

APPENDIX

**MANUFACTURING METHODS AND TECHNOLOGY  
(MANTECH) PROGRAM: MANUFACTURING TECHNIQUES  
FOR A COMPOSITE MAIN ROTOR BLADE FOR THE  
ADVANCED ATTACK HELICOPTER - APPENDICES**

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July 1982

FINAL REPORT

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This manufacturing methods and technology program refined the design for a composite main rotor blade (CMRB) for the AH-64A advanced attack helicopter, perfected the fabrication technology for manufacturing it by wet filament winding process, and demonstrated it through laboratory tests and whirlstand tests. The CMRB replaces the equivalent metal main rotor blade with a weight saving of 24 pounds and a unit production cost saving of \$194,300 per shipset. Ballistic tolerance against 23mm HEI-T was		

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demonstrated, and satisfactory erosion protection and lightning protection methods were incorporated. Flight test information will be added in a later revision of this report.

This volume contains Appendices that pertain to the basic final report.



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APPENDIX A

STATIC STRESS ANALYSIS OF THE COMPOSITE MAIN ROTOR  
BLADE FOR THE AH-64A HELICOPTER



REPORT TITLE Static Stress Analysis for the YAH-64 CMRB		REPORT NO. CMRB 79-005
PREPARED BY APC	3/25/82	CHECKED BY
SUBJECT YAH-64 CMRB Static Analysis		MODEL NO YAH-64

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REPORT TITLE	Static Stress Analysis for the YAH-64 CMRB	REPORT NO	CMRB 79-005
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SUBJECT	YAH-64 CMRB		
<u>REFERENCES</u>			
1. CMRB-79-004 Basic Loads Report for the Composite Main Rotor Blade for the YAH-64 Advanced Attack Helicopter 1 June 1979 Revised July 1979 Revised March 1982			
2. Structural Test Report for the CMRB YAH-64/AAH Feb. 1982.			
3. CMRB 79-041 Safety of Flight Review Airworthiness Substantiation Document Composite Main Rotor Blade for the YAH-64/AAH May 1980, Vol. I and II			

REPORT TITLE Static Analysis for the YAH-64 CMRB		REPORT NO CMRB-79-005
PREPARED BY APC 3-26-82	CHECKED BY	MODEL NO YAH-64
SUBJECT YAH-64 CMRB		

### INTRODUCTION

This appendix contains the revised static and fail safe stress analysis of the YAH-64 CMRB.

Based on this analysis, there will be no failure at ultimate load (1.5x limit) and negligible permanent set under limit loads. In addition, with a critical structure element failed (i.e., one lug in four (4) lug joint) the CMRB will be capable of taking limit loads as ultimate without failure. Permanent set is allowed under these conditions.

The CMRB static loads are given in Section 20 starting on Pg. A20.01. Centrifugal Force vs. Blade station at various rotor speeds along with blade moments are listed. Loads are from Reference 1.

Revised section properties are given on Pg. A30.02 in Table 30-1. A plot of section properties is given on Pg. A30.03.

A summary of all testing done on the CMRB, both the original design and the re-designed blade is shown on pg. A10.04. See also References 2 and 3. Redesign consists of the following:

1. .048" graphite inner skin; was .010" kevlar.
2. Honeycomb supporting the trailing edge skin and swept tip; was Kevlar tubes and Kevlar ribs respectively.
3. .075 graphite channel that runs the length of the blade; was .048" Kevlar web.
4. Double flange bushing (spool) at the attach lub; was a single flange bushing.

The above changes increased the blade strength, however all static testing was done with specimens which were of the original design.

REPORT TITLE Static Analysis for the YAH-64 CMRB		REPORT NO. CMRB-79-005
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SUBJECT YAH-64 CMRB		MODEL NO. YAH-64

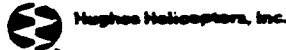
INTRODUCTION - (Cont'd)

Pg. A40.01 shows the cross section of the lugs with double flange bushings (spools) now being used on the CMRB to contain the fibers because they tend to spread or flatten out when loaded. This design also allows the fibers to be wound tightly around the bushing resulting in 10% more fibers being used in the make-up of the lug versus the single flange design. This results in a lug of greater strength.

Pg. A40.02 shows the maximum lug load reach during test (specimen had single flange lug bushings). The lug did not fail (specimen club end failed, Ref. 2) and calculations show the lug can withstand a load 40% higher than ultimate. The test substantiated the attach lugs and root portion of the blade. Analysis for the blade's constant section is shown on Pgs. A50.01 and A50.02.

The tip section of the blade has been structurally substantiated by static test (see Ref. 2). Loading of the tip is shown on Pg. A60.01. The blade tip withstood 356% of limit load.

Structural integrity has been established by analysis and test. For analysis before test see the main body of the report.



A10.04  
CMRB 79-005

### SUMMARY OF TESTS RESULTS

This page presents the results of tests conducted on the Composite Main Rotor Blade for the YAH-64 Advanced Attack Helicopter. The tests were conducted at the Hughes Helicopters Inc. Structures Test Laboratory, Culver City, CA., between January 1980 and August 1981.

One each, Swept Tip specimens were subjected to Static, Ground-Air-Ground, and Fatigue loading. One each, Root-Midspan specimens were subjected to Static and Ground-Air-Ground loading. Five Root specimens were tested under fatigue loading.

Significant test results are as follows:

1. Swept Tip Static, GAG and Fatigue tests.
  - a. 100% radial limit load achieved on swept tip section without failure or permanent set.
  - b. 100% vertical limit load and ultimate load on aft tip weight box without failure or permanent set. 211% radial limit load achieved on swept tip assembly without failure.
  - c. 100% radial limit load achieved on fwd. and aft tip weight boxes without failure.
  - d. 108,000 cycles; representing eight times three GAG cycles per hour for a service life of 4500 hours achieved without failure.
  
2. Root-Midspan Static and GAG tests.
  - a. 100% radial limit load applied statically without yielding or permanent set. Failure at the club end occurred at 149% limit load.
  - b. 108,000 cycles, representing eight times three GAG cycles per hour for a service life of 4500 hours achieved without failure. Lug failed at 33,200 cycles of 125% GAG load.
  
3. Root Fatigue Tests
  - a. Tests conducted on specimens 1 and 2 were considered invalid due to overheating of the test specimen resulting from an excessive test cyclic load rate.
  - b. A premature failure of specimen No. 3 indicated insufficient fatigue strength of the blade attachment lugs as originally designed.
  - c. Specimen 4, which incorporated design configuration changes yielded greatly improved fatigue strength in the lug area although lateral expansion of the lugs was still present.
  - d. Specimen 5, with shimmed lugs which simulated the additional lateral restraint of the longo fibers obtainable from the future use of double flanged lug bushings showed no damage or lateral expansion of the lugs after 947,700 cycles at increased load levels. The last 50,400 cycles were obtained at the mean 1 hour load level. The required number of cycles at the 1 hour load level is 17,340. The root end of the blade could still support centrifugal force when the test was terminated due to increased deflections.

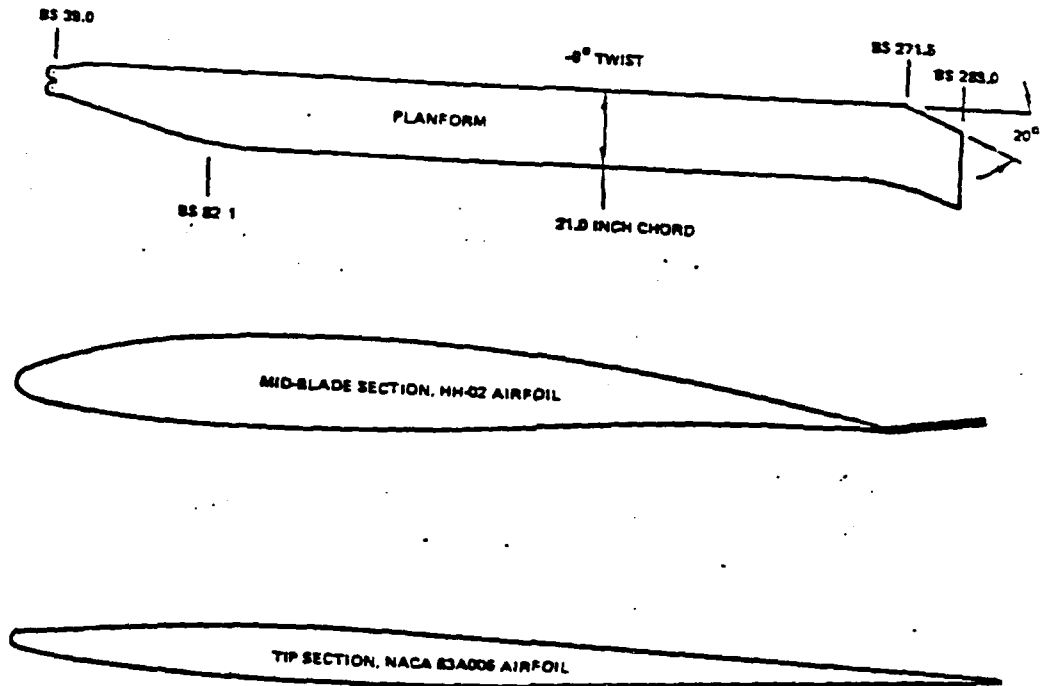
REPORT TITLE YAH-64 Static and Fatigue Analysis		REPORT NO. CMRB-79-005
PREPARED BY APC	3/9/82	CHECKED BY
SUBJECT YAH-64 CMRB		MODEL NO. YAH-64

MINIMUM MARGINS OF SAFETY

Station	Load Condition	Type of Stress	Margin of Safety
39 Attach Lugs	$n_z=3.5, V_f=180 \text{ Kn}$ RPM=289	Tension in Kevlar Windings	.40
191.7 Constant Section	$n_z=3.5, V_f=180 \text{ Kn}$ RPM=289	Compression in Kevlar spar longos in the constant section	.06
87 Constant Section	$n_z=3.5, V_f=180 \text{ Kn}$ RPM=289	Shear due to torsion in $+45^\circ$ layers of the constant section	.05
84 Constant Section	RPM = 0 Max Torque V=0 $n_z=1.0$	Compression in Kevlar spar longos after the T.E. longos have buckled	High
270 Blade Tip	RPM = 376 $V_f=150 \text{ Kn}$ $n_z=3.5$	Tension load applied to tip weight housings and blade tip	High

Hughes Helicopters

A15.02  
CMRB-79-005



YAH-64 CMRB Geometry

Figure 1

REPORT TITLE		REPORT NO
PREPARED BY	3/25/82	CHECKED BY
<u>APC</u>		
SUBJECT		MODEL NO
<u>YAH-64 CMRB</u>		<u>YAH-64</u>
CMRB-79-005		

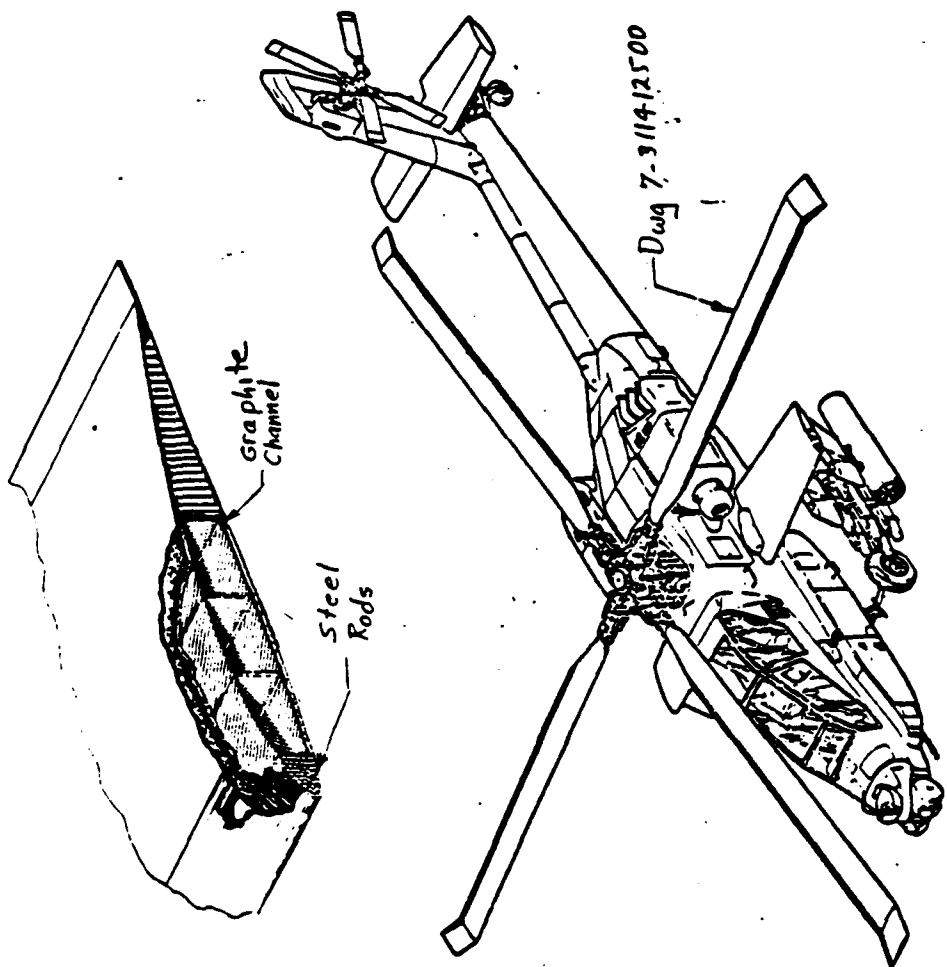


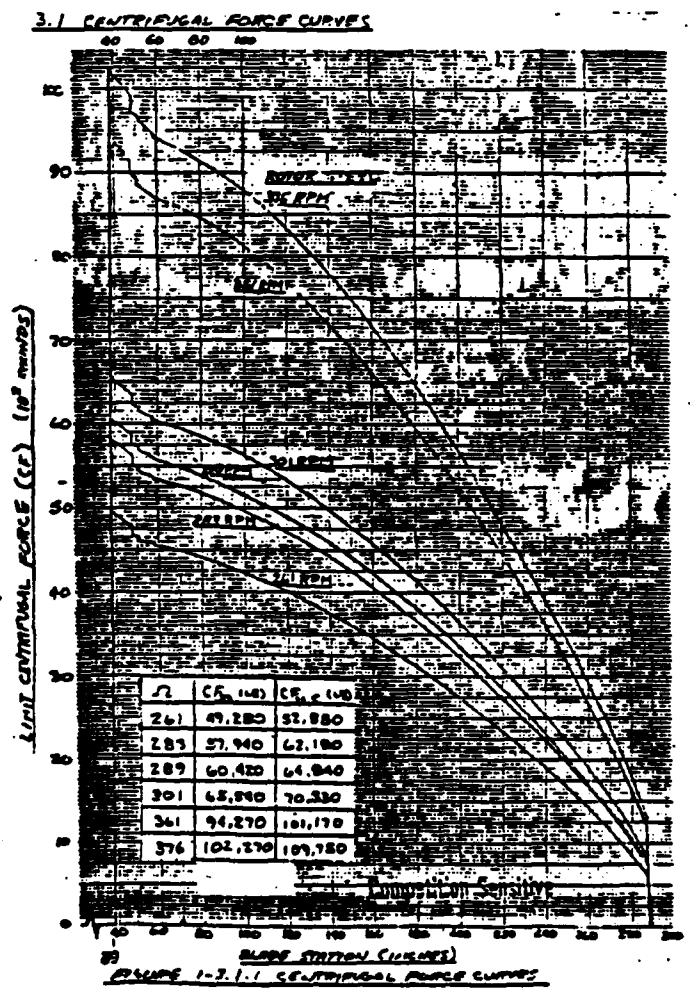
Figure 2

REPORT TITLE		REPORT NO.
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CMRB-79-005

YAH-69

CMRB Centrifugal Force





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SUBJECT			

CMRB loads

Main Rotor Blade Preliminary Limit Loads

Power On

$n_2 = 3.5$ ,  $V = 180$  kn, RPM = 289

r (in.)	$M_T$ (in-lb)		$M_C$ (in-lb)		$M_P$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	← N.A. →				-15000	42000
25.0	+8400	36400	← N.A. →			
34.5	+4400	49700	60000	60900	-15000	33000
44.5	-8800	55300	55900	79400	-12000	33000
59.5	-5000	48700	50000	106000	- 9000	32000
87.0	-3500	26300	37700	133000	- 8000	32000
121.9	-5500	23600	29100	149000	- 5600	32800
156.8	-6000	28300	19900	136000	- 4300	32000
191.7	-8000	42900	12400	97500	- 3500	32000
226.6	-4000	44000	6600	60100	- 2200	22000
256.0	+2000	25200	1200	22900	- 1700	10500
273.0	+4500	14800	300	8300	- 900	4300

NOTE. Lds in tables are from Ref 1

REPORT TITLE		REPORT NO. <u>CMRB-79-005</u>
PREPARED BY <u>HC</u>	<u>3/3/82</u>	CHECKED BY
SUBJECT		MODEL NO. <u>YAH-64</u>

## CMRB Loads

### Main Rotor Blade Preliminary Limit Loads

Power Off, (Limit Rotor Speed)

$n_z = 3.5, V = 150 \text{ kn, RPM} = 376$

r (in.)	$M_p$ (in-lb)		$M_c$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-11000	18000
25.0	- 3600	10200	N.A.		- 9100	14300
34.5	- 4000	13900	-29000	42700	- 7100	13500
44.5	- 1510	15400	-26600	55700	- 9100	14300
59.5	- 940	13600	-23800	74300	- 7100	13500
87.0	- 4000	7300	-18000	93300	- 5800	13400
121.9	- 7600	6600	-13900	104000	- 4200	13300
156.8	-11500	7900	- 9500	95300	- 3200	13500
191.7	-13100	12000	- 5900	68400	- 2900	13400
226.6	- 9300	12300	- 3100	42100	- 2600	9300
256.0	+ 6100	7000	- 570	16100	- 1600	4500
273.0	+ 2700	4100	- 140	5800	- 650	1900

REPORT TITLE		REPORT NO.
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SUBJECT		<u>YAH-64</u>

CMRB Loads

Main Rotor Blade Preliminary Limit Loads

Power Off

$n_2 = 3.5$ ,  $V = 150$  kn, RPM = 301

r (in.)	$M_F$ (in-lb)		$M_C$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-14000	23800
25.0	+8400	23700	N.A.			
34.5	+4400	32400	-25700	54400	-14000	18600
44.5	-8800	36000	-23900	71000	-11500	18900
59.5	-5000	31700	-21400	94800	-9100	17800
87.0	-3500	17100	-16100	119000	-7400	17700
121.9	-5500	15400	-12500	133000	-5400	17500
156.8	-6000	18400	-8500	122000	-4100	17800
191.7	-8000	27900	-5300	87200	-3700	17700
226.6	-4000	28600	-2800	53700	-3300	12300
256.0	+2000	16400	-500	20500	-2100	6000
273.0	+4500	9600	-130	7400	-800	2500



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SUBJECT		<i>YAH-64</i>

CMRB Loads

Main Rotor Blade Preliminary Limit Loads

Power Off, (Design Minimum Rotor Speed)

$n_2 = 3.3$ ,  $V = 150$  kn, RPM = 261

r (in.)	$M_y$ (in-lb)		$M_c$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-14000	30000
25.0	+8400	36400	N.A.			
34.5	+4400	49700	-23000	58000	-14000	23500
44.5	-8800	55300	-21400	72000	-11500	23700
59.5	-5000	48700	-19200	101000	- 9100	22400
87.0	-3500	26300	-14500	127000	- 7400	22100
121.9	-5500	23600	-11200	142000	- 5400	22000
156.8	-6000	28300	- 7600	130000	- 4100	22400
191.7	-8000	42900	- 4750	92900	- 3700	22300
226.6	-4000	44000	- 2500	57200	- 3300	15400
256.0	+2000	25200	- 460	21800	- 2100	7500
273.0	+4500	14800	- 115	7900	- 800	3100

REPORT TITLE		REPORT NO.
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SUBJECT		<u>YAH-64</u>

CMRB Loads

Main Rotor Blade Preliminary Limit Loads

Power On

$n_2 = 2.5$ ,  $V = 204$  kn, RPM = 289

r (in.)	$M_f$ (in-lb)		$M_c$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-14000	20900
25.0	- 820	29600	N.A.			
34.5	-11900	40500	60000	46300	-14000	17500
44.5	- 8600	45000	55900	60400	-11500	17700
59.5	- 6100	39600	50000	80600	- 9100	16700
87.0	- 9000	21400	37700	101000	- 7400	16600
121.9	- 7900	19200	29100	113000	- 5400	16400
156.8	- 6200	23000	19900	103000	- 4100	16700
191.7	- 8300	34900	12400	74100	- 3700	16700
226.6	- 5200	35800	6600	45700	- 3300	11500
256.0	0	20500	1200	17400	- 2100	5600
273.0	+ 1480	12000	300	6300	- 800	2300

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SUBJECT		<u>YAH-64</u>

CMRB Loads

Main Rotor Blade Preliminary Limit Loads

Power On, (Limit Rotor Speed)

$n_2 = 3.5, V = 180 \text{ kn, RPM} = 361$

r (in.)	$M_p$ (in-lb)		$M_c$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-14000	17000
25.0	-3600	15200	N.A.			
34.5	-4000	20800	34000	48700	-14000	13300
44.5	-1510	23100	31700	44300	-11500	13500
59.5	-940	20300	28300	59200	-9100	12700
87.0	-4000	11000	21400	74300	-7400	12600
121.9	-7600	9900	16500	83200	-5400	12500
156.8	-11500	11800	11300	75900	-4100	12700
191.7	-13100	17900	7000	54400	-3700	12600
226.6	-9300	18300	3700	33600	-3300	8800
256.0	+6100	10500	700	12800	-2100	4300
273.0	+2700	6200	200	4600	-800	1800



REPORT TITLE		REPORT NO.
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CMRB-79-005  
YAH-64

CMRB Loads

Main Rotor Blade Preliminary Limit Loads

(Zero Rotor Speed, Maximum Torque)

$n_2 = 1.0, V = 0 \text{ kn, RPM} = 0$

r (in.)	M <sub>p</sub> (in-lb)		M <sub>c</sub> (in-lb)		M <sub>T</sub> (in-lb)	
	Mean*	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	26500	Negligible	N.A.	Negligible	Negligible	Negligible
36.5	19600	↓	79900	↓	↓	↓
44.5	18100		74400			
59.5	16100		66600			
87.0	12660		50200			
121.85	8910		38800			
156.75	5780		26500			
191.65	3270		16500			
226.55	1390		8800			
256.0	320		1600			
273.0	40		400			

\* I<sub>g</sub> static droop moment with respect to a horizontal reference plane.

REPORT TITLE		REPORT NO. <u>CURB-79-001</u>
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SUBJECT		MODEL NO. <u>YAH-64</u>

SECTION PROPERTIES

Section properties are listed in Table 30-1 in this section.  $EI_c$ ,  $EI_f$  and  $GJ$  are shown graphically on page A30.03. On page A30.07 the shear flows due to a 1000 in-lb torque applied to the blade are shown. On page A30.08 is listed the test data from which the calculated torsional stiffness of the blade was verified.



REPORT TITLE		REPORT NO.
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### CMRB Section Properties

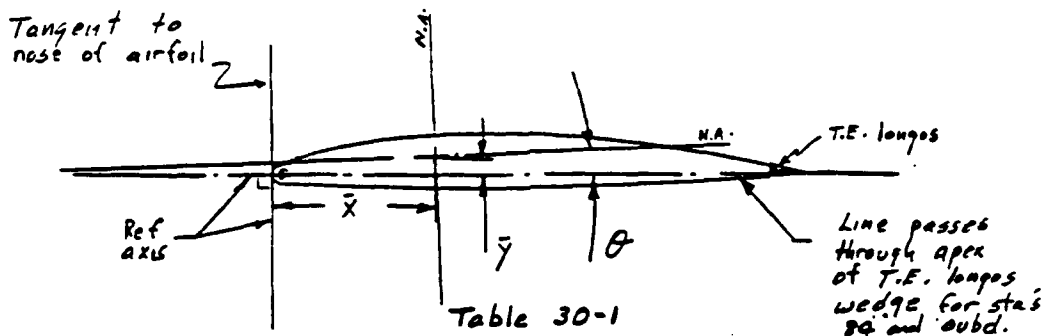
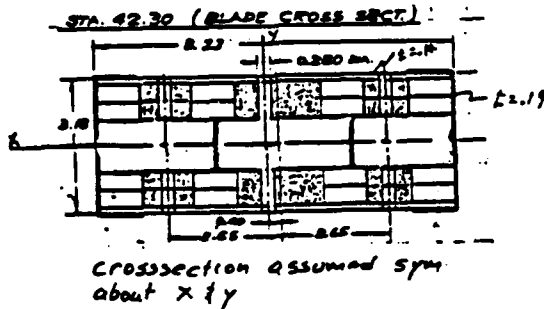


Table 30-1

Blade Sta	EA $\times 10^6$	E <sub>I</sub> F $\times 10^6$	E <sub>I</sub> c $\times 10^6$	GJ $\times 10^6$	$\bar{x}$ in	$\bar{y}$ in	$\theta$ deg
42	23.16	96	596.2	34	See below		0°
55	71.51	49.12	254.4	49.07	4.61	.35	1.66
65	53.04	29.51	297.5	30.49	4.28	.32	1.23
75	42.94	21	946.2	24.74	5.09	.30	.57
84	32.10	15.52	924.0	16.2	4.974	.30	.52
130	35	13.4	898		4.92		.49
160	33.98	12.7	290.72		4.86		.45
Trim Tabs start	175.5	23.98	290.72		4.86	.30	
020 Stl	201	34.39	483.49		5.04	.26	
Back-up strip	201	35.91	995.49		4.914		
260	35.91	13.4	995.49	16.2	4.914		

} 106 rods in N. wt  
} 68 rods in N. wt.

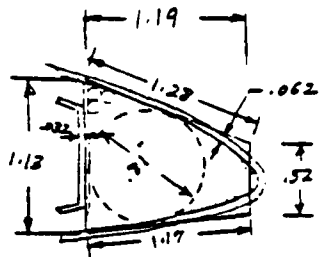
\*Tip wt housing starts at sta 260.





REPORT TITLE		REPORT NO.	
PREPARED BY <u>JPL</u>		CMRB-79-005	
CHECKED BY <u>7/13/79</u>		MODEL NO. <u>YAH-64</u>	
SUBJECT <u>YAH-64 CMRB</u>			

TELESCOPE STIFFNESS - STA 84



$NWt\ area = .8626\ in^2$   
 $Rod\ area = \left(\frac{.023}{2}\right)^2 \pi 68 = .464$   
 $V_f = \frac{.464}{.8626} = .54$   
 $V_m = \frac{.8626 - .464}{.8626} = .46$

Skin  
 $A_i = \frac{.52 + 1.13}{2} \times 1.19 = .982\ in^2$

$\frac{S}{t} = \frac{1.19 + .52 + 1.17}{.024} + \frac{1.13}{.032} = 120 + 35.3 = 155.3$

$G \frac{A F^2}{t/k} = \frac{4 \times .982^2}{155.3} \times 2.532 \times 10^6 = .063 \times 10^6$

Rods + Resin  
 $GJ = \frac{1}{2} \pi \times .405^4 \times .56 \times 10^6 = .024 \times 10^6$

Total GJ for Call 1

$(.063 + .024) \times 10^6 = \frac{4 \times .982^2}{(1.13 + 1.28 + .52 + 1.17)/k} \times 2.532 \times 10^6$

$k = .092 \quad \left(\frac{S}{t}\right) = (1.13 + 1.28 + .52 + 1.17) / .042 = 98$

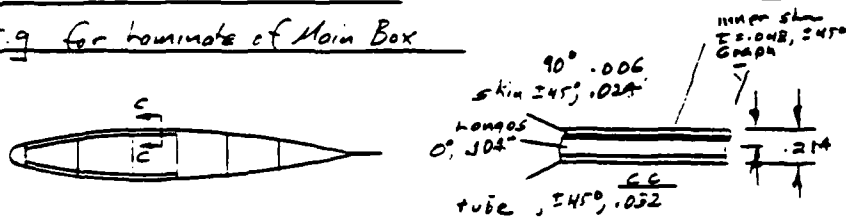
PHYSICAL MICROCHEMICAL PROPERTIES.

LM = ?	0.46
EM = ?	4.7 05
UM = ?	0.35
NF = ?	1.
FIBER NO.	1
VF = ?	0.54
EFL = ?	2.6 06
EFT = ?	2.6 06
F = ?	0.9
GF = ?	1.1 07
EL =	1690357.616
ET =	1168075.837
YLT =	3211397098
GLT =	556064.6481

REPORT TITLE		REPORT NO.
PREPARED BY	CHECKED BY	CARB-79-005
<u>JPC</u>	<u>7/3/79</u>	MODEL NO
SUBJECT		<u>YAH-64</u>

Torsion Stiffness - Sta 84

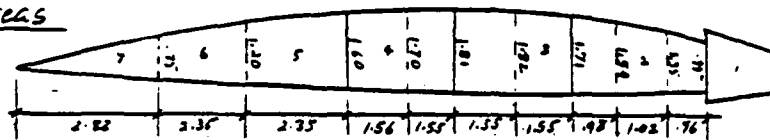
Slur C.G. for laminate of Main Box



$$\bar{Y} = \frac{.024 \times 2.532 \times 0.15 + .048 \times 4.421 \times .054 + .104 \times .2349 \times .13 + .032 \times 2.532 \times .118}{(.024 + .072) \times 2.532 + .104 \times .2349 + .048 \times 4.421}$$

$$\bar{Y} = .084$$

Cell Areas



$$A_1 = .982$$

$$A_2 = \frac{.99 + 1.35}{2} \times .96 + \frac{1.35 + 1.59}{2} \times 1.02 + \frac{1.59 + 1.71}{2} \times .97 = 1.123 + 1.499 + 1.617 = 4.24$$

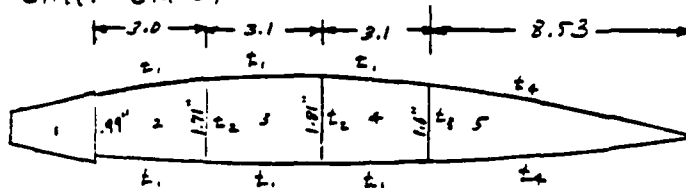
$$A_3 = \frac{1.71 + 1.82}{2} \times 1.55 + \frac{1.82 + 1.87}{2} \times 1.55 = 2.736 + 2.813 = 5.549$$

$$A_4 = \frac{1.31 + 1.70}{2} \times 1.55 + \frac{1.70 + 1.80}{2} \times 1.56 = 2.72 + 2.496 = 5.216$$

$$A_5 = \frac{1.60 + 1.20}{2} \times 2.35 + \frac{1.2 + .75}{2} \times 2.35 + \frac{.75 + 3.32}{2} = 7.02$$

REPORT TITLE		REPORT NO. <u>CMR3-79-005</u>
PREPARED BY <u>HC</u>	<u>11/19/81</u>	CHECKED BY
SUBJECT		MODEL NO. <u>YAH-64</u>

Torsional Stiff. Sta 84

Effective Skin Thickness

$$t_1 = .032 + \frac{.2349}{2.532} \times .104 + \frac{4.421}{2.532} \times .048 + .024 + .006 \frac{.229}{2.532} = .150$$

$$t_2 = .064 \quad , \quad t_3 = \frac{4.421}{2.532} \times .075 + .032 = .163 \quad , \quad t_4 = .0245$$

$$\left(\frac{S}{t}\right)_1 = 98$$

$$\left(\frac{S}{t}\right)_2 = \frac{6}{.15} + \frac{.99}{.042 + .032} + \frac{1.71}{.064} = 80.1$$

$$\left(\frac{S}{t}\right)_3 = \frac{6.2}{.15} + \frac{1.71 + 1.81}{.064} = 96.3$$

$$\left(\frac{S}{t}\right)_4 = \frac{1.81}{.064} + \frac{1.6}{.163} + \frac{6.2}{.15} = 79.4$$

$$\left(\frac{S}{t}\right)_5 = \frac{1.6}{.163} + \frac{2 \times 8.53}{.0254} = 682$$

$$\left(\frac{S}{t}\right)_{1,2} = \frac{.99}{.042 + .032} = 13.4$$

$$\left(\frac{S}{t}\right)_{2,3} = \frac{1.71}{.064} = 26.7$$

$$\left(\frac{S}{t}\right)_{3,4} = \frac{1.81}{.064} = 28.3$$

$$\left(\frac{S}{t}\right)_{4,5} = \frac{1.6}{.163} = 9.82$$

REPORT TITLE		REPORT NO.
PREPARED BY	CHECKED BY	<u>CMRB-79-005</u>
<u>JFF</u>	<u>11/17/81</u>	MODEL NO.
SUBJECT		<u>YAH-64</u>
<u>YAH-64 CMRB</u>		

Torsional Stiff Sta 84

$$\begin{bmatrix} 98 & -13.4 & 0 & 0 & 0 \\ -13.4 & 80.1 & -26.7 & 0 & 0 \\ 0 & -26.7 & 96.3 & -28.3 & 0 \\ 0 & 0 & -28.3 & 81.5 & -9.82 \\ 0 & 0 & 0 & -9.82 & 682 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \\ X_3 \\ X_4 \\ X_5 \end{bmatrix} = \begin{bmatrix} .982 \\ 4.24 \\ 5.55 \\ 5.216 \\ 7.02 \end{bmatrix}$$

23.008

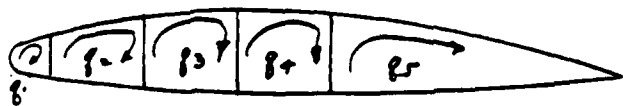
where

$X_1 = 0.0229$	$.0229 \times .982 = .0225$
$X_2 = 0.0942$	$.0942 \times 4.24 = .40$
$X_3 = 0.1123$	$.1123 \times 5.55 = .6233$
$X_4 = 0.1044$	$.1044 \times 5.216 = .545$
$X_5 = 0.0118$	$.0118 \times 7.02 = .0828$

$1.674 \times X_4 = 6.69 = J$

$\theta_1 = \frac{2 \times 1000}{6.69} \times .0229 = 6.85 \text{ } ^\circ/\text{in}$	}	"g" for 1000" of torque
$\theta_2 = \dots \times .0942 = 28 \text{ } ^\circ/\text{in}$		
$\theta_3 = \dots \times .1123 = 33.6 \text{ } ^\circ/\text{in}$		
$\theta_4 = \dots \times .1044 = 31.2 \text{ } ^\circ/\text{in}$		
$\theta_5 = \dots \times .0118 = 3.5 \text{ } ^\circ/\text{in}$		

$GJ = 2.54 \times 10^6 \times 6.69 = 17 \times 10^6 \text{ By calculation}$



REPORT TITLE	REPORT NO.
PREPARED BY APC	CMRB-77-005
CHECKED BY 11/19/81	MODEL NO. YAH-64
SUBJECT YAH-64 CMRB	

Torsional Stiffness Test Data

Table 30-2

COMPOSITE M/R BLADE 100% = 12,000 "lb  
 PAN: 7-311412500  
 S/N: 1002

STA - % LAST	DEGREES / MIN											
	54	69	84	107	130	153	176	199	222	245	265	285
0	6/30	6/0	5/27	4/50	4/08	3/23	2/40	2/10	1/32	0/45	0/49	0/49
20	6/54	5/44	5/03	4/15	3/20	2/24	1/52	0/40	0/81	1/05	2/50	3/50
40	6/09	5/33	4/55	3/53	2/45	1/36	0/29	0/34	1/34	2/40	4/36	4/36
60	6/04	5/22	4/41	3/23	2/07	0/47	0/31	1/47	3/00	4/13	6/33	6/33
80	6/00	5/21	4/30	3/00	1/50	0/00	1/13	3/00	4/24	5/59	8/12	8/12
100	5/59	5/16	4/16	2/40	0/58	0/48	2/28	4/05	5/45	7/27	10/00	10/00
80	6/00	5/21	4/24	3/00	1/30	0/00	1/33	3/00	4/26	6/00	8/19	8/19
60	6/04	5/26	4/37	3/23	2/03	0/37	0/34	1/52	3/05	4/51	6/31	6/31
40	6/06	5/31	4/51	3/17	2/40	1/29	0/22	0/62	1/42	2/53	4/50	4/50
20	6/11	5/40	5/00	4/10	3/17	2/20	1/24	0/35	0/64	1/11	3/00	3/00
0	6/28	5/57	5/29	4/49	4/06	3/22	2/40	2/00	1/26	0/40	0/49	0/49
20	6/49	6/20	5/56	5/29	4/57	4/27	3/57	3/28	2/02	2/38	1/14	1/14
40	6/53	6/24	6/03	5/55	5/27	5/14	4/57	4/41	4/28	4/12	2/55	2/55
60	6/57	6/33	6/15	6/15	6/00	5/57	5/38	5/53	5/53	5/15	4/50	4/50
80	6/58	6/41	6/29	6/41	6/47	6/49	6/58	7/14	7/14	7/22	6/34	6/34
100	7/00	6/47	6/43	7/03	7/19	7/23	7/52	8/09	8/34	8/52	8/14	8/14
80	6/59	6/42	6/32	6/43	6/49	6/52	6/58	7/06	7/18	7/20	6/44	6/44
60	6/55	6/35	6/19	6/18	6/13	6/04	6/00	6/00	6/00	5/56	5/03	5/03
40	6/52	6/27	6/04	5/51	5/39	5/19	5/00	4/47	4/35	4/16	3/10	3/10
20	6/46	6/20	5/56	5/20	5/01	4/27	4/00	3/54	3/12	2/43	1/23	1/23
0	6/33	6/05	5/52	4/58	4/16	3/32	2/52	2/10	1/40	0/58	-0/33	-0/33

REPORT TITLE	REPORT NO. <u>CMRB-79-005</u>
PREPARED BY <u>HC</u>	CHECKED BY
SUBJECT <u>YAH-64 CMRB</u>	MODEL NO. <u>YAH-64</u>

Sta 84 to 176, Blade Torsional Stiffness  
Ref Torsional Stiffness Data

$$\left. \begin{array}{l} \text{Ave torsional} \\ \text{Def Sta 84} \end{array} \right\} = \frac{[-40'16" + (5^{\circ}29' + 5^{\circ}27')/2] + [6^{\circ}43' - (5^{\circ}27' + 5^{\circ}32')/2]}{2}$$

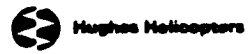
$$= 1^{\circ}12.75' = 1.2125^{\circ}$$

$$\left. \begin{array}{l} \text{Ave torsional} \\ \text{Def Sta 176} \end{array} \right\} = \frac{[20'28" + (2^{\circ}40')] + [7^{\circ}52' - (2^{\circ}40' + 2^{\circ}52')/2]}{2}$$

$$= 5^{\circ}7' = 5.117^{\circ}$$

$$GJ \text{ sta } 84 \text{ to } 176 \} = \frac{57.3 \times 12000(176 - 84)}{5.117^{\circ} - 1.2125^{\circ}} = 16.2 \times 10^6$$

Measured





REPORT TITLE		REPORT NO. CMRB-79-005
PREPARED BY APC	11/19/81	CHECKED BY
SUBJECT YAH-64 CMRB		MODEL NO. YAH-64

Sta 84 to 69, Blade Torsional Stiffness

Ref Torsional Stiffness Data

$$\text{Ave torsional Def Sta 69} \left. \vphantom{\text{Ave torsional}} \right\} = \frac{[-5^{\circ}16' + (6^{\circ}0' + 5^{\circ}59')/2] + [6^{\circ}47' - (6^{\circ}5' + 5^{\circ}59')/2]}{2}$$

$$= .7375^{\circ}$$

$$GJ = \frac{57.3 \times 12000 (84-69)}{1.2125 - .7375} = 21.7 \times 10^6 \text{ measured sta 84 to 69}$$

Sta 54 to 69

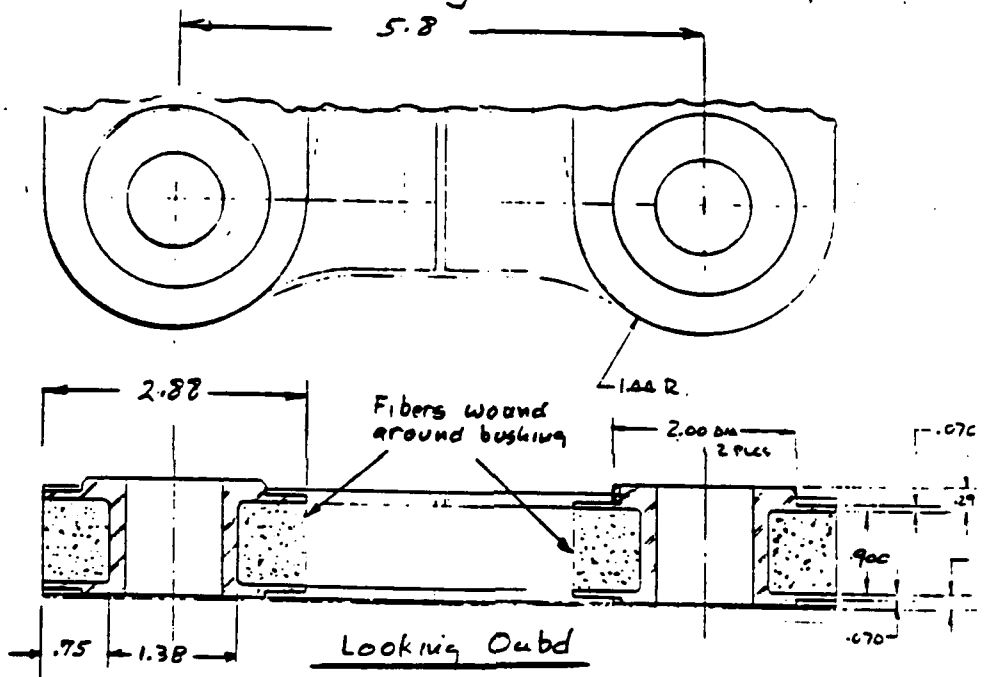
$$\text{Ave torsional Def Sta 54} \left. \vphantom{\text{Ave torsional}} \right\} = \frac{[-5^{\circ}59' + (6^{\circ}30' + 6^{\circ}28')/2] + [7^{\circ} - (6^{\circ}28' + 6^{\circ}33')/2]}{2}$$

$$= .4958^{\circ}$$

$$GJ = \frac{57.3 \times 12000 (69-54)}{.7375 - .4958} = 42.6 \times 10^6 \text{ measured Sta 54 to 69}$$

REPORT TITLE		REPORT NO. <u>CMRB-79-005</u>
PREPARED BY <u>MT</u>	<u>3/2/82</u>	CHECKED BY
SUBJECT		MODEL NO. <u>YAH-60</u>

*Crosssection Root Lugs*



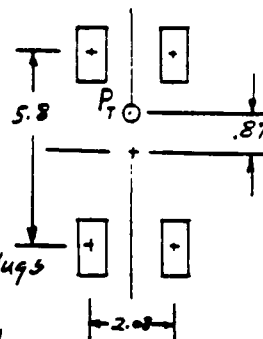
*Cross-section of lug bushings now being used on the CMRB.*

REPORT TITLE	REPORT NO <u>CMRB-79-005</u>
PREPARED BY <u>APC</u>	CHECKED BY <u>3/4/82</u>
SUBJECT	MODEL NO <u>YAH-66</u>

Root Lugs; Calculated Strength Compared with Static Test Applied Ld

$P_T = 187,869 \#$  ult Ref 3 P. A-1

Max lug Load } applied during static test }  $= \frac{3.77 \times 187,869}{2 \times 5.8} \times \frac{149}{150}$   
 $= 60,450 \#$  Ref 2



For the above load the specimen failed at the club end (Sta 123) not at the lugs which are at sta 39. Ref 2 Fig. 4

$K = \frac{1.3(R/r)^2 + .7}{R/r + 1}$  strength reduction factor due to wrapping keular around lug bushing. Ref 3 P. 30.12 Vol II

CMRB Lug Geometry

Allowable tension stress }  $= \left[ 162,500 \right] \div \left[ \frac{1.3(1.44/1.69)^2 + .7}{1.44/1.69 + 1} \right] \cdot .80 = 63,200 \text{ PSI}$   
Reduction factor, environmental etc

Lug Strength =  $2 \times .9 \times .75 \times 63,200 = 85,600 \#$

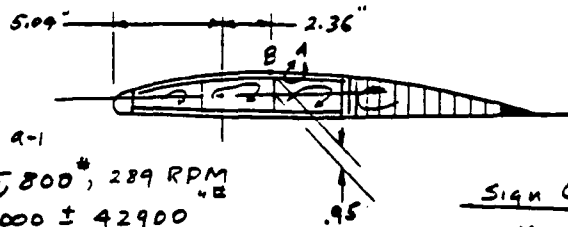
Calculated lug strength is 42% higher than what was applied during static test; The calculated M.S. is:

Vit Lug Load }  $= \frac{150}{149} \times 60,450 = 61,000 \#$

$M.S. = \frac{85,600}{61,000} - 1 = \frac{.40}{\text{ult Attach Lugs}}$

REPORT TITLE	REPORT NO.
PREPARED BY <u>H/C</u>	CHECKED BY
<u>3/5/82</u>	MODEL NO <u>YAH-64</u>
SUBJECT <u>YAH-64 CMRE</u>	

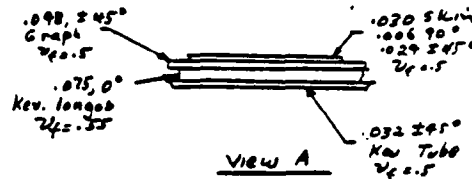
Sta 191.7 Pt. "B"  
CK. Spar Longos, Critical Bending Section



ref Table a-1  
 C.F. = 35,800<sup>#</sup>, 289 RPM  
 $M_F = -8000 \pm 42900$   
 $M_C = 12400 \pm 97500$  " #  
 $M_T = 3900 \pm 32000$

Sign Convention  
 +  $M_F$  - Com. Upper Surface  
 +  $M_C$  - Com. Trailing Edge  
 + Torsion ~ Nose Up

It's assumed the the longos resist bending and C.F. load, and the  $\pm 45^\circ$  layers resist torsion.



$$E_{Ten} = \frac{35800}{39.39} = 1041 \mu\% \cdot \text{Ton.}$$

$$E_f = \frac{-8000 \times .95}{12.7} = 598 \mu\% \cdot \text{Ton.}$$

$$E_c = -\frac{12400 \times 2.36}{984} + \frac{(2\frac{1}{4} - 5.04) 35800 \times 2.36}{984} = -12 \mu\% \cdot \text{com}$$

$$E_{alt} = \frac{42900 \times .95}{12.7} + \frac{97500 \times 2.36}{984} = 5890 + 234 = 3443 \mu\% \cdot \text{alt}$$

$f E, \text{kev, } 24 \pm .55$

$$\text{Max Ax. Ten Str} = (1041 + 724 - 12 + 3443) 10.66 = 55400 \text{ psi Ton}$$

$$\text{Min Ax Str} = (1041 + 598 - 12 - 3443) 10.66 = -19400 \text{ psi com}$$

$$F_{tu} = 162500 \times .8 = 130,000 \text{ psi}$$

Reduction factor  
Environmental etc

$$F_{cu} = \frac{37500 \times .8}{24 \pm .55} = 30,800 \text{ psi}$$

$$MS = \frac{30800}{1.5 \times 19400} - 1 = \frac{.06}{\text{Bend. CK. Pt. "B" Spar longos}}$$

REPORT TITLE		REPORT NO.
PREPARED BY	CHECKED BY	CMRB-77-605
YAH-CMRB	3/8/82	MODEL NO.
		YAH-64

Sta 87, Ck. ±45° layers

It is assumed the ±45° layers resist shear due to torsion.

$$t_{kevlar} = .032 + .024 = .056''$$

$$t_{graph} = .048''$$

$$q = 33.6 \times (8000 + 32000) = 1344 \frac{\#}{\text{in}} \text{ lim}$$

P. 30.07

$$= 2016 \frac{\#}{\text{in}} \text{ ult}$$

Reduction factor  
Environmental effects  
etc.

