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**US Army Corps
of Engineers**

Construction Engineering
Research Laboratory

Human Response to Helicopter Noise: A Test of A-Weighting

by
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Department of Defense and U.S. Army policy has long been to adjust measured helicopter noise levels upwards to account for the special character of helicopter noise in terms of human and community annoyance. In the United States, the A-weighted Day/Night Average Sound Level (DNL) descriptor is used most often for this purpose, but research has shown that it is not completely adequate. Also, many questions remain about human perception of, and response to, helicopter noise and the rattles and vibrations it causes. Since sound exposure level (SEL) is the fundamental building block to DNL, SEL has been used as the unit of study in this research.

This study is an extension of earlier research in which an Army UH-1H (Huey) helicopter was flown over a test site that included a farmhouse, a tent, and a new mobile home. This report documents a follow-up test done with six different helicopters at a California Marine Corps air station to replicate and expand on the findings from the earlier study.

Overall, the data indicate that the A-weighted DNL is inadequate for assessment of helicopter noise. The C-weighted scale was also tried and found inadequate. Helicopter noise measurement by either scale must be corrected to assess the noise in a way that correctly corresponds to human perceptions. For indoor situations, use of A-weighting to assess helicopter noise requires an offset that varies with helicopter A-weighted sound exposure level (ASEL). This offset changes based on the type of helicopter (e.g., number of blades). For two-bladed helicopters, a correction factor of approximately 10 dB should be added to the measured ASEL of the helicopter sound. An 8 dB correction factor should be added to the measured ASEL of a multi-bladed helicopter.

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FOREWORD

This study was conducted for the Army Environmental Office, Office of the Chief of Engineers (OCE), U.S. Army Corps of Engineers (USACE), under Project 62720A896, "Environmental Quality Technology"; Work Unit NN-TGO, "Department of Defense (DOD) Noise Source Human Response Characterization." Cosponsors of this research were the U.S. Marine Corps and the U.S. Navy under FAD90-080002 and FAD90-080062. The OCE technical monitor was LTC Hans Graven, ENVR-E.

This research was performed by the Environmental Division (EN) of the U.S. Army Construction Engineering Research Laboratory (USACERL). Dr. Edward W. Novak is acting Chief of EN. The USACERL technical editor was Gordon L. Cohen, Information Management Office.

COL Everett R. Thomas is Commander and Director of USACERL, and Dr. L.R. Shaffer is Technical Director.

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HUMAN RESPONSE TO HELICOPTER NOISE: A TEST OF A-WEIGHTING

1 INTRODUCTION

Background

How a community responds to helicopter noise is only a partially answered question. Many researchers have tried to find a simple measurement of human annoyance caused by helicopter noise but, so far, no measure is considered completely adequate.¹ An "A-weighted" scale², a sound measure that attempts to emulate how humans respond to impulsive noise, is the most common method in use today. In the U.S., the A-weighted Day/Night Average Sound Level (DNL) descriptor is most commonly used to estimate the percentage of a community that is highly annoyed by noise. However, many questions remain about human perception of helicopter noise and the role of rattles and vibrations in the human and community response to it. For many years it has been the policy of the Department of Defense (DOD) and the U.S. Army to add a constant penalty (adjustment) to measured helicopter noise levels to account for its special character.³ The U.S. Army Construction Engineering Research Laboratory (USACERL), with support from the Federal Aviation Administration (FAA), initiated a major research program to examine descriptors for helicopter noise and study the role of helicopter noise-induced vibration and rattle. The first phase of this program showed that if the helicopter noise induced high levels of window rattling, then A-weighting was inadequate and a large adjustment to the measurement (10 to 20 db) had to be made.⁴

In the first phase of this program, performed near USACERL in Savoy, IL, an Army UH-1H (Huey) helicopter was flown over a test site that included a farmhouse, a tent, and a new mobile home. Subjects were asked to compare the noise of the helicopter flying by to a control noise, and indicate which was more annoying. For each helicopter flyby, a research assistant was asked to rate the amount of rattle present on a three-point scale: "none," "some," or "a lot." The data were analyzed by test location and level of rattle, and curves were developed that established equivalency between the helicopter noise and the control noise. It was found that the human response curve depended on the level of rattle caused by the helicopter, and that the A-weighted curve was not sufficient to fully assess the noise of the UH-1H.⁵

¹ J.B. Ollerhead, *Laboratory Studies of Scales for Measuring Helicopter Noise*, National Aeronautics and Space Administration (NASA) Contractor Report 3610 (NASA, November 1982); John A. Molino, *Should Helicopter Noise Be Measured Differently From Other Aircraft Noise? - A Review of Psychoacoustic Literature*, NASA Contractor Report 3609 (NASA, November 1982).

² American National Standards Institute (ANSI) 512.9-1988, *Quantities and Procedures for Description and Measurement of Environmental Sound, Part 1* (New York, 1988).

³ DOD Instruction 4165.57, *Air Installations Compatible Use Zones (AICUZ)* (DOD, 8 November 1977); Army Regulation 200-1, *Environmental Protection and Enhancement*, Chapter 7, Environmental Noise Abatement Program (Headquarters, Department of the Army [HQDA], Washington, D.C., June 15, 1982).

⁴ Paul D. Schomer and Robert D. Neathammer, "The Role of Helicopter Noise-Induced Vibration and Rattle in Human Response," *J. Acoust. Soc. Am.*, Vol 81, No. 4 (April 1987), pp 966-976.

⁵ Paul D. Schomer and Robert D. Neathammer, *The Role of Vibration and Rattle in Human Response to Helicopter Noise*, Technical Report (TR) N-85/14/ADA162486 (USACERL, September 1985).

The U.S. Navy and U.S. Marine Corps, also interested in properly assessing helicopter noise, proposed tests that would expand on the Savoy findings. These tests were conducted at the Marine Corps Air Station at Tustin, CA (MCAS Tustin).

Purpose

The purpose of the follow-up study at MCAS Tustin, the subject of this report, was to replicate and expand on the findings from the Savoy test. The data would be used to expand the research on an accurate measure to describe human and community response to helicopter noise, and the role played by noise-induced rattle. This test would add to the data available on the effects of different types of helicopters and housing constructions on the human response to helicopter noise.

Approach

The approach to this test was the same as for the Savoy test; this was required since one objective was to replicate the Savoy study. Juries of test subjects were asked to compare the noise from a helicopter flying over to a control white noise. By varying the type of helicopter and the slant distance of the helicopter from the houses containing the juries, a variety of sound exposure levels (SELs) was produced. From these data, statistical equivalencies could be established between various helicopter noises and control noises judged to be equivalently annoying. The other objective—expansion of the Savoy results—was accomplished by performing the test in a new location with different test house construction and different types of helicopters. However, for purposes of comparison with the previous test, the Tustin test included an Army UH-1H helicopter.

Mode of Technology Transfer

The Army will use these data as input to revisions of Army Regulation (AR) 200-1, *Environmental Protection and Enhancement, Chapter 7: Environmental Noise Abatement Program*. It is also expected that the Navy, Marine Corps, U.S. Air Force, and the FAA will use these data as input for developing recommendations on heliports.

2 STUDY CONCEPTS

This study was performed using juries of test participants, some in the living rooms of adjacent test houses (duplexes) and others at an outdoor location in line with these houses. The duplex houses used were enlisted quarters at MCAS Tustin (Figure 1). The general layout of the four test residences (in three structures), the outdoor group (tent site), and the instrumentation truck are shown in Figure 2. Six different types of helicopters were used to create the noise stimuli: CH-53A/B, CH-53E, CH-46E, UH-1H, UH-1N, and AH-1W. These helicopters flew by the test houses at a variety of slant distances to create a wide assortment of single-event SELs.

The test was designed as a paired comparison test in which the subjects were presented with pairs of differing noise stimuli. One noise was generated by the helicopter flying by and the other was white noise played through a loudspeaker. The participants were asked to decide which noise was more annoying. As previously noted, the purposes of this test were to replicate and expand on the Savoy study, so the Savoy test protocol was used.⁶ As in Savoy, the amplitude of the white noise was modulated in a "haystack" pattern. The shape of this modulating pattern was chosen to approximate the 10 dB down time of the passing helicopter. (The 10 dB down time is defined as the time that the helicopter's sound takes to rise from 10 dB below its maximum level to the maximum, and then fall back to 10 dB below the maximum.) Two examples of the haystack distribution are shown in Figure 3.

It is important to note that in this test protocol everything except for the control stimuli is real; real helicopters were used instead of recordings and loudspeakers. This was done to produce the very low-frequency sounds, the rattles, and the vibrations characteristic of helicopter noise. These conditions would be too hard to simulate realistically in a laboratory, so the data had to be taken in this field setting.

Figure 4 shows a typical curve expected from the experiment for a single white-noise control level. Many curves of this type were generated. Each yields a pair of numbers: a helicopter SEL and corresponding control A-weighted SEL (ASEL). This pair of numbers describes a point on the curve where 50 percent of the subjects perceived the helicopter noise to be more annoying than the control white noise and 50 percent perceived it to be less annoying. This point, as marked on Figure 4, was taken as the equivalency point—the point at which the control noise causes the same annoyance as the helicopter noise. The number of decibels that the helicopter noise differs from the equivalently annoying control noise is the "offset," or adjustment. For the example, in Figure 4 the helicopter ASEL is 62 dB and the equivalent control noise ASEL at the 50 percent point is given as 66 dB. Therefore, a 4 dB offset must be added to the A-weighted helicopter SEL to make it equivalent to a white noise having the same annoyance.

Figure 4 is not a straight line; it saturates at 0 and 100 percent. In general, the curve in Figure 4 has a sigmoid shape and, in theory, should be the integral of a normal probability function.⁷ With this assumption, the sigmoid shaped curve can be transformed into a straight line by either plotting the data on normal probability paper or by transforming the individual data points to their corresponding Z-scores. In this transformation it is necessary to assume that the data are a subset of an underlying distribution having a mean of 50 percent. Great care was taken to see that most data were gathered where the sigmoid curve is approximately a straight line. As a result, as is shown later, regression lines fit directly to the

⁶ Paul D. Schomer and Robert D. Neathammer, 1987.

⁷ J.W. Kling and Lorran A. Riggs, *Woodworth and Schlosberg's Experimental Psychology*, 3d Ed., Chapter 2, "Psychophysics" (Holt, Rinehart, and Winston, Inc., 1972).

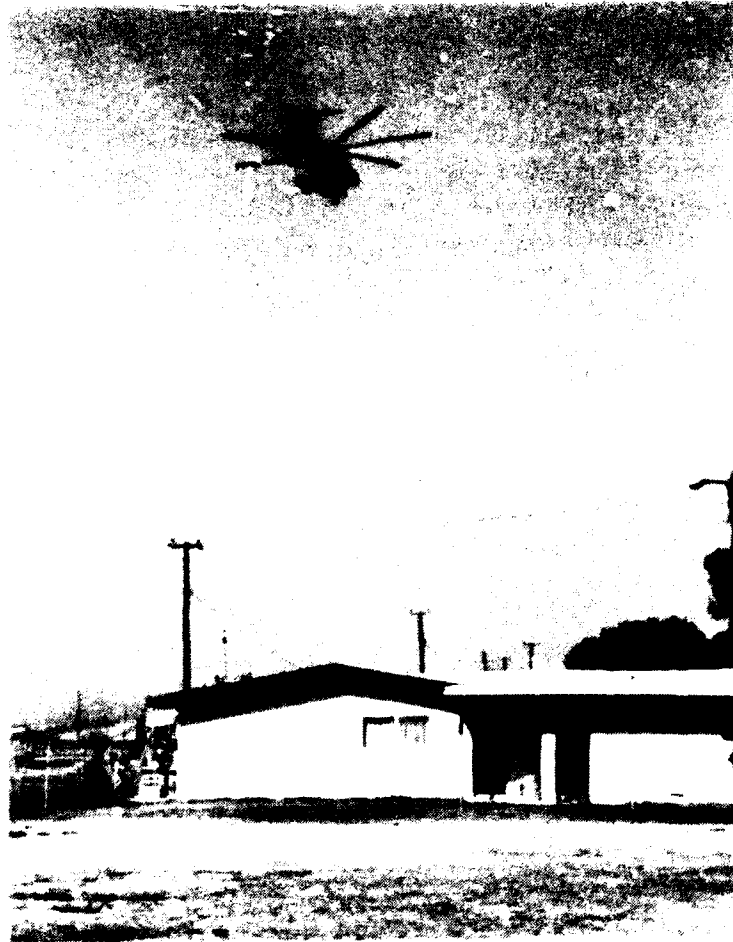


Figure 1. Two Views of MCAS Tustin Test House.

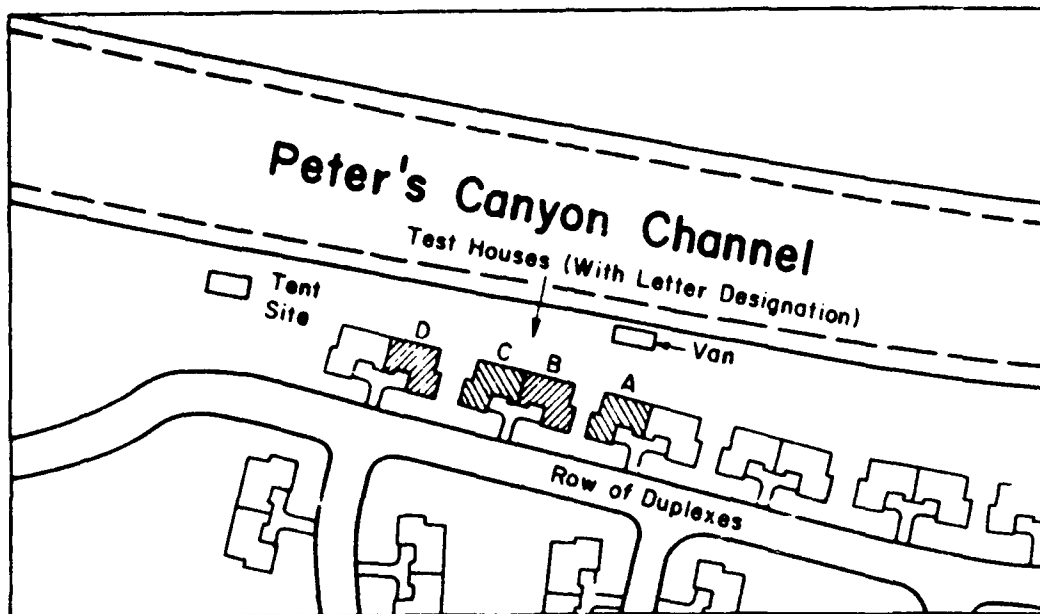


Figure 2. Layout of MCAS Tustin Test Site.

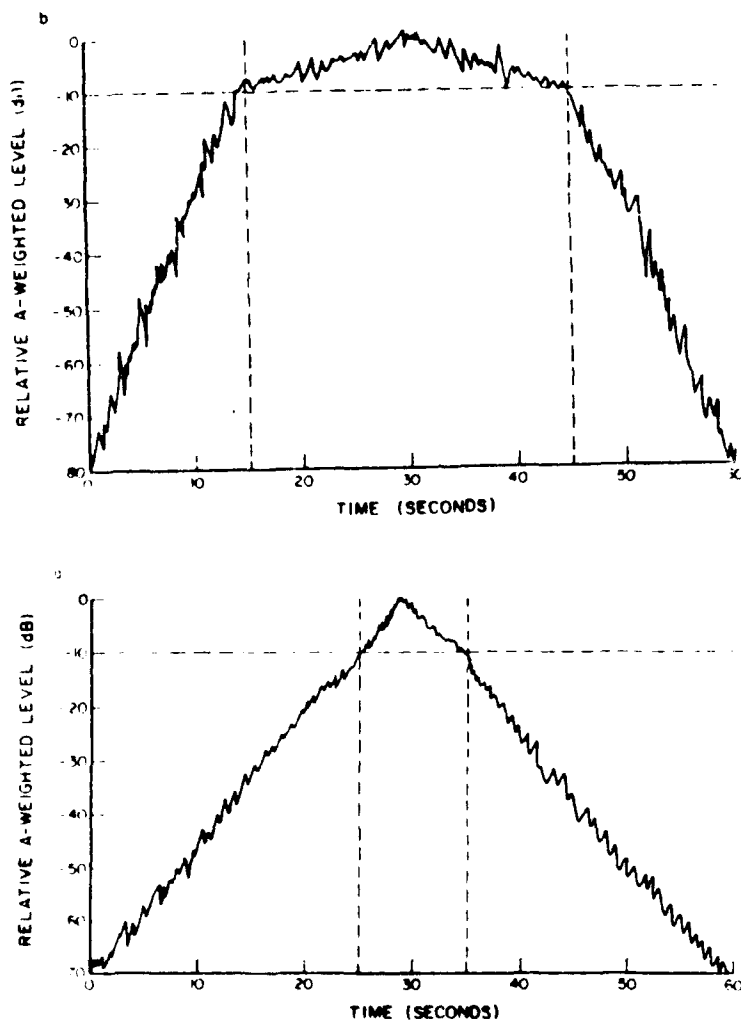


Figure 3. Two Examples of "Haystack" Distribution.

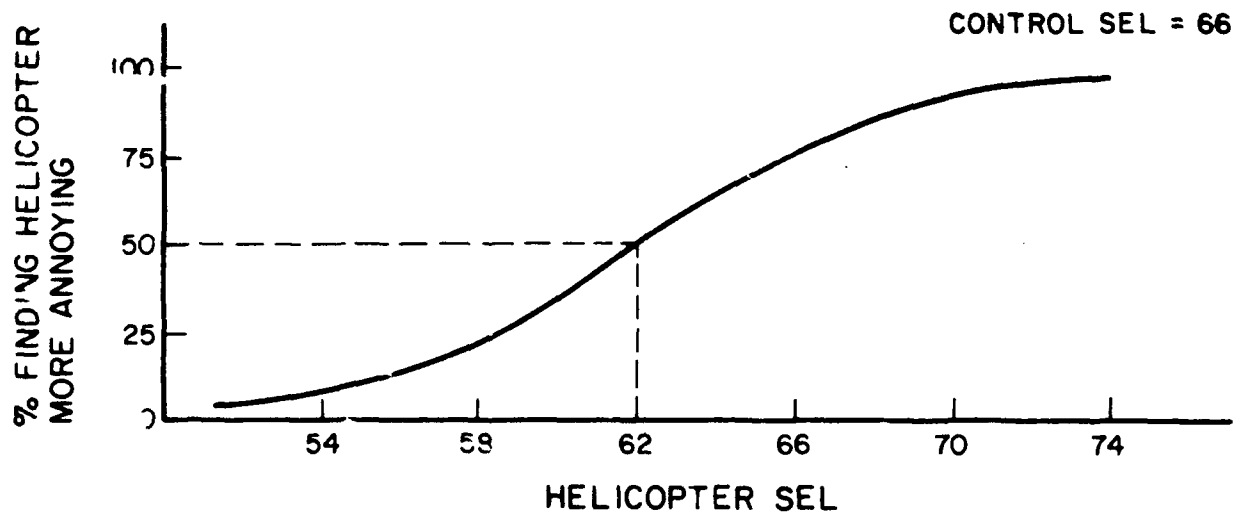


Figure 4. Typical Curve Expected for a Single White-Noise Level.

data are as good or better than lines fit to the Z-scores. So in this analysis, regression lines fit to the raw data are used.

In this test the objective was to collect information on how different helicopters are perceived differently in terms of the noise they generate. Of the six different types of helicopters used, the AH and two UH helicopters are two-bladed; the three CH helicopters are multibladed. Approximately 100 subjects were tested using each of the six helicopter types for a total of about 600 subjects.

It is important to note that concepts such as rattle, vibration, and loudness were not mentioned to test participants. The instructions stated that the subjects should mark their answers according to which stimulus in each pair was "more annoying or bothersome," or which sound they "would rather not hear again if given a choice."

3 DATA COLLECTION

The General Area

The test site, at MCAS Tustin, is in the Los Angeles metropolitan area. As previously noted, three adjacent duplex houses (four residential units) and a field just south of these houses (Figure 2) were used. The test site was at the edge of a residential area. On the other side of the site was a cornfield 1 mile (1.6Km) wide and the airfield. Tests were occasionally halted when there were other helicopters in the area, but the air station rescheduled most of its helicopter maneuvers to avoid conflicting with the test.

The Test Site

The subjects were placed in four living rooms, three of which were constructed exactly the same, and the fourth had only minor differences. Since each of the quarters was actively occupied by an enlisted family, each of the living rooms was furnished slightly differently. The outdoor subjects were placed beneath a raised open-air tent (to protect them from the sun). The measurement truck, in which all the data were collected, was parked in the backyard of one of the houses. An equipment operator in the truck was in charge of coordinating the helicopter and had a good view of the ground track over which the helicopter was flying.

The helicopter flew parallel to the line of houses at 200 ft above ground level (AGL). Four sideline distances were used, as measured from the back of the houses: 50 ft, 500 ft, 1000 ft, and 2000 ft. Figure 5 shows an overview of the general test site, the closest and furthest ground tracks and turns used by the helicopter, and major roads and towns in the area.

The Subjects

To recruit subjects, advertisements were put into many local papers in the Tustin area. Also, school and church groups in the area were contacted to recruit the 600 people needed for this survey. Anyone who wanted to participate was told to call a local number to sign up. Recruits were then mailed information and maps showing how to get to the site. There was a follow-up call the day before the test to make sure that participants understood all directions. All subjects were paid \$40 for participating in the test. They received the money during the break between the first and second half of the test.

The subjects came from all around the area, and varied in age, sex, and background. Table 1 shows a breakdown of the subjects by age and sex.

Data Measurement Equipment

USACERL's test truck was parked in the backyard of the first house, as shown in Figure 2. The truck contained all the instruments for analyzing and recording the sound signals gathered by equipment in the houses and at the outdoor site. Two Larson-Davis 1-in. microphones (model 2570) were placed in each living room at locations calculated to obtain a good representation of the sounds heard by the subjects. The microphone signals were passed through USACERL-developed line drivers set with 30 dB gain and a Pacific amplifier (model 70A-2-2245). The amplifier had a variable gain controlled by the computer

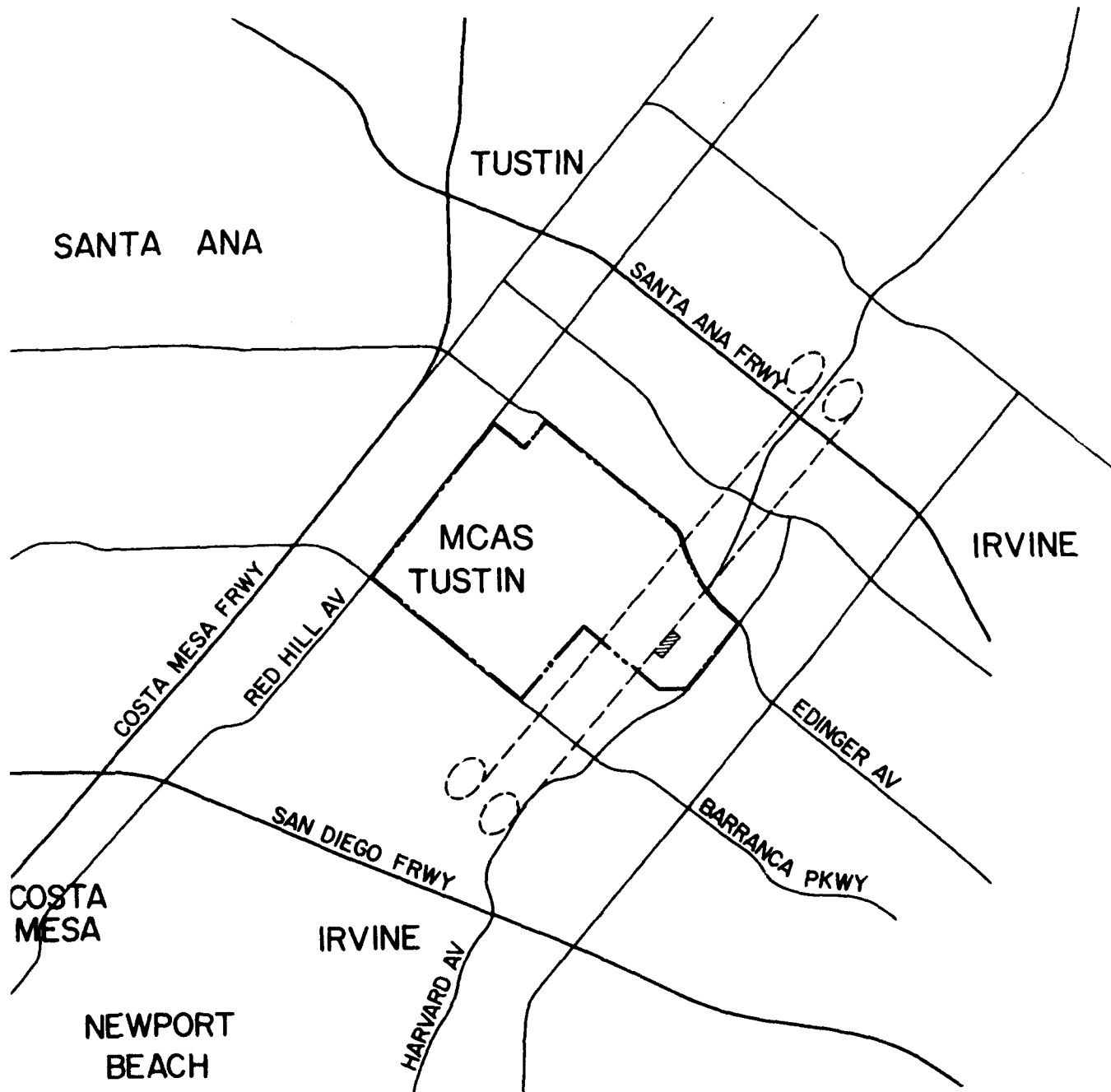


Figure 5. Overall View of Test Area.

Table 1

Breakdown of Test Subjects by Age and Sex

Age	Number of Male Subjects	Number of Female Subjects
<21	60	64
21-30	114	78
31-40	62	64
41-50	34	58
51-60	30	55
61+	42	70

in the truck. At the truck, the signal from each test setting was digitally recorded using the video channel of a Panasonic videocassette recorder (VCR model AG1900) and stereo Sony pulse code modulators (model 501es) specially modified to operate from 0.1 Hz through 10 kHz with no high-frequency pre-emphasis (instead of the normal 20 Hz through 20 kHz range). The signal was analyzed using a USACERL-developed integrating noise monitor and sound exposure level meter. These instruments calculated the A-weighted SEL and A-weighted peak sound level for each stimulus.

Figure 6 illustrates the instrumentation setup. The outdoor data were taken with one B&K 4921 1-in. microphone system placed with the subjects under the tent and another installed 30 ft directly above the test truck. An Endevco accelerometer was placed on the glass porch door of each residence, facing the line of flight of the helicopter. These data were recorded directly onto the audio channel of the VCR. Notes about each run were recorded onto a voice channel of each VCR by the operator in the measurement truck.

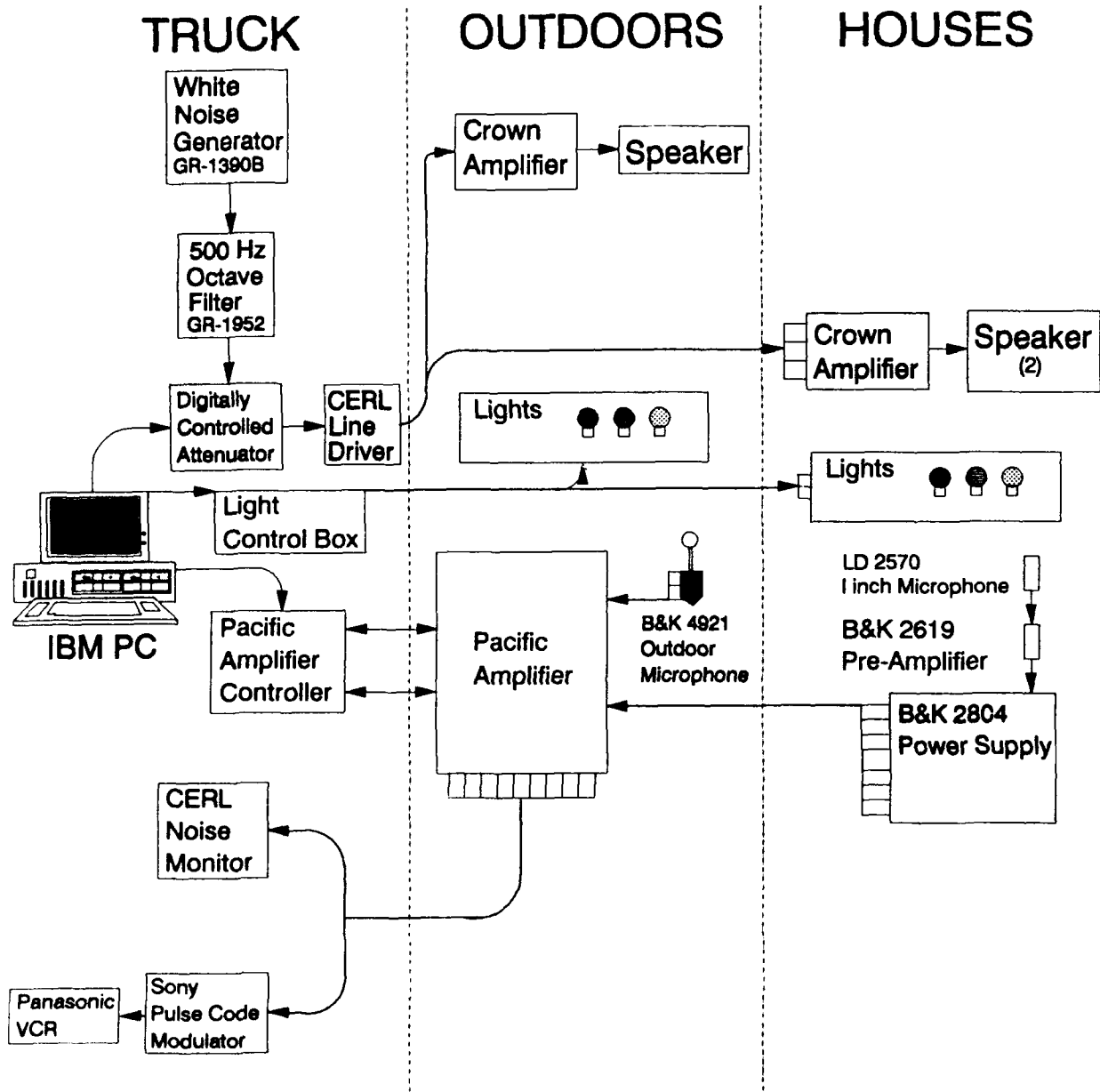
An IBM personal computer (PC) controlled signal amplifier gain and regulated the control noise.

Control Noise

The control noise was created by a white-noise generator and filtered by a 500 Hz octave band filter, and attenuated by a programmable attenuator controlled by the PC. Using the attenuator, the computer controlled the SEL and the 10 dB down times of the control noise.

The indoor control noise stimuli were presented at ASEL intervals of 4 dB, from 56 through 92 dB. Thus 10 different control noise ASELs were generated. In each run, the noise would gradually rise from inaudible to 10 dB below the maximum level, then rise to maximum at a different rate, and finally decay at approximately the same rate (as illustrated in Figure 3). The 10 dB down time of the control noise was varied according to the slant distance and type of helicopter flying by to approximate the amplitude-versus-time pattern of the helicopter's noise.

The control noise in each house was generated by a single loudspeaker. The outdoor control noise was the same as the one used indoors except it was played 20 dB higher. The 20 dB gain was used outdoors because the A-weighted attenuation of a typical house from outdoors to indoors is normally about 20 dB.



NOTE: Pacific amplifier was connected to five monitor/modulator/VCR setups like the one shown—one for each test setting. The power supply and amplifier for indoor recording also had multiple inputs and outputs, as shown above.

Figure 6. Data Measurement Equipment Setup.

The Test

The test took approximately 3 hours, with the morning session starting at 9 a.m. and the afternoon session starting at 2 p.m. The participants met before the test at a parking lot outside the front gate of MCAS Tustin and were driven to the test site by bus. When they got off the bus they received information on how the test was going to be run and a folder containing two different test forms and a consent form. Figures 7, 8, and 9 respectively show the consent form, an annoyance factor form, and a follow-up form. The subjects were then split into random groups of five or six. They were taken to their test house by a USACERL research assistant, who gave them more information about how the test was to be run.

Before the actual test started, there was a pretest to make sure all participants understood what they were to do. The pretest used recorded jet airplane noise and the control white noise as an example test pair. For the first two pretest pairs, the ASEL of the two sounds in each pair differed greatly. In the first pair the first sound was clearly louder; in the second pair the second sound was clearly louder. In the third pair, the SELs of the two noises were equal. USACERL research assistants would check the participants' answers after each pretest run. The first two pretest pairs were used to verify that everyone understood the instructions. If a test subject chose the wrong answer during the pretest, the researcher would re-explain the instructions to everyone. If necessary, more pretest pairs were run until everyone fully understood the instructions.

Each run was conducted in four phases. First, a red light would be lit and subjects would concentrate on the first sound of the pair. Second, a yellow light would be lit and the participants would listen to the second sound of the pair. Each of the noises lasted for approximately 1 minute. Third, a green light would be lit and the subjects would have approximately 15 seconds to mark on the appropriate test form which noise was more annoying. During the green light, the USACERL researchers were also recording their judgment of the rattle levels on their forms. Finally all lights would be turned off, and the subjects would wait until the red light was turned on to start the next pair of sounds. When each light was turned on, a bell would also ring softly to make sure people noticed that a new phase of the run had started.

The PC in the truck controlled all of the lights and the bell along with the amplifier gains and the generation of the control noise. The operator of the PC was in radio and visual contact with the helicopter. In this way, the entire test was very precisely coordinated.

The test consisted of 46 pairs of stimuli. For half the pairs, the helicopter noise would be presented first; for the other half, the control noise would be first. Since it would have been impractical to completely randomize which source of noise came first in any pair, the order of presentation was switched every six or seven runs. The order was switched every other test session, so for one session the helicopter noise would be presented first during the first run; for the next session the control sound would be presented first during the first run.

The annoyance factor test form (Figure 8) was used by the subjects to mark which noise was more bothersome or annoying. Subjects marked the form after every pair of sounds. The subjects were also told to mark how difficult it was to make this decision. They judged difficulty in deciding on a scale of 1 to 5, with 1 being "very easy" and 5 being "very hard." It is important to note that test participants were required to decide which sound of the pair was more annoying or bothersome for every run. Subjects were required to make a decision: they could not say the two sounds were equally annoying, but they could indicate that it was "very hard" to decide.

INFORMATION FOR TEST PARTICIPANTS

You will be asked to compare the annoyance of up to 50 helicopter flyovers with the annoyance of a similar number of other sounds. You will have to listen attentively to these sounds for periods of about an hour between breaks. There will be two of these periods during the test. You may find some of the sounds unpleasantly loud or annoying. None of the sounds will be so loud or long as to impair your hearing in any way.

The only direct benefit to you for participation in the study will be your payment of \$40.00. Payment will be made at the end of the testing period.

If you have any questions about the nature of today's experiment, please ask them now. If you are satisfied with your understanding of what your participation will involve, and are willing to participate, please so indicate by signing the form below.

