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A Wind Dependent Desert Aerosol Model: Radiative Properties

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OptiMetrics, Inc. 50 Mall Road Burlington, MA 01803

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This report presents a desert	aerosol model that predicts aerosol		
radiative properties during backgrou	and and severe dust storm conditions.		
The model treats the desert aerosol	as an external mixture of natural		
Darticles, pure quartz and guartz (contaminated with a small amount of		
hematite. Mie calculations are per	rformed using different size distri-		
butions and indices of refraction f	for each type of particle, and then a		
volume-weighting scheme is used to	obtain the radiative properties of the		
aerosol as a whole.	Micro		
Attenuation coefficients, sinc	gle scattering albedo and asymmetry		
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19. Abstract (cont.)

Also, hematite in the sand particles leads to selective absorption at visible wavelengths, which becomes more pronounced as the wind speed-increases.

The radiative properties of the present model are then compared with other desert aerosol formulations. The comparisons suggest that the absorption at wavelengths between about 0.6 and 2.0 μ m is less than that calculated by previous models.

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1. INTRODUCTION

Aerosols can be found throughout the atmosphere. They can have a role in cloud formation and precipitation processes and plus they can have an impact on the radiation balance of the earth-atmosphere system. The radiative impact will depend on the size, shape and composition of the aerosols, as well as their spatial distribution in the atmosphere and the nature of the underlying surface.

Aerosols can be separated into a set of generic categories based primarily on their (spatial) location in the atmouphere. Each aerosol "type" has its own characteristic optical properties that distinguish it from other aerosols. For most merosol types, a set of parameters exist for calculating aerosol radiative properties with reasonable accuracy.

An important aerosol type is the desert aerosol which is representative of arid and semi-arid regions. This catagory has been added because about one-third of the earth's land surface area consists of arid and semi-arid terrain and because the radiative effects of desert aerosols are important during dust storm conditions. In addition, the source regions of desert aerosols have high solar insolation and strong convective processes that enable the particles to be lifted to altitudes where synoptic-scale air motions can transport the particles well beyond their source regions.

A tentative desert aerosol model was developed¹ for use in the Air Force Geophysics Laboratory (AFGL) model atmospheres. This model was based primitily on recommendations from a meeting of experts conducted by the World Climate Research Programme². It is the purpose of the prest t study to examine the features of that formulation and to present improvements to it.

1.1 Organization of Report

Chapter 2 reviews the literature pertaining to the physical properties of desert aerosols. Chapter 3 presents a model that can be used to calculate desert aerosol radiative properties. Chapter 4 discusses the implications of the new desert aerosol model and compares it against observed data and models used by other researchers. Finally, Chapter 5 summarizes our results.

Shettle, E. P. (1984) Optical and radiative properties of a desert aerosol model, <u>IRS '84: Current Problems in At-</u> <u>mospheric Radiation</u>, G. Flocco, Ed., A. Deepak Publishing, Hampton, VA, 74-77.

World Climate Research Programme (1983) <u>Report of the Experts Meeting on Aerosols and Their Climatic Effects</u>, Deepak, A., and H. E. Gerber, eds. World Climate Program Publication WCP-55, December 1983.

2. PHYSICAL PROPERTIES OF DESERT AEROSOLS

The desert aerosol model that has been recommended by the World Climate Research Programme² and utilized by Shettle¹ is based on a limited data set. The formulation uses data that were obtained primarily in the Middle East, although measurements from other arid and desert locations have been included. Table 1 provides a partial listing of measurements³⁻¹³ that

- d'Almeida, G. and Schutz, L. (1983) Number, mass and volume distributions of mineral aerosol and soils of the Sahara, J. Climate and Appl. Meteor., 22:233-243.
- Patterson, E. M. and Gillette, D. A. (1977) Commonalities in measured size distributions for aerosols having a soil-derived component, J. Geophys. Res., 82:2074-2082.
- 5. Schutz, L. and Jaenicke, R. (1974) Particle number and mass distributions above 10⁻⁴ cm radius in sand and aerosols of the Sahara Desert, <u>J. Appl. Meteor.</u>, <u>13</u>:863-870.
- Levin, Z. and Lindberg, J. D. (1979) Size distribution, chemical composition, and optical properties of urban and desert acrosols in Israel, <u>J. Geophys. Res.</u>, 84:6941-6950.
- Kushelevsky, A., Shani G. and Haccoun A. (1983) Effect of meteorologic conditions on total suspended particulate (TSP) levels and elemental concentration of aerosols in a semi-arid zone (Beer-Sheva, Israel), <u>Tellus</u>, <u>35B</u>:55-64.
- Cahill, T. A., Kusko, B. H., Ashbaugh, L. L., Barone, J. B., Eldred, R. A. and Walther, F. G. (1981) Regional and local determinations of particulate matter and visibility in the southwestern United States during June and July, 1979, <u>Atmospheric Environment</u>, <u>15</u>:2011-2016.
- 9. Annegarn, H. J., Van Greiken, R. E., Bibby, D. M. and Von Blottnitz, F (1983) Background aerosol composition in the Namib Desert, south west Africa (Namibia), <u>Atmospheric</u> <u>Environment</u>, <u>17</u>:2045-2053.
- 10. Pinnick, R. G., Jennings, S. G and Fernandez, G. (1987) Volatility of aerosols in the arid southwestern United States, J. Atmos. Sci., 44:562-576.
- 11. Levin, Z., Joseph, J. H. and Mekler, Y (1980) Properties of Sharav (Khamsin) Dust - Comparison of optical and direct sampling data, J. Atmos. Sci., 37:882-891.

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relate to the physical properties of aerosols in arid or desert environments.

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Table 1. Summary of Measurements of Aerosols from Arid or Semi-arid Environments

LOCATION	PERIOD OF MEASUREMENTS	4EASUREMENT Type	REFERENCE	
Central Sahara	Feb 1979 - Feb 1982	5D	d'Almeida and Schutz ³	
Haswell, Colorado	Unknowņ	8 D	Patterson and Gillette ⁴	
Plains, Texas	Unknown	SD	Patterson and Gillette ⁴	
Camp Derj and Sebha, Libya	Unknown	вD	Schutz and Jaenicke ⁵	
Mitzpe Penon (Negev Desert), Israel	Winter and Early Spring 1976	4 80, RAD Comp	tevin and Lindberg ⁶	
Beer-Sheva, Israel	June 1977 - May 1978	Comp, THL	Kushelevsky et al. ⁷	
Arizona and Utah	June + July 1979	Comp. TML	Cahill et al. ⁸	
Namib Desert	Nov 1976 - April 1977	Comp	Annegarn et ml. ⁹	
Tularosa Basin, NM	Aug 1984 - Aug 1985	Comp, SD	Pinnick et al. 10	
Mitzpe Ramon (Negev Desert), Israel	Dust Scorm on 6 June 1977	SD, HAD	Levin et al. ¹¹	
Grand Canyon, Arizona	Dec 1979 - Nov 1981	TML, RAD	Malm and Johnson ¹²	
Iran and Pakistan	Unknown	RAD	Ottorman et al. 13	

Rey: SD - Size Distributions, Comp - Composition, RAD - Radiative Measurements TML - Total Mass Loadings

12. Malm, W. C. and Johnson, C. E. (1984) Optical characteristics of fine and coarse particulates at Grand Canyon, Arizona, <u>Atmospheric Environment</u>, <u>18</u>:1231-1237.

13. Otterman, J., Fraser, R. S., and Bahethi, O. P. (1982) Characterization of tropospheric desert aerosols at solar wavelengths by multispectral radiometry from Landsat, J. Geophys. Res., 87:1270-1278.

2.1 Source Regions and Transport Characteristics

Desert aerosols have been measured at great distances from their source regions. Saharan aerosols have been measured well into the tropical North Atlantic^{14,15} and in Mediterranean countries^{16,17,18}. Desert aerosols originating from Asian deserts have been measured in the Hawaiian Islands¹⁹. The bulk aerosols in the lower few kilometers of the troposphere over the tropical North Atlantic consist primarily of sea-salt aerosols and mineral aerosols originating from the arid and semi-arid regions of West Africa¹⁴.

These measurements indicate that the aerosols at a given location are not necessarily representative of the underlying soils. d'Almeida and Schutz³ have shown from their data of soil samples and aerosol samples from across the Sahara that the aerosols are largely made up of crustal material that are representative of loose and finely grained soils. They state

- 14. Junge, C. and Jaenicke, R. (1971) New results in background aerosols studies from the Atlantic expedition of the R. V. <u>Meteor</u>, Spring 1969, <u>Aerosol Science</u>, 2:305-314.
- 15. Savoie, D. L. and Prospero, J. M. (1977) Aerosol concentration statistics for the Northern Tropical Atlantic, J. Geophys. Res., 82:5954-5964.
- 16. Schmidt, M., Specht, H. and Fabian, P. (1978) Aerosol measurements at the Algarve Coast of Portugal, <u>Tellus</u>, 30:449-457.
- 17. Ganor, E. and Mamane, Y. (1982) Transport of Saharan dust across the Eastern Mediterranean, <u>Atmospheric Environ-</u> <u>ment</u>, <u>16</u>:581-587.
- Chester, R., Sharples, E. J., Sanders, G. S. and Saydam, A. C. (1984) Saharan dust incursion over the Tyrhenian Sea, <u>Atmospheric Environment</u>, 18:929-935.
- 19. Shaw, G. E. (1980) Transport of Asian desert aerosol to the Hawaiian Islands, <u>J. Appl. Meteor.</u>, <u>19</u>:1254-1259.

that wadis and floodplains near mountains offer probable production source areas for desert aerosols rather than dune-like deposits. These results are consistent with those of Chester et al.¹⁸ who performed an elemental analysis of aerosols from over the Tyrrhenian Sea. Their data indicated that the aerosols are characteristic of crystal material rather than from dune areas.

2.2 Size Distributions

Acrosol size distributions are often modeled by the sum of two or three log normal distributions,

$$\frac{dN(r)}{d\log r} = \sum_{i=1}^{2,3} \frac{N_i}{(2\pi)^{1/2}\log \sigma} \exp\left(-\frac{\left[\log(r/R_i)\right]^2}{2\left(\log \sigma_i\right)^2}\right)$$
(1)

where N(r) is the particle concentration for particles greater than a given radius r, N_i is the total number of particles for the distribution i, a_i is the geometric standard deviation and R_i is the geometric mean radius. The individual distributions are often meant to represent different size classifications that are representative of different production processes. Three size ranges², $10^{-7} < r < 10^{-5}$ cm, $10^{-5} < r < 10^{-4}$ cm and $r > 10^{-4}$, cm are typically used to describe aerosols in the atmosphere. The size ranges are referred to, respectively, as the Aitken or nucleation mode, the large or accumulation mode and the giant or coarse mode.

Based on an analysis of tropospheric aerosol measurements, Patterson and Gillette⁴ characterized the distributions with three modes that they referred to as (respectively), modes C, A and B. Mode C represents particles centered at about 0.02 - 0.5 µm and is representative of background aerosols. Mode A particles cover the radius range 1 - 10 µm and consist of particles produced from the parent soil by a sandblasting process. This component of the size distribution is determined by the lifting force of the local winds. Mode B particles peak at about 30 µm radius and are primarily found when the wind speed is high and the dustloading is significant. Under heavy dust loading conditions, Patterson and Gillette found that only modes A and B were present as a result of soil erosion and sandblasting plus the subsequent injection of this material into the atmosphere. These results suggest that different size distribution formulations were needed to describe background desert and duststorm conditions.

The size distributions used in the tentative AFGL desert aerosol model, which were based on recommendations from the World Climate Research Programme², are shown in Table 2.

Model.	i	N _i (cm ⁻³)	log (σ _i)	R _i (µm)
Background	1	997	0.328	0.0010
	2	842	0.505	0.0218
	3	7.10 × 10 ⁻⁴	0.277	6.24
Dust Storm	1	726	0.247	0.0010
	2	1,140	0.770	0.0188
	3	1.78 × 10 ⁻¹	0.438	10.8

Table 2. Parameters Used in the Background Desert and Desert Dust Storm Aerosol Models¹,²

These values are based primarily on measurements 14, 20, 21 from the Sahara. For calm (or background) conditions, the parameters are similar to those for "remote continental aerosols." The parameters for the dust storm conditions are based on the work of Schutz and Jaenicke⁵, Jaenicke and Schutz²⁰ and d'Almeida and Jaenicke²¹. The major difference between the model for background and dust storm conditions is in the number of large particles in mode 3, the component associated with large particles that are injected by high winds. Therefore, the values for the dust storm model represent extreme values and should be linked to wind velocity.

2.3 Composition

Compositional measurements indicate that desert aerosols are a mixture of different kinds of materials. Desert aerosols consist of a background component and a component representative of local soil sources. Depending upon location, desert aerosols can also have an anthropogenic component.

Simple visual examination of desert dust reveals many of the particles to have a light brown to tan appearance⁶ unlike urban aerosols that are generally gray or black. Elements commonly found in desert aerosols^{6,7,8,9,10} include sodium, calcium, silicon, aluminum and sulfur. Silicon, presumably in

^{20.} Jaenicke, R., and Schutz, L. (1978) A comprehensive study of physical and chemical properties of the surface aerosols in the Cape Verde Islands region, <u>J. Geophys.</u> <u>Res.</u>, 83:3583-3598.

^{21,} d'Almeida, G. A. and Jaenicke, R. (1981) The size distribution of mineral dust, <u>J. Aerosol Sci.</u>, <u>12</u>:160-162.

the form of quartz, and calcium, appear to be the most common elements in the desert $aerosol^{6,7}$. The five most common elements found by Kushelevsky et al.⁷ were calcium, silicon, sulfur, iron and chlorine. Calcium, silicon and iron are primarily crustal in nature while sulfur and chlorine can have both crustal and industrial sources. Chlorine can also be derived from sea spray⁹.

Particles with radii less than about 0.4 μ m appear to have a large ammonium sulfate and ammonium bisulfate component while larger particles have quartz, clay components and other elements associated with soil or crustal sources^{8,9,10,18}. Generally speaking, desert aerosols are not hygroscopic. The only exception to this is a "well aged" desert aerosol in which the background component has acted as a condensation nuclei as a result of numerous trips up and down through the desert atmosphere.

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Abundances of the elements can vary from sample to sample as a function of wind speed (i.e., increased mass loading) and wind direction (i.e., source region). Cahill et al.⁸ observed a seasonal variation in the amount of silicon particulate in samples collected in Arizona and Utah. Their results, which consisted of one year of data, indicated that for particles in the range 3.5 to 15 μ m, the silicon abundance increased to a maximum in the spring and then decreased to a minimum in the winter. Table 3, from Kushelevsky et al.⁷, summarizes how the abundances of these elements can vary on a day-to-day basis and when averaged over different meteorological conditions.

Carbon is generally found in very small abundances in desert aerosols. However, due to its strong absorption, a small increase in the carbon amount, as little as 1%, can lead to a large increase in the total absorption properties of desert aerosols.

Table J. Variation of Elemental Concentrations in Middle Eastern Desert Aerosols as (a) A Function of Source Region and (b) Averaged Over Meteorological Conditions. Measurements were made by Kushelevsky et al. at Beer-Sheva, Israel using Instrumental Neutron Activation Analysis and X-ray Flourescence

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WIND DIRECTION	HEAN WIND SPIRED (m m)	TOTAL BUSPENDED PARTICULATE (g m)	NOTES	Ca	elemental Ri	CONCENTRI	T10NB 70	(\$) c1
W-E	2.04	291		10	9	2	2	2
N-W	2.01	243		18	13	2	2	1
N-W	1.85	160		14	13	4	2	2
W- E	1.67	36	Rain	1	5	4	1	4
N'4-E	2,29	164	HAIN	9	11	3	2	2
W-SE	1,83	50	Rain	19	20	5	4	7
N-2	4,59	561 D	ust Storm	18	21	i	3	0.4
W+EW	2.00	610 D	ust Storm	17	18	1	2	1
W	2.73	1600 0	ust Storm	22	17	0,3	2	0.1
N- E	2.25	613	Sharav	15	14	1	2	1
E-SE-E	2,87	412	Sharav	17	2.1	1	3	1
W Variable	3.16	5080	Sharav	16	18	0.2	3	0.2

the

CONDITIONS	Ca B	limental 81	CONCENTR 8	ATIONS Pe	(4)
Norma 1	12.2	11.5	3.1	1.9	2.5
Hain	12.6	14.6	4.5	2.4	3.6
Dust Storm	16.8	18.0	0.6	2.4	0.5

Note: Sharav, or Khamsin, is a Dust Storm Characterised by Hot Winds from the North African Desert. It Typically Occurs During the Period Between Easter and Pentecost

2.4 Effects of Wind

Enormous amounts of clay and sand can be loaded into the desert atmosphere during windy conditions. During calm condi-

tions the desert aerosol resembles aerosols other than that which would be produced from the underlying soil. In particular, Patterson and Gillette⁴ have studied the composition of the desert aerosol in light, medium and heavy mass loading conditions and have found that particles having radii between 0.02 and 0.5 μ m were generally grey or black and represented the global background aerosol. Furthermore, these particles were always present in the same amount regardless of the amount of mass loading. Similar findings reported in the World Climate Programme² study confirmed that under very calm conditions the composition of the desert aerosol resembles that of a remote continental aerosol.

Local wind conditions provide the mechanism to inject and transport aerosols. Wind also provides a mechanism for the generation of additional aerosols via a sandblasting process. The amount of aerosol injection and generation depends upon factors such as wind speed^{22,23}, soil moisture, and the extent

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^{22.} Gillette, D. A., Blifford, Jr., I. H. and Fryrear, D. W. (1974) The influence of wind velocity on the size distributions of aerosols generated by the wind erosion of soils, J. Geophys. Res., 79:4068-4075.

