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AIR- $\mathrm{N}_{2} \mathrm{O}_{2}$ DECOMPRESSION COMPUTER ALGORITHM DEVELOPMENT

By :
Edward D. Thalmann, CAPT, MC, USN
August 1986

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E. D. THALMANN

CAPT, MC, USN

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#### Abstract

A computer algorithm which can conrute decompression schedules for air or a $\mathrm{N}_{2} \mathrm{O}_{2}$ breathing mix of any $\mathrm{PO}_{2}$ was developed and tested. Testing consisted of 837 man dives on some 38 different profiles. There were 19 air bounce dive profiles from depths of $50-190$ FSW, 5 being no-decompression dives. Four bounce profiles at 100 and 150 FSW were tested breathing a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ throughout. Three profiles at 60,100 and 150 FSW where air was breathed on the bottom and a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ mix was breathed during decompression were tested. There were 10 air repetitive dive profiles at depths of $80,100,120$ and $150 \mathrm{FSW}, 7$ of which were for no-decompression dives. Two long duration multiple level (20-100 FSW) dives where gas switches were made between air and a constant 0.7 ATA $\mathrm{PO}_{2}$ breathing mix were also done. All dives were cold, wet, working dives and all decompression schedules were computed in real time using a HP-1000 computer which constantly monitored chamber depth. A total of 49 cases of decompression sickness (DCS) resulted all of which were successfully treated. The following no-decompression depth/time limits were tested without DCS: 60/66, 100/30, 120/24, 150/14, 190/10. Testing showed that repetitive dive no-decompression limits could probably be extended but that total decompression times for both bounce and repetitive decompression dive had to be exteded considerably compared to U.S. Navy Standard Air Tables. Decompression time for constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ dives could be shortened compared to current tables. The final decompression model uses total gas tension in determining decompression stops and computes a venous oxygen tension from an arterial value based on the hemoglobin disassociation curve and an assumed tissue metabolic rate. Gas uptake is assumed exponential while offgassing is assumed linear while a gas phase is present and exponential thereafter. The final decompression model can compute decompression schedules for a dive of any complexity and any oxygen level with nitrogen as the inert gas. The $\mathrm{rO}_{2}$ may be changed at any time during the dive. The model is suitable for propramming into a small portable microprocessor based decompression computer for real time computations.


## Table of Contents

Page
ABSTRACT/KEY WORDS ..... vii
GLOSSARY ..... viii
INTRODUCTION ..... 1
METHODS ..... 1
General ..... 1
Test Profiles ..... 4
Decompression Model and Computer Algorithms ..... 11
Ascent Criteria ..... 15
RESULTS ..... 18
Air No-Decompression Bounce Dives ..... 19
Air Decompression Bounce Dives ..... 19
Constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ Bounce Dives ..... 27
Air $\rightarrow$ Constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ Bounce Dives. ..... 29
Air Repetitive Dives ..... 30
Decompression Repetitive Dives ..... 31
No-Decompression Repetitive Dives ..... 32
Multi-Level Air/Constant $0.7 \mathrm{ATA}_{\mathrm{PO}_{2}}$ in $\mathrm{N}_{2}$ Dives ..... 34
DISCUSSION ..... 34
Development of Initial Ascent Criteria (VVAL22) ..... 35
EL MK 15/16 DCM-I Testing (VVAL22-29) ..... 38
EL MK 15/16 DCM-II Testing (VVAL50-59) ..... 40
Decompression Sickness Symptoms ..... 42
Final Decompression Model and Tables ..... 43
Decompression Model Limitations ..... 45
CONCLUSIONS ..... 46
FOOTNOTES ..... 48
REFERENCES ..... 49


## FIGURES

Page
FIG. 1 Typical Dive Profile ..... 7
FIG. 2 No-Decompression Dive Profile. ..... 9
TABLES
TABLE 1 Profile Descriptions (Bounce Dives) ..... 5
TABLE 2 Profile Descriptions (Repet/Multi-Level Dives) ..... 6
TABLE 3 Calculation of Arterial and Venous 02, C02, and N2 Tensions For the EL-MK 15/16 DCM ..... 12
TABLE 4 Phase 1 Test Dive Results ..... 20
TABLE 5 Phase 2 Test Dive Results ..... 21
TABLE 6 Phase 3 Test Dive Results ..... 21
TABLE 7 Results of Bounce Dives Tested ..... 22
TABLE 8 Results of Repetitive/Multi-Level Dives Tested ..... 23
TABLE 9 Ascent Criteria Blood Parameters ..... 24
TABLE 10 No-Decompression Limit Comparisons ..... 25
TABLE 11 Decompression Sickness Incidence ..... 28

## APPENDICES

| APPENDIX A | Diver Physical Cha | A-1 to A-6 |
| :---: | :---: | :---: |
| APPENDIX B | Decompression Sickness Descrip | B-1 to B-10 |
| APPENDIX C | Individual Diving Intensity | $\mathrm{C}-1$ to C-6 |
| APPENDIX D | Maximum Permissible Tissue Tension (MPTT) Table | D-1 to D-16 |
| APPENDIX E | Dive Profile Comparison | $\mathrm{E}-1$ to E-12 |
| APPENDIX F | Air Decompression Tables (VVAL59) | F-1 to F-32 |
| APPENDIX G | Constant 0.7 ATA PO2 in N2 Decompression Tables (VVAL59) | G-1 to G-26 |
| APPENDIX H | Constant 0.7 ATA P02 in N2 Phase I \& II Dive Profile Comparison. $\qquad$ | $\mathrm{H}-1$ to $\mathrm{H}-26$ |

## ABSTRACT

A computer algorithm which can compute decompression schedules for air or a $\mathrm{N}_{2} \mathrm{O}_{2}^{-}$breathing mix of any $\mathrm{PO}_{2}^{n}$ was developed and tested. Testing consisted of 837 man dives on some 38 different profiles. There were 19 air bounce dive profiles from depths of $50-190$ FSW, 5 being no-decompression dives. Four bounce profiles at 100 and 150 FSW were tested breathing a constant 0.7 ATA $\mathrm{PO}_{2}^{n}$ in $\mathbb{N}_{2}^{n}$ throughout. Three profiles at 60,100 and 150 FSW where air was breathed on the bottom and a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}^{n}$ in $\mathrm{N}_{2}^{n} \mathrm{mix}$ was breathed during decompression were tested. There were 10 air repetitive dive profiles at depths of $80,100,120$ and $150 \mathrm{FSW}, 7$ of which were for no-decompression dives. Two long duration multiple level (20-100 FSW) dives where gas switches were made between air and a constant 0.7 ATA $\mathrm{PO}_{2}^{\hat{2}}$ breathing mix were also done. All dives were cold, wet, working dives and all decompression schedules were computed in real time using a $\mathrm{HP}-1000$ computer which constantly monitored chamber depth. A total of 49 cases of decompression sickness (desulted all of which were successfully treated. The following no-decompression depth/time limits were tested without Dds: 60/66, 100/30, 120/24, 150/14, 190/10. Testing showed that repetitive dive no-decompression limits could probably be extended but that total decompression times for both bounce and repetitive decompression dive had to be extended considerably compared to U.S. Navy Standard Air Tables. Decompression time for constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ dives could be shortened compared to current tables. The final decompression model uses total gas tension in determining decompression stops and computes a venous oxygen tension from an arterial value based on the hemoglobin disassociation curve and an assumed tissue metabolic rate. Gas uptake is assumed exponential while offgassing is assumed linear while a gas phase is present and exponential thereafter. The final decompression model can compute decompression schedules for a dive of any complexity and any oxygen level with nitrogen as the inert gas. The $\mathrm{PO}_{2}$ may be changed at any time during the dive. The model is suitable for programming into a small portable microprocessor based decompression computer for real time computations.

KEY WORDS:

Air Decompression Tables<br>Computer Algorithm<br>Computer Model<br>Constant Oxygen Partial Pressure<br>Decompression Model<br>Decompression Sickness<br>Decompression Tables<br>Mathematical Model<br>MK 15 UBA<br>MK 16 UBA<br>Nitrogen-Oxygen Decompression Tarles<br>Repetitive Diving,<br>NEDU Test Plan Number $\varepsilon \neq / 30$

| Actual Dive Profile | A table or graph showing the actual depth/time coordinates for an entire dive. |
| :---: | :---: |
| Algorithm | - A sequence of logical steps used to obtain a mathematical result. |
| Ascent Criteria | A set of constraints on a decompression model which defines how ascent may be accomplished without causing decompression sickness. |
| Bottom Time | The elapsed time from leaving the surface until beginning ascent to the first decompression stop (or the surface if a no-decompression dive). |
| Bounce Dive | A dive where descent is made to some depth for a specified time and then decompression is done to the surface without stopping at any depth not required by the decompression schedule. |
| Controlling Tis | The theoretical tissue which will require the longest time to offgas from its current tension to its maximum tension at a given stop depth. |
| Computer Program | A series of instructions directing a computer how to process information to obtain the desired output. A computer program may contain one or more algorithms which perform intermediate calculations. As an example, a computer program for an Underwater Decompression Computer (UDC) may contain algorithms describing gas uptake and elimination, rules for finding the first stop and warning the diver when he is outside of the tested limits. |
| Decompression Model | A series of algorithms which describe how gas is taken up and given off by the body during a dive and what conditions must be met in order to avoid decompression sickness. |
| Decompression Obligation - The total amount of decompression stop time accrued at any time in a dive profile if ascent were begun at that instant at a specified rate. |  |
| Decompression Profile - A table or graph showing the depth-time coordinates for an entire dive including all desired stops and all obligatory decompression stops. |  |



| SAD | Safe Ascent Depth. The shallowest depth which could be ascended to at any time in a dive profile without violating the ascent criteria. The SAD is used in real time decompression profile execution and is computed and displayed by the EL-MK 15/16 RTA. |
| :---: | :---: |
| SDR | Saturation-Desaturation Ratio. The ratio of the theoretical tissue halftime used to compute gas uptake to the halftime used to compute gas elimination. |
| Set Point | The P02 in a closed circuit UBA at which oxygen is added to the breathing loop. |
| TDT | Total Decompression Time. The total time required from leaving the bottom until reaching the surface after taking all required decompression stops. |
| Tension | The partial pressure of a gas in a gas mixture. |
| Theoretical Halftime Tissue - A conceptual area of body tissue whose gas uptake can be described by an exponential term with a time constant $K$ or halftime equal to $\ln (2) / K$. |  |
| Underwat | ion Computer (UDC) - A small microprocessor device carried by a diver which continuously samples depth and updates his decompression obligation. |

Air- $\mathrm{N}_{2} \mathrm{O}_{2}$ Decompression Computer Algorithm Development

By: Edward D. Thalmann, CAPT, MC, USN
INTRODUCTION: Testing of a computer algorithm for diving while breathing a constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ had been completed at the Navy Experimental Diving Unit in August 1980. This algorithm was used to generate a set of decompression tables (1) and is also being programmed into a small, portable wrist-worn Underwater Decompression Computer (UDC) for use with constant $\mathrm{PO}_{2}$ closed-circuit Underwater Breathing Apparatus (UBA). Interest in the Special Warfare Community in being able to switch between a constant $\mathrm{PO}_{2}$ breathing gas and air, coupled with interest in seeing if the constant $\mathrm{PO}_{2}$ algorithm could be extended to air, lead to the study reported here.

The overall plan at the inception of the present study was to develop a computer algorithm which would allow any desired changes in inspired oxygen tension during a dive with nitrogen as the inert gas. An initial feasibility phase looked at what modifications would have to be made to the previously tested Exponential Linear MK $15 / 16$ Decompression Mode1 (EL-MK 15/16 DCM) in order to allow switches in oxygen tensions. Next, a dive series was conducted which was divided into 3 phases. Phases 1 A and $1 B$ examined air bounce dives using both U.S. Navy Standard Air Tables (6) as well as decompression profiles generated using a modified EL-MK $15 / 16$ DCM. Phase 2 looked at additional air bounce dives using only computer generated decompression profiles, repetitive air dives, dives in which the breathing gas was switched between air and a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ and dives breathing a constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ throughout. Phase 3 looked at repetitive air dives and long multiple level dives where switches were made between air and constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$. All phases of the dive series were completed between August and December of 1984. A total of 837 man dives were done which resulted in 49 cases of decompression sickness.

## METHODS:

## General

All 126 divers who participated in this study were active duty Navy or Army divers, or military trained civilians. Divers from the U.S., Canadian and British military participated. The physical characteristics of all divers are given in Appendix A. One of the divers (\#110) was a female. There were 4 separate dive series (Phases $1 A, 1 B, 2$ and 3 ) and some subjects participated in more than one series. Divers were all actively exercising up to the time of their participation in the study and were all in good physical condition. All divers were given thorough diving physical examinations before each dive series began and were examined immediately before and after each dive by a U.S. Navy Diving Medical Officer.

Breathing gas for the dive was either compressed air ( $\mathrm{FO}_{2}=20.95 \%$ ) supplied through open circuit $S C U B A$ regulators or a constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ supplied
by a MK 15 closed circuit UBA. In dives where switches were made between air and the constant 0.7 ATA $O_{2} \mathrm{mix}$, the divers wore the MK 15 on their bac and breathed air from SCUBA regulators attached to a manifold on an underwater habitat.

All divers were thoroughly trained in the use of the MK 15 closed-circuit constant $\mathrm{PO}_{2}$ UBA which had the $\mathrm{PO}_{2}$ setpoint adjusted to 0.7 ATA. A complete description of the MK 15 hardware and operating characteristics is given in references (2) and (3). With a $\mathrm{PO}_{2}$ setpoint of 0.7 ATA , the MK 15 will automatically add oxygen when the $\mathrm{PO}_{2}$ falls to 0.7 ATA . Normally, the $\mathrm{PO}_{2}$ will have a mean level between 0.7 ATA and 0.8 ATA, but could be as low as 0.6 ATA without the UBA indicating a malfunction. This $\mathrm{PO}_{2}$ range is maintained irrespective of depth. There is an alarm light that will warn a diver if his $\mathrm{PO}_{2}$ falls to 0.6 ATA. If this happened during dives in this study, the diver was instructed to manually add oxygen and to change to another UBA if $\mathrm{PO}_{2}$ could not be maintained automatically in the $0.6-0.8$ ATA range. As long as no alarm lights indicated a low $\mathrm{PO}_{2}$, divers were instructed to let the UBA control automatically and no attempt was made to control the $\mathrm{PO}_{2}$ at exactly 0.7 ATA. The diluent used for all MK 15 dives in this series was $100 \%$ nitrogen. Operationally air will be used as a diluent which would result initially in higher oxygen partial pressures immediately after compression as diluent gas is added to the breathing loop to make up volume during descent. By using $100 \%$ nitrogen the oxygen partial pressure during the first portion of time at depth will be lower than it will be when operational dives take place. Since a lower $\mathrm{PO}_{2}$ is presumed to increase decompression obligation, schedules were tested under conditions of maximum decompression stress with respect to oxygen partial pressure.

All dives were conducted in the 15 foot diameter by 46 foot long wet chamber of the Ocean Simulation Facility (OSF) at the Navy Experimental Diving Unit (NEDU) in Panama City, Florida. Divers were generally divided into 10 man teams. While at depth the 10 divers performed intermittent exercise at 75 watts on an electrically braked bicycle ergometer pedalling at 55-60 RPM. Since only 5 bicycle ergometers were available, only half the divers were actually exercising at a given time. Exercise periods lasted 6 minutes after which time the 5 non-exercising divers mounted the ergometers and began exercising. This alternating 6 minute work, 6 minute rest cycle continued until 1 minute prior to decompression at which time all exercise stopped ${ }^{1}$. Previous studies showed that the mean oxygen consumption for divers in wetsuits pedalling 55-60 RPM doing this alternating work/rest cycle was approximately $1.00-1.2 \mathrm{l} / \mathrm{min}$ with a $1.6-1.8 \mathrm{l} / \mathrm{min}$ oxygen consumption during exercise and a $0.4-0.5 \mathrm{l} / \mathrm{min}$ oxygen consumption at rest (1) ${ }^{2}$. All divers remained at rest for the entire decompression.

All dives were done in cold water with divers wearing full $1 / 4$ " neoprene wetsuits consisting of "Farmer John" trousers, jacket, hood, gloves and boots. Water temperature was set ( $\pm 2^{\circ} \mathrm{F}$ ) according to the total dive time as follows: 250 min or greater, $65^{\circ} \mathrm{F} ; 249-190 \mathrm{~min} 60^{\circ} \mathrm{F} ; 179-80 \mathrm{~min} 55^{\circ} \mathrm{F} ; 79 \mathrm{~min}$ or less $50^{\circ} \mathrm{F}$. For repetitive dives, the water temperature was set according to the shortest in-water segment of dive, surface intervals were not
considered in setting water temperatures. Most divers were visibly chilled and shivering when exiting from dives, indicating a significant thermal stress during the dive.

Inspired $\mathrm{CO}_{2}$ was less than 1 mmHg during air dives as confirmed by analysis of the air banks. No $\mathrm{CO}_{2}$ measurements were made when the divers were breathing from the MK 15 but previous experience with this UBA showed that inspired $\mathrm{CO}_{2}$ would not rise above 2 mmHg in a normally functioning UBA during the maximum times it would be in use during these dives (1).

Descent rates were $30-60 \mathrm{FSW} / \mathrm{min}$ depending on diver's ability to clear their ears. Occasionally there were holds on the way down followed by intermittent ascents because of eustachian tube blockage in some divers. Since the decompression schedules were all computed in real time all these holds were taken into account in determining actual decompression obligation. Ascent rates were $60 \mathrm{FSW} / \mathrm{min}$ to $20 \mathrm{FSW}, 40 \mathrm{FSW} / \mathrm{min}$ from 20 to 10 FSW , and 30 FSW/min from 10 FSW to the surface, these being the maximum OSF wet chamber travel rates over these depth ranges.

The wet chamber was pressurized with air for all dives. Occasionally, a diver would have to come off his UBA at depth. A dry underwater refuge was in the wetpot and always contained an air atmosphere. During air dives, breathing refuge atmosphere had no effect on the diver's decompression status. If divers were breathing from the MK 15 UBA, then breathing refuge atmosphere would cause his inspired $\mathrm{PO}_{2}$ to be different from his fellow divers during that time. In these circumstances, if a diver breathed refuge atmosphere for more than a few minutes he was eliminated as a test subject from that particular dive. Chamber occupants (tenders or divers withdrawn from the wetpot) usually breathed an $\mathrm{N}_{2} \mathrm{O}_{2}$ mix which was higher than that being breathed by the divers. This mix was either $40.0 \% 0_{2}$ down to 150 FSW and $32.5 \%$ for deeper dives. During decompression, the same gas breathed at depth was used until a depth of 30 FSW was reached at which point chamber occupants were switched to $100 \% 0_{2}$ for the remainder of decompression. One some of the no-decompression air repetitive dives tenders breathed only chamber air for the entire dive.

The only criteria used to evaluate the safety of a particular dive profile was the occurrence of clinical decompression sickness. The determination as to whether or not a particular diver had decompression sickness was made by an experienced U.S. Navy Diving Medical Officer who evaluated both subjective and objective signs and symptoms. If, in the opinion of the examining Diving Medical Officer (based on diver history and physical examination), decompression sickness was present, then appropriate treatment was instituted. No other criteria (such as ultrasonic doppler monitoring) were used to determine whether or not decompression sickness was present. Usually symptoms of decompression sickness would not manifest themselves until the diver surfaced in which case only the stricken diver was treated. In some instances symptoms occurred while still at depth and when the stricken diver could not be isolated in another chamber all the other divers on that particular dive were treated along with the stricken diver. In these cases,
the asymptomatic divers were not included in the dive statistics at all while the stricken diver was counted as a case of decompression sickness. All treatments for decompression sickness were done using standard U.S. Navy Oxygen Treatment Tables and Procedures (6) unless otherwise noted.

## Test Profiles

A total of 38 different test profiles were used in this dive series and are presented in Tables 1 and 2. These profiles were chosen to cover the depth/time domain of the U.S. Navy Standard Air Tables over the depth range of 50 to 190 FSW. Dives were classified as either bounce dives, repetitive dives, or multi-level dives. Appendix C shows which divers dove on which profile on any given day of the series.

All dives were done using real time decompression profiles generated by a Hewlett-Packard HP 1000 Series Computer using a computer algorithm based on the current version of the EL-MK 15/16 DCM as described below. The computer continuously monitored chamber depth from an Ashcroft Digigauge to an accuracy of $\pm 1$ FSW and updated the diver's decompression status every 2 seconds. Real time algorithms were developed as described elsewhere (1). Real time computation allowed any holds or changes in travel rate during ascent and/or descent to be taken into account thus producing a decompression schedule exactly suited to a particular dive profile. The decompression status was displayed on a video display as the shallowest depth which could be ascended to at any given time without violating the ascent criteria, the so-called Safe Ascent Depth (SAD). During decompression the divers' depth was matched to the SAD which was always computed in 10 FSW increments. The actual dive profiles were continuously recorded and stored by the computer and could be retrieved after the dive. A typical dive profile plot is shown in Figure 1.

When doing real time decompression profiles divers were compressed to the desired depth at a rate of 30 to $60 \mathrm{FSW} / \mathrm{min}$ but occasionally holds occurred so mean descent rate varied considerably from dive to dive. In order to keep profiles at a given depth comparable, the actual time for leaving the bottom was determined by Total Decompression Time (TDT). The Hewlett-Packard HP 1000 computer was programmed to compute TDT every 2 seconds along with the SAD. Thus, every 2 seconds the Diving officer knew exactly how many minutes of decompression would be required if ascent were begun at that instant. Before the dive, a complete set of hard-copy decompression schedules were calculated using the current version of the EL-MK 15/l6 DCM assuming a 60 FSW ascent and descent rate. Each one of these schedules had a total decompression time associated with it. Thus, if the planned dive was 190 FSW for 30 min the divers were compressed to 190 FSW and after arrival stayed at 190 FSW until the TDT as calculated and displayed by the HP 1000 computer was the same as that in the previously computed 190 FSW for 30 min hard-copy decompression schedule. At that instant decompression was begun and accomplished by matching diver depth with the SAD. By using this procedure the actual time at depth was adjusted to take total descent time into account such that upon leaving depth the theoretical tissue tensions for controlling tissues were the same as for the profile in the previously computed hard-copy schedule where a

TABLE 1
PROFILE DESCRIPTIONS
(Bounce Dives)

Profile No.

> Schedule* Depth/Bottom Time (FSW)/(Min)

|  | Air Dives |  |
| :---: | :---: | :---: |
| 1 |  | 50/240 |
| 2 |  | 60/[66] |
| 3 |  | /100 |
| 4 |  | 1120 |
| 5 |  | /180 |
| 6 |  | 80/120 |
| 7 |  | 100/[30] |
| 8 |  | 160 |
| 9 |  | 190 |
| 10 |  | 120/[24] |
| 11 |  | 160 |
| 12 |  | 170 |
| 13 |  | 180 |
| 14 |  | 150/[14] |
| 15 |  | 140 |
| 16 |  | $/ 60$ |
| 17 |  | 190/[10] |
| 15 |  | $/ 30$ |
| 16 |  | 140 |
|  | Constant 0.7 ATA $\mathrm{PO}_{\underline{2}} \underline{\underline{2}}$ in $\underline{\mathrm{N}}_{2}$ |  |
| 20 |  | 100/60 |
| 21 |  | 150/30 |
| 22 |  | 140 |
| 23 |  | 160 |
|  | Air $\rightarrow$ Constant 0.7 ATA PO2 in N 2 |  |
| 24 |  | 60/120 |
| 25 |  | 100/90 |
| 26 |  | 150/40 |

*Times in [ ] are no-decompression times.

TABLE 2
PROFILE DESCRIPTIONS
(Reper/Multi-Level Dives)
 FSW, times in minutes.


FIGURE 1. Typical Dive Profile. The dotted line shows the actual depth while the solid line shows the Safe Ascent Depth (SAD) as computed by the computer algorithm. Decompression was accomplished by matching actual depth to SAD and following it to the surface. The irregularities noted during compression were due to holds because of ear squeezes. Since the decompression was computed in real time by continuously monitoring chamber depth, all of these irregularities were taken into account in the final decompression schedule.
$60 \mathrm{FSW} / \mathrm{min}$ descent rate was assumed. Thus, when a $190 \mathrm{FSW} / 30 \mathrm{~min}$ profile is referred to in this report it means a profile where after arriving at 190 FSW divers stayed at depth until the TDT was the same as for a diver who left the surface and traveled to 190 FSW at exactly 60 FPM and stayed at depth for exactly 26.33 min (total bottom time equal to the 3.66 min descent time plus 26.33 min at depth) and ascended at exactly 60 FPM during decompression. Thus, all profiles began ascent at very close to the same theoretical tissue tensions although actual times at depth may have differed by a few minutes depending on the actual descent time.

Decompression stops were in 10 FSW increments. At the 10 FSW stop, the chamber depth was 3 FSW with divers at the bottom of the 7 foot wetpot water column. Since it generally took 30 sec to travel this last 3 FSW , travel was begun when the HP 1000 computer showed 30 sec remaining at the 10 FSW stop. At the instant the HP 1000 showed that the divers could surface, all divers ascended to the surface and immediately began breathing chamber air. This procedure, when followed, always had the divers within 1 FSW of the surface when the HP 1000 showed that they could ascend to the surface. Once the chamber was actually at the surface, divers swam to the ladder and exited the chamber.

In doing no-decompression dives using the real time computer algorithm, the no-decompression time is that time at which the SAD increases from 0 to 10 FSW indicating the need for a decompression stop. As long as the SAD was 0 , the divers were within no-decompression limits. Thus, at any given depth no-decompression time was the time remaining before the $S A D$ increased from 0 to 10 FSW and this time was displayed and counted down in 2 sec increments. Programming constraints in the real time environment dictated that this time be computed assuming instantaneous ascent. Thus, once at depth, the no-decompression time was computed by calculating the shortest time it would take any tissue to saturate from its current value to its surfacing tension ( 10 FSW row of the Maximum Permissible Tissue Tension Tables, Appendix D). Since some tissue offgassing would always occur during ascent, this instantaneous no-decompression time would always be shorter than no-decompression time calculated assuming a finite ascent rate. To take care of this problem, divers were kept at depth until the HP 1000 showed the divers had accumulated approximately a 30 sec stop at 10 FSW . Ascent was begun at that time and if the stop time upon arrival at 10 FSW was more than 30 sec , a stop was taken until the displayed stop time decreased to 30 sec , at which point the chamber was surfaced and divers came to the surface of the wetpot. Stop times less than 30 sec were ignored. This procedure ensured that the real time no-decompression dives were in fact either right at the limits of the model or even slightly beyond model limits (Figure 2).

When doing dives where the U.S. Navy Standard Air Tables were to be used for decompression, a variation on the real time decompression profile procedure was used to take delays during descent into account. During compression, the real time computer program was running and would calculate and update the displayed value for TDT every two seconds, using the current version of the EL-MK 15/16 DCM. The actual time at depth was determined based


FIGURE 2. No-Decompression Dive Profiles. The profile on top shows a single dive. Upon arrival at 10 FSW there was 1.62 min remaining at this stop. With about 45 sec remaining the chamber was surfaced but the divers remained at 7 FSW in the wetpot until the SAD became 0 FSW at which instant they swam to the surface. The second profile shows a repetitive dive in which ascent was essentially directly to the surface to ensure that divers were at the surface the instant that the SAD decreased to 0 FSW.
on this displayed TDT in exactly the same way as was cone during real time decompression profile diving. However, once leaving the bottom a Standard U.S. Navy Air Decompression Schedule was followed to the surface. It should be noted that this procedure was used only to determine when to leave the bottom, not which Standard Air Decompression Schedule to pick. For instance, a dive to 100 FSW for an equivalent 60 min bottom time may have been decompressed on a 100 FSW for 60 min Standard Air Schedule or in other instances on a 100 FSW for 70 min Standard Air Schedule. The reasons for this will be detailed later.

Air dives were accomplished by having divers dress in their wet suits and don a standard air SCUBA apparatus (open-circuit regulator and tank). They then entered the wetpot and remained on the surface until all other divers were in the water. Then, on signal from the Dive Supervisor, all 10 divers went on their SCUBA regulators and swam to the bottom of the wetpot, a depth of 7 FSW. Dive time began at the instant the divers left the surface of the wetpot and at that time the computer program was started. Since the computer monitored the actual chamber depth, it added 7 FSW to all chamber depths to get the actual diver depth.

Once at the bottom of the wetpot (a depth of 7 FSW to mid chest), all divers were instructed to remain upright with their feet just touching the floor of the wetpot. The bicycle ergometer frame heights were such that exercising and non-exercising divers were within 1 FSW depth of each other at mid chest. Thus, the assumed depth error over an entire dive was $\pm 1$ FSW between divers. While on the bottom, divers did not breathe from their SCUBA bottles but breathed from open-circuit SCUBA regulators coming from a manifold piped from the main OSF air bank. Thus, the divers were insured of an unlimited air supply during the dive and only had to breathe from their SCUBA tanks during movements around the wetpot where the regulators on the manifold would not reach.

When doing dives involving the MK 15 UBA (either exclusively or in combination with air breathing) all compressions were done with the divers breathing from the MK 15. Divers donned their UBAs outside of the chamber and breathed chamber air as they entered the water. After entering the water, all divers switched from breathing air to breathing from the MK 15 UBA at the end of a full inspiration and descended to the bottom of the wetpot in unison on signal from the Dive Supervisor, thus ensuring that computer updates regarding breathing gas changes and depth changes corresponded exactly to what the divers were doing in real time. Dive time began when the divers began breathing from the MK 15. Once at depth, the divers either continued breathing from the MK 15 or breathed air from the manifolded SCUBA regulators in the wetpot as called for by that particular dive profile. All gas switches were done in unison on signal from the Dive Supervisor so that the computer could be instructed to change the breathing gas at the instant all the divers actually switched breathing gas. Decompressions were done either breathing air or from the MK 15 as called for by the dive protocol.

## Decompression Model and Computer Algorithms

The decompression model used to compute the real time decompression profiles in this study was the Exponential-Linear (EL) version of the model used in developing the computer algorithm for constant 0.7 ATA PO 2 in $\mathrm{N}_{2}$ diving and is thoroughly described elsewhere (Appendix A of ref. l). This original decompression model will be referred to as the Exponential-Linear MK 15/16 Decompression Model (EL-MK $15 / 16$ DCM) or the original model. While the decompression model actually encompasses all equations and assumptions considered in the avoidance of decompression sickness (DCS), reference to the EL-MK $15 / 16$ DCM will refer mainly to that portion of the model describing gas uptake and elimination. The other portion of the model which defines the ascent criteria are found in the various Maximum Permissible Tissue Tension (MPTT) Tables which define the maximum gas tension allowed in any of the theoretical halftime tissues at a given depth. Thus, to compute a decompression schedule the EL-MK $15 / 16$ DCM computes tissue tensions based on the particular dive profile and gas uptake and elimination equations then computes decompression stops such that no tissue exceeds its MPTT at any depth. The assumption is that by never having any tissue exceed its MPTT, decompression sickness will be unlikely.

The EL-MK 15/16 DCM was originally developed assuming a constant inspired oxygen partial pressure and assumed that arterial $\mathrm{CO}_{2}$ tension and venous $\mathrm{O}_{2}$ and $\mathrm{CO}_{2}$ tension were constant. Also, venous and tissue oxygen tension are assumed equal. From a physiological standpoint, all these assumptions are reasonable as long as the inspired oxygen tension ( $\mathrm{PO}_{2}$ ) does not change. However, when breathing air it is the inspired oxygen fraction ( $\mathrm{FO}_{2}$ ) which is constant and the inspired oxygen tension will be depth dependent. This will also presumably cause venous (and tissue) oxygen tension to vary depending on the arterial tension and the amount of oxygen extracted from arterial blood by the tissue (the a-v oxygen extraction). During this dive series, two modifications of the EL-MK $15 / 16$ DCM were used, the only difference between them being the way in which arterial and venous oxygen tensions are calculated. The original model will be referred to simply as the EL-MK 15/16 DCM while the two modified versions will be referred to as the EL-MK 15/16 DCM-I and EL-MK 15/16 DCM-II. The differences in the way these three versions handle oxygen is summarized in Table 3.

In the original version of the EL-MK $15 / 16 \mathrm{DCM}$, inspired and alveolar oxygen tensions were assumed equal and arterial oxygen tension differed only by a constant amount from alveolar. This difference, designated as AMBA02, was assumed to be zero during previous algorithm testing (1). The equation used to compute the alveolar (and arterial) oxygen tension for a constant inspired oxygen partial pressure assumed that the inspired oxygen partial pressure was a dry value, that the inspired and alveolar oxygen fractions were equal and that alveolar gas was fully saturated with water vapor.

In the version EL-MK 15/16 DCM-I, the alveolar oxygen tension was computed from the alveolar gas equation ${ }^{3}$ :
table 3
CAICULATION OF ARTERIAL AND VENOUS $\mathrm{O}_{2}, \mathrm{CO}_{2}$, AND $\mathrm{N}_{2}$ TENSIONS FOR THE \&. AK $15 / 16 \mathrm{DCM}$

| Site | Original Version | OCM-I Version | OCM-2 Version |
| :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \left(P_{A M B}-P_{H_{2} O}\right)-\left(1-F_{I_{N_{2}}}\right) \\ & \rho_{\mathrm{I}_{2}} \cdot\left(1-P_{\mathrm{H}_{2} \mathrm{O}} / P_{A M B}\right)[\text { Note } 1] \end{aligned}$ <br> Constant $P_{\text {AMB }}-\left(P_{\mathrm{A}_{2}}+P_{\mathrm{A}_{\mathrm{CO}_{2}}}+P_{\mathrm{H}_{2} \mathrm{O}}\right)$ |  | $\begin{gathered} \left(P_{A M B}-P_{\mathrm{H}_{2}}\right) \cdot\left(1-F_{1_{N_{2}}}\right)-P_{\mathrm{A}_{\mathrm{C}}} \\ \mathrm{P}_{\mathrm{I}_{0_{2}}}-P_{\mathrm{A}_{\mathrm{C}_{2}}} \quad[\text { Note 2] } \\ \text { Constant } \\ P_{\text {AMB }}-\left(P_{\mathrm{A}_{\mathrm{O}_{2}}}+P_{\mathrm{A}_{\mathrm{CO}_{2}}}+P_{\mathrm{H}_{2} \mathrm{O}}\right) \end{gathered}$ |
| Arterial $\begin{aligned} & { }^{{ }^{\mathrm{a}_{\mathrm{O}}^{2}}} \\ & { }^{\mathrm{P} \mathrm{aCO}_{2}} \\ & { }^{\mathrm{P} \mathrm{~d}_{2}} \end{aligned}$ | $\begin{aligned} & P_{\mathrm{AO}_{2}}-\mathrm{AMBAO}_{2} \\ & \mathrm{P}_{\mathrm{A}_{\mathrm{CO}}^{2}} \\ & \mathrm{P}_{\mathrm{A}_{\mathrm{N}_{2}}} \end{aligned}$ | $\begin{aligned} & \mathrm{P}_{\mathrm{A}}-\mathrm{AMBAO}_{2} \\ & \mathrm{P}_{\mathrm{A}_{\mathrm{CO}}^{2}} \\ & \mathrm{P}_{\mathrm{A}_{\mathrm{N}_{2}}} \end{aligned}$ |  |
| Venous/Tissue $\begin{aligned} & \mathrm{P}_{\mathrm{V}_{\mathrm{O}_{2}}} \\ & \mathrm{P}_{\mathrm{V}_{\mathrm{CO}_{2}}} \\ & \mathrm{P}_{\mathrm{V}_{\mathrm{N}_{2}}} \end{aligned}$ | Constant <br> Constant $P_{A M B}-\left(P_{V_{O_{2}}}+{ }^{P} V_{\mathrm{CO}_{2}}+P_{\mathrm{H}_{2} \mathrm{O}}\right)+\text { PBOVP }$ | Constant <br> Constant $P_{A M B}-\left(P_{V_{0_{2}}}+P_{V_{\mathrm{CO}_{2}}}+P_{\mathrm{H}_{2}}\right)+\mathrm{PBOVP}$ | $\mathrm{P}_{\mathrm{a}_{2}{ }_{2}}{ }^{-\mathrm{f}\left(\mathrm{P}_{\mathrm{a}_{\mathrm{O}_{2}}} \cdot \mathrm{P}_{\mathrm{aCO}_{2}} \cdot{ }^{\mathrm{P}_{\mathrm{VCO}_{2}}}, \mathrm{CAVO}_{2}\right.}$ <br> Constant $\mathrm{P}_{\mathrm{AMB}}-\left(\mathrm{P}_{\mathrm{V}_{\mathrm{O}_{2}}}+\mathrm{P}_{\mathrm{V}_{\mathrm{CO}_{2}}}+\mathrm{P}_{\mathrm{H}_{2} \mathrm{O}}\right)+\mathrm{PBOVP}$ |

$A M B A O_{2}$ - Constant alveolar/arterial oxygen tension difference.
$\mathrm{CAVO}_{2}$ - Tissue specific arterial/venous oxygen concentration difference.
$\mathrm{DAAO}_{2}$ - Constant alveolar/arterial oxygen concentration difference.
$\mathrm{F}_{\mathrm{I}_{2}}$ - Inspired nitrogen fraction.
${ }^{F} \mathrm{I}_{0_{2}} \quad-\quad$ oxygen fraction (dry) of inspired gas)
$f(\ldots$.$) - Function which converts \mathrm{OAAO}_{2}$ or $\mathrm{CAVO}_{2}$ to a partial pressure difference. Variable in parenthesis are the independent variables. (See text for function description).
$P_{A M B}$ - Ambsolute ambient hydrostatic pressure
$P_{A} \quad-\quad$ Alveolar gas tension.
$\mathrm{Pa}_{\mathrm{a}} \quad$ - Arterial gas tension.
PBOVP -. Tissue specific gas phase overpressure
$P_{V} \quad-\quad$ Venous or tissue gas tension.
$\mathrm{P}_{\mathrm{H}_{2} \mathrm{O}}$ - Water vapor tension
${ }^{\mathrm{P}} \mathrm{I}_{0_{2}} \quad$ - inspired oxygen partial pressure.

Note $2-P_{\mathrm{I}_{\mathrm{O}_{2}}}$ specified as measured in fully saturated atmosphere, i.e. $\mathrm{P}_{\mathrm{I}_{\mathrm{O}_{2}}}=\mathrm{F}_{\mathrm{I}_{\mathrm{O}_{2}}}\left(\mathrm{P}_{\mathrm{AMB}}-\mathrm{P}_{\mathrm{H}_{2} \mathrm{O}}\right)$.
${ }^{{ }^{P} \mathrm{I}_{2}}$ cannot exceed $\mathrm{P}_{\mathrm{AMB}}-\mathrm{P}_{\mathrm{H}_{2} \mathrm{O}}$ at any depth.

$$
\begin{equation*}
\mathrm{P}_{\mathrm{A}_{\mathrm{O}_{2}}}=\mathrm{P}_{\mathrm{I}_{\mathrm{O}_{2}}}-\left\{\left(\mathrm{P}_{\mathrm{A}_{\mathrm{C}}^{2}}-\mathrm{R}\right)-\mathrm{C}\right\} \tag{1}
\end{equation*}
$$

where:

$$
\begin{aligned}
\mathrm{P}_{\mathrm{I}_{2}} & =\text { Inspired oxygen tension } \\
\mathrm{P}_{\mathrm{A}_{\mathrm{CO}_{2}}} & =\text { alveolar } \mathrm{CO}_{2} \text { tension } \\
\mathrm{C} & =\mathrm{P}_{\mathrm{A}_{\mathrm{CO}_{2}}} \cdot{ }^{\mathrm{F}_{\mathrm{I}_{2}}} \text { •(l-R)/R } \\
\mathrm{F}_{\mathrm{I}_{\mathrm{O}_{2}}} & =\text { inspired oxygen fraction } \\
\mathrm{R} & =\text { respiratory quotient }
\end{aligned}
$$

The value for $R$ was assumed to be 1.0 and the alveolar $\mathrm{CO}_{2}$ level equal to arterial. In the DCM-I version, the inspired oxygen tension when breathing from the MK 15 UBA (or any other closed-circuit UBA) is assumed measured in an atmosphere fully saturated with water vapor, that is:

$$
\mathrm{F}_{\mathrm{I}_{0_{2}}}=\mathrm{P}_{\mathrm{I}_{0_{2}}} /\left(\mathrm{P}_{\mathrm{AMB}}-\mathrm{P}_{\mathrm{H}_{2}}\right)
$$

This means inspired oxygen tension can never exceed the difference between ambient pressure and water vapor pressure ${ }^{4}$ Arterial oxygen tension was assumed to differ from alveolar by a constant amount and venous oxygen and arterial carbon dioxide tensions were assumed constant.

The second modification of the decompression model (EL-MK 15/16 DCM-II) uses the same method of computing alveolar oxygen levels as used for the DCM-I version. However, in computing the arterial oxygen tension, instead of assuming a constant partial pressure difference between alveolar and arterial gas, a constant oxygen concentration difference is assumed corresponding to the degree of arterial-venous shunting in the lung. Equation 1 is used to obtain the alveolar $\mathrm{PO}_{2}$ value which is assumed equal to the alveolar capillary $\mathrm{PO}_{2}$ converted to a concentration in ml/ 100 using a mathematical representation of the hemoglobin dissociation curve as will be described. The assumed concentration difference due to shunting is subtracted and the resultant concentration converted back to a partial pressure (as will be described) which is then the arterial oxygen tension. In the EL-MK 15/16 DCM-II version the venous oxygen tension is also computed from the arterial tension assuming a constant arterial-venous oxygen concentration difference using the same hemoglobin disassociation curve mathematical representation. The mathematic representation used has been previously published (4) and is:

```
S = (ax n}+b\mp@subsup{x}{}{2n})/(1+c\mp@subsup{x}{}{n}+b\mp@subsup{x}{}{2n}
```

where:

$$
\begin{aligned}
& \mathrm{S}=\text { fractional hemoglobin saturation } \\
& \mathrm{a}=0.34332 \\
& \mathrm{~b}=0.64073 \\
& \mathrm{c}=0.34128 \\
& \mathrm{n}=1.58678
\end{aligned}
$$

and:

$$
\begin{equation*}
x=\left(P / P_{50}\right) \cdot 10[0.024(37-T)+0.40(\mathrm{pH}-7.4)+0.06 \log (40 / \mathrm{PCO})] \tag{3}
\end{equation*}
$$

where:

$$
\begin{aligned}
\mathrm{P} & =\text { oxygen partial pressure (mmHg) } \\
\mathrm{P}_{50} & =25 \mathrm{mmHg} \\
\mathrm{~T} & =37^{\circ} \mathrm{C} \\
\mathrm{pH} & =7.4 \\
\mathrm{P}_{\mathrm{CO}} & =\mathrm{CO}_{2} \text { partial pressure }(\mathrm{mmHg})
\end{aligned}
$$

The values for $a, b, c$ and $n$ in Equation 1 were those from reference (4) which minimized the error in computing the saturation fraction $S$. (Another set of values was given in reference (4) which minimized the value of $P$ when Equation 1 is inverted but these were not used). In computing a value for $\mathbf{x}$, P 50 , T and pH where given normal values as shown above and the value for $\mathrm{PCO}_{2}$ was either the arterial or venous value specified in the MPTT Table. The oxygen concentration in $\mathrm{ml} / 100 \mathrm{ml}$ was computed from the formula:
(4)

$$
\mathrm{C}=\mathrm{S} \cdot \mathrm{HBG}+0.003 \cdot \mathrm{PO}_{2}
$$

where:

$$
\begin{aligned}
& \mathrm{C}=\text { oxygen concentration in } \mathrm{ml} / 100 \mathrm{ml} \\
& S=\text { fractional hemoglobin saturation from Equation } 1 \\
& \operatorname{HBG}=\text { maximum hemoglobin } 0_{2} \text { capacity ( } 20 \mathrm{ml} / 100 \mathrm{ml} \text { ) } \\
& 0.003: \text { soluhility of oxygen in plasma (ml/100 ml } \cdot \mathrm{mmHg} \text { ) }
\end{aligned}
$$

Given a value for $\mathrm{PO}_{2}$ and $\mathrm{PCO}_{2}$ the value of C is easily computed using Equations 2, 3, and 4. Once the value for the arterial concentration is nomplitec, the concentration difference due to lung shunting (DAAO2) or tissue metabolism for a specific tissue (CAVO2), as appropriate, is subtracted. This new concentration is then plugged back into Equation 4 which then must be solved for $S$. Reference (4) gives the inverse of Equation 2 which would allow straigntforward calculation of $\mathrm{PO}_{2}$ given a value for S . Unfortunately, this inverse equation neglects the solubility factor in Equation 4 which may become significant at increased $\mathrm{PO}_{2}$ levels. Since Equation 4 cannot be explicitly soived for $\mathrm{PO}_{2}$, a Newton-Raphson iteration is used to obtain a value which will have an error less than $\pm 0.01 \mathrm{mmHg}$. The details of this iteration can ve obtained by perusal of Subroutine UPDTl which is listed elsewhere (5).

In computing changes in inert gas tension, all versions of the EL-MK 15/16 DCM compute all tensions at the ends of linear descents or ascents in one step. However, the equations used to do this assume that the venous oxygen tension will be constant with ascent. When the inspired $\mathrm{PO}_{2}$ is assumed constant this assumption is valid but when using a constant $\mathrm{FO}_{2}$ it is not. Furthermore, since the equations used to compute venous oxygen tension for a given arterial value (Equations 2, 3, 4) are not linear, incorporating the changes in venous oxygen tensions into the expression used to compute inert bas tension is not possible. In order to circumvent this problem, the venous oxygen tension is computed at the beginning of ascent or descent and is assumed constant for the duration of the depth change. This results in a small but insignificant error in computing tissue inert gas tension for the ascent and descent rates used in this study.

## Ascent Criteria

The EL-MK 15/16 DCM uses a table of Maximum Permissible Tissue Tensions (MFTT Table) to determine what the maximum tissue tensions allowed at each depth are. Generally, ascent to the first decompression stop is done so that most tissues are below their MPTT and one tissue (the controlling tissue) is exactly at its MPTT. Once at the first stop, a time must be spent at this fepth until all tissues have offgassed to a value less than or equal to the MPTT for the next shallower stop. This time is the Stop Time. After remaining for the Stop Time, ascent to the next shallower stop is done and another Stop Time computed such that all tissue tensions fall to a value equal to or less than the MPTT valve for the next shallower stop. This process is -epeated until the surface is reached. It should be noted that there is no requirement to ascend from a particular stop depth at the instant all MPTT's Eall below the values for the next shallower stop. Rather the Stop Time is the minimum time which must be spent at a given depth before ascent is Wussibie. In some cases it may be desirable to remain at a particular stop l:netr than the Stop Time, such as when taking the last decompression stop at C ESh.
$\therefore$ of the MPTT Tables used in this study are listed in Appendix D. The : $:=\because i d u a l$ tables are referred to by their VVAL number, and certain MPTT Zuites were used with only certain modifications of the decompression model.
as ciss mocie and long Gables which ias used to compute the constant 0.7 f.TA
Fi= in :i2 Tables presented in reference 1. The MPTT Tables VAL22-29 were
used only with the DCM-I version and VVAL50-59 used only with the DCM-II
version. The body of each MPTT Table in Appendix D gives the maximum tissue
tension in $\mathrm{FS}^{6}$ which can be present before ascent to the next shallower
depth is allowed. The values in the 10 FSW row are the maximum tensions
allowed at 10 FSW in order to make a direct ascent to the surface. These 10
FS\% values are also known as surfacing values. Subsequent rows give values
which cannot be exceeded before ascent to the next shallower stop is allowed,
the 20 FSW values indicating maximum values allowed before ascent to 10 FSW
and so on. Besides the maximum tensions at each depth the MPTT Tables list
several other parameters which are used in computing gas uptake and
elimination. The values just under the tissue halftimes are the Saturation
Desaturation Ratios or $S D R$ which are used to change the halftimes for
offgassing. Below the body of the table are listed a set of Blood Parameters
which are constant values used for various blood tensjons, tissue
overpressures, and oxygen extraction differences. Symbol definitions are
given in Table 3 and the values used for these Blood Parameters in various
stages of model development are given in Table 9. Details of how all the
values in the MPTT Table are used in the decompression model are found
elsewhere (1, 5) and certain aspects of their use will be discussed in this
report as needed.