INFORMED CONSENT FORM

I understand that my participation as a test subject in the experiment being conducted by CERL today will require me to listen to up to 50 helicopter flyovers, and to compare their annoyance relative to an equal number of other sounds. These judgments will be made in the company of other test subjects, seated in groups, for a period of about 1 hour each. I also understand that some of the sounds I will hear may be unpleasantly loud, but that they will not pose any risk of damage to my hearing.

The only direct benefit to me for my participation in the experiment will be the payment made for my time. I understand that I can freely withdraw from participation in the experiment at any time, and that I will be paid for my participation up to the time I decide to stop. I have had the opportunity to discuss the nature of the experiment, and am willing to participate in the study.

DATE: _____ SIGNED: _____

Do you have any reason to believe your hearing is less than normal? Yes _____ No _____.

If, yes, to the best of your ability, please describe your hearing problem. (use the back side of this form if you need more room.)

Figure 7. Consent Form.

SCANTRON FORM NO. 23305-USA

FEED THIS DIRECTION

SCANTRON FORM NO. 23305-USA

8	4	2	1	8	4	2	1	8	4	2	1
A	B	0	1	2	3						
C	D	0	1	2	3	4	5	6	7	8	9
A	B	C	D	1	2	3	4	5	6	7	8
JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0	1	2	3	4	5	6	7	8	9		
8	4	2	1	8	4	2	1	8	4	2	1

TEST # _____ PAGE # _____

SEQ # _____ DAY _____

LOCATION _____ POSITION _____

MONTH _____

YEAR _____

SUBJECT # _____

TEST SUBJECT RESPONSE SHEET

NAME _____

IMPORTANT	
• USE #2 PENCIL	
• MAKE DARK MARKS	
• EXAMPLE: <input type="checkbox"/> A <input type="checkbox"/> B <input checked="" type="checkbox"/> C <input type="checkbox"/> D <input type="checkbox"/> E	
• ERASE COMPLETELY TO CHANGE	

Trial	MARK THE MORE ANNOYING NOISE		HOW HARD WAS IT TO DECIDE?				
	First	Second	Very Easy				Very Hard
1	F	S	1	2	3	4	5
2	F	S	1	2	3	4	5
3	F	S	1	2	3	4	5
4	F	S	1	2	3	4	5
5	F	S	1	2	3	4	5
6	F	S	1	2	3	4	5
7	F	S	1	2	3	4	5
8	F	S	1	2	3	4	5
9	F	S	1	2	3	4	5
10	F	S	1	2	3	4	5
11	F	S	1	2	3	4	5
12	F	S	1	2	3	4	5
13	F	S	1	2	3	4	5
14	F	S	1	2	3	4	5
15	F	S	1	2	3	4	5
16	F	S	1	2	3	4	5
17	F	S	1	2	3	4	5
18	F	S	1	2	3	4	5
19	F	S	1	2	3	4	5
20	F	S	1	2	3	4	5
21	F	S	1	2	3	4	5
22	F	S	1	2	3	4	5
23	F	S	1	2	3	4	5
24	F	S	1	2	3	4	5

Trial	MARK THE MORE ANNOYING NOISE		HOW HARD WAS IT TO DECIDE?				
	First	Second	Very Easy				Very Hard
1	F	S	1	2	3	4	5
2	F	S	1	2	3	4	5
3	F	S	1	2	3	4	5
4	F	S	1	2	3	4	5
5	F	S	1	2	3	4	5
6	F	S	1	2	3	4	5
7	F	S	1	2	3	4	5
8	F	S	1	2	3	4	5
9	F	S	1	2	3	4	5
10	F	S	1	2	3	4	5
11	F	S	1	2	3	4	5
12	F	S	1	2	3	4	5
13	F	S	1	2	3	4	5
14	F	S	1	2	3	4	5
15	F	S	1	2	3	4	5
16	F	S	1	2	3	4	5
17	F	S	1	2	3	4	5
18	F	S	1	2	3	4	5
19	F	S	1	2	3	4	5
20	F	S	1	2	3	4	5
21	F	S	1	2	3	4	5
22	F	S	1	2	3	4	5
23	F	S	1	2	3	4	5
24	F	S	1	2	3	4	5

Figure 8. Annoyance Factor Form.

After the entire test was over, the participants were asked to rate how annoying different components of the noise were on the follow-up form (Figure 9). The noise components were given four arbitrary characteristics: hissing, rumbles, rattles, and loudness. The participants were asked how each characteristic related to their judging of either event as bothersome or annoying. They rated each of the four characteristics for each sound as "not annoying," "somewhat annoying," or "very annoying."

Subject Number _____

During the main part of this test you have observed pairs of events. Please mark how each of the following caused you to find either event bothersome or annoying. Circle your choices.

	Loudspeaker Event			Helicopter Event		
	Not Annoying	Somewhat Annoying	Very Annoying	Not Annoying	Somewhat Annoying	Very Annoying
Hissing	Not Annoying	Somewhat Annoying	Very Annoying	Not Annoying	Somewhat Annoying	Very Annoying
Rumbles	Not Annoying	Somewhat Annoying	Very Annoying	Not Annoying	Somewhat Annoying	Very Annoying
Rattles	Not Annoying	Somewhat Annoying	Very Annoying	Not Annoying	Somewhat Annoying	Very Annoying
Loudness	Not Annoying	Somewhat Annoying	Very Annoying	Not Annoying	Somewhat Annoying	Very Annoying

Other Comments:

Figure 9. Follow-up Form.

4 DATA ANALYSIS

The responses of the participants were analyzed to determine the helicopter ASEL at which 50 percent of the subjects felt that the helicopter sound was more annoying or bothersome than the control sound. Several different types of data were collected: the response data from the subjects, the rattle levels rated by the USACERL research assistants, the ASELs of the various sounds (as measured near the subjects), the nominal value of the control sound ASEL as programmed in the PC, and the acceleration level of vibrations as measured with the accelerometer mounted on the largest window facing the helicopter line of flight.

Data Reduction

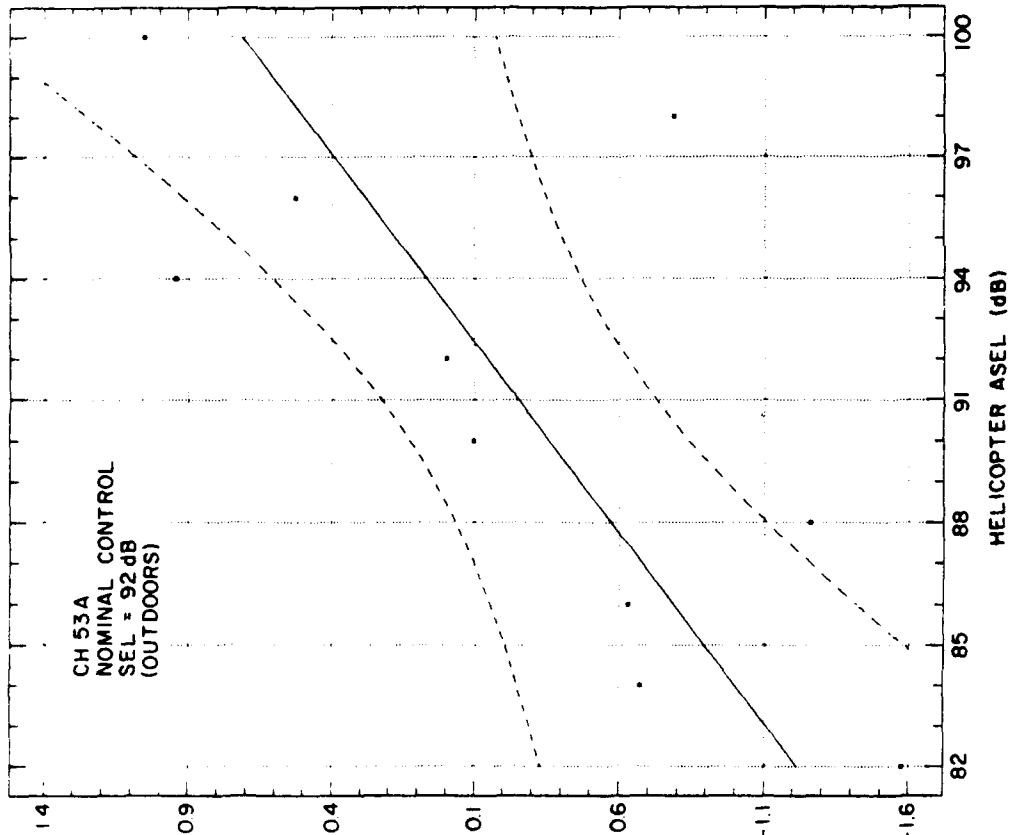
The control noise was originally designed to be produced at 10 different levels, from 56 to 92 dB, with the outdoor noise presented 20 dB higher than inside. Because of slight variations in the measured control levels, the pairs of noises were grouped into categories, or "bins." The control sound was divided into 4 dB-wide bins spread over the 26 dB range used for comparison with the sound of each individual helicopter. The helicopter ASELs were divided into 2 dB-wide bins.

After the pairs of sounds were grouped by control ASEL and helicopter ASEL, the percentage of people who found the helicopter noise more annoying was computed for each pair of stimuli. A simple test was applied to determine a confidence index for any of these percentage calculations. As previously mentioned, the subjects were required to determine the difficulty of deciding which noise was more annoying on a scale of 1 to 5. In any sample where the number of subjects amounted to less than 1.5 times the average difficulty rating reported by those subjects, that datapoint was deleted.

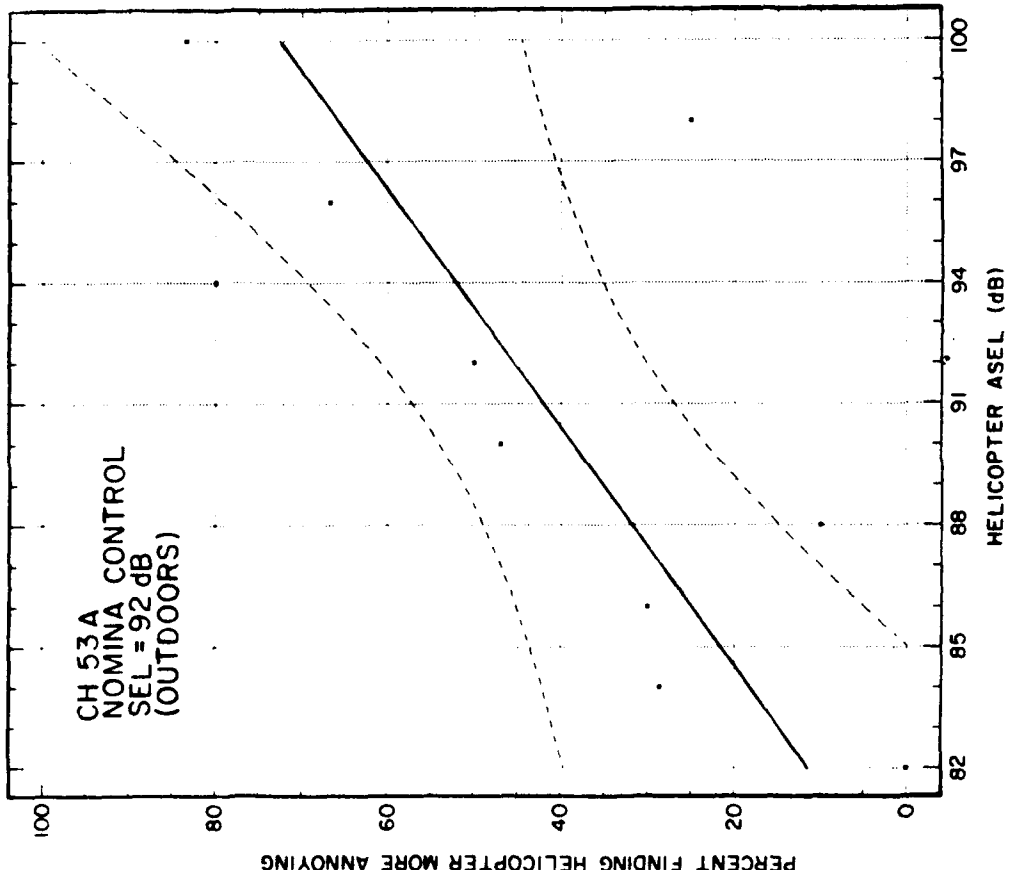
To make sure all of the houses were equivalent sound environments, the response data were divided and analyzed by location. All of the houses showed approximately the same response ± 2 dB, which is well within the expected margin of error for this test. Therefore, all indoor locations were considered to be equivalent and the data for all houses were grouped together.

Originally, as in the earlier test at Savoy, the data were also going to be divided by the level of rattle perceived by the USACERL researchers in the houses. The houses used in this test were chosen partially on the basis of their occupants reporting that rattling occurred during typical helicopter flybys. However, unlike in the earlier test, the USACERL research assistants perceived very little rattle in any of the houses. Therefore, this aspect of the Savoy test could not be replicated in the MCAS Tustin test.

Figure 10a shows a typical data plot. (Figure 10b shows a plot of the same data converted to Z-scores, as discussed in the next paragraph.) A regression line was fit to the data and confidence intervals were graphed. One of these plots was produced for each control noise level and each helicopter. Plots were produced if more than three different helicopter ASELs were observed for a particular control noise ASEL. The entire set of these plots for valid indoor data is published in Appendix A. When the plots were generated, the point at which 50 percent of the subjects felt the helicopter was more annoying than the control noise was found. Error bars were statistically generated for a 95 percent confidence interval. If the error bars fell more than ± 20 from the 50-percent point previously described, this was judged too large and the datapoint was discarded. Thus, for the datapoints finally used, there is a 95 percent chance that 50 percent of the subjects (± 20 percent) found the helicopter noise equivalent to the control noise in



a. Typical plot of data.



b. Same data converted to Z-scores.

Figure 10. Data Plots for Percentage.

terms of annoyance. An example of such discarded data is shown in Figure 11. In this example there was not sufficient helicopter data at high percentages, so the confidence interval was too large.

As noted earlier, the general shape to the data of Figure 10a is a sigmoid curve. However, care was taken to attempt to limit the data to the most "linear" region of the curve and avoid the 0 percent or 100 percent areas. As a test, Figure 10b shows a corresponding plot for the same data after they had been transformed to Z-scores. The entire set of transformed Z-score plots for valid indoor data is contained in Appendix B. Table 2 lists the resulting correlation coefficients for each plot in Appendix A and its corresponding Z-score transformed plot in Appendix B. Examination of the average correlation coefficients and the differences shows that the transformation to Z-scores provides no benefit for data analysis. Therefore, the remainder of this report uses only regression lines fit to the original subject-percentage data.

All valid indoor points calculated from each data plot in Appendix A were grouped by helicopter and plotted. Table 3 lists these data. Figure 12 is an example plot for the CH53E. The control noise judged equivalently annoying to the helicopter noise is shown as a function of helicopter ASEL. A regression line was fit to these data. In this figure, the diagonal shows the result that would have been achieved if the helicopter sound was exactly equivalent to the control sound *at the identical ASEL*. The departure of the fitted line from the diagonal shows the offset or correction as a function of helicopter ASEL.

As previously noted, the valid indoor plots for all of the helicopters tested are shown in Appendix A. Inspection of these plots showed that the results seemed to be significantly affected by how many blades the helicopter had. The response curves (e.g., Figure 11) for all the two-bladed helicopters (UH1H, UH1N, AH1W) were very similar to one another in the region of the curve from which data were taken; all of the multi-bladed helicopters (CH53A/B, CH53E, and CH46E) had similar response curves among themselves also, but the two groups differed from each other. Figure 13 plots the indoor results for these two groups of helicopters. This figure shows the same type of data shown in Figure 12, but shows it for groups instead of individual helicopters. Table 4 lists these data.

Because less outdoor data were gathered—there was only one outdoor group but four indoor groups—less analysis could be performed on it. (Enough outdoor data were collected to create a reliable graph for the AH1W, however.) In an effort to more fully develop the outdoor data, it was reasoned that since the indoor data for all multi-bladed helicopters were similar and grouped together, then all of the outdoor data for the multibladed helicopters could be also grouped together. Even with this grouping, however, there were so few outdoor subjects that much of the data lacked sufficient reliability.* The graphs used to develop the individual outdoor datapoint pairs (as in Figure 10a) are shown in Appendix C. These data are summarized in Figure 13 and Table 4.

* As implied by the design of this study, the emphasis was placed on indoor testing. For test sessions attended by fewer recruits than expected, subjects were located indoors first to assure the collection of an adequate amount of indoor data. Therefore, the number of participants in outdoor tests fluctuated substantially depending on overall attendance. Ultimately this impaired the reliability of the outdoor data collected.

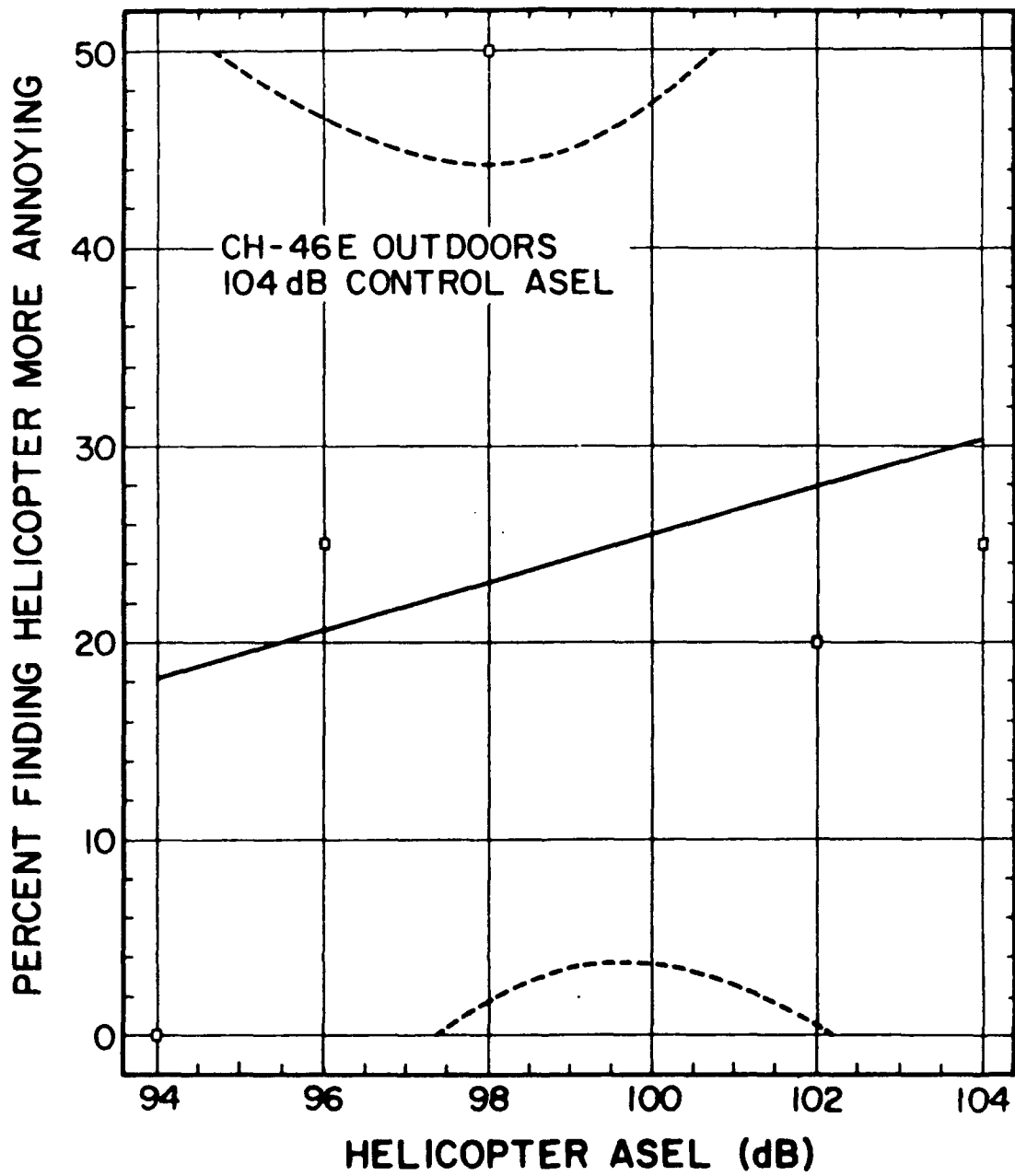


Figure 11. Example of Discarded Data.

Table 2
Correlation Coefficients for Data

HELICOPTER (CONTROL ASEL)	CORRELATION COEFFICIENTS FOR PERCENTS	CORRELATION COEFFICIENTS FOR Z-SCORES
CH53A(60)IN	0.884	0.865
CH53A(68)IN	0.867	0.818
CH53A(72)IN	0.891	0.893
CH53A(80)IN	0.786	0.833
AH1W(100)OUT	0.708	0.695
AH1W(80)OUT	0.700	0.701
AH1W(84)OUT	0.677	0.693
AH1W(92)OUT	0.687	0.645
AH1W(68)IN	0.934	0.970
AH1W(78)IN	0.923	0.922
AH1W(80)IN	0.753	0.744
AH1W(84)IN	0.718	0.718
CH46E(88)OUT	0.874	0.801
CH46E(92)OUT	0.741	0.841
CH46E(96)OUT	0.777	0.843
CH53A(92)OUT	0.732	0.725
CH53A(96)OUT	0.750	0.791
CH53E(100)OUT	0.829	0.906
CH53E(92)OUT	0.431	0.571
CH53E(96)OUT	0.734	0.885
CH46E(100)IN	0.745	0.757
CH46E(84)IN	0.801	0.847
CH46E(92)IN	0.904	0.826
CH46E(92)IN	0.817	0.797
CH53A(88)IN	0.720	0.690
CH53A(92)IN	0.832	0.832
CH53A(96)IN	0.915	0.901
CH53E(100)IN	0.924	0.929
CH53E(96)IN	0.850	0.799
CH46E(64)IN	0.925	0.869
CH46E(68)IN	0.941	0.939
CH46E(72)IN	0.942	0.937
CH46E(76)IN	0.983	0.972
CH46E(84)IN	0.852	0.856

Table 2 (Cont'd)

HELICOPTER (CONTROL ASEL)	CORRELATION COEFFICIENTS FOR PERCENTS	CORRELATION COEFFICIENTS FOR Z-SCORES
CH53E(68)IN	0.965	0.953
CH53E(72)IN	0.850	0.784
CH53E(76)IN	0.900	0.889
CH53E(84)IN	0.857	0.856
CH53E(92)IN	0.971	0.962
UH1H(68)IN	0.394	0.810
UH1H(72)IN	0.852	0.772
UH1H(80)IN	0.963	0.967
UH1N(56)IN	0.459	0.392
UH1N(64)IN	0.898	0.865
UH1N(68)IN	0.984	0.908
UH1N(72)IN	0.974	0.949
UH1N(76)IN	0.910	0.886
UH1N(80)IN	0.956	0.957
TOTAL	39.980	39.763
COUNT	48.000	48.000
AVERAGE	0.833	0.828

Table 3
Offset Data for Indoor Test Locations (by Helicopter)

a. UH1H		b. CH53A		c. CH53E	
Control ASEL (dB)	Helicopter equivalent (dB)	Control ASEL (dB)	Helicopter equivalent (dB)	Control ASEL (dB)	Helicopter equivalent (dB)
68	61	60	53	68	66
72	64	68	64	72	61
76	66	72	66	76	66
80	64	76	71	80	72
		80	73	84	76
				92	79

d. AH1W		e. UH1N		f. CH46E	
Control ASEL (dB)	Helicopter equivalent (dB)	Control ASEL (dB)	Helicopter equivalent (dB)	Control ASEL (dB)	Helicopter equivalent (dB)
64	54	64	58	64	57
68	59	68	60	68	58
72	64	72	62	72	63
76	66	76	66	76	66
80	67	80	69	84	77
84	71	84	73		

Frequency-Weighted Results

Figure 13 shows that, for each helicopter grouping (outdoors or indoors), the offset between the control sound and the equivalent helicopter sound becomes greater as the ASEL of the helicopter sound increases. The data clearly show a relationship between the helicopter ASEL and the resulting decibel offset from the equivalently annoying control noise. Again, as in the Savoy study, the results show that A-weighting did not provide an adequate description of human annoyance by helicopter noise because the offsets were not constant. For the multi-bladed helicopters, the offsets ranged from around 7 dB at low helicopter ASEL to around 10 dB at the highest helicopter ASEL. The offset was found to rise from 6 to 13 dB for the two-bladed helicopters. These results are quite similar to the Savoy results for "a little" rattle,⁸ which was the only condition found at Tustin.

⁸ Paul D. Schomer and Robert D. Neathammer, 1987.

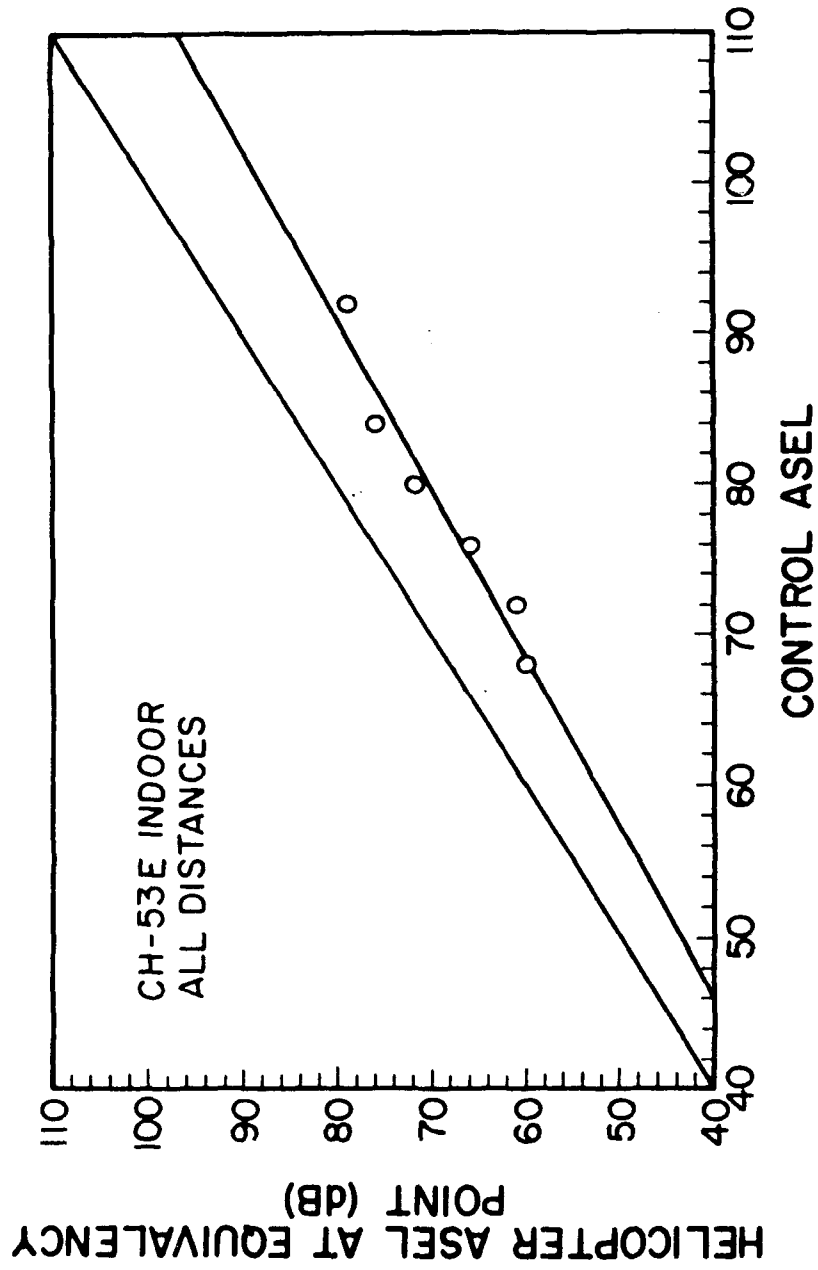


Figure 12. Offset as a Function of Control ASEL for CH-53E.

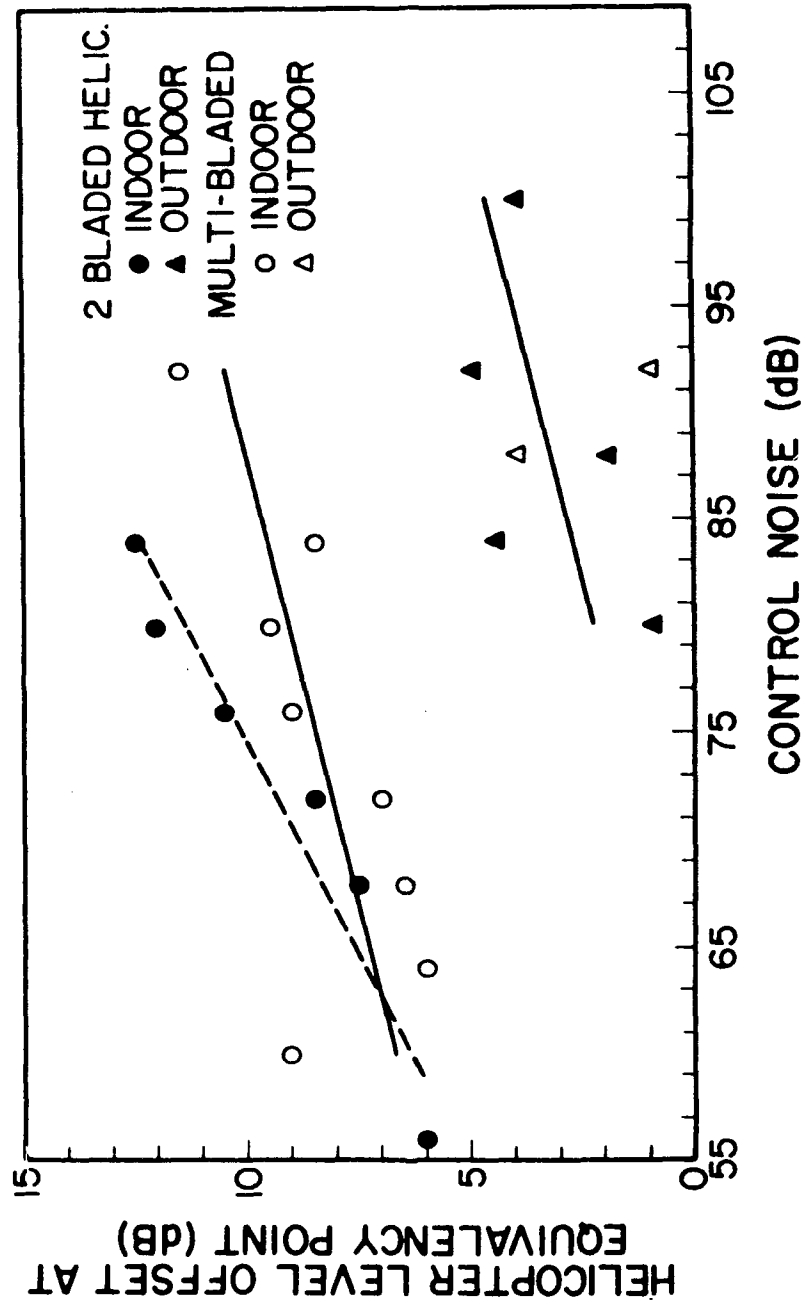


Figure 13. Offset as a Function of Control ASEL for Helicopters Grouped by Number of Blades.

Table 4

Offset Data Grouped by Number of Blades and Test Environment

MULTIBLADED INDOOR		2-BLADED INDOOR		MULTIBLADED OUTDOOR		2-BLADED OUTDOOR	
Control ASEL (dB)	Offset (dB)	Control ASEL (dB)	Offset (dB)	Control ASEL (dB)	Offset (dB)	Control ASEL (dB)	Offset (dB)
60	9	56	6	88	4	80	1
64	6	68	7.5	92	1	84	4.5
68	6.5	72	8.5			88	2
72	7	76	10.5			92	5
76	9	80	12			100	4
80	9.5	84	12.5				
84	8.5						
92	11.5						

To check the hypothesis that a different weighting system might provide a more constant offset, some of the data were reanalyzed using the C-weighting scale⁹ (typically used in measuring blast noise and sonic boom). The offset values changed, but the change did not result in a constant offset from the control noise level. This indicates that the C-weighting scale is just as inappropriate a measure for helicopter noise as the A-weighting scale.

The data seem to indicate that helicopter noise should be measured with a loudness measure such as International Organization for Standardization (ISO) 532b.¹⁰ This measure would take into account the fact that human response to helicopter noise is not a constant function of frequency, but relies on a variety of frequency, duration, and amplitude factors, most of which are not taken into account by the simple weighting curves now commonly used. The most important factor, however, would be the loudness of the noise—not in the common sense of the term, but as defined by ISO 532b. Research on loudness indicates that if one noise is louder than another but their ASELs are equal, then people find the louder noise (as measured by ISO 532b) more annoying.¹¹ Loudness as measured by ISO 532b, then, may be a better measure than ASEL for assessing annoyance. The possibility of using this measure is now under investigation. Qualitatively, the results shown in Figure 13 are explained by this loudness hypothesis.

Effect of Distance on Subjects' Response

One other hypothesis that could explain the variable, helicopter-level-dependent offset between helicopter noise and the control noise would involve the sideline distance between the subjects and the helicopter. The subjects may be more annoyed when hearing that the helicopter was very close to the test houses than when it was farther away. This hypothesis was tested.

⁹ 7A ANSI S 12.9-1988.

¹⁰ International Standard ISO 532b, *Method for Calculating Loudness Level* (ISO, 1975).

¹¹ E. Zwicker, "Meaningful Noise Measurement and Effective Noise Reduction," *Noise Control Engineering Journal*, Vol 29, No. 3 (1987), pp 66-76.

The data from the multibladed helicopters were grouped together to form one large database. Similarly, all of the data from the two-bladed helicopters were collected into a second large set. Data from these two groups were split by the four sideline distances of 50 ft, 500 ft, 1000 ft, and 2000 ft. Then the data, so divided, were analyzed in the same fashion as before. Response curves were generated for each sideline distance and helicopter type (multibladed or two-bladed).

Obviously, when a helicopter is close to the house, the noise from that helicopter will be louder, and more people will be annoyed than when it is farther away. However, each side line distance generated approximately the same regression line on the helicopter response curve (Figure 14). Therefore the effect of distance on the subjects' determination of noise-induced annoyance was judged to be minimal.

