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STRUCTURAL CONCEPT ANALYSIS REPORT FOR THE EAST COAST
AIR COMBAT MANEUVER. (U) CREST ENGINEERING INC TULSA OK
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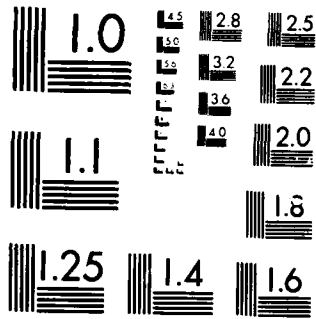
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CREST ENGINEERING, INC.
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RE: Distribution Statement, Contract N72477-76-C-0179, Appendixes A, C and D
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Per Ms. Jacqueline B. Riley, Naval Facilities Engineering Command, Code FPO-1

STRUCTURAL CONCEPT ANALYSIS REPORT
FOR THE
EAST COAST AIR COMBAT MANEUVERING RANGE
OFFSHORE KITTY HAWK, NORTH CAROLINA
CONTRACT NO. N62477-76-C-0179

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REPORT NO. 27-771-92
APPENDIX C. THREE-PILE CONCEPT CALCULATIONS

Prepared for
NAVAL FACILITIES ENGINEERING COMMAND
DEPARTMENT OF THE NAVY
CHESAPEAKE DIVISION

CREST ENGINEERING, INC.
1170 ...
WASHINGTON, D.C. 20004

By
CREST ENGINEERING, INC.
TULSA, OKLAHOMA

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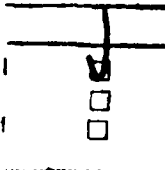

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SECTION 1
INTRODUCTION

1.1 INTRODUCTION

The major objective of this report is to establish an optimized three-pile ocean structure for the U.S. Navy Air Combat Maneuvering Range (ACMR) offshore North Carolina, U.S.A. This report constitutes a portion of the project report on the Structural Concept Analysis.

The function of this report is, therefore, to optimize a three-pile ocean structure so as to reflect a minimum steel weight under the environmental conditions compatible with those used previously in the design of skirt-pile structures.

The conceptual structure considered herein, a three-pile structure with equilaterally spaced jacket legs, is designed for a water depth of 84 feet (MLW). The anchoring of the structure is to be achieved by driving piles through the jacket legs into the seabed. Securing of the jacket is then accomplished by welding of shim plates along the annulus between the jacket leg and piling at the top of the jacket legs. A superstructure consisting of an equipment deck and a top deck will be installed to the piling above the jacket. A boat landing is to be furnished with the jacket. A set of stairways attached to the superstructure shall be furnished to provide connections among the boat landing, equipment deck and the top deck.

In order to attain the stated objective, a system optimization technique is employed in the course of establishing major structural member sizes and dimensions. An objective function of a minimum steel weight is formulated by treating the jacket base spacing as the univariable parameter subjected to the constraints of the drivability and axial load capacity of the piling. The selected structure is then analyzed to examine the member stresses and the reactions on the piling. The computation of the corrosion protection requirements follows. Finally, a three-pile ocean structure with piling size of 36 inches outside diameter and the jacket leg base spacing of 58 feet is established. The structure weighs approximately 500 tons.

1.2 DESIGN CRITERIA

Design criteria presented herein serve as guide lines in the conceptual development of the proposed three-pile structure. These criteria are listed as follows:

A. Environmental Criteria

MLW Depth	84 ft.
Storm Wave Height	62 ft.
Storm Wave Period	12 sec.
Maximum Storm Tide	10 ft.
Maximum Astronomical Tide	4 ft.
Maximum Current (for full depth)	5.4 ft./sec.
Wind Velocity	150 Knots @ (+)30 ft.

The approach of the storm wind and waves can be from any direction.

B. Foundation Criteria

- (1) The basis for the foundation design is a McClelland report to Cubic Corporation entitled "Foundation Investigation East Coast ACMR Ocean Structures, Volume I". The soil information to be used in this analysis is one boring at Site No. 1 in the aforementioned report.
- (2) Due to the nature of the sea bottom, and sea bottom currents, scouring of 5 feet below mudline will be used in the preliminary piling design to develop the theoretical soil resistance to laterally applied loads.

C. Live Loads

The live loads shall be as follows:

Equipment Deck	150 psf
Top Deck	100 psf

The loads shall be distributed uniformly over the entire deck areas.

D. Material

All structural shapes or fabricated tubular goods are assumed to be ASTM A-36 or equal.

E. Corrosion Protection

- (1) All portions of the platform above elevation (-)4' - 0" shall be painted.
- (2) All main structural members located within the splash zone shall have an extra 1/2 inch of sacrificial steel added to their wall thickness. This can be in the form of extra wall thickness or a 1/2 inch steel plate wrap.
- (3) The portion of the platform below elevation (-)4' - 0" will be protected by cathodic protection. This will be provided by sacrificial anodes having a theoretically expected life of ten years.

F. Miscellaneous

- (1) The platform is analyzed as if the annulus between the jacket and piling will be ungrouted.

The criteria employed for determination of structural acceptability are specified by the documents:

- (a) Specification API RP 2A, Recommended Practice for Planning, Designing and Constructing Fixed Offshore Platforms, 7th Edition, American Petroleum Institute, Dallas, Texas, 1976.
- (b) Manual of Steel Construction, 7th Edition, American Institute of Steel Construction, New York, N.Y., 1969.

1.3 DESIGN ASSUMPTIONS

Some assumptions to be used in this analysis are listed as follows:

True batter of piling and jacket leg	1:6
Equipment deck area	500 sq. ft.
Top deck area	1,200 sq. ft.
Spacing between decks	15 ft.

1.4 PROCEDURES OF ANALYSIS

The primary item of concern is the axial loads resulting in the maximum environmental forces. If the maximum required pile capacity is attainable through the available soil information, then the conceptual structure would be considered feasible. In order to obtain such information, Sections 2, 3, and 4 are first developed in this analysis.

A three-pile structure with variable base spacing is then considered under a given set of overturning moment (107,302 ft-kips)* and horizontal force (1,254.6 kips)*. Thus, the relationship between axial pile capacity and jacket base spacing under a set of given loads is established in Section 5.

Section 6 presents a system optimization procedures to select a structure which reflects the minimum steel weight and minimum spacing under the constraints of Sections 2 to 5.

The configuration of the selected structure is proposed (Section 7) and then idealized (Section 8) for further analysis. The basic loading conditions (detailed in Section 9) acting on the structure are computed in accordance with the design criteria. Finally, the selected structure is analyzed as a space frame structure under combinations of various basic loading conditions (Section 10). The structural member stresses from the space frame analysis are compared with the API and AISC Specifications. The structural reactions are again used to check the pile capacity requirements.

* Storm forces from skirt-pile structures under separate contract: Crest Offshore Job No. 27-621-00, to Cubic Corporation.

1.5 DESIGN SUMMARY

Some of the more significant results from the analysis are summarized as follows:

Environmental Forces:

Total wind and wave forces (including boat loading and stairway)	896.7 kips
Total overturning moment (including boat landing and Stairway)	79,573 ft-kips

Pile Axial Loads:

Maximum compressive load	1,858 kips
Maximum tensile load	1,463 kips

Structural Dimensions:

Piling

Outside diameter	36 in.
Penetration below mudline	180 ft.

Jacket

Spacing at mudline	58 ft.
Spacing at work-point level	29 ft.
Height	98 ft. 9 in.

Superstructure

Equipment deck	25 ft. x 20 ft.
Top deck	35 ft. x 35 ft.

Structural Steel Weight

Piling	545,886 lbs.
--------	--------------

Superstructure	138,907 lbs.
Jacket	<u>231,130 lbs.</u>
Total weight (excluding boat landing, stairway and miscellaneous items)	915,923 lbs.

1.6 PERSONNEL RESUMES

The personnel whose resumes follow were actively engaged in this project.

CREST OFFSHORE, INC.

Chingmiin (Charlie) Chern



Senior Engineer

<u>University</u>	<u>Degree</u>	<u>Year</u>
National Taiwan University	Bachelor of Science Civil Engineering	1961
North Dakota State University	Master of Science Civil Engineering	1966
Lehigh University	Ph. D. Civil Engineering	1969
Tulsa University	Graduate Study in Business Administration- Management	1974

Societies, Licenses,
and
Other Activities:

Member American Society of Civil Engineers
Member International Association of Structural and
Bridge Engineers
Member American Society of Engineering Education
Registered Professional Engineer in Oklahoma

Experience:

1973 to Present

Senior
Civil
Engineer

Crest Offshore, Inc.

Engaged in the feasibility studies, structural analysis and design of offshore structures, equipment supports and other various types of petroleum related civil engineering works. Assignments include:

- ... Evaluation of engineering designs from other agencies.
- ... Analysis and design of offshore structures for oil industry.
- ... Analysis and design of supports and foundations for onshore refinery facilities.
- ... Development of a sequence of computer programs for the analysis of offshore structures.

CREST OFFSHORE, INC.

Chingmiin (Charlie) Chern

Senior Civil Engineer

Experience Continued:

1969 to 1973

North Dakota State University

Associate
Professor of
Civil Engineering

Engaged in full-time lecture instruction for civil engineering (graduate school division) and construction management. Also served as consultant to local industry (undergraduate school division) in the area of computer applications in engineering.

1966 to 1969

Fritz Engineering Laboratory

Research
Assistant

Assisted in the design and testing of various types of steel structures.

1966

North Dakota State Highway Department

Highway
Engineer

Responsible for construction surveying.

1965

U.S. Forest Service

Assistant
Crew Chief

Assisted in surveying responsibilities.

SECTION 2
PIPE PILE CAPACITY CURVES

2.1 INTRODUCTION

Axial capacity curves are developed hereinafter for 30", 36", 39" and 42" diameter piling. The method utilized is the empirical procedures, as presented in the McClelland soils report, for pipe piles penetrating through sand and clay alternating strata. The 30" diameter curves are developed to demonstrate the ability to reproduce the McClelland curves and subsequently the same procedure is followed to produce the remaining curves.

by C. Schorn Client U.S. 222 Subject *Stratigraphic Corropt Analysis Bopla*
 Date 3-21-76 Job No. 27-271-92 Calculation *Pipe pile Capacity Curves*

2.2 SOIL DATA

Stratification

A generalized summary of the major soil strata at each site based on the log of boring is given in the following tabulations:

Stratum	Boring 1		Description
	From	To	
I	0	56	Very dense gray fine sand and silty fine sand
II	56	78	Dense gray silty fine sand
III	78	146	Dense gray fine sand
IV	146	170	Medium dense-to-dense gray silty fine sand
V	170	297.5+	Very stiff brown-to-gray silty clay-to-moderately plastic clay

Stratum	Boring 2		Description
	From	To	
I	0	33	Very dense gray fine sand
II	33	45	Very stiff-to-hard gray silty clay
III	45	114	Dense gray silty fine sand-to-silt below 90-ft penetration
IV	114	132	Firm-to-stiff gray silty clay
V	132	190	Medium dense gray sandy silt-to-silt below 160-ft penetration
VI	190	235	Medium dense-to-dense gray silty fine sand
VII	235	290	Very stiff gray silty clay
VIII	290	320.5+	Dense dark gray-to-gray fine sand

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by S. G. ... Client U. S. ... Subject Structural Design of ...
 Date 3-19-72 Job No. 27-771-72 Calculation Tip & Capacity

<u>Stratum</u>	<u>Boring 3</u> <u>Penetration, ft</u>		<u>Description</u>
	<u>From</u>	<u>To</u>	
I	0	107	Dense-to-very dense tan-to-gray fine sand
II	107	160	Medium dense silty fine sand-to-sandy silt below 140-ft penetration
III	160	225	Very stiff-to-stiff gray silty clay
IV	225	243	Medium dense silty fine sand
V	243	260	Very stiff gray silty clay
VI	260	280	Dense gray silty fine sand
VII	280	292	Hard gray sandy clay
VIII	292	326.5+	Medium dense gray silty fine sand

<u>Stratum</u>	<u>Boring 3a</u> <u>Penetration, ft</u>		<u>Description</u>
	<u>From</u>	<u>To</u>	
I	0	175	Very dense-to-medium dense gray fine sand and silty fine sand
II	175	195	Gray clayey silt, slightly sandy
III	195	235	Stiff gray silty clay
IV	235	255	Medium dense-to-dense gray silty fine sand
V	255	275	Hard-to-very stiff gray silty clay
VI	275	289	Dense gray silty fine sand
VII	289	305	Very stiff gray moderately plastic clay
VIII	305	370.5+	Medium dense gray silty fine sand

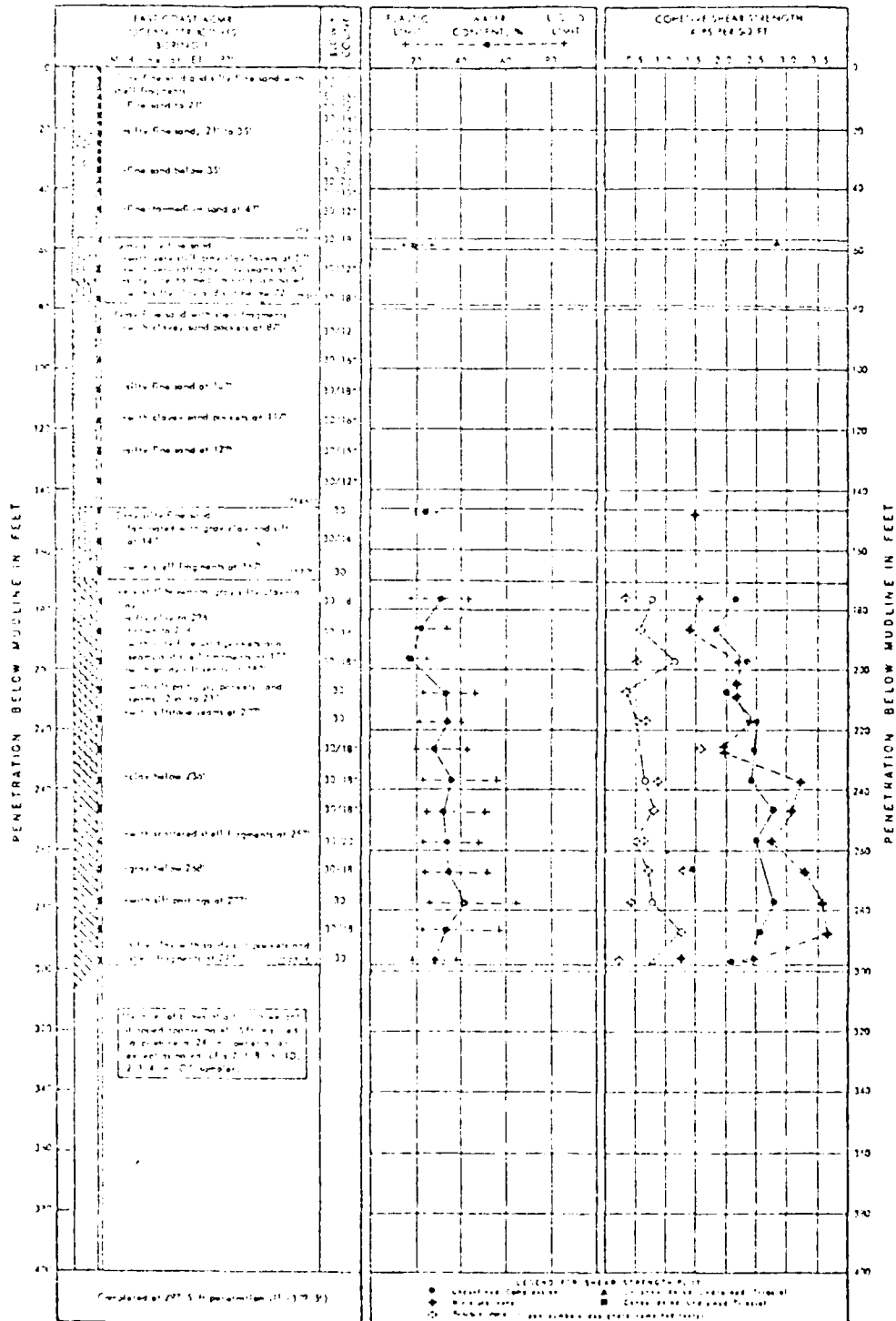
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Sheet 2.5 of 3

By C. Clark Client U.S. NAVY Subject Soil Test Concept Analysis
Date 3-11-64 Job No. 27-721-94 Calculation Pipe Pile Capacity

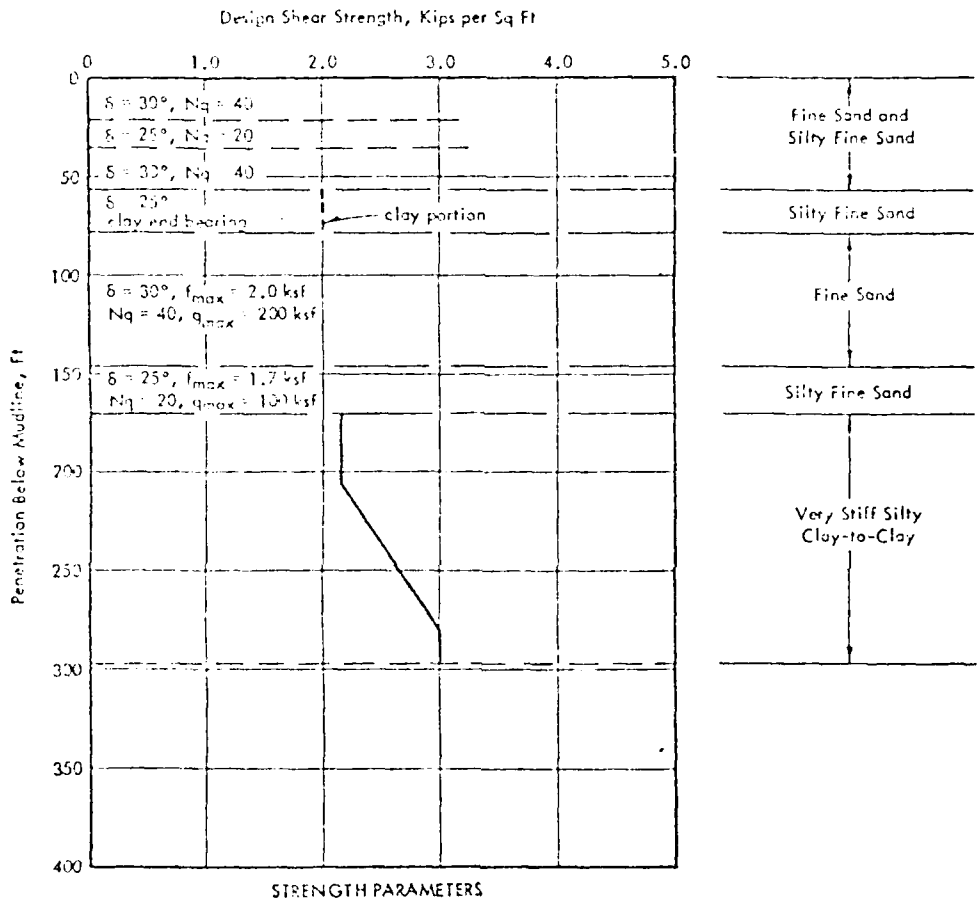
<u>Stratum</u>	<u>Boring #</u>		<u>Description</u>
	<u>From</u>	<u>To</u>	
I	0	102	Very dense-to-dense tan-to-gray fine sand
II	102	136	Medium dense gray silt
III	136	170	Medium dense-to-dense gray silty fine sand
IV	170	207	Dense-to-very dense tan-to-gray fine sand
V	207	250	Very stiff gray moderately plastic clay
VI	250	275	Medium dense gray silt
VII	275	330.5+	Very stiff gray silty clay

by C. P. [unclear] Client U.S. [unclear] Subject Structure on [unclear]
 Date 7-1-57 Job No. 27-721-2 Calculation Page 2192 of 2192



LOG OF BORING AND TEST RESULTS

By: C. Smith Client: U.S. NAVY Subject: Structural Capacity Analysis
 Date: 1-17-76 Job No: 77-171-100 Calculation: Pipe pile Capacity Curves

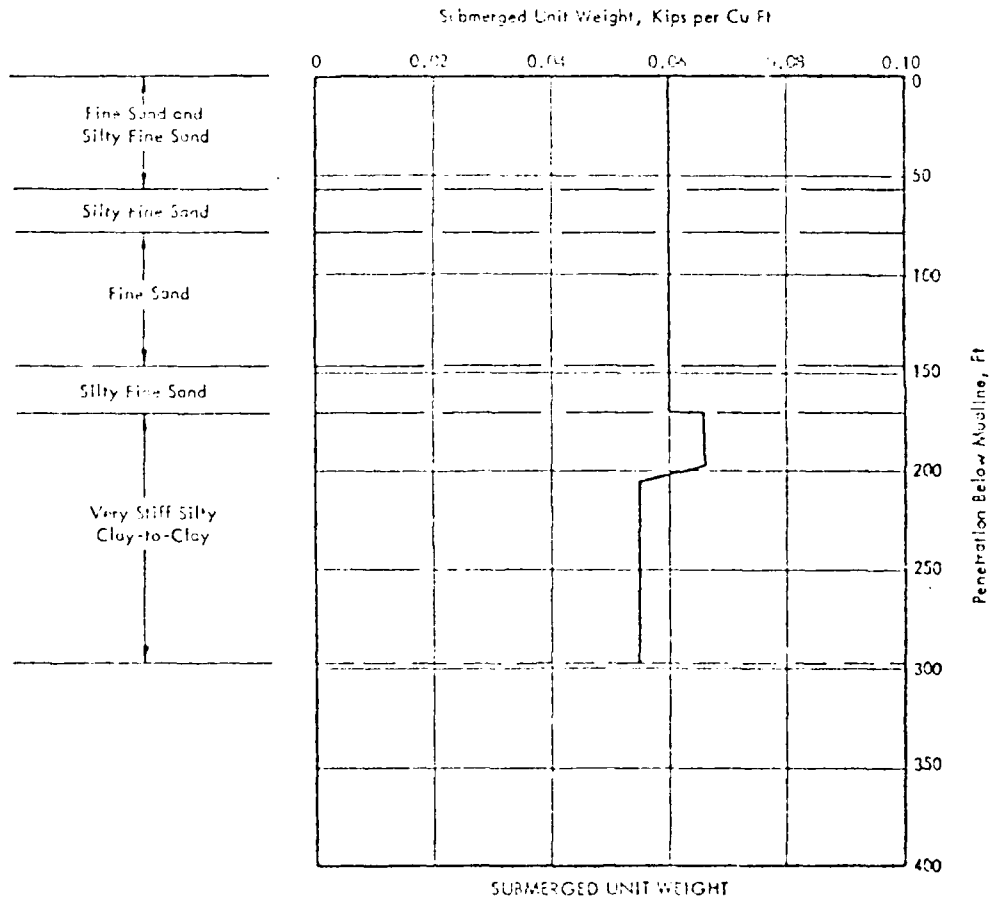


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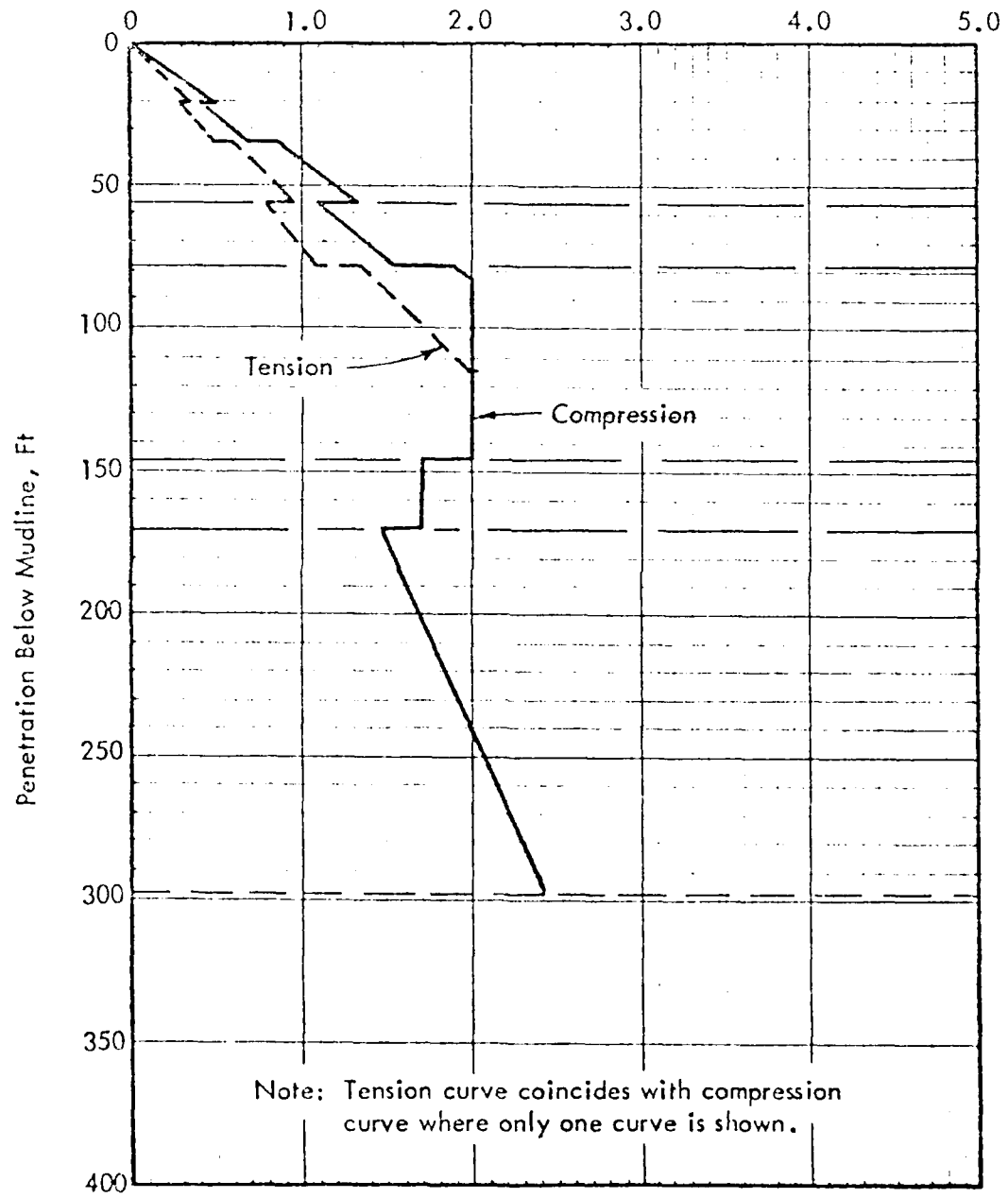
by C. C. Brown Client U.S. NAVY
 Date 3-21-76 Job No. 27771-3

Subject Structural Capacity of
 Calculation Pipe to Capacity Chart



By C. Clark Client U.S. Navy Subject Structural Concept Analysis
Date 3-2-56 Job No. 47-1721-10 Calculation Pile Capacity Curves

Equivalent Unit Skin Friction, Kips per Sq Ft

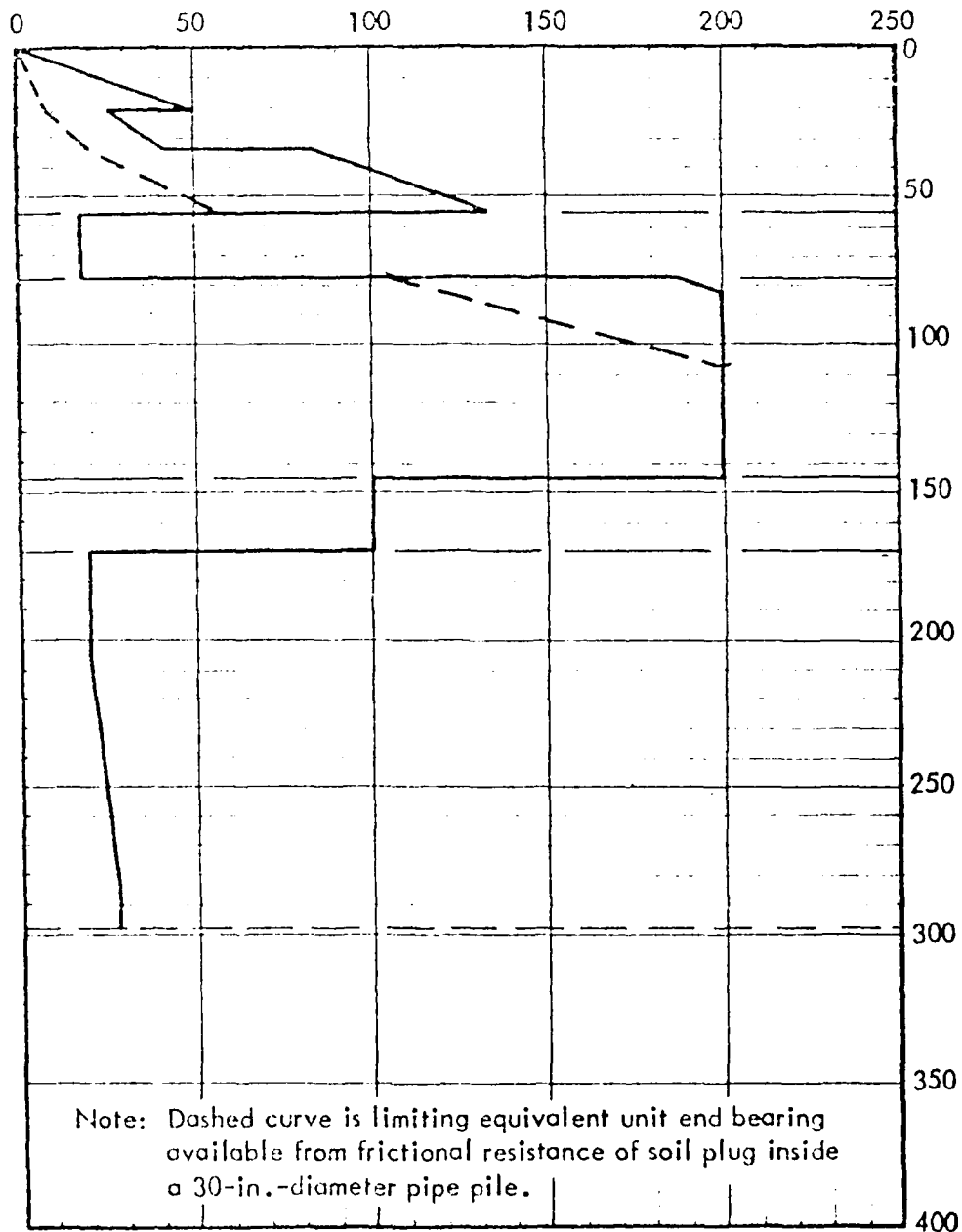


Note: Tension curve coincides with compression curve where only one curve is shown.

EQUIVALENT UNIT SKIN FRICTION

by C. C. [unclear] client U. S. NAVY subject Structural Capacity of [unclear]
Date 3-21-76 Job No. 42-271-22 Calculation [unclear]

Unit End Bearing, Kips per Sq Ft



Note: Dashed curve is limiting equivalent unit end bearing available from frictional resistance of soil plug inside a 30-in.-diameter pipe pile.

UNIT END BEARING

DREST OFFSHORE, INC.

Sheet E-12 of 21

by C. Ch...
 Date 8/21/78

Station 210...
 Calculation King Pile Capacity Curves

DEPTH (FEET)	UNIT SKIN FRICTION (KSF)	UNIT END BEARING (KSF)	SEGMENT LENGTH (FEET)
0	0	0	
20	2.45	9	20
20	2.20	9	
33	2.67	20	15
33	2.85	20	
56	1.30	20	21
56	1.10	18	
79	1.55	12	23
79	1.90	100	
82	2.00	115	3
82	2.00	115	
107	2.00	200	25
107	2.00	200	
115	2.00	200	8
115	2.00	200	
125	2.00	200	30
145	1.70	100	
170	1.70	100	25
170	1.60	20	
195	1.72	20	25
205	1.70	20	
230	2.00	20	25
230	2.20	20	
250	2.40	20	20

Σ = 300 ft

Unit Capacity in Compression

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Sheet 2 of 4

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 3-31-76 Job No 27-771-92 Calculation Pipe Pile Capacity Curves

PENETRATION BELOW MUDLINE	UNIT SKIN FRICTION	UNIT END BEARING	SEGMENT LENGTH
FT	KSF	KSF	FT
0	0	-	20
20	0.29	-	15
35	0.60	-	21
56	0.80	-	23
79	1.35	-	3
82	1.40	-	25
107	2.00	-	8
115	2.00	-	30
145	1.70	-	25
170	1.43	-	35
205	1.72	-	75
280	2.00	-	20

3300 ft

UNIT CAPACITY IN TENSION

By C. P. [unclear] Client H. S. [unclear] Subject Structural Capacity for [unclear]
 Date 2-21-77 Job No. 27-774-72 Calculation Pile Pile Capacity Curves

2.3 PILE CAPACITY IN COMPRESSION

$$Q = Q_s + Q_p$$

where Q_s = skin friction on the wall of the pile

Q_p = end bearing

DEFINITION:

For Cohesive Soils

$$Q_s = \lambda (\bar{\sigma}_m + 2 C_m) A_s$$

where $\bar{\sigma}_m$ = mean effective vertical stress between the mudline and the pile tip

C_m = mean undrained cohesive shear strength along the pile length

λ = dimensionless frictional capacity coefficient (function of pile penetration.)

A_s = equivalent surface area of the pile

Granular Soils

$$Q_s = f A_s$$

where f = the unit skin friction between soil and pile

$$f = K \bar{\sigma}_v \tan \delta$$

K = coefficient of lateral earth pressure

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 3-5-76 Job No 77-771-74 Calculation Pipe Pile Capacity Curves

$\bar{\sigma}_v$ = effective vertical stress

δ = angle of friction, $\delta = \alpha$ for distributed vertical load and $\delta = \alpha/2$ for pile

Note: $K = 0.7$ for compressive load
 $= 0.5$ for tensile load

END BEARING:

$$Q_p = q A_p$$

Cohesive Soils

$$q = c N_c$$

where c = cohesive shear strength

N_c = a dimensionless bearing capacity factor
 (a value of q is assumed)

Granular Soils

$$q = \bar{\sigma}_v N_q$$

where $\bar{\sigma}_v$ = effective vertical stress

N_q = a dimensionless bearing capacity factor
 which is a function of ϕ , the angle of internal friction of the material

By S. J. [unclear] Client U. S. [unclear] Subject Installation of Concrete [unclear]
 Date 2-1-77 Job No. 1-77-2-1 Calculation Penetration [unclear]

Skin Friction Capacity ($Q_s = f_{os} A_s$)

--- Compression ---

O. D. = 30"

$A_s = \pi D (s.l.) = 7.854 (\Delta l) \text{ sq. ft.}$

Penetration Below Mudline (ft)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_{os} (ksf)	Segment Length (Δl) (ft)	Sk. Friction in Segment (kips)	Total Sk. Friction (kips)
0	0				0
20	0.45	0.225	20	35.3	35.3
35	0.40	0.335	15	58.0	93.3
56	0.85	1.075	21	177.3	275.8
79	1.10	1.375	23	248.4	524.2
107	1.65	1.950	3	48.9	570.1
145	2.00	2.00	25	392.7	962.8
170	2.00	2.00	8	125.7	1088.5
205	2.00	2.00	30	471.2	1559.7
220	1.70	1.70	25	333.3	1893.0
255	1.70	1.60	35	431.8	2324.8
280	1.72	2.01	75	1184.0	3508.8
300	2.30	2.35	20	364.1	3872.9
			$\Sigma = 300 \text{ ft.}$		

W. C. Chalmers Client: U.S. NAVY Subject: Structural Capacity Analysis
 Date: 3-21-76 Job No: 2-771-2-1 Calculation: Friction Capacity Curves

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Compression ---

O.D. = 36"

$A_s = \pi D (dL) = 2,325 \text{ sq. FT}$

Penetration Below Mudline (ft)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0				
20	0.45	0.225	20	46.5	46.5
20	0.40	0.225	15	34.9	115.0
35	0.67				
35	0.85	1.075	21	248.3	333.0
56	1.30				
56	1.10	1.375	23	273.1	606.1
79	1.65				
79	1.90	1.950	3	55.1	661.2
82	2.00				
82	2.00	2.00	25	471.3	1,155.3
107	2.00				
107	2.00	2.00	8	150.8	1,306.1
115	2.00				
115	2.00	2.00	30	565.5	1,871.6
145	2.00				
145	1.70	1.70	25	400.5	2,272.2
170	1.70				
170	1.45	1.65	35	527.8	2,800.0
205	1.72				
205	1.72	2.01	75	1,410.8	4,210.8
280	2.30				
280	2.30	2.35	20	443.0	4,653.8
300	2.40				
			$\Sigma = 200 \text{ ft}$		

By C. C. Chen Client U.S. NAVY Subject Structural Concept Analysis (2-4-19)
 Date 3-21-76 Job No. 27-77L-92 Calculation Pipe Rls Capacity Curves

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Compression ---

$O.D. = 39"$

$A_s = \pi D(\Delta L) = 10.21(\Delta L)$ sq. FT

Penetration Below Seabed (ft)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0				0
20	0.45	0.225	20	45.9	45.9
35	0.67	0.535	15	81.9	127.8
56	1.30	1.075	21	230.5	358.3
79	1.65	1.375	23	322.9	681.2
82	2.00	1.950	3	59.7	740.9
107	2.00	2.00	25	510.5	1,251.4
115	2.00	2.00	8	163.4	1,414.8
145	2.00	2.00	30	612.6	2,027.4
170	1.70	1.70	25	433.9	2,461.3
205	1.72	1.60	35	571.8	3,033.1
280	2.30	2.01	75	1539.2	4,572.3
300	2.50	2.35	20	474.9	5,047.2
			$\Sigma = 300$ ft.		

By C. Chen Client U.S. NAVY Subject Stiffness Concept / Capacity
 Date 3-1-78 Job No 27-77L-12 Calculation Pipe Pile Capacity - Compression

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Compression ---

$O.D. = 42"$

$A_s = \pi D (dL) = 10.996 (dL) \text{ sq. ft}$

Penetration Below Mudline (ft)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0				0
20	0.45	0.225	20	49.5	49.5
20	0.40	0.535	15	88.2	137.7
35	0.67				
35	0.85	1.075	21	248.2	385.9
56	1.30				
56	1.10	1.375	23	347.7	733.6
79	1.65				
79	1.80	1.950	3	64.5	798.1
82	2.00				
82	2.00	2.00	25	549.8	1347.9
107	2.00				
107	2.00	2.00	8	175.9	1523.6
115	2.00				
115	2.00	2.00	30	659.3	2182.9
145	1.70				
145	1.70	1.70	25	457.3	2640.2
170	1.48				
170	1.48	1.60	35	616.8	3257.0
205	1.72				
205	1.72	2.01	75	1557.6	4814.6
280	2.20				
280	2.20	2.35	20	516.8	5331.4
300	2.10				
			$\Sigma = 300 \text{ ft}$		

CREST OFFSHORE, INC.

Sheet 213 of 41

By Client H.S. WILLY Subject Structural Concept Analysis
 Date Job No. Calculation Pile Capacity Check

$Q_u = \frac{2}{3} A_p$

Depth (ft)	Soil Type	Q_u	Q_{u1}	Q_{u2}	Q_{u3}
0		0	0	0	0
20		44.2	62.6	74.7	56.6
40	20	98.2	141.4	166.0	132.4
60	20	171.9	247.5	290.5	235.7
80	18	33.4	127.3	143.4	173.2
100	18	513.6	742.4	871.5	1,010.1
120	115	364.7	210.1	954.5	1,065.3
140	115				
160	200	982.0	1,414.0	1,630.0	1,324.0
180	200				
200	200				
220	200				
240	200				
260	100	491.0	707.0	830.0	962.0
280	100				
300	20	98.2	141.4	166.0	132.4
320	20				
340	20				
360	18	137.5	193.0	232.4	239.4
380	18				
400	18				

By C. S. Shaw Client U.S. Navy Subject Structural Concept Analysis (S-110)
 Date Feb 1 1968 Job No. 2-110-1-13 Calculation Pile pile Capacity, Comp.

Ultimate Pile Capacity, (Q - Q_c + Q_p) --- Compression

Penetration Subsoil Line (ft)	30" Ø Q (KIPS)	36" Ø Q (KIPS)	39" Ø Q (KIPS)	42" Ø Q (KIPS)
0	0	0	0	0
10	77.5	106.2	120.6	136.1
20	176.7	239.4	293.8	330.1
35	447.7	578.3	643.3	722.6
56	364.2	482.1	507.7	553.1
70	612.6	756.2	830.6	906.3
79	1,033.7	1,371.3	1,552.7	1,743.7
82	1,134.3	1,497.1	1,695.4	1,904.2
107	1,914.9	2,569.3	2,911.4	3,271.7
107	2,070.3	2,720.1	3,074.3	3,447.6
115	2,641.7	3,285.6	3,627.4	4,107.4
145	2,052.7	2,578.6	2,857.4	3,143.4
170	2,234.5	2,971.2	3,291.3	3,612.7
195	1,811.7	2,413.6	2,627.3	2,842.7
200	2,431.5	2,941.4	3,199.1	3,458.3
230	3,604.3	4,418.2	4,804.7	5,193.5
280	4,223.9	4,861.8	5,284.4	5,710.3

CREST OFFSHORE, INC.

Sheet 2122 of 41

Client U.S. NAVY Subject Structural Concept/Design
 Date 4-1-75 Job No EE-71-74 Calculation Pile Pile Capacity Curve

Design Pile Capacity ($Q_u = Q / F.S.$) --- Compression

F.S. = 1.5

Depth (ft)	30" Q_u (KIPS)	36" Q_u (KIPS)	39" Q_u (KIPS)	42" Q_u (KIPS)
0	0	0	0	0
20	53.0	70.7	80.4	90.7
33	131.1	172.9	195.9	220.1
56	298.5	385.3	432.5	481.7
79	422.8	506.4	553.7	604.5
107	693.1	914.2	1,035.1	1,162.5
127	784.3	952.1	1,120.3	1,269.3
155	1,294.5	1,712.9	1,940.9	2,181.1
172	1,382.3	1,813.4	2,043.3	2,298.4
200	1,674.5	2,190.4	2,452.3	2,738.3
230	1,367.1	1,719.1	1,904.9	2,095.9
250	1,533.7	1,986.1	2,194.2	2,403.5
280	1,627.8	1,609.1	1,751.5	1,895.1
300	1,621.0	1,962.9	2,132.7	2,305.7
320	2,435.5	2,945.9	3,203.1	3,462.3
350	2,692.6	3,241.2	3,522.9	3,806.9

By C. Chubb Client US NAVY Subject Structural Concept Analysis
 Date 4-1-75 Job No. 22-776-1 Calculation Pipe Pile Capacity Chart

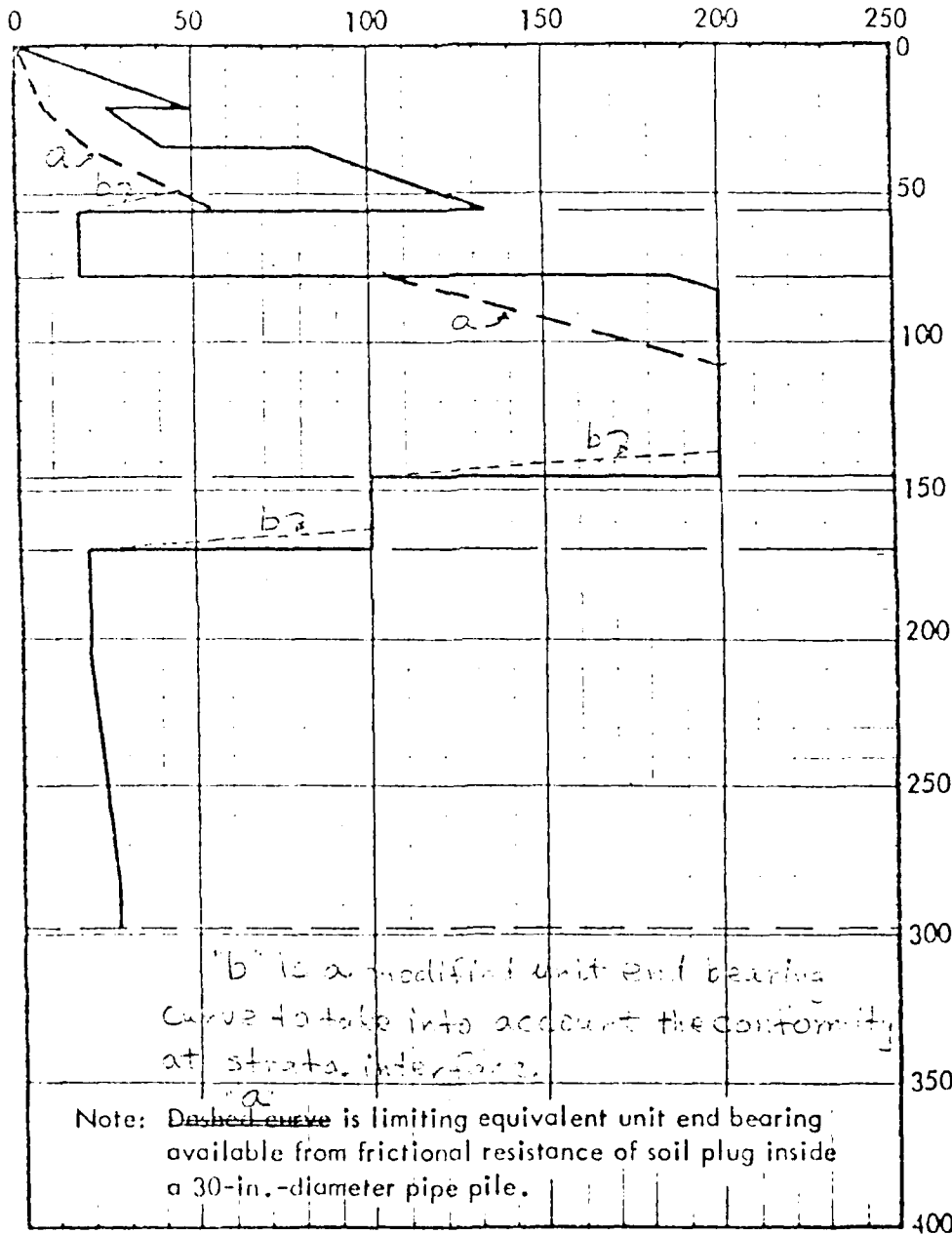
Modification on Unit End Bearing Capacity

It is assumed that the unit end bearing capacity of the higher strength stratum reduces linearly at 3-D (3 times outside diameter) distance above the strata intersurface to conform with that of the lower strength stratum.

for 30" O.D. pipe pile	3-D = 7.5 ft
36" O.D.	= 9.0
39" O.D.	= 9.75
42" O.D.	= 10.5

By Client Subject
 Date Job No. Calculation

Unit End Bearing, Kips per Sq Ft



"b" is a modified unit end bearing curve to take into account the conformity at strata interface.

Note: Dashed curve "a" is limiting equivalent unit end bearing available from frictional resistance of soil plug inside a 30-in.-diameter pipe pile.

UNIT END BEARING

By CLC Client Ch. S. & A. V. L. Subject Final Design & Construction
 Date 4-1-72 Job No. 27-271-35 Calculation Pipe Pile Capacity

30-in. Diameter Pipe Piles

(1) At Penetration 48.5 ft (=56'-7.5')

$$\text{End Bearing } Q_p = (46 \text{ ksf}) \times (4.91') = 225.9 \text{ kips}$$

$$\begin{aligned} \text{Skin Friction } Q_s &= 93.5 + 1.075 \times (21 - 7.5) \times 7.854 \\ (\text{see pg } 2-14) &= 93.5 + 114.0 \\ &= 212.5 \text{ kips} \end{aligned}$$

$$\text{Ultimate Capacity } Q = 225.9 + 212.5 = 438.4 \text{ kips}$$

$$\text{Design Capacity } Q_d = 212.5 \text{ kips}$$

(2) At Penetration 137.5 ft (=145'-7.5')

$$\text{End Bearing } Q_p = (200 \text{ ksf}) \times (4.915') = 982 \text{ kips}$$

$$\begin{aligned} \text{Skin Friction } Q_s &= 1033.5 + 2.0 \times (30 - 7.5) \times 7.854 \\ (\text{see pg } 2-14) &= 1033.5 + 353.4 \\ &= 1,441.9 \text{ kips} \end{aligned}$$

$$\text{Ultimate Capacity } Q = 1,441.9 + 982 = 2,423.9 \text{ kips}$$

$$\text{Design Capacity } Q_d = 1,615.9 \text{ kips}$$

Client: Chesapeake Energy

Subject: Production Concept Technical Report

Date: 4/21/11

Calculation: Pipe Pile Capacity Check

1. Soil Evaluation 110,5 psf (1700 lbs)

End Bearing $Q_p = (300 \times 16) \times (2.915) = 491 \text{ kips}$

SKC Evaluation
(See 2.14) $Q_s = 1557.7 + 170(25 - 7.5) \times 7.554$
 $= 1557.7 + 2235.7$
 $= 1,793.4 \text{ kips}$

Ultimate Capacity $Q_u = 1,793.4 + 491.0$
 $= 2,284.4 \text{ kips}$

Design Capacity $Q_d = 1,552.9 \text{ kips}$

by C. Chapp Client U.S. NAVYSubject Structural Concept (Initial Design)Date 4-1-76 Job No 27-221-73Calculation Pipe Pile Capacity36-in. Diameter Pipe Piles(i) At Penetration 47.0 ft (56'-9.0')

End Bearing $Q_p = (46 \text{ ksf}) \times (7.07 \text{ sq ft}) = 325.2 \text{ kips}$

Skin Friction
(see p. 2-15) $Q_s = 118.0 + 1.075(21-9) \times 9.425$

$$= 118.0 + 121.6$$

$$= 239.6 \text{ kips}$$

Ultimate Capacity $Q = 239.6 + 325.2 = 564.8 \text{ kips}$

Design Capacity $Q_d = 376.5 \text{ kips}$

(ii) At Penetration 136 ft (= 145'-9')

End Bearing $Q_p = (200 \text{ ksf}) \times (7.07 \text{ ft}^2) = 1,414 \text{ kips}$

Skin Friction
(see p. 2-15) $Q_s = 1,306.1 + 2.0 \times (30-9) \times 9.425$

$$= 1,306.1 + 395.9$$

$$= 1,672 \text{ kips}$$

Ultimate Capacity $Q = 1,672 + 1,414 = 3,086.0 \text{ kips}$

Design Capacity $Q_d = 2,057.3 \text{ kips}$

By Carlton, O'Neil, & Smith Subject Structural Concept for Offshore
 Date 1/13/83 Draw No. 22-201-32 Calculation Pile Capacity Calc.