The values in the body of the MPTT Table for VVAL18 and VVAL22-29 represent inert gas tensions while those in VVAL50-59 represent total tissue gas tension as will be discussed. In the original EL-MK 15/16 DCM only tissue inert gas tension was assumed to be important but i. both modifications (DCM-I and DCiI-II) total tissue gas tension, not simply inert gas tension, was assumed to be the critical factor. The venous $\mathrm{CO}_{2}$ tension was assumed constant in both modifications so the only other tissue tension which varied besides the inert gas tension was the tissue oxygen tension which was assumed equal to the venous tension. The methods of handing the changes in venous oxygen tension were different for the DCM-I and DCM-II modifications.

In the EL-MK 15/16 DCM-I, the venous oxygen tension was (artificially) assumed constant and set at the value it would assume had the inspired oxygen tension been 0.7 ATA. The MPTT Table was then adjusted to take into account the change in venous oxygen tension with depth as the inspired oxygen tension breathing air varied from 0.7 ATA. The starting point for this adjustment was VVALi8, the MPTT Table previously developed for computing the constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ Decompression Tables (1). VVAL18 contained values for inert gas tension only, but since the sum of tissue $\mathrm{PO}_{2}, \mathrm{PCO}_{2}$ and $\mathrm{PH}_{2} \mathrm{O}$ were constant, these values differed from total tissue tension by a constant amount which was independent of depth. Thus, by adding this constant value ( $\mathrm{PVO}_{2}+\mathrm{PVCO}_{2}+$ $\mathrm{PH}_{2} \mathrm{O}$ ) to the inert gas tension computed by the gas uptake and elimination equations and by adding the same value to each of the inert gas tensions in the MPTT Table, the model would then be evaluating total gas tensions but would compute exactly the same dec mpression tables. When using a constant oxygen fraction gas (such as air) the venous $\mathrm{CO}_{2}$ and water vapor tensions
would remain constant for a given tissue metabolic rate but the venous oxygen tension would vary depending on the arterial oxygen level. In modifying VWAL18 for use with air the first thing that was done was to postulate a metabolic rate for each tissue compartment which would then specify a particular arterial-venous oxygen concentration difference. This concentration difference could then be converted to a partial pressure change using the mathematical representation of the hemoglobin dissociation curve as previously discussed. At each depth, the difference between the venous $\mathrm{PO}_{2}$ while breathing air and while breathing a constant 0.7 ATA $\mathrm{PO}_{2}$ could be computed. At a depth of 77 FSW , air has a $\mathrm{PO}_{2}$ of 0.7 ATA so this difference would be zero. At shallower depths, air has a lower $\mathrm{PO}_{2}$ than 0.7 ATA so this difference would be negative. That is the venous oxygen tension breathing air would be lower than that breathing a $0.7 \mathrm{ATA} \mathrm{PO} 2_{2}$. Deeper than 77 FSW air has a $\mathrm{PO}_{2}$ greater than 0.7 ATA and the difference would be positive. The inert gas tension is computed as:

$$
P_{V_{N_{2}}}=P_{A M B}-\left(P_{V_{0_{2}}}+P_{V_{C 0_{2}}}+P_{H_{2}}\right)
$$

and as previously mentioned if the arterial oxygen tension is constant, the sum $\left(\mathrm{PVO}_{2}+\mathrm{PVCO}_{2}+\mathrm{PH}_{2} \mathrm{O}\right)$ is constant. However, if the tissue oxygen tension is increased above 0.7 ATA , and one desires to keep the total venous gas tension constant, then the $\mathrm{PVN}_{2}$ must be reduced by exactly the amount hat the $\mathrm{PVO}_{2}$ increassd. Conversely, when breathing air shallower than 77 FSW , the $\mathrm{PVO}_{2}$ will be decreased and the $\mathrm{PVN}_{2}$ is increased by that amount to keep total gas tension constant. Initially, a tissue extraction of 2.39 Vol. \% was chosen empirically for all tissues based on experimental dive results at different $\mathrm{PO}_{2}$ levels, as will be discussed later. Based on this, VVALI8 was adjusted by subtracting the difference between the calculated venous oxygen tension on air less the oxygen tension breathing 0.7 ATA $\mathrm{PO}_{2}$ from each MPTT value. This initial modification of VVALl8 resulted in VVAL22. Although the MPTT Tables VVAL22-29 were modified several times, these venous oxygen tension differences were not changed and are reflected in the difference in MPTT values between VVAL28 and VVAL29. VVAL29 was constructed for a constant $\mathrm{PO}_{2}$ of 0.7 ATA in the breathing gas and each tissue increases its MPTT exactly 10 FSW for each 10 FSW increase in depth (Appendix D). At 0 FSW, the decrease in venous oxygen tension breathing air was calculated to be 0.76 FSW ( 17.5 mmHg ) less than when breathing a $0.7 \mathrm{ATA} \mathrm{PO}_{2}$. Thus, the inert gas tension could be increased by this amount and the total gas tension would be constant. The MPTT values at 10 FSW are those which can be safely sustained at 0 FSW but which must be attained before leaving 10 FSW . These are all 0.76 FSW larger in VVAL2 8 than in VVAL29 reflecting the difference in venous oxygen tensions due to the differences in assumed inspired oxygen tension. As depth increases, the differences between VVAL28 MPTT values and VVAL29 MPTT values decreases and in the 90 FSW row (these are values for leaving 90 FSW or being at 80 FSW ) the sign reverses and the VVAL28 MPTT's become smaller than VVAL29 values. Thus, VVAL28 and VVAL29 are the same MPTT's except VVAL28 is adjusted for varying inspired oxygen tensions assuming a constant $21 \%$ fraction.

The concept of using total tissue gas tension as the determıning factor in causing decompression sickness was used throughout the whole study. When the EL-MK 15/16 DCM-II was instituted, the equations for computing the venous oxygen tensions from inspired (Equations 1 through 4) were included in the model so that the MPTT Table could reflect total inert gas tension for any inspired $\mathrm{PO}_{2}$. However, in the EL-MK $15 / 16 \mathrm{DCM}-\mathrm{II}$, values for the postulated arterial venous shunt in the lung along with the postulated arterial venous oxygen concentration difference for each tissue had to be specified. The value for the lung shunt determines the difference between arterial and alveolar oxygen tension and was given a value of $0.17 \mathrm{Vol} . \%$ (A $4 \%$ shunt assuming a mixed venous oxygen of 40 mmHg and an alveolar value of 100 mmHg on air). This value was assumed independent of inspired oxygen tension. The assumed arterial venous oxygen concentration differences were assumed to be 2.39 Vol. \% throughout the study and are shown as the variable CAV02 in MPTT Tables VVAL50-59 in Appendix D.

The venous $\mathrm{CO}_{2}$ tension was reduced to 1.87 FSW for all MPTT's (VVAL22-59) from the 2.30 FSW value used in the original EL-MK $15 / 16$ DCM using VVAL18. The arterial $\mathrm{CO}_{2}$ value was 1.7 FSW for the entire study which was increased from the 1.5 FSW value used with VVAL18. The gas phase overpressures (PBOVP) were adjusted empirically as testing progressed, these were all set to 0 in the original model.

## RESULTS

The dive series described here was done in three phases, the first phase being subdivided into two parts. Phase 1 A was done over the period from August 23 - September 20, 1984, and Phase 1B from October 3 - October 26. Phase 1 focused mainly on air bound dives but some 38 man dives using a constant $0.7 \mathrm{ATA}_{\mathrm{PO}}^{2}$ in $\mathrm{N}_{2}$ were done in the last part of Phase 1B. Phases 1 A and 1 B consisted of 465 man-dives which resulted in 23 cases of decompression sickness. Results in chronological order are given in Table 4 and detailed descriptions of all cases of DCS are found in Tables B-1 and B-2 of Appendix B. Phase 2 was done over the period from November 5 through November 30, 1984 and consisted of 197 man dives resulting in 17 cases of DCS. This phase consisted of bounce dives, repetitive dives and dives where the breathing gas was changed from air to a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ during decompression. Results in chronological order are given in Table 5 and detailed descriptions of all cases of DCS are found in Table B-3 of Appendix B. Phase 3 went from the loth through the 20 th of December, 1984 and looked mainly at multiple level and repetitive dives. There were 175 man dives done resulting in 9 cases of DCS. There were 175 man dives done resulting in 9 cases of DCS. The chronological results are given in Table 6 and detailed descriptions of all cases of DCS are given in Table B-4 of Appendix B.

The results of all dives grouped according to the type of dive are summarized in Table 7 and 8 . There were 612 man dives on bounce profiles resulting in 29 cases of DCS and 225 man dives on repetitive or multiple level
profiles resulting in 20 cases of DCS. The entire dive series encompassed 837 man dives resulting in 49 cases of DCS. In Table 8 it should be noted that the two cases of DCS in dive tenders have not been included in the dive results. These will be discussed separately.

The chronological sequence of events as given in Tables 4-6 shows that each phase consisted of more than one type of dive (air no-decompression, decompression, constant $0.7 \mathrm{ATA}_{\mathrm{PO}_{2}}$, etc.) and it was this sequence of events which influenced changes in the model as testing progressed. In this section the results will be presented according to the type of profile, some of which spanned several phases. The detailed reasons for adjusting the model based on the chronological sequence of events will be presented in the Discussion section of this report.

## Air No-Decompression Bounce Dives

Table 7 includes the results of all of the 197 man dives done to test no-decompression limits on air. These schedules are identified as the ones with the bottom times in [ ]. No-decompression limits were tested at 60,100 , 120, 150 and 190 FSW. As previously described, the bottom times for these dives were chosen so that a stop time of at least 30 sec was accumulated at 10 FSW and upon arrival at 10 FSW a stop was taken until the stop time decreased to 30 sec at which time the diver surfaced. Thus, in no case were dives less than the predicted no-decompression limit and in most cases divers surfaced having taken only a portion of the calculated decompression time. All of these conditions were taken to mean that the no-decompression limits were tested under conditions of maximum decompression stress. The no-decompression limits tested were all longer than found it he current U.S. Navy Standard Air Tables (6). The 66 min bottom time at 60 FSW is 6 min longer than current air no-decompression limits, the 30 min time at 100 FSW is 5 min longer, the 24 min time at 120 FSW 9 min longer, the 14 min time at 150 FSW 9 min longer, and the 10 min time at 190 FSW 5 min longer. These increased bottom times ranged from $10 \%$ to $100 \%$ greater than current air no-decompression bottom times and the fact that no cases of DCS occurred in the 107 man dives is a testament to the safety of the tested no-decompression limits. Table 10 compares the current air no-decompression limits with the tested limits.

## Air Decompression Bounce Dives

Table 7 summarizes the results of these dives. Of the dives shown in this table, 367 man-dives were Air Decompression Bounce Dives accounting for all 25 cases of decompression sickness (DCS). Three methods of determining decompression schedules were used. Schedules from the U.S. Navy Standard Air Tables (6) were used for some dives and were usually chosen as the next longer schedule than called for by the actual bottom time of the dive. Choosing the next longer schedule is standard procedure for cold hard-working dives (reference 6, Sect: 7.2.3). There were a total of 4 depth/bottom time combinations on which Standard Air Schedules were used $60 \mathrm{FSW} / 100 \mathrm{~min}, 60 / 180$,

TABLE 4
Phase 1 TEST dive results
Bottom Time (min)* Total Man Dives/DCS (Type)
All Dives on Air Unless Otherwise Noted


* All Bottom Times include $60 \mathrm{FSW} / \mathrm{min}$ descent time. Times in [ $]$ are no-decompression time.
\# Where Standard Air Schedules were used, depth/time of schedule used is indicated in this column, otherwise 23 Cases DCS VVAL number of the MPTT Table used to compute the schedule is shown.
- valal29 dives all constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ dives.

Letters Key DCS to Description in Appendix $B$


All Bettom times include $60 \mathrm{fsw} / \mathrm{min}$ descent time
197 Man Dives
17 Cases Dés Profiie No refers to Table 2
©VAL2 aives ail constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ ．
Le：ters Key Oís to Vescridition in Appendix $B$

TABLE 6
PHASE 3 TEST OIVE RESULTS
Bottom Time（min）or Profile No．＂Total Man Dives／DCS（Type）
All Dives on Air Unless Otherwise Noted

| $\begin{gathered} \text { DATE } \\ \hline \quad 1984 \\ \hline \end{gathered}$ | H00 | $\begin{gathered} 50 \mathrm{FSW} \\ \mathrm{~A} \cdot \mathrm{P} \boldsymbol{1} \mathrm{PO} \end{gathered}$ |  | REPEIS | 100 FSW | REPETS | 120 FS | REPETS | 150 FS | REPETS | $\begin{aligned} & \text { MUTT-LCVEL } \\ & \text { AUP } 7 \text { Fl } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12！19 | Wulst． | ．．－．－－．．－ | No． 29 | 2011（1）${ }^{*}$ |  |  |  |  |  |  |  |
| 12／11 | VVAL53 |  | No． 28 | 10／1（1）w | No． 31 | 10／2（1）${ }^{\text {\＃}}$ |  |  |  |  |  |
| 12／12 |  |  | No． 27 | 1010 | No． 31 | 9／0 |  |  |  |  |  |
| 12／13 |  |  | $\begin{aligned} & \text { No. } 28 \\ & \text { No. } 29 \end{aligned}$ | $\begin{aligned} & 10 / 1 / 1 / \mathrm{y} \\ & 9 / 0^{e} \end{aligned}$ |  |  |  |  |  |  |  |
| 12／14 |  |  | No． 27 | 10／0 |  |  |  |  |  |  | No． 38 10／1（1）2 |
| 12／17 | VVAL59 |  |  |  |  |  | No． 32 | 1010 |  |  | No． 37 10／1〈1）dd 1（1） |
| 12／18 |  |  |  |  |  |  |  |  | No． 33 | 10／0 ${ }^{\text {S }}$ | No． 38 8／111700 |
| 12／19 |  |  |  |  |  |  | No． 32 | 10／0 |  |  | No． $37 \quad 10 / 0$ |
| $12 / 25$ |  | $120 \mathrm{~mm} 19 / 0$ |  |  |  |  |  |  |  |  |  |
| ＊All Bottom times include $60 \mathrm{r} \mathbf{5} / \mathrm{min}$ descent time <br> リち Man［い口•• Profile $N$ a refers to rable 2. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

＊OCS in render not shown．See tert and table B－A
d 10 divers completed ist dive
3 Bottom T me of 2 ad dive 2 min longer than planned because of technical error
Letters key OCS to Description in Adpendix B

TABLE 7
RESULTS OF BOUNCE DIVES TESTED
AIR

| Profile No. | $\begin{aligned} & \text { Depth/Time } \\ & \text { (FSW)/(min) } \end{aligned}$ | Std. Air | VVAL22 | VVAL25 | VVAL26 | VVAL28 | $\begin{array}{r} \text { VVAL53 } \\ 154 \\ \hline \end{array}$ | TOTALS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 50/240 |  |  |  |  | 20/0 |  | 20/0 |
| 2 | 60/[66] |  |  |  | 29/0 |  |  | 29/0 |
| 3 | /100 | 9/0 a |  |  |  |  |  | 9/0 |
| 4 | /120 |  |  |  |  | 18/0 |  | 18/0 |
| 5 | /180 | $10 / 3 \mathrm{~b}$ | 20/1 | 10/4 |  |  |  | 40/8 |
| 6 | 80/120 |  |  |  |  |  | 18/1 | 18/1 |
| 7 | 100/[30] |  |  | 20/0 |  |  |  | 20/0 |
| 8 | $/ 60$ | 38/0 c | 30/0 |  |  |  |  | 68/0 |
| 9 | 190 |  |  |  |  | 19/0 |  | 19/0 |
| 10 | 120/[24] |  |  |  |  | 19/0 |  | 19/0 |
| 11 | 160 | 20/1 d |  |  |  | 29/1 |  | 9/0 |
| 12 | 170 |  |  |  |  | 10/2 |  | 18/0 |
| 13 | /80 |  |  |  |  | 10/2 |  | 10/2 |
| 14 | 150/[14] |  |  | 20/0 |  |  |  | 20/0 |
| 15 | 140 |  |  |  | 29/2 | 28/1 |  | 57/3 |
| 16 | 160 |  | 20/5 |  |  |  |  | 20/5 |
| 17 | 190/[10] |  |  | 20/0 |  | 19/0 |  | 19/0 |
| 18 | 130 |  |  |  |  | 19/0 |  | 19/0 |
| 19 | 140 |  |  |  |  | 10/2 |  | 10/2 |
|  | TALS | 77/4 | 70/6 | 50/4 | 58/2 | 20/8 | 18/1 | 474/25 |

a - 60/100 Std. Air Schedule Used.
b - 60/200 Std. Air Schedule Used.
c - 9/0 Using 100/60 Std. Air Schedule.
29/0 Using 100/70 Std. Air Schedule.
d -120/70 Std. Air Schedule Used.
\#-Times in [ ] are no-decompression times.
CONSTANT 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$

| 20 | $100 / 60$ |  |  |
| :---: | :---: | :---: | :---: |
| 21 | $150 / 30$ |  |  |
| 22 | 140 |  |  |
| 23 | 160 | Al1 Dives Used VVAL29 | $27 / 0$ |
|  |  |  | $19 / 0$ |
| TOTALS |  | $9 / 2$ |  |

AIR $\rightarrow$ CONSTANT 0.7 ATA $\mathrm{PO}_{2}$ IN $\mathrm{N}_{2}$

| 24 | $60 / 120$ |  |  |
| :--- | :--- | :--- | :--- | :--- |
| 25 | $100 / 90$ |  |  |
| 26 | $150 / 40$ |  |  |
|  | TOAIS | VVAL59 | $19 / 0$ |
|  | VVAL52 | $19 / 0$ |  |
|  |  | VVAL52 | $19 / 0$ |$|$

TABLE 8

RESULTS OF REPETITIVE/MULTI-LEVEL DIVES TESTED

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Profile No. \& VVAL28 \& VVAL50 \& VVAL52 \& VVAL54 \& VVAL5 \& VVAL56 \& VVAL58 \& VVAL59 \& TOTALS <br>
\hline \& \multirow[b]{11}{*}{$$
\begin{aligned}
& 9 / 3 \\
& 7 / 0
\end{aligned}
$$} \& \multirow[b]{11}{*}{9/2} \& \multirow{11}{*}{$10 / 2$

$8 / 1$} \& \multirow[t]{11}{*}{1
$10 / 3$} \& \multirow[t]{11}{*}{$R$

$16 / 0$} \& \multirow{11}{*}{20/1\#} \& \multirow{11}{*}{\[
$$
\begin{gathered}
20 / 0 \\
20 / 2 \\
9 / 0 \\
\\
19 / 2
\end{gathered}
$$

\]} \& \multirow{11}{*}{\[

$$
\begin{aligned}
& 20 / 0 \\
& 10 / 0
\end{aligned}
$$
\]} \& <br>

\hline 27 \& \& \& \& \& \& \& \& \& 20/0 <br>
\hline 28 \& \& \& \& \& \& \& \& \& 20/2 <br>
\hline 29 \& \& \& \& \& \& \& \& \& 29/1 <br>
\hline 30 \& \& \& \& \& \& \& \& \& 36/5 <br>
\hline 31 \& \& \& \& \& \& \& \& \& 19/2 <br>
\hline 32 \& \& \& \& \& \& \& \& \& 20/0 <br>
\hline 33 \& \& \& \& \& \& \& \& \& 10/0 <br>
\hline 34 \& \& \& \& \& \& \& \& \& 8/1 <br>
\hline 35 \& \& \& \& \& \& \& \& \& 9/3 <br>
\hline 36 \& \& \& \& \& \& \& \& \& 16/2 <br>
\hline \multicolumn{9}{|c|}{Total Air Repetitive Dives} \& 187/16 <br>

\hline \& \& \& $$
\text { AIR } \rightarrow
$$ \& CONSTAN Mul \& \[

0.7 \mathrm{ATA}
\]

i-Level \& $\mathrm{PO}_{2}$ in \& $$
\mathrm{N}_{2} \quad 1
$$ \& \& <br>

\hline 37 \& \& \& \& \& \& \& \& 20/2 \& 20/2 <br>
\hline 38 \& \& \& \& \& \& \& 10/1 \& 8/1 \& 18/2 <br>
\hline \& tal Mul \& ti-Lev \& 1 Dives \& \& \& \& \& \& 38/4 <br>
\hline Total
All \& 16/3 \& 9/2 \& 18/3 \& 10/3 \& 16/0 \& 20/1 \& 78/5 \& 58/3 \& 225/20 <br>
\hline Dives \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

\# DCS in Tender Not Shown. See Text and Table B-4.

TABLE 9

ASCENT CRITERIA BLOOD PARAMETERS
All values in FSW except for those in parenthesis ( ) which are in Volume \%.

|  | ${ }^{\mathrm{P}_{\mathrm{A}}} \mathrm{CO}_{2}$ | $\mathrm{P}_{\mathrm{H}_{2} \mathrm{O}}$ | $\mathrm{PV}_{\mathrm{CO}_{2}}$ | $\mathrm{PVO}_{2}$ | $\mathrm{AMBAO}_{2}$ | PBOVP | $\Delta \mathrm{P} / \Delta \mathrm{P} \\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VVAL18 | 1.5 | 0.0 | 2.30 | 2.0 | 0 | 0 | 10 |
| $\begin{array}{r} \text { VVAL22 } \\ -28 \end{array}$ | 1.7 | 2.0 | 1.87 | 2.8 | 2.46 | 10 | 10@ |
| VVAL29 | 1.7 | 2.0 | 1.87 | 2.8 | 2.46 | 10 | 10 |
|  |  |  |  | CAV02 | DAA02 |  |  |
| VVAL50 | 1.7 | 2.0 | 1.87 | (2.39) | (0.17) | 10 | 10 |
| $\begin{array}{r} \text { VVAL52 } \\ -59 \end{array}$ | 1.7 | 2.0 | 1.87 | (2.39) | (0.17) | 7-36* | 10 |

\# Increase in MPTT for every 10 FSW depth increase.
@ Values adjusted at each depth for changing $\mathrm{PO}_{2}$, see text.

* Different PBOVP specified for each tissue, see Appendix D.

The Surfacing tissue Tensions, and Saturation Desaturation Ratios (SDR's) were varied according to dive results. PBOVP values were changed for WVAL52-59 only.

For Symbol Definition, see Table 3.

TABLE 10

## NO-DECOMPRESSION LIMIT COMPARISONS

| Depth (FSW) | USN Standard Air Limits | Tested Limits | Final VVAL59 Limits |
| :---: | :---: | :---: | :---: |
| 30 | 360\# |  | $\alpha$ |
| 40 | 200 |  | 167 |
| 50 | 100 |  | 88 |
| 60 | 60 | 66 | 61 |
| 70 | 50 |  | 47 |
| 80 | 40 |  | 39 |
| 90 | 30 |  | 31 |
| 100 | 25 | 30 | 26 |
| 110 | 20 |  | 22 |
| 120 | 15 | 24 | 20 |
| 130 | 10 |  | 18 |
| 140 | 10 |  | 16 |
| 150 | 5 | 14 | 14 |
| 160 | 5 |  | 12 |
| 170 | 5 |  | 10 |
| 180 | 5 |  | 9 |
| 190 | 5 | 10 | 9 |

[^0]$100 / 60$, and $120 / 60$. The next longer Standard Air Schedule was for all the 60 FSW/180 min depth/bottom time dives, all the $120 / 60$ dives and 29 man dives at 100 FSW for 60 min . The Standard Air Schedule with the actual bottom dove was used for the $60 / 100$ and 9 man-dives on the $100 / 60$ depth/bottom time combinations. The EL-MK $15 / 16$ DCM-I was used to compute all VVAL22-28 schedules and the EL-MK 15/16 DCM-II was used for the VVAL53/54 schedules as shown in Table 7.

The success of the Standard Air No-Decompression Limits are in contrast to the abysmal failure of some of the Standard Air Decompression Tables. The most notable is the $60 / 180$ dive which was decompressed on the $60 / 200$ Standard Air Schedule. Appendix $E$ shows that this added 14 min to the total decompression time (TDT) compared to the $60 / 180$ Standard Air Schedule but the 3 cases of DCS in 10 man dives testify that this increase was insufficient (Table 4, Table ?). VVAL25 added another 40 min of decompression time but the DCS rate was increased to 4 cases in 10 man dives. One of these cases (subject 110, Table B-l Appendix B) was a particularly resistant case of shoulder pain. A further increase of 42 min of TDT using VVAL22 reduced the DCS incidence to 1 in 20 man-dives but even this small incidence was surfrising considering that the TDT had been increased by a factor of 2.15 over the $60 / 200$ Standard Air Schedule and 2.68 over the $60 / 180$ Standard Air Schedule.

In stark contrast was the experience using the 100 FSW Standard Air Schedules on the 100 FSW/60 min depth/time dives. After doing 29 DCS free dives on the $100 / 70$ Standard Air Schedules, 9 man-dives were done using the 100/60 Standard Air Schedule without experiencing any DCS. The initial study design had VVAL22 schedules being tested first and in retrospect the 100 min TDT was much longer than required. The $100 / 70$ Standard Air Schedule became one of the benchmark schedules and as the decompression model MPTT Tables were modified, it was always done with trying to get the resultant model to predict a decompression schedule for a $100 \mathrm{FSW} / 60 \mathrm{~min}$ dive with the same $\operatorname{TDT}$ as the 100/70 Standard Air Schedule.

The $120 / 70$ Standard Air Schedule was reasonably successful in decompressing a $120 / 60$ dive with only one mild shoulder pain in 20 man-dives. Increasing the TDT to 147 min using VVAL28 decreased the DCS incidence only slightly to 1 in 29 man-dives. The same MPTT, however, produced a considerable incidence of DCS when used to decompress from dives having a 80 and 70 min bottom time at 120 FSW (Tables 4,7 ).

The 150 FSW depth was considered important because that was the deepest depth used in the testing of the 0.7 ATA constant $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ decompression model (1). The VVAL22 air schedule as computed was over 2.5 times longer than the Standard Air Schedule but the 5 cases of DCS in 20 man-dives showed this increase was not adequate. When the bottom time at 150 FSW was reduced to 40 min, VVAL26 proved inadequate giving rise to 2 cases of DCS in 29 man-dives with a TIT over 1.4 times longer than the Standard Air Schedule. VVAL28 reduced the nCS incidence to 1 in 28 man-dives with a TDT 1.62 times longer than the $150 / 40$ standird Air Schedule (Appendix E, Table E-1).

By the end of thatit la the modifications to the MPTT Tables were being htavily influmet $\because \because$ be surts of the no-decompression limits, the success
of the $100 / 70$ Standard Air Schedule and the fact that the $60 / 180$ schedule as computed by VVAL22 did not appear overly conservative although it was 2.68 times longer than the Standard Air Schedule. The search was on for a model which would; (1) Retain the previously tested no-decompression limits, (2) Predict a decompression schedule for a $100 / 60$ dive with a TDT the same as for the $200 / 70$ Standard Air Schedule and, (3) Keep the $60 / 180$ schedule with the same TDT as computed by VVAL22. In addition, it should lengthen the TDT for $150 / 60$ dives beyond those predicted by VVAL22. VVAL28 was derived to fulfill these criteria but succeeded only partially as shown in Appendix E. The $100 / 60$ schedule was only 2 min longer than the Standard Air $100 / 70$ Schedule but the $60 / 180$ Schedule $T D T$ increased 23 min over that predicted by VVAL22. Also the $150 / 60$ schedule had 10 min less TDT than the previously unsafe VVAL22 schedule. In spite of these deficiencies it was used as a starting point for Phase 1B and indeed survived until the end of Phase 1.

Its success on the $50 / 240$ dive showed, if anything, it was too conservative for this long shallow dive. VVAL 28 predicted a schedule 11 min shorter than the VVAL22 schedule for a $60 / 120$ dive but produced no DCS in 18 man-dives. At 190 FSW safe decompression could not be accomplished using WhaL2 8 until the bottom time was shortened from 40 to 30 min even though the 40 min schedule was 2.22 times longer than the Standard Air Schedule and the 30 min schedule only 1.57 times longer.

By the end of Phase 1B, all air bounce diving had been completed except for one 80 FSW schedule for 120 min which was tested at the end of Phase 2 (Table 5). Although this schedule was dove using two different VVAL's (53 and 54) the profiles differed by only 1 min so the results were lumped together. In spite of increasing the TDT by a factor of 2.9 over the Standard Air Schedule there was 1 case of Eype 1 DCS in 18 man-dives.

The $60 \mathrm{FSW} / 100 \mathrm{~min}$ dive done using the Standard Air Schedules started out as a $60 / 180$ dive but was aborted for technical reasons after 100 min . There was no DCS in any of the 9 divers but the schedule was not tested again because of time constraints.

Table 11 summarizes the raw and expected binomial incidences of the air dives. The first line shows no-decompression dives and the second all Air Bounce Dives. Since the $60 / 180$ using the Standard Air Schedules and VVAL25 would fall outside the limits of the final model, these dives (and resulting DCS) can be excluded dropping the expected incidence as shown in the third line. Also, if one restricts the diving depth/bottom domain to $120 / 60$, 150/40, and $190 / 30$ another 50 man-dives and 11 cases of DCS can be eliminated, resulting in an overall expected incidence of $3.2 \%$. However, all the DCS resulted from decompression dives and if these are separated from no-decompression dives, the expected incidence is $4.2 \%$ while for no-decompression dives it is $2.7 \%$ (Table 11).

## Constant 0.7 ATA P02 in N 2 Bounce Dives

All of the 0.7 ATA constant $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ dives were done using VVAL29 and the EL-MK 15/16 DCM I during the last week of Phase 1 B (Table 4) and the first

TABLE 11
DECOMPRESSION SICKNESS INCIDENCE

| Dive Type | Man-Dives | DCS | Incidence |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Raw |  |
| No-Decompression Air | 107 | 0 | 0.0\% | 2.7\% |
| All Air Bounce Dives | 474 | 25 | 5.3\% | 7.1\% |
| Exclusive of $60 / 180$ on VVAL25 \& Std. Air | 454 | 18 | 4.0\% | 5.8\% |
| Limited (All) | 404 | 7 | 1.7\% | 3.2\% |
| Domain*(Decomp. <br> Only) | 297 | 7 | 2.4\% | 4.2\% |
| All 0.7 ATA N202 Dives | 81 | 4 | 4.9\% | 11.3\% |
| Limited Depth/Time Domain" | 46 | 0 | 0.0\% | 6.3\% |
| Air $\rightarrow 0.7$ ATA <br> Bounce Dives | 57 | 0 | 0.0\% | 5.1\% |
| No-Decompression Repetitive Dives | 154 | 10 | 6.5\% | 11.0\% |
| All Repetitive Dives | 187 | 16 | 8.6\% | 12.0\% |
| Exclusive of Profile 30 on VVAL52 \& 54 | 134 | 5 | 3.7\% | 7.2\% |

[^1]week of Phase 2 (Table 5). As 2zeviously descrited in the Ascent Criteria portion of the Methods Section, VVAL29 is VVAL28 adjusted for the theoretical differences in venous $\mathrm{PO}_{2}$ breathing a constant 0.7 ATA $\mathrm{PO}_{2}$ compared to air at the various depths. Thus, VVAL28 and VVAL29 represent the same decompression model. The results of all dives are summarized in Table 7. A complete set of 0.7 ATA $\mathrm{O}_{2}$ in $\mathrm{N}_{2}$ schedules using the EL-MK $15 / 16 \mathrm{DCM}$ and VVAL18 had already been previously tested and published (1, 8).

The $100 \mathrm{FSW} / 60 \mathrm{~min}$ schedule produced no DCS in 27 man-dives in spite of a $28 \%$ ( 18 min ) reduction in TDT from the previously tested VVAL18 schedule (2) (Table E-2, Appendix E). The success of this reduction was particularly gratifying because during the original testing of the $0.7 \mathrm{ATA}_{\mathrm{PO}}^{2}$ in $\mathrm{N}_{2}$ Decompression Tables (8), a schedule having a TDT 8 min longer than the VVAL29 schedule gave 1 case of DCS in 10 man-dives. This previously tested MVAL5 schedule (reference 1, Profile 8, Appendix C) did, however, have decompression stops beginning at 50 FSW , some 20 FSW deeper than the first stop for the VVAL29 schedules.

A 150 FSW/30 min schedule produced no DCS in 19 man-dives in spite of a 30 min (46\%) reduction in TDT from the previously tested VWALI8 schedule (1). In the original testing of the constant $0.7 \mathrm{ATA} \mathrm{O}_{2}$ in $\mathrm{N}_{2}$ decompression schedules, attempts had been made to develop a safe 150/60 schedule which were abandoned due to time constraints and a high incidence of DCS (1, 8). During Phase 1 of this earlier testing (1) schedules with about $130-135 \mathrm{~min}$ TDT appeared safe but later produced an unacceptable incidence of DCS. While the final VVAL18 schedules contained a $150 / 60$ schedule, this was not tested and the bottom time restriction at 150 FSW was set as 30 min . Since the untested VVALI8 schedule had a TDT 77-86 min longer than the earlier $150 / 60$ schedules which had been previously tested and since VVAL29 predicted a further 5 min increase in TDT it was thought that this $150 / 60$ schedule would prove successful. The two cases of DCS in 9 man-dives using VVAL29 showed this increase was not adequate and shortening the bottom time to 40 min reduced the DCS incidence to 2 cases in 26 man-dives which was, however, still unacceptably high. So in the end, reduction in TDT were possible within the previously determined depth/time restrictions applied to VVALI8 (1) without an increased incidence of DCS. Profiles tested outside of this restriction at 150 FSW still produced an unacceptably high incidence of DCS. The final version of the decompression model (VVAL59) resulting from tesing in this study would have lengthened the TDT for the $150 / 60$ profiles by another 60 min but time was not available to test this profile. Table 11 shows the expected incidences of DCS based on the limited testing of these constant 0.7 ATA $\mathrm{PO}_{2}$ schedules but the number of dives was too small to obtain significant predictions.

## Air $\rightarrow$ Constant 0.7 ATA P02 in N 2 Bounce Dives

Up through the middle of Phase 2, testing of the decompression model in real time switching from a constant fraction to a constant percentage of oxygen would not have been possible since the MPTT Tables had to be adjusted
to suit the two different conditions. With the irtroduction of the EL-MK 15, : 0 DCM-II, a single MPTT Table would suffice for both conditions so testing could progress.

Initial testing using VVAL52 focused on 100 FSW and 150 FSW at the maximum bottom times which produced safe profiles on air dives. In all of these dives, a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ was breathed from the MK 15 UBA during descent then air was breathed from arrival on the bottom to arrival at the first stop. At the first stop, a switch was made back to the constant 0.7 ATA PO 2 in $\mathrm{N}_{2}$ breathing medium of the MK 15 and this was breathed to the surface. No DCS Was observed on the 100 FSW and 150 FSW profiles (Table 7) in spite of some impressive reductions in TDT. VVAL52 reduced the TDT for the 100/90 schedule with breathing gas switching by $42 \%$ compared to the VVAL28 air schedule (Table E-1, E-2; Appendix E). The TDT for the $150 / 40$ profile with breathing gas siwtching was reduced $39 \%$ compared to a schedule breathing air throughout.

The 60 FSW/ 120 min profiles was tested with breathing gas switching because VVAL59 predicted a $42 \%$ reduction in TDT compared with the previously tested VVAL28 schedule on air while for the $60 / 180$ schedule the reduction was only $33 \%$ compared with the previously tested VVAL22 air profile (Appendix E). No cases of DCS resulted from the 19 man-dives on this schedule.

The overall results of switching to the higher $\mathrm{PO}_{2}$ during decompression showed that the EL-MK $15 / 16$ DCM-II could adequately handle these $\mathrm{PO}_{2}$ changes. The overall impression from the dive series is that further reductions may have been possible but unfortunately, time was not available for further testing of these profiles. Table 11 shows the expected incidences for this limited testing.

## Air Repetitive Dives

Testing of Air Repetitive Dive profile began in Phase 2 (Table 5) and continued through Phase 3 (Table 6). A total of 187 man-dives were done resulting in 16 cases of DCS and the results are summarized in the the top portion of Table 8 . A total of 10 different repetitive dive profiles were used (Table 2) with 7 being no-decompression and 3 being decompression. The no-decompression profiles were constructed such that both the effects of increasing depth and increasing surface interval could be tested. A series of two no-decompression repetitive dives separated by a 60 minute surface interval at $80,100,120$ and 150 FSW was used to test the effect of increasing depth. Three different surface intervals at 80 FSW served to test the effect of increasing surface interval time. Finally, three successive no-decompression dives at 100 FSW were done to see if the model could handle multiple repetitive dives.

Table E-3 of Appendix E compares the various no-decompression profiles. For all profiles computed by the decompression models tested in this study the no-decompression times for each dive are given in the appropriate "Excursion" column. The first two line entries for each profile show two Standard Air

Table comparisons. The first line shows what the no-decompression times for each excursion would have been if Standard Air Repetitive diving procedures had been followed. If the Residual Nitrogen Time was greater than the no-decompression time, this difference is shown as a negative number. The second line of the "Std Air" entry for each profile shows the amount of decompression time which would have been required for the bottom time enclosed in \{ \}. The first column \{bottom time\} entry shows a typical bottom time actually used in testing. The TDT is given in the TDT column. In succeeding columns the \{bottom time\} is shown with the Residual Nitrogen Time as determined by the Standard Air Repetitive Diving Procedures enclosed in [ ]. The TDT for the Standard Air Decompression schedule with a time equal to the sum of the \{bottom time\} and [Residual Nitrogen Time] is given in the TDT column.

Table E-4 compares the decompression schedules for the three decompression repetitive dive profiles tested, the decompression schedules for the first and second dives shown in the appropriate column.

Decompression Rovetitive Dives:
The first repetitive dive profiles tested were the repetitive decompression profiles at 100 and 150 FSW, Profiles 34,35 and 36 . These profiles were tested during the transition from the EL-MK $15 / 16$ DCM-I to the EL-MK 15/16 DCM-II. VVAL50 was the first MPTT used with the EL-MK 15/16 DCM-II and was calculated to give decompression profiles as close to VVAL28 (using the DCM-I version) as possible.

The 150 FSW repetitive decompression profile (\#36) initially appeared safe, resulting in no DCS in 7 man-dives using VVAL28. When dove again on VVAL50, however, two mild Type I DCS occurred after the second dive (Table 5, Table B-3, Appendix B). Unfortunately, the VVAL28 and VVAL50 profiles were not identical although the small differences were thought to be insignificant. Compared to the Standard Air Profile, however, the decompression times for both the VVAL 28 and the VVAL50 profile were considerably longer. The TDT for the first dive was $63 \%$ to $69 \%$ longer for the computed tables compared to Standard Air Tables and for the second dive $82 \%$ to $77 \%$ longer. On the first dive the decompression stops as computed using the Decompression Models began 10 FSW deeper and were longer at every depth than the Standard Air Table but for the second dive, the decompression model predicted a shallower first stop and a much longer 10 FSW than the Standard Air Table.

The first 9 man-dives on the 100 FSW Profile $\$ 35$ produced 3 cases of DCS. One of these occurred during the surface interval but the diver did not report it and made the second dive after which the pain recurred. Another of the cases of DCS occurred at the 10 FSW stop of the second dive. VVAL52 was created which increased the TDT for both portions of Profile $\# 35$. However, in order to keep testing within a reasonable working day, the second bottom time
 the shorter repetitive bottom time had almost the same TDT as Profile $\# 35$.

ご：ミ こここ ：ncidence ias 1 case in 3 mar－dives blit the pain only sjmptom occurred A＝ 70 FS\％during ascent from the first dive．The circumstances of this symptom（Table $\bar{B}-3$ ，Appendix B）were very unusual and further testing of this profile wouid have been carried out had time allowed．Like Profile $\# 36$ ， Profiles $; 34$ and $\# 35$ predicted significantly longer decompressions than Standard iir Tables for both the first and second dives as shown in Table E－4 of Appendix $E$ ．

The overall raw incidence of DCS for the three repetitive decompression profiles was 6 cases in 33 man－dives or $18 \%$ ．However，the number of trials was too small to draw any statistically significant inferences from them．

No－Decompression Repetitive Dives：
Initial testing of the no－decompression repetitive dives began at the end of Phase 2 with the double 100 FSW Profile $\# 30$（Table 2）．The initial dive using VaLj2 used the previously tested 30 min no－decompression limit which had produced no DCS in 20 man－dives．However，of the 2 cases of DCS which occurred on the first 10 man－dives，one was during the surface interval． VVAL54 shortened the first no－decompression limit by over 1 min and shortened the second no－decompression time by almost 2.5 min （Table E－3，Appendix E）but this resulted in 3 cases of DCS in 10 man－dives．The disconcerting thing here is that all three symptoms occurred after the lst dive，and none of the seven subjects who completed the second dive had any symptoms．There was no procedural reasons which accounted for this rash of DCS on a schedule previously thought to be safe except that these dives were done late in the Phase 2 studies and diver fatigue may have played a role．This phenomenon had been seen previously during Phase $I$ testing of the constant 0.7 ATA PO 2 in $\mathrm{N}_{2}$ Decompression Schedules（8）．At the end of Dive Series I of this previously reported testing，the DCS incidence on profiles having had 25－27 DCS－free dives increased for no apparent reason（reference 8，Table 3）and diver fatigue was postulated．

The next MPTT used fo：the 100 FSW no－decompression repetitive dives was VVAL55 which reduced the first no－decompression time to 26.5 min （only 1.5 min longer than the Standard Air Table limit）but increased the second no－decompression limit to just over 20 min ．Two of the divers who suffered DCS on the VVAL54 schedule dove the VVAL55 schedule（Table C－3，Appendix C） and there was no DCS in 16 man－dives．

In testing the triple 100 FSW repetitive dive（Profile \＃31），VVAL58 retained the 26.5 min no－decompression time for the first dive but reduced the second to 17.74 min ．This no－decompression time was only reduced an additional 1.85 min for the third dive．The two cases of DCS which occurred in the 19 man－dives performed both occurred after completion of the third dive．However，there was a bizarre case of DCS in the dive tender（Subject \＃122）who was in a warm dry chamber some 7 FSW shallower than the diver subjects for the entire dive（Table B－4，Appendix B）．This individual had participated as a diver subject in Phase $1 B$（Table $C-2$ ，Appendix $C$ ）and made 8 dives resulting in $l$ case of DCS after a $120 / 70$ dive on VVAL28（Table B－2， Appendix B）．
The double dive no-decompression profiles with a 50 min surface interval at 80,120 and 150 FSW (Profiles 427,32 and 33 ) produced no DCS in 50 man-dives. If one combines these results with the 16 DCS-free dives on the 100 FSW profile ( $\$ 30$ ) using VVAL55 the expected incidence assuming a binomial distribution is $5.2 \%$ at the $95 \%$ confidence level. The savings in decompression time on these profiles are substantial as shown in the comparisons of Table E-3 of Appendix E. On the 80 FSW profile (\#27) the no-decompression limit for the second dive was almost tripled and 19 min of decompression time saved compared to Standard Air Tables. On the 100 ESW profiles, the 26 min Residual Nitrogen Time resulting from the first dive would have precluded no-decompression diving on the second if Standard Air Tables had been used. The EL-MK $15 / 16$ DCM-II saved some 28 min of TDT on the second and 39 min on the 3rd dive. Similarly, for the 120 and 150 FSW profiles, the Standard Air Tables would have required decompression from both the first and second dives for bottom time tested. As far as the 60 min surface interval double repetitive dives are concerned, it appears substantial amounts of decompression time required by the Standard Air Tables can be safely eliminated. The ability of the decompression model to safely handle a third no-decompression repetitive dive was not sufficiently tested.
The ability of the EL-MK $15 / 16$ DCM-II to handle 80 FSW no-decompression repetitive dives with surface intervals greater than 60 min is not as clear cut. With a 95 min surface interval (Profile 28), VVAL58 increased the no-decompression time for the second dive by $32 \%$. This 30 min bottom time was 18 min longer than allowed by the Standard Air Tables. Two mild cases of DCS occurred in 20 man-dives. After a 180 min surface interval (Profile 29), the no-decompression time for the second dive had increased to within a minute of the initial dive limit using VVAL56 and one case of Type I DCS occurred in 20 man-dives. However, one of the trunk tenders suffered Type I symptoms in spite of being in a warm chamber and 7 FSW shallower than the diver subjects. This subject (\#118) had made 13 dives during Phase $1 B$ and 2 (Table C-2, 3; Appendix C) and suffered only 1 case of Type I DCS. He was breathing air throughout and was warm. After this incident, dive tenders began breathing mixes with $\mathrm{PO}_{2}$ levels higher than air during these types of dives. VWAL58 shortened the second no-decompression time by about 2 min compared to VVAL56 and produced 9 DCS-free dives. Considering that the one case of DCS on VVAL56 was mild and that WAL58 had shortened the second no-decompression limit, no further testing of Profile \#29 was done.
Table 11 summarizes the DCS incidences for the air repetitive dives. Overall there was an $8.6 \%$ raw incidence of DCS. The three decompression profiles ( $34,35,36$ ) resulted in 6 cases of DCS in 33 man-dives ( $18 \%$ raw incidence) but were considerably lengthened by the final VVAL59 MPTT. Unfortunately, time for retesting them was not available. If one just looks at the no-decompression repetitive dives, excluding the decompression dives, the raw incidence drops to $6.5 \%$ but the expected incidence drops only slightly. Profile \#30, using VVAL52 and 54, was considerably changed by VVAL55 resulting in a lowered DCS incidence. Excluding these VVAL52 and 54 dives, the expected incidence for no-decompression repetitive dives drop to 7.2\%.


#### Abstract

The overall results of the testing $:$ Ethe dir Mo－Decompression Rapetitive dives indicated that considerable amounts of decomprression could be saved compared to the requirements of the Standard Air Tables．This is in contzas： to the decompression repetitive dives where substantial increases in TDT were required compared to the Standard Air Tables．The two cases of DCS in the tenders during no－decompression repetitive dive testing was disturbing， however，and may indicate that increased gas uptake in the warm chamber environment more than offset the 7 FSW depth advantage of the tenders．


## Multi－Level Air／Constant 0.7 ATA P02 in N 2 Dives

There were two long multiple level dive profiles tested，both designed to see if the EL－MK 15／16 DCM－II would work with combined depth changes and breathing gas switches．Both of these profiles（\＃37，\＃38 Table 2）are essentially two dives on air separated by a 180－200 min interval breathing 0.7 ATA $\mathrm{PO}_{2}$ at 20 FSW ．Profile $⿰ ⿰ 三 丨 ⿰ 丨 三 38$ had a 20 min downward excursion to 100 FSW after 2 hrs at 20 FSW ．Unfortunately，time was not available to test these profiles using air throughout so the DCS incidence on air is unknown．Profile \＃38 was first tested using VVAL58 which resulted in a single case of Type I DCS which did not respond rapidly to treatment（Table B－4，Appendix B）．The Multi－Level Profiles were such that none of the intermediate excursions required decompression stops，so changing the MPTT＇s would only change the decompression to the surface from the last excursions．Table E－5 of Appendix $E$ shows the final decompression schedule which has only a single decompression stop at 10 FSW ．WVAL59 lengthened the TDT from the final 60 FSW excursion of Profile 38 by 7 min compared to VVAL58 but the incidence of DCS remained essentially unchanged with 1 case in 8 man－dives．Again this was a Type I symptom which did not respond rapidly to compression to 60 FSW（Table B－4， Appendix B）．Profile $⿰ ⿰ 三 丨 ⿰ 丨 三 一$ 37 produced 2 cases of DCS in 20 man－dives one of which occurred 72 hours after completion of the dive．During testing of these multi－1evel dives， 3 out of the 4 cases of DCS which occurred had recurrences during treatment which required recompression．


#### Abstract

There are no currently available procedures for computing decompression schedules for dives of this type except to use a Standard Air Schedule with the total bottom at the maximum depth as shown in the＂Std Air＂entry in Table E－5 of Appendix E．Profile $\# 37$ would have required decompression on an 80／360 Standard Air Schedule requiring 279 minutes of decompression stops．Profile \＃38 would have required decompression on a $100 / 360$ Standard Air schedule which has 415 min of decompression stops．


## DISCUSSION

The main purpose of this study was to see if the computer algorithm which had previously been developed and tested for constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ diving （the EL－MK $15 / 16$ DCM）could be extended to air diving and furthermore could handle gas switches between gases of different oxygen partial pressures．When originally developed，the U．S．Navy Standard Air Tables were computed assumang that oxygen has no effect on the development of DCS but that only the inert gas partial pressure was important（9）．However，in a series of experiments
using goats, Eaton and Hempelman (10) showed that repiacing nitrogen with oxygen did not change the DCS threshold as much as one would expect if oxjgen played no role in causing DCS. Therefore, it must be concluded from Eaton and Hempelman's results that some portion of inspired oxygen tension does play a role in DCS. Conceptually what makes oxygen different from inert gases is its high blood (hemoglobin) solubility which is not linearly related to blood partial pressure and the fact that it is metabolized by tissue. Depending on the tissue metabolic rate, an increase in arterial oxygen tension may result in an insignificant rise in venous oxygen tension for areas of high metabolism or substantial rises for areas with low metabolism. In modifying the EL-MK 15/16 DCM it was decided to base the ascent criteria on total tissue gas tension and develop a scheme for calculating changes in tissue oxygen tension as a function of inspired oxygen tension. It was also assumed that venous and tissue gas tensions were the same. The mathematical representation of the hemoglobin dissociation curve described earlier in this report provides a method of computing venous from arterial oxygen tension but one must specify a metabolic rate for each tissue of interest. This is most conveniently done by specifying the steady state difference between arterial and venous oxygen concentration (CAVO2). The problem then becomes choosing appropriate values for CAV02.

