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A LEARNING TOOL ON THE MAIN FRAME
by
Anthony A. Vraa
September 1989
Thesis Advisor E.A. Milne

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Orbital Mechanics
A Learning Tool On The Main Frame

by

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Submitted in partial fulfillment of the
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ABSTRACT

This thesis consists of an interactive program that enables the student to study the orbital motion of satellites around the earth. The student can investigate the shape of a variety of orbits by varying the initial position and velocity of the satellite, or by supplying select orbital parameters i.e. initial orbital radius, eccentricity, and inclination. Satellite maneuvers can also be studied, like transfer orbits and inclination changes, by command velocity changes at any location in the orbit. Also the effects of the perturbing forces due to the oblateness of the earth, drag for low earth orbits, and gravitational attraction from the sun and moon can be investigated. The orbits are displayed in either the perifocal coordinate system around a model of the earth, or the ground track can be displayed on a map of the world. Orbital data is displayed below the orbital plot. The display is enabled by the use of display integrated software system and plotting language (DISSPLA) subroutines.



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I. INTRODUCTION

A visual aid for students new to orbital mechanics is required to comprehend fully the dynamics of orbital motion. This program is an interactive time step simulation program that calculates and plots either unperturbed or perturbed elliptical orbits. The program interacts with the student in developing the initial orbit. Also the program enables the student with the ability to change the velocity of the satellite at a specific location in the orbit. This feature will permit the student to investigate the effects of commanded velocity changes as in perigee kicks, apogee kicks and inclination changes. The user can also modify the initial position and velocity of the satellite at the completion of any orbit.

The student is given an opportunity to investigate the effects of perturbing forces on the satellites orbit by choosing to have the program calculate the orbit with or without perturbing forces. The variation of parameters method, as seen in [Ref. 1: pp. 396-407], is used in calculating the perturbing orbit. The perturbing forces taken into consideration are the following:

1. the oblateness of the earth
2. drag for low earth orbits
3. gravitational force of the moon
4. gravitational force of the sun

In order to review fully the operation of the program (included in appendix A) and to uncover any problems or limitations that plagued the programming, the program has been divided up as follows:

1. program design
2. unperturbed orbit
3. perturbed orbit
4. velocity changes
5. graphical plots

The programming approach and equations used in each of the above sections will be examined in their respective chapters. A review of the coordinate systems used and their

transformations between them are included in appendix B. Since all the equations used in the calculation of the orbital elements are from reference 1, they will not be reviewed in each chapter but will be included in appendix C for a quick reference. Equations from other sources will be referenced in their respective chapters.

Examples of perturbed and unperturbed orbital plots for a variety of initial orbital parameters are included in appendix D. Included are plots of low earth orbits, transfer orbits and geosynchronous orbits.

II. PROGRAM DESIGN

In designing this program an attempt was made to make it not only as user friendly as possible, but also to make the program as simple as possible to understand. To achieve these goals, the program would have to be written in a logical manner, in a computer language that is easy to follow, the program would have to run on terminals readily available to students (at the Naval Postgraduate School (NPS)), and the program would have to be easily used by students with a minimum amount of computer or orbital mechanics knowledge.

FORTRAN was chosen as the programming language since it is a widely used scientific language and it allows for very structured programming. By programming in a structured format, the program can be expanded in the future with a minimum amount of time required to understand the programming code. FORTRAN also allows for double precision numbers to be used in the calculation of the orbit. This is critical when round off error in single precision could be greater than the actual change that one is trying to model. The equations in the descriptions of the program might not exactly match the equations in the listings because of special programming techniques which must be included in most computer programs to handle such problems as "division by zero".

The display integrated software system and plotting language (DISSPLA) package available on the mainframe computer at NPS was used to enable a variety of graphical displays with a minimum amount of programming. DISSPLA has a set of subroutines that the programmer calls to display data contained in arrays. This requirement forces the program to load arrays with the satellites position in order for it to be plotted. The TEC618 computer terminal and associative plotter was used for ease of gaining hard copy plots of the orbits and the diversity of locations that are available here at NPS. In order to run a program in DISSPLA the user must first define storage space of 1500k and designate temporary disk space, and then call DISSPLA with the program name. This is accomplished with the following commands:

1. DEFINE STORAGE 1500K

2. ICMS
3. TDISK 4 DIS
4. DISSPLA ORBIT

To make the program user friendly, the user is prompted for inputs via the keyboard. The entry is usually a number. A yes or no response can be entered by typing "Y" or a "N". In most cases the program does a check to see if the input is appropriate. In order to make it as easy as possible for the student to get the desired orbit displayed, the program requires only the initial position and velocity of the satellite. The initial position and velocity of the satellite is supplied by the user in one of two ways. The user can input the position and velocity of the satellite, using the perifocal coordinate system (IJK), or the user can let the program place the satellite on the "I" axis of the IJK system at the radius of perigee (RP) distance supplied by the user. This latter choice gives the initial location of the satellite, but to get the velocity the program will prompt the user for one of the following:

1. the actual velocity in the IJK system.
2. the eccentricity (e) of the orbit. In which case the velocity is calculated from the following equations:

$$a = \frac{RP}{1 - e} = \text{semi-major axis}$$

$$ENR = -\frac{\mu}{2a} = \text{energy mass}$$

Where $\mu = MG$

M = mass of earth

G = Universal gravitational constant

$$v = \sqrt{2(ENR + \frac{\mu}{RP})}$$

3. the radius of apogee (RA) The velocity is calculated by first calculating the eccentricity (e) from the following:

$$e = \frac{RA - RP}{RA + RP}$$

With the eccentricity the same equations used above are used to calculate the velocity.

In order to give the velocity a direction the inclination (i) of the orbit is required from the user. The following equations are used to calculate the velocity vector:

$$v_j = 0,0$$

$v_x = 1.23456$

$v_y = 1.23456$

The program will check to ensure that the orbital eccentricity is less than 1.0, if it is not then the program will reject the inputs. After the initial input are accepted, the program will do calculations for the six orbital elements required to describe the size, shape and orientation of the orbit, and to pinpoint the position of the satellite along the orbit at a particular time. This classical set of six orbital elements are as follows:

1. a, semi-major axis.
2. e, eccentricity.
3. i, inclination.
4. Ω , longitude of the ascending node.
5. ω , argument of perigee passage.
6. T, time of perigee passage.

The program actually calculates more orbital elements than the six classical elements required to plot the orbit, this is done in an effort to make the program as robust as possible. This will add in the ability to expand the program in the future.

If the satellite is not initially at the perigee point then the satellite will first be stepped around to the perigee point. The program then enters a loop that calculates the orbit from the perigee point through one complete orbit around the earth and back to the perigee point. The orbit is calculated in steps of 2 times pi divided by an integer, i.e., 2 times pi divided by 50. This step size was used to ensure a smooth orbit for display purposes and also to get within adequate distance to the perigee point or other location for a velocity change. After the loop is completed, the program will offer the user a choice of the following plots to check the orbit:

1. perifocal
2. groundtrack

The program then goes into a loop offering the user the following choices until the user decides to end the program:

1. plot another view of the same orbit.

If the user wishes to plot another view of the same orbit then the user may use this choice to reenter the display portion of the program.

2. plot the next orbit (perturbed or unperturbed).
To plot the next orbit the satellite is stepped around the complete orbit either with or without perturbing forces effecting the satellite.
3. change the initial conditions.
The program goes to the beginning of the program and allows the user to change the initial position and velocity of the satellite.
4. change the velocity at a specific location
Step the satellite around to a specific true anomaly and make a velocity change at that location.
5. clear the previous orbits from the plot.
Clear the memory of all the previous orbits and only retain the current location and velocity as the initial position and velocity.

Before each new orbit, the orbital elements are recalculated.

There are several common assumptions and constants used throughout the program i.e. all bodies are considered to be spherically symmetric (this allows these bodies to be treated as though their masses are concentrated at their centers (point masses)). other assumptions will be covered in their respective chapters.

III. UNPERTURBED ORBIT

The subroutines that calculate the unperturbed orbit are the most widely used subroutines in the entire program. These subroutines are called to step the satellite around to the perigee point from the user supplied initial position and velocity, to calculate the next unperturbed orbit, and for any velocity change. No matter which of these sources supply the initial position and velocity the program calculates the unperturbed orbit in the same manner. The only difference is where in the orbit the satellite is initially when these subroutines are called. Before the unperturbed subroutines are called, the orbital elements are calculated.

The unperturbed subroutines are called by a single subroutine 'UNPRET' which has the following basic algorithm:

1. Increment time by the time step size (DT). The time step was chosen as the period divided by fifty to give a smooth plot, but more importantly to ensure that the satellite is within an acceptable distance from a specific location for a velocity change. The angular error caused by the step size can be as much as $PI/50$ from the desired point for a circular orbit and will increase for more eccentric orbits. This error becomes a factor when the user is making velocity changes, and therefore it will be covered in that chapter in further detail.
2. Calculate the new elements. The calculation of the new elements is the heart of this algorithm. The size, shape and orientation of the orbit remains unchanged. What is required is the position of the satellite along the orbit as a function of time. The problem becomes a matter to solve "the Kepler problem"-predicting the future position and velocity of an orbiting object as a function of some known initial position and velocity and the time of flight [Ref. 1: p. 181]. An algorithm using these principles will follow:
 - a. A time step (DT) is added to the time of flight (TF), time of flight is the elapsed time since the satellite passed the perigee point.
$$TF = TF + DT$$
 - b. The new mean anomaly (MA) is calculated from the new time of flight, and the mean motion (MM).
$$MA = MM \times TF$$
 - c. With the new mean anomaly the new eccentric anomaly (EA) is calculated. Because the solution to the Kepler problem ($MA = EA - e \times \sin(EA)$) is transcendental, an iterative solution based on the Newton method of root finding is used. The root in question is a solution to the equation ($MA - EA + e \times \sin(EA) = 0$). This algorithm takes the form of [Ref. 1: p. 222]:
 - 1) $MA = EA - e \times \sin(EA)$

2.

$$E.A._2 = E.A._1 - \frac{(M.A. - M.A._1)}{(1 - e \times \cos(E.A._1))}$$

Where this equation is applied initially to $E.A. = M.A$ and then reapplied until the difference between $M.A$ and $M.A$, becomes small enough to be ignored.

d. The new true anomaly (v_2) is calculated from:

$$v_2 = \frac{\cos^{-1}(e - \cos(E.A.))}{e \cos(E.A.) - 1}$$

3. Calculate the new position and velocity. The position and velocity are calculated in the perifocal coordinate system (PQW). The PQW system uses the orbit as its fundamental plane and therefore requires only two coordinate to specify the satellite's position and velocity. The z_u coordinate is by definition always equal to zero. The position of the satellite is calculated as:

$$x_w = r \cos v$$

$$y_w = r \sin v$$

$$z_u = 0$$

The velocity of the satellite is calculated as:

$$v_x = \sqrt{\frac{\mu}{r}} (-\sin v)$$

$$v_y = \sqrt{\frac{\mu}{r}} (e + \cos v)$$

$$v_z = 0$$

4. Store position and elements in arrays for plotting. In order for the program to plot the orbit the radius, true anomaly, inclination, and argument of perigee must be stored in arrays. The use of these arrays to plot the orbit will be explained in chapter 6.

5. The process is repeated until the satellite is at the perigee point and the true anomaly is two pi.

The procedure used to calculate the unperturbed orbit leave very little to be modified by a programmer. The only choices that had to be made concerned step size, how to tell the UNFRET subroutine that the perigee point had been reached, and a value of acceptable error for newtons method. For the unperturbed orbit, the step size just had to be small enough to produce a smooth plot of the orbit. Two indicators for perigee were used, one was that the true anomaly was greater than 6.21 radians (two pi equals 6.28 radians) and the time from the previous perigee point will be greater then the period. The two indicators were logically 'and' together to ensure the perigee point was reached.

The disparity between two π and 6.21 radians is due to the error produced by the satellite not beginning the orbit at exactly the perigee point and the step size used go around the orbit. The acceptable size of error for Newton's method was set at 1.0×10^{-10} , because for an unperturbed orbit this would be the major contributor to any error in the orbit and the magnitude of this error would be acceptable. However, in a perturbed orbit there are other factors contributing to determining the acceptable error, and these will be discussed in the next chapter.

IV. PERTURBED ORBIT

The perturbed orbit uses the same basic routines as the unperturbed orbit in stepping the satellite around the earth with one major difference, the perturbing forces produce a time rate of change of the orbital elements that must be applied at each step. The variation of parameters method is used to determine this influence of the perturbing forces on the orbital elements. The analysis is simplified by using the orbital coordinate system 'RSW', as explained in appendix B. The basic algorithm is as follows [Ref. 1: p. 407]:

1. At $t = t_0$, calculate six orbital elements.
2. Compute the perturbing forces and transform it at $t = t_0$ to the 'RSW' SYSTEM.
3. Compute the time rate-of-change of the elements.
4. Calculate the change of elements for one time step, and add the changes to the old values at each step to get the new elements.
5. From the new values of the orbital elements, calculate a position and velocity.
6. Go to the step 2 and repeat until the final time is reached.

The steps in the algorithm will be explained in the following sections:

A. ORBITAL ELEMENTS

The standard orbital elements a , e , i , Ω , ω and T (or M) will be used, where

a = semi-major axis

e = eccentricity

i = inclination

Ω = longitude of ascending node

ω = argument of perigee

T = time of perigee passage

(M_0 = mean anomaly at epoch = $M - n(t - t_0)$). The elements are calculated only at the beginning of the orbit from the initial position and velocity vectors. The elements are then changed continuously throughout the orbit by adding the changes due to the perturbing forces. For the perturbed orbit, the satellite will always begin at the perigee point. This is done so one complete orbit is from perigee point to perigee point.

B. COMPUTE PERTURBING FORCES

The variation of parameters method requires that the perturbing forces be calculated at each step in the orbit. In order to do this a model of each perturbing force must be developed. The following perturbing forces were used in calculating the total perturbing force effecting the satellite:

1. oblateness of the earth
2. atmospheric drag
3. gravitational attraction of the sun
4. gravitational attraction of the moon

The magnitudes of these forces have an enormous range of values and are dependent on the distance the satellite is from the perturbing body. Figure 1 on page 12 shows a graphical representation of the magnitude of the perturbing forces in a log-log plot of perturbing forces per unit mass [Ref. 2: p. IV-61]. The model of each of these forces follows:

1. NON-SPHERICAL EARTH

The earth is not perfectly spherical, but bulges around the equator. The polar and equatorial diameters are 12713.0 Km and 12756.3 Km, respectively. The oblateness results in a perturbing force per unit mass with these components in the 'RSW' coordinate system [Ref. 3: p. 51]:

$$F_r = \frac{(1 - 3\mu J_2 r_e^2)}{2r^3} (1 - 3 \sin^2(i) \sin^2(u_0))$$

$$F_s = \frac{(-3\mu J_2 r_e^2)}{r^3} (\sin^2(i) \sin(u_0) \cos(u_0))$$

$$F_w = \frac{(-3\mu J_2 r_e^2)}{r^3} (\sin(i) \cos(i) \sin(u_0))$$

The variable and constants of these equations are defined below:

i. Variables:

- a. u_0 = the argument of latitude and is equal to the true anomaly v_0 plus the argument of perigee ω .

$$u_0 = v_0 + \omega$$

- b. r = the radius from the center of the earth to the satellite.

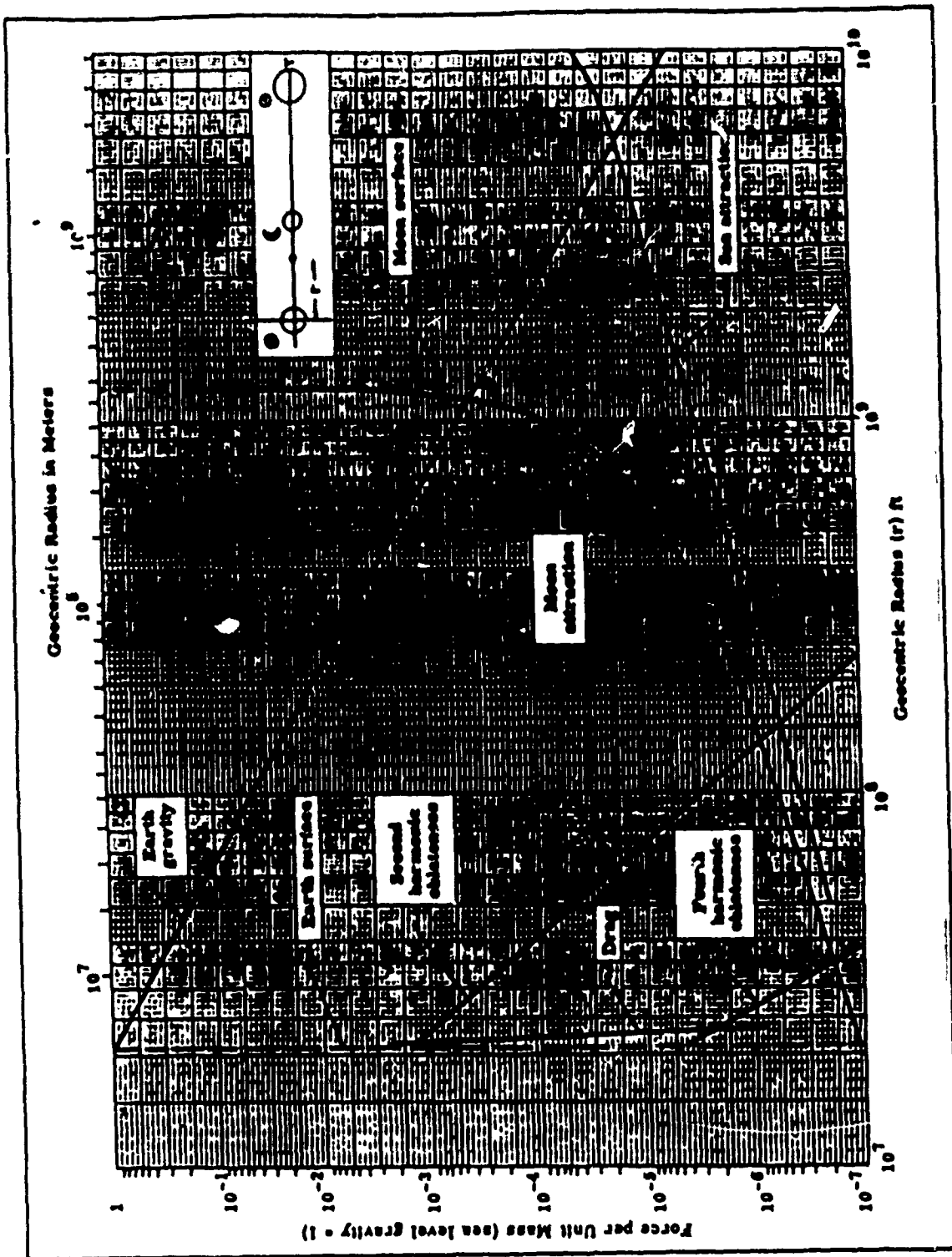


Figure 1. Comparison of perturbation magnitudes.

$$\vec{r} = \vec{r}$$

2. Constants:

a. μ = the gravitational parameter of the earth.

$$\mu = 398601.2 \frac{(\text{km}^3)}{\text{s}^2}$$

b. J_2 = the second harmonic of oblateness coefficient, determined by experimental observations.

$$J_2 = 1.08263E-3$$

c. r_e = the mean radius of the earth,

$$r_e = 6.3782E3 \text{ km}$$

2. ATMOSPHERIC DRAG

The formulation of atmospheric drag equations are plagued with uncertainties of atmospheric fluctuations, frontal areas of orbiting object (if not constant), the drag coefficient, and other parameters. A fairly simple formulation will be given here. Drag, by definition, will be opposite to the velocity of the vehicle relative to the atmosphere. Thus, the perturbing force is

$$\vec{F} = -\left(\frac{1}{2m}\right) \cdot CD \cdot A \cdot DEN \cdot v \cdot \vec{v}$$

The velocity vector is in the 'IJK' system so the resulting force is also in the 'IJK' system. Therefore a transformation to the 'RSW' system is required.

The variables and constants of this equation are defined below:

1. Variables:

a. v = speed of vehicle.

b. CD = the dimensionless drag coefficient. The drag coefficient CD has a value between 1 and 2. It takes a value near 1 when the mean free path of the atmospheric molecules is small compared with the satellite size, and takes a value close to 2 when the mean free path is large compared with the size of the satellite. The drag coefficient will be modeled with $CD = 2$ when the satellites altitude is greater than 550km and equal to 1 otherwise. [Ref. 4: p. 295]

c. DEN = atmospheric density at the vehicle's altitude. The density is spherically symmetric, and will be modeled using exponential steps using the parameters in Table 1 on page 14 and the following formula [Ref. 1: pp. 423-424]:

$$\delta(z) = \delta_0 e^{z/H}$$

Table 1. ATMOSPHERIC PARAMETERS AND VALUES

Altitude (km)	ρ	μ	γ	δ
0.150	1.225E-02	4.74E-02	0.0	1.2225E-02
			150	1.0E-03
150.550	1.79846E-01	4.3614E-02	550	3.0E-8
550	1.015484E-07	2.21698E-07	1500	3.65E-09
			2100	1.0E-12

2. Constants set to typical values:

- a. m = mass of the satellite, set equal to 100kg.
- b. AR = the sectional area of the vehicle perpendicular to the direction of motion.

3. PERTURBATION DUE TO HEAVENLY BODY

The satellite is subject to perturbation forces due to the gravitational effects of the sun and the moon. The perturbation force from a perturbing body is the difference between the gravitational force due to the perturbing body at the satellite and the gravitational force the satellite would experience if it were at the center of the earth. From Figure 2 on page 15, the perturbing force per unit mass of the satellite is

$$\vec{f}_p = \mu_p \frac{\vec{r}_p \vec{r}_p - r_p^2 \vec{i}_p \vec{i}_p}{(r_p^2 - r^2)^{3/2}} - \frac{\mu_p \vec{r}_p}{r_p^3}$$

The variable and constants are defined below:

1. Variables:

- a. r_p = distance from the earth center for the perturbing body
- b. \vec{i}_p = unit vector from the earth to the perturbing body
- c. r = distance from earth center to the satellite
- d. \vec{i}_r = unit vector from the earth to the satellite

2. Constants:

- a. μ_p = gravitational constant of the perturbing body = $M_p G$

The subscript p is to be replaced by s if the perturbing body is the sun, and by m if the perturbing body is the moon. We will assume that $r \ll r_p$, then the equation above becomes

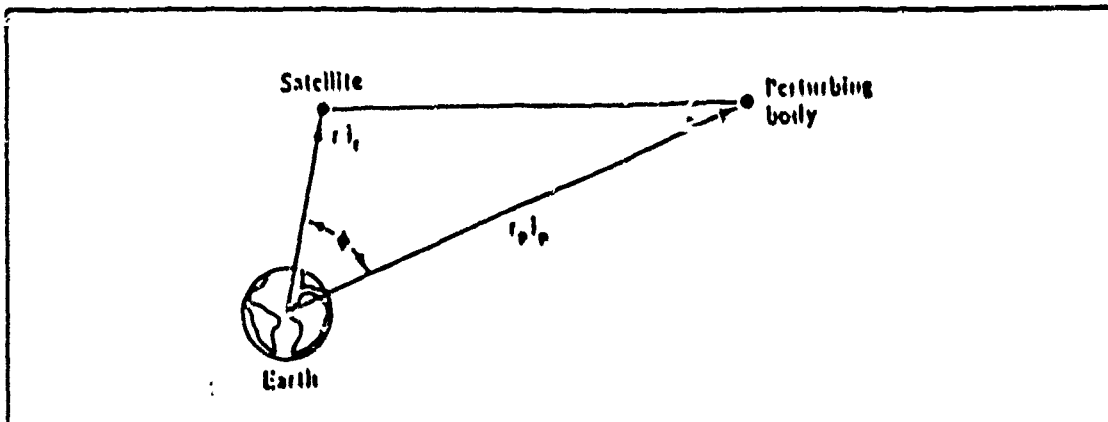


Figure 2. Perturbation forces.

$$\vec{F}_p = \left(\frac{\mu_p}{r_p^2} \right) \left(\frac{r}{r_p} \right) (3(\vec{i}_r \vec{i}_p) \vec{i}_p - \vec{i}_r)$$

The unit vectors \vec{i}_r and \vec{i}_p can be written in terms of the 'IJK' system as:

$$\vec{i}_r = (\cos(\Omega) \cos(u_0) - \sin(\Omega) \cos(i) \sin(u_0)) \vec{I} + (\cos(u_0) \sin(\Omega) + \cos(\omega) \cos(i) \sin(u_0)) \vec{J} + (\sin(i) \sin(u_0)) \vec{K}$$

$$\vec{i}_p = (\cos(\Omega_p) \cos(u_{0p}) - \sin(\Omega_p) \cos(i_p) \sin(u_{0p})) \vec{I} + (\cos(u_{0p}) \sin(\Omega_p) + \cos(\omega_p) \cos(i_p) \sin(u_{0p})) \vec{J} + (\sin(i_p) \sin(u_{0p})) \vec{K}$$

where Ω , i , and u_0 are the orbital elements of the satellites and Ω_p , i_p , and u_{0p} are the orbital elements of the perturbing body. The formulas above use the 'IJK' system, and as such the resultant forces must be transformed to the 'RSW' system. Models of the sun and moon orbits are required to calculate \vec{r}_p and \vec{i}_p . The models used in the program for the sun and moon's orbits follows: [Ref. 3: pp. 73-74]

a. SUN'S POSITION

In order to model the sun's orbit, a number of simplifications had to be made in the actual parameters of the sun's orbit. First the sun will be assumed to be in a circular orbit. This means that the radius (r) to the sun will be constant, and the eccentricity (e) will equal 0.0 instead of its true value of 0.017. The other assumption will

be to place the sun on the 'I' axis of the 'IJK' system at the beginning of the program and have it progress through its orbit as the program runs. These changes will not effect the perturbing force in any noticeable magnitude.

The following variables and constants were used in the program to model the sun's orbit after applying the simplifications: [Ref. 3: pp. 75-78]

1. Constants:

a. Gravitational Constant: $G = 6.67E-11 \frac{(Nm^2)}{kg^2}$

b. Sun's Mass: $m_s = 1.99E30Kg$

c. Sun's Gravitational parameter:

$$\mu_s = 1.32733E20 \frac{Nm^2}{kg}$$

d. Sun's eccentricity: $e_s = 0.0$

e. Radius of orbit, assume sun is in circular orbit: $r_s = 1.49E11m$

f. Sun's inclination: $si = 23.45 \text{ deg.} = 4.09279709d-01 \text{ radians}$

g. Longitude of ascending node: $\Omega_s = 0.0$

h. Argument of perigee: $\omega_s = 0.0$

2. Variables:

a. The true anomaly of the sun's position as a function of the time the satellite has been in orbit:

$$v_s(TT) = \frac{2\pi}{350 \times 24 \times 3600} TT$$

Where TT = true time, the time the satellite has been in orbit (sec)

b. Sun's Position vector: $\vec{r} = r \cos v_s \vec{P} + r \sin v_s \vec{Q}$

c. Unit vector from the earth to the sun: $\vec{i}_s = \frac{\vec{r}_s}{|\vec{r}_s|}$

b. MOON'S POSITION

In modeling the orbit of the moon, similar assumptions were used as with the sun. The moon's orbit will be assumed to be circular, actually the eccentricity is equal to 0.055. By placing the moon initially on the 'I' axis of the 'IJK' system along with the sun, the gravitational forces of the two bodies will combine to a maximum. However; since the moon's orbital period is only 27.3 days, the moon will not stay in this alignment and the magnitude of the combined forces will vary with time. The inclination of the moon's orbit is not constant, but drifts between 18.3 and 28.6 degrees in ten years.

Also the longitude of the ascending node (Ω) oscillates between 13 and -13 degrees. To simplify this the inclination will be chosen as a constant 23.5 degrees and the longitude of the ascending node as 0.0 degrees. For the time period involved in calculating the perturbed orbit, these assumptions will not make any significant difference.

The following variables and constants were used in the program to model the moons orbit, after applying the simplifications:

1. Constants:

a. Gravitational Constant: $G = 6.67E-11 \frac{(Nm^2)}{kg^2}$

b. Moon's Mass: $m_m = 7.35E22 kg$

c. Moon's Gravitational Parameter: $\mu_m = GM_m = 4.90E12 \frac{(Nm^2)}{kg}$

d. Moon's eccentricity: $e_m = 0.0$

e. Radius of orbit, assume moon is in circular orbit: $r_m = 3.844E8 km$

f. Moon's inclination: $i = 23.5 \text{deg.} = 4.10152374E-1 \text{ radians}$

g. Moon's longitude of ascending node: $\Omega_m = 0.0$

h. Moon's argument of perigee: $\omega_m = 0.0$

i. Moon's period: $T = 27.3 \text{ days [period]}$

2. Variables:

a. The true anomaly of the moon's position as a function of the time the satellite has been in orbit: $v_m(TT) = \frac{2\pi}{27.3 \times 24 \times 3600} TT$

b. Moon's position Vector: $\vec{r} = r \cos v_m \vec{P} + r \sin v_m \vec{Q}$

c. Unit vector from earth to moon: $\vec{i}_m = \frac{\vec{r}_m}{|\vec{r}_m|}$

The models of the sun and moons orbit calculates the position vector in the 'PQW' system and therefore the position vector must be transformed to the 'IJK' system.

