



and Rithers' Massess - Masses

# MEROCORY RESCLUTION TEST CHART NATING SECOND CONTRACTS

AD-A 191 ///	MUDOQ TYOCUM	ENTATION PAGE			
		16. RESTRICTIVE MARKIN	GS		
a. SECURITY CLASSIFICATION A CHITY		3. DISTRIBUTION/AVAILAE	ILITY OF REPOP	ат	
MAR 1		Approved for public re	elease; distribu	ition is unlimit	ed.
	)	5. MONITORING ORGANIZ	ATION REPORT	NUMBER(S)	
	ED OFFICE SYMBOL			NI	<u></u>
Naval Ocean Systems Center	(if applicable)	Naval Ocean System	Contor		
c. ADDRESS (City, State and ZIP Code)		7b. ADDRESS (City, State and Z	P Code)		
			,		
San Diego, California 92152-5000		San Diego, California	a 92152-5000		
a. NAME OF FUNDING/SPONSORING ORGANIZATION	8b. OFFICE SYMBOL (if applicable)	9. PROCUREMENT INSTR	UMENT IDENTIFI	CATION NUMBE	R
Naval Sea Systems Command	NSEA				
5. AUDHESS (City, State and ZIP Code)		PROGRAM ELEMENT NO.	NUMBERS	TASK NO	AGENCY
					ACCESSION I
Materials and Mechanics Division Washington, DC 20362		61153N	HM01	SB0230103	DN 530 607
1 TITI F Linclude Service (Isseedington)	· · · · · · · · · · · · · · · · · · ·				
Comparison of the Wall Pressure Fluctuations i Boundary Layers	n Artificially Gener	ated Turbulent Spots, Na	atural Transitio	on, and Turbu	lent
PERSONAL AUTHOR(S)					
T.S. Mauther					
3a. TYPE OF REPORT 13b. TIME COVERED	<u>, , , , , , , , , , , , , , , , , , , </u>	14. DATE OF REPORT ()	ear, Month, Day)	15. PAGE COUN	JT
Professional paper/speech FROM Jan 1988	TO Jan 1988	January 1988			
6. SUPPLEMENTARY NOTATION					
	B. SUBJECT TERMS (	(Continue on reverse if necessary and ide	ntifiy by block number)		
	turbulent bounda	ry layer			
	wall pressure flu	tuations			
9. ABSTRACT (Continue on reverse if necessary and identify by block num	nber)				
I DEMINDER NOUNCERV LEVER I NO RECUILS SHOW THAT	both the rms wall p The zero and favora irrent spot data sho	ressure and the wall pres ble pressure gradient wal ws that, in the presence and for the zero and favo	sure spectra of Il pressure data of an adverse rable pressure	t turbulent spo a are in agreen pressure gradie gradient cases ionally, the ne	ts are influ- nent with ent, the spot's these re- early constant
anced by the local mean flow pressure gradient. I urbulent boundary layer results. However, the cu ms wall pressure is approximately 1.5-2.5 times sults are in general agreement with the adverse pr nagnitude of the spot's adverse pressure gradient	larger than that four ressure gradient data wall pressure spect	a of Huang and Hannan frum indicates a nearly end $F_{1}$	ven distributior	n of energy wit	h frequency.
inced by the local mean flow pressure gradient. I urbulent boundary layer results. However, the cu ms wall pressure is approximately 1.5-2.5 times ults are in general agreement with the adverse pr nagnitude of the spot's adverse pressure gradient 'resented at AIAA 26th Aerospace Sciences Mee	larger than that four ressure gradient data wall pressure spect sting, 11-14 Januar	y 1988, Reno, NV.	ven distributior	a of energy wit	h frequency.
resented at AIAA 26th Aerospace Sciences Mee	larger than that four ressure gradient data wall pressure spect	y 1988, Reno, NV.	(1973). Addition	1 of energy wit	h frequency.
Presented at AIAA 26th Aerospace Sciences Mee	larger than that four ressure gradient data wall pressure spect	y 1988, Reno, NV.	(1973). Addition	1 of energy wit	h frequency.
DISTRIBUTION/AVAILABILITY OF ARSTRACT	larger than that fou ressure gradient data wall pressure spect	y 1988, Reno, NV.	CLASSING TO	1 of energy wit	h frequency.
D DISTRIBUTION/AVAILABILITY OF ABSTRACT	larger than that four ressure gradient data wall pressure spect	21. ABSTRACT SECURITY	CLASSIFICATIO	n of energy wit	h frequency.
D DISTRIBUTION/AVAILABILITY OF ABSTRACT UNCLASSIFIED/UNLIMITED X SAME AS RPT 22. NAME OF RESPONSIBLE INDIVIDUAL	larger than that four ressure gradient data wall pressure spect etting, 11-14 Januar	21. ABSTRACT SECURITY UNCLASSIFIED	CLASSIFICATIO	N	MROI
DISTRIBUTION/AVAILABILITY OF ABSTRACT UNCLASSIFIED/UNLIMITED X SAME AS RPT 2. NAME OF RESPONSIBLE INDIVIDUAL	larger than that four ressure gradient data wall pressure spect etting, 11-14 Januar	21. ABSTRACT SECURITY UNCLASSIFIED 22b. TELEPHONE (Include Are (619) 553-1588	CLASSIFICATIO	N 22c. OFFICE SY	MDOL