## Development of Initial Ascent Criteria (VVAL22)

If one takes the EL-MK $15 / 16$ DCM using VVALI8 as used to compute the Constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ Decompression Table and computes schedules using a constant $21 \%$ oxygen fraction (air) one obtains schedules which are three to five times longer than current USN Standard Air Schedules (Table E-1, Appendix E). On the other end of the spectrum, Vann (11) has calculated and tested two decompression schedules using an $\mathrm{N}_{2}-\mathrm{O}_{2}$ mix of a constant $1.4 \mathrm{ATA} \mathrm{PO}_{2}$ which was reduced to 1.3 ATA and the last decompression stop which was taken at 20 FSW. Vann's model predicted a $100 \mathrm{FSW} / 60 \mathrm{~min}$ schedule with 90 min of decompression stops breathing a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ and only 20 min of stops with a $1.4 / 1.3$ ATA $\mathrm{PO}_{2}$. For a $150 / 60$ schedule the decompression stop time was reduced from 195 min to 105 min . Selected VVAL18 schedules for $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ are shown in Table E-2 of Appendix $E$ and it will be noted that the 100/60 schedule is 27 min shorter than Vann's $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ schedules but the $150 / 60$ is 7 min longer. If $1.4 \mathrm{ATA} \mathrm{PO}_{2}$ schedules are computed using the EL-MK $15 / 16 \mathrm{DCM}$ and VVAL18, the decompression stop times are reduced to 10 min for the $100 / 60$ schedule, much shorter than predicted by Vann. Vann had tested his 1.4/1.3 ATA schedules on 20 man-dives each without DCS and based on this limited experience it was decided that the EL-MK 15/16 DCM should initially be modified to compute $1.4 \mathrm{ATA} \mathrm{PO}_{2}$ schedules with total decompression times close to Vann's. In computing the VVAL18 1.4 ATA schedules the $\mathrm{PO}_{2}$ was assumed to be 1.4 ATA during the last stop which was taken at 20 FSW ( 1.61 ATA ). Vann reduced the $\mathrm{PO}_{2}$ to 1.3 ATA at 20 FSW for technical reasons, which makes his schedules slightly longer than they would have to be if 1.4 ATA was breathed throughout. This excess time provided a bit of "slop" when fitting the EL-MK 15/16 DCM to Vann's data.

In original the EL-MK $15 / 16$ DCM the tissue offgassing rate is linear and goverened by the equation:

$$
\begin{align*}
\text { DPDT } & =\mathrm{SDR} \cdot \mathrm{~K} \cdot\left(\mathrm{P}_{\mathrm{A}_{\mathrm{N}_{2}}}-\mathrm{P}_{\mathrm{V}_{\mathrm{N}_{2}}}\right)  \tag{5}\\
& =\mathrm{SDR} \cdot \mathrm{~K} \cdot\left(\mathrm{P}_{\mathrm{VO}_{2}}+\mathrm{P}_{\mathrm{V}_{\mathrm{CO}_{2}}}-\mathrm{P}_{\mathrm{A}_{\mathrm{CO}}^{2}}-\mathrm{P}_{\mathrm{A}_{\mathrm{O}_{2}}}-\mathrm{PBOVP}\right)
\end{align*}
$$

where:

$$
\begin{aligned}
& \mathrm{P}_{\mathrm{V}_{2}}=\text { Venous nitrogen tension (FSW) } \\
& \mathrm{P}_{\mathrm{A}_{2}}=\text { Arterial nitrogen tension (FSW) } \\
& \mathrm{P}_{\mathrm{V}_{2}}+\mathrm{P}_{02} \mathrm{~V}_{\mathrm{CO}_{2}}-\mathrm{PA}_{\mathrm{CO}_{2}}=2.8 \mathrm{FSW} \text { (Table 9) } \\
& \mathrm{SDR}=\text { Saturation Desaturation Ratio } \\
& \mathrm{K}=\text { exponential time constant } \\
& \mathrm{P}_{\mathrm{A}_{\mathrm{O}_{2}}}=\text { alveolar } \mathrm{PO}_{2} \text { (FSW) }
\end{aligned}
$$

PBOVP $=$ Tissue specific gas phase overpressure (FSW)
(See reference 1 for details)
If one examines the ratio of offgassing rates (DPDT) for different $\mathrm{PO}_{2}$ levels for a given tissue, one will see that the ratio approaches 1.0 as PBOVP increases. That is, by specifying a PBOVP greater than 0.0 , the percentage increase or decrease in DPDT as the $\mathrm{PAO}_{2}$ is raised or lowered from a reference value will decrease. If a reference $\mathrm{PO}_{2}$ level of 0.7 ATA is chosen, the SDR can be decreased as PBOVP is increased so that DPDT calculated at the 0.7 ATA reference value doesn't change. Unfortunately, decompression schedules will change slightly because as PBOVP increases, the tissue tension at which the offgassing rate slows from linear to exponential changes (1). When PBOVP was increased from 0.0 to 10 FSW and the $\operatorname{SDR}$ reduced from 1.0 to 0.67 for all tissues, DPDT at 0.7 ATA ( 23.1 FSW ) $\mathrm{PO}_{2}$ remains unchanged. The 100/60 decompression schedule at 0.7 ATA using the EL-MK $15 / 16$ DCM and VVAL18 (maximum tissue tensions) was unchanged but the $150 / 60$ schedule TDT increased to 221 min ( 14 min increase in 20 FSW stop and 15 min increase at 10 FSW ). When used to compute air schedules, the above modifications to the SDR and PBOVP of VVALI8 reduced the 100/60 decompression schedule TDT from 158:40 to 96:40 and the 150/60 TDT from 383:30 to 297:30. While these air schedules are still 2.5 and 2.6 times longer than USN Standard Air Schedules, they are not much longer than other air schedules which have been proposed, especially the RNPL schedules (12).

The reduction in calculated decompression times using VVALl8 and modifying the values for $\operatorname{SDR}$ and PBOVP was most welcome. However, when schedules using a $1.4 \mathrm{ATA} \mathrm{PO}_{2}$ were computed, the TDT for the $100 / 60$ schedule was increased only 2 min to $12: 40$ and for the $150 / 60$ increased by 17 min to 76:30. These increases were not felt to be close enough to Vann's predictions so it was decided to investigate other methods of modifying the decompression model to somewhat blunt the effect of the large change in TDT with change in inspired $\mathrm{PO}_{2}$ levels. The initial attempt at this was the EL-MK 15/16 DCM-I in which a slight change was made to the way the alveolar $\mathrm{PO}_{2}$ was computed (Table 3) and in which values for other Blood Parameters were changed (Table 9, VVAL 22-28). The change in the way alveolar $\mathrm{PO}_{2}$ was computed prevented computed arterial nitrogen tensions from becoming negative when $100 \% 0_{2}$ was breathed. The arterial $\mathrm{CO}_{2}$ level was assumed to be 40 mmHg which rounded off to 1.7 FSW and water vapor pressure at body temperature 47 mmHg which rounded off to 2.0 FSW. The venous carbon dioxide tension will vary as venous oxygen tension changes and was calculated to change from 41 to 45 mmHg over a venous oxygen tension rage of 50 to 75 mmHg . This change was small and to reduce the complexity of the model a mean value for venous $\mathrm{CO}_{2}$ tension of 43 mmHg ( 1.87 FSW) was chosen which was assumed constant for all venous oxygen tensions. The value of AMBAO2 was supposed to represent the difference between alveolar and arterial oxygen levels and was chosen as the calculated 57 mmHg ( 2.46 FSW ) difference between arterial and alveolar $0_{2}$ at 0.7 ATA inspired oxygen assuming a $4 \%$ shunt in the lungs. This physiological rationalization was soon dispensed with by assuming that arterial and alveolar nitrogen tensions were the same resulting in not having to calculate the arterial oxygen tension for the EL-MK $15 / 16$ DCM-I. The values for PBOVP were kept at 10.0 FSW because of the desirable effect this had on decreasing the magnitude of change in TDT with changes in inspired $\mathrm{PO}_{2}$.

The $\mathrm{PV}_{2}$ value of 2.8 FSW ( 65 mmHg ) for VVAL22-29 represents the assumed value for a tissue with a 2.39 Vol. \% a-v extraction and an inspired $\mathrm{PO}_{2}$ of 0.7 ATA. If $\mathrm{PAO}_{2}$ is computed as shown in the DCM-I column of Table 3 and other values in equation (5) are taken from the VVAL22-28 row of Table 9, it can be shown that an SDR of 0.72 is needed to keep the calculated offgassing rates (DPDT) for a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ the same as in the original EL-MK $15 / 16$ DCM model. Schedules computed for constant 0.7 ATA $\mathrm{PO}_{2}$ using the EL-MK 15/16 DCM-I with VVAL18 but with the VVAL22-28 Blood Parameters (Table 9) and SDR values of 0.72 decreased the TDT for the $100 / 60$ schedule by 1 min and increased the TDT for the $150 / 60$ by 8 min compared to VVAL18 Tables computed using the original model and Blood Parameters. When a constant 1.4 ATA PO 2 was used, it was assumed that the increase in venous oxygen tension would be 120 mmHg (assuming the tissue extracted 2.39 Vol. \% of $0_{2}$ ) or 5.54 FSW . Schedules computed using the DCM-I, VVAL18, and VVAL22-28 Blood Parameters assuming venous $\mathrm{PO}_{2}$ of 5.54 FSW gave a TDT for the $100 / 60$ of $23: 40$ and a TDT for the 150/60 of $109: 30$, very close to the $20: 40$ and $105: 30$ times of Vann's schedules.

The DCM-I model was easily adjusted to compensate for the two different constant $\mathrm{PO}_{2}$ values of 0.7 ATA and 1.4 ATA simply by adjusting the $\mathrm{PVO}_{2} \mathrm{Blood}$ Parameters. If air is used as a breathing gas, the $\mathrm{PVO}_{2}$ value will be different at each depth so simply adjusting $\mathrm{PVO}_{2}$ will not work. To compute


#### Abstract

air schdules, the actual MPTT values were adjusted at each depth as previously described in the Ascent Criteria section. VVAL18 was adjusted in this manner and when combined with the Blood Parameters in the VWAL22-28 row of Table 9, resulted in the new MPTT Table VVAL22 (Appendix D). VVAL22 was then used with the EL-MK 15/16 DCM to compute a set of air decompression schedules. The resulting air schedules are given in Table E-1 of Appendix E. It was VVAL22 and the EL-MK 15/16 DCM-I which was used as the initial method of air table calculation. All MPTT's are given in Appendix D.


To summarize, the original EL-MK 15/16 DCM using VVAL18 was judged unsatisfactory because computed air decompression schedules appeared too long while schedules using a constant $1.4 \mathrm{ATA}_{\mathrm{PO}}^{2}$ appeared too much shorter than schedules which had been previously tested. In order to shorten computed air tables and lengthen the $1.4 \mathrm{ATA}_{\mathrm{PO}}^{2}$ tables the PBOVP was increased from 0.0 to 10 FSW . Since it was desirable to keep 0.7 ATA $\mathrm{PO}_{2}$ Tables as close as possible to those which were previously tested the offgassing rate (DPDT) had to be kept the same and the SDR was decreased from 1.0 to 0.67 to compensate for the change in PBOVP. The result of these adjustments was that air schedule TDT's were reduced but 1.4 ATA $\mathrm{PO}_{2}$ schedules were still too short. The Decompression Model was then changed to the EL-MK 15/16 DCM-I and MPTT values were adjusted to compensate for changes in venous oxygen tension as inspired tension varied from 0.7 ATA. When breathing air, the MPTT adjustment was depth dependent reflecting the different inspired oxygen tensions at various depths. The resulting MPTT Table was VVAL22 which was the first one used for air diving in this study.

## EL-MK 15/16 DCM-I Testing (VVAL22-29)

The initial testing of the EL-MK 15/16 DCM-I with air using VVAL22 gave the impression that the $60 / 180$ and $100 / 60$ schedules were safe but that the deeper $150 / 60$ schedule was not long enough (Table 4). At this point it was decided to dive some USN Standard Air schedules to see what the DCS incidence for these schedules under controlled conditions was. Since the dives were considered cold, hard-working dives the standard USN practice of using the next longer bottom time schedule was implemented. The 100/70 Standard Air Schedule proved DCS-free in 29 man-dives when used to decompress from 100 FSW after a 60 min bottom time. The initial attempt at a $60 / 180$ dive on August 30 was aborted early for technical reasons and decompressed after 100 min on a 60/100 standard air schedule, which was DCS-free in 9 man-dives. Retesting of the $150 / 60$ schedule using VVAL22 confirmed that this schedule, although over 2.5 times longer than the Standard Air Schedule was too short.

Decompression from 60 FSW after 180 min using the $60 / 200$ Standard Air Schedule produced 3 cases of DCS in 10 man-dives. At this point, a return was made to decompression schedules computed by the EL-MK 15/16 DCM-I using the newly computed VVAL25. VVAL25 used the same MPTT values as VVAL22 but the SDR's were increases to 1.0 which put the TDT for a $60 / 180$ dive about halfway between that predicted by the 60/200 Standard Air Schedule and the previously tested VVAL22 schedule. This gave 4 cases of DCS in 10 man-dives and it was decided that the previously tested $60 / 180$ VVAL22 schedule was not too short after all.
while the o0/200 Standard Air Schedule was a total failure in decompressing from a $60 / 180$ dive, 9 divers were decompressed from 100 FSW after 60 min on a $100 / 60$ Standard Air Schedule. This incredible disparity between the safety of the $100 / 70$ and $100 / 60$ Standard Air Tables and the 60/200 Standard Air Table prompted testing of an intermediate schedule. The 120/70 Standard Air Schedule was used to decompress from $120 / 60$ dive and produced only 1 mild knee pain in 20 man-dives.

It is interesting to note that Berghage (7) in a review of fleet diving from 1971-1978 reported that the 100/60 Standard Air Schedule had the highest incidence of DCS according to U.S. Navy dive records, 5 cases in 104 man-dives. This would predict a $10 \%$ incidence assuming a binomial distribution. There were too few dives done using the $100 / 60$ schedule in this study to make a valid comparison. Only two dives were reported by Berghage using the $60 / 180$ schedule (which were DCS-free). As a matter of fact, Berghage reported that only only 35 man-dives were done at 60 FSW with bottom times greater than 70 min . In the 120 FSW range, only 11 dives were reported for the 60 min bottom time (with no DCS) while 2347 were done with shorter bottom times. Clearly, except for the $100 / 60$ schedule, fleet experience for long bottom times at 60 and 120 FSW is minimal.

At this point, it was felt that safe air schedules for the $60 / 180$, $100 / 60$ and $120 / 60$ dives were at hand. At 150 FSW , lengthening of the decompression schedule for the 60 min bottom time would have required an impractical amount of time in the water, so it was decided to try decompression after shortening the bottom time. By changing the VVAL25 SDR's only, VVAL26 was created to put the TDT for a $60 / 180$ dive back to 153 min and to make the TDT for a $150 / 40$ dive about the same as for a 150/50 Standard Air Schedule (88:30). The resultant 150/40 schedule had a TDT of $85: 30$ which made it only 1.4 times longer than the Standard Air $150 / 40$ schedule. This rather mild increase in TDT was thought reasonable based on the success of the $120 / 70$ schedule and the much increased no-decompression limit at 150 FSW which had been successfully tested. The resulting 2 cases of DCS in 29 man-dives was an improvement over the $150 / 60$ incidence and both cases of DCS were mild.

Based on the experience of Phase 1A, VVAL28 was created which attempted to keep the TDT for a $100 / 60$ schedule close to that of the $100 / 70$ Standard Air Schedule, lengthen the $60 / 180$ to a TDT slightly longer than the VVAL22 schedule and lengthen the $150 / 40$ schedule compared to VVAL26. The surfacing MPTT for the 240 min tissue was chosen as 44.26 which would allow surfacing directly from 25 FSW after saturation on air. Bell et al (13) have in fact shown that the no-decompression saturation depth on air is somewhere between 23 and 26 FSW. The changes made to VVAL26 to get VVAL28 were only in the MPTT's for the $120-200$ min tissues because the 10 FSW stops for both the $60 / 180$ and $150 / 60$ schedules were controlled by tissues in that range. The main casualty of WVAL2 28 was the $120 / 60$ schedule which acquired a TDT of 147 min when it appeared that a Standard Air Decompression $120 / 70$ schedule with a TDT of 89 min would suffice. Initial testing of VVAL28 looked very promising with 18 DCS-free dives on the previously unsafe $150 / 40$ and 19 DCS-free dives on a new $100 / 90$ schedule. When a $190 / 40$ dive was attempted there were 2 DCS in 10 man-dives but restricting the bottom time to 30 min at that depth resulted in 19 DCS-free dives. VVAL28 handed a 6 hour 50 FSW dive without DCS in 20 man-dives and produced 18 DCS-free dives for $60 / 120$ schedules.

Attempts to extend the 60 min bottom time at 120 FSW using VVAL28 to 80 or 70 min were unsuccessful giving rise to 2 cases of DCS on each of the 10 man-dives on these schedules. When a 60 min bottom time at 120 FSW was repeated, there was a single case of mild DCS in 29 man-dives showing that the 147 min TDT was not over conservative.

By the end of Phase 1 , VVAL28 had been modified considerably from the starting MPTT, WAL22, and it was desirable to see if 0.7 ATA schedules would prove safe. VVAL28 was modified for a constant 0.7 ATA PO 2 to VVAL29 as previously described (see Ascent Criteria). VVAL29 produced no DCS on significantly shortened $100 / 60$ and $150 / 30$ schedules (compared to VVAL18). This success lead to an attempt to increase the 150 FSW bottom time to 60 min which produced 2 cases of DCS in 9 man-dives. Even backing off to a 40 min bottom time at 150 FSW produced 2 cases of DCS in 26 man-dives.

At this point it appeared VVAL28 would compute air decompression schedules with a low risk of DCS within the following maximum depth/time limits: $50 / 240 ; 60 / 180,100 / 90 ; 120 / 60 ; 150 / 30$; and $190 / 30$. Also, it appeared to allow some shortening of constant 0.7 ATA P02 schedules within previously tested depth/time limits. These restrictions were acceptable from an operation standpoint so further time was not spent trying to extend them. Rather, the models ability to handle repetitive dives was tested.

At the beginning of Phase 2, VVAL28 was tested on some repetitive dives also. VVAL28 initially looked adequate on the 150 FSW air decompression repetitive Profile \#36 but when used on the 100 FSW profile it proved totally inadequate giving rise to 3 cases of DCS in 9 man-dives.

## EL-MK $15 / 16$ DCM-II Testing (VVAL50-59)

At this point a new modification of the decompression model was brought on line, the EL-MK 15/16 DCM-II. This new model now incorporated equations for calculating venous oxygen tension as a function of arterial so that MPTT adjustments for various $\mathrm{PO}_{2}$ levels would not have to be done. VVAL50 was designed to compute air schedules close to VWAL28 and constant 0.7 ATA PO 2 schedules close to VVAL29. Table E-1 of Appendix E shows that VVAL50 air tables were changed only slightly from VVAL28 tables. The 0.7 ATA constant $\mathrm{PO}_{2}$ schedules were almost identical to VVAL29 with the maximum increase in TDT being 1 min. When schedules breathing 1.4 ATA constant $\mathrm{PO}_{2}$ were calculated, the 100/60 schedule TDT was $22: 40$ and the $150 / 60$ was $126: 30$, both times comparing favorably with the 20:40 and 109:30 schedules tested by Vann. So a single model was now at hand which would reasonably fit schedules which were tested on air, a 0.7 ATA constant $\mathrm{PO}_{2}$ and 1.4 ATA constant $\mathrm{PO}_{2}$.

VVAL50 was short lived producing 2 cases of DCS on 9 man-dives on the 150 FSW repetitive dives. Up to now, the gas phase overpressure, PBOVP, had been kept constant at 10 FSW for all tissues and changes in decompression schedules had been brought about by changing the surfacing MPTT's and the SDR's. By slowing offgassing through a decrease in SDR values, the offgassing rate
change is the same at all inspired $\mathrm{PO}_{2}$ values. However, by manipulating the PBOVP, offgassing rates will change more at lower $\mathrm{PO}_{2}$ values than at higher values. Both SDR's and PBOVP values in VVAL50 were changed to get VVAL52 with the specific intent of having a greater slowing of offgassing shallow, especially at the surface during the surface interval. The TDT for the second dive of Profile 35 was increased by 57 min and for the first dive only 3 min with VVAL52. This made profile 35 too long to be tested during a normal work day so the bottom time for second dive was cut to 40 min resulting in Profile 34. The single case of DCS in 8 man-dives using VVAL52 on Profile 34 was a mild knee pain but was atypical in that it was first noted at 70 FSW during ascent. Considering the mildness of the DCS and the length of the decompression schedule it was decided to persist with VVAL52 a while longer.

A series of dives breathing air at depth and 0.7 ATA $\mathrm{PO}_{2}$ during decompression were tested using VVAL52. A total of 87 min of decompression time was taken off the 100/90 schedule compared to the previously tested VVAL28 schedule using air. No DCS occurred in 19 man-dives. More surprising was the 19 DCS-free dives on a $150 / 40$ schedule, one which had produced DCS both using a constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ and air.

It was the results of the next dive tested, a 100 FSW no-decompression repetitive dive which caused VVAL52 to be modified. Not only did 2 cases of DCS occur in 10 man-dives but one occurred after the first dive, a no-decompression limit having previously produced no DCS in 20 man-dives. VVAL5 3 was an intermediate MPTT Table used only on the $80 / 120$ schedule. It was rapidly modified to VVAL54 which had modified SDR's for the $5-40$ min tissue and different MPTT's for the 40 and 120 min tissues compared to VVAL52. These adjustments were designed to decrease the 100/60 TDT toward that for a Standard Air 100/70 (57:40) while decreasing the no-decompression limit for the second 100 FSW dive on Profile $\# 30$. When retested, Profile $\# 30$ using VVAL54 produced 3 cases of DCS after the first 100 FSW no-decompression dive. This rash of DCS caused consideration of diver fatigue as a possible cause of increased DCS incidence. VVAL55 changed the MPTT's for the 40 and 80 min tissue as well as the PBOVP values and increased the 40 FSW SDR to 0.96. This reduced the no-decompression limit for the first 100 FSW dive to 26.5 min, close to the 25 min in the Standard Air Tables while the no-decompression limit for the second dive increased. This change allowed 16 DCS free dives on Profile $\# 30$.

VVAL56 was another transient MPTT Table replaced by VVAL58 after only a single dive. VVAL58 was designed to maintain the best fit to previously tested profiles while decreasing the second no-decompression time for the second 100 FSW dive on Profile $\# 30$ which dropped by well over 2 min compared to VVAL55. The 100 FSW repetitive dive profile was extended to three dives and the two cases of DCS which arose occurred after the last dive. The 80 FSW repetitive dive profiles appeared reasonably safe overall with only 2 mild cases of DCS both occurring after the second dive. VVAL58 was eventually modified to VVAL59 based mainly on the results of the multiple level dives involving switches between air and constant 0.7 ATA $\mathrm{PO}_{2}$ breathing media. This change involved only the SDR for the 40 and 120 min tissue which served to lengthen the TDT for the final decompression on Profiles $\# 37$ and $\# 38$.

Overall, modification of the decompression model was influenced by two forces. One was not to lengthen schedules which were felt to be safe by too much, and the other was to decrease the rate of offgassing at the surface so that repetitive dive no-decompression limits would be shorter. It must be remembered that the Standard Air Repetitive Dive Tables are computed from a different set of premises than the Standard Air Tables. Details of the way the Standard Air Repetitive Dive Tables were calculated are given elesewhere (14), but in summary all repetitive dives assume that the 120 min tissue will always control the second dive. If repetitive dives had been computed using exactly the same premises as used for the Standard Air Single Dive Tables the Residual Nitrogen Times for the second dive would be much shorter than arrived at using current USN procedures. The goal in this study was to use the same model for the entire dive. This resulted in decompression times for repetitive dives involving decompression to increase markedly but it also allowed no-decompression limits for repetitive dives to increase. As testing progressed, it was just not possible to adjust the no-decompression repetitive dive limits without lengthening profiles which already appeared safe. Part of the reason for this may have been the way the model was adjusted. For example, one could have individually adjusted the arterial-venous oxygen extraction and venous $\mathrm{CO}_{2}$ levels for each tissue. Time was simply not available to test this. Also, the effect of individual variation must be taken into account. Certainly some schedules may have proved safer if more dives could have been done on them.

## Decompression Sickness Symptoms

Appendix $C$ shows the diving intensity for all divers in this study. Generally, divers had at least 2 days off between dives. In all there were 49 cases of DCS in 39 different divers and 2 in tenders. A total of 9 divers had DCS more than one time, Divers 49 and 71 having had DCS three times, and Divers 5, 13, 55, 82, 104,115 and 122 having DCS two times. Diver 122 had one of his cases of DCS while serving as a tender, the other tender being subject 118.

There were only 7 cases of Type 2 DCS which occurred in Divers 24, 40, 55, $65,68,104$ and 122. The incidence of Type 2 DCS was $14.3 \%$. This is comparable to the $17 \%$ incidence of Type 2 symptoms in previous $\mathrm{N}_{2} \mathrm{O}_{2}$ dive series ( 1,8 ) and less than half that of the $37 \%$ incidence encountered testing $\mathrm{HeO}_{2}$ decompression tables (15). Of all Type 2 cases encountered, all but 3 were mild changes in peripheral sensation or mild decreases in strength. The 3 exceptions were all severe cerebral symptoms. Diver 40 suffered memory lapses and marked weakness and sensory changes on the right side. He was followed closely with a battery of neuropsychological tests and required 3 Treatment Table 6's for complete relief. Diver 55 suffered an attack of nausea and lower extremity weakness which responded immediately to compression to 60 FSW. Diver 122 had a mild Type 2 symptoms as a subject on a $230 / 70$ dive consisting of decreased sensation over the right knee but suffered a bout of lightheadedness and profound right sided weakness as a tender on Profile \#3l. This individual was the only one to have suffered Type 2 DCS more than once.

All but 6 cases of Type 1 DCS were straightforward which responded initially to a Treatment Table 5 or 6 . Diver 110 suffered a particularly resistant bout of shoulder pain which required multiple treatments. Complete resolution of symptoms took 3 months. Four months after the incident this diver made a 60 FSW experimental air saturation dive without incident. It is interesting to note that this diver was the first and only female to participate in these dive series. Diver 13 had suffered DCS twice, both Type 2 symptoms. On the second occurrence he had a recurrence of symptoms during decompression which required recompression to 60 FSW. Diver 17 was initially treated for knee pain with complete relief on a Treatment Table 5 but 18 hrs later reported shoulder pain. He showed no change in this pain after 20 min at 60 FSW and it was thought this was not DCS so he was brought to the surface. The pain was mild but persisted over the next 3 days and was present just before he made a $150 / 40$ 0.7 ATA constant $\mathrm{PO}_{2}$ dive. The pain disappeared at 150 FSW and never returned so a diagnosis of residual DCS was made retrospectively. Divers 63,33 and 104 all suffered Type 1 symptoms after multiple level dives and all had recurrences during treatment requiring recompression.

There was no particular physical characteristic which set the divers who suffered DCS apart from those who didn't (Appendix A). Also, there was no particular set of physical characteristics distinguishing divers who suffered Type 2 symptoms are those who suffered DCS more than once from other divers. The time of onset of symptoms ranged from immediately post dive up to 40 and 72 hrs post dive and there was no particular pattern to the symptoms except to say shoulder and knee pain predominated.

Overall, all but a single case of DCS occurring on this series responded completely to Standard USN Oxygen Treatment Tables and Procedures. The only exception was Diver 110 who received non-standard treatments after conventional treatments had only provided partial relief.

## Final Decompression Model and Tables

WVAL59 using the EL-MK 15/16 DCM-II was the final result of testing. A complete set of Air Tables is presented in Appendix $F$. The same depth/bottom time combinations in the current USN Air Schedules were used and the limit lines show the division between Standard Air Schedules and Exceptional Exposure Schedules as currently defined (6). The no-decompression limits down to 110 FSW were revised to be close to those already published in the Standard Air Tables (Table 10). This was done in spite of longer limits having proved safe but the reduction was considered prudent in light of the rash of DCS after the first 100 FSW no-decompression dives during Phase 2 . As one moves away from the no-decompression limits, the decompression times get considerably longer than current Standard Air Schedules allow. In trying to compensate for the DCS incidence which occurred on repetitive dives, final bounce dive schedules became longer than some shown to be safe during testing. The $60 / 180$ schedule gained an additional 55 min over the VVAL22 schedule and the $100 / 60$ gained 17 min over the $100 / 70$ Standard Air Schedule.
 amounts of time. The $150 / 60$ picked up 67 min , a $24 \%$ increase over the tested VhL22 schedule and the $190 / 40$ picked up 81 min , a $35 \%$ increase over the tested VVaL28 schedule.

In computing 0.7 ATA constant $\mathrm{PO}_{2}$ schedules, the $100 / 60$ and $150 / 30$ profiles which had proven safe with substantial reduction in decompression time compared to the previously published VVALl8 decompression tables gained back some time but were still shorter than VVALl8 tables. The 150/40 and $150 / 60$ schedules, which had a high DCS incidence gained 32 and 55 min respectively compared to the VVAL29 schedules which were tested. Also, these schedules are longer than VVALl8 schedules. A complete set of 0.7 ATA constant $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ schedule using VVAL59 is given in Appendix $G$.

When VVAL59 is used to compute constant $1.4 \mathrm{ATA}_{\mathrm{PO}}^{2}$ schedules, the TDT for the $100 / 60$ schedule is $20: 40$ and for the $150 / 60$ 135:20. The 100/60 TDT is the same as the 1.4 ATA profile tested by Vann, but the $150 / 60$ is 30 min longer, a result of compromises made in modifying the decompression model based on test results.

Table 11 shows the expected incidence of DCS for the various aspects of the study. The overall expected incidence on air bounce dives was $7.1 \%$. However, by restricting the maximum depth/time limits to the values shown, the expected incidence falls to $3.2 \%$. In previous testing of the constant 0.7 ATA $\mathrm{O}_{2}$ in $\mathrm{N}_{2}$ schedules, the final test results showed 393 dives fell within the final model which gave rise to 8 cases of DCS, giving an expected incidence of $3.5 \%$. Based on this comparison, the expected incidence of the tables resulting from these two studies is about the same.

Testing of the current U.S. Navy Standard Air Tables involved 688 man-dives resulting in 47 cases of $\operatorname{DCS}(16,17)$ while the present study involved 837 man-dives and 49 cases of LCS. In numbers these studies are comparable but not in methods. In testing of Standard Air Tables, only a few dives were done on as many schedules as possible including some 47 different repetitive dive profiles. Once profiles were found safe they were generally not retested. In addition, because of a high incidence of DCS some individual decompression tables had to be empirically modified. The intent of the present study was to develop a single computer algorithm which would compute decompression schedules for complex profiles as well as compute a set of cinventional tables. In this regard, testing involved areas perceived to have the highest decompression risk and it is the overall incidence of DCS which becare irfortant, not the incidence on specific tables. In looking at Table $\therefore$ however, the repetitive dives stand out as having the highest incidence of $[C 3$ of al: the groups tested. Even excluding Profile $\# 30$ using VVAL52 and WAL5: which proved safe when lengthened does little to lower the expected incidence. Excluding these profiles drops the expected incidence considerably to $7.2 \%$. However, Profiles 34,35 , and 36 were much longer than Standard Air Schedules and one would expect their DCS incidence to be lower than Standard Air Schedules.

The remarkably low incidence of DCS when 0.7 ATA $\mathrm{PO}_{2}$ was breathed during decompression from air dives shows that the EL-MK $15 / 16$ DCM-II sufficiently compensate for changes in $\mathrm{PO}_{2}$ level on bounce dives. However, the ability of the model to handle the long multiple level dives remain uncertain because of lack of previous experience in this area. The DCS incidence observed in this study of 4 cases in 38 man-dives is certainly high but the symptoms were all mild. Certainly, more experience in this area is required.

The final VVAL59 Decompression Tables are comparable in TDT to the RNPL Tables for long dives, but have much longer no-decompression times (12). It is interesting that while the RNPL Tables proved very safe in testing, they were rejected by the Royal Navy fleet operators because the no-decompression times were shorter than those known to be safe. Also, decompression times were longer for dives in the current Royal Navy Tables known to be safe or only producing a slight incidence of DCS (18). However, Leitch and Barnard report that the current Royal Navy Tables have an unacceptable risk of about $6 \%$ DCS for depths 140 FSW and deeper for durations exceeding 15 min . Certainly the results of the present dive series would indicate that for long shallow dives or deep dives, the current USN Standard Air tables would have an unacceptable incidence of DCS. The EL-MK 15/16 DCM-II does fit current no-decompression limits nicely and does not increase TDT too much within the depth/time domain of most USN air diving. Certainly based on the high incidence of DCS on the $60 / 180,150 / 60$, and $190 / 40$ schedules, one must conclude that the increases in the lengths of the decompression schedules are fully justified and not over-conservative.

In other areas of this study results are less conclusive but indicate that the EL-MK 15/16 DCM-II predictions of shortening decompressions for constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ dives are reasonable. Indications are that no-decompression times for repetitive dives can be increased compared to current USN procedure but that further testing will be required. However, VVAL59, did shorten repetitive dive no-decompression limits compared to those actually tested so a decreased incidence of DCS would be expected. Certainly, when DCS did occur on repetitive dives in this study it tended to be mild. However, the DCS which occurred in two tenders who were in dry warm chambers and 7 FSW shallower than diver subjects suggests that testing of no-decompression limits in warm water should be done to verify that this will not shorten no-decompression times.

## Decompression Model Limitations

The EL-MK 15/16 DCM-II retains many of the characteristics of previous Neo-Haldanian Models. The most obvious is the retention of 9 perfusion limited tissues. However, the assumption of gas phase formation and consequent linear offgassing (vice exponential) is unique. Also, the fact that oxygen is treated the same as all other dissolved gases and contributes to DCS based on its partial pressure is also unique. In developing the EL-MK 15/16 DCM-II the oxygen extraction differences and venous $\mathrm{CO}_{2}$ tensions for all tissues were assumed to be the same, this being done for simplicity. There is
no reason to expect, however, that this need remain so and making these values tissue dependent may provide a better fit of the model to the available data. Also, changes in inspired oxygen tension are assumed to be instantaneously reflected in arterial and venous levels, a condition which causes switches to $100 \% \mathrm{O}_{2}$ to cause violations of the ascent criteria in certain instances. The answer to this problem remains to be worked out.

On the positive side, the EL-MK 15/l6 DCM-II does provide a reasonable fit to existing data on tested dives of widely varying $\mathrm{PO}_{2}$ levels. The 240 min MPTT's were also adjusted to predict a reason`ble decompression from saturation on air at 60 FSW. The model allows an upward excursion from 60 FSW to 30 FSW and predicts stops of 7 hrs 30 min at $30 \mathrm{FSW}, 10 \mathrm{hrs} 30 \mathrm{~min}$ at 20 FSW and 12 hrs 30 min at 10 FSW for a TDT of 30 hrs 40 min . A total of 9 man-dives were done on this schedule without DCS. Schedules which were previously tested with decompression times less than 30 hours produced DCS, so the 30 hr schedule is not over conservative (19). Overall the EL-MK 15/16 DCM-II remains the most flexible model developed by the USN to date. Although further testing is required in the repetitive dive area this model would probably have a lower overall incidence of DCS than current procedures and would suffice for computing real time decompression schedules for $\mathrm{N}_{2} \mathrm{O}_{2}$ diving for any $\mathrm{PO}_{2}$ level.

In examining the air decompression tables in Appendix $F$, some decompression times are drastically increased compared to current USN Air Tables. This is especially true of the Exceptional Exposure Tables. As an example, the current 60 FSW/720 Exceptional Exposure Air Schedule calls for 266 min of TDT, while the schedule in Appendix $F$ calls for 1496 min . Considering that the saturation decompression schedule discussed above required 1840 min of decompression, 1496 min for a 12 hr bottom time is not unreasonable. The Exceptional Exposure Tables were not formally tested but experience from this study would indicate that the DCS incidence of currently published schedules would be high. Whether or not the increases in TDT predicted by the EL-MK $15 / 16$ DCM-II model outside of the tested depth/time domain are necessary remains to be seen, but the impression from this study is that they are justified.

## CONCLUSIONS

1. Tissue oxygen tension plays a contributing factor in the development of DCS and must be taken into account.
2. Current USN Standard Mir No-Decompression Limits are safe.
3. Decompression Times for dives with long bottom times need to be longer than allowed in current USN Standard Air Tables and the percentage increase in decompression time is greater as bottom time increases.
4. When doing no-decompression repetitive diving, some extension of repetitive, some extension of repetitive dive no-decompression times beyond those for USN Standard Air Tables Repetitive dives are possible.
5. The EL-MK $15 / 16$ DCM-II using VVAL59 should undergo further testing and modification on no-decompression repetitive diving.
6. No-decompression limits for air diving should be tested in warm water.
7. The EL-MK 15/16 DCM-II using VVAL59 could be used for real time decompression schedule calculation for air or air/0.7 ATA $0_{2}-\mathrm{N}_{2}$ diving with an acceptable risk of decompression sickness which should be less than using current USN Standard Air Tables.

1 Some dives had bottom times too short for each team member to do a full 6 -min exercise run. In these cases, each team member exercised for one-half of the available bottom time.

2 NEDU Report 1-84 (1) mistakenly reported divers exercising 10 min at 50 watts. In fact, the exercise protocol for the $\mathrm{N}_{2} \mathrm{O}_{2}$ dives (l) was exactly the same as done in this study.

3 See page 166 of West, J.B. Respiration Physiology, Williams and Wilkins, Baltimore, MD, 1974.

4 The oxygen sensors in the MK 15 UBA measure absolute oxygen partial pressure. Since the MK 15 breathing loop rapidly saturates with water vapor the maximum oxygen partial pressure must be $\operatorname{PAMB}-\mathrm{P}_{\mathrm{H}_{2}} \mathrm{O}^{-}$

5 In this report gas tensions are reported in feet of sea water (FSW), atmospheres (ATA), or mmHg which are related as follows:
$1 \mathrm{ATA}=33 \mathrm{FSW}=760 \mathrm{mmHg}$
$633 \mathrm{FSW}=760 \mathrm{mmHg}=1 \mathrm{ATA}$.

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## APPENDIX A

DIVER PHYSICAL CHARACTERISTICS

## DIVER PBYSICAL CEARACTERISTICS

| DVR | PHASE ${ }^{\text {@ }}$ | AGE | HT | WGT |  | NFOLDS | (mm) | \%FAT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NO. |  | (YRS) | (IN) | (LBS) | TRI | SS | SI | (NOTE 1) |
| 1 | 3 | 31 | 64 | 167 | 9.0 | 19.0 | 13.3 | 20.8 |
| 2* | 2 | 23 | 71 | 179 | 7.5 | 11.0 | 4.0 | 10.9 |
| 3 | 3 | 23 | 69 | 162 | 19.3 | 8.1 | 5.8 | 15.4 |
| 4 | 1 | 30 | 68 | 153 | 6.0 | 13.0 | 3.6 | 14.5 |
| 5* | 2 | 25 | 73 | 197 | 19.0 | 14.6 | 10.0 | 18.6 |
| 6 | 1 | 23 | 67 | 162 | 11.1 | 9.5 | 4.5 | 12.1 |
| 7* | 3 | 24 | 72 | 184 | 4.6 | 9.6 | 4.3 | 8.6 |
| 8 | 0,1 | 22 | 70 | 180 | 9.6 | 13.8 | 3.5 | 12.9 |
| 9 | 1 | 30 | 68 | 157 | 14.0 | 13.5 | 2.8 | 17.6 |
| 10 | 2 | 24 | 71 | 173 | 9.0 | 9.3 | 5.3 | 11.4 |
| 11 | 2 | 25 | 70 | 177 | 5.0 | 7.0 | 3.0 | 6.2 |
| 12 | 2 | 21 | 72 | 192 | 9.3 | 8.0 | 4.0 | 10.2 |
| 13* | 0,1 | 35 | 76 | 195 | 12.1 | 9.5 | 3.5 | 15.6 |
| 14* | 2 | 26 | 72 | 186 | 11.6 | 11.6 | 5.3 | 13.6 |
| 15 | 3 | 25 | 72 | 176 | 5.0 | 7.0 | 3.3 | 6.5 |
| 16 | 0 | 28 | 69 | 164 | 11.6 | 11.6 | 5.6 | 13.7 |
| 17* | 2 | 23 | 72 | 196 | 11.0 | 12.3 | 6.6 | 14.2 |
| 18 | 0 | 46 | 68 | 155 | 4.5 | 7.5 | 3.0 | 10.0 |
| 19 | 3 | 25 | 70 | 151 | 5.0 | 11.5 | 3.5 | 9.5 |
| 20 | 3 | 20 | 70 | 179 | 8.0 | 8.1 | 3.0 | 9.0 |
| 21 | 0,1 | 24 | 72 | 175 | 12.5 | 10.5 | 5.8 | 13.7 |
| 22 | 0,1 | 32 | 72 | 200 | 13.0 | 16.0 | 9.0 | 19.9 |
| 23 | 0 | 37 | 69 | 151 | 6.1 | 15.5 | 10.3 | 18.1 |
| 24 * | 0 | 37 | 70 | 170 | 13.0 | 13.6 | 5.6 | 18.2 |
| 25 | 0,1 | 24 | 68 | 145 | 3.0 | 7.0 | 2.5 | 4.2 |
| 26* | 1 | 27 | 73 | 235 | 22.6 | 25.6 | 8.0 | 21.6 |
| 27* | 2 | 21 | 67 | 159 | 4.0 | 12.8 | 4.3 | 10.1 |
| 28 | 0 | 31 | 72 | 172 | 15.6 | 9.3 | 4.3 | 17.2 |
| 29 | 0,3 | 33 | 70 | 169 | 12.0 | 19.3 | 5.6 | 19.6 |
| 30 | 3 | 32 | 71. | 165 | 6.3 | 9.0 | 2.0 | 11.8 |
| 31 | 0,1,2,3 | 45 | 69 | 162 | 7.6 | 12.3 | 5.3 | 17.0 |
| 32* | 0,1,2 | 30 | 71 | 146 | 10.6 | 8.8 | 4.6 | 15.1 |
| 33* | 1,3 | 22 | 73 | 205 | 19.3 | 15.0 | 6.0 | 17.7 |
| 34 | 1 | 34 | 67 | 160 | 6.6 | 8.3 | 4.0 | 12.7 |
| 35 | 3 | 23 | 72 | 176 | 4.5 | 12.0 | 5.0 | 10.3 |
| 36 | 3 | 21 | 72 | 190 | 4.0 | 10.6 | 2.3 | 7.6 |
| 37* | 0,1,2 | 27 | 71 | 194 | 10.0 | 13.3 | 6.8 | 14.2 |
| 38 | 0,3 | 24 | 72 | 152 | 6.0 | 9.5 | 3.8 | 9.1 |
| 39 | 2 | 20 | 72 | 160 | 5.8 | 10.1 | 5.5 | 10.3 |
| 40* | 0,1 | 40 | 70 | 185 | 8.6 | 14.1 | 5.3 | 18.4 |
| 41 | 0 | 29 | 67 | 154 | 7.3 | 15.6 | 5.0 | 13.4 |
| 42* | 0,1 | 27 | 68 | 152 | 12.5 | 12.8 | 4.0 | 13.9 |
| 43 | 1 | 29 | 72 | 208 | 6.8 | 19.5 | 12.3 | 17.2 |
| 44 | 2 | 20 | 71 | 178 | 10.3 | 14.3 | 5.0 | 14.0 |
| 45 | 1 | 28 | 71 | 155 | 5.5 | 6.8 | 2.0 | 5.7 |
| 46 | 2 | 23 | 74 | 185 | 4.0 | 7.3 | 2.0 | 4.9 |
| 47 | 2 | 23 | 72 | 178 | 12.3 | 11.6 | 3.3 | 13.1 |
| 48 | 0,1 | 24 | 72 | 162 | 3.3 | 8.6 | 2.8 | 6.0 |

## DIVER PHYSICAL CEARACTERISTICS (cont.)

| $\begin{aligned} & \text { DVR } \\ & \text { NO. } \end{aligned}$ | $\text { PHASE }{ }^{@}$ | $\begin{aligned} & \text { AGE } \\ & \text { (YRS) } \end{aligned}$ | $\begin{aligned} & \text { HT } \\ & \text { (IN) } \end{aligned}$ | $\begin{aligned} & \text { WGT } \\ & \text { (LBS) } \end{aligned}$ | SKINFOLDS (mm) |  |  | $\begin{gathered} \text { \%FAT } \\ \text { (NOTE 1) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | TRI | SS | SI |  |
| 49* | 2 | 25 | 69 | 183 | 15.0 | 11.6 | 6.6 | 15.4 |
| 50* | 0 | 24 | 20 | 196 | 9.0 | 8.5 | 2.8 | 9.7 |
| 51 | 3 | 34 | 72 | 208 | 16.6 | 18.3 | 10.6 | 21.8 |
| 52 | 0,1 | 36 | 72 | 189 | 11.3 | 10.6 | 3.8 | 15.8 |
| 53 | 0 | 22 | 69 | 166 | 5.0 | 10.8 | 3.0 | 8.8 |
| 54 | 3 | 25 | 69 | 158 | 5.6 | 11.6 | 3.3 | 9.8 |
| 55* | 0 | 25 | 72 | 171 | 22.6 | 8.0 | 7.6 | 17.0 |
| 56* | 2 | 29 | 71 | 170 | 6.5 | 8.5 | 2.0 | 7.7 |
| 57 | 0 | 26 | 73 | 204 | 15.0 | 16.0 | 7.5 | 17.1 |
| 58 | 0,1 | 29 | 68 | 170 | 11.1 | 10.8 | 14.3 | 16.4 |
| 59 | 3 | 27 | 71 | 192 | 18.8 | 18.0 | 13.1 | 20.2 |
| 60 | 3 | 21 | 72 | 167 | 6.1 | 8.0 | 3.5 | 8.1 |
| 61 | 1 | 23 | 73 | 210 | 8.5 | 10.1 | 6.0 | 11.9 |
| 62 | 1,2 | 29 | 75 | 192 | 8.8 | 11.0 | 3.0 | 11.0 |
| 63 | 3 | 34 | 78 | 252 | 14.1 | 16.0 | 11.0 | 20.8 |
| $64 *$ | 3 | 32 | 68 | 151 | 7.0 | 8.0 | 2.8 | 12.1 |
| 65* | 3 | 37 | 79 | 216 | 8.8 | 9.8 | 4.6 | 14.8 |
| 66 | 2 | 29 | 66 | 177 | 12.3 | 12.0 | 3.0 | 13.1 |
| 67 | 3 | 24 | 70 | 169 | 10.8 | 9.1 | 2.8 | 11.0 |
| 68* | 0,3 | 23 | 71 | 170 | 14.0 | 9.6 | 4.0 | 13.2 |
| 69* | 0 | 23 | 71 | 184 | 7.0 | 11.0 | 5.3 | 11.3 |
| 70* | 0,1,2,3 | 37 | 66 | 174 | 12.5 | 12.6 | 7.0 | 18.2 |
| 71* | 0,3 | 27 | 70 | 183 | 4.8 | 10.8 | 3.1 | 8.7 |
| 72 | 3 | 23 | 69 | 174 | 4.6 | 10.1 | 4.0 | 8.7 |
| 73* | 0,1 | 35 | 71 | 170 | 16.8 | 11.8 | 12.6 | 20.8 |
| 74 | 0 | 26 | 71 | 177 | 11.0 | 11.0 | 7.3 | 13.9 |
| 75 | 1 | 23 | 70 | 156 | 7.0 | 9.1 | 3.0 | 9.0 |
| 76 | 0 | 31 | 68 | 168 | 14.3 | 15.3 | 8.0 | 19.8 |
| 77 | 0 | 31 | 71 | 175 | 11.6 | 18.0 | 6.3 | 19.3 |
| 78* | 3 | 38 | 68 | 197 | 11.6 | 17.3 | 11.1 | 20.5 |
| 79 | 3 | 32 | 73 | 201 | 13.8 | 21.3 | 9.1 | 21.5 |
| 80 | 1 | 31 | 72 | 186 | 17.3 | 17.0 | 6.6 | 20.7 |
| 81* | 2 | 20 | 72 | 170 | 10.6 | 10.3 | 4.6 | 12.3 |
| 82* | 1 | 35 | 69 | 173 | 9.6 | 20.0 | 9.6 | 20.3 |
| 83 | 3 | 21 | 68 | 175 | 10.0 | 8.1 | 4.1 | 10.7 |
| 84 | 3 | 34 | 68 | 171 | 11.3 | 16.0 | 9.0 | 19.4 |
| 85 | 1 | 23 | 70 | 180 | 5.0 | 8.6 | 3.6 | 7.8 |
| 86 | 3 | 22 | 72 | 162 | 3.0 | 6.5 | 2.3 | 3.6 |
| 87 | 0 | 26 | 68 | 166 | 5.3 | 8.3 | 2.6 | 7.1 |
| 88 | 0 | 33 | 69 | 175 | 8.6 | 15.6 | 6.3 | 17.6 |
| 89* | 3 | 27 | 66 | 176 | 9.3 | 16.0 | 8.0 | 15.4 |
| 90 | 3 | 25 | 67 | 137 | 7.0 | 7.5 | 3.3 | 8.2 |
| 91* | 3 | 32 | 63 | 183 | 5.0 | 15.1 | 7.0 | 16.4 |
| 92 | 1 | 20 | 71 | 174 | 10.3 | 12.0 | 4.6 | 12.9 |
| 93 | 2 | 22 | 74 | 178 | 6.0 | 7.0 | 2.0 | 6.2 |
| 94 | 1 | 21 | 65 | 155 | 8.6 | 11.0 | 4.3 | 11.8 |
| 95 | 1 | 43 | 73 | 205 | 16.0 | 15.3 | 9.0 | 23.5 |
| 96 | 1 | 37 | 72 | 160 | 4.0 | 9.3 | 3.0 | 11.2 |

## DIVER PHYSICAL CHARACTERISTICS (cont.)

| DVR P | PHASE ${ }^{\text {® }}$ | AGE | HT | WGT | SKINFOLDS |  | (mm) | \%FAT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NO. |  | (YRS) | ( IN) | (LBS) | TRI | SS | SI | (NOTE 1) |
| 97 | 3 | 27 | 67 | 168 | 13.1 | 11.3 | 7.0 | 14.7 |
| 980 | 0,1,3 | 32 | 70 | 191 | 8.3 | 13.0 | 7.0 | 16.8 |
| 99* | 3 | 20 | 71 | 177 | 8.3 | 10.5 | 3.6 | 10.8 |
| 100 | 3 | 31 | 76 | 216 | 7.1 | 12.0 | 4.0 | 14.7 |
| 101 | 3 | 23 | 72 | 176 | 8.5 | 9.6 | 6.6 | 11.9 |
| 102* | 1,2 | 24 | 68 | 150 | 4.0 | 7.6 | 1.6 | 4.8 |
| 103* | 3 | 24 | 70 | 194 | 9.8 | 11.8 | 2.8 | 11.8 |
| 104* | 2 | 24 | 70 | 160 | 9.5 | 8.1 | 4.0 | 10.4 |
| 105 | 2 | 29 | 71 | 179 | 7.3 | 7.0 | 2.0 | 7.2 |
| 106 | 1.2 | 39 | 73 | 202 | 6.5 | 15.5 | 5.0 | 16.4 |
| 107 | 1,3 | 27 | 71 | 192 | 7.8 | 16.0 | 11.0 | 15.9 |
| 108 | 0 | 24 | 72 | 187 | 11.6 | 8.0 | 4.3 | 11.6 |
| 109 | 0 | 34 | 71 | 198 | 20.8 | 22.8 | 10.6 | 23.7 |
| 110 (F)* | * 0 | 30 | 62 | 126 | 12.6 | 11.0 | 10.8 | 25.8 |
| 111 | 1 | 24 | 67 | 145 | 4.1 | 10.3 | 1.5 | 6.9 |
| 112 | 1 | 26 | 70 | 157 | 6.8 | 10.0 | 3.0 | 9.4 |
| 113 | 2 | 36 | 69 | 185 | 13.3 | 10.3 | 6.6 | 17.5 |
| 114 | 3 | 26 | 68 | 208 | 8.6 | 11.5 | 10.5 | 14.4 |
| 115* | 1,2 | 32 | 67 | 153 | 4.6 | 8.0 | 4.3 | 11.5 |
| 116 | 0 | 40 | 69 | 185 | 10.0 | 15.3 | 7.3 | 20.5 |
| 117* 0 | 0,1,2 | 32 | 71 | 207 | 17.5 | 28.0 | 12.3 | 24.4 |
| 118* 1 | 1,2,3 | 31 | 72 | 175 | 12.5 | 16.3 | 9.3 | 20.0 |
| 119 | 3 | 22 | 69 | 159 | 9.3 | 8.0 | 5.1 | 10.8 |
| 120 | 0 | 21 | 70 | 182 | 7.1 | 11.6 | 4.3 | 11.1 |
| 121* 0 | 0,1,2 | 22 | 71 | 172 | 4.6 | 9.5 | 3.5 | 8.1 |
| 122* | 1 | 29 | 72 | 183 | 5.0 | 7.5 | 6.5 | 8.9 |
| 123 | 0,3 | 31 | 74 | 200 | 12.6 | 10.3 | 6.6 | 17.3 |
| 124 | 3 | 26 | 69 | 184 | 6.6 | 11.6 | 3.6 | 10.5 |
| 125 | 1 | 27 | 67 | 156 | 7.0 | 9.0 | 4.3 | 9.7 |
| 1260 | 0,1,2 | 38 | 70 | 189 | 17.8 | 22.0 | 16.8 | 24.2 |

## MEANS

| ALL | Mean | 27.9 | 20.3 | 177 | 13.7 |
| :--- | :--- | ---: | ---: | ---: | ---: |
| SUBJS. | S.d. | 5.8 | 2.6 | 19.5 | 5.0 |
|  | N | 126 | 126 | 126 | 126 |
|  |  |  |  |  |  |
| SUBJS. Mean 28.1 20.2 179 <br> WITH S.d. 5.5 3.0 20.5 <br> DCS* $N$ 40 40 40 | 14.5 |  |  |  |  |


| SUBJS. | Mean | 27.8 | 20.3 | 176 | 12.9 |
| :--- | :--- | ---: | ---: | ---: | ---: |
| WITIOUT | s.d. | 6.0 | 2.4 | 19.1 | 6.2 |
| DCS | N | 86 | 86 | 86 | 86 |

[^2]Note 1: Body fat percentage computed from rricens (TRI), subscapular (SS). and supra-iliac (SI) skinfolds according to the method of:

Durnin, J.V.G.A. and J. Womersley, Body Fat Assessed from Total Bodv Density and Its Estimation from Skinfold Thickness:
Measurements on 481 Men and Women Aged from 16 to 72 Years. British Journal of Nutrition 32:77-97, 1974.

