



Report No. AMXTH-TE-CR-86091

Installation Restoration General Environmental Technology Development

Contract DAAK 11-82-C-0017 (Task Order 9)

Field Demonstration of Incinerator Feed System For Explosives-Contaminated Soils

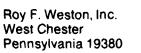
Volume 1 - Technical Report



January 1987

Distribution Unlimited; Approved for Public Release

Prepared for: U.S. ARMY TOXIC AND HAZARDOUS MATERIALS AGENCY Aberdeen Proving Ground (Edgewood Area), Maryland 21010





Unclassified

REPORT DOCUMENTATION		READ INSTRUCTIONS BEFORE COMPLETING FORM
. REPORT NUMBER	2. GOVT ACCESSION NO.	
AMXTH-TE-CR-86091		
. TITLE (and Subditio) Installation Rest	oration General	5. TYPE OF REPORT & PERIOD COVERED
Environmental Technology Dev		Technical Report
Field Demonstration of Incir		June 1984 - January 1987
System for Explosives-Contan	ninated Soils	6. PERFORMING ORG. REPORT NUMBER
-		
AUTHOR()		8. CONTRACT OR GRANT NUMBER(*)
Peter J. Marks		11-92-C-0017
John W. Noland, P.E.		DAAK 11-82-C-0017
PERFORMING ORGANIZATION NAME AND ADDRES	<u> </u>	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Roy F. Weston, Inc.		AREA & WORK UNIT NUMBERS
Weston Way		
West Chester, PA 19380		
1. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
U.S. Army Toxic & Hazardous M	Materials Agency	January 1987
Aberdeen Proving Ground		13. NUMBER OF PAGES
Edgewood Area, MD 21010		69 (Excluding Appendicies
14. MONITORING AGENCY NAME & ADDRESS(II dittor	nt from Controlling Office)	15. SECURITY CLASS. (of this report)
· · ·		Unclassified 15. DECLASSIFICATION/DOWNGRADING
		SCHEDULE
 DISTRIBUTION STATEMENT (of the obstract enforce) SUPPLEMENTARY NOTES Contract Project Officer - 		
19. KEY WORDS (Continue on reverse side if necessary		
Explosives-Contaminated Soil		÷ 1
Incineration Feed System	Feed Conveyor Soil Excavatio	Screw Conveyor Tongue on Motor Current
Materials Handling	Soil Excavation	1
Live Bottom Hopper	Soil Feedrate	Soil Size Distribution
20. ABSTRACT (Castlans en reverse alde # neurosant 4		
This report presents the resu evaluate the suitability of a explosives-contaminated soils Louisiana Army Ammunition Pla report presents the test vari data analysis, and conclusion implementation.	ults of field de an incinerator : s. The project ant from 30 June iables, schedule	emonstration project to feed system for conveying was conducted at the e to 10 July 1986. This e of tests and runs,
DD FORM 1473 EDITION OF ! NOV 55 IS OBS		
DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBS	Uncla	assified SSIFICATION OF THIS PAGE (Men Data Entered)

WESTER

CONTENTS

Page

			_
Paragraph		XECUTIVE SUMMARY	1
	1.1	Background	1
		NTRODUCTION	2
	2.1	Background	2
	2.2	Purpose	5
	2.3	Objectives	5
	2.4	Criteria for successful demonstration	5
	2.5	Test site description	5
	2.6	Test equipment	7
	2.6.1	Live bottom hopper	7
	2.6.2	Cross conveyor	11
	2.6.3	Feed conveyor	12
		EST VARIABLES	13
	3.1	Independent variables	13
	3.2	Control variables	13
	3.2.1	Held constant for all tests	13
	3.2.1.1	Soil excavation	13
	3.2.1.1.1	LAAP soil	13
	3.2.1.1.2	CHAAP soil	16
	3.2.1.2	Soil preparation	
	3.2.2		16
		Controlled at various levels	16
	3.2.2.1	Soil feed rate	18
	3.2.2.2	Duration of testing period	18
	3.3	Response variables	18
	3.3.1	Rotational speed of screw conveyor	18
	3.3.2	Screw conveyor torque	19
		CHEDULE OF TESTS AND RUNS	20
	4.1	Overall test schedule	20
	4.2	Test run sequence/schedule of daily	
		activities	20
		ATA ANALYSIS	27
	5.1	Presentation of CHAAP data	27
	5.1.1	4,000-lb/hr feed system test (Test	
		Run No. 1)	27
	5.1.2	8,000-lb/hr feed system test (Test	
		Runs Nos. 3 and 4)	27
	5.1.3	12,000-lb/hr feed system test (Test	
		Run No. 8)	27
	5.2	Presentation of LAAP data	27
	5.2.1	4,000-lb/hr feed system test (Test	
		Run No. 5)	27
	5.2.2	8,000-lb/hr feed system test (Test	
		Run No. 7)	27
	5.2.3	12,000-1b/hr feed system test (Test	
		Run No. 6)	27

CONTENTS

Paragraph	5.3	Analysis of test data	52
J 1	5.3.1	Soil feed rate	52
	5.3.2	Soil moisture content and bulk	•=
		densities	53
	5.3.3	Soil size distribution	54
	5.3.4	Rotational speed of screw conveyor	54
	5.3.5	Screw conveyor motor amps	58
	5.3.6	LAAP soils explosives concentrations	58
	5.4	Physical observations	58
	5.4.1	Soil excavation, staging, and feeding	
		to the hopper	58
	5.4.2	Live-bottom hopper operation	62
	5.4.3	Cross conveyor operation	62
	5.4.4	Feed conveyor operation	62
	5.4.5	Feed soil characteristics	63
	5.4.6	Control system operation	63
	5.4.7	Shaft purge system operation	63
		CONCLUSIONS AND RECOMMENDATIONS	б5
	6.1	Conclusions	65
	6.2	Recommendations	68

6

DTIC COPY NSPECTED Accesion For -----7 NTIS CENSI DTHO LUB Unacional code Justifie: "on By Distribution / Dist And the second second Dist i A-1 Ì

Page

	\mathbf{w}		Ŋ		
		FIGUR	ES		
'est	Site				

1.	Test Site	5
2.	Incinerator feed system	3
3.	Internal view of live bottom hopper	Э
4.	LAAP lagoon number 4	17
5.	Feed rate during Test Run No. 1, CHAAP	
	soil, 4,000 lb/hr	29
6.	Motor current during Test Run No. 1,	
	CHAAP soil, 4,000 lb/hr	30
7.	Feed rate during Test Run No. 3, CHAAP	
	soil, 8,000 lb/hr, 4-hour test	32
8.	Motor current during Test Run No. 3,	
•••	CHAAP soil, 8,000 lb/hr,	
	4-hour test	33
9.	Feed rate during Test Run No. 4, CHAAP	55
5.	soil, 8,000 lb/hr, 8-hour test	36
10.	Motor current during Test Run No. 4,	50
10.	CHAAP soil, 8,000 lb/hr,	
	8-hour test	27
		37
11.	Feed rate during Test Run No. 8, CHAAP	20
10	soil, 12,000 lb/hr	39
12.	Motor current during Test Run No. 8,	
	CHAAP soil, 12,000 lb/hr	40
13.	Feed rate during Test Run No. 5, LAAP	
	soil, 4,000 lb/hr	42
14.	Motor current during Test Run No. 5,	
	LAAP soil, 4,000 lb/hr	43
15.	Feed rate during Test Run No. 7, LAAP	
	soil, 8,000 lb/hr, 8-hour test	46
16.	Motor current during Test Run No. 7,	
	LAAP soil, 8,000 lb/hr,	
	8-hour test	47
17.	Feed rate during Test Run No. 6, LAAP	
	soil, 12,000 lb/hr	50
18.	Motor current during Test Run No. 6,	
	LAAP soil, 12,000 lb/hr	51
19.	Relationship between live bottom hopper	
	screw speed and variable speed drive	
	settings for all types of soil	56
20.	Relationship between conveyor and feed	
	conveyor screw speeds and variable	
	speed drive settings for all types	
	of soil	57
21.	Motor current for CHAAP soil test	
	runs	59
22.	Motor current for LAAP soil test	
	runs	60
		~ ~

TABLES

	1
1.	List/description of appendices in
	Volume II
2.	Summary of feed system experimental variables
3.	Characteristics of explosives- contaminated soils
4.	Schedule of test runs
5.	Feed systems operational safety controls upset - and/or failure-mode testing
6.	Summary of test data for Test Run No. 1, CHAAP soil, 4,000 lb/hr
7.	Summary of test data for Test Run No. 3, CHAAP soil, 8,000 lb/hr,
	4-hour test

Page

3

14

15 21

23

28

31

34

38

41

44

48

55

61

66

6 7 Summary of test data for Test Run No. 8. 4, CHAAP soil, 8,000 lb/hr, 8-hour test Summary of test data for Test Run No. 9. 8, CHAAP soil, 12,000 lb/hr 10. Summary of test data for Test Run No. 5, LAAP soil, 4,000 lb/hr Summary of test data for Test Run No. 11. 7, LAAP soil, 8,000 lb/hr 12. Summary of test data for Test Run No. 6, LAAP soil, 12,000 lb/hr Summary of soil size distribution data 13. for the CHAAP test runs Summary of soil explosives 14. concentrations for the LAAP test runs Recommendations from the ABL's hazards 15.

analysis of incinerator feed

system (Appendix D)

TABLE



1. EXECUTIVE SUMMARY

Background. A field demonstration 1.1 project was Louisiana Army Ammunition Plant conducted at (LAAP) near suitability of Shreveport, Louisiana to evaluate the an incinerator feed system for conveying explosives-contaminated soils. The field demonstration project was conducted from 30 10 July 1986. Explosives-contaminated soils were June to excavated from Lagoon No. 4 at LAAP for testing. (Total explosives content typically ranged from 10 to 22 percent by In addition, uncontaminated background soils weight.) from Cornhusker Army Ammunition plant (CHAAP) near Grand Island, Nebraska were also excavated and transported to LAPP for testing. Soils discharged from the system were deposited in Lagoon No. 12 at LAAP.

The incinerator feed system consisted of the following three major components:

- (a) Live bottom hopper The live bottom hopper consisted of a loading bin with four cone metering screws in the bottom to control the soil feed rate.
- (b) <u>Cross conveyor</u> The soil from the live bottom hopper discharged into a twin-screw cross conveyor which transferred the soil horizontally from the live bottom hopper to the feed conveyor.
- (c) Feed conveyor In future applications, a water-jacketed twin-screw conveyor will directly feed a rotary kiln incinerator. However, for this testing program, the feed conveyor discharged into an excavation container for transport of the soils back to the lagoon at LAAP.

The field testing evaluated three levels of soil feed rate (i.e., 4,000 lb/hr, 8,000 lb/hr, and 12,000 lb/hr) and two test durations (i.e., 4-hour runs and one 8-hour steady-state run for each soil type). In addition, testing was also performed under upset and/or failure-mode conditions.

This testing program successfully demonstrated the capability of the feed system to consistently deliver 50 percent, 100 percent, and 150 percent of the 8,000 lb/hr design feed rate with two very different soil types. The feed system proved to be capable of conveying solid debris in the soil (i.e., chunks of concrete) up to 6 inches x 6 inches x 6 inches in dimension without jamming the system. The failure mode testing successfully demonstrated that the control system responded as designed to all simulated jams and motor overload conditions.



2. INTRODUCTION

2.1 <u>Background</u>. As a result of past munitions-handling operations, the U.S. Army has numerous lagoons which contain varying amounts of explosives-contaminated sludge. Rotary kiln incineration has been identified and demonstrated as a treatment technology for explosives-contaminated sludge. Prior to the performance of this task order, no safety-approved feed system existed for explosives-contaminated sludge. However, a safety-approved feed system will be required before incineration can be used in the field to decontaminate these sludges.

This report describes the full-scale field demonstration of the safety-approved feed system completed in July 1986. However, the incinerator feed system development was initiated in September 1982 under WESTON's Task Order No. 2 which involved the field demonstration of a pilot scale incineration system for explosives-contaminated soils. To document the chronology of the feed system development, Table 1 presents a list of appendices provided in Volume 2 of this report.

In addition to these appendices, three specific documents directly related to this project were prepared by WESTON and were submitted to USATHAMA. These documents are included by reference only:

Document title	Date submitted to USATHAMA
Test Plan for Propagation and Flame Testing of Explosives-Contaminated Lagoon Soil at Los Alamos National Laboratory (LANL)	March 1985
Safety Plan for a Materials Handling System Test of Explosives-Contaminted Soils at the Louisiana Army Ammunition Plant (LAAP)	June 1985



TABLE 1. LIST/DESCRIPTION OF APPENDICES IN VOLUME II

Appendix		Title/description	
A	Title:	Summary of Incinerator Feed System Development	
		Letter from P. J. Marks to W. E. Sisk dated 20 February 1985. This letter (with attachments) provides an overview of the various designs considered and describes the planned development and testing activities.	
В	Title:	Tests for Propagation of Explosions in Explosives-Contaminated Lagoon Soils	
		This report presents the results of propagation testing conducted by Los Alamos National Laboratories (LANL) on explosives-contaminated lagoon soils from Louisiana Army Ammunition Plant (LAAP), Cornhusker Army Ammunition Plant (CHAAP), and Savanna Army Depot Activity (SADA). This testing was performed to determine if the contaminated soils will propagate an explosive event.	
С	Title:	Flame Testing of Incinerator Feed System Handling Explosives-Contaminated Lagoon Soils	
		This report presents the results of flame testing conducted by LANL on explosives- contaminated lagoon soils from LAAP. The purpose of this testing was to investi- gate the potential for fire or explosion to occur in the feed system due to exposure to the incinerator environment during upset conditions.	



TABLE 1. (CONTINUED)

Appendix		Title/description	
D	Title:	Hazards Analysis of Incinerator Feed System This document presents the results of a Subsystem Hazard Analysis (SSHA) of the incinerator feed system to ensure that the explosives-contaminated lagoon soils can safely be fed to an incinerator while minimizing the risk of injury to operating personnel and equipment damage. This report was supported by sensitivity tests of dried explosives-contaminated lagoon sludges from LAAP, CHAAP, and SADA.	



2.2 <u>Purpose</u>. The purpose of this report is to present the results and conclusions of a field demonstration project that evaluated an incinerator feed system for handling explosivescontaminated soils. A description of test conditions and process equipment is contained herein.

2.3 <u>Objectives</u>. The primary objective of the field demonstration project was to evaluate the suitability of the materials handling feed system for feeding explosivescontaminted soils into a rotary kiln incinerator. Secondary objectives included the following:

- (a) Determination of the impact on system performance of varying design parameters (e.g., soil feed rate, soil moisture content, soil composition, and maximum soil topsize).
- (b) Determination of the optimum range of operational parameters.
- (c) Determination of equipment limitations and failure modes to identify a clear envelope of safe and practical system operation.
- (d) Identification of equipment modifications that would improve system performance, reliability, and/or operational safety.

2.4 <u>Criteria for successful demonstration</u>. The success of the field demonstration project was based upon the ability of the materials handling and feed system to safely and reliably process a minimum of 8,000 lb/hr of explosives-contaminated soils from two installations: LAAP and CHAPP.

2.5 <u>Test site description</u>. The field demonstration project was conducted at LAAP in Shreveport, Louisiana. The location of the test site and the pink water lagoons is shown on Figure 1.

Originally, field demonstration projects were also to be conducted at CAAP near Grand Island, Nebraska and SADA near Savanna, Illinois. However, demonstrations at these installations were not conducted for the following reasons:

- (a) Full erection and disassembly of the feed system at each location would be too costly and time-consuming.
- (b) LAAP soils represented "worst case" conditions, as follows:
 - (1) The LAAP soils were the most highly contaminated, exhibiting explosives concentations as high as 45 percent by weight.
 - (2) The high concentration of explosives made it undesirable to transport LAAP soils to another site for testing.

