

INSTALLATION RESTORATION PROGRAM

(1)

**STEWART AIR NATIONAL GUARD BASE
NEWBURGH, NEW YORK**

SITE INSPECTION REPORT

VOLUME II - APPENDICES

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SITE INSPECTION REPORT
INSTALLATION RESTORATION PROGRAM

VOLUME II

STEWART AIR NATIONAL GUARD BASE
NEWBURGH, NEW YORK

Prepared for:

HAZWRAP SUPPORT CONTRACTOR OFFICE
OAK RIDGE, TENNESSEE 37831

Operated by:

MARTIN MARIETTA ENERGY SYSTEMS, INC.
FOR THE
U.S. DEPARTMENT OF ENERGY

Prepared by:

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PORTLAND, MAINE

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SITE INSPECTION
STEWART AIR NATIONAL GUARD BASE

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APPENDIX A-1 MAGNETIC (TOTAL FIELD) MEASUREMENTS

INTRODUCTION

The magnetic method is a versatile, relatively inexpensive, geophysical exploration technique. Magnetic data can be acquired on land or water, or in the air. Aeromagnetic surveys and deep water marine studies are commonly used as a reconnaissance tool for evaluating hydrocarbon prospects. Land-based or coastal water marine magnetic surveys are usually done for evaluating shallow geologic structures (e.g., shallow mineral deposits) in detail. Such surveys have also been used successfully in locating manmade features; for example, in archeological prospecting.

More recently, the focus of national attention on the hazardous waste problem has prompted routine use of magnetometers for locating repositories of buried (drummed) wastes. Locating and quantifying these materials is essential to any remediation effort, and magnetometer surveys can provide an extra measure of safety to those personnel involved in the clean-up activities.

EARTH MAGNETISM

Although the origin of the earth's magnetic field is not well understood, it is known that the earth behaves magnetically, as if a large bar magnet were located near its center. The axis of this "magnet" is oriented at a small angle, which produces the differences between "true" north and "magnetic" north. The angle is called the declination. The lines of magnetic force are nearly horizontal at the equator and nearly vertical at the poles. The angle between these lines of force and horizontal at any point on the earth's surface is known as the inclination.

The strength of the magnetic field also varies over the surface of the earth, and is stronger at the poles than at the equator. The strength of the field is approximately 60,000 gammas at the poles and 30,000 gammas at the equator (where 1 gamma = 0.00001 Gauss).

The earth's magnetic field (sometimes referred to as its "ambient" field) is modified locally by both naturally occurring and manmade magnetic materials. Two types of magnetization contribute to this: induced and remanent. Induced magnetization refers to the ability of a material to act as a magnet itself, thereby enhancing the ambient field. The more the ambient field is enhanced by a material, the greater is the "magnetic susceptibility" for that material.

Remanent or permanent magnetization often predominates over induced magnetization in igneous rocks and metals. (Remanent refers to rocks, whereas permanent refers to metals). Remanent or permanent magnetization is produced in materials that have been heated above the Curie point, allowing magnetic minerals to align with the earth's ambient field before cooling. The remanent field direction is not, in general, parallel to the earth's present field. It may, in fact, act in the opposite direction. The remanent field combines vectorially with the ambient and induced field components, and any quantitative

interpretation of magnetic data should consider this if such information is available.

INSTRUMENTATION

Although many types of magnetometers are available, by far the most widely used is the "proton precession" type. This device utilizes the precession of spinning protons of hydrogen atoms in a sample of hydrogen-rich fluid (i.e., kerosene, alcohol, or water) to measure the total magnetic field intensity.

Protons spinning in an atomic nucleus behave like tiny magnetic dipoles which can be aligned (polarized) by an external magnetic field. The protons are initially aligned parallel to the earth's field. A second, much stronger magnetic field is produced approximately perpendicular to the earth's field by introducing electric current through a coil of wire. The protons become temporarily aligned with this stronger field. When this stronger field is removed, the protons tend to realign themselves with the earth's field, causing them to precess about this direction at a frequency of about 2,000 Hz. The precessing protons will generate a small electric signal in the same coil used to polarize them, with a frequency proportional to the total magnetic field intensity and independent of the coil orientation. By measuring the signal frequency, one can obtain the absolute value of the total earth's field intensity to an accuracy of 1 gamma or better. The total magnetic field value measured by the proton precession magnetometer is the net vector sum of the ambient earth's field and any local induced and/or remanent (permanent) perturbations.

FIELD TECHNIQUES

In the field, the operator should avoid any source of high magnetic gradients (e.g., powerlines, buildings, or large iron or steel objects). The operator should also avoid carrying any unnecessary metal articles. Magnetic stations are established at intervals that reflect the nature of the survey and the magnetic gradients encountered.

At hazardous waste sites, a typical "rough" reconnaissance grid might start out at a 25-foot interval, and would be closed down to 3 or 5 feet in areas where fine detail is desired. Base station readings should be taken frequently (every 30 to 60 minutes) to provide a check on diurnal variations and magnetic storms that may occur during a survey. Typically, diurnal variations will not exceed a few tens of gammas, but magnetic storms may produce changes in the earth's field of thousands of gammas in a short period of time (the order of hours). If survey requirements dictate, it may be prudent to establish a continuously recording magnetic base station to account for diurnal variations. If a magnetic storm occurs, survey operations should cease until the storm is over.

INTERPRETATION

For typical manmade iron or steel objects, one may quantify estimates for the approximate depth of burial and the amount of metal which produces an observed

magnetic perturbation (or anomaly). The size of the anomaly (T) can be expressed as:

$$T = (M)/(r)^n$$

where "M" is the magnetic moment of the source, "r" is the depth to the source, and "n" is a measure of the rate of decay with distance ($n = 3$ for a dipole source and 2 for a monopole source).

Assuming a dipole source, the weight of a metal object (in pounds) can be expressed by the following relation:

$$\text{Weight} = ((T)*(r)^3)/(M)$$

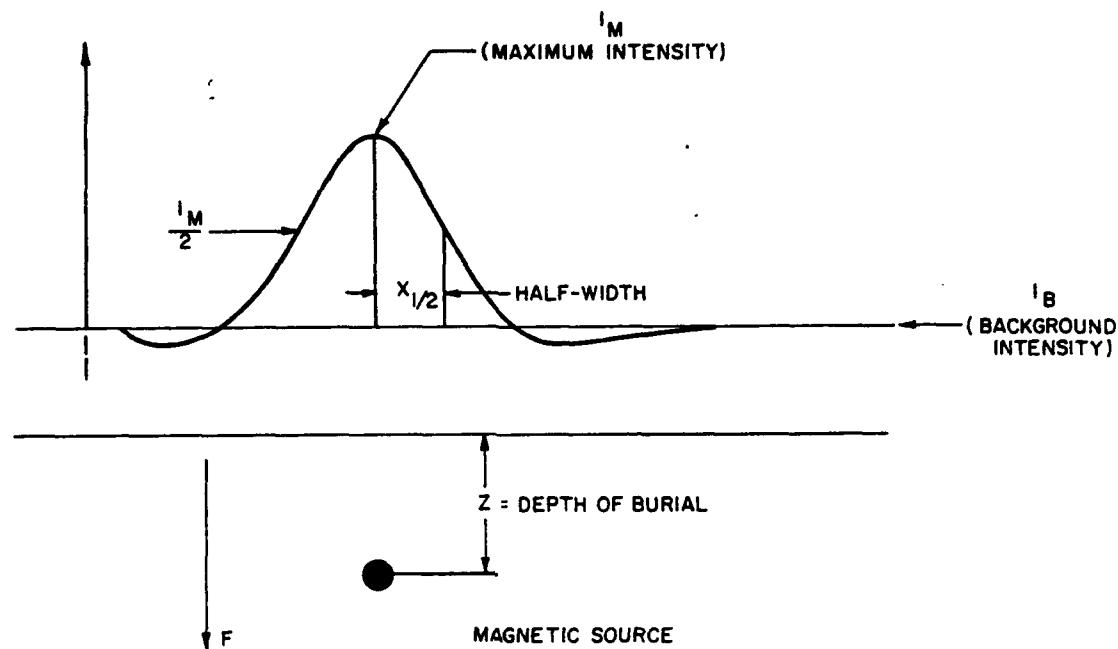
where "M" is the magnetic moment per pound of iron and varies from approximately 175 to 1750, "r" is the depth in feet (below the sensor), and "T" is the anomaly amplitude in gammas.

The depth, "r", of a magnetic source can be estimated by a number of techniques, but perhaps the simplest is by the "half-width" rule. This states that for simple anomaly sources, the depth to the center of the anomaly is equal to the "half-width" of the anomaly. The half-width is the horizontal distance between the maximum value of the anomaly and the point at which the value is one-half the maximum value (Figure A-1).

A further refinement in magnetic studies is permitted with the addition of vertical gradient measurements. This involves the simultaneous acquisition by two sensors of two values of the total field. The sensors are mounted on a staff that is held vertically during a measurement. A known distance (commonly one-half or one meter) separates the sensors on the staff. Vertical gradient measurements tend to be more sensitive to the presence of near surface metal objects than total field values alone. There are commercially available magnetometers that record field data in an internal memory which can be "dumped" onto a personal computer at the completion of field activities. These instruments can record the total field value, the vertical gradient, the time and date of the measurement, and the station location (input by the user), as well as a number of parameters which permit an evaluation of data quality.

The vertical gradient data obtained during the present study are presented as Figures A-2 through A-19. The reader is referred to the main text (Section 5.0) for a discussion of the interpretation and results of these data.

DEPTH CALCULATION/METAL QUANTITY
FOR TOTAL FIELD MEASUREMENTS:



T = MAGNETIC ANOMALY INTENSITY

= MAXIMUM ANOMALY INTENSITY MINUS BACKGROUND INTENSITY

$$= I_M - I_B$$

$$= \frac{M_{fps}}{r^3} = \frac{1.75 \times 10^2 \text{ to } 1.75 \times 10^3}{(1 \text{ to } 2) r^3}$$

where "M_{fps}" is the magnetic moment per pound of iron and "r" is the distance between the magnetometer sensor and the object (the depth of burial) "z" is equal to "r" minus the height of the sensor above the ground.

DEPTH CALCULATION FOR GRADIOMETER MEASUREMENTS

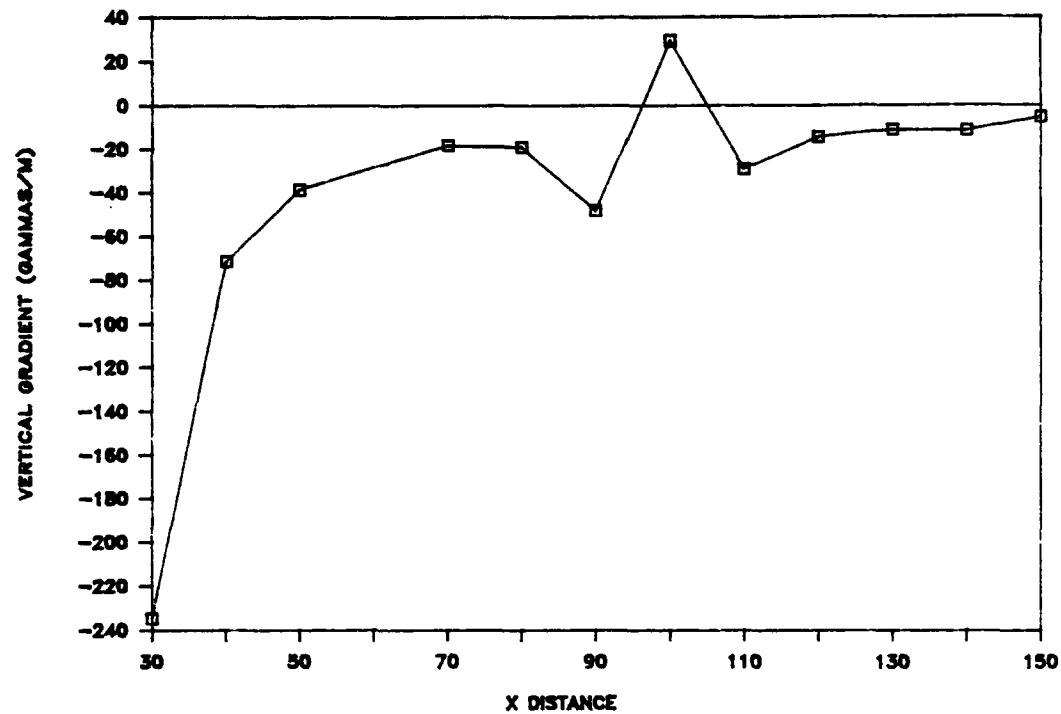
$$r = \frac{-nT}{\frac{dT}{dz}}$$

where "n" is the "falloff" factor and generally varies from 1 to 2, depending on the magnetic source; "r" is the separation between the midpoint between the two sensors and the object.

MAGNETOMETER DATA INTERPRETATION

FIGURE A-1

STEWART AFB - LINE 1+50



STEWART AFB - LINE 2+00

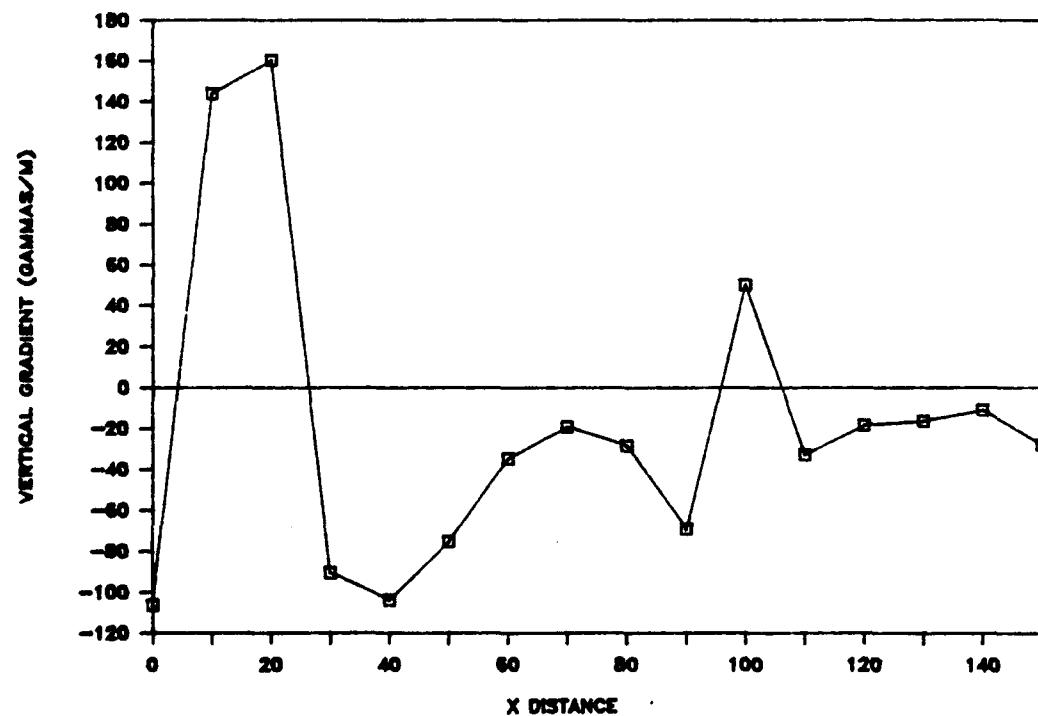
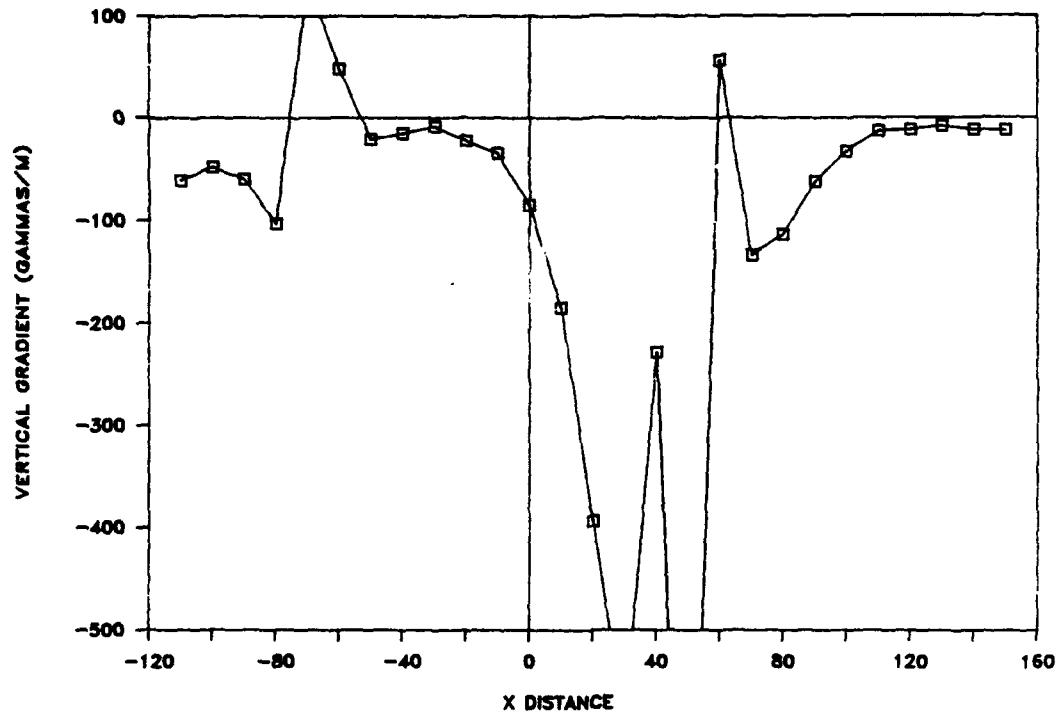


FIGURE A-2

STEWART AFB - LINE 2+50



STEWART AFB - LINE 3+00

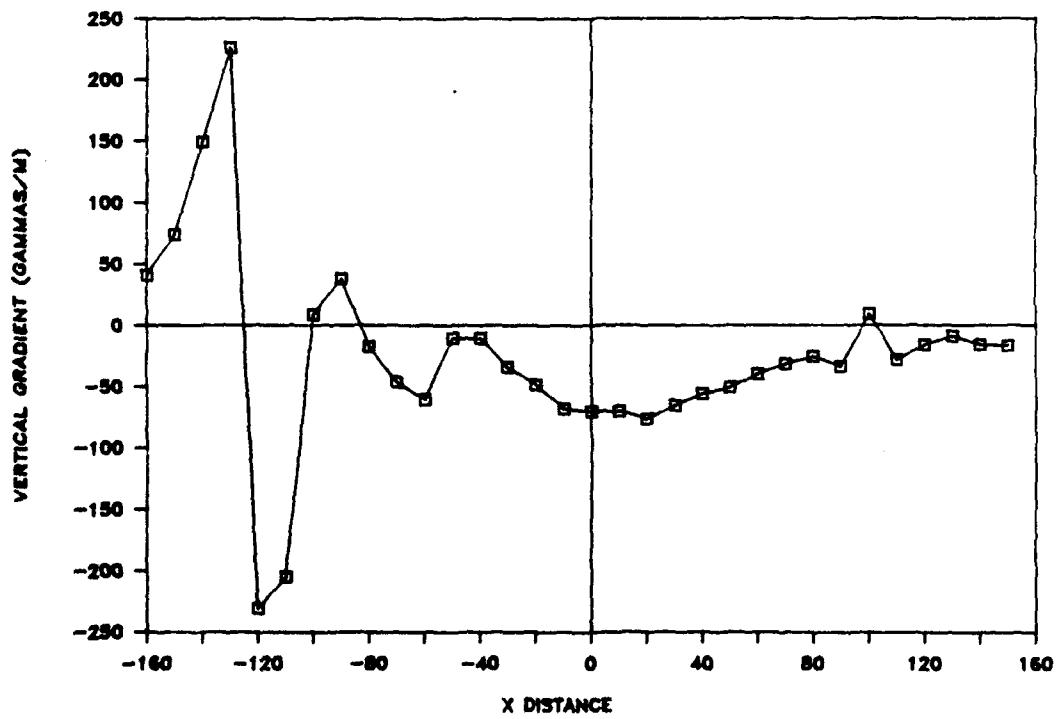
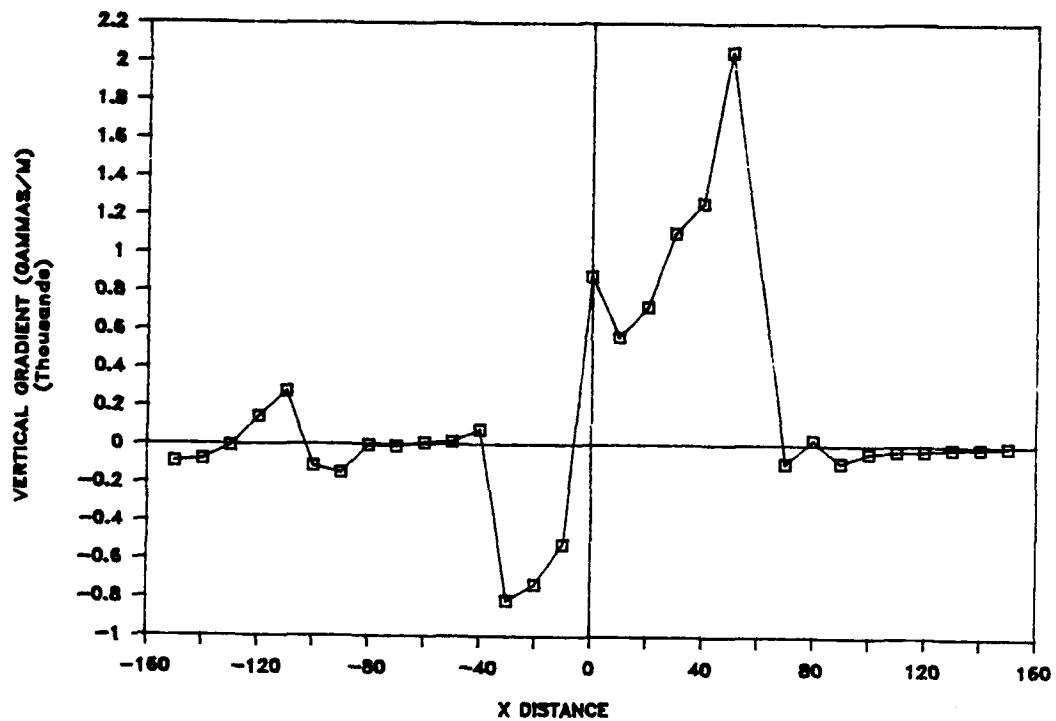


FIGURE A-3

STEWART AFB - LINE 3+50



STEWART AFB - LINE 4+00

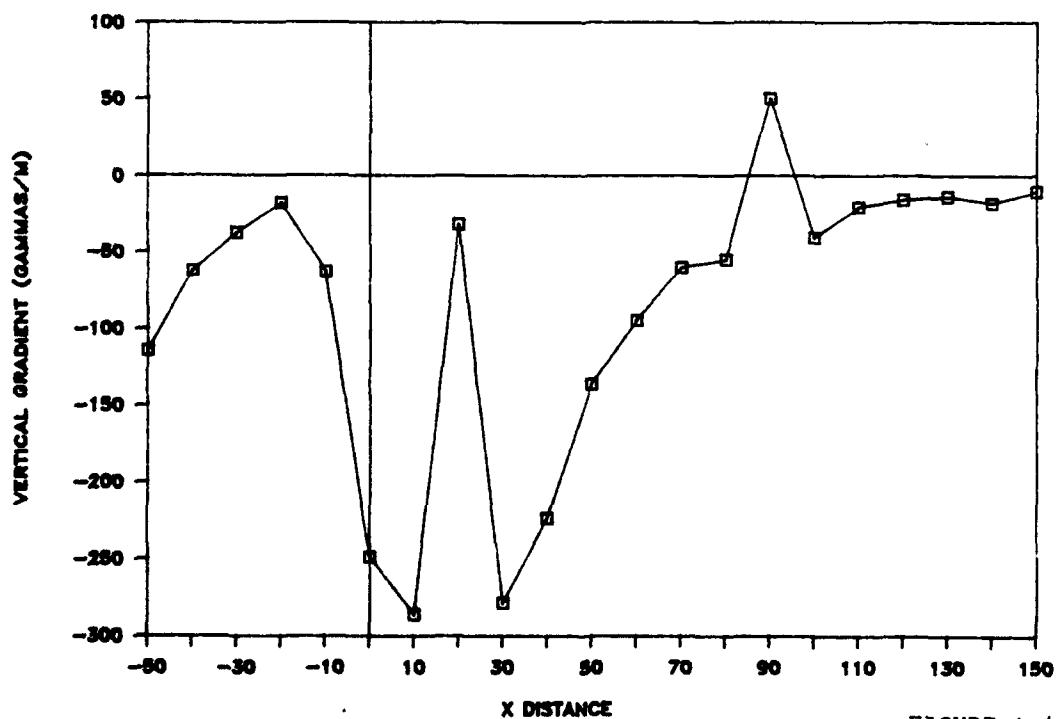
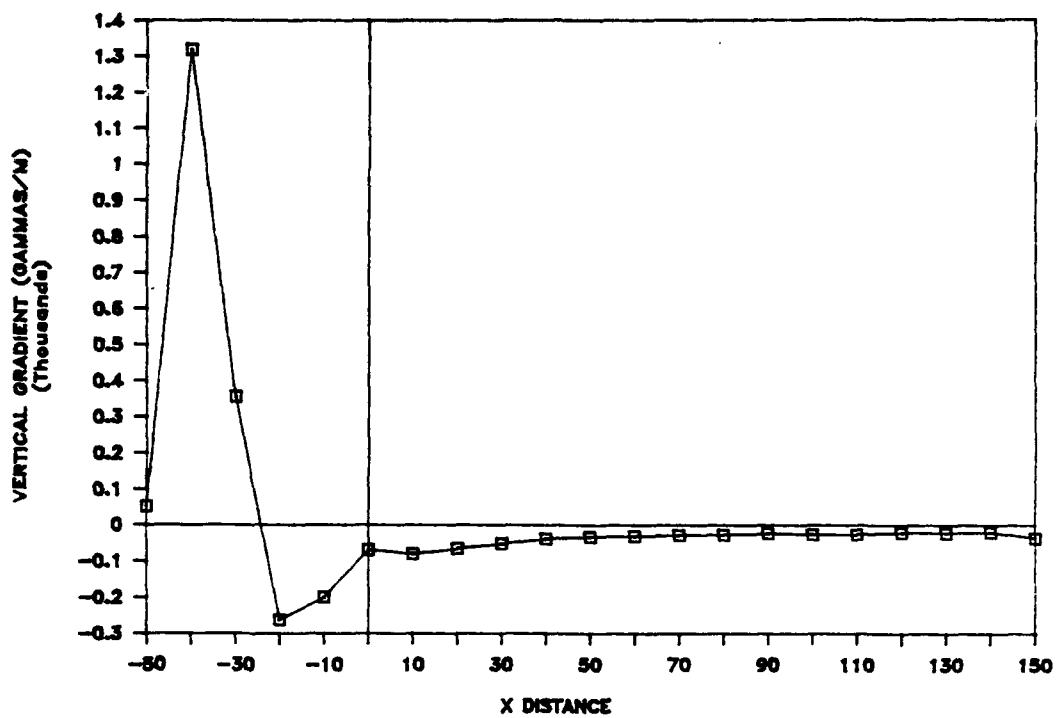


FIGURE A-4

STEWART AFB - LINE 5+00



STEWART AFB - LINE 6+35

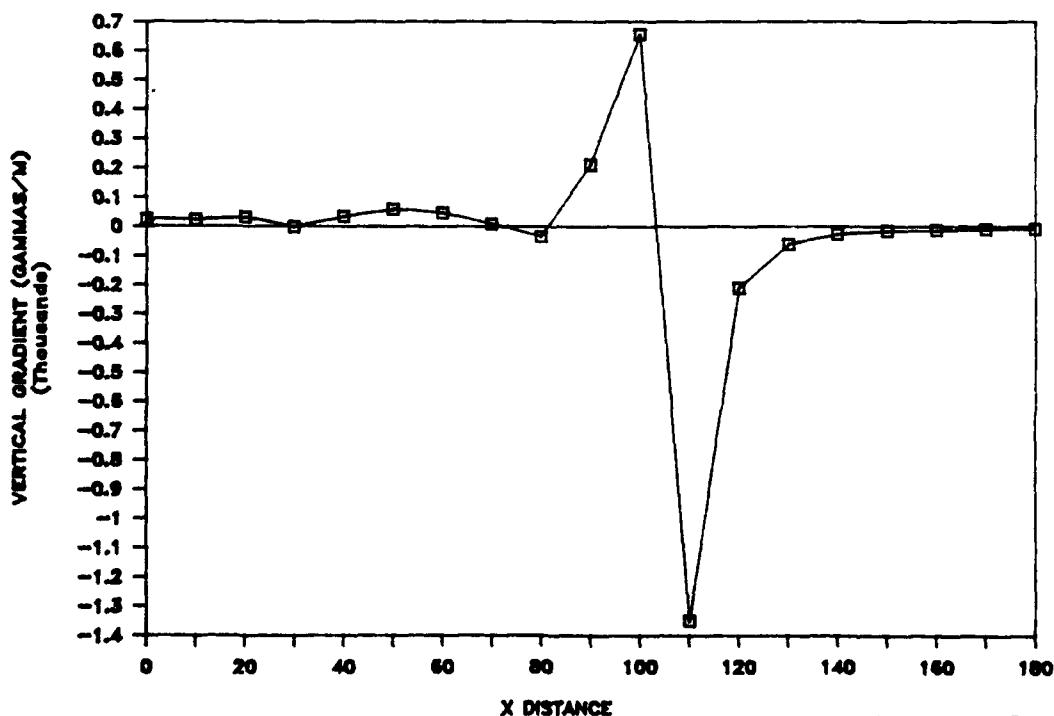


FIGURE A-5

STEWART AFB - LINE 6+65

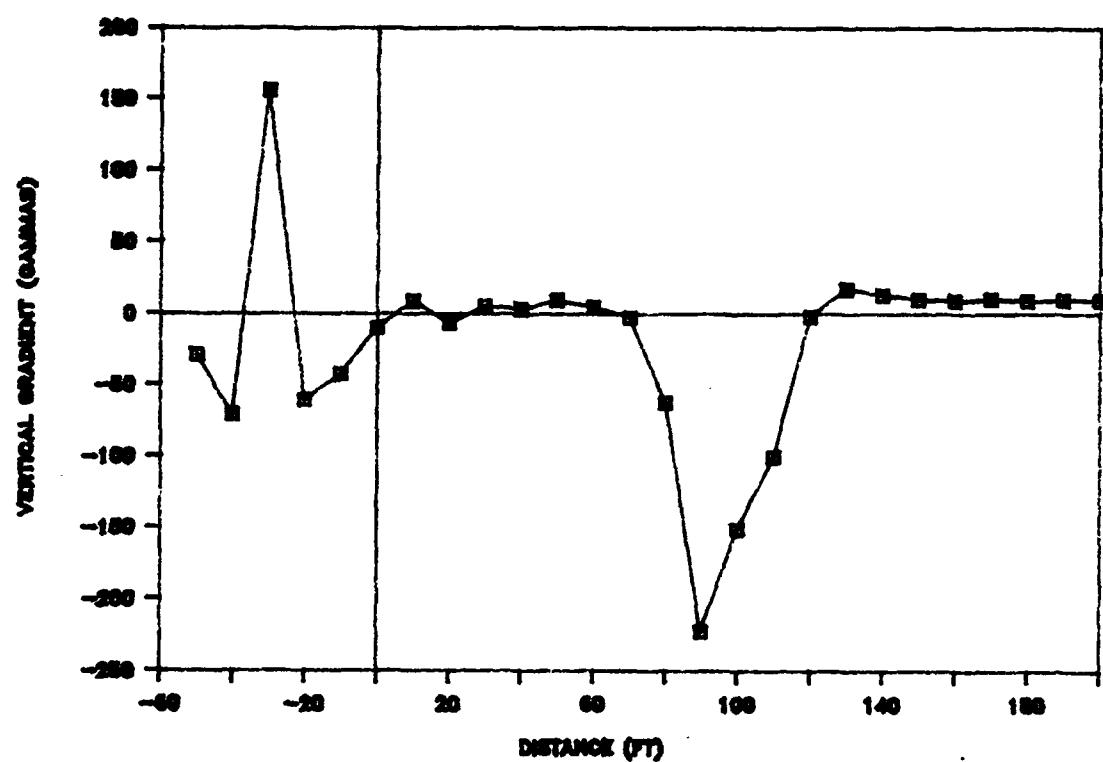
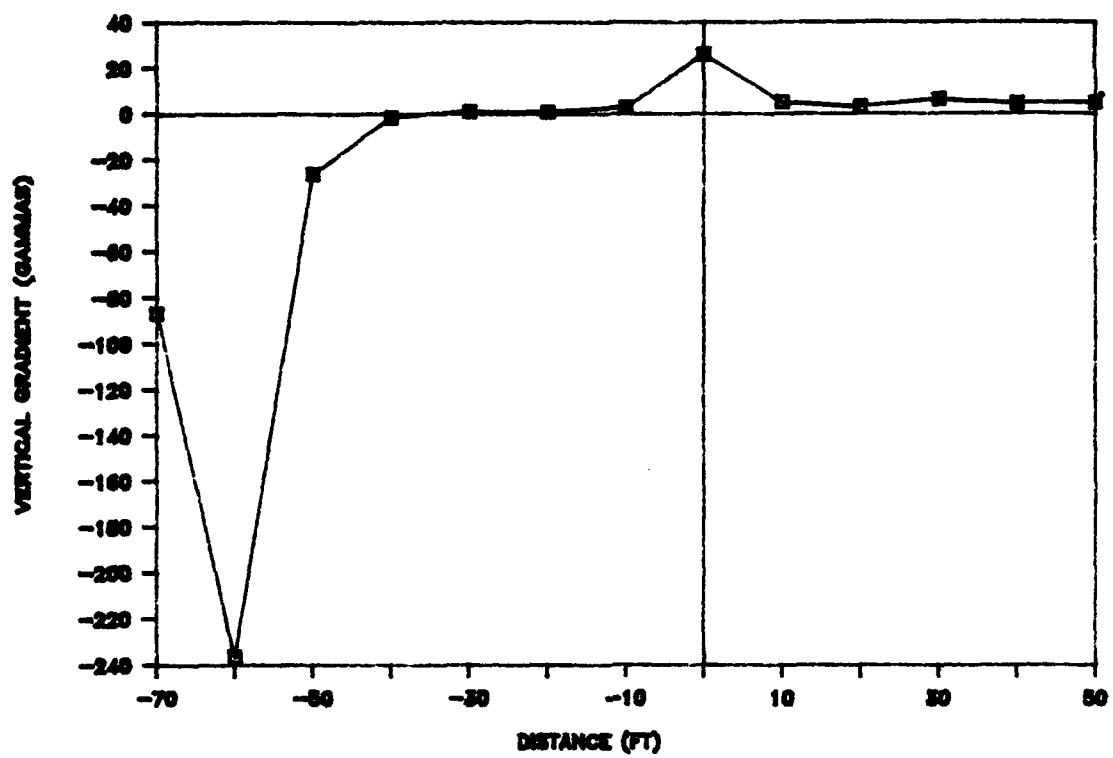


FIGURE A-6

STEWART AFB - LINE 9+00



STEWART AFB - LINE 9+50

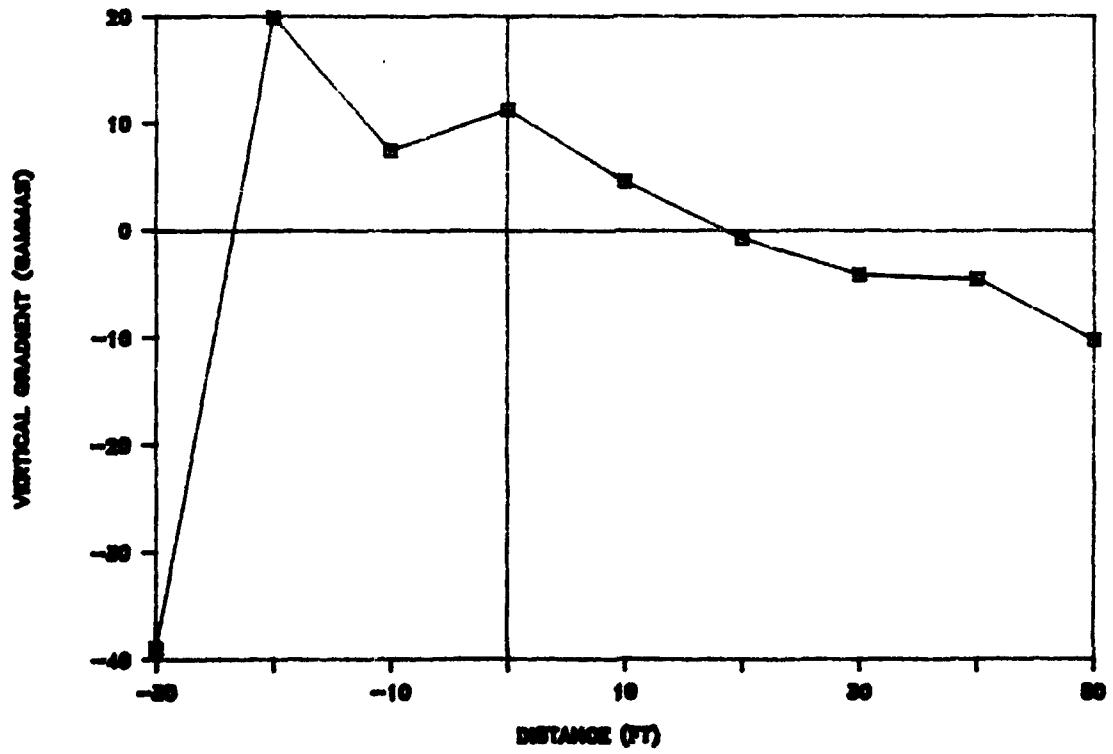
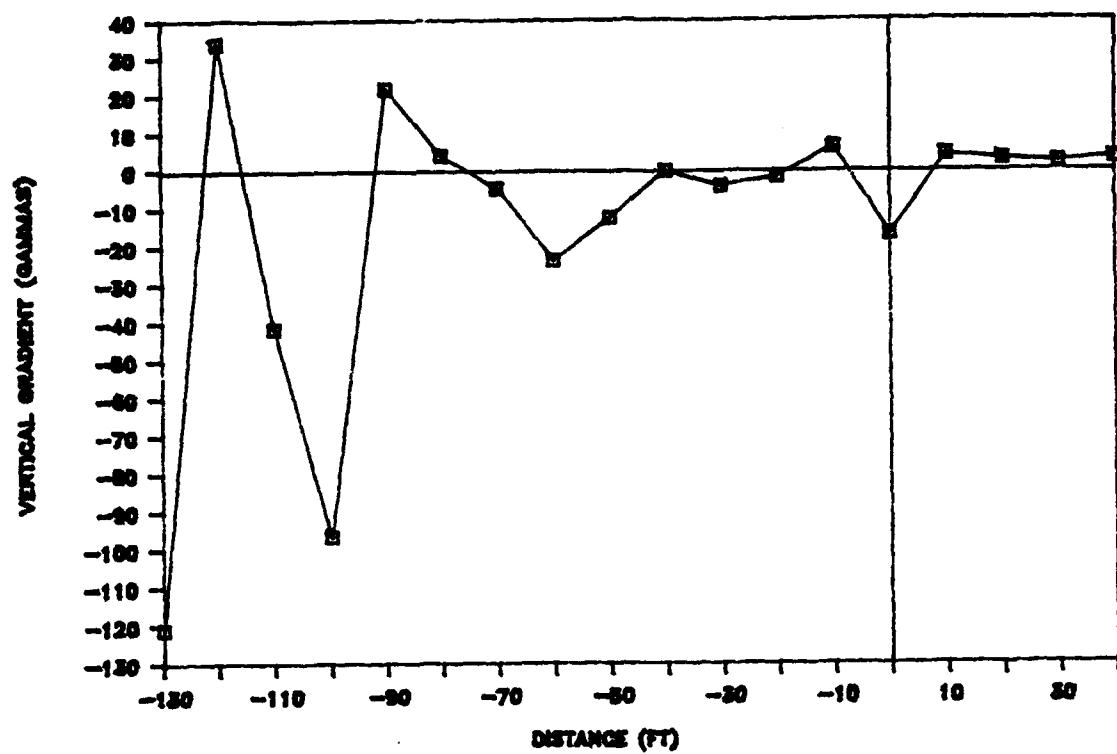


FIGURE A-7

STEWART AFB - LINE 10+50



STEWART AFB - LINE 19+50

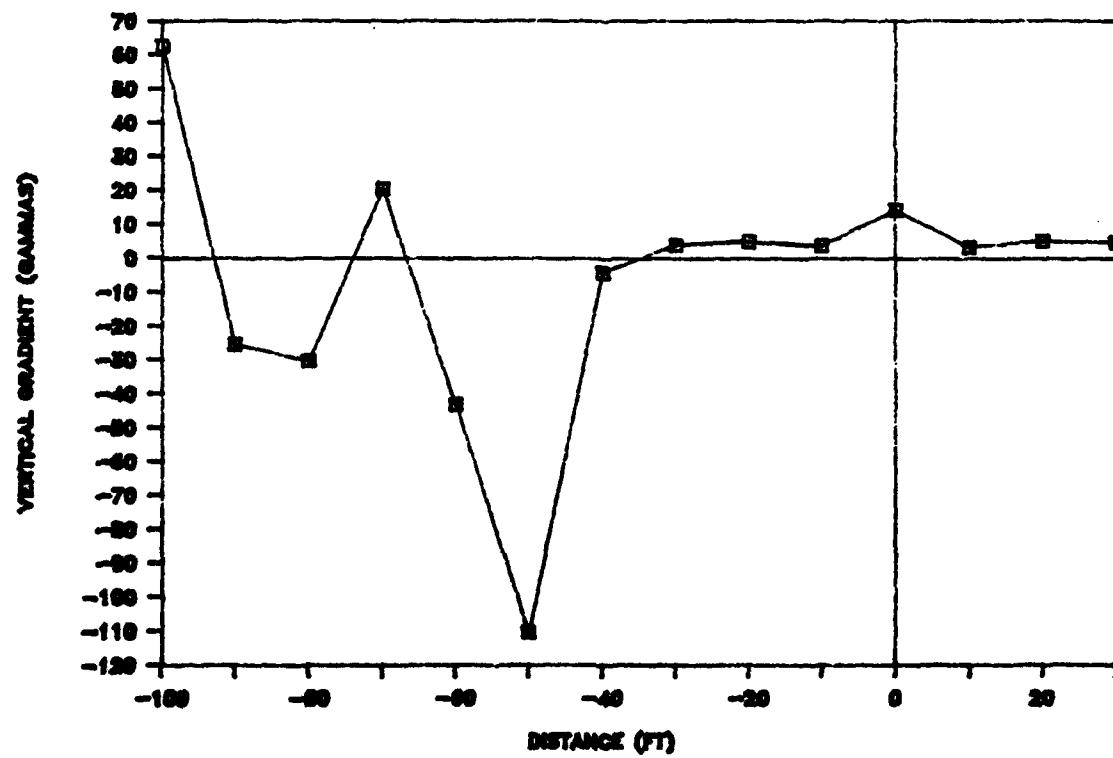
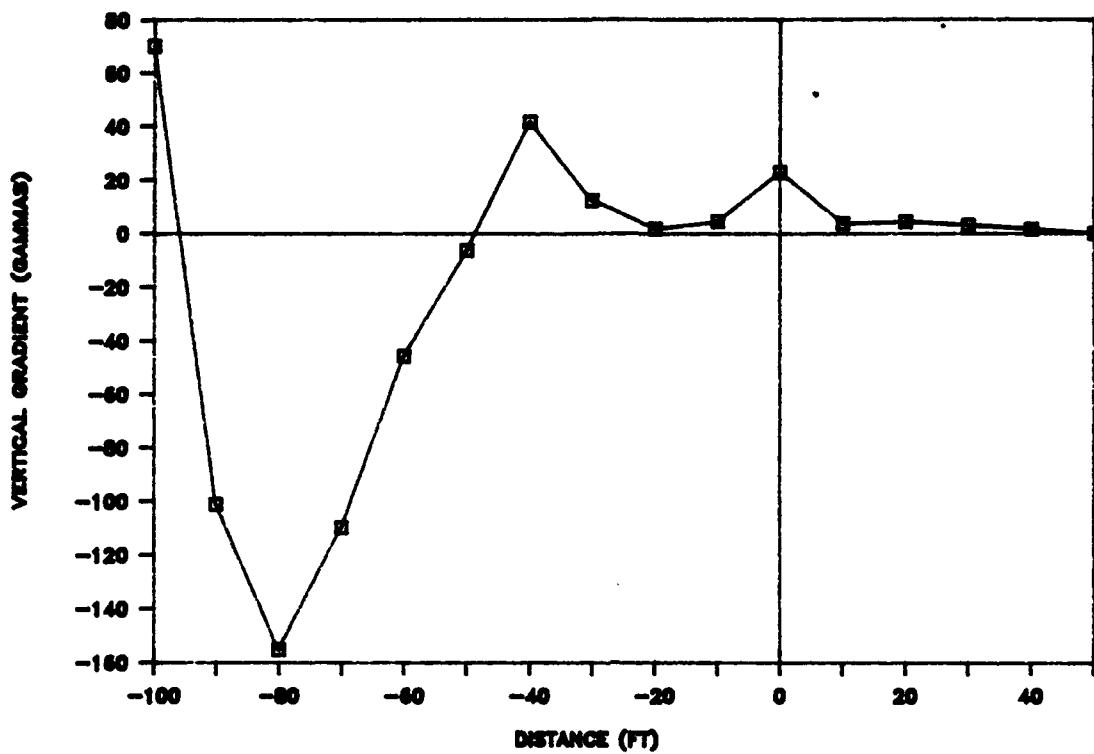


