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# Characterization of PEOS Plasma Parameters and Conduction Phase Properties

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## CHARACTERIZATION OF PEOS PLASMA PARAMETERS AND CONDUCTION PHASE PROPERTIES

### I. INTRODUCTION:

The plasma erosion opening switch (PEOS) is a fast, high power, vacuum opening switch which can be used in a variety of configurations for opening switch power conditioning applications.<sup>1</sup> Plasma is injected, in vacuum, between the electrodes of a generator, or driver, previous to the arrival of the power pulse, and physically just before the load and after the previous power conditioning stages. The plasma acts as a short circuit on one time scale and then opens on a much shorter time scale, generating high voltage and delivering a higher power pulse to the load than could otherwise be expected.

Compiled and summarized in this report are data, previously presented in numerous and disparate forums, that characterize the initial plasma parameters and the conduction phase of the PEOS. Of particular importance is the estimated value of the plasma density (including the effect of plasma wall interactions) and ion collection rate used by the Naval Research Laboratory (NRL) in obtaining agreement between the current controlled (magnetic field penetration) PEOS model and observations from experiments. Also of interest are results of experiments investigating the parametric dependencies of the switch conduction current and characterizing the magnetic field (and inferred current) distribution in the switch. There are several experimentally observed properties that uniquely characterize the conduction and opening phase of the PEOS. Among these are the time delay control of the maximum switch conduction current, the broad, predominately radial current channel, the characteristic fast opening, and the transition from fast opening to slow opening. The most useful PEOS model must self-consistently account for these properties while being

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consistent with the best estimate of the PEOS plasma parameters. Thus, building a credible data base in this area is crucial.

Data concerning the characterization of the initial injected plasma, including plasma-surface interactions, obtained from test stand and in situ measurements are found in Sec. II. In Sec. III, we present data that describe the conduction phase of the PEOS and relate them to the measurements described in Sec. II and the current controlled PEOS model. The current conduction process is characterized through measurements of the internal magnetic field distribution. The work is summarized in Sec. IV.

## II. PEOS PLASMA CHARACTERIZATION:

### A. Test Stand Results:

A test apparatus was assembled consisting of a single, Mendel type plasma gun<sup>2</sup> and simulated planar switch electrodes. A schematic of the experiment is shown in Fig. 1. The electrodes were made up of a 70-80% optically transmitting brass screen and an Aerodag coated aluminum plate. The relative spacings in the x direction (Fig.1) were chosen to be identical to those in the radial direction of the cylindrical geometry used in Gamble I experiments.<sup>1,3,4</sup> In Gamble I the radial separation between the cylindrical inner (cathode) and outer (anode) conductors was 2.5 cm and the radial separation between the plasma source and cathode was 10 cm. The apparatus was evacuated to  $\approx 5 \times 10^{-4}$  torr, very similar to the Gamble I experiments. The capacitor driving the gun (0.6  $\mu$ F) was in the standard "doghouse" configuration<sup>2</sup> at an initial voltage of 25 kV. The current into the gun reached  $\approx 40$  kA in  $\approx 0.5$   $\mu$ s.

## TEST APPARATUS GEOMETRY

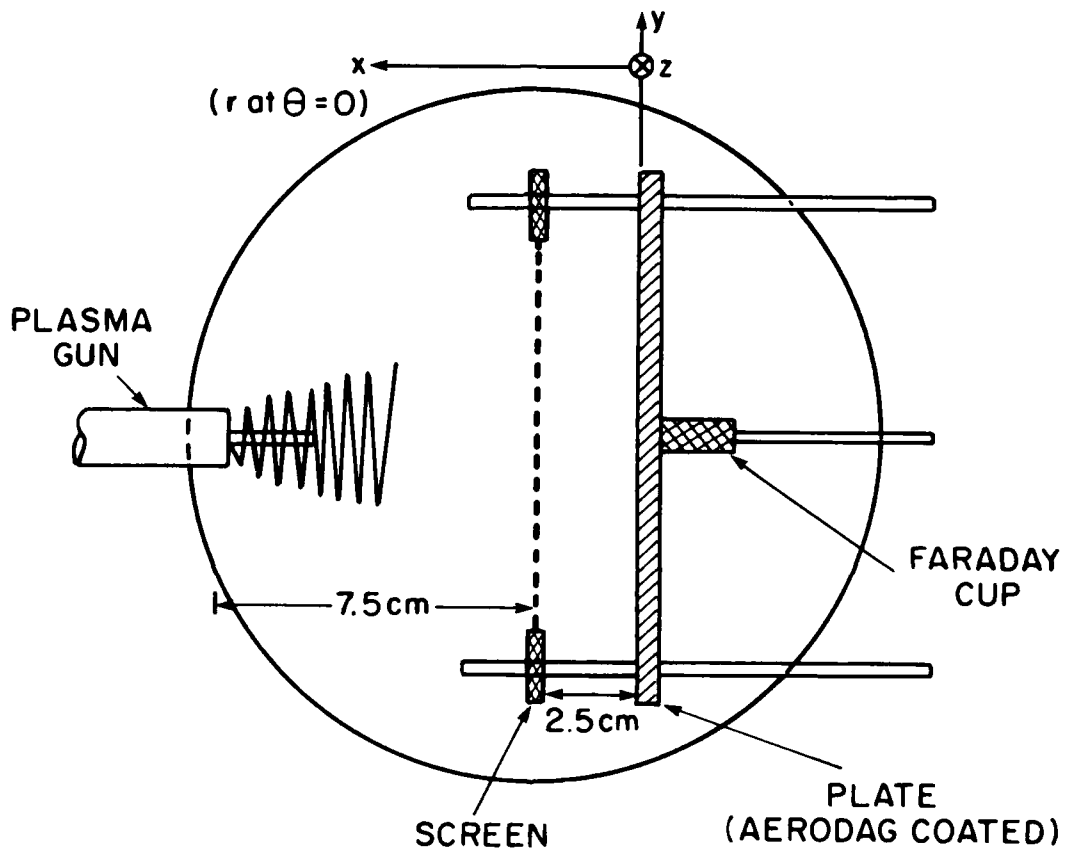


Fig. 1 Schematic of test stand apparatus for measurement of plasma parameters.

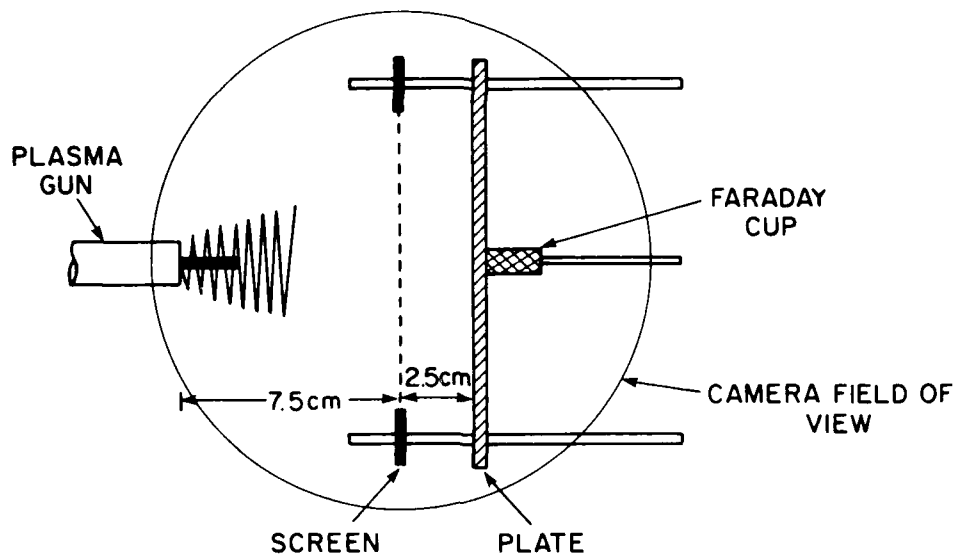
## 1. Time Resolved Photography.<sup>5</sup>

As illustrated in the upper portion of Fig. 2, a framing camera was set up to view the plasma injection region from the side. A sequence of these side viewing framing camera photographs each having 100-ns exposure is shown in the central portion of Fig. 2. The lower portion of Fig. 2 is the signal from a Faraday cup located behind the plate on the axis of the system. Throughout Sec. II, time is measured from the initiation of the gun current.

Visible light does not appear on the plate (cathode) until  $t \approx 1.65 \mu\text{s}$ . This is consistent with gun injected plasma speed of  $\approx 6 \text{ cm}/\mu\text{s}$ . There is no luminosity observed from the inter-electrode region at this time and exposure level. We estimate from the photos that at  $t \approx 2.2 \mu\text{s}$ , the light at the cathode extends into the inter-electrode region  $\approx 10\%$  of the plate screen (cathode-anode) separation, which corresponds to  $\leq 0.2 \text{ cm}$  of emitting plasma. At  $t > 2.2 \mu\text{s}$  both electrodes are quite luminous and some weak emission appears from the inter-electrode region. Data from PEOS experiments<sup>1,3</sup> indicate that fast switching deteriorates rapidly when Gamble I is fired at  $t > 2.2 \mu\text{s}$ . The Faraday cup signal shown in Fig. 2 is well past peak and near zero at  $t \geq 2.2 \mu\text{s}$ .

An illustration of the setup used for side viewing streak photography with the test stand apparatus is shown in the upper portion of Fig. 3. Two streak records at different sweep rates, one slow ( $\approx 7\text{-}\mu\text{s}$  full sweep) and the other fast ( $\approx 3\text{-}\mu\text{s}$  full sweep), are displayed in the central portion of Fig. 3. The Faraday cup signal is shown again for reference in the lower portion of the figure. The gun generated plasma front has an apparent speed of 5-6 cm/ $\mu\text{s}$ . At  $t \geq 2 \mu\text{s}$  a weakly luminous front appears





f/2.2, 100 ns EXPOSURE

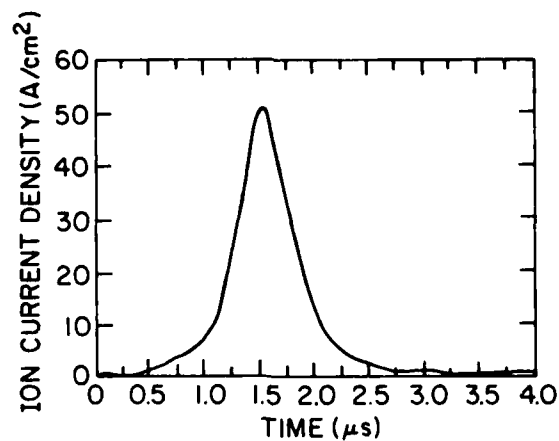
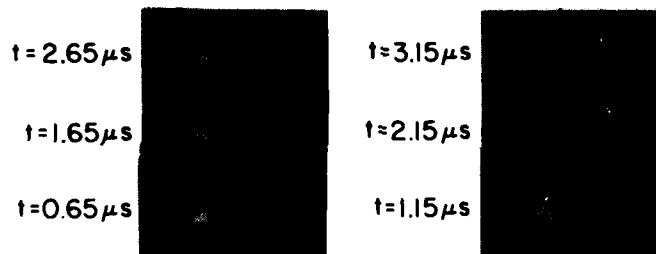


Fig. 2 Upper: Illustration of framing camera field of view for test stand experiments. Middle: Sequence of framing camera photographs. Lower: Faraday cup signal.

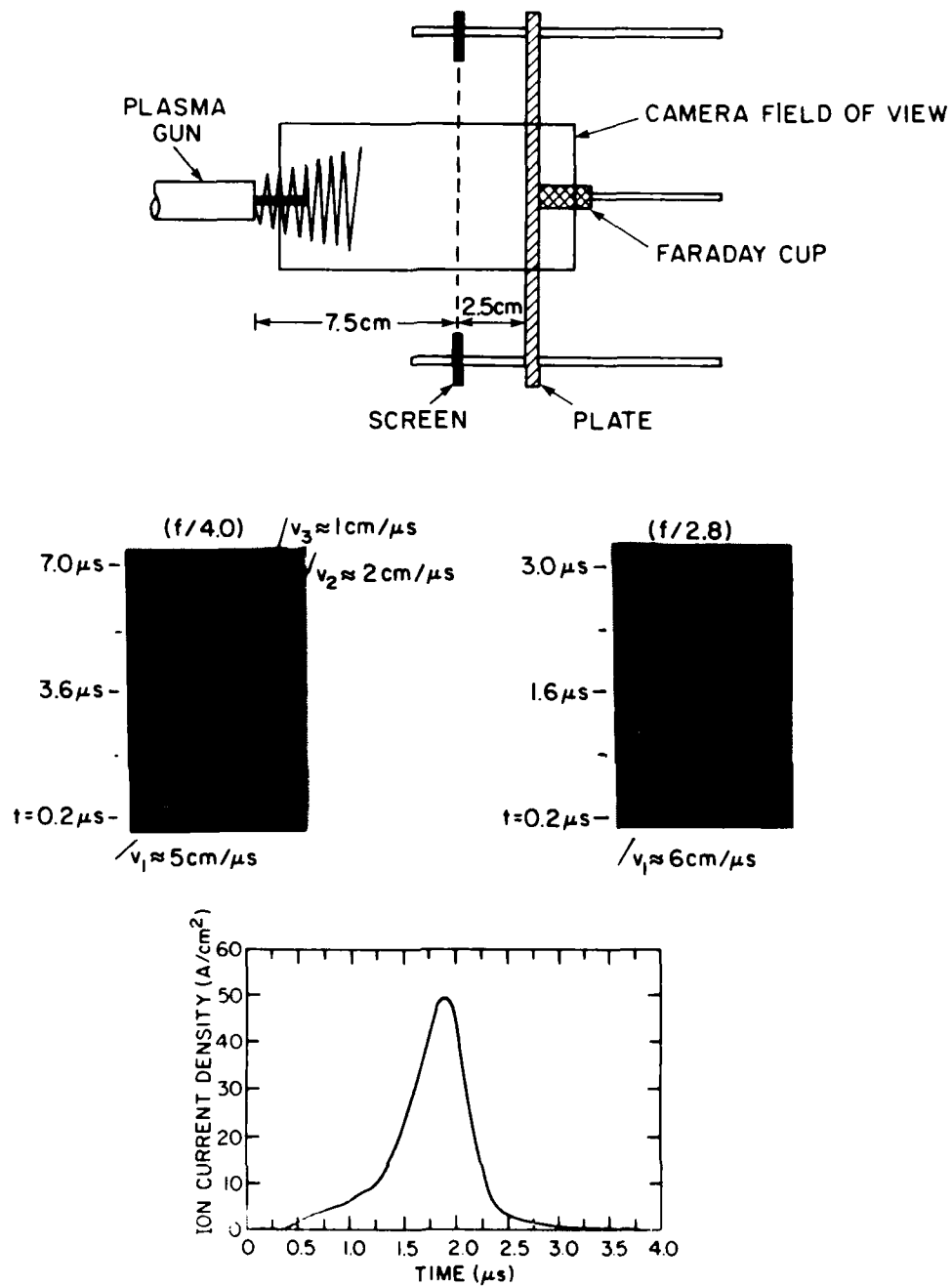


Fig. 3 Upper: Illustration of streak camera field of view for test stand experiments. Middle: Two streak photographs with different time sweeps. Lower: Faraday cup signal.

to move off the screen (anode) at a speed of 1-2 cm/ $\mu$ s. The region of high luminosity at the electrode surfaces occupies  $\leq 10\%$  of the inter-electrode spacing ( $\leq 0.2$  cm) at  $t = 2 \mu$ s and then expands at a speed  $\leq 1$ cm/ $\mu$ s. These results are all consistent with the framing camera photographs in Fig. 2. Again, it is important to note that fast switching is observed<sup>1,3</sup> if Gamble I is fired when  $t \leq 2.2 \mu$ s. After this time, the relative light emission from the surfaces increases, the Faraday cup signal decreases and the switching action degrades.

## 2. Spectroscopy.

The same apparatus described above was used to make both time integrated<sup>5</sup> and time resolved<sup>6</sup> spectroscopic measurements. The experimental arrangement is illustrated in Fig. 4 with the relative spacings between the gun, screen, and plate identical to what is shown in Fig. 1. The entrance slit of the 0.5-m monochromator and lens were adjusted to observe light from a 1-mm wide cross section of the plasma and the mirror could be adjusted to select any line-of-sight parallel to, and between, the plate and screen. The exit slit of the monochromator was chosen to only allow light from a single spectral line to be observed. The line emission was recorded using a photomultiplier operated in its linear response range. A relative calibration of the monochromator-photomultiplier system was performed. Depending on the region of the spectrum, the system sensitivity could change by a factor of  $\sim 6$  over a range of  $\leq 500 \text{ \AA}$ .

If  $N^Z(u)$  represents the density of ions ( $\text{cm}^{-3}$ ) of charge state  $Z$  in the upper (excited) state,  $u$ , of an atomic transition,  $u \Rightarrow 1$

# SPECTROSCOPY EXPERIMENTAL SET UP

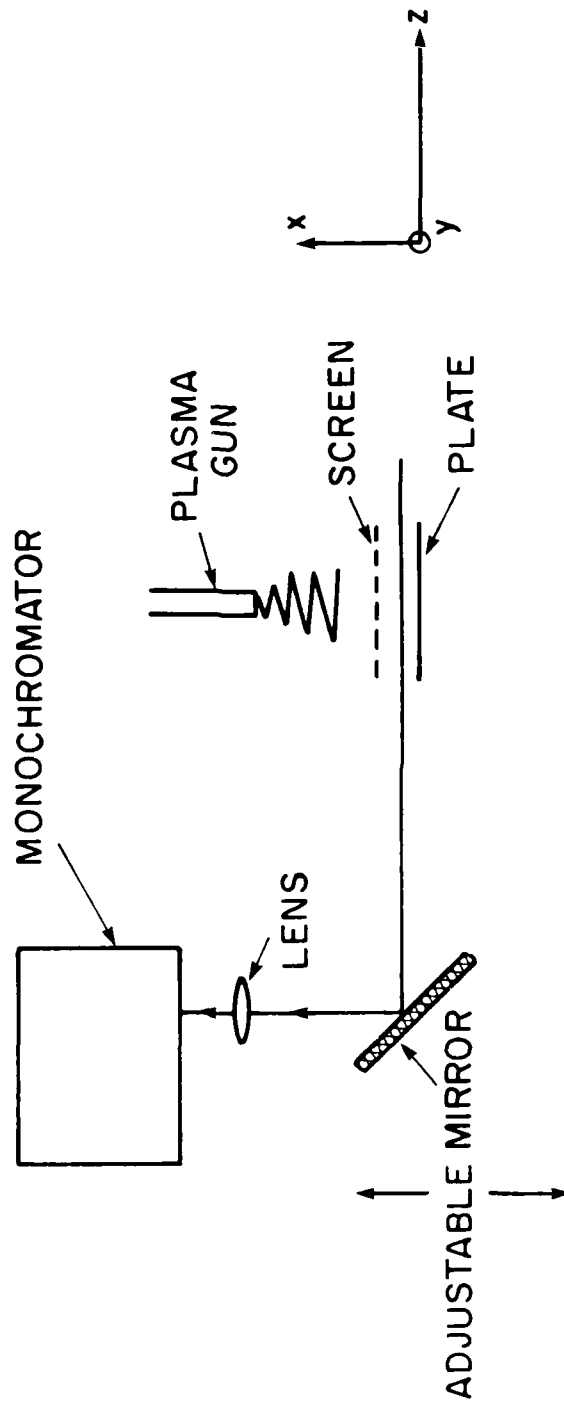


Fig. 4 Schematic of setup for spectroscopic measurements.