Shear capability of the ±45° layers } =  $(.048 \times 37098 + .056 \times 15600) \cdot 8$

P. 20.02  
Max Torque

P. 100.06

$$= 2123 \frac{\#}{\text{in}} \text{ @ } 20.11$$

$$MS = \frac{2123}{2016} - 1 = \underline{\underline{.05}}$$

Shr. Ck  
±45° layers

Stress applied to spar cap longerons during static test

$$\text{Stress applied to longerons during test } = \frac{187869}{38.1} \frac{149}{150} \times 10.66 = 52,000 \text{ PSI}$$

P. 190.02

P. 30.02

Ratio of stress applied during test and calculated ultimate stress } =  $\frac{52,000}{1.5 \times 55,400} = .63$

P. 150.01

REPORT TITLE		REPORT NO CMRB-79-005	
PREPARED BY APC	3/26/82	CHECKED BY	MODEL NO. YAH-64
SUBJECT YAH-64 CMRB			

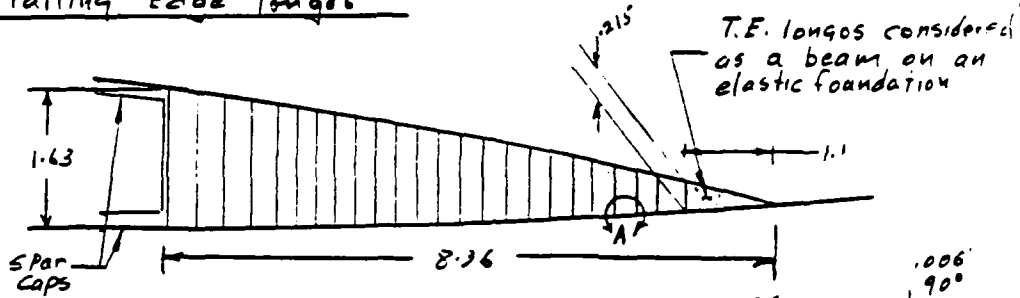
TRAILING EDGE

The buckling load for the trailing edge is calculated assuming it to be a column on an elastic foundation. Comparing the buckling load with the applied load it can be seen that the trailing edge will not buckle at limit load for the Maximum Rotor Torque condition.

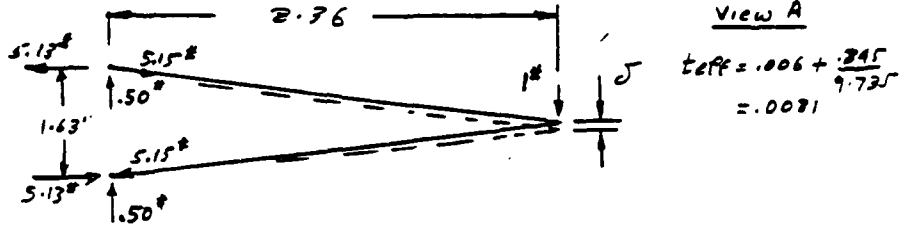
The analysis shows that the spar caps can resist the remaining bending load after the trailing edge buckles above limit load. That is the instant the trailing edge buckles elastically at a stress of 16,900 psi; the spar caps will pick up the remaining load preventing any inelastic buckling of the trailing edge. Since only elastic buckling occurs, no failure results.

REPORT TITLE	REPORT NO. CMBP-77-005
PREPARED BY JTC	CHECKED BY 3/5/82
SUBJECT	MODEL NO. YAH-64

Trailing Edge Longos



From the T.E. longos to the spar caps will be idealized as a truss.



$$\bar{v} = \frac{PL}{AE} = \frac{5.13 \times 8.36}{.0081 \times 9.735 \times 10^6} = .000544''$$

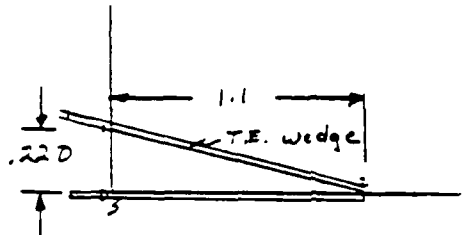
Internal Energy  $\int = \frac{1}{2} \bar{v} \times 5.15 \times 2 = .000544 \times 5.15 = .0028$

External Energy  $\int = \frac{1}{2} \bar{v} ; \bar{v} = 2 \times .0028 = .0056$

Spring Rate =  $\frac{1}{.0056} = .179 \text{ #/in}$

REPORT TITLE		REPORT NO <u>CMRB-79-005</u>
PREPARED BY <u>AVE</u>	3/5/82	CHECKED BY
SUBJECT		MODEL NO <u>YA17-64</u>

Trailing Edge Lougas



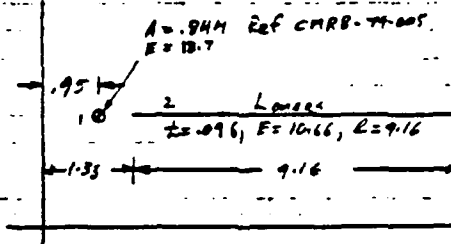
$x = .37$   
 $y = -.073$   
 $A = .121$   
 $I_x = 325 \times 10^{-6}$   
 $I_y = 8 \times 10^{-3}$   
 $I_{xy} = 873 \times 10^{-6}$   
 $EI = 17.23 \times 10^6 \times 309 \times 10^{-6}$   
 $= 5600 \text{ T.E. wedge only}$

	X	Y
0	0	0
1	0	.220
2	1.1	0
3	0	0



REPORT TITLE	REPORT NO. CMRB-79-005
PREPARED BY A. Cilli	CHECKED BY
SUBJECT YAH-64 CMRB	MODEL NO. YAH-64

Calculation of I<sub>chord</sub>. Aff skin and T.E. assumed Buckled



Item	A	E	EA	X	EAX	EAX <sup>2</sup>	I <sub>o</sub>
1	.844	10.7	15.73	.45	14.99	14.99	0
2	1.91	10.66	19.29	5.91	114.0	673.8	135.18
			35.07		129	688.8	135.18

$$EI_{longqs} = \frac{2 \times .099 \times 9.16^3}{12} \times 10.66 = 135.18$$

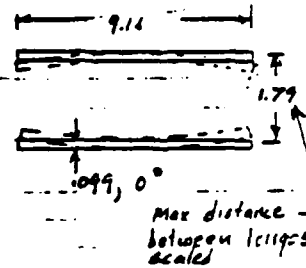
$$\bar{X} = \frac{129}{35.07} = 3.68$$

$$EI_{chord} = 135.18 + 688.8 - 3.68 \times 129 = 319$$

To account for curvature of longqs

$$I_{Flap} = \left( .90 \times \frac{1.79}{2} \right)^2 \times 9.16 \times .099 \times 10.66 \times 2$$

$$= 12.54 \quad \text{Longqs only}$$



REPORT TITLE		REPORT NO.
PREPARED BY <u>APC</u>		<u>CMRB-79-005</u>
3/5/82	CHECKED BY	MODEL NO.
SUBJECT <u>YAH-64 CMRB</u>		<u>YAH-64</u>

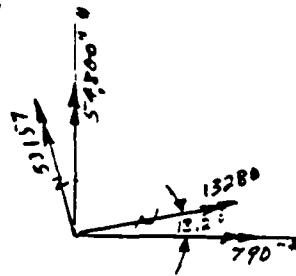
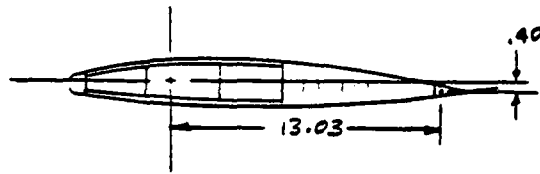
Trailing Edge Longos

$$m = \left[ \frac{KL^4}{\pi^4 EI} \right]^{1/4} = \left[ \frac{179 \times (288 - 82)^4}{\pi^4 \times 5600} \right]^{1/4} = 28$$

Ref 3  
P. 97  
Main body  
of Rp.

$$P_{cr} = \frac{2m^2 \pi^2 EI}{L^2} = \frac{2 \times 28^2 \times \pi^2 \times 5600}{206^2} = 2042$$

T.E. Buckling stress =  $2042 / .121 = 16,900 \text{ PSI}$



Ref 3 P. 9  
Vol I  
Zero Rotor Speed  
Max Torque

$$f = \left[ \frac{54795 \times 13.03}{924} + \frac{790 \times .4}{15.52} \right] 17.23$$

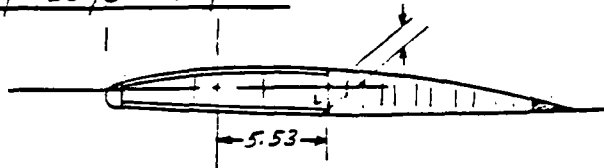
$$= 13,660 \text{ PSI}$$

$$MS = \frac{16900}{13700} - 1 = \underline{\underline{.23}}$$

Limit  
Stability  
Shows that for  
LIMIT LOADS  
the T.E. longos  
will not buckle.

REPORT TITLE		REPORT NO.
PREPARED BY	CHECKED BY	CHARS-79-005
APC	3/5/82	MODEL NO.
SUBJECT		YAH-64
YAH-CMRB		

Trailing Edge Longos



Stress at Pt. "L" due to 1.23 times limit load } =  $\left[ \frac{54795 \times 5.53}{927} + \frac{790 \times .70}{15.52} \right] 10.66 \times 1.23 = 4,800 \text{ psi}$

Stress at Pt. "L" due to balance of ultimate load } =  $\left[ \frac{54795 \times 6.81}{349} + \frac{790 \times .7}{12.54} \right] (1.5 - 1.23) \times 10.66$   
 = 3204 psi

Stress at Pt. "L" after the T.E. longos have buckled } = 4800 + 3204 = 8000 psi com.

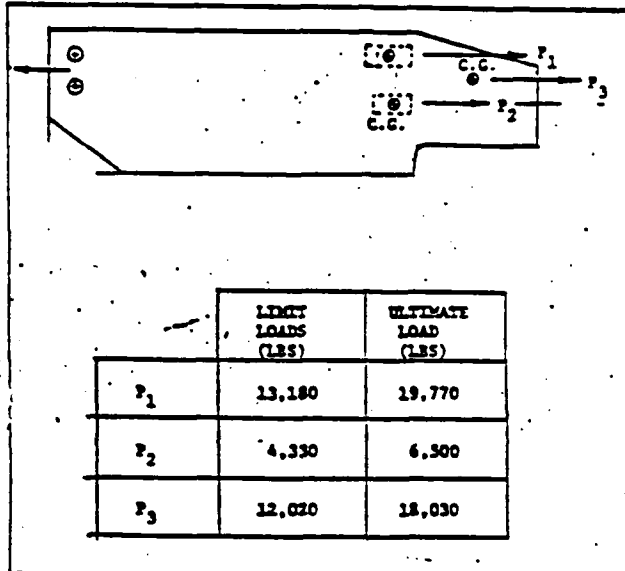
Allowable com. stress for Kevlar,  $\nu_f = .55$  } =  $.8 \times 38500 = 30,800 \text{ psi}$   
 Reduction factor, Environmental effects etc.

MS =  $\frac{30800}{8000} - 1 = \text{High}$

ABOVE LIMIT LOAD  
 This shows that after the T.E. longos have buckled the spar cap longos will resist the remaining bending and that ultimate can be applied to the blade without failure.  
 LONG

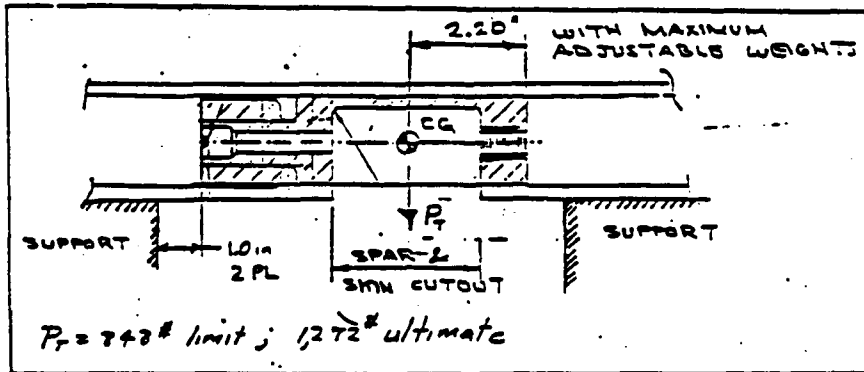
REPORT TITLE		REPORT NO
PREPARED BY <u>APC</u>		<u>CMRB-77-005</u>
3/8/82	CHECKED BY	MODEL NO
SUBJECT <u>YAH-64 - CMRB</u>		<u>YAH-64</u>

Blade Tip - Substantiated by Test



Load Configuration: Sump; Tip Radial Static Test

NOTE: Tip resisted 356% of the above limit loads without failure (Ref. 2, P<sub>3</sub> & P<sub>2</sub>) etc; MS = High



Load Configuration, Aft Weight Assy. Vertical Load Test

APPENDIX B

FATIGUE ANALYSIS OF THE COMPOSITE MAIN ROTOR  
BLADE FOR THE AH-64A HELICOPTER



REPORT TITLE <b>Fatigue Analysis for the YAH-64 CMRB</b>		REPORT NO. <b>CMRB-79-006</b>
PREPARED BY <b>APC</b>	CHECKED BY <b>3/25/82</b>	MODEL NO. <b>YAH-64</b>
SUBJECT <b>CMRB Fatigue Analysis</b>		

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B10	Introduction	B10.03
B10	Summary of Component Lives	B10.04
B10	Summary of Test Results	B10.05
B15	Root Fatigue Test Results and Applied Loads	B15.01
B15	Swept Tip Test Results and Applied Loads	B15.02
B20	Fatigue Test Results Plotted	B20.01
B30	CMRB and Metal Blade Flight Allowables Compared	B30.01
B40	Graphs Substantiating CMRB Fatigue Strength Compared to Blade Flight Loads and Metal Blade Allowables	B40.01

REPORT TITLE	Fatigue Analysis for the YAH-64 CMRB	REPORT NO.	CMRB 79-006
PREPARED BY	APC 3/25/82	CHECKED BY	
		MODEL NO.	YAH-64
SUBJECT	CMRB - Fatigue Analysis		
<u>REFERENCES</u>			
1. CMRB-79-004 Basic Loads Report for the Composite Main Rotor Blade for the YAH-64 Advanced Attack Helicopter 1 June 1979 Revised July 1979 Revised March 1982			
2. Structural Test Report for the CMRB YAH-64/AAH Feb. 1982			
3. CMRB 79-041 Safety of Flight Review Airworthiness Substantiation Document Composite Main Rotor Blade for the YAH-64/AAH May 1980, Vol. I and II			



REPORT TITLE Fatigue Analysis for the YAH-64 CMRB		REPORT NO. CMRB-79-006
PREPARED BY APC 3/25/82	CHECKED BY	MODEL NO. YAH-64
SUBJECT CMRB Fatigue Analysis		

#### INTRODUCTION

Fatigue life of the CMRB is equal to or greater than 4500 hours as required per Specification Number AMC-SS-AAH-H10000. Also with a critical element failed the CMRB is capable of a minimum of thirty (30) minutes of flight after initial failure.

The revised fatigue life of the CMRB has been substantiated by a combination of analysis and component fatigue tests. A summary of test results is shown on Pg. A10.05. Fatigue analysis of the blade before testing is presented in the main body of the report.

Five root specimens were tested. The first two specimens were root-midspan specimens. The purpose being to test the blades root-end and mid-span simultaneously. During testing of the specimens 1 and 2 premature lug failures occurred at 8000 and 24000 respectively due to the high rate of cyclic loading (approximately 13 Hz), which cause heating of the lugs and an undue rise in temperature leading to early failure. 13-Hz was the resonant frequency of the specimen.

A premature failure of specimen No. 3 indicated insufficient fatigue strength of the blade attachment lugs as originally designed. Specimen 4, which incorporated design configuration changes yielded greatly improved fatigue strength in the lug area although lateral expansion of the lugs was still present.

The present design of the blade lugs has a double flange bushing (spool) to contain the fibers because they tend to spread or flatten out when loaded. The previous tested blade specimens had bushings with only a single flange. To structurally simulate the current design in the fatigue test, shims were placed between the link assembly and the blade lugs for specimen 5.

Specimen 5, with shimmed lugs showed no damage or lateral expansion of the lugs after 947,700 cycles at increased load levels. The last 50,400 cycles were obtained at the mean 1 hour load level. The required number of cycles at the 1 hour load level is 17,340. The root end of the blade could still support centrifugal force when the test was terminated due to increased deflections.

REPORT TITLE Fatigue Analysis for the YAH-64 CMRB		REPORT NO. CMRB-79-005	
PREPARED BY APC	3/26/82	CHECKED BY	MODEL NO. YAH-64
SUBJECT CMRB Fatigue Analysis			

INTRODUCTION - (Cont'd)

Other changes to the original design that increase the fatigue strength are as follows:

1. .048" graphite inner skin; was .010" Kevlar.
2. Honeycomb supporting the trailing edge skin and swept tip; was Kevlar tubes and Kevlar ribs respectively.
3. .075 graphite channel that runs the length of the blade; was .048 Kevlar web.

A summary of loads and test results is given on Pg. B15.01 for specimens 3, 4, and 5; and on Pg. B10.05 is a summary of all testing done on the CMRB.

One swept tip was tested. Loads and results are shown on Pg. B15.02. The swept tip is of original design with .010" Kevlar inner skin and Kevlar ribs supporting the skin. The present design has honeycomb supporting the skin and is stronger.

From test results shown on Pg. B15.01 and Pg. B15.02, flight L-N fatigue curves are developed starting on Pg. B20.01. For flap bending and chord bending curves, the most conservative combination of 45° and 0° curve shapes is used. This is because either the 45° or 0° fibers may fail first. For torsion, only the 0° curve shape is used since torsion is resisted as axial load in the ±45° fibers. The attach lug curve shape is based on the 0° fibers. The mean test curve at the endurance limit is reduced as follows:

L-N CURVE SCATTER REDUCTION FACTORS

Number of Fatigue Test Specimens	Percent of Mean L-N Curve Used
1	50%
2	65%
3	75%
4 or more	Statistical analysis (M-3σ)

REPORT TITLE	Fatigue Analysis for the YAH-64 CMRB		REPORT NO.	CMRB-79-006
PREPARED BY	APC	3/26/62	CHECKED BY	
SUBJECT	CMRB Fatigue Analysis			
<p><u>INTRODUCTION - (Cont'd)</u></p> <p>Values obtained for endurance limit, 10 hour and 1 hour flight allowables are shown on Pg. B30.01 and compared to metal blade allowables.</p> <p>Starting on Pg. B40.01 the values on Pg. B30.01 for endurance limit and one hour are shown graphically along with the applied blade load curve. From these curves the fatigue strength of the CMRB can be compared to the metal blade and the load applied to the blade.</p>				

REPORT TITLE <b>Fatigue Analysis for the YAH-64 CMRB</b>	REPORT NO. <b>CMRB-79-006</b>
PREPARED BY <b>AFC</b>	CHECKED BY <b>3/25/82</b>
SUBJECT <b>CMRB Fatigue Analysis</b>	

REPORT TITLE <b>FATIGUE ANALYSIS FOR THE YAH-64 ADVANCED ATTACK HELICOPTER COMPOSITE MAIN ROTOR BLADE</b>	REPORT NO. <b>CMRB-79-006</b>
PREPARED BY <b>AFC</b>	CHECKED BY <b>11-5-79</b>
SUBJECT <b>CMRB - FATIGUE ANALYSIS</b>	

SUMMARY OF COMPONENT LIVES

ITEM	CONDITION	PAGE	LIFE
ROOT LDCS	WEIGHTED FATIGUE	30.20	> 4500 HOURS
	CAC	30.21	100,000 HOURS
	VULNERABILITY (ONE LDC FAILED)	30.22	MORE THAN 30 MINUTES
VIBRATION ABSORBER BRACKET	FATIGUE	31.13	INFINITE
		31.17	
		31.19	
ROOT CLOSE-OUT	WEIGHTED FATIGUE	40.04	INFINITE
STA 55	WEIGHTED FATIGUE	50.04	> 4500 HOURS
STA 84	WEIGHTED FATIGUE	60.04	> 4500 HOURS
STA 160	WEIGHTED FATIGUE	70.03	> 4500 HOURS
STA 192	WEIGHTED FATIGUE	70.06	> 4500 HOURS
TIP COMPONENTS	CAC	80.01	INFINITE



### SUMMARY OF TESTS RESULTS

This page presents the results of tests conducted on the Composite Main Rotor Blade for the YAH-64 Advanced Attack Helicopter. The tests were conducted at the Hughes Helicopters Inc. Structures Test Laboratory, Culver City, CA., between January 1980 and August 1981.

One each, Swept Tip specimens were subjected to Static, Ground-Air-Ground, and Fatigue loading. One each, Root-Midspan specimens were subjected to Static and Ground-Air-Ground loading. Five Root specimens were tested under fatigue loading.

Significant test results are as follows:

1. Swept Tip Static, GAG and Fatigue tests.
  - a. 100% radial limit load achieved on swept tip section without failure or permanent set.
  - b. 100% vertical limit load and ultimate load on aft tip weight box without failure or permanent set. 211% radial limit load achieved on swept tip assembly without failure.
  - c. 366% radial limit load achieved on fwd. and aft tip weight boxes without failure.
  - d. 108,000 cycles, representing eight times three GAG cycles per hour for a service life of 4500 hours achieved without failure.
  
2. Root-Midspan Static and GAG tests.
  - a. 100% radial limit load applied statically without yielding or permanent set. Failure at the club end occurred at 149% limit load.
  - b. 108,000 cycles, representing eight times three GAG cycles per hour for a service life of 4500 hours achieved without failure. Lug failed at 33,200 cycles of 125% GAG load.
  
3. Root Fatigue Tests
  - a. Tests conducted on specimens 1 and 2 were considered invalid due to overheating of the test specimen resulting from an excessive test cyclic load rate.
  - b. A premature failure of specimen No. 3 indicated insufficient fatigue strength of the blade attachment lugs as originally designed.
  - c. Specimen 4, which incorporated design configuration changes yielded greatly improved fatigue strength in the lug area although lateral expansion of the lugs was still present.
  - d. Specimen 5, with shimmed lugs which simulated the additional lateral restraint of the longo fibers obtainable from the future use of double flanged lug bushings showed no damage or lateral expansion of the lugs after 947,700 cycles at increased load levels. The last 50,400 cycles were obtained at the mean 1 hour load level. The required number of cycles at the 1 hour load level is 17,340. The root end of the blade could still support centrifugal force when the test was terminated due to increased deflections.

REPORT TITLE <b>Fatigue Analysis for the YAH-64 CMRB</b>	REPORT NO. <b>CMRB-79-006</b>
PREPARED BY <b>APC</b>	CHECKED BY
<b>2/26/82</b>	
MODEL NO. <b>YAH-64</b>	

SUBJECT  
**CMRB Fatigue Analysis**  
**Root Fatigue Test Results and Applied Loads**

See Pgs 38 & 39 Ref 2.

Specimen Description	3		4		5	
	3rd Specimen	Original Design	1st Specimen	Redesigned Specimen	2nd Specimen	Redesigned Specimen
Upper Lug	LL-1	.4x1L-2	LL-3	LL-4	LL-5	LL-8
	S/N 017	S/N 1002	S/N 1003			
Mid Lug	39	± 39,200	± 39,200	± 43,950	± 43,950	± 54,500
	41	± 32,100	± 36,000	± 36,000	± 40,360	± 50,000
Mid Lug	69	± 35,200	± 30,000	± 30,800	± 31,500	± 40,300
	86	± 24,100	± 5,600	± 16,000	± 18,400	± 32,000
Mid Lug	39	± 50,900	± 20,160	± 50,400	± 87,900	± 109,100
	49	± 51,900	± 20,760	± 52,500	± 85,100	± 94,520
Mid Lug	69	± 55,900	± 22,960	± 55,900	± 79,300	± 72,352
	96	± 53,000	± 21,200	± 53,500	± 93,300	± 57,000
Mid Lug	39	± 8390	± 2,356	± 13,830	± 18,500	± 23,100
	48	± 7990	± 3,196	± 13,600	± 19,300	± 22,407
C.F.	6042018	± 2,720	± 13,000	± 17,600	± 17,600	± 20,328
	6042018					6042018
Results	First	Second	First	Second	First	Second
	Frig 2 H <sub>2</sub> : 733,100N Upper Lug bushing rotated	Frig 2 H <sub>2</sub> : 79,900N Reversed pushing to obtain heating for thr.	Frig 2 H <sub>2</sub> : 1210N No damage	2 H <sub>2</sub> : 73,200N Upper off 2 lum Lug bushings loose. Expansion of lug 100%. Expansion of lug matrix indicates matrix is failing. X-ray analysis verifies this.	2 H <sub>2</sub> : 258,000N T.E. Skin buckled, repaired.	2 H <sub>2</sub> : 50,900N. Dec at str 39 110% stress of lug failed just oppd

NOTE: Original design had kevlar inner skin and tubes in T.E. of airfoil. Redesigned specimen has graphite inner skin and honeycomb in T.E. of airfoil. None of the above specimens had the double flange bushing (spool) that is now being used. Lugs of the 2nd redesigned specimen were shimmed to simulate the spool bushing.

REPORT TITLE <i>Fatigue Analysis for the VAH-64 CMRB</i>	REPORT NO. <i>CMRB-79-006</i>
PREPARED BY <i>APC</i>	CHECKED BY
<i>2/26/82</i>	
MODEL NO. <i>VAH-64</i>	
SUBJECT <i>CMRB Fatigue Analysis</i>	

Swept Tip Fatigue Results and Applied Loads

*Ref 3 Pg 24*

Test Results, Swept Tip Fatigue Test

LOAD LEVEL	FATIGUE MOMENTS (IN-LB.)			COMMENTS
	Sta. 266.5		Sta. 260	
	M <sub>Flap</sub>	M <sub>Chord</sub>	M <sub>Torsion</sub>	
1	+9227	+5670	+1100	1 X 10 <sup>6</sup> CYCLES. NO FAILURE
2	+11534	+7088	+1376	1 X 10 <sup>6</sup> CYCLES. NO FAILURE
3	+13841	+8505	+1650	162,000 CYCLES. NO FAILURE TEST TERMINATED.

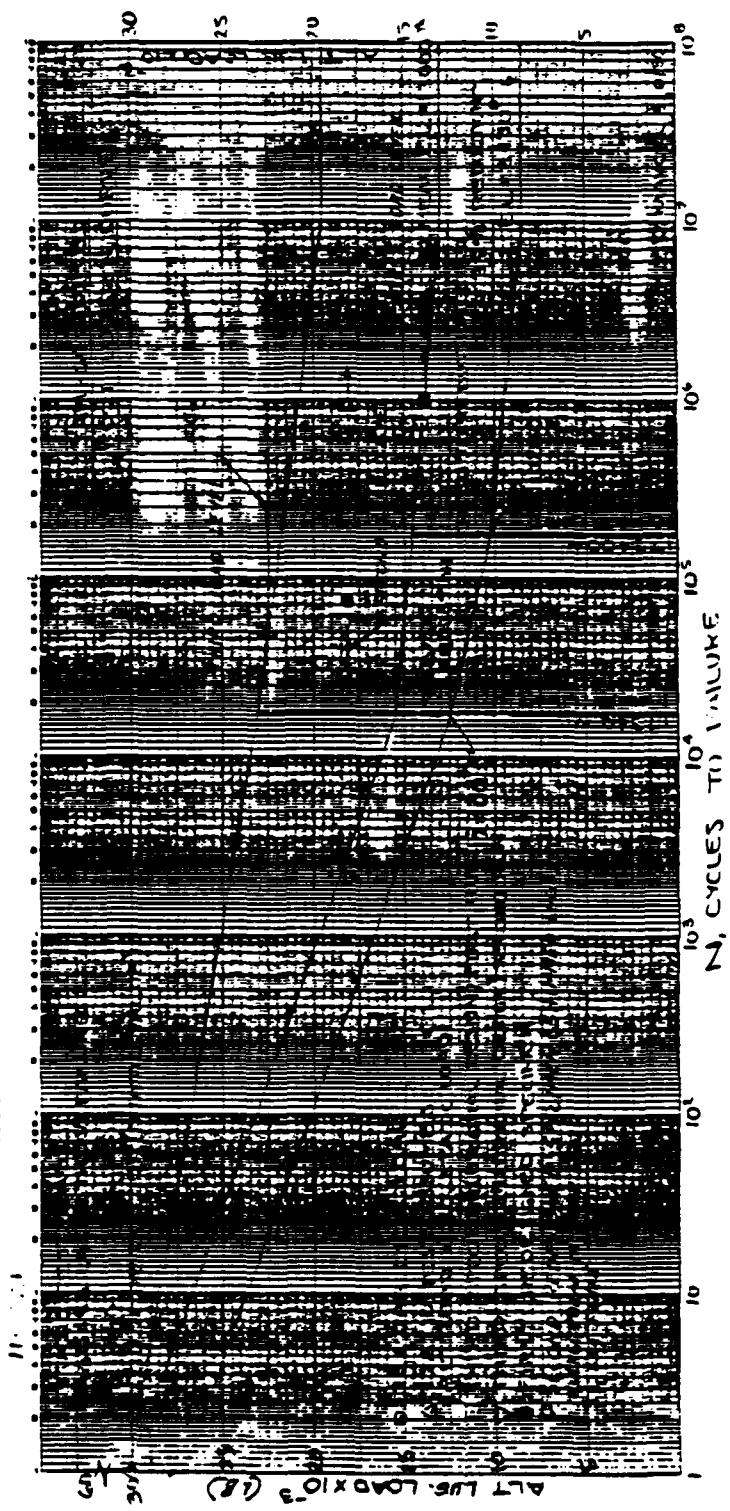
Fatigue Bending Moment Distribution, Load Level 1  
Swept Tip Fatigue Test

CYCLES	STATION (IN.)	M <sub>C</sub>	M <sub>T</sub>
		+(in.-lb)	+(in.-lb)
5600	250	17013	16653
	260	4186	10680
	266.5	2670	9227
22590	250	17532	16965
	260	4069	10679
	266.5	5670	9227
29300	250	15268	16742
	260	N.A.	10679
	266.5	5670	9227

NOTE: Specimen was the original design (Kevlar inner skin). Present design has an graphite inner skin which has greater strength.

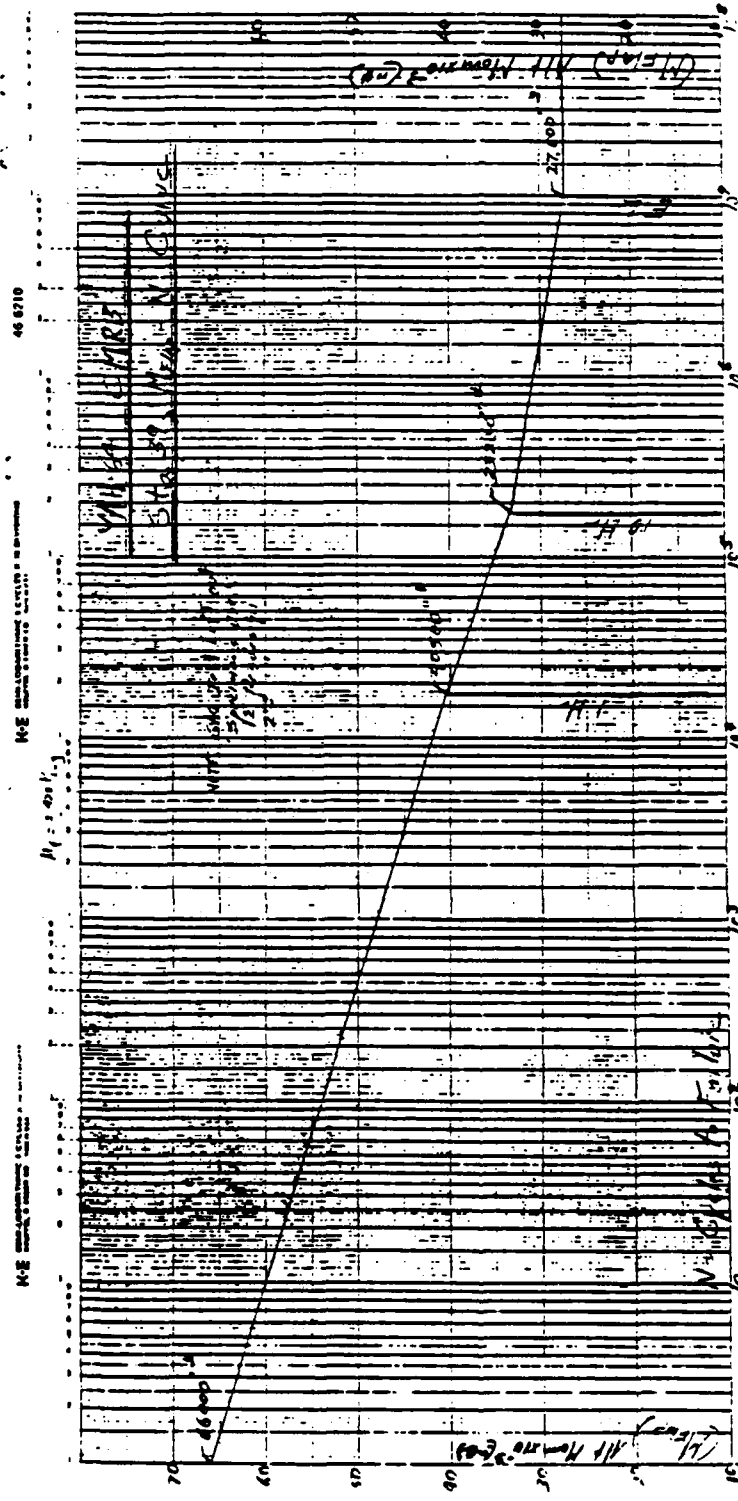






*Above data is just for added information on testing of the blade lugs.*

B20.01.1  
CIRB-79-006



820.02  
CIRB-79-006

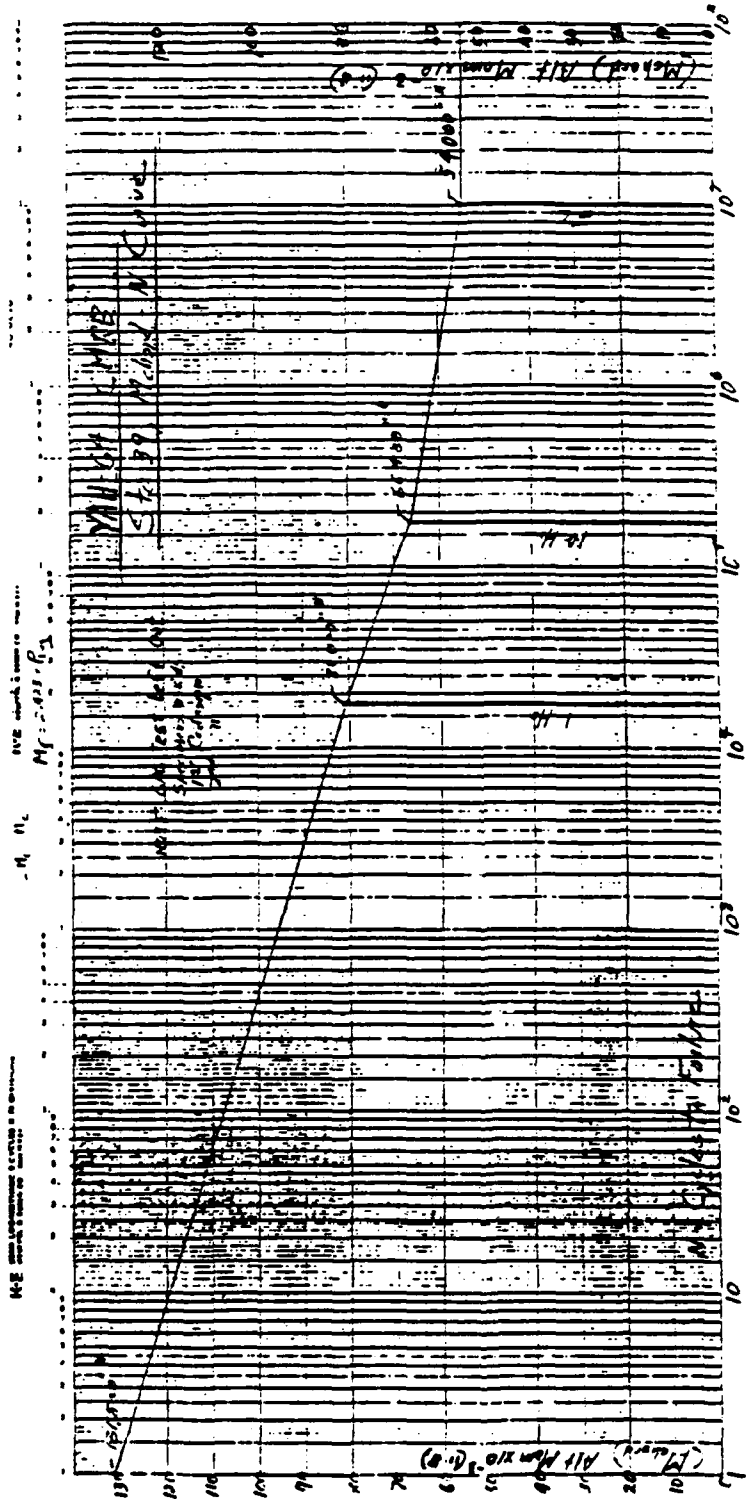
Assumed:  
at Stag 39

Then:

$$M_c = 2MF$$

$$P_{Lug} = \frac{MF}{2 \times 2.08} + \frac{2MF}{2 \times 5.8}$$

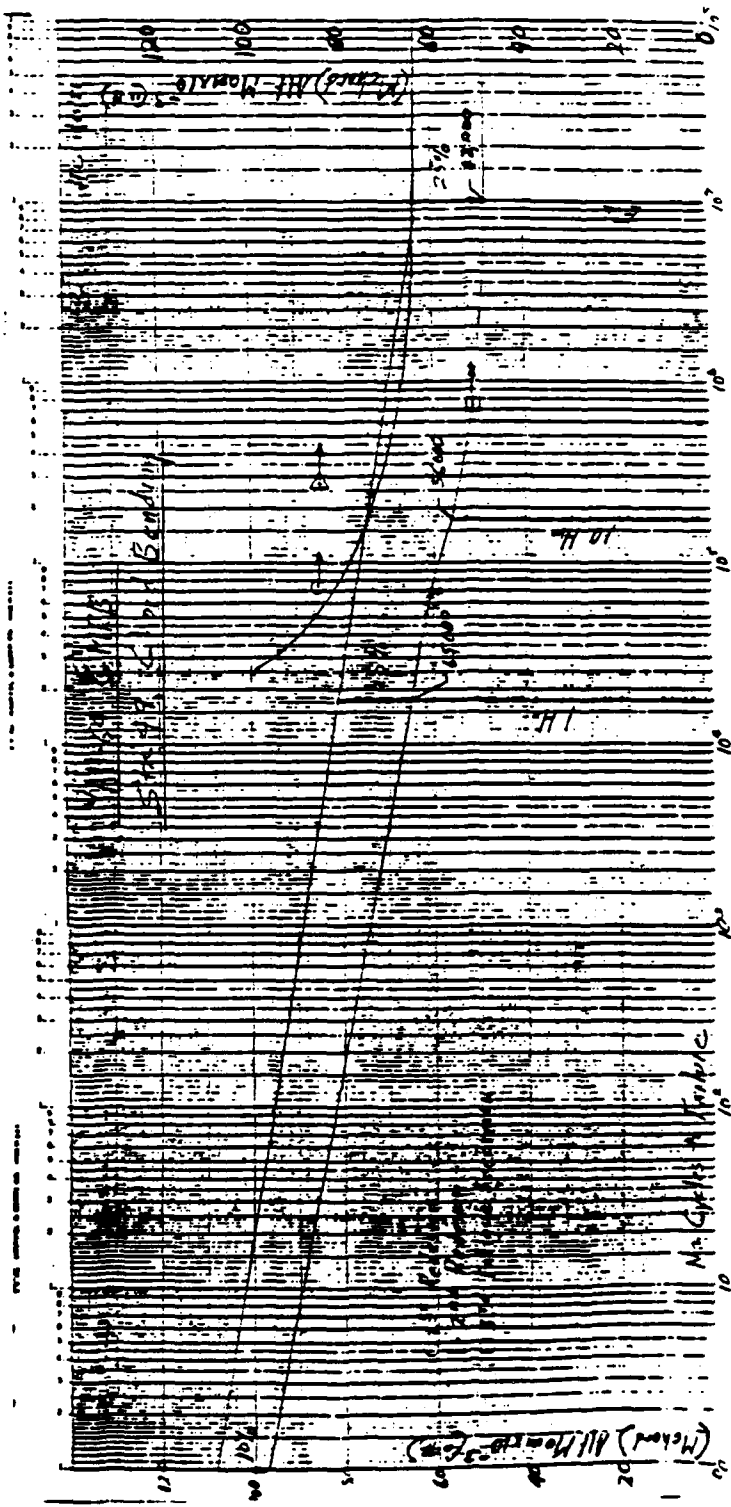
where Plug is from Pg A20.01



B20.03  
CIRB-79-006

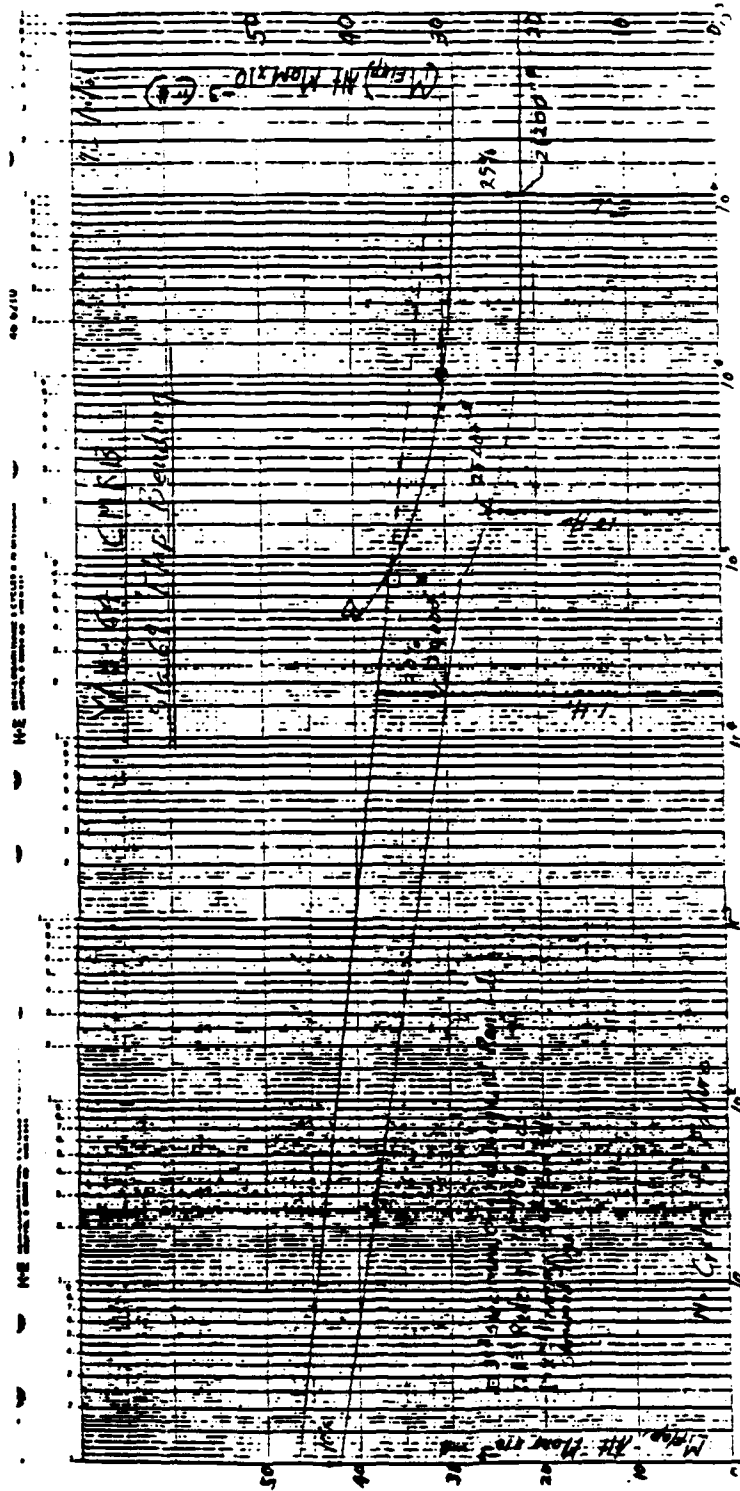
Assumed:  $M_c = 2 MF$   
at Sta 39  
Then: See Pg A20.02