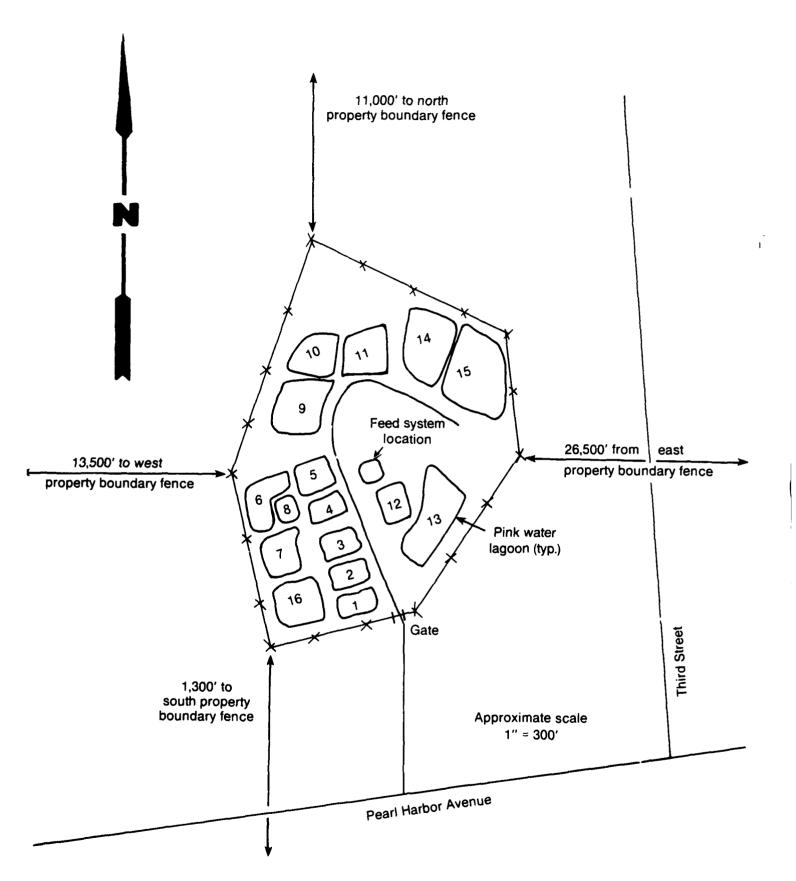


Figure 1. Test Site.

- (3) The physical properties of LAAP soils (i.e., highly plastic clay) presented the greatest materials handling challenge to the feed system.
- Although testing was not to be conducted at CHAAP, (C) from CHAAP had to be tested because this soils installation is an immediate candidate for cleanup via rotary-kiln incineration. However, due to potential delays involved with transporting regulatory soils, background explosives-contaminated (uncontaminated) soils were transported to LAAP for testing.
- (d) SADA soils were not tested because there was no apparent advantage in doing so. SADA soils are sandy; therefore, they would not present a significant materials handling problem (as compared to the highly plastic clay soils at LAAP). In addition, explosives concentrations were much lower than those associated with LAAP soils.

2.6 <u>Test equipment</u>. The incinerator feed system consisted of the following three major components:

- (a) Live-bottom hopper.
- (b) Cross conveyor.
- (c) Feed conveyor.

A photograph of the incinerator feed system installed at LAAP is presented in Figure 2. A description of each component, specifications, and construction details are contained in the following subsections.

2.6.1 Live bottom hopper. Excavated soils were fed to the live bottom hopper using a tracked excavator (see Appendix E). The bottom of the hopper was equipped with four cone metering screws. The cone metering screws were selected because they have been proven in other applications to provide the most consistent and reliable method of feed rate control and to minimize the potential for hopper bridging. The hopper was designed to handle a maximum of 18,000 pounds of soil per hour. A photograph of the four metering screws in the bottom of the live bottom hopper is shown in Figure 3. The specification and construction of the hopper are described as follows:

Screws were 12 inches in diameter and of the "cone" displacement design with solid flights on the cone and ribbon flights on the balance of the screws. Ribbon flights were selected since they have proven to be the most reliable for handling clay soils. The screw shaft was 5-inch Schedule 120 (1/2-inch wall) bushed to 3 15/16-inch shaft size. The ribbon flights were 2 1/2 inch x 1/2 inch thick; posts were 2 inch x 1/2 inch at degrees around the shaft. The ribbon 120 was hard-faced with stellite on the outer edge and face.

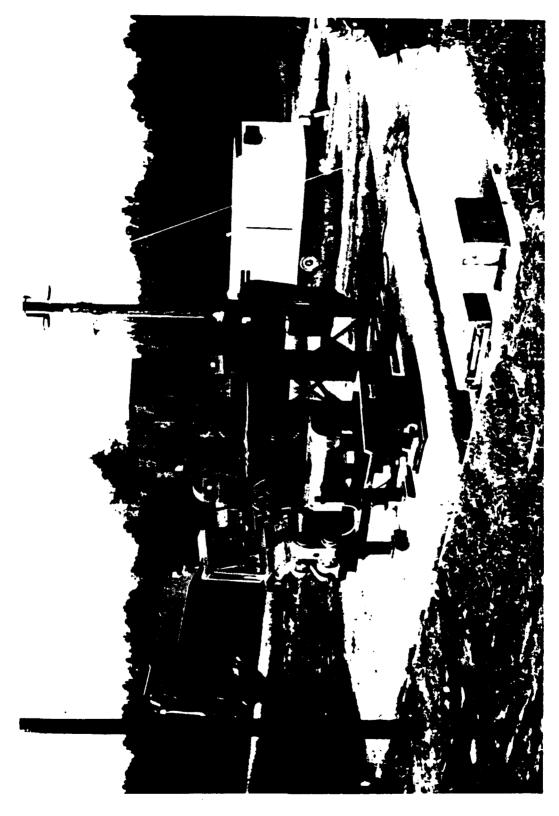


Figure 2. Incinerator feed system.



Figure 3. Internal view of live bottom hopper.

- The screws were counter-rotating, right- and left-hand flighting driven by steel spur gears, No. 3 diametrical pitch (DP) with a 3-inch face mounted on 3 15/16-inch drive shafts. Counter-rotating twin screws were also selected since they have proven to be the most reliable for handling clay soils. Final screw speed was 5 rpm maximum with a 9 to 1 turndown.
- The trough for the quad screw feeder was 1/4-inch plate with external reinforcing ribs and bracing. The inside of the trough had "hip-roof" dividers between the screws.
- The trough ends were 3/8-inch plate, with external pedestals for the bearing supports. The spur gears were straddle-mounted by bearings.
- The drive was a 15-hp, totally enclosed, fan cooled (TEFC) with a 9 to 1 variable speed reducer coupled to an in-line reducer. A chain drive connected the reducer and one of the center feed-screw drive shafts. The drive was mounted directly to the feeder and included all Occupational Safety and Health Act (OSHA) approved guards for the gears and the chain drive.
- A bin was permanently mounted over the top of the four metering screws as part of the live bottom hopper. This bin was 4 feet x 6 feet x 4 feet. The bin walls tapered to provide at least 2 degrees negative pitch to prevent bridging in the hopper. The walls were reinforced by ribbing and by 3-inch x 3-inch x 3/8-inch angles. A "breaker bar" grid was placed near the top of the bin to break large lumps and to protect personnel.



- The entire feeder and bin were mounted on 8-inch x 31 1b H beams that supported this equipment approximately 9 feet above the base plate of the support columns. The support steel was all of bolted construction.
- The equipment was completely assembled and tested in the fabricator's plant prior to shipping. The equipment received one coat of primer and a finish coat of epoxy paint.
- All screw conveyor shaft seals where the shafts penetrated the conveyor housing were oil purged to prevent the migration of explosives into the bearing assemblies.

2.6.2 Cross conveyor. Soils were discharged from the live bottom hopper and dropped approximately 2 feet to the feed end of the cross conveyor. This 2-foot drop at conveyor transfer points was included in the design to preclude the propagation of an explosion from one conveyor to another. The twin screw cross conveyor was equipped with right- and left-hand counter-rotating screws. The screws were 12 inches in diameter and 12-1/2 feet long. The components of the cross conveyor were as follows:

- 12-inch diameter ribbon flights, 2-1/2 inch x 1/2-inch ribbon-mounted on 5-inch Schedule 120 pipe bushed for 3-inch diameter shafts. No internal hanger bearing.
- The screws were driven by steel spur gears, 3-inch DP with a 3-inch face.
- The trough was 1/4-inch plate with a 3/16-inch plate cover.
- Trough ends were 3/8-inch plate, outboard pedestalbearing supports, and straddle-mounted bearings at the spur gears.
- The drive was a 7 1/2-hp TEFC U.S. Reliance varispeed drive. There was a No. 100 chain drive to the screw conveyor drive shaft. Final top speed of the screw was 15 rpm with a 9 to 1 turndown.
- Complete motor mount was provided and directly fastened to the conveyor. The gearing and the chain drive had OSHA guards.
- All screw conveyor shaft seals where the shafts penetrated the conveyor housing were oil purged to prevent the migration of explosives into the bearing assemblies.



2.6.3 Feed conveyor. Soils discharged from the cross conveyor and dropped approximately 2 feet to the feed end of the feed conveyor. This twin-screw feeder will ultimately feed soils to a rotary kiln incinerator. For the field demonstration program, however, the feed conveyor discharged soils into self-dumping steel hoppers for transport back to the lagoon (see Appendix F). The components of the feed conveyor were as follows:

- The construction and specifications for the feed conveyor are the same as those presented for the cross conveyor (as discussed in Subsection 2.6.2). The unit was 6 feet in length and was fabricated of Inconel 625.
- The inner and the outer housings were 1/4-inch plate. Interior baffles between the inner housing and the outer jacket were designed to direct the water in a circular pattern, starting at the feed end and returning through the inside of the screw shafts from the discharge end of the conveyor.
- The two screws had water-cooled center pipes (the axles). The connection was a Johnson coupling with input and output through the same end. No cooling water was circulated for this project.
- The screws were driven by a 15-hp TEFC varispeed motor and reducer identical to the unit described for the live-bottom hopper, except that the maximum speed was 15 rpm with a 9 to 1 turndown.
- The screws were overhung from the two bearings on the drive end. They also had a stabilizing bearing on the inside of the discharge end which was a dry sleeve bearing made of carbon-ceramic material suitable for very high temperatures. The shaft riding in this sleeve bearing was Inconel 625 with an overlap of stellite. These bearings had renewable inserts and were only for stabilizing the discharge end by absorbing some of the side thrust.
- All screw conveyor shaft seals where the shafts penetrated the conveyor housing were oil purged to prevent the migration of explosives into the bearing assemblies.



3. TEST VARIABLES

The variables of the testing program can be classified as follows:

- (a) Independent variables. Those whose value was fixed for test operations. No attempts were made to modify or control independent variables.
- (b) Control variables. Those whose value was selected and maintained during test operations.
- (c) Response variables. Those whose value was a function of the selected operating conditions.

Table 2 provides a summary of test variables for the incinerator feed system field demonstration program.

3.1 <u>Independent variables</u>. As shown in Table 2, there were two independent variables associated with the field demonstration program at each potential remedial action site: soil explosives concentration and soil composition. A summary of the soil explosives concentrations and compositions for each of the two installations based upon previous data appears in Table 3. Again, although CHAAP soils are contaminated, soils chosen for testing were uncontaminated. Soil physical properties, however, were very similar for both.

3.2 Control variables.

3.2.1 Held constant for all tests. As shown in Table 2, two control variables (soil excavation and soil preparation) were held constant for all of the tests.

3.2.1.1 Soil excavation.

3.2.1.1.1 LAAP soil. The selection of LAAP Lagoon No. 4 for excavation the soil for the testing program was based upon the following criteria:

- LAAP Lagoon No. 4 had free-standing water which ensured that the soil was saturated and minimized the risk of potential functioning of the explosivescontaminated soil during excavation.
- LAAP Lagoon No. 4 had adequate access for excavation operations and an adequate supply of uncontaminated water available nearby for washdown and equipment decontamination.
- LAAP Lagoon No. 4 was located as close as practical to the selected site for installation of the feed system to minimize transportation distances.



TABLE 2. SUMMARY OF FEED SYSTEM EXPERIMENTAL VARIABLES

A. INDEPENDENT VARIABLES

- Soil explosives concentration
- Soil composition

B. <u>CONTROL VARIABLES</u>

- Held constant for all tests
 - Soil excavation
 Soil preparation
- Controlled at various levels
 - Soil feed rate
 - Duration of test

C. <u>RESPONSE VARIABLES</u>

- Rotational speed of screw conveyors
 - Live-bottom hopper
 - Cross conveyor
 - Feed conveyor
- Screw conveyor torque (i.e., motor amps)
 - Live-bottom hopper
 - Cros conveyor
 - Feed conveyor
- Physical observations



TABLE 3. CHARACTERISTICS OF EXPLOSIVES-CONTAMINATED SOILS

Description	Cornhusker Army Ammunition Plant ^{1,2} (CHAAP)	Louisiana Army Ammunition Plant ³ (LAAP)
Soil matrix	Silty clay	Clay
Moisture content	Unknown	25 - 30%
Ash content (as received)	Unknown	54 - 66%
Explosives content (dry basis)		
- TNT	<3.8%	5 - 14%
- RDX	Not detected	3 - 10%
– HMX	Not detected	0.6 - 1.4%
- Other	< 0.2%	<0.06%
- Total explosives	< 4%	10 - 22%
Heating value	Unknown	600 - 1,200 Btu/lt

¹Based on sampling results from "Cornhusker Army Ammunition Plant," Final Report, Report No. DRXTH-AS-CR-82155, August 1982.

²Note: Uncontaminated soils from CHAAP exhibiting similar physical characteristics were used for testing the feed system. ³Based on sampling results from "Task 2. Incineration Test of Explosives-Contaminated Soils at Savanna Army Depot Activity, Savanna, Illinois," Final Report, Report Number DRXTH-TE-CR-84277, April 1984.



A photograph of LAAP Lagoon No. 4 is shown in Figure 4. the saturated soil was removed from Lagoon No. 4 using a tracked excavator (see Appendix E). The tracked excavator loaded the saturated soil into a 12-cubic yard capacity dump truck. The dump truck bed was elevated at an approximate 20-degree angle to promote draining of free liquid through the tail gate, allowing the liquid to drain directly back into Lagoon No. 4. After allowing adequate time for drainage of free liquid (typically overnight), the truck dumped the excavated soil into the bermed feed soil staging area adjacent to the test site.

3.2.1.1.2 CHAAP Soil. CHAAP soil excavated was and transported to the LAAP site in two 12-cubic yard capacity dump trucks. то avoid potential regulatory delays due to explosives-contaminated soils, uncontaminated transporting background soil was used. The soil was dumped at a staging area the test site and covered with visquene to minimize near moisture loss or gain. Prior to beginning the testing program the soil was loaded into the dump truck using the tracked excavator and transported to a separate bermed staging area adjacent to the test site.

Soil preparation. From this point on, the LAAP and 3.2.1.2 CHAAP soils were handled in exactly the same manner. The soils were reclaimed from the feed soil staging area by the tracked of excavator. The operator used the bucket the tracked excavator to sift through the soil and identify any large debris that would require removal. A technician assisted the operator by manually removing any oversized debris. The technician also collected a grab sample from each bucket load to form a composite feed sample for each test run. The purpose of the composite feed sample was to allow analysis of feed soil size distribution, and explosives moisture content, soil content (LAAP soils only).

