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WIND TUNNEL MEASUREMENTS OF THE  
MAGNUS INDUCED SURFACE PRESSURES ON  
A SPINNING ARTILLERY PROJECTILE  
MODEL IN THE TRANSONIC SPEED REGIME

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RESEARCH DIRECTORATE

September 1986

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## PREFACE

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This report has been approved for release to the public.

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The fabrication of the wind tunnel model and sting components was accomplished by the Experimental Fabrication Branch, Research, Development and Engineering Support Directorate, Chemical Research, Development and Engineering Center (formerly the Chemical Systems Laboratory). In particular, the exceptional skills of Coy Barker, David Blake, Kenneth Younger, Scotty Johnson, and Llewellyn Thompson provided the high quality test items required.

A key element in the success of this study was the o-ring utilized in the sliding seal. The cooperative efforts of Ike Royster and Dutch Haddock of the Parker Hannifin Corporation in providing advice and samples facilitated the evaluation and selection of the required o-ring configuration and material.

Access to the NASA Ames, 14-foot transonic wind tunnel was gained through the test justification support provided by Harold R. Vaughn and Albert E. Hodapp of the Aeroballistic Division, Sandia National Laboratories and Carman Spinelli, XM785 Project Manager at the U.S. Army Armament Research and Development Center.

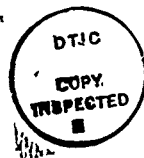
Important guidance for the test procedure and interpretation of the resulting data was obtained from Dr. William Oberkampf of the Aeroballistic Division, Sandia National Laboratories.

Individuals from the Aerodynamics Research and Concepts Assistance Branch also contributed to this effort. Owen C. Smith, Jr., in addition to his previous efforts in developing the sliding seal design, participated in several of the functional check-outs of the model and instrumentation systems prior to the wind tunnel test. Daniel J. Weber developed the computer program necessary to analyze the relatively large volume of complex data reduction associated with force and moment coefficient pressure integration.

Finally, the authors express their appreciation to Abraham Flatau for his encouragement and support, which allowed the sliding seal experimental technique to be sequentially evolved from the initial concept in 1975 to the current application.

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## WIND TUNNEL MEASUREMENTS OF THE MAGNUS INDUCED SURFACE PRESSURES ON A SPINNING ARTILLERY PROJECTILE MODEL IN THE TRANSONIC SPEED REGIME

### 1. INTRODUCTION

A spinning projectile in flight produces aerodynamic surface pressures that have led to the so-called Magnus effect. This external aerodynamic phenomenon due to the combination of projectile spin and angle of attack produces forces and associated moments that have resulted in flight instabilities for several military projectiles.<sup>1-3</sup> Although the Magnus force is only a 10th to a 100th of the normal force, it can have a large detrimental influence on range and accuracy. Figure 1 contains flight test data illustrating the yaw growth experienced by an artillery projectile experiencing a Magnus instability. A concerted effort has been underway to experimentally investigate the fundamental Magnus phenomena and to develop theoretical models and analytical techniques to describe the effect.<sup>4,5</sup>

This report presents wind-tunnel test measurements of the aerodynamic surface pressures on a full scale spinning model of the M549/XM785 artillery projectile in the transonic speed regime. The model, a secant ogive, cylinder, boattail configuration with an 8-inch diameter and a 5.5 caliber length, was evaluated both with and without a rotating band. The model was tested in the NASA-Ames 14 Foot Transonic Wind Tunnel. Circumferential pressure distributions were obtained at several longitudinal locations on the model, with emphasis on the cylindrical and boattail sections. The model was tested at angles of attack of 0, 4, and 10 degrees and spin rates of 0 and 4,900 rpm. All testing was done at a Mach number of 0.94, which corresponds to the critical Mach number for this projectile configuration.

The model configuration, scale, and test conditions were selected to complement a series of wind-tunnel tests conducted by the Ballistics Research Laboratory (BRL) that involved an extensive wind-tunnel investigation of a similar projectile configuration and scale at the NASA-Langley 8-Foot Transonic Wind Tunnel.<sup>6,7</sup> During these tests, the aerodynamic forces and moments as well as velocity profiles of the boundary layer were obtained on both a spinning and non-spinning model. The aerodynamic surface pressures were also measured, but only for the non-spinning condition.

The tests were conducted to extend the data base for this projectile configuration and represent the first time that the aerodynamic surface pressures have been experimentally determined on any spinning projectile. Several other test objectives were also achieved as shown in Figure 2. The results allow a detailed insight into the Magnus phenomena as well as providing experimental data to support the evolution and validation of theoretical and numerical analyses. In addition, the test demonstrated the use of a new experimental method to obtain surface pressure data.

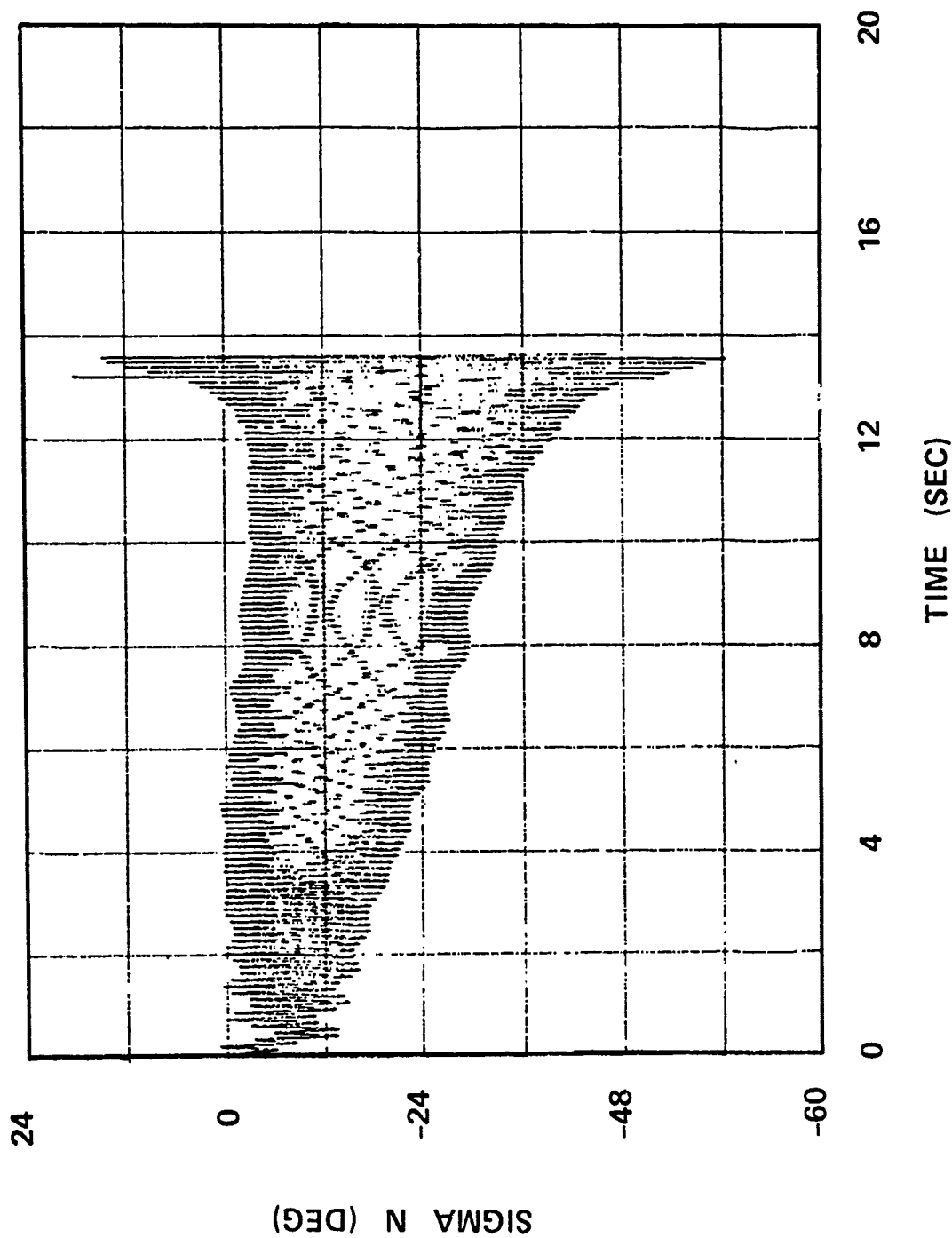


Figure 1. Time History of Projectile Yawing Motion Resulting from Magnus Instability

- DETERMINE MAGNUS CHARACTERISTICS OF PROJECTILE AT CRITICAL (TRANSONIC) MACH NUMBER
  - EFFECT OF SPIN
  - EFFECT OF ANGLE OF ATTACK
    - ATTACHED FLOW ( $\alpha = 4^\circ$ )
    - SEPARATED FLOW ( $\alpha = 10^\circ$ )
  - EFFECT OF ROTATING BAND
- COMPLETE PREVIOUS TEST DATA
  - FORCE AND MOMENT
  - NON-SPINNING SURFACE PRESSURE
  - BOUNDARY LAYER
- INTERPRET GENERAL MAGNUS PHENOMENA
- DEMONSTRATE NEW TESTING TECHNIQUE
- PROVIDE DATA TO SUPPORT AND VERIFY THEORETICAL COMPUTATIONS

Figure 2. Objectives of the Wind Tunnel Tests

Mach number 0.94 represents the critical Mach number for this projectile (i.e., the condition where the projectile possesses the maximum destabilizing aerodynamic effects). Figure 3 depicts the flow field that exists over the projectile at this transonic condition. The shadowgraph shows that two separate shock waves occur: one just downstream of the ogive/cylinder junction and the other just downstream of the cylinder/boattail junction. This combination of subsonic and supersonic flow produce a complex surface pressure distribution as shown.

In addition to the basic angle of attack of 0 degree, the test included angles of attack of 4 and 10 degrees because they produce an attached flow and separated flow, respectively, over the boattail region of the model. The aerodynamic characteristics undergo a significant change between these two angles of attack, and the resulting pressure data would be of great interest. The spin rate of 4,900 rpm represents a tip speed ratio of .17 corresponding to a Mach 0.94 muzzle velocity condition. Finally, the influence of the rotating band on the Magnus surface pressures in the transonic speed region is of particular concern. This situation is currently being addressed by using computational fluid dynamic methods, and little experimental data exists to support or verify these theoretical analyses.<sup>8,9</sup>

## 2. BACKGROUND

During the past several years, the Aerodynamics Research and Concepts Assistance Branch has systematically evolved a new and unique method to experimentally measure the aerodynamic pressures acting over the external surface of the spinning wind tunnel model. The method is based on an unconventional model design and instrumentation arrangement. The model is composed of two parts. A non-spinning inner portion of the wind tunnel model, containing the instrumentation, detects the surface pressure through a series of vent holes in the spinning outer portion of the model, the pressure being retained for measurement by means of a sliding seal arrangement.<sup>10</sup> This method avoids the problems and limitations of conventional test techniques<sup>11,12</sup> and allows surface pressures to be measured on spinning bodies at any attitude and flow regime. In addition, the body can include indentations or protuberances.

The validity and performance capability of the testing method has been demonstrated in stages, beginning with a simple spinning right-circular cylinder in cross flow that verified the basic concept.<sup>13</sup> A second major series of tests involved the measurement of the surface pressures on a spinning Magnus autorotor,<sup>14</sup> which extended the testing method to bodies having irregular surface features and an unsteady, periodic flow field. Other studies investigated improved instrumentation elements, in particular, the critical sliding seal units. This latter work evolved a magnetic fluid seal<sup>15</sup> (to reduce friction effects), a miniature sized seal, and a remotely selectable pneumatic seal, all intended to increase the versatility and accuracy of the testing method. These efforts were funded by the BRL, CRDEC, and Sandia National Laboratories, respectively. Portions of the material presented in this report have been disseminated through presentations at conferences<sup>16</sup> and articles in technical journals.<sup>17</sup> A concise summary of the evolution of the experimental technique and the results obtained has also been published.<sup>18</sup>

# TRANSONIC FLOW FIELD

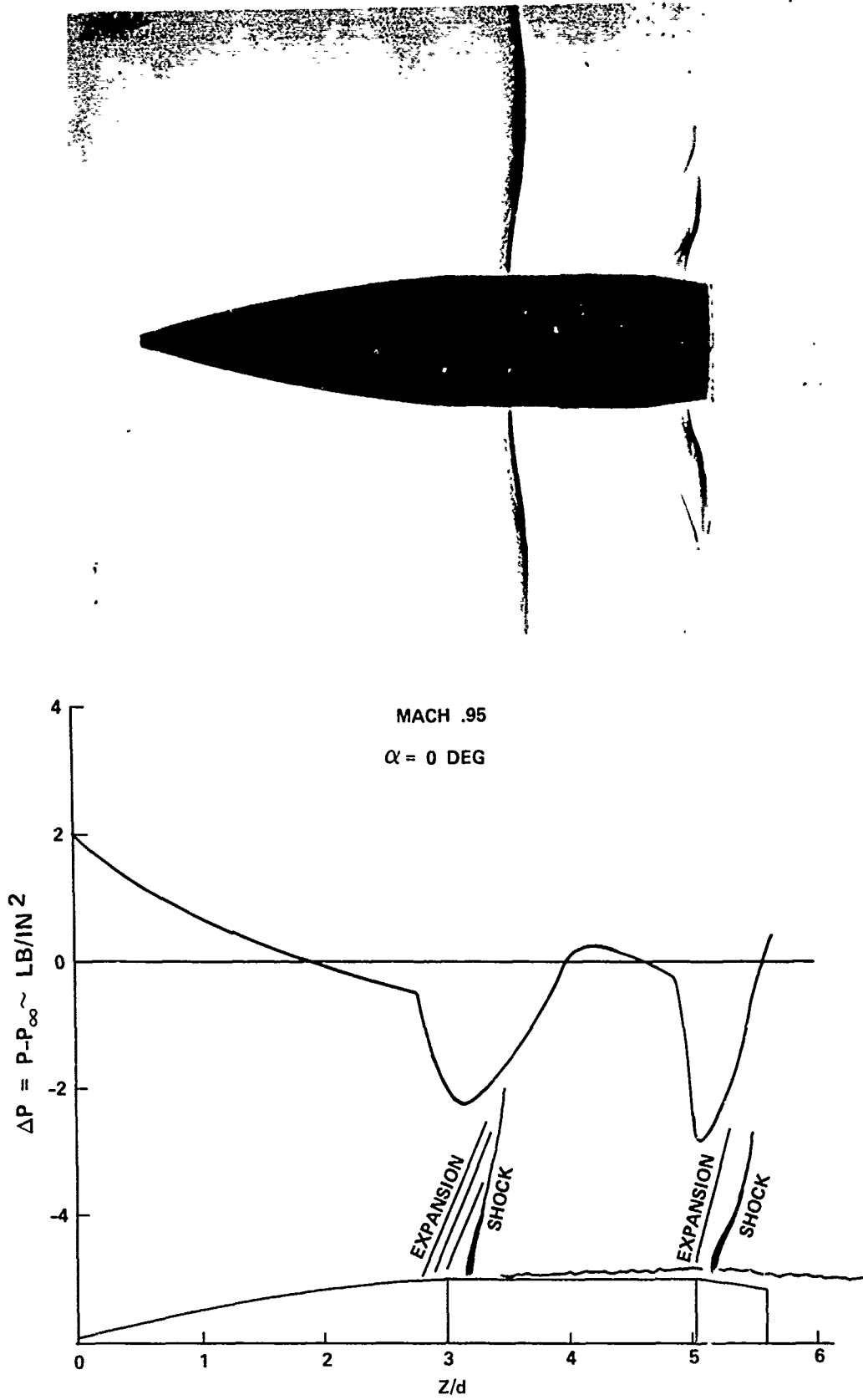


Figure 3. Transonic Flow Field and Surface Pressure Distribution

### 3. MODEL DESCRIPTION

The external model configuration and model sting arrangement are shown in Figures 4 and 5, respectively. The model was composed of a 3 caliber secant ogive, a 2 caliber cylindrical, and a 7-degree, 0.5-caliber boattail. The projectile represents a 130-percent scale model of the M549/XM785 155-mm artillery projectile; however, it closely resembles the baseline projectile shape being analyzed by the BRL. The model also included the flat nose and wrench grooves of a standard fuze. The model's external shaping and scale were also identical to the model used in the Langley tests. The aft end of the model sting was attached directly to the wind tunnel roll head assembly which, in turn, was attached to the tunnel angle-of-attack sector sting.

A schematic drawing of the model's internal arrangement is shown in Figure 6. Detailed engineering drawings of the model components are included for your convenience in the last appendix in this report (Appendix D). The model consisted of an aluminum core containing the spin motor, pressure taps, and scanivalve mechanism. The model core was stationary (i.e., non-spinning) with respect to the model sting. The steel shell, representing the outer contour of the projectile was attached to the core by means of front and rear bearings and connected to the spin motor through an axial drive shaft at the nose. A set of four vent holes at 90-degree circumferential intervals were located through the shell at each of 20 longitudinal stations along the model. These vent holes which were 0.0625 inch in diameter coincided with the 20 pressure taps contained in the outer surface of the core section. Only two taps are shown in Figure 6 for clarity.

Two scanivalves, located in the core, were used as switching devices to allow the remote selection and engagement of the pressure tap seal units. The scanivalves were simultaneously driven by a common index/drive unit, also located in the model core. One scanivalve directed pneumatic air to a particular pressure tap seal unit to force it outward against the inner surface of the spinning shell. Concurrently, the other scanivalve directed the surface pressure being measured at that tap out through the sting to the pressure transducer and associated recording equipment located outside the tunnel. Figures 7 and 8 contain photographs of the model core with the shell removed to illustrate the scanivalve installation and the pressure tap locations, respectively.

The gap between the face of the pressure tap seal unit and the inner surface of the shell was sealed by means of a circular o-ring located on the outer face of the seal unit. The cavity created by engaging the seal unit with the shell was open to the pressure acting on the outside surface of the shell when the vent hole was aligned with the seal unit, as illustrated in Figure 9. Once the vent hole in the spinning shell rotated past this aligned position, the o-ring caused the cavity to retain the pressure. After a sufficient number of shell revolutions, the cavity eventually assumed a constant pressure equal to the pressure acting on the surface of the spinning shell at that particular circumferential location. Details of the pressure tap seal units are contained in Figure 10, and a photograph of them is shown in Figure 11. Figure 12 depicts the seal units installed in the boattail section of the core. The outer surface of each seal unit was contoured to match the radius of the inner shell surface at that location. The Parker-Hannifan No. 2-204-N827-80 o-rings, 0.5 inch diameter, were composed of lubricant-impregnated carboxylated nitrile rubber and were retained in the circular groove of the seal block by high viscosity silicone

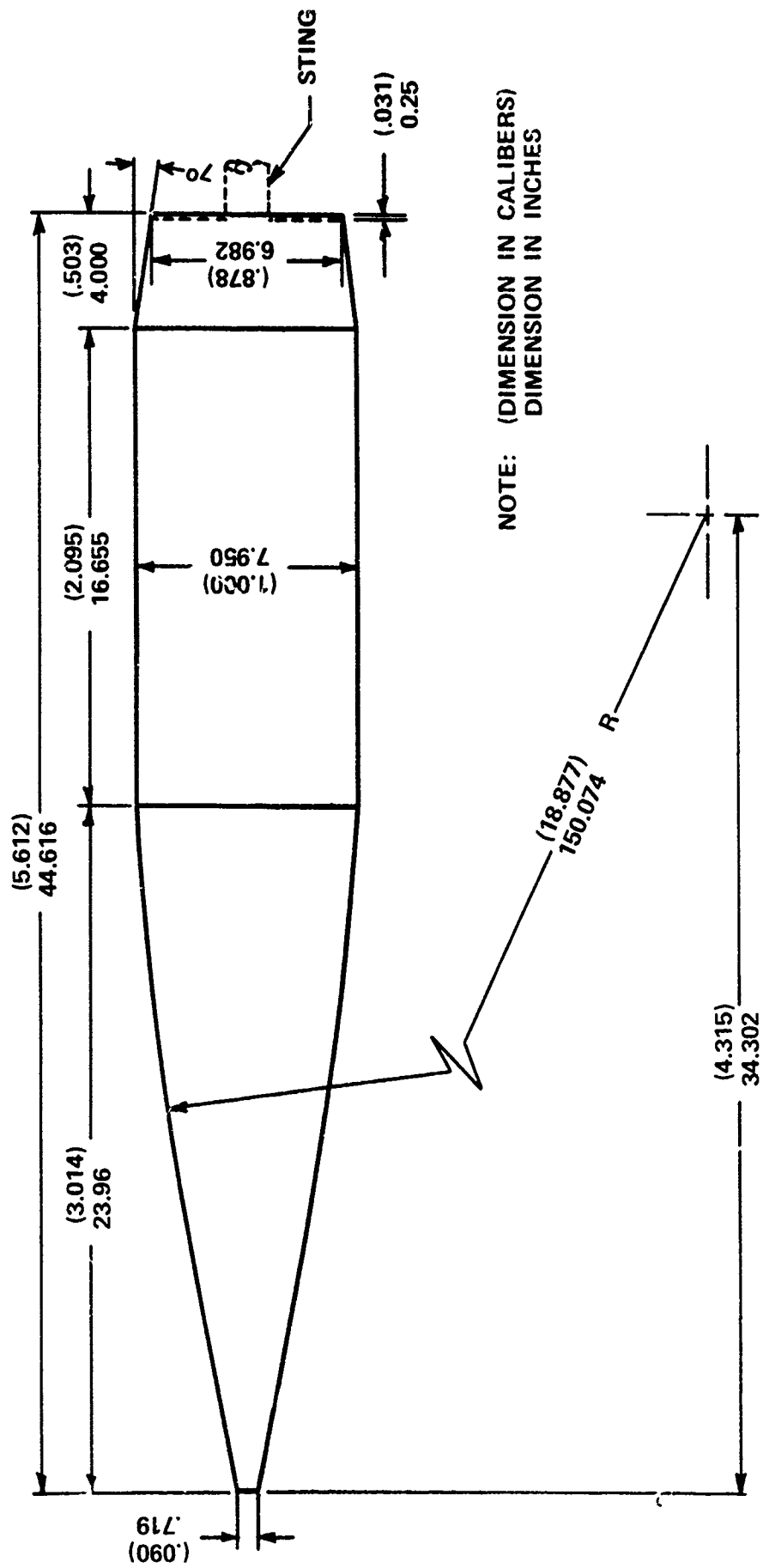


Figure 4. External Configuration of the Wind Tunnel Model



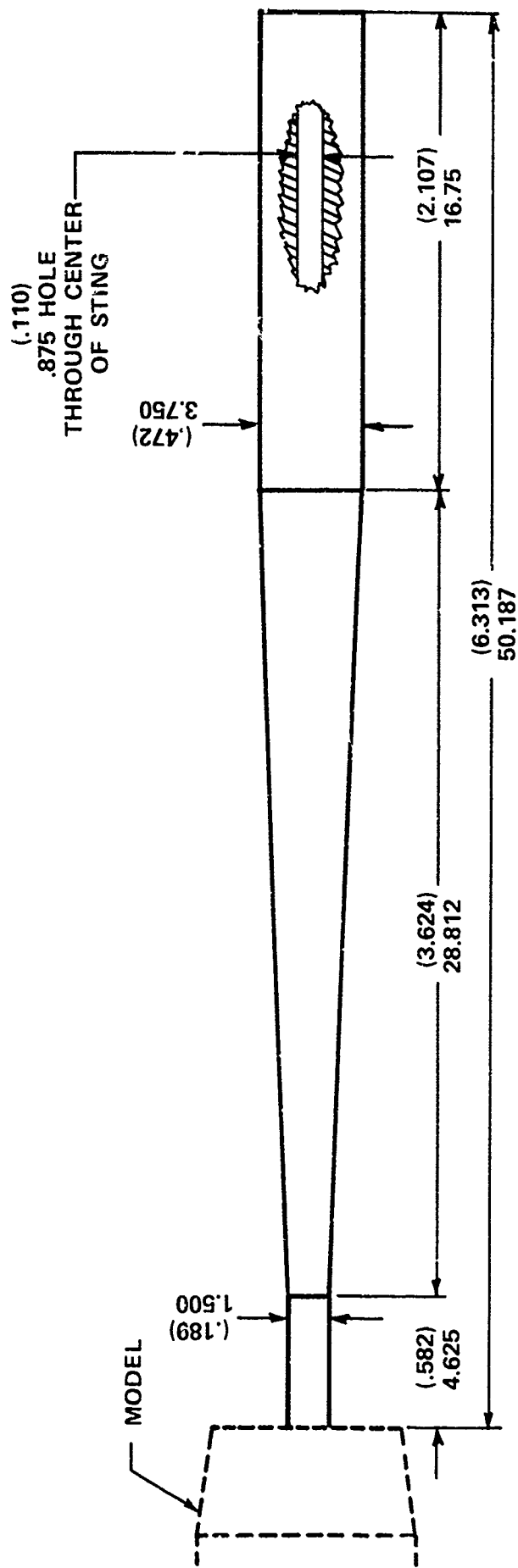


Figure 5. Sting Arrangement for the Wind Tunnel Model

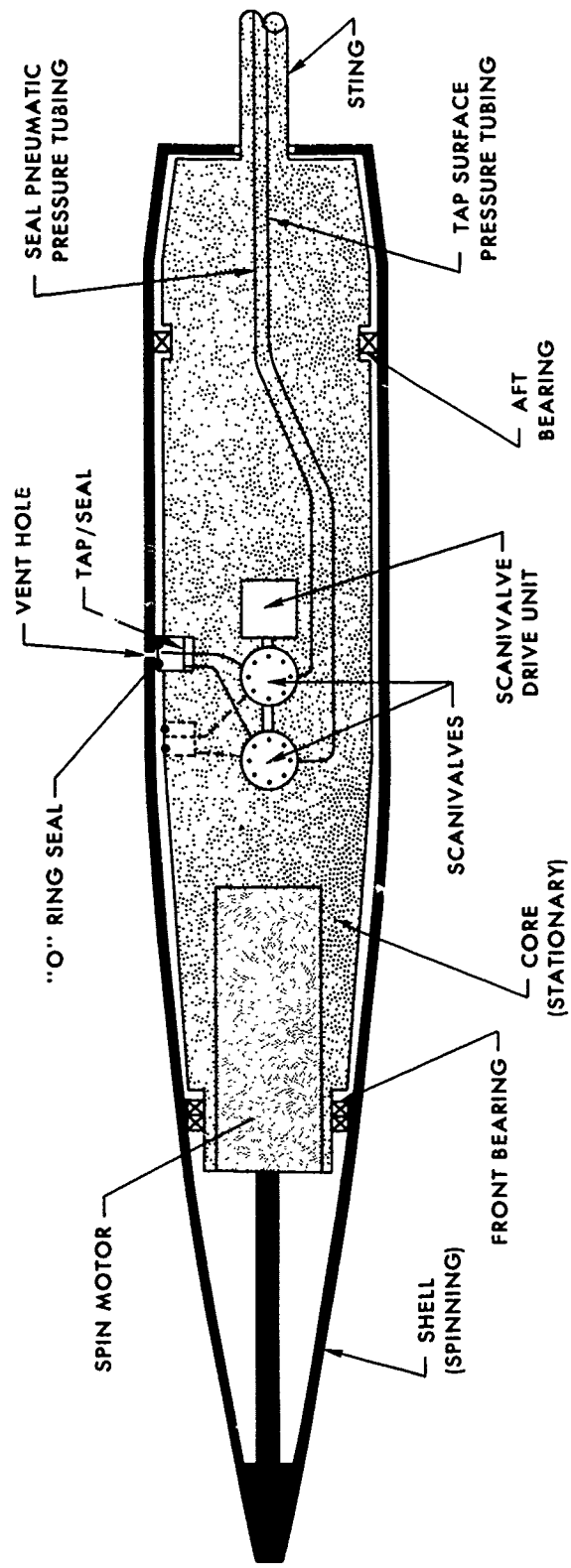


Figure 6. Internal Configuration of the Wind Tunnel Model



Figure 7. Photograph of the Model Core Showing Scanivalve Installation

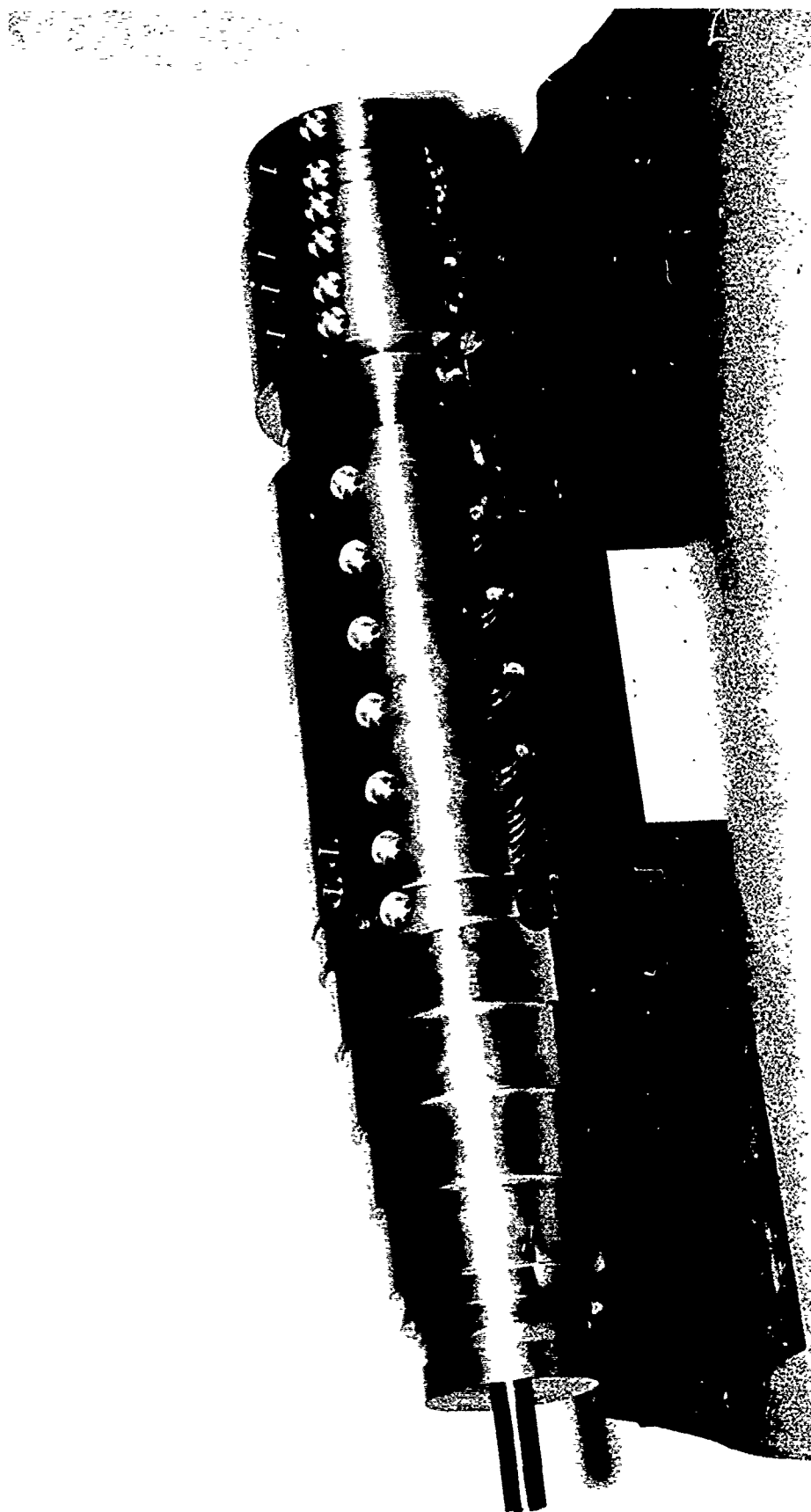


Figure 8. Photograph of the Model Core Showing Pressure Tap Locations

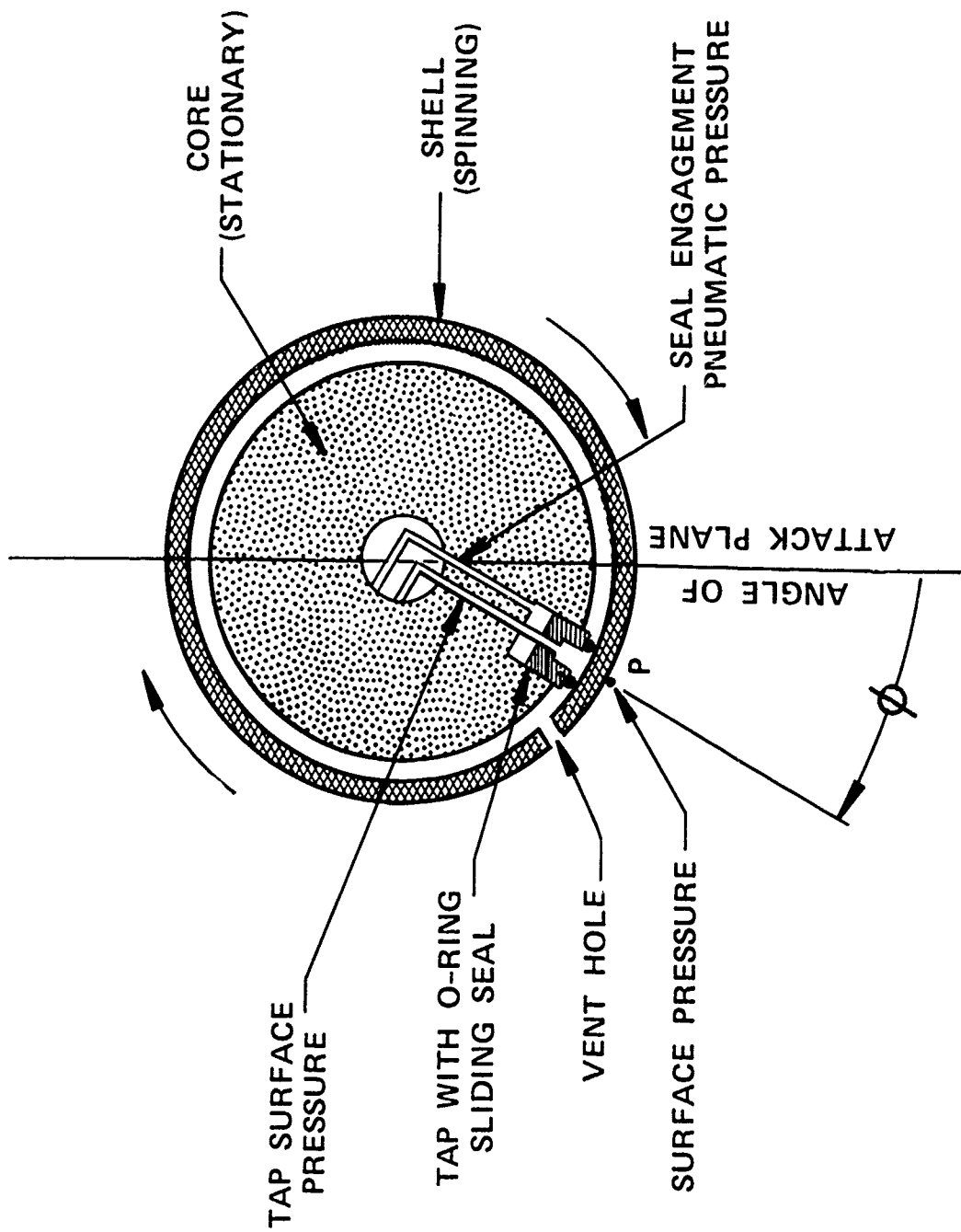
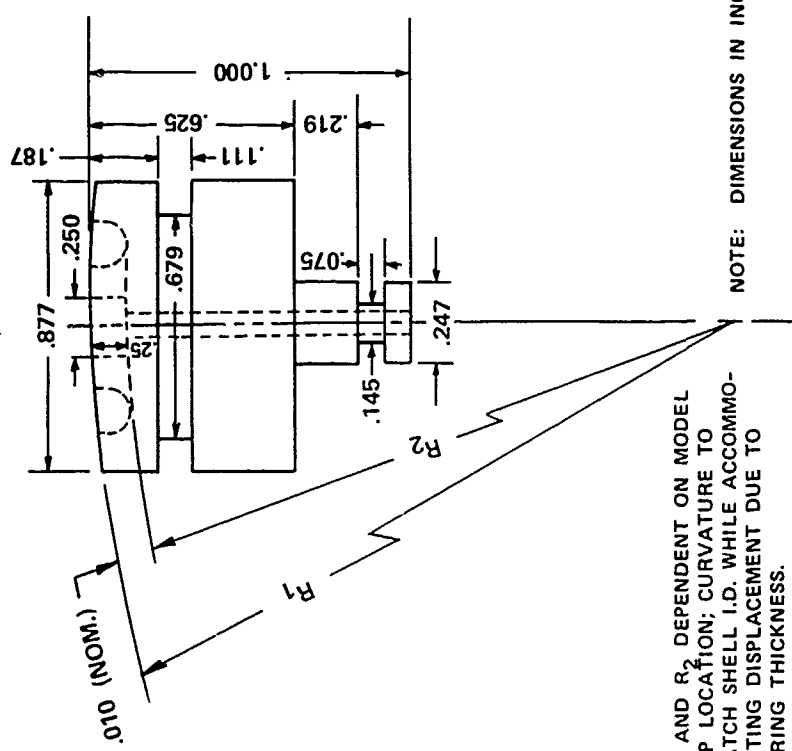
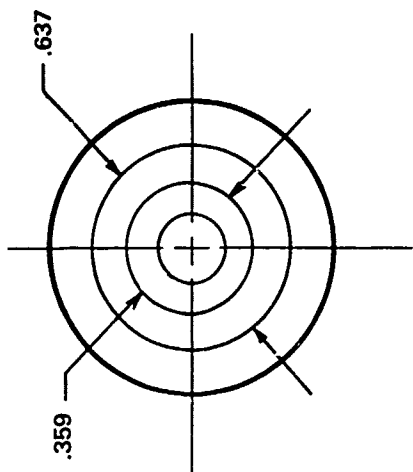


Figure 9. Surface Pressure Measurement Technique



NOTE: DIMENSIONS IN INCHES

$R_1$  AND  $R_2$  DEPENDENT ON MODEL TAP LOCATION; CURVATURE TO MATCH SHELL I.D. WHILE ACCOMMODATING DISPLACEMENT DUE TO O RING THICKNESS.

Figure 10. Details of the Pressure Tap Seal Unit

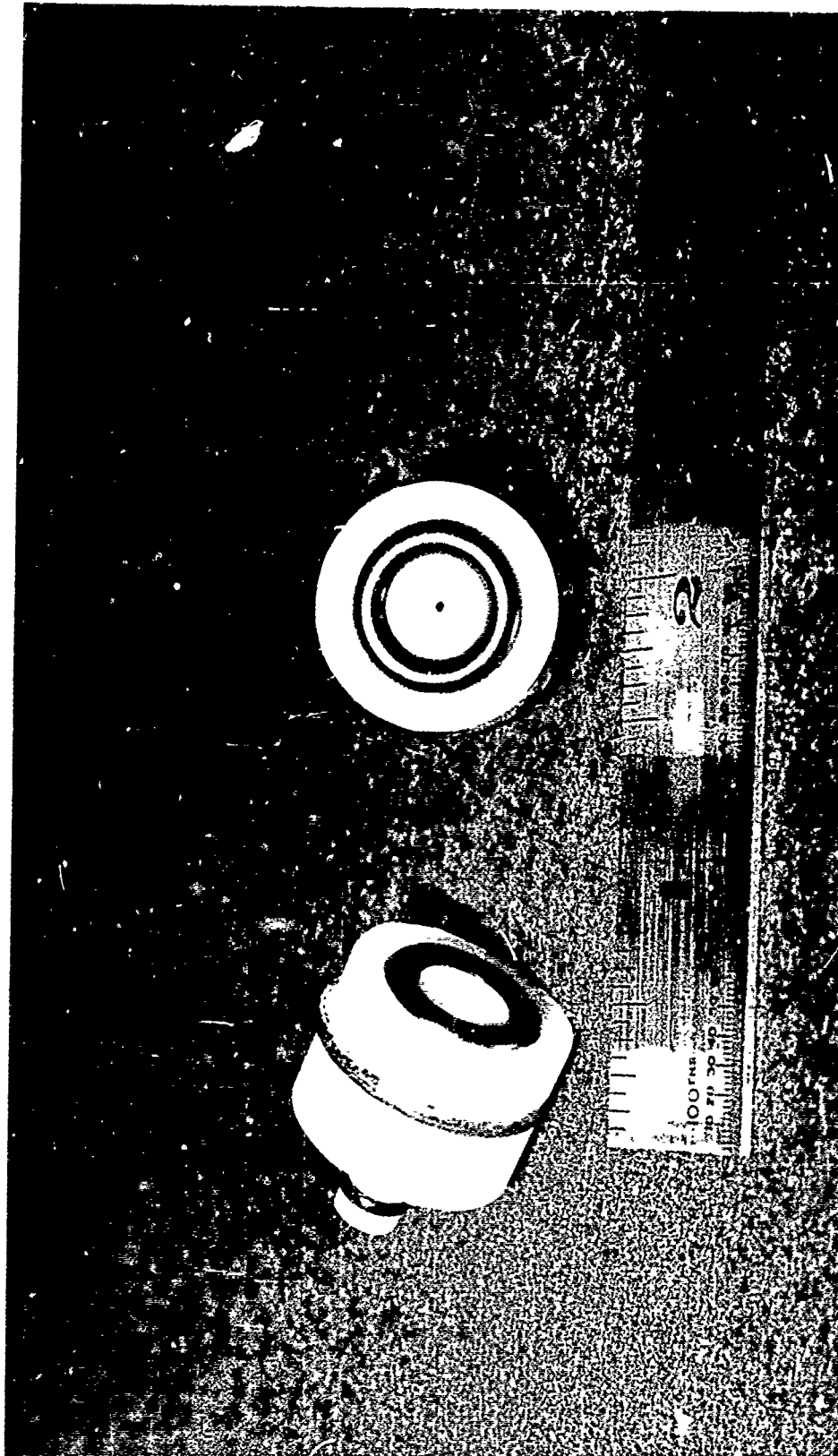


Figure 11. Photograph of Pressure Tap Seal Units

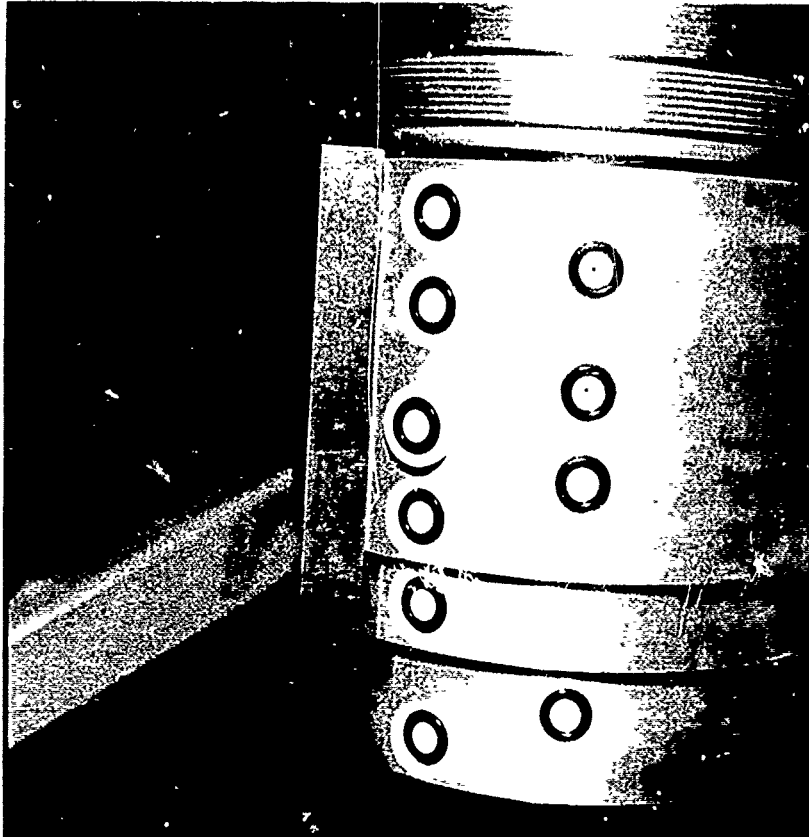


Figure 12. Photograph of Model Boattail  
Section of Core Showing Installed  
Pressure Tap Seal Units



oil. Pressure measurements at various points on the surface of the spinning body were obtained by positioning the core and the attached tap to different roll attitudes relative to the angle-of-attack plane. This was accomplished by means of a remotely settable roll head located between the model sting and the tunnel angle-of-attack sector sting. The roll head allowed the model core to be sequentially set to various roll orientations.

The steel shell was made up of two basic parts. The forward part included the ogive and most of the cylindrical section. The aft part included the boattail and the portion of the cylindrical section in the area of the rotating band. The model could be tested with or without the rotating band by simply changing the aft part of the shell. Figure 13 shows the aft shell section that included the rotating band. The rotating band, which represented a post-fired condition, was machined directly into the aft shell section. Vent holes were also located on the rotating band lands and grooves, allowing measurements at these positions. The model included an enclosed base similar to the actual projectile.

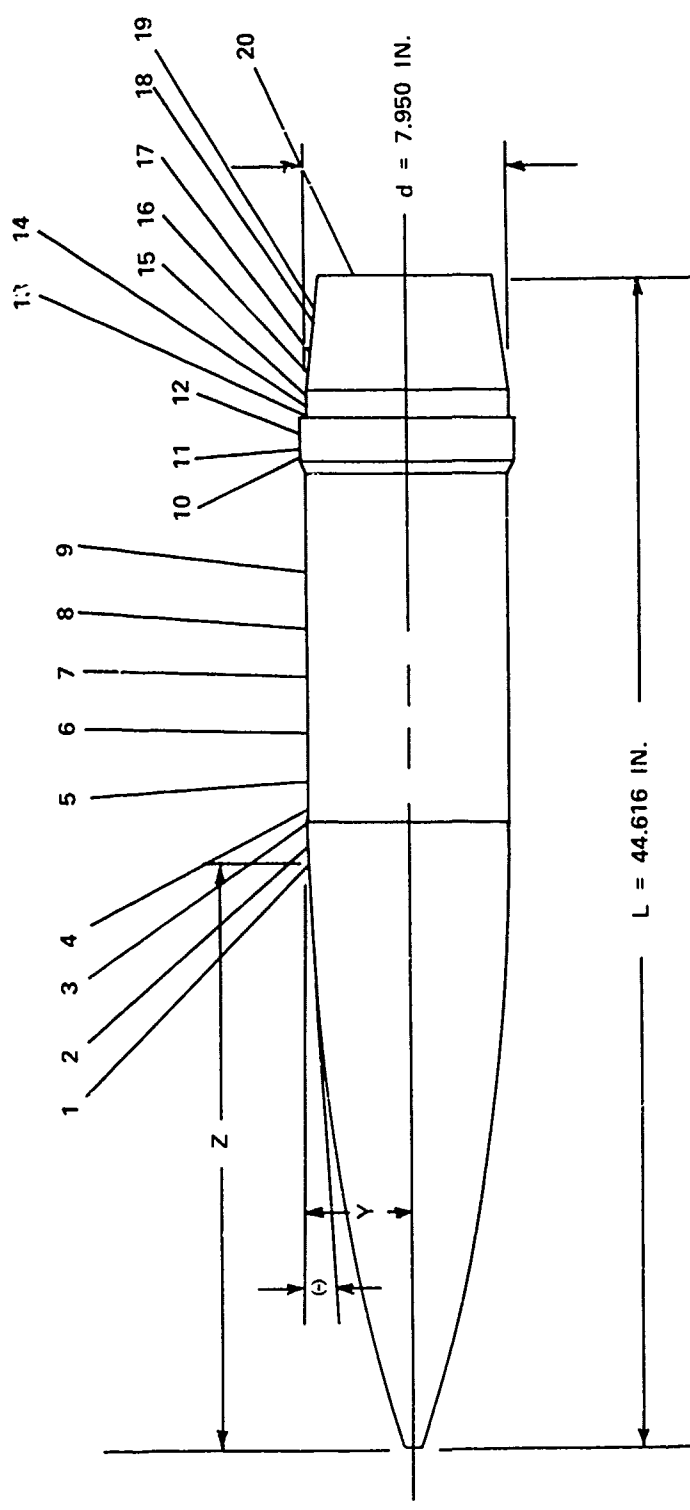
The longitudinal locations of the pressure taps for the 20 vent holes are defined in Figure 14. The tap locations were selected to match those used in the non-spinning surface pressure model used in the Langley tests. Some taps were offset 30 degrees to the main line of taps to allow closer longitudinal spacing than could be achieved with the seal units in a single line. The taps were concentrated over the cylindrical and boattail portion of the model because the Magnus effect primarily occurs in this area. Also, the flow over the ogive and the resultant small Magnus effect can be analyzed quite accurately by current theoretical means. One tap was located to measure the surface pressure on the base of the model at a radial location .09 calibers in from the edge of the boattail. Detailed drawings of the model and sting components are included in Appendix D.

All operation and instrumentation wiring and tubing were routed from the model to a special console located outside the tunnel test section through a hole .875 inch in diameter located down the length of the model sting. This hole contained the operating wires, thermocouple wires, and the cooling water tubing for the motor, the scanivalve operating wires, the engagement pneumatic pressure tubing and signal pressure tubing for the taps, and the thermocouple wires for the model bearings. The instrumentation and operating interfaces are detailed in Figure 15. The water-cooled, variable frequency/variable voltage electric motor was rated at 5 hp for the nominal 5,000 rpm model spin rate. This condition was easily achieved with 150 V/150 cps obtained from the tunnel generator system. The motor operated at about 10 amps and the motor temperature never exceeded 100 °F even after sustained operation of up to 8 hours. Model spin was smooth and, once established, never varied more than 50 rpm from the nominal 4,900 rpm. Engagement of a pressure tap seal unit reduced the spin rate about 100 rpm. Model bearing temperatures never exceeded 100 °F even under sustained spinning for several hours with the tunnel operating at a stagnation temperature of 130 °F. The model had no perceivable pitch or yaw motion during the test and possessed no vibration under all conditions of spin and angles of attack. During this test, the model was spun at 5,000 rpm for a total of 55 hours. Even after these 16,500,000 revolutions, the model bearings appeared to be as good as new. A photograph of the model installed in the wind tunnel test section is shown in Figure 16. The model core weighed 100 pounds, the model shell, 65 pounds, and the model sting, 85 pounds.