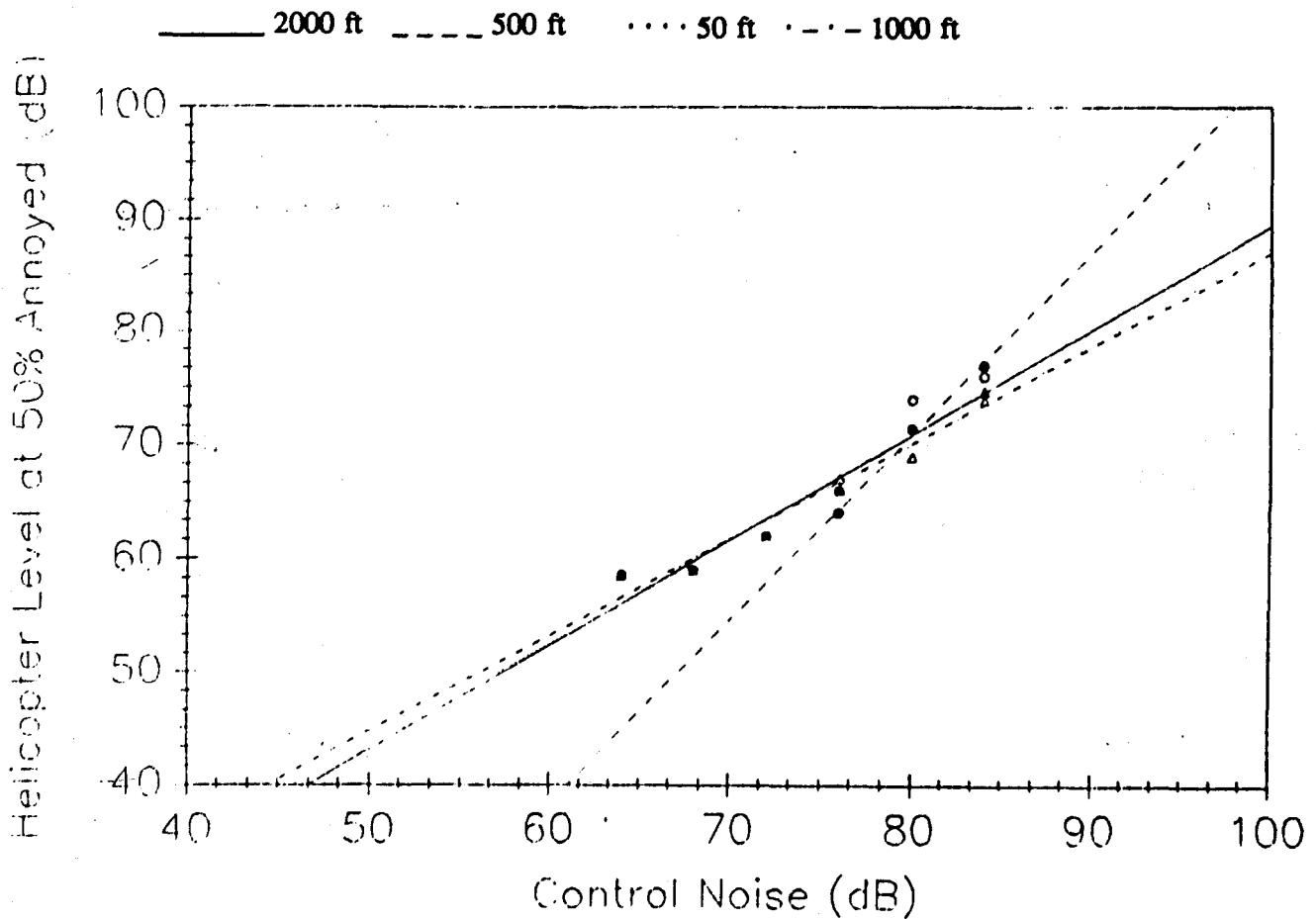


Figure 14. Subject Response to Different Sideline Distances.

5 CONCLUSIONS AND RECOMMENDATIONS

Overall, the additional data collected at MCAS Tustin indicates that the A-weighted measurement scale is inadequate for the assessment of helicopter noise. The C-weighting scale provides no discernible improvement over the A-scale. A correction must be added to the helicopter noise measured by either scale in order to assess a helicopter sound in a way that accurately corresponds to people's perceptions.

Use of A-weighting to assess helicopter sounds requires an offset which varies with helicopter ASEL. This offset changes based on the type of helicopter being used: two-bladed helicopter or multibladed helicopter.

For two-bladed helicopters, a correction factor of approximately 10 dB should be added to the ASEL of helicopter sound noise as measured indoors. An 8 dB correction factor should be added to the ASEL of a multibladed helicopter as measured indoors. These correction factors are the approximate averages of the decibel offsets found and shown in Figure 13 and Table 4.

Further analysis of this data should be performed to specifically assess the use of a loudness scale such as ISO 532b as a way to measure human response to helicopter noise.

METRIC CONVERSION TABLE

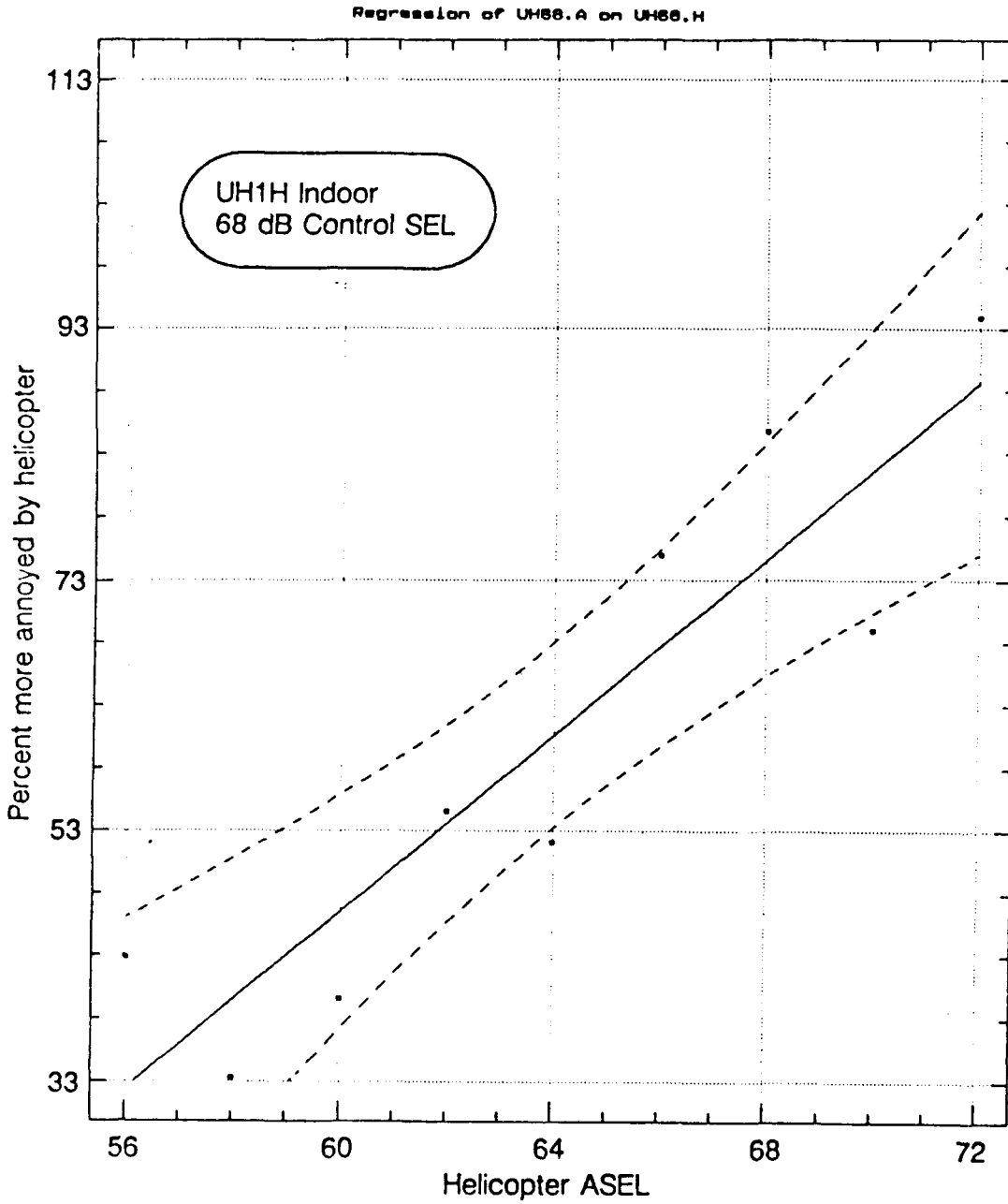
1 mi	=	1.61 km
1 ft	=	0.305 m
1 in	=	2.540 cm

REFERENCES

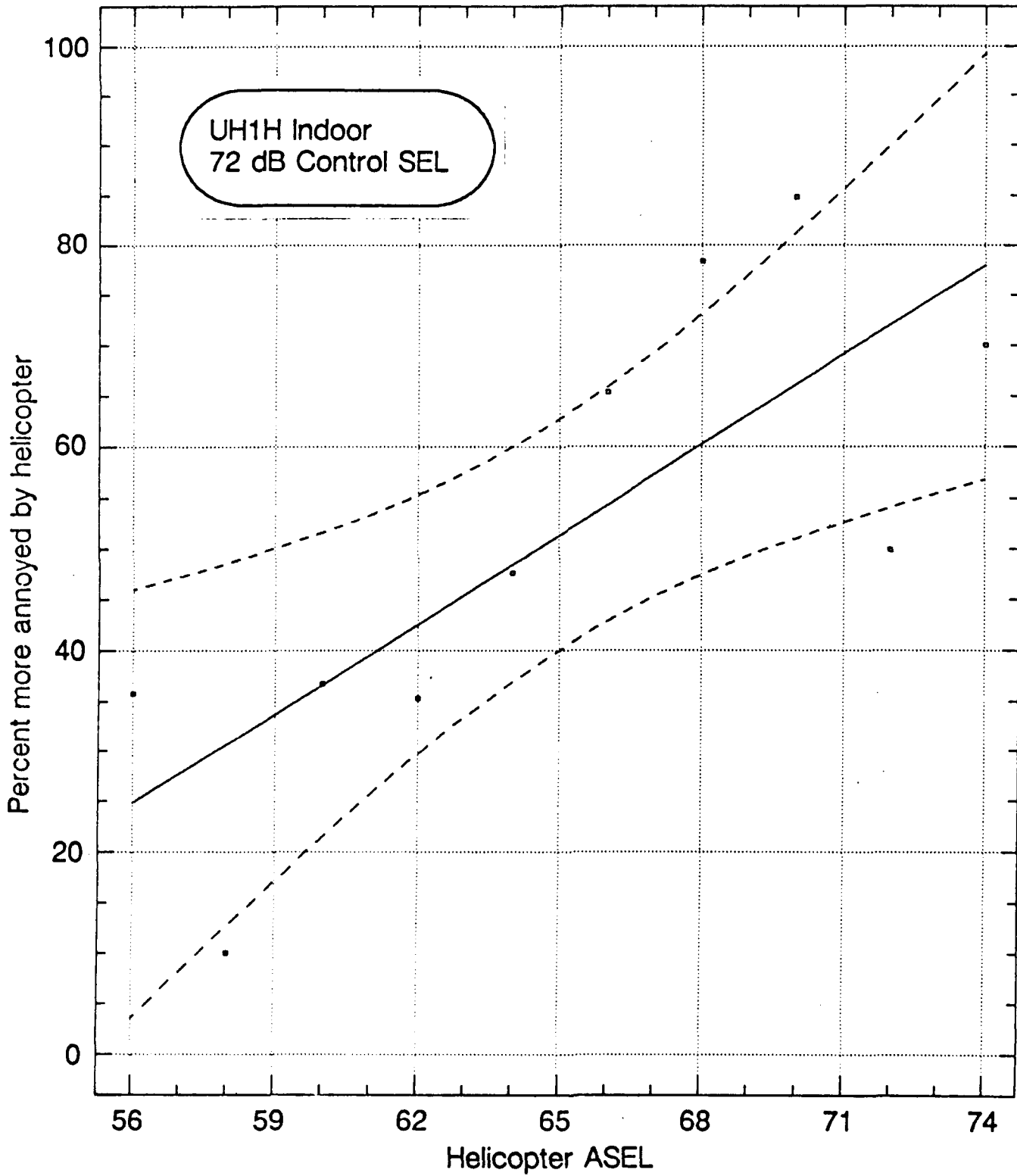
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- Zwicker, E., "Meaningful Noise Measurement and Effective Noise Reduction," *Noise Control Engineering Journal*, Vol 29, No. 3 (1987), pp 66-76.

APPENDIX A

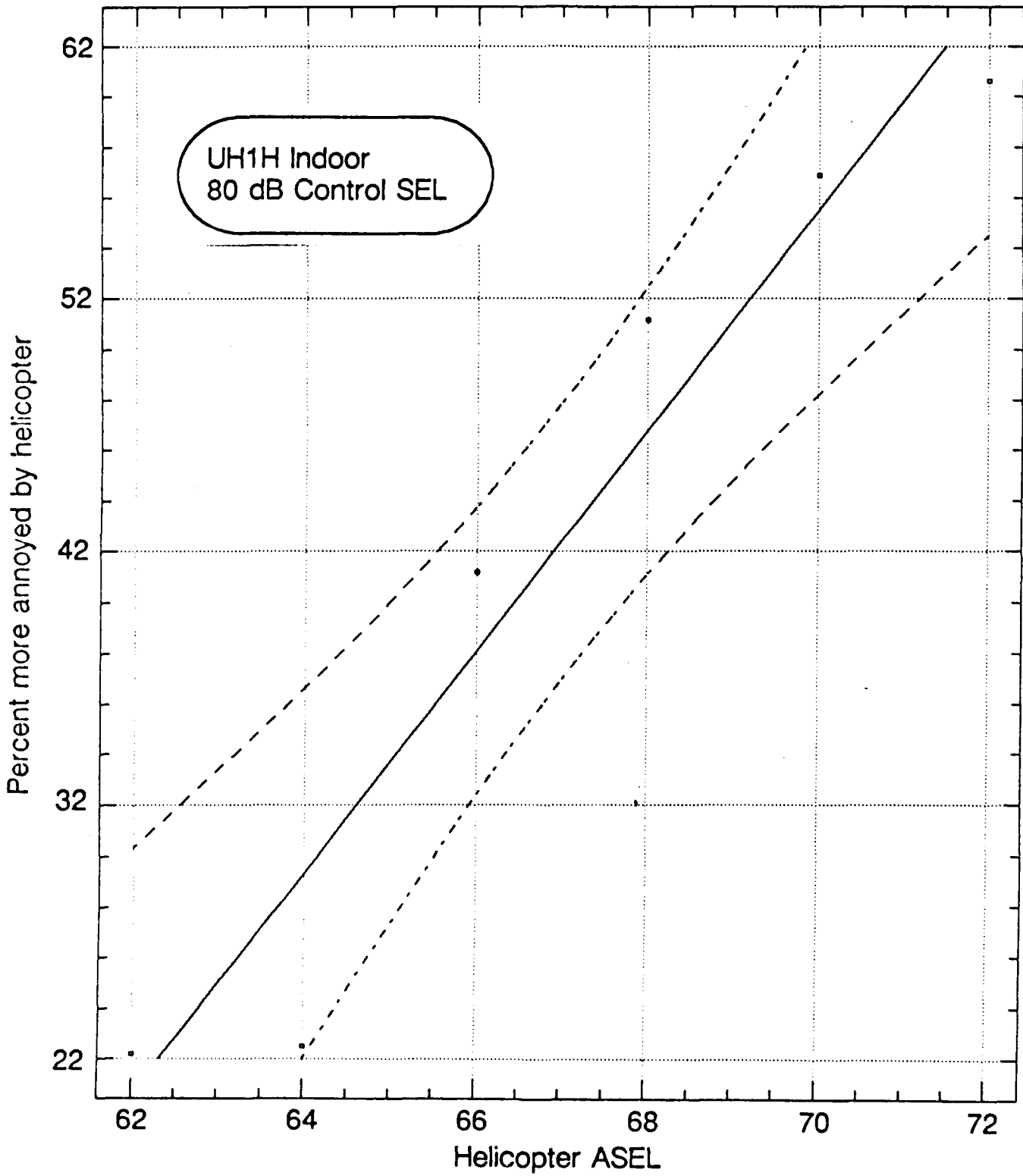
PLOTS OF MCAS TUSTIN INDOOR TEST DATA ARRANGED BY HELICOPTER IN ASCENDING ORDER OF CONTROL SEL