(iii) At Pile tip 161.0 ft (=170' - 9.0')

$$\text{End Bearing } Q_p = (100 \text{ ksf}) (11.07 \text{ sq ft}) = 707 \text{ kips}$$

$$\text{Skin Friction } Q_s = 1371.6 + 1.70 (20-9) (9.425)$$

(See pp. 2-15)

$$= 1371.6 + 256.4$$

$$= 2,128 \text{ kips}$$

$$\text{Ultimate Capacity } \bar{Q}_u = 2,128 + 707 = 2,835 \text{ kips}$$

$$\text{Design Capacity } Q_d = 1390 \text{ kips}$$

Dr. C. Chappin Client U.S. NAVY Subject Structural Concept Analysis
 Date 1-7-72 Job No. 42-771-72 Calculation Pipe Pile Capacity

39-in. Diameter Pipe Piles

(i) At Penetration 46.25' (=56'-9.75')

End Bearing $Q_p = (16 \text{ ksf}) \times (8.30 \text{ ft}) = 331.3 \text{ kips}$

Skin Friction
(see p. 2-16) $Q_s = 127.3 + 1.075 \times (21 - 9.75) \times 10.21$
 $= 127.3 + 123.3$
 $= 251.3 \text{ kips}$

Ultimate Capacity $Q = 251.3 + 331.3 = 633.1 \text{ kips}$

Design Capacity $Q_d = 422.1 \text{ kips}$

(ii) At Penetration 139.25' (=145'-9.75')

End Bearing $Q_p = 200 \times 8.30 = 1,660 \text{ kips}$

Skin Friction
(see p. 2-16) $Q_s = 1,414.8 + 2.0 \times (30 - 9.75) \times 10.21$
 $= 1,414.8 + 413.5$
 $= 1,828.3 \text{ kips}$

Ultimate Capacity $Q = 1,828.3 + 1,660 = 3,488.3 \text{ kips}$

Design Capacity $Q_d = 2,325.3 \text{ kips}$

Client U.S. Navy Subject Structural Concept Design
 Date 8-1-76 Job No. 87-771-2E Calculation Pile Capacity

At Position 163.5 ft (120' - 9.75')

End Bearing $Q_p = 100 \times 8.30 = 830 \text{ kips}$

Sk. Fr. $Q_s = 2.0274 + 1.70(25 - 9.75) \times 10.21$
 (see 2.16)
 $= 2.0274 + 264.7$
 $= 2.074.1 \text{ kips}$

Ultimate Capacity $Q_u = 2.074.1 + 830 = 3.122.1 \text{ kips}$

Design Capacity $Q_d = 2.081.4 \text{ kips}$

By C. Chien Client M. S. NALCO Subject Structural Concept Analysis
 Date 4-1-76 Job No 22-72-92 Calculation Pipe Pile Capacity

42-in Diameter Pipe Pile:

(1) At Penetration 40.5' (=55'-10.5')

End Bearing $Q_p = 46 \times 9.62 = 442.5 \text{ kips}$

Skin Friction $Q_s = 137.7 + 1.075(21 - 10.5) \times 10.996$
 (See Pg. 2-17)
 $= 137.7 + 124.1$
 $= 261.8 \text{ kips}$

Ultimate Capacity $Q = 261.8 + 442.5 = 704.3 \text{ kips}$

Design Capacity $Q_d = 469.5 \text{ kips}$

(2) At Penetration 134.5' (=145'-10.5')

End Bearing $Q_p = 200 \times 9.62 = 1,924 \text{ kips}$

Skin Friction $Q_s = 1,523.6 + 2.0(30 - 10.5) \times 10.996$
 (See Pg. 2-17)
 $= 1,523.6 + 423.5$
 $= 1,952.4 \text{ kips}$

Ultimate Capacity $Q = 1,952.4 + 1,924 = 3,876.4 \text{ kips}$

Design Capacity $Q_d = 2,584.3 \text{ kips}$

By C. S. Jones Date 11/2/1977 Subject Structural Concrete Pile Capacity
 Date 4-2-78 Job No. 27-771-7A Calculation Pile Pile Capacity

(iii) At Penetration 139.5 ft (=170' - 10.5')

$$\text{End Bearing } Q_p = 100 \times 9.62 = 962 \text{ kips}$$

$$\text{Skin Friction } Q_s = 2,193.4 + 1.79 \times (25 - 10.5) \times 10.996$$

(S-2.17)

$$= 2,193.4 + 271.1$$

$$= 2,464.5 \text{ kips}$$

$$\text{Ultimate Capacity } Q_u = 2,464.5 + 962 = 3,426.5 \text{ kips}$$

$$\text{Design Capacity } Q_d = 2,277.7 \text{ kips}$$

By: C. S. [unclear] Client: U.S.N.V. Subject: Structural Concept Analysis of
Date: 4-28-72 Job No: 27-221-72 Calculation: Pile Capacity Calculations

2.4 PILE CAPACITY IN TENSION

$$Q = Q_s$$

where Q_s = skin friction on the wall of the pile

Project: _____ Subject: _____ (Page)
 Date: _____ Calculation: _____

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Tension ---

O.D. = 30"

$A_s = \pi D(\Delta L) = 7.07(\Delta L)$ SQ. FT

Penetration Below Mudline (ft)	Unit Skin Friction (ksf)	Ave. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kip)	Total Skin Friction (kip)
0	0	0.165	20	23.9	0
20	0.33				23.9
20 35	0.29 0.46	0.375	15	44.2	70.1
35 56	0.60 0.95	0.775	21	127.8	197.9
56 79	0.80 1.10	0.950	23	171.6	369.5
79 82	1.35 1.43	1.390	3	22.8	402.3
82 107	1.43 2.00	1.715	25	336.7	739.0
107 115	2.00 2.00	2.00	8	125.7	864.7
115 145	2.00 2.00	2.00	30	471.2	1,335.9
145 170	1.70 1.70	1.70	25	333.2	1,669.7
170 205	1.48 1.72	1.60	35	439.8	2,109.5
205 280	1.72 2.30	2.01	75	1,184.0	3,293.5
280 300	2.20 2.10	2.35	20	369.1	3,662.6
			$\Sigma = 200$ ft		

By C. J. ... Date 4/11/77 Subject St. ...
 Date ... Job No. ... Calculation ...

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Tension ---

O.D. = 36"

$A_s = \pi D (\Delta L) = 3,423 (\Delta L) \text{ sq. ft}$

Penetration Below Shellin (ft)	Unit Skin Friction (ksf)	Ave. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (ft)	Sk. Friction in Segment (kips)	Total sk. Friction (kips)
0	0				0
20	0.33	0.165	20	31.1	31.1
20 35	0.29 0.46	0.375	15	53.0	84.1
35 56	0.60 0.95	0.775	21	153.4	237.5
56 79	0.80 1.10	0.950	23	205.9	443.4
79 82	1.35 1.43	1.390	3	39.3	482.7
82 107	1.43 2.00	1.715	25	404.1	886.8
107 115	2.00 2.00	2.00	8	130.8	1,037.6
115 145	2.00 2.00	2.00	30	563.5	1,603.1
145 170	1.70 1.70	1.70	25	400.6	2,003.7
170 205	1.48 1.72	1.60	35	527.8	2,531.5
205 280	1.72 2.30	2.01	75	1,420.8	3,952.3
280 300	2.30 2.50	2.35	20	443.0	4,395.3
			$\Sigma = 200 \text{ ft}$		

By J. J. Jones Client U.S. Navy Subject Structural Support Analysis 13-212
 Date 11-1-64 Job No 7-211-1 Calculation Soil Friction Capacity

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Tension ---

O.D. = 39"

$A_s = \pi D (\Delta L) = 10.21 (\Delta L)$ SQ. FT

Penetration Below Surface (ft.)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0	0.165	20	33.7	0
20	0.33	0.375	15	57.4	33.7
35	0.46	0.775	21	166.2	91.1
56	0.95	0.950	23	223.1	357.3
79	1.10	1.390	3	42.6	480.4
82	1.43	1.715	25	437.8	523.0
107	2.00	2.00	8	163.4	960.8
115	2.00	2.00	30	612.6	1,124.2
145	2.00	1.70	25	433.9	1,736.9
170	1.70	1.60	35	571.8	2,170.7
205	1.72	2.01	75	1,533.2	2,742.5
280	2.30	2.35	20	479.9	4,221.7
300	2.30				4,761.6
			$\Sigma = 300$ ft		

CREST OFFSHORE, INC.

Sheet 2 of 4

By C. Clark Date 4/2/77 Sub. No. 15 Job No. 27771-10 Calculation 15.2.2.1

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Tension ---

O.D. = 42"

$A_s = \pi D(\Delta L) = 12.976(\Delta L)$ sq. ft

Penetration Below Mullion (ft)	Unit Skin Friction (ksf)	Ave. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (ft)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0				0
20	0.33	0.165	20	36.3	36.3
20 35	0.29 0.46	0.375	15	61.9	98.2
35 56	0.60 0.95	0.775	21	179.0	277.2
56 79	0.80 1.10	0.950	23	240.3	517.5
79 82	1.35 1.43	1.390	3	45.9	563.4
82 107	1.43 2.00	1.715	25	471.5	1,034.9
107 115	2.00 2.00	2.00	8	175.9	1,210.8
115 145	2.00 2.00	2.00	30	659.8	1,870.6
145 170	1.70 1.70	1.70	25	467.3	2,337.9
170 205	1.48 1.72	1.60	35	615.3	2,953.7
205 220	1.72 2.20	2.01	75	1,637.6	4,591.3
220 300	2.20 2.35	2.35	20	516.8	5,108.1
			$\Sigma = 300$		

By: J. J. [unclear] Client: U.S. [unclear] Subject: Offshore Concrete [unclear]
 Date: 1-1-72 Job No: 21-11-32 Calculation: Pipe Pipe Capacity Curves

42" Dia Pipe (Q₁ - Q₂) --- Tension

Penetration Substrate (Ft)	30"Ø Q (KIPS)	36"Ø Q (KIPS)	39"Ø Q (KIPS)	42"Ø Q (KIPS)
0	0	0	0	0
20	23.9	31.1	33.7	36.3
35	70.1	84.1	91.1	78.2
56	197.9	237.3	257.3	277.2
79	369.3	443.4	480.4	517.5
82	403.3	482.7	523.0	563.4
107	733.0	886.8	960.8	1,034.1
115	834.7	1,037.6	1,124.2	1,210.8
145	1,333.9	1,603.1	1,736.8	1,870.6
170	1,663.7	2,003.7	2,170.7	2,337.9
205	2,109.5	2,531.5	2,742.9	2,953.7
250	3,293.5	3,832.3	4,231.7	4,611.3
300	3,662.6	4,395.3	4,761.6	5,128.1

Client U.S. NRP Subject Structural Connection
 Date 1-28-86 Job No. 22-772-107 Calculation Pipe pile Cap and Curves

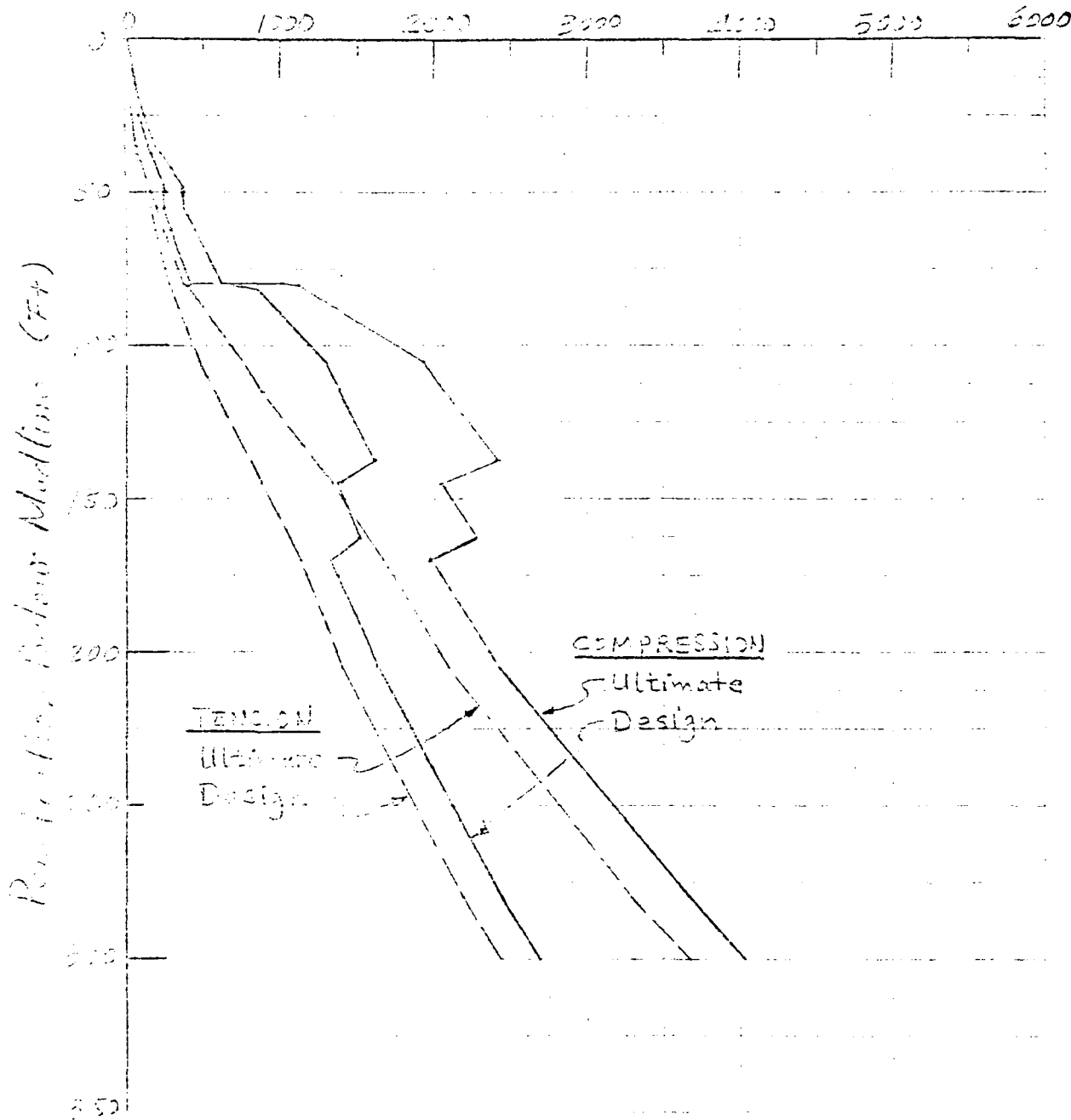
Design Pipe Capacity ($Q_d = Q/F.S.$) --- Tension

F.S. = 1.5

Penetration Elevation (Ft)	30" Q_d (kips)	36" Q_d (kips)	39" Q_d (kips)	42" Q_d (kips)
0	0	0	0	0
20	17.3	20.7	22.5	24.2
30	43.7	56.1	60.7	65.5
35	131.9	153.3	171.5	184.8
56	245.3	295.6	320.5	343.0
79	268.2	321.2	348.7	373.6
82	422.7	591.2	640.5	689.9
107	576.3	691.7	742.5	807.2
115	820.6	1062.7	1157.9	1247.1
143	1112.1	1335.2	1447.1	1552.6
170	1406.3	1627.7	1823.3	1969.1
205	2192.7	2634.2	2854.5	3074.2
280	3421.7	3930.2	3174.4	3418.7

Client: U.S. M.I.D. Subject: Structural Concept Hydrocode
Date: 4-11-92 Job No: 3-1-171-92 Calculation: Pipe Pile Capacity Curves

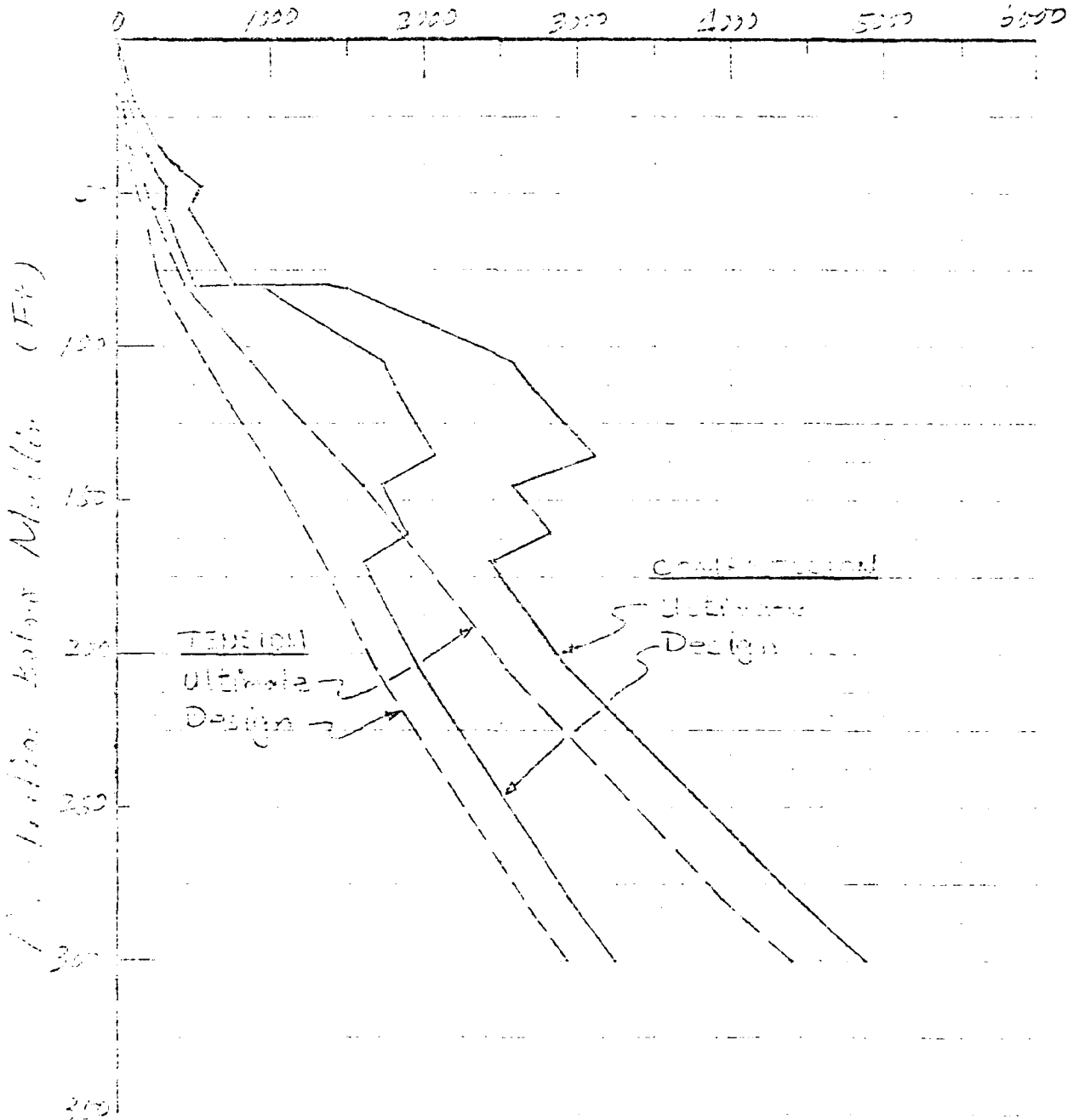
Pile Capacity (Kips)



30 in. Diameter Pipe Piles

By C. Chinn Client U.S. Navy Subject Structural Concept Analysis
Date 4-1-77 Job No. 22-721-71 Calculation Pile Capacity

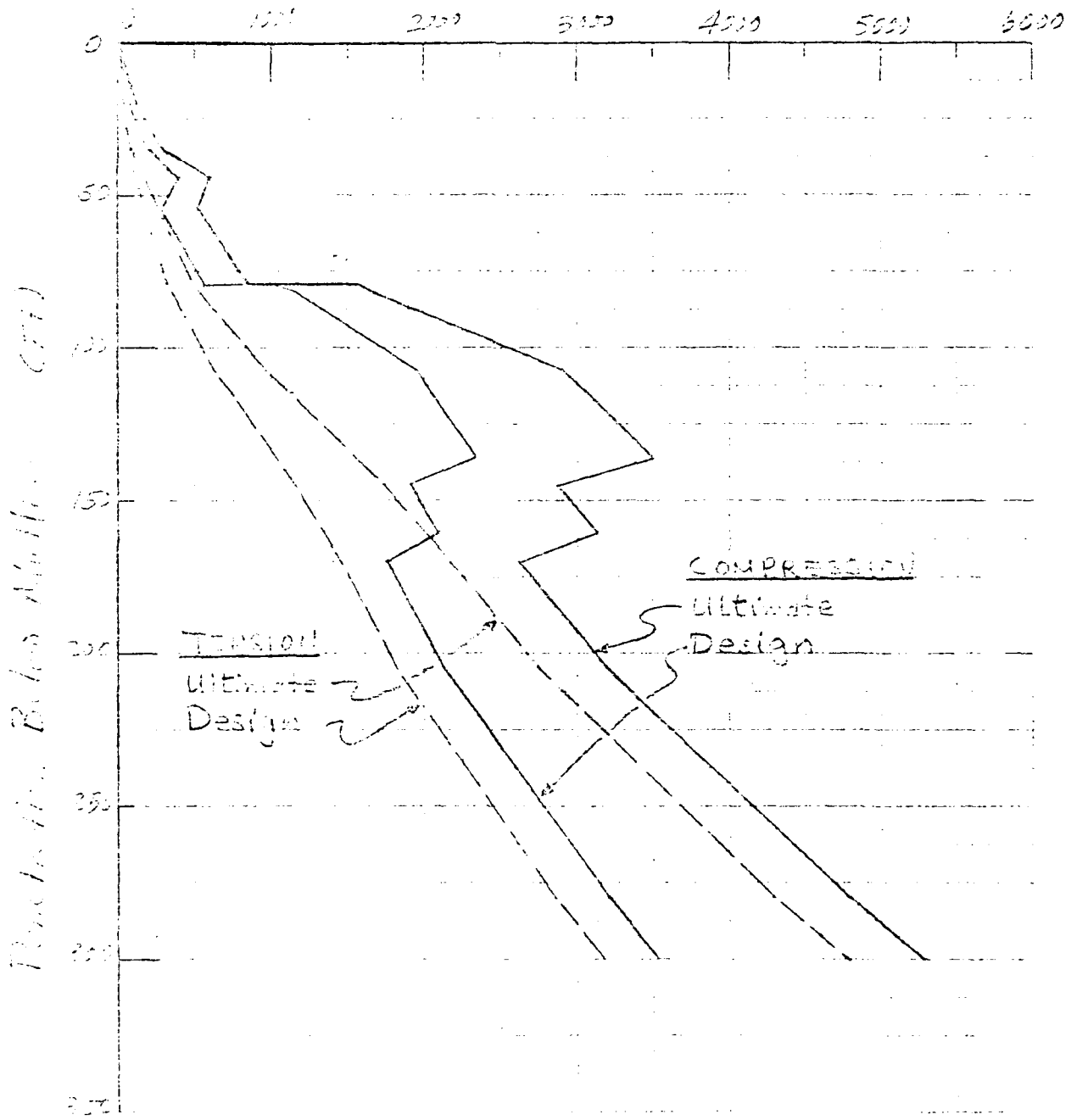
Pile Capacity (kips)



36-in. Diameter Pipe Piles

By E. J. [unclear] Client U.S. NAVY Subject Structural Capacity Analysis
Date 12-7-66 Job No. 27-12-92 Calculation Pile Capacity Curves

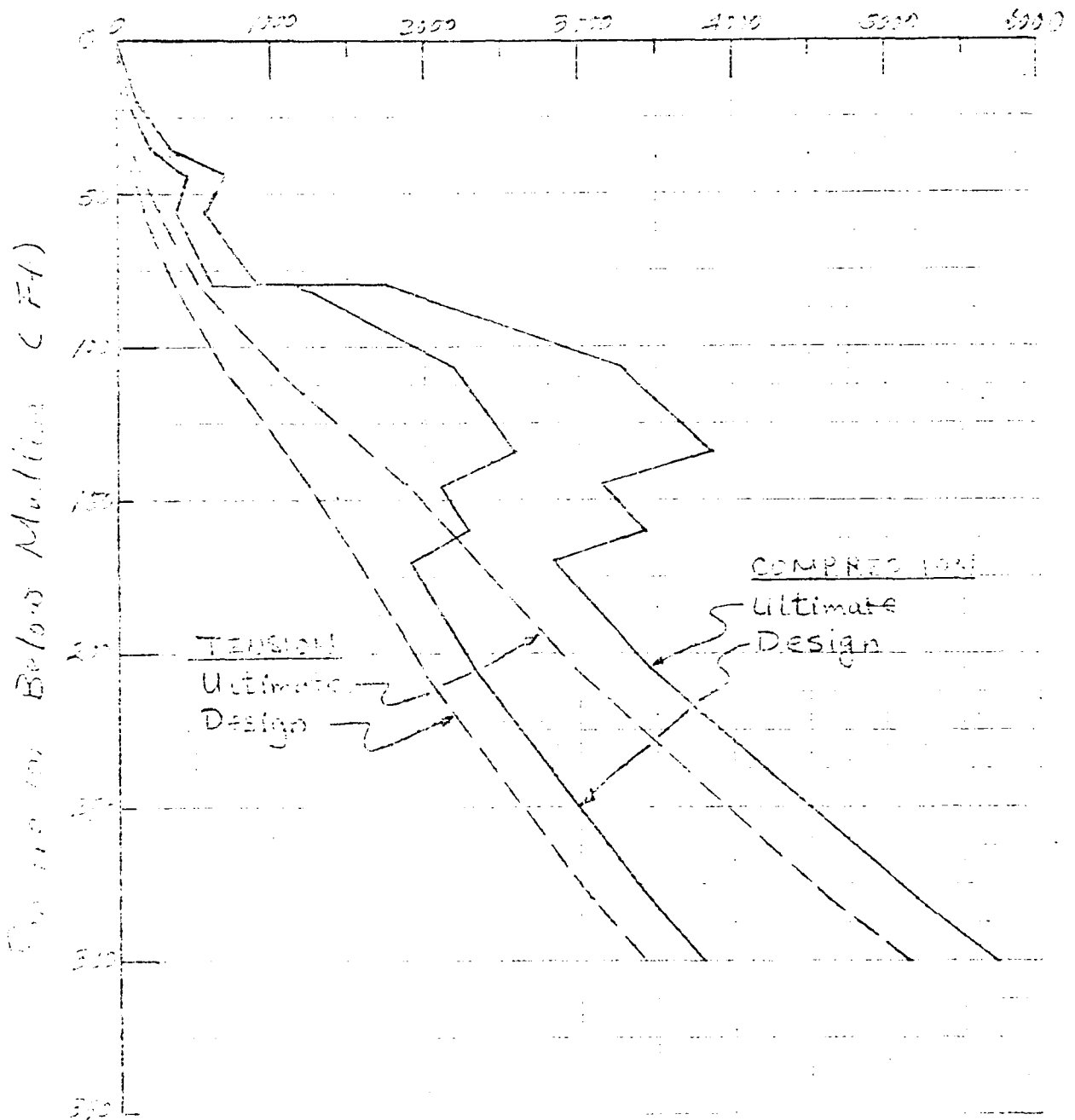
Pile Capacity (kips)



39-in. Diameter Pipe Piles

Client U.S. NAVY Subject Structural Concept Study
Date 4/1/72 Job No. 87-271-72 Calculation Pile Capacity Curves

Pile Capacity (kips)



42-in Diameter Pipe Piles

SECTION 3

PILE DRIVING RESISTANCE CURVES

3.1 INTRODUCTION

Driving resistance curves are developed using the stress wave approach as presented in the McClelland Report. It should be noted that these curves are empirical and approximate and in no way assume attainment of the desired penetration.

By C. Cherr Client U.S. NAVY Subject Structural Concepts Analysis (3-212)
Date 4-22-76 Job No. 27-271-92 Calculation Pile Driving Resistance Curves

3-2 30-IN. DIAMETER PIPE PILES

Estimated Driving Resistance

= 50% skin Friction in Clay

100% skin Friction in Sand

No End Bearing

CREST OFFSHORE, INC.

Sheet 203 of 25

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-14-76 Job No. 27-771-92 Calculation Pile Driving Resistance Curves

Skin Friction Capacity ($Q_s = f_{s} A_s$)

--- Compression ---

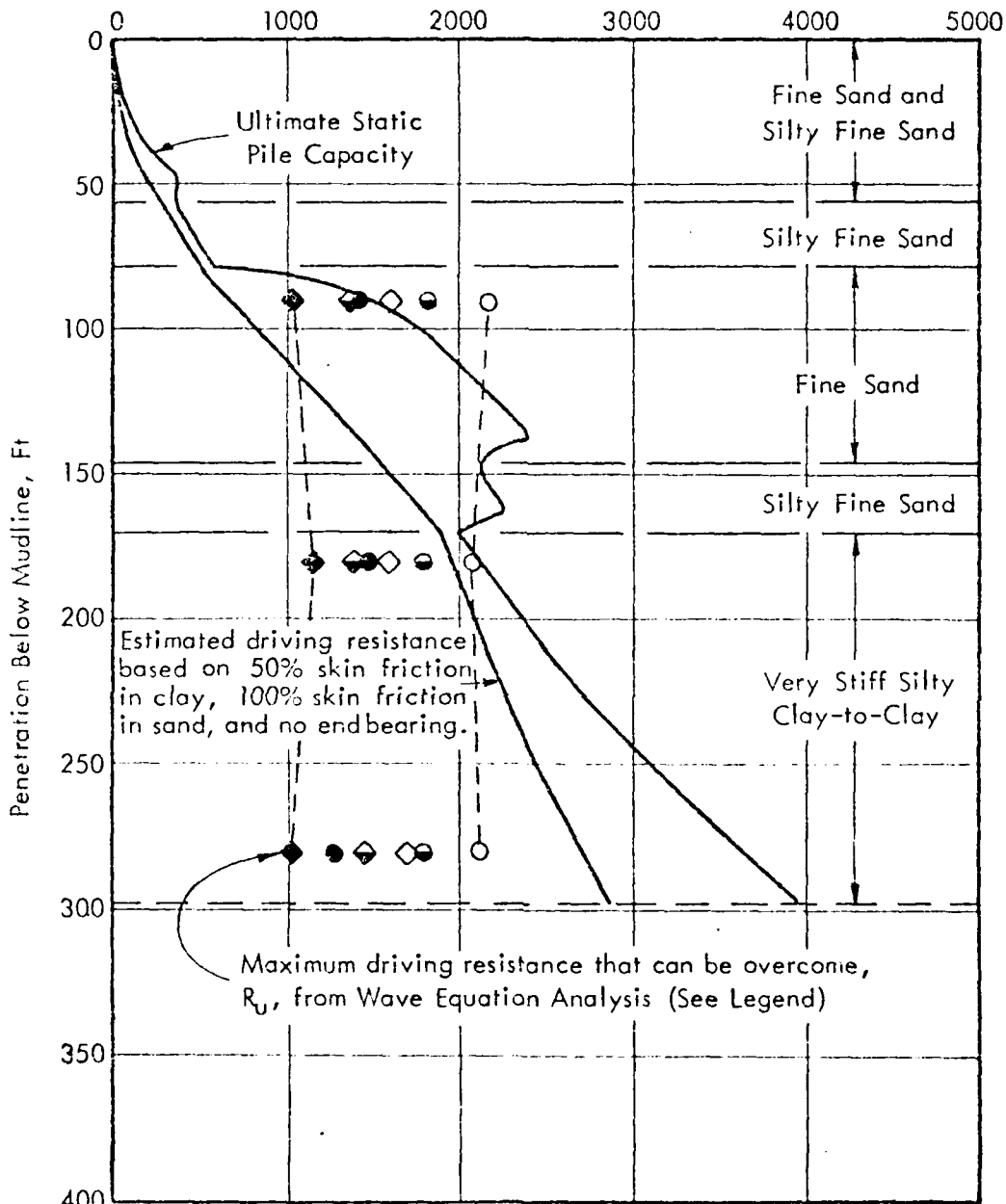
$O.D. = 30"$

$A_s = \pi D (\Delta L) = 7.854 (\Delta L) \text{ SQFT}$

Penetration Below Mudline (ft)	Unit Skin Friction (ksf)	Avg. Unit Skin Friction f_s (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total skin Friction (kips)
0	0				0
20	0.45	0.225	20	35.3	35.3
20 35	0.40 0.67	0.535	15	63.0	98.3
35 56	0.85 1.30	1.075	21	177.3	275.6
56 79	1.10 1.65	1.375	23	248.4	524.0
79 82	1.30 2.00	1.950	3	45.9	570.1
82 107	2.00 2.00	2.00	25	392.7	962.8
107 115	2.00 2.00	2.00	8	125.7	1088.5
115 145	2.00 2.00	2.00	30	471.2	1559.7
145 170	1.70 1.70	1.70	25	333.8	1893.5
170 205	1.48 1.72	1.60	35	213.9 *	2113.4
205 280	1.72 2.20	2.01	75	149.9 592.0 +	2705.4
280 300	2.30 2.10	2.35	20	154.5 + 259.1	2864.7
			$\Sigma = 300 \text{ ft}$		
* 50% SKIN FRICTION IN CLAY					

By C. J. ... Client U.S. NAVY Subject Structural Concept for ...
 Date 4-14-76 Job No. 27-171-92 Calculation Pile Driving Resistance Curves

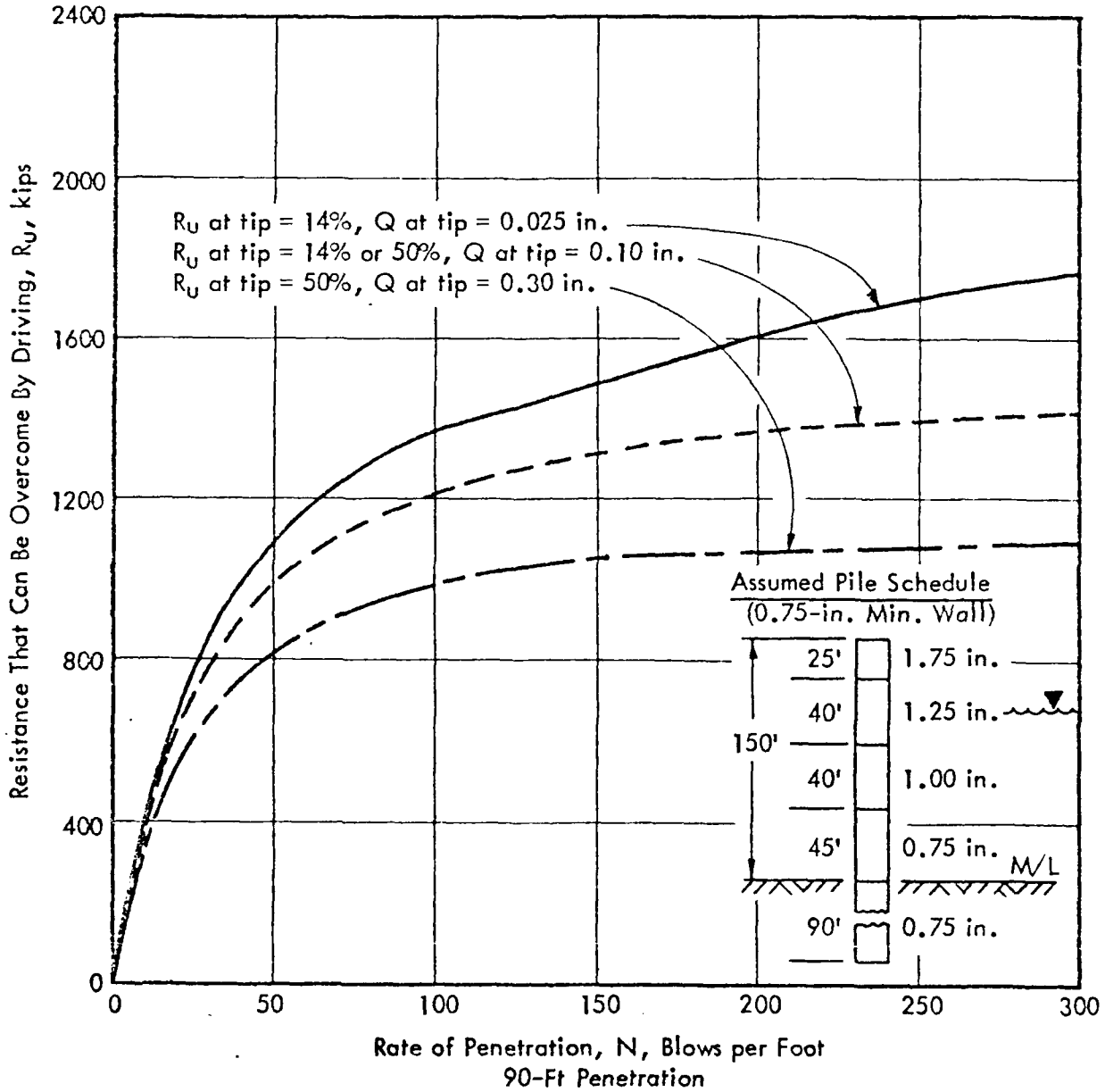
Ultimate Static Pile Capacity, Kips
 Estimated Driving Resistance, Kips



Boring 1

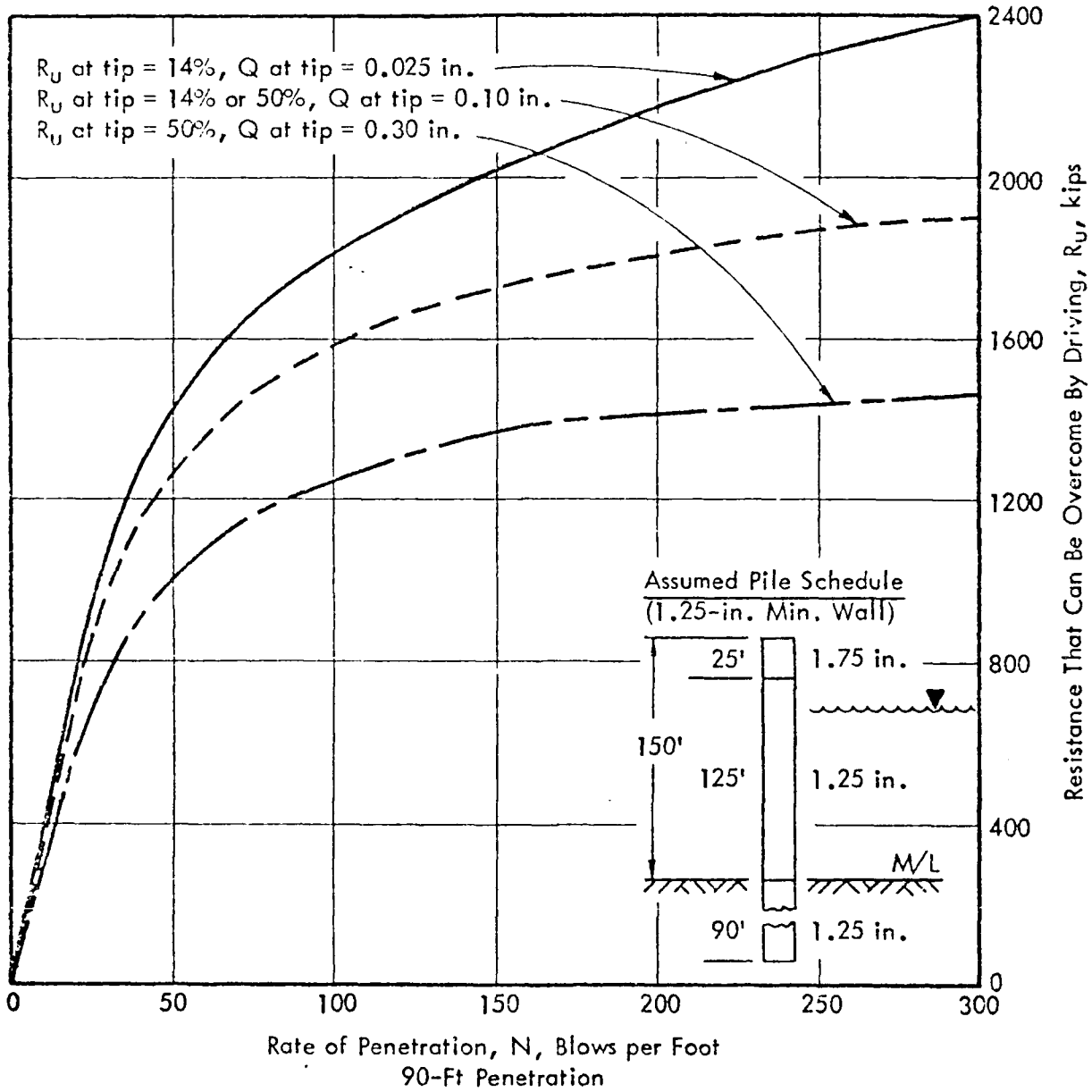
LEGEND					
Symbol		R_u at tip, %, for pile penetration of			Q at tip, inches
0.75-in. Min. Wall	1.25-in. Min. Wall	90'	180'	280'	
◆	●	50	50	2	0.3
◇	○	50 or 14	35 or 6	2	0.1
◇	○	14	14	2	0.025

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-14-76 Job No. 7-771-72 Calculation Pile Driving Resistance Curves

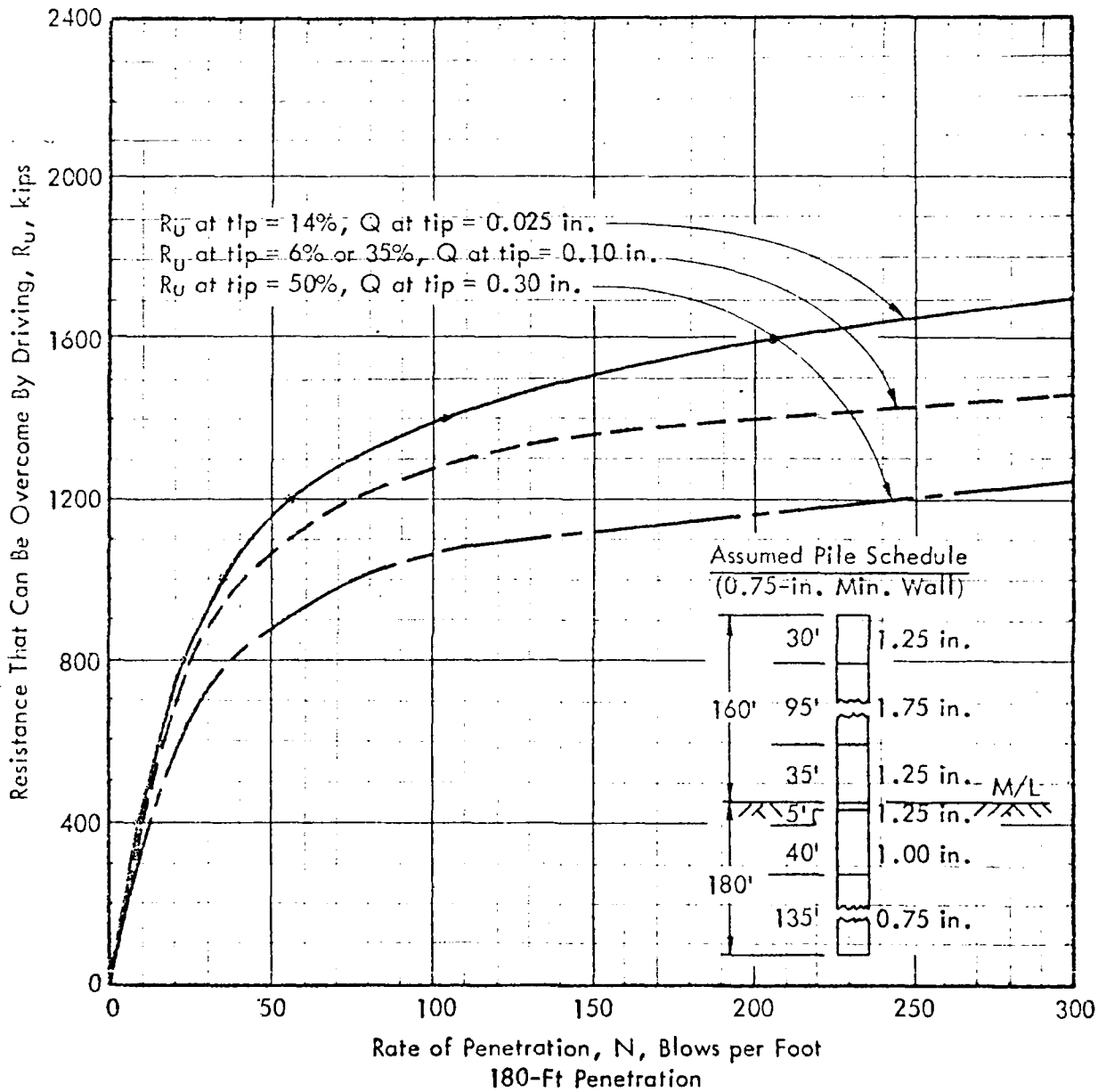


Vulcan 040 Hammer	% R_U at tip - See Above
Wt. of Ram = 40,000 lbs	Spring Constant = 2.78×10^6 lbs/in.
Rated Energy = 120,000 ft-lbs	Damping Factor, side & tip, $J = 0.15$
Hammer Efficiency = 0.75	Quake Factor, side, $Q = 0.10$ in.
Wt. of Pile Cap = 27,800 lbs	Quake Factor, tip, - See Above

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis of pile
 Date 4-15-76 Job No. 27-771-92 Calculation Pile Driving Resistance Curves

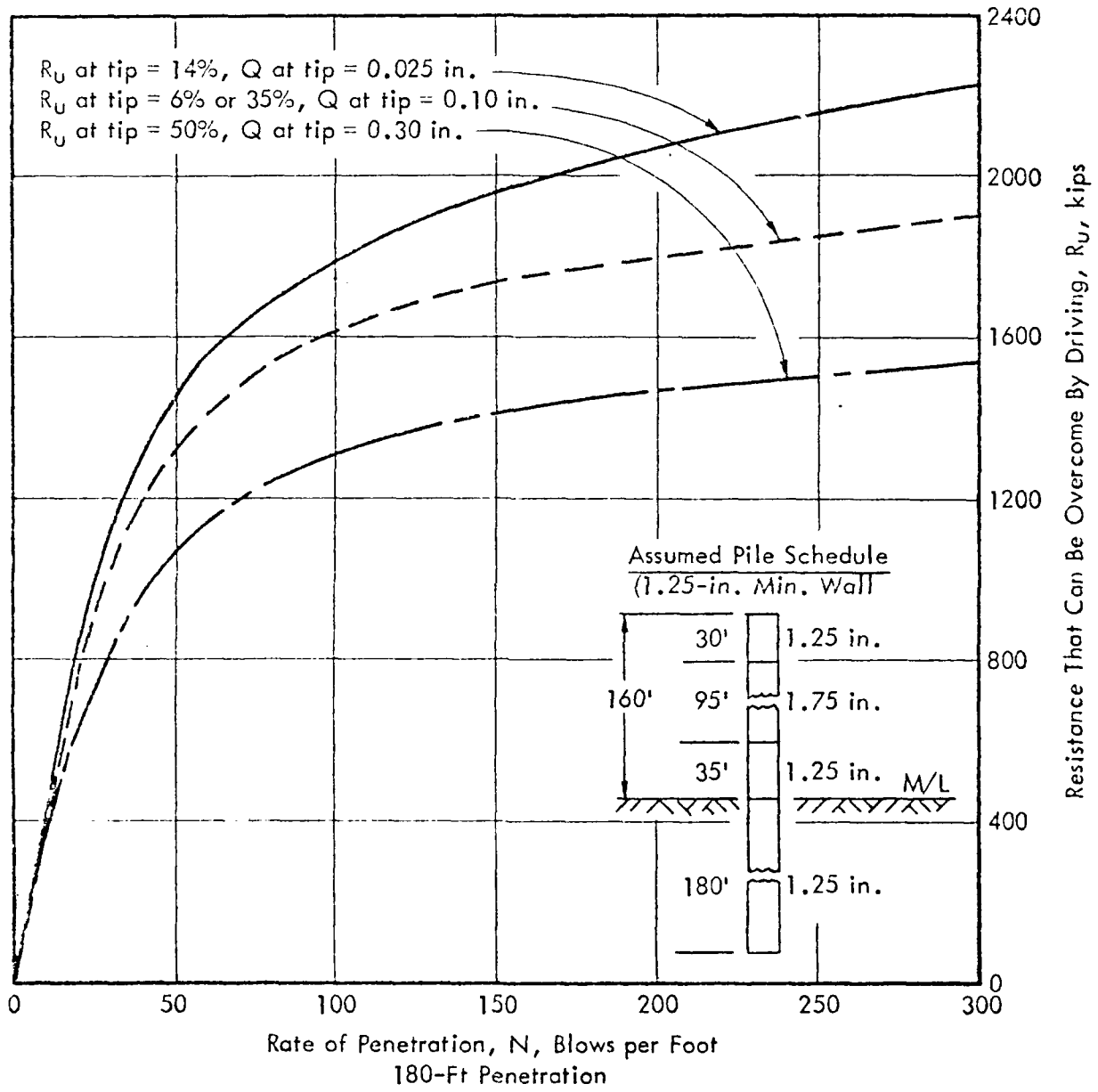


By C. Chern Client U.S. Navy Subject Structural Concept Analysis
 Date 11-96 Job No. 27-271-91 Calculation Pile Driving Resistance Curves

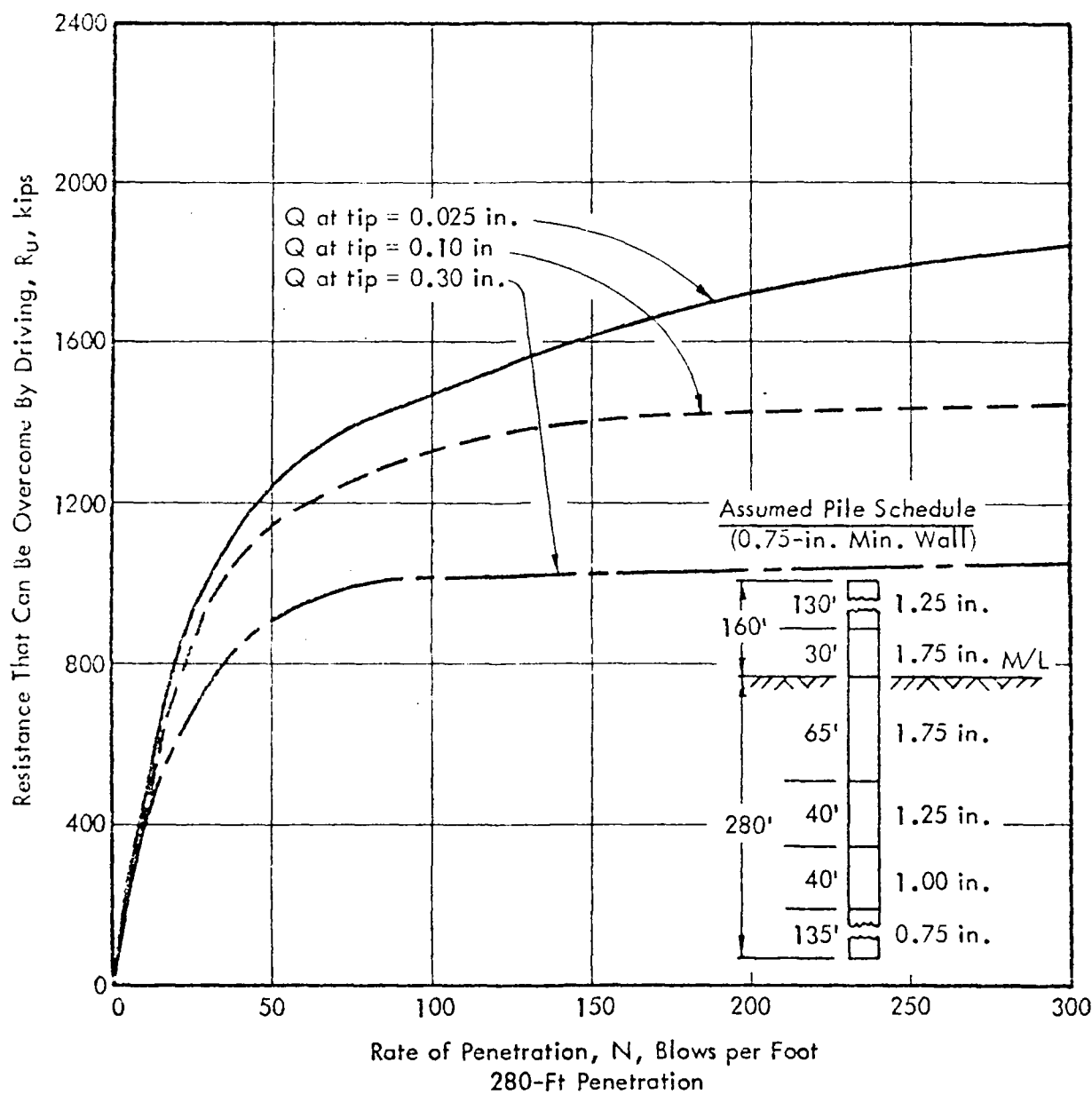


Vulcan 040 Hammer	% R_U at tip - See Above
Wt. of Ram = 40,000 lbs	Spring Constant = 2.78×10^6 lbs/in.
Rated Energy = 120,000 ft-lbs	Damping Factor, side & tip, $J = 0.15$
Hammer Efficiency = 0.75	Quake Factor, side, $Q = 0.10$ in.
Wt. of Pile Cap = 27,800 lbs	Quake Factor, tip, - See Above