Figure 13. Photograph of Boattail Section of Model Shell

TAP NO.	TAP LOCATION				Y (Y/d)	θ DEG	TAP LOCATION NOTES	TAP CIRCUMFERENTIAL LOCATION WRT MAIN TAPS (DEG)
	Z (IN.)	Z/L	Z/d	Y (IN.)				
1	22.449	.503	2.824	3.875	.487	4.5	OGIVE	0
2	23.450	.526	2.950	3.969	.499	4.5		30
3	23.961	.537	3.014	3.975	.5	0	OGIVE/CYLINDER JUNCTION	0
4	24.461	.548	3.077	3.975	.5	0	CYLINDER	30
5	25.461	.571	3.203	3.975	.5	0		0
6	27.461	.615	3.454	3.975	.5	0		
7	29.461	.660	3.706	3.975	.5	0	ROTATING BAND	
8	31.461	.705	3.957	3.975	.5	0		
9	33.461	.750	4.209	3.975	.5	0		
10	37.821	.848	4.757	3.975	.5	0		
11	38.321	.859	4.820	3.975	.5	0		
12	38.821	.870	4.883	3.975	.5	0		
13	39.616	.888	4.983	3.975	.5	0	CYLINDER	30
14	40.116	.899	5.046	3.975	.5	0	CYLINDER/BOATTAIL JUNCTION	0
15	40.616	.910	5.109	3.975	.5	0	BOATTAIL	30
16	41.151	.922	5.176	3.938	.495	7.0		0
17	42.159	.945	5.303	3.813	.425	7.0		0
18	43.236	.969	5.438	3.688	.480	7.0		30
19	43.725	.980	5.500	3.625	.456	7.0		0
20	44.616	.994	5.578	2.750	.346	90°	BASE	90



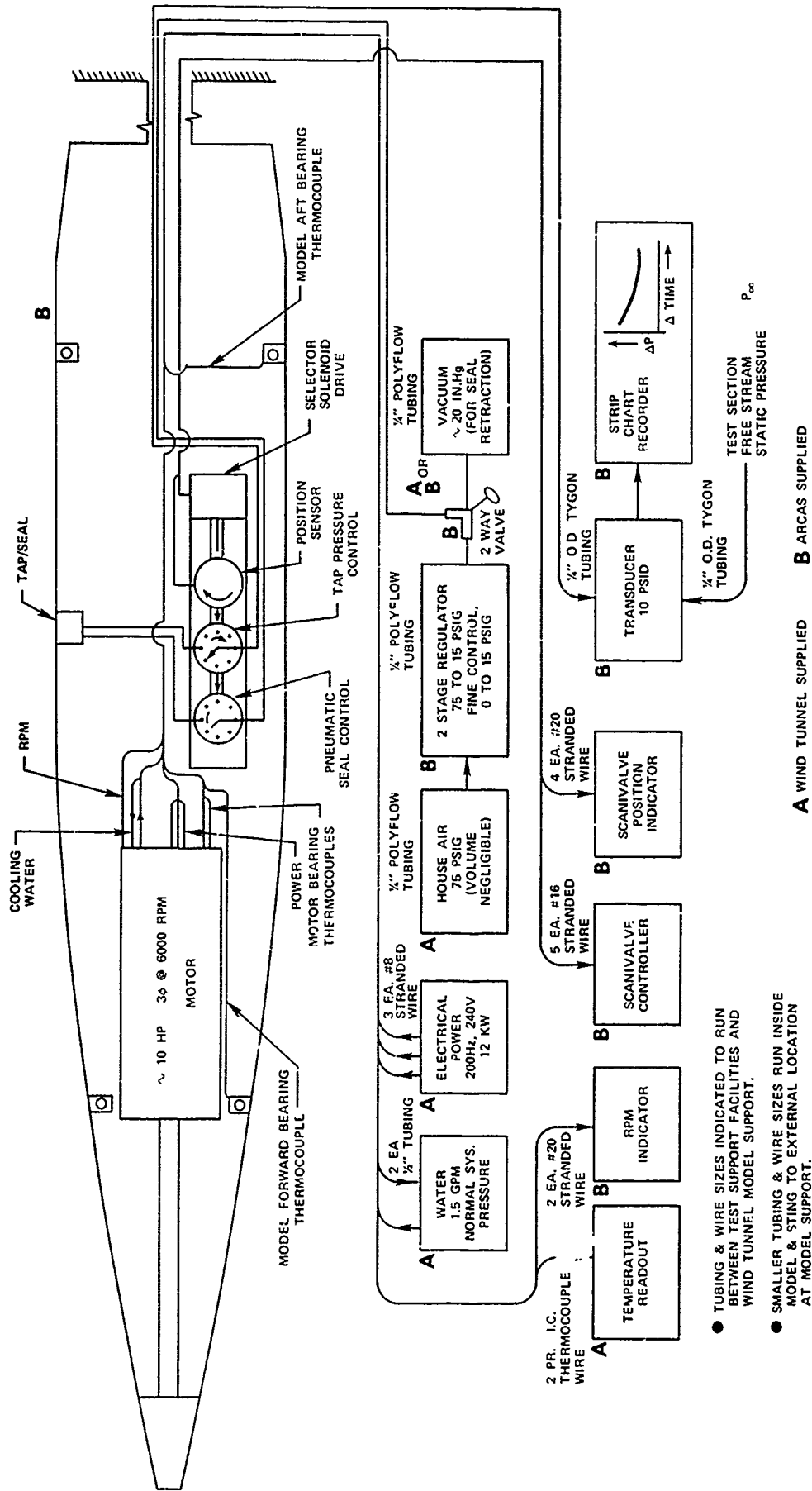


Figure 15. Details of Model Operation and Instrumentation Interfacing

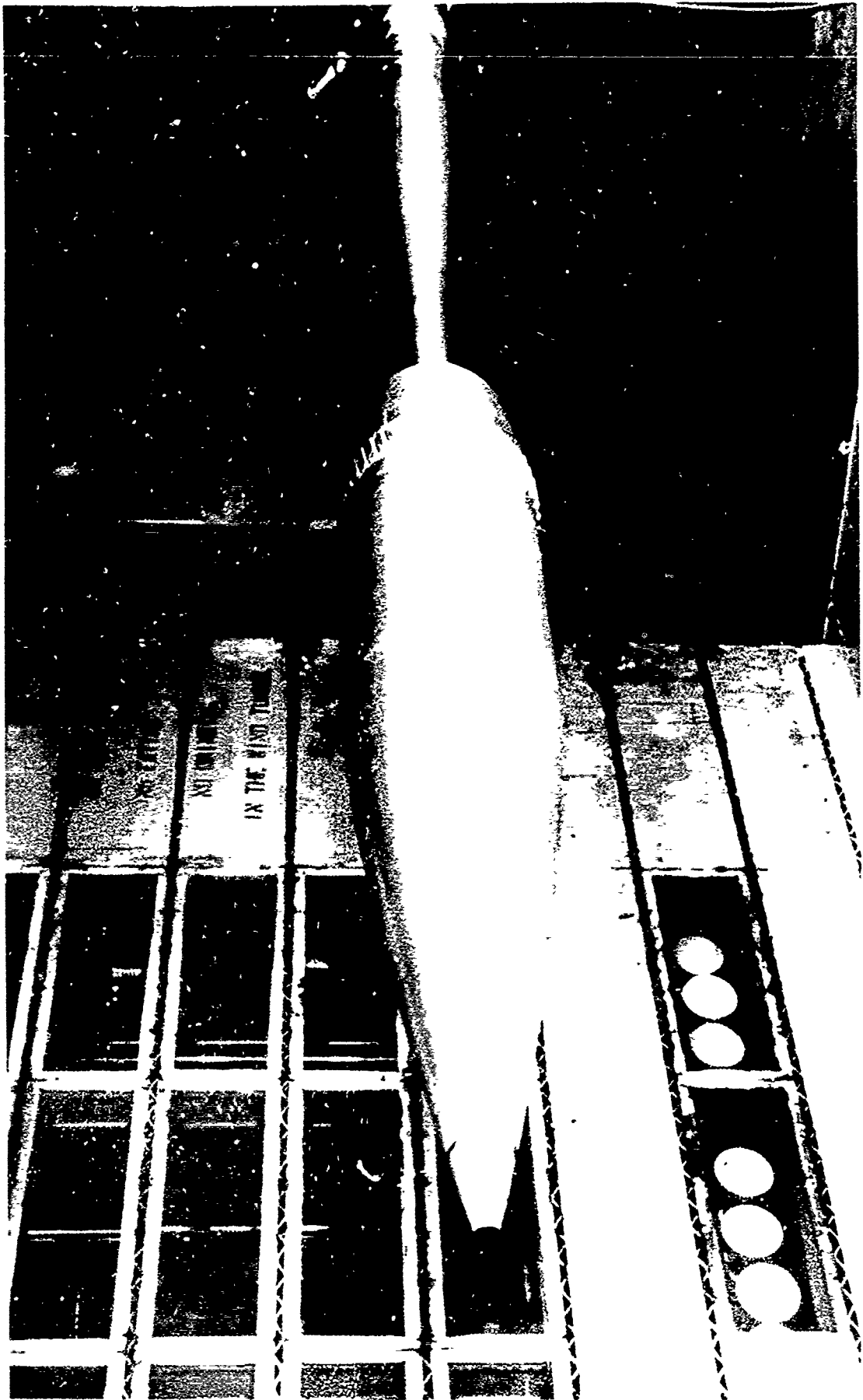


Figure 16. Photograph of Model Installed in 14-Foot Transonic Wind Tunnel



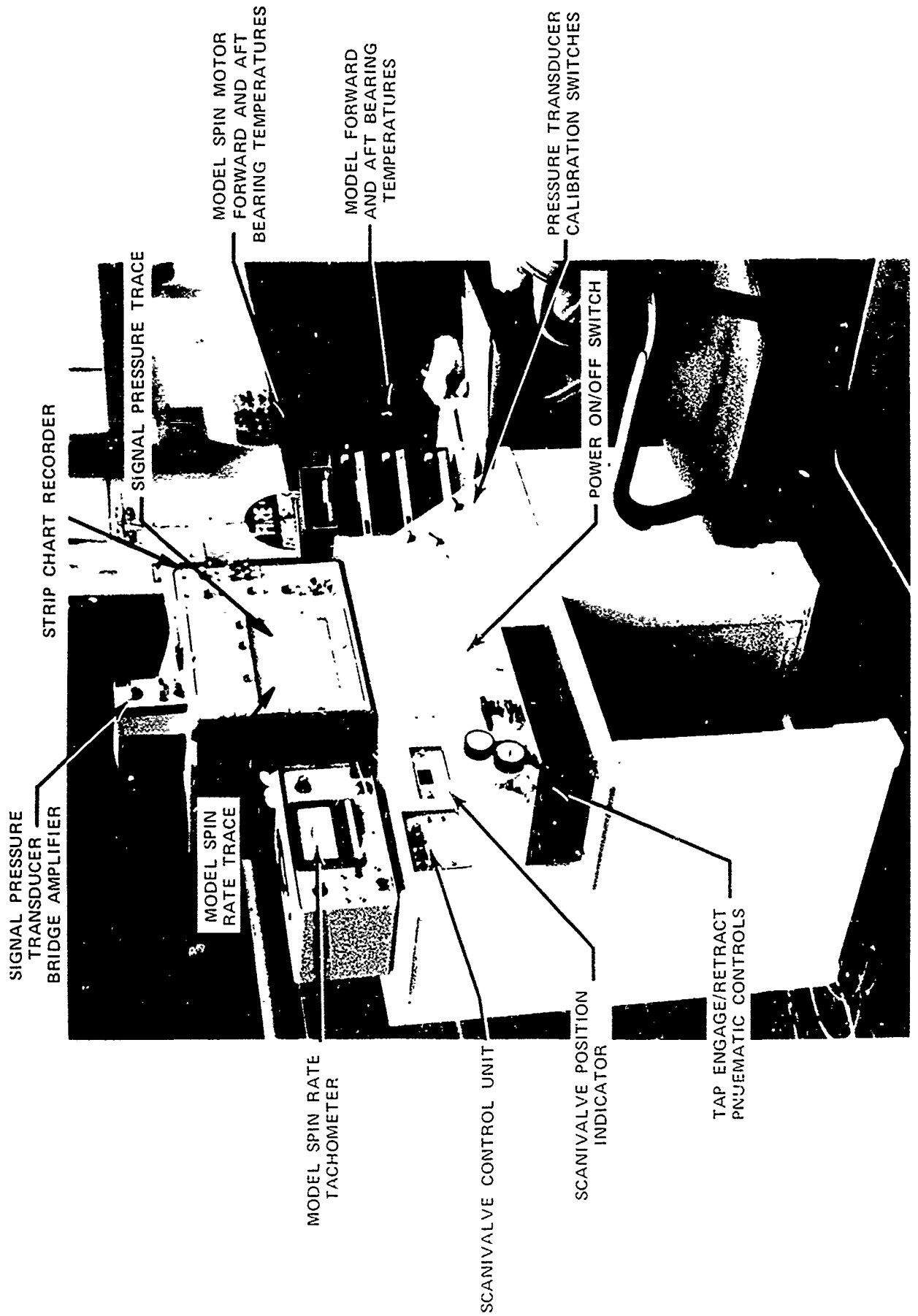
Figure 16. Continued

The special console, shown in Figure 17, was located in the tunnel control room and contained the single differential pressure transducer used to measure the surface pressure of the model with respect to the test section's free stream static pressure. The strip chart recorder continuously displayed the output of the pressure transducer as a function of time, thereby allowing the quality of the data to be assessed as testing proceeded. The console included the capability to remotely zero and calibrate the transducer while the tunnel was operating. Pressure tap selection, engagement, and disengagement were accomplished by controls located in the console. The model rotational speed and critical model bearing temperatures were also monitored with instrumentation located on the control console. Changes in the angle of attack, roll head movement, and model spin motor operations were controlled by wind tunnel personnel. Calibration of the roll angle of the model core was done by machining an indexed flat surface on the model sting. This surface was aligned with the primary row of model pressure taps as the zero degree reference. A clinometer placed on the flat allowed model roll alignment to within 1 minute of arc.

#### 4. TEST PROCEDURE

The wind tunnel test program is summarized in Figure 18. All testing was done at a Mach number of 0.94. The model was tested at angles of attack of 0, 4, and 10 degrees for model spin rates of 0 and 4,900 rpm. Because of the constant circumferential pressure distribution for the runs at 0 degree angle of attack, pressures were measured at 45-degree increments of roll, resulting in eight readings per longitudinal location. For the runs at 4 and 10 degrees angle of attack, pressures were measured every 10 degrees of roll, resulting in 36 readings per longitudinal location. Due to time constraints, data for the model with the rotating band were only taken at 0 and 10 degree angles of attack. Also, only the 12 rear most taps were used for the rotating band case because the presence of the band did not affect the forward pressures.

The test procedure was to establish the tunnel air flow at the test Mach number for a given model configuration and angle-of-attack condition. The model was spun up to the desired test spin rate. A single pressure tap seal unit was then remotely engaged by means of the scanivalve selector, which directed high-pressure air to the tap location. A pneumatic pressure of about 5 psi was sufficient to force the designated tap o-ring out against the inner surface of the model shell to provide the sliding seal function. The engaged pressure tap was then able to detect the surface pressure at that location. When the pressure was visually determined to be constant from the strip chart recorder, the wind tunnel data acquisition system recorded the value, reduced it to coefficient form, and printed it out along with the tunnel conditions at that time. The model core was then rotated to the next circumferential position by means of the remotely controlled roll head and the procedure repeated until a complete circumferential circuit was completed. Figure 19 presents a portion of the strip chart record. About 60 to 90 seconds were required for the measured pressure to reach its constant equilibrium value. This pressure was directed through the second scanivalve and down the model support sting via plastic tubing to the pressure transducer located in the data recording console. At the completion of a circumferential circuit, the tap was disengaged and the next tap engaged. Engagement and disengagement of seals could be accomplished remotely while the model was spinning and the tunnel operating.





**WIND TUNNEL TEST PROGRAM  
NASA AMES 14-FT TRANSONIC TUNNEL  
TEST NO. 463, 8 FEB 83 - 6 MAR 83**

SERIES NUMBER	ROTATING BAND	MACH NO.	ANGLE OF ATTACK (DEG)	SPIN RATE (RPM)	PRESSURE READINGS			CIRCUMFERENTIAL INCREMENTS	RUN NUMBER
					LONGITUDINAL LOCATIONS	CIRCUMFERENTIAL LOCATIONS			
1	OFF	.94	0	0	20	8	45°	7-11, 12-25	
2			↓	-4,900	↓	↓	↓	73-92	
3			4	0	36	36	10°	30-49	
4			↓	-4,900	↓	↓	↓	98-112	
5			10	0	↓	↓	↓	113-122, 127-135	
6			↓	-4,900	↓	↓	↓	50-69	
7	ON		0	0	10	8	10°	144-154	
8			↓	-4,900	↓	↓	↓	181-192	
9			10	0	36	36	10°	157-168	
10			↓	-4,900	↓	↓	↓	169-180	

\*NOTE: 1) SPIN RATE CORRESPONDS TO  $pd/2V$  OF .162 FOR 7.95 INCH DIAMETER MODEL.  
 2) NOMINAL TEST SECTION CONDITIONS:  $T_o = 130^\circ\text{F}$ ,  $R_d = 4 \times 10^6/\text{FT}$ ,  $q = 743 \text{ LB/FT}^2$ ,  
 $P_\infty = 8.35 \text{ LB/IN}^2$

Figure 18. Wind Tunnel Test Program



The relatively long time required for the pressure to become constant was due to the 150-foot length of tubing between the model and the transducer. This resulted in seal engagement times of about 40 minutes to complete a circumferential survey at a particular longitudinal location. Over 12 hours were needed to test a single model configuration. Locating the transducer in the control room had several advantages, such as ease of calibration, absence of temperature effects, and the provision of pressure pulse damping volume. With the test method validated, in future use of this technique, the transducer could be located in the model or in the sector sting with a marked reduction in tube length, pressure lag time, and consequent data acquisition time.

After each spinning test, the shell was removed and the o-rings changed. In most cases, the o-rings showed little or no wear. In fact, one seal was engaged for over 75 minutes without experiencing any detectable wear. However, certain tap locations did produce severe o-ring wear, as noted in Table 1. For the non-spinning tests, the model shell was simply locked to the core by a set screw with the vent holes aligned with their respective taps. This allowed the shell and core to be rotated together by the roll head. Certain operational difficulties were encountered during the initial portion of the test. When fully retracted, the seal blocks would cover the pneumatic port, reducing the effective base area over which the engaging air pressure could act. Also, in the retracted position, the clearance between the seal block and the inside diameter of the shell was great enough to occasionally allow an o-ring to escape from its groove in the seal block. Both problems were effectively eliminated by placing a wire ring with a 0.30-inch diameter beneath the seal block. This prevented the base of the seal block from covering the pneumatic pressure port and reduced the clearance between the shell and seal so that the o-ring could not be dislodged from its groove in the seal block. It was found that 600,000 CS silicone fluid could be used to help retain the o-rings in their grooves. Following an o-ring change, each seal was sequentially engaged and the shell manually rotated back and forth to mate the contour of the seal with the internal contour of the shell to ensure seal engagement and alignment with the inside surface of the shell. The seals were then retracted prior to starting of the test run.

## 5. ANALYSIS OF RESULTS

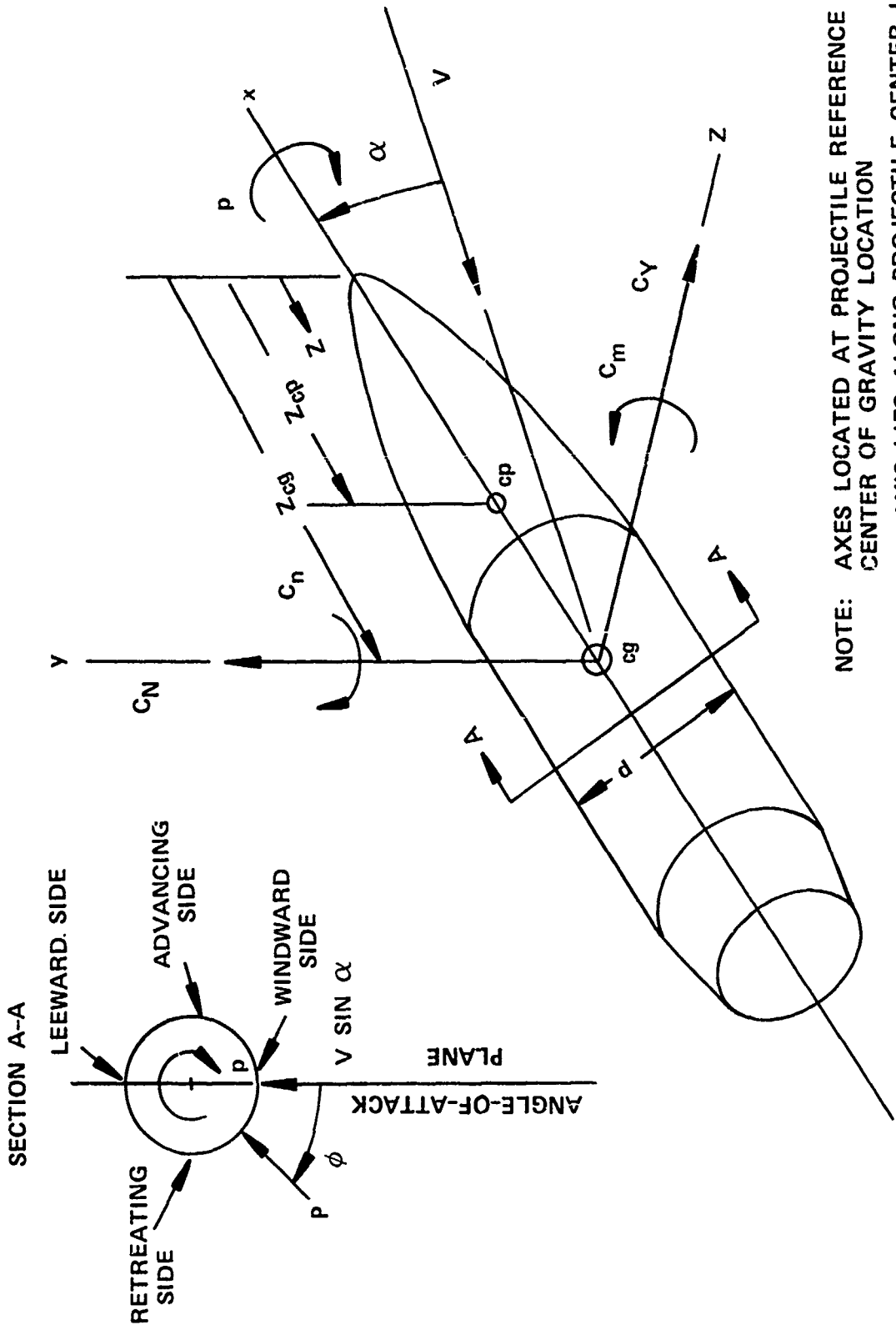
### 5.1 General.

The surface pressure data were reduced to coefficient form as defined in Figure 20. All of the wind tunnel data are tabulated in Appendix A, which lists the pressure coefficient measured at each circumferential and longitudinal location for a particular test run. The data are also provided in plotted form in Appendix B. The differential pressures measured and the associated pressure coefficients are plotted as a function of circumferential angle for each longitudinal tap location. Each set of data is presented for a specific model configuration for both the spinning and non-spinning cases. These data are available for use in evolving or validating theoretical or computational fluid dynamic analyses of the Magnus effect.

The following sections include examples of specific effects and observed phenomena obtained during this test.

Table 1. Summary of O-Ring Wear During Test

RUN	TAP NO.	ROTATING BAND	$\alpha$ (DEG)	COMMENTS
81	9	OFF	0	GREASE BLACKENED AROUND SOME SEALS, NO NOTICEABLE WEAR ON ANY O RINGS, DATA APPEARED OK
92	20		4	
93	1		10	O RING HAD SOME SURFACE SCRATCHES
102	10			O RING BADLY WORN, DATA ERRATIC
127	1			O RING WORN
144	14	ON		O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
145	15			O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
146	16			O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
152	10			O RING BAD
153	11			O RING WORN
164	16		0	O RING WORN
165	17			O RING WORN
166	18			SEALBLOCK STEM BROKEN, ALLOWING PNEUMATIC AND TEST PRESSURES TO COMMUNICATE



NOTE: AXES LOCATED AT PROJECTILE REFERENCE CENTER OF GRAVITY LOCATION  
 $x$  - AXIS LIES ALONG PROJECTILE CENTER LINE  
 $y$  - AXIS IS NORMAL TO  $x$  - AXIS AND LIES IN ANGLE-OF-ATTACK PLANE  
 $z$  - AXIS IS NORMAL TO ANGLE-OF-ATTACK PLANE

Figure 20. Definition of Terms

## 5.2 Surface Pressure Distribution.

Figure 21 shows the pressure measured along the projectile for an angle of attack of 0 degrees for both the spinning and non-spinning cases. Note that spin produces slightly reduced pressures at most locations. These data illustrate the ability of the testing method to accurately measure even these small pressure effects. During the test, pressure differences of .025 psi could be determined. The non-spinning data in Figure 21 show excellent agreement with the previous NASA-Langley test data.

Figure 22 contains circumferential surface pressure data at a point on the boattail under spinning conditions. The model was spun in a counter-clockwise direction (pilot's view) in order to provide a tightening effect on the right-hand threaded shell components. This negative spin resulted in a positive Magnus force as defined in Figure 16. Data are shown for two separate tests and illustrate the excellent repeatability obtained, even for the severe pressure variations present.

Figure 23 shows similar pressure data measured on another boattail location for the model spinning in opposite directions. These data illustrate that no asymmetric bias was present with the model or instrumentation. The Magnus effect is clearly illustrated in Figure 24, which shows the difference in the circumferential pressure distribution due to spin. A net negative pressure difference is produced on the retreating side of the projectile and a positive pressure difference on the advancing side, resulting in an additive effect to the Magnus force. These data indicate that spin produces both a circumferential shift as well as a distortion of the non-spinning pressure distribution.

The effect of angle of attack on the circumferential surface pressure distribution at a point on the boattail under spinning conditions is shown in Figure 25. Note that the pressure asymmetry that produces the Magnus force is most pronounced at the largest angle of attack. The resultant local force in the angle-of-attack plane denoted by  $C_{N_i}$  (computed by integrating the circumferential pressure distribution) does not change with angle of attack for this location. However, the resultant force normal to the angle-of-attack plane  $C_{y_i}$  (i.e., the Magnus force) increases nonlinearly with angle of attack. These data also illustrate the presence of a negative pressure "hump" on the advancing side of the leeward point of the projectile ( $\phi = 140$  degrees). This effect is present at all longitudinal locations for the spinning projectile at an angle of attack of 10 degrees, as illustrated in Figure 26, but does not occur at an angle of attack of 4 degrees. This hump may be due to the presence of an attached vortex on the leeward side of the projectile at the larger angle of attack.

## 5.3 Force and Moment Distribution.

The circumferential pressure distributions were integrated to determine the resultant normal force (in the angle-of-attack plane) and side force (normal to the angle-of-attack plane) at each longitudinal tap location. These local forces are presented in coefficient form as  $C_{N_i}$  and  $C_{y_i}$ , respectively as defined in

Figure 20. These coefficients indicate the detailed influence of the Magnus effect at various longitudinal positions on the projectile.

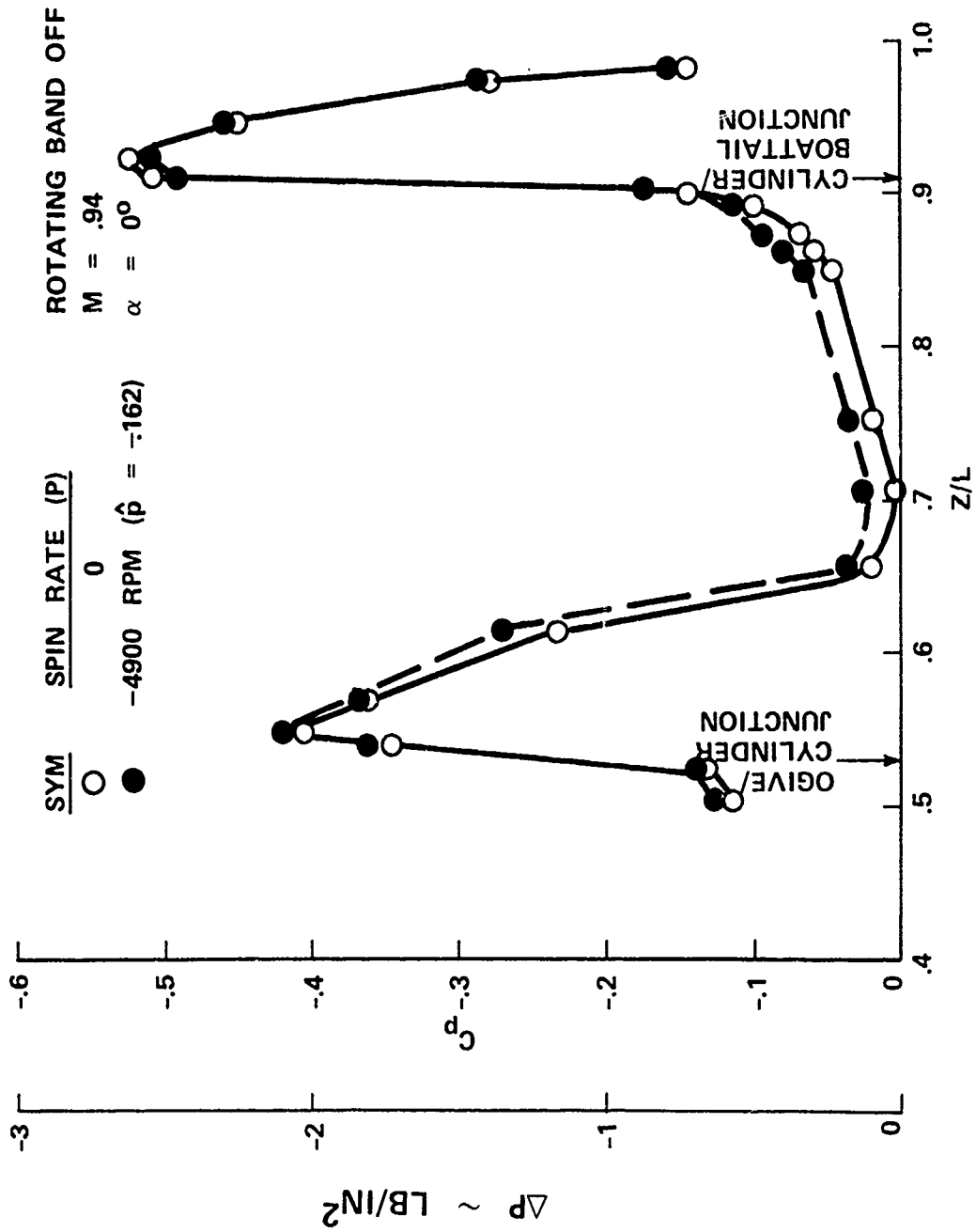


Figure 21. Effect of Spin on Longitudinal Surface Pressure Distribution for  $\alpha = 0$  Degrees

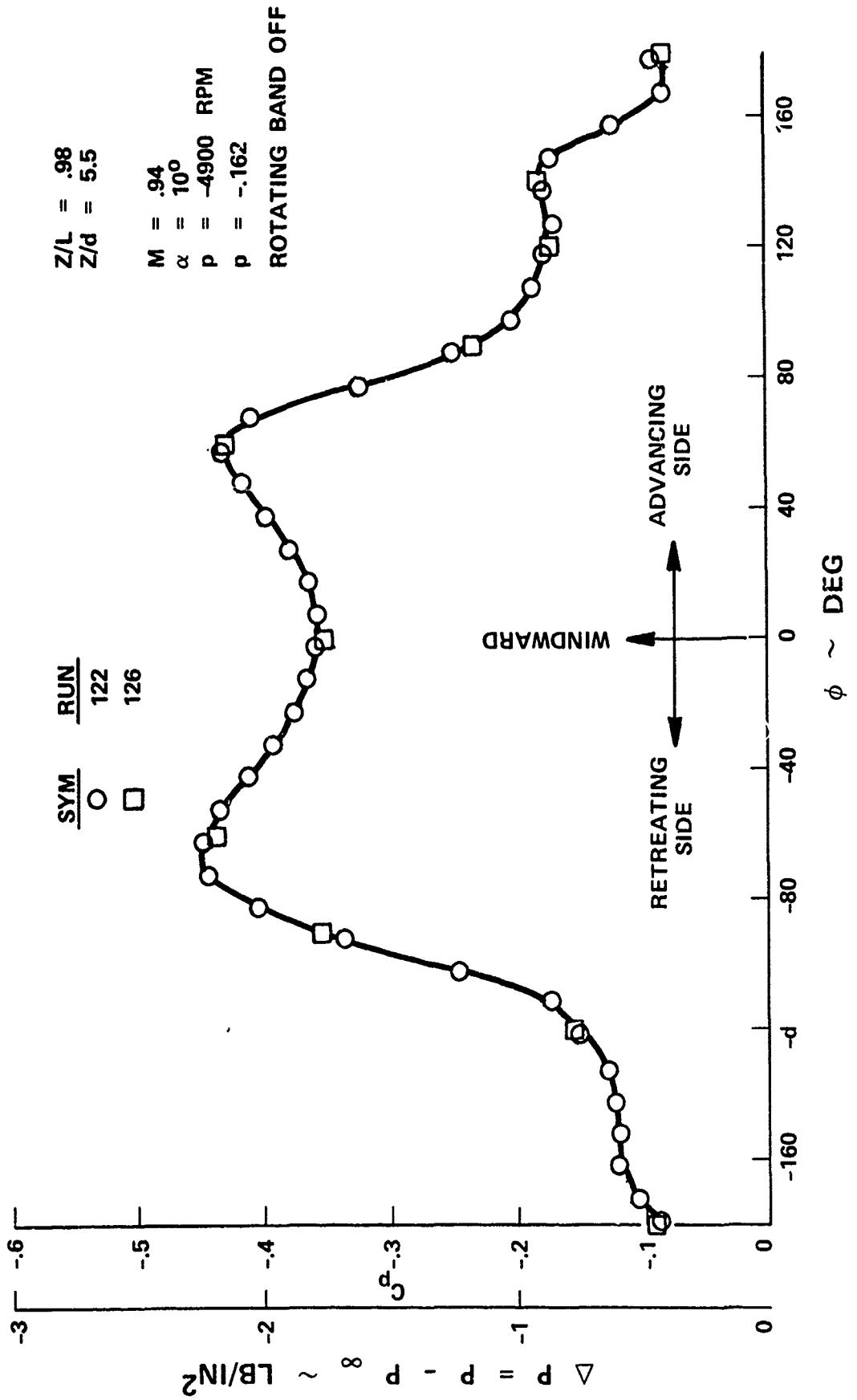


Figure 22. Circumferential Pressure Distribution on Boattail - Demonstration of Repeatability



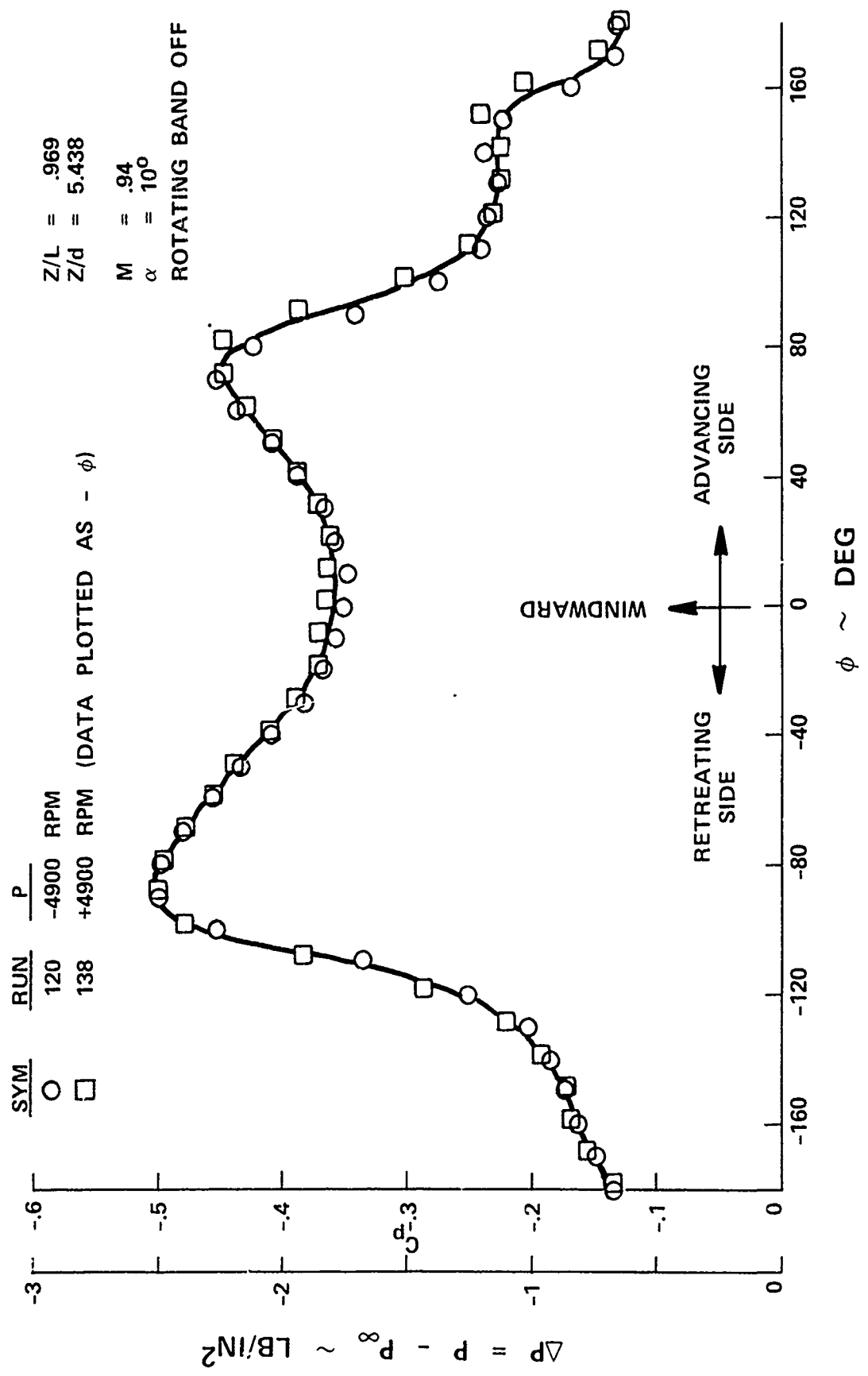


Figure 23. Circumferential Pressure Distribution on Boattail -

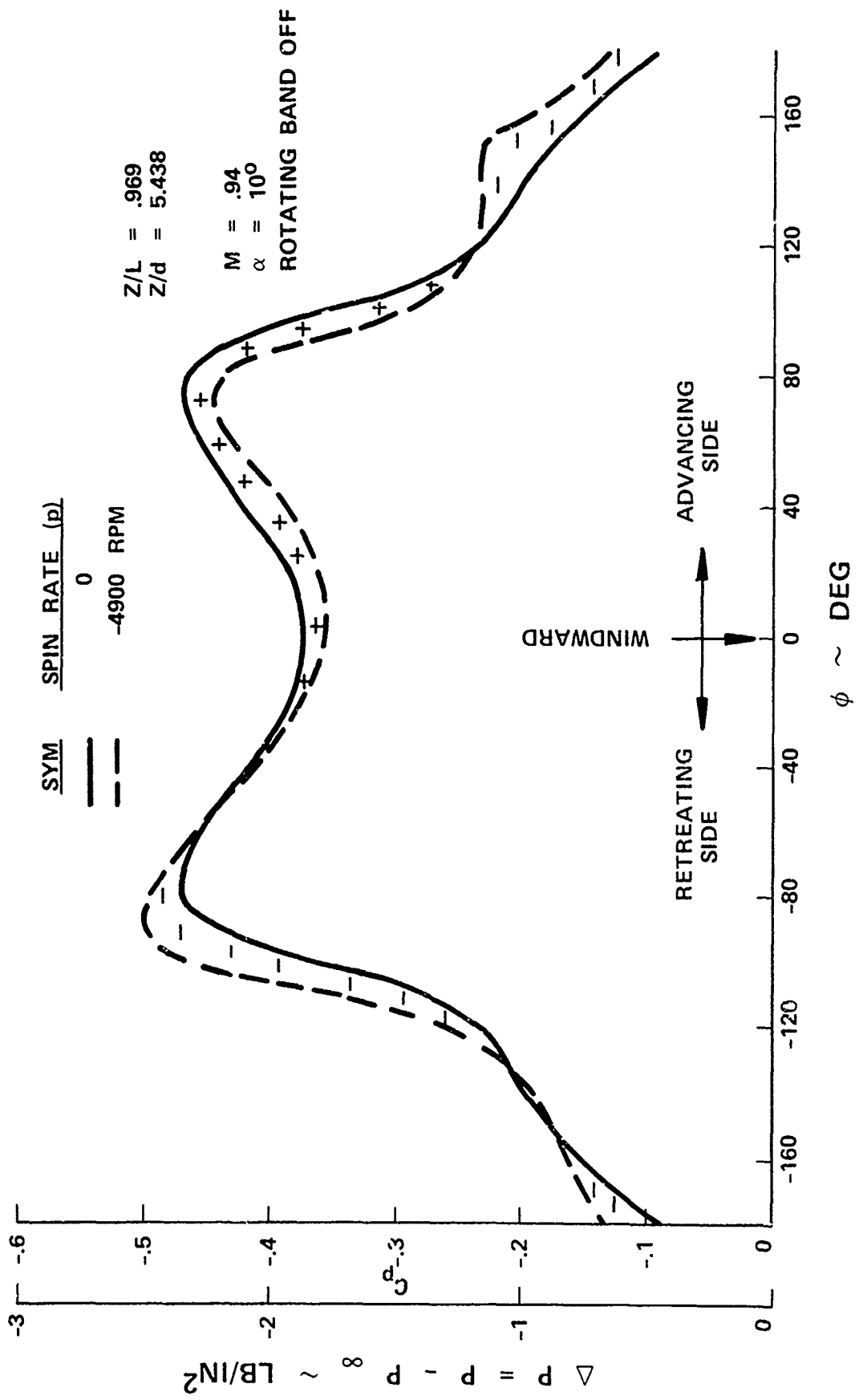
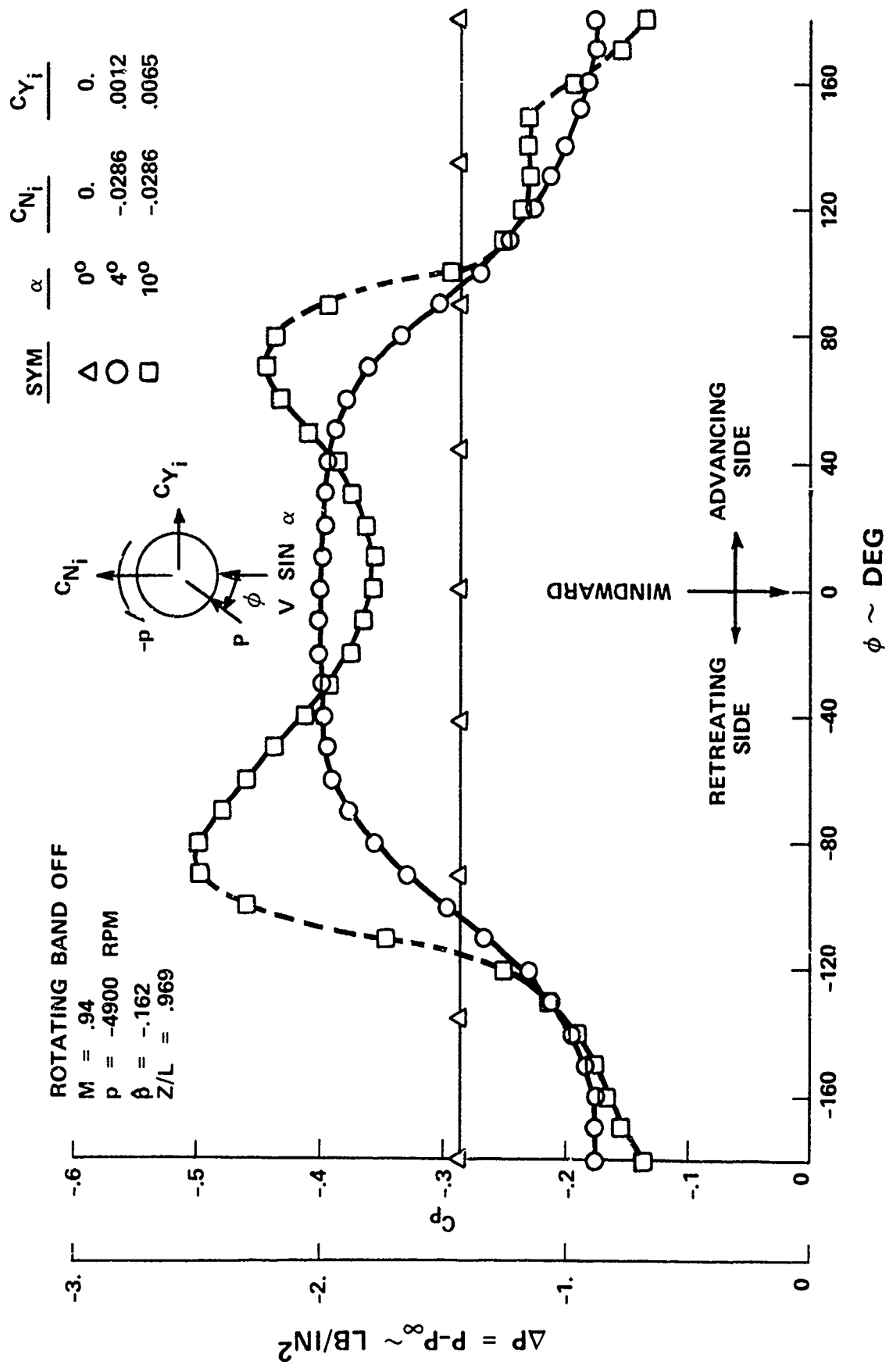


Figure 24. Effect of Spin on Boattail Circumferential Pressure



ROTATING BAND OFF

MACH. = .94

$\alpha = 10^\circ$

$p = -4900$  RPM

- = CENTER OF HUMP
- ◊ = LIMITS OF EFFECT

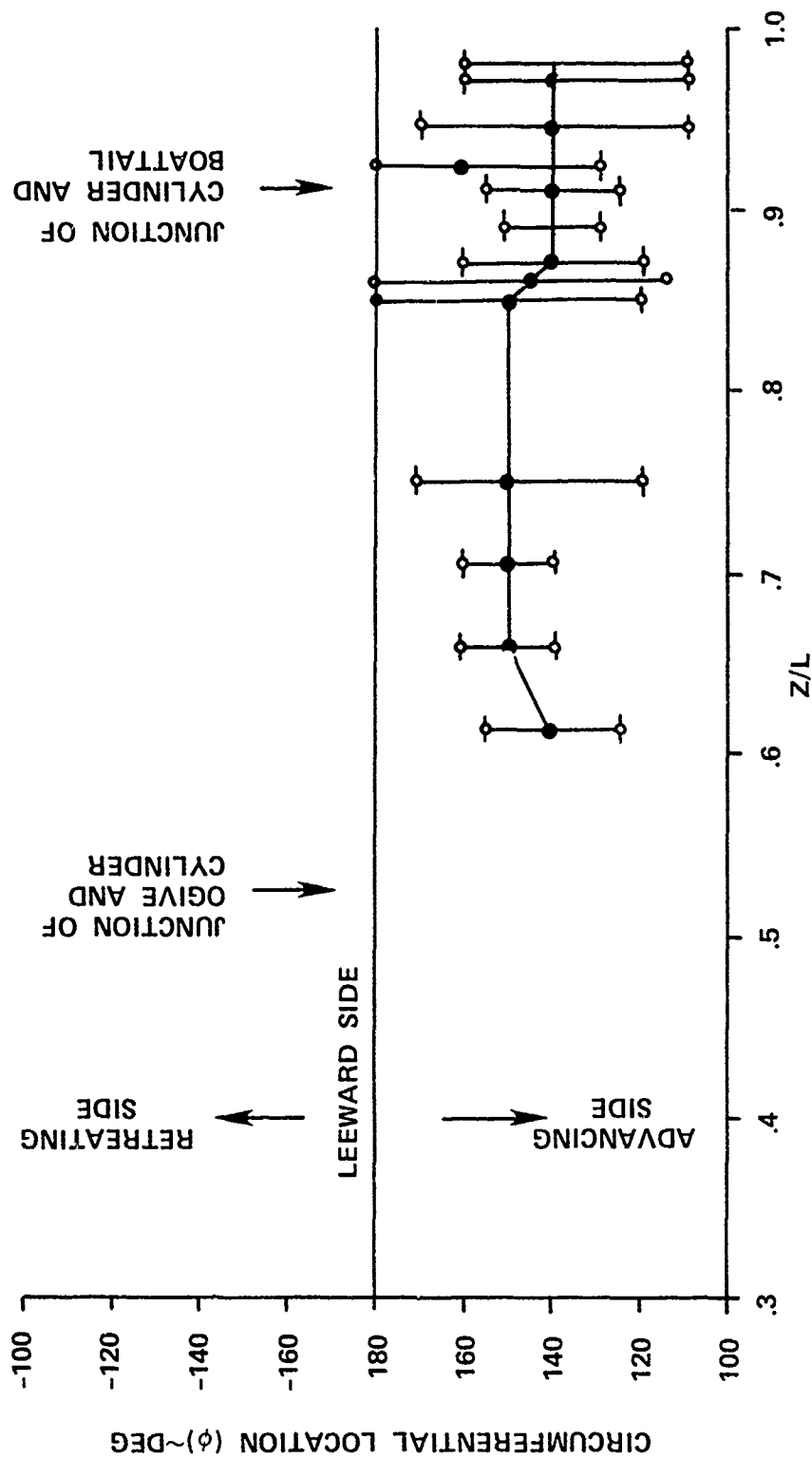


Figure 26. Circumferential Location of Negative Pressure Hump as a Function of Longitudinal Location ( $\alpha = 10$  Degrees)

The resulting normal and side force distributions are shown in Figures 27 through 29 for angles of attack of 0, 4, and 10 degrees, respectively. As expected, the Magnus-induced side force is significantly less than the normal force. Figure 30 shows the side force at an enlarged scale, indicating that the largest Magnus effect occurs over the boattail.

Although a net positive Magnus force results for both the 4 and 10 degree angles of attack, there are longitudinal regions on the projectile where the local Magnus force acts in a negative sense. For the 10-degree case, this situation only occurs in the vicinity of the shock waves; whereas for the 4-degree case, it is also present on the cylindrical section and at the aft portion of the boattail. Note that the greatest Magnus side force occurs on the cylindrical portion of the projectile for the 4-degree case and on the boattail for the 10-degree case. A particularly large Magnus side force is present on the boattail at a 10-degree angle of attack. This large Magnus force, in combination with the large moment arm between the boattail and projectile center of gravity, results in a significant Magnus yawing moment.

By integrating the local force coefficients in a longitudinal sense, the normal force and side (i.e., Magnus) force coefficients can be determined for each component (i.e., ogive, cylinder, and boattail), as well as for the total projectile. In a similar fashion, pitching moments and yawing (i.e., Magnus) moments can also be computed, as well as their respective centers of pressure. The moment terms are referred to a reference point representing the nominal center of gravity of the actual projectile located .625 calibers from the nose.

These terms are summarized in Appendix C and include the coefficient derivatives for force and moment with respect to angle of attack and nondimensional spin rates. The detailed derivations of the local normal and Magnus side force and their centers of pressure are also contained in Appendix C. The use of these derivatives both facilitate interpretation of the data and allow comparison with results from other studies. The relative contributions of the various projectile components to the Magnus force and moment terms depicted in Figure 30 are summarized in Table 2. These quantitative values further demonstrate the importance of the boattail in producing the Magnus effect.

The influence of spin on the normal force distribution for angles of attack of 0, 4, and 10 degrees is indicated in Figures 31 through 33. At both angles of attack, the presence of spin decreases the negative normal force acting on the forward portion of the cylindrical section of the projectile and decreases the positive normal force acting over the aft portion of the cylindrical section, which should result in a larger positive force and pitching moment for the spinning case.

The effect of angle of attack on the normal force and moment terms are contained in Table 3 for the non-spinning case and in Table 4 for the spinning case. Tables 5 and 6 show the effect of spin on the normal force and moment terms for angles of attack of 4 and 10 degrees, respectively.

