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# THE SHOCK AND VIBRATION DIGEST

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# LITERATURE REVIEW: survey and analysis of the Shock and Vibration literature

The monthly Literature Review, a subjective critique and summary of the literature, consists of two to four reviews each month, 3,000 to 4,000 words in length. The purpose of this section is to present a "digest" of literature over a period of three years. Planned by the Technical Editor, this section provides the **DIGEST** reader with up-to-date insights into current technology in more than 150 topic areas. Review articles include technical information from articles, reports, and unpublished proceedings. Each article also contains a minor tutorial of the technical area under discussion, a survey and evaluation of the new literature, and recommendations. Review articles are written by experts in the shock and vibration field.















101. Goldsmith, W., "Impact: the Collision of Solids," Applied Mech. Rev., 16, pp 855-866 (1963).
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103. Scott, R.A., "Linear Elastic Wave Propagation. An annotated bibliography; Parts I and II," Shock Vib. Dig., 10 (2/3), pp 25-41; 11-41 (1978).
104. Kolaky, H. Stress Waves in Solids, Clarendon Press, Oxford (1953).
105. Goldsmith, W., Impact: the Theory and Physical Behaviour of Colliding Systems, Edward Arnold Publ., London (1960).
106. Johnson, W., Impact strength of Materials, Edward Arnold, London (1972).
107. Miklowitz, J., The Theory of Elastic Waves and Waveguides, North Holland, Amsterdam (1978).





methods as numerical integration procedures and transfer matrix methods would have been desirable. In general, the book is easy to read and understandable. The extensive use of vector diagrams should lead to a better understanding by the reader of the component forces involved in mechanical vibrations. The graphic illustrations are well presented and easy to follow. A useful and novel aspect of the book is that it suggests

many simple experimental setups for observing various vibration phenomena. Working through these experiments would be an interesting way to learn the subject for those studying vibrations for the first time.

T.S. Sankar  
Concordia University  
Montreal, Canada













## AVAILABILITY OF PUBLICATIONS ABSTRACTED

None of the publications are available at SVIC or at the Vibration Institute, except those generated by either organization.

**Periodical articles, society papers, and papers presented at conferences** may be obtained at the Engineering Societies Library, 345 East 47th Street, New York, NY 10017; or Library of Congress, Washington, D.C., when not available in local or company libraries.

**Government reports** may be purchased from National Technical Information Service, Springfield, VA 22161. They are identified at the end of bibliographic citation by an NTIS order number with prefixes such as AD, N, NTIS, PB, DE, NUREG, DOE, and ERATL.

**Ph.D. dissertations** are identified by a DA order number and are available from University Microfilms International, Dissertation Copies, P.O. Box 1764, Ann Arbor, MI 48108.

**U.S. patents and patent applications** may be ordered by patent or patent application number from Commissioner of Patents, Washington, D.C. 20231.

**Chinese publications**, identified by a CSTA order number, are available in Chinese or English translation from International Information Service, Ltd., P.O. Box 24683, ABD Post Office, Hong Kong.

**Institution of Mechanical Engineers publications** are available in U.S.: SAE Customer Service, Dept. 676, 400 Commonwealth Drive, Warrendale, PA 15096, by quoting the SAE-MEP number.

When ordering, the pertinent order number should always be included, not the DIGEST abstract number.

A List of Periodicals Scanned is published in issues, 1, 6, and 12.

















































































M.J.L. Tierneho, A.M. Bos  
Twente University of Technology, Enschede, The Netherlands  
J. Franklin Inst., 319 (1/2), pp 37-50 (Jan/Feb 1985) 21 figs, 10 refs

**KEY WORDS:** Bond graph technique, Mathematical models

A method to model mechanical systems with multibond graphs is described. The method is based on the description of the vector velocity relation of a moving point in a rotating system. This relation is incorporated in a bond graph. It is explained how connected mechanical linkages must be handled. Two simple examples are presented.

86-933

**Determination of Normal Modes from Identified Complex Modes**

H.G. Natke, D. Rotert  
Curt-Risch-Institut für Dynamik, Schall- und Messtechnik der Universität Hannover, Fed. Rep. Germany  
Z. Flugwiss. Weltraumforsch., 2 (2), pp 82-88 (Mar/Apr 1985) 2 tables, 12 refs (in German)

**KEY WORDS:** System identification techniques, Normal modes, Damped modes

Cases occur in practice in which the measured eigenmodes of the damped elastomechanical system are available and normal modes are desired. This problem is solved by improving an existing computational model, using measured eigenquantities (incomplete and erroneous) in a sub-system formulation. This improved computational model is then used to compute the eigenquantities of the associated undamped system. Computational examples show the influence of errors.