(where  $l$  represents the lower state of the transition), then the emission coefficient,  $\epsilon$ , is given by

$$\epsilon = \frac{\Delta E_{ul}}{4\pi} A_{ul} N^Z(u) \left[ \frac{\text{watts}}{\text{cm}^3\text{-sterad}} \right], \quad (1)$$

where  $\Delta E_{ul}$  is the energy emitted in the transition (joules) and  $A_{ul}$  is the transition probability ( $\text{sec}^{-1}$ ). For optically thin lines, the monochromater measures the integral of  $\epsilon$  along the line-of-sight. Depending on the plasma conditions, models<sup>7</sup> can be assumed for both the relationship between  $N^Z(u)$  and  $N^Z(g)$ , the density of ions of charge state  $Z$  in the ground (unexcited) state, and the relationship between the ground state densities of ions of various charge states. For example, in an equilibrium corona model,<sup>7</sup> which is appropriate for many low density ( $\leq 5 \times 10^{14} \text{ cm}^{-3}$ ), high temperature ( $\geq 1 \text{ eV}$ ) plasmas, collisional ionization and excitation by electrons are balanced by radiative recombination and decay, respectively. Thus, it can be shown<sup>7</sup> that for a plasma in which a coronal equilibrium exists

$$\frac{N^Z(g)}{N^{Z+1}(g)} = \frac{\alpha(T_e, Z+1, g)}{S(T_e, Z, g)}, \quad (2)$$

and

$$\frac{N^Z(u)}{N^Z(g)} = n_e \frac{X_{gu}(T_e)}{\sum_{j < u} A_{ju}}, \quad (3)$$

where  $\alpha$ ,  $S$ , and  $X$  are the radiative recombination, collisional ionization, and collisional excitation rate coefficients, respectively,  $T_e$  is the electron temperature, and  $n_e$  is the electron density (also known as the plasma density). The sum in Eq.(3) is over all states  $j < u$ . The units of  $\alpha$ ,  $S$  and  $X$  are  $\text{cm}^3/\text{sec}$ . As can be seen from Eqs. (1)-(3), the plasma properties (density and temperature) and the relative ion density in a

given charge state are highly interrelated. Moreover, the relationship is very model dependent.

A more complete analysis of the distribution of excited states and charge species can be obtained from the collisional-radiative (CR) model.<sup>7</sup> Here, more atomic excitation, relaxation, ionization, and recombination processes are included and the problem rapidly becomes untractable analytically. Numerical calculations using the CR model were performed<sup>8</sup> for a carbon plasma in equilibrium, having ion densities of  $n_i = 10^{13} \text{ cm}^{-3}$ ,  $10^{14} \text{ cm}^{-3}$ , and  $10^{15} \text{ cm}^{-3}$  and at  $T_e = 1, 3, 5, 7$  and  $10 \text{ eV}$  for each density. By comparing predicted line intensity ratios with the observed ratios,  $T_e$  and  $n_e$  can be roughly bracketed, assuming a pure carbon plasma in CR equilibrium and recognizing the model has a necessarily finite nature (i.e. all possible transitions and processes are not included). Note that because of the uncertainties involved in the calculations, the temperatures and densities inferred in this manner only can be used to support other, more direct measurements.

Initial experiments were performed with no screen or plate in the system. Time resolved measurements of emission from CI (2478.6 Å), CII (2837.0 Å), CIII (2296.9 Å), and  $H_\beta$  (4861.3 Å) indicated that under these conditions, only the CIII (doubly ionized carbon) radiation could be observed during any reasonable time of interest ( $\leq 5 \mu\text{s}$ ). We conclude this on the basis of not being able to observe radiation from the other species even when the sensitivity of the measurement was increased by a factor  $\geq 50$ . This observation was confirmed by time integrated spectroscopy, which showed little or no emission from other carbon charge states or other plasma species unless the screen was present. From these results one can conclude that the plasma ejected from the gun is primarily  $C^{++}$  and possibly protons (no measurements of protons were attempted). As described in what

follows, similar data taken with the screen and plate indicate emission from other species near the surfaces, but only for  $t > 1.5 \mu\text{s}$ . For times of interest,  $t < 2 \mu\text{s}$ , the emission from the region between the surfaces does not differ significantly from the case with no surfaces present.

Based on the numerical calculations using the CR model and the measured relative line strengths we estimate that  $10^{13} \text{ cm}^{-3} \leq n_i \leq 10^{14} \text{ cm}^{-3}$  and  $4 \text{ eV} \leq T_e \leq 8 \text{ eV}$ . Over this range the model predicts  $\geq 80\%$  of the carbon is doubly ionized, i.e.,  $\text{C}^{++}$ . Because  $n_e = \langle Z \rangle n_i$ , where  $\langle Z \rangle$  is the effective ion charge state, the average electron density for the gun produced plasma ranges  $2 \times 10^{13} \text{ cm}^{-3} \leq n_e \leq 2 \times 10^{14} \text{ cm}^{-3}$ . Analytical estimates of the relevant atomic rate processes for these conditions imply that for the gun produced plasma alone, the ionization equilibrium is "frozen-in." That is, when the plasma is produced, or very soon after, the relative densities of ions in various charge states reach an equilibrium that stays fixed for many tens of microseconds. The temperature and density were independently measured to be  $\sim 5 \text{ eV}$  and  $\sim 5 \times 10^{13} \text{ cm}^{-3}$  (see Sec. II. A. 3 -4), for which the equilibrium CR calculation predicts that  $> 80\%$  of the carbon is doubly ionized.

In Fig. 5, the time history of the emission from the  $2296.9 \text{ \AA}$  line of CIII, measured with and without the screen, is shown at  $x \approx 2.4 \text{ cm}$  (see Fig. 1). With the screen present, the initial intensity is  $\approx 30\%$  lower, probably a result of the finite screen transparency. However, the emission increases rapidly at  $t > 1.5 \mu\text{s}$ , indicating some kind of plasma-wall interaction phenomenon near the screen. It is at this time (or shortly after) that the streak and framing camera photography indicate enhanced light emission from the screen and plate.

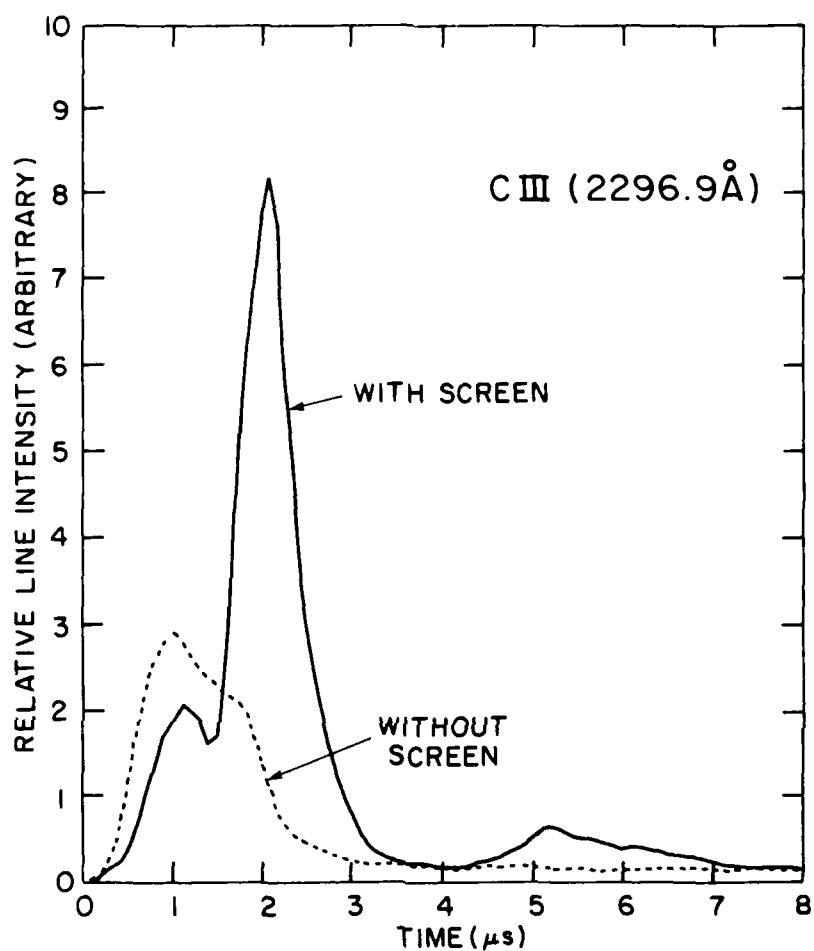


Fig. 5 Time history of CIII (2296.9 Å) spectral line comparing emission with and without screen.



A compilation of the line emission data with surfaces is shown in Fig. 6. Here the CI, CII and CIII emission lines as well as emission from  $H_{\beta}$  (neutral hydrogen) are compared at three inter-electrode positions as a function of time. At  $t \leq 1.5 \mu s$ , there is significant CIII emission everywhere, but no emission from the other carbon species and, as described earlier, no emission is observed from these species when no screen is present. At  $t \approx 1.5 \mu s$ , emission from CII, CI and  $H_{\beta}$  appears from both the screen and plate at roughly the same time. (Note that at a drift speed of  $\geq 7 \text{ cm}/\mu s$ , the gun produced plasma only takes  $\leq 350 \text{ ns}$  to cross the inter-electrode gap.) Clearly, the observed emission from CII, CI and  $H_{\beta}$  is a result of the presence of the metal surfaces. No significant emission is observed from CII, CI or  $H_{\beta}$  at the intermediate position ( $x = 1.5 \text{ cm}$ ) for another  $0.5 - 0.75 \mu s$ . Thus, the ions with  $Z < 2$  that are created as a result of the interaction of the gun generated plasma with the walls diffuse into the region between the electrodes at an effective speed of  $\approx 1 \text{ cm}/\mu s$  (assuming diffusion occurs from both surfaces). This result is consistent with the streak and framing camera photography.

The results of the CR model numerical calculations for this case indicate that for  $t \geq 2.5 \mu s$ , at the measurement locations nearest the surfaces, the ion density has increased slightly to  $n_i \approx 10^{14} \text{ cm}^{-3}$  and the electron temperature has fallen to  $T_e \leq 1 \text{ eV}$ . Under these conditions, the plasma is predominately CII so that  $\langle Z \rangle = 1$  and  $n_e \approx n_i$ . For times of interest ( $t \leq 2 \mu s$ ) in the region between the surfaces, the conditions are very similar to those observed with no surfaces present, which implies  $n_e$  and  $T_e$  are roughly the same as they are when no surfaces are present. Note that here the validity of the assumption of equilibrium used in the CR model is highly questionable, particularly in the transient situation of the injected plasma interacting with the surfaces.

RELATIVE LINE INTENSITIES

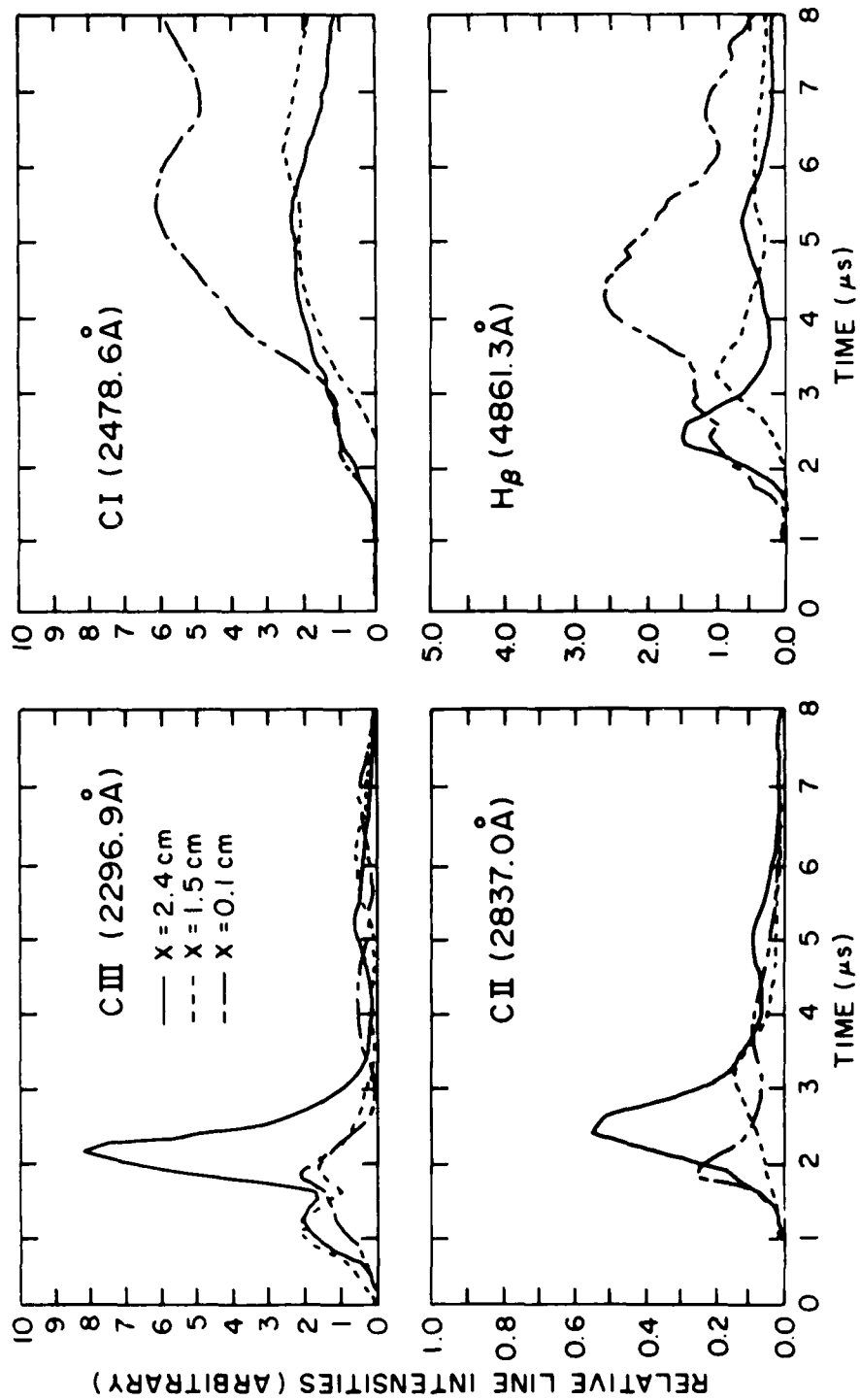


Fig. 6 Time histories of CIII (2296.9 Å), CII (2837.0 Å), CI (2478.6 Å), and H<sub>β</sub> (4861.3 Å) spectral lines at three locations.

We summarize the results of the visible photography and spectroscopy as follows: The gun injected ions are predominately carbon with an effective charge of  $\langle Z \rangle \approx 2$ . The proton fraction has not been determined. If the gun injected plasma was in CR equilibrium the average electron temperature and density would be  $T_e \approx 6$  eV and  $n_e \approx 7 \times 10^{13} \text{ cm}^{-3}$ . No neutral carbon radiation is observed. The temperature and density were independently measured to be in the range of  $\sim 5$  eV and  $\sim 5 \times 10^{13} \text{ cm}^{-3}$  (see Sec. II. A. 3-4). The equilibrium CR calculations for these parameters predict that  $> 80\%$  of the carbon is doubly ionized. When surfaces are present, the bulk of the plasma between the screen and plate remains unchanged for  $t < 2 \mu\text{s}$ . As a result of plasma-wall interactions, lower charge state carbon (CI and CII) and hydrogen evolve from the surfaces after  $t \approx 1.5 \mu\text{s}$ . These species then drift into the region between the screen and plate at an effective speed of  $\approx 1 \text{ cm}/\mu\text{s}$ . Based on the CR equilibrium calculations, we speculate that for  $t \geq 2.5 \mu\text{s}$ , at  $\approx 0.2 \text{ cm}$  from the screen and plate,  $n_e \approx 10^{14} \text{ cm}^{-3}$  and  $T_e \leq 1 \text{ eV}$ .

### 3. Microwave Measurements.

Microwaves are commonly used to measure electron density in plasmas.<sup>9,10</sup> This method is desirable because it is non-perturbing and independent of plasma flow velocity, temperature, and other parameters. Transmission and interferometric measurements were attempted using the test stand described earlier. The general arrangement is shown in Fig. 7. A carbon plasma gun injects plasma between two microwave horns. No additional surfaces or screens were used in these measurements. The sending horn is powered by a Klystron tube that produces microwaves of

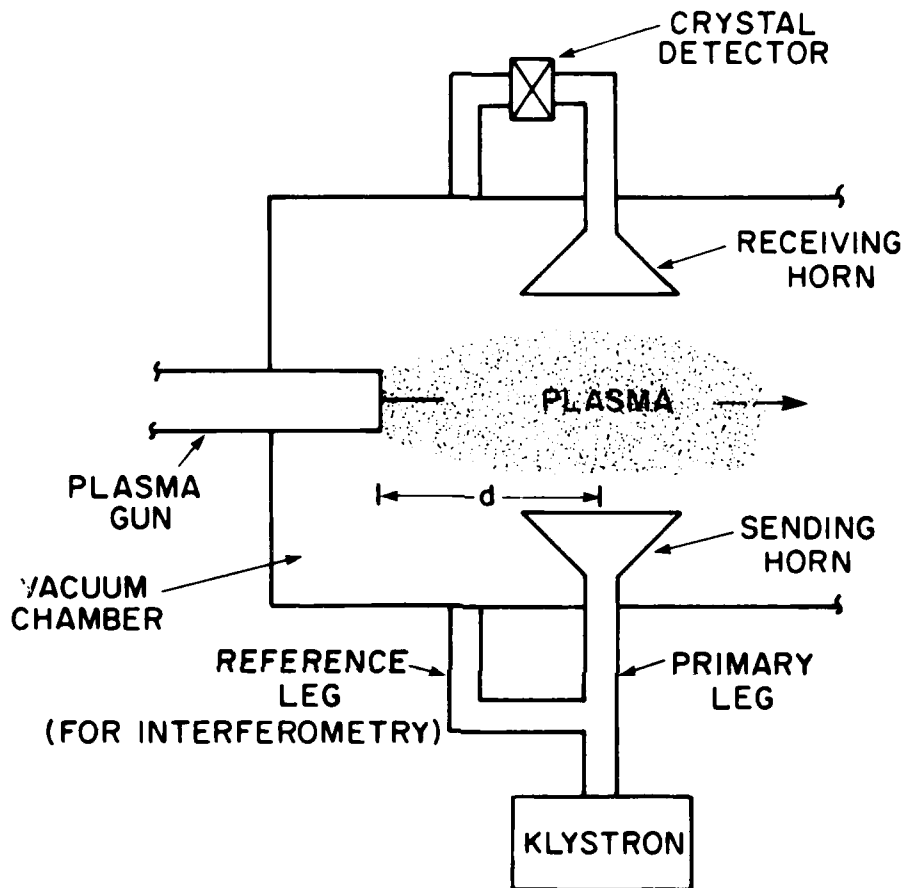


Fig. 7 Schematic of set up for microwave measurements of plasma density.

