \*WEIGHT +0.270258 R\*\*2 = 0.0917  
NECK-THORAX WRT THORAX = -0.002989 \*STANDING +0.231867 R\*\*2 = 0.0022  
NECK-THORAX WRT THORAX = -0.001829 \*WEIGHT +0.005958 \*STANDING -0.078373 R\*\*2 = 0.0991

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX Z COORDINATE

NECK-THORAX WRT THORAX = -0.012330 \*WEIGHT -5.068301 R\*\*2 = 0.3482  
NECK-THORAX WRT THORAX = -0.154705 \*STANDING +3.014805 R\*\*2 = 0.3946  
NECK-THORAX WRT THORAX = -0.008315 \*WEIGHT -0.114029 \*STANDING +1.604334 R\*\*2 = 0.5256

REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK X COORDINATE

HEAD-NECK WRT NECK = 0.001385 \*WEIGHT -0.874711 R\*\*2 = 0.0086  
HEAD-NECK WRT NECK = -0.025848 \*STANDING +0.961229 R\*\*2 = 0.0216  
HEAD-NECK WRT NECK = 0.002773 \*WEIGHT -0.039412 \*STANDING +1.431563 R\*\*2 = 0.0502

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REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK Y COORDINATE

HEAD-NECK WRT NECK = -0.000777 \*WEIGHT +0.102504 R\*\*2 = 0.0207  
HEAD-NECK WRT NECK = 0.002285 \*STANDING -0.151979 R\*\*2 = 0.0013  
HEAD-NECK WRT NECK = -0.001036 \*WEIGHT +0.007351 \*STANDING -0.327647 R\*\*2 = 0.0317

REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK Z COORDINATE

HEAD-NECK WRT NECK = -0.000979 \*WEIGHT -2.031634 R\*\*2 = 0.0116  
 HEAD-NECK WRT NECK = -0.026838 \*STANDING -0.465923 R\*\*2 = 0.0628  
 HEAD-NECK WRT NECK = -0.000041 \*WEIGHT -0.026639 \*STANDING -0.472829 R\*\*2 = 0.0629

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS X COORDINATE

LEFT HIP WRT PELVIS = -0.004163 \*WEIGHT +1.208000 R\*\*2 = 0.0367  
 LEFT HIP WRT PELVIS = -0.009597 \*STANDING +1.230671 R\*\*2 = 0.0014  
 LEFT HIP WRT PELVIS = -0.004621 \*WEIGHT +0.013008 \*STANDING +0.446799 R\*\*2 = 0.0388

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS Y COORDINATE

LEFT HIP WRT PELVIS = -0.007290 \*WEIGHT -1.228729 R\*\*2 = 0.4431  
 LEFT HIP WRT PELVIS = -0.013859 \*STANDING -1.376161 R\*\*2 = 0.0115  
 LEFT HIP WRT PELVIS = -0.008218 \*WEIGHT +0.026342 \*STANDING -2.770156 R\*\*2 = 0.4776

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS Z COORDINATE

LEFT HIP WRT PELVIS = 0.004525 \*WEIGHT +2.157463 R\*\*2 = 0.2473  
 LEFT HIP WRT PELVIS = 0.013873 \*STANDING +1.914401 R\*\*2 = 0.0167  
 LEFT HIP WRT PELVIS = 0.004876 \*WEIGHT -0.009982 \*STANDING +2.741591 R\*\*2 = 0.2545

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH X COORDINATE

LEFT KNEE WRT THIGH = 0.003749 \*WEIGHT +0.226837 R\*\*2 = 0.0658  
 LEFT KNEE WRT THIGH = -0.019642 \*STANDING +2.001882 R\*\*2 = 0.0130  
 LEFT KNEE WRT THIGH = 0.005364 \*WEIGHT -0.045884 \*STANDING +2.911839 R\*\*2 = 0.1245

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH Y COORDINATE

LEFT KNEE WRT THIGH = -0.001190 \*WEIGHT -0.391704 R\*\*2 = 0.0232  
 LEFT KNEE WRT THIGH = -0.029322 \*STANDING +1.301907 R\*\*2 = 0.1012  
 LEFT KNEE WRT THIGH = -0.000191 \*WEIGHT -0.028390 \*STANDING +1.269591 R\*\*2 = 0.1017

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH Z COORDINATE

LEFT KNEE WRT THIGH = 0.001195 \*WEIGHT +9.148730 R\*\*2 = 0.0031  
 LEFT KNEE WRT THIGH = 0.193124 \*STANDING -2.942030 R\*\*2 = 0.5754  
 LEFT KNEE WRT THIGH = -0.006771 \*WEIGHT +0.226249 \*STANDING -4.090649 R\*\*2 = 0.6567

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF X COORDINATE

LEFT ANKLE WRT CALF = 0.004811 \*WEIGHT -0.109920 R\*\*2 = 0.1557  
 LEFT ANKLE WRT CALF = 0.009918 \*STANDING -0.061637 R\*\*2 = 0.0048  
 LEFT ANKLE WRT CALF = 0.005390 \*WEIGHT -0.016450 \*STANDING +0.852695 R\*\*2 = 0.1665

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF Y COORDINATE

LEFT ANKLE WRT CALF = 0.002479 \*WEIGHT +0.490224 R\*\*2 = 0.2546  
 LEFT ANKLE WRT CALF = 0.002794 \*STANDING +0.662149 R\*\*2 = 0.0023  
 LEFT ANKLE WRT CALF = 0.002876 \*WEIGHT -0.011276 \*STANDING +1.150037 R\*\*2 = 0.2859

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF Z COORDINATE

LEFT ANKLE WRT CALF = 0.010244 \*WEIGHT +7.665443 R\*\*2 = 0.3177  
 LEFT ANKLE WRT CALF = 0.169399 \*STANDING -1.644392 R\*\*2 = 0.6253  
 LEFT ANKLE WRT CALF = 0.005169 \*WEIGHT +0.144112 \*STANDING -0.767549 R\*\*2 = 0.6923

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX X COORDINATE

LEFT SHOULDER WRT THORAX = -0.005016 \*WEIGHT -0.624416 R\*\*2 = 0.0653  
 LEFT SHOULDER WRT THORAX = -0.025529 \*STANDING +0.289319 R\*\*2 = 0.0122  
 LEFT SHOULDER WRT THORAX = -0.004974 \*WEIGHT -0.001195 \*STANDING -0.554493 R\*\*2 = 0.0653

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX Y COORDINATE

LEFT SHOULDER WRT THORAX = -0.007228 \*WEIGHT -4.502333 R\*\*2 = 0.2780  
 LEFT SHOULDER WRT THORAX = -0.048877 \*STANDING -2.418194 R\*\*2 = 0.0915  
 LEFT SHOULDER WRT THORAX = -0.006653 \*WEIGHT -0.016329 \*STANDING -3.546826 R\*\*2 = 0.2865



REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX Z COORDINATE

LEFT SHOULDER WRT THORAX = -0.009839 \*WEIGHT -2.292073 R\*\*2 = 0.2738  
 LEFT SHOULDER WRT THORAX = -0.104962 \*STANDING +2.984474 R\*\*2 = 0.2243  
 LEFT SHOULDER WRT THORAX = -0.007421 \*WEIGHT -0.068658 \*STANDING +1.725595 R\*\*2 = 0.3532

REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM X COORDINATE

LEFT ELBOW WRT UPPER ARM = -0.002178 \*WEIGHT +0.306781 R\*\*2 = 0.1352  
 LEFT ELBOW WRT UPPER ARM = 0.004684 \*STANDING -0.297477 R\*\*2 = 0.0045  
 LEFT ELBOW WRT UPPER ARM = -0.002831 \*WEIGHT +0.018533 \*STANDING -0.777683 R\*\*2 = 0.1935

REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM Y COORDINATE

LEFT ELBOW WRT UPPER ARM = 0.001552 \*WEIGHT +0.094641 R\*\*2 = 0.0784  
 LEFT ELBOW WRT UPPER ARM = -0.021026 \*STANDING +1.648055 R\*\*2 = 0.1036  
 LEFT ELBOW WRT UPPER ARM = 0.002770 \*WEIGHT -0.034576 \*STANDING +2.117934 R\*\*2 = 0.3103

REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM Z COORDINATE

LEFT ELBOW WRT UPPER ARM = 0.001443 \*WEIGHT +4.768148 R\*\*2 = 0.0160  
 LEFT ELBOW WRT UPPER ARM = 0.101351 \*STANDING -1.462191 R\*\*2 = 0.5685  
 LEFT ELBOW WRT UPPER ARM = -0.002569 \*WEIGHT +0.113917 \*STANDING -1.897919 R\*\*2 = 0.6105

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM X COORDINATE

LEFT WRIST WRT FOREARM = -0.002159 \*WEIGHT -0.398799 R\*\*2 = 0.2280  
 LEFT WRIST WRT FOREARM = 0.002610 \*STANDING -0.868622 R\*\*2 = 0.0024  
 LEFT WRIST WRT FOREARM = -0.002719 \*WEIGHT +0.015910 \*STANDING -1.329823 R\*\*2 = 0.3019

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM Y COORDINATE

LEFT WRIST WRT FOREARM = 0.002050 \*WEIGHT +0.268465 R\*\*2 = 0.0911  
 LEFT WRIST WRT FOREARM = 0.006644 \*STANDING +0.135630 R\*\*2 = 0.0069  
 LEFT WRIST WRT FOREARM = 0.002195 \*WEIGHT -0.004092 \*STANDING +0.507902 R\*\*2 = 0.0932

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM Z COORDINATE

LEFT WRIST WRT FOREARM = 0.005970 \*WEIGHT +4.827643 R\*\*2 = 0.2493  
 LEFT WRIST WRT FOREARM = 0.088721 \*STANDING +0.036891 R\*\*2 = 0.3964  
 LEFT WRIST WRT FOREARM = 0.003438 \*WEIGHT +0.071904 \*STANDING +0.620039 R\*\*2 = 0.4648

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN X COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = -0.019772 \*WEIGHT +0.143418 R\*\*2 = 0.6802  
 ABDOMEN-PELVIS WRT ABDOMEN = -0.021236 \*STANDING -1.294467 R\*\*2 = 0.0056  
 ABDOMEN-PELVIS WRT ABDOMEN = -0.022984 \*WEIGHT +0.091198 \*STANDING -5.193227 R\*\*2 = 0.7664

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN Y COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = -0.002098 \*WEIGHT +0.328813 R\*\*2 = 0.0836  
ABDOMEN-PELVIS WRT ABDOMEN = 0.011969 \*STANDING -0.726543 R\*\*2 = 0.0196  
ABDOMEN-PELVIS WRT ABDOMEN = -0.003043 \*WEIGHT +0.026858 \*STANDING -1.242811 R\*\*2 = 0.1653

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN Z COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = -0.006352 \*WEIGHT +3.602727 R\*\*2 = 0.1045  
ABDOMEN-PELVIS WRT ABDOMEN = -0.026823 \*STANDING +4.410323 R\*\*2 = 0.0134  
ABDOMEN-PELVIS WRT ABDOMEN = -0.006533 \*WEIGHT +0.005138 \*STANDING +3.302052 R\*\*2 = 0.1049

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX X COORDINATE

THORAX-ABDOMEN WRT THORAX = -0.009861 \*WEIGHT +0.983155 R\*\*2 = 0.4431  
THORAX-ABDOMEN WRT THORAX = -0.003191 \*STANDING -0.203739 R\*\*2 = 0.0003  
THORAX-ABDOMEN WRT THORAX = -0.011778 \*WEIGHT +0.054425 \*STANDING -2.201607 R\*\*2 = 0.5236

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX Y COORDINATE

THORAX-ABDOMEN WRT THORAX = -0.001615 \*WEIGHT +0.263659 R\*\*2 = 0.1030  
THORAX-ABDOMEN WRT THORAX = -0.005550 \*STANDING +0.388480 R\*\*2 = 0.0088  
THORAX-ABDOMEN WRT THORAX = -0.001715 \*WEIGHT +0.002837 \*STANDING +0.097628 R\*\*2 = 0.1049

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX Z COORDINATE

THORAX-ABDOMEN WRT THORAX = -0.000672 \*WEIGHT +6.499148 R\*\*2 = 0.0018  
 THORAX-ABDOMEN WRT THORAX = 0.116738 \*STANDING -1.005807 R\*\*2 = 0.3878  
 THORAX-ABDOMEN WRT THORAX = -0.005777 \*WEIGHT +0.145001 \*STANDING -1.985855 R\*\*2 = 0.4971

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK X COORDINATE

NECK-THORAX WRT NECK = -0.007552 \*WEIGHT +1.201707 R\*\*2 = 0.3833  
 NECK-THORAX WRT NECK = 0.007321 \*STANDING -0.327148 R\*\*2 = 0.0026  
 NECK-THORAX WRT NECK = -0.009435 \*WEIGHT +0.053479 \*STANDING -1.927716 R\*\*2 = 0.4978

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK Y COORDINATE

NECK-THORAX WRT NECK = -0.000118 \*WEIGHT +0.087301 R\*\*2 = 0.0005  
 NECK-THORAX WRT NECK = 0.001304 \*STANDING -0.012118 R\*\*2 = 0.0004  
 NECK-THORAX WRT NECK = -0.000198 \*WEIGHT +0.002273 \*STANDING -0.045733 R\*\*2 = 0.0016

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK Z COORDINATE

NECK-THORAX WRT NECK = -0.001914 \*WEIGHT +1.874695 R\*\*2 = 0.0169  
 NECK-THORAX WRT NECK = 0.009939 \*STANDING +0.974095 R\*\*2 = 0.0033  
 NECK-THORAX WRT NECK = -0.002735 \*WEIGHT +0.023319 \*STANDING +0.510109 R\*\*2 = 0.0319

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD X COORDINATE

HEAD-NECK WRT HEAD = -0.001043 \*WEIGHT +0.447425 R\*\*2 = 0.0118  
 HEAD-NECK WRT HEAD = -0.012418 \*STANDING +1.088722 R\*\*2 = 0.0120  
 HEAD-NECK WRT HEAD = -0.000732 \*WEIGHT -0.008838 \*STANDING +(.964575 R\*\*2 = 0.0168

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD Y COORDINATE

HEAD-NECK WRT HEAD = 0.000004 \*WEIGHT -0.008092 R\*\*2 = 0.0000  
 HEAD-NECK WRT HEAD = -0.002926 \*STANDING +0.178242 R\*\*2 = 0.0050  
 HEAD-NECK WRT HEAD = 0.000130 \*WEIGHT -0.003560 \*STANDING +0.200243 R\*\*2 = 0.0062

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD Z COORDINATE

HEAD-NECK WRT HEAD = -0.000348 \*WEIGHT +2.562778 R\*\*2 = 0.0030  
 HEAD-NECK WRT HEAD = 0.012146 \*STANDING +1.742763 R\*\*2 = 0.0263  
 HEAD-NECK WRT HEAD = -0.000937 \*WEIGHT +0.016730 \*STANDING +1.583809 R\*\*2 = 0.0442

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH X COORDINATE

LEFT HIP WRT THIGH = 0.000567 \*WEIGHT +0.796702 R\*\*2 = 0.0015  
 LEFT HIP WRT THIGH = 0.013522 \*STANDING +0.021085 R\*\*2 = 0.0058  
 LEFT HIP WRT THIGH = 0.000134 \*WEIGHT +0.012865 \*STANDING +0.043868 R\*\*2 = 0.0059

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH Y COORDINATE

LEFT HIP WRT THIGH = 0.003034 \*WEIGHT +1.338086 R\*\*2 = 0.1030  
 LEFT HIP WRT THIGH = 0.033907 \*STANDING -0.386833 R\*\*2 = 0.0926  
 LEFT HIP WRT THIGH = 0.002223 \*WEIGHT +0.023035 \*STANDING -0.009823 R\*\*2 = 0.1384

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH Z COORDINATE

LEFT HIP WRT THIGH = -0.002696 \*WEIGHT -5.490560 R\*\*2 = 0.0266  
 LEFT HIP WRT THIGH = -0.143511 \*STANDING +3.239372 R\*\*2 = 0.5424  
 LEFT HIP WRT THIGH = 0.002848 \*WEIGHT -0.157442 \*STANDING +3.722436 R\*\*2 = 0.5670

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF X COORDINATE

LEFT KNEE WRT CALF = 0.000358 \*WEIGHT +0.555212 R\*\*2 = 0.0027  
 LEFT KNEE WRT CALF = -0.015328 \*STANDING +1.578664 R\*\*2 = 0.0359  
 LEFT KNEE WRT CALF = 0.001085 \*WEIGHT -0.020634 \*STANDING +1.762649 R\*\*2 = 0.0566

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF Y COORDINATE

LEFT KNEE WRT CALF = -0.001305 \*WEIGHT +0.739006 R\*\*2 = 0.0688  
 LEFT KNEE WRT CALF = -0.003399 \*STANDING +0.770943 R\*\*2 = 0.0034  
 LEFT KNEE WRT CALF = -0.001432 \*WEIGHT +0.003604 \*STANDING +0.528090 R\*\*2 = 0.0719

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF Z COORDINATE

LEFT KNEE WRT CALF = -0.001815 \*WEIGHT -5.912482 R\*\*2 = 0.0179  
 LEFT KNEE WRT CALF = -0.112359 \*STANDING +0.964099 R\*\*2 = 0.4941  
 LEFT KNEE WRT CALF = 0.002587 \*WEIGHT -0.125014 \*STANDING +1.402925 R\*\*2 = 0.5242

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT X COORDINATE

LEFT ANKLE WRT FOOT = 0.000096 \*WEIGHT -1.759546 R\*\*2 = 0.0003  
 LEFT ANKLE WRT FOOT = -0.011883 \*STANDING -0.991690 R\*\*2 = 0.0345  
 LEFT ANKLE WRT FOOT = 0.000621 \*WEIGHT -0.014923 \*STANDING -0.886272 R\*\*2 = 0.0453

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT Y COORDINATE

LEFT ANKLE WRT FOOT = -0.000619 \*WEIGHT +0.327165 R\*\*2 = 0.0276  
 LEFT ANKLE WRT FOOT = -0.001436 \*STANDING +0.331144 R\*\*2 = 0.0011  
 LEFT ANKLE WRT FOOT = -0.000686 \*WEIGHT +0.001922 \*STANDING +0.214693 R\*\*2 = 0.0292

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT Z COORDINATE

LEFT ANKLE WRT FOOT = -0.000618 \*WEIGHT -1.390017 R\*\*2 = 0.0272  
 LEFT ANKLE WRT FOOT = -0.026004 \*STANDING +0.173574 R\*\*2 = 0.3464  
 LEFT ANKLE WRT FOOT = 0.000359 \*WEIGHT -0.027762 \*STANDING +0.234536 R\*\*2 = 0.3540

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM X COORDINATE

LEFT SHOULDER WRT UPPER ARM = -0.000450 \*WEIGHT -0.943311 R\*\*2 = 0.0036  
 LEFT SHOULDER WRT UPPER ARM = -0.003679 \*STANDING -0.773132 R\*\*2 = 0.0017  
 LEFT SHOULDER WRT UPPER ARM = -0.000387 \*WEIGHT -0.001787 \*STANDING -0.838722 R\*\*2 = 0.0040

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM Y COORDINATE

LEFT SHOULDER WRT UPPER ARM = 0.000301 \*WEIGHT +0.307212 R\*\*2 = 0.0013  
 LEFT SHOULDER WRT UPPER ARM = -0.030760 \*STANDING +2.302225 R\*\*2 = 0.0967  
 LEFT SHOULDER WRT UPPER ARM = 0.001672 \*WEIGHT -0.038941 \*STANDING +2.585896 R\*\*2 = 0.1296

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM Z COORDINATE

LEFT SHOULDER WRT UPPER ARM = -0.010772 \*WEIGHT -3.607257 R\*\*2 = 0.4711  
 LEFT SHOULDER WRT UPPER ARM = -0.118178 \*STANDING +2.376788 R\*\*2 = 0.4082  
 LEFT SHOULDER WRT UPPER ARM = -0.007986 \*WEIGHT -0.079112 \*STANDING +1.022113 R\*\*2 = 0.6225

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM X COORDINATE

LEFT ELBOW WRT FOREARM = -0.003082 \*WEIGHT +0.571416 R\*\*2 = 0.1963  
 LEFT ELBOW WRT FOREARM = 0.010734 \*STANDING -0.544126 R\*\*2 = 0.0171  
 LEFT ELBOW WRT FOREARM = -0.004179 \*WEIGHT +0.031179 \*STANDING -1.253089 R\*\*2 = 0.3160



REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM Y COORDINATE

LEFT ELBOW WRT FOREARM = 0.002733 \*WEIGHT -0.439706 R\*\*2 = 0.2903  
 LEFT ELBOW WRT FOREARM = 0.011124 \*STANDING -0.760839 R\*\*2 = 0.0346  
 LEFT ELBOW WRT FOREARM = 0.002828 \*WEIGHT -0.002710 \*STANDING -0.281113 R\*\*2 = 0.2920

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM Z COORDINATE

LEFT ELBOW WRT FOREARM = -0.001266 \*WEIGHT -3.837578 R\*\*2 = 0.0301  
 LEFT ELBOW WRT FOREARM = -0.062200 \*STANDING -0.067568 R\*\*2 = 0.5233  
 LEFT ELBOW WRT FOREARM = 0.001117 \*WEIGHT -0.067663 \*STANDING +0.121867 R\*\*2 = 0.5427

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND X COORDINATE

LEFT WRIST WRT HAND = -0.001162 \*WEIGHT +0.177910 R\*\*2 = 0.0120  
 LEFT WRIST WRT HAND = -0.004494 \*STANDING +0.299369 R\*\*2 = 0.0013  
 LEFT WRIST WRT HAND = -0.001213 \*WEIGHT +0.001441 \*STANDING +0.093573 R\*\*2 = 0.0121

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND Y COORDINATE

LEFT WRIST WRT HAND = 0.000030 \*WEIGHT +0.556676 R\*\*2 = 0.0001  
 LEFT WRIST WRT HAND = 0.001113 \*STANDING +0.490214 R\*\*2 = 0.0007  
 LEFT WRIST WRT HAND = -0.000011 \*WEIGHT +0.001169 \*STANDING +0.488283 R\*\*2 = 0.0007

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND Z COORDINATE

LEFT WRIST WRT HAND = -0.000769 \*WEIGHT -1.983893 R\*\*2 = 0.0228  
 LEFT WRIST WRT HAND = -0.027999 \*STANDING -0.314857 R\*\*2 = 0.2176  
 LEFT WRIST WRT HAND = 0.000263 \*WEIGHT -0.029283 \*STANDING -0.270318 R\*\*2 = 0.2198

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND X COORDINATE

LEFT ELBOW WRT FOREARM + HAND = -0.003248 \*WEIGHT +0.846465 R\*\*2 = 0.2196  
 LEFT ELBOW WRT FOREARM + HAND = 0.000803 \*STANDING +0.337849 R\*\*2 = 0.0001  
 LEFT ELBOW WRT FOREARM + HAND = -0.003958 \*WEIGHT +0.020166 \*STANDING -0.333610 R\*\*2 = 0.2701

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND Y COORDINATE

LEFT ELBOW WRT FOREARM + HAND = 0.002549 \*WEIGHT -0.665277 R\*\*2 = 0.1429  
 LEFT ELBOW WRT FOREARM + HAND = 0.014558 \*STANDING -1.230285 R\*\*2 = 0.0336  
 LEFT ELBOW WRT FOREARM + HAND = 0.002460 \*WEIGHT +0.002525 \*STANDING -0.813010 R\*\*2 = 0.1437

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND Z COORDINATE

LEFT ELBOW WRT FOREARM + HAND = 0.001749 \*WEIGHT -6.363632 R\*\*2 = 0.0238  
 LEFT ELBOW WRT FOREARM + HAND = -0.079112 \*STANDING -1.095296 R\*\*2 = 0.3509  
 LEFT ELBOW WRT FOREARM + HAND = 0.005479 \*WEIGHT -0.105913 \*STANDING -0.165942 R\*\*2 = 0.5444

REGRESSION EQUATIONS FOR ADULT MALE JOINT CENTER LOCATIONS

PREDICTING VARIABLES  
 WEIGHT RANGE: 118.00 264.00 MEAN: 173.60 S.D.: 21.440  
 STANDING HEIGHT RANGE: 62.17 77.64 MEAN: 69.82 S.D.: 2.437

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS X COORDINATE

ABDOMEN-PELVIS WRT PELVIS = -0.007468 \*WEIGHT +0.336494 R\*\*2 = 0.2171  
 ABDOMEN-PELVIS WRT PELVIS = -0.055467 \*STANDING +2.940071 R\*\*2 = 0.2056  
 ABDOMEN-PELVIS WRT PELVIS = -0.004973 \*WEIGHT -0.020925 \*STANDING +1.373596 R\*\*2 = 0.2221

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REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS Y COORDINATE

ABDOMEN-PELVIS WRT PELVIS = 0.001240 \*WEIGHT -0.190457 R\*\*2 = 0.0645  
 ABDOMEN-PELVIS WRT PELVIS = 0.014645 \*STANDING -1.002466 R\*\*2 = 0.1544  
 ABDOMEN-PELVIS WRT PELVIS = -0.002943 \*WEIGHT +0.035087 \*STANDING -1.929495 R\*\*2 = 0.2168

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT PELVIS Z COORDINATE

ABDOMEN-PELVIS WRT PELVIS = -0.005949 \*WEIGHT -1.587701 R\*\*2 = 0.1774  
 ABDOMEN-PELVIS WRT PELVIS = -0.046001 \*STANDING +0.613143 R\*\*2 = 0.1821  
 ABDOMEN-PELVIS WRT PELVIS = -0.002704 \*WEIGHT -0.027220 \*STANDING -0.238589 R\*\*2 = 0.1884

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN X COORDINATE

THORAX-ABDOMEN WRT ABDOMEN = -0.008732 \*WEIGHT -0.225546 R\*\*2 = 0.4097  
 THORAX-ABDOMEN WRT ABDOMEN = -0.054611 \*STANDING +2.102789 R\*\*2 = 0.2750  
 THORAX-ABDOMEN WRT ABDOMEN = -0.012925 \*WEIGHT +0.035172 \*STANDING -1.968791 R\*\*2 = 0.4293

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN Y COORDINATE

THORAX-ABDOMEN WRT ABDOMEN = 0.000424 \*WEIGHT +0.045566 R\*\*2 = 0.0030  
 THORAX-ABDOMEN WRT ABDOMEN = 0.005690 \*STANDING -0.279903 R\*\*2 = 0.0092  
 THORAX-ABDOMEN WRT ABDOMEN = -0.001483 \*WEIGHT +0.015994 \*STANDING -0.747169 R\*\*2 = 0.0154

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT ABDOMEN Z COORDINATE

THORAX-ABDOMEN WRT ABDOMEN = -0.001523 \*WEIGHT -0.617623 R\*\*2 = 0.0669  
 THORAX-ABDOMEN WRT ABDOMEN = -0.012164 \*STANDING -0.027172 R\*\*2 = 0.0732  
 THORAX-ABDOMEN WRT ABDOMEN = -0.000425 \*WEIGHT -0.009209 \*STANDING -0.161189 R\*\*2 = 0.0741

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX X COORDINATE

NECK-THORAX WRT THORAX = -0.004370 \*WEIGHT +0.506433 R\*\*2 = 0.1844  
 NECK-THORAX WRT THORAX = -0.021594 \*STANDING +1.270817 R\*\*2 = 0.0773  
 NECK-THORAX WRT THORAX = -0.010448 \*WEIGHT +0.050980 \*STANDING -2.020320 R\*\*2 = 0.2584

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX Y COORDINATE

NECK-THORAX WRT THORAX = 0.000351 \*WEIGHT -0.081110 R\*\*2 = 0.0047  
 NECK-THORAX WRT THORAX = 0.006307 \*STANDING -0.461996 R\*\*2 = 0.0262  
 NECK-THORAX WRT THORAX = -0.002332 \*WEIGHT +0.022507 \*STANDING -1.196661 R\*\*2 = 0.0621

REGRESSION EQUATIONS FOR NECK-THORAX WRT THORAX Z COORDINATE

NECK-THORAX WRT THORAX = -0.018898 \*WEIGHT -4.412312 R\*\*2 = 0.6222  
 NECK-THORAX WRT THORAX = -0.145204 \*STANDING +2.514372 R\*\*2 = 0.6305  
 NECK-THORAX WRT THORAX = -0.009230 \*WEIGHT -0.081093 \*STANDING -0.393043 R\*\*2 = 0.6560

REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK X COORDINATE

HEAD-NECK WRT NECK = -0.002543 \*WEIGHT +0.025044 R\*\*2 = 0.0286  
 HEAD-NECK WRT NECK = -0.030706 \*STANDING +1.737397 R\*\*2 = 0.0716  
 HEAD-NECK WRT NECK = 0.006505 \*WEIGHT -0.075888 \*STANDING +3.786370 R\*\*2 = 0.1038

REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK Y COORDINATE

HEAD-NECK WRT NECK = 0.001546 \*WEIGHT -0.173776 R\*\*2 = 0.0554  
 HEAD-NECK WRT NECK = 0.004449 \*STANDING -0.221235 R\*\*2 = 0.0079  
 HEAD-NECK WRT NECK = 0.005912 \*WEIGHT -0.036615 \*STANDING +1.640983 R\*\*2 = 0.1470

REGRESSION EQUATIONS FOR HEAD-NECK WRT NECK Z COORDINATE

HEAD-NECK WRT NECK = -0.005257 \*WEIGHT -1.917117 R\*\*2 = 0.3484  
 HEAD-NECK WRT NECK = -0.037224 \*STANDING -0.211768 R\*\*2 = 0.2998  
 HEAD-NECK WRT NECK = -0.004769 \*WEIGHT -0.004100 \*STANDING -1.713902 R\*\*2 = 0.3490

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS X COORDINATE

LEFT HIP WRT PELVIS = 0.003450 \*WEIGHT -1.409181 R\*\*2 = 0.0566  
 LEFT HIP WRT PELVIS = 0.027144 \*STANDING -2.718103 R\*\*2 = 0.0602  
 LEFT HIP WRT PELVIS = 0.001244 \*WEIGHT +0.018500 \*STANDING -2.326116 R\*\*2 = 0.0614

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS Y COORDINATE

LEFT HIP WRT PELVIS = -0.003493 \*WEIGHT -1.525887 R\*\*2 = 0.0315  
 LEFT HIP WRT PELVIS = -0.021645 \*STANDING -0.608464 R\*\*2 = 0.1251  
 LEFT HIP WRT PELVIS = -0.005308 \*WEIGHT +0.015223 \*STANDING -2.280386 R\*\*2 = 0.2004

REGRESSION EQUATIONS FOR LEFT HIP WRT PELVIS Z COORDINATE

LEFT HIP WRT PELVIS = 0.007201 \*WEIGHT +0.213696 R\*\*2 = 0.2082  
 LEFT HIP WRT PELVIS = 0.046697 \*STANDING -1.822410 R\*\*2 = 0.1503  
 LEFT HIP WRT PELVIS = 0.009509 \*WEIGHT -0.019355 \*STANDING +1.173000 R\*\*2 = 0.2126

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH X COORDINATE

LEFT KNEE WRT THIGH = 0.001399 \*WEIGHT -0.473292 R\*\*2 = 0.0210  
 LEFT KNEE WRT THIGH = 0.011302 \*STANDING -1.024659 R\*\*2 = 0.0235  
 LEFT KNEE WRT THIGH = 0.000301 \*WEIGHT +0.009211 \*STANDING -C.929842 R\*\*2 = 0.0237

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH Y COORDINATE

LEFT KNEE WRT THIGH = -0.002624 \*WEIGHT +0.076015 R\*\*2 = 0.3286  
 LEFT KNEE WRT THIGH = -0.017356 \*STANDING +0.841626 R\*\*2 = 0.2466  
 LEFT KNEE WRT THIGH = -0.003231 \*WEIGHT +0.005090 \*STANDING -0.176244 R\*\*2 = 0.3322

REGRESSION EQUATIONS FOR LEFT KNEE WRT THIGH Z COORDINATE

LEFT KNEE WRT THIGH = 0.019553 \*WEIGHT +6.437359 R\*\*2 = 0.6807  
 LEFT KNEE WRT THIGH = 0.168181 \*STANDING -1.983336 R\*\*2 = 0.8644  
 LEFT KNEE WRT THIGH = -0.002902 \*WEIGHT +0.188340 \*STANDING -2.897506 R\*\*2 = 0.8670

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF X COORDINATE

LEFT ANKLE WRT CALF = 0.001353 \*WEIGHT +0.160367 R\*\*2 = 0.0265  
 LEFT ANKLE WRT CALF = 0.011264 \*STANDING -0.396212 R\*\*2 = 0.0315  
 LEFT ANKLE WRT CALF = 0.000059 \*WEIGHT +0.010855 \*STANDING -0.377643 R\*\*2 = 0.0315

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF Y COORDINATE

LEFT ANKLE WRT CALF = 0.001027 \*WEIGHT +0.579538 R\*\*2 = 0.0833  
 LEFT ANKLE WRT CALF = 0.007310 \*STANDING +0.243695 R\*\*2 = 0.0724  
 LEFT ANKLE WRT CALF = 0.000904 \*WEIGHT +0.001030 \*STANDING +0.528482 R\*\*2 = 0.0835

REGRESSION EQUATIONS FOR LEFT ANKLE WRT CALF Z COORDINATE

LEFT ANKLE WRT CALF = 0.022061 \*WEIGHT +5.987117 R\*\*2 = 0.6751  
 LEFT ANKLE WRT CALF = 0.190912 \*STANDING -3.594633 R\*\*2 = 0.8678  
 LEFT ANKLE WRT CALF = -0.004078 \*WEIGHT +0.219241 \*STANDING -4.879344 R\*\*2 = 0.8718

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX X COORDINATE

LEFT SHOULDER WRT THORAX = -0.003569 \*WEIGHT -0.330012 R\*\*2 = 0.0306  
 LEFT SHOULDER WRT THORAX = -0.021080 \*STANDING +0.534831 R\*\*2 = 0.0183  
 LEFT SHOULDER WRT THORAX = -0.006147 \*WEIGHT +0.021617 \*STANDING -1.401451 R\*\*2 = 0.0339

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX Y COORDINATE

LEFT SHOULDER WRT THORAX = -0.010585 \*WEIGHT -4.756775 R\*\*2 = 0.4825  
 LEFT SHOULDER WRT THORAX = -0.081562 \*STANDING -0.860951 R\*\*2 = 0.4917  
 LEFT SHOULDER WRT THORAX = -0.005011 \*WEIGHT -0.046756 \*STANDING -2.439382 R\*\*2 = 0.5103



REGRESSION EQUATIONS FOR LEFT SHOULDER WRT THORAX Z COORDINATE

LEFT SHOULDER WRT THORAX = -0.019759 \*WEIGHT -0.941024 R\*\*2 = 0.7469  
 LEFT SHOULDER WRT THORAX = -0.145784 \*STANDING +5.879542 R\*\*2 = 0.6979  
 LEFT SHOULDER WRT THORAX = -0.013836 \*WEIGHT -0.049677 \*STANDING +1.521159 R\*\*2 = 0.7608

REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM X COORDINATE

LEFT ELBOW WRT UPPER ARM = 0.000236 \*WEIGHT -0.687652 R\*\*2 = 0.0041  
 LEFT ELBOW WRT UPPER ARM = -0.000164 \*STANDING -0.636033 R\*\*2 = 0.0000  
 LEFT ELBOW WRT UPPER ARM = 0.001486 \*WEIGHT -0.010484 \*STANDING -0.168033 R\*\*2 = 0.0281

REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM Y COORDINATE

LEFT ELBOW WRT UPPER ARM = 0.002549 \*WEIGHT -0.032913 R\*\*2 = 0.3721  
 LEFT ELBOW WRT UPPER ARM = 0.015905 \*STANDING -0.709936 R\*\*2 = 0.2486  
 LEFT ELBOW WRT UPPER ARM = 0.003801 \*WEIGHT -0.010496 \*STANDING +0.487316 R\*\*2 = 0.3907

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REGRESSION EQUATIONS FOR LEFT ELBOW WRT UPPER ARM Z COORDINATE

LEFT ELBOW WRT UPPER ARM = 0.010936 \*WEIGHT +3.729019 R\*\*2 = 0.6643  
 LEFT ELBOW WRT UPPER ARM = 0.087840 \*STANDING -0.545825 R\*\*2 = 0.7356  
 LEFT ELBOW WRT UPPER ARM = 0.002694 \*WEIGHT +0.069127 \*STANDING +0.302829 R\*\*2 = 0.7426

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM X COORDINATE

LEFT WRIST WRT FOREARM = -0.000335 \*WEIGHT +0.421124 R\*\*2 = 0.0017  
 LEFT WRIST WRT FOREARM = -0.002143 \*STANDING +0.513798 R\*\*2 = 0.0012  
 LEFT WRIST WRT FOREARM = -0.000462 \*WEIGHT +0.001068 \*STANDING +0.368203 R\*\*2 = 0.0018

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM Y COORDINATE

LEFT WRIST WRT FOREARM = -0.001105 \*WEIGHT +0.209175 R\*\*2 = 0.0900  
 LEFT WRIST WRT FOREARM = -0.005287 \*STANDING +0.390359 R\*\*2 = 0.0354  
 LEFT WRIST WRT FOREARM = -0.002761 \*WEIGHT +0.013894 \*STANDING -0.479452 R\*\*2 = 0.1320

REGRESSION EQUATIONS FOR LEFT WRIST WRT FOREARM Z COORDINATE

LEFT WRIST WRT FOREARM = 0.012050 \*WEIGHT +4.379713 R\*\*2 = 0.6704  
 LEFT WRIST WRT FOREARM = 0.104273 \*STANDING -0.853654 R\*\*2 = 0.8617  
 LEFT WRIST WRT FOREARM = -0.002226 \*WEIGHT +0.119738 \*STANDING -1.554957 R\*\*2 = 0.8656

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN X COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = -0.009768 \*WEIGHT -0.707969 R\*\*2 = 0.4324  
 ABDOMEN-PELVIS WRT ABDOMEN = -0.073331 \*STANDING +2.751955 R\*\*2 = 0.4183  
 ABDOMEN-PELVIS WRT ABDOMEN = -0.005966 \*WEIGHT -0.031889 \*STANDING +0.872569 R\*\*2 = 0.4460

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN Y COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = 0.002777 \*WEIGHT -0.319296 R\*\*2 = 0.1224  
 ABDOMEN-PELVIS WRT ABDOMEN = 0.025420 \*STANDING -1.622431 R\*\*2 = 0.1760  
 ABDOMEN-PELVIS WRT ABDOMEN = -0.001476 \*WEIGHT +0.035671 \*STANDING -.087294 R\*\*2 = 0.1820

REGRESSION EQUATIONS FOR ABDOMEN-PELVIS WRT ABDOMEN Z COORDINATE

ABDOMEN-PELVIS WRT ABDOMEN = 0.002103 \*WEIGHT +1.966064 R\*\*2 = 0.0130  
 ABDOMEN-PELVIS WRT ABDOMEN = 0.001903 \*STANDING +2.191356 R\*\*2 = 0.0002  
 ABDOMEN-PELVIS WRT ABDOMEN = 0.010917 \*WEIGHT -0.073932 \*STANDING +5.630429 R\*\*2 = 0.0604

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX X COORDINATE

THORAX-ABDOMEN WRT THORAX = -0.004447 \*WEIGHT +0.471228 R\*\*2 = 0.1976  
 THORAX-ABDOMEN WRT THORAX = -0.021669 \*STANDING +1.227710 R\*\*2 = 0.0805  
 THORAX-ABDOMEN WRT THORAX = -0.010845 \*WEIGHT +0.053662 \*STANDING -2.188490 R\*\*2 = 0.2825

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX Y COORDINATE

THORAX-ABDOMEN WRT THORAX = 0.000258 \*WEIGHT -0.052755 R\*\*2 = 0.0026  
 THORAX-ABDOMEN WRT THORAX = 0.004892 \*STANDING -0.350661 R\*\*2 = 0.0162  
 THORAX-ABDOMEN WRT THORAX = -0.001894 \*WEIGHT +0.018048 \*STANDING -0.947308 R\*\*2 = 0.0405

REGRESSION EQUATIONS FOR THORAX-ABDOMEN WRT THORAX Z COORDINATE  
 THORAX-ABDOMEN WRT THORAX = 0.011163 \*WEIGHT +5.473922 R\*\*2 = 0.4827  
 THORAX-ABDOMEN WRT THORAX = 0.093852 \*STANDING +0.817770 R\*\*2 = 0.5855  
 THORAX-ABDOMEN WRT THORAX = -0.000152 \*WEIGHT +0.094911 \*STANDING +0.769741 R\*\*2 = 0.5856

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK X COORDINATE  
 NECK-THORAX WRT NECK = -0.005924 \*WEIGHT +0.970814 R\*\*2 = 0.3759  
 NECK-THORAX WRT NECK = -0.032818 \*STANDING +2.254789 R\*\*2 = 0.1980  
 NECK-THORAX WRT NECK = -0.011702 \*WEIGHT +0.048470 \*STANDING -1.431534 R\*\*2 = 0.4501