The tracked excavator then loaded the reclaimed feed soil directly into the live-bottom hopper. Soil spills were quickly washed into a drainage trench using a fire hose. The drainage trench discharged directly into pink water Lagoon No. 12. As an explosion and fire hazard safety precaution, the fire hose was also used to ensure that all mechanical equipment in contact with the explosives-contaminated soil remained wet.

3.2.2 Controlled at various levels. The two variables that were controlled at various levels to evaluate the impact upon system performance were soil feed rate and duration of the testing period.

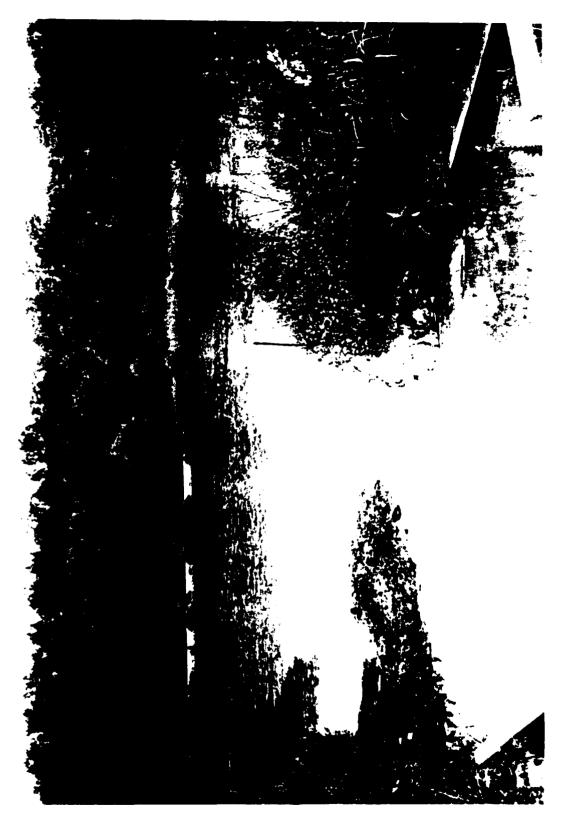


Figure 4. LAAP lagoon no. 4.



3.2.2.1 Soil feed rate. The design soil feed rate for the materials handling feed system was 8,000 lb/hr. However, to fully evaluate the performance of the system, response variables were also measured at soil feed rates of 50 percent of the design rate (4,000 lb/hr) and 150 percent of the design rate (12,000 lb/hr). This allowed evaluation of system performance over the expected range of operation.

3.2.2.2 Duration of testing period. Generally, the test duration was 4 hours of continuous operation. For both soil types, however, one test run was conducted at the design feed rate (8,000 lb/hr) for 8 hours of continuous operation. The purpose of this longer duration testing was to evaluate how the system would perform over a typical operating shift rotation.

3.3 <u>Response variables</u>. Two response variables were measured separately for each of the three major system components, as shown in Table 2. They were the rotational speed of the screw conveyors and the screw conveyor torques (measured as motor amps) for each of the following:

- (a) Live bottom hopper.
- (b) Cross conveyor.
- (c) Feed conveyor.

3.3.1 Rotational speed of screw conveyors. The rotational speed of the screw conveyors is an important parameter since it relates directly to the conveyor tip speed. Allegany Ballistics Laboratory (see Appendix D) recommended that the conveyor tip speeds be maintained below 2 feet per second when handling explosives-contaminated soils. A summary of the potential rotational speeds and design operating range for each conveyor section of the feed system is provided below:

Description	Live bottom hopper	Cross conveyor	Feed conveyor
Range of settings for variable speed drive	0 - 7	0 - 7	0 - 7



Description	Live bottom hopper	Cross conveyor	Feed conveyor
Conveyor rotation speeds correspondin to the foregoing variable speed drive setting:	g		
Revolutions per minute (rpm)	0.6 - 4.2	16 - 88	18 - 106
Conveyor tip speed (ft/sec)	0.03 - 0.21	0.8 - 4.4	0.9 - 5.3
Conveyor rotational speeds used during the testing program			
Revolutions per minute (rpm)	1.0 - 3.2	16 - 26	18 - 32
Conveyor tip speed (ft/sec)	0.03 - 0.17	0.8 - 1.3	0.9 - 1.6

Due to the relatively slow rotational speed of the screw conveyors, this response variable was measured by direct visual observation. Physical observation (i.e., counting the revolutions), combined with use of a stop watch to ensure accurate timing, allowed accurate estimation of screw conveyor rotational speeds.

3.3.2 Screw conveyor torque. Torque for each of the conveyors was measured indirectly by recording the respective drive motor current readings (in amperes) directly from the meters for each drive motor located on the control panel.

-19-



4. SCHEDULE OF TESTS AND RUNS

To maximize the information gained and minimize the downtime during the pilot study, the schedule of testing activities was carefully planned. The objective of this section is to outline the following:

- (a) Overall test schedule.
- (b) Test run sequence/schedule of daily activities.

Overall test schedule. A schedule of test runs and 4.1 soil type, feed rate, and test duration are shown on Table 4. As shown, test run No. 2 was not completed. During operation, a switch on the cross conveyor malfunctioned (i.e., limit indicated motor amps on cross conveyor were above the set point) and resulted in repeated shutdowns of the hopper conveyor. The reason for the shutdowns was not immediately apparent and much time was spent in investigating the problem. Consequently, there was insufficient time to complete a 4-hour test run. It was decided to rerun this test at the end of the project (as Test Run No. 8). The limit switch was properly adjusted and resulted in no further system shutdowns. In retrospect, although the problem resulted in downtime, it demonstrated the effectiveness of the system for safely discontinuing soil feed in the event of a system failure and the need for panel indicator lights to remain lighted after the warning annuniciator is silenced to determine which limit switch caused the shutdown.

Note that a 4-hour test run for LAAP soil was also not completed. Originally, as with the CHAAP soil, two test runs were to be evaluated for the 8,000 lb/hr feed rate, a 4-hour run and an 8-hour steady-state run. The steady-state run presented a greater challenge to the feed system and, since nothing significant was learned when both the short and long duration runs were conducted on CHAAP soil, the short test run for LAAP soil was deleted from the schedule.

4.2 <u>Test run sequence/schedule of daily activities</u>. The typical daily schedule for system testing during the 4-hour test runs was as follows:



Test run number	Date (1986)	Soil type	Feed rate (lb/hr)	Test <u>duration</u> Target			
1	June 30	CHAAP	4,000	4	4		
2	June 31	CHAAP	12,000	4	2*		
3	July 1	CHAAP	8,000	4	4		
4	July 2	CHAAP	8,000	8	8		
5	July 8	LAAP	4,000	4	5		
6	July 8	LAAP	12,000	4	4.5		
7	July 9	LAAP	8,000	8	8		
8	July 10	CHAAP	12,000	4	4.5		

TABLE 4. SCHEDULE OF TEST RUNS

*Test Run No. 2 was not completed. This test was repeated as Test Run No. 8.

-21-

.....

Activity		Duration
Feed uncontaminated soil Feed contaminated soil Feed uncontaminated soil Equipment cleanup/decontamination	Total	l hour 4 hours 1 hour <u>2 hours</u> 8 hours

The typical daily schedule for system testing during the 8-hour test runs was as follows:

Activity		Duration
Feed uncontaminated soil Feed contaminated soil Feed uncontaminated soil Equipment cleanup/decontamination	Total	l hour 8 hours 1 hour <u>2 hours</u> 12 hours

Testing was also performed under upset- and/or failure-mode conditions. The objective of this phase of testing was to check all of the alarm systems.

A summary of the alarm systems tested, the simulated cause of the alarm, the system response, and the appropriate operator response is provided in Table 5.



TABLE 5. FEED SYSTEMS OPERATIONAL SAFETY CONTROLSUPSET- AND/OR FAILURE-MODE TESTING

	Description	Potential cause	System response	Operator response
1.	Low motor amps in live bottom hopper	Hopper empty or at very low level. Bridging in hopper.	Alarm.	If hopper is empty or at very low level, feed back- ground soil.
				If not, shut down system and clear bridging in hopper.
2.	High motor amps in live bottom hopper	Hopper overloaded. Partial jamming of screws.	Alarm.	Continue operating without feeding any more soil to hopper.
				Monitor motor amps closely.
3.	High-high motor amps in live bottom hopper	Jam in live bottom hopper screws.	Alarm. Screws will automatically reverse partial	If live bottom hopper shuts down, remove access door and clear jam.
			revolution and attempt to restart.	Restart system and monitor motor amps closely.
			If jam persists, prior procedures will repeat once, then live bottom hopper will shut down.	



TABLE 5. (CONTINUED)

Description	Potential cause	System response	Operator response
 High motor amps in cross conveyor 	Conveyor over- loaded.	Alarm.	Monitor motor amps closely.
	Partial jamming of screws.	Live bottom hopper will shut down.	Restart live bottom hopper once motor amps decrease to
		Live bottom hopper must be manually restart- ed once cross conveyor motor amps decrease to acceptable level.	acceptable level.
5. High-high motor amps in cross	Jam in cross conveyor screws.	Alarm	Monitor motor amps closely.
conveyor		Live bottom hopper will shut down.	Restart live bottom hopper once motor amps decrease to
		Cross conveyor	acceptable level.
		screws will automatically reverse partial revolution and attempt to restart.	If jam persists and cross conveyor shuts down, shut down system and clear the jam.
		Live bottom hopper must be manually restart- ed once cross conveyor motor amps decrease to acceptable level.	Restart cross conveyor, then live bottom hopper, and monitor motor amps closely.
		If jam persists, prior procedure will repeat once, then cross convey will shut down.	or



TABLE 5. (CONTINUED)

Description	Potential cause	System response	Operator response
6. High motor amps in feed conveyor	Conveyor over- loaded.	Alarm.	Monitor motor amps closely.
	Partial jamming of screws.	Live bottom hopper and cross conveyor will shut down. Cross conveyor then live bottom hopper must be restarted man- ually once feed conveyor motor amps decrease to acceptable level.	acceptable level.
7. High-high motor amps in feed conveyor	Jam in feed conveyor screws.	Alarm. Live bottom hopper and cross conveyor will shut down. Feed conveyor screws will automatically reverse partial revolution and attempt to restart.	Monitor motor amps closely. Restart cross conveyor, then live bottom hopper once motor amps decrease to acceptable level. If jam persists and feed conveyor shuts down, shut down system and clear the jam.
		Cross conveyor, then live bottom hopper must be manually restart- ed once feed conveyor motor amps decrease to acceptable level.	Restart feed con- veyor, then restart cross conveyor and live bottom hopper and monitor motor amps closely.

.....



TABLE 5. (CONTINUED)

Description	Potential cause	System response	Operator response
		If jam persists,	
		prior procedure	
		will repeat once,	
		then feed conveyo	or
		will shut down.	
8. Emergency shutdown	Loss of electrical power.	Alarm.	Determine reason for shutdown.
	Operator hits	System will shut	If due to loss of
	"panic" button.	down automati-	electrical power,
	-	cally.	ensure that
			electrical power is
		System must be	reinstated prior to
	·	manually re-	attempting to
		started once	restart system.
		the reason for	
		shutdown has	If due to operator
		been corrected.	initiation, ensure
			that the reason
			for shutdown has
			been corrected.
			Initiate equipment
			startup procedures.

---- ----



5. DATA ANALYSIS

5.1 Presentation of CHAAP Data

5.1.1 4,000-lb/hr feed system test (Test Run No. 1). The data for the 4,000-lb/hr CHAAP feed system test (Run No. 1) are summarized in Table 6. Figure 5 is a graphic plot of the variation in actual feed rate during Test Run No. 1 compared to the target feed rate of 4,000 lb/hr. Figure 6 provides a graphic plot of the variation in motor amps for the hopper conveyor, cross conveyor, and feed conveyor during Test Run No. 1.

5.1.2 8,000 lb/hr feed system test (Test Run Nos 3 and 4). The data for the 4-hour, 8,000-lb/hr CHAAP feed system (Run No. 3) are summarized in Table 7. Graphic plots of the variation in actual feed rates and motor amps during Test Run No. 3 are presented in Figures 7 and 8, respectively.

The data for the 8-hour, 8,000-lb/hr CHAAP feed system test (Run No. 4) are summarized in Table 8. Graphic plots of the variation in actual feed rates and motor amps during Test Run No. 3 are presented in Figures 9 and 10, respectively.

5.1.3 12,000-1b/hr feed system test (Test Run No. 8). The data for the 12,000-1b/hr CHAAP feed system test (Run No. 8) are summarized in Table 9. Graphic plots of the variation in actual feed rates and motor amps during Test run No. 8 are presented in Figures 11 and 12, respectively.

5.2 Presentation of LAAP data

5.2.1 4,000-lb/hr feed system test (Test Run No. 5). The data for the 4,000-lb/hr LAAP feed system test (Test Run No. 5) are summarized in Table 10. Graphic plots of the variation in actual feed rates and motor amps are presented in Figures 13 and 14, respectively.

5.2.2. 8,000-lb/hr feed system test (Test Run No. 7). The data for the 8-hour, 8,000-lb/hr LAAP feed system test (Run No. 7) are summarized in Table 11. Graphic plots of the variation in actual feed rates and motor amps during Test Run No. 7 are presented in Figures 15 and 16, respectively.

5.2.3 12,000-1b/hr feed system test (Test Run No. 6). The data for the 12,000-1b/hr LAAP feed system test (Run No. 6) are summarized in Table 12. Graphic plots of the variation in actual feed rates and motor amps during Test Run No. 6 are presented in Figures 17 and 18, respectively.