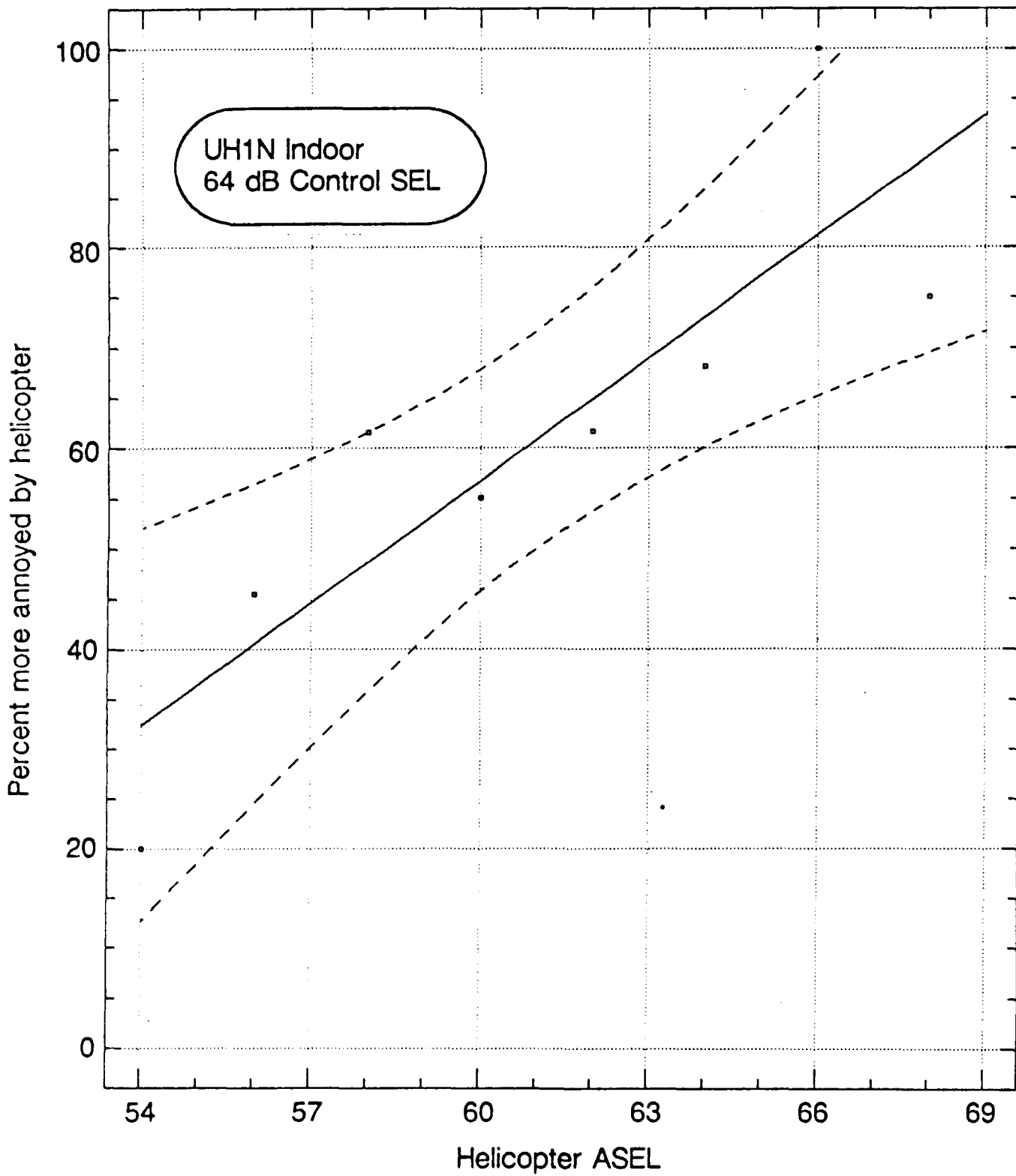
Regression of UH72.A on UH72.H



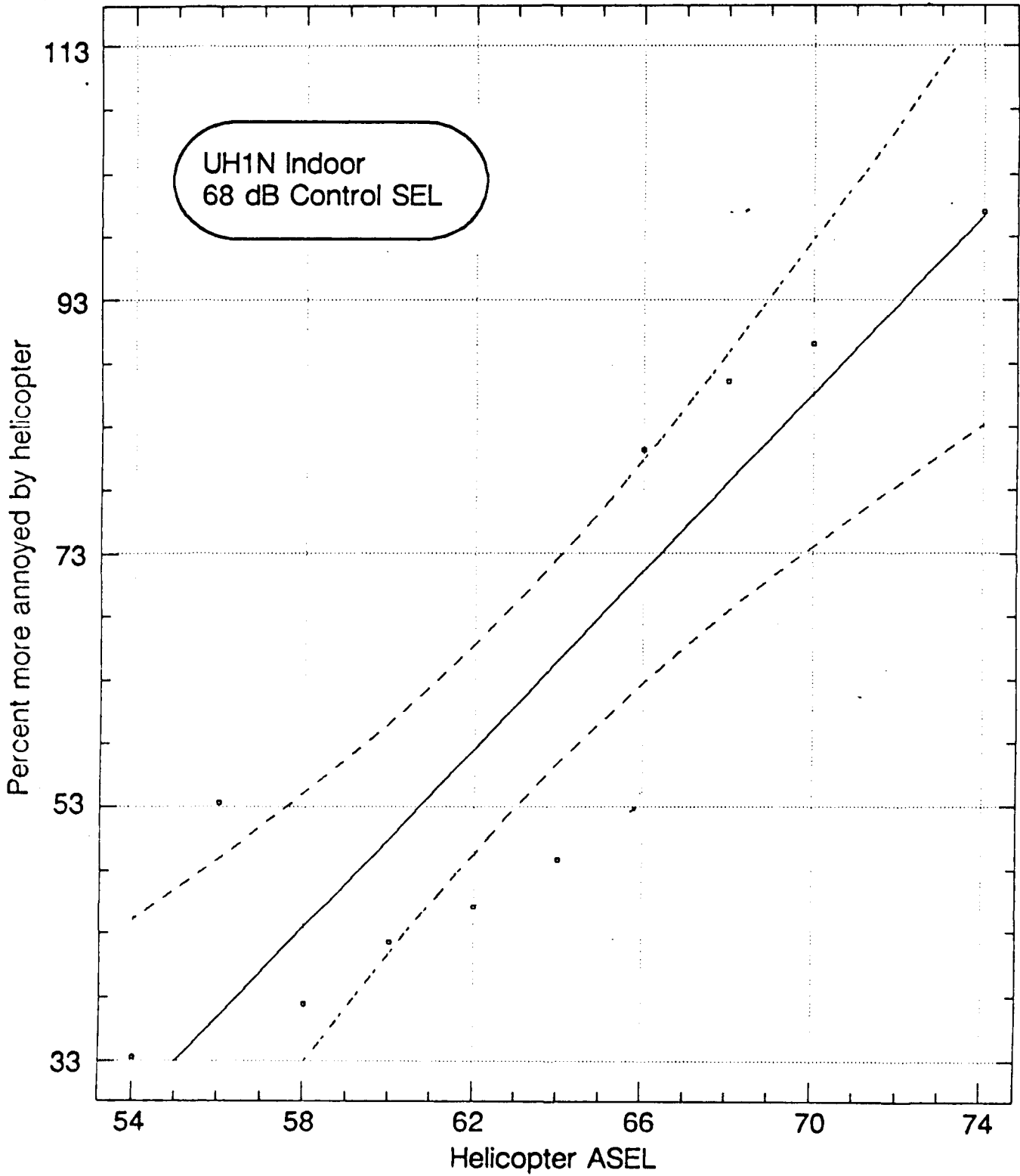
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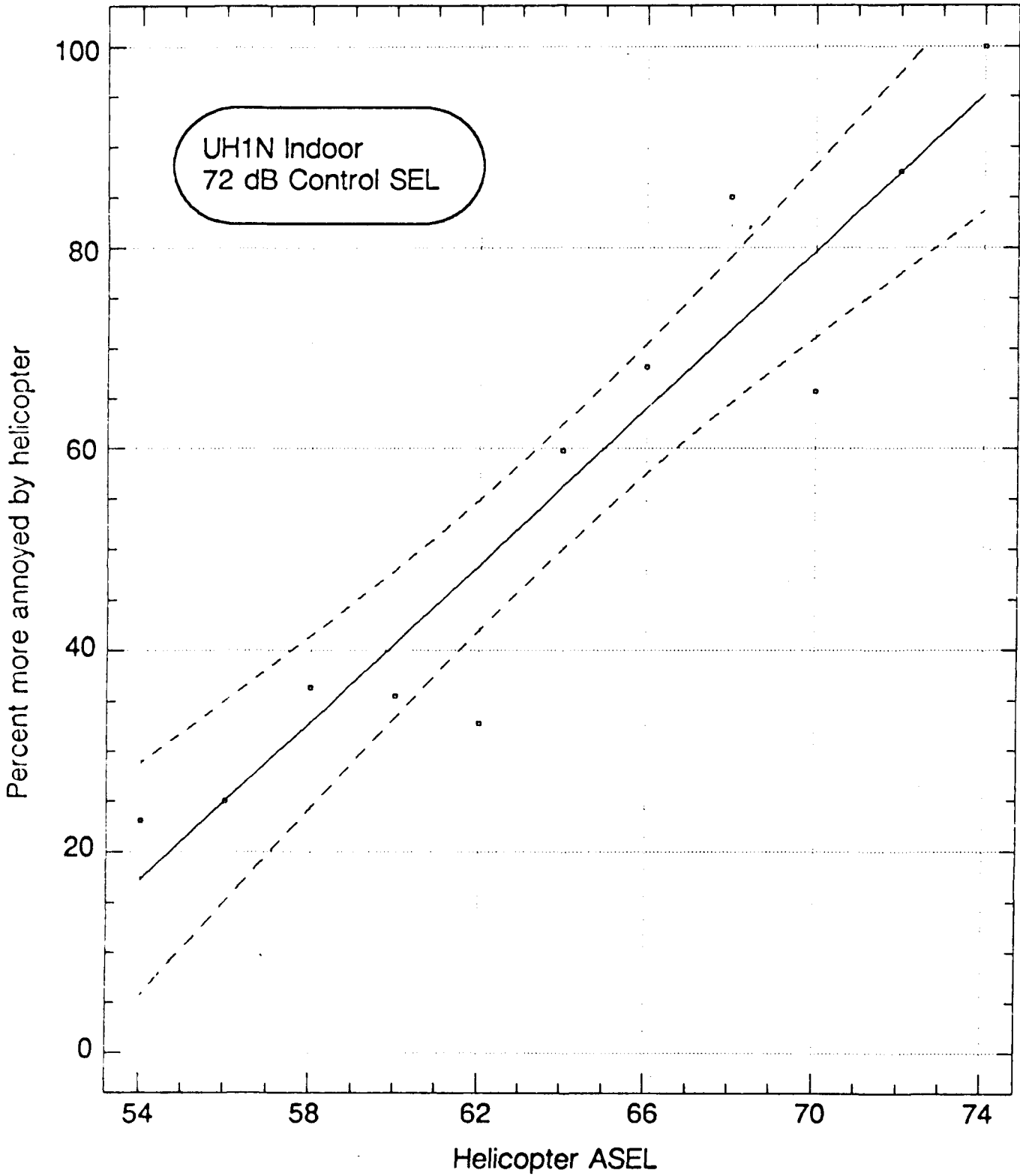
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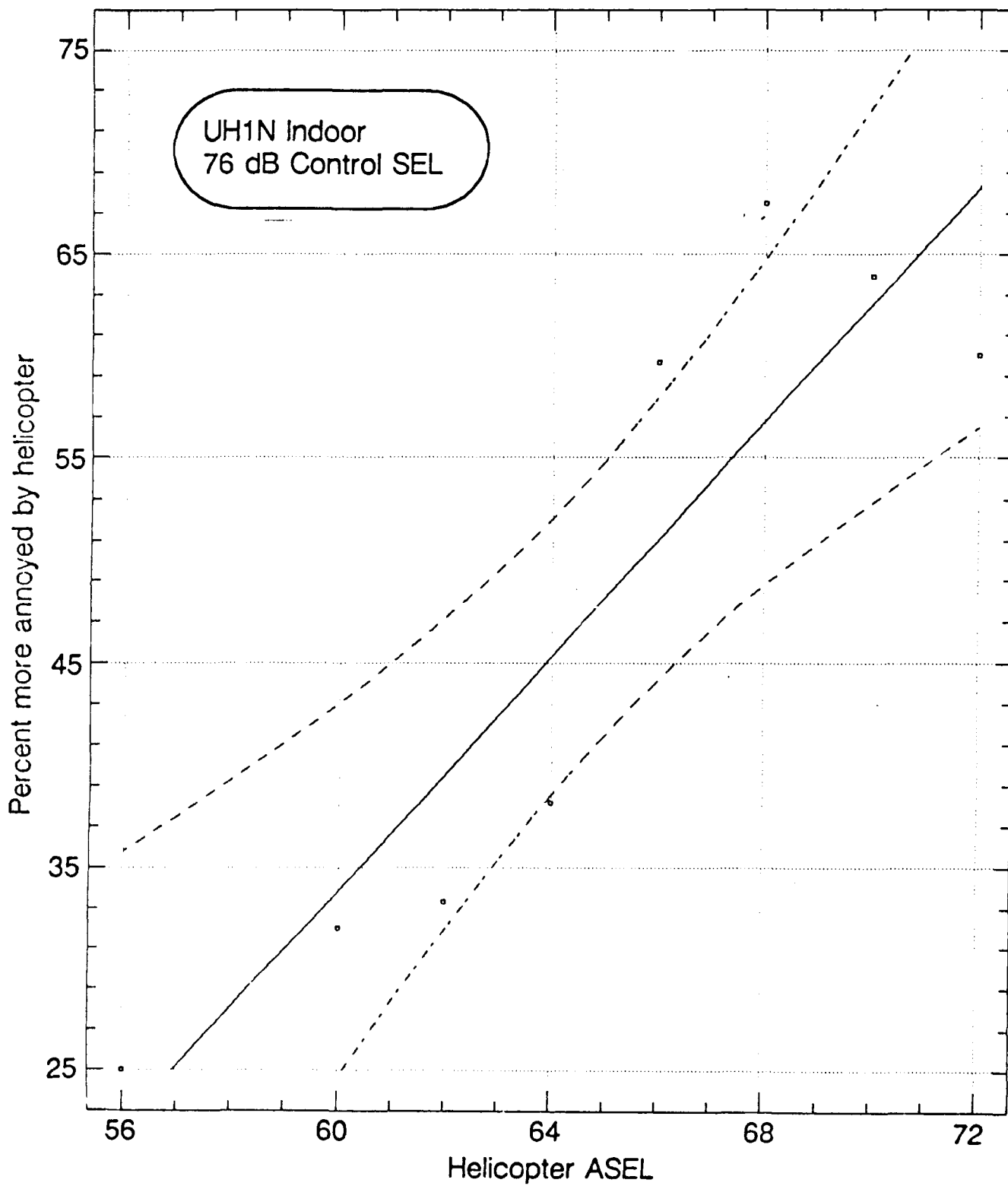
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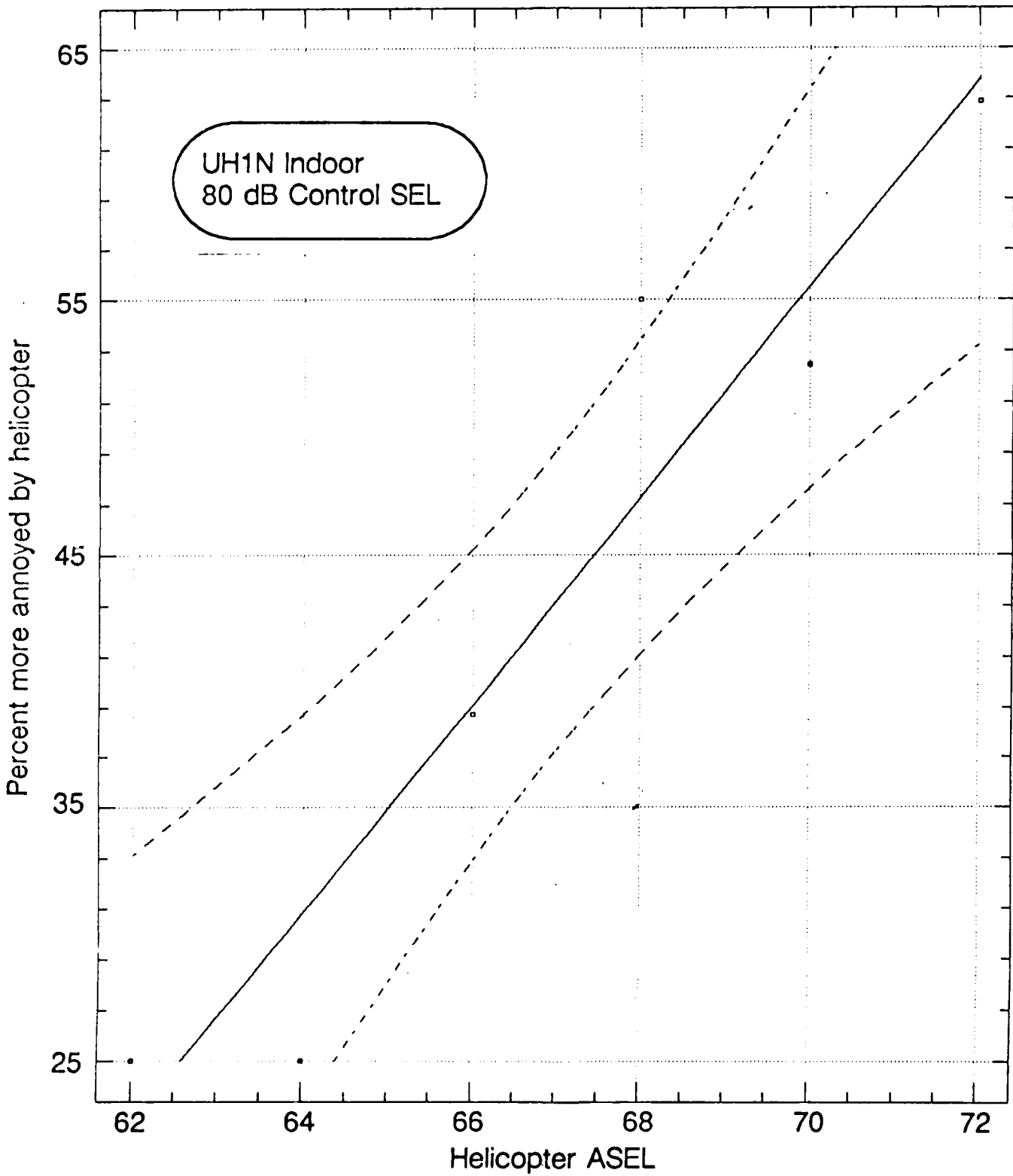
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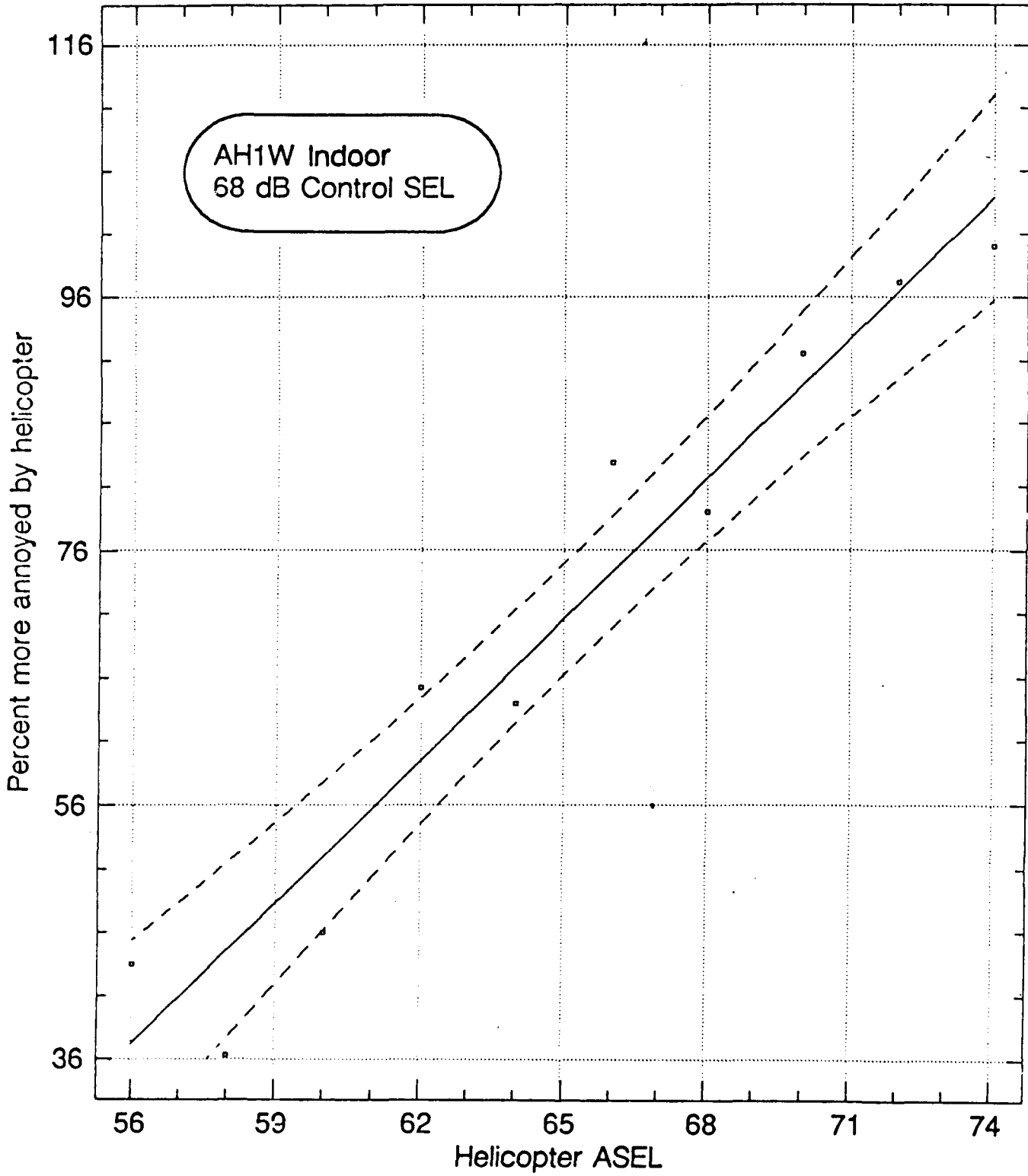
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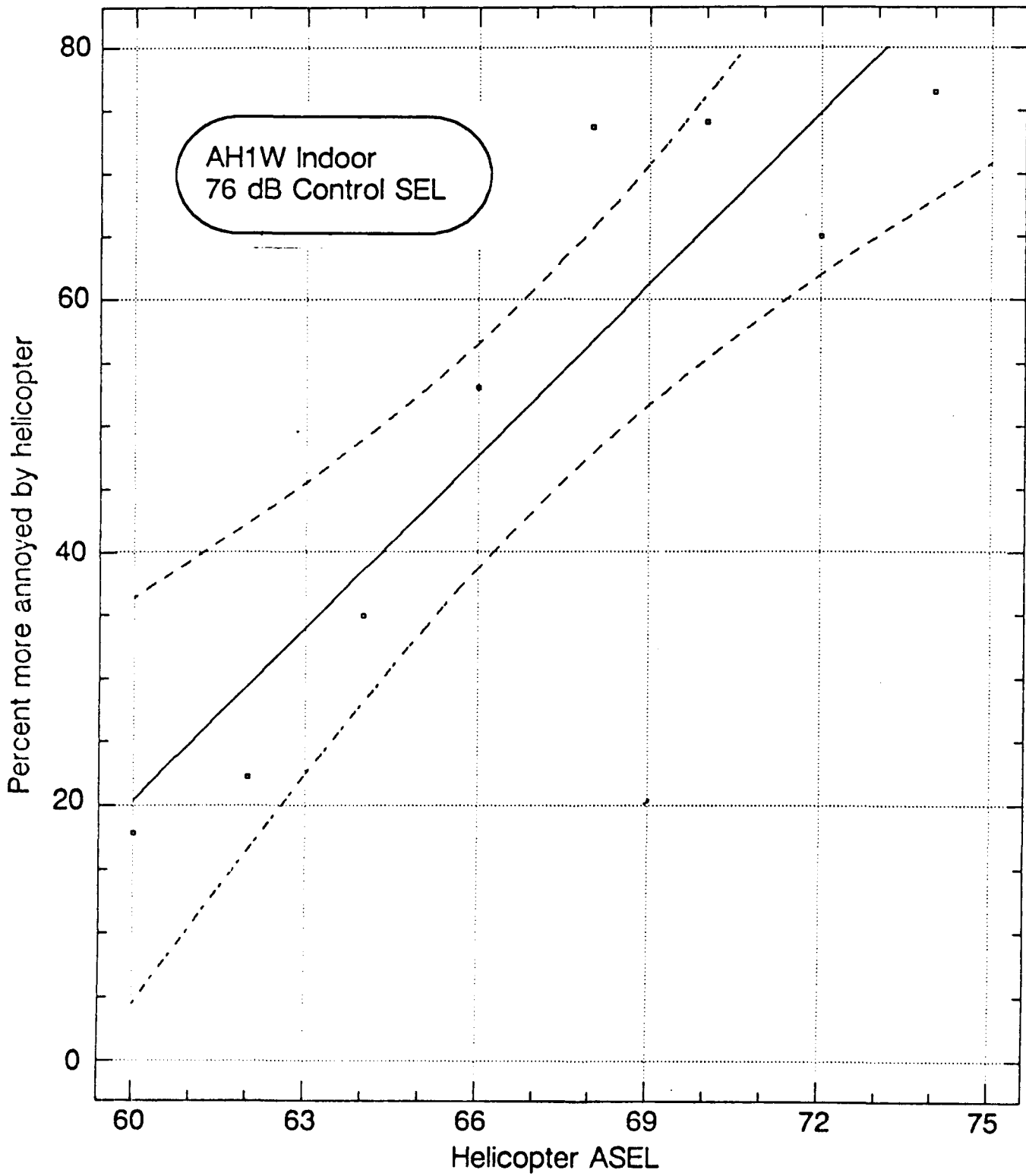
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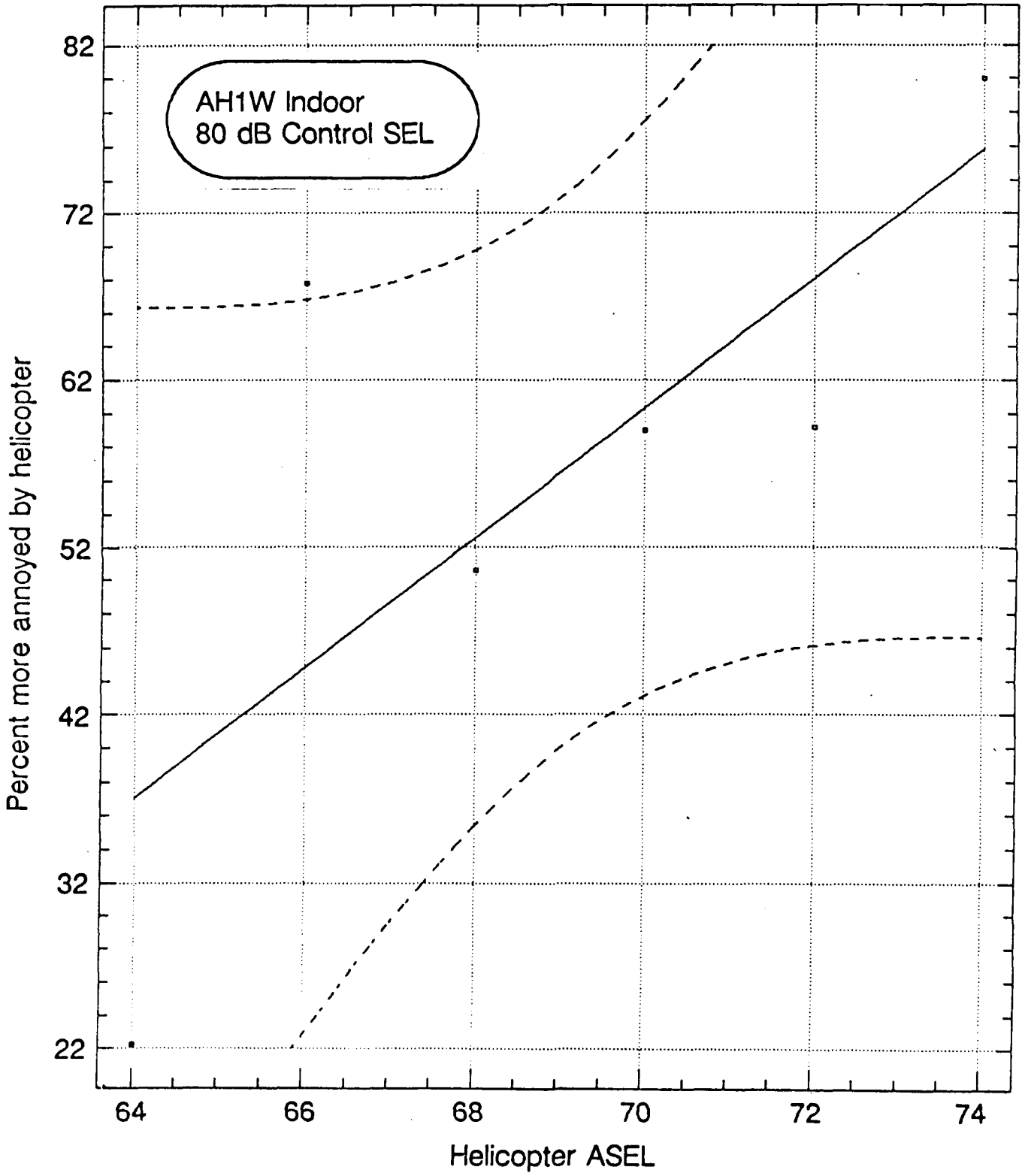
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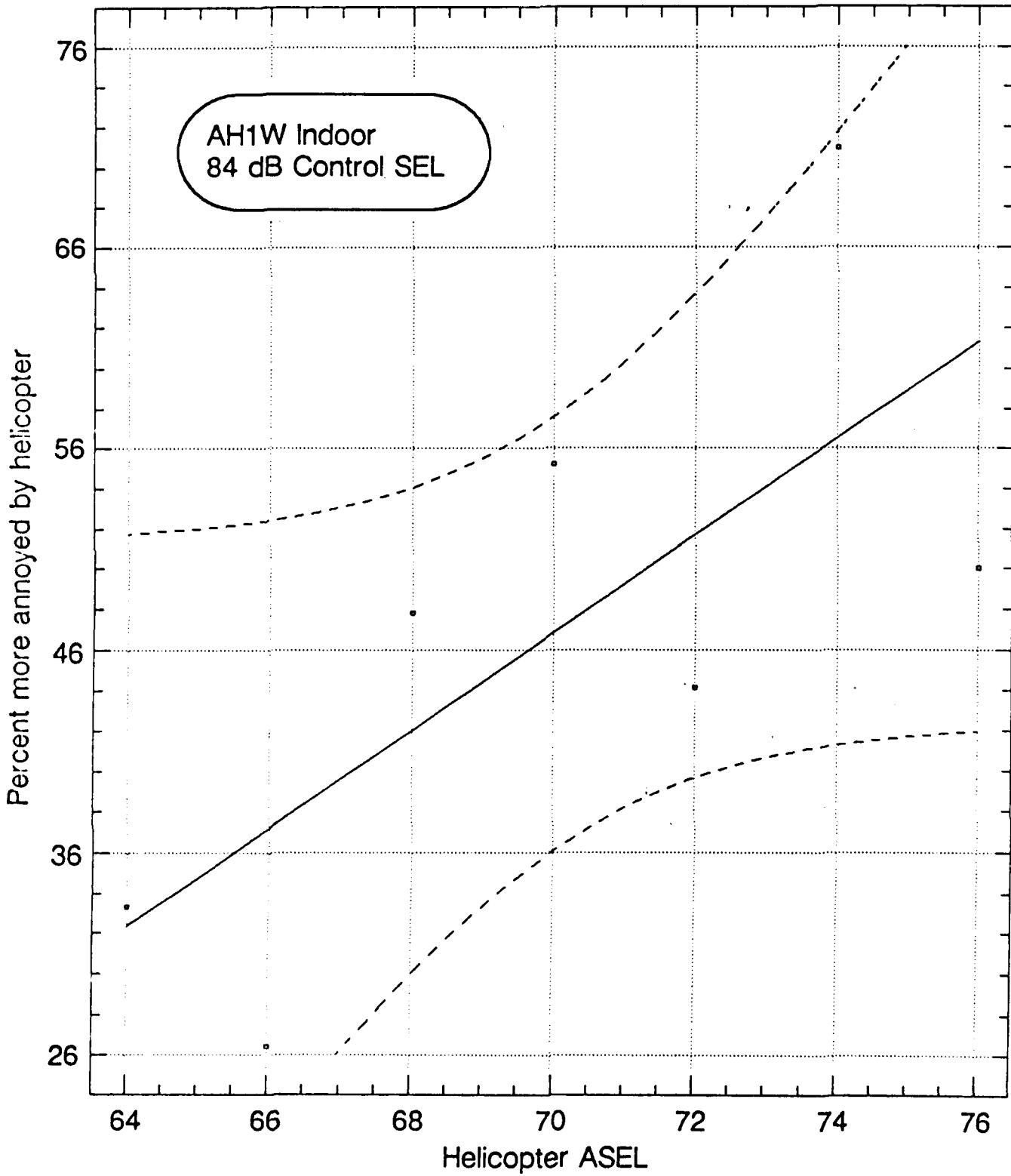
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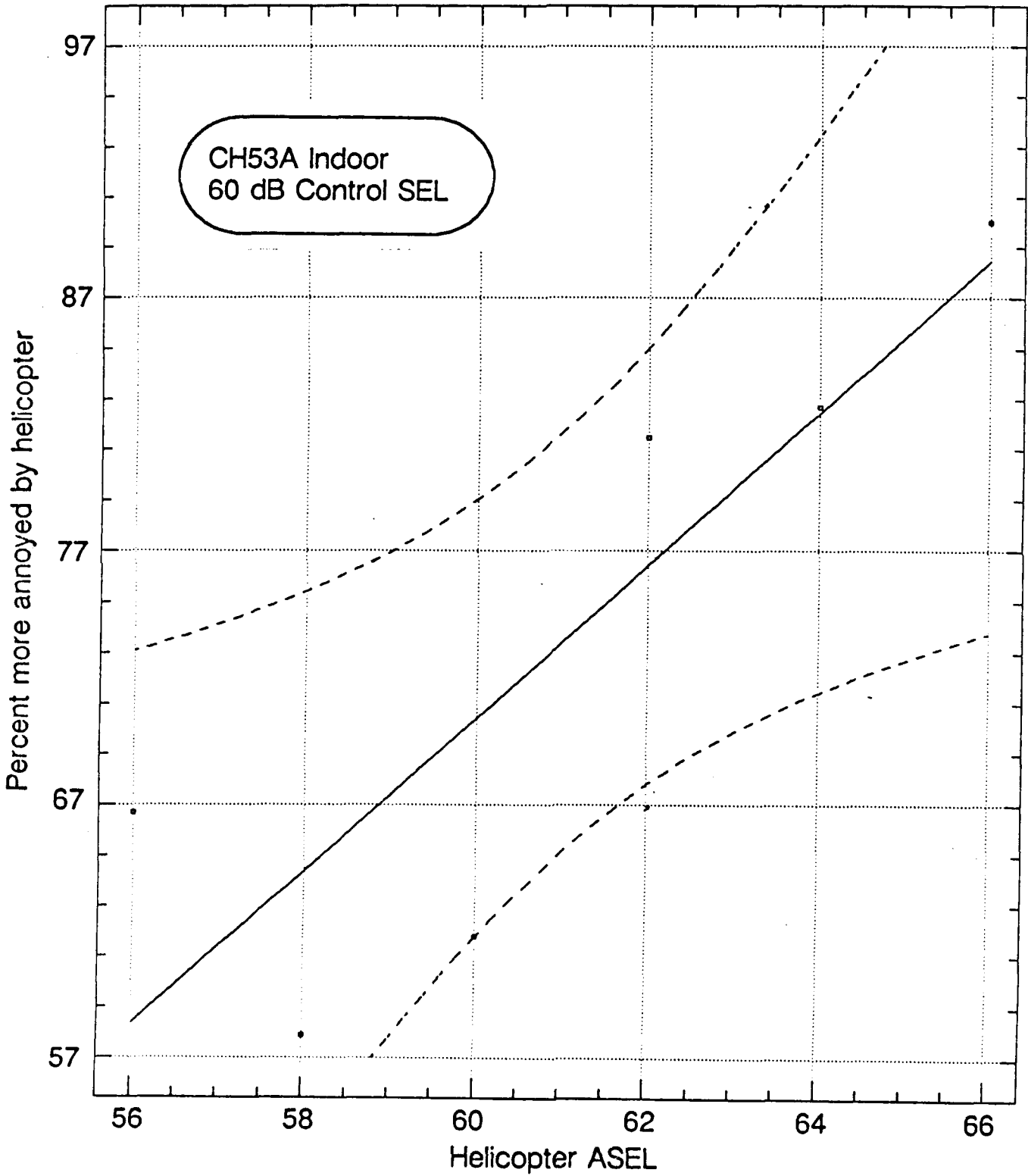
Regression of AH80.A on AH80.H