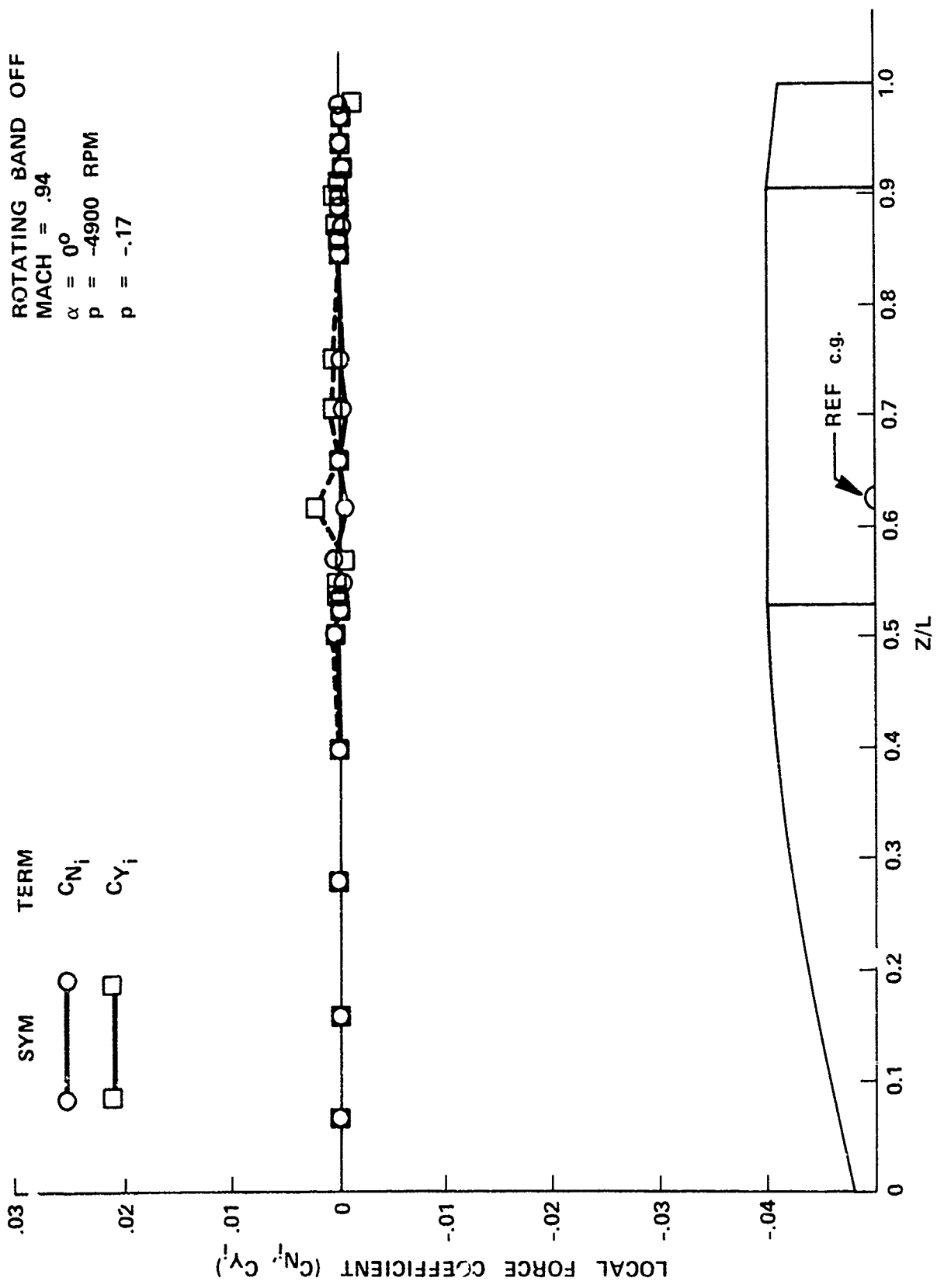


Figure 27. Normal and Side Force Longitudinal Distribution on Spinning Model  
( $\alpha = 0$  Degrees)

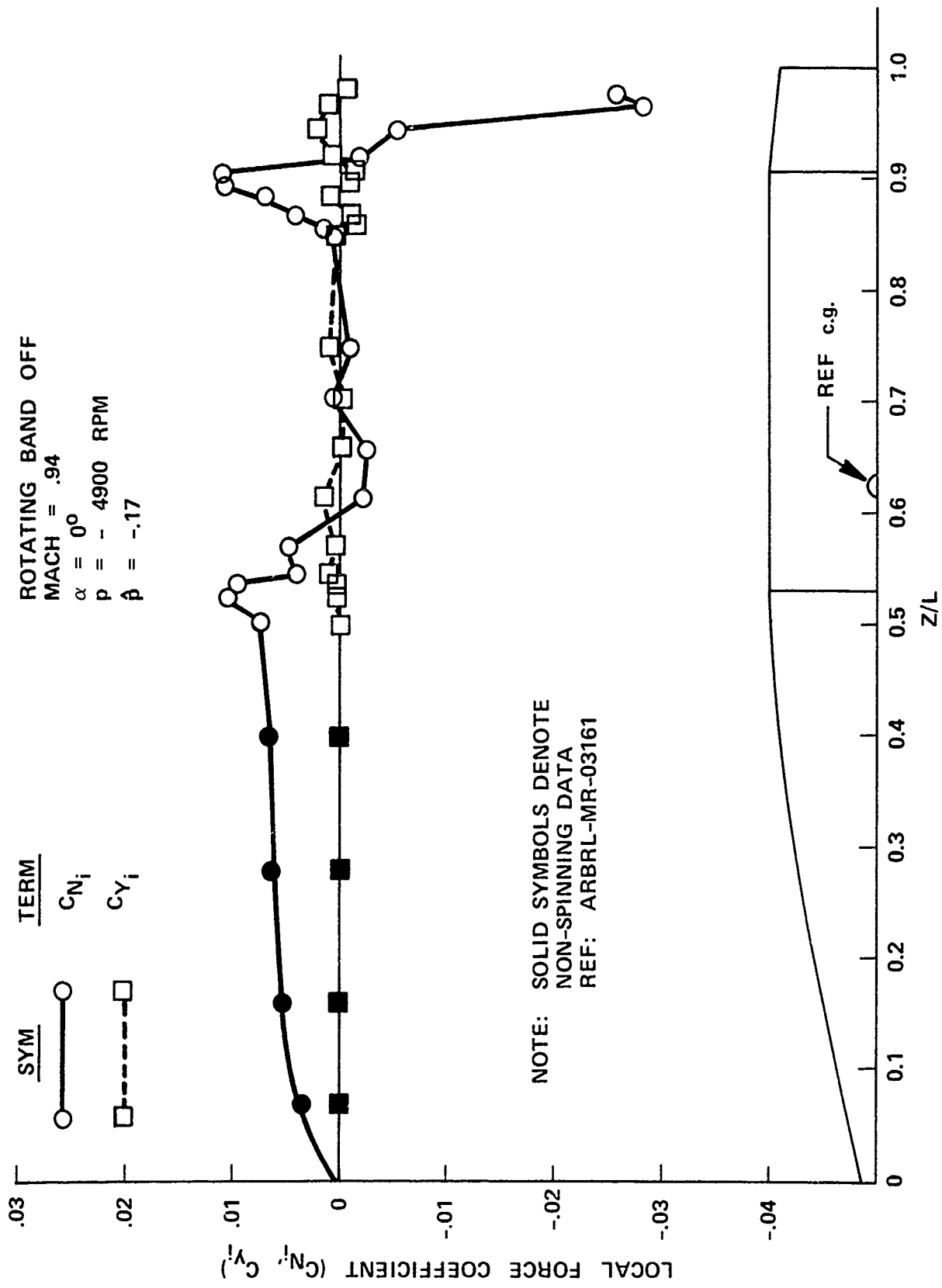


Figure 28. Normal and Side Force Longitudinal Distribution on Spinning Model  
( $\alpha = 4$  Degrees)

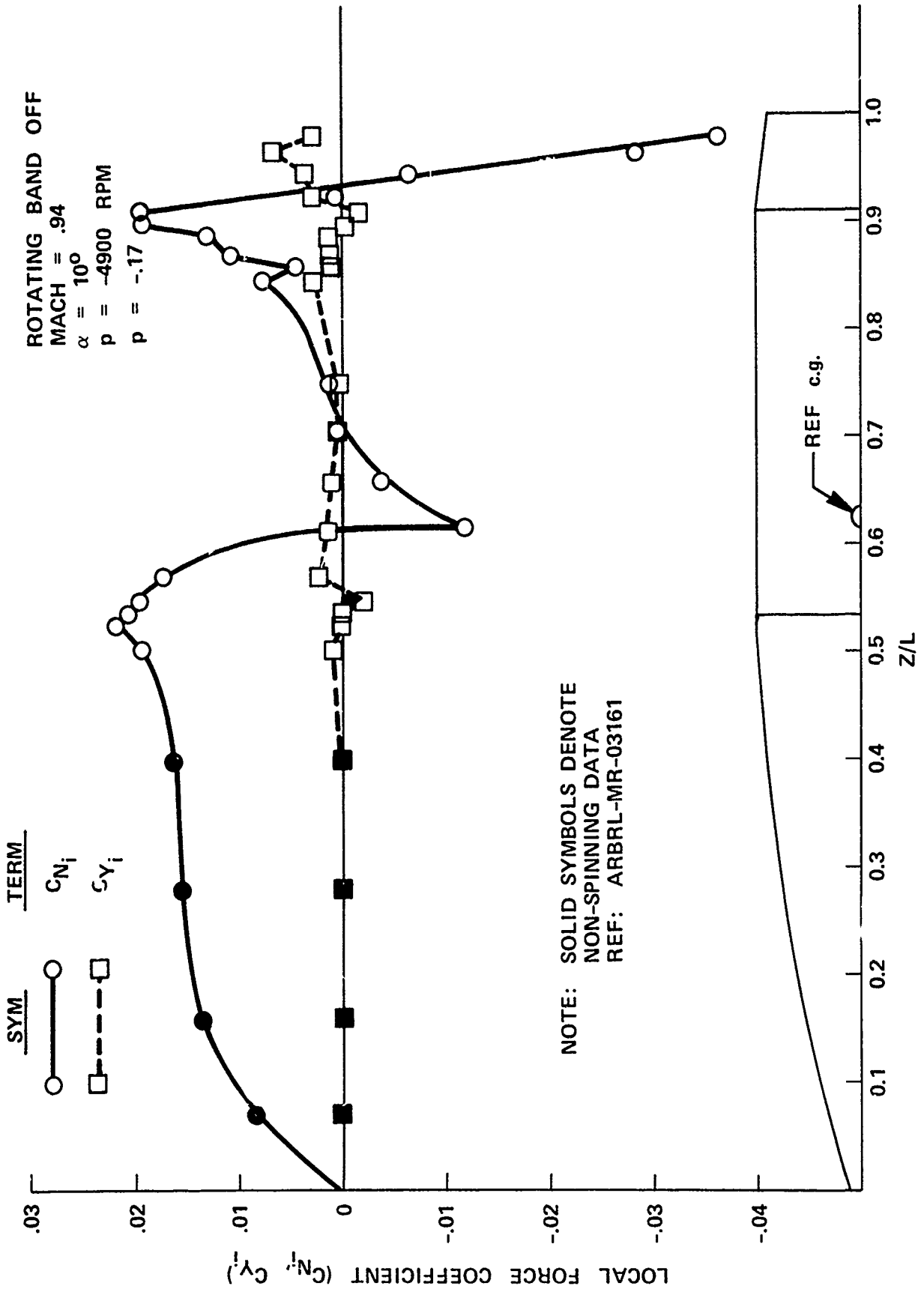


Figure 29. Normal and Side Force Longitudinal Distribution on Spinning Model ( $\alpha = 10$  Degrees)



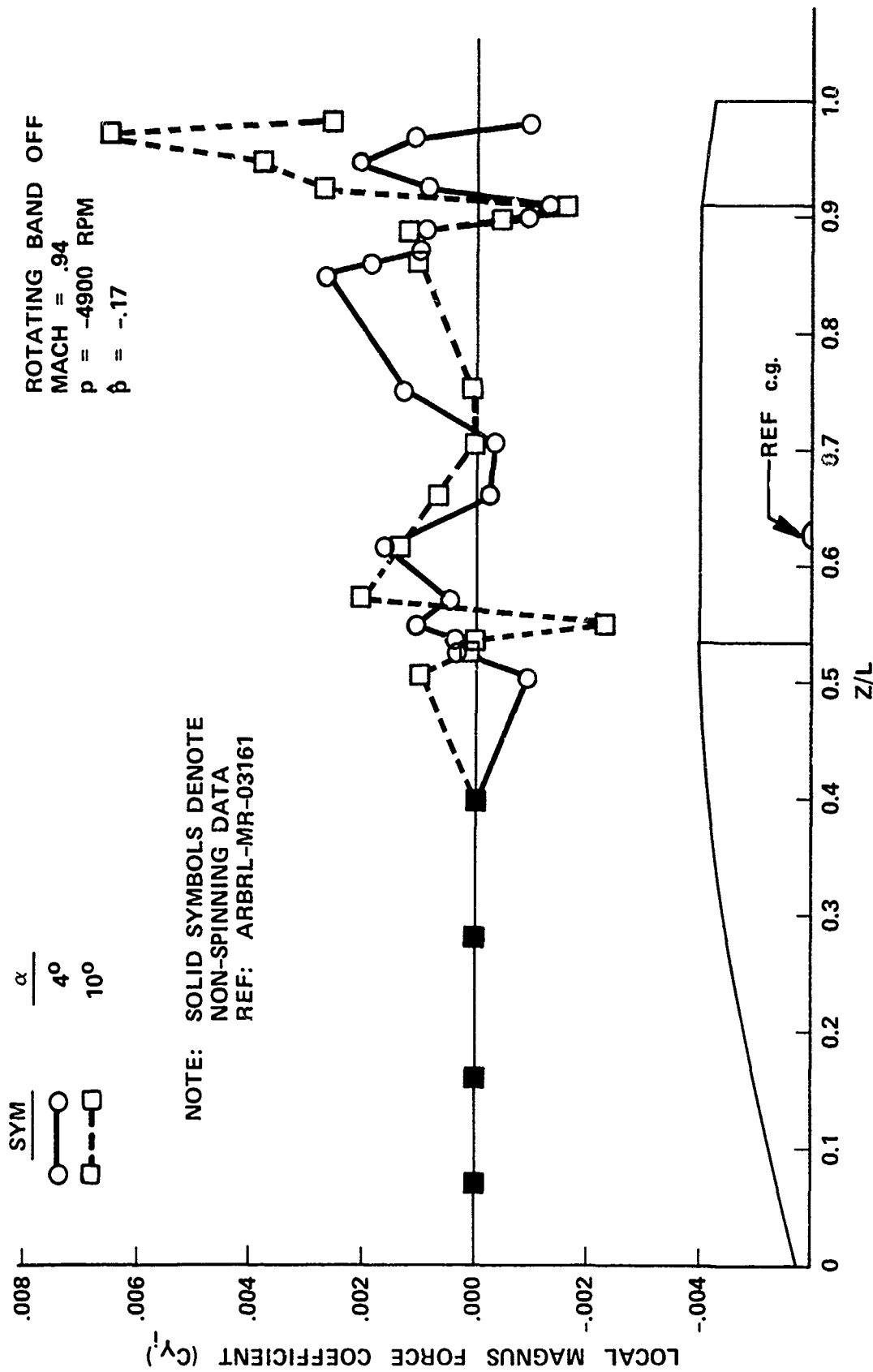


Figure 30. Side Force Longitudinal Distribution on Spinning Model for  $\alpha = 4$  Degrees and  $\alpha = 10$  Degrees

Table 2. Side Force and Moment Terms for  $\alpha = 4$  Degrees and  $\alpha = 10$  Degrees (Rotating Band Off)

TERM	$\alpha = 4^\circ$	$\alpha = 10^\circ$
MODEL CONFIGURATION: 3 CALIBER OGIVE		
2 CALIBER CYLINDER		
.5 CALIBER BOATTAIL		
ROTATING BAND OFF		
$Z_{cg}/L = .625$		
TEST CONDITIONS: MACH .94		
$pd/2V = .162$		
$C_{Y_p}$ (OGIVE)	.000	-.004
$C_{Y_p}$ (CYLINDER)	-.085	-.092
$C_{Y_p}$ (BOATTAIL)	-.019	-.080
$C_{Y_p}$ (TOTAL)	-.104	-.176
$C_{n_p}$ (OGIVE)	.000	-.003
$C_{n_p}$ (CYLINDER)	.056	.063
$C_{n_p}$ (BOATTAIL)	.033	.148
$C_{n_p}$ (TOTAL)	.090	.208
$Z_{cp}/L$ (MAGNUS)	.779	.836

ROTATING BAND OFF  
 MACH = .94  
 $\alpha = 0^\circ$

<u>SYM</u>	<u>P</u>	<u><math>\hat{p}</math></u>
○	0	0
□	-4900	-.17

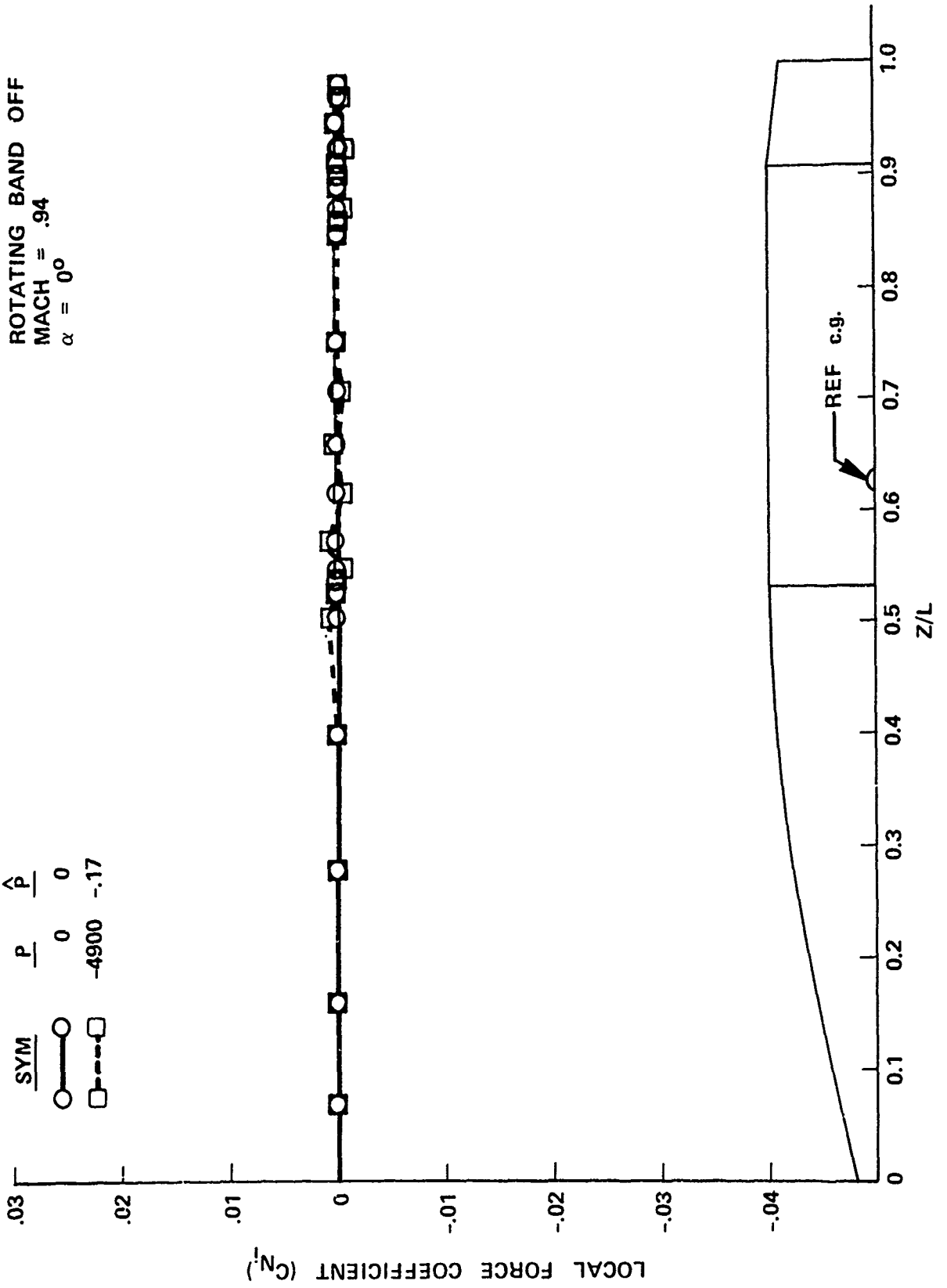


Figure 31. Effect of Spin on Normal force Longitudinal Distribution  
 ( $\alpha = 0$  Degrees)

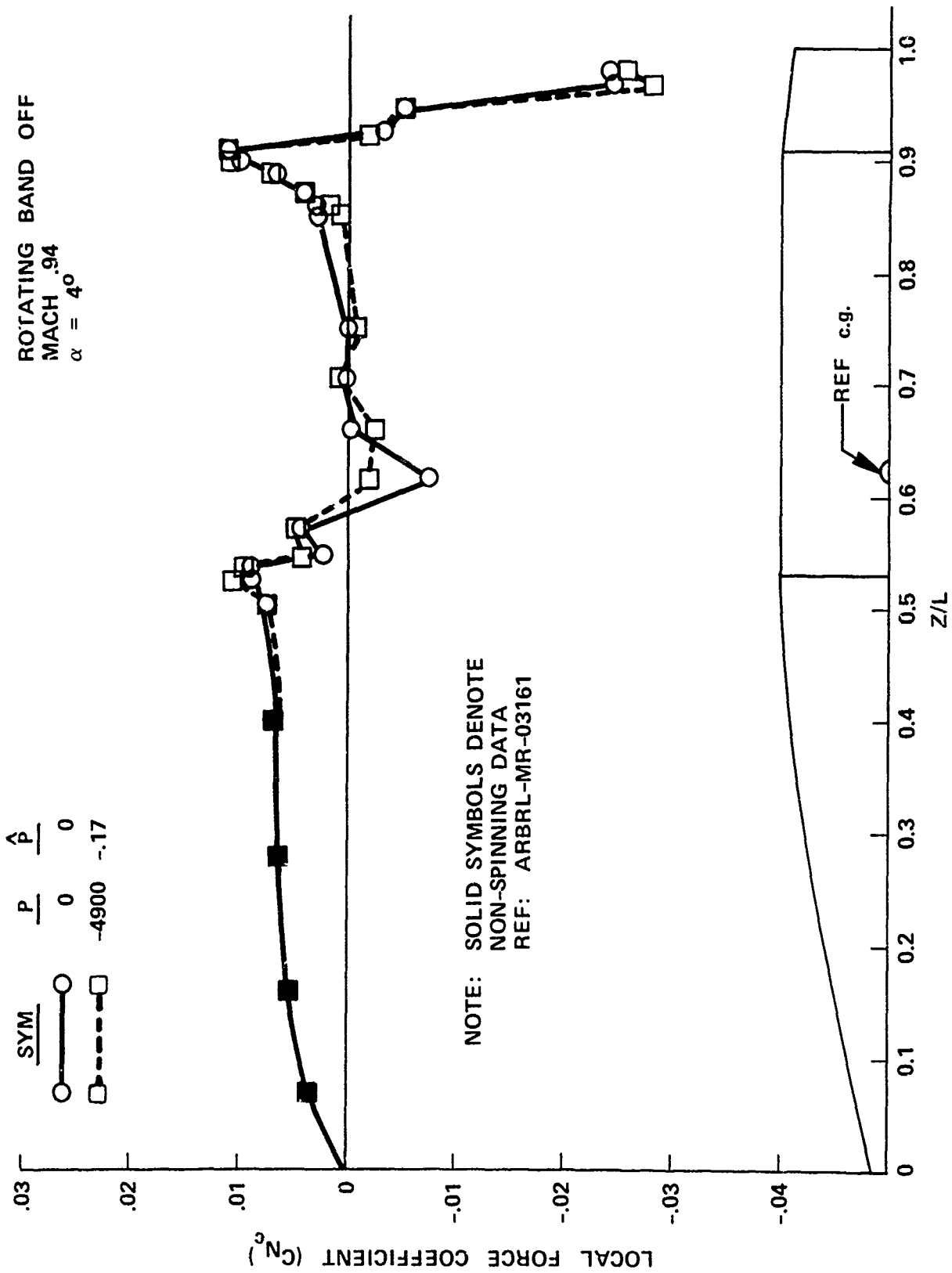


Figure 32. Effect of Spin on Normal Force Longitudinal Distribution  
( $\alpha = 4$  Degrees)

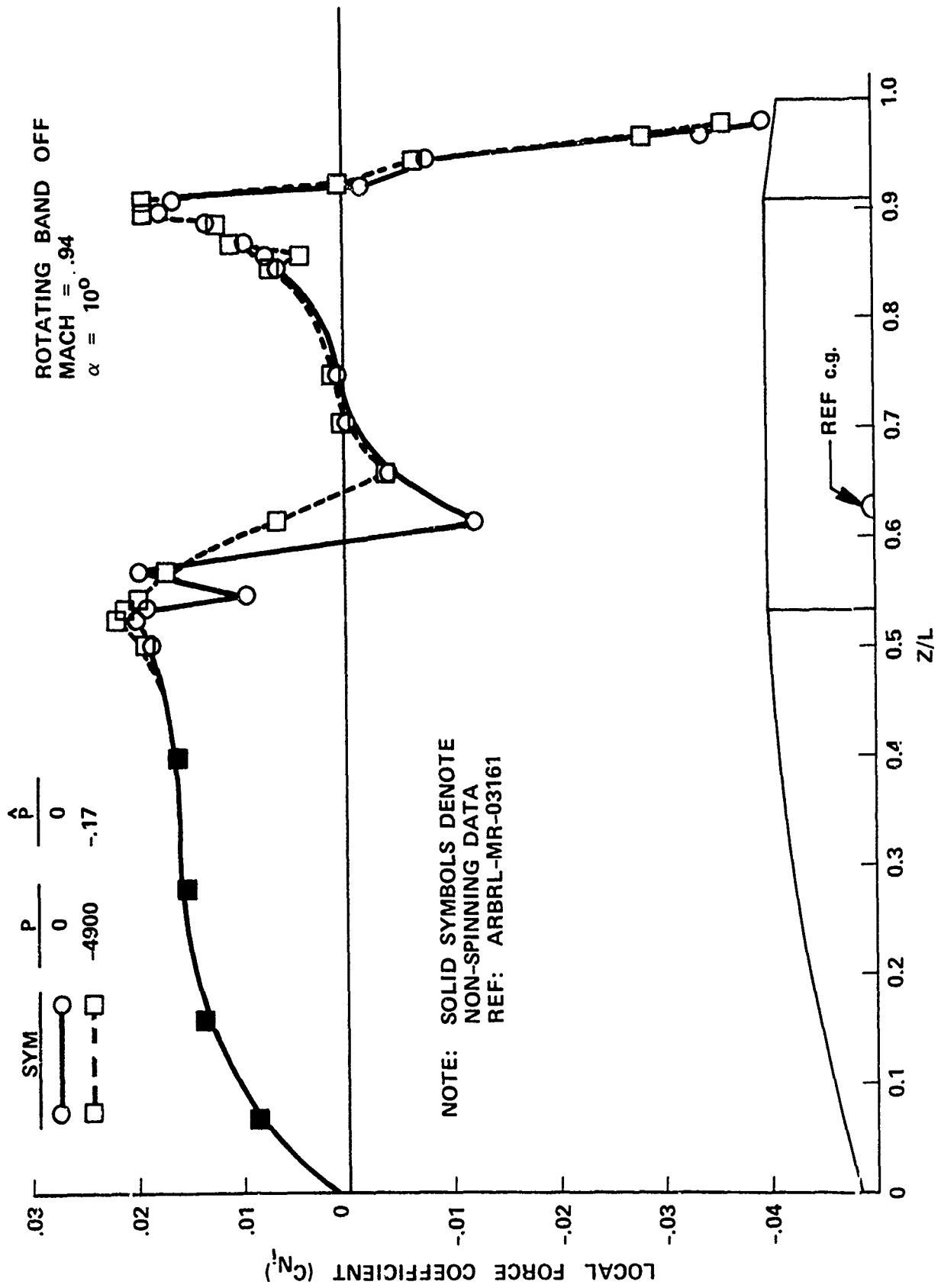


Figure 33. Effect of Spin on Normal Force Longitudinal Distribution  
( $\alpha = 10$  Degrees)

Table 3. Effect of Angle of Attack on Normal Force and Moment Terms for  $\hat{p} = 0$  (Rotating Band Off)

MODEL CONFIGURATION-	TERM	$\alpha = 4^\circ$	$\alpha = 10^\circ$
3 CALIBER OGIVE	$C_{N_\alpha}$ (OGIVE)	1.94	1.93
2 CALIBER CYLINDER	$C_{N_\alpha}$ (CYLINDER)	.25	.33
.5 CALIBER BOATTAIL	$C_{N_\alpha}$ (BOATTAIL)	-.64	-.36
ROTATING BAND OFF	$C_{N_\alpha}$ (TOTAL)	1.55	1.90
$Z_{cg}/L = .625$			
TEST CONDITIONS:			
MACH .94	$C_{m_\alpha}$ (OGIVE)	3.45	3.46
$pd/2v = 0$	$C_{m_\alpha}$ (CYLINDER)	-.50	-.35
	$C_{m_\alpha}$ (BOATTAIL)	1.22	.70
	$C_{m_\alpha}$ (TOTAL)	4.17	3.82
	$Z_{cp}/L$	.15	.30

Table 4. Effect of Angle of Attack on Normal force and Moment Terms for  $\hat{p} = -.162$  (Rotating Band Off)

MODEL CONFIGURATION-	TERM	$\alpha = 4^\circ$	$\alpha = 10^\circ$
3 CALIBER OGIVE	$C_{N_\alpha}$ (OGIVE)	1.96	1.94
2 CALIBER CYLINDER	$C_{N_\alpha}$ (CYLINDER)	.30	.60
.5 CALIBER BOATTAIL	$C_{N_\alpha}$ (BOATTAIL)	-.68	-.31
ROTATING BAND OFF	$C_{N_\alpha}$ (TOTAL)	1.59	2.24
$Z_{cg}/L = .625$			
TEST CONDITIONS:			
MACH .94	$C_{m_\alpha}$ (OGIVE)	3.47	3.47
$pd/2V = .162$	$C_{m_\alpha}$ (CYLINDER)	-.36	-.36
	$C_{m_\alpha}$ (BOATTAIL)	1.30	.60
	$C_{m_\alpha}$ (TOTAL)	4.41	3.71
	$Z_{cp}/L$	.13	.33

Table 5. Effect of Spin on Normal force and Moment Terms for  
 $\alpha = 4$  degrees (Rotating Band Off)

MODEL CONFIGURATION:	TERM	$p = 0$ ( $\hat{p} = 0$ )	$p = -4900$ RPM ( $\hat{p} = -.162$ )
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CAL BOATTAIL REF c.g. AT Z/L = .625	$C_{N_{\alpha}}$ (OG:VE)	1.94	1.96
	$C_{N_{\alpha}}$ (CYLINDER)	.25	.30
	$C_{N_{\alpha}}$ (BOATTAIL)	-.64	-.68
	$C_{N_{\alpha}}$ (TOTAL)	1.55	1.59
MACH .94 $\alpha = 4^{\circ}$ $R_d = 4 \times 10^6$ /FT	$C_{m_{\alpha}}$ (OGIVE)	3.45	3.47
	$C_{m_{\alpha}}$ (CYLINDER)	-.50	-.36
	$C_{m_{\alpha}}$ (BOATTAIL)	1.22	1.30
	$C_{m_{\alpha}}$ (TOTAL)	4.17	4.41
	$Z_{cp}/L$	.15	.13



Table 6. Effect of Spin on Normal Force and Moment Terms for  
 $\alpha = 10$  Degrees (Rotating Band Off)

TERM	$\dot{\hat{p}} = 0$ ( $\hat{p} = 0$ )	$\dot{\hat{p}} = -4900$ RPM ( $\hat{p} = -.162$ )	
MODEL CONFIGURATION: 8 INCH DIAMETER MODEL 3 CALIBER OGIVE	$C_{N\alpha}$ (OGIVE)	1.93	1.94
2 CALIBER CYLINDER	$C_{N\alpha}$ (CYLINDER)	.33	.60
.5 CAL BOATTAIL	$C_{N\alpha}$ (BOATTAIL)	-.36	-.31
REF c.g. AT Z/L = .625	$C_{N\alpha}$ (TOTAL)	1.90	2.24
TEST CONDITION: MACH .94	$C_{m\alpha}$ (OGIVE)	3.46	3.47
$\alpha = 10^\circ$	$C_{m\alpha}$ (CYLINDER)	-.35	-.36
$R_d = 4 \times 10^6$ / FT	$C_{m\alpha}$ (BOATTAIL)	-.70	.60
	$C_{m\alpha}$ (TOTAL)	3.82	3.71
	$Z_{cp}/L$	.27	.33

#### 5.4 Rotating Band Effect.

Details of the rotating band configuration used with the model are contained in Appendix D. Figure 34 compares the longitudinal surface pressure distribution over the non-spinning model at zero angle of attack, both with and without the rotating band. The presence of the rotating band creates larger negative surface pressures in the area of the band and has the effect of moving the low pressure expansion region over the boattail slightly forward. The effect of spin on the pressure distribution over the spinning model with the rotating band at zero angle of attack is illustrated in Figure 35. Spin has the main effect of evening out the pressures on the lands and in the grooves of the rotating band which could be important to theoretical and numerical analyses. The influence of the rotating band on the side force distribution of the spinning model at an angle of attack of 10 degrees is presented in Figure 36. As can be seen, the presence of the rotating band results in significantly larger local Magnus forces in the band area compared to the no band case. On the boattail, the effect of the rotating band reduces the peak local Magnus force, as well as the area over which it acts, relative to the no rotating band condition. The relatively large effects of the band on the cylinder and boattail are essentially self-compensating and result in very little difference in the total Magnus force and moment coefficients between the rotating band on and off cases, as shown in Table 7.

The normal force distribution due to spin for the projectile with rotating band at a 10 degree angle of attack is shown in Figure 37. The effect of the rotating band on the normal force and moment terms is contained in Table 8. For the projectile having the rotating band, the influence of spin is to reduce the local normal force over both the cylinder and the boattail compared to the non-spinning case. The net result is that the spinning projectile possesses a greatly reduced normal force and a slightly lower pitching moment than when not spinning.

#### 5.5 Base Pressure.

Data obtained from pressure tap 20, located on the rear facing surface of the projectile model base, are summarized in Figure 38. At an angle of attack of 0 degrees, the base pressure is very small, and, in fact, is positive for the spinning case. The pressure becomes more negative with increasing angle of attack. No definite trend is evident with spin and angle of attack.

#### 5.6 Comparison of Surface Pressure Test Results With Other Data Sources.

The data from the surface pressure wind tunnel test can be compared with data from other experimental and theoretical sources in order to validate and assess the results. First, the non-spinning pressure distribution from this test can be directly compared with similar data obtained on a model configuration and size in the Langley 16-Foot Transonic Wind Tunnel.<sup>7</sup> Because of the non-spinning condition, only the normal force and moment terms are available and are shown for angles of attack of 4 and 10 degrees in Tables 9 and 10, respectively. Although both projectile models had identical ogive and cylindrical sections, the Langley test model included a 1-caliber boattail; whereas the Ames test model we used had a 0.5-caliber boattail. This difference is evident in the force and moment terms for the boattail and the subsequently larger coefficient derivative for the unstable pitching moment of the larger boattail.

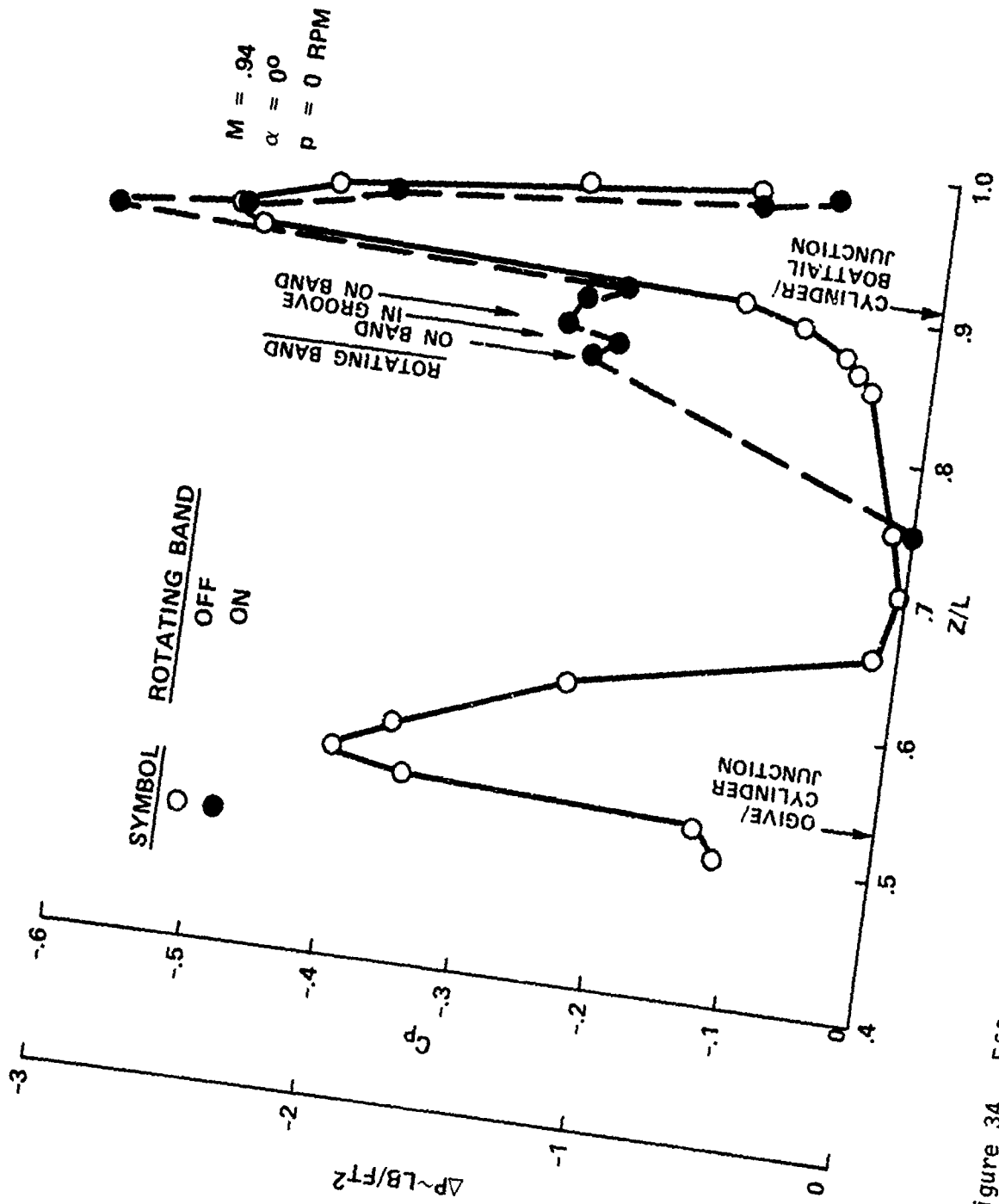


Figure 34. Effect of Rotating Band on Longitudinal Pressure Distribution ( $\alpha = 0$  Degree)

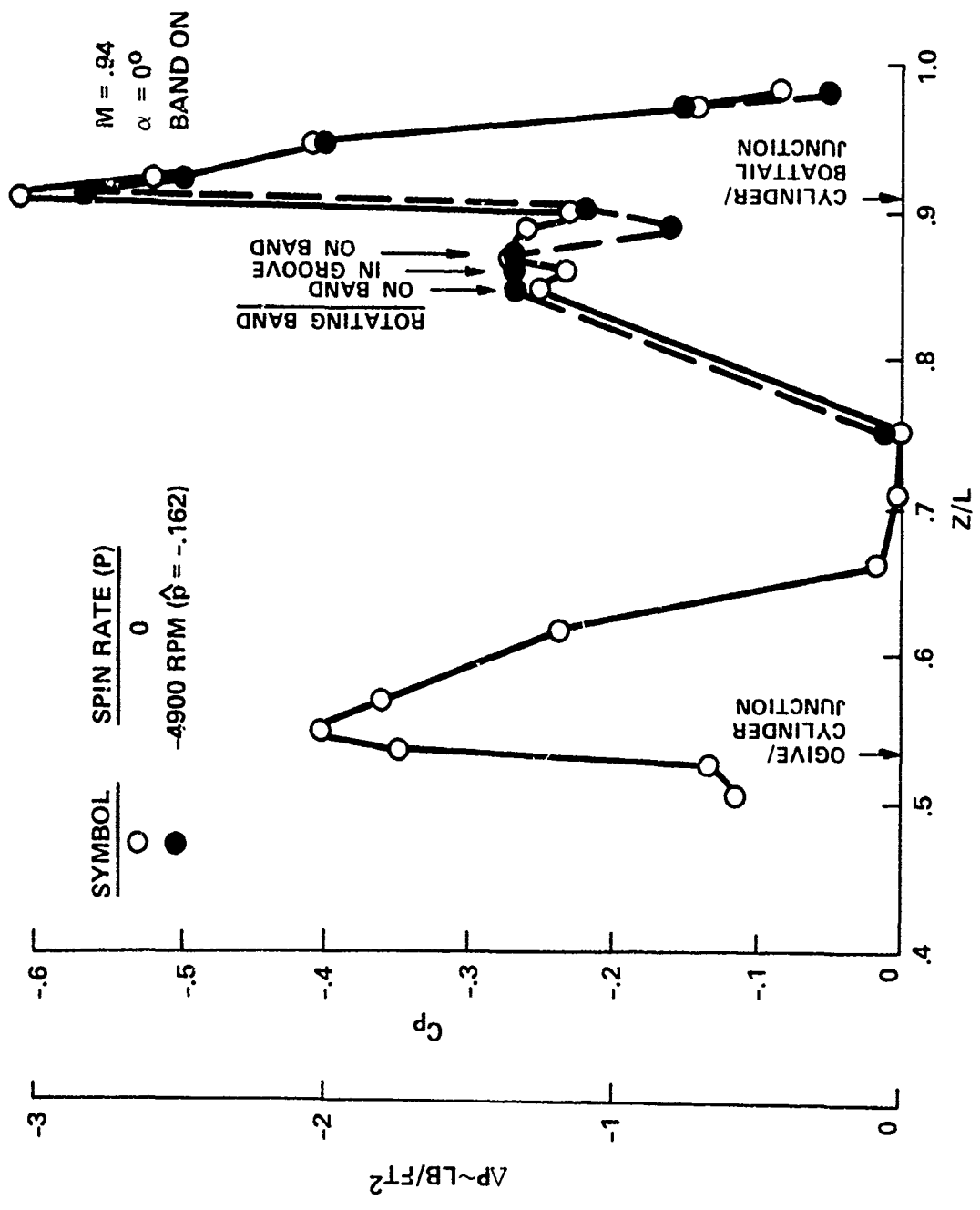


Figure 35. Effect of Spin on Longitudinal Pressure Distribution Over Model With rotating Band ( $\alpha = 0$  Degrees)

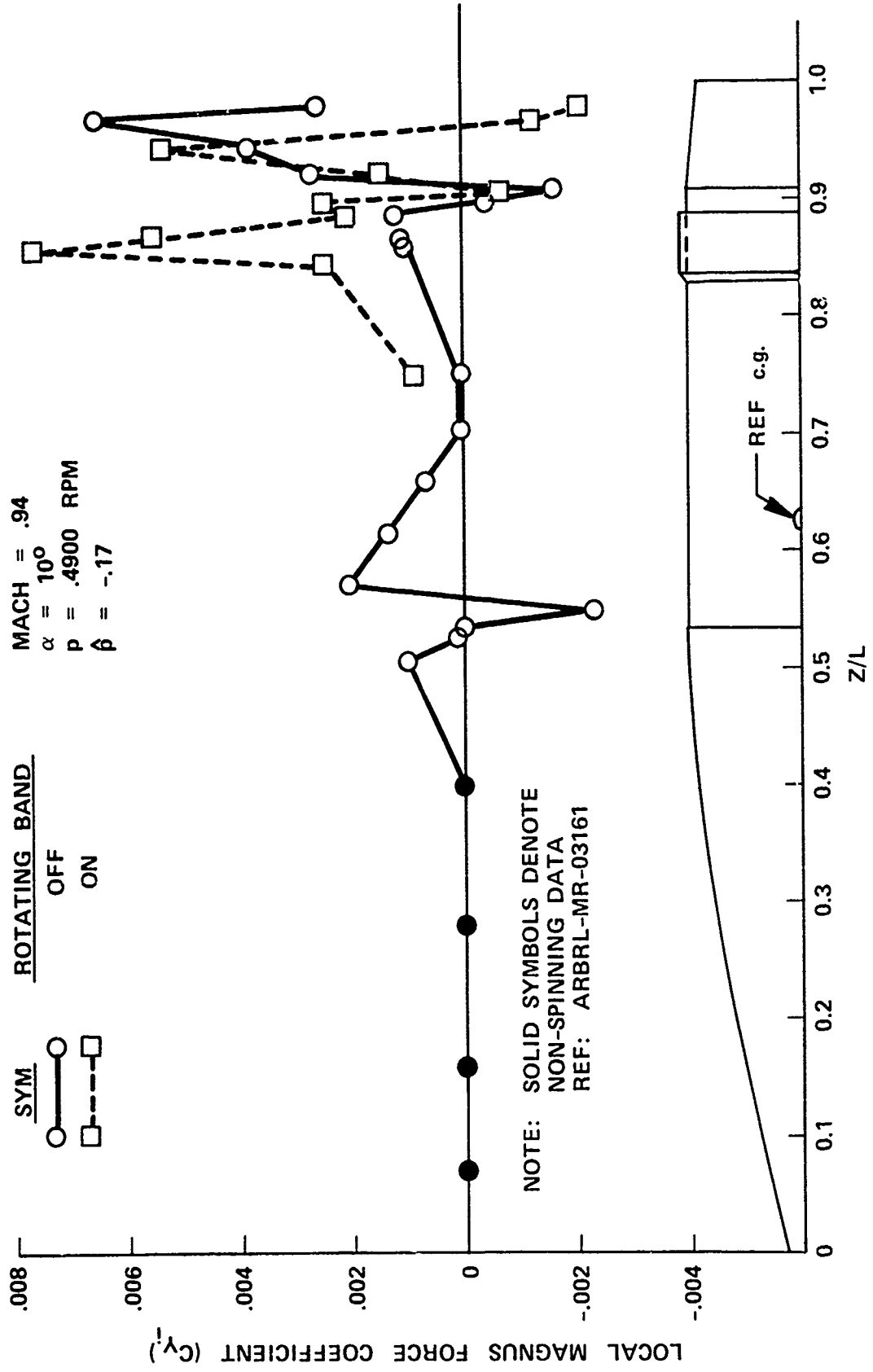


Figure 36. Magnus Side force Distribution on Spinning Model With and Without Rotating Band ( $\alpha = 10$  Degrees)

Table 7. Effect of Rotating Band on Side Force and Moment Terms  
 ( $\alpha = 10$  Degrees)

MODEL CONFIGURATION:	TERM	ROTATING BAND OFF	ROTATING BAND ON
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL	$C_{Y_p}$ (OGIVE)	-.004	-.004
	$C_{Y_p}$ (CYLINDER)	-.092	-.149
	$C_{Y_p}$ (BOATTAIL)	-.080	-.026
	$C_{Y_p}$ (TOTAL)	-.176	-.179
TEST CONDITIONS: MACH .94 pd/2V = .162	$C_{n_p}$ (OGIVE)	-.003	-.003
	$C_{n_p}$ (CYLINDER)	.063	-.139
	$C_{n_p}$ (BOATTAIL)	.148	.043
	$C_{n_p}$ (TOTAL)	.208	.180
	$Z_{cp/L}$ (MAGNUS)	.836	.804

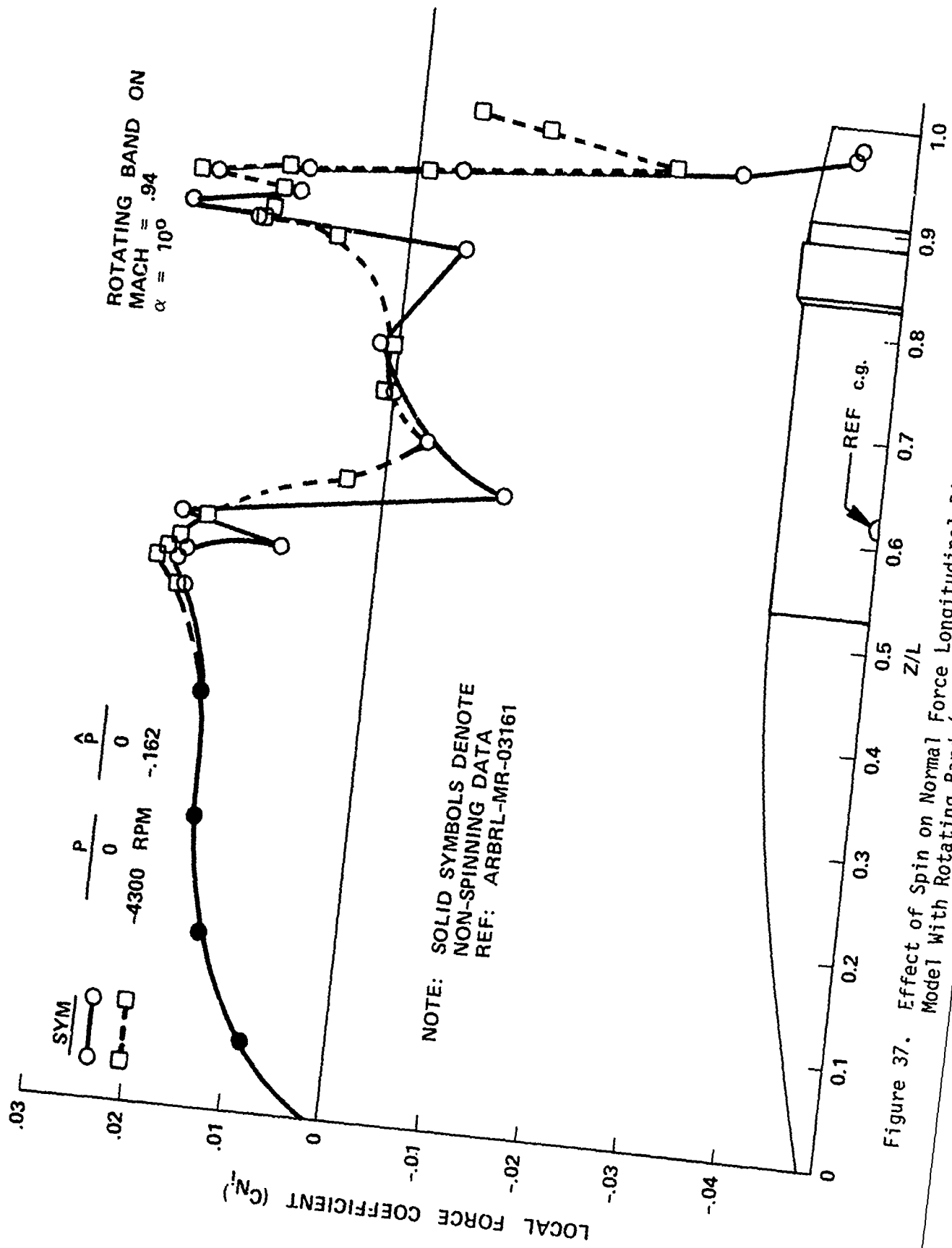


Figure 37. Effect of Spin on Normal Force Longitudinal Distribution Over Model With Rotating Band ( $\alpha = 10$  Degrees)

Table 8. Effect of Rotating Band on Normal Force and Moment Terms  
 ( $\alpha = 10$  Degrees)

MODEL CONFIGURATION:	TERM	ROTATING BAND	
		OFF	ON
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CAL BOATTAIL REF c.g. AT Z/L = .625	$C_{N_\alpha}$ (OGIVE)	1.94	1.95
	$C_{N_\alpha}$ (CYLINDER)	.60	.62
	$C_{N_\alpha}$ (BOATTAIL)	-.31	-.25
	$C_{N_\alpha}$ (TOTAL)	2.24	2.32
TEST CONDITION: MACH .94 $\alpha = 10^\circ$ $R_d = 4 \times 10^6$ /FT $p = -4900$ RPM $\hat{p} = -.162$	$C_{m_\alpha}$ (OGIVE)	3.47	3.47
	$C_{m_\alpha}$ (CYLINDER)	-.36	-.39
	$C_{m_\alpha}$ (BOATTAIL)	.60	.46
	$C_{m_\alpha}$ (TOTAL)	3.71	3.54
	$Z_{cp}/L$	.33	.35



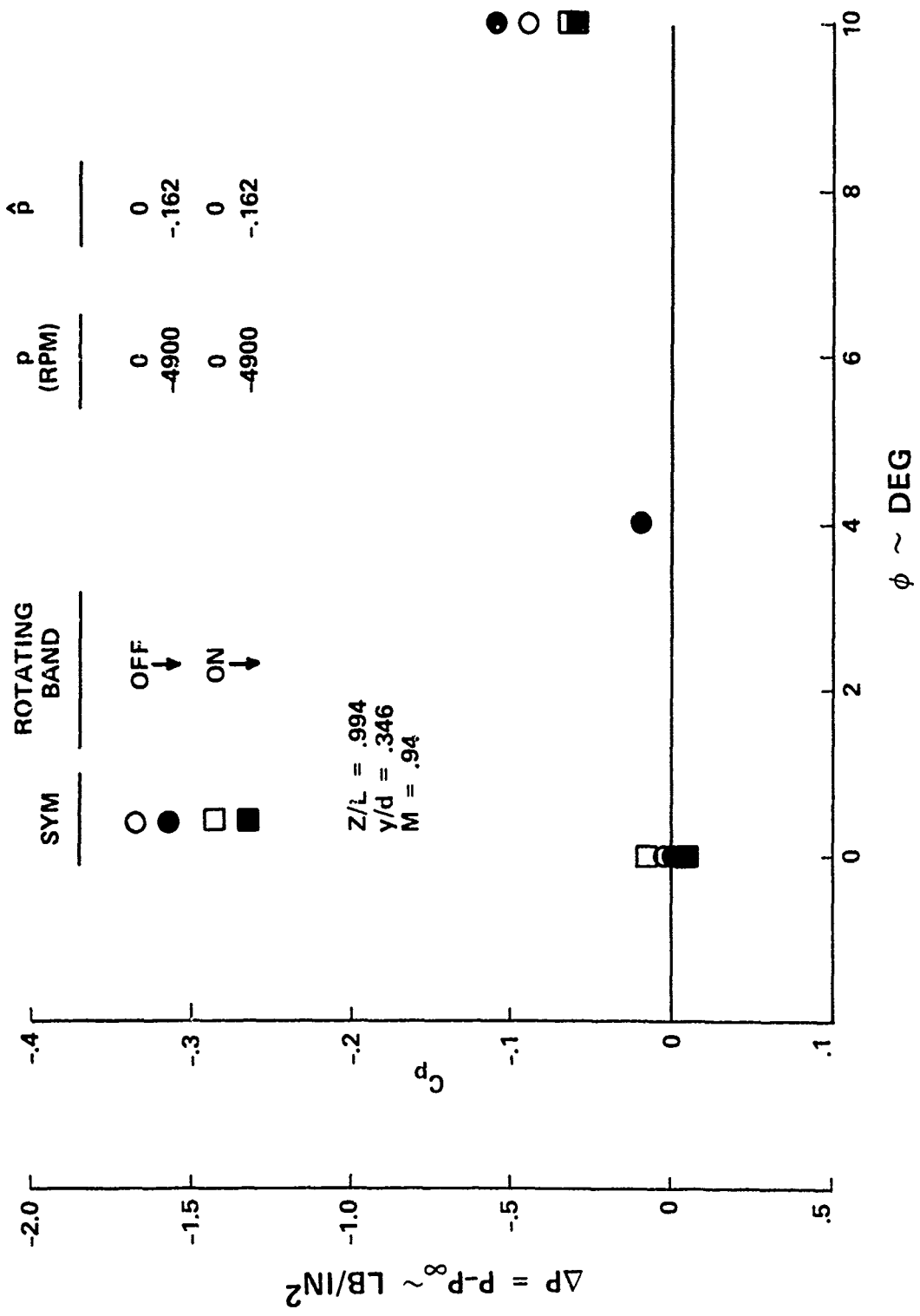


Figure 38. Effect of Angle of Attack and Spin on Model 1 Base Pressure

Table 9. Comparison of Normal Force and Moment Data on Non-Spinning Model from Surface Pressure Test Data ( $\alpha = 4$  Degrees)

TERM	PRESSURE MODEL	
	NASA-AMIES 14-FT TRANSONIC .5 CAL BOATTAIL	NASA-LANGLEY 16-FT TRANSONIC 1 CAL BOATTAIL
$C_{N_{\alpha}}$ (OGIVE)	1.94	2.05
$C_{N_{\alpha}}$ (CYLINDER)	.25	.17
$C_{N_{\alpha}}$ (BOATTAIL)	-.64	-.60
$C_{N_{\alpha}}$ (TOTAL)	1.55	1.62
$C_{m_{\alpha}}$ (OGIVE)	3.45	3.57
$C_{m_{\alpha}}$ (CYLINDER)	-.50	-.14
$C_{m_{\alpha}}$ (BOATTAIL)	1.22	1.07
$C_{m_{\alpha}}$ (TOTAL)	4.17	4.50
$Z_{cp}/L$	.145	.130

MODEL CONFIGURATION: 8 INCH DIAMETER MODEL  
 3 CALIBER OGIVE  
 2 CALIBER CYLINDER  
 ROTATING BAND OFF  
 (SEE NOTE FOR BOATTAIL)  
 REF c.g. AT Z/L = .625

TEST CONDITION: MACH .94  
 $\alpha = 4^{\circ}$   
 $R_d = 4 \times 10^6 / \text{FT}$   
 $p = 0$  RPM

Table 10. Comparison of Normal Force and Moment Data on Non-Spinning Model from Surface Pressure Test Data ( $\alpha = 10$  Degrees)

MODEL CONFIGURATION:	8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER (SEE NOTE FOR BOATTAIL) ROTATING BAND OFF REF c.g. AT Z/L = .625	TERM	PRESSURE MODEL NASA-AMES 14-FT TRANSONIC .5 CAL BOATTAIL	PRESSURE MODEL NASA-LANGLEY 16-FT TRANSONIC 1 CAL BOATTAIL
TEST CONDITION:	MACH .94 $\alpha = 10^\circ$ $R_d = 4 \times 10^6 / \text{FT}$ $p = 0$ RPM	$C_{N_{\alpha}}$ (OGIVE)	1.93	2.02
		$C_{N_{\alpha}}$ (CYLINDER)	.33	.21
		$C_{N_{\alpha}}$ (BOATTAIL)	-.36	-.67
		$C_{N_{\alpha}}$ (TOTAL)	1.90	1.56
		$C_{m_{\alpha}}$ (OGIVE)	3.46	3.55
		$C_{m_{\alpha}}$ (CYLINDER)	-.35	-.20
		$C_{m_{\alpha}}$ (BOATTAIL)	.70	1.14
		$C_{m_{\alpha}}$ (TOTAL)	3.82	4.50
		$Z_{cp}/L$	.27	.11

An internal balance was employed to directly measure the force and moment acting on a spinning projectile model.<sup>2</sup> Using this method, only the total force and moment coefficients could be determined. These directly measured terms are compared in Tables 11 and 12 with the same terms obtained by integrating the results of the surface pressure tests. The comparison is excellent, especially for the 10 degree angle-of-attack case where the model configurations both include rotating bands and are most similar.

One of the primary objectives of this test was to obtain experimental data that could be used to evaluate and evolve the Computational Fluid Dynamic (CFD) codes being developed to predict the flow field and resulting aerodynamic effects on spinning projectiles. A CFD code currently under development was used to calculate the aerodynamic terms for a projectile configuration and flight condition identical to that used in the wind tunnel test. The code is based on the solution to the thin-layer Navier-Stokes equations, as described by Nietubicz et al.,<sup>8</sup> and was run on a CRAY I computer. Table 13 compares the normal force term from the code with that from the surface pressure wind tunnel test and illustrates the excellent agreement achieved. The Magnus terms are compared in Table 14. In this case, the code under predicts the Magnus force by a significant amount.

## 6. CONCLUSIONS

- The sliding seal technique is capable of accurately measuring the Magnus-induced surface pressures on a spinning projectile wind tunnel model at transonic Mach numbers.
- Check runs showed excellent repeatability and demonstrated the absence of model or instrumentation asymmetries.
- Surface pressure data obtained in this test showed good agreement with the surface pressure data obtained on an identical, non-spinning model at the NASA-Langley 8-Foot Transonic Wind Tunnel.
- Total coefficients for Magnus force and moment computed by integrating the measured surface pressure data showed good agreement with directly measured force and moment data obtained from other spinning models.
- The data indicated the quantitative influence of spin and angle of attack and reveal that, for a given condition, different portions of the projectile can experience both positive and negative local Magnus forces.
- Quantitative pressure data were obtained to indicate the relative contribution of the various projectile elements (i.e., ogive, cylinder, boattail, rotating band) to the Magnus effect.
- A significant negative pressure region was detected on the advancing side of the leeward location at all longitudinal stations for a 10-degree angle of attack. This phenomenon was not noted at a 4-degree angle of attack.
- Base pressures at the test Mach number were found to be near free-stream static values.