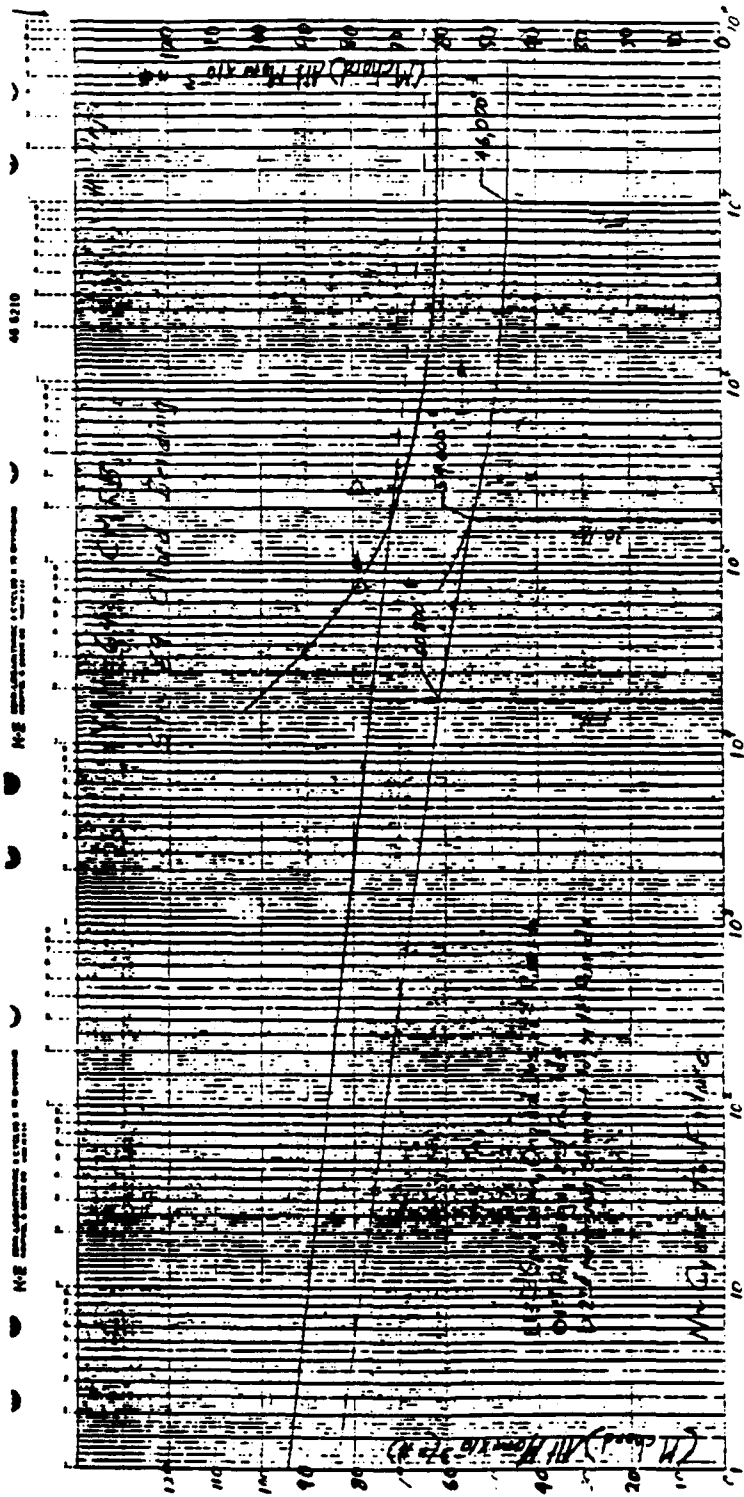


B20.05  
 CIRB-79-006

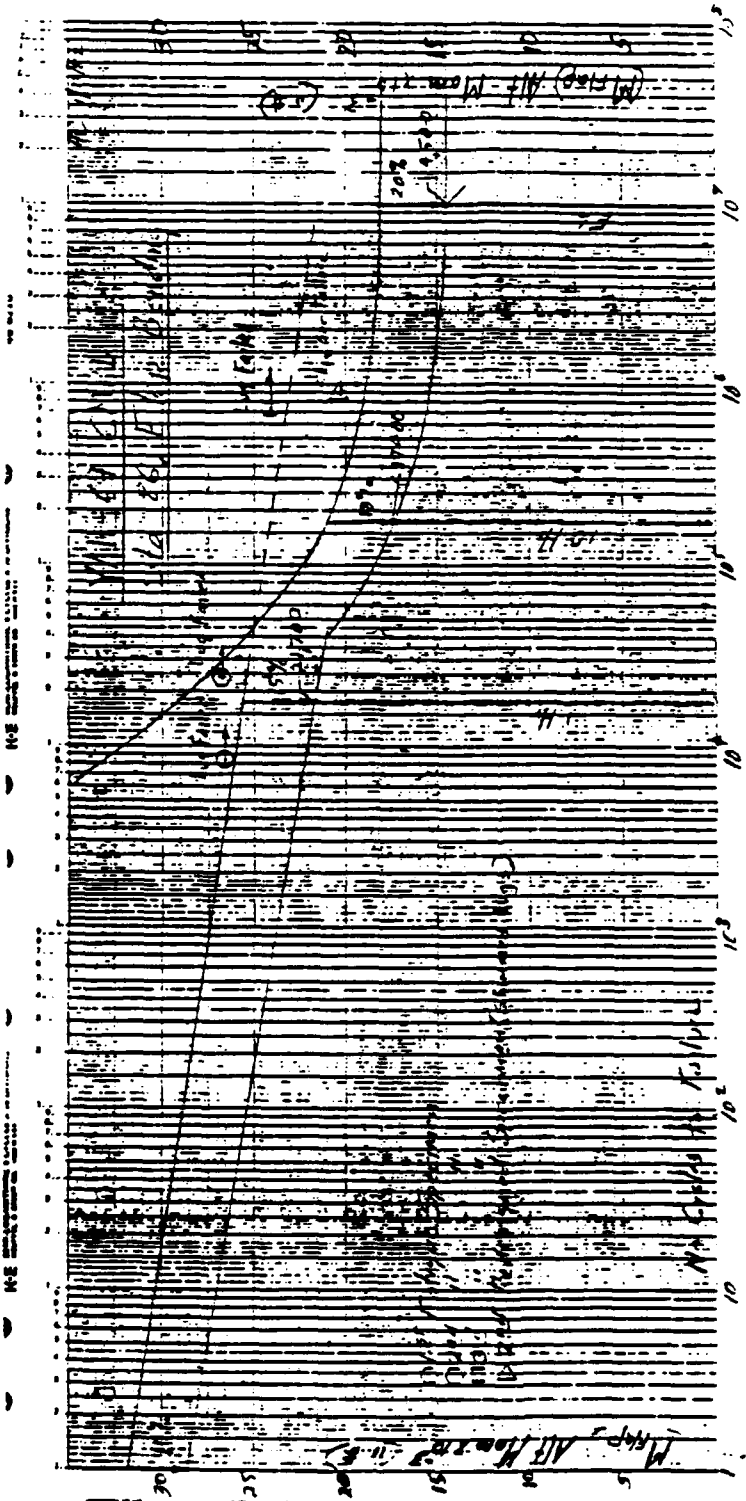
820.06  
CIRB-79-006



B20.07  
CI1RB-79-006

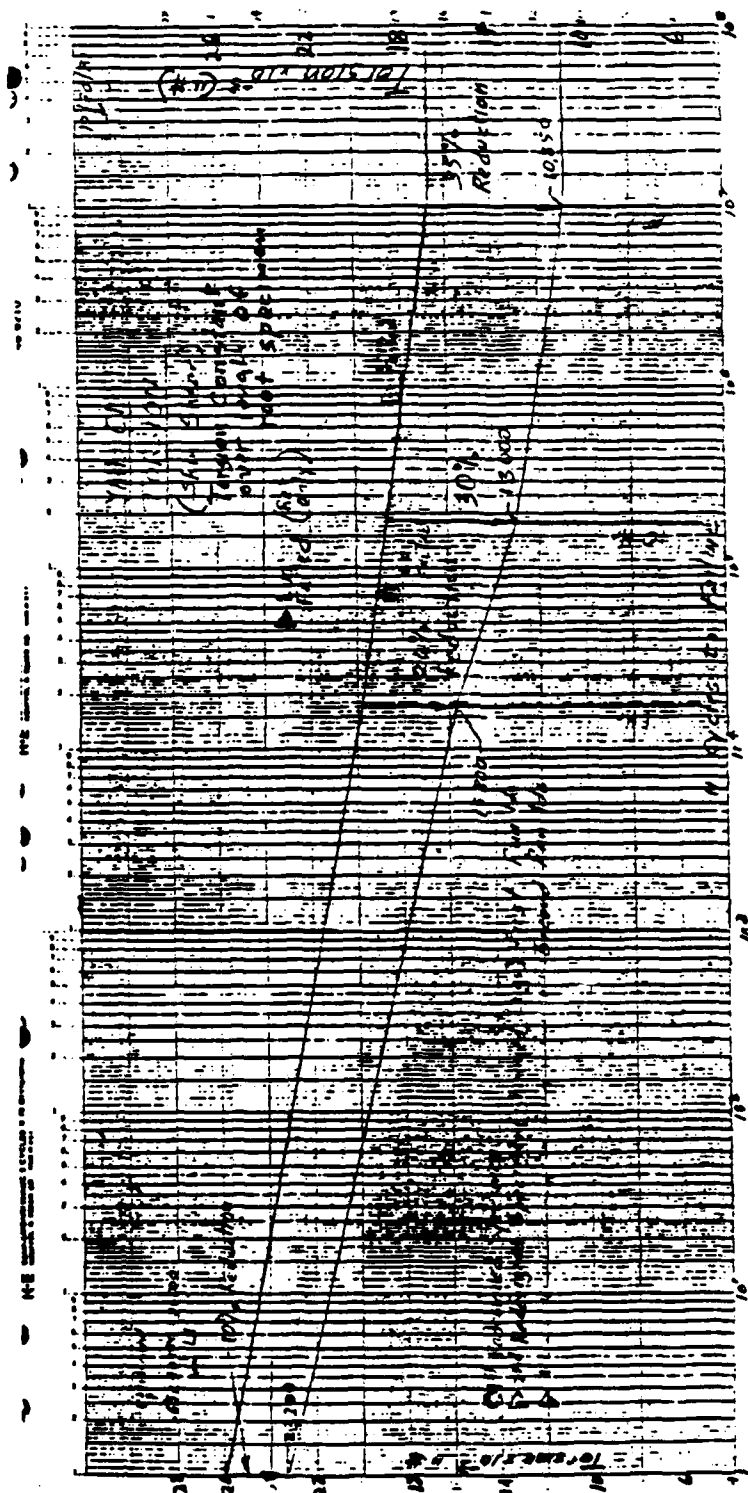


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CIRG-79-006



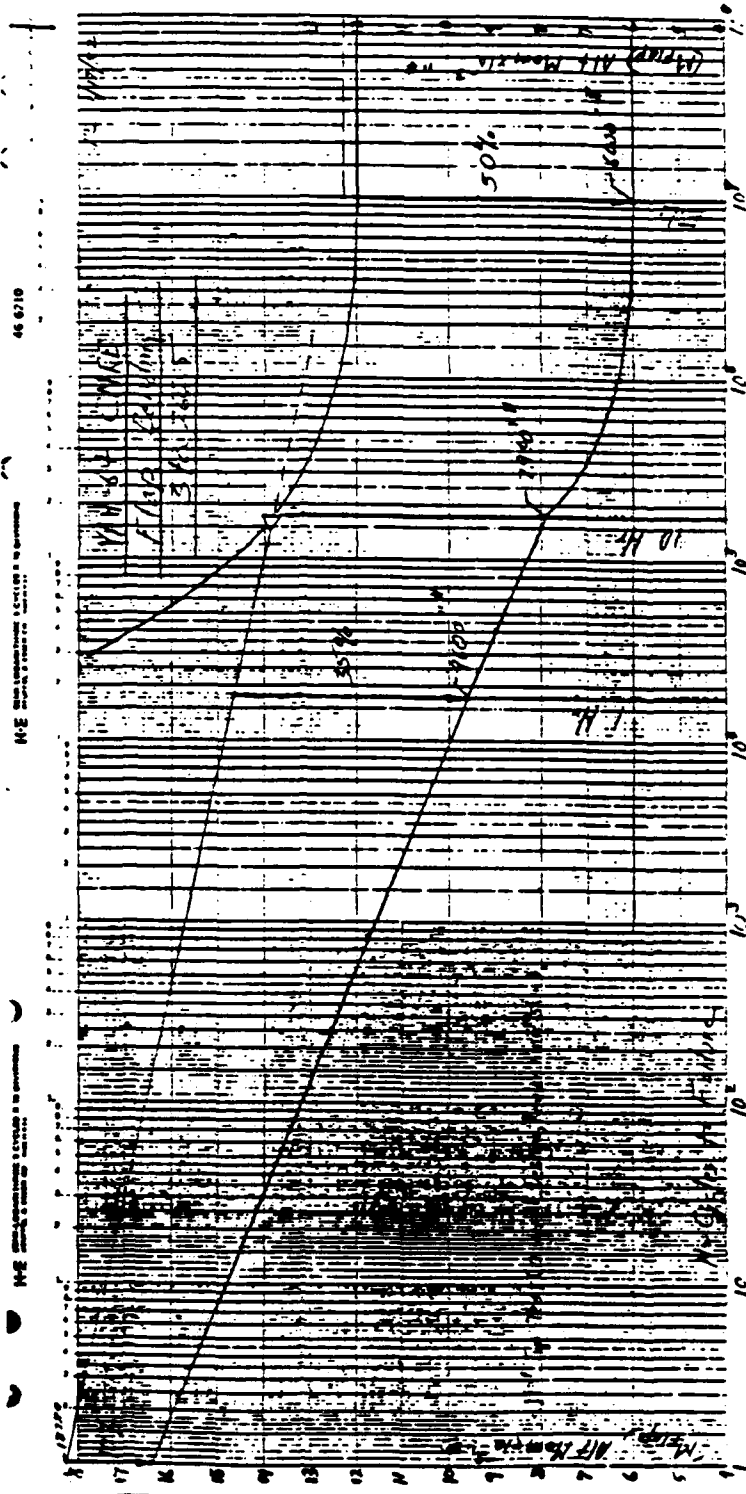






B20.10  
 CIRB-79-006

B20.11  
CMRB-79-006







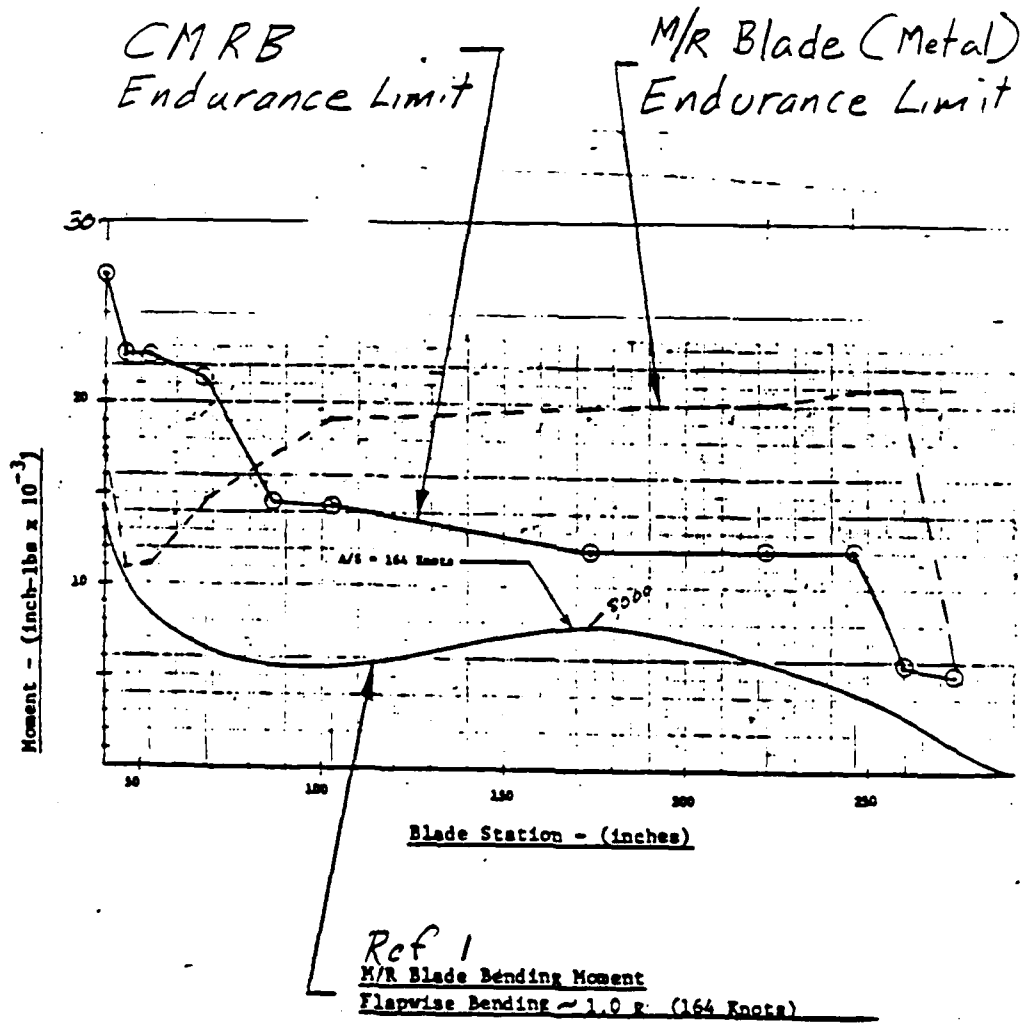
COMPARISON OF THE COMPOSITE M/R BLADE  
ALLOWABLES WITH THE METAL BLADE

		Allowable Loads (Cyclic)						
		Composite Blade			Metal Blade			
Sta	Mom	Endurance Limit (n #)	10 Hour Limit (n #)	1 Hour Limit (n #)	Endurance Limit (n #)	10 Hour Limit (n #)	1 Hour Limit (n #)	
39	M <sub>f</sub>	27,000	33,200	40,500	17,435	25,800	43,580	□
	M <sub>c</sub>	54,000	66,400	81,000	34,860	51,600	87,160	
46	M <sub>f</sub>	22800	28000	37200	10845	16130	27240	*
	M <sub>c</sub>	48000	56000	65000	34860	51600	87160	* 1/4
51.3	M <sub>f</sub>	22800	28000	37200	11,300	12,090	19,970	* 1/2
	M <sub>c</sub>	48000	56000	65,000	×	×	×	*
53	M <sub>f</sub>	22800	28000	37200	×	×	×	*
	M <sub>c</sub>	48000	56000	65,000	32,470	34,700	57,390	*
69	M <sub>f</sub>	21200	25000	30000	14,700	15,700	26,000	*
	M <sub>c</sub>	46000	54000	60800	49,600	51,500	66,400	*
103	M <sub>f</sub>	13920	16700	20800	19000	20,500	33,400	* 1/4
	M <sub>c</sub>	50400	62,900	78,500	50000	52,000	67,000	* 1/2
174	M <sub>f</sub>	12,000	14,300	18,000	19,900	21,500	35,000	* 1/2
	M <sub>c</sub>	50,400	62,900	78,500	58,100	60,400	77,800	*
222	M <sub>f</sub>	12,000	14,300	18,000	20,400	22,000	35,900	* 1/2
	M <sub>c</sub>	50,400	62,900	78,500	×	×	×	*
246	M <sub>f</sub>	12,000	14,300	18,000	21,100	22,800	37,100	* 1/2
	M <sub>c</sub>	50,400	62,900	78,500	57,000	59,300	76,400	*
260	M <sub>c</sub>	6000	7900	9600	21100	22800	37,100	* 1/4
266.5	M <sub>c</sub>	3700	4900	5800	×	×	×	*
274	M <sub>f</sub>	5300	6770	8400	4090	4900	9300	*
	M <sub>c</sub>				×	×	×	*
104.5	M <sub>c</sub>	10,850	13,000	15,800	8000	8,640	14,000	□

\* 45° and 0° Curve shapes used  
□ 0° Curve Shape used

# FLAP BENDING

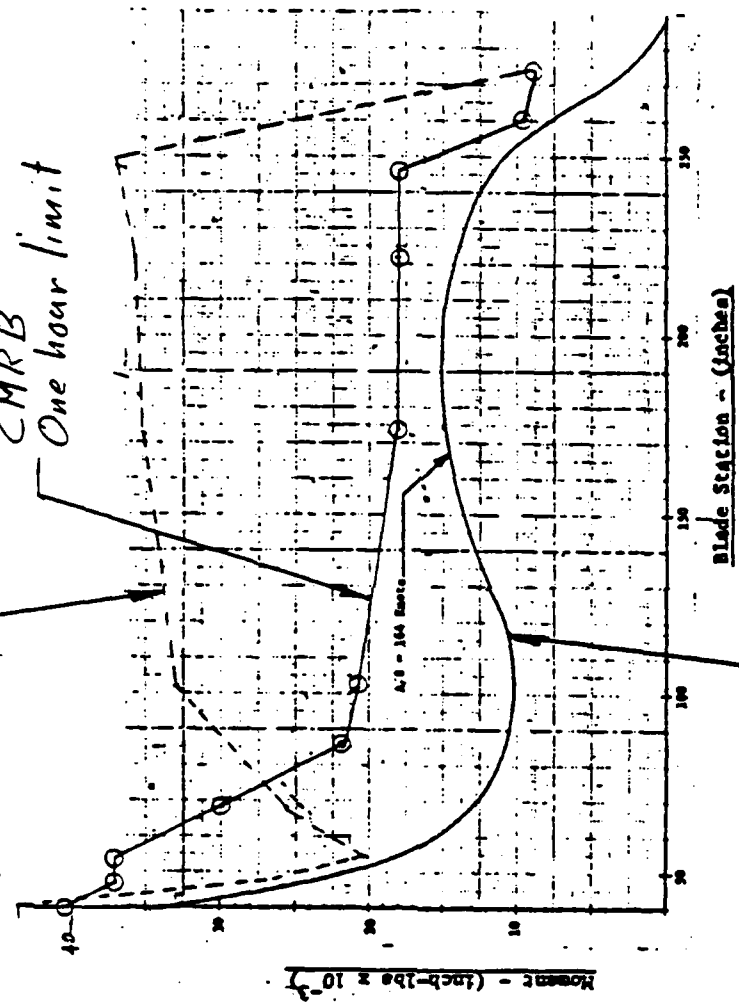
26 BLADE STA.



Flap Bending vs Blade  $\tau_a$

M/R Blade (Metal)  
One hour limit

CMRB  
One hour limit



Ref 1  
M/R Blade Bending Moment  
Flap-line Bending - Manoeuvre 2.5A (164 Knots)

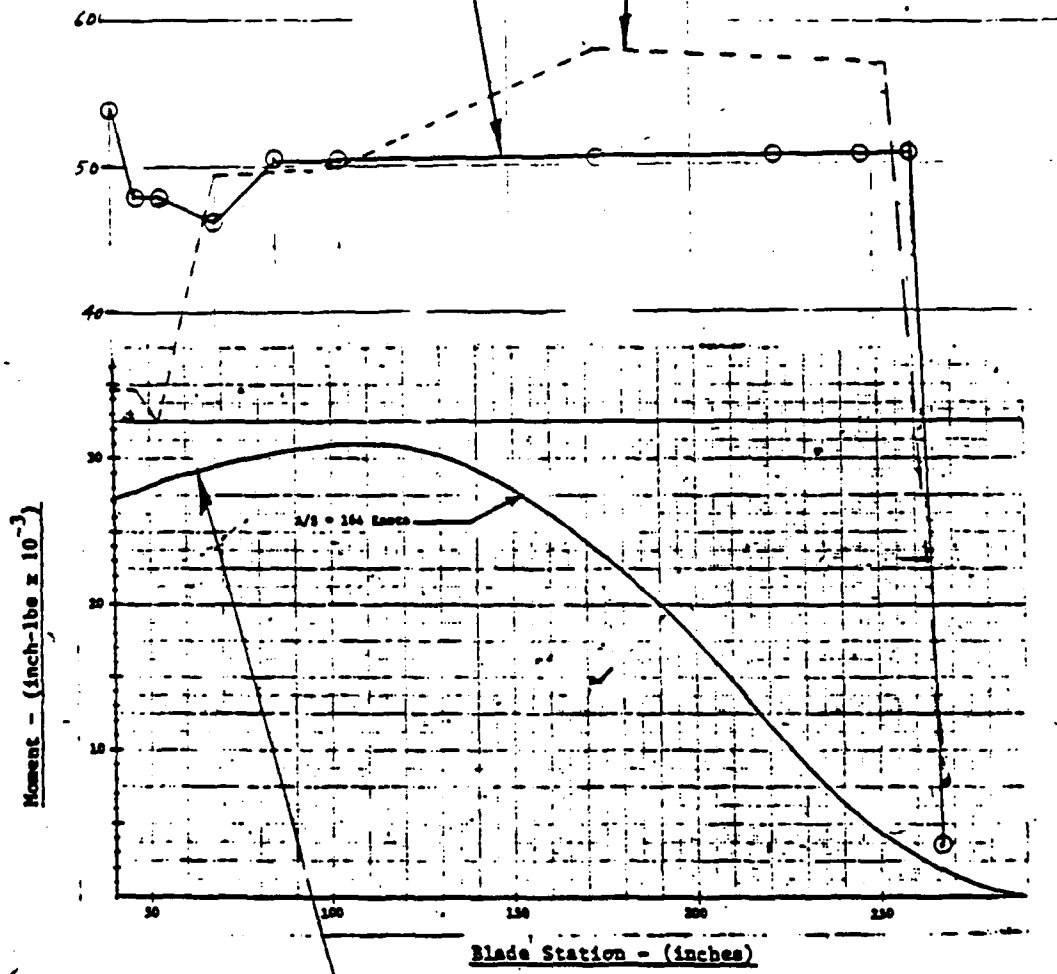
B40.02  
CMRB-79-006



# Chord Bending vs Blade Sta.

CMRB  
Endurance limit  
Chord Bending

M/R Blade (Metal)  
Endurance limit  
Chord Bending

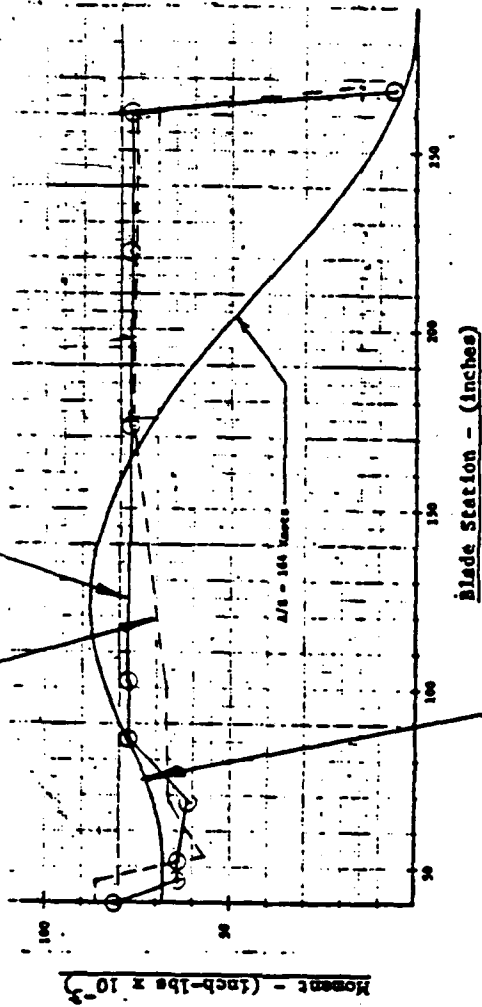


Ref 1  
M/R Blade Bending Moment  
Chordwise Bending ~ 1.0 g (164 Knots)

# Chord Bending vs Blade Sta

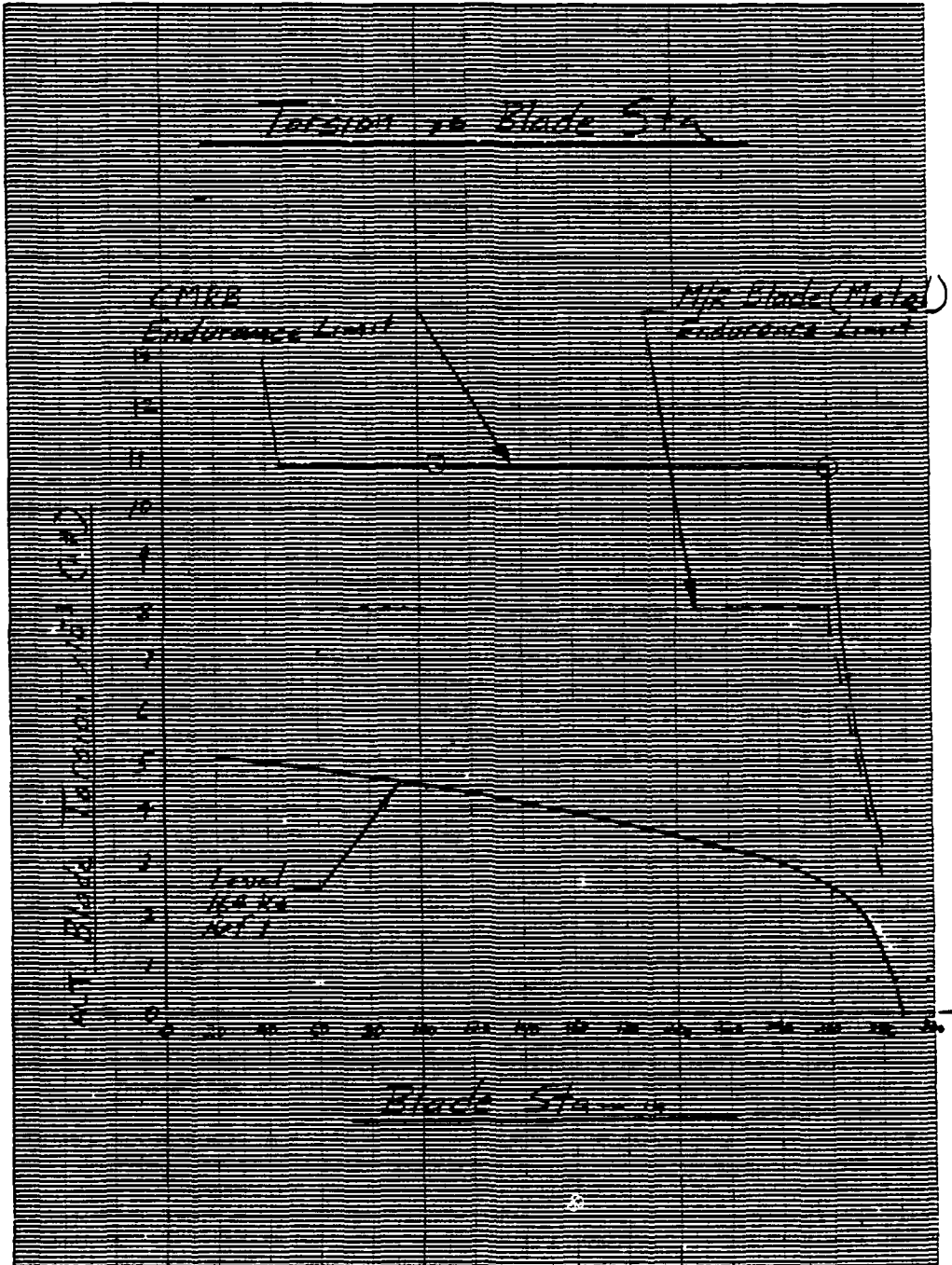
M/R Blade (Metal)  
One hour limit

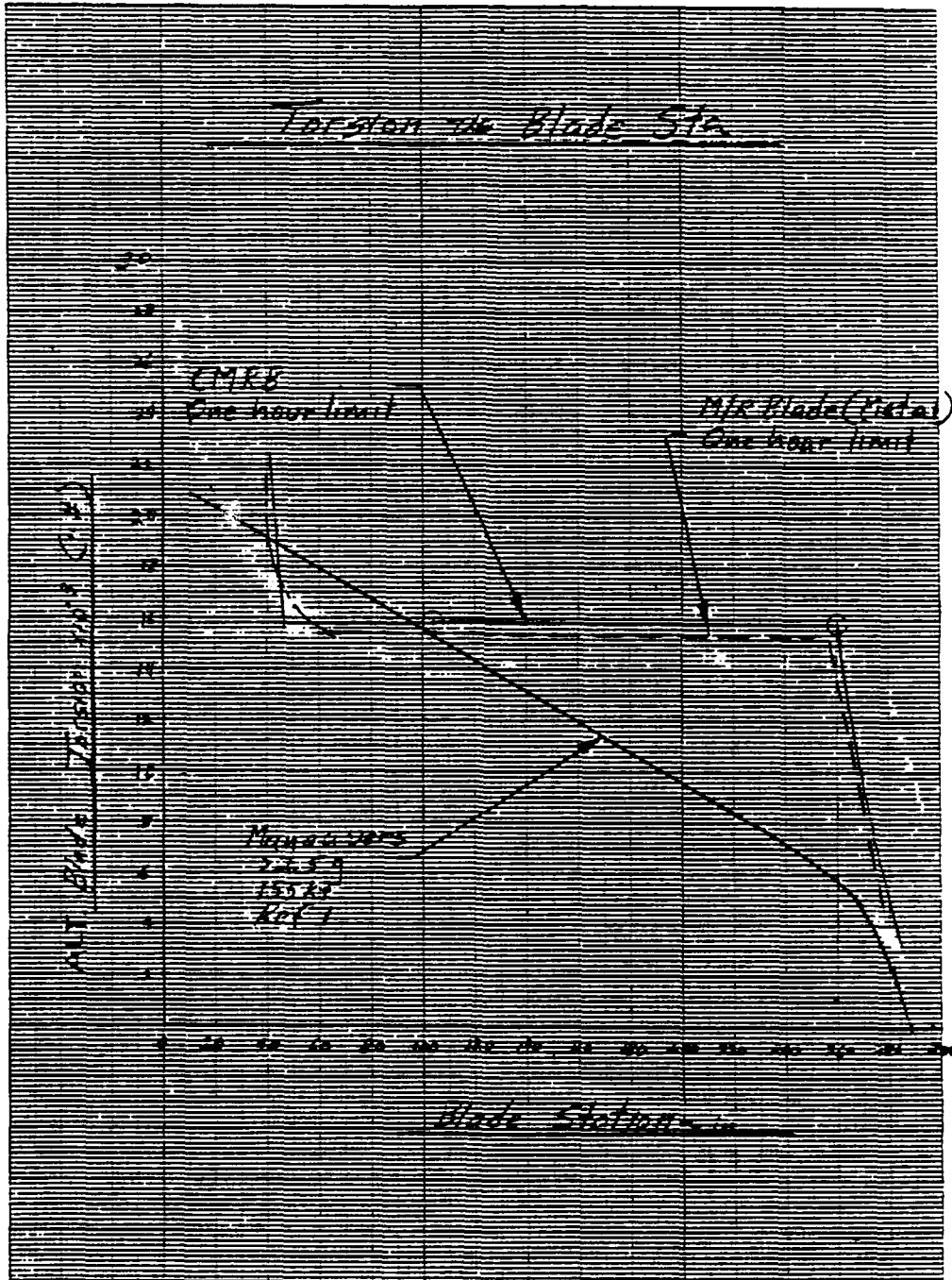
CMRB  
One hour limit



Ref 1

M/R Blade Bending Moment  
Chordwise Bending - Maneuvers 2.5g (164 Knots)





APPENDIX C

STRUCTURAL ANALYSIS OF A BALLISTICALLY  
DAMAGED COMPOSITE MAIN ROTOR  
BLADE FOR THE  
AH-64A HELICOPTER



REPORT TITLE		REPORT NO.	
Static Stress Analysis for the YAH-64 AAH CMRB		CMRB-79-005	
PREPARED BY	4-7-82	CHECKED BY	MODEL NO.
D. Mancill			YAH-64

SUBJECT

INTRODUCTION

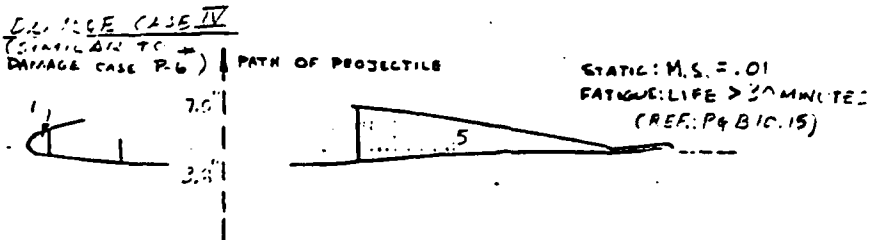
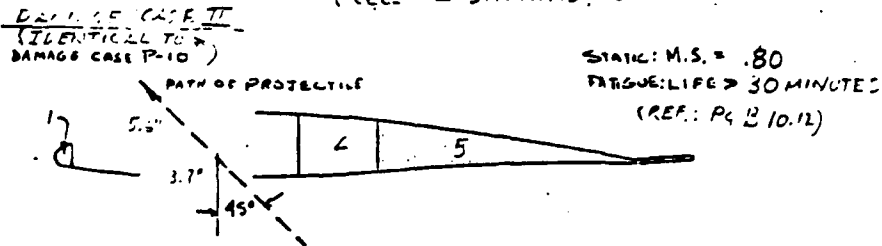
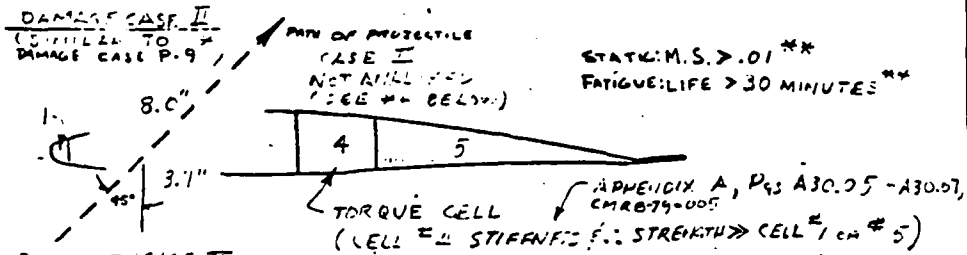
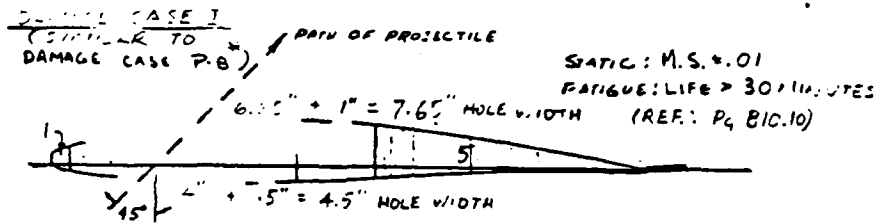
This appendix contains the structural analysis of the ballistically damaged YAH-64 CMRB.

Based on this analysis, there will be no failure at the limit vulnerability condition ( $N_2 = 2.0g$ ,  $V = 150$  kn, RPM 289). The fatigue life of the CMRB after sustaining ballistic damage is greater than 30 minutes.

The damage model is based on an impact by a 23mm high explosive incendiary (HEI) projectile. Extent of the ballistic damage is based on experience with the metal YAH-64 main rotor blade and the composite multi-tubular spar main rotor blade for the AH-1G.

REPORT TITLE STATIC STRESS ANALYSIS FOR THE YAH-64 AAH CMRE		REPORT NO. CMRB-79-005
PREPARED BY J. CRANDELL 4-15-82	CHECKED BY	MODEL NO. YAH-64
SUBJECT		

SUMMARY



\* REF: P4 5.35, HUGHES HELICOPTERS REPORT NO. 77-5-1002, STRUCTURAL ANALYSIS OF BALLISTICALLY DAMAGED MRB FOR YAH-64 AAH, 30 APR 1974.  
 \*\* SIMILAR TO DAMAGE CASE I, BUT WITH 3 TORQUE CELLS REMAINING INSTEAD OF 2; ∴ LESS CRITICAL BY INSPECTION (NO DIFFERENTIAL BENDING).



Table C-1. Main Rotor Blade Preliminary Vulnerability Loads

$n_z = 2.0g$ ,  $V = 150$  kn,  $RPM = 289$

r (in.)	$M_F$ (in-lb)		$M_C$ (in-lb)		$M_T$ (in-lb)	
	Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
11.0	N.A.				-8200	15900
25.0	+3500	20200	N.A.			
34.5	+5600	27600	32000	50200		
44.5	+3900	30800	29800	52500	-8200	8500
59.5	+ 900	27100	26700	55300	-6800	8600
87.0	-2900	14700	20100	69400	-5300	8100
121.9	-4300	13200	15500	77800	-4300	8000
156.8	-5700	15800	10600	71000	-3100	7900
191.7*	-5700	24000	6600	50900	-2400	8100
226.6	-3200	24600	3500	31400	-2200	8000
256.0	+4100	14100	640	12000	-1900	5600
273.0	+1700	8300	160	4300	-1200	2700
					- 500	1110

CONSTANT  
SECTION  
OUTBD

REF.: Table C-7, Pg 11, Hughes Helicopters Report No. 77-5-8000-2, Apr. '81

**SIGN CONVENTION:**

- (+)  $M_F$  ~ COMPRESSION IN UPPER SURFACE
- (+)  $M_C$  ~ COMPRESSION IN TRAILING EDGE
- (+)  $M_T$  ~ NOSE UP

\* CRITICAL STATION DUE TO THE HIGHEST COMBINATION OF MOMENTS AND TORSION, GOVERNED BY FLAPWISE BENDING.

Table C-2. Main Rotor Blade Preliminary Vulnerability Fatigue Spectrum

r (in.)	Number of Cycles	M <sub>F</sub> (in-lb)		M <sub>C</sub> (in-lb)		M <sub>T</sub> (in-lb)	
		Mean	Cyclic	Mean	Cyclic	Mean	Cyclic
25	20	3500	13700	-	-	-8200	10800
	29	3500	13700	-	-	-6800	8500
	96	3500	8200	-	-	-4800	5400
	983	negl.	2800	-	-	-2900	2500
	7542	negl.	1900	-	-	-1900	1850
34.5	20	5600	18700	32000	31800	-8200	8400
	29	5600	18700	32000	29600	-6800	6600
	96	5600	11200	30000	22700	-4800	4200
	983	negl.	3700	-4000	14500	-2900	2000
	7542	negl.	2500	-4000	11600	-1900	1450
44.5	20	3900	20800	29800	41500	-7500	8600
	29	3900	20800	29800	38600	-6200	5900
	96	3900	12400	27700	29600	-4400	3700
	983	negl.	5000	-3700	14900	-2700	1000
	7542	negl.	3400	-3700	11900	-1700	700
226.55*	20	-3200	16600	3500	31400	-2100	6800
	29	-3200	16600	3500	29200	-1700	5400
	96	-3200	9900	3500	22400	-1200	3400
	983	negl.	3400	negl.	4100	-700	1600
	7542	negl.	2300	negl.	3300	-500	1200

REF: Table A-10, Hughes Helicopters Report No. 77-5-8000-2, April 1981

NUMBER OF LOAD CYCLES FOR 30 MINUTES FOR  
 ONCE/REVOLUTION OCCURRENCE:

$$N = 30 \times 289 = 8670 \text{ CYCLES}$$

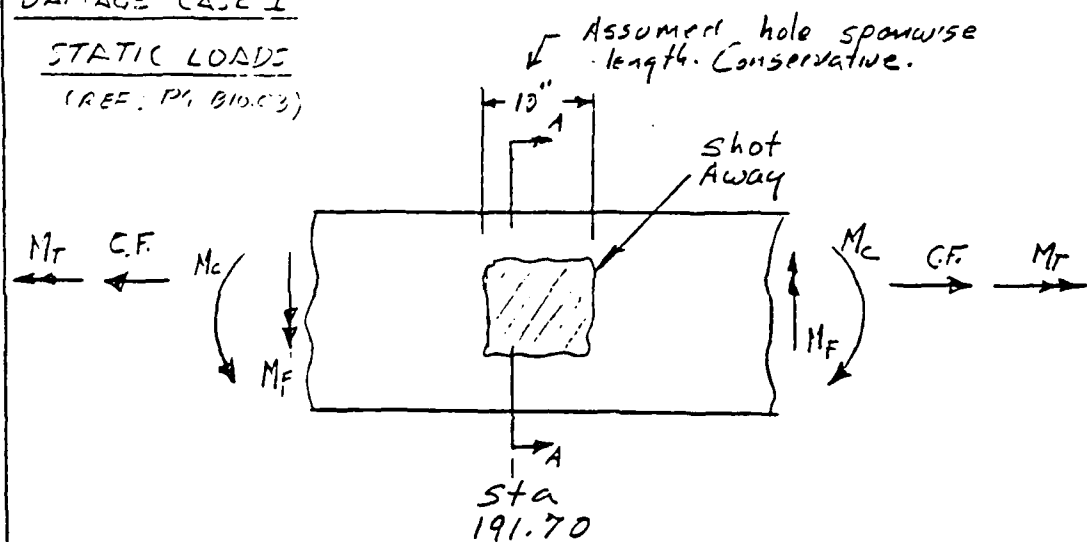
\* CRITICAL STATION FOR MAXIMUM LOADING AT CONSTANT  
 SECTIONAL AREA OF STA. 870.

REPORT TITLE		REPORT NO. CMRB-79-005
PREPARED BY AZ	4/12/83	CHECKED BY
SUBJECT CMRB Ballistic Ana		MODEL NO. YAH-64

DAMAGE CASE I

STATIC LOADS

(REF: PG B10.03)



$$M_F = (-5700 \pm 24,000) \cdot 0.8^* = -4,560 \pm 19,200$$

$$M_c = 6,600 \pm 50,900$$

$$M_T = -2,200 \pm 8,000$$

AND  
 $CF = 36,000^{\#}$  FOR 285 RPM (REF: PG 220.01)

\* Testing of ballistically damaged rotor blades at Hughes indicates that the damage area acts like a partial elastic hinge which will reduce the flapwise moment by 20%. This is shown on pg 9 of the following ref:

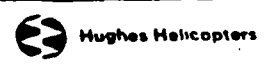
Paper No. 12

Damage Tolerant Design of the YAH-64 Main Rotor Blade

Malcolm F. Symonds  
 Chief, Rotor Analysis

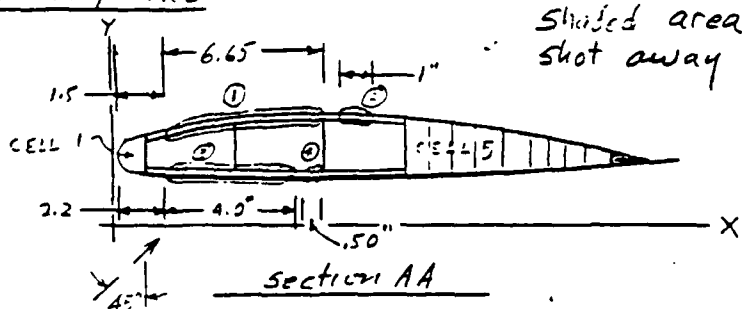
Hughes Helicopters  
 Division of Summa Corporation  
 Culver City, California

Presented at the AHS/Ames Conference on Helicopter Structures Technology, Nov. 16-18, 1977.



REPORT TITLE		REPORT NO.
PREPARED BY MPC		CMRB-79-005
4/9/82	CHECKED BY	MODEL NO.
SUBJECT CMRB Ballistic Aug.		YAH-69

## Section Properties (DAMAGE CASE I)



\* Ref APPA CMRB-79-505 P. A30.02

	EA	X	Y	EAX	EAY	EI <sub>c</sub>	EAY	EAY <sup>2</sup>	EI <sub>F</sub>
Basic Section*	34.39	5.09	1.491	173.32	275.56	925.5	51.27	76.45	12.7
①	-6.17	4.32	2.43	-30.54	-145.1	-23.17	-14.99	-36.43	-2.02
②	-9.361	9.8	2.553	-9.17	-90.0	-.08	-2.39	-6.10	-.0
③	-3.83	4.272	.772	-16.2	-68.6	-5.2	-2.96	-2.28	-.014
④	-.468	7.04	.747	-3.29	-23.2	-9.8	-.35	-.261	-.0

22.99

114.6

546.7

945.3

30.58

31.38

12.48

$$\bar{X} = \frac{114.6}{22.99} = 5.0''$$

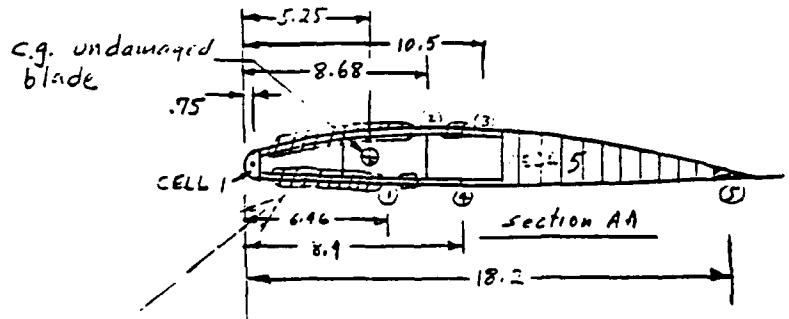
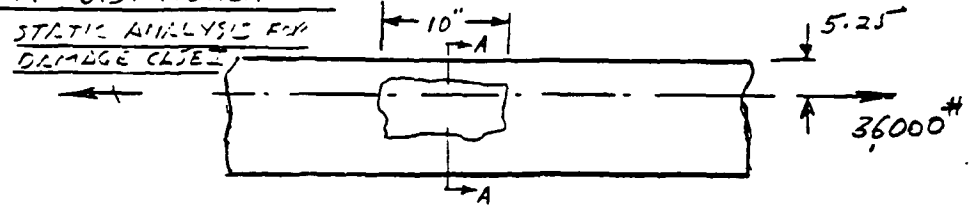
$$\bar{Y} = \frac{30.58}{22.99} = 1.33''$$

$$EI_F = 12.48 + 31.38 - 1.33 \times 30.58 = 3.2 \text{ LB-IN}^2$$

$$EI_c = 546.7 + 945.3 - 5.0 \times 114.6 = 919 \text{ LB-IN}^2$$

REPORT TITLE	REPORT NO. CMRB-79-005
PREPARED BY APC	CHECKED BY
4/12/82	MODEL NO. YAH-64
SUBJECT CMPB Ballistic Ana.	