and a start of the start of the



AIAA-88-0409 Comparison of the Wall Pressure Fluctuations in Artificially Generated Turbulent Spots, Natural Transition and Turbulent Boundary Layers T.S. Mautner, Naval Ocean Systems Center, San Diego, CA

Accesson Por
NTIS CRAME N : OTIC TAB [] U. annuncied [] Justing segment
By Distribution 1
Free tradies in the town of
Dist Australian A
A-1

# AIAA 26th Aerospace Sciences Meeting January 11-14, 1988/Reno, Nevada

ି ର

128

For permission to copy or republish, contact the American Institute of Aeronautics and Astronautics 370 L'Enfant Promenade, S.W., Washington, D.C. 20024

## COMPARISON OF THE WALL PRESSURE FLUCTUATIONS IN ARTIFICIALLY GENERATED TURBULENT SPOTS, NATURAL TRANSITION AND TURBULENT BOUNDARY LAVERS

Thomas S. Mautner Naval Ocean Systems Center San Diego, CA 92152-5000

# ABSTRACT

Experiments have been conducted to measure the wall pressure fluctuations associated with artificially generated turbulent spots in a laminar boundary layer. The results show that both the rms wall pressure and the wall pressure spectra of turbulent spots are influenced by the local mean flow pressure gradient. The zero and favorable pressure gradient wall pressure data are in agreement with turbulent boundary layer results. However, the current spot data shows that, in the presence of an adverse pressure gradient, the spot's rms wall pressure is approximately 1.5-2.5 times larger than that found for the zero and favorable pressure gradient cases. These results are in general agreement with the adverse pressure gradient data of Huang and Hannan (1975). Additionally, the nearly constant magnitude of the spot's adverse pressure gradient wall pressure spectrum indicates a nearly even distribution of energy with frequency.

#### NOMENCLATURE

В	Probability density function
С	Constant
đ	Transducer diameter
ť	Frequency
N	Frequency of occurrence
P	Wall pressure
(p <sup>-2</sup> ) <sup>12</sup>	RMS wall pressure
(p <sup>-2</sup> ) <sup>-2</sup>	Mean value of rms wall pressure
q	Free stream dynamic pressure
R.,	Reynolds number = $U_{\infty}x/\nu$
t	Time
uí	Longitudinal turbulence intensity
U.	Free stream velocity
U.	Friction velocity = $(\tau_w/\rho)^{\frac{1}{2}}$
x	Longitudinal coordinate
у	Vertical coordinate
3	Falkner-Skan parameter
δ,	Boundary layer thickness
δ*	Boundary layer displacement thickness
ω	Angular frequency
Φ	Wall pressure spectra
ρ	Density
τ.,	Wall shear stress
ν	Kinematic viscosity

# INTRODUCTION

Knowledge of the wall pressure fluctuations beneath transitional and turbulent flows is required in order to understand and reduce aerodynamically and hydrodynamically generated noise. Measurements inside and outside turbulent boundary layers indicate that the wall pressure fluctuations generated by turbulence may well be the dominant mechanism in the generation of near field noise (self-noise). It is also known that panel vibration, for example, results from the spatial integration of the wall pressure field and its interaction with the structure's response function. Thus, if the wall pressure fluctuations are coupled with the vibratory modes of the structure, there will be a significant increase in the sound level radiated into the far field (for review articles see: Flowes Williams, 1969; Willmarth, 1975).