**PARAMETER IDENTIFICATION**

86-934

**Application of a Method for Identifying Incomplete System Matrices Using Vibration Test Data (Anwendung der Identifikation unvollständiger Systemmatrizen aus Schwingungstestdaten)**

M. Link

Universität Gesamthochschule Kassel  
Z. Flugwiss. Weltraumforsch., 2 (3), pp 178-187 (May/June 1985) 9 figs, 2 tables, 4 refs (in German)

**KEY WORDS:** Parameter identification technique, Mass coefficients, Stiffness coefficients, Damping coefficients, Experimental data

In a preceding paper a theory of incomplete system matrix identification was presented. With this theory it is possible to identify the incomplete physical mass, stiffness and damping matrix as well as the modal characteristics of a structure from incomplete dynamic excitation. The excitation is called incomplete if the number  $r$  of excited modes is smaller than the number  $p$  of measuring degrees of freedom. In the present paper, two applications are presented.

86-935

**Theory of a Method for Identifying Incomplete System Matrices from Vibration Test Data (Theorie eines Verfahrens zur Identifikation unvollständiger strukturdynamischer Systemmatrizen aus Schwingungstestdaten)**

M. Link

Universität Gesamthochschule Kassel  
Z. Flugwiss. Weltraumforsch., 2 (2), pp 76-82 (Mar/Apr 1985) 5 refs (in German)

**KEY WORDS:** Parameter identification technique, Mass coefficients, Stiffness coefficients, Damping coefficients, Experimental data

A method is presented for the identification of the physical and modal mass, stiffness and damping matrices of a structure in the case of incomplete excitation.

86-936

**Parameter Identification in Distributed Systems**

H. Baruh, L. Meirovitch

Rutgers Univ., New Brunswick, NJ  
J. Sound Vib., 101 (4), pp 551-564 (Aug 22, 1985) 2 figs, 3 tables, 15 refs

**KEY WORDS:** Parameter identification technique, Mass coefficients, Stiffness coefficients, Damping coefficients

A method for the identification of the parameters entering into the equations of motion of distributed systems is described. Because the

motion of distributed systems is described in terms of partial differential equations, these parameters are in general continuous functions of the spatial variables. For vibrating systems, these parameters ordinarily represent the mass, stiffness and damping distributions. These distributions are expanded in terms of finite series of known functions of the spatial variables multiplied by undetermined coefficients. A method for the identification of the eigensolution is also presented.

86-937

**An Evaluation of a Class of Practical Optimization Techniques for Structural Dynamics Applications**

S.F. Masri, S.D. Werner  
University of Southern California, Los Angeles, CA  
Earthquake Engrg. Struc. Dynam., 13 (5), pp 635-649 (Sept/Oct 1985) 7 figs, 16 refs

**KEY WORDS:** Parameter identification technique, Optimization

A class of practical optimization techniques for parameter identification of realistic structural dynamic systems is evaluated. The techniques involve quasi-Newton methods together with an efficient procedure for estimating complicated error functions. Extensive numerical and graphical results demonstrate the effects of various optimization algorithm parameters on the rate of convergence of the objective function, the parameter vector error norm and the gradient norm. Guidelines are presented as an aid for addressing several significant issues in the practical application of structural dynamics optimization procedures.

86-938

**Identification of Unsteady Aerodynamics and Aeroelastic Integro-Differential Systems**

N.K. Gupta, K.W. Iliff  
NASA Hugh L. Dryden Flight Res. Ctr., Edwards, CA  
Rept. No. H-1313, NASA-TM-86749, 32 pp (Aug 1985) N85-32851/6/GAR

**KEY WORDS:** Parameter identification technique

The problem of estimating integro-differential models based on test or simulation data is dealt with. The identification techniques proposed for

estimating parameters in models described by differential equations need to be considerably extended to deal with the integral terms. Conditions under which the integral terms may be approximated by algebraic values are discussed. The integro-differential models discussed are related to indicial models proposed by aerodynamicists to describe unsteady flow.

## DESIGN TECHNIQUES

86-939

**Design Spectra for Degrading Systems**

G.J. Al-Sulaimani, J.M. Roessett  
Univ. of Petroleum and Minerals, Dhahran, Saudi Arabia  
ASCE J. Struc. Engrg., 111 (12), pp 2611-2623 (Dec 1985) 5 figs, 1 table, 18 refs

**KEY WORDS:** Seismic response spectra, Seismic design, Reinforced concrete

The effect of stiffness or strength degradation, or both, under cyclic loading on the seismic response of single-degree-of-freedom inelastic systems with 5% initial damping is investigated. Rules are proposed to construct inelastic design spectra for these systems (typical or reinforced concrete construction) as a function of the desired displacement (or ductility) ratio. These rules complement those used at present based on the response of simple elasto-plastic systems without any degradation.