APPENDIX B
DECOMPRESSION SICKNESS DESCRIPTIONS

TABLE B-1

## decompression sickness descriptiuns

Phase IA


TABLE B-1
(CONTINUED)

| Tahlei | iver | Date' 84 | 'Profile! |  | Tonser Time |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 Kev ! | in. | 1 Mod | 'FSh/Min! | DCS Type and Location | Post Dive | Comments |
| 1 ' |  | , | 1 |  | + |  |
| e | 50 | 9/7 | 160/180! | (1) R. shoulder pain. | $21 / 2 \mathrm{hrs}$ | Complete rellef after one $\mathrm{O}_{2}$ period at 60 |
| 1 |  | vVAL2 5 |  |  |  | FSW, Treatment Table 6. |
| $1 \quad 1$ |  | 1 | 1 |  | 1 |  |
| 11 | 55 | ! | 1 | (2) Extreme fatigue follow- | 13 hrs | Nausea gone after 5 min at 60 FSW . Com- |
| 1 |  | 1 | $!$ | ed by nausea and bilat.! |  | plete relief after 2 nd $\mathrm{O}_{2}$ period. Treat- |
| 1 |  | 1 | 1 | lower extremity pares- |  | ment Table 6 with 1 extension at 60 FSW . |
| 11 |  | 1 | 1 | thesias. | , |  |
| 1 |  | $!$ | , |  | 1 |  |
| ! | 70 | 1 | 1 | (1) R. shoulder pain. | 3 hrs | Complete relief upon arrival at 60 FSW . |
| 1 |  | 1 | 1 |  | 1 | Treatment Table 5. |
| $1-1$ |  | 1 | 1 |  | ! |  |
| 1 f 1 | 71 | + 9/10 | +120/60 | (1) L. shoulder pain (mild) | $10^{\prime}$ Stop | First noted at depth. Increased over 40 |
| 11 |  | 'Std.Air | I |  |  | min post-dive. Complete rellef upon arri- |
| $1 \quad 1$ |  | !120/70 | + |  | 1 | val at 60 FSW , Treatment Table 5. |
| 1 |  | 1 | ! |  | 1 |  |
| 1 ¢ ! | 73 | 9/17 | $1150 / 40$ | (1) R. knee pain. | 5 hrs | Reported for treatment 15 hrs post dive. |
| 11 |  | 1 WVAL2S |  |  | $\dagger$ i | Complete relief after 3 rd $\mathrm{O}_{2}$ period at 60 |
| 1 |  | , | 1 |  | I | 1 FSW, Treatment Table 6, with 1 extension |
| ! |  | 1 | 1 |  | $1+$ | 1 at 60 FSW . |
| 1 |  | T | I |  | 1 - | - |
| 1 h i | 37 | ! 9/20 | 1150/40 ! | (1) Shoulder pain. | 7 hrs | Complete relief on compression to 60 FSW . |
| 11 |  | 1 vVAL26 | 11 |  | 1 | Treatment Table 5. |
| 1 |  | 1 | 1 |  | 1 |  |
| 1 |  | I | T |  | I | I |
| $!$ |  | 1 | $!$ |  | 1 | ! |
| 1 |  | 1 | 1 |  | I | I |
| 1 |  | 1 | 11 |  | ! | 1 |
| 1 |  | 1 | 11 |  | 1 | ! |
| 1 |  | 1 | 11 |  | , | , |
| 1 |  | 1 | 11 |  | , | , |
| 1 |  | i | 1 |  | 1 | , |
| 1 |  | , | 11 |  | , | I |
| 1 |  | 1 | 11 |  | 1 | 1 |
| 1 |  | 1 | 11 |  | 1 | - |
| 1 |  | 1 | 11 |  | ! | I |
| 1 |  | 1 | 11 |  | 1 | , |
| 1 |  | 1 | 1 |  | , |  |
| , |  | 1 | 11 |  | 1 1 | ! |
| , |  | , | $1 \quad 1$ |  | I | ! |
| ' |  | 1 | 1 |  | 1 | ! |
| 1 |  | 1 | 11 |  | 1 | - |
| 1 |  | 1 | 11 |  | $1 \times$ | 1 |
| , |  | 1 | 11 |  | $1 \sim$ | $!$ |
| $1 \quad 1$ |  | 1 | 11 |  | 1 | , |
| , |  | 1 | 1 |  | 1 - | I |
| 1 |  | 1 | 11 |  | 1 | 1 |
| 1 |  | 1 | 1 |  | i | 1 |
| 1 |  | , | $1 \quad 1$ |  | $1 \times$ | $!$ |
| , |  | 1 | 1 ! |  | 1 | ! |
| 1 |  | 1 | $1 \cdot$ |  | , | 1 |
| 1 |  | , | $1 \quad 1$ |  | 1 - | 1 |
| 1 |  | 1 | $1 \quad 1$ |  | , | , |
| 1 |  | 1 | $1 \quad 1$ |  | 1 - | , |
| 1 |  | ' | 11 |  | 1 - | 1 |
| 1 |  | 1 | 1 |  | 1 - | , |
| 1 |  | ' | 1 |  | 1 , | 1 |
| , |  | ; | , |  | 1 - | 1 |
| ' |  |  | 1 |  | $1 \times$ | + |
| , |  | , | 1 |  | $!$ | , |
| * |  | ' | 1 |  | $1 \times$ | , |
| , |  | ' | , |  | $1 \times$ | 1 |
| 1 |  | 1 | 1 |  | 1 , | ; |
| , |  |  | 1 |  | 1 , | ' |
|  |  |  | ' |  | 1 | 1 |

TABLE B-2
DECOMPRESSION SICKNESS DESCRIPTIONS
PHASE 1B

| Table 14 Key 1 | Diver | 1 Date ${ }^{1} 84$ | $\begin{array}{\|l\|} \hline 4 \mid \text { Profile } \\ \mid \text { FSW/Min } \\ \hline \end{array}$ | DCS Type and Location | $\begin{aligned} & \text { Tonset Time } \\ & \text { Post Dive } \end{aligned}$ | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1- |  | 1 | 1 |  |  |  |
| 1 | 121 | $110 / 9$ | 1190/40 | (1) R. knee ache. | 3 hrs | Knee ache initially fleeting. Complete |
| 1 \| |  | IVVAL28 |  | R. shoulder pain. |  | rellef of knee pain on compression to |
| 1 |  | $i$ | 1 |  |  | 60 FSW. 50\% relief shoulder symptoms after ${ }^{\text {d }}$ |
| 1 |  | i | 1 |  | + | 3rd $\mathrm{O}_{2}$ period. Treatment Table 6 with 2 |
| 11 |  | 1 | 1 |  |  | extensions at 60 FSW . |
| 11 |  | 1 | 1 |  | 1 |  |
| 1 | 82 | 1 | 1 | (1) Ankle pain. | 4 hrs | Complete relief after $3 \mathrm{O}_{2}$ periods at 60 |
| 11 |  | 1 | 1 |  | ) | FSW. Treatment Table 6 with 1 extension |
| I |  | 1 | 1 |  | ! | ar 60 FSW . |
| 1 |  | ! | 1 |  |  |  |
| j | 118 | \| 10/16 | 120/80 | (1) R. knee pain. | 7 hrs | Substantial relief upon arrival at 60 FSW .1 |
| 1 |  | IVVAL28 |  |  |  | Complete relief by 2 nd $\mathrm{O}_{2}$ period. Treat- |
| 1 1 |  | 1 | 1 |  | 1 | ment Table 6. Recurred at 45 FSW during |
| 1 |  | I | I |  | 1 | \| ascent, recompressed to 60 FSW , complete |
| 11 |  | 1 | 1 |  | 1 | \| rellef by 2 nd $\mathrm{O}_{2}$ period. Treatment Table 6 \| |
| 11 |  | 1 | I |  |  | \| with 1 extension at 30 FSW . |
| 11 |  | 1 | 1 |  | 1 | 1 l |
| 1 | 40 | 1 | 1 | (2)Post-dive fatigue, | 40 hrs | Knee pain gone upon arrival at 60 FSW . |
| 11 |  | ; | 1 | Memory lapses, L. knee |  | Complete relief all symptoms after 3rd $\mathrm{O}_{2}$ |
| 1 |  | I | 1 | pain. Decreased sensa- |  | period. All neuropsychological tests WNL |
| 1 |  | ! | 11 | tion to pinprick R. |  | at 60 FSW except for SDMT which improved |
| 11 |  | । | 1 | temple and R. trunk. |  | but not WNL. Treatment Table 6 with 2 ex- |
| 1 |  | 1 | 1 | Decreased grip strength. |  | tensions at 60 FSW and 1 extension at 30 |
| 11 |  | ! | 1 | Decreased neuropsycho- |  | FSW. |
| 11 |  | , | 1 | logical function on |  |  |
| 11 |  | 1 | $i$ | Trails A, Symbol Digit |  | 1 |
| 11 |  | 1 | $!$ | Modality Test (SDMT) | 1 |  |
| 11 |  | 1 | 1 | and Wechsler memory |  |  |
| 11 |  | 1 | 1 | test. | 1 | ! |
| 11 |  | 1 | 11 | (2) Difficulty remembering | 96 hrs | Given Treatment Table 6. TTMA and affect |
| 11 |  | 1 | 11 | and concentrating. Low |  | normal after treatment. 48 hrs after this |
| 11 |  | 1 | $1 \quad 1$ | score on Thurston Test | I | treatment still complained of poor con- |
| 11 |  | ! | 1 | of Mental Alertness | ! | centration. Subjective improvement after |
| 1 |  | I | 1 | (TTMA). Flat affect. | 1 | completion of another Treatment Table 6. |
| $1{ }^{-}$ |  | I | 1 |  | 1 |  |
| k | 122 | 1 10/18 | 1120/70 | (1) L. knee pain. | 10' Stop | Pain first noted at depth but went away. |
| 1 |  | IVVAL28 | ! | (2) Decreased sensation | 2 Min | Recurred 2 min post-dive. Pain $80 \%$ gone on |
|  |  |  | I | over R . knee. | 1 M | arrival at 60 FSW . Complete relief at 30 |
| 11 |  | 1 | 1 |  | 1 | FSW after 1 extension at 60 FSW . Treatment |
| 11 |  | ! | ! |  | $!$ | Table 6. |
| 1 1 |  | 1 | i |  | , | ! |
| 11 | 102 | 1 | $i \quad 1$ | (1) L. elbow pain. | 16 hrs | Complete relief at 30 FSW during compres- |
| $!$ |  | 1 | 1 |  | $!$ | 1 sion. Treatment Table 5. |
| 1 |  | T | T |  | T |  |
| 1 | 26 | - 10/23 | 120/60 | (1) R. shoulder and arm | 2.5 hrs | Pain mild at first, increased in intensity |
| 11 |  | IVVAL28 | 1 | pain. | 1 | over next several hours. Reported for |
| 11 |  |  | 1 |  | 1 | treatment 5 hrs post-dive. Shoulder pain |
| 11 |  |  | 11 |  | , | gone on arrival at 60 FSW . Arm pain gone |
| 11 |  | 1 | 1 |  | I | ! after 3rd $\mathrm{O}_{2}$ period. Treatment Table 6 |
| 1 |  | 1 | 1 |  | 1 | 1 with l extension at 60 FSW . |

TABIER R-3

Pllast?


TABLE B-3
(CONTINUED)


TABLE: B-4

DECOMPRESSION SICKNESS DHSCRIYTIONS

PHASt: 3

(CONTINUEU)
(T) Tencer

Profile number. See Table ?


appendix C
INDIVIDUAL DIVING INTENSITY

TABLE C-1
PHASE IA INDIVIDUAL DIVING INTENSITY

Body of Table Show Profile No. (Table 1; Appendix E)

| $\begin{aligned} & \text { Diver } \\ & \text { No. } \\ & \hline \end{aligned}$ | August 1984 |  |  |  |  |  | September 1984 |  |  |  |  |  |  | $\begin{array}{\|c} \text { Diver } \\ \text { No. } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 23 | 24 | 27 | 28 | 30 | 31 | 4 | 6 | 7 | 10 | 13 | 17 | 20 |  |
| 8 | 8 |  |  | 5 |  | 8 |  |  | 8 8 | 7 | 11 | 15 | 2 | 8 |
| 13 |  |  | 8 |  |  |  |  | 5* |  | 7 | 14 | 15 | 2 | 13 |
| 16 | 8 |  |  |  |  |  |  |  |  | 7 | 14 | 2 | 2 | 16 |
| 18 |  |  |  |  |  |  |  |  |  | 7 |  |  |  | 18 |
| 21 |  |  |  | 5 |  | 8 | 16 | 5 | 8 | 7 | 11 | 15 | 2 | 21 |
| 22 |  | 16 | 8 |  | 3 |  |  |  | 8 | 11 | 14 | 2 | 15 | 22 |
| 23 |  | 16 |  | 5 |  |  |  |  |  |  | 14 | 15 |  | 23 |
| 24 |  | 16* |  |  |  |  |  | 5 |  | 11 | 14 | 2 |  | 24 |
| 25 | 8 |  |  | 5 |  | 8 | 16 |  | 8 | 7 | 11 | 15 | 2 | 25 |
| 28 |  |  | 5 |  |  |  |  |  |  |  |  |  | 15 | 28 |
| 29 | 8 |  |  |  |  | 8 | 16 |  | 5 | 7 | 11 | 15 |  | 29 |
| 31 |  |  |  |  |  | 8 | 16 |  |  |  | 14 |  |  | 31 |
| 32 |  |  | 5* |  | 3 |  |  | 5 |  |  | 11 | 15 |  | 32 |
| 37 |  | 16 | 8 |  | 3 |  |  | 5 |  | 11 | 14 | 2 | 15* | 37 |
| 38 | 8 |  |  | 5 |  |  | 16 |  | 8 | 7 | 11 |  | 2 | 38 |
| 40 |  |  | 8 |  | 8 |  |  |  |  |  |  |  |  | 40 |
| 41 | 8 |  |  | 5 |  | 8 | 16 |  | 8 | 7 | 11 | 15 | 2 | 41 |
| 42 | 8 |  | 5 |  |  |  |  | 5* |  | 7 | 14 | 15 | 2 | 42 |
| 48 | 8 |  | 5 |  | 8 |  | 16 |  | 5 | 7 | 14 | 15 | 2 | 48 |
| 50 | 8 |  | 5 |  | 8 |  | 16 |  | 5* | 7 | 14 | 15 | 2 | 50 |
| 52 | 8 |  | 5 |  |  | 8 |  |  |  | 11 | 14 | 15 | 2 | 52 |
| 53 | 8 |  |  | 5 |  | 8 | 16 |  | 8 | 7 | 11 | 15 | 2 | 53 |
| 55 |  |  | 5 |  | 8 |  | 16* |  | 5* |  |  |  |  | 55 |
| 57 |  |  |  | 5 |  |  | 16 |  |  | 7 |  |  |  | 57 |
| 58 |  |  |  |  | 8 |  |  |  |  |  |  |  | 15 | 58 |
| 68 |  |  | 5 |  | 8 |  | 16* |  |  | 7 | 14 | 15 | 2 | 68 |
| 69 | 8 |  | 5 |  | 8 |  | 16* |  | 5 | 7 | 14 | 15 | 2 | 69 |
| 70 | 8 |  |  |  |  | 8 | 16 |  | 5* | 7 | 14 | 15 | 2 | 70 |
| 71 |  | 16* | 8 |  | 3 |  |  | 5* |  | 11* | 14 | 2 | 15 | 71 |
| 73 | 8 |  |  |  |  |  |  |  |  |  |  | 15* |  | 73 |
| 74 |  | 16 | 8 |  | 3 |  |  | 5 |  | 11 | 14 | 2 | 15 | 74 |
| 76 | 8 |  |  |  |  |  |  |  |  | 11 |  |  |  | 76 |
| 77 |  | 16 |  |  |  |  |  |  |  |  | 11 |  |  | 77 |
| 87 | 8 |  | 5 |  | 8 |  | 16 |  | 5 | 7 | 14 | 15 | 2 | 87 |
| 88 |  | 16 | 8 |  | 3 |  | 16 |  | 5 | 7 |  | 15 |  | 88 |
| 98 |  |  |  |  |  |  | 16 |  | 5 |  |  |  |  | 98 |
| 108 |  | 16 | 8 |  | 3 |  |  | 5 |  | 11 | 14 | 2 | 15 | 108 |
| 109 |  |  |  |  | 8 |  |  |  | 8 |  |  |  | 2 | 109 |
| 110 |  |  |  |  |  |  | 16 |  | 5* |  |  |  |  | 110 |
| 116 | 8 |  |  | 5 |  |  |  |  |  |  |  |  | 2 | 116 |
| 117 | 8 |  |  |  |  |  |  |  |  | 11 | 14 |  |  | 117 |
| 120 |  | 16 | 8 |  | 3 |  |  | 5 |  | 11 | 14 | 2 | 15 | 120 |
| 121 | 8 |  |  | 5 |  | 8 | 16 |  | 8 | 7 | 11 | 15 | 2 | 121 |
| 123 |  |  | 8 |  |  |  |  |  |  |  |  | 2 | 2 | 123 |
| 126 | 8 |  |  |  | 3 |  | 16 |  | 8 |  |  |  | 15 | 126 |

@ Did Not Complete Dive

* Decompression Sickness

TABLE C-2

PHASE 1B INDIVIDUAL DIVING INTENSITY
Body of Table Shows Profile No. (Table 1, Appendix E)

| Diver No. | 3 | 4 | 5 | 9 | 12 |  | $\begin{aligned} & \text { ber } \\ & 16 \\ & \hline \end{aligned}$ | $\begin{array}{r} 984 \\ 18 \\ \hline \end{array}$ | 19 | 22 | 23 | 25 | 26 | $\begin{gathered} \text { Diver } \\ \text { No. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 |  | 9 |  | 17 | 18 |  | 13 |  | 1 |  | 11 |  | 4 | 4 |
| 6 |  | 9 |  | 17 | $18^{@}$ |  | 13 |  | 1 | 20 |  | 21 |  | 6 |
| 8 | 15 |  |  | 17 | 10 | 18 |  | 12 |  |  |  |  |  | 8 |
| 9 |  |  |  |  |  |  |  |  | 1 |  |  |  |  | 9 |
| 13 |  |  | 9 |  | 10 |  |  |  |  |  |  | 21 |  | 13 |
| 21 | 15 |  | 9 | 17 | 10 | 1 |  | 12 |  | 20 |  | 21 |  | 21 |
| 22 |  |  |  |  |  |  |  | 12 |  |  |  |  |  | 22 |
| 25 | 15 |  | 9 | 17 | 10 | 1 |  | 12 |  | 20 |  |  | $4^{\text {a }}$ | 25 |
| 26 | $15^{\text {® }}$ |  |  | 19 | 10 | 18 |  | 4 |  |  | $11^{*}$ |  | 4 | 26 |
| 31 |  |  |  |  | 18 |  |  |  |  | 20 |  | 21 |  | 31 |
| 32 | 15 |  |  | 17 | 18 | 1 |  | 12 |  |  |  |  |  | 32 |
| 33 | 15 |  |  | 19 | 10 | 18 |  | 4 |  |  | 11 |  |  | 33 |
| 34 |  |  |  | 17 | 18 |  |  |  |  |  |  |  |  | 34 |
| 37 |  | 9 |  | 17 |  |  | 13 |  | 1 | 20 |  | 21 |  | 37 |
| 40 |  |  |  |  |  |  | $13^{*}$ |  |  |  |  |  |  | 40 |
| 42 |  | 9 |  |  |  |  |  |  |  | 20 |  | 21 |  | 42 |
| 43 |  |  |  |  |  | 1 |  | 4 |  |  |  |  |  | 43 |
| 45 |  | 9 |  | 17 | 18 |  | 13 |  | 1 |  | 11 |  | $4^{\text {e }}$ | 45 |
| 48 | 15 |  |  | 17 | 10 | 1 |  | 12 |  |  | 11 |  | 4 | 48 |
| 52 | 15 |  |  | 17 | 10 |  |  |  | 1 | 20 |  |  |  | 52 |
| 58 | 15 |  |  |  | 10 | 18 |  | 4 |  | 20 |  | 21 |  | 58 |
| 61 | 15 |  |  | 19 | 10 | 18 |  | 4 |  |  | 11 |  | 4 | 61 |
| 62 | 15 |  |  | 19 | 10 | 18 |  | 4 |  | 20 |  | 21 |  | 62 |
| 70 | 15 |  | 9 | 17 | 10 |  | 13 |  |  | 20 |  | 21 |  | 70 |
| 73 |  |  | 9 |  |  |  |  |  |  | 20 |  | 21 |  | 73 |
| 75 | 15 |  |  | 19 | 10 | 18 |  | 4 |  |  |  |  |  | 75 |
| 80 |  |  |  |  |  | 18 |  | 4 |  |  |  |  |  | 80 |
| 82 |  |  |  | 19* |  |  |  |  |  |  |  |  |  | 82 |
| 85 |  | 9 |  | 17 | 18 |  | 13 |  | 1 |  | 11 |  | 4 | 85 |
| 92 |  | 9 |  | 17 | 18 |  |  |  | 1 | 20 |  | 21 |  | 92 |
| 94 | $15^{\text {@ }}$ |  | 9 | $17^{\text {® }}$ | $10^{\text {d }}$ | 1 |  | 12 |  |  | 11 |  | 4 | 94 |
| 95 |  |  |  |  |  |  |  |  |  | 20 |  |  |  | 95 |
| 96 | 15 |  |  | 19 | 10 | 18 |  | 4 |  |  | 11 |  |  | 96 |
| 98 |  |  |  |  |  | 1 |  |  |  |  |  |  |  | 98 |
| 102 | 15 |  | 9 | 17 | 10 | 1 |  | 12* |  | $20^{\text {® }}$ |  | 21 |  | 102 |
| 106 | 15 |  |  |  |  |  |  |  |  | 20 |  | 21 |  | 106 |
| 107 | 15 |  | 9 | 17 | 10 | 1 |  | 12 |  | 20 |  | 21 |  | 107 |
| 111 |  | 9 |  | 17 | 10 |  | 13 |  | 1 | 20 |  | 21 |  | 111 |
| 112 | 15 |  |  | 19 | 10 | 18 |  | 4 |  | 20 |  |  | 4 | 112 |
| 115 | 15 |  |  |  | 18 |  |  |  | 1 |  |  | 21 |  | 115 |
| 117 |  | 9 |  |  |  |  |  |  |  | 20 |  | 21 |  | 117 |
| 118 |  | 9 |  | 17 | 18 |  | $13^{*}$ |  |  |  | 11 |  | 4 | 118 |
| 121 |  |  |  | $19^{*}$ |  |  |  |  |  |  |  |  |  | 121 |
| 122 | 15 |  | 9 | 17 | 10 | 1 |  | 12* |  | 20 |  | 21 |  | 122 |
| 125 |  |  |  |  |  |  |  |  |  |  |  | 21 |  | 125 |
| 126 |  |  |  | 19 |  |  | 13 |  |  |  |  |  |  | 126 |

[^3]TABLE C-3
PHASE 2 INDIVIDUAL DIVING INTENSITY
Body of Table Shows Profile No. (Tables $1 \& 2$, Appendix E)

| Diver No. | November 1984 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \text { Diver } \\ \text { No. } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 20 |  | 11 |  | 22* |  |  | 36 |  | 25 |  | 26 |  | 30 |  | 30 | 2 |
| 5 | 15 |  | 11 |  | 22 |  | 35* |  |  | 25 |  | 30*@ |  |  | 6 |  | 5 |
| 10 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  | 30 |  | 30 | 10 |
| 11 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  | 6 |  | 11 |
| 12 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  | 6 |  | 12 |
| 14 |  | 23 |  | 22 |  | 36 |  |  | $34^{\text {@* }}$ |  | 26 |  | 6 |  | 6 |  | 14 |
| 17 |  | 23* |  | 22 |  |  |  |  | $34^{\text {® }}$ |  | 26 |  | 6 |  |  |  | 17 |
| 27 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  | $30^{\text {* }}$ |  | 30 | 27 |
| 31 |  |  |  |  |  |  |  |  |  |  |  | 26 |  |  |  | 30 | 31 |
| 32 |  |  |  |  |  |  |  |  |  |  |  |  |  | 30 |  | 30 | 32 |
| 37 | 15 |  | 11 |  |  |  | 35 |  |  | 25 |  | 30 |  |  | 6 |  | 37 |
| 39 |  | 23 |  | 22 |  | 36 |  |  | 34 |  | 26 |  | 6 |  | 6 |  | 39 |
| 44 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  | 30 |  | 30 | 44 |
| 46 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  |  |  | 46 |
| 47 |  | 23 |  | 22 |  | 36 |  |  | 34 |  | 26 |  | 6 |  |  | 30 | 47 |
| 49 | 15* |  | 11 |  | 22 |  | 35* |  |  | 25 |  | 30* |  |  |  |  | 49 |
| 56 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  | $30 * 0$ |  | 30 | 56 |
| 62 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  | 6 |  | 62 |
| 66 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  | 6 |  | 66 |
| 70 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  |  |  | 30 | 70 |
| 81 | $20^{\text {® }}$ |  | 11 |  | 22 |  |  | 36* |  | 25 |  | 26 |  | 30*@ |  |  | 81 |
| 93 | 20 |  | 11 |  | 22 |  |  | 36 |  | 25 |  | 26 |  | 30 |  | 30 | 93 |
| 102 |  | 23 |  | $22^{\text {® }}$ |  | 36 |  |  | 34 |  | 26 |  | 6 |  |  | 30 | 102 |
| 104 | 15 |  | 11 |  | 22 |  | 35* |  |  | 25 |  | 30 |  |  | 6* |  | 104 |
| 105 | 15 |  | 11 |  | 22 |  | 35 |  |  | 25 |  | 30 |  |  |  |  | 105 |
| 106 |  |  |  |  |  |  |  |  |  |  |  |  |  | 30 |  | 30 | 106 |
| 113 |  | 23 |  | 22 |  | 36 |  |  | 34 |  | 26 |  | 6 |  |  | 30 | 113 |
| 115 | 20 |  | 11 |  | 22* |  |  | 36* |  | 25 |  | 26 |  |  |  |  | 115 |
| 117 |  | $23^{\text {* }}$ |  | 22 |  | 36 |  |  | 34 |  | 26 |  | $6{ }^{\text {@ }}$ |  |  | 30 | 117 |
| 118 |  | 23 |  | 22 |  | 36 |  |  | 34 |  | 26 |  | 6 |  | 6 |  | 118 |
| 121 |  | 23 |  | 22 |  | $36^{\text {® }}$ |  |  | 34 |  | 26 |  | 6 |  |  | 30 | 121 |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 30 | 126 |

@ Did Not Complete Dive

* Decompression Sickness

TABLE C-4
PHASE 3 INDIVIDUAL DIVING INTENSITY
Body of Table Shows Profile No. (Tables $1 \& 2$, Appendix E)

| $\left\lvert\, \begin{aligned} & \hline \text { Diver } \\ & \text { No. } \end{aligned}\right.$ | December 1984 |  |  |  |  |  |  |  |  | Diver |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 11 | 12 | 13 | 14 | 17 | 18 | 19 | 20 |  |
| 1 |  | 28 |  | 29 |  | 32 |  | 37 |  | 1 |
| 3 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 3 |
| 7 |  | $28^{*}$ |  | 29 |  | 32 |  | 37 |  | 7 |
| 15 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 15 |
| 19 |  | 31 |  | 28 |  | 32 |  |  | 24 | 19 |
| 20 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 20 |
| 29 |  | 28 |  | 29 |  | 32 |  | 37 |  | 29 |
| 30 |  | 28 |  | 29 |  | 32 |  | 37 |  | 30 |
| 31 |  |  |  |  |  |  | 33 |  | 24 | 31 |
| 33 |  | 28 |  | 29 |  | $37^{*}$ |  |  | 24 | 33 |
| 35 |  | 31 |  | 28 |  |  |  | 32 |  | 35 |
| 36 |  | 28 |  | 29 |  | 32 |  | 37 |  | 36 |
| 38 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 38 |
| 51 |  | 28 |  | 29 |  | 32 |  | 37 |  | 51 |
| 54 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 54 |
| 59 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 59 |
| 60 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 60 |
| 63 |  | 31 |  | 28 |  |  | 38 |  | 24 | 63 |
| 64 | 29 |  | 27 |  | 38* |  | 33 |  | 24 | 64 |
| 65 | 29 |  | 31 |  | 27 | $37^{*}$ |  |  |  | 65 |
| 67 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 67 |
| 68 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 68 |
| 70 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 70 |
| 71 |  | 31 |  | 28 |  |  | 38 |  | 24 | 71 |
| 72 |  | 31 |  | 28 |  |  | 38 |  |  | 72 |
| 78 |  |  |  | 28*@ |  |  | 38 |  | 24 | 78 |
| 79 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 79 |
| 83 | 29 |  | 31 |  | 27 | 37 |  | 32 |  | 83 |
| 84 | 29 |  | 27 |  | 38 |  |  |  | 24 | 84 |
| 88 |  | 31 |  | 28 |  |  | 38 |  | 24 | 88 |
| 89 |  | 31* |  |  | 27 |  |  | 37 |  | 89 |
| 90 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 90 |
| 91 |  | 31* |  |  |  |  | 38 |  | 24 | 91 |
| 97 |  | 28 |  | 29 |  | 32 |  | 37 |  | 97 |
| 98 |  |  |  |  |  |  |  |  |  | 98 |
| 99 | 29* |  | $31^{\text {® }}$ | 28 |  | 37 |  | 32 |  | 99 |
| 100 |  |  |  |  |  |  |  |  |  | 100 |
| 101 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 101 |
| 103 |  | 31 |  | 28 |  |  | 38* |  |  | 103 |
| 107 |  | 31 |  | 28 |  |  | 38 |  | 24 | 107 |
| 114 | 29 |  | 27 |  | 38 |  | 33 |  | 24 | 114 |
| 118 T | 29* |  |  |  |  |  |  |  |  | 118 T |
| 119 |  | 28 |  | $21^{\text {® }}$ |  | 32 |  | 37 |  | 119 |
| 122 T |  | 31* |  |  |  |  |  |  |  | 122 T |
| 123 | 29 |  | 31 |  | 27 |  |  | 32 |  | 123 |
| $\underline{124}$ |  | 28 |  | 29 |  | 32 |  | 37 |  | 124 |

© Did Not Complete Dive

* Decompression Sickness

T Tender


## TARIE OF MAMTMUM FFFMISEIELE TIESU＇F TEREIGME

：VFHL 1：Z－NITROTAET：
TISSUE HALIF－TIMES．

| CEFTH |  | 5 ＋1／d | 10 MIt | 20 MTH | 40 MIH | $80 \mathrm{MIJ:}$ | 1こ！M11： | 160114 | $\therefore$ Ofrith | 4）M11： |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1．（19）SuF． | 1．00 SLF． | 1．00 ECF | 1．Un $\because[i F$ | 1．00 | 1．Hu SOF | 1．80 EFF | 1．！日成吅 | 1．$\because 1 / \mathrm{F}$ |
| 10 | F－31 | 120.000 | 98.0100 | 78.0170 | 5¢，गo u | 48.5010 | 45.500 | 44，501 | 44.000 | 45.509 |
| ar | $F=1$, | $1 \div 6.000$ | $10 \leqslant .010$ | 88．（1） | 因， 000 | E¢，5r | 55.5017 | 54.505 | 54.080 | 5756 |
| S！ | F\％ | 140.0010 | 118．010 | 98，01］ 0 |  | 6\％，डin | －5．59！ | 64 En | 64 060 | ¢又 5fir |
| 44 | $F \equiv W^{\prime}$ | 150．400 | 128.000 | 108．01） 0 | SE． 000 | re． 5 | 「5．500 | 74.50 | 74． 000 | －5 5 |
| $5 \pm$ | Fsh | 1F．0．400 | 130． 10 | 113．41） | Fe． 900 | е¢，S0 | ¢5 500 | Et．5ib | E4 int | $\because 2$ |
| E ！ | F＇did |  | $14 \mathrm{c}, 010$ | 128．（1） 0 | （16． | 98，5111 | －，5！！ | －4．E110 | 94000 | 33． 3014 |
| $\cdots$ | $F \equiv 1$. | 180．000 | 15s．000 | 135．000 | 116，000 | 108．54］ | 105.50 | 104．5017 | 104．000 | 113．5in |
| A． | $F=W$ | 130.000 | 168.000 | 149．01？ | 1えら，0！！ | 118.5 | 115.500 | 114.5011 | 114.0019 | 113．519 |
| Gu | $F=0$ | 200． C 110 | 1 18\％． 010 | 155．（1） 11 | 156，白保 | 129．Eい1 | 125.564 | 124． 510 |  | 125 ¢0， |
| $10 \%$ | F $=4$ ， | 210.0100 | 188.000 | 153．010 | 140．1000 | 138.500 | $15 \% 500$ | 134．560 | $1 \pm 4.900$ | 159．50ii |
| 11 is | Fご高 | ここの．609 | 153．000 | 175．（1） 0 | 156，边吅 | 148．5：\％ | 145.500 | 144，5！ | 14400 | 147， 51 |
| 120 | F＇Sd | 230.11001 | 205 （11） 0 | 188，01） | 168．000 | 153． 5111 | $15 \% 5010$ | 154．5010 | 15ヶ，！ 100 | 1¢3．こ！！！ |
| 150 | $F$ Ful | 240,010 | 218.010 | $198.011) 0$ | 176．000 | 168．500 | 165．500 | 154500 | 184．009 | 163，「！0 |
| 140 | FSu | $\because 513.000$ | 225.000 | 203 （11） 0 | 135， 000 | 178.56 in | 175 540 | 174，5010 | 174.060 | 1－3，500 |
| 150 | FS ${ }^{1}$ | 260.010 | 233．0150 | 218.0150 | 176．000 | 188．5010 | 185．5ib | 184．506 | 1－4． 510 | 185，506 |
| 180 | FSd | 270.000 | 248.000 | 223．01） | 206．900 | 198，509 | 195． 500 | 194．500 | 154．100 | 19\％． 5 （1） |
| 170 | Fcid | 250.0101 | 258.000 | 238，（1） 0 | 216．000 | 209．509 | 205.509 | 204.500 | 294.400 | こ07，501t |
| 130 | FSW | 290.000 | 258．000 | 248．（11） 0 | 226．000 | 218，50！ | 215．500 | 214．509 | $\therefore 1+100$ | －1 ，560 |
| 100 | FSW | Fro．aro | 278.000 | 258．000 | 230，000 | 228．5f0 | $2 ¢ 5500$ | 2－4．50\％ | ここ4．1000 | 223.560 |
| 201 | F5d | 310.000 | 288．000 | 268．090 | 246．000 | 238，500 | 23E，500 | 234．500 | 224，100 | －2 |
| 210 | FS込 | ことの，0n0 | 298．（1） 1 | 273．000 | 256，ग00 | 24－590 | 二45．500 | 244.500 | 244.900 | ごT，E（1） |
| ご心 | FSW | 3－0，חr | 306.0100 | 2E8， 0190 | 266，0t0 | 255，500 | 255．569 | 254.509 | 254，409 | $\therefore \because 3.541$ |
| c 31 | FSh |  | 318.100 | 278.000 | 2FE， 000 | 26E， 500 | 205．500 | 264．503 | 玉e4，060 |  |
| 24 | FSul | 350.010 | 323 ． 100 | 308.090 | 266， 000 | ごす．500 | 275．500 | 274．500 | 274． 010 | 2\％3．500 |
| 250 |  | उE0，0no | 338,000 | 318.000 | 296，000 | 288，5rio | 285，501 | 2¢4．500 | 264，1000 | 263，5f1） |
| 2E！ | FSul | F\％o． 100 | 349.100 | 328．000 | ごヒ，0i0 | 290，5rio | 295，500 | 294.500 | 2－4， 100 | 2735017 |
| ご | F5u | 350.000 | 358.000 | 338.010 | 316.000 | 308．5（1） | 305.500 | 304.500 | 304.900 | 303．50n |
| ご．6 | FSW | 3－0．010！ | 3¢8． 100 | 348 ，（11） 0 | 326．000 | 318，507 | －15．500 | 314.500 | －14．1000 | 315．509 |
| 守 | FSW | 40 n .010 | 378.000 | 359， 010 | 336.000 | 328,500 | 525，500 | 324， 500 | ここれ，000 | こここ，5年い |
| 200 | FSW | 410.000 | 388.0100 | 368，010 | $34 \mathrm{E}, 000$ | 336.500 | 335.500 | 334.500 | 334.900 | 335.501 |

ELODE PGRMMETERS
（PRESSUFE IH FSH； 35 FSU＝ 1 ATH）

| $1 \mathrm{HO}^{\text {a }}$ | FH2O | PVEO2 | PV®2 | AMEAn2 | FEr，i－ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1．\％ 0 | 0.00 | 2.30 | 2.00 | 0.00 | a． 0 \％ |

TJS:こ'F HFIF-TM:C:

| $\therefore$ FFib | $\begin{array}{cc} 5 & \text { HIH } \\ \therefore & \because f ; \end{array}$ | $\begin{aligned} & 10 \mathrm{MJH} \\ & 7 Z E C \mathrm{~F} \end{aligned}$ | $\begin{aligned} & 20 \text { MIH } \\ & .32 S H A \end{aligned}$ | $\begin{aligned} & 4 i \quad M P H \\ & -2 \therefore r \end{aligned}$ | $\begin{array}{ll} 8 u & \text { M1 } \\ \therefore Z & \because F \end{array}$ |  |  |  | $\begin{aligned} & -40 \mathrm{AIm} \\ & -E \mathrm{E}=\mathrm{F} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 litith | 1c！ | 9\％，780 | 78．760 | 56.764 | 4 4，＜t1： | 4 ¢，くら号 | 4こ．26成 | 44．7Ei | 44，269 |
|  | 1， 5 \％ 50 | $10 \% 50$ | 26．590 | ¢n．5\％ | 59， 0 | 5 | E5．0\％0 | 54.50 | 5.7 ¢0， |
| r $+1,1$ | 140.500 | 118.500 | 78．500 | 76． 519 | Eq．日＂ | ¢ 6 ¢ 017 | E5． 10 | 64.50 | －4 900 |
| ．1：1＋． 1.1 | 154．410 | 12E．4ty | $10 \% .410$ | 56.410 | ¢\％ 519 | 75．${ }^{\text {¢ }}$ | －4， 911 | 74410 | －5， 910 |
| $i=\times 1.1$ | 1－11， 510 | 136300 | $11 \% 300$ | \＃6．3Fi | 5\％＝－ | 安它家号 | 3480 | E4， 500 | ¢5， 0 |
| －－ 4 i | 180， 30 | 143.280 | 12，玉E0 | $1 \mathrm{lt} \times \mathrm{E}$ |  | 95.50 | 94．780 | －4， E | 93， 70 |
| －－ 1,11 | 1\％it， 19 | 158.194 | 135，190 | 115．150 |  | 1安，ビち | 104.65 | 194．190 | 159．640 |
| $\therefore \mathrm{B}+\mathrm{ta}$ | $3 \square \%$ On | 163．060 | 148.060 | $1 c_{6}^{6} .040$ | 118 560 | 115.560 | 114.560 | 114．860 | 11350 |
| $\rightarrow 1+81 i$ |  | 17\％．960 | 15\％．960 | 155， 661 | 1\％8．400 | 185．460 | 124，460 | 1ご．FE！ | 1ご 4.40 |
| 1．． 5 － 6 | $\because 12 \mathrm{~B}$ | 1ここ． | 16\％．824 | 145 5－5 | 1ごこご宁 |  | 154 ご！ |  | 1－3． |
| 1： $1+1$, | こ1； 9 | 137．6F！ | 17\％．6\％ | 15589 | $14 \% .170$ | 145．170 | 144196 | 147，67！ | 1s玉．1才， |
| $\because \therefore \therefore=\therefore 1$ | $\therefore-4-0$ | cit．450 | 185．490 | 165.470 | 157.750 | 15.590 | 155．590 | 152.470 | 152， 9 |
| $13!+8$ ¢ | $\cdots \therefore 150$ | 217．150 | 197，150 | 175．150 | 16T，E\％O | 164．8E1 | 15\％，650 | 15こ．150 | 16－2．60 |
| $1+4+24$ | 2． 3.840 | 2ごも． $2+0$ | 206.840 | 184.340 | 177．340 | 174.340 | 173.340 | 172．840 | 172．341 |
| 15，F\％d | $\leq 5$ | 250.490 | 216.490 | 194.490 | 13\％．930 | 183．350 | 152．950 | 182，43i | 181.970 |
| 1511 F＝1， | ¢ ¢ ，0！ |  | 2こe 060 | 204 リン |  | 1\％\％ 5 | 172.58 | 132,400 | 1 F 1. |
| 1 it $5=4$ | $\because \cdots$ | 2心5． 240 | 235.240 | 213.2411 | 205.740 | 202．741 | 201.741 | 201240 | 200.740 |
|  | 26,240 | 264．${ }^{\text {2 }} 40$ | 244.240 | 玉2c． 240 | 214．74n | 211.740 | 210.740 | 210,540 | 206.7410 |
| $1 \% F \%$ | 2－5－i， |  | こちご大の可 | 230.760 | 22さ． 2 ¢ |  | 217.240 | $\pm 18.760$ | \％18．260 |
|  | 303．030 | 251.030 | 2.61 .030 | 239.030 | 231．530 | 226．550 | 2゙こ．530 | $22 \%$ 030 | 2こけ，556 |
| $\because: 0 F \%$ | 520．000 | 299．000 | 275.010 | 256.000 | 245．509 | 245.500 | 244.500 | 244.000 | －4．5，500 |
| $\because F=14$ | $355,6 \mathrm{Br}$ |  | 2 cs ¢ 110 |  | ご天， 50 | ごッ ，500 | 254． 510 |  | E3，50 |
|  | 540.000 | 318.0010 | 238.010 | 2\％ 5.000 | 2－6． 50 |  | 264 500 | $\therefore \mathrm{ET} 4.000$ | 263． 500 |
| － $10 \mathrm{~F}=1 \mathrm{~d}$ | 5゙．is（1）0 | $3=8.000$ | 50S．010 | 202．000 | ごら，E60 | こちら，E00 | 274．500 | 2－4．000 | 275．500 |
| $\therefore \mathrm{F}$ | उrit पity | 335．0110 | ज18．010 | ¢ 56.000 | 2E\％，E¢0 | くお5，E0y | くら4．500 | ごく4， 000 | ことて，500 |
| $\therefore \therefore+6$ |  | 34\％．000 | 328.000 | 306.000 | 2\％ 5.546 | 295.500 | 294．500 | 294， 000 | － 33.500 |
| $\therefore F=10$ | 3s？600 | 35.3000 | 335.000 | 316． 000 | З18，51， | T05．Sot | 304,500 | Ti4．090 | 313,560 |
| $\therefore 1 . F \mid r$ | 7 | 36\％． 900 | 348.0150 | 3ट6． 0 U0 | 31：Etur | ¢1 | 514500 | ड14，000 | \＃1 |
| $\cdots \mathrm{F}$ | qlio．onn | 378，ono | 358.000 | 356.000 | 398.510 | 5 F 5 5 50 | 324．500 | 324.001 | ここち．500 |
| $\because F \% 1 i$ | 41リ 100 | aes ono | 365,010 | $34 E .000$ | 358， 50 ¢ | －35，500 | 354.500 | ここ4．000 | 23．500 |

BLOR FOFAMFTEFS
$\therefore$ FRESGIIFF IN FSM； 32 FS $!=1$ OTH？
（Hin：FH2O
1.74 fVerg？

P4O：
AMEAR2
FEG：F
亿品
1.87
c．
$2.4 t$


TARLE GF MAYIMMN FFFNTSSTRAE TI :二UF TFH: TMH:
:VAl25-NTTPOGF

TlSBUF HALF-TIAE:


ELOMO FAPAMIFTEF:
(FFESEUEE IH FSH; 32 FSH=1 HTO;

Fr:CP:
7

FH20
200
fiver
PW?
HMFPT?
FEIT: IF
2.4

11 a!