4.3-mm wavelength (70-GHz frequency) The Klystron provides continuous microwave radiation at a power level of a few 100 mW. The receiving horn collects a fraction (<10%) of the incident energy and the power received is monitored with a crystal detector. This is the simple arrangement used for transmission measurements. Alternatively, the detected microwaves that tranverse the plasma can be added to those detected from a reference leg (i.e., microwaves that traverse a known path that does not intersect the plasma) to form an interferometer. The power in the summed waves is monitored by a detector for interference measurements.

Microwaves travel through a plasma with little attenuation as long as the electron density is below a critical value,  $n_c$ . This critical density is found by equating the electron plasma frequency to the microwave frequency:

$$n_c = 1.24 \times 10^{-8} f^2 = 1.12 \times 10^{13} / \lambda^2, \quad (4)$$

where  $f$ (Hz) and  $\lambda$ (cm) are the microwave frequency and wavelength, respectively. Microwaves will propagate through the plasma with little attenuation (reflection) if  $n_e < n_c$ . For the source used here,  $\lambda = 0.43$  cm and  $n_c = 6 \times 10^{13} \text{ cm}^{-3}$ . When  $n_e > n_c$ , the microwaves are said to be "cut off." This is the principle behind the transmission measurements. The received signal goes to zero when the density somewhere between the horns exceeds  $n_c$  ( $6 \times 10^{13} \text{ cm}^{-3}$ ). Transmission resumes as the density decays away and  $n_e < n_c$ . Limited information can be gained by inspecting the signals before or after cutoff using this measurement technique.

The transmitted power was measured for two cases:  $d = 20$  cm and  $d = 10$  cm (10 cm being the "standard" operating distance in PEOS

experiments<sup>2,3</sup>). Sample data are shown in Fig. 8(a) (at 5  $\mu\text{s}/\text{div}$ ) and Fig. 8(b) (at 1  $\mu\text{s}/\text{div}$ ) for  $d = 20$  cm. Full power (no plasma) corresponds to 1.0 and zero power (no microwaves) corresponds to zero on these traces. The gun current is shown in Fig. 8(c) for timing purposes. As can easily be seen, the microwaves are cut off between 4 and 5  $\mu\text{s}$  after the initiation of the gun current. The peak density remains above  $6 \times 10^{13} \text{ cm}^{-3}$  for  $5 \mu\text{s} \leq t \leq 15 \mu\text{s}$ . Some effects from the presence of plasma are evident for 40  $\mu\text{s}$ . With the gun moved closer to the horns, cutoff occurs earlier, as would be expected. Sample data with  $d=10$  cm are shown in Fig. 9. They indicate cutoff 2.5  $\mu\text{s}$  after the start of the gun current (the initiation of the gun current was at  $t = 2 \mu\text{s}$  on this figure). This agrees with the crude spectroscopic estimates discussed earlier. The peak density stays above  $6 \times 10^{13} \text{ cm}^{-3}$  for at least the next 6  $\mu\text{s}$ . The time response of the detectors is too slow to follow changes faster than  $\approx 1 \mu\text{s}$  so the signals shown in Figs. 8 and 9 can not show any faster time dependence of the microwave power.

Interferometry can be used to measure  $n_e$  as a function of time for  $n_e < n_c$ . The microwaves associated with the primary leg are added to those of a "reference leg," which is tapped off the primary leg before traversing the plasma (see Fig. 7). The phases of the two waves are adjusted so that when no plasma is present they add (constructive interference) and the magnitudes are adjusted so that they are equal. The presence of the plasma will introduce a phase shift in the primary leg. For example, a  $180^\circ$  phase shift in the received waves will cause total destructive interference. Thus, power detected will vary with time as the

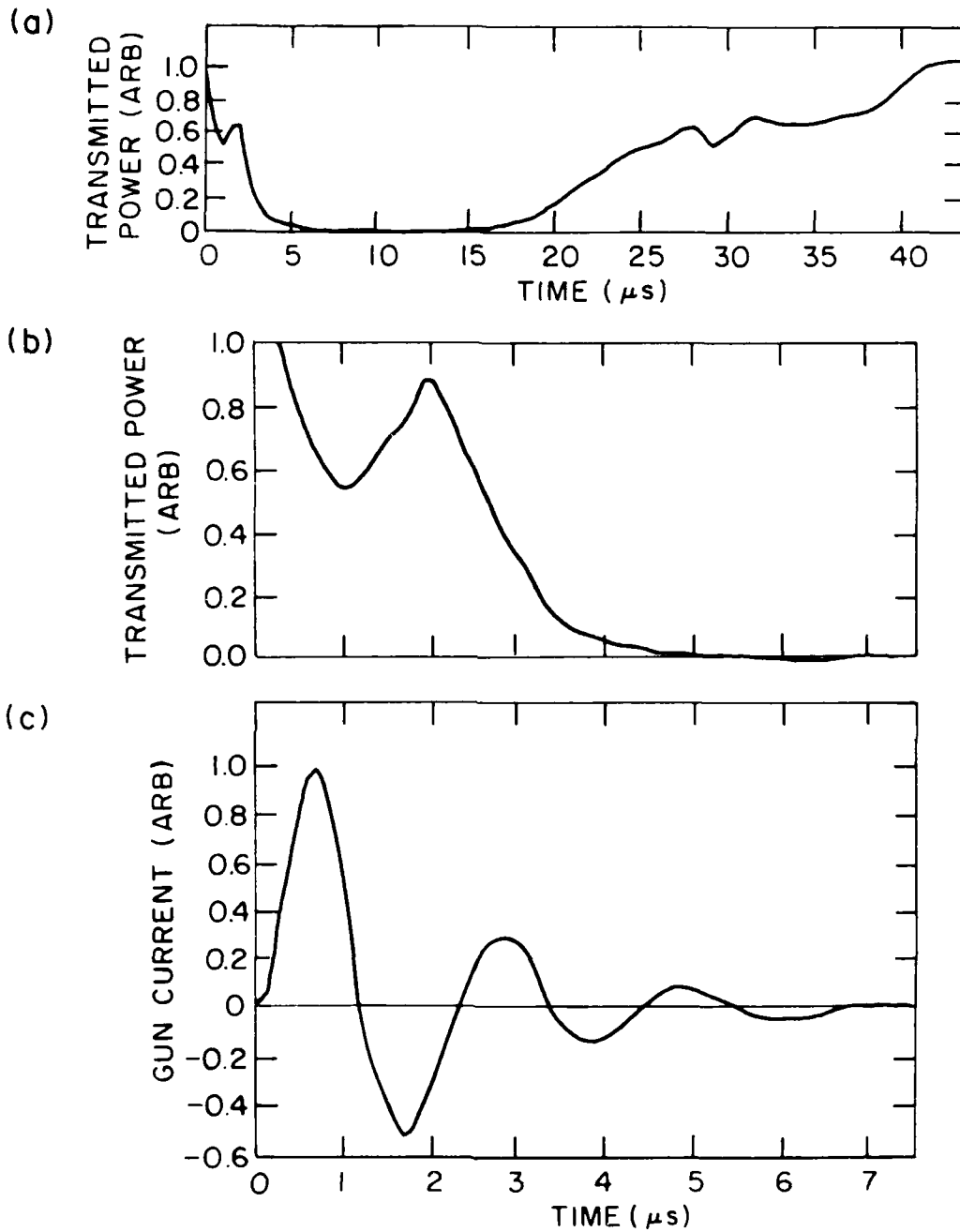


Fig. 8 Illustration of microwave cutoff measurements at  $d=20\text{cm}$ . The plasma density is  $> 6 \times 10^{13} \text{ cm}^{-3}$  at  $t = 5 \mu\text{s}$ .

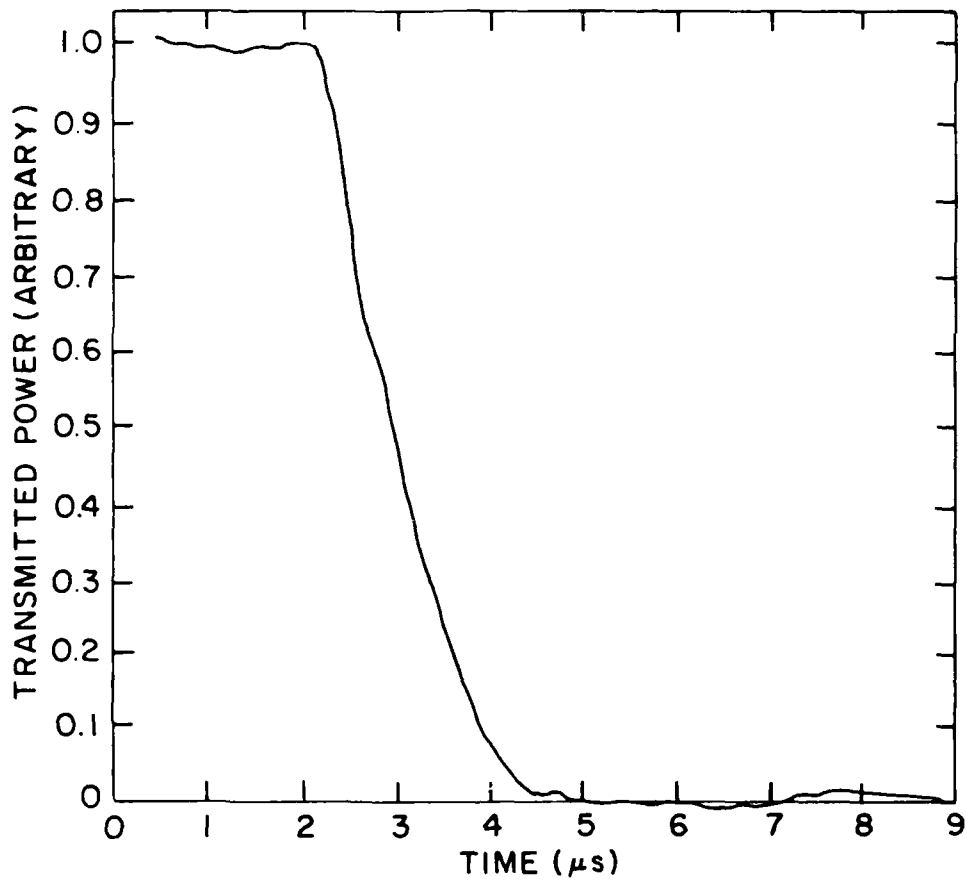


Fig. 9 Illustration of microwave transmission measurements at  $d=10$  cm. The plasma density is  $> 6 \times 10^{13} \text{ cm}^{-3}$  at  $t = 2.5 \mu\text{s}$  (here, gun current starts at  $t = 2.0 \mu\text{s}$ ).



density between the horns changes. The phase change for microwaves traversing a length L of plasma is given by:

$$\Delta\phi = \approx \frac{2\pi}{\lambda} \int_0^L \left[ 1 - \left( 1 - \frac{n_e(x)}{n_c} \right)^{1/2} \right] dx \approx \frac{\pi}{\lambda n_c} \int_0^L n_e(x) dx, \quad (5)$$

where dx is an elemental length along L and we assumed  $n_e \ll n_c$ . By analyzing the interference signal one can obtain  $\Delta\phi$ . Then  $n_e$  can be determined from Eq. (5) if the spacial variation of  $n_e$  is known.

Here, the interferometer uses one detector to measure the power in the summed waves from the reference leg and primary leg (Fig. 7). The primary microwaves have amplitude B(t) and phase change  $\Delta\phi$  from the plasma. The power in the summed waves is then

$$P \propto A^2 + B(t)^2 + 2AB(t) \cos [\Delta\phi(t)], \quad (6)$$

where A is the amplitude of the reference microwaves and  $B(t=0) = A$ . If B(t) is constant (= A), the detected power will oscillate between a maximum value of  $4A^2$  and a minimum of 0 as  $\Delta\phi$  changes from 0 to  $\pi$ . In the actual experiment B is a strong function of time (e.g., for  $n_e > n_c$ ,  $B = 0$ ).

Results with a single detector are shown in Fig. 10 for  $d = 10$  cm at 1  $\mu\text{s}/\text{div}$  and 10  $\mu\text{s}/\text{div}$ . When the microwaves are cutoff,  $B = 0$  and  $P \propto A^2$ . This occurs between  $t = 3$  and 20  $\mu\text{s}$ . There should be many oscillations between  $t = 2$  and 3  $\mu\text{s}$  as the density builds up to  $6 \times 10^{13} \text{ cm}^{-3}$ , but the detector cannot follow the rapid density variation because of its limited time response (as discussed above). When the density

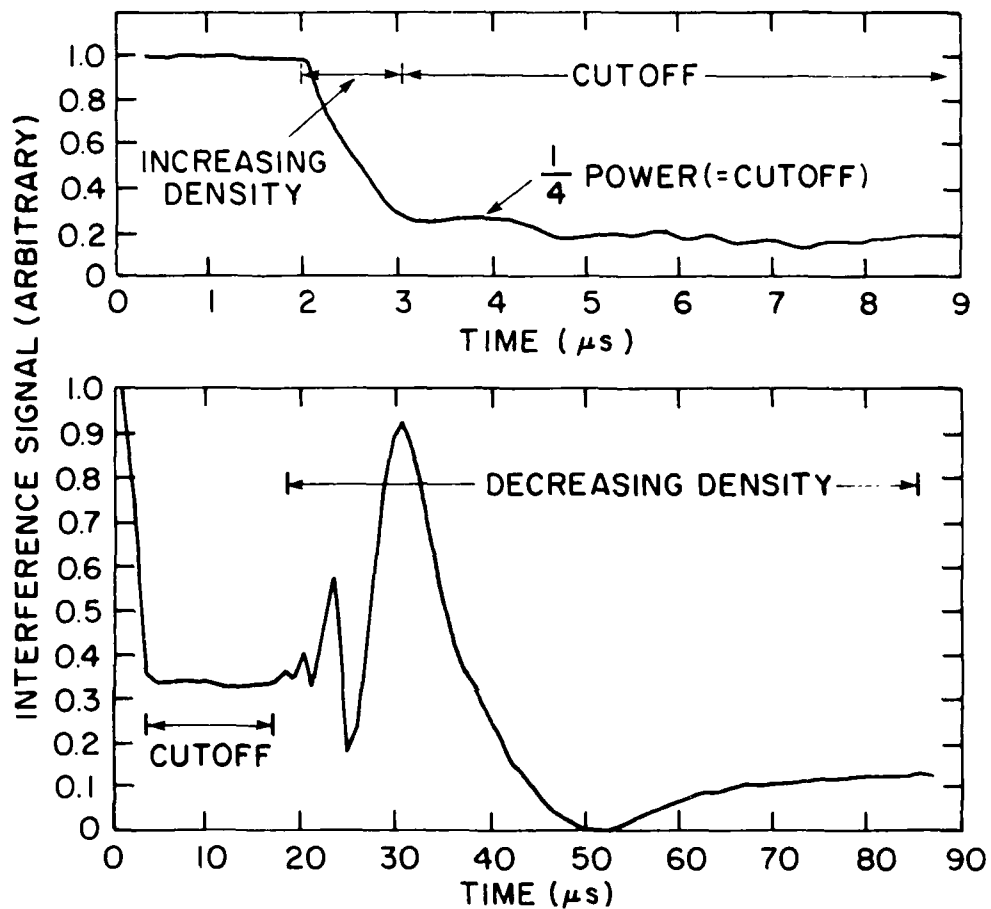


Fig. 10 Illustration of microwave interference measurements at  $d = 20$  cm. Fringes associated with increasing density for  $2 \mu s > t > 3 \mu s$  cannot be resolved because of slow detector response.

decays ( $n_e < 6 \times 10^{13} \text{ cm}^{-3}$ ), oscillations are seen on the slow time sweep for  $t > 20 \text{ } \mu\text{s}$ . Each maximum and minimum corresponds to a change in  $\Delta\phi$  of  $180^\circ$  (so-called "fringes"). For future measurements, better time response is required to monitor density changes in the first  $2 \text{ } \mu\text{s}$  and more detector channels are needed to unambiguously determine if  $\Delta\phi$  is increasing or decreasing.

To "slow down" the density time dependence, the gun-horn distance was increased to  $d = 60 \text{ cm}$ . Interference signals are shown in Fig. 11 at  $1 \text{ } \mu\text{s}/\text{div}$  and  $10 \text{ } \mu\text{s}/\text{div}$ . The detector time response was improved by lowering the termination resistance, but this also decreased the sensitivity. The  $1 \text{ } \mu\text{s}/\text{div}$  trace shows a  $180^\circ$  phase shift  $3 \text{ } \mu\text{s}$  after the start of the gun current, corresponding to an average density of  $2 \times 10^{12} \text{ cm}^{-3}$  over a length of  $12.5 \text{ cm}$  (the diameter of the aperture) for a plasma moving at  $\approx 15\text{-}20 \text{ cm}/\mu\text{s}$ . After  $7 \text{ } \mu\text{s}$ , the density is about  $4 \times 10^{12} \text{ cm}^{-3}$ , etc. The  $10 \text{ } \mu\text{s}/\text{div}$  trace shows the density rise and decay for  $60 \text{ } \mu\text{s}$ . The peak density is probably at  $t = 15 \text{ } \mu\text{s}$ , the second minimum of the interference signal. A second detector sensitive to  $\sin(\Delta\phi)$  is needed to accurately determine  $\Delta\phi$ .

In summary, the microwave transmission measurements yield  $n_e \geq 6 \times 10^{13} \text{ cm}^{-3}$  when  $t \geq 2.5 \text{ } \mu\text{s}$ ,  $10 \text{ cm}$  from the gun. This is supported by the spectroscopic data. The density (somewhere in the line of sight of the microwaves traversing the plasma) remains  $\geq 6 \times 10^{13} \text{ cm}^{-3}$  for  $15\text{-}20 \text{ } \mu\text{s}$ . Although an interference signal has been detected, the measurement technique must be refined to obtain better data. Time resolved density determination using interferometer techniques will be possible with more and faster detectors. (Note in passing that the Faraday cup signal is usually zero at  $t > 2 \text{ } \mu\text{s}$ .)