By C. Chera Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-11-76 Job No. 27-771-92 Calculation Pile Driving Resistance Curves

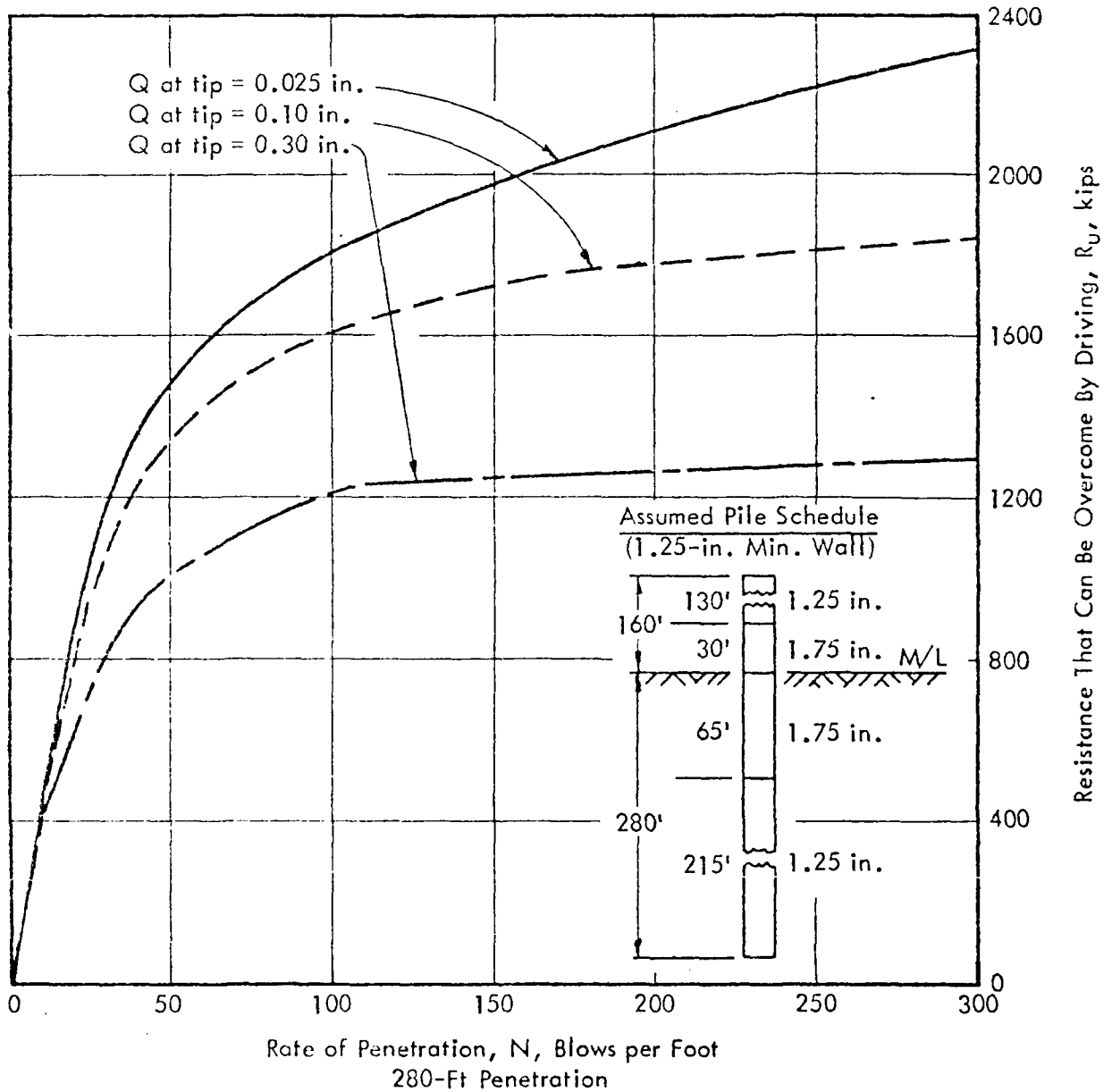


By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-18-76 Job No. 37-771-92 Calculation Pile Driving Resistance Curves



Vulcan 040 Hammer	% R_U at tip = 2%
Wt. of Ram = 40,000 lbs	Spring Constant = 2.78×10^6 lbs/in.
Rated Energy = 120,000 ft-lbs	Damping Factor, side & tip, $J = 0.15$
Hammer Efficiency = 0.75	Quake Factor, side, $Q = 0.10$ in.
Wt. of Pile Cap = 27,800 lbs	Quake Factor, tip, - See Above

By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-14-76 Job No. 2777-92 Calculation Pile Driving Resistance Curves



By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
Date 4-24-76 Job No. 87-771-85 Calculation Pile Driving Resistance

3.3 36-IN. DIAMETER PIPE PILES

The data and the "STRESS WAVE ANALYSIS PROGRAM" printouts used to plot the pile driving resistance curves set forth in this section were compiled in APPENDIX A.2

By C. Chern Client U.S. NAVY Subject Structural Concepts Analysis
 Date 4-14-76 Job No. 27-771-22 Calculation Pile Driving Resistance

Skin Friction Capacity ($Q_s = f_{as} A_s$)

--- Compression ---

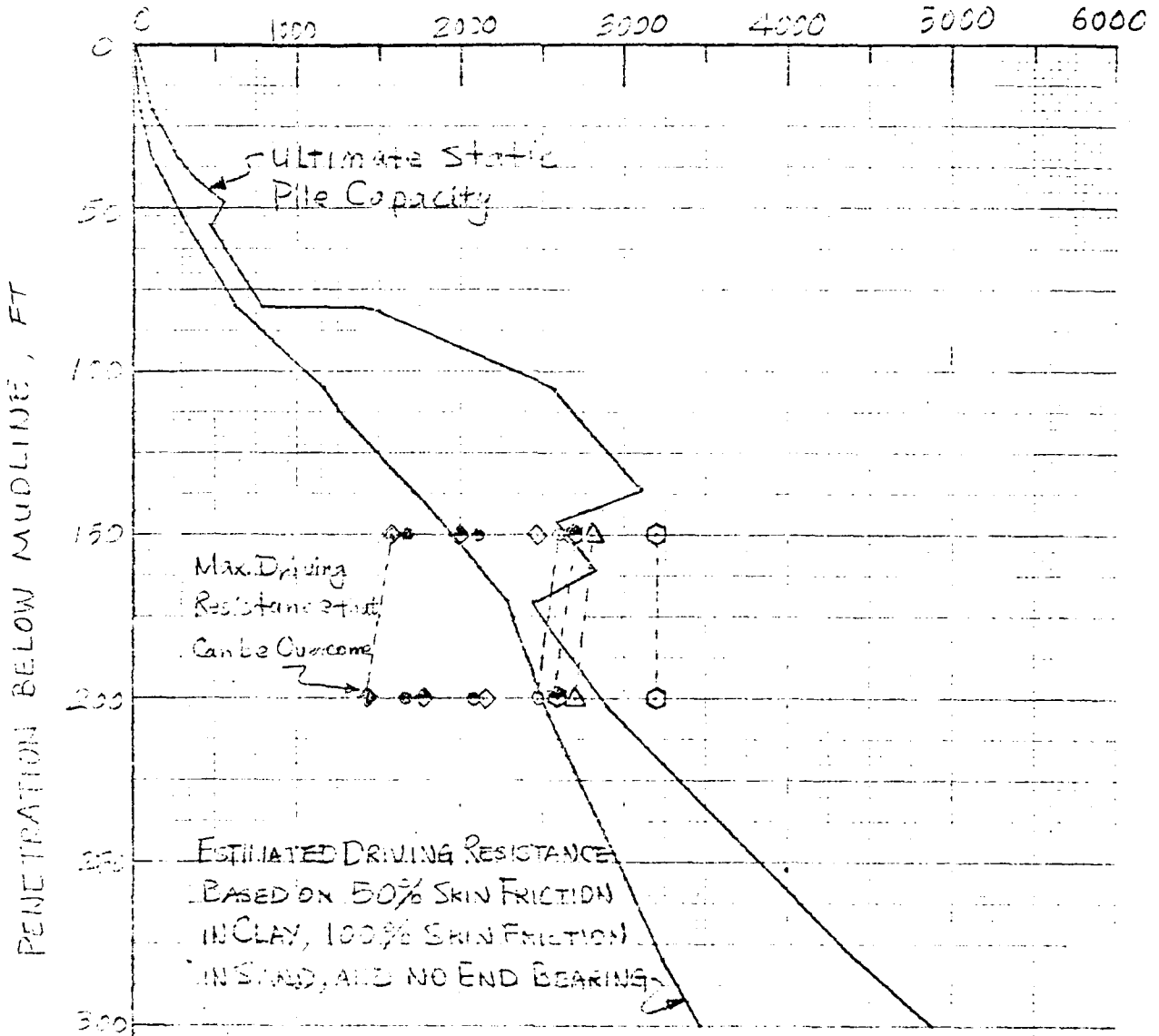
O.D. = 26"

$A_s = \pi D (L) = 2.428(L)$ SQ. FT

Penetration Below 10 min (ft)	Unit Skin Friction (ksf)	Avail. Unit Skin Friction f_{as} (ksf)	Segment Length (ΔL) (FT)	Skin Friction in Segment (kips)	Total Skin Friction (kips)
0	0				0
20	0.45	0.225	20	42.4	42.4
20 35	0.40	0.535	15	75.6	118.0
35 56	0.85	1.075	21	212.8	330.8
56 79	1.10	1.375	23	298.1	628.9
79 82	1.20	1.950	3	55.1	684.0
82 107	2.00	2.00	25	471.3	1155.3
107 115	2.00	2.00	8	150.8	1,306.1
115 145	2.00	2.00	30	565.5	1,871.6
145 170	1.70	1.70	25	400.6	2,272.2
170 205	1.45	1.60	35	263.2*	2,535.1
205 280	1.72	2.01	75	710.4*	3,245.5
280 300	2.30	2.35	20	221.5*	3,467.0
	2.40				
				$Z = 300$ ft	
26" O.D. SKIN FRICTION IN CLAY					

by C. C. Carr Client U.S. Navy Subject Structural Concept Analysis
 Date 4-14-76 Job No. 27-77-92 Calculation Pile Driving Resistance

ULTIMATE STATIC PILE CAPACITY, KIPS
 ESTIMATED DRIVING RESISTANCE, KIPS

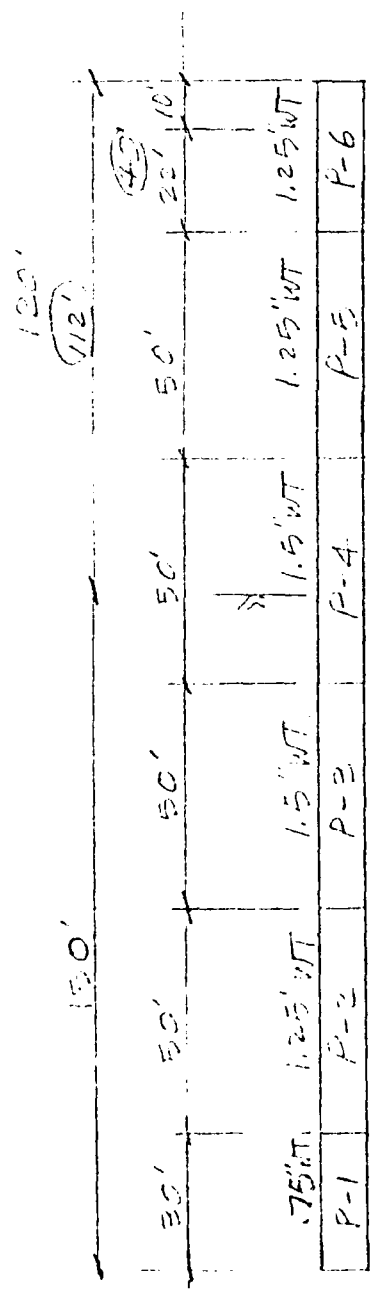


SYMBOL			Ru at Pile Tip, %		Q at Pile Tip, in.	Hammer
1.75" WT Min.	1.25" WT Min.	1.5" WT Min.	150'	200'		
◆	○		50	50	.3	Vulcan
◆	○		35	35	.1	040
◇	○	△	14	14	.025	
		⊙	35	35	.1	Vulcan
		○	14	14	.025	060

36-IN. DIAMETER PIPE PILES

By C. Chan Client LES 1407 Subject Installation Concept Analysis
 Date 5-15-95 Job No. 27-771-9 Calculation Installation Concept

Assumed Pile Schedule -- 150 FT PENETRATION
 .75" WALL THK. MIN.



Vulcan 040 Hammer
 Wt. of Ram = 40,000 lbs
 Rated Energy = 120,000 ft-lbs
 Hammer Efficiency = 0.75
 Wt. of Pile Cap = 27,800 lbs

R_u at tip = 14%, Q at tip = 0.025 in.
 R_u at tip = 6% or 35%, Q at tip = 0.10 in.
 R_u at tip = 50%, Q at tip = 0.30 in.

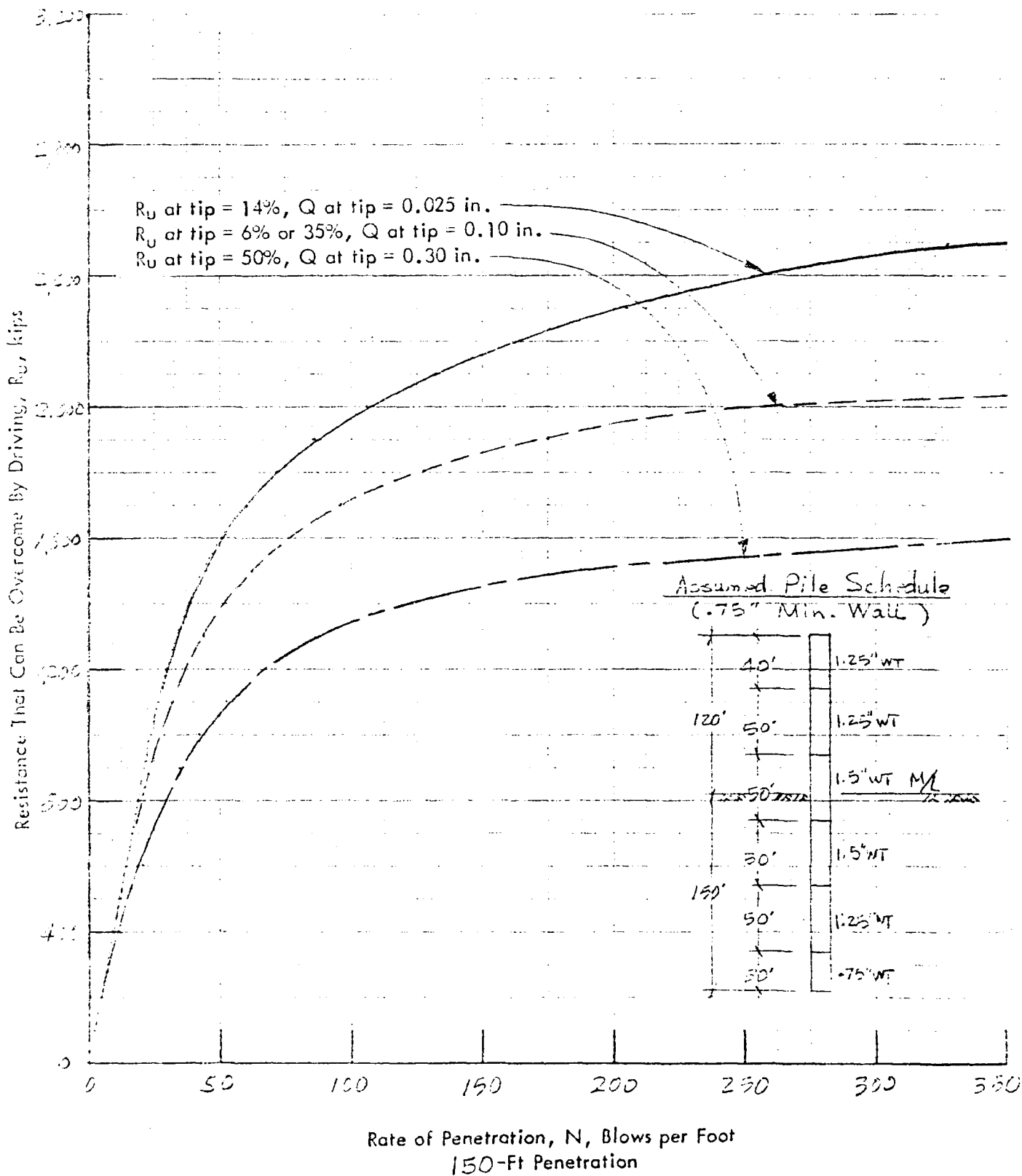
Spring Constant = 2.78×10^6 lbs/in.
 Damping Factor, side & tip, $J = 0.15$
 Quake Factor, side, $Q = 0.10$ in.
 Quake Factor, tip, - See Above

By C. Chern Client U.S. NAVY

Subject Structural Concept Analysis

Date 4-12-75 Job No. 27-771 95

Calculation Pile Driving Resistance



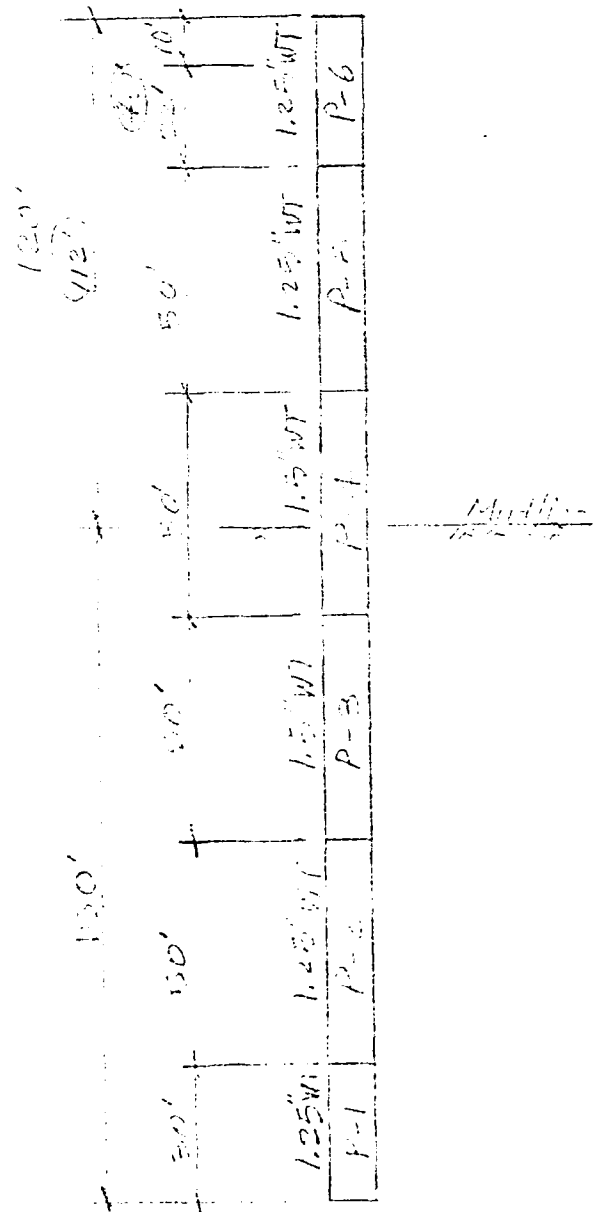
By C. Chern Client U.S. NAVY

Subject Shannon Point Expansion

Date 4-19-76 Job No. 27-771-22

Calculation Pile Driving Results - Case

Assumed Pile Schedule -- 150 FT PENETRATION
1.25" WALL THK. MIN.

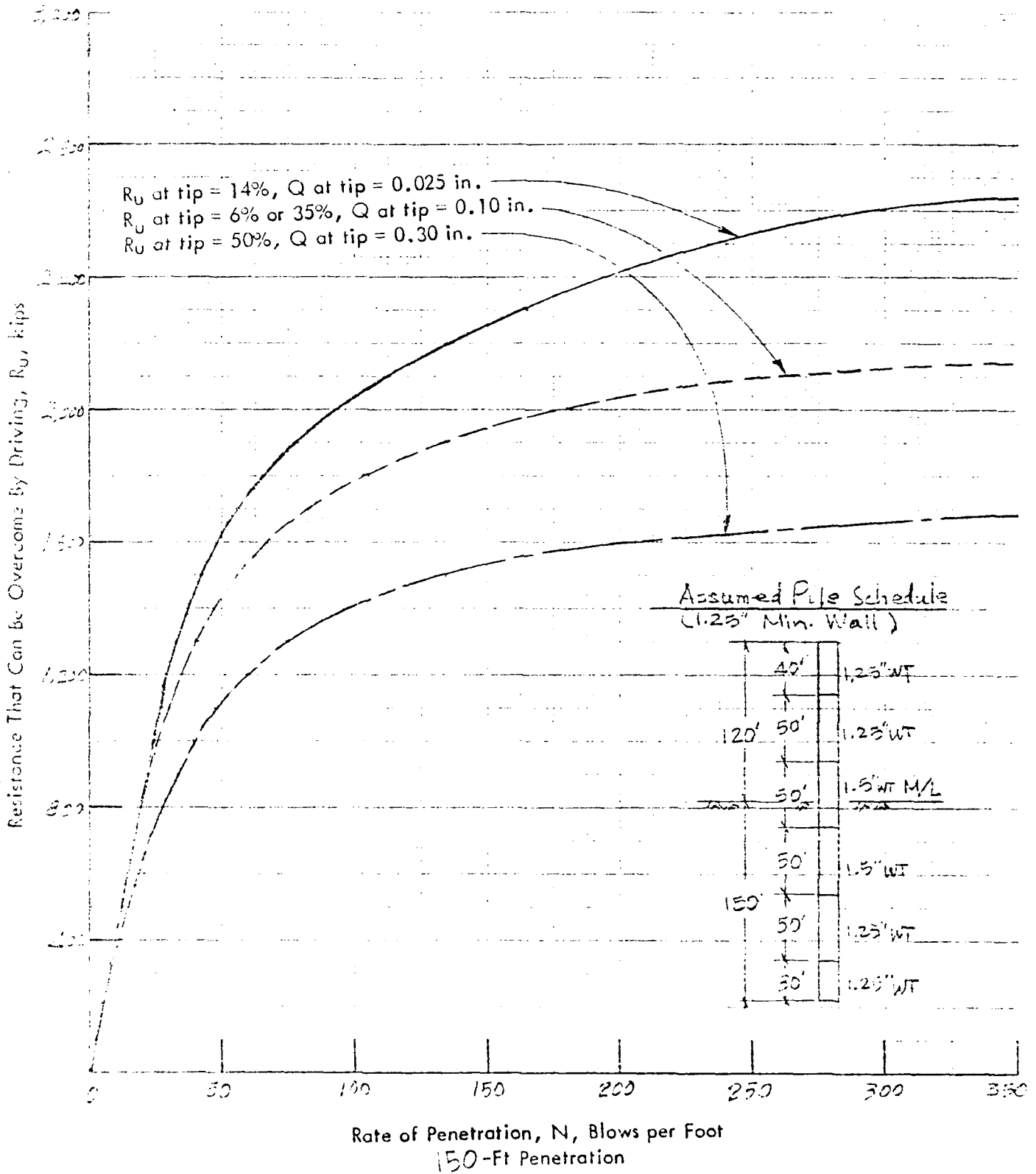


Vulcan 040 Hammer
Wt. of Ram = 40,000 lbs
Rated Energy = 120,000 ft-lbs
Hammer Efficiency = 0.75
Wt. of Pile Cap = 27,800 lbs

R_U at tip = 14%, Q at tip = 0.025 in.
 R_U at tip = 6% or 35%, Q at tip = 0.10 in.
 R_U at tip = 50%, Q at tip = 0.30 in.

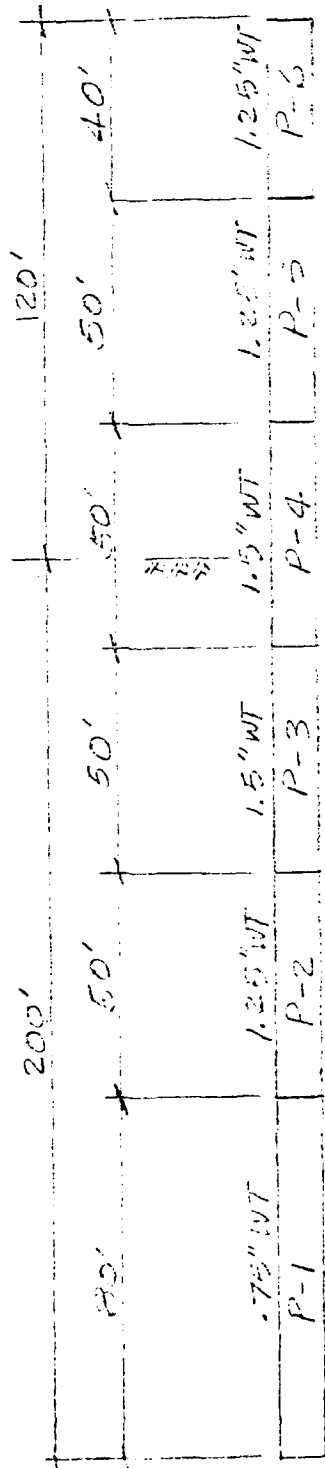
Spring Constant = 2.78×10^6 lbs/in.
Damping Factor, side & tip, $J = 0.15$
Quake Factor, side, $Q = 0.10$ in.
Quake Factor, tip, - See Above

By C. Chero Client U.S. NAVY Subject Structural Concept Analysis (12)
 Date 4-30-66 Job No. 27-771-92 Calculation Pile Driving Analysis



By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-19-76 Job No. 27-771-12 Calculation Pile Driving Resistance Curves

Assumed Pile Schedule -- 200 FT PENETRATION
.75" WALL THK. MIN.



Mating
~~12-15-76~~

Vulcan 040 Hammer
 Wt. of Ram = 40,000 lbs
 Rated Energy = 120,000 ft-lbs
 Hammer Efficiency = 0.75
 Wt. of Pile Cap = 27,800 lbs

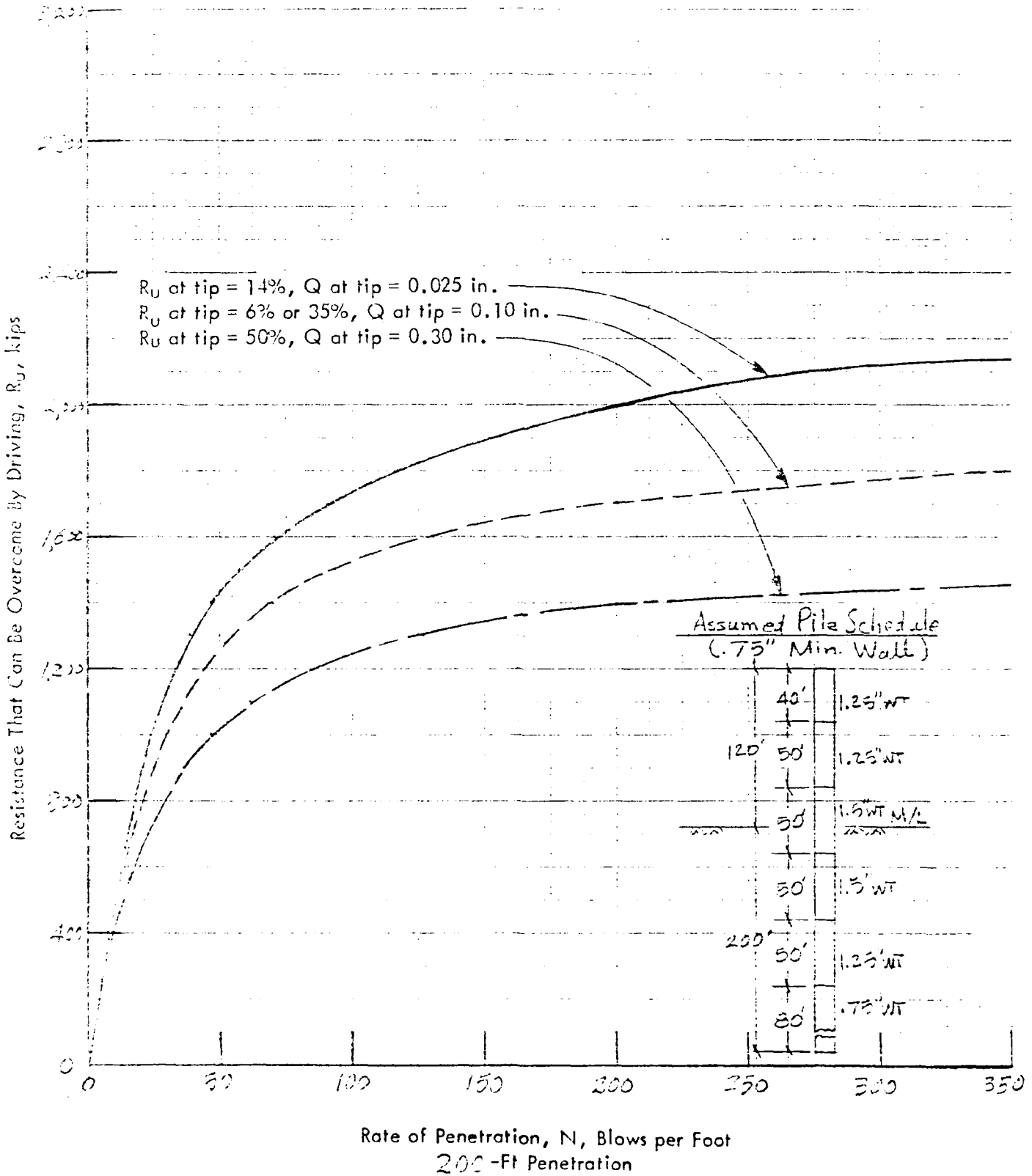
Spring Constant = 2.78×10^6 lbs/in.
 Damping Factor, side & tip, J = 0.15
 Quake Factor, side, Q = 0.10 in.
 Quake Factor, tip, - See Above

By C. Chas. Client U.S. NAVY

Subject Structure Concept Analysis

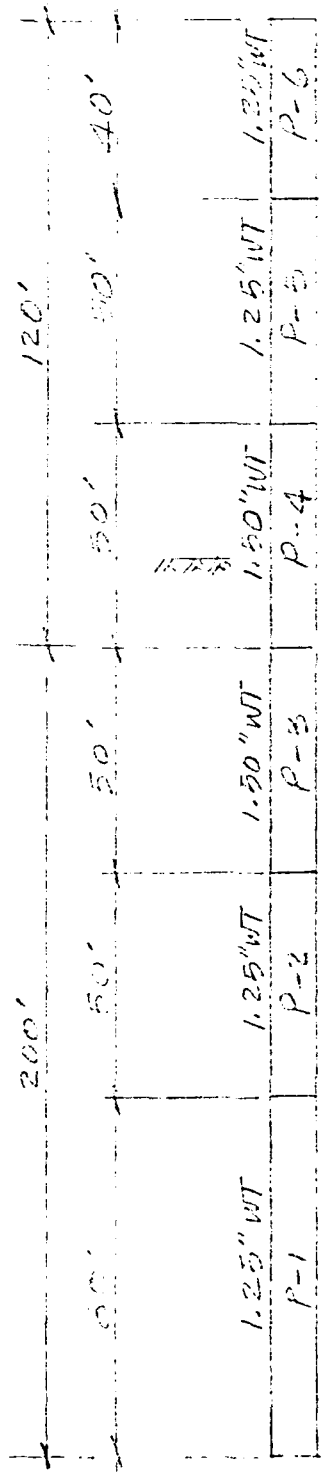
Date 4-20-75 Job No. 27-771-22

Calculation Pile Driving Resistance



By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-19-76 Job No. 27-571-92 Calculation Pile Driving Resistance

Assumed Pile Schedule -- 200 FT PENETRATION
 1.25" WALL THK. MIN.



Mudline
 15' 0" 0"

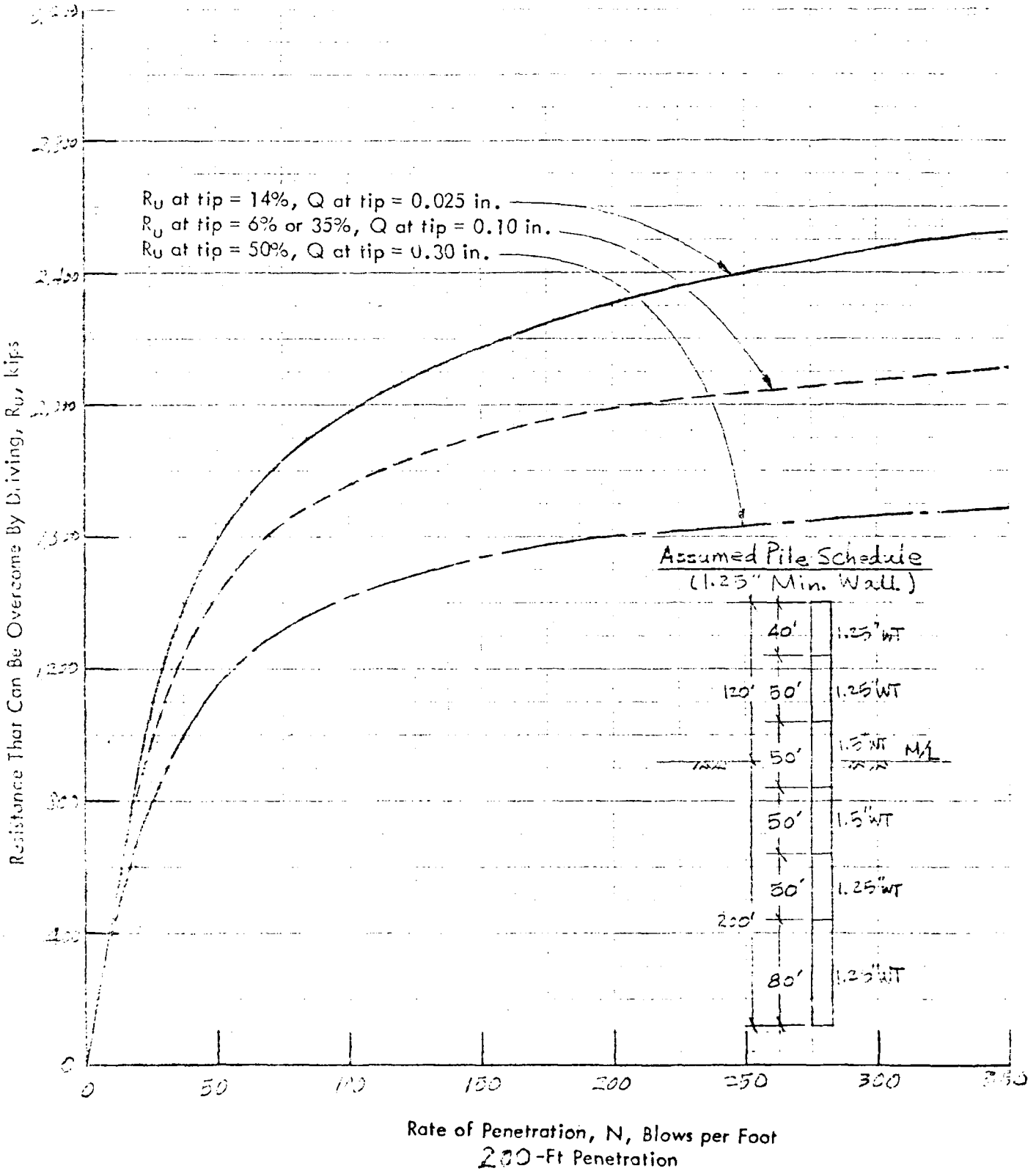
Vulcan 040 Hammer
 Wt. of Ram = 40,000 lbs
 Rated Energy = 120,000 ft-lbs
 Hammer Efficiency = 0.75
 Wt. of Pile Cap = 27,800 lbs

Spring Constant = 2.78×10^6 lbs/in.
 Damping Factor, side & tip, J = 0.15
 Quake Factor, side, Q = 0.10 in.
 Quake Factor, tip, - See Above

CREST OFFSHORE, INC.

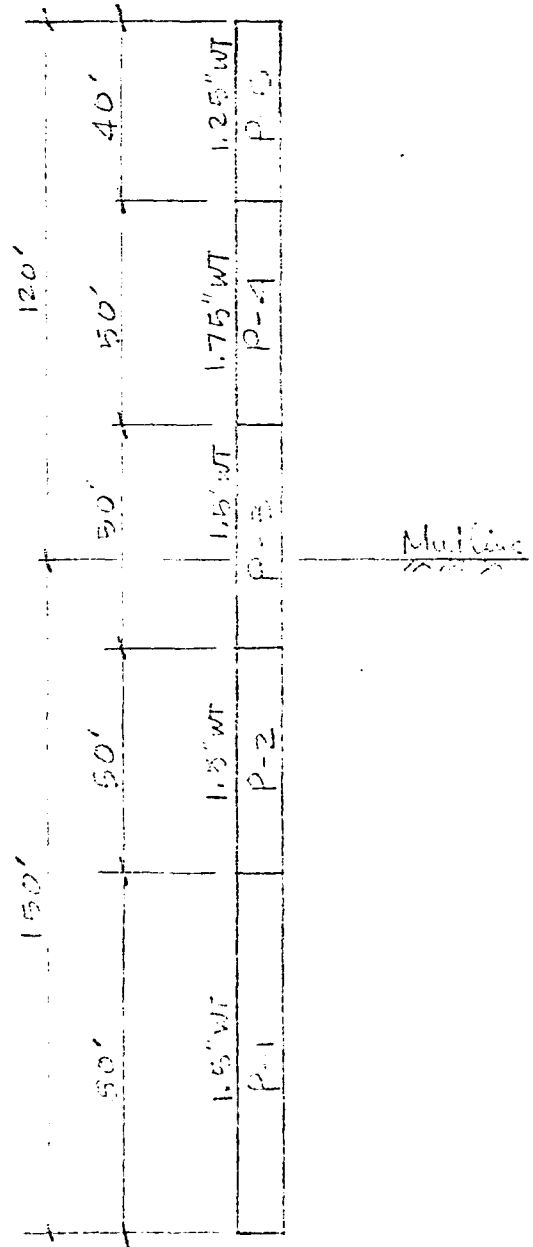
Sheet 3 of 10

By D. J. Carr Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-28-76 Job No. 27-111-92 Calculation Pile Driving Resistance Curves



By C. Chern Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-20-75 Job No. 27-771-92 Calculation Pile Driving Resistance Curves

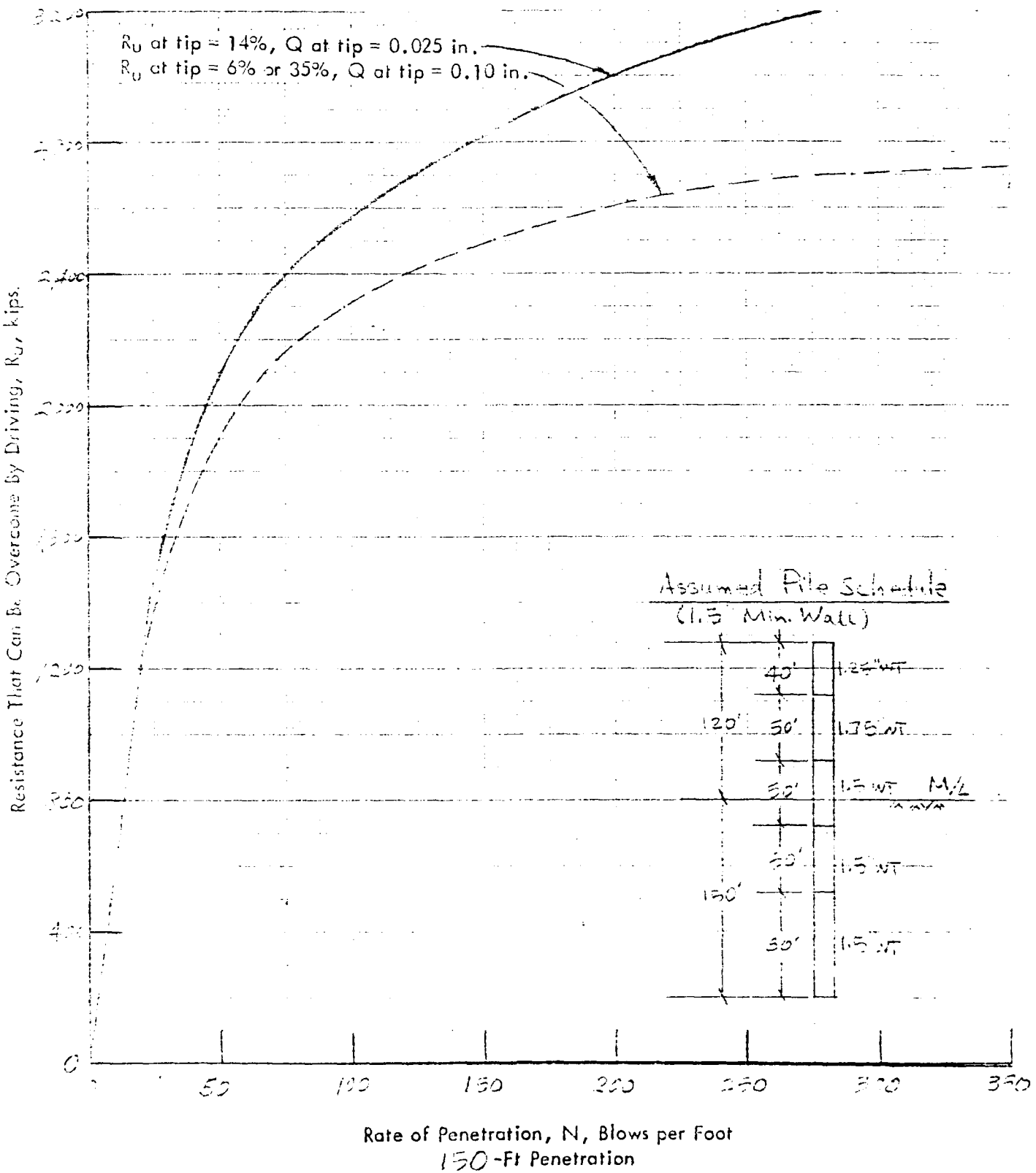
Assumed Pile Schedule -- 150 FT PENETRATION
 1.5" WALL THK. MIN.



Vulcan 060 Hammer
 Wt. of Ram = 60,000 lbs
 Rated Energy = 180,000 ft-lbs
 Hammer Efficiency = 0.75
 Wt. of Pile Cap = 40,200 lbs

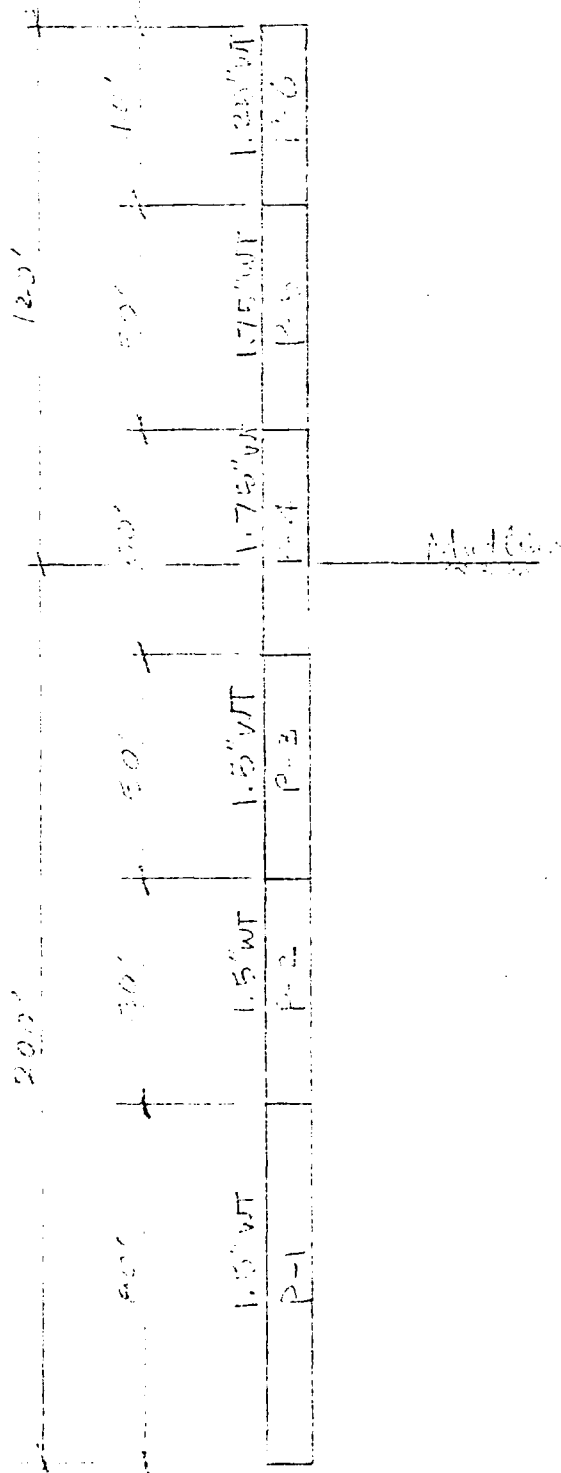
Spring Constant = 3.24×10^6 lbs/in.
 Damping Factor, side & tip, J = 0.15
 Quake Factor, side, Q = 0.10 in.
 Quake Factor, tip, - See Above

By C. C. Carr Client U.S. NAVY Subject Structural Concept Assessment
 Date 4-22-76 Job No. 27-771-92 Calculation Pile Driving Resistance Curve



By C. Chou Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-22-76 Job No. 22-111-92 Calculated on Pile Driving Resistance

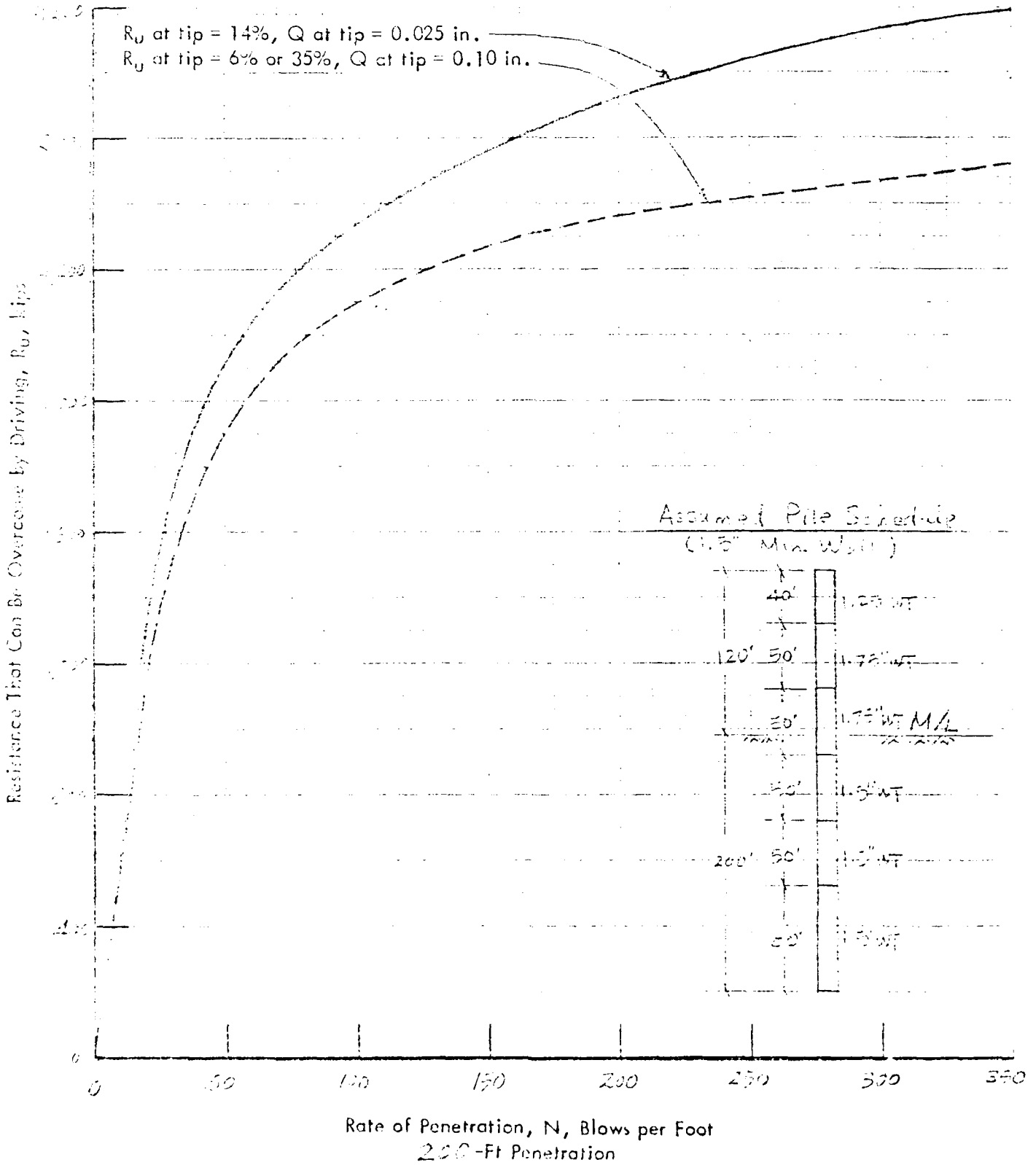
Assumed Pile Schedule -- 200 FT PENETRATION
 1.5' WALL THK. MIN.