This paper is declared a work of the U.S. Government and is not subject to copyright protection in the United States. Many detailed investigations have been performed on the fluctuating wall pressure beneath turbulent boundary layers utilizing both transducers mounted flush with the wall and those fitted with pinhole caps. From the research it has been determined that the energy associated with the turbulent wall pressure fluctuations is distributed over a wide frequency range with the major portion of the rms wall pressure magnitude arising from the convective range. It is also believed that the low wave number region may provide more  $\neg$ ffective excitation of structures than the convective region. Emmerling et al (1973) and Bull and Thomas (1976) have summarized the available experimental results, which show significant high frequency contributions to the pressure spectrum when the transducer size is reduced such that  $dU_{\pi}/\nu < 100$ . Their summaries and some more recent experimental results are reproduced in table 1 and figure 1.

In comparison to the turbulent boundary layer results, only a limited amount of data is available on the wall pressure fluctuations associated with natural transition and, more specifically, individual turbulent spots. The measurements of DeMetz and Casarella (1973) and Huang and Hannan (1975) have established certain statistical properties, in term of intermittency, of the wall pressure fluctuations during natural transition. It is not possible to infer individual spot properties from these measurements since the spots were occurring randomly and their measurements were made at uncontrollable locations within the spots. However, DeMetz and Casarella concluded that the magnitude of the intermittent wall pressure bursts during natural transition is approximately equal to the values measured in zero pressure gradient turbulent boundary layers. Also, the measurements of Huang and Hannan show that the rms wall pressure fluctuations occurring during natural transition, in the presence of a strong adverse pressure gradient, were 2-3 times larger than those found in a turbulent boundary layer. Finally, the recent wall pressure measurements by Johansson et al (1987) provide a comparison of the rms wall pressure measured in zero pressure gradient turbulent boundary layer (( $p^{2}$ )<sup>1/2</sup>/q=0.0078) and in a turbulent spot (( $p^{2}$ )<sup>1/2</sup>/q=0.0094).

The purpose of this paper is to report experimental data on the rms wall pressure fluctuations associated with artificially generated turbulent spots convecting in a laminar boundary layer. The spot data, for zero, favorable and adverse pressure gradients, will be compared to available wall pressure data in order to identify the relationship between the rms wall pressure fluctuations of a spot and that measured during natural transition and in turbulent boundary layers. Since wall pressure fluctuations are a direct measure of the surface excitation forces produced by the boundary layer, flow data of this type may be used to evaluate the vibrational and hydroacoustic responses of a structure.

#### MEASUREMENTS

The present measurements were made at a nominal free stream velocities of  $U_{\infty} = 7.8$ , 10 and 11 m/s in the closedcircuit wind tunnel of the Department of Applied Mechanics and Engineering Sciences at the University of California, San Diego. The flat plate on which the spots were generated and other experimental apparatus were the same as that used in some previous studies (Mautner and Van Atta, 1982; Mautner, 1983). The measured laminar boundary layer pressure gradients, as indicated by the Falkner-Skan parameter  $\beta$ , are given in table 2. The centerline turbulent spot data were obtained at longitudinal positions x=91.4, 121.9 and 152.4 cm downstream of the plate's leading edge. The wall pressure fluctuations were measured using a B&K model 4138 0.32 cm diameter condenser microphone whose sensing area was reduced by using a 0.8 mm diameter pinhole in the plate's surface. The microphone was connected to a B&K 2609 measuring amplifier. For each spot the wall pressure signature was represented by 2048 digital samples, the sampling being triggered by the spot generator (x=30.4 cm) signal. For the pressure record from each spot, the rms value ( $p^{-2}$ )<sup>16</sup> was calculated. Then for 500 values of ( $p^{-2}$ )<sup>16</sup>, at a particular x location and pressure gradient, the mean value, ( $p^{-2}$ )<sup>15</sup> was calculated. The values of the standard deviation were calculated for  $U_{\infty}=10$  m/s.