FIGURE A-8

STEWART AFB - LINE 20+00



STEWART AFB - LINE 20+50

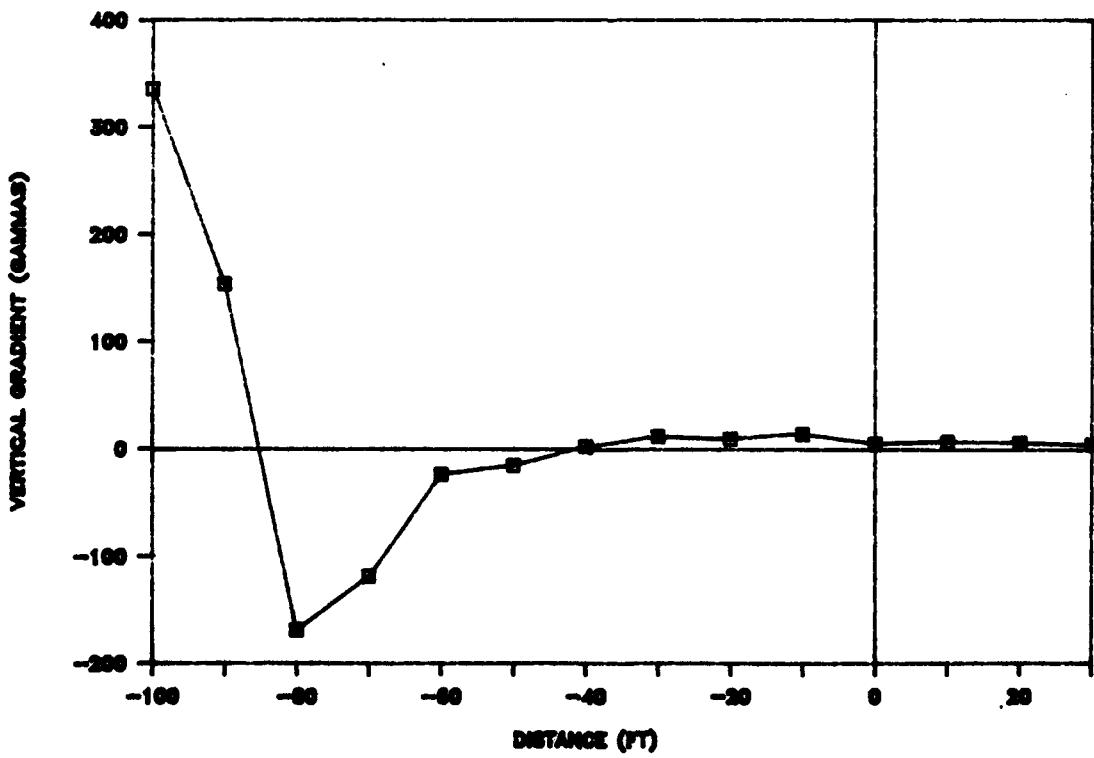


FIGURE A-9

STEWART AFB - LINE 21+00

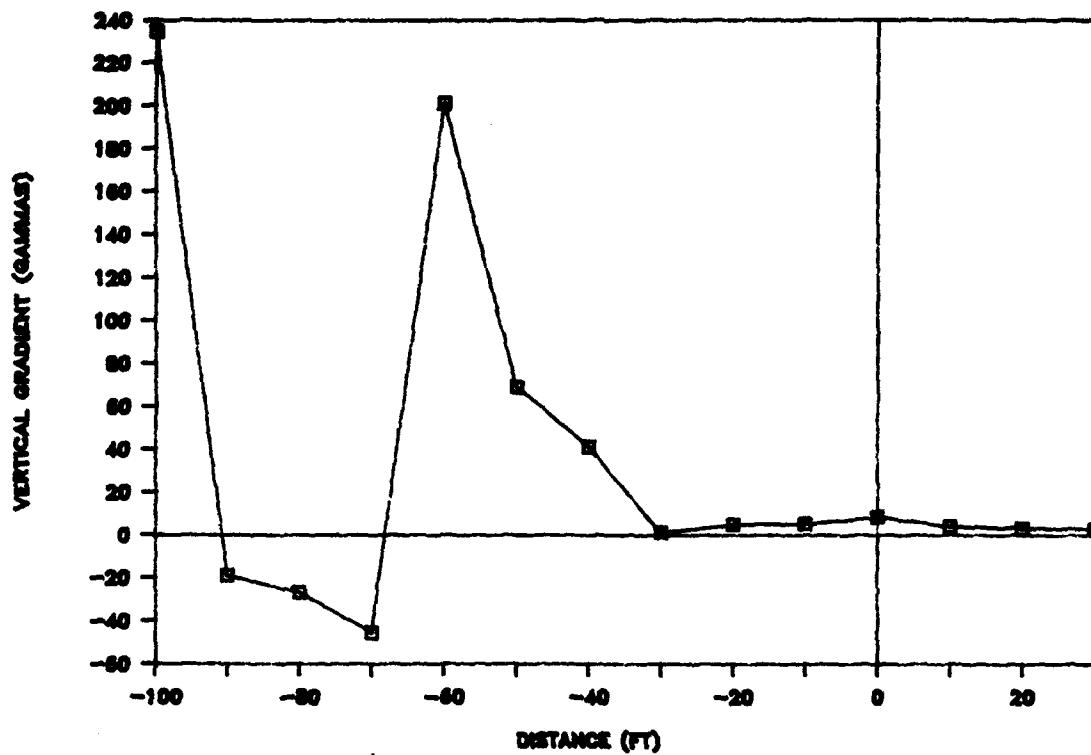
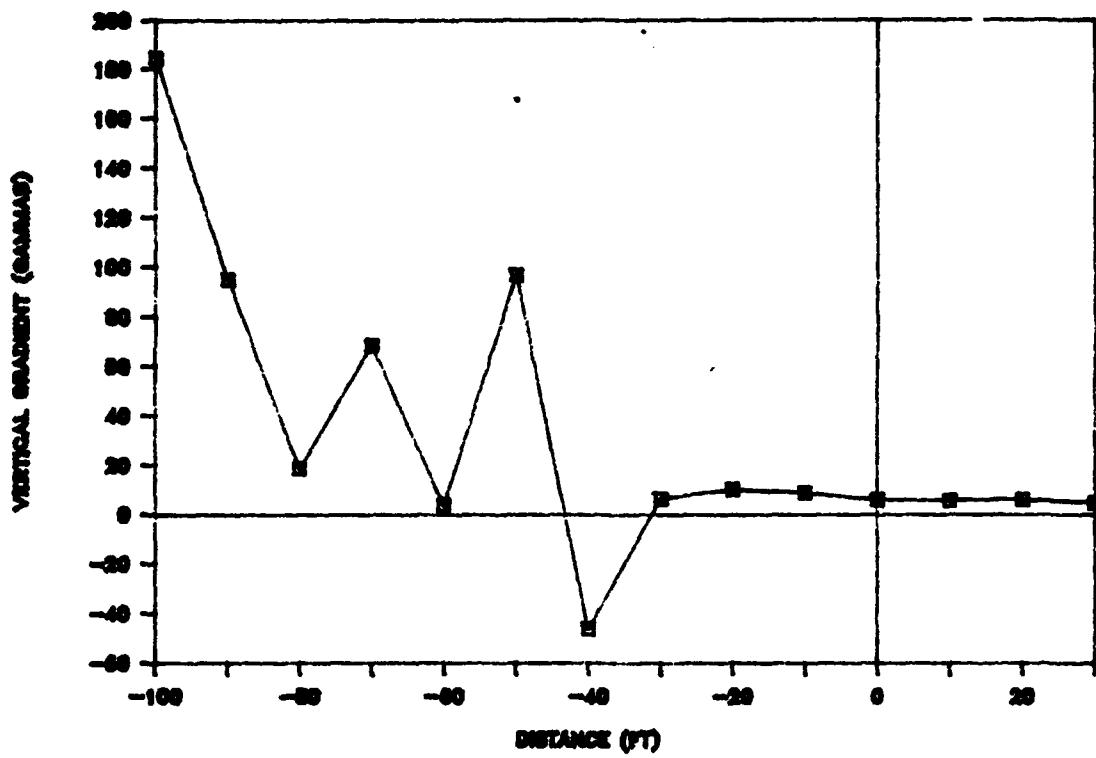


FIGURE A-10

STEWART AFB - LINE 21+50



STEWART AFB - LINE 22+00

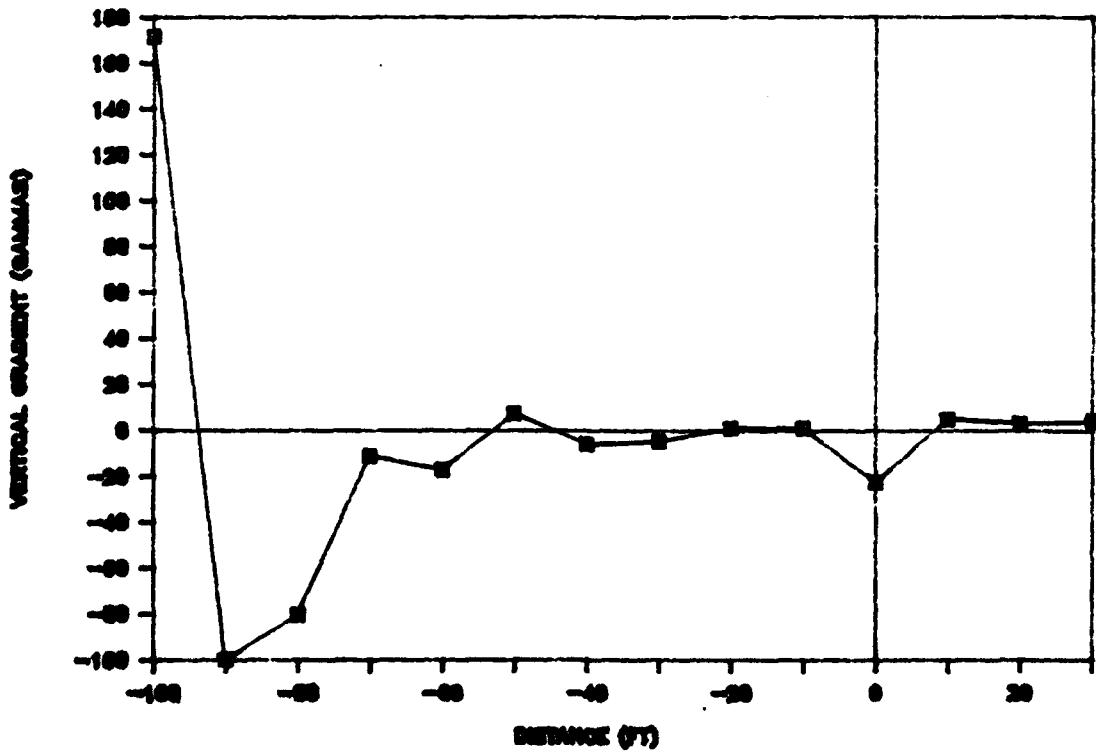
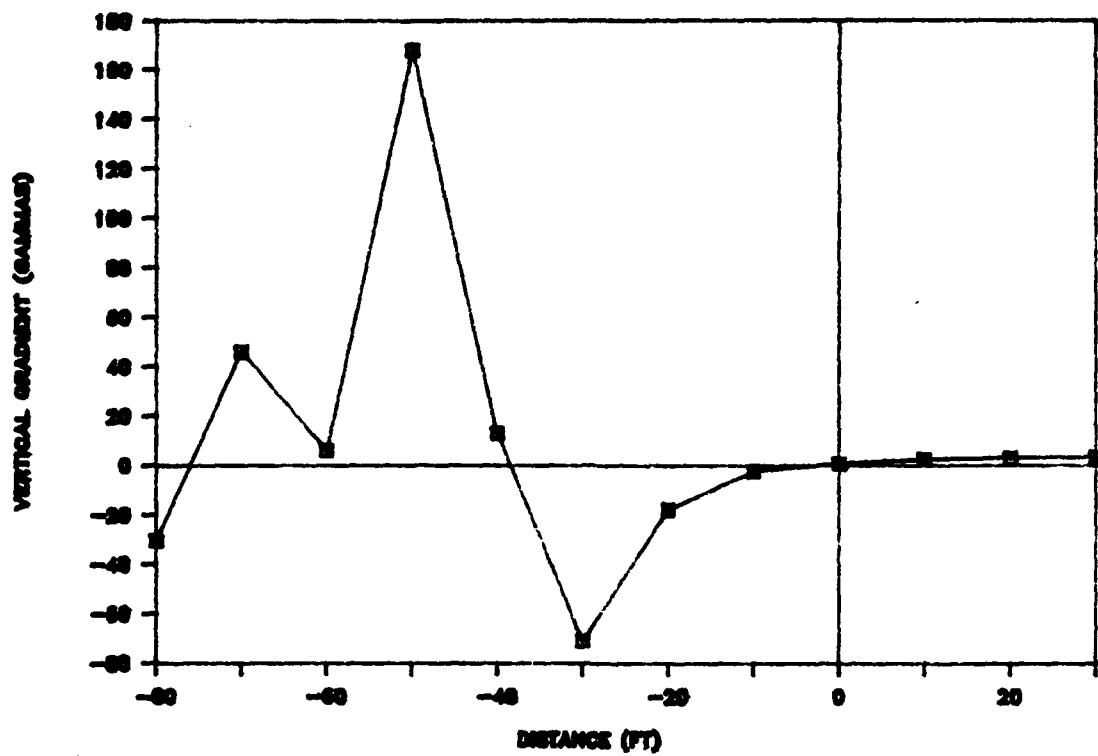


FIGURE A-11

STEWART AFB - LINE 22+50



STEWART AFB - LINE 23+00

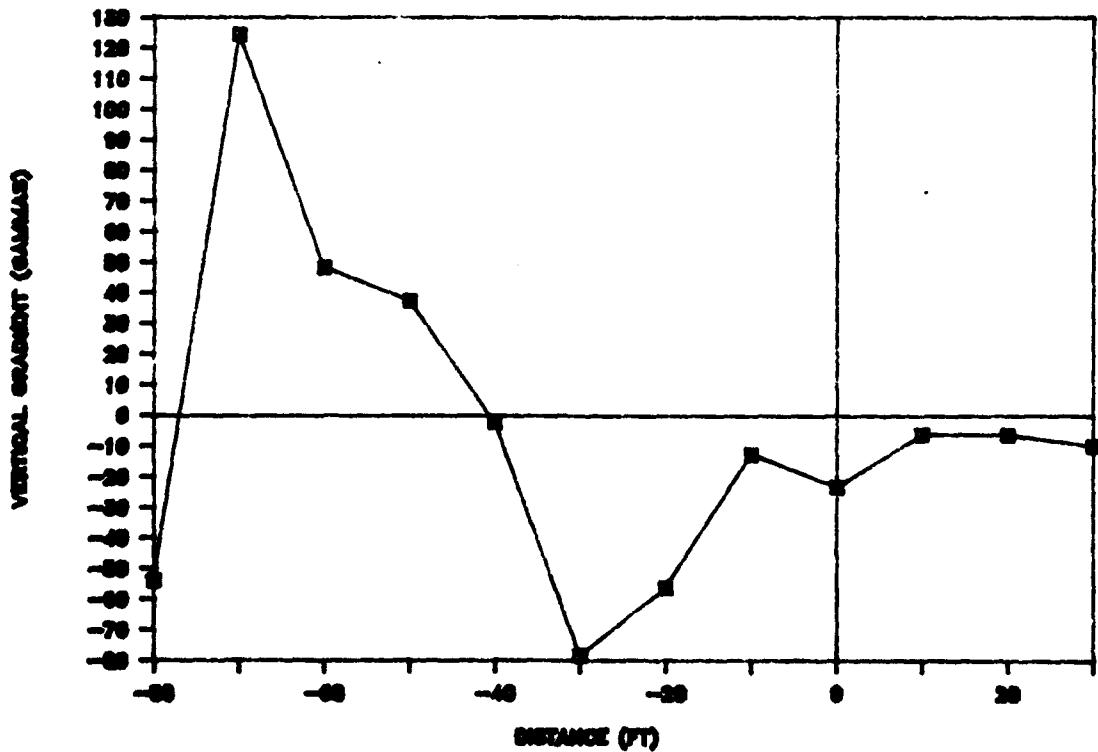
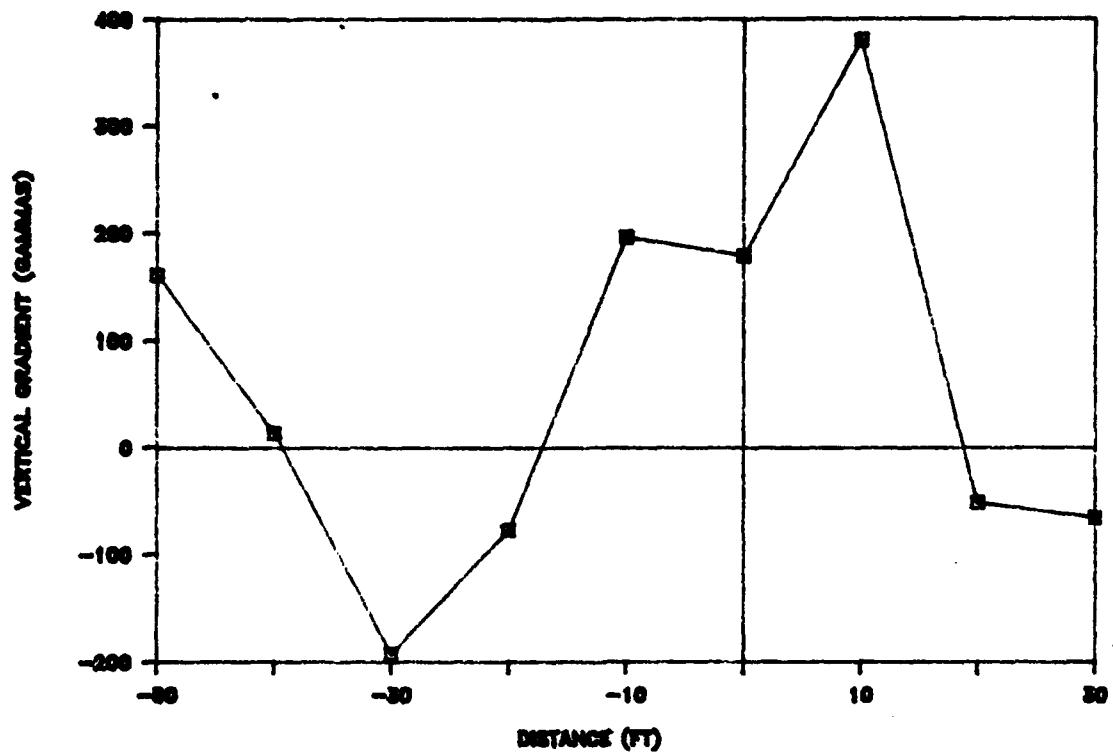


FIGURE A-12

STEWART AFB - LINE 23+50



STEWART AFB - LINE 24+00

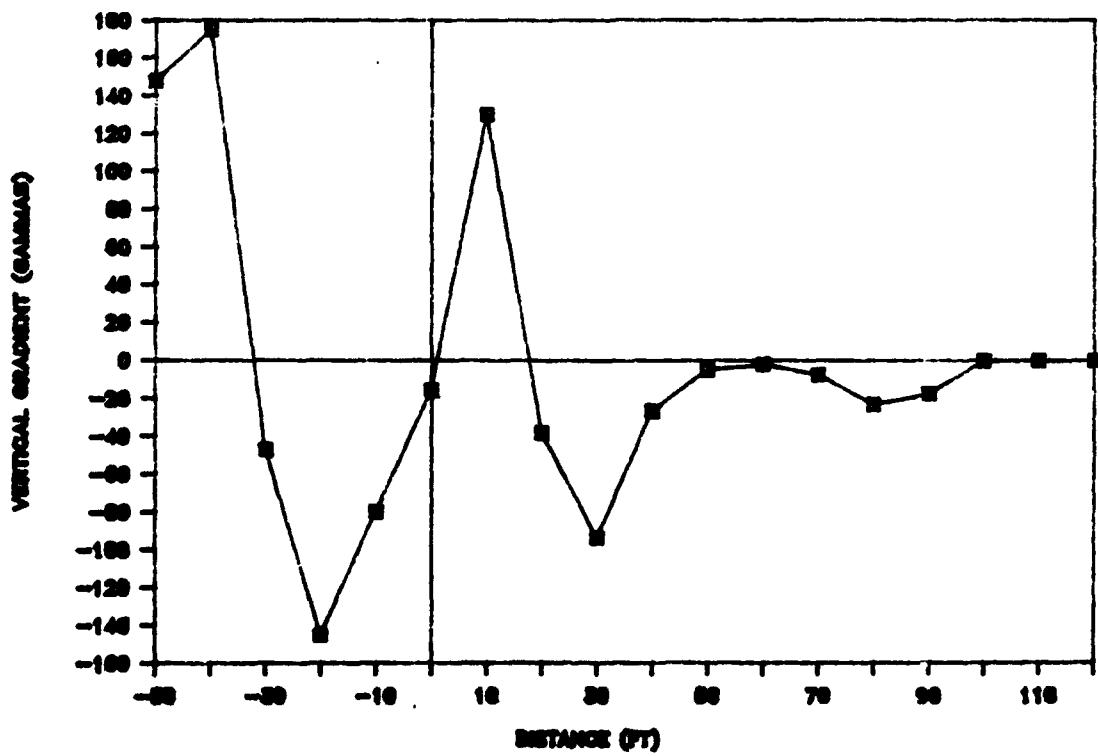
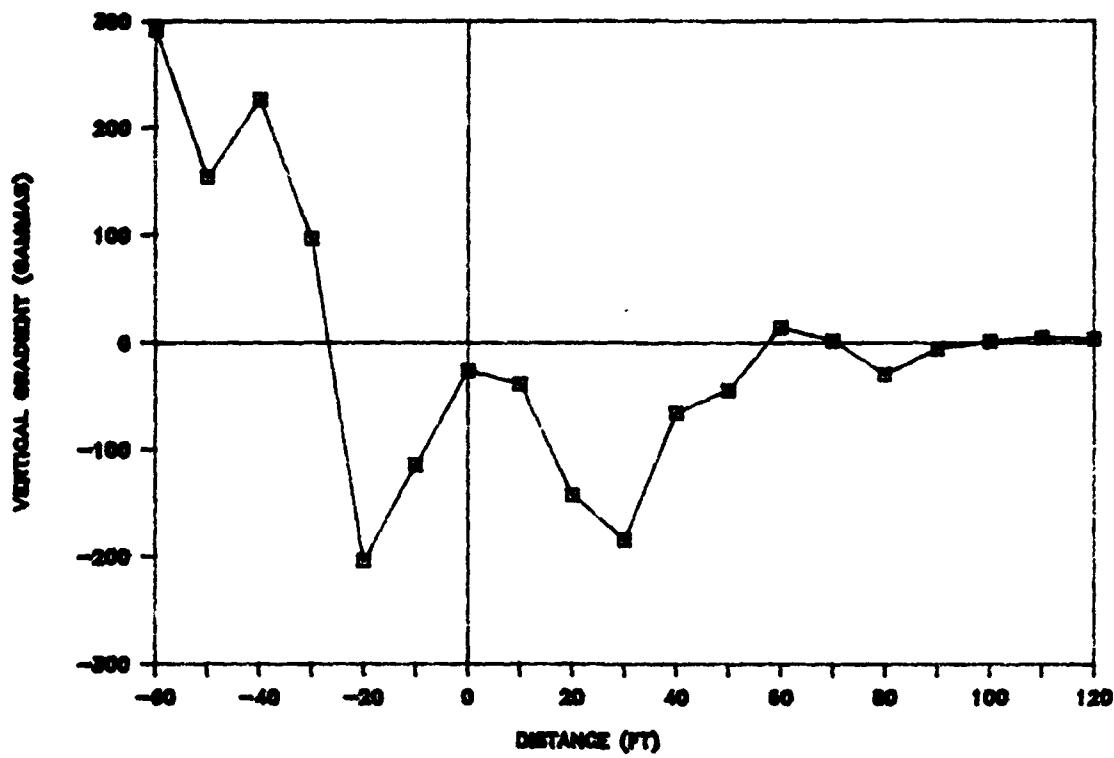


FIGURE A-13

STEWART AFB - LINE 24+50



STEWART AFB - LINE 25+00

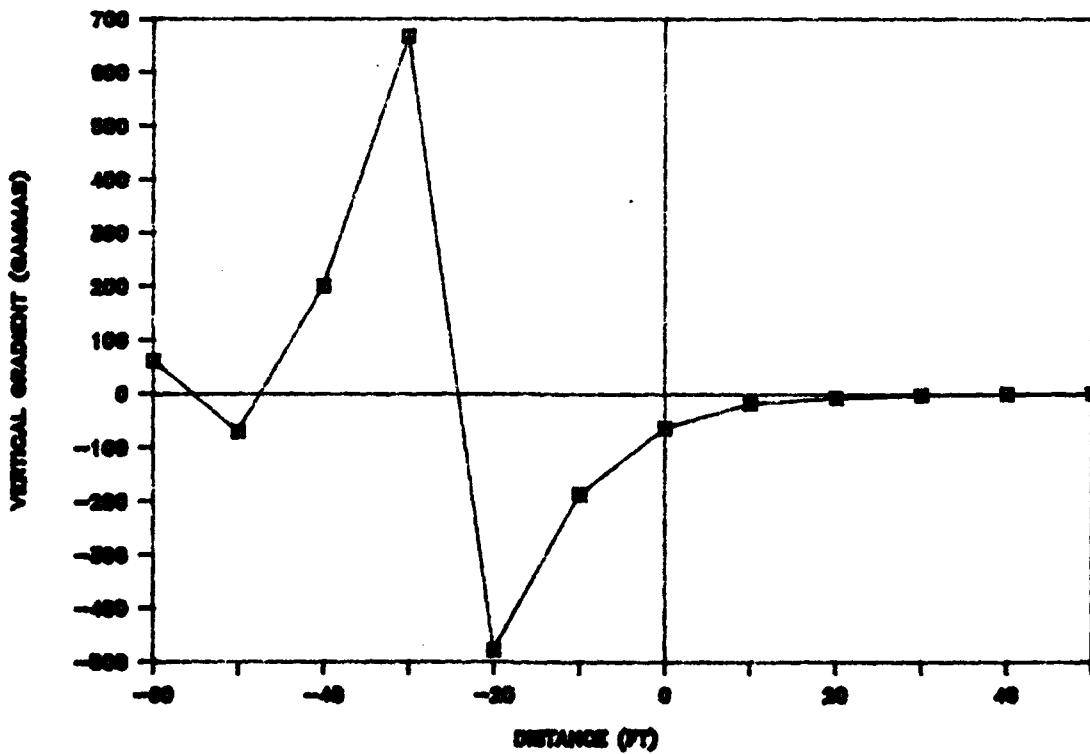
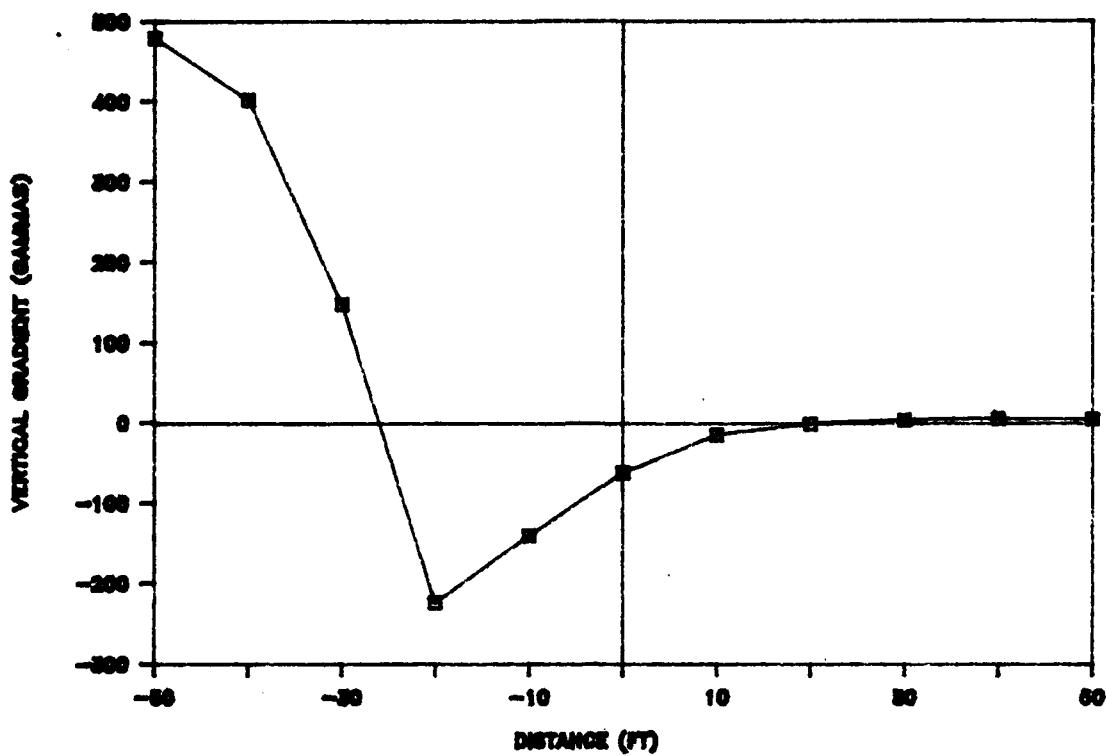


FIGURE A-14

STEWART AFB - LINE 25+50



STEWART AFB - LINE 26+00

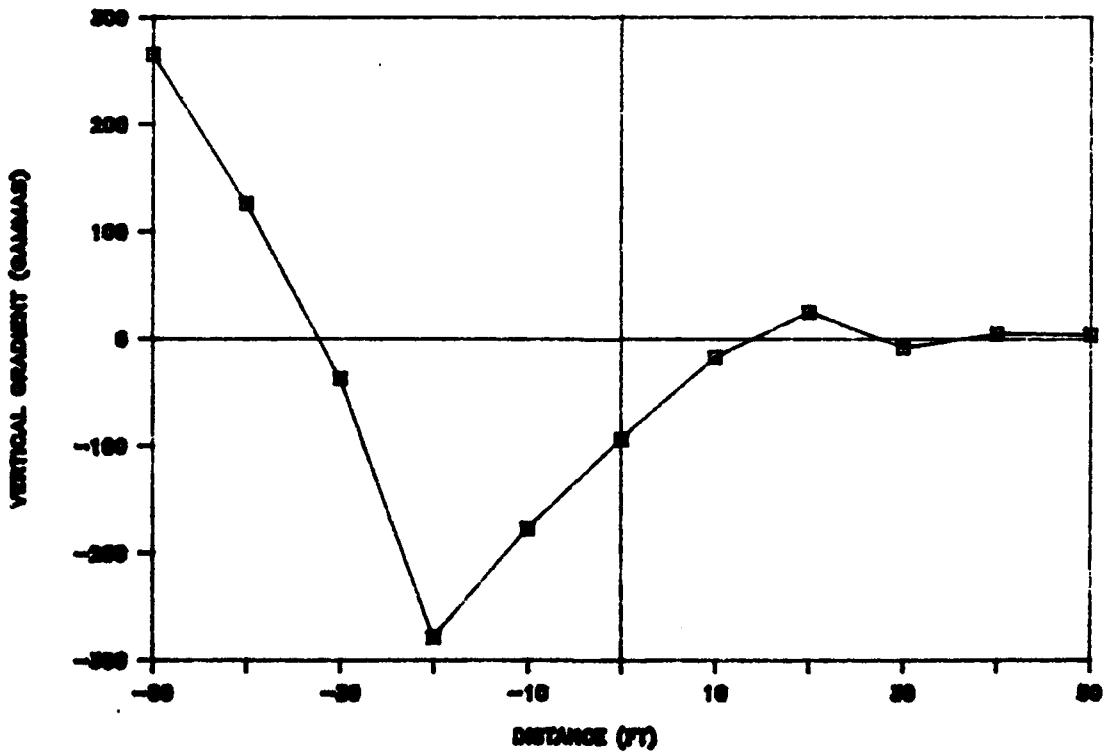
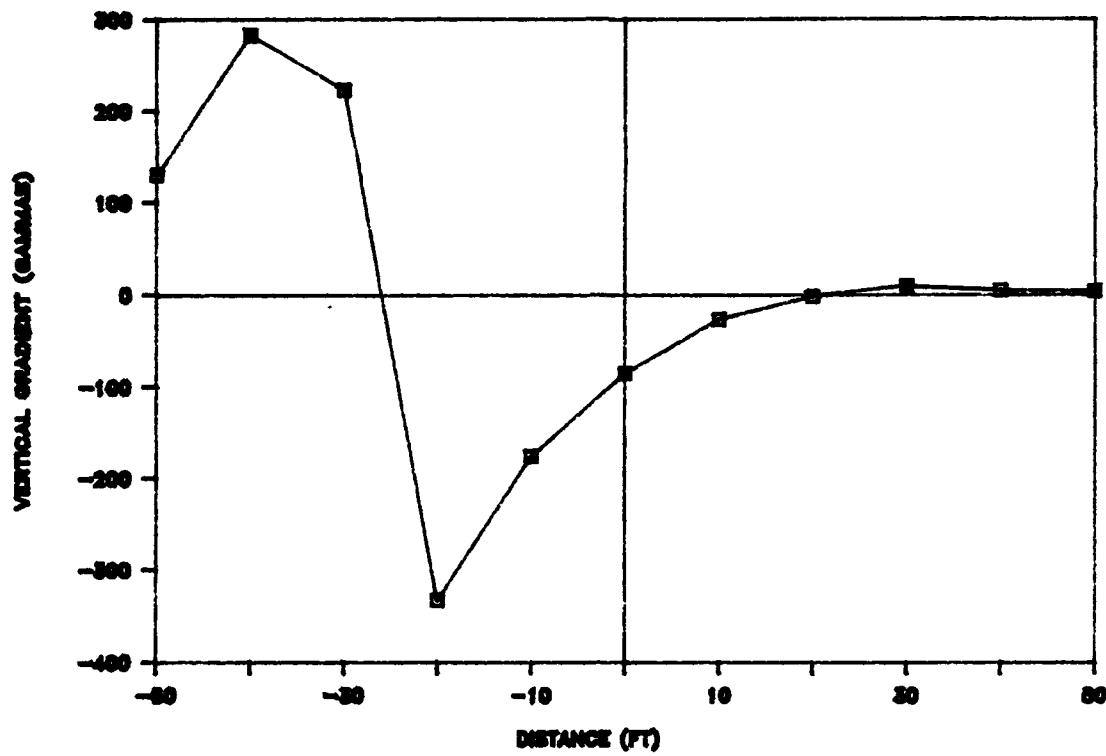


FIGURE A-15

STEWART AFB - LINE 26+50



STEWART AFB - LINE 27+00

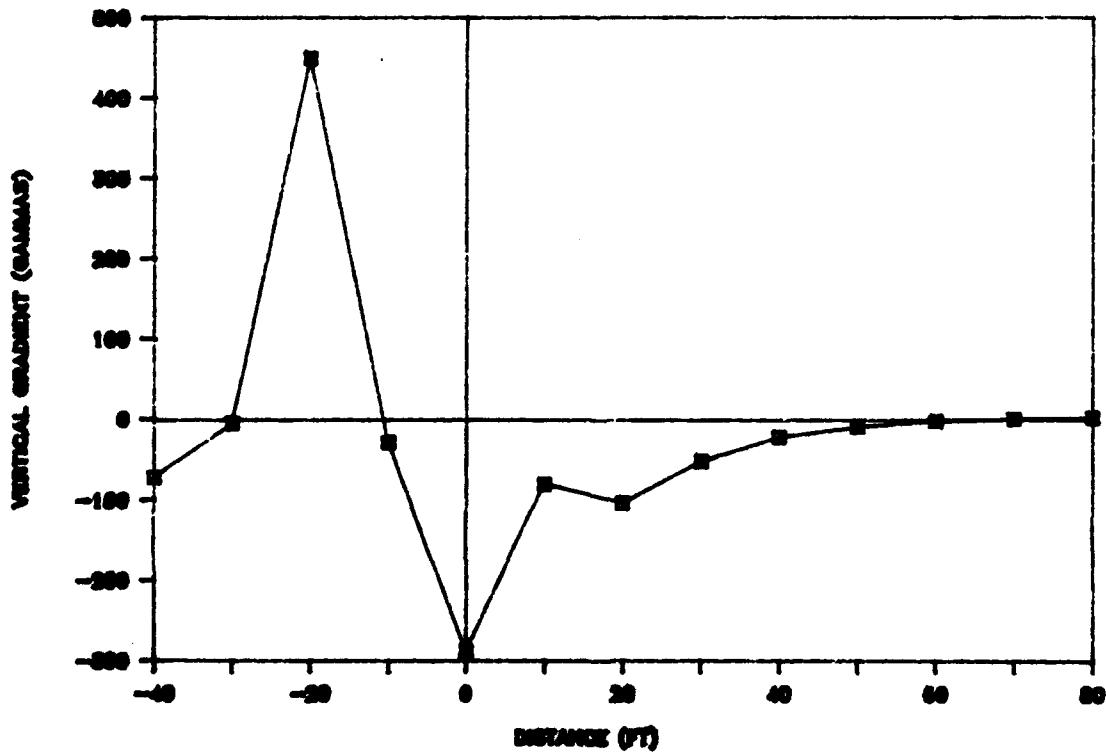
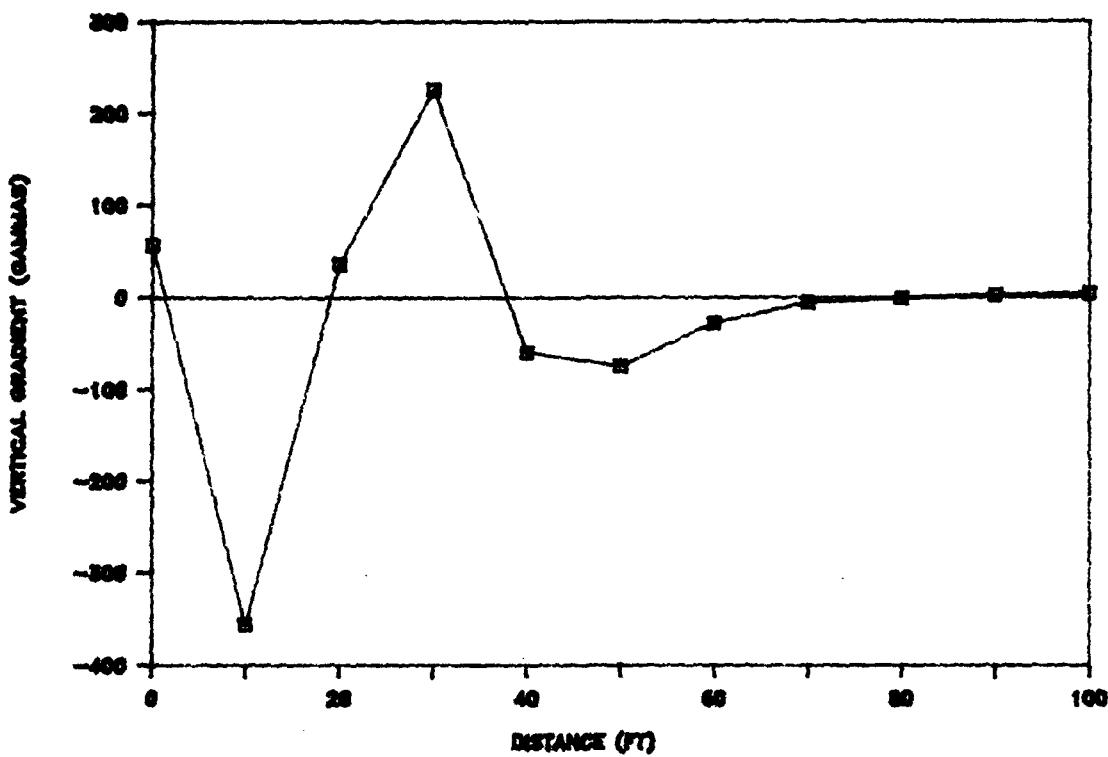