Figure 11. Comparison of Side Force and Moment Data on Spinning From Surface Pressure and Direct Force Tests for  $\alpha = 4$  Degrees

MODEL CONFIGURATION:	TERM	INTEGRATION OF SURFACE PRESSURE DATA	DIRECT FORCE AND MOMENT DATA, REF: BRLMR22B4
3 CALIBER OGIVE	$C_{Y_p}$ (OGIVE)	-004	-
2 CALIBER CYLINDER	$C_{Y_p}$ (CYLINDER)	-.149	-
.5 CALIBER BOATTAIL	$C_{Y_p}$ (BOATTAIL)	-.026	-
ROTATING BAND ON	$C_{Y_p}$ (TOTAL)	-.179	-.175
$Z_{cg}/L = .625$			
TEST CONDITIONS:	$C_{n_n}$ (OGIVE)	-.003	-
MACH .94	$C_{n_p}$ (CYLINDER)	.139	-
$\alpha = 10^\circ$	$C_{n_p}$ (BOATTAIL)	.043	-
$\rho V^2/L = .162$	$C_{n_p}$ (TOTAL)	.180	.180
	$Z_{cp}/L$ (MAGNUS)	.804	.808

Table 12. Comparison of Side Force and Moment Data on Spinning Model from Surface Pressure and Direct Force Tests for  $\alpha = 10$  Degrees

MODEL CONFIGURATION:	TERM	* INTEGRATION OF SURFACE PRESSURE DATA	** DIRECT FORCE AND MOMENT DATA, REF: BRLMR22B4
3 CALIBER OGIVE	$C_{Y_p}$ (OGIVE)	.000	-
2 CALIBER CYLINDER	$C_{Y_p}$ (CYLINDER)	-.085	-
.5 CALIBER BOATTAIL	$C_{Y_p}$ (BOATTAIL)	-.019	-
** ROTATING BAND OFF	$C_{Y_p}$ (TOTAL)	-.104	-.090
** ROTATING BAND ON			
$Z_{cg}/L = .625$			
MACH .94	$C_{n_p}$ (OGIVE)	.000	-
$\alpha = 10^\circ$	$C_{n_p}$ (CYLINDER)	.056	-
$pd/2V = .162$	$C_{n_p}$ (BOATTAIL)	.033	-
	$C_{n_p}$ (TOTAL)	.090	.085
	$Z_{cp}/L$ (MAGNUS)	.779	.793

Table 13. Comparison of Normal Force and Moment Terms From Surface Pressure Test Data and Computational Fluid Dynamic Code

MODEL CONFIGURATION:	TERM	INTEGRATION OF SURFACE PRESSURE WIND TUNNEL TEST DATA	COMPUTATIONAL FLUID DYNAMIC CODE
8 INCH DIAMETER MODEL	$C_{N_{\alpha}}$ (OGIVE)	1.96	
3 CALIBER OGIVE	$C_{N_{\alpha}}$ (CYLINDER)	.30	
2 CALIBER CYLINDER	$C_{N_{\alpha}}$ (BOATTAIL)	-.68	
.5 CALIBER BOATTAIL	$C_{N_{\alpha}}$ (TOTAL)	1.59	1.58
ROTATING BAND OFF			
REF c.g. AT Z/L = .625			
TEST CONDITIONS:			
MACH .94	$C_{m_{\alpha}}$ (OGIVE)	3.47	
$\alpha = 4^{\circ}$	$C_{m_{\alpha}}$ (CYLINDER)	-.36	
$R_d = 4 \times 10^6 / \text{FT}$	$C_{m_{\alpha}}$ (BOATTAIL)	1.30	
$\rho d^2 / 2V = .162$	$C_{m_{\alpha}}$ (TOTAL)	4.41	
	$Z_{cp}/L$	.13	

Table 14. Comparison of Side Force and Moment Terms from Surface Pressure Test Data and Computational Fluid Dynamic Code

MODEL CONFIGURATION:	TERM:	INTEGRATION OF SURFACE PRESSURE WIND TUNNEL TEST DATA	COMPUTATIONAL FLUID DYNAMIC CODE
8 INCH DIAMETER MODEL	$C_{Y_p}$ (OGIVE)	.000	
3 CALIBER OGIVE	$C_{Y_p}$ (CYLINDER)	-.085	
2 CALIBER CYLINDER	$C_{Y_p}$ (BOATTAIL)	-.019	
.5 CALIBER BOATTAIL	$C_{Y_p}$ (TOTAL)	-.104	-.015
ROTATING BAND OFF			
$Z_{cg}/L = .625$			
MACH .94			
$\alpha = 4^\circ$			
$R_d = 4 \times 10^6 / FT$			
$pd/2V = .162$			
	$C_{n_p}$ (OGIVE)	.000	
	$C_{n_p}$ (CYLINDER)	.056	
	$C_{n_p}$ (BOATTAIL)	.033	
	$C_{n_p}$ (TOTAL)	.090	
	$Z_{cp}/L$ (MAGNUS)	.78	



- The presence of the rotating band influenced the Magnus effects both upstream and downstream of the band, but in a compensating manner resulting in very little difference in the total Magnus effect between the band-off and band-on cases.
- Model components and instrumentation functioned well; however, pressure settling times of about 60 seconds were experienced. Future tests should employ shorter lengths of pressure tubing to decrease the data acquisition time.

## LITERATURE CITED

1. Oskay, V., and Mermagen, W. H. ARBRL-MR-2545. Transonic Flight Dynamics of Long Shell. Ballistics Research Laboratory. October 1975. UNCLASSIFIED Report.
2. Platau, A. S., and Nielson, G. T. I. ARBRL-MR-2284. Some Aerodynamic Characteristics of the Artillery Projectile XM549. Ballistics Research Laboratory. April 1973. UNCLASSIFIED Report.
3. Whyte, R. H., Burnett, J. R., Hathaway, W. H., and Brown, E. F. ARCLD-CR-80023. Analysis of Free Flight Aerodynamic Range Data of the 155mm M549 Projectile. Large Caliber Weapons Systems Laboratory, October 1980. UNCLASSIFIED Report.
4. Sturek, W. B. et al. Computations of Magnus Effects for a Yawed, Spinning Body of Revolution. Am. Instit. Aeronaut. Astronaut. J. 16 (No. 7), 687-692 (July 1978).
5. Shiff, L. B., and Sturek, W. B. Numerical Simulation of Steady Supersonic Flow Over an Ogive-Cylinder-Boattail Body. Am. Instit. Aeronaut. Astronaut. J. Paper 80-0066, January 1980.
6. Nietubicz, C. J., Inger, G. R., and Danberg, J. E. A Theoretical and Experimental Investigation of a Transonic Projectile Flow Field. Am. Instit. Aeronaut. Astronaut. J. Paper 82-0101. January 1982.
7. Kayser, L. D., and Whiton, F. ARBRL-MR-03161. Surface Pressure Measurements on a Boattail Projectile Shape at Transonic Speeds. Ballistics Research Laboratory. March 1982. UNCLASSIFIED Report.
8. Nietubicz, C. J., Sturek W. B., and Heavey, K. R. ARBRL-TR-02515. Computation of Projectile Magnus Effects at Transonic Velocities. Ballistics Research Laboratory. August 1983. UNCLASSIFIED Report.
9. Danberg, J. E., Heavey, K. R., and Miller, M. C. ARBRL-MR-3447. Computational Simulation of Transonic Flow Over Projectile Rotating Band and Comparison With Experiment. Ballistics Research Laboratory. May 1985. UNCLASSIFIED Report.
10. Miller, M. C. Surface Pressure Measurements on a Spinning Wind Tunnel Model. Am. Instit. Aeronaut. Astronaut. J. 14, 1669 (December 1976).
11. Kayser, L. D., Sturek, W. B., and Yanta, W. J. Measurements in the Turbulent Boundary Layer of a Yawed, Spinning Body of Revolution at Mach 3.0 With a Laser Velocimeter and Impact Probe. Am. Instit. Aeronaut. Astronaut. J. Paper 78-824. July 1974.
12. D'Amico, W. P. ARBRL-TM-03017. Demonstration of a Technique for the Measurement of Surface Pressures on Spinning Wind Tunnel Models via Telemetry. Ballistics Research Laboratory. April 1980. UNCLASSIFIED Report.

13. Miller, M. C. ED-TR-76070. A Technique to Measure the Pressure Distribution Acting on the Surface of a Spinning Body in a Wind Tunnel. Edgewood Arsenal. September 1976. UNCLASSIFIED Report.

14. Miller, M. C. Wind Tunnel Measurements of the Surface Pressure Distribution on a Spinning Magnus Rotor. Am. Instit. Aeronaut. Astronaut. J. of Aircraft 16 (No. 12), 815 (December 1979).

15. Miller, M. C. ARCSL-TR-77018. A Magnetic Fluid Seal for Measurement of Aerodynamic Surface Pressures. Chemical Systems Laboratory Report. April 1977. UNCLASSIFIED Report.

16. Miller, M. C. ARCSL-SP-83001. Vol II, pp 25-60. Wind Tunnel Measurements of the Magnus Induced Surface Pressures on a Spinning Artillery Projectile Model. Proceedings of the ARRADCOM Aeroballistics and Fluid Dynamics Technology Conference, 28-30 September 1982. June 1983. UNCLASSIFIED Report.

17. Miller, M. C. Surface Pressure Measurements on a Transonic Spinning Projectile. Am. Instit. Aeronaut. Astronaut. J. of Spacecraft and Rockets 22 (No. 2), 112-118 (March-April 1985).

18. Miller, M. C. Experimental Measurements of the Aerodynamics Surface Pressures on Spinning Bodies. Proceedings of the International Congress of Instrumentation in Aerospace Simulation Facilities, pp 117-130, September 1983.

## GLOSSARY

$C_N$	normal force coefficient $N/qS$
$C_{N_i}$	local normal force coefficient,  $\frac{360/\Delta\phi}{\sum_{j=1}^2 C_{p_j}} \frac{d_i \Delta z_i \sin\Delta\phi \cos\phi_j}{\pi d^2}$
$C_{N_\alpha}$	$\partial C_N / \partial \alpha$
$C_m$	pitching moment coefficient, $PM/qsd$
$C_{m_\alpha}$	$\partial C_m / \partial \alpha$
$C_n$	yawing moment coefficient, $YM/qsd$
$C_{n_p}$	$\partial C_n / \partial \hat{p}$
$C_p$	pressure coefficient, $(P - P_\infty)/q$
$C_y$	side force coefficient
$C_{y_i}$	local side force coefficient,  $\frac{360/\Delta\phi}{\sum_{j=1}^2 C_{p_j}} \frac{d_i \Delta z_i \sin\Delta\phi \sin\phi_j}{\pi d^2}$
$C_{y_p}$	$\partial C_y / \partial \hat{p}$
$d$	model reference diameter (7.95 inches)
$i$	subscript denotes value at location $Z_i$
$j$	subscript denotes value at location $\phi_j$
$L$	projectile length (44.616 inches)
$M$	Mach number
$N$	normal force

P	surface pressure
$P_\infty$	free stream static pressure
PM	pitching moment
p	spin rate
$\hat{p}$	tip speed ratio, $pd/2V$
q	dynamic pressure, $\rho v^2/2$
$R_d$	Reynolds number, $v/\nu$
S	reference area, $\pi d^2/4$
SF	side force
SIGMA N	angle between the projectile center line and the sun direction
$T_\infty$	free stream temperature
t	time
V	total free stream velocity
x, y, z	body axes
YM	yawing moment
Z	distance along model measured from nose
$Z_{cg}$	longitudinal location of reference center of gravity from nose
$Z_{cp}/L$	normal force center-of-pressure location from nose, $.625 - .1782(C_{m_\alpha}/C_{N_\alpha})$
$Z_{cp}/L$ (Magnus)	Magnus force center-of-pressure location from nose, $.625 + .1782(C_{n_p}/C_{Y_p})$
$\alpha$	angle of attack
$\Delta P$	$P - P_\infty$
$\Delta\phi$	increment between circumferential locations
$\nu$	air kinematic viscosity
$\pi$	ratio of circle circumference to diameter

$\rho$  air density  
 $\phi_j$  circumferential location  
 $\theta$  angle of projectile surface to projectile centerline

## APPENDIX A

### TABULATED WIND TUNNEL TEST DATA

This appendix presents the measured pressure data in tabulated format. Each set of data relates to a specific model configuration and test condition: rotating band on or rotating band off, angle of attack of 0, 4, or 10 degrees, and spinning or non-spinning. The resulting pressure coefficients are presented as a function of azimuthal location ( $\phi$ ) for each longitudinal tap location (Z/L).

Data for the ogive area obtained during the Langley non-spinning test are also included to provide the total pressure distribution. The appendix figures contain the following data:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)	Run no.
A1	OFF	0	0	7-11, 12-25
A2	OFF	0	4900	73-92
A3	OFF	4	0	30-49
A4	OFF	4	4900	98-112
A5	OFF	10	0	113-122, 127-135
A6	OFF	10	4900	50-69
A7	ON	0	0	144-154
A8	ON	0	4900	181-192
A9	ON	10	0	157-168
A10	ON	10	4900	169-180

Appendix A

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07  
 TAP LOCATION (Z/D): 0.393

0.16 0.20 0.4 0.5  
 0.896 1.571 2.245 2.866

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.114	0.027	-0.044	-0.145	0.000
22.5	0.000	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000	0.000
67.5	0.000	0.000	0.000	0.000	0.000
90.0	0.123	0.000	-0.037	0.000	0.000
112.5	0.000	0.000	0.000	-0.100	0.000
135.0	0.000	0.000	0.000	0.000	0.000
157.5	0.000	0.000	0.000	0.000	0.000
180.0	0.132	0.000	0.000	0.000	0.000
202.5	0.000	0.000	-0.039	-0.101	0.000
225.0	0.000	0.000	0.000	0.000	0.000
247.5	0.000	0.000	0.000	0.000	0.000
270.0	0.123	0.000	0.000	0.000	0.000
292.5	0.000	0.000	-0.040	-0.100	0.000
315.0	0.000	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 4.95 IN.  
 ROTATING SHARD: 0  
 X/RATIO: 0.94  
 ANGLE OF ATTACK (ALPHA): 0 DEG.  
 SPIN RATE (P): 0 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0  
 X CG/L: 0.625112067

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.583  
 TAP LOCATION (Z/D): 2.824

0.526 0.537 0.548 0.571  
 2.95 3.014 3.077 3.283

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
10.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
20.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
30.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
40.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
50.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
60.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
70.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
80.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
90.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
100.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
120.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
140.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
150.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
170.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
180.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
190.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
200.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
210.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
220.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
230.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
240.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
250.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
260.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
270.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
280.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
290.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
300.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
320.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
330.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
340.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006
350.0	-0.116	-0.133	-0.352	-0.488	-0.240	-0.019	-0.006



TAP LOCATION (Z/L):	0.75	0.87	0.899	0.91	0.922
TAP LOCATION (Z/D):	4.757	4.863	5.046	5.169	5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0
0.0	-0.045	-0.067	-0.100	-0.144	-0.188
10.0	-0.045	-0.067	-0.100	-0.144	-0.188
20.0	-0.045	-0.067	-0.100	-0.144	-0.188
30.0	-0.045	-0.067	-0.100	-0.144	-0.188
40.0	-0.045	-0.067	-0.100	-0.144	-0.188
50.0	-0.045	-0.067	-0.100	-0.144	-0.188
60.0	-0.045	-0.067	-0.100	-0.144	-0.188
70.0	-0.045	-0.067	-0.100	-0.144	-0.188
80.0	-0.045	-0.067	-0.100	-0.144	-0.188
90.0	-0.045	-0.067	-0.100	-0.144	-0.188
100.0	-0.045	-0.067	-0.100	-0.144	-0.188
110.0	-0.045	-0.067	-0.100	-0.144	-0.188
120.0	-0.045	-0.067	-0.100	-0.144	-0.188
130.0	-0.045	-0.067	-0.100	-0.144	-0.188
140.0	-0.045	-0.067	-0.100	-0.144	-0.188
150.0	-0.045	-0.067	-0.100	-0.144	-0.188
160.0	-0.045	-0.067	-0.100	-0.144	-0.188
170.0	-0.045	-0.067	-0.100	-0.144	-0.188
180.0	-0.045	-0.067	-0.100	-0.144	-0.188
190.0	-0.045	-0.067	-0.100	-0.144	-0.188
200.0	-0.045	-0.067	-0.100	-0.144	-0.188
210.0	-0.045	-0.067	-0.100	-0.144	-0.188
220.0	-0.045	-0.067	-0.100	-0.144	-0.188
230.0	-0.045	-0.067	-0.100	-0.144	-0.188
240.0	-0.045	-0.067	-0.100	-0.144	-0.188
250.0	-0.045	-0.067	-0.100	-0.144	-0.188
260.0	-0.045	-0.067	-0.100	-0.144	-0.188
270.0	-0.045	-0.067	-0.100	-0.144	-0.188
280.0	-0.045	-0.067	-0.100	-0.144	-0.188
290.0	-0.045	-0.067	-0.100	-0.144	-0.188
300.0	-0.045	-0.067	-0.100	-0.144	-0.188
310.0	-0.045	-0.067	-0.100	-0.144	-0.188
320.0	-0.045	-0.067	-0.100	-0.144	-0.188
330.0	-0.045	-0.067	-0.100	-0.144	-0.188
340.0	-0.045	-0.067	-0.100	-0.144	-0.188
350.0	-0.045	-0.067	-0.100	-0.144	-0.188

Appendix A

TAP LOCATION (Z/L):	0.945	0.96	0.969	0.98	0.98
TAP LOCATION (Z/D):	5.383	5.5	5.438	5.5	5.438
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0
0.0	-0.455	-0.270	-0.142	-0.142	-0.142
10.0	-0.455	-0.270	-0.142	-0.142	-0.142
20.0	-0.455	-0.270	-0.142	-0.142	-0.142
30.0	-0.455	-0.270	-0.142	-0.142	-0.142
40.0	-0.455	-0.270	-0.142	-0.142	-0.142
50.0	-0.455	-0.270	-0.142	-0.142	-0.142
60.0	-0.455	-0.270	-0.142	-0.142	-0.142
70.0	-0.455	-0.270	-0.142	-0.142	-0.142
80.0	-0.455	-0.270	-0.142	-0.142	-0.142
90.0	-0.455	-0.270	-0.142	-0.142	-0.142
100.0	-0.455	-0.270	-0.142	-0.142	-0.142
110.0	-0.455	-0.270	-0.142	-0.142	-0.142
120.0	-0.455	-0.270	-0.142	-0.142	-0.142
130.0	-0.455	-0.270	-0.142	-0.142	-0.142
140.0	-0.455	-0.270	-0.142	-0.142	-0.142
150.0	-0.455	-0.270	-0.142	-0.142	-0.142
160.0	-0.455	-0.270	-0.142	-0.142	-0.142
170.0	-0.455	-0.270	-0.142	-0.142	-0.142
180.0	-0.455	-0.270	-0.142	-0.142	-0.142
190.0	-0.455	-0.270	-0.142	-0.142	-0.142
200.0	-0.455	-0.270	-0.142	-0.142	-0.142
210.0	-0.455	-0.270	-0.142	-0.142	-0.142
220.0	-0.455	-0.270	-0.142	-0.142	-0.142
230.0	-0.455	-0.270	-0.142	-0.142	-0.142
240.0	-0.455	-0.270	-0.142	-0.142	-0.142
250.0	-0.455	-0.270	-0.142	-0.142	-0.142
260.0	-0.455	-0.270	-0.142	-0.142	-0.142
270.0	-0.455	-0.270	-0.142	-0.142	-0.142
280.0	-0.455	-0.270	-0.142	-0.142	-0.142
290.0	-0.455	-0.270	-0.142	-0.142	-0.142
300.0	-0.455	-0.270	-0.142	-0.142	-0.142
310.0	-0.455	-0.270	-0.142	-0.142	-0.142
320.0	-0.455	-0.270	-0.142	-0.142	-0.142
330.0	-0.455	-0.270	-0.142	-0.142	-0.142
340.0	-0.455	-0.270	-0.142	-0.142	-0.142
350.0	-0.455	-0.270	-0.142	-0.142	-0.142

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: OFF  
 MACH NO.: 0.94 DEG.  
 ANGLE OF ATTACK (ALPHA): 0 REV/MIN  
 SPIN RATE (P): 0  
 TIP SPEED RATIO (PD/2V): 0.625112867  
 X CG/L

Figure A-1. (Cont'd)

Appendix A

DATA SOURCE : LANGLEY

TMP LOCATION (Z/L): 0.07  
 TMP LOCATION (Z/B): 0.333

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.114	0.027	-0.044	-0.106	-0.404	-0.404
22.5	0.000	0.000	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000	0.000	0.000
67.5	0.000	0.000	-0.037	-0.160	-0.404	-0.404
90.0	0.123	0.000	0.000	0.000	0.000	0.000
112.5	0.000	0.000	0.000	0.000	0.000	0.000
135.0	0.000	0.000	0.000	0.000	0.000	0.000
157.5	0.000	0.000	-0.039	-0.161	-0.404	-0.404
180.0	0.122	0.000	0.000	0.000	0.000	0.000
202.5	0.000	0.000	0.000	0.000	0.000	0.000
225.0	0.000	0.000	0.000	0.000	0.000	0.000
247.5	0.122	0.000	-0.037	-0.160	-0.404	-0.404
270.0	0.000	0.000	0.000	0.000	0.000	0.000
292.5	0.000	0.000	0.000	0.000	0.000	0.000
315.0	0.000	0.000	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BARRIE: OFF  
 INCL. ANGLE: 0.94 DEG.  
 WIND DIRECTION (ALPHA): 4900 REV/MIN  
 WIND SPEED (V): 0.152027427  
 TIP SPEED RATIO (TSR): 0.625112667  
 X CP-L

DATA SOURCE : RMES

TMP LOCATION (Z/L): 0.503  
 TMP LOCATION (Z/B): 2.024

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.157	-0.148	-0.361	-0.428	-0.366	-0.366
18.0	-0.157	-0.148	-0.361	-0.428	-0.366	-0.366
36.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
54.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
72.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
90.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
108.0	-0.128	-0.140	-0.360	-0.428	-0.366	-0.366
126.0	-0.128	-0.140	-0.360	-0.428	-0.366	-0.366
144.0	-0.128	-0.140	-0.360	-0.428	-0.366	-0.366
162.0	-0.129	-0.140	-0.360	-0.428	-0.366	-0.366
180.0	-0.129	-0.140	-0.360	-0.428	-0.366	-0.366
198.0	-0.129	-0.140	-0.360	-0.428	-0.366	-0.366
216.0	-0.135	-0.140	-0.364	-0.428	-0.372	-0.372
234.0	-0.135	-0.140	-0.362	-0.428	-0.371	-0.371
252.0	-0.134	-0.140	-0.362	-0.428	-0.369	-0.369
270.0	-0.132	-0.140	-0.361	-0.428	-0.368	-0.368
288.0	-0.131	-0.140	-0.361	-0.428	-0.367	-0.367
306.0	-0.128	-0.140	-0.361	-0.428	-0.367	-0.367
324.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
342.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366
360.0	-0.127	-0.140	-0.361	-0.428	-0.366	-0.366

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BARRIE: OFF  
 INCL. ANGLE: 0.94 DEG.  
 WIND DIRECTION (ALPHA): 4900 REV/MIN  
 WIND SPEED (V): 0.152027427  
 TIP SPEED RATIO (TSR): 0.625112667  
 X CP-L

Figure A-2. Rotating Band Off,  $\alpha = 0^\circ$ ,  $P = 4900$  rpm

TAP LOCATION (Z/D):	0.75	0.845	0.922	0.91	0.922
TAP LOCATION (Z/D):	4.269	4.583	5.046	5.109	5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0	20.0	30.0	40.0
PRESSURE COEFFICIENT (CP)	0.830	0.870	0.910	0.950	0.990
0.0	0.830	0.870	0.910	0.950	0.990
10.0	0.830	0.870	0.910	0.950	0.990
20.0	0.830	0.870	0.910	0.950	0.990
30.0	0.830	0.870	0.910	0.950	0.990
40.0	0.830	0.870	0.910	0.950	0.990
50.0	0.830	0.870	0.910	0.950	0.990
60.0	0.830	0.870	0.910	0.950	0.990
70.0	0.830	0.870	0.910	0.950	0.990
80.0	0.830	0.870	0.910	0.950	0.990
90.0	0.830	0.870	0.910	0.950	0.990
100.0	0.830	0.870	0.910	0.950	0.990
110.0	0.830	0.870	0.910	0.950	0.990
120.0	0.830	0.870	0.910	0.950	0.990
130.0	0.830	0.870	0.910	0.950	0.990
140.0	0.830	0.870	0.910	0.950	0.990
150.0	0.830	0.870	0.910	0.950	0.990
160.0	0.830	0.870	0.910	0.950	0.990
170.0	0.830	0.870	0.910	0.950	0.990
180.0	0.830	0.870	0.910	0.950	0.990
190.0	0.830	0.870	0.910	0.950	0.990
200.0	0.830	0.870	0.910	0.950	0.990
210.0	0.830	0.870	0.910	0.950	0.990
220.0	0.830	0.870	0.910	0.950	0.990
230.0	0.830	0.870	0.910	0.950	0.990
240.0	0.830	0.870	0.910	0.950	0.990
250.0	0.830	0.870	0.910	0.950	0.990
260.0	0.830	0.870	0.910	0.950	0.990
270.0	0.830	0.870	0.910	0.950	0.990
280.0	0.830	0.870	0.910	0.950	0.990
290.0	0.830	0.870	0.910	0.950	0.990
300.0	0.830	0.870	0.910	0.950	0.990
310.0	0.830	0.870	0.910	0.950	0.990
320.0	0.830	0.870	0.910	0.950	0.990
330.0	0.830	0.870	0.910	0.950	0.990
340.0	0.830	0.870	0.910	0.950	0.990
350.0	0.830	0.870	0.910	0.950	0.990

TAP LOCATION (Z/D):	0.969	0.98
TAP LOCATION (Z/D):	5.438	5.5
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0
PRESSURE COEFFICIENT (CP)	0.969	0.98
0.0	0.969	0.98
10.0	0.969	0.98
20.0	0.969	0.98
30.0	0.969	0.98
40.0	0.969	0.98
50.0	0.969	0.98
60.0	0.969	0.98
70.0	0.969	0.98
80.0	0.969	0.98
90.0	0.969	0.98
100.0	0.969	0.98
110.0	0.969	0.98
120.0	0.969	0.98
130.0	0.969	0.98
140.0	0.969	0.98
150.0	0.969	0.98
160.0	0.969	0.98
170.0	0.969	0.98
180.0	0.969	0.98
190.0	0.969	0.98
200.0	0.969	0.98
210.0	0.969	0.98
220.0	0.969	0.98
230.0	0.969	0.98
240.0	0.969	0.98
250.0	0.969	0.98
260.0	0.969	0.98
270.0	0.969	0.98
280.0	0.969	0.98
290.0	0.969	0.98
300.0	0.969	0.98
310.0	0.969	0.98
320.0	0.969	0.98
330.0	0.969	0.98
340.0	0.969	0.98
350.0	0.969	0.98

DPE LENGTH (L): 44.616 IN.  
 DPE DIRECTION (D): 7.95 IN.  
 SPINNING END: OFF  
 MACH NO.: 0.94  
 ANGLE OF ATTACK (ALPHA): 4900 DEG/REV/MIN  
 SPIN RATE (P): 0.62827427  
 TIP SPEED RATIO (PB/2V): 0.625112067  
 X CG/L

Figure A-2. (Cont'd)

Appendix A

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07  
TAP LOCATION (Z/D): 0.393

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.11	0.079	0.091	0.088	0.088
22.5	0.128	0.075	-0.002	-0.002	-0.002
45.0	0.129	0.060	-0.016	-0.016	-0.016
67.5	0.117	0.042	-0.033	-0.033	-0.033
90.0	0.110	0.021	-0.051	-0.051	-0.051
112.5	0.093	0.006	-0.064	-0.064	-0.064
135.0	0.073	-0.004	-0.071	-0.071	-0.071
157.5	0.051	-0.009	-0.074	-0.074	-0.074
180.0	0.027	-0.026	-0.074	-0.074	-0.074
202.5	0.003	-0.049	-0.074	-0.074	-0.074
225.0	0.023	-0.084	-0.071	-0.071	-0.071
247.5	0.052	-0.106	-0.064	-0.064	-0.064
270.0	0.110	0.021	-0.033	-0.033	-0.033
292.5	0.132	0.042	-0.016	-0.016	-0.016
315.0	0.152	0.060	-0.002	-0.002	-0.002
337.5	0.163	0.075			

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.503  
TAP LOCATION (Z/D): 2.824

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.079	0.088	0.080	0.080	0.080
10.0	0.090	-0.002	-0.002	-0.002	-0.002
20.0	0.090	-0.009	-0.008	-0.008	-0.008
30.0	0.103	-0.102	-0.312	-0.312	-0.312
40.0	0.108	-0.108	-0.318	-0.318	-0.318
50.0	0.118	-0.117	-0.324	-0.324	-0.324
60.0	0.125	-0.120	-0.331	-0.331	-0.331
70.0	0.130	-0.125	-0.338	-0.338	-0.338
80.0	0.135	-0.130	-0.346	-0.346	-0.346
90.0	0.141	-0.144	-0.354	-0.354	-0.354
100.0	0.142	-0.149	-0.361	-0.361	-0.361
110.0	0.145	-0.153	-0.368	-0.368	-0.368
120.0	0.145	-0.156	-0.371	-0.371	-0.371
130.0	0.145	-0.160	-0.372	-0.372	-0.372
140.0	0.144	-0.162	-0.375	-0.375	-0.375
150.0	0.144	-0.164	-0.376	-0.376	-0.376
160.0	0.144	-0.165	-0.376	-0.376	-0.376
170.0	0.145	-0.164	-0.375	-0.375	-0.375
180.0	0.145	-0.164	-0.374	-0.374	-0.374
190.0	0.145	-0.163	-0.373	-0.373	-0.373
200.0	0.145	-0.162	-0.372	-0.372	-0.372
210.0	0.144	-0.160	-0.371	-0.371	-0.371
220.0	0.144	-0.158	-0.370	-0.370	-0.370
230.0	0.144	-0.156	-0.369	-0.369	-0.369
240.0	0.144	-0.154	-0.368	-0.368	-0.368
250.0	0.144	-0.152	-0.367	-0.367	-0.367
260.0	0.143	-0.150	-0.366	-0.366	-0.366
270.0	0.143	-0.148	-0.365	-0.365	-0.365
280.0	0.143	-0.146	-0.364	-0.364	-0.364
290.0	0.142	-0.144	-0.363	-0.363	-0.363
300.0	0.142	-0.142	-0.362	-0.362	-0.362
310.0	0.141	-0.141	-0.361	-0.361	-0.361
320.0	0.141	-0.140	-0.360	-0.360	-0.360
330.0	0.141	-0.139	-0.359	-0.359	-0.359
340.0	0.141	-0.138	-0.358	-0.358	-0.358
350.0	0.141	-0.137	-0.357	-0.357	-0.357
360.0	0.141	-0.136	-0.356	-0.356	-0.356

REF. LENGTH (L): 44.516 IN.  
REF. DIAMETER (D): 7.95 IN.  
ROTATING BAND: OFF  
MACH NO.: 0.94  
ANGLE OF ATTACK (ALPHA): 4 DEG.  
SPEED RATE (P): 0 REV/MIN  
TIP SPEED RATIO (PD/2V): 0  
X CCL: 0.625112667

0.5	0.4	0.28	0.5	0.5	0.5
2.806	2.245	1.571	2.806	2.806	2.806
-0.379	-0.468	0.091	-0.379	-0.379	-0.379
-0.382	-0.472	-0.002	-0.382	-0.382	-0.382
-0.382	-0.478	-0.016	-0.382	-0.382	-0.382
-0.396	-0.498	-0.033	-0.396	-0.396	-0.396
-0.426	-0.513	-0.051	-0.426	-0.426	-0.426
-0.423	-0.524	-0.064	-0.423	-0.423	-0.423
-0.419	-0.530	-0.071	-0.419	-0.419	-0.419
-0.415	-0.532	-0.074	-0.415	-0.415	-0.415
-0.423	-0.532	-0.074	-0.423	-0.423	-0.423
-0.424	-0.530	-0.071	-0.424	-0.424	-0.424
-0.420	-0.524	-0.064	-0.420	-0.420	-0.420
-0.402	-0.513	-0.051	-0.402	-0.402	-0.402
-0.392	-0.498	-0.033	-0.392	-0.392	-0.392
-0.382	-0.472	-0.016	-0.382	-0.382	-0.382

0.613	0.571	0.548	0.613	0.613	0.613
3.706	3.203	3.077	3.706	3.706	3.706
0.112	-0.340	-0.392	0.112	0.112	0.112
-0.018	-0.340	-0.393	-0.018	-0.018	-0.018
-0.019	-0.342	-0.396	-0.019	-0.019	-0.019
-0.020	-0.346	-0.399	-0.020	-0.020	-0.020
-0.021	-0.352	-0.404	-0.021	-0.021	-0.021
-0.023	-0.358	-0.409	-0.023	-0.023	-0.023
-0.025	-0.365	-0.413	-0.025	-0.025	-0.025
-0.027	-0.372	-0.417	-0.027	-0.027	-0.027
-0.029	-0.379	-0.421	-0.029	-0.029	-0.029
-0.029	-0.383	-0.423	-0.029	-0.029	-0.029
-0.029	-0.383	-0.423	-0.029	-0.029	-0.029
-0.029	-0.382	-0.422	-0.029	-0.029	-0.029
-0.028	-0.379	-0.421	-0.028	-0.028	-0.028
-0.016	-0.375	-0.417	-0.016	-0.016	-0.016
-0.014	-0.371	-0.412	-0.014	-0.014	-0.014
-0.012	-0.376	-0.407	-0.012	-0.012	-0.012
-0.012	-0.370	-0.402	-0.012	-0.012	-0.012
-0.012	-0.370	-0.400	-0.012	-0.012	-0.012
-0.013	-0.370	-0.418	-0.013	-0.013	-0.013
-0.014	-0.375	-0.413	-0.014	-0.014	-0.014
-0.017	-0.379	-0.423	-0.017	-0.017	-0.017
-0.020	-0.382	-0.424	-0.020	-0.020	-0.020
-0.022	-0.385	-0.425	-0.022	-0.022	-0.022
-0.024	-0.385	-0.426	-0.024	-0.024	-0.024
-0.026	-0.392	-0.423	-0.026	-0.026	-0.026
-0.025	-0.377	-0.421	-0.025	-0.025	-0.025
-0.024	-0.371	-0.417	-0.024	-0.024	-0.024
-0.022	-0.357	-0.411	-0.022	-0.022	-0.022
-0.019	-0.351	-0.403	-0.019	-0.019	-0.019
-0.019	-0.346	-0.399	-0.019	-0.019	-0.019
-0.017	-0.342	-0.396	-0.017	-0.017	-0.017
-0.015	-0.340	-0.393	-0.015	-0.015	-0.015

Figure A-3. Rotating Band Off,  $\alpha = 4^\circ$ ,  $P = 0$  rpm

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)	
	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE
0.0	-0.001	0.760	0.848	0.859	0.87	0.888	0.892	0.899	0.903	0.908	0.914	
10.0	-0.003	0.767	0.855	0.866	0.883	0.894	0.901	0.908	0.915	0.922	0.929	
20.0	-0.007	0.777	0.863	0.874	0.891	0.902	0.909	0.916	0.923	0.930	0.937	
30.0	-0.012	0.787	0.871	0.882	0.899	0.910	0.917	0.924	0.931	0.938	0.945	
40.0	-0.016	0.797	0.879	0.890	0.907	0.918	0.925	0.932	0.939	0.946	0.953	
50.0	-0.021	0.807	0.887	0.898	0.915	0.926	0.933	0.940	0.947	0.954	0.961	
60.0	-0.026	0.817	0.895	0.906	0.923	0.934	0.941	0.948	0.955	0.962	0.969	
70.0	-0.031	0.827	0.903	0.914	0.931	0.942	0.949	0.956	0.963	0.970	0.977	
80.0	-0.036	0.837	0.911	0.922	0.939	0.950	0.957	0.964	0.971	0.978	0.985	
90.0	-0.041	0.847	0.919	0.930	0.947	0.958	0.965	0.972	0.979	0.986	0.993	
100.0	-0.046	0.857	0.927	0.938	0.955	0.966	0.973	0.980	0.987	0.994	1.001	
110.0	-0.051	0.867	0.935	0.946	0.963	0.974	0.981	0.988	0.995	1.002	1.009	
120.0	-0.056	0.877	0.943	0.954	0.971	0.982	0.989	0.996	1.003	1.010	1.017	
130.0	-0.061	0.887	0.951	0.962	0.979	0.990	0.997	1.004	1.011	1.018	1.025	
140.0	-0.066	0.897	0.959	0.970	0.987	0.998	1.005	1.012	1.019	1.026	1.033	
150.0	-0.071	0.907	0.967	0.978	0.995	1.006	1.013	1.020	1.027	1.034	1.041	
160.0	-0.076	0.917	0.975	0.986	1.003	1.014	1.021	1.028	1.035	1.042	1.049	
170.0	-0.081	0.927	0.983	0.994	1.011	1.022	1.029	1.036	1.043	1.050	1.057	
180.0	-0.086	0.937	0.991	1.002	1.019	1.030	1.037	1.044	1.051	1.058	1.065	
190.0	-0.091	0.947	0.999	1.010	1.027	1.038	1.045	1.052	1.059	1.066	1.073	
200.0	-0.096	0.957	1.007	1.018	1.035	1.046	1.053	1.060	1.067	1.074	1.081	
210.0	-0.101	0.967	1.015	1.026	1.043	1.054	1.061	1.068	1.075	1.082	1.089	
220.0	-0.106	0.977	1.023	1.034	1.051	1.062	1.069	1.076	1.083	1.090	1.097	
230.0	-0.111	0.987	1.031	1.042	1.059	1.070	1.077	1.084	1.091	1.098	1.105	
240.0	-0.116	0.997	1.039	1.050	1.067	1.078	1.085	1.092	1.099	1.106	1.113	
250.0	-0.121	1.007	1.047	1.058	1.075	1.086	1.093	1.100	1.107	1.114	1.121	
260.0	-0.126	1.017	1.055	1.066	1.083	1.094	1.101	1.108	1.115	1.122	1.129	
270.0	-0.131	1.027	1.063	1.074	1.091	1.102	1.109	1.116	1.123	1.130	1.137	
280.0	-0.136	1.037	1.071	1.082	1.100	1.111	1.118	1.125	1.132	1.139	1.146	
290.0	-0.141	1.047	1.079	1.090	1.107	1.118	1.125	1.132	1.139	1.146	1.153	
300.0	-0.146	1.057	1.087	1.098	1.115	1.126	1.133	1.140	1.147	1.154	1.161	
310.0	-0.151	1.067	1.095	1.106	1.123	1.134	1.141	1.148	1.155	1.162	1.169	
320.0	-0.156	1.077	1.103	1.114	1.131	1.142	1.149	1.156	1.163	1.170	1.177	
330.0	-0.161	1.087	1.111	1.122	1.139	1.150	1.157	1.164	1.171	1.178	1.185	
340.0	-0.166	1.097	1.119	1.130	1.147	1.158	1.165	1.172	1.179	1.186	1.193	
350.0	-0.171	1.107	1.127	1.138	1.155	1.166	1.173	1.180	1.187	1.194	1.201	
360.0	-0.176	1.117	1.135	1.146	1.163	1.174	1.181	1.188	1.195	1.202	1.209	

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)		TAP LOCATION (2.1 IN.)	
	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE	COEFFICIENT (CP)	PRESSURE
0.0	-0.450	0.722	0.455	0.466	0.473	0.484	0.491	0.498	0.505	0.512	0.519	
10.0	-0.454	0.732	0.463	0.474	0.491	0.502	0.509	0.516	0.523	0.530	0.537	
20.0	-0.458	0.742	0.471	0.482	0.500	0.511	0.518	0.525	0.532	0.539	0.546	
30.0	-0.462	0.752	0.479	0.490	0.508	0.519	0.526	0.533	0.540	0.547	0.554	
40.0	-0.466	0.762	0.487	0.498	0.516	0.527	0.534	0.541	0.548	0.555	0.562	
50.0	-0.470	0.772	0.495	0.506	0.524	0.535	0.542	0.549	0.556	0.563	0.570	
60.0	-0.474	0.782	0.503	0.514	0.532	0.543	0.550	0.557	0.564	0.571	0.578	
70.0	-0.478	0.792	0.511	0.522	0.540	0.551	0.558	0.565	0.572	0.579	0.586	
80.0	-0.482	0.802	0.519	0.530	0.548	0.559	0.566	0.573	0.580	0.587	0.594	
90.0	-0.486	0.812	0.527	0.538	0.556	0.567	0.574	0.581	0.588	0.595	0.602	
100.0	-0.490	0.822	0.535	0.546	0.564	0.575	0.582	0.589	0.596	0.603	0.610	
110.0	-0.494	0.832	0.543	0.554	0.572	0.583	0.590	0.597	0.604	0.611	0.618	
120.0	-0.498	0.842	0.551	0.562	0.580	0.591	0.598	0.605	0.612	0.619	0.626	
130.0	-0.502	0.852	0.559	0.570	0.588	0.599	0.606	0.613	0.620	0.627	0.634	
140.0	-0.506	0.862	0.567	0.578	0.596	0.607	0.614	0.621	0.628	0.635	0.642	
150.0	-0.510	0.872	0.575	0.586	0.604	0.615	0.622	0.629	0.636	0.643	0.650	
160.0	-0.514	0.882	0.583	0.594	0.612	0.623	0.630	0.637	0.644	0.651	0.658	
170.0	-0.518	0.892	0.591	0.602	0.620	0.631	0.638	0.645	0.652	0.659	0.666	
180.0	-0.522	0.902	0.599	0.610	0.628	0.639	0.646	0.653	0.660	0.667	0.674	
190.0	-0.526	0.912	0.607	0.618	0.636	0.647	0.654	0.661	0.668	0.675	0.682	
200.0	-0.530	0.922	0.615	0.626	0.644	0.655	0.662	0.669	0.676	0.683	0.690	
210.0	-0.534	0.932	0.623	0.634	0.652	0.663	0.670	0.677	0.684	0.691	0.698	
220.0	-0.538	0.942	0.631	0.642	0.660	0.671	0.678	0.685	0.692	0.699	0.706	
230.0	-0.542	0.952	0.639	0.650	0.668	0.679	0.686	0.693	0.700	0.707	0.714	
240.0	-0.546	0.962	0.647	0.658	0.676	0.687	0.694	0.701	0.708	0.715	0.722	
250.0	-0.550	0.972	0.655	0.666	0.684	0.695	0.702	0.709	0.716	0.723	0.730	
260.0	-0.554	0.982	0.663	0.674	0.692	0.703	0.710	0.717	0.724	0.731	0.738	
270.0	-0.558	0.992	0.671	0.682	0.700	0.711	0.718	0.725	0.732	0.739	0.746	
280.0	-0.562	1.002	0.679	0.690	0.708	0.719	0.726	0.733	0.740	0.747	0.754	
290.0	-0.566	1.012	0.687	0.698	0.716	0.727	0.734	0.741	0.748	0.755	0.762	
300.0	-0.570	1.022	0.695	0.706	0.724	0.735	0.742	0.749	0.756	0.763	0.770	
310.0	-0.574	1.032	0.703	0.714	0.732	0.743	0.750	0.757	0.764	0.771	0.778	
320.0	-0.578	1.042	0.711	0.722	0.740	0.751	0.758	0.765	0.772	0.779	0.786	
330.0	-0.582	1.052	0.719	0.730	0.748	0.759	0.766	0.773	0.780	0.787	0.794	
340.0	-0.586	1.062	0.727	0.738	0.756	0.767	0.774	0.781	0.788	0.795	0.802	
350.0	-0.590	1.072	0.735	0.746	0.764	0.775	0.782	0.789	0.796	0.803	0.810	

REF. LENGTH (L) IN.  
 REF. DIAMETER (D) IN.  
 ROTATING BAND: OFF FS  
 MACH NO.: 0.34  
 ANGLE OF ATTACK: 0 DEG  
 SPIN RATE (P) 1/RPM  
 TIP SPEED RATIO (TSR) 2.7  
 K (C.G.L) 0.00511067

Figure A-3. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07  
TAP LOCATION (Z/D): 0.393

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)
0.0	0.168
22.5	0.168
45.0	0.069
67.5	0.132
90.0	0.110
112.5	0.092
135.0	0.079
157.5	0.073
180.0	0.071
202.5	0.073
225.0	0.079
247.5	0.092
270.0	0.110
292.5	0.132
315.0	0.168
337.5	0.168

PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.079	0.001	0.002	0.001
0.075	-0.002	-0.002	-0.002
0.069	-0.016	-0.008	-0.008
0.042	-0.033	-0.013	-0.013
0.021	-0.051	-0.024	-0.024
0.006	-0.064	-0.030	-0.030
-0.004	-0.071	-0.037	-0.037
-0.009	-0.074	-0.041	-0.041
-0.010	-0.074	-0.042	-0.042
-0.009	-0.071	-0.040	-0.040
-0.004	-0.064	-0.037	-0.037
0.006	-0.051	-0.030	-0.030
0.021	-0.033	-0.024	-0.024
0.042	-0.016	-0.013	-0.013
0.069	-0.002	-0.002	-0.002
0.075	-0.001	-0.001	-0.001

REF. LENGTH (L): 4.516 IN.  
ROTATING BAND: 7.35 IN.  
REF. DIAMETER (D): 4.94 DEC.  
MACH NO.: 4900 REV/MIN  
ANGLE STE (S): 0.162927427  
TAP SPEED RATIO (PD/2V): 0.625112667  
X CG/L

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.533  
TAP LOCATION (Z/D): 2.324

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)
0.0	-0.104
10.0	-0.107
20.0	-0.119
30.0	-0.123
40.0	-0.131
50.0	-0.142
60.0	-0.149
70.0	-0.156
80.0	-0.164
90.0	-0.168
100.0	-0.165
120.0	-0.162
130.0	-0.162
140.0	-0.162
150.0	-0.162
160.0	-0.163
170.0	-0.161
180.0	-0.161
190.0	-0.159
200.0	-0.158
210.0	-0.155
220.0	-0.156
230.0	-0.164
240.0	-0.160
250.0	-0.156
260.0	-0.153
270.0	-0.146
280.0	-0.138
290.0	-0.133
300.0	-0.127
310.0	-0.123
320.0	-0.114
330.0	-0.104
350.0	-0.106

PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
-0.098	0.536	0.537	0.548	0.615
-0.100	2.75	3.014	3.077	3.786
-0.107	-0.098	-0.086	-0.089	-0.087
-0.119	-0.101	-0.092	-0.092	-0.081
-0.123	-0.104	-0.096	-0.096	-0.084
-0.131	-0.111	-0.098	-0.098	-0.084
-0.142	-0.118	-0.102	-0.102	-0.082
-0.149	-0.124	-0.105	-0.105	-0.082
-0.156	-0.135	-0.108	-0.108	-0.080
-0.164	-0.143	-0.111	-0.111	-0.079
-0.168	-0.150	-0.112	-0.112	-0.078
-0.165	-0.157	-0.113	-0.113	-0.078
-0.162	-0.162	-0.114	-0.114	-0.077
-0.162	-0.162	-0.114	-0.114	-0.077
-0.162	-0.162	-0.114	-0.114	-0.077
-0.163	-0.163	-0.113	-0.113	-0.077
-0.161	-0.161	-0.111	-0.111	-0.077
-0.161	-0.161	-0.109	-0.109	-0.077
-0.159	-0.159	-0.107	-0.107	-0.077
-0.158	-0.158	-0.106	-0.106	-0.077
-0.155	-0.155	-0.104	-0.104	-0.077
-0.156	-0.156	-0.103	-0.103	-0.077
-0.164	-0.164	-0.102	-0.102	-0.077
-0.160	-0.160	-0.101	-0.101	-0.077
-0.156	-0.156	-0.100	-0.100	-0.077
-0.153	-0.153	-0.099	-0.099	-0.077
-0.146	-0.146	-0.098	-0.098	-0.077
-0.138	-0.138	-0.097	-0.097	-0.077
-0.133	-0.133	-0.096	-0.096	-0.077
-0.127	-0.127	-0.095	-0.095	-0.077
-0.123	-0.123	-0.094	-0.094	-0.077
-0.114	-0.114	-0.093	-0.093	-0.077
-0.104	-0.104	-0.092	-0.092	-0.077
-0.106	-0.106	-0.091	-0.091	-0.077

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L): 0.75	TAP LOCATION (Z/D): 4.757	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.75	4.757	0.948	0.859	0.888	0.87	0.859
10.0	4.757	4.82	0.946	0.854	0.883	0.862	0.859
20.0	0.832	0.834	-0.046	-0.034	-0.083	-0.083	0.859
30.0	-0.012	-0.038	-0.038	-0.038	-0.084	-0.084	0.859
40.0	-0.031	-0.035	-0.013	-0.035	-0.084	-0.084	0.859
50.0	-0.034	-0.032	-0.032	-0.032	-0.090	-0.090	0.859
60.0	-0.039	-0.027	-0.027	-0.027	-0.094	-0.094	0.859
70.0	-0.045	-0.027	-0.027	-0.027	-0.102	-0.102	0.859
80.0	-0.029	-0.052	-0.052	-0.052	-0.108	-0.108	0.859
90.0	-0.031	-0.034	-0.034	-0.034	-0.114	-0.114	0.859
100.0	-0.032	-0.082	-0.082	-0.082	-0.120	-0.120	0.859
110.0	-0.044	-0.036	-0.036	-0.036	-0.125	-0.125	0.859
120.0	-0.042	-0.040	-0.040	-0.040	-0.127	-0.127	0.859
130.0	-0.039	-0.082	-0.082	-0.082	-0.131	-0.131	0.859
140.0	-0.028	-0.033	-0.033	-0.033	-0.134	-0.134	0.859
150.0	-0.025	-0.028	-0.028	-0.028	-0.138	-0.138	0.859
160.0	-0.022	-0.029	-0.029	-0.029	-0.138	-0.138	0.859
170.0	-0.020	-0.049	-0.049	-0.049	-0.137	-0.137	0.859
180.0	-0.019	-0.055	-0.055	-0.055	-0.135	-0.135	0.859
190.0	-0.019	-0.046	-0.046	-0.046	-0.135	-0.135	0.859
200.0	-0.015	-0.048	-0.048	-0.048	-0.135	-0.135	0.859
210.0	-0.016	-0.053	-0.053	-0.053	-0.134	-0.134	0.859
220.0	-0.010	-0.053	-0.053	-0.053	-0.135	-0.135	0.859
230.0	-0.024	-0.031	-0.031	-0.031	-0.135	-0.135	0.859
240.0	-0.024	-0.030	-0.030	-0.030	-0.129	-0.129	0.859
250.0	-0.031	-0.052	-0.052	-0.052	-0.124	-0.124	0.859
260.0	-0.031	-0.054	-0.054	-0.054	-0.123	-0.123	0.859
270.0	-0.027	-0.049	-0.049	-0.049	-0.118	-0.118	0.859
280.0	-0.027	-0.045	-0.045	-0.045	-0.111	-0.111	0.859
290.0	-0.025	-0.046	-0.046	-0.046	-0.106	-0.106	0.859
300.0	-0.021	-0.042	-0.042	-0.042	-0.097	-0.097	0.859
310.0	-0.021	-0.032	-0.032	-0.032	-0.092	-0.092	0.859
320.0	-0.017	-0.040	-0.040	-0.040	-0.088	-0.088	0.859
330.0	-0.015	-0.034	-0.034	-0.034	-0.085	-0.085	0.859
340.0	-0.012	-0.050	-0.050	-0.050	-0.085	-0.085	0.859
350.0	-0.013	-0.050	-0.050	-0.050	-0.085	-0.085	0.859

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L): 0.91	TAP LOCATION (Z/D): 5.176	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.91	5.176	0.945	0.969	0.98	0.98	0.969
10.0	5.176	5.438	0.945	0.969	0.98	0.98	0.969
20.0	-0.439	-0.398	-0.455	-0.398	-0.480	-0.326	0.969
30.0	-0.435	-0.453	-0.453	-0.398	-0.326	-0.326	0.969
40.0	-0.441	-0.454	-0.454	-0.394	-0.316	-0.316	0.969
50.0	-0.445	-0.452	-0.452	-0.394	-0.280	-0.280	0.969
60.0	-0.452	-0.456	-0.456	-0.379	-0.258	-0.258	0.969
70.0	-0.473	-0.456	-0.466	-0.351	-0.231	-0.231	0.969
80.0	-0.484	-0.529	-0.468	-0.300	-0.206	-0.206	0.969
90.0	-0.494	-0.530	-0.469	-0.272	-0.178	-0.178	0.969
100.0	-0.302	-0.529	-0.465	-0.247	-0.164	-0.164	0.969
110.0	-0.312	-0.528	-0.455	-0.226	-0.150	-0.150	0.969
120.0	-0.321	-0.520	-0.442	-0.213	-0.146	-0.146	0.969
130.0	-0.325	-0.512	-0.430	-0.200	-0.138	-0.138	0.969
140.0	-0.328	-0.505	-0.418	-0.191	-0.123	-0.123	0.969
150.0	-0.329	-0.503	-0.405	-0.180	-0.109	-0.109	0.969
160.0	-0.327	-0.499	-0.394	-0.178	-0.101	-0.101	0.969
170.0	-0.326	-0.497	-0.392	-0.174	-0.102	-0.102	0.969
180.0	-0.324	-0.494	-0.395	-0.174	-0.102	-0.102	0.969
190.0	-0.324	-0.484	-0.395	-0.174	-0.102	-0.102	0.969
200.0	-0.319	-0.472	-0.419	-0.183	-0.107	-0.107	0.969
210.0	-0.312	-0.472	-0.419	-0.183	-0.107	-0.107	0.969
220.0	-0.311	-0.475	-0.454	-0.210	-0.123	-0.123	0.969
230.0	-0.304	-0.478	-0.464	-0.222	-0.133	-0.133	0.969
240.0	-0.301	-0.478	-0.466	-0.222	-0.142	-0.142	0.969
250.0	-0.301	-0.477	-0.472	-0.226	-0.155	-0.155	0.969
260.0	-0.299	-0.477	-0.472	-0.226	-0.174	-0.174	0.969
270.0	-0.299	-0.472	-0.472	-0.226	-0.200	-0.200	0.969
280.0	-0.299	-0.472	-0.471	-0.226	-0.231	-0.231	0.969
290.0	-0.299	-0.472	-0.471	-0.226	-0.256	-0.256	0.969
300.0	-0.299	-0.472	-0.466	-0.226	-0.272	-0.272	0.969
310.0	-0.299	-0.472	-0.460	-0.226	-0.288	-0.288	0.969
320.0	-0.299	-0.472	-0.457	-0.226	-0.306	-0.306	0.969
330.0	-0.299	-0.472	-0.457	-0.226	-0.321	-0.321	0.969
340.0	-0.299	-0.472	-0.454	-0.226	-0.336	-0.336	0.969
350.0	-0.299	-0.472	-0.454	-0.226	-0.350	-0.350	0.969

REF. LENGTH (L): 44.516 IN.  
 ROTATING BAND: 7.95 IN.  
 MACH NO.: 0.94  
 ANGLE OF ATTACK (ALPHA): 4 DEG  
 SPIN RATE (P): 4900 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0.52027427  
 X CG/L: 0.625112067

Figure A-4. (Cont'd)