RUM 1 6/30/86 CHAAP SOIL TARGET FEED: 4,000 LB/HR

ואטרך טי טטרדשאו עי ובטו טעוא זעה ובטו אטא איי יי יואאי שייני אייטעריבעיוא

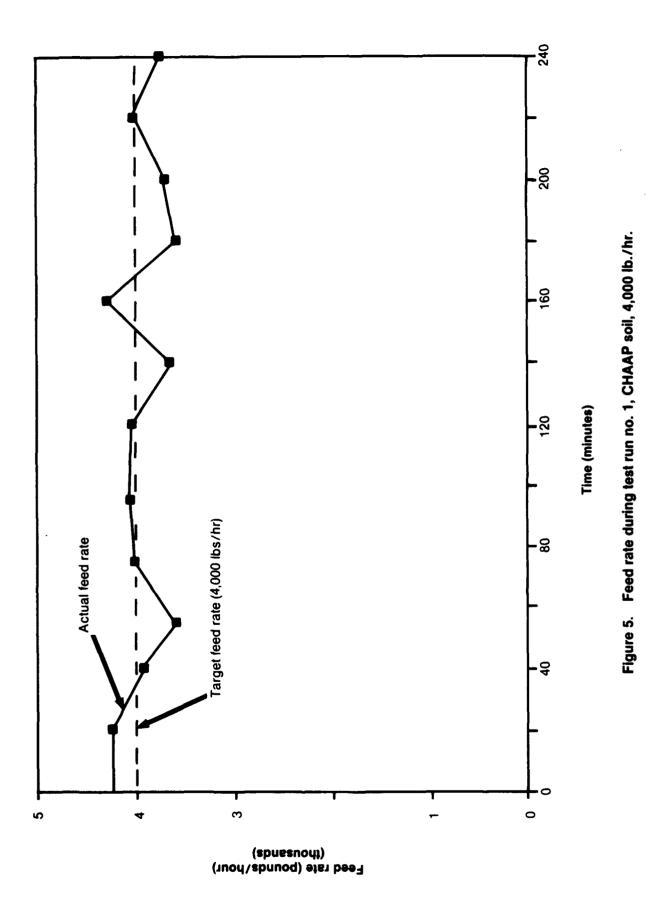
er (22	ۍ	ۍ	L.	າທາ	n	د ،	ഹഹ	Ľ	ר	ഗഗ	ۍ د		n	5	S	
hopper بط (۲) (۲) ²	2.5 2.5	2.5	2.5	~			, N	2.5	, С	j	2.5		Ċ	C·7	2.5	5.	
t <u>tom ho</u> Speed (rpm)		-	-	-		-			-	-		-		-	-	-	
Live bottom hopper Dr.ve Speed setting (rpm) (%)²		-	-	-		-			-	-		_	-	-	-	-	
(%) ²	36 36	36	36	36	98 8 98 8	5	36	8.S	36	3	88	65	46	5	65	65	
<u>Cross Conveyor</u> Prive Speed etting (rpm) (%	14.5 14.5	14.5	14.5	14 5	14.5	<u>,</u>	14.5	14.5	3 14	2	14.5	26	76	0,7	26	26	
<u>Cross</u> Drive setting	00	0	0	-	000	•	•		c	.	• •	0.1	0		1.0	1.0	
<u>уог</u> (%) ²	52 52	52	52	52	323	70	22	25	53	5	222	75	76	2	75	75	
Feed conveyor ive Speed ting (ppm) (%	21	12	21	16	125	- 7	23	57	10		22	30	08	2	30	30	
<u>Feed</u> Drive setting	0.4	0.4	0.4	7 U	.4.4	t. D	0.4	0.4 7	7 U		0.4 0.4		-	-	1.1		
L	11.76 11.76	11.76	11.76	AL CL	11.76	0/-14	12.18	12.6	12 6		12.6 12.18	12.18	76 11	2	11.76	11.76	
Live bottom hopper Moto (%)' amps	28 28	28	28	50	388	07	53	50	υz	8 3	8 S	29	a c	3	28	28	
<mark>Cross conveyor</mark> Motor (%) ¹ amps	6.6 6.82	6.82	6.82	2 04	7.04	0.02	7.04	7.48	7 26		7.26 7.26	8.14	97. B	00.0	8.36	8.14	
	30 30	31	١٤	22	182	5	32	34 34	33))	R 8	37	87.	5	38	37	
<u>Feed conveyor</u> Motor (%) amps	10.5 10.5	10.5	10.5		10.5			0.5 10.5			10.5 10.92	10.92	10 5	•	10.5	•	
Feed ((%)	25 25	25	25	25	32%	Ŋ	25	32	25	3	52 52 52	26	36	3	25	25	
Feed rate (1b/ hr)		4,233	3,915	3,596	4,011	4,053		4,039	3,651	4,299	3.588		3,714	4,026		3,759	
Net weight soil hopper (1b)		114,1	1,305	899	1,337	1,361		1,083	1,219	1,433			1,238	1,342		1,253	
Duration of hopper fill cycle (minutes)		20	20	15	20	20	L	9	20	20	20		20	20		20	
Time (min- utes)	0]5	30 30	40 45	55 60	82 52	8 S	105	135	140	160	165 180	195	200	220	225	240	

'(%) indicates percent of full load motor amps. full load motor amps are as follows: feed conveyor - 42 amps, cross conveyor - 22 amps, and hopper conveyor - 42 amps. *(%) indicates percent of maximum safe conveyor tip speed of 2 feet per second (40 rpm).

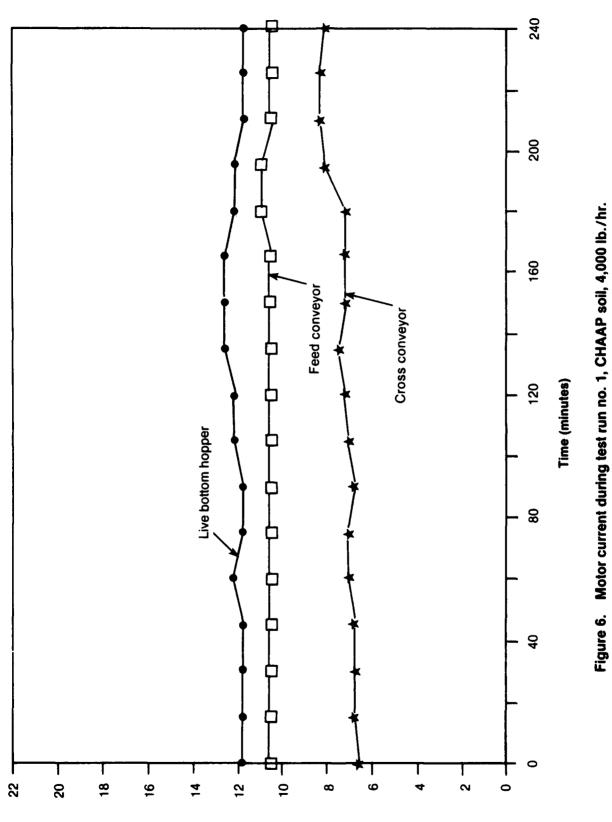
-28-

0492B





-29-



Motor current (amps)

-
Ë
4-HUUK
, 8,000-LB/HK,
SUIL
СНААР
r,
NG.
KUN
IESI
FUR
IESI DAIA FUR IESI H
IESI
5
SUMMARY (
:
IABLE

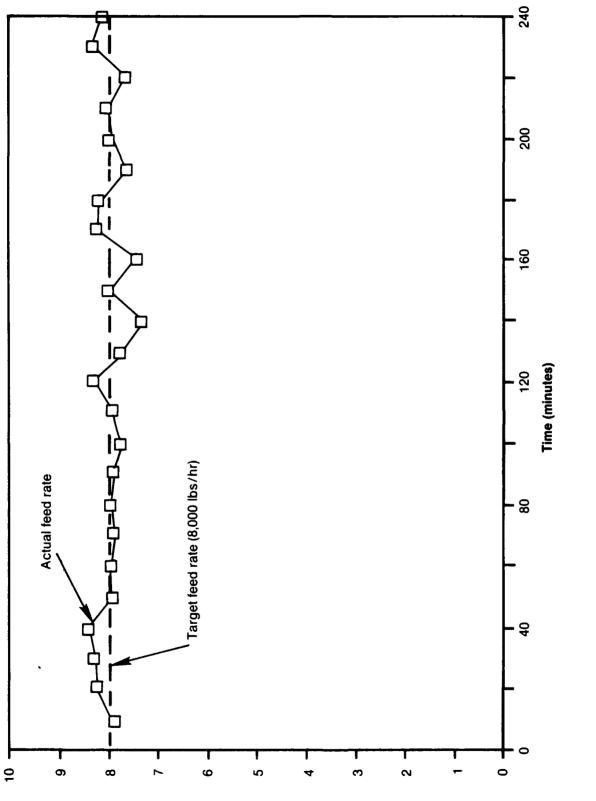
RUM 3 7/1/86 CHAAP SOIL TARGET FEED: 8,000 LB/HR (4-HOUR RUN)

<u>ц</u>	ł																			
1 (%)	2	S	S	S	S	S	ç		S	2		5	2	ç		ъ	S	S	ഹ	2
tom hy Speed (rpm)	~	2	2	2	2	~	2		2	2		2	2	2		2	2	2	2	2
<u>Live bottom hopper</u> Drive Speed setting (rpm) (%)	3.0	3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0		3.0	3.0	3.0		3.0	3.0	3.0	3.0	3.0
1 1 1 (%)	65	65	65	65	65	65	65		65	65		65	65	65		65	65	65	65	65
Convey Speed (rpm)	26	26	26	26	26	26	26		26	26		26	26	26		26	26	26	26	26
<u>Cross Conveyor</u> Drive Speed setting (rpm) (%	1.0	1.0	1.0	1.0	1.0	1.0	1.0		1.0	1.0		1.0	1.0	1.0		1.0	1.0	1.0	1.0	1.0
70r (%)	75	75	75	75	75	75	75		75	75		75	75	75		75	75	75	75	75
Feed conveyor ive Speed ting (ppm) (2	30	30	30	30	30	30	30		30	30		30	30	30		30	30	30	30	30
<u>Feed</u> Drive setting	<u>-</u>	1.1	1.1	l.,I	1 .1	l.1	l.1		1.1	1.1		1.1	l	l.I		1.1	ו.ו	l.!	l.1	l.1
5	13.02	13.44	13.44	12.6	13.44	13.44	13.44		13.44	13.44		13.44	13.44	13.44		13.44	13.44	13.44	13.44	12.18
Live bottom <u>hopper</u> Moto	31	32	32	30	32	32	32		32	32		32	32	32		32	32	32	32	29
<mark>Cross conveyor</mark> Motor (%) amps	8.8	9.24	9.46	8.8	8.8	8.8	8.8		8.8	9.24		9.24	9.02	9.24		9.02	9.24	9.46	9.68	9.46
<mark>Cross c</mark> (%)	40	42	43	40	40	40	40		40	42		42	41	42		41	42	43	44	43
<u>Feed conveyor</u> Motor (%) amps	10.5	10.5	10.5	10.5	10.5	10.5	10.5		10.92	10.92		10.92	10.92	10.92		10.92	10.92	10.92	11.34	11.34
Eeed c. (%)	25	25	25	25	25	25	25		36	26		26	26	26		26	26	26	27	27
Feed rate (1b/ hr)		006,1	8,286 8,286	0,410	7,986	n76'1	106.1	7,915		194,1	8,286 7,780		7,926		8,220 8,173	077 6	600'1	7,926 8,004	1,092	8,304 8,118
Net weight of soil in hopper (1b)	200	C7C'I	1,3/4	505° 1	1,320	100	ck1 , 1	1,451 1,166	,	/ch, ľ	1,381 1,167		1,320		1,320	1 405	1,400	1,321	1,282	1,384 1,353
Duration of hopper fill cycle (minutes)	-	2	222	2 9	292	-	ת	= °		=	0 ⁶		222	2	0 6		= :	<u>.</u>	0	0
Time (min- utes)	0	ទកន	285	\$ 8 2	285	52	<u>8</u> 6	16	105	120	121	135	150	165	170	180	195	210	225 225	230 240

WESTERN

-31-

0492B



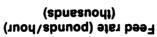


Figure 7. Feed during test run no. 3, CHAAP soil, 8,000 lb./hr., 4-hour test.

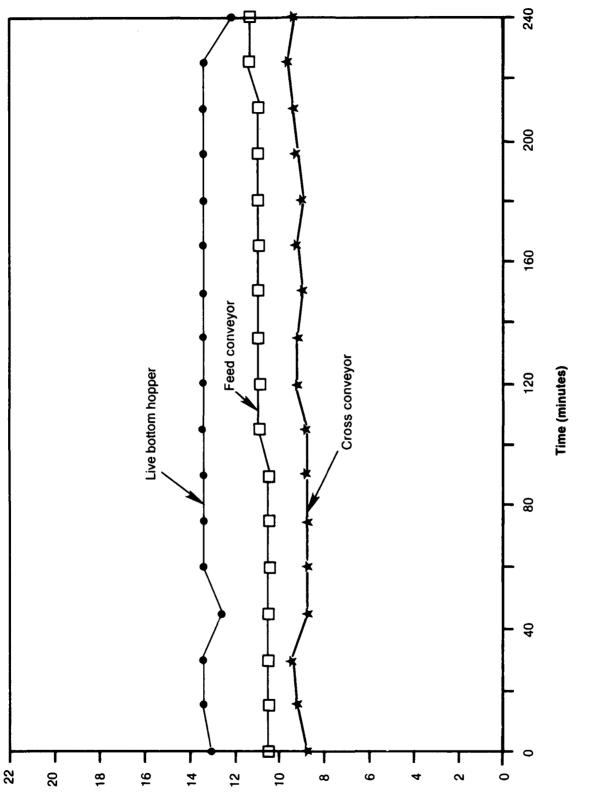


Figure 8. Motor current during test run no. 3, CHAAP soil, 8,000 lb./hr., 4-hour test.

Motor current (amps)

RUN 4 7/2/86 Chaap Soil Target Feed: 8,000 lb/HR (8-Hour Run)

닉											_	_							_
1 1 1 1	1	S	2	S	5	5	5	6.2		6.2	6.9	6.9		5.8	5.8	S	5.5		5.5 2
Live battom hopper Drive Speed (%)		2	2	2	2	2	2	2.5		2.5	2.75	2.75		2.33	2.33	5	2.2	((7.2
Live bot Drive		3.0	3.0	3.0	3.0	3.0	3.0	3.8		3.8	4.0	4.0		3.7	3.7	3.0	3.2		3.2
Live b Drive	set		,	(-)	(,,	(1)	,			(*)	7	7		(*)	(•)	(•)		,	.,
<u>or</u>	19	65	65	ςŋ	65	65	65	65		65	65	65		65	65	65	65	L	çõ
Cross Conveyor Trive Speed		5	<u>, o</u>	5	5	5	.0	Ň		50		5		.0			50		0
		26	26	26	26	26	26	26		26	26	26		26	26	26	26		97
<u>Cross</u> Drive	אררו	1.0	1.0	1.0	1.0	1.0	1.0	1.0		1.0	1.0	1.0		1.0	1.0	1.0	1.0		0.1
0r 121	(~)	75	75	75	75	75	75	75		75	75	75		75	75	75	75	ł	ئ
CONVEYOR Spred		30	30	30	30	30	30	30		30	30	30		30	30	30	30	ç	9 2
Feed Drive		٦.				1.1	1.1			-	-	-		-					
		-	-					•		-	-	-		و ا	_	4			
Live bottom hopper Motor	sdillo	12.6	12.6	12.6	12.6	12.6	12.6	12.6		12.6	13.44	13.44		13.86	13.86	13.44	13.44		9.21
Live bot M	(*)	30	30	30	30	30	30	30		30	32	32		33	33	32	32	ć	50
Motor Amotor	sching	6.6	6.9	6.6	6.6	10.56	0.11	0.11		10.78	0.11	12.1		0.11	10.78	0.11	11.22	- -	o.
Cross converge Motor Amotor						-	•				-			-	-	-	-		
<u>(%)</u>	(a)	45	45	45	45	48	50	50		49	50	55		50	49	50	51	5	nc
<u>Feed conveyor</u> Motor		10.5	10.5	10.5	10.5	10.5	10.5	10.5		10.5	10.5	10.5		10.92	10.92	10.92	10.92		c.01
CODY			•				•				-			-	-	-			
Feed (2)	(%)	25	25	25	25	25	25	25		25	25	25		26	26	26	26	ιc	ç
Feed rate (1b/ hr)		CI8 7	1011	0.268 8,268	007.0	7,446	F03, 1	0,900	7,238 7,840	020 5	7,020	200,0	9, 008 9, 153	8 78 <i>1</i>	9,306	007 2	600.1	8,013 8,000	7,706
Net weight of soil in ///		CUC I		6/2,1 378		241	<u>t</u> 1	101	1,327 1,176	000	053		1,281		396			202	, 156
Z a v o-		-						-		-				` -	:		-		-
Duration of hopper fill (minutes)	(minutes)	o,	2	222	2 2	222	2 5	2	[⁶	1	- o c	2 0	20	σ	`6 <u>;</u>	: :	=	6	6
Time (main-	(ca)n	00	528	200	42 42	209 209	55.8	86	16 001	105	071	135	147	150 156	165	180	195	198 207	216