FIGURE A-16

STEWART AFB - LINE 27+50



STEWART AFB - LINE 28+00

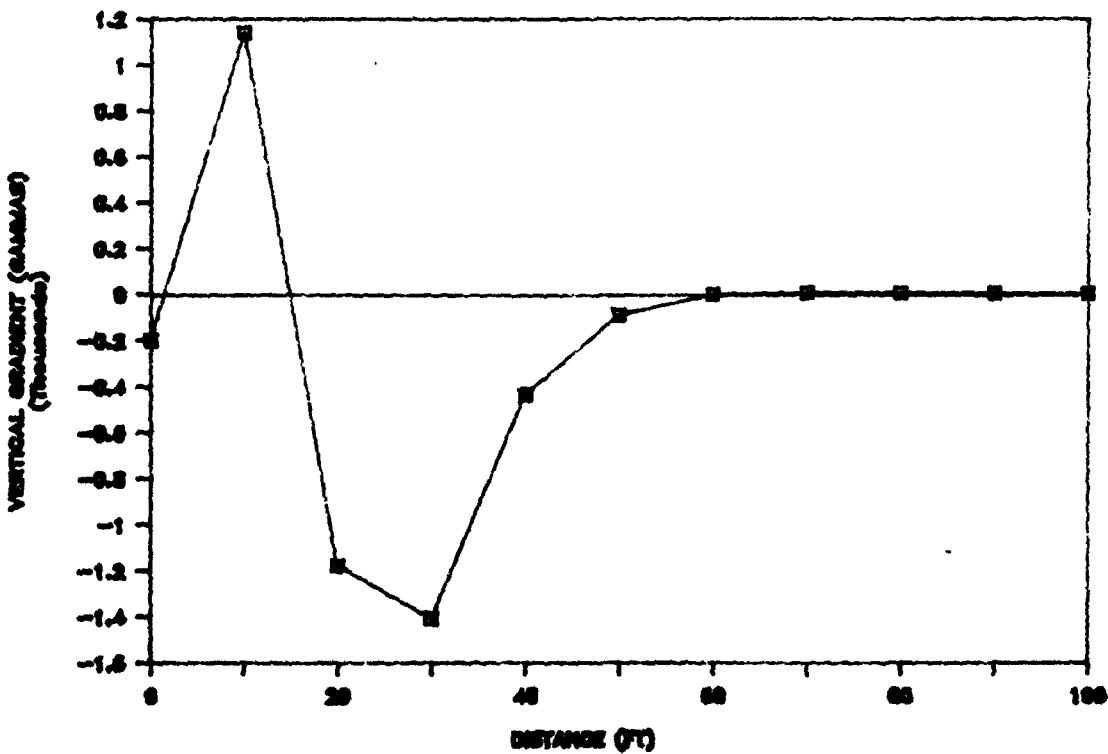
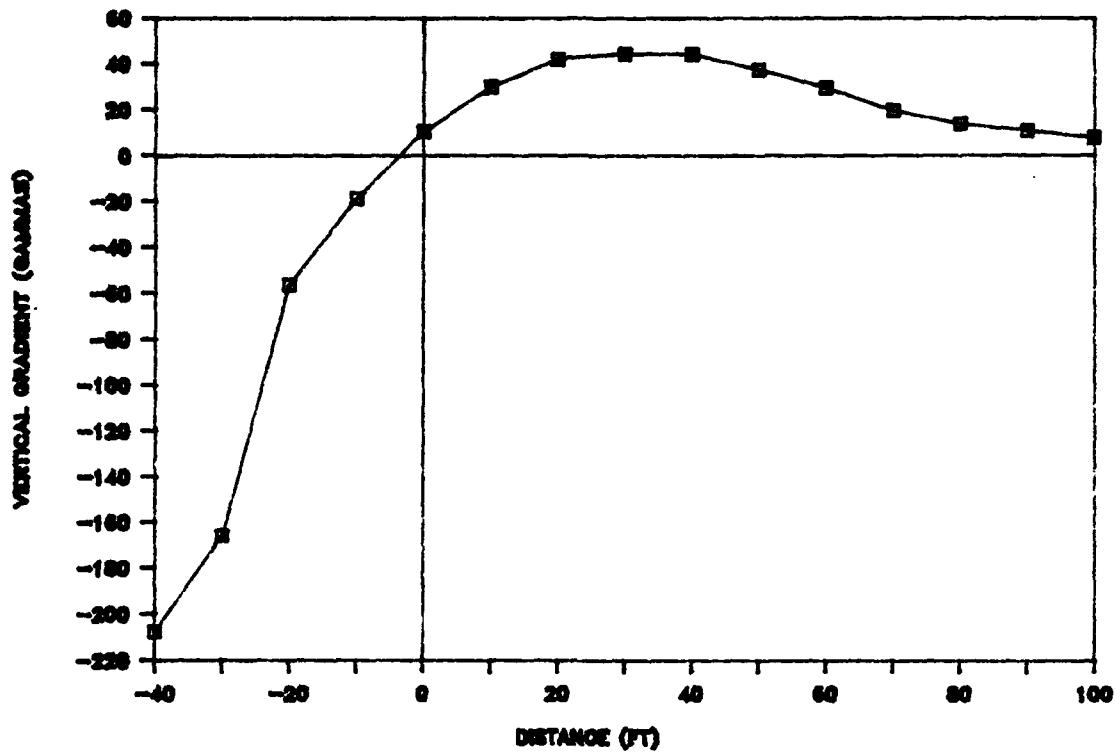


FIGURE A-17

STEWART AFB - LINE 28+35



STEWART AFB - LINE 30+50

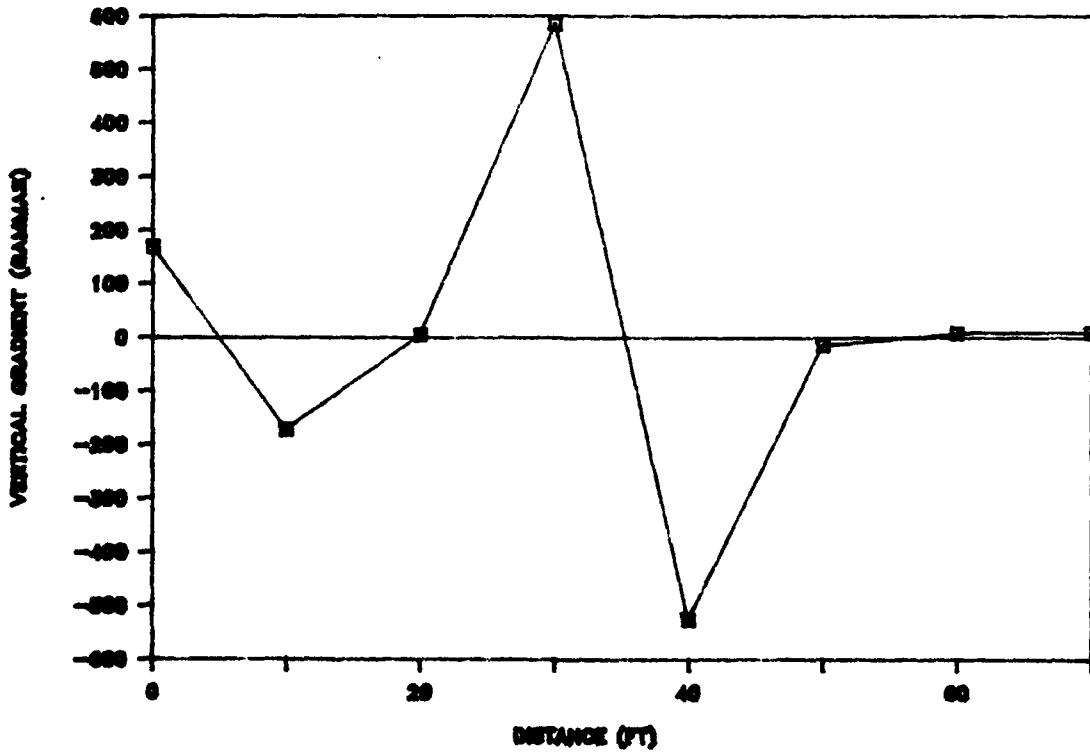


FIGURE A-18

STEWART AFB - LINE 30+80

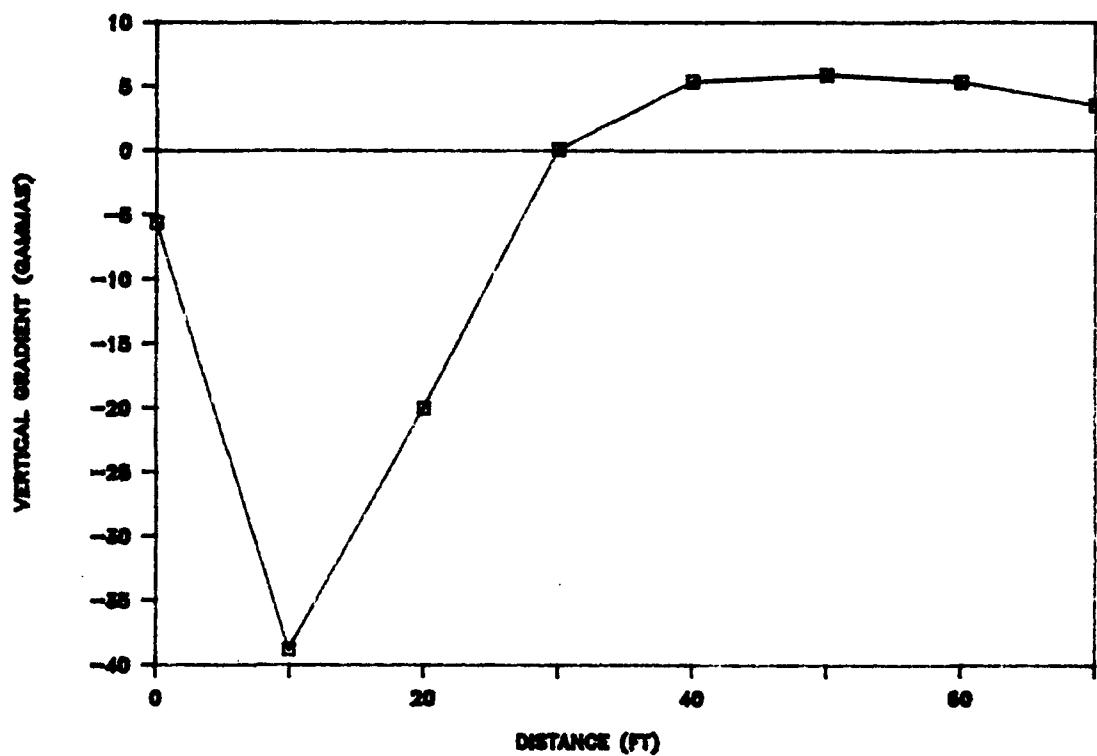


FIGURE A-19

APPENDIX A-2 TERRAIN CONDUCTIVITY MEASUREMENTS

INTRODUCTION

Terrain conductivity surveys, also referred to as EMI (electro-magnetic induction) surveys, have traditionally been used in mineral exploration for tracing conductive ore bodies (i.e., massive sulfides). More recently, conductivity surveys have been widely used for tracing conductive contaminant plumes in groundwater. Leachate from municipal landfills tends to be much more conductive than naturally occurring groundwater. Accordingly, the shape, extent, and relative impact of a plume can be studied with terrain conductivity surveys. Such surveys have also been successfully used in studying some organic contamination in soil and groundwater, since the conductivity of most organic chemicals is much lower than naturally occurring soils and groundwater.

Because the instrument never comes in contact with the ground, data acquisition is more rapid than conventional, galvanic, earth-resistivity surveys. However, quantification of conductivity data to yield a layered-earth solution is more difficult than with conventional earth resistivity.

INSTRUMENTATION

Two popular instruments used in terrain conductivity surveys are the EM-31 and EM-34-3, both manufactured by Geonics, Ltd., in Mississauga, Ontario. These instruments, which have proven to be rapid-reconnaissance exploration tools, are used to assess the conductivity values for soil and rock materials.

Simply stated, the instrumentation, which consists of a transmitter and receiver, operates in the following manner. The transmitter is energized by an alternating current that produces a magnetic field, designated as the primary field, H_p . This artificial magnetic field induces small electric currents to flow in the earth which, in turn, produce a secondary magnetic field, H_s . This secondary magnetic field is complexly related to the transmitter/receiver separation and to the operating frequency of the transmitter, both of which are selected by the operator. The ratio of the secondary field to the primary field (H_s/H_p), under conditions that are commonly fulfilled in the field, is linearly proportional to the terrain conductivity. It is the ratio that is sensed by the receiver and converted into conductivity values in units of millimhos per meter. Although it is difficult to define the thicknesses and "true" conductivity of individual subsurface layers, the instrument measures very precisely the "apparent" conductivity of a volume of underlying earth materials. The apparent conductivity value is comprised of the sum of the contributions from each layer that is "sampled" by the transmitter-receiver array. The volume (and therefore the depth) of earth materials sampled increases with increasing separation between the transmitter and receiver. The separation is fixed with the EM-31 (3 meters), but is operator-selectable with the EM 34-3 at 10, 20, or 40 meters.

Each instrument can be used in either the horizontal dipole or vertical dipole mode. Selection of the operational dipole mode depends on the depth of

sampling desired, and the desired sensitivity of the instrument to materials at various depths, relative to the transmitter-receiver coil separation. Table A-1 shows the relationship of effective depth of exploration.

INTERPRETATION

The relative response of the instrument to materials at various depths can be estimated by examining Figure A-20, which shows a comparison of the relative responses for vertical and horizontal dipoles. The vertical axis describes the relative contribution to the secondary magnetic field, arising from a thin layer at a given depth, z . The horizontal axis shows how this response varies as a function of the ratio (z/s), where "z" is the depth of the thin layer described previously and "s" is the transmitter/receiver separation.

Figure A-20 demonstrates that in the vertical dipole mode, the contribution to the secondary magnetic field from near-surface materials is very small, but reaches a maximum at a depth "z" of approximately $0.4*s$. The contribution is significant, although diminished, at a depth of $1.5*s$. This depth represents the effective depth of exploration in the vertical dipole mode (Table A-1).

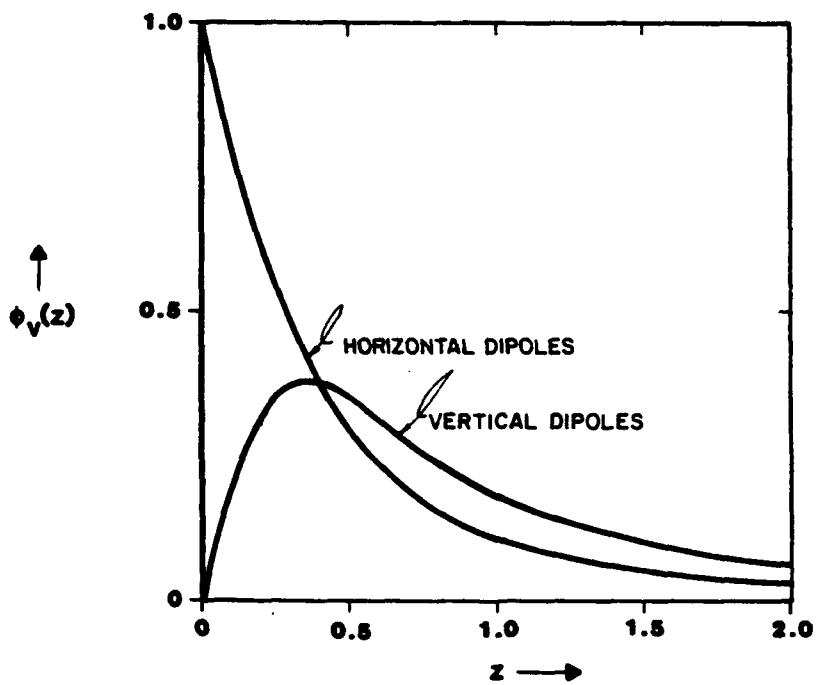
In the horizontal dipole mode, the contribution to the secondary magnetic field, arising from near-surface materials, is a maximum and decreases with increased depth. The contribution is also significant at a depth of about $0.75*s$. This depth represents the effective depth of exploration in the horizontal dipole mode (Table A-1).

The terrain conductivity data acquired during the present study are presented in Figure A-21. The reader is referred to the main text for a brief discussion of these data.

TABLE A-1

TERRAIN CONDUCTIVITY MEASUREMENTS
EFFECTIVE DEPTH OF EXPLORATION

<u>Instrument</u>	<u>Coil Separation</u>	<u>Vertical Dipole</u>	<u>Horizontal Dipole</u>
EM 31	3m	4.5m	2.25m
EM 34-3	10m	15m	7.5m
	20m	30m	15m
	40m	60m	30m



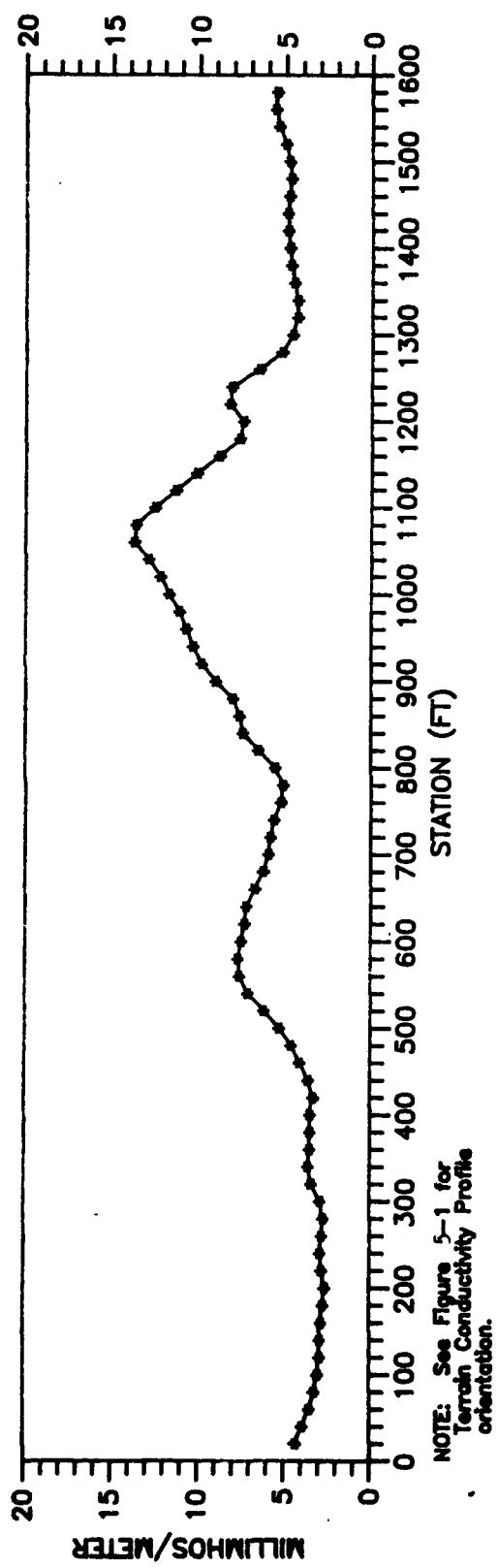
Note: " $\phi_v(z)$ " is the relative contribution to the secondary magnetic field intensity from material in a thin layer (dz) located at (normalized) depth "z".

"z" is the depth of the thin layer (dz) divided by the intercoil spacing between transmitter and receiver.

TERRAIN CONDUCTIVITY SURVEY COMPARISON OF RELATIVE RESPONSES FOR VERTICAL AND HORIZONTAL DIPOLES

FIGURE A-20

TERRAIN CONDUCTIVITY PROFILE - LINE 1
STEWART AIR FORCE BASE



TERRAIN CONDUCTIVITY PROFILE - LINE 2
STEWART AIR FORCE BASE

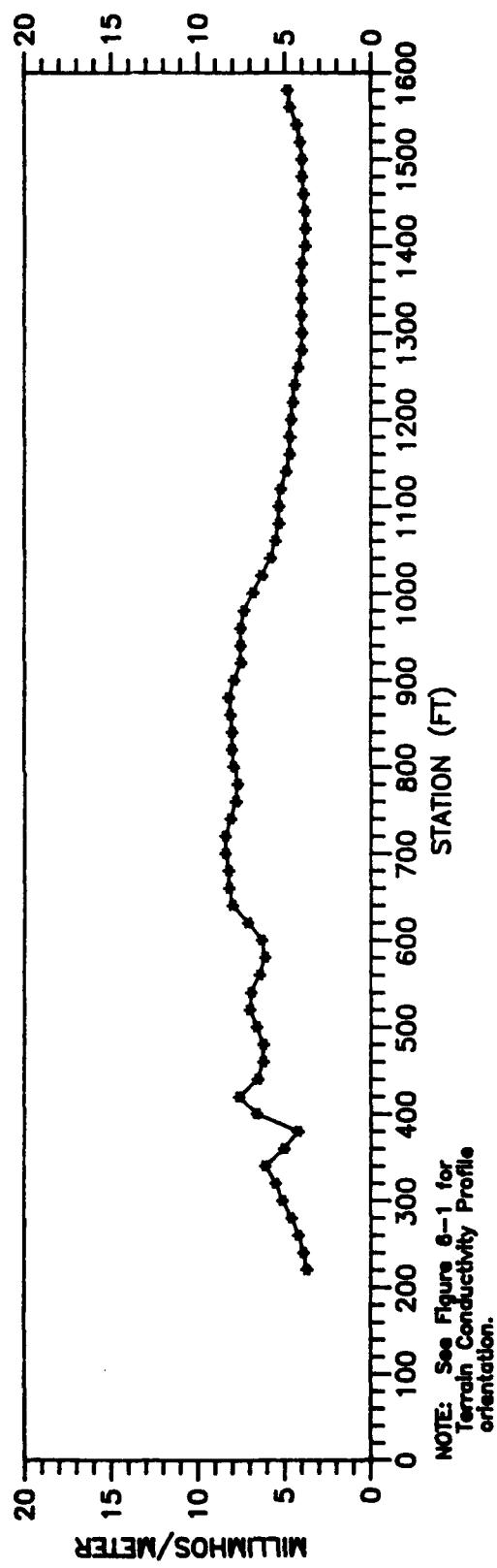


FIGURE A-21

APPENDIX B
BORING LOGS AND INSTALLATION DETAILS

- B-1 SOIL BORING LOGS (INCLUDING PEIZOMETER AND MONITORING WELL INSTALLATION DIAGRAMS)**
- B-2 ROCK CORE LOGS**
- B-3 MONITORING WELL INSTALLATION SHEETS**

APPENDIX B-1

**SOIL BORING LOGS (INCLUDING PIEZOMETER AND
MONITORING WELL INSTALLATION DIAGRAMS)**

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-100

PROJECT NO. 5139-01

CONTRACTOR: ENTRIX CONSULTING GROUPS

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED 8/13/87 **COMPLTD.** 8/14/87

METHOD Spur casing

CASING SIZE 4" I.D.

HNU TIP 10.6

PROTECTION LEVEL B C D

GROUND FL

SOIL DRILLED

ROCK DRILLED

ET BELOW GROUND

LOGGED BY

CHECKED BY

DATE

W. BROWN GROVES 55.6'

* UL-THIN WALL SPLIT SPOON R-ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM							BORING NO. JTB-100			
CLIENT STEWART AIR NATIONAL GUARD BASE							PROJECT NO. 5139-01			
CONTRACTOR EMPIRE SOILS INVESTIGATIONS				DATE STARTED 8/13/87 COMPLTD. 8/14/87						
METHOD Spun casing	CASING SIZE 4" I.D.			HNU TIP 10.6			PROTECTION LEVEL B C D			
GROUND EL 433.93	SOIL DRILLED 45.6'			ROCK DRILLED 10'			FT BELOW GROUND 55.6			
LOGGED BY J. Urquhart	CHECKED BY FEB			DATE 11-10-87						
DEPTH (FT)	HNU AMB. AIR SAMPLE & TYPE NO.	CLP SAMPLE	GC RECOVERY	HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION			GRAPHICAL LITHOLOGY	BLOWS/6-IN	WELL DATA EL. (FT)
40	Bkg	S-9	X		Sandy Silt	Grey fine sandy silt with little clay, trace gravel. Clay structure has thin laminations. Widely graded, moist, cohesive medium dense to dense.		ML	24 47 4760 94	
45		S-10	X	.2	Shale	Black, dark grey extremely weathered shale, Fe staining on fractured surfaces, thinly bedded.			84100	
50					Roller bit 45.6' to 55.6'					
55					B.O.B. 55.6'					
60										

* U=THIN WALL S=SPLIT SPOON R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM								BORING NO. JTB-101
CLIENT STEWART AIR NATIONAL GUARD BASE								PROJECT NO. 5139-01
CONTRACTOR EMPIRE SOILS INVESTIGATIONS				DATE STARTED 8/4/87		CCMPLTD. 8/7/87		
METHOD HSA/Spun casing				CASING SIZE 4" I.D.		HNU TIP 10.6		PROTECTION LEVEL B C D
GROUND EL 437.64				SOIL DRILLED 37.7'		ROCK DRILLED 8.8'		FT BELOW GROUND 46.5
LOGGED BY S. Pinette				CHECKED BY FFB	DATE 11-10-87	Page 2 of 2		
DEPTH ft	(ft) INN AMB AIR SAMPLE & TYPE NO. SAMPLE	CIP INN HEADSPACE (ppm)	GC RECOVERY INN	SOIL/ROCK DESCRIPTION			GRAPHICAL LITHOLOGY SOIL CLASS OR ROCK FRACTURES	WELL DATA BLOWS/6-IN or RQD % 20 40 60 80 EL. (ft)
40	R-1			Shale	Medium gray, well cleaned @ 45°, staining on cleavage surfaces, very broken;			
45	R-2				Sandstone interbedded with shale at 42.6 to 43.3			
50				B.O.B. @ 46.5'				

* U= THIN WALL S= SPLIT SPOON R= ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JMW-101

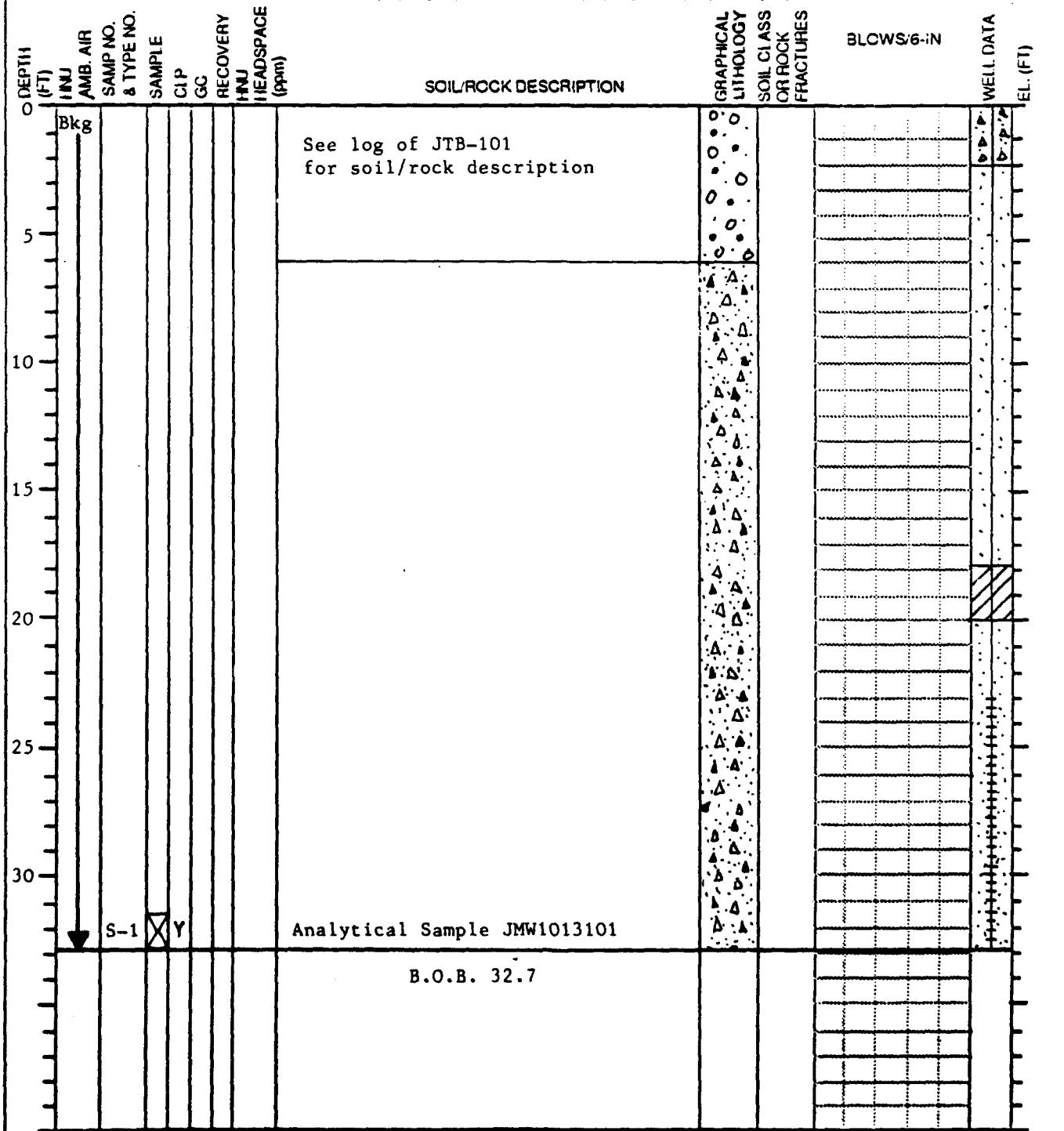
PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS **DATE STARTED** 8-7-87 **COMPLTD.** 8-10-87

METHOD HSA Casing Size 4-1/2" I.D. HNU Tip 10.6 Protection Level B C D

GROUND Elevation 427.82 SOIL DRILLED 32.5' ROCK DRILLED 0.2' FT. BELOW GROUND 32.7'

LOGGED BY T. Longley CHECKED BY FFR DATE 11-10-87



* U= THIN WALL S= SPLIT SPOON R= ROCK

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM								BORING NO. JTB-102				
CLIENT STEWART AIR NATIONAL GUARD BASE								PROJECT NO. 5139-01				
CONTRACTOR EMPIRE SOILS INVESTIGATIONS				DATE STARTED 8/11/87		COMPLTD. 8/13/87						
METHOD Spun Casing				CASING SIZE 4" I.D.		HNU TIP 10.6		PROTECTION LEVEL B C D				
GROUND EL 427.62				SOIL DRILLED 51.6'		ROCK DRILLED 10'		FT BELOW GROUND 61.6'				
LOGGED BY J. Urquhart				CHECKED BY FFB		DATE 11-10-87						
DEPTH (FT)	HNU AMB. AIR SAMPLE NO. & TYPE NO.	SAMPLE CLP	GC	RECOVERY %	HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION		GRAPHICAL LITHOLOGY	SOIL CLASS OR ROCK FRACTURES	BLOWS/6-IN N	WELL DATA EL. (FT)	
0	Bkg	S-1	X		1.5	Sandy Silt Topsoil & Ablation Till	Brown with organics, loose, over brownish grey fine sandy silt, trace gravel, trace coarse sand, widely graded, dry loose	O	SM	7 12 17 19 29	4	
5								O				
10								O				
15		S-2	X	Y	1.5	Silt Basal Till	Brownish grey silt with trace fine sand, some gravel, widely graded, slightly moist, very dense basal till	A	ML	30 5953 70 112	4	
20		S-3	X		0.8	Silt Basal Till	Analytical Sample JTB1021201 Dark grey silt with trace fine sand some gravel, widely graded, moist, very dense, basal till	A	ML	36 5665 51 121	4	
25		S-4	X		1.2	Gravelly Silt Basal Till	Dark grey silt with trace fine sand much gravel, moist, very dense, basal till	A	ML	2255 64100 119	4	
30		S-5	X		1.1		Dark grey silt with trace fine sand much gravel. Isolated light grey clay lenses, moist, cohesive, plastic, very dense, basal till	A	ML	5970 81100 151	4	
35		S-6	X		0.9	Silt	Brownish grey silt with trace fine sand, little clay, some gravel. Moist very dense, basal till	A	ML	43 55 68100 123	4	
40												

* U=THIN WALL

S=SPLIT SPOON

R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM
BORING NO. JTB-102

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED
COMPLTD. 8/13/87

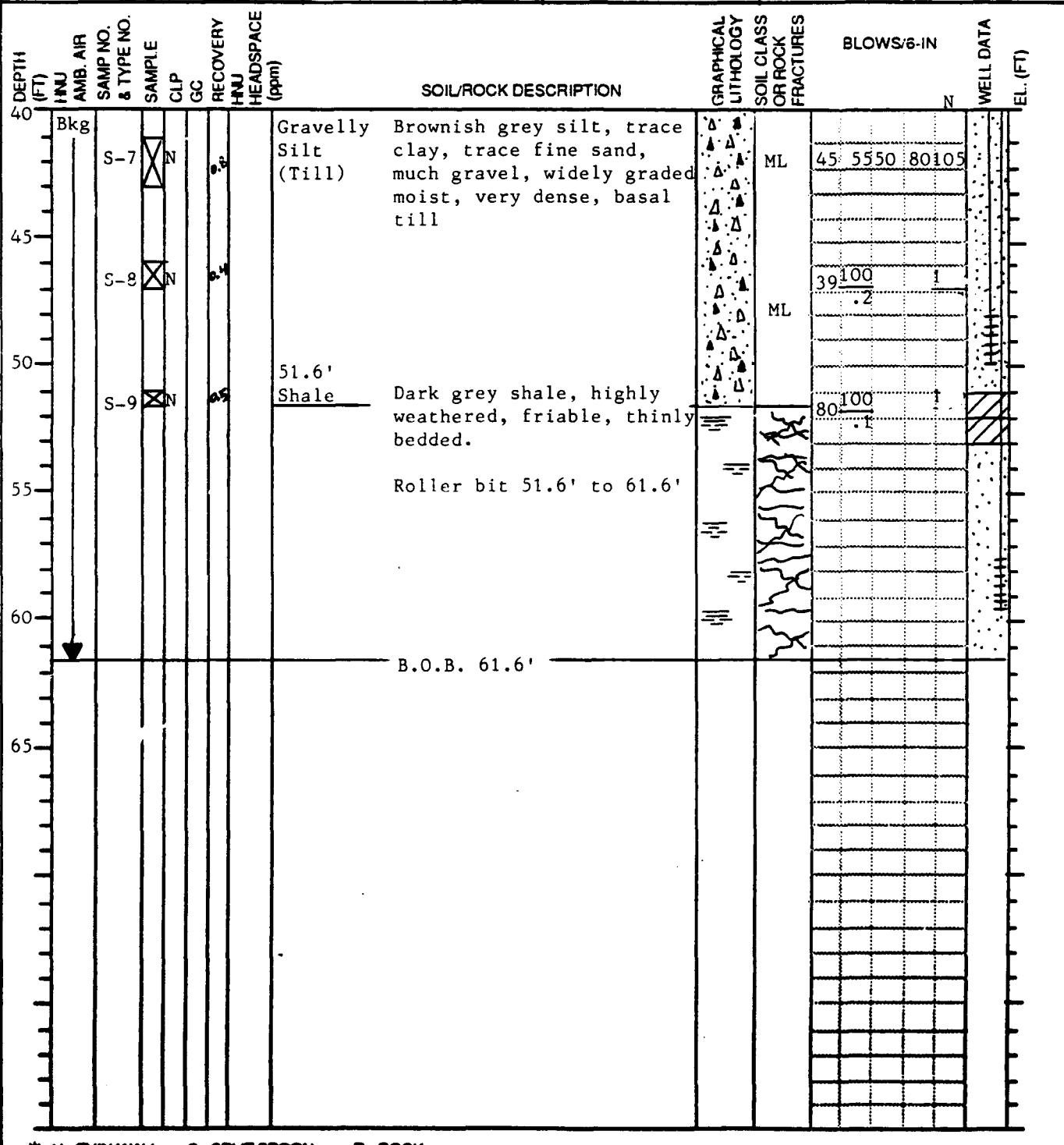
METHOD Spun casing

CASING SIZE 4" I.D. **HNU TIP** 10.6 **PROTECTION LEVEL** B C D

GROUND EL 427.62

SOIL DRILLED 51.6 **ROCK DRILLED** 10' **FT BELOW GROUND** 61.6'

LOGGED BY J. Urquhart

CHECKED BY FFB **DATE** 11-10-87

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM
BORING NO. JTB-103

CLIENT	STEWART AIR NATIONAL GUARD BASE	PROJECT NO.	5139-01
CONTRACTOR	EMPIRE SOILS INVESTIGATIONS	DATE STARTED	8/12/87 COMPLTD. 8/14/87
METHOD	Spin casing/coring	CASING SIZE	4" I.D.
GROUND EL	432.54	SOIL DRILLED	41'
LOGGED BY	T. Longley	CHECKED BY	FFB
DEPTH (FT)	HNU AMB. AIR SAMPLE & TYPE NO. CLP	GC RECOVERY HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION

DEPTH (FT)	HNU AMB. AIR SAMPLE & TYPE NO. CLP	GC RECOVERY HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION	GRAPHICAL LITHOLOGY	SOIL CLASS OR ROCK FRACTURES	BLOWS/6-IN or RQD %		WELL DATA EL. (FT)	
						N	ML		
0	Bkg	S-1	X	10	Bkg	Sandy Silt Tan fine sandy silt, Over trace coarse sand, trace gravel, dry, loose, over Silty Sand tan gravelly, silty sand Fill & Ablation Till	• • • • • • • • • •	SM	8 3350/0.0
5	S-2	X Y	17	Bkg	Silt & Sand Basal Till	Brown, trace gravel, trace clay, well graded, damp, non-plastic, very dense, massive structure Analytical Sample JTB1030501	△ △ △ △ △ △	SM	36 30 3137 61
10	S-3	X	18	Bkg		While tri-coning, water return turned grey at 13'.	△ △ △ △ △ △		26 22 3575 57
15	S-4	X	19	Bkg	Sandy Silt	Gray, trace fine gravel, non to slightly plastic, evenly graded, dense, damp	△ △ △ △ △ △	ML	11 21 4267 63
20	S-5	X	20	Bkg		As above but appears like weathered bedrock, very dense, damp, cemented till, trace gravel is all gray shale	△ △ △ △ △ △		12276
25	S-6	X	21	Bkg		As above but with little sand	△ △ △ △ △ △		3289100/0.4
30	S-7	X	22	Bkg		Gray, trace coarse sand, trace gravel, trace clay very well sorted, very dense, non-plastic, damp	△ △ △ △ △ △		13 139 83100/.3
35	S-8	X	23	Bkg		As above, but around a $\frac{1}{2}$ " lense of very well sorted fine sand	△ △ △ △ △ △		33 57100/.3
40	S-9		24	Bkg	Silty Sand	Yellowish-brown with little coarse shale fragments, damp	△ △ △ △ △ △	SM	29 47100/.1

* U= THIN WALL S=SPLIT SPOON R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM							BORING NO. JTB-103		
CLIENT STEWART AIR NATIONAL GUARD BASE							PROJECT NO. 5139-01		
CONTRACTOR EMPIRE SOILS INVESTIGATIONS				DATE STARTED 8/12/87 COMPLTD. 8/14/87					
METHOD Spin casing-coring	CASING SIZE 4" I.D.			HNU TIP 10.6			PROTECTION LEVEL B C D		
GROUND EL 432.54	SOIL DRILLED 40'			ROCK DRILLED 11.4'			FT BELOW GROUND 51.4'		
LOGGED BY T. Longley	CHECKED BY FFB			DATE 11-10-87					
DEPTH (FT)	HNU AMB AIR SAMPLE NO. & TYPE NO. SAMPLE	CLP GC	RECOVERY HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION			GRAPHICAL LITHOLOGY	SOIL CLASS OR ROCK FRACTIONS	BLOWS/6-IN
40				Extremely weathered bedrock, water return is brown				SM	
45	S-10	69	Bkg	Sand & Silt (Weathered Rock)	Brown, trace gravel, very dense, wet; few distinct brown mottles; weathered rock				100/.1
46	S-11	61	Bkg		Black & brown w/little clay, moist, lensoid, very hard				100/.3
50	S-12	60	Bkg		B.O.B. @ 51.4' Solid Rock				
55									
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* U=THIN WALL S=SPLIT SPOON R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-104

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED 8/11/87 **COMPLTD.** 8/12/87

METHOD Spin casing-coring Casing Size 4" I.D.

HNU TIP 10.6 PROTECTION LEVEL B C D

GROUND EL

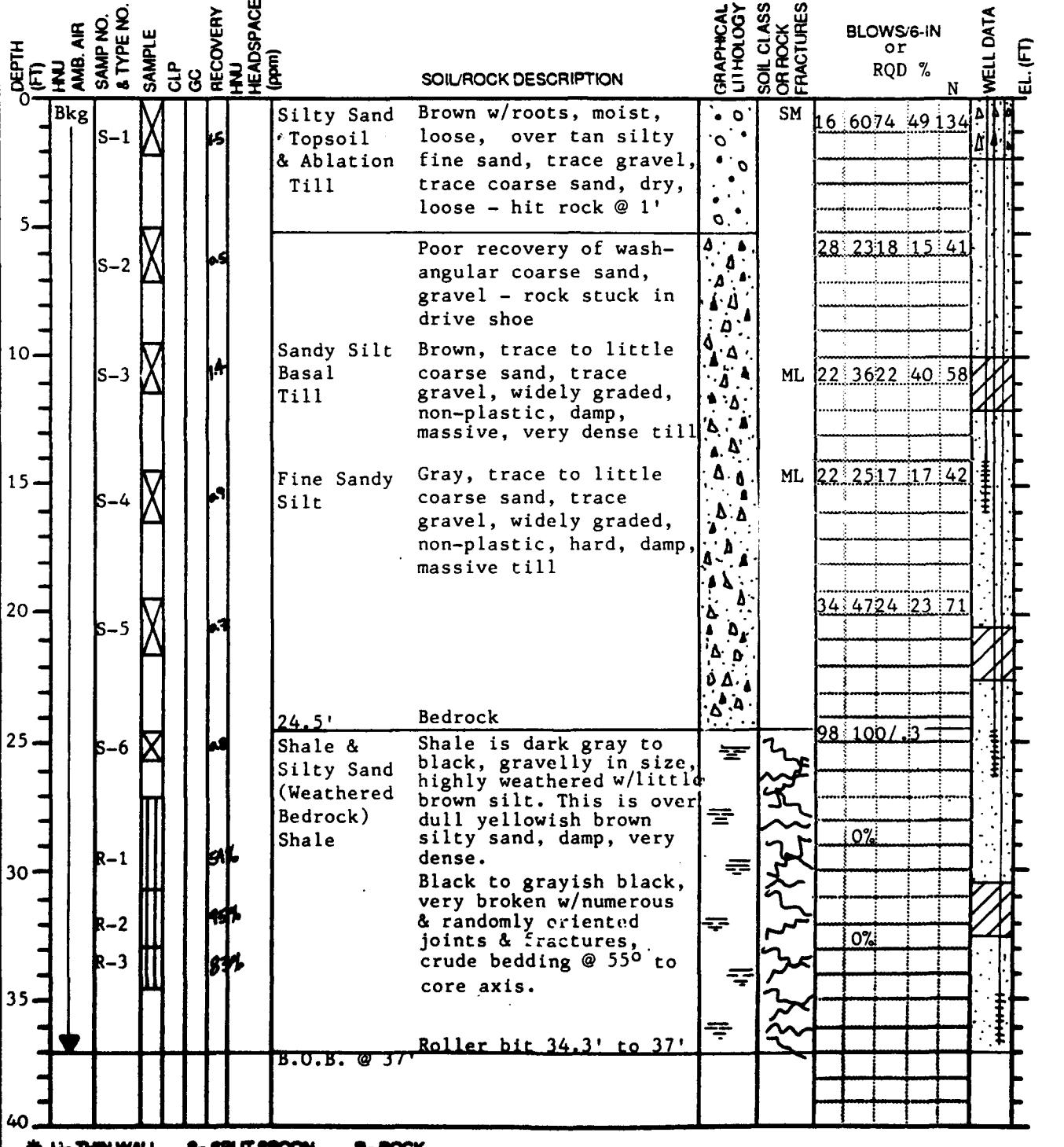
ROCK DRILLED 10' **FT BELOW GROUND** 37.0

LOGGED BY T. Leppla

DATE 11.10.87

• Longue

11-10-87



* U=THIN WALL S=SPLIT SPOON R=ROCK

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-105

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

METHOD Spin casting serial Casing Size 400 T.D.