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK Y COORDINATE  
 NECK-THORAX WRT NECK = -0.000261 \*WEIGHT -0.090962 R\*\*2 = 0.0013  
 NECK-THORAX WRT NECK = 0.011608 \*STANDING -0.946521 R\*\*2 = 0.0435  
 NECK-THORAX WRT NECK = -0.009571 \*WEIGHT +0.078094 \*STANDING -3.961594 R\*\*2 = 0.3394

REGRESSION EQUATIONS FOR NECK-THORAX WRT NECK Z COORDINATE  
 NECK-THORAX WRT NECK = 0.000381 \*WEIGHT +1.742971 R\*\*2 = 0.0013  
 NECK-THORAX WRT NECK = 0.001530 \*STANDING +1.701043 R\*\*2 = 0.0004  
 NECK-THORAX WRT NECK = 0.001158 \*WEIGHT -0.006514 \*STANDING +2.065822 R\*\*2 = 0.0024

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD X COORDINATE

HEAD-NECK WRT HEAD = -0.000144 \*WEIGHT +0.308559 R\*\*2 = 0.0004  
 HEAD-NECK WRT HEAD = 0.001555 \*STANDING +0.175426 R\*\*2 = 0.0008  
 HEAD-NECK WRT HEAD = -0.001915 \*WEIGHT +0.014854 \*STANDING -0.427684 R\*\*2 = 0.0125

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD Y COORDINATE

HEAD-NECK WRT HEAD = 0.000205 \*WEIGHT -0.021428 R\*\*2 = 0.0035  
 HEAD-NECK WRT HEAD = 0.000182 \*STANDING +0.000749 R\*\*2 = 0.0000  
 HEAD-NECK WRT HEAD = 0.001066 \*WEIGHT -0.007220 \*STANDING +0.336399 R\*\*2 = 0.0165

REGRESSION EQUATIONS FOR HEAD-NECK WRT HEAD Z COORDINATE

HEAD-NECK WRT HEAD = -0.001653 \*WEIGHT +2.690120 R\*\*2 = 0.0647  
 HEAD-NECK WRT HEAD = -0.007078 \*STANDING +2.903101 R\*\*2 = 0.0204  
 HEAD-NECK WRT HEAD = -0.004709 \*WEIGHT +0.025629 \*STANDING +1.419823 R\*\*2 = 0.1106

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH X COORDINATE

LEFT HIP WRT THIGH = 0.008018 \*WEIGHT -1.745973 R\*\*2 = 0.2395  
 LEFT HIP WRT THIGH = 0.041092 \*STANDING -3.251331 R\*\*2 = 0.1080  
 LEFT HIP WRT THIGH = 0.018149 \*WEIGHT -0.084976 \*STANDING +2.465770 R\*\*2 = 0.3188

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH Y COORDINATE

LEFT HIP WRT THIGH = 0.005854 \*WEIGHT +0.946000 R\*\*2 = 0.4474  
 LEFT HIP WRT THIGH = 0.040538 \*STANDING -0.889305 R\*\*2 = 0.3682  
 LEFT HIP WRT THIGH = 0.005940 \*WEIGHT -0.000721 \*STANDING +0.981737 R\*\*2 = 0.4474

REGRESSION EQUATIONS FOR LEFT HIP WRT THIGH Z COORDINATE

LEFT HIP WRT THIGH = -0.012406 \*WEIGHT -5.428231 R\*\*2 = 0.4001  
 LEFT HIP WRT THIGH = -0.116746 \*STANDING +0.616039 R\*\*2 = 0.6082  
 LEFT HIP WRT THIGH = 0.008809 \*WEIGHT -0.177933 \*STANDING +3.390843 R\*\*2 = 0.6429

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF X COORDINATE

LEFT KNEE WRT CALF = 0.002519 \*WEIGHT +0.214312 R\*\*2 = 0.0980  
 LEFT KNEE WRT CALF = 0.011798 \*STANDING -0.180944 R\*\*2 = 0.0369  
 LEFT KNEE WRT CALF = 0.006473 \*WEIGHT -0.033166 \*STANDING +1.858137 R\*\*2 = 0.1482

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF Y COORDINATE

LEFT KNEE WRT CALF = 0.001446 \*WEIGHT +0.313320 R\*\*2 = 0.1105  
 LEFT KNEE WRT CALF = 0.005467 \*STANDING +0.177735 R\*\*2 = 0.0271  
 LEFT KNEE WRT CALF = 0.004624 \*WEIGHT -0.026653 \*STANDING +1.634335 R\*\*2 = 0.2211

REGRESSION EQUATIONS FOR LEFT KNEE WRT CALF Z COORDINATE

LEFT KNEE WRT CALF = -0.010462 \*WEIGHT -5.139949 R\*\*2 = 0.4213  
 LEFT KNEE WRT CALF = -0.105511 \*STANDING +0.450460 R\*\*2 = 0.7355  
 LEFT KNEE WRT CALF = 0.012325 \*WEIGHT -0.191127 \*STANDING +0.333065 R\*\*2 = 0.8360

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT X COORDINATE

LEFT ANKLE WRT FOOT = -0.003922 \*WEIGHT -2.088906 R\*\*2 = 0.2652  
 LEFT ANKLE WRT FOOT = -0.029067 \*STANDING -0.725991 R\*\*2 = 0.2500  
 LEFT ANKLE WRT FOOT = -0.002656 \*WEIGHT -0.010619 \*STANDING -1.562600 R\*\*2 = 0.2709

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT Y COORDINATE

LEFT ANKLE WRT FOOT = 0.001036 \*WEIGHT +0.140367 R\*\*2 = 0.0565  
 LEFT ANKLE WRT FOOT = 0.003455 \*STANDING +0.075380 R\*\*2 = 0.0108  
 LEFT ANKLE WRT FOOT = 0.003630 \*WEIGHT -0.021757 \*STANDING +1.218738 R\*\*2 = 0.1301

REGRESSION EQUATIONS FOR LEFT ANKLE WRT FOOT Z COORDINATE

LEFT ANKLE WRT FOOT = -0.002927 \*WEIGHT -0.870575 R\*\*2 = 0.2768  
 LEFT ANKLE WRT FOOT = -0.022221 \*STANDING +0.183444 R\*\*2 = 0.2737  
 LEFT ANKLE WRT FOOT = -0.001618 \*WEIGHT -0.010984 \*STANDING -0.326148 R\*\*2 = 0.2883

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM X COORDINATE

LEFT SHOULDER WRT UPPER ARM = 0.000830 \*WEIGHT +0.370250 R\*\*2 = 0.0100  
LEFT SHOULDER WRT UPPER ARM = 0.004095 \*STANDING +0.225499 R\*\*2 = 0.0042  
LEFT SHOULDER WRT UPPER ARM = 0.001988 \*WEIGHT -0.009715 \*STANDING +0.851770 R\*\*2 = 0.0141

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM Y COORDINATE

LEFT SHOULDER WRT UPPER ARM = -0.001289 \*WEIGHT +0.438159 R\*\*2 = 0.0216  
LEFT SHOULDER WRT UPPER ARM = -0.011100 \*STANDING +0.994151 R\*\*2 = 0.0275  
LEFT SHOULDER WRT UPPER ARM = 0.000199 \*WEIGHT -0.012485 \*STANDING +1.056967 R\*\*2 = 0.0276

REGRESSION EQUATIONS FOR LEFT SHOULDER WRT UPPER ARM Z COORDINATE

LEFT SHOULDER WRT UPPER ARM = -0.017979 \*WEIGHT -2.702344 R\*\*2 = 0.8340  
LEFT SHOULDER WRT UPPER ARM = -0.133190 \*STANDING +3.541350 R\*\*2 = 0.7856  
LEFT SHOULDER WRT UPPER ARM = -0.012218 \*WEIGHT -0.048317 \*STANDING -0.307549 R\*\*2 = 0.8518

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REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM X COORDINATE

LEFT ELBOW WRT FOREARM = -0.001087 \*WEIGHT -0.343308 R\*\*2 = 0.0606  
LEFT ELBOW WRT FOREARM = -0.009549 \*STANDING +0.138748 R\*\*2 = 0.0803  
LEFT ELBOW WRT FOREARM = 0.000299 \*WEIGHT -0.011628 \*STANDING +0.233035 R\*\*2 = 0.0811



REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM Y COORDINATE

LEFT ELBOW WRT FOREARM = 0.000202 \*WEIGHT -0.262384 R\*\*2 = 0.0013  
 LEFT ELBOW WRT FOREARM = 0.000980 \*STANDING -0.296420 R\*\*2 = 0.0005  
 LEFT ELBOW WRT FOREARM = 0.000497 \*WEIGHT -0.002470 \*STANDING -0.139945 R\*\*2 = 0.0019

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM Z COORDINATE

LEFT ELBOW WRT FOREARM = -0.008121 \*WEIGHT -3.248134 R\*\*2 = 0.6328  
 LEFT ELBOW WRT FOREARM = -0.068772 \*STANDING +0.173893 R\*\*2 = 0.7790  
 LEFT ELBOW WRT FOREARM = 0.000458 \*WEIGHT -0.071954 \*STANDING +0.318213 R\*\*2 = 0.7793

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND X COORDINATE

LEFT WRIST WRT HAND = -0.001576 \*WEIGHT +0.381869 R\*\*2 = 0.0315  
 LEFT WRIST WRT HAND = -0.015469 \*STANDING +1.194259 R\*\*2 = 0.0520  
 LEFT WRIST WRT HAND = 0.001561 \*WEIGHT --0.026309 \*STANDING +1.685847 R\*\*2 = 0.0573

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND Y COORDINATE

LEFT WRIST WRT HAND = -0.000876 \*WEIGHT -0.409282 R\*\*2 = 0.0359  
 LEFT WRIST WRT HAND = -0.009216 \*STANDING +0.085499 R\*\*2 = 0.0682  
 LEFT WRIST WRT HAND = 0.001297 \*WEIGHT -0.018228 \*STANDING +0.494186 R\*\*2 = 0.0817

REGRESSION EQUATIONS FOR LEFT WRIST WRT HAND Z COORDINATE

LEFT WRIST WRT HAND = -0.003239 \*WEIGHT -2.065060 R\*\*2 = 0.4129  
 LEFT WRIST WRT HAND = -0.026859 \*STANDING -0.740092 R\*\*2 = 0.4873  
 LEFT WRIST WRT HAND = -0.000215 \*WEIGHT -0.025368 \*STANDING -0.807723 R\*\*2 = 0.4876

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND X COORDINATE

LEFT ELBOW WRT FOREARM + HAND = -0.001534 \*WEIGHT -0.248755 R\*\*2 = 0.0500  
 LEFT ELBOW WRT FOREARM + HAND = -0.013239 \*STANDING +0.415082 R\*\*2 = 0.0640  
 LEFT ELBOW WRT FOREARM + HAND = 0.000261 \*WEIGHT -0.015052 \*STANDING +0.497303 R\*\*2 = 0.0642

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND Y COORDINATE

LEFT ELBOW WRT FOREARM + HAND = 0.000104 \*WEIGHT -0.323101 R\*\*2 = 0.0003  
 LEFT ELBOW WRT FOREARM + HAND = 0.000634 \*STANDING -0.349634 R\*\*2 = 0.0002  
 LEFT ELBOW WRT FOREARM + HAND = 0.000167 \*WEIGHT -0.000523 \*STANDING -0.297182 R\*\*2 = 0.0003

REGRESSION EQUATIONS FOR LEFT ELBOW WRT FOREARM + HAND Z COORDINATE

LEFT ELBOW WRT FOREARM + HAND = -0.009904 \*WEIGHT -5.421995 R\*\*2 = 0.4954  
 LEFT ELBOW WRT FOREARM + HAND = -0.091470 \*STANDING -0.717790 R\*\*2 = 0.7253  
 LEFT ELBOW WRT FOREARM + HAND = 0.005827 \*WEIGHT -0.131946 \*STANDING +1.117759 R\*\*2 = 0.7548

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APPENDIX C  
PRINCIPAL MOMENTS OF INERTIA REGRESSION EQUATIONS

This appendix contains a complete listing of the X, Y, and Z principal moments of inertia regression equations developed for the adult human female and the adult human male options. The regression equations are based on human stereophotometric data (McConville, et al., 1980; Young, et al., 1983). The predicting variables are weight (lb) and standing height (in). The predicted principal moments of inertia are in slugs-inches squared. At the top of each set of regression equations are listed the range of values, mean, and standard deviation of the predicting variables within that subject type option. For the principal moments of each segment, a separate regression equation is given against each of the predicting variables. The last regression equation is a multiple regression equation based on both predicting variables. With each regression equation, the coefficient of determination ( $R^2$ ) is given. The regression equations are based on 46 female subjects and 31 male subjects.

REGRESSION EQUATIONS FOR THE ADULT FEMALE PRINCIPAL MOMENTS OF INERTIA

PREDICTING VARIABLES

WEIGHT                    RANGE: 85.00            200.00            MEAN: 127.30            S.D.: 16.590  
 STANDING HEIGHT        RANGE: 56.93            72.05            MEAN: 63.82            S.D.: 2.364

REGRESSION EQUATIONS FOR PELVIS X MOMENT

PELVIS X MOMENT        = 0.163756 \*WEIGHT    -13.500050            R\*\*2 = 0.8909  
 PELVIS X MOMENT        = 0.559154 \*STANDING -25.921050            R\*\*2 = 0.0748  
 PELVIS X MOMENT        = 0.174048 \*WEIGHT    -0.292277 \*STANDING +3.603102            R\*\*2 = 0.9078

REGRESSION EQUATIONS FOR PELVIS Y MOMENT

PELVIS Y MOMENT        = 0.161932 \*WEIGHT    -15.090490            R\*\*2 = 0.8391  
 PELVIS Y MOMENT        = 0.347382 \*STANDING -14.325520            R\*\*2 = 0.0278  
 PELVIS Y MOMENT        = 0.180853 \*WEIGHT    -0.537341 \*STANDING +16.353070            R\*\*2 = 0.8942

REGRESSION EQUATIONS FOR PELVIS Z MOMENT

PELVIS Z MOMENT        = 0.256230 \*WEIGHT    -22.912750            R\*\*2 = 0.8749  
 PELVIS Z MOMENT        = 0.647401 \*STANDING -27.906070            R\*\*2 = 0.0402  
 PELVIS Z MOMENT        = 0.282011 \*WEIGHT    -0.732180 \*STANDING +19.932170            R\*\*2 = 0.9175

REGRESSION EQUATIONS FOR ABDOMEN X MOMENT

ABDOMEN X MOMENT = 0.031055 \*WEIGHT -2.473941 R\*\*2 = 0.2987  
 ABDOMEN X MOMENT = -0.101966 \*STANDING +8.374269 R\*\*2 = 0.0232  
 ABDOMEN X MOMENT = 0.041855 \*WEIGHT -0.306717 \*STANDING +15.474200 R\*\*2 = 0.4722

REGRESSION EQUATIONS FOR ABDOMEN Y MOMENT

ABDOMEN Y MOMENT = 0.025354 \*WEIGHT -2.300540 R\*\*2 = 0.2752  
 ABDOMEN Y MOMENT = -0.120106 \*STANDING +8.895873 R\*\*2 = 0.0445  
 ABDOMEN Y MOMENT = 0.035739 \*WEIGHT -0.294939 \*STANDING +14.958350 R\*\*2 = 0.4971

REGRESSION EQUATIONS FOR ABDOMEN Z MOMENT

ABDOMEN Z MOMENT = 0.054539 \*WEIGHT -4.781197 R\*\*2 = 0.3359  
 ABDOMEN Z MOMENT = -0.168868 \*STANDING +13.622860 R\*\*2 = 0.0232  
 ABDOMEN Z MOMENT = 0.073073 \*WEIGHT -0.526336 \*STANDING +26.018390 R\*\*2 = 0.5223

REGRESSION EQUATIONS FOR THORAX X MOMENT

THORAX X MOMENT = 0.301112 \*WEIGHT -12.786380 R\*\*2 = 0.7948  
 THORAX X MOMENT = 1.634667 \*STANDING -74.125640 R\*\*2 = 0.1686  
 THORAX X MOMENT = 0.294236 \*WEIGHT + 0.195281 \*STANDING -24.213590 R\*\*2 = 0.7968

REGRESSION EQUATIONS FOR THORAX Y MOMENT

THORAX Y MOMENT = 0.239654 \*WEIGHT -11.027040 R\*\*2 = 0.7959  
 THORAX Y MOMENT = 1.409968 \*STANDING -66.762300 R\*\*2 = 0.1983  
 THORAX Y MOMENT = 0.229547 \*WEIGHT +0.287040 \*STANDING -27.823750 R\*\*2 = 0.8027

REGRESSION EQUATIONS FOR THORAX Z MOMENT

THORAX Z MOMENT = 0.241791 \*WEIGHT -14.322190 R\*\*2 = 0.8408  
 THORAX Z MOMENT = 0.882539 \*STANDING -36.276030 R\*\*2 = 0.0806  
 THORAX Z MOMENT = 0.254565 \*WEIGHT -0.362777 \*STANDING +6.906433 R\*\*2 = 0.8521

REGRESSION EQUATIONS FOR NECK X MOMENT

NECK X MOMENT = 0.000609 \*WEIGHT +0.024464 R\*\*2 = 0.2657  
 NECK X MOMENT = 0.007888 \*STANDING -0.390459 R\*\*2 = 0.3209  
 NECK X MOMENT = 0.000400 \*WEIGHT +0.005931 \*STANDING -0.322579 R\*\*2 = 0.4158

REGRESSION EQUATIONS FOR NECK Y MOMENT

NECK Y MOMENT = 0.000637 \*WEIGHT +0.049083 R\*\*2 = 0.2170  
 NECK Y MOMENT = 0.008916 \*STANDING -0.427217 R\*\*2 = 0.3065  
 NECK Y MOMENT = 0.000390 \*WEIGHT +0.007010 \*STANDING -0.361095 R\*\*2 = 0.3738

REGRESSION EQUATIONS FOR NECK Z MOMENT

NECK Z MOMENT = 0.001055 \*WEIGHT +0.004830 R\*\*2 = 0.4597  
 NECK Z MOMENT = 0.007630 \*STANDING -0.330893 R\*\*2 = 0.1732  
 NECK Z MOMENT = 0.000950 \*WEIGHT +0.002985 \*STANDING -0.169815 R\*\*2 = 0.4816

REGRESSION EQUATIONS FOR HEAD X MOMENT

HEAD X MOMENT = 0.003316 \*WEIGHT +1.350839 R\*\*2 = 0.1717  
 HEAD X MOMENT = 0.014106 \*STANDING +0.922638 R\*\*2 = 0.0224  
 HEAD X MOMENT = 0.003406 \*WEIGHT -0.002556 \*STANDING +1.500424 R\*\*2 = 0.1723

REGRESSION EQUATIONS FOR HEAD Y MOMENT

HEAD Y MOMENT = 0.003768 \*WEIGHT +1.486574 R\*\*2 = 0.1671  
 HEAD Y MOMENT = 0.017871 \*STANDING +0.883056 R\*\*2 = 0.0271  
 HEAD Y MOMENT = 0.003792 \*WEIGHT -0.000679 \*STANDING +1.526312 R\*\*2 = 0.1671

REGRESSION EQUATIONS FOR HEAD Z MOMENT

HEAD Z MOMENT = 0.002513 \*WEIGHT +1.021677 R\*\*2 = 0.2127  
 HEAD Z MOMENT = 0.010754 \*STANDING +0.693090 R\*\*2 = 0.0280  
 HEAD Z MOMENT = 0.002578 \*WEIGHT -0.001858 \*STANDING +1.130428 R\*\*2 = 0.2134



REGRESSION EQUATIONS FOR THIGH X MOMENT

THIGH X MOMENT = 0.010001 \*WEIGHT +0.181037 R\*\*2 = 0.6511  
 THIGH X MOMENT = 0.086858 \*STANDING -3.923329 R\*\*2 = 0.3535  
 THIGH X MOMENT = 0.008388 \*WEIGHT +0.045824 \*STANDING -2.500468 R\*\*2 = 0.7326

REGRESSION EQUATIONS FOR THIGH Y MOMENT

THIGH Y MOMENT = 0.009711 \*WEIGHT +0.192135 R\*\*2 = 0.6421  
 THIGH Y MOMENT = 0.085729 \*STANDING -3.881509 R\*\*2 = 0.3602  
 THIGH Y MOMENT = 0.008085 \*WEIGHT +0.046176 \*STANDING -2.509969 R\*\*2 = 0.7286