DATA SOURCE : LANGLEY

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L):	TAP LOCATION (Z/D):	0.07	0.16	0.28	0.4	0.5
			0.393	0.898	1.571	2.245	2.886
0.0	0.272	0.172	0.083	0.008	-0.322	-0.339	4-.616 IN.
22.5	0.249	0.149	0.061	0.002	-0.303	-0.339	7-.95 IN.
45.0	0.185	0.087	0.002	0.002	-0.445	-0.445	OFF
67.5	0.103	0.088	-0.071	-0.071	-0.468	-0.468	0.94 DEG.
90.0	0.035	-0.056	-0.125	-0.125	-0.471	-0.471	10 REV/MIN
112.5	-0.080	-0.084	-0.136	-0.136	-0.446	-0.446	0.625112067
135.0	-0.093	-0.091	-0.108	-0.108	-0.447	-0.447	
157.5	0.005	-0.052	-0.118	-0.118	-0.446	-0.446	
180.0	0.002	-0.072	-0.098	-0.098	-0.447	-0.447	
202.5	-0.003	-0.081	-0.108	-0.108	-0.446	-0.446	
225.0	0.000	-0.084	-0.118	-0.118	-0.445	-0.445	
247.5	0.035	-0.056	-0.125	-0.125	-0.445	-0.445	
270.0	0.103	0.088	-0.071	-0.071	-0.383	-0.383	
292.5	0.185	0.087	0.002	0.002	-0.339	-0.339	
315.0	0.249	0.149	0.061	0.061	-0.270	-0.270	
337.5	0.272	0.172	0.083	0.083	-0.200	-0.200	

REF. LENGTH (L):  
 REF. DIAMETER (D):  
 ROTATING BAND:  
 MACH NO.:  
 ANGLE OF ATTACK (ALPHA):  
 SPIN RATE (P):  
 X CG/L

DATA SOURCE : AMES

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L):	TAP LOCATION (Z/D):	0.503	0.526	0.537	0.548	0.571	0.615	0.66	0.705
			2.824	2.75	3.014	3.077	3.203	3.454	3.706	3.957
0.0	-0.010	-0.030	-0.030	-0.030	-0.250	-0.351	-0.560	-0.166	-0.024	-0.012
20.0	-0.018	-0.041	-0.041	-0.041	-0.357	-0.458	-0.668	-0.174	-0.030	-0.089
40.0	-0.030	-0.060	-0.060	-0.060	-0.458	-0.559	-0.769	-0.186	-0.040	-0.086
60.0	-0.084	-0.078	-0.078	-0.078	-0.559	-0.660	-0.870	-0.203	-0.052	-0.014
80.0	-0.117	-0.131	-0.131	-0.131	-0.660	-0.761	-0.971	-0.229	-0.068	-0.029
100.0	-0.146	-0.161	-0.161	-0.161	-0.761	-0.862	-1.072	-0.259	-0.081	-0.068
120.0	-0.170	-0.190	-0.190	-0.190	-0.862	-0.963	-1.173	-0.289	-0.099	-0.086
140.0	-0.195	-0.210	-0.210	-0.210	-0.963	-1.064	-1.274	-0.320	-0.118	-0.095
160.0	-0.216	-0.230	-0.230	-0.230	-1.064	-1.165	-1.375	-0.350	-0.138	-0.092
180.0	-0.224	-0.238	-0.238	-0.238	-1.165	-1.266	-1.476	-0.380	-0.158	-0.079
190.0	-0.225	-0.238	-0.238	-0.238	-1.266	-1.367	-1.577	-0.410	-0.178	-0.060
200.0	-0.220	-0.237	-0.237	-0.237	-1.367	-1.468	-1.678	-0.430	-0.198	-0.045
210.0	-0.213	-0.229	-0.229	-0.229	-1.468	-1.569	-1.779	-0.450	-0.218	-0.030
220.0	-0.200	-0.219	-0.219	-0.219	-1.569	-1.670	-1.880	-0.470	-0.238	-0.025
230.0	-0.211	-0.227	-0.227	-0.227	-1.670	-1.771	-1.981	-0.490	-0.258	-0.018
240.0	-0.221	-0.232	-0.232	-0.232	-1.771	-1.872	-2.082	-0.510	-0.278	-0.003
250.0	-0.225	-0.234	-0.234	-0.234	-1.872	-1.973	-2.183	-0.530	-0.298	-0.005
260.0	-0.223	-0.233	-0.233	-0.233	-1.973	-2.074	-2.284	-0.550	-0.318	-0.020
270.0	-0.214	-0.230	-0.230	-0.230	-2.074	-2.175	-2.385	-0.570	-0.338	-0.035
280.0	-0.175	-0.200	-0.200	-0.200	-2.175	-2.276	-2.486	-0.590	-0.358	-0.050
290.0	-0.110	-0.150	-0.150	-0.150	-2.276	-2.377	-2.587	-0.610	-0.378	-0.065
300.0	-0.083	-0.131	-0.131	-0.131	-2.377	-2.478	-2.688	-0.630	-0.398	-0.080
310.0	-0.083	-0.131	-0.131	-0.131	-2.478	-2.579	-2.789	-0.650	-0.418	-0.095
320.0	-0.083	-0.131	-0.131	-0.131	-2.579	-2.680	-2.890	-0.670	-0.438	-0.110
330.0	-0.083	-0.131	-0.131	-0.131	-2.680	-2.781	-2.991	-0.690	-0.458	-0.125
340.0	-0.083	-0.131	-0.131	-0.131	-2.781	-2.882	-3.092	-0.710	-0.478	-0.140
350.0	-0.030	-0.060	-0.060	-0.060	-2.882	-2.983	-3.193	-0.730	-0.498	-0.155
	-0.019	-0.041	-0.041	-0.041	-2.983	-3.084	-3.294	-0.750	-0.518	-0.170

Figure A-5. Rotating Band Off,  $\alpha = 10^\circ$ ,  $P = 0$  rpm



TAP LOCATION (Z/L):	0.75	0.848	0.859	0.87	0.888	0.899	0.91	0.922
TAP LOCATION (Z/D):	4.269	4.757	4.82	4.883	4.983	5.046	5.109	5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0
0.0	-0.010	-0.000	-0.003	-0.011	-0.023	-0.043	-0.412	-0.521
10.0	-0.009	-0.011	-0.004	-0.024	-0.045	-0.065	-0.428	-0.536
20.0	-0.008	-0.030	-0.040	-0.041	-0.085	-0.104	-0.442	-0.550
30.0	-0.019	-0.052	-0.061	-0.062	-0.105	-0.141	-0.462	-0.565
40.0	-0.036	-0.074	-0.085	-0.099	-0.130	-0.154	-0.485	-0.581
50.0	-0.052	-0.095	-0.108	-0.121	-0.154	-0.179	-0.506	-0.600
60.0	-0.052	-0.114	-0.129	-0.143	-0.174	-0.199	-0.525	-0.613
70.0	-0.109	-0.124	-0.141	-0.153	-0.184	-0.208	-0.540	-0.621
80.0	-0.107	-0.130	-0.143	-0.144	-0.178	-0.215	-0.565	-0.614
90.0	-0.101	-0.120	-0.134	-0.133	-0.172	-0.220	-0.575	-0.614
100.0	-0.091	-0.103	-0.113	-0.113	-0.172	-0.223	-0.580	-0.614
110.0	-0.075	-0.095	-0.108	-0.108	-0.171	-0.220	-0.574	-0.606
120.0	-0.055	-0.085	-0.103	-0.122	-0.168	-0.225	-0.571	-0.596
130.0	-0.042	-0.071	-0.103	-0.119	-0.154	-0.220	-0.574	-0.596
140.0	-0.030	-0.059	-0.093	-0.106	-0.154	-0.220	-0.559	-0.572
150.0	-0.020	-0.046	-0.075	-0.074	-0.139	-0.173	-0.527	-0.572
160.0	-0.012	-0.033	-0.059	-0.074	-0.124	-0.154	-0.490	-0.598
170.0	-0.008	-0.023	-0.046	-0.074	-0.109	-0.139	-0.527	-0.572
180.0	-0.012	-0.026	-0.046	-0.066	-0.106	-0.139	-0.574	-0.496
190.0	-0.020	-0.033	-0.059	-0.085	-0.122	-0.154	-0.574	-0.496
200.0	-0.030	-0.046	-0.085	-0.103	-0.139	-0.173	-0.581	-0.541
210.0	-0.042	-0.059	-0.103	-0.119	-0.154	-0.173	-0.574	-0.541
220.0	-0.052	-0.071	-0.103	-0.122	-0.154	-0.173	-0.574	-0.541
230.0	-0.052	-0.085	-0.108	-0.122	-0.154	-0.173	-0.574	-0.541
240.0	-0.061	-0.103	-0.119	-0.122	-0.154	-0.173	-0.574	-0.541
250.0	-0.061	-0.124	-0.129	-0.122	-0.154	-0.173	-0.574	-0.541
260.0	-0.111	-0.130	-0.143	-0.143	-0.173	-0.199	-0.563	-0.621
270.0	-0.104	-0.124	-0.143	-0.131	-0.173	-0.199	-0.540	-0.613
280.0	-0.096	-0.115	-0.125	-0.125	-0.173	-0.199	-0.525	-0.600
290.0	-0.074	-0.095	-0.108	-0.112	-0.154	-0.173	-0.525	-0.581
300.0	-0.054	-0.084	-0.085	-0.090	-0.139	-0.154	-0.485	-0.565
310.0	-0.033	-0.061	-0.061	-0.064	-0.124	-0.139	-0.442	-0.550
320.0	-0.013	-0.030	-0.040	-0.044	-0.106	-0.139	-0.428	-0.536
330.0	-0.008	-0.021	-0.021	-0.021	-0.085	-0.106	-0.428	-0.527
340.0	-0.008	-0.003	-0.011	-0.010	-0.010	-0.050	-0.428	-0.527
350.0	-0.004	-0.003	-0.011	-0.010	-0.010	-0.050	-0.428	-0.527

TAP LOCATION (Z/L):	0.945	0.969	0.98	0.98	0.98
TAP LOCATION (Z/D):	5.303	5.438	5.5	5.5	5.5
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0	20.0	30.0	40.0
0.0	-0.426	-0.370	-0.358	-0.358	-0.358
10.0	-0.436	-0.386	-0.388	-0.388	-0.388
20.0	-0.447	-0.400	-0.400	-0.400	-0.400
30.0	-0.450	-0.411	-0.411	-0.411	-0.411
40.0	-0.450	-0.411	-0.411	-0.411	-0.411
50.0	-0.450	-0.411	-0.411	-0.411	-0.411
60.0	-0.450	-0.411	-0.411	-0.411	-0.411
70.0	-0.450	-0.411	-0.411	-0.411	-0.411
80.0	-0.450	-0.411	-0.411	-0.411	-0.411
90.0	-0.450	-0.411	-0.411	-0.411	-0.411
100.0	-0.450	-0.411	-0.411	-0.411	-0.411
110.0	-0.450	-0.411	-0.411	-0.411	-0.411
120.0	-0.450	-0.411	-0.411	-0.411	-0.411
130.0	-0.450	-0.411	-0.411	-0.411	-0.411
140.0	-0.450	-0.411	-0.411	-0.411	-0.411
150.0	-0.450	-0.411	-0.411	-0.411	-0.411
160.0	-0.450	-0.411	-0.411	-0.411	-0.411
170.0	-0.450	-0.411	-0.411	-0.411	-0.411
180.0	-0.450	-0.411	-0.411	-0.411	-0.411
190.0	-0.450	-0.411	-0.411	-0.411	-0.411
200.0	-0.450	-0.411	-0.411	-0.411	-0.411
210.0	-0.450	-0.411	-0.411	-0.411	-0.411
220.0	-0.450	-0.411	-0.411	-0.411	-0.411
230.0	-0.450	-0.411	-0.411	-0.411	-0.411
240.0	-0.450	-0.411	-0.411	-0.411	-0.411
250.0	-0.450	-0.411	-0.411	-0.411	-0.411
260.0	-0.450	-0.411	-0.411	-0.411	-0.411
270.0	-0.450	-0.411	-0.411	-0.411	-0.411
280.0	-0.450	-0.411	-0.411	-0.411	-0.411
290.0	-0.450	-0.411	-0.411	-0.411	-0.411
300.0	-0.450	-0.411	-0.411	-0.411	-0.411
310.0	-0.450	-0.411	-0.411	-0.411	-0.411
320.0	-0.450	-0.411	-0.411	-0.411	-0.411
330.0	-0.450	-0.411	-0.411	-0.411	-0.411
340.0	-0.450	-0.411	-0.411	-0.411	-0.411
350.0	-0.450	-0.411	-0.411	-0.411	-0.411

RPS LENGTH (L): 44.816 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: 0.94 IN.  
 MACH NO.: 0  
 ANGLE OF ATTACK (ALPHA): 0  
 SPIN RATE (PSI): 0  
 TIP SPEED RATIO (PSI/V): 0.6251-067  
 X CCL

Figure A-5. (Cont'd)

DATA SOURCE : LANGLEY

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L):	0.07	0.15	0.28	0.4	0.5
	TAP LOCATION (Z/D):	0.393	0.898	1.571	2.245	2.806
0.0		0.272	0.172	0.083	0.000	-0.322
22.5		0.249	0.149	0.061	-0.020	-0.334
45.0		0.185	0.087	0.002	-0.075	-0.383
67.5		0.035	-0.056	-0.071	-0.142	-0.445
90.0		0.000	-0.084	-0.125	-0.194	-0.468
112.5		0.003	-0.091	-0.130	-0.199	-0.471
135.0		0.005	-0.062	-0.118	-0.182	-0.445
157.5		0.003	-0.074	-0.124	-0.184	-0.447
180.0		0.002	-0.081	-0.118	-0.184	-0.471
202.5		0.003	-0.084	-0.120	-0.184	-0.461
225.0		0.000	-0.079	-0.125	-0.187	-0.458
247.5		0.027	-0.084	-0.125	-0.142	-0.445
270.0		0.075	-0.078	-0.071	-0.075	-0.383
292.5		0.103	0.008	0.062	0.020	-0.334
315.0		0.155	0.087	0.144	0.061	
337.5		0.249	0.144	0.061	0.020	

REF. LENGTH (L): 44.816 IN.  
 PE. DIAMETER (D): 7.55 IN.  
 ROTATING BAND: OFF  
 MACH NO.: 0.44 DEG.  
 ANGLE OF ATTACK (ALPHA): 10  
 SPIN RATE (P): 4980 REV./MIN  
 TIP SPEED (FT/SEC): 0.1620\_742.7  
 X F/G/L: 0.52513067

DATA SOURCE : RHES

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L):	0.503	0.526	0.537	0.548	0.571	0.615	0.65	0.705
	TAP LOCATION (Z/D):	2.824	2.95	3.014	3.077	3.203	3.454	3.706	3.957
0.0		-0.075	-0.039	-0.250	-0.340	-0.295	-0.155	-0.023	0.013
18.0		-0.07	-0.04	-0.255	-0.339	-0.25	-0.124	-0.024	0.011
36.0		-0.055	-0.055	-0.266	-0.350	-0.270	-0.156	-0.024	0.009
54.0		-0.097	-0.101	-0.282	-0.367	-0.291	-0.203	-0.015	-0.015
72.0		-0.117	-0.111	-0.3	-0.387	-0.318	-0.259	-0.068	-0.035
90.0		-0.155	-0.131	-0.356	-0.411	-0.345	-0.359	-0.081	-0.050
108.0		-0.174	-0.187	-0.38	-0.434	-0.37	-0.389	-0.096	-0.062
126.0		-0.179	-0.187	-0.38	-0.460	-0.407	-0.312	-0.106	-0.074
144.0		-0.174	-0.174	-0.410	-0.485	-0.428	-0.329	-0.109	0.065
162.0		-0.153	-0.149	-0.419	-0.492	-0.449	-0.338	-0.105	-0.038
180.0		-0.126	-0.124	-0.432	-0.504	-0.458	-0.321	-0.106	-0.063
198.0		-0.103	-0.103	-0.445	-0.502	-0.458	-0.277	-0.092	-0.055
216.0		-0.089	-0.084	-0.442	-0.500	-0.452	-0.216	-0.082	-0.053
234.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.168	-0.065	-0.048
252.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.130	-0.047	-0.041
270.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038
288.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038
306.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038
324.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038
342.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038
360.0		-0.075	-0.075	-0.442	-0.500	-0.452	-0.109	-0.039	-0.038

TAP LOCATION (Z/L):	0.75	0.846	0.859	0.87	0.888	0.899	0.91	0.922
TAP LOCATION (Z/D):	4.209	4.757	4.82	4.883	4.983	5.046	5.189	5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	18.0	36.0	54.0	72.0	90.0	108.0	126.0
0.0	-0.005	-0.009	-0.038	-0.013	-0.045	-0.054	-0.382	-0.304
18.0	-0.014	-0.010	-0.045	-0.026	-0.052	-0.064	-0.395	-0.308
36.0	-0.033	-0.019	-0.045	-0.045	-0.072	-0.071	-0.414	-0.318
54.0	-0.058	-0.036	-0.065	-0.065	-0.093	-0.093	-0.433	-0.335
72.0	-0.076	-0.051	-0.080	-0.094	-0.116	-0.119	-0.457	-0.356
90.0	-0.109	-0.103	-0.094	-0.121	-0.140	-0.149	-0.477	-0.374
108.0	-0.116	-0.134	-0.109	-0.145	-0.162	-0.167	-0.507	-0.388
126.0	-0.115	-0.137	-0.105	-0.152	-0.177	-0.179	-0.527	-0.397
144.0	-0.097	-0.130	-0.110	-0.159	-0.188	-0.190	-0.541	-0.415
162.0	-0.080	-0.120	-0.111	-0.159	-0.191	-0.191	-0.573	-0.398
180.0	-0.071	-0.110	-0.102	-0.149	-0.191	-0.260	-0.581	-0.501
200.0	-0.054	-0.110	-0.102	-0.149	-0.199	-0.263	-0.598	-0.501
220.0	-0.052	-0.119	-0.103	-0.167	-0.211	-0.275	-0.568	-0.506
240.0	-0.040	-0.119	-0.098	-0.159	-0.197	-0.250	-0.510	-0.524
260.0	-0.031	-0.095	-0.098	-0.158	-0.158	-0.172	-0.487	-0.500
280.0	-0.011	-0.078	-0.075	-0.093	-0.135	-0.172	-0.475	-0.475
300.0	-0.031	-0.070	-0.079	-0.147	-0.159	-0.233	-0.549	-0.469
320.0	-0.036	-0.076	-0.081	-0.115	-0.159	-0.239	-0.549	-0.484
340.0	-0.045	-0.098	-0.097	-0.171	-0.171	-0.229	-0.567	-0.537
360.0	-0.079	-0.099	-0.097	-0.123	-0.172	-0.229	-0.567	-0.537
0.0	-0.046	-0.115	-0.109	-0.140	-0.179	-0.230	-0.541	-0.515
18.0	-0.100	-0.149	-0.110	-0.159	-0.191	-0.230	-0.540	-0.522
36.0	-0.112	-0.160	-0.110	-0.185	-0.201	-0.234	-0.532	-0.523
54.0	-0.117	-0.169	-0.114	-0.181	-0.206	-0.231	-0.522	-0.519
72.0	-0.114	-0.162	-0.115	-0.175	-0.201	-0.229	-0.507	-0.509
90.0	-0.114	-0.156	-0.115	-0.167	-0.185	-0.201	-0.472	-0.504
108.0	-0.100	-0.141	-0.102	-0.159	-0.159	-0.181	-0.462	-0.522
126.0	-0.081	-0.123	-0.098	-0.146	-0.136	-0.153	-0.440	-0.540
144.0	-0.060	-0.109	-0.095	-0.137	-0.120	-0.161	-0.420	-0.540
162.0	-0.041	-0.094	-0.085	-0.120	-0.099	-0.178	-0.400	-0.521
180.0	-0.026	-0.084	-0.087	-0.097	-0.089	-0.178	-0.400	-0.521
200.0	-0.012	-0.071	-0.049	-0.108	-0.07	-0.065	-0.388	-0.511

TAP LOCATION (Z/L):	0.945	0.959	0.96	0.98	0.988	0.99	0.98	0.98
TAP LOCATION (Z/D):	5.303	5.438	5.49	5.5	5.438	5.438	5.438	5.438
CIRCUMFERENTIAL ANGLE (PHI)	0.0	18.0	36.0	54.0	72.0	90.0	108.0	126.0
0.0	-0.421	-0.421	-0.320	-0.352	-0.352	-0.352	-0.352	-0.352
18.0	-0.424	-0.424	-0.320	-0.369	-0.369	-0.369	-0.369	-0.369
36.0	-0.430	-0.430	-0.389	-0.381	-0.381	-0.381	-0.381	-0.381
54.0	-0.487	-0.487	-0.410	-0.420	-0.420	-0.420	-0.420	-0.420
72.0	-0.505	-0.505	-0.435	-0.431	-0.431	-0.431	-0.431	-0.431
90.0	-0.530	-0.530	-0.452	-0.465	-0.465	-0.465	-0.465	-0.465
108.0	-0.548	-0.548	-0.423	-0.310	-0.310	-0.310	-0.310	-0.310
126.0	-0.550	-0.550	-0.341	-0.244	-0.244	-0.244	-0.244	-0.244
144.0	-0.524	-0.524	-0.276	-0.201	-0.201	-0.201	-0.201	-0.201
162.0	-0.450	-0.450	-0.241	-0.186	-0.186	-0.186	-0.186	-0.186
180.0	-0.415	-0.415	-0.236	-0.177	-0.177	-0.177	-0.177	-0.177
200.0	-0.413	-0.413	-0.229	-0.171	-0.171	-0.171	-0.171	-0.171
220.0	-0.446	-0.446	-0.239	-0.176	-0.176	-0.176	-0.176	-0.176
240.0	-0.447	-0.447	-0.224	-0.170	-0.170	-0.170	-0.170	-0.170
260.0	-0.403	-0.403	-0.165	-0.176	-0.176	-0.176	-0.176	-0.176
280.0	-0.374	-0.374	-0.133	-0.080	-0.080	-0.080	-0.080	-0.080
300.0	-0.373	-0.373	-0.149	-0.106	-0.106	-0.106	-0.106	-0.106
320.0	-0.320	-0.320	-0.164	-0.120	-0.120	-0.120	-0.120	-0.120
340.0	-0.327	-0.327	-0.175	-0.120	-0.120	-0.120	-0.120	-0.120
360.0	-0.386	-0.386	-0.185	-0.123	-0.123	-0.123	-0.123	-0.123
0.0	-0.460	-0.460	-0.201	-0.134	-0.134	-0.134	-0.134	-0.134
18.0	-0.538	-0.538	-0.236	-0.151	-0.151	-0.151	-0.151	-0.151
36.0	-0.567	-0.567	-0.451	-0.186	-0.186	-0.186	-0.186	-0.186
54.0	-0.570	-0.570	-0.451	-0.355	-0.355	-0.355	-0.355	-0.355
72.0	-0.568	-0.568	-0.499	-0.352	-0.352	-0.352	-0.352	-0.352
90.0	-0.557	-0.557	-0.499	-0.413	-0.413	-0.413	-0.413	-0.413
108.0	-0.545	-0.545	-0.453	-0.445	-0.445	-0.445	-0.445	-0.445
126.0	-0.501	-0.501	-0.430	-0.430	-0.430	-0.430	-0.430	-0.430
144.0	-0.479	-0.479	-0.385	-0.409	-0.409	-0.409	-0.409	-0.409
162.0	-0.452	-0.452	-0.387	-0.387	-0.387	-0.387	-0.387	-0.387
180.0	-0.426	-0.426	-0.356	-0.356	-0.356	-0.356	-0.356	-0.356

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.9 IN.  
 STATISTIC GAP (D): 0.94  
 WICH NO.: 4900 DEF 65LV/MIN  
 ANGLE OF ATTACK (ALPHA): 0.6520274  
 SPIN RATE (P): 0.525112067  
 TIP SPEED RATIO (PD/2V): 0.525112067  
 X CG/L

Figure A-6. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07  
 TAP LOCATION (Z/D): 0.332

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.114	0.127	-0.044	-0.106	-0.484	0.571	0.515
10.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40.0	0.000	0.000	-0.037	-0.100	-0.406	0.000	0.000
50.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
60.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70.0	0.000	0.000	-0.037	-0.101	-0.406	0.000	0.000
80.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
90.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
100.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
110.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
120.0	0.000	0.000	-0.037	-0.100	-0.406	0.000	0.000
130.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
140.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
150.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
160.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
170.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
180.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
190.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
200.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
210.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
220.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
230.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
240.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
250.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
260.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
270.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
280.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
290.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
300.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
310.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
320.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
330.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
340.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
350.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
360.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: ON  
 MACH NO.: 0.54  
 ANGLE OF ATTACK (ALPHA): 0 DEG.  
 SPIN RATE (P): 0 REV/MIN  
 T.P. SPEED RATIO (PD/2V): 0  
 X CG/L: 0.625112067

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.503  
 TAP LOCATION (Z/D): 2.324

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.548	0.515
10.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
20.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
30.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
40.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
50.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
60.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
70.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
80.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
90.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
100.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
110.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
120.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
130.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
140.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
150.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
160.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
170.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
180.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
190.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
200.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
210.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
220.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
230.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
240.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
250.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
260.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
270.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
280.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
290.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
300.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
310.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
320.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
330.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
340.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
350.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515
360.0	-0.116	-0.133	-0.352	-0.408	-0.363	0.571	0.515

TAP LOCATION (Z/L): 0.75		0.848		0.87		0.888		0.892		0.91	
TAP LOCATION (Z/D): 4.209		4.757		4.883		4.983		5.046		5.109	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
10.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
20.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
30.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
40.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
50.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
60.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
70.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
80.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
90.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
100.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
110.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
120.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
130.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
140.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
150.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
160.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
170.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
180.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
190.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
200.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
210.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
220.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
230.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
240.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
250.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
260.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
270.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
280.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
290.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
300.0	0.003	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
310.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
320.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
330.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
340.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
350.0	0.002	-0.231	-0.261	-0.275	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231

TAP LOCATION (Z/L): 0.945		0.969		0.99	
TAP LOCATION (Z/D): 5.303		5.438		5.5	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.412	-0.142	-0.090	-0.089	-0.089
10.0	-0.412	-0.142	-0.089	-0.088	-0.088
20.0	-0.413	-0.142	-0.088	-0.087	-0.087
30.0	-0.413	-0.142	-0.087	-0.086	-0.086
40.0	-0.414	-0.143	-0.086	-0.085	-0.085
50.0	-0.414	-0.143	-0.085	-0.084	-0.084
60.0	-0.415	-0.143	-0.084	-0.083	-0.083
70.0	-0.415	-0.143	-0.083	-0.082	-0.082
80.0	-0.416	-0.143	-0.083	-0.081	-0.081
90.0	-0.416	-0.143	-0.083	-0.080	-0.080
100.0	-0.415	-0.143	-0.083	-0.080	-0.080
110.0	-0.415	-0.143	-0.083	-0.079	-0.079
120.0	-0.414	-0.143	-0.084	-0.078	-0.078
130.0	-0.413	-0.142	-0.084	-0.078	-0.078
140.0	-0.412	-0.141	-0.085	-0.079	-0.079
150.0	-0.411	-0.140	-0.085	-0.079	-0.079
160.0	-0.410	-0.139	-0.085	-0.079	-0.079
170.0	-0.409	-0.138	-0.085	-0.079	-0.079
180.0	-0.409	-0.137	-0.085	-0.079	-0.079
190.0	-0.410	-0.136	-0.085	-0.079	-0.079
200.0	-0.410	-0.135	-0.085	-0.079	-0.079
210.0	-0.410	-0.135	-0.085	-0.079	-0.079
220.0	-0.409	-0.134	-0.085	-0.079	-0.079
230.0	-0.409	-0.134	-0.085	-0.079	-0.079
240.0	-0.409	-0.134	-0.085	-0.079	-0.079
250.0	-0.408	-0.133	-0.085	-0.079	-0.079
260.0	-0.408	-0.133	-0.085	-0.079	-0.079
270.0	-0.406	-0.132	-0.085	-0.079	-0.079
280.0	-0.406	-0.132	-0.085	-0.079	-0.079
290.0	-0.407	-0.132	-0.085	-0.079	-0.079
300.0	-0.408	-0.132	-0.085	-0.079	-0.079
310.0	-0.410	-0.140	-0.083	-0.083	-0.083
320.0	-0.410	-0.140	-0.083	-0.083	-0.083
330.0	-0.410	-0.140	-0.083	-0.083	-0.083
340.0	-0.411	-0.141	-0.083	-0.083	-0.083
350.0	-0.412	-0.141	-0.083	-0.083	-0.083

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 POTATING BAND: ON  
 ARCH NO.: 0-94  
 ANGLE OF ATTACK (ALPHA): 0 DEG.  
 SPIN RATE (CP): 0 REV/MIN  
 TIP SPEED RATIO (TD/2V): 0  
 X CCL: 0.625112667

Figure A-7. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/D):	0.97	0.28	0.4	0.5
TAP LOCATION (Z/D):	0.33	1.571	2.245	2.886
CIRCUMFERENTIAL				
ANGLE (PHI)	0.114	0.000	0.105	0.000
*****	0.000	0.000	0.000	0.000
0.0	0.000	0.000	0.000	0.000
22.5	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000
67.5	0.000	0.000	0.000	0.000
90.0	0.000	0.000	0.000	0.000
112.5	0.000	0.000	0.000	0.000
135.0	0.000	0.000	0.000	0.000
157.5	0.000	0.000	0.000	0.000
180.0	0.000	0.000	0.000	0.000
202.5	0.000	0.000	0.000	0.000
225.0	0.000	0.000	0.000	0.000
247.5	0.000	0.000	0.000	0.000
270.0	0.000	0.000	0.000	0.000
292.5	0.000	0.000	0.000	0.000
315.0	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000
360.0	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: ON  
 MACH NO.: 0.94 DEC  
 ANGLE OF ATTACK (ALPHA): 0.000 DEG  
 SPIN RATE (P): 0.162827427  
 TIP SPEED RATIO (PD/2V): 0.625112667  
 X CG/L

DATA SOURCE : oAES

TAP LOCATION (Z/D):	0.526	0.549	0.615	0.66
TAP LOCATION (Z/D):	2.35	3.877	3.434	3.766
CIRCUMFERENTIAL				
ANGLE (PHI)	0.583	0.371	0.371	0.785
*****	2.824	3.283	3.434	3.937
0.0	-0.127	-0.361	-0.274	-0.036
10.0	-0.127	-0.361	-0.274	-0.036
20.0	-0.127	-0.361	-0.274	-0.036
30.0	-0.127	-0.361	-0.274	-0.036
40.0	-0.127	-0.361	-0.274	-0.036
50.0	-0.127	-0.361	-0.274	-0.036
60.0	-0.127	-0.361	-0.274	-0.036
70.0	-0.127	-0.361	-0.274	-0.036
80.0	-0.127	-0.361	-0.274	-0.036
90.0	-0.128	-0.360	-0.268	-0.036
100.0	-0.128	-0.360	-0.268	-0.036
120.0	-0.128	-0.360	-0.268	-0.036
140.0	-0.140	-0.368	-0.258	-0.036
160.0	-0.140	-0.368	-0.258	-0.036
180.0	-0.140	-0.368	-0.258	-0.036
200.0	-0.140	-0.368	-0.258	-0.036
220.0	-0.140	-0.368	-0.258	-0.036
240.0	-0.140	-0.368	-0.258	-0.036
260.0	-0.140	-0.368	-0.258	-0.036
280.0	-0.140	-0.368	-0.258	-0.036
300.0	-0.140	-0.368	-0.258	-0.036
320.0	-0.140	-0.368	-0.258	-0.036
340.0	-0.140	-0.368	-0.258	-0.036
360.0	-0.140	-0.368	-0.258	-0.036

Figure A-8. Rotating Band On,  $\alpha = 0^\circ$ ,  $P = 4900$  rpm

TAP LOCATION (Z/D):	0.75	0.848	0.859	0.87	0.888	0.899	0.91	0.922
TAP LOCATION (Z/D):	4.269	4.757	4.82	4.883	4.983	5.086	5.189	5.176
CIRCUMFERENTIAL								
ANGLE (PHI)								
0.0	-0.013	-0.267	-0.278	-0.282	-0.178	-0.223	-0.547	-0.503
10.0	-0.013	-0.265	-0.269	-0.218	-0.178	-0.223	-0.545	-0.501
20.0	-0.013	-0.265	-0.269	-0.221	-0.178	-0.221	-0.542	-0.499
30.0	-0.012	-0.264	-0.267	-0.223	-0.166	-0.219	-0.547	-0.494
40.0	-0.011	-0.264	-0.267	-0.233	-0.166	-0.218	-0.551	-0.492
50.0	-0.011	-0.263	-0.267	-0.238	-0.164	-0.215	-0.559	-0.487
60.0	-0.010	-0.262	-0.267	-0.243	-0.162	-0.212	-0.564	-0.485
70.0	-0.010	-0.262	-0.267	-0.244	-0.159	-0.210	-0.568	-0.482
80.0	-0.010	-0.262	-0.266	-0.244	-0.159	-0.210	-0.572	-0.482
90.0	-0.010	-0.262	-0.265	-0.249	-0.157	-0.216	-0.575	-0.484
100.0	-0.010	-0.264	-0.265	-0.251	-0.157	-0.216	-0.580	-0.486
110.0	-0.010	-0.267	-0.267	-0.252	-0.157	-0.221	-0.580	-0.485
120.0	-0.010	-0.268	-0.269	-0.258	-0.157	-0.224	-0.580	-0.489
130.0	-0.010	-0.268	-0.269	-0.259	-0.155	-0.227	-0.588	-0.490
140.0	-0.010	-0.268	-0.270	-0.262	-0.155	-0.230	-0.588	-0.491
150.0	-0.010	-0.269	-0.270	-0.265	-0.154	-0.234	-0.591	-0.493
160.0	-0.010	-0.269	-0.270	-0.265	-0.153	-0.236	-0.591	-0.495
170.0	-0.010	-0.269	-0.270	-0.267	-0.153	-0.236	-0.591	-0.495
180.0	-0.010	-0.270	-0.270	-0.267	-0.153	-0.236	-0.591	-0.495
190.0	-0.010	-0.270	-0.271	-0.267	-0.153	-0.236	-0.591	-0.495
200.0	-0.009	-0.270	-0.271	-0.267	-0.152	-0.236	-0.591	-0.495
210.0	-0.009	-0.270	-0.271	-0.267	-0.152	-0.236	-0.591	-0.495
220.0	-0.009	-0.270	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
230.0	-0.009	-0.270	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
240.0	-0.009	-0.270	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
250.0	-0.009	-0.271	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
260.0	-0.009	-0.271	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
270.0	-0.009	-0.271	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
280.0	-0.009	-0.271	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
290.0	-0.009	-0.271	-0.272	-0.267	-0.152	-0.236	-0.591	-0.495
300.0	-0.010	-0.271	-0.271	-0.268	-0.152	-0.236	-0.591	-0.495
310.0	-0.010	-0.271	-0.271	-0.268	-0.152	-0.236	-0.591	-0.495
320.0	-0.010	-0.271	-0.271	-0.268	-0.152	-0.236	-0.591	-0.495
330.0	-0.010	-0.271	-0.271	-0.268	-0.152	-0.236	-0.591	-0.495
340.0	-0.012	-0.267	-0.270	-0.267	-0.170	-0.222	-0.591	-0.502
350.0	-0.013	-0.267	-0.270	-0.267	-0.170	-0.222	-0.591	-0.503

TAP LOCATION (Z/L):	0.945	0.969	0.98	0.98	0.988	0.999	0.99	0.922
TAP LOCATION (Z/D):	5.303	5.438	5.5	5.5	5.5	5.5	5.5	5.176
CIRCUMFERENTIAL								
ANGLE (PHI)								
0.0	-0.402	-0.058	-0.058	-0.058	-0.058	-0.058	-0.058	-0.058
10.0	-0.401	-0.059	-0.058	-0.058	-0.058	-0.058	-0.058	-0.058
20.0	-0.399	-0.059	-0.059	-0.059	-0.059	-0.059	-0.059	-0.059
30.0	-0.399	-0.056	-0.058	-0.058	-0.058	-0.058	-0.058	-0.058
40.0	-0.398	-0.056	-0.058	-0.058	-0.058	-0.058	-0.058	-0.058
50.0	-0.397	-0.052	-0.052	-0.052	-0.052	-0.052	-0.052	-0.052
60.0	-0.397	-0.050	-0.050	-0.050	-0.050	-0.050	-0.050	-0.050
70.0	-0.392	-0.047	-0.045	-0.045	-0.045	-0.045	-0.045	-0.045
80.0	-0.391	-0.045	-0.045	-0.045	-0.045	-0.045	-0.045	-0.045
90.0	-0.392	-0.044	-0.044	-0.044	-0.044	-0.044	-0.044	-0.044
100.0	-0.393	-0.043	-0.043	-0.043	-0.043	-0.043	-0.043	-0.043
110.0	-0.394	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040
120.0	-0.396	-0.038	-0.038	-0.038	-0.038	-0.038	-0.038	-0.038
130.0	-0.397	-0.036	-0.036	-0.036	-0.036	-0.036	-0.036	-0.036
140.0	-0.398	-0.034	-0.034	-0.034	-0.034	-0.034	-0.034	-0.034
150.0	-0.399	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033
160.0	-0.400	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
170.0	-0.400	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
180.0	-0.400	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
190.0	-0.400	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
200.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
210.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
220.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
230.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
240.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
250.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
260.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
270.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
280.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
290.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
300.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
310.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
320.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
330.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
340.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032
350.0	-0.401	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032	-0.032

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: 0.94 DEG.  
 MACH NO.: 4.988 REV/MIN  
 ANGLE OF ATTACK (ALPHA): 0.162027427  
 SPIN RATE (P): 0.623112067  
 TIP SPEED RATIO (PD/2U): X CG/L

Figure A-8. (Cont'd)





LOCATION (Z/L): LOCATION (Z/D):	0.75 4.289	0.848 4.757	0.859 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.922 5.176
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.81	0.283	-0.146	-0.131	-0.181	-0.121	-0.328	-0.483
10.0	0.87	-0.293	-0.141	-0.136	-0.192	-0.129	-0.327	-0.488
20.0	0.919	-0.312	-0.148	-0.143	-0.199	-0.129	-0.344	-0.499
30.0	0.883	-0.339	-0.166	-0.167	-0.204	-0.147	-0.366	-0.509
40.0	-0.015	-0.352	-0.187	-0.192	-0.256	-0.156	-0.382	-0.523
50.0	-0.036	-0.396	-0.211	-0.220	-0.252	-0.221	-0.415	-0.573
60.0	-0.088	-0.428	-0.241	-0.256	-0.278	-0.247	-0.452	-0.594
70.0	-0.074	-0.467	-0.274	-0.284	-0.298	-0.278	-0.488	-0.608
80.0	-0.089	-0.435	-0.309	-0.311	-0.308	-0.285	-0.497	-0.598
90.0	-0.088	-0.445	-0.337	-0.341	-0.327	-0.285	-0.527	-0.558
100.0	-0.085	-0.433	-0.351	-0.341	-0.343	-0.281	-0.651	-0.558
110.0	-0.068	-0.421	-0.336	-0.341	-0.336	-0.281	-0.648	-0.478
120.0	-0.052	-0.341	-0.318	-0.340	-0.289	-0.304	-0.629	-0.432
130.0	-0.033	-0.283	-0.318	-0.340	-0.269	-0.304	-0.629	-0.432
140.0	-0.015	-0.261	-0.297	-0.334	-0.271	-0.307	-0.684	-0.441
150.0	0.003	-0.253	-0.282	-0.320	-0.251	-0.308	-0.617	-0.441
160.0	0.001	-0.237	-0.266	-0.294	-0.247	-0.308	-0.640	-0.441
170.0	0.003	-0.224	-0.250	-0.283	-0.247	-0.293	-0.629	-0.441
180.0	-0.003	-0.244	-0.238	-0.263	-0.235	-0.293	-0.629	-0.441
200.0	-0.010	-0.253	-0.233	-0.253	-0.233	-0.288	-0.629	-0.441
210.0	-0.017	-0.273	-0.233	-0.253	-0.233	-0.288	-0.629	-0.441
220.0	-0.024	-0.305	-0.249	-0.263	-0.233	-0.288	-0.629	-0.441
230.0	-0.034	-0.335	-0.269	-0.283	-0.233	-0.288	-0.629	-0.441
240.0	-0.043	-0.369	-0.293	-0.311	-0.252	-0.288	-0.629	-0.441
250.0	-0.061	-0.405	-0.329	-0.334	-0.276	-0.310	-0.629	-0.441
260.0	-0.080	-0.443	-0.375	-0.354	-0.324	-0.308	-0.629	-0.441
270.0	-0.084	-0.423	-0.375	-0.352	-0.324	-0.306	-0.629	-0.441
280.0	-0.076	-0.406	-0.346	-0.336	-0.342	-0.313	-0.629	-0.441
290.0	-0.056	-0.392	-0.319	-0.314	-0.330	-0.302	-0.629	-0.441
300.0	-0.045	-0.369	-0.281	-0.293	-0.311	-0.278	-0.629	-0.441
310.0	-0.045	-0.346	-0.263	-0.273	-0.290	-0.250	-0.629	-0.441
320.0	-0.022	-0.336	-0.229	-0.234	-0.242	-0.219	-0.629	-0.441
330.0	-0.003	-0.312	-0.199	-0.199	-0.242	-0.185	-0.629	-0.441
340.0	0.016	-0.299	-0.171	-0.168	-0.228	-0.161	-0.629	-0.441
350.0	0.024	-0.289	-0.153	-0.147	-0.228	-0.129	-0.629	-0.441

TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.945 5.303	0.969 5.438	0.98 5.5
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.421	-0.375	-0.368
10.0	-0.428	-0.371	-0.375
20.0	-0.435	-0.362	-0.383
30.0	-0.450	-0.397	-0.399
40.0	-0.471	-0.418	-0.414
50.0	-0.492	-0.436	-0.415
60.0	-0.518	-0.455	-0.411
70.0	-0.535	-0.458	-0.358
80.0	-0.532	-0.411	-0.269
90.0	-0.524	-0.333	-0.187
100.0	-0.468	-0.259	-0.137
110.0	-0.318	-0.177	-0.080
120.0	-0.255	-0.123	-0.081
130.0	-0.231	-0.117	-0.071
140.0	-0.229	-0.109	-0.073
150.0	-0.227	-0.107	-0.069
160.0	-0.200	-0.068	-0.054
170.0	-0.168	-0.055	-0.024
180.0	-0.183	-0.055	-0.066
190.0	-0.208	-0.088	-0.083
200.0	-0.224	-0.110	-0.092
210.0	-0.237	-0.126	-0.094
220.0	-0.252	-0.131	-0.094
230.0	-0.272	-0.142	-0.094
240.0	-0.291	-0.153	-0.101
250.0	-0.310	-0.168	-0.109
260.0	-0.327	-0.178	-0.121
270.0	-0.337	-0.185	-0.127
280.0	-0.336	-0.185	-0.127
290.0	-0.326	-0.178	-0.127
300.0	-0.306	-0.163	-0.127
310.0	-0.283	-0.143	-0.127
320.0	-0.257	-0.117	-0.127
330.0	-0.229	-0.087	-0.127
340.0	-0.200	-0.057	-0.127
350.0	-0.172	-0.027	-0.127

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: ON  
 MAGN. NO.: 0.94  
 ANGLE OF ATTACK (ALPHA): 10 DEG.  
 SPIN RATE (P): 0 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0  
 X CG/L 0.625112867

Figure A-9. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L):	0.07	0.16	0.28	0.4	0.5
TAP LOCATION (Z/D):	0.393	0.898	1.571	2.245	2.886
CIRCUMFERENTIAL					
ANGLE (PHI)					
*****					
0.0	0.272	0.172	0.083	0.008	-0.223
22.5	0.249	0.149	0.061	-0.029	-0.323
45.0	0.185	0.087	-0.002	-0.059	-0.393
67.5	0.103	0.008	-0.071	-0.175	-0.445
90.0	0.005	-0.056	-0.125	-0.182	-0.468
112.5	-0.080	-0.084	-0.136	-0.199	-0.482
135.0	-0.003	-0.081	-0.130	-0.184	-0.471
157.5	0.006	-0.072	-0.118	-0.164	-0.446
180.0	0.013	-0.059	-0.098	-0.152	-0.447
202.5	0.005	-0.072	-0.118	-0.154	-0.446
225.0	-0.003	-0.081	-0.138	-0.184	-0.471
247.5	0.020	-0.084	-0.136	-0.199	-0.486
270.0	0.103	-0.056	-0.125	-0.182	-0.468
292.5	0.185	0.008	-0.071	-0.175	-0.445
315.0	0.249	0.087	0.002	-0.059	-0.393
337.5	0.272	0.149	0.061	-0.029	-0.323

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: ON  
 MACH NO.: 0.94  
 ANGLE OF ATTACK (ALPHA): 10 DEG.  
 SPIN RATE (P): 4900 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0.162827427  
 X CC/L 0.625112867

DATA SOURCE : NMEP

TAP LOCATION (Z/L):	0.583	0.526	0.537	0.548	0.571	0.615	0.66	0.705
TAP LOCATION (Z/D):	2.824	2.95	3.014	3.077	3.203	3.454	3.786	3.957
CIRCUMFERENTIAL								
ANGLE (PHI)								
*****								
0.0	0.227	0.222	0.249	0.339	0.532	-0.139	-0.824	0.013
15.0	0.230	0.225	0.252	0.342	0.535	-0.140	-0.824	0.011
30.0	0.233	0.228	0.255	0.345	0.538	-0.141	-0.824	0.008
45.0	0.236	0.231	0.258	0.348	0.541	-0.142	-0.824	0.005
60.0	0.239	0.234	0.261	0.351	0.544	-0.143	-0.824	0.002
75.0	0.242	0.237	0.264	0.354	0.547	-0.144	-0.824	0.000
90.0	0.245	0.240	0.267	0.357	0.550	-0.145	-0.824	0.000
105.0	0.248	0.243	0.270	0.360	0.553	-0.146	-0.824	0.000
120.0	0.251	0.246	0.273	0.363	0.556	-0.147	-0.824	0.000
135.0	0.254	0.249	0.276	0.366	0.559	-0.148	-0.824	0.000
150.0	0.257	0.252	0.279	0.369	0.562	-0.149	-0.824	0.000
165.0	0.260	0.255	0.282	0.372	0.565	-0.150	-0.824	0.000
180.0	0.263	0.258	0.285	0.375	0.568	-0.151	-0.824	0.000
195.0	0.266	0.261	0.288	0.378	0.571	-0.152	-0.824	0.000
210.0	0.269	0.264	0.291	0.381	0.574	-0.153	-0.824	0.000
225.0	0.272	0.267	0.294	0.384	0.577	-0.154	-0.824	0.000
240.0	0.275	0.270	0.297	0.387	0.580	-0.155	-0.824	0.000
255.0	0.278	0.273	0.300	0.390	0.583	-0.156	-0.824	0.000
270.0	0.281	0.276	0.303	0.393	0.586	-0.157	-0.824	0.000
285.0	0.284	0.279	0.306	0.396	0.589	-0.158	-0.824	0.000
300.0	0.287	0.282	0.309	0.399	0.592	-0.159	-0.824	0.000
315.0	0.290	0.285	0.312	0.402	0.595	-0.160	-0.824	0.000
330.0	0.293	0.288	0.315	0.405	0.598	-0.161	-0.824	0.000
345.0	0.296	0.291	0.318	0.408	0.601	-0.162	-0.824	0.000
360.0	0.299	0.294	0.321	0.411	0.604	-0.163	-0.824	0.000

TAP LOCATION (Z/L): TAP LOCATION (Z/D):		0.75 4.289	0.848 4.757	0.899 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.92 5.176
CIRCUMFERENTIAL ANGLE (PHI)	CIRCUMFERENTIAL ANGLE (PHI)	0.81	0.889	0.107	0.106	0.184	0.151	0.197	0.412
		Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)
0.0	0.0	0.811	-0.889	-0.107	-0.106	-0.184	-0.151	-0.197	-0.412
10.0	10.0	0.888	-0.810	-0.105	-0.185	-0.184	-0.154	-0.584	-0.418
20.0	20.0	0.862	-0.819	-0.106	-0.186	-0.185	-0.154	-0.584	-0.418
30.0	30.0	-0.812	-0.836	-0.109	-0.186	-0.112	-0.148	-0.515	-0.451
40.0	40.0	-0.839	-0.859	-0.106	-0.111	-0.109	-0.166	-0.537	-0.531
50.0	50.0	-0.844	-0.861	-0.108	-0.113	-0.133	-0.196	-0.561	-0.531
60.0	60.0	-0.857	-0.883	-0.108	-0.121	-0.121	-0.232	-0.584	-0.543
70.0	70.0	-0.875	-0.894	-0.114	-0.128	-0.146	-0.265	-0.602	-0.547
80.0	80.0	-0.886	-0.914	-0.132	-0.137	-0.168	-0.291	-0.617	-0.556
90.0	90.0	-0.899	-0.937	-0.156	-0.156	-0.180	-0.295	-0.626	-0.543
100.0	100.0	-0.867	-0.938	-0.195	-0.176	-0.176	-0.299	-0.621	-0.507
110.0	110.0	-0.852	-0.920	-0.182	-0.182	-0.173	-0.307	-0.604	-0.479
120.0	120.0	-0.852	-0.919	-0.185	-0.184	-0.173	-0.319	-0.604	-0.445
130.0	130.0	-0.848	-0.919	-0.189	-0.189	-0.178	-0.319	-0.599	-0.445
140.0	140.0	-0.843	-0.921	-0.201	-0.219	-0.198	-0.317	-0.649	-0.455
150.0	150.0	-0.825	-0.922	-0.202	-0.219	-0.237	-0.317	-0.658	-0.455
160.0	160.0	-0.801	-0.954	-0.281	-0.221	-0.237	-0.384	-0.658	-0.455
170.0	170.0	-0.804	-0.976	-0.281	-0.221	-0.227	-0.384	-0.615	-0.418
180.0	180.0	-0.808	-0.976	-0.240	-0.218	-0.227	-0.384	-0.615	-0.418
190.0	190.0	-0.824	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
200.0	200.0	-0.844	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
210.0	210.0	-0.863	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
220.0	220.0	-0.875	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
230.0	230.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
240.0	240.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
250.0	250.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
260.0	260.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
270.0	270.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
280.0	280.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
290.0	290.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
300.0	300.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
310.0	310.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
320.0	320.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
330.0	330.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
340.0	340.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418
350.0	350.0	-0.899	-0.999	-0.248	-0.218	-0.227	-0.384	-0.615	-0.418

TAP LOCATION (Z/L): TAP LOCATION (Z/D):		0.945 5.383	0.969 5.438	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5
CIRCUMFERENTIAL ANGLE (PHI)	CIRCUMFERENTIAL ANGLE (PHI)	0.389	0.389	0.389	0.389	0.389	0.389	0.389	0.389
		Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)	Coefficient (CP)
0.0	0.0	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389
10.0	10.0	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389
20.0	20.0	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389	-0.389
30.0	30.0	-0.425	-0.425	-0.425	-0.425	-0.425	-0.425	-0.425	-0.425
40.0	40.0	-0.448	-0.448	-0.448	-0.448	-0.448	-0.448	-0.448	-0.448
50.0	50.0	-0.477	-0.477	-0.477	-0.477	-0.477	-0.477	-0.477	-0.477
60.0	60.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
70.0	70.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
80.0	80.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
90.0	90.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
100.0	100.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
110.0	110.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
120.0	120.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
130.0	130.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
140.0	140.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
150.0	150.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
160.0	160.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
170.0	170.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
180.0	180.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
190.0	190.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
200.0	200.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
210.0	210.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
220.0	220.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
230.0	230.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
240.0	240.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
250.0	250.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
260.0	260.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
270.0	270.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
280.0	280.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
290.0	290.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
300.0	300.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
310.0	310.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
320.0	320.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
330.0	330.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
340.0	340.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484
350.0	350.0	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484	-0.484

REF. LENGTH (L): 44.616 IN.  
REF. DIAMETER (D): 7.95 IN.  
ROTATING BAND: ON  
ANGLE OF ATTACK (ALPHA): 0.94 DEG  
SPIN RATE (P): 10 REV/MIN  
TIP SPEED RATIO (PD/2V): 0.162027427  
X CG/L: 0.625112067

Figure A-10. (Cont'd)

## APPENDIX B

### PLOTTED WIND TUNNEL TEST DATA

This appendix contains the measured pressure data in plotted format. Each set of plots relates to a specific model configuration and test condition with data for both the spinning and non-spinning cases presented on each plot. The appendix figures include the following data:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)
B1	OFF	0	0, 4900
B2	OFF	4	0, 4900
B3	OFF	10	0, 4900
B4	ON	0	0, 4900
B5	ON	10	0, 4900

Because of the computer format, some of the terms in Appendix B are different from those of the main report text. The following define these terms:

<u>Term</u>	<u>Symbol used in report text</u>
P-P STATIC	$\Delta P$
C.P.	$C_p$
PHI	$\phi$