Vulcan 060 Hammer
 Wt. of Ram = 60,000 lbs
 Rated Energy = 180,000 ft-lbs
 Hammer Efficiency = 0.75
 Wt. of Pile Cap = 40,200 lbs

Spring Constant = 3.24×10^6 lbs/in.
 Damping Factor, side & tip, J = 0.15
 Quake Factor, side, Q = 0.10 in.
 Quake Factor, tip, - See Above

By C. P. ... Client U.S. NAVY Subject Structural Concept Analysis
 Date ... Job No. 22-721-72 Calculation Pile Driving Resistance



SECTION 4
LATERALLY LOADED PILE CAPACITY

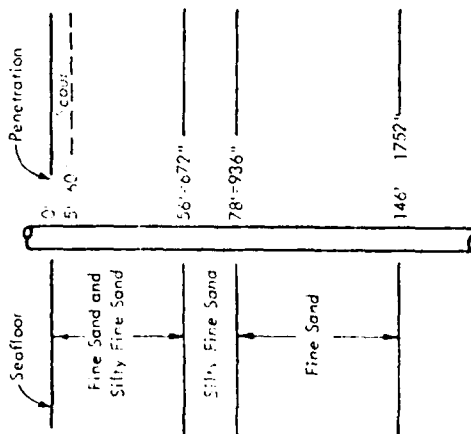
4.1 INTRODUCTION

This section evaluates the pipe pile capacity under lateral loads. The computer program used to perform the computation was developed by T. A. Haliburton at Oklahoma State University. The program printouts were compiled in APPENDIX A.3.

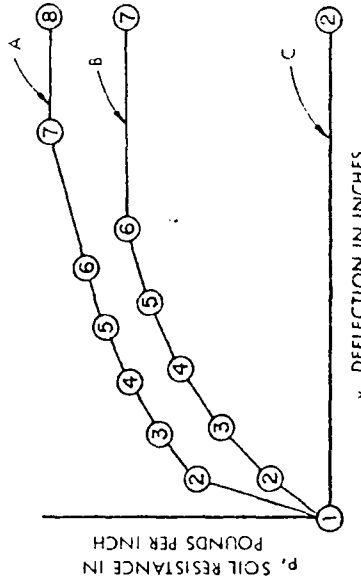
By C. Chern Client U.S. NAVY Subject Structural Concept Examination
 Date 4-15-76 Job No. 27-771-92 Calculation Lateral Bored Pile Capacity

4.2 SOIL DATA

Elevation, inches	Terminal Cone	1 1/2" DIAMETER PILE PILES																						
		Location of Test Points																						
		Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	Y10	Y11	Y12	Y13	Y14	Y15	Y16	Y17	Y18	Y19	Y20	Y21	Y22	
87.5	3																							
86	2	0.014	71	0.013	100	0.16	124	0.23	146	0.50	159	1.13	203	20.00	203	20.00	203	20.00	203	20.00	203	20.00	203	20.00
84	1	0.028	159	0.063	475	0.17	772	0.29	995	0.50	1287	1.13	2039	20.00	2039	20.00	2039	20.00	2039	20.00	2039	20.00	2039	20.00
82	0	0.037	591	0.071	1056	0.19	1446	0.30	2101	0.50	2783	1.13	4324	20.00	4324	20.00	4324	20.00	4324	20.00	4324	20.00	4324	20.00
80	0	0.051	827	0.123	734	0.17	1153	0.29	1493	0.50	1923	1.13	3092	20.00	3092	20.00	3092	20.00	3092	20.00	3092	20.00	3092	20.00
78	0	0.017	375	0.066	1145	0.17	1854	0.29	2341	0.50	3022	1.13	4836	20.00	4836	20.00	4836	20.00	4836	20.00	4836	20.00	4836	20.00
76	0	0.019	63	0.069	1430	0.17	2272	0.29	2924	0.50	3774	1.13	6039	20.00	6039	20.00	6039	20.00	6039	20.00	6039	20.00	6039	20.00
74	0	0.025	277	0.059	3119	0.19	4477	0.30	5611	0.50	7114	1.13	11383	20.00	11383	20.00	11383	20.00	11383	20.00	11383	20.00	11383	20.00
72	0	0.034	3131	0.120	4553	0.19	6966	0.30	8729	0.50	11067	1.13	17707	20.00	17707	20.00	17707	20.00	17707	20.00	17707	20.00	17707	20.00
70	0	0.034	553	0.13	750	0.34	1316	0.84	1382	2.10	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00
68	0	0.054	553	0.15	750	0.34	1316	0.84	1382	2.10	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00	1875	20.00
66	0	0.034	4446	0.090	5756	0.19	9743	0.30	12157	0.50	15414	1.13	24663	20.00	24663	20.00	24663	20.00	24663	20.00	24663	20.00	24663	20.00
64	0	0.038	4424	0.090	12651	0.19	18739	0.30	22736	0.50	28853	1.13	46155	20.00	46155	20.00	46155	20.00	46155	20.00	46155	20.00	46155	20.00



STRATIGRAPHY ASSUMED FOR P-Y DATA



TYPICAL CURVES

P-Y DATA

Boring 1

By C. Chen Client U.S. NAVY

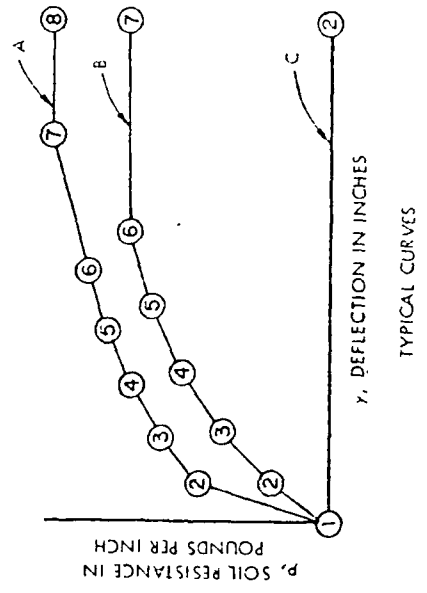
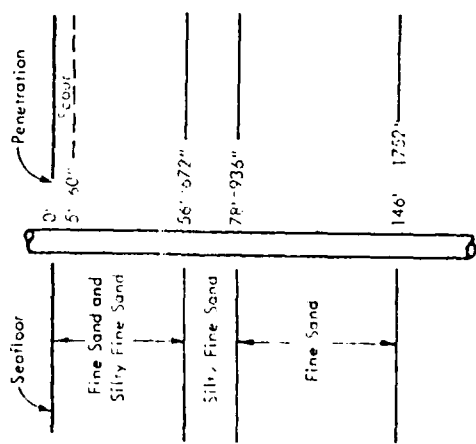
Subject Structure Concept Analysis

Date 4-13-76 Job No. 27-77L-2

Calculation Latent Dynamic Pipe Capacity

FIG-19. Diameter Pipe Fields

Radius inches	Jctn Curve	Cumulative of Curve Points																					
		Y1	P1	Z1	Y2	P2	Z2	Y3	P3	Z3	Y4	P4	Z4										
00.160	C	0	0	0	0.070	120	0.18	145	0.20	168	0.20	190	1.13	249	20.0	247	20.0	247	20.0	247	20.0	247	20.0
36	A	0	0	85	0.063	574	0.17	926	0.20	1194	0.20	1544	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
163	A	0	0	0	0.063	574	0.17	926	0.20	1194	0.20	1544	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
212	A	0	0	117	0.071	1267	0.18	1975	0.20	2521	0.20	3241	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
254	A	0	0	320	0.063	857	0.17	1390	0.20	1797	0.20	2320	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
336	A	0	0	606	0.066	1374	0.17	2189	0.20	2809	0.20	3626	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
420	A	0	0	756	0.066	1716	0.17	2734	0.20	3509	0.20	4929	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
430	A	0	0	812	0.090	5743	0.19	5226	0.20	6723	0.20	8527	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
672	A	0	0	0	0.090	5824	0.19	8395	0.20	10475	0.20	13280	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
673	B	0	0	624	0.13	700	0.24	1222	0.24	1658	0.24	2310	20.0	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
950	B	0	0	0	0.13	900	0.24	1222	0.24	1658	0.24	2310	20.0	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
957	A	0	0	0	0.090	8107	0.19	11692	0.20	14528	0.20	18497	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0
1752	A	0	0	0	0.090	15181	0.19	21387	0.20	27307	0.20	34624	1.13	247	20.0	247	20.0	247	20.0	247	20.0	247	20.0



P-Y DATA
 Boring 1

STRATIGRAPHY ASSUMED FOR P-Y DATA

By C. Chere Client U.S. NAVY Subject Structural Concept Analysis of pile
Date 4-22-76 Job No. 27-771-92 Calculation Lateral Loaded Pile Capacity

4.3 SECTION PROPERTIES

(1) Dimensions
36" O.D. x 1.75" WT

$$I_1 = 27,633.00 \text{ in}^4$$

$$A_1 = 183.3 \text{ in}^2$$

36" O.D. x 1.50" WT

$$I_2 = 24,234.25 \text{ in}^4$$

$$A_2 = 162.58 \text{ in}^2$$

By C. Clark Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-13-76 Job No. 27-771-92 Calculation Intermittent Pile Cap

(ii) Pile Top Restraint

$$k = \frac{3.5EI}{L} \quad \left(= \frac{M}{\theta} \right)$$

where E = 29,000 ksi

36" x 1.75" WT I = 27,683.0 in⁴

L = 384" = 32' "

$$k = \frac{3.5 \times 29,000 \times 27,683.0}{384}$$

$$= 7,317,251 \text{ in-kips/rad.}$$

$\frac{k}{EI} = \dots$

By C. Charr Client U.S. Navy Subject Structural Connections for ^{(B) pile} ~~brackets~~
 Date 4-22-76 Job No. 27-771.92 Calculation Latent Local Pile Capacity

(iii) Loadings at Pile Top (Pile C)

(See Computer Printout) Mom due to wind and wave
SEALOAD-2

$M_w + M_{sw} = 64,837 \text{ FT-KIP}$

Mom. due to boat landing

$M_b = 4,206 \text{ FT-KIP}$

Mom. due to stairs

$M_s = 10,123 \text{ FT-KIP}$

Total moment $M = 79,171 \text{ FT-KIP}$
 at midline

Total vertical load $P = 433 \text{ KIP}$

Shear due to wind and wave

$V_w + V_{WN} = 744 \text{ KIPS}$

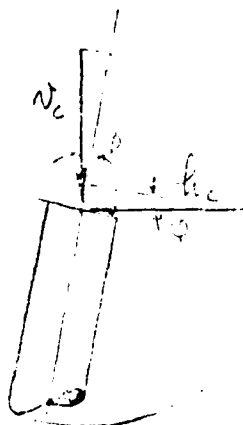
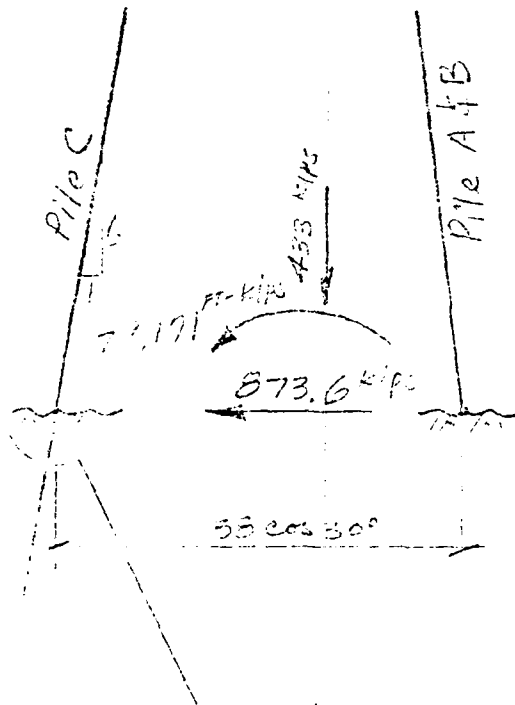
Shear due to Boat Landing

$V_b = 45.4 \text{ KIPS}$

Shear due to Stairs

$V_s = 51.2 \text{ KIPS}$

Total Shear = 873.6 KIPS
 at midline.



By C. Clark Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-22-76 Job No. 27-771-92 Calculation Lateral Load/Pile Capacity

Max. Compression

$$V_c = \frac{1}{3} V = 291.2 \text{ kips}$$

$$U_c = \frac{M}{330440} + \frac{P}{3} = 1576.2 + 144.3$$

$$= 1720.5 \text{ kips}^{**}$$

Axial Compression

$$A_c = U_c \cos \phi + V_c \sin \phi$$

$$= 1720.5 \times \frac{6}{\sqrt{37}} + 291.2 \times \frac{1}{\sqrt{37}}$$

$$= 1697.1 + 47.9$$

$$= 1745.0 \text{ kips}$$

Shear

(under Axial Compression)

$$S_c = U_c \cos \phi - V_c \sin \phi$$

$$= 291.2 \times \frac{6}{\sqrt{37}} - 1720.5 \times \frac{1}{\sqrt{37}}$$

$$= 287.2 - 282.8$$

$$= 4.4 \text{ kips}$$

check: ** $U_c = 1860 \text{ kips}$ (Axial compression including live and
 additional load/leakage equipment down and
 $S_c = 287.2 - 305.8$ top down)
 $= 18.6 \text{ kips} < 51.8 \text{ kips (allowable axial tension)}$

By C. Chern Client U.S. NAVY

Subject Structural Concept Analysis

Date 4-22-76 Job No. 27-771-92

Calculation Lateral Load/Pile Capacity

Max. Tension

$$v_t = \frac{M}{58 \cos 30^\circ} - \frac{P}{3} = 1431.9 \text{ KIPS}$$

$$h_t = h_c = 291.2 \text{ KIPS}$$

Axial Tension

$$A_t = v_t \cos \phi + h_t \sin \phi$$

$$= 1431.9 \times \frac{6}{\sqrt{37}} + 291.2 \times \frac{1}{\sqrt{37}}$$

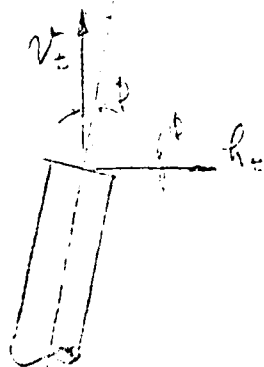
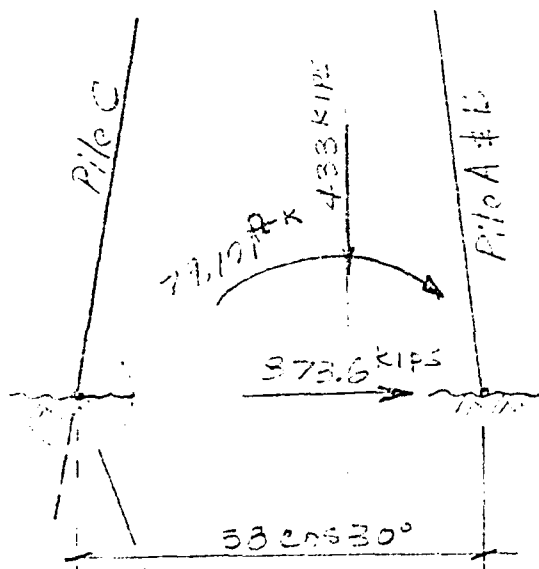
$$= 1460 \text{ KIPS}$$

Shear

$$S_t = v_t \sin \phi - h_t \cos \phi$$

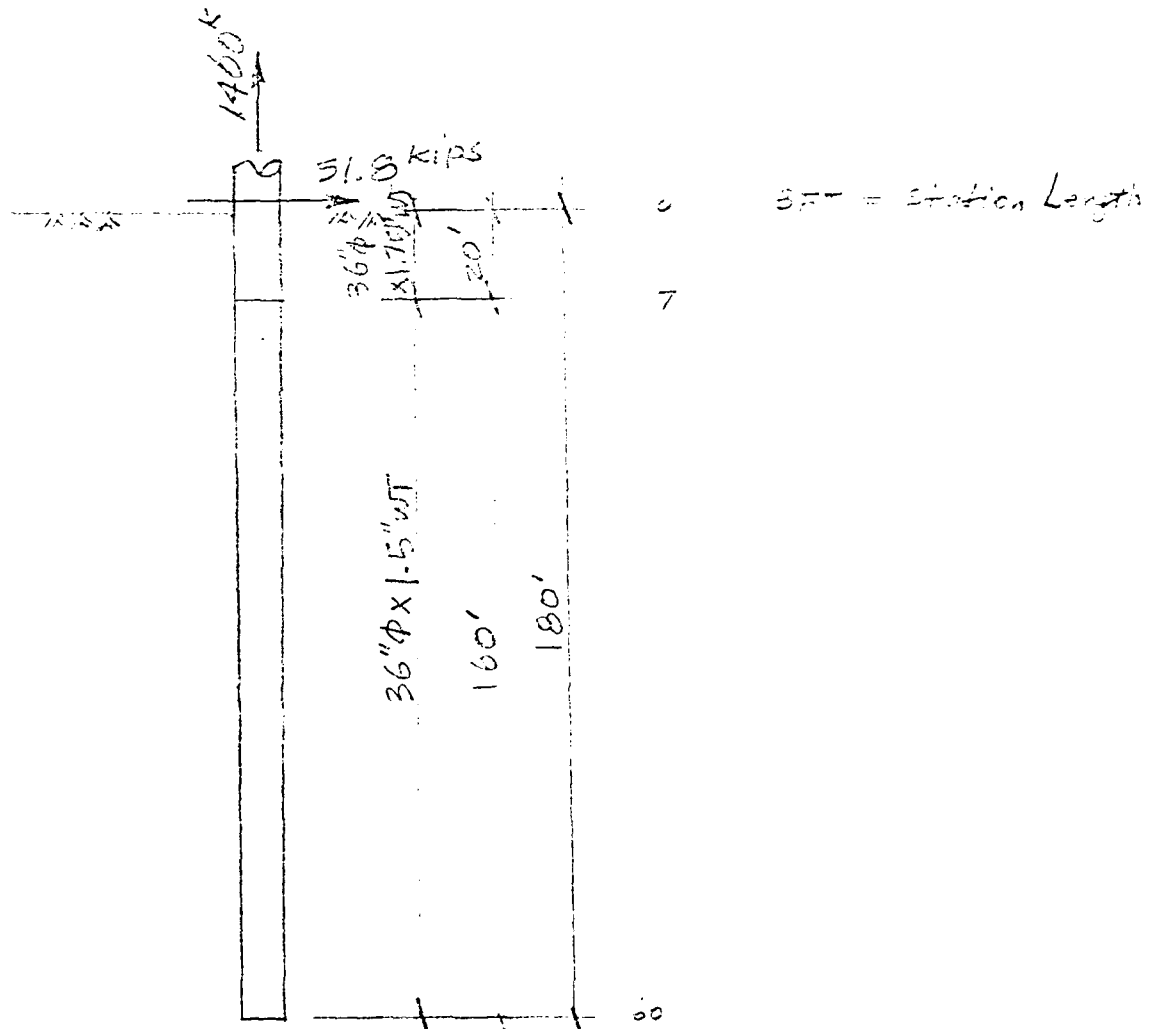
$$= 1431.9 \times \frac{1}{\sqrt{37}} - 291.2 \times \frac{6}{\sqrt{37}}$$

$$= -51.8 \text{ KIPS}$$



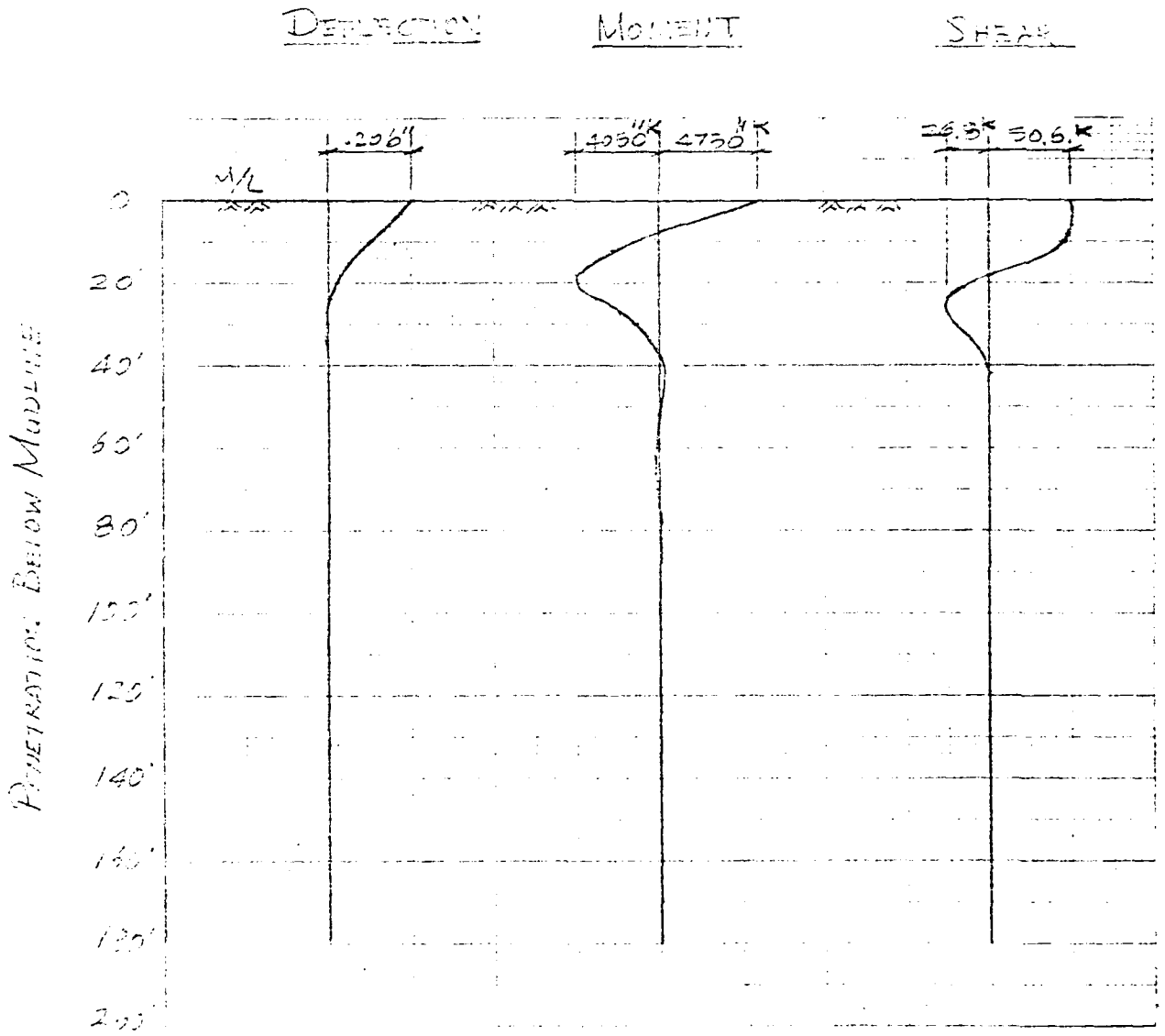
By C. Chace Client U.S. NAVY Subject Structural Concept Analysis
Date 4-22-76 Job No. 27-771-92 Calculation Laterally Loaded Pile Capacity

(iv) Estimated Penetration - 150 FT Below mud line



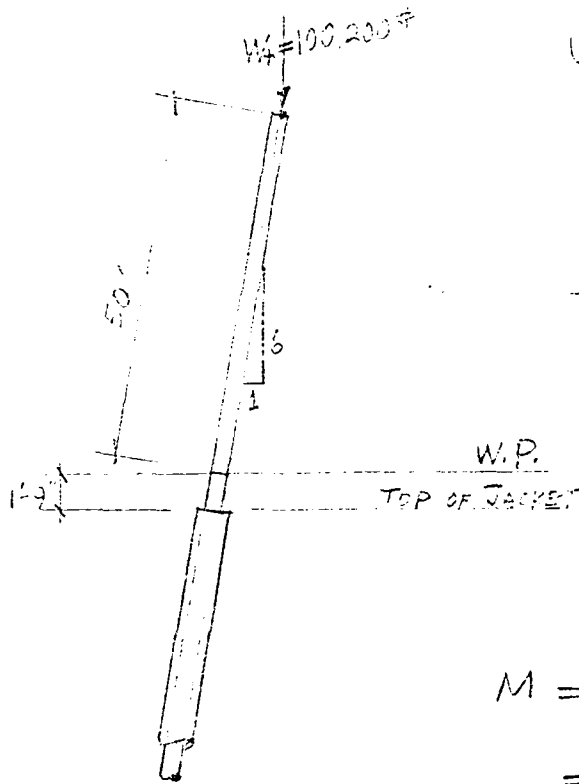
By C. Chern Client U.S. NAVY Structural Concept Analysis
Date 4-23-76 Job No. 27-771-92 Calculation Load by Load Pile Capacity

4.4 SHEAR, MOMENT AND DEFLECTION DIAGRAMS



By C. Chao Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-23-76 Job No. 27-771-92 Calculation Laterally Loaded Pile Capacity

4.5 MINIMUM WALL THICKNESS REQUIREMENTS



Use Vulcan 060 Hammer

Wt. of Hammer = 62,000 LBS

Wt. of Pile Cap = 40,200 LBS

Total Wt. = 100,200 LBS

Bending moment at the top of jacket leg is

$$M = 100,200 \times \left[\frac{1}{6} (51.75) \right]$$

$$= 864,225 \text{ ft-lbs}$$

Axial Compression at the top of jacket leg (Pile)

$$P = 100,200 \times \frac{6}{\sqrt{37}} = 98,837 \text{ LBS}$$

36" O.D. x 1.25" WT $I = 20,630 \text{ in}^4$

$A = 136.5 \text{ in}^2$

Combined Stress $\sigma_c = \frac{M d}{I} + \frac{P}{A}$

$$\sigma_c = \frac{(864,225 \times 12) \times 18}{20,630} + \frac{98,837}{136.5}$$

CREST OFFSHORE, INC.

Sheet 4.12 of 12 ^{73 file}

By S. Chern Client U.S. NAVY Subject Structural Concept Analysis
Date 4-23-76 Job No. 27-771-72 Calculation Latent Lateral Pile Capacity

$$\begin{aligned}\sigma_c &= 9,773 \text{ psi} \\ &= 9.8 \text{ ksi}\end{aligned}$$

Use Impact factor of 2 for the dynamic effect on piles during driving:

$$\sigma_{c,d} = 2 \times \sigma_c = 19.6 \text{ ksi} < 22 \text{ ksi}$$

Say O.K.

SECTION 5
AXIAL PILE CAPACITY REQUIREMENTS

5.1 INTRODUCTION

The attempt of this section is to develop axial pile capacity requirements for the three-pile structure under a set of given loading conditions. The results serve as guide lines for optimizing structural steel weight as presented in the following section (Section 6).

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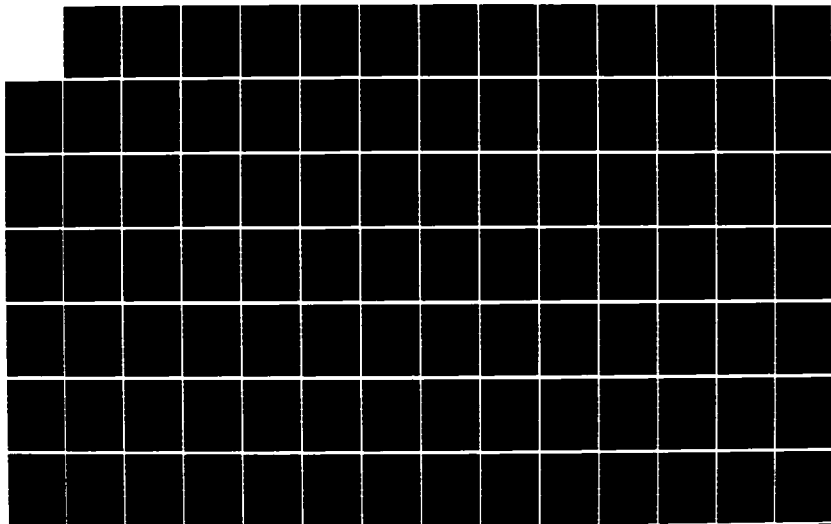
STRUCTURAL CONCEPT ANALYSIS REPORT FOR THE EAST COAST
AIR COMBAT MANEUVER. (U) CREST ENGINEERING INC TULSA OK
MAY 76 27-771-92-APP-C CHES/NAVFAC-FPO-7601-APP-C
N62477-76-C-0179

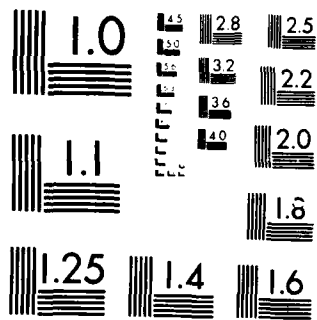
2/7

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F/G 13/13

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963-A

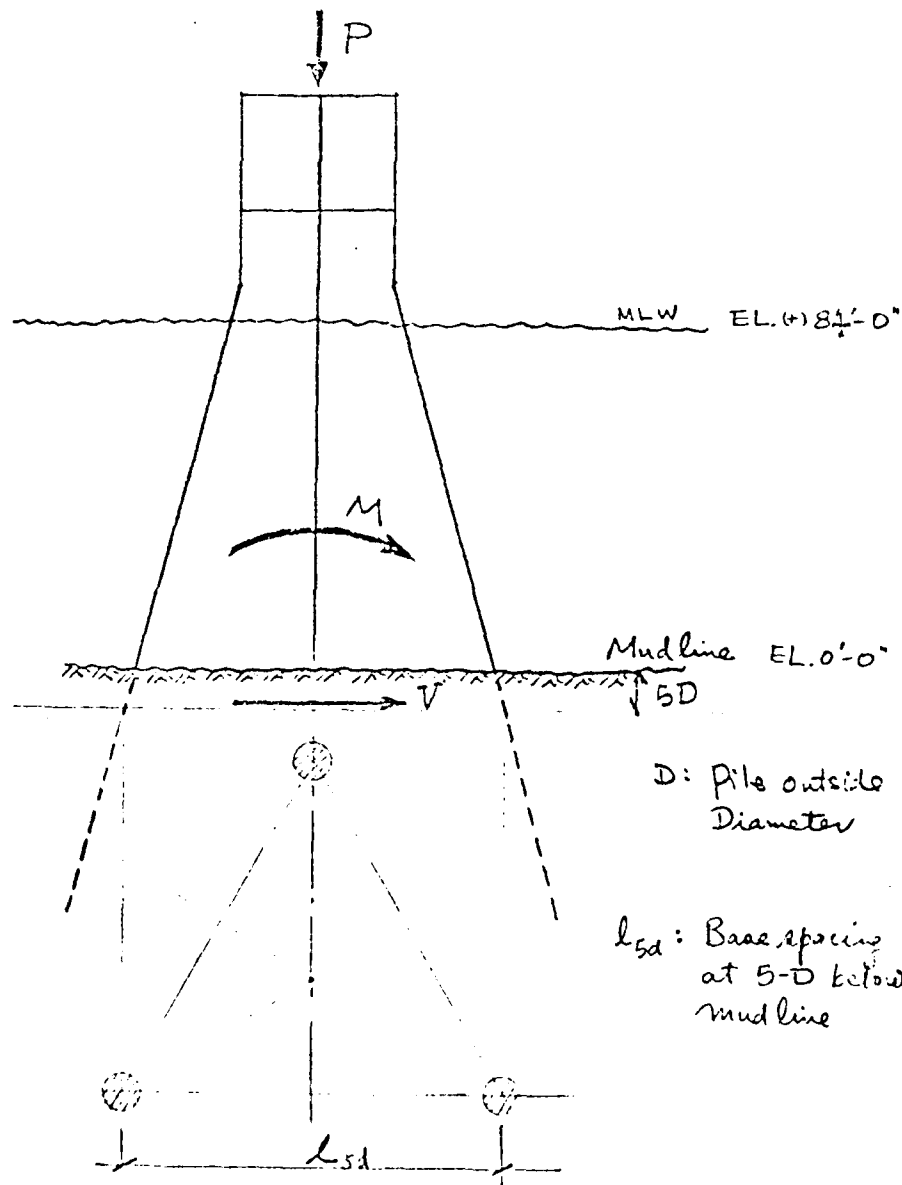
By C. Chen Client U.S. NAVY Subject Structural Concrete Analysis
Date 8-28-76 Job No. 27-271-9E Calculation Wind Pile Capillary Reg. T

E.02 LOADING CONDITIONS ON STRUCTURE

Total Gravity Load $P = 450$ kips

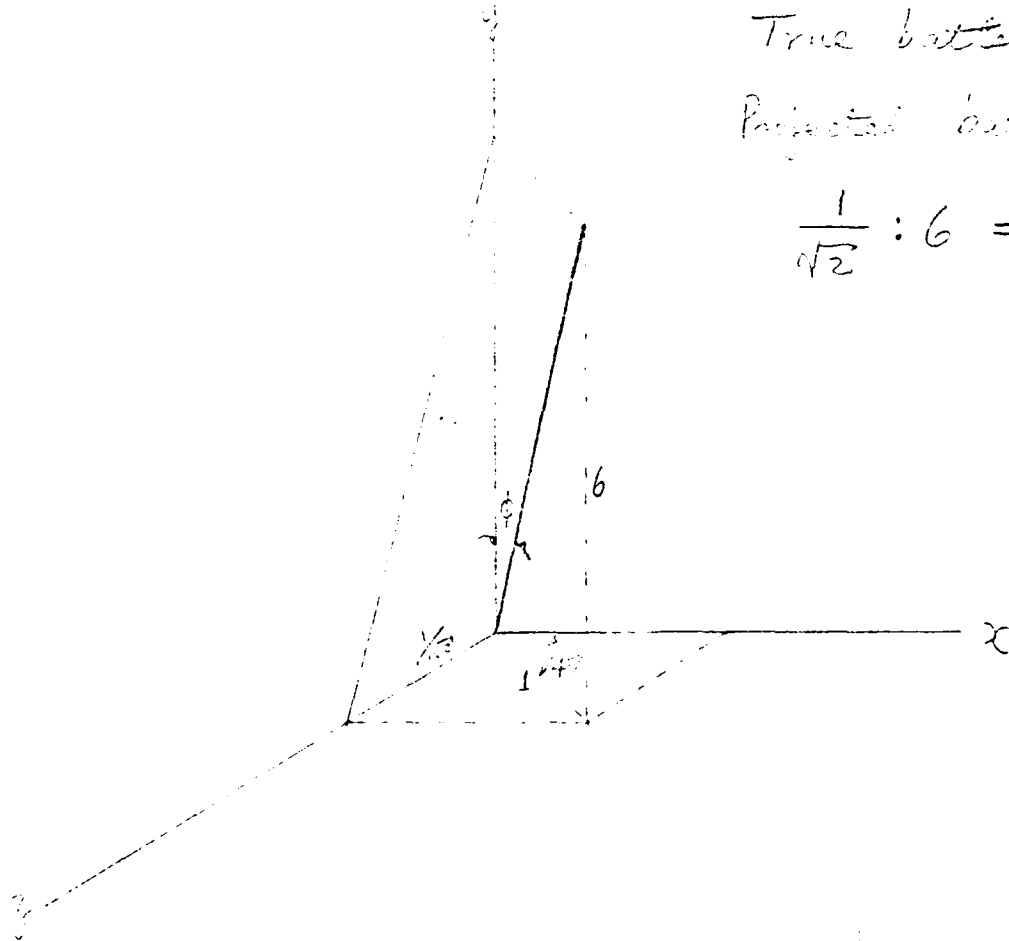
Base shear $V = 1254.6$ kips

Moment $M = 1,07,302$ ft-kips

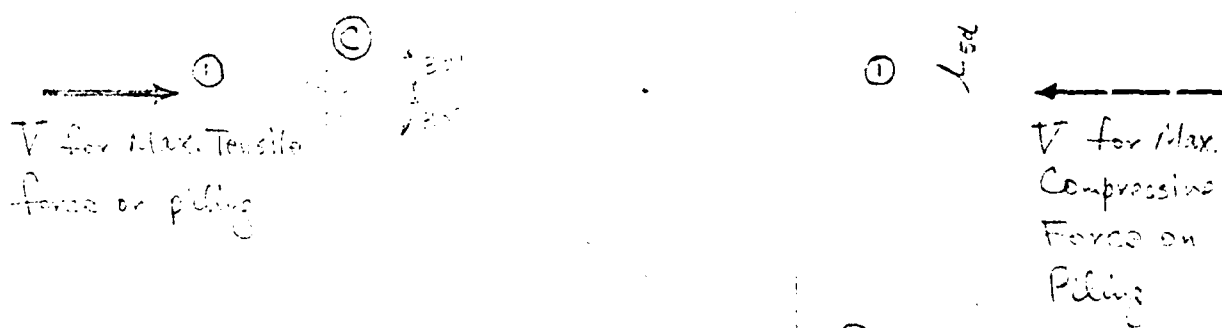


By C. Clark Client U.S. Navy Subject Structural Concept Analysis
 Date 8-20-76 Job No. 27-71-72 Calculation Axial Pile Capacity

True batter of piles 1:6
 Projected batter of piles
 $\frac{1}{\sqrt{2}} : 6 = 1 : 8.485$



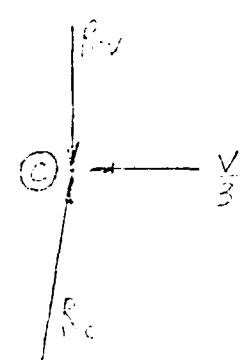
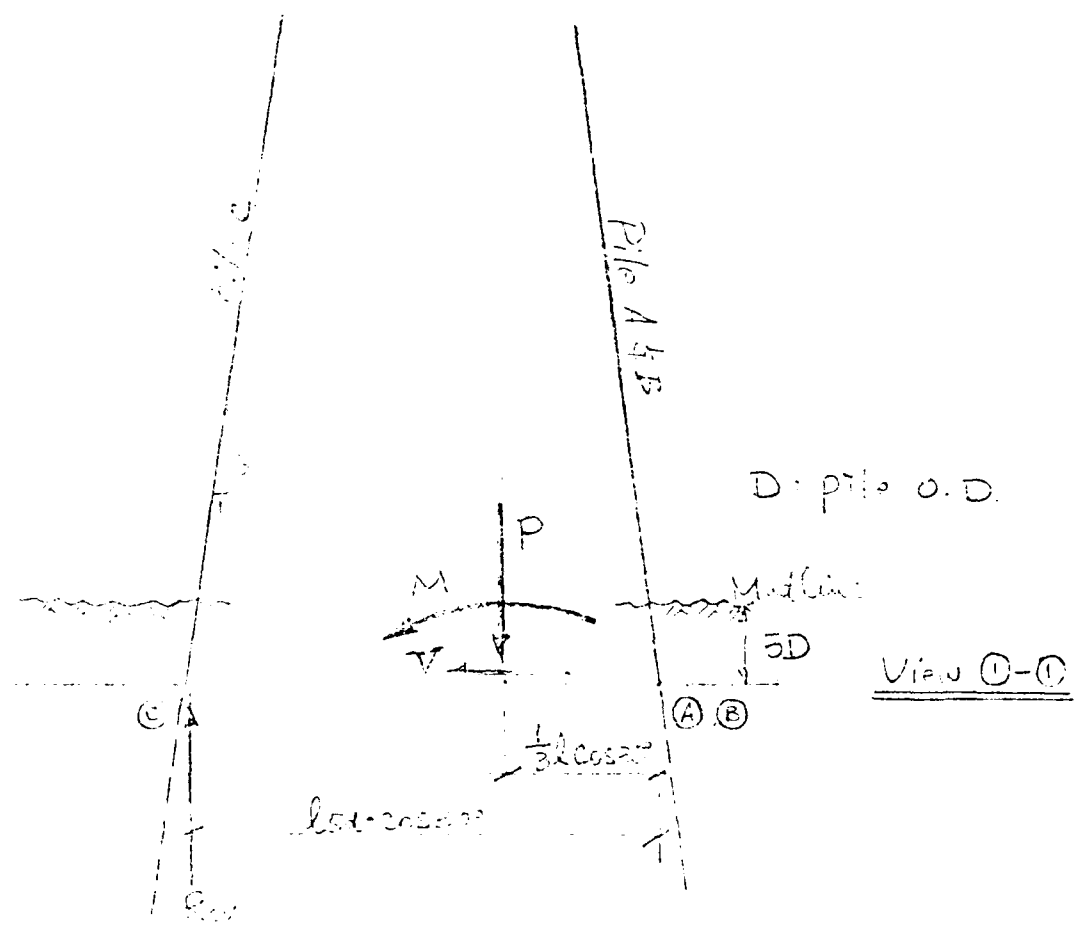
PLAN AT BD BELOW MUDLINE



$L \cos 30^\circ$
 $\frac{1}{3} (L \cos 30^\circ)$

By S. C. [unclear] Client Shell [unclear] Subject Design of Concrete Pile
 Date 3-28-73 Job No. 57-771-3 Calculation Axial Pile Capacity

5.3 PILE CAPACITY REQUIREMENT IN COMPRESSION



$$R_c = \frac{6}{\sqrt{37}} R_{cv} + \frac{1}{\sqrt{37}} \frac{V}{3} \quad (1)$$

$$R_{cv} = \frac{\sqrt{37}}{6} R_c - \frac{1}{13} V \quad (2)$$

By C. P. Hearn Client U.S. Navy Subject Structural Concept Analysis
 Date 2-2-75 Job No. 37-751-24 Calculator on Excel file Capacity Report

Summation of moments about axis A-B

$$R_{cs} l \cos 30^\circ = M + \frac{P l_{st} \cos 30^\circ}{3} \quad (3)$$

$$\left(R_{cs} - \frac{P}{3} \right) l_{st} \cos 30^\circ = M$$

$$l_{st} = \frac{M}{\left(R_{cs} - \frac{P}{3} \right) \cos 30^\circ} \quad (4)$$

Substituting Eq. (3) into Eq. (4)

$$l_{st} = \frac{M}{\left(\frac{\sqrt{37}}{6} R_c - \frac{V}{18} - \frac{P}{3} \right) \cos 30^\circ} \quad (5)$$

$M = 107,302 \text{ ft kips}$

$D = 455 \text{ kips}$

$\frac{P}{3} = 150$

$V = 1254.6 \text{ kips}$

$\frac{V}{18} = 69.7$

$$l_{st} = \frac{123,902}{\frac{\sqrt{37}}{6} R_c - 219.7} \quad (5a)$$

$$(R_c)_{min} = \frac{6 \times 219.7}{\sqrt{37}} = 216.7 \text{ kips}$$

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Sheet 22 of 14

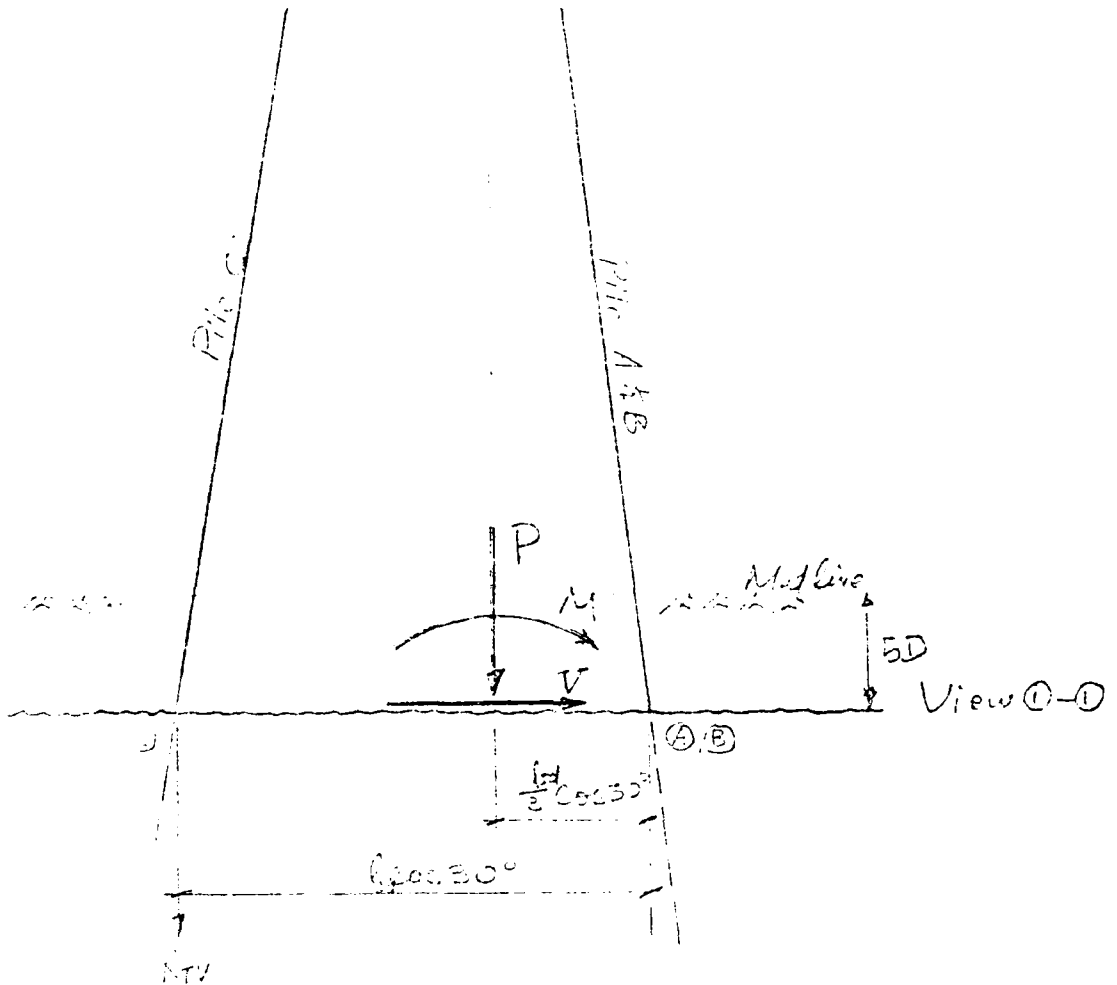
By C. Chen Client U.S. NAVY Subject Structural Concept Analysis of
 Date 3-28-72 Job No. 27-771-74 Calculation Allowable Capacity of Pile

$$L_{st} = \frac{123,900}{\frac{\sqrt{37}}{6} R_c - 219.7}$$

R_c (k's)	$\frac{\sqrt{37}}{6} R_c - 219.7$	$L_{st} = \frac{123,900}{\frac{\sqrt{37}}{6} R_c - 219.7}$ (ft)
216.7	0	∞
500.	287.2	431.4
750.	540.6	229.2
1,000.	794.1	156.0
1,250.	1,047.5	118.3
1,500.	1,301.0	95.2
1,750.	1,554.4	79.7
2,000.	1,807.9	68.5
2,250.	2,061.3	60.1
2,500.	2,314.8	53.5
2,750.	2,568.2	48.2
3,000.	2,821.7	43.9

By C. C. ... Client U. S. ... Subject Chart 1 - Crest Offshore (S. 11)
 Date 3-22-79 Job No. 87-771-94 Calculation Abutment Capacity Report

5.4 PILE CAPACITY REQUIREMENT IN TENSION



Moment of resistance about axis ①-②

$$R_{TU} \left(L \cos 30^\circ - \frac{PL}{3} \cos 30^\circ \right) = M \quad (6)$$

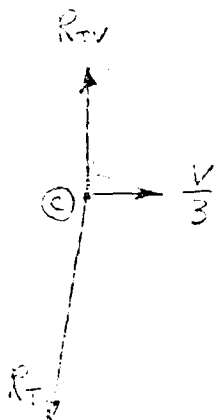
$$L_{st} = \frac{M}{\left(R_{TU} + \frac{P}{3} \right) \cos 30^\circ} \quad (7)$$

By S. D. ... Client U.S. Navy

Subject Structural Concrete Analysis

Date 8-2-75 Job No. 27-72-1-2

Calculation Wind Pill Capacity



$$R_T = \frac{6}{\sqrt{37}} R_{TV} + \frac{1}{\sqrt{37}} \left(\frac{V}{3} \right)$$

$$R_{TV} = \frac{\sqrt{37}}{6} R_T - \frac{V}{18} \quad (8)$$

Substituting Eq. (8) into Eq. (7)

$$\phi = \frac{M}{\left(\frac{\sqrt{37}}{6} R_T - \frac{V}{18} + \frac{P}{3} \right) \cos 30^\circ} \quad (9)$$

$M = 107,302 \text{ ft-kips}$

$P = 450 \text{ kips}$

$V = 1284.6 \text{ kips}$

$\frac{V}{18} = 69.7$

$$\phi = \frac{123,902}{\frac{\sqrt{37}}{6} R_T + 30.3}$$

$R_T \geq 0 \quad \phi_{max} = 1543.0 \text{ ft}$

as for $R_T = 0$

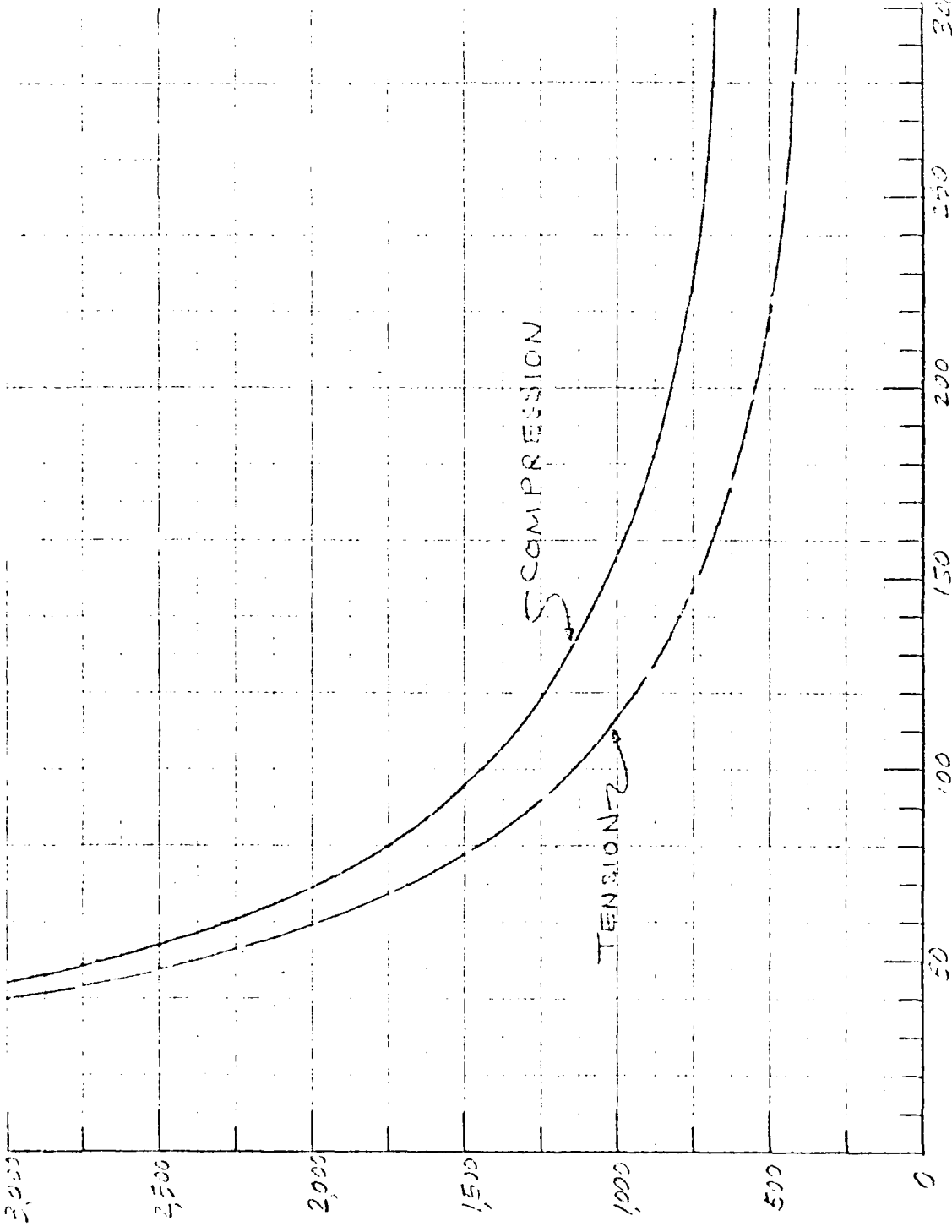
CREST OFFSHORE, INC.