C. RATE-OF-CHANGE OF ORBITAL ELEMENTS

The derivations and equations of the rates-of-change of the orbital elements are contained in reference 1 pages 398 to 406. Therefore; only a summary of the actual analytic expressions for the rate-of-change of the parameters in terms of the perturbations will follow:

1. Rate-of-change of the semi-major axis:

$$\frac{dr}{dt} = \left[\frac{2e \sin v}{a^2 \sqrt{1-e^2}} \right] F_r - \left[\frac{2a \sqrt{1-e^2}}{a^2 r} \right] F_t$$

Where n' is the mean motion of the satellites orbit.

$$n' = \sqrt{\frac{\mu}{a^3}}$$

2. Rate-of-change of the eccentricity:

$$\frac{de}{dt} = \left[\frac{\sqrt{1-e^2} \sin v_0}{n'a} \right] F_r + \left[\frac{\sqrt{1-e^2}}{n'a^2 e} \right] \left[\frac{a^2(1-e^2)}{r} - r \right] F_t$$

3. Rate-of-change of the inclination:

$$\frac{di}{dt} = \left[\frac{r \cos u_0}{n'a^2 \sqrt{1-e^2}} \right] F_w$$

4. Rate-of-change of the longitude of the ascending node:

$$\frac{d\Omega}{dt} = \left[\frac{r \sin u_0}{n'a^2 \sqrt{1-e^2} \sin i} \right] F_w$$

5. Rate-of-change of the argument of perigee:

$$\frac{d\omega}{dt} = \left(\frac{d\omega}{dt} \right)_r + \left(\frac{d\omega}{dt} \right)_t + \left(\frac{d\omega}{dt} \right)_w$$

Where,

$$\left(\frac{d\omega}{dt} \right)_r = \left[\frac{-\sqrt{1-e^2} \cos v_0}{n'ae} \right] F_r$$

$$\left(\frac{d\omega}{dt} \right)_t = \left[\frac{p}{ch} \right] \left[\sin v_0 \left(1 + \frac{1}{1+e \cos v_0} \right) \right] F_t$$

$$\left(\frac{d\omega}{dt} \right)_w = \left[\frac{-r \cot i \sin u_0}{n'a^2 \sqrt{1-e^2}} \right] F_w$$

6. Rate-of-change of the eccentric anomaly:

$$\frac{dE.A}{dt} = \frac{1}{\sin(E.A)} \frac{[(\sin v_0 + \frac{de}{dt})(1+e \cos v_0) - (\cos v_0 + e)(\frac{de}{dt} \cos v_0 + e \sin v_0)]}{[1+e \cos v_0]^2}$$

7. Rate-of-change of the mean anomaly:

$$\frac{dM.A}{dt} = \frac{dE.A}{dt} - \frac{de}{dt} \sin(E.A) - e \times \cos \frac{(E.A)dE.A}{dt} - \frac{dn'}{dt} (t-t_0)$$

This equation reduces to the following for circular and ecliptic orbits
 $(e = 0)$.

$$\frac{dM}{dt} = \frac{-1}{a} \left[\frac{2r}{a} - \frac{(1-e^2)}{e} \cos v \right] F_r - \left[\frac{1-e^2}{a^2 a e} \right] \left[1 - \frac{r}{a(1-e^2)} \right] \sin v F_t = r \frac{dn'}{dt}$$

Where the Rate-of-change of the mean motion:

$$\frac{dn'}{dt} = \left[\frac{-3\mu}{2a'^3} \right] \frac{da}{dt}$$

[ref. 1 p. 396-407]

D. NEW ORBITAL ELEMENTS

The change of each element is calculated by multiplying the rate-of-change of the element by the time step (DT). The change in the orbital elements are then added to the current values of the elements to give the new orbital elements. With the new elements calculated, the satellite is stepped forward and the new position and velocity are calculated in the same manner as the unperturbed orbit (chapter 3). Also as with the unperturbed orbit, the process is repeated until the satellite is at the perigee point, indicated by the time of flight (TF) equal to the period of the perturbed orbit.

V. VELOCITY CHANGES

The ability of the student to change the velocity of the satellite at any position in the orbit is a vital element in this program. With velocity changes the student can investigate the effects of varying the satellites velocity as in transfer orbits and inclination changes. In order to simplify the program the unperturbed orbit is used throughout this routine. The velocity change algorithm used in the program follows:

1. Rotate to velocity change location.

The user is given the choice of changing the velocity of the satellite at the perigee, apogee or at any true anomaly. If the user chooses perigee or apogee as the change locations, the true anomaly is set equal to zero or π radians respectively. With the location of the velocity change, the satellite is first stepped around to the desired true anomaly. The stepping is identical with the unperturbed orbit with the exception that the stepping terminates when the true anomaly is greater or equal to the desired true anomaly. With a step size of one fiftieth of the period, the satellite is actually stepped around to a location near the desired location. This variance can be reduced by decreasing the step size but this would increase the computation time. This error will be a major factor in precise calculations of transfer orbits, or any other orbital maneuver where precise velocity changes are required. However, this program is not a tool to calculate precise orbital maneuvers, but rather a learning tool for the student to get a feel for the results of velocity changes in a satellite's orbit.

2. Change the velocity.

With the satellite at the desired location, the program calculates and displays for the user the satellite's current velocity, escape velocity and circular velocity (the velocity required to circularize the orbit). The program will not allow velocities greater than or equal to the escape velocity. The user is given the option to enter a new velocity in the 'JK' system or to change the magnitude of the velocity in the orbital plane. If the user chooses to change the velocity in the orbital plane, the program will prompt the user for the magnitude of the velocity change, and multiply this change by a unit vector in the direction of the satellites velocity. This velocity change vector is then added to the satellites velocity vector, to calculate the new velocity vector.

3. Calculate new elements.

The orbital elements are calculated with the new velocity vector and the satellite's position vector.

4. Complete the orbit.

The program will complete the orbit to the new perigee point using the satellite's position, new velocity and new elements. There are a number of problems that arise if the satellite is just stepped around to the perigee point. For example, with velocity changes in the orbital plane the apogee and perigee directions can physically swap. This is a problem when plotting with the perifocal coordinate system because the X_1 axis points toward perigee. To avoid problems like this the arrays used in plotting the orbit must be cleared and the satellite's current position

and velocity be treated as initial conditions. However, to compare the old and new orbits there is a desire to retain as much of the previous orbit as possible. The velocity changes were divided into the following four cases to handle these problems:

- a. Change velocity in the orbital plane at the perigee point with the new velocity greater than the circular velocity. The perigee point will remain the same so the satellite is stepped around using the unperturbed subroutines.
- b. Change velocity in the orbital plane at the perigee point with the new velocity less than or equal to the circular velocity. The perigee and apogee directions will switch so the plotting arrays are first cleared and stored with the current location data. Because the satellite is now at the apogee point the satellite is stepped around to the perigee point storing the second half of the orbit. The entire next orbit is calculated and stored to get a complete orbit.
- c. Change velocity in the orbital plane at the apogee point with the new velocity less than the circular velocity. The perigee and apogee directions will remain the same, so the satellite is stepped around to the perigee point completing the orbit.
- d. This last case catches all the following velocity changes: velocity change in the orbital plane at the apogee point with the new velocity greater than or equal to the circular velocity, velocity changes at any other true anomaly in the orbital plane, and any velocity change out of the orbital plane. The plotting arrays are cleared and stored with the current location data. No matter where in the orbit the satellite is, the satellite is first stepped around to the perigee point, and to ensure a complete orbit is plotted the entire next orbit is also calculated and stored.

VI. GRAPHICAL PLOTS

The program provides two types of graphical displays of the orbit, a display in the perifocal coordinate system and a display of the satellite's ground track. Each display type is useful in observing different aspects of the orbit. The perifocal display will allow the user to see how certain orbital parameters change with different initial positions and velocities, and also how the parameters change with velocity changes at varying positions in the orbit. The ground track will enable the user to gain an appreciation for the physical location of the satellite above the earth, and see how the orbital parameter affects the path of the satellite. The ground track will also display the precession of a sequence of orbits. Both displays plot the position steps to give the user an understanding of how the satellite speeds up at perigee and slows down around apogee.

The DISSPLA package on the mainframe computer was used to enable the plotting of the orbits. The versatility of plotting subroutines of DISSPLA makes the actual programming of the orbit a simple matter of initializing DISSPLA for the type of monitor being used, setting up the plotting area, initializing the axis and axis scale, and then plotting the desired curve from points contained in arrays. This is a simplified explanation of DISSPLA, but for further details on DISSPLA programming refer to the DISSPLA user's manual [Ref. 5]. DISSPLA also supplies subroutines to draw a variety of projections of the world and fill the projections with coast lines, latitude lines and longitude lines. There are a couple of DISSPLA requirements that did require special handling in the program. The requirement that the data be supplied in arrays forced the program to load arrays with the required position and parameters and to keep a counter for the number in the arrays. The array format requires the size of the array be specified in the beginning of the program. The array size needs to be large enough to hold a number of orbits, but not so large as to waste storage space. The program will continue to add orbital data to the arrays until the user chooses to delete the previous orbits. If a new initial position and velocity is entered or if the arrays will overflow with the next orbit the arrays will automatically delete all previous orbits. DISSPLA also requires that all data be in single precision format. The program calculates all orbits in double precision in order to limit the effect of round-off error, but by using the single precision data for plotting will not affect the accuracy of the plot in any way.

The subroutines used to display the orbits will be covered in the following three sections:

A. PERIFOCAL PLOT

The plotting of the orbit in the perifocal coordinate system is the easier of the two types of plots. Since the perifocal coordinate system has the orbital plane as the fundamental plane, the only requirements to describe the orbit in the perifocal coordinate system are arrays with the true anomaly and the radius to the satellite. To give the user a sense of the size of the plot, the axis length varies with the eccentricity and semi-major axis length. Also a plot of the earth is plotted to the same scale, with the pole or center of the plot on the origin of the axis. The latitude of the earth at the center of the plot will vary with the inclination of the orbit. This plot will allow the user to see a relative view of the satellite's coverage in the minus 'Z' axis direction of the perifocal coordinate system.

B. GROUND TRACK

The ground track plot is a very complex subroutine compared with the perifocal plot. Because the ground track is not a continuous curve a procedure to handle the satellite ending at one end of the plot and wrapping around to the other end was developed. The wrap around problem is avoided in most orbits by plotting the orbit in segments with the following two rules. Each segment begins at the beginning of a new plot or at the edge of the plot area, and ending when the satellite would wrap around to the other side of the plot. At the beginning of a segment if the position of the satellite is within five degrees of the edge of the plot, that position and any other positions within that five degree boundary will not be plotted. The segment will end when the satellite is within ten degrees of the edge of the plot. The above restrictions imposed on the segments of the plot will not substantially affect the interpretation or usefulness of the plot. The ground track is plotted on top of a cylindrical equidistant projection of the world, with the world coast lines and a longitude-latitude grid for reference.

C. DATA

Information concerning the orbit is displayed on the lower half of the plot. The information is designed to supply the user with enough of the basic orbital elements and other parameters affecting the orbit to be able to evaluate what basic type of orbit the satellite is in, and the effects of velocity changes and perturbing forces have on the orbit. The following data are plotted: inclination (i), semi-major axis (a), eccentricity (e), period

(per), apogee and perigee velocity and radius, average time rate-of-change of orbital elements, and the average magnitude of perturbing forces per unit mass.

VII. CONCLUSIONS AND RECOMMENDATIONS

The program supplies the student with an interactive tool to study the orbital motion of satellites around the earth. The student can investigate a variety of orbits by varying the orbital parameters, command velocity changes, and observe the effects of perturbing forces.

The student is provided with two options for entering the initial position and velocity of the satellite. The program could be expanded to provide the student with the additional options of entering either orbital parameters or a ground observation data and have the program calculate the initial position and velocity from this data. Also the student is limited to orbits with eccentricities less than one (elliptic orbits). The program could be also be expanded to include more eccentric orbit for Lunar, interplanetary, and missile trajectories. The perturbing orbit is calculated for orbits around the earth with relatively small perturbing forces in relation to the earths gravitational force. This fact will cause the program to produce false results if the student tries to calculate lunar trajectories. Special routines would have to be employed when the perturbing force (the moons gravitational attraction) is comparable to the earths gravitational attraction. This will not become a factor for studying current satellite orbits out to the geosynchronous radius of 42241.1km.

The velocity change subroutines move the satellite to a location close to the desired location before a velocity change is imposed. By reducing the step size in the velocity change subroutine, this error could be reduced. Precise orbital transfer maneuvers can be modeled by reducing this error caused by the positioning of the satellite prior to changing the velocity. The program will currently provide the student with useful plots for gaining experience with various transfer orbits by varying the magnitude and location of the velocity changes.

The output of the calculations of the orbit are arrays loaded with the satellite's position and select orbital parameters. The `DISPLA` subroutines that plot the points are not unique. The program would become portable to personal computers with these graphics subroutines written in `FORTRAN` and included in the program.

A final recommendation is that the display of the ground track could be modified to show ground coverage, number of satellites in a constellation, and other elements necessary for planning a real-world artificial satellite application.

APPENDIX A. ORBIT PROGRAM

*	PROGRAM ORBIT	ORB00010
*	THIS PROGRAM IS AN INTERACTIVE TIME STEP SIMULATION OF	ORB00020
*	SATELLITES AROUND THE EARTH. PERTURBED AND UNPERTURBED ORBITS	ORB00030
*	ARE CALCULATED AND PLOTTED. VELOCITY CHANGES ARE ALSO PERMITTED	ORB00040
*	AT SPECIFIED TRUE ANOMALIES.	ORB00050
*	A LIST OF VARIABLES USED BY THE MAIN PROGRAM FOLLOWS.	ORB00060
*	A = SEMI-MAJOR AXIS	ORB00070
*	AL = ARGUMENT OF LONGITUDE	ORB00080
*	AP = ARGUMENT OF PERIGEE	ORB00090
*	CHTA = VELOCITY CHANGE LOCATION TRUE ANOMALY	ORB00100
*	DT = TIME STEP	ORB00110
*	E = ECCENTRICITY	ORB00120
*	EA = ECCENTRIC ANOMALY	ORB00130
*	EI = I VECTOR OF ECCENTRICITY	ORB00140
*	EJ = J VECTOR OF ECCENTRICITY	ORB00150
*	EK = K VECTOR OF ECCENTRICITY	ORB00160
*	FR = R VECTOR OF TOTAL FORCE	ORB00170
*	FS = S VECTOR OF TOTAL FORCE	ORB00180
*	FW = W VECTOR OF TOTAL FORCE	ORB00190
*	H = ANGULAR MOMENTUM	ORB00200
*	HI = I VECTOR OF ANGULAR MOMENTUM	ORB00210
*	HJ = J VECTOR OF ANGULAR MOMENTUM	ORB00220
*	HK = K VECTOR OF ANGULAR MOMENTUM	ORB00230
*	I = INCLINATION	ORB00240
*	IOPT1 = PERTURBED OR UNPERTURBED OPTION	ORB00250
*	IOPT2 = OPTIONS: PLOT NEXT ORBIT, CHANGE INITIAL VALUES,	ORB00260
*	CHANGE VELOCITY, PLOT ANOTHER VIEW OF ORBIT, QUIT	ORB00270
*	LAN = LONGITUDE OF ASCENDING NODE	ORB00280
*	LP = LONGITUDE OF PERIGEE	ORB00290
*	MA = MEAN ANOMALY	ORB00300
*	MM = MEAN MOTION	ORB00310
*	MU = GRAVITATIONAL PARAMETER	ORB00320
*	N = ASCENDING NODE	ORB00330
*	NI = I VECTOR OF ASCENDING NODE	ORB00340
*	NJ = J VECTOR OF ASCENDING NODE	ORB00350
*	NK = K VECTOR OF ASCENDING NODE	ORB00360
*	NUM = STEP COUNTER	ORB00370
*	P = SEMI-LATUS RECTUM	ORB00380
*	PER = PERIOD OF ORBIT	ORB00390
*	PI = PI	ORB00400
*	RA = RADIUS OF APOGEE	ORB00410
*	RE = RADIUS OF EARTH	ORB00420
*	R = ORBITAL RADIUS	ORB00430
*	RI = I VECTOR OF ORBITAL RADIUS	ORB00440
*	RJ = J VECTOR OF ORBITAL RADIUS	ORB00450
*	RK = K VECTOR OF ORBITAL RADIUS	ORB00460
*	T = TIME COUNTER IN ORBIT	ORB00470
*	TA = TRUE ANOMALY	ORB00480
*	TDA = TOTAL CHANGE IN SEMI-MAJOR AXIS	ORB00490
*	TDAP = TOTAL CHANGE IN ARGUMENT OF PERIGEE	ORB00500
*		ORB00510

*	TDE = TOTAL CHANGE IN ECCENTRICITY	ORB00520
*	TDH = TOTAL CHANGE IN ANGULAR MOMENTUM	ORB00530
*	TDI = TOTAL CHANGE IN INCLINATION	ORB00540
*	TDMA = TOTAL CHANGE IN MEAN ANOMALY	ORB00550
*	TDMN = TOTAL CHANGE IN MEAN MOTION	ORB00560
*	TDLAN = TOTAL CHANGE IN LONGITUDE OF ASCENDING NODE	ORB00570
*	TF = TIME OF FLIGHT	ORB00580
*	TFDRA = TOTAL FORCE OF DRAG	ORB00590
*	TFEA = TOTAL FORCE OF EARTH'S OBLATENESS	ORB00600
*	TFMO = TOTAL FORCE FROM MOON	ORB00610
*	TFSU = TOTAL FORCE FROM SUN	ORB00620
*	TL = TRUE Longitude AT EPOCH	ORB00630
*	TT = TRUE TIME SINCE SATELLITE HAS BEEN IN ORBIT	ORB00640
*	V = SATELLITE VELOCITY	ORB00650
*	VI = I VECTOR OF SATELLITE VELOCITY	ORB00660
*	VJ = J VECTOR OF SATELLITE VELOCITY	ORB00670
*	VK = K VECTOR OF SATELLITE VELOCITY	ORB00680
		ORB00690
*	A LIST OF THE ARRAYS USED FOLLOWS:	ORB00700
		ORB00710
*	AINRAY = INCLINATION	ORB00720
*	APRAY = ARGUMENT OF PERIGEE	ORB00730
*	RARAY = RADIUS	ORB00740
*	RIRAY = I VECTOR OF RADIUS	ORB00750
*	RJRAY = J VECTOR OF RADIUS	ORB00760
*	RKRAY = K VECTOR OF RADIUS	ORB00770
*	TARAY = TRUE ANOMALY	ORB00780
*	TIMRAY = TIME	ORB00790
		ORB00800
*	A LIST OF SUBROUTINES CALLED BY THE MAIN PROGRAM WILL FOLLOW:	ORB00810
		ORB00820
*	CALCEL = CALCULATES THE ORBITAL ELEMENTS	ORB00830
*	CHGVEL = ALLOW THE USER TO CHANGE THE VELOCITY OF THE SATELLITE	ORB00840
*	INPUTS = PROMPTS USER FOR INITIAL POSITION AND VELOCITY	ORB00850
*	INTSUM = INITIALIZES THE SUMS IN THE ARRAYS	ORB00860
*	NEWELT = CALCULATE NEW ORBITAL ELEMENTS FROM TIME STEP	ORB00870
*	NEWPOS = CALCULATE NEW POSITION VECTOR	ORB00880
*	NEWVEL = CALCULATE NEW VELOCITY VECTOR	ORB00890
*	OPTION = GIVE THE USER THE OPTIONS Permitted IN THE PROGRAM	ORB00900
*	PLOTS = PLOTS THE ORBITS	ORB00910
*	PRETUR = CALCULATES THE PERTURBED ORBIT	ORB00920
*	STORE = STORE THE POSITION DATA IN ARRAYS	ORB00930
*	UNPRET = CALCULATE THE UNPERTURBED ORBIT	ORB00940
		ORB00950
*	BEGIN MAIN PROGRAM	ORB00960
		ORB00970
	DOUBLE PRECISION PI,MU,RI,RJ,RK,R,VI,VJ,VK,V,HI,HJ,HK,H,	ORB00980
+	NI,NJ,NK,N,P,EI,EJ,EK,E,A,I,LAN,AP,TA,AL,LP,TL,PER,EA,	ORB00990
+	MM,MA,T,DT,TF,FR,FS,FW,TT,CHTA,RA,VA,TEMPTA,RE	ORB01000
		ORB01010
	DIMENSION TARAY(500),RARAY(500),RIRAY(500),RJRAY(500),RKRAY(500),	ORB01020
+	AINRAY(500),APRAY(500),TIMRAY(500)	ORB01030
		ORB01040
	CHARACTER*1,LOOP,YORN,ORLOOP	ORB01050
		ORB01060
	PI = 3.141592653589794	ORB01070

	MU = 3.986012D+05	ORB01080
	RE = 6.378145D+03	ORB01090
*	USER INTRO TO PROGRAM	ORB01100
	CALL INTRO	ORB01110
*	ENTERED MAIN PROGRAM LOOP	ORB01120
	LOOP = 'Y'	ORB01130
10	IF (LOOP .EQ. 'Y') THEN	ORB01140
		ORB01150
		ORB01160
		ORB01170
*	INITIALIZE STEP COUNTER AND TRUE TIME	ORB01180
20	NUM = 1	ORB01190
	TT = 0.0	ORB01200
		ORB01210
*	PROMPT USER FOR INITIAL POSITION AND VELOCITY	ORB01220
	CALL INPUTS(RI,RJ,RK,R,VI,VJ,VK,V,MU,LOOP,PI)	ORB01230
		ORB01240
*	EXIT PROGRAM	ORB01250
	IF (LOOP .EQ. 'N') THEN	ORB01260
	GOTO 10	ORB01270
	ENDIF	ORB01280
		ORB01290
*	CALCULATE AND STORE ORBITAL ELEMENTS	ORB01300
	CALL CALCEL(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,	ORB01310
+	LP,TA,PER,EA,MA,AP,AL,TF,P,PI,MU,MM,N,H,HI,HJ)	ORB01320
	CALL STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,RARAY,TARAY,	ORB01330
+	NUM,I,AP,AINRAY,APRAY,TT,TIMRAY)	ORB01340
		ORB01350
*	PRINT DATE FOR USER TO REVIEW	ORB01360
	PRINT*, 'VI =', VI, ' KM/S'	ORB01370
	PRINT*, 'VJ =', VJ, ' KM/S'	ORB01380
	PRINT*, 'VK =', VK, ' KM/S'	ORB01390
	PRINT*, 'V =', V, ' KM/S'	ORB01400
	PRINT*, 'RI =', RI, ' KM'	ORB01410
	PRINT*, 'RJ =', RJ, ' KM'	ORB01420
	PRINT*, 'RK =', RK, ' KM'	ORB01430
	PRINT*, 'R =', R, ' KM'	ORB01440
	PRINT*, 'ECCENTRICITY =', E	ORB01450
	DEGI = SNGL((180.0/PI)*I)	ORB01460
	PRINT*, 'INCLINATION =', DEGI, ' DEGREES'	ORB01470
	PERHRS = SNGL(PER/3600.0)	ORB01480
	PRINT*, 'PERIOD =', PERHRS, ' HOURS'	ORB01490
	PRINT*, 'ARE THESE VALUES CORRECT? ENTER "Y" OR "N" :'	ORB01500
	READ*, YORN	ORB01510
	CALL EXCMS('CLRSCRN')	ORB01520
	IF (.NOT. YORN .EQ. 'Y') THEN	ORB01530
	GOTO 20	ORB01540
	ENDIF	ORB01550
		ORB01560
*	CALCULATE TIME STEP AND SET TIMER TO ONE TIME STEP	ORB01570
	DT = PER/50	ORB01580
	T = DT	ORB01590
		ORB01600
*	STEP SATELLITE TO PERIGEE POINT AND RECORD	ORB01610
50	IF ((TA.GT.0.063).AND.(TA.LT.6.21)) THEN	ORB01620
	TT = TT + DT	ORB01630

	CALL NEWELT(NM,MA,E,EA,TA,TF,DT,PI,PER)	ORB01640
	CALL NPOS(RI,RJ,RK,R,LAN,AP,I,TA,A,E)	ORB01650
	CALL NVEL(E,P,TA,LAN,AP,I,VI,VJ,VK,V,MU)	ORB01660
	NUM = NUM + 1	ORB01670
	CALL STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,RARAY,TARAY,	ORB01680
	NUM,I,AP,AINRAY,APRAY,TT,TIMRAY)	ORB01690
	T = T + DT	ORB01700
	GOTO 50	ORB01710
	ENDIF	ORB01720
*	CALCULATE ELEMENTS FROM PERIGEE POINT	ORB01730
	CALL CALCEL(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,	ORB01740
	LP,TA,PER,EA,MA,AP,AL,TF,P,PI,MU,MM,N,H,HI,HJ)	ORB01750
		ORB01760
	DT = PER/50	ORB01770
	T = DT	ORB01780
		ORB01790
		ORB01800
*	STORE FIRST Unperturbed ORBIT	ORB01810
	CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB01820
	MU,PI,H,A,E,N,TA,P,MM,MA,EA,TF,T,NUM,RIRAY,RJRAY,	ORB01830
	RKRAY,RARAY,TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB01840
		ORB01850
*	INITIALIZE SUMS FOR FORCE AND ORBITAL ELEMENT CHANGES TO ZERO	ORB01860
	CALL INTSUM(TFEA,TFSU,TFMO,TFDRA,TDI,TDA,TDE,TDM,TDMA,TDLAN,	ORB01870
	TDH,TDAP)	ORB01880
		ORB01890
		ORB01900
*	PLOT FIRST UNPERTURBED ORBIT	ORB01910
70	CALL PLOTS(RIRAY,RJRAY,RKRAY,RARAY,TARAY,NUM,PI,I,LP,A,E,TF,	ORB01920
	AINRAY,APRAY,TIMRAY,TFEA,TFSU,TFMO,TFDRA,PER,TDI,TDA,	ORB01930
	TDE,TDM,TDMA,TDLAN,TDH,TDAP,MM,MA,LAN,H,AP,R,V)	ORB01940
		ORB01950
*	BEGIN NEW ORBIT OPTIONS	ORB01960
*	IOFT1 = 1. Unperturbed ORBIT	ORB01970
*	= 2. Perturbed ORBIT	ORB01980
*	= 3. QUIT	ORB01990
*	IOFT2 = 1. PLOT NEXT ORBIT	ORB02000
*	= 2. CHANGE INITIAL VALUES	ORB02010
*	= 3. CHANGE VELOCITY AT A SPECIFIC TRUE Anomaly	ORB02020
*	= 4. PLOT ANOTHER VIEW OF SAME ORBIT	ORB02030
*		ORB02040
*	ALSO ASKED IF WANT TO CLEAR ALL PREVIOUS ORBITS	ORB02050
		ORB02060
*	CALCULATE ELEMENTS AT PERIGEE	ORB02070
80	CALL CALCEL(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,	ORB02080
	LP,TA,PER,EA,MA,AP,AL,TF,P,PI,MU,MM,N,H,HI,HJ)	ORB02090
		ORB02100
*	CHECK FOR POSSIBLE ARRAY OVERFLOW	ORB02110
	IF (NUM .GT. 425) THEN	ORB02120
	PRINT*, 'ARRAYS ARE FULL'	ORB02130
	PRINT*, 'PREVIOUS ORBITS WILL BE ERASED!'	ORB02140
	NUM = 1	ORB02150
	CALL STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,RARAY,TARAY,	ORB02160
	NUM,I,AP,AINRAY,APRAY,TT,TIMRAY)	ORB02170
	ENDIF	ORB02180
		ORB02190
*	PROMPT USER FOR DESIRED OPTION	

	CALL OPTION(IOPT1, ICPT2, NUM, RIRAY, RJRAY, RKRAY, RARAY,	ORB02200
+	TARAY, AINRAY, APRAY, TIMRAY)	ORB02210
		ORB02220
*	Initialize SUMS FOR FORCE AND ORBITAL ELEMENT CHANGES TO ZERO	ORB02230
+	CALL INTSUM(TFEA, TFSU, TFMO, TFDRA, TDI, TDA, TDE, TDMM, TDMA, TDLAN,	ORB02240
	TDH, TDAP)	ORB02250
		ORB02260
*	SET TIME COUNTER TO ONE TIME STEP	ORB02270
	T = DT	ORB02280
		ORB02290
*	OPTION: PLOT THE NEXT ORBIT	ORB02300
	IF (IOPT2 .EQ. 1) THEN	ORB02310
		ORB02320
*	CALCULATE AND PLOT UNPERTURBED ORBIT	ORB02330
	IF(IOPT1 .EQ. 1) THEN	ORB02340
	CALL UNPRET(DT, PER, AL, LAN, AP, I, RI, RJ,	ORB02350
+	RK, R, VI, VJ, VK, V, MU, PI, H, A,	ORB02360
+	E, N, TA, P, MM, MA, EA, TF, T, NUM, RIRAY, RJRAY, RKRAY,	ORB02370
+	RARAY, TARAY, AINRAY, APRAY, TIMRAY, TT)	ORB02380
	CALL PLOTS(RIRAY, RJRAY, RKRAY, RARAY, TARAY, NUM,	ORB02390
+	PI, I, LP, A, E, TF, AINRAY, APRAY, TIMRAY,	ORB02400
+	TFEA, TFSU, TFMO, TFDRA, PER,	ORB02410
+	TDI, TDA, TDE, TDMM, TDMA, TDLAN, TDH, TDAP,	ORB02420
+	MM, MA, LAN, H, AP, R, V)	ORB02430
		ORB02440
*	CALCULATE AND PLOT PERTURBED ORBIT	ORB02450
	ELSEIF(IOPT1 .EQ. 2) THEN	ORB02460
	CALL PRETUR(DT, PER, AL, LAN, AP, I,	ORB02470
+	RI, RJ, RK, R, VI, VJ, VK, V, FR, FS, FW,	ORB02480
+	MU, PI, H, A, E, N, TA, P, MM, MA, EA, TF, T, NUM,	ORB02490
+	RIRAY, RJRAY, RKRAY, RARAY, TARAY, AINRAY, APRAY,	ORB02500
+	TIMRAY, TT, TFEA, TFSU, TFMO, TFDRA,	ORB02510
+	TDI, TDA, TDE, TDMM, TDMA, TDLAN, TDH, TDAP)	ORB02520
	CALL PLOTS(RIRAY, RJRAY, RKRAY, RARAY, TARAY, NUM,	ORB02530
+	PI, I, LP, A, E, TF, AINRAY, APRAY, TIMRAY,	ORB02540
+	TFEA, TFSU, TFMO, TFDRA, PER,	ORB02550
+	TDI, TDA, TDE, TDMM, TDMA, TDLAN, TDH, TDAP,	ORB02560
+	MM, MA, LAN, H, AP, R, V)	ORB02570
	ENDIF	ORB02580
		ORB02590
*	GOTO THE BEGINNING OF THE PROGRAM TO CHANGE THE INITIAL VALUES	ORB02600
	ELSEIF (IOPT2 .EQ. 2) THEN	ORB02610
	GOTO 20	ORB02620
		ORB02630
*	CHANGE VELOCITY AT A SPECIFIC TRUE ANOMALY AND	ORB02640
*	PLOT THE NEW ORBIT	ORB02650
	ELSEIF (IOPT2 .EQ. 3) THEN	ORB02660
	CALL CHGVEL(DT, PER, AL, LAN, AP, I, RI, RJ, RK, R,	ORB02670
+	VI, VJ, VK, V, MU, PI,	ORB02680
+	H, A, E, N, TA, P, MM, MA, EA, TF, T, NUM, RIRAY,	ORB02690
+	RJRAY, RKRAY, RARAY, TARAY, AINRAY, APRAY,	ORB02700
+	TIMRAY, TT, EI, EJ, EK, LP, HI, HJ, IOPT1,	ORB02710
+	TFEA, TFSU, TFMO, TFDRA, TDI, TDA, TDE, TDMM,	ORB02720
+	TDMA, TDLAN, TDH, TDAP)	ORB02730
	CALL PLOTS(RIRAY, RJRAY, RKRAY, RARAY, TARAY, NUM,	ORB02740
+	PI, I, LP, A, E, TF, AINRAY, APRAY, TIMRAY,	ORB02750