-34-

0492B

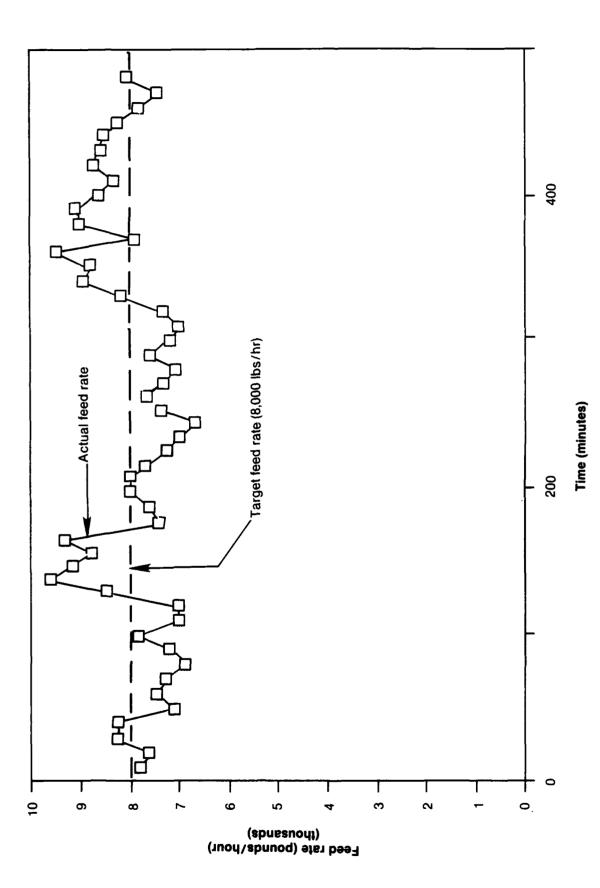
TABLE 8. (CONTINUED)

RUM 4 7/2/86 CHAAP SOIL TARGET FEED: 8,000 LB/HR (8-HOUR RUN)

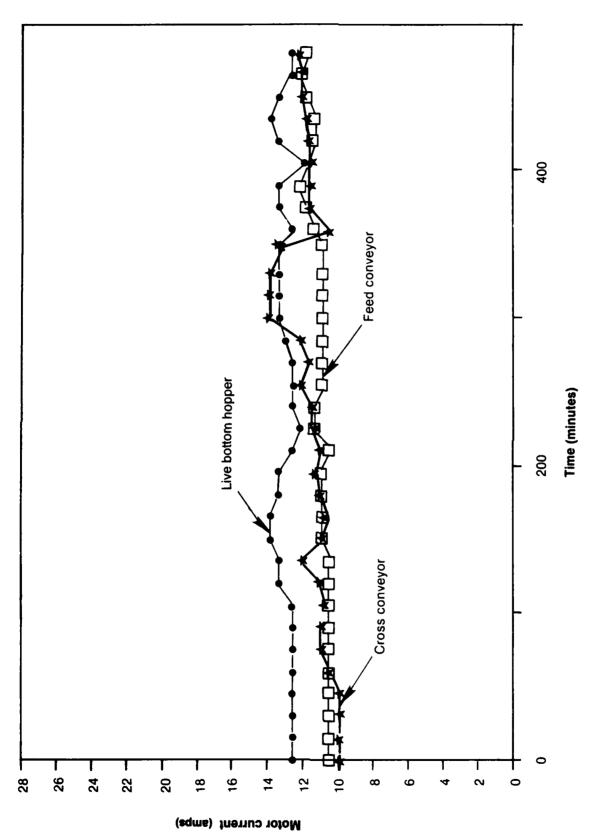
<i>.</i> .																		
10000Er	5.5	5.5	5.5	5.5	6.0	6.0	6.5	6.5	6.5 6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	
t <u>tom h</u> c Speed (rpm)	2.2	2.2	2.2	2.2	2.4	2.4	2.6	2.6	2.6 2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	
<mark>Live bottom hopper</mark> Drive Speed setting (rpm) (%)	3.2	3.2	3.2	3.2	3.6	3.6	3.9	3.9	3.9 3.9	3.9	3.9	3.9	3.9	3.9	3.9	3.9	3.9	
<u>yor</u> (%)	65	65	65	65	65	65	65	65	65 65	65	65	65	65	65	65	65	65	
Conve Speed (rpm)	26	26	26	26	26	26	26	26	26 26	26	26	26	26	26	26	26	26	
<u>Cross Conveyor</u> Drive Speed setting (rpm) (%	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
X0r (%)	75	75	75	75	75	75	75	75	75 75	75	75	75	75	75	75	75	75	
conveyor Speed (ppm) (%	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	
<u>Feed</u> Drive setting	1.1	1.1	1.1	l.1	۲.1	1.1	۲.1	[]		1.1	1.1	l.1	ו.ו	l.I	1.1	1.1	l.'	
ottom <u>er</u> Motor amps	12.18	12.6	12.6	12.6	13.02	13.44	13.44	13.44	13.44 12.6	13.44	13.44	11.76	13.44	13.86	13.44	12.6	12.6	
Live bottom <u>hopper</u> Moto (%) amps	29	30	30	30	31	32	32	32	30 30	32	32	28	32	33	32	30	30	
Cr <u>oss conveyor</u> Motor (%) amps	11.44	11.44	12.1	11.66	12.1	13.86	13.86	13.86	13.2 10.56	11.66	11.66	11.66	11.66	11.88	12.1	12.1	12.32	
Cross (%)	52	52	55	53	55	63	63	63	60 48	53	53	53	53	54	55	55	56	
Feed conveyor Motor (%) amps	11.34	11.34	10.92	10.92	10.92	10.92	10.92	10.92	10.92 11.34	11.76	12.18	11.76	11.34	11.34	11.76	12.18	11.76	
(%)	27	27	26	26	26	26	26	26	26 27	28	29	28	27	27	28	29	28	
Feed rate (1b/ hr)	7,240	6,666	14C,1	7,326	7,067	7,188	1 324	8,178 8,178 8,916	8,832 9,486	+00''	9,072 9,072	0,066	0, 340 8, 724 8, 586	0, 500 0 5 2 2	8,274 8,274		8,058	-35
Net weight of soil in (lb)	1,086	111,1	1,150	660'1	1,060	1,198 1,198	0/1,1	1,486	1,472		1,512	000 1	1,454		1,379		1,343	
Duration of hopper fill cycle (minutes)	60	<u>ه</u> و	י מ	, 6	6	229		200	000	2 9	222	2 9	223	2 2	222	2 9	20	
Time (min- utes)	225	240 244 244	255 255	270	280 285	062 300	315	330 340 340	360 360 360 370	375	390	405	420	435	450	465	480	0000

WISTER

04928









12,000-LB/HR
HAAP SOIL,
NO. 8, C
TEST RUN
FOR
TEST DATA
SUMMARY OF
TABLE 9.

RUN 8 7/10/86 CHAAP SOIL TARGET FEED: 12,000 LB/HR

I																						
0000er (%)	6.8	6.8	6.8	6.8	6.8		7.0	-		7.2		7.2	7.2	с r			7.2	с г	7.1	7.2		
t <u>om h</u> Speed (rpm)	2.7	2.7	2.7	2.7	2.7		2.8	0 0	C8.2	2.9		2.9	2.9	0 0			2.9	c c	£.7	2.9		
<mark>Liv<u>e bottom hopper</u> Drive Speed</mark> setting (rpm) (%)	4.0	4.0	4.0	4.0	4.0		4.35		4.4	4.5		4.5	4.5	2	•		4.5		4.0	4.5		
зуаг 1 (%)	65	65	65	65	65		65	.,	60	65		65	65	Ϋ́	5		65	72	C 0	65		
Conveyor Speed (rpm) (%	26	26	26	26	26		26	56	97	26		26	26	26	3		26	76	07	26		
<u>Cross</u> Drive setting	1.0	1.0	1.0	1.0	1.0		1.0	- -	0.1	1.0		1.0	1.0		-		1.0	- -	.	1.0		
<u>уог</u> (%)	75	75	75	75	75		75	ŀ	5	75		75	75	75	2		75	76	c /	75		
<u>conveyor</u> Speed (ppm) (%	30	30	30	30	30		30	Ċ	20	30		30	30	30	Ŗ		30	UC.	n c	30		
<u>Feed</u> Drive setting	1.1	1.1	ו.ו	1.1	1.1		1.1	-	-	l.l		l.1	г. Т	-			1.1	-	-	l.1		
ottom Ler Motor amps	15.96	12.6	12.6	12.6	11.34		11.34	, , ,	0.21	12.6		12.6	13.86	12 6	0.7		12.6	9 61	0.21	12.6		
Live bottom hopper Moto (%) amps	38	30	30	30	27		27	ć	<u>ع</u> ا	30		30	33	30	Ş		30	00	20	30		
CONVEYOF Motor amps	9.9	10.34	10.34	11.0	6.9		9.9		11.44	6.9		6.9	8.8	0			9.9	c	r.r	9.9		
Cross (2)	45	47	47	50	45		45	ŝ	76	45		45	40	45	7		45	AF	ņ	45		
l conveyor Motor amps	10.5	12.6	12.6	12.6	11.34		11.76	5	9.21	12.6		12.6	12.6	12 6			12.6	2 61	0.21	12.6		
Feed c (%)	25	30	30	30	27		28	ę	95	30		30	30	30		·	30	00	20	30		
feed rate (1b/ hr)	FOL LL	11,595	12,127	11,067	non' i i	11,886 11,073 9,916	•	11,453	11,207	12,533	12,327	040'11	12,160 11,753	11,647	11,566	11,647 10,008	000,01	11,784	11,202	612 11	9,402	10,812
Net weight of soil in (lb)	067 1	1,546	1,819	1,660 2,007	1,002	1,783 1,661 1,818		1,718	1,681	1,880	1,849		1,824 1,763			1,747	00,1	1,964	1,867	1 063	1,567	1,802
Duration of hopper fil cycle (minutes)	c	מס יד	6	စစ္စ	ת	و و		⁶ 0	6	6 0	5	r	თთ	6	6	6 9	2	0	10	01	0	0
Time (min- utes)	00	255	% R	42 42 42	4 G	63 72 83	60	92 102	9 E	120	138	150	156 165	174	183	192 202	210	212	222	220	242	252

-38-

0492B

WISTER

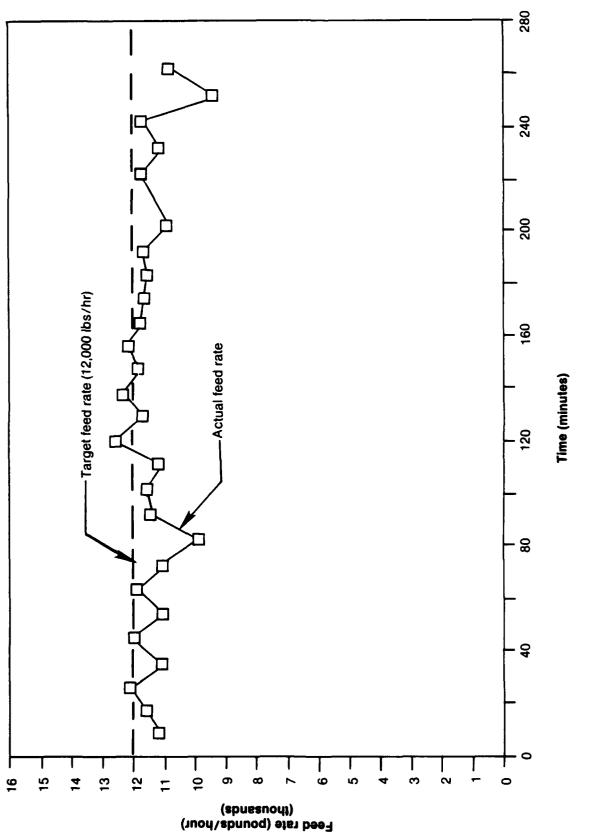
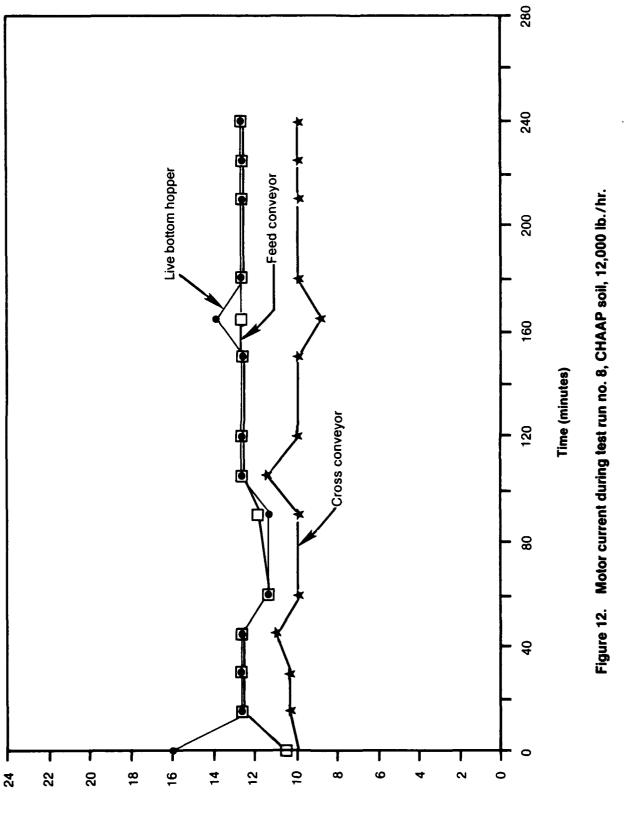


Figure 11. Feed rate during test run no. 8, CHAAP soil, 12,000 lb./hr.



Motor current (amps)

-40-

TABLE 10. SUMMARY OF TEST DATA FOR TEST RUN NO. 5, LAAP SOIL, 4,000-LB/HR

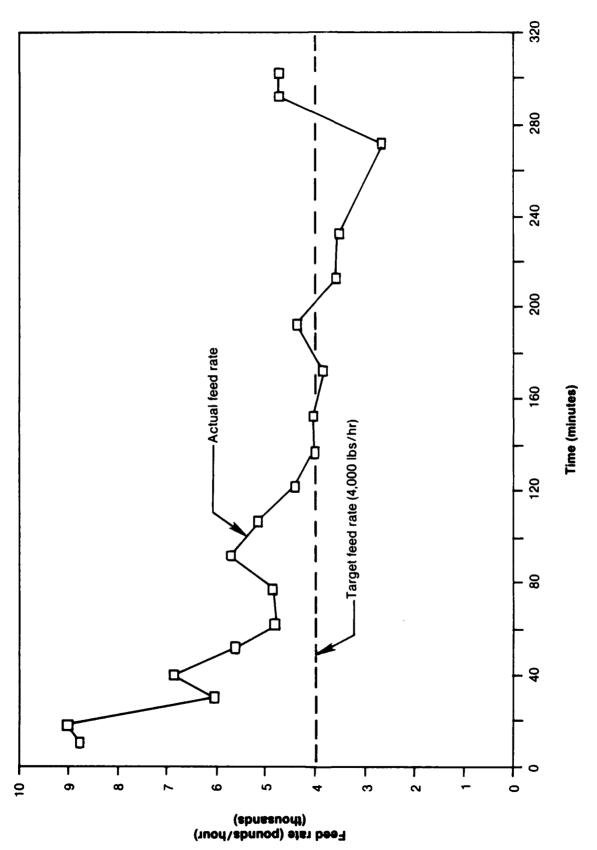
RUN 5 7/8/86 LAAP SOIL TARGET FEED: 4,000 LB/HR (B-HOUR RUN)