Sheet 5.22 of 14

Client U.S. NAVY Subject Structural Concept Analysis
 Date 8-3-82 Job No. 27-0311-21 Calculation Edge Pile Capacity Req'd

R_T (kips)	$\frac{\sqrt{37}}{6} R_T + 30.3$	$\left(= \frac{123.002}{\frac{\sqrt{37}}{6} R_T + 50.3} \right)$
0	30.3	1543.0
250	333.7	371.2
500	537.2	211.0
750	640.6	147.4
1000	1,094.1	113.2
1,250	1,347.5	91.9
1,500	1,601.0	77.4
1,750	1,854.4	66.5
2,000	2,107.9	58.7
2,250	2,361.3	52.3
2,500	2,614.8	47.4
2,750	2,868.2	43.2
3,000	3,121.7	39.7

By C. Chen Date 11/5/11 Project Shelter Cove
Job No 27-27-21 Calculation 4.0.10.10



BASE SPACING (FT)
(5-D Below Mudline)

REQUIRED PIPE PILE CAPACITY (KIPS)

by C. P. Beck, OMA, U.S. 2117Subject: Structural Concept (Substructure)Date: 3-2-78 Job No: 27-11-11Calculation: Wind Res. Cap. of PileLOADS ON P-PILE STRUCTURE (C=1)

Total Gravity Load $SP_c = 620.5$
 $RP_c = 455.5$ kips

Base Shear $V = 836.7$ kips

Moment $M = 79,598$ ft-kips

Wave Coefficient

$$L = \frac{M}{\left(\frac{\sqrt{37}}{6} R_c - \frac{V}{15} - \frac{P_c}{3}\right) \cos 30^\circ}$$

$$= \frac{79,598}{\left(\frac{\sqrt{37}}{6} R_c - \frac{836.7}{15} - \frac{620.5}{3}\right) \cos 30^\circ} = \frac{91,859}{\frac{\sqrt{37}}{6} R_c - 256.2}$$

Wave Force

$$L = \frac{M}{\left(\frac{\sqrt{37}}{6} R_T - \frac{V}{15} - \frac{P_c}{3}\right) \cos 30^\circ}$$

$$= \frac{79,598}{\left(\frac{\sqrt{37}}{6} R_T - \frac{836.7}{15} + \frac{455.5}{3}\right) \cos 30^\circ}$$

$$= \frac{91,827}{\frac{\sqrt{37}}{6} R_T + 106.2}$$

CREST OFFSHORE, INC.

Sheet 2.17 of 24

By C. [unclear] Client U.S. NAVY Subject Support of [unclear]
 Date 5-2-55 Job No. 27-02-15 Calculation 2.17 - [unclear]

$$L = \frac{91.889}{\frac{\sqrt{37}}{6} R_c - 256.2}$$

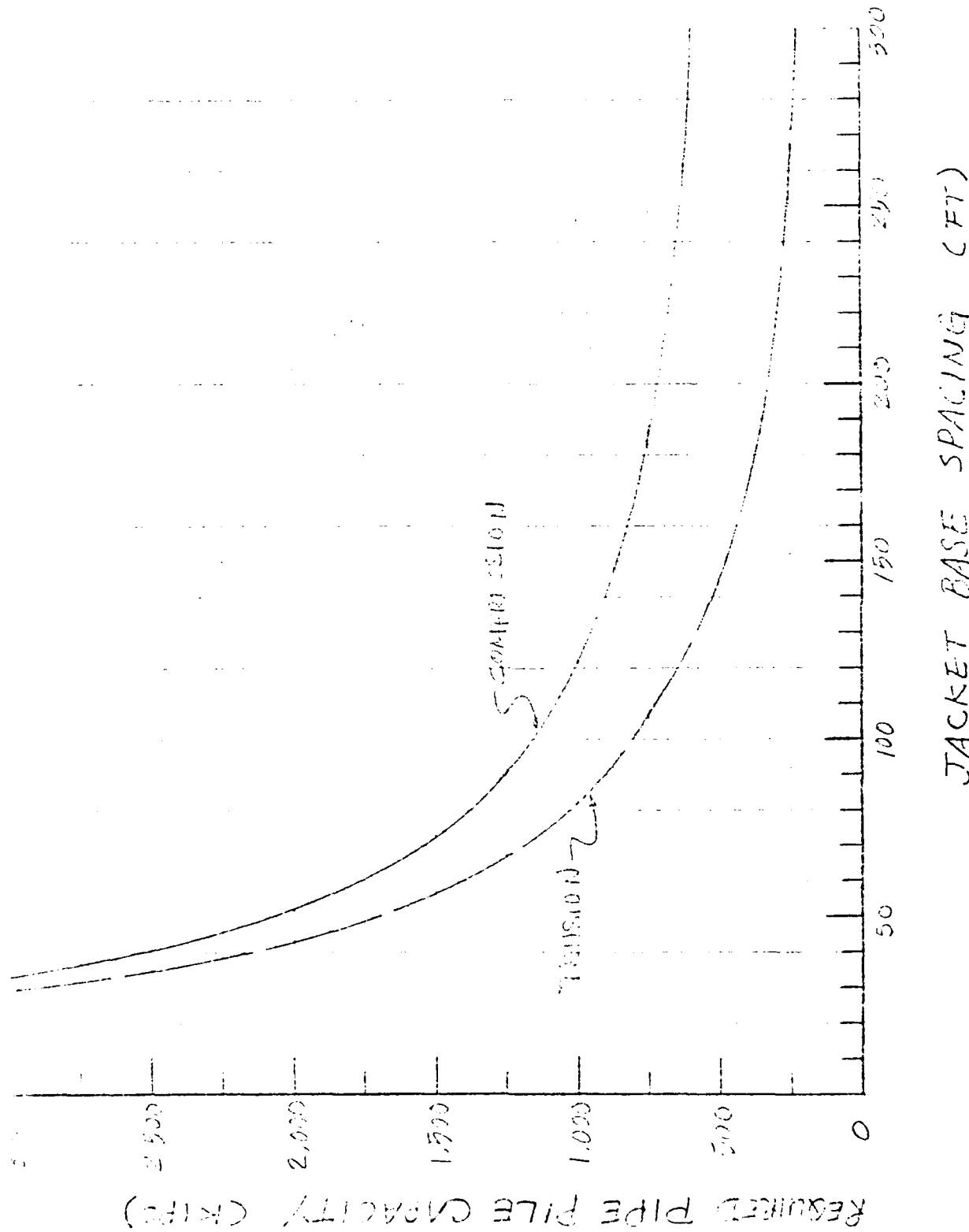
R_c	$\frac{\sqrt{37}}{6} R_c - 256.2$	$L = \frac{91.889}{\frac{\sqrt{37}}{6} R_c - 256.2}$
KIPS	KIPS	FT
256.7	0	∞
300.	250.7	366.5
350.	504.1	182.3
400.	757.6	121.3
450.	1,011.0	90.9
500.	1,264.5	72.7
550.	1,517.9	60.5
600.	1,771.4	51.9
650.	2,024.8	45.4
700.	2,278.3	40.3
750.	2,531.7	36.3
800.	2,785.2	33.0

Client: Shell Subject: St. Charles
 Date: 5-2-77 Job No: 2-177-1 Calculation: St. Charles

$$C = \frac{91.559}{\frac{\sqrt{37}}{6} R_T + 106.2}$$

R_T	$\frac{\sqrt{37}}{6} R_T + 106.2$	$C = \frac{91.559}{\frac{\sqrt{37}}{6} R_T + 106.2}$
KIPS	KIPS	FT
0	106.2	865.2
250	359.6	255.5
500	613.1	149.9
750	866.5	106.0
1,000	1,120.0	82.0
1,250	1,373.4	66.9
1,500	1,626.9	56.5
1,750	1,880.3	48.9
2,000	2,133.8	43.1
2,250	2,387.2	38.5
2,500	2,640.7	34.8
2,750	2,894.1	31.8
3,000	3,147.6	29.2

By B. C. ... Client U. S. ... Subject Structural Concept for Jacket
Date 2-17-76 Job No. 2-111-76 Calculation Wind Pile Capacity, Page 1



JACKET BASE SPACING (FT)

SECTION 6
STRUCTURAL STEEL WEIGHT VARIATION

6.1 INTRODUCTION

Set forth herein is the computations of the structural steel weights, respectively, for the piling sizes of 36", 39" and 42".

In the process of computations, the following member sizes of the structural components were assumed to be common regardless of varying piling diameters.

- (1) Bracings
- (2) Jacket Leg wall thickness
- (3) Superstructures
- (4) Miscellaneous items such as boat landing, stairway, etc.

By C. Chen Client W. W. W. W. Subject Structural Concept Analysis of
 Date 4-25-96 Job No. 7-111-92 Description Structural Steel W. W. W. W.

6.2 PLAN AND ELEVATION

(a) Plan View of Jacket

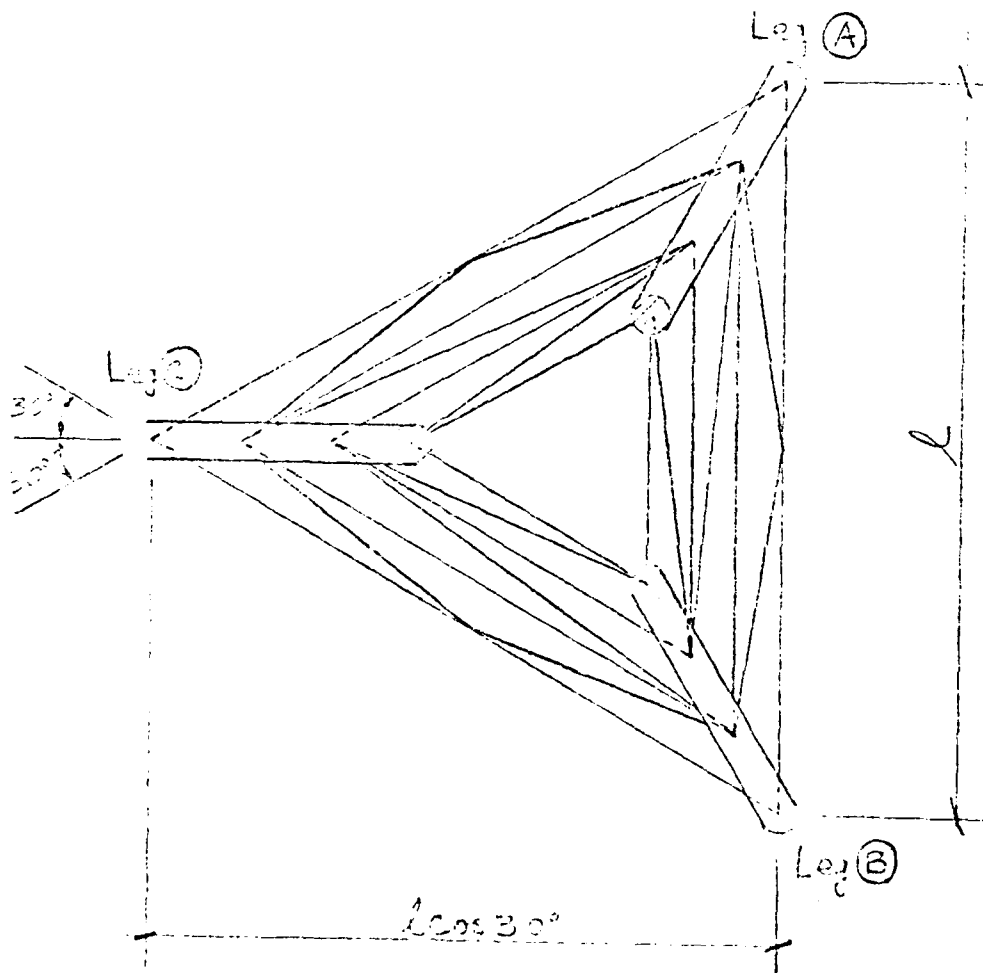
Member Sizes:

(i) Bracing: See Pg. 6.07

(ii) Leg: $(D+4)$ " O.D. x .5" WT, See Pg. 6.09

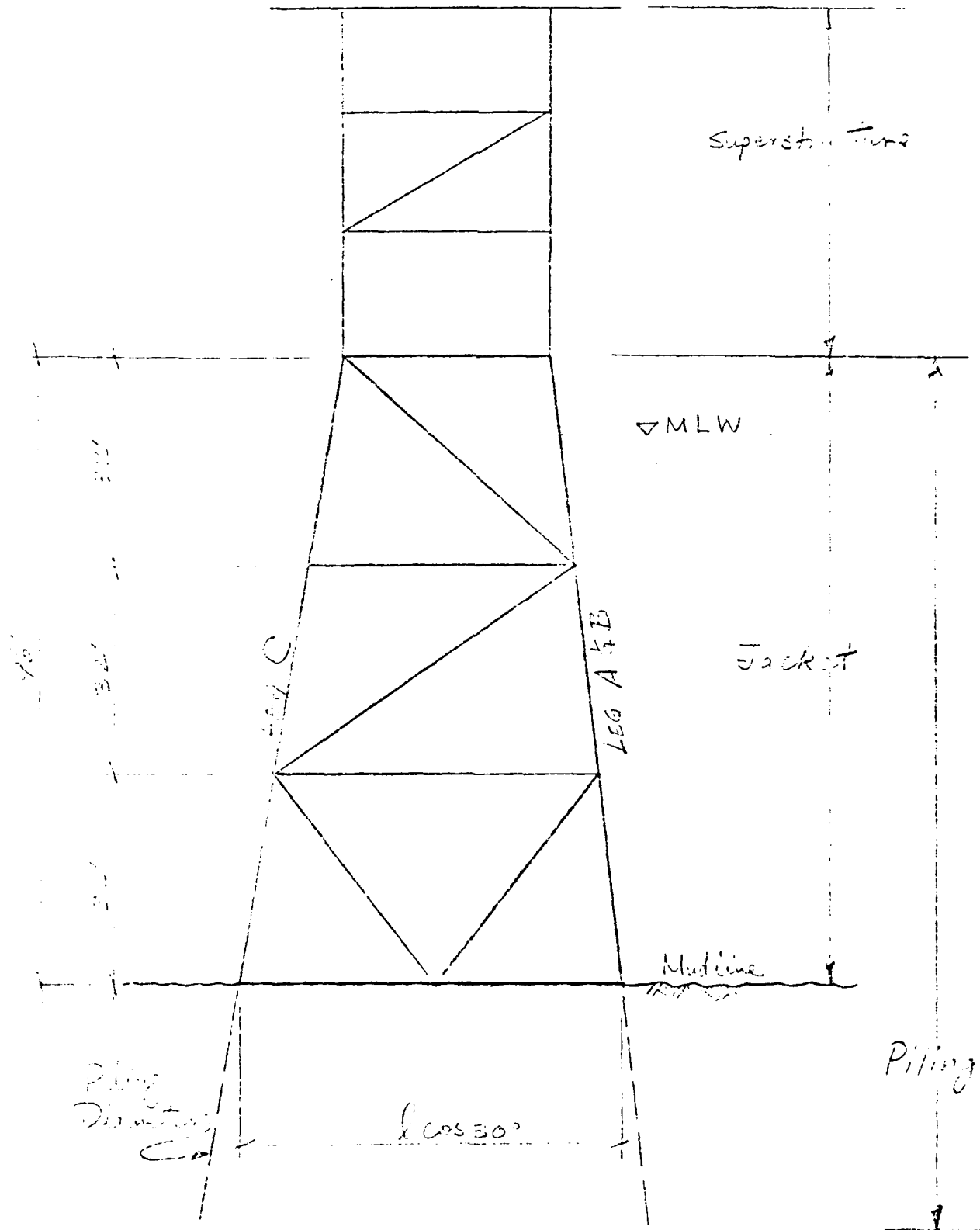
(iii) Leg Joint Cap: $(D+5)$ " O.D. x 1" WT, See Pg. 6.09

* D = O.D. of Pipe Piles



By C. Green Client U.S. NAVY Subject Structural Concept Analysis
Date 4-24-92 Job No. 27 711-92 Calculation Structural Steel Verification

(B) Elevation of 3-Pile Structure

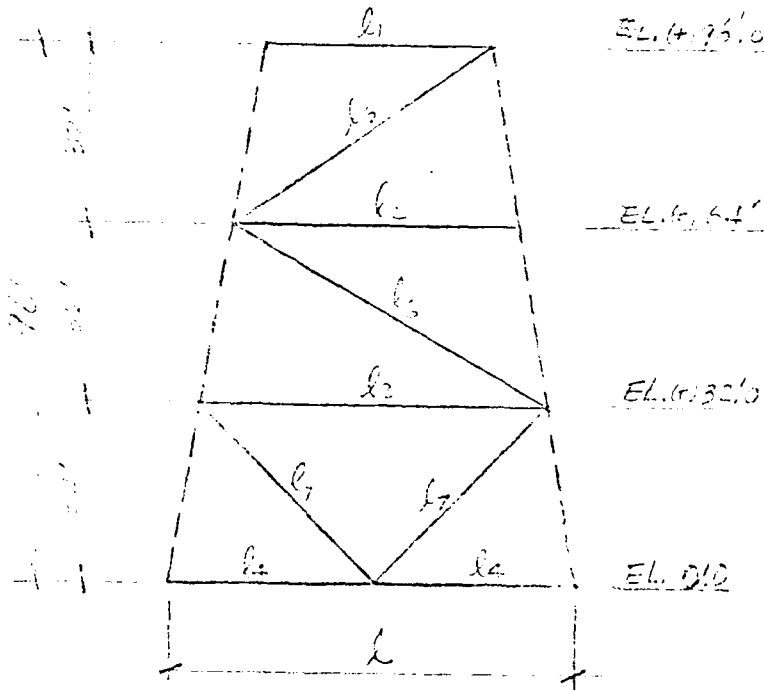


By C. Chou Client U.S. Navy Subject Structural Concept Analysis
 Date 4-26-76 Job No. 27-771-22 Calculation Structure - Steel Structure

6.3 WEIGHT OF STRUCTURES

referring to Plan View shown on Fig. 6.02

1) Enclaves (3 Rows)



$$l_1 \cos 30^\circ = (l \cos 30^\circ - \frac{46}{3}(1 - \cos 30^\circ))$$

$$= (l - 16(1.5)) / \cos 30^\circ$$

$$= l - 27.7 \text{ (ft)}$$

$$l_2 = (l - l_1) \times \frac{1}{3} + l_1$$

$$= \frac{1}{3}l + \frac{2}{3}l_1 = l - 18.46$$

$$l_3 = (l - l_1) \times \frac{2}{3} - l_1$$

$$= \frac{2}{3}l + \frac{1}{3}l_1 = l - 9.23$$

$$l_4 = \frac{1}{2}l$$

$$l_5 = \sqrt{32^2 + [l_1 - \frac{1}{2}(l_2 - l_1)]^2}$$

$$= \sqrt{1024 + .25(l_1 + l_2)^2}$$

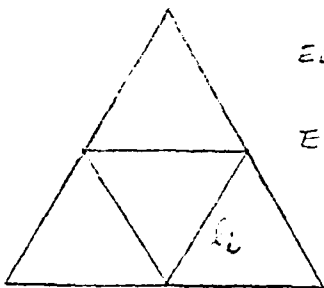
$$= \sqrt{1024 + .25(l - 9.23)^2}$$

$$l_6 = \sqrt{32^2 + [l_2 + \frac{1}{2}(l_3 - l_2)]^2}$$

$$= \sqrt{1024 + .25(l_2 + l_3)^2}$$

$$= \sqrt{1024 + .25(2(-27.7))^2}$$

$$= \sqrt{1024 + ((-13.85))^2}$$



EL. 0.00 $l_8 = l_9 = l_{10}$

EL. 32' $l_7 = l_{11} = \frac{1}{2}l_3$

EL. 64' $l_6 = l_{12} = \frac{1}{3}l_2$

EL. 96' $l_5 = l_{11} = \frac{1}{2}l_1$

By C. Chern Client U. CANARY Subject Structural Concrete Analysis 13-01
 Date 4-26-76 Job No. 27-721-92 Calculation Structural Steel 14 Analysis

$$l_7 = \sqrt{32^2 + \left(\frac{1}{2}l_3\right)^2}$$

$$= \sqrt{1024 + \frac{.25}{9}(L + L - 27.7)^2}$$

$$= \sqrt{1024 + \frac{1}{9}(L - 13.85)^2}$$

$$l_8 = l_2 = \frac{1}{2}L$$

$$l_4 = \frac{1}{2}l_3 = \frac{1}{2}L - 4.61$$

$$l_{10} = \frac{1}{2}l_2 = \frac{1}{2}L - 9.23$$

$$l_{11} = \frac{1}{2}l_1 = \frac{1}{2}L - 13.85$$

Total Length $L = l_1 + l_2 + l_3 + 2l_4 + l_5 + l_6 + 2l_7$
 $+ 3l_8^* + 3l_9^* + 3l_{10}^* + 3l_{11}^*$
 $= (L - 27.7) + (L - 18.46) + (L - 9.23) + 2\left(\frac{1}{2}L\right)$
 $+ \sqrt{1024 + .25(L - 9.23)^2} + \sqrt{1024 + (L - 13.85)^2}$
 $+ 2\sqrt{1024 + .111(L - 13.85)^2} + 1.5L + (1.5L - 13.83)$
 $+ (1.5L - 27.7) + (1.5L - 41.55)$
 $= (10L - 138.47) + \sqrt{1024 + .25(L - 9.23)^2}$
 $+ \sqrt{1024 + (L - 13.85)^2}$
 $+ \sqrt{1024 + .11(L - 13.85)^2}$

* Values increased to take into account
 the weight of angles or extra thickness
 for corrosion protection

CREST OFFSHORE, INC.

Sheet 206 of 21

Date: 11/1/82 Client: U.S. NAVY

Subject: Steel Deck Corrosion Protection
 Calculation: Structural Steel Deck Protection

l	$1024 + 0.47$	$(1024 + .25(l - 9.25))^2$	$\sqrt{1024 + (l - 15.25)^2}$	$\sqrt{1024 + 11(l - 15.25)^2}$	L Total Length (FT)
50	361.53	37.94	42.23	34.17	481.52
55	411.53	37.34	52.13	34.79	531.19
60	461.53	40.85	56.16	35.47	581.01
65	511.53	44.14	60.33	36.22	630.52
70	561.53	47.13	64.63	37.02	680.21
75	611.53	49.88	69.02	37.88	730.31
80	661.53	47.71	73.48	38.50	781.52
85	711.53	49.59	78.01	39.76	833.89
90	761.53	51.53	82.60	40.77	887.13

CREST OFFSHORE, INC.

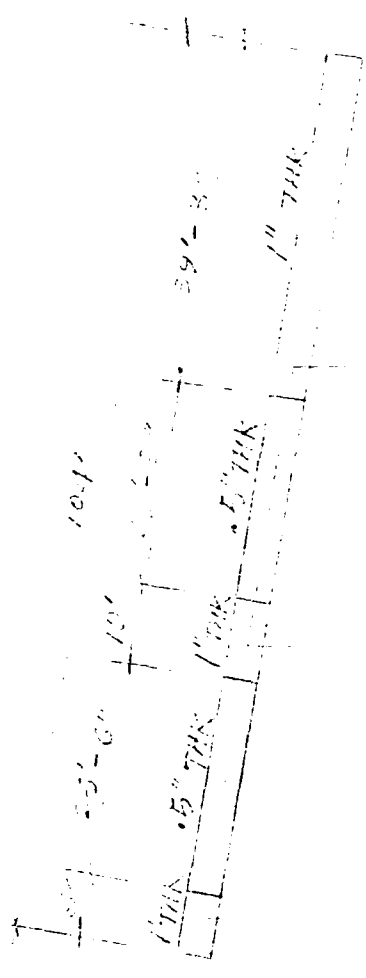
Sheet 6.07 of 27

By C. Chere Client NAVY Subject Structural Concepts Review
 Date 4-26-76 Job No 27-771-92 Calculation Structural Steel Wt. Utilization

BASE SPACING (FT)	BRACE MEMBER SIZE	TOTAL BRACE MEMBER LENGTH (FT)	UNIT WEIGHT (LBS/FT)	TOTAL WEIGHT (LBS)
50	18"φ x .5" WT	441.92	33.43	45,035
55	"	537.79	"	50,256
60	"	594.01	"	55,510
65	20"φ x .5" WT	650.52	104.13	67,739
70	"	707.31	"	73,652
75	"	764.31	"	79,588
80	22"φ x .5" WT	821.52	114.81	94,319
85	"	878.89	"	100,905
90	"	936.43	"	107,512

By C. Chen Client H.S. MATH Subject Structural Concept Analysis
Date 4-27-92 Job No. E7-111-92 Calculation Structural Steel Verification

(1) Jacket Legs (3-Rows)



Wall 1" THK 55'-3"

Wall .5" THK 43'-9"

By: Chen Date: 11/11/11
 Job No: 27-271-92

Subject: Structural Analysis
 Calculation: Structural Steel

Pipe O.D. (in)	SCHEDULE			L-59			Total Weight (LBS)
	SIZE x LENGTH	WGT WT (LBS/FT)	WEIGHT (LBS)	SIZE x LENGTH	WGT WT (LBS/FT)	WEIGHT (LBS)	
36	40" x 48.75'	210.93	10,283	41" x 59.25'	47.51	19,600	29,883
39	43" x 48.75'	226.95	11,064	44" x 59.25'	49.55	25,374	36,438
42	46" x 48.75'	242.97	11,845	47" x 59.25'	49.55	27,144	38,989

CREST OFFSHORE, INC.

Sheet 642 of 27

Client: Shell Subject: 1st & 2nd Quarter Accounting
 Date: 12/1/78 Job No: 573-100-90 Calculation: Set Weight

Oil Pipes (3-Resid)

		36" O.D.	38" O.D.	42" O.D.
100'	100' of 2-6	483.92 x 40 = 13,857#	503.97 x 40 = 20,159#	544.02 x 40 = 21,761#
	100' of 1-5	640.17 x 30 = 32,017#	696.21 x 30 = 34,811#	732.28 x 30 = 37,614#
100'	100' of 1-5	32,007#	34,811#	37,614#
	100' of 2-6	552.90 x 30 = 27,635#	600.76 x 30 = 30,038#	648.82 x 30 = 32,441#
100'	100' of 2-6	27,635#	30,038#	32,441#
	100' of 1-5	552.9(AH)	600.76(AH)	648.82(AH)
TOTAL		137,841	149,857	161,371
		+ 552.7 AH	+ 600.76(AH)	+ 648.82(AH)

By C.R. [unclear] Client U.S. NAVY Subject Structural Concrete Analysis
 Date 4-27-82 Job No 27-271-95 Calculation Strength of Steel Wt. Variation

36-in. Diameter Pipe Piles

BASE SPACING		READ PILE CAPACITY		READ PILE	PILE SEGMENT P-1	
k	k_{sl}	COMPRESSION	TENSION	Penetration	ΔH	$552.7(\Delta H)$
FT	FT	KIPS	KIPS	FT	FT	LEB
50	54.33	2,450	2,150	242.5	122.5	67,706
55	59.33	2,300	2,000	230.0	110.0	60,797
60	64.33	2,125	1,825	217.5	97.5	53,888
65	69.33	2,000	1,700	207.5	87.5	48,361
70	74.33	1,875	1,575	192.5*	72.5	40,071
75	79.33	1,750	1,450	182.5*	62.5	34,544
80	84.33	1,650	1,350	170.0*	50.0	27,635
85	89.33	1,575	1,275	162.5*	42.5	23,490
90	94.33	1,500	1,200	157.5*	37.5	20,726

Note: k = base spacing at midline

k_{sl} = base spacing at B-D line & midline

$(k_{sl} = k + 4.33 \text{ ft})$

ΔH = pile segment length shown on Pg. 6.10

(ΔH = Read Penetration - 120 ft)

* denotes tension control

by C. Clark Client U.S. Navy Subject Structural Concept Analysis
 Date 1-27-73 Job No. 27-77L-9a Calculation Structural Steel Design

30-in. Diameter Pipe Piles

BASE SPACING		REQ'D PILE CAPACITY		REQ'D PILE PENETRATION	PILE SEGMENT P-1	
(l_{sd}	COMPRESSION	TENSION		ΔH	$600.76(\Delta H)$
FT	FT	KIPS	KIPS	FT	FT	LBS
50	54.69	2,450	2,150	227.5	107.5	64,532
55	59.69	2,500	2,000	217.5	97.5	58,574
60	64.69	2,125	1,825	206.0*	85.0	51,065
65	69.69	2,000	1,700	192.5*	72.5	43,535
70	74.69	1,875	1,550	177.5*	57.5	34,544
75	79.69	1,750	1,450	170.0*	50.0	30,038
80	84.69	1,650	1,350	160.0*	40.0	24,030
85	89.69	1,575	1,275	153.0*	35.0	21,027
90	94.69	1,500	1,200	147.5*	27.5	16,921

Note: (= base spacing at mudline

l_{sd} = base spacing at 5-D below mudline
 ($l_{sd} = l + 4.69$ ft)

ΔH = Pile segmental length shown on Fig. 6.10
 (ΔH = Req'd Penetration - 120 ft)

* denotes tension control

By S. Charn Client U.S. #17 Subject Structural Concept Analysis
 Date 4-27-76 Job No 27-771-92 Calculation Structural Stability Analysis

42-in. Diameter Pipe Piles

BASE SPACING		REQ'D PILE CAPACITY		REQ'D PILE PENETRATION	PILE SEGMENT P-1	
l	l_{sd}	COMPRESSION	TENSION		ΔH	$642.82(\Delta H)$
FT	FT	KIPS	KIPS	FT	FT	LBS
60	55.05	2,450	2,150	217.5*	87.5	63,260
55	60.05	2,300	2,000	207.5*	87.5	56,772
65	65.05	2,125	1,825	192.5*	72.5	47,037
50	70.05	2,000	1,700	182.5*	62.5	40,551
70	75.05	1,875	1,550	170.0*	50.0	32,441
75	80.05	1,750	1,450	162.5*	42.5	27,575
80	85.05	1,650	1,350	152.5*	32.5	21,087
85	90.05	1,575	1,275	147.5*	27.5	17,843
90	95.05	1,500	1,200	142.5*	22.5	14,533

Notes: l = base spacing at mudline

l_{sd} = base spacing at 5-D below mudline
 ($l_{sd} = l + 5.05$ ft)

ΔH = Pile segment length (depth shown on Fig. 6.10)
 ($\Delta H =$ Req'd penetration - 120 ft)

* denotes tension control

Client U.S. Gulf

Subject Structural Concept Proposed

Job No. 27-13-1-2

Calculation Structural Steel Piling

PILING WEIGHT

(Refer to P. 6.10)

PILE SPACING AT MID-LINE FT	PILING WEIGHT		
	36" O.D. LBS	39" O.D. LBS	42" O.D. LBS
50	205,547	214,439	223,131
55	193,633	208,431	218,643
60	191,729	200,922	208,910
65	183,202	193,412	202,422
70	177,312	184,401	194,312
75	172,333	179,895	189,446
80	165,476	173,887	182,958
85	161,331	170,884	179,714
90	158,357	166,378	176,460

By C. C. Chou Client U. S. NAVY Subject Structure of Concept Review
 Date 4-5-76 Job No. 22-721-24 Calculation Structural Steel Weight

(V) TOTAL WEIGHT OF STRUCTURE

$$W_T = W_P + W_J + W_S + W_M \quad (1)$$

where W_T = Total Weight of Structure

W_P = Weight of Piling

W_J = Weight of Jacket

W_S = Weight of Superstructure

W_M = Weight of Miscellaneous Items,
 such as boat landing, walkway, etc.

Since it is assumed that the superstructure and the miscellaneous items can be designed in the same amount of steel weight regardless of the change of jacket base spacing, i.e.,

$$W_S + W_M = \text{Constant} \quad (2)$$

Subtracting Eq. (2) from both sides of Eq. (1), it gives

$$W = W_P + W_J \quad (3)$$

where W = weight of piling and jacket

CREST OFFSHORE, INC.

Sheet 6.16. 27

By C. Clark Client U.S. Navy Subject Structural Design Analysis
 Date 4-27-76 Job No. 27-771-92 Calculation Structure St. L. Wt. Design

One-third weight of W (Eq. 3) is added to the sum
 the weights shown in Para 6.07, 6.09 and 6.14.

34 - IN. DIAMETER PILING

BASE SPACE AT MIDLINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	53,375	45,035	205,347	284,465
55	"	50,256	193,633	282,730
60	"	55,510	191,729	251,125
65	"	67,739	156,222	237,827
70	"	73,652	177,712	235,450
75	"	74,588	172,555	235,359
80	"	94,319	166,275	293,631
85	"	100,925	161,331	236,122
90	"	107,512	158,267	235,965

By: C. Chern Client: U.S. NAVY Subject: Structure Concept Analysis
 Date: 8-27-76 Job No. 27-271-1-1 Calculation: Structure Stability Variation

39 - IN. DIAMETER PILING

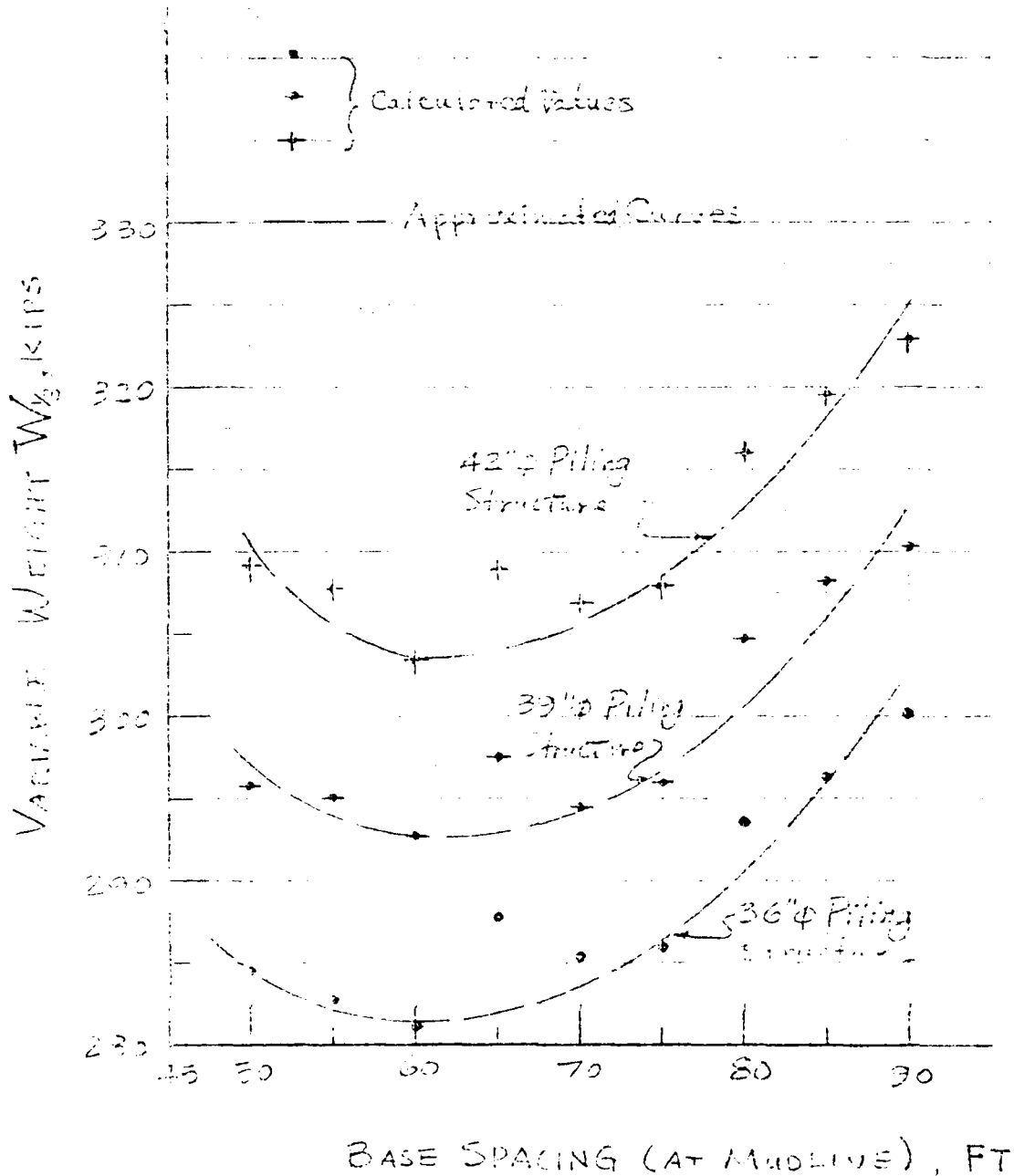
BASE SPACE AT MUDLINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	37,438	45,035	214,439	296,912
55	"	50,256	208,431	298,125
60	"	55,510	202,922	298,870
65	"	67,739	193,412	297,359
70	"	73,652	184,491	294,491
75	"	79,588	179,893	295,921
80	"	94,319	173,837	304,644
85	"	100,905	170,032	308,227
90	"	107,512	182,909	310,528

By C. C. Lamm Client U.S. Navy Subject Structural Concept Analysis
 Date 12-27-26 Job No. 27-25-1-1 Calculation Structural Steel Weight

42 - IN. DIAMETER PILING

BASE SPAC'G AT MUDLINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	33 33	45,035	228,131	309,155
55	"	50,256	215,643	307,883
60	"	55,510	203,910	303,409
65	"	67,739	202,422	309,160
70	"	73,652	194,312	306,953
75	"	79,588	187,446	305,023
80	"	94,319	182,938	316,266
85	"	100,905	179,114	319,023
90	"	107,512	175,460	322,961

27 C. S. Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-22-76 Job No. 27-771-92 Calculation of Structural Stiffness Variation



By C. C. Baker Client M. S. W. Co. Subject Structural Concept for pile (piles)
 Date 11/11/71 Job No. 27071-71 Calculation Struct. of Steel Pile Wharves

Revised in accordance with Graph shown on Pg 5-14

36 - IN. Diameter Pipe Piles

EASING DEPTH	HEAD PILE CAPACITY		HEAD PILE PENETRATION	PILE SETTING P-L	
	COMPRESSION	TENSION		ΔH	552.7(ΔH)
FT	KIPS	KIPS	FT	FT	LEBS
50	2,075	1,700	212.5	92.5	51,125
55	1,900	1,550	192.5*	72.5	40,071
60	1,750	1,400	175.0*	55.0	30,399
65	1,650	1,275	162.5*	42.5	23,490
70	1,550	1,175	155.0*	35.0	19,345
75	1,450	1,100	147.5*	27.5	15,199
80	1,375	1,025	140.0*	20.0	11,054
85	1,300	950	135.0*	15.0	8,291
90	1,250	900	132.5*	12.5	6,909

Notes: ΔH = (pilot Penetration - 120 ft)

Pg. 6-10

* denotes tension control

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis (3-pile)
 Date 5-12-76 Job No. 27-771-92 Calculation Structural Steel Wt. Variation

Revised in Accordance with Graph shown on Pg 5.14

39 - IN. Diameter Pipe Piles

BASE SPAC'G	REQ'D PILE CAPACITY		REQ'D PILE PENETRATION	PILE SEGMENT P-1	
	COMPRESSION	TENSION		ΔH	600.76(ΔH)
FT	KIPS	KIPS	FT	FT	LBS
50	2,075	1,700	192.5*	72.5	43,555.
55	1,900	1,550	177.5*	57.5	34,344.
60	1,750	1,400	165.0*	45.0	27,034.
65	1,650	1,275	155.0*	35.0	21,027.
70	1,550	1,175	145.0*	25.0	15,019.
75	1,450	1,100	140.0*	20.0	12,015.
80	1,375	1,025	135.0*	15.0	9,011.
85	1,300	950	130.0*	10.0	6,008.
90	1,250	900	125.0*	5.0	3,004.

Notes: $\Delta H = (\text{Req'd Penetration} - 120 \text{ ft})$ Pg. 6-10

* denotes tension control

By C. Chern Client U.S. NAVY Subject Structural Concept Analysis (3-pile)
 Date 5-12-76 Job No 27-771-92 Calculation Structural Steel Wt. Variation

Revised in Accordance with Graph shown on Pg 5.14

42 - IN. Diameter Pipe Piles

BASE SPAC'G	REQ'D PILE CAPACITY		REQ'D PILE PENETRATION	PILE SEGMENT P-1	
	COMPRESSION	TENSION		ΔH	$643.32(\Delta H)$
FT	KIPS	KIPS	FT	FT	LBS
50	2,075	1,700	182.5*	62.5	40,351.
55	1,900	1,550	167.5*	47.5	30,819.
60	1,750	1,400	157.5*	37.5	24,331.
65	1,650	1,275	147.5*	27.5	17,843.
70	1,550	1,175	140.0*	20.0	12,976.
75	1,450	1,100	135.0*	15.0	9,732.
80	1,375	1,025	130.0*	10.0	6,488.
85	1,300	950	125.0*	5.0	3,244.
90	1,250	900	120.0*	0	0.

Notes: $\Delta H = (\text{Req'd Penetration} - 120 \text{ ft})$

Pg. 6-10

* denotes tension control

By C. Chera Client U.S. NAVY Subject Structural Concept Analysis (3000)
 Date 5-10-75 Job No 27-771-92 Calculation Structural Steel Wt Variation

PILING WEIGHT (REVISED)

(Refer to Pg. 6.10)

BASE SPACING AT MUD LINE	PILING WEIGHT		
	36" O.D.	39" O.D.	42" O.D.
FT	LBS	LBS	LBS
50	122,966	193,412	202,422
55	177,912	184,401	192,690
60	166,240	176,891	186,202
65	161,331	170,854	179,714
70	157,186	164,876	174,847
75	153,040	161,872	171,603
80	148,895	158,868	168,359
85	144,750	155,863	165,115
90	144,750	152,861	161,871

CREST OFFSHORE, INC.

Sheet 624 of 27

By C. [unclear] Client H. S. [unclear] Project Structure Concept Analysis (P-10)
 Date 10/1/68 Job No. 10000000 Calculation Footings & Pile Weight

W_{1/3}

36 - IN. DIAMETER PILING

PILE SPACE AT MAX LINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	37,886	45,035	182,966	267,887
55	"	50,256	177,912	262,054
60	"	55,510	168,240	257,636
65	"	67,739	161,331	262,956
70	"	73,652	157,186	264,724
75	"	79,348	153,040	266,514
80	"	94,317	143,895	277,100
85	"	100,903	146,132	280,923
90	"	107,512	144,750	283,143

CREST OFFSHORE, INC.

Sheet 622 of 27

By C. Chern Client U.S. Navy Subject Structural Concept Analysis (3-pile)
 Date 5-10-76 Job No 27771-96 Calculation Structural Steel Wt Variation

W_{1/3}

39 - 111. DIAMETER PILING

BASE SPACE AT Mud LINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	36,485	45,035	193,412	274,932
55	"	50,256	184,401	271,047
60	"	55,510	176,891	268,839
65	"	67,739	170,884	275,061
70	"	73,652	164,376	274,966
75	"	79,588	161,872	277,898
80	"	94,319	159,868	289,625
85	"	100,905	155,365	293,208
90	"	107,512	152,861	296,811

CREST OFFSHORE, INC.

Sheet 626 of 27

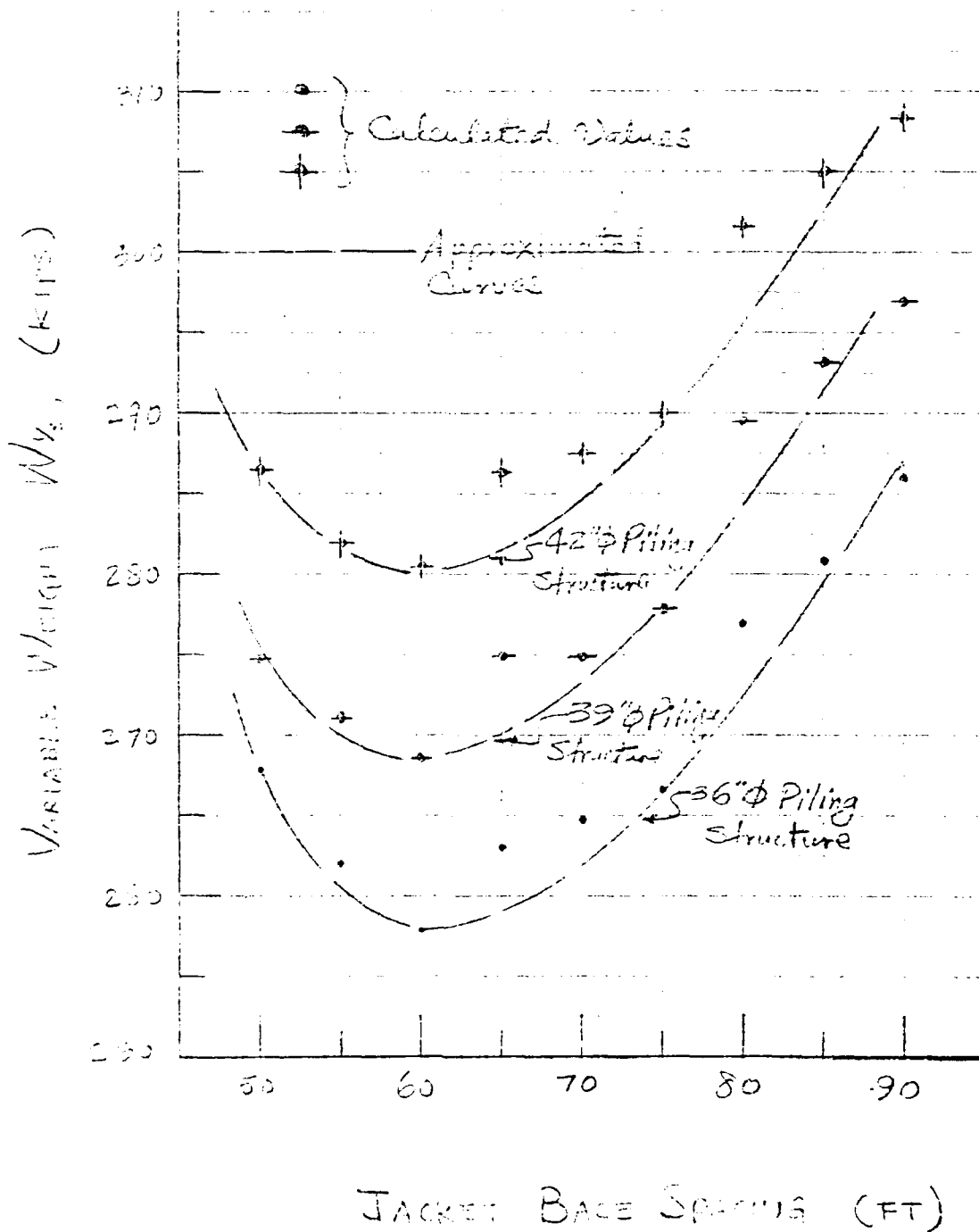
By C. Cherry Client U.S. Navy Subject Structural Concept Analysis (3-pile)
 Date 3-10-76 Job No. 1771-96 Calculation Structural Steel Wt. Variation

W_{1/2}

42 - IN. DIAMETER PILING

BASE SPACE AT MUD LINE	WEIGHT			
	JACKET		PILING	TOTAL
	LEG	BRACES		
FT	LBS	LBS	LBS	LBS
50	33,929	45,035	202,422	286,446
55	"	50,256	192,690	281,935
60	"	55,510	186,202	280,701
65	"	67,739	179,714	286,442
70	"	73,652	174,847	287,488
75	"	79,588	171,603	290,180
80	"	94,319	168,559	301,667
85	"	100,905	165,115	305,009
90	"	107,512	161,871	308,372

By C. Cooper Client G. S. Wynn Subject Structural Concept Analysis of Piling
 Date 5-19-72 Job No 27-726-24 Calculation Structural Steel 14' Jacket



SECTION 7

STRUCTURAL CONFIGURATION

7.1 INTRODUCTION

Set forth herein is the conceptual configuration for the three-pile structure. This configuration was selected primarily on the basis of weight optimization as presented previously.

CREST OFFSHORE, INC.