TARIE OF MAYINIM FEFMISSIELE TISSHF TEHSTINC
GVifich－HITEOGFi
TlSSUE HAR．F－TIMES

| 「－¢！！ | ¢ M1\％ | 10 MJH | 20 MIN | 40114 | 80 MTH | 18！MIN | 16．1H14 | 二itumid | $\therefore 40 \mathrm{MIN}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 － | 1．70 S［号 | 1．55 S［Fi | 1．35 E05 | 1．00 505 | デ $\because \mathrm{C}$ | 64 S［F | $455[P$ | 335 CF |
| 14.14 | $1 \pm 0,760$ | 98．760 | 73．760 | 56.760 | 49，250 | 46.200 | 45.260 | 44．760 | 44.250 |
| $\therefore F: 8$ | 150.590 | 103，590 | 82，590 | 66.50 | 57.1050 | 56.090 | $55.0 \pm 0$ | 54.59 | 54．950 |
| $\bigcirc \mathrm{O}$ | 14\％．560 | 118.500 | 98，500 | 75．500 | 6\％．96 | ES．000 | 65.000 | 24，560 | 64.000 |
|  | 150．410 | 126.410 | 108．410 | 96．410 | 78.910 |  | 74.910 | 74.411 | －3， 910 |
| －！Fごこれ | 16日． | 13 E ． 30 | 118．360 | G6，369 | 88． 840 | 85， 860 | 84.850 | 34．350 | 85.860 |
| $\cdots \mathrm{F}$ ¢ F |  | 148． 290 | 125.290 |  | 93．780 | 95， 780 | 54.780 | 94250 | 二－ 78 |
| －FSu | 180， 19 | 150．190 | 138， 190 | 116.19 | 108.69 | 105， 60 | 104， 694 | 104．190 | 1示安 |
| Ei FSU | 1\％0，060 | 163． 160 | 143，060 | 1安安，リ¢ | 118.559 | 115，560 | 114．560 | 114，16 9 | 113．5た！ |
| $\because \because \mathrm{F}=\mathrm{d}$ | 159．960 | 177．SE＠ | 157．Э¢ | 155．3E0 | 128．460 | 125．460 | 124．460 |  | $1 \div 3.460$ |
| 1い号 F | －¢ E ¢ | 1日大． | 167， $\mathrm{BFO}_{0}$ | 14E，Ex | 1む゙，シit | 155，5\％ | 154． 5 c |  | 1 |
| $1145=14$ |  | 177， 5 | 175．590 | 155．651 | 145．150 | 145.150 | 144．130 | 147．644 | 145．150 |
| 1－F Ful | くこう．4 4 | $207.4 \div 0$ | 187.490 | 165．490 | 157.990 | 154．950 | 153．350 | 152490 | 152． 90 |
|  | c－ 150 | 217，150 | 197，150 | 17E，15！ | 167．65i | 164，E5i | 153，ES！ | $163 \cdot 15$ | 16\％－5il |
| 14i．Fsul | 349.810 | ごご840 | 206.840 | 184.840 | 177．340 | 174， 340 | 173，3419 |  | 1rこ 340 |
| 15 \％F Sid | 253.470 | 236.470 | 215.490 | 154.490 | 18ら．990 | 123.990 | 182，970 | 12.430 | 181.390 |
| 1－4 FEM | cis． 10 | 246.020 | ご6． 120 | c） $0 \cdot 1.020$ | 136.55 | 155.580 | 192，500 | 1\％2， 0 20 | 1\％1． 5 |
| 1F\％5 ¢ | 2．5．290 | 2「5．240 | 255.240 | 213.240 | $20 \% .740$ | 202.740 | 201.740 | $=01.2+0$ | $\therefore 04.740$ |
| 180 F ¢ 16 | 235． 240 | 254．240 | 244．240 | 22こ．240 | 214.740 | 211.740 | 210.740 | 210.240 | こ69．741） |
| $17 \mathrm{\square}$ | －$\ddagger 4.760$ | ごご大日 | こここ．ア60 | 230.760 | こと3．2ら门 | 二厶儿，ze0 | こ19，\％60 | 21：．7E゙い | ごも．こらけ |
| $\therefore 0 \square+5 W$ | 303.030 | 281.030 | 261．030 | 235．030 | 231．530 | 228.550 | 227．550 | 2ご，050 |  |
| $\because 10 \mathrm{FGH}$ | 320.000 | 2\％6， 000 | 278．000 | 25\％． 000 | 248，50n | 245.500 | 244．500 | 244.000 |  |
| celi Fsw | ES0，000 | 308.0100 | C8E， 010 | 266．000 | 25\％．501 | こらこ，5！0 | 254． 500 | 254， 610 | $\because \because$ ，E10 |
| －F F W | －40． 000 | 318.000 | 258．010 | ごら，000 | 268．541 | 二心5，500 | 264．500 | こら4．090 | 203．50 |
| 94．1FFin | こち0，¢00 | 523．010 | 308.010 | 25\％．000 | 2゙®．5！9 | 2\％ 500 | 274．500 | ご4，000 | 二小3．500 |
| $\therefore \because$ Fこい | こey． | 3ड | 318．019 | 它馬，900 | 28す． 500 | 285，500 | 264．514 | ここ4．600 |  |
| c－F F \％ | ara gino | 348．000 | 328．010 | 306.000 | 298．500 | 255．500 | 254．500 | 274.000 | 二59．500 |
|  | ごこ0．0000 | 35\％， 100 | 338.0130 | 31E．000 | 308.504 | 305，500 | E04，500 | 304.000 | 513．500 |
| －Fth |  | SE8． 100 | 348.010 | 326，040 | $318.5 \% 4$ | 515．500 | 314．500 | 314.000 | 513．550 |
| －Fちい | 41.0 .40 | 373．000 | 358.000 | ЗडE， 000 | 328．5c！ | 525．500 | 324．500 | ご24．000 | $3 こ 5.500$ |
| T！！F F＝， | 410,50 | 383．000 | 368．010 | 346,000 | 338.500 |  | 334.500 | 3 34 ， 00 | 3ご気吅 |
| －－－－－ | －－－－－－ | －－－－－－－ | －－－－－－－ | －－－－－－－ |  |  |  |  |  |

GLONT Faprmeters
©FEESSUPE IN FEM： 35 FSH： 1 ATA ：
トロー
$\because \cdot 0$

Fuege
pū́
2.50

AMEAOZ
2.46

## FEnYF

10.0010

## 

## 

TISSIE HALF-TIMFE


ELOUD PARAMETERS
(PRESSIIFE IN FSU; उJ FSザ=1 AT: ;
F.rr: $\quad \mathrm{FHzC}_{2}$
E. 00

PVECI2
Fwn
2.60

AMEAOC
2.46

FEG':
10.000
table of maximum permissible tissue tensions
(V'FLL29- NITROGEH)
TISSIUE HALF-TIMES

blood papameters
(PRESSURE IN FSU; 33 FSU=1 ATA)

FACSI
PH20
2.00

PVEO2
1.87
puoz
2.80

AMEAOZ
FR日vF
2.46
10.000

$\therefore$ サWALS：WITEUEH
TISSUE HMIF－TJMES

| ［EFTH |  | 5 MIN | 10 MIH | 20 MIf | 43 MtH | EGMJH | $1 \therefore 0 \mathrm{mIN}$ | 160 mIN | E09 MIM | $\cdots$－ 4 Helt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fr Erp | ． 76 SNP | ． 9 e | ． 5 ¢ | GEEI．F | $\cdots \mathrm{F}$ | ¢f ¢f\％ |  | 9，$\because 1 \cdot \mathrm{~F}$ |
| 14 | $F \equiv 6$ | 126，670 | 114.670 | 84，6\％ | 62．670 | Et，170 | 50.5 ¢0 | E\％．670 | 50.420 | 50.170 |
| 29 | $F=$ ， | 136．6：0 | 124．670 | 94，¢？ 0 | 72．00 | S空170 | く0． 50 | 60，$\% 0$ | 6i）421 | $\because 1.170$ |
| す！ | FSha | 146．670 | 134．670 | 104．570 |  | －170 | F0 Fio | 70.670 | 70.421 | 73．1－0 |
| 40 | $F \leq h$ | 156．670 | 144.670 | 114.670 | 92.670 | 気 1\％0 | 80． $0^{20}$ | วリ．6？ | （1）．42！ | －0．170 |
| 50 |  | 166，6－0 | 154．670 | 124.50 | 102.670 | 5s． 1 号 | $90.9 こ ゙ 1$ |  | 90 4ごい | 3i1． 1 |
| 内i | Fこい | 176．670 | 164.670 | 174．67 | 112.670 | 105．1－10 |  |  | 110．0゙い | 18！ 18 |
| 70 | FSW | 186．670 | 174，670 | 144． ¢ $_{\text {F }}$ |  | 115．150 | 1；景，于20 |  | 111．420 | $11!10$ |
| Ei | FSb | 176.670 | 184．6す0 | 154． | 132． | 125．1ヶ！ | 120.520 | 1くす．心が | 1边 4\％ |  |
| 90 | F三！ | 205.670 | 194.670 | 164．「品 | 142．ET0 | 135．170 | 130． 3 ¢ | 150．5゙品 | 170．430 | 17n．tid |
| 109 | $F=11$ | 216.670 | 204.670 | 174．678 | 152， 50 | 145．170 | 140.324 | 145.6 | 141．4？ | 141：97 |
| 110 | $F$ Fid | 2 c 5 E 70 | 214.570 | 184，670 | 15\％．0．0 | 15\％，170 | 9 ¢ 0，ヨa | 159，穴： | 154．4\％ |  |
| 120 | Fこい | 236．670 | 224．670 | 194，6－0 | 1てこ．E「0 | 1－c．170 | 160.720 | 1セすジロ | 160．4 ${ }^{11}$ | 1－！ 1 ¢ ！！ |
| 17 B | FSW | 246．670 | 234．670 | 204.50 | 18べら0 | 1？1\％ |  | 170．6\％ | 1，0．4．1） | 1－1．170 |
| 140 | FSai | 256．670 | 244．670 | 214，670 | 192．6ro | $185.1 \%$ |  | 180 ¢ ¢ | 180．4c0 | $1: 0.19$ |
| 150 | F5 | 266．670 | 254，670 | 224．6ア0 | 2！2．Eヶ口 | 1FE，1F | 1二0．40 | 1\％n，¢0 | $190.4=1$ | 1－6．170 |
| 150 | FEW | 276．670 | 264.670 | 234．670 | こ12．ET0 | 20ヶ．1品 | 200． 000 |  | $\therefore 10.420$ | この而，1－19 |
| 170 | F Stu | 286，670 | 274．670 | $2+4.670$ | 2こ2，-1 | 二15．1－0 | ¢10， 21 | $\therefore 16$ | $=110$ | ミ1i 1－1 |
| 180 | $F 口 \begin{aligned} & \text { F }\end{aligned}$ | 296．670 | 284．6r0 | 26．4．6「行 | 2ق2．670 | 2\％5，1－0 | こrr．ヲご | こ，二－ | $\therefore 1.410$ | ごの，1－ |
| 130 | FSW | 306.670 | 294.670 | 264．670 | ごごビ吅 | 235．170 | ご吅，Эら | $\therefore 30.68$ | $\underline{2} 9.4 \%$ | ご1．17 |
| ¢00 | FSU | 316.670 | 304，670 | 2ア4．E7！ |  | こ4F，170 | $\therefore 40.350$ | く49，¢\％ |  | ¢41．1才 |
| E10 | FSU | 326．670 | 314.670 | 284， 570 | ごん，¢フ0 | 255，1\％ | こヶ0．$\because=0$ | こ50．67？ | ＂！，40！ | $\because 6.17$ |
| ごす | FSW | 336.670 | 324．670 | 294.570 |  | $\geq 0^{\circ} \mathrm{O}, 170$ | 26ti $\because 15$ |  | $\therefore-8.41$ | －54．180 |
| こす | FこH | 346．670 | 334.670 | 304.650 | 云示，シ0 | c $\bar{\square}$ |  | ごが曻 | $\therefore 1.4: 1$ | $\therefore \because 1-10$ |
| 2411 | FS！ | 35心．670 | 344.670 | 314.670 | 2F，可 | 二ar，1－n | 二小け，Эご | － 6 ¢－ 0 | 2n0．4：＂ | 二小，1－8 |
| 250 | $F \subseteq W$ | 366．670 | 354．670 | 324， 570 | 302.570 | 295．100 | 240．3ご1 | 230.650 | ＜ $40.4 \%$ | 208170 |
| 260 | FSW | 376.670 | 364.670 | 334．670 | З | 三里，1\％0 |  | 3010.670 | $360.4 \overline{4}$ | ज14， 15 |
| －79 | FSH | 356.670 | 374.670 | 344 فフ0 | 3ご心可 | 玉1二 170 | 310 \％ 30 |  | 390，4\％u |  |
| 250 | FGW | 396.670 | 384．670 | 354．6．70 |  | Tas．1－0 |  | $\geq 20.6 .0$ | 5i0．420 | 3． 1.170 |
| 290 | FSU | 4 UE． 670 | 354.670 | 354,670 | 玉42．6－4 | SE5，1：4 | 350.30 | ごい，守安 | 35\％，4\％ | 35 ¢ 1－0 |
| 360 | FSW | 416.670 | 404.670 | 374，670 | $35 \mathrm{x} \because \mathrm{G}$ | 345.180 | 741． 321 | 「4＇6ic | 341，4？ | $3+4.17$ |

## GLODC Fafonmetfeg




| CHVO2 | 2．39 | 2.39 | 2.39 | 2．3F | こ． | 2.3 | 2．39 | ご， | $\because 3 \exists$ | Oit． |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FVET？ | 1.87 | 1.67 | 1．5r | 1．87 | 1．8i | 1.6 | 1.8 | 1．$\dot{\square}$ | 1 －$\square^{\circ}$ | cFst |
| FEDYF | 22．00 | 20．00 | 18.00 | 15．00 | 10．00 | 7.10 | T．00 | 7.00 | $\bigcirc .013$ | ¢FSn |

TAELE dF MAKIMUM FEFHISJIELE TIS：IUE TENSIDH：S
VWfins－HITFOLSFII


## BLODD PAFAMETEF：

## （PFEGEURE IN FSH； 33 FSH ATA）

| PAC02 | （FSU） | PH20＜FSN） | DAAOESVOL $\because$ ） |
| :---: | :---: | :---: | :---: |
| 0 |  | 2.00 |  |


| CNat | 2.39 | 2.39 | 2．35 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 | （YOL $\because$ ） |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FVにくて | 1.87 | 1.87 | 1.87 | 1.87 | 1．8\％ | 1.87 | 1．87 | 1.87 | 1．88 | （FGH． |
| FEOUF | 22.00 | 20.00 | 18．00 | 11.00 | 10.00 | ？．00 | 7．00 | 7． 00 | 7.00 | （FSO） |



## 

TISSUE HPLF－TIMES

| ［EETH | EMIH | 10 MTH | citatid | 41 MIH | Eti HTH | 1ご！MItid | 15in MIH | ＝6す MIt！ | ご隹 Mit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4＇EnF | .50 SいF | ． 5 ¢ | ¢ $\quad \therefore$ cc | 3－Eto | 72 S0F | rin Sle | $4=\therefore 5$ | 4155 |
| 10 F | 120．670 | 114．67 | 玉4 ジ̇U | 61.40 | E5， 170 | 51.980 | E0．670 | E0， 400 | Ei， 17 |
| ごFFS | 15ら．670 | 124.670 | 94．だロ | P1．Ero | 65.170 | 61.320 | 4．0．679 | 64． 4 Eis | 60.170 |
| 36FEd | 14＋i．670 | 134.670 | 104．6．76 | 81.60 | 75.170 | 71.920 | 7 （i， 670 | F1．4i8 | 70，170 |
| 4 4，FSW | 156．670 | 144．6゙ア0 | 114．E\％ |  | 区玉．170 | E1．9\％ | Bu． $\mathrm{Br}_{0}$ | 20， 400 | 玉日．tru |
| ¢if FSli | 150．650 | 154．670 | ごす。らす。 | 101．＊こ0 | $\cdots 5.170$ | 91.900 | 品 ¢\％号 | 30.424 | 919.170 |
| EG F Sis | 1\％ヵ．$\%$ \％ | 164.670 | 134．6．0 | 111，¢\％ | 105．170 |  | 10 ¢！¢ ¢ |  | 100.170 |
| ¢ F ¢ | 136.670 | 174．670 | 144．6．70 | 121． 60 | 115，170 | $111 . F 20$ |  | 119，4c0 | 110.170 |
| G：FSW | 196．670 | 184.670 | 154．6\％0 | 131.50 | 125， 170 | 121．320 | 124．670 | 1＊ 0.450 | 120.170 |
| $\because 0$ F w | 206．670 | 194．670 | 164．670 | 141.670 | 135．170 | 131． $0^{-10}$ | 130，6「或 | $1 \div 0.420$ | 130.170 |
|  | 216.670 | 204.670 | 1ヵ4，が可 | 15150 | 145，170 | 141，きこけ | 14！¢90 | 1410，421 | 1411．179 |
| $110 \mathrm{~F}=1.1$ | 2ご，6T0 | 214.570 | 184．880 | 161.80 | 159，170 | 1こ1，Эごす | 15GEFO | 158．420 | 150.170 |
| 1：0FEM | c3e．6\％ | 224．670 | 194.80 | 171．0\％0 | 165．170 | 1e1．95リ |  | 184．420 | 1－1．170 |
| 190 FEW | 245.670 | 234．670 | 204.670 | 181．6ro | 17E．170 | 171． 120 $^{\text {c }}$ | 170．6く0 | 170．42！ | 1\％ט．170 |
| $140 \mathrm{~F}=\mathrm{W}$ | 2̇6．6\％0 | 244.670 | 214.670 | 191.670 | 185，170 | 121． 320 | 180．670 | 150．420 | 180.170 |
| 150Fsht | 266．6ア0 | 254．670 | 2ご，シア0 | 201．570 | 1奖，170 | 171．720 | 150 宁品 | 170．4ej | 170．170 |
| IEM FSW | C76．670 | 264．670 | 2．4．6．70 | 211．ET0 | 己心c， 170 | 201，気 | 200．670 |  | 200.170 |
| 1；F Sa | 2E6．670 | 274．670 | 244．60 | 2＜1．Eri | 21：1－0 | ご1．すご | 210.580 | こ 110.420 | 211.170 |
| 1＊F Fu | c．te． 6 ¢0 | 284.670 | 254.850 | 2こ1，©示 | 2c5，170 | ご，ヨご号 | ここ0．6\％ 0 | 200.420 | 220.170 |
| $1905 \%$ | 306.670 | $2 \div 4.670$ | 264，E70 | 241，670 | $23 心 170$ | 231.320 | 230．60 | 250.42 u | 250．170 |
| COO F Sid | 316.670 | 304．670 | 274．670 | 251．670 | 245.170 | 241.720 | 240.670 | $340.4 \mathrm{c}^{\circ}$ | 240.170 |
| $\geq 10$ FSM | ごさら，670 | 314．670 | 2\％4．67 | 261．6ア0 | 25.5190 | 251， 920 | 250，6\％0 | 230．420 | 250．170 |
| $\therefore 0 \mathrm{FSH}$ | 336．670 | 324.670 | 274，670 | 2゙1， 60 | 2¢5．1－0 | 2－1．920 | ごg．E\％ | 7r0．409 | 260.170 |
| $236 F=1 i$ | 34E， 670 | 334.670 | 304，合行 | 281，\％\％ | ご或，170 | 2\％1． 200 | 二＇G，6－ | こro．4ric | $こ \because 6.170$ |
| $z+0$ FSb | 3E6．650 | 344.670 | 314.670 | 231.67 | 2SE， 170 | こS1．320 | 280,670 | $\therefore \therefore 0.400$ | $=20.170$ |
| 二上0 FSM | 366.670 | 354.670 | $3 ¢ 4$ 670 | 301.600 | 295，170 | 2＇51．920 | 2 F 0.6 ¢ | － $01.42 \%$ | －91． 170 |
| टebl F5d | 376.670 | 364.670 | 354．670 | 311.670 | 305，170 | 301.920 | S00，670 | 3100.420 | ご10．170 |
| ごO FSH | 386.670 | 374.670 | 344.690 | 321.60 | 315， 170 | 311．720 | F10．Eア0 | 510.420 | 310.170 |
| SEC FE， | 356．670 | 364．670 | 354．6宁0 | 3ड1．¢00 | 3こら，170 | $3: 1.920$ |  | $\overline{5 c o .4 c} 0$ | $3<0.970$ |
| 二 +0 F S 4 | 406.670 | 344．670 | 3「4．6\％0 | 341，E\％0 | 335， 170 | 331.920 |  | 3.30 .420 | 350．170 |
| ज0n FE， | 416.670 | 404．670 | 3¢4． 5 ¢0 | 351．6：0 | 二45．170 | 341．920 | こ40．5゙0 | ご10．420 | 340.170 |

## ELOOR FOFAHETEFS

〔FFESSURE IH FSU； $3 \Xi$ FSU ATA）


| rovor | 2.39 | 2.39 |
| :--- | ---: | ---: |
| Fing | 1.87 | 1.87 |
| FEDVF | 36.00 | 36.00 |

TAELE OF MAXTMIM FEF：ATSEIETE TISSIF TEHETINE
©VVALES－MITFGGE！

## TISEUF HALF－TIUES

| IEFFTH |  | 5 MJH | 10 MIH | 20 MIit | 40 MIH | E0 MIN | 120 MIH | 160 MIt | EO0 Mİd | 240 MIH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ． 40 SEF | ． 50 SOF： | 55 SOF | ． 96 S［FF | Sts SDF | 72 S0F | ． 60 SDF | ． 45 SOF | ． 40 SCF |
| 10 | Fsbu | 126．670 | 114.670 | 77.000 | 61.170 | 54.800 | 51.920 | 50.670 | 50.420 | 50.170 |
| 20 | FSW | 136.670 | 124.670 | 87.000 | 71.170 | 64.300 | 61.520 | 60.670 | 60.400 | E0．170 |
| 34 |  | 146．670 | 134.670 | 97.000 | 81.170 | 74．800 | 71.920 | 74.670 | 70.420 | 70，170 |
| 40 | Fこい | 156，670 | 144．670 | 107.000 | 91.170 | 84.800 | 81.720 | 80.670 | 80.400 | 80.170 |
| 511 | FSW | 166．6す） | 154．670 | 117.000 | 101.150 | 94.800 | 51.920 | 90.670 | $\bigcirc 0.420$ | 90，170 |
| ¢ | $F=1$ | 176，67 | 164．670 | 127．000 | 111．170 | 104．800 | 101，Э゙¢ | fing 6\％ | 100.420 | 100.90 |
| 70 | $F=W$ | $16 ¢, 67 \overline{0}$ | 174.670 | 137．000 | 121.170 | 114.800 | 111．920 | 110.670 | 110.420 | 110.170 |
| \％ 0 | $F \leq W$ | 196，670 | 184．670 | 147.000 | 131.170 | 124， 800 | 121.920 | 120.670 | 120.420 | 120．170 |
| 70 | Fsh | 206.670 | 194．670 | 157．000 | 141.170 | 134．800 | 131.920 | 130，670 | 130．420 | 130， 170 |
| 100 | FSn | 216．670 | 204．670 | 167．000 | 151.170 | 144．800 | 141.920 | 140．670 | 140.420 | 140．170 |
| 118 | FSk | 2¢6．670 | 214.670 | 17\％．000 | 161，170 | 154.800 | 151．320 | 150，670 | 150.420 | 150．1．0 |
| 120 | $F \cdot 1$ | 2すか．ETG | 224.670 | 187．000 | 171．170 | 164．360 | 161，Эこす | 160.680 | 164，420 | 1E！．1安 |
| 130 | FSb1 | 246．670 | 234.670 | 197．000 | 181.170 | 174．960 | 171．920 | 170．6\％0 | $1 \overline{10.420 ~}$ | 1Fi． 1 守 |
| 140 | FSw | 256.670 | 244．670 | 207.000 | 191．170 | 184.800 | 181.920 | 180.650 | 180．420 | 180．170 |
| 150 | FSu | ć66．670 | 254.670 | 217． 100 | 201.170 | 174．800 | 191.920 | 190.670 | 140．420 | 190.170 |
| 160 | $F: 50$ | 2゙6．670 | 264．670 | 227．000 | 211.170 | 204.800 | 201.920 | 200.670 | 200，4 20 | 200.170 |
| 170 | FS ${ }^{\text {S }}$ | 296.670 | 274．570 | 23\％．00\％ | 221.170 | 214.800 | 211.920 | 210.670 | 210.450 | 210.170 |
| 130 | F5d | 2゙5．670 | 284．570 | 247．004 | 231.170 | 224.800 | 221， 290 | 2¢0，670 | 260,420 | 220.170 |
| 190 | FSW | 366.670 | 294．670 | 257．000 | 241．170 | 234． 80 | 231.920 | 230.650 | 230.480 | 230.170 |
| 200 | $F S t$ | 316.670 | 304,670 |  | 251.170 | 244． 300 | 241.920 | 240.670 | 240.480 | 240.170 |
| く10 | FS $\mathrm{F}^{1}$ | 326.670 | 314.670 | 2す\％，000 | 261.170 | 2心4．800 | ご1． 520 | 250，670 | 2二u． 420 | 2．50．17 |
| こと0 | F5U1 | 336.670 | 324.670 | 287．000 | 271．170 | 264.800 | こも1．F20 | 260．6．50 | 2t．0．420 | 250．170 |
| 236 | $F: \%$ | 346.670 | 334.670 | $2 \% 6.000$ | 231．170 | 274．300 | 271.320 | 270.670 | 2；0，42！ | 2 20．170 |
| 2＋4 | F5n | 3Et，670 | 344．670 | 307．000 | 291.170 | 254，\％1： | 281．920 | 280，670 | 200．42！ | 2こ日，170 |
| ごい | FSul | उEE． 670 | 354，670 | $31 \% .000$ | 301.170 | ご4．300 | 291.320 | 290.670 | $2 \div 0.420$ | 290.170 |
| 2¢0 | FS！ | З今E，670 | 364，670 | 327．000 | 311.170 | 304.300 | 301.920 | 300.670 | 360.420 | 300.170 |
| こ？ | FSu | 386．670 | 374．670 | 337.000 | 321.170 | 514．800 | 311.920 | 510．670 | $310.4 \overrightarrow{20}$ | 310.170 |
| ב：$\because 0$ | FSW | 3.46 .670 | 364.670 | 34\％．0n0 | 331.170 | 玉こ4．800 | 321．320 | 320.670 | 320.420 | 320.170 |
| $\because+0$ | FSH | 406.670 | 354.670 | 357， 900 | 341.170 | 354,300 | 331.920 | 350，670 | 350.420 | 330.170 |
| a！ | F $=1.1$ | 416.670 | 414.670 | 367.000 | 351.170 | 344.500 | 341.920 | 540．670 | 340.420 | 340.170 |

BLOOC FMFGMETEFE
〔PFESSUPE IN FSU； 3 I FSG MTA）


|  |
| :---: |
| ゆ1． |
| FE1． |


| 2.39 | 2.39 |
| ---: | ---: |
| 1.87 | 1.87 |
| 36.00 | 36.00 |

2.37
1.57
29.00

| 2.39 | 2.39 |
| ---: | ---: |
| 1.67 | 1.27 |
| 19.00 | 10.00 |

2.39
1.57
7.00
$\therefore .39$
1.50
600
2.30
$1.8 i$
7.00
2.39
1.37
7.00

『しL $\because$ ？
©FSIN：

## TISEUE HOLF－TIMES



ELGMIT FAEAMFTEFSS
$\because$ FFESSHFE IH：FSH： 3 ：FSH TTA：


| rus | 2.37 | 2.37 | 2．3． | E．3F | 2.37 | 2．ぶ可 | こ．54 | 37 | $\therefore 77$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $F \cdot \mathrm{CB}$ | 1.87 | 1．87 | 1． | 1．8； | $1 . \mathrm{Br}$ | 1.8 | 1． 2.8 | 87 | －． 3. | － 20. |
| Frojp | 36.110 | 36．00 | 25.00 | 19.00 | 10.00 | 7 ． 10 | 7．in | －． 10 | －，in | F |

TARLE GF MBYDMUM FEFMISGIELE TIE日E TEHSIGtS
GVALSS－HITFMGEH
TISSUE HGLF－TIMES

| EFTH | 5 MIH | 10 MIN | 20 MIN | 40 MIH | EUMIN | $1 E 0$ MIN | 160 MIN | ごすOMN | 24011 H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ． 40 SiF． | ． 50 SUR | ，5E SLF | ． 9050 | ． 9 E Sof | ． i ECF | ． 60 SLR | 45 SO | 40 56 |
| 10 FSW | 126．650 | 114.670 | 77.0000 | 61.510 | 54.800 | 51.700 | 50.670 | 50.420 | 50.170 |
| 20 FEW | 136.670 | 124.670 | 87.000 | 71.510 | 64.809 | 61.700 | 60.670 | 60.420 | E1）． 170 |
| 30 FSN | 146.670 | 134.670 | 97．000 | 81.510 | 74.800 | 71.700. | 70.670 | 70.420 | 710.170 |
| 411 Fsid | 156.670 | 144.670 | 118.000 | 91.510 | 84.80 | 31.700 | 80.670 | E6，420 | Bij 170 |
| 50 FSO | 166．670 | 154.670 | 117．000 | 101.510 | 94.800 | 91.700 | 90.670 | 50.420 | 90.170 |
| ¢4 FSW | 176.670 | 164.670 | 127．000 | 111.510 | 104，800 | 101.700 | 100.680 | 100.450 | 100.170 |
| $76 F E W$ | 166.650 | 174.670 | 13\％．000 | 121.510 | 114.800 | 111.700 | 110.650 | 110.420 | 110.170 |
| 99 Fsh | 176670 | 184．670 | 147．000 | 131.510 | 124.800 | 121.700 | 120．670 | 120．470 | 120．170 |
| 90 FSh | 206.670 | 194.670 | 157．000 | 141.510 | 134．800 | 131.700 | 130.650 | 130.420 | 130.170 |
| 100 Fsid | 216.670 | 204.670 | 167.000 | 151.510 | 144.800 | 141.700 | 140.670 | 140140 | 149.170 |
| 110 FSW | 226．670 | 214.670 | 17\％．000 | 161．510 | 154．800 | 151.700 | 150.670 | 150．4E0 | 156， 170 |
| 120 FSt | 236．670 | 224．670 | 185．000 | $1 \overline{16} 510$ | 164.800 | 161．700 | 160.670 | 160.420 | 160．170 |
| 190 FSW | 246．670 | 234．670 | 197.000 | 1ה1．510 | 174.800 | 171．700 | 170．6ア0 | 170.420 | 176．170 |
| 14 F 54 | 256.670 | 244.670 | 207.000 | 191．510 | 184.800 | 181.700 | 180.670 | 180.420 | 180.170 |
| 150 FSH | 265.670 | 254．670 | 217.000 | 201.510 | 194.800 | 191.700 | 190.670 | 190.420 | 190．170 |
| 150 FSU | 276.670 | 204.670 | 225．000 | 211.514 | 204.800 | 201.700 | 2010．ET0 | 200.420 | 200．170 |
| 1？0 FSH | 286．670 | 274.670 | 257.000 | 221.510 | 214.800 | 211.700 | 210.670 | 210.420 | 210.170 |
| 150 F | 276.670 | 284．670 | 247．000 | 231.510 | 224．300 | 221.700 | 220.670 | 220.420 | 220．170 |
| 170 FSW | 306.670 | 294.670 | 25．7．000 | 241．510 | 234.300 | 231.700 | 230.670 | 230．420 | E30．170 |
| 2（1）FSW | 316.670 | 304.670 | 26．7．00\％ | 251．510 | 244．800 | 241.700 | 240.670 | 240.420 | 2＋0，170 |
| C10 FSW | 326.670 | 314.670 | 275．000 | 2E1．510 | 254，800 | 251．700 | 250．630 | 250.420 | 250．170 |
| zeO FSW | 35\％．6：0 | 324．670 | 2\％7．000 | － 21.510 | 264800 | 261．700 | 260．ET0 | $2 \mathrm{Es0.420}$ | 200．170 |
| $\therefore 34$ F5u | $3+6.670$ | 354.670 | 237.000 | 281.510 | 274．800 | 271.700 | 270.670 | 270.420 | $270.1 \% 0$ |
| 240 FSu | 356.670 | 344.670 | 30.7000 | 291.510 | 284． 900 | 281.700 | 280.670 | 280.420 | 2E®．170 |
| 250 FSW | 366.670 | 354．670 | 317.000 | 301.510 | 294．800 | 291.700 | 290.670 | 290.420 | $2 \because 0,170$ |
| 260 FSU | 376.670 | 364.670 | 325．000 | 311.510 | 304.800 | 301.700 | 300.670 | 300.420 | 300.170 |
| \％0 FSM | 366．670 | 354.650 | 327．000 | 321.510 | 514.800 | 311.700 | 310.670 | 310.420 | 310.170 |
| 20\％F\％ | 356.670 | 384.670 | 347.000 | 331.510 | 3¢4．800 | 321.700 | 320.670 | 3＜0．420 | 320.170 |
| वat FSu | 416.670 | 354．670 | 357.400 | 341.510 | 334.800 | 331.700 | 330.670 | $350.42 \pi$ | 390.170 |
| Sun FSH | 416.650 | 404．650 | 367.000 | 351.510 | 344.800 | 341.700 | 340.670 | 340.420 | 340.170 |

ELDND FAFAMETERS
〔FFESGURE IN FSU； $3 \mathbf{3}$ FSH RTA：

| $\begin{gathered} \text { FOTO2 } \\ 1.86 \end{gathered}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.39 | 2．34 | 2.39 | 2．33 | 2.39 | 2.39 | 2.39 | くVOL \％ |
| 1.67 | 1.87 | 1.87 | 1.87 | 1．87 | 1.87 | 1.87 | （FSW） |
| 29.00 | 13.00 | 10.00 | 7.00 | －． 00 | 7.00 | 7． 00 | （FSid） |



## 

T15SUF HOLH－T1UES

| $\because$ CFIM | EMIH | 10 MIN | $20 \mathrm{MLi4}$ | 40 MIt | －11 Mri | 120 c 1 lt | 160 PMIti | 209 MIP | 2411．M |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 it | ，E9 Suk | Eこ ーL゙ | ． $5.51+$ | St $\because \mathrm{CH}$ | ．frestm | ＋！－ | ． $4 \%$ \％¢ | 4 CL |
|  |  |  |  | E1511 | －1 | 51 － |  | c－－－－ |  |
| $11 \%$ 号 | 185．670 | 114.6 | $\vec{\square}$ | 61.511 | E4， 4 ¢ 4 | 51.70 | 50.670 | 56.480 | E0．170 |
| －1 F F | 17大．6可 | 124．6．0 | E\％Mity | 71.514 | E4．Etin | ¢ 1.70 | 6日，穴0 | E11．4 4 | 6it 170 |
| F：F\％\％ | 145．670 | 134．670 | 95.604 | 81．510 | 74.600 | 71.700 | －0．6－0 | 「0）4ご1 | （i） 170 |
| 4 F \％i | $15 \in 670$ | 144．670 | 167．000 | 91.510 | 8.4 S． 80 | उ1． | 80.670 | E0． 4 ¢ | E19．170 |
| Eif F－ | 186，6－4 | 154．E゙吅 | 117，新 | 101.511 | E．4 En | $\rightarrow 1.800$ | \＃景穴品 | $\cdots 4 \dot{4}$ | \％11．170 |
| －F F U | 170．670 | 164．ETO | 127．000 | 111.516 | 101．864 | 10i，$\quad$ ¢ 60 | 100．5\％0 | 1104こ0 | 110．170 |
| $\cdots$－F F ！！ | 16 E ． 60 | 174．670 | 137，प\％ | 181．51i | 114．804 | 111.70 |  |  | 119.170 |
| ai $F=t$ | 198． 60 | 134．6すu | 147，प6 | 151．51 | 1ご，Sun | 12.700 | 1くず大す！ | 10420 | 1：1，170 |
| $\rightarrow$（1）F $\because 1.1$ | $\therefore 60.670$ | 134．ロ゙0 | 157．006 | 141．519 | 134．3014 | 151．$\overline{8} 00$ |  | 159．42u | 15is， 17 |
| ！！id F\％n | こ1F．6\％ 0 | co4．E70 | 16F．009 | 151．51和 | 144．504 | 1＋1． 710 | $140 \div 0$ | 141140 | 1415，175 |
| ：！！F－， |  | こ14 它吕 | 18：9019 | 181．Et | 1 5.4 .514 | $9 \square 1.70$ | 150 | 15114 | 1－11，1－0 |
| ！－F Eni | こうさ．00 | こご，ご㑑 | 12\％．000 | 1－1．5il | 164． 500 | 1－1． 500 | ！¢ E ¢ ¢ | 180.40 | 1－8．176 |
| i $=$ a F － H | 己車里， 0 | $2 こ 4.570$ | $1 \%$ ， | 181，510 | 174： 819 | 171． | 1F日，号保 | 150，4 20 | 1：0．170 |
| ：40 FE114 | 256．6F0 | 244．850 | $\overline{207}$ ，000 | 1－91．$\square_{1} 10$ | 134．30！ | 151． F | 1：0，－－ | 180，4家苟 | 150.170 |
| 156 F5日 | 258，670 | 25－1．670 | ご？以！！ | E01．5i！ | 174． 50 | 171.70 |  | 1－0．400 | 176．1ヶ¢ |
| 15：F Sa： | 27e，6？ | 254．670 |  | 211，上！！ | coly 00 | 201.700 | こ00，ジ， | $\therefore$ ¢0，4 $=0$ | 200.170 |
|  |  | ごれ ¢゙す |  | $\because 1=11$ | $\therefore 14.8 \cdots 11$ | E11．ru！ | ご！－¢！ | $\therefore 10.420$ | こ11190 |
| 1－，F－1．i | 235670 | 264．670 | $24 \% .000$ | 2 z 21．5 | 204 － 217 | $\because 21.500$ | ことら，6－ | $\therefore=0.420$ | $=00.170$ |
| $1 \rightarrow F=1.1$ | 30reoio | 2F4．670 | 25\％．000 | 241．514 | $\because: 4.301$ | －31．700 | 250．6行 | $\therefore 30.40$ | 234． 9 ¢ |
|  | 319670 | \＃i4．6\％0 | 2－r，0nio | －1．510 | 244， 50 | $2+1.700$ | こ4n． 5 ¢ | $\therefore$＋19，4\％ | $2+i, 17 i$ |
| $\therefore 1: F S \pi$ | 326．670 | 314.650 | 27\％．000 | 261．510 | －54．300 | 251．r00 | 550．6－0 | $\therefore 50400$ | 玉59．170 |
| －if F\％H |  | ご乐里： | こと，0¢ | 二1． 51 it | Sed Sin | 如1． Cu | $\therefore$ ¢0． 0 或 | こrit 4 ¢ | crat 17 |
| －iFF」， | す山ictor | 374．6：0 |  | 2\％，¢10 |  | $=71.760$ | ごす。大ア0 | ごい，100 | こっ1．1号 |
|  | 356．6F0 | 344．580 | 307.006 | 29.51 ¢ | －84． 00 | 玉 1．-70 | 2siociou | $\therefore 517401$ | 2：$=1$－ |
| $\therefore \mathrm{F}$ 相 | 的を，6\％0 | 354，Eiv | こ！ 7 ， 010 | 301.510 | ぐ4． 500 | 2 F 1.740 | 290.65 | 2כ0，420 | 230170 |
|  | アデのだ！ | 364．5斤0 | こご，び四 | 511.510 | 304， 500 | 301.700 | 300,680 | 300.420 | T01，170 |
| ¢，F Fsll | ころ4． 0 | 374.870 | 3ア\％．00！ | 3\％1．E14 | 314.808 | 311,700 | 319.6 － 0 | －19．420 | 510.150 |
| $\therefore 0 \mathrm{~F} 51$ ！ | $T$ TE，A O |  | 34. ，6\％ | 33． 314 |  | 3c1． 50 | 云它如安 | F－0．4\％ | 3－1，－－ |
| －－$\quad F=1.4$ | 416.6 | $334.6 \% 0$ |  | 741．5io | 334．$\overline{6} 010$ | 321．700 |  | 30，4\％0 | 320，1－0 |
| $\therefore$ ？ 5 F．i | 4 4＊6－0 | 47960 | すer． 0 Ono | 351.510 | 544． 800 | 241．700 | 4 4 ¢ ¢ 0 | 7．40．426 | 3.10 .150 |
| ．．．．．．－ | －－ | －－－－ | －－－－－－－ | $------$ |  |  |  |  | －－－－－－－ |

El InTM FNEAMETEFS
$\therefore$ FFEGGMFE IM FSi：？S FSi，ATA；

1．70 2．0！－1：

| Curaz | － 5.5 | 2.54 | 2.74 | c． $\mathrm{c}_{\text {a }}$ | 2． 3.9 | 2．53 | $\therefore 3$ | 2.33 | 2.37 | ¢ ¢ ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frab | 1.87 | 1.97 | 1．61 | 1．8． | 1．8i | 1． Fr | 1．8： | 1.57 | 1．70 | －F5， |
| FFrom | 36．00 | 3e．no | 29， 90 | 130 | 10.911 | B．${ }^{\text {a }}$ | － 00 | 7.90 | －． 14 | FSt |

## APPENDIX E

DIVE PROFILE COMPARISONS

TABLE E-1
Dive Profile Comparison: Air Decompression Bounce

| Profiles FSW/Min | VVAL | $\begin{array}{r} \text { STOPS (FSW) } \\ 20 \\ \hline \end{array}$ | 10 | Total Decomp. Time (min:sec) |
| :---: | :---: | :---: | :---: | :---: |
| Profile \#1 | Std Air | 9 | 47 | 47:50 |
|  | 18 |  | 229 | 238:50 |
|  | 22 |  | 135 | 135:50 |
| 50/240 | 25 |  | 97 | 97:50 |
|  | 26 |  | 135 | 135:50 |
|  | 28* |  | 158 | 158:50 |
|  | 50 | 1 | 157 | 158:50 |
|  | 52 | 1 | 194 | 195:50 |
|  | 53 | 1 | 183 | 184:50 |
|  | 54 | 1 | 183 | 184:50 |
|  | 55 | 3 | 181 | 184:50 |
|  | 56 | 3 | 181 | 184:50 |
|  | 58 | 3 | 181 | 184:50 |
|  | 59 | 3 | 186 | 189:50 |
| Profile \#3 | Std Air* |  | 14 | 15:00 |
|  | 18 |  | 69 | 70:00 |
|  | 22 |  | 38 | 39:00 |
| 60/100 | 25 |  | 28 | 29:00 |
|  | 26 |  | 22 | 23:00 |
|  | 28* |  | 22 | 23:00 |
|  | 50 |  | 23 | 24:00 |
|  | 52 |  | 24 | 25:00 |
|  | 53 |  | 31 | 32:00 |
|  | 54 |  | 28 | 29:00 |
|  | 55 |  | 27 | 28:00 |
|  | 56 |  | 27 | 28:00 |
|  | 58 |  | 30 | 31:00 |
|  | 59 |  | 31 | 32:00 |
| Profile | Std Air |  | 26 | 27:00 |
|  | 18 |  | 123 | 124:00 |
|  | 22 |  | 67 | 68:00 |
| 60/120 | 25 |  | 48 | 49:00 |
|  | 26 |  | 48 | 49:00 |
|  | 28* |  | 56 | 57:00 |
|  | 50 |  | 59 | 60:00 |
|  | 52 |  | 71 | 72:00 |
|  | 53 | 2 | 49 | 52:00 |
|  | 54 | 2 | 49 | 52:00 |
|  | 55 | 2 | 51 | 54:00 |
|  | 56 |  | 54 | 55:00 |
|  | 58 | 2 | 57 | 56:00 |
|  | 59 | 2 | 56 | 59:00 |
|  |  |  |  | (Continued) |




MICROCOPY RESOLUTION TEST CHART
national bureau of standaros-1963-A

TABLE E-1 (Continued)
Dive Profile Comparison: Air Decompression Bounce

| Profiles FSW/Min | VVAL | $\begin{array}{r} \hline \text { STOPS (FSW) } \\ 30 \\ \hline \end{array}$ | 20 | 10 | Total Decomp. Time (min:sec) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Profile \#5 | Std Air |  |  | 56 | 57:00 |
|  | (60/200)* |  | 1 | 69 | 71:00 |
|  | 18 |  | 48 | 205 | 254:00 |
|  | 22* |  | 28 | 124 | 153:00 |
|  | 25* |  | 20 | 90 | 111:00 |
| 60/180 | 26 |  | 20 | 132 | 153:00 |
|  | 28 |  | 20 | 155 | 176:00 |
|  | 50 |  | 21 | 154 | 176:00 |
|  | 52 |  | 21 | 191 | 213:00 |
|  | 53 |  | 21 | 170 | 192:00 |
|  | 54 |  | 21 | 170 | 192:00 |
|  | 55 |  | 24 | 168 | 193:00 |
|  | 56 |  | 24 | 172 | 197:00 |
|  | 58 |  | 24 | 172 | 197:00 |
|  | 59 |  | 24 | 183 | 208:00 |
| Profile $\# 6$ | Std Air |  | 17 | 56 | 74:20 |
|  | 18 | 21 | 69 | 184 | 275:20 |
|  | 22 | 14 | 49 | 112 | 176:20 |
| 80/120 | 25 | 10 | 36 | 80 | 127:20 |
|  | 26 | 7 | 37 | 127 | 172:20 |
|  | 28 | 7 | 37 | 149 | 194:20 |
|  | 50 | 3 | 36 | 150 | 195:20 |
|  | 52 | 8 | 38 | 186 | 233:20 |
|  | 53* | 13 | 34 | 166 | 214:20 |
|  | 54* | 14 | 32 | 168 | 215:20 |
|  | 55 | 11 | 38 | 163 | 213:20 |
|  | 56 | 8 | 41 | 166 | 216:20 |
|  | 58 | 13 | 36 | 168 | 218:20 |
|  | 59 | 14 | 35 | 182 | 232:20 |
| Profile \#8 | Std Air* |  | 9 | 28 | 38:40 |
|  | (100/70)* |  | 17 | 39 | 57:40 |
|  | 18 |  | 64 | 93 | 158:40 |
|  | 22* |  | 43 | 56 | 100:40 |
| 100/60 | 25* |  | 31 | 40 | 72:40 |
|  | 26 |  | 23 | 35 | 59:40 |
|  | 28 |  | 23 | 35 | 59:40 |
|  | 50 |  | 23 | 38 | 62:40 |
|  | 52 |  | 25 | 43 | 69:40 |
|  | 53 |  | 34 | 38 | 73:40 |
|  | 54 |  | 32 | 34 | 67:40 |
|  | 55 | 4 | 20 | 42 | 67:40 |
|  | 56 | 4 | 17 | 45 | 67:40 |
|  | 58 | 4 | 28 | 36 | 69:40 |
|  | 59 | 4 | 30 | 39 | 74:40 |

[^4](Continued)

TABLE E-1 (Continued)
Dive Profile Comparison: Air Decompression Bounce

| Profiles FSW/Min | VVAL | $\begin{gathered} \text { STOPS (F } \\ 40 \\ \hline \end{gathered}$ |  | 20 | 10 | Total Decomp. <br> Time (min:sec) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Profile \#9 100/90 | Std Air |  | 3 | 23 | 57 | 84:40 |
|  | 18 | 3 | 55 | 70 | 155 | 284:40 |
|  | 22 | 1 | 44 | 49 | 105 | 200:40 |
|  | 25 | 1 | 31 | 35 | 76 | 144:40 |
|  | 26 | 1 | 23 | 33 | 128 | 186:40 |
|  | 28* | 1 | 23 | 33 | 151 | 209:40 |
|  | 50 | 1 | 22 | 34 | 150 | 208:40 |
|  | 52 | 1 | 25 | 33 | 188 | 248:40 |
|  | 53 | 4 | 30 | 34 | 163 | 232:40 |
|  | 54 | 4 | 30 | 32 | 165 | 232:40 |
|  | 55 | 4 | 21 | 38 | 164 | 228:40 |
|  | 56 | 1 | 22 | 39 | 167 | 230:40 |
|  | 58 | 4 | 30 | 32 | 170 | 237:40 |
|  | 59 | 4 | 32 | 34 | 179 | 250:40 |
| Profile \#11 | Std Air |  | 2 | 22 | 45 | 71:00 |
|  | (120/70)* |  | 9 | 23 | 55 | 89:00 |
|  | 18 |  | 52 | 69 | 92 | 215:00 |
|  | 22 |  | 39 | 49 | 63 | 153:00 |
| 120/60 | 25 |  | 28 | 35 | 46 | 111:00 |
|  | 26 |  | 21 | 26 | 76 | 125:00 |
|  | 28* |  | 21 | 26 | 98 | 147:00 |
|  | 50 |  | 20 | 26 | 100 | 148:00 |
|  | 52 |  | 23 | 27 | 121 | 173:00 |
|  | 53 |  | 31 | 33 | 93 | 159:00 |
|  | 54 |  | 30 | 32 | 94 | 158:00 |
|  | 55 | 8 | 15 | 23 | 109 | 157:00 |
|  | 56 | 8 | 14 | 21 | 116 | 161:00 |
|  | 58 | 8 | 21 | 33 | 103 | 167:00 |
|  | 59 | 8 | 23 | 34 | 110 | 177:00 |
| Profile \#12 | Std Air |  | 9 | 23 | 55 | 89:00 |
|  | 18 | 22 | 55 | 69 | 141 | 289:00 |
|  | 22 | 17 | 44 | 49 | 99 | 211:00 |
| 120/70 | 25 | 12 | 32 | 35 | 71 | 152:00 |
|  | 26 | 9 | 23 | 30 | 124 | 188:00 |
|  | 28* | 9 | 23 | 30 | 147 | 211:00 |
|  | 50 | 9 | 23 | 30 | 147 | 211:00 |
|  | 52 | 10 | 26 | 29 | 183 | 250:00 |
|  | 53 | 15 | 30 | 34 | 154 | 235:00 |
|  | 54 | 16 | 30 | 32 | 156 | 236:00 |
|  | 55 | 13 | 21 | 35 | 158 | 229:00 |
|  | 56 | 13 | 18 | 37 | 162 | 232:00 |
|  | 58 | 15 | 29 | 33 | 160 | 239:00 |
|  | 59 | 16 | 31 | 34 | 170 | 253:00 |

(Continued)
*Profiles Actually Tested.