^{23.} Gillette, D. A. (1978) Tests with a portable wind tunnel for determining wind erosion threshold velocities, <u>Atmo-</u> <u>spheric Environment</u>, <u>12</u>:2309-2313.

of vegetation²⁴, so⁴) texture and the amount of soil crust-ing²⁵.

Soil movement as a result of aerodynamic forces occurs for wind speeds above a given threshold value. This wind speed threshold will vary as a function of soil condition and on the amounts of nonerodible elements, such as rocks and pebbles, on top of the soil. Utilizing a portable wind tunnel, Gillette²³ examined the threshold velocities for three different kinds of soils, two types of desert soil and one farmland soil. A relatively smooth desert soil had a threshold velocity of 34.2 cm s⁻¹ while one with a pebble covering had a threshold velocity of 121.9 cm s⁻¹.

The size distribution of the aerosols that are injected into the air as a result of wind erosion has been found to be similar to that of the underlying soil²⁴.

2.5 Indices of Refraction

The index of refraction characterizes the optical properties of a particular material. It can be expressed as the complex number,

m = n + ik,

(2)

- 24. Gillette, D. A., Blifford, Jr., I. H. and Fenster, C. R. (1972) Measurements of aerosol size distributions and vertical fluxes of aerosols on land subject to wind erosion, <u>J. Appl. Meteor.</u>, <u>11</u>:977-987.
- 25. Gillette, D. A. (1978) A wind tunnel simulation of the erosion of soil: Effect of soil texture, sandblasting, wind speed, and soil consolidation on dust production, <u>Atmospheric Environment</u>, 12:1735-1743.

where n and k are related to the phase velocity and attenuation, respectively, of an electromagnetic wave as it passes through the material. In general, the index of refraction of a material will not be the same for all wavelengths of radiation.

2.5.1 An Assessment of the Available Measurement Techniques

Measuring the optical properties of any material is not a trivial job. Three techniques are commonly used to determine the index of refraction of aerosols: in situ measurements, laboratory measurements made on a compressed disk of the collected sample and KBr pellets and laboratory measurements of diffuse reflectance. The laboratory measurements usually involve collecting the aerosol on a filter and must avoid evaporation of volatile compounds and contamination from the admixture of other aerosols, such as clouds or gases.

2.5.1.1 In Situ Measurements

In situ measurements of particle size distribution and the angular dependence of scattering can be used to predict the optical properties of aerosols (Grams et al.²⁶). The index of refraction is then equal to the value, which when used in Mie calculations, replicates the observed scattering pattern. Unfortunately, this technique involves a few assumptions that may be risky. First, the particles are assumed to be spherical. This assumption is valid for some aerosols,

^{26.} Grams, G. W., Blifford, Jr., I. H., Gillette, D. A. and Russell, P. B. (1974) Complex index of refraction of airborne soil particles, J. Appl. Meteor., 13:459-471.

such as those found near oceans, but not for desert aerosols, especially fresh ones. A second point to keep in mind is that this technique may not be appropriate for materials in which scattering dominates over absorption. That is, small errors in the measured scattered intensity can lead to large errors in the inferred absorption²⁷. Finally, inaccurate representation of the particle size distribution, when used in the Mie calculations, can give rise to erroneous values for the imaginary index.

2.5.1.2 An Aerosol Sample Suspended in a KBr Disk

The optical constants of desert aerosols have been determined by Levin and Lindberg⁶ and by Volz²⁸ by compressing the particles into a disk with pellets of KBr and then measuring the reflectance and transmittance. Next these measurements are interposed with solutions to electromagnetic boundary value problems for plane surfaces to infer the optical properties of the aerosol. Unfortunately, it is sometimes difficult or questionable to determine the optical constants of desert aerosols using this technique. That is, the technique cannot be used for visible wavelengths because scattering dominates over absorption. Also, the underlying electromagnetic theories used to calculate the optical properties are only valid for homogeneous materials; however, the airborne desert

^{27.} Bohren, C. F., Private Communication.

Volz, F. E. (1973) Infrared optical constants of ammonium sulfate, Sahara dust, volcanic pumice and flyash, <u>Appl.</u> <u>Opt.</u>, 12:564-568.

aerosol is composed of discrete particles, each having its own composition.

2.5.1.3 Diffuse Reflection Techniques

The method of diffuse reflection involves mixing the aerosol with a barium sulfate powder and measuring the diffuse reflectance with a spectrophotometer. With these measurements and the diffuse reflectance of pure barium sulfate, the imaginary part of the index of refraction is then determined using the equations of the Kubelka-Munk theory of diffuse reflectance. This technique has been used by Patterson et al.²⁹ and by Levin and Lindberg⁶ to determine k of desert aerosols.

2.5.2 Reported Values of the Indices of Refraction for Desert Aerosols

2.5.2.1 Real Part

All available measurements report the n of desert aerosols to be between about 1.5 and 1.6 for visible wavelengths. These values are referred to rather casually because, for spheres at least, the specific choice of n will not significantly affect the absorption, scattering and extinction coefficients. In fact, some of the experimental techniques must assume a real index in order to determine the imaginary part.

Values for n approach a minimum in the 5 - 8 μ m region and a local maxima around 10 μ m and 25 μ m. These peaks of the real part roughly correspond to the peaks in the absorption.

^{29.} Patterson, E. M., Gillette, D. A. and Stockton, B. H. (1977) Complex index of refraction between 300 and 700 nm for Saharan aerosols, J. Geophys. Res., 82:3153-3160.

This is expected because the behavior of n is related to the **behavior of k**.

2.5.2.2 Imaginary Part

The measurements of k for desert aerosols are given in Figure 1 from Carlson and Benjamin³⁰. Most measurements, regardless of technique, place the imaginary index for visible wavelengths between about 0.001 and 0.04. Generally speaking, absorption is slightly less at red wavelengths than at blue wavelengths and reaches a minimum near 1.0 um. Unfortunately at many wavelengths in the visible, the various measurements of k are different from each other. These large descrepancies are a problem because when the different values are used in radiative transfer calculations, they can give rise to a wide range of values for the absorption of solar radiation.

The measurements of k suggest that it is quite variable in the infrared. The magnitude of k is smallest at the shorter IR wavelengths and reaches a local maxima at wavelengths within the 8 - 12 µm atmospheric window and around 20 µm. These peaks in the window region are due to the abcorption by quartz and the various clays present in the aerosol. Although most sets of measurements place the peaks near the same wavelengths, there are striking differences in the magnitudes of absorption.

^{30.} Carlson, T. N. and Benjamin, S. G. (1980) Radiative Heating Rates for Saharan Dust, J. Atmos. Sci., 37:193-213.



Figure 1. Values of the Imaginary Index of the Desert Aerosol Reported by Other Researchers (From Carlson and Benjamin³⁰). See Carlson and Benjamin³⁰ for the references cited in this figure

2.5.3 Concerns Over the Reported Values

It is generally agreed that the optical constants of desert aerosols reported in the literature probably represent average or effective values because the desert aerosol is an inhomogeneous material. The problem with using average values is that they do not accurately describe the radiative properties of desert aerosols. The radiative properties of any multicomponent material depend on how the components are mixed. In the case of desert acroscls, most of the absorption is due to the small, discrete carbon-based particles from the background global aerosol. The problem is that when the average indices of refraction are used in radiative transfer calculations, each particle is treated as though it has the same optical parameters, which is clearly not true. In high wind conditions when greater amounts of less absorbant, local dust and sand are lofted, the relative contributions of the highly absorbant carbon particles to the total radiative impact of the desert aerosols are lessened.

It is important to examine the consequences of using the values cited in the literature. Because the typical desert aerosol does contain a small amount of highly absorbing material, such as carbon or hematite, one would expect the values for k (in the visible), to be greater than those for pure quartz or various clays, which have values of k of about 10^{-6} . However, all of the values for k in Figure 1 are too high. To demonstrate this, let us calculate the "penetration depth" of a 0.55 µm wave as it passes through a single desert aerosol

particle. (This argument is taken from Bohren and Huffman³¹.) For the purposes of the argument, the penetration depth will be defined as the distance where the transmission through the particle T is reduced to 1%. A value of 1% transmission is chosen because it defines a particle as appearing black when placed in front of a light source. If reflection effects are ignored (which is a reasonable assumption), then the wave will be attenuated exponentially

$$\mathbf{T} = \exp(-\mathbf{a}\mathbf{z}) \tag{3}$$

where the absorption coefficient, a, equals $4\pi k/\lambda$. Solving this expression for z gives

$$z = -\ln(T)/(4\pi k/\lambda)$$
 (4)

Now, letting T = 0.01, k = 0.001, and $\lambda = 0.55 \mu m$, the resulting penetration depth is 200 μm . Desert aerosol particles with diameters of 200 μm are common in the desert atmosphere during dust storms, but our penetration depth calculation implies that the desert aerosol is black, which observations show not to be the case (See Section 2.3). Therefore, the quoted values for k must be approached cautiously. Since all measurement techniques yield physically unrealistic values for k, our dilemma may be due to the nature of the desort aerosol itself. Specifically, an atmosphere containing a desert aerosol is an inhomogeneous and "dirty" medium and, therefore,

^{31.} Bohren, C. F. and Huffman, D. (1983) Absorption and Scattering of Light by Small Particles, Wiley-Interscience, New York.

using a single value for the index of refraction at each wavelength is not the best way to approach the problem. It would be better to treat the aerosol as a heterogeneous mixture of different types of particles.

2.6 Radiative Impacts

Desert aerosols have been studied extensively due to their pervasiveness in the atmosphere and due to their potentially significant radiative impacts. The desert dusts are speculated to have an impact on the radiative balance of the tropical North Atlantic and on the climatology of the desert areas themselves.

Carlson and Benjamin³⁰ have studied the effects of Saharan dust on the radiative fluxes and heating/cooling rates in the atmosphere over the ocean, as well as for cloud-free cases over the desert. Their study showed that the downward radiative flux into the ocean or desert surface decreased in the presence of desert dust and that the heating of the atmosphere increased, leading to a stabilizing effect on the temperature lapse rate. Over the ocean (for conditions representative of the summertime eastern Atlantic), the increased heating amounted to about 1 K day⁻¹, averaged between 1000 mb and 500 mb.

In terms of the net radiative impact at the top of the atmosphere, Carlson and Benjamin found that desert dust had little impact over a cloud free ocean. The surface cooling resulting from the decreased downward infrared flux was nearly compensated for by the increased atmospheric heating. How-

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ever, over highly reflecting surfaces such as clouds or the desert floor, the presence of desert dust in the atmosphere leads to a net system warming as a result of a decrease in the earth-atmosphere system albedo.

Guedalia et al.³² demonstrated that the presence of a desert dust layer at night increases the downward infrared flux at the surface and the radiative cooling rate at the top of the haze layer. Within the first few hundred meters of the haze layer, the radiative cooling rate first increases with the increasing dust concentration but eventually reaches a limiting value. However, the increases in radiative effects with increasing dust concentrations that occur at the top of the haze layer and the surface could give rise to vertical instabilities.

The radiative impact of desert aerosols changes during dust storm conditions. Levin et al.¹¹ reported that in the wavelength region 0.3 - 1.7 μ m, the imaginary part of the index of refraction of desert dust in the Negev desert was lower by a factor of 3 - 5 during a Sharav period as compared to a normal weather period. This was due to the increased contributions of local dust, which is less absorbant to the total aerosol burden than much of the background aerosol. Malm and Johnson¹² observed similar decreases in total aerosol absorption with increases in windblown dust in measurements made at the Grand Canyon. These conclusions are also consistent with results of Otterman et al.¹³ who used Landsat data to characterize desert aerosols over Iran and Pakistan.

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2.7 Conclusions That Can Be Drawn From Previous Studies

Measurements of size distributions and mass loadings indicate that local wind speed controls the numbers of large particles. Therefore, this mode of the distribution should be wind speed dependent.

The compositional data indicate that desert aerosols consist of a mixture of different sized particles with different compositions. Small particles ($r < 0.5 \mu m$) tend to be associated with the generally observed background aerosol. Larger particles are associated with soil and crustal sources. Therefore, a model for desert aerosols would need to include different size distributions for each aerosol component.

The studies of the radiative impact of desert aerosols indicate that desert aerosols can have an impact in the atmosphere in desert regions as well as in air masses in which the dust is imbedded. The radiative impact is not easily established due to the radiative effects of the underlying surface. The studies of radiative effects of desert aerosols also point out that the radiative impacts change during dust storm conditions as a result of the less absorbant, locally produced dust taking up a larger share of the total aerosol burden. This result requires that not only must a separate set of size distributions be considered, but also for an associated set of indices of refraction for each of the aerosol components.

3. THE PRESENT DESERT AEROSOL MODEL

3.1 Overview

The present model separates the desert aerosol into its three major components by composition and uses a different log normal size distribution and set of indices of refraction for each component. The components represent carbonaceous particles, water soluble particles and sand. The sand component consists of two kinds of particles, pure quartz and quartz contaminated with a small amount of hematite (iron oxide, Fe_2O_3). Mie calculations are performed separately for each component and then weighted according to their volume fraction of the total aerosol. The following radiative parameters were calculated:

- 1) extinction coefficient in km^{-1}
- 2) scattering coefficient in km⁻¹
- 3) absorption coefficient in km⁻¹
- 4) single scattering albedo
- 5) asymmetry parameter.

The calculations were performed for 68 wavelengths between 0.2 and 300 μ m. The density and aerosol fraction by volume for background conditions of each component is summarized in Table 4. The aerosol fractions by volume in Table 4 are the same as those for a remote continental aerosol (see page 83 of the World Climate Research Programme²).

Table 4. Jensity of Each Component of the Desert Aerosol Model and Aerosol Fraction by Volume for Background Conditions

AEROSOL COMPONENT	DENSITY (g/cm ³)	AEROSOL Fraction By Volume
Carboneacous	2.000	0.001
Water Soluble	1.769	0.299
Sand	2.650	0.700
Total		1.00

3.2 Wind Speed Dependence On Aerosol Loading

The present model assumes that the volume (or mass) of the water soluble and carbonaceous components remains the same as that for background conditions. Consequently all extra mass loading due to the wind is from sand. The mass loading equation of Jaenicke³³ is the basis for the wind speed dependence

c = 52.77 exp (0.30 u)

(5)

where c is the mass concentration in $\mu g m^{-3}$ of air and u is the wind speed in ms⁻¹ at a height of 10 meters. This equation is an average based on values in the literature gathered

^{33.} Jaenicke, R. (1984) Aerosol Physics and Chemistry, Meteorology Volume, <u>Landolt-Boernstein Numerical Data and</u> <u>Functional Relationships in Science and Technology</u>, to be published by Springer-Verlag.

by Jaenicke. It is meant to represent a generic desert aerosol and is valid only within the mixing layer.

As mentioned in Section 3.1, the present model uses a different size distribution for each component of the desert aerosol. For reference, these size distributions and the range of the Mie calculations are given in Table 5. It is

Table 5. Wind Speed Dependence of the Desert Aerosol Size Distribution Paramenters

	_	SIZE DISTRIBUTION PARAMETERS			
AEROSOL Component	WIND SPEED (ms)	2°1 (µm)	Log(o _j)	Comments	USED IN MIL CALCULATIONS (µm)
Carbonaceous	0 - 30	0.0118	0.301	wмu ² (р. 31)	0.0005 - 100
Water Soluble	u - 30	0.0285	U,350	wмо ² (р. 31)	0.0005 - 100
<u>, , , , , , , , , , , , , , , , , , , </u>	0	6.24	0,277	Coarae Mode of the Romotu Continental Mudel of Jaenicke ³	0.05 - 100
fand	10	7,76	0.331	Linear Interpolation of the Values at	0.05 - 300
24114	20	9,28	0.384	o and so aya	0.05 ~ 750
	20	10.80	0.438	Coarsu Mode of the Dust Story Model of Jaenicke	0.05 - 1000

important to note that the mode radius and the standard deviation of the sand component increase as the wind speed increases. The standard deviation is increased so that the smaller sand particles are retained.
Values for the aerosol fractions by volume, absolute volumes and absolute masses as a function of wind speed are given in Table 6. (The method of determining the values in Table 6 described in Appendix A.) The total particle concentration i**s** for each component, N, is then equal to the absolute volume in Table 6 divided by the volume for 1 particle (the later is known from the Mie calculations). These "inferred" values of N_{i} can then be used to generate number density and area distributions for the present desert acrosol model (see Figs. 2 and 3). Figure 3 shows not only that the amount of scattering material increases as the wind speed increases, but the peak of the area distribution curve, which indicates the range of particles that contribute most to the radiative properties of the aerosol, shifts toward larger particle sizes. Here it should be reemphasized that values of N, used in Figs. 2 and 3 are not based on direct measurements but give total aerosol masses that are consistent with Eq. 5. The present model has adopted this approach instead of using the observed size distributions recently reported by d'Almaida³⁴. This is because his size distribution parameters do not behave consistently as a function of wind speed; that is, in going from background to wind blown dust conditions, the number density for the middle mode of the d'Almeida model decreases, which is not realistic.

^{34.} d'Almeida, G. A. (1987) On the variability of desert aerosol radiative characteristics, <u>J. Geophys. Res.</u>, <u>92</u>:3017-3026.