Sheet 7.02 of 16

BY S. J. [unclear] Client U. S. W. [unclear] Subject Structural Concept Analysis
Date 4-29-76 Job No. 27-171-95 Calculation Structural Configuration

6.2 PLANS AND ELEVATIONS

By C. C. ... Client U.S. NAVY

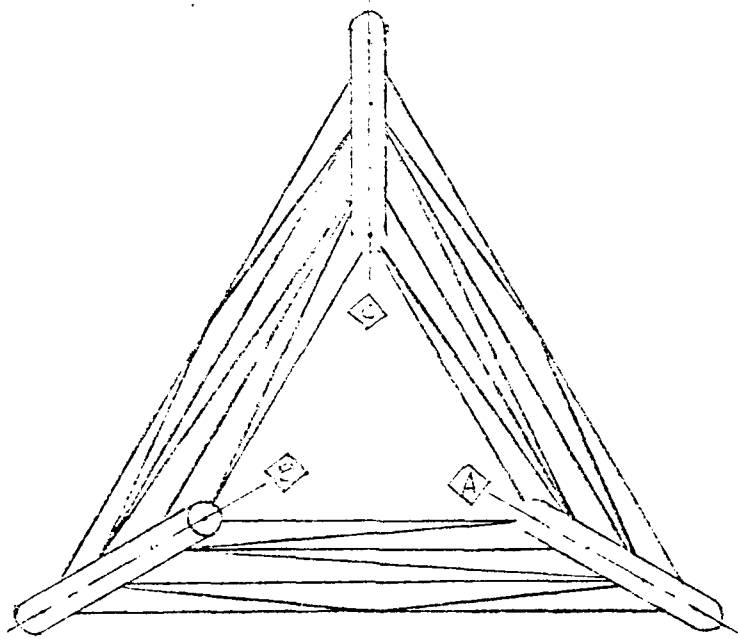
Subject Structural Concept Analysis

Date 4-2-53 Job No. 27-271-92

Calculation Structural Connections

KEY PLAN

SCALE : $\frac{1}{16}'' = 1'-0''$



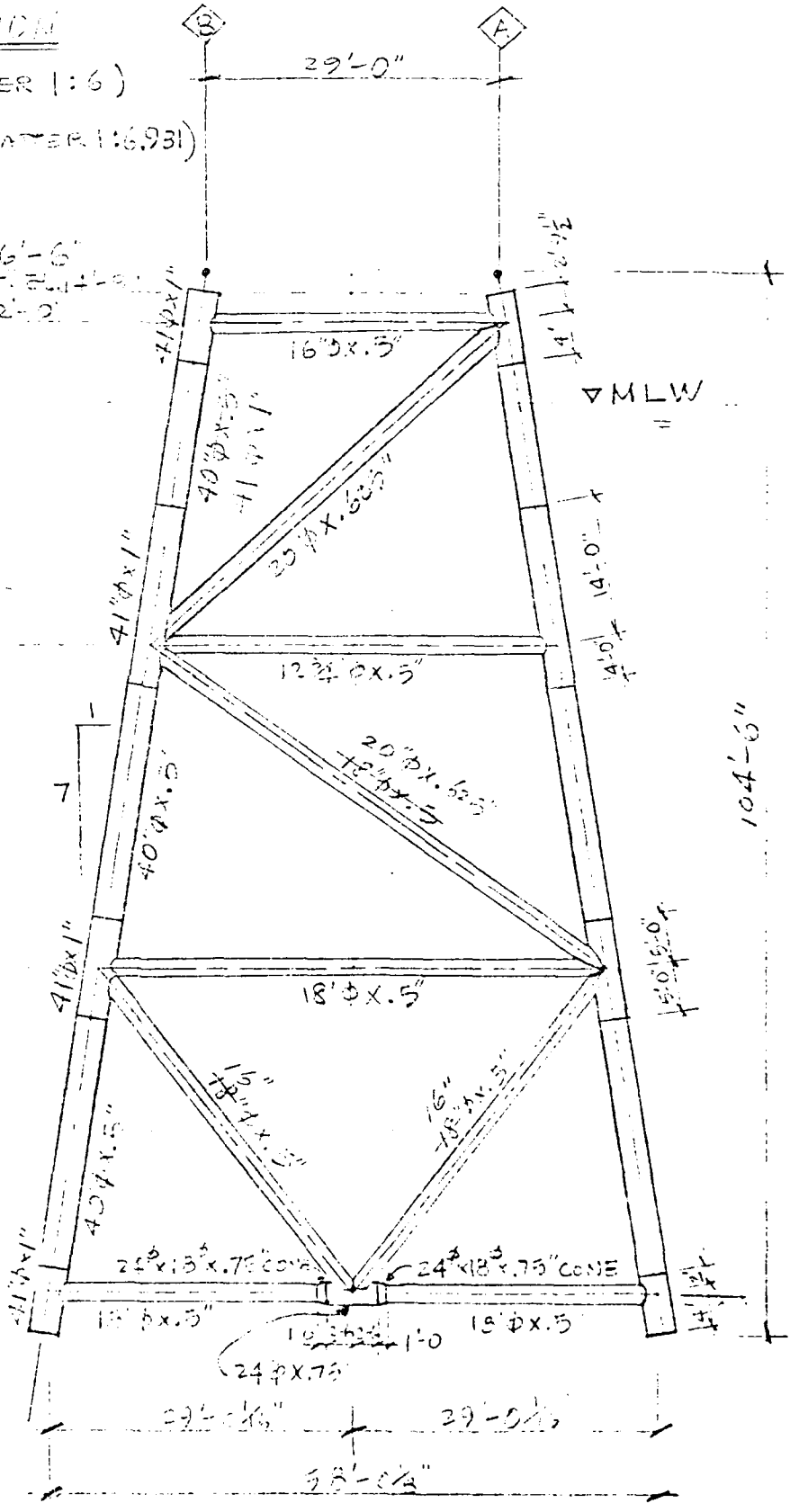
By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-2-76 Job No. 27-771-92 Calculation Structural Configuration

JACKET ELEVATION

(TRUE BATTER 1:6)
 (APPROXIMATE BATTER 1:6.931)

Row
 ⬡ — ⬡
 ⬡ — ⬡
 ⬡ — ⬡

$$\begin{aligned}
 &= 29 + 2 \cdot \left(\frac{102.5}{6}\right) \cos 30^\circ \\
 &= 29 + 29.012 \\
 &= 58.012 \text{ ft} \\
 &= 58' - 0\frac{1}{8}'' \quad \text{EL. (A) } 20' - 0'' \\
 &= 63' - 2\frac{1}{8}'' \quad \text{EL. (A) } 52' - 0''
 \end{aligned}$$

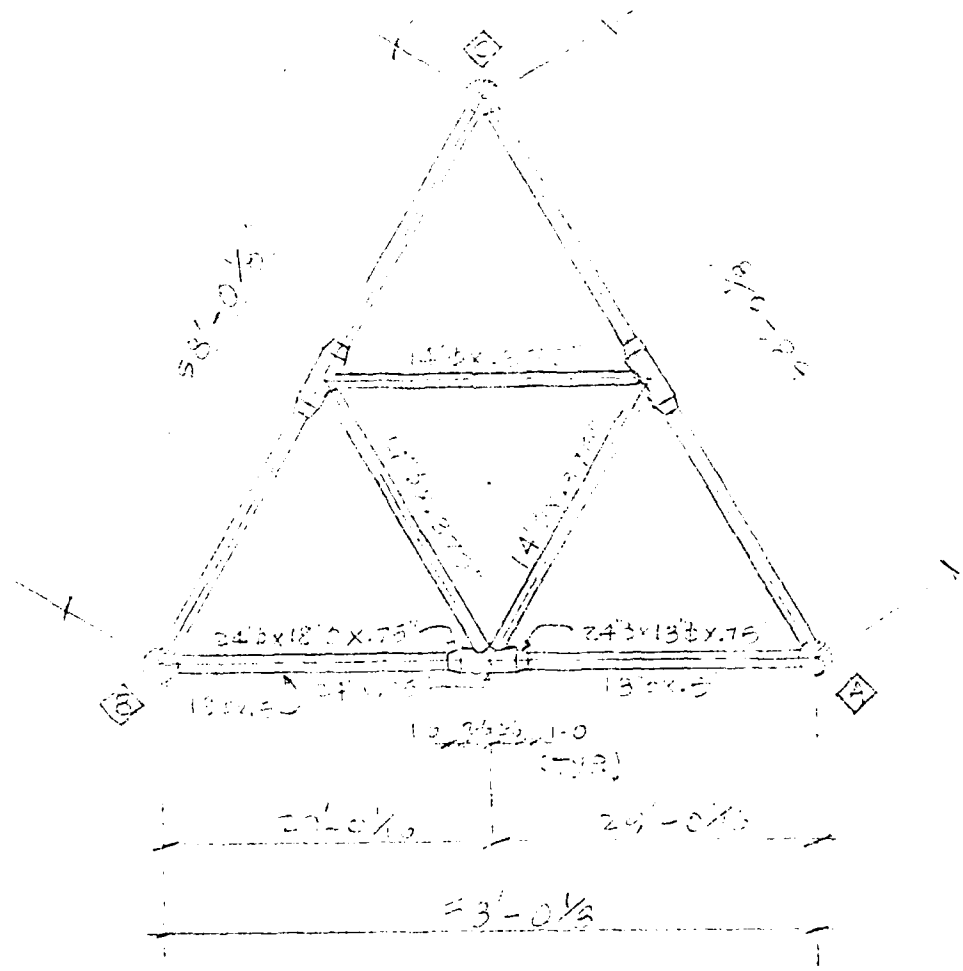


Some 1/8" = 1'-0"

By C.S. [Signature] Client U.S. NAVY Subject Structural Concept Analysis
Date 4-22-92 Job No. 27-221-92 Calculation Structural Configuration

PLAN OF EL. 113.4'-0"

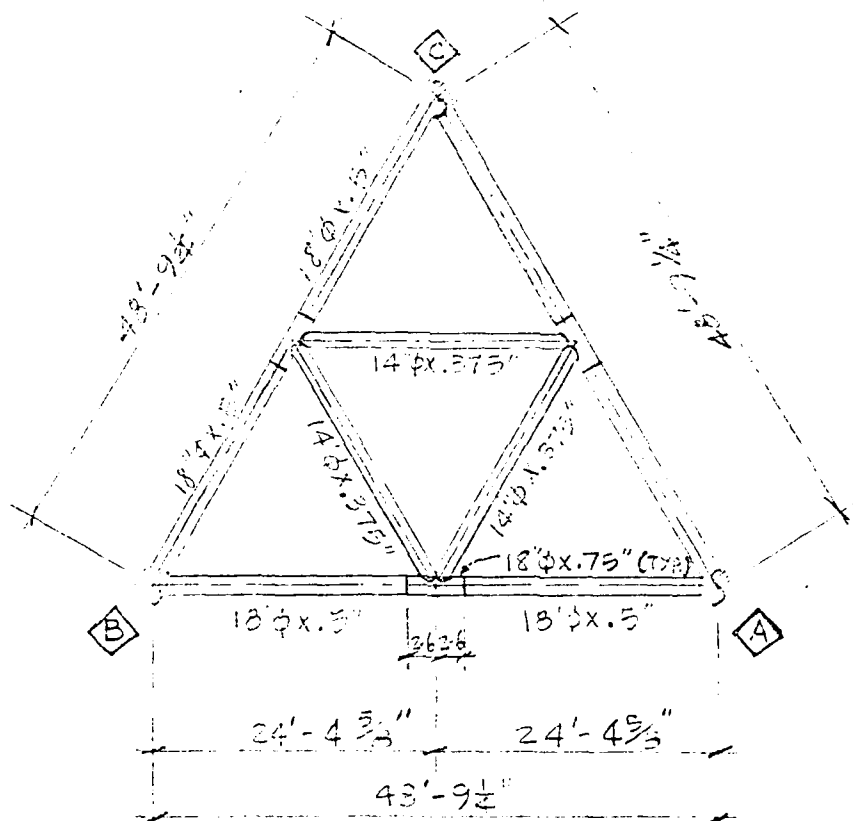
Scale: $1/8" = 1'-0"$



By J. Chinn Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-6-78 Job No 27-171-72 Calculation Structural Configuration

PLAN @ EL. (+) 52'-0"

SCALE 1/16" = 1'-0"

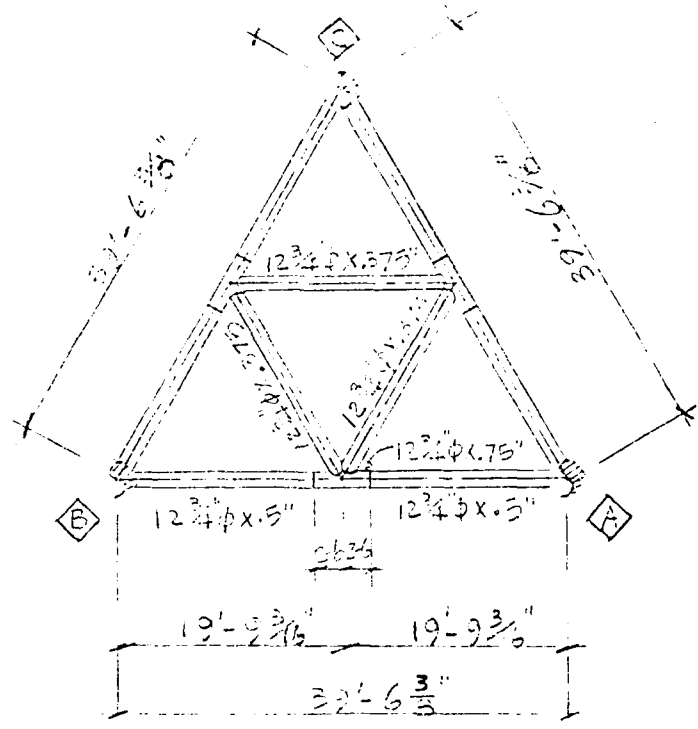


$$\begin{aligned}
 * L &= 29 + 2 \cdot \left(\frac{63.3}{6} \right) \cos 30^\circ \\
 &= 29 + 19.7542 \\
 &= 48'-9 \frac{1}{4}"
 \end{aligned}$$

By C. S. ... Client U.S. ... Subject Structural Concept Development
 Date 4-6-76 Job No. 27-211-74 Calculation Structural Foundation

PLAN @ EL. 20'-0"

SCALE = $\frac{1}{16}'' = 1'-0''$



$$\begin{aligned}
 * & (20.9 + 2 \left(\frac{20.9}{6} \right) \cos 30^\circ) \\
 & = 20.9 + 10.3065 \\
 & = 31'-6 \frac{3}{8}''
 \end{aligned}$$

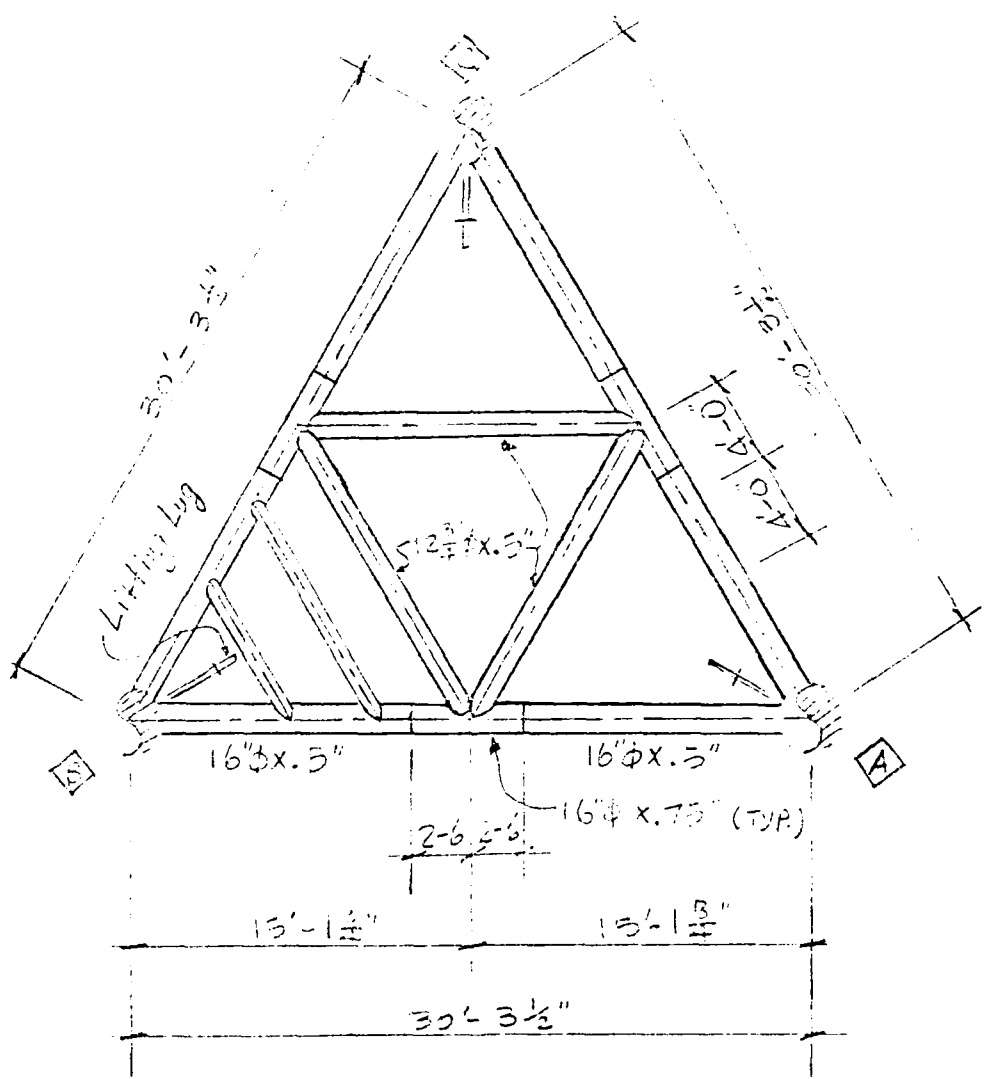
Project Crest U.S. No. 1
Date 12-1-72 Job No. 22-1-72

Subject Steel Truss Concept for
Calculation Structural Analysis

PLAN OF EL. (+) 12'-0"

(TOP OF ALL PIPE EL. (+) 12'-0")

SCALE 1/2" = 1'-0"

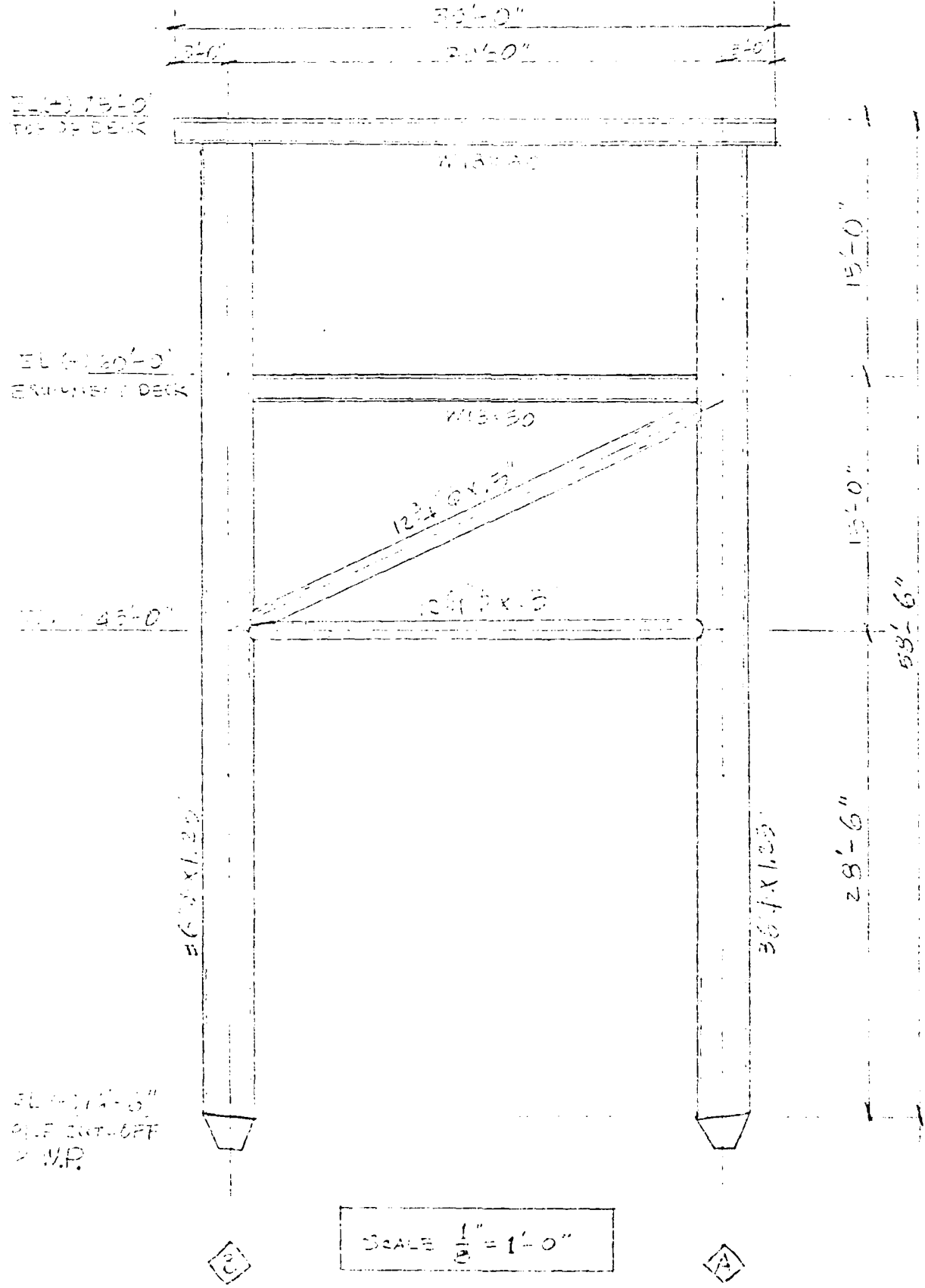


* $1 = 29 + 2 \left(\frac{1}{2} \right) \text{COVERS}$
 $= 29 + 1.0$
 $= 30'-3 \frac{1}{2}"$

CREST OFFSHORE, INC.

Sheet 7 of 15
 13-11-82

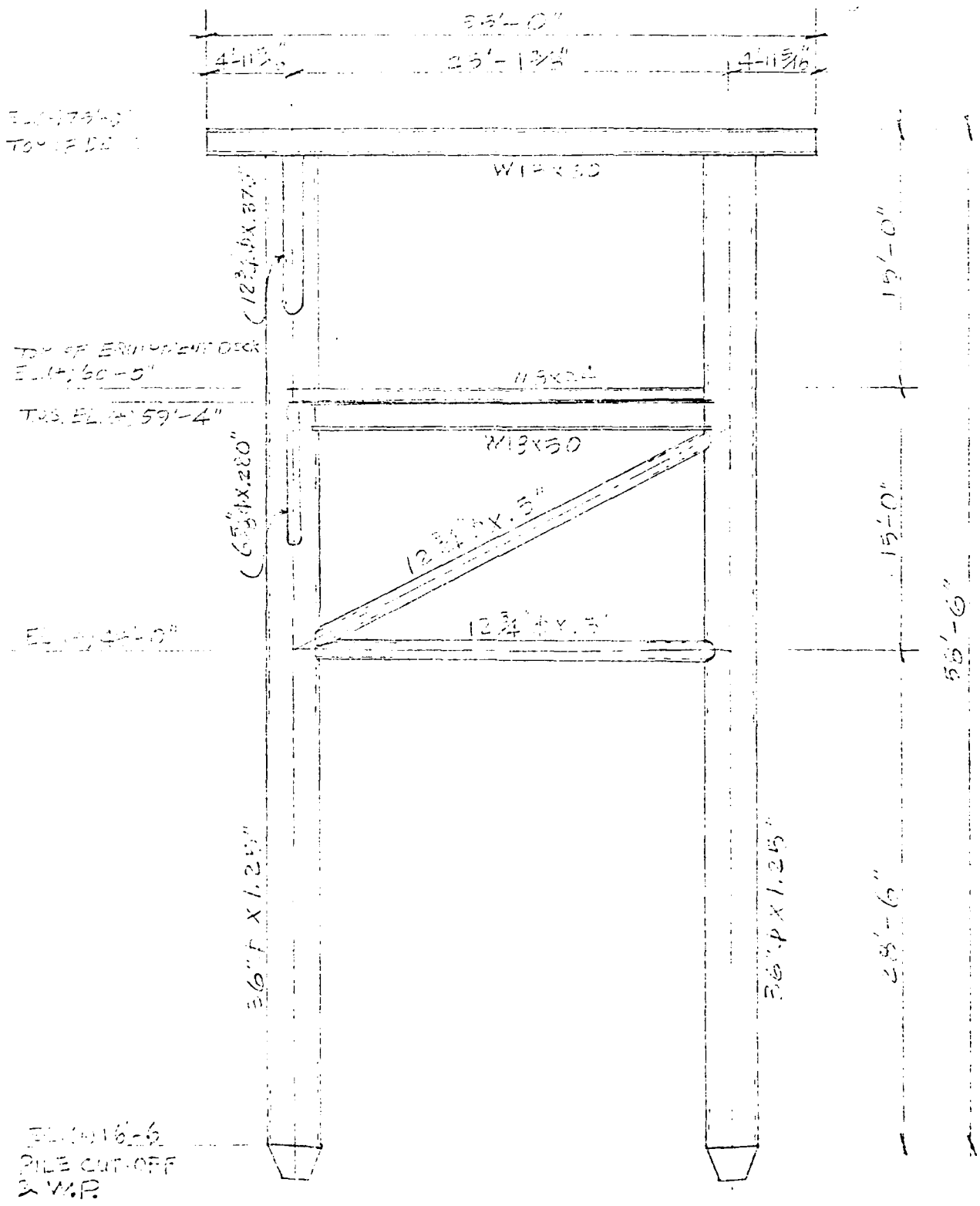
By [Signature] Client U.S. Navy Subject Structural Concept Analysis
 Date 1-27-82 Job No. 271-82 Calculation Structural Configuration



CREST OFFSHORE, INC.

Sheet 7.12 of 13

By C. Chan Client U.S. NAVY Subject Structural Concept Analysis
 Date 1-7-76 Job No. 76-12-72 Calculation Structural Calculations



EL. (+) 73'-0"
TOP OF DECK

TOP OF EQUIPMENT DECK
EL. (+) 60'-0"

TOS. EL. (+) 59'-4"

EL. (+) 44'-0"

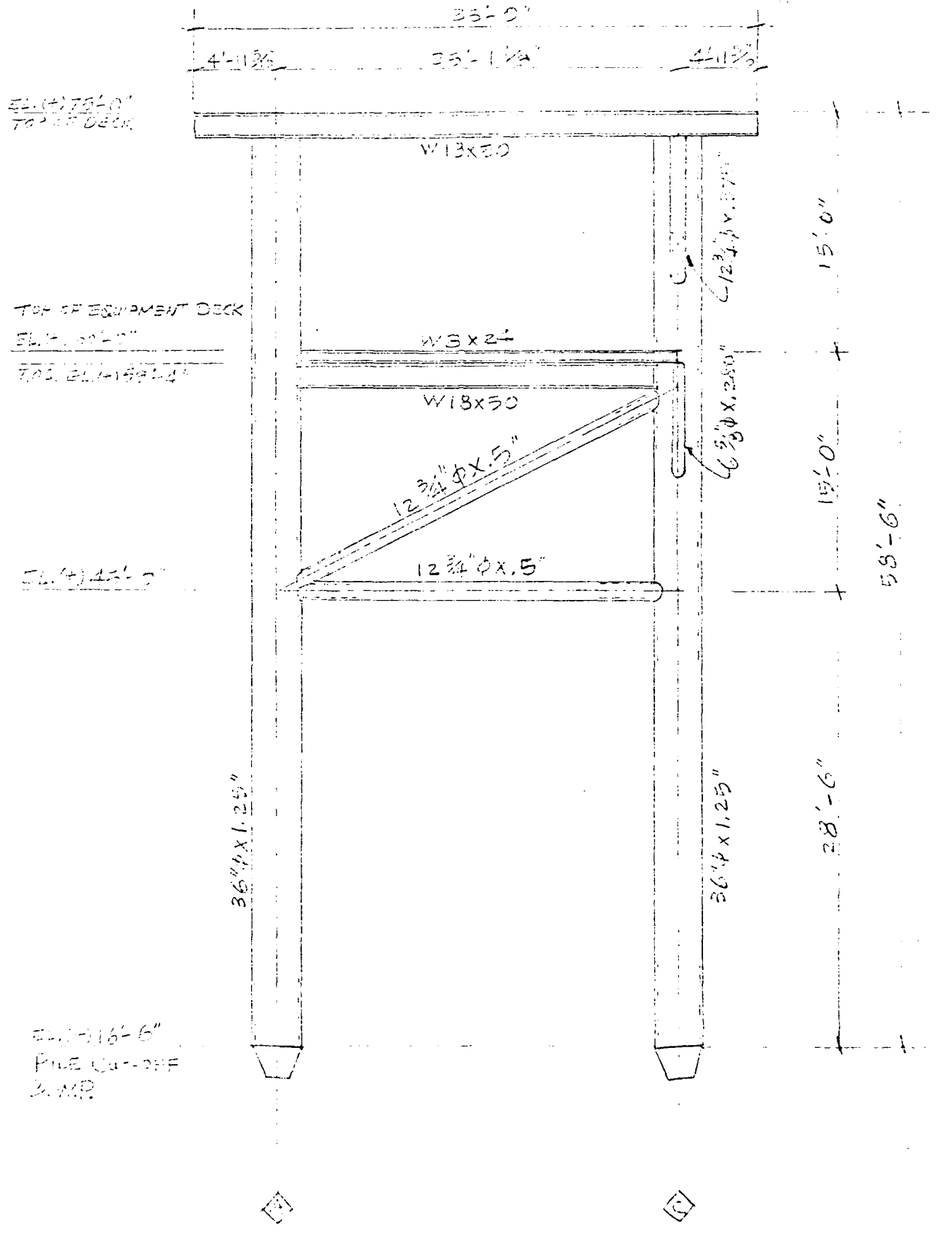
EL. (+) 16'-6"
PILE CUT-OFF
2 W.P.

*23.0780' = 23.115'
= 25'-1 3/8"

④

⑤

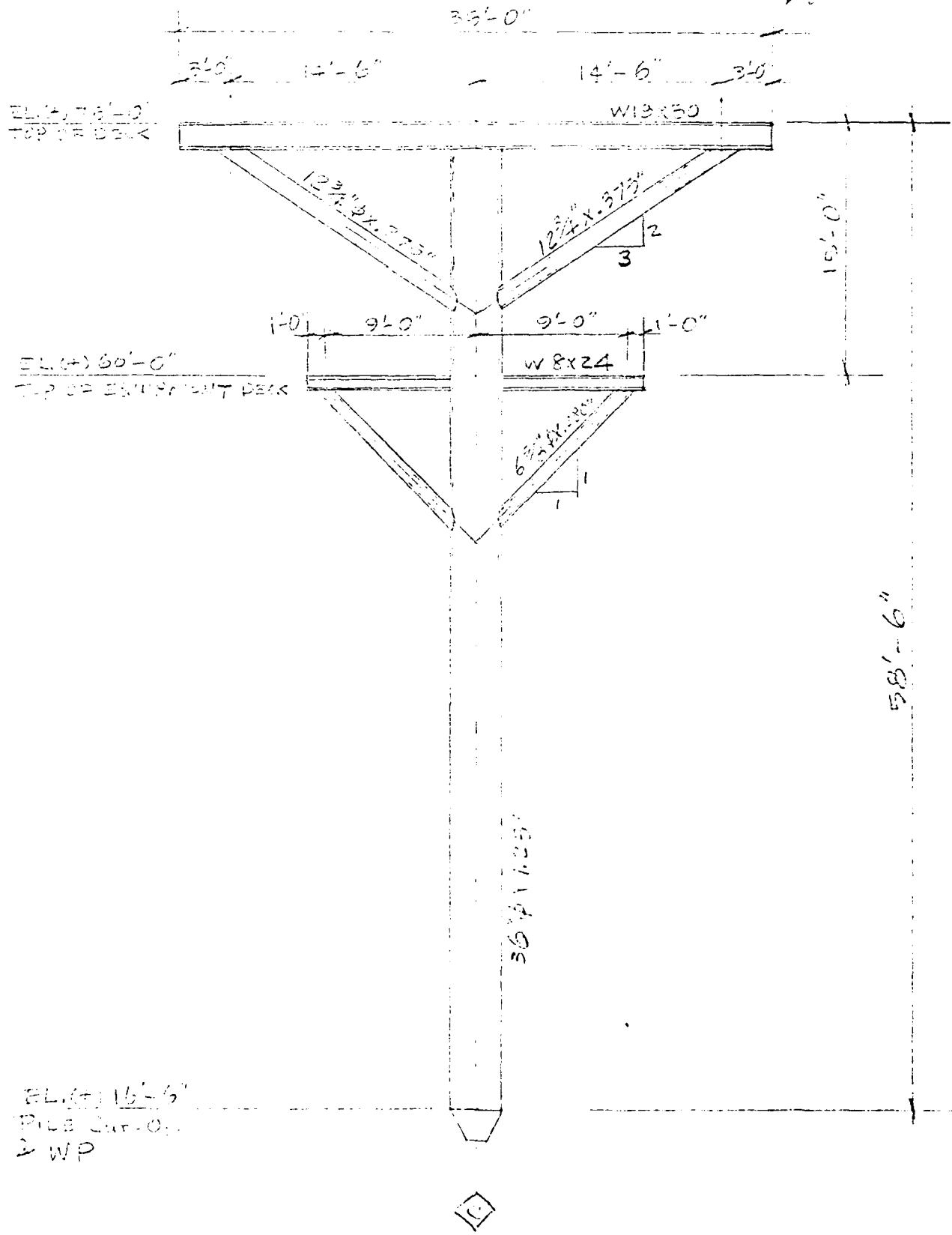
By Client U.S. NAVY Subject Support of Concept model
Date 4-2-76 Job No. 27-721-22 Calculation Star Truss Configuration



CREST OFFSHORE, INC.

Sheet 7.12 of 12

By Client Subject
Date Job No. Calculation



EL (+) 15'-6"
PILE CAP
2 WP

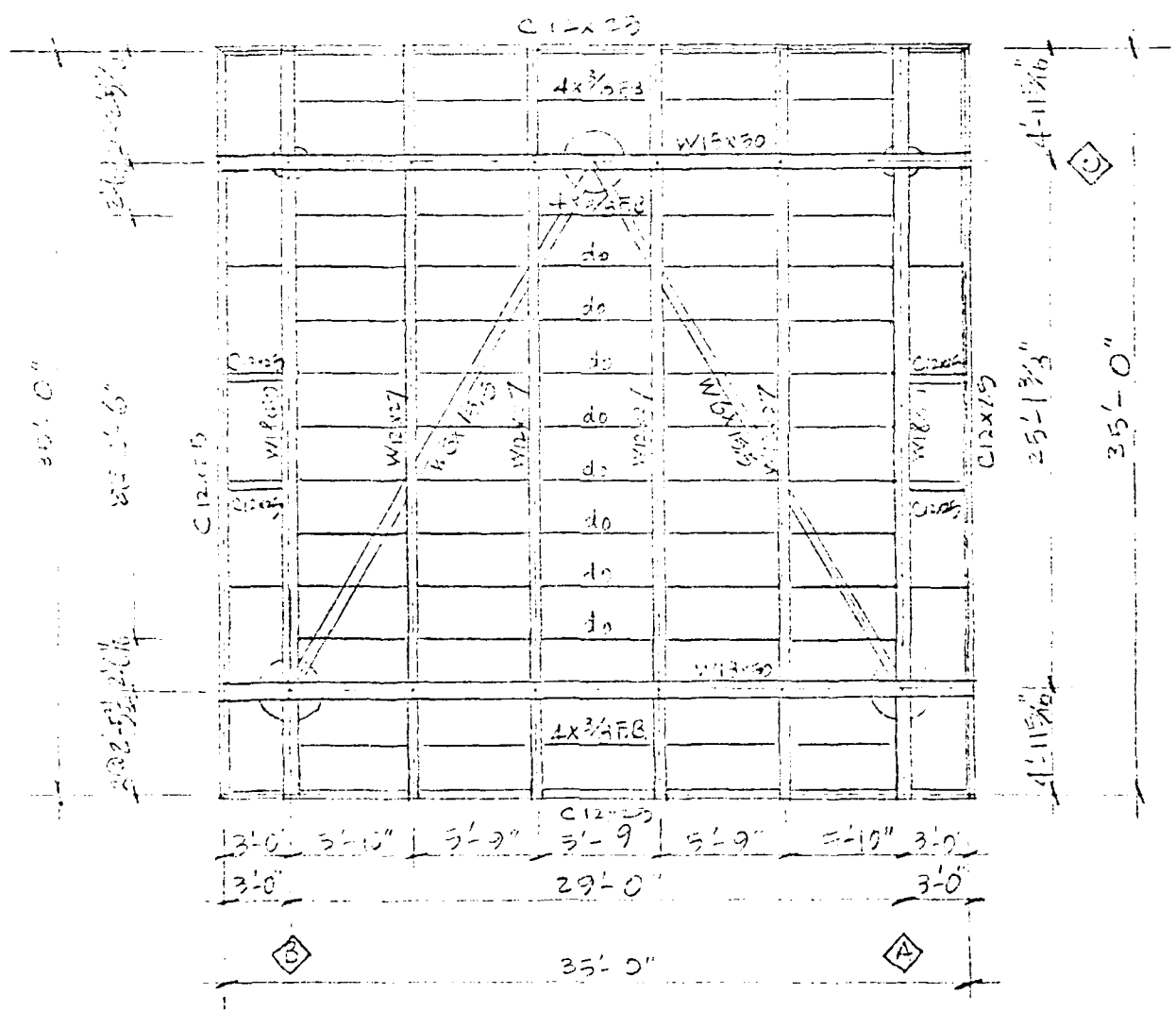
CREST OFFSHORE, INC.

Sheet 7-13 of 13 (3.014)

By C. Clark Client U.S. NAVY Subject Structural Layout of Platform
 Date 7-6-76 Job No. 27-771-22 Calculation Structural Configuration

PLAN @ EL(4) 75'-0"

SCALE $\frac{1}{8}'' = 1'-0''$



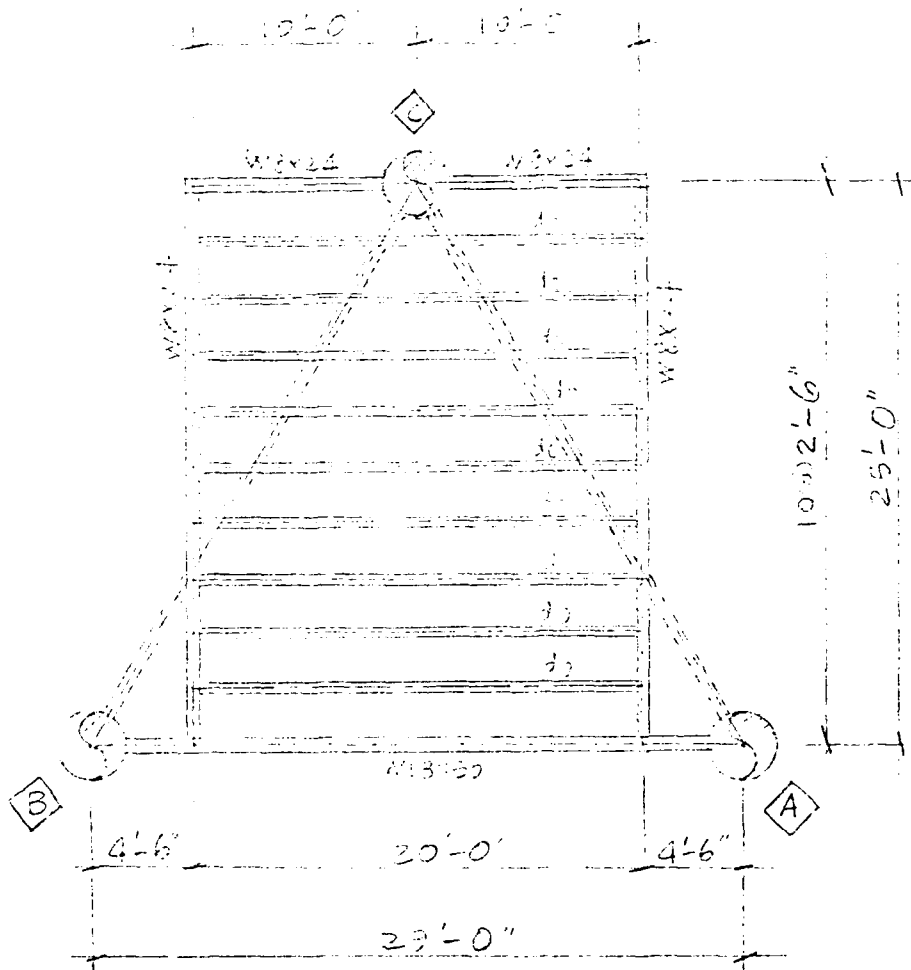
DREST OFFSHORE, INC.

Sheet 7-14 of 12 13-11

By C. J. [unclear] Client U.S. NAVY Subject Structural Concept for [unclear]
Date 4-2-75 Job No 27-021-10 Calculation Structural Configuration

PLAN @ EL. 4'-6"-0"

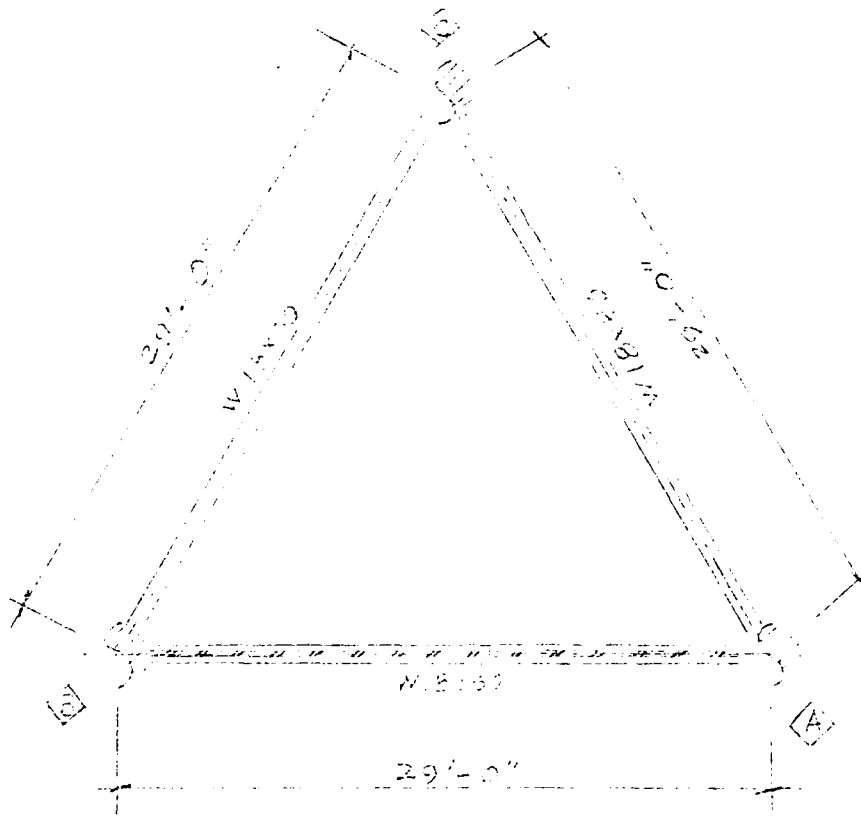
SCALE $\frac{1}{8}'' = 1'-0''$



R. C. Chock Client U.S. Navy Subject Structural Concept for Deck
Date 4-2-78 Job No. 27-771-92 Calculation Structural Configuration

PLAN @ EL. (+) 59'-4"

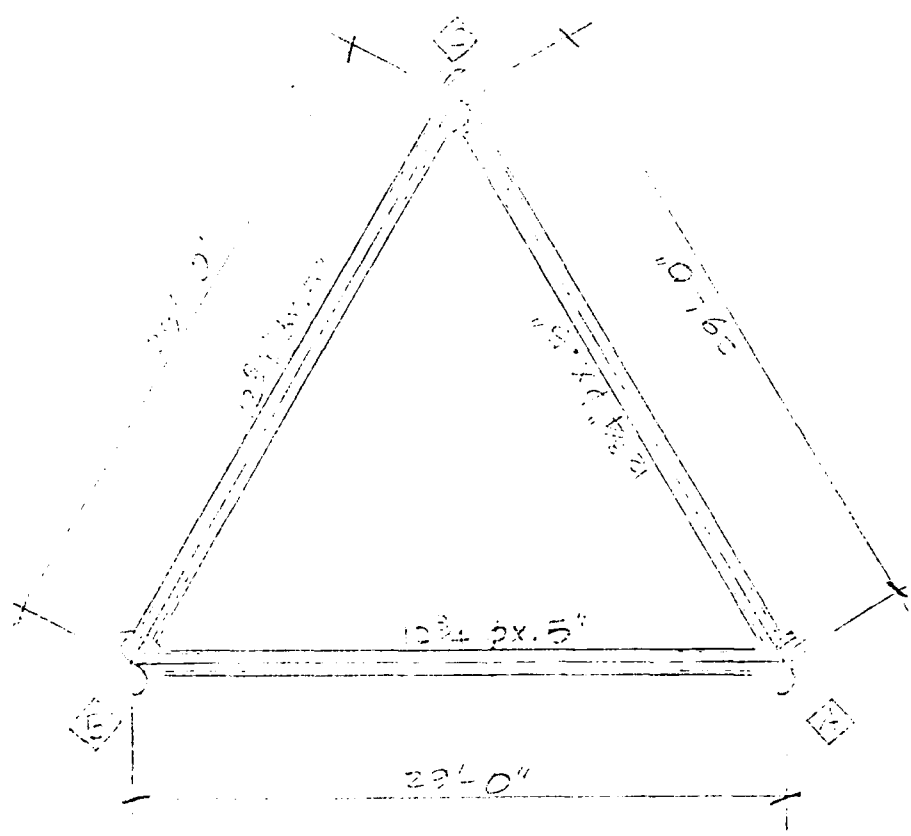
Scale = $\frac{1}{3}'' = 1'-0''$



By S. Chan Client U.S. NAVY
Date 4-6-75 Job No. 27-771-24

Subject Structural Concept Analysis
Calculation Structural Configuration

PLAN @ ELEV 45'-0"



SECTION 8
STRUCTURAL IDEALIZATION

8.1 INTRODUCTION

The material within this section establishes the mathematical idealization of the three-pile structural concept. This material consists of joint coordinates, member locations, member sizes and location of reactions.

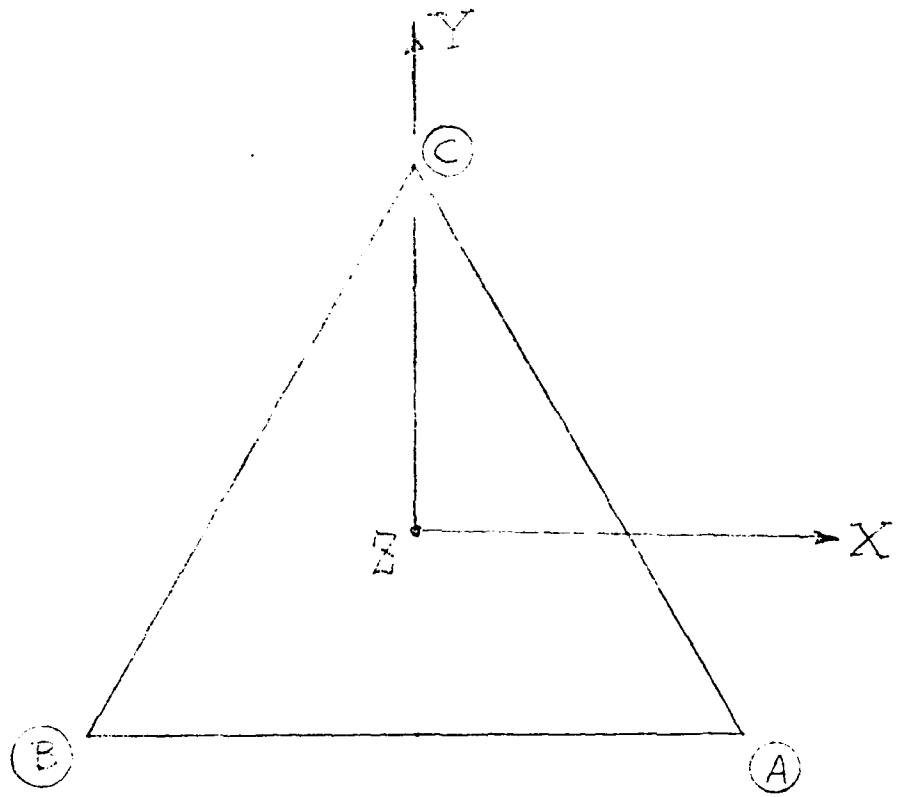
By C. Chinn Client U.S. NAVY Subject Structural General Analysis
Date 4-29-76 Job No. 27-771-03 Calculation Structural Investigation

8.2 PLANS AND ELEVATIONS

by C. Chinn Client U.S. NAVY Subject Structural Concept Analysis
Date 4-8-76 Job No. 27-721-92 Calculation Structural Identification

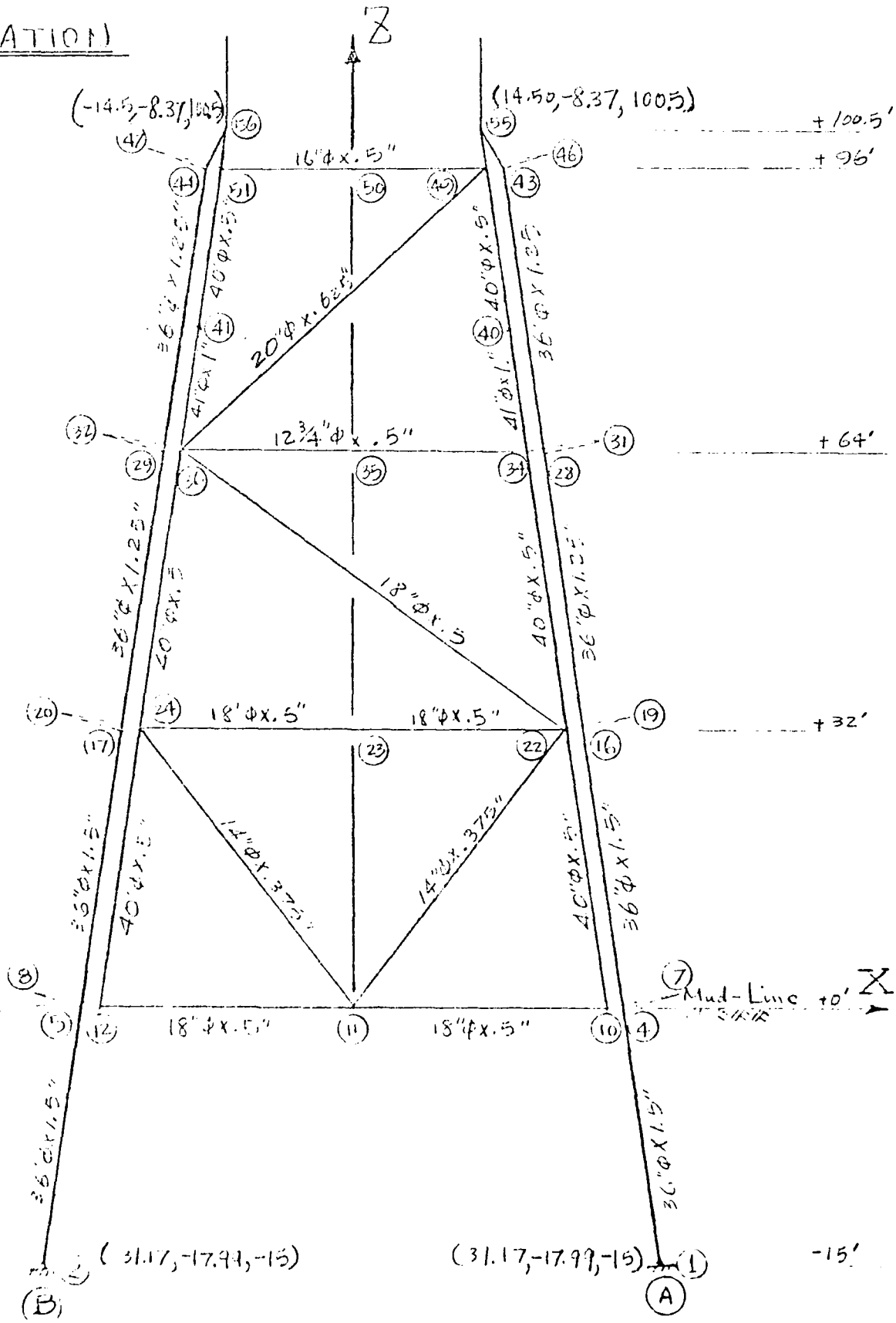
KEY PLAN

SCALE $\frac{1}{16}'' = 1'-0''$

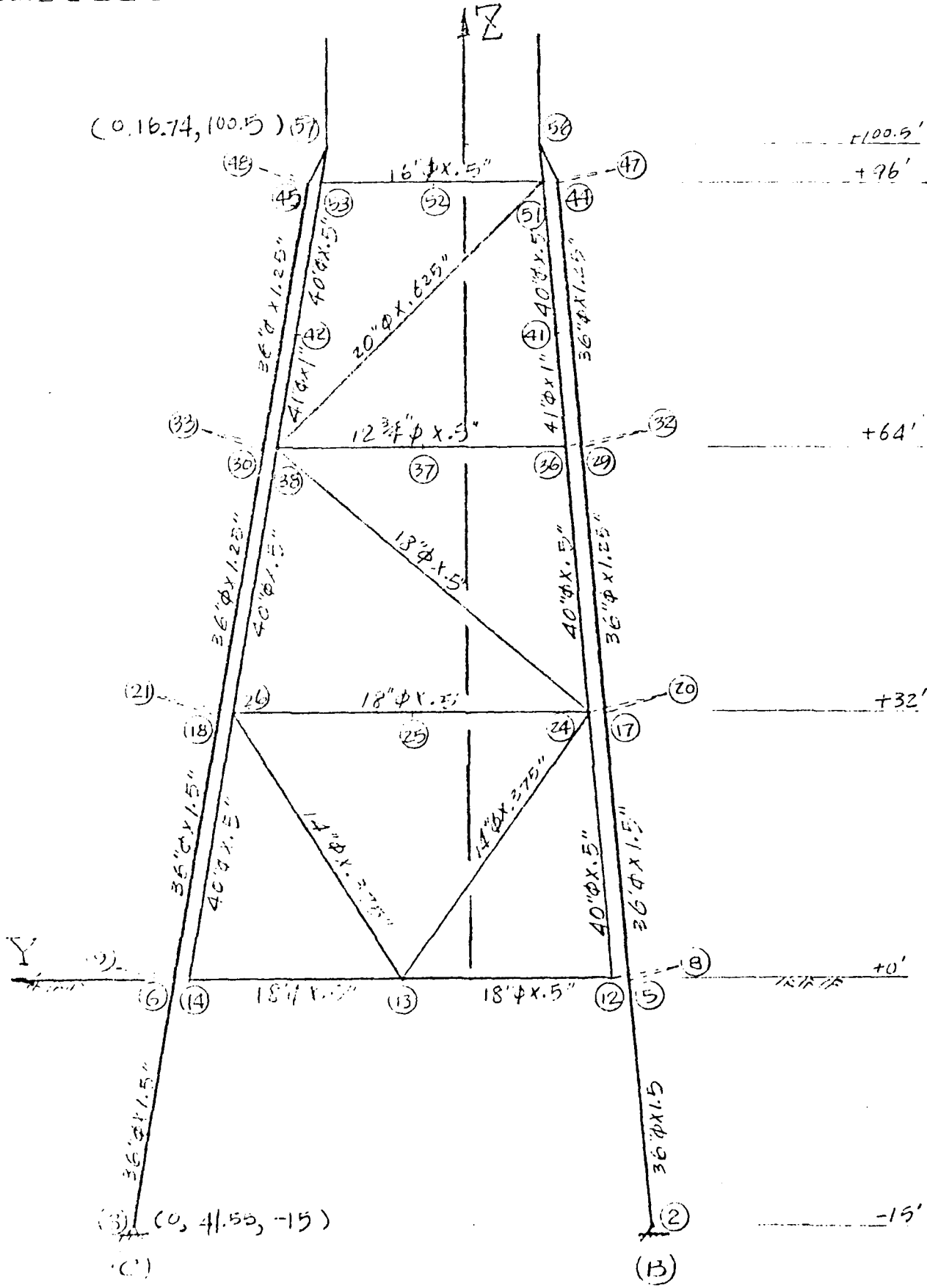


By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-2-73 Job No. 27-771-21 Calculation Struct. Idealization