TABLE E-1 (Continued)
Dive Profile Comparison: Air Decompression Bounce

| Profiles FSW/Min | VVAL | STOPS (FSW) |  |  |  |  | Total Decomp. Time (min: sec) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Profile 非13 | Std Air |  |  | 15 | 27 | 63 | 107:00 |
|  | 18 |  | 42 | 56 | 69 | 196 | 365:00 |
|  | 22 |  | 35 | 43 | 50 | 135 | 265:00 |
| 120/80 | 25 |  | 25 | 31 | 36 | 97 | 191:00 |
|  | 26 |  | 18 | 24 | 47 | 155 | 246:00 |
|  | 28* |  | 18 | 24 | 51 | 170 | 265:00 |
|  | 50 |  | 18 | 23 | 53 | 169 | 265:00 |
|  | 52 |  | 21 | 25 | 60 | 208 | 316:00 |
|  | 53 |  | 27 | 31 | 37 | 223 | 320:00 |
|  | 54 |  | 28 | 30 | 37 | 223 | 320:00 |
|  | 55 | 3 | 18 | 22 | 54 | 210 | 309:00 |
|  | 56 | 3 | 15 | 22 | 56 | 106 | 304:00 |
|  | 58 | 3 | 24 | 29 | 44 | 219 | 321:00 |
|  | 59 | 3 | 26 | 31 | 46 | 220 | 328:00 |
| Profile \#15 | Std Air |  |  | 5 | 19 | 33 | 59:30 |
|  | 18 |  | 9 | 28 | 69 | 93 | 201:30 |
|  | 22 |  | 7 | 22 | 48 | 56 | 135:30 |
| 150/40 | 25 |  | 5 | 15 | 36 | 40 | 98:30 |
|  | 26* |  | 3 | 12 | 26 | 42 | 85:30 |
|  | 28* |  | 3 | 12 | 26 | 53 | 96:30 |
|  | 50 |  | 3 | 12 | 26 | 57 | 100:30 |
|  | 52 |  | 4 | 13 | 27 | 68 | 114:30 |
|  | 53 |  | 4 | 19 | 34 | 42 | 101:30 |
|  | 54 |  | 4 | 21 | 32 | 43 | 102:30 |
|  | 55 | 2 | 13 | 14 | 15 | 65 | 111:30 |
|  | 56 | 2 | 13 | 14 | 14 | 70 | 115:30 |
|  | 58 | 2 | 13 | 14 | 25 | 62 | 118:30 |
|  | 59 | 2 | 13 | 14 | 29 | 64 | 124:30 |
| Profile \#16 | Std Air |  | 3 | 19 | 26 | 62 | 112:30 |
|  | 18 | 18 | 45 | 55 | 70 | 196 | 383:30 |
|  | 22* | 16 | 38 | 43 | 50 | 134 | 283:30 |
| 150/60 | 25 | 11 | 28 | 31 | 35 | 97 | 204:30 |
|  | 26 | 8 | 20 | 24 | 46 | 152 | 252:30 |
|  | 28 | 8 | 20 | 24 | 48 | 171 | 273:30 |
|  | 50 | 8 | 20 | 23 | 50 | 168 | 271:30 |
|  | 52 | 9 | 23 | 26 | 57 | 207 | 324:30 |
|  | 53 | 13 | 28 | 30 | 37 | 224 | 334:30 |
|  | 54 | 15 | 28 | 30 | 37 | 226 | 338:30 |
|  | 55 | 813 | 13 | 20 | 59 | 217 | 332:30 |
|  | 56 | 813 | 13 | 17 | 62 | 215 | 330:30 |
|  | 58 | 813 | 18 | 30 | 50 | 224 | 345:30 |
|  | 59 | $8 \quad 13$ | 21 | 31 | 53 | 222 | 350:30 |

(Continued)

TABLE E-1 (Continued)
Diwe Profile Comparison: Air Decompression Bounce

| $\begin{aligned} & \text { Profiles } \\ & \text { FSW/Min } \end{aligned}$ | VVAL | STOPS (FSW) |  |  |  |  |  |  | Total Decomp. Time (minisec) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 70 | 60 | 50 | 40 | 30 | 20 | 10 |  |
| Profile \#18 | Std Air |  |  |  | 1 | d | 19 | 32 | 63:10 |
|  | 18 |  | 3 | 10 | 11 | 26 | 56 | 92 | 201:10 |
|  | 22 |  | 3 | 9 | 9 | 20 | 41 | 57 | 142:10 |
| 190/30 | 25 |  | 2 | 6 | 7 | 14 | 30 | 41 | 103:10 |
|  | 26 |  | 1 | 3 | 5 | 10 | 25 | 43 | $90: 10$ |
|  | 28* |  | 1 | 3 | 5 | 10 | 25 | 52 | 99:10 |
|  | 50 |  |  | 1 | 8 | 10 | 24 | 54 | 100:10 |
|  | 52 |  |  | 1 | 10 | 11 | 25 | 65 | 115:10 |
|  | 53 |  |  | 1 | 10 | 15 | 34 | 39 | 102:10 |
|  | 54 |  |  | 3 | 9 | 19 | 32 | 41 | 107:10 |
|  | 55 |  |  | 11 | 13 | 14 | 14 | 69 | 124:10 |
|  | 56 |  |  | 11 | 13 | 14 | 14 | 73 | 128:10 |
|  | 58 |  |  | 11 | 13 | 14 | 21 | 68 | 130:10 |
|  | 59 |  |  | 11 | 13 | 14 | 25 | 70 | 136:10 |
| Profile \#19 | Std Air |  |  |  | 8 | 14 | 23 | 55 | 103:10 |
|  | 18 | 3 | 8 | 20 | 23 | 50 | 69 | 170 | 346:10 |
|  | 22 | 3 | 8 | 17 | 20 | 40 | 49 | 113 | 253:10 |
| 190/40 | 25 | 2 | 5 | 13 | 14 | 29 | 36 | 77 | 179:10 |
|  | 26* | 1 | 3 | 9 | 11 | 23 | 32 | 125 | 207:10 |
|  | 28* | 1 | 3 | 9 | 11 | 23 | 32 | 147 | 229:10 |
|  | 50 |  | 5 | 8 | 10 | 23 | 32 | 147 | 228:10 |
|  | 52 |  | 6 | 10 | 12 | 25 | 32 | 186 | 274:10 |
|  | 53 |  | 6 | 10 | 19 | 30 | 34 | 160 | 262:10 |
|  | 54 |  | 7 | 11 | 23 | 30 | 32 | 164 | 270:10 |
|  | 55 | 6 | 11 | 13 | 13 | 13 | 48 | 178 | 285:10 |
|  | 56 | 6 | 11 | 13 | 13 | 13 | 48 | 183 | 290:10 |
|  | 58 | 6 | 11 | 13 | 13 | 23 | 38 | 187 | 294:10 |
|  | 59 | 6 | 11 | 13 | 13 | 27 | 35 | 202 | 310:10 |

[^5]TABLE E-2
Dive Profile Comparison: 0.7 ATA $0_{2}-\mathrm{N}_{2}$ Bounce
Constant 0.7 ATA $0_{2}$ in $\mathrm{N}_{2}$

| Profiles FSW/Min | VVAL | STOPS (FSW) |  |  |  |  |  |  | Total Decomp. Time (min:sec) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Profile \#20 | 18 |  |  |  |  | 7 | 28 | 28 | 64:40 |
|  | 29* |  |  |  |  | 3 | 15 | 27 | 46:40 |
|  | 52 |  |  |  |  | 4 | 18 | 27 | 50:40 |
| 100/60 | 58 |  |  |  |  | 7 | 20 | 20 | 48:40 |
|  | 59 |  |  |  |  | 7 | 21 | 22 | 51:40 |
| Profile \#21 | 18 |  |  | 1 | 7 | 8 | 17 | 29 | 64:30 |
|  | 29* |  |  |  | 3 | 4 | 10 | 15 | 34:30 |
|  | 52 |  |  |  | 1 | 8 | 12 | 18 | 41:30 |
| 150/30 | 58 |  |  |  | 9 | 11 | 11 | 16 | 49:30 |
|  | 59 |  |  |  | 9 | 11 | 11 | 19 | 52:30 |
| Profile \#22 | 18 |  |  | 7 | 15 | 19 | 28 | 28 | 99:30 |
|  | 29* |  |  | 3 | 6 | 12 | 15 | 45 | 84:30 |
|  | 52 |  |  | 4 | 8 | 14 | 18 | 48 | 94:30 |
| 150/40 | 58 |  | 3 | 11 | 11 | 11 | 17 | 46 | 101:30 |
|  | 59 |  | 3 | 11 | 11 | 11 | 20 | 48 | 106:30 |
| Profile \#23 | 18 | 4 | 14 | 22 | 28 | 29 | 30 | 75 | 204:30 |
|  | 29* | 1 | 7 | 13 | 15 | 14 | 57 | 100 | 209:30 |
|  | 52 | 2 | 8 | 15 | 18 | 18 | 58 | 111 | 232:30 |
| 150/60 | 58 | 11 | 11 | 11 | 19 | 20 | 55 | 132 | 261:30 |
|  | 59 | 11 | 11 | 11 | 22 | 21 | 58 | 128 | 264:30 |

Air $\rightarrow$ Constant $0.7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$

| Profile \#24 | 18 |  |  |  |  | 38 | 39:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29 |  |  |  |  | 34 | 35:00 |
|  | 52 |  |  |  |  | 37 | 38:00 |
| 60/120 | 58 |  |  |  | 2 | 28 | 31:00 |
|  | 59* |  |  |  | 2 | 30 | 33:00 |
| Profile \#25 | 18 |  | 2 | 28 | 29 | 47 | 107:40 |
|  | 29 |  | 1 | 15 | 20 | 75 | 112:40 |
|  | 52* |  | 1 | 18 | 19 | 83 | 122:40 |
| 100/90 | 58 |  | 4 | 20 | 20 | 73 | 118:40 |
|  | 59 |  | 4 | 22 | 21 | 77 | 125:40 |
| Profile \#26 | 18 |  | 6 | 15 | 28 | 28 | 79:30 |
|  | 29 |  | 3 | 8 | 15 | 26 | 54:30 |
|  | 52* |  | 3 | 10 | 18 | 25 | 58:30 |
| 150/40 | 58 | 2 | 11 | 11 | 14 | 21 | 61:30 |
|  | 59 | 2 | 11 | 11 | 16 | 22 | 64:30 |

[^6]TABLE E-3
Dive Profile Comparison: Air No-Decompression Repets
Body of table shows No-Decompression Time in minutes which includes descent time at $60 \mathrm{FSW} / \mathrm{min}$.


TABLE E－3（Continued）
Dive Profile Comparison：Air No－Decompression Repets
Body of table shows No－Decompression Time in minutes which includes descent time at $60 \mathrm{FSW} / \mathrm{min}$ ．

| $\begin{aligned} & \text { Profiles } \\ & \text { FSW/Min } \end{aligned}$ | VVAL | 1st Excursion TDT非 | 2nd Excursion TDT非 | 3rd Excursion TDT非 |
| :---: | :---: | :---: | :---: | :---: |
| Profile $\# 30$ | Std Air | $\begin{array}{ll} 25 \\ \{30\} @ & 5 \end{array}$ | $\{20\}+[26] \text { - } 28$ | －－－－－－－－－－－－－－－ |
|  | 18 | 29.73 | 5.81 | －－－－－－－－－ |
|  | 22 | 30.78 | 10.84 | －－－－－－－－－ |
| 100／ND | 25 | 30.78 | 14.28 | －－－－－－－－－ |
|  | 26 | 30.78 | 18.30 | －－－－－－－－ |
| $60 \mathrm{Min} \mathrm{S.I}$. | 28 | 30.78 | 18.30 | －－－－－－－－－ |
|  | 50 | 30.49 | 19.02 | －－－－－－－－－ |
| 100／ND | 52＊ | 30.49 | 18.23 | －－－－－－－－－ |
|  | 53 | 29.25 | 14.99 | －－－－－－－－－ |
|  | 54＊ | 29.25 | 15.84 | －－－－－－－－－ |
|  | 55＊ | 26.50 | 20.06 | －－－－－－－－－ |
|  | 56 | 26.50 | 20.15 | －－－－－－－－－－ |
|  | 58 | 26.50 | 17.74 | －－－－－－－－－ |
|  | 59 | 26.50 | 18.06 | －－－－－－－－－ |
| Profile \＃31 | Std Air | 25 | －1 |  |
|  |  | \｛30\}@ 5 | $\{20\}+[26] @ 28$ | $\{19\}+[38]$ ¢ 39 |
|  | 18 | 29.73 | 5.81 | 5.81 |
|  | 22 | 30.78 | 10.84 | 10.84 |
| 100／ND | 25 | 30.78 | 14.28 | 14.28 |
|  | 26 | 30.78 | 18.30 | 18.30 |
| $60 \mathrm{Min} \mathrm{S.I}$. | 28 | 30.78 | 18.30 | 18.30 |
|  | 50 | 30.49 | 19.02 | 18.42 |
| 100／ND | 52 | 30.49 | 18.73 | 15.67 |
|  | 53 | 29.25 | 14.99 | 14.99 |
| 60 Min S．I． | 54 | 29.25 | 15.84 | 15.84 |
|  | 55 | 26.50 | 20.06 | 18.94 |
| 100／ND | 56 | 26.50 | 20.15 | 18.86 |
|  | 58＊ | 26.50 | 17.74 | 15.89 |
|  | 59 | 26.50 | 18.06 | 15.15 |

（Continued）

Dive Profile Comparison: Air No-Decompression Repets
Body of table shows No-Decompression Time in minutes which includes descent time at $60 \mathrm{FSW} / \mathrm{min}$.

| $\begin{aligned} & \text { Profiles } \\ & \text { FSW/Min } \end{aligned}$ | VVAL | 1st Excur | TDT非 | 2nd Excursion | TDT ${ }^{\text {\# }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Profile \#32 | Std Air | $15$ |  | \{14 $\}^{0}+[21]{ }^{\text {a }}$ | 32 |
|  | 18 | 23.34 |  | 4.85 |  |
|  | 22 | 23.92 |  | 8.86 |  |
| 120/ND | 25 | 24.36 |  | 11.18 |  |
|  | 26 | 24.45 |  | 14.29 |  |
| $60 \mathrm{Min} \mathrm{S.I}$. | 28 | 24.45 |  | 14.29 |  |
|  | 50 | 24.24 |  | 14.87 |  |
| 120/ND | 52 | 24.24 |  | 14.65 |  |
|  | 53 | 23.31 |  | 11.72 |  |
|  | 54 | 23.31 |  | 12.39 |  |
|  | 55 | 20.21 |  | 15.04 |  |
|  | 56 | 20.21 |  | 15.04 |  |
|  | 58* | 20.21 |  | 14.63 |  |
|  | 59 | 20.21 |  | 14.14 |  |
| Profile \#33 | Std Air |  |  | \{1\} $+\stackrel{0}{[14] @} 24$ |  |
|  |  | $\{15\}^{\text {e }}$ | 6 |  |  |  |
|  | 18 | 14.58 |  | 6.79 |  |
|  | 22 | 14.79 |  | 7.31 |  |
| 150/ND | 25 | 15.58 |  | 11.04 |  |
|  | 26 | 16.45 |  | 12.66 |  |
| 95 Min S.I. | 28 | 16.45 |  | 12.66 |  |
|  | 50 | 18.09 |  | 11.67 |  |
| 80/ND | 52 | 16.16 |  | 12.58 |  |
|  | $\begin{aligned} & 53 \\ & 54 \end{aligned}$ | 16.16 |  | 10.34 |  |
|  |  | 14.42 |  | 10.96 |  |
|  | 55 | 14.42 |  | 11.23 |  |
|  | 56 | 14.42 |  | 11.23 |  |
|  | 58* | $14.42$ |  | $11.23$ |  |
|  | 59 | $14.42$ |  | 11.23 |  |

[^7]\# Total Decompression Time required by Standard Air Schedule.
\& Times in \{ \} are bottom time, times in [ ] Residual Nitrogen time according to Standard Air Tables (see text).

TABLE E-4
Dive Profile Comparison: Air Decompression Repets


[^8]TABLE E-5
Dive Profile Comparison: Multi-Level Air/Constant 0.7 ATA $\mathrm{PO}_{2}$ in $\mathrm{N}_{2}$

| Profiles FSW/Min | VVAL | STOPS (FSW) |  |  | 10 | Total Decomp. Time (min:sec) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Profile \#37 | Std Air | 80/360 |  |  |  | 280:20 |
|  | 18 |  |  |  | 74 | 75:20 |
| 80/60 (Air) | 28 | Final | Decompression | from | 60 | 61:20 |
| 20/180 (0.7 $\mathrm{PO}_{2}$ ) | 29 |  | 80 FSW |  | 75 | 76:20 |
| 80/50 (Air) | 52 |  | after |  | 76 | 77:20 |
|  | 58 |  | 50 min |  | 60 | 61:20 |
|  | 59* |  |  |  | 68 | 69:20 |
| Profile \#38 | Std Air | 100/360 |  |  |  | 416:40 |
|  | 18 |  |  |  | 11 | 12:00 |
| 80/60 (Air) | 28 | Fina | Decompression | from | 33 | 34:00 |
| 100/120(0.7 P02) | 29 |  | 60 FSW |  | 48 | 49:00 |
| 100/20 (0.7 P02) | 52 |  | after |  | 43 | 43:00 |
| 20/60 (0.7 $\mathrm{PO}_{2}$ ) | 58* |  | 40 min |  | 27 | 27:00 |
| 60/40 (Air) | 59* |  |  |  | 34 | 34:00 |

* Profiles Actually Tested.

Note: No decompression stops were required until arrival at 10 FSW during final ascent to the surface.

## APPENDIX F

AIR DECOMPRESSION TABLES (VVAL59)
Tables in feet with 10 FSW Stop Depth Increment and in meters with 3 MSW Stop Depth Increments

MPTT Tables are included for reference in FSW and MSW.

## 『VHLOG－MITROGEN

TISSUE HMLF－TIMES

| くご「．． | $\begin{array}{r} 5 M I N \\ +950 F \end{array}$ | $\begin{array}{r} 10 \mathrm{MIN} \\ .50 \leqslant 0 R \end{array}$ | $\begin{aligned} & 2 i j 1 t i \\ & E 5 E 0 F \end{aligned}$ | $\begin{aligned} 4015 N \\ 85306 \end{aligned}$ | $\begin{aligned} & 80 \mathrm{MIH} \\ & .7630 \mathrm{~F} \end{aligned}$ | $\begin{aligned} & 129 \mathrm{MIN} \\ & \text { ES } \mathrm{SUF} \end{aligned}$ |  | $\begin{aligned} & \therefore 4 \text { M! } \\ & .4=30 F \end{aligned}$ | $\begin{aligned} & 24910 \\ & .405 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \because \mathrm{FSin}$ | 126．670 | 114．E70 | アテ， 0 ¢！ | $61.5: 0$ | 54.800 | 51.750 | 50.670 | 50．42？ | E9， 170 |
| こ！FSu | 15\％．673 | 124．670 | Er． 100 | 71．519 | 64.300 | 51.700. | 60．ET0 | 60，420 | ¢is， 17 ¢ |
| E\％FEH | 146.670 | 134.670 | 97.000 | 81．510 | 74.800 | 71.700 | 70.670 | 70.420 | －0．170 |
| 4 F F 51 | 156．679 | 144.670 | 105．000 | 91.510 | 84.300 | 81． 7 良 | 80.570 | E0．42！ | B0． 17 |
| Ei FSul | 166．670 | 154.670 | 117．1000 | 101．510 | 94.3010 | 31.700 | 90.670 | 70.420 | 70．176 |
| ¢？FSU | 176．670 | 164．670 | 127．0010 | 111.510 | 104．300 | 101.700 | 103，670 | 110．420 | 1015 |
|  | 136．670 | 174．670 | 1こ7．000 | 121．5：4 | 114．300 | 111.700 | 110，¢\％ | 119.420 | 119817 |
| 3 ¢ F $n$ | 19E，670 | 184.670 | 147.000 | 131.510 | 124.800 | 121．700 | 120．570 | 120.420 | 120．170 |
| $\because \mathrm{F}=\mathrm{M}$ | こ06．670 | 194．670 | 157．000 | 141．51！ | 134．300 | 1．31．700 | $150,6 \%$ | 170.420 | 1 30.15 |
| 140＝3\％ | 218.670 | 204.650 | 167．000 | 151．514 | 144.800 | 141.700 | 140．500 | 14i． 4 2is | 145.170 |
| 119 FSH | 226．570 | 214.670 | 177．000 | 161．510 | 154.300 | 151． F 0 | 150．670 | 150．420 | 150.170 |
| －F Fid | 255，670 | 224．670 | 157.000 | 171，510 | 104． 500 | 161.700 | 180．670 | 1E0，420 | $1 \leq 0.170$ |
| ！こ～FこW | 246．670 | 234．670 | 137．000 | 181．510 | 174.300 | 171.700 |  | 170.420 | 170．170 |
| 1＋ | 256．670 | 244．670 | 207．000 | 191．510 | 184．800 | 181.700 | 180,670 | 180，420 | $18017 \%$ |
| 15 ？F＝ 4 | 2¢6．570 | 254．670 | 217.000 | 201．510 | 194.800 | 191．700 | 150．670 | 150， 420 | 198.170 |
|  | 2テ6．6゙9 | 264，676 | 227．000 | 211．519 | 204.800 | 201.700 | 200.600 | こ00．4こ0 | 293．170 |
| 今心 Fこli | 266．670 | 274．670 | 257．000 | 221． 510 | 214.800 | 211.70 | 210．670 | － 10.450 | E11．170 |
| 1517 F | 278.670 | 284．670 | 247.000 | 231．510 | 224.300 | 221.700 | 220.650 | $\geq 00.450$ | 220．170 |
| 1为 FE？ | 306.670 | 234．670 | 257．000 | 241．510 | 234.800 | 231.700 | 250.670 | $=20 .+20$ | E30．170 |
| 2ia FSil | 316.670 | 304.670 | 267．000 | 251． 510 | 244．300 | 241.700 | 240，67！ | こ40．4こ！ | E40．170 |
| 210 F5in | 326．670 | 314.670 | 277．000 | 2E1．51！ | 254．300 | 251．700 | 250.670 | こE0．4ご1 | －51］．170 |
| 二二口 F 三ri | 35 6.670 | 324．E70 | 267．000 | こ71．510 | $\pm 64.900$ | 2E1．700 | 二E0．ETO |  | E¢0．1F0 |
|  | $34 \div .670$ | 354.670 | 275．000 | 261．510 | ET4．800 | 271．700 | ごロ 0 | ご0 4 $=1$ | 二－0．15\％ |
| $\therefore+0$ Ean | 356，670 | 344.670 | 507.1000 | 291.510 | $=34.300$ | 281．700 | 280． | 280．420 | 280.170 |
| ごせ Fこれ | 吠た ¢フ！ | 354．67！ | 317 ，409 | 391.510 | $3 \pm 4.3010$ | 271.700 | 290.670 | 29049 | 290.170 |
| 二⿺⿻⿻一㇂㇒丶幺小）F\％ | ぶゼ家0 | 364.670 | 327.1000 | 311.510 | 304．301） | 301.700 | こ00．850 | 300＋2i | 3130.170 |
| ？ P F Ba | 可感 | 374.670 | 337，100 | 321.519 | 314.200 | 311.710 | 310.670 | 310.420 | 310.170 |
| こ！E＝ain | ご可 | 384.670 | 3＋7， 010 | 351.514 | ここ4． 300 | 321.700 | こと！．670 |  | すこ0．t「茄 |
| $\therefore \rightarrow F \mathrm{lai}$ | 40 Ec ¢ 6 | 394．670 | 357．030 | 341.510 | 354.300 | 331.700 | こ？0．570 | $5 \geq 0.420$ | 330.170 |
| 三小 $F=\cdots$ | 41 －¢ ¢ | 404.670 | 367．000 | 351．510 | 344， 500 | 341.700 | 3417， 0 | 34リ．42！ | 340，170 |

## QLODD FAFAMETECE

：PRESSUPE IN FSW： 33 FSM ATA）

| FACO2 | （FSW） | FH2O ©FSti | CVOL |
| :---: | :---: | :---: | :---: |
| 1.70 |  | 2.00 | 170 |


| 2.39 | 2.39 |
| ---: | ---: |
| 1.87 | 1.87 |
| 56.00 | 36.00 |


| 2.37 | 2.37 | 2.35 | 2.35 |
| ---: | ---: | ---: | ---: |
| 1.87 | 1.87 | 1.87 | 1.37 |
| 29.00 | 13.00 | 10.00 | 7.00 |

2.39
1.87
7.00
2.37
1.87
8.00


TBLP1 WVAL59 (FEET )


## TBLPI VVAL59 (FEET )

21.00 FIMED FE2 IN NITROGEN RATES: DESEENT GO FFM: ASEENT GO FFM


| 60 | 100 | $0: 50$ |  |  | 31 | 32:00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60 | 120 | 0, 40 |  | 2 | 56 | 59:00 |
| 60 | 140 | 0:40 |  | 8 | 108 | 117:00 |
| 60 | 160 | 0:40 |  | 1.3 | 152 | 166:00 |
| 60 | 180 | 0:40 |  | 24 | 183 | 208:00 |
| 60 | 200 | 0:40 |  | 36 | 213 | 250:00 |
| 60 | 240 | 0:40 |  | 85 | 313 | 399:00 |
| 60 | 360 | 0:30 | 9 | 203 | E02 | 815:00 |
| 60 | 430 | 0:30 | 57 | 35. | 734 | 1145:00 |
| 60 | 220 | 0:30 | 158 | 588 | 749 | 1496:10 |

7047 1:10

|  |  | 0 | 1:10 |
| :---: | :---: | :---: | :---: |
|  |  | 4 | 5:10 |
|  |  | 18 | 19:10 |
|  |  | 30 | 31:10 |
|  | 2 | 38 | 41:10 |
|  | 10 | 38 | 49:10 |
|  | 16 | 59 | 75:10 |
|  | 21 | 91 | 113:10 |
|  | 26 | 120 | 147:10 |
|  | 30 | 146 | 177:10 |
|  | 34 | 172 | 207:10 |
| 1 | 43 | 191 | 236:10 |
| 3 | 50 | 210 | 264:10 |
| 5 | 63 | 226 | 295:10 |



TGIFI 分VHEG•FEE：



| 90 | 90 | 1：00 |  |  | $1 .$. | 4. | 1\％ | 1日里： |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 100 | 1：00 |  |  | $\therefore 1$ | 5.4 | ： |  |
| 90 | 110 | 1：00 |  |  | $\therefore 4$ | 3 | $\therefore$－！ | $\because \because \because$ |
| 90 | 120 | $0 \cdot 50$ |  | ＇ | $\because$ | $5:$ | $\cdots$ | F1r．ar |
| －30 | 130 | O：50 |  | 5 | 1 | $\underline{2}$ | 3 | 5x－${ }^{1}$ |
| 100 | 26 | 1：40 |  |  |  |  | 9 | 1：4\％ |
| 100 | 50 | 1：30 |  |  |  |  | $i$ | $\therefore 411$ |
| 100 | 40 | 1：20 |  |  |  | 4 | $\therefore \therefore$ | $38: 4$ |
| 100 | 50 | 1：20 |  |  |  | $1:$ | 37 | Fera |
| 100 | E0 | 1：10 |  |  | 4 | 210 | 37 | 14.11 |
| 1010 | 7 | 1：10 |  |  | 14 | 3：－ | 81 | \％i $\ddagger$ |
| 100 | Ei | 1：10 |  |  | 26 | 34 | 13ヶ | 1ミ： 11 |
| 1010 | 90 | 1：00 |  | 4 | 3 | 54 | 175 | 25149 |
| 100 | 100 | 1：00 |  | $1:$ | 31 | 45 | 20 | 36540 |
| 100 | 110 | 1： 10 |  | 13 | 32 | $3:$ | $24^{\circ}$ | $37-8$ |
| 100 | 120 | 1：00 |  | 24 | 51 | 117 | 704 |  |
| limit | lirie |  |  |  |  |  |  |  |
| 100 | 130 | $0: 50$ | 13 | ？： | 118 | $\therefore 0$ | －24 | 102541 |
| 100 | 240 | 0：50 | 20 | 97 | 10. | $45:$ | 74 | 145040 |
| 100 | 360 | （1）：40 | 4.4 | 159 | $40 \%$ | n5 | i43 | E6en 40 |
| 100 | 480 | 0 －40 | 14. | 378 | 57 | ret | 14.4 | $\cdots 7 \%$－ |
| 100 | 220 | 0：40 | 327 | 489 | 554 | $\underline{6}$ | 149 | 235411 |
| 110 | 22 | 1：50 |  |  |  |  | 4 | 1 ： 50 |
| 110 | 25 | 1：40 |  |  |  |  | 5 | ¢ 5 ¢ |
| 110 | 30 | 1：40 |  |  |  |  | 15 | 1セ： 5 |
|  |  |  |  |  |  |  |  |  |



TELPI YサHLSS EFEET



| 130 | 20 | 2：00 |  |  |  |  | 6 | － 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130 | 25 | 1：50 |  |  |  | 3 | 15 | －1． 1 |
| 130 | 30 | 1：50 |  |  |  | 13 | 25 | 4110 |
| 130 | 40 | 1：40 |  |  | 14 | 19 | $3:$ | 7a．110 |
| 130 | 50 | 1：30 |  | 10 | $1=$ | 3.4 | 78 | $12+14$ |
| 130 | 60 | 1：20 | 4 | 13 | 37 | 34 | 150 | －30：10 |
| 130 | 70 | 1：20 | $\exists$ | 2 | 1 | $\overline{4}$ | ق̈ | ¢！：！ |
| 150 | 80 | 1：20 | 1 r. | 28 | 51 | $\rightarrow \square$ | $\therefore 1$ | $441: 11$ |
| $\begin{gathered} 1 \text { init } \\ 130 \\ \hline \end{gathered}$ | line 30 | 1111 | － | －－ | I | 14 | SE | 5－10 |


| 140 | 18 | こ：20 |  |  |  |  |  |  |  |  | \％ | $\therefore \mathrm{O}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 140 | 211 | 2：10 |  |  |  |  |  |  |  |  | 1. | $1 \therefore \therefore 1$ |
| 140 | 25 | $2 \cdot 00$ |  |  |  |  |  |  |  | 10 | 18 | 玉uct |
| 140 | 511 | 1：5010 |  |  |  |  |  |  | $\because$ | 15 | $\because$ |  |
| 140 | 40 | 1：40 |  |  |  |  |  |  | $1:$ | $\because$ | 36 | F－ |
| 140 | 50 | 1：30 |  |  |  |  | $\therefore$ | $1:$ | $\because 9$ | $\therefore$ | $: 1 ;$ | $\because \square$ |
| 140 | E． | 1：30 |  |  |  |  | $1 \because$ | $!$ | $\bar{z}$ | 4 | $1 \% 1$ | ． 7 \％${ }^{\text {a }}$ |
| 1410 | 70 | 1： |  |  |  | 5 | 1. | $\because$ | $\because$ | $\cdots$ | －ris | $4 \mathrm{H}^{--}$ |
| 140 | 60 | 1：20 |  |  |  | $\square$ | 2 | $\therefore$ | $\div 1$ | $1 ;$ | $\because 49$ | －80， |
| limit | 11rif． |  |  |  |  |  | －－－ |  |  |  |  |  |
| 140 | 90 | 120 |  |  |  | 1 m | $\therefore$ | $\therefore$ | 4 | 1．： | $4 \cdots$ | ： |
| 140 | 160 | 1：19 |  |  | 14 | $2 \cdot 4$ | $\because$ | $\because$ | $15 \cdot$ | $\cdots$ | －デ | $\therefore \square=\therefore$ |
| 140 | 1：0 | 1－110 |  | 11 | 2マ | ii | $\therefore 3$ | 14.4 | A．$\because 4$ |  | － | 1：：¢ ¢ |
| 140 | 240 | 1：06 |  | 1： | 37 | ：-1 | 124 | $\therefore 7$ | 4 ¢ | ATE | －4－ | ； |
| 146 | 3 Ba | 6：50 | 9 | 57 | 110 | $1 \because$ | － | 19， | 「． 5. | － | －4． | 91．．．${ }^{\text {a }}$ |
| 140 | 490 | 0：50 | 30 | 76 | 197 | 24 | 4 E | $1 \therefore$ | $5 \cdot 4$ | $\therefore \square$ | －4＂ | $\because 4 \%$－ |
| F－8 |  |  |  |  |  |  |  |  |  |  |  |  |

TELFI UYमLSS \&FEET ;
21. GO: FISED FGZ IN NITPOGEN RATES: [ESCENT GO FFM: ASCENT 60 FPM






| 170 | 30 | $2: 10$ |  |  |  |  |  |  |  | 12 | 13 | 13 | 38 | $83: 511$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 170 | 40 | 1：50 |  |  |  |  |  | 4 | $1 \because$ | 13 | 18 | 34 | 132 | $215: 14$ |
| 170 | 50 | 1：40 |  |  |  |  | 4 | 12 | 12 | 17 | 31 | 50 | 2 c 1 | 94.519 |
| 170 | 60 | 1：30 |  |  |  | 1 | 11 | 12 | 15 | 28 | 31 | 150 | ここ | 50.50 |
| 1iruit | line |  |  |  |  |  |  |  |  |  |  |  |  | －－－－－－ |
| 170 | 70 | 1：30 |  |  |  | 6 | 12 | 15 | 20 | 28 | 48 | 1－7 | 455 | $\overrightarrow{7} \overrightarrow{5}$ ： |
| 170 | 90 | $1: 20$ |  |  | 2 | 11 | 20 | 24 | 26 | 37 | 153 | 274 | 671 | $1220: 50$ |
| 170 | 120 | 1：20 |  |  | 14 | 21 | 22 | 25 | 44 | 144 | $\therefore 67$ | ミ18 | 748 | $1741: 50$ |
| 170 | 180 | 1：101 |  | 15 | 20 | 21 | 41 | 103 | 123 | 268 | 478 | E\％ | 743 |  |
| 170 | 240 | 1：00 | 4 | 19 | 30 | 52 | 10 | 117 | 278 | 413 | 55 | E．3E | 749 | 25E2：50 |
| 170 | 360 | 1：00 | 18 | 43 | 91 | 98 | 218 | 300 | 438 | 489 | 557 | E® | 748 | 3ESS： |
| $\underline{170}$ | 480 | 1：00 | 46 | 85 | 113 | 241 | 311 | 577 | 433 | 487 | 553 | E36 | 749 | $4050: 50$ |


| 180 | 9 | 3：00 |  |  |  |  |  |  | 11 | 5： 010 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 180 | 10 | $2: 50$ |  |  |  |  |  |  | 1 | 4 ： 910 |
| 180 | 15 | 2 ： 30 |  |  |  |  | 1 | 4 | $\ddagger$ | 1： 010 |
| 180 | 20 | $2: 20$ |  |  |  | 1 | 4 | 1． | 20 | 41 － 19 |
| 180 | 25 | $2: 20$ |  |  |  | 5 | 14 | 14 | 3 | ヵ9：118 |
| 180 | 30 | 2：10 |  |  | 4 | 15 | 14 | $\therefore \therefore$ | 41 | 9＊： 0 |
| 180 | 40 | 2：00 |  | 11 | 12 | 13 | 2 c | 55 | 165 | $261: 00$ |
| 180 | 50 | 1：50 | 11 | 12 | 12 | 22 | 31 | 85 | 200 | 4JE：O！ |
| 180 | 60 | $1: 40$ | 11 | 12 | 20 | 29 | 33 | 旦 | $3 E$ |  |


| 190 | 9 | 3：10 |  |  |  | $\square$ | 9：111 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190 | 10 | 3：00 |  |  |  | 3 | 0： 19 |
| 190 | 15 | 2：40 |  | 3 | 4 | 12 | 2こ： 10 |
| 190 | 20 | $2: 30$ | 3 | 6 | 14 | 24 | $50: 119$ |

TEIFI VUA！59 ©FEET



| 190 | ：： | $=20$ |  |  |  |  |  |  |  | 2 | 3 | 14 | 14 | 37 | 75：10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $19 \%$ | 30 | $2 \cdot 0$ |  |  |  |  |  |  |  | 11 | 13 | 14 | 25 | 70 | 136：10 |
| 190 | 411 | 2：10 |  |  |  |  |  | $E$ | 11 | 15 | 13 | $\therefore 7$ | 35 | 208 | $310: 19$ |
| S：mit | lime |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 041 | 5 | 1：\％11 |  |  |  |  | $\overline{7}$ | 11 | 12 | 12 | 25 | 51 | 120 | 317 | 541910 |
| 120 | E9 | 1.41 |  |  |  | 5 | 10 | 12 | 11 | 25 | 20 | 52 | 187 | 4 ES | 797：10 |
| litit | 11 rir |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\therefore$ ail | 5 | 3.20 |  |  |  |  |  |  |  |  |  |  |  | 0 | $3: 20$ |
| － 10 | 10 | 3：80 |  |  |  |  |  |  |  |  |  |  | 1 | 4 | シャロ |
| $\bigcirc 0$ | 15 | $2 \cdot 47$ |  |  |  |  |  |  |  |  | 2 | 4 | 4 | 13 | 20：ciol |
| $\because 00$ | $\therefore 0$ | c： 70 |  |  |  |  |  |  |  | $\sim$ | 4 | 8 | 14 | 28 | $53: 20$ |
| 210 | 2 | 2 O |  |  |  |  |  |  | 1 | 3 | 12 | 14 | 17 | 38 | 68： 20 |
| \％ 10 | 56 | 20 |  |  |  |  |  |  | 5 | 12 | 1. | 14 | 29 | 9.9 |  |
| 2610 | 40 | c． |  |  |  |  | 1 | 11 | 12 | 12 | 13 | 32 | 50 | 220 | $354: 20$ |
| 200 | 50 | 1：50 |  |  |  | 3 | 11 | 11 | 12 | 15 | 28 | 32 | 150 | 365 | 636：20 |
| 2 Br | $\therefore 0$ | 1：411 |  |  | 1 | 11 | 10 | 12 | 15 | Eter | 28 | 86 | 137 | 55？ | 930：20 |
| 2100 | 419 | 1：30 |  | 5 | 10 | 12 | $\vdots 1$ | 22 | 24 | 38 | 134 | 175 | 5019 | 748 | $1695: 20$ |
| c！！ | $1 \because 0$ | 1：30 |  | 14 | 19 | 17 | 2i | 23 | 57 | 129 | 154 | 411 | 634 | 747 | $2232: 20$ |
| c | 1511 | 1：111 | $<17$ | 17 | 19 | 26 | 54 | 107 | 117 | 26. | 411 | 554 | 636 | 749 | こヨアテ：くす |
| $\therefore \therefore \therefore$ | 210 | 1：10 | 1010 | 25 | 36 | 82 | $9 E$ | 121 | 28： | $38 i$ | $48=$ | 554 | 636 | 749 | 348ri 20 |
| $\underline{\square}$ | $3+0$ | 10 | 2 C | 37 | 05 | 129 | 247 | 304 | 395 | 433 | 490 | 553 | 636 | 149 | $4171: 20$ |
| 11 mat | 1．ric |  |  |  |  |  |  |  |  |  |  |  |  |  | － |
| ＜1 9 | $\because$ | इ：$\square^{\text {a }}$ |  |  |  |  |  |  |  |  |  |  |  | 0 | $5: 50$ |
| $\therefore 11$ | 16 | $7: 10$ |  |  |  |  |  |  |  |  |  |  | 3 | 4 | $10 \cdot 30$ |
| $\therefore 10$ | ！- | －： 511 |  |  |  |  |  |  |  |  | 4 | 4 | 4 | 16 | 31.30 |
| $\therefore 11$ | ＇i | $\therefore 311$ |  |  |  |  |  |  | 1 | 4 | 3 | 11 | 15 | 30 | 67． 30 |
| ． 11 |  | ： 30 |  |  |  |  |  |  | $\because$ | 6 | 12 | 13 | $\therefore 1$ | 45 | 104．30 |

TBLP $\because \because H L 5 F$ GEET
21.00\% FIXEO FG2 IN NITRGGFN FATES: UEGEENT GO FFM AGGFT EO FFM


| $\underline{10}$ | 30 | 200 |  |  | 1 | 9 | $1 \bar{c}^{\prime}$ | 13 | 14 | 74 | $1 \because 4$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 210 | 41 | $2: 10$ |  | 7 | 11 | 12 | 12 | 18 | ¥ | - | E5: | 7 |
| - 216 | 50 | 2:00 | F |  | 11 | 12 | 19 | 7 |  |  | 413 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


| 220 | 10 | $3: 10$ |  |  |  |  |  |  | 1 | 4 | 4 | ! $\because 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \Sigma 0$ | 15 | 2:50 |  |  |  |  | 3 | $\overline{3}$ | 4 | $i$ | $1-$ | \% $\quad .7$ |
| $22^{20}$ | 20 | $2: 40$ |  |  |  | 4 | $\Xi$ | 4 | 15 | $1=$ | 7.4 | $5 \cdot 411$ |
| 220 | $\mathrm{c}^{5}$ | 2.30 |  |  | 3 | 3 | : | $1:$ | 14 | 5 | $\because$ | 14.4 |
| 220 | 30 | c: 30 |  |  | 4 | $1 \ddot{7}$ | 12 | 17 | 17 | 55 | 15 | $\therefore 4.5 \cdot 4$ |
| cid | 41 | $2: 10$ | $\bar{z}$ | 19 | 11 | 12 | $1:$ | 2 | 31 | 112 | 303 | 515.40 |
| 50 | 50 | $\therefore 000$ |  | 1. | 11 | 1. | 2 | $\underline{2}$ | . | E | 5 | $\operatorname{siz} 4!$ |
| $1 \mathrm{~m}_{1} \mathrm{t}$ | 10. |  |  |  |  |  |  |  |  |  |  |  |



TBLPI VVALSY \&FEET


TELFi YuH! EG FEET




| 280 | 10 | 3:40 |  |  |  |  |  |  | 2 | 3 | 4 | 4 | $\dot{\square}$ | 20 | 4.:411 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 280 | 15 | 3:10 |  |  |  | 2 | 3 | 3 | 3 | 4 | 3 | $1:$ | $1 \div$ | $3 \sim$ | E8:410 |
| 280 | 20 | 2:50 |  | 1 | 3 | 3 | 3 | 3 | 5 | 11 | 13 | 14 | 34 | $1 \Xi$ | $215: 411$ |
| 280 | 25 | 2:40 | 1 | 3 | 2 | 3 | 3 | 9 | 12 | 12 | 15 | 29 | 49 | 219 | SEj d 4 |
| 280 | 30 | 2:40 | 2 | 3 | 3 | 5 | 11 | 11 | 12 | 12 | 24 | Se: | 13 F | 35 | 55940 |


| 280 | 40 | 2:40 |  | 6 | 10 | 10 | 10 | 11 | 11 | 16 | 26 | 33 | 131 |  | 694 | 1129:40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| limit line- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 290 | 5 | 4:50 |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | 4 4: |
| 290 | 10 | 3:50 |  |  |  |  |  |  |  | 2 | 4 | 3 | 4 | 4 | $1:$ | $35: 5$ |
| 290 | 15 | 3:10 |  |  |  | 1 | 2 | 4 | 3 | 3 | 4 | 3 | 14 | 20 | 36 | 96.5 |
| 290 | 20 | 3:00 |  |  | 3 | 3 | 3 | 3 | 3 | 4 | 13 | 13 | 17 | 35 | 147 | 248:50 |
| 290 | 25 | 2:50 |  | 3 | 3 | 2 | 3 | 4 | 11 | 11 | 1.3 | 15 | 31 | 73 | 234 | $407: 50$ |
| 290 | 30 | 2:40 | 1 | 3 | 3 | 3 | 8 | 11 | 11 | 12 | 12 | 28 | 35 | 160 | 3: | 65c: 50 |
| 290 | 40 | 2:40 | 3 | 9 | 9 | 10 | 10 | 11 | 11 | 20 | 26 | 41 | 151 | $26^{\circ}$ | $6 E 5$ | 1237:50 |
| linit line- |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 300 | 5 | 5:00 |  |  |  |  |  |  |  |  |  |  |  |  | 0 | $5: 06$ |
| 300 | 10 | 3:50 |  |  |  |  |  |  | 2 | 3 | 4 | 3 | 4 | 13 | 28 | 6-\% : 0 |
| 300 | 15 | 3:20 |  |  |  | 2 | 3 | 3 | 4 | 3 | 3 | 6 | 14 | 23 | 37 | 10500 |
| 300 | 20 | 3:00 |  | 2 | 3 | 3 | 3 | 3 | 3 | 7 | 12 | 13 | za | 35 | 178 | 253:00 |
| 300 | 25 | 2:50 | 2 | 3 | 3 | 2 | 3 | 6 | 12 | 11 | 13 | 18 | 32 | 98 | 279 | 487:00 |
|  |  |  |  |  |  |  |  | F-1 |  |  |  |  |  |  |  |  |