	+	TFEA, TFSU, TFMO, TFDRA, PER,	ORB02760
	+	TDI, TDA, TDE, TDM, TDMA, TDLAN, TDH, TDAP,	ORB02770
	+	MI, MA, LAN, H, AP, R, V)	ORB02780
*		PLOT ANOTHER VIEW OF THE SAME ORBIT	ORB02790
		ELSEIF (IOPT2 .EQ. 4) THEN	ORB02800
		CALL PLOTS(RIRAY, RJRAY, RKRAY, RARAY, TARAY, NCM,	ORB02810
	+	PI, I, LP, A, E, TF, AINRAY, APRAY, TIMRAY,	ORB02820
	+	TFEA, TFSU, TFMO, TFDRA, PER,	ORB02830
	+	TDI, TDA, TDE, TDM, TDMA, TDLAN, TDH, TDAP,	ORB02840
	+	MI, MA, LAN, H, AP)	ORB02850
			ORB02860
			ORB02870
*		STOP THE PROGRAM	ORB02880
		ELSEIF (IOPT2 .EQ. 5) THEN	ORB02890
		GOTO 90	ORB02900
		ELSE	ORB02910
		PRINT*, 'INVALID ENTRY!'	ORB02920
		GOTO 80	ORB02930
		ENDIF	ORB02940
			ORB02950
*		CHECK IF SATELLITE Impacted THE EARTH AND GO TO THE BEGINNING	ORB02960
		IF (R .LE. 6450.0) THEN	ORB02970
		PRINT*, 'SATELLITE WILL IMPACT THE EARTH!!!'	ORB02980
		PRINT*, 'PROGRAM WILL RESET TO THE BEGINNING'	ORB02990
		GOTO 20	ORB03000
		ENDIF	ORB03010
			ORB03020
*		GOTO THE TOP OF THE OPTION LOOP	ORB03030
		GOTO 60	ORB03040
			ORB03050
*		GIVE THE USER A CHANCE TO RECOVER THE PROGRAM	ORB03060
90		PRINT*, 'THIS IS YOUR LAST CHANCE!'	ORB03070
		PRINT*, 'DO YOU WANT TO CONTINUE?'	ORB03080
		PRINT*, 'AND GOTO THE Beginning OF THE PROGRAM?'	ORB03090
		PRINT*, 'ENTER "Y" OR "N" :'	ORB03100
		READ*, LOOP	ORB03110
		PRINT*, LOOP	ORB03120
		GOTO 10	ORB03130
		ENDIF	ORB03140
			ORB03150
*		DISSPLA SUBROUTINE TO TELL GRAPHICS TERMINAL PLOTTING	ORB03160
*		SESSION IS DONE	ORB03170
		CALL DONEPL	ORB03180
		STOP	ORB03190
		END	ORB03200
			ORB03210
		*****	ORB03220
			ORB03230
		SUBROUTINE INTRO	ORB03240
*		THIS SUBROUTINE WILL GIVE THE USER A Brief INTRODUCTION OF THE	ORB03250
*		USES OF THE PROGRAM	ORB03260
			ORB03270
		PRINT*, 'THIS PROGRAM IS A GRAPHICS DISPLAY OF Satellite ORBITS.'	ORB03280
		PRINT*, 'YOU WILL BE ASKED TO INPUT THE INITIAL VELOCITY AND'	ORB03290
		PRINT*, 'POSITION VECTORS OF THE Satellite. THE PROGRAM WILL'	ORB03300
		PRINT*, 'THEN CALCULATE THE ORBITAL PARAMETERS AND THE'	ORB03310

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PRINT*, 'Unperturbed ORBIT. THE USER WILL THEN HAVE THE' ORB03320
PRINT*, 'CHOICE OF DISPLAYS:' ORB03330
PRINT*, '-PERIFICAL (SHOWS RELATIVE SIZE OF ORBIT)' ORB03340
PRINT*, '-Equatorial (SHOWS ORBIT INCLINED, USER INPUT' ORB03350
PRINT*, 'LONGITUDE TO VIEW AT)' ORB03360
PRINT*, '-GROUND TRACK' ORB03370
PRINT*, ' ' ORB03380
PRINT*, 'THE USER IS THEN ASKED TO CHOOSE ONE OF THE FOLLOWING:' ORB03390
PRINT*, '-Unperturbed ORBITS' ORB03400
PRINT*, '-Perturbed ORBITS' ORB03410
PRINT*, '-VELOCITY CHANGES' ORB03420
PRINT*, 'THE USER'S CHOICE WILL BE USED IN DEVELOPING THE' ORB03430
PRINT*, 'GRAPHICAL OUTPUT.' ORB03440
PRINT*, ' ' ORB03450
PRINT*, 'THE USER IS THEN GIVEN THE FOLLOWING CHOICES:' ORB03460
PRINT*, '-CLEAR ALL THE PREVIOUS ORBITS' ORB03470
PRINT*, '-CHANGE THE INITIAL PARAMETERS' ORB03480
PRINT*, '-CHANGE VELOCITY AT A SPECIFIC TRUE Anomaly' ORB03490
PRINT*, '-PLOT ANOTHER VIEW OF THE SAME ORBIT' ORB03500
RETURN ORB03510
END ORB03520

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SUBROUTINE OPTION(IOPT1, IOPT2, NUM, RIRAY, RJRAY, RKRAY, RARAY, ORB03530
+ TARAY, AINRAY, APRAY, TIMRAY) ORB03540
* THIS SUBROUTINE GIVES THE USER A CHOICE OF OPERATIONS THAT CAN BE ORB03550
* PERFORMED ON THE PROGRAM AND RETURNS THE USERS CHOICE WITH ORB03560
* VARIABLES IOPT1 AND IOPT2 ORB03570
DIMENSION RIRAY(500), RJRAY(500), RKRAY(500), RARAY(500), TARAY(500), ORB03600
+ AINRAY(500), APRAY(500), TIMRAY(500) ORB03610
CHARACTER*1, YORN ORB03620
IOPT1 = 0 ORB03630
* PROMPT USER FOR OPTION ORB03640
103 PRINT*, 'WHICH OF THE FOLLOWING OPTIONS WOULD YOU LIKE:' ORB03650
PRINT*, ' 1. -CALCULATE THE NEXT ORBIT USING THE SAME' ORB03660
PRINT*, ' PARAMETERS' ORB03670
PRINT*, ' 2. -CHANGE THE INITIAL PARAMETERS OF THE ORBIT' ORB03680
PRINT*, ' 3. -CHANGE THE VELOCITY AT A POINT IN THE ORBIT' ORB03690
PRINT*, ' (THE UNPERTURBED ORBIT WILL BE USED)' ORB03700
PRINT*, ' 4. -PLOT ANOTHER VIEW OF THE ORBIT(S)' ORB03710
PRINT*, ' 5. -QUIT' ORB03720
PRINT*, 'ENTER 1, 2, 3, 4, OR 5:' ORB03730
READ*, IOPT2 ORB03740
PRINT*, IOPT2 ORB03750
CALL EXCMS('CLRSCRN') ORB03760
IF ( IOPT2 .GT. 5) THEN ORB03770
GOTO 103 ORB03780
ENDIF ORB03790
* Prompt USER FOR TYPE OF ORBIT DESIRED ORB03800
105 IF (IOPT2 .EQ. 1) THEN ORB03810
PRINT*, 'WHICH TYPE OF ORBIT WOULD YOU LIKE TO SEE,' ORB03820
PRINT*, ' 1. -Unperturbed ORBITS' ORB03830
ORB03840
ORB03850
ORB03860
ORB03870

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PRINT*, ' 2.-Perturbed ORBITS'
PRINT*, ' ENTER 1 OR 2:'
READ*, IOPT1
PRINT*, IOPT1
CALL EXCMS('CLRSCRN')
IF ((IOPT1 .NE. 1) .AND. (IOPT1 .NE. 2)) THEN
    PRINT*, 'INVALID ENTRY!'
    GOTO 105
ENDIF
ENDIF
107 * PROMPT USER TO CLEAR PREVIOUS ORBITS
IF ((IOPT2 .EQ. 1) .OR. (IOPT2 .EQ. 3)) THEN
    PRINT*, 'DO YOU WANT TO CLEAR THE PREVIOUS ORBITS?'
    PRINT*, 'ENTER "Y" OR "N" : '
    READ*, YORN
    PRINT*, YORN
    CALL EXCMS('Clrscrn')
    IF (YORN .EQ. 'Y') THEN
        RIRAY(1) = RIRAY(NUM)
        RJRAY(1) = RJRAY(NUM)
        RKRAY(1) = RKRAY(NUM)
        RARAY(1) = RARAY(NUM)
        TARAY(1) = TARAY(NUM)
        AINRAY(1) = AINRAY(NUM)
        APRAY(1) = APRAY(NUM)
        TIMRAY(1) = TIMRAY(NUM)
        NUM = 1
    ELSEIF (YORN .NE. 'N') THEN
        PRINT*, 'INVALID ENTRY!!'
        PRINT*, 'ALL INPUTS MUST BE CAPITOL LETTERS'
        GOTO 107
    ENDIF
ENDIF
* CHECK FOR INVALID OPTION
IF ((IOPT2 .NE. 1) .AND. (IOPT2 .NE. 2) .AND. (IOPT2 .NE. 3) .AND.
+ (IOPT2 .NE. 4) .AND. (IOPT2 .NE. 5)) THEN
    PRINT*, 'INVALID ENTRY!'
    GOTO 103
ENDIF
RETURN
END

*****
* COORDINATE TRANSFORMATIONS
*****

SUBROUTINE PQWIJK(LAN,AP,INC,P,Q,W,I,J,K)
* THIS SUBROUTINE TRANSFORMS PQW COORDINATES TO IJK COORDINATES

DOUBLE PRECISION INC,P,Q,W,I,J,K,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,LAN,AP
R11 = DCOS(LAN)*DCOS(AP) - DSIN(LAN)*DSIN(AP)*DCOS(INC)
R12 = -DCOS(LAN)*DSIN(AP) - DSIN(LAN)*DCOS(AP)*DCOS(INC)
R13 = DSIN(LAN)*DSIN(INC)

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ORB03880
ORB03890
ORB03900
ORB03910
ORB03920
ORB03930
ORB03940
ORB03950
ORB03960
ORB03970
ORB03980
ORB03990
ORB04000
ORB04010
ORB04020
ORB04030
ORB04040
ORB04050
ORB04060
ORB04070
ORB04080
ORB04090
ORB04100
ORB04110
ORB04120
ORB04130
ORB04140
ORB04150
ORB04160
ORB04170
ORB04180
ORB04190
ORB04200
ORB04210
ORB04220
ORB04230
ORB04240
ORB04250
ORB04260
ORB04270
ORB04280
ORB04290
ORB04300
ORB04310
ORB04320
ORB04330
ORB04340
ORB04350
ORB04360
ORB04370
ORB04380
ORB04390
ORB04400
ORB04410
ORB04420
ORB04430

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```

R21 = DSIN(LAN)*DCOS(AP) + DCOS(LAN)*DSIN(AP)*DCOS( INC)
R22 = -DSIN(LAN)*DSIN(AP) + DCOS(LAN)*DCOS(AP)*DCOS( INC)
R23 = -DCOS(LAN)*DSIN( INC)
R31 = DSIN(AP)*DSIN( INC)
R32 = DCOS(AP)*DSIN( INC)
R33 = DCOS( INC)
I = R11*P + R12*Q + R13*W
J = R21*P + R22*Q + R23*W
K = R31*P + R32*Q + R33*W
RETURN
END

```

```

ORB04440
ORB04450
ORB04460
ORB04470
ORB04480
ORB04490
ORB04500
ORB04510
ORB04520
ORB04530
ORB04540
ORB04550
ORB04560

```

```

* SUBROUTINE IJKPQW(LAN,AP,INC,I,J,K,P,Q,W)
  THIS SUBROUTINE TRANSFORMS IJK COORDINATES TO PQW COORDINATES

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```

DOUBLE PRECISION INC,I,J,K,P,Q,W,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,LAN,AP
R11 = DCOS(LAN)*DCOS(AP) - DSIN(LAN)*DSIN(AP)*DCOS( INC)
R21 = -DCOS(LAN)*DSIN(AP) - DSIN(LAN)*DCOS(AP)*DCOS( INC)
R31 = DSIN(LAN)*DSIN( INC)
R12 = DSIN(LAN)*DCOS(AP) + DCOS(LAN)*DSIN(AP)*DCOS( INC)
R22 = -DSIN(LAN)*DSIN(AP) + DCOS(LAN)*DCOS(AP)*DCOS( INC)
R32 = -DCOS(LAN)*DSIN( INC)
R13 = DSIN(AP)*DSIN( INC)
R23 = DCOS(AP)*DSIN( INC)
R33 = DCOS( INC)
P = R11*I + R12*J + R13*K
Q = R21*I + R22*J + R23*K
W = R31*I + R32*J + R33*K
RETURN
END

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ORB04570
ORB04580
ORB04590
ORB04600
ORB04610
ORB04620
ORB04630
ORB04640
ORB04650
ORB04660
ORB04670
ORB04680
ORB04690
ORB04700
ORB04710
ORB04720
ORB04730
ORB04740
ORB04750
ORB04760
ORB04770

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```

* SUBROUTINE IJKRSW(LAN,AL,INC,I,J,K,R,S,W)
  THIS SUBROUTINE CHANGES FROM IJK COORDINATES TO RSW COORDINATES

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```

DOUBLE PRECISION INC,I,J,K,R,S,W,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,LAN,AL
R11 = DCOS(LAN)*DCOS(AL) - DSIN(LAN)*DCOS( INC)*DSIN(AL)
R12 = DSIN(LAN)*DCOS(AL) + DSIN(AL)*DCOS(LAN)*DCOS( INC)
R13 = DSIN( INC)*DSIN(AL)
R21 = -DCOS(LAN)*DSIN(AL) - DSIN(LAN)*DCOS( INC)*DCOS(AL)
R22 = -DSIN(LAN)*DSIN(AL) + DCOS(LAN)*DCOS( INC)*DCOS(AL)
R23 = DSIN( INC)*DCOS(AL)
R31 = DSIN(LAN)*DSIN( INC)
R32 = -DCOS(LAN)*DSIN( INC)
R33 = DCOS( INC)
R = R11*I + R12*J + R13*K
S = R21*I + R22*J + R23*K
W = R31*I + R32*J + R33*K
RETURN
END

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ORB04780
ORB04790
ORB04800
ORB04810
ORB04820
ORB04830
ORB04840
ORB04850
ORB04860
ORB04870
ORB04880
ORB04890
ORB04900
ORB04910
ORB04920
ORB04930
ORB04940
ORB04950
ORB04960
ORB04970
ORB04980

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```

*****
SUBROUTINE RSWIJK(LAN,AL,INC,R,S,W,I,J,K)
* THIS SUBROUTINE CHANGES FROM RSW COORDINATES TO IJK COORDINATES

DOUBLE PRECISION INC,R,S,W,I,J,K,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,LAN,AL
R11 = DCOS(LAN)*DCOS(AL) - DSIN(LAN)*DCOS( INC)*DSIN(AL)
R21 = DSIN(LAN)*DCOS(AL) + DSIN(AL)*DCOS(LAN)*DCOS( INC)
R31 = DSIN( INC)*DSIN(AL)
R12 = -DCOS(LAN)*DSIN(AL)-DSIN(LAN)*DCOS( INC)*DCOS(AL)
R22 = -DSIN(LAN)*DSIN(AL) + DCOS(LAN)*DCOS( INC)*DCOS(AL)
R32 = DSIN( INC)*DCOS(AL)
R13 = DSIN(LAN)*DSIN( INC)
R23 = -DCOS(LAN)*DSIN( INC)
R33 = DCOS( INC)
I = R11*R + R12*S + R13*W
J = R21*R + R22*S + R23*W
K = R31*R + R32*S + R33*W
RETURN
END

*****
SUBROUTINE PQWRSW(TA,P,Q,W,R,S,WN)
* THIS SUBROUTINE CHANGES FROM PQW COORDINATES TO RSW COORDINATES

DOUBLE PRECISION P,Q,W,R,S,WN,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,TA
R11 = DCOS(TA)
R12 = DSIN(TA)
R13 = 0.0
R21 = -DSIN(TA)
R22 = DCOS(TA)
R23 = 0.0
R31 = 0.0
R32 = 0.0
R33 = 1.0
R = R11*P + R12*Q + R13*W
S = R21*P + R22*Q + R23*W
WN = R31*P + R32*Q + R33*W
RETURN
END

*****
SUBROUTINE RSWPQW(TA,R,S,W,P,Q,WN)
* THIS SUBROUTINE CHANGES FROM RSW COORDINATES TO PQW COORDINATES

DOUBLE PRECISION R,S,W,P,Q,WN,R11,R12,R13,R21,R22,R23,
+ R31,R32,R33,TA
R11 = DCOS(TA)
R21 = DSIN(TA)
R31 = 0.0
R12 = -DSIN(TA)

```

```

ORB04990
ORB05000
ORB05010
ORB05020
ORB05030
ORB05040
ORB05050
ORB05060
ORB05070
ORB05080
ORB05090
ORB05100
ORB05110
ORB05120
ORB05130
ORB05140
ORB05150
ORB05160
ORB05170
ORB05180
ORB05190
ORB05200
ORB05210
ORB05220
ORB05230
ORB05240
ORB05250
ORB05260
ORB05270
ORB05280
ORB05290
ORB05300
ORB05310
ORB05320
ORB05330
ORB05340
ORB05350
ORB05360
ORB05370
ORB05380
ORB05390
ORB05400
ORB05410
ORB05420
ORB05430
ORB05440
ORB05450
ORB05460
ORB05470
ORB05480
ORB05490
ORB05500
ORB05510
ORB05520
ORB05530
ORB05540

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```

R22 = DCOS(TA)
R32 = 0.0
R13 = 0.0
R23 = 0.0
R33 = 1.0
P = R11*R + R12*S + R13*W
Q = R21*R + R22*S + R23*W
WN = R31*R + R32*S + R33*W
RETURN
END

```

```

ORB05550
ORB05560
ORB05570
ORB05580
ORB05590
ORB05600
ORB05610
ORB05620
ORB05630
ORB05640
ORB05650
ORB05660
ORB05670
ORB05680
ORB05690
ORB05700
ORB05710
ORB05720
ORB05730
ORB05740
ORB05750
ORB05760
ORB05770
ORB05780
ORB05790
ORB05800
ORB05810
ORB05820
ORB05830
ORB05840
ORB05850
ORB05860
ORB05870
ORB05880
ORB05890
ORB05900
ORB05910
ORB05920
ORB05930
ORB05940
ORB05950
ORB05960
ORB05970
ORB05980
ORB05990
ORB06000
ORB06010
ORB06020
ORB06030
ORB06040
ORB06050
ORB06060
ORB06070
ORB06080
ORB06090
ORB06100

```

```

*****
* STORE ELEMENTS IN ARRAYS
*****

```

```

SUBROUTINE STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,RARAY,TARAY,NUM,
+ I,AP,AINRAY,APRAY,TT,TIMRAY)
* THIS SUBROUTINE STORES THE POSITION AND ELEMENTS IN ARRAYS IN
* SINGLE PRECISION FORM, FOR PLOTTING

DOUBLE PRECISION RI,RJ,RK,R,TA,I,AP,TT

DIMENSION RIRAY(500),RJRAY(500),RKRAY(500),RARAY(500),TARAY(500),
+ AINRAY(500),APRAY(500),TIMRAY(500)

RIRAY(NUM) = SNGL(RI)
RJRAY(NUM) = SNGL(RJ)
RKRAY(NUM) = SNGL(RK)
RARAY(NUM) = SNGL(R)
TARAY(NUM) = SNGL(TA)
AINRAY(NUM) = SNGL(I)
APRAY(NUM) = SNGL(AP)
TIMRAY(NUM) = SNGL(TT)
RETURN
END

```

```

*****
* INITIAL POSITION, VELOCITY
*****

```

```

SUBROUTINE INPUTS(RI,RJ,RK,R,VI,VJ,VK,V,MU,QUIT PI)
* THIS SUBROUTINE GIVES THE USER A CHOICE TO EITHER ENTER THE
* INITIAL POSITION AND VELOCITY VECTOR OR TO INPUT THE PROGRAM
* CALCULATE THE INITIAL POSITION AND VELOCITY FROM USER PROMPTED
* INPUTS

* SUBROUTINES CALLED FROM THIS SUBROUTINE:
* INELTS = Prompts USER FOR ORBITAL ELEMENTS
* IPOS = PROMPTS USER FOR INITIAL POSITION (IJK)
* IVEL = PROMPTS USER FOR INITIAL Velocity (IJK)

DOUBLE PRECISION RI,RJ,RK,R,VI,VJ,VK,V,MU,PI
CHARACTER*1,QUIT

* PROMPT USER FOR METHOD TO ENTER INPUTS
195 PRINT*, 'IN WHICH MANNER WOULD YOU LIKE TO INPUT THE INITIAL'

```

```

PRINT*, 'POSITION AND VELOCITY OF THE SATELLITE?'
PRINT*, ' 1: BY Inputting THE INITIAL POSITION AND VELOCITY'
PRINT*, ' VECTORS IN THE PERIFOCAL COORDINATE SYSTEM (IJK)'
PRINT*, ' 2: BY LETTING THE SATELLITE BE PLACED ON THE "I"'
PRINT*, ' AXIS OF THE (IJK) SYSTEM AT A DESIRED RADIUS OF'
PRINT*, ' PERIGEE(RP) AND INPUTTING EITHER A DESIRED RADIUS'
PRINT*, ' OF APOGEE(RA), A DESIRED ECCENTRICITY(E), OR THE'
PRINT*, ' DESIRED VELOCITY AT THAT RADIUS, AND A DESIRED'
PRINT*, ' INCLINATION(I).'
PRINT*, ' 3: QUIT'
PRINT*, 'ENTER 1, 2 OR 3:'
READ*, ICHC
PRINT*, ICHC
CALL EXCMS('CLRSCRN')

* USER INPUTS POSITION AND VELOCITY VECTORS
IF (ICHC .EQ. 1) THEN
  CALL IFOS(RI,RJ,RK,R)
  CALL IVEL(VI,VJ,VK,V,R,MU)

* USER INPUTS ORBITAL ELEMENTS TO GET POSITION AND VELOCITY
ELSEIF (ICHC .EQ. 2) THEN
  CALL INELTS(RI,RJ,RK,R,VI,VJ,VK,V,MU,PI)

* STOP PROGRAM
ELSEIF (ICHC .EQ. 3) THEN
  QUIT = 'N'
ELSE
  PRINT*, 'INVALID ENTRY! TRY AGAIN!'
  GOTO 195
ENDIF
RETURN
END

*****

SUBROUTINE IFOS(RI,RJ,RK,R)
* THIS SUBROUTINE ASKS THE USER FOR THE INITIAL POSITION OF THE
* Satellite IN GEOCENTRIC-EQUATORIAL COORDINATE SYSTEM

DOUBLE PRECISION RI,RJ,RK,R

CHARACTER*1, CHOICE
LOGICAL CORREC
CORREC = .FALSE.

* PROMPT USER FOR VELOCITY VECTOR
180 IF(.NOT.CORREC) THEN
  CALL EXCMS('CLRSCRN')
  PRINT*, 'ENTER RADIUS VECTOR VALUES IN "KM"'
  PRINT*, 'RADIUS OF THE EARTH = 6400 KM'
  CORREC = .TRUE.
  PRINT*, 'ENTER RI : '
  READ*, RI
  PRINT*, 'RI = ', RI, 'KM'
  PRINT*, 'ENTER RJ : '

```

```

ORB06110
ORB06120
ORB06130
ORB06140
ORB06150
ORB06160
ORB06170
ORB06180
ORB06190
ORB06200
ORB06210
ORB06220
ORB06230
ORB06240
ORB06250
ORB06260
ORB06270
ORB06280
ORB06290
ORB06300
ORB06310
ORB06320
ORB06330
ORB06340
ORB06350
ORB06360
ORB06370
ORB06380
ORB06390
ORB06400
ORB06410
ORB06420
ORB06430
ORB06440
ORB06450
ORB06460
ORB06470
ORB06480
ORB06490
ORB06500
ORB06510
ORB06520
ORB06530
ORB06540
ORB06550
ORB06560
ORB06570
ORB06580
ORB06590
ORB06600
ORB06610
ORB06620
ORB06630
ORB06640
ORB06650
ORB06660

```

```

READ*,RJ
PRINT*, 'RJ = ',RJ, 'KM'
PRINT*, 'ENTER RK : '
READ*,RK
PRINT*, 'RK = ',RK, 'KM'
*
CALCULATE TOTAL R
R = DSQRT((RI**2) + (RJ**2) + (RK**2))
PRINT*, 'R = ',R, 'KM'
IF (R .LE. 6400.0) THEN
    PRINT*, 'RADIUS TOO SMALL!! ENTER NEW VALUES!!'
    GOTO 150
ENDIF
*
CHECK WITH USER THAT Values ARE CORRECT
PRINT*, 'ARE THESE VALUES CORRECT?'
PRINT*, 'ENTER "Y" OR "N" : '
READ*,CHOICE
CHOICE = 'Y'
PRINT*,CHOICE
IF (CHOICE.EQ. 'Y') THEN
    CORREC = .TRUE.
ENDIF
GOTO 180
ENDIF
RETURN
END
*****

SUBROUTINE IVEL(VI,VJ,VK,V,R,MU)
* THIS SUBROUTINE ASKS THE USER FOR THE INITIAL VELOCITY OF THE
* Satellite
DOUBLE PRECISION VI,VJ,VK,V,R,VCIR,VMAX,MU
CHARACTER*1, CHOICE
LOGICAL CORREC
CORREC = .FALSE.
*
CALCULATE ESCAPE VELOCITY AND CIRCULAR VELOCITY AND PROMPT USER
* FOR VELOCITY VECTOR
190 IF(.NOT. CORREC) THEN
    CALL EXCMS('CLRSCRN')
    VCIR = DSQRT(MU/R)
    VMAX = DSQRT((2.0*MU)/R)
    PRINT*, 'CIRCULAR VELOCITY = ',VCIR, 'KM/SEC'
    PRINT*, 'MAXIMUM VELOCITY = ',VMAX, 'KM/SEC'
    CORREC = .TRUE.
    PRINT*, 'ENTER VELOCITY VECTOR IN (KM/SEC)'
    PRINT*, 'ENTER VI : '
    READ*,VI
    PRINT*, 'VI = ',VI, 'KM/SEC'
    PRINT*, 'ENTER VJ : '
    READ*,VJ

```

```

ORB06670
ORB06680
ORB06690
ORB06700
ORB06710
ORB06720
ORB06730
ORB06740
ORB06750
ORB06760
ORB06770
ORB06780
ORB06790
ORB06800
ORB06810
ORB06820
ORB06830
ORB06840
ORB06850
ORB06860
ORB06870
ORB06880
ORB06890
ORB06900
ORB06910
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ORB06930
ORB06940
ORB06950
ORB06960
ORB06970
ORB06980
ORB06990
ORB07000
ORB07010
ORB07020
ORB07030
ORB07040
ORB07050
ORB07060
ORB07070
ORB07080
ORB07090
ORB07100
ORB07110
ORB07120
ORB07130
ORB07140
ORB07150
ORB07160
ORB07170
ORB07180
ORB07190
ORB07200
ORB07210
ORB07220

```

```

PRINT*, 'VJ = ', VJ, 'KM/SEC'
PRINT*, 'ENTER VK : '
READ*, VK
PRINT*, 'VK = ', VK, 'KM/SEC'
*
CALCULATE TOTAL VELOCITY (V)
V = DSQRT((VI**2) + (VJ**2) + (VK**2))
PRINT*, 'V = ', V, 'KM/SEC'
*
CHECK WITH USER THAT VALUES ARE CORRECTS
PRINT*, 'ARE THESE VALUES CORRECT?'
PRINT*, '    ENTER "Y" OR "N" : '
READ*, CHOICE
CHOICE = 'Y'
PRINT*, CHOICE
IF (CHOICE.EQ. 'Y') THEN
    CORREC = .TRUE.
ENDIF
IF (V .GE. VMAX) THEN
    PRINT*, 'VELOCITY IS GREATER THAN THE ESCAPE VELOCITY!!'
    PRINT*, 'RE-ENTER VELOCITY!!!'
    CORREC = .FALSE.
ENDIF
GOTO 190
ENDIF
RETURN
END
*****
SUBROUTINE INELTS(RI, RJ, RK, R, VI, VJ, VK, V, MU, PI)
*
SATELLITE PLACED ON 'I' AXIS AND USER SUPPLY ORBITAL ELEMENTS TO
*
GET INITIAL POSITION AND VELOCITY
*****
DOUBLE PRECISION RI, RJ, RK, R, VI, VJ, VK, V, MU, I, ENR, A, E, RP, RA, PI, VMAX
CHARACTER*1, CHOICE
*
PROMPT USER FOR PERIGEE RADIUS
198 PRINT*, 'ENTER RADIUS OF PERIGEE(RP) IN (KM), FOR EXAMPLE: '
PRINT*, 'LOW EARTH ORBIT (LEO), RP = 6600.0 KM'
PRINT*, 'GEOSYNCRONOUS ORBIT, RP = 42241.1 KM'
PRINT*, 'ENTER RP: '
PRINT*, '"RP" MUST BE > 6400KM'
READ*, RP
PRINT*, RP
*
CHECK FOR VALID RADIUS
IF (RP .LT. 6400.0) THEN
    PRINT*, 'YOUR "RP" IS TOO SMALL!!'
    GOTO 198
ENDIF
*
PROMPT USER FOR TYPE OF INPUT
PRINT*, 'DO YOU WANT TO ENTER THE ECCENTRICITY (E), '
PRINT*, 'RADIUS OF APOGEE (RA), OR VELOCITY (V)?'
PRINT*, 'ENTER "E", "R", OR "V": '

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```

ORB07230
ORB07240
ORB07250
ORB07260
ORB07270
ORB07280
ORB07290
ORB07300
ORB07310
ORB07320
ORB07330
ORB07340
ORB07350
ORB07360
ORB07370
ORB07380
ORB07390
ORB07400
ORB07410
ORB07420
ORB07430
ORB07440
ORB07450
ORB07460
ORB07470
ORB07480
ORB07490
ORB07500
ORB07510
ORB07520
ORB07530
ORB07540
ORB07550
ORB07560
ORB07570
ORB07580
ORB07590
ORB07600
ORB07610
ORB07620
ORB07630
ORB07640
ORB07650
ORB07660
ORB07670
ORB07680
ORB07690
ORB07700
ORB07710
ORB07720
ORB07730
ORB07740
ORB07750
ORB07760
ORB07770
ORB07780

```

READ*,CHOICE	ORB07790
PRINT*,CHOICE	ORB07800
CALL ENCLS('CLRSRN')	ORB07810
	ORB07820
* USER ENTERS Eccentricity AND SEMI-MAJOR AXIS, ENERGY AND VELOCITY	ORB07830
* IS CALCULATED IN THAT ORDER	ORB07840
IF (CHOICE .EQ. 'E') THEN	ORB07850
PRINT*, 'ENTER ECCENTRICITY (E):'	ORB07860
PRINT*, '0.0 <= E < 1.0'	ORB07870
READ*,E	ORB07880
PRINT*,E	ORB07890
	ORB07900
* CHECK FOR VALID ECCENTRICITY	ORB07910
IF ((E .LT. 0.0) .OR. (E .GE. 1.0)) THEN	ORB07920
PRINT*, 'INVALID "E"'	ORB07930
GOTO 198	ORB07940
ENDIF	ORB07950
A = RP/(1-E)	ORB07960
ENR = -MU/(2.0*A)	ORB07970
V = DSQRT(2*(ENR+(MU/RP)))	ORB07980
	ORB07990
* USER INPUTS RADIUS OF APOGEE AND ECCENTRICITY IS CALCULATED	ORB08000
* THEN SEMI-MAJOR AXIS, ENERGY AND THEN VELOCITY.	ORB08010
ELSEIF (CHOICE .EQ. 'R') THEN	ORB08020
PRINT*, 'ENTER RADIUS OF APOGEE (RA) IN KM: '	ORB08030
PRINT*, '"RA" MUST BE >="RP", "RP" = ',RP	ORB08040
READ*,RA	ORB08050
PRINT*,RA	ORB08060
	ORB08070
* CHECK FOR VALID RADIUS OF APOGEE	ORB08080
IF (RA .LT. RP) THEN	ORB08090
PRINT*, 'YOUR "RA" IS TOO SMALL!!'	ORB08100
GOTO 198	ORB08110
ENDIF	ORB08120
E = (RA-RP)/(RA+RP)	ORB08130
A = RP/(1-E)	ORB08140
ENR = -MU/(2.0*A)	ORB08150
V = DSQRT(2*(ENR+(MU/RP)))	ORB08160
	ORB08170
* USER INPUTS MAGNITUDE OF VELOCITY, PROGRAM PROVIDES CIRCULAR	ORB08180
* AND ESCAPE VELOCITY FOR COMPARISON AND TO CHECK FOR VALID	ORB08190
* INPUTS	ORB08200
ELSEIF (CHOICE .EQ. 'V') THEN	ORB08210
PRINT*, 'ENTER VELOCITY IN KM/SEC: '	ORB08220
PRINT*, 'THE MINIMUM VELOCITY ALLOWED IS FOR A CIRCULAR ORBIT'	ORB08230
VCIRC = SQRT(SNGL(MU/RP))	ORB08240
PRINT*, 'ORBIT. V(Circular) = ',VCIRC, ' KM/S'	ORB08250
VMAX = DSQRT(2*(MU/RP))	ORB08260
PRINT*, 'THE MAXIMUM VELOCITY < ',VMAX, ' KM/S'	ORB08270
READ*,V	ORB08280
PRINT*,V	ORB08290
IF (V .LT. VCIRC) THEN	ORB08300
PRINT*, 'VELOCITY TOO SMALL!'	ORB08310
GOTO 198	ORB08320
ENDIF	ORB08330
IF (V .GE. VMAX) THEN	ORB08340