C.F. Distribution



AREA	EA	X	EAX
1) .6 x .185 x 5.06	.562	6.46	3.65
2) 1.15 x .185 x 5.06	1.08	8.68	9.40
3) .2 x .185 x 5.06	.187	10.5	1.97
4) 3.2 x .185 x 5.06	3.0	2.9	26.66
5) .11 x 17.25	1.9	18.2	34.5
	6.7		76.13

$$x = \frac{76.13}{6.7} = 11.36$$

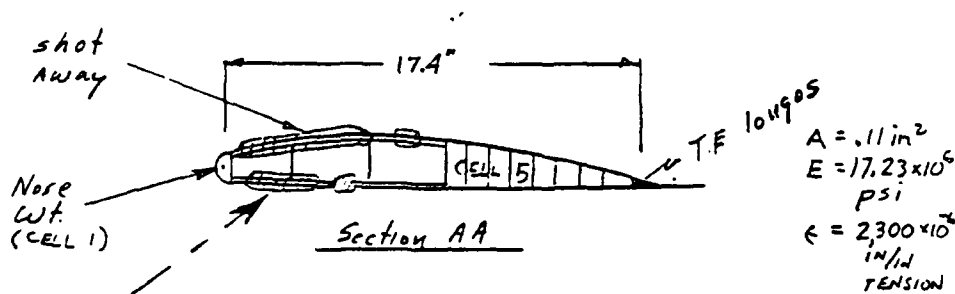
In the damaged area the c.f. distributes to the fwd end aft portion of the remaining structure as follows:

$$C.F. \text{ aft section} = \frac{5.25 - .75}{11.4 - .75} \times 36000 = 15,200\#$$

$$\text{Strain on aft portion of remaining structure} = \frac{15,200}{6.7} = 2300 \text{ u/in Ten. due to C.F.}$$

REPORT TITLE	REPORT NO. CMRB-79-005
PREPARED BY LPC	CHECKED BY 4/12/82
SUBJECT CMRB Ballistic Ana.	MODEL NO. YAH-64

### Resistance of $M_c$ (DAMAGE CASE I)



$$M_c = 6,600 \pm 50,900 = 57,500 \text{ } \# \text{ Cm. in T.E. longos; Ten Nose Wt.}$$

Assuming  $M_c$  is resisted as a couple load at the Nose wt and T.E. longos:

$$\text{Com. load in } T.E. \text{ longos } = \frac{57,500}{17.4} = 3,304 \text{ } \#$$

$$\text{CF. load resisted by the T.E. longos } = .11 \times 2,300 \times 17.23 = 4,359 \text{ } \# \text{ Ten load.}$$

Ref CMRB 79-005 App. A, P. A51.05

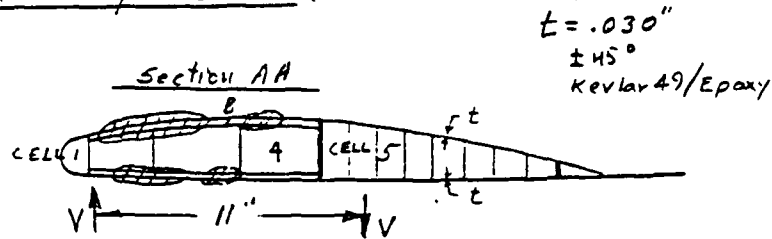
$$\text{Column load that the T.E. longos can resist } = 16,900 \times .11 = 1,859 \text{ } \# \text{ Allowable compression load.}$$

$$M.S. = \frac{4,359 + 1,859}{3,304} - 1 = .88$$

Above M.S. shows that the damaged blade will resist chordwise bending.

REPORT TITLE		REPORT NO. CMRB-79-005
PREPARED BY MPC	4/9/82	CHECKED BY
SUBJECT CMRB Ballistic Anal.		MODEL NO. YAH-64

Torque resisted by cell \*5 (DAMAGE CASE I)



$t = .030''$   
 $\pm 45^\circ$   
Kevlar 49/Epoxy

$$\left. \begin{array}{l} \text{"g" resisted} \\ \text{by skin} \end{array} \right\} = 15,600 \times .030 = 468 \text{ #/in}$$

$$q = \frac{T}{2A}$$

Allowable Shear for Kevlar/Epoxy

Appendix A P. A30.05 CMRB-79-005

$$T = 468 \times 2 \times 7.02 = 6,570 \text{ #}$$

Remaining torque is resisted as a couple as shown where:

$$V = \frac{8000 + 2200 - 6,570}{11} = 330 \text{ #}$$

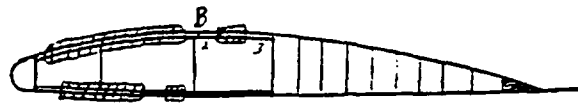
Remaining torque is resisted as differential bending. See analysis for point "B" shown above.

\* CELL 1 CONSERVATIVELY NEGLECTED (CONTRIBUTION SMALL).

REPORT TITLE		REPORT NO. CMRB-79-005
PREPARED BY LPC	4/12/82	CHECKED BY
SUBJECT CMRB Ballistic Ana.		MODEL NO. YAH-64

Resistance of  $M_F$ ,  $M_T$  and C.F. (DAMAGE CASE I)

Point "B" critical



$$M_F = -4,560 \pm 19,200 = 14,640 \text{ " # } \text{ COM. upper surface.}$$

$$\text{Mom at edge of damaged area due to differential bending} \left. \begin{array}{l} \text{Due to} \\ \text{CF} \end{array} \right\} = \frac{I_D}{z} \times 330 = 1,650 \text{ " #}$$

↓ Damaged area length

$$\text{Strain at "B"} \left. \begin{array}{l} \text{Due to} \\ \text{CF} \end{array} \right\} = 2,300 - \frac{1,650}{1.8 \times (1.27)} - \frac{14,640 \times 1.17}{3.2}$$

Distance between caps      cap area

$$= 3,700 \mu \text{ " / " } \text{ COM.}$$

(REF: Pg 1310.15)

$$MS = \frac{3,750}{3,700} - 1 = \underline{\underline{.01}}$$

Ref stress strain curve  
↓ (Pg 1310.15)

Above M.S. shows damaged area of blade will resist  $M_F$ .



REPORT TITLE		REPORT NO.
PREPARED BY	CHECKED BY	CMRB-79-005
JC	4/15/82	MODEL NO. YAH-64
SUBJECT		
CMRB BALLISTIC ANA		

DIVISION CASE I

FATIGUE ANALYSIS AT STA. 226.57 (SAME X-SECT. AS AT STA 191.7)

C.F. = 36,000 LB. @ 209 RPM

$M_D = (-3,200 \pm 16,600) \times 8^* = -2,560 \pm 13,280 \text{ IN-LB}$

$M_C = 3,570 \pm 31,400 \text{ IN-LB}$  (FATIGUE LOAD REF.: PG. B10.04)

$M_T = -2,100 \pm 6,800 \text{ IN-LB} \Rightarrow 0 \pm 2330 \text{ IN-LB}^{**}$

VERY CONSERVATIVELY LET  $N = 8670$  CYCLES; THEN:

$$f = \frac{-(-2,560 \pm 13,280) \cdot 1.17}{3.2} - \left( \frac{\pm 2330 \times 10}{11} \times \frac{10}{2} \right) / 1.871.27 + 2,300 @ \text{PT. B}$$

$= 936 \pm 4,876 \pm 463 + 2,300$

$= 3,236 \pm 5,319 \text{ IN-LB}$

$E = 10.66 \times 10^6 \text{ PSI FOR KEVLAR/EPXY LAMINATES}$

$f = fE = 34,500 \pm 56,700 \text{ PSI}$

$= 91,200 \text{ PSI (TENS.)}, -22,200 \text{ PSI (COMPR.)}$

$F_{tu}' = 165,000 \text{ PSI}$  (Pg B10.13 OR B10.17)

$F_{tc}' = 31,980 \text{ PSI}$  (Pg B10.13)

TENS. M.S. =  $\frac{165,000}{91,200} - 1 = \underline{\underline{.75}}$   
 COMPR. M.S. =  $\frac{31,980}{-22,200} - 1 = \underline{\underline{.44}}$  } > STATIC M.S. = .01

THEREFORE, BY INSPECTION, LIFE AFTER IMPLICIT IS MUCH GREATER THAN 30 MINUTES & LESS CRITICAL THAN FOR THE STATIC COND. (Pg B10.10).

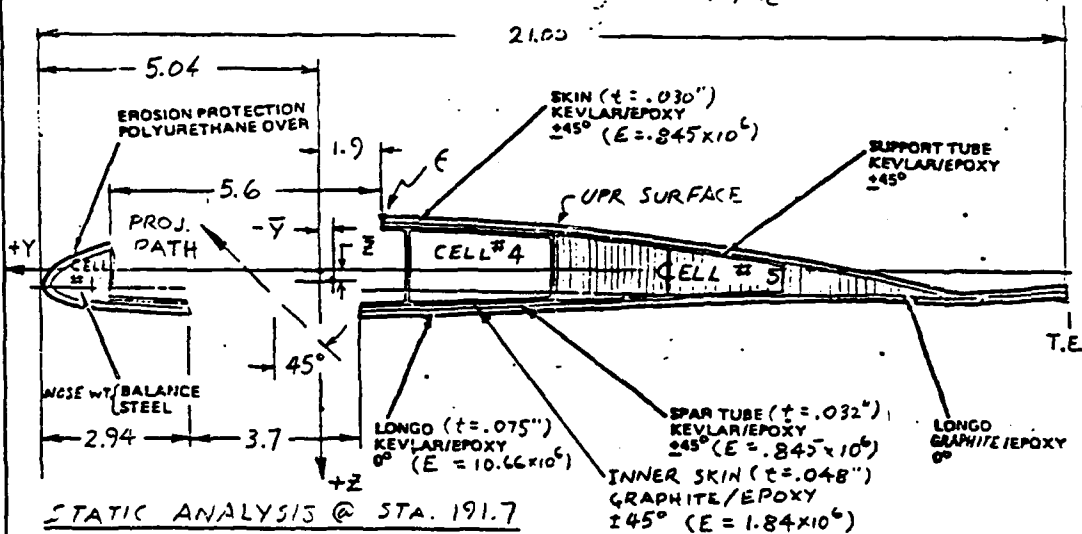
\* CELL 5 RESISTS 3,510 IN-LB (Pg B10.09).

\* SEE PG B10.05.

REPORT TITLE <b>STATIC STRESS ANALYSIS FOR THE YAH-64 AAH CMRB</b>		REPORT NO. <b>CMRB-79-005</b>
PREPARED BY <b>J.L. CRANDELL</b>	CHECKED BY	MODEL NO. <b>YAH-64</b>
SUBJECT <b>VULNERABILITY ANALYSIS OF CMRB BLADE</b>		

DAMAGE CASE III

(+) M<sub>F</sub> ~ COMPR. UPR SURFACE  
(+) M<sub>C</sub> ~ COMPR. IN T.E.



STATIC ANALYSIS @ STA. 191.7

C.F. = 3 = 300 LB. FOR 289 RPM

M<sub>F</sub> = -5,700 ± 24,000 IN-LB

M<sub>C</sub> = 6,600 ± 50,900 IN-LB @ 1/4 CHORD

M<sub>T</sub> = -2,200 ± 8,000 IN-LB

$\bar{E}A = 25.65 \times 10^6 \text{ LB}$ ,  $\bar{E} = 5.08 \times 10^6$

$\bar{E}I_F = 6.46 \times 10^6 \text{ LB-IN}^2$

$\bar{E}I_C = 963.05 \times 10^6 \text{ LB-IN}^2$

$\bar{z} = .09 \text{ IN}$ ,  $-1.18 - \bar{z} = -1.27 \text{ IN}$

MOMENTS FOR MAX. COMPR. STRAIN,  $\epsilon$ , ARE:  $\bar{y} = -.22 \text{ IN}$ ,  $5.04 - \bar{y} = 5.26 \text{ IN}$

$M'_F = (.8)^* (M_F + C.F. \times \bar{z}) = .8 \times [(-5,700 + 24,000) + 36,000 \times .09] = 17,232 \text{ IN-LB}$

$M'_C = M_C + [(5.04 - \bar{y}) - \frac{5.26 - 5.25}{4}] \times C.F. = (6,600 + 50,900) + .01 \times C.F. = 57,860 \text{ IN-LB}$

RESULTING STRAIN IS (ALL OF M<sub>T</sub> MAINLY REACTED BY STIFF, STRONG CELL #4):

$\epsilon = \epsilon_F + \epsilon_C + \epsilon_{CF} = \frac{M'_F \times (-1.18 - \bar{z})}{\bar{E}I_F} + \frac{M'_C \times (-1.9 - \bar{y})}{\bar{E}I_C} + \frac{C.F.}{EA}$   
 $= \frac{17,232 \times -1.27}{6.46} + \frac{57,860 \times -1.68}{963.05} + \frac{36,000}{25.65} = -2,085 \mu\text{-IN/IN (COMPR)}$

$\epsilon_{ALL} = 3,750 \mu\text{-IN/IN (Pg B10.16)} \ \& \ \text{STATIC M.S.} = \frac{\epsilon_{ALL} - 1}{|\epsilon|} = \frac{3750 - 1}{2,085} = .80$

ABOVE A.I.S. SHOWS DAMAGED AREA OF BLADE WILL RESIST THE APPLIED LOADS.

\* SEE "\*" ON PAGE B10.05.

REPORT TITLE STATIC STRESS ANALYSIS FOR THE YAH-64 ASH CMRB		REPORT NO. CMRB-79-005
PREPARED BY J.L. CRANDALL	CHECKED BY	MODEL NO. YAH-64
SUBJECT VULNERABILITY ANALYSIS OF CMRB BLADE		

FATIGUE ANALYSIS @ STA 226.55 (SAME X-SECT. AS @ STA 191.7)  
(DAMAGE LIFE III)

C.F. = 36,000 LB. @ 287 RPM (FATIGUE LOAD REF.: PG B10.04)

$M_R = -3,200 \pm 16,600$  IN-LB  
 $M_C = 3,500 \pm 31,400$  IN-LB  
 $M_T = -2,100 \pm 6,800$  IN-LB

CONSERVATIVELY LET  
 $N = 8670$  CYCLES  
 FOR 30 MINUTES

$M_R' = .8 \times [(-3,200 + 36,000 \times .09) \pm 16,600] = 40 \pm 13,280$  IN-LB.

$M_C' = (3,500 \pm 31,400) + .01 \times C.F. = 3,860 \pm 31,400$  IN-LB

$f = \frac{(40 \pm 13,280)(-1.27)}{6.46} + \frac{(3,860 \pm 31,400)(-1.68)}{963.05} + \frac{36,000}{25.65}$

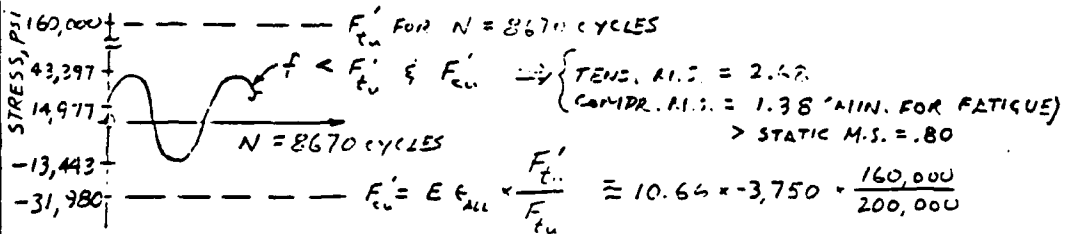
$= (0 \pm 2,611) + (-7 \pm 55) + 1,404$

$= 1,405 \pm 2,666$   $\mu$ -IN/IN\*

$E = 10.66 \times 10^6$  PSI FOR KEVLAR49/EPOXY LONGOS

$f = \epsilon E = 14,977 \pm 28,420$   $\mu$ IN/IN =  $43,397 \mu$ IN (TENS.) /  $-13,423 \mu$ IN (COMP.)

GRAPHICALLY  $f$  IS COMPARED WITH ALLOWABLES FOR  $N=8670$  CYCLES AS FOLLOWS:



THEREFORE, BY INSPECTION, LIFE AFTER IMPACT IS MUCH GREATER THAN 30 MINUTES & LESS CRITICAL THAN FOR THE STATIC COND. (PG B10.12).

\*  $10^{-6}$  IN/IN. \*\* SEE BENT DATA CURVE ON PG B10.17



REPORT TITLE		REPORT NO. CMRB-79-005
PREPARED BY JC	4/15/82	CHECKED BY
SUBJECT CMRB BALLISTIC ANA.		MODEL NO. YAH-64

DAMAGE CASE IV

STATIC LOADS:

$$M_F = .8 \cdot (-5,700 \pm 24,000) = -4,560 \pm 19,200$$

$$M_C = 6,600 \pm 5,090 \quad C.F. = 36,000 \# \text{ FOR } 289 \text{ RPM}$$

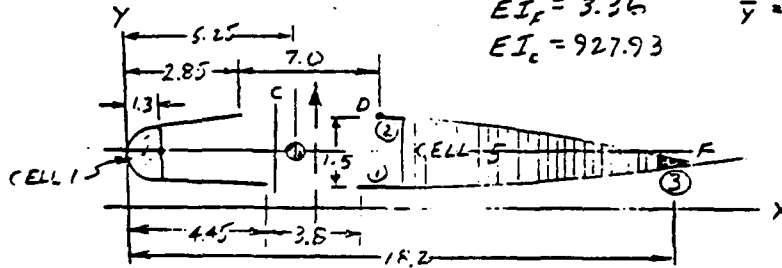
$$M_T = -2,200 \pm 8,000$$

SECT. PROP.

$$EA = 24.25 \quad \bar{x} = 4.49$$

$$EI_F = 3.36 \quad \bar{y} = 1.32"$$

$$EI_C = 927.93$$



C.F. DISTRIBUTION

ELEM	EA	(x-1.3)	EA(x-1.3)
①	$3.25 \times 18.5 \times 5.06 = 3.05$	8.58	26.17
②	$1.65 \times 18.5 \times 5.06 = 1.55$	9.38	14.54
③	$.11 \times 17.23 = 1.90$	16.9	32.11
$\Sigma$	6.50	~	72.82

$$x = \frac{72.82}{6.50} = 11.20"$$

$$C.F. \text{ AFT SECT.} = \frac{5.25 - 1.3}{11.20 - 1.3} \times 36,000 = 14,364 \#$$

$$E \text{ AFT SECT.} = \frac{14,364}{6.50} = 2,210 \text{ lb./in.} \text{ TENS.}$$

\* SEE "F" ON PAGE C10.05.

REPORT TITLE		REPORT NO.
PREPARED BY	4/15/82	C-MRB-79-005
JC	CHECKED BY	MODEL NO.
SUBJECT		YAH-64

STATIC ANALYSIS (DAMAGE CASE IV)RESISTANCE OF  $M_c$ 

$M_c = 57,500 \text{ in}^2$  COMPR. IN T.E. LONGS; TENS. NOSE WT.

ASSUMING  $M_c$  RESISTED AS A COUPLE LOAD AT THE NOSE WT. & T.E. LONGS:

$$\left. \begin{array}{l} \text{COMPR. LOAD IN} \\ \text{T.E. LONGS} \end{array} \right\} = \frac{57,500}{182-13} = 3,402 \#$$

$$\left. \begin{array}{l} \text{CF LOADS RESISTED} \\ \text{BY THE T.E. LONGS} \end{array} \right\} = .11 \times 2,210 \times 17.23 = 4,189 \#$$

$$\left. \begin{array}{l} \text{COLUMN LOAD THAT} \\ \text{T.E. LONGS CAN RESIST} \end{array} \right\} = 16,900 \times .11 = 1,859 \# \quad \begin{array}{l} \text{ALLOW. COMPR.} \\ \text{LOAD} \end{array}$$

$$A.S. = \frac{4,189 + 1,859}{3,402} = \underline{\underline{.77}}$$

RESISTANCE OF  $M_r$ ,  $M_T$  & C.F.

$$M_r = 14,640 \#$$

$$\left. \begin{array}{l} \text{MIN. @ EDGE OF DAMAGED} \\ \text{AREA DUE TO DIFF. BEND.} \end{array} \right\} = \frac{10}{2} \times 330 = 1,650 \text{ in}^2 \quad \begin{array}{l} \text{(PG B10.10)} \end{array}$$

$$\left. \begin{array}{l} \text{STRAIN @ "D" (PG B10.14),} \\ \text{=} \left| \frac{2,210 - 1,650}{1.5 - 1.55} - \frac{14,640 \times 1.19}{3.36} \right| \\ \text{=} 3,685 \mu\text{-IN/IN COMPR.} \end{array} \right\}$$

$$\epsilon_{ALL} = 3,750 \mu\text{-IN/IN}$$

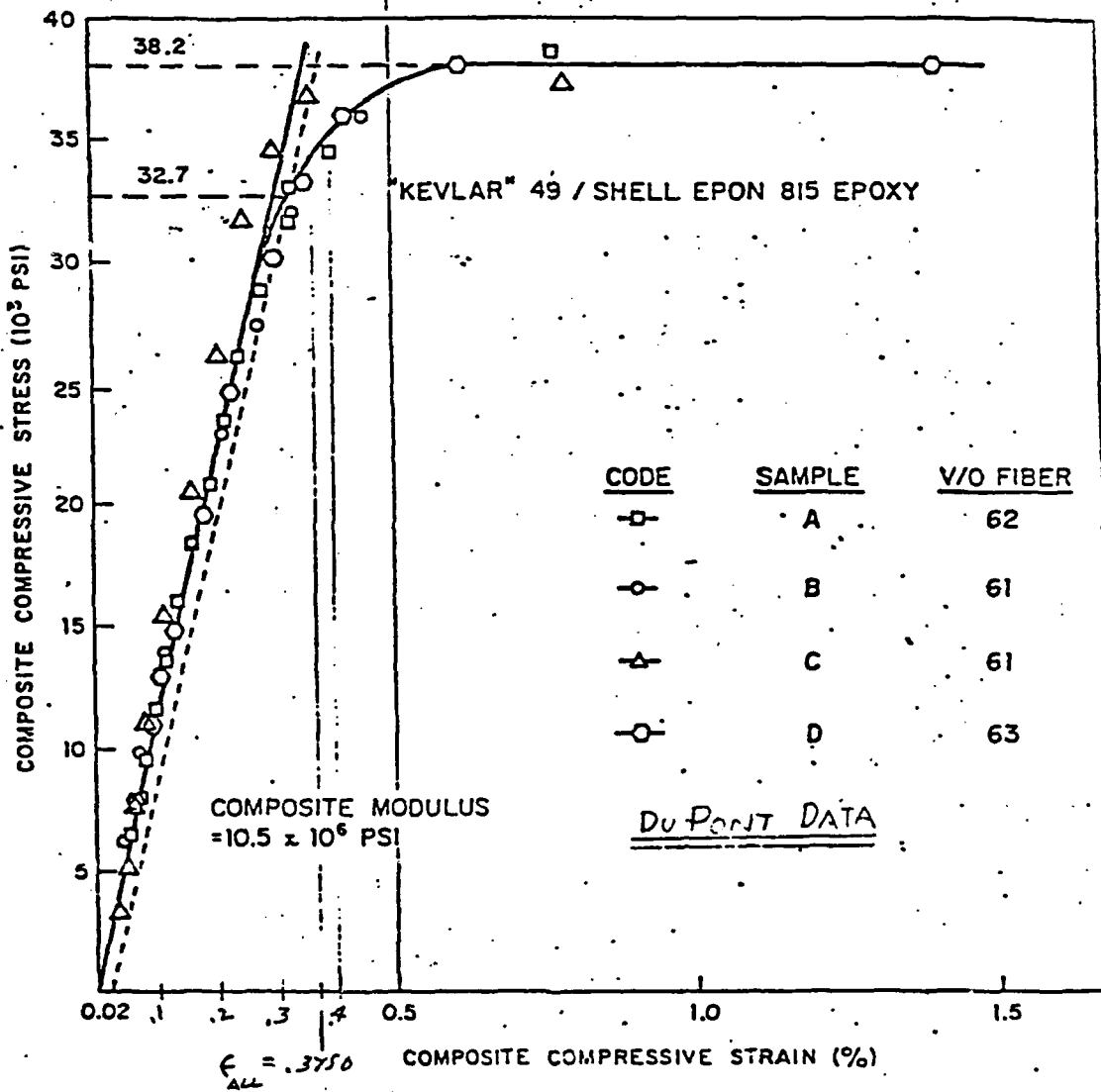
$$A.S. = \frac{3,750}{3,685} - 1 = \underline{\underline{.01}}$$

FATIGUE ANALYSIS (DAMAGE CASE IV)

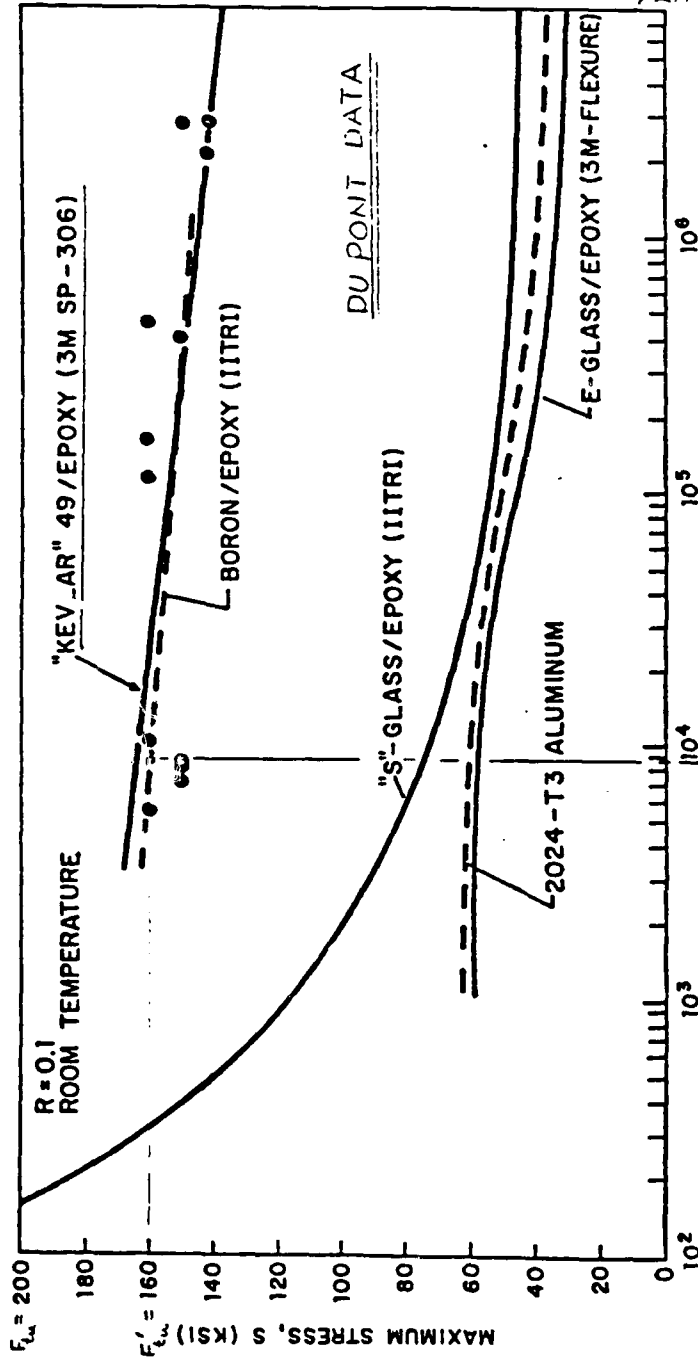
THIS CASE HAS THE SAME STATIC MARGIN-OF-SAFETY AS FOR CASE I; THEREFORE:

- FATIGUE LIFE > 30 MINUTES
- FATIGUE M.S.  $\approx$  .44 (PG B10.11)

UNIDIRECTIONAL COMPOSITE  
COMPRESSIVE STRESS-STRAIN CURVE



TENSION-TENSION FATIGUE BEHAVIOR OF UNIDIRECTIONAL COMPOSITES AND ALUMINUM



CMRB-79-005  
YAH-64

C10.17

NUMBER OF CYCLES TO FAILURE, N

$$\left. \begin{array}{l} 8670 \text{ CYCLES} \\ (30 \text{ MINUTES} \\ \text{OF FLIGHT}) \end{array} \right\} \text{MAX STRESS} \cong \frac{160}{200} \cdot (\text{ULT. STRESS}) = .80 \times (\text{ULT. STRESS})$$

APPENDIX D

DYNAMIC ANALYSIS OF THE COMPOSITE  
MAIN ROTOR BLADE FOR THE  
AH-64A HELICOPTER





This appendix supplements the dynamics section of the CMRB final report. It summarizes mode shapes in Figures D-1a through D-1n that show mode shape plots for the CMRB with cyclic boundary conditions.

At frequencies where there are significant real and imaginary deflections, both components are plotted.

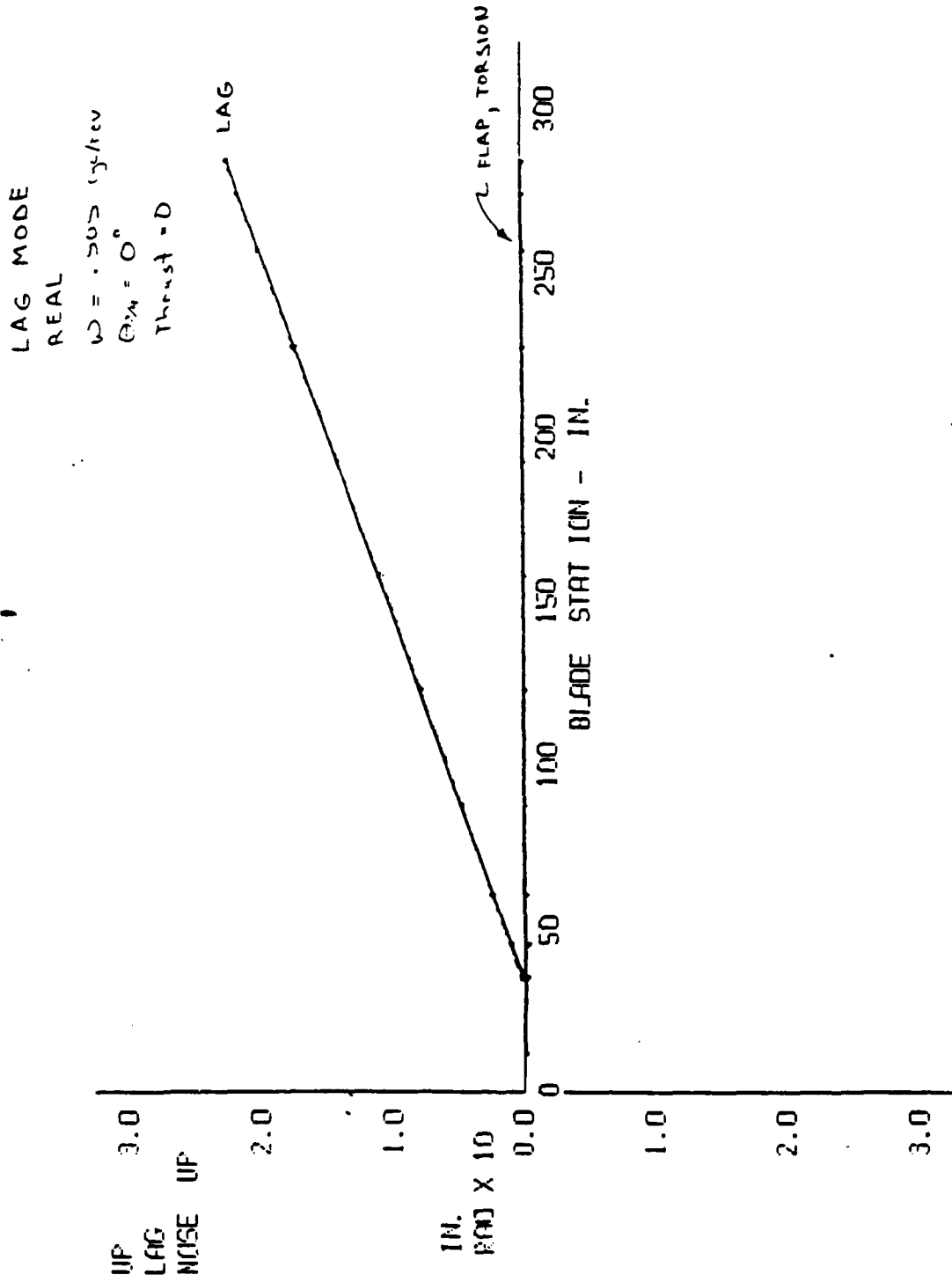


Figure D-1a. CMRB mode shapes.

FLAP MODE  
 REAL  
 $\omega = 1.051 \text{ cycles}$   
 $\theta_{\text{tip}} = 0^\circ$   
 Thrust = 0

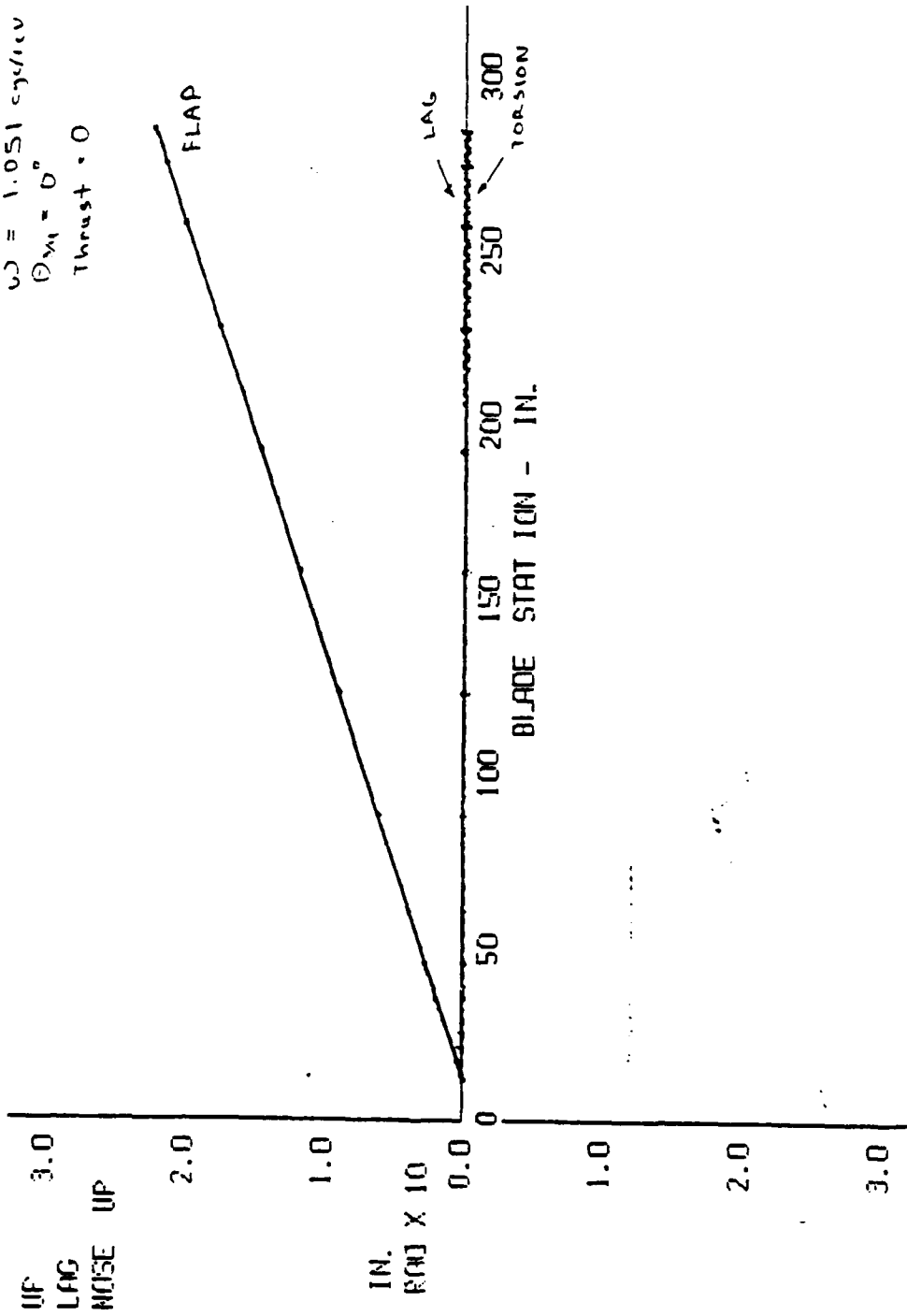


Figure D-1b. CMRB mode shapes.

1<sup>st</sup> FLAP BENDING MODE  
 REAL  
 $\omega = 2.739 \text{ cyc/rev}$   
 $\theta_{\text{tip}} = 0^\circ$   
 Thrust = 0

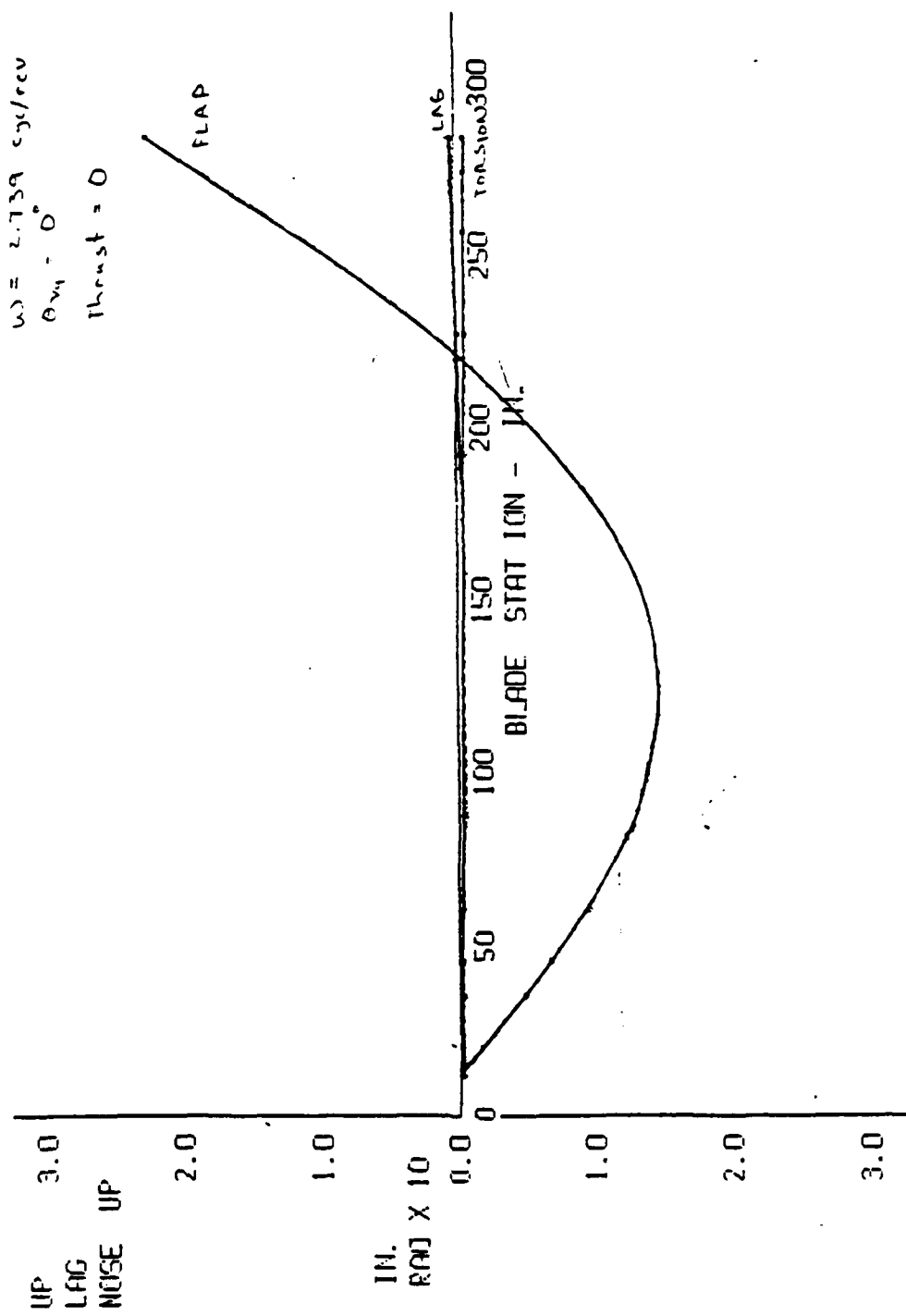


Figure D-1c. CMRB mode shapes.

1<sup>st</sup> FLAP BENDING MODE  
 IMAGINARY  
 $\omega = 2.739$  cyc/rev  
 $\epsilon_{24} = 0$   
 THRUST = 0

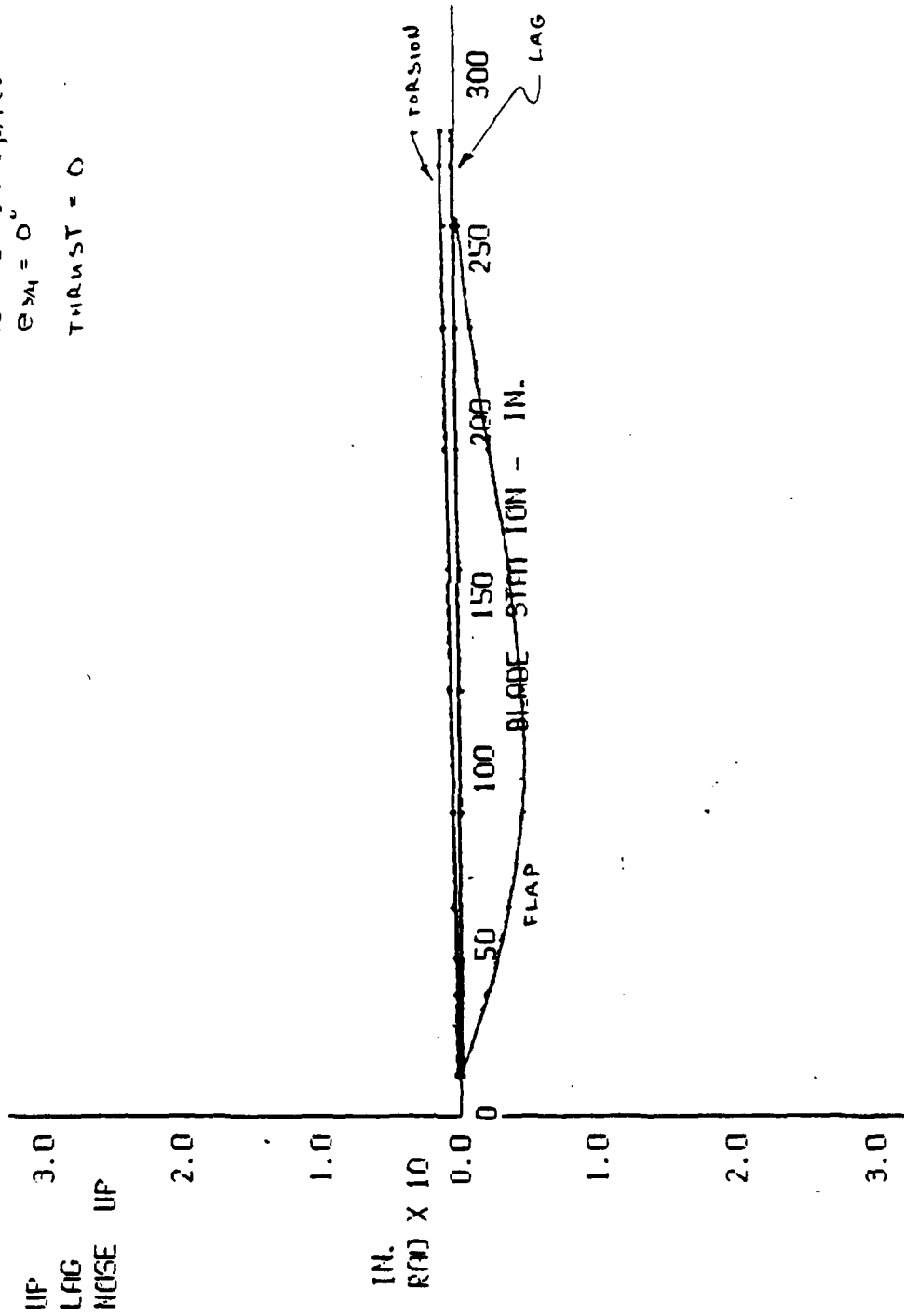


Figure D-1d. CMRB mode shapes.