ELEVATION



by S. C. ... Client U.S. ... Subject Structural Concept Analysis
Date 4-2-76 Job No 27-271-22 Calculation Structural

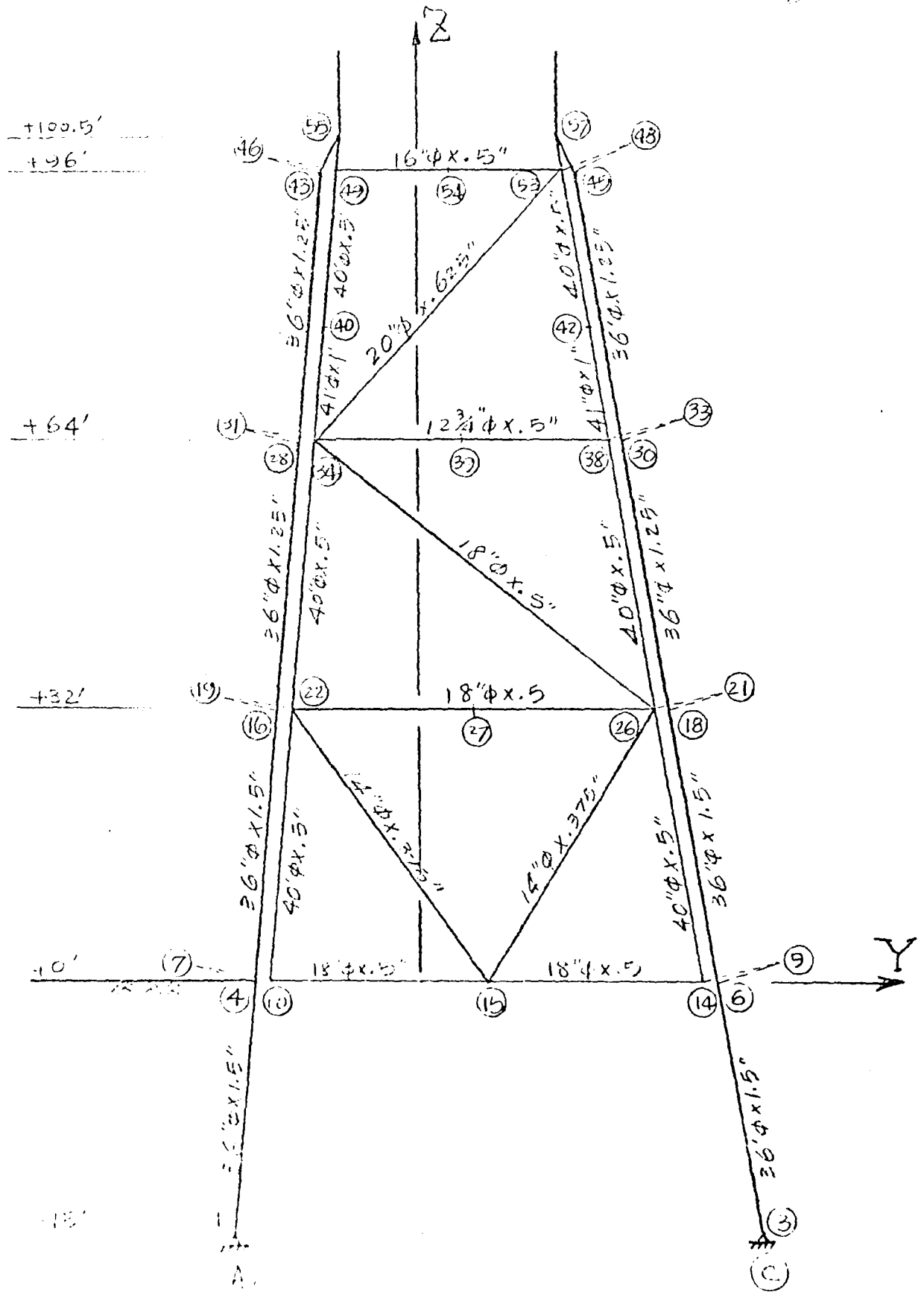


By C. S. [unclear] Client U.S. NAVY

Subject Structural Concept Analysis

Date 1-2-75 Job No. 37-221-12

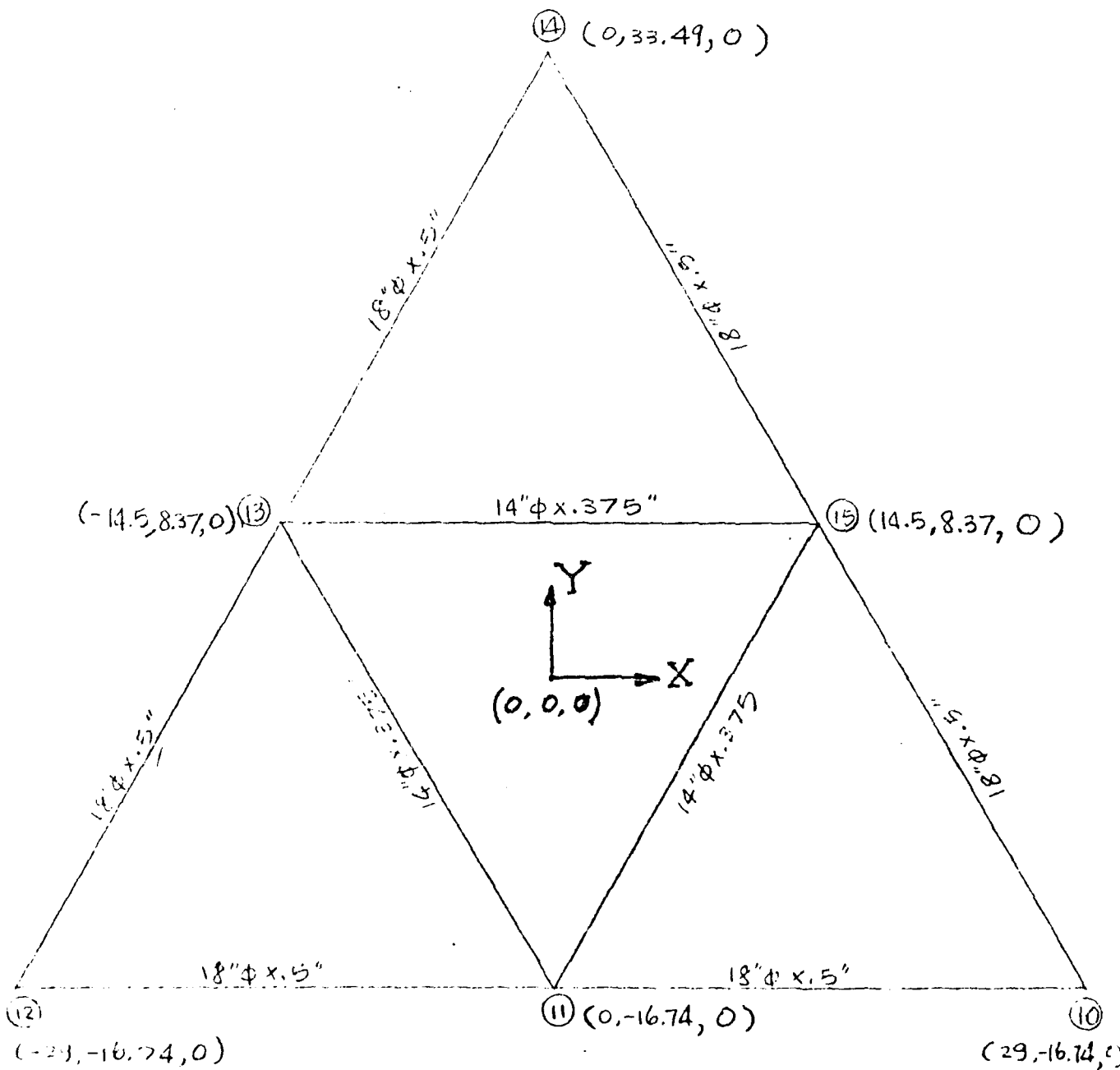
Calculation Structural Analysis



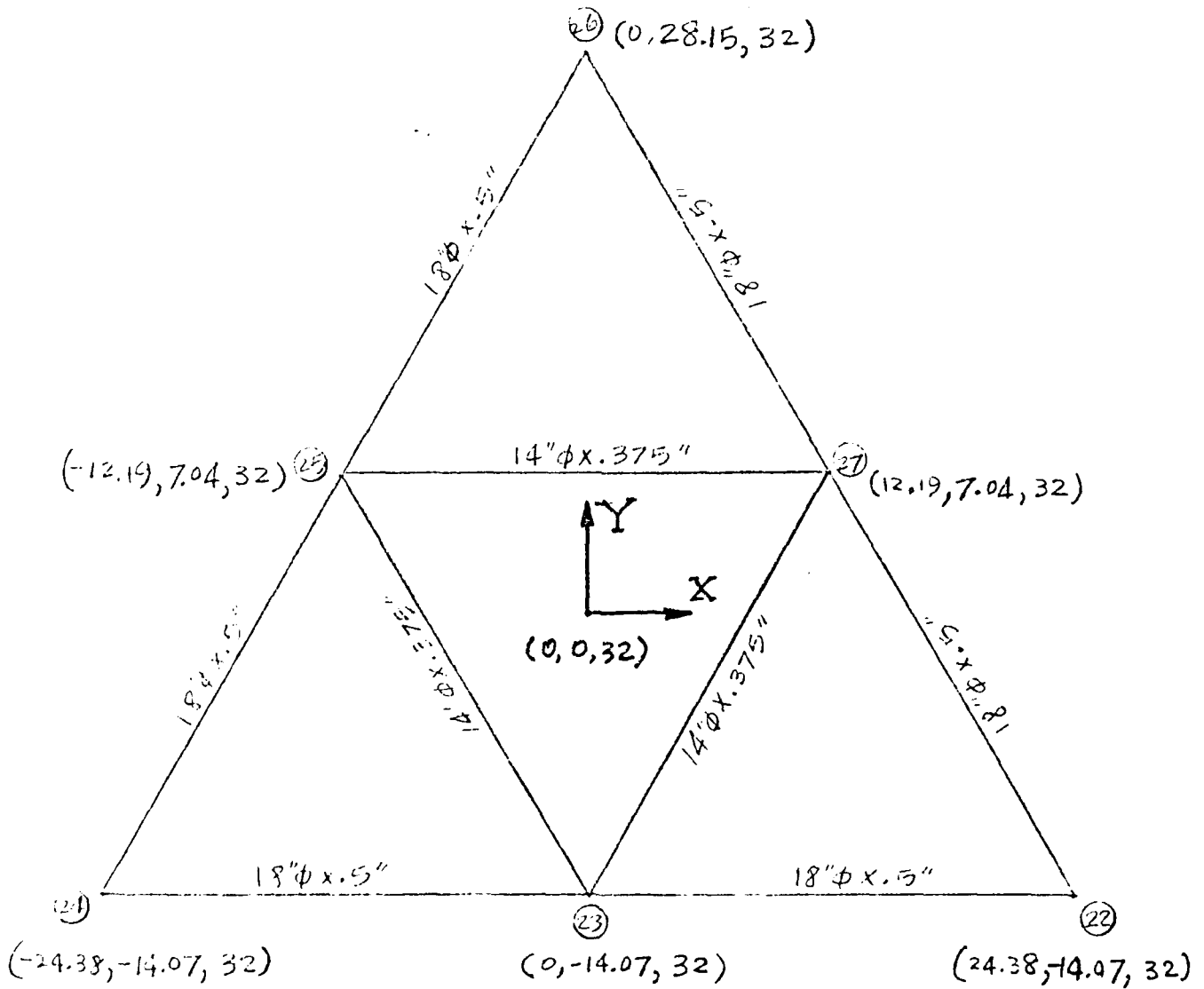
By C. J. ... Client Shell Subject Structural Concept Analysis (S-CAL)
Date 4-2-76 Job No 22-771-73 Calculation Structural Identification

PLAN

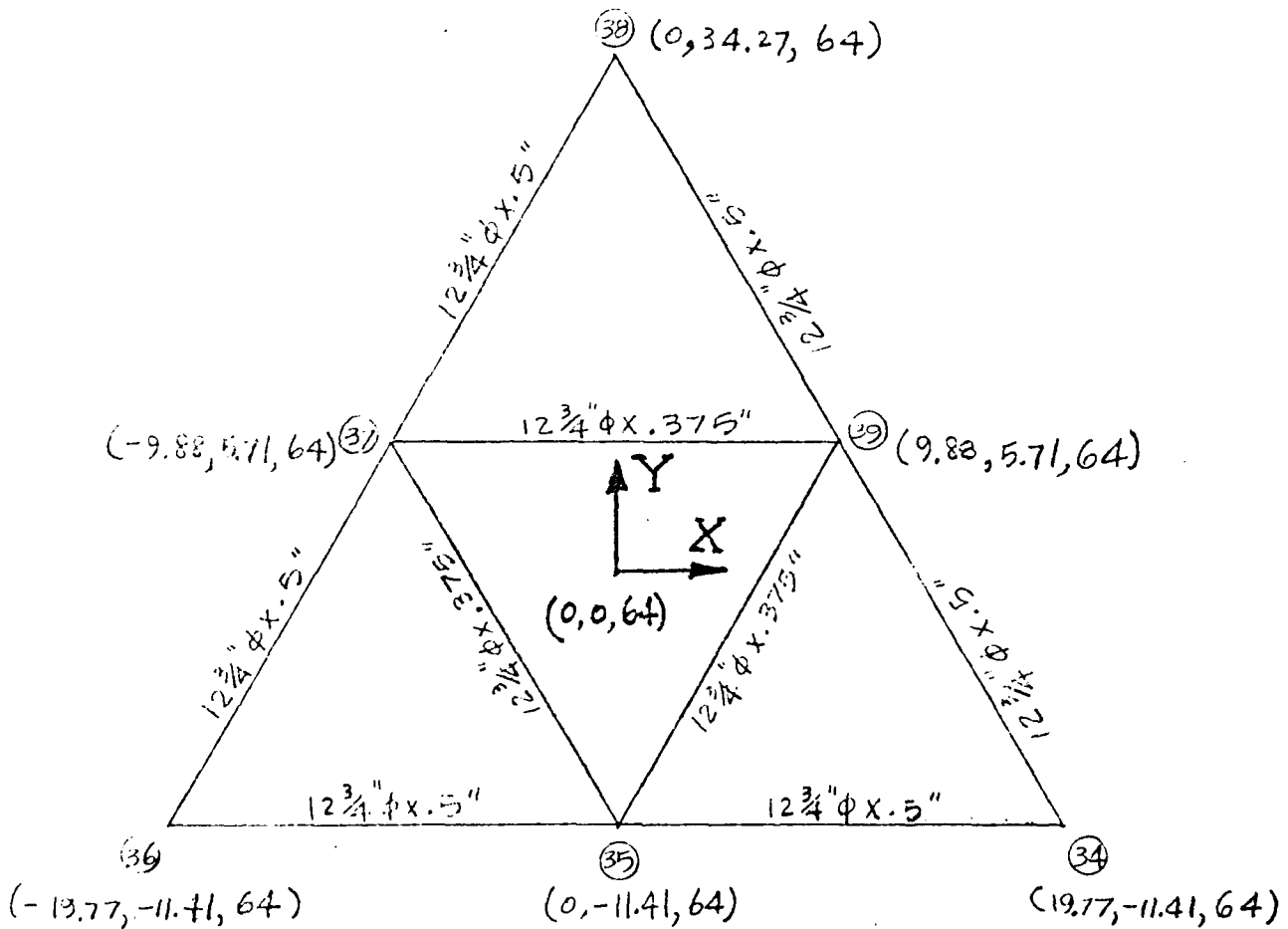
SCALE $\frac{1}{8}" 1' 0"$



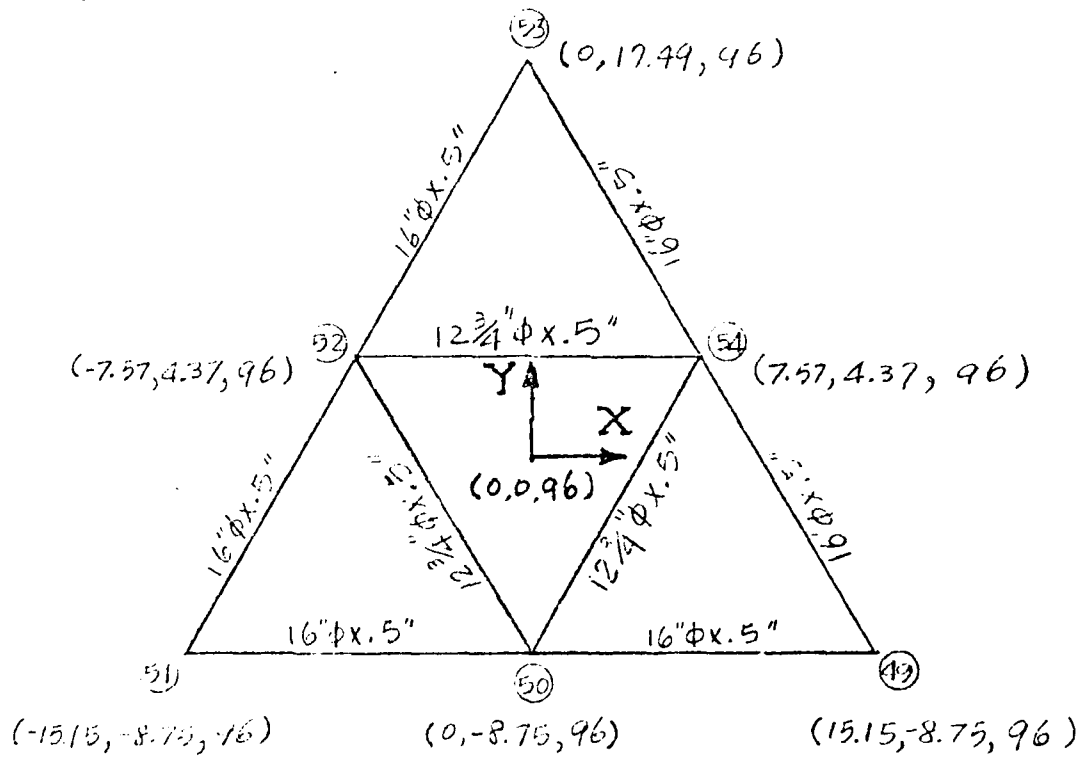
By C. Chen Client USMIX Subject Structural Concept Analysis
Date 4-2-76 Job No. 27-071-02 Calculation Structural Identification



By C. Chow Client U.S. NAVY Subject Structural Concept Design
Date 4-7-76 Job No. 2077-02 Calculation Structural Investigation



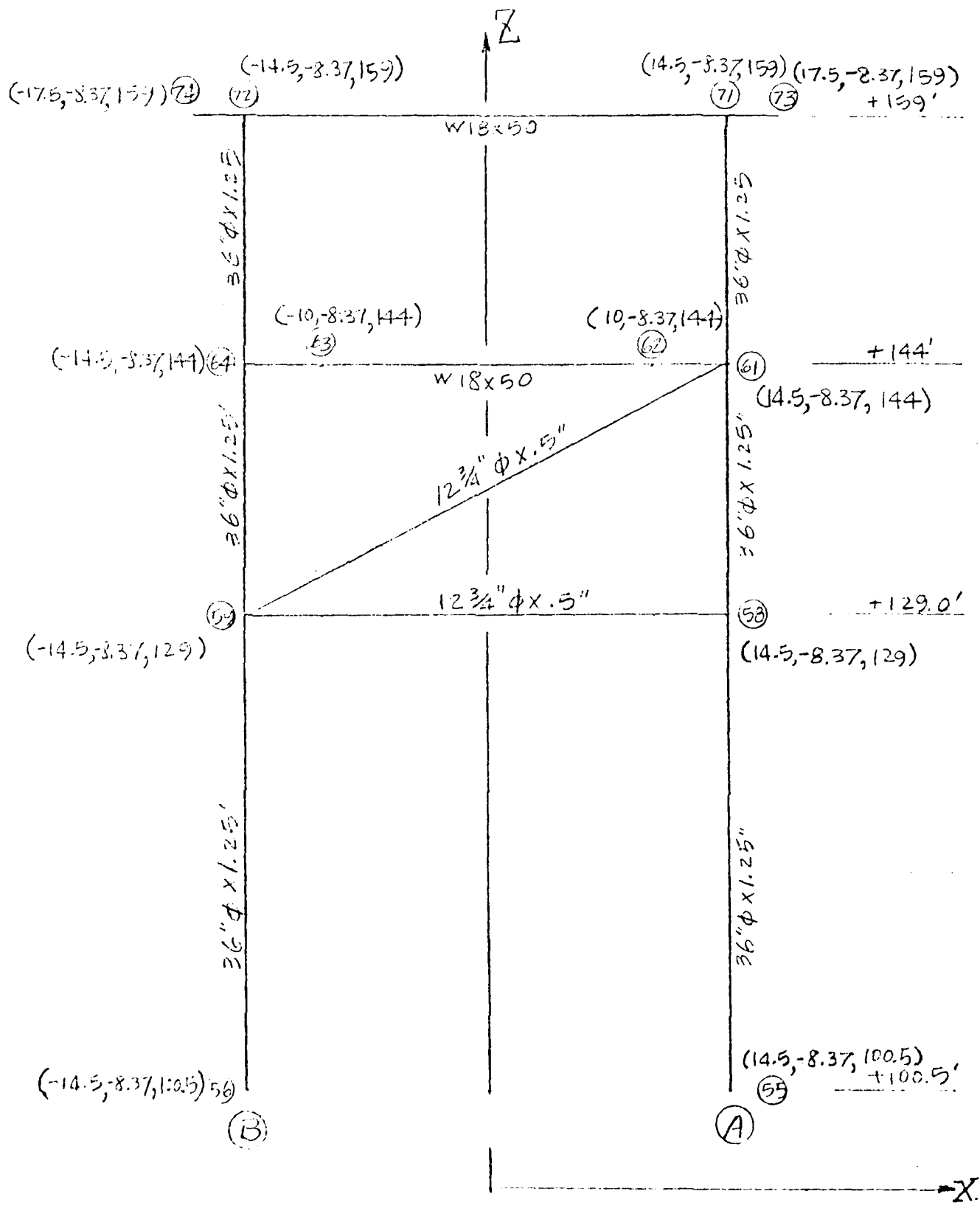
By C. Brown Client U.S. NAVY Subject Structural Concept Analysis
Date 4-7-76 Job No. 3-1-71-92 Calculation Structural Identification



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Sheet 2.11 of 17

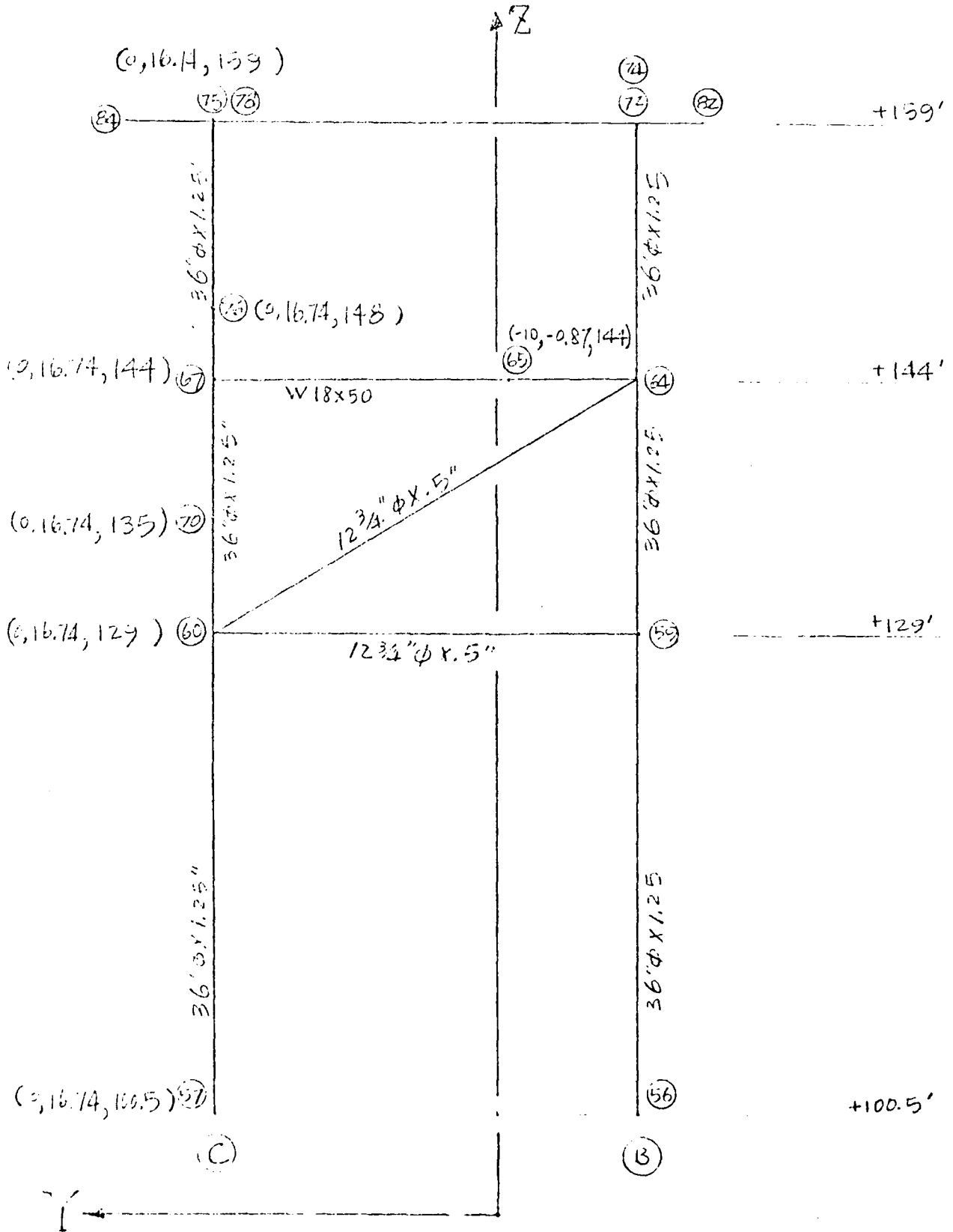
Client U.S. NAVY Subject Structural Design of Platform
 Date 11/12/72 Job No. 27771-92 Calculation Structural Investigation



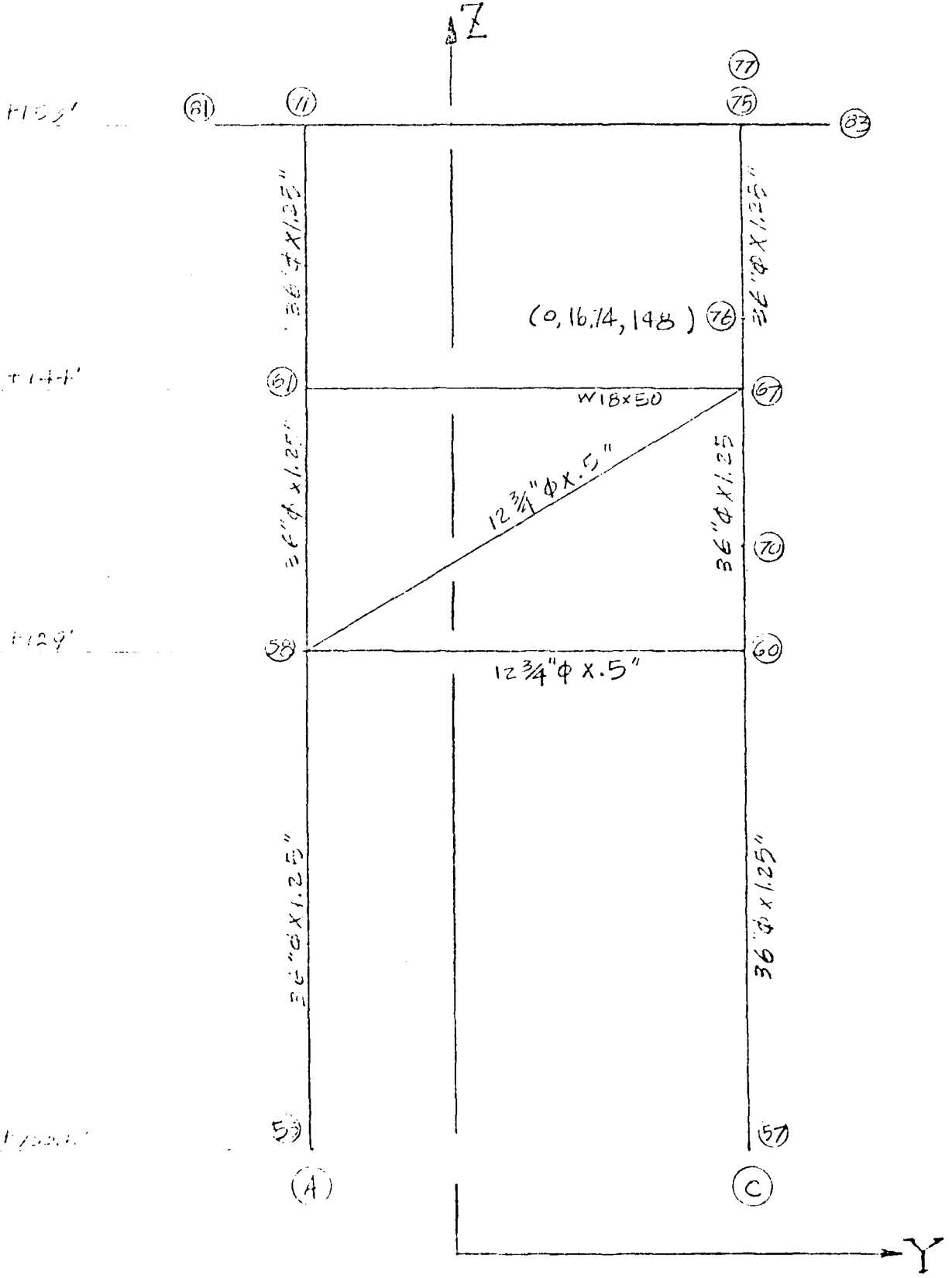
CREST OFFSHORE, INC.

Sheet 212 of 27

By C. C. [unclear] Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-2-76 Job No. 37-271-24 Calculation Structural Investigation



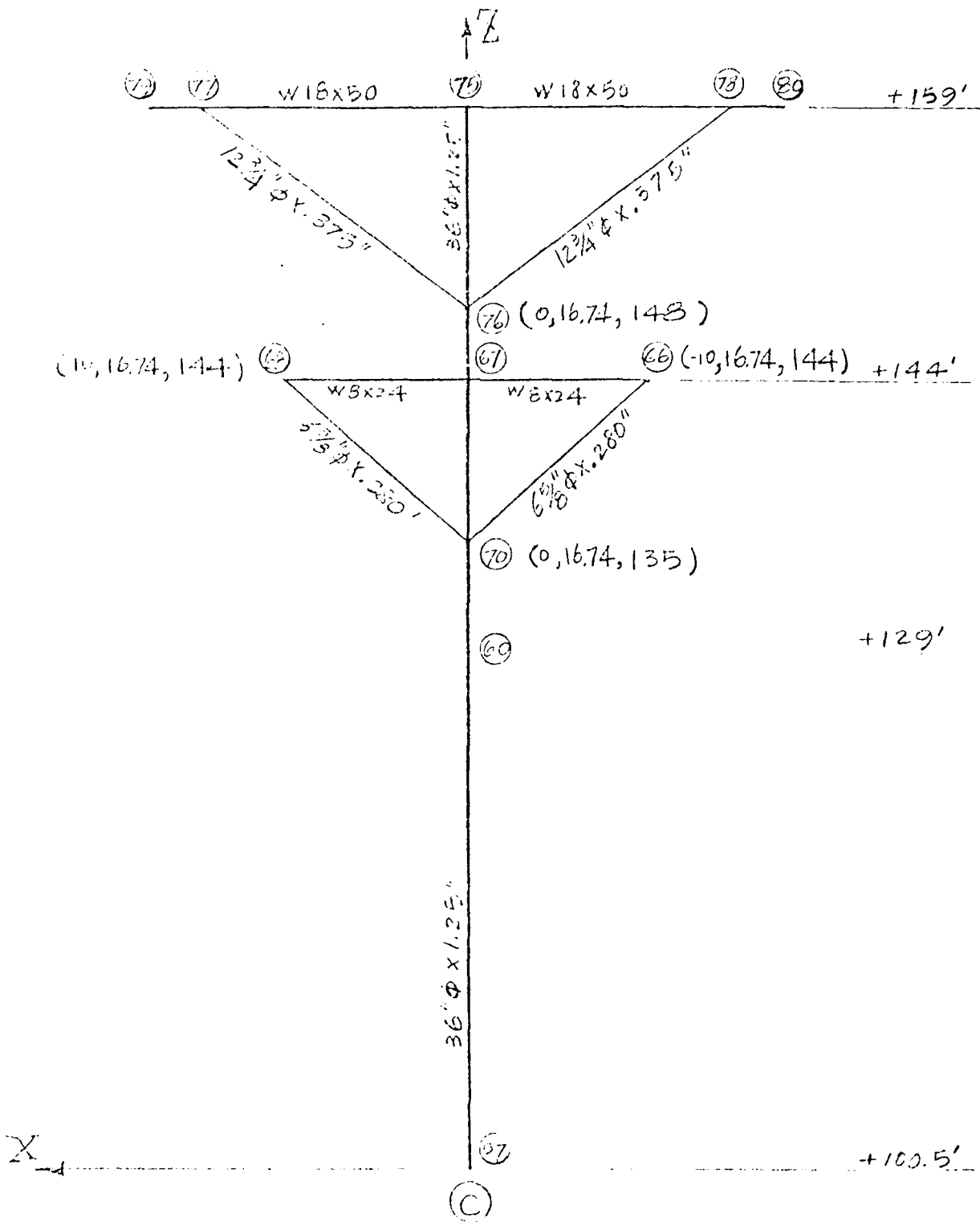
by C. Cherny Client U.S. Navy Subject Deck Structure Analysis
 Date 4-7-76 Job No. 27-57-11-12 Calculation Structural Design



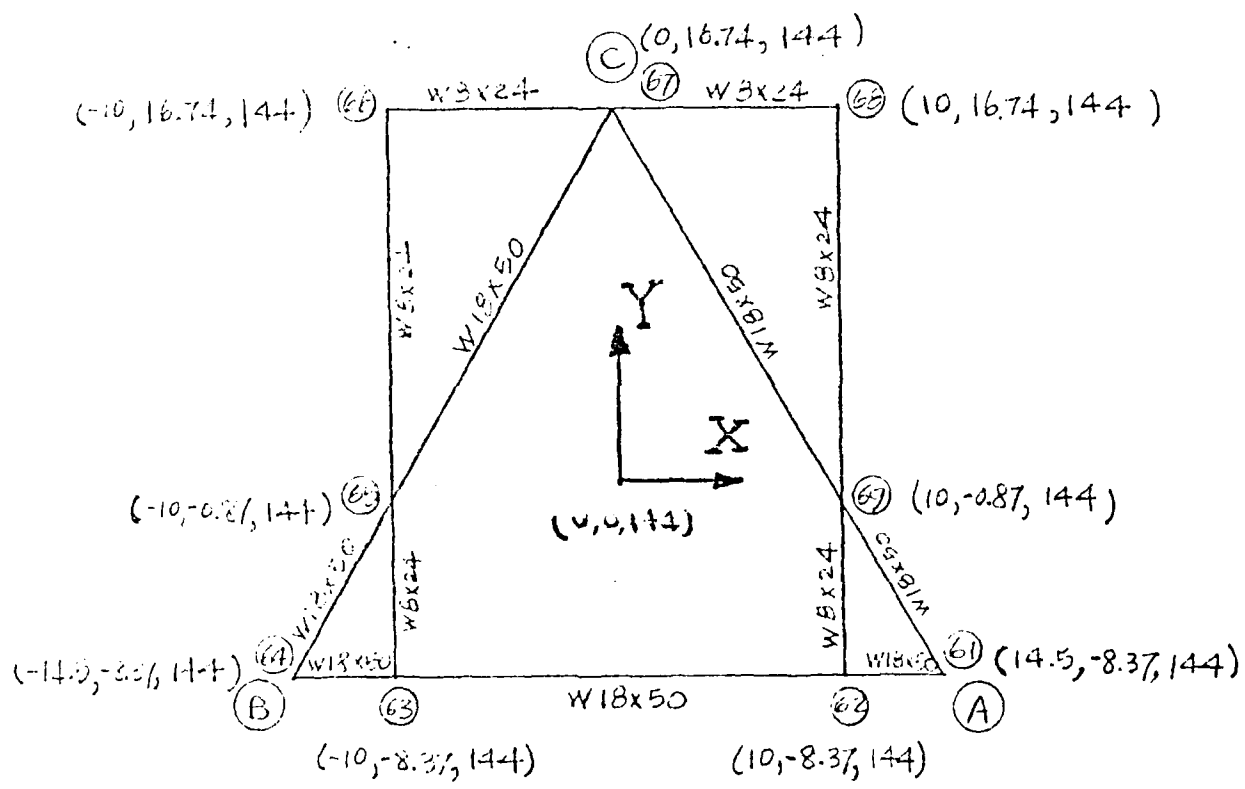
CREST OFFSHORE, INC.

Sheet 8.1 of 17

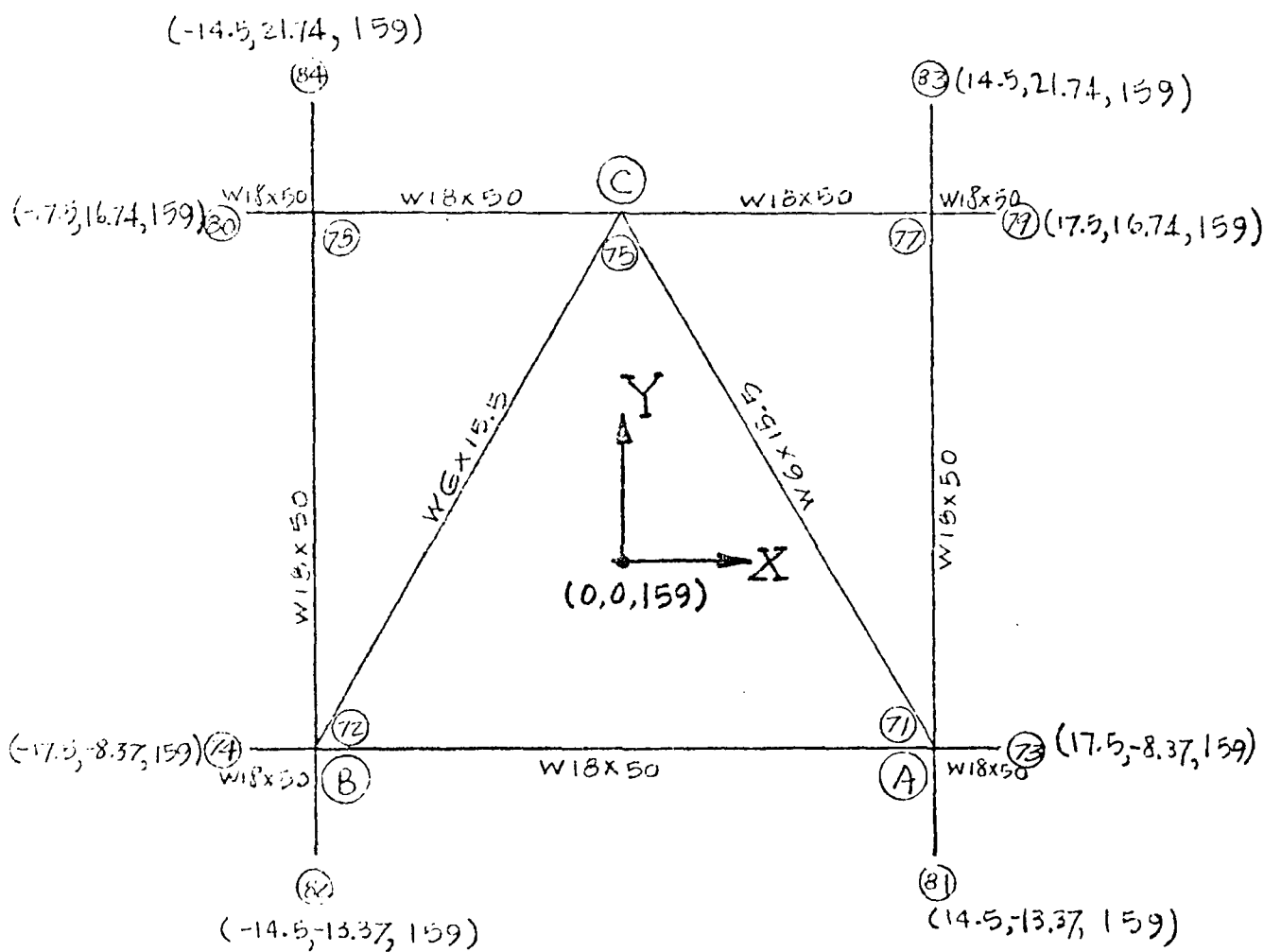
By C. Ch... Client U.S. NAVY Subject Structural Concept Analysis
Date 4-8-76 Job No. EZ-1771-32 Calculation Structural Identification



By C. C. Chen Client U.S. NAVY Subject Structural Concept Analysis
Date 4-2-76 Job No EZ-77192 Calculation Structural Idealization



By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
Date 4-3-76 Job No. 27-771-92 Calculation Structural Idealization



By C. Cherry Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-8-76 Job No. 27-77L-92 Calculation Structural Identification

Member Group Designation

- P10 = Pile group #1 36" ϕ x 1.75" WT
 P20 = Pile group #2 36" ϕ x 1.25" WT
 JL1 = Jacket Leg group #1 40" ϕ x .5" WT
 JL2 = Jacket Leg group #2 41" ϕ x 1.0" WT
 BR1 = Bracing 20" ϕ x .625"
 BR2 = Bracing 13" ϕ x .5"
 BR3 = Bracing 16" ϕ x .5"
 BR4 = Bracing 14" ϕ x .375"
 BR5 = Bracing 12 $\frac{3}{4}$ " ϕ x .5"
 BR6 = Bracing 12 $\frac{3}{4}$ " ϕ x .375"
 BR7 = Bracing 6 $\frac{5}{8}$ " ϕ x .280
 WBN = Fictitious wish-bone members 5" x 10" x 1" THK
 STL = Superstructure legs 36" ϕ x 1.25" WT
 W18 = W 18 x 50
 W10 = W 10 x 24
 W06 = W 6 x 15.5

SECTION 9
BASIC LOADING CONDITIONS

9.1 INTRODUCTION

The calculations establishing design loads are presented herein. These loads are comprised of gravity loads, buoyancy and storm forces.

By C. Ch... Client U.S. NAVY Subject Structural Concept Analysis of
Date 4-22-76 Job No. 27-721-24 Calculation Basic Loading Conditions

3.2 DEAD LOADS

The dead weight tabulated in this section was for the preliminary design only. No effort was made to update the weight due to subsequent modification on the structural components.

CREST OFFSHORE, INC.

Sheet 2.03 of 27

By S. CHASE Client U.S. NAVY
 Date 4-2-92 Job No. 27-771-92

Subject Structural Concept Analysis
 Calculation Basic Loading Conditions
 0

TACKET

MEMBER SIZE	MEMBER LENGTH	NO. REQUIRED	TOTAL LENGTH	UNIT WEIGHT	TOTAL WEIGHT
IN. X IN.	FT		FT	LB/FT	LBS
41" O.D. X 1" WT	6.0	3	18.0	427.2	7,689.6
	10.0	3	30.0		12,816.3
	18.0	3	54.0		23,069.3
	6.79	3	20.4		8,714.9
			122.4		52,290.1
40" O.D. X .5" WT	25.44	3	76.3	210.9	16,091.7
	23.44	3	70.3		14,826.3
	14.44	3	43.3		9,132.0
			189.9		40,050.0
24" O.D. X .75" WT	5.0	3	15.0	186.2	2,793.0
24" x 18" x .75" CONE		6		160.0	960.0
3" O.D. X .75" WT	3.0	3	15.0	138.2	2,073.0
18" O.D. X .5" WT	31.0	6	144.0	93.5	13,464.0
	40.2	6	241.2		22,552.2
	20.5	6	123.0		11,500.5
	54.5	3	163.5		15,287.3
					671.7

CREST OFFSHORE, INC.

Sheet 9.02 of 27

By C. C. [unclear] Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-12-76 Job No. 11-171-92 Calculation Basic Loading Conditions

MEMBER SIZE	MEMBER LENGTH	NO. REQUIRED	TOTAL LENGTH	UNIT WEIGHT	TOTAL WEIGHT
IN. X IN.	FT		FT	LBS/FT	LBS
14.0" O.D. X .375" WT	29.0	3	87.0	54.6	4,750.2
	27.4	3	73.2		3,996.7
			160.2		8,746.9
18 3/4" O.D. X .75" WT	5.0	3	15.0	96.1	1,441.5
2 1/2" O.D. X .5" WT	17.25	6	103.5	68.4	6,768.9
	12.5	3	37.5		2,452.5
			141.0		9,221.4
12 1/2" O.D. X .375" WT	19.7	3	59.1	49.6	2,931.4
20" O.D. X .625" WT	47.3	3	141.9	129.3	18,347.7
16" O.D. X .75" WT	5	3	15.0	122.2	1,833.0
18" O.D. X .75" WT	12.5	6	75.0	82.8	6,210.0
6 3/4" O.D. X .250" WT	10.0	3	30.0	19.0	570.0
	5.0	3	15.0		285.0
	2.5	3	7.5		142.5
			52.5		997.5
TOTAL					210,670#

By C. Cho Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-12-76 Job No. 22-22692 Calculation Bracing Conditions

SUPERSTRUCTURE

MEMBER SIZE	MEMBER LENGTH	NO. REQUIRED	TOTAL LENGTH	UNIT WEIGHT	TOTAL WEIGHT
	FT		FT	LBS/FT	LBS
6 3/8" D. X 1.125 WT	57.0	3	171.0	464.0	79,344.0
2 1/2" D. X .5 WT	26.0	3	78.0	65.4	3,101.2
	28.6	3	85.8		5,611.3
			163.8		10,712.5
2 1/2" D. X .375 WT	16.7	2	33.4	49.6	1,656.6
6 3/8" D. X .250 WT	11.2	2	22.4	18.0	423.6
W 13 X 50	26.0	3	78.0	50.0	3,900.0
	35.0	4	140.0		7,000.0
			218.0		10,920.0
W 12 X 27	35.0	4	140.0	27.0	3,780.0
W 8 X 24	25.0	2	50.0	24.0	1,200.0
	20.0	10	200.0		4,800.0
			250.0		6,000.0
C 12 X 7.5	35.0	4	140.0	25.0	3,500.0
	3.0	4	12.0		300.0
			152.0		3,800.0
W 6 X 13.5	25.0	2	50.0	16.9	806.0

CREST OFFSHORE, INC.

Sheet 7.6 of 27

by C. Chen Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-12-76 Job No 27-1771-92 Calculation Basic Loading Conditions

MEMBER SIZE	MEMBER LENGTH	NO. REQUIRED	TOTAL LENGTH	UNIT WEIGHT	TOTAL WEIGHT
	FT		FT	LBS/FT	LBS
4x3 F.B.	5.75	33	189.8	5.10	963.0
	5.83	22	128.3		694.3
	3.0	4	12.0		61.2
			330.1		1,683.5
1/2" x 1/2"	35x35	1	1,225.0 ²	10.2	12,495.0
	20x25	1	500.0		5,100.0
			1,725.0 ²		17,595.0
TOTAL					136,703.2 [#]

CREST OFFSHORE, INC.

