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Molecular Composites from the Phase Separation
at Low Temperatures of Kevlar and
Diaminophenylindane Polyimide in Sulfuric Acid

by

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19 ABSTRACT (Continue on reverse if necessary and identify by block number) In a molecular composite, a ductile matrix is reinforced with a stiff, strong, rigid-rod polymer molecule. One of the approaches used to make a rigid-rod molecular composite involves the physical mixing by coprecipitation of single-phase solutions of a rigid-rod and a flexible-coil polymer in a common solvent. We and others have reported previously on the preparation of three-dimensional fibrous materials using the phase separation of polymer solutions at low temperature and sublimation or extraction of the solvent. It is conceivable that a molecular composite would give a superior 3D fibrous material by combining the strength of the rigid-rod macromolecules with the better processibility of the random-coil polymer. This preprint describes our attempts to test this hypothesis. "Molecular composites" from Kevlar and diaminophenylindane polyimide were fabricated by quenching sulfuric acid solutions. The structure and properties of the resulting three-dimensional fibrous structures were then determined. CHIOX			
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Procedure

Solutions were prepared from a 25:75 ratio of Kevlar and Matrimid 5218 in 96% sulfuric acid at different concentrations of polymer (from 1% to 20% by wt). In addition, solutions of the two polymers were prepared at 4% total polymer concentration by weight but with different ratio of the two polymers (from a 19:1 to 1:19 Kevlar:Matrimid in 20 uniform increments). The gel points of the solutions were measured using a low temperature bath programmed at either 2°C/min or 0.2°C/min.

Three dimensional fibrous materials were made by placing the solutions into capped, cylindrical polyethylene molds (1.5 cm x 2.5 cm) and cooling to -80°C at a rate of 2°C/min. The gels, generally transparent, were removed from the mold and extracted overnight using a 50/50 methanol/ water mixture at -45°C . This was followed by overnight extraction with 75/25 water/methanol at -15°C; and, finally, 100% H₂O for one week at 0°C, changing the solvent every day. After this, the three- dimensional materials were freeze dried at 50 millitorr.

The morphology of the reinforcements was studied using a scanning electron microscope (Model Amray 1000A) at 20 kV. Optical microscopy studies of the composites were done with a polarizing microscope (Nikon metaphoto). The embedding media used were: EMI (4-ethyl-2-methylimidazole) (2%) in Epon 815 and commercial epoxy penetrant ("wood rot cure").

Composites

A third polymer (epoxy resin) was incorporated into the three dimensional materials. To accomplish this, The 3D material was placed into a polyethylene mold and covered with degassed epoxy. The mold was put under a

vacuum until no more air bubbles were observed (2 hours at 50 millitorr). Then the mold was capped and the epoxy cured at room temperature for 24 hours; or, in the case of the Epon 815/2% EMI, at 90-100°C for 24 hours.

Mechanical Measurements

Because of their small size, the stiffness of the composites was measured using a penetrometer. (The L.S. Starrett Co. cat #4101). Tests were done on a polished surface of the composite and in the adjacent unreinforced matrix. The stylus was a commercial needle from Ogura Jewell Industry, Co., LTD the (radius 10^{-2} mm). Tensile compliance, was calculated according to the method described by Clough, Gillen and Quintana.⁵

Results and Discussion

The structure obtained by SEM showed a rope-like structure with small cells (1-10 microns)(Fig. 1). As the ratio of the polyimide to Kevlar was increased, nodules of polyimide were formed on the Kevlar-rich struts, implying phase separation. The nodules of polyimide found at large concentration of this polymer were found to be related to the solvent. This conclusion is based on a comparison of materials made from the polyimide dissolve in dioxane vs sulfuric acid. The morphologies of materials from this solvent are different from those made using sulfuric acid (Fig. 2). In addition, a comparative study of sublimation vs extraction in the processing of the reinforcements suggest that the mere fact that the acid is extracted (rather than sublimed) is not important.