86-940

**Generation of Floor Response Spectra Including Oscillator-Structure Interaction**

T. Igusa, A. der Kiureghian  
University of California, Berkeley, CA  
Earthquake Engrg. Struc. Dynam., 13 (5), pp 661-676 (Sept/Oct 1985) 8 figs, 3 tables, 29 refs

**KEY WORDS:** Equipment-structure interaction, Seismic design, Floors, Response spectra

A method is presented for generating floor response spectra for aseismic design of equipment attached to primary structures. The method accurately accounts for tuning, interaction and non-classical damping, which are inherent characteristics of composite oscillator-structure systems. The method is accurate to the order of

perturbation and is computationally efficient, as it avoids time-history analysis and does not require numerical eigenvalue evaluation of the composite oscillator-structure system. The results of a parametric study demonstrate the accuracy of the method and illustrate several key features of floor response spectra.

machinery vibrations and theoretical investigation of the transmission properties of foundations and of soils. A detailed evaluation of results and recommendations for the design of textile mills is included.

## GENERAL TOPICS

### CONFERENCE PROCEEDINGS

86-941

**Vibration-Emission by Textile Mills and the Design of Weaving Hall (Untersuchungen der von Webereien ausgehenden Schwingungs-emissionen und Hinweise zu Websaal-Bauplanungen)**

H.G. Natke, R. Thiede, K. Elmer  
Curt-Risch-Institut f. Dynamic, Schall-u. Messtchnik, U . Hannover, Fed Rep Germany  
Published by TNW-Textil-Industrie Service, GmbH, Moldkestr. 19, 4400 Münster, Fed. Rep. Germany (1985) 100 pp, Price 50.00 DM plus handling (in German)

**KEY WORDS:** Vibration control, Industrial facilities, Textiles

Vibration in the vicinity of textile mills was investigated experimentally and theoretically. The investigation comprised the measurement of

### BIBLIOGRAPHIES

86-942

**Feasibility of Simplifying Coupled Lag-Flap-Torsional Models for Rotor Blade Stability in Forward Flight**

G.R. Nilakantan, G.H. Gaonkar  
Hindustan Aeronautics Ltd., Bangalore, India  
Vertica, 2 (3), pp 241-256 (1985) 22 figs, 18 refs

**KEY WORDS:** Propeller blades, Helicopters, Torsional response

The feasibility of simplifying coupled lag-flap-torsional models is explored for the low-frequency stability of isolated hingeless rotor blades in forward flight. Under linear and quasilinear propulsive trim conditions, stability is investigated for four cases: a base-line model with elastic lag bending, flap bending and torsion degrees of freedom, the modified elastic lag-flap model that neglects only torsional dynamic effects, and the rigid blade models with and without quasi-steady approximation to torsion. The method of equivalent Lock number and drag coefficient is used for qualitative insights into dynamic inflow effects.







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# CALENDAR

## MAY

5-9 32nd Annual Technical Meeting of the Institute of Environmental Sciences [IES] Dallas/Ft. Worth Airport, TX (IES, 940 E. Northwest Highway, Mt. Prospect, IL 60056 -(312) 255-1561)

12-16 Acoustical Society of America, Spring Meeting [ASA] Cleveland, OH (ASA Hqs.)

## JUNE

3-6 Symposium and Exhibit on Noise Control [Hungarian Optical, Acoustical, and Cinematographic Society; National Environmental Protection Authority of Hungary] Szeged, Hungary (Mrs. Ildiko Baba, OPAKFI, Anker koz 1, 1061 Budapest, Hungary)

8-12 Symposium on Dynamic Behavior of Composite Materials, Components and Structures [Society for Experimental Mechanics] New Orleans, LA (R.F. Gibson, Mech. Engrg. Dept., University of Idaho, Moscow, ID 83843 - (208) 885-7432)

24-26 Machinery Vibration Monitoring and Analysis Meeting [Vibration Institute] Las Vegas, NV (Dr. Ronald L. Eshleman, Director, The Vibration Institute, 101 W. 55th St., Suite 206, Clarendon Hills, IL 60514 - (312) 654-2254)

## JULY

20-24 International Computers in Engineering Conference and Exhibition [ASME] Chicago, IL (ASME)

21-23 INTER-NOISE 86 [Institute of Noise Control Engineering] Cambridge, MA (Professor Richard H. Lyon, Chairman, INTER-NOISE 86, INTER-NOISE 86 Secretariat, MIT Special Events Office, Room 7-111, Cambridge, MA 02139)