Table 6. Mass Loading of the Desert Aerosol as a Function of Wind Speed. The parameters C_i, v_i and m_i are the aerosol fraction by volume, volume concentration and mass per unit volume of air, respectively

				1	C #s -]		20	- 1 - 1 - 1		30		
AEHOSOL COMPONENT	". ں	• ,ч ,	•	٦. ر	5	.	ت. ت	Э	, int	Ű	^	
Carbonaceocs	0-001	0.022	0.044	5-91 X 05-5	C.622	0.044	2.75 X 16 ⁻⁶	C.622	0.044	1.37 x 10 ⁻⁷	0.022	0.014
Water Soluile	<u>562.0</u>	6.613	11.69	0.6164	e : e	59-77	8.23 X 10-4	£.613	11.69	4.69 x 10 ⁻⁵	é .613	11.69
Sand	6 . TOJ	£.2I	41.67	0.5835	395.5	1046.1	0.9992	8029.1	1.772.12	6655-O	161353.9	427587.8
rotel	1.000	22.1	52.7	1.090	€02°2	1059.8	1.000	6035.7	21288.9	1.000	161360.5	427549.5
the mite		1		نب • •								

of Air CT ACTOSOL CB The units are de

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Figure 2. Number Density Distribution of the Desert Aerosol for Four Wind Speeds



Figure 3. Area Distribution of the Desert Aerosol for Four Wind Speeds

3.3 Indices of Refraction

3.3.1 Carbonaceous and Water Soluble Components

The indices of refraction for the carbonaceous and water soluble components are listed in Tables 7 and 8 respectively. Figure 4 presents these values in pictorial form. (The values at 40 µm have been used for the 50 to 300 µm region because indices of refraction were not available for these wavelengths.) The values for the carbonaceous component are taken from the work of Shettle and Fenn³⁵, and they represent various types of carbon blacks and soots. The water soluble component utilizes the index of refraction measurements made by Teon, Pollock and Khare³⁶ for pure crystalline ammonium sulfate.

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3.3.2 Sand Component

The hematite in the sand particles is assumed to be in the form of discrete pigments embedded within the quartz. This assumption is reasonable based on the visual examination of sand. An equation originally proposed by Maxwell-Garnett³⁷ is then used to obtain average indices of refraction for sand. The expression is given by

^{35.} Shettle, E. P. and Fenn, R. W. (1979) Models for the Aerosols of the Lower Atmosphere and the Effects of Humidity Variations on Their Optical Properties, AFGL-TR-79-0214, 20 Sept 1979, ADA085951.

^{36.} Toon, O. B., Pollock, J. B. and Khare, B. N. (1976) The optical constants of several atmospheric aerosols species: Ammonium sulfate, aluminum oxide and sodium chloride, J. Geophys. Res., 81:5733-5748.

^{37.} Maxwell-Garnett, J.C. (1904) Colours in metal glasses and in metallic films, Philo. Trans. R. Soc., A203:385-420.

Table 7. Indices of Refraction for Carbonaceous Material. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value given, then the previous power of 10 is implied)

WAVELENGTH R (µm)	INDEX OF REFRACTION n k	WAVELENGTH (µm)	INDEX OF REFRACTION n k
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 8.500\\ 8.700\\ 9.000\\ 9.200\\ 9.200\\ 9.500\\ 9.800\\ 10.000\\ 10.591\\ 11.000\\ 11.500\\ 12.500\\ 13.000\\ 14.000\\ 14.000\\ 14.000\\ 14.600\\ 15.000\\ 14.600\\ 15.000\\ 16.400\\ 17.200\\ 18.500\\ 20.000\\ 16.400\\ 17.200\\ 18.500\\ 20.000\\ 15.000\\ 21.300\\ 22.500\\ 25.000\\ 27.900\\ 30.000\\ 35.000\\ 40.000\\ 50.000\\ 60.000\\ 80.000\\ 100.000\\ 150.000\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

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Table 8. Indices of Refraction for Ammonium Sulfate. The numbers in parentheses in the k columns are the power of 30 following the value of k (if no value given, then the previous power of 10 is implied)

WAVELENGTH	INDEX OF REFRACTION n k	WAVELENGTH (µm)	INDEX OF REFRACTION D k
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.000 2.250 2.500 2.500 2.700 3.000 3.200 3.200 3.392 3.500 3.750 4.000 4.500 5.500 6.000 6.000 6.200 6.500 7.200 7.900	$\begin{array}{c} 1.55 & 1.0(-7) \\ 1.55 & 1.0 \\ 1.54 & 1.0 \\ 1.54 & 1.0 \\ 1.54 & 1.0 \\ 1.54 & 1.0 \\ 1.54 & 1.0 \\ 1.53 & 1.0 \\ 1.53 & 1.0 \\ 1.52 & 1.0 \\ 1.52 & 1.0 \\ 1.52 & 1.5 \\ 1.51 & 1.8(-6) \\ 1.50 & 1.7(-5) \\ 1.49 & 7.7 \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.47 & 1.0(-3) \\ 1.48 & 7.6 \\ 1.41 & 2.0(-3) \\ 1.49 & 2.6(-1) \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.58 & 3.6(-2) \\ 1.55 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.46 & 6.5 \\ 1.41 & 8.0 \\ 1.35 & 1.3(-2) \\ 1.31 & 1.8 \\ 1.19 & 4.9 \\ 1.93 & 5.4(-1) \\ 1.36 & 7.5(-2) \\ 1.61 & 1.6 \\ 1.61 & 1.7 \\ 1.61 & 1.6 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.5(-2) \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1.61 & 1.7 \\ 1.61 & 1.4 \\ 1.61 & 1.4 \\ 1.50 & 7.3(-3) \\ 1.61 & 1.4 \\ 1$	<pre>) 8.500 8.700 9.000 9.200 9.500 9.800 10.000 10.591 11.000 11.500 12.500) 13.000) 14.000 14.800 15.000) 16.400 17.200) 16.400 17.200) 16.400 17.200) 18.000) 18.500) 20.000) 21.300 22.500 25.000) 27.900 30.000) 27.900 30.000) 35.000) 35.000) 35.000) 35.000) 35.000) 35.000) 35.000) 35.000) 30.000) 35.000) 30.000) 30.000] 30.0000] 30.0000] 30.0000] 30.0000] 30.0000] 30.00000000000000000000000000000000000</pre>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$



Figure 4. Indices of Refraction of Carbonaceous Material and Ammonium Sulfate, (a) Real part and (b) Imaginary Part

$$e_{av} = e_{m} \begin{bmatrix} 3f\left(\frac{e - e_{m}}{e + 2e_{m}}\right) \\ 1 + \frac{1 - f\left(\frac{e - e_{m}}{e + 2e_{m}}\right) \end{bmatrix}}{(6)}$$

where for our problem, e_{av} , e and e_m are the complex dielectric constants of sand, hematite and quartz respectively, and f is the volume fraction of hematite in the sand particles. The complex dielectric constant of a material is related to its complex index of refraction by

$$Re(e) = n^2 - k^2$$
 (7)

and

$$Imag(e) = 2n k$$
. (8)

A recent comparison of different effective media theories by Chylek et al.³⁸ showed that the Maxwell-Garnett approximation gave acceptable results.

The use of Maxwell-Garnett theory requires indices of refraction for quartz and hematite. To account for anisotropic behavior of quartz, separate index of refraction data have been obtained for the ordinary ray (o-ray) and extraordinary ray (e-ray) of pure crystalline quartz. The values are listed in Tables 9 and 10, and come from five sources:

^{38.} Chylek, P., Srivastava, V., Pinnick, R. G. and Wang, R. T. (1988) Scattering of electromagnetic waves by composite spherical particles: experiment and effective medium approximations, <u>Appl. Opt.</u>, 27:2396-2404.

Table 9. Indices of Refraction for the O-Ray of Quartz. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value given, then the previous power of 10 is implied)

WAVELENGTH (µm)	INDRA RBFRAC D	op Tion k	WAVELENGTH (µm)	INDEX REFRAC n	OF Tion k
$\begin{array}{c} 0.200\\ 0.250\\ 0.300\\ 0.337\\ 0.400\\ 0.488\\ 0.515\\ 0.550\\ 0.633\\ 0.694\\ 0.860\\ 1.060\\ 1.300\\ 1.536\\ 1.800\\ 2.000\\ 2.250\\ 2.500\\ 2.500\\ 2.500\\ 2.500\\ 3.000\\ 3.200\\ 3.392\\ 3.500\\ 3.750\\ 4.000\\ 4.500\\ 5.500\\ 6.000\\ 5.500\\ 6.000\\ 6.200\\ 6.500\\ 7.200\\ 7.900\\ 8.200\\ \end{array}$	$\begin{array}{c} 1.649\\ 1.606\\ 1.584\\ 1.568\\ 1.559\\ 1.550\\ 1.548\\ 1.542\\ 1.541\\ 1.537\\ 1.534\\ 1.531\\ 1.534\\ 1.531\\ 1.538\\ 1.524\\ 1.5516\\ 1.5516\\ 1.499\\ 1.483\\ 1.483\\ 1.483\\ 1.483\\ 1.483\\ 1.462\\ 1.445\\ 1.371\\ 1.325\\ 1.293\\ 1.246\\ 1.065\\ 0.141\end{array}$	$\begin{array}{c} 1.00(-8)\\ 1.00\\ 1$	8.500 8.700 9.000 9.200 9.500 9.800 10.000 10.591 11.000 12.500 13.000 14.000 14.000 14.000 15.000 15.000 15.000 22.500 25.000 27.900 30.000 35.000 40.000 50.000 60.000 80.000 150.000 10.0000 10.0000 10.0000 10.0000 10.000000 10.0000 10.0000000 10.0000	0.114 0.131 0.176 0.633 4.497 3.014 2.663 2.188 2.013 1.587 2.174 1.768 1.587 2.174 1.768 1.587 1.580 1.289 1.456 1.289 2.729 2.5005 2.224 2.175 2.120 2.109	1.26(0) 1.41 2.61 4.55 $3.92(-1)$ $8.69(-2)$ 5.17 2.22 1.73 1.88 $2.27(0)$ $5.19(-2)$ 3.48 2.29 1.54 $9.75(-3)$ $1.20(-2)$ 1.77 2.52 $7.66(-1)$ $2.57(0)$ $9.41(-1)$ $1.85(0)$ $2.16(-2)$ 1.08 $4.98(-3)$ 3.29 2.86 2.24 3.69 $9.55(-4)$ 8.72 7.96

Table 10. Indices of Refraction for the E-Ray of Quartz. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value given, the the previous power of 10 is implied)

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- 1) Gray³⁹ and Peterson and Weinman⁴⁰ for the visible and near IR regime
- 2) Drummond 41 for the region from 2.3 to 7.0 μm
- 3) Spitzer and Kleinman⁴² for the region 7.0 to 40.0 μm
- 4) Philipp⁴³ for the region 40 to 300 μm_{\star}

Figure 5 gives these indices of refraction in pictorial form.

Indices of refraction for hematite are listed in Table 11 and shown in Figure 6. The values are based on the work from four researchers:

- 1) Galuza et al.⁴⁴ for the 0.2 to 0.4 μ m region
- 2) Kerker et al.⁴⁵ for the 0.4 to 0.8 μ m region
- 3) Steyer⁴⁶ for the 4 to 20 μ m region
- 39. Gray, D. C. (1963), <u>American Institute of Physics Hand-</u> book, McGraw-Hill, New York, NY, 1963, 2nd Edition.
- 40. Peterson, J. T. and Weinman, J. A. (1969) Optical properties of quartz dust particles at infrared wavelengths, <u>J. Geophys. Res.</u>, 74:6947-6957.
- 41. Drummond, D. G. (1936) Absorption coefficients of crystal quartz in the infrared, <u>Proc. Roy. Soc. (London)-Se-</u> ries A, <u>153</u>:328-338.
- 42. Spitzer, W. G. and Kleinman, D. A. (1961) Infrared lattice bands of quartz, <u>Phys. Rev.</u>, <u>121</u>:1324-1335.
- 43. Philipp, H. R. (1985) Silicon dioxide (SiO₂), type-α (crystalline), in <u>Handbook of Optical Constants of</u> <u>Solids</u>, Edited by E. D. Palik, 719-747.
- 44. Galuza, A. J., Eremenko, V. V. and Kirichenko, A. P. (1979) Analysis of hematite reflection spectrum by the Kramers-Kronig method, <u>Sov. Phys. Solid State</u>, <u>21</u>:654-656.
- 45. Kerker, M., Scheiner, P., Cooke, D. D. and Kratohvil, J. P. (1979) Absorption index and color of colloidal hematite, J. Colloid. Interface Sci., 71:176-187.
- 46. Steyer, T. R. (1974) Infrared optical properties of some solids of possible interest in astronomy and atmospheric physics, Ph.D. Thesis, Department of Physics, University of Arizona.



Figure 5. Indices of Refraction of Quartz, (a) Real part and (b) Imaginary Part

Table 11. Indices of Refraction for Hematite. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value given, then the previous power of 10 is implied)

WAVBLBNGTH (µm)	INDEX REFRAC D	COF TION K	WAVELBNGTH (µm)	INDEX REFRAC n	of Tion k
0.200	1.560	1.28(0)	8.500	2.363	3.10(-3)
0.250	2.070	1.33	8.700	2.343	4.07
0.300	2.320	1.18	9.000	2.317	5.00
0.337	2.430	1.09	9.200	2.290	5.93
0.400	2.674	5.23(-1)	9.500	2.253	1.33
0.400	3.0/4	∡.JU 1 E0	9.800	2.21/	0./3
0.515	3 103	1.30 1.30	10,000	2,177	1 30/21
0.550	3,102		11 000	2.103	1.59(-2.
0.033	2 920	3.74(-37	11 560	1 945	2 1 3
0.660	2.730	4.00	12,500	1.746	3.66
1.060	2 660	3 00(-5)	13,000	1 636	4.75
1.300	2.640	1.00	14,000	1.246	8.01
1,536	2.630	5.50(-6)	14.800	0.769	2.17(-1)
1.800	2.620	4.00	15.000	0,592	3.07
2.000	2.610	4.50	16.400	0.244	1.64(0)
2.250	2.610	5.00	17.200	0.350	2.38
2.500	2.610	6.00	18.000	0.711	3.35
2.700	2,610	8.00	18.500	1.468	4.14
3.000	2.610	1.00(-5)	20,000	2.812	1.47
3.200	2,610	1.10	21.300	1.643	2.57
3.392	2.610	1.10	22.500	2,940	4.29
3.500	2.610	1.20	25.000	2.644	1.02
3.750	2.610	1.20	27.900	0,558	2.68
4.000	2.603	4.90	30.000	0,583	4.80
4.500	2.593	4.63	35.000	13.862	- 1. OI(')
5.000	2.580	4,1	40,000	7.370	3.8/(*1)
5,009	2,00/ 0 5,17	ี่ ข _{ึ่} ∴ ".ว.(.~.4) บ่าว	50.000	5.U39 5.A7A	5 97(-2)
0.000 6 300	2.24/ 2.527	1 01(2)		511/4	3,33(*2)
0.200 6 500	2 820	1 1 4	100.000	5.100 A 474	2, 4 0
7 200	2,220	ょ • ↓ ** 1 りつ	150.000	4 961	1 30
7.900	2.427	1.23	200.000	1.874	1.01
8.2(0	2,390	2.17	300.000	4.790	6.56(-3)



Figure 6. Indices of Refraction of Hematite, (a) Real part and (b) Imaginary Part

4) Onari et al.⁴⁷ for the 10 to 300 μ m region In Table 11, the values for the 0.8 to 4 μ m region are estimates because indices of refraction are not available. Also the values beyond 4 μ m represent average indices of refraction since hematite, like quartz, is anisotropic in this region. The average indices of refraction are calculated using

$$m_{avg} = 2m_{o-ray}/3 + m_{e-ray}/3$$
(9)

where the 2/3 to 1/3 ratio is used because two of the optical axes of hematite are the same. (Although it is not correct to average indices of refraction, the resulting values are sufficient for use in Eqs. 6 - 8. That is, for small concentrations of hematite, the anisotropic effects from quartz dominate those of the hematite.) For the 10 to 20 μ m region, the measurements by Stever⁴⁶ and Onari et al.⁴⁷ have been averaged together before applying Eq. 9. The weighting scheme is given by

$$m(\lambda) = w(\lambda)m_{g}(\lambda) + (1 - w(\lambda))m_{O}(\lambda)$$
(10)

where m_{S} and m_{O} are the complex indices of refraction from Steyer and Onari et al. and

 $w(\lambda) = \begin{cases} 1, & \lambda \leq 10 \\ (\lambda - 20)^2 (2\lambda - 10)/1000, & \frac{\lambda}{10} \leq \lambda \leq 20 \\ 0, & 20 \leq \lambda \end{cases}$ (11)

^{47.} Onari, S., Arai, T. and Kudo, K. (1977) Infrared lattice vibrations and dielectric dispersion in a -Fe₂O₃, <u>Phys.</u> <u>Rev. B</u>, <u>16</u>:1717-1721.