GROUND FL 303-60

LOGGED BY T. Longley &

SEARCHED BY J. Urquhart | CHECKED BY FFB

REVIEW OF THE LITERATURE

* U-THIN WALL S-SPLIT SPOON R-ROCK

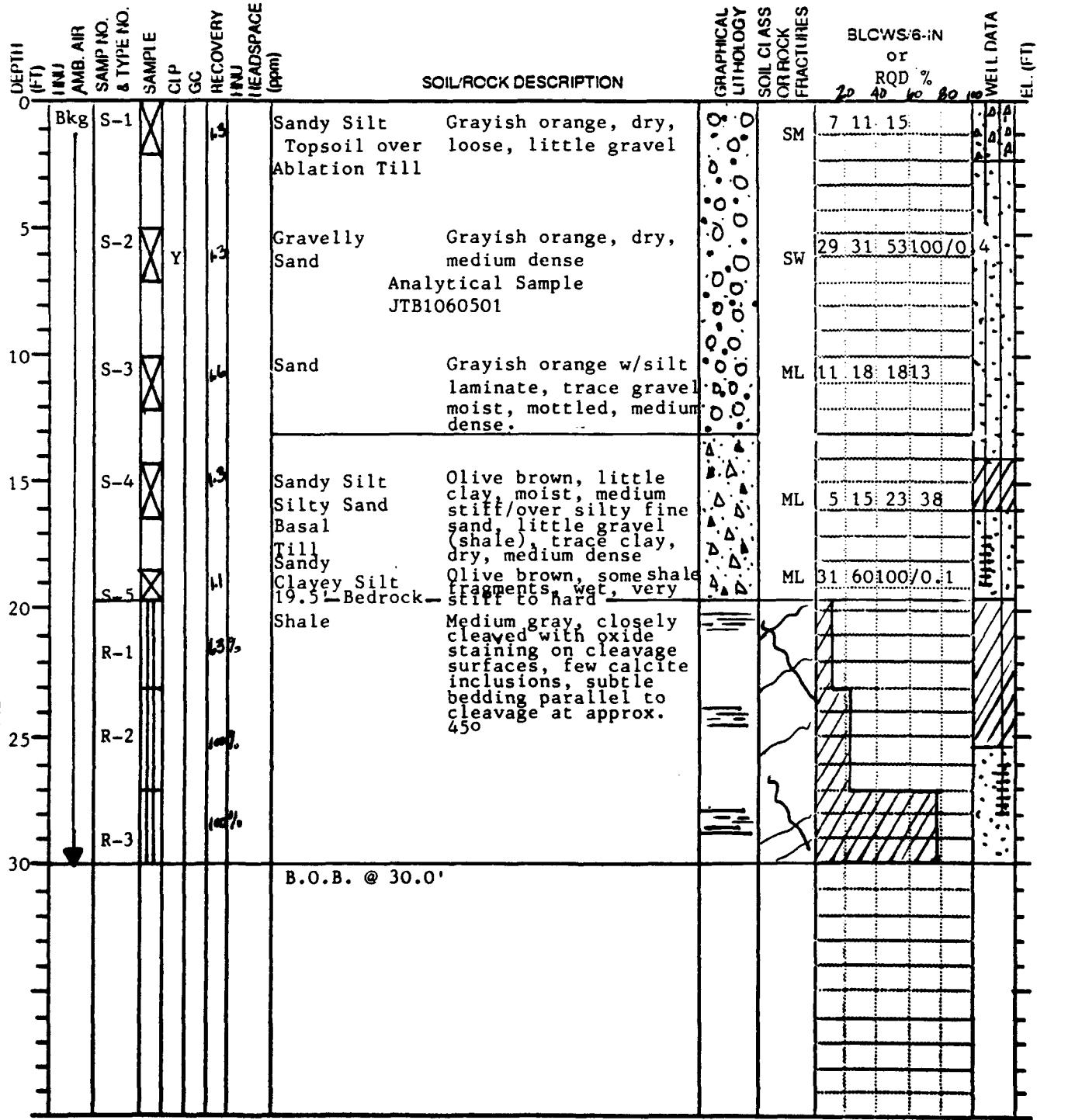
L.E.C. JORDAN CO.

*Cored cobbles; not boxed

INSTALLATION RESTORATION PROGRAM
BORING NO. JTB-106

CLIENT	STEWART AIR NATIONAL GUARD BASE	PROJECT NO.	5139-01
CONTRACTCR	EMPIRE SOILS INVESTIGATIONS	DATE STARTED	7/30/87 CCMPLTD. 8/4/87
METHOD	HSA/Rock core	CASING SIZE	4.25"
GROUND EL	386.97	HNU TIP	10.6
LOGGED BY	S. Pinette	SOIL DRILLED	19.5'
		ROCK DRILLED	10.5'
		FT BELOW GROUND	30.0
		CHECKED BY	FFB
		DATE	11-10-87

Page 1 of 1



* U=THIN WALL S=SPLIT SPOON R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-107

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SONS INVESTIGATIONS

DATE STARTED 7/30/87 COMPI LTD 8/3/87

METHOD : Casing size / mm. & P.

PROTECTION LEVEL B C D

GROUND FL

SOIL DRILLED

ROCK DRILLED at **16 FT. BELOW GROUND** 100%

LOGGED BY

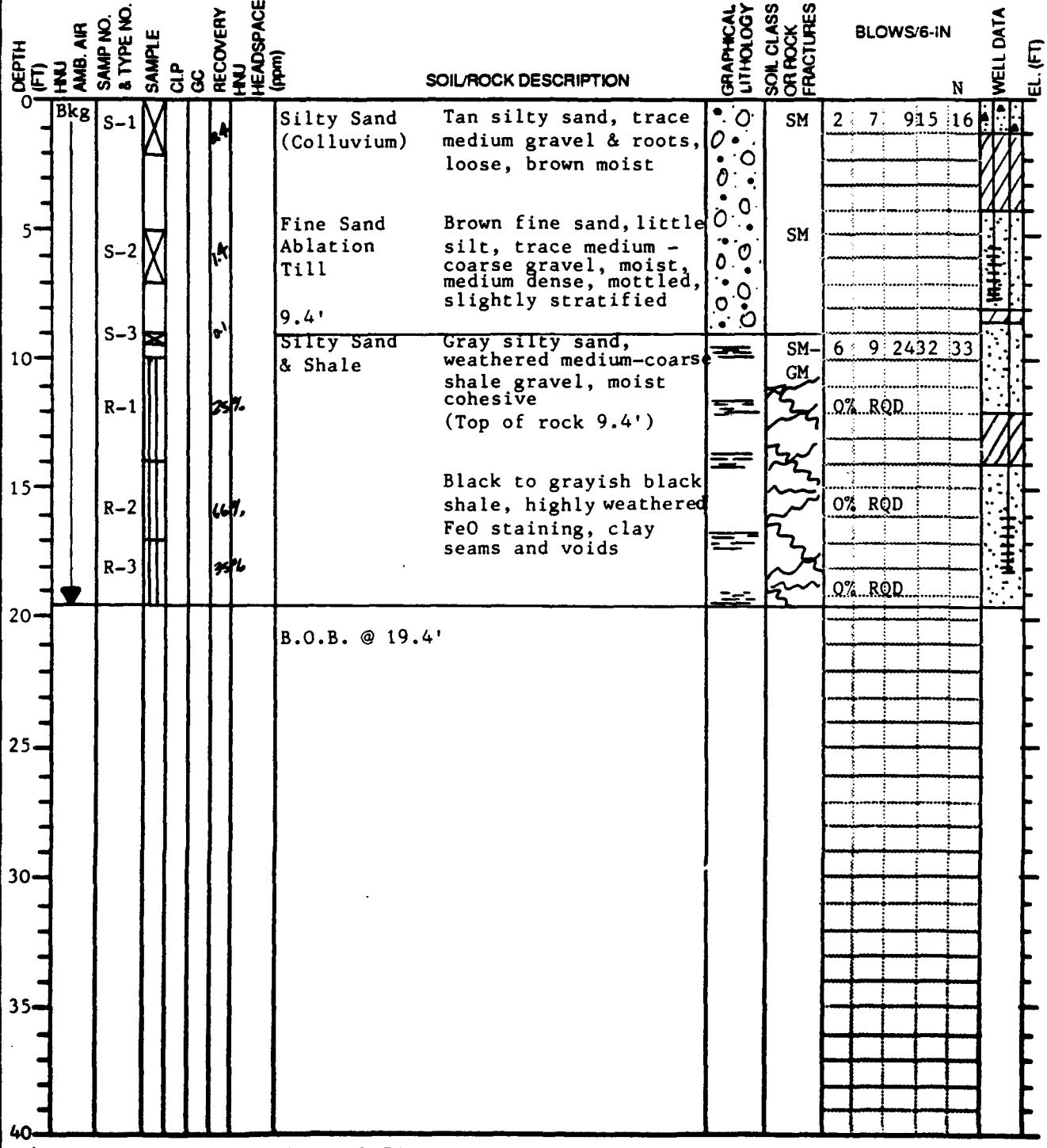
SOIL DRILLED 10.0

ROCK SHELLS 9.4 FT BELOW GROUND 19.4

LOGGED BY L. Heale

CHECKED BY FFB

DATE 11-10-87



* U=THIN WALL S=SPLIT SPOON R=ROCK

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JMW-107

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED 7/30/87 COMPLTD. 8/3/87

METHOD 4 25" HSA

CASING SIZE N/A

HNII TIP 10.6

PROTECTION LEVEL B C D

GROUND FL

SOIL DRILLED # 31-0

BOCK DRILLED

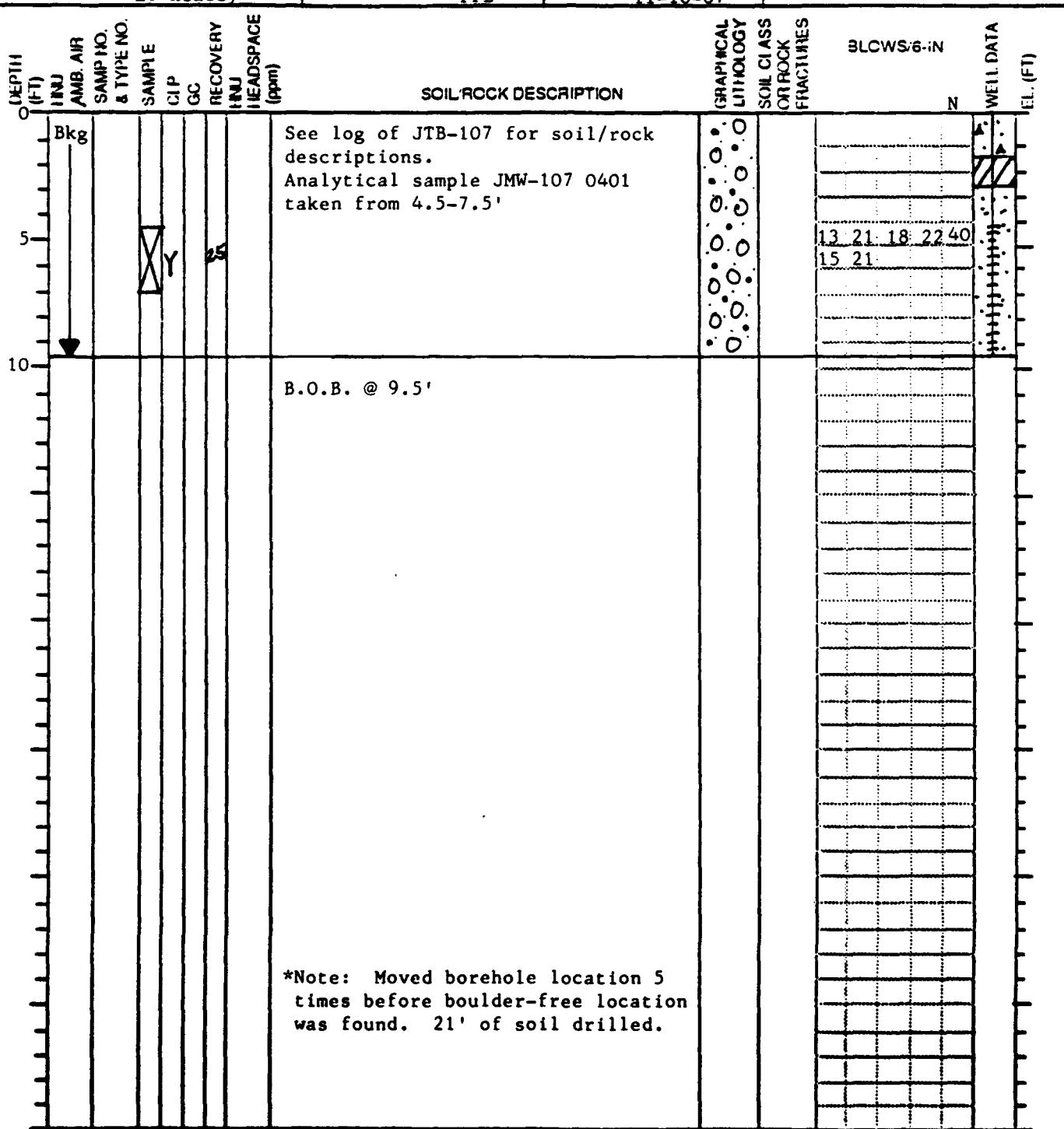
FT. BELOW GROUND 0.5

LOGGED BY : 11-1-1

CHECKED BY

DATE 11-19-87

Digitized by srujanika@gmail.com



* U=THIN WALL S=SPLIT SPOON R=ROCK

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-108

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED 8/3/87 COMPLTD. 8/4/87

METHOD HSA/Cerine

GROUND EL 367-34

LOGGED BY T. Longley

卷之三

HNU TIP 10.6

PROTECTION LEVEL B C

FT BELOW GROUND 22.8

VER

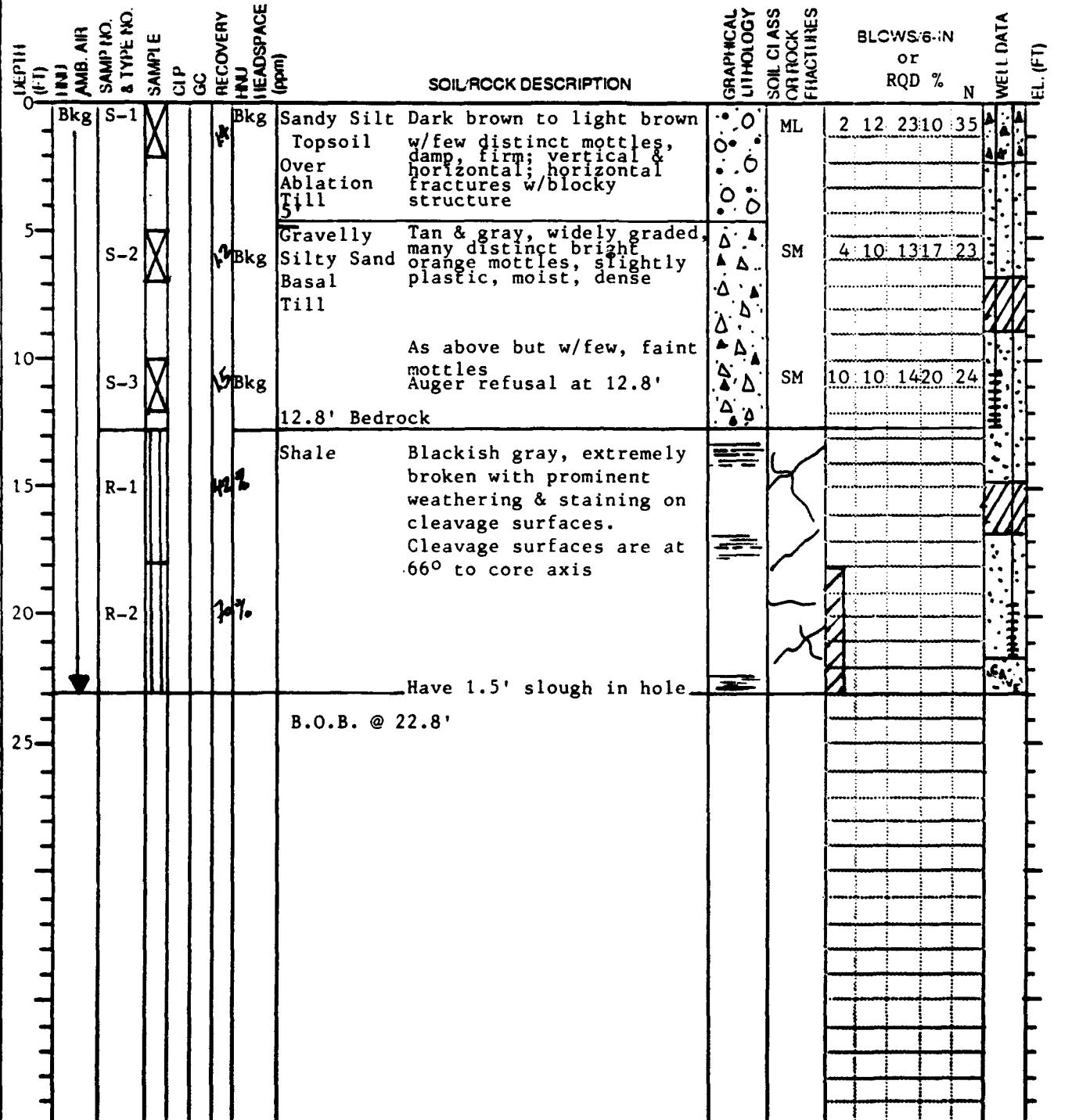
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W H A S S / C G R H E (P)

106

API

SCRIPTION



* = THIN WALL S = SPLIT SPOON R = ROCK

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. MW-108

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED

CCMPL LTD.

METHOD USA

CASING SIZE 4-25" T.D. HNU TIP 10.6

GROUND EL 368 34

SOIL DRILLED

508.54

12
CHECKED BY FEB

I. LONLEY

www.english-test.net

11-18-87

PROTECTION LEVEL B C D

DEPTHL
FT)
AMBIENT
AMB. AIR
SAMPLE
NO.
TYPE NO.
CLP
GC
RECOVERY
NJ
HEADSPACE
(ppm)

SOIL/ROCK DESCRIPTION

**GRAPHICAL
PHOTOLOGY
OIL CLASS
OR ROCK
STRUCTURES**

BLCS/6-N
or
RQD %

WELL DATA

0 Bkg S-1 X Bkg Silty Sand Brown, dry, loose, trace
Topsoil & gravel, roots at top
Till

5

Analytical Sample JMW1080701

10 S-2 X Y Silty Sand Brown, trace to little
Till gravel, moist to wet
firm, well graded w/few
distinct yellow mottles.
S-2 filled VOA jar, S-3
filled remaining jars

S-3 X Y

B.O.B. @ 12'

15

* LI-THIN WALL

[Silicon.com](http://www.silicon.com)

2 rock

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-109

CLIENT STEWART AIR NATIONAL GUARD BASE

PROJECT NO. 5139-01

CONTRACTOR EMPIRE SOILS INVESTIGATIONS

DATE STARTED 8/4/87 COMPLTD.

METHOD H.S.A./Saini et al.

B HNII TIP 1

PROTECTION LEVEL B C D

GROUND FL

ROCK DBII

FT. BELOW GROUND

LOGGED BY

DATE

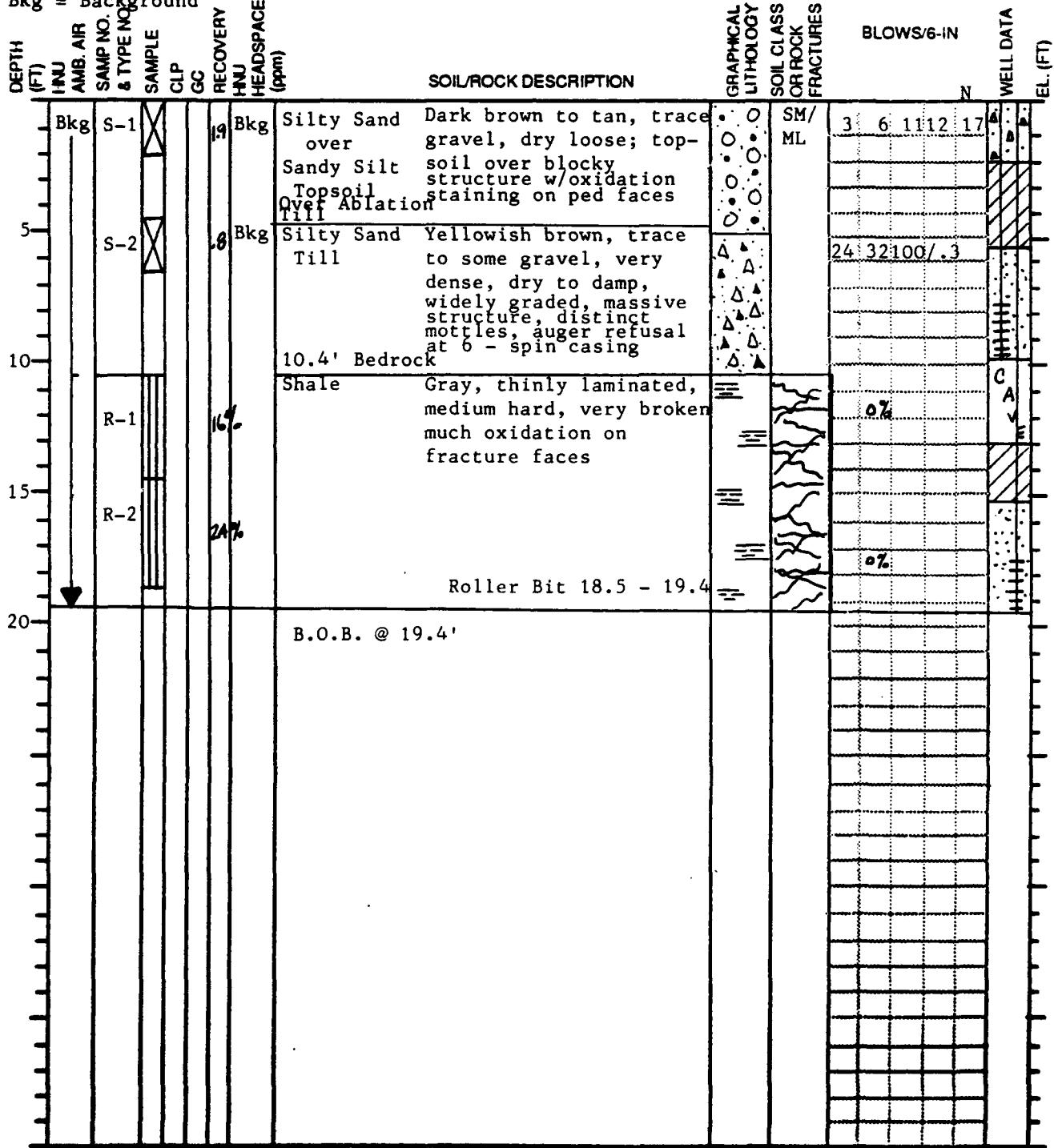
19.4

Bkg = Background

www 113

Digitized by srujanika@gmail.com

Bkg = Background
= 0



* U. S. TIN WALL

the next screen

4-rock

L.E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM								BORING NO. MW-109			
CLIENT STEWART AIR NATIONAL GUARD BASE								PROJECT NO. 5139-01			
CONTRACTOR EMPIRE SOILS INVESTIGATIONS				DATE STARTED		COMPLTD.					
METHOD Spin casing		CASING SIZE 4" I.D.		HNU TIP 10.6		PROTECTION LEVEL B C D					
GROUND EL 372.02		SOIL DRILLED 11'		ROCK DRILLED NA		FT BELOW GROUND 11.0					
LOGGED BY T. Longley		CHECKED BY FFB		DATE 11-10-87							
Bkg - Background											
DEPTH (FT)	HNU AMB. AIR	SAMP NO. & TYPE NO.	SAMPLE	CLP GC	RECOVERY HNU HEADSPACE (ppm)	SOIL/ROCK DESCRIPTION	GRAPHICAL LITHOLOGY	SOIL CLASS OR ROCK FRACTION	BLOWS/6-IN or RQD %		
Bkg	S-1			.9	Bkg 1.0	Silty Fine Sand Topsoil & Till	Dark brown topsoil w/ roots, moist, firm over grayish brown silty fine sand w/trace to little gravel, dry, dense w/many distinct orange mottles	SM	7 9 21 32 30		
5	S-2			1.4	Bkg 2.0	Silty Sand Till	Olive brown (sand is fine to coarse) well graded, dense moist; gravel zone at 6'; many distinct reddish brown mottles	SM	12 31 24 11 55		
10	S-3					Silty Sand & Weathered Rock	Yellowish brown gravelly well graded, trace clay moist, dense, over black & brown weathered shale, prom. ox., dense moist, trace clay	SM	12 14 19 20 33		
						Bedrock					
						B.O.B. @ 11'					
15											

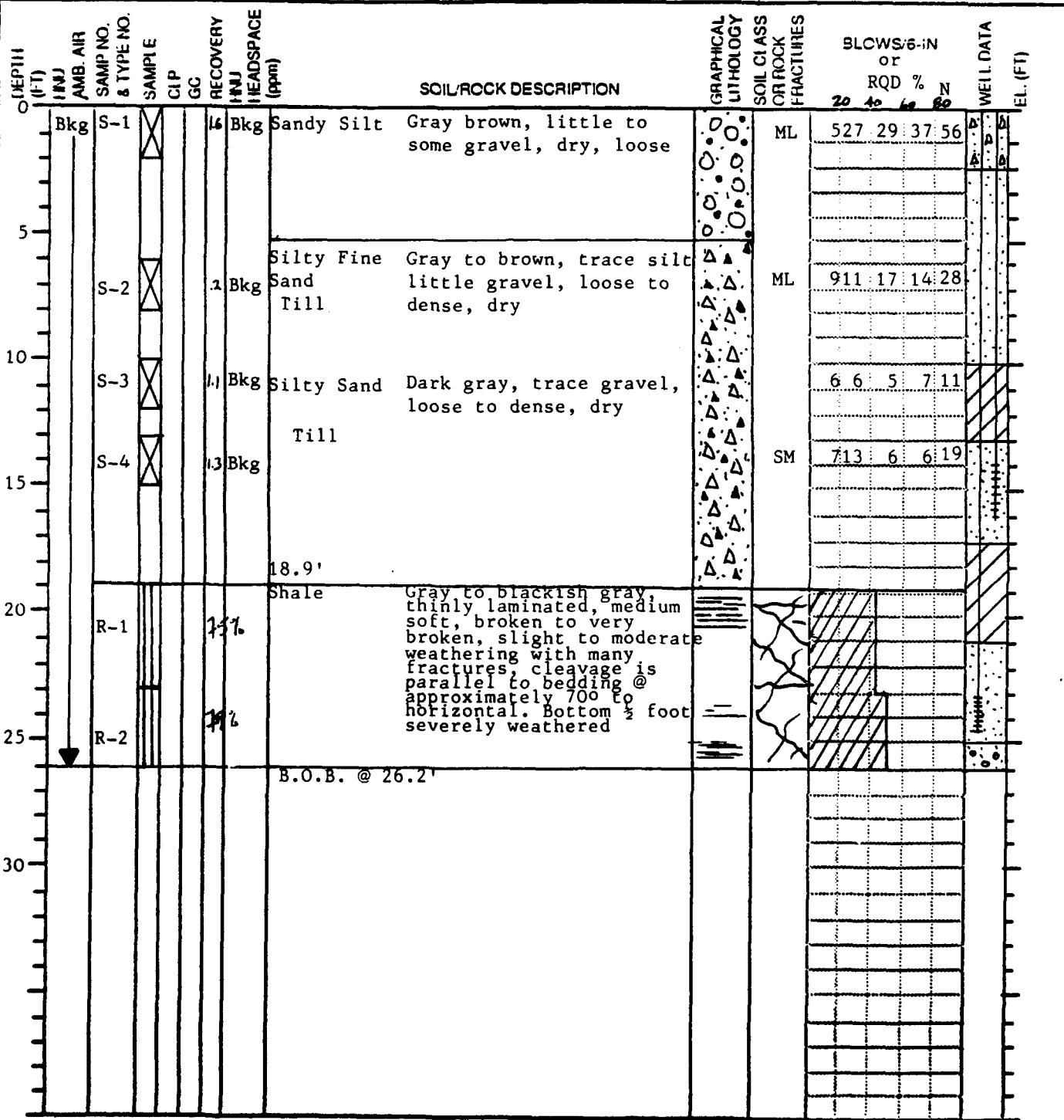
* U=THIN WALL S=SPLIT SPOON R=ROCK

E.C. JORDAN CO.

INSTALLATION RESTORATION PROGRAM

BORING NO. JTB-110

CLIENT	STEWART AIR NATIONAL GUARD BASE	PROJECT NO.	5139-01
CONTRACTOR	EMPIRE SOILS INVESTIGATIONS	DATE STARTED	7/29/87 CCMPLTD. 7/29/87
METHOD	HSA	CASING SIZE	4½"
GROUND EL	361.34	SOIL DRILLED	18.9'
LOGGED BY	J. Urquhart	CHECKED BY	FFB
DATE	11-10-87		



* U=THIN WALL S=SPLIT SPOON R=ROCK

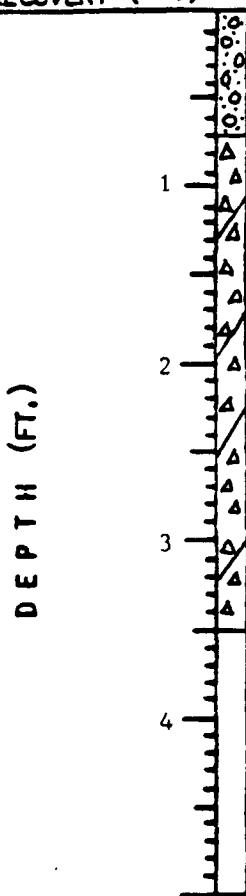
E.C. JORDAN CO.

APPENDIX B-2
ROCK CORE LOGS

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 2

Project No.	5139-01	Project Name	Stewart ANGB		Boring No.	JTB-101
Logged By	S. Pinette	Date	8-6-87		Protection Level	D
Core Diameter	NX ($\approx 2"$)	Core Run No.	R-1			Depth 37.0 ft to 41.5 ft. (4.5)
Core Recovery	3.5 ft.	RQD	0 %	Core Quality Very poor		

CORE RECOVERY (FT.).3 FT.
CORE RECOVERY

Soil - Till

Highly broken and
FracturedROCK DESCRIPTION AND IDENTIFICATION

Upper 0.7' (37.0'-37.7') is olive grey till mixed with medium grey shale fragments.

remainder of core is medium grey shale; well cleaved; cleavage planes stained rusty brown and medium greenish brown; cleavage oriented at 45° to core axis. Only 4 pieces of core are at least 1" in diameter.

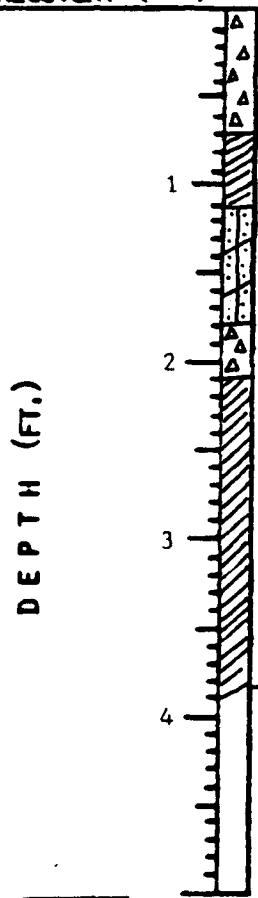
End of Core

770

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-101
Logged By S. Pinette	Date 8-7-87	Protection Level D
Core Diameter NX ($\approx 2"$)	Core Run No. R-2	Depth 41.5 ft to 46.5 ft. (5)
Core Recovery 3.9 ft.	RQD 36 %	Core Quality Poor to fair

CORE RECOVERY (FT.)TOTAL 3.9 (5.0).3 FT. CORE RECOVERY

Feldspathic Sandstone

End of Core

TOTAL 1.8 (5.0)7836ROCK DESCRIPTION AND IDENTIFICATION

Shale - predominantly medium grey, closely cleaved; cleavage plane oriented at 45° to core axis; cleavage surface stained medium greenish brown and, in frequently, rusty brown (goethite); vertical joint (parallel to core axis) discontinuous (0.1') in shale

Feldspathic Sandstone --
0.7' bed interbedded with shale
(42.6' to 43.3') fine grain, light grey/tan color; laminated parallel to cleavage in shale; relatively massive

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 1

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-102
Logged By J. Urquhart	Date 8-12-87	Protection Level D
Core Diameter Roller Bit 3.5"	Core Run No.	Depth 51.6 ft to 61.6 ft.
Core Recovery 0* ft.	RQD 0 %	Core Quality

*No rock core made - hole advanced into rock with
tri-cone roller bit.

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

DEPTH (FT.)



TOTAL () TOTAL ()

ECJORDANCO

VISUAL IDENTIFICATION OF ROCK CORES

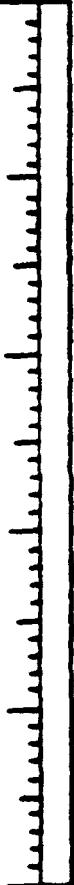
SHEET 1 OF 1

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-103
Logged By T. Longley	Date 8-14-87	Protection Level D
Core Diameter Roller Bit 3.5"	Core Run No. --	Depth 43 ft to 51.4 ft.
Core Recovery 0* ft.	RQD 0 %	Core Quality

*No rock core made - hole advanced into rock with
tri-cone roller bit.

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

DEPTH (FT.)

TOTAL () TOTAL ()

EC.JORDANCO

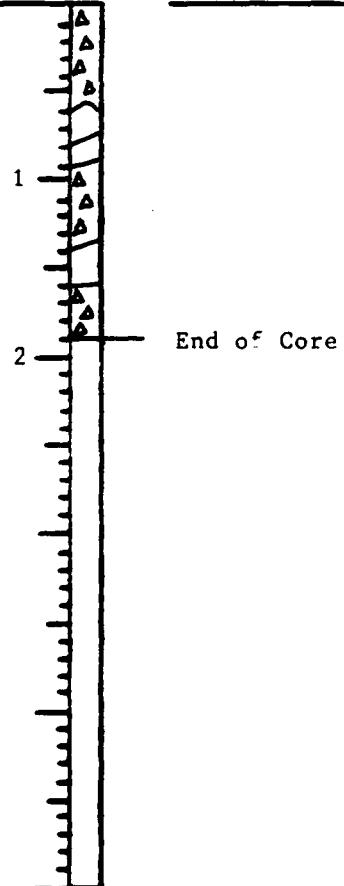
VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-104
Logged By T. Longley	Date 8-11-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-1	Depth 27 ft to 30.5 ft. (3.5)
Core Recovery 1.9 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERY

DEPTH (FT.)

TOTAL 1.9 (3.5)TOTAL 0 (3.5)540ROCK DESCRIPTION AND IDENTIFICATION

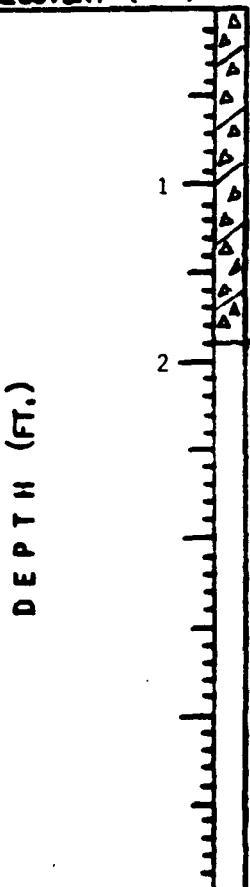
Black to grayish black shale, highly fractured and broken with numerous interconnecting, randomly oriented joints and open fractures. No one piece is as large as 4"; most are less than 2". Weathering of fractures is moderately fresh, especially near 30', which has moderate staining and distinct FeO and Mn O₂ staining on fracture faces. No distinct layering or foliation

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VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-104
Logged By T. Longley	Date 8-12-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-2	Depth 30.5 ft to 32.5 ft. (2')
Core Recovery 1.9 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT. CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Same rock type as in R-1 - highly fractured and broken shale, common joints and fractures, few open $\frac{1}{2}$ " in size; top of run is extremely broken and pebbly, bottom $\frac{1}{2}$ ' of recovered core is severely weathered rock (prevented penetration and caused core block), very (soil-like) weak and crumbly; one rock piece shows bedding at 55° to long core axis; FeO & MnO₂ is faint to distinct throughout core

Some fragments exhibit highly sheared and rehealed rock.

Thin interbedded layers of feldspathic sandstone

TOTAL 1.9 (2)TOTAL 0' (2')95%0 %

EC.JORDANCO

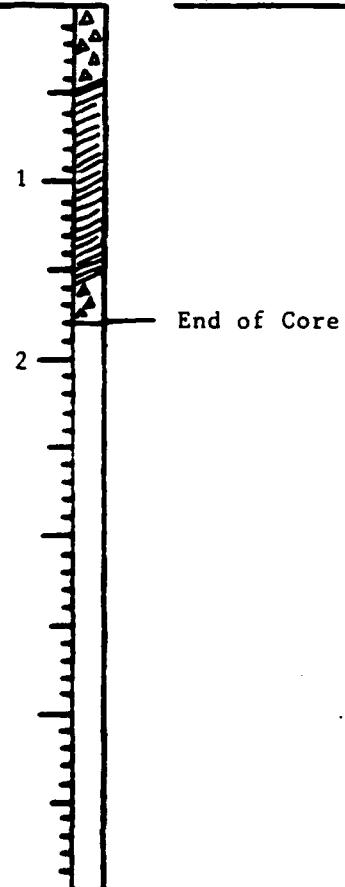
VISUAL IDENTIFICATION OF ROCK CORES

SHEET 3 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-104
Logged By T. Longley	Date 8-12-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-3	Depth 32.5 ft to 34.3 ft. (1.8')
Core Recovery 1.8 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERY

DEPTH (FT.)

TOTAL 1.5 (1.8) TOTAL 0 (1.8)83 0ROCK DESCRIPTION AND IDENTIFICATIONShale

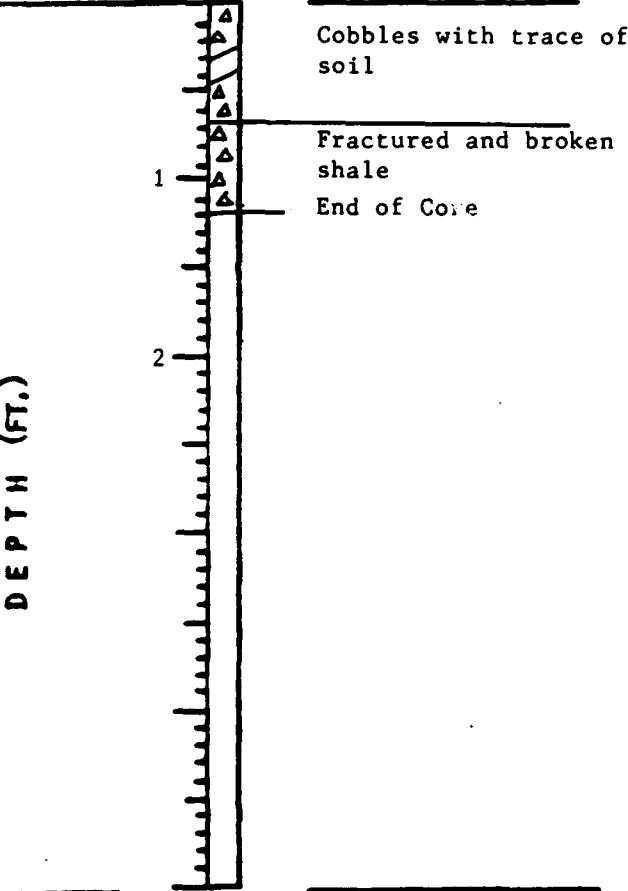
Same as above; extremely fractured and broken, crumbly, very weak, moderate to severe weathering; no piece of core longer than 1". Top of recovery is slough from soil zone - pebbles and gravel

Core recovery is very subjective due to the poor rock quality

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 1

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-105
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-3*	Depth 25.6 ft to 27.9 ft. (2.3)
Core Recovery 1.2 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale - medium grey colored; closely spaced cleaved planes are well developed and stained medium brown (FeO/MnO); cleavage and stratification are parallel and oriented at 26° with respect to core axis; trace calcite pedes and veinlets occur throughout, oriented both parallel and transverse to bedding/cleavage

Note: Majority of core breaks occur along cleavage planes; no joints evident in this run

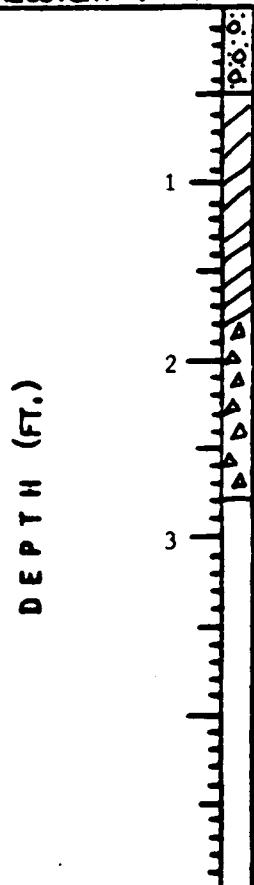
*R-1 and R-2 in soil only

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VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-106
Logged By S. Pinette	Date 8-3-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-1	Depth 19.5 ft to 23.0 ft. (3.5)
Core Recovery 2.3 ft.	RQD 9 %	Core Quality Poor

CORE RECOVERY (FT.)3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

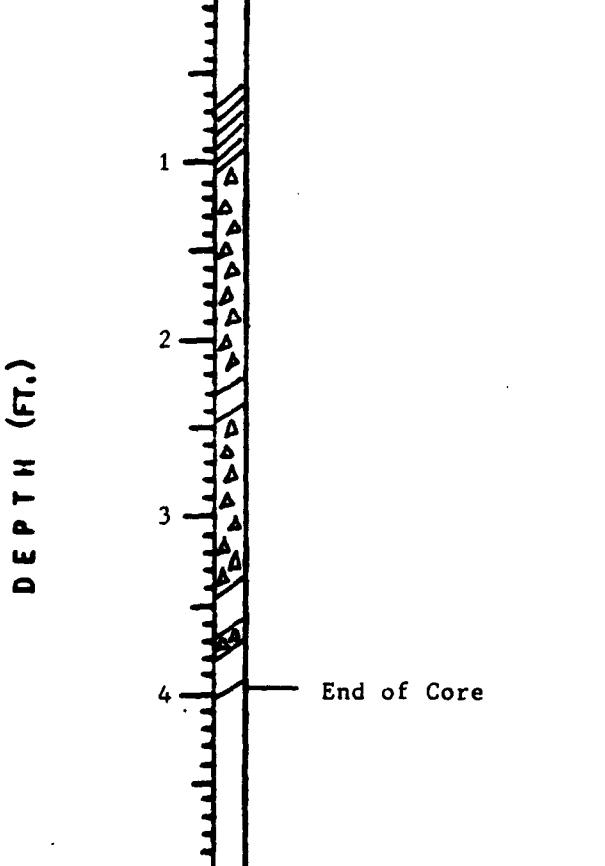
Shale - Medium grey colored; closely spaced cleaved planes are well developed and stained medium brown (FeO/MnO); cleavage and stratification are parallel and oriented at 40-50° with respect to core axis; trace calcite peds and veinlets occur throughout, oriented both parallel and transverse to bedding/cleavage

Note: Majority of core breaks occur along cleavage planes; no joints evident in this run

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-106
Logged By S. Pinette	Date 8-4-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-2	Depth 23.0 ft to 27.0 ft. (4.0)
Core Recovery 4.0 ft.	RQD 18 %	Core Quality Fair to poor

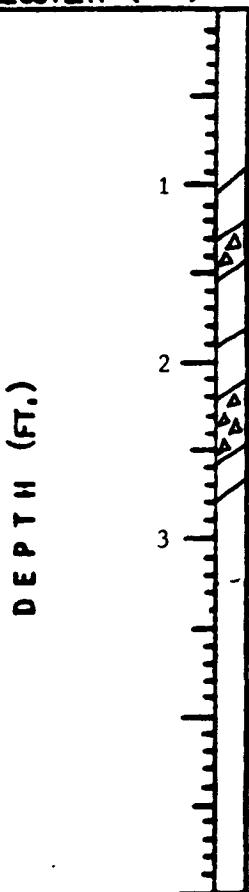
CORE RECOVERY (FT.).3 FT.
CORE RECOVERYTOTAL 4.0 (4.0)TOTAL 0.7 (4)10018ROCK DESCRIPTION AND IDENTIFICATION

Shale - essentially same as described for R-1; discontinuous, poorly developed joints present; oriented 90° to cleavage plane; joint surface stained iron-oxide (geothite) rusty yellowish brown color which is distinct from stain on cleavage surfaces; joints are relatively sparse

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 3 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-106
Logged By S. Pinette	Date 8-4-87	Protection Level D
Core Diameter NX (2")	Core Run No. R-3	Depth 27.0 ft to 30.0 ft. (3.0)
Core Recovery 2.8 ft.	RQD 78 %	Core Quality Good

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

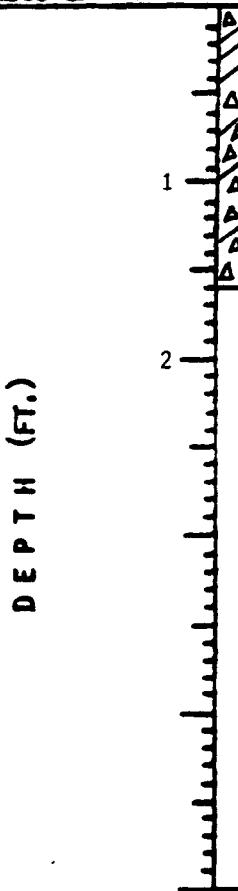
Shale as described in R-2 above; joints are more abundant and slightly better developed than in R-2; joints spaces as closely as 1 inch in some core sections

100% 78%

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-107
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-1	Depth 10 ft to 14 ft. (4)
Core Recovery 1.6 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale

gray shale

highly fractured and broken
slicken sides throughout
reddish brown to yellowish stain
on most all surfaces

DEPTH (FT.)