#### **RESULTS AND DISCUSSION**

The calculated values of the turbulent spot's rms wall pressure fluctuations are summarized in table 2, and the results for the three pressure gradients are indicated by the hashed area in figure 1. The results show that  $(p'^2)^{\frac{16}{2}}/q$  for the zero and favorable pressure gradients are approximately equal to the values measured by "pinhole" transducers in zero pressure gradient turbulent boundary layers (table 1 and figure 1). The one exception, in the current results, is the zero pressure gradient data at x=121.9 cm, where the higher values of  $(p^{+2})^{\frac{1}{2}}$  are attributed to a slight variation in the pressure gradient along the flat plate. The experiments by Bull and Thomas (1976) resulted in the conclusion that wall pressure measurements made with "pinholes" are in error for  $\omega \nu / U_r > \approx 0.1$ . The error in the wall pressure spectra would tend to reduce the "pinhole" data to that obtained by flush mounted transducers. Since the boundary layer parameters, such as wall shear stress, vary through the spot (Mautner, 1983) no corrections were applied to the current spot  $(p'^2)^{16}$ data.

A direct comparison of the current zero spot pressure gradient data at x=152.4 cm and  $U_{\infty}$ =10 m s can be made with the spot wall pressure measurements of Johansson et al (1987). Johansson et al made their wall pressure measurements at x=154cm and  $U_{\infty}$ =10 m/s and obtained a (p<sup>2</sup>)<sup>42</sup>/q=0.0094 which is in reasonable agreement with the current zero pressure gradient spot data. The magnitude of the current  $(p'^2)^{12}/q$  for both zero and favorable pressure gradient spot data is in good agreement with the zero and favorable pressure gradient turbulent boundary layer results for equivalent values of  $dU_{\nu}\nu$ . The nearly equal magnitude of the spot's  $(p'^2)^{b_0}$ , q for both the zero and favorable pressure gradient is also in qualitative agreement with, for example, the results of Schloemer (1967). It should also be noted that both Wygnanski (1981) and Narasimha et al (1984), from their spot measurements, concluded that a favorable pressure gradient provides a stabilizing effect thus slowing down the growth and breakdown process associated with spots. Therefore, it may be the stabilizing effect of a favorable pressure gradient, in both transitional and turbulent flows, which contributes to the nearly equal  $(p^{\prime 2})^{\frac{1}{2}}/q$  measured in both zero and favorable gradient flows. Finally, Johansson et al (1987) concluded from their turbulent boundary layer and spot wall pressure measurements that the mechanism generating the large wall pressure peaks, which in turn contribute to  $(p^{-2})^{-2}$ , appear to be the same in turbulent boundary layers and transitional flows.

However, when subjected to an adverse pressure gradient, the turbulent spot's rms wall pressure fluctuations are 1.5-2.5 times larger than either the zero or favorable pressure gradient results (table 2). The measured increases are in general agreement with the results of Huang and Hannan (1975). They found  $(p'2)^{16}/q \approx 0.038$  during natural transition on a forebody of revolution subjected to a strong adverse pressure gradient as compared to  $(p'2)^{16}/q \approx 0.015$  in a turbulent boundary layer with a mild, adverse pressure gradient. The increased  $(p'2)^{16}$  for the turbulent spot, and presumably for natural transition, is consistent with the larger velocity fluctuations (u') measured by Mautner (1983) in the adverse pressure gradient flow as compared to u' for a spot in a zero pressure gradient flow (for example, see Antonia et al, 1981). Higher velocity fluctuations were also measured by Schloemer (1967) and Burton (1973) in their adverse pressure gradient turbulent boundary layers. The 40% reduction in the spot's (p'2)<sup>16</sup> from x=91.4 to 121.9 cm is due to the spot's adjustment to the constant pressure gradient region. This adjustment plus the subsequent 30% increase in (p'2)<sup>16</sup> from x-121.9 to 152.4 cm indicate the sensitivity of the spot's (p'2)<sup>16</sup> magnitude to the local mean flow pressure gradient.