24-31 12th International Congress on Acoustics, Toronto, Canada (12th ICA Secretariat, P.O. Box 123, Station Q, Toronto, Ontario, Canada M4T 2L7)

## SEPTEMBER

14-17 International Conference on Rotordynamics [IFToMM and Japan Society of Mechanical Engineers] Tokyo, Japan (Japan Society of Mechanical Engineers, Sanshin Hokusei Bldg., 4-9, Yoyogi 2-chome, Shibuyak-ku, Tokyo, Japan)

22-25 World Congress on Computational Mechanics [International Association of Computational Mechanics] Austin, Texas (WCCM/TICOM, The University of Texas at Austin, Austin, TX 78712)

29-30 VDI Vibrations Meeting [Society of German Engineers] Wurzburg, Fed. Rep. Germany (Society of German Engineers)

## OCTOBER

5-8 Design Automation Conference [ASME] Columbus, OH (ASME)

5-8 Mechanisms Conference [ASME] Columbus, OH (ASME)

7-9 2nd International Symposium on Shipboard Acoustics ISSA '86 [Institute of Applied Physics TNO] The Hague, The Netherlands (J. Buiten, Institute of Applied Physics TNO, P.O. Box 155, 2600 AD Delft, The Netherlands, Telephone: xx31 15787053, Telex: 38091 tpdtd nl)

**14-16 57th Shock and Vibration Symposium**  
[Shock and Vibration Information Center] New Orleans, LA (Dr. J. Gordan Showalter, Acting Director, SVIC, Naval Research Lab., Code 5804, Washington, D.C. 20375-5000 - (202) 767-2220)

**19-23 Power Generation Conference [ASME]**  
Portland, OR (ASME)

**20-22 Lubrication Conference [ASME]** Pittsburgh, PA (ASME)

**3-6 14th Space Simulation Conference [IES, AIAA, ASTM, NASA]** Baltimore, MD (Institute of Environmental Sciences, 940 E. Northwest Highway, Mt. Prospect, IL 60056 - (312) 255-1561)

**30-5 American Society of Mechanical Engineers, Winter Annual Meeting [ASME]** San Francisco, CA (ASME)

**CALENDAR ACRONYM DEFINITIONS  
AND ADDRESSES OF SOCIETY HEADQUARTERS**

<b>AHS</b>	American Helicopter Society 1325 18 St. N.W. Washington, D.C. 20036	<b>IMEchE</b>	Institution of Mechanical Engineers 1 Birdcage Walk, Westminster London SW1, UK
<b>AIAA</b>	American Institute of Aeronautics and Astronautics 1633 Broadway New York, NY 10019	<b>IFTOMM</b>	International Federation for Theory of Machines and Mechanisms U.S. Council for TMM c/o Univ. Mass., Dept. ME Amherst, MA 01002
<b>ASA</b>	Acoustical Society of America 335 E. 45th St. New York, NY 10017	<b>INCE</b>	Institute of Noise Control Engineering P.O. Box 3206, Arlington Branch Poughkeepsie, NY 12603
<b>ASCE</b>	American Society of Civil Engineers United Engineering Center 345 E. 47th St. New York, NY 10017	<b>ISA</b>	Instrument Society of America 67 Alexander Dr. Research Triangle Pk., NC 27709
<b>ASLE</b>	American Society of Lubrication Engineers 838 Busse Highway Park Ridge, IL 60068	<b>SAE</b>	* Society of Automotive Engineers 400 Commonwealth Dr. Warrendale, PA 15096
<b>ASME</b>	American Society of Mechanical Engineers United Engineering Center 345 E. 47th St. New York, NY 10017	<b>SEE</b>	Society of Environmental Engineers Owles Hall, Buntingford, Hertz. SG9 9PL, England
<b>ASTM</b>	American Society for Testing and Materials 1916 Race St. Philadelphia, PA 19103	<b>SESA</b>	Society for Experimental Mechanics (formerly Society for Experimental Stress Analysis) 14 Fairfield Dr. Brookfield Center, CT 06805
<b>ICF</b>	International Congress on Fracture Tohoku University Sendai, Japan	<b>SNAME</b>	Society of Naval Architects and Marine Engineers 74 Trinity Pl. New York, NY 10006
<b>IEEE</b>	Institute of Electrical and Elec- tronics Engineers United Engineering Center 345 E. 47th St. New York, NY 10017	<b>SPE</b>	Society of Petroleum Engineers 6200 N. Central Expressway Dallas, TX 75206
<b>IES</b>	Institute of Environmental Sci- ences 940 E. Northwest Highway Mt. Prospect, IL 60056	<b>SVIC</b>	Shock and Vibration Information Center Naval Research Laboratory Code 5804 Washington, D.C. 20375-5000