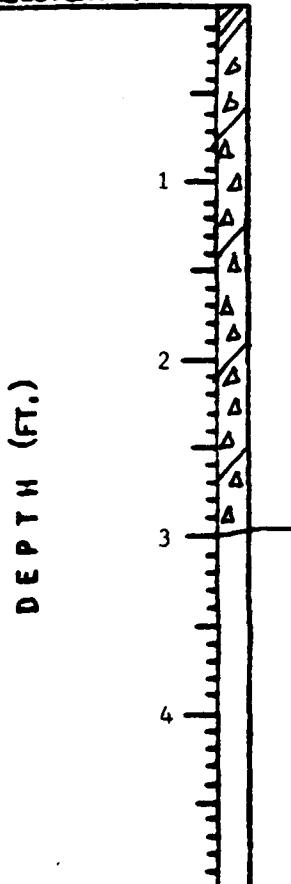
TOTAL 1.6 (4)TOTAL 0 (4)400

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VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-107
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX (2")	Core Run No. R-2	Depth 14 ft to 17 ft. (3')
Core Recovery 4' ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale - Gray, thinly laminated medium-hard, highly fractured and broken, slight to moderate weathering staining on all fracture surfaces

Cleavage is 36° to core axis and is // to bedding lineation

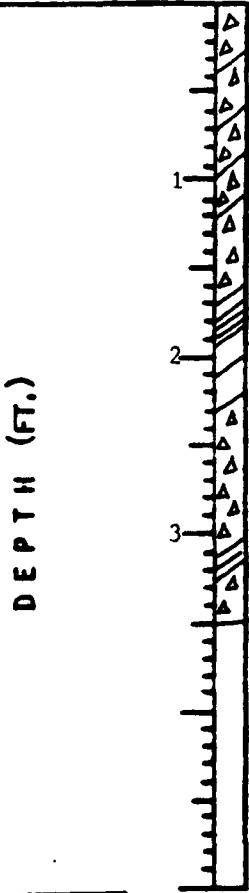
TOTAL 4 (4)TOTAL 0 (3)1000

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VISUAL IDENTIFICATION OF ROCK CORES

SHEET 3 OF 3

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-107
Logged By T. Longley	Date 8-20-87	Protection Level D
Core Diameter NX (\approx 2")	Core Run No. R-3	Depth 17 ft to 19.3 ft. (2.3)
Core Recovery 3.5 ft.*	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT. CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale - Same as R-1 and R-2

TOTAL 3.5 (2.3)TOTAL 0 (2.3)100 *0 *

*R-3 recovered some of the broken fragments from R-2

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-108
Logged By T. Longley	Date 8-20-87	Protection Level D
Core Diameter NX (2")	Core Run No. R-1	Depth 12.8 ft to 17.8 ft. (5)
Core Recovery 1.4 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale - gray to blackish gray thinly laminated medium soft to medium hard with depth, highly fractured and broken, medium weathering at top to slight with depth

DEPTH (FT.)

.3 FT.
CORE RECOVERY

End of Core

Cleavage 50° to long axis

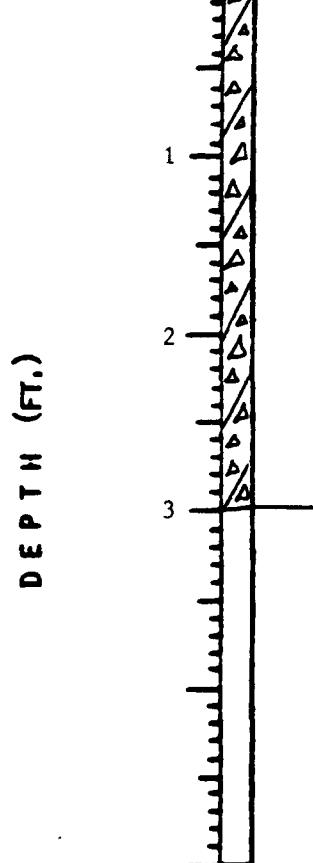
TOTAL 1.4' (5)TOTAL 0 (5)280

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VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-108
Logged By T. Longley	Date 8-20-87	Protection Level D
Core Diameter NX 42"	Core Run No. R-2	Depth 17.8 ft to 22.8 ft. (5)
Core Recovery 3.0 ft.	RQD 14 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYTOTAL 3 () TOTAL .7 (5)6014ROCK DESCRIPTION AND IDENTIFICATION

Shale - blackish gray to black
thinly laminated, medium hard to
hard, fresh to slight weathering
highly fractured and broken

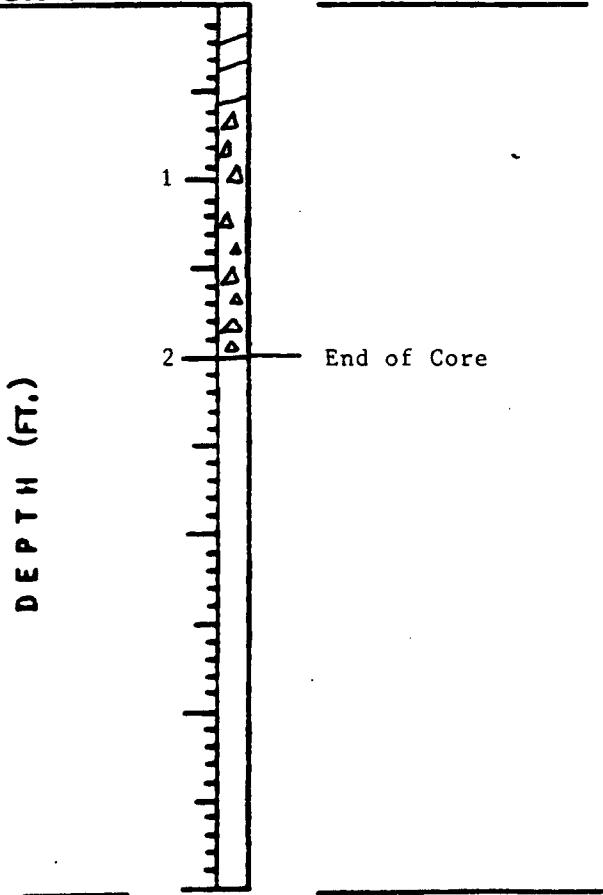
Cleavage is // to laminations and at
45° to long axis

Trace of disseminated pyrite

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-109
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX (#2")	Core Run No. R-1	Depth 10 ft to 14.3 ft. (4.3')
Core Recovery 2.0 ft.	RQD 0 %	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYTOTAL 2.0 (4.3)TOTAL 0 (4.3)470ROCK DESCRIPTION AND IDENTIFICATION

Shale - gray, thinly laminated, medium hard, highly fractured and broken, fresh to slight weathering

Can't measure Δ 's at all due to broken nature of rock

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-109
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX 42"	Core Run No. R-2	Depth 14.3 ft to 18.5 ft. (4.2)
Core Recovery 1.8 ft.	RQD 0%	Core Quality Very poor

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATION

Shale same as above - recovered very short pieces but these show more weathering on all fracture faces

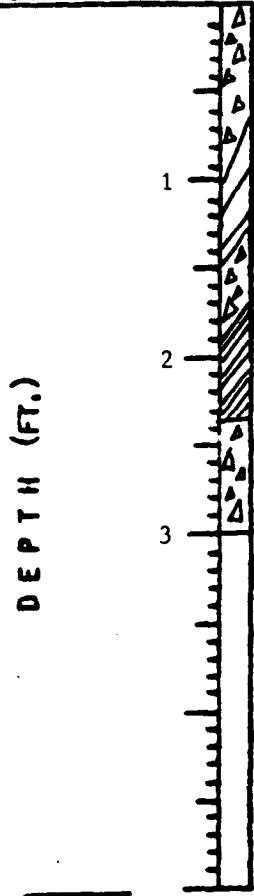
DEPTH (FT.)

TOTAL 1.8 (4.2)TOTAL 0 (4.2)430

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 1 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-110
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX 42"	Core Run No. R-1	Depth 18.9 ft to 22.9 ft. (4')
Core Recovery 3 ft.	RQD 42 %	Core Quality Fair

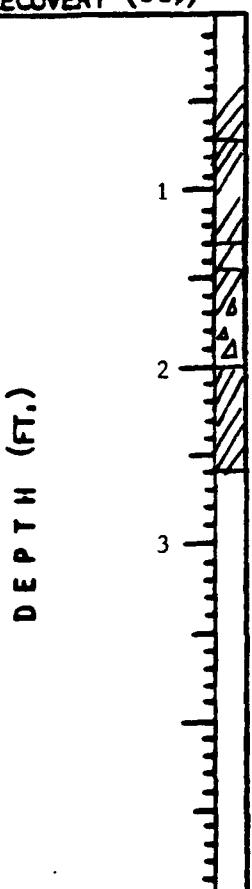
CORE RECOVERY (FT.).3 FT.
CORE RECOVERYTOTAL 3' (4')TOTAL 20" (48")7562ROCK DESCRIPTION AND IDENTIFICATION

Shale - gray to blackish gray, thinly laminated, medium soft, moderately fractured and broken, 42% RQD, slight to moderate weathering with many fractures showing bright oxidation staining.
 Cleavage is // to bedding and at 20° to core axis.
 Few fractures up to 60° to axis
 Few open vugs
 Very crumbly at bottom of run

VISUAL IDENTIFICATION OF ROCK CORES

SHEET 2 OF 2

Project No. 5139-01	Project Name Stewart ANGB	Boring No. JTB-110
Logged By T. Longley	Date 8-19-87	Protection Level D
Core Diameter NX 42"	Core Run No. R-2	Depth 22.9 ft to 26.2 ft. (3.3')
Core Recovery 2.6 ft.	RQD 52 %	Core Quality Fair

CORE RECOVERY (FT.).3 FT.
CORE RECOVERYROCK DESCRIPTION AND IDENTIFICATIONShale - As above but less fractured

Last 9" of core is severely weathered along fracture faces

End c. Core

DEPTH (FT.)

TOTAL 2.6 (3.3)TOTAL 1.7 (3.3)79%52%

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APPENDIX B-3

MONITORING WELL INSTALLATION SHEETS

SITE Stewart ANGB

JOB NO. 5139-01

MONITORING WELL DESIGNATION JMW-101

INSTALLATION DATE 8/3/87

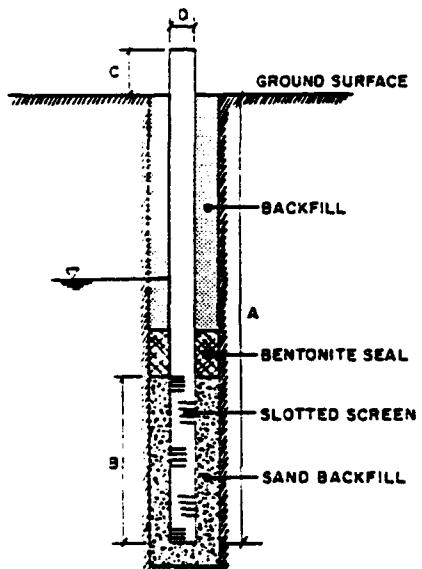
DIAMETER OF WELL 0.166'

MATERIAL SCH 40 PVC

LOCKING PROTECTIVE COVER YES NO

ECJ DRILLER DEVELOPED YES NO

WELL CONSTRUCTION



A = 32.75'

NOTES

10' SCREEN LENGTH

B = 12.0'

C = 2.41 CASING

D = 0.166'

WATER LEVEL RANGE 31.44

ELEVATION OF WELL AT GRADE _____

GROUNDWATER INFORMATION

APPROXIMATE RECHARGE/YIELD _____

WELL SCREEN POSITIONED IN TILL
(i.e. till, clay, rock)

GROUNDWATER MONITORING/SAMPLING DATA

RECOMMENDED TYPE OF EQUIPMENT TO FLUSH WELL _____

RECOMMENDED AMOUNT OF FLUSHING _____

SAMPLING PROCEDURES

SITE Stewart ANGB

JOB NO. 5139-01

MONITORING WELL DESIGNATION JMW - 107

INSTALLATION DATE 8/3/87

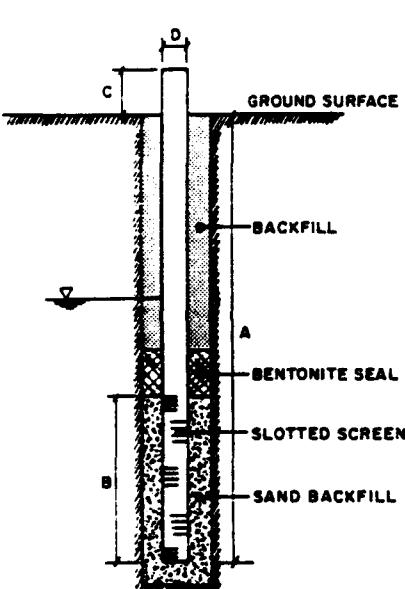
DIAMETER OF WELL 0.166 FT

MATERIAL SCH. 40 PVC; 0.010" SLOTTED SCREEN

LOCKING PROTECTIVE COVER YES NO

DRILLER DEVELOPED YES NO

WELL CONSTRUCTION



A = 9.38'

NOTES

5' SCREEN LENGTH

B = 7.0'

C = 3.25' CASING

D = 0.166'

WATER LEVEL RANGE 10.25 - 10.55

ELEVATION OF WELL AT GRADE _____

GROUNDWATER INFORMATION

APPROXIMATE RECHARGE / YIELD _____

WELL SCREEN POSITIONED IN TILL
(i.e. till, clay, rock)

GROUNDWATER MONITORING/SAMPLING DATA

RECOMMENDED TYPE OF EQUIPMENT TO FLUSH WELL _____

RECOMMENDED AMOUNT OF FLUSHING _____

SAMPLING PROCEDURES

SITE Stewart ANGB

JOB NO. 5139-01

MONITORING WELL DESIGNATION MW - 108

INSTALLATION DATE 8/4/87

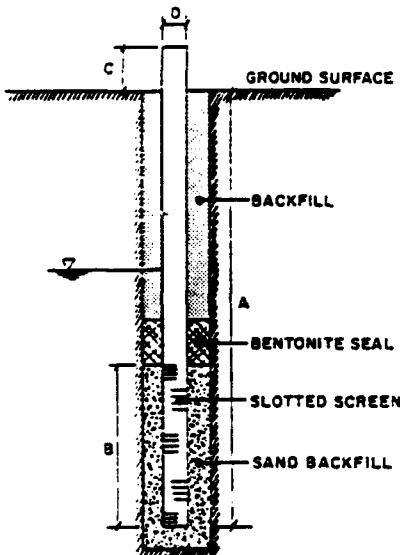
DIAMETER OF WELL 0.166 FT

MATERIAL sch. 40 PVC; 0.010" SLOT SIZE SCREEN

LOCKING PROTECTIVE COVER YES NO

ECI DRILLER DEVELOPED YES NO

WELL CONSTRUCTION



A = 10.97'

NOTES

5' SCREEN LENGTH

B = 7.0'

C = 2.59' CASING

D = 0.166'

WATER LEVEL RANGE 8.5 - 8.7

ELEVATION OF WELL AT GRADE _____

GROUNDWATER INFORMATION

APPROXIMATE RECHARGE/YIELD _____

WELL SCREEN POSITIONED IN TILL
(i.e. till, clay, rock)

GROUNDWATER MONITORING/SAMPLING DATA

RECOMMENDED TYPE OF EQUIPMENT TO FLUSH WELL _____

RECOMMENDED AMOUNT OF FLUSHING _____

SAMPLING PROCEDURES

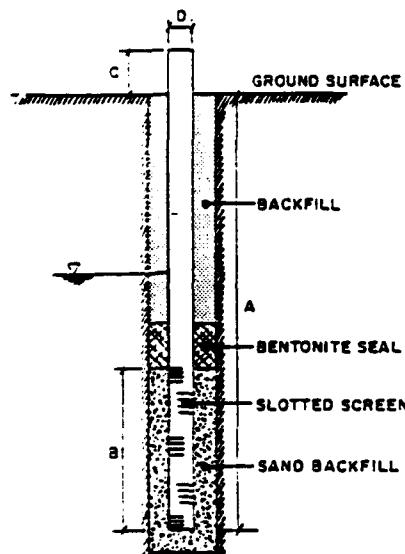
SITE Stewart ANGB JOB NO. 5139-01

MONITORING WELL DESIGNATION JMW - 109 INSTALLATION DATE 8/6/87

DIAMETER OF WELL 0.166' MATERIAL sch. 40 PVC ; 0.010 SLOT SIZE SCREEN

LOCKING PROTECTIVE COVER YES NO DRILLER DEVELOPED YES NO

WELL CONSTRUCTION



A = 10.25' NOTES

B = 7.0' 5' SCREEN LENGTH

C = 2.45' CASING

D = 0.166'

WATER LEVEL RANGE 10.05 - 10.12

ELEVATION OF WELL AT GRADE _____

GROUNDWATER INFORMATION

APPROXIMATE RECHARGE/YIELD _____

WELL SCREEN POSITIONED IN TILL
(i.e. till, clay, rock)

GROUNDWATER MONITORING/SAMPLING DATA

RECOMMENDED TYPE OF EQUIPMENT TO FLUSH WELL _____

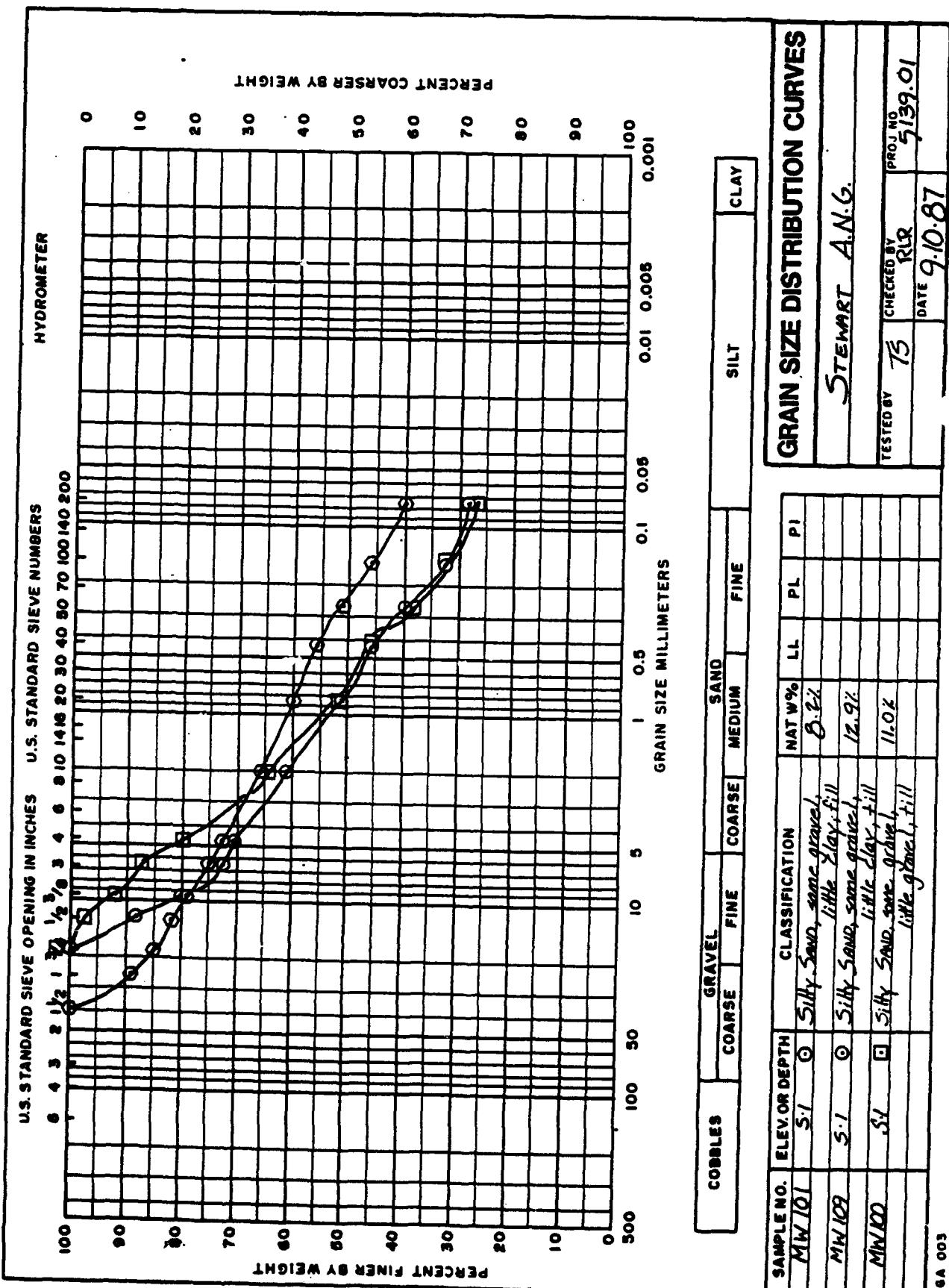
RECOMMENDED AMOUNT OF FLUSHING _____

SAMPLING PROCEDURES

APPENDIX C
LABORATORY DATA

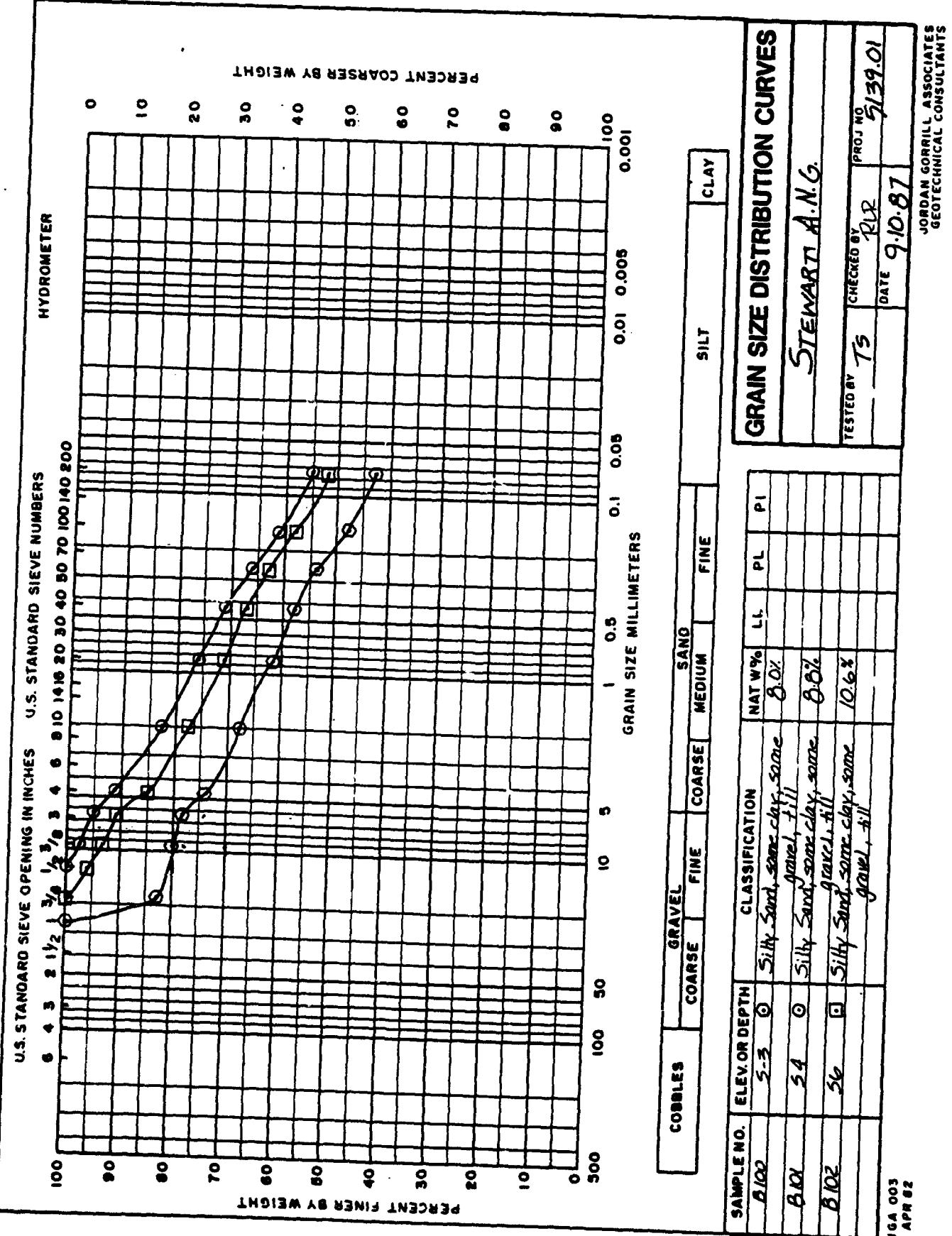
C-1 GRAIN-SIZE DISTRIBUTION CURVES
C-2 SIEVE ANALYSIS DATA

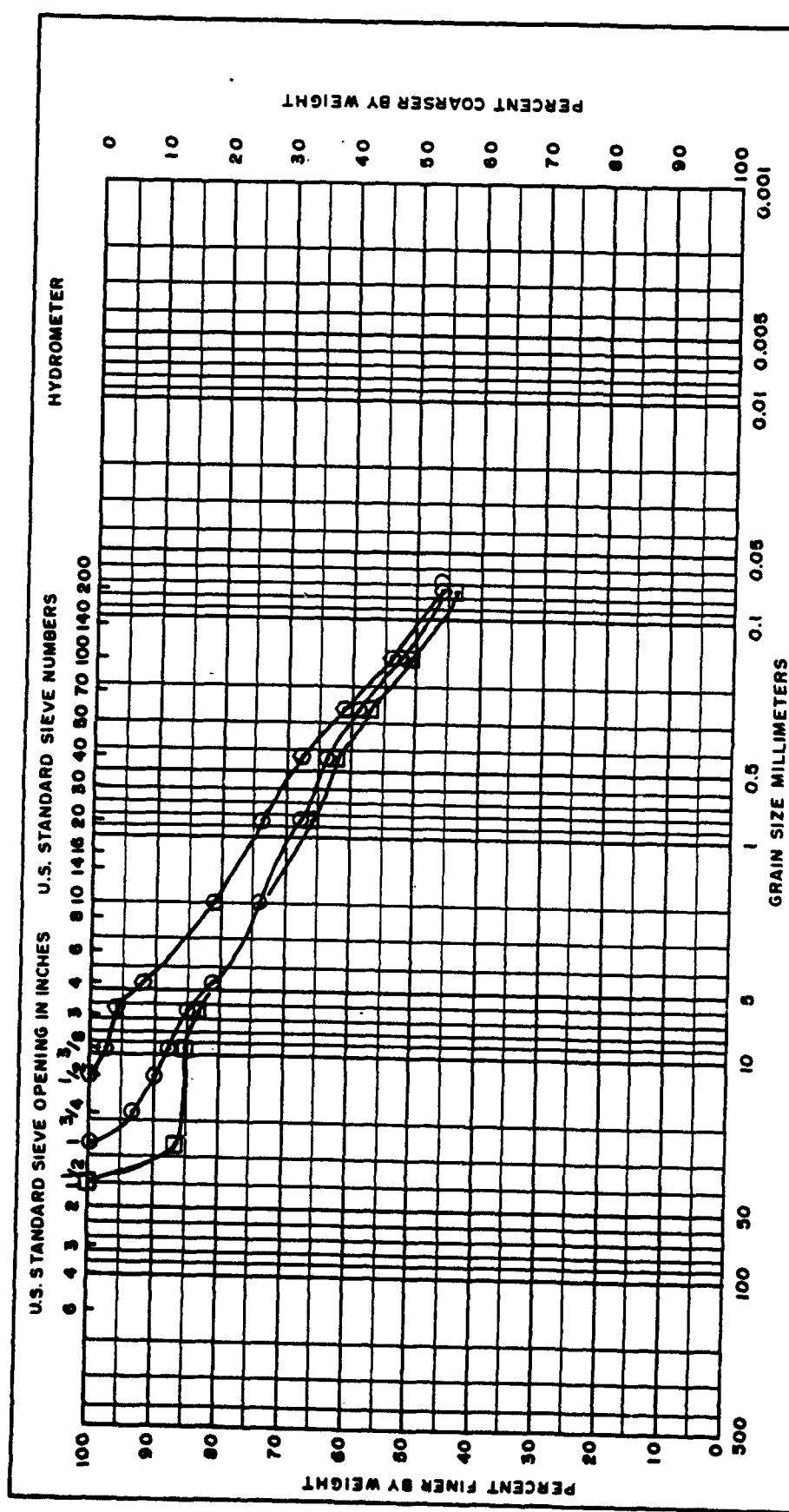
APPENDIX C-1
GRAIN-SIZE DISTRIBUTION CURVES



SAMPLE NO.	ELEV. OR DEPTH	CLASSIFICATION	NAT W%	LL	PL	PI
MW 101	S.I.	○ Silty Sand, some gravel,	8.2%			
MW 102	S.I.	○ Silty Sand, little clay, fill				
MW 103	S.I.	□ Silty Sand, some gravel, little clay, fill	12.9%			

JGA 003
1 APR 82



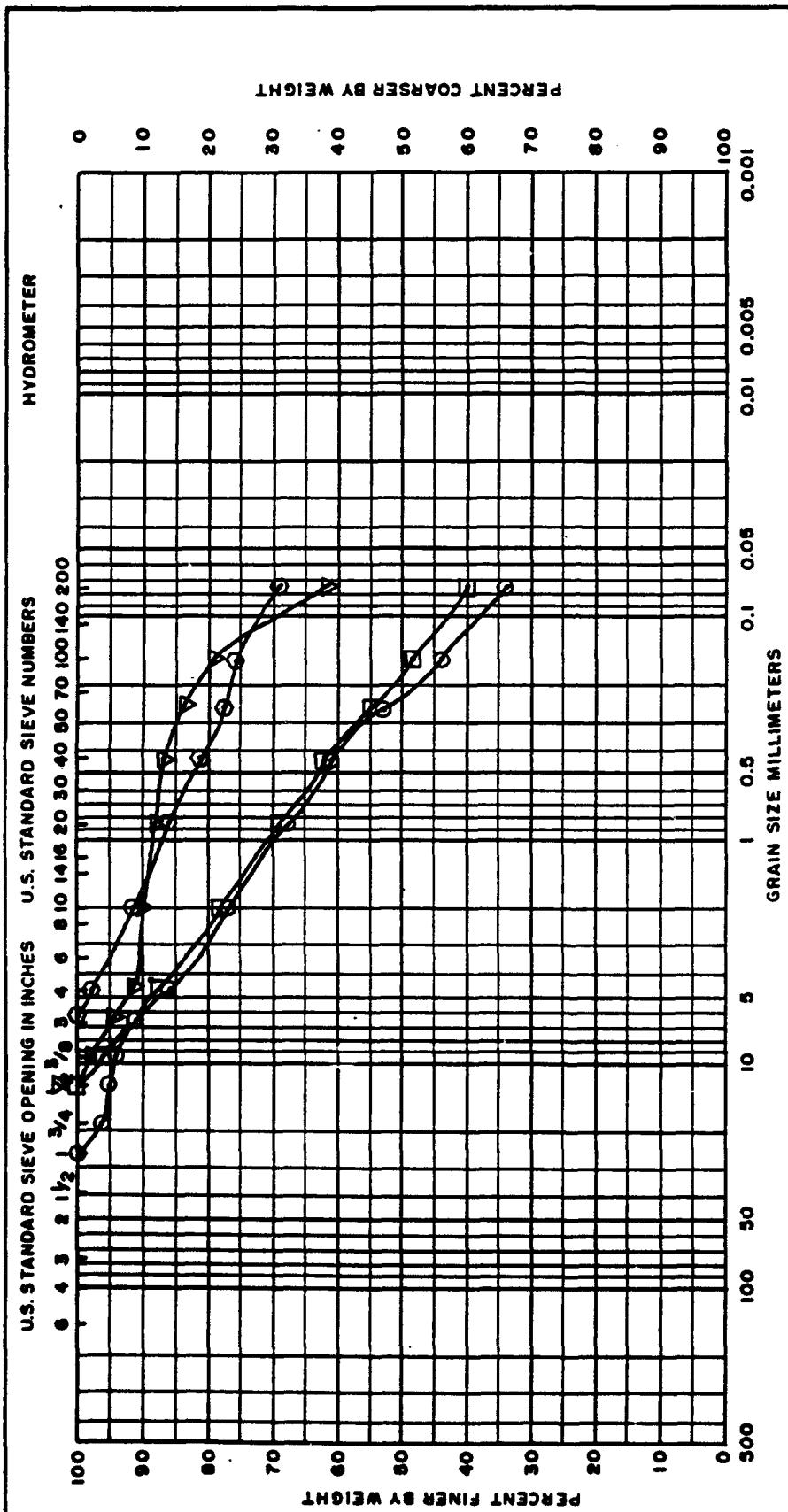


COBBLES	GRAVEL			SAND			CLAY
	COARSE	FINE	COARSE	MEEDIUM	FINE	SILT	

SAMPLE NO.	ELEV. OR DEPTN	CLASSIFICATION	NAT. W%	L.L.	P.L.	P.I.
B103	52	Silt Sand, little clay, trace fine gravels	10.0%			
B103	57	Silt Sand, little clay, little fine gravels	9.1%			
B104	54	Silt Sand, little clay, little gravel	8.5%			

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JORDAN GORRIEL ASSOCIATES
GEOTECHNICAL CONSULTANTS



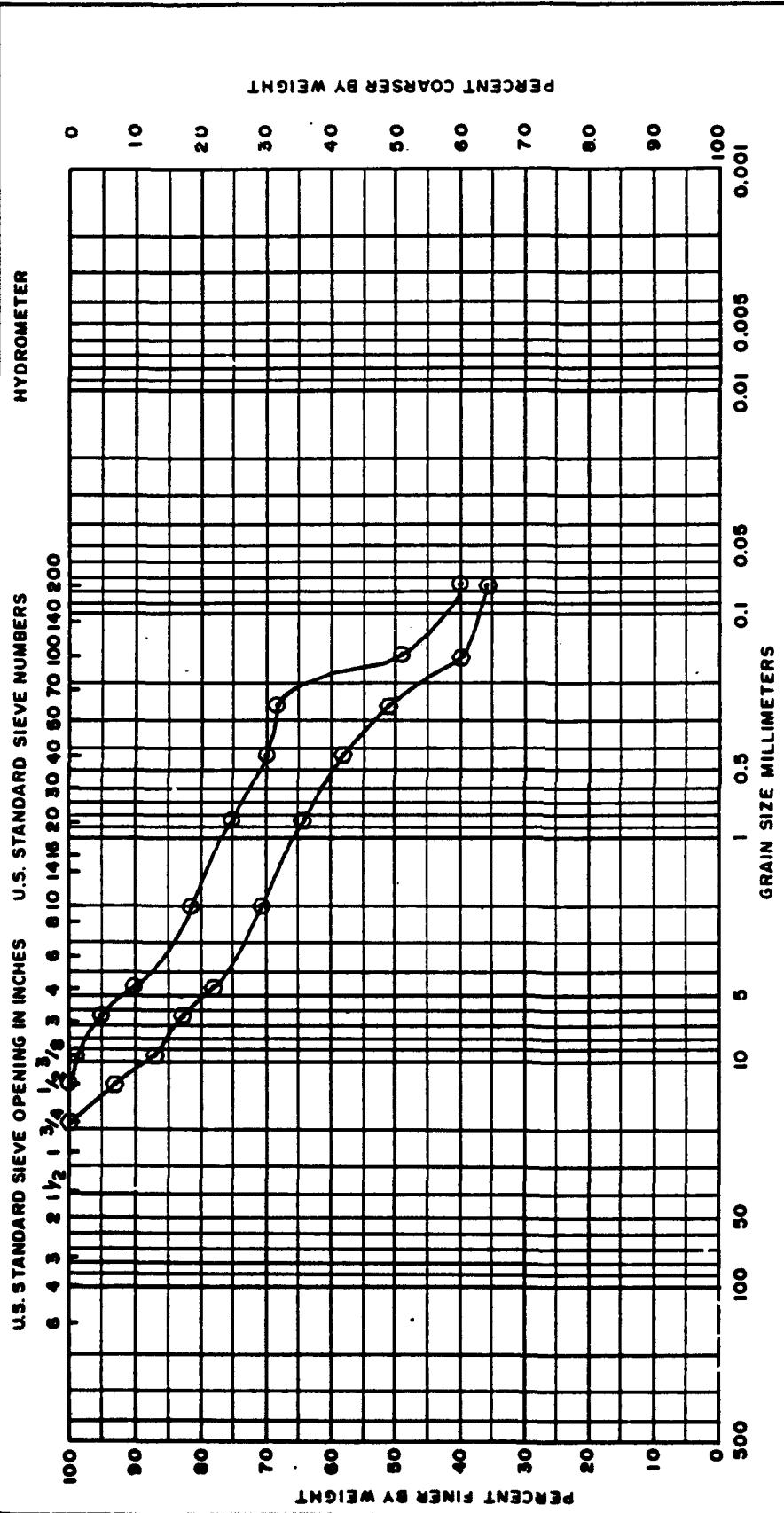
COBBLES	GRAVEL			SAND			SILT	CLAY
	COARSE	FINE	COARSE	MEEDIUM	FINE			

GRAIN SIZE DISTRIBUTION CURVES

S. STEWART ANS					
TESTED BY	DATE	PROJ NO	CHECKED BY	DATE	
B105	55	0	Silt and sand, stratified	13.6%	
B106	53	0	Sand, some silt, little gravel	12.2%	
B106	55	0	Silty sand, some clay, little gravel	13.2%	
B107	32	▽		17.2%	

JORDAN GORRIEL ASSOCIATES
GEOTECHNICAL CONSULTANTS

16A 003
MAP 82



GRAIN SIZE DISTRIBUTION CURVES

JORDAN GORRIK ASSOCIATES
GEOTECHNICAL CONSULTANTS

J6A 003
1 APR 82

APPENDIX C-2
SIEVE ANALYSIS DATA

"LEVEL D"
WATER CONTENT - GENERAL

PROJECT STEWART ANC DATE 9 3 37
JOB NO. 5139.31

BORING AND SAMPLE NO.		MW101 S1	MW109 S1	MW109 S3	B100 S3	B101-S4	B102 S6
WEIGHT IN GRAMS	TARE NO.	34	106	75	53	50	5
	TARE PLUS WET SOIL	207.4	226.7	242.5	251.6	229.6	229.7
	TARE PLUS DRY SOIL	289.7	207.4	224.5	237.3	215.3	249.3
	WATER	w _w	17.7	19.3	18.0	14.3	4.3
	TARE		72.7	58.2	61.1	58.8	53.0
	DRY SOIL	w _s	217.0	149.2	163.4	178.5	162.5
	WATER CONTENT, %	w	8.2	12.9	11.0	8.0	10.6

SAMPLE DESCRIPTION

BORING AND SAMPLE NO.		B103 S2	B103 S7	B104 S4	B105 S5	B106 S3	B106 S5
WEIGHT IN GRAMS	TARE NO.	60	8	4	53	70	3
	TARE PLUS WET SOIL	279.8	234.8	261.8	183.3	222.1	263.3
	TARE PLUS DRY SOIL	259.1	221.1	245.4	167.3	224.1	236.6
	WATER	w _w	20.7	13.7	16.4	15.5	23.0
	TARE		52.5	52.1	53.4	53.7	58.6
	DRY SOIL	w _s	206.6	159.0	192.0	114.1	203.5
	WATER CONTENT, %	w	10.0	8.1	8.5	13.6	12.2

SAMPLE DESCRIPTION

BORING AND SAMPLE NO.		B107 S2	B103 S3	B110 S4			
WEIGHT IN GRAMS	TARE NO.	25	19	51			
	TARE PLUS WET SOIL	234.9	232.7	237.2			
	TARE PLUS DRY SOIL	210.5	213.8	215.3			
	WATER	w _w	24.4	18.9	21.9		
	TARE		68.7	55.7	52.8		
	DRY SOIL	w _s	141.8	158.1	162.5		
	WATER CONTENT, %	w	17.2	12.0	13.5		

SAMPLE DESCRIPTION

REMARKS high 17.2(B107) Low 8.0(B103) AVE = 11.2%

TECHNICIAN TS COMPUTED BY TS CHECKED BY TS

PROJECT

STEWART A.N.G.