1<sup>st</sup> TORSION MODE  
 REAL  
 $\omega = 4.272 \text{ cyc/rev}$   
 $\phi_{21} = 0^\circ$   
 THRUST = 0

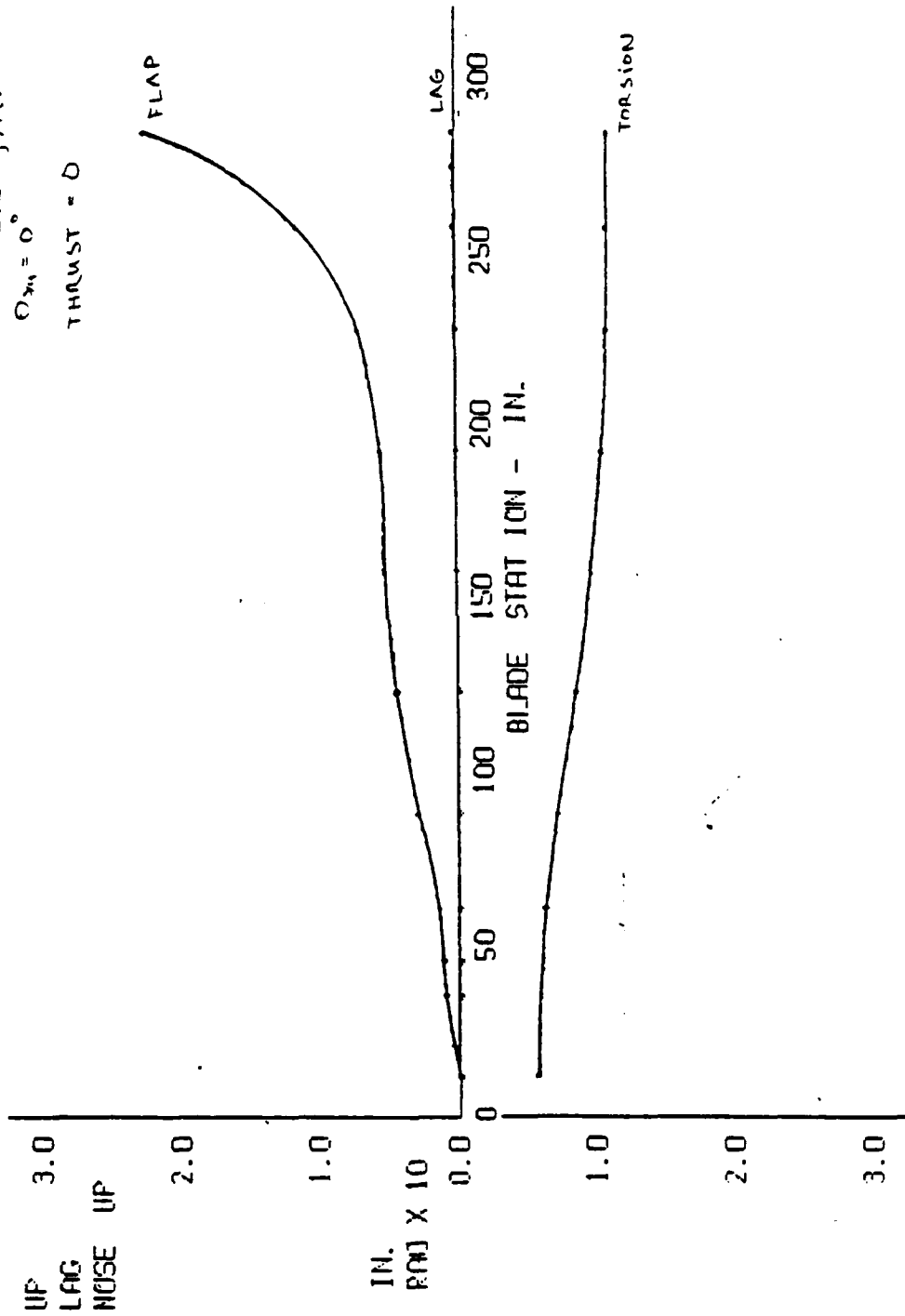
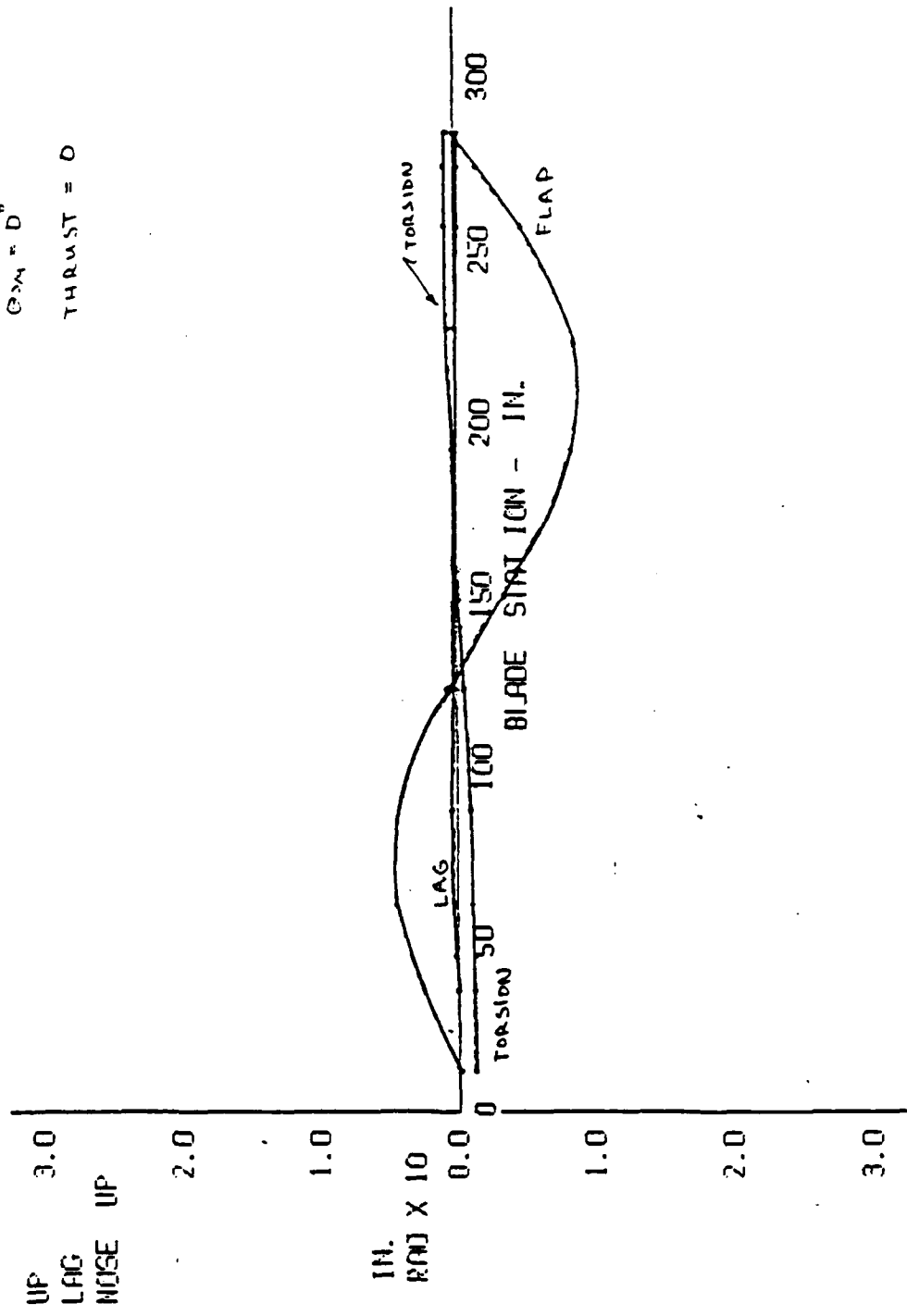


Figure D-1e. CMRB mode shapes.

1<sup>st</sup> TORSION MODE  
 IMAGINARY  
 $\omega = 4.272 \text{ cyc/rev}$   
 $GJ \theta = D$   
 THRUST = 0



D-9

Figure D-1f. CMRB mode shapes.



2<sup>nd</sup> FLAP BENDING MODE  
 REAL  
 $\omega = 4.651 \text{ c/s/r/cv}$   
 $\sigma_{\text{flap}} = 0$   
 THRUST = 0

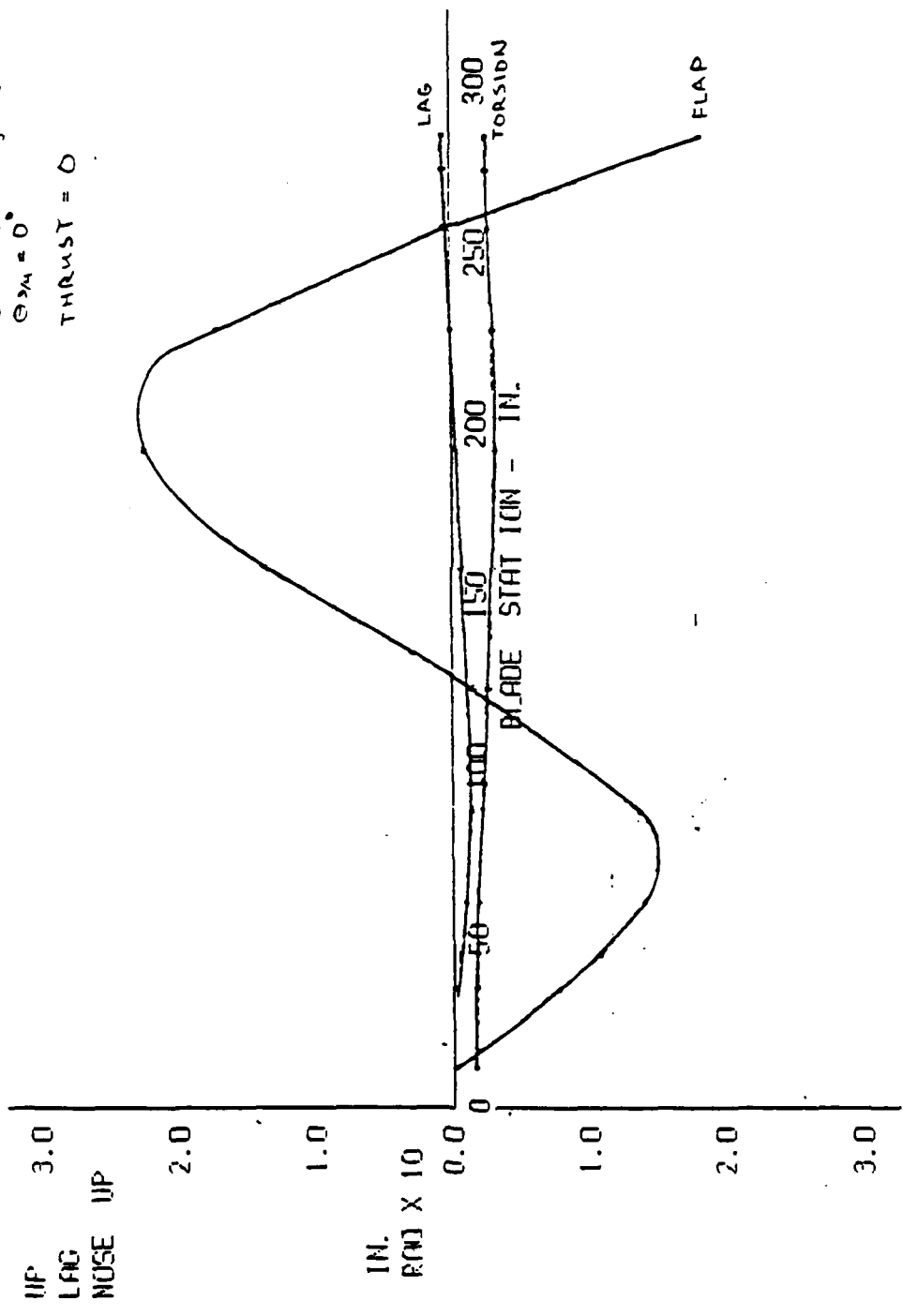


Figure D-1g. CMRB mode shapes.

2<sup>nd</sup> FLAP BENDING MODE  
 IMAGINARY  
 $\omega = 4.651 \text{ } \omega_r / \text{rev}$   
 $\theta_{3M} = 0^\circ$   
 THRUST = 0

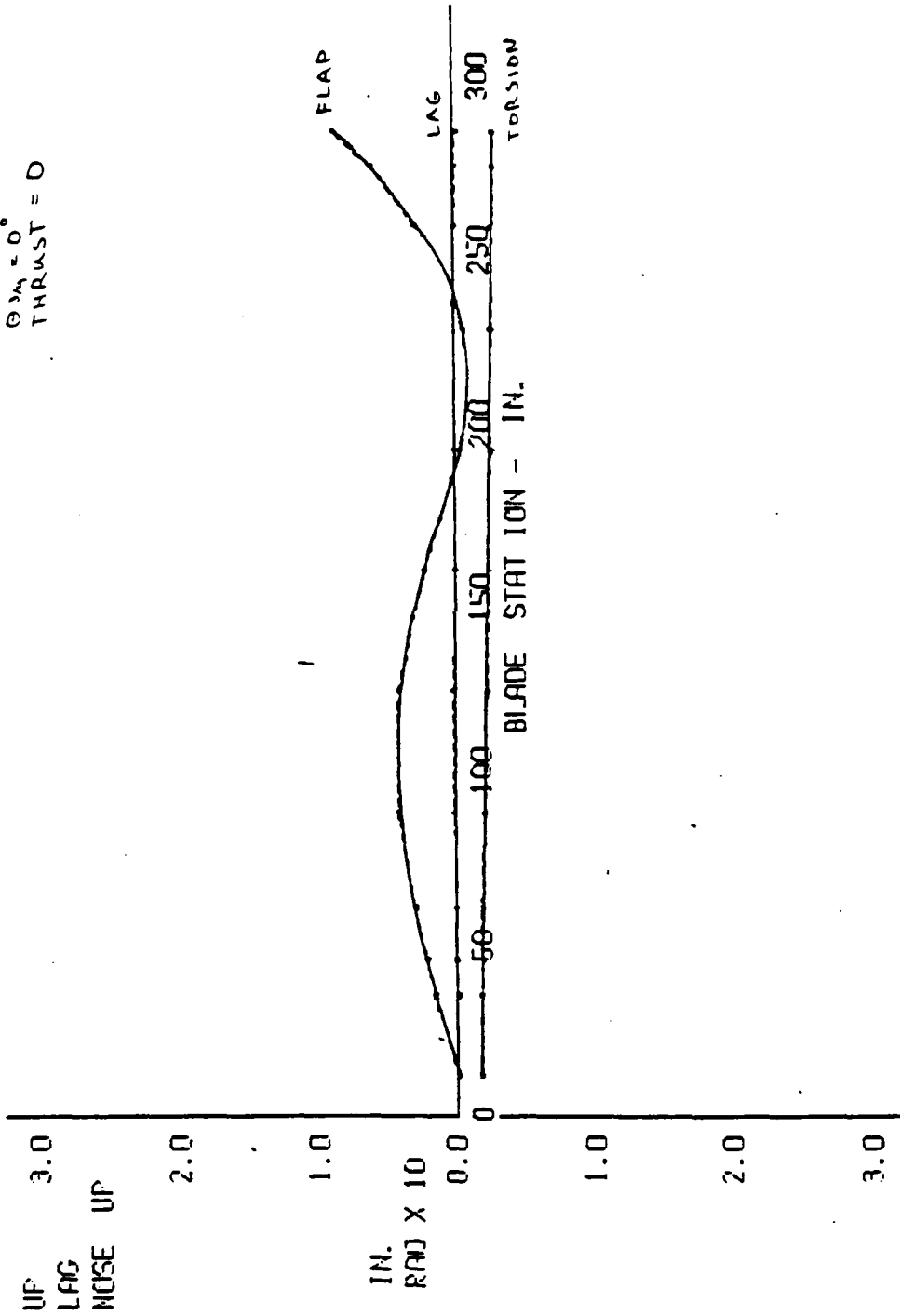


Figure D-1h. CMRB mode shapes.

1<sup>st</sup> CIRCUMWISE BENDING MODE

REAL

$\omega = 6.568$  cyc/rev

$\phi_{\text{tip}} = 0^\circ$

THRUST = D

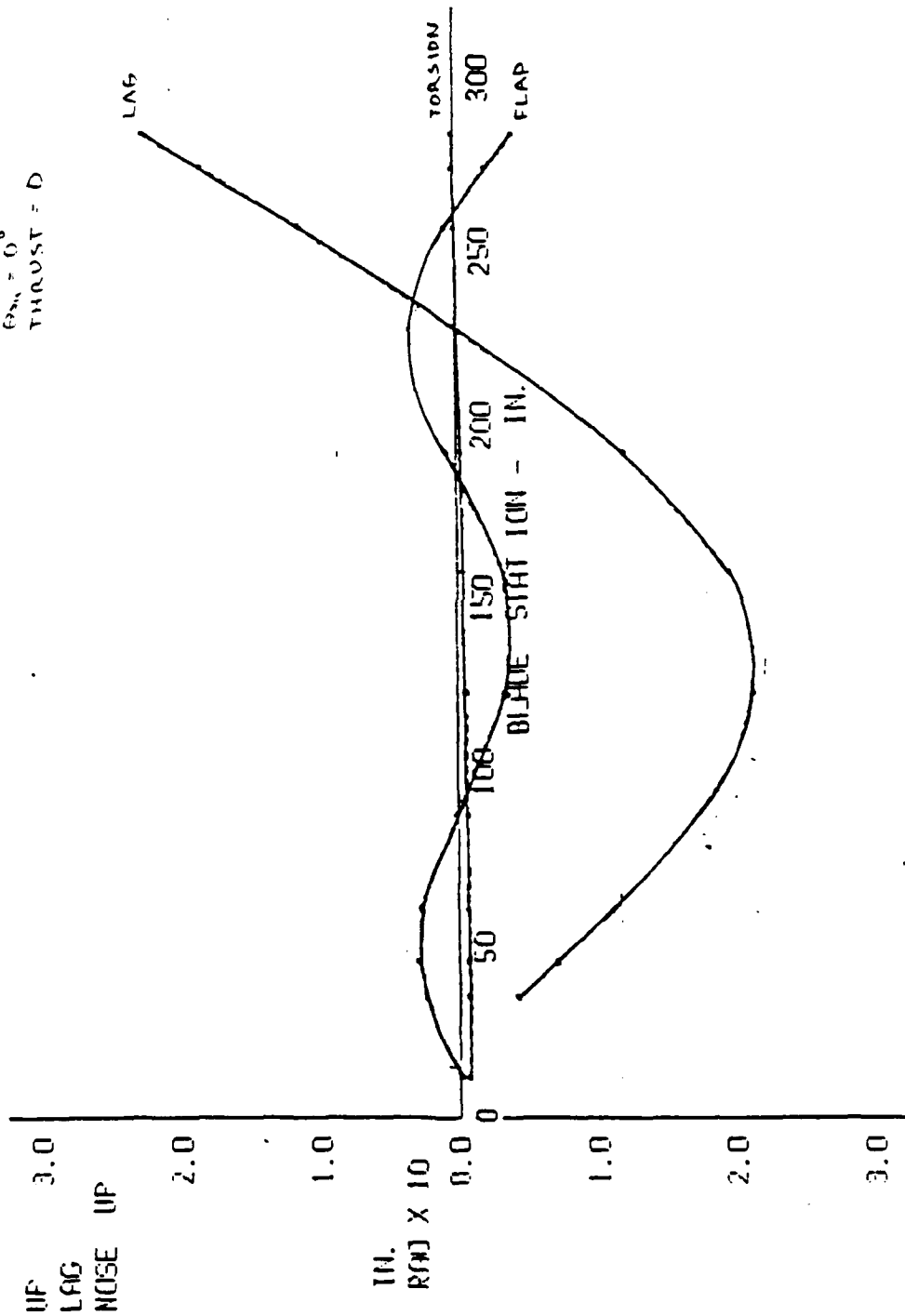


Figure D-1i. CMRB mode shapes.

1<sup>st</sup> CIRCUMVERSE BENDING MODE  
 IMAGINARY  
 $\omega = 6.568 \text{ CY/REV}$   
 $\beta_{1/2} = 0^\circ$   
 THRUST = 0

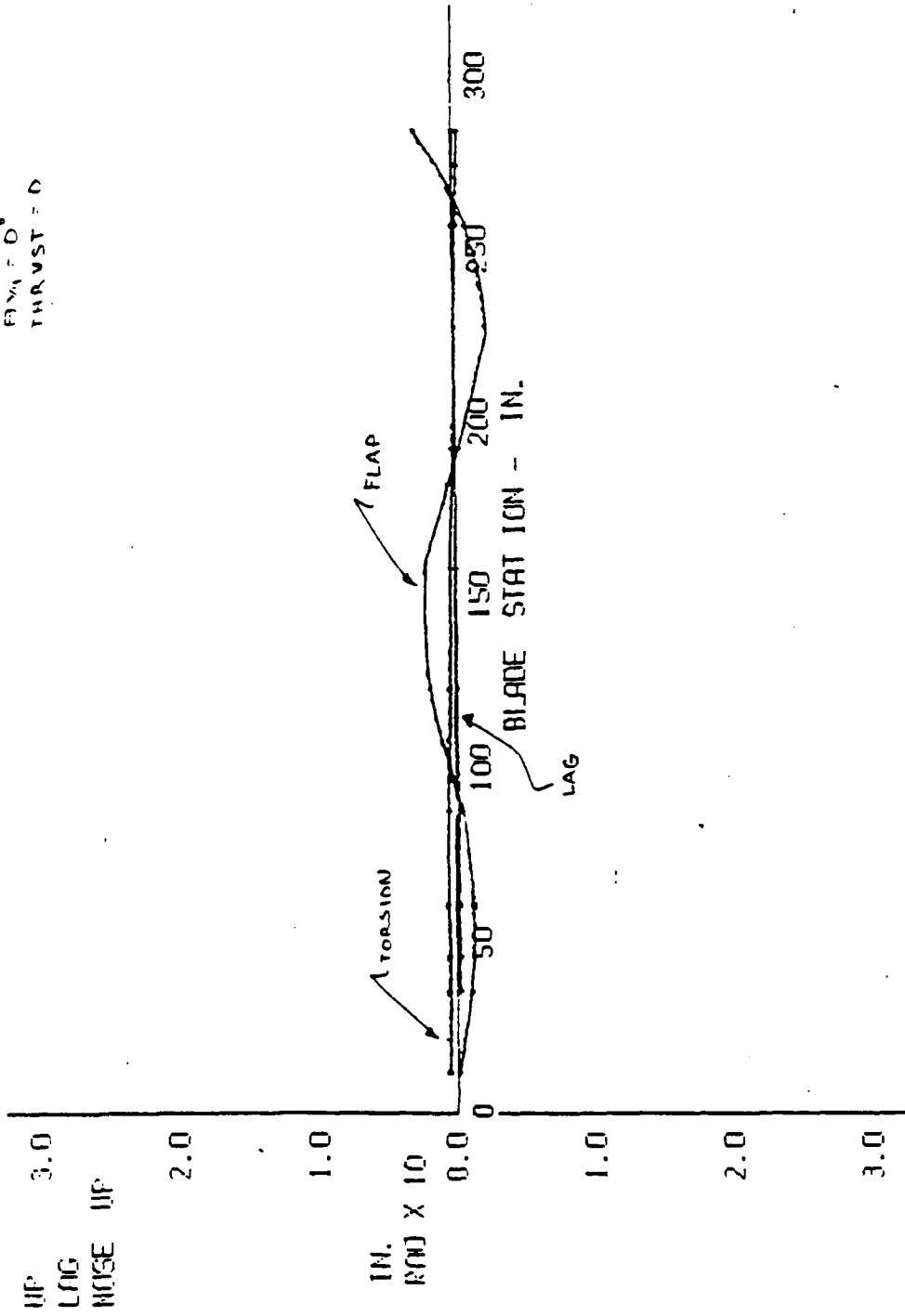


Figure D-1j. CMRB mode shapes.

3<sup>rd</sup> FLAPWISE BENDING MODE

REAL

$\omega = 7.112$

$\beta_{\text{tip}} = 0^\circ$

THRUST = 0

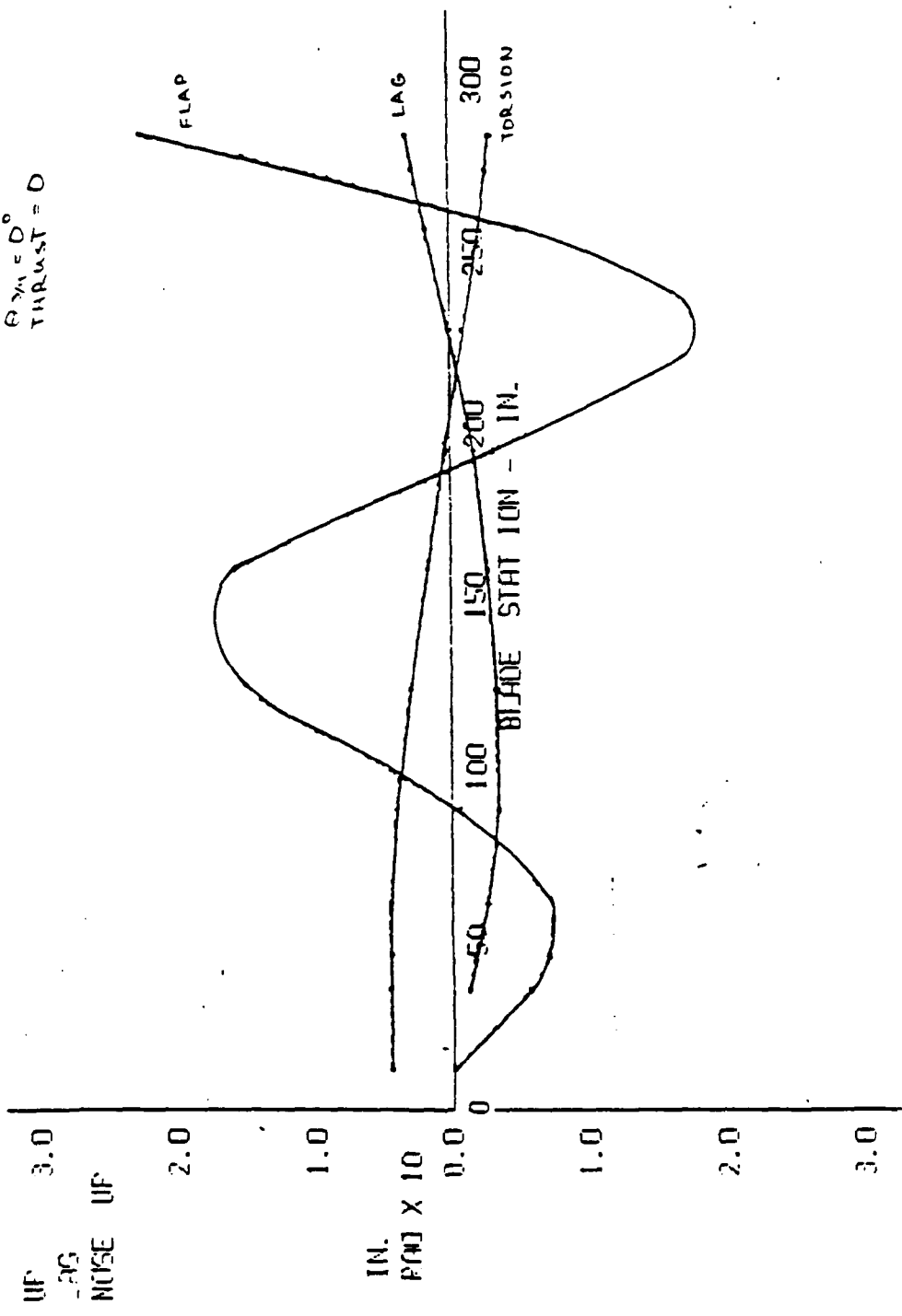


Figure D-1k. CMRB mode shapes.

3<sup>rd</sup> FLAPWISE BENDING MODE  
 IMAGINARY  
 $\omega = 7.112$   
 $\theta_M = 0^\circ$   
 THRUST = 0

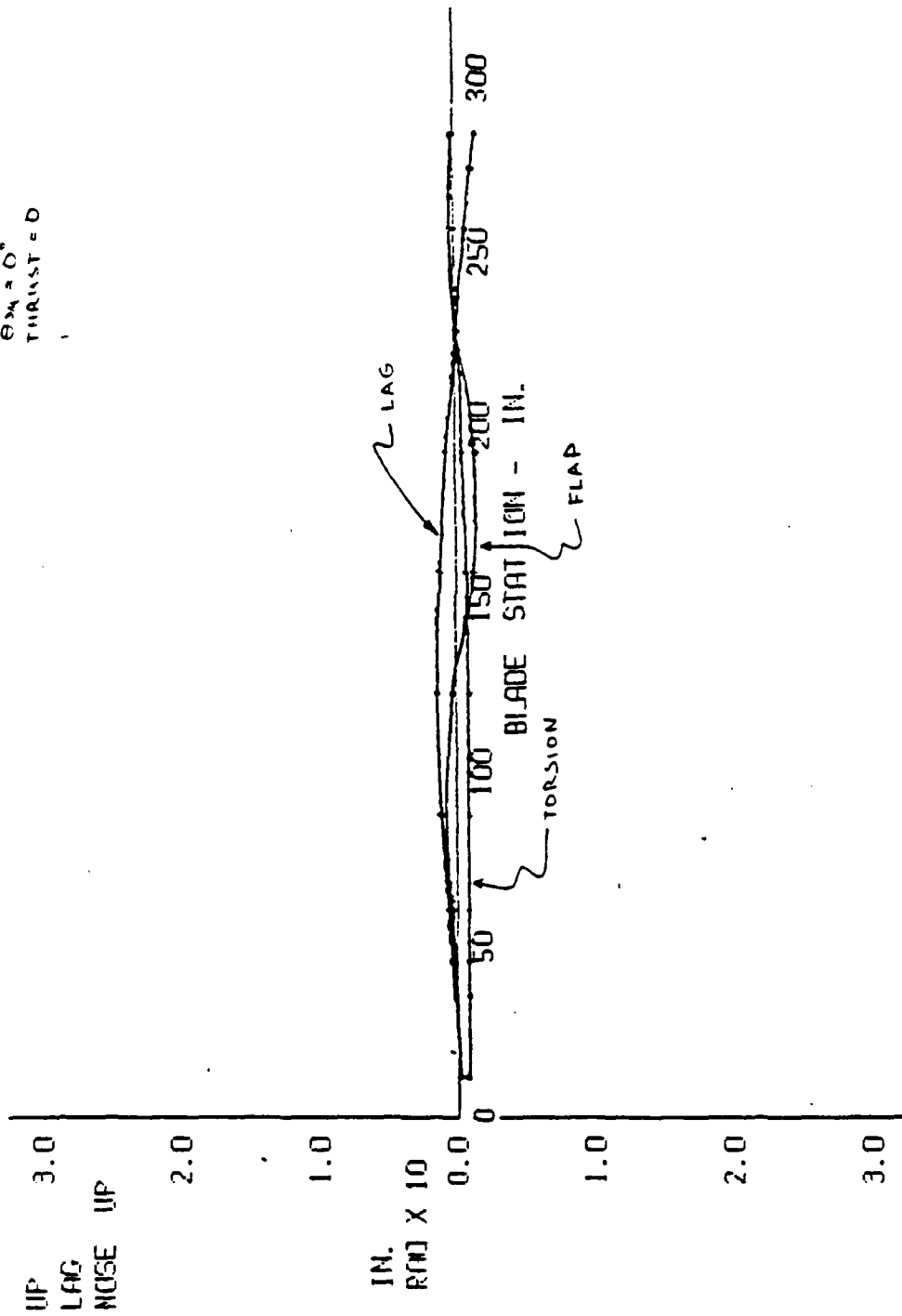


Figure D-11. CMRB mode shapes.

2<sup>nd</sup> TORSION MODE  
 REAL  
 $\omega = 8.443 \text{ rad/rev}$   
 $\theta_{\text{tip}} = 0^\circ$   
 THRUST = 0

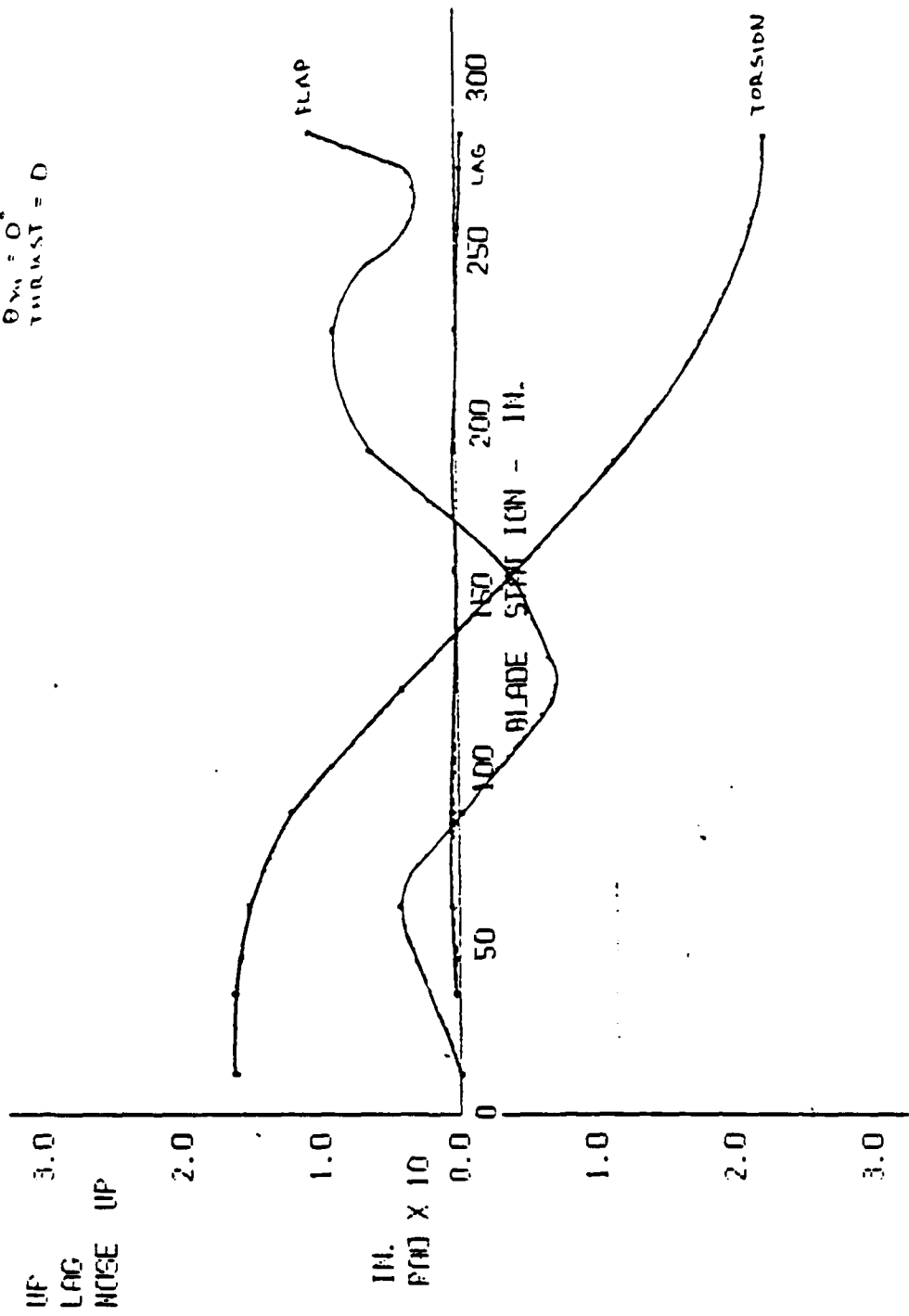


Figure D-1m. CMRB mode shapes.

2<sup>nd</sup> TORSION MODE  
 IMAGINARY  
 $\omega = 8.443 \text{ cps/rev}$   
 $\theta_{max} = 0^\circ$   
 THRUST = 0

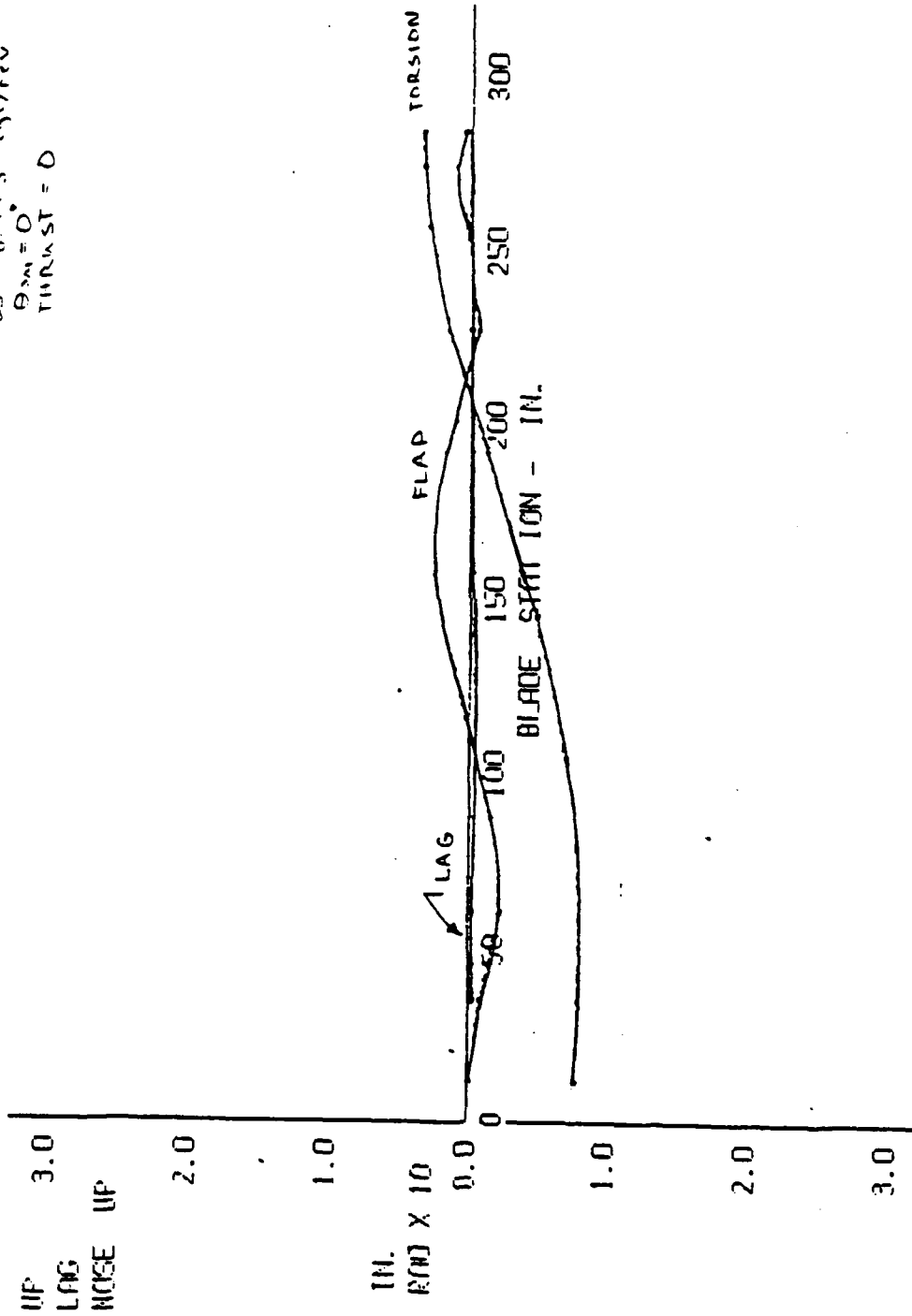


Figure D-1n. CMRB mode shapes.



APPENDIX E

ENGINEERING PROCESS MANUAL FOR FABRICATING THE  
COMPOSITE MAIN ROTOR BLADE  
FOR THE AH-64A HELICOPTER

*All even pages are missing  
and are not available*

*30 aug 89*

## 1. SCOPE

1.1 This process bulletin establishes the materials and processes required to fabricate the Model 77 composite main rotor blade (CMRB) PN 7-311412500. It is currently in preliminary form and will be finalized before production begins.

## 2. APPLICABLE DOCUMENTS

2.1 Government documents. The following documents, of the issue in effect on date of the initiation for bids or request for proposal, form a part of this specification to the extent specified herein. In case of conflict between these documents and this specification, the requirements of this specification shall prevail.

## SPECIFICATIONS

Federal

QQ-W-423	Wire, Steel, Corrosion Resisting
RR-W-360	Wire Fabric, Industrial
TT-I-735	Isopropyl Alcohol
TT-M-261	Methyl Ethyl Ketone, Technical
MMM-A-132	Adhesive, Heat Resistant, Airframe Structural, Metal to Metal

Military

MIL-C-9084	Cloth, Glass, Finished, for Resin Laminates
MIL-T-21014	Tungsten Base, High Density Metal (Sintered or Hot Pressed)
MIL-A-21180	Aluminum Alloy Casting, High Strength
MIL-S-22473	Sealing, Locking and Retaining Compounds, Single-Component
MIL-R-60346	Roving, Glass, Fibrous (for Filament Winding Applications)

*E-2 not avail.*

HMS 16-1164	High Strength Organic Fiber (Kevlar) Reinforcements, Yarn and Fiber
HMS 16-1171	Adhesive for Polyurethane Bonding
HMS 17-1172	Polyurethane, Rain Erosion Resistant Elastomer
HMS 17-1175	Polyurethane Foam, Self-Skinning, Self-Extinguishing, Closed Cell, Rigid
HP 1-17	Heat Treatment of 17-4PH and 15-5PH Precipitation Hardenable Corrosion Resistant Steels
HP 4-35	Anodic Treatment of Aluminum Alloys for Metal-to-Metal Bonding
HP 5-10	Environmental Sealing
HP 6-3	Torquing of Aircraft Bolts, Screws, and Nuts
HP 6-5	Magnetic Particle Inspection
HP 8-5	Identification of Detail Parts and Assemblies
HP 9-20	Etching and Priming of Tungsten Alloys for Adhesive Bonding
HP 9-26	Etch and Prime of Austenitic Corrosion-Resistant Steel for Adhesive Bonding
HP 10-7	Shelf Life
HP 15-42	Fabrication of Reinforced Plastics
HP 15-45	Application of Liquid Locking Compound for Sealing and Retaining Metal Fasteners, Bearings, and Bushings
HP 15-67	Fabrication of Composite Parts by Filament Winding Method
HP 16-21	Structural Metal-to-Metal Bonding

*E-4 not avail.*

7-311412615	Forward channel mold
7-311412616	Aft channel mold
7-311412617	Trailing edge longo mold
7-311412618	Root end wedge mold
7-311412619	Form block
7-311412620	Root end dam mold
7-311412625	Template (erosion strip buildup)
7-311412629	Index plate, end plate
7-311412630	Tool assembly layout
7-311412632	Template guide setup
7-311412633	End dome detail winding mandrel
7-311412636	Spar broom winding fixture
7-311412638	Spacer - tip core and mold
7-311412639	Skin layup layout
7-311412640	Bushing location fixture
7-311412641	Blade cooling fixture
7-311412642	Root end dam locator
7-311412643	Filler - dummy tube and trailing edge longo
7-311412644	Tip weight locator
7-311412645	Spar wedge template
7-311412646	Template spar cap tip
7-311412647	Staging table

*E-6 not avail*

**Microballoons**

Polyurethane erosion strip bonding adhesive and primer (HMS 16-1171)

Polyurethane erosion strip bonding adhesive and primer (HMS 17-1172)

Resin and hardeners (HMS 16-1115)

S-glass roving (MIL-R-60346, Type IV, Class 1)

Tungsten (MIL-T-21014)

Urethane foam (HMS 17-1175)

Wire rods, 316 CRES (QQ-W-423)

**3.2.2 Shop aids.**

**Double-back tape**

Isopropyl alcohol (TT-I-735)

**Metal spacer**

Methyl ethyl ketone (MEK) (TT-M-261)

Mold release (Ram 225, or equivalent)

Peel ply (Air Tech, Tool Tech, or equivalent)

Polyethylene, film, 2-mil, embossed

Polyvinyl alcohol

Scrim cloth

Sealant tape

Styrofoam, sheet, 1/2-inch (12.7 mm)

Tedlar film, 1-mil

Teflon plugs

Wax (Trewax, or equivalent)

Wrightlon tube (Vac Pac, 3-mil) (7400 LF, 0.003)

*E-8 not avail.*

3.3.2 Fabrication of reinforced plastic subassemblies. Reinforced plastic subassemblies shall be fabricated in accordance with HP 15-42 and HP 15-67. Colored cotton thread may be used within the fiberglass laminates to indicate the fiber orientation.

3.3.2.1 Fiberglass subassemblies shall be fabricated with a nylon peel ply which shall be removed just prior to the bonding operation. All peel plies shall be marked "Remove Peel Ply" with letters no smaller than 1/4 inch (6.35 mm) in accordance with HP 8-5.

3.3.2.2 Fiberglass may be spliced in the filler area and 60-degree wraps of spar tubes only. Splices shall be overlapped at least 1 inch (25.4 mm).

3.3.2.3 Fiber volume requirements and dry:wet fiber weight ratios are specified below.

3.3.2.3.1 A 50-percent fiber volume and a  $0.56 \pm 0.03$  dry:wet fiber weight ratio are required for Kevlar 49 fabric and rovings.

3.3.2.3.2 A 55-percent fiber volume and a  $0.60 \pm 0.03$  dry:wet fiber weight ratio are required for graphite fabric and rovings.

3.3.2.3.3 Fiber volume and dry:wet fiber weight ratios shall be performed as required by this EPB in accordance with the techniques specified in HP 15-67.

3.3.2.4 Storage of any filament wound or other uncured component awaiting incorporation into a blade shall be done at low temperatures, in accordance with the guidelines set forth in HP 15-67.

3.3.2.5 HMS 16-1164 (Kevlar) yarns and fabrics shall be dried out prior to impregnation in accordance with HP 15-67.

3.3.3 Fabrication records. The following information is required to be recorded in the individual planning for each blade fabricated (including individual components).

3.3.3.1 Fabrication, start and completion time.

3.3.3.2 Lot, batch, or any other applicable identification numbers for all materials used.

3.3.3.3 Resin mixing, dates and times.

*E-10 not avail.*

3.3.4.4 Leading edge balance weight rods. The 316 CRES stainless steel balance rods shall be processed as follows.

3.3.4.4.1 The required number and lengths are as specified in 3.3.6.1.1.

3.3.4.4.2 Etch and prime the cut rods in accordance with HP 9-26.

3.3.4.4.3 Identify in accordance with HP 8-5 and seal in a polyethylene bag until ready for use.

3.3.4.5 Tungsten leading edge balance weight. The tungsten balance weight shall be prepared as follows.

3.3.4.5.1 Etch and prime in accordance with HP 9-20.

3.3.4.5.2 Identify in accordance with HP 8-5 and seal in a polyethylene bag until ready for use.

3.3.4.6 Backing strips. The 301 CRES stainless steel backing strips shall be processed as follows.

3.3.4.6.1 Etch and prime in accordance with HP 9-26.

3.3.4.6.2 Identify in accordance with HP 8-5 and seal in a polyethylene bag until ready for further use.

3.3.4.7 Aluminum wire mesh (7-311412547). The 5056 aluminum lightning screen (RR-W-360, Type I, Class 2) shall be processed as follows.

3.3.4.7.1 Clean using MEK (TT-M-261) spray, repeated as required to remove any visible contamination.

3.3.4.7.2 Identify in accordance with HP 8-5 and seal in a polyethylene bag until ready for further use.

3.3.5 Curing. The minimal acceptable cure cycle is dependent on the adhesive and resin system used. The most frequently used acceptable cure cycles are as follows. When any deviation from these is used it must be with the consent of the HHI Materials Processes and Standards Department, as indicated by the signature of the cognizant MP&S engineer on the applicable shop planning.

*E-12 not avail.*

3.3.6.2 Voids greater than 0.125 inch (3.175 mm) in depth shall be repaired as follows:

#### WARNING

Fire hazard; solvent is dangerous when exposed to heat or flame; use only with plenty of ventilation away from smoke and flames. Flashpoint 22°F (-5.5°C).

3.3.6.2.1 Solvent wipe area with TT-M-261 MEK.

3.3.6.2.2 Scuff sand the area with 180 - 320 grit paper to remove any gloss from the resin surface. Solvent clean as in 3.6.3.2.1.

3.3.6.2.3 Mix and apply HMS 16-1068, Class 3 adhesive in accordance with HP 16-25, filling voids flush with the surrounding surfaces.

#### 3.3.7 Secondary bonding operations.

3.3.7.1 Film adhesive bonding operations shall use HMS 16-1111, Class 3 adhesive in accordance with HP 16-30.

3.3.7.2 Paste adhesive bonding operation shall use HMS 16-1068, Class 3, adhesive in accordance with HP 16-25.

3.3.7.3 Electrical connections shall be sealed using HMS 16-1147, Class 2 adhesive in accordance with HP 5-10.

3.3.7.4 The 7-3114152516-11 erosion strip shall be bonded in accordance with EPB 16-139.

3.3.8 Finish (paint). Finish in accordance with EPB 4-230.

3.3.9 Weight and balance. Weight and balance procedures shall be in accordance with EPB 30-164. Install weight retention fitting doors and secure fasteners using MIL-S-22473, Grade C in accordance with HP 15-45. Torque fasteners to 25-35 inch-pounds (2.8-4.0 N·m) in accordance with HP 6-3.

#### 4. QUALITY ASSURANCE

4.1 Provisions of the NDE plan apply.

*E-14 not avail*



6. NOTES

6.1 Intended use. This process is intended for use in the fabrication of the composite main rotor blades for the Model 77 helicopter.

7. APPROVED VENDORS

Not applicable

*E-16 not avail*

APPENDIX F

NONDESTRUCTIVE EVALUATION PLAN  
OF THE  
COMPOSITE MAIN ROTOR BLADE  
FOR THE AH-64A HELICOPTER



## NONDESTRUCTIVE EVALUATION PLAN

This nondestructive evaluation (NDE) and nondamaging testing (NDT) plan is proposed for the production CMRB to assure structural quality by:

- Detecting critical flaws
- Measuring structural integrity
- Evaluating consistency of fabrication

It will be reevaluated after the first block of production blades is completed, and modified if necessary. This proposed plan anticipates the potential for the occasional occurrence of flaws, defects, and fabrication errors that can degrade the structural quality, it establishes the optimal NDT equipment and procedures for evaluating these possible defects, and it quantifies the tolerance limits that are acceptable for defects and manufacturing inaccuracies.