```

      PRINT*, 'VELOCITY TO GREAT!!'
      GOTO 198
    ENDIF
  ELSE
    PRINT*, 'INVALID ENTRY! TRY AGAIN'
    GOTO 198
  ENDIF

```

```

*   INCLINATION NEEDED TO GIVE Velocity A Direction
    PRINT*, 'ENTER INCLINATION (I) IN DEGREES:'
    READ*, I
    PRINT*, I
    I = (PI/180.0)*I
    VK = V*DSIN(I)
    VJ = V*DCOS(I)
    VI = 0.0

*   RADIUS VECTOR SET
    RI = RP
    RJ = 0.0
    RK = 0.0
    R = RP
    RETURN
    END

```

```

*****
* CALCULATE THE ORBITAL ELEMENTS
*****

```

```

      SUBROUTINE CALCEL(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,
+      LP,TA,PER,EA,MA,AP,AL,TF,P,PI,MU,MM,N,H,HI,HJ)
*   THIS SUBROUTINE CALLS THE INDIVIDUAL SUBROUTINES TO CALCULATE THE
*   ORBITAL ELEMENTS

*   THIS SUBROUTINE CALLS THE FOLLOWING SUBROUTINES(RETURNED VALUES)
*   ENERGY = ENERGY PER MASS (ENR)
*   ANGMOM = ANGULAR MOMENTUM (H,HI,HJ,HK)
*   NODE = NODE VECTOR (N,NI,NJ,NK)
*   LATREC = SEMI-LATUS RECTUS (P)
*   ECC = ECCENTRICITY (E,EI,EJ,EK)
*   SMAXIS = SEMI-MAJOR AXIS (A)
*   INCL = INCLINATION (I)
*   ASNODE = LONGITUDE OF ASCENDING NODE (LAN)
*   ARP = ARGUMENT OF PERIGEE (AP)
*   IJKPQW = 'IJK' SYSTEM TO 'PQW' SYSTEM
*   TANOM = TRUE ANOMALY (TA)
*   ARLAT = ARGUMENT OF LATITUDE (AL)
*   LONPER = LONGITUDE OF Perigee (LP)
*   TLON = TRUE LONGITUDE (TL)
*   PERIOD = PERIOD (PER)
*   ECCAN = ECCENTRIC ANOMALY (EA)
*   MEANMO = MEAN MOTION (MM)
*   MEANAN = MEAN ANOMALY (MA)
*   TFLIGHT = TIME OF FLIGHT (TF)

      DOUBLE PRECISION RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,AL,

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```

ORB08350
ORB08360
ORB08370
ORB08380
ORB08390
ORB08400
ORB08410
ORB08420
ORB08430
ORB08440
ORB08450
ORB08460
ORB08470
ORB08480
ORB08490
ORB08500
ORB08510
ORB08520
ORB08530
ORB08540
ORB08550
ORB08560
ORB08570
ORB08580
ORB08590
ORB08600
ORB08610
ORB08620
ORB08630
ORB08640
ORB08650
ORB08660
ORB08670
ORB08680
ORB08690
ORB08700
ORB08710
ORB08720
ORB08730
ORB08740
ORB08750
ORB08760
ORB08770
ORB08780
ORB08790
ORB08800
ORB08810
ORB08820
ORB08830
ORB08840
ORB08850
ORB08860
ORB08870
ORB08880
ORB08890
ORB08900

```

```

+ LP,TA,PER,EA,MA,AP,TF,HI,HJ,HK,H,NI,NJ,NK,N,P,PI,MU,MM,ENR, ORB08910
+ TL,RP,RQ,RW,NP,NQ,NW ORB08920
CALL ENERGY(V,R,MU,ENR) ORB08930
CALL ANGMOM(RI,RJ,RK,VI,VJ,VK,HI,HJ,HK,H) ORB08940
CALL NODE(HI,HJ,NI,NJ,NK,N) ORB08950
CALL LATREC(H,P,MU) ORB08960
CALL ECC(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,MU) ORB08970
CALL SMANIS(MU,ENR,A) ORB08980
CALL INCL(HK,H,I,PI) ORB08990
ORB09000
* SPECIAL CASE IF INCLINATION = 0.0 ORB09010
IF (I.NE.0.0) THEN ORB09020
CALL ASNODE(NI,N,LAN,NJ,PI) ORB09030
CALL ARP(NI,NJ,N,EI,EJ,EK,E,AP,PI,NP,NQ,LAN) ORB09040
ELSE ORB09050
LAN = 0.0 ORB09060
AP = 0.0 ORB09070
ENDIF ORB09080
ORB09090
* COORDINATE TRANSFORMATION OF 'R' AND 'V' VECTORS ORB09100
CALL IJKPQW(LAN,AP,I,RI,RJ,RK,RP,RQ,RW) ORB09110
CALL IJKPQW(LAN,AP,I,NI,NJ,NK,NP,NQ,NW) ORB09120
CALL TANON(EI,EJ,EK,E,RI,RJ,RK,RP,RQ,RW,R,VI,VJ,VK,TA,PI) ORB09130
ORB09140
* SPECIAL CASE FOR Inclination = 0.0 ORB09150
IF (I.NE.0.0) THEN ORB09160
CALL ARLAT(NI,NJ,NK,N,RI,RJ,RK,R,AL,PI,TA,AP) ORB09170
ELSE ORB09180
AL = TA ORB09190
ENDIF ORB09200
ORB09210
CALL LONPER(LAN,AP,LP) ORB09220
CALL TLON(LAN,AP,TA,TL) ORB09230
CALL PERIOD(A,PER,PI,MU) ORB09240
CALL ECCAN(E,TA,EA,PI) ORB09250
CALL MEANMO(A,MM,MU) ORB09260
CALL MEANAN(EA,E,MA) ORB09270
CALL TFLGHT(MM,MA,TF) ORB09280
RETURN ORB09290
END ORB09300
ORB09310
***** ORB09320
SUBROUTINE ENERGY(V,R,MU,ENR) ORB09330
* THIS SUBROUTINE CALCULATES THE ENERGY OF THE ORBIT ORB09340
ORB09350
DOUBLE PRECISION V,R,MU,ENR ORB09360
ORB09370
ENR = ((V**2)/2) - (MU/R) ORB09380
ORB09390
RETURN ORB09400
END ORB09410
ORB09420
***** ORB09430
ORB09440
SUBROUTINE ANGMOM(RI,RJ,RK,VI,VJ,VK,HI,HJ,HK,H) ORB09450
* THIS SUBROUTINE CALCULATES THE ANGULAR MOMENTUM ORB09460

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DOUBLE PRECISION RI,RJ,RK,VI,VJ,VK,HI,HJ,HK,H	ORB09470
HI = (RJ * VK) - (RK * VJ)	ORB09480
HJ = (RK * VI) - (RI * VK)	ORB09490
HK = (RI * VJ) - (RJ * VI)	ORB09500
H = DSQRT((HI**2) + (HJ**2) + (HK**2))	ORB09510
RETURN	ORB09520
END	ORB09530
*****	ORB09540
*****	ORB09550
*****	ORB09560
*****	ORB09570
*****	ORB09580
*****	ORB09590
* SUBROUTINE NODE(HI,HJ,NI,NJ,NK,N)	ORB09600
THIS SUBROUTINE CALCULATES THE NODE VECTOR	ORB09610
DOUBLE PRECISION HI,HJ,NI,NJ,NK,N	ORB09620
NI = -HJ	ORB09630
NJ = HI	ORB09640
NK = 0.0	ORB09650
N = DSQRT((NI**2) + (NJ**2))	ORB09660
RETURN	ORB09670
END	ORB09680
*****	ORB09690
*****	ORB09700
*****	ORB09710
*****	ORB09720
*****	ORB09730
* SUBROUTINE LATREC(H,P,MU)	ORB09740
THIS SUBROUTINE CALCULATES THE SEMI-LATUS RECTUM	ORB09750
DOUBLE PRECISION H,P,MU	ORB09760
P = (H**2)/MU	ORB09770
RETURN	ORB09780
END	ORB09790
*****	ORB09800
*****	ORB09810
*****	ORB09820
*****	ORB09830
* SUBROUTINE ECC(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,MU)	ORB09840
THIS SUBROUTINE CALCULATES THE ECCENTRICITY	ORB09850
DOUBLE PRECISION RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,MU,DOT	ORB09860
CALCULATE DOT PRODUCT OF 'R' AND 'V' VECTORS	ORB09870
DOT = (RI*VI) + (RJ*VJ) + (RK*VK)	ORB09880
EI = (1.0D+00/MU) * (((V**2) - (MU/R)) * RI - (DOT)*VI)	ORB09890
EJ = (1.0D+00/MU) * (((V**2) - (MU/R)) * RJ - (DOT)*VJ)	ORB09900
EK = (1.0D+00/MU) * (((V**2) - (MU/R)) * RK - (DOT)*VK)	ORB09910
E = DSQRT((EI**2) + (EJ**2) + (EK**2))	ORB09920
RETURN	ORB09930
END	ORB09940
*****	ORB09950
*****	ORB09960
*****	ORB09970
*****	ORB09980
*****	ORB09990
* SUBROUTINE SMAXIS(MU,ENR,A)	ORB10000
THIS SUBROUTINE Calculates THE SEMI-MAJOR AXIS	ORB10010
	ORB10020

```

DOUBLE PRECISION MU,ENR,A
A = -MU/(2*ENR)
RETURN
END
*****

SUBROUTINE INCL(HK,H,I,PI)
* THIS SUBROUTINE CALCULATES THE INCLINATION
* 'I' ALWAYS LESS THAN 180 DEGREES

DOUBLE PRECISION HK,H,I,PI

I = DACOS(HK/H)
RETURN
END
*****

SUBROUTINE ASNODE(NI,N,LAN,NJ,PI)
* THIS SUBROUTINE CALCULATES THE LONGITUDE OF THE ASCENDING NODE
* IF 'NJ' > 0 THEN 'LAN' < 180 DEGREES

DOUBLE PRECISION NI,N,LAN,NJ,PI

LAN = DATAN2(NJ,NI)
IF (LAN .LT. 0.0) THEN
  LAN = (2*PI) + LAN
ENDIF
RETURN
END
*****

SUBROUTINE ARP(NI,NJ,N,EI,EJ,EK,E,AP,PI,NP,NQ,LAN)
* THIS SUBROUTINE CALCULATES THE ARGUMENT OF Perigee
* IF 'EK' GREATER THAN 0 THEN 'AP' < 180
* VARIABLE TEMP USED AS A Temporary VALUE FOR ARCTAN

DOUBLE PRECISION NI,NJ,N,EI,EJ,EK,E,AP,PI,NQ,NP,TEMP,LAN

IF ((EI .EQ. 0.0) .AND. (EJ .EQ. 0.0)) THEN
  AP = 0.0
ELSE
  TEMP = DATAN2(EJ,EI)
  IF (TEMP .GT. LAN) THEN
    AP = TEMP - LAN
  ELSE
    AP = (2*PI) - (LAN - TEMP)
  ENDIF
  IF (AP .LT. 0.0) THEN
    AP = (2*PI) + AP
  ENDIF
  IF (AP .GT. (2*PI)) THEN
    AP = AP - (2*PI)
  ENDIF
ENDIF

```

```

ORB10030
ORB10040
ORB10050
ORB10060
ORB10070
ORB10080
ORB10090
ORB10100
ORB10110
ORB10120
ORB10130
ORB10140
ORB10150
ORB10160
ORB10170
ORB10180
ORB10190
ORB10200
ORB10210
ORB10220
ORB10230
ORB10240
ORB10250
ORB10260
ORB10270
ORB10280
ORB10290
ORB10300
ORB10310
ORB10320
ORB10330
ORB10340
ORB10350
ORB10360
ORB10370
ORB10380
ORB10390
ORB10400
ORB10410
ORB10420
ORB10430
ORB10440
ORB10450
ORB10460
ORB10470
ORB10480
ORB10490
ORB10500
ORB10510
ORB10520
ORB10530
ORB10540
ORB10550
ORB10560
ORB10570
ORB10580

```

ENDIF
ENDIF
RETURN
END

SUBROUTINE TANOM(EI,EJ,EK,E,RI,RJ,RK,RP,RQ,RW,R,VI,VJ,VK,
+ TA,PI)
* THIS SUBROUTINE CALCULATES THE TRUE Anomaly
* IF (R DOT V) > 0 THEN TA < 180 DEGREES

DOUBLE PRECISION DOT,EI,EJ,EK,E,RI,RJ,RK,R,VI,VJ,VK,TA,PI,
+ RP,RQ,RW

TA = DATAN2(RQ,RP)
IF (TA .LT. 0.0) THEN
TA = (2 * PI) + TA
ENDIF
RETURN
END

SUBROUTINE ARLAT(NI,NJ,NK,N,RI,RJ,RK,R,AL,PI,TA,AP)
* THIS SUBROUTINE CALCULATES THE ARGUMENT OF LATITUDE
* IF (RK > 0) THEN AL < 180 DEGREES

DOUBLE PRECISION NI,NJ,NK,N,RI,RJ,RK,R,AL,PI,TA,AP

AL = TA + AP
RETURN
END

SUBROUTINE LONPER(LAN,AP,LP)
* THIS SUBROUTINE CALCULATES THE LONGITUDE OF PERIGEE

DOUBLE PRECISION LAN,AP,LP

LP = LAN + AP
RETURN
END

SUBROUTINE TLON(LAN,AP,TA,TL)
* THIS SUBROUTINE CALCULATES THE TRUE LONGITUDE AT EPOCH

DOUBLE PRECISION LAN,AP,TA,TL

TL = AP + LAN + TA
RETURN
END

ORB10590
ORB10600
ORB10610
ORB10620
ORB10630
ORB10640
ORB10650
ORB10660
ORB10670
ORB10680
ORB10690
ORB10700
ORB10710
ORB10720
ORB10730
ORB10740
ORB10750
ORB10760
ORB10770
ORB10780
ORB10790
ORB10800
ORB10810
ORB10820
ORB10830
ORB10840
ORB10850
ORB10860
ORB10870
ORB10880
ORB10890
ORB10900
ORB10910
ORB10920
ORB10930
ORB10940
ORB10950
ORB10960
ORB10970
ORB10980
ORB10990
ORB11000
ORB11010
ORB11020
ORB11030
ORB11040
ORB11050
ORB11060
ORB11070
ORB11080
ORB11090
ORB11100
ORB11110
ORB11120
ORB11130

```

SUBROUTINE PERIOD(A,PER,PI,MU)
* THIS SUBROUTINE CALCULATES THE PERIOD

DOUBLE PRECISION A,PER,PI,MU

PER = 2.0D+00*(PI)*DSQRT((A**3)/MU)
RETURN
END

```

```

SUBROUTINE ECCAN(E,TA,EA,PI)
* THIS SUBROUTINE CALCULATES THE ECCENTRIC Anomaly

DOUBLE PRECISION E,TA,EA,PI

EA = DACCS((E + DCOS(TA))/(1.0D+00 + E*DCOS(TA)))
IF (TA .GT. PI) THEN
  EA = (2*PI) - EA
ENDIF
RETURN
END

```

```

SUBROUTINE MEANMO(A,MM,MU)
* THIS SUBROUTINE CALCULATES THE MEAN MOTION

DOUBLE PRECISION A,MM,MU

MM = DSQRT(MU/(A**3))
RETURN
END

```

```

SUBROUTINE MEANAN(EA,E,MA)
* THIS SUBROUTINE CALCULATES THE MEAN Anomaly

DOUBLE PRECISION EA,E,MA

MA = EA - E*DSIN(EA)
RETURN
END

```

```

SUBROUTINE TFLGHT(MM,MA,TF)
* THIS SUBROUTINE CALCULATES THE TIME OF FLIGHT

DOUBLE PRECISION MM,MA,TF

TF = (1/MM)*MA

```

ORB11140
ORB11150
ORB11160
ORB11170
ORB11180
ORB11190
ORB11200
ORB11210
ORB11220
ORB11230
ORB11240
ORB11250
ORB11260
ORB11270
ORB11280
ORB11290
ORB11300
ORB11310
ORB11320
ORB11330
ORB11340
ORB11350
ORB11360
ORB11370
ORB11380
ORB11390
ORB11400
ORB11410
ORB11420
ORB11430
ORB11440
ORB11450
ORB11460
ORB11470
ORB11480
ORB11490
ORB11500
ORB11510
ORB11520
ORB11530
ORB11540
ORB11550
ORB11560
ORB11570
ORB11580
ORB11590
ORB11600
ORB11610
ORB11620
ORB11630
ORB11640
ORB11650
ORB11660
ORB11670
ORB11680
ORB11690

RETURN
END

ORB11700
ORB11710
ORB11720
ORB11730
ORB11740
ORB11750
ORB11760
ORB11770
ORB11780
ORB11790
ORB11800
ORB11810
ORB11820
ORB11830
ORB11840
ORB11850
ORB11860
ORB11870
ORB11880
ORB11890
ORB11900
ORB11910
ORB11920
ORB11930
ORB11940
ORB11950
ORB11960
ORB11970
ORB11980
ORB11990
ORB12000
ORB12010
ORB12020
ORB12030
ORB12040
ORB12050
ORB12060
ORB12070
ORB12080
ORB12090
ORB12100
ORB12110
ORB12120
ORB12130
ORB12140
ORB12150
ORB12160
ORB12170
ORB12180
ORB12190
ORB12200
ORB12210
ORB12220
ORB12230
ORB12240
ORB12250

* CALCULATE UNPERTURBED ORBIT

SUBROUTINE UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,
+ VI,VJ,VK,V,MU,PI,H,A,E,N,TA,P,MM,MA,EA,
+ TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,TARAY,AINRAY,APRAY,TIMRAY,
+ TT)

* THIS SUBROUTINE CALCULATE THE UNPERTURBED ORBIT

* THIS SUBROUTINE CALLS THE FOLLOWING SUBROUTINES:

* NEWELT = CALCULATE NEW ELEMENTS AFTER TIME STEP

* NEWPOS = CALCULATE NEW POSITION AFTER TIME STEP

* NEWVEL = CALCULATE NEW VELOCITY AFTER TIME STEP

* STORE = STORES POSITION IN ARRAYS

DOUBLE PRECISION T,DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,
+ MU,PI,H,A,E,N,TA,P,MM,MA,EA,TF,TT

DIMENSION RARAY(500),TARAY(500),RIRAY(500),RJRAY(500),
+ RKRAY(500),AINRAY(500),APRAY(500),TIMRAY(500)

* SET TRUE ANOMALY TO NEGATIVE SO LOOP CAN BE EXECUTED

IF (TA .GT. 6.21) THEN

TA = TA - (2*PI)

ENDIF

* CONTINUE AROUND ORBIT TILL CLOSE TO PERIGEE

230 IF ((TA .LE. 6.21) .AND. (T .LE. PER)) THEN

* INCREMENT TRUE TIME

TT = TT + DT

CALL NEWELT(MM,MA,E,EA,TA,TF,DT,PI,PER)

CALL NPOS(RI,RJ,RK,R,LAN,AP,I,TA,A,E)

CALL NVEL(E,P,TA,LAN,AP,I,VI,VJ,VK,V,MU)

* INCREMENT STEP COUNTER AND STORE VALUES

NUM = NUM + 1

+ CALL STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,
+ RARAY,TARAY,NUM,I,AP,AINRAY,APRAY,
+ TT,TIMRAY)

* INCREMENT TIME STEP COUNTER

T = T + DT

GOTO 230

ENDIF

RETURN

END

* CALCULATE THE UNPERTURBED NEW ELEMENTS

```

SUBROUTINE NEWELT(MM,MA,E,EA,TA,TF,DT,PI,PER)
* THIS SUBROUTINE CALCULATES THE Unperturbed NEW ELEMENTS
*
* THIS SUBROUTINE CALLS THE FOLLOWING SUBROUTINES:
* NEA = NEW ECCENTRIC ANOMALY
* NTA = NEW TRUE ANOMALY
*
DOUBLE PRECISION MM,MA,E,EA,TA,TF,DT,PI,PER
*
* Increment TIME OF FLIGHT AND CHECK IF TF GREATER THAN PERIOD
TF = TF + DT
IF (TF .GT. PER) THEN
    TF = TF - PER
ENDIF
*
* CALCULATE MEAN ANOMALY AND USE TO FIND ECCENTRIC Anomaly THEN NEW
* TRUE ANOMALY
MA = MM*(TF)
CALL NEA(MA,E,EA)
CALL NTA(EA,E,TA,PI)
RETURN
END
*****
* CALCULATE PERTURBED ORBIT
*****
SUBROUTINE PRETUR(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,
+ VI,VJ,VK,V,FR,FS,FW,MU,PI,H,A,E,N,TA,P,MM,MA,EA,
+ TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,TARAY,AINRAY,APRAY,TIMRAY,
+ TF,TFEA,TFSU,TFMO,TFDRA,TDI,TDA,TDE,TDMM,TDMA,TDLAN,TDH,TDAP)
* THIS SUBROUTINE CALCULATES THE PERTURBED ORBIT.
*
* THIS SUBROUTINE CALLS THE FOLLOWING SUBROUTINES:
* TFORCE = CALCULATE THE TOTAL PERTURBING FORCE ON THE SATELLITE
* PNEWEL = CALCULATE THE Perturbed NEW ELEMENTS
* NPOS = NEW POSITION AFTER TIME STEP
* NVEL = NEW VELOCITY AFTER TIME STEP
* PERIOD = PERIOD OF PERTURBED ORBIT
* STORE = STORE POSITION AND ELEMENTS IN ARRAYS FOR PLOTTING
*
DOUBLE PRECISION T,DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,
+ FR,FS,FW,MU,PI,H,A,E,N,TA,P,MM,MA,EA,TF,TT,
+ DI,DA,DE,DMM,DMA,DLAN,DH,DAP,EI,EJ,EK,HI,HJ,LP,M,
+ DVR,DVS,DVW,DVI,DVJ,DVK
*
DIMENSION RARAY(500),TARAY(500),RIRAY(500),RJRAY(500),
+ RKRAY(500),AINRAY(500),APRAY(500),TIMRAY(500)
*
* SET MEAN RADIUS OF EARTH
RE = 6400.0
*
DT = PER/50
T = DT
IF (TA .GT. 6.21) THEN
    TA = TA - (2*PI)

```

```

ORB12260
ORB12270
ORB12280
ORB12290
ORB12300
ORB12310
ORB12320
ORB12330
ORB12340
ORB12350
ORB12360
ORB12370
ORB12380
ORB12390
ORB12400
ORB12410
ORB12420
ORB12430
ORB12440
ORB12450
ORB12460
ORB12470
ORB12480
ORB12490
ORB12500
ORB12510
ORB12520
ORB12530
ORB12540
ORB12550
ORB12560
ORB12570
ORB12580
ORB12590
ORB12600
ORB12610
ORB12620
ORB12630
ORB12640
ORB12650
ORB12660
ORB12670
ORB12680
ORB12690
ORB12700
ORB12710
ORB12720
ORB12730
ORB12740
ORB12750
ORB12760
ORB12770
ORB12780
ORB12790
ORB12800
ORB12810

```

ENDIF	ORB12820
IF (TF .GE. PER) THEN	ORB12830
TF = TF - PER	ORB12840
ENDIF	ORB12850
* CONTINUE Around ORBIT FOR ONE PERIOD	ORB12860
240 IF ((TF .LT. PER) .AND. (T .LT. PER)) THEN	ORB12870
	ORB12880
	ORB12890
* INCREMENT TRUE TIME	ORB12900
TT = TT + DT	ORB12910
CALL TFORCE(AL, LAN, AP, I, RI, RJ, RK, R, VI, VJ, VK, V,	ORB12920
+ TT, FR, FS, FW, MU, PI,	ORB12930
+ FEA, FSU, FMO, FDRA, FOR,	ORB12940
+ EI, EJ, EK, E, A, T, LP, TA, PER, EA, MA, TF, P,	ORB12950
+ MM, N, H, HI, HJ, DT)	ORB12960
CALL PNEWEL(FR, FS, FW, H, R, A, E, N, TA, DT, I, LAN, AL,	ORB12970
+ AP, P, MM, MA, EA, TF, T, MU, PI,	ORB12980
+ DI, DA, DE, DMM, DMA, DLAN, DH, DAP)	ORB12990
CALL NPOS(RI, RJ, RK, R, LAN, AP, I, TA, A, E)	ORB13000
CALL NVEL(E, P, TA, LAN, AP, I, VI, VJ, VK, V, MU)	ORB13010
	ORB13020
* CALCULATE NEW PERIOD AND RESET TIME STEP AND TIME COUNTER	ORB13030
* IF NOT AT END OF ORBIT	ORB13040
IF (T .LT. (PER-DT)) THEN	ORB13050
CALL PERIOD(A, PER, PI, NU)	ORB13060
DT = PER/50	ORB13070
T = TF	ORB13080
ENDIF	ORB13090
	ORB13100
* INCREMENT STEP COUNTER	ORB13110
NUM = NUM + 1	ORB13120
241 CALL STORE(RI, RJ, RK, R, TA, RIRAY, RJRAY, RKRAY,	ORB13130
+ RARAY, TARAY, NUM, I, AP, AINRAY, APRAY,	ORB13140
+ TT, TIMRAY)	ORB13150
	ORB13160
* TOTAL ELEMENT CHANGES	ORB13170
TDI = TDI + SNGL(ABS(DI))	ORB13180
TDA = TDA + SNGL(ABS(DA))	ORB13190
TDE = TDE + SNGL(ABS(DE))	ORB13200
TDMM = TDMM + SNGL(ABS(DMM))	ORB13210
TDMA = TDMA + SNGL(ABS(DMA))	ORB13220
TDLAN = TDLAN + SNGL(ABS(DLAN))	ORB13230
TDH = TDH + SNGL(ABS(DH))	ORB13240
TDAP = TDAP + SNGL(ABS(DAP))	ORB13250
TFEA = TFEA + FEA	ORB13260
TFSU = TFSU + FSU	ORB13270
TFMO = TFMO + FMO	ORB13280
TFDRA = TFDRA + FDRA	ORB13290
	ORB13300
* CHECK FOR IMPACT	ORB13310
IF (R .LE. RE) THEN	ORB13320
PRINT*, 'SATELLITE WILL IMPACT THE EARTH!!'	ORB13330
T = PER	ORB13340
ENDIF	ORB13350
	ORB13360
* INCREMENT TIME COUNTER	ORB13370

```

T = T + DT
GOTO 240
ENDIF
RETURN
END

```

```

ORB13380
ORB13390
ORB13400
ORB13410
ORB13420
ORB13430
ORB13440
ORB13450
ORB13460
ORB13470
ORB13480
ORB13490
ORB13500
ORB13510
ORB13520
ORB13530
ORB13540
ORB13550
ORB13560
ORB13570
ORB13580
ORB13590
ORB13600
ORB13610
ORB13620
ORB13630
ORB13640
ORB13650
ORB13660
ORB13670
ORB13680
ORB13690
ORB13700
ORB13710
ORB13720
ORB13730
ORB13740
ORB13750
ORB13760
ORB13770
ORB13780
ORB13790
ORB13800
ORB13810
ORB13820
ORB13830
ORB13840
ORB13850
ORB13860
ORB13870
ORB13880
ORB13890
ORB13900
ORB13910
ORB13920
ORB13930

```

```

*****
* CALCULATE THE PERTURBING FORCES
*****

```

```

SUBROUTINE TFORCE(AL, LAN, AP, I, RI, RJ, RK, R, VI, VJ, VK, V, TT,
+ FR, FS, FW, MU, PI, FEA, FSU, FMO, FDRA, FOR,
+ EI, EJ, EK, E, A, T, LP, TA, PER, EA, MA, TF, P,
+ MM, N, H, HI, HJ, DT)
* THIS SUBROUTINE SUMS ALL THE PERTURBING FORCES FOR THE TOTAL
* PERTURBING FORCE.

```

```

* THE FOLLOWING SUBROUTINES WERE CALLED:
* OBERT = OBLATENESS OF THE EARTH
* FSUN = GRAVITATIONAL Attraction OF THE SUN
* FMOON = GRAVITATIONAL Attraction OF THE MOON
* FDRAG = DRAG FORCES

```

```

DOUBLE PRECISION FER, FES, FEW, FSR, FSS, FSW, FMR, FMS, FMW, MU, PI,
+ FDR, FDS, FDW, FR, FS, FW, RI, RJ, RK, R, AL, I, TT, LAN, AP, VI, VJ, VK, V,
+ EI, EJ, EK, E, A, T, LP, TA, PER, EA, MA, TF, P,
+ MM, N, H, HI, HJ, DT

```

```

CALL OBEART(RI, RJ, RK, R, AL, I, FER, FES, FEW, MU)
CALL FSUN(TT, RI, RJ, RK, R, FSR, FSS, FSW, PI)
CALL FMOON(TT, RI, RJ, RK, R, FMR, FMS, FMW, PI)
CALL FDRAG(RI, RJ, RK, R, VI, VJ, VK, V, LAN, AP, I, FDR, FDS, FDW,
+ EI, EJ, EK, E, A, T, LP, TA, PER, EA, MA, AL, TF, P, PI, MU,
+ MM, N, H, HI, HJ, DT)

```

```

* SUM VECTOR FORCES
FR = FER + FSR + FMR + FDR
FS = FES + FSS + FMS + FDS
FW = FEW + FSW + FMW + FDW

```

```

* CALCULATE TOTAL FORCE FROM EACH, AND TOTAL OF ALL
FEA = SNGL(SQRT((FER**2)+(FES**2)+(FEW**2)))
FSU = SNGL(SQRT((FSR**2)+(FSS**2)+(FSW**2)))
FMO = SNGL(SQRT((FMR**2)+(FMS**2)+(FMW**2)))
FDRA = SNGL(SQRT((FDR**2)+(FDS**2)+(FDW**2)))
FOR = SNGL(SQRT((FR**2)+(FS**2)+(FW**2)))

```

```

RETURN
END

```

```

*****

```

```

SUBROUTINE OBEART(RI, RJ, RK, R, AL, I, FER, FES, FEW, MU)
* THIS SUBROUTINE CALCULATES THE PERTURBING FORCE DUE TO THE
* OBLIQUENESS OF THE EARTH.