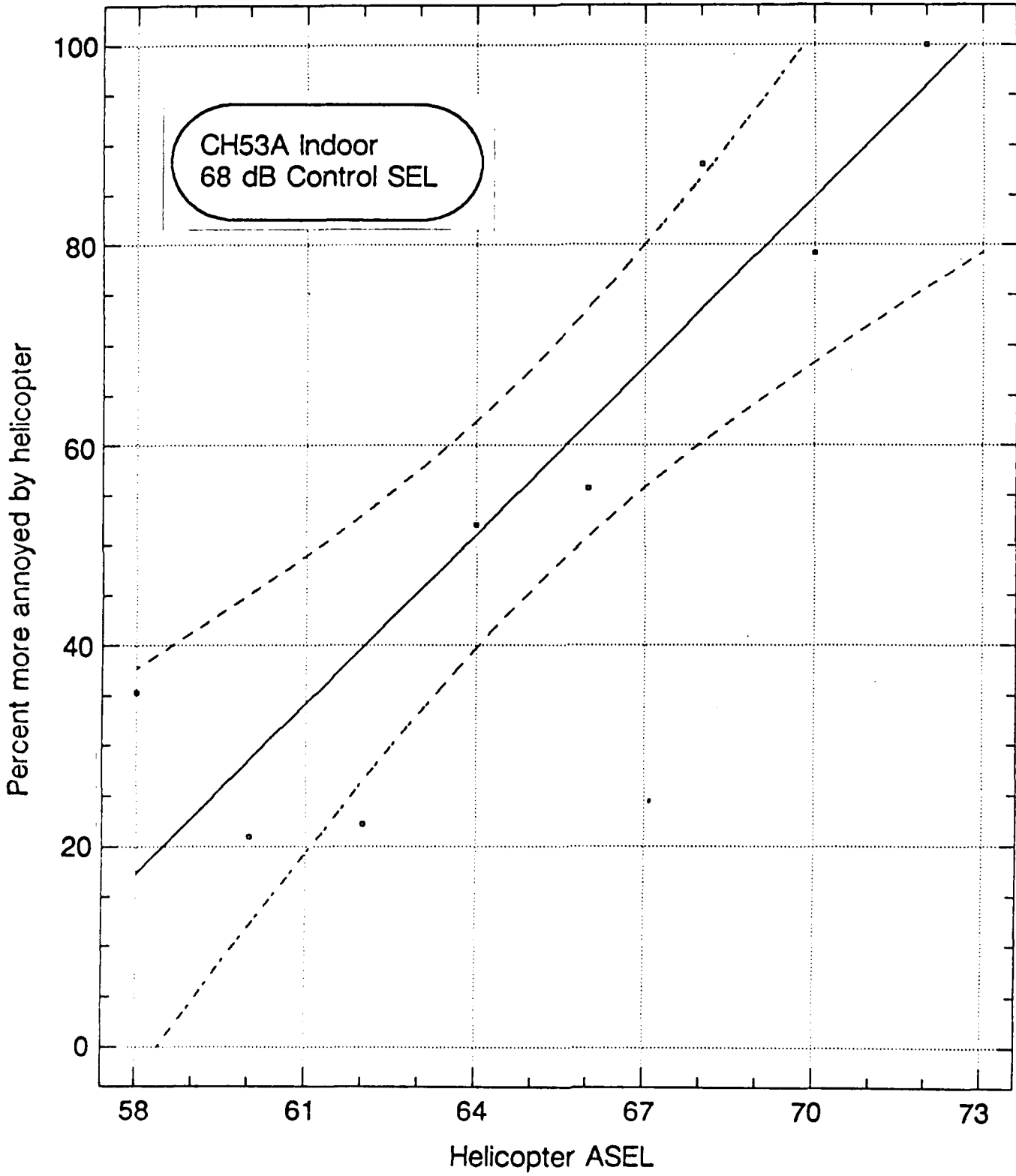
Regression of AH84.A on AH84.H



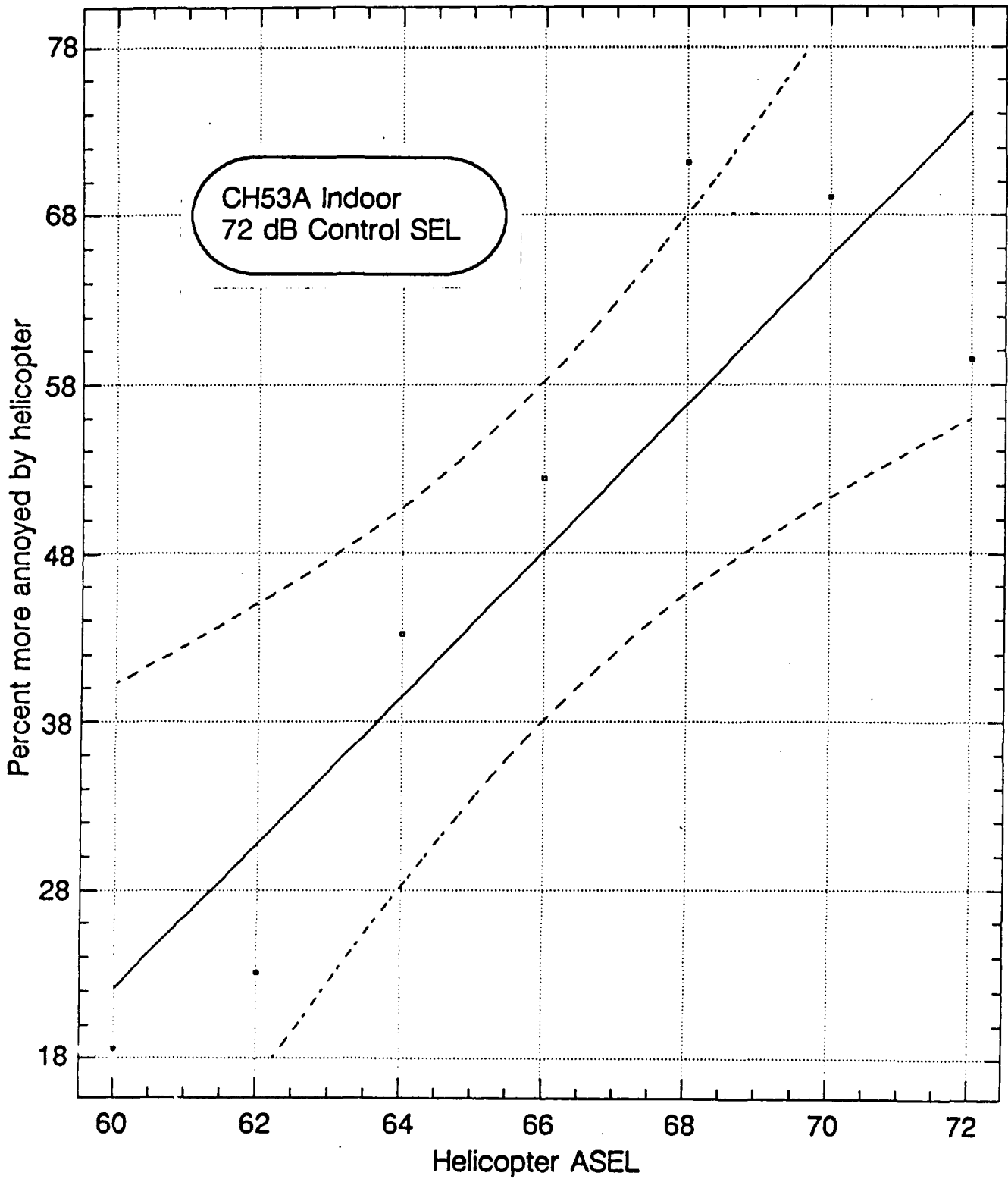
Regression of A5360.A on A5360.H



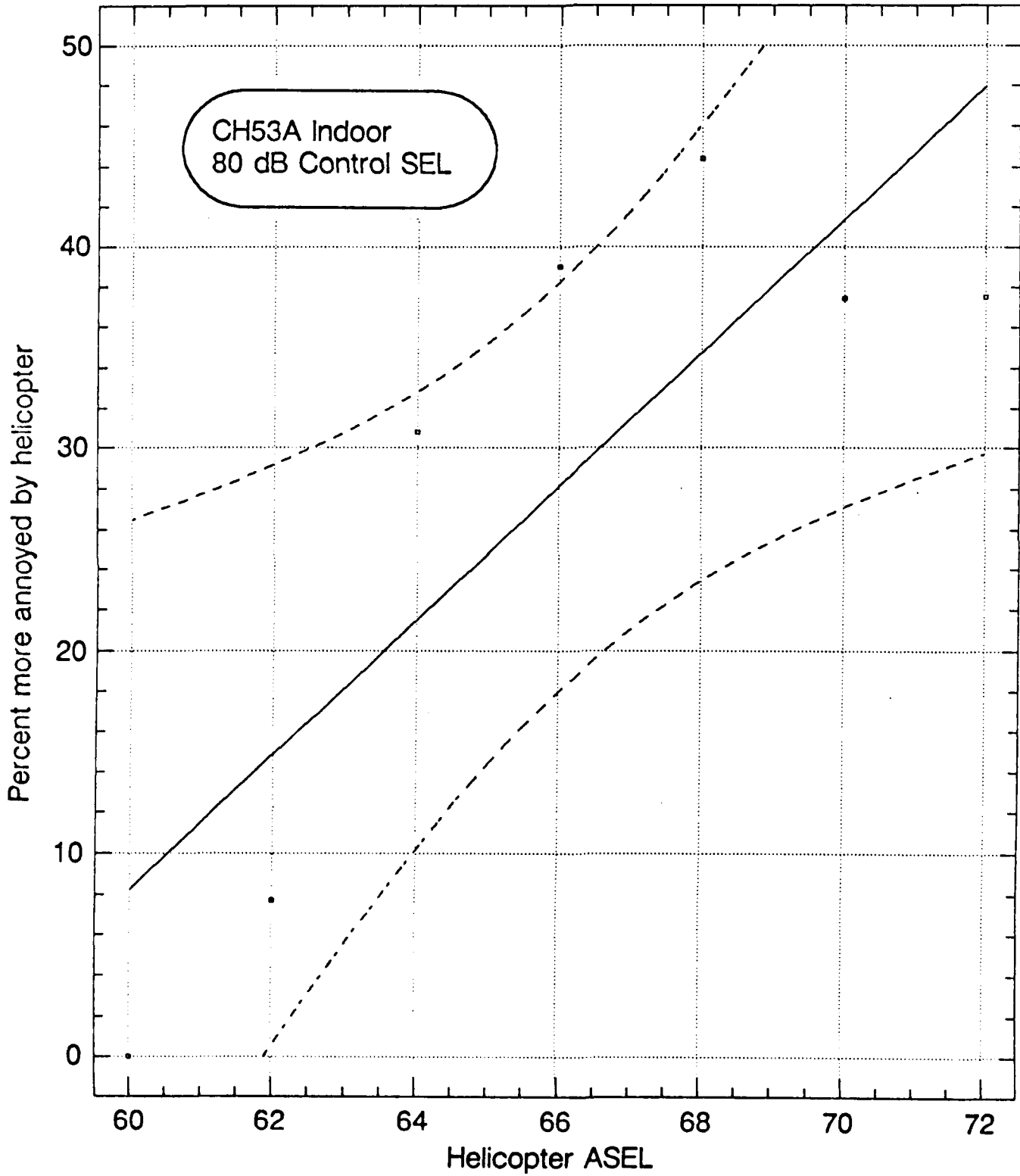
Regression of A5368.A on A5368.H



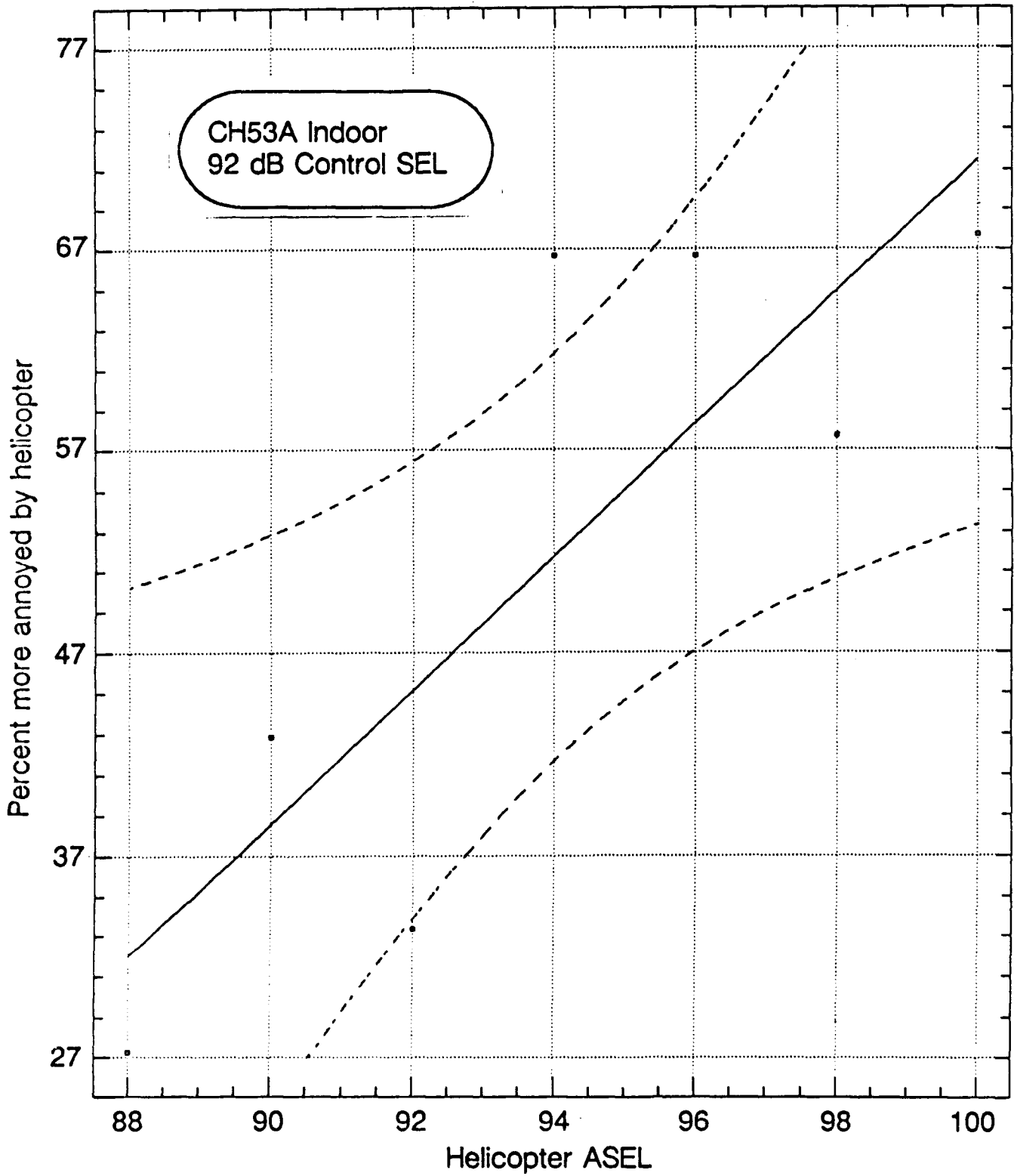
Regression of A5372.A on A5372.H



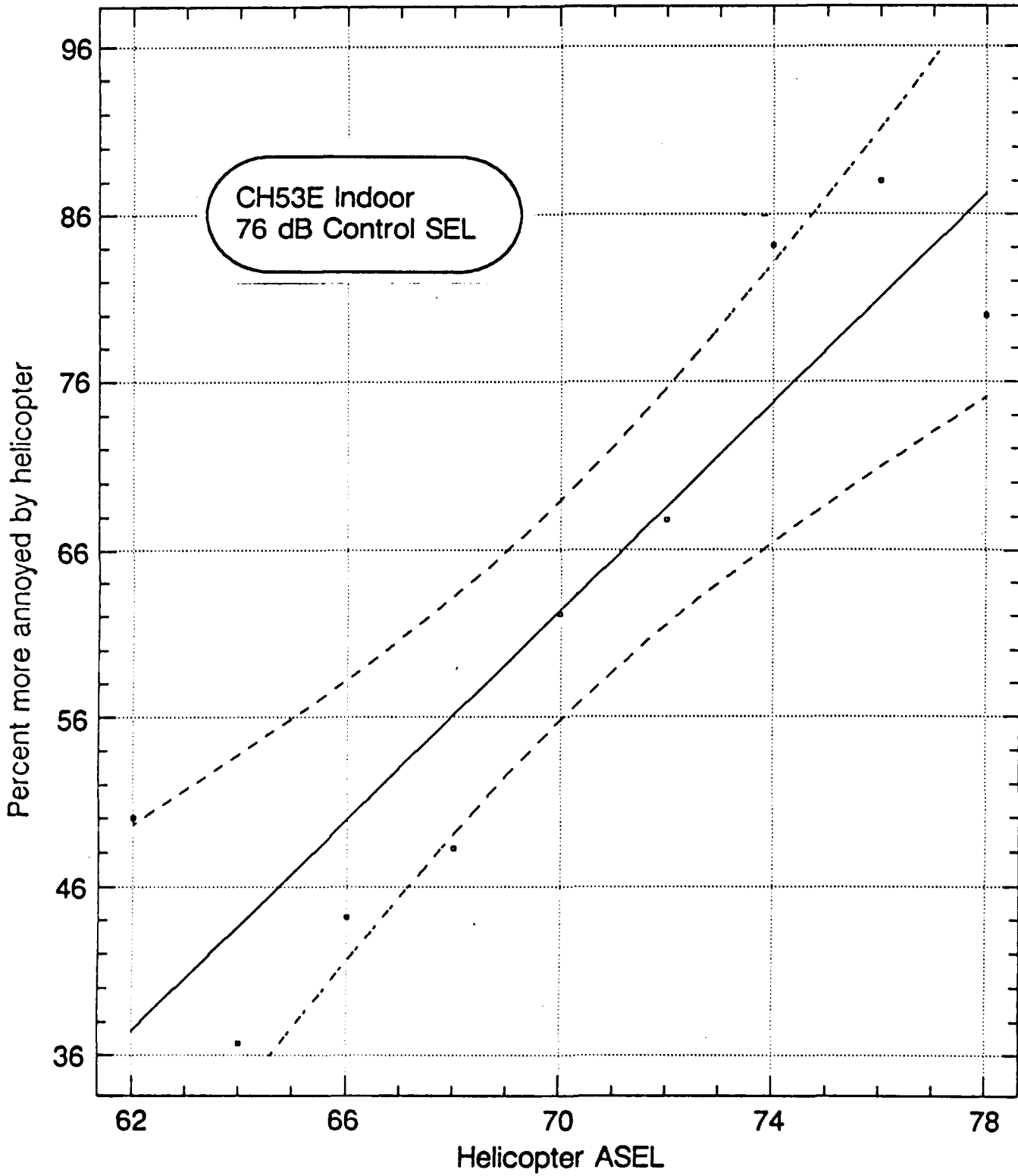
Regression of A6380.A on A6380.H



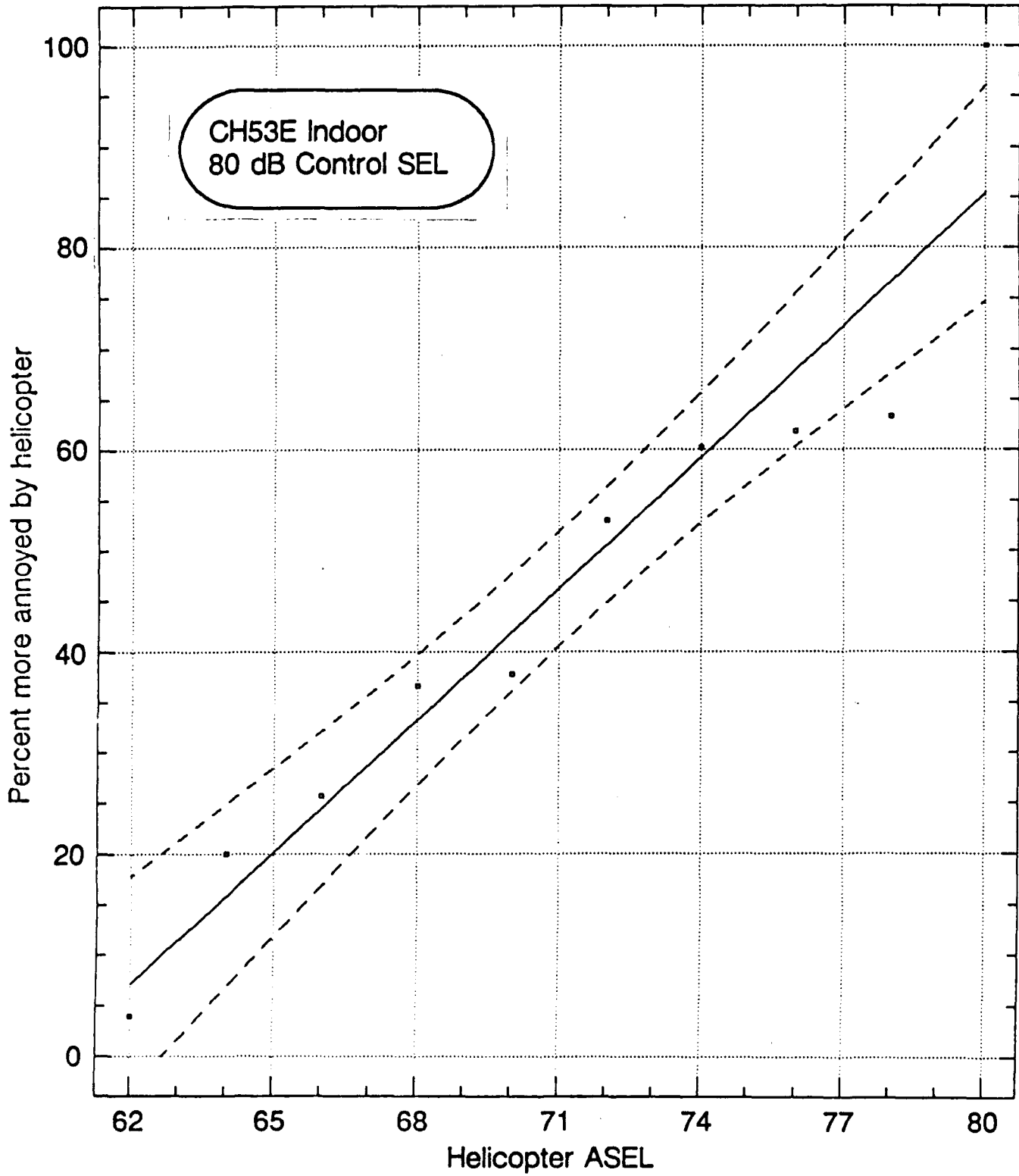
Regression of CH53A92.A on CH53A92.H



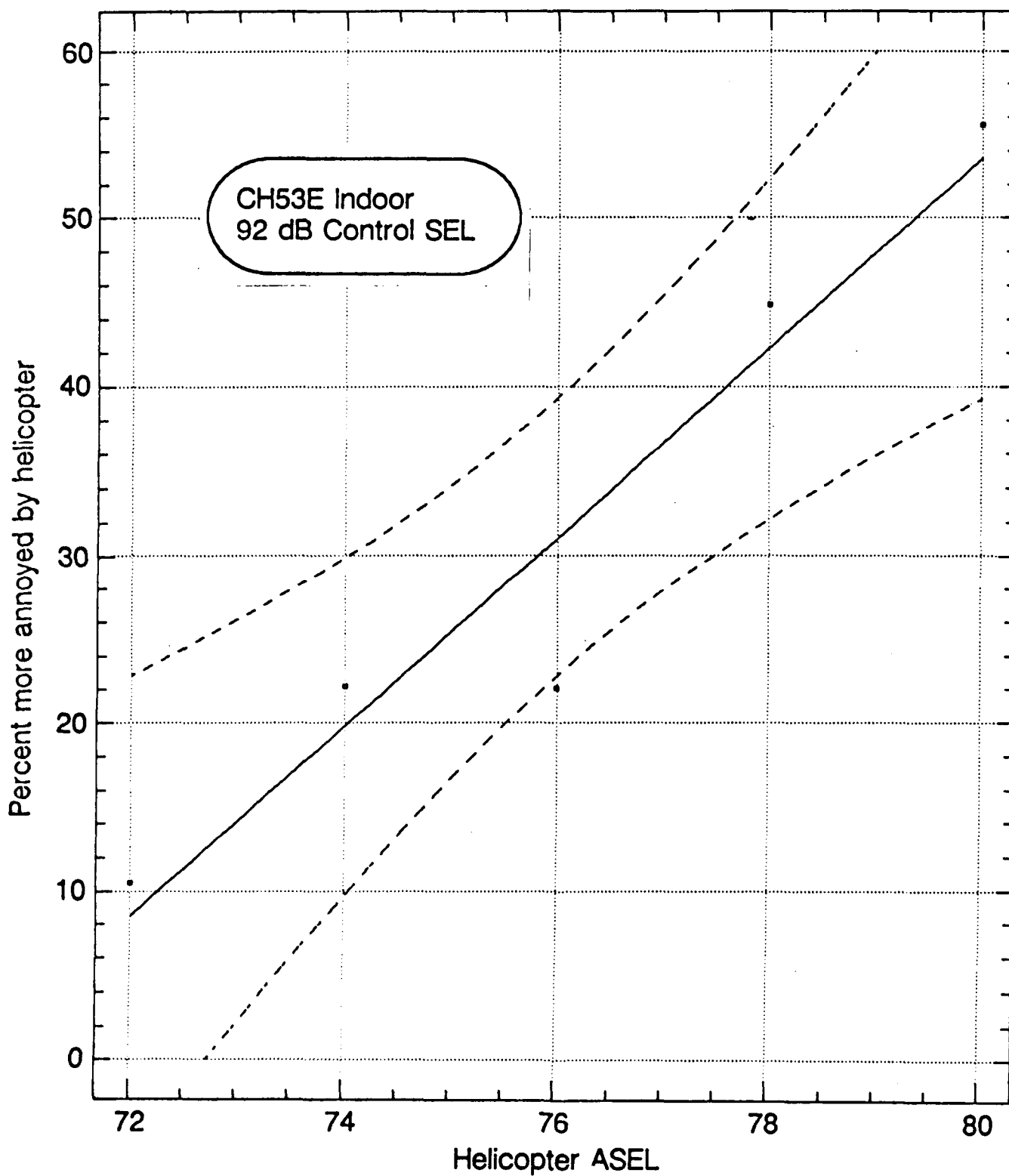
Regression of E5376.A on E5376.H



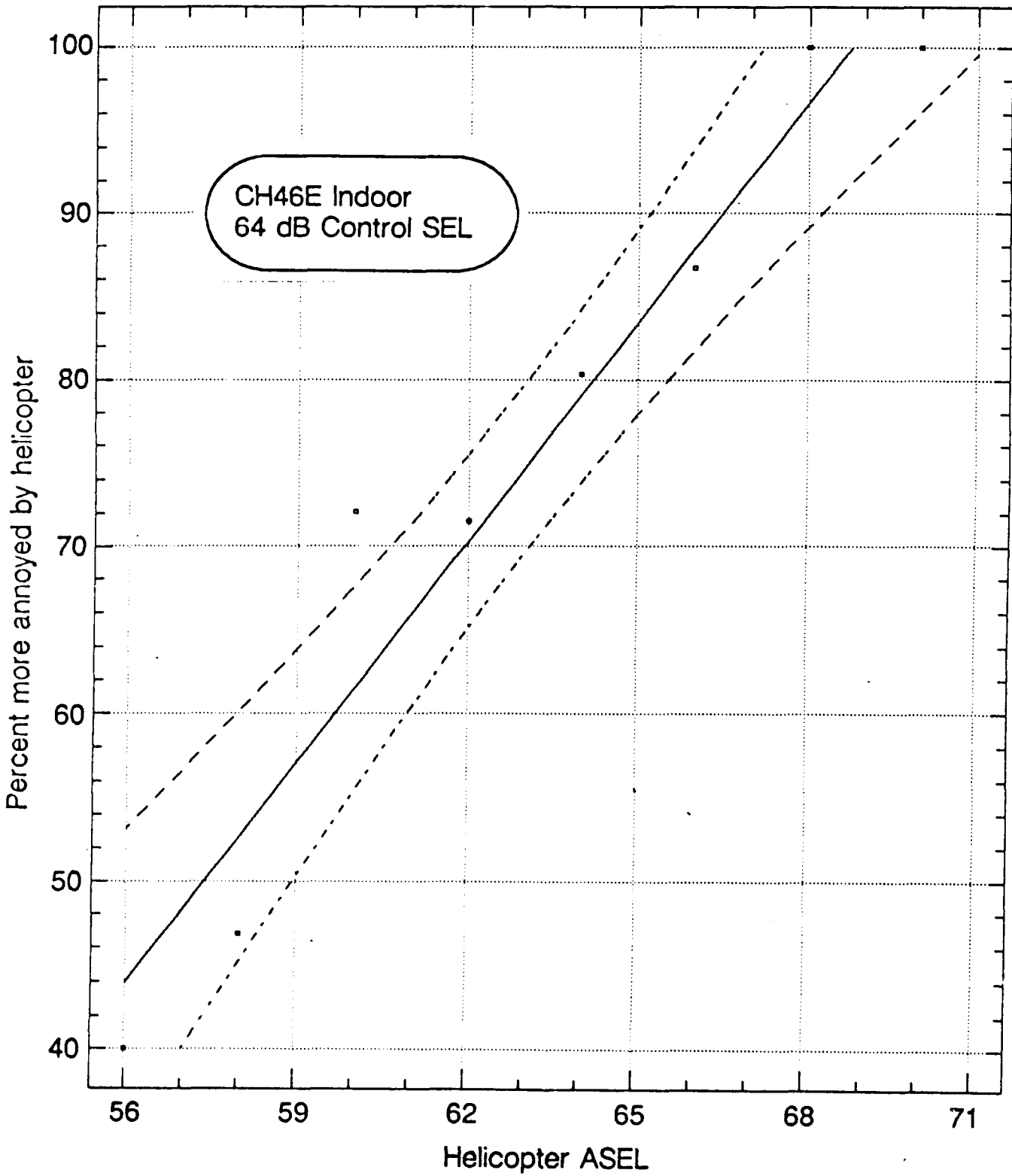
Regression of E5380.A on E5380.H



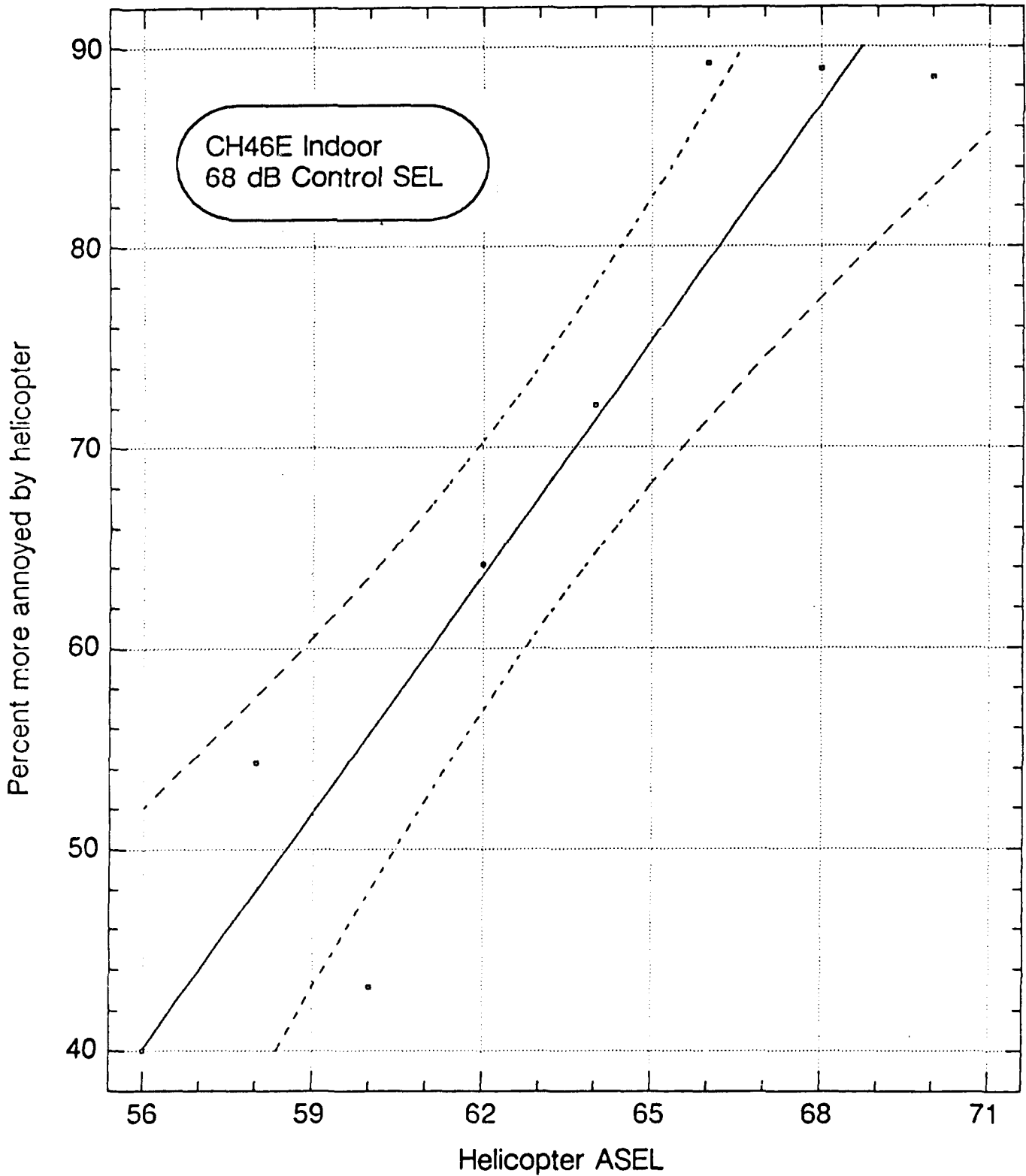