COMP. BY TS

CHK. BY RLR

JOB NO 5130.01

DATE 7.31.87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING MW101 NUMBER S1 DEPTH

MOISTURE CONTENT

TARE NO 34 Wt. 72.7

SAMPLE+TARE, i 307.4

SAMPLE+TARE, f 289.7

SAMPLE, f 217.0

MOISTURE 17.7

% W_c 2.2

% OF FINES

TARE NO 34 Wt. 72.7

SAMPLE+TARE, i 289.7

SAMPLE+TARE, f 203.5

Wt. SOIL LOST 86.2

Wt. SOIL, i 217.0

% of FINES 39.7 /

HYDROMETER ANALYSIS

SAMPLE SIZE i

MENISCUS CORR (M)

DISP. AGENT

AMOUNT CORR(C_d)

	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
COARSE ANALYSIS	3					
	1½					
	1		23.4	10.8	89.2	
	¾		32.5	15.0	85.0	
	½		40.2	18.5	81.5	
	⅓		41.2	2.2	97.8	
	¼		55.3	25.6	74.4	
	4		58.3	27.1	72.9	
	PAN					
	Wt. i		Wt. f		% Loss	
FINE ANALYSIS	4					
	10		73.1	33.7	66.3	
	20		86.4	39.8	60.2	
	40		95.5	44.0	56.0	
	60		105.4	48.6	51.4	
	100		117.0	53.9	46.1	
	200		130.5	6.1	93.9	
	PAN		130.9	—	—	—
	Wt. i		Wt. f	% Loss	C.F.	

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √ L/T	% Finer	CORRECTED
	0								
	½								
	1								
	2								
	4								
	8								
	15								
	30								
	60								
	120								
	240								
	480								
	1440								

$$\% \text{ FINEER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \quad ((R - Cd + M) - 1) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

EQUICORDANCE

PROJECT

STEWART A.N.G

COMP. BY

CHK. BY

JOB NO

RLR

DATE 8-3-67

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING MW109 NUMBER S-1 DEPTH

<u>MOISTURE CONTENT</u>	
TARE NO	10.6
Wt.	58.2
SAMPLE + TARE, i	226.7
SAMPLE + TARE, f	207.4
SAMPLE, f	149.2
MOISTURE	19.3
% Wc	12.5

<u>% OF FINES</u>	
TARE NO	10.6
Wt.	58.2
SAMPLE + TARE, i	207.4
SAMPLE + TARE, f	165.2
Wt. SOIL LOST	42.2
Wt. SOIL, i	149.2
% of FINES	28.2 ³

<u>HYDROMETER ANALYSIS</u>	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT	CORR(Cd)

COARSE ANALYSIS	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
	3					
	1½					
	1					
	¾	18.0	2.1	95.5	5.5	
	½	19.6	13.1	51.5	51.5	
	⅜	30.3	22.5	74.5	25.5	
	¼	40.1	26.9	65.1	34.9	
	4	13.0	2.9	91.5	8.5	
	PAN					
FINE ANALYSIS	WT. i	WT. f		% LOSS		
	4		.	-		
	10	58.5	39.2	40.8	61	
	20	72.9	48.9	51.1	51	
	40	81.2	54.4	45.6	46	
	60	89.7	60.1	39.9	40	
	100	99.3	66.6	33.4	33	
	200	106.5	71.4	25.6	26	
	PAN	106.6	—	—	—	
WT. i		WT. f	% LOSS	C.F.		

TIME ΔT MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K $\sqrt{\frac{L}{T}}$ SIZE	% Finer	CORRECTED
0								
½								
1								
2								
4								
8								
15								
30								
60								
120								
240								
480								
1440								

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART ANC

COMP. BY TS

CHK. BY RLR

JOB NO 5139.61

DATE 8-31-67

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING MW109 NUMBER 5-3 DEPTH

MOISTURE CONTENT

TARE NO. 75 Wt. 61.1SAMPLE + TARE, i 242.5SAMPLE + TARE, f 242.5SAMPLE, f 182.4MOISTURE 12.0% W_c 12.0

% OF FINES

TARE NO. 75 Wt. 61.1SAMPLE + TARE, i 224.5SAMPLE + TARE, f 151.5Wt. SOIL LOST 43.0Wt. SOIL, i 163.4% of FINES 26.3'

HYDROMETER ANALYSIS

SAMPLE SIZE i _____

MENISCUS CORR (M) _____

DISP. AGENT _____

AMOUNT CORR(C_d) _____

SIEVE	Wt. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1½					
1					
¾					
½					
⅓					
¼					
4					
PAN			-		
	Wt. i	Wt. f		% Loss	
	4		-	-	
	10	59.1	36.2	53.5	64
	20	78.4	48.0	52.0	52
	40	90.3	55.3	44.7	45
	60	100.6	61.6	38.4	38
	100	110.1	67.4	32.6	33
	200	120.0	73.4	26.6	27
	PAN	120.2	73.6	-	-
	Wt. i	Wt. f	% Loss	C.F.	

TIME	ΔT	MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-C _d +M CALC	$d = K \sqrt{\frac{L}{T}}$	SIZE	% Finer	CORRECTED
	0										
	½										
	1										
	2										
	4										
	8										
	15										
	30										
	60										
	120										
	240										
	480										
	1440										

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - C_d + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART ANC

COMP. BY

CHK. BY

JOB NO

DATE

5/20/68

8-3-68

GRAIN SIZE ANALYSIS

SAMPLE I.D.: BORING 300 NUMBER S-3 DEPTH

MOISTURE CONTENT

TARE N^o 58 Wt. 58.8
 SAMPLE + TARE, i 251.6
 SAMPLE + TARE, f 237.3
 SAMPLE, f 178.5
 MOISTURE 14.3
 % W_c 3.0%

% OF FINES

TARE N^o 88 Wt. 58.8
 SAMPLE + TARE, i 237.3
 SAMPLE + TARE, f 160.6
 Wt. SOIL LOST 76.7
 Wt. SOIL, i 178.5
 % of FINES 43.0

HYDROMETER ANALYSIS

SAMPLE SIZE i
 MENISCUS CORR (M)
 DISP. AGENT
 AMOUNT CORR (C_d)

	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
COARSE ANALYSIS	3					
	1 1/2					
	1		-		100	100
	3/4	50.1		16.9	52.1	52.1
	1/2	-	-	-	-	-
	3/8	22.5		10.6	25.4	25.4
	1/4	38.5		21.6	73.4	73.4
	4	15.3		25.7	74.3	74.3
	PAN	-				
	Wt. i		Wt. f		% Loss	
FINE ANALYSIS	4		-		-	
	10	56.3		31.8	68.2	68
	20	67.3		37.7	62.3	62
	40	74.8		41.9	58.1	58
	60	82.8		46.4	53.6	52
	100	93.0		52.1	47.9	48
	200	102.0		57.1	42.9	43
	PAN	-				
	Wt. i		Wt. f		% Loss	
	C.F.					

TIME	AT MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-C _d +M CALC	d=K √ $\frac{L}{T}$ SIZE	% Finer	CORRECTED
	0								
	1/2								
	1								
	2								
	4								
	8								
	15								
	30								
	60								
	120								
	240								
	480								
	1440								

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_{s-1}} \right) \times \frac{100}{W_i} \left((R - C_d + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

EDGORDANCO

PROJECT

STEWART ANC

COMP. BY TS

JOB NO 5135.01

CHK. BY RLR

DATE 8-5-62

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING B 101 NUMBER 54 DEPTH

MOISTURE CONTENT

TARE N^o 56 Wt. 53.0

SAMPLE+TARE, i 229.6

SAMPLE+TARE, f 215.3

SAMPLE, f 162.3

MOISTURE 14.3

% W_c 5.3

% OF FINES

TARE N^o 56 Wt. 53.0

SAMPLE+TARE, i 215.3

SAMPLE+TARE, f 126.5

Wt. SOIL LOST 88.8

Wt. SOIL, i 162.3

% of FINES 54.7

HYDROMETER ANALYSIS

SAMPLE SIZE i

MENISCUS CORR (M)

DISP. AGENT

AMOUNT CORR(C_d)

	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
COARSE ANALYSIS	3					
	1½					
	1					
	¾					
	½			0	100	100
	3/8		3.2	2.0%	98	98
	1/4		5.7	5.5	94.5	95
	4		14.8	9.1	88.9	91
	PAN				—	—
	Wt. i		Wt. f		% LOSS	
FINE ANALYSIS	4				—	—
	10		23.1	17.3	82.7	83
	20		39.5	22.3	75.7	76
	40		47.2	29.1	70.9	71
	60		55.1	33.9	66.1	66
	100		63.9	39.4	60.6	61
	200		73.3	45.2	54.3	55
	PAN		73.3	45.3	—	—
	Wt. i		Wt. f	% LOSS	C.F.	

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-C _d +M CALC	d=K √ $\frac{L}{T}$ SIZE	% Finer	CORRECTED
	0								
	½								
	1								
	2								
	4								
	8								
	15								
	30								
	60								
	120								
	240								
	480								
	1440								

$$\% \text{ FINEER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \quad ((R - C_d + M) - 1) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

ED JORDAN CO

PROJECT

STEWART ANG

COMP. BY TS

JOB NO 5139.61

CHK. BY RC

DATE 8-3-67

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING B102 NUMBER 5-6 DEPTH

MOISTURE CONTENT	
TARE N <small>o</small>	5 Wt. 52.3
SAMPLE + TARE, i	249.7
SAMPLE + TARE, f	249.0
SAMPLE, f	196.2
MOISTURE	20.7
% Wc	10.61

% OF FINES	
TARE N <small>o</small>	5 Wt. 52.3
SAMPLE + TARE, i	249.0
SAMPLE + TARE, f	146.2
Wt. SOIL LOST	102.8
Wt. SOIL, i	196.2
% of FINES	52.41

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT CORR(Cd)	

COARSE ANALYSIS	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
	3					
	1½					
	1					
	¾					
	½					
	¾					
	¼					
	4					
	PAN					
FINE ANALYSIS	WT. i	WT. f		% LOSS		
	4					
	10			72.8	77.2	77
	20			79.2	70.8	71
	40			32.8	67.2	67
	60			37.4	62.6	63
	100			42.5	57.5	58
	200			47.6	52.4	52
	PAN			—	—	—
WT. i		WT. f	% LOSS	C.F.		

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √ $\frac{L}{T}$	SIZE	% Finer	CORRECTED
0										
½										
1										
2										
4										
8										
15										
30										
60										
120										
240										
480										
1440										

$$\% \text{ FINE} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

EDJC RD AND CO

PROJECT	STEWART AVE	COMP. BY	JOB NO
		S	5139.61
		CHK. BY	DATE
		R.R.	8-31-87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING 5102 NUMBER 5-2 DEPTH

MOISTURE CONTENT

TARE NO. 60 Wt. 52.5
 SAMPLE + TARE, i 279.6
 SAMPLE + TARE, f 259.1
 SAMPLE, f 206.6
 MOISTURE _____
 % Wc 10.0

% OF FINES

TARE NO. 60 Wt. 52.5
 SAMPLE + TARE, i 259.1
 SAMPLE + TARE, f 164.0
 Wt. SOIL LOST 95.1
 Wt. SOIL, i 206.6
 % of FINES 46.0

HYDROMETER ANALYSIS

SAMPLE SIZE i _____
 MENISCUS CORR (M) _____
 DISP. AGENT _____
 AMOUNT CORR(Cd) _____

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1½					
1					
¾					
½					
⅓	4.0	1.9	98.1	93	-
¼	9.2	4.5	95.5	96	-
4	17.0	8.2	91.8	92	-
PAN					
	Wt. i	Wt. f		% Loss	
	4	-	-	-	-
	10	38.2	18.4	81.6	82
	20	54.3	26.3	73.7	74
	40	67.1	32.5	67.5	68
	60	80.2	38.8	61.2	61
	100	96.2	46.6	53.4	54
	200	111.4	53.9	46.1	46
	PAN	111.6	-	-	-
	Wt. i	Wt. f	% Loss	C.F.	

TIME	ΔT MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √ $\frac{L}{T}$	SIZE	% Finer	CORRECTED
	0									
	½									
	1									
	2									
	4									
	8									
	15									
	30									
	60									
	120									
	240									
	480									
	1440									

$$\% \text{ FINE} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART ANC

COMP. BY

CHK. BY

JOB NO

DATE

5130.6

8-5-87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING 5103 NUMBER 5-7 DEPTH

MOISTURE CONTENT	
TARE NO	8
Wt.	52.1
SAMPLE + TARE, i	234.8
SAMPLE + TARE, f	221.1
SAMPLE, f	169.0
MOISTURE	13.7
% Wc	8.1

% OF FINES	
TARE NO	8
Wt.	52.1
SAMPLE + TARE, i	221.1
SAMPLE + TARE, f	143.3
Wt. SOIL LOST	77.8
Wt. SOIL, i	169.0
% of FINES	46.0

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT CORR(Cd)	

COARSE ANALYSIS	SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
		WITH TARE	WITHOUT TARE			
	3					
	1 1/2					
	1					
	3/4		12.1	7.2	92.8	93
	1/2		17.7	10.5	29.5	32
	3/8		2.2	1.2	37.5	35
	1/4		24.6	14.6	55.4	55
	4		31.5	18.6	5.2	3
	PAN					
FINE ANALYSIS	WT. i			WT. f		% LOSS
	4					-
	10		43.6	25.3	74.2	74
	20		53.5	31.7	68.3	68
	40		60.9	36.0	64.0	64
	60		68.9	40.3	59.2	59
	100		79.0	46.7	53.3	53
	200		91.2	54.0	46.0	46
	PAN		91.4	-	-	
	WT. i		WT. f	% LOSS	C.F.	

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √ $\frac{L}{T}$	% Finer	Corrected
0									
1/2									
1									
2									
4									
8									
15									
30									
60									
120									
240									
480									
1440									

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

EQUIPMENT

PROJECT

STEWART ANG

COMP. BY TS

JOB NO 5130.01

CHK. BY F.E.

DATE 8-31-87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING 3104 NUMBER S-4 DEPTH

MOISTURE CONTENT

TARE NO 1 Wt. 53.4
 SAMPLE + TARE, i 261.8
 SAMPLE + TARE, f 245.4
 SAMPLE, f 192.0
 MOISTURE 16.4
 % Wc 3.5 /

% OF FINES

TARE NO 4 Wt. 53.4
 SAMPLE + TARE, i 245.4
 SAMPLE + TARE, f 160.3
 Wt. SOIL LOST 85.1
 Wt. SOIL, i 192.0
 % of FINES 44.3 /

HYDROMETER ANALYSIS

SAMPLE SIZE i
 MENISCUS CORR (M)
 DISP. AGENT
 AMOUNT CORR (Cd)

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'
	WITH TARE	WITHOUT TARE			
3					
1 1/2					
1	25.7	13.4	100	100	
3/4	—	—	—	—	
1/2	—	—	—	—	
3/8	27.0	15	—	—	
1/4	31.2	23	—	—	
4	37.0	19.3	—	—	
PAN					
Wt. i		Wt. f		% LOSS	
4					
10	50.6	26.4	73.6	74	/
20	62.8	32.7	67.3	67	
40	71.8	37.4	62.6	63	/
60	82.1	42.3	57.2	57	
100	93.9	48.9	51.1	51	/
200	106.8	55.6	44.4	44	
PAN	107.0	—			
Wt. i		Wt. f	% LOSS	C.F.	

TIME	ΔT MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √ L / T	SIZE	% Finer	CORRECT
0										
1/2										
1										
2										
4										
8										
15										
30										
60										
120										
240										
480										
1440										

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSU}$$

EDUCRDA

PROJECT

STEWART ANG

COMP. BY TS

CHK. BY UR

JOB NO 5134.01

DATE 8-31-87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING 105 NUMBER 55 DEPTH

MOISTURE CONTENT	
TARE N <small>o</small>	53
Wt.	53.7
SAMPLE + TARE, i	163.3
SAMPLE + TARE, f	167.8
SAMPLE, f	114.1
MOISTURE	15.5
% Wc	13.6

% OF FINES	
TARE N <small>o</small>	53
Wt.	53.7
SAMPLE + TARE, i	167.8
SAMPLE + TARE, f	220.9
Wt. SOIL LOST	78.9
Wt. SOIL, i	114.1
% of FINES	69.1

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT CORR (Cd)	

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1 1/2					
1					
3/4					
1/2					
3/8					
1/4		-		100	100
4		3.2	1.9	98.1	98
PAN					
WT. i		WT. f	% LOSS		
4		-			
10		9.7	8.5	91.5	92
20		16.5	14.5	85.5	86
40		21.0	18.4	81.6	82
60		25.3	22.2	77.8	78
100		30.2	26.5	74.5	76
200		35.2	30.9	69.1	69
PAN		35.2	-	-	-
WT. i		WT. f	% LOSS		

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √L/T SIZE	% Finer	CORRECTED
0									
1/2									
1									
2									
4									
8									
15									
30									
60									
120									
240									
480									
1440									

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_{s-1}} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART A.N.C.

COMP. BY

TS

CHK. BY

RLR

JOB NO

5139.01

DATE

8.31.87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING

3106

NUMBER 53

DEPTH

MOISTURE CONTENT

TARE NO 70 Wt. 58.6

SAMPLE + TARE, i 289.1

SAMPLE + TARE, f 264.1

SAMPLE, f 205.5

MOISTURE 25.0

% Wc 12.2

% OF FINES

TARE NO 70 Wt. 58.6

SAMPLE + TARE, i 264.1

SAMPLE + TARE, f 195.0

Wt. SOIL LOST 69.1

Wt. SOIL, i 205.5

% of FINES 33.6

HYDROMETER ANALYSIS

SAMPLE SIZE i

MENISCUS CORR (M)

DISP. AGENT

AMOUNT CORR (Cd)

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1 1/2					
1				100	100
3/4	7.1	3.5	3.5	96.5	97
1/2	9.7	4.7	4.7	95.3	95
3/8	11.6	5.6	5.6	94.4	94
1/4	18.7	9.1	9.1	90.9	91
4	28.1	13.7	13.7	56.3	86
PAN					
Wt. i					% Loss
4					—
10	46.8	22.8	22.8	77.2	77
20	65.4	31.8	31.8	68.2	68
40	80.2	39.0	39.0	61.0	61
60	97.3	47.4	47.4	52.6	53
100	116.3	56.6	56.6	44.4	44
200	135.8	66.1	66.1	33.9	34
PAN	136.5	—	—	—	—
Wt. i					C.F.

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K √(L/T) SIZE	% Finer	CORRECTED
0									
1/2									
1									
2									
4									
8									
15									
30									
60									
120									
240									
480									
1440									

$$\% \text{ FINE} = \left[\left(\frac{G_s}{G_{s-1}} \right) \times \frac{100}{W_i} \left((R - C_d + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

ECJORDANCO

PROJECT

STEWART ANG

COMP. BY

TS

CHK. BY

RLR

JOB NO

5136.01

DATE

8.31.87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING 5106 NUMBER 55 DEPTH

MOISTURE CONTENT	
TARE NO	3
Wt.	51.9
SAMPLE + TARE, i	263.3
SAMPLE + TARE, f	238.6
SAMPLE, f	186.7
MOISTURE	24.7
% Wc	13.2%

% OF FINES	
TARE NO	3
Wt.	51.9
SAMPLE + TARE, i	238.6
SAMPLE + TARE, f	164.5
Wt. SOIL LOST	74.1
Wt. SOIL, i	186.7
% of FINES	39.9%

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT CORR (Cd)	

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1½					
1					
¾					
½					
⅓	8.0	4.3	95.7	95%	
¼	16.8	9.0	91.0	91%	
4	24.3	13.0	87.0	87%	
PAN					
COARSE ANALYSIS	WT. i	WT. f	% LOSS		
	4	-			
10	41.7	22.3	77.7	78	
20	58.2	31.2	68.8	69%	
40	71.0	38.0	62.0	62	
60	83.7	44.8	55.2	55%	
100	97.0	52.0	48.0	48	
200	112.0	60.0	40.0	40	
PAN	112.8	-	-	-	
FINE ANALYSIS	WT. i	WT. f	% LOSS	C.F.	

TIME	Δt	MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K√L/T SIZE	% Finer	Corrected
	0							.		
	½									
	1									
	2									
	4									
	8									
	15									
	30									
	60									
	120									
	240									
	480									
	1440									

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_f} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART ANG

COMP. BY

TS
RLE

JOB NO

5139.01

DATE

8.31.87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING B 107 E NUMBER S-2 DEPTH

MOISTURE CONTENT	
TARE NO	25
Wt.	8.7
SAMPLE + TARE, i	234.9
SAMPLE + TARE, f	210.5
SAMPLE, f	141.8
MOISTURE	24.4
% Wc	7.2

% OF FINES	
TARE NO	25
Wt.	8.7
SAMPLE + TARE, i	210.5
SAMPLE + TARE, f	123.6
Wt. SOIL LOST	86.9
Wt. SOIL, f	141.8
% of FINES	6.3%

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT	CORR (Cd)

SIEVE	Wt. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1½					
1					
¾					
½					
⅓					
¼					
4					
PAN					

	Wt. i	Wt. f	% Loss	
4				—
10		13.6	9.6	90
20		16.5	11.6	88.4
40		18.8	13.3	86.7
60		22.6	15.9	84.1
100		30.3	21.4	78.6
200		53.4	37.7	62.3
PAN		54.9	—	—

	Wt. i	Wt. f	% Loss	C.F.
4				
10				
20				
40				
60				
100				
200				
PAN				

TIME	Δt MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K $\sqrt{\frac{L}{T}}$	% Finer	CORRECTED
	0								
	½								
	1								
	2								
	4								
	8								
	15								
	30								
	60								
	120								
	240								
	480								
	1440								

$$\% \text{ FINE} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT STEWART ANC

COMP. BY TS
CHK. BY BLR

JOB NO 5134.01
DATE 3.31.37

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING B108 NUMBER 53 · DEPTH

MOISTURE CONTENT	
TARE NO 19	Wt. 55.7
SAMPLE+TARE, i	232.7
SAMPLE+TARE, f	213.8
SAMPLE, f	158.1
MOISTURE	18.9
% W _c	12.0%

% OF FINES	
TARE NO 19	Wt. 55.7
SAMPLE+TARE, i	213.5
SAMPLE+TARE, f	158.8
Wt. SOIL LOST	55.0
Wt. SOIL, i	158.1
% of FINES	34.8 35.2

HYDROMETER ANALYSIS	
SAMPLE SIZE i	
MENISCUS CORR (M)	
DISP. AGENT	
AMOUNT	CORR (C _d)

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1½					
1					
¾					
½					
⅓					
¼					
4					
PAN					

COARSE ANALYSIS	WT. i	WT. f	% LOSS	
4				
10	45.9	29.0	71.0	71
20	57.6	36.4	63.6	64
40	66.4	42.0	58.0	58
60	77.6	49.1	50.9	51
100	95.1	60.2	39.8	40
200	103.2	61.9	35.5	35
PAN	103.3			

FINE ANALYSIS	WT. i	WT. f	% LOSS		C.F.
4					
10					
20					
40					
60					
100					
200					
PAN					

TIME	ΔT MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L EFF.DPTH.	R-Cd+M CALC	d=K √ $\frac{L}{T}$	SIZE	% Finer	CORRECTED
	0									
	½									
	1									
	2									
	4									
	8									
	15									
	30									
	60									
	120									
	240									
	480									
	1440									

$$\% \text{ FINE} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - C_d + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

PROJECT

STEWART ANG

COMP. BY TS

CHK. BY RLR

JOB NO

5136.01

DATE

8-31-87

GRAIN SIZE ANALYSIS

SAMPLE I.D: BORING B 110 NUMBER 54 DEPTH

MOISTURE CONTENT

TARE NO # 51 Wt. 52.8

SAMPLE + TARE, i 237.2

SAMPLE + TARE, f 215.3

SAMPLE, f 162.5

MOISTURE 21.9

% Wc 13.5

% OF FINES

TARE NO # 51 Wt. 52.8

SAMPLE + TARE, i 215.3

SAMPLE + TARE, f 150.4

Wt. SOIL LOST 64.9

Wt. SOIL, i 162.5

% of FINES 40.0%

HYDROMETER ANALYSIS

SAMPLE SIZE i

MENISCUS CORR (M)

DISP. AGENT

AMOUNT CORR (Cd)

SIEVE	WT. RETAINED		% RET	% PASS	CORRECT'D
	WITH TARE	WITHOUT TARE			
3					
1 1/2					
1					
3/4					
1/2	0		100	100	
3/8	1.8	1.1	22.0	77.0	
1/4	8.2	5.1	44.9	55.1	
4	16.1	9.9	20.1	79.9	
PAN					
	Wt. i	Wt. f		% Loss	
	4				
	10	29.7	18.3	81.7	82
	20	40.3	24.8	75.2	75
	40	48.5	30.0	70.0	70
	60	60.2	31.7	58.3	58
	100	82.3	50.7	49.3	49
	200	98.1	60.4	39.6	40
	PAN	98.3	60.5	—	—
	Wt. i	Wt. f	% Loss	C.F.	

TIME	Δt	MIN	TEMP/K	ACTUAL HYDRO	R CORR'D	L Eff.Dpth.	R-Cd+M CALC	d=K $\sqrt{\frac{L}{T}}$ SIZE	% Finer	CORRECTED
		0								
		1/2								
		1								
		2								
		4								
		8								
		15								
		30								
		60								
		120								
		240								
		480								
		1440								

$$\% \text{ FINER} = \left[\left(\frac{G_s}{G_s - 1} \right) \times \frac{100}{W_i} \left((R - Cd + M) - 1 \right) \right] \times 1000 \quad G_s \quad \text{REAL / ASSUMED}$$

ECJORDAN CO

APPENDIX D
FIELD PERMEABILITY TEST DATA

TABLE D-1
RISING HEAD PERMEABILITY TEST DATA

JMW108 PERTEST		JMW109 PERTEST		JMW107 PERTEST		JMW101 PERTEST	
Diameter of riser	= 0.166						
Length of zone	= 7	Length of zone	= 7	Length of zone	= 12	Length of zone	= 12
Diameter of zone	= 0.66	Diameter of zone	= 0.666	Diameter of zone	= 0.66	Diameter of zone	= 0.333
Static water level	= 8.36	Static water level	= 9.91	Static water level	= 10.13	Static water level	= 31.23
Number of readings	= 20	Number of readings	= 14	Number of readings	= 18	Number of readings	= 16

Time (min.)	Excess Head (ft.)						
0	5.1	0	2.04	.5	1.98	0	1.41
1	4.88	.5	1.93	1	1.9	.5	1.34
2	4.67	1	1.87	1.5	1.86	1	1.34
3	4.41	2	1.73	2	1.84	2	1.24
4	4.09	3	1.59	3	1.78	3	1.20
5	3.88	4	1.48	4	1.75	4	1.17
6	3.66	5	1.39	5	1.69	5	1.13
7	3.42	6	1.3	6	1.65	6	1.13
8	3.2	7	1.22	7	1.61	7	1.11
9	2.97	8	1.15	8	1.57	8	1.09
10	2.78	9	1.08	9	1.53	9	1.08
11	2.58	10	1.01	10	1.49	10	1.07
12	2.41	15	0.74	15	1.14	15	1.02
13	2.26	20	0.61	21	0.89	20	0.94
14	2.11			29	0.49	25	0.88
15	1.95			30	0.47	30	0.84
20	1.38			40	0.17		
25	0.88			50	0.13		
30	0.61						
35	0.48						

$$K = 5.13 \times 10^{-5} \text{ cm/sec}$$

$$K = 4.20 \times 10^{-5} \text{ cm/sec}$$

$$K = 2.24 \times 10^{-5} \text{ cm/sec}$$

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APPENDIX E
ANALYTICAL RESULTS

ORGANIC AND INORGANIC QUALIFIERS

- U Indicates the parameter was analyzed for but was not detected at the value preceding the flag. This value represents the CRDL corrected for dilution where appropriate.
- J Indicates an estimated value.
- B Indicates the parameter was present in the associated method blank.
- R Indicates the value was rejected.
- JB A combination of the J and B flags. Indicates an estimated value due to possible method blank contamination.
- UJB A combination of the U, J, and B flags. Indicated that, due to contamination found in the method blank, the detection limit was revised.
- CRDL Contract Required Detection Limit
- IDL Instrument Detection Limit
- RDL Revised Detection Limit due to blank contamination
- NA Not Analyzed
- NR Not Required
- Analyzed but not detected
- ND Not Detected
- II Indistinguishable Isomers

INORGANIC QUALIFIERS

Concentration (C) Qualifiers:

[] = The reported value is less than the CRDL but greater than the IDL.

U = The analyte was analyzed for but not detected.

(Q) Qualifiers:

E = The reported value is estimated because of the presence of interference. If the problem applies to all samples, an explanatory note must be included under "Comments" on the cover sheet. If it is an isolated problem, a note should be included on the specific Form I=IN.

M = Duplicate injection precision not met.

N = Spiked sample recovery not within control limits.

S = The reported value was determined by the method of standard additions (MSA).

W = Post-digestion spike for Furnace AA analysis is out of control limits (85-115%), while sample absorbance is less than 50% of spike absorbance.

* = Duplicate Analysis not within control limits.

- = Correlation coefficient for the MSA is less than 0.995.

Method (M) Qualifiers:

P = ICP

A = Flame AA

F = Furnace AA

CV = Manual Cold Vapor AA

AV = Automated Cold Vapor AA

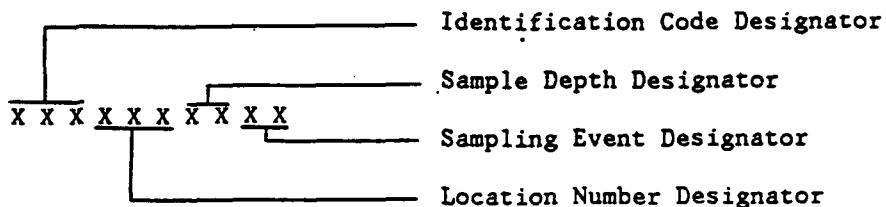
AS = Semiautomated Spectrophotometric

C = Manual Spectrophotometric

T = Titrimetric

NR = The analyte is not required to be analyzed

SAMPLE IDENTIFICATION NUMBER EXPLANATION



Identification Code Designator - J = E.C. Jordan
MW = Monitoring Well
TB = Test Boring
SD = Surface Soil/Sediment
SW = Surface Water .

Location Number Designator - Three-digit number that represents a location

Sample Depth Designator - Two-digit number that represents sample depth interval (i.e., 01 = 0 to 1 foot, 31 = 30 to 31 feet, xx = water sample)

Sampling Event Designator - Two-digit number that represents the sampling event at the same location (i.e., 01 = first sampling event, 04 = fourth sampling event)

Miscellaneous

JDUP - Jordan Duplicate Sample
MSD - Matrix Spike Duplicate
MS01 - Matrix Spike First Event
JSAMP - Jordan Soil Sampler Blank
JSBL - Jordan Water Sampler Blank
JFBL - Jordan Field Filter Blank
JTBL - Jordan Trip Blank (Water Samplers)
JMW 108 R1 = Replicate 1
JMW 108 R2 = Replicate 2
JMW 108 R3 = Replicate 3

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	JDUPO1XXXX01	JSD10000101	JSD1000MSD	JSD1000MSD
COMPUSCHEM ID	144607	144003	144009	144017
DATE SAMPLED	07/30/87	07/30/87	07/30/87	07/30/87
DEPTH (ft)	0	1	0	0
MATRIX	SOIL	SOIL	SOIL	SOIL
<u>INORGANIC COMPOUNDS (mg/kg)</u>				
ARSENIC	2	3.4 N	4.4 S	4.3 N
BERYLLIUM	1	1 []	1.1 []	1 []
CADMIUM	1	3.6	3.7	-
CHROMIUM	2	-	1.5	1.8
COPPER	10	16	4.4	40
LEAD	1	9.1	9.5 []	24
MERCURY	22	N	27 N	-
NICKEL	0.02	-	-	-
THALLIUM	6	1.7	20	15
ZINC	2	-	-	-
BARIUM	4	81	10.4	78
IRON	40	75	86	72
MANGANESE	20	24600	32600	23700
VANADIUM	3	1020	1190	987
ALUMINUM	10	1.7	2.2	1.7
COBALT	40	12800	15600	12000
MAGNESIUM	10	9.3 []	11 []	9.4 []
CALCIUM	10000	5310 E	6520 E	5080 E
POTASSIUM	10000	7250	9060	7620
CYANIDE	10000	1420 []	1510 []	1390 []
PERCENT SOLIDS	0.5	-	-	-
	6.4	56	61	59

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	JDUFO1XXX01	JSD1000101	JSD1000501
COMPUCHEM ID	144007	144003	144017
DATE SAMPLED	07/30/87	07/30/87	07/30/87
DEPTH (ft)	0	1	0
MATRIX	SOIL	SOIL	SOIL
<u>VOLATILE ORGANIC COMPOUNDS</u> ($\mu\text{g}/\text{kg}$)	<u>DETECTION LIMIT</u>		
BENZENE	5	-	-
CHLOROFORM	5	-	-
METHYLENE CHLORIDE	5	28 B	50 B
ACETONE	10	29 B	14 J B
<u>SEMI-VOLATILE ORGANIC COMPOUNDS</u> ($\mu\text{g}/\text{kg}$)			
ACENAPHTHENE	-	-	-
ANTHRACENE	330	-	-
BENZO(A)ANTHRACENE	350	-	-
BENZO(A)PYRENE	330	-	-
BENZO(B)FLUORANTHENE	330	-	-
BENZO(K)FLUORANTHENE	330	-	-
BIS(2-ETHYLHEXYL)PHTHALATE	330	-	-
CHRYSENE	330	-	-
FLUORANTHENE	330	-	-
PHENANTHRENE	330	-	-
PYRENE	330	-	-
<u>PESTICIDES</u> ($\mu\text{g}/\text{kg}$)			
4,4'-DDT	16	2300 C	3100 C
4,4'-DDE	16	190	230
4,4'-DDD	16	170	130
<u>PH SULFATE, CHLORIDE, FLUORIDE</u> ($\mu\text{g}/\text{kg}$)			
FLUORIDE	7.7	7.8	7.7
CHLORIDE	1.4	1.4	1.7
PERCENT SOLIDS	64	56	61
			59

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	ECJ SAMPLE ID	JSD1010101	JSD1020101
COMPUCHEM ID	144005	144006	144006
DATE SAMPLED	07/30/87	07/30/87	07/30/87
DEPTH (ft)	1	1	1
MATRIX	SOIL	SOIL	SOIL
INORGANIC COMPOUNDS (mg/kg)			
ARSENIC	2	3 N	2.4 □ N
BERYLLIUM	1	0.61 □	0.47 □
CADMIUM	1	1.1 □	2.9
CHROMIUM	2	11	8.7
COPPER	10	7.4	7.8 □
LEAD	1	24 N	29 N
MERCURY	0.02	-	0.26 N
NICKEL	8	15	-
THALLIUM	2	-	-
ZINC	4	59	43
BARIUM	40	58	44 □
IRON	20	15900	9650
MANGANESE	3	2310	282
VANADIUM	10	15	12 □
ALUMINUM	40	7370	6400
COBALT	10	6.8 □	2.3 □
MAGNESIUM	1000	2880 E	1990 E
CALCIUM	1000	3430	3980
POTASSIUM	-	-	-
CYANIDE	0.5	-	-
PERCENT SOLIDS	78	74	74

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	JSD1010101	JSD1020101
COMPUCHEM ID	144005	144006
DATE SAMPLED	07/30/87	07/30/87
DEPTH (ft)	1	1
MATRIX	SOIL	SOIL
VOLATILE ORGANIC COMPOUNDS ($\mu\text{g/kg}$)		DETECTION LIMIT
BENZENE	5	5
CHLOROFORM	5	1.3 J
METHYLENE CHLORIDE	5	-
ACETONE	10	32 B 33 B
SEMI-VOLATILE ORGANIC COMPOUNDS ($\mu\text{g/kg}$)		
ACENAPHTHENE	330	52 J
ANTHRACENE	330	87 J
BENZO(A)ANTHRACENE	330	300 J
BENZO(A)PYRENE	330	260 J
BENZO(B)FLUORANTHENE	330	450 II
BENZO(K)FLUORANTHENE	330	450 II
BIS(2-ETHYLHEXYL)PHTHALATE	330	120 J
CHRYSENE	330	370 J
FLUORANTHENE	350	620 J
PHENANTHRENE	330	500 J
PYRENE	330	540 J
PESTICIDES ($\mu\text{g/kg}$)		
4,4'-DDT	16	-
4,4'-DDE	16	-
4,4'-DDD	16	-
PH SULFATE, CHLORIDE, FLUORIDE ($\mu\text{g/kg}$)		
FLUORIDE	7.5	7.4
CHLORIDE	0.6	0.67
PERCENT SOLIDS	78	74

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

POINT	ECJ SAMPLE ID	DETECTION LIMIT ($\mu\text{g/l}$)	
COMPUCHEM ID	J5AIP10101	2.5	[]
DATE SAMPLE	143986	-	
DEPTH (ft)	07/30/87	-	
MATRIX	1	WATER	
INORGANIC COMPOUNDS ($\mu\text{g/l}$)			
ARSENIC	10		
BERYLLIUM	5		
CADMIUM	5		
CHROMIUM	-		
COPPER	10		
LEAD	25		
MERCURY	7.1	[]	
NICKEL	5	[]	
THALLIUM	0.2	-	
ZINC	40		
BARIUM	10		
IRON	200		
MANGANESE	200		
VANADIUM	100		
ALUMINUM	15		
COBALT	50		
MAGNESIUM	5000		
CALCIUM	5000		
POTASSIUM	136	[]	E
CYANIDE	5000	-	
	10	86	N *

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

POINT
 ECJ SAMPLE ID
 COMPUCHEM ID
 DATE SAMPLE
 DEPTH (ft)
 MATRIX

<u>VOLATILE ORGANIC COMPOUNDS</u>	<u>DETECTION LIMIT (ug/l)</u>
BENZENE	5
CHLOROFORM	5
METHYLENE CHLORIDE	5
ACETONE	10
<u>SEMI-VOLATILE ORGANIC COMPOUNDS (ug/l)</u>	
ACENAPHTHENE	10
ANTHRACENE	10
BENZO(A)ANTHRACENE	10
BENZO(A)PYRENE	10
BENZO(B)FLUORANTHENE	10
BENZO(K)FLUORANTHENE	10
BIS(2-ETHYLHEXYL)PHTHALATE	10
CHRYSENE	10
FLUORANTHENE	10
PHENANTHRENE	10
PYRENE	10
<u>PESTICIDES (ug/l)</u>	
4,4'-DDT	0.1
4,4'-DDE	0.1
4,4'-DDD	0.1
<u>PH SULFATE, CHLORIDE, FLUORIDE (ug/l)</u>	
FLUORIDE	6.6
CHLORIDE	-

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	JMW1013101 145627 08/10/87 31	JMW1070401 144191 08/01/87 4	JMW1080701 144768 08/04/87 7	JMW1090501 145249 08/06/87 5
MATRIX	SOIL	SOIL	SOIL	SOIL
INORGANIC COMPOUNDS ($\mu\text{g}/\text{kg}$)				
ARSENIC	DETECTION LIMIT	3.4 N 0.52 [J]	1.7 [J] N 0.42 [J]	2.3 N 0.44 [J]
BERYLLIUM	1	-	-	0.52 [J]
CAIUM	2	1.1	1.1	-
CHROMIUM	5	25 E	6.7	1.2
COPPER	1	9.5 N	9.6 N	24 E
LEAD	0.02	-	-	20
MERCURY	8	1.3	1.1	0.13 N
NICKEL	4	11.7	5.4	0.13 N
ZINC	40	52	28 [J]	1.7
BARIUM	20	16800	17700	65
IRON	3	790	594	44 [J]
MANGANESE	10	1.2	1.0 [J]	21400
VANADIUM	40	8140	7810	504
ALUMINUM	10	5.1 [J]	4.8 [J]	999
COBALT	100	5830 E	3370 E	10
MAGNESIUM	1000	30900	16000	10 [J]
CALCIUM	1000	-	2120	1.4
POTASSIUM	1000	-	883 [J]	9220
VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{kg}$)				
BENZENE	5	-	1.7 J B	-
CHLOROFORM	5	2.2 J	5.3 J B	3.6 J
METHYLENE CHLORIDE	5	70 B	24 B	27 B
TOLUENE	5	-	-	-
ACETONE	10	-	1.4 B	58 B
SEMI-VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{kg}$)				
BIS(2-ETHYLHEXYL)PHthalate	350	53 J B	-	-
DIETHYLPHthalate	350	1100 B	17 B	-
DI-N-BUTYLPHthalate	350	71 J	-	-
PCBs ($\mu\text{g}/\text{kg}$)				
PCB AROCLOR-1254	160	210	-	-
PH SULFATE, CHLORIDE, FLUORIDE ($\mu\text{g}/\text{kg}$)				
PH	9.3	7.5	8	7.2
SULFATE	1100	-	-	-
FLUORIDE	-	0.44	0.44	1.8
CHLORIDE	39	-	-	3.5
PERCENT SOLIDS	67	67	64	68

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	DATE SAMPLED	DEPTH (ft)	MATRIX	DETECTION LIMIT	JTB1021201	JTB1030501	JTB1050701	JTB1060501
COMPUChem 10	08/11/87	12	SOIL	0.02	1.1	1.1	1.1	0.45
CADMIUM		5	SOIL	0.02	7	9.2	14	-
CHROMIUM		5	SOIL	0.02	7	28	6.7	-
COPPER		5	SOIL	0.02	16	-	12	-
LEAD		5	SOIL	0.02	16	16	48	-
MERCURY		5	SOIL	0.02	40	40	41	-
NICKEL		5	SOIL	0.02	471	575	595	-
ZINC		5	SOIL	0.02	8190	7940	7950	-
BARIUM		20	SOIL	0.02	19400	18500	18100	-
IRON		20	SOIL	0.02	40	36	41	-
MANGANESE		3	SOIL	0.02	471	12	12	-
VANADIUM		10	SOIL	0.02	8190	5.6	4.4	-
ALUMINUM		40	SOIL	0.02	6150	4070	3470	-
COBALT		10	SOIL	0.02	E	E	E	-
MAGNESIUM		100	SOIL	0.02	25500	28300	4690	-
CALCIUM		100	SOIL	0.02	-	-	837	-
POTASSIUM		100	SOIL	0.02	-	-	-	-
VOLATILE ORGANIC COMPOUNDS (ug/kg)								
BENZENE		5	SOIL	5	3.4	-	-	-
CHLOROFORM		5	SOIL	92	B	23	31	25
METHYLENE CHLORIDE		5	SOIL	-	-	3	B	B
TOLUENE		5	SOIL	27	B	32	B	-
ACETONE		10	SOIL	-	-	-	25	47
SEMI-VOLATILE ORGANIC COMPOUNDS (ug/kg)								
BIT(2-ETHYLHEXYL)PHthalate		330	SOIL	230	J	53	-	85
DIETHYLPHthalate		330	SOIL	1000	B	35	B	J
DI-N-BUTYLPHthalate		330	SOIL	-	-	49	-	-
PCBs (ug/kg)		160	SOIL	210	-	-	-	-
AROCLOr-1254		-	-	-	-	-	-	-
pH, SULFATE, CHLORIDE, FLUORIDE (mg/kg)								
pH		9.2	SOIL	8.9	-	7.7	6.9	-
SULFATE		590	SOIL	-	-	66	-	-
FLUORIDE		-	SOIL	-	-	-	0.29	-
CHLORIDE		40	SOIL	14	-	21	-	-
PERCENT SOLIDS		90	SOIL	89	-	93	84	-