```


DOUBLE PRECISION J2,RE,FER,FES,FEW,RI,RJ,SK,R,AL,I,MU,M

J2 = 1.082364D-03
RE = 6.3782E+03

FER = ((-3.0D+00*MU*J2*(RE**2))/(2.0D+00*(R**4)))
+ (1.0D+00 - (3.0D+00*((DSIN(I))**2) * ((DSIN(AL))**2)))
FES = ((-3.0D+00*MU*J2*(RE**2))/(R**4))
+ (((DSIN(I))**2)*(DSIN(AL))*(DCOS(AL)))
FEW = ((-3.0D+00*MU*J2*(RE**2))/(R**4))
+ (DSIN(I)*DCOS(I)*DSIN(AL))
RETURN
END

SUBROUTINE FSUN(TT,RI,RJ,RK,R,FSR,FSS,FSW,PI)
* THIS SUBROUTINE CALCULATES THE PERTURBING FORCE DUE TO THE SUN

* THE FOLLOWING SUBROUTINES ARE CALLED:
* SUNPOS = SUNS POSITION ORBITING AROUND EARTH
* HEVBOD = PERTURBING FORCE FROM A Heavenly BODY

DOUBLE PRECISION FSR,FSS,FSW,PI,
+ RSI,RSJ,RSK,SLAN,SI,SAL,SMU,TT,RI,RJ,RK,R,RS

* SUNS GRAVITATIONAL PARAMETER
SMC = 1.3271544D+11
CALL SUNPOS(TT,RSI,RSJ,RSK,RS,SLAN,SI,SAL,PI)
CALL HEVBOD(RI,RJ,RK,R,RSI,RSJ,RSK,RS,SLAN,SAL,SI,SMU,FSR,FSS,FSW)
RETURN
END

SUBROUTINE FMOON(TT,RI,RJ,RK,R,FMR,FMS,FMW,PI)
* THIS SUBROUTINE CALCULATES THE PERTURBING FORCE DUE TO The MOON

* THE FOLLOWING SUBROUTINE ARE CALLED:
* MONPOS = MOONS POSITION ORBITING AROUND THE EARTH
* HEVBOD = PERTURBING FORCE FROM A HEAVENLY BODY

DOUBLE PRECISION FMR,FMS,FMW,RMI,RMJ,RMK,MLAN,MI,MAL,MMU,
+ TT,RI,RJ,RK,R,PM,PI

* MOONS GRAVITATIONAL PARAMETER
MMU = 4.90287D+03
CALL MONPOS(TT,RMI,RMJ,RMK,PM,MLAN,MI,MAL,PI)
CALL HEVBOD(RI,RJ,RK,R,RMI,RMJ,RMK,PM,MLAN,MAL,MI,MMU,FMR,FMS,FMW)
RETURN
END

SUBROUTINE HEVBOD(RI,RJ,RK,R,RPI,RPJ,RPK,RP,LAN,AL,INC,NUP,

ORB13940
ORB13950
ORB13960
ORB13970
ORB13980
ORB13990
ORB14000
ORB14010
ORB14020
ORB14030
ORB14040
ORB14050
ORB14060
ORB14070
ORB14080
ORB14090
ORB14100
ORB14110
ORB14120
ORB14130
ORB14140
ORB14150
ORB14160
ORB14170
ORB14180
ORB14190
ORB14200
ORB14210
ORB14220
ORB14230
ORB14240
ORB14250
ORB14260
ORB14270
ORB14280
ORB14290
ORB14300
ORB14310
ORB14320
ORB14330
ORB14340
ORB14350
ORB14360
ORB14370
ORB14380
ORB14390
ORB14400
ORB14410
ORB14420
ORB14430
ORB14440
ORB14450
ORB14460
ORB14470
ORB14480
ORB14490

```

+   FHR,FHS,FHW)
*   THIS SUBROUTINE CALCULATES THE PERTURBING FORCE DUE TO A
*   HEAVENLY BODY.
*   THE FOLLOWING SUBROUTINE WAS CALLED:
*   IJKRSW = 'IJK' SYSTEM TO THE 'RSW' SYSTEM
      DOUBLE PRECISION DOT,FHI,FHJ,FHK,RI,RJ,RK,R,RPI,RPJ,RPK,RP,
+   LAN,AL,INC,MUP,I,J,K,IP,JP,KP,M,FHR,FHS,FHW
*   CALCULATE UNIT VECTOR FOR SATELLITE AND PERTURBING BODIES POSITION
      I = RI/R
      J = RJ/R
      K = RK/R
      IP = RPI/RP
      JP = RPJ/RP
      KP = RPK/RP
*   CALCULATE DOT PRODUCT OF UNIT VECTORS
      DOT = (( I*IP )+( J*JP )+( K*KP ))
*   CALCULATE FORCES IN THE 'IJK' SYSTEM
      FHI = (MUP/(RP**2))*(K/RP)*(3.0D+00*DOT*(IP)-(I))
      FHJ = (MUP/(RP**2))*(R/RP)*(3.0D+00*DOT*(JP)-(J))
      FHK = (MUP/(RP**2))*(R/RP)*(3.0D+00*DOT*(KP)-(K))
*   Transform FORCES TO THE RSW SYSTEM
      CALL IJKRSW(LAN,AL,INC,FHI,FHJ,FHK,FHR,FHS,FHW)
      RETURN
      END
*****
      SUBROUTINE SUNPOS(TT,RSI,RSJ,RSK,RS,SLAN,SI,SAL,PI)
*   THIS SUBROUTINE CALCULATES THE SUNS POSITION
*   VARIABLES USED TO DESCRIBE THE SUNS ORBIT:
*   SI = SUNS INCLINATION
*   SLAN= SUNS Longitude OF ASCENDING NODE
*   SAP = SUNS ARGUMENT OF PERIGEE
*   RS = SUNS ORBITAL RADIUS
*   STA = SUNS TRUE ANOMALY
*   SAL = SUNS ARGUMENT OF LONGITUDE
      DOUBLE PRECISION SLAN,SI,SAL,RS,STA,SAP,TT,RSI,RSK,
+   RSJ,RSP,RSQ,RSW,PI
      SI = 4.09279709D-01
      SLAN = 0.0D+00
      SAP = 0.0D+00
      RS = 1.4959965D+08
      STA = ((2.0*PI)/(365.0 * 86400.0) * TT)
      SAL = STA + SAP
*   CALCULATE SUNS POSITION IN 'PQW' SYSTEM
      RSP = RS*DCOS(STA)

```

```

ORB14500
ORB14510
ORB14520
ORB14530
ORB14540
ORB14550
ORB14560
ORB14570
ORB14580
ORB14590
ORB14600
ORB14610
ORB14620
ORB14630
ORB14640
ORB14650
ORB14660
ORB14670
ORB14680
ORB14690
ORB14700
ORB14710
ORB14720
ORB14730
ORB14740
ORB14750
ORB14760
ORB14770
ORB14780
ORB14790
ORB14800
ORB14810
ORB14820
ORB14830
ORB14840
ORB14850
ORB14860
ORB14870
ORB14880
ORB14890
ORB14900
ORB14910
ORB14920
ORB14930
ORB14940
ORB14950
ORB14960
ORB14970
ORB14980
ORB14990
ORB15000
ORB15010
ORB15020
ORB15030
ORB15040
ORB15050

```

```

RSQ = RS*DSIN(STA)
RSW = 0.0D+00
* TRANSFORM POSITION TO 'IJK' SYSTEM
CALL PQWIJK(SLAN,SAP,SI,RSP,RSQ,RSW,RSI,RSJ,RSK)
RETURN
END
*****
SUBROUTINE MONPOS(TT,RMI,RMJ,RMK,RM,MLAN,MI,MAL,PI)
* THIS SUBROUTINE CALCULATES THE MOONS POSITION
* VARIABLES USED TO DESCRIBE THE SUNS ORBIT:
* MI = MOONS INCLINATION
* MLAN = MOONS Longitude OF ASCENDING NODE
* MAP = MOONS ARGUMENT OF PERIGEE
* RM = MOONS ORBITAL RADIUS
* MTA = MOONS TRUE ANOMALY
* MAL = MOONS ARGUMENT OF LONGITUDE
DOUBLE PRECISION MLAN,MAL,RM,TM,MTA,RMP,RMQ,RMW,
+ RMI,RMJ,RMK,PI
MI = 4.99164166D-01
RM = 3.844D+05
MLAN = 0.0
MTA = ((2.0*PI)/(27.3 * 3600) * TT)
MAP = 0.0D+00
MAL = MTA
* CALCULATE MOON POSITION IN 'PQW' SYSTEM
RMP = RM*DCOS(MTA)
RMQ = RM*DSIN(MTA)
RMW = 0
* TRANSFORM POSITION TO 'IJK' SYSTEM
CALL PQWIJK(MLAN,MAP,MI,RMP,RMQ,RMW,RMI,RMJ,RMK)
RETURN
END
*****
SUBROUTINE FDRAG(RI,RJ,RK,R,VI,VJ,VK,V,LAN,AP,I,FDR,FDS,FDW,
+ EI,EJ,EK,E,A,T,LP,TA,PER,EA,MA,AL,TF,P,PI,MU,
+ MM,N,H,HI,HJ,DT)
* THIS SUBROUTINE CALCULATES THE PERTURBING FORCE DUE TO DRAG
* THE FOLLOWING VARIABLES ARE USED TO MODEL THE ATMOSPHERE:
* RE = RADIUS OF EARTH
* M = MASS OF SATELLITE
* AR = FRONTAL SURFACE AREA OF SATELLITE
* Z = ALTITUDE OF SATELLITE
* K = EXPONENTIAL DECAY FACTOR
* DENO = NORMAL DENSITY
* CD = COEFFICIENT OF DRAG

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```

ORB15060
ORB15070
ORB15080
ORB15090
ORB15100
ORB15110
ORB15120
ORB15130
ORB15140
ORB15150
ORB15160
ORB15170
ORB15180
ORB15190
ORB15200
ORB15210
ORB15220
ORB15230
ORB15240
ORB15250
ORB15260
ORB15270
ORB15280
ORB15290
ORB15300
ORB15310
ORB15320
ORB15330
ORB15340
ORB15350
ORB15360
ORB15370
ORB15380
ORB15390
ORB15400
ORB15410
ORB15420
ORB15430
ORB15440
ORB15450
ORB15460
ORB15470
ORB15480
ORB15490
ORB15500
ORB15510
ORB15520
ORB15530
ORB15540
ORB15550
ORB15560
ORB15570
ORB15580
ORB15590
ORB15600
ORB15610

```

```

+
+
+
+
DOUBLE PRECISION  MAG,M,K,FDR,FDS,FDW,RE,AR,Z,DENO,CD,DEN,
FDJ,FDK,FDI,RI,RJ,RK,VI,VJ,VK,V,LAN,AP,I,R,
EI,EJ,EN,E,A,T,LP,TA,PER,EA,MA,AL,TF,P,PI,MU,
MM,N,H,HI,HJ,DT,DVR,DVS,DW,DVI,DVJ,DVK
ORB15620
ORB15630
ORB15640
ORB15650
ORB15660
ORB15670
ORB15680
ORB15690
ORB15700
ORB15710
ORB15720
ORB15730
ORB15740
ORB15750
ORB15760
ORB15770
ORB15780
ORB15790
ORB15800
ORB15810
ORB15820
ORB15830
ORB15840
ORB15850
ORB15860
ORB15870
ORB15880
ORB15890
ORB15900
ORB15910
ORB15920
ORB15930
ORB15940
ORB15950
ORB15960
ORB15970
ORB15980
ORB15990
ORB16000
ORB16010
ORB16020
ORB16030
ORB16040
ORB16050
ORB16060
ORB16070
ORB16080
ORB16090
ORB16100
ORB16110
ORB16120
ORB16130
ORB16140
ORB16150
ORB16160
ORB16170

RE = 6.378145D+03
M = 1.0D+02
AR = 2.0D+01
Z = R - RE

*
*   DEPENDING ON ALTITUDE SET ATMOSPHERE VARIABLES
*   IF (Z. LE. 1.5D+02) THEN
*       K = 4.74D-02
*       DENO = 1.225D+00
*       CD = 1.0D+00
*   ELSEIF (Z. LE. 5.5D+02) THEN
*       K = 3.4614D-02
*       DENO = 1.79846D-01
*       CD = 2.0D+00
*   ELSE
*       K = 2.21698D-3
*       DENO = 1.015484D-07
*       CD = 2.0D+00
*   ENDIF

*
*   CALCULATE ATMOSPHERIC DENSITY
*   DEN = DENO * DEXP(-K*Z)

*
*   CALCULATE MAGNITUDE OF DRAG FORCE AND LIMIT IT TO 1.0E-20
*   MAG = -(0.5D+00)*CD*AR*DEN*V*(1.0D-03)/M
*   IF (ABS(MAG) .LT. 1.0D-20) THEN
*       MAG = -1.0D-20
*   ENDIF

*
*   GIVE DRAG FORCE A Direction OF MINUS THE VELOCITY
*   FDR = 0.0
*   FDS = MAG * V
*   FDW = 0.0
*   RETURN
*   END

*****
* CALCULATE PERTURBED NEW ELEMENTS
*****

SUBROUTINE PNEWEL(FR,FS,FW,H,R,A,E,N,TA,DT,I,LAN,AL,AP,P,
+ MM,MA,EA,TF,T,MU,PI,DI,DA,DE,DMN,DMA,DLAN,DH,DAP)
* THIS SUBROUTINE CALCULATES THE NEW ELEMENTS FROM THE PREVIOUS
* ELEMENTS ADDED TO THE RATES OF CHANGE FOR ONE STEP

*
* THE FOLLOWING SUBROUTINES ARE CALLED:
* RATE = CALCULATES RATES OF CHANGE OF ORBITAL ELEMENTS
* NANGMO = NEW ANGULAR MOMENTUM (NEWH)
* NSMA = NEW SEMI-MAJOR AXIS (NEWA)
* NECC = NEW ECCENTRICITY (NEWEC)

```

★	NINCL = NEW INCLINATION (NEWI)	ORB16180
★	NASNOD = NEW LONGITUDE OF ASCENDING NODE (NEWLAN)	ORB16190
★	NARPER = NEW ARGUMENT OF PERIGEE (NEWAP)	ORB16200
★	NINMO = NEW MEAN MOTION (NEWMM)	ORB16210
★	MEANMO = MEAN MOTION (MM)	ORB16220
★	NNMAN = NEW MEAN ANOMALY (NEWMA)	ORB16230
★	NEA = NEW ECCENTRIC ANOMALY (EA)	ORB16240
★	NTA = NEW TRUE ANOMALY (TA)	ORB16250
★	TFLGHT = TIME OF FLIGHT (TF)	ORB16260
		ORB16270
	DOUBLE PRECISION FR,FS,FW,DMM,H,R,A,E,N,TA,DT,I,LAN,AL,AP,P,	ORB16280
+	MM,MA,EA,TF,T,MU,PI,DA,DH,DE,DI,DLAN,DAP,DMA,	ORB16290
+	NEWH,NEWA,NEWE,NEWI,NEWLAN,NEWAP,NEWMM	ORB16300
		ORB16310
★	INCREMENT TIME OF FLIGHT BY ONE TIME STEP AND CALCULATE RATES	ORB16320
	TF = TF + DT	ORB16330
	CALL RATES(DH,DA,DE,DI,DLAN,DAP,DMM,DMA,E,MM,R,A,FR,FS,FW,	ORB16340
+	TA,AL,H,P,T,MU,I)	ORB16350
		ORB16360
★	CALCULATE NEW ELEMENTS	ORB16370
	CALL NANGMO(H,DT,DH,NEWH)	ORB16380
	CALL NSMA(A,DT,DA,NEWA)	ORB16390
	CALL NECC(E,DT,DE,NEWE)	ORB16400
	CALL NINCL(I,DT,DI,NEWI)	ORB16410
	CALL NASNOD(LAN,DT,DLAN,NEWLAN)	ORB16420
	CALL NARPER(AP,DT,DAP,NEWAP)	ORB16430
		ORB16440
★	SET ELEMENTS TO NEW ELEMENTS	ORB16450
	A = NEWA	ORB16460
	E = NEWE	ORB16470
	I = NEWI	ORB16480
	LAN = NEWLAN	ORB16490
	AP = NEWAP	ORB16500
	P = A * (1 - E**2)	ORB16510
		ORB16520
★	MOVE THE SATELLITE ONE TIME STEP	ORB16530
	CALL MEANMO(A,MM,MU)	ORB16540
	CALL NNMAN(MA,MM,DT,TF,DMA,PI)	ORB16550
	CALL NEA(MA,E,EA)	ORB16560
	CALL NTA(EA,E,TA,PI)	ORB16570
	CALL TFLGHT(NM,MA,TF)	ORB16580
	AL = TA + AP	ORB16590
	RETURN	ORB16600
	END	ORB16610
		ORB16620
	*****	ORB16630
★	CALCULATE THE RATES OF CHANGE OF THE ORBITAL Elements	ORB16640
	*****	ORB16650
		ORB16660
	SUBROUTINE RATES(DH,DA,DE,DI,DLAN,DAP,DMM,DMA,E,MM,R,A,FR,FS,FW,	ORB16670
+	TA,AL,H,P,T,MU,I)	ORB16680
★	THIS SUBROUTINE CALLS THE FOLLOWING SUBROUTINES TO CALCULATE THE	ORB16690
★	TIME RATE-OF- CHANGE OF THE ORBITAL ELEMENTS:	ORB16700
★	RSMAX = RATE-OF-CHANGE OF THE SEMI-MAJOR AXIS (DA)	ORB16710
★	RECC = RATE-OF-CHANGE OF THE ECCENTRICITY (DE)	ORB16720
★	RINC = RATE-OF-CHANGE OF THE INCLINATION (DI)	ORB16730

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* RLAN = RATE-OF-CHANGE OF THE Longitude OF THE ASCENDING NODE ORB16740
* (DLAN) ORB16750
* RAP = RATE-OF-CHANGE OF THE ARGUMENT OF PERIGEE (DAP) ORB16760
* RMM = RATE-OF-Change OF THE MEAN MOTION (DMM) ORB16770
* RMA = RATE-OF-CHANGE OF THE MEAN ANOMALY (DMA) ORB16780
* RANGMO = RATE-OF-CHANGE OF THE ANGULAR MOMENTUM (DH) ORB16790
ORB16800
DOUBLE PRECISION DH,DA,DE,DI,DLAN,DAP,DMM,DMA,E,MM,R,A,FR,FS,FW, ORB16810
+ TA,AL,H,P,T,MU,I ORB16820
ORB16830
CALL RSMAN(E,MM,R,A,FR,FS,DA,TA) ORB16840
CALL RECC(E,MM,R,A,FR,FS,TA,DE) ORB16850
CALL RINC(E,MM,R,A,FW,AL,DI) ORB16860
CALL RLAN(E,MM,R,A,I,FW,AL,DLAN) ORB16870
CALL RAP(E,MM,R,A,I,H,P,AL,TA,FR,FS,FW,DAP) ORB16880
CALL RMM(MM,A,DMM,DA,MU) ORB16890
CALL RMA(E,MM,R,A,TA,DMM,FR,FS,DMA,T) ORB16900
CALL RANGMO(R,FS,FW,DH) ORB16910
RETURN ORB16920
END ORB16930
ORB16940
***** ORB16950
ORB16960
SUBROUTINE RANGMO(R,FS,FW,DH) ORB16970
* THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE ORB16980
* ANGULAR MOMENTUM ORB16990
DOUBLE PRECISION FS,FW,DHW,DHS,DH,R ORB17000
ORB17010
DHW = R * FS ORB17020
DHS = R * FW ORB17030
DH = DSQRT((DHW**2) + (DHS**2)) ORB17040
RETURN ORB17050
END ORB17060
ORB17070
***** ORB17080
ORB17090
SUBROUTINE RSMAN(E,MM,R,A,FR,FS,DA,TA) ORB17100
* THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE SEMI-MAJOR ORB17110
* AXIS ORB17120
DOUBLE PRECISION DA,FR,FS,E,MM,R,A,TA,ET ORB17130
ORB17140
* TRAP (E) SO DENOMINATOR DOES NOT GOTO ZERO ORB17150
IF (E.GT.0.9) THEN ORB17160
ET = 0.9 ORB17170
ELSE ORB17180
ET = E ORB17190
ENDIF ORB17200
DA = ((2.0D+00*E *DSIN(TA))/(MM *DSQRT(1.0D+00-(ET**2))))*FR + ORB17210
+ ((2.0D+00*A*DSQRT(1.0D+00-(E **2)))/(MM *R))*FS ORB17220
RETURN ORB17230
END ORB17240
ORB17250
***** ORB17260
ORB17270
ORB17280
ORB17290

```

<pre> SUBROUTINE RECC(E,MM,R,A,FR,FS,TA,DE) THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE ECCENTRICITY DOUBLE PRECISION DE,FR,FS,E,MM,R,A,TA,ET TRAP (E) SO DENOMINATOR DOES NOT GOTO ZERO IF (E.LT.0.1) THEN ET = 0.1 ELSE ET = E ENDIF DE = ((DSQRT(1.0D+00 - (E **2))*SIN(TA))/(MM *A))*FR + + ((DSQRT(1.0D+00 - (E **2)))/(MM *ET*(A**2)))* + ((A**2)*(1.0D+00 - (E **2))/(R) - (R))*FS RETURN END </pre>	<pre> ORB17300 ORB17310 ORB17320 ORB17330 ORB17340 ORB17350 ORB17360 ORB17370 ORB17380 ORB17390 ORB17400 ORB17410 ORB17420 ORB17430 ORB17440 ORB17450 ORB17460 ORB17470 ORB17480 ORB17490 ORB17500 ORB17510 ORB17520 ORB17530 ORB17540 ORB17550 ORB17560 ORB17570 ORB17580 ORB17590 ORB17600 ORB17610 ORB17620 ORB17630 ORB17640 ORB17650 ORB17660 ORB17670 ORB17680 ORB17690 ORB17700 ORB17710 ORB17720 ORB17730 ORB17740 ORB17750 ORB17760 ORB17770 ORB17780 ORB17790 ORB17800 ORB17810 ORB17820 ORB17830 ORB17840 ORB17850 </pre>
<pre> ***** </pre>	
<pre> SUBROUTINE RLAN(E,MM,R,A,I,FW,AL,DLAN) THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE LONGITUDE OF THE ASCENDING NODE DOUBLE PRECISION DLAN,FW,E,MM,R,A,I,AL,ET,IT TRAP (E) AND (I) SO DENOMINATOR DOES NOT GOTO ZERO IF (E.GT.0.9) THEN ET = 0.9 ELSE ET = E ENDIF IF (I.LT.0.01745) THEN IT = 0.01745 ELSE IT = I ENDIF DLAN = (R*FW*DSIN(AL))/(MM *(A**2)*DSQRT(1.0D+00 - (ET**2))* + DSIN(IT)) RETURN END </pre>	<pre> ORB17470 ORB17480 ORB17490 ORB17500 ORB17510 ORB17520 ORB17530 ORB17540 ORB17550 ORB17560 ORB17570 ORB17580 ORB17590 ORB17600 ORB17610 ORB17620 ORB17630 ORB17640 ORB17650 ORB17660 ORB17670 ORB17680 ORB17690 ORB17700 ORB17710 ORB17720 ORB17730 ORB17740 ORB17750 ORB17760 ORB17770 ORB17780 ORB17790 ORB17800 ORB17810 ORB17820 ORB17830 ORB17840 ORB17850 </pre>
<pre> ***** </pre>	
<pre> SUBROUTINE RAP(E,MM,R,A,I,H,P,AL,TA,FR,FS,FW,DAP) THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE ARGUMENT OF PERIGEE DOUBLE PRECISION DAPR,DAPS,DAPW,DAP,FR,FS,FW,E,MM,R,I,H,P,AL,TA, + ET,A,IT TRAP (E) AND (I) SO DENOMINATOR DOES NOT GOTO ZERO IF (I.LT.0.01745) THEN IT = 0.01745 ELSE IT = I ENDIF </pre>	<pre> ORB17710 ORB17720 ORB17730 ORB17740 ORB17750 ORB17760 ORB17770 ORB17780 ORB17790 ORB17800 ORB17810 ORB17820 ORB17830 ORB17840 ORB17850 </pre>

```

IF (E.GT.0.9) THEN
  ET = 0.9
ELSEIF (E.LT.0.1) THEN
  ET = 0.1
ELSE
  ET = E
ENDIF
DAPR = (-DSQRT(1.0+00 - (E **2))*DCOS(TA))/(MM *A*ET) * FR
DAPS = (P/(ET*M))*(DSIN(TA))*
+ (1.0D+00 + 1.0D+00/(1.0D+00 + ET*DCOS(TA))) *FS
DAPW = (-R*(1.0D+00/DTAN(IT))*DSIN(AL))/
+ (MM *(A**2)*DSQRT(1.0D+00 - (ET**2)))*FW
DAP = DAPR + DAPS + DAPW
RETURN
END
*****
* SUBROUTINE RINC(E,MM,R,A,FW,AL,DI)
  THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE INCLINATION
  DOUBLE PRECISION DI,FW,E,MM,R,A,AL,ET
* TRAP (E) SO DENOMINATOR DOES NOT GOTO ZERO
  IF (E.GT.0.9) THEN
    ET = 0.9
  ELSE
    ET = E
  ENDIF
  DI = (R*FW*DCOS(AL))/(MM *(A**2)*DSQRT(1.0D+00 - (ET**2)))
  RETURN
  END
*****
* SUBROUTINE RMM(MM,A,DMM,DA,MU)
  THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE MEAN MOTION
  DOUBLE PRECISION DMM,DA,MM,A,MU
  DMM =((-3.0D+00*MU)/(2.0D+00*MM *(A**4)))* DA
  RETURN
  END
*****
* SUBROUTINE RMA(E,MM,R,A,TA,DMM,FR,FS,DMA,T)
  THIS SUBROUTINE CALCULATES THE RATE OF CHANGE OF THE MEAN Anomaly
  DOUBLE PRECISION DMAA,DMAB,DMAC,DMAD,DMM,FR,FS,DMA,E,MM,R,A,TA,
+ ET,T
* TRAP (E) SO DENOMINATOR DOES NOT GOTO ZERO
  IF (E.GT.0.9) THEN
    ET = 0.9
  ELSEIF (E.LT.0.1) THEN

```

```

ORB17860
ORB17870
ORB17880
ORB17890
ORB17900
ORB17910
ORB17920
ORB17930
ORB17940
ORB17950
ORB17960
ORB17970
ORB17980
ORB17990
ORB18000
ORB18010
ORB18020
ORB18030
ORB18040
ORB18050
ORB18060
ORB18070
ORB18080
ORB18090
ORB18100
ORB18110
ORB18120
ORB18130
ORB18140
ORB18150
ORB18160
ORB18170
ORB18180
ORB18190
ORB18200
ORB18210
ORB18220
ORB18230
ORB18240
ORB18250
ORB18260
ORB18270
ORB18280
ORB18290
ORB18300
ORB18310
ORB18320
ORB18330
ORB18340
ORB18350
ORB18360
ORB18370
ORB18380
ORB18390
ORB18400
ORB18410

```



```

      ET = 0.1
    ELSE
      ET = E
    ENDIF
    DMA = (-1.0D+00/(MM *A))2
  + ((2.0D+00*R)/A) - ((1 - (E **2))/ET)*DCOS(TA)) * FR -
  + (1-(E **2))/(MM *A*ET)*(1+ R/(A*(1-(E**2))))*(SIN(TA)*FS)-
  + (T * DMM)
  RETURN
  END

```

ORB18420
ORB18430
ORB18440
ORB18450
ORB18460
ORB18470
ORB18480
ORB18490
ORB18500
ORB18510
ORB18520

* CALCULATE THE NEW ORBITAL ELEMENTS

```

  SUBROUTINE NSMA(A,DT,DA,NEWA)
* THIS SUBROUTINE CALCULATES THE NEW SEMI-MAJOR AXIS

  DOUBLE PRECISION DA,DT,A,NEWA

  NEWA = A + DA*DT
  RETURN
  END

```

ORB18530
ORB18540
ORB18550
ORB18560
ORB18570
ORB18580
ORB18590
ORB18600
ORB18610
ORB18620
ORB18630
ORB18640
ORB18650

```

  SUBROUTINE NECC(E,DT,DE,NEWE)
* THIS SUBROUTINE CALCULATES THE NEW ECCENTRICITY

  DOUBLE PRECISION DE,DT,E,NEWE

  NEWE = E + DE*DT
  RETURN
  END

```

ORB18660
ORB18670
ORB18680
ORB18690
ORB18700
ORB18710
ORB18720
ORB18730
ORB18740
ORB18750
ORB18760

```

  SUBROUTINE NINCL(I,DT,DI,NEWI)
* THIS SUBROUTINE CALCULATES THE NEW INCLINATION

  DOUBLE PRECISION DI,DT,I,NEWI

  NEWI = I + DI*DT
  RETURN
  END

```

ORB18770
ORB18780
ORB18790
ORB18800
ORB18810
ORB18820
ORB18830
ORB18840
ORB18850
ORB18860
ORB18870

```

  SUBROUTINE NASNOD(LAN,DT,DLAN,NEWLAN)
* THIS SUBROUTINE CALCULATES THE NEW LONGITUDE OF THE ASCENDING NODE

  DOUBLE PRECISION DLAN,DT,LAN,NEWLAN

  NEWLAN = LAN + DLAN*DT
  RETURN
  END

```

ORB18880
ORB18890
ORB18900
ORB18910
ORB18920
ORB18930
ORB18940
ORB18950
ORB18960
ORB18970

```

SUBROUTINE NARPER(AP,DT,DAP,NEWAP)
* THIS SUBROUTINE CALCULATES THE NEW ARGUMENT OF PERIGEE

DOUBLE PRECISION DAP,DT,AP,NEWAP

NEWAP = AP + DAP*DT
RETURN
END

```

```

SUBROUTINE MNAN(MA,MM,DT,TF,DMA,PI)
* THIS SUBROUTINE CALCULATES THE NEW MEAN Anomaly

DOUBLE PRECISION DMM,FR,FS,DMA,DT,MA,E,R,A,TA,MM,TF,T,PI

MA = MM*(TF) + DMA*DT
IF (MA .GT. (2*PI)) THEN
  MA = MA - (2*PI)
ENDIF
RETURN
END

```

```

SUBROUTINE MNMO(MM,DMM,DT,NEWMM)
* THIS SUBROUTINE CALCULATE THE NEW MEAN MOTION

DOUBLE PRECISION DMM,DT,MM,NEWMM

NEWMM = MM + DMM*DT
RETURN
END

```

```

SUBROUTINE NEA(MA,E,EA)
* THIS SUBROUTINE CALCULATES THE NEW ECCENTRIC ANOMOLY BY USING
* NEWTONS METHOD OF ROOT FINDING

DOUBLE PRECISION EAN,MAN,MA,E,EA,DIFF

* LET (EA) EQUAL (MA) FOR INITIAL GUESS AT ROOT
EA = MA
EAN = EA + (MA - EA + E*DSIN(EA))/(1.0D+00 - E*DCOS(EA))
MAN = EAN - E*SIN(EAN)