REGRESSION EQUATIONS FOR THIGH Z MOMENT

THIGH Z MOMENT = 0.001081 \*WEIGHT -0.049435 R\*\*2 = 0.7459  
 THIGH Z MOMENT = 0.004096 \*STANDING -0.157097 R\*\*2 = 0.0771  
 THIGH Z MOMENT = 0.001132 \*WEIGHT -0.001441 \*STANDING +0.034888 R\*\*2 = 0.7538

REGRESSION EQUATIONS FOR CALF X MOMENT

CALF X MOMENT = 0.028391 \*WEIGHT -0.062710 R\*\*2 = 0.5802  
 CALF X MOMENT = 0.239876 \*STANDING -11.289330 R\*\*2 = 0.2981  
 CALF X MOMENT = 0.024095 \*WEIGHT +0.122004 \*STANDING -7.202003 R\*\*2 = 0.6440

REGRESSION EQUATIONS FOR CALF Y MOMENT

CALF Y MOMENT = 0.028043 \*WEIGHT -0.030029 R\*\*2 = 0.5785  
 CALF Y MOMENT = 0.240618 \*STANDING -11.352770 R\*\*2 = 0.3066  
 CALF Y MOMENT = 0.023643 \*WEIGHT +0.124957 \*STANDING -7.342105 R\*\*2 = 0.6469

REGRESSION EQUATIONS FOR CALF Z MOMENT

CALF Z MOMENT = 0.006683 \*WEIGHT -0.412023 R\*\*2 = 0.7348  
 CALF Z MOMENT = 0.030000 \*STANDING -1.374711 R\*\*2 = 0.1066  
 CALF Z MOMENT = 0.006798 \*WEIGHT -0.003254 \*STANDING -0.221596 R\*\*2 = 0.7358

REGRESSION EQUATIONS FOR FOOT Z MOMENT

FOOT Z MOMENT = 0.000298 \*WEIGHT +0.013433 R\*\*2 = 0.3877  
 FOOT Z MOMENT = 0.003700 \*STANDING -0.179437 R\*\*2 = 0.4296  
 FOOT Z MOMENT = 0.000203 \*WEIGHT +0.002708 \*STANDING -0.145019 R\*\*2 = 0.5782

REGRESSION EQUATIONS FOR FOOT Y MOMENT

FOOT Y MOMENT = 0.001336 \*WEIGHT +0.055107 R\*\*2 = 0.4350  
 FOOT Y MOMENT = 0.018162 \*STANDING -0.909509 R\*\*2 = 0.5785  
 FOOT Y MOMENT = 0.000842 \*WEIGHT +0.014045 \*STANDING -0.766749 R\*\*2 = 0.7214

REGRESSION EQUATIONS FOR FOOT X MOMENT

FOOT X MOMENT = 0.001379 \*WEIGHT +0.059885 R\*\*2 = 0.4444  
 FOOT X MOMENT = 0.018299 \*STANDING -0.907403 R\*\*2 = 0.5633  
 FOOT X MOMENT = 0.000887 \*WEIGHT +0.013958 \*STANDING -0.756870 R\*\*2 = 0.7157

REGRESSION EQUATIONS FOR UPPER ARM X MOMENT

UPPER ARM X MOMENT = 0.008832 \*WEIGHT -0.318302 R\*\*2 = 0.7883  
 UPPER ARM X MOMENT = 0.071212 \*STANDING -3.594248 R\*\*2 = 0.3689  
 UPPER ARM X MOMENT = 0.007641 \*WEIGHT +0.033833 \*STANDING -2.298105 R\*\*2 = 0.8572

REGRESSION EQUATIONS FOR UPPER ARM Y MOMENT

UPPER ARM Y MOMENT = 0.010102 \*WEIGHT -0.444038 R\*\*2 = 0.8268  
 UPPER ARM Y MOMENT = 0.072898 \*STANDING -3.648074 R\*\*2 = 0.3099  
 UPPER ARM Y MOMENT = 0.009104 \*WEIGHT +0.028364 \*STANDING -2.103820 R\*\*2 = 0.8656

REGRESSION EQUATIONS FOR UPPER ARM Z MOMENT

UPPER ARM Z MOMENT = 0.003440 \*WEIGHT -0.280054 R\*\*2 = 0.8998  
 UPPER ARM Z MOMENT = 0.013084 \*STANDING -0.625907 R\*\*2 = 0.0937  
 UPPER ARM Z MOMENT = 0.003599 \*WEIGHT -0.004524 \*STANDING -0.015321 R\*\*2 = 0.9090

REGRESSION EQUATIONS FOR FOREARM X MOMENT

FOREARM X MOMENT = 0.003558 \*WEIGHT -0.061760 R\*\*2 = 0.6509  
 FOREARM X MOMENT = 0.026886 \*STANDING -1.267104 R\*\*2 = 0.2675  
 FOREARM X MOMENT = 0.003155 \*WEIGHT +0.011453 \*STANDING -0.731933 R\*\*2 = 0.6911

REGRESSION EQUATIONS FOR FOREARM Y MOMENT

FOREARM Y MOMENT = 0.003352 \*WEIGHT -0.051225 R\*\*2 = 0.6341  
 FOREARM Y MOMENT = 0.026467 \*STANDING -1.259055 R\*\*2 = 0.2846  
 FOREARM Y MOMENT = 0.002923 \*WEIGHT +0.012167 \*STANDING -0.763188 R\*\*2 = 0.6839

REGRESSION EQUATIONS FOR FOREARM Z MOMENT

FOREARM Z MOMENT = 0.000969 \*WEIGHT -0.057900 R\*\*2 = 0.7556  
 FOREARM Z MOMENT = 0.003471 \*STANDING -0.141681 R\*\*2 = 0.0698  
 FOREARM Z MOMENT = 0.001023 \*WEIGHT -0.001535 \*STANDING +0.031913 R\*\*2 = 0.7669

REGRESSION EQUATIONS FOR HAND X MOMENT

HAND X MOMENT = 0.000389 \*WEIGHT +0.025665 R\*\*2 = 0.3857  
 HAND X MOMENT = 0.003603 \*STANDING -0.148178 R\*\*2 = 0.2377  
 HAND X MOMENT = 0.000317 \*WEIGHT +0.002052 \*STANDING -0.094394 R\*\*2 = 0.4495

REGRESSION EQUATIONS FOR HAND Y MOMENT

HAND Y MOMENT = 0.000320 \*WEIGHT +0.022715 R\*\*2 = 0.3766  
 HAND Y MOMENT = 0.003186 \*STANDING -0.134415 R\*\*2 = 0.2684  
 HAND Y MOMENT = 0.000251 \*WEIGHT +0.001957 \*STANDING -0.091781 R\*\*2 = 0.4604

REGRESSION EQUATIONS FOR HAND Z MOMENT

HAND Z MOMENT = 0.000112 \*WEIGHT +0.005927 R\*\*2 = 0.3822  
 HAND Z MOMENT = 0.000718 \*STANDING -0.023783 R\*\*2 = 0.1120  
 HAND Z MOMENT = 0.000105 \*WEIGHT +0.000202 \*STANDING -0.005915 R\*\*2 = 0.3896

REGRESSION EQUATIONS FOR FOREARM PLUS HAND X MOMENT

FOREARM + HAND X MOMENT= 0.010001 \*WEIGHT +0.181037 R\*\*2 = 0.6511  
 FOREARM + HAND X MOMENT= 0.086858 \*STANDING -3.923329 R\*\*2 = 0.3535  
 FOREARM + HAND X MOMENT= 0.008388 \*WEIGHT +0.045824 \*STANDING -2.500468 R\*\*2 = 0.7326

REGRESSION EQUATIONS FOR FOREARM PLUS HAND Y MOMENT

FOREARM + HAND Y MOMENT= 0.009711 \*WEIGHT +0.192135 R\*\*2 = 0.6421  
 FOREARM + HAND Y MOMENT= 0.085729 \*STANDING -3.881509 R\*\*2 = 0.3602  
 FOREARM + HAND Y MOMENT= 0.008085 \*WEIGHT +0.046176 \*STANDING -2.509969 R\*\*2 = 0.7286

REGRESSION EQUATIONS FOR FOREARM PLUS HAND Z MOMENT

FOREARM + HAND Z MOMENT= 0.001081 \*WEIGHT -0.049435

FOREARM + HAND Z MOMENT= 0.004096 \*STANDING -0.157097

FOREARM + HAND Z MOMENT= 0.001132 \*WEIGHT -0.001441 \*STANDING +0.034888

R\*\*2 = 0.7459

R\*\*2 = 0.0771

R\*\*2 = 0.7538

REGRESSION EQUATIONS FOR ADULT MALE PRINCIPAL MOMENTS OF INERTIA

PREDICTING VARIABLES

WEIGHT RANGE: 118.00 264.00 MEAN: 173.60 S.D.: 21.440  
 STANDING HEIGHT RANGE: 62.17 77.64 MEAN: 69.82 S.D.: 2.437

REGRESSION EQUATIONS FOR PELVIS X MOMENT

PELVIS X MOMENT = 0.117920 \*WEIGHT -9.541327 R\*\*2 = 0.8049  
 PELVIS X MOMENT = 0.771563 \*STANDING -43.364990 R\*\*2 = 0.5914  
 PELVIS X MOMENT = 0.150906 \*WEIGHT -0.276669 \*STANDING +4.171488 R\*\*2 = 0.8179

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REGRESSION EQUATIONS FOR PELVIS Y MOMENT

PELVIS Y MOMENT = 0.111156 \*WEIGHT -9.275152 R\*\*2 = 0.7515  
 PELVIS Y MOMENT = 0.721944 \*STANDING -40.783950 R\*\*2 = 0.5441  
 PELVIS Y MOMENT = 0.145972 \*WEIGHT -0.292018 \*STANDING +5.198404 R\*\*2 = 0.7668

REGRESSION EQUATIONS FOR PELVIS Z MOMENT

PELVIS Z MOMENT = 0.138637 \*WEIGHT -11.424750 R\*\*2 = 0.7516  
 PELVIS Z MOMENT = 0.895104 \*STANDING -50.351390 R\*\*2 = 0.5378  
 PELVIS Z MOMENT = 0.185753 \*WEIGHT -0.395182 \*STANDING +8.162018 R\*\*2 = 0.7696

REGRESSION EQUATIONS FOR ABDOMEN X MOMENT

ABDOMEN X MOMENT = 0.016729 \*WEIGHT' -1.190717 R\*\*2 = 0.4715  
 ABDOMEN X MOMENT = 0.106385 \*STANLING -5.774367 R\*\*2 = 0.3273  
 ABDOMEN X MOMENT = 0.023542 \*WEIGHT -0.057141 \*STANDING +1.641403 R\*\*2 = 0.4877

REGRESSION EQUATIONS FOR ABDOMEN Y MOMENT

ABDOMEN Y MOMENT = 0.009820 \*WEIGHT -0.755341 R\*\*2 = 0.4073  
 ABDOMEN Y MOMENT = 0.059706 \*STANDING -3.254342 R\*\*2 = 0.2585  
 ABDOMEN Y MOMENT = 0.015721 \*WEIGHT -0.049498 \*STANDING +1.697984 R\*\*2 = 0.4378

REGRESSION EQUATIONS FOR ABDOMEN Z MOMENT

ABDOMEN Z MOMENT = 0.026073 \*WEIGHT -1.943402 R\*\*2 = 0.4752  
 ABDOMEN Z MOMENT = 0.163224 \*STANDING -8.906807 R\*\*2 = 0.3197  
 ABDOMEN Z MOMENT = 0.038481 \*WEIGHT -0.104076 \*STANDING +3.214991 R\*\*2 = 0.4976

REGRESSION EQUATIONS FOR THORAX X MOMENT

THORAX X MOMENT = 0.530761 \*WEIGHT -39.709080 R\*\*2 = 0.9315  
 THORAX X MOMENT = 3.724962 \*STANDING -209.56920 R\*\*2 = 0.7875  
 THORAX X MOMENT = 0.504281 \*WEIGHT +0.222097 \*STANDING -50.717090 R\*\*2 = 0.9320



REGRESSION EQUATIONS FOR THORAX Y MOMENT

|                 |   |          |           |            |               |
|-----------------|---|----------|-----------|------------|---------------|
| THORAX Y MOMENT | = | 0.401215 | *WEIGHT   | -31.048660 | R**2 = 0.9176 |
| THORAX Y MOMENT | = | 2.804530 | *STANDING | -158.66330 | R**2 = 0.7696 |
| THORAX Y MOMENT | = | 0.389010 | *WEIGHT   | +0.102369  | R**2 = 0.9178 |
|                 |   |          | *STANDING | -36.122420 |               |

REGRESSION EQUATIONS FOR THORAX Z MOMENT

|                 |   |          |           |            |               |
|-----------------|---|----------|-----------|------------|---------------|
| THORAX Z MOMENT | = | 0.339041 | *WEIGHT   | -26.329640 | R**2 = 0.9561 |
| THORAX Z MOMENT | = | 2.289070 | *STANDING | -128.51820 | R**2 = 0.7480 |
| THORAX Z MOMENT | = | 0.384835 | *WEIGHT   | -0.384092  | R**2 = 0.9597 |
|                 |   |          | *STANDING | -7.292557  |               |

REGRESSION EQUATIONS FOR NECK X MOMENT

|               |   |          |           |           |               |
|---------------|---|----------|-----------|-----------|---------------|
| NECK X MOMENT | = | 0.001387 | *WEIGHT   | -0.057555 | R**2 = 0.5120 |
| NECK X MOMENT | = | 0.008977 | *STANDING | -0.448591 | R**2 = 0.3683 |
| NECK X MOMENT | = | 0.001842 | *WEIGHT   | -0.003815 | R**2 = 0.5234 |
|               |   |          | *STANDING | +0.131522 |               |

REGRESSION EQUATIONS FOR NECK Y MOMENT

|               |   |          |           |           |               |
|---------------|---|----------|-----------|-----------|---------------|
| NECK Y MOMENT | = | 0.001538 | *WEIGHT   | -0.046986 | R**2 = 0.5249 |
| NECK Y MOMENT | = | 0.009658 | *STANDING | -0.459772 | R**2 = 0.3551 |
| NECK Y MOMENT | = | 0.002251 | *WEIGHT   | -0.005980 | R**2 = 0.5483 |
|               |   |          | *STANDING | +0.249402 |               |

REGRESSION EQUATIONS FOR NECK Z MOMENT

NECK Z MOMENT = 0.002032 \*WEIGHT -0.080039 R\*\*2 = 0.5675  
 NECK Z MOMENT = 0.012447 \*STANDING -0.603564 R\*\*2 = 0.3654  
 NECK Z MOMENT = 0.003190 \*WEIGHT -0.009710 \*STANDING +0.401225 R\*\*2 = 0.6057

REGRESSION EQUATIONS FOR HEAD X MOMENT

HEAD X MOMENT = 0.003680 \*WEIGHT +1.541396 R\*\*2 = 0.1550  
 HEAD X MOMENT = 0.029540 \*STANDING +0.104170 R\*\*2 = 0.1715  
 HEAD X MOMENT = 0.000918 \*WEIGHT +0.023162 \*STANDING +0.393387 R\*\*2 = 0.1732

REGRESSION EQUATIONS FOR HEAD Y MOMENT

HEAD Y MOMENT = 0.004619 \*WEIGHT +1.686967 R\*\*2 = 0.1563  
 HEAD Y MOMENT = 0.037161 \*STANDING -0.122760 R\*\*2 = 0.1737  
 HEAD Y MOMENT = 0.001097 \*WEIGHT +0.029538 \*STANDING +0.222949 R\*\*2 = 0.1752

REGRESSION EQUATIONS FOR HEAD Z MOMENT

HEAD Z MOMENT = 0.002481 \*WEIGHT +1.179516 R\*\*2 = 0.1883  
 HEAD Z MOMENT = 0.018242 \*STANDING +0.327581 R\*\*2 = 0.1747  
 HEAD Z MOMENT = 0.001784 \*WEIGHT +0.005853 \*STANDING +0.889437 R\*\*2 = 0.1914

REGRESSION EQUATIONS FOR THIGH X MOMENT

THIGH X MOMENT = 0.025793 \*WEIGHT -1.226292 R\*\*2 = 0.7960  
 THIGH X MOMENT = 0.198665 \*STANDING -10.713900 R\*\*2 = 0.8106  
 THIGH X MOMENT = 0.012263 \*WEIGHT +0.113484 \*STANDING -6.850978 R\*\*2 = 0.8415

REGRESSION EQUATIONS FOR THIGH Y MOMENT

THIGH Y MOMENT = 0.025638 \*WEIGHT -1.215490 R\*\*2 = 0.7976  
 THIGH Y MOMENT = 0.197470 \*STANDING -10.645990 R\*\*2 = 0.8122  
 THIGH Y MOMENT = 0.012191 \*WEIGHT +0.112791 \*STANDING -6.805867 R\*\*2 = 0.8431

REGRESSION EQUATIONS FOR THIGH Z MOMENT

THIGH Z MOMENT = 0.001576 \*WEIGHT -0.089792 R\*\*2 = 0.7937  
 THIGH Z MOMENT = 0.010433 \*STANDING -0.550339 R\*\*2 = 0.5971  
 THIGH Z MOMENT = 0.001932 \*WEIGHT -0.002988 \*STANDING +0.058323 R\*\*2 = 0.8022

REGRESSION EQUATIONS FOR CALF X MOMENT

CALF X MOMENT = 0.059151 \*WEIGHT -3.966057 R\*\*2 = 0.8120  
 CALF X MOMENT = 0.472882 \*STANDING -26.931780 R\*\*2 = 0.8908  
 CALF X MOMENT = 0.016127 \*WEIGHT +0.360857 \*STANDING -21.851520 R\*\*2 = 0.9011

REGRESSION EQUATIONS FOR CALF Y MOMENT

CALF Y MOMENT = 0.059948 \*WEIGHT -4.009954 R\*\*2 = 0.8125  
 CALF Y MOMENT = 0.478795 \*STANDING -27.253020 R\*\*2 = 0.8896  
 CALF Y MOMENT = 0.016664 \*WEIGHT +0.363043 \*STANDING -22.003800 R\*\*2 = 0.9004

REGRESSION EQUATIONS FOR CALF Z MOMENT

CALF Z MOMENT = 0.006279 \*WEIGHT -0.366041 R\*\*2 = 0.8423  
 CALF Z MOMENT = 0.045091 \*STANDING -2.447107 R\*\*2 = 0.7456  
 CALF Z MOMENT = 0.005253 \*WEIGHT +0.008599 \*STANDING -0.792265 R\*\*2 = 0.8470

REGRESSION EQUATIONS FOR FOOT Z MOMENT

FOOT Z MOMENT = 0.000680 \*WEIGHT -0.031023 R\*\*2 = 0.7643  
 FOOT Z MOMENT = 0.005213 \*STANDING -0.279382 R\*\*2 = 0.7704  
 FOOT Z MOMENT = 0.000342 \*WEIGHT +0.002840 \*STANDING -0.171776 R\*\*2 = 0.8036

REGRESSION EQUATIONS FOR FOOT Y MOMENT

FOOT Y MOMENT = 0.003810 \*WEIGHT -0.199205 R\*\*2 = 0.6925  
 FOOT Y MOMENT = 0.030630 \*STANDING -1.690426 R\*\*2 = 0.7683  
 FOOT Y MOMENT = 0.000920 \*WEIGHT +0.024242 \*STANDING -1.400724 R\*\*2 = 0.7752

REGRESSION EQUATIONS FOR FOOT X MOMENT

FOOT X MOMENT = 0.003966 \*WEIGHT -0.201562 R\*\*2 = 0.7064  
 FOOT X MOMENT = 0.031694 \*STANDING -1.740607 R\*\*2 = 0.7744  
 FOOT X MOMENT = 0.001088 \*WEIGHT +0.024139 \*STANDING -1.397969 R\*\*2 = 0.7836

REGRESSION EQUATIONS FOR UPPER ARM X MOMENT

UPPER ARM X MOMENT = 0.014407 \*WEIGHT -1.124170 R\*\*2 = 0.8534  
 UPPER ARM X MOMENT = 0.102891 \*STANDING -5.859214 R\*\*2 = 0.7471  
 UPPER ARM X MOMENT = 0.012455 \*WEIGHT +0.016378 \*STANDING -1.935950 R\*\*2 = 0.8567

REGRESSION EQUATIONS FOR UPPER ARM Y MOMENT

UPPER ARM Y MOMENT = 0.015635 \*WEIGHT -1.253754 R\*\*2 = 0.8512  
 UPPER ARM Y MOMENT = 0.110026 \*STANDING -6.278232 R\*\*2 = 0.7235  
 UPPER ARM Y MOMENT = 0.014648 \*WEIGHT +0.008278 \*STANDING -1.664030 R\*\*2 = 0.8519