For a boundary layer, Kraichnan (1956) formulated a qualitative relationship between the pressure and shear forces which states that the ratio of the rms wall pressure and the wall shear stress  $(r_w)$  equals a constant,  $(p'^2)^{\frac{1}{2}}/r_w=C=6$ . Recent experimental results have determined that the constant C is on the order of 3 with typical values of 2.6 found by Willmarth and Roos (1965) and 3.4 by Blake (1970). For the current zero and favorable pressure gradient spot data, the ratio of the  $(p'^2)^{\frac{1}{2}}$  values in table 2 and  $r_w$  calculated using Prandtl's equation

$$(U_{\tau}/U_{\infty})^2 = 0.0296 \ R_{ex}^{-1/5}$$
(1)

yield a range of values for C of 2.5-3.5. This calculation shows that both the zero and favorable pressure gradient spot data scale well with the wall shear stress and that the results are consistent with the zero pressure gradient turbulent boundary layer results. However, when the adverse pressure gradient spot (p'2)<sup>16</sup> data are normalized by  $\tau_w$ , a value of C=12 is obtained. In order to obtain C≈3, an unrealistic value of  $U_w'U_{\infty}\approx0.064$  would be required, indicating that the adverse pressure gradient spot data results do not scale with the local wall shear stress. A similar result was found by Burton (1973) for a turbulent boundary layer having an adverse pressure gradient. Additionally, wall shear stress measurements by Mautner (1983) for spot's in an adverse pressure gradient show values of  $U_w'U_{\infty} \approx 0.033-0.038$  at x=152.4 cm and  $u_{\infty}=10$  m/s. This compares to  $U_w'U_{\infty} \approx 0.043$  calculated using Prandtl's equation.

Thus far the measurements for the wall pressure fluctuations associated with transitional and turbulent flows have been characterized by a single value of  $(p'^2)^{\frac{1}{2}}$  which is representative of a mean flow condition. This method is satisfactory in characterizing the statistically steady properties of a turbulent boundary layer. However, the final stage of boundary layer transition is composed of randomly occurring spots, and previous measurements of  $(p'^2)^{\frac{1}{2}}$  during transition have not identified the statistical distribution of the spot's  $(p'^2)^{\frac{1}{2}}$  magnitude nor its relationship to the generation of acoustic noise.

To examine the variation of  $(p'^2)^{\frac{1}{2}}$  about its mean value, plots of the frequency of occurrence N of a particular magnitude  $(p'^2)^{\frac{1}{2}}$  as a function of  $(p'^2)^{\frac{1}{2}}/(p'^2)^{\frac{1}{2}}$  were constructed. For each pressure gradient and  $U_{\infty} \approx 10$  m/s, the values of  $(p^{-2})^{\frac{1}{2}}$  from 500 spots at each x location were categorized using a 0.5 standard deviation bandwidth. The results in figures 2-4 show that, for each pressure gradient, the N distributions at each x exhibit excellent similarity. The N distributions for the zero and favorable pressure gradients (figures 2-3) are approximately equal and the  $(p^{-2})^{\frac{1}{2}}$  magnitudes are broadly distributed about the mean. In contrast, N distributions for the adverse pressure gradient (figure 4) show a 20-25% increase in the number of  $(p^{-2})^{-2}$  values occurring at the mean and that the remaining (p<sup>-2</sup>  $(p^{-2})^{\frac{1}{2}}$  values are more concentrated about the mean. This character of the N distribution indicates that, even though  $(p'^2)'$ ' is a broadband property of the wall pressure field, the small variation in the magnitude of  $(p^{-2})^{\frac{14}{2}}$  in the adverse pressure gradient data would provide a stronger driving force on a structure which may result in higher self- and radiated noise levels.