* CHECK DIFFERENCE (DIFF)
DIFF = ABS(MA -MAN)
EA = EAN

* CONTINUE TO INTERATE UNTIL DIFFERENCE IS NEGLIGIBLE
200 IF(DIFF.GT.0.000000001) THEN

```

ORB18980
ORB18990
ORB19000
ORB19010
ORB19020
ORB19030
ORB19040
ORB19050
ORB19060
ORB19070
ORB19080
ORB19090
ORB19100
ORB19110
ORB19120
ORB19130
ORB19140
ORB19150
ORB19160
ORB19170
ORB19180
ORB19190
ORB19200
ORB19210
ORB19220
ORB19230
ORB19240
ORB19250
ORB19260
ORB19270
ORB19280
ORB19290
ORB19300
ORB19310
ORB19320
ORB19330
ORB19340
ORB19350
ORB19360
ORB19370
ORB19380
ORB19390
ORB19400
ORB19410
ORB19420
ORB19430
ORB19440
ORB19450
ORB19460
ORB19470
ORB19480
ORB19490
ORB19500
ORB19510
ORB19520
ORB19530

EAN = EA + (MA - EA + E*DSIN(EA))/(1.0D+00 - E*DCOS(EA))	ORB19540
MAN = EAN - E*DSIN(EAN)	ORB19550
EA = EAN	ORB19560
DIFF = ABS(MA - MAN)	ORB19570
GOTO 200	ORB19580
ENDIF	ORB19590
EA = EAN	ORB19600
RETURN	ORB19610
END	ORB19620

* SUBROUTINE NTA(EA,E,TA,PI) THIS SUBROUTINE CALCULATES THE NEW TRUE Anomaly DOUBLE PRECISION EA,E,TA,PI TA = DACOS((E - DCOS(EA))/(E*DCOS(EA) - 1.0D+00)) IF (EA.GT.PI) THEN TA = (2*PI) - TA ENDIF RETURN END	ORB19630 ORB19640 ORB19650 ORB19660 ORB19670 ORB19680 ORB19690 ORB19700 ORB19710 ORB19720 ORB19730 ORB19740 ORB19750 ORB19760 ORB19770

* SUBROUTINE NANGMO(H,DT,DH,NEWH) THIS SUBROUTINE CALCULATES THE NEW ANGULAR MOMENTUM DOUBLE PRECISION DH,DT,H,NEWH NEWH = H + DH*DT RETURN END	ORB19780 ORB19790 ORB19800 ORB19810 ORB19820 ORB19830 ORB19840 ORB19850 ORB19860 ORB19870 ORB19880

* SUBROUTINE INTSUM(TFEA,TFSU,TFMO,TFDRA,TDI,TDA,TDE,TDMM,TDMA, TDLAN,TDH,TDAP) THIS SUBROUTINE INITIALIZES THE SUMS OF FORCES AND ELEMENT CHANGES	ORB19890 ORB19900 ORB19910 ORB19920 ORB19930
TFEA = 0.0 TFSU = 0.0 TFMO = 0.0 TFDRA = 0.0 TDI = 0.0 TDA = 0.0 TDE = 0.0 TDMM = 0.0 TDMA = 0.0 TDLAN = 0.0 TDH = 0.0 TDAP = 0.0 RETURN END	ORB19940 ORB19950 ORB19960 ORB19970 ORB19980 ORB19990 ORB20000 ORB20010 ORB20020 ORB20030 ORB20040 ORB20050 ORB20060 ORB20070 ORB20080

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*****
* CALCULATE THE NEW POSITION AND VELOCITY VECTORS
*****
      SUBROUTINE NPOS(RI,RJ,RK,R,LAN,AP,INC,TA,A,E)
* THIS SUBROUTINE CALCULATES THE NEW POSITION VECTOR

      DOUBLE PRECISION XW,YW,ZW,INC,RI,RJ,RK,R,LAN,AP,TA,A,E

* CALCULATE POSITION VECTOR IN 'PQW' SYSTEM
  R = (A*(1 - (E**2)))/(1 + E*DCOS(TA))
  XW = R*DCOS(TA)
  YW = R*DSIN(TA)
  ZW = 0

* TRANSFORM POSITION TO 'IJK' SYSTEM
  CALL PQWIJK(LAN,AP,INC,XW,YW,ZW,RI,RJ,RK)
  R = DSQRT((RI**2) + (RJ**2) + (RK**2))
  RETURN
  END

*****

      SUBROUTINE NVEL(E,P,TA,LAN,AP,INC,VI,VJ,VK,V,MU)
* THIS SUBROUTINE CALCULATES THE NEW VELOCITY VECTOR

      DOUBLE PRECISION INC,VP,VQ,VW,MU,E,P,TA,LAN,AP,VI,VJ,VK,V

* CALCULATE VELOCITY IN 'PQW' SYSTEM
  VP = DSQRT(MU/P)*(-DSIN(TA))
  VQ = DSQRT(MU/P)*(E + DCOS(TA))
  VW = 0.0D+00

* TRANSFORM VELOCITY INTO 'IJK' SYSTEM
  CALL PQWIJK(LAN,AP,INC,VP,VQ,VW,VI,VJ,VK)
  V = DSQRT((VI**2) + (VJ**2) + (VK**2))
  RETURN
  END

*****
* VELOCITY CHANGE
*****

      SUBROUTINE CHGVEL(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,
+ VI,VJ,VK,V,MU,PI,H,A,E,N,TA,P,MM,MA,EA,
+ TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,TARAY,AINRAY,APRAY,TIMRAY,
+ TT,EI,EJ,EK,LP,HI,HJ,IOPT1,TFEA,TFSU,TFMO,TFDRA,
+ TDI,TDA,TDE,TDMM,TDMA,TDLAN,TDH,TDAP)
* THIS SUBROUTINE CALCULATE VELOCITY CHANGES

* THE FOLLOWING SUBROUTINES ARE CALLED:
* TACHG = RETURNS TRUE ANOMALY FOR VELOCITY CHANGE LOCATION (CHTA)
* AND AN INDICATOR OF LOCATION (ITA)
* CALCEL = CALCULATE Orbital ELEMENTS
* UNPREZ = CALCULATE UNPERTURBED ORBIT

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ORB20090
ORB20100
ORB20110
ORB20120
ORB20130
ORB20140
ORB20150
ORB20160
ORB20170
ORB20180
ORB20190
ORB20200
ORB20210
ORB20220
ORB20230
ORB20240
ORB20250
ORB20260
ORB20270
ORB20280
ORB20290
ORB20300
ORB20310
ORB20320
ORB20330
ORB20340
ORB20350
ORB20360
ORB20370
ORB20380
ORB20390
ORB20400
ORB20410
ORB20420
ORB20430
ORB20440
ORB20450
ORB20460
ORB20470
ORB20480
ORB20490
ORB20500
ORB20510
ORB20520
ORB20530
ORB20540
ORB20550
ORB20560
ORB20570
ORB20580
ORB20590
ORB20600
ORB20610
ORB20620
ORB20630
ORB20640

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* NPOS = CALCULATE NEW POSITION	JRB20650
* NVEL = CALCULATE NEW VELOCITY	ORB20660
* STORE = STORE POSITION AND ELEMENTS IN ARRAYS	ORB20670
* ENERGY = ENERGY OF SATELLITE	ORB20680
* ECC = ECCENTRICITY	ORB20690
* SMANIS = SEMI-MAJOR AXIS	ORB20700
DOUBLE PRECISION T,DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB20710
+ MU,PI,H,A,E,N,TA,P,MM,MA,EA,TF,TT,	ORB20720
+ NEWVI,NEWVJ,NEWVK,NEWV,VMAX,CHTA,EI,EJ,EK,LP,HI,HJ,VCIR,	ORB20730
+ DI,DE,DA,DM,DMA,DLAN,DH,DAP,NWEI,NEWJ,NEWK,NEWL,NEWNR,	ORB20740
+ NEWA,NEWRP,RE	ORB20750
DIMENSION RARAY(500),TARAY(500),RIRAY(500),RJRAY(500),	ORB20760
+ RKRAY(500),AINRAY(500),APRAY(500),TIMRAY(500)	ORB20770
CHARACTER*1,YORN,PYORN	ORB20780
RE = 6.3782D+03	ORB20790
* PROMPT THE USER FOR THE VELOCITY CHANGE LOCATION	ORB20800
CALL TACNG(PI,CHTA,ITA)	ORB20810
* SET TIME COUNTER TO ONE TIME STEP	ORB20820
T = DT	ORB20830
* ROTATE TO THE VELOCITY CHANGE LOCATION	ORB20840
* THIS IS IDENTICAL TO THE Unperturbed ORBIT WITH THE EXCEPTION	ORB20850
* THAT A COMPLETE ORBIT IS NOT CALCULATED	ORB20860
PRINT*, 'ROTATE TO VELOCITY CHANGE LOCATION'	ORB20870
IF ((ITA.EQ.2) .OR. (ITA.EQ.3)) THEN	ORB20880
PRINT*, 'BEFORE TA =', TA	ORB20890
IF (TA .GT. 6.21) THEN	ORB20900
TA = TA - (2*PI)	ORB20910
ENDIF	ORB20920
250 IF((T.LE.PER).AND.(TA.LT.CHTA)) THEN	ORB20930
* PRINT*, 'TA =', TA	ORB20940
NUM = NUM + 1	ORB20950
TT = TT + DT	ORB20960
CALL NEWLT(MM,MA,E,EA,TA,TF,DT,PI,PER)	ORB20970
CALL NPOS(RI,RJ,RK,R,LAN,AP,I,TA,A,E)	ORB20980
CALL NVEL(E,P,TA,LAN,AP,I,VI,VJ,VK,V,MU)	ORB20990
CALL STORE(RI,RJ,RK,R,TA,RIRAY,RJRAY,RKRAY,RARAY,	ORB21000
+ TARAY,NUM,I,AP,AINRAY,APRAY,TT,TIMRAY)	ORB21010
T = T + DT	ORB21020
GOTO 250	ORB21030
ENDIF	ORB21040
IF (TF .GE. PER) THEN	ORB21050
TF = TF - PER	ORB21060
ENDIF	ORB21070
ENDIF	ORB21080
* PRINT ESCAPE VELOCITY AND CIRCULAR VELOCITY FOR Reference	ORB21090
CALL EXCMS('CLRSCRN')	ORB21100
PRINT*, 'AFTER TA =', TA	ORB21110
PRINT*, 'THIS SHOULD BE THE DESIRED RADIUS RP OR RA'	ORB21120
	ORB21130
	ORB21140
	ORB21150
	ORB21160
	ORB21170
	ORB21180
	ORB21190
	ORB21200

360	PRINT*, 'RADIUS =', R	ORB21210
	PRINT*, 'VELOCITY =', V	ORB21220
	VMAX = DSQRT(2.0*(MU / R))	ORB21230
	PRINT*, 'MAX VELOCITY AT THIS RADIUS IS:', VMAX	ORB21240
	VCIR = DSQRT(MU/R)	ORB21250
	PRINT*, 'CIRCULAR VELOCITY AT THIS RADIUS IS:', VCIR	ORB21260
		ORB21270
*	PROMPT USER TO CHANGE VELOCITY IN ORBITAL PLANE	ORB21280
	PRINT*, 'DO YOU WANT TO CHANGE THE VELOCITY IN THE ORBITAL PLANE?'	ORB21290
	PRINT*, 'ENTER "Y" OR "N" :'	ORB21300
	READ*, PYORN	ORB21310
	PRINT*, PYORN	ORB21320
	IF (PYORN .EQ. 'Y') THEN	ORB21330
	PRINT*, 'GIVE THE TOTAL CHANGE IN VELOCITY, I. E. 5.0 KM.'	ORB21340
	PRINT*, 'THE PROGRAM WILL FIGURE OUT THE FINAL VELOCITY VECTOR'	ORB21350
	PRINT*, ' ENTER VELOCITY CHANGE: '	ORB21360
	READ*, CHGV	ORB21370
	PRINT*, CHGV	ORB21380
		ORB21390
*	CALCULATE NEW VELOCITY FOR CHANGE IN THE ORBITAL PLANE	ORB21400
	NEWVI = VI + (CHGV * VI / V)	ORB21410
	NEWVJ = VJ + (CHGV * VJ / V)	ORB21420
	NEWVK = VK + (CHGV * VK / V)	ORB21430
		ORB21440
*	Velocity CHANGE OUT OF ORBITAL PLANE	ORB21450
	ELSEIF (PYORN .EQ. 'N') THEN	ORB21460
	PRINT*, ' ENTER THE NEW VELOCITY VECTOR: '	ORB21470
	PRINT*, ' ENTER THE NEW VI'	ORB21480
	READ*, NEWVI	ORB21490
	PRINT*, NEWVI	ORB21500
	PRINT*, ' ENTER THE NEW VJ'	ORB21510
	READ*, NEWVJ	ORB21520
	PRINT*, NEWVJ	ORB21530
	PRINT*, ' ENTER THE NEW VK'	ORB21540
	READ*, NEWVK	ORB21550
	PRINT*, NEWVK	ORB21560
	NUM = 1	ORB21570
	ITA = 3	ORB21580
	ELSE	ORB21590
	CALL EXCMS('GLRSCRN')	ORB21600
	GOTO 260	ORB21610
	ENDIF	ORB21620
		ORB21630
*	PRINT NEW VELOCITY FOR USER TO CHECK	ORB21640
	NEWV = DSQRT((NEWVI**2) + (NEWVJ**2) + (NEWVK**2))	ORB21650
	PRINT*, 'NEW VI =', NEWVI	ORB21660
	PRINT*, 'NEW VJ =', NEWVJ	ORB21670
	PRINT*, 'NEW VK =', NEWVK	ORB21680
	PRINT*, 'NEW V =', NEWV	ORB21690
	PRINT*, 'ARE THESE VALUES THE ONES YOU WANT?'	ORB21700
	PRINT*, 'ENTER "Y" OR "N" :'	ORB21710
	READ*, YORN	ORB21720
	PRINT*, YORN	ORB21730
	IF (YORN .EQ. 'N') THEN	ORB21740
	CALL EXCMS('CLRSCRN')	ORB21750
	GOTO 260	ORB21760

<pre> ENDIF * CHECK FOR VALID VELOCITY IF (NEWV .GT. VMAX) THEN PRINT*, 'YOUR VELOCITY IS TO GREAT !! ' GOTO 260 ENDIF * Calculate PERIGEE RADIUS TO SEE IF SATELLITE WILL IMPACT EARTH CALL ENERGY(NEWV,R,MU,NEWENR) CALL ECC(RI,RJ,RK,R,NEWVI,NEWVJ,NEWVK,NEWV,NEWEI,NEWVJ,NEWVK, + NEWV,MU) CALL SMAXIS(MU,NEWENR,NEWA) NEWRP = NEWA*(1.0 - NEWV) IF (NEWRP .LE. RE) THEN PRINT*, 'YOUR VELOCITY AT THIS POINT IS TO SMALL!!! ' PRINT*, 'THE SATELLITE WILL IMPACT THE EARTH!! ' PRINT*, 'THE SATELLITES RADIUS OF PERIGEE WOULD BE ',NEWRP PRINT*, 'A NEW VELOCITY WILL HAVE TO BE ENTERED!! ' GOTO 260 ENDIF * ACCEPT NEW VELOCITY VI = NEWVI VJ = NEWVJ VK = NEWVK V = NEWV * CALCULATE NEW ELEMENT WITH NEW VELOCITY AND SET TIME STEP CALL CALCEL(RI,RJ,RK,R,VI,VJ,VK,V,EI,EJ,EK,E,A,I,LAN,LP,TA, + PER,EA,MA,AP,AL,TF,P,PI,MU,MM,N,H,HI,HJ) DT = PER/50.0 T = DT * THE FOUR Different CASES OF VELOCITY CHANGES FOLLOWS: * VELOCITY CHANGE AT PERIGEE, AND NEWV > V Circular IF((ITA. EQ. 1). AND. (NEWV. GT. VCIR))THEN CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V, + MU,PI,H,A,E,N,TA,P,MM, + MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY, + TARAY,AINRAY,APRAY,TIMRAY,TT) * Change VELOCITY AT PERIGEE, AND NEWV <= V CIRCULAR * APOGEE AND PERIGEE SWAP ELSEIF ((ITA. EQ. 1). AND. (NEWV. LE. VCIR))THEN * CLEAR PREVIOUS PLOTS NUM = 1 CALL STORE(RI,RJ,RK,R,TA,RIKAY,RJRAY,RKRAY,RARAY,TARAY, + NUM,I,AP,AINRAY,APRAY,TT,TIMRAY) T = PER/2 * STEP SATELLITE TO NEW PERIGEE, ONLY A HALF ORBIT CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V, + MU,PI,H,A,E,N,TA,P,MM, </pre>	<pre> ORB21770 ORB21780 ORB21790 ORB21800 ORB21810 ORB21820 ORB21830 ORB21840 ORB21850 ORB21860 ORB21870 ORB21880 ORB21890 ORB21900 ORB21910 ORB21920 ORB21930 ORB21940 ORB21950 ORB21960 ORB21970 ORB21980 ORB21990 ORB22000 ORB22010 ORB22020 ORB22030 ORB22040 ORB22050 ORB22060 ORB22070 ORB22080 ORB22090 ORB22100 ORB22110 ORB22120 ORB22130 ORB22140 ORB22150 ORB22160 ORB22170 ORB22180 ORB22190 ORB22200 ORB22210 ORB22220 ORB22230 ORB22240 ORB22250 ORB22260 ORB22270 ORB22280 ORB22290 ORB22300 ORB22310 ORB22320 </pre>
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	+	MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,	ORB22330
	+	TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB22340
*		RESET TIME COUNTER TO ONE TIME STEP	ORB22350
		T = DT	ORB22360
			ORB22370
			ORB22380
*		CALCULATE COMPLETE NEXT ORBIT	ORB22390
		CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB22400
	+	MU,PI,H,A,E,N,TA,P,MM,	ORB22410
	+	MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,	ORB22420
	+	TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB22430
			ORB22440
*		CHANGE VELOCITY AT APOGEE, AND NEW V < V CIRCULAR	ORB22450
		ELSEIF ((ITA. EQ. 2) .AND. (NEWV .LT. VCIR)) THEN	ORB22460
		T = PER/2	ORB22470
			ORB22480
			ORB22490
*		FINISH ORBIT	ORB22500
		CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB22510
	+	MU,PI,H,A,E,N,TA,P,MM,	ORB22520
	+	MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,	ORB22530
	+	TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB22540
			ORB22550
*		CHANGE VELOCITY AT Apogee, AND NEWV >= V CIRCULAR	ORB22560
*		OR AT ANY OTHER TRUE Anomaly	ORB22570
		ELSEIF (((ITA. EQ. 2).AND. (NEWV. GE. VCIR)) .OR. (ITA. EQ. 3)) THEN	ORB22580
			ORB22590
		IF (TA .GT. 6.21) THEN	ORB22600
		TA = TA - (2*PI)	ORB22610
		ENDIF	ORB22620
			ORB22630
*		CLEAR PREVIOUS ORBITS AND STEP SATELLITE TO NEW PERIGEE	ORB22640
		T = TF	ORB22650
		NUM = 1	ORB22660
		CALL STORE(RI,RJ,RK,R,TA,RIPAY,RJRAY,RKRAY,RARAY,TARAY,	ORB22670
	+	NUM,I,AP,AINRAY,APRAY,TT,TIMRAY)	ORB22680
		CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB22690
	+	MU,PI,H,A,E,N,TA,P,MM,	ORB22700
	+	MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,	ORB22710
	+	TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB22720
		IF (TF .GE. PER) THEN	ORB22730
		TF = TF - PER	ORB22740
		ENDIF	ORB22750
			ORB22760
*		CALCULATE COMPLETE NEXT ORBIT	ORB22770
		T = DT	ORB22780
		CALL UNPRET(DT,PER,AL,LAN,AP,I,RI,RJ,RK,R,VI,VJ,VK,V,	ORB22790
	+	MU,PI,H,A,E,N,TA,P,MM,	ORB22800
	+	MA,EA,TF,T,NUM,RIRAY,RJRAY,RKRAY,RARAY,	ORB22810
	+	TARAY,AINRAY,APRAY,TIMRAY,TT)	ORB22820
		ENDIF	ORB22830
		RETURN	ORB22840
		END	ORB22850
			ORB22860
			ORB22870
			ORB22880


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SUBROUTINE TACNG(PI,CHTA,ITA)
* THIS SUBROUTINE Asks THE USER FOR VELOCITY CHANGE LOCATION
DOUBLE PRECISION CHTA,PI
CALL EXCHS('CLRSRN')
PRINT*, 'WHERE DO YOU WANT TO CHANGE THE VELOCITY?'
PRINT*, ' 1. AT CURRENT PERIGEE'
PRINT*, ' 2. AT CURRENT Apogee'
PRINT*, ' 3. AT A SPECIFIC TRUE Anomaly'
PRINT*, 'ENTER "1", "2" OR "3"'
READ*, ITA
PRINT*, ITA
* SET TRUE ANOMALY CHANGE LOCATION (CHTA) TO DESIRED LOCATION
IF (ITA .EQ. 1) THEN
  CHTA = 0.0
ENDIF
IF (ITA .EQ. 2) THEN
  CHTA = PI
ENDIF
IF (ITA .EQ. 3) THEN
  PRINT*, 'AT WHAT TRUE ANOMALY DO YOU WANT TO CHANGE THE'
  PRINT*, 'VELOCITY?'
  PRINT*, 'ENTER TRUE ANOMALY IN DEGREES'
  READ*, CHTA
  PRINT*, CHTA
  CHTA = CHTA * PI / 180
ENDIF
RETURN
END

*****
* OUTPUT PLOTS
*****
SUBROUTINE PLOTS(RIRAY,RJRAY,RKRAY,RARAY,TARAY,NUM,PI,INC,LP,A,
+ E,TF,AINRAY,APRAY,TIMRAY,TFEA,TFSU,TFMO,TFDRA,
+ PER,TDI,TDA,TDE,TDMM,TDMA,TDLAN,TDH,TDAP,
+ MM,MA,LAN,H,AP,R,V)
* THIS SUBROUTINE ASKS THE USER FOR THE TYPE OF OUTPUT THAT IS
* DESIRED PERIFOCAL, GROUND TRACK OR TO SKIP THE PLOT.
* THE FOLLOWING SUBROUTINES ARE CALLED:
* PERIF = PLOT PERIFOCAL ORBIT
* GRTRK = PLOT GROUND TRACK
* DATE = DISPLAYS DATA ON PLOT
* TEC618 = SET Disspla TO TEC 618 OUTPUT
* ENDPL = END THIS DISSPLA PLOT
* REFER TO DISSPLA USER'S MANUAL FOR EXPLANATION OF DISSPLA
* SUBROUTINES
DOUBLE PRECISION PI,A,E,INC,LP,TF,PER,MM,MA,LAN,H,AP,R,V
DIMENSION RIRAY(500),RJRAY(500),RKRAY(500),RARAY(500),TARAY(500),

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ORB22890
ORB22900
ORB22910
ORB22920
ORB22930
ORB22940
ORB22950
ORB22960
ORB22970
ORB22980
ORB22990
ORB23000
ORB23010
ORB23020
ORB23030
ORB23040
ORB23050
ORB23060
ORB23070
ORB23080
ORB23090
ORB23100
ORB23110
ORB23120
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ORB23200
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ORB23310
ORB23320
ORB23330
ORB23340
ORB23350
ORB23360
ORB23370
ORB23380
ORB23390
ORB23400
ORB23410
ORB23420
ORB23430
ORB23440

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+ AINRAY(500),APRAY(500),TIMRAY(500)	ORB23450
CHARACTER*1,YORN	ORB23460
CALL EXCMS('CLRSCRN')	ORB23470
	ORB23480
	ORB23490
* CALCULATE SINGLE PRECISION VARIABLES	ORB23500
SPI = SNGL(PI)	ORB23510
SA = SNGL(A)	ORB23520
SE = SNGL(E)	ORB23530
SINC = SNGL(INC)	ORB23540
SLP = SNGL(LP)	ORB23550
STF = SNGL(TF)	ORB23560
SPER = SNGL(PER)	ORB23570
SMM = SNGL(MM)	ORB23580
SMA = SNGL(MA)	ORB23590
SLAN = SNGL(LAN)	ORB23600
SH = SNGL(H)	ORB23610
SAP = SNGL(AP)	ORB23620
SV = SNGL(V)	ORB23630
SR = SNGL(R)	ORB23640
	ORB23650
	ORB23660
* PROMPT USER FOR DISPLAY TYPE	ORB23670
340 PRINT*, 'WHAT TYPE OF Display IS DESIRED: '	ORB23680
PRINT*, ' 1. PERIFOCAL'	ORB23690
PRINT*, ' 2. GROUND TRACK'	ORB23700
PRINT*, ' 3. SKIP PLOT'	ORB23710
PRINT*, 'ENTER 1,2,3,4: '	ORB23720
READ*, INPUT	ORB23730
PRINT350, INPUT	ORB23740
350 FORMAT(I4)	ORB23750
	ORB23760
CALL TEK618	ORB23770
	ORB23780
* CALL APPROPRIATE PLOT	ORB23790
IF (INPUT .EQ. 1) THEN	ORB23800
CALL PERIF(RARAY, TARAY, NUM, SPI, SINC, SLP, SA, SE)	ORB23810
ELSEIF (INPUT .EQ. 2) THEN	ORB23820
CALL GRTRK(AINRAY, APRAY, TARAY, STF, NUM, TIMRAY)	ORB23830
ELSEIF (INPUT .EQ. 3) THEN	ORB23840
GOTO 360	ORB23850
ELSE	ORB23860
PRINT*, 'INVALID ENTRY!'	ORB23870
GOTO 340	ORB23880
*NDIF	ORB23890
	ORB23900
* DISPLAY DATA	ORB23910
CALL DATA(SINC, SA, SE, TFEA, TFSU, TFMO, TFDRA, SPER, SPI, TDI, TDA, TDE,	ORB23920
+ TDM, TDMA, TDLAN, TDH, TDAP, SMM, SMA, SLAN, SH, SAP, SV, SR)	ORB23930
CALL ENDPL(0)	ORB23940
	ORB23950
* PROMPT USER IF ANOTHER DISPLAY TYPE IS DESIRED	ORB23960
PRINT*, 'WOULD YOU LIKE ANOTHER PLOT USING THE SAME ORBITAL'	ORB23970
PRINT*, 'PARAMETERS AND DATA: '	ORB23980
PRINT*, 'ENTER "Y" OR "N" : '	ORB23990
READ*, YORN	ORB24000
PRINT*, YORN	

IF (YORN .EQ. 'Y') THEN	ORB24010
GOTO 340	ORB24020
ENDIF	ORB24030
360 RETURN	ORB24040
END	ORB24050
*****	ORB24060
SUBROUTINE PERIF(RARAY,TARAY,NUM,PI,INC,LP,A,E)	ORB24070
* THIS SUBROUTINE PLOTS OUT THE RESULTS OF THE PROGRAM USING THE	ORB24080
* DISPLAY FEATURE ON THE MAIN FRAME.	ORB24090
* REFER TO DISSPLA USERS GUIDE FOR EXPLANATION OF DISSPLA	ORB24100
* SUBROUTINES.	ORB24110
REAL INC,LP	JRB24120
DIMENSION TARAY(500),RARAY(500),RIRAY(500),RJRAY(500),RKRAY(500)	ORB24130
I = 1	ORB24140
* SET SCALE OF AXIS	ORB24150
RSTEP = (A*(1+E)) / 3	ORB24160
CALL TEN618	ORB24170
CALL RESET(3HALL)	ORB24180
CALL SCMPX	ORB24190
CALL PHYSOR(1.25,4.)	ORB24200
CALL AREA2D(6.,6.)	ORB24210
CALL MESSAG('PERIFOCAL COORDINATE SYSTEM\$',100,1.0,6.5)	ORB24220
CALL XNAME('XW',2)	ORB24230
CALL YNAME('YW',2)	ORB24240
CALL XAXANG(90.0)	ORB24250
CALL YAXANG(0.0)	ORB24260
CALL INTAXS	ORB24270
CALL POLAR(1.,RSTEP,3.,3.)	ORB24280
CALL POLY3	ORB24290
CALL NOCHEK	ORB24300
CALL CURVE(TARAY,RARAY,NUM,1)	ORB24310
CALL COMPLX	ORB24320
CALL HEIGHT(.2)	ORB24330
CALL RESET('COMPLEX')	ORB24340
CALL RESET('HEIGHT')	ORB24350
CALL ENDGR(0)	ORB24360
* Display EARTH PLOT	ORB24370
CALL EARTH1(A,E,INC,PI,RSTEP)	ORB24380
RETURN	ORB24390
END	ORB24400
*****	ORB24410
SUBROUTINE EARTH1(A,E,INC,PI,RSTEP)	ORB24420
* THIS SUBROUTINE PLOTS A VIEW OF THE WORLD, LOOKING DOWN THE 'Z'	ORB24430
* AXIS, PLACED ON THE ORIGIN. THE Latitude IS FIXED, BUT THE	ORB24440
* LONGITUDE VARIES WITH THE INCLINATION.	ORB24450
* REFER TO DISSPLA USER'S MANUAL FOR EXPLANATION OF DISSPLA	ORB24460
* SUBROUTINES	ORB24470
	ORB24480
	ORB24490
	ORB24500
	ORB24510
	ORB24520
	ORB24530
	ORB24540
	ORB24550
	ORB24560

REAL INC
COMMON IWORK(3800)
DATA IWDIM/3800/

RE = 6378.145

* SCALE THE EARTH PLOT AND CENTER ON THE ORIGIN
SCFAC = RE/RSTEP
SCFAC2 = SCFAC * 2.0
XPHS = 1.25 + 3.0 - SCFAC
YPHS = 4.0 + 3.0 - SCFAC
YPOLE = 90 - (INC * 180 / PI)
IF(YPOLE .GT. 90) THEN
 YPOLE = YPOLE - 90
ENDIF
YORIG = YPOLE - 90
YMAX = YPOLE + 90
CALL RESET(3HALL)
CALL PHYSOR(XPHS,YPHS)
CALL PROJECT('LAMBERT EQ/AREA')
CALL MAPOLE(0.0,YPOLE)
CALL AREA2D(SCFAC2,SCFAC2)
CALL THKFRM(0.02)
CALL GRAF(-90.,30.,90.,YORIG,30.,YMAX)
CALL FRAME
CALL MAPFIL('MAPDTA')
CALL LBLANK('LAND',IWDIM)
CALL GRID(1,1)
CALL LBLANK('WATER',IWDIM)
CALL DASH
CALL GRID(1,1)
CALL RESET('DASH')
CALL ENDGR(0)
RETURN
END

SUBROUTINE GRTRK(AINRAY,APRAY,TARAY,TF,NUM,TIMRAY)

DIMENSION AINRAY(500),APRAY(500),TARAY(500),
+ ELARAY(500),ELORAY(500),TLONG(500),TLAT(500),TIMRAY(500)

RE = 6.3782E+03
EROT = 7.292115856E-05
STF = (TF)
I = 1

* LOAD ARRAYS WITH LATITUDE AND LONGITUDE

410 IF (I .LE. NUM) THEN
 X = RE*COS(APRAY(I))*COS(TARAY(I))-RE*SIN(APRAY(I))*
 + SIN(TARAY(I))
 Y = RE*COS(AINRAY(I))*SIN(APRAY(I))*COS(TARAY(I)) +
 + RE*COS(AINRAY(I))*COS(APRAY(I))*SIN(TARAY(I))
 Z = RE*SIN(AINRAY(I))*SIN(APRAY(I))*COS(TARAY(I)) +
 + RE*SIN(AINRAY(I))*COS(APRAY(I))*SIN(TARAY(I))

ORB24570
ORB24580
ORB24590
ORB24600
ORB24610
ORB24620
ORB24630
ORB24640
ORB24650
ORB24660
ORB24670
ORB24680
ORB24690
ORB24700
ORB24710
ORB24720
ORB24730
ORB24740
ORB24750
ORB24760
ORB24770
ORB24780
ORB24790
ORB24800
ORB24810
ORB24820
ORB24830
ORB24840
ORB24850
ORB24860
ORB24870
ORB24880
ORB24890
ORB24900
ORB24910
ORB24920
ORB24930
ORB24940
ORB24950
ORB24960
ORB24970
ORB24980
ORB24990
ORB25000
ORB25010
ORB25020
ORB25030
ORB25040
ORB25050
ORB25060
ORB25070
ORB25080
ORB25090
ORB25100
ORB25110
ORB25120

		ORB25130
*	CALCULATE LATITUDE	ORB25140
	ELARAY(I) = (ASIN(Z/RE)) * (180/3.14159)	ORB25150
		ORB25160
*	TRAP 'X' AND 'Y' FOR ARCTAN IN CALCULATING LONGITUDE	ORB25170
	IF((Y .LE. 10) .AND. (Y .GE. 0.0)) THEN	ORB25180
	Y = 10.	ORB25190
	ELSEIF ((Y .GE. -10) .AND. (Y .LE. 0.0)) THEN	ORB25200
	Y = -10.	ORB25210
	ENDIF	ORB25220
	IF((X .LE. 10) .AND. (X .GE. 0.0)) THEN	ORB25230
	X = 10.	ORB25240
	ELSEIF ((X .GE. -10) .AND. (X .LE. 0.0)) THEN	ORB25250
	X = -10.	ORB25260
	ENDIF	ORB25270
		ORB25280
*	CALCULATE LONGITUDE	ORB25290
	ELORAY(I) = (ATAN2(Y,X) - (EROT*TIMRAY(I))) * (180/3.14159)	ORB25300
		ORB25310
*	MODIFY LONGITUDES TO (-180 TO 180)	ORB25320
420	IF (ELORAY(I) .LT. -180) THEN	ORB25330
	ELORAY(I) = ELORAY(I) + 360	ORB25340
	GOTO 420	ORB25350
	ENDIF	ORB25360
	I = I + 1	ORB25370
	GOTO 410	ORB25380
	ENDIF	ORB25390
		ORB25400
*	SET DISSFLA	ORB25410
	CALL TEN61S	ORB25420
	CALL RESET(3HALL)	ORB25430
	CALL YANANG (0.)	ORB25440
	CALL PHYSOR(1.0,6.0)	ORB25450
	CALL XNAME(' ',1)	ORB25460
	CALL YNAME(' ',1)	ORB25470
	CALL AREA2D(7.5,3.75)	ORB25480
	CALL HEADIN ('GROUND TRACKS',100,1.5,1)	ORB25490
	CALL SCMPLN	ORB25500
	CALL MAPGR(-180.,90.,180.,-90.,30.,90.)	ORB25510
	CALL GRID (1,1)	ORB25520
	CALL MAPFIL ('MAPDTA')	ORB25530
	I = 1	ORB25540
		ORB25550
*	IGNORE Boundary POINTS	ORB25560
430	IF ((ELORAY(I) .LT. -175) .OR.	ORB25570
	+ (ELORAY(I) .GT. 175) .OR.	ORB25580
	+ (ELARAY(I) .LT. -85) .OR.	ORB25590
	+ (ELARAY(I) .GT. 85)) THEN	ORB25600
	I = I + 1	ORB25610
	GOTO 430	ORB25620
	ENDIF	ORB25630
		ORB25640
	ITEMP = 1	ORB25650
		ORB25660
*	LOAD FIRST POINT OF NEW PLOT SEGMENT	ORB25670
	IF (I .LE. NUM) THEN	ORB25680

	TLONG(ITEMP) = ELORAY(I)	ORB25690
	TLAT(ITEMP) = ELARAY(I)	ORB25700
	I = I + 1	ORB25710
*	IF (I .GE. NUM) THEN	ORB25720
*	CALL POLY3	ORB25730
*	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB25740
*	ENDIF	ORB25750
	ENDIF	ORB25760
		ORB25770
*	LOAD SECOND POINT IN LINE SEGMENT	ORB25780
	IF (I .LE. NUM) THEN	ORB25790
	ITEMP = ITEMP + 1	ORB25800
	TLONG(ITEMP) = ELORAY(I)	ORB25810
	TLAT(ITEMP) = ELARAY(I)	ORB25820
	I = I + 1	ORB25830
	IF (I .GE. NUM) THEN	ORB25840
	CALL POLY3	ORB25850
	CALL NOCHEK	ORB25860
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB25870
	ENDIF	ORB25880
	ENDIF	ORB25890
		ORB25900
*	LOOP UNTIL SEGMENT REACHES EDGE OR NO MORE POINTS	ORB25910
440	IF (I .LE. NUM) THEN	ORB25920
		ORB25930
*	BOTH LAT AND LONG INCREASING	ORB25940
	IF((ELORAY(I - 2) .LE. ELORAY(I - 1)) .AND.	ORB25950
+	(ELARAY(I - 2) .LE. ELARAY(I - 1))) THEN	ORB25960
	IF((ELORAY(I) .LT. -170) .OR.	ORB25970
+	(ELARAY(I) .LT. -80)) THEN	ORB25980
	CALL POLY3	ORB25990
	CALL NOCHEK	ORB26000
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26010
	GOTO 430	ORB26020
	ELSE	ORB26030
	ITL = ITEMP + 1	ORB26040
	TLONG(ITEMP) = ELORAY(I)	ORB26050
	TLAT(ITEMP) = ELARAY(I)	ORB26060
	ENDIF	ORB26070
		ORB26080
*	BOTH LAT AND LONG DECREASING	ORB26090
	ELSEIF((ELORAY(I - 2) .GT. ELORAY(I - 1)) .AND.	ORB26100
+	(ELARAY(I - 2) .GT. ELARAY(I - 1))) THEN	ORB26110
	IF((ELORAY(I) .GT. 170) .OR.	ORB26120
+	(ELARAY(I) .GT. 80)) THEN	ORB26130
	CALL POLY3	ORB26140
	CALL NOCHEK	ORB26150
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26160
	GOTO 430	ORB26170
	ELSE	ORB26180
	ITEMP = ITEMP + 1	ORB26190
	TLONG(ITEMP) = ELORAY(I)	ORB26200
	TLAT(ITEMP) = ELARAY(I)	ORB26210
	ENDIF	ORB26220
		ORB26230
*	LAT INCREASING, LONG. DECREASING	ORB26240

	ELSEIF((ELORAY(I - 2) .GT. ELORAY(I - 1)) .AND.	ORB26250
+	(ELARAY(I - 2) .LE. ELARAY(I - 1))) THEN	ORB26260
	IF((ELORAY(I) .GT. 170) .OR.	ORB26270
+	(ELARAY(I) .LT. -80)) THEN	ORB26280
	CALL POLY3	ORB26290
	CALL NOCHEK	ORB26300
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26310
	GOTO 430	ORB26320
	ELSE	ORB26330
	ITEMP = ITEMP + 1	ORB26340
	TLONG(ITEMP) = ELORAY(I)	ORB26350
	TLAT(ITEMP) = ELARAY(I)	ORB26360
	ENDIF	ORB26370
		ORB26380
*	LAT. DECREASING, LONG. INCREASING	ORB26390
	ELSEIF((ELORAY(I - 2) .LE. ELORAY(I - 1)) .AND.	ORB26400
+	(ELARAY(I - 2) .GT. ELARAY(I - 1))) THEN	ORB26410
	IF((ELORAY(I) .LT. -170) .OR.	ORB26420
+	(ELARAY(I) .GT. 80)) THEN	ORB26430
	CALL POLY3	ORB26440
	CALL NOCHEK	ORB26450
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26460
	GOTO 430	ORB26470
	ELSE	ORB26480
	ITEMP = ITEMP + 1	ORB26490
	TLONG(ITEMP) = ELORAY(I)	ORB26500
	TLAT(ITEMP) = ELARAY(I)	ORB26510
	ENDIF	ORB26520
	ENDIF	ORB26530
	IF(I .EQ. NUM) THEN	ORB26540
	CALL POLY3	ORB26550
	CALL NOCHEK	ORB26560
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26570
	ENDIF	ORB26580
	I = I + 1	ORB26590
	GOTO 440	ORB26600
	ENDIF	ORB26610
		ORB26620
	CALL POLY3	ORB26630
	CALL NOCHEK	ORB26640
	CALL CURVE(TLONG,TLAT,ITEMP,1)	ORB26650
		ORB26660
		ORB26670
		ORB26680
	CALL COMPLX	ORB26690
	CALL HEIGHT(.2)	ORB26700
	CALL THKFRM (0.03)	ORB26710
	CALL FRAME	ORB26720
	CALL RESET('COMPLX')	ORB26730
	CALL RESET('HEIGHT')	ORB26740
	CALL ENDGR (0)	ORB26750
	RETURN	ORB26760
	END	ORB26770
		ORB26780
	*****	ORB26790
		ORB26800

	SUBROUTINE DATA(I,A,E,TFEA,TFSU,TFMO,TFDRA,PER,PI,TDI,TDA,TDE,	ORB26810
	+ TDMM,TDMA,TDLAN,TDH,TDAP,MM,MA,LAN,H,AP,V,R)	ORB26820
*	THIS SUBROUTINE Displays THE ORBITAL DATA FOR BOTH THE PERIFOCAL	ORB26830
*	AND THE GROUND TRACK PLOTS.	ORB26840
*	REFER TO DISSPLA USER'S MANUAL FOR EXPLANATION OF DISSPLA	ORB26850
*	SUBROUTINES	ORB26860
	REAL I,MM,MA,LAN	ORB26870
	MU = 3.986012E+05	ORB26880
		ORB26890
*	CALCULATE THE AVERAGE FORCES FROM THE TOTAL MAGNITUDE OF	ORB26900
*	FORCE CHANGES	ORB26910
	AVGFE = TFEA/50.0	ORB26920
	AVGFS = TFSU / 50.0	ORB26930
	AVGFM = TFMO / 50.0	ORB26940
	AVGFD = TFDRA / 50.0	ORB26950
		ORB26960
		ORB26970
*	CALCULATE ORBITAL ELEMENTS IN Usable UNITS	ORB26980
	PERH = PER/3600	ORB26990
		ORB27000
	DI = I * (180.0/PI)	ORB27010
	DLAN = LAN * (180.0/PI)	ORB27020
	DAP = AP * (180.0/PI)	ORB27030
		ORB27040
*	CALCULATE Average CHANGE IN ELEMENTS FOR ONE PERIOD	ORB27050
	AVGDI = TDI / 50.0	ORB27060
	AVGDA = TDA / 50.0	ORB27070
	AVGDE = TDE / 50.0	ORB27080
	AVGDMM = TDMM / 50.0	ORB27090
	AVGDMA = TDMA / 50.0	ORB27100
	AVGLAN = TDLAN / 50.0	ORB27110
	AVGDH = TDH / 50.0	ORB27120
	AVGDAP = TDAP / 50.0	ORB27130
		ORB27140
		ORB27150
*	CALCULATE RADIUS'S AND VELOCITIES	ORB27160
	ENR = ((V**2)/2) - (MU/R)	ORB27170
	RP = A*(1 - E)	ORB27180
	RA = A*(1 + E)	ORB27190
	VP = SQRT(2*(ENR + (MU/RP)))	ORB27200
	VA = SQRT(2*(ENR + (MU/RA)))	ORB27210
		ORB27220
		ORB27230
*	SET DISSPLA	ORB27240
	CALL RESET(3HALL)	ORB27250
	CALL SCMPLN	ORB27260
	CALL PHYSOR(0.0,0.0)	ORB27270
	CALL AREA2D(8.5,4.0)	ORB27280
		ORB27290
*	PRINT DATA	ORB27300
	CALL MESSAG('I = \$',100,0.25,3.67)	ORB27310
	CALL REALNO(DI,3,'ABUT','ABUT')	ORB27320
	CALL MESSAG(' DEG. \$',100,'ABUT','ABUT')	ORB27330
	CALL MESSAG(' A = \$',100,'ABUT','ABUT')	ORB27340
	CALL REALNO(A,1,'ABUT','ABUT')	ORB27350
	CALL MESSAG(' KM\$ ',100,'ABUT','ABUT')	ORB27360

CALL MESSAG(' E = \$', 100, 'ABUT', 'ABUT')	ORB27370
CALL REALNO(E, 3, 'ABUT', 'ABUT')	ORB27380
CALL MESSAG(' PER = \$', 100, 'ABUT', 'ABUT')	ORB27390
CALL REALNO(PERH, 2, 'ABUT', 'ABUT')	ORB27400
CALL MESSAG(' HOURS\$', 100, 'ABUT', 'ABUT')	ORB27410
	ORB27420
CALL MESSAG(' AVERAGE RATE OF CHANGE OF ELEMENTS PER SECOND \$',	ORB27430
+ 100, 1.0, 3.0)	ORB27440
	ORB27450
CALL MESSAG(' DI/DT = \$', 100, 0.25, 2.67)	ORB27460
CALL REALNO(AVGDI, -2, 'ABUT', 'ABUT')	ORB27470
CALL MESSAG(' DA/DT = \$', 100, 'ABUT', 'ABUT')	ORB27480
CALL REALNO(AVGDA, -2, 'ABUT', 'ABUT')	ORB27490
CALL MESSAG(' DE/DT = \$', 100, 'ABUT', 'ABUT')	ORB27500
CALL REALNO(AVGDE, -2, 'ABUT', 'ABUT')	ORB27510
	ORB27520