Regression of E5392.A on E5392.H



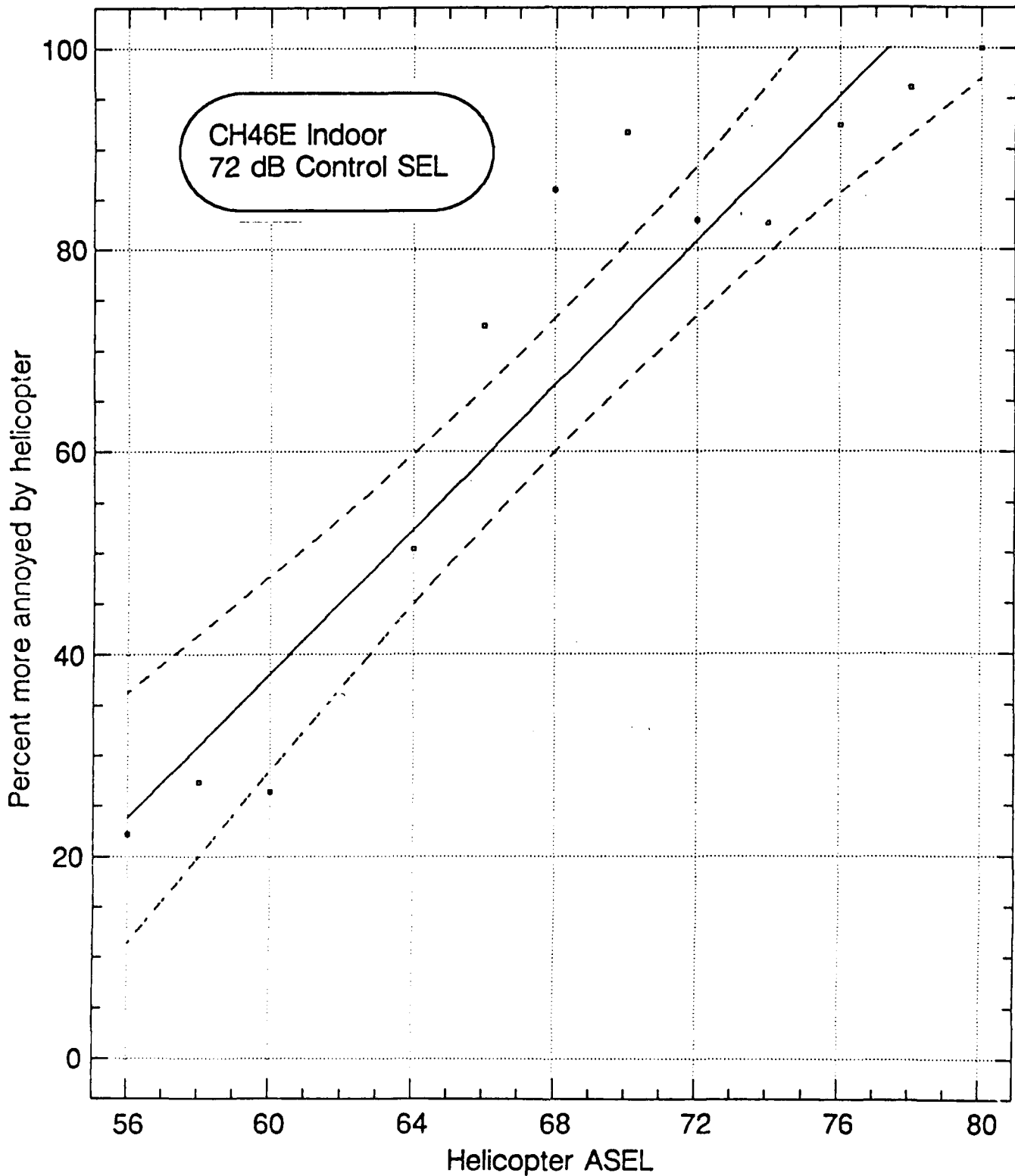
Regression of E4664.A on E4664.H



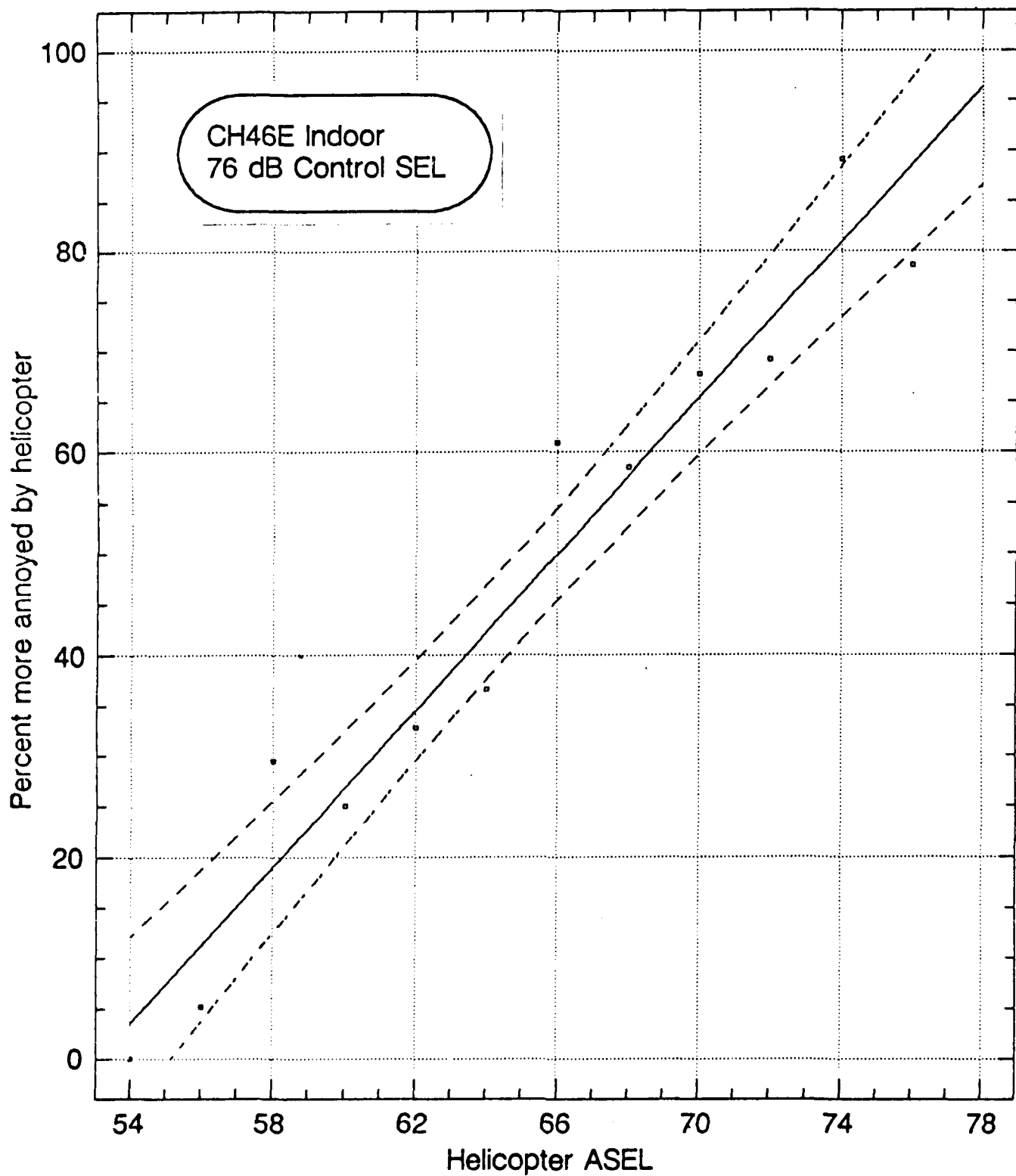
Regression of E4668.A on E4668.H



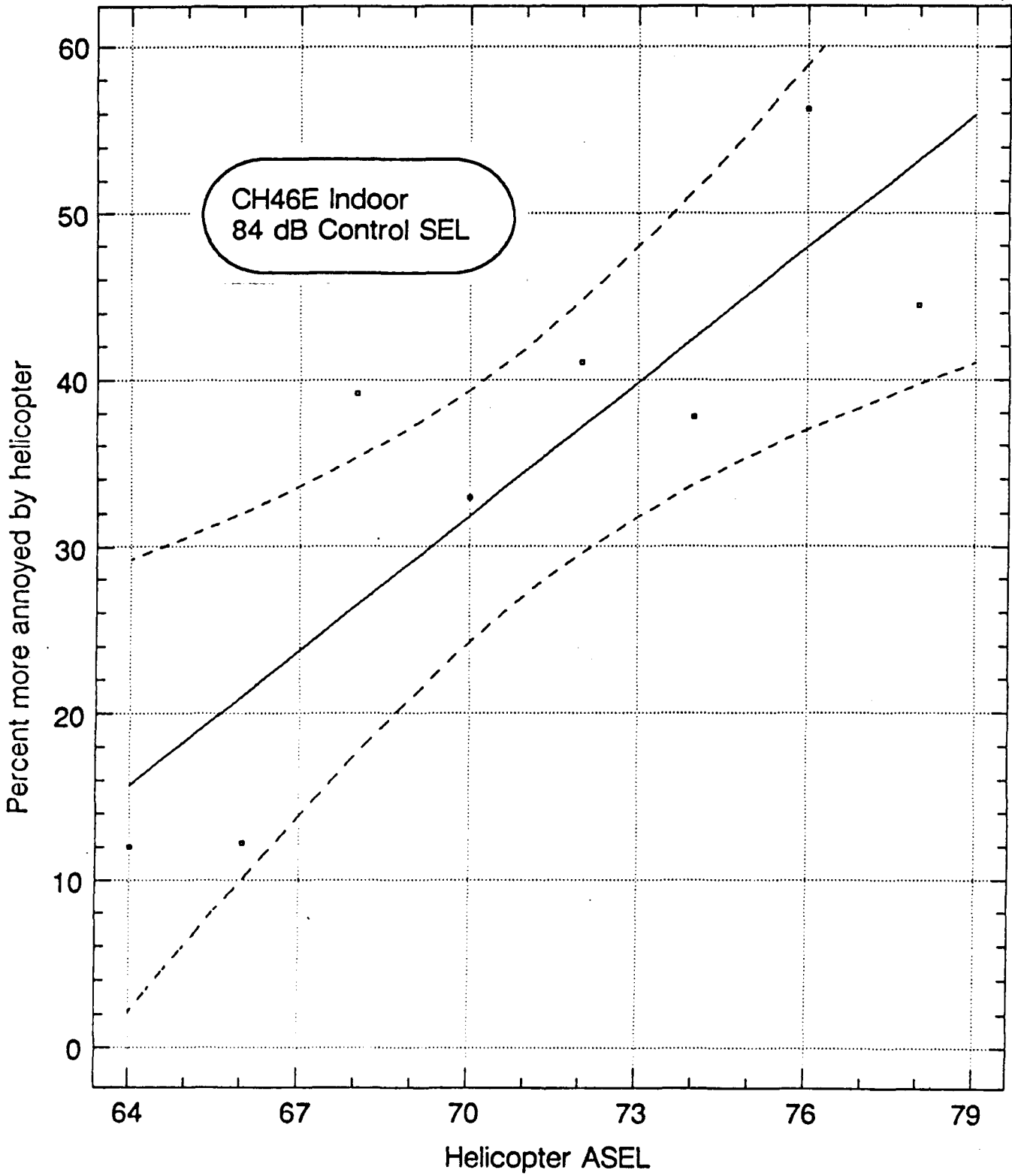
Regression of E4672.A on E4672.H



Regression of E4676.A on E4676.H

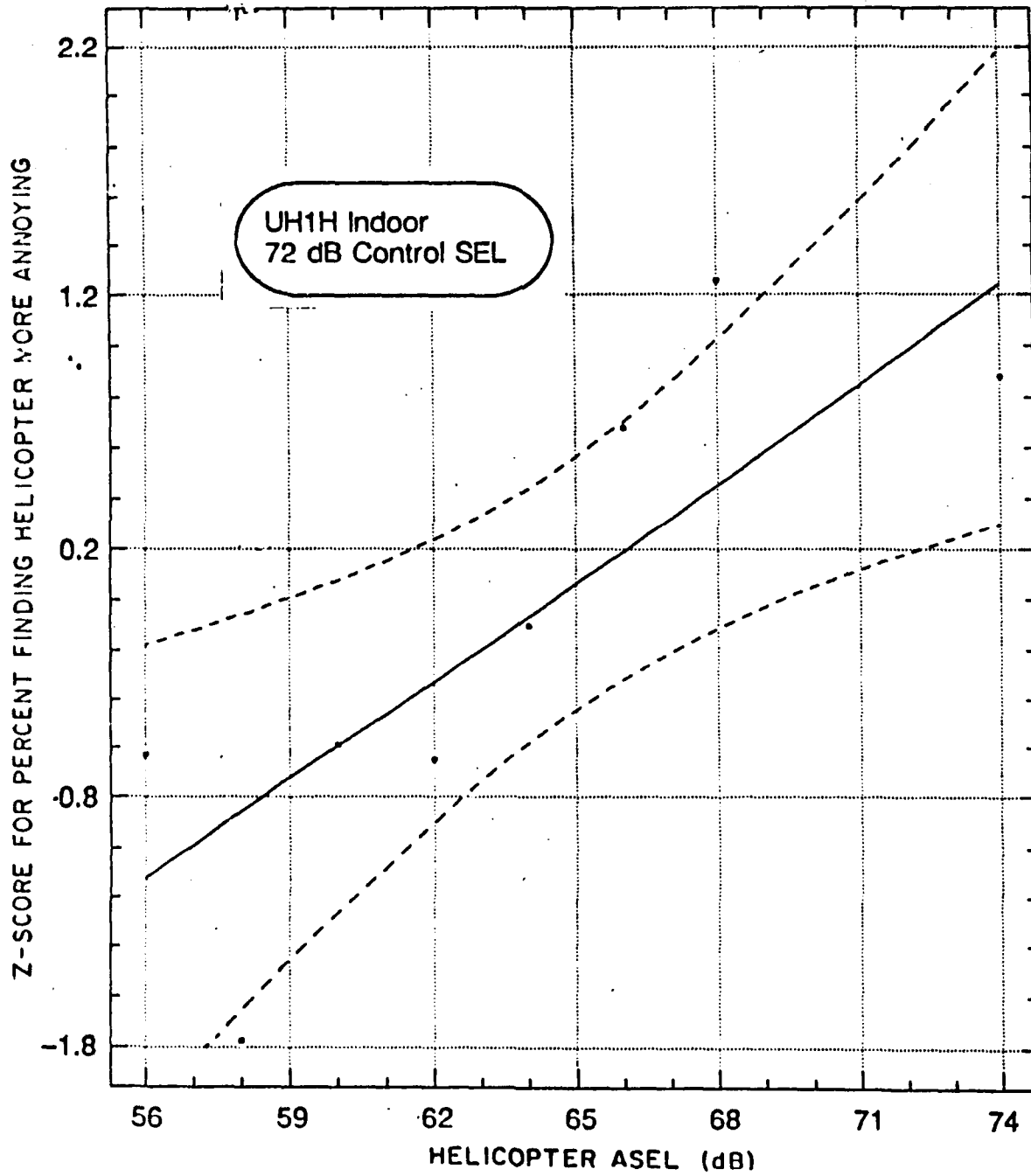


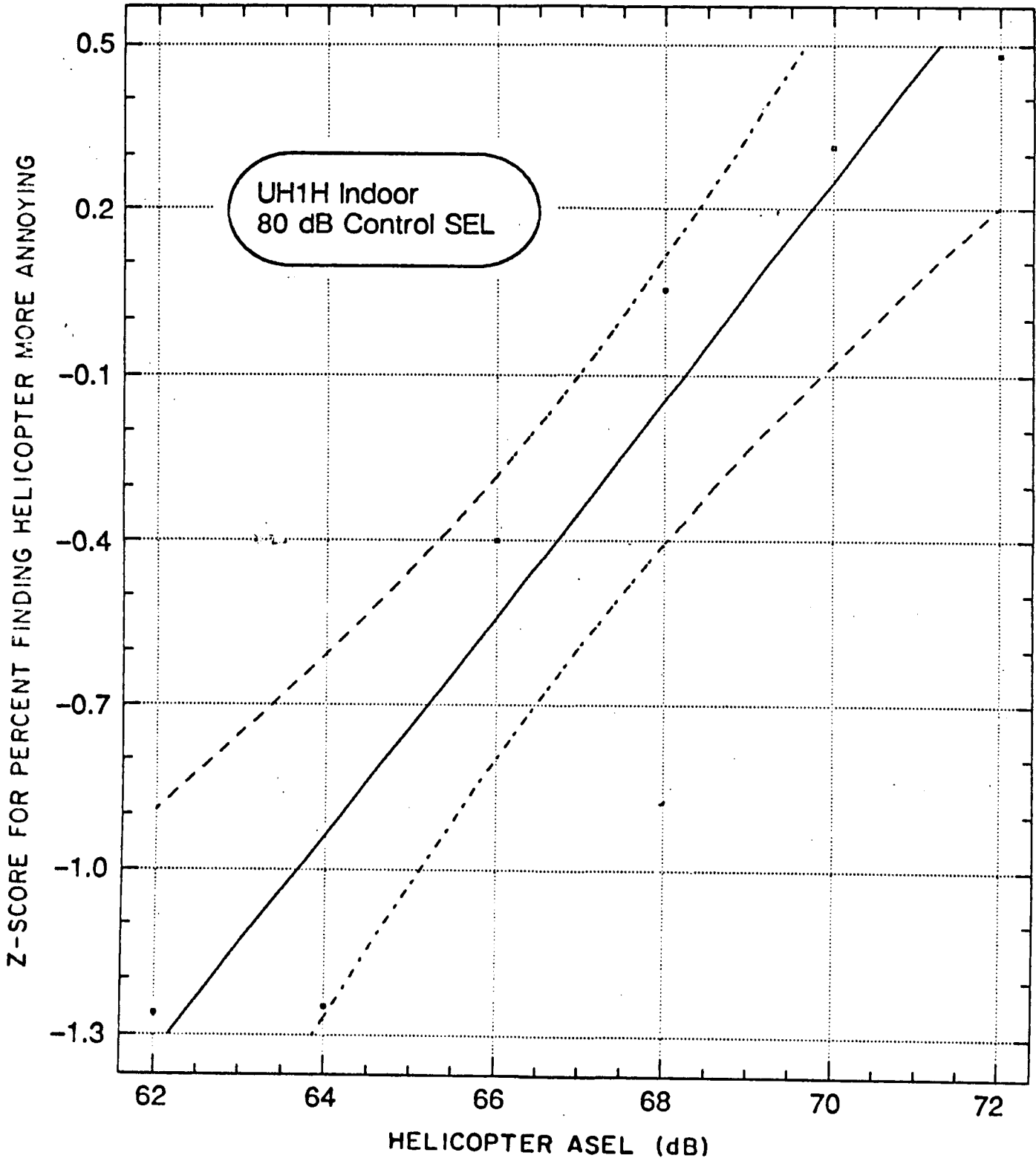
Regression of E4684.A on E4684.H

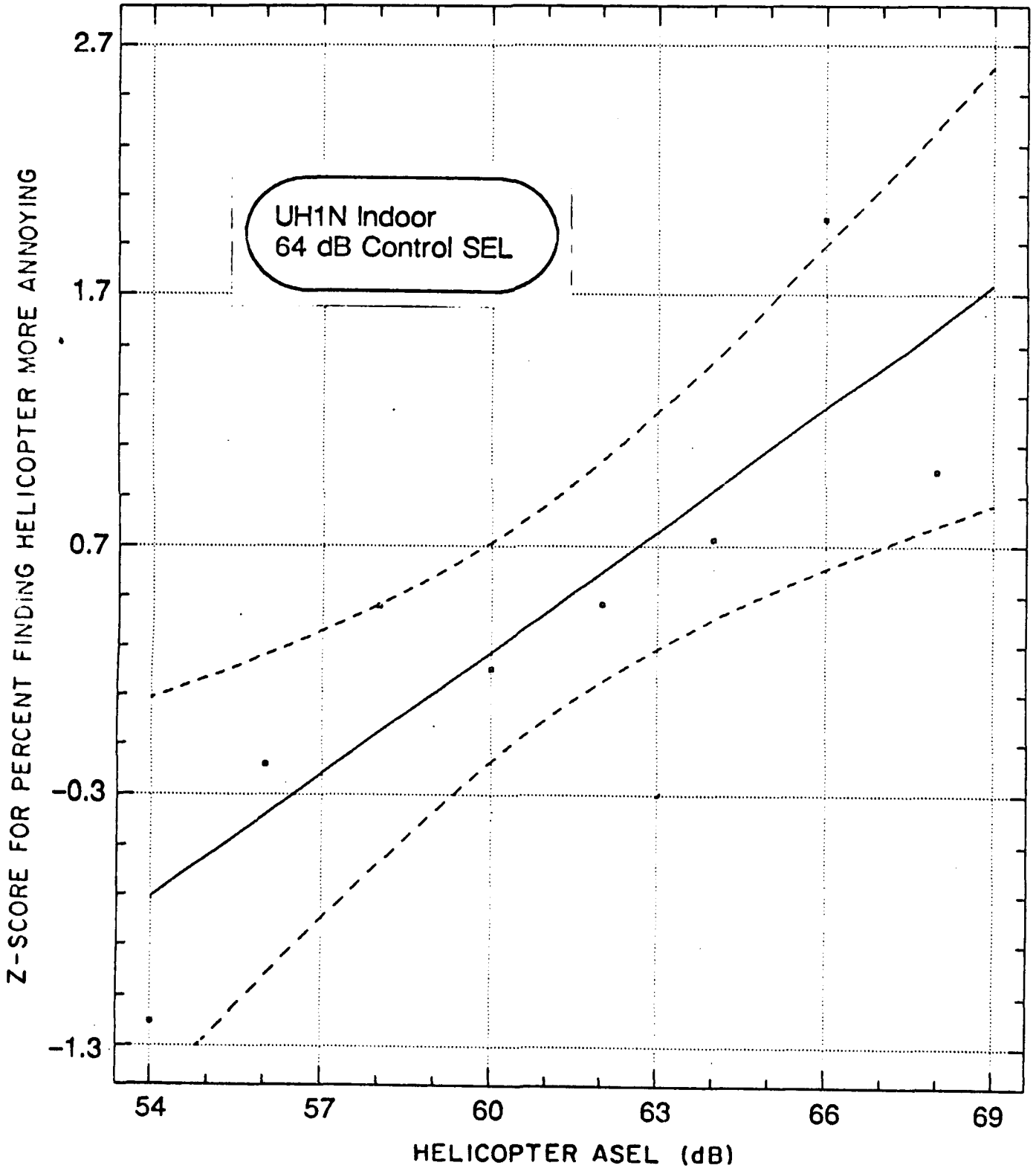


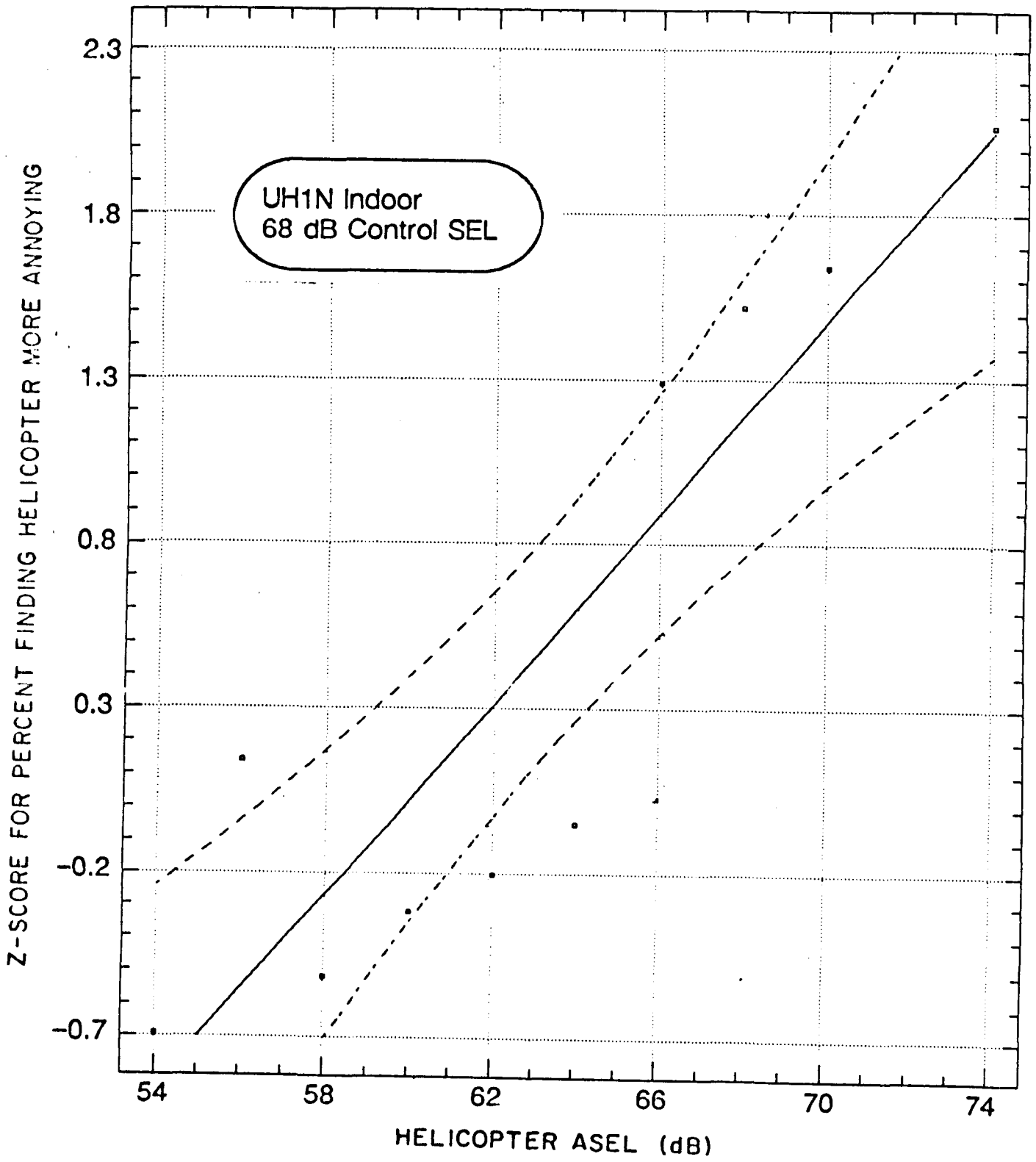
APPENDIX B

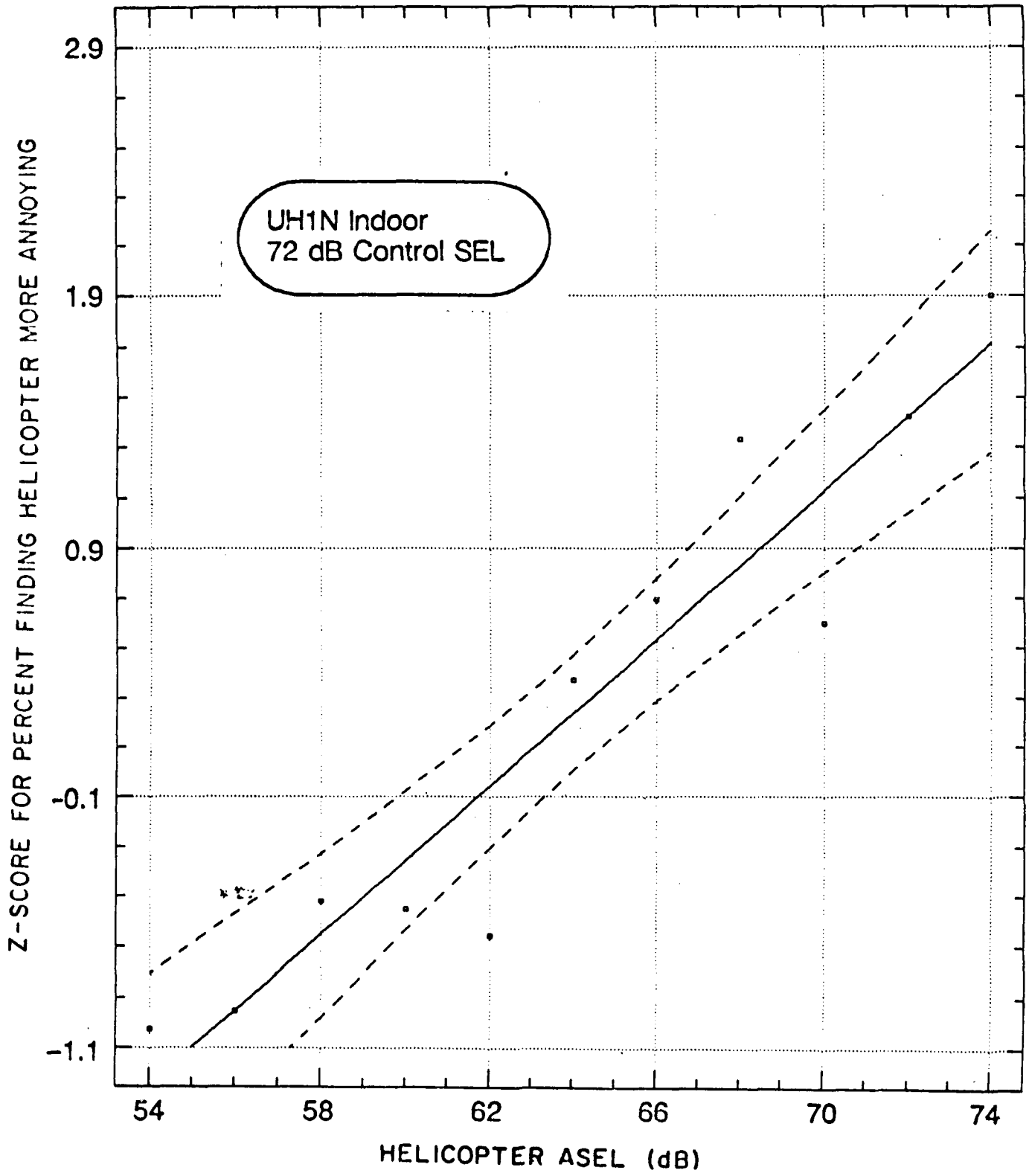
PLOTS OF MCAS TUSTIN INDOOR TEST DATA CONVERTED TO Z-SCORES
ARRANGED BY HELICOPTER IN ASCENDING ORDER OF CONTROL SEL