.												
000er (%)	2.5	2.2	2.0	1.9	1.8	1.8	9.1	 		1.6) - -	1.5
<mark>Live buttom hoppe</mark> r Drive Speed setting (rpm) (%)	1.0	0.9	0.8	0.75	0.7	0.7	0.65	٥.0 0	2	0.65		0.6
<mark>Live bot</mark> Drive setting	ו.ו	0.6	0.5	0.4	0.38	0.35	0.25	- 0		0.2		0.0
1 (2)	65	65	65	65	65	65	3 2 2	د م)	65	}	65
Convey Speed (rpm)	26	26	26	26	26	26	26 26	92	,	26		26
<u>Cross Conveyor</u> Drive Speed setting (rpm) (%)	1.0	1.0	1.0	1.0	1.0	1.0	0.1			0.1		0.1
<u>каг</u> (х)	75	75	75	75	75	75	75	ۍ ۲	2	75)	75
feed conveyor ive Speed ting (ppm) (2	30	30	30	30	30	30	88	38	8	30	}	90
Feed conveyor Drive Speed setting (ppm) (%)	ו.ו	l.I	1.1	ı.ı	1.1	1.1				1.1		l.l
v. oottom <u>hopper</u> Motor t) amps	10.5							10.5		10.5		10.5
Live oottom <u>hopper</u> (%) amps	25							25	ì	25		25
<mark>Cross (onveyor</mark> Motor (%) amps	7.26							6.38		5.94		5.94
Cross ((%)	33							29	ì	27	i	27
<u>Feed conveyor</u> Motor (%) amps	10.5							10.5		10.5		10.5
Eeed c (%)	25							25		25		25
Feed rate hr)	076 0	9,018	6,852	5,605 4,818	4,868 5.712	5,152	4,424	4,028	4,052		4,386 3,603	3,528 2,681 4,746 4,740
Net weight of in hopper (1b)	7 466	1,240	1,142	1,121 803	1,217	1,288	1,106	1,00,1	1,013		1,462 1,201	1,176 1,787 1,582 1,582
Duration of hopper fill cycle (minutes)	ġ	<u>o</u> eo 9	20	12	<u>र</u> र	15	15 i	د	15		20 20	20 20 10 20
Time (min- utes)	09	2 8 9	2 2	82	126	107	122	151	152	188	212	218 232 272 302 302

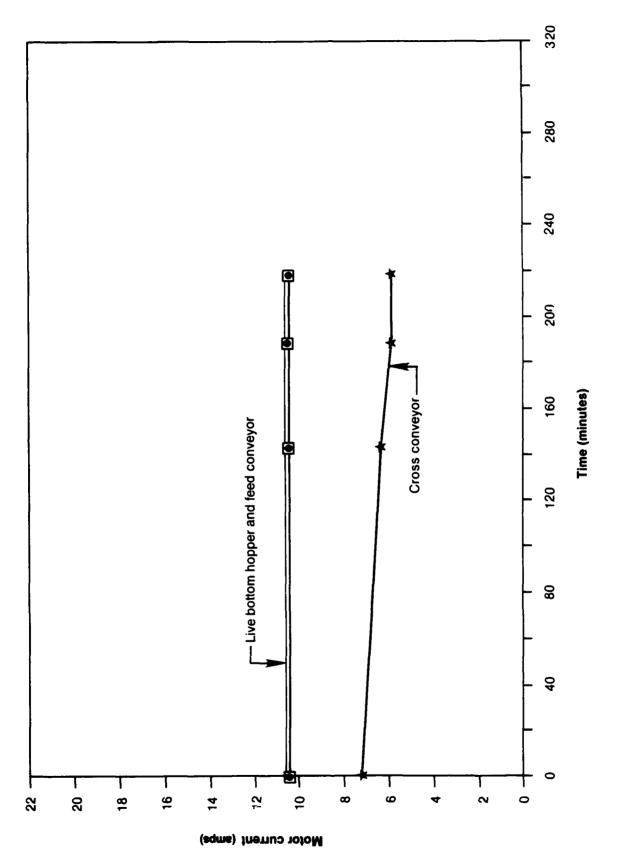
-41-

1

WESTERN









RUN 7 7/9/86 LAAP SOIL TARGET FEED: 8,000 L8/HR (8-HOUR RUN)

_ EL	0		6.	σ) a	o	c	α		ñ			8.		α	5	8.		80	
happe ed (%)	2.0		-	-		-				-			-		-	-	-		1.8	
ottom h Speed g (rpm)	0.8		0.75	1 0		N	, ,	0.7	, c	0.1			0.7		5 0		0.7		0.7	
<mark>Live bottom happe</mark> r Drive Speed setting (rpm) (%)	0.5		0.4	5 U		c.D		0.3		0.3			0.3		2 U		0.3		0.3	
(%)	65	65	65	ΥΥ Υ	5 3	6	Ļ	65 65	ų	çõ			65		55	3	65		65	
<mark>Cross Conveyor</mark> rive Speed tting (rpm) (%	26	26	26	26	25	07	Č	56 26	č	97			26		26	2	26		26	
<u>Cross</u> Drive setting	1.0	1.0	1.0			-	,	0.0	-	0.1			1.0		0 1	-	1.0		1.0	
(z)	75	75	75	75	2 2	2	ļ	د 57	;	3			75		75	2	75		75	
<u>Feed conveyor</u> ive Speed ting (ppm) (%	30	30	30	30		2	ė	30	ć	30			30		30	3	30		30	
<u>Feed</u> Drive setting	1.1	1.1	1.1	-		-				-			1.1			-	l.1		1.1	
ottom <u>Er</u> Motor amps	10.5	10.5	10.5	10 5		c.0		2.01 10.5		c.01			10.5		10 5		10.5		10.5	
Live bottom hopper Moto (%) amps	25	25	25	25	3 2	9	1	52 52	Ľ	ç			25		25	2	25		25	
Cross conveyor Motor (%) amps	7.26	7.26	6.6	يد بر	20.0	07.1	Ì	7.26	č	07.1			7.26		6 6	2	6.6		7.26	
Cross ((%)	33	33	30	٥۶	3	•••	ć		ć	55			33		30	2	30		33	
Feed conveyor Motor (%) amps	10.5	10.5	10.5	3 UL		c.01		c.01		c.0I			10.5		10 5		10.5		10.5	
eed c	25	25	25	25	3 2	ŝ	į	52 52	, u	ç 7			25		25	3	25		25	
Feed rate hr)	00V C1	064,21	10, 300	12,564 10,368	7,188	8,934	8,676	8,524 8.672	8,100		8,574	8,160		7,633	076,1	8,484		7,953 8,121		7,600
Net weight of in hopper (lb)	COV C	COU, 2	1,110	2,094 1,728	1,198	1,489	2,169	2, 131	2,160		2,028	2,448		1,781	7 445	2,828		2,651		2,515
Duration of hopper fill cycle (minutes)	9	2 9	2	00	01	01	13	र र	16	đ	07 07	8		4	07	20	:	202	2	21
Time (min- utes)	0	ទីសន	283	844	223	00 62	75	96 201	121	<u>.</u>	141	169	180	183	5U2	223	240	243 263	270	284

-44-

0492B

WISICEN

(CONTINUED)	
TABLE 11.	

RUN 7 7/9/86 LAAP SOIL TARGET FEED: 8,000 LB/HR (8-HOUR RUN)

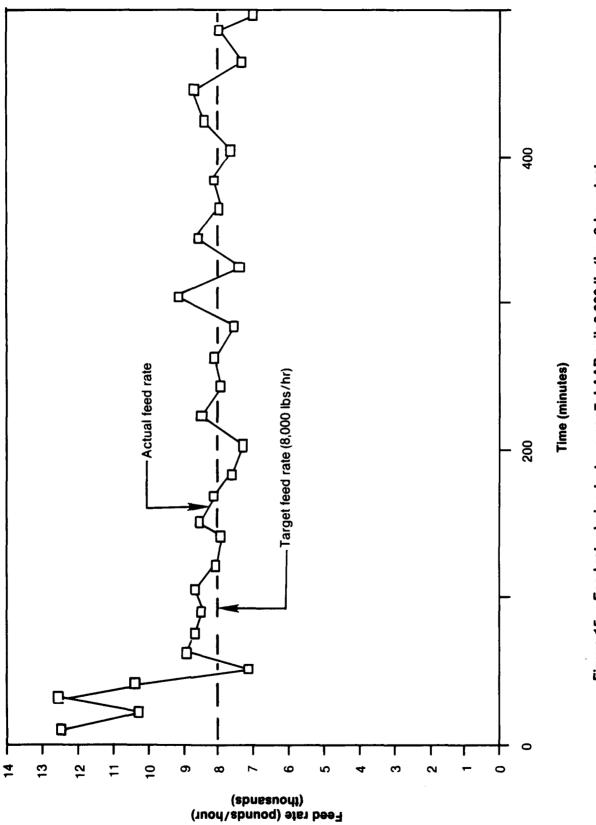
1

	1									
000001	1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8 1.8	1.8
<mark>Live bottom hopper</mark> Drive Speed setting (rpm) (%)	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
<u>Live bot</u> Drive setting	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3 0.3	0.3
101 (%)	65	65	65	65	65	65	65	65	65 65	65
<u>Conve</u>) Speed (rpm)	26	26	26	26	26	26	26	26	26 26	26
<u>Cross Conveyor</u> Drive Speed Setting (rpm) (%	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
<u>vo</u> r (%)	75	75	75	75	75	75	75	75	75 75	75
Feed conveyor ive Speed ting (ppm) (%	30	30	30	30	30	30	30	30	9 0 9	30
e D	. .	l.1	ו.ו	1.1	l.1	1.1	1.1	l.I	22	1.1
Live bottom happer Mator - amps s	10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5 10.5	10.5
Live bottom <u>hopper</u> (%) amps	25	25	25	52	25	25	25	25	22 25	25
<u>Cross conveyor</u> Motor (%) amps	7.26	9.46	6.6	9.24	7.26	7.26	7.26	7.26	10.56 7.7	8.8
<mark>(ross</mark> (%)	33	43	45	42	33	33	33	33	48 35	40
Feed conveyor Motor (%) amps	10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5 10.5	10.5
Feed (%)	25	25	25	25	25	25	25	25	25 25	25
Feed rate (1b/ hr)	9,156 7,731	8,598	8 022	0,ULL 8 142	7 60A	000''	817.8	21.262		7,996 7,044
Net weight of in hopper (1b)	3,052	2.866	2 674	2 714	2 566			2.454		2,932 1,174
Duration of hopper fil cycle (minutes)	20	20	2	2 2	2 2	20	20	20	1	22 0
Time (min- utes)	300 304 324	344	355	375 384	390	405	425	445 464	465 485	486 496 500

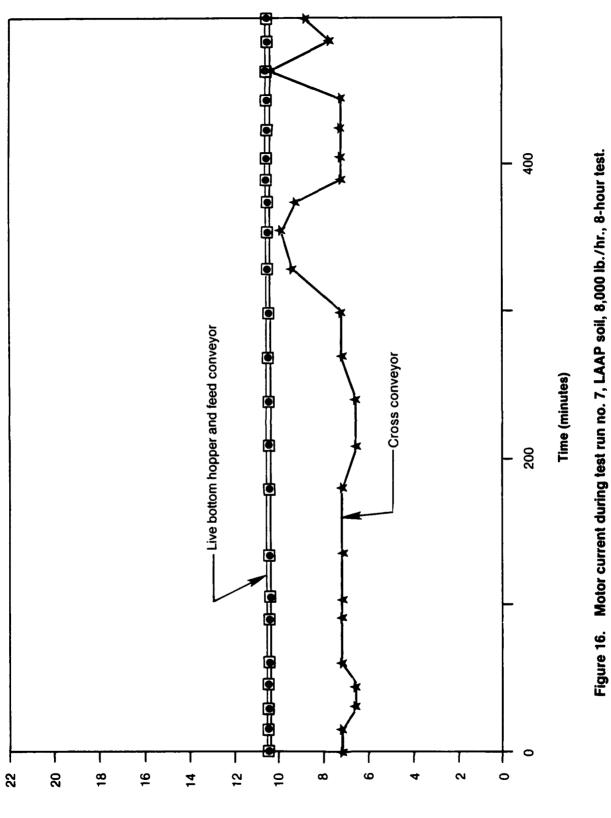
-45-

04928

WESTEN







Motor current (amps)

RUN 6 7/8/86 LAAP SOIL TARGET FEED: 12,000 L8/HR

(%)	3.2	3.4 3.2	3.4	3.4	3.2	3.2	3.2	3.2	3.2	3.2	3.2
<u>ive bottom hoppe</u> r Drive Speed setting (rpm) (%)	1.3	1.35	1.35	1.35	1.3	1.3	1.3	1.3	1.3	1.3	1.3
<mark>Live bot</mark> Drive setting	1.3	1.4	1.4	1.4	1.35	1.35	1.35	1.3	1.3	1.3	1.3
evor d (%)	65	65 65	65	65	65	65	65	65	65	65	65
<mark>Cross Conveyor</mark> rive Speed tting (rpm) (%	26	26 26	26	26	26	26	26	26	26	26	26
<u>Cross</u> Drive setting	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
<u>40r</u> (%)	75	75 75	75	75	75	75	75	75	75	75	75
<u>conveyor</u> Speed (ppm) (%	30	90 90 90 90	30	30	30	30	30	30	30	30	30
<u>Feed</u> Drive setting	1.1		l.I	1.1	1.1	1.1	ו.ו	1.1	l	l.1	l.l
Live bottom <u>hopper</u> Motor (%) amps				10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5
Live bott <u>hopper</u> Mc (%) an				25	25	25	25	25	25	25	25
<u>Cross conveyor</u> Motor (%) amps				7.26	8.8	11.	۲.۲	9.24	1.1	8.58	8.8
<mark>Cross</mark> (%)				33	40	50	35	42	35	39	40
Feed conveyor Motor (%) amps				10.5	10.5	10.5	10.5	10.5	10.5	10.5	10.5
Feed ((%)				25	25	25	25	25	25	25	25
Feed rate (1b/ hr)	15,437 9,917	13,568	10,338	10,017	13,452	047,21	0,0,0 13,398	16,933 13,848	11,058 11,208	11,200 6 558	18,600
Net weight of in hopper (1b)	1,801	1,583	1,723	600'7	767'7	116,1	2,233	2,540 2,308	1,943 1,868	1 /03	2,480
Duration of hopper fil cycle (minutes)	~~'	ș	220	<u>و</u> م	2 0	- م	2 2	6 0		2	ēα
Time (min- utes)	0~4	32.82	6 73 3	325	80	888	100	120	135	150	159

WISTER

-48-

0492**B**

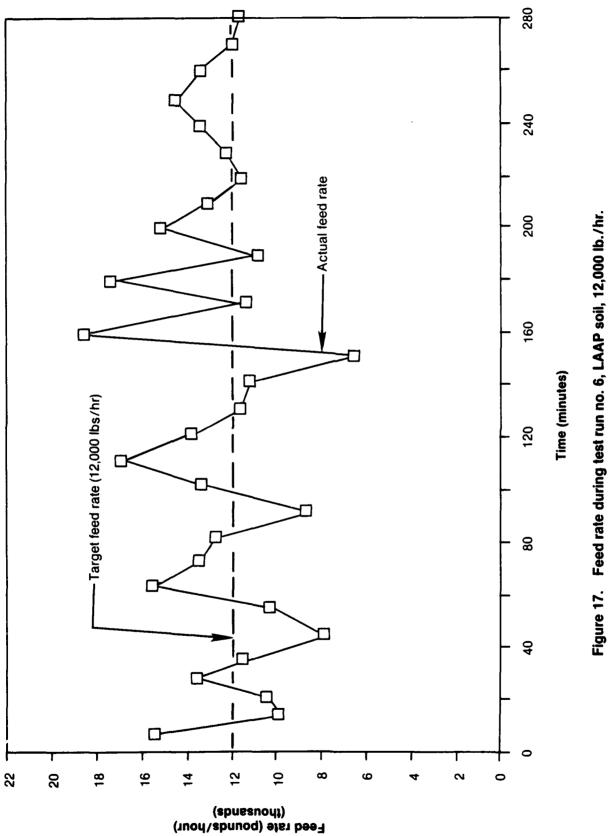
RUN 6 7/8/86 LAAP SOIL TARGET FE	ä	12,000 LB/HR	¥															
Time (min- utes)	Duration of hopper fil cycle (minutes)	Net weight of soil in hopper (]b)	Feed rate (lb/ hr)	Feed c (%)	Eeed conveyor Motor (%) amps		<u>Cross convevor</u> Motor (%) amps	Live b (%)	Live bottom hopper Motor (%) amps s	e D	<mark>Feed conveyor</mark> rive Speed (ting (ppm) (%	0C (%)	Cross Drive setting	Conve Speed (rpm)	<u>, yor</u> (%)	Live bul Drive setting	Live bultom hopper Drive Speed setting (rpm) (%)	0000000
171	12 8	2,280 2,320	11,400 17,400						 									
180 189	01	1.808	10.848	25	10.5	33	7.26	25	10.5	l.,	30	75	1.0	26	65	1.3	1.3	3.2
195 199 200	0	2,526	15,156	25	10.5	33	7.26	25	10.5	1.1	30	75	1.0	26	65	1.3	1.3	3.2
210	2 0	2, 102 1,932	260, CI	25	10.5	45	6.6	25	10.5	1.1	30	75	1.0	26	65	1.3	1.3	3.2
225 229 239	00	2,033 2,239	12,198	25	10.5	50	0.11	25	10.5	l.1	30	75	1.0	26	65	1.3	1.3	3.2
240 249	10	2.418	14.500	25	10.5	50	11.0	25	10.5	l.1	30	75	1.0	26	65	1.3	1.3	3.2
260 270 280	<u> </u>	2,458 2,005 1,940	13,407 12,030 11,640	25	10.5	50	11.0	25	10.5	1.1	30	75	1.0	26	65	1.3	1.3	3.2