Table 12. Indices of Refraction for Sand Having a Volume Fraction of Hematite of 5%. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value-given, then the previous power of 10 is implied)

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WAVELENGTH (µm)	(0-1) A	AY) k	(B-R N	AY) A	WAVELENGTH (um)	К~О~Ж В	ж ХУ)	(E-R n	(YA X
0.200	1.657	7.36(-2)	1.657	7,36(-2)	8,500	0.220	1.52(0)	0.153	1.47(0)
0.250	1.646	5.80	1,646	5.80	8.700	0.425	1.R0	1.037	1.03
0.300	1.630	4.45	1,630	4.45	9.000	0.199	2.33	0.241	2.00
0.137	1.617	3.84	1.617	3.84	9,200	0.622	4.31	1.639	6.13
0.400	1.607	1.66	1.607	1.66	9.500	4.385	3.74(-1)	3.816	2.18(+1
0.488	1,608	5.39(-3)	1.608	5.39(-3)	9.800	2.973	8,29(-2)	2.827	6.60(-2
0.515	1,607	3.98	1,607	3,98	10,000	2.639	4.95	2.552	4.22
0.550	1.605	2.33	1,605	2,33	10,591	2,184	2.18	2.153	2,02
0.633	1.598	2.57(+4)	1,598	2.57(-4)	11.000	2.014	1.73	2.001	1.59
0.694	1.595	2.76(+5)	1.595	2.76(-5)	11.500	1.839	1.89	1.854	1.56
0.860	1.586	1.22(-4)	1.586	1.221-4)	12,500	1.576	2.14(0)	1.263	1,26(-)
1.040	1.680	9.54(-7)	1,580	9.54(-7)	13.000	2.147	5.17(-21	2.575	3.05
1.300	1.577	3.27	1.577	3.27	14.000	1.741	3.71	1.792	1.97(-)
1.536	1.574	1.85	1.574	1.05	14.800	1.778	3.05	1.625	2.08
1.800	1.569	1.37	1.569	1.37	15.000	1 727	2.52	1.584	2.28
2.000	1,965	1.53	1.565	1.53	16.400	1.368	1.22(-1)	1.146	2.57(-1
2.250	1.561	1.69	1.561	1.69	17,200	1.748	2.98	1.244	9.091-1
2.500	1.556	6.76	1.556	9.19	18.000	1.433	5 231-21	0.457	2.301-
2.700	1.551	9.54	1.551	1.36(-6)	18.500	1.242	4.20	0.214	1.0410
3,000	1.545	2.641-51	1.545	8.58	20.400	0.125	8.25(-1)	1.330	4.78
3.200	1.539	6.951-61	1.539	4.28	41.300	0.270	2.58(0)	2.948	2.77(-)
3.392	1.533	6.59	1.533	5.91	22.500	5.540	1.15	2.531	1.66
3.500	1.529	1.44	1.524	8.49	21.000	0.812	1.114	1.505	1.26
3.750	1.519	5.851.51	1.619	3.63(-5)	27.900	2.442	2.04(-1)	4.651	8.68
4.000	1.508	2.11	1.508	7.11	30.000	2.951	1.62	3.605	6.48
4.500	1.488	4.96(-4)	1.408	3.52(-4)	11.000	2.477	1.41(-2)	2.647	7.43(-
1.000	1.464	5.51(+3)	1.464	4. 171-1)	40.000	2.358	6.89(-3)	2.470	1.08
5.500	1.410	5.42	1 418	5.12	50.000	2.324	4.46	2.177	3.361-
6.000	1.372	6.65	1. 172	4.74	60.000	1.280	3.24	2.129	2.11
6.200	1.340	7.73	1.340	7.71	80.006	2.247	4.31	2.289	1.27
6.500	1.294	5.76	1.294	7 24	100.000	2.226	1.40	2.272	9.421.
7.200	1.111	1 241-25	1.10	1.461-21	150.000	2.214	1.15	2.257	5.27
7.500	0.623	8.15	0.601	8.99	200.000	2 204	4 471-A1	2.252	1 6 4
									1100

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Table 13. Indices of Refraction for Sand Having a Volume Fraction of Hematite of 10%. The numbers in parentheses in the k columns are the power of 10 following the value of k (if no value given, then the previous power of 10 is implied)

MAVHLENGTH (m)	(0-k 6	AY) A	(k-A n	AY) k	WAVELENGTH (µm)	(ט-א ח	AY) k	(≌∸R n	¥ (۲۸
0.200	1.665	1.47(-1)	1.663	1.47(-1)	8.500	0.336	1.83(0)	0.239	1.74(0)
0.250	1.686	1.17	1.686	1.17	8.700	0.954	2.19	1.557	7.09(-1)
0.300	1.677	9.00(-2)	1.677	9.00(-2)	9.000	0.221	2.06	0.251	2.56(0)
0.337	1.665	7.78	1.665	7,78	9.200	0.612	4.07	1.590	5.85
0.400	1.656	3,35	1.656	3.35	9,500	4.274	3.56(-1)	3,733	2.07(-1)
0.408	1.667	1.09	1.667	1.09	9.800	2.933	7.89(-2)	2.794	6.29(-2)
0.515	1.666	8.09(-3)	1.666	8.09(-3)	10.000	2.615	4.74	2.533	4.05
0.550	1.664	4.74	1.664	4.74	10.591	2.180	2.14	2,151	1.98
0.633	1.655	5.22(-4)	1.655	5.22(-4)	11.000	2.015	1.72	2.003	1.60
0.694	1.650	5.61(-5)	1.650	5.61(-5)	11,500	1.844	1.90	1,859	1,59
0.860	1.635	2.46(-4)	1.635	2.46(-4)	12.500	1.564	2.02(0)	1,305	1.23(-1)
1.060	3.627	1,92(-6)	1.627	1,92(-6)	13.000	2.119	5.15(-2)	2,524	2,91
1.300	1.623	6.51(-7)	1.623	6.51(-7)	14.000	1.715	3.94	1.762	2.29(-2)
1.536	1.620	3.63	1.620	3.63	14.800	1,727	3.01	1.580	2.93
1.800	1.615	2.67	1.615	2.67	15.000	1.669	3.48	1.533	3.33
2.000	1.611	3.00	1.611	1.00	16.400	1.163	2.31(-1)	0.955	4.81(-1)
2.250	1.607	3.31	1.607	3.31	17.200	2.011	6.55	1.404	1.53
2.500	1.602	8.58	1.602	1.09(-6)	18.000	1.584	9.12(-2)	0.489	2.49
2.700	1.597	1.19(-6)	1.547	1.59	18.500	1.346	6.03	0.229	1.10(0)
1.000	1.541	2.60(-5)	1.591	6.69	20.000	0.145	8.66(~1)	1.389	4.57
3.200	3.545	7.13(-6)	1.585	4.53	21.300	0.346	2.59(0)	2.853	4.48(-1)
3.392	1.579	6.78	1.574	6.17	22,500	5.370	1.35	2.698	2.95
3.500	1.576	8.66	1 576	8.66	25.000	0.946	1.84	1.559	1.54
3.750	1.56	5 751-51	1.566	1.58(~5)	27.900	2.162	3.82(-1)	4.400	9.15
	1.555	7.10	1.555	7,10	30.000	3.446	1.53	4,196	1.41(0)
4.500	1.535	4.86(-4)	1.535	3.451-41	35.000	2.655	2.43:-21	2.836	3.691-2)
5.000	1.511	5.39(-3)	1.511	4.27(-3)	40.000	2.491	1.07	2.606	1.51
5,500	1.466	5 13	1.466	5,03	50,000	2.446	6.13(-3)	2.495	5.09(+3)
8.000	1.420	6.56	1.420	4.68	60,000	2,380	4.28	2.436	3.19
6.200	1.184	7.64	1.389	7.64	80,000	2.347	4.94	2.389	1.92
6.500	1 142	5 71	1.342	7 17	100.000	2.326	1.07	2,370	1.43
7.200	1.161	1.241-21	1.160	1.461-21	150.000	2.310	1.41	2.352	8.24(-4)
7 900	0.662	9 22	0.614	9 36	200.000	2.294	1.21	2.347	5.68
					100 000				

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Figure 7. Real Part of the Index of Refraction for Sand Having Hematite Concentrations of 0, 5 and 10%, (a) O-Ray and (b) E-Ray



Wavelength (micrometer)

Figure 8. Imaginary Part of the Index of Refraction for Sand Having Hematite Concentrations of 0, 5 and 10%, (a) O-Ray and (b) E-Ray

where the weighting function has the properties that: w(10) = 1, w(20) = 0 and the derivative of $w(\chi)$ goes to zero for $\chi = 10$, 20.

Equations 6 - 8 and the data in Tables 9 - 11 have been used to obtain indices of refraction for sand having hematite concentrations of 5 and 10%. The results are listed in Tables 12 and 13, and are shown in Figures 7 and 8. These volume fractions, along with f = 0% (pure quartz), encompass the range of hematite concentrations in sand^{7,48}.

Tables 12 and 13 suggest that the concentration of hematite in the sand component will strongly affect the radiative properties of the aerosci as a whole. This is especially true for the $0.2 - 0.6 \ \mu m$ wavelength region where the imaginary index varies from 10^{-8} to 10^{-1} . Therefore, Mie calculations were performed for sand having hematite concentrations of 0, 5 and 10%. The results and implications of these calculations will be discussed in Section 4.1.

It should be mentioned that for each hematite concentration, separate Mie calculations were performed for the o-ray and e-ray. The radiative properties for a given concentration of hematite are then obtained as two thirds of the o-ray values plus one third of the e-ray values. The two-thirds to one-third ratio is used because, like hematite, two of the three optical axes of quartz are the same. (Note in this case, Mie calculations are being averaged, not indices of re-

^{48.} Egan, W. G. (1985) <u>Photometry and Polarization in Remote</u> <u>Sensing</u>, Elsevier Science Publishing, New York, pp. 398~ 399.

fraction.) Dealing with birefrigent materials in this manner is, strictly speaking, only valid for particles that are small compared with the wavelength. Since our sand particles approach the geometric optics limit, the approach may not be truly applicable.

3.3.3 Discussion of the Indices of Refraction

The use of a separate set of optical constants for each mode of the size distribution is the main difference between the present model and the previous desert aerosol models of Shettle¹ and of d'Almeida³⁴. (They both use only one set of optical constants for all particles making up the aerosol.) The distinction between the two approaches is subtle, but im-In the present model, the indices of refraction for portant. each component are based on measurements of pure substances while the Shettle and d'Almeida models use average indices of refraction which attempt to characterize the complex mixture of discrete particles comprising the desert aerosol. Because they have different physical meanings, it is difficult to make a direct comparison between the average indices of refraction used by Shettle and by d'Almeida, which are based on those in the literature, and the ones used in the present model. However, the advantage of using optical constants obtained from bulk measurements is that they tend to be more accurate.

3.4 Method of Determining the Optical Properties of Multicomponent Mixtures

When performing the radiative calculations for each aerosol component, a number density of 1 particle cm^{-3} of air

was used for simplicity. The attenuation coefficients corresponding to 1 particle cm⁻³ were then converted to those having the absolute volumes given in Table 6. (The conversion factor is the actual volume of the aerosol component divided by the volume for 1 particle cm⁻³.) These attenuation coefficients were then added together to obtain the volume-weighted attenuation coefficients. In turn, the single scattering albedo, w_0 , of the aerosol is equal to the volume-weighted scattering coefficient divided by the volume-weighted extinction coefficient.

By definition, the method of determining the volumeweighted asymmetry parameter, g, is different from that for the attenuation coefficients. Here, g represents the average cosine of the scattering angle for a fictitious 1 particle cm^{-3} of air. g is thus calculated using the following equation:

$$g(\lambda) = \frac{\sum g_i(\lambda) X_i(\lambda) N_i}{\sum X_i(\lambda) N_i}$$
(12)

where X_i is the scattering coefficient for 1 particle cm⁻³ and g_i is the asymmetry parameter for each component.

4.1 Results for Various Concentrations of Hematite in the Sand Component

An effort has been made to determine how the radiative properties of the desert aerosol are affected by the concentration of hematite in the sand component. (The presence of hematite is important because it is a selective absorber at visible wavelengths.) Seven cases have been investigated in this report, each representing a possible composition for the sand component. The cases are summarized in Table 14.

	Percentage the	of Particle Sand Compon	s Making Up ent
Case No.	f = 0%	f ≖ 5%	f = 10%
1	100	0	0
2	0	100	U
3	0	0	100
4	50	50	0
5	50	0	50
6	0	50	50
7	33,3	33.3	33.3

Table 14. Various Compositions of the Sand Component Investigated in this Report

Cases 1 - 3 represent sand components that have hematite concentrations of 0, 5 and 10%, respectively. In Cases 4 - 6, the sand component is composed of two types of particles, each having its own hematite content. Here the two types of particles have the same size distribution as before, but have only 50% of the total number of sand particles. In Case 7, the size distribution of the sand component contains an equal number of particles having hematite contents of 0, 5 and 10%.

The radiative properties of the descrt aerosol were determined using each of the sand components given in Table 14. A preliminary survey of the results showed that the extinction coefficients for Cases 1 - 7 are essentially the same. (This is expected since extinction is driven primarily by the size distribution.) Furthermore, Cases 2, 3, 6 and 7 gave similar values for the absorption coefficient which suggests that for our size distribution, the effects of hematite concentrations of 5 and 10% are about the same.

Figures 9(a) and 9(b) give absorption coefficients and single scattering albedos as a function of wavelength for a wind speed of 0 ms⁻¹. (Only Cases 1, 3 and 5 have been plotted because, as mentioned above, the effects of hematite concentrations of 5% and 10% are about the same.) In Figure 9(a), it can be seen that beyond about 1 μ m, absorption coefficients are similar for Cases 1, 3 and 5. At UV and visible wavelengths, the presence of hematite in the sand component gives increased absorption as expected. In Figure 9(b), the higher absorption for Cases 3 and 5 leads to lower single







Figure 10. Desert Aerosol Model (a) Absorption Coefficients and (b) Single Scattering Albedos using Cases 1, 3 and 5 for the Sand Component with 10 ms⁻¹ Wind Speed Conditions

scattering albedos at UV and visible wavelengths. The minima near 16 and 30 mm for Cases 3 and 5 are directly related to the absorption bands of hematite at these wavelengths.

Similar plots of absorption coefficient and single scattering albedo are given in Figures 10 - 12 for wind speeds of 10, 20 and 30 ms⁻¹. The same observations can be made for Cases 1, 3 and 5, but the differences at UV and visible wavelengths become more pronounced as the wind speed increases.

4.2 Choosing a Sand Component for the Desert Aerosol Model

We have selected Case 5 to represent the sand component in the present desert aerosol model. Case 5 was chosen because it represents a "middle of the road" estimate of the absorption at UV and visible wavelengths. That is, Cases 1 and 3 give the extrema of absorption and, therefore, Case 5 best represents the range of the calculations. For reference, the results of the Mie calculations for Case 5, as well as for the carbonaceous and water soluble components, are given in Appendix B.

4.3 General Discussion of the Desert Aerosol Model

This section gives the results for the present desert aerosol model where, as discussed in Section 4.2, the sand component consists of quartz particles and quartz particles contaminated with a 10% concentration of hematite. Figures 13 through 16 give the attenuation coefficients as a function of wavelength for 0, 10, 20 and 30 ms⁻¹ wind speed conditions. The 0 ms⁻¹ and 30 ms⁻¹ winds are meant to represent background



Figure 11. Desert Aerosol Model (a) Absorption Coefficients and (b) Single Scattering Albedos using Cases 1, 3 and 5 for the Sand Component with 20 $\rm ms^{-1}$ Wind Speed Conditions



Figure 12. Desert Aerosel Model (a) Absorption Coefficients and (b) Single Scattering Albedos using Cases 1, 3 and 5 for the Sand Component with 30 $\rm ms^{-1}$ Wind Speed Conditions



Figure 13. Descrit Aerosol Model Attenuation Coefficients Versus Waveleigth for 0 ms-1 Wind Speed Conditions



Figure 14. Describeress Model Attenuation Coefficients Versus Wavelength for 10 ms⁻¹ Wind Speed Conditions



Wavelength (micrometer) Figure 15. Desert Aerosol Model Attenuation Coefficients Versus Wavelength for 20 ms-1 Wind Speed Conditions



Figure 16. Desert Aerosol Model Attenuation Coefficients Versus Wavelength for 30 ms⁻¹ Wind Speed Conditions

and severe dust storm conditions respectively. For reference, the values in Figures 13 - 16 have been tabulated in Appendix C.

A number of important features in Figures 13 - 16 are worth mentioning. First, there is selective absorption at visible wavelengths which becomes more pronounced as the wind speed increases. The selective absorption is due to the hematite in the sand component and will make the desert aerosol appear slightly reddish in color during dust storm conditions. The carbonaceous particles contribute very little to the total absorption of visible radiation primarily because their abundance is too small.

A second thing to observe in Figures 13 - 16 is the structure in the IR absorption. The peaks in the absorption near 3, 7 and 9 µm for 0 ms⁻¹ wind speed conditions are primarily due to the strong absorption bands of ammonium sulfate. For dust storm conditions however, the obsorption in the IR is dominated by the sand component. Interestingly, there are minima in the absorption and maxima in the scattering near 8 and 20 µm, which correspond to the centers of the strong crystal lattice absorption bands of quartz. It is believed that this phenomenon is a result of the quartz in the sand component acting as a reflector. To show this, consider an electromagnetic wave propagating in air as it encounters a plane boundary having a complex index of refraction, m = n + ik.

Reflectance
$$\frac{(n-1)^2 + k^2}{(n+1)^2 + k^2}$$
 (13)

When $n \ll 1$, $n \gg 1$ or $k \gg 1$ (as is the case for the absorption bands of quartz), the reflectance approaches 1.0. Thus the incident radiation is reflected and the absorption drops because the incident wave cannot penetrate the material to be absorbed.

Finally, it can be seen from Figures 13 - 16 that the extinction is wavelength dependent for winds of 0 ms^{-1} but nearly constant at 20 and 30 ms⁻¹. These differences are driven by the relative contributions of the aerosol components. For winds of 0 ms^{-1} , only the smaller water soluble particles with respect to the wavelength dominate the extinction at visible and near IR wavelengths and, therefore, a wavelength dependence exists. On the otherhand, in high wind speed conditions, the extinction is dominated by the much larger sand particles that approach the geometric optics regime.

Figure 17 gives the values of single scattering albedo for 0 ms and 30 ms⁻¹ wind speed conditions. At the UV and shorter visible wavelengths, the single scattering albedos decrease significantly as the wind speed increases. This effect becomes less pronounced, however, for the longer visible and near IR wavelengths. In the middle IR region, single scattering albedos for 0 and 30 ms⁻¹ winds exhibit a high degree of atructure. Specifically, the sharp minima near 3, 7 and 9 μ m

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can be attributed to the absorption by ammonimum sulfate. For winds of 30 ms⁻¹, the large peaks near 9 and 20 μ m relate to the excess scattering by the quartz in the sand component which was discussed earlier. Beyond about 40 μ m, single scattering albedos for 0 ms⁻¹ winds are much lower than those for 30 ms⁻¹ winds. This should not be interpreted as significant absorption, however, because the magnitude of the absorption is small beyond 40 μ m for 0 ms⁻¹ winds.