Table F-1 lists defects, flaws, and fabrication errors that were experienced in the CMRB MM and T prototypes manufactured to date. The list is an anticipatory forecast for the production blade, and will be updated upon completion of the blade preproduction program. At that time, a better categorization can be made with respect to defect types, likelihood of occurrence, size, location, probability of growth rates, and better analysis of the structural criticality of the various defects. The tentative consequences of the flaws described in the rightmost column of Table F-1 will be upgraded after a more substantive data base is accumulated. A part of the work yet to be done will be the establishment of a set of structural criteria that provide "test/don't test" guidelines; i. e. ,

- "Search, inspect, test, and NDE flaws, defects and error that each individually degrade the strength, modulus, fatigue resistance of the MRB by more than 5 percent of its initial or unflawed value."

Table F-2 lists potential techniques and associated instrumentation for evaluating the CMRB. Table F-3 indicates the present evaluation of the success of these techniques.

TABLE F-1. POTENTIAL PRODUCTION FLAWS THAT MAY OCCUR IN THE CMRB

Type of Defect	Consequences When Defect Exceeds Tolerance Levels
Interlaminar delamination	Delamination grows with cycling, causing local buckling.
Disbonded, debonded honeycomb/interface	Flutter and loss of blade stiffness and rigidity.
Porosity	Degradation of shear strength of epoxy matrix
Void	Local weakening of strength and modulus.
Resin rich, filament-poor area	Tensile strength and modulus decrease with decreasing fiber volume ratio.
Resin starved area	Compressive strength and shear strength decrease with increasing unwetted filament-to-resin ratio.
Spartube rib buckle	Loss of bending stiffness and torsional rigidity.
Thick bond lines	Shear rigidity of bondline is inversely proportional to its thickness.
Tip or leading edge mislocation	Blade won't track, or cannot be balanced easily.
Root end bushing misfit, splits, voids, cracks, separations	Potential for premature root end blade fracture in fatigue.
Foreign objects, inclusions	Some degradation of blade durability from inclusions.

TABLE F-1. POTENTIAL PRODUCTION FLAWS THAT  
MAY OCCUR IN THE CMRB (CONT)

Type of Defect	Consequences When Defect Exceeds Tolerance Levels
Filled honeycomb cells	Excessive material in the cells bleed from surrounding skin to point of resin starvation.
Misoriented plies, waviness	Localized weakening of stiffness and strength, lowered fatigue resistance.
Reworked area	Reintroduction of stress concentrators and fatigue nucleation.
Overlap, underlap, gap	Local loss of stiffness, rigidity, and fatigue resistance.
Internal dent, damage	Local loss of strength and fatigue resistance.
Inhomogeneous cure	Degradation of strength and stiffness over wide area.
Mislocation of root-end bushing	Reduction of bushing wall and/or flange thickness during final machining, with accompanying reduction in strength.

TABLE F-2. INSPECTION NDE METHODS AH-64A CMRB

Technique	Instrument/ Equipment	Inspection/Test Frequency <sup>(a)</sup>
<ul style="list-style-type: none"> <li>● Visual detection                             <ul style="list-style-type: none"> <li>- Normal illumination</li> <li>- High intensity light</li> </ul> </li> </ul>	Inspector S150 Xenon Lamp	Every blade Every blade
<ul style="list-style-type: none"> <li>● Audible detection                             <ul style="list-style-type: none"> <li>- Manual Tapping</li> <li>- Sonic Brush</li> </ul> </li> </ul>	Inspector NASA Sonic Brush	Every blade Every blade
<ul style="list-style-type: none"> <li>● Ultrasonic scanning                             <ul style="list-style-type: none"> <li>- Pulse/echo attenuation</li> <li>- Pulse/echo impedance</li> <li>- Ultrasonic pulse, acoustic echo</li> </ul> </li> </ul>	Mark II Harmonic Bond Tester: EPB-15-138. Bondascope 2100  206 AU	Every blade in lot 1  Every second blade in lot 1 Every third blade in lot 1
<ul style="list-style-type: none"> <li>● X-ray radiography                             <ul style="list-style-type: none"> <li>- Microfocused, video-taped</li> <li>- Conventional, negative film to scale</li> </ul> </li> </ul>	Magnaflux NDT 9/6  Cedtech	Every blade in lot 1 Questionable blades from microfocus X-ray.
<ul style="list-style-type: none"> <li>● Impulse/modal response signature</li> </ul>	PCB K291 A05 tapper	Every blade
<ul style="list-style-type: none"> <li>● Structural quality measurement, rigidity, frequencies and hysteresis</li> </ul>	See Figure F-1	Every second blade or TBD

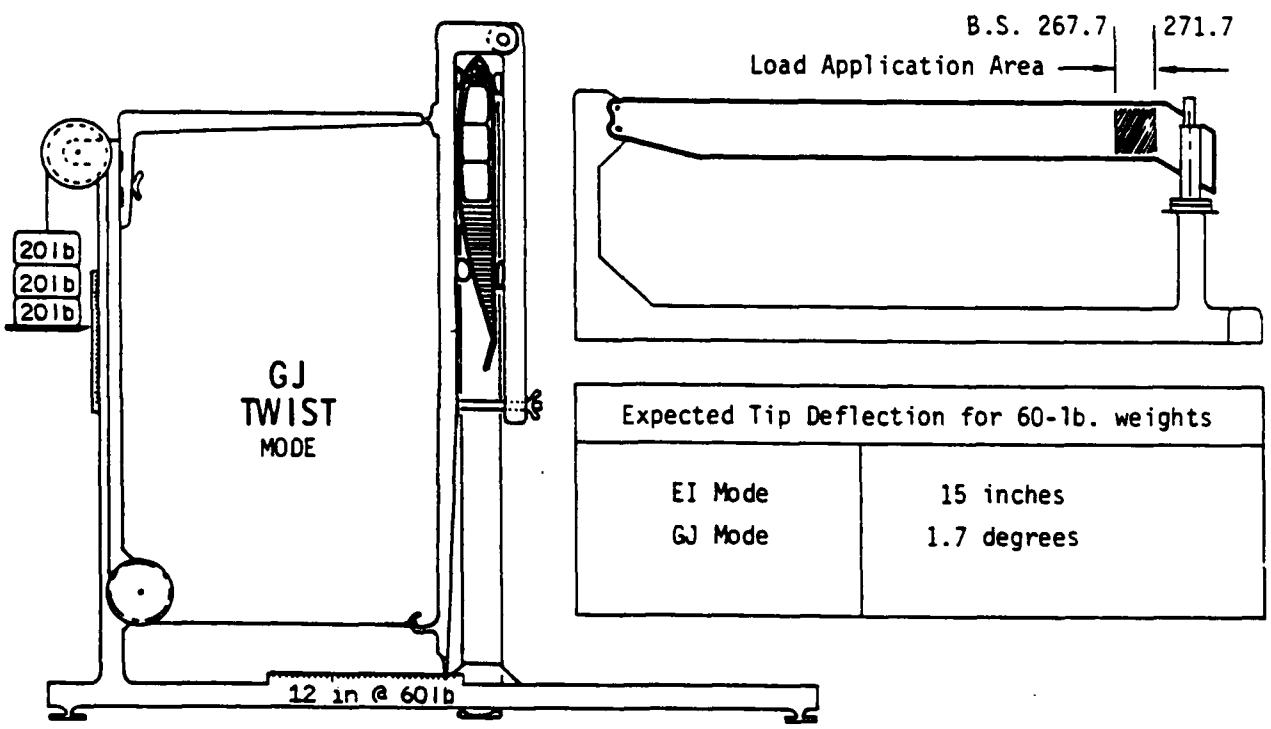
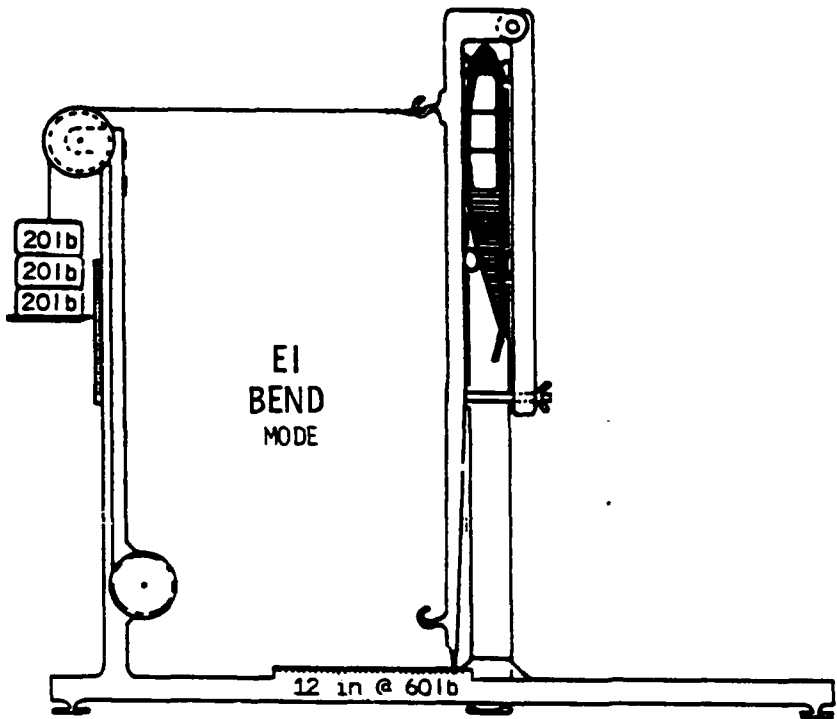
(a) NDT techniques and the frequency of inspection will be recommended after the 20th blade is produced.

TABLE F-3. NDT/DEFECT MATRIX

	Delaminations	Disbond	Porosities	Voids	Resin-rich	Resin-poor	Rib geometry	Thick bond	Weight mislocation	Bushing loose	Foreign objects	Filled cells	Ply misorientation	Rework	Overlaps, gaps	Dents, damage	Miscure	Bushing mislocation
Visual																		
Normal	•	•			•	•		●					•	•				●
High intensity	•	•	•	•			•	•	●	•	•		•	•	•			
Audible																		
Tapping	•	•		•				•			•							
Sonic brush	•	•		•				•			•							
Ultrasonic																		
Attenuation	●	●	•	•	•	•		•								•	•	
Impedance	●	●	•	•	•	•		•	•	•	•	•				•	•	
Acoustic echo	•	•	●	●	•	•		•			•	●		•	•	•	•	
X-ray																		
Microfocus	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	
Conventional	●	●		•	•	•	•	•	•	•	•	•	•	•	•			
Pulse response	•	•	•		•	•	•	•	•	•		•						●
Structural quality	•	•	•		•	•		•	•	•		•		•		•		

Dot size indicates likelihood of detection





FIXTURE FOR MEASURING ROTOR BLADE STIFFNESS

Figure F-1. Fixture for measuring rotor blade stiffness.

A tentative level of acceptable quality is defined by the following flaws, defects, or irregularities. Those that fall within these tolerances will be considered acceptable (minor) manufacturing errors. Figures F-2 through F-15 illustrate these flaws and their tolerances. Those that exceed these tolerances will be submitted to the Material Review Board and treated as unacceptable until disposed of by the Board.

- Skins shall be wrinkle-free over 80 percent of the surface area. No single wrinkle shall exceed 4.0 square inches in extent. Wrinkle pits perpendicular to the surface shall not exceed 0.06 inch in depth. Overriding folds in the plane of the skin shall not exceed 0.15 inch. No two wrinkles shall be closer than 10.0 inches nor shall there be more than five distinctly separate wrinkles in a blade.
- Longos shall be free of waviness over 99 percent of their volume in the lug area and 80 percent over the remainder of the blade. No single wave shall have an aspect ratio smaller than 20.
- Spartube sidewalls shall not deviate from vertical straightness by more than 0.05 inch, and from spanwise straightness by more than 0.50 inch.
- Interlaminar Resin overthickness shall be less than 0.010 inch in the bushing area and less than 0.030 in the longo straight sections.
- Bushings shall adhere to longos and fillers. No single disbond shall exceed 0.06 square inch in area. No more than 3 disbonds 0.06 square inch in size, shall occur per bushing.
- Filler cracks shall not extend more than 1 inch in the spanwise direction, nor more than 0.1 inch in chordwise direction.
- Outer Skins shall adhere to spar caps, and inner skins shall adhere to longos over 95 percent of their interfaces. No single delamination or disbond shall exceed 1.0 inch on an axis, nor shall disbonds be within less than 4.0 inches of each other.
- Fiber/matrix ratios shall rely on in-process control.
- Filament alignment shall be within  $\pm 3$  degrees of the correct orientation for all fibers.

- Honeycomb core shall adhere to the skins over a minimum of 90 percent of cell edges. No cell edge disbond will extend beyond 10 cells, nor shall disbanded cell sets be closer than 4 inches.
- Leading edge weights shall be bonded over at least 90 percent of their surfaces, and shall be positioned within  $\pm 0.05$  inch of their intended chordwise position and within  $\pm 0.2$  inch of their intended spanwise position.
- Tip weights shall be bonded over at least 90 percent of their surfaces.
- Torsional rigidity shall be within  $\pm 6$  percent of the moving cumulative average of tested blades.
- The root end bushing shall be located within drawing tolerance.

All production CMRB inspection and NDE Planning Packages shall be jointly reviewed and approved by Quality Engineering, Materials, Processes, and Specifications (MP&S) and cognizant Design/Technical Engineering and shall be in conformance with the instructions in Quality Assurance Production Plan for the CMRB.

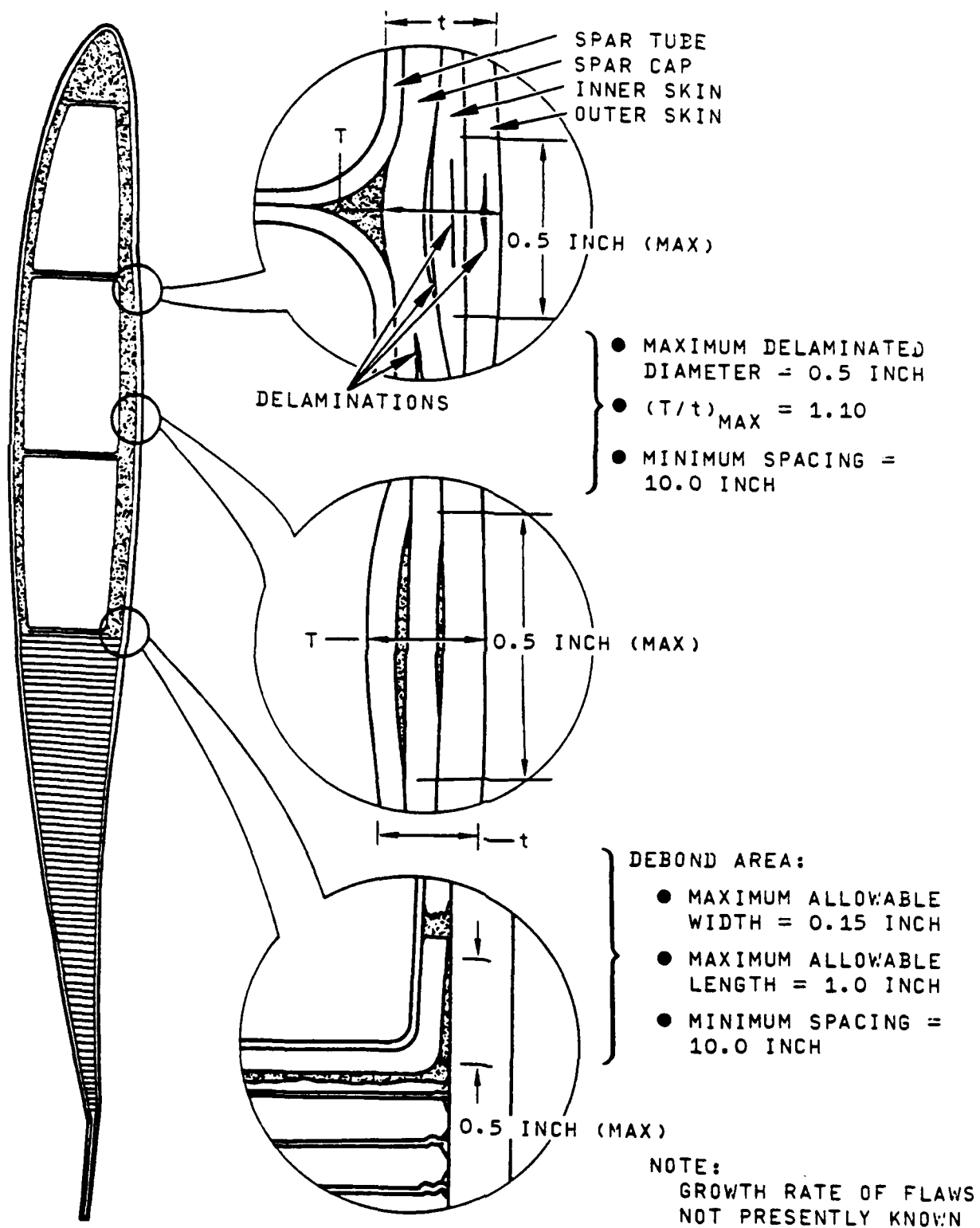
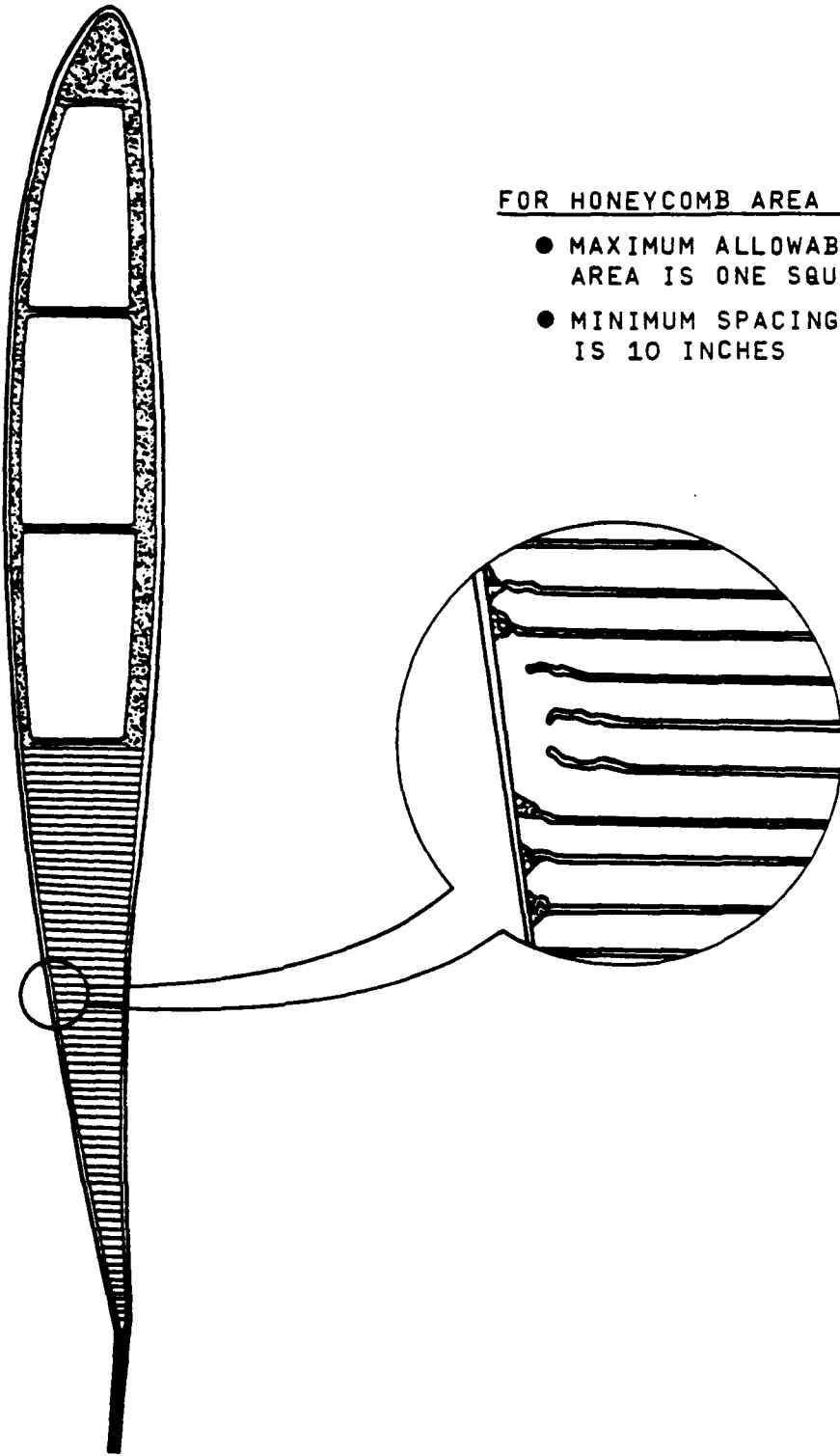


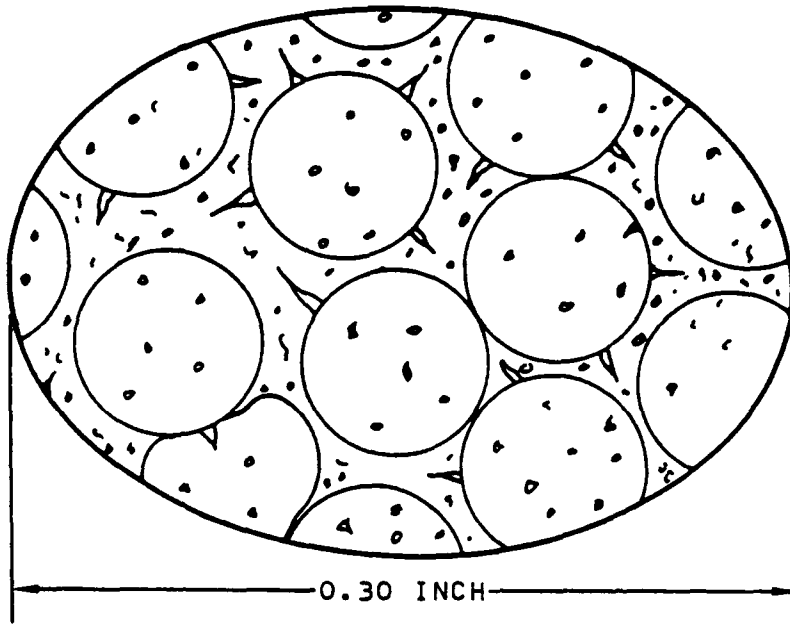
Figure F-2. Potential delamination.



FOR HONEYCOMB AREA ONLY

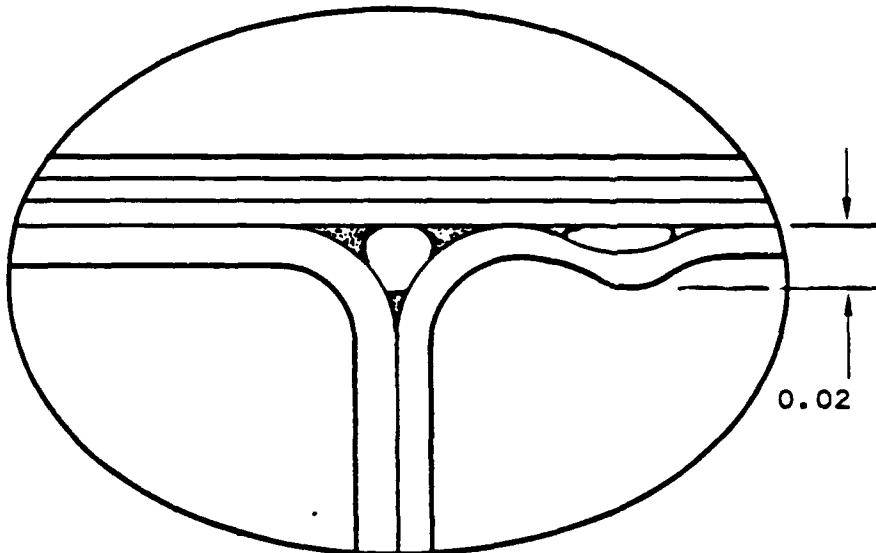
- MAXIMUM ALLOWABLE UNBONDED AREA IS ONE SQUARE INCH
- MINIMUM SPACING FOR FLAWS IS 10 INCHES

Figure F-3. Disbonded honeycomb.



- MAXIMUM ALLOWABLE POROSITY DIAMETER IS 0.30 INCH
- MINIMUM SPACING FOR FLAWS IS 5 INCHES

Figure F-4. Porosities.



- MAXIMUM VOID LENGTH IS 0.5 INCH
- MINIMUM SPACING FOR FLAWS IS 5 INCHES

0.02 INCH (MAXIMUM)

Figure F-5. Voids

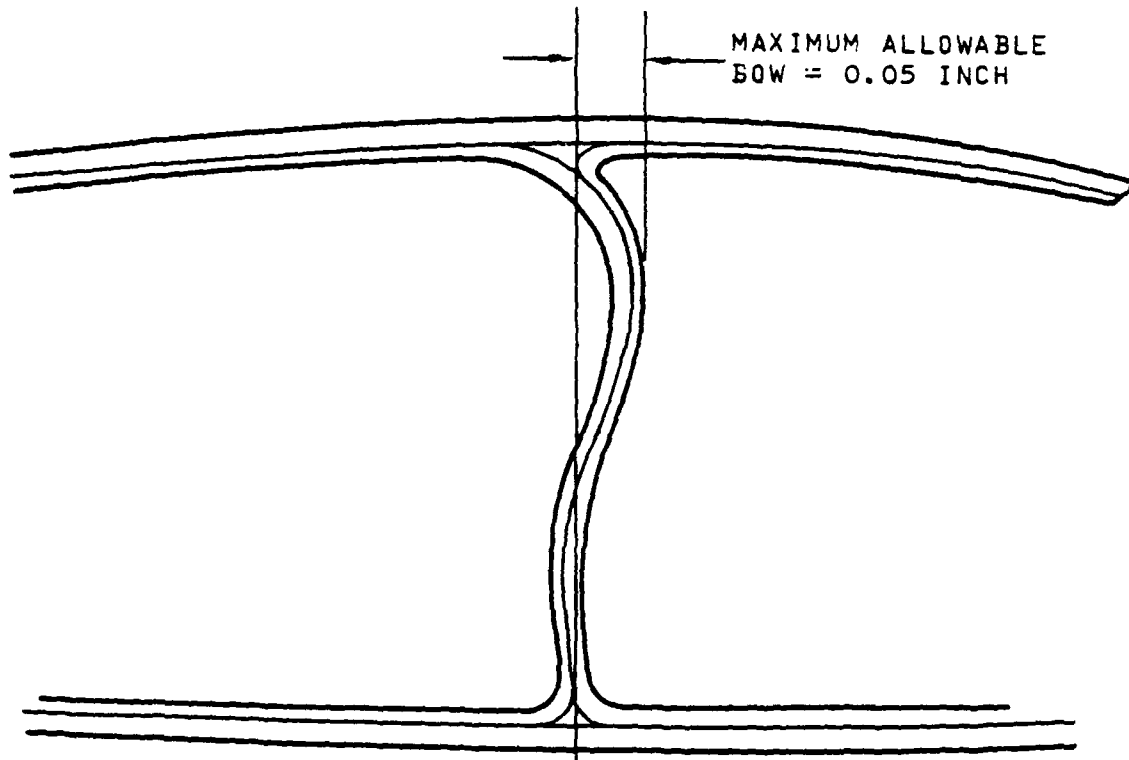


Figure F-6. Spartube rib defect.

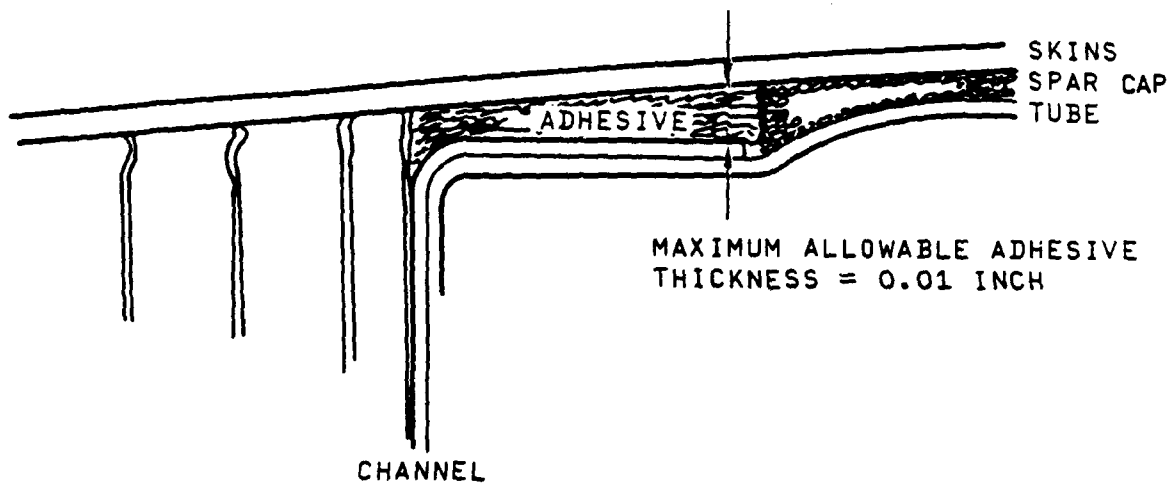


Figure F-7. Thick bondline, irregular adhesive thickness.

LEADING EDGE WEIGHT DISPLACEMENT  
NOT TO EXCEED 0.05 INCH

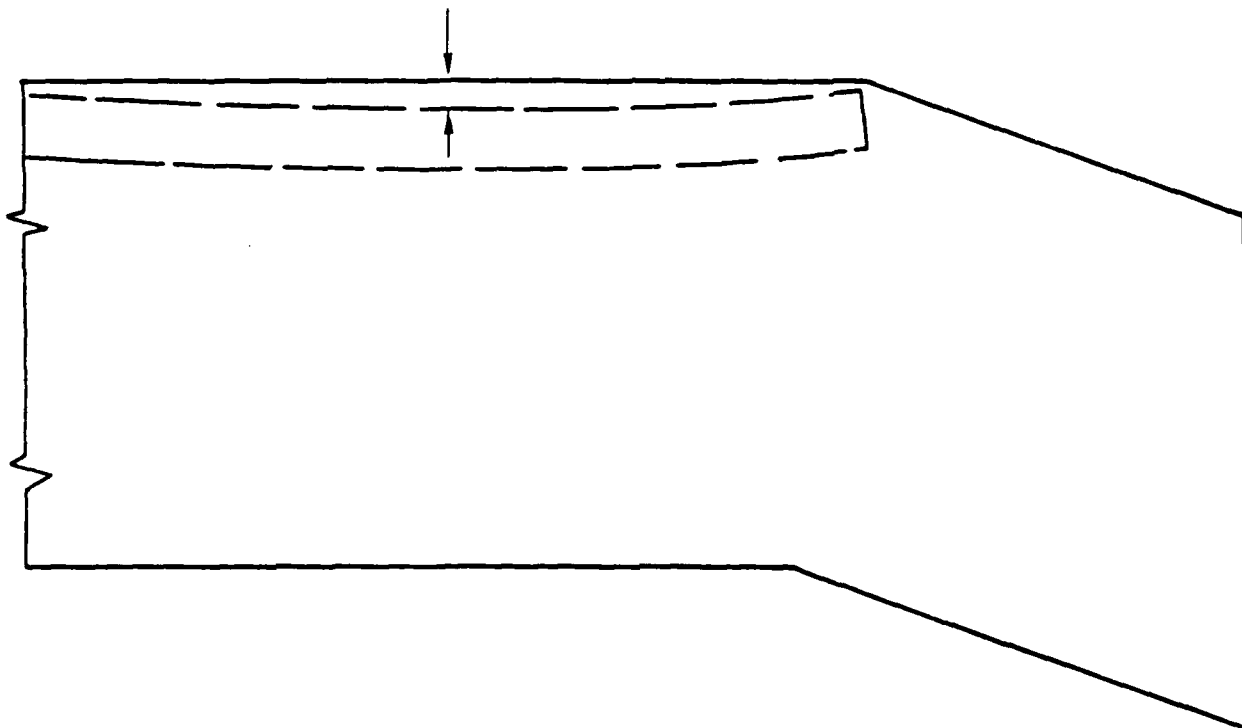
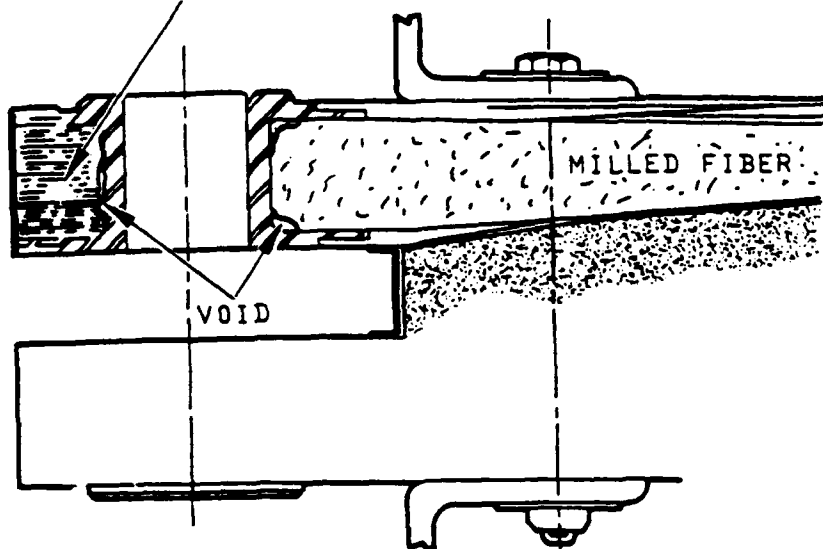


Figure F-8. Leading edge weight location tolerance.

VOID OR INCLUSION



- SUBMIT TO MRB AND STRESS ENGINEERING FOR REVIEW OF ANY FLAWS IN LUG AREA
- CHECK FOR RESIN-CRACKS

Figure F-9. Root end lug area.



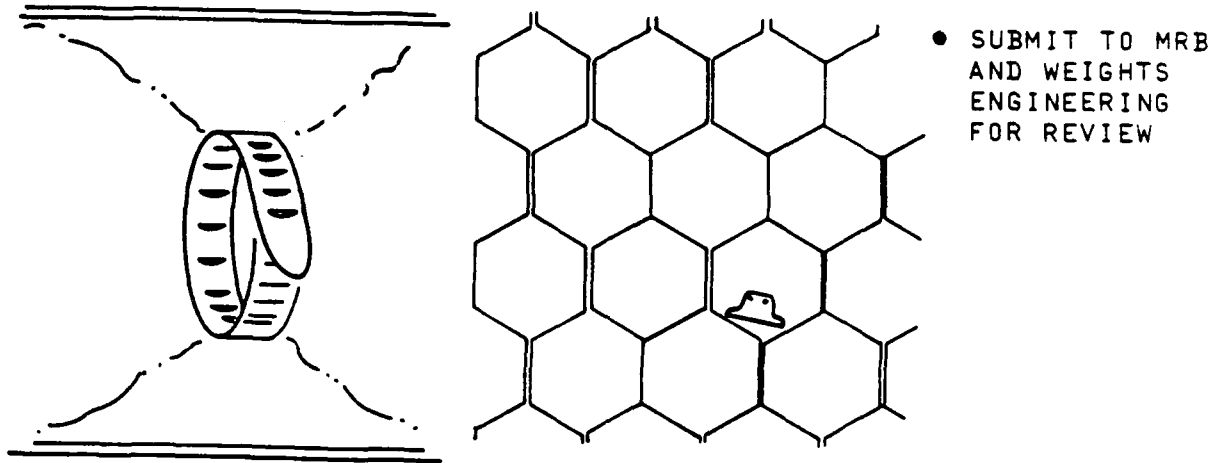


Figure F-10. Foreign objects x-rayed in blade.

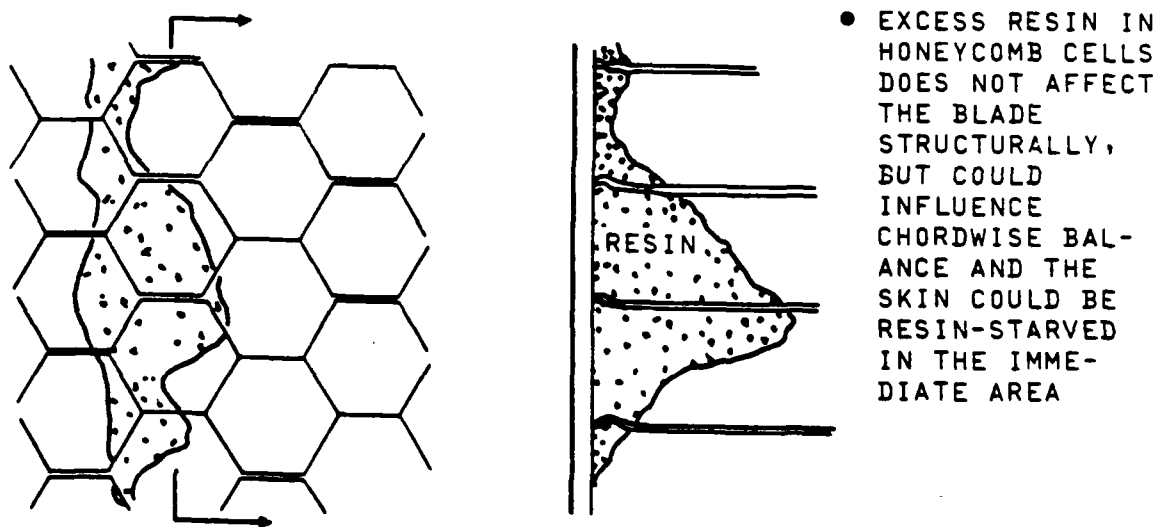
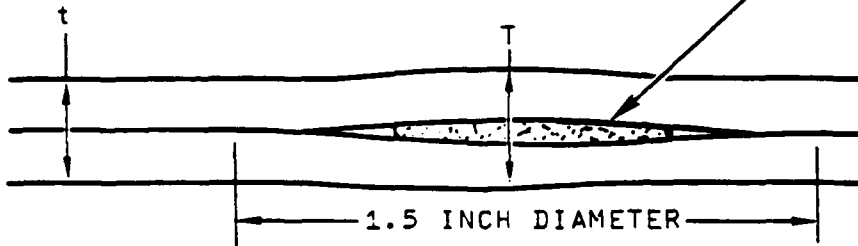
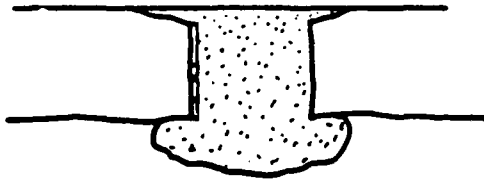


Figure F-11. Honeycomb core cells partially filled with resin.

HYPODERMICALLY REFILLED DELAMINATION

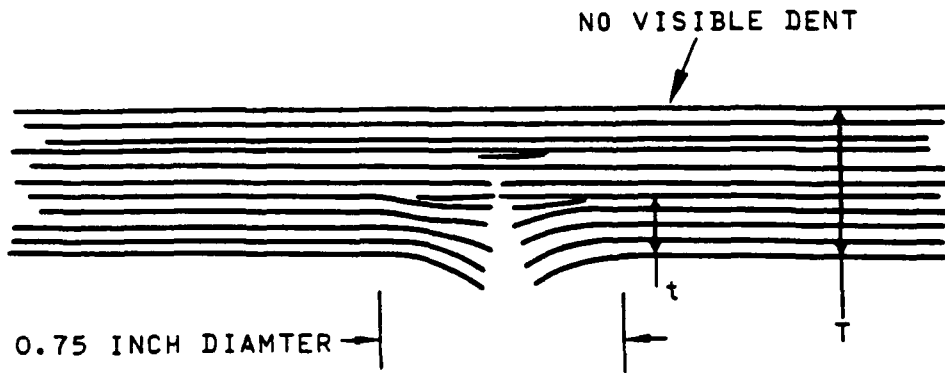


- $\frac{T}{t} \leq 1.10$
- FILL WITH RESIN
- MINIMUM FLAW SPACING IS 10 INCHES



- MIS-DRILLED HOLE UP TO 0.125 INCH DIAMETER BETWEEN B.S. 47 AND 268 MAY BE FILLED WITH RESIN

Figure 12. Reworked areas.



- $\left(\frac{t}{T}\right) \leq 0.1$
- MAXIMUM ALLOWABLE DIAMETER IS 0.75 INCH
- MINIMUM FLAW SPACING IS 5 INCHES

Figure F-13. Dent from tool drop or hammering.

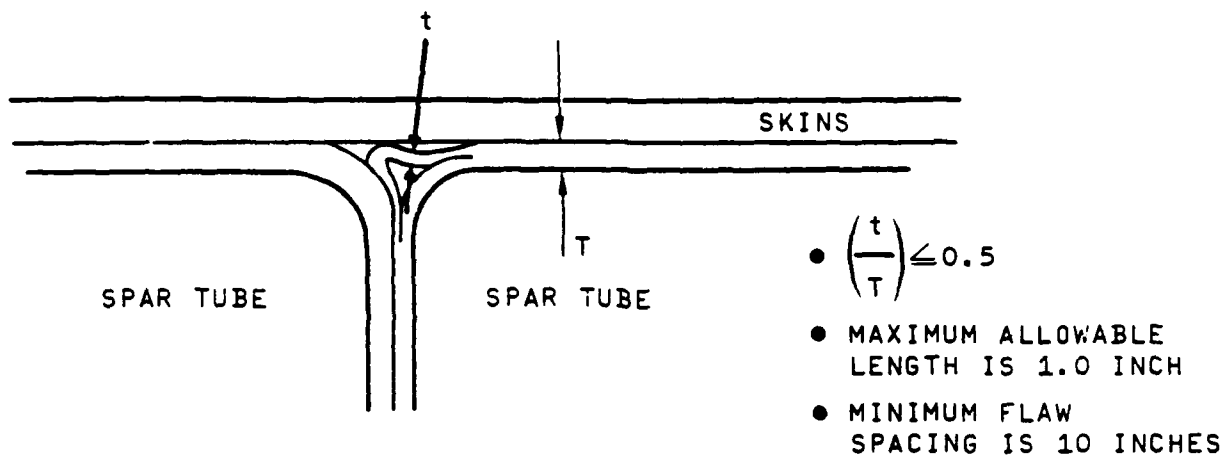


Figure F-14. Overlap, underlap, and gaps.

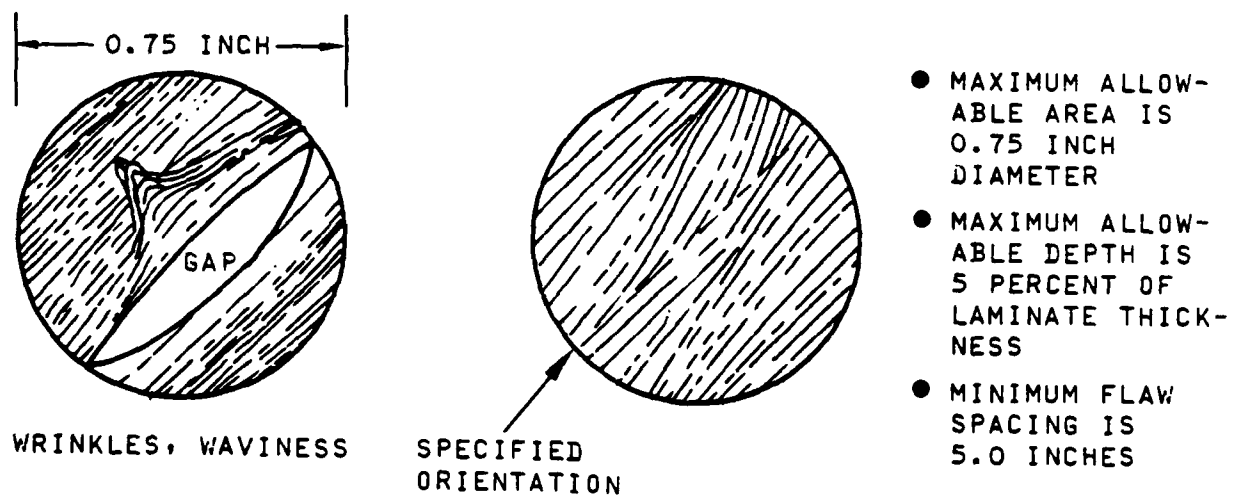


Figure F-15. Improper fly laydown.

APPENDIX G

FAILURE MODES, EFFECTS, AND CRITICALITY  
ANALYSIS OF THE COMPOSITE  
MAIN ROTOR BLADE FOR  
THE AH-64A HELICOPTER



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 1 OF 2  
 REV 1.00 DATE 12-15-91

PREPARED BY: J. JONES

WBS NO 711

SUBSYSTEM: ROTOR GEARING - MAIN MOTOR

7-111417 SUB-DATA (3RD) BLADE ASSEMBLY

REF NO. (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINTACTS (1)	V	I	D	COMMENTS/COMPENSATING PROVISIONS (12)	
				SUBSYSTEM (5)	AIR VEHICLE (6)						
7-111417-576	CLOSURE ASSEMBLY - IN-TROAND Provides gear high speed advancing blade tip aerodynamic performance by the location of the aft portion of the swept tip.	(a) Cracked or broken skin  (b) Debanding of the skin from the Nuxes/Woveycomb core.  (c) Structural failure (complete).	Visual Inspection, MFI  Visual Inspection, MFI  Visual Inspection, system response.	Slight degradation of blade performance.  Same as above.  Blade becomes unstable.	Possibility of slight vibration.  Same as above.  Possibility of abort due to vibration.	.015  1x2  1	1  1  1	1  1  1	1  1  1	-45 S  -45 S  -06 S -06 M	Deformation of the out-board aft closure may cause a change in blade tip path resulting in an out-of-track condition.  Same as above.  Partial loss of the closure would result in rotor imbalance and/or out-of-track condition. Vibration would vary, depending on the flight envelope.

NOTE:  
 Source 1 - CBZA, B and C series Helicopter Rotor Blade Inflow and wrap rate data analysis (ISAMRII, technical report 71-58).  
 Source 2 - Reliability and Maintainability Analysis for Model 410 main rotor blade (88-75).  
 Source 3 - Engineering judgement.



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 7 OF 22

DATE 12-13-81

REV A

PREPARED BY T. JONES

7-311412500-3A3H CHRBL BLADE ASSEMBLY

WAS NO 711

SUBSYSTEM ROTOR GROUP - MAIN ROTOR

7-311412500-3A3H CHRBL BLADE ASSEMBLY

REF NO. (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (7)	D V	T I M E	W O R L D	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)					
7-31141-2511-11	CLANSIRE, INWARD Emboss the blade root area and portions of the blade leading and trailing edges. Fabrication from REVLAR and bonded to blade.	(a) Cracked or broken  (b) Inboard-d	Visual Inspection, NDI  Visual Inspection, NDI	Slight to negligible degradation of blade performance  Degradation of blade performance dependent upon extent of delamination.	None  None	001	1 1 1	0	0	In process control limits the possibility of delamination.