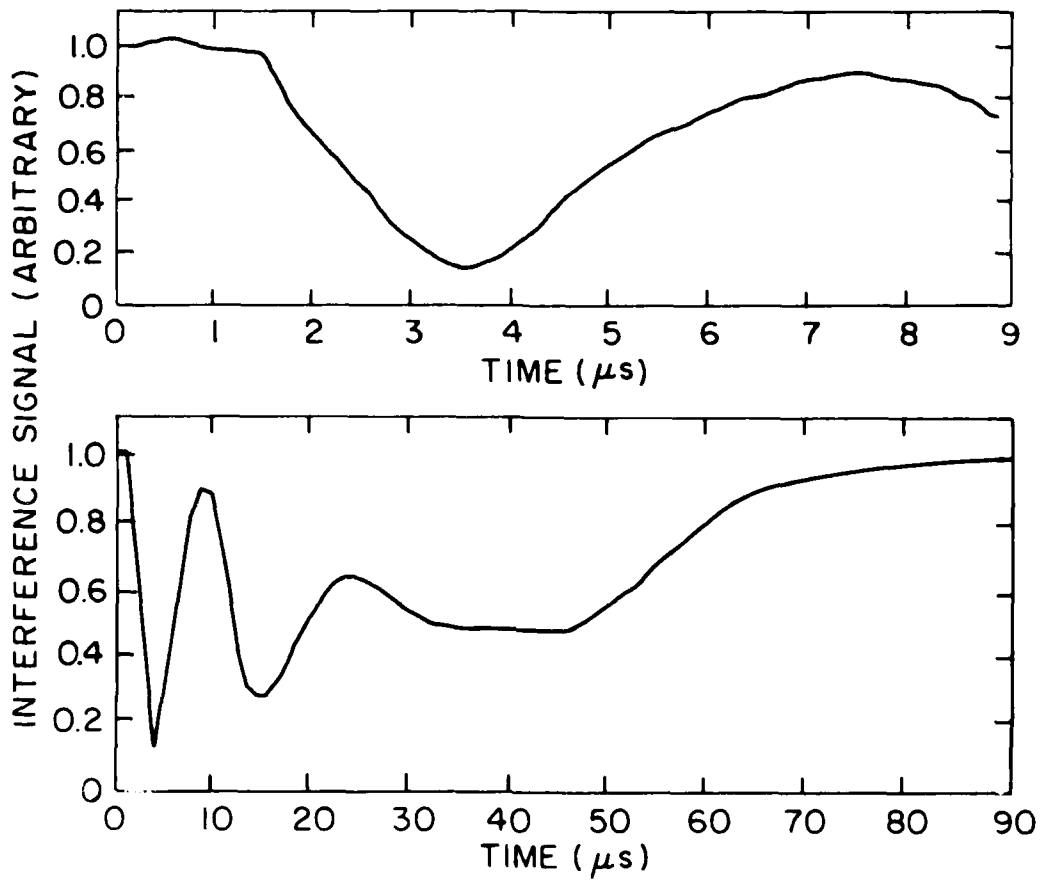


Fig. 11 Illustration of microwave interference measurements at  $d = 60$  cm. The time variation of  $n_e$  is much slower at this large separation distance, so the slow detector response does not prevent resolving fringes.

#### 4. Electric Probe Measurements.

The electron density associated with the gun produced plasma was determined on the test stand apparatus<sup>6</sup> using a double floating electric probe.<sup>11</sup> By varying the voltage between the probe electrodes on a shot-to-shot basis, an I-V characteristic for the probe at any time during the plasma discharge could be generated. The plasma temperature can be determined from the shape of the I-V characteristic.<sup>11</sup> Assuming the probe areas are equal the net current measured in the probe circuit,  $I_p$ , is given by<sup>11</sup>

$$I_p = I_i \tanh(eV/2kT_e). \quad (7)$$

Here,  $I_i$  is the ion saturation current (obtained from the probe characteristic),  $V$  is the applied voltage between the probes, and  $k$  is Boltzmann's constant. Equation (7) is used to calculate  $T_e$ .

The electron density is related to  $I_i$  through

$$I_i = \langle Z \rangle en_i \langle v \rangle A = en_e \langle v \rangle A, \quad (8)$$

where  $e$  is the electron charge,  $A$  is the probe collection area, and  $\langle v \rangle$  is the ion collection velocity appropriately averaged over the probe surface. Two limiting cases are: 1) high velocity, directed plasma flow, which applies at early times in the gun discharge and 2) a quiescent, thermal plasma. If the plasma flow speed  $v_D \gg c_s$ , where  $c_s$  is the ion sound speed  $= \sqrt{kT_e/M_i}$  ( $M_i$  is the ion mass), Eq. (8) results in<sup>12</sup>

$$n_e = \frac{1}{2rl} \left( \frac{I_i}{ev_d} \right) \quad (v_D \gg c_s) . \quad (9)$$

Here  $r$  and  $l$  are the probe radius and length, respectively. Typically  $r \approx 0.025 - 0.05$  cm and  $l \approx 0.5$  cm. For the thermal plasma case,  $\langle v \rangle \approx c_s$  and use of Eq. (8) results in<sup>11</sup>

$$n_e = \left( \frac{1.64}{Ae} \right) \frac{I_i}{\sqrt{kT_e/m_i}} \quad (v_D \leq c_s) . \quad (10)$$

where the dimensionless factor 1.64 is a geometrical correction. Because of uncertainties in the value of  $\langle v \rangle$  and  $A$ , the value of  $n_e$  determined by Eqs. (9) and (10) can be uncertain by a factor  $\approx 2$ .

Measurements were made on the test stand apparatus with a probe and biased Faraday cup 10 cm from the gun and no screen present. Typical results are shown in Fig. 12. The gun current is an underdamped sinusoid with a peak value of 35 kA and .5  $\mu$ s quarter period. The Faraday cup and double electric probe are biased to collect ion saturation current. Both probes peak at the same time,  $t = 1.6$   $\mu$ s. At later times, the electric probe has a large signal while the Faraday cup signal drops to zero. This is attributed to a decrease in plasma flow velocity, making the Faraday cup insensitive to the ambient plasma density which is recorded by the electric probe. The microwave transmission measurements, described in the previous section, indicate cutoff ( $n_e > 6 \times 10^{13}$  cm<sup>-3</sup>) at  $\approx 2.5$   $\mu$ s, as indicated in Fig. 12. The data indicate that at  $t \approx 1.6$   $\mu$ s,  $n_i \approx 1.5 \times 10^{13}$  cm<sup>-3</sup> (Eq. (9)) with  $v_D \approx 6 \times 10^6$  cm/sec. These data are supported by the spectroscopic and microwave transmission measurements. The temperature is  $T_e \approx 6$  eV. Later in time, the density increases to  $> 10^{14}$  cm<sup>-3</sup>.

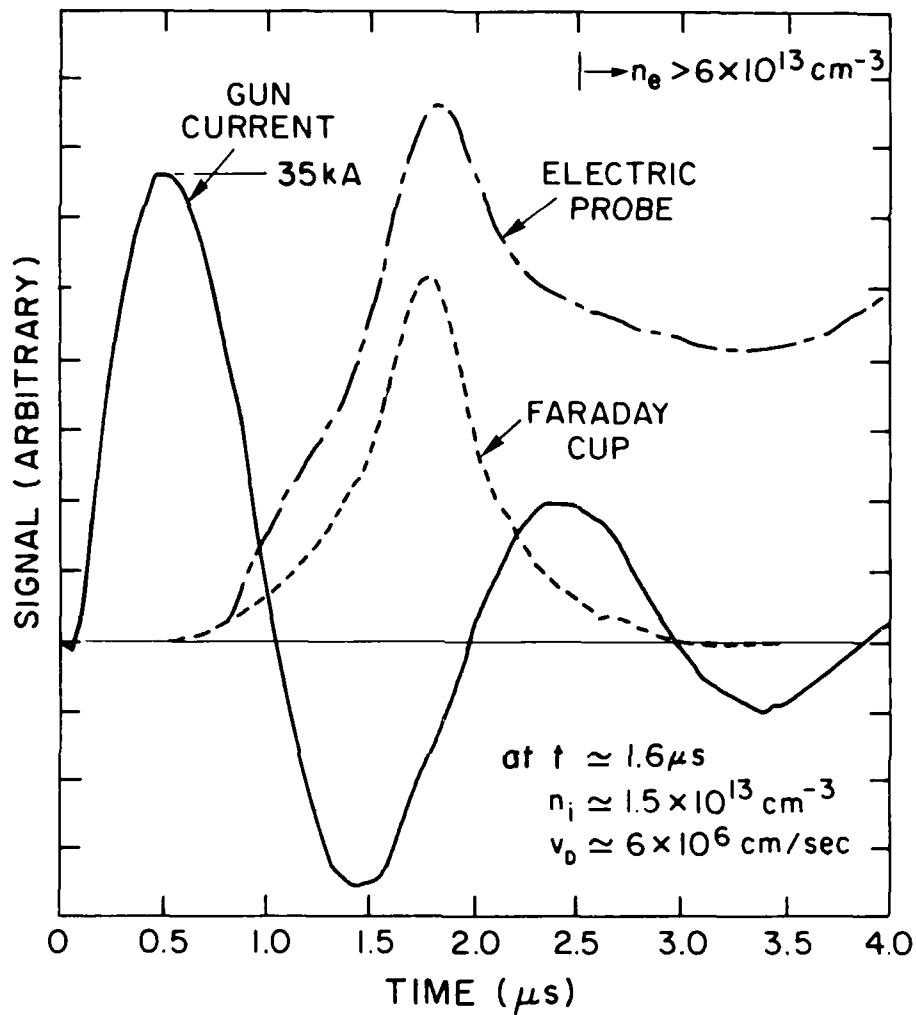


Fig. 12 Typical data from double floating electric probe and Faraday cup located 10 cm from a plasma gun. Also shown is the gun current.

## B. In Situ Measurements.

Results from in situ electric probe measurements<sup>6</sup> are displayed in Fig. 13. The in situ measurements were made inside Gamble I without firing the generator, to characterize the plasma conditions at the time when the PEOS begins to carry current in the presence of electrodes. The switch region was  $\approx 6$  cm in length and  $z=0$  defines the geometrical location of the generator end of the switch. On an actual Gamble I shot, the load would be at  $z \approx 24$  cm. Three guns were used, placed 10 cm from the cathode and  $120^\circ$  apart. For all data shown in Fig. 13,  $T_e \approx 7$  eV. In the left hand portion of Fig. 13 the axial variation of  $n_e$  at  $t \approx 1.8 \mu\text{s}$  (approximately the time of peak Faraday cup signal) is shown. This is the time that would result in optimum switching for Gamble I. The measurements were made midway between the center conductor and outer conductor, under the position of one gun. As seen from the figure, the density maximum is  $n_e \approx 6 \times 10^{13} \text{ cm}^{-3}$  in the middle of the switch region and falls off toward the load and generator ends. The azimuthal variation, shown in the right hand portion of Fig. 13, was obtained in the midplane of the switch region ( $z = 3$  cm) and radially midway between the inner and outer conductors. The data were not as reproducible in this measurement in comparison with the reproducibility of the axial measurements, but they are quite acceptable. Again, these data are taken at  $t \approx 1.8 \mu\text{s}$ . To within  $\pm 35\%$  the density is uniform azimuthally with  $n_e \approx 4.5 \times 10^{13} \text{ cm}^{-3}$  and some suggestion of peaking near the gun locations. Thus, for times of interest ( $t < 2 \mu\text{s}$ ), the plasma density and temperature in the inter-electrode region are essentially the same as those associated with the gun generated plasma when no surfaces are present. These results are supported by the spectroscopic and photographic



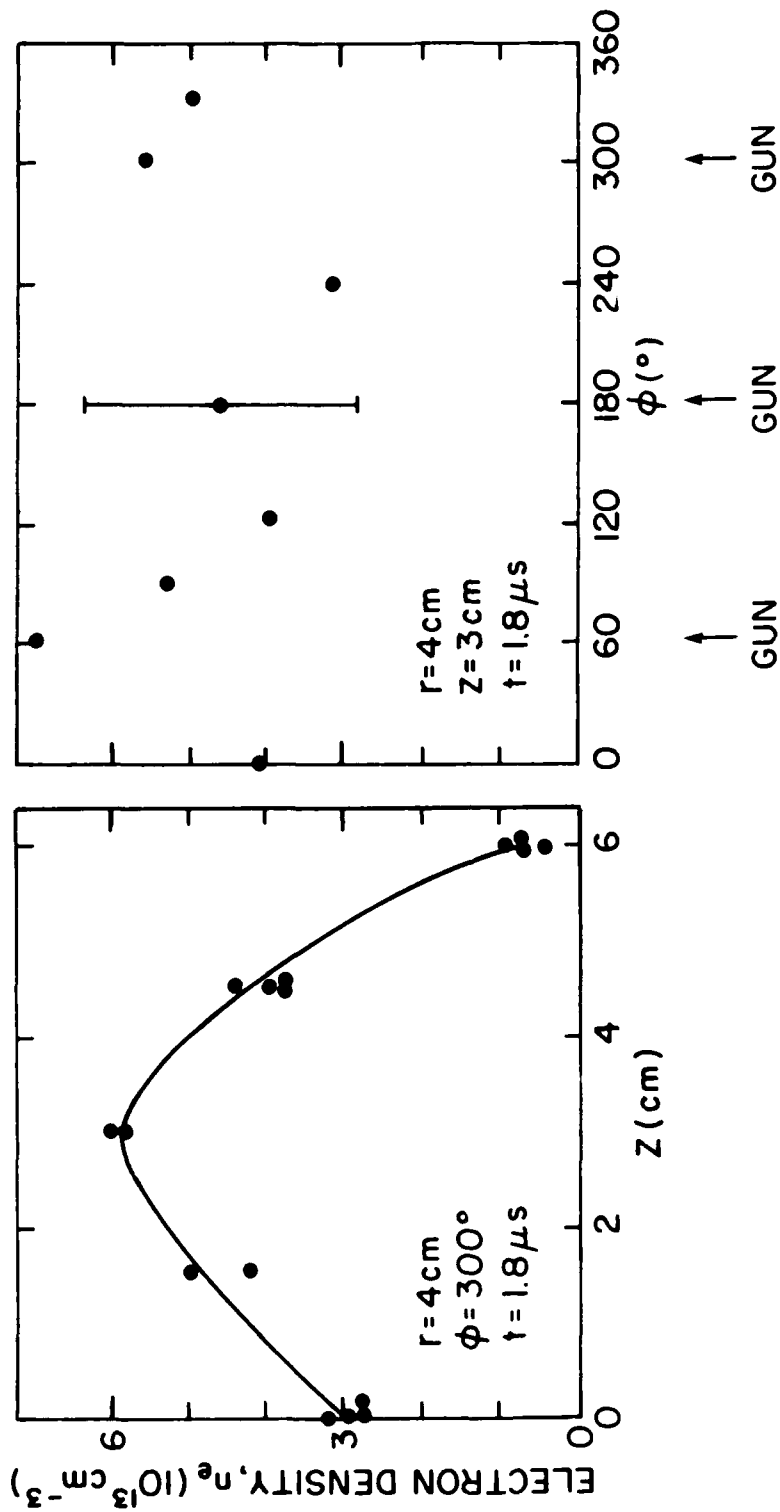


Fig. 13 Electron density distribution in the axial and azimuthal directions at  $t = 1.8 \mu\text{s}$ , determined from double floating electric probe.

data taken on the test stand. The density continues to rise to  $3 \times 10^{14} \text{ cm}^{-3}$  at  $t = 6 \text{ } \mu\text{s}$ . Another important point is that the degree of uniformity illustrated in Fig. 13 using the Gamble I geometry and three plasma guns is apparently sufficient to observe good switch behavior.

The data presented in Sec. II give a consistent picture of the carbon gun plasma parameters. The plasma is primarily doubly ionized carbon,  $\langle Z \rangle = 2$ , with an electron temperature of  $T_e \approx 6 - 8 \text{ eV}$ . The electron density increases in time and reaches  $\approx 6 \times 10^{13} \text{ cm}^{-3}$ , 10 cm from the source, at  $t \approx 2.5 \text{ } \mu\text{s}$ . The plasma flow velocity is  $5 - 10 \text{ cm}/\mu\text{s}$ , higher than the ion sound speed  $c_s \approx 1 \text{ cm}/\mu\text{s}$ . For  $t < 2 \text{ } \mu\text{s}$ , the bulk of the inter-electrode plasma is unaffected by the presence of the metal electrode surfaces. The density between the surfaces continues to increase and temperature decreases with time to  $n_e \approx 3 \times 10^{14} \text{ cm}^{-3}$  and  $T_e \approx \text{eV}$  at  $t \geq 6 \text{ } \mu\text{s}$ . Lower charge state carbon (CI and CII) and hydrogen evolve from the electrode surfaces  $\approx 1.5 \text{ } \mu\text{s}$  after the source is fired and begin to slowly diffuse into the inter-electrode region at  $\approx 1 \text{ cm}/\mu\text{s}$ . These measurements give the approximate values that have been used by NRL in successfully modeling the PEOS.

The flashboard sources have not been as extensively diagnosed as the plasma guns. The approximate values of the plasma parameters are expected to be the same, based on observed switch performance.

### III. CONDUCTION PHASE CHARACTERIZATION

#### A. Time Resolved Photography.

A sequence of streak camera photographs taken of the switch region during Gamble I PEOS experiments<sup>5</sup> is shown in Fig. 14. The load was a short circuit. Three equally spaced plasma guns were located 10 cm from the 2.5-cm radius cathode. Here, time is measured from the initiation of the generator current. Four photographs are shown with the associated current waveforms. Each photograph corresponds to a specific time delay,  $\tau_D$ , between firing the plasma guns and the initiation of current flow through the switch. At  $\tau_D = 1.3 \mu\text{s}$ , no current is carried by the switch and the only visible light is that from the gun region. For the next photograph  $\tau_D = 1.9 \mu\text{s}$ , which is near the optimal delay for switching purposes. As current flows through the switch the outer, screen electrode (anode) becomes bright first, followed by a less intense emission from the inner-electrode (cathode). The region between electrodes does not become bright and the discharge is apparently diffuse. For  $\tau_D = 2.8 \mu\text{s}$ , the switching action is sluggish. More current is carried by the switch for a longer time and both electrodes are bright, the anode lighting up first. The inter-electrode region is still diffuse. When  $\tau_D = 4.5 \mu\text{s}$ , the switch conducts all the current and the inter-electrode region becomes very bright, probably indicating an arc. This may be a result of the plasma associated with surface interactions as discussed in Sec. II. Intense light from the electrodes or switch region is not observed in the absence of switch current. This indicates that there is an interaction at the electrodes during the conduction phase. The emitted light appearing on the anode side

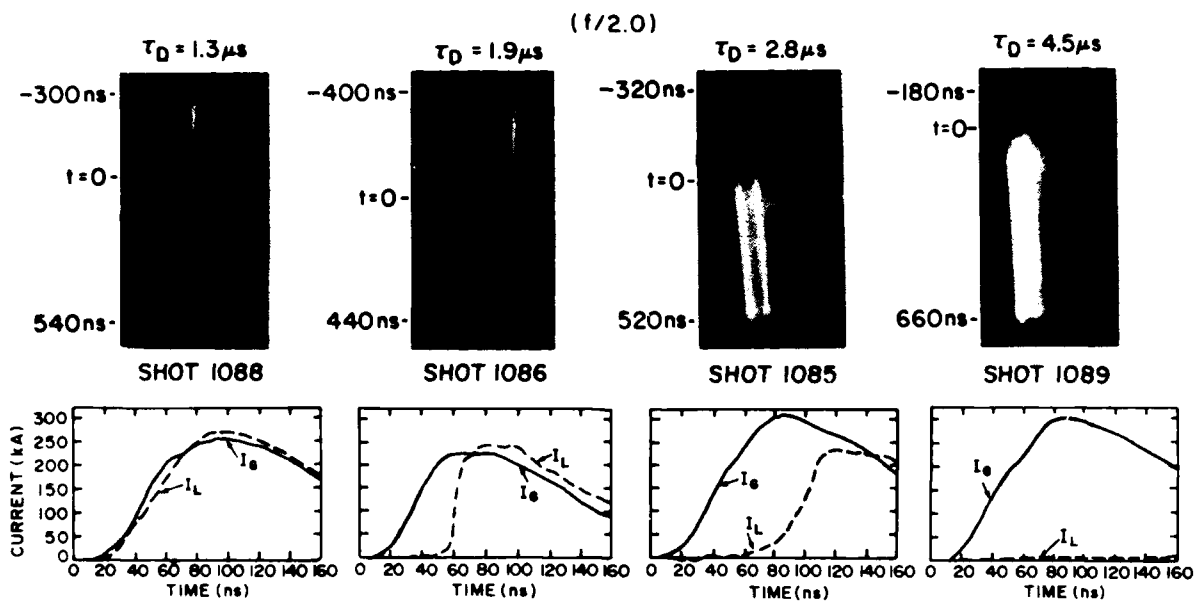
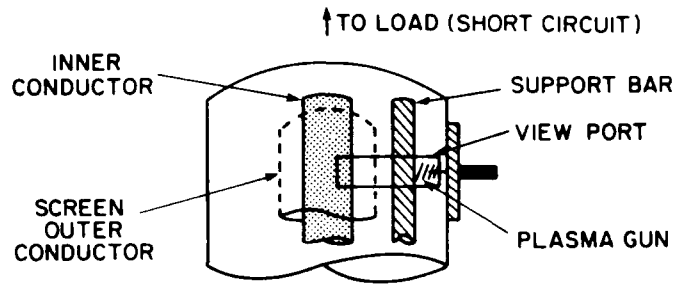


Fig. 14 Upper: Arrangement for streak camera photography during a shot on Gamble I. Middle, lower: Four streak photographs and current traces for various generator delay times.

first may be a result of the anode being a semi-transparent screen. The cathode is solid aluminum, so, in contrast with the screen, light emitted from the far side of the cylinder is not included in the line of sight. At this exposure level, light emitted from the inner and outer conductors as a result of the initial injected plasma (Figs. 2 and 3) is not visible. Thus, the emitted light in these regions are associated with the switch carrying current. This strongly suggests that electrons are emitted from the entire cathode surface.