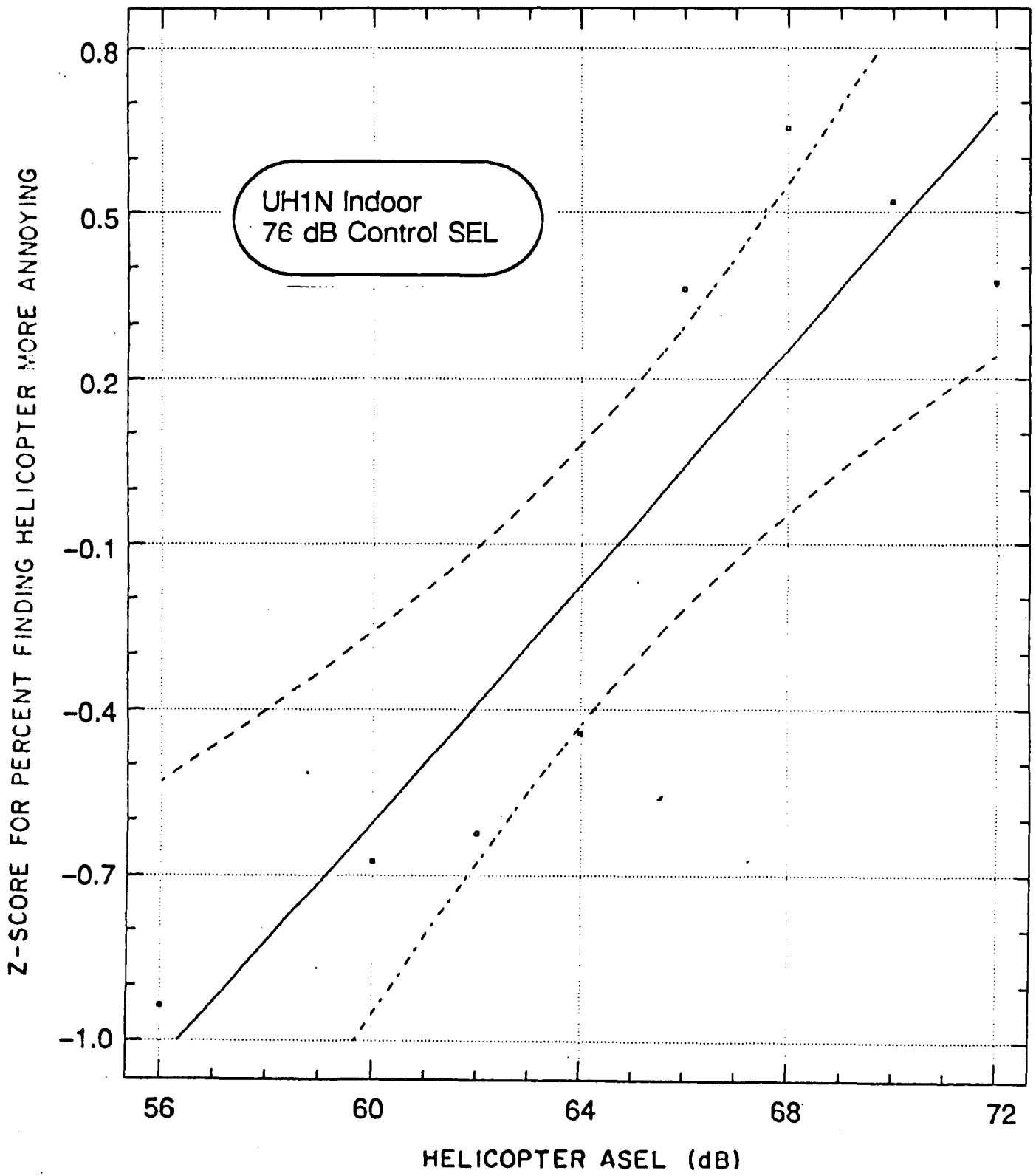


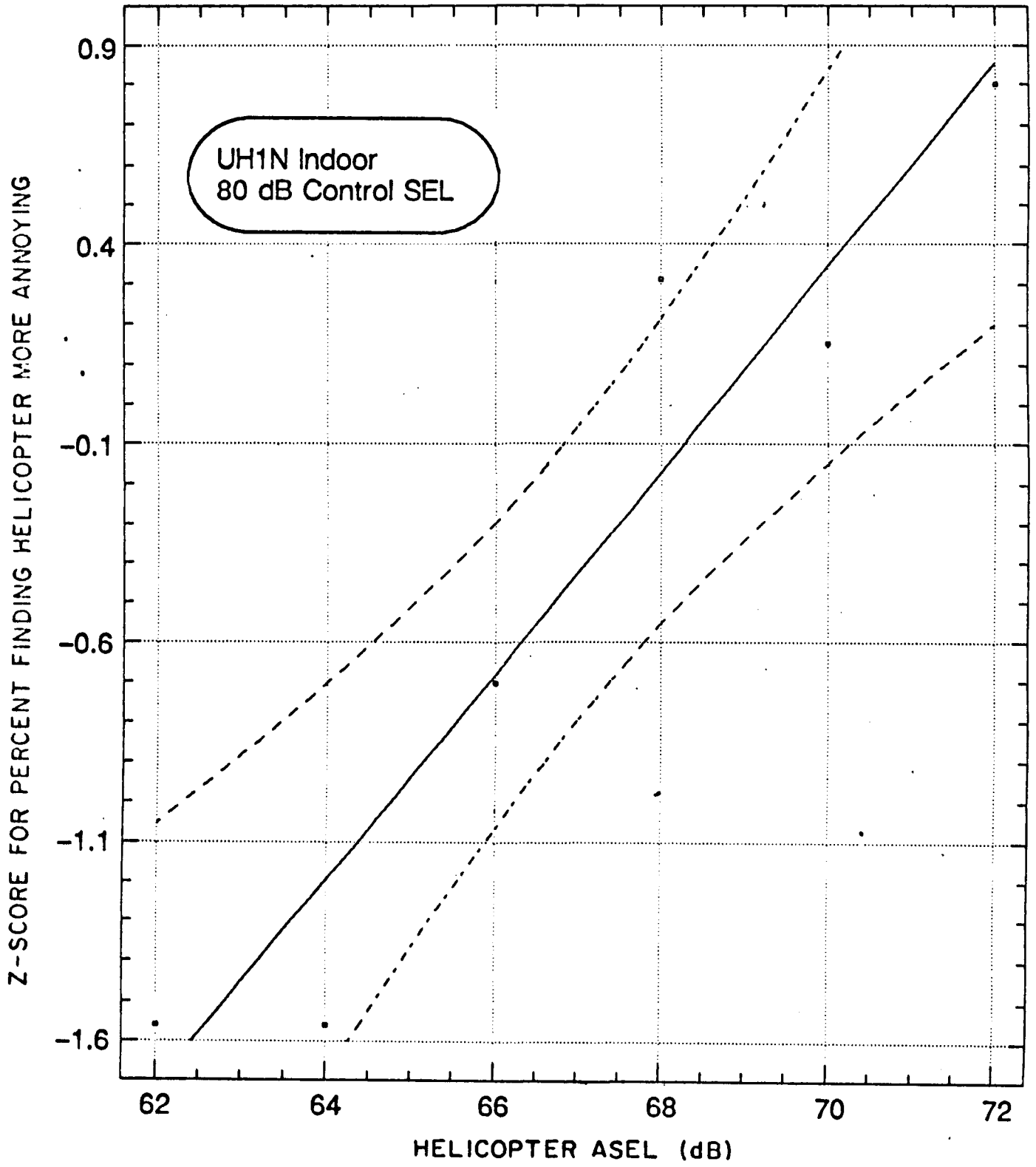








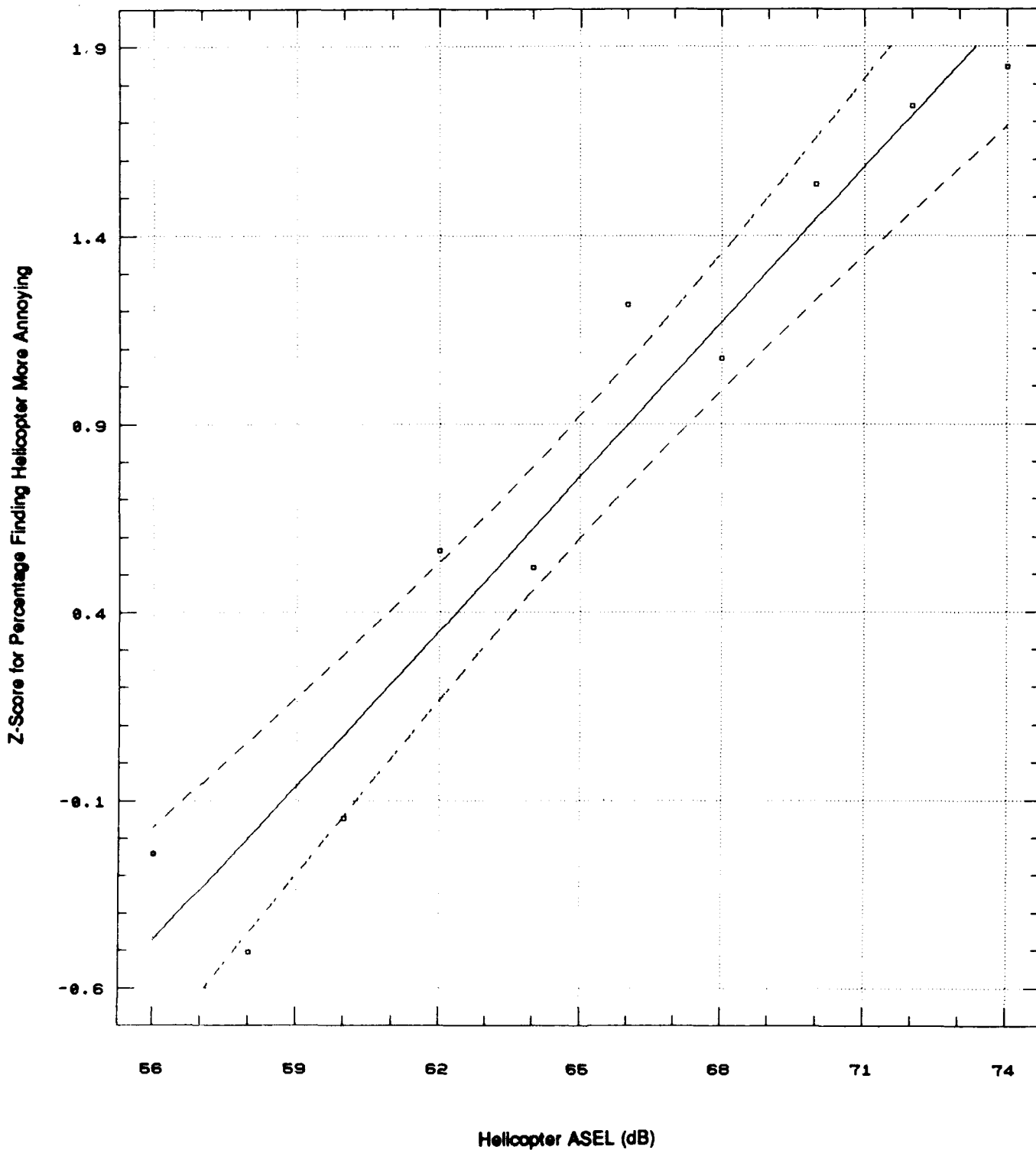




UH1N Indoor
80 dB Control SEL

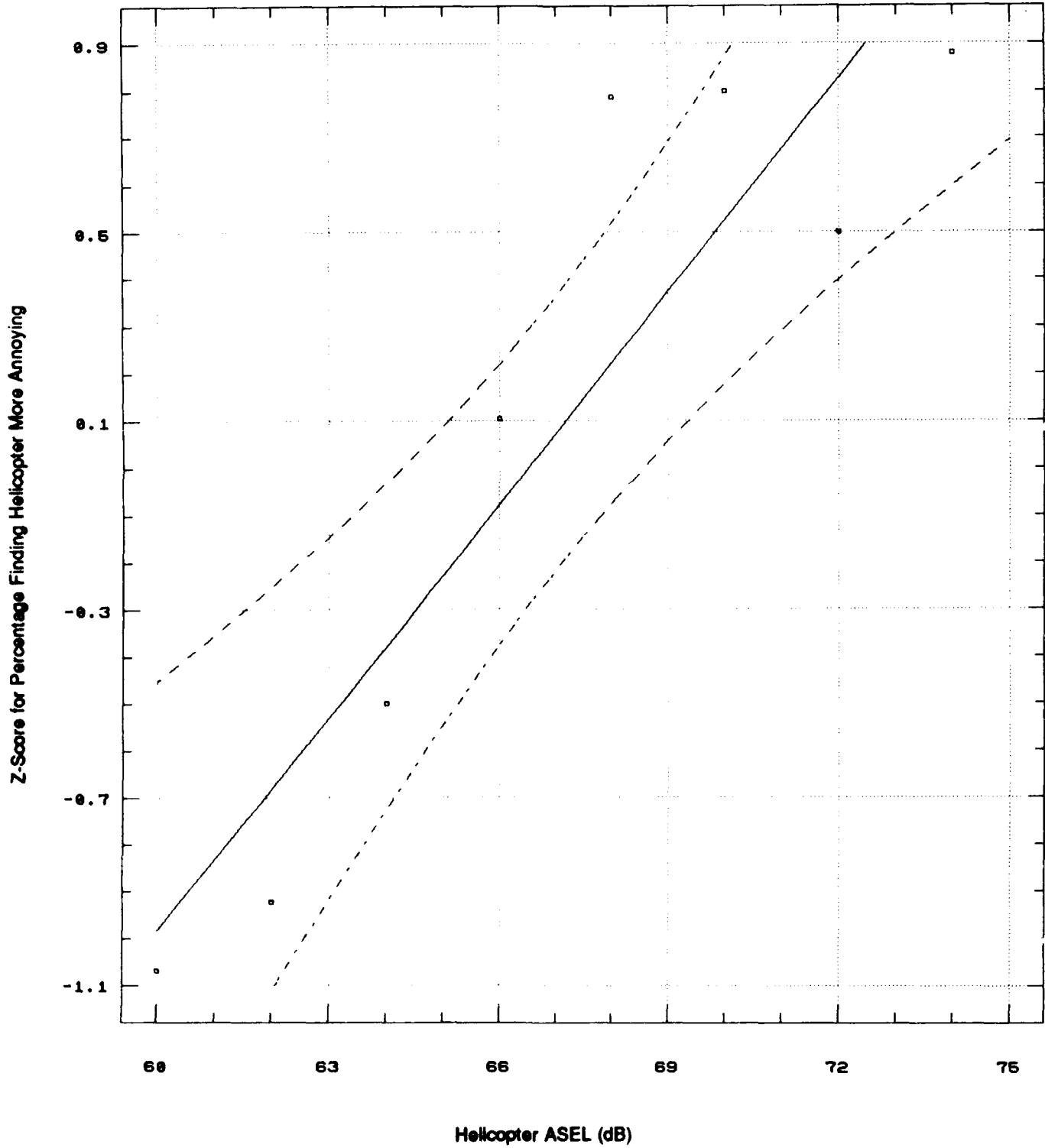
Regression of AH68.Z on AH68.H

AHIW Indoor
68 dB Control SEL



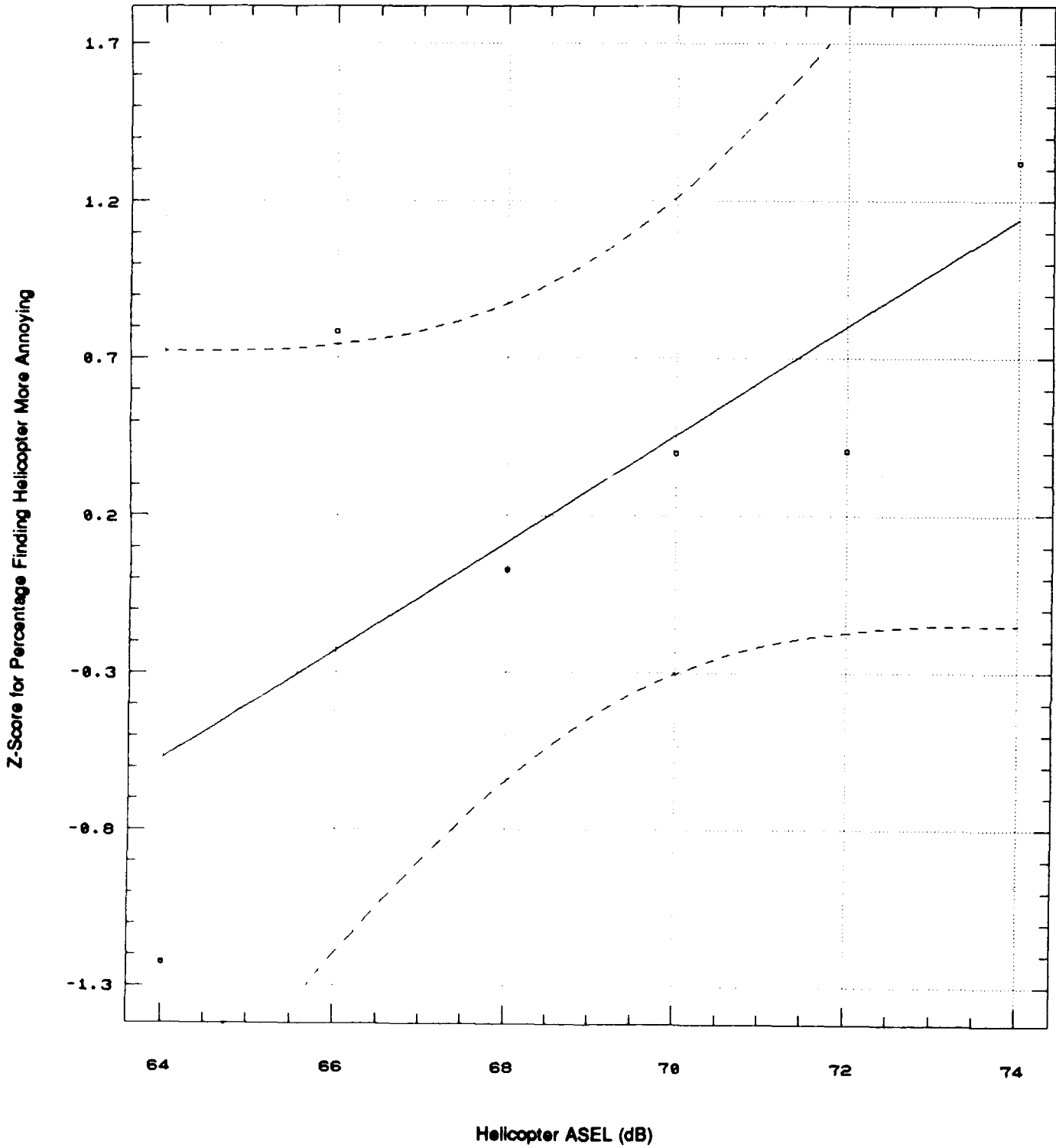
Regression of AH76.Z on AH76.H

AHIW Indoor
76 dB Control SEL



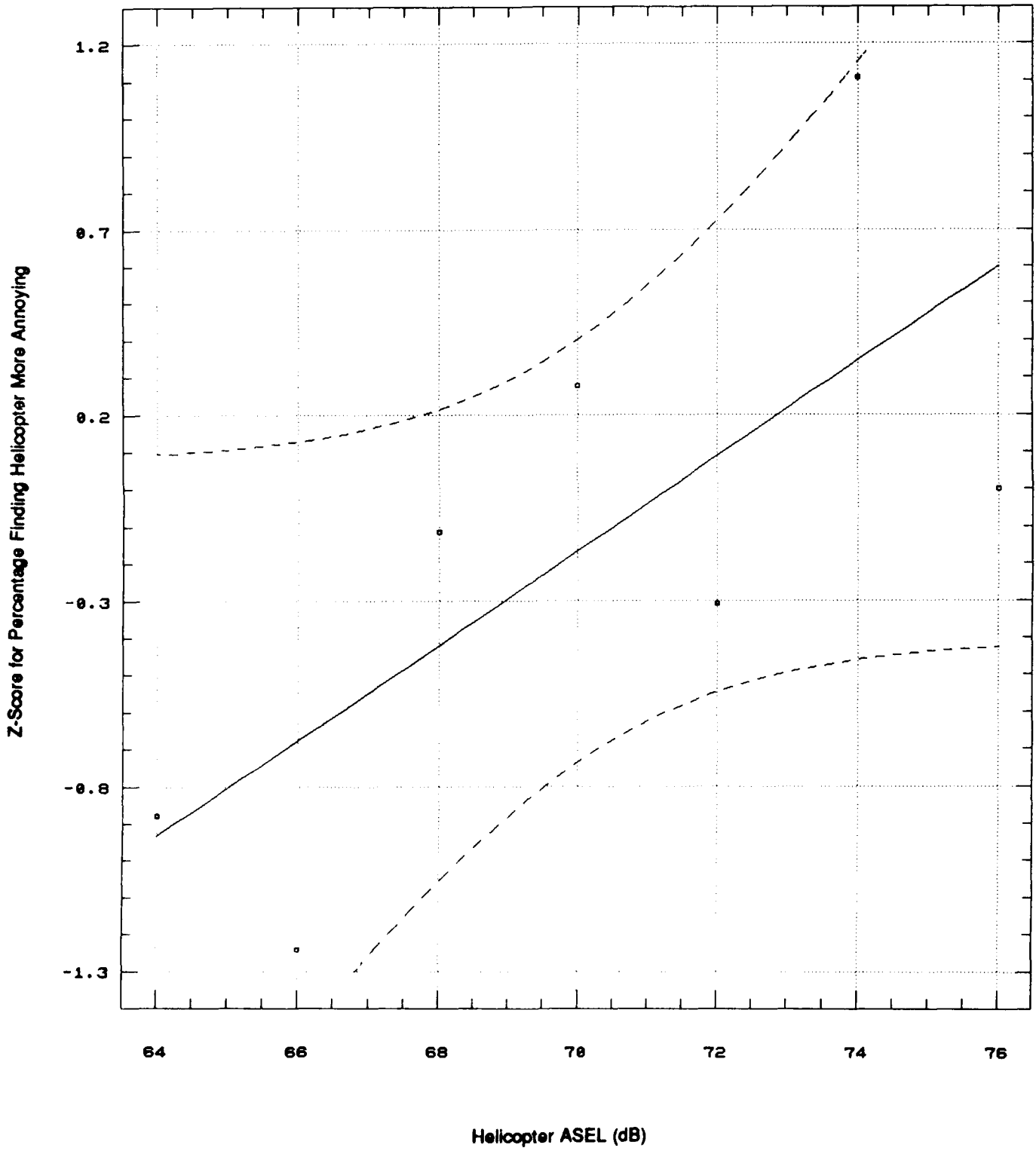
Regression of AH80.Z on AH80.H

AHIW Indoor
80 dB Control SEL



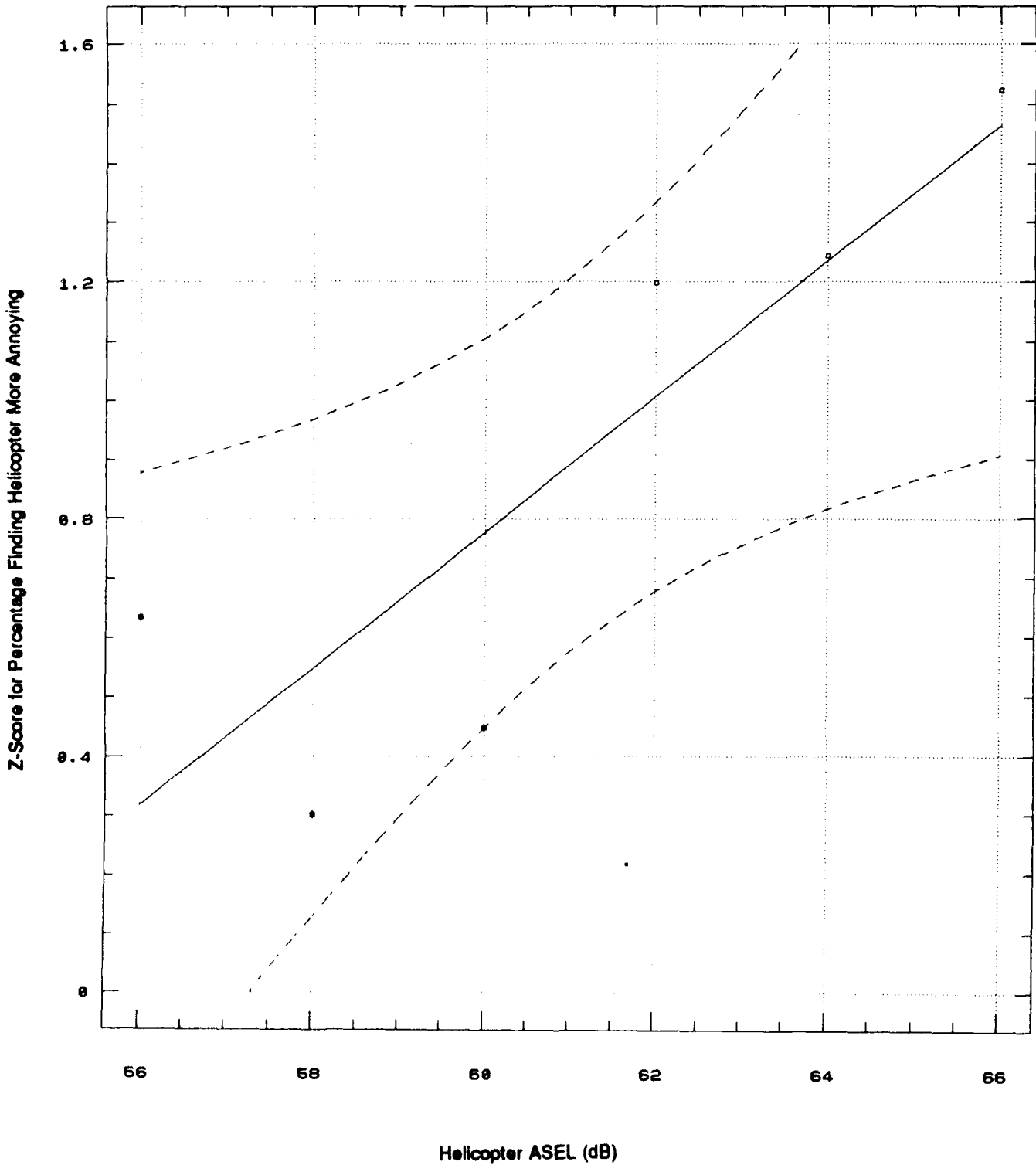
Regression of AH84.Z on AH84.H

AHIW Indoor
84 dB Control SEL

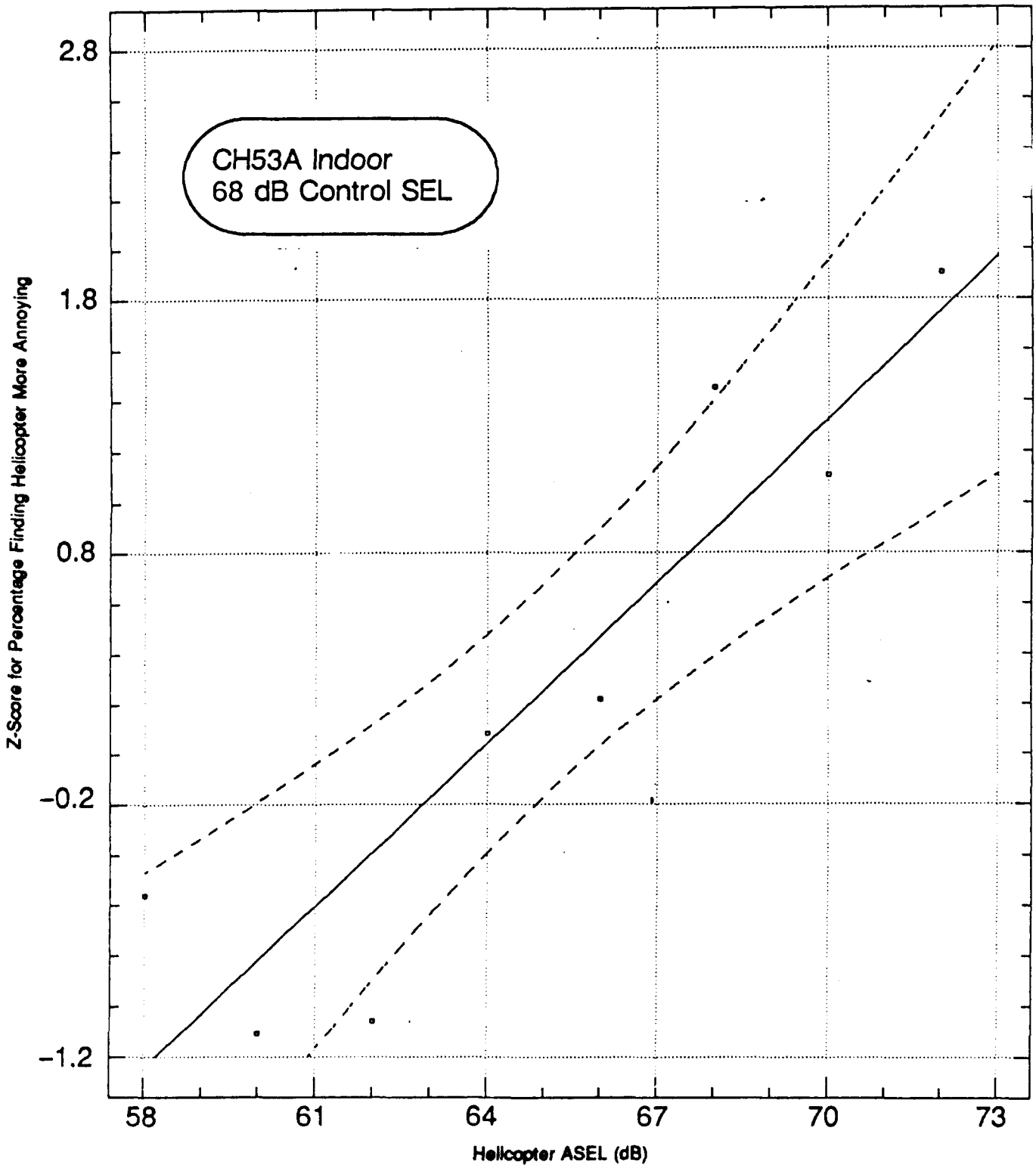


Regression of A5360.Z on A5360.H

CH53A Indoor
60 dB Control SEL

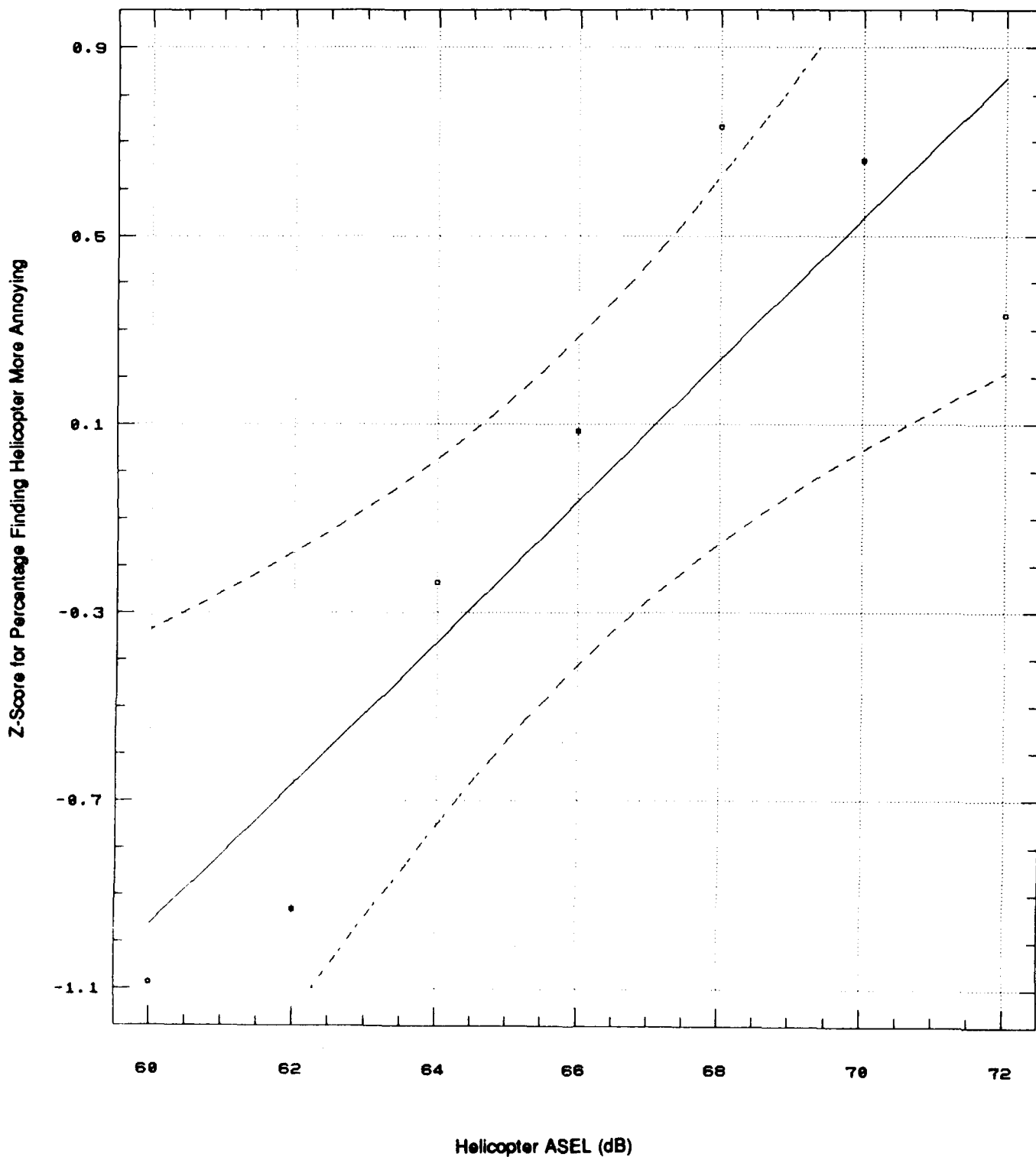


Regression of A5368.Z on A5368.H



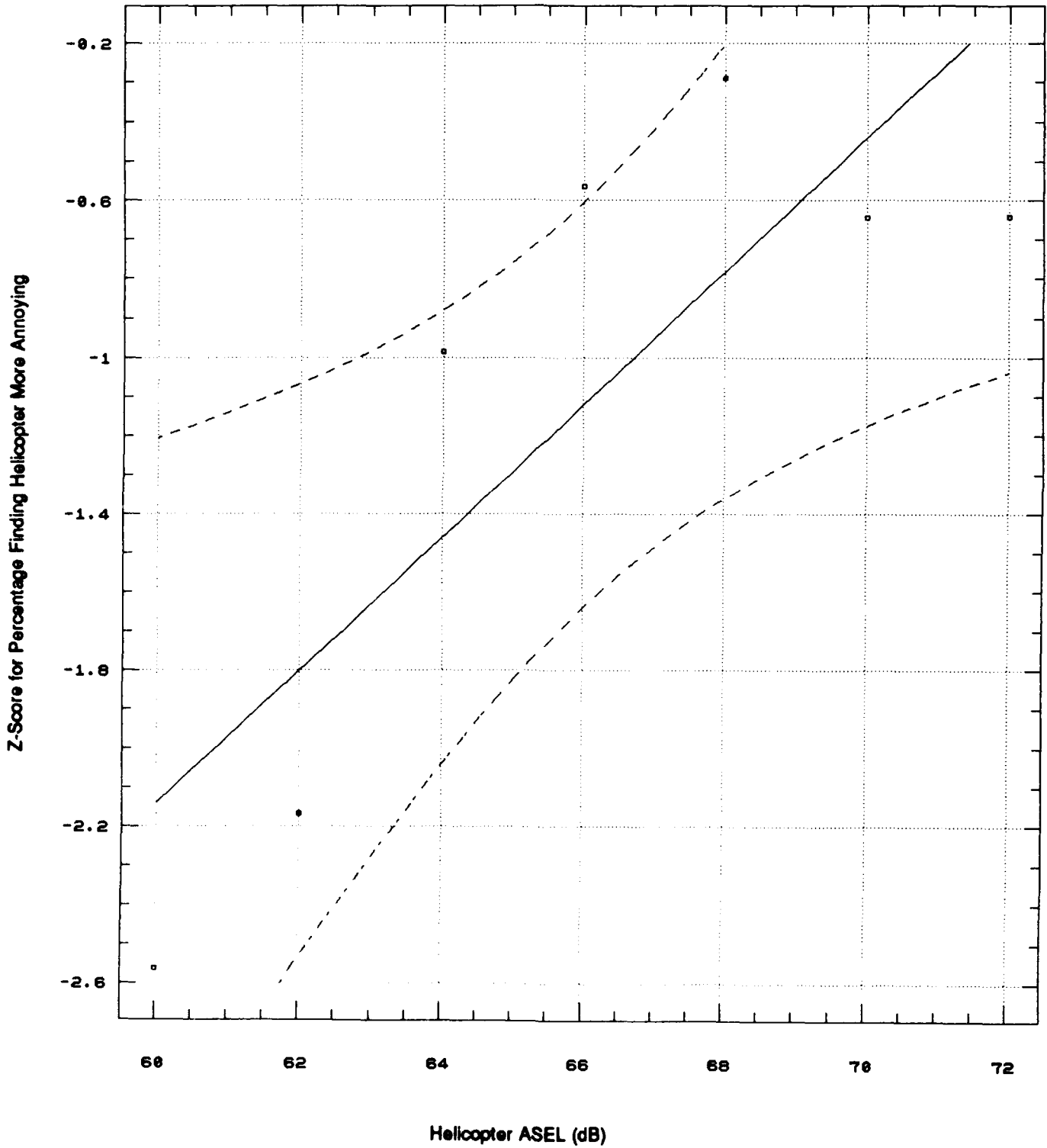
Regression of A5372.Z on A5372.H

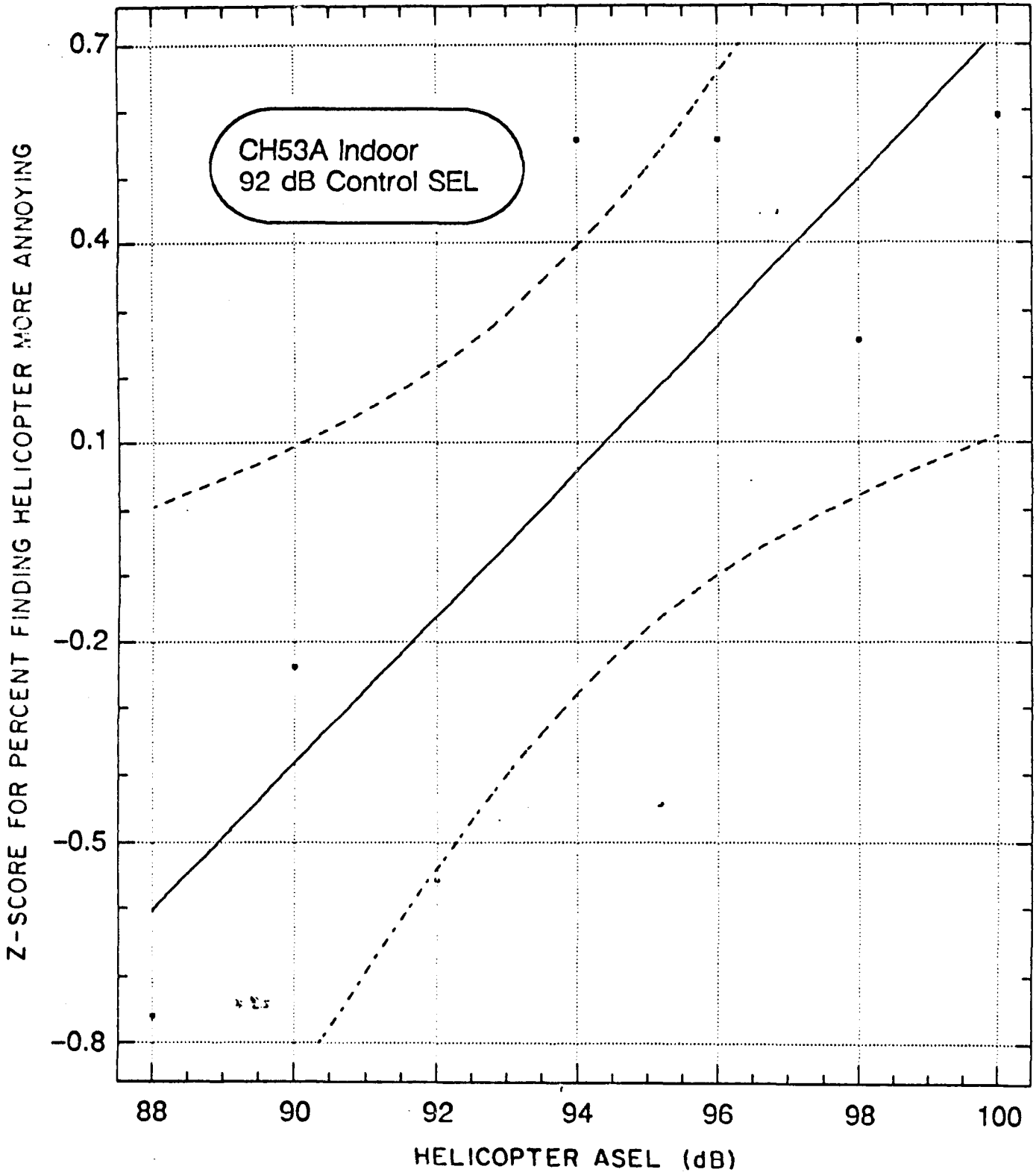
CH53A Indoor
72 dB Control SEL

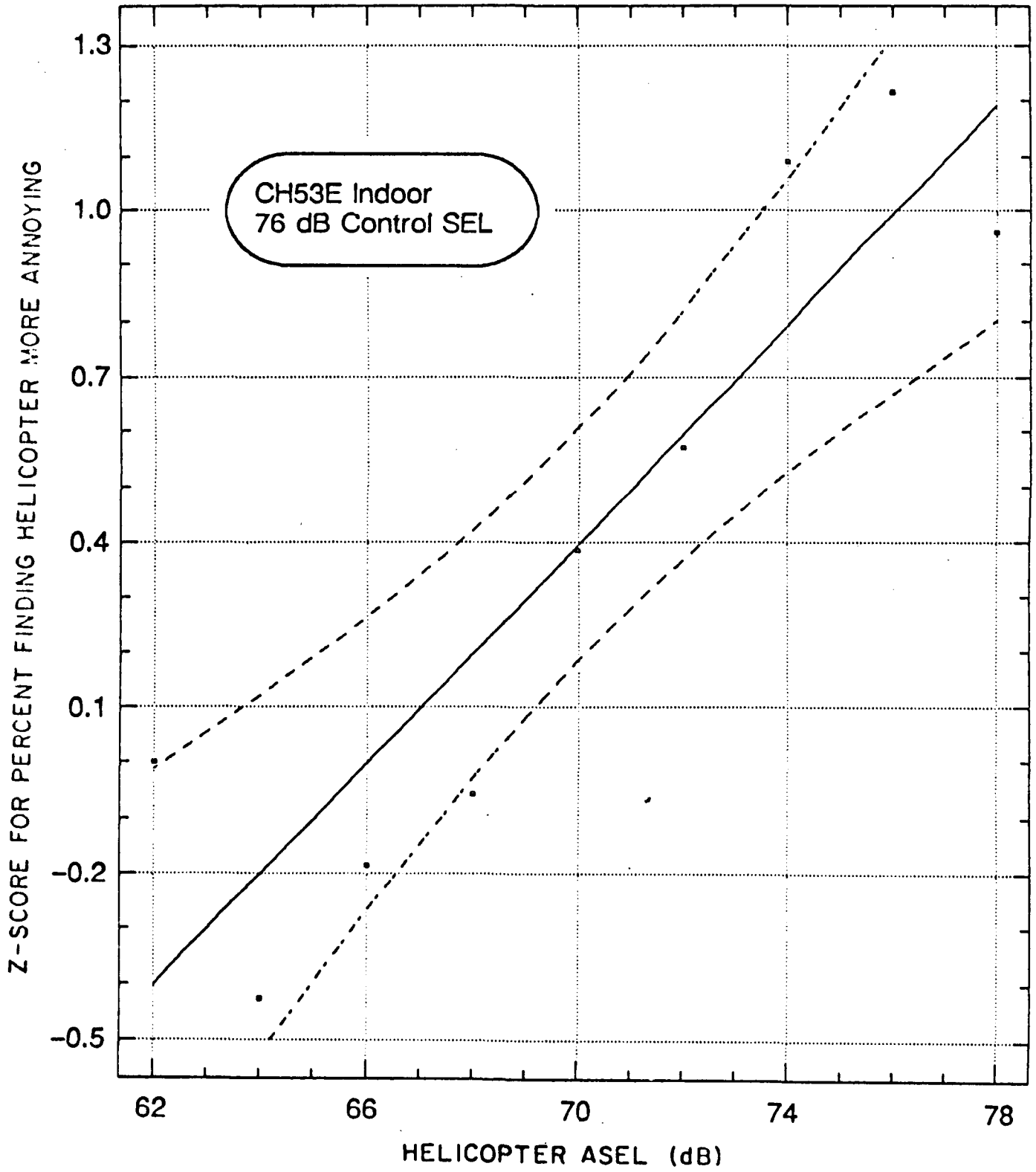


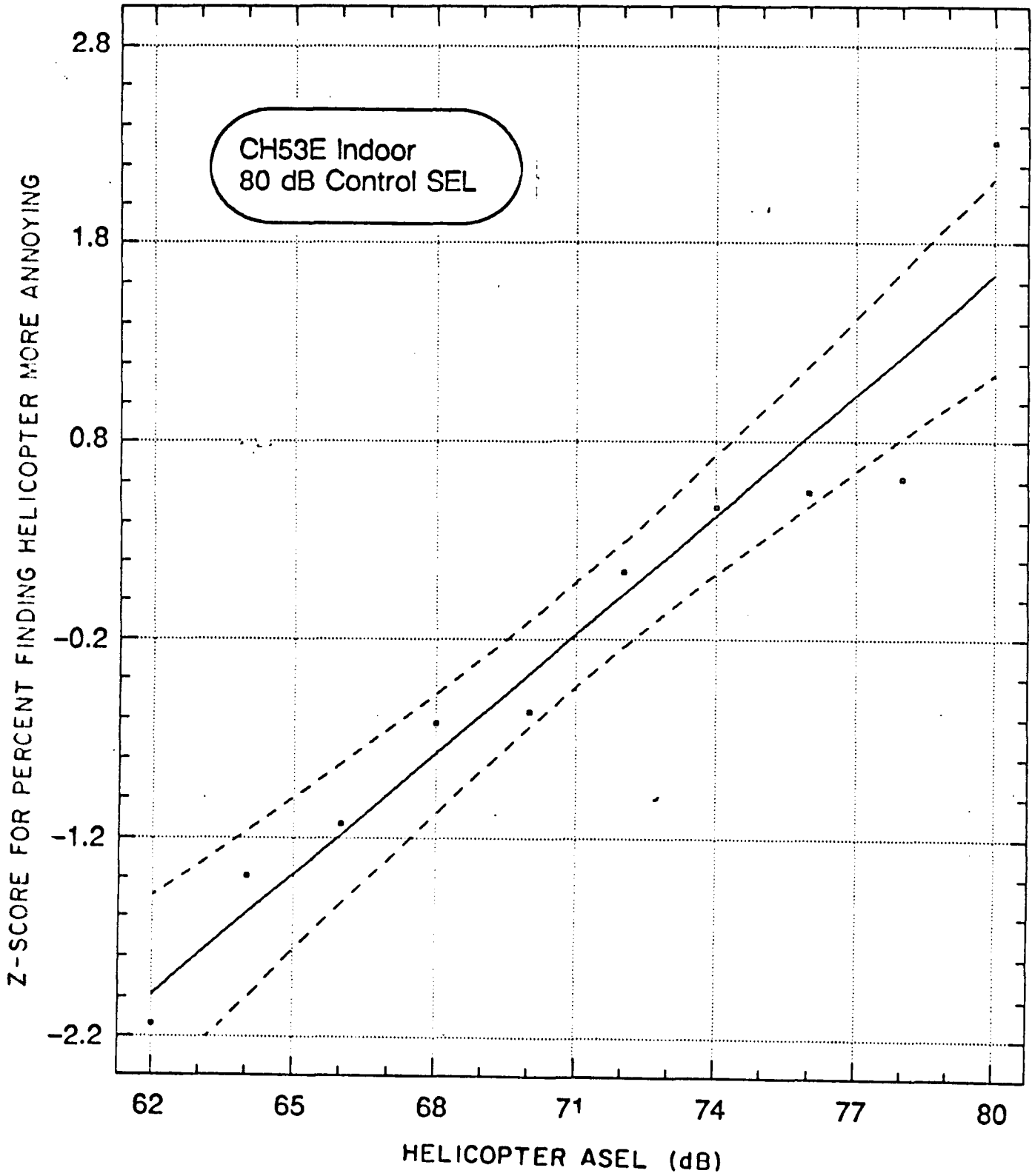
Regression of A5380.Z on A5380.H

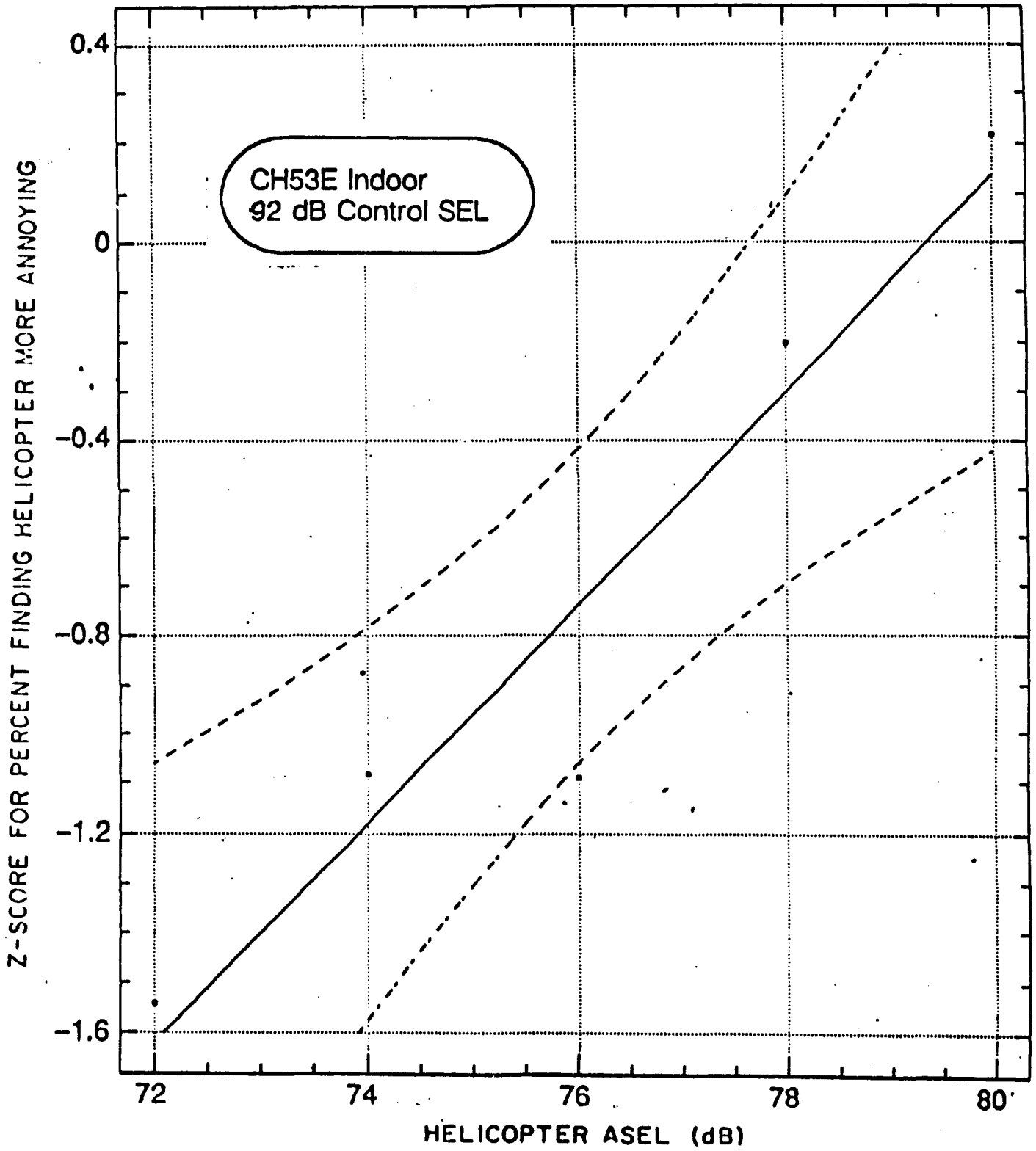
CH53A Indoor
80 dB Control SEL