GVVALEF－HITFOMEN

## TISSUE HALF－TIMES

| DEPTH |  | 5 MIN | 10 MIH | 2011 H | 40 MIN | 80 MTH | 120 MTV | 16日 | $\therefore 00111!$ | 24－M［11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ． 40 SDP | ． 50 SOR | ． 55 SER | ． 965 SF | GE SUR | アと地 | E！j［F | 4： 3 CL | $41: \because \mathrm{F} \cdot \mathrm{H}$ |
| 3 | MSW | 126.670 | 114.670 | 77.000 | 61.510 | 54.900 | 51.700 | 50，670 | 50420 | 5i） 170 |
| 6 | M -4 | 136.513 | 124．513 | 86．843 | 71．3E？ | C4．E43 | 61.543 | 60.513 | E020\％ | －1．117 |
| 9 | $\mathrm{M}=1.1$ | 146．355 | 134，355 | 96．6\％5 | 81．1．5 | 74．4ん5 | 71．3ヶ5 | 7 ¢ 5 5 | $70.10 \div$ | $\dot{\square} \dot{\square}$ |
| 12 | MSud | 156．173 | 144.198 | 10ヶ，523 | 91．リご | 64． 323 | 81．228 | $811.17 \%$ | 77.743 | ア－¢－ |
| 15 | MS61 | 166.140 | 154．040 | 116.37 B | 100.850 | 94．17！ | 51.47 | 5i1． 040 | 89．730 | 8ち．511 |
| 12 | MSW | 175．893 | 163.883 | 126．213 | 110.723 | 104.013 | 100.913 | 99.883 | 99.633 | 77.383 |
| 21 | MS ${ }^{\text {M }}$ | 195．725 | 173．725 | 156，055 | 120．5官 | 119．855 | 110.755 | 107.725 | 109.485 | 107．2こう |
| 24 | MSt | 135，5E\％ | 183.568 | 145.843 | $130.41 \%$ | $123.6 \pm 4$ | 1ご号安 | 11ヶ，5¢ | 11\％．31j | $11^{\circ} \mathrm{H}$ ，14\％ |
| 27 | MSd | 205.410 | 193.410 | 155．74i | $140 . \bar{c}=13$ | 13.3 .5411 | 130.440 | 1こう．41！ | 127.160 | 1ご 910 |
| 30 | MEld | 215，25． | 203，253 | 165．537 | 150，193 | 143.387 | 140.203 | 134．2E？ | 189．0！？ | 13＊，757 |
| 33 | MSU | 225．035 | 213.095 | 175．425 | 159．935 | 153．225 | 150，125 | 149．075 | 143．845 | 147．595 |
| 36 | MSul | 234．935 | 222．938 | 185．268 | 169．778 | 163．06C | 15.368 | 156．735 | 15E．6こ | 15\％．43\％ |
| 37 | MSid | 244，780 | 232，780 | 135．11！ | 179．6ご！ | 1「こ．う1！ | 18．7．81 |  | 1ヶ゙ 5ら！ |  |
| 42 | MSW | 254．623 | 242．623 | 204．953 | 189．4sis | 182.753 | 179．653 | 178．ジ | 1\％்．3i3 | 1ヶ\％ 123 |
| 45 | MSt | 264．465 | 25．2，465 | 214．795 | 199．305． | 192．55 | 18ら．4\％ | 18\％45E | 1： 215 | 15\％\％¢ |
| 48 | MSu | 274．305 | 262．308 | 224．638 | 209．148 | 202．436 | 139.335 | 138.305 | $1 \because 5.0, \%$ | 1\％7． |
| 51 | MSW | 284．150 | 272，150 | 234.490 | 218.950 | く12．2゙す | ＜1\％，18is | こ0： 150 | ご5． $70 \%$ | こいす。気吅 |
| 54 | MSld | 293.953 | 281．953 | 244．3ここ | 228，83 | 22c．$=3$ | $21 \%$ 12う | －1，933 | 217.743 | こ1，．4\％ |
| 57 | HEW | 303.836 | 291.836 | 254．155 | 238．675 | 231．3F | 228．865 | 227． 235 | 2．7．529 | 2ご，355 |
| 69 | MSW | 313.678 | 301.678 | 264．008 | 248．518 | ¢41．80： | 235．708 | こう「．6こう | $\because \because .4 \mathrm{c}$ | 23：178 |
| 63 | MSH | 323．524 | 311.521 | 273．65！ | 25S． 360 |  | 24\％，56 | これが「品 | これす。ごすい | 24：日i |
| bi | MSd | 333，363 | 321.363 | 283．693 | 268．203 | 2E1．473 | 258．3す5 | ミ5．$\vec{\square}$ | ご「．11引 | こ「ー．3ヵこ |
| 6.9 | MSW | 343.206 | 331.206 | $2 \pm 3.536$ | 278．046 | 271．336 | 268．256 | 26i． 2100 | 266． $55 \%$ | 26n． 7 （1） |
| 72 | MSW | 353．048 | 341.048 | 303．378 | 287.888 | 2お1．175 | 278．078 | 27\％．045 | ごに，793 | ごー 5．75 |
| r 5 | MSW | 362.891 | 350.891 | 313．221 | 297．751 | 291．021 | 287．921 | 286．81 | 2ヵも．641 | 2ミく 3＊ |
| 78 |  | 372．733 | 360.733 | 3ころ．063 | 307.575 | 304.863 | 297．7心玉 | ごャ，可ご | $\therefore>6.40$ | 29ヶ，ごき |
| 81 | MSW | 382.576 | 370.576 | 332.906 | 317.416 | 310.705 | 307.606 | 306.57 | 310． 3 － | 305 －年 |
| 84 | M -1.1 | 392．418 | 380.418 | 342．74\％ | 327.258 | 320.548 | 317.448 | 316.418 | －16．183 | 315．71\％ |
| 87 | MSW | 402.261 | 390.261 | 352．591 | 337． 101 | 330.351 | 327．291 | ここと，こE1 | उこE． 011 | こここ．TE1 |
| 90 | MSW | 412.103 | 400.103 | 362.433 | 346.943 | 340.233 | 337．133 | 356.107 | E35．85 | $335.60 \%$ |

## TELFI YUALSG ©METEFE:



TELFI MVMLS 9 METEF:
21.00\% FIXEG FG2 IN NITRUGEN RATES: DESEENT 15 MFM: ASIENT $1 E$ MFM



24 $4111:<1$

TBLFI VYALSG (METEFS )



| 27 | 32 | 1:30 |  |  | 0 | 1:30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 40 | 1:20 |  |  | 13 | 14:30 |
| 27 | 50 | 1:10 |  | 2 | 30 | 33:30 |
| 27 | 60 | 1:10 |  | 13 | 34 | 48:30 |
| 27 | 70 | 1:10 |  | 26 | 37 | 64:30 |
| 27 | -10 | $1: 40$ | 5 | 30 | 34 | 110:30 |
| 27 | 90 | 1:00 | 13 | 30 | 116 | 160:30 |
| 27 | 100 | 1:00 | 20 | 30 | 154 | 205:30 |






TBLPI YVALS5 (METEFE?

| $21.00 \%$ |  | FIXEO FGZ |  |  | NITROGEN |  |  | FATES | : DESCEHT |  | T 18 | MFM | ; GSEENT |  | $\begin{aligned} & 18 \mathrm{MPM} \\ & \text { TGTHI } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LEFTH | 日TM | TM TD | 36. | 33 | $\begin{gathered} \text { OELOMFFES } \\ \text { STOF } \end{gathered}$ |  |  | $\begin{aligned} & \text { SSION } \\ & \text { TINE } \end{aligned}$ | $\begin{aligned} & \text { STGFE :MSW) } \\ & \text { (MIH: } \end{aligned}$ |  |  | 7 |  | 3 |  |
| ¢MSW | TIM | $\begin{aligned} & \text { FIRST } \\ & \text { STOF } \\ & \text { (M:S } \end{aligned}$ |  |  |  |  |  | ¢ |  |  |  | $\begin{array}{r} \text { ACENY } \\ \text { YIME } \\ \text { GM:S } \end{array}$ |  |  |
|  |  |  |  |  | 30 | 27 | 24 |  | 21 | 13 | 15 |  | 12 |  |  |
| 53 | 69 | 1: 20 |  |  |  |  |  |  |  |  |  | 13 | 36 | 5 | 101:50 |
| $\therefore 3$ | $\checkmark$ | 1:10 |  |  |  |  |  |  |  |  | 3 | 23 | 5 | 114 | 171:50 |
| 3 | 60 | 1:10 |  |  |  |  |  |  |  |  | 9 | 28 | 30 | 165 | 23.30 |
| 33 | 96 | 1:10 |  |  |  |  |  |  |  |  | 13 | 27 | 44 | 207 | 2970 |
| 33 | 106 | 1:00 |  |  |  |  |  |  |  | 1 | 24 | 23 | B1 | 250 | 385:50 |
| 3 H | 20 | $\bar{c}: 10$ |  |  |  |  |  |  |  |  |  |  |  | 0 | 2:00 |
| 36 | 5 | 1:50 |  |  |  |  |  |  |  |  |  |  |  | 11 | 13:00 |
| 3 E | 31 | 1:411 |  |  |  |  |  |  |  |  |  |  | 5 | 17 | 24:00 |
| 35 | 411 | 1:90 |  |  |  |  |  |  |  |  |  | 5 | 14 | 31 | $52: 00$ |
| 3 E | 59 | 1:20 |  |  |  |  |  |  |  |  | 1 | 13 | 25 | 37 | 73:00 |
| 3 E | E0 | 1:09 |  |  |  |  |  |  |  |  | 7 | 19 | 30 | 98 | 156:00 |
| 3 | 7 | 1: 20 |  |  |  |  |  |  |  |  | 13 | 27 | 30 | 155 | 227:00 |
| in | 80 | 1:19 |  |  |  |  |  |  |  | 2 | 22 | 27 | 42 | 206 | 301:00 |
| 36 | 94 | 1:10 |  |  |  |  |  |  |  | 5 | 25 | 27 | 56 | 259 | 407:00 |
| $\because$ | 160 | 1:10 |  |  |  |  |  |  |  | 15 | 25 | 29 | 120 | 331 | 528; 00 |
| 3 P | 120 | 1:00 |  |  |  |  |  |  | 4 | 23 | c 4 | 59 | 175 | 472 | 257:00 |
| ar | 1-17 | 1:00 |  |  |  |  |  |  | 20 | 34 | 84 | 15.2 | 40 E | 719 | 1417:00 |
| 3 | 2411 | 11:5i |  |  |  |  |  | 5 | 37 | 76 | 135 | 320 | 565 | 738 | 1884:00 |
| E | 350 | $\therefore$ - ¢ ¢ |  |  |  |  |  | 29 | 97 | 151 | 348 | 525 | 629 | 739 | 2522:00 |
| Ti | 4: is | 19: 50 |  |  |  |  |  | 80 | 141 | 317 | 456 | 547 | 630 | 739 | 2918:00 |
| -3E | 720 | 日:90 |  |  |  |  | 23 | $1 ? 4$ | 325 | 435 | 485 | 548 | 629 | 133 | 3360:00 |
| 30 | 15 | 2:10 |  |  |  |  |  |  |  |  |  |  |  | 0 | 2:10 |
| $2:$ | $\because 0$ | $\vec{c}: 10$ |  |  |  |  |  |  |  |  |  |  |  | 4 | E:10 |
| ic | 25 | 1.50 |  |  |  |  |  |  |  |  |  |  | 2 | 15 | $19: 10$ |

TBIFI VWA！SG METEFS
21．00\％FIAED FO2 IN NITROGEN RATES OEGENT $1 E$ MFM．MEGENT $1 E$ MFH


| 39 | 30 | 1：501 |  |  |  | 3 |  | 7. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 35 | 40 | 1：40 |  |  | 17 | $\because$ | $:=$ | $\alpha$ |
| 39 | 50 | 1：30 |  | 9 | 13 | $\therefore$ | $\therefore \because$ | ： 1 |
| 39 | 60 | 1：20 | $\bar{\square}$ | 13 | $\because$ | 21 | 17\％ | 7 |
| 39 | Fi | 1： 20 | $\theta$ | $1 \%$ | ：－ | ．${ }^{\prime}$ | 14 | $\therefore-$ |
| 37 | 80 |  | $1=$ | $2{ }^{2}$ | $\because-$ | $\because$ | ＇ | $\cdots$ |
| $\begin{gathered} \text { limit } \\ \hline \end{gathered}$ | $\begin{gathered} \text { line } \\ =0 \\ \hline \end{gathered}$ | 1：10 | $\therefore 1$ | $\pm$ | $\therefore$ |  | こ： |  |


| 42 | 10 | c：20 |  |  |  |  |  |  |  |  |  | $\therefore 1$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 42 | 24 | $2: 10$ |  |  |  |  |  |  |  |  | $1: 1$ | $12 \ldots$ |
| 42 | E | $\therefore 000$ |  |  |  |  |  |  |  | $=$ | $1-$ | －こ！ |
| 42 | 43 | 1：50 |  |  |  |  |  |  | 4 | 1.4 | － |  |
| 42 | 40 | 1：40 |  |  |  |  |  | $\cdots$ | 17 | 17 | $\therefore$ | i |
| 42 | 50 | 1：30 |  |  |  |  | 4 | 15 | 15 | 711 | 11.8 | 1rsar |
| 42 | 50 | 1：30 |  |  |  |  | 11 | 15 | $\because$ | $\square-$ | 1－年 | ＋0．3 |
| 42 | 70 | 1：co |  |  |  | 4 | 18 | $\overline{2}$ | 2 | $r . z$ | $\therefore$ | \％ras |
| 42 | 60 | 1：$=0$ |  |  |  | 8 | 15 | 2 | c． | $1: ?$ | 3こう | Sこと． 0 |
| limit |  |  |  |  |  |  |  |  |  | －－－ |  |  |
| 42 | 70 | 1：20 |  |  |  | 13 | $\square$ | 24 | 4. | $16!$ | 411 | －6： |
| $4{ }^{5}$ | 120 | 1：10 |  |  | 11 | $\therefore 1$ | $\because$ | 4.4 | $13 \%$ | CO＝ | 64 | 1141．20 |
| 42 | $18 i$ | 1．00 |  | 9 | $\bar{c}^{0}$ | 33 | 7 | 175 | ciin | $5 \cdot 4$ | 37 | 1874 ću |
| 42 | 246 | 1：100 |  | 15 | 41 | 74 | 120 | 2 r | 44. | 427 | $\therefore 5$ |  |
| $42^{2}$ | 300 | 9，¢9 | 7 | $4 \%$ | 99 | $1+3$ | 315 | 412 | 54 | E31 | こざ |  |
| $4 \overline{7}$ | $48 \%$ | IT： 5 | $z^{5}$ | $\bar{c}$ | 15 t | $\cdots$ | 41 ¢ | $4=$ |  | 二品 | 3 | ふア®－ |
| $-4=$ | 72 | 0：50 | 53 | 007 | O2 | 20. | 4 y | 45 | Eis | $\cdots$ | $\because$ | 204\％ | $4 \% \quad 10<\pi 0$

TELF 1 VYHLEG (METEFS)



DE OMFFESSJOW STOFS (MSW) STOF TIAES (MIN.

TOTAL heCENT TIME (M:S)


TE:F1 UWO! E CMETEFS




$54 \quad 15 \quad 2: 40$
$16 \cdot 00$
$5420 \quad 2: 30$
55:00
$54 \quad 25 \quad 2: 20$
$4 \quad 14 \quad 14 \quad 24 \quad 54100$
$5430 \quad 2: 10$
$3 \quad 15 \quad 14 \quad 14 \quad 4 \%$ 天
$5440 \quad 2: 00$
$1012 \quad 13 \quad 15 \quad 30194 \quad \div 4 \cdot 10$
$54 \quad 50 \quad 1: 50$




TELPY VVALSG (METEFS)
21.00\% FIXED FUZ IN NITROGEN RATES: OESEENT 18 MFM; ASCENT 18 MFM

| DEPTH | BTM | TM TO |  |  |  | DECOMFFESSIOH STOFS (MSW) |  |  |  |  |  |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\therefore$ MS4. | TIM | FIRST |  |  |  |  | ST | T | CE | MIN |  |  |  |  |  | ASCENT |
|  | ( $\mathrm{N}^{\text {) }}$ | STUF |  |  |  |  |  |  |  |  |  |  |  |  |  | TIME |
|  |  | (M: ${ }^{\text {\% }}$ | 37 | 36 | 33 | 30 | 27 | 24 | 21 | 16 | 15 | 12 | 9 | 6 | 3 | (M:5) |


| 51 | 80 | 1:401 |  |  |  |  | 4 | 10 | 12 | 11 | 17 | 25 | 51 | 163 | 428 | 7300:10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| lıthit | 1 lnf |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| bu | $\varepsilon$ | 3: 20 |  |  |  |  |  |  |  |  |  |  |  |  | 0 | $3: 20$ |
| E! | 10 | $3: 10$ |  |  |  |  |  |  |  |  |  |  |  |  | 4 | $7: 20$ |
| fil | 15 | $\therefore: 41$ |  |  |  |  |  |  |  |  |  | 1 | 4 | 4 | 13 | $25: 20$ |
| -. 1 | 二10 | 2030 |  |  |  |  |  |  |  |  | 2 | 3 | 8 | 14 | 20 | $50: 20$ |
| 8 | $\therefore 5$ | $\therefore 30$ |  |  |  |  |  |  |  |  | 4 | 11 | 14 | 14 | 32 | 78:20 |
| ¢-11 | 30 | $\ddot{\sigma}: \underline{0}$ |  |  |  |  |  |  |  | 3 | 12 | 13 | 14 | 20 | 87 | 152:20 |
| en | 40 | 2:10 |  |  |  |  |  |  | 11 | 12 | 12 | 13 | 21 | 49 | 205 | 326:20 |
| \% 0 | 40 | 1:50 |  |  |  |  | 2 | 11 | 11 | 11 | 13 | 21 | 36 | 135 | 345 | $551: 20$ |
| F.6 | 50 | 1:50 |  |  |  |  | 11 | 10 | 12 | 11 | 20 | 25 | 79 | 175 | 516 | 862:20 |
| -i | 98 | 1:30 |  |  | 4 | 10 | 10 | 17 | 20 | 21 | 44 | 111 | 173 | 459 | 739 | 1611:20 |
| tor | 1 c.9 | 1:30 |  |  | 11 | 17 | 17 | 19 | 24 | 48 | 120 | 154 | 386 | 610 | 739 | $2150: 20$ |
| fir | 16 | 1:111 | 1 | 15 | 15 | 16 | 35 | 44 | 99 | i 11 | 258 | 393 | 548 | 630 | ア38 | 2904 : 20 |
| -i | $2+10$ | $1 \cdot 10$ | 8 | 14 | 27 | 56 | 70 | 93 | 131 | 274 | 36.9 | 485 | 548 | 629 | 739 | $3425: 20$ |
| - E® | $3-4$ | 1:10 |  |  |  | 89 | 131 | 246 | 295 | 394 | 434 | 485 | 548 | 629 | 737 | 4114:20 |
| $\begin{gathered} 110.3 t \\ 0.9 \end{gathered}$ | $11 r i 6$ | $\cdots$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 7 | $3: 30$ |  |  |  |  |  |  |  |  |  |  |  |  | 0 | $3: 30$ |
| 13 | 10 | 3:111 |  |  |  |  |  |  |  |  |  |  |  | $\overline{2}$ | 4 | $9: 30$ |
| r. 3 | 15 | 2:5i |  |  |  |  |  |  |  |  |  | 3 | 4 | 4 | 15 | 29:30 |
| 8 | 20 | $2: 30$ |  |  |  |  |  |  |  | 1 | 3 | 4 | 10 | 14 | 23 | 53:30 |
| 03 | 3 | 2030 |  |  |  |  |  |  |  | 3 | 5 | 12 | 14 | 14 | 43 | 94:30 |
| 03 | 311 | 20 |  |  |  |  |  |  | 1 | 8 | 12 | 13 | 13 | 24 | 115 | 189:30 |
| 8 | 40 | $2: 10$ |  |  |  |  |  | 6 | 11 | 12 | 12 | 13 | 25 | 74 | 228 | 384:30 |
| e 3 | 51 | E:00 |  |  |  |  | 9 | 10 | 11 | 12 | 12 | 25 | 45 | 158 | 376 | 682:30 |
| ifmat | 1116 |  |  |  |  |  |  | --- |  |  |  |  |  |  |  | $\cdots$ |
|  | , | $3: 40$ |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 3:40 |

TREFI धVAIGE AMETEFE
21．00\％FIKED FU2 IN NITROEEN FATES：OESEENT 18 MFH：ASCEHT $1 E$ MFM

DEPTH ETM TM TO ©MSII ：TIM FIRST （N）STOF



| 78 | $1!$ | － 311 |  |  |  |  |  |  |  | 4 | 4 | 4 | 1 rab |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | $1=$ | － 110 |  |  |  |  | 3 | $\bar{\square}$ | 4 | 4 | $1 i$ | 15 | $45: 60$ |
| Fic | $\dot{c}$ | $\therefore 10$ |  |  | 1 | F | 4 | 7 | B | 1.7 | 1.4 | 30 | E0．00 |
| $\therefore$ | $\therefore$ | c．111 |  |  | 3 | 4 | 4 | $1 \%$ | 1 | 14 | $\cdots$ | 119 | 10： 010 |
| $\therefore$ | ご1 | $\therefore \square$ |  | 1 | 4 | 7 | 11 | 12 | 13 | $1 \bar{i}$ | 4 | 163 |  |
| $\therefore$ | 411 | $\therefore こ ゙$ | 3 | 10 | 11 | 11 | 11 | 1： | $\therefore 1$ | $4=$ | 1.12 | －－ 4 | H4F． 10 |
| $\leq$ | $\cdots$ | E1： | 10 | 10 | 11 | 11 | 11 | 2 | 2 | $\because \pm$ | ＂ | F1 | 14.96 |

TBLFI WVATS ©METEFS：
$21.00 \because$ FIWEO FQS IN NITROGEH
RATES：LESCENT 18 MFM：ACIEHT 18 MPH

| VFFTH | ETM | THT日 |  |  |  |  |  | ［ELDMFFESS］ON STDFS（HSA） |  |  |  |  |  |  |  |  |  |  |  | Ti．THL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.118 | TIH | F95\％ |  |  |  |  |  |  | STO | T | E S | MI |  |  |  |  |  |  |  | H CCENT |
|  | 1 F ， | 三 Ti．F |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | TIFE゙ |
|  |  | （M，${ }^{\text {c }}$ | 51 | 48 | 45 | 42 | 39 | 36 | 3.3 | 30 | 27 | 24 | 21 | 18 | 15 | 12 | $\exists$ | $E$ | 3 | CM13． |



TBLF1 WMBLSF（METEFG）
21．00\％FIXED FOS IN NITROCEN
PATES：DESCENT IE MFM；GSEENT 18 MFM

| CEFTH ：MC．！ | ETH TIM | TM TM FIPST |  |  |  |  |  |  |  | STMF | ESSI | OH： | TOF: $\mathrm{MH}$ | $\langle M=$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 1 \％ |
|  |  | （N：S） | 57 | 54 | 51 | 43 | 45 | 42 | 39 | 36 | 33 | 30 | 27 | 24 | 21 | 13 | 15 | 12 | 9 | 6 | ज | 14： 5 ） |
| －31 | 40 | 2：30 |  |  |  |  |  |  |  | 1 | 9 | 10 | 10 | 10 | 11 | 12 | 17 | 31 | 92 | 186 | 554 | 44？ |
| $\begin{gathered} 11 n i t \\ 34 \end{gathered}$ | $\begin{gathered} 1!\text { ne } \\ 5 \end{gathered}$ | 4：40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | II | 4：412 |
| 34 | 10 | 3：50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 3 | 4 | 4 | $\bar{j}$ | 27：4ir |
| 94 | 15 | $3: 10$ |  |  |  |  |  |  |  |  |  |  | 1 | 3 | 3 | 4 | 3 | 4 | 10 | 14 | 70 | Fe．an |
| 54 | 20 | 2：50 |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 3 | $\overline{3}$ | 4 | 9 | 17 | 14 | 24 | 111 | 130：40 |
| 94 | 25 | 2：50 |  |  |  |  |  |  |  |  | 3 | 3 | 3 | 3 | 8 | 11 | 12 | 13 | 29 | 45 | 175 | こごア 4 |
| 84 | 30 | $2: 40$ |  |  |  |  |  |  |  | 2 | 2 | 3 | 5 | 11 | 11 | 12 | 12 | 15 | 33 | 119 | $31^{\circ}$ | $5.45: 411$ |
| 84 | 40 | 2：40 |  |  |  |  |  |  |  | 6 | 9 | 10 | 10 | 10 | 12 | 11 | 213 | 40 | 109 | 211 | biz | 1455：40 |
| $\begin{gathered} \text { linit } \\ \text { E? } \end{gathered}$ | $\begin{gathered} \text { line } \\ 5 \end{gathered}$ | 4：50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | --5 $4-50$ |
| 87 | 10 | 3：50 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 | 3 | 4 | 4 | 3 | 11 | 315 |
| － | $1 \equiv$ | 3：24 |  |  |  |  |  |  |  |  |  |  | 3 | 3 | 3 | 5 | 4 | 4 | $1:$ | 14 | $\pm$ | EE： 0 |
| 87 | 21 | 3：00 |  |  |  |  |  |  |  |  | 2 | 3 | 3 | 3 | ． 3 | 4 | 12 | 13 | 13 | 27 | 135 | 215：50 |
| 87 | 2 º | 2：50 |  |  |  |  |  |  |  | $\overline{2}$ | 3 | 3 | 3 | 3 | 10 | 12 | 12 | 15 | 22 | $\therefore 4$ | 2こ1 |  |
| $8 i$ | 30 | 2：40 |  |  |  |  |  |  | 1 | 3 | 2 | 3 | a | 11 | 11 | 12 | 12 | 18 | 41 | 137 | 353 | $8.21: 50$ |
| 37 | 40 | 2140 |  |  |  |  |  |  | 3 | 8 | 9 | 10 | 10 | 11 | 11. | 11 | 23 | 42 | 127 | 254 | 652 | 1101：50 |
| $\begin{gathered} \text { linit } \\ 9(i \end{gathered}$ | $\begin{gathered} \text { line. } \\ 5 \end{gathered}$ | 5：00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | $5: 90$ |
| 90 | 10 | 4：00 |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 | 4 | 3 | 4 | 4 | 12 | $35: 90$ |
| 40 | 15 | 3：20 |  |  |  |  |  |  |  |  |  | 2 | 3 | 3 | 3 | 3 | 4 | 5 | 13 | 17 | 40 | 98：00 |
| 90 | $\geq 0$ | 3：00 |  |  |  |  |  |  |  | $z$ | 2 | 3 | 3 | 3 | 3 | $\bar{i}$ | 12 | 12 | 15 | 31 | 154 |  |
| 915 | － 5 | 2：50 |  |  |  |  |  |  | 2 | c | 3 | 3 | 3 | 5 | 11 | 12 | 12 | 13 | 25 | 88 | $25 \therefore$ | 436：000 |
| 30 | 30 | 2：50 |  |  |  |  |  |  | 3 | 3 | 2 | 4 | 10 | 11 | 11 | 11 | 13 | 20 | 49 | 155 | 355 | 672：00 |
| 30 | 40 | 2：40 |  |  |  |  |  | 2 | 5 | 9 | 9 | 10 | 10 | 11 | 11 | 14 | 23 | 57 | 145 | 295 | $66:$ | 13ロ3：0n |
| 50 | 60 | 2：10 |  |  | 1 | 7 | 8 | 8 | 9 | 7 | 9 | 10 | 12 | 18 | 27 | 47 | 107 | 145 | 366 | 59 | 737 | 2124：00 |
| $\ddagger 0$ | 915 | 1：50 | 3 | 7 | 7 | 7 | $\varepsilon$ | 9 | 9 | 14 | 16 | 16 | 35 | 42 | 100 | 107 | 244 | 386 | 547 | 630 | 739 | $2735: 10$ |



TBLFI
thele of maximum pefilssigle tissur tenstona
（VVALES－NITFOGEN
TISSIJE Hol．f－times

| ［EFPTH |  | 5 MIN | 10 HIH | 20 MIH | 40 NIN | 30 MIH | 120 MIN | 160 MIN | 200 MJH | 240 MIN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ． 40 S0F | ． 50 S0F | ． 55 S0F | ． $5 \pm 5 \mathrm{LF}$ | ． 9650 F | ． GB SUN | ． 60 SDF | ． 95 SuF | 40 jur |
| 10 | FSU | 126．670 | 114.670 | 27．000 | 61.510 | 54.800 | 51.700 | 50.670 | 50.420 | 50.170 |
| 20 | FSW | 156.670 | 124.670 | 87． 010 | 71.510 | 64．800 | 61.700 | 60．6ア0 | $60.42^{\circ} 15$ | 60.170 |
| 30 | FSd | 146.670 | 134.670 | 97.000 | 81．510 | 74.300 | 81.700 | T0．ero | 70.4211 | 70.170 |
| 40 | FEH | 156.670 | 144.670 | 107.010 | 91．E10 | 84.800 | 81.700 | g0，era | 80.420 | ci） 170 |
| 50 | FSU | 166．670 | 154．670 | 117．00！ | 101.510 | 94.800 | 91.700 | $90 . \cos 0$ | 70.420 | 90.170 |
| ¢0 | FSid | 176．650 | 164．650 | 127．000 | 111.510 | 104．800 | 101．700 | 100．E50 | 110.420 | 100．170 |
| 70 | FEin | 136．670 | 174.670 | 137．000 | 121.510 | 114.800 | 111.700 | 110.670 | 110.450 | 110.170 |
| 30 | FSH | 176.670 | 184.670 | 147．000 | 131.510 | 124.800 | 121．700 | 120.670 | 120.420 | 120．170 |
| 5 | FSい | 200．670 | 194.670 | 157．000 | 141.510 | 134．800 | 131.700 | 150.650 | 120.480 | 15.170 |
| 106 | Fsw | 216.670 | 214.670 | 16\％．000 | 151.510 | 144.800 | 141．700 | 141．850 | 1411.420 | 144．170 |
| 110 | F®\＃ | 226.670 | 214.670 | 177.000 | 161.510 | 154.800 | 151.700 | 150．670 | 150．420 | 150．170 |
| 120 | FSh | 236.670 | 224.670 | 187.000 | 171.510 | 164.800 | 161．700 | 160．670 | 160.420 | 160.170 |
| 1.30 | Fsu | 246.670 | 234.670 | 197．000 | 181.510 | 174．800 | 171．700 | 170.680 | 170.420 | 170.170 |
| 140 | FSU | 256．670 | 244.670 | 205.000 | 191.510 | 184．800 | 181.700 | 150．670 | 100．4：0 | 160．170 |
| 150 | $\mathrm{F}=4$ | 265.670 | 254．670 | 217．000 | 201.510 | 194.600 | 191.700 | 190.680 | 190．42！ | 190.170 |
| 180 | FSW | 276．6．0 | 264.670 | 227.000 | 211.510 | 204.800 | 201.700 | cub，ero | 200．420 | 200.170 |
| 170 | Fsin | 286.650 | 274.674 | 235．000 | 221.510 | 214.800 | 211.700 | 210．6－0 | $210.45^{\circ} \mathrm{j}$ | 219．170 |
| 134 | FSW | 276.670 | 284.670 | 247.000 | 231.510 | 2et． 800 | 221.700 | 220，¢－0 | 220.420 | 220.170 |
| 130 | FSid | 360.670 | c94．670 | 25．7．000 | 241.510 | 234.800 | 231.700 | 250．60 | 2\％0．420 | 230.170 |
| c $0_{1}$ | FSW | 316.670 | 304，670 | 26．9．000 | 251．519 | 244.8010 | 241.700 | 240.670 | 240．420 | 241．170 |
| 210 | Fsod | 326.670 | 314.670 | 277.000 | 261.510 | 554．860 | 251.700 | 259．5－0 | 250.420 | 259， 170 |
| 2¢！ | FS | 336．670 | 324.670 | 2ar． 080 | 271．510 | 2\％4．8010 | 2e1． 700 | 2encera | 2 ta .42 u | 2ra．170 |
| 230 | $F S W$ | 346.670 | 334.670 | 297．000 | 281.510 | 274.800 | 251．700 | 276.670 | 270.420 | 270.170 |
| 240 | FSい | 356.670 | 344．670 | 307.000 | 231.510 | 284．300 | 281.700 | 200.670 | 280.420 | 280.170 |
| 250 | Fsid | 366.670 | 354.670 | 317.000 | 301.510 | 294．300 | 291.700 | 290.670 | 290.420 | 250．170 |
| こ¢0 | FSH | 376.670 | 364.670 | 325．000 | 311.510 | 304.800 | 301.700 | 300，ero | $300.4 \div 0$ | 300.170 |
| 270 | FSth | 366.676 | 3r4．E70 | 35．．000 | 3 Sc 1.510 | 314.800 | 311.700 | 310.650 | 310.420 | 310.180 |
| －0 | FSIM | 35E．670 | 364.670 | $3+7.000$ | 331.510 | $3 \% 4.3010$ | 321.700 | 320.650 | 320．420 | 320.170 |
| ¢90 | $F \leq W$ | 416．670 | 354.670 | 35．7．000 | 341.510 | 354.800 | 331.700 | 350.650 | 350.420 | 330.170 |
| $\bigcirc$ | F：M | 416.670 | 404.670 | 365．010 | 351， 510 | 344.80 | 341.700 | 940， 00 | 340．420 | 3410.170 |

BLODC FAFAMETEFS
$\therefore$ PFESGUPE IN FSU； $\bar{S}$ F FSM ATA，

| $\begin{aligned} & \text { FATGZ iF } \\ & 1.70 \end{aligned}$ |  .170 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.35 | 2.35 | 2.39 | 2.35 | 2.39 | 2.35 | 2．39 | （vüt \％） |
| 1.87 | 1．8\％ | 1.87 | 1.87 | 1.87 | 1．87 | 1．57 | （FSL） |
| 29．10 | 13．190 | 10.00 | 7.00 | 7.00 | $\therefore 00$ | 7.00 | （FSW） |


| Envos | 2.39 | 2．39 | 2.35 | 2.35 | 2.39 | 2.35 | 2.39 | 2.35 | 2．39 | （Vül \％） |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F Fras： | 1.87 | 1.87 | 1.87 | 1．8》 | 1.87 | 1.87 | 1.87 | 1.87 | 1.57 | （FSI．， |
| FF：IUF | 36， 06 | 36.0 | 29.10 | 13．00 | 10.00 | 7.00 | 7.00 | $\therefore 00$ | 7.00 | （FSい） |

## TELF 1 WMLSS \&FEET

70 ATA FIMEE PGZ IN NTTRGTEF FATES: DESEFNT EO FF:G ASCENT EA FE:



TELF！YVALS（FEET ）
FO ATA FISFG FOE IN NITPOCEN RATES：DESEENT GO FFM：ASCENT GO FFM



300 0：40
$107107: 50$
5036010
115 115：50
E0 5T0 0：40
123 123：50
E． 11000040
131 131：50
$50 \quad 30 \quad 0: 40$
139 139：50
60 70 1：00
$0 \quad 1: 00$

$5 \quad 6: 00$
$00900: 50$
E．i $100 \quad 0: 50$
$8 \quad 9: 00$

11 12：00
セ0 110 0：50
14 15：00
$60120 \quad 0: 50$
19 20：00
E11 $130 \quad 0: 50$
24 25：00
6ri 140 8：50
35 36：00
60 150 0：50
$50160 \quad 0: 40$
ní 170 0；40
$60 \quad 180 \quad 0: 40$
$60 \quad 190 \quad 0: 40$
6 78 85：00
60 200 $0: 40$
ジ ごロ 0：40
$602200: 40$
$602300: 40$
E0 $240 \quad 0: 40$

|  | 46 | $47: 00$ |
| :--- | :--- | :--- |
| 1 | 55 | $57: 00$ |
| 2 | 64 | $67: 00$ |
| 3 | 72 | $75: 00$ |
| 6 | 78 | $85: 00$ |
| 9 | 83 | $93: 00$ |

$1288101: 00$
$1496 \quad 111: 00$
$16 \quad 104 \quad 121: 00$
20116 137：00

PO ATA FIXED PGE IN NITEDIEN RATEE：DEERENT GO FFN．AGENT EA FFA QFPTH
GFSW：

## OEC OMFFESSION STOFE AFGH： <br> TOTMI

 CFSW：TIM FIRET STOF TINES（MIHHECENT （ni） 5 TOF

$60250: 40$

$$
25 \quad 12 \overline{25} \quad 15 \cdot 06
$$

EO 260 0：40 $32137 \quad 170: 10$
$00 \quad 270 \quad 0: 40$
36 146 185：00
$60 \quad 280 \quad 0: 40$

$$
43 \text { 15e z0ण:00 }
$$


$4 \approx 16421306$
$603000: 40$

$603100: 40$
$56182 \quad 2900$
$60 \quad 320 \quad 0: 40$
Et 19225400
$603300: 40$
6420426900
E0 340 0：40

$60350 \quad 0: 40$
31220300100
$60360 \quad 0: 40$
$75239315: 00$
$603700: 40$
ア5 250 3この：00
60 350 0：40
3425834000
$60 \quad 390 \quad 0: 40$
$89266 \quad 350: 110$
$70 \quad 49 \quad 1: 10$
$0 \quad 1: 10$
$70 \quad 50 \quad 1: 00$

| 0 | $1: 10$ |
| :--- | :--- |
| 1 | $2: 10$ |
| $\exists$ | $10: 10$ |

$70 \quad 70 \quad 1: 00$

| 15 | $16: 10$ |
| ---: | ---: |
| 21 | $22: 10$ |
| 4 | 21 |
| 8 | $20: 10$ |
|  | $32: 10$ |

$701000: 50$
1136 4末：10
$70 \quad 110 \quad 0: 50$
$144964: 10$

TBLFI WVMLSG \＆FEET
－O ATH FIKEU FOE IN MITRUGEN RATES：DESCEHT EO FFM；ASCEHT EO FFM

| ［EPTH | ETM | TM TU |  |  |  | CECOM | FF | S10 | $5 T$ | S | Sid |  |  |  | TOTAL． |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ＜FSW | TIM | FIRET |  |  |  |  | TF | TITAE | （ | W： |  |  |  |  | AECEHT |
|  | ¢ | STGF |  |  |  |  |  |  |  |  |  |  |  |  | TIME |
|  |  | －M ：$: ~=~$ | 120 | 110 | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 | 10 | （MS） |


| 71 | 13 | 0：50 |  | 16 | 61 | 78：10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pi | 1すい | U：¢ ¢ |  | 18 | 73 | 92：10 |
| 70 | 150 | 19：00 |  | 22 | 82 | 105：10 |
| 79 |  | 11：50 |  | 27 | 89 | 117：10 |
| 70 | 15 | 11：40 | 1 | 31 | 97 | 130：10 |
| limit | 11 tie |  |  |  |  |  |
| 「11 | 134 | $4: 40$ | $\bar{z}$ | 38 | 167 | 148： 10 |
| 70 | 190 | i1：40 | 2 | 48 | 122 | 173：10 |
| 70 | 200 | 6：40 | 3 | 57 | 136 | 197：10 |
| 70 | 210 | 0：40 | 5 | 65 | 149 | 220：10 |
| 76 | 2 E | $0: 40$ | 5 | 71 | 162 | 242：10 |
| 79 | 230 | $0 \cdot 40$ | 11 | 76 | 175 | 263：10 |
| 70 | 240 | 0：40 | 1.3 | 82 | 186 | 282：10 |
| $i 1$ | 250 | $0: 40$ | 15 | 88 | 201 | 305：10 |
| 75 | 200 | 0： 40 | 18 | 92 | 219 | 330：10 |
| 51 | 20 | 10：40 | cil | 96 | 235 | 352：10 |
| － 0 | 260 | 0：40 | 23 | 100 | 251 | 375：10 |
| $\therefore 1$ | 290 | 0：40 | 29 | 104 | 264 | 398：10 |
| 76 | 300 | 0：40 | 34 | 107 | 277 | 421：10 |
| 79 | 519 | 4：49 | $4!$ | 116 | 286 | 443：10 |
| i | $3 \%$ | 11：419 | 45 | 126 | $29 \%$ | 454：10 |
| 76 | 370 | 19：40 | 49 | 137 | 297 | 484：10 |
| $7 \%$ | 340 | 0：40 | 54 | 146 | 303 | 504：10 |
| －-0 | 350 | 11：40 | 58 | 150 | 308 | 523：10 |
| E\｜ | 5 | 1： 20 |  |  | 0 | 1：20 |

TELPI YWr！ 59 EFET
PO ATA FIXEO FGZ IN NITROLEN FATEE：DESGENT GO FFM；HGEFT GU FFH


| 80 | 40 | 1：10 |  |  |  |  | 3 シ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E0 | 50 | 1：10 |  |  |  | 17 | $14 \cdot \%$ |
| 80 | 60 | 1：00 |  |  | 1 | 21 | 23 － |
| 80 | 70 | 1：00 |  |  | $\exists$ | $\cdots$ | 5i Cou |
| 80 | 80 | 1：00 |  |  | 15 | 22 | 30： 2 |
| 80 | 90 | 1：00 |  |  | 21 | 35 | 5500 |
| $\begin{gathered} \text { limit } \\ \text { Bn } \end{gathered}$ | $\begin{aligned} & 1 \text { ine } \\ & 100 \end{aligned}$ | 19：50 |  | 4 | 21 | $5!$ | 7－909 |
| 80 | 110 | 0；50 |  | $\xi$ | $\check{\square}$ | 67 | 9720 |
| 80 | 120 | 11：50 |  | 11 | 21 | $E$ | 115－ |
| 80 | 120 | 9：50 |  | 1.4 | $\Xi$ | 95 | 132： 20 |
| 80 | 140 | 0； 50 |  | 15 | 3 | 101 | 1500 |
| 80 | 150 | i1： 50 |  | 13 | $4 \dot{5}$ | 115 | 180．20 |
| 80 | 100 | 9：50 |  | 17 | 5 | 159 | $\therefore \therefore 20$ |
| 60 | 170 | $0: 50$ |  | 2 | 6 | 15 | 24＊${ }^{-1}$ |
| 60 | 130 | 19：4i1 | 1 | $2 \%$ | $\bar{i}$ | 167 | ごミご， |
| E0 | 170 | 10：4 | $z$ | Si！ | 35 | 15ら | 可安： |
| 80 | 2010 | 11：411 | $z$ | 34 | 43 | 14－ |  |
| 80 | 210 | 0：40 | $\square$ | 37 | 100 | 213 | 3世6： |
| $E 0$ | 220 | 01910 | 4 | 4 | 1110 | 245 | 75.30 |
| Ei | 270 | i1：4i1 | － | $\therefore:$ | 111 | $\because 4$ | $4, \square!$ |
| E0 | 2411 | 0：40 | ： | \％ | 107 | $\therefore \because$ | $45-$－ |
| G0 | 25 | 0：40 | 11 | $\therefore=$ | 124 | E－ | $4 \mathrm{~A}, ~-1$ |
| 80 | 261 | 6：111 | 1： | － 4 | 13－ | ．-1 | $\therefore \therefore^{-1}$ |
| 80 | 270 | 4． 410 | 1 | \％ | 15. | Fic | $0.1+\cdots$ |

TGLPY MAMSG iFEET
「OATA FISEOFO天 IN MITPOGEN RQTES: DESCENT 60 FPM; ASCENT 60 FPM


| 90 | 2 | 1:30 |  |  |  | 0 | 1:30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 30 | 1:20 |  |  |  | 1 | 2:30 |
| 90 | 40 | 1:20 |  |  |  | 13 | 14:30 |
| 90 | 5 | 1:10 |  |  | 5 | 20 | 26:30 |
| 90 | e. 0 | 1:10 |  |  | 15 | 21 | 37:30 |
| 90 | $i 0$ | 1:00 |  | 2 | 22 | 21 | 46:30 |
| 11 mat | line |  |  |  |  |  |  |
| 90 | 30 | 1:00 |  | 10 | 21 | 42 | 74:30 |
| Fi | 94 | 1:00 |  | 16 | 21 | 61 | 99:30 |
| $\rightarrow 1$ | 100 | 1:00 |  | 21 | 22 | 79 | 123:30 |
| 90 | 110 | $0 ; 50$ | 4 | 22 | 23 | 97 | 147:30 |
| 90 | 120 | $0: 50$ | 8 | 22 | 38 | 103 | 172:30 |
| 90 | 130 | 0:50 | 11 | 22 | 55 | 125 | 214:30 |
| 90 | 140 | 0; 50 | 14 | 21 | 71 | 146 | 253:30 |
| 90 | 150 | $0: 50$ | 16 | 25 | 83 | 166 | 291:30 |
| 90 | 100 | 0:50 | 18 | 30 | 92 | 186 | 327:30 |
| 90 | 170 | 0; 50 | 20 | 36 | 100 | 207 | 364:30 |
| 90 | 150 | $0 \cdot 50$ | 21 | 49 | 101 | 2.35 | 407:30 |
| $-90$ | 190 | 0:40 | 123 | 61 | 101 | 263 | 450:30 |
| 100 | 24 | 1:40 |  |  |  | 0 | 1:40 |




UEFTH ETM TM TU （FSW）TIM FIRET （M）ETGF
 $100 \quad 25 \quad 1: 30$
$100301: 30$
$10035 \quad 1: 20$
$100 \quad 40 \quad 1: 20$
$10045 \quad 1: 20$
$10050 \quad 1: 10$
$10055 \quad 1: 10$
$10060 \quad 1: 10$
$100651: 10$

1 （11） $751: 00 \quad 1 \quad 212150.90$
$100 \quad 80 \quad 1: 00$
$100 \quad 90 \quad 1: 00$ 11 28 21 $\because 0$ 145：40
$100100 \quad 1: 00$
$172 \boldsymbol{3} 300170: 40$
$1001100: 50 \quad 122 \quad 21 \quad 59122 \quad 220: 40$

| 110 | 20 | $1: 50$ | 0 |
| :--- | :--- | :--- | :--- |

1i0 25 $1: 40 \quad$ 日 ヨ ヨ
$110301: 30$ 4 19 16： 0
$\begin{array}{llll}110 & 35 & 1: 30 & 10 \\ 15 & \text { E®：} 50\end{array}$
$110401: 20411 \quad 49$

linit line－－－．

|  | 11 | 18 | 21 | $51: 50$ |
| :---: | :---: | :---: | :---: | :---: |
| 3 | 11 | 22 | 24 | $61: 50$ |
| 6 | 15 | 21 | 40 | $83: 50$ |

G－9

TELFI VVALSG GFEET

- OTM FIMFE FRE IN NITROGEN RATES: [DESEENT $6 O$ FFM; ASCENT 60 FFM



TEIFY ，GOEG FEET


DEPTH ETM TM TO〔FSU〕 TIN FINGT （H）STGF


130 60 ：10


$150 \quad 10 \quad 2: 30$

| 150 | 15 | $\bar{z} 10$ |  |  | $z$ | 5 | $\cdots: 30$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 | 20 | ¢ 00 |  | $z$ | 5 | 11 | $\because 30$ |
| 150 | 25 | $\therefore 80$ |  | 11 | 1. | 17 | 5r 311 |
| 150 | 50 | 1：50 | $\because$ | 11 | 11 | 14 | $9 \mathrm{E}=11$ |
| limjt． | 11 me |  |  |  |  |  |  |
| 150 | 55 | 1．4i1 | 1 | 11 | 1.1 | 24 | E， 30 |


| 150 | 40 | 1：30 |  | $\therefore$ | 11 | $1 i$ | 1 i | $2 i$ | 45 | 19， 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 | 45 | 1：30 |  | 3 | 11 | 11 | $1-$ | $\because \dagger$ | 71 | 14： 96 |
| 150 | 50 | 1：c！ | $\bar{\square}$ | 11 | 1. | 11 | $\therefore$ | $\therefore i$ | $3:$ | 1－9 |
| 150 | 60 | －\％ | 11 | 11 | 11 | $\therefore$ | $\therefore{ }^{1}$ | － | $i \because$ | － 24.11 |
| 150 | 70 | 1：10 | e 11 | 11 | － | $\therefore$ | $\therefore 1$ | FF | $17:$ | そ－：〒－ |