ROTATING BAND = OFF  
 WASH NUMBER = 54  
 ANGLE OF ATTACK (DEG) = 0

SYMBOL      SPIN RATE (RPM)  
 Δ            0  
 ○            1000

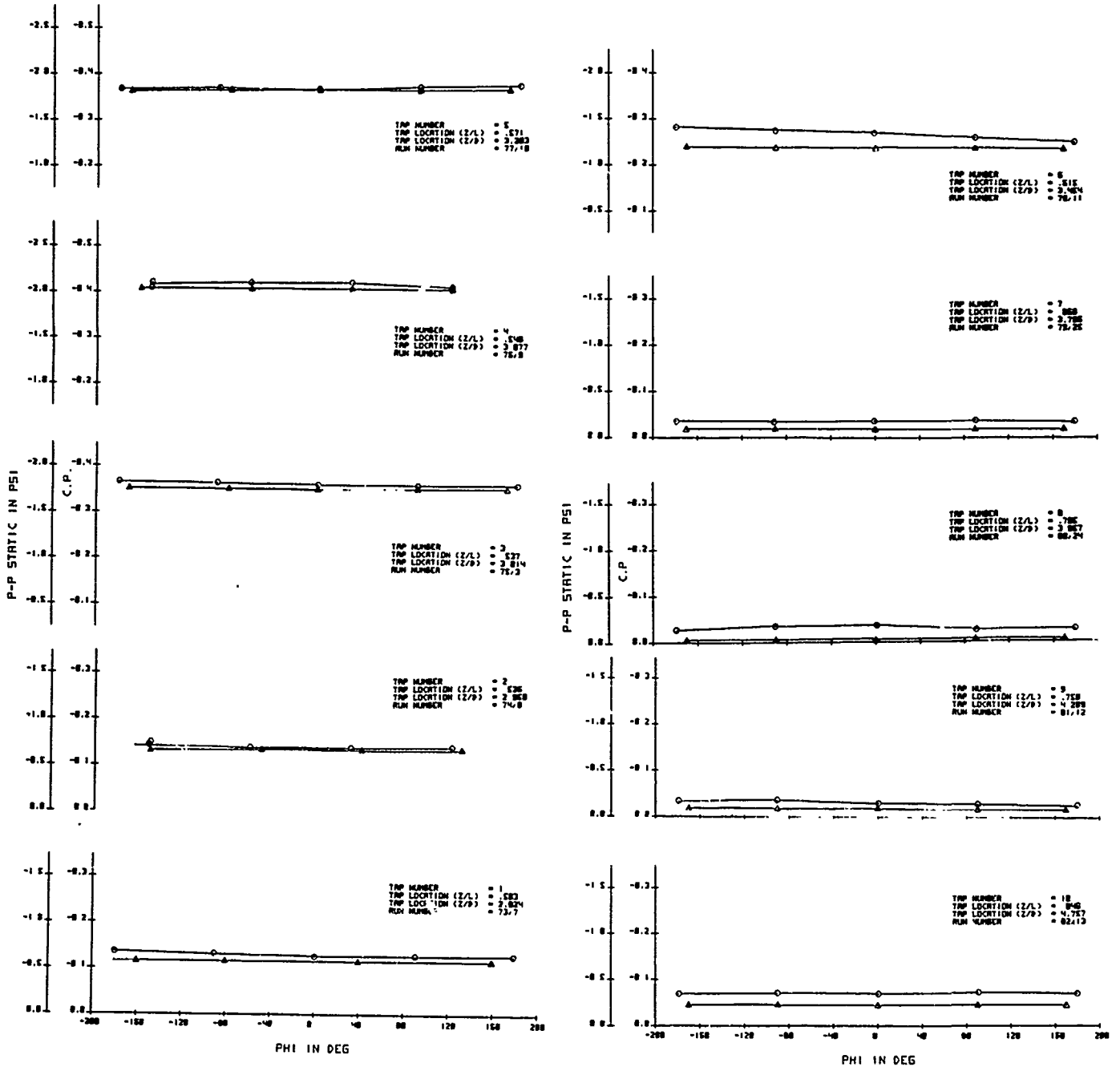


Figure B-1. Rotating Band Off,  $\alpha = 0^\circ$

ROTATION GROUP    • DFT  
 HATCH NUMBER    • 54  
 NUMBER OF ATTACKS    • 8

SYMBOL    SPIN RATE (RPM)  
 Δ    0  
 ○    1000

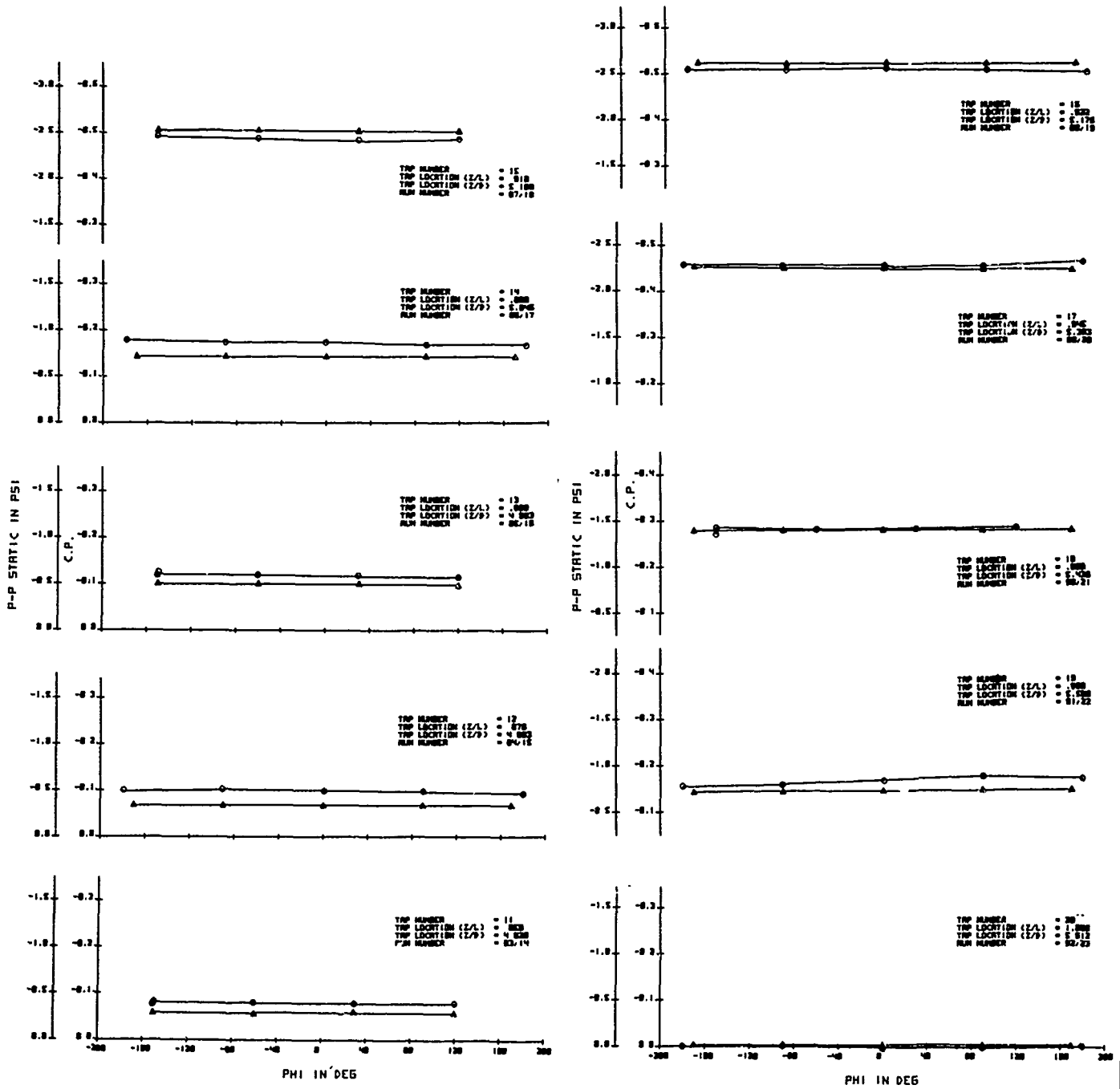


Figure B-1 (Continued)

ROTATING BAND OFF  
 RICH NUMBER = 34  
 TABLE OF ATTRIBUTES = 4

SYMBOL SPIN RATE (RPM)  
 Δ 0  
 ○ 1000

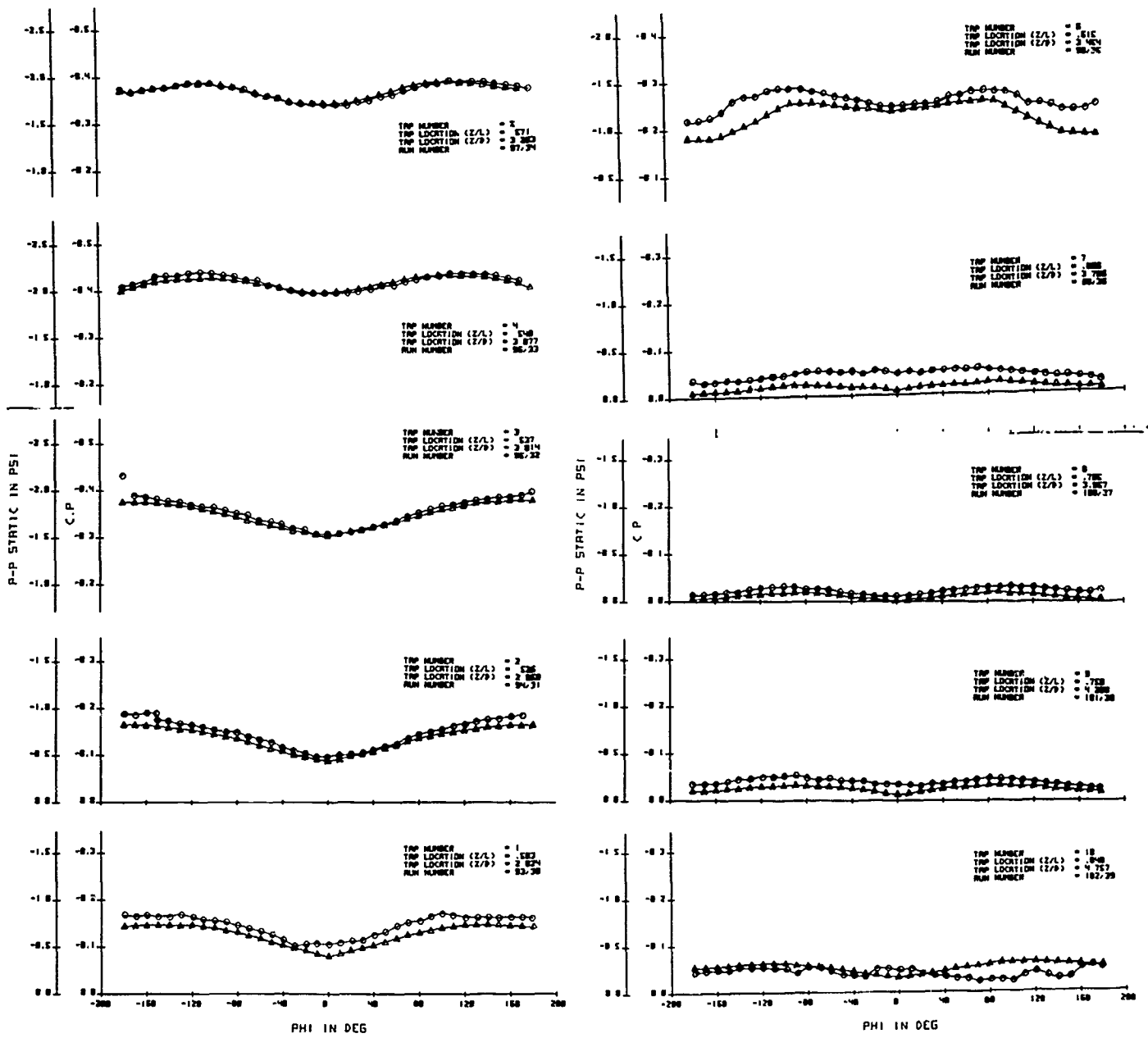


Figure B-2. Rotating Band Off,  $\alpha = 4^\circ$

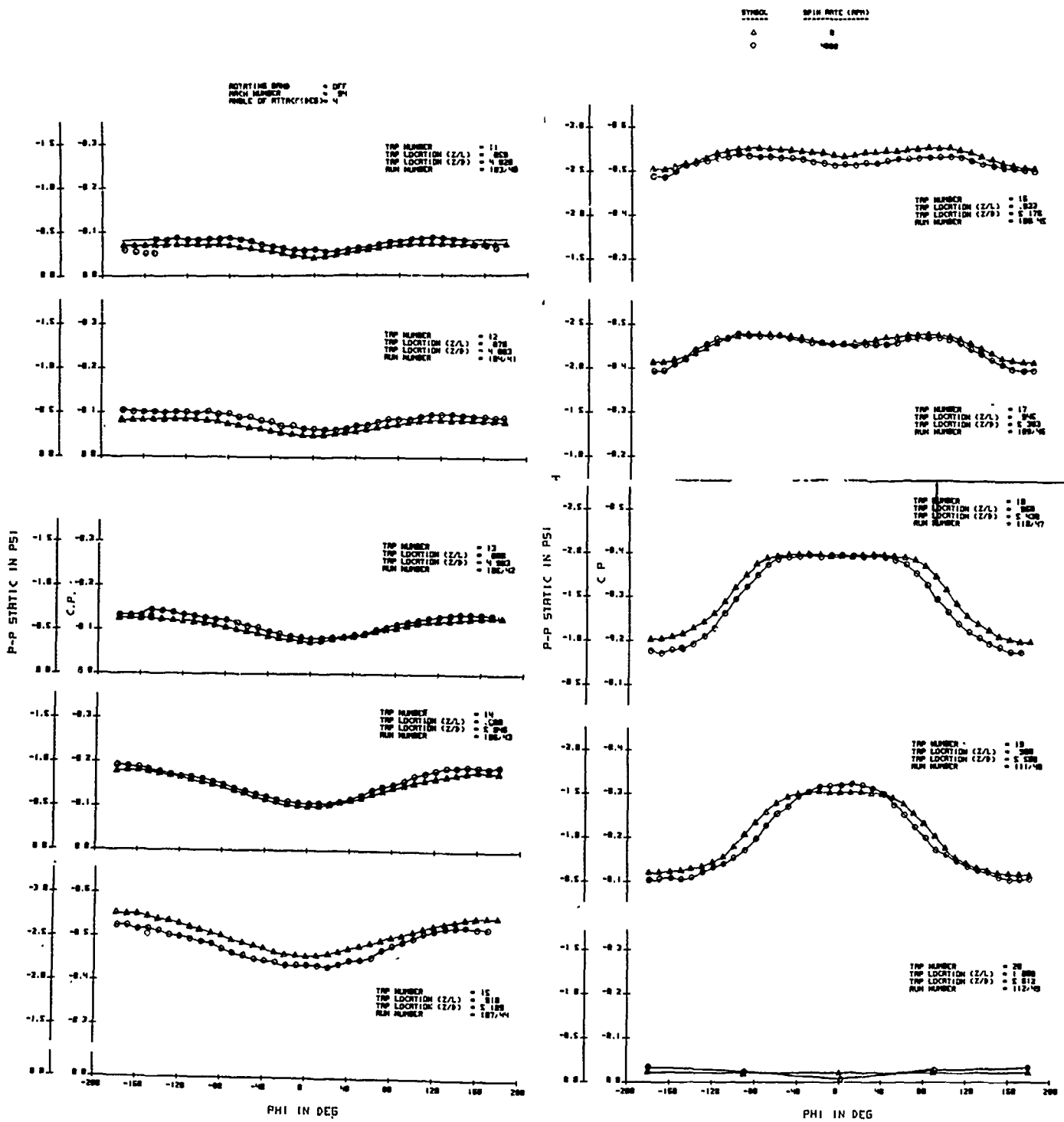


Figure B-2 (Continued)



TABLE OF SYMBOLS  
 SYMBOL  
 A  
 O

SPIN RATE (RPM)  
 0  
 1000

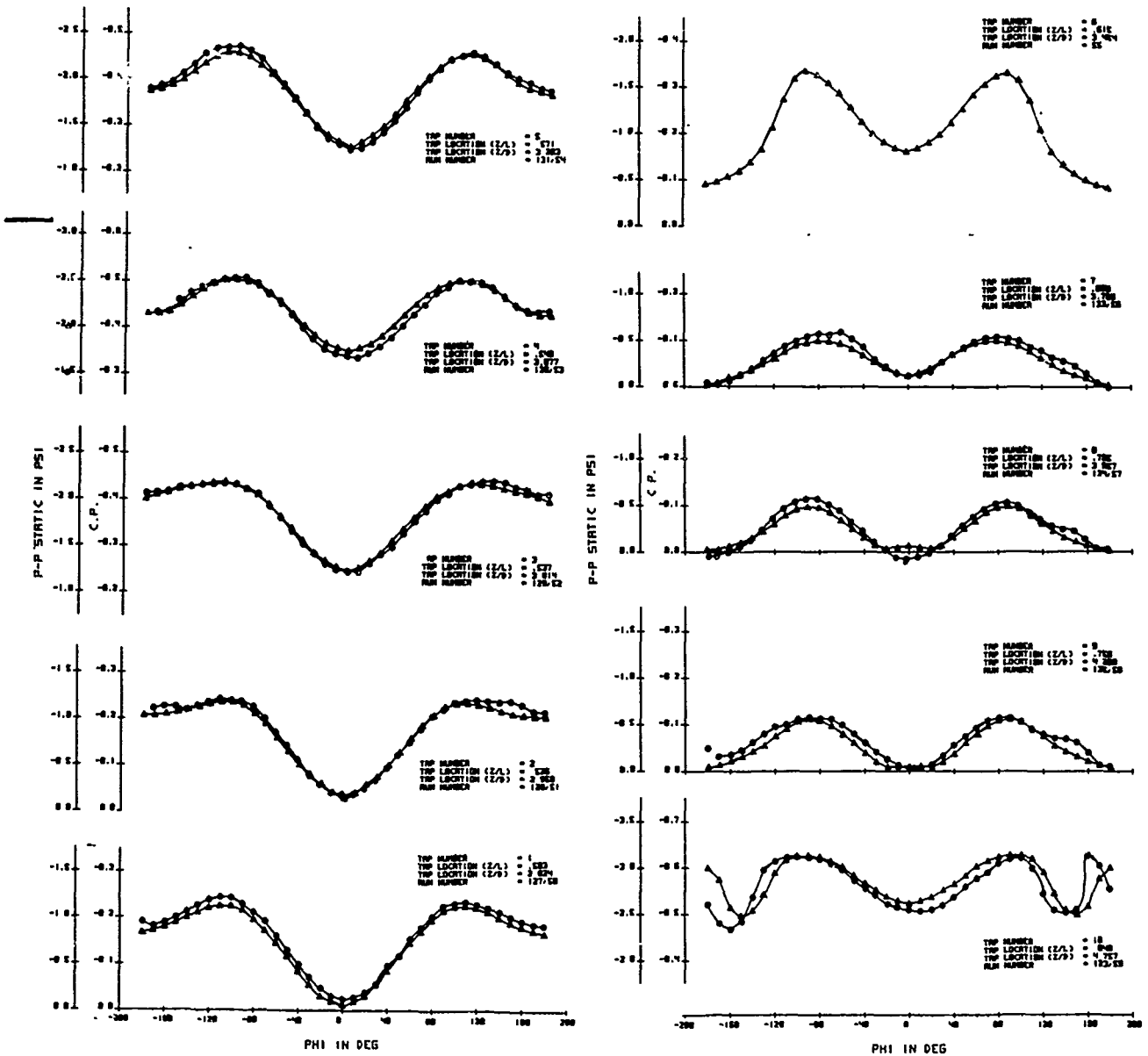


Figure B-3. Rotating Band Off,  $\alpha = 10^\circ$

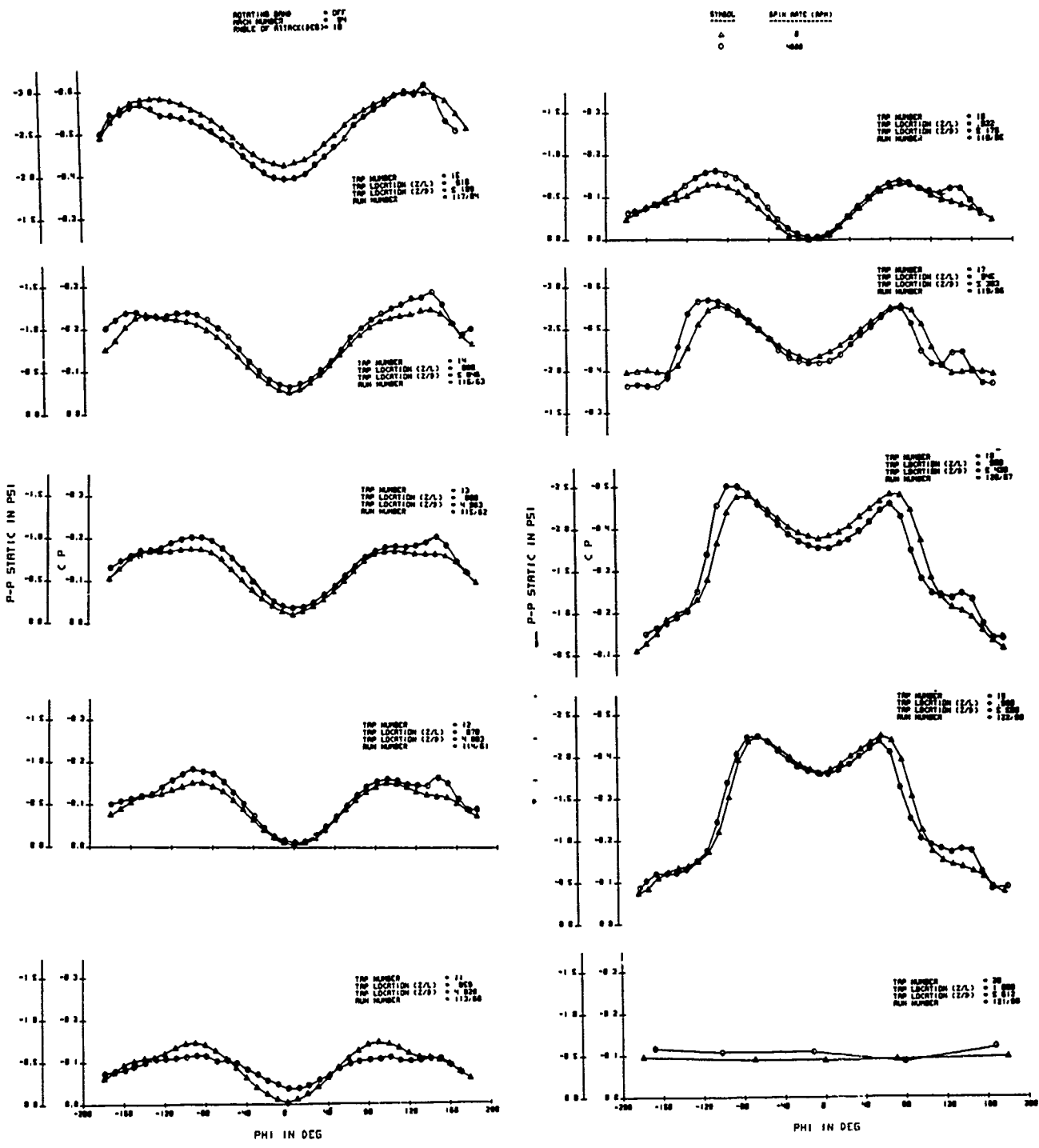


Figure B-3 (Continued)

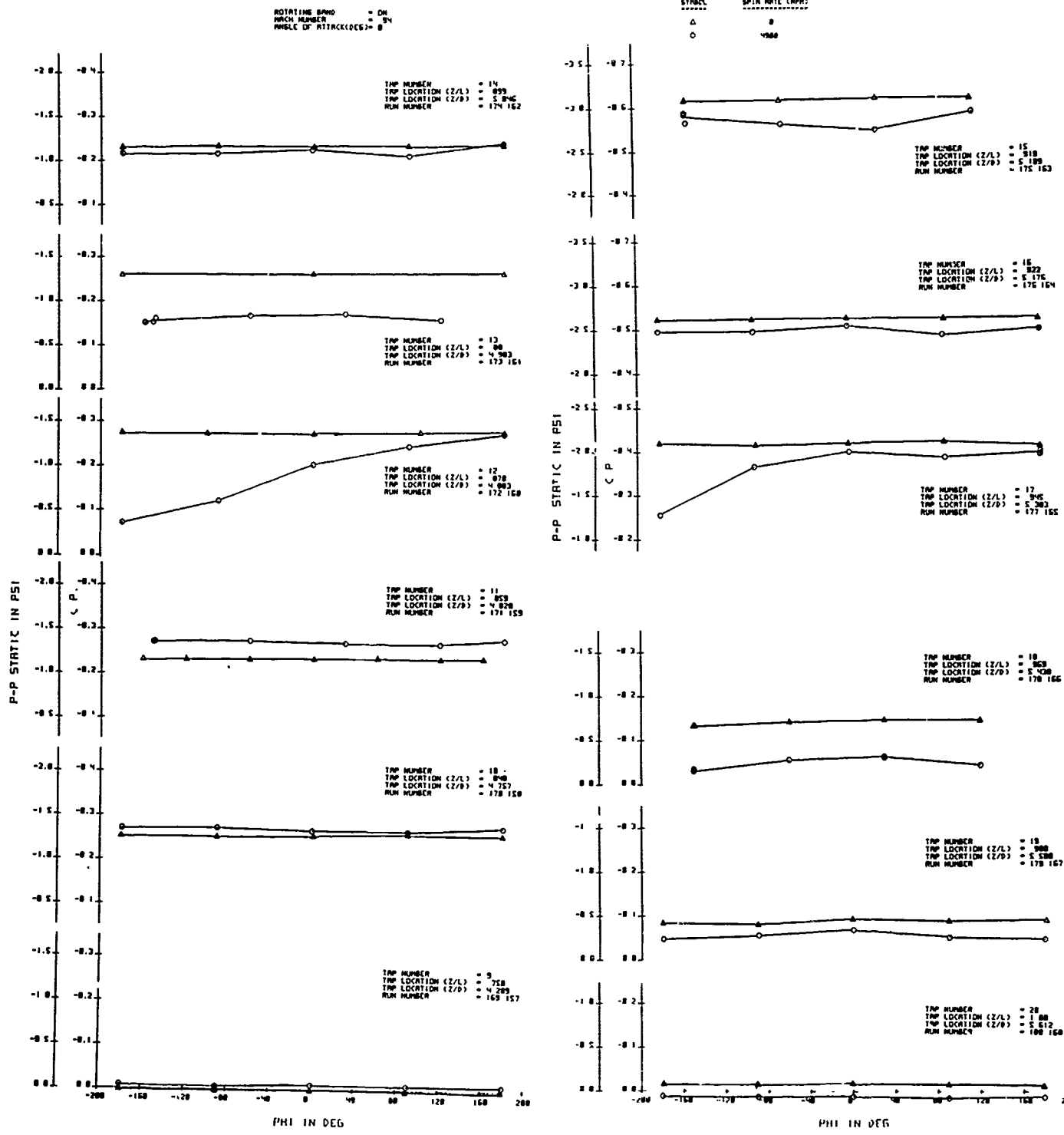


Figure B-4. Rotating Band On,  $\alpha = 0^\circ$

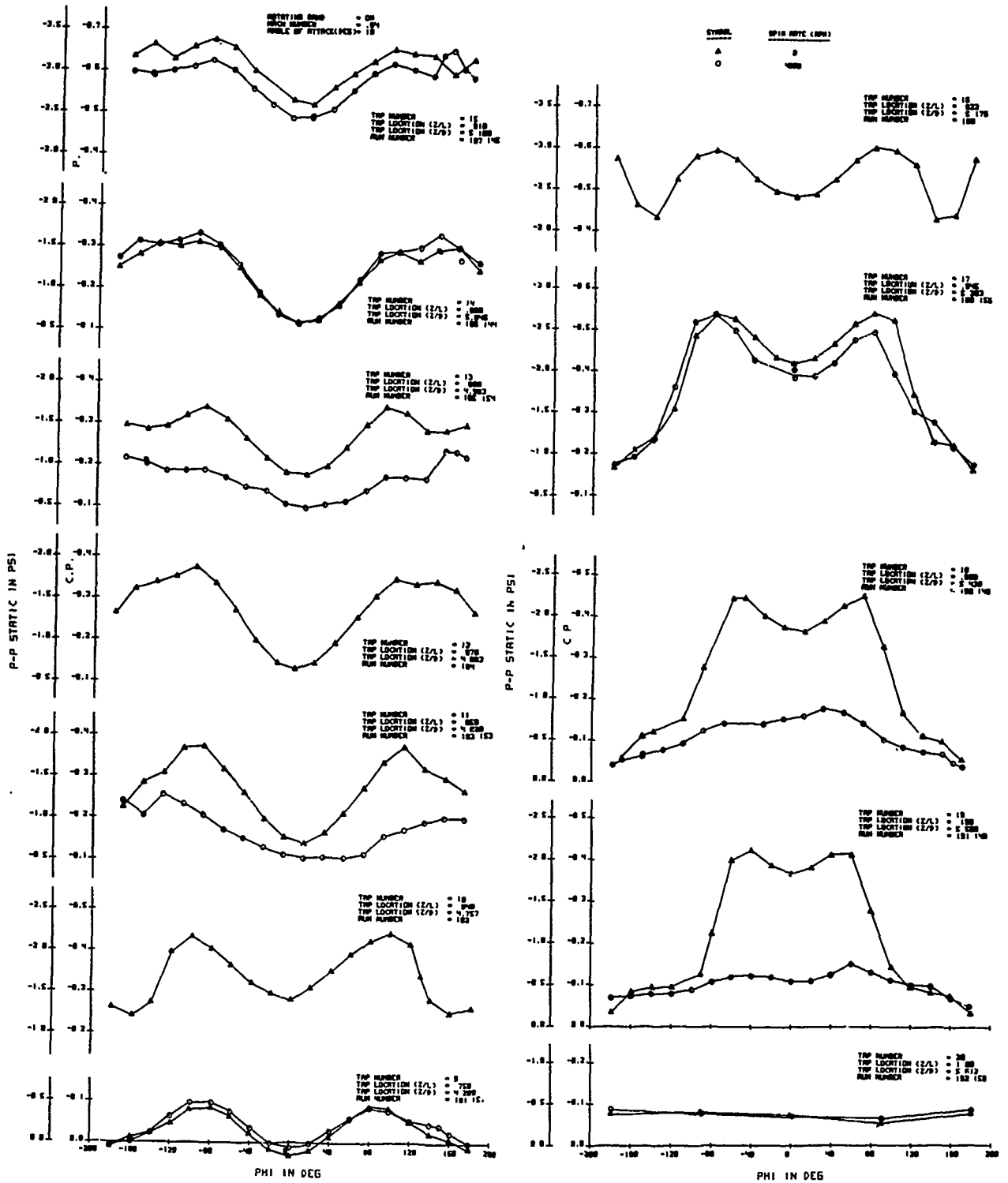


Figure B-5. Rotating Band On,  $\alpha = 10^\circ$

## APPENDIX C

### FORCE AND MOMENT TERMS COMPUTED FROM SURFACE PRESSURE DATA

This appendix contains both local and total force and moment coefficients and related terms as computed from the measured surface pressure data. Each set of data relates to a specific model configuration and test condition as follows:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)
C1	OFF	0	0
C2	OFF	0	4900
C3	OFF	4	0
C4	OFF	4	4900
C5	OFF	10	0
C6	OFF	10	4900
C7	ON	0	0
C8	ON	0	4900
C9	ON	10	0
C10	ON	10	4900

These data indicate the total coefficient values as well as the contribution to the coefficient values due to the nose, cylinder, and boattail portions of model where:

<u>Portion</u>	<u>Region (Z/L)</u>
nose	0 to .537
cylinder	.537 to .910
boattail	.910 to 1.00

The terms are listed for the longitudinal location at which they were computed. Because of the computer format, some of the terms are different from those in the main report text. The following define these terms:

<u>Terms</u>	<u>Symbol used in report text</u>	<u>Definition (if not in report text)</u>
XCG/L	$X_{cg}/L$	
ZI/L	$Z_i/L$	
ZI	$Z_i$	
DZI	$\Delta Z_i$	
DIA	$d_i$	Diameter of model at $Z_i$
CNI LOCAL	$C_N$	Local normal force coefficient normal to local surface
CN	$C_{N_i}$	Local normal force coefficient normal to longitudinal (Z) axis
C SUM	$\sum C_{N_i}$	Summation of local normal force coefficients from nose
CM	$C_{M_i}$	Local pitching moment coefficient
CYI LOCAL	$C_{Y_i}$	Local side (Magnus) force coefficient normal to local surface
CY SUM	$\sum C_Y$	Summation of local side (Magnus) force coefficients from nose
Cn	$C_{n_i}$	Local yawing (Magnus) moment coefficient
NORMAL FORCE COEFFICIENT	$C_N$	Total normal force coefficient
PITCHING MOMENT COEFFICIENT (NOSE)	$C_M$	Total pitching moment coefficient referred to tip of nose ( $Z/L = 0$ )
PITCHING MOMENT COEFFICIENT (CG)		Total pitching moment coefficient referred to Ref C.G. ( $Z/L = .625$ )
NORMAL FORCE COEFFICIENT (NOSE)		Normal force coefficient due to nose portion of model
PITCHING MOMENT COEFFICIENT (NOSE) (NOSE)		Pitching moment coefficient due to nose portion of model referred to tip of nose ( $Z/L = 0$ )

PITCHING MOMENT  
COEFFICIENT  
(CG) (NOSE)

Pitching moment coefficient due  
to nose portion of model referred  
to Ref C.G. ( $Z/L = .625$ )

NORMAL FORCE  
COEFFICIENT  
(CYL)

Normal force coefficient due to  
cylindrical portion of model

PITCHING MOMENT  
COEFFICIENT  
(CYL) (NOSE)

Pitching moment coefficient due  
to cylindrical portion of model  
referred to tip of nose ( $Z/L = 0$ )

PITCHING MOMENT  
COEFFICIENT  
(CG) (CYL)

Pitching moment coefficient due  
to cylindrical portion of model  
referred to Ref C.G. ( $Z/L = .625$ )

NORMAL FORCE  
COEFFICIENT  
(BT)

Normal force coefficient due to  
boattail portion of model

PITCHING MOMENT  
COEFFICIENT  
(NOSE) (BT)

Pitching moment coefficient due  
to boattail portion of model  
referred to tip of nose ( $Z/L = 0$ )

PITCHING MOMENT  
COEFFICIENT  
(CG) (BT)

Pitching moment coefficient due  
to boattail portion of model  
referred to Ref C.G. ( $Z/L = .625$ )

REF. LENGTH (L): 44.616 III.  
 REF. DIAMETER (D): 7.95 III.  
 ROTATING BAND: OFF  
 MACH NO.: 0.94 DEG.  
 ANGLE OF ATTACK (ALPHA): 0 REV/MIN  
 SPIN RATE (P): 0  
 TIP SPEED RATIO (PD/2V): 0.625112067  
 X CG-L

ZI/L	ZI	DZI	DIA.	CHL	CH	CH	CH	ZI/L	ZI	DZI	DIA.	CVI	CY	CY	CM
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
0.970	3.123	5.130	2.125	-0.0003	0.0003	-0.0003	-0.0003	0.070	3.123	5.130	2.125	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.160	7.139	4.685	3.812	-0.0004	-0.0004	-0.0007	-0.0005	0.160	7.139	4.685	3.812	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.280	12.492	5.354	5.375	-0.0005	-0.0005	-0.0019	-0.0014	0.280	12.492	5.354	5.375	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.400	17.846	4.908	6.875	-0.0007	-0.0007	-0.0019	-0.0028	0.400	17.846	4.908	6.875	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.500	22.308	2.302	7.718	-0.0001	-0.0001	-0.0018	-0.0024	0.500	22.308	2.302	7.718	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.503	22.449	0.571	7.750	0.0000	0.0000	-0.0018	-0.0024	0.503	22.449	0.571	7.750	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.526	23.450	0.756	7.937	0.0000	0.0000	-0.0018	-0.0024	0.526	23.450	0.756	7.937	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.537	23.951	0.586	7.950	0.0000	0.0000	-0.0018	-0.0024	0.537	23.951	0.586	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.549	24.461	0.750	7.950	0.0000	0.0000	-0.0018	-0.0024	0.549	24.461	0.750	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.615	27.461	2.000	7.950	0.0000	0.0000	-0.0018	-0.0024	0.615	27.461	2.000	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.615	27.461	2.000	7.950	0.0000	0.0000	-0.0018	-0.0024	0.615	27.461	2.000	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.628	27.461	2.000	7.950	0.0000	0.0000	-0.0018	-0.0024	0.628	27.461	2.000	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.700	31.461	3.180	7.950	0.0000	0.0000	-0.0018	-0.0024	0.700	31.461	3.180	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.848	37.821	2.430	7.950	0.0000	0.0000	-0.0018	-0.0024	0.848	37.821	2.430	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.859	38.321	0.548	7.950	0.0000	0.0000	-0.0018	-0.0024	0.859	38.321	0.548	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.870	38.821	0.648	7.950	0.0000	0.0000	-0.0018	-0.0024	0.870	38.821	0.648	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.888	39.616	0.648	7.950	0.0000	0.0000	-0.0018	-0.0024	0.888	39.616	0.648	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.899	40.116	0.500	7.950	0.0000	0.0000	-0.0018	-0.0024	0.899	40.116	0.500	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.910	40.616	0.518	7.950	0.0000	0.0000	-0.0018	-0.0024	0.910	40.616	0.518	7.950	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.922	41.151	0.772	7.975	0.0000	0.0000	-0.0018	-0.0024	0.922	41.151	0.772	7.975	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.945	42.159	1.043	7.975	0.0000	0.0000	-0.0018	-0.0024	0.945	42.159	1.043	7.975	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.969	43.235	0.783	7.259	0.0000	0.0000	-0.0018	-0.0024	0.969	43.235	0.783	7.259	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.980	43.725	0.690	7.259	0.0000	0.0000	-0.0018	-0.0024	0.980	43.725	0.690	7.259	0.00E+00	0.00E+00	0.00E+00	0.00E+00

NORMAL FORCE COEFFICIENT (NOSE) = -1.79196E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) = -2.42109E-03  
 PITCHING MOMENT COEFFICIENT (CG) = -3.06544E-03  
 NORMAL FORCE COEFFICIENT (NOSE) (NOSE) = -1.79196E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) (NOSE) = -2.42109E-03  
 PITCHING MOMENT COEFFICIENT (CG) (NOSE) = -3.06544E-03  
 NORMAL FORCE COEFFICIENT (CYL) = 4.31000E-12  
 PITCHING MOMENT COEFFICIENT (CYL) (CYL) = 1.61200E-11  
 PITCHING MOMENT COEFFICIENT (CG) (CYL) = -9.99761E-11  
 NORMAL FORCE COEFFICIENT (BT) = 2.06000E-12  
 PITCHING MOMENT COEFFICIENT (NOSE) (BT) = 1.09800E-11  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -3.75316E-12

Figure C-1. Rotating Band Off,  $\alpha = 0^\circ$  P = 0 rpm



REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BANDS: OFF  
 MACH NO.: 0.94 DEG.  
 ANGLE OF ATTACK (ALPHA): 0  
 SPIN RATE (P): 4900 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0.162027427  
 X CG/L: 0.625112067

ZI/L	ZI	DZI	DIA.	LOCAL	CM	CN	CN	SUM	CM	ZI/L	ZI	DZI	DIA.	LOCAL	CVI	CY	CY	SUM	CM
0.970	3.123	5.138	2.125	-0.0003	-0.0003	0.0000	0.0000	-0.0003	-0.0001	0.970	3.123	5.138	2.125	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.160	7.139	4.685	3.812	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	0.160	7.139	4.685	3.812	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.800	12.492	5.354	5.375	-0.0006	-0.0006	-0.0006	-0.0006	-0.0006	-0.0006	0.800	12.492	5.354	5.375	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.990	17.846	4.988	6.875	-0.0007	-0.0007	-0.0007	-0.0007	-0.0007	-0.0007	0.990	17.846	4.988	6.875	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.980	22.388	2.382	7.718	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.980	22.388	2.382	7.718	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.990	22.449	0.571	7.750	0.0004	0.0004	0.0004	0.0004	0.0004	0.0004	0.990	22.449	0.571	7.750	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.926	23.458	0.756	7.537	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.926	23.458	0.756	7.537	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.937	23.961	0.586	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.937	23.961	0.586	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.548	24.461	0.750	7.500	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	0.548	24.461	0.750	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.571	25.461	1.500	7.500	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	0.571	25.461	1.500	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.615	27.461	2.000	7.500	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	0.615	27.461	2.000	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.588	27.461	2.000	7.500	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	-0.0012	0.588	27.461	2.000	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.750	31.461	3.188	7.500	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	0.750	31.461	3.188	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.780	31.461	3.188	7.500	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	0.780	31.461	3.188	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.859	38.321	0.500	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.859	38.321	0.500	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.870	38.321	0.648	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.870	38.321	0.648	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.899	39.616	0.648	7.500	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	0.899	39.616	0.648	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.888	40.116	0.500	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.888	40.116	0.500	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.910	40.616	0.518	7.500	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.910	40.616	0.518	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.945	42.159	1.043	7.500	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004	0.945	42.159	1.043	7.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.969	43.236	0.783	7.375	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	0.969	43.236	0.783	7.375	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.980	43.725	0.690	7.250	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.980	43.725	0.690	7.250	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

NORMAL FORCE COEFFICIENT (NOSE) = -4.34259E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) = -0.013313269  
 PITCHING MOMENT COEFFICIENT (CG) (NOSE) = -1.92129E-03  
 PITCHING MOMENT COEFFICIENT (CG) (NOSE) = -0.026801532  
 PITCHING MOMENT COEFFICIENT (CG) (NOSE) = -0.011857803  
 PITCHING MOMENT COEFFICIENT (BT) = -1.39720E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -1.38473E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -3.59718E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -8.62373E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -0.022281040  
 PITCHING MOMENT COEFFICIENT (CYL) (CYL) = -2.46248E-03  
 PITCHING MOMENT COEFFICIENT (CYL) (CYL) = -2.44275E-03  
 PITCHING MOMENT COEFFICIENT (CYL) (CYL) = -0.015197904  
 PITCHING MOMENT COEFFICIENT (CYL) (CYL) = 0.213359E-04  
 PITCHING MOMENT COEFFICIENT (NOSE) (BT) = -4.82828E-04  
 PITCHING MOMENT COEFFICIENT (NOSE) (BT) = -2.52499E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = 0.31143E-04  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = -2.97991E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = 5.12965E-03

Figure C-2. Rotating Band Off,  $\alpha = 0^\circ$ ,  $P = 4900$  rpm

REF. LENGTH (L): 44.616 IN.  
 ROTATING BAND: 7.95 IN.  
 HATCH HO. 1: 0.94  
 ANGLE OF ATTACK (ALPHA): 4 DEG.  
 SPIN RATE (P): 0 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0.625112067  
 X CG/L

ZI/L	ZI	DZI	DIA.	CH	CH	CH	ZI/L	DZI	DIA.	CH	CH	ZI	DZI	DIA.	CH	CH	CY	CY	CY	CH
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
0.878	3.123	5.130	2.125	0.0172	0.0168	0.0168	0.878	3.123	5.130	2.125	0.0168	3.123	5.130	2.125	0.0168	0.0168	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.160	7.139	4.585	3.812	0.0249	0.0414	0.0286	0.160	7.139	4.585	3.812	0.0286	7.139	4.585	3.812	0.0286	0.0414	-6.10E-14	-6.10E-14	-6.10E-14	-6.10E-14
0.280	12.492	5.354	5.375	0.0343	0.0753	0.0339	0.280	12.492	5.354	5.375	0.0339	12.492	5.354	5.375	0.0339	0.0753	-1.31E-14	-1.31E-14	-1.31E-14	-1.31E-14
0.400	17.846	4.988	6.875	0.0338	0.1088	0.0335	0.400	17.846	4.988	6.875	0.0335	17.846	4.988	6.875	0.0335	0.1088	-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13
0.500	22.388	2.302	7.718	0.0113	0.1201	0.0113	0.500	22.388	2.302	7.718	0.0113	22.388	2.302	7.718	0.0113	0.1201	-7.53E-13	-7.53E-13	-7.53E-13	-7.53E-13
0.580	25.449	0.571	7.750	0.0040	0.1241	0.0040	0.580	25.449	0.571	7.750	0.0040	25.449	0.571	7.750	0.0040	0.1241	-5.1E-13	-5.1E-13	-5.1E-13	-5.1E-13
0.526	23.450	0.571	7.750	0.0066	0.1307	0.0066	0.526	23.450	0.571	7.750	0.0066	23.450	0.571	7.750	0.0066	0.1307	5.55E-05	5.55E-05	5.55E-05	5.55E-05
0.537	23.961	0.596	7.950	0.0045	0.1352	0.0045	0.537	23.961	0.596	7.950	0.0045	23.961	0.596	7.950	0.0045	0.1352	1.08E-04	1.08E-04	1.08E-04	1.08E-04
0.548	24.461	0.750	7.950	0.0017	0.1368	0.0017	0.548	24.461	0.750	7.950	0.0017	24.461	0.750	7.950	0.0017	0.1368	-2.79E-05	-2.79E-05	-2.79E-05	-2.79E-05
0.615	25.461	1.980	7.950	0.0063	0.1431	0.0063	0.615	25.461	1.980	7.950	0.0063	25.461	1.980	7.950	0.0063	0.1431	-4.78E-04	-4.78E-04	-4.78E-04	-4.78E-04
0.660	29.461	2.080	7.950	-0.0011	0.1272	-0.0011	0.660	29.461	2.080	7.950	-0.0011	29.461	2.080	7.950	-0.0011	0.1272	-3.39E-04	-3.39E-04	-3.39E-04	-3.39E-04
0.785	31.461	3.180	7.950	0.0002	0.1262	0.0002	0.785	31.461	3.180	7.950	0.0002	31.461	3.180	7.950	0.0002	0.1262	2.39E-04	2.39E-04	2.39E-04	2.39E-04
0.848	33.461	3.180	7.950	0.0008	0.1271	0.0008	0.848	33.461	3.180	7.950	0.0008	33.461	3.180	7.950	0.0008	0.1271	2.85E-04	2.85E-04	2.85E-04	2.85E-04
0.859	34.821	0.500	7.950	0.0092	0.1321	0.0092	0.859	34.821	0.500	7.950	0.0092	34.821	0.500	7.950	0.0092	0.1321	2.14E-04	2.14E-04	2.14E-04	2.14E-04
0.870	38.821	0.548	7.950	0.0032	0.1349	0.0032	0.870	38.821	0.548	7.950	0.0032	38.821	0.548	7.950	0.0032	0.1349	6.38E-06	6.38E-06	6.38E-06	6.38E-06
0.898	40.821	0.598	7.950	0.0042	0.1378	0.0042	0.898	40.821	0.598	7.950	0.0042	40.821	0.598	7.950	0.0042	0.1378	-1.05E-05	-1.05E-05	-1.05E-05	-1.05E-05
0.910	48.616	0.598	7.950	0.0045	0.1429	0.0045	0.910	48.616	0.598	7.950	0.0045	48.616	0.598	7.950	0.0045	0.1429	3.32E-05	3.32E-05	3.32E-05	3.32E-05
0.922	41.151	0.772	7.950	0.0057	0.1556	0.0057	0.922	41.151	0.772	7.950	0.0057	41.151	0.772	7.950	0.0057	0.1556	3.08E-05	3.08E-05	3.08E-05	3.08E-05
0.945	42.159	1.043	7.625	-0.0029	0.1457	-0.0029	0.945	42.159	1.043	7.625	-0.0029	42.159	1.043	7.625	-0.0029	0.1457	1.09E-04	1.09E-04	1.09E-04	1.09E-04
0.969	43.235	0.783	7.375	-0.0057	0.1441	-0.0057	0.969	43.235	0.783	7.375	-0.0057	43.235	0.783	7.375	-0.0057	0.1441	2.06E-04	2.06E-04	2.06E-04	2.06E-04
0.980	43.725	0.650	7.250	-0.0168	0.1031	-0.0168	0.980	43.725	0.650	7.250	-0.0168	43.725	0.650	7.250	-0.0168	0.1031	2.27E-04	2.27E-04	2.27E-04	2.27E-04

FORCE COEFFICIENT (NOSE) = 1.77513E-03  
 MOMENT COEFFICIENT (CG) = 8.10339E-03  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA = -1.87594E-03  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA = -0.025426803  
 FORCE COEFFICIENT (NOSE) = 1.356229E-04  
 MOMENT COEFFICIENT (CG) (CYL) = 3.91289E-04  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 8.45194E-05  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 1.94274E-03  
 FORCE COEFFICIENT (NOSE) = 1.21065E-03  
 MOMENT COEFFICIENT (CG) (CYL) = 8.67788E-04  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 3.55719E-03  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -3.12848E-04  
 FORCE COEFFICIENT (NOSE) = 0.012436145  
 MOMENT COEFFICIENT (CG) (CYL) = -7.34589E-03  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 7.17099E-04  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 4.15091E-03  
 FORCE COEFFICIENT (NOSE) = 1.44762E-03  
 MOMENT COEFFICIENT (CG) (CYL) = 0.011803921  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -0.0202735658

MAGNUS FORCE COEFFICIENT (NOSE) = 0.18814826  
 MOMENT COEFFICIENT (CG) = 0.088224461  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA = 0.291166634  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA = 1.5498869534  
 MAGNUS FORCE COEFFICIENT (NOSE) = 4.170654823  
 MOMENT COEFFICIENT (CG) (CYL) = 0.135161454  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 0.24182759  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 1.5368045364  
 MAGNUS FORCE COEFFICIENT (NOSE) = 3.453038863  
 MOMENT COEFFICIENT (CG) (CYL) = 0.017486246  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 0.096240782  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -0.031766686  
 MAGNUS FORCE COEFFICIENT (NOSE) = 0.249326109  
 MOMENT COEFFICIENT (CG) (CYL) = -0.503887761  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -0.044422884  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -0.241118998  
 MAGNUS FORCE COEFFICIENT (NOSE) = 0.882795651  
 MOMENT COEFFICIENT (CG) (CYL) = -0.636310939  
 FORCE COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = -0.636310939  
 MOMENT COEFFICIENT DERIVATIVE WRT ALPHA (NOSE) = 1.221463721

Figure C-3. Rotating Band Off,  $\alpha = 4^\circ$ ,  $\dot{\rho} = 0$  rpm

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: OFF  
 MACH NO.: 8.94 DEG.  
 SPIN RATE (RPM): 4900 REV/MIN  
 TIP SPEED RATIO (PD/2V): 0.16207427  
 X CC/L 0.625112867

ZI/L	ZI	DZI	DZI	DIA	LOCAL	CH	CH	CM	ZI/L	ZI	JZI	DIA	DIA	LOCAL	CY	CY	CH
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
NORMAL	0.980	3.123	5.130	2.125	0.0172	0.0168	0.0168	0.0066	0.070	3.123	5.130	2.125	2.125	0.00E+00	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.670	7.139	4.585	0.249	0.0249	0.0249	0.0249	0.0066	0.150	7.139	4.585	0.249	0.249	-7.59E-14	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.800	12.492	5.334	0.0343	0.0343	0.0343	0.0343	0.0066	0.280	12.492	5.334	0.280	0.280	-1.51E-14	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.400	17.046	4.908	0.0338	0.0338	0.0338	0.0338	0.0066	0.400	17.046	4.908	0.400	0.400	-1.03E-13	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.993	22.308	2.302	0.0113	0.0113	0.0113	0.0113	0.0066	0.500	22.308	2.302	0.500	0.500	-1.03E-13	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.500	22.449	0.571	0.0041	0.0041	0.0041	0.0041	0.0066	0.503	22.449	0.571	0.503	0.503	-5.97E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.526	23.450	0.756	0.0080	0.0080	0.0080	0.0080	0.0066	0.526	23.450	0.756	0.526	0.526	-2.80E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.337	23.961	0.386	0.0049	0.0049	0.0049	0.0049	0.0066	0.537	23.961	0.386	0.537	0.537	-2.86E-05	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.476	24.461	0.586	0.0031	0.0031	0.0031	0.0031	0.0066	0.548	24.461	0.586	0.548	0.548	-1.99E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.271	24.961	0.750	0.0024	0.0024	0.0024	0.0024	0.0066	0.571	24.961	0.750	0.571	0.571	-8.23E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.650	25.461	1.300	0.0074	0.0074	0.0074	0.0074	0.0066	0.615	25.461	1.300	0.615	0.615	-4.75E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.211	25.961	2.000	0.0042	0.0042	0.0042	0.0042	0.0066	0.660	25.961	2.000	0.660	0.660	-4.75E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.785	26.461	2.800	0.0020	0.0020	0.0020	0.0020	0.0066	0.785	26.461	2.800	0.785	0.785	-5.68E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.400	26.961	3.100	0.0020	0.0020	0.0020	0.0020	0.0066	0.848	26.961	3.100	0.848	0.848	-4.19E-03	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.948	27.461	2.430	0.0008	0.0008	0.0008	0.0008	0.0066	0.948	27.461	2.430	0.948	0.948	-3.72E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.559	27.961	0.500	0.0026	0.0026	0.0026	0.0026	0.0066	0.980	27.961	0.500	0.980	0.980	-3.72E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.888	28.461	0.648	0.0045	0.0045	0.0045	0.0045	0.0066	0.989	28.461	0.648	0.989	0.989	-4.46E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.970	28.961	0.648	0.0052	0.0052	0.0052	0.0052	0.0066	0.999	28.961	0.648	0.999	0.999	-4.46E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.899	29.461	0.500	0.0054	0.0054	0.0054	0.0054	0.0066	0.910	29.461	0.500	0.910	0.910	-4.46E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.910	29.961	0.518	0.0054	0.0054	0.0054	0.0054	0.0066	0.922	29.961	0.518	0.922	0.922	-4.46E-04	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.945	30.461	0.772	0.0015	0.0015	0.0015	0.0015	0.0066	0.945	30.461	0.772	0.945	0.945	-2.19E-03	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.969	30.961	1.043	0.0037	0.0037	0.0037	0.0037	0.0066	0.969	30.961	1.043	0.969	0.969	-2.19E-03	0.00E+00	0.00E+00	0.00E+00
NORMAL	0.980	31.461	0.783	0.0234	0.0234	0.0234	0.0234	0.0066	0.980	31.461	0.783	0.980	0.980	-6.35E-04	0.00E+00	0.00E+00	0.00E+00
PITCHING	0.980	31.961	0.690	0.0179	0.0179	0.0179	0.0179	0.0066	0.980	31.961	0.690	0.980	0.980	-6.35E-04	0.00E+00	0.00E+00	0.00E+00

LOCAL	CY	CY	CH	LOCAL	CY	CY	CH
*****	*****	*****	*****	*****	*****	*****	*****
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
-7.59E-14	-7.59E-14	-7.59E-14	-7.59E-14	-7.59E-14	-7.59E-14	-7.59E-14	-7.59E-14
-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13	-1.03E-13
-5.97E-04	-5.97E-04	-5.97E-04	-5.97E-04	-5.97E-04	-5.97E-04	-5.97E-04	-5.97E-04
-2.80E-04	-2.80E-04	-2.80E-04	-2.80E-04	-2.80E-04	-2.80E-04	-2.80E-04	-2.80E-04
-2.86E-05	-2.86E-05	-2.86E-05	-2.86E-05	-2.86E-05	-2.86E-05	-2.86E-05	-2.86E-05
-1.99E-04	-1.99E-04	-1.99E-04	-1.99E-04	-1.99E-04	-1.99E-04	-1.99E-04	-1.99E-04
-8.23E-04	-8.23E-04	-8.23E-04	-8.23E-04	-8.23E-04	-8.23E-04	-8.23E-04	-8.23E-04
-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04
-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04	-4.75E-04
-5.68E-04	-5.68E-04	-5.68E-04	-5.68E-04	-5.68E-04	-5.68E-04	-5.68E-04	-5.68E-04
-4.19E-03	-4.19E-03	-4.19E-03	-4.19E-03	-4.19E-03	-4.19E-03	-4.19E-03	-4.19E-03
-3.72E-04	-3.72E-04	-3.72E-04	-3.72E-04	-3.72E-04	-3.72E-04	-3.72E-04	-3.72E-04
-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04
-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04	-4.46E-04
-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03
-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03	-2.19E-03
-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04
-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04	-6.35E-04

MAGNUS	FORCE	MOMENT	COEFFICIENT	NOSE	NOSE	NOSE	NOSE
*****	*****	*****	*****	*****	*****	*****	*****
0.11119353	0.137107864	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719
0.682261684	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.021162364
0.287597773	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.099898399
1.351810884	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	-0.025449874
0.689825693	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.382413944
1.898426212	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.382413944
0.137107864	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	-0.157393194
0.238861519	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.047160885
0.242136983	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	-0.255449554
1.963954587	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.099898399
3.468335672	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	-0.6755047
0.846281573	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	1.305919142
1.4944419719	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.291087170
0.021162364	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.561392087
0.099898399	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
-0.025449874	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.382413944	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.382413944	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
-0.157393194	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.047160885	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
-0.255449554	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.099898399	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
-0.6755047	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
1.305919142	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.291087170	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000
0.561392087	0.238861519	0.242136983	1.963954587	3.468335672	0.846281573	1.4944419719	0.000000000