The same optical arrangement of Fig. 14 was employed with a faster sweep for the streak camera. The result is illustrated in Fig. 15. Here again the light from the anode surface appears first at  $t \approx 60$  ns. Note that this light appears after the conduction phase, as seen from the current trace in the lower portion of the figure. This may be a result of the finite time for atomic excitation, an indication that the plasma density within several millimeters of the cathode is not high enough during conduction for strong light emission to occur. Using approximate relations for collisional excitation rates,<sup>7</sup> one can very crudely estimate that to see light emission resulting from collisional excitation during conduction ( $\leq 100$  ns),  $n_e > 10^{15} \text{ cm}^{-3}$  is required near the surface. We conjecture from the spectroscopic results (Sec II.A.2) that before conduction begins, 0.2 cm from the surfaces,  $n_e \sim 10^{14} \text{ cm}^{-3}$ .

Shown in Fig. 16 is a somewhat different optical arrangement used on the Pollux device by the group at Karlsruhe to observe light emission along a portion of the PEOS cathode.<sup>13</sup> The light emission begins on the generator side of the PEOS and proceeds to the load side at a speed of

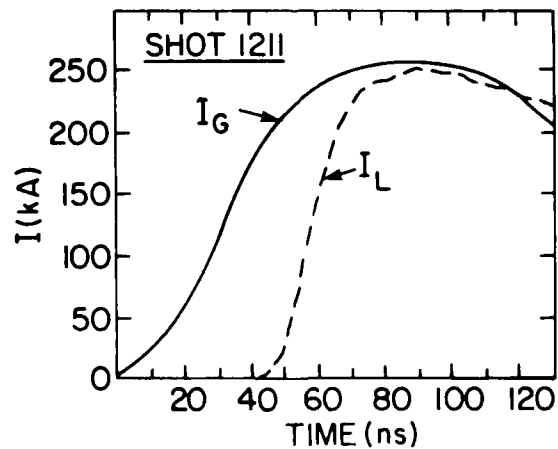
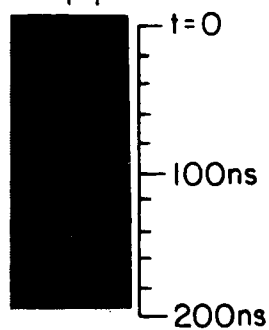
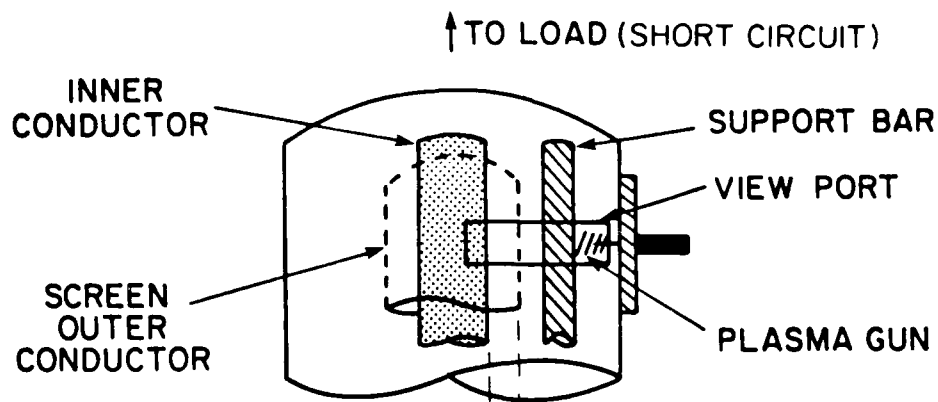


Fig. 15 Upper: Arrangement for fast streak camera photography during a shot on Gamble II. Middle, lower: Fast streak photograph and current trace.

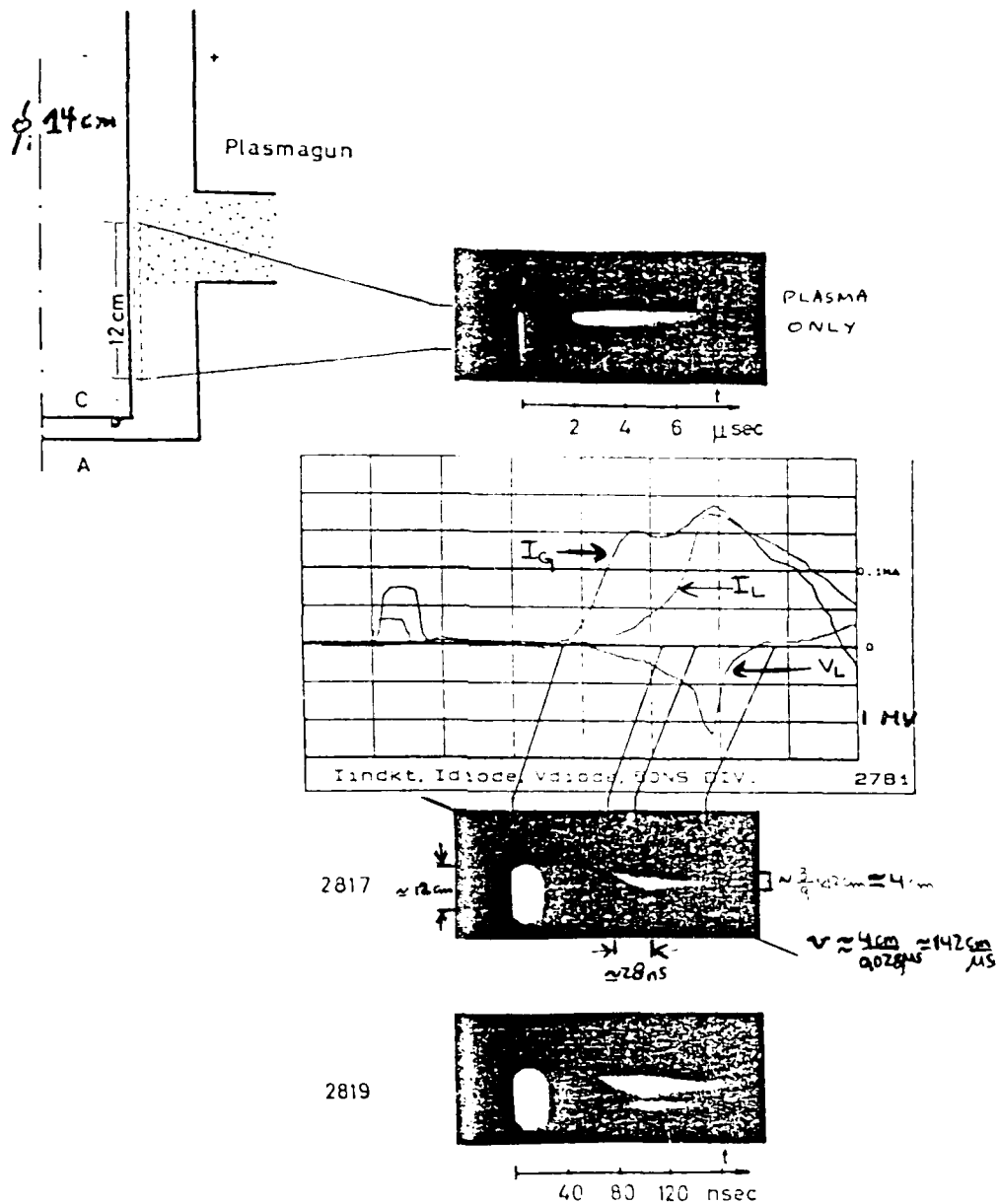


Fig. 16 Upper: Arrangement for fast streak camera photography during a shot on Pollux. Middle, lower: Current traces and fast streak photographs. (Data from Ref. 13).

$\approx 150 \text{ cm}/\mu\text{s}$ . The Karlsruhe group suggests<sup>13</sup> that the interpretation of these photographic data supports the previously proposed NRL current controlled conduction phase model.<sup>1,14,15</sup> If the magnetic field penetration is slow compared with the current rise the critical current density for erosion is exceeded locally, before the current is carried throughout the full axial extent of the switch plasma. In this case the erosion front migrates through the switch plasma. The conduction time is determined by the speed of this erosion front and the axial extent of the plasma. As soon as the erosion front reaches the load end of the switch plasma, the switch begins to open. This interpretation agrees with the conduction current measurements and magnetic probe data presented in the next section.

#### B. Conduction Current Scaling

A fundamental aspect of the NRL current controlled PEOS model<sup>1,14,15</sup> is the assertion that the switch conducts with no voltage appearing at the load end of the switch up to a current limit that is specified by the injected plasma conditions as follows:

$$I_s^0 \approx I_e^0 = \left( \frac{m_i}{Zm_e} \right)^{1/2} Ze (n_i \langle v \rangle) 2\pi r_c l_0 . \quad (11)$$

This current limit is derived from the Child-Langmuir, non-relativistic, bipolar, space-charge-limited flow condition in cylindrical geometry. Here  $I_s^0(I_e^0)$  is the peak switch (electron) current,  $m_e$  is the electron mass,  $r_c$  is the PEOS cathode radius,  $l_0$  is the initial switch length, and  $\langle v \rangle$  the average radial component of the ion velocity at the cathode surface. The term in brackets,  $n_i \langle v \rangle$ , is the ion flux density at the cathode associated with the



injected plasma. We have assumed for this work that the effect of axial  $\bar{J} \times \bar{B}$  forces can be neglected. This assumption is supported by experiments in which the PEOS has successfully opened (albeit more slowly than for short conduction time experiments) after conducting for several hundred nanoseconds (see Ref. 14 and Sec. III.B.4 below).

1. Scaling of  $I_S^0$  of with  $\tau_D (n_i \langle v \rangle)$ .

According to Eq. (11),  $I_S^0 \propto n_i \langle v \rangle$ . The quantity  $n_i \langle v \rangle$  is extremely difficult to measure. Measurements of  $n_i$  alone (in the bulk of the plasma) using spectroscopy, microwave transmission, and double floating electric probes are described in Sec II. Usually one uses for  $\langle v \rangle$  the injected plasma drift speed  $v_d$ . At best, this is an overestimate of  $\langle v \rangle$ . One control over  $n_i \langle v \rangle$  the experimentalist has is the relative generator-to-gun delay time,  $\tau_D$ . The measurements (including Faraday cups<sup>5,6</sup>) all suggest that with delays of interest for fast switching ( $\tau_D < 2.2 \mu s$ ), as  $\tau_D$  increases  $n_i$  also increases. If one assumes that  $\langle v \rangle$  scales as the time of flight ( $1/\tau_D$ ), then  $n_i$  increases fast enough that  $n_i \langle v \rangle$  also increases as  $\tau_D$  increases (as is supported by the usual interpretation of the Faraday cup signal, at least until it peaks). Thus, by varying  $\tau_D$  the measured peak switch current can be used in conjunction with Eq. (11) and the estimates of  $n_i \langle v \rangle$  in a simple, self-consistency check. This by no means constitutes a measurement of  $n_i \langle v \rangle$  and only supports the scaling of  $I_S^0$  with  $n_i \langle v \rangle$  in an approximate way.

Using Gamble I with a short circuit load,  $I_S^0$  was measured as a function of  $\tau_D$ .<sup>5</sup> This was accomplished by simply taking the difference between the measured generator and load currents for shots with various  $\tau_D$ . The ion density and drift velocity at different  $\tau_D$  were estimated as described

above from double floating probes and Faraday cups and used in Eq. (11) to predict  $I_S^0$ . Results of these measurements are displayed in Fig. 17. The model and experimental results agree. Note that the values for  $n_i$  and  $\langle v \rangle$  used in this analysis were not measured at the gap-plasma boundary, but represent our best estimate of those parameters in the bulk of the plasma.

### 2. Scaling of $I_S^0$ with $n_i$ .

The effect on  $I_S^0$  of varying only the density was investigated by adding more plasma guns and using the same  $\tau_D$ . Results from Gamble I where  $I_S^0$  was measured as a function of  $\tau_D$  with 3 and 6 guns are displayed in Fig. 18. Doubling the number of guns and firing at the same  $\tau_D$  presumably increases  $n_i$  by a factor  $\sim 2$  and, from Eq. (11), should roughly double  $I_S^0$ . The data indicate that within the scatter  $I_S^0$  increases by a factor  $\approx 1.5$ , about 25% less than predicted. This discrepancy must be investigated further. Note that simply doubling the number of sources may not double the effective density. The scatter in  $I_S^0$  for a given arrangement of guns at any one  $\tau_D$  is  $\leq \pm 5\%$  (Fig. 18). The scatter is more typically  $\leq \pm 10\%$  over all our experience on Gamble I, Gamble II, and Blackjack 5 with guns and flashboards. Data with six guns are also shown with a smaller storage inductance (115 nH vs. 185 nH). This was done to access higher current levels.

### 3. Scaling of $I_S^0$ with $r_c$ .

Using Gamble I with a short circuit load and three guns, the effect of varying the cathode radius on  $I_S^0$  was investigated.<sup>6</sup> Three different cathode radii were used;  $r_c = 2.5, 1.25,$  and  $0.63$  cm. In each

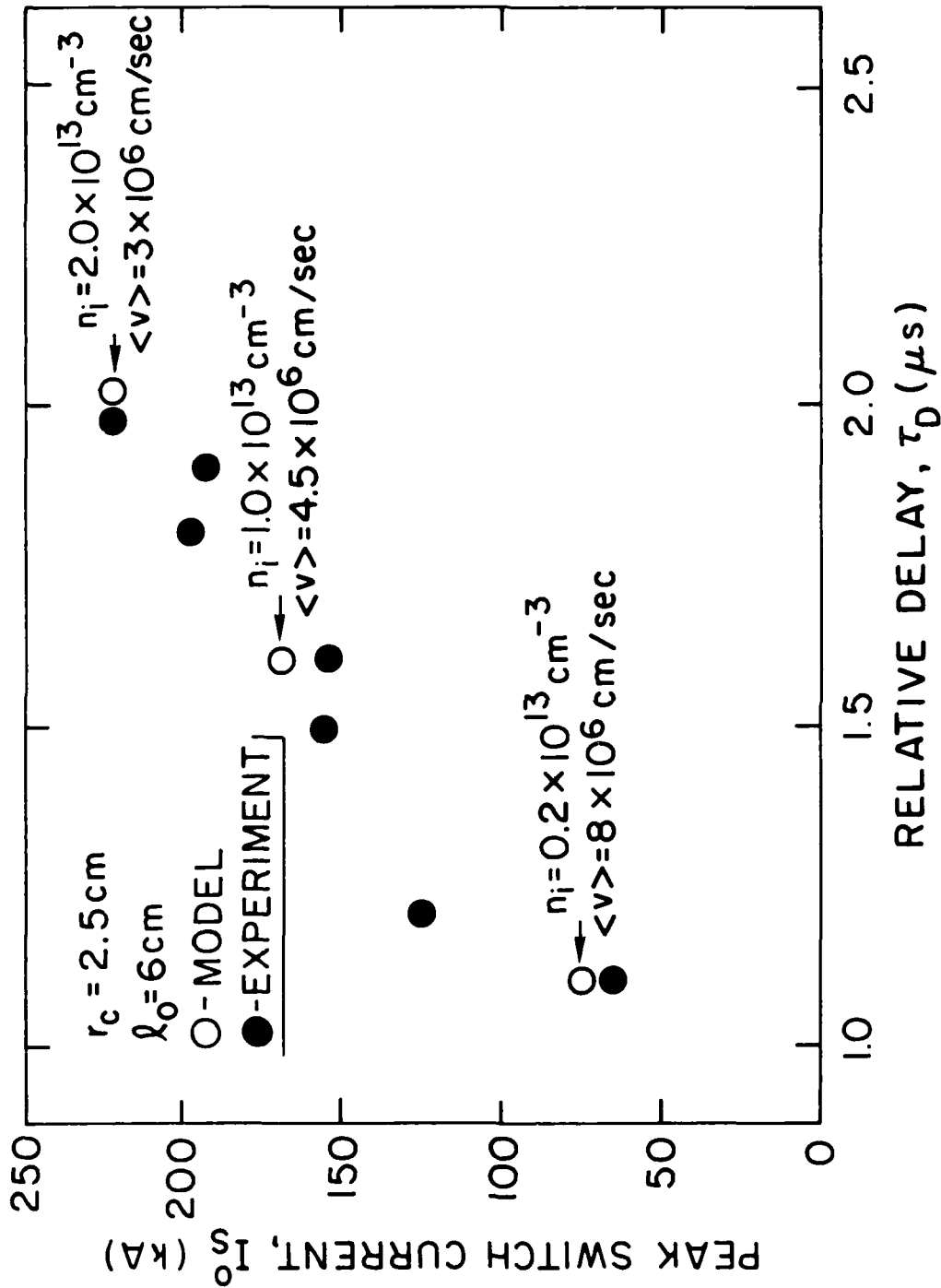


Fig. 17 Peak switch current,  $I_s^0$ , as a function of delay time,  $\tau_D$ . Also shown is result of calculation using best estimate of  $n_i \langle v \rangle$ .