Figure 18 gives the values of the asymmetry parameter as a function of wavelength for 0 and 30 ms⁻¹ wind speed conditions. Generally speaking, the values for dust storm conditions are greater than those for background conditions throughout the 0.2 to 300 μ m region. This should not be a surprise because the scattering for dust storm conditions is dominated by the large sand particles (with respect to the wavelength of radiation) which have their scattering peaked in the forward direction.

4.4 Comparison with Other Reseachers

This section compares the present desert aerosol model with the models of Shettle¹ and d'Almeida³⁴. The comparisons are limited to the 0.4 - 40 μ m wavelength region because the Shettle and d'Almeida models end at 40 μ m. For reference, the number densities distributions of the present desert aerosol and the d'Almeida model are compared in Figure 19 and the area distributions are compared in Figure 20. The curves for the d'Almeida model are derived from the trimodal lognormal size distributions that d'Almedia used when performing his radia-



Figure 18. Desert Aerosol Model Asymmetry Parameter Versus Wavelength for 0 and 30 $\rm ms^{-1}$ Wind Speed Conditions



Figure 19. Number Density Distributions for the Present 34 Desert Acrosol Model (solid lines) and Those of d'Almeida (dashed lines)

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Figure 20. Area Distributions for the Present Desert Aerosol Model (solid lines) and Those of d'Almeida⁵⁴ (dashed lines)

tive transfer calculations, not the observed size distribution data. (d'Almeida's size distribution parameters for background, wind carrying dust and sandstorm conditions are based on data gathered when the horizontal visibility was greater than 8 km, between 2 to 7 km and less than 2 km, respectively.) The size distributions of the present desert aerosol model and the Shettle model are essentially the same.

Figures 21(a) and 21(b) compare the wavelength dependent extinction coefficients against those of Shettle and d'Almeida, respectively. The present model gives values that are close to those of Shettle because both models use similar size distributions. Figure 21(b) suggests that the values of d'Almeida for background conditions are much greater than The differences appear to be a result of d'Almeida ours. defining his background conditions in terms of "clear" visibility and not wind speed, and some mass loading due to the wind may be occurring. The extinction calculated by d'Almeida for sandstorm conditions show strong variations with wavelength while ours do not. The structure beyond about 1 um arises because much of the mass loading in the d'Almeida model is from particles that are smaller than ours and not in the geometric optics limit. Figures 22(a) and 22(b) give comparisons of the scattering coefficients.

Figures 23(a) and 23(b) compare the values of absorption coefficient as a function of wavelength against those of Shettle and d'Almeida respectively. (To avoid cluttering the figures, only the values for 0 and 30 ms⁻¹ have been plotted.)



Figure 21. Comparison of Extinction Coefficients for the Desert Aerosol Model with These of (a) Shettle¹ and (b) $d^{+}Aimeida^{-34}$



wavelength (micrometer) Figure 22. Comparison of Scattering Coefficients for the Desert Aerosol Model with Those of (a) Shettle¹ and (b) d'Almeida³⁴



Figure 23. Comparison of Absorption Coefficients of the Desert Acrosol Model with (a) Those of Shettle and (b) Those of d'Almeida³⁴

In Figure 23(a), the magnitude of absorption for 0 ms⁻¹ wind speeds is about one order less than the background model of Shettle. For dust storm conditions, the present and the Shettle models are similar in the middle IR region, but the present model gives far less absorption at the longer visible and the near IR wavelengths. Similar observations can be made about Figure 23(b). Absorption coefficients of the d'Almeida background model are about to orders of magnitude greater than ours and for dust storm conditions, the two models agree in the middle IR region. As with the Shettle model, the d'Almeida model for dust storm conditions predicts more absorption than the present model at longer visible and near IR

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wavelengths. (This is the main difference between the three models and it is directly related to the way the present model deals with the index of refraction.)

Figure 24 compares single scattering albedos against those of Shettle and d'Almeida. In Figure 24(a), albedos for 0 ms⁻¹ wind speeds are greater than the background models of Shettle and d'Almeida throughout the visible and near IR regime. The three models are in reasonable agreement between about 3 and 10 µm, but significant differences exist beyond 20 µm. In Figure 24(b), all three models show increasing albedos when going from UV to near IR wavelengths, but the absolute magnitudes differ from each other. Specifically, albedos for 30 ms⁻¹ wind speeds are much higher than the dust storm models or Shettle and d'Almeida which is a direct consequence of the way the present model deals with the index of refraction. Also, Figure 24(b) suggests that the large peaks near 9 and 20 µm are not seen in the previous two models.

Comparisons of the asymmetry parameter as a function of wavelength are given in Figures 25(a) and 25(b) for background and for dust storm conditions, respectively. For background conditions, there is very little agreement between the three models, especially at visible and near IR wavelengths. In dust storm conditions, asymmetry parameters are similar for the three models. This should come as no surprise bacause the scattering for dust storm conditions is dominated by the large (with respect to the wavelength of radiation) sand particles which have their scattering peaked in the forward direction.







Figure 25. Comparison of Asymmetry Parameter for the Desert Aerosol Model with Those of Shettle¹ and d'Almeida³⁴, (a) Background and (b) Dust Storm Conditions

4.5 Comparison with Observations

In order to compare the three models with observed data, the extinction at 0.55 µm can be converted to visit anges. V, using the formula

 $V = 3.912/Extinction at 0.55 \mu m$.

Both the present and the Shettle background model to visual ranges of about 80 km, while the d'Alassian ground model yields a value close to 20 km. Model visual range at White Sands, New Mexico by Pitch and at Big Bend, Texas by Malm et al.⁵⁰ indicate ities of 80 km occur frequently in desert. and which adds credibility to the present model. These surements may also suggest that the extinction in the America model may be too high for background conditions.

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^{49.} Pitchford, A., Pitchford, M., Malm, W., Flocchini, R., Cahill, T. and Walther, E. (1981) Regional Analysis of Factors Affecting Visual Air Quality, <u>Atmospheric Envi-</u> ronment, <u>15</u>:2043-2054.

^{50.} Malm, W. C., Walther, E. G., O'Dell, K. and Kleine (1981) Visibility in the Southwestern United States from Summer 1978 to Spring 1979, <u>Atmospheric Environment</u>, <u>15</u>:2031-2042.

5. SUMMARY AND CONCLUSIONS

A description and dust storm conditions has been presented. The model differs from previous descriptions around models in that it treats the description around a being a three-component mixture, with each component having its cwn size distribution and set of indices of refraction. Mass loading during dust storms has been incorporated into the model also. Results from the pretent model for dust storm conditions indicate more selective absorption of visible and near IR radiation when compared with previous description and set in the field of climate research.

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Appendix A

Aerosol Fractions by Volume as a Function of Wind Speed The introduction of mass loading into our model means that the aerosol fraction by volume of each component, C_i , depends on wind speed, u. The C_i 's can be calculated in a straight forward manner because all extra mass loading due to the wind is assumed to be sand. The first step is to determine the mass of each component per unit volume of air for background conditions (i.e., u = 0). To do this, let m_1, m_2 and m_3 be the mass of carbonaceous, water soluble and sand material per unit volume of air. Because the present desert aerosol model assumes that the mass of carbonaceous and water soluble material is independent of wind speed, these components will be called \overline{m}_1 and \overline{m}_2 , respectively. The mass of sand per unit volume of air depends on the wind speed (Eq. 5 of the text) and will be called $m_3(u)$. The total mass of the aerosol per unit volume of air, M(u), is then given by

$$M(u) = \overline{m_1} + \overline{m_2} + m_3(u)$$
 (A-1)

which can be written in terms of the density, ρ , and volume concentration, v, of each component

$$M(u) = \rho_1 \bar{v}_1 + \rho_2 \bar{v}_2 + \rho_3 v_3(u) . \qquad (A-2)$$

The definition of aerosol fraction by volume, $C_i = v_i/V$ where V is the total aerosol volume per unit volume of air, is then substituted into Eq. A-2 and solved for V

$$V(u) = M(u) / (C_1(u)\rho_1 + C_2(u)\rho_2 + C_3(u)\rho_3) . \qquad (A-3)$$

The total aerosol volume for background conditions, V(0), can be determined from Eq. A-3 using M(0) (Eq. 5 of the text) plus $C_{i}(0)$ and ρ_{i} from Table 4. It then follows that the mass, $m_{i}(0)$, and the volume concentration, $v_{i}(0)$, of each component is given by

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$$m_{\pm}(0) = C_{\pm}(0) V(0) \rho_{\pm}$$
 (A-4)

and

$$V_{i}(0) = C_{i}(0)V(0)$$
 (A-5)

where i = 1 to 3.

Having found \overline{v}_1 and \overline{v}_2 , the aerosol fractions by volume for each component can be computed for any wind speed. Specifically, Eq. A-2 is solved for $v_3(u)$ where M(u) is obtained from Eq. 5 of the text. The volume concentrations of the aerosol components are then converted to an aerosol fractions by volume using

 $C_{1,2}(u) = \overline{V}_{1,2}/V(u)$ (A-6)

and

$$C_{2}(u) = v_{2}(u)/V(u)$$
 (A-7)

where V(u) is the sum of \vec{v}_1 , \vec{v}_2 and $v_3(u)$.

A-2

Appendix B

Mie Scattering Calculations for the Three Components

This appendix gives the results of Mie calculations for the three components of the present desert aerosol model. Tables B-1 and B-2 give the results for the carbonaceous component and the water soluble component, respectively. In Tables B-3 through B-7, the results are given for the sand component at four wind speeds. Note that because of round-off, the radiative properties at some wavelengths are not internally consistent to the least significant digit. The calculations were performed using a number density of 1 particle per cm³ of air and the size distribution parameters given in Table 5 of the text. For reference, Table B-7 gives the surface area and volume of the aerosol components that correspond to a number density of 1 particle per cm³ of air. Table B-1. Mie Scattering Results for the Carbonaceous Component Normalized to 1 Particle cm⁻³. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied) 1:1

	ATTENUATION		<u></u>		
WAVELENGTH (_lm)	Extinction	Scattering	Absorption	۳ _o	g :
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.694 0.860 1.060 1.060 1.300 1.536 1.800 2.000 2.250 2.500 2.500 2.500 2.500 3.200 3.200 3.392 3.500 3.750 4.000 4.500 5.500 6.200 6.200 6.200 6.200 6.500 7.200 7.900 8.200 8.500 8.500 8.700	1.39(-6) 1.36 1.21 1.07 $8.61(-7)$ 6.59 6.14 5.54 4.50 3.97 2.97 2.29 1.80 1.49 1.27 1.14 1.01 $9.08(-8)$ 8.44 7.74 7.11 6.75 6.58 6.12 5.72 5.06 4.49 4.07 3.68 3.55 3.38 3.08 2.74 2.65 2.55 2.47	4.52(-7) 4.17 3.79 3.16 2.30 1.52 1.35 1.16 $8.19(-8)$ 6.48 3.61 1.96 1.06 $6.21(-9)$ 3.77 2.65 1.77 1.23 $9.44(-10)$ 6.54 5.23 4.27 3.86 3.04 2.43 1.58 1.08 $7.56(-11)$ 5.51 4.89 4.10 2.80 2.04 1.78 1.57 1.44	9.35(-7) 9.38 8.33 7.52 6.31 5.07 4.79 4.38 3.68 3.32 2.60 2.10 1.69 1.43 1.23 1.11 9.91(-8) 8.96 8.34 7.68 7.06 6.70 6.54 6.09 5.69 5.04 4.48 4.06 3.67 3.55 3.38 3.08 2.74 2.65 2.54 2.46	0.326 0.308 0.313 0.296 0.267 0.231 0.220 0.182 0.163 0.122 0.085 0.059 0.042 0.030 0.023 0.018 0.014 0.011 0.001 0.001 0.001 0.001 0.001	$\begin{array}{c} 0.581\\ 0.502\\ 0.454\\ 0.429\\ 0.396\\ 0.358\\ 0.358\\ 0.358\\ 0.311\\ 0.293\\ 0.253\\ 0.214\\ 0.179\\ 0.153\\ 0.253\\ 0.214\\ 0.179\\ 0.153\\ 0.131\\ 0.117\\ 0.103\\ 0.091\\ 0.083\\ 0.072\\ 0.065\\ 0.065\\ 0.055\\ 0.055\\ 0.055\\ 0.055\\ 0.055\\ 0.028\\ 0.027\\ 0.028\\ 0.027\\ 0.025\\ 0.021\\ 0.018\\ 0.017\\ 0.016\\ 0.015\end{array}$

B-2

Table B-1. (cont.)

	ATTENUATIO				
WAVELENGTE (µm)	Extinction	Scattering	Absorption	Wo	g
9.000 9.200 9.500 9.800 10.000 10.591 11.000 11.500 12.500 13.000 14.000 14.000 14.000 14.000 15.000 16.400 17.200 18.000 18.500 20.000 21.300 22.500 25.000 27.900 30.000 35.000 40.000 50.000 60.000 80.000 100.000 150.000 200.000	2.39(-8) 2.32 2.26 2.18 2.13 2.02 1.93 1.85 1.68 1.62 1.49 1.41 1.39 1.26 1.20 1.13 1.10 1.00 1.00 $9.42(-9)$ 8.85 7.92 7.05 6.51 5.50 4.70 3.76 3.13 2.35 1.88 1.25 $9.39(-10)$	1.27(-11) 1.17 1.04 $9.29(-12)$ 8.64 6.94 5.99 5.07 3.70 3.20 2.43 1.98 1.87 1.34 1.12 $9.45(-13)$ 8.52 6.39 5.01 4.07 2.72 1.78 1.36 $7.58(-14)$ 4.56 1.87 $9.00(-15)$ 2.85 1.17 $2.30(-16)$ $7.29(-17)$	2.39(-8) 2.32 2.25 2.18 2.13 2.02 1.93 1.85 1.68 1.62 1.49 1.41 1.39 1.26 1.20 1.13 1.10 1.00 9.42(-9) 8.85 7.92 7.05 6.51 5.50 4.70 3.76 3.13 2.35 1.88 1.25 9.39(-10)		$\begin{array}{c} 0.015\\ 0.014\\ 0.013\\ 0.013\\ 0.012\\ 0.012\\ 0.010\\ 0.009\\ 0.009\\ 0.009\\ 0.009\\ 0.009\\ 0.009\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.007\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.002\\ 0.002\\ 0.002\\ 0.001\\ 0.000\\ 0.$

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Table B-2. Mie Scattering Results for the Water Soluble Component Normalized to 1 Particle cm⁻³. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied)

	ATTENUATIO	************************			
WAVELENGT'H (µm)	Bxtinction	Scattering	Absorption	Wo	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.000 2.250 2.500 2.500 2.500 2.500 3.200 3.200 3.200 3.392 3.500 3.750 4.000 5.500 5	2.33(-5) 2.13 1.89 1.74 1.51 1.23 1.14 1.05 8.52(-6) 7.47 5.31 3.5° 2.29 1.54 1.03 7.72(-7) 5.53 3.81 2.83 7.69 1.71(-6) 1.14 9.49(-7) 3.67 2.11 1.16 7.70(-8) 5.87 5.96 7.02 1.64(-7) 9.95 1.90 3.14 8.04 2.13(-6)	2.33 (-5) 2.13 1.89 1.74 1.51 1.23 1.14 1.05 8.52 (-6) 7.47 5.31 3.55 2.29 1.54 1.03 7.61 (-7) 5.42 3.78 2.67 9.88 (-8) 2.00 (-7) 2.40 2.24 1.87 1.45 8.55 (-8) 5.23 3.07 1.69 1.19 3.95 (-9) 5.29 (-8) 6.96 (-9) 1.80 3.53 1.89 (-8)	2.36 (-11) 1.84 1.47 1.32 1.04 9.18 (-12) 7.51 7.20 5.70 5.04 5.64 5.03 (-11) 3.57 (-10) 1.28 (-9) 1.02 1.16 (-8) 1.10 3.06 (-9) 1.60 (-8) 6.70 (-7) 1.51 (-6) 9.05 (-7) 7.25 1.80 6.60 (-8) 3.07 2.47 2.80 4.27 5.83 1.60 (-7) 9.43 1.83 3.12 8.00 2.01 (-6)	1.00C 1.000 0.999 0.944 0.129 0.510 0.523 0.024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0024 0.0004 0.0000	$\begin{array}{c} 0.658\\ 0.654\\ 0.656\\ 0.652\\ 0.645\\ 0.635\\ 0.635\\ 0.637\\ 0.627\\ 0.620\\ 0.580\\ 0.556\\ 0.534\\ 0.510\\ 0.493\\ 0.454\\ 0.510\\ 0.493\\ 0.473\\ 0.454\\ 0.391\\ 0.343\\ 0.355\\ 0.356\\ 0.355\\ 0.356\\ 0.353\\ 0.355\\ 0.356\\ 0.353\\ 0.307\\ 0.284\\ 0.250\\ 0.223\\ 0.190\\ 0.168\\ 0.126\\ 0.091\\ \end{array}$

B-4

Table B-2. (cont.)