The N distributions provide information about the variation of  $(p^{\prime 2})^{b_0}$  over a large number of spots; however, they do not provide any information about the contribution of the spot's "random" wall pressure fluctuations in determining the value of  $(p^{-2})^{\frac{1}{2}}$ . To examine this issue, probability density functions were calculated. For  $U_{\infty}$ =10 m/s and each pressure gradient at x=152.4 cm, the probability density function for 500 spots were calculated and then averaged. The calculated probability density functions, B(p<sup>-</sup>), shown in figure 5 are given in terms of  $B(p')\Delta p'$ , which represents the fraction of the total samples in the p' to p'+ $\Delta p'$  band ( p'  $\Delta p' = 0$  occurs at  $(p'^2)^{\frac{1}{2}}$  ). The results show that B(p') for all three pressure gradients are nearly equal and that small positive values of p' are more probable than small negative values of pillt is this statistical nature of p' that not only results in the 1.5-2.5 increase in  $(p'^2)$ <sup>3</sup>, but also. like the N distributions, indicates the presence of an intense wall pressure field during boundary layer transition under the influence of an adverse pressure gradient.

The calculated values of  $(p^{r_2})^{t_0}$  and the N distributions provide broadband (in frequency) information about the turbulent spot. To obtain the distribution of energy with frequency, the spectra of the spot's wall pressure field were computed from the finite length, digitized time series p(t). For  $U_{\infty}=10$  m/s and each pressure gradient at x=152.4 cm, the spectra,  $\Phi(f)$ , for 100 spots were calculated and then averaged. The non-dimensional spectra are presented in figure 6. No corrections for the finite size of the transducer were applied to the spectra.

The spot's zero and favorable pressure gradient spectra (figure 6 a and b) are approximately equal and verify the nearly equal magnitudes of  $(p'2)^{\frac{1}{2}}$  given in table 2. These spectra are also in qualitative agreement with the turbulent boundary results of Blake (1970), Bull (1967) and Burton (1973) for a zero pressure gradient and Schloemer (1967) for a mild, adverse pressure gradient. The lower values of Schloemer's zero and favorable pressure gradient spectra are probably due to his larger transducer size and lower turbulent intensities.

For the adverse pressure gradient, the spot's wall pressure spectrum shows a nearly constant magnitude with frequency, which is in contrast to the rapid spectral decrease with increasing frequency found for both the zero and favorable pressure gradient spectra. Schloemer pointed out that the adverse pressure gradient spectrum for a turbulent boundary layer has a large magnitude, especially at lower frequencies, due to the increase in the longitudinal turbulent intensities (u') near the wall,  $y/\delta_t < 0.6$ . Similarity, the distribution of u' with y in the current spot data (Mautner, 1983) shows a higher level of u' throughout the central region as compared too the zero pressure gradient spot data of Antonia et al (1981), thereby producing the increased magnitude of (p'<sup>2</sup>)<sup>10</sup> and its spectrum.

Lauchle (1978) has derived an expression for the acoustic efficiency of boundary layer transition and compared it to the acoustic efficiency of a turbulent boundary layer. He determined that the flow noise generated by transition is more efficiently radiated into the far field than the noise generated by a fully developed turbulent boundary layer (approximately 3 orders of magnitude in his example). At least for the current adverse pressure gradient spot data, the nearly constant magnitude of the spectra would indicate a greater possibility of the spot's wall pressure field coupling with both the structure and the propagating modes of the acoustic field to produce more intense near and far field noise levels.

## SUMMARY

The current experimental results show that the magnitude of  $(p^{-2})^{\frac{1}{2}}$  and the spectra of the turbulent spot phase of boundary layer transition are strongly influenced by the local mean flow pressure gradient. The current spot data verifies the results of Huang and Hannan (1975) and shows that boundary layer transition in the presence of an adverse pressure gradient will result in  $(p^{-2})^{\frac{1}{2}}$  values which are approximately 1.5-2.5 times larger than that found for a zero or favorable pressure gradient. Additionally, the nearly constant magnitude of the spot's adverse pressure gradient spectrum indicates a nearly even distribution of energy with frequency.