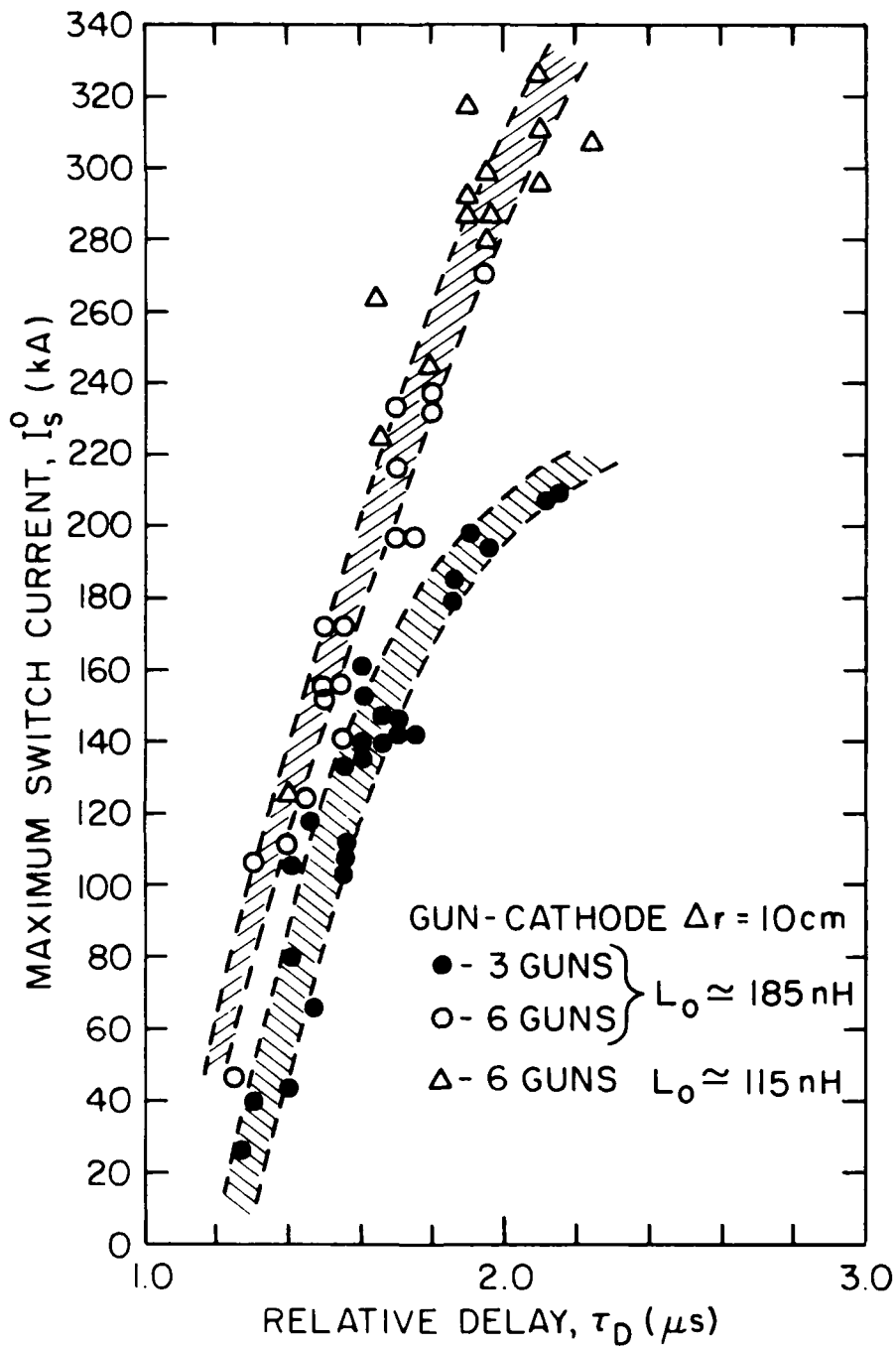


Fig. 18 Peak switch current,  $I_s^0$ , as a function of delay time,  $\tau_D$ , for 3 and 6 guns. Also shown are data with 6 guns and reduced storage inductance.

case the gun-cathode distance was fixed at 10 cm, the switch AK gap was fixed at 2.5 cm, and three guns were used with  $\tau_D \approx 1.6 \mu s$ . The results are plotted in Fig. 19. Also shown are the calculated  $I_S^0$  using Eq. 11. The calculation was normalized at  $r_c = 1.25$  cm. Also,  $n_i$  was scaled with  $r_c$  ( $n_i \propto 1/r_c$ ) to account for a density variation resulting from the change in volume of the switch region. The measurement and calculation agree over this limited range of data.

#### 4. Scaling of $I_S^0$ with Constant $n_i l_0$ .

A third switch conduction scaling experiment was performed on Gamble I, in which the product  $n_i l_0$  was held constant while  $n_i$  and  $l_0$  were each varied.<sup>16</sup> This was accomplished as illustrated in Fig. 20 by using the same 12 plasma guns distributed uniformly over 10-, 20-, and 30-cm lengths. When  $l_0$  was increased, the axial density of plasma sources was decreased by the same factor. The distance between the guns to the PEOS cathode was increased to 15 cm (the usual case being 10 cm) and  $r_c = 2.5$  cm. The results are plotted in Fig. 21. Within the scatter ( $\approx \pm 25$  kA),  $I_S^0$  is independent of  $l_0$  for a given  $\tau_D$  when the product  $n_i l_0$  is held constant, in agreement with Eq. (11). Also plotted in Fig. 20 are data from the recent POP experiment.<sup>14</sup> Here a capacitor bank directly drives the identical Gamble I hardware used to obtain the other data in the figure at about half the current but for a factor of  $\approx 10$  longer time. For up to  $\approx 100$  kA, the scaling of Eq. (11) holds at a factor 10 longer conduction time, demonstrating the current controlled nature of the PEOS conduction. Above 100 kA other factors, such as the capacitor bank being drained of charge, the time variation of the plasma flux density at the cathode, and modification to the bipolar flow condition (not discussed here), may be important.

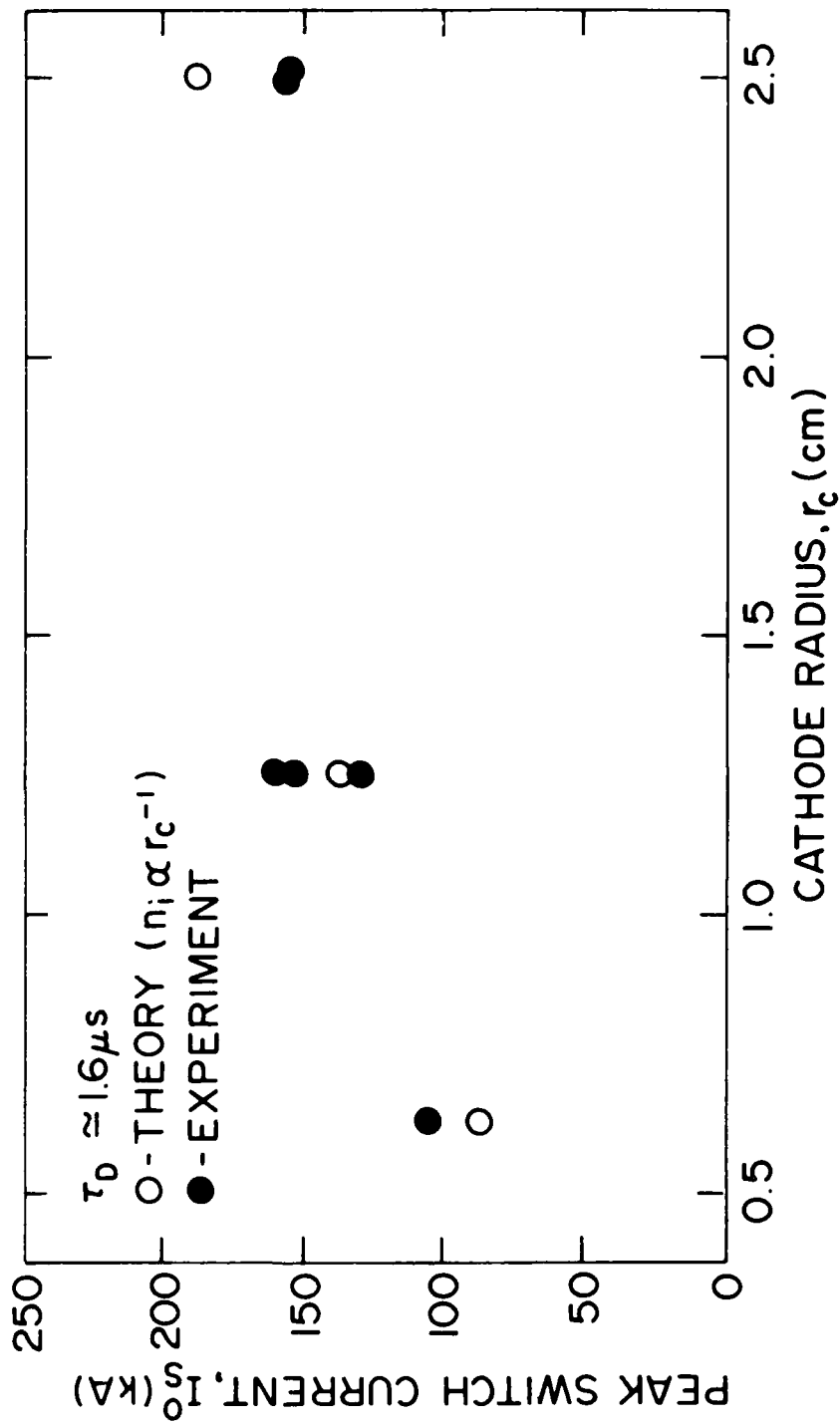


Fig. 19 Peak switch current,  $I_s^0$ , as a function of cathode radius,  $r_c$ . Also shown is result of calculation. For calculation, density was scaled with  $r_c$  to account for volume change.

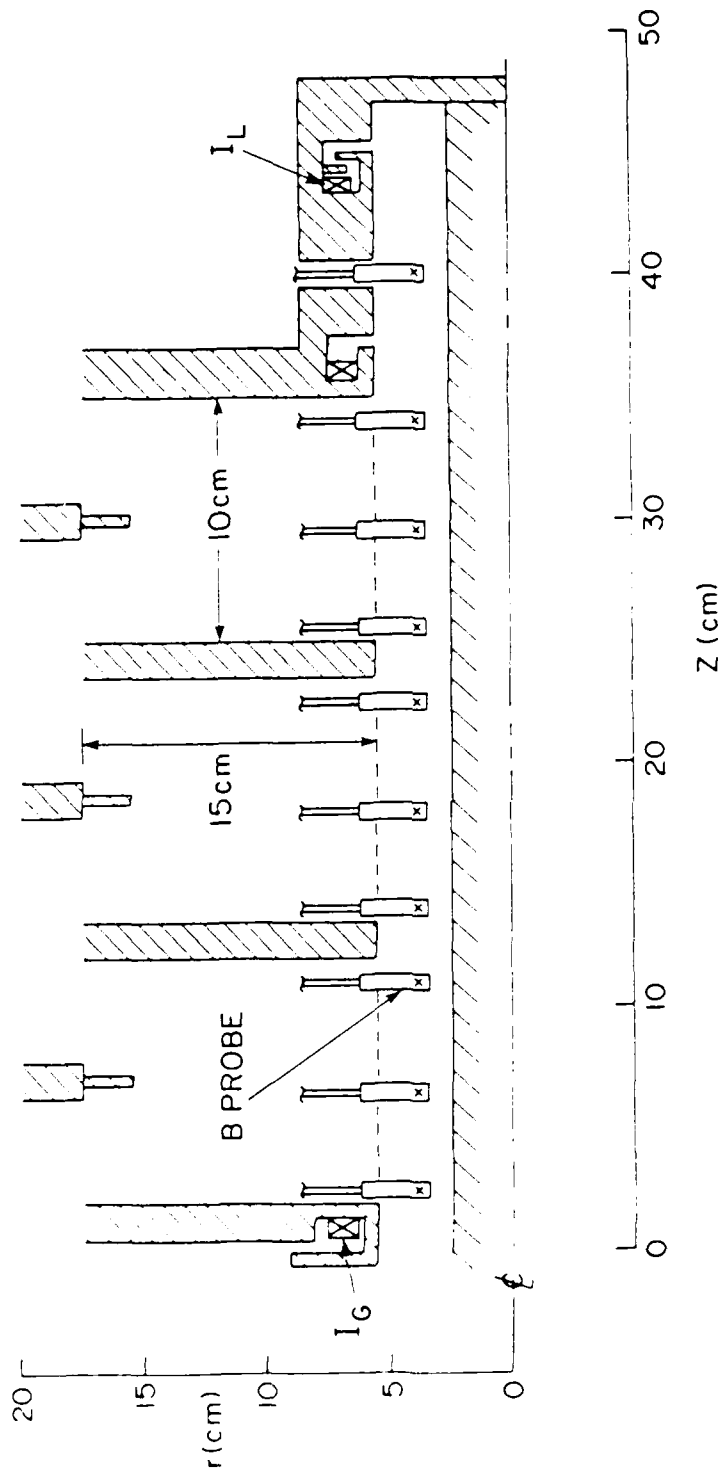


Fig. 20 Schematic of setup on Gamble I for varying  $n_i$  and  $l_0$  while keeping  $n_i l_0$  constant. Also shown are locations for magnetic probes.

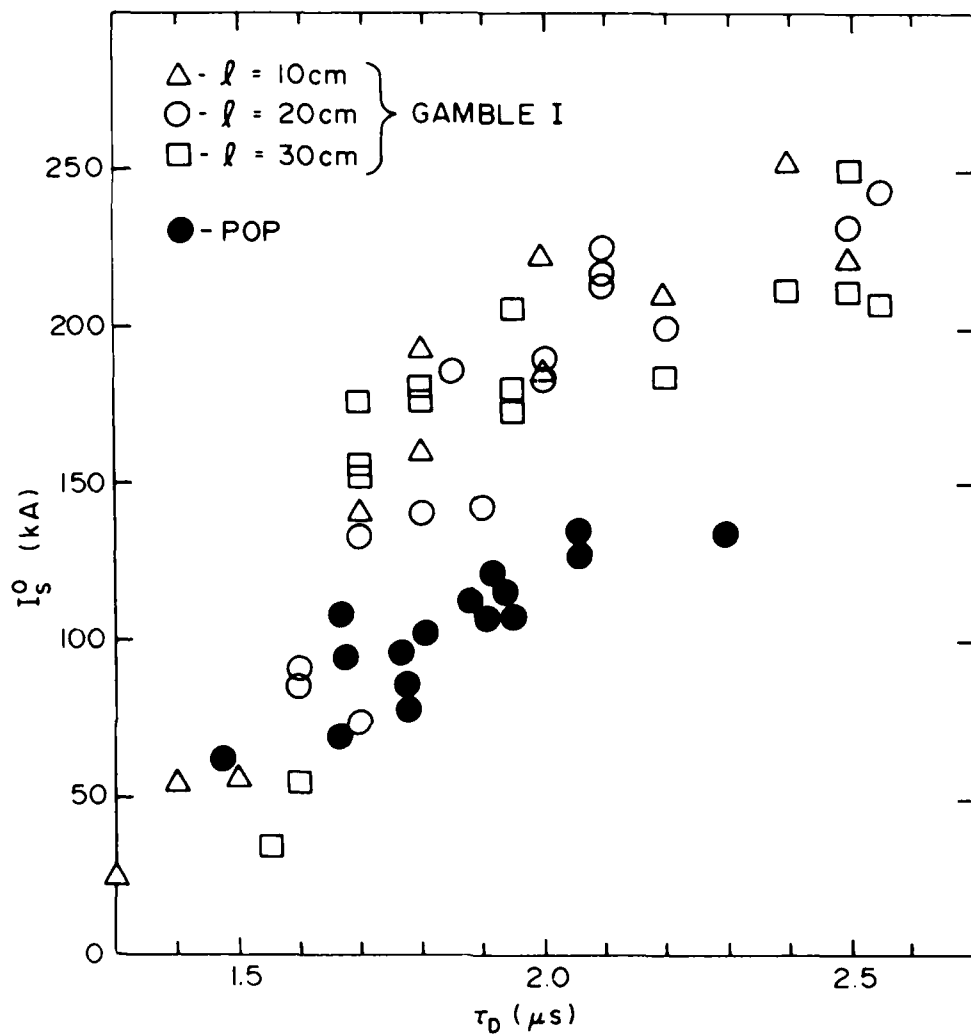


Fig. 21 Peak switch current,  $I_s^0$ , as a function of relative delay time,  $\tau_D$ , for 10-20-, and 30-cm long switch where  $n_i l_o$  was constant for each  $\tau_D$ . Also shown are results with the same  $n_i l_o$  but a factor 10 longer conduction time (POP).



To summarize Sec III.B, the peak current conducted by the PEOS scales approximately in accordance with Eq. (11). The estimates for the values of the plasma parameters obtained from the measurements described in Sec. II and the measured peak switch current are consistent with Eq. (11). The conduction phase of the PEOS appears, from the external current measurements, to be current controlled. Internal measurements of the magnetic field, discussed in what follows, support this assertion and reveal the details of the current distribution in the PEOS.