REGRESSION EQUATIONS FOR UPPER ARM Z MOMENT

UPPER ARM Z MOMENT = 0.003008 \*WEIGHT -0.243573 R\*\*2 = 0.7795  
 UPPER ARM Z MOMENT = 0.019116 \*STANDING -1.066814 R\*\*2 = 0.5403  
 UPPER ARM Z MOMENT = 0.004244 \*WEIGHT -0.010361 \*STANDING +0.269960 R\*\*2 = 0.8068

REGRESSION EQUATIONS FOR FOREARM X MOMENT

FOREARM X MOMENT = 0.008108 \*WEIGHT -0.490309 R\*\*2 = 0.8397  
 FOREARM X MOMENT = 0.060581 \*STANDING -3.342158 R\*\*2 = 0.8047  
 FOREARM X MOMENT = 0.005150 \*WEIGHT +0.024805 \*STANDING -1.719764 R\*\*2 = 0.8629

REGRESSION EQUATIONS FOR FOREARM Y MOMENT

FOREARM Y MOMENT = 0.008330 \*WEIGHT -0.507917 R\*\*2 = 0.8418  
 FOREARM Y MOMENT = 0.061938 \*STANDING -3.416692 R\*\*2 = 0.7986  
 FOREARM Y MOMENT = 0.005504 \*WEIGHT +0.023708 \*STANDING -1.682993 R\*\*2 = 0.8619

REGRESSION EQUATIONS FOR FOREARM Z MOMENT

FOREARM Z MOMENT = 0.001237 \*WEIGHT -0.080312 R\*\*2 = 0.7807  
 FOREARM Z MOMENT = 0.008022 \*STANDING -0.430113 R\*\*2 = 0.5636  
 FOREARM Z MOMENT = 0.001633 \*WEIGHT -0.003318 \*STANDING +0.084157 R\*\*2 = 0.7972

REGRESSION EQUATIONS FOR HAND X MOMENT

HAND X MOMENT = 0.000903 \*WEIGHT -0.017110 R\*\*2 = 0.6547  
 HAND X MOMENT = 0.006996 \*STANDING -0.352180 R\*\*2 = 0.6751  
 HAND X MOMENT = 0.000399 \*WEIGHT +0.004227 \*STANDING -0.226637 R\*\*2 = 0.6970

REGRESSION EQUATIONS FOR HAND Y MOMENT

HAND Y MOMENT = 0.000736 \*WEIGHT -0.013369 R\*\*2 = 0.6358  
 HAND Y MOMENT = 0.005787 \*STANDING -0.292308 R\*\*2 = 0.6741  
 HAND Y MOMENT = 0.000270 \*WEIGHT +0.003913 \*STANDING -0.207325 R\*\*2 = 0.6888

REGRESSION EQUATIONS FOR HAND Z MOMENT

HAND Z MOMENT = 0.000290 \*WEIGHT -0.006137 R\*\*2 = 0.7508  
 HAND Z MOMENT = 0.002093 \*STANDING -0.102979 R\*\*2 = 0.6714  
 HAND Z MOMENT = 0.000235 \*WEIGHT +0.000459 \*STANDING -0.028883 R\*\*2 = 0.7564

REGRESSION EQUATIONS FOR FOREARM PLUS HAND X MOMENT

FOREARM + HAND X MOMENT = 0.025793 \*WEIGHT -1.226292 R\*\*2 = 0.7960  
 FOREARM + HAND X MOMENT = 0.198665 \*STANDING -10.713900 R\*\*2 = 0.8106  
 FOREARM + HAND X MOMENT = 0.012263 \*WEIGHT +0.113484 \*STANDING -6.850978 R\*\*2 = 0.8415

REGRESSION EQUATIONS FOR FOREARM PLUS HAND Y MOMENT

FOREARM + HAND Y MOMENT = 0.025638 \*WEIGHT -1.215490 R\*\*2 = 0.7976  
 FOREARM + HAND Y MOMENT = 0.197470 \*STANDING -10.645990 R\*\*2 = 0.8122  
 FOREARM + HAND Y MOMENT = 0.012191 \*WEIGHT +0.112791 \*STANDING -6.805867 R\*\*2 = 0.8431

REGRESSION EQUATIONS FOR FOREARM PLUS HAND Z MOMENT

FOREARM + HAND Z MOMENT= 0.001576 \*WEIGHT -0.089792  
FOREARM + HAND Z MOMENT= 0.010433 \*STANDING -0.550339  
FOREARM + HAND Z MOMENT= 0.001932 \*WEIGHT -0.002988 \*STANDING +0.058323

R\*\*2 = 0.7937  
R\*\*2 = 0.5971  
R\*\*2 = 0.8022



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APPENDIX D  
VOLUME REGRESSION EQUATIONS

This appendix contains a complete listing of the segment volume regression equations developed for the adult human female and the adult human male options. The regression equations are based on human stereophotometric volume data (McConville, et al., 1980; Young, et al., 1983). The predicting variables are weight (lb) and standing height (in). The predicted segment volumes are in cubic inches. At the top of each set of regression equations are listed the range of values, mean, and standard deviation of the predicting variables within that subject type option. For the volume of each segment, a separate regression equation is given against each of the predicting variables. The last regression equation is a multiple regression equation based on both predicting variables. With each regression equation, the coefficient of determination ( $R^2$ ) is given. The regression equations are based on 46 female subjects and 31 male subjects.

REGRESSION EQUATIONS FOR ADULT FEMALE SEGMENT VOLUME

PREDICTING VARIABLES  
 WEIGHT                    RANGE: 85.00            200.00            MEAN: 127.30            S.D.: 16.590  
 STANDING HEIGHT        RANGE: 56.93            72.05            MEAN: 63.82            S.D.: 2.364

REGRESSION EQUATIONS FOR PELVIS VOLUME

PELVIS VOLUME            = 6.726632 \*WEIGHT    -329.739300            R\*\*2 = 0.8796  
 PELVIS VOLUME            = 20.382420 \*STANDING -675.801500            R\*\*2 = 0.0581  
 PELVIS VOLUME            = 7.259390 \*WEIGHT    -15.130090 \*STANDING +555.627400            R\*\*2 = 0.9061

REGRESSION EQUATIONS FOR ABDOMEN VOLUME

ABDOMEN VOLUME           = 1.381251 \*WEIGHT    -22.733250            R\*\*2 = 0.1825  
 ABDOMEN VOLUME           = -7.833098 \*STANDING +669.115500            R\*\*2 = 0.0423  
 ABDOMEN VOLUME           = 2.001907 \*WEIGHT    -17.626310 \*STANDING+1008.704000            R\*\*2 = 0.3596

REGRESSION EQUATIONS FOR THORAX VOLUME

THORAX VOLUME            = 7.337825 \*WEIGHT    +75.115720            R\*\*2 = 0.8692  
 THORAX VOLUME            = 35.735550 \*STANDING -1159.42000            R\*\*2 = 0.1484  
 THORAX VOLUME            = 7.344659 \*WEIGHT    -0.194087 \*STANDING +86.472870            R\*\*2 = 0.8692

REGRESSION EQUATIONS FOR NECK VOLUME

NECK VOLUME = 0.128394 \*WEIGHT +26.857100 R\*\*2 = 0.2260  
 NECK VOLUME = 1.911736 \*STANDING -76.406010 R\*\*2 = 0.3607  
 NECK VOLUME = 0.073788 \*WEIGHT +1.550769 \*STANDING -63.889100 R\*\*2 = 0.4224

REGRESSION EQUATIONS FOR HEAD VOLUME

HEAD VOLUME = 0.264502 \*WEIGHT +200.341900 R\*\*2 = 0.2018  
 HEAD VOLUME = 1.134469 \*STANDING +165.596000 R\*\*2 = 0.0267  
 HEAD VOLUME = 0.271286 \*WEIGHT -0.192644 \*STANDING +211.614900 R\*\*2 = 0.2025

REGRESSION EQUATIONS FOR THIGH VOLUME

THIGH VOLUME = 4.303679 \*WEIGHT +7.249268 R\*\*2 = 0.8300  
 THIGH VOLUME = 28.505460 \*STANDING -1195.84300 R\*\*2 = 0.2621  
 THIGH VOLUME = 3.986669 \*WEIGHT +9.002912 \*STANDING -519.573000 R\*\*2 = 0.8517

REGRESSION EQUATIONS FOR CALF VOLUME

CALF VOLUME = 1.181796 \*WEIGHT +24.553420 R\*\*2 = 0.7279  
 CALF VOLUME = 7.057509 \*STANDING -256.930700 R\*\*2 = 0.1868  
 CALF VOLUME = 1.127505 \*WEIGHT +1.541819 \*STANDING -65.669080 R\*\*2 = 0.7352

REGRESSION EQUATIONS FOR FOOT VOLUME

FOOT VOLUME = 0.140151 \*WEIGHT +21.595400 R\*\*2 = 0.4114  
 FOOT VOLUME = 1.821366 \*STANDING -74.274540 R\*\*2 = 0.5001  
 FOOT VOLUME = 0.091837 \*WEIGHT +1.372106 \*STANDING -58.695980 R\*\*2 = 0.6463

REGRESSION EQUATIONS FOR UPPER ARM VOLUME

UPPER ARM VOLUME = 0.771218 \*WEIGHT -13.685230 R\*\*2 = 0.9243  
 UPPER ARM VOLUME = 3.988159 \*STANDING -158.182600 R\*\*2 = 0.1779  
 UPPER ARM VOLUME = 0.762054 \*WEIGHT +0.260234 \*STANDING -28.913310 R\*\*2 = 0.9250

REGRESSION EQUATIONS FOR FOREARM VOLUME

FOREARM VOLUME = 0.368884 \*WEIGHT +4.717636 R\*\*2 = 0.7614  
 FOREARM VOLUME = 1.873929 \*STANDING -62.260620 R\*\*2 = 0.1414  
 FOREARM VOLUME = 0.365933 \*WEIGHT +0.083808 \*STANDING -0.186533 R\*\*2 = 0.7616

REGRESSION EQUATIONS FOR HAND VOLUME

HAND VOLUME = 0.064923 \*WEIGHT +11.545190 R\*\*2 = 0.4192  
 HAND VOLUME = 0.496572 \*STANDING -10.828770 R\*\*2 = 0.1765  
 HAND VOLUME = 0.057309 \*WEIGHT +0.216218 \*STANDING -1.107230 R\*\*2 = 0.4468

REGRESSION EQUATIONS FOR FOREARM PLUS HAND VOLUME

FOREARM + HAND VOLUME = 0.433808 \*WEIGHT +16.262700

FOREARM + HAND VOLUME = 2.370267 \*STANDING -73.074510

FOREARM + HAND VOLUME = 0.423253 \*WEIGHT +0.299737 \*STANDING -1.277008

R\*\*2 = 0.7521

R\*\*2 = 0.1616

R\*\*2 = 0.7543

REGRESSION EQUATIONS FOR ADULT MALE SEGMENT VOLUME

PREDICTING VARIABLES

WEIGHT RANGE: 118.00 264.00 MEAN: 173.60 S.D.: 21.440  
 STANDING HEIGHT RANGE: 62.17 77.64 MEAN: 69.82 S.D.: 2.437

REGRESSION EQUATIONS FOR PELVIS VOLUME

PELVIS VOLUME = 4.765337 \*WEIGHT -116.890400 R\*\*2 = 0.7760  
 PELVIS VOLUME = 31.264240 \*STANDING -1489.63800 R\*\*2 = 0.5733  
 PELVIS VOLUME = 6.039989 \*WEIGHT -10.691090 \*STANDING +413.002000 R\*\*2 = 0.7875

REGRESSION EQUATIONS FOR ABDOMEN VOLUME

ABDOMEN VOLUME = 0.759174 \*WEIGHT +13.403290 R\*\*2 = 0.2698  
 ABDOMEN VOLUME = 4.660814 \*STANDING -182.934400 R\*\*2 = 0.1745  
 ABDOMEN VOLUME = 1.184239 \*WEIGHT -3.565218 \*STANDING +190.109500 R\*\*2 = 0.2873

REGRESSION EQUATIONS FOR THORAX VOLUME

THORAX VOLUME = 9.568200 \*WEIGHT -142.278600 R\*\*2 = 0.9522  
 THORAX VOLUME = 65.865370 \*STANDING -3114.55300 R\*\*2 = 0.7745  
 THORAX VOLUME = 9.983014 \*WEIGHT -3.479255 \*STANDING +30.167790 R\*\*2 = 0.9526

REGRESSION EQUATIONS FOR NECK VOLUME

NECK VOLUME = 0.283901 \*WEIGHT +15.277530 R\*\*2 = 0.5468  
 NECK VOLUME = 1.825996 \*STANDING -63.947340 R\*\*2 = 0.3883  
 NECK VOLUME = 0.385245 \*WEIGHT -0.850014 \*STANDING +57.407520 R\*\*2 = 0.5613

REGRESSION EQUATIONS FOR HEAD VOLUME

HEAD VOLUME = 0.251318 \*WEIGHT +223.758300 R\*\*2 = 0.1628  
 HEAD VOLUME = 1.927238 \*STANDING +131.907200 R\*\*2 = 0.1643  
 HEAD VOLUME = 0.125367 \*WEIGHT +1.056407 \*STANDING +171.398700 R\*\*2 = 0.1712

REGRESSION EQUATIONS FOR THIGH VOLUME

THIGH VOLUME = 3.366777 \*WEIGHT +22.178710 R\*\*2 = 0.9117  
 THIGH VOLUME = 24.206470 \*STANDING -1095.67700 R\*\*2 = 0.8089  
 THIGH VOLUME = 2.797834 \*WEIGHT +4.771981 \*STANDING -214.339100 R\*\*2 = 0.9171

REGRESSION EQUATIONS FOR CALF VOLUME

CALF VOLUME = 1.252436 \*WEIGHT +21.243680 R\*\*2 = 0.8473  
 CALF VOLUME = 9.460768 \*STANDING -426.461700 R\*\*2 = 0.8298  
 CALF VOLUME = 0.724384 \*WEIGHT +4.429010 \*STANDING -198.275400 R\*\*2 = 0.8785



REGRESSION EQUATIONS FOR FOOT VOLUME

FOOT VOLUME = 0.291110 \*WEIGHT +9.215927 R\*\*2 = 0.7735  
 FOOT VOLUME = 2.257187 \*STANDING -98.911440 R\*\*2 = 0.7981  
 FOOT VOLUME = 0.128008 \*WEIGHT +1.368013 \*STANDING -58.588170 R\*\*2 = 0.8238

REGRESSION EQUATIONS FOR UPPER ARM VOLUME

UPPER ARM VOLUME = 0.757131 \*WEIGHT -10.831830 R\*\*2 = 0.8642  
 UPPER ARM VOLUME = 5.123630 \*STANDING -239.858200 R\*\*2 = 0.6793  
 UPPER ARM VOLUME = 0.851218 \*WEIGHT -0.789154 \*STANDING +28.281800 R\*\*2 = 0.8670

REGRESSION EQUATIONS FOR FOREARM VOLUME

FOREARM VOLUME = 0.451460 \*WEIGHT +6.405045 R\*\*2 = 0.8453  
 FOREARM VOLUME = 3.096293 \*STANDING -133.036500 R\*\*2 = 0.6825  
 FOREARM VOLUME = 0.478980 \*WEIGHT -0.230826 \*STANDING +17.645720 R\*\*2 = 0.8460

REGRESSION EQUATIONS FOR HAND VOLUME

HAND VOLUME = 0.122105 \*WEIGHT +10.425090 R\*\*2 = 0.7538  
 HAND VOLUME = 0.899664 \*STANDING -31.637040 R\*\*2 = 0.7023  
 HAND VOLUME = 0.086374 \*WEIGHT +0.299688 \*STANDING -4.428604 R\*\*2 = 0.7672

REGRESSION EQUATIONS FOR FOREARM PLUS HAND VOLUME

FOREARM + HAND VOLUME = 0.573555 \*WEIGHT +16.831600

FOREARM + HAND VOLUME = 3.996506 \*STANDING -164.711900

FOREARM + HAND VOLUME = 0.564920 \*WEIGHT +0.072425 \*STANDING +13.241960

R\*\*2 = 0.8482

R\*\*2 = 0.7069

R\*\*2 = 0.8483

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APPENDIX E  
ANTHROPOMETRIC TERMS AND LANDMARK DESCRIPTIONS

**Abduct:** to move from the axis of the body or one of its parts.

**Acromiale Landmark (right and left):** the most lateral point on the lateral margin of the acromial process of each scapula--a point on the tip of each shoulder.

**Acomion:** same as acromiale.

**Ankle Landmark:** the level of the minimum circumference of the ankle as established by measuring. Proximal to the malleoli (rounded bony prominences on either side of ankle).

**Anterior:** pertaining to the front of the body; as opposed to posterior.

**Anterior Superior Iliac Spine (right and left) (females):** the inferior point of each anterior superior iliac spine of the ilium.

**Anterior Superior Iliac Spine (right and left) (males):** the most prominent point of each anterior superior iliac spine of the ilium.

**Axilla:** the arm pit.

**Biceps Landmark:** the level of maximum bulge of the tensed biceps when the arm is bent to a right angle.

**Biceps Circumference Landmark:** same as biceps landmark.

**Brow Ridges:** the bony ridges of the anterior forehead which lie above the orbits of the eye.

**Bustpoint Landmarks:** most anterior protrusion of the right bra pocket.

**Buttock Landmark:** the maximum posterior protrusion of the right buttock.

**Calf Landmark (right and left):** the level of the maximum circumference of the calf as established by measurement.

**Cervicale:** the superior tip of the spine of the 7th cervical vertebra. (The protrusion of the spinal column at the base of the neck.)

**Clavicale (right and left):** The point on the most imminent prominence of the superior aspect of the medial end of each clavicle.

**Dactylion:** the tip of the middle finger.

**Distal:** the end of a body segment farthest from the head; opposed to proximal.

**Epicondyle:** bony eminence at the distal end of the humerus and femur.

**Extend:** to move adjacent segments so that the angle between them is increased as when the leg is straightened; opposite of flex.

**Femoral Epicondyle, Lateral (right and left):** the lateral point on the lateral epicondyle of each femur.

**Femoral Epicondyle, Medial (right and left):** the medial point on the medial epicondyle of each femur.

**Femur:** the thigh bone.

**Flex:** to move a joint in such a direction as to bring together the two parts which it connects, as when the elbow is bent.

**Forearm Landmark:** a level one tape width (6mm) distal to the crotch of the elbow with the elbow flexed 90 degrees.

**Frankfort Plane:** the standard horizontal plane or orientation of the head. The plane is established by a line passing through the right tragion and the lowest point of the right orbit (eye socket).

**Glabella:** the most anterior point of the forehead between the brow ridges in the midsagittal plane.

**Gluteal Furrow:** the furrow at the juncture of the buttock and thigh.

**Humeral Epicondyle, Lateral (right and left):** the lateral point on the lateral epicondyle of each humerus with the arm in the anatomical position.

**Humeral Epicondyle, Medial (right and left):** the medial point on the medial epicondyle of each humerus with the arm in the anatomical position.

**Humerus:** the upper arm bone.

**Hyperextend:** to overextend a limb or part of the body.

**Ilium:** the upper one of three bones composing either lateral half of the pelvis.

**Inferior:** below in relation to another structure; lower.

**Lateral:** lying near or toward the sides of the body; opposed to

medial.

**Lower Arm Circumference Landmark:** the level of maximum circumference of the tensed lower arm when the arm is bent to a right angle.

**Malleolus, Lateral (right and left):** the most lateral point on the lateral bony protrusion of each ankle.

**Malleolus, Medial (right and left):** the most medial point on the medial bony protrusion of each ankle.

**Medial:** lying near or towards the midline of the body; opposed to lateral.

**Menton:** the point of the tip of the chin in the midsagittal plane.

**Metacarpal:** pertaining to the long bones of the hand between the wrist and the phalanges.

**Metatarsal:** pertaining to the long bones of the foot between the tarsus and the phalanges.

**Midpatella:** a point one-half the distance between the superior and inferior margins of the patella.

**Midsagittal Plane:** the vertical plane which divides the body into right and left halves.

**Neck Landmarks:** at the level of the juncture of the neck with the shoulders. This level is established by laying a string tie or a tape around the base of the neck.

**Occiput:** a bone forming the posterior base of the skull.

**Omphalion:** the level of the midpoint of the naval.

**Patella:** the kneecap.

**Phalanges:** the bones of the fingers and toes.

**Popliteal:** pertaining to the area of the back of the leg directly behind the knee.

**Posterior:** pertaining to the back of the body; as opposed to anterior.

**Posterior Superior Iliac Midspine:** the point on the mid-spine made at the level of the posterior superior iliac spines. A dimple often indicates the site of this iliac spine.