FORM 1300REV (10/77)



FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 3 OF 22  
REV A DATE 12/15/11

PREPARED BY J. JONES

WBS NO 711

7-111612500-1A01 CHNR BLADE ASSY

SUBSYSTEM ROTOR LUBRIC MAIN ROTOR

REF NO (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACINS (7)	QTY (8)	TIME (9)	COST (10)	NO OF PEOPLE (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)						
7-111612517 and 1	ROTOR BLADE ASSY When opened, allows access to the adjustable hinge, stem balance weights for installation, removal or adjustment. Fabricated from 6061-T6 aluminum alloy and secured by 4 screws.	(a) Cracked  (b) Bent or loose.	Visual Inspection  Visual Inspection	None  Degraded blade performance due to lack of aerodynamic stability.	None  Possibility of a out-of-track condition.	.012  .	1  2	1  .	.70  .30	S  S	



FORM 1788-01-1 (08/71)



FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 4 OF 22

REV J. JONES DATE 12 15 81

PREPARED BY

W.B.S. NO. 711

SUBSYSTEM ROTOR GROUP-MAIN ROTOR

7-111412500-3A01 (100% BLADE ASSEMBLY)

REF NO (1)	ITEM Nomenclature & Function (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (7)	QTY (8)	OCCURRANCE RATE (9)	SEVERITY (10)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)					
7-11141-251A	WEIGHT, ADJUSTABLE - BLADE ASSEMBLY, SUPT TIP, MAIN ROTOR, AAH COMPOSITE BLADES Allows effective tuning of the blade in both the spanwise and chordwise directions. The tungsten alloy weights, A/R for the No. 1 spar tube and A/R for the No. 3 spar tube, are secured by a bolt, nut and washer.	(a) Structural failure (crack, bolt or washer).  (b) Mismatched loose (bolt or nut).	Sound of loose objects during rotor coast down and/or blade movement.  Same as above.	None  None	Too slight to notice.  None	000  000	1  1	A/R 1  A/R 1	40  60	5  5

FORM 1310000 (10/71)



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 01 OF 22

PREPARED BY J. J. JONES REV A DATE 12-15-81

SUBSYSTEM: ROTOR COMP. MAIN ROTOR WBS NO 711

7-11412500-1 AMH LRRR BLADE ASSY

REF NO (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (5)	QTY (6)	MODE (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (8)	AIR VEHICLE (9)				
7-11412516-11	FRICION SEPTIC BLADE ASSY SHEET TIP MAIN ROTOR, AMH COMPACTOR BLADES Provides erosion protection of the blade. Consists of thermoplastic elastomer (Elastane) 9.5 inch wide, bonded along the leading edge of the blade.	(a) Torn, shedded, eroded.  (b) Debanded/peeling.	Visual inspection  Visual inspection	Degraded erosion protection.  Degraded erosion protection.	None  Possible slight vibration.	162	1	.70 S  .10 S	

Form 1370 Rev 11/80/77



FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEETS 6 OF 22  
 DATE 11/2/81

PREPARED BY J. JONES REV

7-11141Z-00 MAIN PROP BLADE ASSEMBLY

WBS NO 711

SUBSYSTEM MAIN GROUP MAIN ROTOR

REF NO. (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINTENANCE (7)	QTY (8)	I T A G E (9)	M O D E L (10)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)					
7-11141 Z-08	BUSHING, ATTACH, SUPPORT TIP MAIN ROTOR, AMB COMPOSITE BLADE Four metallic bushings are permanently attached at the clevis to resist the high radial load exerted by the expandable bushings.	(a) Fractured/cracked. (b) Galled or scored	Visual Inspection Visual Inspection	Possible degraded blade retention Difficulty in removing or installing blade attaching pin.	None None	0.10	167	1	110 S	Failure due to excessive load (low test) - spin force not carried the full G.P. load

FORM 1218 REV 11/81





FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 8 OF 22

REV. A DATE: 12-12-81

PREPARED BY J. JONES

WBS NO 711

SYSTEM GROUP: MAIN MOTOR

7-11412500 144N CYMB BLADE ASSEMBLY

REF NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNDESIRABLE MAINT ACTS (7)	Y (8)	X (9)	Z (10)	COMMENTS/COMPLEMENTING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)					
7-311A1 7511 7511	SPAR TUBE There are 1 spar tubes, each serving as an alternate load path in case of ballistic damage and also providing a small amount of structural stiffness. Intentionally scored from Revlar 49.	(a) Cracked (one)  (b) Separated/handling voids. (one)	MI1 technique  MI1 technique.	Degraded performance  Same as above (a).	None  None	.003  .003	1  1	.50  .50	5  5	Other spar tubes serve as alternate load paths.  Same as above (a). In-process inspection will detect debonding / redundancy is provided by design.

7-11412500 007 1/10/12



# FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET: 9 OF 22  
 REV: A DATE: 12-15-81

PREPARED BY: J. J. JUMBS

WBS NO: 711  
 7-111412500-1, A41 0300 Blade Assembly

REF NO. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (17)	P (18)	Q (19)	R (20)	S (21)	COMMENTS/RECOMMENDATIONS/PROVISIONS (22)
				SUBSYSTEM (5)	AIR VEHICLE (6)						
7-111412516	<p><b>CORE ASSEMBLY, AP1</b></p> <p>The core assembly makes up the AP1 portion of the blade airfoil and adds to the chordwise and torsional stiffness.</p> <p>Assembly consists of a composite fabric channel, P/W 7-111412513, a Honeycomb Core, P/W 7-111412512 and graphite trailing edge joints, P/W 7-111412516</p>	<p>a) Channel, P/W 7-111412513</p> <ol style="list-style-type: none"> <li>Delaminated</li> <li>Bonding voids</li> </ol> <p>b) Core, P/W 7-111412512</p> <ol style="list-style-type: none"> <li>Separation of splice joints</li> </ol> <p>c) Trailing edge joints, P/W 7-111412516</p> <ol style="list-style-type: none"> <li>Bonding voids</li> <li>Cracked</li> </ol>	<p>Visual inspection N.D.I.</p> <p>Same as above</p> <p>N.D.I.</p> <p>Visual inspection N.D.I.</p> <p>Visual inspection</p>	<p>Possibility of slight degradation of blade performance</p> <p>Same as above</p> <p>None</p> <p>Same as a) 1 above</p> <p>Same as a) 1 above</p>	<p>Possibility of slight vibration</p> <p>Same as above</p> <p>None</p> <p>Possibility of vibration due to airfoil deformation</p> <p>Same as above</p>	011	15	1	1	04 S 01 M .25 S .15 S 15 S 05 M 30 S 05 M	<p>Airfoil deformation along the channel may cause a out-of-track condition</p> <p>SKIN to core bond would eliminate any deformation due to splice separation.</p> <p>Vibration due to blade out-of-track depends on amt of airfoil deformation</p> <p>Trailing edge subjected to light loads only</p>



FORM 1238 (REV 11/80)

FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 10 OF 22  
 REV A DATE 11/11/71

PREPARED BY J. JONES

WBS NO 711

SUBSYSTEM ROTOR CARRIER MAIN ROTOR

7-31141Z506-1AAR-010R BLADE ASSEMBLY

REF NO. (1)	ITEM NOMENCLATURE & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL DESIGNED MAINTENANCE FACTORS (7)	Y M E (10)	S I L (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)				
7-31141-2537-47, 49, 51, 53	SPAR CAP ASSEMBLY Primary members that provide flap wise stiffness for the blade. Fabricated from Kevlar 49. The assembly consists of an inner skin, spar sub-assemblies, and spar wraps and a graphite inner skin.	(a) Cracked  (b) Delaminated, delaminated	NDI technique  NDI technique	Degradation of blade performance.  Loss of blade performance.	No immediate effect.  Possible mission abort	.001  .001	1  1	S  S	A crack, depending on size and location, would decrease the flapwise stiffness, resulting in a out-of-track condition with a change of power

FORM 1728-001 (10/71)



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 11 OF 22  
 REV. A DATE 11/11/72

PREPARED BY: J. JONES

W.B.S. NO 111

7-31141/MD 1 AIR OHR BLADE ASSEMBLY

ITEM NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (7)		P (8)	Q (9)	R (10)	S (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)	UMA (1000 Hr)	SOURCE					
7-31141 25M NSP-11	SEIN, DRIBBLEP, INWARD Provides skin reinforcement to meet blade torsional requirements. Consists of a lower and upper assembly fabricated from Kovlar 49.	(a) Cracked  (b) Delaminated, delaminated.	NDI technique or visual inspection	possible degraded blade performance	No effect		1	1	1	1	45	Should be discovered in daily inspection
			NDI technique or visual inspection	Loss of blade torsional restraint.	Possibility of vertical vibration.						45 10 M	Blade rake angle may change more than other blades due to deflection doubler.

FORM 1320-004 (10/71)





**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 12 OF 22  
 REV A DATE 12-12-71

PREPARED BY J. JONES

WBS NO 711

7-311A12500-3 AHI COMB BLADE ASSEMBLY

REF AND. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNDESIRABLE MAINT ACTS (7)	V (8)	I (9)	D (10)	S (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)						
7-311A12519	ROUNDER, INWARD CAP Provides cap reinforcement to meet blade structural requirements. Consists of 23 Rivets & 40 Fabricated plates.	(a) Cracked  (c) Deformed, delaminated.	AMI technique  AMI technique	Degraded blade performance.  Degraded blade performance.	No effect  Possibility of vertical vibration.	.01 162	2 1			.10 5  .60 5 .02 5	



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 11 OF 22  
REV A DATE 12-15-81

PREPARED BY J. JONES

SUBSYSTEM ROTOR GROUP MAIN ROTOR WBS NO. 711

7-311412500-1AAR COMB BLADE ASSEMBLY

REF NO. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (7)	V	Y	D	O	P	COMMERCIAL/OPERATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)							
7-311412500-1AAR	WEDGE, INBOARD - BLADE ASST. SHEET TIP MAIN ROTOR, AAR COMPOSITE BLADES	(a) Cracked	NPI technique	No effect	No effect	.001	1	1				
2, 4	Fills the triangular cavity between the inboard inner packs and bushings to ensure structural integrity of the blade root area. Consists of resin impregnated milled E-glass fibers.	(b) Debonded	NPI technique	Loss of root structural integrity and blade performance degraded.	No effect							



FORM 3370 (1-1-81)

**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 1A OF 22  
 REV A DATE 12-15-81

PREPARED BY J. JAMES

SUBSYSTEM ROTOR DRIVE MAIN MOTOR

WBS NO 711

7-311417500-MAIN TMR BLADE ASSEMBLY

REF NO. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT (5)		TOTAL UNDESIRABLE MAINT ACTS (7)	CIRCUIT (10)	COMMENTS/CONSIDERATIONS/PROVISIONS (11)	
				SUBSYSTEM (5a)	AIR VEHICLE (5b)				MAINT SOURCE (6)
7-311417541	<p>COMP ASSEMBLY - COMPOSITE MAIN MAIN ROTOR BLADE SUPPORT TIP</p> <p>Fills the forward section of the swept tip region to ensure structural integrity. Consists of Kevlar AS, resin impregnated fibers and foam.</p>	<p>(a) Cracked</p> <p>(b) Delaminated, delaminated</p>	<p>(a) technique</p> <p>(b) technique</p>	<p>Degraded swept tip structural integrity and blade performance.</p> <p>Loss of swept tip structural integrity and blade performance.</p>	<p>No effect</p> <p>Possibility of out-of-track due to change in tip air foil in-process control blade delamination possibilities.</p>	.001 167	1	.50 S	.50 S

FORM 1330 REV (10/79)



FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 15 OF 22  
 REV. A DATE 12-15-81

PREPARED BY J. JONES

WBS NO. 711

7-311612-50C-314H CRIB BLADE ASSEMBLY

REF NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (5)	PRIORITY (6)	TOLERANCE (7)	REPAIR (8)	REPLACEMENT (9)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5a)	AIR VEHICLE (5b)						
7-311612-50C-314H	SKIN, OUTER Provides a major portion of the blade torsional stiffness and shear for the spar caps and the trailing edge longerons. Consists of one continuous piece of 0.062 inch thick Revalor 49.	(a) Cracked  (b) Delaminated, debonded.	Visual inspection  NDI, visual inspection	Degraded blade performance.  Loss of blade performance.	No immediate effect.  Possibility of vibration.	.041 142	1	1	40	S	Should be found on daily inspection and repaired as required.
									45	S	Change in air foil may cause an out-of-track condition. In-process control limits delamination possibilities.



FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)

SHEET 16 OF 22

REV A DATE 12-15-81

PREPARED BY J. JONES

WBS NO 711

SUBSYSTEM: AUTOM GROUP MAIN BUTTER

7-31141250E-100R OVER BLADE ASSEMBLY

REF NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL CRITICALITY WEIGHTING FACTOR (5)			COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)	WHA (1000 HR) (7)	BOUNCE (8)	NOISE (9)	
7-31141 2502-9 -11, -13 15, 19, 21, 23, and 25	<p>LIGHTNING SCREEN BLADE ASSY SUPPORT TIP MAIN BUTTER AAR COMPOSITE BLADES</p> <p>Shields all metallic components in the blade, provides lightning protection of the blades and provides a continuous electrical path into the hub (the shield is conductively bonded to the blade root bushings). Consists of 200 x 200 mesh 2 mil wire dia, 5056 aluminum.</p>	<p>(a) Cracked, discontinuities.</p> <p>(b) Bonding voids.</p>	<p>IRI technique</p> <p>IRI technique</p>	<p>Possible loss of some lightning shield protection.</p> <p>Possibility of some loss of blade performance.</p>	<p>No effect.</p> <p>Possibility of vibration.</p>	<p>.001</p> <p>162</p>	<p>1</p> <p>30</p> <p>5</p>	<p>NO</p> <p>NO</p> <p>NO</p>	<p>Change in airfoil due to welds, may cause an out-of-track. In-process control limits the possibility of bonding voids.</p>



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 12 OF 22  
 REV A DATE 12-15-81

PREPARED BY J. JONES

SUBSYSTEM ROTOR GROUP-MAIN ROTOR WBS NO 711

7-111A12XN - MAIN COMB BLADE ASSEMBLY

REF NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODE/S (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNDESIRABLE MAINT ACTS (7)	P (8)	Q (9)	R (10)	S (11)	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)						
7-111A12548	<p>OFFICER, FORWARD TIP-BLADE ASSEMBLY SHEET TIP MAIN ROTOR, AIR COMPOSITE BLADE</p> <p>Located in the outboard end of the No. 1 spar tube, provides for effective tuning of the blade in the spanwise and chordwise direction. Fabricated from 17-4PH CRES &amp; integrally wound into the spar</p>	<p>(a) Damaged threads</p> <p>(b) Bonding voids</p>	<p>Found during inspection or balance adjustment.</p> <p>Wet technique</p>	None	None	.001	1	1	.40	S	
				None	None				.60	S	



**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET 18 OF 22  
REV A DATE 12-13-91

PREPARED BY: J. JONES

W.B.S. NO 711

SUBSYSTEM: ROTOR GROUP-MAIN ROTOR

7-311412500-3401 CMBR BLADP ASSEMBLY

REF NO. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNSCHEDULED MAINT ACTS (7)	1 0 1 2 3 4 5 6 7 8 9 10 11 12	COMMENTS/COMPENSATING PROVISIONS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)			
7-31141 7540	WEIGHT, AFT TIP-BLADP ASST. SHEET TIP MAIN ROTOR, AIR TURBOPROP BLADP. located in the outboard end of the No. 3 spar tube, provides for effective tuning of the blade in the spanwise and chordwise direction. Fabricated from A136-T6 Alcoa & integrally wound into the spar	(a) Damaged threads  (b) Bonding voids	Visual inspection or balance adjustment.  NBI technique	None  No effect	None  None	1  1	1  1	







**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SUBSYSTEM: BLTWR COMP MAIN ROTOR WBS NO: 711 PREPARED BY: J. JONES REV: A SHEET: 20 OF 22 DATE: 12-11-81

7-311417-000, AAN OVER BLADE ASSEMBLY

REF NO (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHOD OF DETECTION (4)	FAILURE EFFECT		TOTAL UNDESIRABLE FACTORS (10) (11)	COMMENTS/CONTINGENCY PROVIDERS (12)
				SUBSYSTEM (5)	AIR VEHICLE (6)		
7-31141 2554	BACKING STRIP-BLADDER ASSEMBLY SHEET TIP MAIN ROTOR, AAN COMPOSITE BLADES Stainless steel backing strip for the tip chrome plating elastomer erosion strip. (Lslame)	(a) Cracked  (b) Bonding voids  (c) Eroded/peened	NIT technique and/or inspection when replacing strip.  NIT technique  Visual	None  None  Possibility of slight vibration.	None  None  Possibility of slight vibration.	.075  .10  .35  .35	(12)

**FAILURE MODES, EFFECTS AND CRITICALITY ANALYSIS (FMECA)**

SHEET: 21 OF 22  
 PREPARED BY: J. Jones DATE: 12-15-61

SUBSYSTEM: ROTOR GRIP MAIN MOTOR W.B.N. NO. 711

7-111A12-10-J AM UMR Blade Assembly

REF. NO. (1)	ITEM DESCRIPTION & FUNCTION (2)	FAILURE MODES (3)	METHODS OF DETECTION (4)	FAILURE EFFECT		TOTAL UNDESIRABLE EFFECTS (5)		COMMENTS/CONSIDERATIONS/PROVISIONS (12)
				SUBSYSTEM (M)	AIR VEHICLE (N)	AREA (100%) (6)	PERCENTAGE (7)	
7-111A12-5A1 and 1	<p><b>HINGE-IRIM TAB</b></p> <p>Fabricated from .016 sheet Al. Alloy 2024-T1. The hinge is located on the top side and the -3 is located on the bottom of the trailing edge from Sta. 175.50 to Sta. 246.00. The tab is bent up or down, at various stations so as to aerodynamically change the blade airfoil making it compatible with the other blades.</p>	<p>a) Cracked</p> <p>b) Bonding voids</p>	<p>Visual, inspection</p> <p>Visual, inspection</p>	<p>Possible degradation of blade performance</p> <p>None</p>	<p>Possibility of out-of-track vibration</p> <p>None</p>	<p>.015</p> <p>263</p> <p>16</p>	<p>AS</p> <p>115</p> <p>40</p>	<p>Amount of vibration would depend on size and location of crack</p>



FORM 1278-50-1 (10/71)

**IRM LEVEL  
FAILURE MODES, EFFECTS AND CRITICAL ANALYSIS (FMECA)**

SUBSYSTEM: MAIN MOTOR      REV: 22      SHEET: 22      OF: 22      DATE: 12-15-81  
 PREPARED BY: I. JONES  
 RU: CNR      BU: 7-311412504-3      REV: 01  
 SUB: 7-311412504-3      BU: 7-311412504-3      REV: 01  
 SUB: 7-311412504-3      BU: 7-311412504-3      REV: 01

ITEM PART NO. DESCRIPTION	FAILURE MODES	DETECT OR DETECTION	FAILURE EFFECT		ITEM FAILURE RATE (10 <sup>-6</sup> /HR)	Y T M E C O D E	COMMUNICATIONS/REPAIRING PROVISIONS
			RU (S)	SUBSYSTEM (M)			
BLADE HEATING  Electro thermally heating elements of the de-icer are bonded to the leading edge of the blade. The de-icer is divided internally into five cordage heating zones along the leading edge of the blade. Each zone is heated sequentially to melt the bond between the ice and the blade surface to allow centrifugal and aerodynamic forces to sweep the loosened ice away. The de-icer mat extends over 9.2 percent of the top surface chord length and 26 percent of the lower surface chord from the blade leading edge.	(a) De-icer blanket 15-200-23 P/N 7-311412546 1. Blanket element cracked. 2. Bonding voids. 3. Open in electrical wiring from connector to blanket.  (b) Receptacle-electrical connection for blade de-icing. 15-00025 P/N 103123-R-8 JER14W 1. Open/shorted pins 2. Bent pins/cracked receptacle (c) Receptacle - vibration receptacle to the connector bracket arm. 15-200-25 P/N 103123-15A10A 1. Cracked/loose  (d) Connector bracket arm 15-200-26 P/N 7-311412517 1. Cracked/bent 2. Fractured	(a) None (b) None (c) Visual (d) Visual	Possibility of degraded de-icing in that zone.  No effect on de-icing.  Loss of de-icing capability for that blank.  Loss of de-icing capability for that blade.  Same as above (a).  Same as above (a).  None  None, but may result in a secondary failure, such as a loose connector and/or broken wire.	.045    243	1    1	12 S 04 S 45 F 01 M  13 S 01 M 08 S 01 S  08 S 03 S	Amount of vibration, due to rotor imbalance will depend on amount of ice build-up. In-process control limits the possibility of voids.  Mission abort would depend on vibration on the result of ice build-up on that blade.  Same as above (a).



APPENDIX H  
STRESS ANALYSIS



The static and fatigue stress analyses for the CMRB show that it is satisfactory, structurally, for the mission of the AH-64A. For the undamaged blade, the analysis shows that there will be no failure at ultimate load (1.5 x limit load), and negligible permanent set under limit loads. Table H-1 summarizes the minimum margins of safety for critical regions of the blade. Positive margins are shown throughout. This finding was verified by the laboratory tests.

TABLE H-1. MINIMUM STATIC MARGINS OF SAFETY

Blade Station	Item	Load Condition	Type of Stress	Margin of Safety
39	Attach Lugs	RPM = 289 V = 180 Kts $M_z = 3.5$	Tension in Kevlar Windings	0.40
191.7	Constant Section	RPM = 289 V = 180 Kts $M_z = 3.5$	Compression in Kevlar spar longos in the constant section	0.06
87	Constant Section	RPM = 289 V = 180 Kts $M_z = 3.5$	Shear due to torsion in $\pm 45^\circ$ layers of the constant section	0.05
89	Constant Section	RPM = 0 Max Torque V = 0 Kts $n_z = 1.0$	Compression in Kevlar spar longos after the T. E. longos have buckled	High
270	Blade Tip	RPM = 376 $V_f = 150$ Kts $n_z = 3.5$	Tension load applied to tip weight housings and blade tip	High

The fatigue life of the CMRB has been substantiated by a combination of analysis and component fatigue tests. In using the test data, the endurance limit is reduced for scatter effects according to Table H-2. The life for the various sections of the CMRB are presented in Table H-3. That the CMRB has an adequate static margin of safety and a fatigue life in excess of 4500 hours has been verified by laboratory test of full-scale specimens.

TABLE H-2. L-N CURVE SCATTER REDUCTION FACTORS

Number of Fatigue Test Specimens	Percent of Mean L-N Curve Used
1	50%
2	65%
3	75%
4 or more	Statistical analysis (M-3 $\sigma$ )

TABLE H-3. FATIGUE ANALYSIS - SUMMARY OF COMPONENT LIVES

Blade Station	Item	Condition	Life
39	Root Lugs	Weighted Fatigue	4,500 hours
		Ground-Air-Ground	100,000 hours
39	Root Close-Out	Weighted Fatigue	Infinite
55	Root Doubler	Weighted Fatigue	4,500 hours
84	Constant Section	Weighted Fatigue	4,500 hours
160	Constant Section	Weighted Fatigue	4,500 hours
192	Constant Section	Weighted Fatigue	4,500 hours
270	Tip Components	Gag	Infinite

Ballistic survivability calculations show that the CMRB can fly a minimum of 30 minutes after being damaged by a 23mm HEI-T projectile. Figure H-1 summarizes the results of the survivability analysis.

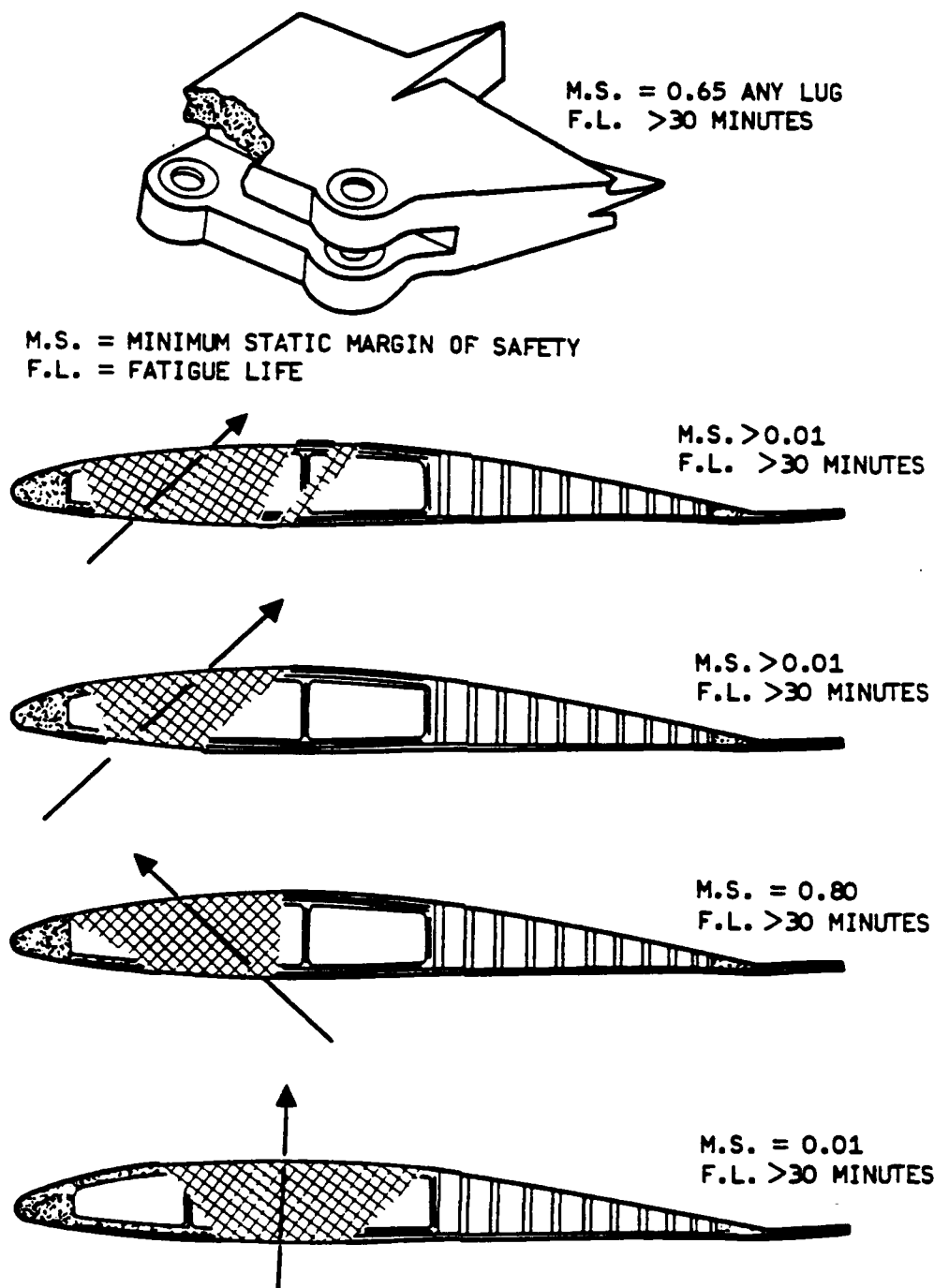


Figure H-1. Ballistic survivability summary - 23mm HEI-T threat.



APPENDIX I  
MASS PROPERTIES

The mass properties of the CMRB are summarized in Tables I-1 and I-2. The figures show the distribution of weight, chordwise center of gravity, and pitching inertia along the span of the blade. Table I-1, the rotor blade group (shipset of four blades) weight chart specified by Reference I-1, shows a CMRB group weight of 603.2 pounds - a 24.6-pound reduction from the metal blade group. Table I-2 documents the CMRB center of gravity characteristics for three zones along the blade span that were required for blade dynamic analysis. The polar moment of inertia of each CMRB is 993 slug-feet-squared as compared with 1017 slug-feet-squared for the metal blade. This is anticipated to have a negligible effect on autorotation performance.

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I-1 Military Standard - Weight and Balance Data Reporting Forms for Aircraft (including Rotorcraft), MIL-STD-1347A Part II, 30 September 1977.

TABLE I-1. AH-64A ROTOR/BLADE GROUP WEIGHT

		Metal		CMRB			
1.							
2.							
3.							
4.							
5.							
6.							
7.							
8.	Spar/Tube-Front	87.1		143.6			
9.	Spar/Tube-Intermed.	64.3		14.4			
10.	Spar/Tube-Rear	65.1		19.6			
11.	Interspar-Cover			107.2			
12.							
13.							
14.							
15.	Interspar Adhesive	11.5		-			
16.							
17.							
18.							
19.							
20.	Leading Edge-Cover	94.6		16.4			
21.							
22.							
23.							
24.	L. E. De-Ice Blanket	13.9		6.8			
25.							
26.							
27.							
28.	Trailing Edge-Member	-		20.0			
29.	Trailing Edge Cover	25.5		-			

TABLE I-1. AH-64A ROTOR/BLADE GROUP WEIGHT (CONT)

		Metal		CMRB			
30.							
31.	Trailing Edge Ribs	0.9		-			
32.	Trailing Edge-Core	8.1		6.8			
33.							
34.							
35.	Trailing Edge-Adhes	12.1		5.2			
36.							
37.							
38.							
39.							
40.	Tips	33.9		16.0			
41.							
42.							
43.							
44.							
45.	Balance Weights-Tip	14.7		12.8			
46.	Bal. Wts. -Lead. Edge	95.1		152.8			
47.							
48.							
49.	Trim Tab	11.0		2.0			
50.							
51.	Root End-Fittings	73.1		57.6			
52.	Root End-Fasteners	10.5		3.6			
53.	Exterior Finish	6.3		5.2			
54.	Static Discharge	0.1		0.8			
55.	M/R Mfg. Allowance	-		12.4			
56.	Column Totals	627.8		603.2			
57.							

TABLE I-2. CENTER OF GRAVITY CHARACTERISTICS

		Center of Gravity				
		Weight (lb)	BS (in.)	Chord (in.)	% Chord	Dynamic Criteria % Chord
CMRB	Root (BS 37 to 82)	41.34	55.34	5.78	27.5	≤27.6
	Mid (BS 82 to 244)	72.34	162.95	5.37	25.6	≤26.5
	Tip (BS 244 to 288)	<u>33.62</u>	<u>266.13</u>	<u>5.25</u>	<u>25.0</u>	<u>≤25.0</u>
	Total	147.30	156.30	5.46	26.0	26.4
		(Shipset: 589.20 lb)*				(Spanwise moment = 23,500 lb-in)

\*603.2 lb in Table I-1 includes manufacturing allowance.

APPENDIX J

AEROELASTICITY AND MECHANICAL STABILITY



The stability of the CMRB and support structure was investigated by a linear eigenvalue analysis and by a nonlinear transient analysis described in Reference 8. The eigenvalue analysis couples an eleven-cell single blade to a simple model of the hub flexibility and fuselage rigid body degrees of freedom. The rotor support flexibility and fuselage rigid body degrees of freedom are necessarily isotropic for this linear analysis. Coupling terms are included to relate blade pitch changes to hub motion. This idealization of the system is adequate to represent the advancing and regressive cyclic modes of the system, the most important of which is the advancing whirl mode. The nonlinear transient analysis allows the anisotropic properties of the rotor system to be represented and includes all four blades, lateral and longitudinal control stiffnesses, hub constraints, fuselage free-body modes, and two fuselage bending modes. Each blade is represented by five degrees of freedom: two flap modes, two torsion modes, and one lead-lag mode.

Cyclic and collective resonance diagrams, including the influence of aerodynamic forces, are presented in Figures J-1 and J-2, respectively, and show good separation between natural frequencies and forcing functions for all modes except for the second torsion mode and the  $7\Omega$  line. However, this mode is very well damped and was impossible to excite during the whirlstand test, and is considered to be acceptable for the CMRB. Figure J-3 shows modal damping ratios as a function of rotor speed for a series of forward speeds, and Tables J-1 through J-3 show the corresponding natural frequencies. Forward speed is accounted for by applying aerodynamic forces corresponding to the 90-degree azimuth position (advancing blade).

Figure J-4 shows the whirl mode damping for the severe condition obtained from the linear eigenvalue analysis. The most critical condition ( $\theta_{3/4} = 6$  degrees,  $N_Z = 3.5$ ) has a stability boundary above 130 percent  $N_R$ .

Advancing lag mode stability boundaries are presented in Figure J-5 and show a low boundary for the case of high load factors at low collective pitch settings (cyclic pullup in autorotation). However, in comparing this figure with Figure B-7 of Reference J-1, the CMRB is shown to have an improvement in the advancing lag mode stability boundaries over that of the metal

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J-1 Silverthorn, L. J.; Childers, H. M., and Neff, J. R., Preliminary Aeroelasticity and Mechanical Stability Report YAH-64 Advanced Attack Helicopter, Hughes Helicopters, Inc. Report No. 77-X-8001, June 1976.



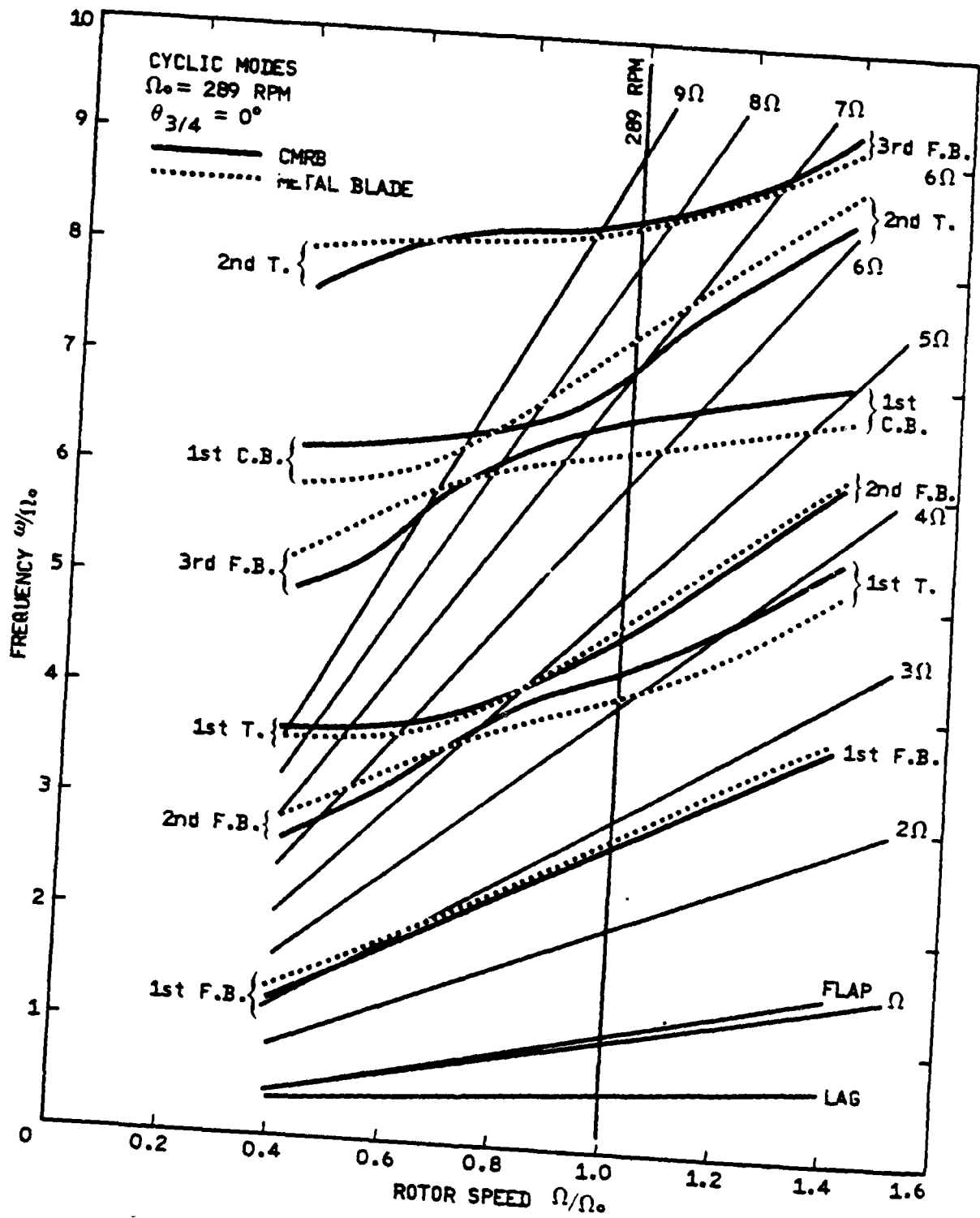


Figure J-1. CMRB cyclic resonance diagram.

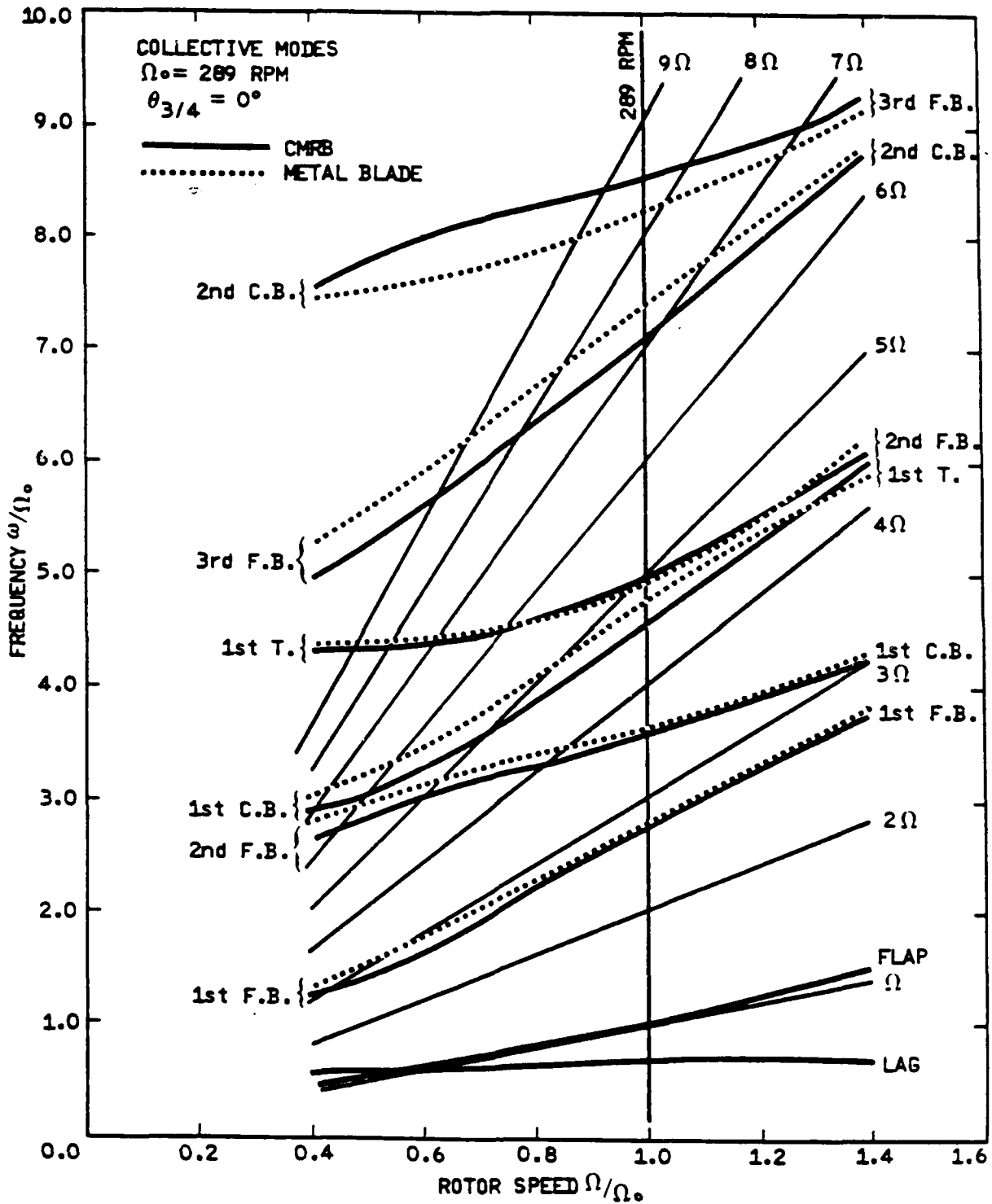


Figure J-2. CMRB collective resonance diagram.

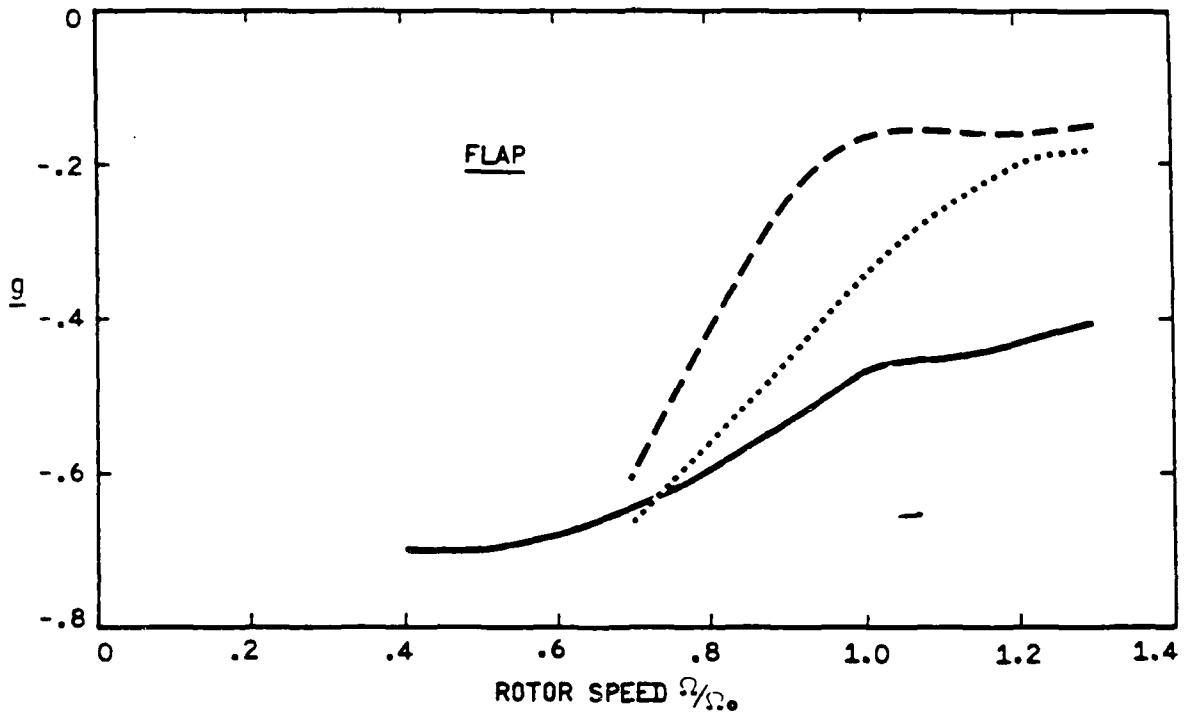
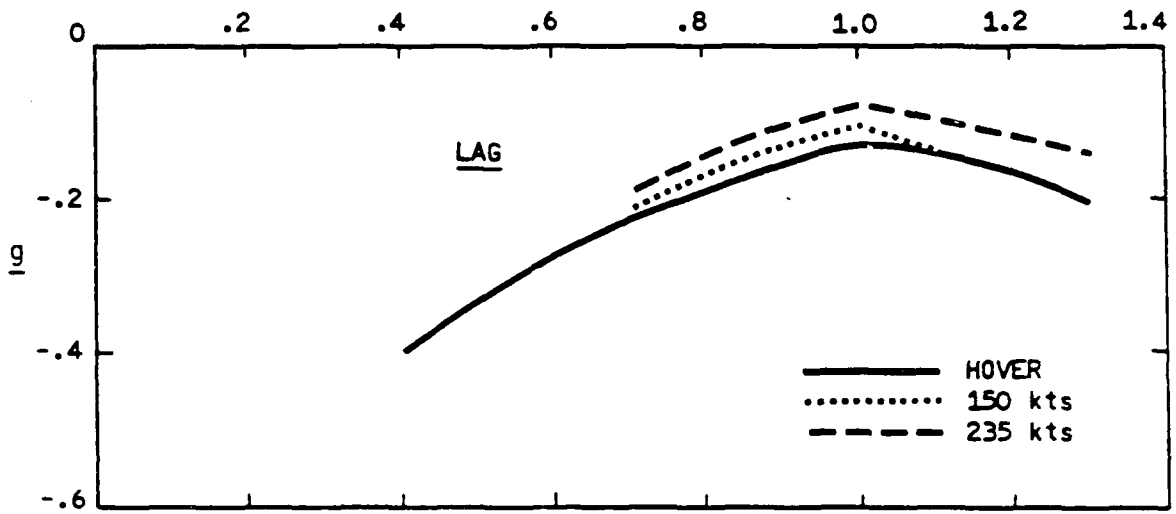


Figure J-3. CMRB modal damping versus rotor speed (sheet 1 of 4).

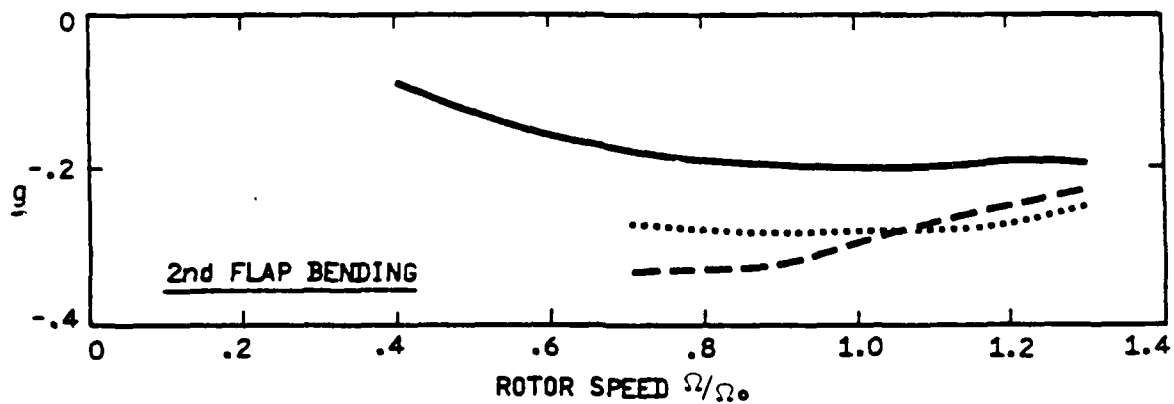
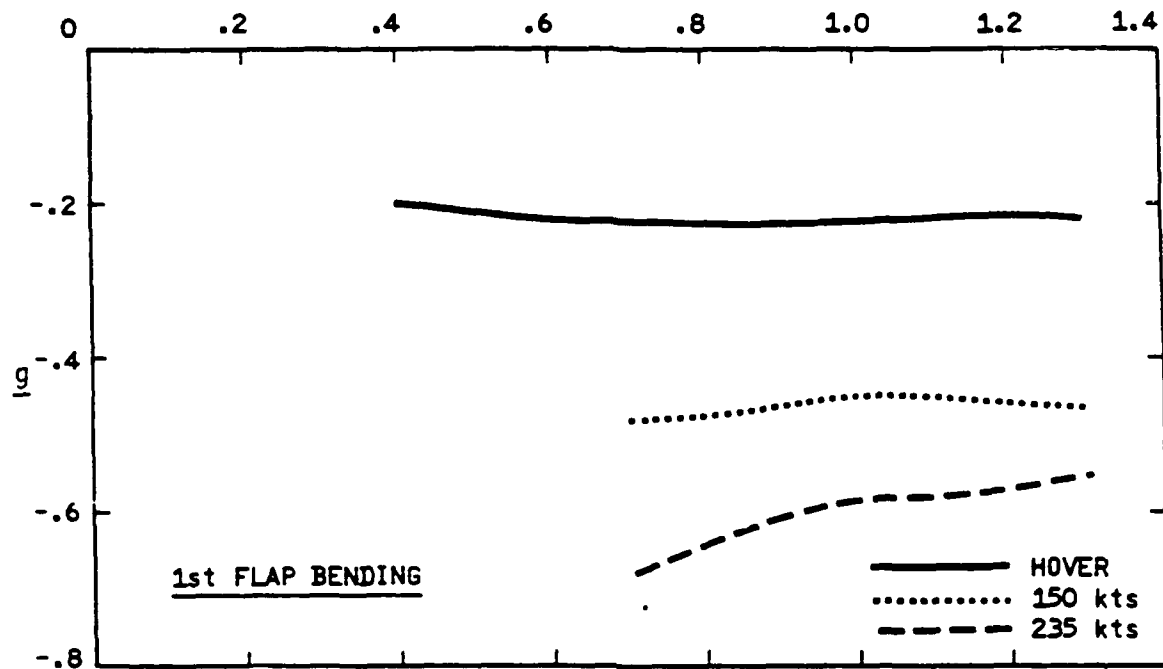


Figure J-3. CMRB modal damping versus rotor speed (Sheet 2 of 4).