TABLE 12. (CONTINUED)

-01-

04928

WESTEN



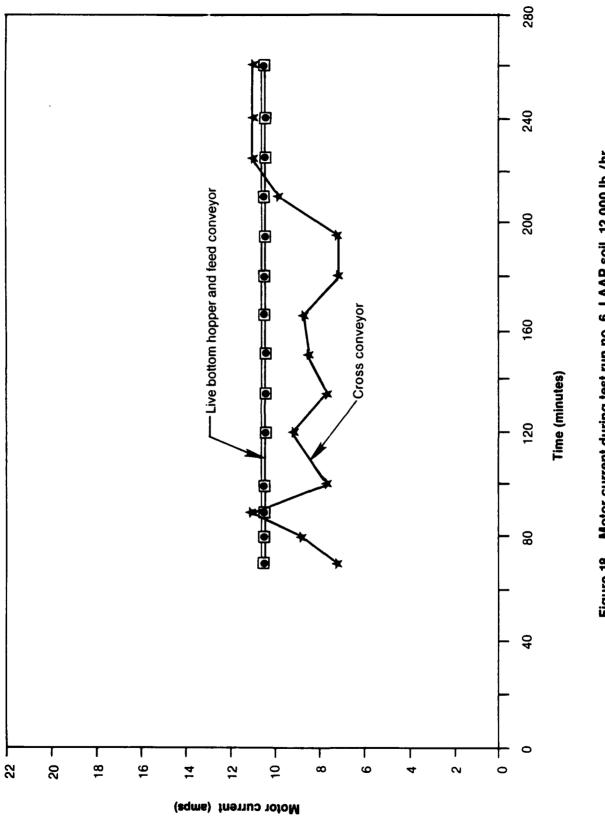


Figure 18. Motor current during test run no. 6, LAAP soil, 12,000 lb./hr.



5.3 <u>Analysis of test data</u>. This section provides an analysis of the following system parameters:

- Soil feed rate.
- Soil moisture content and bulk density.
- Soil size distribution.
- Rotational speed of screw conveyors.
- Screw conveyor motor current.
- LAAP soil explosives concentrations.

5.3.1 Soil feed rate. A summary of the average and range feed rate data for each of the test runs is provided below:

Soil type	Run no.	Target <u>feed rate</u> (lb/hr)	(ave	feed rate <u>rage)</u> (% of target)	Range of feed rates (lb/hr) (% of targe	_
CHAAP	1	4,000	3,907	97.7	3,596- 4,299 89.9-107.	5
CHAAP	3	8,000	7,967	99.6	7,434-8,418 92.9-105.	2
CHAAP	4	8,000	7,791	97.4	6,666-9,608 83.3-120.	1
CHAAP	8	12,000	11,451	95.4	9,402-12,533 78.4-104.	4
LAAP	5	4,000	5,099	127.5	2,681-9,018 67.0-225.	4
LAAP	7	8,000	8,541	106.7	7,044-12,498 88.0-156.	2
LAAP	6	12,000	12,617	105.1	6,558-18,600 54.6-155.	0

As shown in this summary, the full range of target feed rates (i.e., 4,000-12,000 lb/hr) was achieved for the CHAAP and LAAP soils. The feed system maintained feed rates very close to the target values for the CHAAP soils (i.e., average feed rate 95.4-99.6 percent of the target values). The instantaneous variations in CHAAP feed rates were typically within ±10 percent and in the most extreme cases still within ±20 percent of the target values. With the exception of Test Run No. 5, which is misleading due to operator error (the feed rate was decreased seven times during the test run before the feed rate was below 4,000 lb/hr), the feed system also maintained feed rates very close to the target values for the LAAP soils (i.e., 105.1-106.7 percent of the target values). However, for the LAAP soils, the instantaneous variations in feed rates were more significant with typical variations within ±20 percent and extreme variations as much as ±50 percent of the target values. The reason for the wider range of variations for the LAAP soils is discussed in Subsection 5.4.

-52-

0492B

5.3.2 Soil moisture content and bulk densities. The soil moisture content and soil bulk densities for the test runs are summarized as follows:

Soil type	Run no.	Feed soil or processed soil	Soil moisture content (%)	Soil bulk density
			(%)	
СНААР	l	Feed soil	16.4	
CHAAP	1	Processed soil	17.5	77 lb/ft ³
CHAAP	3	Feed soil	16.7	
CHAAP	3	Processed soil	16.4	71 lb/ft ³
CHAAP	4	Feed soil	15.2	
CHAAP	4	Processed soil	15.9	70 lb/ft ³
CHAAP	8	Feed soil	16.1	
CHAAP	8	Processed soil	17.4	78 lb/ft ³
LAAP	5	Feed soil	*	
LAAP	5	Processed soil	*	107 lb/ft ³
LAAP	7	Feed soil	*	
LAAP	7	Processed soil	*	116 lb/ft ³
LAAP	6	Feed soil	*	
LAAP	6	Processed soil	*	118 lb/ft ³

*Soil moisture content data were not available for the draft technical report. These data will be provided in the final report.

The CHAAP soil moisture content ranged from 15.2-17.5 percent with an average of 16.4 percent. The CHAAP soil bulk density for the processed soil (discharged from the feed system) ranged from 70-78 lb/ft³ with an average of 74 lb/ft³.

The LAAP soil moisture content data were not available for this report due to difficulty in locating a subcontractor that was willing to perform moisture content and size distribution testing on explosives-contaminated soils. These samples have been submitted to the Allegany Ballistics Laboratory, and the results will be submitted as an addendum to this report. The LAAP soil bulk density for the processed soil ranged from 107-118 lb/ft³ with an average of 114 lb/ft³.

-53-



5.3.3 Soil size distribution. The soil size distribution data for the CHAAP test runs are summarized in Table 13. The actual soil gradation curves for the feed soil and processed soil for each CHAAP run are presented in Appendix G. As shown in Table 13, the CHAAP soil size distribution data are very consistent. These results are summarized below:

Soil	Size	Percent	tages
classification	range	Average	Range
Cobbles	>3"	0	0
Gravel – coarse	3" - 3/4"	0	0
- fine	3/4" - 4 mesh	0	0
Sand - coarse	4 - 10 mesh	1.6	1-3
- medium	10 - 40 mesh	4.9	4-6
- fine	40 - 200 mesh	16.3	13-19
Silt or clay	<200 mesh	77.2	75-82

5.3.4 Rotational speed of screw conveyor. Figure 19 provides a graphical plot of the relationship between the Reeves variable speed drive setting and the measured live bottom hopper screw speed (in rpm) and screw tip speed (in feet per second). As shown in Figure 19, this is a relatively linear relationship. It is important to note that even at the maximum variable speed drive setting of "7.0," that the screw tip speed is nearly an order of magnitude below the recommended maximum tip speed for explosives-contaminated soils of 2 feet per second.

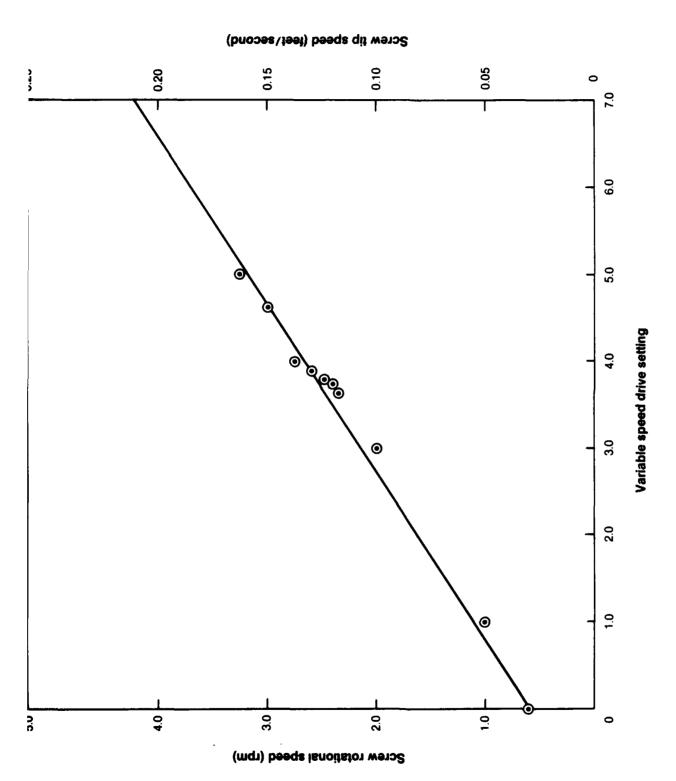
Figure 20 provides a similar graphical plot for the cross conveyor and feed conveyor. Again, the relationships are linear. However, these conveyors are capable of exceeling the recommended maximum tip speed of 2 feet per second for explosives-contaminated soils.

The relationships presented in Figures 19 and 20 are totally independent of the type of soil being fed. They simply illustrate the mechanical relationship of the gear drive settings to the rotational speed of the respective screws. Actual corresponding feed rates are dependent upon soil density and material handling characteristics. Subsection 6.2 provides recommendations relative to maintaining conveyor tip speed below the 2-foot-per-second safety criterion.

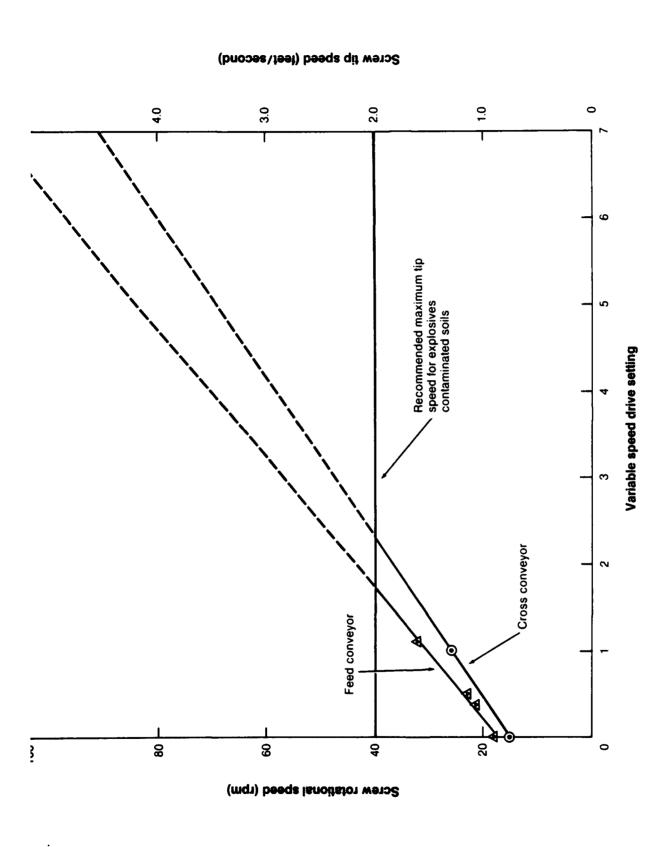


TABLE	13.	SUMMARY OF	SOIL	SIZE	DISTRIBUTION	DATA	FOR
		THE	CHAAP	TEST	RUNS		

	Perce	ent by g Grav		in each	size o Sand		<u>ication</u> Silt or	
CHAAP run no.	Cob- bles ≻3"	Coarse 3"- 3/4"		Coarse 4-10 mesh		n Fine 40-200 mesh	clay	To- tal
l - Feed	0	0	0	3	4	17	76	100
l - Processed	0	0	0	2	5	18	75	100
3 - Feed	0	0	0	1	5	19	75	100
3 - Processed	0	0	0	1	5	16	78	100
4 - Feed	0	0	0	1	6	15	78	100
4 - Processed	0	0	0	1	6	16	77	100
8 - Feed	0	0	0	1	4	13	82	100
8 - Processed	0	0	0	2	5	16	77	100











5.3.5 Screw conveyor motor current. The live bottom conveyor, cross conveyor, and feed conveyor motor current (both average and range data) are graphically presented for each CHAAP soil test run in Figure 21. A similar graphical plot for the LAAP soil test runs is presented in Figure 22.

5.3.6 LAAP soils explosives concentrations. A summary of the feed soil and processed soil explosives concentrations is provided in Table 14. In addition, after Run No. 7, the 8-hour run at 8,000 lb/hr, samples were taken from several points in the system where soil was compacted in the cross conveyor trough. The reason for this testing was to evaluate whether explosives have a tendency to concentrate within the feed system. This sample is labeled "Run No. 7-Accumulated." As shown in Table 14, the explosives concentrations for "Run No. 7-Accumulated" were somewhat than for "Run No. lower 7-Processed," which indicates no tendency of explosives to concentrate within the feed system. However, there was such a high degree of variability between explosives concentrations in "Run No. 7-Feed" and "Run No. 7-Processed" that these results must be considered inconclusive.

5.4 <u>Physical observations</u>. The field testing activities can be broken down into seven major areas:

- (1) Soil excavation, staging, and feeding to the hopper.
- (2) Live bottom hopper operation.
- (3) Cross conveyor operation.
- (4) Feed soil characteristics.
- (5) Feed conveyor operation.
- (6) Control system operation.
- (7) Shaft seal purge system operation.

This section provides a summary of physical observations regarding each of the foregoing areas.

5.4.1 Soil excavation, staging, and feeding to the hopper. The method used for soil excavation, staging, and feeding to the hopper for the LAAP soil was in accordance with the proposed future full-scale operational procedures. The procedure worked very well. The only problem was the inability of the tracked-excavator operator to observe the level of soil in the hopper.