**Proximal:** the end of a body segment nearest the head; opposed to distal.

**Radial Styloid (right and left):** the distal end of each radius.

**Radiale:** the uppermost point on the lateral margin of the head of the radius.

**Radius:** the bone of the forearm on the thumb side of the arm.

**Scapula:** the shoulder blade.

**Scye:** a tailoring term to designate the armhole of a garment. Refers here to landmarks which approximate the lower level of the axilla.

**Stylian:** same as radial styloid.

**Superior:** above in relation to another structure; higher.



**Suprapatella:** the superior point on the patella while it is in the relaxed position.

**Symphysion (females):** the anterior point in the midsagittal plane on the notch of the superior border of the pubic symphysis, the anterior juncture of the pelvic bones.

**Symphysion (males):** the lowest point on the superior border of the pubic symphysis, the anterior juncture of the pelvic bones.

**Tenth Rib:** the inferior point on the inferior border of the lowest of the two tenth ribs. The midspine landmark is made at this level but marked on the midspine.

**Tibiale:** the uppermost point of the medial margin of the tibia (shin bone).

**Tragion (right and left):** the point located at the notch just above the tragus of each ear. This point corresponds to the upper edge of the ear hole.

**Tragus:** the small cartilaginous flap of flesh in front of the ear hole.

**Trochanterion (right and left):** the superior point on the greater trochanter of each femur.

**Ulna:** one of the bones of the forearm on the little finger side of the arm.

**Ulnar Styliod (right and left):** the most distal point of each ulna.

**Vertex:** the top of the head.

**Waist Landmark:** the level established by the subject placing an elastic tape around her "natural waist".

**Wrist Landmark (females):** the level of the extension of the radial styliion point across the anterior surface of the forearm perpendicular to the long axis of the forearm.

**Wrist Landmark (males):** the level of minimum circumference of the wrist just above (toward the elbow) the bony prominences on each side of the wrist.

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APPENDIX F  
ANTHROPOMETRY DESCRIPTIONS

Appendix F contains a description of each body dimension required by GEBODIII given in the order as referenced by the program. Neither the 1967 nor the 1968 USAF anthropometric survey included all the needed measurements. When a needed measurement was not taken from a survey, that measurement was derived from available measurements. A description of the available measurements is given. Since hand depth was not measured in the 1968 USAF female survey, refer to the male description. The first set of descriptions are for the adult human female and are taken directly from the 1968 survey report, Clauser, et al. (1972). The second set of descriptions are for the adult human male and are taken directly from the 1967 survey report, Grunhofer and Kroh (1975).

## ADULT HUMAN FEMALE ANTHROPOMETRY DESCRIPTIONS

The number in parentheses following each description is the number by which this variable is identified in the original 1968 USAF survey.

0. WEIGHT: Subject stands on scales (nude or wearing lightweight undergarments) with feet parallel and weight distributed equally on both feet. (2)
1. STANDING HEIGHT: Subject stands erect, head in the Frankfort plane, heels together, and weight distributed equally on both feet. With the arm of the anthropometer firmly touching the scalp, measure the vertical distance from the standing surface to the top of the head. (7)
2. SHOULDER HEIGHT: Subject stands erect looking straight ahead, heels together, and weight distributed equally on both feet. With an anthropometer, measure the vertical distance from the standing surface to the right acromiale landmark. (10)
3. ARMPIT HEIGHT: Measurement derived by subtracting Scye Circumference divided by  $\pi$  from Shoulder Height (see above).

Scye Circumference: Subject stands erect looking straight ahead. The right arm is abducted sufficiently to allow placement of a tape into the axilla. With a tape passing through the axilla, over the anterior and posterior-vertical scye landmarks and over the right acromiale landmark, measure the circumference of the scye. The axillary tissue is not compressed. (53)

4. WAIST HEIGHT: Subject stands erect looking straight ahead,

heels together, and weight distributed equally on both feet. With an anthropometer, measure the vertical distance from the standing surface to the anterior waist landmark. (13)

5. SEATED HEIGHT: Subject sits erect, head in the Frankfort plane, upper arms hanging relaxed, forearms and hands extended forward horizontally. With the anthropometer arm firmly touching the scalp, measure the vertical distance from the sitting surface to the top of the head. (23)
6. HEAD LENGTH: Subject sits. With a spreading caliper, measure in the midsagittal plane the maximum length of the head between the glabella landmark and the occiput. (96)
7. HEAD BREADTH: Subject sits. With a spreading caliper measure the maximum horizontal breadth of the head above the level of the ears. (97)
8. HEAD TO CHIN HEIGHT: Subject stands under the headboard looking straight ahead. The headboard is adjusted so that its vertical and horizontal planes are in firm contact with the back and the top of the head. Positioning the head in the Frankfort plane and using the special gauge, measure the vertical distance from the horizontal plane to the menton landmark. (104)
9. NECK CIRCUMFERENCE: Subject sits erect, head in the Frankfort plane. A piece of dental tape is placed around the neck, passing over all four neck landmarks. The measurer marks off with her thumbnail a length of tape corresponding to the subject's neck circumference, and then measures this tape segment with a standard tape. (36)
10. SHOULDER BREADTH: Subject sits erect looking straight ahead, upper arms hanging relaxed, forearms and hands

extended forward horizontally. With a beam caliper, measure the distance between the acromiale landmarks. (63)

11. CHEST DEPTH: Subject stands erect looking straight ahead, heels together, and weight distributed equally on both feet. With a beam caliper, measure the horizontal depth of the trunk at the level of the bustpoint landmarks. The reading is made at the point of maximum quiet inspiration. (74)
12. CHEST BREADTH: Subject stands erect looking straight ahead with arms slightly abducted. With a beam caliper, measure the horizontal distance across the trunk at the level of the bustpoint landmarks. (74)
13. WAIST DEPTH: Subject stands erect looking straight ahead, arms at sides, heels together, and weight distributed equally on both feet. With a beam caliper, measure the horizontal depth of the trunk at the level of the waist landmarks. The reading is made at the point of maximum quiet inspiration. The subject must not pull in her stomach. (75)
14. WAIST BREADTH: Subject stands erect looking straight ahead with arms slightly abducted. With a beam caliper, measure the horizontal breadth across the trunk at the level of the waist landmarks. (67)
15. BUTTOCK DEPTH: Subject stands erect, heels together and weight distributed equally on both feet. With a beam caliper, measure the horizontal depth of the trunk at the level of the buttock landmark. (77)

16. **HIP BREADTH, STANDING:** Subject stands erect, heels together and weight distributed equally on both feet. With a beam caliper, measure the maximum horizontal breadth of the hips. (68)
17. **SHOULDER TO ELBOW LENGTH:** Subject stands erect looking straight ahead and with arms relaxed. With a beam caliper held parallel to the long axis of the right upper arm, measure the distance from the acromiale landmark to the radiale landmark. (31)
18. **FOREARM-HAND LENGTH:** Measurement derived by summing Radiale-Stylian Length and Hand Length (see below).

Radiale-Stylian Length: Subject stands erect with arms relaxed. With a beam caliper held parallel to the long axis of the right forearm, measure the distance from the radiale landmark to the stylian landmark. (32)

19. **BICEPS CIRCUMFERENCE:** Subject stands with right arm slightly abducted. With a tape held in a plane perpendicular to the long axis of the upper arm, measure the circumference of the arm at the level of the biceps landmark. (55)
20. **ELBOW CIRCUMFERENCE:** Subject stands, right upper arm raised so that its long axis is horizontal, elbow flexed 90 degrees, fist tightly clenched and biceps strongly contracted. With a tape passing over the tip and through the crotch of the elbow, measure the circumference of the elbow. (59)
21. **FOREARM CIRCUMFERENCE:** Subject stands erect with right arm slightly abducted and hand relaxed. With a tape held in a



plane perpendicular to the long axis of the forearm, measure the circumference of the arm at the level of the forearm landmark. (60)

22. WRIST CIRCUMFERENCE: Subject stands with right arm slightly abducted. With a tape held in a plane perpendicular to the long axis of the forearm and hand, measure the circumference of the wrist at the level of the styliion landmark. (62)
23. KNEE HEIGHT, SEATED: Measurement derived by summing Knee Circumference (see below) divided by  $2\pi$  and Tibiale Height.

Tibiale Height: Subject stands erect, heels together, and weight distributed equally on both feet. With an anthropometer, measure the vertical distance from the standing surface to the tibiale landmark on the right leg. (18)

24. THIGH CIRCUMFERENCE: Subject stands erect, heels approximately 10 cm apart, and weight distributed equally on both feet. With a tape held in a plane perpendicular to the long axis of the right thigh measure the circumference of the thigh at the level of the lowest point on the gluteal furrow. Where the furrow is deeply indented, the measurement is made just distal to the furrow.
25. UPPER LEG CIRCUMFERENCE: Measurement derived by summing the Thigh Circumference (45) (see above) and the Knee Circumference (46) (see below) and dividing the sum by two to obtain the average.
26. KNEE CIRCUMFERENCE: Subject stands erect, heels approximately 10 cm apart, and weight distributed equally on both feet. With a tape held in a plane perpendicular to the long axis of the right leg, measure the circumference of the

knee at the level of the midpatella landmark. The subject must not tense her knee during the measurement. (46)

27. CALF CIRCUMFERENCE: Subject stands erect, heels approximately 10 cm apart, and weight distributed equally on both feet. With a tape held in a plane perpendicular to the long axis of the right lower leg, measure the circumference of the calf at the level of the calf landmark. (47)
28. ANKLE CIRCUMFERENCE: Subject stands erect with weight distributed equally on both feet. With a tape held in a plane perpendicular to the long axis of the right lower leg, measure the circumference of the leg at the level of the ankle landmark. (49)
29. ANKLE HEIGHT, OUTSIDE: Subject stands with weight distributed equally on both feet. With the special measuring block, measure the vertical distance from the standing surface to the lateral malleolus landmark on the right leg. (21)
30. FOOT BREADTH: Subject stands erect, right foot in the measuring box, left foot on a board of equal height, and weight distributed equally. The right foot is positioned so that its long axis is parallel to the side of the box, the heel touches the rear of the box, and the medial metatarsal-phalangeal joint touches the widest part of the foot, measure on the scale of the box the breadth of the foot. (95)
31. FOOT LENGTH: Subject stands erect, right foot in the measuring box, left foot on a board of equal height, and weight distributed equally. The right foot is positioned so that its long axis is parallel to the side of the box, the heel touches the rear of the box, and the medial metatarsal-

phalangeal joint touches the side of the box. With the measuring block touching the tip of the most protruding toe, measure on the scale of the box the length of the foot.

(94)

32. **HAND BREADTH:** Subject sits, right forearm and hand raised with palm down. The fingers are together and straight but not hyper-extended. With a sliding caliper, measure the breadth of the hand between metacarpal-phalangeal joints II and V. (92)

33. **HAND LENGTH:** Subject sits, right forearm and hand raised with palm up. The fingers are together and straight but not hyper-extended. With the bar of a sliding caliper parallel to the long axis of the hand, measure the distance from the wrist landmark to the dactylion. (91)

## ADULT HUMAN MALE ANTHROPOMETRIC DESCRIPTIONS

The number in parentheses following each description is the number by which this variable is identified in the original 1967 USAF survey.

0. WEIGHT: Subject is nude. The scale is read to the nearest pound. (2)
1. STANDING HEIGHT: Subject stands erect with head in the Frankfort plane. With the anthropometer arm touching the scalp, measure the vertical distance from the standing surface to the top of the head. (13)
2. SHOULDER HEIGHT: Subject stands erect. Using the anthropometer, measure the vertical distance from the standing surface to the right acromiale landmark. (15)
3. ARMPIT HEIGHT: Measurement derived by subtracting Scye Circumference divided by  $\pi$  from Shoulder Height (see above).

Scye Circumference: Subject stands, his right arm initially raised, and then lowered after the tape is in place. Measure the circumference of the scye with the tape placed as high as possible in the right armpit and passing vertically over the shoulder. (103)

4. WAIST HEIGHT: Subject stands erect, his head in the Frankfort plane. Using an anthropometer, measure the distance from the standing surface to the omphalion landmark. The subject must not pull in his stomach. (21)
5. SEATED HEIGHT: Subject sits erect, his head in the Frankfort plane, his upper arms hanging relaxed, and his

forearms and hands extended forward horizontally. Using an anthropometer, measure the vertical distance from the sitting surface to the top of the head. (32)

6. HEAD LENGTH: Subject sits. With a spreading caliper, measure the maximum length of the head between the glabella and the occiput in the midsagittal plane. (150)
7. HEAD BREADTH: Subject sits. Holding the spreading caliper near the tips, measure the maximum breadth of the head in a line perpendicular to the midsagittal plane. (156)
8. HEAD TO CHIN HEIGHT: Subject stands comfortably under the headboard with his head oriented in the Frankfort plane. The headboard slide is then adjusted so that its wall and ceiling surfaces are in firm contact with the back and vertex of the subject's head. His head is rechecked for orientation and for continued contact at both points. Using the headboard caliper, measure the vertical distance from vertex to the menton landmark. (179)
9. NECK CIRCUMFERENCE: Subject stands erect, his head in the Frankfort plane. Holding the tape perpendicular to the long axis of the neck, measure the maximum circumference of the neck, including the Adam's apple. (66)
10. SHOULDER BREADTH: Subject sits erect, his head in the Frankfort plane, his arms hanging relaxed, and his forearms and hands extended forward horizontally. Using a beam caliper, measure the horizontal distance between the right and left acromiale landmarks. (50)
11. CHEST DEPTH: Subject stands erect, his head in the Frankfort plane. With a beam caliper, measure the horizontal depth of the trunk at the level of the nipples.

The reading is made at the point of maximum quiet inspiration. (62)

12. CHEST BREADTH: Subject stands erect, his head in the Frankfort plane, and his arms slightly abducted. Using a beam caliper, measure the horizontal distance across the trunk at the level of the nipples. (52)
13. WAIST DEPTH: Subject stands erect, his head in the Frankfort plane. Using a beam caliper, measure the horizontal depth of the trunk at the level of the omphalion landmark. The reading is made at the point of maximum quiet inspiration. The subject must not pull in his stomach. (63)
14. WAIST BREADTH: Subject stands erect, his head in the Frankfort plane. Using a beam caliper, measure the horizontal distance across the trunk at the level of the omphalion landmark. (53)
15. BUTTOCK DEPTH: Subject stands erect, his head in the Frankfort plane. Using a beam caliper, measure the horizontal depth of the trunk at the level of maximum protrusion of the buttocks. (64)
16. HIP BREADTH, STANDING: Subject stands erect, feet together. Using a beam caliper, measure the horizontal distance across the widest portion of the hips. (55)
17. SHOULDER TO ELBOW LENGTH: Subject sits erect, his head in the Frankfort plane, his arms hanging relaxed, and his forearms and hands extended forward horizontally. Using a beam caliper, measure the vertical distance from the right acromiale landmark to the bottom of the elbow (olecranon process). (42)

18. **FOREARM-HAND LENGTH:** Measurement derived by adding the Elbow-Wrist Length and Wrist Height, and then subtracting Dactylion Height.

**Elbow-Wrist Length:** Subject stands erect, his right upper arm hanging at side, his lower arm and hand extended forward horizontally. Using the beam caliper, measure the distance from the tip of the right elbow to the stylium landmark. (44)

**Wrist Height:** Subject stands erect, his arms hanging naturally at his sides. Using the anthropometer, measure the vertical distance from the standing surface to the stylium landmark on the right wrist. (17)

**Dactylion Height:** Subject stands erect with his arms hanging at his sides, his elbows fully extended and his fingers pointing to the standing surface. Using the anthropometer, measure the vertical distance from the standing surface to the tip of the right middle finger. (18)

19. **BICEPS CIRCUMFERENCE:** Measurement derived by summing Biceps Circumference, Extended, Right; Biceps Circumference, Extended, Left; Biceps Circumference, Flexed, Right; and Biceps Circumference, Flexed, Left. This sum is then divided by four to obtain the average.

**Biceps Circumference, Extended, Right:** Subject stands erect, his right arm extended with the hand about 30 cm from the side of the body. Holding the tape perpendicular to the long axis of the upper arm, measure the circumference of the arm at the biceps circumference landmark. (104)

Biceps Circumference, Extended, Left: Subject stands erect, his left arm extended with the hand about 30 cm from the side of the body. Holding the tape perpendicular to the long axis of the upper arm, measure the circumference of the arm at the biceps circumference landmark. (105)

Biceps Circumference, Flexed, Right: Subject bends his right arm to about a right angle and makes a fist while holding the upper arm horizontally. Using the tape, measure the circumference of the arm at the biceps circumference landmark. (106)

Biceps Circumference, Flexed, Left: Subject bends his left arm to about a right angle and makes a fist while holding the upper arm horizontally. Using the tape, measure the circumference of the arm at the biceps circumference landmark. (107)

20. ELBOW CIRCUMFERENCE: Subject bends his right arm to about a right angle and makes a fist while holding the upper arm horizontally. With the tape passing over the tip and through the crotch of the elbow, measure the circumference of the elbow. (109)
21. FOREARM CIRCUMFERENCE: Subject stands, his right elbow extended and his hand about 30 cm from the side of the body. Holding the tape perpendicular to the long axis of the arm, measure the circumference of the arm at the level of the lower arm circumference landmark. (110)
22. WRIST CIRCUMFERENCE: Subject stands, his right elbow extended, with the hand about 30 cm from the side of the body. Holding the tape perpendicular to the long axis of



the lower arm, measure the circumference of the wrist at the level of the wrist landmark. (112)

23. **KNEE HEIGHT, SEATED:** Subject sits with his feet resting on a surface adjusted so that the knees are bent at about right angles. Using an anthropometer, measure the vertical distance from the footrest surface to the suprapatella landmark on the right knee. (37)
24. **THIGH CIRCUMFERENCE:** Subject stands with his legs slightly apart. Holding the tape in a plane at right angles to the long axis of the right leg at the level of the lowest point on the gluteal furrow, measure the circumference of the upper thigh. (96)
25. **UPPER LEG CIRCUMFERENCE:** Subject stands erect. Holding a tape in a horizontal plane, measure the circumference of the knee at the level of the center of the relaxed patella. (98)
26. **KNEE CIRCUMFERENCE:** Subject sits erect, his feet resting on a surface so that the knees are bent at about right angles. With the tape passing under the popliteal area of the right leg and brought up at about a 45-degree angle over the knee, measure the maximum circumference of the right knee. (99)
27. **CALF CIRCUMFERENCE:** Subject stands with legs slightly apart. Holding a tape in a plane perpendicular to the long axis of the leg, measure the maximum circumference of the right calf. (100)
28. **ANKLE CIRCUMFERENCE:** Subject stands with legs slightly apart. Holding a tape in a plane perpendicular to the long axis of the leg, measure the minimum circumference of the right ankle. (102)

29. ANKLE HEIGHT, OUTSIDE: Subject stands with his right foot slightly forward and his weight equally distributed on both feet. Touch the measuring-block scale against the lateral side of the foot and measure the height of the landmark indicating the minimum circumference of the right ankle. (31)
30. FOOT BREADTH: Subject stands with his right foot in the foot box, the foot just touching the side and rear walls, its long axis parallel to the side wall, and his weight equally distributed on both feet. With the block touching the widest part of the foot, measure foot width from the side wall, using the scale on the floor of the box. (127)
31. FOOT LENGTH: Subject stands with his right foot in the foot box, the foot just touching the side and rear walls, its long axis parallel to the side wall, and his weight equally distributed on both feet. With the block touching the tip of the longest toe, measure foot length from the rear wall, using the scale on the floor of the box. (125)
32. HAND BREADTH: Subject sits with his right hand resting on a table, palm up, fingers extended and together. The thumb is held away from the hand. Using the sliding caliper, measure the maximum breadth from Metacarpale II to Metacarpale V. (136)
33. HAND LENGTH: Subject sits with his right hand resting flat on a table, palm up, fingers extended and together. With the bar of the sliding caliper parallel to the long axis of the hand, measure the distance from the wrist landmark to the tip of the longest finger. (134)
34. HAND DEPTH: Subject's right hand is held palm down with fingers extended and together, narrow profile towards the

measurerer. Maintaining light pressure on the spreading caliper, measure the thickness of the hand at the metacarpal-phalangeal joint of the third finger. (140)

APPENDIX G  
SUMMARY STATISTICS

The summary statistics given in Appendix G lists, for each variable (in alphabetical order), the mean, standard deviation (STD), a measure of symmetry in distribution (SKEW), a measure of kurtosis in distribution (KURT), the coefficient of variation (CV), minimum dimensional value (MIN), and the maximum dimensional value (MAX). The 1968 USAF survey statistics are based on N = 1905; the 1967 USAF survey statistics are based on N = 2420. Weight is expressed in pounds and all other dimensional values are expressed in inches. The statistics for both surveys were obtained using the Anthropometric Data Base at the Center for Anthropometric Research Data (Robinson, Robinette, and Zehner, 1989). The computational methods used to calculate these statistics can be found in Clauser, et al. (1972). The symmetry statistic (skewness) as given in that reference is subtracted from 3.00, so that a symmetric distribution approaches a skewness value of 0.0 rather than 3.0.