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

POINT	ECJ SAMPLE ID	TRIP B	TRIP BLANK
COMPUCHEM ID		1,45579	
DATE SAMPLED		08/07/87	
DEPTH (ft)	2	0	
MATRIX	WA	50	
<u>INORGANIC COMPOUNDS (ug/l)</u>			
<u>ARSENIC</u>			
BERYLLIUM	1.0	5	
CADMIUM		5	
CHROMIUM		10	
COPPER		25	
LEAD		5	
MERCURY		0.2	
NICKEL		40	
ZINC		20	
BARIUM		200	
IRON		100	
MANGANESE		15	
VANADIUM		50	
ALUMINUM		200	
COBALT		50	
MAGNESIUM		5000	
CALCIUM		5000	
POTASSIUM		5000	
<u>VOLATILE ORGANIC COMPOUNDS (ug/l)</u>			
<u>BENZENE</u>		5	
CHLOROFORM		5	
METHYLENE CHLORIDE		5	
TOLUENE		5	
ACETONE		10	
<u>SEMI-VOLATILE ORGANIC COMPOUNDS (ug/l)</u>			
BIT(2-ETHYLHEXYL)PHthalATE	10	-	
DIETHYLPHthalATE	10	-	
DI-N-BUTYLPHthalATE	10	-	
PCBs (ug/l)	1	-	
AROCLOR-1254			
<u>PH SULFATE, CHLORIDE, FLuORIDE (ug/l)</u>			
PH	6.1	-	
SULFATE		-	
FLuORIDE		-	
CHLORIDE		2	

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID COMPUCHEM ID DATE SAMPLED MATRIX	INORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)	DETECTION LIMIT	WA	WB
ARSENIC	200	739	-	-
BARIUM	10	3.8	□	E
CALCIUM	200	4.3	□	E
COPPER	5000	155000	-	-
IRON	25	9.7	□	-
MAGNESIUM	100	1460	-	-
MANGANESE	5000	34800	-	-
MERCURY	15	87	-	-
SODIUM	0.2	-	-	-
ZINC	5000	18900	-	-
VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)				
METHYLENE CHLORIDE	5	2.2	JB	4.4 JB
ACETONE	10	-	-	-
1,1,1-TRICHLOROETHANE	5	-	-	-
1,1-DICHLOROETHANE	5	-	-	-
TRANS-1,2-DICHLOROETHENE	5	-	-	-
CHLOROFORM	5	-	-	-
CHLOROMETHANE	10	-	-	-
BROMOMETHANE	10	-	-	-
VINYL CHLORIDE	10	-	-	-
CHLOROETHANE	10	-	-	-
SEMI-VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)	1.0	-	-	-
BIS-(2-ETHYLHEXYL)PHthalate	1.0	-	-	-
PESTICIDES/PCBs ($\mu\text{g}/\text{l}$)	1.0	-	-	-
4-A-ODT	0.1	0.57	-	-
ORGANIC HERBICIDES ($\mu\text{g}/\text{l}$)				
2,4-D	4	-	-	-
2,4,5-TP (SILVER)	1	-	-	-
2,4,5-T	1	-	-	-
ORGANIC PESTICIDES ($\mu\text{g}/\text{l}$)				
DISULFOTON	1	-	-	-
METHYL PARATHION	0.5	-	-	-
PARATHION	0.5	-	-	-
PHORATE	0.5	-	-	-
SULFOTEP	0.5	-	-	-
PH. SULFATE, FLUORIDE, CHLORIDE ($\mu\text{g}/\text{l}$)	0.5	-	-	-
SULFATE	6.8	-	-	-
FLUORIDE	320	-	-	-
CHLORIDE	0.2	-	-	-

APPENDIX E
ANALYTICAL RESULTS
STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID
COMPUCHEM ID
DATE SAMPLED
MATRIX

INORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)	DETECTION LIMIT	JMW107XX01 150770		JDUP-1XX01 150759		JMW107XX01 150746		JMW108XX01 150751		JMW108R101 150752	
		WA	WA								
ALUMINUM	200	-	-	-	-	-	-	-	-	-	-
ARSENIC	1.0	4.2	[]	4.3	[]	4.1	[]	4	[]	3.9	[]
BARIUM	200	96	[] E	29	[] E	35	[] E	59	[] E	58	[] E
CALCIUM	5000	306000	-	128000	-	204000	-	212000	-	210000	-
COPPER	25	-	-	-	-	-	-	-	-	-	-
IRON	100	466	-	112	-	41	[]	154	-	-	-
MAGNESIUM	5000	89900	-	17800	-	19400	-	27700	-	206	-
MANGANESE	15	2750	-	9430	-	160	-	5940	-	27300	-
MERCURY	0.2	-	-	-	-	-	-	-	-	5240	-
SODIUM	5000	117000	-	46400	-	35700	-	101000	-	98600	-
ZINC	20	13	[]	13	[]	22	-	16	[]	23	-
<u>VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)</u>											
<u>METHYLENE CHLORIDE</u>											
ACETONE	5	4.9	JB	4.3	JB	3.8	J	8.2	B	5.2	B
1,1,1-TRICHLOROETHANE	10	-	-	-	-	-	-	-	-	-	-
1,1-DICHLOROETHANE	5	-	-	-	-	-	-	-	-	-	-
TRANS-1,2-DICHLOROETHENE	5	-	-	-	-	-	-	-	-	-	-
CHLOROFORM	5	-	-	-	-	-	-	-	-	-	-
CHLOROMETHANE	5	4.3	J	4.0	J	4.9	J	8.6	J	2.3	J
BROMOMETHANE	10	-	-	-	-	-	-	-	-	-	-
VINYL CHLORIDE	10	-	-	-	-	-	-	-	-	-	-
CHLOROETHANE	10	-	-	-	-	-	-	-	-	-	-
SEMI-VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)	10	-	-	-	-	-	-	-	-	-	-
BIS-(2-ETHYLHEXYL)PHthalate	10	-	-	-	-	-	-	-	-	-	-
PESTICIDES/PCBs ($\mu\text{g}/\text{l}$)	10	7.2	J	-	-	-	-	-	-	-	-
4,4'-DDT	0.1	-	-	-	-	-	-	-	-	-	-
<u>ORGANIC HERBICIDES ($\mu\text{g}/\text{l}$)</u>											
2,4-D	-	-	-	-	-	-	-	-	-	-	-
2,4,5-TP (SILVEX)	4	-	-	-	-	-	-	-	-	-	-
2,4,5-T	1	-	-	-	-	-	-	-	-	-	-
<u>ORGANIC PESTICIDES ($\mu\text{g}/\text{l}$)</u>											
DISULFOTON	1	-	-	-	-	-	-	-	-	-	-
METHYL PARATHION	0.5	-	-	-	-	-	-	-	-	-	-
PARATHION	0.5	-	-	-	-	-	-	-	-	-	-
PHORATE	0.5	-	-	-	-	-	-	-	-	-	-
SULFOTEPP	0.5	-	-	-	-	-	-	-	-	-	-
PH. SULFATE, FLUORIDE, CHLORIDE	($\mu\text{g}/\text{l}$)	0.5	-	-	-	-	-	-	-	-	-
SULFATE	6.8	6.4	-	-	-	-	-	-	-	-	-
FLUORIDE	1300	40	-	-	-	-	-	-	-	-	-
CHLORIDE	0.16	0.16	-	-	-	-	-	-	-	-	-
	11	67	-	-	-	-	-	-	-	-	-
			6.7	6.45	0.45	0.1	0.54	6.6	6.0	0.12	250

APPENDIX E
ANALYTICAL RESULTS

STEWART AIR NATIONAL GUARD BASE

ECJ SAMPLE ID	COMPUCHEM ID	DATE SAMPLED	STEWART AIR NATIONAL GUARD BASE	JMM108R201 150765	JMM108R301 150756	JMM109XX01 150762	J5BL-1XXX01 150755	JFBL-1XXX01 150771
INORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)			DETECTION LIMIT	WA	WA	WA	WA	WA
ALUMINUM			200	-	-	-	-	-
ARSENIC			10	3.7	3.6	3.6	-	3
BARIUM			200	59	58	30	30	30
CALCIUM			5000	213000	211000	128000	E	E
COPPER			25	-	-	-	-	-
IRON			100	131	89	50	118	129
MAGNESIUM			5000	28100	27000	17700	67	11
MANGANESE			15	5800	5650	9150	-	-
MERCURY			0.2	-	-	-	-	-
SODIUM			5000	100000	101000	45900	-	-
ZINC			20	20	14	11	11	9.8
VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)								
METHYLENE CHLORIDE			5	3.7	3.9	JB	3.7	J
ACETONE			10	-	-	-	-	4
1,1,1-TRICHLOROETHANE			5	1.8	1.7	J	-	-
1,1-DICHLOROETHANE			5	-	-	-	-	-
TRANS-1,2-DICHLOROETHENE			5	-	-	-	-	-
CHLOROFORM			5	-	-	-	-	-
CHLOROMETHANE			10	-	-	-	-	-
BROMOMETHANE			10	-	-	-	-	-
VINYL CHLORIDE			10	-	-	-	-	-
CHLOROETHANE			10	-	-	-	-	-
SEMI-VOLATILE ORGANIC COMPOUNDS ($\mu\text{g}/\text{l}$)			1.2	J	5.5	J	5.5	J
BIS-(2-ETHYLHEXYL)PHthalate			10	1.3	26	8	8	8
PESTICIDES/PCBs ($\mu\text{g}/\text{l}$)			0.1	-	-	-	-	-
4,4'-DDT			-	-	-	-	-	-
ORGANIC HERBICIDES ($\mu\text{g}/\text{l}$)								
2,4-D			1	-	-	-	-	-
2,4,5-TP (SILVER)			1	-	-	-	-	-
2,4,5-T			1	-	-	-	-	-
ORGANIC PESTICIDES ($\mu\text{g}/\text{l}$)								
DISUFOTON			0.5	-	-	-	-	-
METHYL PARATHION			0.5	-	-	-	-	-
PARATHION			0.5	-	-	-	-	-
PHORATE			0.5	-	-	-	-	-
SULFOTEPP			0.5	-	-	-	-	-
PH SULFATE, FLUORIDE, CHLORIDE ($\mu\text{g}/\text{l}$)								
SULFATE			6.5	-	-	-	-	-
FLUORIDE			4.6	-	-	-	-	-
CHLORIDE			<1	-	-	-	-	-
			NR	-	-	-	-	-
			<6	-	-	-	-	-
			0.04	-	-	-	-	-
			0.22	-	-	-	-	-
			68	-	-	-	-	-

APPENDIX F
SURFACE AND GROUNDWATER FIELD SAMPLE DATA RECORDS

ECJORDANCO

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SURFACE WATER /SEDIMENT FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG - TASK NO. 1 JOB NO 5139-00STATION NO/LOCATION SW- 1 DATE 9-2-87SKETCH ON BACK PHOTOGRAPHS ROLL NO/EXPOSURE NO 1/56⁶⁻⁷FIELD DATA TIME: START 10:00 AIR TEMP. 80°FEND 11:00 WEATHER SunnyWATER DEPTH @ SAMPLE LOCATION 1' WIDTH OF STREAM 60 sq'
PondTYPE OF STREAM SAMPLE Pond SAMPLE METHOD GrabSTREAM VELOCITY MEASUREMENTS YES NOFIELD DATA COLLECTED IN SITU TEMP 16.1 °C IN BOTTLE SP. COND 1023 @ 25°C pH 7.1DISSOLVED OXYGEN N/A PPM METER VOA LEVEL(PPM) AMBIENT N/A WINKLER SAMPLE LOCATION N/AHEADSPACE N/ATYPE/DESCRIPTION OF SEDIMENT SEE SAMPLE DATA RECORD SD-DEPTH OF SEDIMENT SAMPLE - EQUIPMENT USED -

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
204, 205		40ml	H ₂ O	No	4°C	VOA NCLP - COP
206, 207		1-liter	H ₂ O	No	4°C	EXT. ORG. NCLP - COP
208, 209		1-liter	H ₂ O	No	4°C	Pest/PCB NCLP - COP
210		1-liter	H ₂ O	No	HNO ₃	METALS NCLP - COP
211, 212		1-liter	H ₂ O	No	4°C	ORGANOPHOSPHORUS PEST - 8140/3940-8140
213, 214		1-liter	H ₂ O	No	4°C	CHLORINATE HERBICIDE 8150
215		250ml	H ₂ O	No	4°C	CHLORIDE/SULFATE
216		125ml	H ₂ O	No	4°C	FLUORIDE

REMARKS/OBSERVATIONS Water sample slightly turbid - sample collected 9-2 (short Heavy Rainfall on 8-31) Sample collected on southwest corner of pond.SAMPLER B. Schoenard / T. McMullen

NO D.B. Battery Dead

4405 Compu Chem Code JSW001XX01

EC.JORDANCO

PAGE _____ OF _____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK No. 1 JOB NO 5139-00STATION NO/LOCATION MW-101 DATE 9/1/87SKETCH ON BACK PHOTOGRAPHS ROLL NO/EXPOSURE NO 111-ZFIELD DATA TIME: START 9:30 AM 9/1 AIR TEMP 75° F
END 8:00 AM 1/2 WEATHER SUNNYWATER DEPTH 11.00' TOP WELL WELL DEPTH 34' ± WELL MATERIAL PVC
 TOP CASING WELL DIAM. 2"WELL STICK-UP 2.39 WELL/CASING 0.23'SAMPLING EQUIPMENT USED Peristaltic / 5.5. Barlow VOLUME PURGED 4.97L
~~IN-LINE FILTER~~ VACUUM FILTERFIELD DATA COLLECTION IN SITU VOA LEVEL(PPM) AMBIENT 0.4 ppm
 IN BOTTLE SAMPLE LOCATION 0.4 ppm
HEADSPACE -SAMPLE PURGE DATA

<u>4</u> GAL	<u>8</u> GAL	<u>12</u> GAL	<u>-</u> GAL
TEMP <u>17.1</u> °C	TEMP <u>-</u> °C	TEMP <u>-</u> °C	TEMP <u>-</u> °C
SP. COND <u>2123</u> @25°C	SP. COND <u>-</u> @25°C	SP. COND <u>-</u> @25°C	SP. COND <u>-</u> @25°C
pH <u>7.3</u>	pH <u>-</u>	pH <u>-</u>	pH <u>-</u>
EN <u>-</u>	EN <u>-</u>	EN <u>-</u>	EN <u>-</u>

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL	ANALYSIS REQUESTED
100, 101		40ml	H ₂ O	No	4°C	VOA - NCLP - COP
102, 103		1-liter	H ₂ O	No	4°C	EXT. ORG. - NCLP - COP
104, 105		1-liter	H ₂ O	No	4°C	PEST/PCB NCLP-COP
106		1-liter	H ₂ O	YES	4°C	METALS NCLP-COP
107, 108		1-liter	H ₂ O	No	4°C	ORGANOPHOSPHORUS PEST. 840/930-840
109, 110		1-liter	H ₂ O	No	4°C	CHLORINATED HERBICIDE - 8150
111		250ml	H ₂ O	YES	4°C	CHLORIDE/SULPATE
112		125ml	H ₂ O	No	4°C	FLUORIDE
			

REMARKS/OBSERVATIONS 1 Volume = 3.7 gal.Purged well dry at 1 volume. Sample appeared clear - no odorSampled well next day - 9/2/87SAMPLER B.Schonard / J.M.Mulken

DG #1

465 COMM CHRM CODE: JMW101XNO1

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GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK No. 1 JOB NO 5139-00STATION NO/LOCATION MW-107 DATE 9-1-87SKETCH ON BACK PHOTOGRAPHS YES NO ROLL NO/EXPOSURE NO 5+9 9/2/87

FIELD DATA TIME: START 12:30⁹¹ AIR TEMP 75°F
 END 13:15⁹² WEATHER Partly Cloudy

WATER DEPTH 10.51 TOP WELL WELL DEPTH 11.5± WELL MATERIAL PVC
 TOP CASING WELL DIAM. 2"

WELL STICK-UP 3.25' WELL/CASING 0.24'SAMPLING EQUIPMENT USED Percustaltic / 5.5. Barlowe VOLUME PURGED .2 gal
IN-LINE FILTER Vacuum Filter

FIELD DATA COLLECTION IN SITU VOA LEVEL (PPM) AMBIENT 0.4 ppm
 IN BOTTLE SAMPLE LOCATION 0.4 ppm
 HEADSPACE -

SAMPLE PURGE DATA

<input checked="" type="checkbox"/>	<u>12</u> GAL	<input type="checkbox"/>	<u>-</u> GAL	<input type="checkbox"/>	<u>-</u> GAL	<input type="checkbox"/>	<u>-</u> GAL
TEMP	<u>15.6</u> °C	TEMP	<u>-</u> °C	TEMP	<u>-</u> °C	TEMP	<u>-</u> °C
SP. COND	<u>1317</u> @25°C	SP. COND	<u>-</u> @25°C	SP. COND	<u>-</u> @25°C	SP. COND	<u>-</u> @25°C
pH	<u>6.5</u>	pH	<u>-</u>	pH	<u>-</u>	pH	<u>-</u>
EN	<u>-</u>	EN	<u>-</u>	EN	<u>-</u>	EN	<u>-</u>

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
113,114		40ml	H ₂ O	No	4°C	VOA - NCLP - COP
115,116		1-liter	H ₂ O	No	4°C	EXT. ORG. - NCLP - COP
117,118		1-liter	H ₂ O	No	4°C	PEST/PCB NCLP-COP
119		1-liter	H ₂ O	YES	4°C	METALS NCLP-COP
120,121		1-liter	H ₂ O	No	4°C	ORGANOPHOSPHORUS PEST. 8140/330-8140
122,123		1-liter	H ₂ O	No	4°C	CHLORINATED HERBICIDE - 8150
124		250ml	H ₂ O	YES	4°C	CHLORIDES/SULFATE
125		125ml	H ₂ O	No	4°C	FLUORIDE
			

REMARKS/OBSERVATIONS 1 Volume = .2 gal

Purged dry at 1 volume. Sample appears turbid brown color

Sampled next day 9-2-87

SAMPLER B. Schoenard / J. M. Mullen ..

DB # 4

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PAGE _____ OF _____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK No. 1 JOB NO 5139-00STATION NO/LOCATION MW-108 DATE 4-1-87SKETCH ON BACK YES NO REP #1, 2, 3 PHOTOGRAPHS YES NO ROLL NO/EXPOSURE NO 1-3FIELD DATATIME: START 13:15 AIR TEMP 75°FEND 14:00 WEATHER Partly Cloudy15:00WATER DEPTH 8.46' TOP WELL WELL DEPTH 13' ± WELL MATERIAL PVC
 TOP CASING WELL DIAM. 2"WELL STICK-UP 2.50 WELL/CASING 0.13SAMPLING EQUIPMENT USED Peristaltic / 5.5. Barlow VOLUME PURGED .8 gal
IN-LINE FILTER VACUUM FILTERFIELD DATA COLLECTION IN SITU VOA LEVEL(PPM) AMBIENT -4
 IN BOTTLE SAMPLE LOCATION -4
HEADSPACE -SAMPLE PURGE DATA

<u>1</u>	<u>.8</u> GAL	<u>1</u>	<u>-</u> GAL	<u>1</u>	<u>-</u> GAL	<u>1</u>	<u>-</u> GAL
TEMP	<u>15.6</u> °C	TEMP	<u>-</u> °C	TEMP	<u>-</u> °C	TEMP	<u>-</u> °C
SP. COND	<u>1130</u> @25°C	SP. COND	<u>-</u> @25°C	SP. COND	<u>-</u> @25°C	SP. COND	<u>-</u> @25°C
pH	<u>6.1</u>	pH	<u>-</u>	pH	<u>-</u>	pH	<u>-</u>
EN	<u>-</u>	EN	<u>-</u>	EN	<u>-</u>	EN	<u>-</u>

Rep #3	BOTTLE ID	LAB ID Rep #1, Rep #2	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
514, 515	126, 127	501, 502	507, 508	40ml	H ₂ O	No	VOC
516, 517	128, 129	503, 504	509, 510	1-liter	H ₂ O	No	4°C
518, 519	130, 131	504, 505	511, 512	1-liter	H ₂ O	No	4°C
520	132	506	513	1-liter	H ₂ O	YES	4°C
	133, 134			1-liter	H ₂ O	No	4°C
	135, 136			1-liter	H ₂ O	No	4°C
	137			750ml	H ₂ O	YES	4°C
	138			125ml	H ₂ O	No	4°C

REMARKS/OBSERVATIONS / Volume = .8 gal

Purged Dry at 1 Volume - Sample Appearance: Clear with silts in bottom of well, when agitated sample became SAMPLER B. Schoenard / J. McMullen
turbid (Brown). DR #3

CHES COMMON CHEM CODE: JMW108XX01

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PAGE ____ OF ____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK NO. 1 JOB NO 5139-00STATION NO/LOCATION MW - 109 DATE 9-1-97SKETCH ON BACK YES NO PHOTOGRAPHS YES NO ROLL NO/EXPOSURE NO 14-5FIELD DATA TIME: START 11:30 AIR TEMP 80°F
END 18:00 WEATHER SunnyWATER DEPTH 8.23' TOP WELL WELL DEPTH 12' ± WELL MATERIAL PVC
 TOP CASING WELL DIAM. 2 1/2"WELL STICK-UP 2.45 WELL/CASING 13'SAMPLING EQUIPMENT USED Pesticlatic / 5.5. Barlow VOLUME PURGED 1 gal
IN-LINE FILTERFIELD DATA COLLECTION IN SITU VOA LEVEL (PPM) AMBIENT 1.0
 IN BOTTLE SAMPLE LOCATION 1.0
HEADSPACE -

<u>SP. COND</u> <u>.5</u> <u>GAL</u>	<u>SP. COND</u> <u>1</u> <u>GAL</u>	<u>SP. COND</u> <u>1.5</u> <u>GAL</u>	<u>SP. COND</u> <u>-</u> <u>GAL</u>
TEMP <u>15.6</u> °C	TEMP <u>15.3</u> °C	TEMP <u>-</u> °C	TEMP <u>-</u> °C
SP. COND <u>697</u> @ <u>25°C</u>	SP. COND <u>937</u> @ <u>25°C</u>	SP. COND <u>-</u> @ <u>25°C</u>	SP. COND <u>-</u> @ <u>25°C</u>
pH <u>6.8</u>	pH <u>6.6</u>	pH <u>-</u>	pH <u>-</u>
EN <u>-</u>	EN <u>-</u>	EN <u>-</u>	EN <u>-</u>

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
139, 140	152, 153	40ml	H ₂ O	No	4°C	VOA - NCLP - COP
141, 142	154, 155	1-liter	H ₂ O	No	4°C	Ext. ORG. - NCLP - COP
143, 144	156, 157	1-liter	H ₂ O	No	4°C	PEST/PCB NCLP-COP
145	158	1-liter	H ₂ O	YES	4°C	METALS NCLP - COP
146, 147	159, 160	1-liter	H ₂ O	No	4°C	ORGANOPHOSPHORUS PEST. 8140/3350-8140
148, 149	161, 162	1-liter	H ₂ O	No	4°C	CHLORINATED HERBICIDE - 8150
150	163	250ml	H ₂ O	YES	4°C	CHLORIDE/SULFATE
151	164	125ml	H ₂ O	No	4°C	FLUORIDE
			

REMARKS/OBSERVATIONS 1 Volume = 16 gal
Purged Dry at 2 volumes. Sample Appearance: Turbid - Light Gray Silts + FinesSAMPLER A.Schoenard/J. McMillen
DB#2Dup 1 matches Compu chem codes JDUP-1xx01
CHES COMPAN CHEM CODE: JMW109xx01

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PAGE _____ OF _____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK NO. 1 JOB NO 5139-00STATION NO/LOCATION SB - 1 DATE 9-2-87SKETCH ON BACK PHOTOGRAPHS ROLL NO/EXPOSURE NO NA

FIELD DATA TIME: START 11:30 AIR TEMP 75°F
 END 12:00 WEATHER SUNNY

WATER DEPTH NA TOP WELL WELL DEPTH NA WELL MATERIAL NA
 TOP CASING WELL DIAM. NA

WELL STICK-UP NA WELL/CASING NASAMPLING EQUIPMENT USED / 5.5. Barlow IN-LINE FILTER VOLUME PURGED NA

FIELD DATA COLLECTION IN SITU VOA LEVEL (PPM) AMBIENT NA
 IN BOTTLE NA SAMPLE LOCATION NA
 HEADSPACE NA

SAMPLE PURGE DATA

(<u>0</u>) <u>GAL</u>			
TEMP <u>— °C</u>	TEMP <u>— °C</u>	TEMP <u>— °C</u>	TEMP <u>— °C</u>
SP. COND <u>— @25°C</u>			
pH <u>—</u>	pH <u>—</u>	pH <u>—</u>	pH <u>—</u>
EN <u>—</u>	EN <u>—</u>	EN <u>—</u>	EN <u>—</u>

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED PRES./VOL.	ANALYSIS REQUESTED
165, 166		40ml	H ₂ O	No	VOA - NCLP - COP
167, 168		1-liter	H ₂ O	No	EXT. ORG. - NCLP - COP
169, 170		1-liter	H ₂ O	No	PEST/PCB NCLP-COP
171		1-liter	H ₂ O	YES	METALS NCLP-COP
172, 173		1-liter	H ₂ O	No	ORGANOPHOSPHORUS PEST. 840/330-840
174, 175		1-liter	H ₂ O	No	CHLORINATED HERBICIDE -8150
176		250ml	H ₂ O	YES	CHLORIDE/SULFATE
177		125ml	H ₂ O	No	FLUORIDE

REMARKS/OBSERVATIONS 1 Volume = NA

Fitter Sample Blank done in field with
 tank water from C.C. Jordan Staging area. SAMPLER R. Schoenard / T. M. Miller
(S.S. Barlow)

CHES COMMON CHRM CODE: JSBL-1XX01

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PAGE ____ OF ____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK NO. 1 JOB NO 5139-00STATION NO/LOCATION FB-1 DATE 9.2.87SKETCH ON BACK YES NO PHOTOGRAPHS YES NO ROLL NO/EXPOSURE NO NA

FIELD DATA TIME: START 11:00 AIR TEMP 75°F
END 11:15 WEATHER SUNNY

WATER DEPTH NA TOP WELL WELL DEPTH NA WELL MATERIAL NA
 TOP CASING WELL DIAM. NA

WELL STICK-UP NA WELL/CASING NASAMPLING EQUIPMENT USED VACUUM P.H./S.S. DRAFTER VOLUME PURGED NA
~~IN-LINE FILTER~~

FIELD DATA COLLECTION IN SITU VOA LEVEL(PPM) AMBIENT NA
 IN BOTTLE SAMPLE LOCATION NA
HEADSPACE NA

SAMPLE PURGE DATA

<u>QD</u> <u>GAL</u>	<u>QD</u> <u>GAL</u>	<u>QD</u> <u>GAL</u>	<u>QD</u> <u>GAL</u>
TEMP <u>°C</u>	TEMP <u>°C</u>	TEMP <u>°C</u>	TEMP <u>°C</u>
SP.COND <u>Ω25°C</u>	SP.COND <u>Ω25°C</u>	SP.COND <u>Ω25°C</u>	SP.COND <u>Ω25°C</u>
pH <u>—</u>	pH <u>—</u>	pH <u>—</u>	pH <u>—</u>
EN <u>—</u>	EN <u>—</u>	EN <u>—</u>	EN <u>—</u>

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
		40ml	H ₂ O	NA	4°C	VOA-NCLP-COP
		1-liter	H ₂ O	NA	4°C	EXT.ORG.-NCLP-ZOP
		Filter	H ₂ O	NA	4°C	TEST/PCB NCLP-COP
184		1-liter	H ₂ O	YES	4°C	METALS NCLP-COP
		1-liter	H ₂ O	NA	4°C	ORGANOPHOSPHORUS
		1-liter	H ₂ O	NA	4°C	TEST/PCB NCLP-ZOP
189		200ml	H ₂ O	YES	4°C	CHLORIDE/SULFATE
		125ml	H ₂ O	NO	4°C	FLUORIDE
		

REMARKS/OBSERVATIONS / Volumes = NA

Filter Blank Made up in field with blank
filter from Staging area (vacuum filter)

SAMPLES BY (Signature) /S. McMullen/

HES COMMON CHEM CODE: JFBL-1XX01

ECJORDANCO

PAGE _____ OF _____

GROUNDWATER FIELD SAMPLE DATA RECORD

PROJECT STEWART ANG TASK NO. 1 JOB NO 5139-00

STATION NO/LOCATION TB-1 DATE 9.2.87

SKETCH ON BACK PHOTOGRAPHS ROLL NO/EXPOSURE NO NA

FIELD DATA TIME: START 12:00 AIR TEMP 75°F
END 12:15 WEATHER SUNNY

WATER DEPTH NA TOP WELL
 TOP CASING WELL DEPTH NA WELL MATERIAL NA
WELL DIAM. NA

WELL STICK-UP NA WELL/CASING NA

SAMPLING EQUIPMENT USED NA / S.S. Filter VOLUME PURGED NA
IN-LINE FILTERS

FIELD DATA COLLECTION IN SITU VOA LEVEL(PPM) AMBIENT NA
 BOTTLE NA SAMPLE LOCATION
HEADSPACE

SAMPLE PURGE DATA
 GAL GAL GAL GAL
TEMP °C TEMP °C TEMP °C TEMP °C
SP.COND @25°C SP.COND @25°C SP.COND @25°C SP.COND @25°C
pH pH pH pH
EN EN EN EN

BOTTLE ID	LAB ID	VOL	MATERIAL	FILTERED	PRES./VOL.	ANALYSIS REQUESTED
191, 192		40ml	H ₂ O	No	8°C	VOA - NCLP - Co ⁶⁰
		1-liter	H ₂ O	No	8°C	EXT. O&G. - NCLP - Co ⁶⁰
		1-liter	H ₂ O	No	8°C	ASST/PCB NCLP - Co ⁶⁰
		1-liter	H ₂ O	YES	8°C	METALS - NCLP - Co ⁶⁰
		1-liter	H ₂ O	No	8°C	ORGANOPHOSPHORUS TEST: 810/530-810
		1-liter	H ₂ O	No	8°C	CHLORINATED HERBICIDE - 8150
		2ml	H ₂ O	YES	8°C	ANIONIC/SULFATE
		125ml	H ₂ O	No	8°C	FLUORIDE
			

REMARKS/OBSERVATIONS / Volume = NA

Trip Blanks done in field with C.C.Jordan
Blank water from Staging Area.

SAMPLER B. Schaeffer / S. McMillen

APPENDIX G
DAMES AND MOORE - BORING AND MONITORING WELL DATA

MAJOR DIVISIONS			GRAPH SYMBOL	LETTER SYMBOL	TYPICAL DESCRIPTIONS
COARSE GRAINED SOILS	'GRAVEL AND GRAVELLY SOILS MORE THAN 50% OF COARSE FRAGMENT RETAINED ON NO. 4 SIEVE'	CLEAN GRAVELS (LITTLE OR NO FINES)		GW	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES
		GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines
		CLEAN SAND (LITTLE OR NO FINES)		GM	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES
	SAND AND SILTY SOILS MORE THAN 50% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE MORE THAN 50% OF COARSE FRAGMENT PASSING NO. 4 SIEVE	CLEAN SAND (LITTLE OR NO FINES)		GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SP	Poorly-graded sands, gravelly sands, little or no fines
FINE GRAINED SOILS	SILTS AND CLAYS LIQUID LIMIT LESS THAN 50 MORE THAN 50% OF MATERIAL IS SMALLER THAN NO. 200 SIEVE SIZE	SILTS AND CLAYS LIQUID LIMIT LESS THAN 50		SM	SILTY SANDS, SAND-SILT MIXTURES
		SILTS AND CLAYS LIQUID LIMIT LESS THAN 50		SC	CLAYEY SANDS, SAND-CLAY MIXTURES
		SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50		ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
		SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
		SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50		OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
		SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50		MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
		HIGHLY ORGANIC SOILS		CH	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS
		HIGHLY ORGANIC SOILS		OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
		HIGHLY ORGANIC SOILS		PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BOUNDARLING SOIL CLASSIFICATIONS.

SOIL CLASSIFICATION CHART

UNIFIED SOIL CLASSIFICATION SYSTEM

DAMES & MOORE
BORING LOG

Page 1 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-1
SURFACE ELEV: 436.0'

DRILLING METHOD: Hollow stem auger

SAMPLING METHOD: Split spoon

DATE STARTED: 9/12/85

DATE FINISHED: 9/16/85

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
1	48	SS	0		Brown moist silt and fine to medium sand, little medium gravel grading to brownish-gray, silt, dry, some fine gravel and coarse sand, little coarse to medium gravel Hnu=0ppm
			1	SM	
			2	--	
			3	ML	
			4		Gray dry silt, little fine to medium gravel, little sand Hnu=0ppm
2	103	SS	5		boulder drilled at 8.0'
			6		
			7		
			8		
			9		
3	88	SS	10		grades to some sand, little fine to coarse gravel Hnu=0ppm
			11		
			12		
			13		
			14		
4	128	SS	15		cobble at 15.0'
			16		
			17		
			18		
			19		
5	77	SS	20		

FIGURE A-2A

DAMES & MOORE
BORING LOG

Page 2 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-1

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
			20		
			21		
			22		
			23		boulder at 23.0'
			24		
6	108	SS	25		grades to little sand
			26		Hnu=<0ppm
			27		
			28	ML	
			29		
7	146	SS	30		Hnu=<1ppm
			31		
			32		
			33		
			34		
8	80/2"	SS	35		Hnu=<1ppm
			36		
			37		
			38		Brown with iron staining, fissile,
			39		weathered shale, dry to moist wet zone
			40		from 40'1" to 40'2", some silt
9	100/3"	SS			

FIGURE A-28

DAMES & MOORE
BORING LOG

Page 3 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-1

SAMPLE NO.	BLows/ft	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
			40	WEATHERED	
			41		
			42		
			43		
			44		
10	100/5"	SS	45	ROCK	grades to gray, dry with iron staining
			46		
			47		
			48		Bedrock, spoon refusal, no sample Hnu=0ppm
			49		
	100/0"		50		Boring terminated at a depth of 50.0 feet on 9/16/85

NOTE: Hnu readings are field detections of organic vapors given off by soil samples; measured with an Hnu photoionization meter set to a 9.8 span.

DAMES & MOORE
BORING LOG

Page 1 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-2
SURFACE ELEV: 433.5'

DRILLING METHOD: Hollow stem auger

SAMPLING METHOD: Split spoon

DATE STARTED: 9/18/85
DATE FINISHED: 9/19/85

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
1	32	SS	0		Brown, mottled dry to moist, fine sand and silt, little fine gravel Hnu=0ppm
			1		
			2	SP	
			3		
			4		
2	100	SS	5	SM	Brown, dry fine sand, little fine to medium gravel Hnu=0ppm
			6		
			7		Brown, moist, fine sand, little medium to coarse sand and fine gravel, trace silt Hnu=0ppm
			8	SP	
			9		
3	92	SS	10		grades to dry, less gravel
			11		
			12		
			13		Gray, moist, silt, little fine to medium gravel, little fine sand Hnu=0ppm
			14		
4	75	SS	15		
			16	ML	
			17		
			18		
			19		
			20		

DAMES & MOORE
BORING LOG

Page 2 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-2

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
			20		
	100/5"		21		no soil sample; cuttings are gray silt drilled boulder at 21 feet
			22		
			23		
			24		
5	80	SS	25		grades to dry to slightly moist, little fine to medium sand, little fine to coarse gravel Hnu=10ppm
			26		
			27	ML	
			28		
			29		
6	20/1"	SS	30		no soil sample; cuttings are gray silt
			31		
			32		
			33		
			34		
7	100/1"	SS	35		Brown-gray with iron stains, weathered, slightly metamorphosed shale Hnu=200ppm
			36		
			37		
			38		
			39		
8	100/1/2"	SS	40	ROCK	Hnu=8ppm

FIGURE A-3B

DAMES & MOORE
BORING LOG

Page 3 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-2

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
			40		
			41		
			42		
			43		
			44		
100/0"	SS	45		B E D R O C K	Spoon bounces; bedrock
			46		
			47		
			48		
			49		
50/0"		50			Boring terminated at a depth of 50.0 feet on 9/19/85

NOTE: Hnu readings are field detections of organic vapors given off by soil samples; measured with an Hnu photoionization meter set to a 9.8 span.

FIGURE A-3C

DAMES & MOORE
BORING LOG

Page 1 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-3
SURFACE ELEV: 432.6'

DRILLING METHOD: Hollow stem auger

SAMPLING METHOD: Split spoon

DATE STARTED: 9/24/85
DATE FINISHED: 9/26/85

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
1	46	SS	0		Gray-brown, dry to slightly moist, mottled fine sand, some fine to medium gravel, little silt Hnu=0ppm boulder at 3.0'
			1		
			2		
			3		
			4		
2	31	SS	5		grades to mottled, tan-light brown, moist Hnu=0ppm boulder at 8.0'
			6		
			7		
			8		
			9		
3	74	SS	10		Hnu=0ppm boulder at 12.0'
			11		
			12		
			13		
			14		
4	52	SS	15		Tan to light brown, moist, fine sand, some fine to coarse gravel, trace silt Hnu=0ppm
			16		
			17		
			18		
			19		
5	86	SS	20	SM	Yellow-tan, dry to slightly moist, fine

FIGURE A-4A

DAMES & MOORE
BORING LOG

Page 2 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-3

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPH	MATERIAL DESCRIPTION
			20		sand and silt, little fine to medium gravel
			21	SM	grades to brown, dry, no gravel
			22	-----	grades to gray slightly moist
			23		Gray, slightly moist silt, some fine to medium gravel, some fine sand Hnu=0ppm
			24		
6	50/6"	SS	25		
			26		
			27		
			28		
			29		
7	50/3"	SS	30		cobble at 30.0' grades to dry, little fine to coarse gravel Hnu=0ppm
			31	ML	
			32		
			33		
			34		
8	70/1/2"	SS	35		grades to no gravel Hnu=0ppm
			36		
			37		
			38		
			39		
	50/1/2"		40		grades to light gray silt and gravel

FIGURE A-4B

DAMES & MOORE
BORING LOG

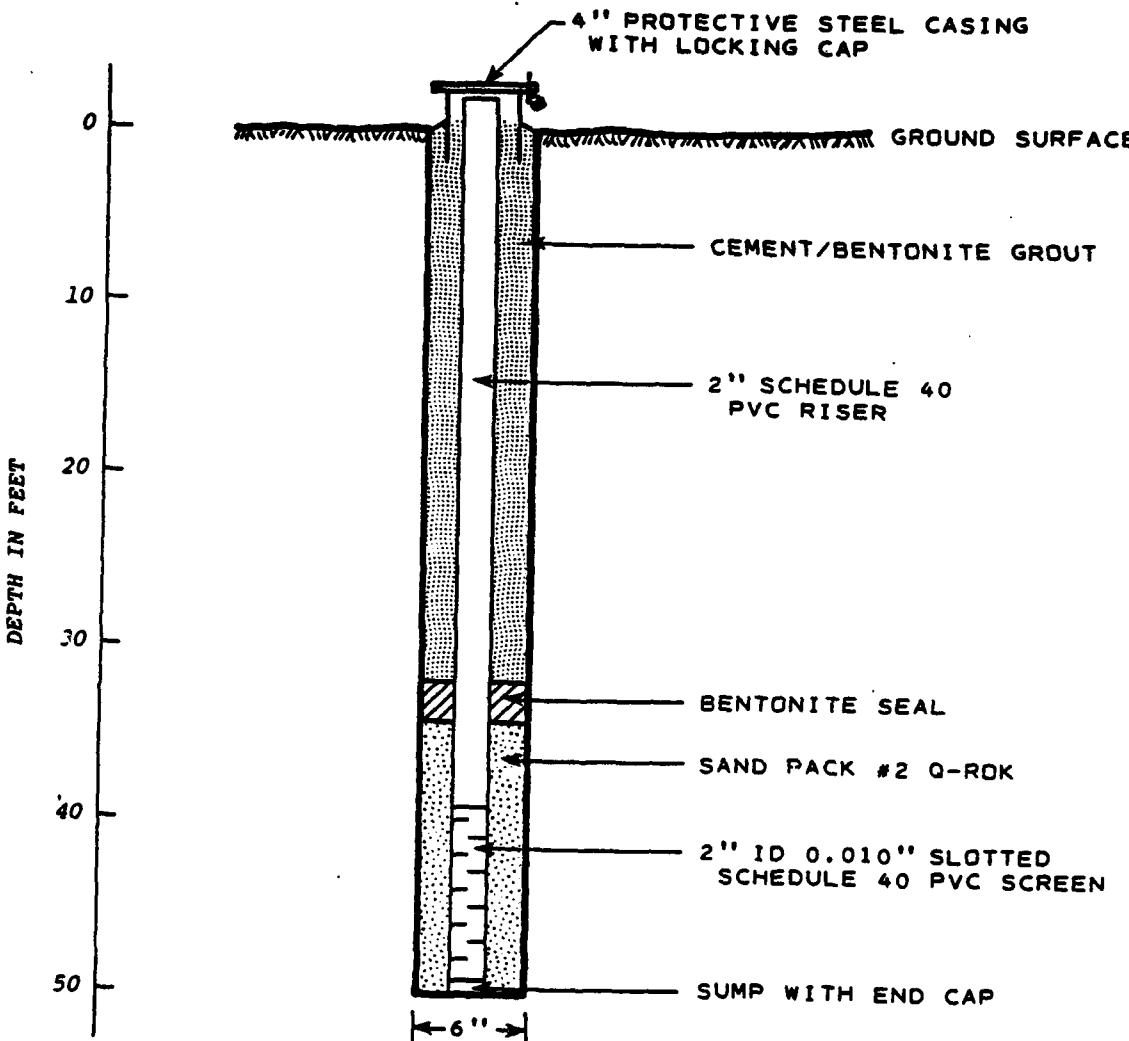
Page 3 of 3

CLIENT: STEWART AIR NATIONAL GUARD BASE
LOCATION: NEWBURGH, NY

BORING NO.: SW-3

SAMPLE NO.	BLOWS/FT	SAMPLE TYPE	DEPTH IN FT.	SOIL GRAPE	MATERIAL DESCRIPTION
			49		Hnu=0 ppm
			41	ML	
			42		
			43		Weathered rock Hnu=0 ppm
			44		
9	70/1"	SS	45		Shale drilled easy from 44 1/2 to 45 feet bedrock Hnu=0 ppm
			46		
			47		
			48		
			49		Boring terminated at a depth of 49.5 feet on 9/26/85
			50		

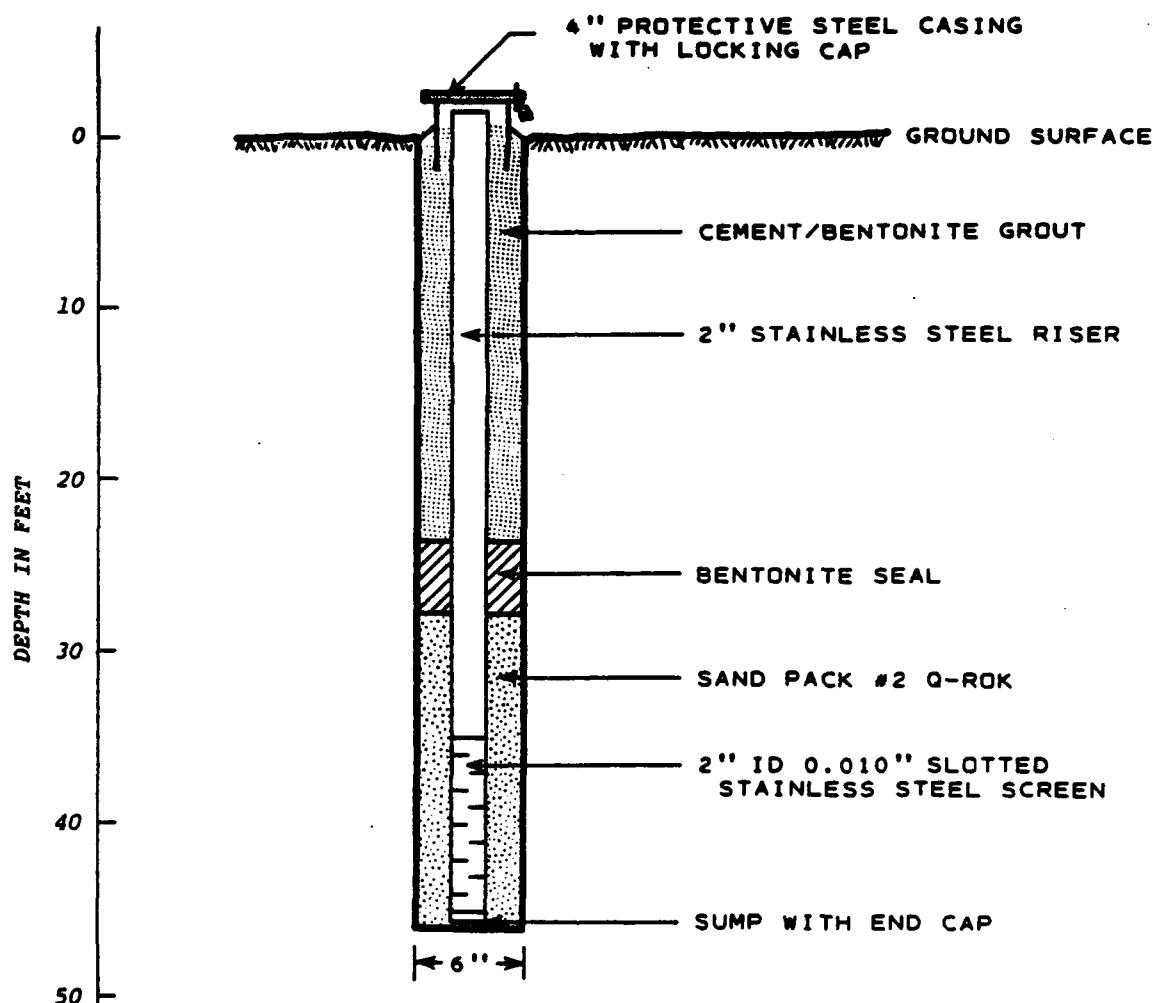
NOTE: Hnu readings are field detections of organic vapors given off by soil samples; measured with an Hnu photoionization meter set to a 9.8 span.