	ATTENUATIO				
WAVELENGTH (µm)	Extinction	Scattering	Absorption	W _o	g
9.000 9.200 9.500 9.500 9.500 10.000 10.591 11.000 11.500 12.500 13.000 14.000 14.000 14.800 15.000 16.400 17.200 18.000 18.500 20.000 21.300 22.500 25.000 25.000 25.000 25.000 35.000 40.000 50.000 50.000 60.000 80.000 150.000 150.000 200.000 300.0000 300.000 300.0000 300.0000 300.0000 300.0000 300.0000 300.0000 300.0000 300.0000 300.0000 300.0000 300.00000 300.0000 300.0000 300.0000	3.62(-6) 1.42 $4.72(-7)$ 2.41 1.59 $7.94(-8)$ 6.17 4.02 2.81 2.67 2.46 2.83 3.05 $2.21(-7)$ $3.81(-8)$ 2.01 1.63 1.55 1.84 2.27 3.30 5.95 $1.07(-7)$ 2.96 2.39 1.91 1.59 1.19 $9.53(-8)$ 6.35 4.76 3.17	1.08(-7) $6.55(-8)$ 4.09 3.03 2.36 1.45 1.13 $8.59(-9)$ 5.21 4.19 2.65 1.65 1.42 5.97 2.93 1.50 1.19 $7.48(-10)$ 5.28 3.82 2.12 $9.97(-11)$ 5.60 $1.03(-10)$ 1.83 $7.53(-11)$ 3.63 1.14 $4.67(-12)$ $9.18(-13)$ 2.90 $5.71(-14)$	3.51(-6) 1.35 $4.32(-7)$ 2.11 1.36 $6.49(-8)$ 5.04 3.16 2.29 2.25 2.20 2.66 2.91 $2.15(-7)$ $3.51(-8)$ 1.86 1.51 1.48 1.79 2.23 3.28 5.94 $1.07(-7)$ 2.96 2.39 1.91 1.59 1.91 1.59 1.19 $9.53(-8)$ 6.35 4.76 3.17	$\begin{array}{c} 0.030\\ 0.046\\ 0.087\\ 0.125\\ 0.148\\ 0.183\\ 0.182\\ 0.214\\ 0.185\\ 0.157\\ 0.108\\ 0.058\\ 0.046\\ 0.027\\ 0.077\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.075\\ 0.073\\ 0.007\\ 0.007\\ 0.000\\ 0.$	0.046 0.067 0.185 0.217 0.215 0.201 0.191 0.162 0.153 0.153 0.122 0.137 0.122 0.137 0.122 0.137 0.122 0.137 0.093 0.093 0.083 0.075 0.061 0.027 0.028 0.020 0.003 0.002 0.001

Table B-3. Mie Scattering Results for the Sand Component With a 0 ms⁻¹ Wind Normalized to 1 Particle cm⁻³. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value) given, then the previous power of 10 is implied)

	ATTENUATIO		•		
WAVELENGTE	Extinction	Scattering	Absorption	Work	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.250 2.500 2.500 2.500 2.500 3.200 3.200 3.200 3.392 3.500 3.750 4.000 4.500 5.500 5.500 6.000 5.500 5.500 5.000 5.500 5.000 5.500 5.000 5.500 5.000 5.500 5.000 5.500 5.500 6.000 5.500 5.500 6.000 5.500 5	5.62(-1) 5.64 5.65 5.66 5.68 5.70 5.71 5.71 5.73 5.74 5.78 5.82 5.86 5.91 5.92	$\begin{array}{c} 4.38(-1)\\ 4.40\\ 4.40\\ 4.40\\ 4.41\\ 4.45\\ 4.48\\ 4.57\\ 5.37\\ 5.70\\ 5.63\\ 5.86\\ 5.91\\ 5.95\\ 5.95\\ 5.95\\ 5.91\\ 5.95\\ 6.00\\ 6.11\\ 6.14\\ 6.17\\ 6.22\\ 6.22\\ 6.24\\ 8.25\\ 5.48\\ 5.65\\ 5.79\\ 5.65\\ 5.71\\ 6.07\\ 4.05\\ 5.36\\ 5$	1.24(-1) $1.24(-1)$ 1.24 1.25 1.25 1.25 1.23 1.14 $3.60(-2)$ $4.58(-3)$ $1.51(-2)$ $1.19(-4)$ $3.72(-5)$ 1.59 1.25 1.19 $1.269(-4)$ $2.69(-4)$ $2.69(-4)$ 2.99 3.49 $1.97(-3)$ 2.51 $1.33(-2)$ 9.99 9.60 9.74 $1.13(-1)$ $9.09(-2)$ $1.20(-1)$ 1.37 $8.03(-2)$ $1.06(-1)$ 1.63	0.780 0.780 0.780 0.779 0.779 0.778 0.780 0.785 0.801 0.937 0.992 0.974 1.000 0.998 1.000 0.9997 0.9997 0.855 0.855 0.855 0.855 0.875 0.875 0.758 0.756	0.784 0.798 0.802 0.802 0.802 0.802 0.801 0.798 0.795 0.795 0.795 0.795 0.795 0.7768 0.7763 0.7763 0.7763 0.7763 0.7763 0.7763 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.8310 0.8327 0.5763 0.5763 0.5780 0.5783 0.5784 0.57763 0.5783 0.57783 0.5783 0.57783 0.57783 0.57783 0.5783 0.57783 0.57783 0.57783 0.57783 0.57783 0.57783 0.57783 0.5783 0.5783 0.57783 0.5783 0.

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	ATTENUATIO	N COEFFICIE	NTS (km ⁻¹)		
NAVELENGTH (1 cm)	Bxtinction	Scattering	Absorption	Wa	g
9.000	8.36(-1)	7.52(-1)	8.34(-2)	0.900	0.57
9.200	/.U8 6 52	0.41 4 14	0.68 2 38(m1)	0,906	0.55
9.800	6.67	4.08	2.59	0.611	0.72
10.000	6.74	4.33	2.41	0.642	0.70
10.591	6.87	5,07	1.79	0.739	0.65
11.000	6,98	5.41	1.57	0.776	0.64
11,500	7.12	5.53	1.59	0.777	0.66
12.500	7.11	4.35	2.76	0.607	0.75
13.000	7.06	4.28	2.78	0.606	0.71
14.000	7.40	5.4/ % 00	1.99	0.734	0.665
15.000	7.62	5.60	1.77	0.700	0.04.
16.400	6.49	4,50	1.99	0.652	0.72
17.200	6.54	4,32	2.22	0.638	0.81
18.000	6.35	4,60	1.75	0.731	0.80
18.500	5.76	4.21	1.54	0.727	0.810
20.000	6,81	5,86	9.44(-2)	0,862	0.52
21.300	8.92	7.12	1.81(-1)	0.780	0.53
22.500	7.19	4.63	2.55	0.645	0.54
23.000	8.2/	5.16	3,11	0.622	0.654
30 000	7.91	4,93	2,00	0.045	0.454
35.000	R 24	7 28	2.20	0.701	0.41
40.000	8.34	7.85	4.92	0.941	0.385
50.000	8.12	7,90	2.21	0.973	0.386
60.000	7.53	7.40	1.26	0.984	0,395
80.000	6.04	5,95	9.34(-3)	0.985	0,404
00.000	4.64	4.61	2.54	0,995	0.404
50.000	2.33	2.33	9.06(-4)	0.996	0.396
00.000	1.20	1.20	4.02	0.997	0.378
00.000	3,72(-2)	3.71(-2)	1,45	0.996	0.330

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Table B-4. Mie Scattering Results for the Sand Component With a 10 ms Wind Normalized to 1 Particle cm . The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied)

****	ATTENUATIO				
WAVELENGTH (µm)	Extinction	Scattering	Absorption	۷o	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.960 1.060 1.300 1.536 1.800 2.250 2.250 2.500 2.250 2.500 3.200 3.200 3.200 3.200 3.200 3.500 3.500 3.500 5.500 5.500 5.500 5.500 5.500 3.200 3.200 3.200 3.200 3.200 3.500 3.500 5	1.22(0) 1.23 1.23 1.23 1.23 1.24 1.24 1.24 1.24 1.24 1.24 1.25 1.26 1.26 1.26 1.26 1.27 1.28 1.28 1.29 1.30 1.30 1.30 1.31 1.31 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.33 1.34 1.35 1.37 1.38 1.39 1.41 1.29 1.23 1.33 1.50 1.50	9.55(-1) 9.57 9.59 9.59 9.61 5.65 9.67 9.78 1.13(0) 1.23 1.20 1.26 1.26 1.26 1.26 1.26 1.27 1.28 1.20 1.28 1.20 1.30 1.30 1.31 1.32 1.29 1.05 1.07 1.09 1.12 9.11 1.16(0) 1.31 1.20	2.69(-1) 2.69 2.71 2.72 2.73 2.73 2.71 2.62 1.18 $1.80(-2)$ 5.50 $4.53(-4)$ 1.31 $6.54(-5)$ 3.93 3.98 3.94 $1.64(-4)$ 2.19 $3.54(-3)$ 1.06 1.02 1.32 7.46 9.55 $4.83(-2)$ $3.02(-1)$ 2.99 3.40 2.88 3.71 3.22 1.67 1.83 3.01	0.780 0.780 0.780 0.779 0.779 0.780 0.780 0.780 0.780 0.780 0.780 0.905 0.986 1.000 0.9999 0.9999 0.9999 0.9999 0.7755 0.7856 0.7755 0.7856 0.7960 0.7950	0.785 0.796 0.801 0.805 0.807 0.806 0.807 0.808 0.808 0.808 0.808 0.809 0.809 0.7995 0.7995 0.7795 0.7795 0.7789 0.7789 0.7789 0.7789 0.7789 0.7789 0.7789 0.8512 0.8067 0.802 0.7795 0.7789 0.7789 0.8512 0.8574 0.8986 0.8067 0.8578 0.8578 0.8579 0.8579 0.8579 0.8579 0.8578 0.8579 0.8579 0.8579 0.8579 0.8579 0.8579 0.8579 0.8574 0.580 0.580 0.580 0.580

Table B-4. (cont.)

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	ATTENUATION		4		
WAVEJ-ENGTH (µm)	Extinction	Scattering	Absorption	• •	g
9.000 9.200 9.500 9.800 10.000 10.591 11.000 11.500 12.500 13.000 14.800 14.800 15.000 16.400 17.200 18.000 16.400 17.200 18.000 20.000 21.300 22.500 25.000 27.900 30.000 35.000 40.000 50.000 50.000 100.000 100.000 10.000 10.000 100.0000 100.000 100.0000 100.0000 100.0000 100.0000 100.0000 100.0000 100.0000 100.0000 100.00000 100.0000 100.00000 100.00000 100.0000	1.66(D) 1.49 1.37 1.39 1.40 1.42 1.43 1.45 1.49 1.45 1.49 1.51 1.52 1.40 1.42 1.42 1.42 1.51 1.52 1.40 1.42 1.42 1.42 1.51 1.52 1.40 1.42 1.55 1.57 1.64 1.69 1.73 1.74 1.67 1.54 1.18 8.67(-1) 4.76	1.51(0) 1.35 $8.93(-1)$ 8.48 8.69 9.71 $1.02(0)$ 1.03 $9.23(-1)$ 8.55 9.93 $1.05(0)$ 1.09 $9.26(-1)$ 9.06 9.88 9.85 $1.28(0)$ 1.43 $9.68(-1)$ $1.08(0)$ $9.97(-1)$ $1.09(0)$ 1.39 1.54 1.66 1.69 1.53 1.18 $8.64(-1)$ 4.74	1.53(-1) 1.37 4.78 5.45 5.35 4.50 4.10 4.19 5.65 5.95 4.99 4.61 4.30 4.77 5.09 4.61 4.30 4.77 5.09 4.35 3.89 1.83 3.53 5.12 6.16 5.55 4.76 2.59 1.49 $7.52(-2)$ 4.86 4.21 1.36 $6.03(-3)$ 3.31 1.46	0.908 0.908 0.651 0.609 0.619 0.714 0.711 0.617 0.631 0.631 0.631 0.631 0.631 0.631 0.631 0.631 0.631 0.631 0.634 0.715 0.634 0.6554 0.641 0.634 0.654 0.641 0.659 0.634 0.6554 0.641 0.659 0.641 0.634 0.6554 0.643 0.6554 0.644 0.9572 0.9572 0.9955 0.9956 0.9975 0.9997	0.581 0.564 0.712 0.769 0.766 0.734 0.726 0.723 0.774 0.773 0.752 0.752 0.752 0.758 0.836 0.833 0.561 0.598 0.624 0.5517 0.461 0.444 0.415 0.409 0.401

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Table B-5. Mie Scattering Results for the Sand Gomponent With a 20 ma $^{-1}$ Wind Normalized to 1 furticle cm $^{-1}$. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied) COMPANY STATES

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,	in a suite	ATTENUAT10	N COEFFICIE	NTS (km ⁻¹)	No. The R.	an in an an a	n an
	WAVELENGTH (µm)	Extinction	Scattering	Absorption	W _O	g	
· · · · · · · · · · ·	0.200	2.61(0)	2.03(0)	5,73(-1)	0.780	0.787	
	0.250	2.61	2.04	5.73	0.780	0.798	
	0.300	2.61	2.04	5.75	0.780	0.803	
	0.337	2.62	2.04	5.77	0.780	0.80	
	0.400	2.62	2.04	5.80	0.779	0.809	
	0.488	2.63	2.05	5.79	0.780	0.810	
	0.515	2.63	2.05	5.78	0.780	0.811	
	0.550	2.63	2.06	5.70	0.784	0.811	
	0.633	2.63	2.29	3.44	0.870	0.811	
	0.694	2.64	2.57	6.86(-2)	0.974	0.811	
	0.860	2.65	2.46	1.87(-1)	0.930	0.810	
	1.060	2.66	2.65	1.85(-3)	1.000	0.809	
	1.300	2.67	2.66	5.28(-4)	1.000	0.807	
	1.536	2.68	2.68	2.53	1.000	0.807	
	1,800	2.69	2.69	1.62	1.000	0.806	
	2.000	2.69	2.69	1.63	1.000	0.804	
	2.250	2.70	2.70	1.58	1.000	0.804	
	2.500	2.71	2.71	6.43	1.000	0.804	
	2.700	2.72	2.72	8.50	1.000	0.803	
	3.000	2.73	2.72	1.41(-2)	0.995	0.804	
	3.200	2.73	2.73	4.01(-3)	0.998	0.805	
	3.392	2.75	2.74	4.00	0.999	0.803	
	3.500	2.75	2.74	5.18	0.998	0.804	
	3.750	2.76	2.73	2,76(-2)	0.990	0.807	
	4.000	2.76	2.73	3.60	0.987	0.810	
	4.500	2.78	2.60	1,73(-1)	0.938	0.825	
	5.000	2.80	1.98	8.22	0.706	0.883	
	5.500	2.82	2.01	8.09	0.713	0.887	
	6.000	2.83	2.01	8.21	0.710	0.895	
	6.200	2.85	1.94	9.08	0.681	0.909	
	6.500	2.87	2.06	8.08	0.718	0.913	
	7.200	2.81	1.82	9.90	0.648	0.988	
	7.900	2.66	1.94	7.16	0.730	0.808	
	8.200	2.78	2.44	3.43	0.877	0.613	
	8,500	3.00	2.67	3.27	0.892	0.570	
	8.700	3.01	2.45	5.65	0.811	0.573	

	ATTRNIATIO	CORPETCIE	NTS (km ⁻¹)		
WAVELENGTH (1) m)	Bxtinction	Scattering	Absorption	₩0	g
9.000 9.200 9.500 9.500 10.000 10.591 11.000 11.500 12.500 13.000 14.000 14.800 15.000 16.400 17.200 16.400 17.200 16.400 17.200 18.000 16.400 21.300 22.500 25.000 27.900 30.000 35.000 40.000 50.000 80.000 100.000 150.000	3.25(0) 3.06 2.84 2.87 2.88 2.90 2.92 2.94 3.03 2.95 3.00 3.02 3.03 2.95 2.96 2.96 3.02 3.01 3.37 3.12 3.14 3.24 3.32 3.42 3.42 3.42 3.54 3.54 3.28 2.92	2.98(0) 2.78 1.88 1.76 1.75 1.86 1.93 1.93 1.93 1.93 1.93 1.93 1.93 1.93	2.71(-1) 2.75 9.57 $1.11(0)$ 1.12 1.04 $9.88(-1)$ $1.01(0)$ 1.12 1.23 1.14 1.09 1.04 1.09 1.04 1.09 1.13 $9.97(-1)$ 9.13 3.54 6.75 $1.02(0)$ 1.18 1.13 $9.86(-1)$ 6.35 4.17 2.27 1.51 1.41 $5.13(-2)$ 2.67 1.72	0.917 0.910 0.663 0.613 0.610 0.642 0.661 0.655 0.628 0.655 0.628 0.618 0.640 0.657 0.619 0.613 0.664 0.657 0.619 0.6613 0.666 0.692 0.6883 0.664 0.664 0.664 0.664 0.664 0.664 0.6686 0.797 0.874 0.987 0.9957 0.994	$\begin{array}{c} 0.576\\ 0.567\\ 0.721\\ 0.789\\ 0.802\\ 0.795\\ 0.791\\ 0.807\\ 0.784\\ 0.821\\ 0.821\\ 0.790\\ 0.777\\ 0.805\\ 0.821\\ 0.790\\ 0.777\\ 0.805\\ 0.842\\ 0.777\\ 0.805\\ 0.623\\ 0.623\\ 0.623\\ 0.623\\ 0.631\\ 0.603\\ 0.517\\ 0.485\\ 0.453\\ 0.422\\ 0.417\\ \end{array}$

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Table B-6. Mie Scattering Results for the Sand Component With a 30 ms⁻¹ Wind Normalized to 1 Particle cm⁻³. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied)

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	ATTENUATIO	N COEFFICIE	NTS (km ⁻¹)		
WAVELENGTH (1m)	Extinction	Scattering	Absorption	- Wo	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.000 2.250 2.500 2.500 2.500 3.200 3.200 3.392 3.500 3.750 4.000 4.500 5.500 6.200 5.500 6.200 7.200 7.200 7.200 7.200 8.200 8.500 8.700	5.60(0) 5.61 5.62 5.62 5.62 5.63 5.63 5.64 5.65 5.65 5.66 5.68 5.70 5.72 5.72 5.77 5.77 5.77 5.77 5.77 5.77 5.77 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.81 5.91 5.95 5.91 5.95 5.97 5.98 5.91 5.95 5.97 5.98 5.95 5.97 5.98 5.91 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.95 5.97 5.98 5.97 5.98 5.97 5.98 5.97 5.98 5.97 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.98 5.72 5.89 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.80 5.80 5.80 5.72 5.80 5.80 5.80 5.90 5.80 5.90 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.80 5.72 5.90 5.72 5.90 5.72 5.90 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5	4.37(0) 4.38 4.38 4.38 4.39 4.39 4.39 4.40 4.72 5.40 5.07 5.67 5.67 5.69 5.70 5.72 5.74 5.75 5.76 5.77 5.75 5.76 5.77 5.78 5.70 5.72 5.70 5.72 5.70 5.72 5.73 5.78 5.70 5.72 5.70 5.72 5.72 5.70 5.72 5.72 5.72 5.70 5.72 5.72 5.72 5.72 5.72 5.72 5.72 5.72	1.23(0) 1.23 1.24 1.24 1.24 1.24 1.24 1.24 1.23 $9.21(-1)$ 2.55 5.92 $7.60(-3)$ 2.14 1.03 $6.58(-4)$ 6.80 6.58 $2.61(-3)$ 3.52 $5.59(-2)$ 1.62 1.60 2.07 $1.09(-1)$ 1.41 6.15 $2.09(0)$ 2.08 2.11 2.25 2.10 2.44 1.58 $7.18(-1)$ 6.18 $1.10(0)$	0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.955 0.896 1.0000 0.9997 0.9977 0.9976 0.644 0.645 0.878 0.878 0.990 0.990 0.990 0.990 0.995 0.644 0.645 0.645 0.645 0.645 0.645 0.645 0.878 0.878 0.900 0.821	0.788 0.799 0.804 0.808 0.810 0.812 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.813 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.812 0.813 0.814 0.812 0.812 0.813 0.812 0.813 0.812 0.813 0.813 0.813 0.812 0.813 0.813 0.813 0.812 0.813 0.814 0.812 0.813 0.814 0.813 0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.850 0.824 0.913 0.925 0.935 0.935 0.993 0.935 0.990 0.808 0.990 0.808 0.995 0.956 0.956 0.565

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Table B-6. (Cont.)