SUMMARY STATISTICS

1968 USAF FEMALES

| VARIABLE NAME       | MEAN  | STD  | SKEW | KURT | CV   | MIN  | MAX  |
|---------------------|-------|------|------|------|------|------|------|
| ANKLE CIRC          | 8.29  | .50  | .26  | -.05 | 6.11 | 6.8  | 10.0 |
| ANKLE HT, OUTSIDE   | 2.66  | .23  | .04  | .23  | 8.67 | 1.9  | 3.4  |
| BICEPS CIRC         | 10.08 | .90  | .62  | 1.04 | 8.96 | 7.6  | 14.7 |
| BUTTOCK DEPTH       | 8.32  | .70  | .54  | .95  | 8.46 | 6.3  | 12.0 |
| CALF CIRC           | 13.44 | .88  | .25  | .29  | 6.58 | 10.5 | 17.5 |
| CHEST BREADTH       | 11.02 | .75  | .47  | .39  | 6.84 | 8.7  | 14.1 |
| CHEST DEPTH         | 9.30  | .75  | .66  | .71  | 8.17 | 7.2  | 12.7 |
| ELBOW CIRC          | 10.62 | .70  | .26  | .31  | 6.61 | 8.4  | 14.0 |
| FOOT BREADTH        | 3.49  | .19  | .26  | .55  | 5.61 | 2.7  | 4.3  |
| FOOT LENGTH         | 9.47  | .44  | .12  | -.14 | 4.69 | 8.2  | 10.8 |
| FOREARM CIRC        | 9.24  | .54  | .38  | .63  | 5.87 | 7.7  | 11.8 |
| HAND BREADTH        | 2.97  | .15  | -.01 | .03  | 5.16 | 2.4  | 3.4  |
| HAND LENGTH         | 7.23  | .37  | .25  | .02  | 5.22 | 6.0  | 8.6  |
| HEAD BREADTH        | 5.71  | .23  | .11  | .16  | 4.10 | 4.9  | 6.7  |
| HEAD LENGTH         | 7.24  | .26  | .03  | -.05 | 3.69 | 6.4  | 8.1  |
| HEAD TO CHIN HT     | 8.62  | .44  | .15  | .31  | 5.20 | 7.2  | 10.5 |
| HIP BR, STANDING    | 13.76 | .87  | .39  | .44  | 6.34 | 11.2 | 17.3 |
| KNEE CIRC           | 14.29 | .89  | .45  | .44  | 6.24 | 12.0 | 17.9 |
| NECK CIRC           | 13.28 | .66  | .30  | .11  | 4.97 | 11.2 | 15.7 |
| RADIALE-STYLION LTH | 9.20  | .53  | .14  | .03  | 5.85 | 7.5  | 11.0 |
| SCYE CIRC           | 14.60 | .90  | .42  | .64  | 6.17 | 11.2 | 19.2 |
| SEATED HEIGHT       | 33.70 | 1.24 | .08  | -.14 | 3.70 | 29.6 | 37.9 |
| SHOULDER BREADTH    | 14.11 | .64  | .09  | .19  | 4.57 | 12.1 | 16.3 |
| SHOULDER HEIGHT     | 51.91 | 2.15 | .14  | -.21 | 4.16 | 45.7 | 59.8 |
| SHOULDER TO ELBOW L | 12.20 | .64  | -.02 | .02  | 5.24 | 9.9  | 14.3 |
| STANDING HEIGHT     | 63.82 | 2.36 | .16  | -.22 | 3.70 | 56.9 | 72.0 |
| TIBIALE HEIGHT      | 16.52 | .93  | .22  | .02  | 5.66 | 13.4 | 19.5 |
| THIGH CIRC          | 21.83 | 1.66 | .32  | .42  | 7.61 | 17.1 | 28.3 |
| WAIST BREADTH       | 9.49  | .76  | .52  | .55  | 8.02 | 7.4  | 12.8 |
| WAIST DEPTH         | 6.69  | .65  | 1.14 | 2.42 | 9.83 | 5.1  | 10.0 |
| WAIST HEIGHT        | 39.48 | 1.77 | .15  | -.14 | 4.49 | 34.3 | 45.4 |

SUMMARY STATISTICS  
1968 USAF FEMALES  
(CONTINUED)

| VARIABLE NAME | MEAN   | STD   | SKEW | KURT | CV    | MIN  | MAX   |
|---------------|--------|-------|------|------|-------|------|-------|
| WEIGHT        | 127.28 | 16.59 | .64  | .86  | 13.03 | 85.0 | 200.0 |
| WRIST CIRC    | 5.88   | .27   | .26  | .14  | 4.76  | 4.9  | 6.9   |

SUMMARY STATISTICS

1967 USAF MALES

| VARIABLE NAME       | MEAN  | STD  | SKEW | KURT | CV   | MIN  | MAX  |
|---------------------|-------|------|------|------|------|------|------|
| ANKLE CIRC          | 8.82  | .49  | .19  | .12  | 5.64 | 7.1  | 10.5 |
| ANKLE HT, OUTSIDE   | 5.40  | .45  | .36  | -.04 | 8.35 | 4.0  | 7.0  |
| BICEPS CIRC, EX, L  | 11.96 | .92  | .10  | .00  | 7.70 | 8.6  | 15.1 |
| BICEPS CIRC, EX, R  | 12.12 | .92  | .12  | .00  | 7.59 | 9.1  | 15.2 |
| BICEPS CIRC, FL, L  | 12.64 | .88  | .16  | .06  | 6.99 | 9.9  | 15.7 |
| BICEPS CIRC, FL, R  | 12.88 | .88  | .12  | .05  | 6.90 | 9.9  | 16.0 |
| BUTTOCK DEPTH       | 9.43  | .80  | .19  | .14  | 8.57 | 6.7  | 13.3 |
| CALF CIRC           | 14.64 | .89  | .11  | .09  | 6.10 | 11.8 | 17.7 |
| CHEST BREADTH       | 12.90 | .83  | .34  | .24  | 6.46 | 10.2 | 16.3 |
| CHEST DEPTH         | 9.65  | .75  | .12  | -.02 | 7.87 | 7.5  | 12.4 |
| DACTYLION HEIGHT    | 26.44 | 1.38 | .11  | -.07 | 5.23 | 22.4 | 31.0 |
| ELBOW CIRC          | 12.29 | .68  | .18  | -.02 | 5.59 | 10.1 | 14.5 |
| ELBOW-WRIST LTH     | 11.80 | .55  | .10  | .06  | 4.71 | 10.0 | 13.6 |
| FOOT BREADTH        | 3.84  | .19  | .31  | .20  | 5.07 | 3.3  | 4.6  |
| FOOT LENGTH         | 10.64 | .46  | .15  | .09  | 4.40 | 9.1  | 12.3 |
| FOREARM CIRC        | 11.08 | .57  | .10  | -.07 | 5.19 | 9.2  | 12.8 |
| HAND BREADTH        | 3.50  | .16  | .12  | -.04 | 4.66 | 2.9  | 4.0  |
| HAND DEPTH          | 1.09  | .08  | .02  | .74  | 7.56 | .7   | 1.4  |
| HAND LENGTH         | 7.52  | .32  | .16  | .02  | 4.29 | 6.5  | 8.7  |
| HEAD BREADTH        | 6.14  | .21  | .13  | -.06 | 3.48 | 5.4  | 6.9  |
| HEAD LENGTH         | 7.82  | .26  | .10  | .18  | 3.39 | 6.8  | 8.8  |
| HEAD TO CHIN HT     | 8.96  | .40  | -.02 | -.13 | 4.49 | 7.5  | 10.2 |
| HIP BR, STANDING    | 13.88 | .74  | .28  | .57  | 5.35 | 11.2 | 17.5 |
| KNEE CIRC           | 15.47 | .83  | .30  | .22  | 5.40 | 13.1 | 19.1 |
| KNEE HT, SEATED     | 21.95 | .98  | .09  | .03  | 4.46 | 18.7 | 25.2 |
| NECK CIRC           | 15.09 | .75  | .29  | .19  | 4.98 | 12.8 | 17.7 |
| SCYE CIRC           | 19.03 | 1.09 | .08  | .00  | 5.76 | 15.9 | 23.3 |
| SEATED HEIGHT       | 36.68 | 1.25 | .09  | -.03 | 3.41 | 31.8 | 41.2 |
| SHOULDER BREADTH    | 16.03 | .76  | -.07 | .19  | 4.77 | 13.3 | 18.6 |
| SHOULDER HEIGHT     | 57.16 | 2.26 | .02  | -.08 | 3.96 | 50.3 | 64.7 |
| SHOULDER TO ELBOW L | 14.15 | .67  | .11  | -.05 | 4.77 | 12.0 | 16.8 |

SUMMARY STATISTICS  
 1967 USAF MALES  
 (CONTINUED)

| VARIABLE NAME   | MEAN   | STD   | SKEW | KURT | CV    | MIN   | MAX   |
|-----------------|--------|-------|------|------|-------|-------|-------|
| STANDING HEIGHT | 69.81  | 2.43  | .06  | -.14 | 3.49  | 62.1  | 77.6  |
| THIGH CIRC      | 23.15  | 1.74  | .11  | .17  | 7.54  | 17.9  | 29.8  |
| UPPER LEG CIRC  | 15.22  | .81   | .19  | .28  | 5.36  | 12.4  | 18.9  |
| WAIST BREADTH   | 12.18  | .94   | .33  | .60  | 7.72  | 9.2   | 17.3  |
| WAIST DEPTH     | 8.78   | .85   | .37  | .37  | 9.78  | 6.4   | 13.2  |
| WAIST HEIGHT    | 41.91  | 1.85  | .04  | -.06 | 4.44  | 36.1  | 48.7  |
| WEIGHT          | 173.59 | 21.45 | .31  | .09  | 12.35 | 117.9 | 264.0 |
| WRIST CIRC      | 6.92   | .36   | .35  | .07  | 5.23  | 5.9   | 8.1   |
| WRIST HEIGHT    | 34.08  | 1.55  | .12  | -.05 | 4.55  | 29.6  | 39.5  |



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APPENDIX H  
EXAMPLE OUTPUT LISTINGS

Appendix H contains an example output listing for the 15 segment configuration, and an example output listing for the 17 segment configuration.

SAMPLE FIFTEEN SEGMENT OUTPUT

ADULT HUMAN MALE

SELECTED BODY DIMENSIONS

|                 |       |     |
|-----------------|-------|-----|
| WEIGHT          | 168.5 | LB. |
| STANDING HEIGHT | 68.10 | IN. |

COMPUTED BODY DIMENSIONS

|    |                          |       |     |
|----|--------------------------|-------|-----|
| 0  | WEIGHT                   | 168.5 | LB. |
| 1  | STANDING HEIGHT          | 68.10 | IN. |
| 2  | SHOULDER HEIGHT          | 55.66 | IN. |
| 3  | ARMPIT HEIGHT            | 49.66 | IN. |
| 4  | WAIST HEIGHT             | 40.69 | IN. |
| 5  | SEATED HEIGHT            | 36.00 | IN. |
| 6  | HEAD LENGTH              | 7.783 | IN. |
| 7  | HEAD BREADTH             | 6.127 | IN. |
| 8  | HEAD TO CHIN HEIGHT      | 8.885 | IN. |
| 9  | NECK CIRCUMFERENCE       | 15.06 | IN. |
| 10 | SHOULDER BREADTH         | 15.87 | IN. |
| 11 | CHEST DEPTH              | 9.635 | IN. |
| 12 | CHEST BREADTH            | 12.84 | IN. |
| 13 | WAIST DEPTH              | 8.791 | IN. |
| 14 | WAIST BREADTH            | 12.11 | IN. |
| 15 | BUTTOCK DEPTH            | 9.416 | IN. |
| 16 | HIP BREADTH, STANDING    | 13.74 | IN. |
| 17 | SHOULDER TO ELBOW LENGTH | 13.80 | IN. |
| 18 | FOREARM-HAND LENGTH      | 19.00 | IN. |
| 19 | BICEPS CIRCUMFERENCE     | 12.41 | IN. |
| 20 | ELBOW CIRCUMFERENCE      | 12.16 | IN. |
| 21 | FOREARM CIRCUMFERENCE    | 11.03 | IN. |
| 22 | WRIST CIRCUMFERENCE      | 6.861 | IN. |
| 23 | KNEE HEIGHT, SEATED      | 21.36 | IN. |
| 24 | THIGH CIRCUMFERENCE      | 23.10 | IN. |
| 25 | UPPER LEG CIRCUMFERENCE  | 15.06 | IN. |
| 26 | KNEE CIRCUMFERENCE       | 15.30 | IN. |
| 27 | CALF CIRCUMFERENCE       | 14.59 | IN. |
| 28 | ANKLE CIRCUMFERENCE      | 8.755 | IN. |
| 29 | ANKLE HEIGHT, OUTSIDE    | 5.247 | IN. |
| 30 | FOOT BREADTH             | 3.794 | IN. |
| 31 | FOOT LENGTH              | 10.43 | IN. |

WEIGHT CORRECTION FACTOR = .963

SAMPLE FIFTEEN SEGMENT OUTPUT  
 CRASH VICTIM PARAMETERS (3-D)

| SEGMENT<br>I SYM PLOT | WEIGHT<br>(LB. ) | PRINCIPAL MOMENT OF INERTIA<br>(LB-SEC**2-IN) |        |        | SEGMENT CONTACT ELLIPSOID<br>CENTER (IN) |       |        | PRINCIPAL AXES (DEG) |        |       |     |       |       |
|-----------------------|------------------|---|--------|--------|--|-------|--------|----------------------|--------|-------|-----|-------|-------|
|                       |                  | X   | Y      | Z      | X  | Y     | Z      | YAW                  | PITCH  | ROLL  |     |       |       |
| 1 LI 1                | 24.444           | .8965   | .8257  | 1.0458 | 4.708                                    | 6.871 | 3.548  | -.471                | .000   | .352  | .00 | .00   | .00   |
| 2 CT 2                | 5.109            | .1431   | .0813  | .2176  | 4.396                                    | 6.055 | 3.893  | -1.465               | .000   | -.411 | .00 | .00   | .00   |
| 3 UT 3                | 51.324           | 4.1149  | 3.0331 | 2.6163 | 4.817                                    | 6.419 | 6.735  | .000                 | .000   | .000  | .00 | 14.40 | .00   |
| 4 W 4                 | 2.242            | .0152   | .0185  | .0231  | 2.396                                    | 2.396 | 2.977  | -.479                | .000   | 1.719 | .00 | .00   | .00   |
| 5 H 5                 | 9.200            | .1771   | .2016  | .1324  | 3.892                                    | 3.063 | 5.641  | -1.112               | .000   | .000  | .00 | 36.00 | .00   |
| 6 RUL 6               | 20.249           | .2453   | .2441  | .0150  | 3.037                                    | 3.037 | 11.482 | .000                 | -.322  | .000  | .00 | .00   | .00   |
| 7 RLL 7               | 7.841            | .4534   | .4606  | .0565  | 2.322                                    | 2.322 | 8.752  | .929                 | -1.197 | .000  | .00 | .00   | .00   |
| 8 RF 8                | 1.953            | .0358   | .0338  | .0066  | 2.624                                    | 1.897 | 5.216  | 2.099                | -.697  | .000  | .00 | 8.40  | -6.10 |
| 9 LUL 9               | 20.249           | .2453   | .2441  | .0150  | 3.037                                    | 3.037 | 11.482 | .000                 | .322   | .000  | .00 | .00   | .00   |
| 10 LLL A              | 7.841            | .4534   | .4606  | .0565  | 2.322                                    | 2.322 | 8.752  | .929                 | 1.197  | .000  | .00 | .00   | .00   |
| 11 LF B               | 1.953            | .0358   | .0338  | .0066  | 2.624                                    | 1.897 | 5.216  | 2.099                | .697   | .000  | .00 | 8.40  | 6.10  |
| 12 RUA C              | 4.104            | .1065   | .1140  | .0233  | 1.975                                    | 1.975 | 6.898  | .000                 | -.240  | .000  | .00 | .00   | .00   |
| 13 RLA D              | 3.944            | .2453   | .2441  | .0150  | 1.756                                    | 1.756 | 9.499  | .000                 | .609   | 1.187 | .00 | .00   | .00   |
| 14 LUA E              | 4.104            | .1065   | .1140  | .0233  | 1.975                                    | 1.975 | 6.898  | .000                 | .240   | .000  | .00 | .00   | .00   |
| 15 LLA F              | 3.944            | .2453   | .2441  | .0150  | 1.756                                    | 1.756 | 9.499  | .000                 | -.609  | 1.187 | .00 | .00   | .00   |

| JOINT<br>J SYM PLOT JNT PIN | LOCATION(IN) - SEG(JNT) |       |       | LOCATION(IN) - SEG(J+1) |       |       | JOINT AXIS(DEG) - SEG(JNT) |       |      | JOINT AXIS(DEG) - SEG(J+1) |        |      |
|-----------------------------|-------------------------|-------|-------|-------------------------|-------|-------|----------------------------|-------|------|----------------------------|--------|------|
|                             | X                       | Y     | Z     | X                       | Y     | Z     | YAW                        | PITCH | ROLL | YAW                        | PITCH  | ROLL |
| 1 P M 1 0                   | -1.40                   | .00   | -2.31 | -2.30                   | .00   | 2.44  | .00                        | .00   | .00  | .00                        | 5.00   | .00  |
| 2 W N 2 0                   | -1.75                   | .00   | -.86  | -.36                    | .00   | 7.21  | .00                        | .00   | .00  | .00                        | 5.00   | .00  |
| 3 WP O 3 0                  | -.31                    | .00   | -7.47 | -1.00                   | .00   | 1.52  | .00                        | .00   | .00  | .00                        | 10.00  | .00  |
| 4 HP P 4 0                  | 1.15                    | .00   | -2.56 | .26                     | .00   | 2.37  | .00                        | .00   | .00  | .00                        | 10.00  | .00  |
| 5 RH Q 1 0                  | -.54                    | 2.14  | 1.60  | -.26                    | -1.93 | -7.24 | .00                        | .00   | .00  | .00                        | -45.00 | .00  |
| 6 RK R 6 1                  | -.25                    | .37   | 9.44  | .69                     | -.60  | -6.61 | .00                        | .00   | .00  | .00                        | 60.00  | .00  |
| 7 RA S 7 0                  | .37                     | -.75  | 9.36  | 1.35                    | -.35  | -2.73 | .00                        | 90.00 | .00  | .00                        | 10.00  | .00  |
| 8 LH T 1 0                  | -.54                    | -2.14 | 1.60  | -.26                    | 1.93  | -7.24 | .00                        | .00   | .00  | .00                        | -45.00 | .00  |
| 9 LK U 9 1                  | -.25                    | -.37  | 9.44  | .69                     | .60   | -6.61 | .00                        | .00   | .00  | .00                        | 60.00  | .00  |
| 10 LA V 10 0                | .37                     | .75   | 9.36  | 1.35                    | .35   | -2.73 | .00                        | 90.00 | .00  | .00                        | 10.00  | .00  |
| 11 RS W 3 0                 | -.97                    | 6.47  | -4.19 | .53                     | -.24  | -5.66 | .00                        | .00   | .00  | .00                        | -4.10  | .00  |
| 12 RE X 12 1                | -.63                    | -.41  | 5.46  | -.48                    | .30   | -6.89 | .00                        | .00   | .00  | .00                        | -70.00 | .00  |
| 13 LS Y 3 0                 | -.97                    | -6.47 | -4.19 | .53                     | .24   | -5.66 | .00                        | .00   | .00  | .00                        | -4.10  | .00  |
| 14 LE Z 14 1                | -.63                    | .41   | 5.46  | -.48                    | -.30  | -6.89 | .00                        | .00   | .00  | .00                        | -70.00 | .00  |