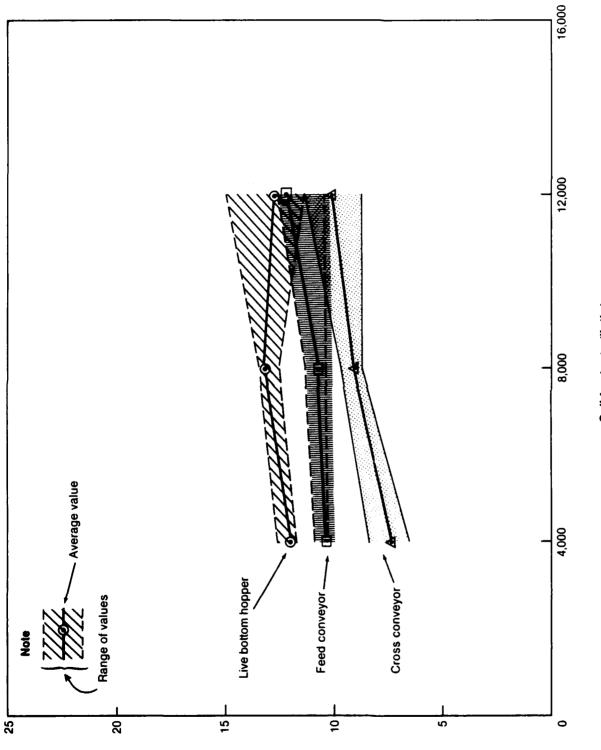


Figure 21. Motor current for CHAAP soil test runs.

Soil feed rate (lb/hr)

Conveyor motor current (amps)

-59-

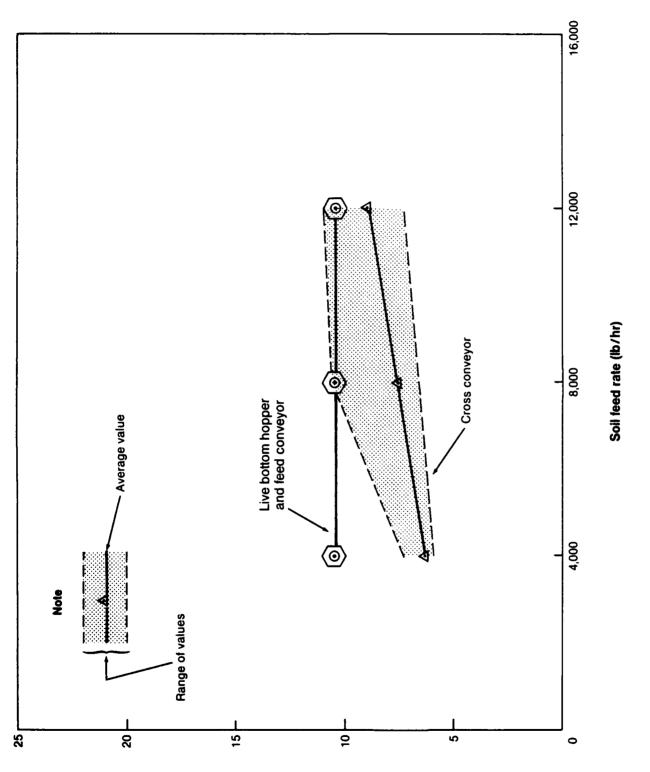


Figure 22. Motor current for LAAP soil test runs.

Conveyor motor current (amps)



TABLE 14.SUMMARY OF SOIL EXPLOSIVES CONCENTRATIONS FOR
THE LAAP TEST RUNS

LAAP run no.	2,4,6-TNT	RDX	нмх	Tetryl	Others	Totals
5 - Feed	5,833	3,357	824		77	10,091
5 - Processed	8,918	4,290	1,232	47	59	14,546
6 - Feed	169,900	26,540	6,300	3,290	60	206,090
6 - Processed	74,690	16,570	4,040	250		95,550
7 - Feed	93,990	20,141	4,830	320		119,281
7 - Processed	163,000	93,500	21,730			278,230
7 - Accumulated	1 160,900	31,840	6,820	1,040		200,600
Detection						
limits ²	1.0	0.8	1.4	0.8	0.6	

¹Legend

2,4,6-TNT RDX HMX	-	2,4,6 Trinitrotoluene 1,3,5-Trinitro-Hexahydro-1,3,5-Triazine 1,3,5,7-Tetranitro-Octahydro-1,3,5,7-
		Tetracyclooctane
Tetryl	_	Tetrahitromethylaniline
Others		1,3,5-Trinitrobenzene,
		1,3-Dinitrobenzene,
		Nitrobenzene,
		2,6-Dinitrotoluene, and
		2,4-Dinitrotoluene.
		(All numbers are reported as 1,3,5-Trinitro-
•		benzene.)
² Analyzed	by	high performance liquid chromatography (HPLC)

using USATHAMA Method 8H.



5.4.2 Live bottom hopper operation. The live bottom hopper proved to be a very effective and reliable metering device for maintaining system feed rate. During the formal test runs more than 300,000 pounds of soil were processed with no downtime due to hopper bridging, jams, or equipment malfunction. Control of system feed rate was provided exclusively by the live bottom hopper. The cross conveyor and feed conveyor were set at rotational speeds nearly an order of magnitude faster than the live bottom hopper. This approach was taken to minimize the potential for soil buildup and potential jamming in the cross conveyor and feed conveyor.

There was a slight tendency for bridging at the front of the live bottom hopper due to the recessed lip of the access doors. This could be corrected by building up the faces of these doors to eliminate the recess.

All feed rate conditions for both soil types were achieved without exceeding 75 percent of the maximum recommended conveyor tip speed of 2 feet per second.

Cross conveyor operation. The cross 5.4.3 conveyor operated flawlessly for the CHAAP soils. For the LAAP soils, there was a slight tendency for buildup of the sticky plastic clay to the conveyor flights. However, the clay soils would only build up to a certain level at which time the twin, counter-rotating, ribbon flight screws tended to self-clean. The net result was instantaneous decreased and increased feed rates as the material was building up or breaking free, respectively. However, over longer averaging periods (i.e., 20-40 minutes), the average feed rates were relatively stable.

All feed rate conditions for both soil types were achieved without exceeding 65 percent of the maximum recommended conveyor tip speed of 2 feet per second.

5.4.4 Feed conveyor operation. The feed conveyor operated flawlessly for both CHAAP and LAAP soils. It was not possible to observe whether similar buildups were experienced for the LAAP soil as for the cross conveyor. It is assumed that similar buildup did occur. However, due to the short length of the feed conveyor compared to the cross conveyor, the net impact was much less significant.

All feed rate conditions for both soil types were achieved without exceeding 10 percent of the maximum recommended conveyor tip speed of 2 feet per second.



5.4.5 Feed soil characteristics. The CHAAP soil had much lower moisture content than the LAAP soil. As a result, the CHAAP soil discharging from the feed conveyor was broken up into rather consistent lumps ranging from 0 to 1 inch in diameter. The LAAP soil discharging from the feed conveyor came out as considerably larger clumps of wet plastic clay. Both of the material consistencies would be quite acceptable for introduction into the rotary kiln.

5.4.6 Control system operation. All control system functions were tested while processing uncontaminated CHAAP soil. Jams were simulated individually in all three conveyors by lowering the motor amp limit switches. Lowering the "high" limit switch for each conveyor until it tripped simulated an overloaded condition for the conveyor. This condition simply alarms the operator and shuts down upstream conveyors until the overload condition clears. At this time, the upstream conveyors become permissive and the operator can manually restart them. Lowering the "high-high" limit switch for each conveyor until it tripped simulated a jam for the conveyor. This condition alarms the operator, shuts down upstream conveyors, and automatically reverses the conveyor for 3/4 of a revolution. The conveyor then automatically attempts to restart in a forward direction. If it jams again, this procedure automatically repeats. If it jams again, the conveyor automatically shuts down. Once the jam is cleared the conveyor and upstream conveyor become permissive and the operator can manually restart them.

All of the alarm conditions specified previously in Table 5 were tested as discussed above and functioned properly.

5.4.7 Shaft purge system operation. A shaft seal purge system was installed to preclude migration of explosivescontaminated material into the seals. The shaft bearings are all outboard of the material flow path. The shaft seals are compression seals filled with braided Teflon®. Originally, a compressed air purge was to be installed. However, during installation it was decided that a low pressure (i.e., gravity feed) oil seal purge system was more advantageous for the following reasons:

- (a) A compressed air purge could over-pressurize the seal, causing the opening of a free path for contamination into the seal.
- (b) The compression seals are not well suited for compressed air purge.
- (c) The flow of air through the seal would tend to dry the seal internals, resulting in a potentially hazardous situation due to explosives sensitivity.

0492B



(d) If a fire were to propagate within the feed system, introducing air through the seals would introduce oxygen which may promote the fire.

Therefore, a gravity oil seal purge system was installed which performed very well.



6. CONCLUSIONS AND RECOMMENDATIONS

6.1 <u>Conclusions</u>

- (a) The feed system successfully demonstrated the ability to safely and reliably process 50 to 150 percent of the design feed rate (8,000 lb/hr) of explosivescontaminated soils. During the formal test runs more than 300,000 pounds of soil were processed.
- (b) With the exception of lump size reduction for the CHAAP soil, the feed system did not significantly affect the feed soil grain size distribution.
- (c) Curves were developed which correlate variable speed drive settings with conveyor rotational speeds (in rpms) and tip speeds (in feet per second).
- (d) Curves were developed which correlate conveyor motor amps with soil feed rate. Variations in motor amps do not appear to be significant enough to serve as a basis for predicting or controlling the feed rate.
- (e) A practical soil excavation, staging, and feeding technique was developed for full-scale field operations.
- (f) The live-bottom hopper proved to be a very reliable and effective metering device for maintaining system feed rate.
- (g) The control system was fully tested and functioned properly.
- (h) The gravity oil seal purge system performed very well. It was easy to monitor and to maintain.
- (i) Analysis of soils compacted in the conveyor trough after Test Run No. 7 demonstrated no tendency for explosives to accumulate in the system during operation. However, due to the short duration of the test and the variability of explosives concentration in the feed and processed soils, these results are inconclusive.
- (j) Table 15 provides a summary of the recommendations from the "Hazards Analysis of Incinerator Feed System (see Appendix D) conducted by Allegany Ballistics Laboratory (ABL) and how the recommendations were applied during actual field tests of the feed system.

	Recommendations		How applied during the field tests of the feed system
Ē	The mandatory recommendations are:		Responses to Mandatory Recommendations
<u>-</u>	1. The incinerator feed system (IFS) must be operated remotely (unattended) when handling explosives-contaminated soils. The separation between the operating unit and personnel must be based on standard distance tables which take into consideration the hopper's capacity, compaction, explosive concentration, the potential blast overpressure, thermal radiation from a fire ball, and primary fragment dispersion from an explosion.		1. The control panel was located approximately 100 feet from the feed system to allow remote operation. Video cameras were installed to allow observation of the feed system remotely. Personnel access was minimized to the fullest extent practical when processing the LAAP explosives-contaminated soils. Fire hoses were used to continuously wet the entire test area and lagoon soils to reduce soil sensitivity.
~	Wooden "bang" boards must be installed on the top flanges of the hopper to prevent accidental metal-to-metal contact of the dumper and hopper.	~	Wooden "bang" boards were installed on the top flanges of the hopper. Also, plywood sheets were installed on the weigh scale and concrete pad areas where the self-dumping hoppers were staged to reduce potential for metal-to-metal or metal-to-concrete friction.
ς.	 Procedures and rules must be established calling out acceptable tools and techniques for clearing hopper bridging and screw jams. Nonsparking metal tools may not be adequate or proper due to the impact process potentials of the materials. 		In addition to using nonsparking tools, the standard procedure for cleaning hopper bridging (which never happened) or screw jams was to first deluge the area with the fire hose to reduce the material sensitivity.

The nonmandatory recommendations are:

- Lagoon material should be inspected prior to dumping to assure it is damp, and does not contain rocks or foreign metal materials.
- Rock, frozen, or dried lumps should not be fed to the IFS.
- 3. Adequate water should be available for dampening lagoon material, remote fire fighting, wash out, and initiation suppression.
- Jams in screw conveyors should be washed to remove all possible contamination before attempting repairs. Jams in screw 4
- Washings of the IFS should be collected for disposal or directed back to the lagoon to prevent contaminating additional soil. ۍ .
- All area tools should be accounted for prior to starting or resuming operation of the IFS.

<u>Responses to Nonmandatory Recommendations</u>

- was inspected manually and oversize rocks and foreign metal materials were removed. Lagoon material -
- All LAAP lagoon soils were saturated with water prior to feeding to the system. 2.
- Water supply at the LAAP site was more than adequate. ÷.
- See Note 3 above. This was standard operating procedure. 4.
- All washings were dircted to lagoon No. 12, which was adjacent to the test site. ۍ .
- All area tools were accounted for prior to starting or resuming system operation. و.

1	Recommendations		How applied during the field tests of the feed system
~	7. Consideration should be given to using wooden. plastic, or fiberglass materials of construction for shovels, rakes, hoes, and hopper bridge clearing rods.	٦.	7. Shovels and tools to be used for cleaning bridging were either wood and brass or plastic.
00	8. A combustion products infrared analyzer with samplers located above the hopper and at the final screw outlet may detect early signs of decomposition or initiation and allow for shutdown and the addition of quenching water.	в.	This system was not applicable for the field test since the system was not actually feeding an incinerator. Video monitors were used to allow remote observation of smoke or fire.
6	9. Personnel in the area should be protected with flame-resistant cloth coveralls.	9.	9. Personnel exposed to the explosives-contaminated soils wore Tyvek overalls. Due to high ambient temperatures, heavy flame-resistant cloth overalls were not recommended.



6.2 Recommendations

- (a) It is recommended that the feed system (incorporating the modifications described herein) be made available to DOD contractors for use on incineration remedial action projects.
- (b) It is recommended that the live-bottom hopper variable speed drive be used to manually control system feed rate. The cross conveyor and feed conveyor should be run at 25 and 30 rpm, respectively. This will preclude material buildup in these conveyors while operating at speeds below the recommended maximum tip speeds.
- (c) It is recommended that a warning sign and a physical stop (i.e., bolt) be placed on the variable speed drives for the cross conveyor and feed conveyors to limit conveyor tip speeds to no more than 2 feet per second. The recommended maximum variable speed drive setting for the feed conveyor is 1.5 and 2.0 for the cross conveyor.
- (d) It is recommended that a large convex mirror be placed above the live-bottom hopper to allow the tracked excavation operator visual observation of the soil level in the hopper.
- (e) It is recommended that the live-bottom hopper doors be built up with a metal plate to provide a smooth internal surface and preclude bridging in the hopper.
- (f) It is recommended that the control system be modified so that the system diagnostic warning lights on the control panel remain on after the annunciator is silenced.
- ABL's recommendations, (q) Based on additional testing should be considered to determine whether the higher concentrations of explosives such as found in the LAAP sludge will respond with sustained burning and transition to an explosion at energy levels above those in the process, and which exceed the equivalent energy levels of the sensitivity tests, but which are much lower than the energy levels associated with propagation tests.
- (h) Upon review of this report, the Department of Defense Explosives Safety Board (DDESB) and the U.S. Army Armament, Munitions and Chemical Command Field Safety Activity (FSA) have determined the following:
 - (1) The incinerator feed system test has demonstrated the capability of the feed system to safely transport the explosives-contaminated soils that were used during the test. However, because of the nonhomogeneity of lagoon sediments, operational procedures should be established to ensure that the explosives content of the sediment is less than 25 percent dry weight before it is



introduced into the feed system. In lieu of this, operation protection must be provided against hazardous fragments and overpressure, assuming the maximum credible event to be a detonation involving the total amount of explosives in the feed system and the incinerator.

- (2) All sediment at an operational site should be adequately wetted to preclude the initiation of a fire or detonation prior to introduction of the sediment into the incinerator, i.e., within the feed system. A capability should be established to maintain an adequate sediment moisture content in the feed system during periods of extended shutdown.
- (3) An integrated systems test of the feed system and the incinerator should be conducted under actual operating conditions before system parameters are finalized. A site plan and safety submission for this test should be prepared and submitted to DDESB and FSA for approval prior to the start of the test. The results of this test will provide the basis for a DDESB review of the site plans and safety submissions required for sediment decontamination operations at selected Army installations.