	ATTBNUATIO	N COEFFICIE	NTS (km ⁻¹)		
WAVELENGTH (µm)	Extinction	Scattering	Absorption	W o	g
9.000 9.200 9.500 9.800 10.000 10.591 11.000 12.500 12.500 13.000 14.000 14.000 14.800 15.000 16.400 17.200 18.000 18.500 20.000 21.300 22.500 25.000 25.000 27.900 30.000 35.000 40.000 50.000 60.000 150.0000 150.0000 150.0000 150.0000 150.0000 150.0000 150.0000 150.00000 150.0000 150.0000 150.00000 150.000	6.53(0) 6.36 5.97 6.01 6.02 6.08 6.10 6.26 6.12 6.12 6.23 6.23 6.23 6.23 6.23 6.24 6.24 6.31 6.24 6.31 6.99 6.24 6.77 6.41 6.59 6.70 6.88 7.01 7.24 7.35 7.41 7.22 6.53	6.04(0) 5.80 4.01 3.72 3.66 3.73 3.80 3.75 4.00 3.59 3.64 3.75 3.64 3.75 3.64 3.67 3.61 5.69 4.19 4.34 4.96 5.54 6.19 6.53 6.79 7.18 7.15 6.49	4.87(-1) 5.55 1.96(0) 2.29 2.36 2.33 2.29 2.34 2.25 2.54 2.54 2.54 2.54 2.47 2.41 2.45 2.51 2.23 2.07 7.03(-1) 1.30(0) 2.05 2.28 2.33 2.10 1.64 1.16 6.87(-1) 4.78 4.50 1.73 1.04 7.17(-2) 4.25	0.925 0.912 0.673 0.619 0.609 0.615 0.624 0.638 0.589 0.603 0.614 0.595 0.641 0.668 0.595 0.641 0.668 0.668 0.6637 0.6597 0.672 0.675 0.674 0.932 0.938 0.9994	0.566 0.564 0.724 0.799 0.833 0.835 0.855 0.788 0.842 0.843 0.843 0.833 0.852 0.864 0.843 0.850 0.850 0.850 0.581 0.640 0.747 0.689 0.620 0.5534 0.5534 0.5534 0.5534 0.5534 0.5532 0.483 0.427

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Table B-7. Surface Area and Volume of Each Aerosol Component of the Desert Aerosol Model Ler Unit Volume of Air for a Number Density of 1 Particle cm

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Aerosol Component ()	Surface Area m ² cm ⁻³ of Air)	Volume (µm ³ cm ⁻³ of Air)		
Carbonaceous	1.14 × 10 ⁻³	5.97 X 10 ⁻⁵		
Water Soluble	9.35 x 10 ⁻³	1.80 X 10 ⁻³		
Sand: 0 ms ⁻¹ Wind	2.76 X 10 ²	6.30 X 10 ³		
Sand: 10 ms ⁻¹ Wind	6.04 X 10 ²	2.66 X 10 ⁴		
Sand: 20 ms ⁻¹ Wind	1.29 X 10 ³	1.12 x 10 ⁵		
Sand: 30 ms ⁻¹ Wind	2.78 X 10 ³	4.76 X 10 ⁵		

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Appendix C

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Radiative Properties of the Desert Aerosol Model as a Function of Wind Speed

This appendix gives the tabulated radiative properties of the present desert aerosol model. Tables C-1 through C-4 give values for wind speeds of 0, 10, 20 and 30 ms⁻¹ respectively. As discussed in the main text, these results were obtained using sand component that is a mixture of quartz particles and quartz particles contaminated with hematite. Note because of round-off, the radiative properties at some wavelengths are not internally consistent to the least significant digit.

For reference, Tables C-5 through C-7 give the angular scattering, P, of the desert aerosol model for wavelengths of 0.55, 1.06 and 10.591 m respectively. Figures C-1 through C-3 present these results in pictorial form. The method of determining the angular scattering for a multicomponent mixture of particles is similar to that for the asymmetry parameter which was described in Section 3.4 of the main text. The values have been normalized so that

 $\frac{1}{4\pi}\int \mathbf{P}(\theta)d\theta = 1 \qquad (C-1)$

where θ is the solid angle.

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Table C-1. Radiative Properties of the Desert Aerosol for 0 ms⁻¹ Wind Speed Conditions. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied)

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	ATTENUATION COEFFICIENTS (km ⁻¹)				
WAVELENGTH	Extinction	Scattering	Absorption	va	9
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.250 2.500 2.500 2.500 2.500 3.200 3.200 3.392 3.500 3.750 4.000 5.500 5.500 6.200 5.500 6.200 7.200 7.200 7.200 8.500 8.700	8.73(-2) 7.99 7.13 6.58 5.70 4.68 4.33 4.01 3.28 2.90 2.10 1.45 9.90(-3) 7.16 5.27 4.35 3.55 2.92 2.57 4.36 7.83 5.75 5.03 2.91 2.34 2.01 1.89 1.89 1.95 2.33 4.95 2.33 4.95 2.33 4.95 2.05 2.67 4.79 9.28	8.67(-2) 7.93 7.07 6.52 5.65 4.63 4.28 3.96 3.26 2.88 2.09 1.45 9.84(-3) 7.10 5.22 4.26 3.47 2.88 2.48 1.87 2.25 2.40 2.35 2.22 2.07 1.85 1.54 1.50 1.48 1.50 1.19 1.04 1.32 1.58].50	6.49(-4) 6.51 6.14 5.86 5.43 4.94 4.79 4.42 2.25 1.34 1.33 7.81(-5) 6.41 5.76 4.93 8.38 7.70 4.45 8.96 2.49(-3) 5.58 3.34 2.69 6.88(-4) 2.69 1.64 3.52 3.53 4.09 5.05 8.21 3.76(-3) 1.02 1.35 3.20 7.78	0.993 0.991 0.991 0.9991 0.9990 0.989 0.989 0.9993 0.9993 0.9993 0.9993 0.9993 0.9993 0.9993 0.9994 0.9994 0.9991 0.9991 0.9991 0.9991 0.9991 0.9991 0.9992 0.9993 0.9933 0.993	$\begin{array}{c} \textbf{C.660}\\ \textbf{0.657}\\ \textbf{0.658}\\ \textbf{0.655}\\ \textbf{0.649}\\ \textbf{0.642}\\ \textbf{0.638}\\ \textbf{0.638}\\ \textbf{0.638}\\ \textbf{0.622}\\ \textbf{0.638}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.583}\\ \textbf{0.631}\\ \textbf{0.631}\\ \textbf{0.6482}\\ \textbf{0.631}\\ \textbf{0.6482}\\ \textbf{0.730}\\ \textbf{0.6482}\\ \textbf{0.757}\\ \textbf{0.842}\\ \textbf{0.831}\\ \textbf{0.614}\\ \textbf{0.593}\\ \textbf{0.617} \end{array}$

a Table C-1. (cont.). The second of a second s

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WAVELENGTH	Extinction	Scattering	Absorption	W o	g
9.000 9.200 9.500 9.500 9.800 10.000 10.591 11.000 12.500 13.000 14.000 14.800 15.000 16.400 17.200 18.000 18.000 21.300 22.500 25.000 27.900 30.000 35.000 40.000 50.000 50.000 100.000 50.000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.00000 30.0000 30.0000 30.0000 30.0000 30.0000 30.0000 30.00000 30.00000 30.00000 30.00000 30.000000 30.00000000000000000000000000000000000	1.54(-2) $6.94(-3)$ 3.34 2.53 2.25 1.98 1.95 1.90 1.86 1.84 1.93 1.97 1.99 2.41 1.75 1.64 1.48 1.73 2.26 1.85 2.15 2.09 2.30 3.11 2.93 2.69 2.43 1.92 1.49 $8.06(-4)$ 4.70 2.08	2.24(-3) 1.81 1.17 1.11 1.5 1.30 1.37 1.39 1.09 1.06 1.35 1.43 1.48 1.13 1.48 1.13 1.48 1.13 1.07 1.14 1.04 1.44 1.75 1.14 1.04 1.44 1.75 1.14 1.27 1.21 1.35 1.79 1.93 1.94 1.82 1.46 1.13 $5.71(-4)$ 2.94 $9.09(-5)$	1.31(-2) $5.13(-3)$ 2.18 1.42 1.10 $6.86(-4)$ 5.76 5.13 7.68 7.72 5.74 5.38 5.06 $1.28(-3)$ $6.78(-4)$ 5.02 4.38 2.90 5.12 7.12 8.86 8.79 9.55 $1.32(-3)$ 1.00 $7.56(-4)$ 6.16 4.61 3.56 2.36 1.76 1.17	$\begin{array}{c} 0.146\\ 0.261\\ 0.349\\ 0.439\\ 0.511\\ 0.654\\ 0.704\\ 0.730\\ 0.586\\ 0.580\\ 0.702\\ 0.726\\ 0.745\\ 0.612\\ 0.693\\ 0.745\\ 0.612\\ 0.693\\ 0.773\\ 0.615\\ 0.588\\ 0.579\\ 0.588\\ 0.579\\ 0.585\\ 0.574\\ 0.658\\ 0.719\\ 0.747\\ 0.760\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.761\\ 0.763\\ 0.437\\ \end{array}$	0.489 0.492 0.633 0.676 0.6633 0.650 0.747 0.711 0.678 0.671 0.675 0.754 0.675 0.754 0.531 0.552 0.5570 0.5531 0.5531 0.5531 0.5531 0.5533 0.470 0.385 0.372 0.363 0.369 0.377 0.364 0.328

Table C-2. Radiative Properties of the Desert Aerosol for 10 ms⁻¹ Wind Speed Conditions. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied) and the second secon

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	ATTENUATION COEFFICIENTS (km ⁻¹)			- <u></u>	
WAVELENGTH ()m)	Extinction	Scattering	Absorption	Wo	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.060 1.300 1.536 1.800 2.250 2.250 2.500 2.250 2.500 3.000 3.200 3.200 3.392 3.500 3.750 4.000 5.500 5	1.04(-1) 9.68(-2) 8.83 8.27 7.40 6.39 6.03 5.71 5.00 4.61 3.82 3.18 2.73 2.46 2.29 2.20 2.13 2.07 2.04 2.23 2.59 2.31 2.06 2.04 2.05 2.08 2.16 2.09 2.16 2.29 1.91 2.09 2.53 2.98	9.98(-2) 9.25 8.39 7.84 6.97 5.96 5.61 5.31 4.81 4.57 3.73 3.17 2.72 2.46 2.28 2.19 2.12 2.07 2.03 1.98 2.03 2.05 2.04 2.03 2.05 2.04 2.03 2.05 1.599 1.61 1.62 1.57 1.67 1.396 1.73 1.96 1.80	4.36(-3) $4.36(-3)$ $4.36(-3)$ $4.36(-3)$ $4.25(-3)$ $4.21(-4)$ $9.16(-5)$ $6.59(-5)$ $6.59(-5)$ $6.59(-5)$ $6.59(-5)$ $7.94(-4)$ $4.68(-5)$ $7.94(-4)$ $4.66(-3)$ $4.62(-3)$	0.958 0.955 0.951 0.948 0.933 0.930 0.9922 0.9922 0.9997 0.9997 0.9998 0.9999 0.9998 0.9988 0.7778 0.7748 0.7730 0.826 0.99888 0.9988 0.9988 0.9988 0.99888 0.99888	$\begin{array}{c} 0.684\\ 0.683\\ 0.688\\ 0.688\\ 0.688\\ 0.6887\\ 0.6922\\ 0.6994\\ 0.6994\\ 0.6997\\ 0.7728\\ 0.7757\\ 0.7757\\ 0.7757\\ 0.7759\\ 0.7759\\ 0.88462\\ 0.8862\\ 0.8862\\ 0.8862\\ 0.8862\\ 0.8862\\ 0.8862\\ 0.8859\\ 0.6295\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0.642\\ 0.5952\\ 0$

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	ATTENUATION	N COEFFICIE	NTS (km ⁻¹)		
WAVELENGTH (1mm)	Extinction	Scattering	Absorption		
9.000 9.200 9.500 9.800 10.000 10.591 11.000 12.500 13.000 14.000 14.800 15.000 16.400 17.200 18.000 18.500 20.000 21.300 22.500 25.000 27.900 30.000 50.000 40.000 50.000 80.000 150.000 300.000 300.000	3.80(-2) 2.73 2.22 2.16 2.15 2.15 2.16 2.17 2.23 2.17 2.23 2.26 2.27 2.17 2.12 2.13 2.05 2.18 2.67 2.21 2.55 2.33 2.38 2.56 2.60 2.65 2.65 2.65 2.65 2.65 2.65 2.65 2.53 2.33 1.78 1.31 $7.20(-3)$	2.28(-2) 2.03 1.35 1.27 1.30 1.45 1.53 1.54 1.38 1.27 1.48 1.56 1.62 1.38 1.35 1.47 1.47 1.47 1.47 1.47 1.47 1.47 1.47 1.47 1.42 1.62 1.49 1.63 2.06 2.29 2.47 2.52 2.43 2.28 1.75 1.29 $7.06(-3)$	1.52(-2) $7.00(-3)$ 8.72 8.90 8.47 6.95 6.30 6.37 8.50 8.95 7.52 6.96 6.52 7.90 7.72 6.55 5.85 2.78 5.33 7.72 9.30 8.48 7.48 4.95 3.10 1.82 1.31 1.07 $5.52(-4)$ 3.23 2.24 1.38	$\begin{array}{c} 0.601\\ 0.744\\ 0.607\\ 0.589\\ 0.606\\ 0.676\\ 0.708\\ 0.707\\ 0.618\\ 0.587\\ 0.663\\ 0.692\\ 0.713\\ 0.636\\ 0.636\\ 0.636\\ 0.636\\ 0.635\\ 0.635\\ 0.635\\ 0.635\\ 0.635\\ 0.6851\\ 0.635\\ 0.635\\ 0.6851\\ 0.951\\ 0.951\\ 0.958\\ 0.951\\ 0.958\\ 0.981\\ $	0.578 0.562 0.711 0.765 0.761 0.725 0.725 0.742 0.742 0.745 0.841 0.612 0.477 0.4409 0.392 0.385 0.380 0.380

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Table C-3. Radiative Properties of the Desert Aerosol for 20 ms⁻¹ Wind Speed Conditions. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied) attenuation with the second ्रोः । प्राप्तः : ... राष्ट्राः :