TELF1 YYALSG《FEET ？
PO ATH FINEO FOZ IN NITRUSEN RATES：OESEENT 60 FPM；ASCENT EO FFM


| $\begin{gathered} 120 i t \\ 160 \end{gathered}$ | 11 9 | $2: 40$ |  |  |  |  |  |  | 10 |  | 2：40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 160 | 10 | $2 \cdot 30$ |  |  |  |  |  |  |  | 1 | 3：40 |
| 100 | 15 | $2: 10$ |  |  |  |  |  | 1 | 3 | 7 | 13：40 |
| 160 | 20 | $2 \cdot 00$ |  |  |  |  | 1 | 4 | 10 | 10 | 27：40 |
| 160 | ご | 2：00 |  |  |  |  | 6 | 11 | 10 | 15 | 44：40 |
| 160 | 30 | 1：5010 |  |  |  | 5 | 11 | 11 | 11 | ¿1 | 61：40 |
| 100 | 40 | 1：411 |  |  | 11 | 11 | 11 | 13 | 22 | 66 | 136：40 |
| 169 | 50 | 1：20 | 1 | 11 | 11 | 11 | 15 | 22 | 39 | 103 | 215：40 |
| 1imst | lirie |  |  |  |  |  |  |  |  |  |  |
| 170 | $E$ | $2 \cdot 50$ |  |  |  |  |  |  |  | 0 | 2：50 |
| 179 | 111 | 2：411 |  |  |  |  |  |  |  | 3 | 5：50 |
| 170 | 15 | c： 10 |  |  |  |  | 1 | 3 | 3 | 8 | 17：50 |
| 170 | 20 | 200 |  |  |  | 1 | 3 | 5 | 11 | 11 | 33：50 |
| 170 | 25 | 2：00 |  |  |  | 3 | 9 | 11 | 10 | 18 | 53：50 |
| 10 | 34 | 1：50 |  |  | 1 | 11 | 11 | 11 | 13 | 27 | 76：50 |
| 179 | 40 | 1：411 |  | 8 | 11 | 11 | 11 | 17 | 22 | 86 | 168：50 |
| 176 | 50 | 1：30 | 10 | 11 | 11 | 11 | 20 | 21 | 64 | 136 | 280：50 |

$\square$

© VVALSE－HITEOCEN
T15SUF HELF－TJHF：

| GFFIti |  | 5．MIH | 10 MIH | 20 MJN | 40 MJN | 80 Mrti | 120 117\％ | 18\％MTH | －it Mn | 2ticmin |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ． 40 SiP | ． 50 SOF | 55 SOF | .9685 .5 | ． 96 SLF | ． 72 StF | 60 $-1 . F$ | 45． ECF | 40 Sif |
| 亏 | M\％ 4 | 126.670 | 114．670 | 77.900 | 61.510 | 54.600 | 51.70 | E日．¢0 | E0．4\％i | 50.170 |
| $\varepsilon$ | $\mathrm{H}+\mathrm{O}$ | 13E．513 | 124.513 | 86． 843 | 71.35 .3 | 64.643 | 61.543 | ¢ 4515 | －0． 0 ¢ | ＋19．013 |
| $\square$ | 11： 11 | 14E．355 | 134.355 | 96.655 | $81.1 \%$ | 74.465 | \％1．355 | F4， 5 | 70.105 | 69．555 |
| 17 | MS凩 | 156．178 | 144．148 | 146．528 | 91．038 | 94．329 | 91．223 | （4，15\％ | －3．7．12 | 73．63 |
| 13 | 1－1： | 166． 10.9 | 1.4 .040 | 116．370 | 100.890 | 94．170 | $91.0 \%$ | $\div 0.040$ | 29．790 | 85．54 |
| 18 | $\mathrm{H} \div \mathrm{H}$ | 175． 5 ¢ 3 | 163.823 | 1\％6．213 | 110.723 | 10.4013 | 100.915 | 95.853 | 95．535 | 95．383 |
| $\therefore 1$ | $\mathrm{N} \div 1 . \mathrm{H}$ | 185.725 | 173．725 | 136.055 | 120．555 | 113.855 | 110.755 | 107.75 | 107．4\％ | 109.225 |
| 4 | H\％6 | 195.548 | 183.508 | 145．535 | 1.30 .418 | 123．69\％ | 100.55 | 119.58 | 119218 | 11\％．06\％ |
| $\therefore \overrightarrow{1}$ | $\mathrm{H}-\mathrm{H}$ | 205．410 | 193．410 | 155．740 | 140．250 | 135．541 | 130，44i | 127.410 | 12\％．16il | 12\％．910 |
| － 1 | $\mathrm{M}=6 \mathrm{i}$ | 215．223 | 203.253 | 165．593 | 150.075 | 143．333 | 140.293 | 139．253 | 137003 | 137．75\％ |
| 53 | － | 225．8．35 | 213.195 | 175．425 | 159.935 | 153．225 | 150．125 | 147．095 | 14\％．84 | 14－．555 |
| 3 | M 5 U | 234．938 | 222．338 | 185．263 | 163．77\％ | 163，063 | 159．783 | 158．738 | 15e．683 | 15＊．433 |
| 35 | M， | 244．780 | 232．789 | 195．110 | 175．625 | 172.910 | 167.810 | 168．780 | 16350 | 16\％．280 |
| $4:$ | $\mathrm{M}<\mathrm{H}$ | ご54．6こ3 | こ4こ．Eこ3 | ¢014 953 | 189．465 | 18\％．75 | 179．853 | 17E E23 | 1里，37 | 1洨．123 |
| 45 | $\mathrm{N}=14$ | 264.455 | 252．445 | 214.705 | 199．305 | 192.595 | 189．4．5 | 189．465 | 189．215 | 187．955 |
| 4：4 | $\mathrm{N}=1: 1$ | 274，303 | 262.309 | 224.633 | 209，14＊ | 20\％．435 | 193．539 | 195． 30 | $192.05 \%$ | 147.803 |
| 51 | NSW | 234.150 | 272．150 | 234.481 | 218.990 | 212.280 | 207.180 | 208.150 | 207.700 | 205.650 |
| 5.4 | MSH | 293.953 | 281．933 | 244.323 | 228．853 | 222．123 | 219.023 | 217．973 | 217．74 | 217．473 |
| 57 | H8， | 303.836 | 291．836 | 254．15 | 238.65 | 231.955 | 2c8． 65 |  | $227.53 \%$ | ここけ．335 |
| ＋9 | MSい | 313.678 | 301.678 | 264．009 | 248．518 | 241.809 | 238.702 | 237．673 | こ5．429 | 257．178 |
| $E$ | $1: 5$ | 323．5．1 | 311.521 | 272850 | 258，350 | 2E1．E50 | 249.550 | 二47，50 | $\therefore+7.5-0$ | 24．020 |
| ¢ 8 | 17－1．1 | 335．363 | 321．36： | 253．695 | 260.205 | ＜61．4．3 | 258.393 | こrs． 5 ¢ | O7．113 | 256．853 |
| 8.7 | 15：4 | 34.3 .206 | 331.206 | 2\％3．536 | 278．04t | 271．336 | こex．est | $=0.7 .206$ | Ste． 95 | 266.705 |
| 72 | $\mathrm{H} \because \mathrm{Cl}$ | 353.048 | 34：．048 | 313.375 | 287．228 | 281．178 | 275．076 | こ「こ．049 | 2－6．750 | 276．54\％ |
| $\cdots$ | M－n | 352．891 | 350.231 | 313.221 | 2Ч：．331 | 291.021 | 28？．921 | 236.841 | 2世6．641 | 285．351 |
| 7\％ | M：10 | 372.833 | 360.733 | 322，06．3 | 307.573 | 300.863 | 29：．763 | 296.753 | 296．483 | 296．233 |
| $\because$ | M．M | 382596 | 370，57t | 328．90\％ | 317．416 | 310．706 | 317．60\％ | Ereser | 30e 20 | 304．076 |
| E． | H：1 | 352．419 | 380.418 | 34E． 745 | 327．25s | 320.545 | 317.44 | $316+13$ | 315．16\％ | 315.913 |
| ¢－ | M： 1.4 | 40.26 .1 | 390.261 | 35．2．591 | 355．111 | 330，391 | 3こう．291 | こと心．ct 1 | 326．011 | 5こ． 761 |
| 50 | M -1.1 | 412.103 | 400.103 | 362．433 | 346，943 | 34n．233 | 337．133 | 336.103 | 335.853 | 335，607 |

ELOUR FPFHMETEF：

 1．i！2．t！

| cavor | 2.39 | 2.35 | 2.39 | 2.35 | 2.35 | 2.37 | 2.35 | 2.39 | 2.39 | （VIL $\therefore$ ） |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ruros | 1.87 | 1.87 | 1.87 | 1． 27 | 1．87 | 1.87 | 1．37 | 1．ar | 1．87 | （FSts： |
| PGMT | 36． 610 | 35.00 | \％ 9.10 | 13．0n | 10.00 | \％，\％10 | $\therefore$－0\％ | 7 ，itir | T．00 | ＇Fid |

TBLF 1 YQAS AMETEES




## TELFI VUALSG ©METERS

.70 ATA FISED POQ IH NITROEEA RATES: DESEENT 20 MFH: ASCENT 20 MFM


| 15 | 370 | $0: 36$ |
| :--- | :--- | :--- |
| 15 | 380 | $0: 36$ |
| 15 | 390 | $0: 36$ | $109109: 45$


| 18 | 79 | $0: 54$ | 0 | $0: 54$ |
| :--- | :--- | :--- | :--- | :--- |
| 18 | 80 | $0: 45$ | 3 | $3: 54$ |
| 18 | 90 | $0: 45$ | 6 | $6: 54$ |
| $1:$ | 100 | $0: 45$ | 9 | $9: 54$ |
| 18 | 110 | $0: 45$ | 11 | $11: 54$ |


| 18 | 120 | $0: 45$ |
| :--- | :--- | :--- |
| $16: 54$ |  |  |


| 18 | 130 | $0: 45$ |
| :--- | :--- | :--- |
| $21: 54$ |  |  |


| 13 | 140 | $0: 4$ |
| :--- | :--- | :--- |
| $28: 54$ |  |  |


| 18 | 150 | $0: 45$ |
| :--- | :--- | :--- |$\quad 38 \quad 38,54$


| 160 | 60 | $48: 54$ |
| :--- | :--- | :--- |


| 18 | 170 | 0 |
| :--- | :--- | :--- | $45 \quad 57 \quad 57: 54$


| 13 | 180 | $0: 36$ |
| :--- | :--- | :--- |
| $65: 54$ |  |  |


| 18 | $19: 36$ | 3 | 70 |
| :--- | :--- | :--- | :--- |

$18 \quad 200 \quad 0: 36 \quad 6 \quad 65 \quad 81: 54$

| 18 | 210 | $0: 36$ |
| :--- | :--- | :--- |$\quad 9 \quad 81 \quad 90: 54$


| 13 | 220 | $0: 36$ | $11 \quad 90 \quad 101: 54$ |
| :--- | :--- | :--- | :--- |


| 18 | 230 | $0: 36$ |
| :--- | :--- | :--- |$\quad 14 \quad 97 \quad 111: 54$


| 13 | 240 | $0: 36$ |
| :--- | :--- | :--- |$\quad 16 \quad 106 \quad 122: 54$


| 18 | 250 | $0: 36$ |
| :--- | :--- | :--- | $20 \quad 118 \quad 138: 54$


| 18 | 260 | $0: 36$ | 25 |
| :--- | :--- | :--- | :--- |
| 129 | $154: 54$ |  |  |


| 18 | 270 | $0: 36$ | 30 | 139 | 169,54 |
| :--- | :--- | :--- | :--- | :--- | :--- |

TBLFI WWH! 9 ©METEF:
. PO ATA FIXED PQZ IN NITROEEN FATES: DESEENT 20 MFM: GEOENT ZO MFN $\begin{aligned} & \text { DEPTH BTM TM TO } \\ & \text { (MSN) } \text { TIM FIRST } \\ & \text { (H) STUF } \\ & \text { (M:S) }\end{aligned}$

DECOMFFESSION STOPS (MSW:
STOP TIMES (HIN)
$36 \quad 33 \quad 30$
$33-20 \quad 27$ $\begin{array}{lllll}24 & 21 & 18 & 15 & 12\end{array}$

TOTAL HETENT

TIME
6M:5)


TBLFI WVALSG (METEFS:

FO HTA FIXED FOE IN HITRUGEN RATES: DESEENT 20 MFM; ASCENT 20 MPM

| DEFTH | ETM | TM TH |  |  |  | 0 | F.E | S10 | Sto | 5 | 15u |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\because$ MSW | T1M | FIFST |  |  |  |  | OF | TIME | ( | H |  |  |  |  | ASCENT |
|  | (H) | STuF |  |  |  |  |  |  |  |  |  |  |  |  | TIME |
|  |  | - M: S | 3 r | 33 | 30 | 27 | 24 | 21 | 18 | 15 | 12 | 9 | 0 | 3 | (M:S) |


| < 1 | $1 \%$ | 19:4 ${ }^{\text {F }}$ |  | 29 | 9u | 120:03 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11mı | 11re |  |  |  |  |  |
| cı | 1*1: | 11: 45 |  | 33 | 102 | 136:03 |
| 21 | 190 | 0. 36 | 1 | 41 | 115 | 158:0.3 |
| 21 | 200 | 6: 36 | 1 | 50 | 130 | 182:03 |
| 21 | 210 | 0:300 | 2 | 58 | 143 | 204:03 |
| 21 | 2゙シ | 9, 36 | 5 | 64 | 156 | 226:03 |
| 21 | 230 | 0:36 | 8 | 68 | 169 | 246:0.3 |
| $\because 1$ | 240 | $0: 36$ | 10 | 74 | 181 | 266:03 |
| $\therefore 1$ | 250 | $0: 36$ | 13 | 78 | 193 | 235:03 |
| $\therefore 1$ | 260 | $0: 36$ | 15 | 82 | 210 | $308: 03$ |
| $\because 1$ | 270 | $0: 36$ | 17 | 36 | 227 | 331: 03 |
| $\cdots 1$ | 200 | 0.30 | 19 | 95 | 238 | 353:03 |
| 21 | 290 | 0:36 | 22 | 101 | 251 | 375:03 |
| 21 | 300 | 0:36 | 27 | 106 | 263 | 397:03 |
| 21 | 310 | 0, 36 | 32 | 110 | 275 | 418:03 |
| 21 | $3 \div 0$ | $0: 36$ | 36 | 119 | 283 | 4.39:03 |
| 21 | 351 | 11:36 | 41 | 129 | 288 | 459:03 |
| 21 | 340 | 0.36 | 45 | 139 | 294 | 479:03 |
| -21 | 350 | 10:36 | 49 | 149 | 299 | 498:03 |


| 24 | 29 | $1: 12$ |
| :--- | :--- | :--- |
| 24 | 40 | $1: 03$ |
| 24 | 50 | $1: 03$ |
| 24 | 60 | $1: 03$ |
| 24 | 70 | $0: 54$ |


|  | 0 | $1: 12$ |
| ---: | ---: | ---: |
| 1 | $2: 12$ |  |
|  | 10 | $11: 12$ |
|  | 18 | $1 \xi: 12$ |
| 6 | 19 | $2 \epsilon: 12$ |

G-18

TBLFI WYHLEO METEFS
7 A ATA FIXED FGZ IN NITEUGEN FATES: DESEENT ZU MFH: ASCEMT 天U MFM $\begin{aligned} & \text { DEPTH ETM TM TG } \\ & \text { (MSW) } \text { TM FIFST } \\ & \text { (M) } \text { STGP } \\ & \text { (M:S) }\end{aligned}$ [DEOUFFESS]DN STDFS EMEM: STOF TIMES (MTN)

Tital AEEET


| 24 | 80 | 0:54 |  |  | 12 | 20 | $33: 12$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 24 | 90 | 0:54 |  |  | $1 \overrightarrow{1}$ | 25 | 4 C |
| 24 | 100 | 0:45 |  | 2 | 19 | 45 | E. $0^{\text {a }}$ |
| limit | line |  |  |  |  |  |  |
| 24 | 110 | 0:45 |  | 5 | 19 | en | $E \cdot 12$ |
| 24 | 120 | 0:45 |  | E | 21 | \% | 1020 |
| 24 | 130 | 0:45 |  | 11 | 25 | 28 | 19:18 |
| 24 | 140 | 0.45 |  | 13 | 311 | 96 | 144: 1 |
| 24 | 150 | 0:45 |  | 14 | 41 | 109 | 104:15 |
| 24 | 160 | 0:45 |  | 16 | 5 | 12i | 15e:12 |
| 24 | 170 | 0:45 |  | 19 | E1 | 145 | 2-5:12 |
| 24 | 180 | $0: 45$ |  | $\therefore 4$ | Qis | 157 | 20:13 |
| 24 | 190 | 0:45 |  | 29 | 75 | 173 | $283 \cdot 12$ |
| 24 | 200 | $0 ; 36$ | 1 | $\square 2$ | 22 | 194 | $310: 12$ |
| 24 | 210 | 0:36 | 1 | 30 | 88 | 21.3 | 35: 12 |
| 24 | 220 | 0:36 | 2 | 40 | 95 | 2.5 | $3 \mathrm{B0} 12$ |
| 24 | 230 | $0 \cdot 36$ | 2 | 50 | 95 | 25: | 4 n : 2 |
| 24 | 240 | 0136 | 5 | 5 | 195 | 267 | 474:12 |
| 24 | 250 | 0:36 | 9 | $\theta 1$ | 117 | 278 | $40^{5}$ - 12 |
| 24 | 260 | 0:36 | 10 | GA | 132 | 286 | $495 \cdot 12$ |
| 24 | 270 | 0:36 | 15 | Fi | 14 m | 29 | 59 E |
| 24 | 250 | 0:36 | 15 | it | 159 | 300 | $5.51: 12$ |
| 24 | 290 | 0:36 | 17 | z0 | 172 | 30 | ETE: 1 |
| 24 | 300 | 0:36 | 19 | 8.4 | 154 | 314 | 602:1? |
| 24 | 310 | 0:36 | 20 | 4 | 196 | 310 | 825:12 |

TBLPI VYALSG《METERS〉
PO ATA FIXIEO POE IN NITRUGEN RATES: DESCENT 20 MPM; ASCENT 20 MPM



TELFI MYBLEE METEEG
PO ATA FISED FGE IN NITROGEH FGTES: DESCEHT 20 MFH: AEGENT ËO MFM



TELPI $/$ YALSG GMETERS:
PO ATA FIKED POZ IN NITRDGEN RATES: OESEENT 20 MFH: ASCENT 20 MPM


| 30 | 20 | 1:39 |  |  |  |  | 4 |  | $5: 48$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Te | -5 | 1:30 |  |  |  |  | 2 | 11 | 14:48 |
| SE | 90 | 1:30 |  |  |  |  | 10 | 11 | 22:48 |
| 36 | 3 | 1:ci |  |  |  | 5 | 11 | 13 | 30:48 |
| 36 | $4 \%$ | 1:21 |  |  |  | 11 | 10 | 17 | 37:48 |
| $\begin{gathered} \text { limit } \\ 36 \end{gathered}$ | $11 \mathrm{n}=$ 45 | 1:12 |  |  | 5 | 10 | 12 | 19 | 47:48 |
| 36 | 50 | 1:12 |  |  | 5 | 11 | 16 | 26 | 62:48 |
| 36 | 55 | 1:0.3 |  | 1 | 11 | 11 | 18 | 42 | 84:48 |
| 56 | 619 | 1:0.3 |  | 3 | 11 | 15 | 19 | 55 | 104;48 |
| 36 | 70 | 1:03 |  | 8 | 13 | 19 | 21 | 82 | 144:48 |
| 36 | 80 | 1:03 |  | 12 | 18 | 19 | 38 | 102 | 190:48 |
| 39 | 16 | 1:57 |  |  |  |  |  | 0 | 1:57 |
| 39 | 20 | 1:48 |  |  |  |  |  | 9 | 10:57 |
| 39 | 25 | 1:39 |  |  |  |  | 8 | 11 | 20,57 |
| 35 | 34 | 1:30 |  |  |  | 6 | 11 | 10 | 28:57 |
| 39 | 3 | 1:21 |  |  | 2 | 11 | 11 | 14 | 39:57 |
| 37 | 4 | 1:21 |  |  | 8 | 11 | 10 | 18 | 48:57 |
| limit. | line |  |  |  |  |  |  |  |  |
| 35 | 45 | 1:12 |  | 2 | 11 | 11 | 13 | 29 | 67:57 |
| 37 | 50 | 1:12 |  | E | 11 | 11 | 17 | 46 | 92:57 |
| 3.4 | 60 | 1:03 | 2 | 11 | 11 | 17 | 19 | 78 | 139:57 |
| -39 | 70 | 1:03 | 7 | 11 | 17 | 19 | 36 | 101 | 191:57 |
| $4{ }^{\circ}$ | 13 | 2;06 |  |  |  |  |  | 0 | 2:06 |
| 42 | 15 | $\therefore: 57$ |  |  |  |  |  | 2 | 4:06 |
| $4 \%$ | 20 | 1:4\% |  |  |  |  | 4 | 10 | 16:06 |

TELP $\quad$, VMS




$46451: 24 \quad 11111011$ 19 Ta 13E:18



$48 \quad 1$ is z:15 $\quad 1 \quad 3: \overline{4}$


$48251: 48 \quad 5 \quad 11 \quad 1011 \quad 39: 24$
$48301: 39 \quad 5 \quad 10111115 \quad 54: 24$


$51102: 24 \quad 7 \quad 5: 33$

$51201: 48 \quad 1 \quad 3 \quad 4 \quad 1111$ 30:33

$51301: 4 \theta \quad 11111111$ 2e 58:34

$51 \quad 50 \quad 1: 21$
9111011131959127 E1:3

TBLPI VWALSG (METERS)
PO ATA FIXED FO2 IN NITROGEN RATES: DESCENT 20 MPM; ASCENT 20 MPM


$45112: 15 \quad 0 \quad 0 \quad 2: 15$
$451: 57 \quad 1 \begin{array}{ll}45 & 15\end{array}$

$45 \quad 251: 48 \quad 10 \quad 10 \quad 11 \quad 33: 15$


| 46 | 10 | $2: 18$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 46 | 15 | $2: 10$ |
| 46 | 20 | $1: 51$ |
| 46 | 25 | $1: 42$ |
| 46 | 30 | $1: 42$ |


| PHASE I \& II DIVE PROFILE COMPARISON |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PROFILE 1 (175/30)*2; 10/60 |  |  |  |  |  |
| Stops (FSW) | MVALI | MVAL2 | \# MVAL3 | VVAL29 | VVAL59 |
| 175 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 70 | --- | --- | --- | 0.87 | --- |
| 60 | --- | 0.09 | 1.38 | 2.82 | 10.28 |
| 50 | 1.45 | 2.52 | 3.26 | 3.30 | 10.90 |
| 40 | 5.09 | 6.02 | 6.51 | 6.38 | 10.90 |
| 30 | 7.70 | 6.91 | 10.06 | 11.04 | 10.90 |
| 20 | 16.90 | 16.37 | 17.51 | 14.87 | 19.08 |
| 10 | 60.00 | 60.00 | 60.00 | 60.00 | 60.00 |
| 175 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 70 | --- | --- | --- | 0.69 | 3.18 |
| 60 | --- | 0.01 | 1.30 | 2.82 | 10.90 |
| 50 | 1.37 | 2.52 | 3.20 | 2.82 | 10.90 |
| 40 | 5.12 | 6.05 | 6.51 | 8.68 | 10.90 |
| 30 | 13.82 | 12.32 | 15.51 | 19.95 | 19.96 |
| 20 | 23.13 | 28.95 | 30.76 | 80.44 | 96.09 |
| 10 | 48.31 | 52.42 | 57.03 | 215.06 | 202.43 |
| TOTAL | 254.22 | 265.51 | 284.37 | 501.07 | 547.76 |
| RESULTS <br> (Dives/DCS) | 8/2 | 19/1 | 25/0 |  |  |

[^9]PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 2 175/60

| Stops <br> (FSW) | \# <br> MVAL1 | $\#$ <br> MVAL2 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 175 | 60.00 | 60.00 | 60.00 | 60.00 |
| 100 | -- | --- | $-\ldots$ | 3.63 |
| 90 | -- | $-\cdots$ | 3.11 | 10.90 |
| 80 | $-\ldots$ | -- | 6.38 | 10.90 |
| 70 | 1.09 | 3.23 | 8.80 | 10.90 |
| 60 | 6.51 | 5.37 | 14.87 | 17.10 |
| 50 | 13.42 | 12.88 | 14.87 | 21.45 |
| 40 | 14.40 | 14.40 | 19.52 | 21.45 |
| 30 | 18.35 | 24.61 | 52.29 | 65.46 |
| 20 | 36.15 | 36.92 | 85.09 | 100.04 |
| 10 | 55.14 | 59.26 | 263.10 | 257.57 |
|  |  |  |  |  |
| TOTAL | 210.88 | 222.50 | 533.85 | 585.23 |
| RESULTS | $10 / 3$ | $9 / 2$ |  |  |

[^10]$$
\mathrm{H}-2
$$

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 3 (150/30)*2; 30/120

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\stackrel{\#}{\text { MVAL2 }}$ | $\stackrel{\#}{\text { MVAL3 }}$ | $\stackrel{\text { \# }}{\text { MVAL5 }}$ | VVAL18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 |  | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 90 | --- | --- | 0.58 | --- | --- | --- |
| 80 | --- | --- | 1.52 | --- | --- | --- |
| 70 | --- | --- | 2.94 | -- | --- | --- |
| 60 | --- | --- | 3.56 | --- | --- | --- |
| 50 | --- | 0.65 | 3.77 | 2.33 | 0.19 | 2.54 |
| 40 | 2.23 | 3.22 | 7.69 | 6.94 | -2.82 | 10.90 |
| 30 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 | 120.00 |
| 150 | 30.00 | 30.00 | 30.00 | - 30.00 | 30.00 | 30.00 |
| 90 | --- | --- | 0.60 | --- | --- | --- |
| 80 | --- | --- | 1.52 | --- | --- | --- |
| 70 | --- | --- | 3.24 | --- | --- | --- |
| 60 | --- | --- | 3.56 | --- | --- | --- |
| 50 | --- | 0.89 | 5.08 | 3.37 | 0.60 | 9.56 |
| 40 | 3.70 | 5.02 | 8.16 | 14.89 | 4.89 | 10.90 |
| 30 | 9.27 | 12.78 | 11.85 | 28.26 . | 14.87 | 16.38 |
| 20 | 24.83 | 26.93 | 20.38 | 31.04 | 56.19 | 55.07 |
| 10 | 50.25 | 54.72 | 44.88 | 72.84 | 115.91 | 137.85 |
| total | 279.28 | 293.20 | 308.32 | 348.67 | 384.47 | 432.20 |
| RESULT <br> (Dives | $\text { ocs })^{8 / 0}$ | 39/1 | 28/0 |  |  |  |

\# Profiles actually tested.

## PHASE I \& II DIVE PROFILE COMPARISON

 PROFILE $4(125 / 30) * 3 ;(10 / 30) * 20$| Stops <br> (FSW) | MVAL2 | MVAL3 | MVAL5 | VVAL 18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 125 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 70 | --- | - | 0.76 | --- | - | - |
| 60 | --- | --- | 1.86 | --- | --- | --- |
| 50 | --- | --- | 3.77 | - | --- | - |
| 40 | --- | -- | 4.00 | --- | - | --- |
| 30 | 1.78 | 3.09 | 7.44 | 0.71 | --- | 5.87 |
| 20 | 7.05 | 7.81 | 9.24 | 10.85 | 5.52 | 10.90 |
| 10 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 125 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 70 | -- | --- | 0.75 | --- | --- | -- |
| 60 | -- | - | 1.80 | --- | --- | - |
| 50 | --- | - | 3.77 | --- | --- | -- |
| 40 | --- | - | 4.00 | 4.47 | --- | 5.66 |
| 30 | 3.37 | 5.52 | 8.67 | 28.26 | 8.71 | 12.44 |
| 20 | 14.84 | 17.51 | 15.48 | 28.26 | 14.87 | 21.45 |
| 10 | - | - | 30.00 | 30.00 | 30.00 | 30.00 |
| 125 | - | -- | 30.00 | 30.00 | 30.00 | 30.00 |
| 70 | --- | --- | 0.75 | --- | --- | --- |
| 60 | --- | --- | 1.78 | --- | --- | --- |
| 50 | --- | --- | 3.77 | --- | - | --- |
| 40 | --- | --- | 4.00 | 4.47 | --- | 3.05 |
| 30 | 2.80 | 6.12 | 8.39 | 28.26 | 8.71 | 18.33 |
| 20 | 24.15 | 25.43 | 16.34 | 28.26 | 66.23 | 56.64 |
| 10 | 49.71 | 53.69 | 41.27 | 60.84 | 164.39 | 156.76 |
| TOTAL | 265.53 | 280.99 | 299.69 | 356.23 | 430.27 | 452.93 |
| RESULTS <br> (Dives/ | $\text { DCS }{ }^{10 / 0}$ | $37 / 2$ | 40/0 |  |  |  |

[^11]
## PHASE I \& II DIVE PROFILE COMPARISON

```
PROFILE 5 (75/30)*5 ; (10/15)*4
```

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\stackrel{\#}{\text { MVAL2 }}$ | $\begin{gathered} \# \\ \text { MVAL3 } \end{gathered}$ | $\stackrel{\#}{\text { MVAL5 }}$ | WALI8 | WVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 75 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 30 | --- | --- | 1.29 | --- | --- | --- |
| 20 | --- | --- | 4.17 | --- | --- | --- |
| 10 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 |
| 75 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 30 | --- | --- | 1.29 | --- | --- | --- |
| 20 | --- | --- | 4.87 | --- | --- | --- |
| 10 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 |
| 75 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 30 | --- | --- | 1.29 | --- | --- | --- |
| 20 | --- | --- | 5.39 | --- | --- | --- |
| 10 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 |
| 75 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 30 | --- | - | 1.29 | --- | --- | --- |
| 20 | --- | 0.58 | 5.39 | 10.40 | --- | 5.77 |
| 10 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 |
| 75 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 |
| 30 | --- | --- | 1.29 | --- | --- | --- |
| 20 | --- | 1.66 | 5.39 | 10.91 | 4.33 | 6.37 |
| 10 | 36.30 | 43.00 | 24.58 | 57.65 | 84.32 | 90.32 |
| TOTAL | 257.47 | 266.40 | 277.40 | 300.12 | 309.82 | 326.63 |
| RESULT <br> (Dives | $D C S)^{7 / 0}$ | 18/0 | 30/0 |  |  |  |

\# Profiles actually tested.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 6 ( $150 / 60$ )

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\stackrel{\#}{\text { MVAL2 }}$ | $\stackrel{\text { M }}{\text { MVL3 }}$ | MVAL 4 | $\stackrel{\#}{\text { MVAL5 }}$ | VVAL18 | $\begin{gathered} \text { F } \\ \text { VVAL29 } \end{gathered}$ | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 | 60.00 | 60.00 | 60.00 | 60.00 | 60.00 | 60.00 | 60.00 |
| 100 | ---- | ---- | ---- | 0.03 | ---- | ---- | -- |
| 90 | ---- | ---- | ---- | 1.59 | ---- | - | ---- |
| 80 | ---- | ---- | ---- | 3.19 | ---- | ---- | 1.28 |
| 70 | ---- | -- | ---- | 5.71 | 5.31 | 1.73 | 10.90 |
| 60 | 0.86 | 3.12 | 4.48 | 7.26 | 14.05 | 6.67 | 10.90 |
| 50 | 5.80 | 7.65 | 9.80 | 7.69 | 26.20 | 14.87 | 13.86 |
| 40 | 12.58 | 15.09 | 16.22 | 14.74 | 28.26 | 14.87 | 21.45 |
| 30 | 15.55 | 16.21 | 17.50 | 17.50 | 28.26 | 18.10 | 21.45 |
| 20 | 30.91 | 33.60 | 40.38 | 26.77 | 33.92 | 62.30 | 67.55 |
| 10 | 43.32 | 53.34 | 63.07 | 42.80 | 78.31 | 112.81 | 141.49 |
| TOTAL | 179.02 | 194.01 | 216.46 | 192.28 | 279.31 | 296.35 | 353.88 |
| RESULT <br> (Dives |  | 38/4 | $10 / 1$ | 20/3 |  | $9 / 2$ |  |

\# Profiles actually tested.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 7 150/45

| $\begin{gathered} \text { Stops } \\ \text { (FSW) } \end{gathered}$ | $\stackrel{\#}{\text { MVAL5 }}$ | VVAL18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 150 | 45.00 | 45.00 | 45.00 | 45.00 |
| 100 | 0.01 | --- | --- | --- |
| 90 | 0.76 | --- | --- | --- |
| 80 | 3.17 | --- | --- | --- |
| 70 | 3.36 | --- | - | 0.40 |
| 60 | 5.48 | 4.12 | --- | 10.90 |
| 50 | 7.69 | 14.05 | 6.38 | 10.90 |
| 40 | 8.16 | 17.30 | 10.43 | 10.90 |
| 30 | 15.26 | 28.26 | 14.87 | 18.47 |
| 20 | 18.63 | 28.26 | 18.46 | 21.45 |
| 10 | 33.87 | 38.11 | 73.33 | 81.32 |
| TOTAL | 146.38 | 180.10 | 174.68 | 204.34 |
| RESULTS (Dives/DCS) | 10/3 |  |  |  |

\# Profiles actually tested.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 8 100/60

| $\begin{aligned} & \text { Stops } \\ & (F S W) \end{aligned}$ | $\stackrel{\#}{\text { MVAL5 }}$ | VVALI8 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 100 | 60.00 | 60.00 | 60.00 | 60.00 |
| 50 | 2.38 | --- | --- | --- |
| 40 | 5.78 | --- | --- | --- |
| 30 | 8.68 | 8.67 | 3.86 | 8.35 |
| 20 | 14.21 | 28.26 | 14.87 | 21.45 |
| 10 | 19.85 | 28.26 | 30.93 | 22.13 |
| total | 114.23 | 128.52 | 113.00 | 115.26 |
| RESULTS (Dives/DCS) | 10/1 |  | 27/0 |  |

[^12]PhASE I \& II DIVE PROFILE COMPARISON
PROFILE 9 150/30

| $\begin{gathered} \text { Stops } \\ \text { (FSW) } \end{gathered}$ | MVAL5 | VVAL18 | VVAL29 | WAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 150 | 30.00 | 30.00 | 30.00 | 30.00 |
| 90 | 0.58 | --- | --- | --- |
| 80 | 1.52 | --- | --- | --- |
| 70 | 2.94 | --- | --- | --- |
| 60 | 3.56 | -- | --- | --- |
| 50 | 3.77 | 2.33 | 0.19 | 2.54 |
| 40 | 7.69 | 6.94 | 2.82 | 10.90 |
| 30 | 8.68 | 11.58 | 5.83 | 10.90 |
| 20 | 14.01 | 21.62 | 13.02 | 11.20 |
| 10 | 19.85 | 28.26 | 16.50 | 21.45 |
| TOTAL | 97.59 | 105.73 | 73.36 | 91.99 |
| RESULTS (Dives/DCS) | 20/0 |  | 19/0 |  |

\# Profiles actually tested.

PHASE I \& II DIVE PROFILE COMPARISON

## PROFILE 10 100/45

| Stops <br> (FSW) | $\stackrel{\#}{\text { MVAL5 }}$ | VVAL18 | WAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 100 | 45.00 | 45.00 | 45.00 | 45.00 |
| 50 | 1. ${ }^{\text {a }}$ | --- | --- | --- |
| 40 | 4.00 | --- | --- | --- |
| 30 | 7.18 | --- | --- | --- |
| 20 | 9.24 | 12.59 | 5.99 | 11.41 |
| 10 | 17.97 | 28.26 | 14.87 | 21.45 |
| TOTAL | 88.44 | 89.18 | 69.19 | 81.20 |
| RESULTS (Dives/DCS) | 20/0 |  |  |  |

\# Profiles actually tested.

|  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Profiles actually tested.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 12 75/120

| Stops <br> (FSW) | MVAL5 | VVAL18 | WVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
| 75 | 120.00 | 120.00 | 120.00 | 120.00 |
| 30 | 6.23 | -- | -1. | 1.46 |
| 20 | 16.79 | 28.12 | 15.33 | 21.45 |
| 10 | 28.25 | 52.12 | 67.60 | 66.04 |
| TOTAL | 173.75 | 202.74 | 205.43 | 211.45 |

\# Profiles actually tested.
$\mathrm{H}-12$

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 20 ( $60 / \mathrm{ND}$ )*3; $(0 / 80) * 2$

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\stackrel{\#}{\#}{ }_{\text {MVAL83 }}$ | $\begin{gathered} \# \\ \text { MVAL92 } \end{gathered}$ | $\stackrel{\#}{\text { MVAL97 }}$ | $\begin{gathered} \# \\ \text { VVAL14 } \end{gathered}$ | VVAL18 | WVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60 | 71.06 | 66.64 | 66.64 | 83.58 | 73.20 | 75.60 | 69.52 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 60 | 43.41 | 44.95 | 41.30 | $\begin{gathered} 22.45 \\ (31.84) \end{gathered}$ | $\begin{gathered} 23.18 \\ (34.75) \end{gathered}$ | 51.93 | 50.41 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 60 | 42.63 | 34.85 | 40.22 | $\begin{gathered} 16.05 \\ (25.95) \end{gathered}$ | $\begin{gathered} 23.18 \\ (30.27) \end{gathered}$ | 26.84 | 27.73 |
| total | 323.10 | 309.44 | 314.16 | $\begin{gathered} 288.08 \\ (307.37) \end{gathered}$ | $\begin{gathered} 285.55 \\ (304.22) \end{gathered}$ | 320.37 | 313.66 |
| RESULTS <br> (Dives) DCS) | 10/1 | 9/0 | 10/0 | 10/1 |  |  |  |

\# Profile actually tested.
Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1) and were used in tested profiles.

\# Profiles actually tested.
Times in parenthesis assume $30 \% \mathrm{O}_{2}$ at 1 ATA (See Note 1) and were used in tested profiles.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 22 ( $100 /$ ND)*4; (0/80)*3

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\begin{gathered} \# \\ \text { MVAL92 } \end{gathered}$ | $\begin{gathered} \# \\ \text { MVAL97 } \end{gathered}$ | $\begin{gathered} \# \\ \text { VVALO9 } \end{gathered}$ | $\begin{gathered} \# \\ \text { VVAL14 } \end{gathered}$ | VVAL18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 18.23 | 18.23 | 19.84 | 28.47 | 26.18 | 26.59 | 22.34 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 100 | 18.20 | 18.20 | $\begin{gathered} 10.59 \\ (14.56) \end{gathered}$ | $\begin{gathered} 5.78 \\ (9.79) \end{gathered}$ | $\begin{gathered} 5.48 \\ (9.36) \end{gathered}$ | 19.75 | 17.54 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 100 | 18.20 | 16.98 | $\begin{gathered} 5.86 \\ (9.36) \end{gathered}$ | $\begin{gathered} 5.78 \\ (9.79) \end{gathered}$ | $\begin{gathered} 5.48 \\ (9.36) \end{gathered}$ | 15.66 | 16.04 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 100 | 13.63 | 15.78 | $\begin{gathered} 5.48 \\ (9.36) \end{gathered}$ | $\begin{gathered} 5.78 \\ (9.79) \end{gathered}$ | $\begin{gathered} 5.48 \\ (9.36) \end{gathered}$ | 9.53 | 10.65 |
| total | 321.59 | 322.52 | $\begin{gathered} 295.11 \\ (306.45) \end{gathered}$ | $\begin{gathered} 299.14 \\ (311.17) \end{gathered}$ | $\begin{gathered} 295.96 \\ (307.59) \end{gathered}$ | 324.87 | 319.90 |
| RESULTS <br> (Dives) DCS) | 10/0 | 10/1 | 9/0 | 10/0 |  |  |  |

\# Profile actually tested.

Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1) and were used in tested profiles.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 23 ( $80 / \mathrm{NO}$ )*4; ( $0 / 80)^{* 2}$; ( $\left.0 / 60\right)^{* 1}$

| $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | $\stackrel{\text { MVAL97 }}{\text { \# }}$ | $\stackrel{\text { \# }}{\text { VVALO9 }}$ | VVALI8 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | 35.66 | 38.65 | 38.65 | 39.39 | 37.06 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 80 | 25.85 | $\begin{gathered} 9.46 \\ (15.27) \end{gathered}$ | $\begin{gathered} 9.46 \\ (15.27) \end{gathered}$ | 30.19 | 24.73 |
| 0 | 80.00 | 80.00 | 80.00 | 80.00 | 80.00 |
| 80 | 23.08 | $\begin{gathered} 9.46 \\ (14.45) \end{gathered}$ | $\begin{gathered} 9.46 \\ (15.27) \end{gathered}$ | 19.86 | 24.47 |
| 0 | 60.00 | 60.00 | 60.00 | 60.00 | 60.00 |
| 80 | 19.01 | $\begin{gathered} 6.25 \\ (9.15) \end{gathered}$ | $\begin{gathered} 7.29 \\ (11.8 i) \end{gathered}$ | :0.93 | 8.36 |
| total | 334.27 | $\begin{gathered} 294.48 \\ (308.19) \end{gathered}$ | $\begin{gathered} 295.52 \\ (311.73) \end{gathered}$ | 331.02 | 325.29 |
| RESULTS <br> (Dives/DCS) | 18/2 | 19/0 |  |  |  |

\# Profiles actually tested.

Times in parenthesis assume $30 \% \mathrm{O}_{2}$ at 1 ATA (See Note 1) and were used in tested profiles.


[^13]Times in parenthesis assume $30 \% 0_{2}$ at $\underset{H-17}{ } 1$ ATA (See Note 1 ).

| PHASE I \& II DIVE PROFILE COMPARISON |  |  |  |
| :---: | :---: | :---: | :---: |
|  | PROFILE 24A (150/30)*2; 0/80 |  |  |
| Stops (FSW) | VVAL18 | VVAL29 | VVAL59 |
| 150 | 30.00 | 30.00 | 30.00 |
| 50 | 2.33 | 0.19 | 2.54 |
| 40 | 6.94 | 2.82 | 6.94 |
| 30 | 11.58 | 5.83 | 11.58 |
| 20 | 21.62 | 13.02 | 21.62 |
| 10 | 28.26 | 16.50 | 28.26 |
| 0 | 80.00 | 80.00 | 80.00 |
| 150 | 30.00 | 30.00 | 30.00 |
| 40 | $\begin{gathered} 21.87 \\ (17.83) \end{gathered}$ | 2.82 | 10.90 |
| 30 | $\begin{gathered} 28.26 \\ (28.26) \end{gathered}$ | 11.14 | 11.79 |
| 20 | $\begin{gathered} 28.26 \\ (28.26) \end{gathered}$ | 37.40 | 38.53 |
| 10 | $\begin{gathered} 52.63 \\ (47.10) \end{gathered}$ | 92.34 | 113.67 |
| TOTAL | $\begin{gathered} 356.37 \\ (344.31) \end{gathered}$ | 332.24 | 387.17 |
| RESULTS <br> (Dives/DCS) | 10/1 |  |  |

[^14]Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1 ) but were not used in tested profiles.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 25A (100/60, 50) ; 0/80

|  | Stops <br> (FSW) | $\#$ <br> VVAL.18 | VVAL29 |
| :--- | :---: | :---: | ---: |$\quad$ VVAL59

\# Profiles actually tested.

Times in parenthesis assume $30 \% \mathrm{O}_{2}$ at 1 ATA (See Note 1) but were not used for tested profiles.

|  | PHASE I \& II DIVE PROFILE COMPARISON PROFILE 26 ( $80 / 90,85$ ) ; 0/60 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Stops } \\ & \text { (FSW) } \end{aligned}$ | VVAL18 | VVAL29 | VVAL59 |
|  | 80 | 90.00 | 90.00 | 90.00 |
|  | 20 | 25.32 | 12.55 | 20.86 |
|  | 10 | 35.68 | 42.45 | 35.67 |
|  | 0 | 60.00 | 60.00 | 60.00 |
|  | 80 | 85.00 | 85.00 | 85.00 |
|  | 20 | $\begin{gathered} 46.10 \\ (45.93) \end{gathered}$ | 44.33 | 2.07 |
|  | 10 | $\begin{gathered} 68.56 \\ (67.39) \end{gathered}$ | 159.27 | 51.25 |
| TOTAL |  | $\begin{gathered} 425.15 \\ (419.84) \end{gathered}$ | 498.93 | 150.63 |

Times in parenthesis assume $30 \% \mathrm{O}_{2}$ at 1 ATA (See Note 1 ).

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 27 ( $120 / \mathrm{ND}$ )*4; ( $0 / 80$ )*2 ; ( $0 / 60$ )*

|  | Stops <br> (FSW) | WVAL18 | VVAL29 |
| :--- | :---: | :---: | ---: |$\quad$ VVAL59

\# Profiles actually tested.

Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1) and were used
for tested profiles.

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 28 ( $140 /$ ND)*3; $(0 / 80) * 2 ;(0 / 60)$

|  | Stops <br> (FSW) | VVAL18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: | :---: |
|  | 140 | 10.67 | 12.85 | 10.61 |
|  | 0 | 80.00 | 80.00 | 80.00 |
|  | 140 | 5.96 | 12.25 | 9.63 |
|  | 0 | $(8.39)$ |  |  |
|  | 140 | 80.00 | 80.00 | 80.00 |
|  | 0 | $(4.44)$ | 10.30 | 9.31 |
|  | 140 | 60.00 | 60.00 | 60.00 |
|  |  | 1.30 | 3.26 | 6.46 |
|  |  | 258.96 | 277.33 | 274.68 |
|  |  | $(265.24)$ |  |  |

Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1).

PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 29 ( $150 /$ ND)*4; ( $0 / 80$ )*2; (0/60)*1

|  | Stops <br> (FSW) | VVALI8 | VVAL29 |
| :---: | :---: | :---: | ---: | WVAL59

Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1 ).
PHASE I \& II DIVE PROFILE COMPARISON
PROFILE 30 50/ND; $0.80 ; 80 /$ ND

| Stops <br> (FSW) | WVAL18 | VVAL29 | VVAL59 |
| :---: | :---: | :---: | :---: |
| 50 | 142.22 | 146.91 | 140.43 |
| 0 | 80.00 | 80.00 | 80.00 |
|  | 80 | 7.77 |  |
| $(13.15)$ | 16.88 | 18.35 |  |
| TOTAL |  | 234.32 | 248.13 |

\# Profiles actually tested
Times in parenthesis assume $30 \% 0_{2}$ at 1 ATA (See Note 1) and were used for tested profiles.

Note 1. During Phase II testing of the constant $\mathrm{C} .7 \mathrm{ATA} \mathrm{PO}_{2}$ in $\mathrm{N}_{2}$ Decompression Model, certain surface intervals were assumed to occur with the diver breathing a $30 \% \mathrm{O}_{2} \mathrm{mix}$. The times shown in parenthesis are those resulting from breathing this high $\mathrm{PO}_{2}$. Profiles $20,21,22,23,27$, and 30 were tested assuming that this higher $\mathrm{PO}_{2}$ was breathed during surface intervals. Note that this increase in $\mathrm{PO}_{2}$ was an adjustment to the computer program only, the divers actually breathed air during the surface interval but dove on the schedules indicated by the times in parenthesis. See reference (1) for details.

$$
12.86
$$


[^0]:    \# 360 min was the maximum time anticipated in developing USN Standard Air Decompression Limits.

[^1]:    * Maximum Depth/Time Limits: $60 / 180,100 / 90,120 / 60,150 / 40,190 / 30$
    \# Maximum Depth/Time Limits: $100 / 60,150 / 30$

[^2]:    O- Phase code $0=1 \mathrm{~A}, 1=1 \mathrm{~B}, 2=2,3=3$
    F-female

    * Divers who suffered symptoms of decompression sickness

[^3]:    @ Did Not Complete Dive

    * Decompression Sickness

[^4]:    *Profiles Actually Tested.

[^5]:    *Profiles Actually Tested.

[^6]:    *Profiles Actually Tested.

[^7]:    * Profiles Actually Tested.


    ## S.I. Surface Interval

    ND No Decompression

[^8]:    * Profiles Actually Tested.

[^9]:    \# Profiles actually tested.

[^10]:    \# Profiles actually tested.

[^11]:    \# Profiles actually tested.

[^12]:    \# Profiles actually tested

[^13]:    \# Profiles actually tested.

[^14]:    \# Profiles actually tested