Figure C-4. Rotating Band Off,  $\alpha = 4^\circ$ ,  $P = 4900$  rpm



REF. LENGTH (L): 44.616 IH.  
 ROTATING BAND: 7.95 IN.  
 RICH. NO.: 0.94  
 CH. NO.: 1900  
 SPIN RATE (P): -4900 DEG  
 TIP SPEED RATIO (PD/2V): 0.625112067  
 X CG/L

ZI/L	ZI (IN)	DZI (IN)	DIA. (IN)	CHI LOCAL	CHI SUM	CH	ZI/L (IN)	ZI (IN)	DZI	DIA. (IN)	CYL LOCAL	CYL SUM	CY	CM
0.070	3.123	5.130	2.125	0.0432	0.0432	0.0170	0.070	3.123	5.130	2.125	0.0432	0.0432	0.21E-15	3.20E-15
0.280	12.492	4.885	3.812	0.0652	0.1074	0.0746	0.160	7.139	4.885	3.812	0.1074	0.17E-13	-1.07E-13	-1.00E-13
0.480	27.946	5.354	5.375	0.0830	0.1894	0.2095	0.280	12.492	5.354	5.375	0.1894	-4.14E-13	-5.32E-13	-5.32E-13
0.680	52.308	4.908	6.975	0.0901	0.2689	0.2912	0.480	27.946	4.908	6.975	0.2689	-1.11E-13	-3.07E-13	-9.43E-13
0.880	76.756	2.592	7.758	0.0368	0.3056	0.3043	0.680	52.308	2.592	7.758	0.3056	5.89E-13	8.87E-13	1.44E-12
0.930	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.880	76.756	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.937	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.937	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.948	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.948	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.951	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.951	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.955	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.955	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.960	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.960	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.965	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.965	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.970	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.970	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.975	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.975	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.980	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.980	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.985	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.985	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.990	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.990	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
0.995	81.250	0.756	7.937	0.0185	0.3240	0.3043	0.995	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12
1.000	81.250	0.756	7.937	0.0185	0.3240	0.3043	1.000	81.250	0.756	7.937	0.3056	5.89E-13	8.87E-13	1.44E-12

Figure C-6. Rotating Band Off,  $\alpha = 10^\circ$ , P = 4900 rpm

REF. LENGTH (L): 44.616 INL  
 REF. DIAMETER (D): 7.95 INL  
 ROTATING BAND:  
 MACH NO.: 0.94 DEC.  
 ANGLE OF ATTACK (ALPHA): 0 PEV/NIH  
 SPIN RATE (P): 0  
 TIP SPEED RATIO (FD/2V): 0.625112967  
 X CG-L

ZI-L	ZI	DZ1	DIA	CYI	CY	CY SUM	CH	DZ1	ZI-L	CH	DZ1	DIA	CYI	CY	CY SUM	CH
(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)	(IN)
0.070	3.123	5.130	3.125	-0.0003	-0.0003	0.0000	0.0000	0.070	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.160	7.119	4.685	3.812	-0.0004	-0.0005	-0.0001	-0.0001	0.160	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.280	12.492	5.354	5.375	-0.0005	-0.0014	-0.0014	-0.0014	0.280	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.400	17.866	4.302	5.875	-0.0007	-0.0025	-0.0025	-0.0025	0.400	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.500	22.308	2.302	7.718	-0.0011	-0.0038	-0.0038	-0.0038	0.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.583	22.449	0.571	7.750	-0.0013	-0.0053	-0.0053	-0.0053	0.583	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.526	23.430	0.756	7.937	-0.0018	-0.0074	-0.0074	-0.0074	0.526	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.537	23.961	0.506	7.950	-0.0024	-0.0102	-0.0102	-0.0102	0.537	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.571	24.461	0.750	7.950	-0.0033	-0.0141	-0.0141	-0.0141	0.571	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.520	25.461	1.500	7.950	-0.0048	-0.0204	-0.0204	-0.0204	0.520	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.460	26.461	2.000	7.950	-0.0070	-0.0294	-0.0294	-0.0294	0.460	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.780	27.461	2.000	7.950	-0.0103	-0.0428	-0.0428	-0.0428	0.780	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.750	28.461	2.180	7.950	-0.0138	-0.0602	-0.0602	-0.0602	0.750	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.848	29.461	2.180	7.950	-0.0187	-0.0828	-0.0828	-0.0828	0.848	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.859	30.461	2.500	7.950	-0.0251	-0.1116	-0.1116	-0.1116	0.859	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.870	31.461	0.642	7.950	-0.0321	-0.1476	-0.1476	-0.1476	0.870	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.888	32.461	0.642	7.950	-0.0406	-0.1932	-0.1932	-0.1932	0.888	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.899	33.461	0.500	7.950	-0.0508	-0.2508	-0.2508	-0.2508	0.899	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.910	34.461	0.519	7.950	-0.0638	-0.3228	-0.3228	-0.3228	0.910	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.922	35.461	0.777	7.950	-0.0798	-0.4116	-0.4116	-0.4116	0.922	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.945	36.461	1.045	7.950	-0.1002	-0.5196	-0.5196	-0.5196	0.945	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.969	37.461	0.750	7.950	-0.1263	-0.6528	-0.6528	-0.6528	0.969	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.980	38.461	0.650	7.950	-0.1593	-0.8160	-0.8160	-0.8160	0.980	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

NORMAL FORCE COEFFICIENT (NOSE) = -3.6943E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) = 0.0120E-04  
 PITCHING MOMENT COEFFICIENT (CG) = -9.2100E-04  
 NORMAL FORCE COEFFICIENT (NOSE) (NOSE) = -1.7919E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) (NOSE) = -2.4210E-03  
 PITCHING MOMENT COEFFICIENT (CG) (NOSE) = -3.3654E-03  
 NORMAL FORCE COEFFICIENT (CYL) = -6.8579E-04  
 PITCHING MOMENT COEFFICIENT (NOSE) (CYL) = -2.9598E-03  
 PITCHING MOMENT COEFFICIENT (CG) (CYL) = 6.2411E-04  
 NORMAL FORCE COEFFICIENT (BT) = -1.2371E-03  
 PITCHING MOMENT COEFFICIENT (NOSE) (BT) = -6.6603E-03  
 PITCHING MOMENT COEFFICIENT (CG) (BT) = 2.3202E-03

FORCE COEFFICIENT (NOSE) = -2.9888E-03  
 MOMENT COEFFICIENT (NOSE) = -0.015271450  
 MOMENT COEFFICIENT (CG) = 4.7860E-03  
 FORCE COEFFICIENT (NOSE) = -2.6944E-03  
 MOMENT COEFFICIENT (NOSE) = -8.1333E-13  
 MOMENT COEFFICIENT (CG) (NOSE) = -1.3194E-13  
 FORCE COEFFICIENT (CYL) = -1.0027E-03  
 MOMENT COEFFICIENT (NOSE) (CYL) = -6.5859E-03  
 MOMENT COEFFICIENT (CG) (CYL) = 1.6177E-03  
 FORCE COEFFICIENT (BT) = -1.6875E-03  
 MOMENT COEFFICIENT (NOSE) (BT) = -9.0861E-03  
 MOMENT COEFFICIENT (CG) (BT) = 3.1682E-03

Figure C-7. Rotating Band On,  $\alpha = 0^\circ$ ,  $P = 0$  rpm

44.516 IN.  
 7.95 IN.  
 ON  
 0.94 DEG.  
 4900 REV/MIN  
 0.16207427  
 0.625112067

REF. LENGTH (L):  
 REF. DIAMETER (D):  
 ROTATING BAND:  
 MACH NO.:  
 ANGLE OF ATTACK (ALPHA):  
 SPIN RATE (P):  
 TIP SPEED RATIO (PD/2V):  
 X C/VL

Z1/L	Z1	DZ1	MIR	CH1	CH	CH	Z1/L	Z1/L	DZ1	MIR	CH1	CH	CH	Z1/L	Z1/L	DZ1	MIR	CH1	CH	CH	CY	CY	CY	CH
0.070	3.123	5.130	2.125	-0.0003	-0.0003	-0.0003	0.070	0.070	5.130	2.125	-0.0003	-0.0003	-0.0003	0.070	0.070	5.130	2.125	-0.0003	-0.0003	-0.0003	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.160	7.139	4.685	3.812	-0.0004	-0.0004	-0.0004	0.160	0.160	4.685	3.812	-0.0004	-0.0004	-0.0004	0.160	0.160	4.685	3.812	-0.0004	-0.0004	-0.0004	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.280	12.432	5.354	5.375	-0.0006	-0.0006	-0.0006	0.280	0.280	5.354	5.375	-0.0006	-0.0006	-0.0006	0.280	0.280	5.354	5.375	-0.0006	-0.0006	-0.0006	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.400	17.846	4.908	4.875	-0.0007	-0.0007	-0.0007	0.400	0.400	4.908	4.875	-0.0007	-0.0007	-0.0007	0.400	0.400	4.908	4.875	-0.0007	-0.0007	-0.0007	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.500	22.308	2.302	7.718	-0.0008	-0.0008	-0.0008	0.500	0.500	2.302	7.718	-0.0008	-0.0008	-0.0008	0.500	0.500	2.302	7.718	-0.0008	-0.0008	-0.0008	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.600	22.449	0.571	7.750	-0.0008	-0.0008	-0.0008	0.600	0.600	0.571	7.750	-0.0008	-0.0008	-0.0008	0.600	0.600	0.571	7.750	-0.0008	-0.0008	-0.0008	2.39E-04	2.39E-04	2.39E-04	6.75E-04
0.626	23.450	0.756	7.937	-0.0008	-0.0008	-0.0008	0.626	0.626	0.756	7.937	-0.0008	-0.0008	-0.0008	0.626	0.626	0.756	7.937	-0.0008	-0.0008	-0.0008	1.09E-13	1.09E-13	1.09E-13	6.75E-04
0.637	23.961	0.586	7.950	-0.0008	-0.0008	-0.0008	0.637	0.637	0.586	7.950	-0.0008	-0.0008	-0.0008	0.637	0.637	0.586	7.950	-0.0008	-0.0008	-0.0008	6.46E-05	6.46E-05	6.46E-05	8.70E-04
0.648	24.461	1.500	7.950	-0.0007	-0.0007	-0.0007	0.648	0.648	1.500	7.950	-0.0007	-0.0007	-0.0007	0.648	0.648	1.500	7.950	-0.0007	-0.0007	-0.0007	4.15E-04	4.15E-04	4.15E-04	2.15E-03
0.651	25.461	2.000	7.950	-0.0007	-0.0007	-0.0007	0.651	0.651	2.000	7.950	-0.0007	-0.0007	-0.0007	0.651	0.651	2.000	7.950	-0.0007	-0.0007	-0.0007	4.75E-03	4.75E-03	4.75E-03	5.08E-04
0.655	27.461	2.000	7.950	-0.0007	-0.0007	-0.0007	0.655	0.655	2.000	7.950	-0.0007	-0.0007	-0.0007	0.655	0.655	2.000	7.950	-0.0007	-0.0007	-0.0007	2.14E-14	2.14E-14	2.14E-14	1.69E-02
0.658	29.461	2.000	7.950	-0.0007	-0.0007	-0.0007	0.658	0.658	2.000	7.950	-0.0007	-0.0007	-0.0007	0.658	0.658	2.000	7.950	-0.0007	-0.0007	-0.0007	1.63E-03	1.63E-03	1.63E-03	3.9E-02
0.659	31.461	3.180	7.950	-0.0007	-0.0007	-0.0007	0.659	0.659	3.180	7.950	-0.0007	-0.0007	-0.0007	0.659	0.659	3.180	7.950	-0.0007	-0.0007	-0.0007	1.08E-03	1.08E-03	1.08E-03	1.88E-02
0.660	33.461	3.180	7.950	-0.0007	-0.0007	-0.0007	0.660	0.660	3.180	7.950	-0.0007	-0.0007	-0.0007	0.660	0.660	3.180	7.950	-0.0007	-0.0007	-0.0007	3.70E-04	3.70E-04	3.70E-04	3.09E-02
0.664	35.461	2.430	7.950	-0.0006	-0.0006	-0.0006	0.664	0.664	2.430	7.950	-0.0006	-0.0006	-0.0006	0.664	0.664	2.430	7.950	-0.0006	-0.0006	-0.0006	1.22E-02	1.22E-02	1.22E-02	2.90E-02
0.659	36.321	0.500	7.950	-0.0006	-0.0006	-0.0006	0.659	0.659	0.500	7.950	-0.0006	-0.0006	-0.0006	0.659	0.659	0.500	7.950	-0.0006	-0.0006	-0.0006	1.59E-04	1.59E-04	1.59E-04	3.82E-02
0.870	38.321	0.648	7.950	-0.0016	-0.0016	-0.0016	0.870	0.870	0.648	7.950	-0.0016	-0.0016	-0.0016	0.870	0.870	0.648	7.950	-0.0016	-0.0016	-0.0016	2.14E-04	2.14E-04	2.14E-04	2.71E-02
0.868	39.816	0.500	7.950	-0.0014	-0.0014	-0.0014	0.868	0.868	0.500	7.950	-0.0014	-0.0014	-0.0014	0.868	0.868	0.500	7.950	-0.0014	-0.0014	-0.0014	1.02E-05	1.02E-05	1.02E-05	3.85E-03
0.899	40.116	0.648	7.950	-0.0023	-0.0023	-0.0023	0.899	0.899	0.648	7.950	-0.0023	-0.0023	-0.0023	0.899	0.899	0.648	7.950	-0.0023	-0.0023	-0.0023	1.08E-03	1.08E-03	1.08E-03	2.78E-02
0.910	40.616	0.518	7.950	-0.0023	-0.0023	-0.0023	0.910	0.910	0.518	7.950	-0.0023	-0.0023	-0.0023	0.910	0.910	0.518	7.950	-0.0023	-0.0023	-0.0023	6.60E-03	6.60E-03	6.60E-03	2.16E-02
0.922	41.151	0.772	7.875	-0.0008	-0.0008	-0.0008	0.922	0.922	0.772	7.875	-0.0008	-0.0008	-0.0008	0.922	0.922	0.772	7.875	-0.0008	-0.0008	-0.0008	1.60E-04	1.60E-04	1.60E-04	5.63E-02
0.945	42.159	1.043	7.825	-0.0065	-0.0065	-0.0065	0.945	0.945	1.043	7.825	-0.0065	-0.0065	-0.0065	0.945	0.945	1.043	7.825	-0.0065	-0.0065	-0.0065	1.60E-04	1.60E-04	1.60E-04	5.72E-02
0.965	43.236	0.783	7.375	-0.0027	-0.0027	-0.0027	0.965	0.965	0.783	7.375	-0.0027	-0.0027	-0.0027	0.965	0.965	0.783	7.375	-0.0027	-0.0027	-0.0027	4.02E-04	4.02E-04	4.02E-04	5.50E-02
0.980	43.725	0.690	7.250	-0.0014	-0.0014	-0.0014	0.980	0.980	0.690	7.250	-0.0014	-0.0014	-0.0014	0.980	0.980	0.690	7.250	-0.0014	-0.0014	-0.0014	0.00E+00	0.00E+00	0.00E+00	0.00E+00

NORMAL	FORCE COEFFICIENT (NOSE)	MAGNUS	FORCE COEFFICIENT (NOSE)	3.03610E-04
PITCHING	MOMENT COEFFICIENT (NOSE)	MAGNUS	MOMENT COEFFICIENT (NOSE)	0.59618E-04
PITCHING	MOMENT COEFFICIENT (CG)	MAGNUS	MOMENT COEFFICIENT (CG)	1.55499E-04
NORMAL	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE	MAGNUS	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE (NOSE)	1.87382E-03
MOMENT	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE	MAGNUS	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE (NOSE)	1.20458E-03
NORMAL	FORCE COEFFICIENT (NOSE)	MAGNUS	FORCE COEFFICIENT (NOSE)	-4.15853E-03
PITCHING	MOMENT COEFFICIENT (NOSE)	MAGNUS	MOMENT COEFFICIENT (NOSE)	-0.028021873
PITCHING	MOMENT COEFFICIENT (CG)	MAGNUS	MOMENT COEFFICIENT (CG)	0.013433025
NORMAL	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE (CYL)	MAGNUS	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE (CYL)	-0.025655581
MOMENT	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE (CYL)	MAGNUS	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE (CYL)	-0.082905870
NORMAL	FORCE COEFFICIENT (BT)	MAGNUS	FORCE COEFFICIENT (BT)	-5.22627E-03
PITCHING	MOMENT COEFFICIENT (BT)	MAGNUS	MOMENT COEFFICIENT (BT)	-0.024289201
PITCHING	MOMENT COEFFICIENT (CG)	MAGNUS	MOMENT COEFFICIENT (CG)	-0.032274001
NORMAL	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE (BT)	MAGNUS	FORCE COEFFICIENT DERIVATIVE WRT SPIN RATE (BT)	0.0563413805
MOMENT	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE (BT)	MAGNUS	COEFFICIENT (CG) DERIVATIVE WRT SPIN RATE (BT)	0.0563413805

Figure C-8. Rotating Band On,  $\alpha = 0^\circ$ , P = 4900 rpm

REF. LENGTH (L): 44.616 IN.  
 REF. DIAMETER (D): 7.95 IN.  
 ROTATING BAND: 0.34  
 MACH NO.: 10 DEG.  
 ANGLE OF ATTACK (ALPHA): 0 FEV/MIN  
 SPIN RATE (P): 0  
 TIP SPEED RATIO (PD.2M): 0.655112067  
 X CG/L

ZI/L	ZI	DZI	DIA.	CHI	CH	CH	LH	ZI/L	DZI	DIA.	CYI	CY	C7	CM
*****	(IN)	(IN)	(IN)	*****	*****	*****	*****	(IN)	(IN)	(IN)	LOCAL	*****	SUM	*****
0.070	3.123	5.130	2.125	0.0432	0.0432	0.0432	0.070	0.070	3.123	5.130	8.40E-15	8.21E-15	-1.07E-15	3.23E-15
0.160	7.139	4.685	3.112	0.0652	0.0932	0.0652	0.160	0.160	7.139	4.685	-1.17E-13	-1.15E-13	-1.07E-13	-1.00E-13
0.280	12.482	5.354	5.375	0.0830	0.0832	0.0830	0.280	0.280	12.482	5.354	-3.11E-13	-3.07E-13	-4.14E-13	-3.82E-13
0.400	17.846	4.908	6.875	0.0801	0.0750	0.0801	0.400	0.400	17.846	4.908	-1.66E-13	-1.65E-13	-1.78E-13	-1.93E-13
0.500	22.308	2.302	7.718	0.0328	0.0327	0.0328	0.500	0.500	22.308	2.302	8.39E-03	8.37E-03	3.95E-03	1.92E-02
0.550	22.449	0.571	7.750	0.0108	0.0107	0.0108	0.550	0.550	22.449	0.571	-1.22E-13	-1.21E-13	-1.37E-13	-1.37E-13
0.556	23.450	0.160	7.937	0.0038	0.0038	0.0038	0.556	0.556	23.450	0.160	-9.32E-14	-9.31E-14	-1.37E-13	-1.37E-13
0.571	23.961	0.506	7.950	0.0151	0.0150	0.0151	0.571	0.571	23.961	0.506	-1.30E-14	-1.30E-14	-1.37E-13	-1.37E-13
0.578	24.461	1.500	7.950	0.0096	0.0096	0.0096	0.578	0.578	24.461	1.500	-1.50E-05	-1.50E-05	-1.37E-13	-1.37E-13
0.571	25.461	1.500	7.950	0.0072	0.0072	0.0072	0.571	0.571	25.461	1.500	-1.39E-14	-1.39E-14	-1.37E-13	-1.37E-13
0.615	27.461	2.000	7.950	-0.0243	-0.0243	-0.0243	0.615	0.615	27.461	2.000	-2.34E-14	-2.34E-14	-2.97E-05	-2.97E-05
0.660	29.461	2.000	7.950	-0.0084	-0.0084	-0.0084	0.660	0.660	29.461	2.000	-8.90E-15	-8.90E-15	-2.97E-05	-2.97E-05
0.705	31.461	2.000	7.950	-0.0004	-0.0004	-0.0004	0.705	0.705	31.461	2.000	-3.95E-04	-3.95E-04	-3.55E-04	-3.55E-04
0.750	33.461	3.180	7.950	0.0060	0.0060	0.0060	0.750	0.750	33.461	3.180	-7.80E-04	-7.80E-04	-6.26E-03	-6.26E-03
0.808	37.821	2.430	7.950	-0.0142	-0.0142	-0.0142	0.808	0.808	37.821	2.430	-3.95E-04	-3.95E-04	-6.26E-03	-6.26E-03
0.857	38.321	0.500	7.950	0.0076	0.0076	0.0076	0.857	0.857	38.321	0.500	1.44E-03	1.44E-03	-5.21E-03	-5.21E-03
0.868	38.321	0.548	7.950	0.0140	0.0140	0.0140	0.868	0.868	38.321	0.548	1.61E-03	1.61E-03	-5.21E-03	-5.21E-03
0.899	40.116	0.500	7.950	0.0025	0.0025	0.0025	0.899	0.899	40.116	0.500	1.70E-03	1.70E-03	-4.88E-03	-4.88E-03
0.910	40.616	0.518	7.950	0.0025	0.0025	0.0025	0.910	0.910	40.616	0.518	1.23E-03	1.23E-03	-3.17E-03	-3.17E-03
0.922	41.151	0.772	7.950	-0.0035	-0.0035	-0.0035	0.922	0.922	41.151	0.772	-1.08E-03	-1.08E-03	-2.99E-03	-2.99E-03
0.945	42.159	1.043	7.950	-0.0036	-0.0036	-0.0036	0.945	0.945	42.159	1.043	-1.88E-03	-1.88E-03	-4.85E-03	-4.85E-03
0.969	43.236	0.783	7.950	-0.0347	-0.0347	-0.0347	0.969	0.969	43.236	0.783	-1.90E-03	-1.90E-03	-4.85E-03	-4.85E-03
0.980	43.735	0.690	7.950	-0.0311	-0.0311	-0.0311	0.980	0.980	43.735	0.690	-8.37E-04	-8.37E-04	-7.62E-03	-7.62E-03

NORMAL	FORCE COEFFICIENT (NOSE)	== 7.61633E-03
PITCHING	MOMENT COEFFICIENT (NOSE)	== -0.038172328
PITCHING	MOMENT COEFFICIENT (CG)	== 0.011453891
NORMAL	FORCE COEFFICIENT (NOSE)	== -0.043638374
PITCHING	MOMENT COEFFICIENT (CG)	== 0.055625561
NORMAL	FORCE COEFFICIENT (NOSE)	== 1.37064E-05
PITCHING	MOMENT COEFFICIENT (NOSE)	== 3.87037E-05
NORMAL	FORCE COEFFICIENT (CG)	== 9.38667E-06
PITCHING	MOMENT COEFFICIENT (CG)	== 7.85317E-05
NORMAL	FORCE COEFFICIENT (NOSE)	== 5.37473E-05
PITCHING	MOMENT COEFFICIENT (NOSE)	== 1.95856E-03
NORMAL	FORCE COEFFICIENT (CG)	== 6.8068E-03
PITCHING	MOMENT COEFFICIENT (CG)	== 0.01232730
NORMAL	FORCE COEFFICIENT (NOSE)	== 5.55199E-03
PITCHING	MOMENT COEFFICIENT (NOSE)	== -5.67148E-03
NORMAL	FORCE COEFFICIENT (CG)	== -0.030372055
PITCHING	MOMENT COEFFICIENT (CG)	== 0.010475506
NORMAL	FORCE COEFFICIENT (NOSE)	== -0.032495136
PITCHING	MOMENT COEFFICIENT (NOSE)	== 0.0660820236

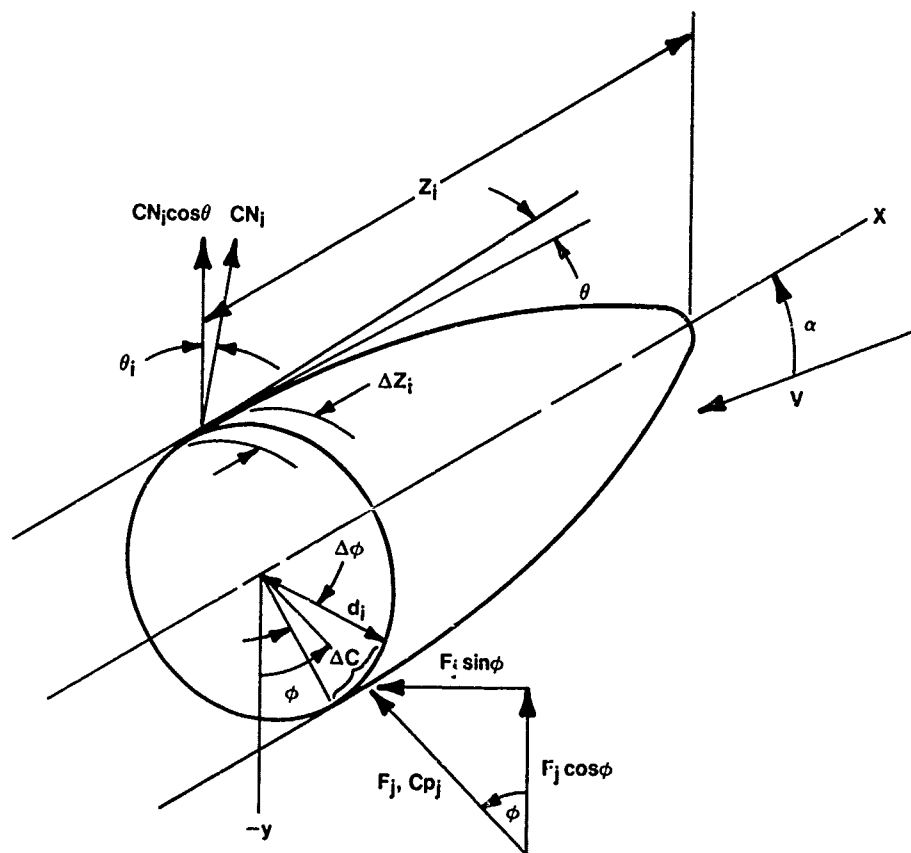
Figure C-9. Rotating Band On,  $\alpha = 10^\circ$ ,  $P = 0^\circ$  rpm





The following are derivations of selected data reduction terms included in Appendix C.

1. Derivation of Local Force and Moment Coefficient:



At pressure tap location  $Z_i$ :  $\Delta P_j = C_{p_j} q$

$$F_j = C_{p_j} q S_j$$

$$q = \frac{\rho v^2}{2}$$

$$S_j = \Delta C \Delta Z_i$$

$$\Delta C = \frac{d_i}{2} \sin \Delta \phi$$

$$S_j = \frac{d_i}{2} \Delta Z_i \sin \Delta \phi$$

$$F_j = C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta \phi$$

$$N_i = \sum_{j=1}^{360/\Delta\phi} F_j \cos \phi_j$$

$$N_i = \sum_{j=1}^{360/\Delta\phi} C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta\phi \cos \phi_j$$

$$C_{N_i} = \frac{N_i}{qs}$$

$$s = \frac{\pi d^2}{4}$$

$$C_{N_i} = \sum_{j=1}^{360/\Delta\phi} 2 C_{p_j} \frac{d_i \Delta Z_i \sin \Delta\phi \cos \phi_j}{\pi d^2}$$

$$C_{N_i} = \frac{2 d_i \Delta Z_i \sin \Delta\phi}{\pi d^2} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \cos \phi_j$$

similarly:

$$C_{y_i} = \frac{2 d_i \Delta Z_i \sin \Delta\phi}{\pi d^2} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \sin \phi_j$$

$$\Delta\phi = 10^\circ$$

$$j = 1 \longrightarrow 36$$

$$C_N = \sum_{i=1}^{27} C_{N_i} \Delta Z_i \cos \theta_i$$

For this report,  $i = 1 \longrightarrow 27$  includes data from the 19 tap locations used in the Ames test model, plus data from 8 ogive locations obtained in reference 7.

where:

$$\Delta Z_i = \frac{Z_{i+1} - Z_i}{2} + \frac{Z_i - Z_{i-1}}{2}$$

$$\Delta Z_i = \frac{Z_{i+1} - Z_{i-1}}{2}$$

$$\textcircled{0} \quad Z_i = 1 \quad Z_{i-1} = L - Z_{i-1}$$

$$\textcircled{0} \quad Z_i = 27 \quad Z_{i+1} = L$$

similarly:

$$C_y = \sum_{i=1}^{27} C_{y_i} \Delta Z_i \cos \theta$$

$$M_i = N_i Z_i$$

$$M_i = \sum_{j=1}^{360/\Delta\phi} F_j Z_i \cos \phi_j$$

$$M_i = \sum_{j=1}^{360/\Delta\phi} C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta\phi Z_i \cos \phi_j$$

$$C_{m_i} = \frac{M_i}{qsd}$$

$$S = \frac{\pi d^2}{4}$$

$$C_{m_i} = \sum_{j=1}^{360/\Delta\phi} \frac{2 C_{p_j} d_i \Delta Z_i Z_i \sin \Delta\phi \cos \phi_j}{\pi d^3}$$

$$C_{m_i} = \frac{2 d_i \Delta Z_i Z_i \sin \Delta\phi}{\pi d^3} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \cos \phi_j$$

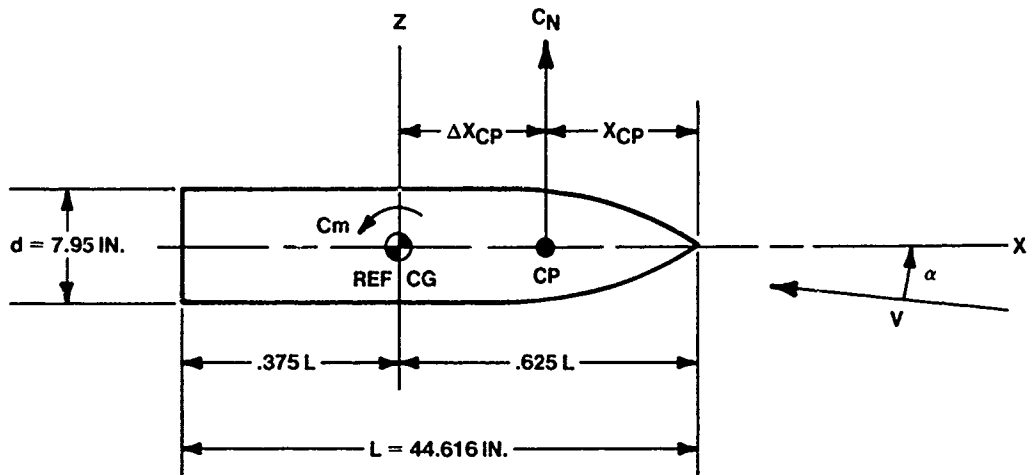
similarly:

$$C_{n_i} = \frac{2 d_i \Delta Z_i Z_i \sin \Delta\phi}{\pi d^3} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \sin \phi_j$$

$$C_{m_{\text{nose}}} = \sum_{i=1}^{27} C_{m_i} \Delta Z_i$$

$$C_{n_{\text{nose}}} = \sum_{i=1}^{27} C_{n_i} \Delta Z_i$$

2. Derivation of Normal Force and Magnus Force Centers of Pressure Locations:



$$X_{cp} + \Delta X_{cp} = .625L$$

$$\frac{X_{cp}}{L} + \frac{\Delta X_{cp}}{L} = .625$$

$$\frac{X_{cp}}{L} + \frac{\Delta X_{cp}}{L} \frac{d}{L} = .625$$

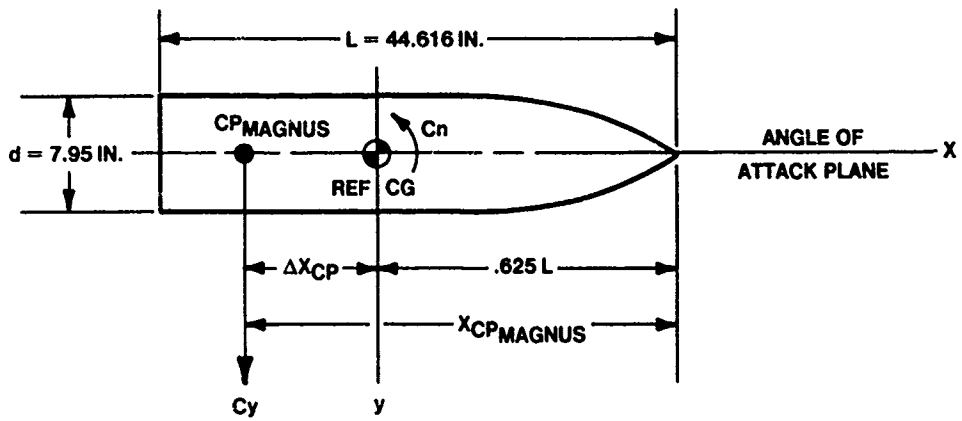
$$\frac{X_{cp}}{L} = .625 - \frac{d}{L} \frac{\Delta X_{cp}}{d}$$

$$\frac{\Delta X_{cp}}{d} = \frac{C_{m\alpha}}{C_{N\alpha}}$$

$$\frac{X_{cp}}{L} = .625 - \frac{7.95}{44.616} \frac{C_{m\alpha}}{C_{N\alpha}}$$

$$\frac{X_{cp}}{L} = .625 - .1782 \frac{C_{m\alpha}}{C_{N\alpha}}$$





$$x_{cp\text{MAGNUS}} = \Delta x_{cp\text{MAGNUS}} + .625L$$

$$\frac{x_{cp\text{MAGNUS}}}{L} = \frac{\Delta x_{cp\text{MAGNUS}}}{L} + .625$$

$$\frac{x_{cp\text{MAGNUS}}}{L} = \frac{\Delta x_{cp\text{MAGNUS}}}{L} \cdot \frac{d}{L} + .625$$

$$\frac{x_{cp\text{MAGNUS}}}{L} = .1782 \frac{\Delta x_{cp\text{MAGNUS}}}{d} + .625$$

$$\frac{\Delta x_{cp\text{MAGNUS}}}{d} = \frac{C_{n_p}}{C_{y_p}}$$

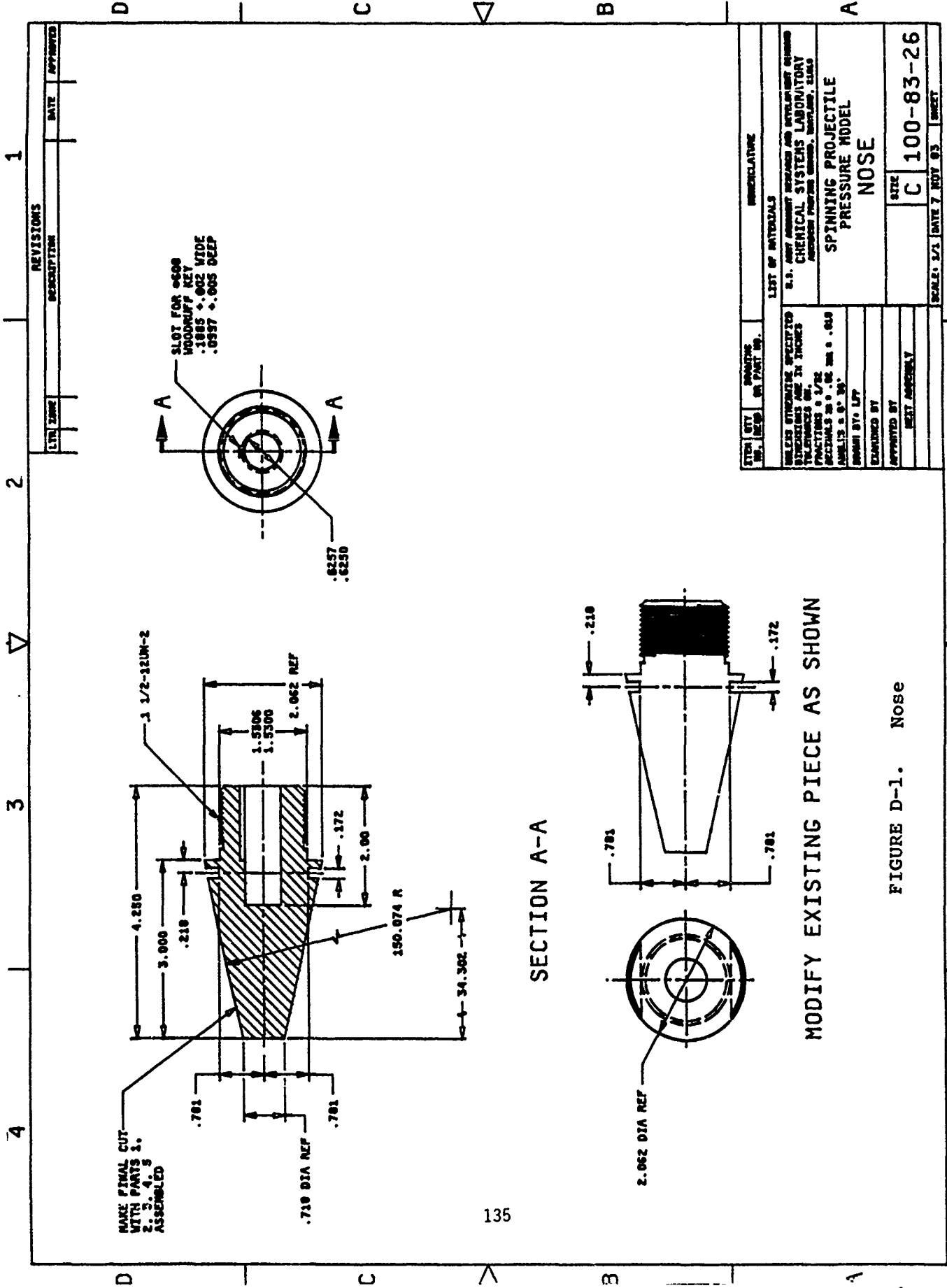
$$\frac{x_{cp\text{MAGNUS}}}{L} = .625 + .1782 \frac{C_{n_p}}{C_{y_p}}$$

APPENDIX D  
ENGINEERING DRAWINGS OF WIND  
TUNNEL MODEL COMPONENTS

Appendix D contains the engineering drawings of the model and sting components, including an assembly drawing.

Figure

- D-1     Nose
- D-2     Junction Ring
- D-3     Forward Bearing Lock Ring
- D-4     Aft Bearing Lock Ring
- D-5     Drive Shaft
- D-6     Armature Adapter Lock Nut
- D-7     Motor Drive Adapter
- D-8     Motor Lock Screw
- D-9     Strut Nut
- D-10    Core/Sting Lock Pin
- D-11    Forward Ogive
- D-12    Tail Section, Version A (Rotating Band Off)
- D-13    Forward Core Motor/Bearing Support Section
- D-14    Strut
- D-15    Aft Core Section
- D-16    Spinning Projectile Pressure Model Assembly
- D-17    Mid Section
- D-18    Tail Section, Version B (Rotating Band On)
- D-19    Main Core Section (View 1)
- D-20    Main Core Section (View 2)



MAKE FINAL CUT  
WITH PARTS 1,  
2, 3, 4, 5  
ASSEMBLED

SLOT FOR #608  
WOODRUFF KEY  
.1885 ± .002 WIDE  
.0537 ± .005 DEEP

SECTION A-A

MODIFY EXISTING PIECE AS SHOWN

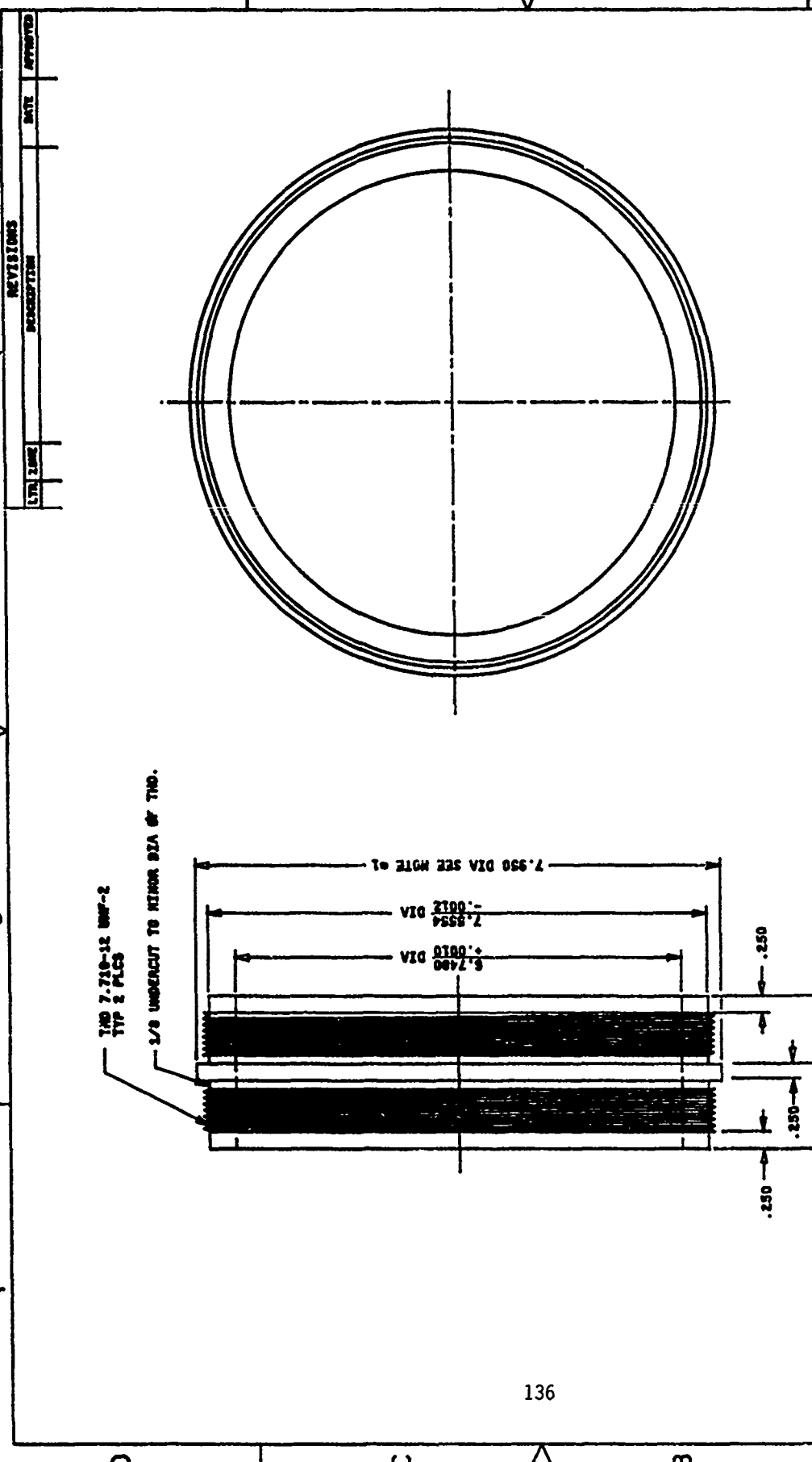
FIGURE D-1. Nose

REVISONS		DATE	APPROVED
LTN	ZONE	DESCRIPTION	

ITEM	QTY	ISSUING	OR PART NO.	DESCRIPTION
LIST OF MATERIALS				
U.S. GOVT. PROPERTY - REPRODUCED AND DISTRIBUTION LIMITED				
CHEMICAL SYSTEMS LABORATORY				
AMERICAN PHARMACEUTICAL COMPANY, NEW YORK, N.Y.				
SPINNING PROJECTILE				
PRESSURE MODEL				
NOSE				
DRAWN BY: LPT				
EXAMINED BY:				
APPROVED BY:				
BEST ASSEMBLY				
SCALE: 3/4"		DATE: 7 NOV 63		SHEET
				1

1 2 3 4



REV. NO.	DESCRIPTION	DATE	APPROVED
1			

ITEM NO.	QTY	DESCRIPTION	UNIT
1	1	JUNCTION RING	EA

LIST OF MATERIALS
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES
TOLERANCES ARE:
FRACTIONS ± 0.005
DECIMALS ± 0.010
ANGLES ± 0.5°
DRAWN BY: CWM
CHECKED BY:
APPROVED BY:
TEST ASSEMBLY:

SCALE	DATE	SHEET
100-83-29	7 NOV 83	1

NOTE  
3-FINISH O.D. WITH PARTS 1,2,3,4 AND 5 ASSEMBLED.

FIGURE D-2. Junction Ring

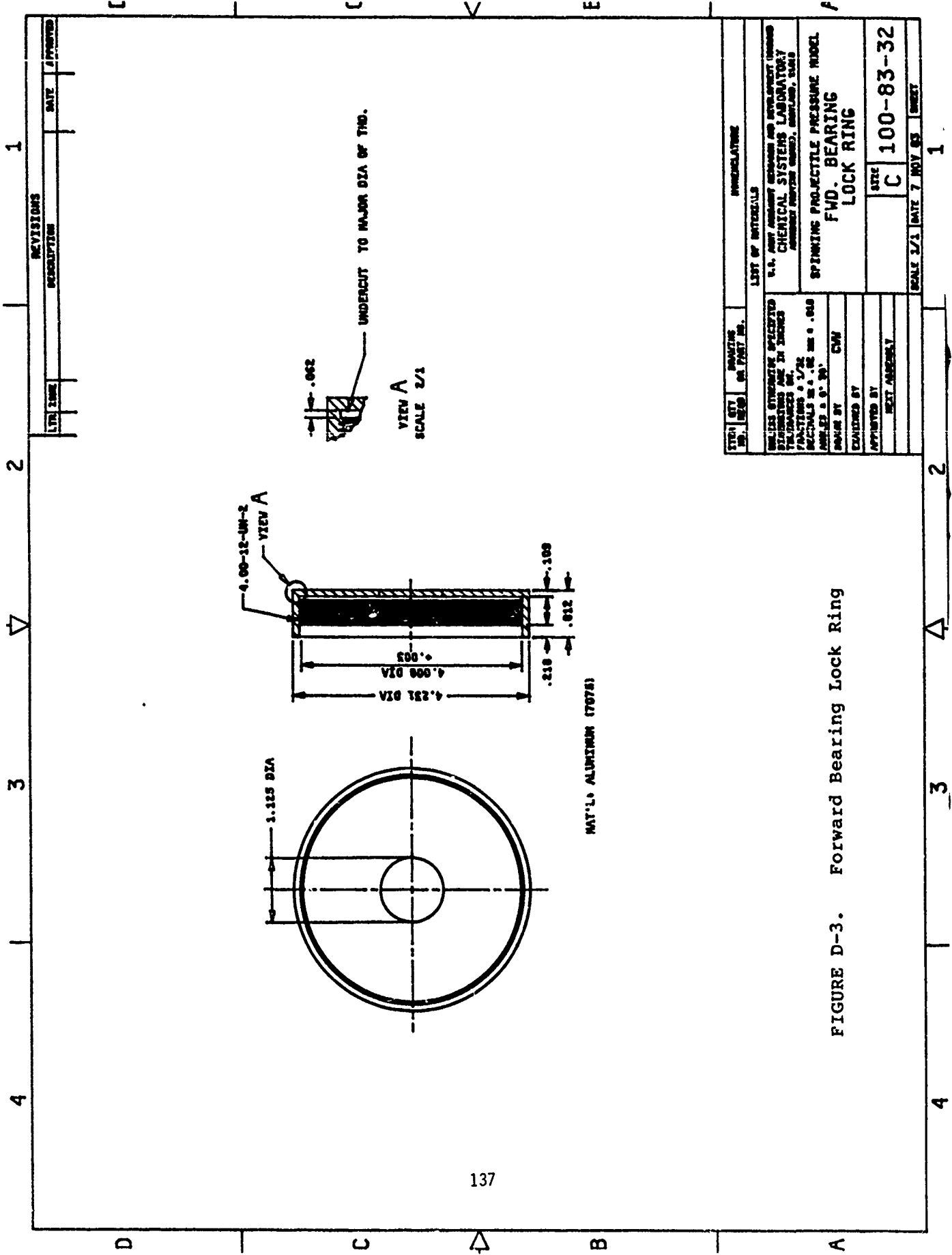
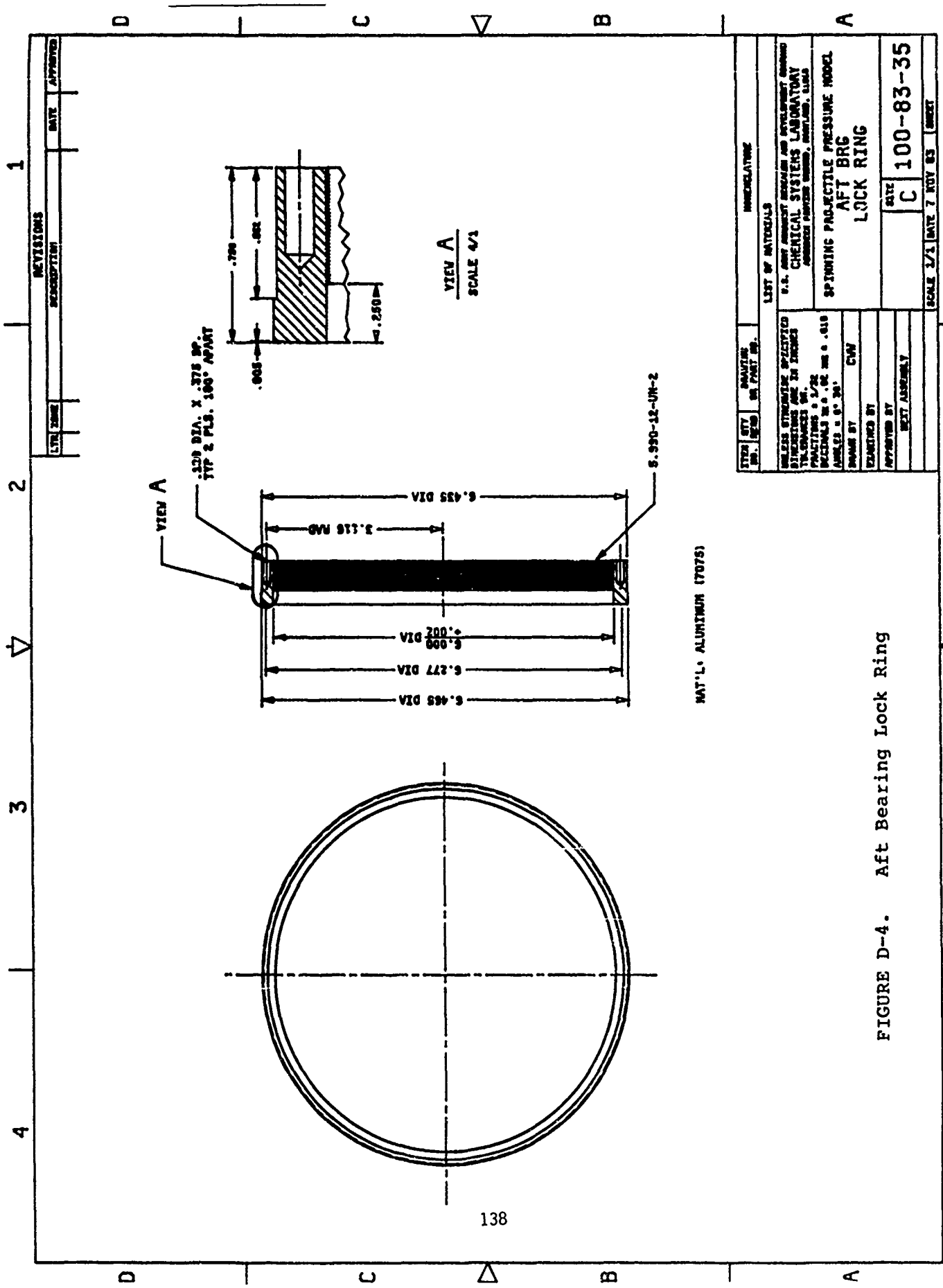


FIGURE D-3. Forward Bearing Lock Ring

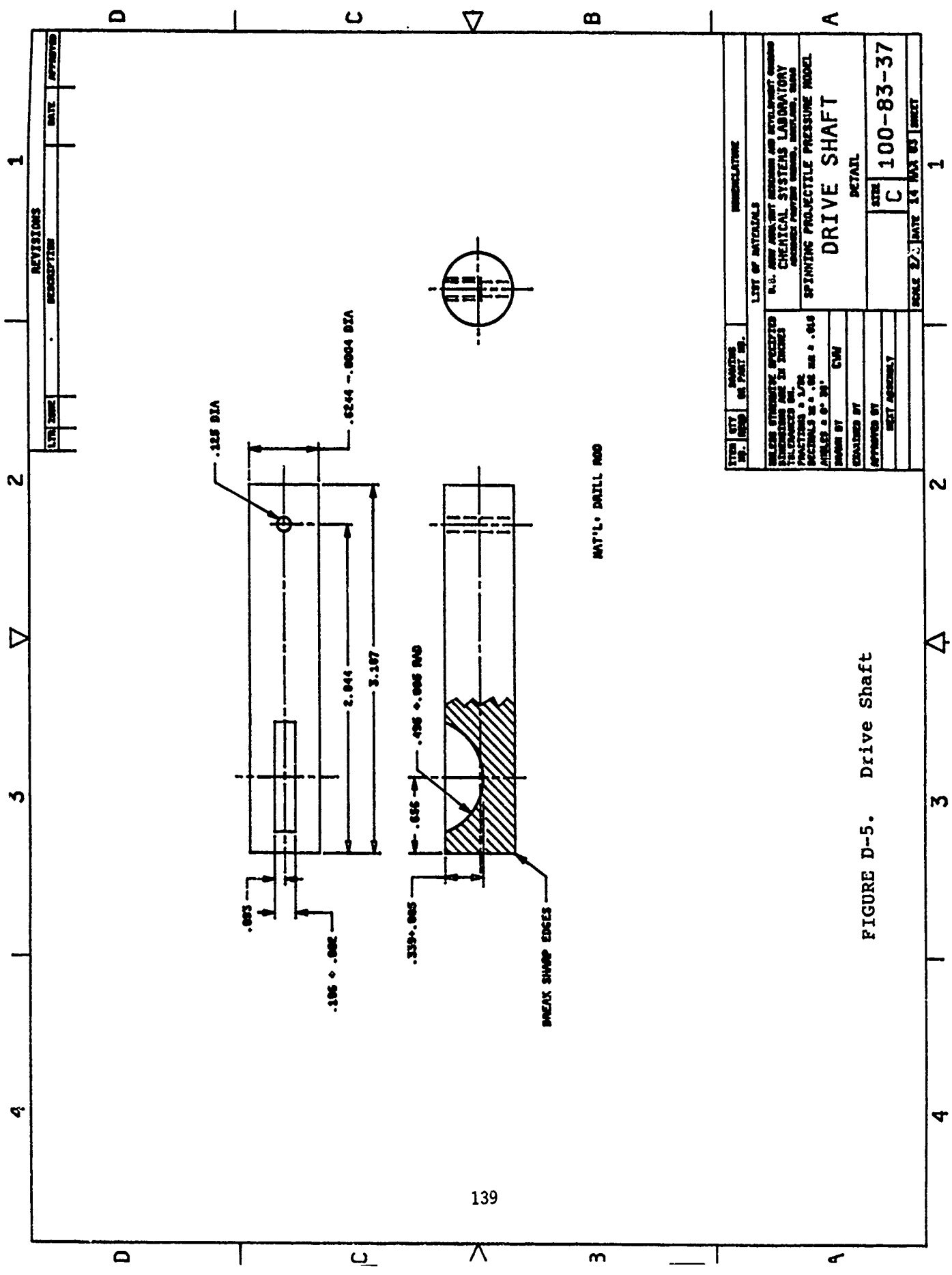
STRY	QTY	DRAWING	SYMBOLS
NO.	REQD	OR PART NO.	SYMBOLS
LIST OF INTERCHANGES			
U.S. GOVT WORKING DRAWING AND INSTRUMENT NUMBER CHEMICAL SYSTEMS LABORATORY ARMY RESEARCH OFFICE (Durham), DURHAM, N.C.			
SPINNING PROJECTILE PRESSURE MODEL FWD. BEARING LOCK RING			
SCALE 3/1			DATE 7 NOV 63
SHEET 1/1			SHEET



REVISIONS	
DATE	APPROVED
DESCRIPTION	
LTR. NO.	