The above results indicate that a transitional flow, when subjected to an adverse pressure gradient, will produce a stronger driving force on a structure over a wide frequency range. This condition may lead to a higher degree of coupling between the wall pressure field and the structure resulting in higher levels of both structure borne (self-noise) and fluid borne (far field) noise levels.

# ACKNOWLEDGEMENTS

This work was supported in part by the Naval Ocean Systems Center Independent Research Program and in part by the NAVSEA Torpedo Hydrodynamics and Hydroacoustics Program.

#### REFERENCES

Antonia, R., Chambers, A. and Van Atta, C., "Simultaneous Temperature and Velocity Measurements in the Plane of Symmetry of a Transitional Turbulent Spot," J. Fluid Mech., Vol. 108, p. 317, 1981.

Blake, W., "Turbulent Boundary Layer Wall Pressure fluctuations on Smooth and Rough Walls," J. Fluid Mech., Vol. 44, p. 637, 1970.

Bull, M., "Wall Pressure Fluctuations Associated With Subsonic Turbulent Boundary Layer Flow," J. Fluid Mech., Vol. 28, p. 719, 1967.

Bull, M. and Thomas, A., "High Frequency Wall Pressure Fluctuations in Turbulent Boundary Layers," Physics of Fluids, Vol. 19, p. 597, 1976.

Burton, T., "Wall Pressure Fluctuations at Smooth and Rough Surfaces Under Turbulent Boundary Layers With Favorable and Adverse Pressure Gradients," M.I.T. Acoustics and Vibration Laboratory Report No. 70208-9, 1973.

Daniels, M. and Lauchle, G., " Wall Pressure Fluctuations and Acoustics in Turbulent Pipe Flow," ARL/PSU TR 86-006, 1986.

DeMetz, F. and Casarella, M., "An Experimental Study of the Intermittent Properties of the Boundary Layer Pressure Field During Transition On A Flat Plate," NSRDC Report No. 4140, 1973.

Emmerling, R., Meier, G., and Dinkelacker, A., "Investigation of the Instantaneous Structure of the Wall Pressure Under a Turbulent Boundary Layer," AGARD Conference Proceedings No. 131 on Noise Mechanisms, p. 24.1, 1973.

Flowes Williams, J.E., "Hydrodynamic Noise," Annual Review of Fluid Mechanics, Vol. 1, p. 197, 1969.

Huang, T. and Hannan, D., "Pressure Fluctuations in the Region of Flow Transition," DTNSRDC Report No. 4723, 1975.

Johansson, A., Her, J. and Haritonidis, J., "On the Generation of High Amplitude Wall Pressure Peaks in Turbulent Boundary Layers and Spots," J. Fluid Mech., Vol. 175, p. 119, 1987.

Kraichnan, R., "Pressure Fluctuations in Turbulent Flow Over a Flat Plate," JASA, Vol. 28, p. 378, 1956.

Lauchle, G., "Acoustic Efficiency of Boundary Layer Transition," ARL/PSU TM 78-285, 1978.

Mautner, T. and Van Atta, C., "An experimental Study of the Wall Pressure Field Associated With a Turbulent Spot in a Laminar Boundary Layer," J. Fluid Mech., Vol. 118, p. 59, 1982.

Mautner, T., "Investigation of the Wall Pressure, Wall Shear Stress and Velocity Fields Associated With a Turbulent Spot in a Laminar Boundary Layer," Ph.D. Thesis, University of California, San Diego, 1983.

Narasimha, R., Subramanian, C. and Badi Narayanan, M., "Turbulent Spot Growth in Favorable Pressure Gradients," AIAA J., Vol. 22, p. 837, 1984.

Schewe, G., "On the Structure and Resolution of Wall Pressure Fluctuations Associated With Turbulent Boundary Layer Flow," J. Fluid Mech., Vol. 134, p. 311, 1983.

Schloemer, H., "Effects of Pressure Gradients on Turbulent Boundary Layer Wall Pressure Fluctuations," JASA, Vol. 42, p. 93, 1967.