	ATTENUATION COEFFICIENTS (km ⁻¹)				
AVELENGTH (1m)	Extinction	Scattering	Absorption		Я
0.200	2.73(-1)	2.32(-1)	4.16(-2)	0.848	0.772
0.250	2.66	2.25	4.15	0.844	0.778
0.300	2.58	2.16	4.17	0.838	0.786
0.337	2.53	2.11	4.18	0.835	0.791
0.400	2.44	2.02	4.19	0.828	0.796
0.488	2.34	1.92	4.18	0.821	0.802
0.515	2.31	1.89	4.17	0.819	0.806
0.550	2.28	1.87	4.11	0.819	0.808
0.633	2.21	1.96	2.49	0.887	0.799
0.694	2.17	2.12	5.06(-3)	0.977	0.780
0.860	2.10	1.96	1.35(-2)	0.936	0.795
1.060	2.04	2 04	2 11(-4)	0.999	0.783
1.300	2.00	2.00	1 02	1.000	0.785
1.536	1,98	1.98	7 57(-5)	1.000	0 787
1.800	1.97	1.97	6 04	1,000	0.788
2.000	1.97	1.97	9 55	1 000	0.788
2.250	1 96	1 96	8 84	1 000	0.700
2.500	1 97	1.36	9.06	1 000	0 789
2.700	1.97	1.96	1 51(-4)	0 999	0.789
3.000	1.99	1.96	3.50(~3)	0 982	0.791
3.200	2.03	1.97	5.87	0.971	0.791
3, 192	2 02	1.98	3.63	0 982	0.788
3 500	2 01	1 98	3 06	D 985	0.790
3 750	2 00	1 97	2 67	0.900	0 793
A 000	1 44	1 97	2 85	0.986	0 795
	2 00	1 99	1 26(-2)	0.000	0.175
5 000	2.00	1 40	I.20(-2) E 03	0.906	0.010
5.000	2.01	1,42	9.92 5.03	0.700	0.073
5.500	2.03	1 A 6	5.83 5.07	0.712	0.0//
6.000 6.000	2.04 2.05	1 40	0.94	0.710	0.004
	2.03	1 AQ	5,33 5 07	0,001	0.090
7 200	2.07	1 21	3.8/	0.710	0.900
7.200	4.00	1 30	(.4) 5 00	0.03/	0.970
7.900	1.92	1.39	5.22	0.728	0.832
8.200	2.UI	1,75	2.50	0.872	0.620
8,500	2.19	1.92	2,64	0.879	0.590
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Table C-3.	(cont.)
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	ATTENUATION COEFFICIENTS (km ⁻¹)				
WAVELENGTH (µm)	Extinction	Scattering	Absorption	Wo	g
9.000 9.200 9.500 9.500 10.000 10.591 11.000 11.500 12.500 13.000 14.000 14.800 15.000 16.400 17.200 18.500 20.000 18.500 21.300 21.300 22.500 25.000 25.000 27.900 30.000 35.000 40.000 50.000 60.000 80.000 150.000 200.000	2.47(-1) 2.25 2.06 2.07 2.07 2.09 2.10 2.12 2.18 2.12 2.18 2.12 2.18 2.12 2.13 2.10 2.12 2.13 2.10 2.12 2.13 2.17 2.52 2.17 2.52 2.17 2.52 2.17 2.52 2.17 2.52 2.57 2.55 2.36 2.10 1.59	2.15(-1) 2.00 1.36 1.27 1.26 1.34 1.39 1.39 1.39 1.37 1.24 1.33 1.31 1.31 1.31 1.41 1.47 1.92 2.04 1.44 1.57 1.43 1.55 1.86 2.09 2.30 2.40 2.46 2.51 2.34 2.05 1.59	3.24(-2) 2.47 7.04 8.06 8.12 7.51 7.12 7.30 8.06 8.83 8.24 7.83 7.49 7.89 8.14 7.18 6.77 2.55 4.86 7.31 8.50 8.11 7.13 4.82 3.09 1.70 1.15 1.06 4.04(-3) 2.15 1.41 7.97(-4)	0.869 0.890 0.658 0.611 0.609 0.641 0.655 0.630 0.584 0.655 0.630 0.657 0.624 0.657 0.624 0.657 0.624 0.663 0.663 0.692 0.6883 0.663 0.693 0.663 0.693 0.693 0.954 0.954 0.954 0.955 0.931 0.959 0.959	$\begin{array}{c} 0.580\\ 0.570\\ 0.570\\ 0.725\\ 0.790\\ 0.801\\ 0.794\\ 0.790\\ 0.826\\ 0.826\\ 0.826\\ 0.826\\ 0.826\\ 0.826\\ 0.829\\ 0.826\\ 0.829\\ 0.826\\ 0.829\\ 0.826\\ 0.829\\ 0.$

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Table C-4. Radiative Properties of the Desert Aerosol for 30 ms⁻¹ Wind Speed Conditions. The numbers in parentheses in the attenuation columns are the power of 10 following the value of attenuation (if no value given, then the previous power of 10 is implied) accompany of any with a statement of the statement

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	ATTENUATION COEFFICIENTS (km ⁻¹)				
WAVELBNGTH (µm)	Extinction	Scattering	Absorption	Wo	g
0.200 0.250 0.300 0.337 0.400 0.488 0.515 0.550 0.633 0.694 0.860 1.600 1.536 1.800 2.000 2.250 2.500 2.500 2.500 3.200 3.200 3.392 3.500 3.750 4.000 4.500 5.500 5.500 6.200 5.500 6.200 5.500 6.200 5.500 5.500 6.200 5.500 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.200 5.500 6.2000 6.200 6.200 6.200 6.500 7.200 8.500 8.500 8.700	1.98(0) 1.98 1.97 1.97 1.97 1.95 1.95 1.95 1.95 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.94 1.95 1.9	1.57(0) 1.56 1.55 1.55 1.55 1.53 1.53 1.53 1.53 1.63 1.63 1.94 1.94 1.94 1.94 1.94 1.94 1.95 1.95 1.95 1.95 1.95 1.95 1.96 1.97 1.96 1.94 1.94 1.94 1.95 1.78 1.30 1.20 1.40 1.75 1.88 1.72	4.18(-1) 4.17 4.19 4.20 4.21 4.21 4.21 4.21 4.21 4.21 4.18 3.12 8.65(-2) 2.01(-1) 2.65(-3) 7.90(-4) 4.08 2.72 3.14 3.00 9.30 1.28(-3) 2.14(-2) 1.11 8.76(-3) 9.69 3.77(-2) 4.79 2.08(-1) 7.09 7.04 7.14 7.63 7.11 8.30 5.36 2.45 2.12 3.81	0.789 0.789 0.789 0.788 0.787 0.785 0.784 0.785 0.785 0.784 0.785 0.955 0.999 1.0000 0.9999 0.9995 0.6448 0.6451 0.64914 0.64914 0.878 0.8799 0.878 0.8799 0.878 0.8799 0.878 0.8799 0.878 0.8799 0.878 0.8799 0.819 0.819	$\begin{array}{c} 0.829\\ 0.836\\ 0.841\\ 0.844\\ 0.844\\ 0.847\\ 0.850\\ 0.850\\ 0.850\\ 0.850\\ 0.850\\ 0.850\\ 0.850\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.799\\ 0.802\\ 0.801\\ 0.801\\ 0.801\\ 0.801\\ 0.801\\ 0.801\\ 0.801\\ 0.803\\ 0.905\\ 0.915\\ 0.926\\ 0.915\\ 0.926\\ 0.915\\ 0.926\\ 0.915\\ 0.926\\ 0.915\\ 0.926\\ 0.926\\ 0.832\\ 0.617\\ 0.583\\ 0.638\end{array}$

1 ⁴ - 11 - 11	ATTENUATION COEFFICIENTS (km ⁻¹)					 	
WAVELENGTH (1m)	Bxtinction	Scattering	Absorption	٣٥	g		••••••
9.000	2.22(0)	2.05(0)	1,78(-1)	0.920	07.571		
3.200	2.18	1.97	1.93	0.911	0.567	}	
9.500	2.02	1.36	6.64	0.672	0.729		-
9.800	2.04	1.26	7.77	0.619	0.801		
10.000	2 04	1 24	7 99	0.608	0 820		
10 591	2 05	1 26	7 90	0 615	0.020		
11 000	2.05	1 20	7.50	0.624	0.0.2		
11 500	2.00	1 27	7 0 4	0.616	0.055		
12 500	2.07	1 76	7.24	0.010	0.055		
12.000	2.12	7,20	7.03	0.040	0.794		
13.000	2.07	1 22		0.500	0.045		
14.000	2.10	1.43	0.01	0.509	0.071		
14.000	2.11	1.27	8.30	0.603	0.862		
15.000	2.11	1.29	8.10	0.013	0.859		
10,400	2.07	1.23	8.31	0.59/	0.892		
17.200	2.09	1.24	8.49	0.594	0.892		
18.000	2.09	1.33	/.50	0.638	0.86/		
18.500	2.12	1.41	7.01	0.668	0.841		
20.000	2.14	90	2.38	0.889	0.587		
21.300	2.37	1.93	4.42	0.813	0.649		
22,500	2.11	1.42	5.95	0.6/1	0.708		
25.000	2.29	1.52	7.74	0.663	0.756		
27,900	2.17	1.38	7.90	0.637	0.738		
30.000	2.18	1.47	7.11	0.674	0.702		
35,000	2.23	1.68	5.56	0.751	0.649		
40.000	2.27	1.88	3.93	0.827	0.602		
50,000	2.33	2.10	2.33	0.900	0.553		
60.000	2.38	2.21	1.63	0.932	0.528		
80.000	2.45	2.30	1.53	0.938	0.502		
100.000	2.49	2.43	5.88(-2)	0.976	0.471		
L 50.00 0	2.51	2.48	3.56	0.986	0.440		
200.000	2.45	2.42	2.45	0.990	0.423		
300,000	2.21	2.20	1.45	0.993	0.406		

Table C-4. (cont.)

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Table C-r. Normalized Angular Scattering Function for the Desert Aerosol Model as a Function of Wind Speed for a Wavelength of 0.55 $\,\mu m$

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A THURSDAY	AZIMUTH	NORMALIZ	ति सिंह्य ते हैं। साल विश्वास सम्रोत इ.स. हा स्ट्री साल विश्वास सम्रोत			
• • • • • • • • • • • • • • • • • • •	ANGLE (degrees)	0 ms ⁻¹	10 ms ⁻¹	20 ms ⁻¹	30 ms ⁻¹	
	0.00 2.00 4.00 6.00 8.00 10.00 12.00 14.00 16.00 20.00 22.00 24.00 26.00 28.00 30.00 32.00 34.00 36.00 38.00 40.00 50.00 60.00 70.00 80.00 90.00 100.00 125.00 135.00 140.00 155.00 155.00 160.00 175.00 180.00	8.10(1) 1.27(0) 9.15(-1) 8.39 7.79 7.22 6.67 6.14 5.63 5.16 4.71 4.30 3.92 3.56 3.24 2.94 2.67 2.43 2.20 2.00 1.81 1.13 7.17(-2) 4.71 3.23 2.34 1.81 1.53 1.40 1.38 1.39 1.40 1.38 1.39 1.40 1.38 1.39 1.40 1.38 1.39 1.40 1.38 1.39 1.40 1.38 1.39 1.40 1.38 1.91 2.09 2.33 2.80 3.06	3.41(3) 9.69(-1) 7.51 6.65 5.56 5.11 4.69 4.30 3.94 3.60 3.29 3.00 2.73 2.49 2.27 2.06 1.88 1.70 1.55 9.65(-2) 6.13 3.98 2.65 1.88 1.45 1.22 1.12 1.12 1.12 1.12 1.12 1.15 1.99 1.25 1.33 1.42 1.80 2.64 2.83 3.70 4.01	$\begin{array}{c} 4.54(4) \\ 4.10(0) \\ 8.65(-1) \\ 4.86 \\ 3.86 \\ 3.41 \\ 3.11 \\ 2.84 \\ 2.63 \\ 2.29 \\ 2.29 \\ 2.11 \\ 1.94 \\ 1.84 \\ 1.67 \\ 1.55 \\ 1.43 \\ 1.30 \\ 1.21 \\ 1.09 \\ 9.66(-2) \\ 6.20 \\ 3.90 \\ 2.39 \\ 1.51 \\ 8.91(-3) \\ 6.58 \\ 5.63 \\ 5.57 \\ 5.48 \\ 5.64 \\ 5.57 \\ 5.48 $	$2 \cdot 29(5)$ $3 \cdot 04(0)$ $6 \cdot 06(-1)$ $3 \cdot 48$ $2 \cdot 84$ $2 \cdot 37$ $2 \cdot 20$ $2 \cdot 11$ $1 \cdot 93$ $1 \cdot 78$ $1 \cdot 71$ $1 \cdot 64$ $1 \cdot 51$ $1 \cdot 36$ $1 \cdot 29$ $1 \cdot 16$ $1 \cdot 10$ $3 \cdot 90(-2)$ $9 \cdot 57$ $8 \cdot 71$ $7 \cdot 98$ $5 \cdot 07$ $3 \cdot 01$ $1 \cdot 84$ $1 \cdot 04$ $5 \cdot 15(-3)$ $3 \cdot 67$ $3 \cdot 33$ $3 \cdot 20$ $3 \cdot 72$ $3 \cdot 48$ $3 \cdot 42$ $3 \cdot 18$ $3 \cdot 17$ $3 \cdot 24$ $3 \cdot 33$ $8 \cdot 41$ $4 \cdot 08(-2)$ $4 \cdot 09$ $5 \cdot 82$ $6 \cdot 37$	





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Table C-6. Normalized Angular Scattering Function for the Desert Aerosol Model as a Function of Wind Speed for a Wavelength of 1.06 $\mu\nu$

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ASIMUTH	NUKMALI	ZED ANGULAR	SCATTERING F	UNCTION
ANGLE (degrees)	0 ms ⁻¹	10 ms ⁻¹	20 ms ⁻¹	30 ms ⁻¹
$\begin{array}{c} 0 & 0 \\ 2 & 0 \\ 2 & 0 \\ 2 & 0 \\ 4 & 0 \\ 6 & 0 \\ 8 & 0 \\ 1 \\ 0 & 0 \\ 1 \\ 2 & 0 \\ 1 \\ 2 & 0 \\ 1 \\ 4 & 0 \\ 1 \\ 6 & 0 \\ 1 \\ 2 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0$	$\begin{array}{c} 6.14(1) \\ 2.91(0) \\ 1.07 \\ 8.56(-1) \\ 7.67 \\ 7.02 \\ 6.45 \\ 5.93 \\ 5.44 \\ 4.98 \\ 4.55 \\ 4.15 \\ 3.79 \\ 3.45 \\ 3.14 \\ 2.85 \\ 2.59 \\ 2.36 \\ 2.14 \\ 1.95 \\ 1.77 \\ 1.10 \\ 7.00(-2) \\ 4.60 \\ 3.13 \\ 2.24 \\ 1.72 \\ 1.44 \\ 1.32 \\ 1.30 \\ 1.31 \\ 1.35 \\ 1.41 \\ 1.49 \\ 1.59 \\ 1.71 \\ 2.00 \\ 2.37 \end{array}$	$ \begin{array}{c} 1 & 56 (3) \\ 7 & 87 (0) \\ 1 & 40 \\ 7 & 65 (-1) \\ 5 & 93 \\ 5 & 12 \\ 4 & 60 \\ 4 & 21 \\ 3 & 88 \\ 3 & 57 \\ 3 & 28 \\ 3 & 03 \\ 2 & 78 \\ 2 & 57 \\ 2 & 36 \\ 2 & 16 \\ 1 & 98 \\ 1 & 82 \\ 1 & 66 \\ 1 & 52 \\ 1 & 40 \\ 8 & 88 (-2) \\ 5 & 57 \\ 3 & 63 \\ 2 & 24 \\ 1 & 43 \\ 1 & 02 \\ 8 & 19 (-3) \\ 7 & 39 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 \\ 7 & 30 $	1.13(4) 7.28(0) 1.18 5.75(-1) 4.20 3.53 3.20 2.91 2.72 2.59 2.43 2.28 2.06 1.93 1.79 1.70 1.55 1.41 1.33 1.22 1.16 7.57(-2) 4.68 2.90 1.51 7.81(-3) 4.58 3.55 3.34 3.29 3.18 3.26 3.30 3.71 4.36 5.02 3.12(-2) 3.82	$\begin{array}{c} 4.90(4)\\ 4.69(0)\\ 8.63(-1)\\ 4.59\\ 3.64\\ 3.04\\ 2.91\\ 2.60\\ 2.47\\ 2.35\\ 2.21\\ 2.07\\ 1.97\\ 1.86\\ 1.71\\ 1.59\\ 1.49\\ 1.37\\ 1.28\\ 1.20\\ 1.10\\ 7.25(-2)\\ 4.46\\ 2.70\\ 1.36\\ 6.13(-3)\\ 3.35\\ 2.52\\ 2.57\\ 2.53\\ 2.44\\ 2.49\\ 2.44\\ 2.77\\ 3.24\\ 3.82\\ 3.44(-2)\\ 3.62\\ \end{array}$

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Figure C-2. Normalized Angular Scattering Function of the Desert Aerosol for a Wavelength of 1.06 µm

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Table C-7. Normalized Angular Scattering Function for the Desert Aerosol Model as a Function of Wind Speed for a Wavelength of 10.591 µm

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	AZIMUTE	NORMALIZ	NORMALIZED ANGULAR SCATTERING		
ANGLE (degrees		0 ms ⁻¹	10 ms ⁻¹	20 ms ⁻¹	30 ms ⁻¹
	0.00	8.46(0)	3.89(1)	1.85(2)	7.89(2)
	2.00	7.17	1.90	3.04(1)	3.31(1)
	4.00	4.96	8.20(0)	8.64(0)	6.96(0)
	6.00	3.30	4.03	3.45	2.47
	10.00	2.20	2.20	1.08	1.14 6.10(1)
		1,50	P 31(~1)	9.3/(-1) 5.75	3 78
	14.00	7.57(-1)	5 60	3 82	2 52
	16.00	5.61	3.98	2.69	1.80
	18.00	4.27	2.95	2.00	1.35
	20.00	3,34	2,27	1.55	1,06
	22.00	2.68	1.81	1.25	8.63(-2)
	24.00	2.20	1.49	1.03	7.23
	26.00	1.84	1.25	8.79(-2)	6.21
	28.00	1.58	1.08	7.63	5.44
	30.00	1.37	9.45(-2)	6.73	4.84
	32.00	1.21	8.4U 7 50	6.UJ 5.47	4,30
	34.00	1,00 9 76(-2)	7.50 K 40	5,47	3.90
	38.00	8,90	6.35	4.64	3 40
	40.00	8.18	5.89	4.32	3.18
	50.00	5.80	4.33	3.24	2.43
	60.00	4,43	3.42	2,60	1,99
	70.00	3,55	2.80	2.17	1,69
	80.00	2.94	2.35	1.85	1,48
	90.00	2.49	2,01	1.61	1.32
	100.00	2.17	1.76	1.43	1.20
	110.00	1.96	1.58	1.30	1.11
		1.83	1.46	1.21	1.06
	125.00	.1.79 1.79	1.42	1,18	1.03
	135.00	1 80	1 29	1,10	1 01
	140.00	1.87	1.42	1.15	1.01
	145.00	1,99	1.48	1,18	1.02
	150.00	2.22	1.60	1,24	1.05
	155.00	2.57	1.80	1.34	1.10
	160.00	3.14	2.14	1.52	1.18
	165.00	4.06	2.74	1.85	1.35
	170.00	5.48	3.73	2.42	1.64
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