CARDS B.4

JOINT TORQUE CHARACTERISTICS

| JOINT | FLEXURAL SPRING CHARACTERISTICS                  |                 |             |                          | TORSIONAL SPRING CHARACTERISTICS |  |                 |             |                          |                  |
|-------|--|-----------------|-------------|--------------------------|----------------------------------|--|-----------------|-------------|--------------------------|------------------|
|       | SPRING COEF. ( IN. LB. / DEG**J)<br>LINEAR (J=1) | QUADRATIC (J=2) | CUBIC (J=3) | ENERGY DISSIPATION COEF. | JOINT STOP (DEG)                 | SPRING COEF. ( IN. LB. / DEG**J)<br>LINEAR (J=1) | QUADRATIC (J=2) | CUBIC (J=3) | ENERGY DISSIPATION COEF. | JOINT STOP (DEG) |
| 1 P   | .000   | 10.000          | .000        | .700                     | 20.000                           | .000   | 10.000          | .000        | .700                     | 5.000            |
| 2 W   | .000   | 10.000          | .000        | .700                     | 20.000                           | .000   | 10.000          | .000        | .700                     | 35.000           |
| 3 NP  | .000   | 5.000           | .000        | .700                     | 25.000                           | .000   | 10.000          | .000        | .700                     | 35.000           |
| 4 HP  | .000   | 5.000           | .000        | .700                     | 25.000                           | .000   | 10.000          | .000        | .700                     | 35.000           |
| 5 RE  | .000   | 10.000          | .000        | .700                     | 70.000                           | .000   | .800            | .000        | .700                     | 40.000           |
| 6 RK  | .000   | 1.800           | .000        | .700                     | 60.000                           | .000   | .000            | .000        | .000                     | .000             |
| 7 RA  | .000   | 7.000           | .000        | .700                     | 35.000                           | .000   | 10.000          | .000        | .700                     | 26.000           |
| 8 LE  | .000   | 10.000          | .000        | .700                     | 70.000                           | .000   | .800            | .000        | .700                     | 40.000           |
| 9 LK  | .000   | 1.800           | .000        | .700                     | 60.000                           | .000   | .000            | .000        | .000                     | .000             |
| 10 LA | .000   | 7.000           | .000        | .700                     | 35.000                           | .000   | 10.000          | .000        | .700                     | 26.000           |
| 11 RS | .000   | 10.000          | .000        | .700                     | 122.500                          | .000   | 10.000          | .000        | .700                     | 65.000           |
| 12 RE | .000   | 1.800           | .000        | .700                     | 70.000                           | .000   | .000            | .000        | .000                     | .000             |
| 13 LS | .000   | 10.000          | .000        | .700                     | 122.500                          | .000   | 10.000          | .000        | .700                     | 65.000           |
| 14 LE | .000   | 1.800           | .000        | .700                     | 70.000                           | .000   | .000            | .000        | .000                     | .000             |

CARDS B.5

JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

| JOINT | VISCOSITY CHARACTERISTICS       |                                    |  | LOCK-UNLOCK CONDITIONS                    |   |   | IMPULSE RESTITUTION COEFFICIENT |
|-------|---------------------------------|------------------------------------|--|---|---|---|---------------------------------|
|       | COEFFICIENT ( IN. LB. SEC./DEG) | COULOMB FRICTION COEF. ( IN. LB. ) | FULL FRICTION ANGULAR VELOCITY ( DEG/SEC.) | MAX TORQUE FOR A LOCKED JOINT ( IN. LB. ) | MIN TORQUE FOR UNLOCKED JOINT ( IN. LB. ) | MIN. ANG. VELOCITY FOR UNLOCKED JOINT ( RAD/SEC.) |                                 |
| 1 P   | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 2 W   | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 3 NP  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 4 HP  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 5 RE  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 6 RK  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 7 RA  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 8 LE  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 9 LK  | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 10 LA | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 11 RS | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 12 RE | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 13 LS | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |
| 14 LE | .100                            | .00                                | 30.00                                      | .00                                       | .00                                       | .00   | .00                             |

SEGMENT INTEGRATION CONVERGENCE TEST INPUT

| SEGMENT<br>NO. SYM | ANGULAR VELOCITIES<br>(RAD/SEC.) |               |               | LINEAR VELOCITIES<br>(IN./SEC.) |               |               | ANGULAR ACCELERATIONS<br>(RAD/SEC.**2) |               |               | LINEAR ACCELERATIONS<br>(IN./SEC.**2) |               |               |
|--------------------|----------------------------------|---------------|---------------|---------------------------------|---------------|---------------|--|---------------|---------------|---------------------------------------|---------------|---------------|
|                    | MAG.<br>TEST                     | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                    | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                           | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                          | ABS.<br>ERROR | REL.<br>ERROR |
| 1                  | LT                               | .010          | .010          | .0100                           | .010          | .010          | .100                                   | .100          | .1000         | .100                                  | .100          | .0100         |
| 2                  | CT                               | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 3                  | UT                               | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 4                  | N                                | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 5                  | H                                | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 6                  | RUL                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 7                  | RLI                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 8                  | RF                               | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 9                  | LUL                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 10                 | LLL                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 11                 | LF                               | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 12                 | RUA                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 13                 | RLA                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 14                 | LUA                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |
| 15                 | LLA                              | .010          | .010          | .0100                           | .000          | .000          | .100                                   | .100          | .1000         | .000                                  | .000          | .0000         |

SAMPLE SEVENTEEN SEGMENT OUTPUT

ADULT HUMAN MALE

SELECTED BODY DIMENSIONS

|                 |       |     |
|-----------------|-------|-----|
| WEIGHT          | 168.5 | LB. |
| STANDING HEIGHT | 68.10 | IN. |

COMPUTED BODY DIMENSIONS

|    |                          |       |     |
|----|--------------------------|-------|-----|
| 0  | WEIGHT                   | 168.5 | LB. |
| 1  | STANDING HEIGHT          | 68.10 | IN. |
| 2  | SHOULDER HEIGHT          | 55.66 | IN. |
| 3  | ARMPIT HEIGHT            | 49.66 | IN. |
| 4  | WAIST HEIGHT             | 40.69 | IN. |
| 5  | SEATED HEIGHT            | 36.00 | IN. |
| 6  | HEAD LENGTH              | 7.783 | IN. |
| 7  | HEAD BREADTH             | 6.127 | IN. |
| 8  | HEAD TO CHIN HEIGHT      | 8.885 | IN. |
| 9  | NECK CIRCUMFERENCE       | 15.06 | IN. |
| 10 | SHOULDER BREADTH         | 15.87 | IN. |
| 11 | CHEST DEPTH              | 9.635 | IN. |
| 12 | CHEST BREADTH            | 12.84 | IN. |
| 13 | WAIST DEPTH              | 8.791 | IN. |
| 14 | WAIST BREADTH            | 12.11 | IN. |
| 15 | BUTTOCK DEPTH            | 9.416 | IN. |
| 16 | HIP BREADTH, STANDING    | 13.74 | IN. |
| 17 | SHOULDER TO ELBOW LENGTH | 13.80 | IN. |
| 18 | FOREARM-HAND LENGTH      | 19.00 | IN. |
| 19 | BICEPS CIRCUMFERENCE     | 12.41 | IN. |
| 20 | ELBOW CIRCUMFERENCE      | 12.16 | IN. |
| 21 | FOREARM CIRCUMFERENCE    | 11.03 | IN. |
| 22 | WRIST CIRCUMFERENCE      | 6.861 | IN. |
| 23 | KNEE HEIGHT, SEATED      | 21.36 | IN. |
| 24 | THIGH CIRCUMFERENCE      | 23.10 | IN. |
| 25 | UPPER LEG CIRCUMFERENCE  | 15.06 | IN. |
| 26 | KNEE CIRCUMFERENCE       | 15.30 | IN. |
| 27 | CALF CIRCUMFERENCE       | 14.59 | IN. |
| 28 | ANKLE CIRCUMFERENCE      | 8.755 | IN. |
| 29 | ANKLE HEIGHT, OUTSIDE    | 5.247 | IN. |
| 30 | FOOT BREADTH             | 3.794 | IN. |
| 31 | FOOT LENGTH              | 10.43 | IN. |
| 32 | HAND BREADTH             | 3.460 | IN. |
| 33 | HAND LENGTH              | 7.374 | IN. |
| 34 | HAND DEPTH               | 1.077 | IN. |

WEIGHT CORRECTION FACTOR = .963

SAMPLE SEVENTEEN SEGMENT OUTPUT

CRASH VICTIM PARAMETERS (3-D)

| SEGMENT<br>I SYM PLOT | WEIGHT<br>(LB.) | PRINCIPAL MOMENT OF INERTIA<br>(LB-SEC**2-IN) |        |        | SEGMENT CONTACT ELLIPSOID<br>CENTER (IN) |        |       | PRINCIPAL AXES (DEG) |        |        |        |       |        |       |       |
|-----------------------|-----------------|---|--------|--------|--|--------|-------|----------------------|--------|--------|--------|-------|--------|-------|-------|
|                       |                 | X   | Y      | Z      | X  | Y      | Z     | YAW                  | PITCH  | ROLL   |        |       |        |       |       |
| 1                     | LT              | 1   | 24.444 | .8965  | .8257                                    | 1.0458 | 4.708 | 6.871                | 3.548  | -4.71  | .000   | .352  | .00    | .00   | .00   |
| 2                     | CT              | 2   | 5.109  | .1431  | .0813                                    | .2176  | 4.396 | 6.055                | 3.893  | -1.465 | .000   | -.411 | .00    | .00   | .00   |
| 3                     | UT              | 3   | 51.324 | 4.1149 | 3.0331                                   | 2.6163 | 4.817 | 6.419                | 6.735  | .000   | .000   | .000  | .00    | 14.40 | .00   |
| 4                     | N               | 4   | 2.242  | .0152  | .0185                                    | .0231  | 2.396 | 2.396                | 2.977  | -.479  | .000   | 1.719 | .00    | .00   | .00   |
| 5                     | H               | 5   | 9.200  | .1771  | .2016                                    | .1324  | 3.892 | 3.063                | 5.641  | -1.112 | .000   | .000  | .00    | 36.00 | .00   |
| 6                     | RUL             | 6   | 20.249 | 2.453  | 2.441                                    | .0150  | 3.037 | 3.037                | 11.482 | .000   | -.322  | .000  | .00    | .00   | .00   |
| 7                     | RL              | 7   | 7.841  | 4.534  | 4.606                                    | .0565  | 2.322 | 2.322                | 8.752  | .929   | -1.197 | .000  | .00    | .00   | .00   |
| 8                     | RF              | 8   | 1.953  | .0358  | .0338                                    | .0066  | 2.624 | 1.897                | 5.216  | 2.099  | -.697  | .000  | -4.00  | 8.40  | -6.10 |
| 9                     | LUL             | 9   | 20.249 | 2.453  | 2.441                                    | .0150  | 3.037 | 3.037                | 11.482 | .000   | .322   | .000  | .00    | .00   | .00   |
| 10                    | LLL             | A   | 7.841  | 4.534  | 4.606                                    | .0565  | 2.322 | 2.322                | 8.752  | .929   | 1.197  | .000  | .00    | .00   | .00   |
| 11                    | LF              | B   | 1.953  | .0358  | .0338                                    | .0066  | 2.624 | 1.897                | 5.216  | 2.099  | -.697  | .000  | 4.00   | 8.40  | 6.10  |
| 12                    | RUA             | C   | 4.104  | 1.065  | 1.140                                    | .0233  | 1.975 | 1.975                | 6.898  | .000   | -.240  | .000  | .00    | .00   | .00   |
| 13                    | RLA             | D   | 2.882  | .0698  | .0716                                    | .0111  | 1.756 | 1.756                | 5.812  | .000   | .449   | .000  | .00    | .00   | .00   |
| 14                    | RE              | E   | 1.062  | .0107  | .0087                                    | .0035  | .538  | 1.730                | 3.687  | .000   | 1.057  | .000  | -14.00 | 6.00  | -7.70 |
| 15                    | LUA             | F   | 4.104  | 1.065  | 1.140                                    | .0233  | 1.975 | 1.975                | 6.898  | .000   | .240   | .000  | .00    | .00   | .00   |
| 16                    | LLA             | G   | 2.882  | .0698  | .0716                                    | .0111  | 1.756 | 1.756                | 5.812  | .000   | -.449  | .000  | .00    | .00   | .00   |
| 17                    | LE              | H   | 1.062  | .0107  | .0087                                    | .0035  | .538  | 1.730                | 3.687  | .000   | -1.057 | .000  | 14.00  | 6.00  | 7.70  |

CARDS B.2

CARDS B.3

| JOINT<br>J SYM PLOT JNT PIN | LOCATION(IN) - SEG(JNT) |   |    | LOCATION(IN) - SEG(J+1) |       |       | JOINT AXIS(DEG) - SEG(JNT) |       |       | JOINT AXIS(DEG) - SEG(J+1) |       |      |     |        |     |
|-----------------------------|-------------------------|---|----|-------------------------|-------|-------|----------------------------|-------|-------|----------------------------|-------|------|-----|--------|-----|
|                             | X                       | Y | Z  | X                       | Y     | Z     | YAW                        | PITCH | ROLL  | YAW                        | PITCH | ROLL |     |        |     |
| 1                           | P                       | K | 1  | 0                       | -1.40 | .00   | -2.31                      | -2.30 | .00   | 2.44                       | .00   | .00  | .00 | 5.00   | .00 |
| 2                           | W                       | L | 2  | 0                       | -1.75 | .00   | -.86                       | -.36  | .00   | 7.21                       | .00   | .00  | .00 | 5.00   | .00 |
| 3                           | MP                      | M | 3  | 0                       | -.31  | .00   | -7.47                      | -1.00 | .00   | 1.52                       | .00   | .00  | .00 | 10.00  | .00 |
| 4                           | HP                      | N | 4  | 0                       | 1.15  | .00   | -2.56                      | .26   | .00   | 2.37                       | .00   | .00  | .00 | 10.00  | .00 |
| 5                           | RH                      | O | 1  | 0                       | -.54  | 2.14  | 1.60                       | -.26  | -1.93 | -7.24                      | .00   | .00  | .00 | -45.00 | .00 |
| 6                           | RK                      | P | 6  | 1                       | -.25  | .37   | 9.44                       | .69   | -.60  | -6.61                      | .00   | .00  | .00 | 60.00  | .00 |
| 7                           | RA                      | Q | 7  | 0                       | .37   | -.75  | 9.36                       | 1.35  | -.35  | -2.73                      | .00   | .00  | .00 | 10.00  | .00 |
| 8                           | LE                      | R | 1  | 0                       | -.54  | -2.14 | 1.60                       | -.26  | 1.93  | -7.24                      | .00   | .00  | .00 | -45.00 | .00 |
| 9                           | LK                      | S | 9  | 1                       | -.25  | -.37  | 9.44                       | .69   | .60   | -6.61                      | .00   | .00  | .00 | 60.00  | .00 |
| 10                          | LA                      | T | 10 | 0                       | .37   | .75   | 9.36                       | 1.35  | .35   | -2.73                      | .00   | .00  | .00 | 10.00  | .00 |
| 11                          | RS                      | U | 3  | 0                       | -.97  | 6.47  | -4.19                      | .53   | -.24  | -5.66                      | .00   | .00  | .00 | -4.10  | .00 |
| 12                          | RE                      | V | 12 | 1                       | -.63  | -.41  | 5.46                       | -.51  | .22   | -4.50                      | .00   | .00  | .00 | -70.00 | .00 |
| 13                          | RW                      | W | 13 | 0                       | .36   | -.00  | 6.22                       | .16   | .53   | -2.57                      | .00   | .00  | .00 | .00    | .00 |
| 14                          | LS                      | X | 3  | 0                       | -.97  | -6.47 | -4.19                      | .53   | .24   | -5.66                      | .00   | .00  | .00 | -4.10  | .00 |
| 15                          | LE                      | Y | 15 | 1                       | -.63  | .41   | 5.46                       | -.51  | -.22  | -4.50                      | .00   | .00  | .00 | -70.00 | .00 |
| 16                          | LW                      | Z | 16 | 0                       | .36   | .00   | 6.22                       | .16   | -.53  | -2.57                      | .00   | .00  | .00 | .00    | .00 |



JOINT TORQUE CHARACTERISTICS

CARDS B. 4

FLEXURAL SPRING CHARACTERISTICS

| JOINT | FLEXURAL SPRING CHARACTERISTICS |                 |             | TORSIONAL SPRING CHARACTERISTICS |                 |             | ENERGY DISSIPATION COEF. | JOINT STOP (DEG) | ENERGY DISSIPATION COEF. | JOINT STOP (DEG) |
|-------|---------------------------------|-----------------|-------------|----------------------------------|-----------------|-------------|--------------------------|------------------|--------------------------|------------------|
|       | SPRING COEF. (J=1) LINEAR       | QUADRATIC (J=2) | CUBIC (J=3) | SPRING COEF. (J=1) LINEAR        | QUADRATIC (J=2) | CUBIC (J=3) |                          |                  |                          |                  |
| 1 P   | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 20.000           | .700                     | 5.000            |
| 2 W   | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 20.000           | .700                     | 35.000           |
| 3 NP  | .000                            | 5.000           | .000        | .000                             | 5.000           | .000        | .700                     | 25.000           | .700                     | 35.000           |
| 4 RP  | .000                            | 5.000           | .000        | .000                             | 5.000           | .000        | .700                     | 25.000           | .700                     | 35.000           |
| 5 RH  | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 70.000           | .700                     | 40.000           |
| 6 RK  | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 60.000           | .000                     | .000             |
| 7 RA  | .000                            | 7.000           | .000        | .000                             | 7.000           | .000        | .700                     | 35.000           | .700                     | 26.000           |
| 8 LH  | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 70.000           | .700                     | 40.000           |
| 9 LK  | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 60.000           | .000                     | .000             |
| 10 LA | .000                            | 7.000           | .000        | .000                             | 7.000           | .000        | .700                     | 35.000           | .700                     | 26.000           |
| 11 RS | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 122.500          | .700                     | 65.000           |
| 12 RE | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 70.000           | .000                     | .000             |
| 13 RW | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 35.000           | .700                     | 45.000           |
| 14 LS | .000                            | 10.000          | .000        | .000                             | 10.000          | .000        | .700                     | 122.500          | .700                     | 65.000           |
| 15 LE | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 70.000           | .000                     | .000             |
| 16 LW | .000                            | 1.800           | .000        | .000                             | 1.800           | .000        | .700                     | 35.000           | .700                     | 45.000           |

JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

CARDS B. 5

| JOINT | VISCOUS CHARACTERISTICS       |                            |                             | LOCK-UNLOCK CONDITIONS                  |   |  | FULL FRICTION COEFF. (DEG/SEC.) | MAX TORQUE FOR A LOCKED JOINT ( INLB. ) | MIN TORQUE FOR UNLOCKED JOINT ( INLB. ) | MIN. ANG. VELOCITY FOR UNLOCKED JOINT (RAD/SEC.) | IMPULSE RESTITUTION COEFFICIENT |
|-------|-------------------------------|----------------------------|-----------------------------|---|---|--|---------------------------------|---|---|--|---------------------------------|
|       | COEFFICIENT ( INLB. SEC./DEG) | COULOMB FRICTION ( INLB. ) | ANGULAR VELOCITY (DEG/SEC.) | MAX TORQUE FOR A LOCKED JOINT ( INLB. ) | MIN TORQUE FOR UNLOCKED JOINT ( INLB. ) | MIN. ANG. VELOCITY FOR UNLOCKED JOINT (RAD/SEC.) |                                 |   |   |  |                                 |
| 1 P   | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 2 W   | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 3 NP  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 4 RP  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 5 RH  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 6 RK  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 7 RA  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 8 LH  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 9 LK  | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 10 LA | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 11 RS | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 12 RE | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 13 RW | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 14 LS | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 15 LE | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |
| 16 LW | .100                          | .00                        | 30.00                       | .00                                     | .00                                     | .00  | 30.00                           | .00                                     | .00                                     | .00  | .00                             |

SEGMENT INTEGRATION CONVERGENCE TEST INPUT

| SEGMENT<br>NO. SYM | ANGULAR VELOCITIES<br>(RAD/SEC.) |               |               | LINEAR VELOCITIES<br>( IN/SEC.) |               |               | ANGULAR ACCELERATIONS<br>(RAD/SEC.**2) |               |               | LINEAR ACCELERATIONS<br>( IN/SEC.**2) |               |               |
|--------------------|----------------------------------|---------------|---------------|---------------------------------|---------------|---------------|--|---------------|---------------|---------------------------------------|---------------|---------------|
|                    | MAG.<br>TEST                     | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                    | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                           | ABS.<br>ERROR | REL.<br>ERROR | MAG.<br>TEST                          | ABS.<br>ERROR | REL.<br>ERROR |
| 1                  | LT                               | .010          | .010          | .0100                           | .010          | .010          | .010                                   | .100          | .1000         | .100                                  | .100          | .0100         |
| 2                  | CT                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 3                  | UT                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 4                  | M                                | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 5                  | H                                | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 6                  | RUL                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 7                  | RLI                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 8                  | RF                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 9                  | LUL                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 10                 | LLL                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 11                 | LF                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 12                 | RUA                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 13                 | RLA                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 14                 | RE                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 15                 | LUA                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 16                 | LLA                              | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |
| 17                 | LH                               | .010          | .010          | .0100                           | .000          | .000          | .0000                                  | .100          | .1000         | .000                                  | .000          | .0000         |

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