ITEM NO.	QTY	DESCRIPTION	UNIT
<b>LIST OF MATERIALS</b> U.S. AIR FORCE AMMUNITION RESEARCH AND DEVELOPMENT DIVISION CHEMICAL SYSTEMS LABORATORY CHEMICAL SYSTEMS DIVISION, WRIGHT-PATTERSON AIR FORCE BASE, OHIO			
SPINNING PROJECTILE PRESSURE MODEL AFT BRG LOCK RING			
DESIGNED BY	CWJ	DATE	C
EXAMINED BY		SCALE	3/2
APPROVED BY		DATE	7 NOV 83
NEXT ASSEMBLY			
SCALE 3/2			1

FIGURE D-4. Aft Bearing Lock Ring



TITLE	CITY	STATE	DATE
DRIVE SHAFT			
LIST OF MATERIALS			
U.S. ARMY AMMUNITION RESEARCH AND DEVELOPMENT CENTER CHEMICAL SYSTEMS LABORATORY GENERAL PROJECT NUMBER: BAC100, SUBNO			
SPINNING PROJECTILE PRESSURE MODEL			
DRIVE SHAFT			
DETAIL			
SIZE	C	DATE	100-83-37
SCALE	2:1	DATE	14 MAR 83
SHEET 1 OF 1			

FIGURE D-5. Drive Shaft

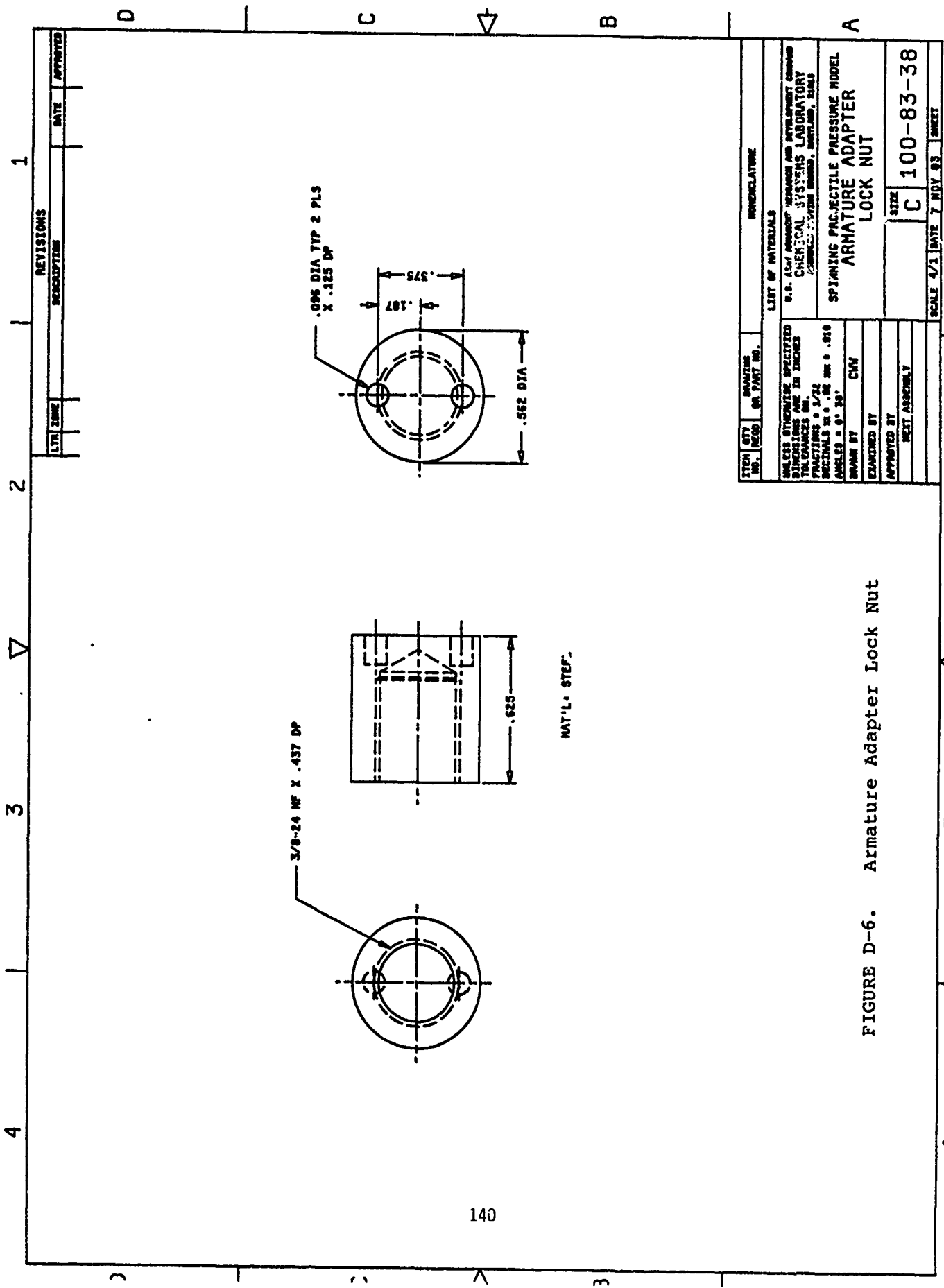


FIGURE D-6. Armature Adapter Lock Nut

REVISIONS	
DATE	APPROVED

ITEM NO.	QTY	REMARKS OR PART NO.	INVENTORY
LIST OF MATERIALS			
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES			
TOLERANCES ARE:			
FRACTIONS ± 1/32			
DECIMALS ± 0.005			
ANGLES ± 0.30°			
DRAWN BY CW			
EXAMINED BY			
APPROVED BY			
BEST ASSEMBLY			
SCALE 4/1			DATE 7 NOV 83
SIZE C			100-83-38
SHEET 7			TOTAL SHEETS 1



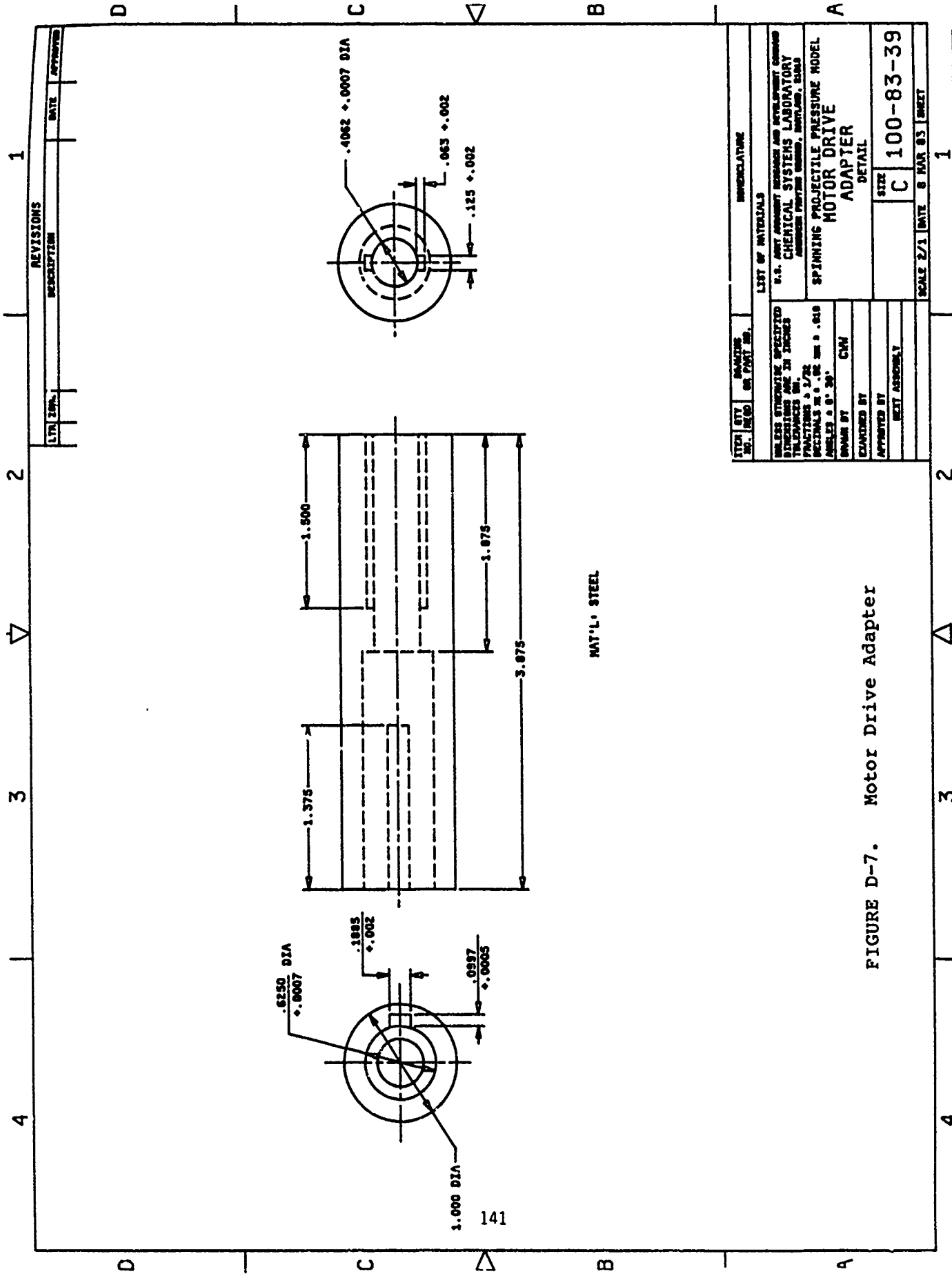
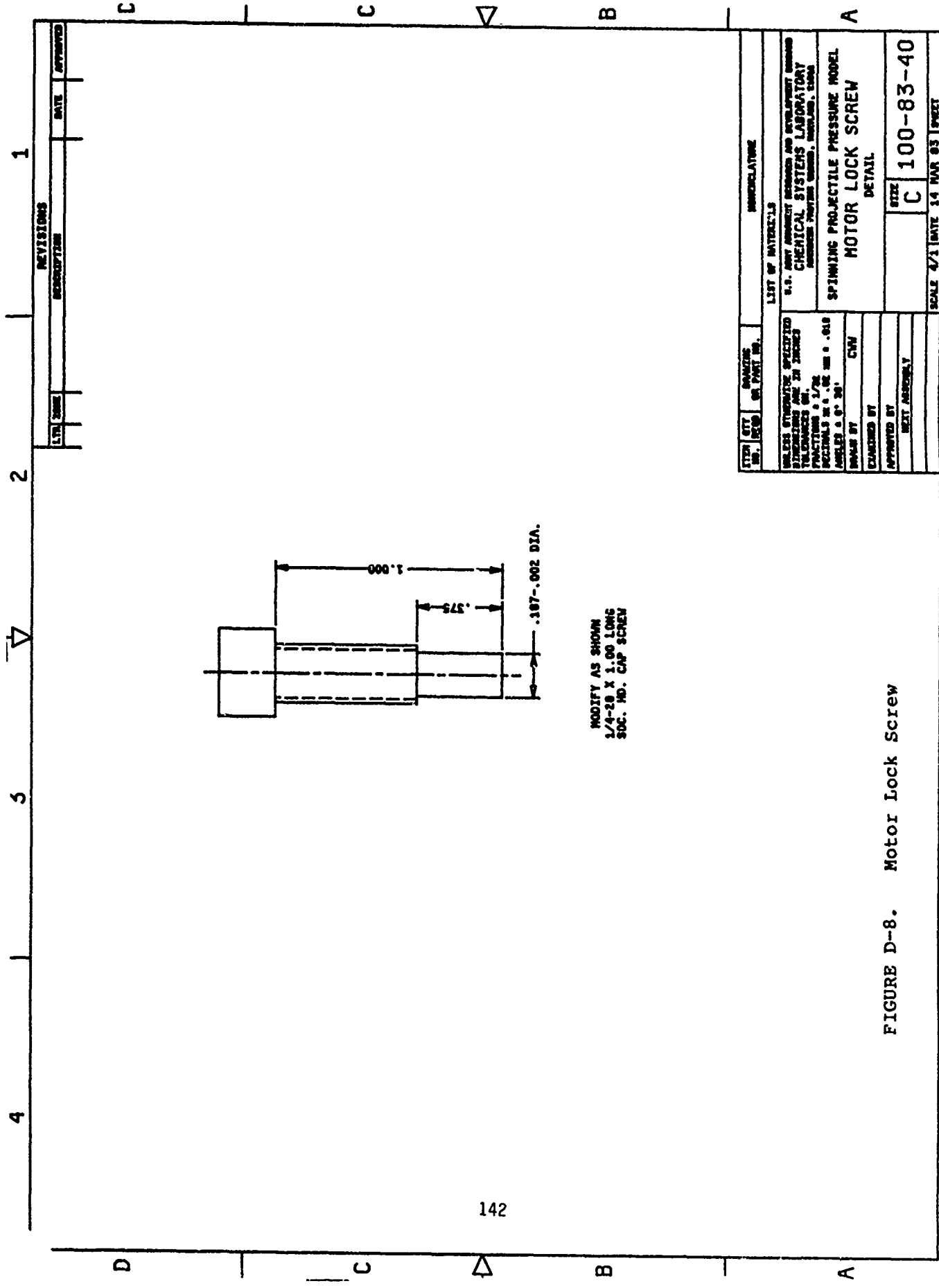


FIGURE D-7. Motor Drive Adapter



MODIFY AS SHOWN  
 1/4-28 X 1.00 LONG  
 SOC. HD. CAP SCREW

FIGURE D-8. Motor Lock Screw

REVISIONS	
NO.	DATE

ITEM NO.	QUANTITY	DESCRIPTION
LIST OF MATERIALS		
U.S. ARMY AMMUNITION RESEARCH AND DEVELOPMENT CENTER CHEMICAL SYSTEMS LABORATORY 3715 BRADLEY ROAD, FORT MONROE, VIRGINIA 22034		
SPINNING PROJECTILE PRESSURE MODEL		
MOTOR LOCK SCREW		
DETAIL		
APPROVED BY	DATE	SCALE
		1:1
		14 MAR 83
		1 SHEET

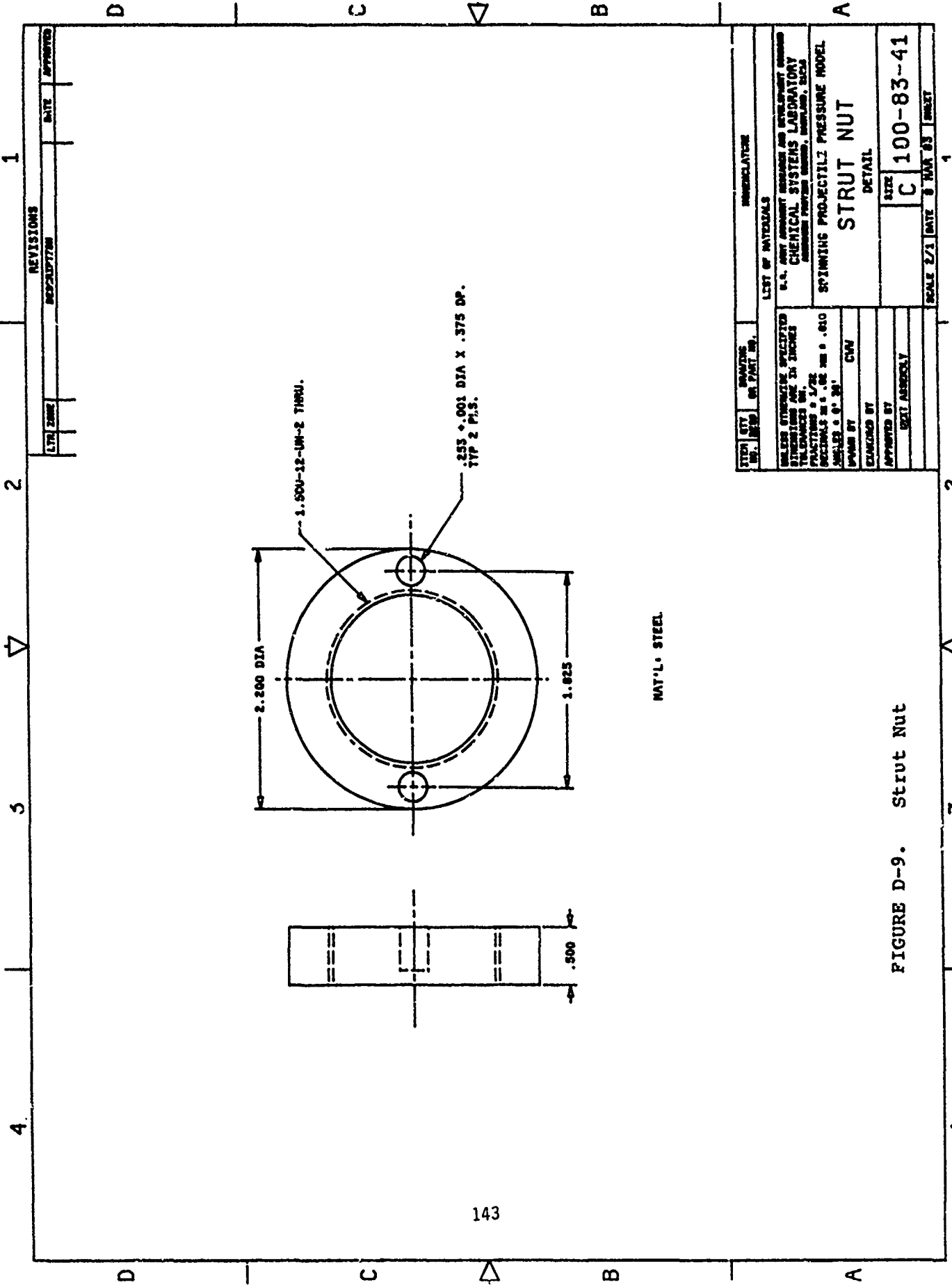


FIGURE D-9. Strut Nut

REVISIONS		DATE	APPROVED
1	INITIALS		
2			
3			
4			
5			

STEP	QTY	REMARKS	INTEGRATOR
1	1	OR PART NO.	
LIST OF MATERIALS			
UNLESS OTHERWISE SPECIFIED TOLERANCES ARE IN INCHES			
U.S. ARMY ARMY AIR FORCE AND DEVELOPMENT ENGINEERING			
CHEMICAL SYSTEMS LABORATORY			
AMMUNITION PROOFING CENTER, WASHINGTON, D.C.			
SPRINTING PROJECTILE PRESSURE MODEL			
STRUT NUT			
DETAIL			
DRAWN BY			SIZE
CHECKED BY			C
APPROVED BY			SCALE
DATE			8 MAR 83
SHEET			1

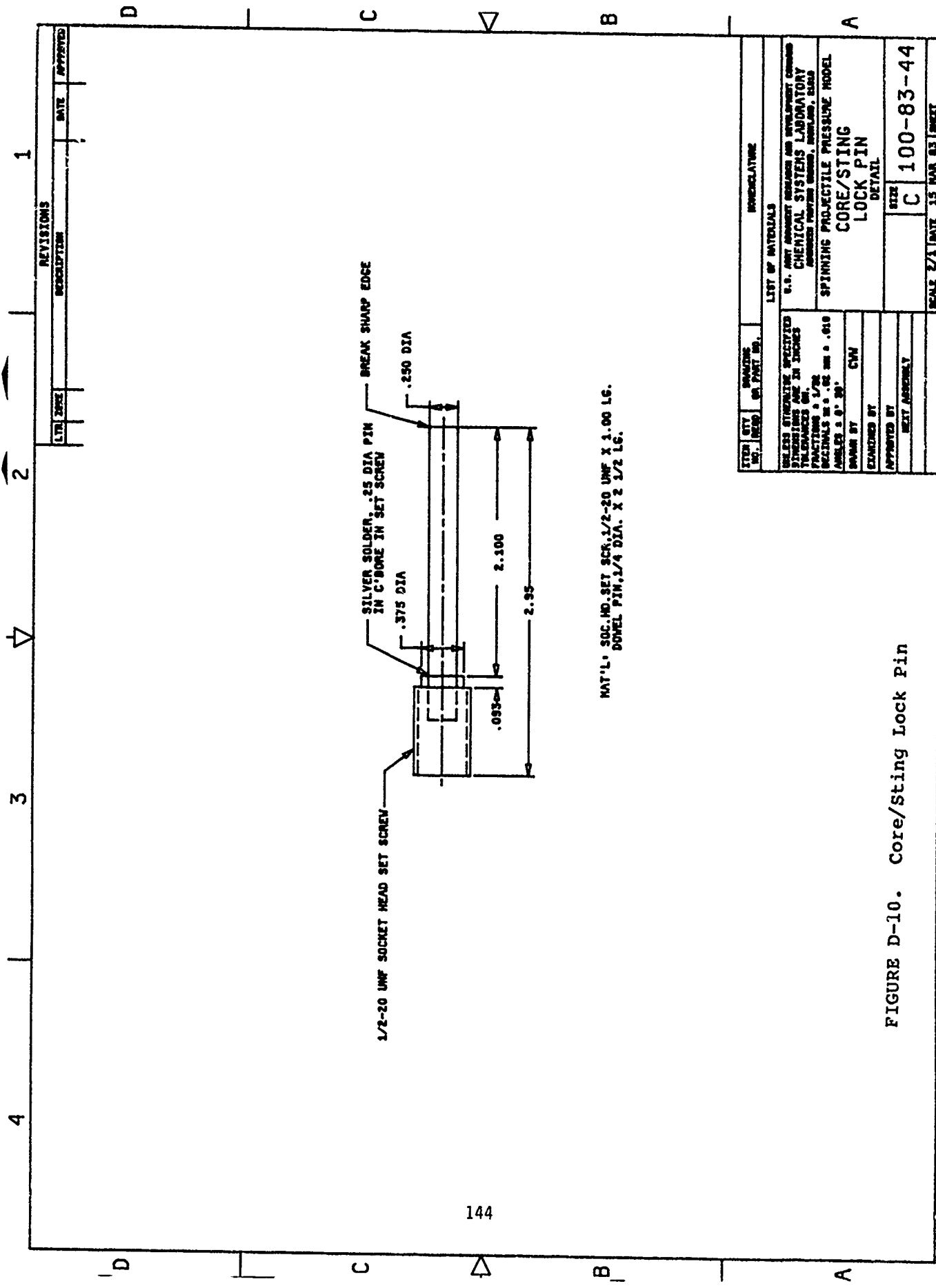


FIGURE D-10. Core/Sting Lock Pin

REVISIONS		DATE	APPROVED
1	REVISED		

ITER NO.	QTY REQD	ISSUES ON PART NO.	DESCRIPTION
LIST OF MATERIALS			
U.S. ARMY SPECIFIED SPECIFICATIONS IN INCHES TOLERANCES UNLESS OTHERWISE SPECIFIED FRACTIONS 1/2 DECIMALS TO 2 DECIMALS ANGLES 5, 10, 30			
U.S. ARMY ARMBRST RESERVE AND DEVELOPMENT COMMAND CHEMICAL SYSTEMS LABORATORY ARMBRST PROJECTS BRANCH, BETHLEHEM, PA			
SPINNING PROJECTILE PRESSURE MODEL			
CORE/STING LOCK PIN			
DETAIL			
DRAWN BY			CHK
EXAMINED BY			
APPROVED BY			
BEST ASSEMBLY			
SIZE			C
100-83-44			
SCALE 2/1 (DATE 15 MAR 83) SHEET			

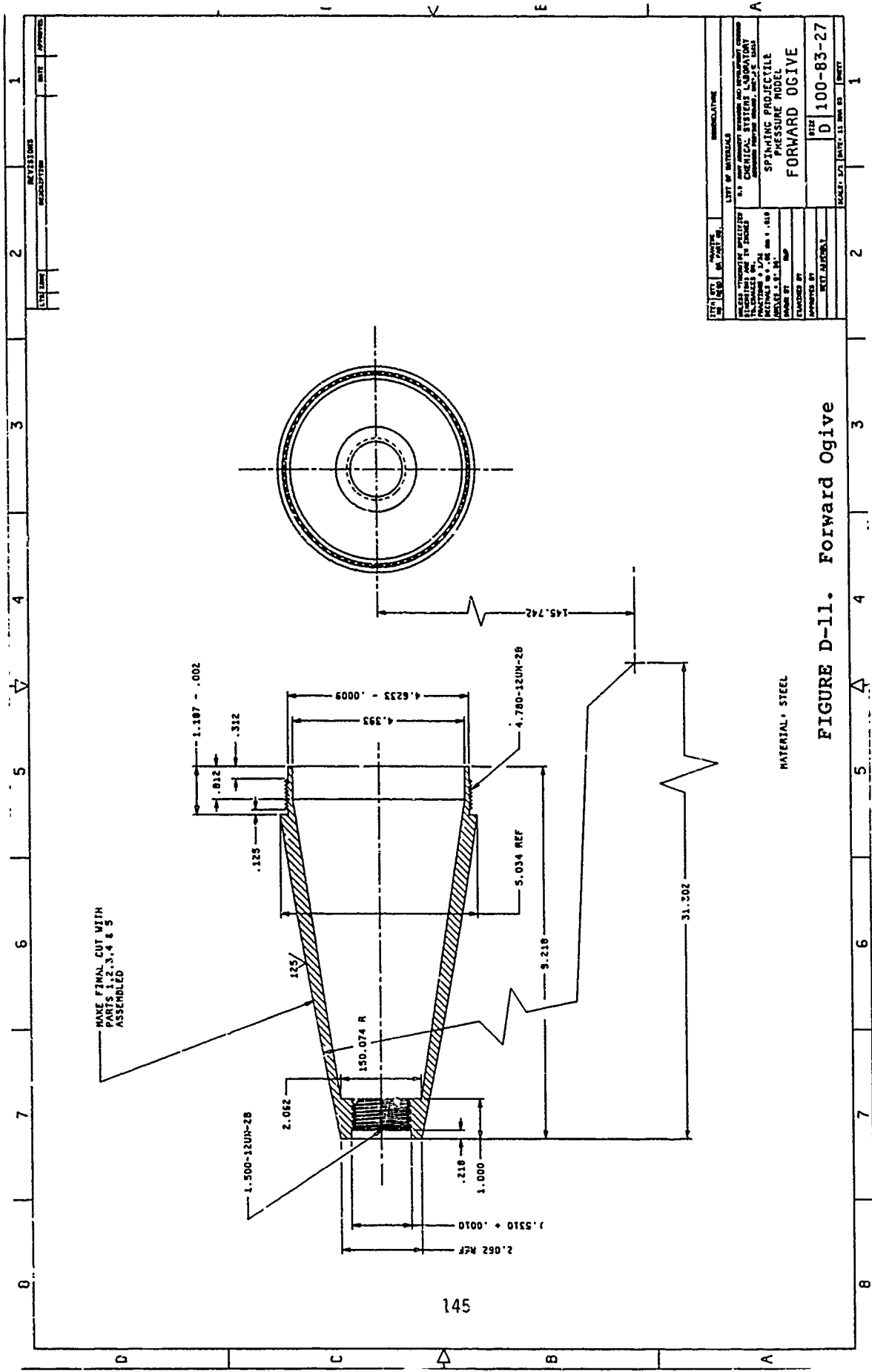


FIGURE D-11. Forward Ogive

ITEM NO.	QUANTITY	DESCRIPTION
1	1	FORWARD OGI

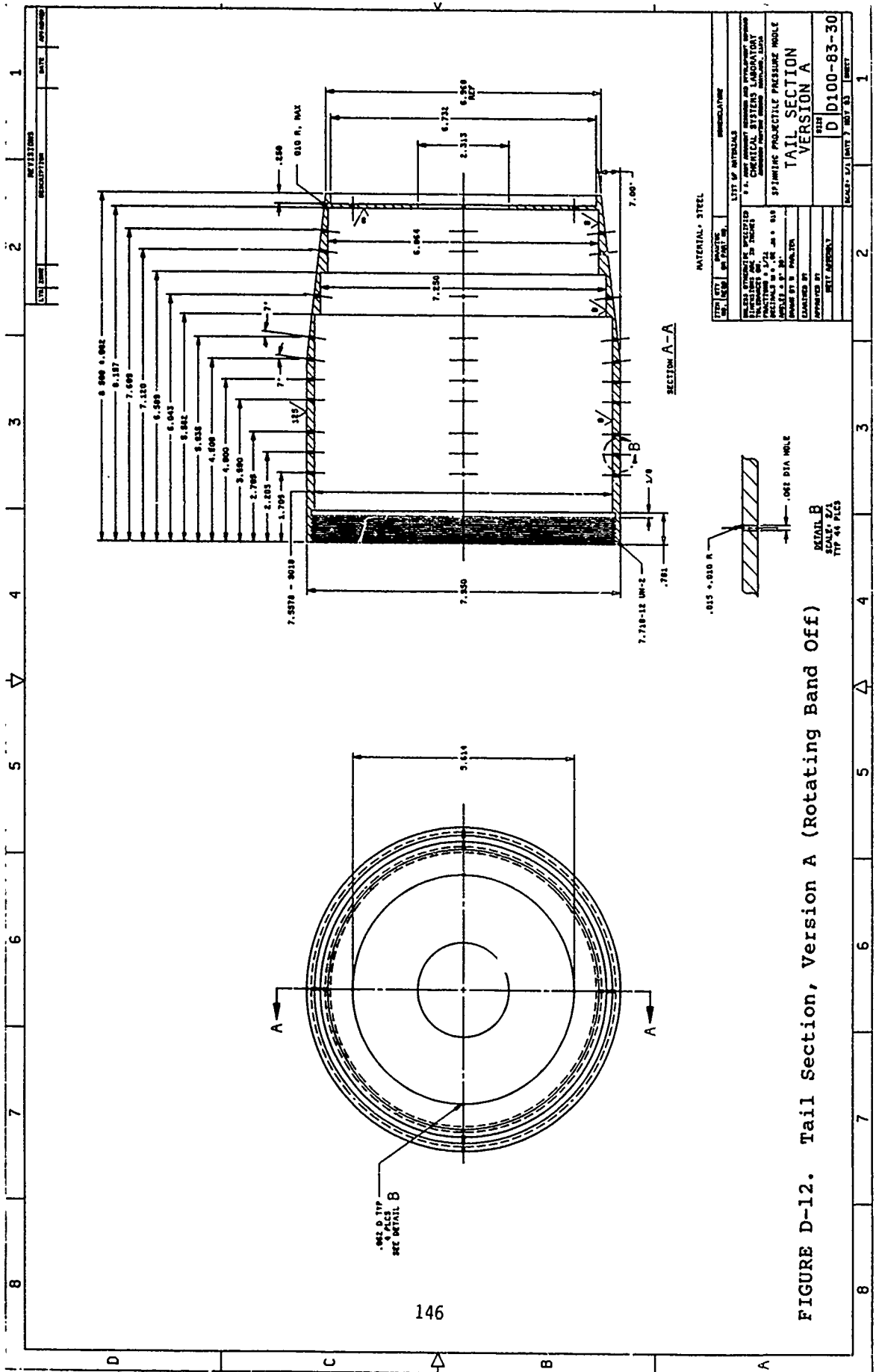
LIST OF MATERIALS	DESCRIPTION
1	STEEL

DESIGNED BY	DATE
APPROVED BY	DATE

PROJECT NO.	DATE	REV.	BY
100-83-27	11 MAR 63	D	1



MATERIAL - STEEL	
ITEM NO.	DESCRIPTION
1	STEEL
2	STEEL
3	STEEL
4	STEEL
5	STEEL
6	STEEL
7	STEEL
8	STEEL
LIST OF MATERIALS	
1. U.S. ARMY CORP. AND AFFILIATED ORGANIZATIONS 2. U.S. CHEMICAL SYSTEMS LABORATORY 3. U.S. AIR FORCE 4. U.S. NAVY 5. U.S. MARINE CORPS 6. U.S. COAST AND GEODETIC SURVEY 7. U.S. AIR FORCE 8. U.S. ARMY CORP. AND AFFILIATED ORGANIZATIONS 9. U.S. NAVY 10. U.S. MARINE CORPS 11. U.S. AIR FORCE 12. U.S. COAST AND GEODETIC SURVEY	
TAIL SECTION VERSION A	
SCALE: 1/2"	DATE: 7 1957 43
FIG. NO. D100-83-30	SHEET 1

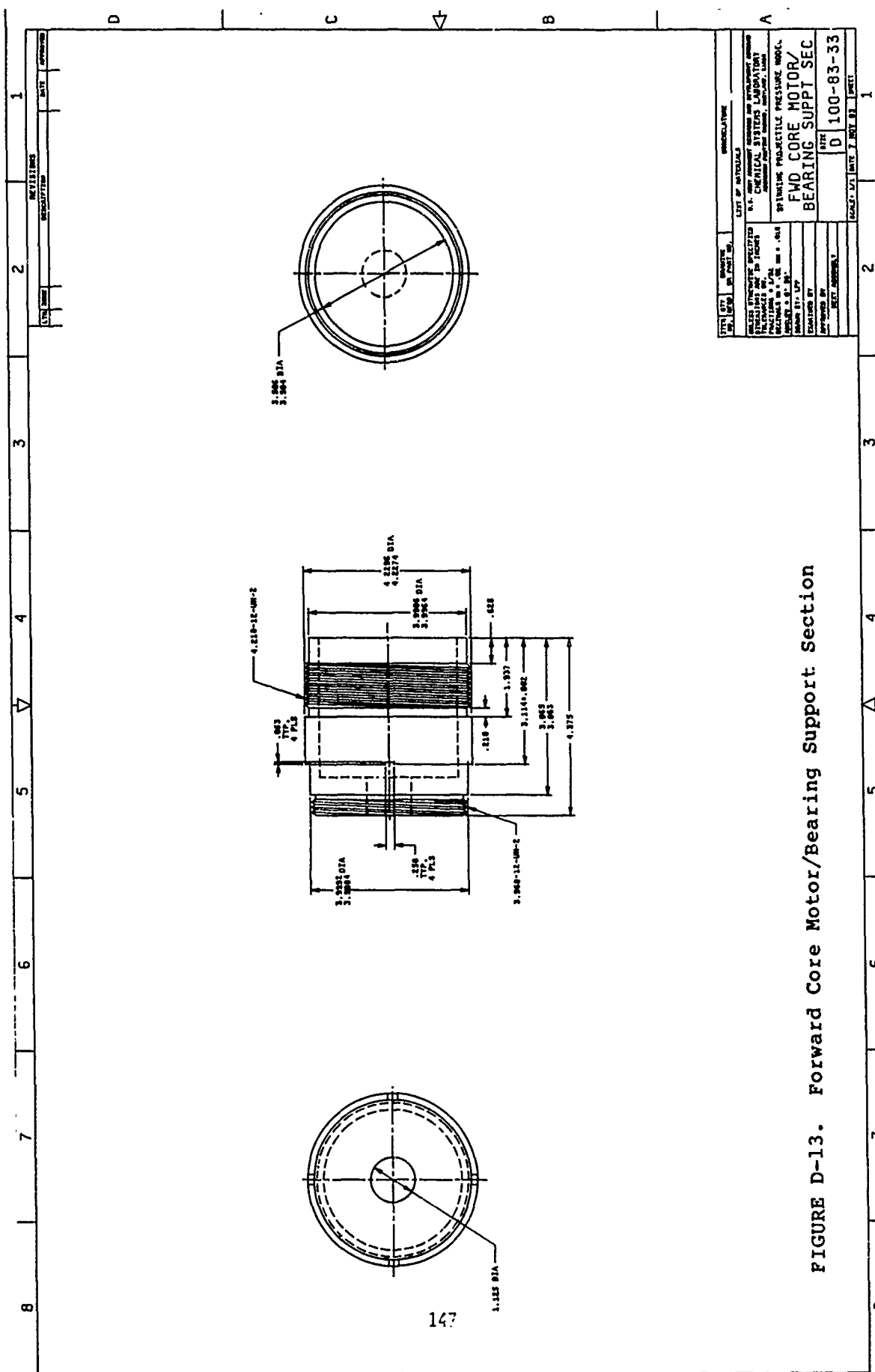
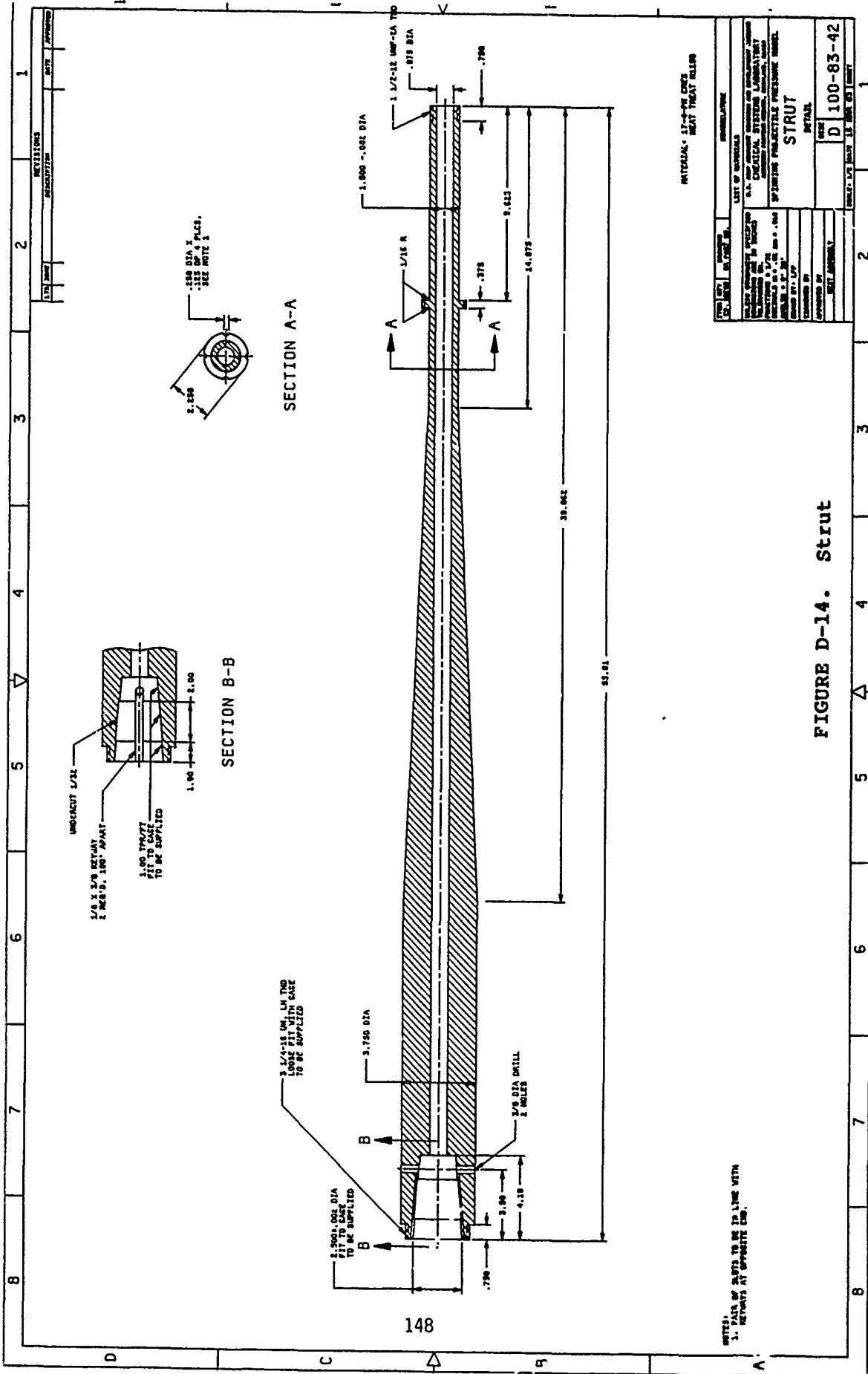


FIGURE D-13. Forward Core Motor/Bearing Support Section

ITEM NO.	QUANTITY	DESCRIPTION	UNIT
1	1	FORWARD CORE MOTOR/BEARING SUPPORT SECTION	PC
2	1	BEARING SUPPORT SECTION	PC
3	1	FORWARD CORE MOTOR	PC
4	1	BEARING SUPPORT SECTION	PC
5	1	FORWARD CORE MOTOR	PC
6	1	BEARING SUPPORT SECTION	PC
7	1	FORWARD CORE MOTOR	PC
8	1	BEARING SUPPORT SECTION	PC

LIST OF MATERIALS	DATE
U.S. CHEMICAL SYSTEMS LABORATORY	
SPINNING PROPELLANT PRESSURE MODEL	
FWD CORE MOTOR/ BEARING SUPPT SEC	
DATE	D 100-83-33
DESIGNED BY	
CHECKED BY	
APPROVED BY	
SCALE: 1/2" = 1" (DATE 7, 1983 BY J. BRET)	



NOTES:  
 1. PAIR OF PARTS TO BE IN LINE WITH  
 2. RETRAYS AT OPPOSITE END.

**FIGURE D-14. Strut**

REV	DATE	BY	CHKD
LIST OF MATERIALS			
MATERIALS SPECIFIED FOR THIS DRAWING ARE THE PROPERTY OF THE DESIGNER AND ARE NOT TO BE REPRODUCED OR USED FOR ANY OTHER PURPOSE WITHOUT THE WRITTEN PERMISSION OF THE DESIGNER.			
DESIGNED BY: L.P.			
CHECKED BY:			
APPROVED BY:			
MATERIAL: 17-7PH CRES HEAT TREAT ROLLER			
PART NAME: STRUT			
DRAWING NO: D 100-83-42			
SCALE: 1/2" = 1"			



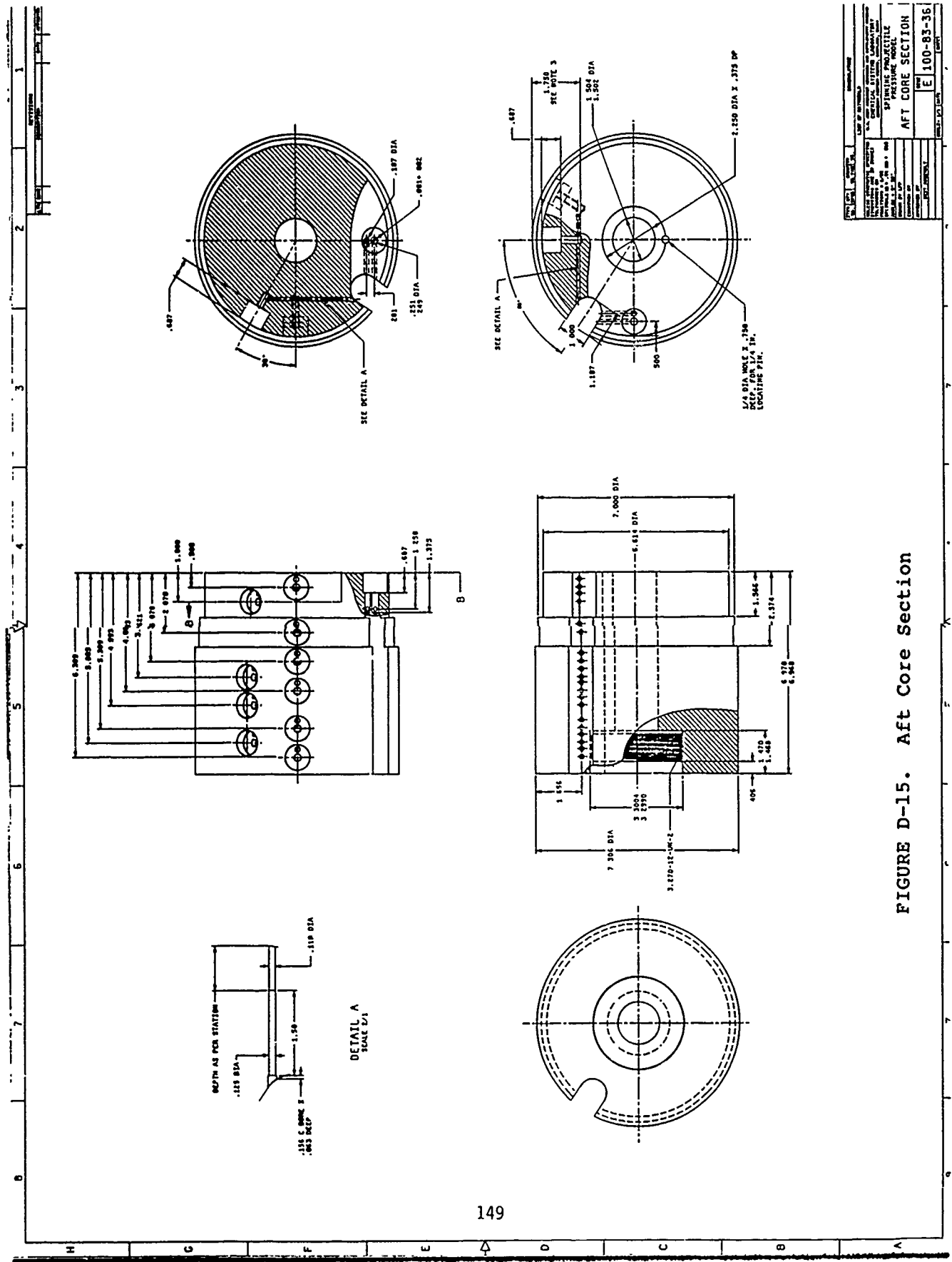
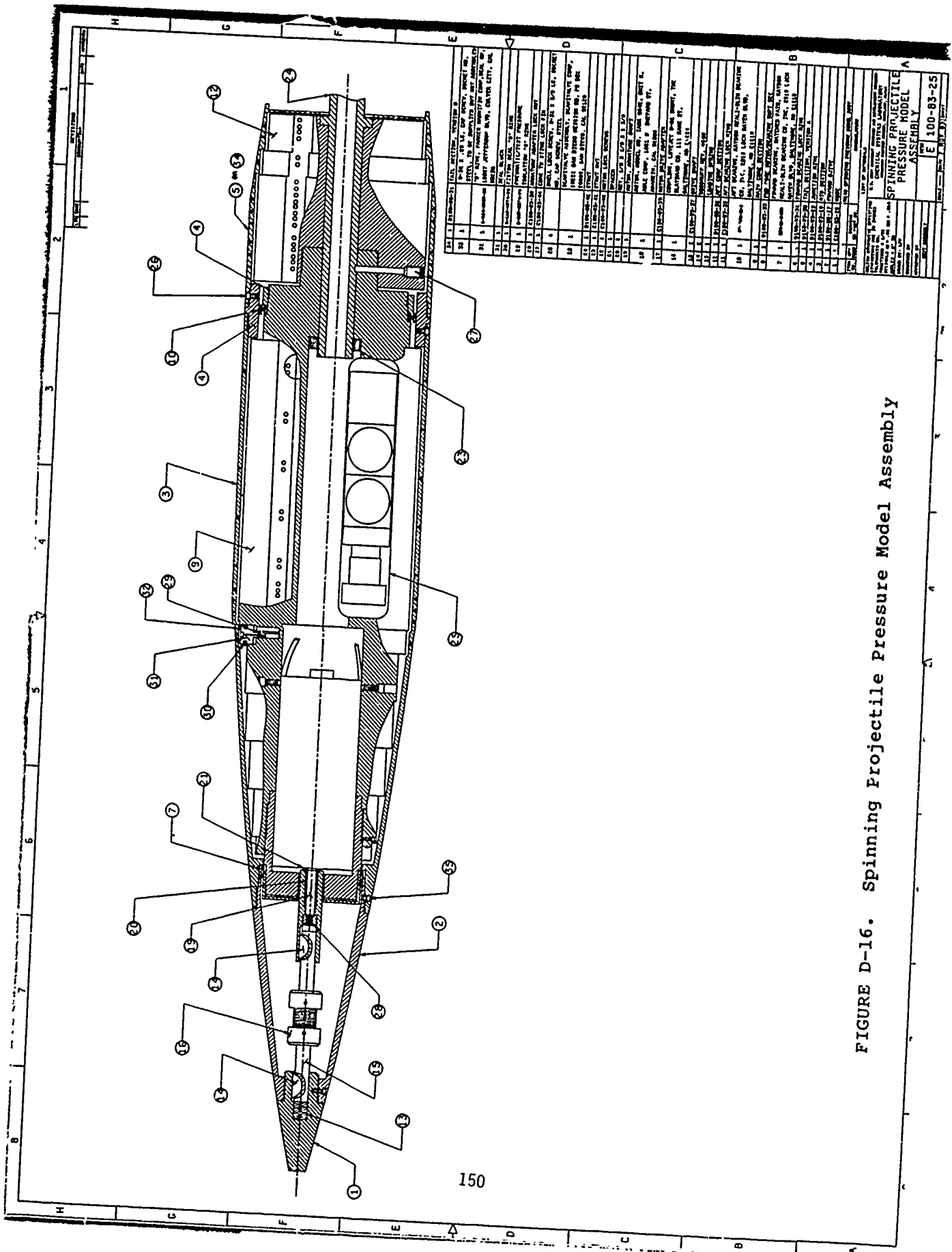


FIGURE D-15. Aft Core Section



NO.	DESCRIPTION	QTY.	UNIT	SYMBOL	REVISION
1	PROPELLANT GRAIN	1	PC	1	
2	NOSE CONE	1	PC	1	
3	NOSE CONE	1	PC	1	
4	NOSE CONE	1	PC	1	
5	NOSE CONE	1	PC	1	
6	NOSE CONE	1	PC	1	
7	NOSE CONE	1	PC	1	
8	NOSE CONE	1	PC	1	
9	NOSE CONE	1	PC	1	
10	NOSE CONE	1	PC	1	
11	NOSE CONE	1	PC	1	
12	NOSE CONE	1	PC	1	
13	NOSE CONE	1	PC	1	
14	NOSE CONE	1	PC	1	
15	NOSE CONE	1	PC	1	
16	NOSE CONE	1	PC	1	
17	NOSE CONE	1	PC	1	
18	NOSE CONE	1	PC	1	
19	NOSE CONE	1	PC	1	
20	NOSE CONE	1	PC	1	
21	NOSE CONE	1	PC	1	
22	NOSE CONE	1	PC	1	
23	NOSE CONE	1	PC	1	
24	NOSE CONE	1	PC	1	
25	NOSE CONE	1	PC	1	
26	NOSE CONE	1	PC	1	
27	NOSE CONE	1	PC	1	
28	NOSE CONE	1	PC	1	
29	NOSE CONE	1	PC	1	
30	NOSE CONE	1	PC	1	
31	NOSE CONE	1	PC	1	
32	NOSE CONE	1	PC	1	
33	NOSE CONE	1	PC	1	
34	NOSE CONE	1	PC	1	
35	NOSE CONE	1	PC	1	

FIGURE D-16. Spinning Projectile Pressure Model Assembly

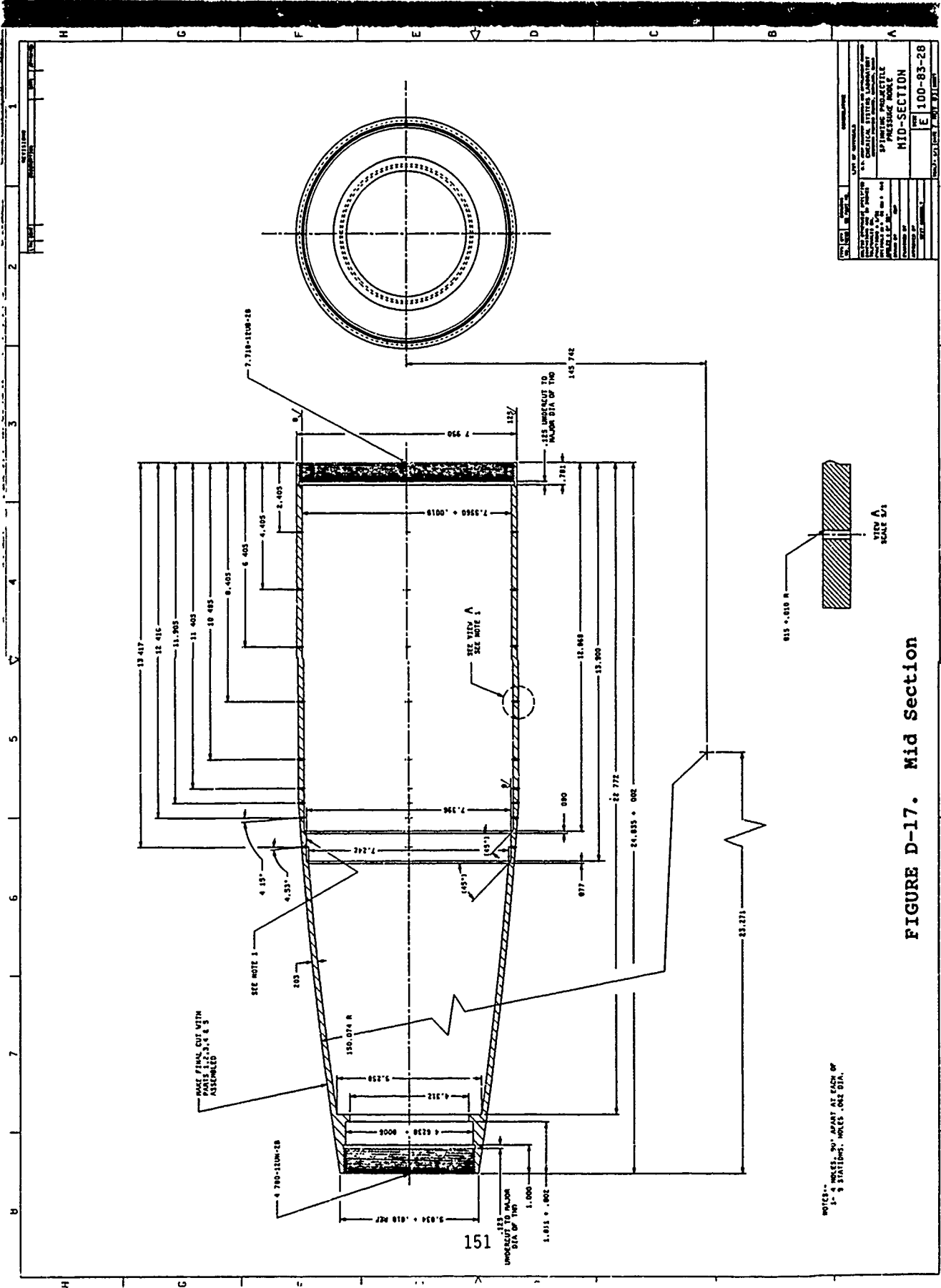


FIGURE D-17. Mid Section