Preliminary penetration results suggest that the fibrous materials are increasing the modulus of the epoxy by about 20%. If the modulus of the

reinforcement were that of fully aligned Kevlar (~ 130 GPa), a modulus increase of 11% would be expected, assuming random placement of the fibers. Thus, our results are consistent with an efficient reinforcement of the epoxy matrix by the 3-D fibrous structures.

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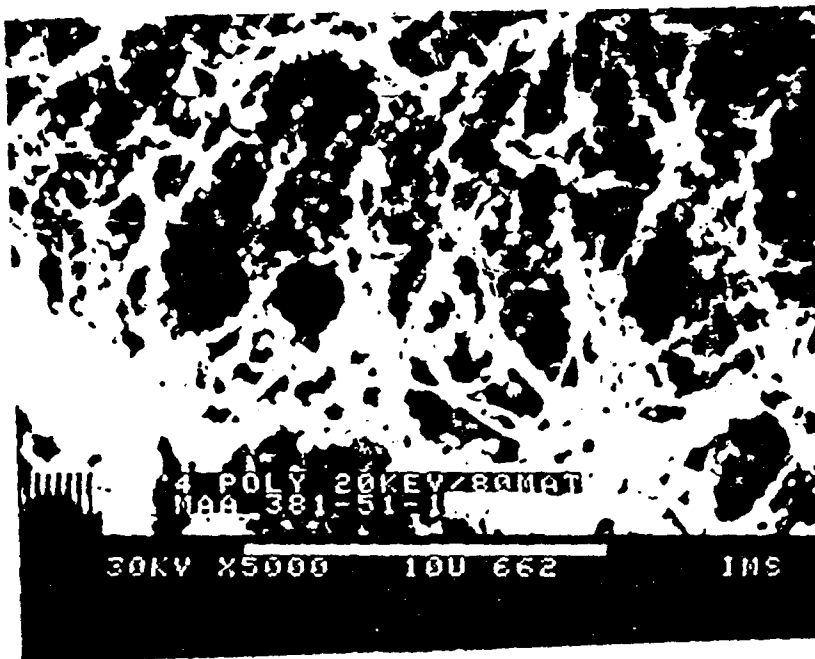


Figure 1. SEM of a three dimensional reinforcement containing 20% Kevlar and 80% matrimid 5218 prepared in 96% sulfuric acid.

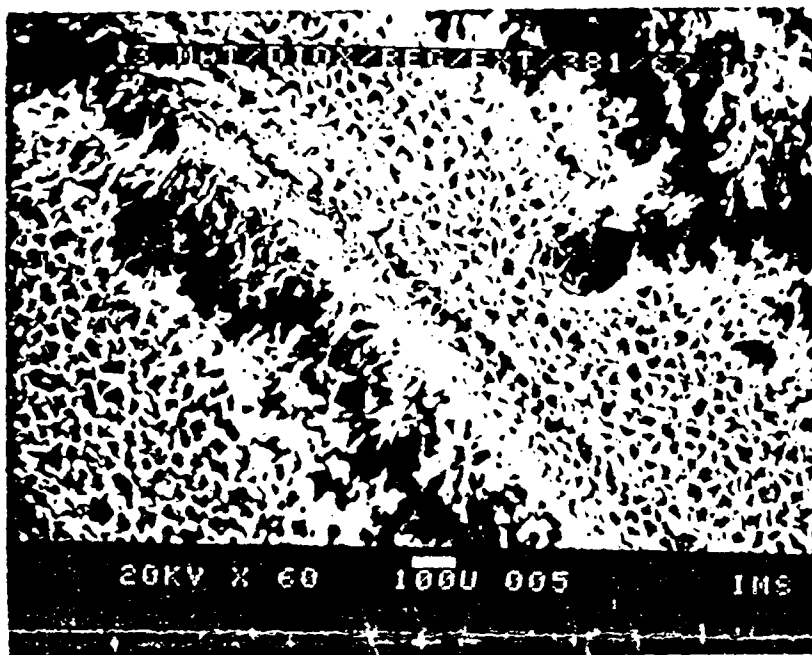


Figure 2. SEM of a 3% Matrimid 5218 reinforcement prepared in Dioxane.

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