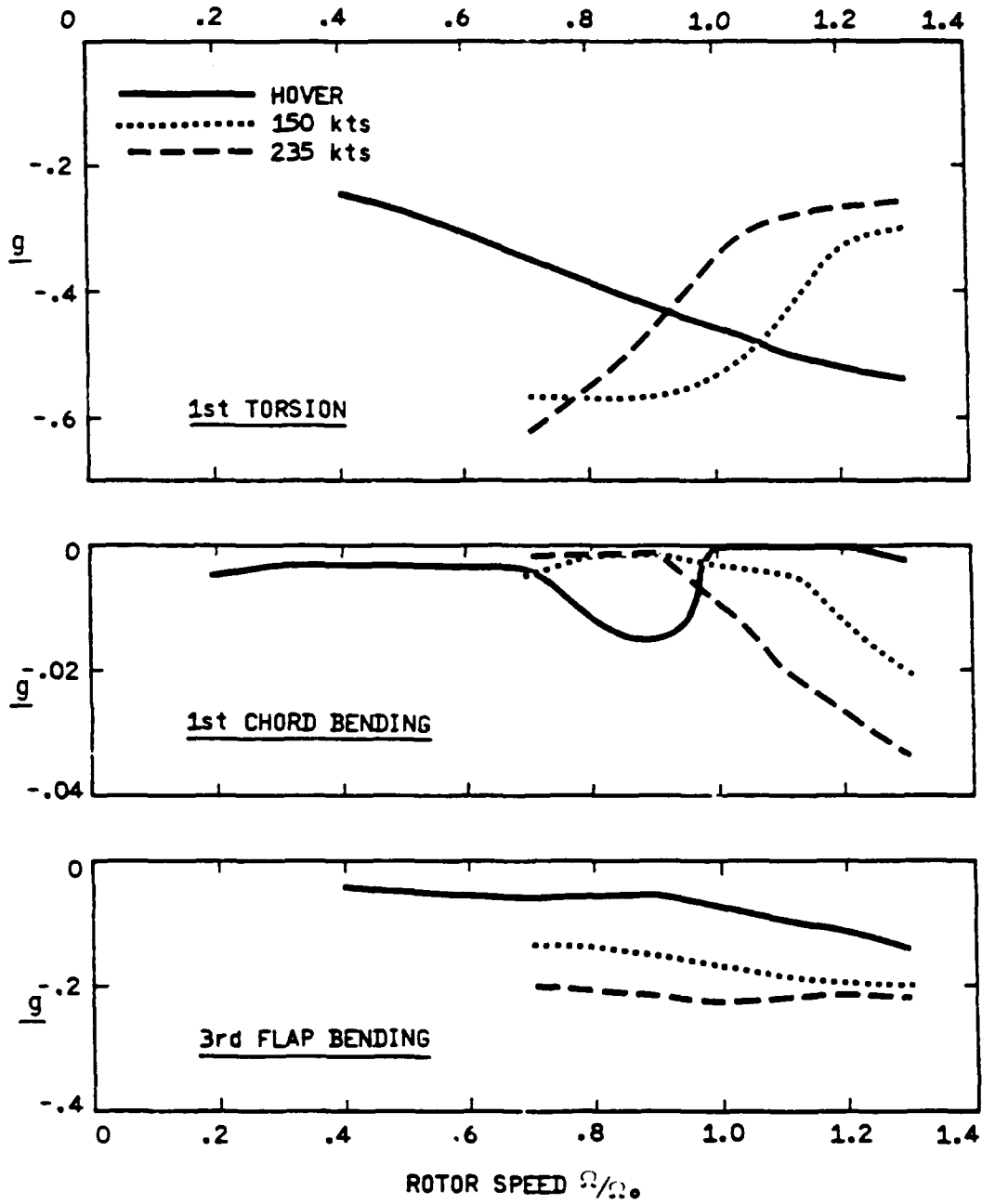


Figure J-3. CMRB modal damping versus rotor speed (Sheet 3 of 4).

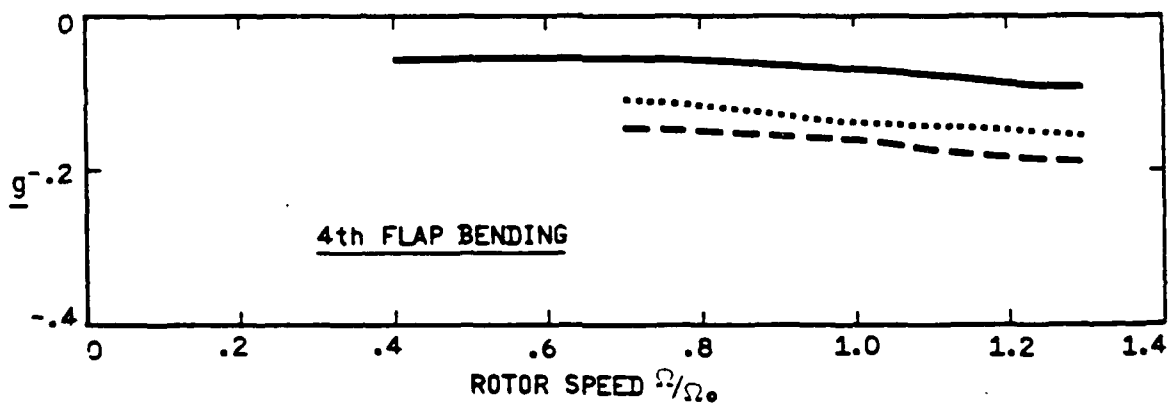
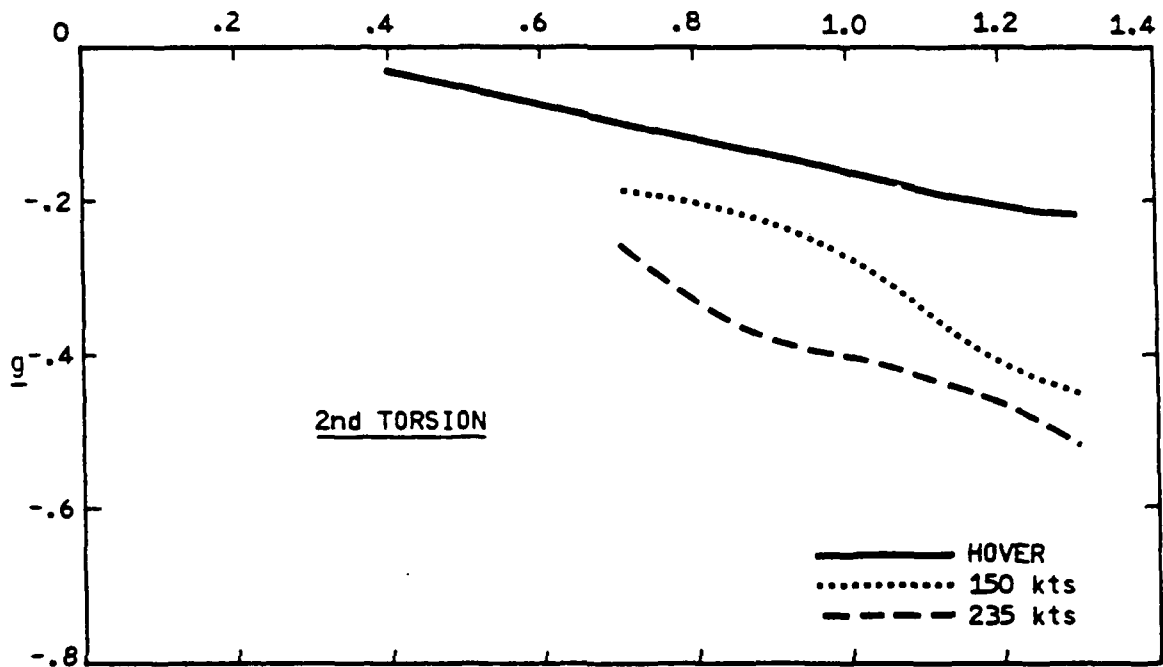


Figure J-3. CMRB modal damping versus rotor speed (Sheet 4 of 4).

TABLE J-1. CMRB DAMPED NATURAL FREQUENCIES,  
 3.5 g,  $\theta_{3/4} = 12^\circ$ , HOVER

Root No	Frequency (cyc/rev)								
	116 rpm	202 rpm	260 rpm	289 rpm	318 rpm	347 rpm	376 rpm		
1	0.667	0.500	0.450	0.432	0.431	0.426	0.421		
2	1.189	1.194	1.214	1.221	1.191	1.174	1.166		
3	3.163	2.830	2.767	2.749	2.740	2.735	2.724		
4	6.731	5.028	4.470	4.256	4.107	3.985	3.849		
5	9.001	5.447	4.771	4.654	4.566	4.489	4.424		
6	12.24	8.256	6.953	6.388	5.942	5.568	5.256		
7	15.23	9.061	7.525	7.121	6.809	6.534	6.250		
8	19.12	12.06	9.561	8.733	8.015	7.458	7.049		
9	20.98	12.46	10.65	10.06	9.593	9.217	8.907		

TABLE J-2. CMRB DAMPED NATURAL FREQUENCIES,  
 3.5 g,  $\theta_{3/4} = 12^\circ$ ,  $V = 150$  KNOTS

Root No	Frequency (cyc/rev)					
	202 rpm	260 rpm	289 rpm	318 rpm	347 rpm	376 rpm
1	0.484	0.430	0.412	0.409	0.412	0.417
2	1.254	1.299	1.304	1.260	1.213	1.172
3	2.876	2.782	2.736	2.711	2.684	2.657
4	5.008	4.575	4.450	4.428	4.381	4.303
5	6.596	5.796	5.618	5.568	5.435	5.168
6	8.404	7.055	6.455	6.017	5.645	5.328
7	8.923	7.415	7.042	6.775	6.612	6.436
8	12.44	9.926	9.188	8.809	8.868	8.664
9	12.50	10.73	10.13	9.641	9.248	8.928



TABLE J-3. CMRB DAMPED NATURAL FREQUENCIES,  
 $3.5 \text{ g}$ ,  $\theta_{3/4} = 12^\circ$   $V = 235 \text{ KNOTS}$

Root No	Frequency (cyc/rev)							
	202 rpm	260 rpm	289 rpm	318 rpm	347 rpm	376 rpm		
1	0.497	0.434	0.421	0.428	0.435	0.434		
2	1.266	1.287	1.262	1.201	1.151	1.124		
3	2.881	2.755	2.702	2.661	2.629	2.603		
4	5.017	4.691	4.592	4.476	4.389	4.328		
5	7.537	6.990	6.492	6.049	5.668	5.345		
6	8.467	7.110	6.706	6.261	5.875	5.554		
7	8.850	7.387	7.090	6.853	6.634	6.460		
8	12.53	10.74	10.13	9.648	9.269	8.936		
9	12.74	10.87	10.93	-	10.42	10.07		

$\Omega_0 = 289$  RPM  
 STATIONARY SYSTEM  
 $V = 0$  kts  
 $3.5 g$

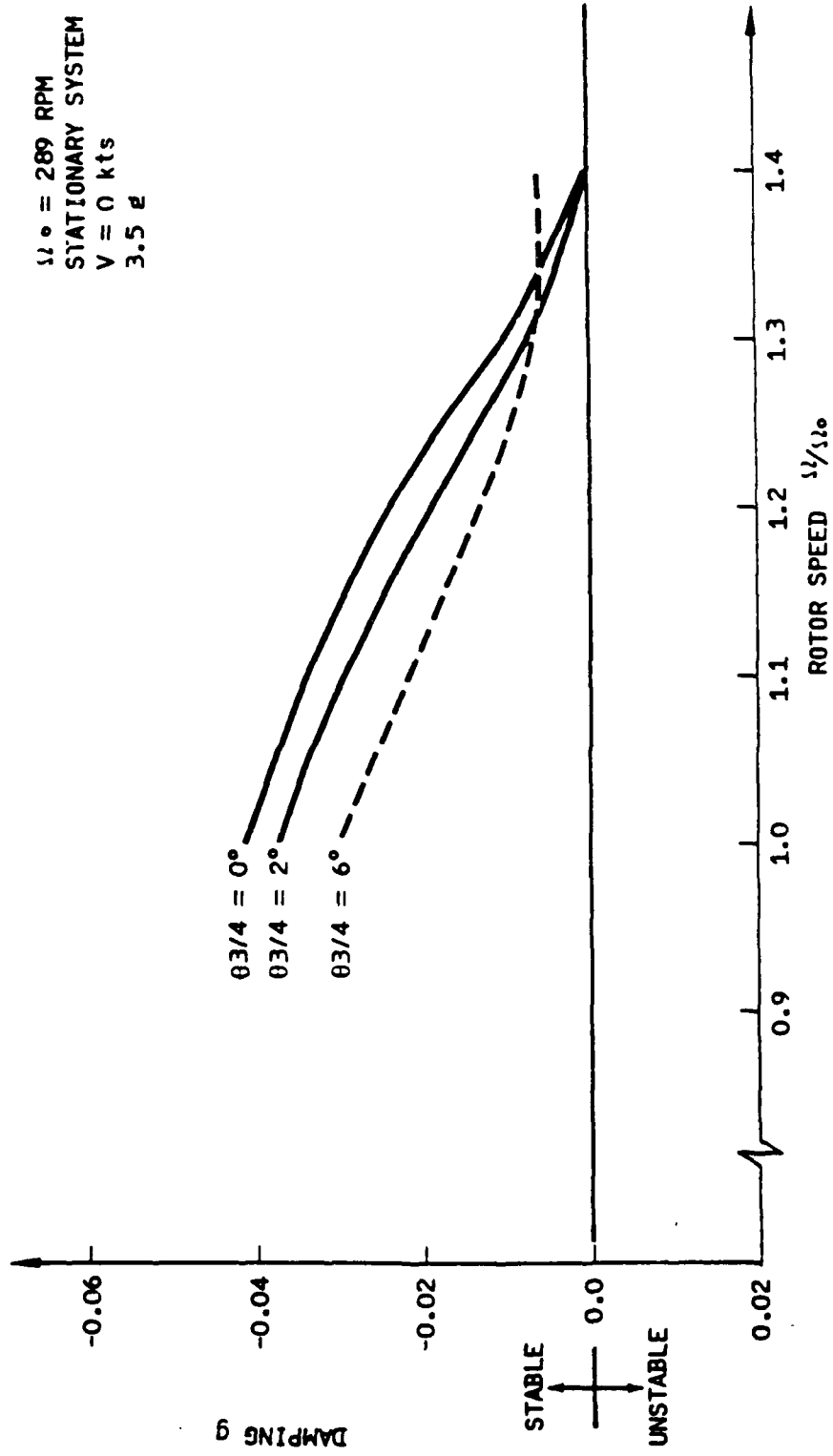


Figure J-4. Advancing whirl mode damping.

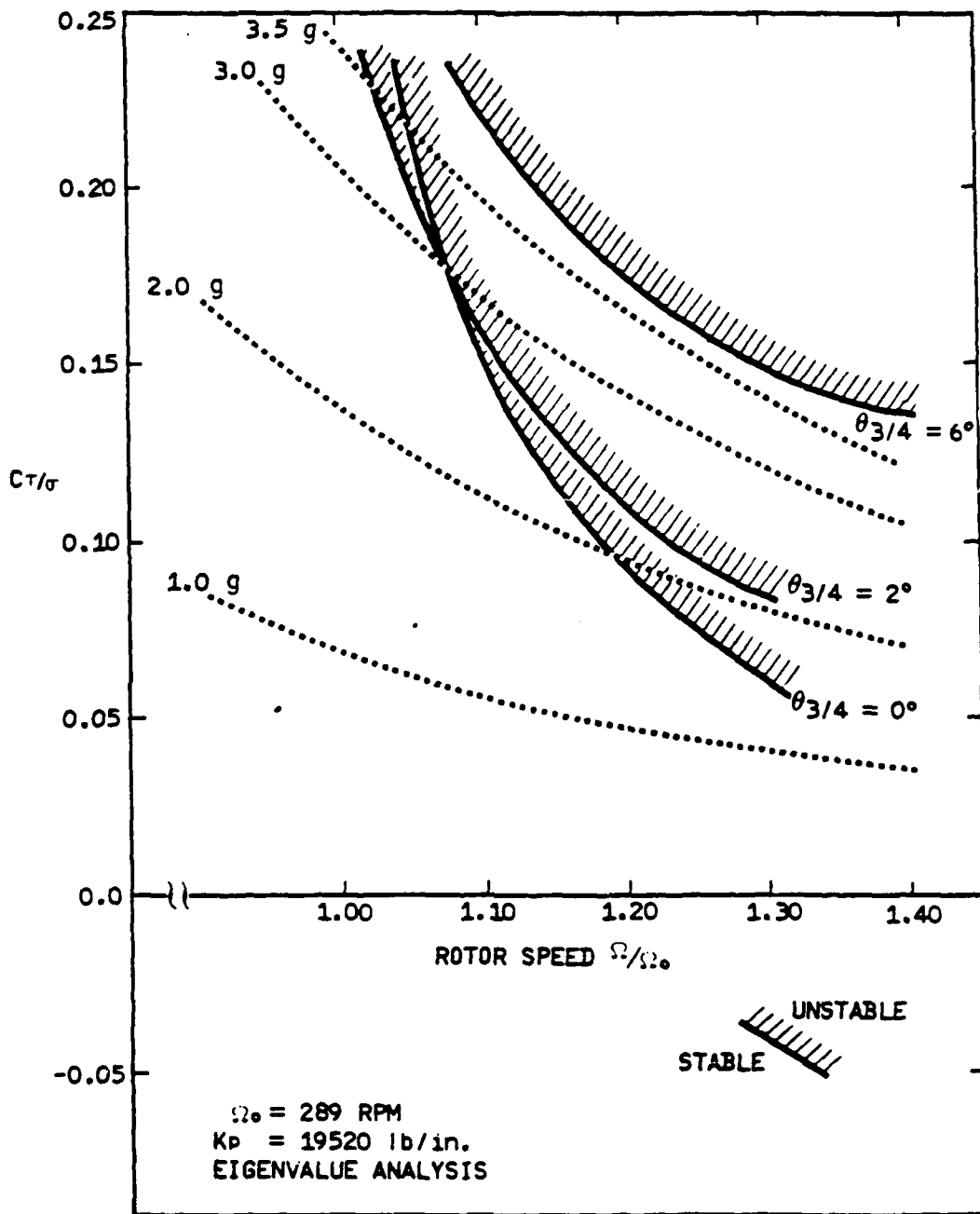


Figure J-5. CMRB advancing lag mode stability boundaries.

blade. Reference J-1 shows that the linear eigenvalue analysis is conservative compared to the four blade transient analysis.

A transient analysis was run for the most severe advancing lag mode case ( $\theta_{3/4} = 0$  degree,  $N_z = 3.5g$ , 376 rpm). An initial chordwise excitation was applied to one of the blades and the decay of the mast bending response was measured to calculate damping. The results shown in Figure J-6 indicate that the condition is stable with a modal damping of  $g = -0.033$ . It is, therefore, concluded that the advancing lag mode stability boundary is greater than 130 percent  $N_R$ .

For the mechanical instability (ground resonance) analysis of the AH-64A with the composite main rotor blades, the most important parameter is the blade first moment about the lag hinge. As shown in Table J-4, both the blade weight and first moment are less for the CMRB than for the metal main rotor blade. Since the lead-lag dampers and airframe are unchanged for the CMRB, the reduced blade first moment will give increased ground resonance stability margins. Therefore, the AH-64A with composite main rotor blades should have at least as good ground resonance stability as that demonstrated with the metal blades.

In summary, the advancing whirl mode stability boundary is above 130 percent  $N_R$  for all load factors and collective pitch settings, the advancing lag mode stability boundary is above 130 percent  $N_R$ , there are no flutter or divergence limitations within the operating spectrum of  $N_{DL}$  (130 percent  $N_R$ ) and 115 percent of  $V_{DL}$ , and mechanical stability margins are similar to those of the AH-64A with the metal blades. With respect to the torsional stability of the main rotor drive system, the only difference in the system with the CMRB installed from that with the metal blade installed is a minor reduction in rotor inertia from 0.829 slug-feet<sup>2</sup> for the metal blades to 0.783 slug-feet<sup>2</sup> for the CMRB. Hence, both systems are anticipated to perform similarly.

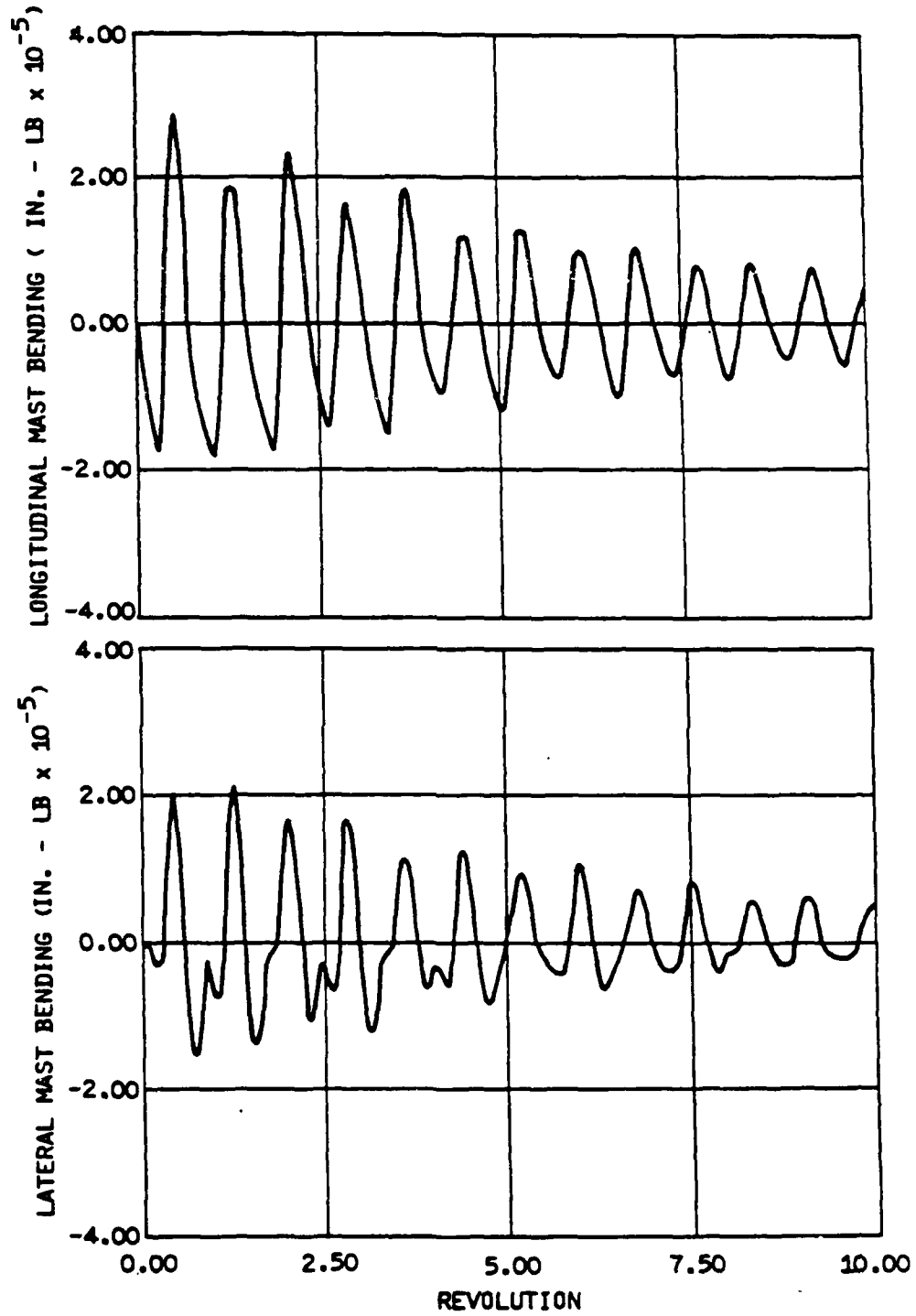


Figure J-6. Main rotor mast bending  
 $N_z = 3.5g$ ,  $\theta_{3/4} = 0$  degree,  
 376 rpm.

TABLE J-4. MAIN ROTOR BLADE WEIGHT AND MOMENT COMPARISON

	Metal Blade	CMRB	% Change
Weight (lb)	154.3	147.3	-4.5
$\sigma_{\xi}^*$ (in-lb)	18,980	17,940	-5.5
$I_i$ (slug-ft <sup>2</sup> )**	1,017	993	-2.4

\* $\sigma_{\xi}$  = Blade first moment about the lag hinge (r = 34.5 inches)

\*\* $I_i$  = Rotor blade polar moment of inertia about rotor shaft

APPENDIX K  
RELIABILITY ASSESSMENT

K-2



Reliability assessment of the CMRB is based on a Failure Modes, Effects, and Criticality Analysis (FMECA) that considers degradation of reliability that may occur during subassembly manufacturing processes, final blade assembly manufacturing processes, and in-service operations. The types of defects contributing to reliability degradation, the effects on blade and air vehicle performance (as determined by the FMECA), and compensating provisions wherein these defects can or are being ameliorated are discussed below.

The significant contributors to reliability degradation are hazards induced during air vehicle operation and maintenance, including thermal cycling, shock, vibration, aircraft fluids, rotor downwash (induced airborne particles and foreign object damage), rocket debris, rough handling, impact with terrain objects, maintenance, and contact with work stands and ground vehicles. Design allowables tend to compensate for some of these hazards and the resultant degradation may be readily visible. However, the resultant degradation due to those hazards, but not readily visible, can only be determined by an effect and adequate nondestructive evaluation or nondestructive test technique. Based on results of previous testing and for equivalent material thickness, the order of damage tolerance is as follows. Kevlar is the most damage tolerant, graphite is much less damage tolerant, and fiberglass is intermediate. Sandwich construction has poorer impact resistance than monolithic constructions and tends to suffer reductions in strength due to subsurface damage.

Being made primarily of advanced composite materials, corrosion as a failure mode will be essentially non-existent for the CMRB. Of the metal parts that could be subject to corrosion, the 304 CRES tip weight is passivated, the A356-T6 aluminum aft tip weight and 6061 T4 aluminum adjustable weights are chromic acid anodized, tungsten adjustable weights are etched and primed, 17-4 PH bushings and forward tip weight are passivated, and the 316 CRES balance rods are wiped with MEK prior to being embedded in the epoxy matrix.

Delamination of the Kevlar plies can occur during in-service operations resulting in loss of blade performance and possible excessive vibration. The FMECA has determined that 20 percent of the failure rate is attributed to delamination with resulting reliability degradation. These delaminations can be detected using non-destructive inspection techniques.

While porosity or voids within the elements themselves should not occur because rigid inspection techniques would have discovered them prior to assembly, porosity or voids can occur between any of the blade components

during the temperature-pressure curing process. Porosity or voids contribute approximately 4 percent to the total failure rate of the CMRB, according to the FMECA. The remoteness of their occurrence is based on the nondestructive inspection (NDI) and/or nondestructive evaluation (NDE) techniques used on the CMRB after its initial molding, or after in-service repair.

Resin-starved areas result in delamination as well as an upset of the fiber/resin density ratio. Resin-rich areas result in an upset of the desired fiber/resin density ratio. Both resin-starved or resin-rich areas can contribute to blade imbalance and loss of effective blade performance. These conditions can only occur during manufacturing, not during in-service operations, and would be discovered during inprocess control. The resin-rich or resin-starved defect is not considered as a failure mode in the FMECA since it would be a failure mechanism (cause) of a delamination failure mode. Unbonded areas defects would be prevalent only during the final manufacturing phase. Debonding can occur during the final manufacturing process as well as in-service operations. Reliability degradation caused by debonding results in degraded blade performance and excessive blade vibration thus affecting air vehicle performance. Debonding represents about 20 percent of the failure rate as determined by the FMECA. Bond line consistency will prevent debonding during in-service operations.

Rain erosion and ultraviolet (UV) radiation contribute greatly to environmental degradation of CMRB reliability. Sand and dust can be classified as FOD-induced erosion, as in maintenance-induced damage due to tool marks or tool drops. A leading edge erosion strip tends to protect against erosion. All trimmed edges are capped to prevent water absorption. The blade is painted with an epoxy primer and a urethane top coat to preclude degradation of the Kevlar and epoxy from UV radiation.

Three areas of the blade that are candidates for repair are the leading edge, the multitubular spar area, and the aft portion of the blade. The root end region is considered to be not repairable. The thermoplastic elastomer (Estane) leading edge erosion material may be repaired on the helicopter by:

- Repair local pitting
  - Cut away and repair local area
  - Remove entirely, and bond on new Estane strip
- } use kit furnished by manufacturer

The repair technique for the multitubular spar area is anticipated to include trimming away damaged material, scarfing the blade skin around the hole, emplacing spar tube repair segments, applying a 0-degree longo/ $\pm 45$ -degree composite skin patch, bonding the patch in place with heat and pressure, and sanding and painting the area. The repair technique for the aft portion of the blade will be to trim away the damaged skin and underlying honeycomb. A small repair area will be filled with glass milled fiber/epoxy paste - a piece of honeycomb will be cut to fit and bonded into larger damaged areas. The procedure for patching and the skill required will be similar to that for the spar area. Tip weight adjustment may be required to compensate for the location and weight of the repair patches.

HHI plans to estimate the damage that can be safely repaired and then define the skin, longo, and spar repair materials and adhesives that are necessary to perform the repair. HHI plans to select one CMRB, make a repair to it in each of the two zones, and subject the blade to a midspan fatigue test to evaluate the effectiveness of the repair during the full qualification effort.

A failure reporting system based on the Army-developed RAM/LOG (Reliability Availability Maintainability/Logistics) data collection methodology (AMSAV-L form 1249, 1250, 1252, 1266) will be instituted with the beginning of flight test. These forms will be used to record all failures that occur during the test program. Then a qualitative reliability assessment will be made based on the data that results. This assessment will then be evaluated against the comparative reliability value of the metal blade that is currently used on the AH-64A flight vehicles.

APPENDIX L  
MAINTAINABILITY ASSESSMENT



The Maintainability Engineering Analysis (MEA) for the CMRB addressed all the failure modes and effects data that are reported in the Reliability Assessment section as representing unscheduled maintenance items. The scheduled maintenance part of this MEA includes both daily and phased inspection. Phased inspection includes routine preparatory cleaning and selected preventive maintenance tasks. This MEA for Aviation Unit Maintenance (AVUM), Aviation Intermediate Maintenance (AVIM), and Depot Maintenance (DEPOT) predicts maintenance man-hours per flight hour as listed in Table L-1.

The repair limits and maintenance organization levels that are listed in Table L-2 are based on design criteria and stress evaluations. The repair level is considered to be very conservative inasmuch as many of the minor damage listings could be downgraded to the next lower maintenance level from AVIM to AVUM. In fact, because of the slow damage propagation rates of the CMRB, many repairs could receive temporary AVUM repairs and be operated for an additional 10 hours, or until a scheduled preventative maintenance check.

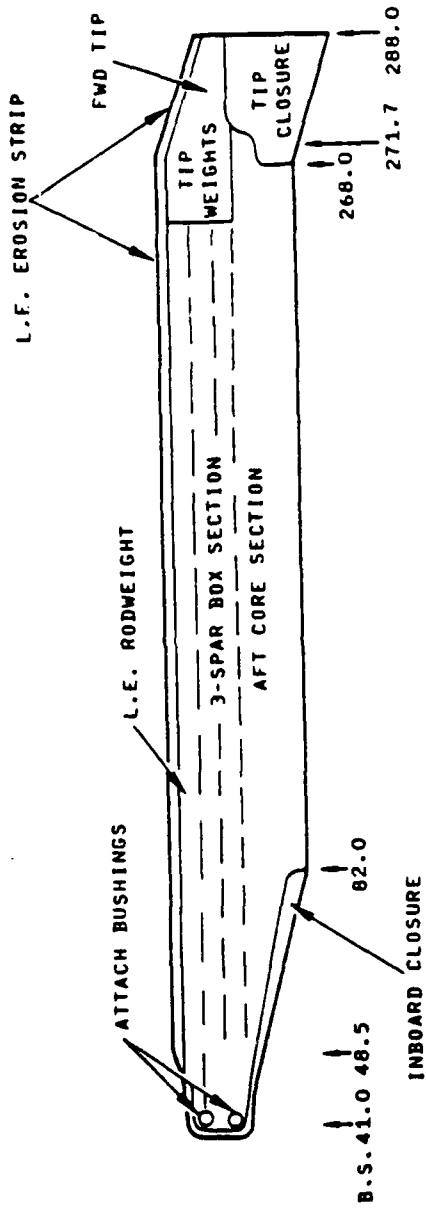
The repair procedures that are outlined in Table L-3 address the major and minor damage listed in Table L-2. While HHI's Maintainability Engineers consider these repair procedures to be within the current State-of-the-Art, it is realized that the aerospace industry is putting increased emphasis on composite structures and their repair causing the current state-of-the-art to change significantly.

As new technology becomes available, it will be incorporated into the repair procedure. During the CMRB production program it is planned to further refine the depot level repair procedures.

TABLE L-1. MAINTENANCE MAN-HOURS/FLIGHT HOUR

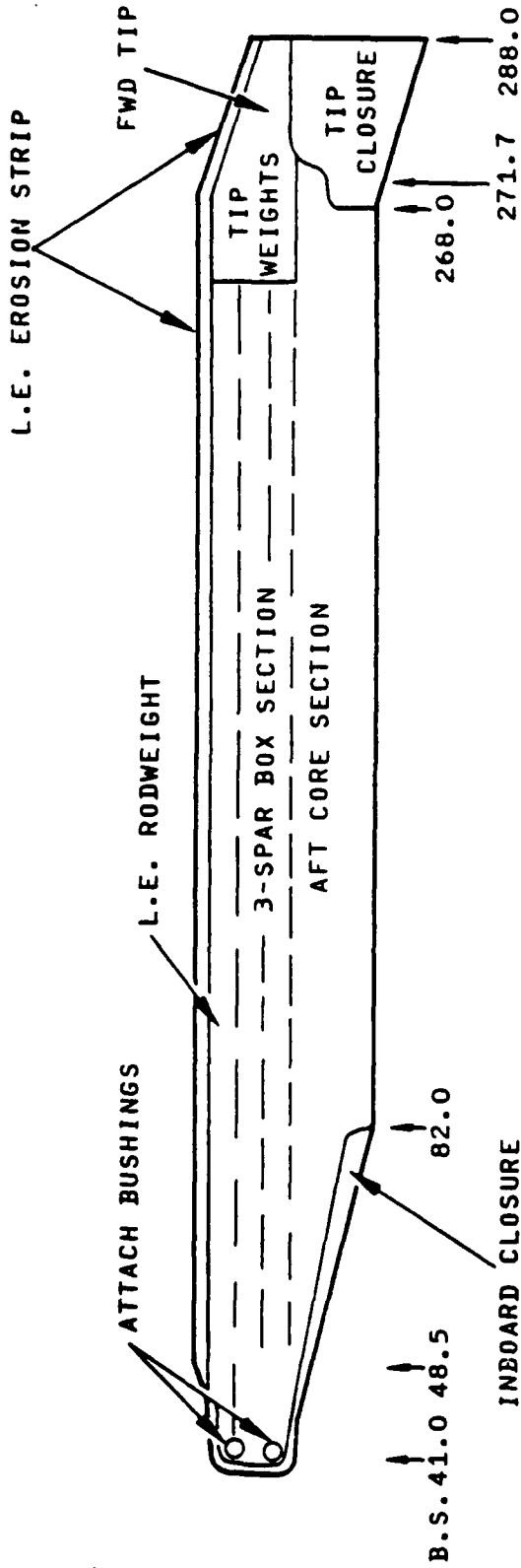
Level	Scheduled	Unscheduled	Total
AVUM	0.00898	0.0200	0.02898
AVIM	0.01473	0.0125	0.02723
DEPOT	0.00697	-	0.00697
	<u>0.03068</u>	<u>0.0325</u>	<u>0.06318</u>

TABLE L-2. CMRB DAMAGE LIMITS AND MAINTENANCE LEVELS



Repair Area	Minor Damage	Limit	Repair Level	Major Damage	Limit	Repair Level
L.F. Erosion Strip	Cuts, nicks, missing	4 in	AVUM	More than 4 in	None	AVIM
L. Edge Back Strip	Cuts, nicks	4 in	AVUM	More than 4 in	34 in	AVIM
L. Edge Rod Weight	Cut thru	4 Rods	AVIM	4 in to . in	7 in	AVIM
L. Edge Debonding	Crack - 3 in	4 in	AVIM	More than 4 in	-	DEPOT
Attach Bushings	Scratches	None	AVUM	Loose/cracked	-	DEPOT
BS 37.5 to 48	Nicks, finish	None	AVUM	Cracks/Debond	TBD	DEPOT
Inboard Closure	Debond/Delam	6 in	AVIM	Replace	None	AVIM
Spar Box 1, 2, 3: BS 49 to 271	Debond/Delam/Hole	1 in	AVIM	Cracks	1 Spar/1.5 in	AVIM
Aft Core Section	Debond/Delam	1 in	AVIM	Holes/Damage	4 in x 10 in long	AVIM
Trail Edge	Debond/Delam	6 in	AVUM	24 in - 48 in	60 in	AVIM
Hinge Tab	Cracked	1 Section 11.3 in	AVIM	To 8 Sections	None	AVIM
Tip Weight Area	None	-	-	Loose Stationary	-	DEPOT
Tip Weight Area	Loose Adj Wgts	-	AVUM	-	-	-
Forward Tip	Erosion	Minor	AVIM	Major	-	AVIM
Forward Tip	Hole/Delam	4 sq in	AVIM	Remove & Replace	-	DEPOT
Tip Closure	Hole/Delam	12.25 sq in	AVIM	Remove & Replace	-	DEPOT

TABLE L-3. CMRB REPAIR PROCEDURES



Area	Damage	Repair
L. E. Polyurethane Erosion Strip	<p>Minor cuts, nicks, 4 inches of strip missing.</p> <p>Major - More than 4 inches of strip missing.</p>	<p>Clean area, remove loose/frayed strip material. Fill with material from repair kit. Clean adhesive from area where erosion strip was removed, radius corners, prepare patch from like material, fit with minimum E. Dist. Bond in place and fill gaps from kit material.</p> <p>Remove loose or damaged erosion strip material. Clean adhesive, repair any backstrip damage. Prepare and fit, bond in place, heat if required. Fill edge gaps with kit material.</p>



TABLE L-3. CMRB REPAIR PROCEDURES (CONT)

Area	Damage	Repair
L.E. Backstrip	<p>Minor - cuts, nicks</p> <p>Major backstrip eroded through or missing.</p>	<p>Sand nicks and fill with epoxy. Cure, sand to fair with adjacent material. Patch with erosion strip kit.</p> <p>Sand with 320 WD paper. Fair to undamaged material. Lay in repair cloth. Epoxy, cure, sand smooth, and fair. Prepare erosion strip to overlap, repair ends 3 inches and bond in place. Fill butt end with kit material.</p>
L.E. Rodweight	<p>Minor - 4 rods cut through (TR)*</p> <p>Major - Same procedure</p>	<p>Remove erosion strip 4 inches past damage, remove backstrip 1 inch past damage, radius damage, fill with epoxy material EA 960 filler, cure and blend. Cover area with backstrip Kevlar 49 material and bond using adhesive EA 934NA cure, blend, and install erosion strip using adhesive A1503B1A1343B Estane cement and accelerator, fill edge gaps with kit material.</p>
L.E. Edge	<p>Minor - 3 inch crack. (TR)*</p> <p>Major</p>	<p>Clean air dry fill crack with EA 934NA and use.</p> <p>Depot specialized repair scrap potential 80 percent.</p>

\*(TR) designates temporary repair - permanent repair may be delayed up to 10 flight hours.

TABLE L-3. CMRB REPAIR PROCEDURES (CONT)

Area	Damage	Repair
Attach Bushings	Minor scratches	Polish and measure for limits using inside measuring micrometer.
ST 37.5 to 48	Major fretted, cracked loose	Depot - specialized repair part.
	Minor - scratches, nicks	Blend and refinish.
Inboard Closure	Major - cracks delamination	Depot specialized repair scrap rate 85 percent
	Minor - debonded/delam	Rebond using EA 934NA. Standard practices apply. Remove with router. Bond repair part in place with EA 934NA, fill and blend, refinish
Spar Box No. 1, 2, 3 STA 49 to 271	Major - TE crushed	Drill hole to accommodate hypo needle and fill void with EA 934NA. Apply pressure to surface to squeeze out excess adhesive. Apply pressure and heat as required. Accomplish flush plug patch using EA 934NA. Standard practices apply.
	Minor - debond/delam 1 inch hole	Rout damage only. Apply patch of Kevlar 49 with EA 934NA (Maintain filament direction), cover damage only may be expanded to 2.5 inches (No spar, no doubler damage).
	Major cracked outer cover, doubler 1.5 inch limit/spar only	

TABLE L-3. CMRB REPAIR PROCEDURES (CONT)

Area	Damage	Repair
Aft Core Section	Minor - one face sheet debonded 6 inches	<p>Rout out debonded face sheet as required until bonded core/sheet is established. Prepare Kevlar sheet stock, fit and clean. Apply EA 934NA to both sheet and core contact surface. Install. Apply pressure and heat if required, blend surface. Remove finish to allow for 3 inch doubler patch overlap. Doubler patch of same materials and adhesive. Apply lightning mesh with 0.5 inch overlap. Apply doubler over top, apply poly sheet to insulate pressure pad, apply pressure pads, apply heat if required - cure - remove heat, pressure pads, poly sheet - blend as required and refinish.</p>
Aft Core Section	Major - holes through or damage to core and both face sheets.	<p>Rout out damage from both face plates, rout out damaged core, cut replacement core. Clamp flush face plate and doubler in place. Install core (dry) and rout contour. Fit top plate, check contours, and cut lightning mesh, disassemble, and clean. Apply EA 934NA to all contact surfaces and assemble. Apply filler, poly sheet, and pressure pads, remove poly sheet. Blend as required and refinish. Direction filaments apply.</p>

TABLE L-3. CMRB REPAIR PROCEDURES (CONT)

Area	Damage	Repair
Trailing Edge	<p>Minor - delamination (TR)*</p> <p>Major - delamination extended 60 inches, crushed trail edge</p>	<p>Air clean, inject EA 934NA. Apply poly sheet. Apply clamp blocks and clamp, cure, remove clamps, blocks, and sheet. Sand to blend and refinish.</p> <p>Same as above. Rout out damage, scarf repair longo 5-to-1 at both ends. Scarf longo at undamaged ends. Apply adhesive and install. Fabricate core and face sheets. Fabricate doublers, cut lightning mesh. Assemble dry for fit check. Apply adhesive EA 932NA to all contact surfaces. Assemble, apply poly sheet, apply pressure and heat if required. Cure - remove heat, remove pressure and poly sheet. Apply filler EA 960F, cure, sand to blend, and refinish.</p>
Hinge Tab	<p>Minor crack or damaged to 11.3 inches</p>	<p>The hinge tab is a repair part and is provided in section lengths of 11.3 inches. Repair applies to both major and minor.</p>

\*(TR) designates temporary repair - permanent repair may be delayed up to 10 flight hours.

TABLE L-3. CMRB REPAIR PROCEDURES (CONT)

Area	Damage	Repair
	Major - 8 sections or 90 inch replacement	Rout damaged tab sections to remove, being careful not to remove material from trailing edge. Clean surface and bond repair in place, block, and clamp. Heat if required. Remove clamps and blocks, clean, and blend overrun. Bend tab using special tool to original setting and refinish.
Tip Weight Area	Major - loose stationary weights	Depot action only.
Tip Weight	Minor - loose adjustment weights	Tighten mounting and adjusting bolts.
Forward Tip	Minor - erosion	Fill pits with EA 960F, sand smooth with 320 WD, and refinish.
Forward Tip	Major - delamination	Air clean - apply EA 934NA and pressure bond cure - remove pressure pads, clean and refinish.
	Hole to 40 sq in	Rout out damage, fill void with foam, patch with Kevlar 49 and EA 934NH, fair with EA 960F, and blend - refinish.
Aft Tip Closure	Minor - delamination Hole to 12.25 sq in (TR)*	Same as repair No. 9.

\*(TR) designates temporary repair - permanent repair may be delayed up to 10 flight hours.

Because of its high safety factor and slow damage propagation rate, the CMRB is able to withstand minor damage while remaining serviceable. However, a temporary repair that is essentially cosmetic will keep out dirt and moisture and retain the necessary aerodynamic shape until it is convenient to make a permanent repair. Repair man-hours for those items listed as minor are estimated to require 1.6 to 2.4 man-hours plus cure time of 2 hours at ambient temperature of 77°F, or 30 minutes with supplemental heat. Major damage repairs at the AVIM level are estimated to require an average of 7 man-hours. In addition, the cure times given above must be added.

Depot level repairs were not estimated and will require specific engineering for custom repair designs.

APPENDIX M

REFERENCES

M-2



- I-1. Military Standard - Weight and Balance Data Reporting Forms for Aircraft (Including Rotorcraft), MIL-STD-1347A Part II, 30 September 1977.
  
- J-1. Silverthorn, L. J. , Childers, H. M. , and Neff, J. R. , Preliminary Aeroelasticity and Mechanical Stability Report YAH-64 Advanced Attack Helicopter, Hughes Helicopters, Inc. Report No. 77-X-8001, June 1976.

APPENDIX N

DRAWING LIST FOR THE COMPOSITE  
MAIN ROTOR BLADE FOR THE  
AH-64A HELICOPTER

N-2

Drawing Number	Revision	Title
7-311412500	R	Blade
7-311412508	D	Blade Ordinates
7-311412509	A	Lines Definition
7-311412511	M	Closure, Inboard
7-311412512	E	Door
7-311412514	D	Weight
7-311412515	C	Bolt
7-311412516	E	Erosion Strip
7-311412517	F	Bracket Assembly
7-311412530	G	Weight Assembly
7-311412531	C	Spar Tube No. 1
7-311412532	B	Spar Tube No. 2
7-311412533	C	Spar Tube No. 3
7-311412536	J	Longo, T. E.
7-311412537	L	Cap Assembly
7-311412538	H	Doubler Assembly, Skin
7-311412539	E	Doubler, Cap
7-311412541	F	Wedge, Inboard
7-311412542	K	Wedge, Spar Cap
7-311412543	H	Core Assembly, Tip
7-311412545	D	Skin
7-311412546	G	De-icer Blanket
7-311412547	E	Lightning Screen
7-311412548	J	Weight, Forward, Tip
7-311412549	K	Weight, Aft, Tip
7-311412550	B	Tip Weight, Leading Edge

Drawing Number	Revision	Title
7-311412551	-	Rod
7-311412553	A	Backing Strip
7-311412554	-	Backing Strip, Tip
7-311412556	C	Bracket Assembly
7-300412557	G	Root End Dam
7-311412559	A	Cap, Leading Edge
7-311412561	E	Hinge, Trim Tab
7-311412563	G	Plate, Face
7-311412567	F	Plate Clevis
7-311412568	B	Bushing
7-311412569	C	Inner Skin
7-311412570	A	Absorber Assembly
7-311412572	D	Core, Aft
7-311412573	D	Channel
7-311412574	G	Core Assembly, Aft
7-311412575	B	Filler Doubler
7-311412576	C	Closure, Outboard
7-311412577	-	Strip, Fairing
7-311412581	B	Target Set