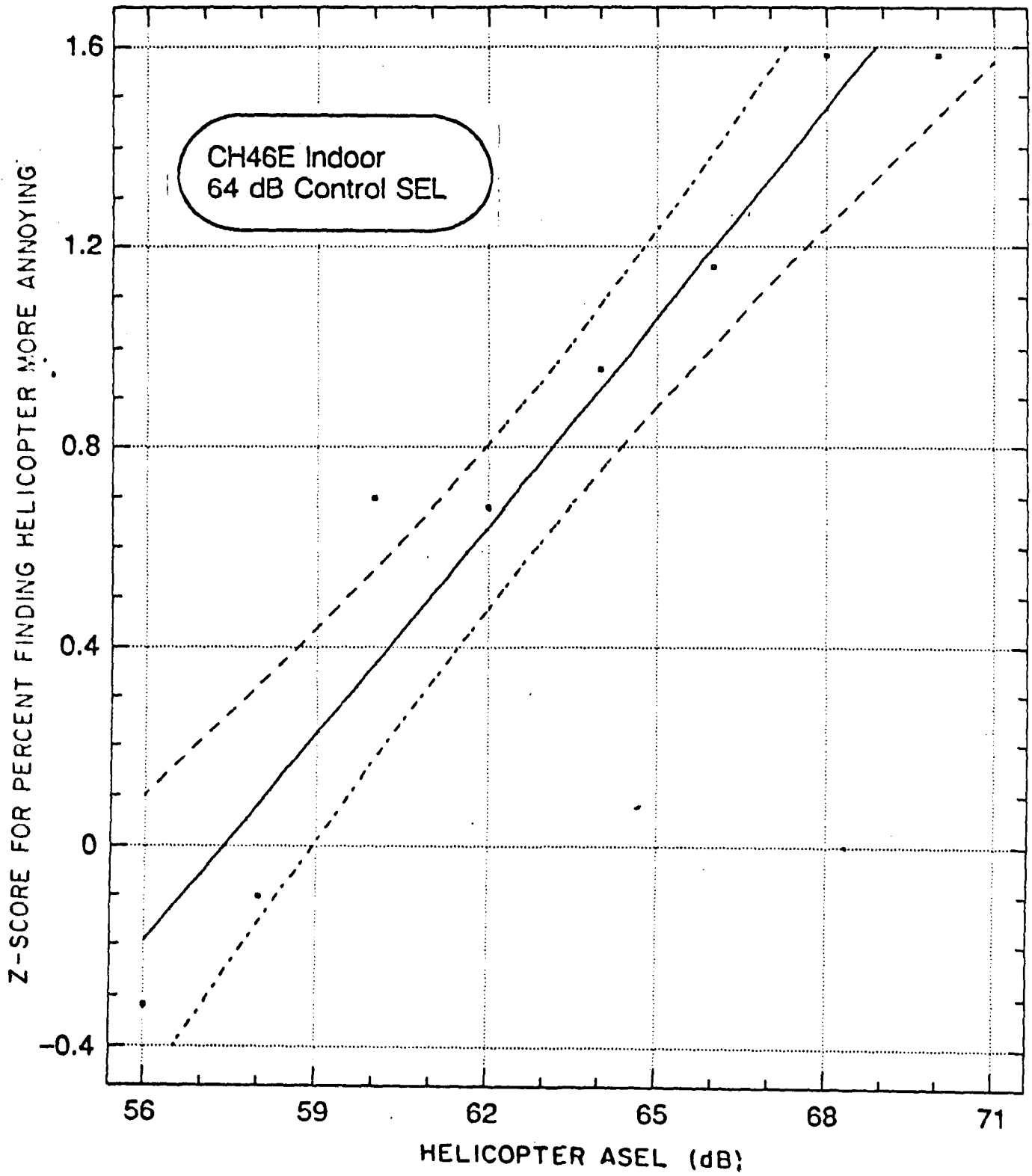


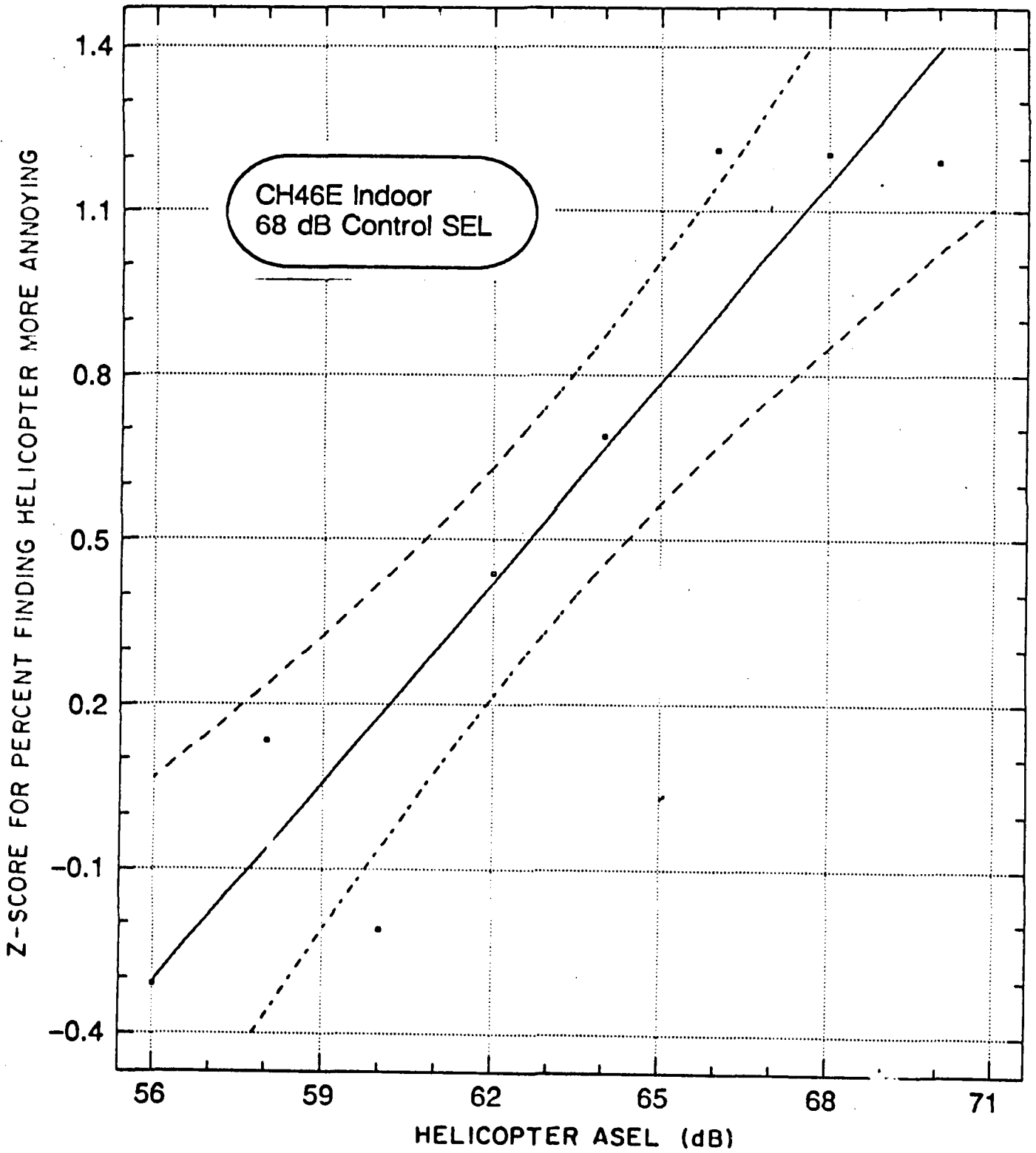


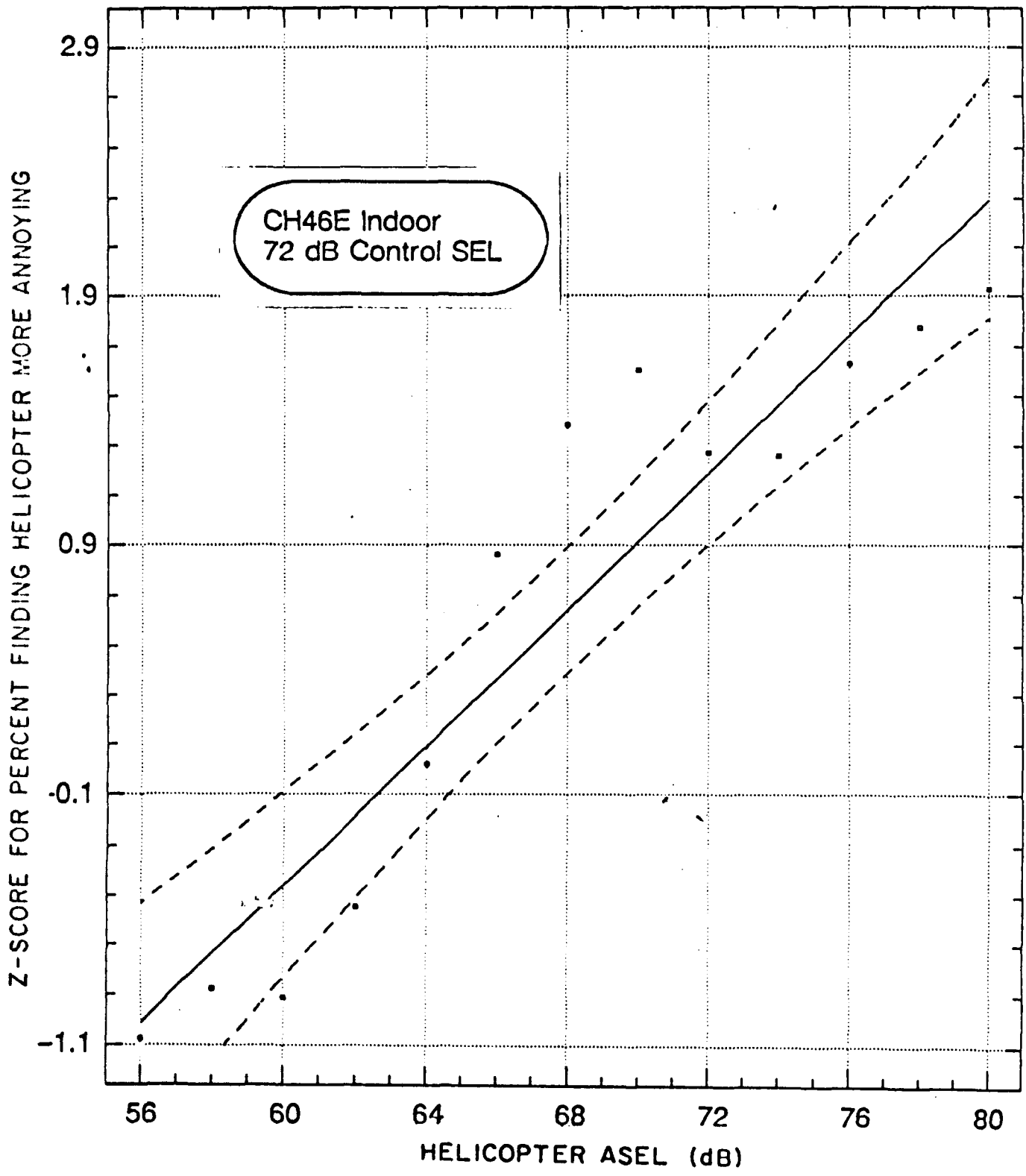


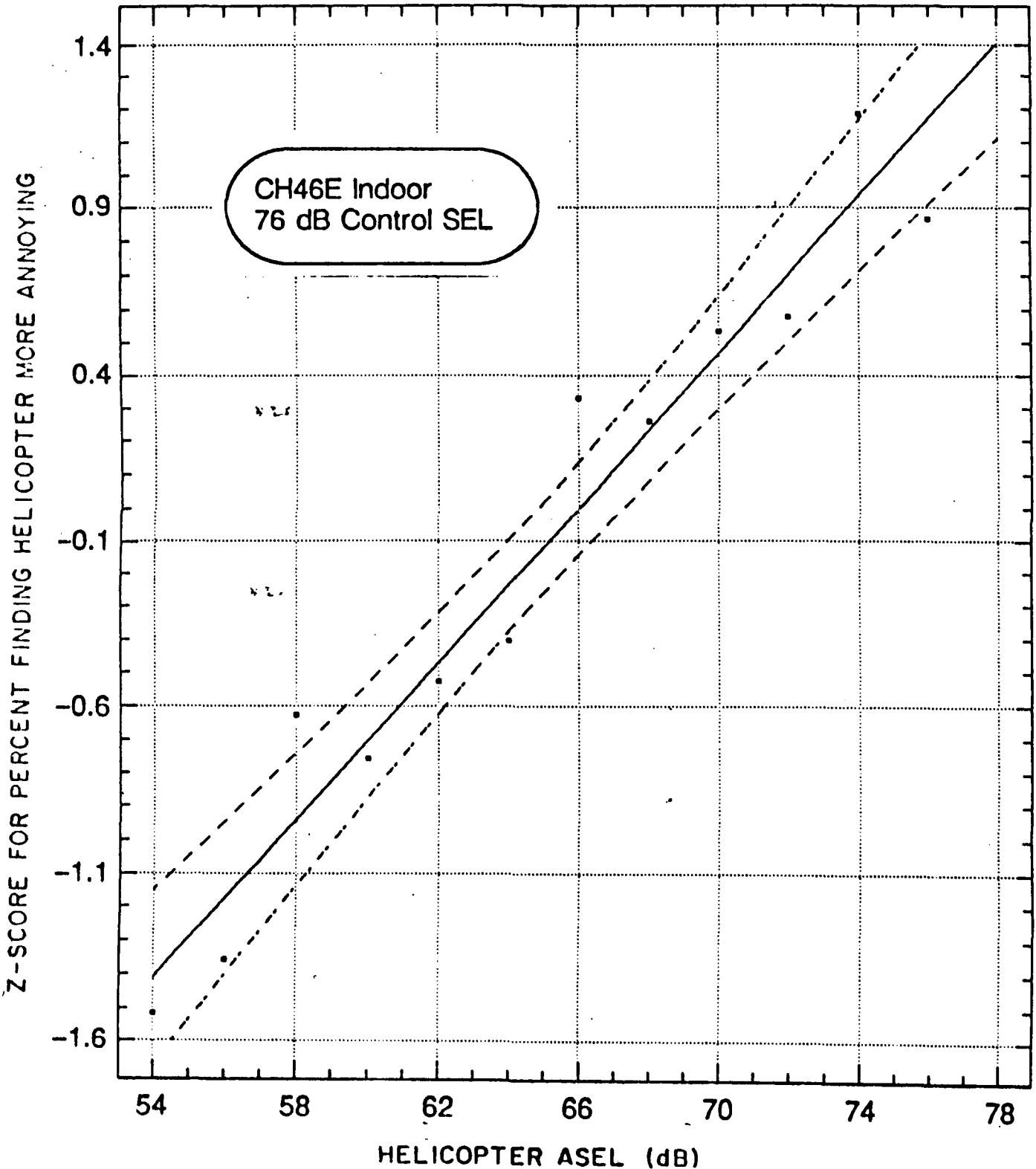


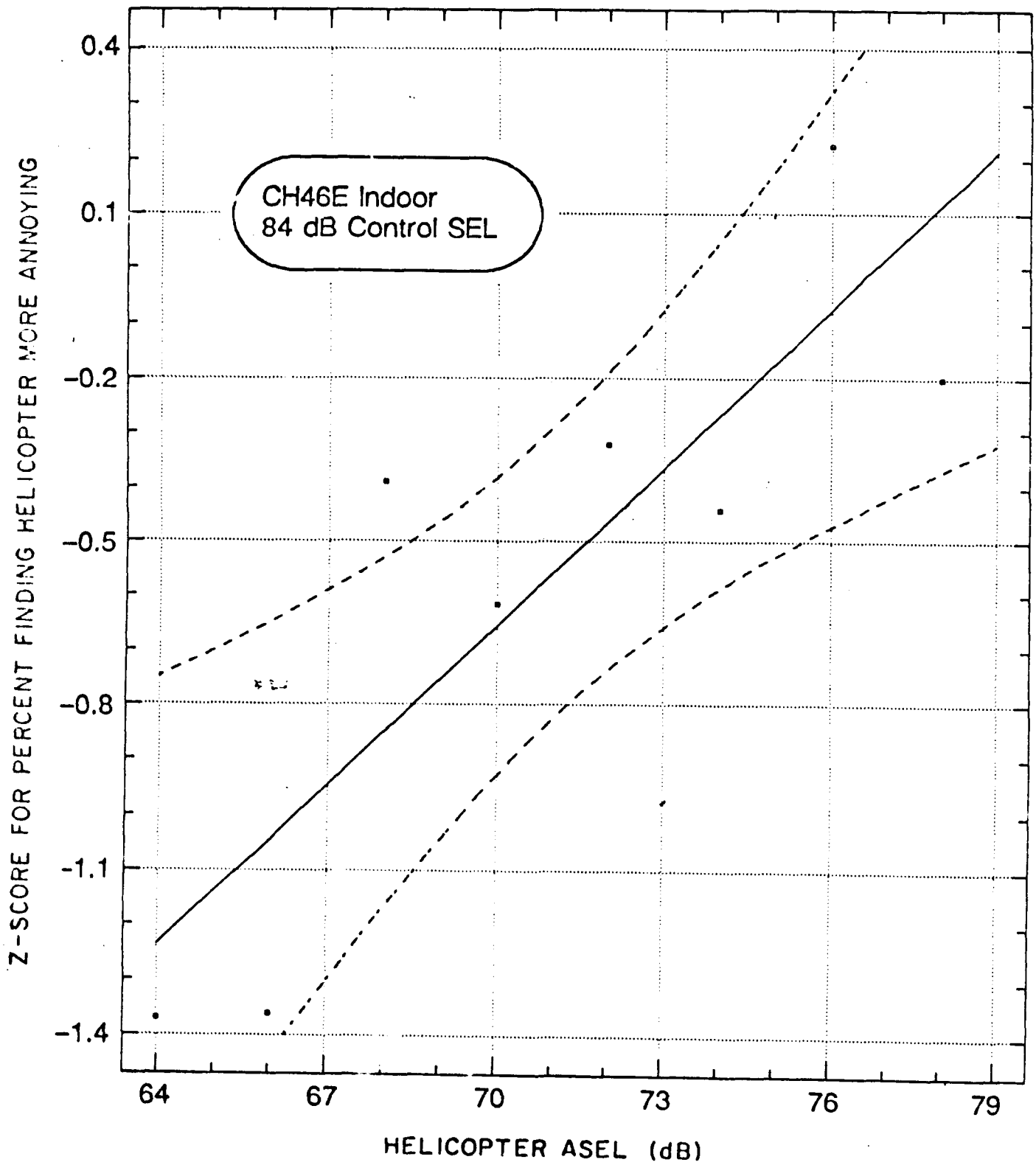
CH53E Indoor
92 dB Control SEL









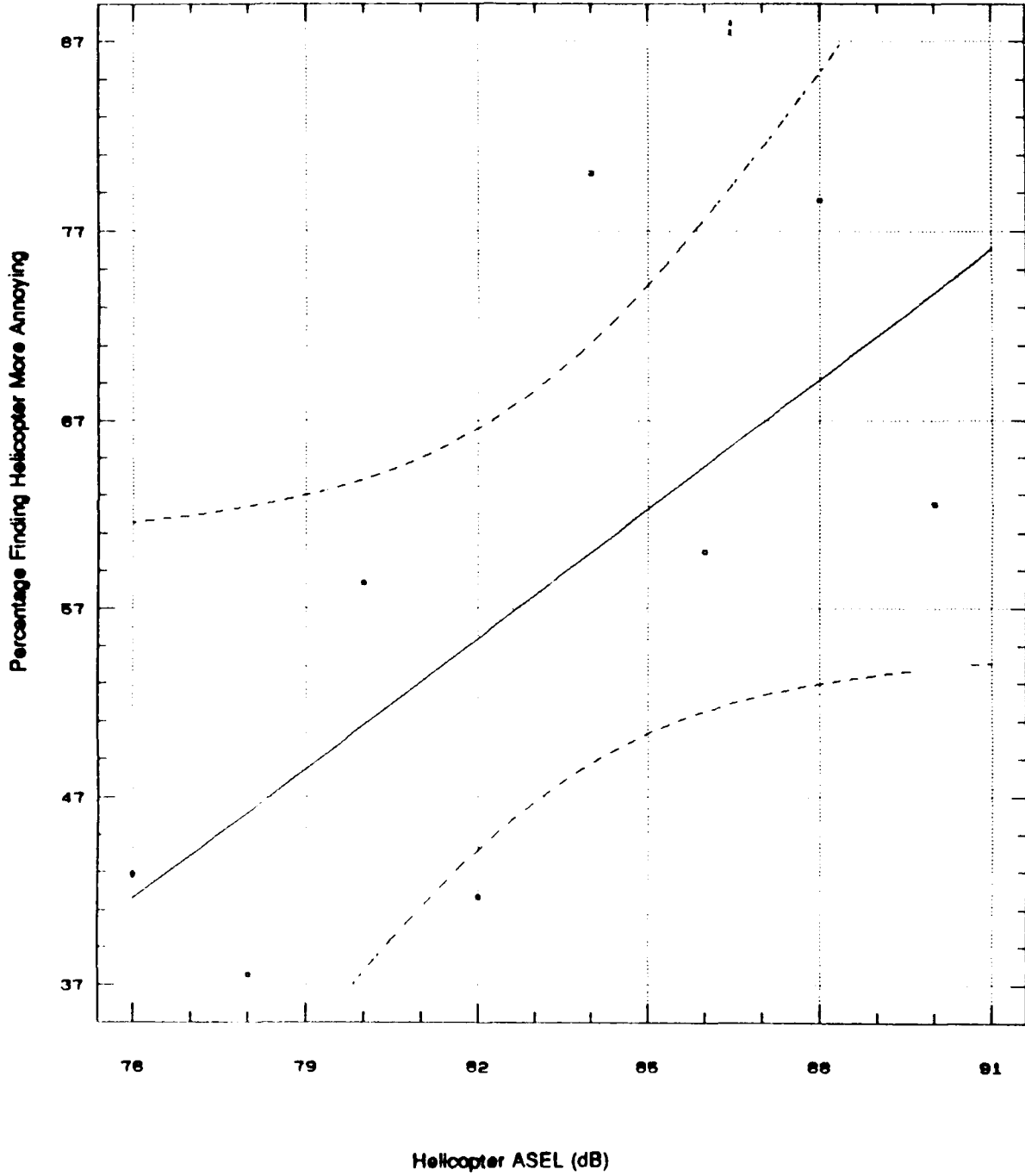


APPENDIX C

PLOTS OF MCAS TUSTIN OUTDOOR TEST DATA

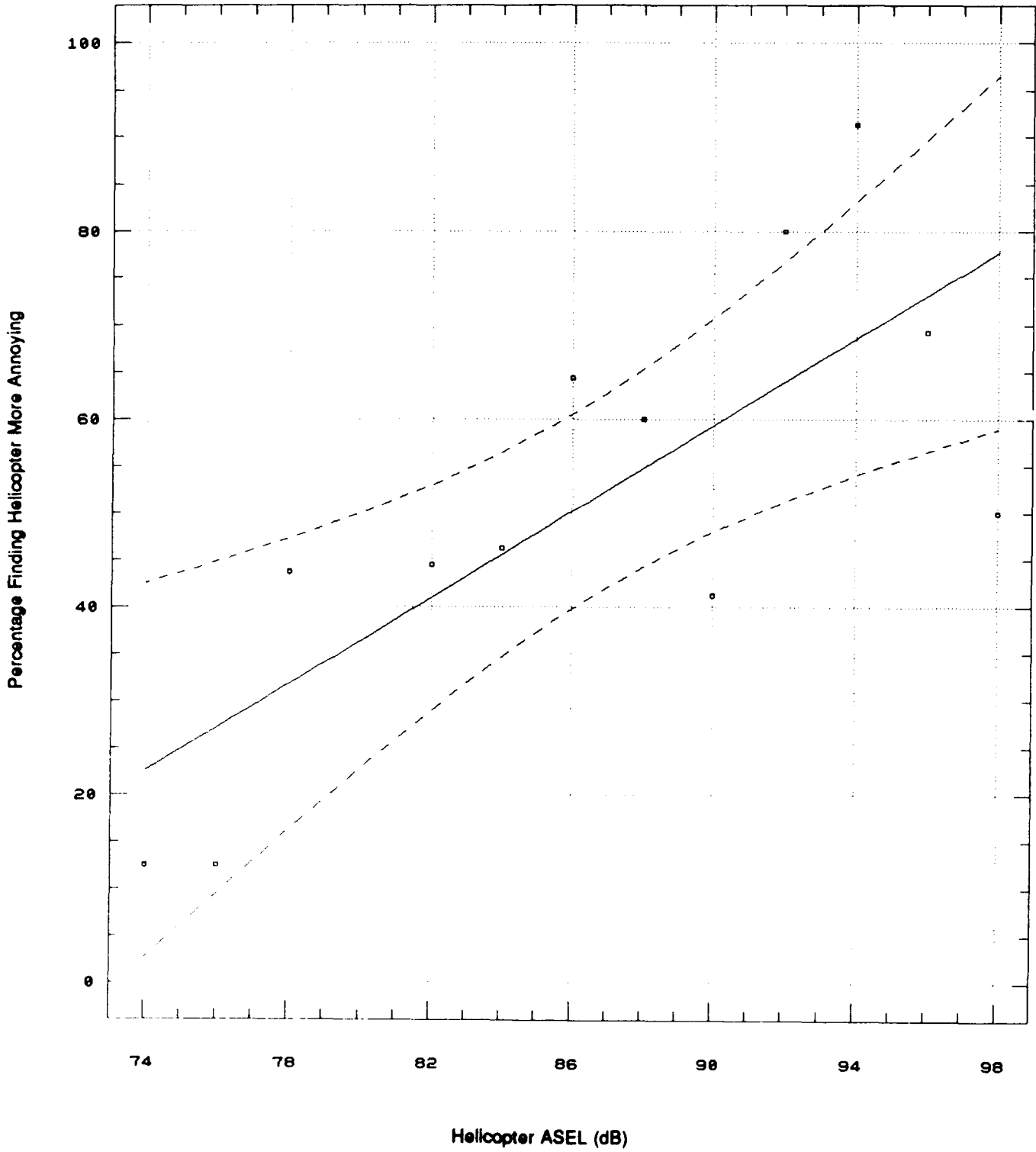
Regression of AW1W084.ANNOY on AH1W084.SEL

AHIW Outdoor
84 dB Control SEL



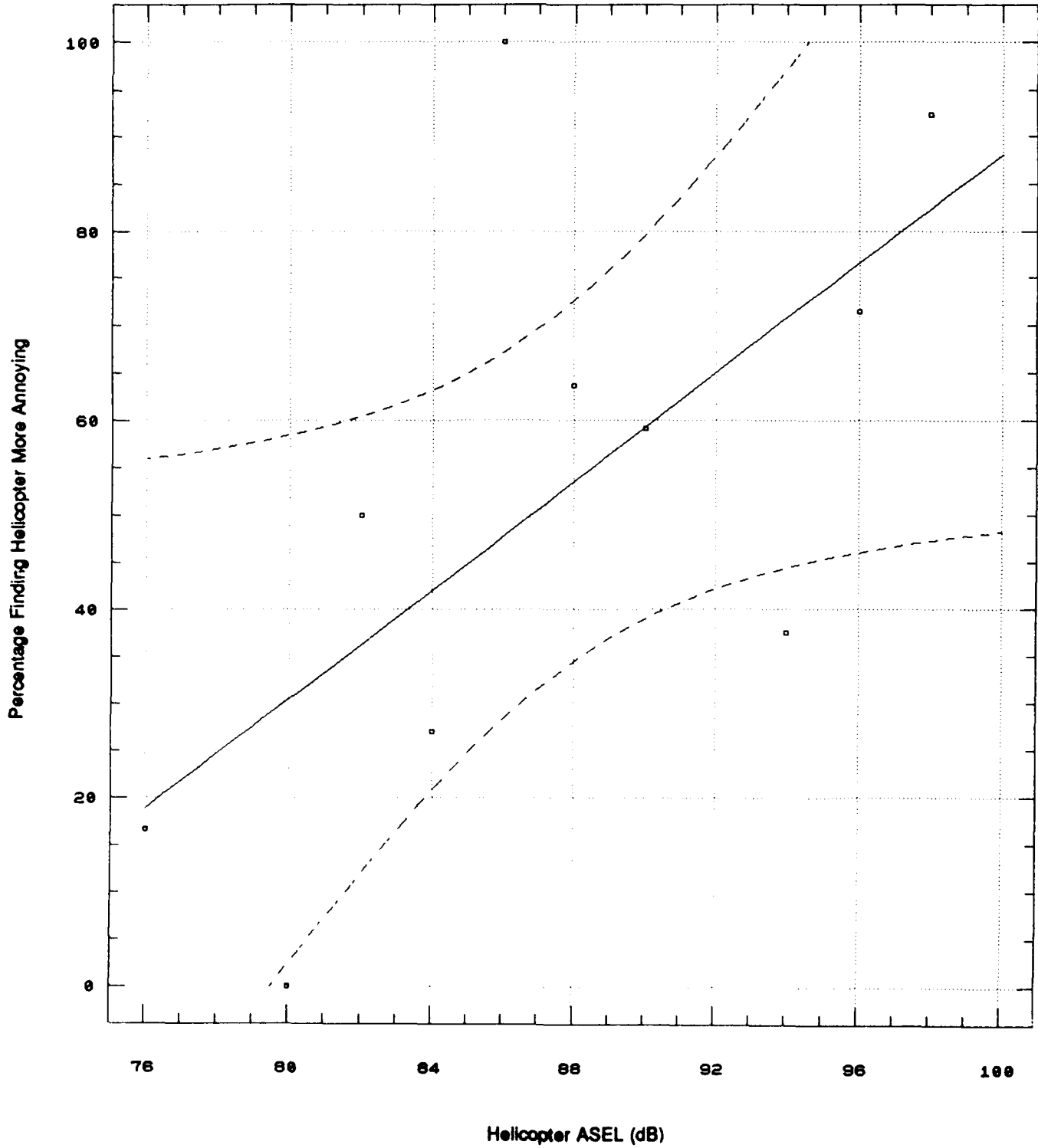
Regression of AW1W088.ANNOY on AH1W088.SEL

AHIW Outdoor
88 dB Control SEL



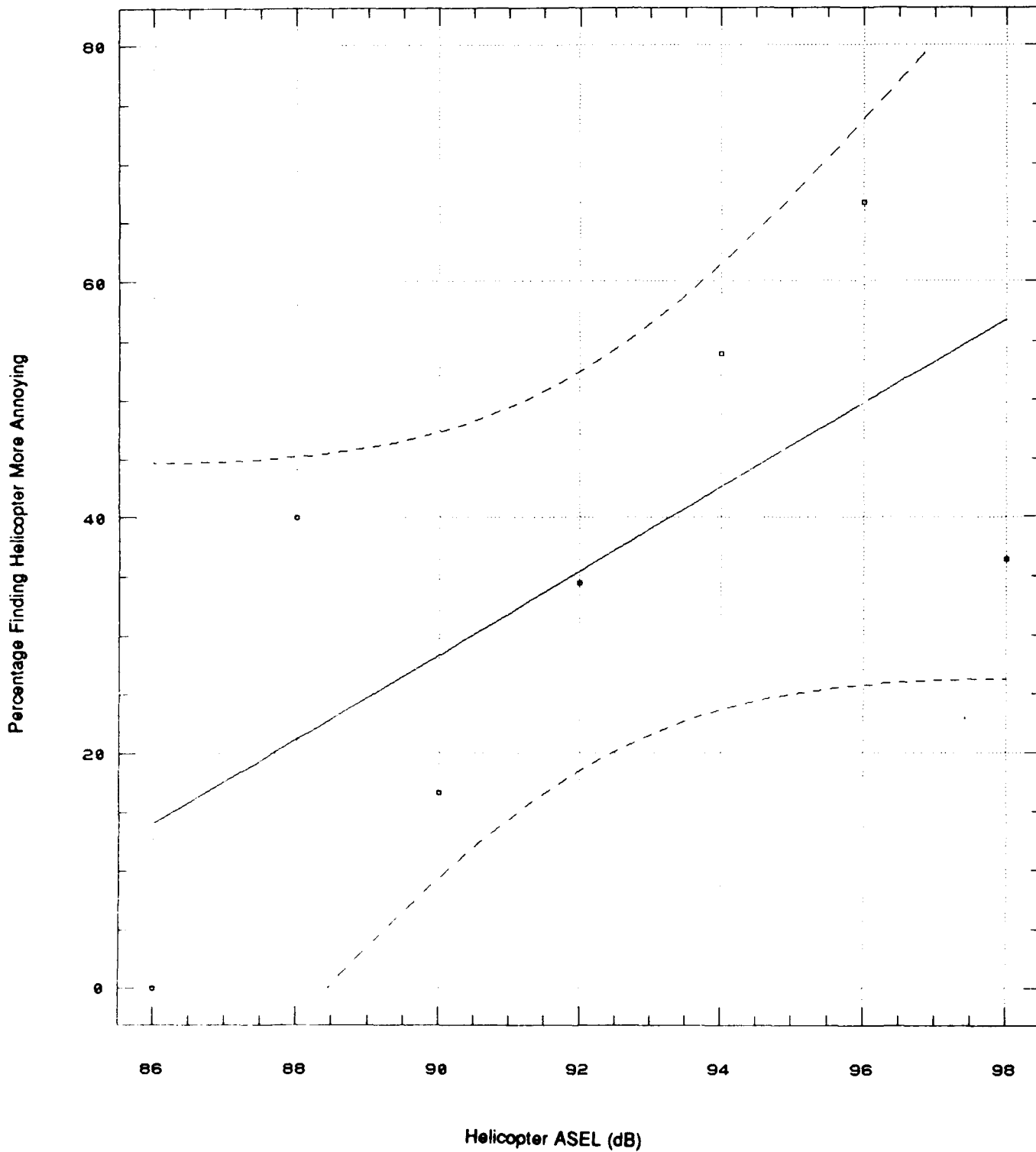
Regression of AW1WO92.ANNOY on AH1WO92.SEL

AHIW Outdoor
92 dB Control SEL



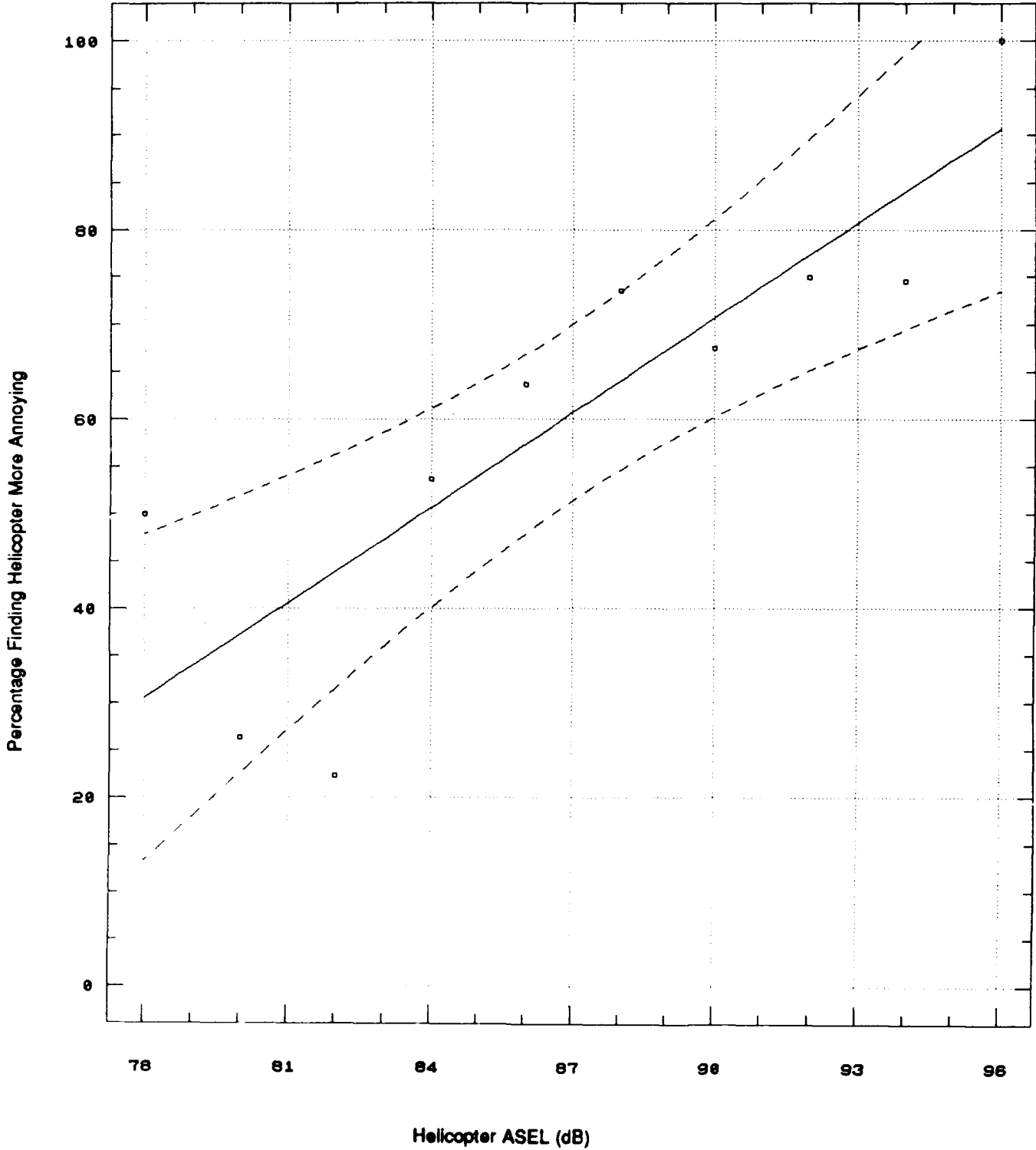
Regression of AW1WO100.ANNOY on AH1WO100.SEL

AHIW Outdoor
100 dB Control SEL



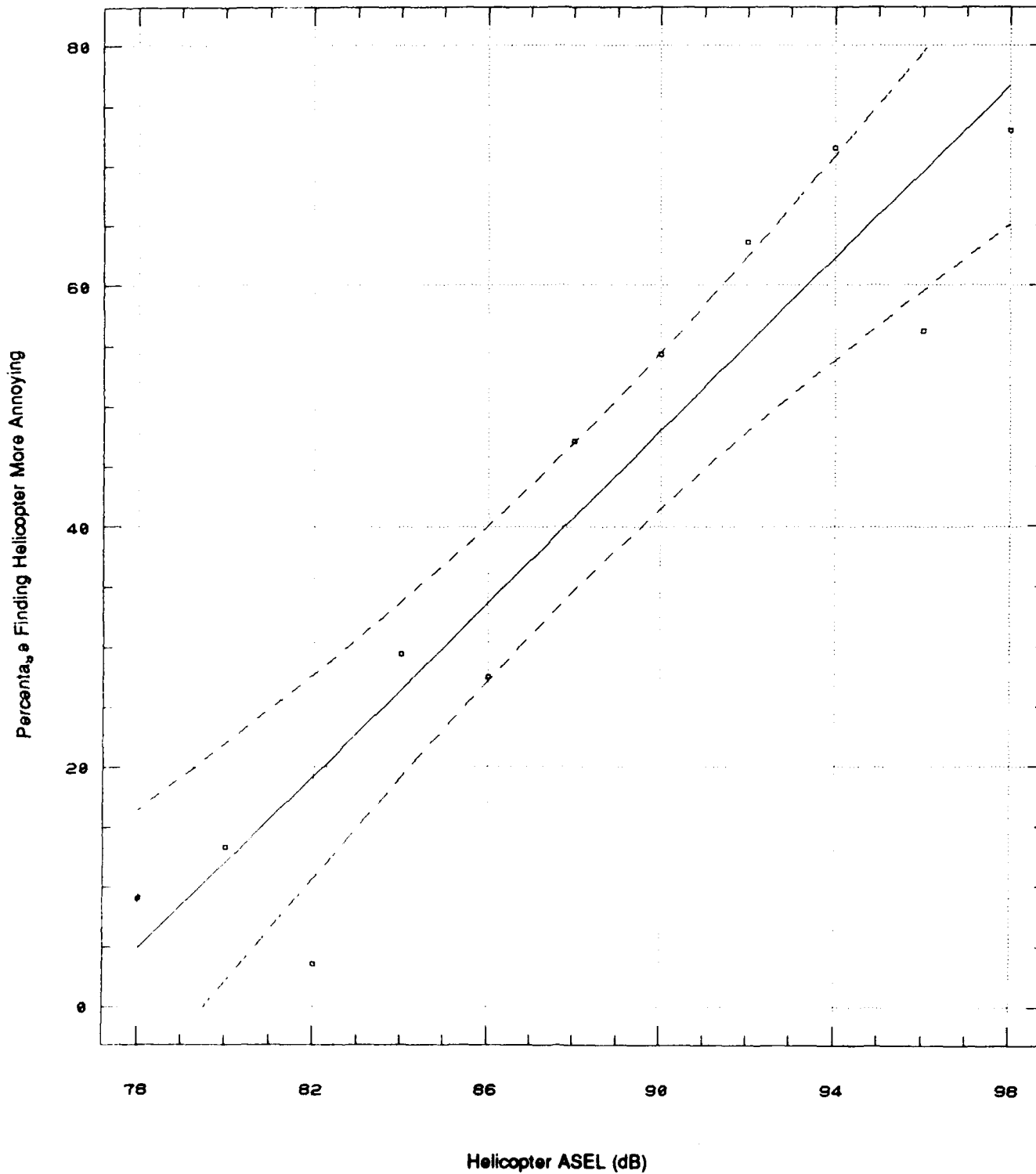
Regression of OUTCH88.ANNOY on OUTCH88.SEL

ALL CH Helicopters Outdoor
88 dB Control SEL



Regression of OUTCH92.ANNOY on OUTCH92.SEL

ALL CH Helicopters Outdoor
92 dB Control SEL



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