Willmarth, W. and Roos, F., "Resolution and Structure of the Wall Pressure field Beneath a Turbulent Boundary Layer," J. Fluid Mech., Vol. 22, p. 81, 1965.

Willmarth, W., "Pressure Fluctuations Beneath Turbulent Boundary Layers," Annual Review of Fluid Mechanics, Vol. 7, p. 13, 1975.

Wygnanski, L., "The Effects of Reynolds Number and Pressure Gradient on the Transitional Spot in a Laminar Boundary Layer. Lecture Notes in Physics, ed J. Jimenez, Vol. 136, p. 304, 1981.

Table 1. Measurements of Turbulent Boundary Layer Wall Pressure Fluctuations on Smooth Walls.

	L.		$b/_{q_1}(\varepsilon, d)$	Transducer	Pressure	Symbol
Investigator	(s.m)	dU, /v	x 10 <sup>3</sup>	Lype	Gradient	- 18
Willmarth & Row (1965)	2	861	54	Flush	Zero	•
Schloemer	7.	101	5.2	Flush	Zcro	
(1967)	2 <b>-</b>	1515	205		NGA	
	×7	142	50		Favorable	5
	5	501	81		PHN	•
	7	=	7.8		Adverse	
Bull	001	159	50	Flush	Zero	D
Blake (1970)		45	10.6	Pinhole	Zero	×
Emmorlino	85	8	6.01	Pinhole	7610	
ct al (1973)		17	6.6	h-lush		2
		202	5.5			
Bull &	- 1-	47	68	Flush	7 cro	
T homas	36.3	57	6.6			
(9761)		2	6.3 7	-	•	1
		97	<	Pinholc	7610	
		20 02	1.0			
Burton	5.	60	10.3	Pinholc	Strong	<
(1973)	3,	102	10.0		Favorable	>
	50	134	9.8			2
	30	38	7.8-8.4		Strong	<b>×</b>
			0.01-0.0		20120	<
Huang & Hannan (1975)	91		150	Pinhol <b>c</b>	Adverse	C
Schewe	19	10	9.6	Flush	Zero	Z
(1983)		39	93	Measured		
		75	<del></del>			
		168	÷.4			
		6	10.5	Flush	Zcro	
		: 6	10.3	Corrected		•
_		15	10.8			
		333	101 88			
Duniels &	12		10.6	Flush	7 cro	
Lauchle (1986)		7	107			
Johansson	<u> </u>	65	7 8	Flush	Zcro	•
ct al (1987)						
Normalized by 1	ocal q					

Table 2. RMS Wall Pressure Fluctuations For Individual Turbulent Spots.

0.0005 0.0005 0.0005
0.010 0.011 0.010
0.3 0.3 0.3
0.01 10.0
91.4 121.9 152.4
Favorable

5





Figure 1. Variation of measured rms wall pressure fluctuations with transducer size and type. /// - Current data. See table 1 for additional symbols.

Figure 3. Frequency of occurrence distribution of rms wall pressure for 500 spots - favorable pressure gradient and  $U_{\infty}$ =10 m/s.  $\Box$ , x=91.4 cm;  $\bigcirc$ , x=121.9 cm;  $\triangle$ , x=152.4 cm.





Figure 2: Frequency of occurrence distribution of rms wall pressure for 500 spots - zero pressure gradient and  $U_{\infty}$ =10 m/s.  $\Box$ , x=91.4 cm;  $\bigcirc$ , x=121.9 cm;  $\Delta$ , x=152.4 cm.

Figure 4. Frequency of occurrence distribution of rms wall pressure for 500 spots - adverse pressure gradient and  $U_{\infty}=10$  m/s.  $\Box$ , x=91.4 cm;  $\bigcirc$ , x=121.9 cm;  $\Delta$ , x=152.4 cm.



Figure 5. Probability density function of p'.  $U_\infty{=}10~m/s;~x{=}152.4~cm;~a)$  zero, b) favorable, and c) adverse pressure gradients.



Figure 6. Comparison of the nondimensional power spectrum for a) zero, b) favorable and c) adverse pressure gradients.

202000000000