WELL SCHEMATIC
SW-1

SHANES & MOORE

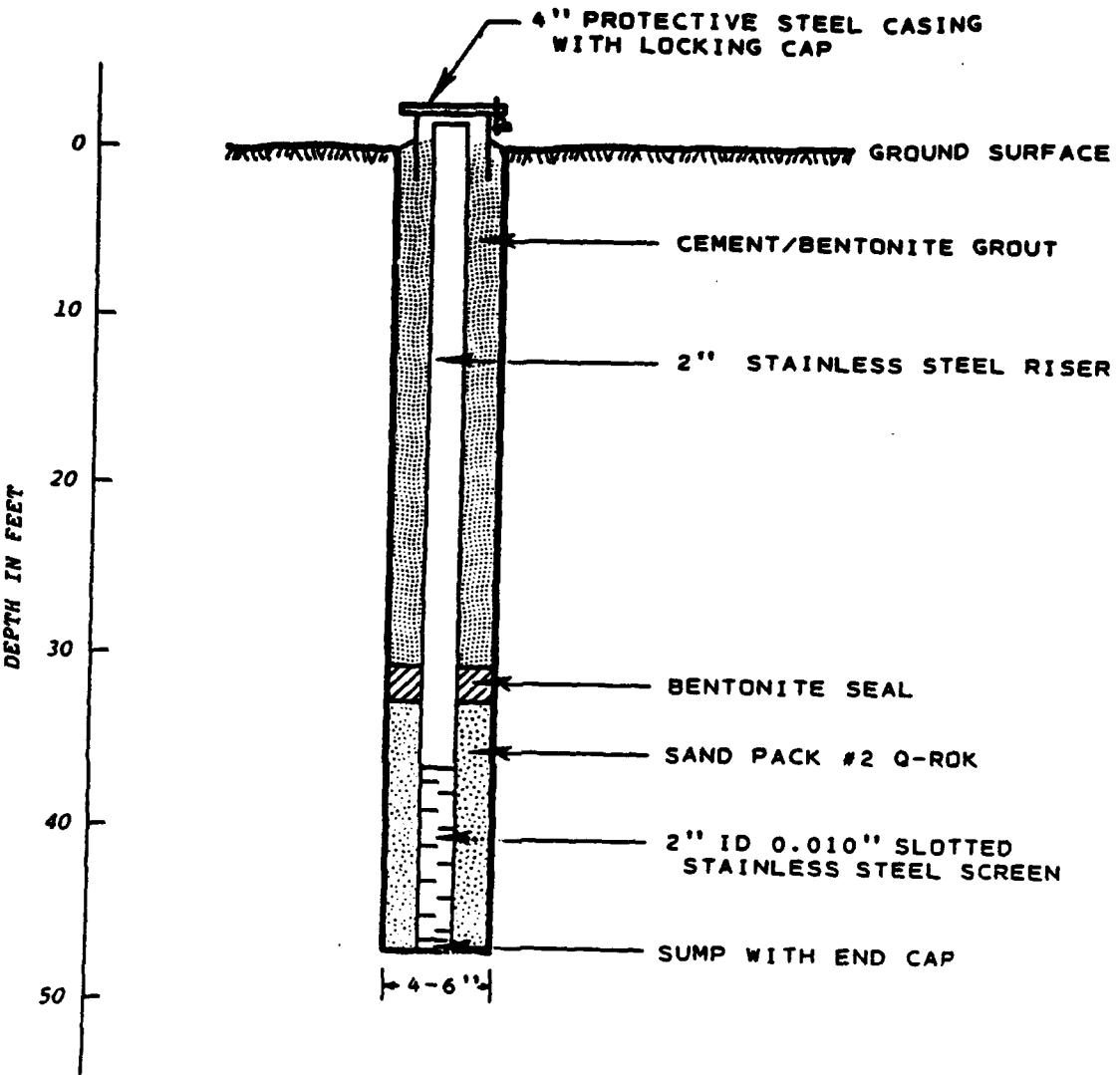
FIGURE A-5



WELL SCHEMATIC
SW-2

SHANNON & MOORE

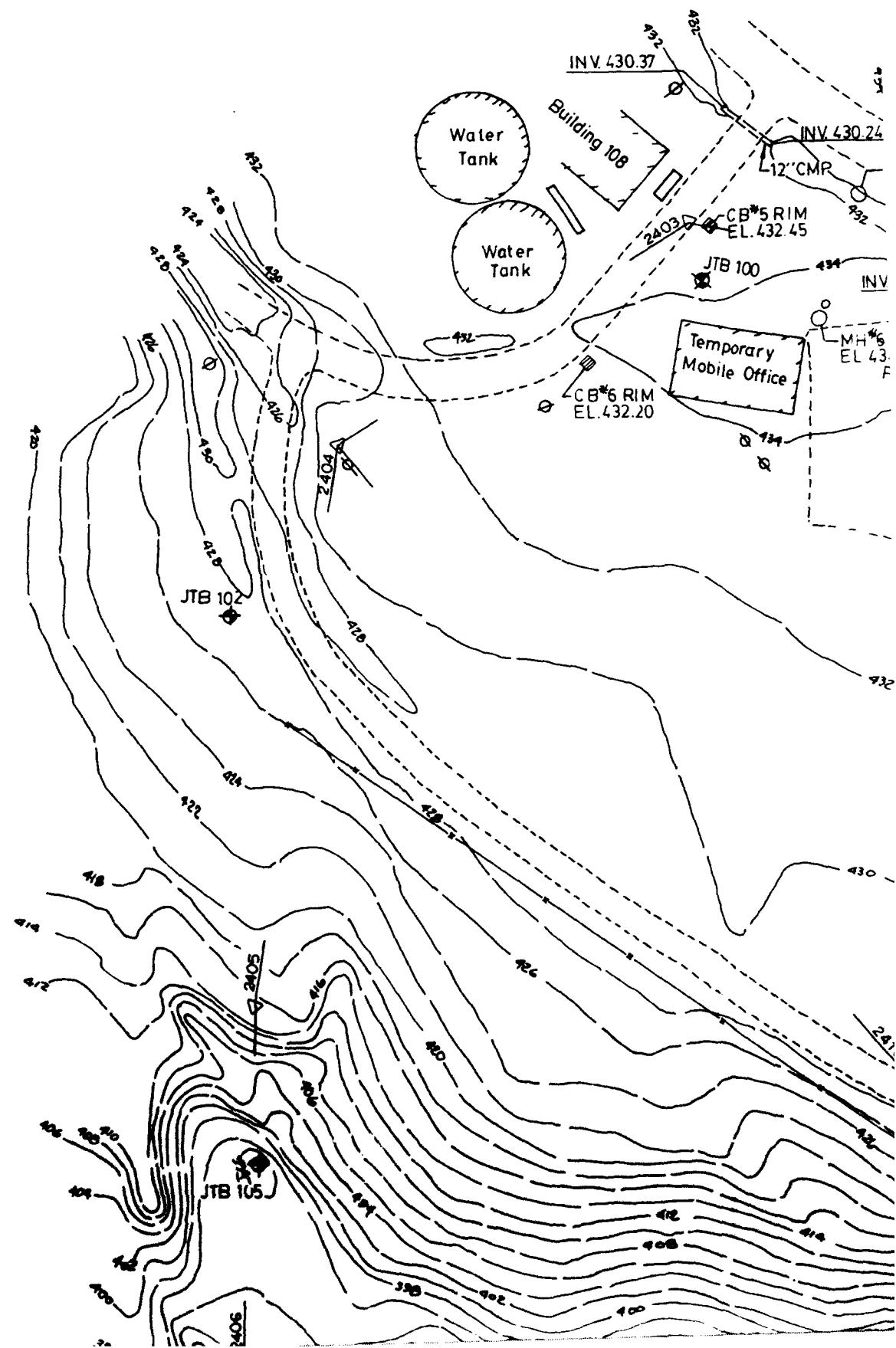
FIGURE A-6

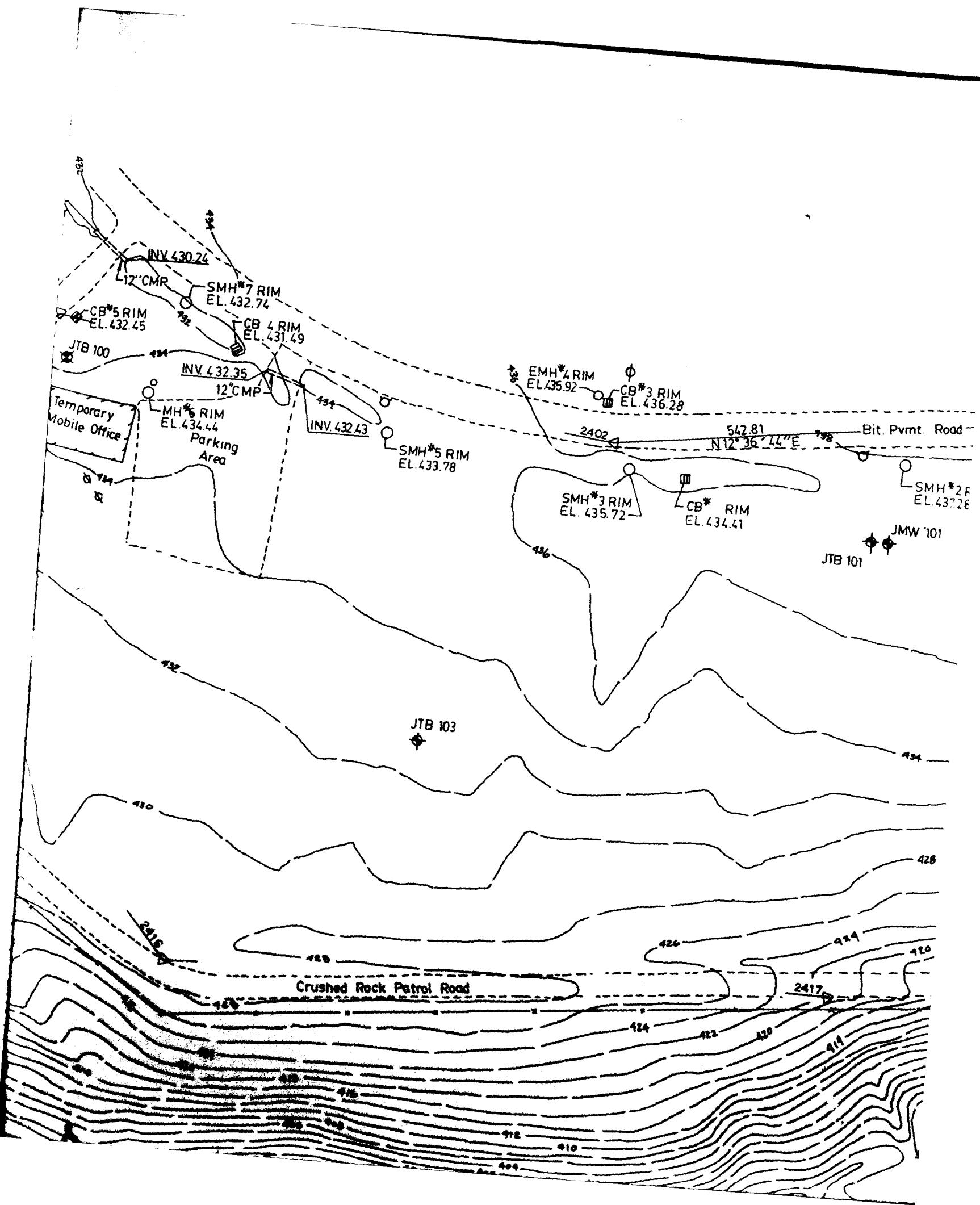


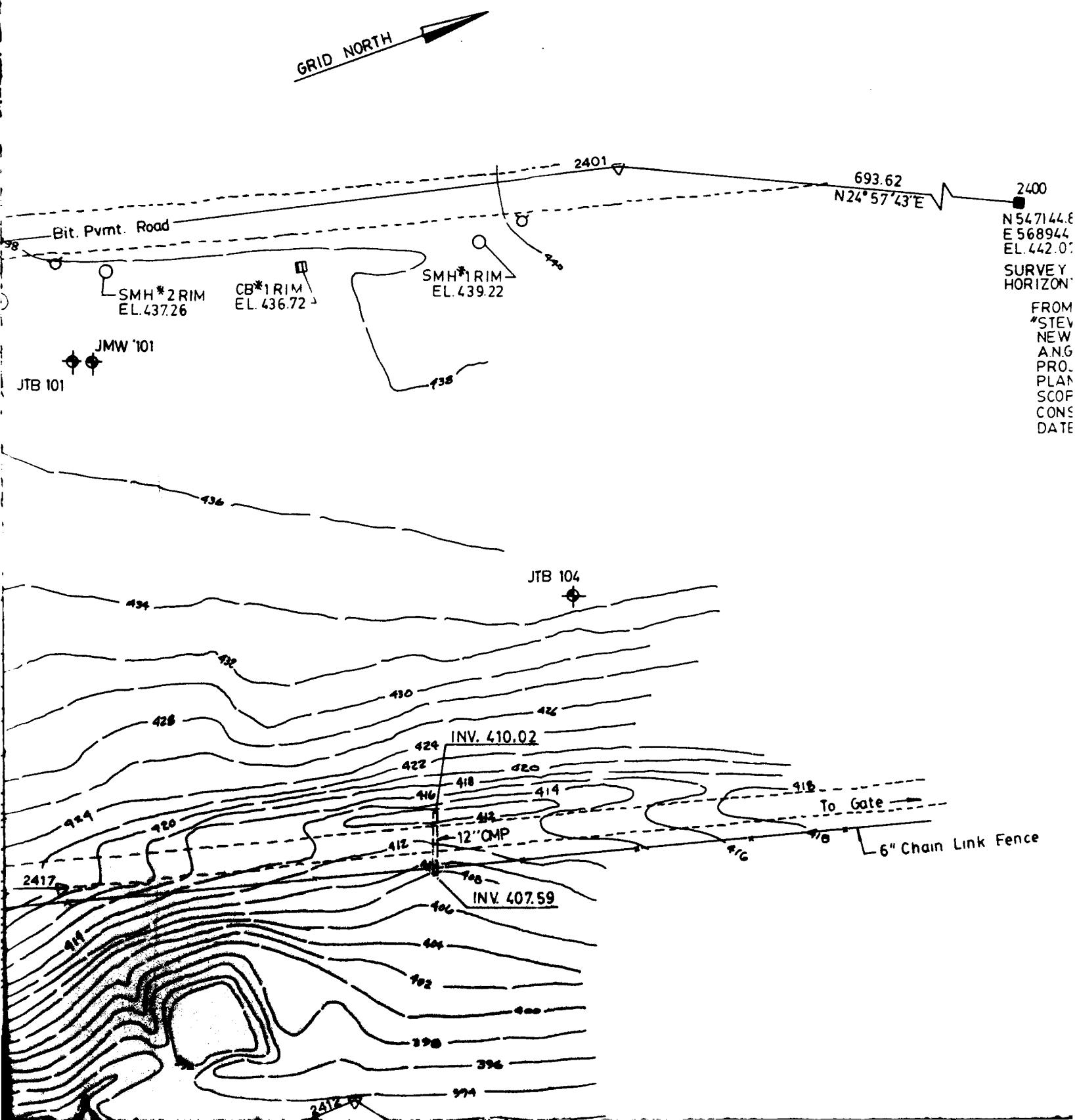
WELL SCHEMATIC
SW-3

DANNE B. MOORE

FIGURE A-7







01
 693.62
 N24°57'43"E
 2400
 N 547144.81
 E 568944.85
 EL.442.07

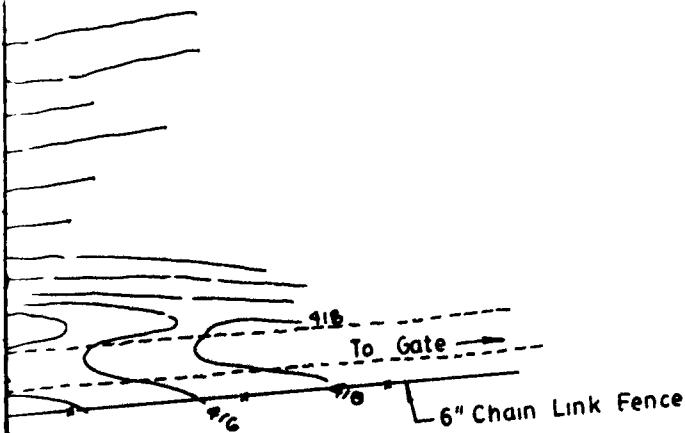
SURVEY MONUMENT USED FOR
 HORIZONTAL & VERTICAL CONTROL

FROM PLAN,
 "STEWART INT. AIRPORT
 NEWBURGH, NEW YORK
 A.N.G. & USMC R INSTALLATION
 PROJECT NO. 43164 (B) SITE
 PLAN PREPARATION PROJECT
 SCOPE. TRANSPALN ENGINEERING
 CONSULTING ENGINEERS SHT.2
 DATED 2/24/86"

STEWART A.

JTB AND JMW F

WELL INDENT.	GROUND ELEV.	TOP RIS
JTB 104	435.54	A=437.62 B=
JMW 101	437.83	440.00
JTB 101	437.64	A=439.50 B=
JTB 103	432.54	A=434.56 B=
JTB 100	433.93	A=436.06 B=
JTB 102	427.62	A=430.27 B=
JTB 105	392.69	A=394.23 B=
JMW 107	364.14	367.21
JTB 107	364.79	A=367.15 B=
JMW 108	373.28	370.73
JTB 108	372.28	A=370.10 B=
JMW 109	377.02	374.32
JTB 109	371.72	A=374.01 B=
JTB 106	386.97	A=389.78 B=THEADKD
JTB 110	361.34	A=THEADKD B=363.98

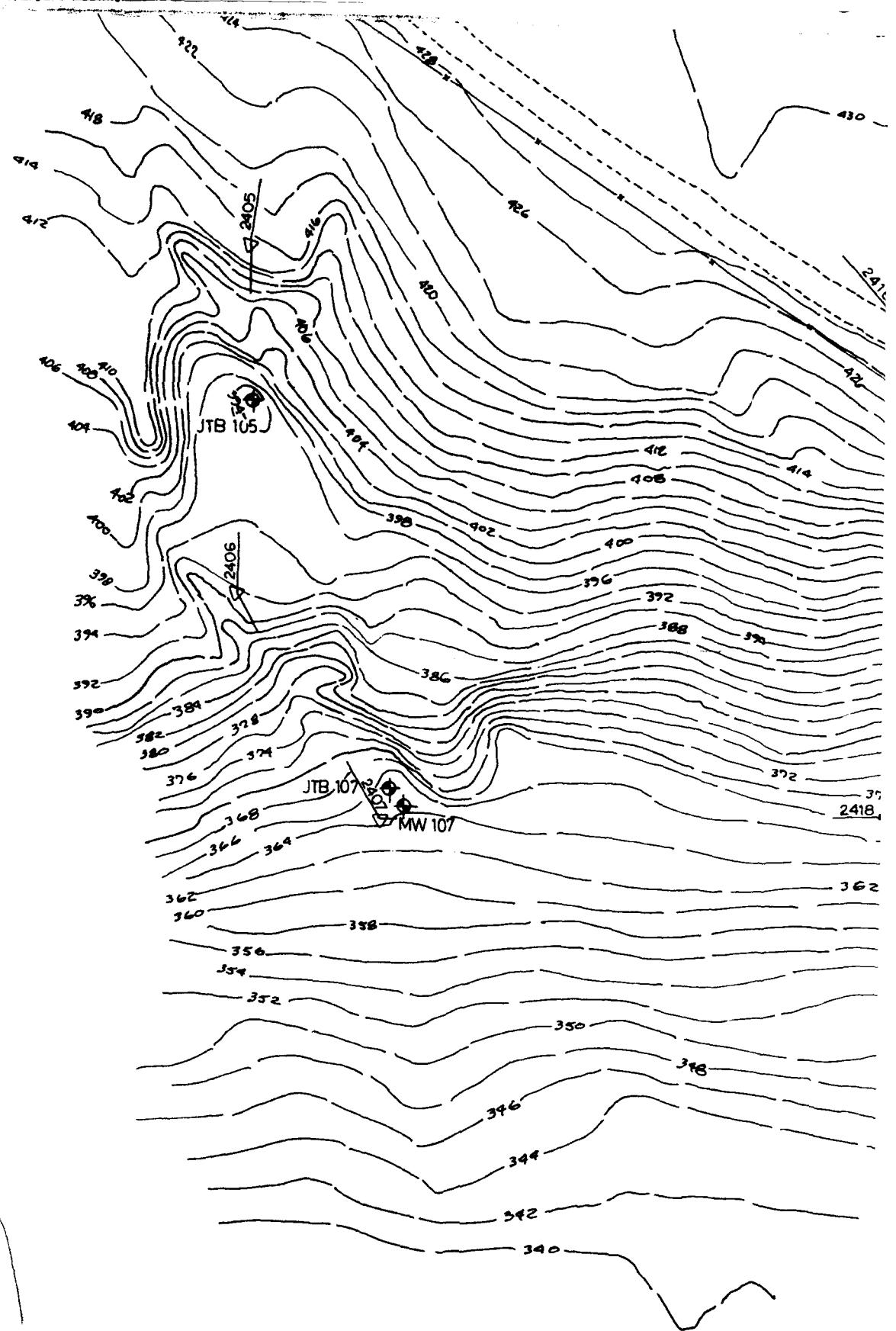


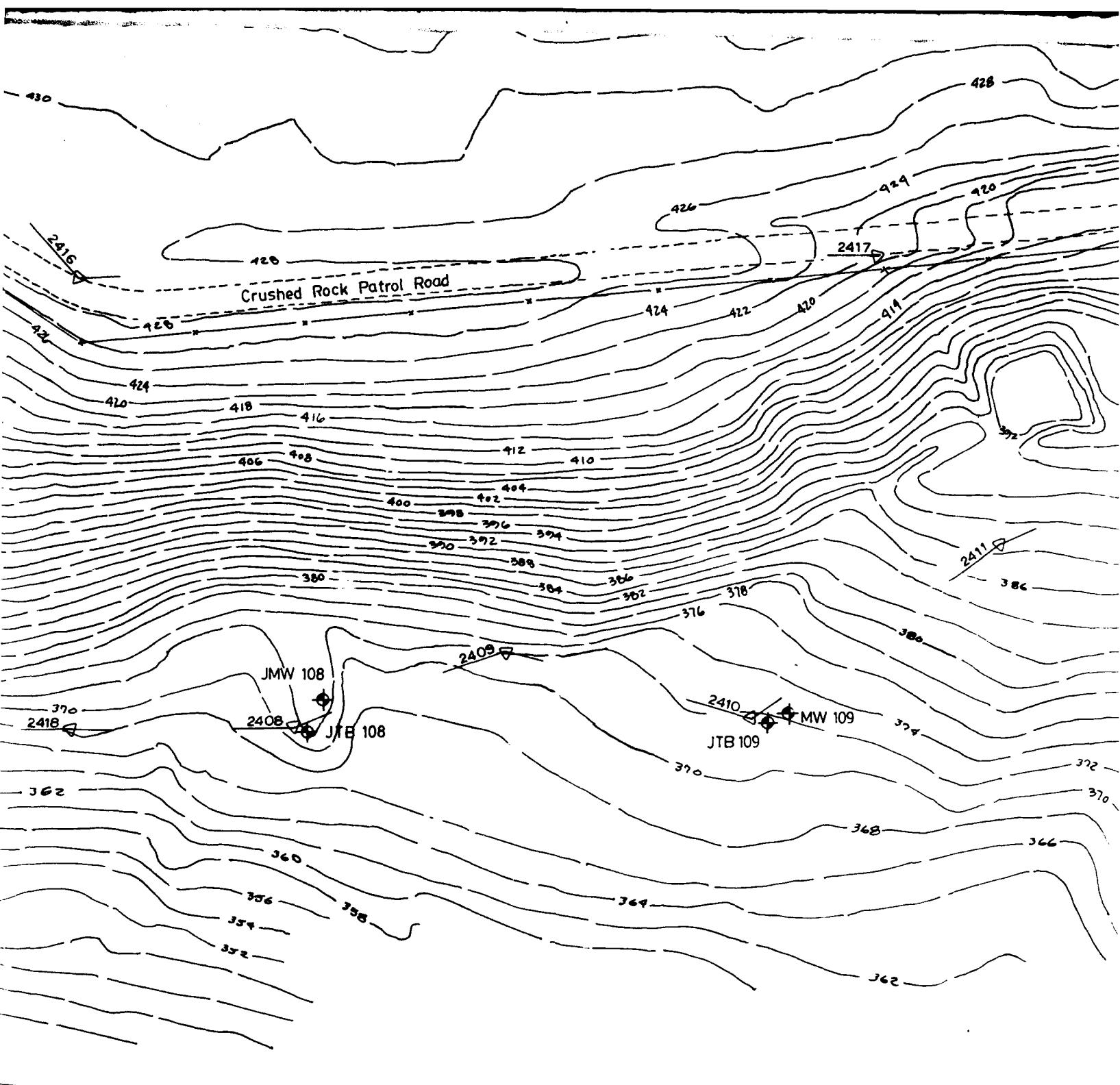
MONUMENT USED FOR
AL & VERTICAL CONTROL

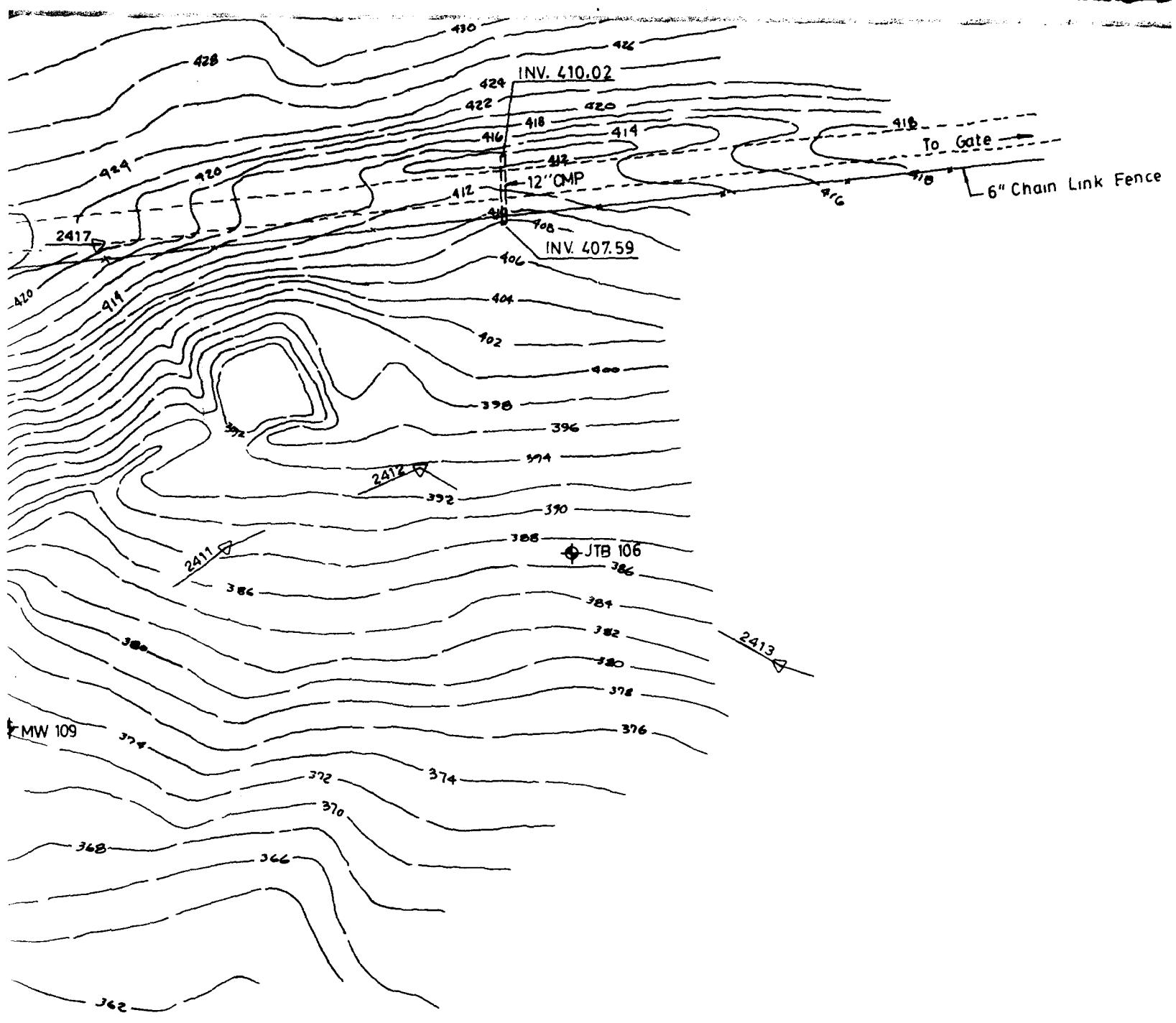
PLAN,
ART INT. AIRPORT
URGH NEW YORK
& USMC INSTALLATION
ECT NO. 43164 (B) SITE
PREPARATION PROJECT
TRANSPLAN ENGINEERING
LTING ENGINEERS SHT.2
2/24/86"

STEWART A.F.B.

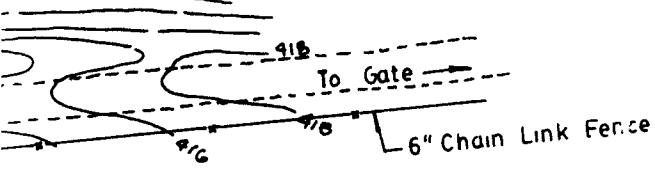
WELL INDENT.	GROUND ELEV.	JTB AND JMW EKV DATA		
		TOP RISER ELEV.	TOP CASING ELEV.	
JTB 104	435.54	A=437.62 B=437.69 C=437.69		437.95
JMW 101	437.83	440.00		440.21
JTB 101	437.64	A=439.50 B=439.65		440.15
JTB 103	432.54	A=434.56 B=434.71		435.48
JTB 100	433.93	A=436.06 B=436.29		436.60
JTB 102	427.62	A=430.27 B=430.37 C=430.27		430.36
JTB 105	392.69	A=394.23 B=394.43 C=394.57		394.57
JMW 107	364.14	367.21		367.43
JTB 107	364.79	A=367.15 B=367.22		367.99
JMW 108	373.28	370.73		370.85
JTB 108	372.28	A=370.10 B=370.21		370.25
JMW 109	377.02	374.32		374.45
JTB 109	371.72	A=374.01 B=374.02		374.01
JTB 106	386.97	A=389.78 B=THREADED PIPE 389.88		389.95
JTB 110	361.34	A=THREADED PVC 353.88 B=363.98		364.22







JTB 100	433.93	A=436.06 B=436
JTB 102	427.62	A=430.27 B=430
JTB 105	392.69	A=394.23 B=394
JMW 107	364.14	367.21
JTB 107	364.79	A=367.15 B=367
JMW 108	373.28	370.73
JTB 108	372.28	A=370.10 B=370
JMW 109	377.02	374.32
JTB 109	371.72	A=374.01 B=374
JTB 106	386.97	A=389.78 B=THREADED PIP
JTB 110	361.34	A=THREADED PVC B=363.98



2413

LEGEND:

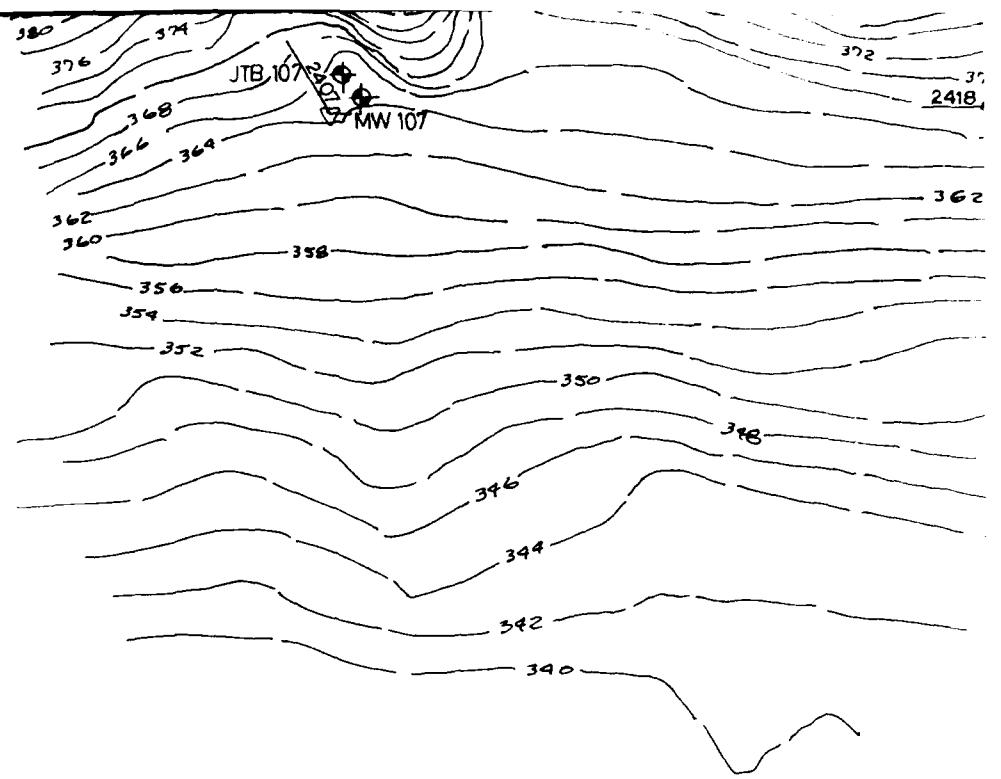
JTB 110

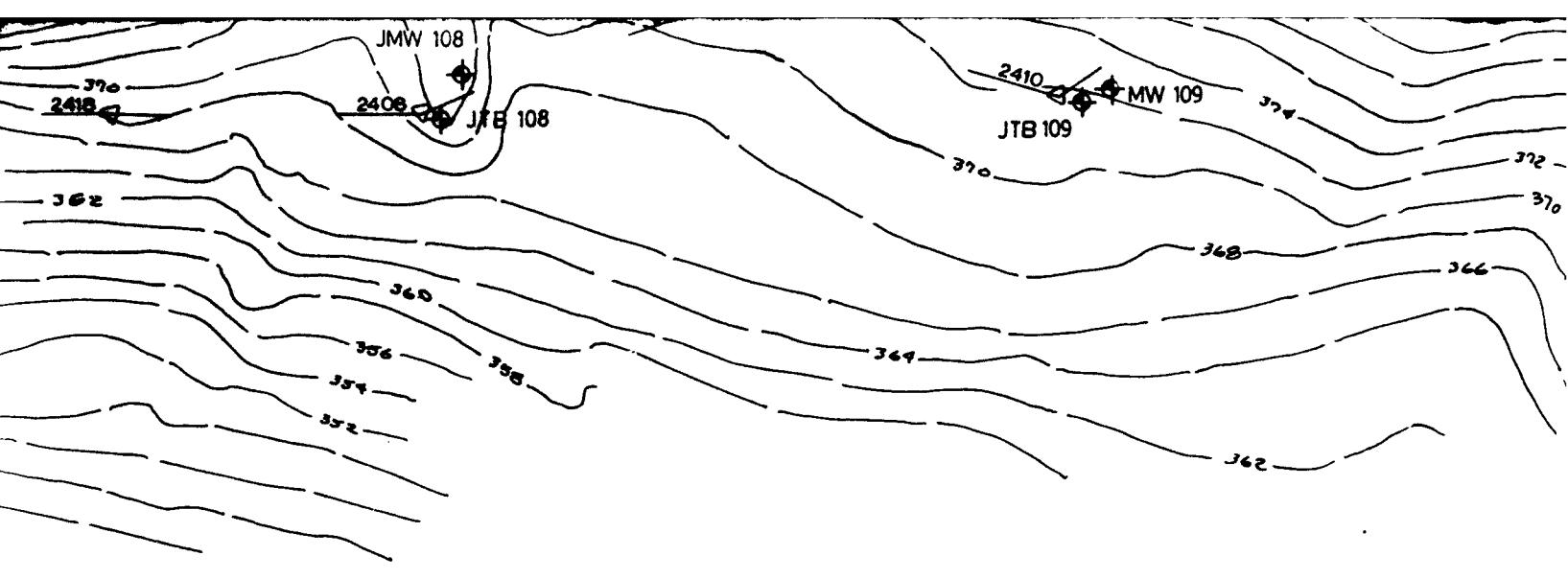
- JTB 107 TEST BORING
- MW 107 MONITORING
- HYDRANT
- POLE
- CATCH BASIN
- FENCE
- MANHOLE
- HORIZONTAL SURVEY POINT

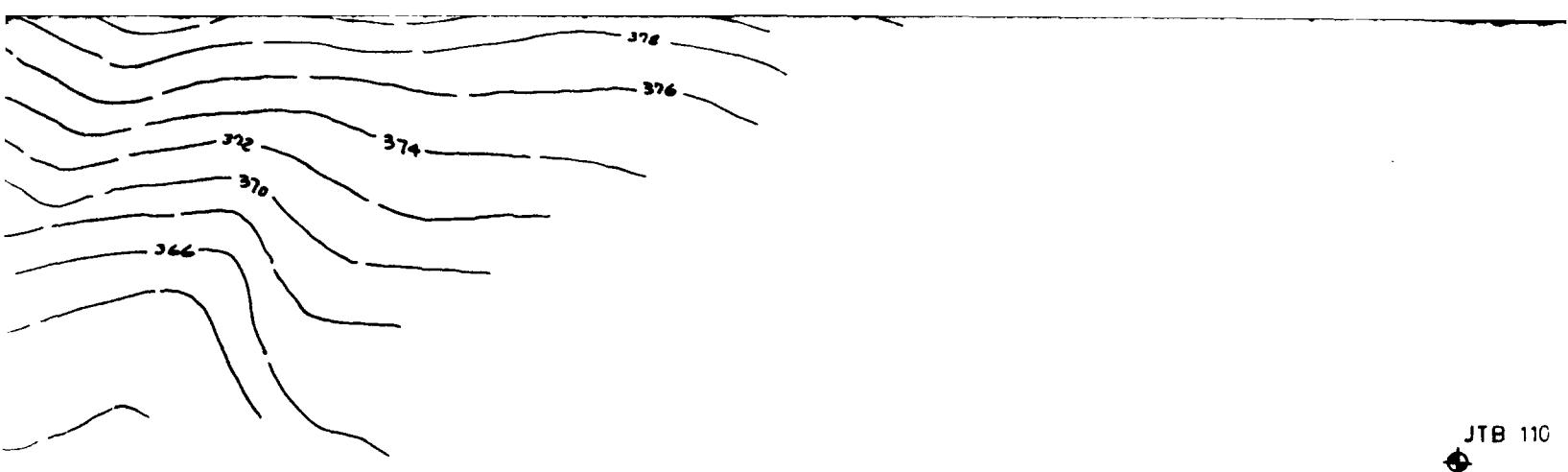
JTB 100	433.93	A=436.06 B=436.29	436.60
JTB 102	427.62	A=430.27 B=430.37 C=430.27	430.36
JTB 105	392.69	A=394.23 B=394.43 C=394.57	394.57
JMW 107	364.14	367.21	367.43
JTB 107	364.79	A=367.15 B=367.22	367.99
JMW 108	373.28	370.73	370.85
JTB 108	372.28	A=370.10 B=370.21	370.25
JMW 109	377.02	374.32	374.45
JTB 109	371.72	A=374.01 B=374.02	374.01
JTB 106	386.97	A=389.78 B=THREADED PIPE 389.88	389.95
JTB 110	361.34	A=THREADED PVC 353.88 B=363.98	364.22

LEGEND:

- ◆ JTB 107 TEST BORING
- ◆ MW 107 MONITORING WELL
- HYDRANT
- POLE
- CATCH BASIN
- FENCE
- MANHOLE
- HORIZONTAL SURVEY POINT







JTB 110

JTB 110

LEGEND:

- ◆ JTB 107 TEST BORING
- ◆ MW 107 MONITORING WELL
- HYDRANT
- POLE
- CATCH BASIN
- FENCE
- MANHOLE
- ~~△ 2410~~ HORIZONTAL SURVEY POINT

INCO

EE&G

DESIGN	
DRAWN <u>John</u>	11-16-87
CHED.	
ED.	

TITLE STEWART INTERNATIONAL AIRPORT
NEWBURGH, NEW YORK

SITE CONDITIONS PLAN