### C. Magnetic Field Measurements.

A schematic of the setup for measuring the magnetic field in the PEOS<sup>15</sup> during conduction and opening is given in Fig. 22. Five small probes measure the local magnetic field in the PEOS plasma during fast opening shots. The dots represent typical measurement locations. The probes are potted inside 5-mm diam quartz tubes, inserted into the switching region through the screen anode, and oriented to measure the azimuthal field,  $B_{\theta}(t)$ . Usually five axial locations ( $z$ ) at a common radius ( $r$ ) were sampled on a single shot. The probes are calibrated on shots with no plasma relative to the Rogowski loops that measure the generator ( $I_G$ ) and load ( $I_L$ ) current. Several experimental checks were made to determine the perturbative influence of the probes on the measurement. The presence of the probes does not affect the measured currents  $I_G$  and  $I_L$  and the signal obtained from any probe in a given position is independent of the location of other probes. The plasma energy loading on the probes is too small to ablate significant material from the quartz during the time of interest, as evidenced by the condition of the

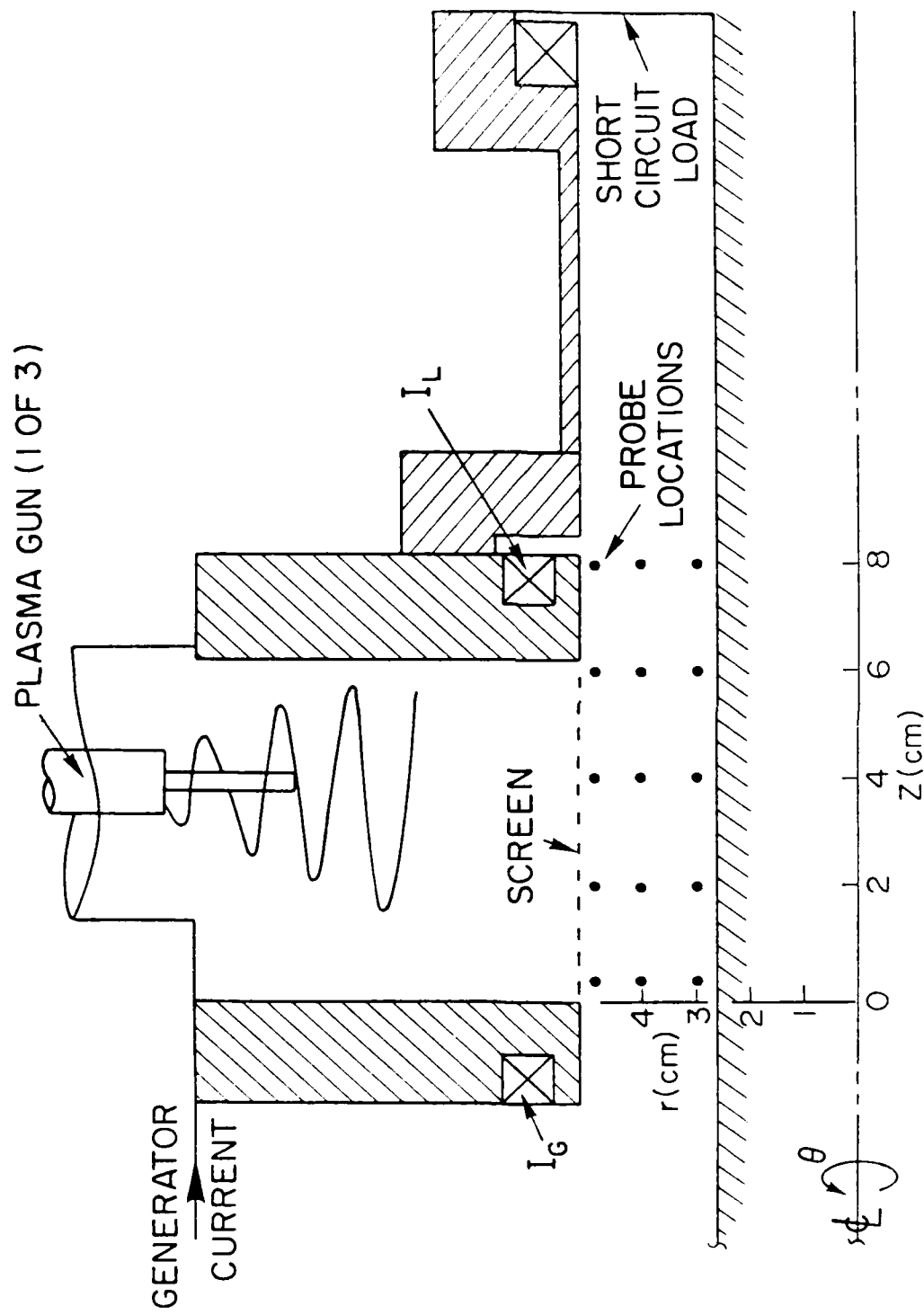


Fig. 22 Schematic of setup for magnetic probe measurements.

probes after use and as supported by analytical estimates. The probe signal goes to zero when it is placed outside the screen. Finally, the probes have a sub-nanosecond response time.

In Fig. 23(a), the probe signals for a fast opening shot are plotted in units of current for various axial positions at the same  $r$ .<sup>6</sup> Also plotted is  $I_L$ . If the field is azimuthally symmetric, then the magnetic field,  $B_\theta$ , measured by the probe is related to the current,  $I$ , flowing under the probe through a circle of radius  $r$  by

$$I(\text{A}) = B_\theta (\text{G}) \times 5r(\text{cm}), \quad (12)$$

where  $r$  is the probe radial position. In this case the difference between the signal seen by two probes at the same  $r$  but different  $z$  is associated with the current flowing under one probe but over the other and thus having a radial component to its flow. As seen in the figure, the current steadily penetrates into the switch plasma with switch opening beginning when the current reaches the load end of the plasma.

To check the assumption of azimuthal symmetry, the probes were arrayed azimuthally at the same  $r$  and  $z$ . Data for the case<sup>6</sup> of a fast opening shot are shown in Fig. 23(b). To within measurement accuracy, the signals indicate an azimuthally symmetric discharge verifying the use of Eq. (12).

These results (for fast opening) are contrasted with a shot at a longer  $\tau_D$  where a slow opening was observed<sup>6</sup> in Fig. 24. As shown in

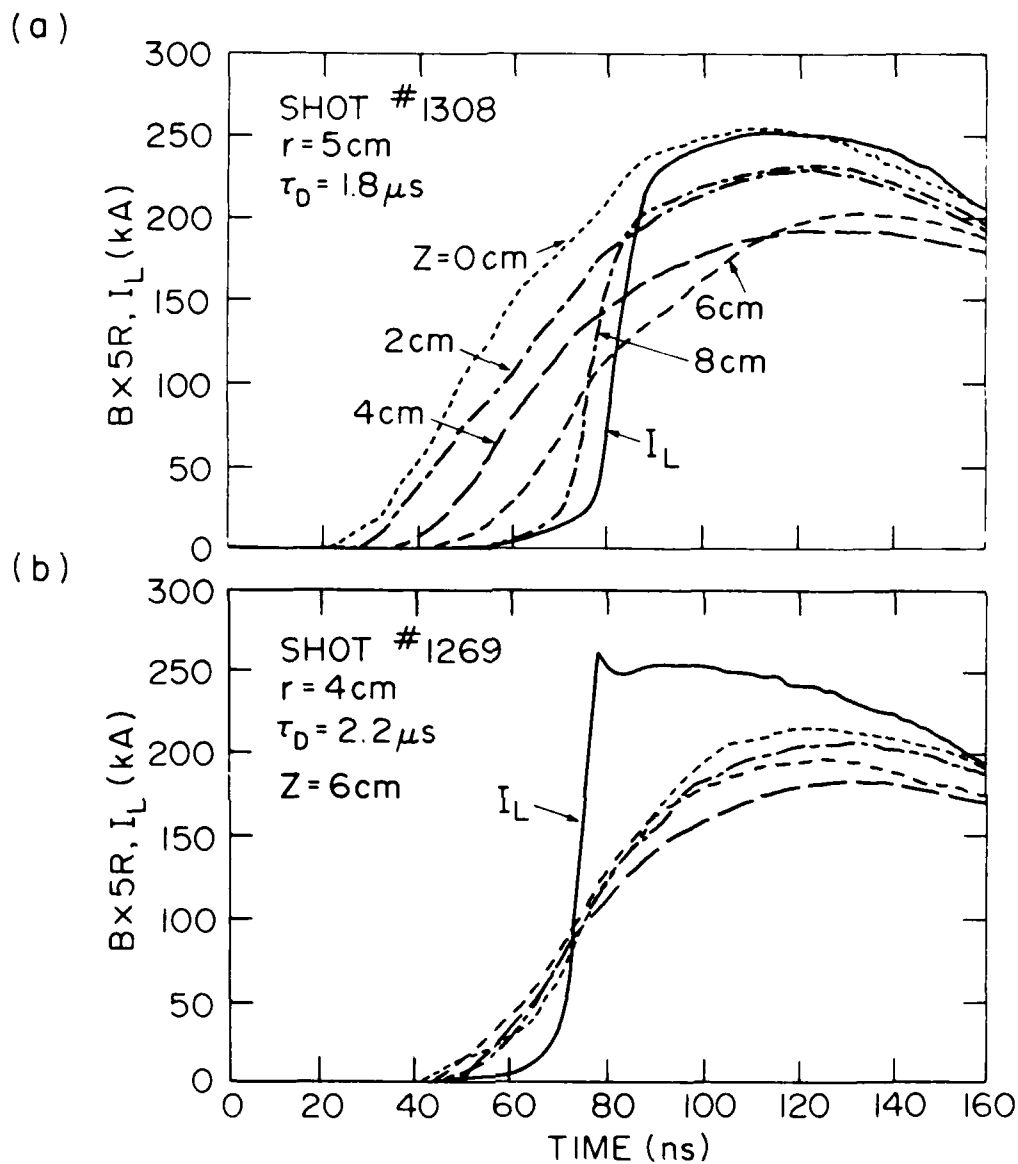


Fig. 23 (a) Magnetic probe signals, in units of current, as a function of time at five axial positions for a fast opening shot. (b) Magnetic probe signals, in units of current, as a function of time at four azimuthal positions for a fast opening shot.

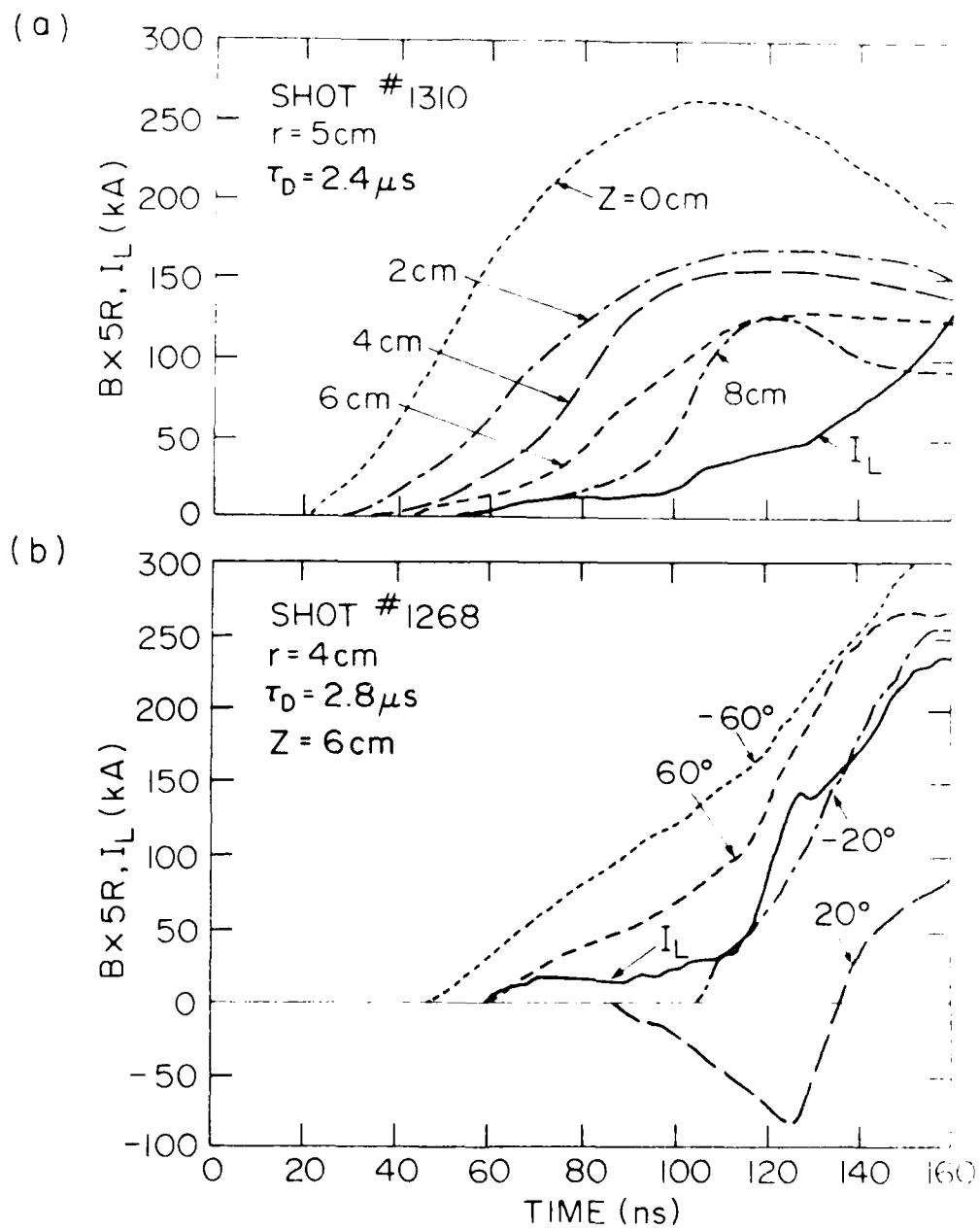


Fig. 24 (a,b) Same as Fig. 21(a,b), except for a slot opening angle.

Fig. 24(a), the current still penetrates along  $z$ . However, as shown in Fig. 24(b), the discharge is clearly not azimuthally symmetric and interpretation of the probe signals as current according to Eq. (12) is incorrect. In this case, the discharge appears to be highly filamentary. Recall that the time resolved visible photography, described in the previous section, indicates the nature of the discharge is qualitatively different depending on value of  $\tau_D$  (see Fig. 14). Also, the results of time resolved photographic, spectroscopic, microwave, and electric probe measurements described in Sec. II suggest that at large  $\tau_D$  the switch plasma characteristics are significantly different (high density, low  $\langle v \rangle$ ) from those at small  $\tau_D$ .

The rate of penetration of magnetic field into the switch plasma was investigated<sup>17</sup> by using an axial array of 10 probes located radially midway between the PEOS anode and cathode in a 30-cm long switch as illustrated in Fig. 20. The long switch allows many probes to be used, improving spacial resolution. The axial position of the leading edge of the magnetic field (i.e., the first non-zero point of the traces in Fig. 23(a)) is plotted as a function of time for shots with different delay times in Fig. 25. Fast switching occurs for  $\tau_D = 1.6$  and  $2.0 \mu\text{s}$ . For these delays the front speed,  $v_F$ , is fairly constant and very high,  $\geq 10^3 \text{ cm}/\mu\text{s}$ . These observations argue against any mass motion associated with this front speed. As the time delay increases,  $v_F$  decreases. This is a result of the larger density associated with larger  $\tau_D$ . At the largest  $\tau_D$ , the front never reaches the load end of the switch and the switch does not open.

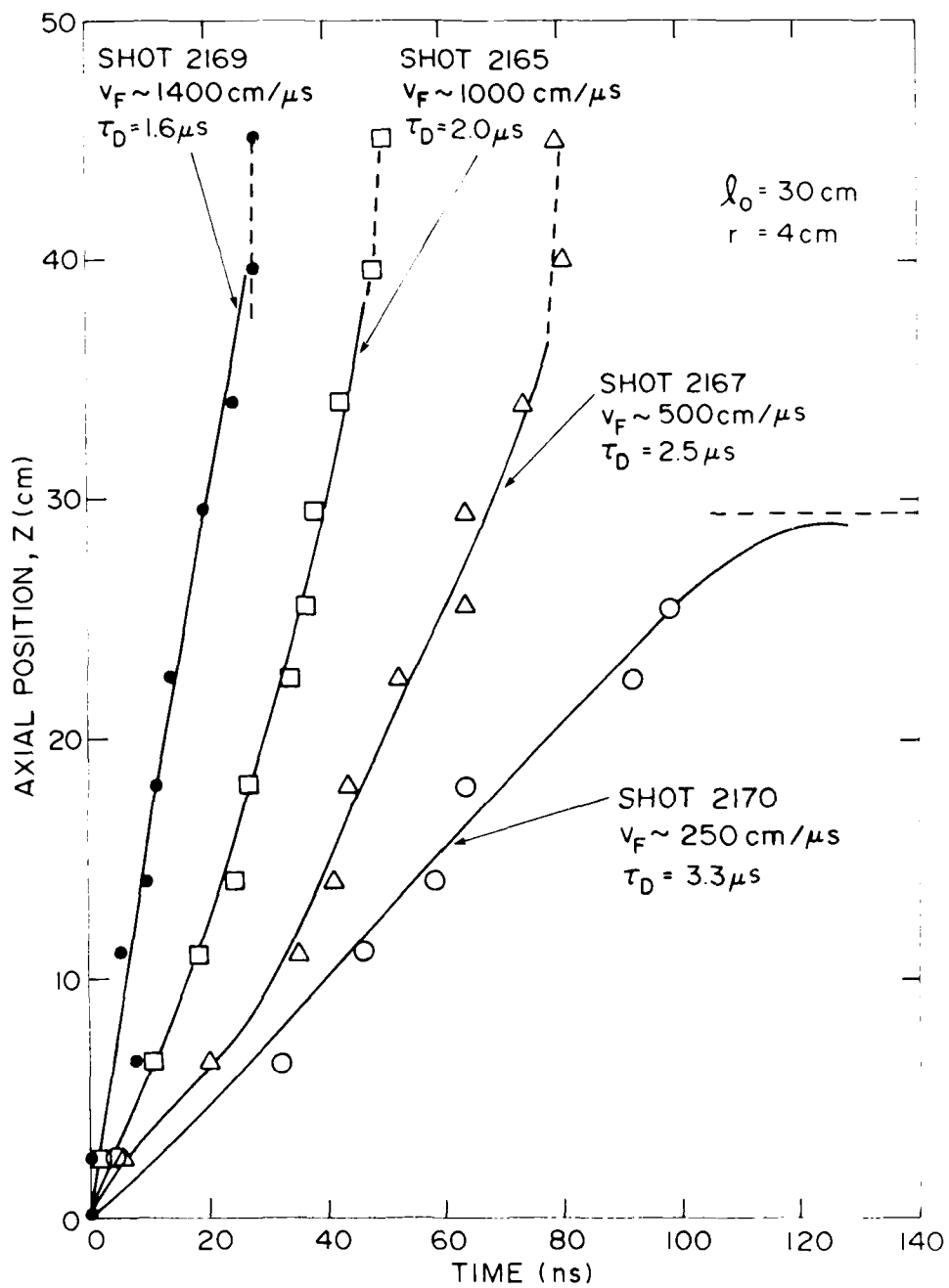


Fig. 25 The axial position of the leading edge of the magnetic field (current channel) front as a function of time for four time delays.

The distribution of current in the switch was characterized by plotting the probe signal as a function of axial position,  $z$ , at given times. These data are displayed for 10- and 30-cm long switches on Gamble I<sup>17</sup> in Figs. 26 and 27. When the initial switch length,  $l_0$ , was increased by a factor of 3, the axial density of plasma sources was decreased by 3, so  $n_1 l_0$  was held constant as described previously. The probes were located radially midway between the switch anode and cathode. Because the current is azimuthally symmetric on fast opening shots (Fig. 23(b)), the probe signals are plotted in units of current, in accordance with Eq. (12). As per the previous discussion and the  $\bar{\nabla} \times \bar{B}$  Maxwell equation, the axial derivative of the current distributions are proportional to the local radial current density. The data for the two cases look remarkably similar. The current is conducted over a fairly broad region, roughly half the original switch length in both cases. Note that the collisionless skin depth,  $c/\omega_{pe}$ , where  $c$  is the speed of light and  $\omega_{pe}$  the electron plasma frequency, is only a few millimeters for the injected plasma conditions. The current density remains nearly constant during the conduction phase, and the switch begins to open when the leading edge of the current channel reaches the load end of the switch plasma. These observations motivate the conduction phase portion of the current controlled PEOS model,<sup>15</sup> in which the switch current density remains approximately constant while the switch current increases during conduction, until the current channel can no longer broaden, i.e., a current limit is reached. They also give insight into the mechanisms responsible for the peak conduction current scaling results discussed previously in Sec. III.B.1.4 (Figs. 17-19 and Fig. 21).