CALL MESSAG(' DMM/DT = \$', 100, 0.25, 2.33)	ORB27530
CALL REALNO(AVGDM, -2, 'ABUT', 'ABUT')	ORB27540
CALL MESSAG(' DMA/DT = \$', 100, 'ABUT', 'ABUT')	ORB27550
CALL REALNO(AVGDMA, -2, 'ABUT', 'ABUT')	ORB27560
CALL MESSAG(' DLN/DT = \$', 100, 'ABUT', 'ABUT')	ORB27570
CALL REALNO(AVGLN, -2, 'ABUT', 'ABUT')	ORB27580
	ORB27590
CALL MESSAG(' DH/DT = \$', 100, 0.25, 2.00)	ORB27600
CALL REALNO(AVGDH, -2, 'ABUT', 'ABUT')	ORB27610
CALL MESSAG(' DAP/DT = \$', 100, 'ABUT', 'ABUT')	ORB27620
CALL REALNO(AVGDA, -2, 'ABUT', 'ABUT')	ORB27630
	ORB27640
CALL MESSAG(' AVERAGE MAGNITUDE OF FORCES PER UNIT MASS (KM/S**2)	ORB27650
+ \$', 100, 1.0, 1.67)	ORB27660
	ORB27670
CALL MESSAG(' EARTH = \$', 100, 0.10, 1.33)	ORB27680
CALL REALNO(AVGFE, -1, 'ABUT', 'ABUT')	ORB27690
CALL MESSAG(' MOON = \$', 100, 'ABUT', 'ABUT')	ORB27700
CALL REALNO(AVGFM, -1, 'ABUT', 'ABUT')	ORB27710
CALL MESSAG(' SUN = \$', 100, 'ABUT', 'ABUT')	ORB27720
CALL REALNO(AVGFS, -1, 'ABUT', 'ABUT')	ORB27730
CALL MESSAG(' DRAG = \$', 100, 'ABUT', 'ABUT')	ORB27740
CALL REALNO(AVGFD, -1, 'ABUT', 'ABUT')	ORB27750
	ORB27760
CALL MESSAG(' PERIGEE\$', 100, 2.75, 1.0)	ORB27770
CALL MESSAG(' Apogee\$', 100, 'ABUT', 'ABUT')	ORB27780
	ORB27790
CALL MESSAG(' RADIUS (KM)\$', 100, 0.25, 0.67)	ORB27800
CALL MESSAG(' RP = \$', 100, 2.75, 0.67)	ORB27810
CALL REALNO(RP, 1, 'ABUT', 'ABUT')	ORB27820
CALL MESSAG(' \$', 100, 'ABUT', 'ABUT')	ORB27830
CALL MESSAG(' RA = \$', 100, 'ABUT', 'ABUT')	ORB27840
CALL REALNO(RA, 1, 'ABUT', 'ABUT')	ORB27850
	ORB27860
CALL MESSAG(' VELOCITY (KM/SEC)\$', 100, 0.25, 0.33)	ORB27870
CALL MESSAG(' VP = \$', 100, 2.75, 0.33)	ORB27880
CALL REALNO(VP, 2, 'ABUT', 'ABUT')	ORB27890
CALL MESSAG(' \$', 100, 'ABUT', 'ABUT')	ORB27900
CALL MESSAG(' VA = \$', 100, 'ABUT', 'ABUT')	ORB27910
CALL REALNO(VA, 2, 'ABUT', 'ABUT')	ORB27920

CALL RESET('COMPLY')
CALL ENDGR(0)
RETURN
END

ORB27930
ORB27940
ORB27950
ORB27960
ORB27970
ORB27980

APPENDIX B. COORDINATE SYSTEMS

A. 'IJK': GEOCENTRIC - EQUATORIAL

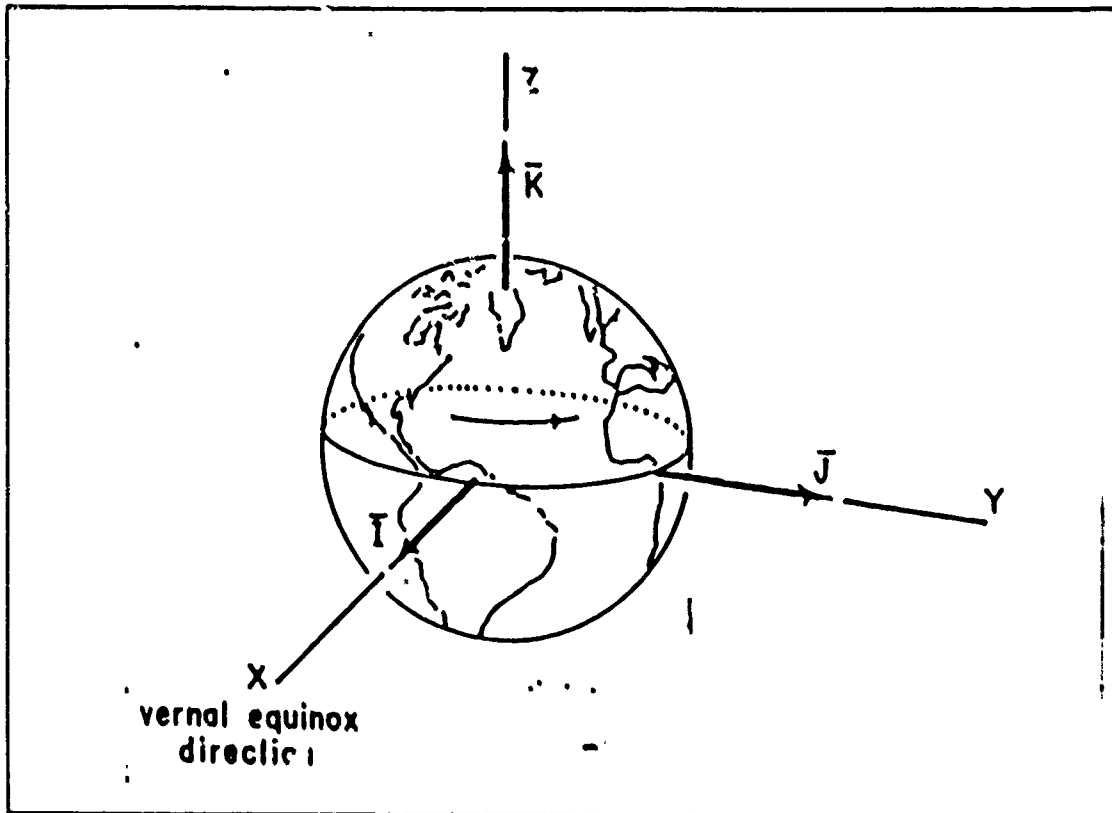


Figure 3. Geocentric-equatorial coordinate system

The geocentric-equatorial system as seen in Figure 3 has its origin at the earth's center. The fundamental plane is in the equator and the positive X-axis points in the vernal equinox direction. The Z-axis points in the direction of the north pole. This system is not fixed to the earth and turning with it; rather, the geocentric-equatorial frame is nonrotating with respect to the stars (except for precession of the equinoxes) and the earth turns relative to it. Unit vectors, \bar{I} , \bar{J} , and \bar{K} shown in Figure 3, lie along the X, Y, and Z respectively. [Ref. 1: p.55]

B. 'PQW': PERIFOCAL

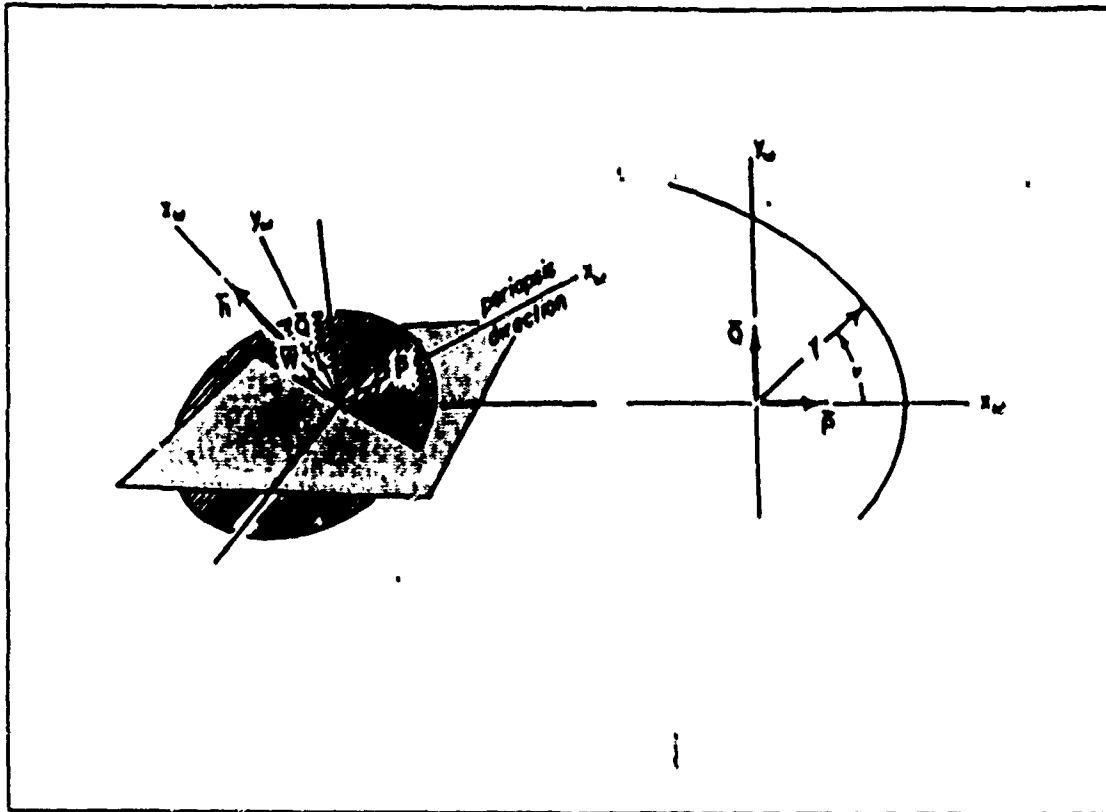


Figure 4. Perifocal coordinate system

The perifocal coordinate system has its fundamental plane in the plane of the satellite's orbit as seen in Figure 4. The coordinate axes are named, X_p , Y_p and Z_p . The X_p axis points toward the perigee; the Y_p axis is rotated 90 degrees in the direction of orbital motion and lies in the orbital plane; the Z_p axis along \vec{h} completes the right-handed perifocal system. Unit vectors in the direction of X_p , Y_p and Z_p are called \vec{P} , \vec{Q} and \vec{W} respectively. [Ref. 1: p.57]

C. 'RSW': ORBITAL

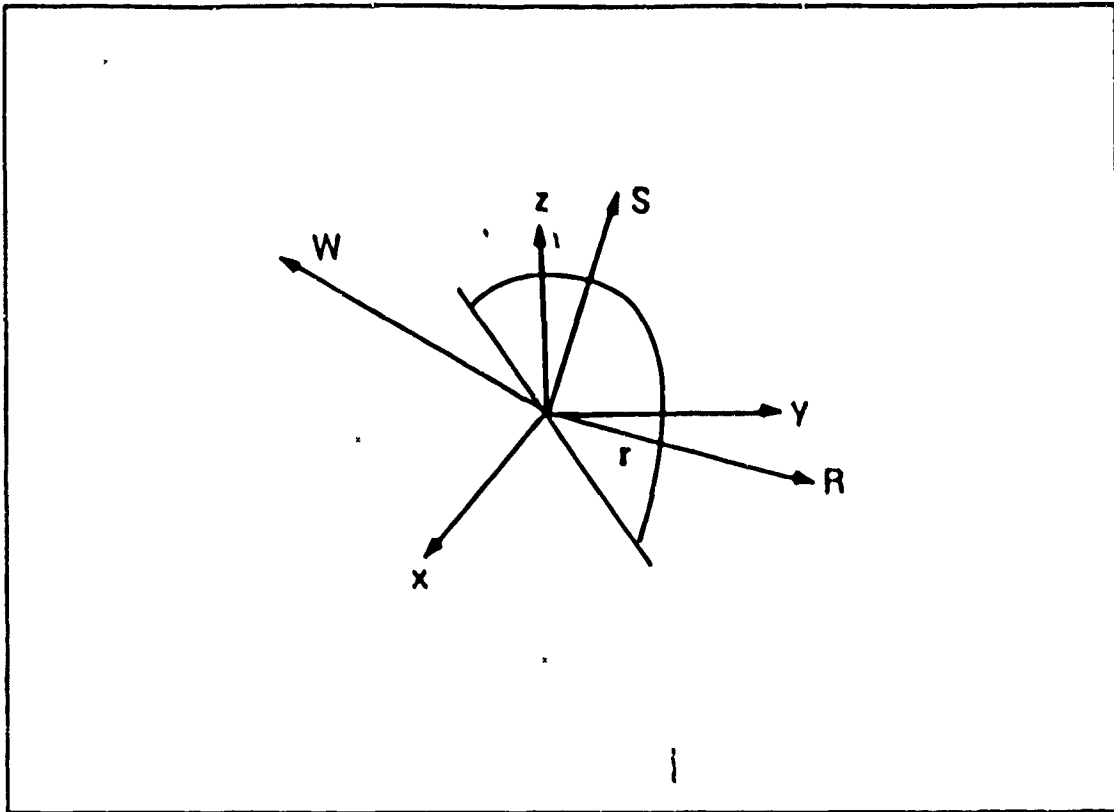


Figure 5. Orbital coordinate system

(Figure 9.4-1, Ref. 1)

The orbital coordinate system has its principle axis, R (unit vector r), along the instantaneous radius vector, r as seen in Figure 5. The axis S is rotated 90 degrees from R in the direction of increasing true anomaly. The third axis, W , is perpendicular to both R and S . Note that this coordinate system is simply rotated v_0 from the PQW perifocal system. [Ref. 1: p.398]

D. COORDINATE TRANSFORMATIONS

The coordinate transformations, for the previous coordinate systems, use angular rotations about the axis to evaluate the transformation matrix. The matrix elements r_{ij} are calculated, then applied to the old vector to get the vector in the new coordinate system. The following orbital elements are used:

Ω = longitude of ascending node

ω = argument of perigee

i = inclination

u_0 = argument of latitude

v_0 = true anomaly

The coordinate transformations follow [Ref. 1: p.74-83]

1. PQW to IJK

$$\begin{aligned} r_{11} &= \cos \Omega \cos \omega - \sin \Omega \sin \omega \cos i \\ r_{12} &= -\cos \Omega \sin \omega - \sin \Omega \cos \omega \cos i \\ r_{13} &= \sin \Omega \cos \omega \\ r_{21} &= \sin \Omega \cos \omega + \cos \Omega \sin \omega \cos i \\ r_{22} &= -\sin \Omega \sin \omega + \cos \Omega \cos \omega \cos i \\ r_{23} &= -\cos \Omega \sin i \\ r_{31} &= \sin \omega \sin i \\ r_{32} &= \cos \omega \sin i \\ r_{33} &= \cos i \\ \vec{I} &= r_{11}\vec{P} + r_{12}\vec{Q} + r_{13}\vec{W} \\ \vec{J} &= r_{21}\vec{P} + r_{22}\vec{Q} + r_{23}\vec{W} \\ \vec{K} &= r_{31}\vec{P} + r_{32}\vec{Q} + r_{33}\vec{W} \end{aligned}$$

2. IJK to PQW (inverse of #1)

$$\begin{aligned} \vec{P} &= r_{11}\vec{I} + r_{21}\vec{J} + r_{31}\vec{K} \\ \vec{Q} &= r_{12}\vec{I} + r_{22}\vec{J} + r_{32}\vec{K} \\ \vec{W} &= r_{13}\vec{I} + r_{23}\vec{J} + r_{33}\vec{K} \end{aligned}$$

3. IJK to RSW

$$\begin{aligned} r_{11} &= \cos \Omega \cos u_0 - \sin \Omega \sin u_0 \cos i \\ r_{12} &= \sin \Omega \cos u_0 + \sin u_0 \cos \Omega \cos i \\ r_{13} &= \sin i \sin u_0 \\ r_{21} &= -\cos \Omega \sin u_0 - \sin \Omega \cos u_0 \cos i \\ r_{22} &= -\sin \Omega \sin u_0 + \cos \Omega \cos u_0 \cos i \\ r_{23} &= \cos u_0 \sin i \\ r_{31} &= \sin \Omega \sin i \\ r_{32} &= -\cos \Omega \sin i \\ r_{33} &= \cos i \\ \vec{R} &= r_{11}\vec{I} + r_{12}\vec{J} + r_{13}\vec{K} \\ \vec{S} &= r_{21}\vec{I} + r_{22}\vec{J} + r_{23}\vec{K} \\ \vec{W} &= r_{31}\vec{I} + r_{32}\vec{J} + r_{33}\vec{K} \end{aligned}$$

4. RSW to IJK (inverse of #3)

$$\vec{I} = r_{11}\vec{R} + r_{21}\vec{S} + r_{31}\vec{H}$$

$$\vec{J} = r_{12}\vec{R} + r_{22}\vec{S} + r_{32}\vec{H}$$

$$\vec{K} = r_{13}\vec{R} + r_{23}\vec{S} + r_{33}\vec{H}$$

5. PQW to RSW

$$r_{11} = \cos v_0$$

$$r_{12} = \sin v_0$$

$$r_{13} = 0.0$$

$$r_{21} = -\sin v_0$$

$$r_{22} = \cos v_0$$

$$r_{23} = 0.0$$

$$r_{31} = 0.0$$

$$r_{32} = 0.0$$

$$r_{33} = 1.0$$

$$\vec{R} = r_{11}\vec{P} + r_{12}\vec{Q} + r_{13}\vec{H}$$

$$\vec{S} = r_{21}\vec{P} + r_{22}\vec{Q} + r_{23}\vec{H}$$

$$\vec{H} = r_{31}\vec{P} + r_{32}\vec{Q} + r_{33}\vec{H}$$

6. RSW to PQW (inverse of #5)

$$\vec{P} = r_{11}\vec{R} + r_{21}\vec{S} + r_{31}\vec{H}$$

$$\vec{Q} = r_{12}\vec{R} + r_{22}\vec{S} + r_{32}\vec{H}$$

$$\vec{H} = r_{13}\vec{R} + r_{23}\vec{S} + r_{33}\vec{H}$$

APPENDIX C. ORBITAL ELEMENTS

The user is assumed to be studying orbital mechanics and should understand the orbital elements and how to calculate them. A brief description of the elements and the equations used to calculate the elements follow. For a detailed explanation of the elements and the equations to calculate them refer to Chapters 1 and 2 of reference 1. Figure 6 on page 83 shows the orbital elements in the Geocentric-Equatorial and perifocal coordinate system.

1. Angular Momentum (h):

The specific angular momentum is a constant of the motion of the satellite, defined as $\vec{h} = \vec{r} \times \vec{v}$.

$$\vec{h} = \vec{r} \times \vec{v} = h_i \vec{I} + h_j \vec{J} + h_k \vec{K}$$

$$h_i = r_j v_k - r_k v_j$$

$$h_j = r_k v_i - r_i v_k$$

$$h_k = r_i v_j - r_j v_i$$

$$h = \sqrt{h_i^2 + h_j^2 + h_k^2}$$

2. Node Vector (n):

The node vector is a vector pointing along the line of nodes in the direction of the ascending node.

$$\vec{n} = \vec{K} \times \vec{h} = -h_j \vec{I} + h_i \vec{J}$$

$$n = \sqrt{h_j^2 + h_i^2}$$

3. Semi-latus rectum (p):

The semi-latus rectum is a geometric constant of the conic section.

$$p = \frac{h^2}{\mu}$$

4. Eccentricity (e):

The eccentricity is a constant defining the shape of the conic orbit.

$$\vec{e} = \frac{1}{\mu} \left[(v^2 - \frac{\mu}{r}) \vec{r} - (\vec{r} \cdot \vec{v}) \vec{v} \right]$$

$$e = |\vec{e}|$$

5. Semi-major axis (a):

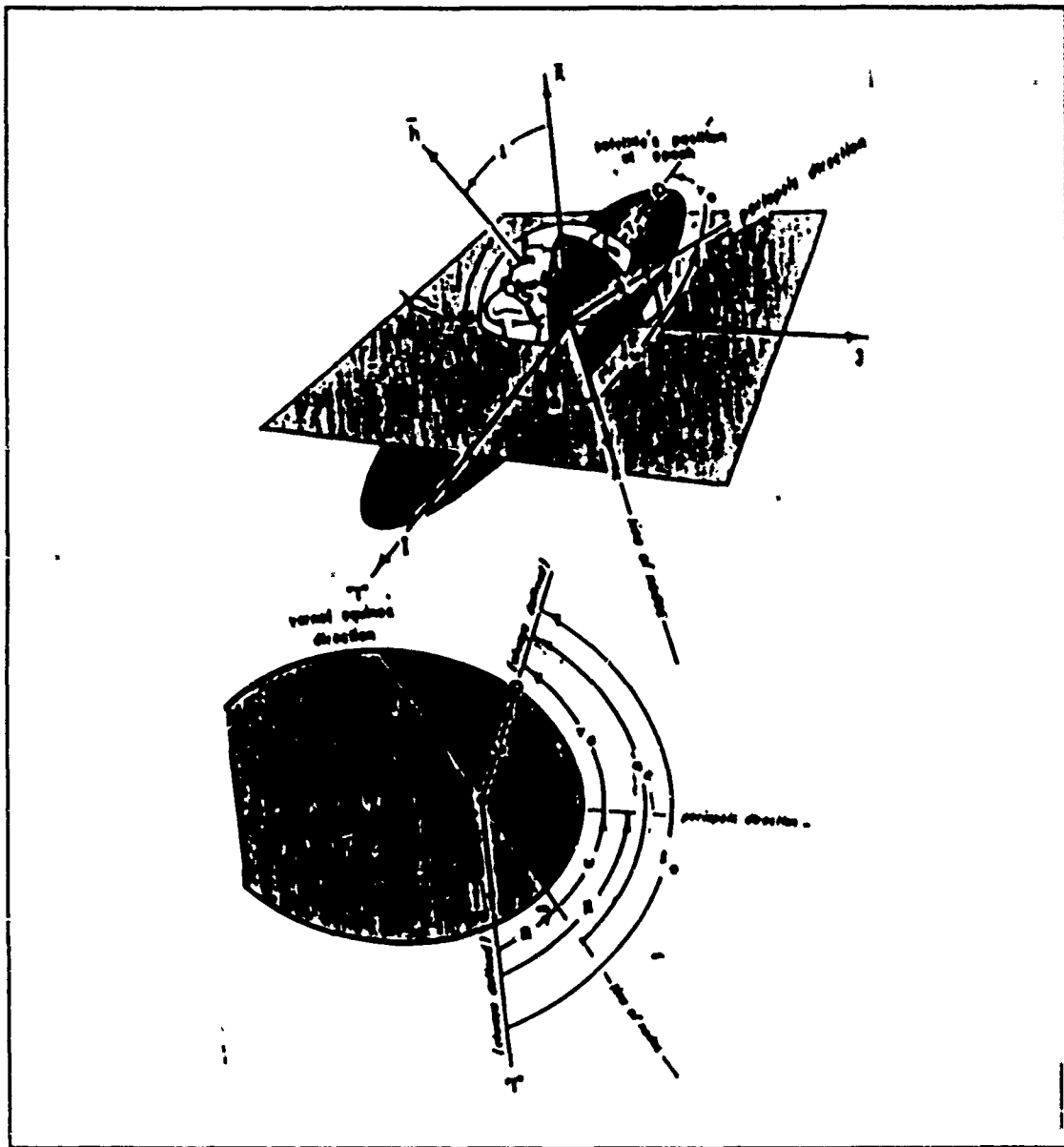


Figure 6. Orbital elements

The semi-major axis is a constant defining the size of the orbit.

$$a = \frac{(1 - e^2)}{f}$$

6. Inclination (i):

The inclination is the angle between the 'K' unit vector in the 'IJK' system and the angular momentum vector, 'h'.

$$i = \cos^{-1} \left(\frac{\bar{h} \cdot \bar{K}}{h} \right) = \cos^{-1} \left(\frac{h_z}{h} \right)$$

7. Longitude of ascending node (Ω):

The longitude of the ascending node is the angle in the fundamental plane, between the 'I' unit vector and the point where the satellite crosses through the fundamental plane in a northerly direction (ascending node) measured counter-clockwise when viewed from the north side of the fundamental plane.

$$\Omega = \cos^{-1} \left(\frac{n_z}{n} \right)$$

8. Argument of perigee (ω):

The argument of perigee is the angle in the plane of the satellite's orbit, between the ascending node and the perigee point, measured in the direction of the satellite's motion.

$$\omega = \cos^{-1} \left(\frac{\bar{n} \cdot \bar{e}}{ne} \right) = \cos^{-1} \frac{(n_1 e_1 + n_2 e_2)}{ne}$$

9. True anomaly at epoch (v_0):

The true anomaly at epoch is the angle in the plane of the satellite's orbit, between perigee and the position of the satellite at a particular time, t_0 , called the "epoch".

$$v_0 = \cos^{-1} \left(\frac{\bar{e} \cdot \bar{r}}{er} \right)$$

10. Argument of latitude (u):

The argument of latitude is the angle in the plane of the orbit, between the ascending node and the radius vector to the satellite at time t_0 .

$$u_0 = \cos^{-1} \left(\frac{\bar{n} \cdot \bar{r}}{nr} \right)$$

11. Longitude of perigee (Π):

The longitude of perigee is the angle from 'I' to perigee measured eastward to the ascending node and then in the orbital plane to perigee.

$$\Pi = \Omega + \omega$$

12. True longitude at epoch (l_0):

The true longitude at epoch is the angle between 'I' and r_0 (the radius vector to the satellite at t_0 measured eastward to the ascending node and then in the orbital plane to r_0).

$$l_0 = \omega + \Omega + v_0$$

13. Period (per):

The period is the time the for the satellite to complete one orbit.

$$Per = 2 \frac{\sqrt{a^3}}{\mu}$$

14. Eccentric anomaly (EA):

The eccentric anomaly is the angle between the perigee and a position on an auxiliary circle circumscribed about the ellipse where a perpendicular line to the major axis has been extended from the epoch location of the satellite to the auxiliary circle.

$$EA = \cos^{-1} \frac{e + \cos(v)}{1 + e \cos(v)}$$

15. Mean motion (n'):

The mean motion is defined below:

$$n' = \sqrt{\frac{\mu}{a^3}}$$

16. Mean anomaly (MA):

The mean anomaly is defined below:

$$MA = n'(t - T) = EA - e \sin(EA)$$

17. Time of flight (TF):

The time of flight is the elapsed time from when the satellite was at perigee to the current epoch.

$$(t - T) = \sqrt{\frac{a^3}{\mu}} (EA - e \sin(EA))$$

APPENDIX D. SAMPLE ORBITS

To demonstrate the capabilities of the program, a variety of orbital plots will follow:

1. Low earth orbit (LEO).

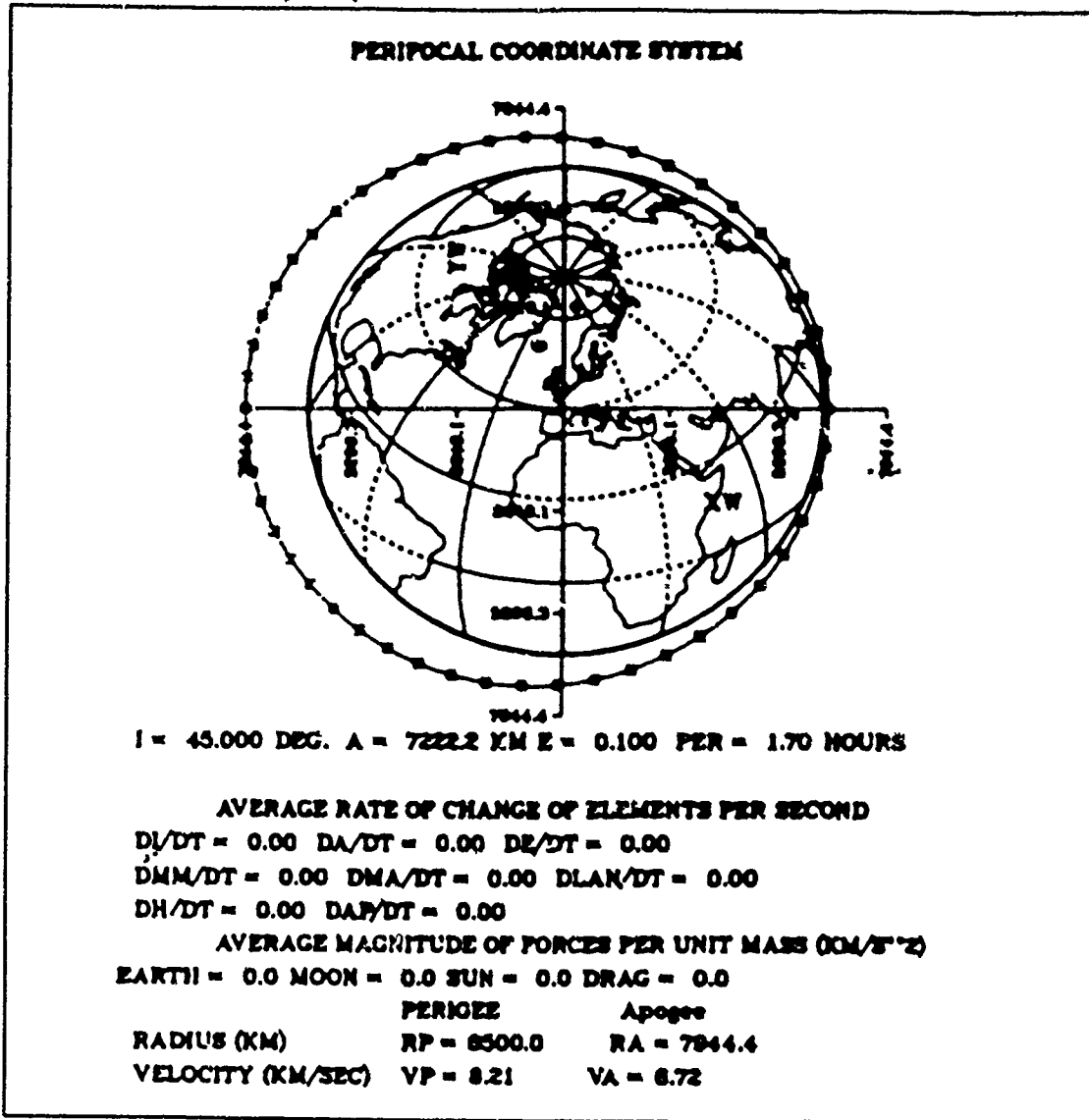


Figure 7. Unperturbed Low Earth Orbit (LEO)

Figure 7 shows the perifocal plot of a satellite in an unperturbed low earth orbit (LEO). The initial parameters of the orbit were entered as follows:
 radius of perigee (RP) = 6500 km
 eccentricity (e) = 0.1
 inclination (i) = 45 degrees.

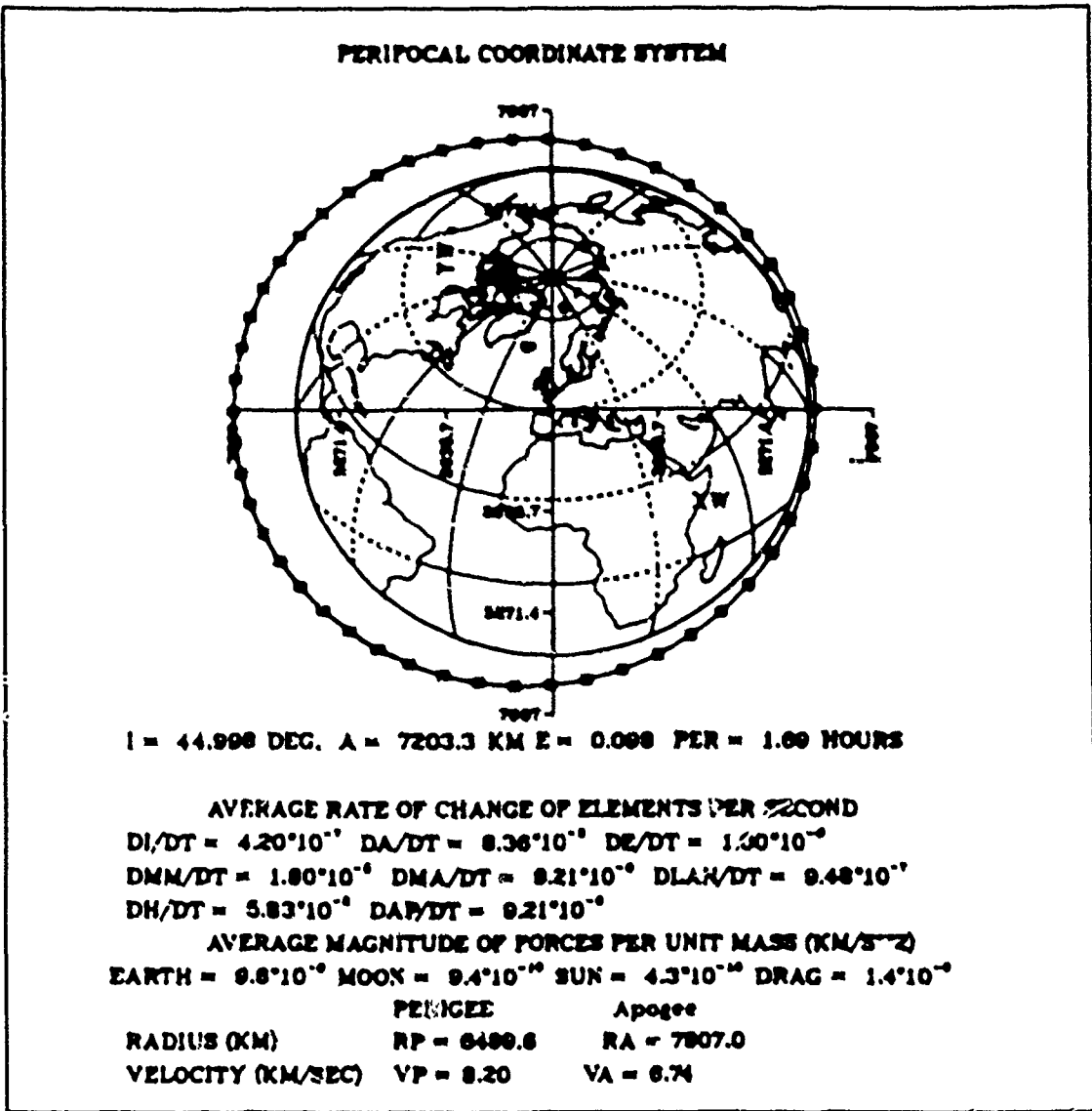


Figure 8. Perturbed Low Earth Orbit (LEO)

With perturbing forces applied to the previous LEO, the drag force will be the dominate perturbing force. The drag will act as a negative velocity change applied in the area of perigee. with the result of decreasing the semi-major axis length, this in effect will decrease the eccentricity of the orbit, as can be seen by comparing the orbital data of the unperturbed LEO in Figure 7 on page S6 with the orbital data of the perturbed LEO in Figure 8.

2. Circular orbit.

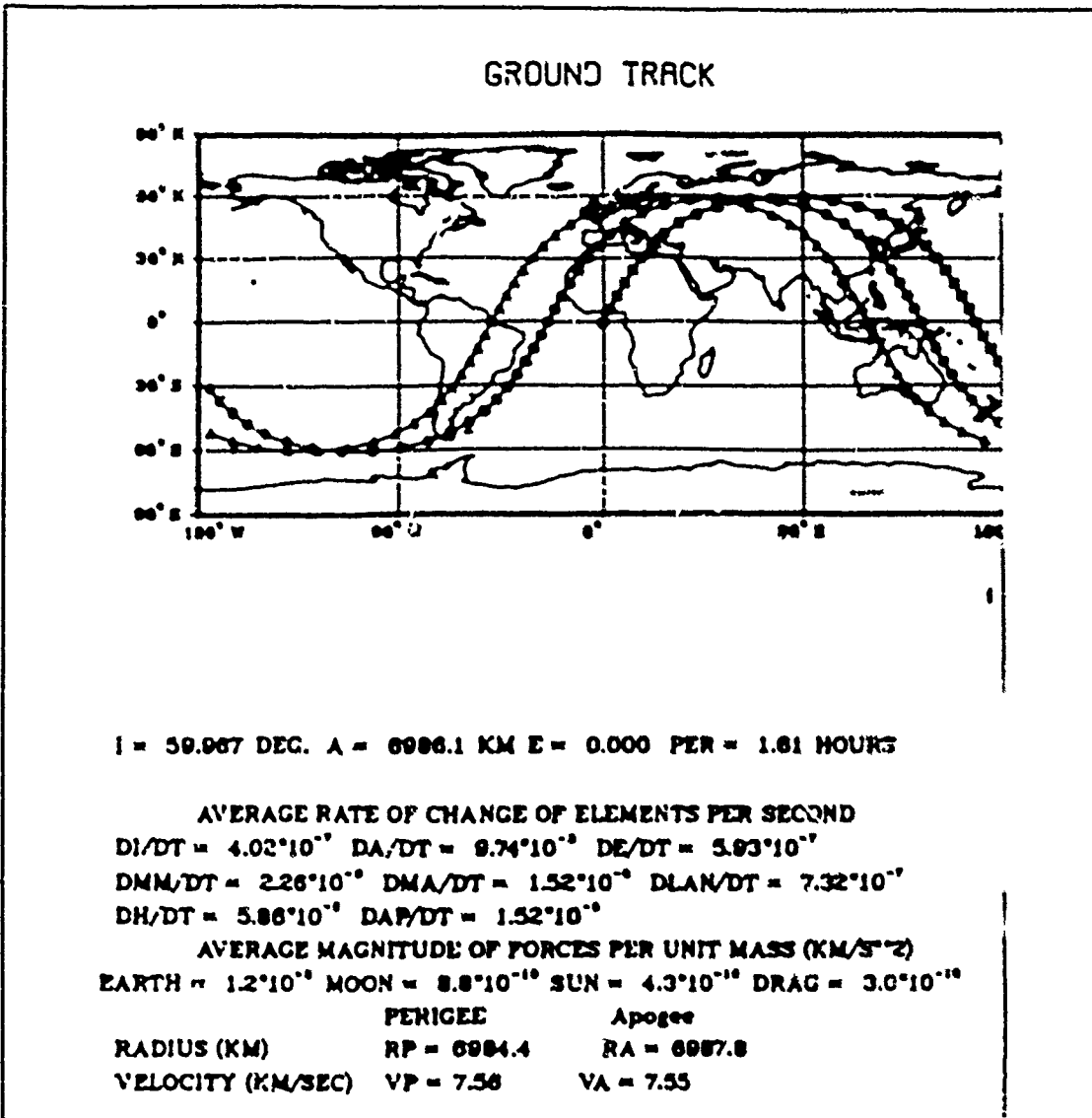


Figure 9. Circular Orbit

An example of the plot of the ground track of a sequence of three 60 degree inclined perturbed circular orbits with a radius of 7000 km is shown in Figure 9. The sequence of orbits displays the precession of the orbit around the earth.

3. Transfer orbit.

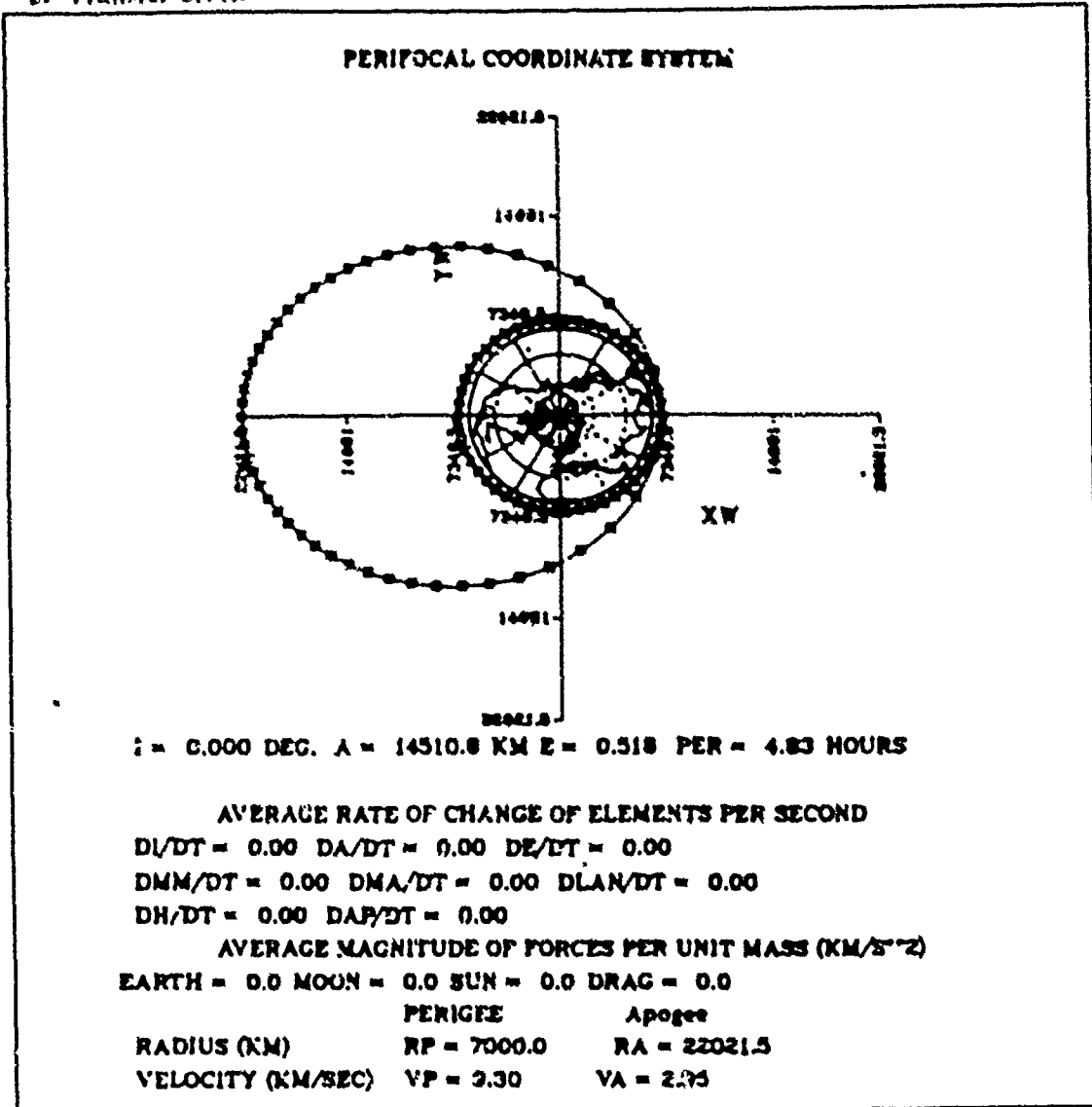


Figure 10. Transfer Orbit

The transfer orbit between a circular, equatorial LEO and a molniya orbit (high eccentric orbit) is shown in Figure 10. A velocity increase of 1.75 km/s was applied at the perigee to simulate a perigee kick to boost the satellite into the molniya orbit. A similar velocity change could then be applied at apogee to create a high altitude circular orbit, or a negative velocity change applied at perigee could be used to bring the satellite back to a LEO.

4. Geosynchronous orbit

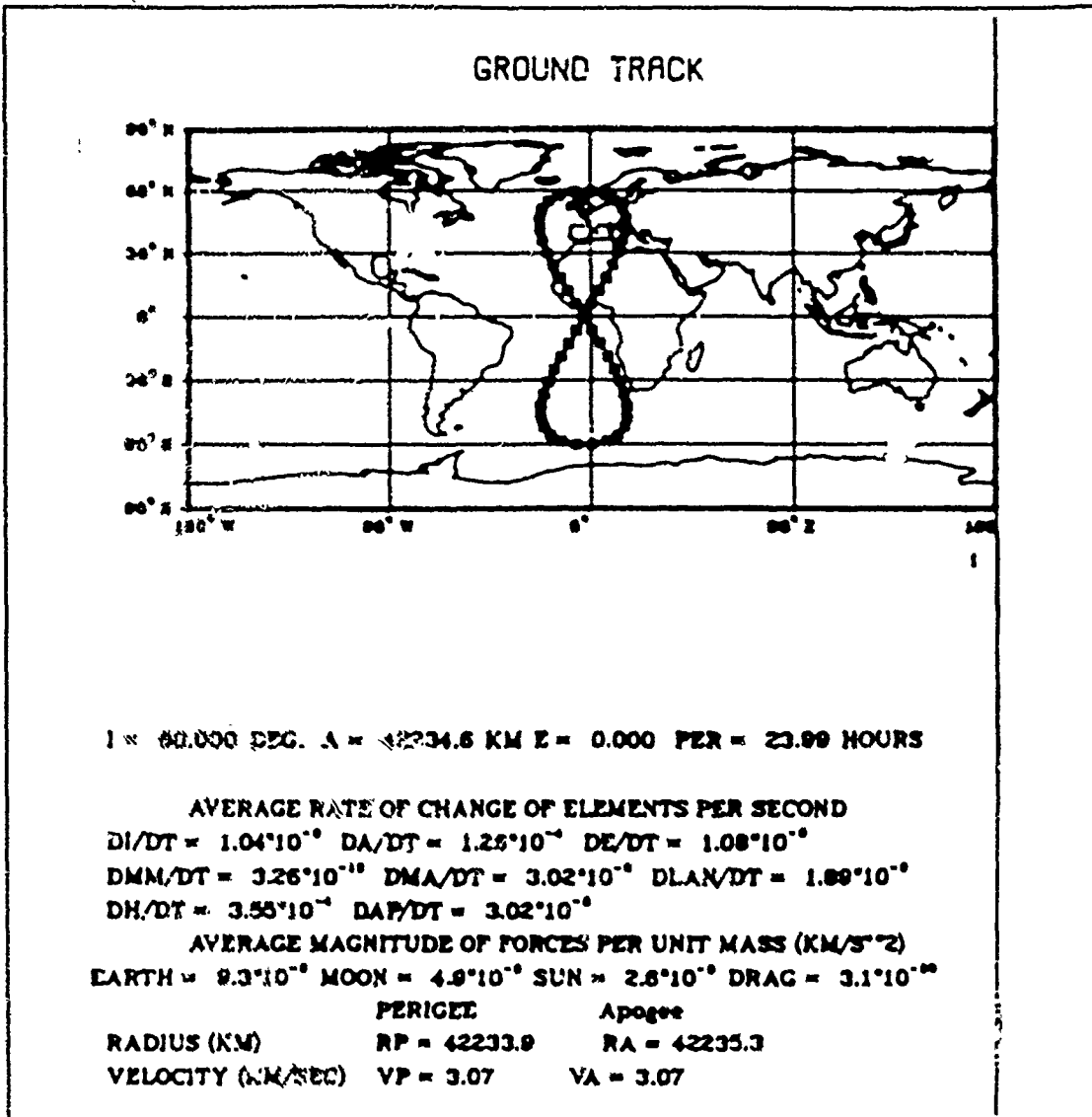


Figure 11. Geosynchronous Orbit

The ground track of a perturbed geosynchronous orbit inclined 60 degrees is shown in Figure 11. The orbit displays the figure eight typical with inclined geosynchronous orbits.

LIST OF REFERENCES

1. Bate, R.R., Mueller, D.D., and White, J.E., *Fundamentals of Astrodynamics*, Dover Publications, Inc., 1971.
2. Martin Marietta Corporation, Space Systems Division, *Orbital Flight Handbook*, volume 1, 1963.
3. Agrawal, B.N., *Design of Geosynchronous Spacecraft*, Prentice-Hall, Inc., 1968.
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