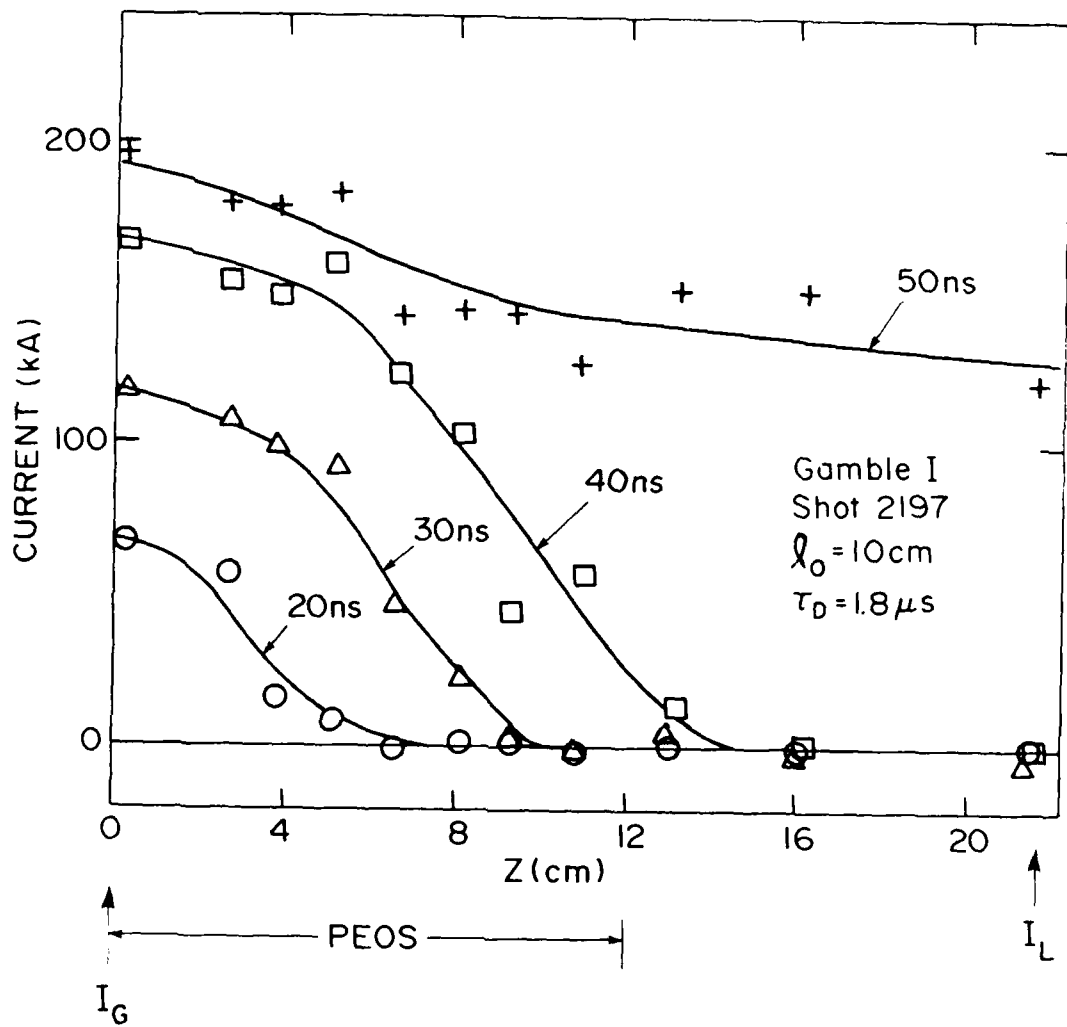


Fig. 26 Current distribution at various times in a 10-cm PEOS on Gamble I.

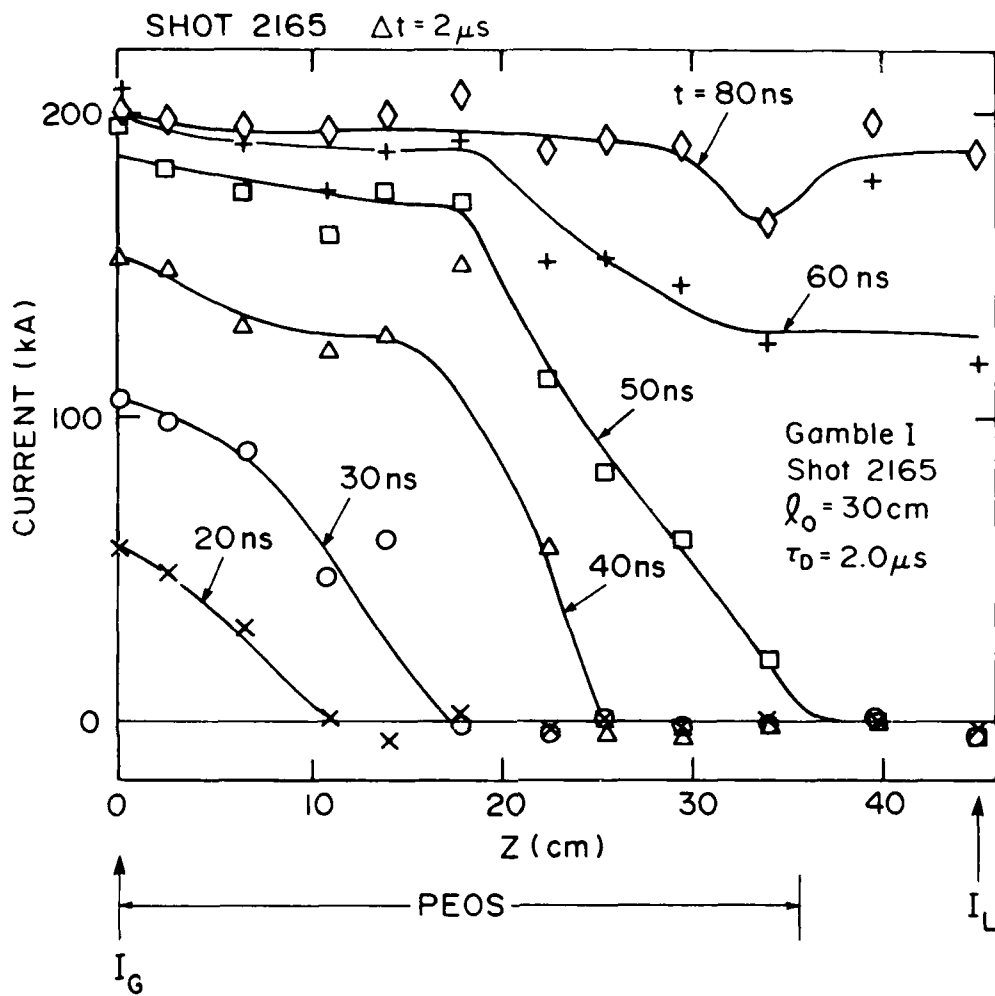


Fig. 27 Current distribution at various times in a 30-cm PEOS on Gamble I.

These results are also observed in the recent, previously described POP experiment,<sup>14</sup> as illustrated in Fig. 28. The data indicate the same broad current channel and constant, radial current density features of the Gamble I data shown in Figs. 26 and 27 (taken at one tenth the conduction time). The time delay in this case was smaller than in Figs. 26 and 27, so the switch opened at a lower value of current.

Direct verification of the radial nature of the current flow during conduction is provided by magnetic probes separated in radius by  $\sim 1$  cm and placed at the same axial location during a shot.<sup>6</sup> Measurements over the entire switch region indicate that at a given  $z$  the magnetic field front arrives at all radii simultaneously as it moves steadily through the axial extent of the switch plasma.

Indirect support of the radial nature of the current flow and azimuthal symmetry during conduction comes from measurements with floating potential probes.<sup>18</sup> The probes were placed at the same axial position, but separated in radius and azimuth. The probe signals indicate the presence of high energy electrons. The signal arrival time was identical at the different radial and azimuthal positions. When the probes were placed at the different axial positions but at the same  $r$ , the signal arrival time tracked the magnetic field front speed,  $v_f$  (see Fig. 25).

An important point in discussing the conduction phase of the current controlled PEOS model is that the measurements made in the switch plasma are used to infer the magnetic field (current) penetration at the cathode.<sup>15</sup> Probes placed as close as 0.5 cm from the cathode show the same

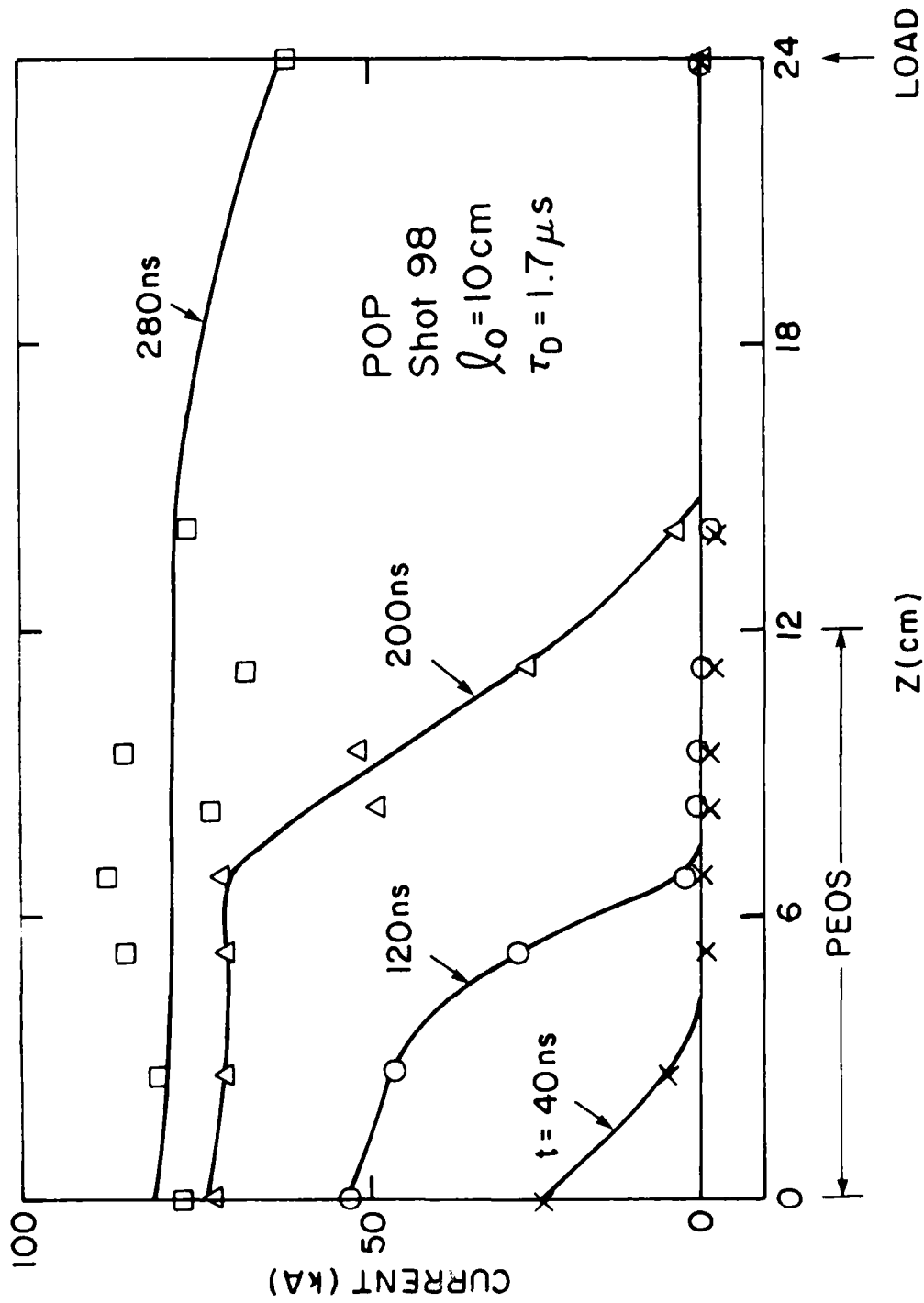


Fig. 28 Current distribution at various times in a 10-cm PEOS on POP.

behavior described above. Supportive data are provided by results from the recent (June 1986) Sandia National Laboratories-Naval Research Laboratory/Maxwell Laboratories, Inc. PPOS experiment on Blackjack 5 in support of PBFA II. Data from a surface magnetic probe placed in the switch cathode 2 cm from the load end of the 12 cm long switch are shown in Fig. 29.<sup>19</sup> The probe detected no current (magnetic field) for  $\approx 65$  ns, then current at the probe location was measured for 15 ns before it began flowing in the load. This result is supported by the streak photography done by the group at Karlsruhe<sup>13</sup> (see Fig. 16), which suggests current penetration along the cathode at rates similar to  $v_F$ .

To summarize Sec. III.C, for time delays where fast switching occurs ( $\tau_D \leq 2.2 \mu\text{s}$ ) the switch current is azimuthally symmetric and flows radially in a broad ( $\gg c/\omega_{pe}$ ), current channel. The switch begins to open when the leading edge of the current channel reaches the load side of the switch plasma. For usual operating conditions both the magnitude and the constancy of the rate of current penetration is incompatible with associated mass motion.

#### IV. SUMMARY:

In this report, we have presented results of measurements that: (1) characterize the initial switch plasma, (2) identify the parameters influencing the peak conduction current, and (3) reveal the nature of the current conduction process.

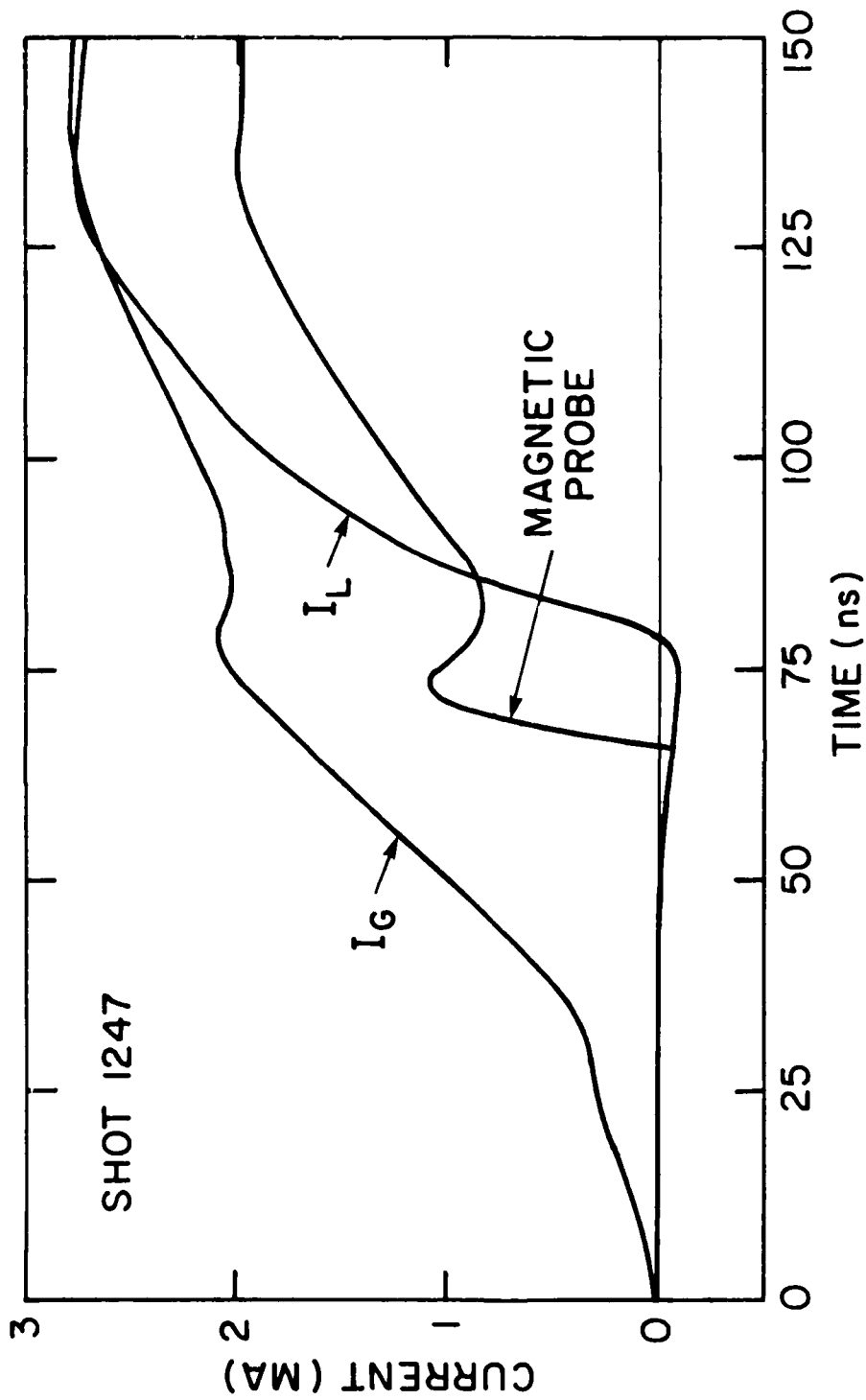


Fig. 29 Current measurements from the Blackjack 5/PBFA II experiment. The magnetic probe is located 2 cm from the load side of the 12-cm long switch. (Data from ref. 19).

Data from time resolved photographic, spectroscopic, microwave, and electric probe measurements present a consistent picture of the initial plasma conditions. These measurements give the approximate values that have been used by NRL in successfully modeling the PEOS. The plasma is primarily doubly ionized carbon,  $\langle Z \rangle = 2$ , with an electron temperature of  $T_e \approx 4-8$  eV. The electron density increases in time and reaches  $\approx 6 \times 10^{13} \text{ cm}^{-3}$  at 7-10 cm from the source 2  $\mu\text{s}$  after the source is fired. At this time the bulk of the inter-electrode plasma is unaffected by the presence of the metal electrode surfaces. The density between the surfaces continues to increase and temperature decrease with time to  $n_e \approx 3 \times 10^{14} \text{ cm}^{-3}$  and  $T_e \approx 5$  eV at  $\approx 6 \mu\text{s}$  after the source is fired. Also, lower charge state carbon (C and  $\text{C}^+$ ) and neutral hydrogen evolve from the electrode surfaces  $\approx 1.5 \mu\text{s}$  after the source is fired and begin to diffuse into the inter-electrode region at  $\approx 1 \text{ cm}/\mu\text{s}$  changing, among other parameters,  $\langle Z \rangle$ . Note that the Faraday cup signals begin to decrease at  $\approx 2 \mu\text{s}$  after the plasma source is fired, in apparent contradiction to the other diagnostics.

The switch conduction current was studied by varying the switch geometry and conduction time. The measured peak current conducted by the PEOS scales approximately in accordance with Eq. (11) using the values for the plasma parameters measured in the bulk of the plasma. For the case investigated here, the peak conduction current was, to first order, independent of conduction time.

Spacially and temporally resolved magnetic probe measurements reveal that over a wide range of parameters the switch current is azimuthally

symmetric and flows in a broad ( $\gg c/\omega_{pe}$ ), predominately radial current channel for delay times when fast switching is observed. The radial current channel front moves steadily through the switch until its leading edge reaches the load side of the switch plasma, whereupon the switch begins opening into a short circuit load. For usual operating conditions the magnitude and constancy of the rate of current channel penetration are incompatible with associated mass motion. With longer delay times, when the opening is degraded, the discharge is not symmetric. This may be related to the change in plasma parameters. For delay times where no switching occurs, the current channel never reaches the load side of the switch plasma.

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