Sheet 7.07 of 27

By C. Chen Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-18-76 Job No. 22-171-92 Calculation Pile Loading Conditions

PILINGS -- Measured To 5-D Below Mudline

MEMBER SIZE	MEMBER LENGTH	NO. REQUIRED	TOTAL LENGTH	UNIT WEIGHT	TOTAL WEIGHT
	FT		FT	LBS/FT	LBS
36" O.D. X 1.75" WT	47.65	3	142.95	552.7	79,008.5
36" O.D. X 1.25" WT	69.44	3	208.33	463.9	96,644.3
TOTAL					175,652.8

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Sheet 9.26 of 27

by C. Chern Client U.S. NAVY Subject Structural Concept Analysis
Date 4-13-76 Job No. 27-171-92 Calculation Basic Loading Conditions

SUMMARY

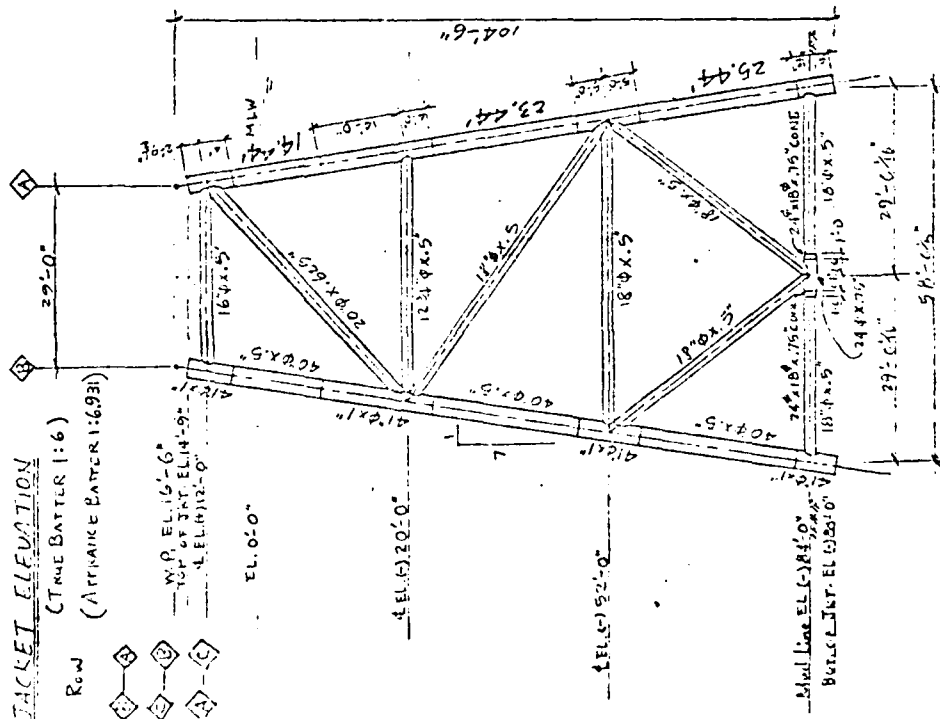
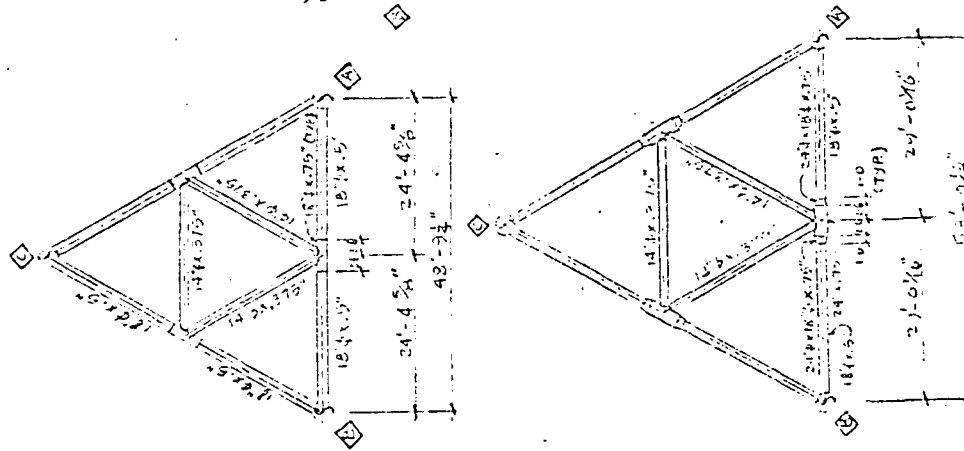
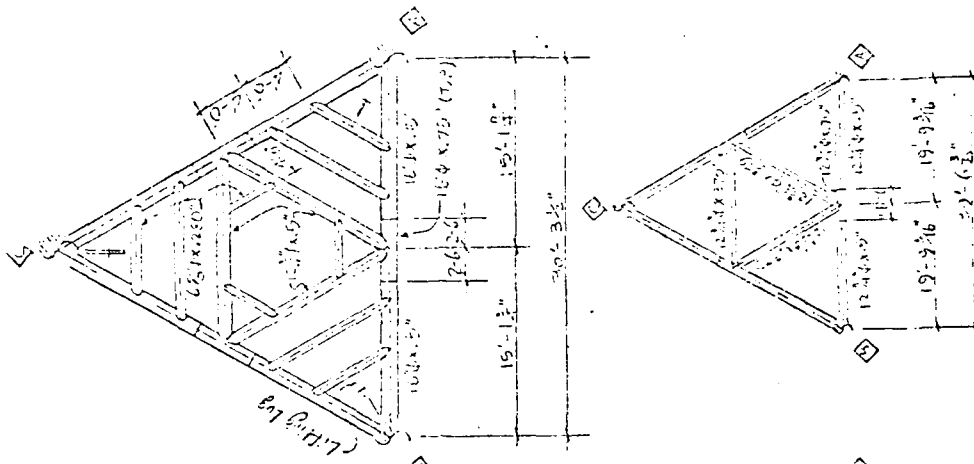
JACKET 210.7 KIPS

SUPERSTRUCTURE 136.7 KIPS
(EXCLUDING AUXILIARY
ATTACHMENT)

PILINGS 175.7 KIPS
(EXCLUDING PORTIONS
BEYOND 5-D BELOW
MUDLINE)

523.1 KIPS

By C. Chen Client U.S. Navy Subject Structural Concept Analysis
 Date 4-12-76 Job No. 27-771-22 Calculation Beam Loading Conditions



TACKET ELEVATION
 (TRUE BATTER 1:6)
 (ALTERNATE BATTER 1:6.93)

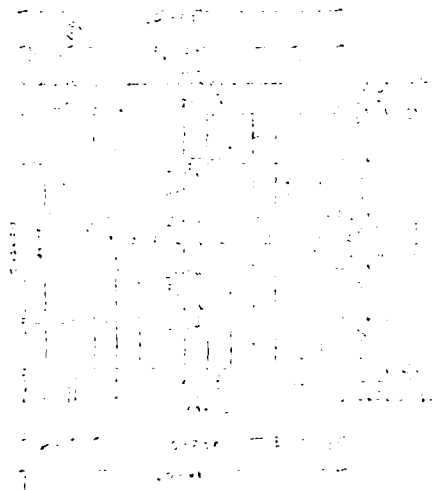
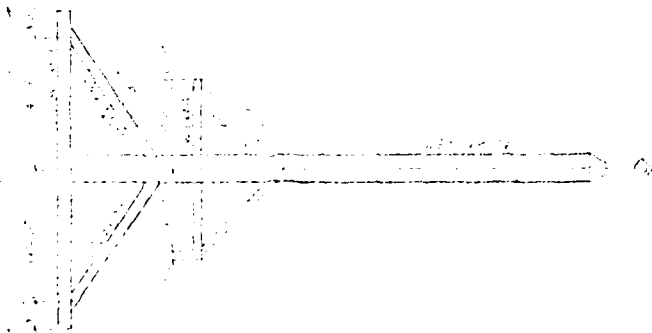
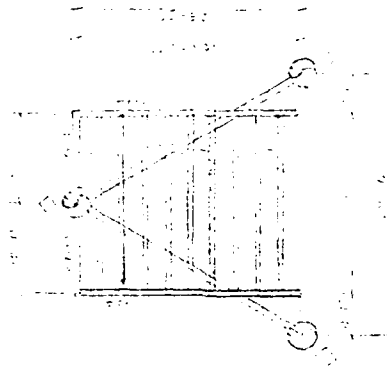
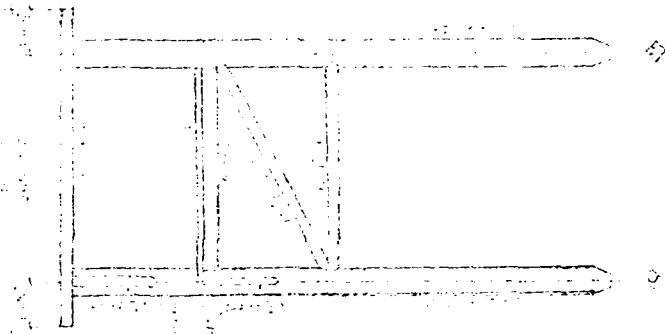
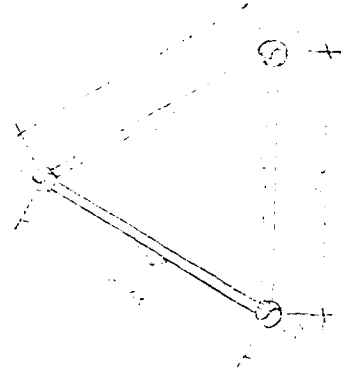
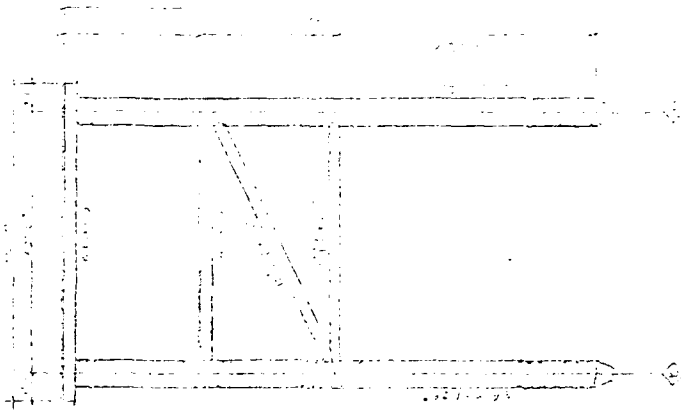
Row A B C
 D E F G H I J K L M N O P Q R S T U V W X Y Z

M.P. EL. 15'-0"
 TOP OF 3RD EL. 14'-9"
 1st EL. 14'-0"

CREST OFFSHORE, INC.

Sheet 9.10 of 27

By C. Johnson Client U.S. Navy Subject Structural Control Analysis
Date 4-11-76 Job No. 27-271-1A Calculation Basic Loadings



Dr. S. S. S. Client U.S. NAVY Subject Structure in Concept Analysis
Data 4-21-76 Job No. 27-774-1 Calculation Basic Loading Calculations

9.3 BUOYANCY

The buoyancy effect on the structure was tabulated in this section. These data were for early stage of preliminary design only. No effort was made to update the data due to subsequent modifications in member sizes.

The application of buoyancy to the space frame analysis will be directly from SEALOAD-2 program presented in SECTION 10, Space Frame Analysis.

CREST OFFSHORE, INC.

Sheet 012 of 27

By C. Chere Client U.S. Navy Subject Structure Control Analysis
Date 4-12-76 Job No 27-271-22 Calculation 5-2-76

Max. Crest Elevation = +142' above mean low

Member Size	Member Length	Unit Volume	Buoyancy $\gamma = 64 \frac{\text{lb}}{\text{cu ft}}$	Moment Arm (Dist. to CG)	Overturning Moment
IN. X IN.	FT	FT ³ /FT	LBS	FT	FT-LBS
40" O.D. X 1.5" WT	100.5	0.43	2,766	41.85	115,757
40" O.D. X 1.5" WT	100.5 X 2	0.43	5,532	4.19	23,179
36" O.D. X 1.5" WT	32.4	1.13	2,343	47.56	111,433
36" O.D. X 1.5" WT	32.4 X 2	1.13	4,686	2.67	12,512
36" O.D. X 2.5" WT	64.8	0.43	3,739	37.36	147,915
36" O.D. X 2.5" WT	64.8 X 2	0.43	7,478	5.33	42,064
24" O.D. X 2.5" WT	41.5	7.07	18,778	33.48	628,687
24" O.D. X 2.5" WT	41.5 X 2	7.07	37,556	8.37	314,344
24" O.D. X 1.5" WT	32.4 X 2	1.77	13,140	25.11	309,945
14" O.D. X 1.5" WT	29.0	1.07	1,936	25.11	49,868
14" O.D. X 1.5" WT	29.0 X 2	1.07	3,872	12.56	48,388
14" O.D. X 1.5" WT	40.2 X 2	1.07	11,012	25.11	276,511
14" O.D. X 1.5" WT	29.0 X 2	1.07	3,506	1.33	7,623
18" O.D. X 1.5" WT	43.7 X 2	1.77	11,045	20.98	262,650
18" O.D. X 1.5" WT	43.7 X 2	1.77	5,522	2.67	14,744

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Sheet 14 of 27

By: Client: U.S. NAVY Subject: Structure of Concrete Deck
 Date: Job No: Calculation: Basic Load Case

MEMBER SIZE	MEMBER LENGTH	UNIT VOLUME	BUOYANCY/ $\gamma = 64 \frac{\text{lbs}}{\text{cu ft}}$	MOMENT AREA	OVERTURNING MOMENT
IN. x IN.	FT	FT ³ /FT	LBS	FT	FT-LBS
16" O.D. x .375" WT	24.4	1.07	1,671	23.30	39,770
14" O.D. x .375" WT	24.4 x 2	1.07	3,342	13.24	44,248
18" O.D. x .5" WT	24.5 x 2	1.77	12,348	23.98	293,635
18" O.D. x .8" WT	54.5	1.77	6,174	4.0	24,696
12" O.D. x .5" WT	31.5 x 2	0.89	4,300	22.45	101,025
12" O.D. x .5" WT	29.5	0.89	2,260	5.53	11,993
12" O.D. x .375" WT	19.7	0.89	1,122	22.45	25,191
12" O.D. x .375" WT	19.7 x 2	0.89	2,244	13.89	31,169
20" O.D. x .625" WT	47.3 x 2	2.19	13,200	22.45	296,340
20" O.D. x .625" WT	47.3	2.19	6,600	7.91	52,206
16" O.D. x .5" WT	20.0	1.40	3,376	21.37	114,885
16" O.D. x .5" WT	20	1.40	2,639	8.38	22,525
12" O.D. x .5" WT	15	0.89	854	21.37	18,250
12" O.D. x .5" WT	15 x 2	0.89	1,708	14.28	25,415
12" O.D. x .5" WT	29 x 2	0.89	3,304	20.94	69,186
12" O.D. x .5" WT	27	0.89	1,652	8.33	13,761

CREST OFFSHORE, INC.

Sheet 214 of 27

By C. C. [unclear] Client U.S. [unclear] Subject Structural Concept Analysis
 Date 4-19-66 Job No. 27-721-92 Calculation Basic Loading Conditions

MEMBER SIZE	MEMBER LENGTH	UNIT VOLUME	BUOYANCY $\rho = 64 \frac{\text{LBS}}{\text{CU FT}}$	MOMENT ARM	OVERTURNING MOMENT
IN. x IN.	FT	FT ³ /FT	LBS	FT	FT-LBS
2 1/2" x 2 1/2" WT	28.55	0.89	1,632	8.75	13,676
2 1/2" x 2 1/2" WT	28.55 x 2	0.89	3,264	20.94	68,348
TOTAL			209,404 [#]		3,653,137

by C. P. Brown Client U. S. NAVY

Subject Structural Concept Analysis of

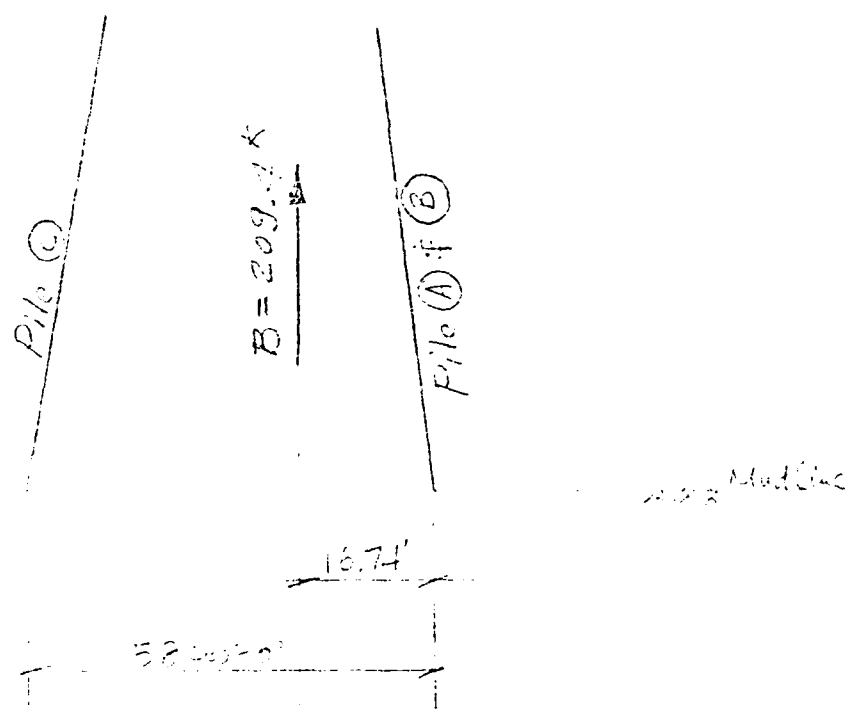
Job No. 27-07122

Calculation Basic Loads Co. 1972

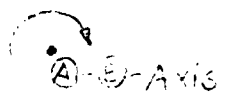
SUMMARY

BUOYANCY $B = 209.4 \text{ kips}$

OVERTURNING MOMENT ABOUT
A-E AXIS $M_B = 3,653 \text{ ft-kips}$



$3,653 \text{ ft-kips}$



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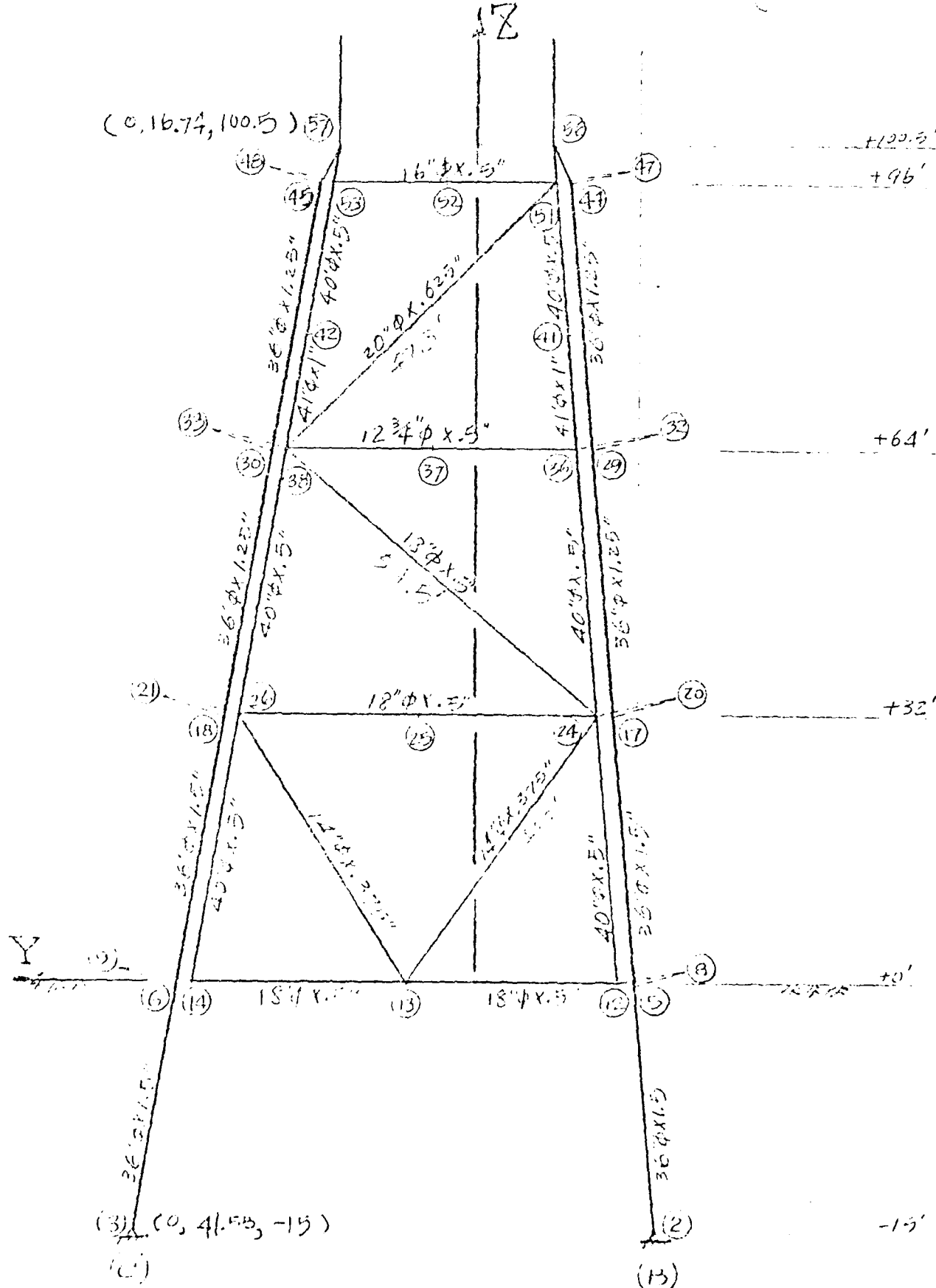
Sheet 21 of 27

By C. R. [unclear] Client U.S. NAVY

Subject Structural Concept Analysis of [unclear]

Date 4-2-72 Job No. 27-271-92

Calculation Build Loading Conditions



By P. R. / 100 Client U.S. NAVY Subject Structural Concept Analysis
Date 4-22-78 Job No. 27-771-12 Calculation Basic Loading Conditions

6-3 LIVE LOADS

The specified live loads for the structure are as follows:

- (1) 150 psf on equipment deck
- (2) 100 psf on top deck

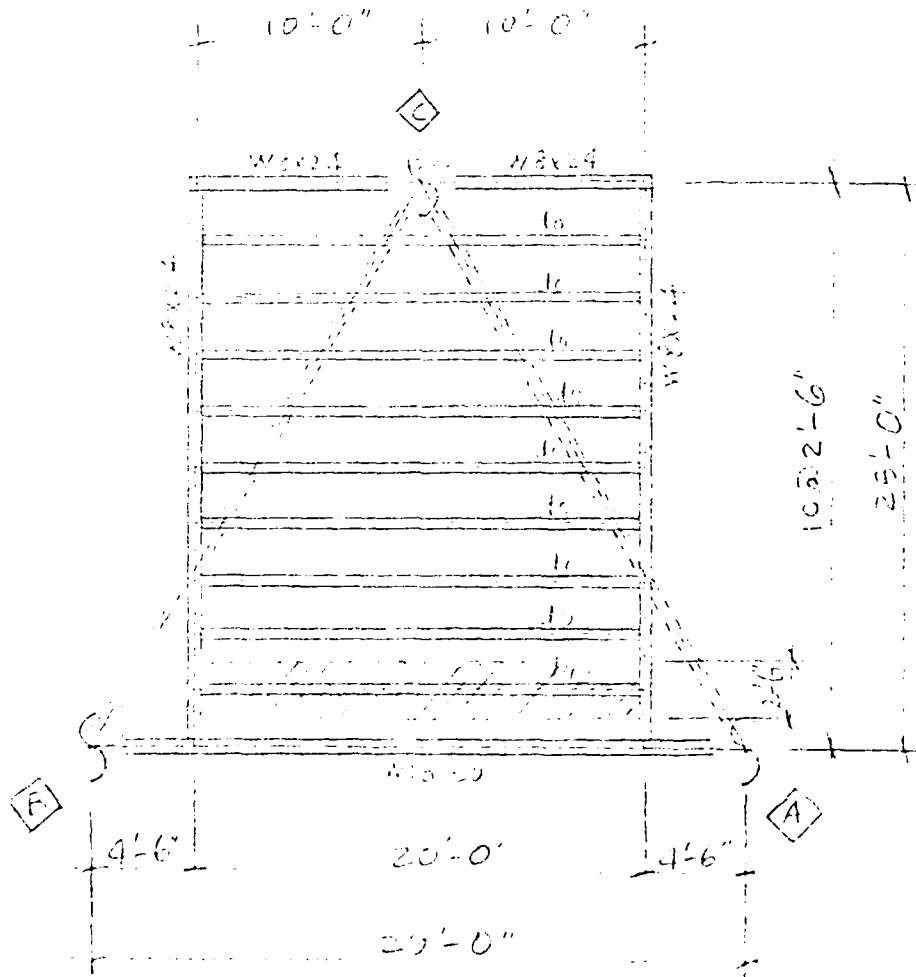
The live loads were used to check the size of deck beams and deck plate reinforcements.

By C. CREED Client U.S. NAVY Subject Structural Load Analysis
Date 4-2-76 Job No. 27-71-92 Calculation Equip. Loading Deck

LIVE LOADS ON EQUIPMENT DECK

DESIGN LOADS (GIVEN) = 150 PSF

SCALE $\frac{1}{8}'' = 1'-0''$



By C. Chere Client U.S. NAVY Subject Structural Concept Analysis
 Date 4-2-76 Job No. 27-771-92 Calculation Basic Loading Conditions

Check Beam W8x24

Span $(= 20'-0")$

Tributary Area $A = 2.5 \times 20 = 50 \text{ sq. ft.}$

Live Load $W_{LL} = 150 \times 50 = 7500 \#$

$\frac{1}{4} \text{\"} \text{ PL}$ $W_{DL1} = 10.2 \times 50 = 510 \#$

W8x24 $W_{DL2} = 24 \times 20 = 480 \#$

Total Weight = 8430 \#

$w = 424.5 \#/\text{ft}$

Max. Mom. $M = \frac{wL^2}{8} = \frac{424.5 \times 20^2 \times 12}{8} = 254.7 \text{\"} \text{K}$

$W_{8x24} \quad I_x = 20.8 \text{ in}^4$

Max. Stress $\sigma = \frac{254.7}{20.8} = 12.25 \text{ ksi} < 22 \text{ ksi}$

O.K.

* Note: Continuous sealed welds of $\frac{1}{4} \text{\"} \text{ plate}$ and the stiffeners/flange will provide sufficient lateral support to the composite flange against lateral buckling.

By C. Chan Client U.S. NAVY

Subject Structural Connect. Details

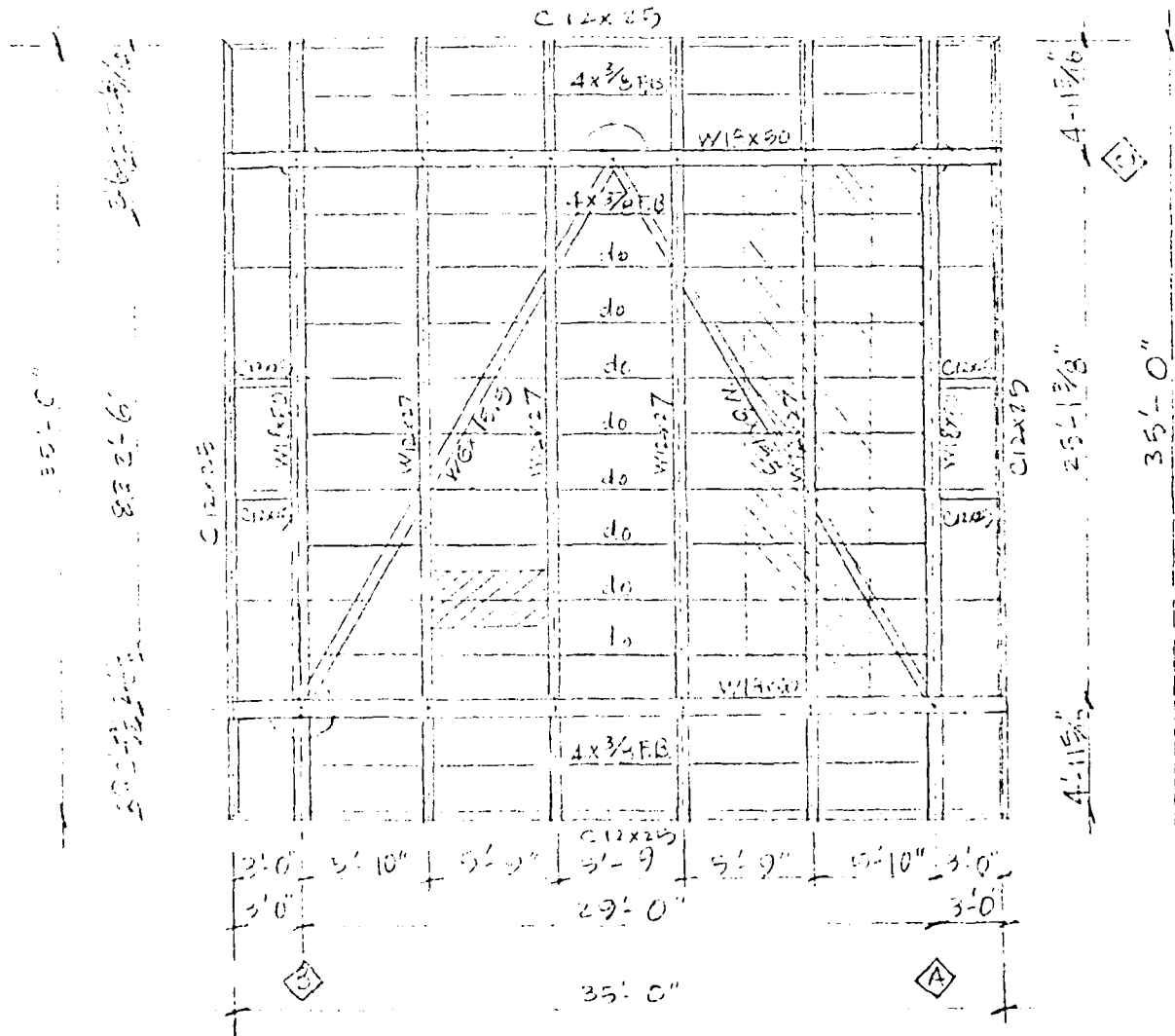
Date 4-2-66 Job No. 7-711

Calculation Basic Loading Conditions

LIVE LOADS ON TOP DECK

Decked Load (Uniform) = 100 PSF

SCALE $\frac{1}{8}'' = 1'-0''$



By J. Ch... Client U.S. NAVY Subject Structural Concept
 Date 4-9-76 Job No. 27-771-92 Calculation Beam Loading Conditions

Check Beam W12x27

span $l = 23' - 0"$
 Tributary Area $A = 6.75 \times 23 = 143.75 \text{ sq. ft.}$
 Live Load $W_{LL} = 10 \times 143.75 = 1437.5 \#$
 $\frac{1}{2} D$ $W_{DL1} = 10.25 \times 143.75 = 1473.75 \#$
 W12x27 $W_{DL2} = 27 \times 23 = 675 \#$
 Total $= 16 \times 16 \#$
 $w = 680 \#/ft$

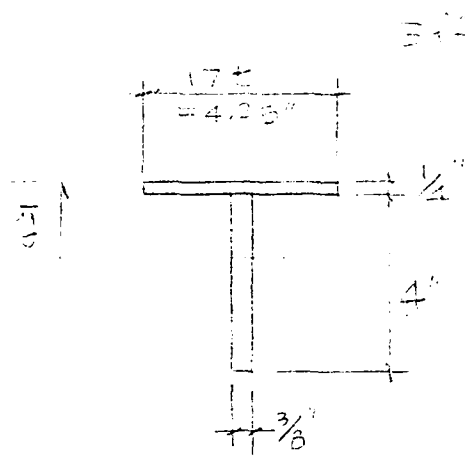
Max. Mom. $M = \frac{wl^2}{8} = \frac{0.68 \times 23^2 \times 12}{8} = 613.75 \text{ K}$

W12x27 $S_x = 4.2 \text{ in}^3$

Max. Stress $\sigma = \frac{613.75}{4.2} = 146 \text{ ksi} < 22 \text{ ksi}$
 O.K.

By C. Chrys Client U.S. NAVY Subject Structural Calculations
 Date 4-6-52 Job No. 3335-72 Calculation Basic Loading Conditions

Check 4x3/8 Flat Bars



Effective width $b = 17 \times 0.7 \times \frac{1}{4} = 4.25"$

Span $(= 3')$

Tributary Area = $5.75 \times 2.5 = 14.4'$

Live Load $W_{LL} = 50 \times 14.4 = 1440'$

1/4" PL $W_{DL1} = 10.2 \times 14.4 = 147'$

4x3/8" F.B. $W_{DL2} = 5.10 \times 3.75 = 27'$

Total 1616'

$W = 281 \# / \text{ft}$

Max. Mom. $M = \frac{281 \times 5.75^2 \times 0.125}{8} = 13.9 \text{ "K}$

$\bar{y} = \frac{.25 \times 4.25 \times 1.25 + .375 \times 4 \times 2.25}{.25 \times 4.25 + .375 \times 4} = \frac{3.51}{2.70} = 1.3"$

$I = \frac{1}{12} \times \frac{1}{4} \times 4.25^3 + \frac{3}{8} \times 4 \times (2 - 1.25)^2 + 4.25 \times \frac{1}{4} \times (1.3 - 0.125)^2$
 $= 2 + 1.334 + 1.467$
 $= 4.821 \text{ in}^4$

$S = \frac{4.821}{4 - (1.3 - .25)} = 1.63 \text{ in}^3$

Max. tensile stress $\frac{M}{S} = \frac{13.9}{1.634} = 8.51 \text{ ksi} < 22 \text{ ksi}$
 O.K.

By C. S. Lane Client U.S. NAVY Subject Struct. of Concept Aircraft
Date 4-27-71 Job No 27-771-34 Calculation Basic Loading Conditions

9.3 WIND LOADS

Set forth herein is the basic wind load data for the input into SEALOAD-2 computer program. The computer program printout is presented in A-4 Wave and Wind Loads of APPENDIX A.

AD-A164 421

STRUCTURAL CONCEPT ANALYSIS REPORT FOR THE EAST COAST
AIR COMBAT MANEUVER. (U) CREST ENGINEERING INC TULSA OK
MAY 76 27-771-92-APP-C CHES/NAVFAC-FPO-7601-APP-C

3/7

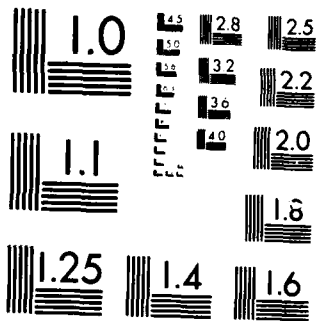
UNCLASSIFIED

N62477-76-C-0179

F/G 13/13

NL

The table consists of 13 columns and 10 rows. The top row contains 13 blacked-out cells. The remaining 9 rows each contain 13 blacked-out cells. The grid is used for data entry or analysis, but the content is obscured by blacking out.



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

By: C. J. [unclear] Date: 11/14/74 Subject: Structural Connections
 Date: 4-2-76 Job No: 27-771-92 Calculation: Basic Loading Connections

* Ref: Notes from Steve Pitzer, 12-14-74

WIND FORCES

$$F = 0.00256 C_s A C_H V^2$$

F = force in lbs.

V = velocity @ 30 ft elev. = 150 knots = 173 mph

$C_s = 1.5$ for flat surfaces

$= 1.0$ for cyl. surfaces

A = projected area of surface (sq ft)

$C_H =$ height coeff = $(H/30)^{2.7}$

Calculate psf wind force on flat surfaces:

$$F/A @ 30 \text{ ft elev} = (0.00256)(1.5)(1)(173)^2 = 115 \text{ psf}$$

$$F/A @ 75 \text{ ft elev} = (115)\left(\frac{75}{30}\right)^{2.7} = 115(1.3) = 150 \text{ psf}$$

For cylindrical members.

$$F/A @ 30 \text{ ft} = 77 \text{ psf}$$

$$F/A @ 75 \text{ ft} = 100 \text{ psf}$$

{ Elev referenced
to MLW }

by George J. ... Client Shell ... Subject Struct. of ...
 Date ... Job No. ... Calculation ...

Wind Force Area Calc:

- 1. Wind pressure = 150 psf (Flat)
- 100 psf (cylindrical)

2. Assume:

- A. Projected Area Above top deck due to fence is 45' x 2' h.
- B. Area from top of top deck to bottom of lower deck is solid plate

Calculations

$$F_{\text{top deck}} = 45 \times 2 \times 150 = 13.5^k$$

$$F_{\text{between decks}} = 33.5 \times 33.5 \times .15 = 55.7$$

Stairways & Landings =

Landings: (12' x 2' x .15)	=	4.8
Stays: (21' x 2' x .15)	=	6.3
Antennas		2.0
		82.3 ^k

27 wind is at 45° to structure axis

Wind Force on each FACE:

Top Deck = (.707)(13.5) = 9.55^k

Lower Deck = (.707)(82.3 - 13.5) = 48.8^k

By C. C. Berry Client Shell Subject Structural Plan - Bridge
 Date 7-2-76 Job No. 27-221-2 Calculation EMC Loading Studies

Wind Area & Area Vertical Centroid Location

Segment #1

Projected Area of top deck and face

$$A_1 = 45 \times 2 = 90 \text{ sq. FT}$$

(width) x (height)

$$\text{Centroid from mid-line} = 15.9 \text{ ft}$$

Segment #2

$\frac{2}{3}$ Area below top of air and equipment deck
 is a solid plate

$$A_2 = \frac{2}{3}(29 \times 15) = 290 \text{ sq. FT}$$

$$\text{Centroid from mid-line} = 17.5 - 10 = 7.5 \text{ ft}$$

Client: Shell International Subject: Design of Platform A-100
Date: 11/1/77 Job No. 27-271-1 Calculation: Design Wave Conditions

3-6 WAVE LOADS

Wave loads on the structure are generated through the SEALOCC-2 computer program. Detailed report format are presented in A-4 class of Wave Loads in APPENDIX A.

Design wave characteristics was presented in Sec. 1-2, Design Criteria.

SECTION 10
SPACE FRAME ANALYSIS

10.1 INTRODUCTION

The three-pile structure in this section has satisfied the preliminary design procedures described previously (from SECTION 2 to SECTION 9). The main objective of the space frame analysis is to confirm the integrity of the proposed structure subjected to specified environmental conditions.

The space frame analysis set forth herein utilizes the available computer programs available at Synercom Technology, Inc., Houston, Texas. The program processing procedures are as follows:

- (1) Set up SEALOAD-2 program to obtain desired wind, wave and dead weight (including buoyancy effect) loadings on the structural components.
- (2) Update loadings in Step (1) due to additional dead weight and live loads on the structure.
- (3) Perform space frame analysis by using STRAN computer program.

The program printouts are presented in A.5 Space Frame Analysis in APPENDIX A.

By: C. P. H. Client: U.S. Navy Project: Structural Concept Analysis
 Date: 12/12/01 Job No.: 02-001-12 Calculation: Splice Force Analysis

10.2 INPUT DATA

1. SEA-DAL Program will calculate wind and wave load on structure adjusted by the buoyancy effect.
- *2. Addition of wind and wave forces due to boat landings and stairways --- input as joint loads
- *3. Additional dry weight of the superstructure:
 - a. Secondary deck beams (joists)
 - b. Floor plates
 - c. Handrails, bulkheads, safety nets, etc.
 --- input as joint loads
- *4. Live loads on top deck and equip. on decks

LOADING SCHEMES DESIGNATIONS :

LOADING 1 WIND AND WAVE (90° APPROX. from +X-AXIS)
 (JACKET & SUPERSTRUCTURE)

LOADING 2 WIND AND WAVE (270° APPROX. from +X-AXIS)
 (JACKET & SUPERSTRUCTURE)

LOADING 3 DEAD LOADS (Dry Weight + Buoyancy)

*LOADING 4 ADDITIONAL WIND AND WAVE (Boat Landings, Stairs)
 + Y-axis

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Sheet 12 of 21

CV Client U.S. Gulf Subject Structural Element Analysis
Date 4-1-76 Job No. 57-1-9 Calculation Frame Analysis

** Load 5 Addition - Dead Loads (see drawing)

** Load 6 Live Loads

Load 7 Combined Load $(= (2-4) + (3-5))$ Max. Tensile

Load 8 Combined Load $(= (1+4) + (3-5) + 6)$
Max. Compression

By S. C. ... Client ... Subject Structural Concept Design
 Date 1/16 Job No. ET-771-92 Calculation Space Frame Analysis

Load No. 4 Additional Wind and Wave From E. - Landing Stairs

(1) East Landing Moment at Mullion = 4.206 FT-KIPS
 Shear = 43.4 KIPS

Equivalent Conc. Loads at

$$L_e = \frac{4.206}{43.4} = 86.9 \text{ FT from mullion}$$

Equally distributed at

Mullion (4) - (5) $l = 76 - 73 = 13'$
 (6) - (7) $l_p = 86.9 - 73 = 8.9'$

(2) Stairways Moment at Mullion = 10.123 FT-KIPS
 Shear = 31.2 KIPS

Equivalent Conc. Loads at

$$L_e = \frac{10.123}{31.2} = 124.7 \text{ FT from mullion}$$

Equally distributed at

Mullion (3) - (5) $l = 123 - 100.5 = 22.5'$
 (5) - (7) $l_p = 124.7 - 100.5 = 24.2'$

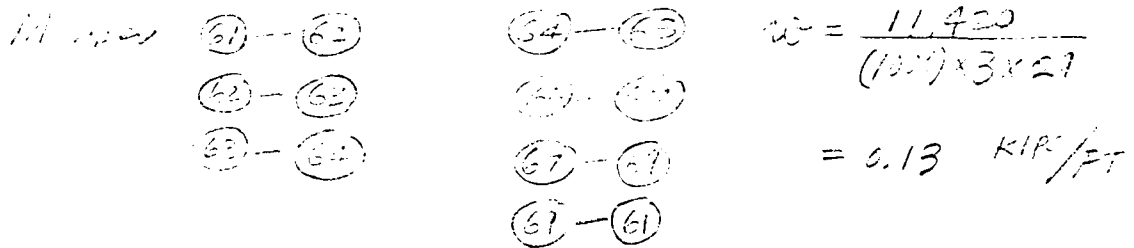
By [Signature] Client U.S. Navy Subject Structure, Support Analysis
 Date 4-1-86 Job No. 31-111-12 Calculation Spine Deck Loads

Load on S Horizontal Deck Loads

Equipment Deck:

4" x 4"	5,100 #
4" x 4"	4,520 #
Horizontal Deck Structure	<u>2,000 #</u>
	11,420 #

Uniformly distributed on Beams



TOP DECK:

1/4" x 12"	12,495 #
4' x 3' x 3" F.R.	1,684 #
W14 x 27	3,730 #
C12 x 25	<u>3,800 #</u>
	21,795 #
Safety Nets	<u>2,000 #</u>
	23,795 #

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Sheet 10 of 17

By C. C. [unclear] Client [unclear] Subject: Structural Cont. of [unclear]
Date 4-21-82 Job No. 82-271-92 Calculation: [unclear]

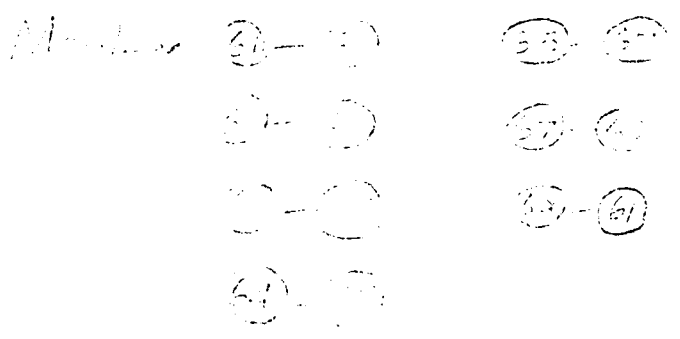
Equally distributed at 3 leg tips: 7.93 kips

LOADING & LIVE LOADS

Deck Deck: 150 PSF

Total Live Load = $150 \times 20 \times 3 = 75000 \#$

Uniformly distributed on Beams



$$w = \frac{75000}{100 \times 3 \times 3}$$

$$= 0.86 \text{ KIPS/FT}$$

Top Deck: 100 PSF

Total Live Load = $100 \times 33 \times 33 = 122,300 \#$

Equally distributed at 3 leg tips: 40.53 kips

By [Signature] Client Ullrich Drawn Structural Concept Engineers
Date 2/27/74 Job No. 27-2-1174 Calculation Spine Frame Analysis

Revised Coordinates for Points 1, 2 & 3

Point ① $x = 11.3 + \frac{1.85}{6} \cos 30^\circ = 22.37$

$y = -8.17 - \frac{1.85}{6} \sin 30^\circ = -17.25$

$z = -6.00$

Point ② $x = 22.47$

$y = -17.25$

$z = -6.00$

Point ③ $x = 0$

$y = 16.74 + \frac{10.65}{6} = 34.44$

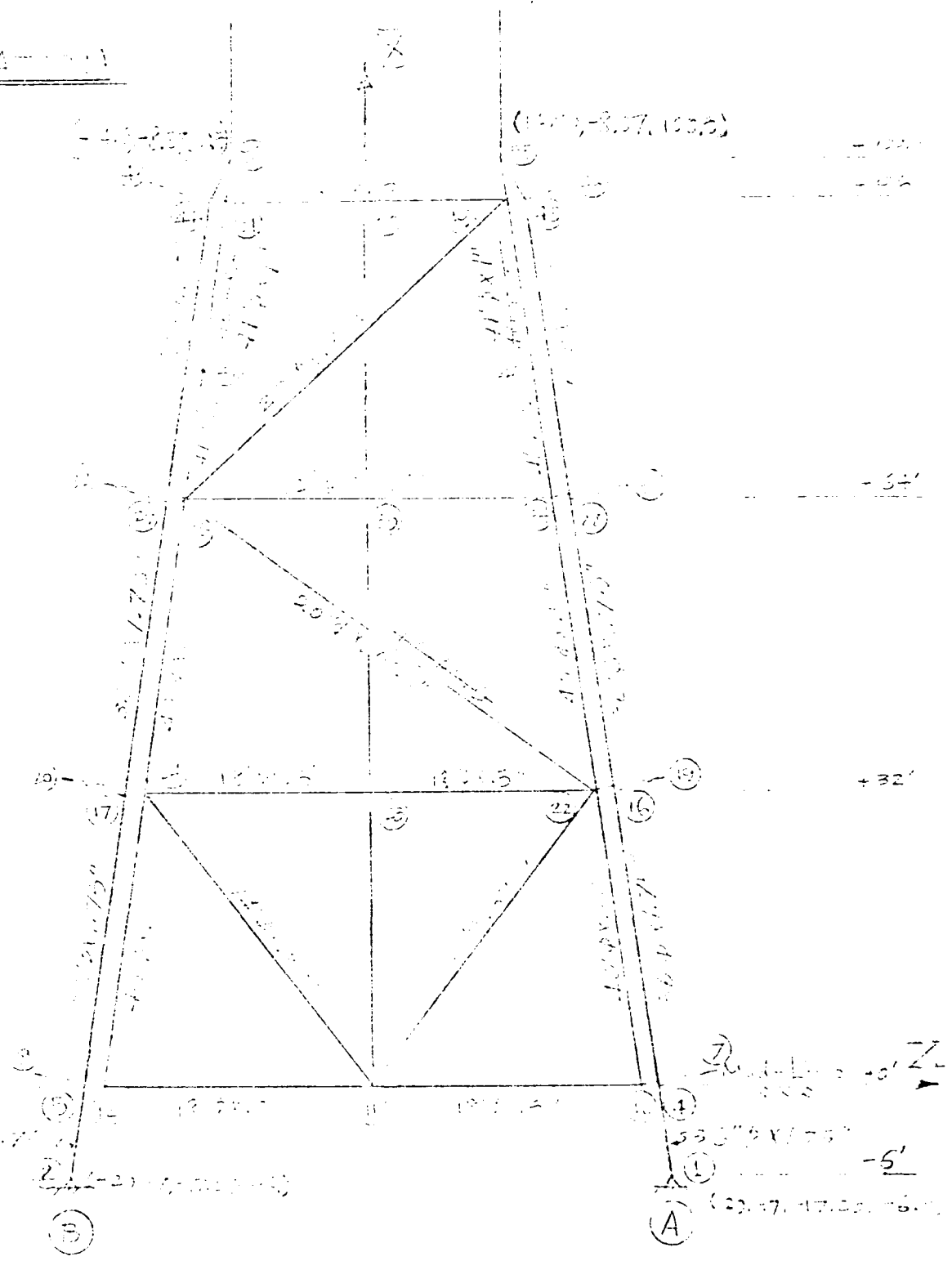
$z = -6.00$

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Scale 1/4" = 100'

Client U.S. Navy Date 10/1/58
 Calculation Area of Polygon

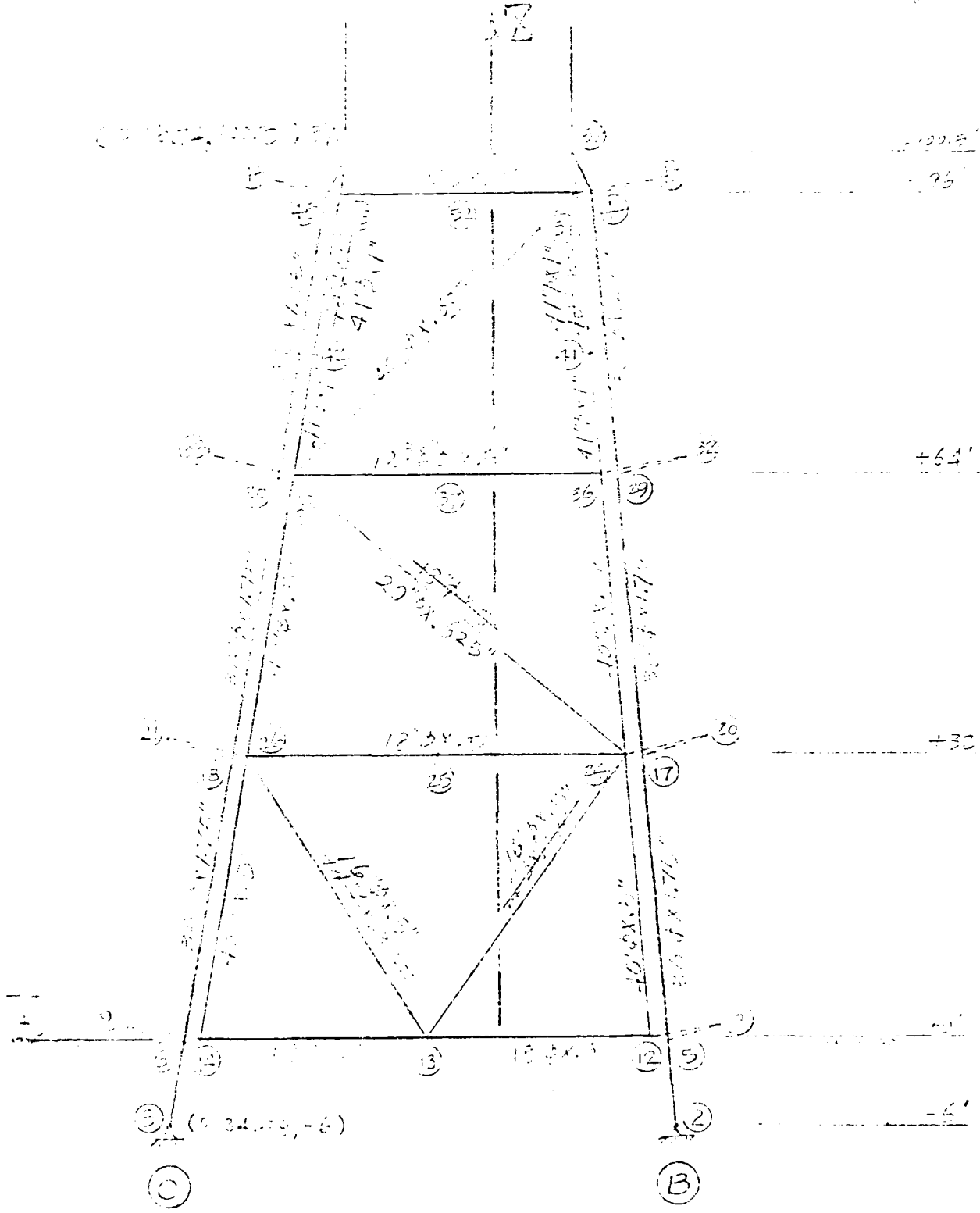
Area of Polygon



Area of Polygon = 10,000 sq. ft.
 Area of Triangle = 1,000 sq. ft.
 Area of Triangle = 1,000 sq. ft.
 Area of Triangle = 1,000 sq. ft.
 Area of Triangle = 1,000 sq. ft.

Client: Shell
Date: 4/26/72 Job No: 27-771-12

Project: Structural Concept Analysis
Calculation: Space Frame Analysis



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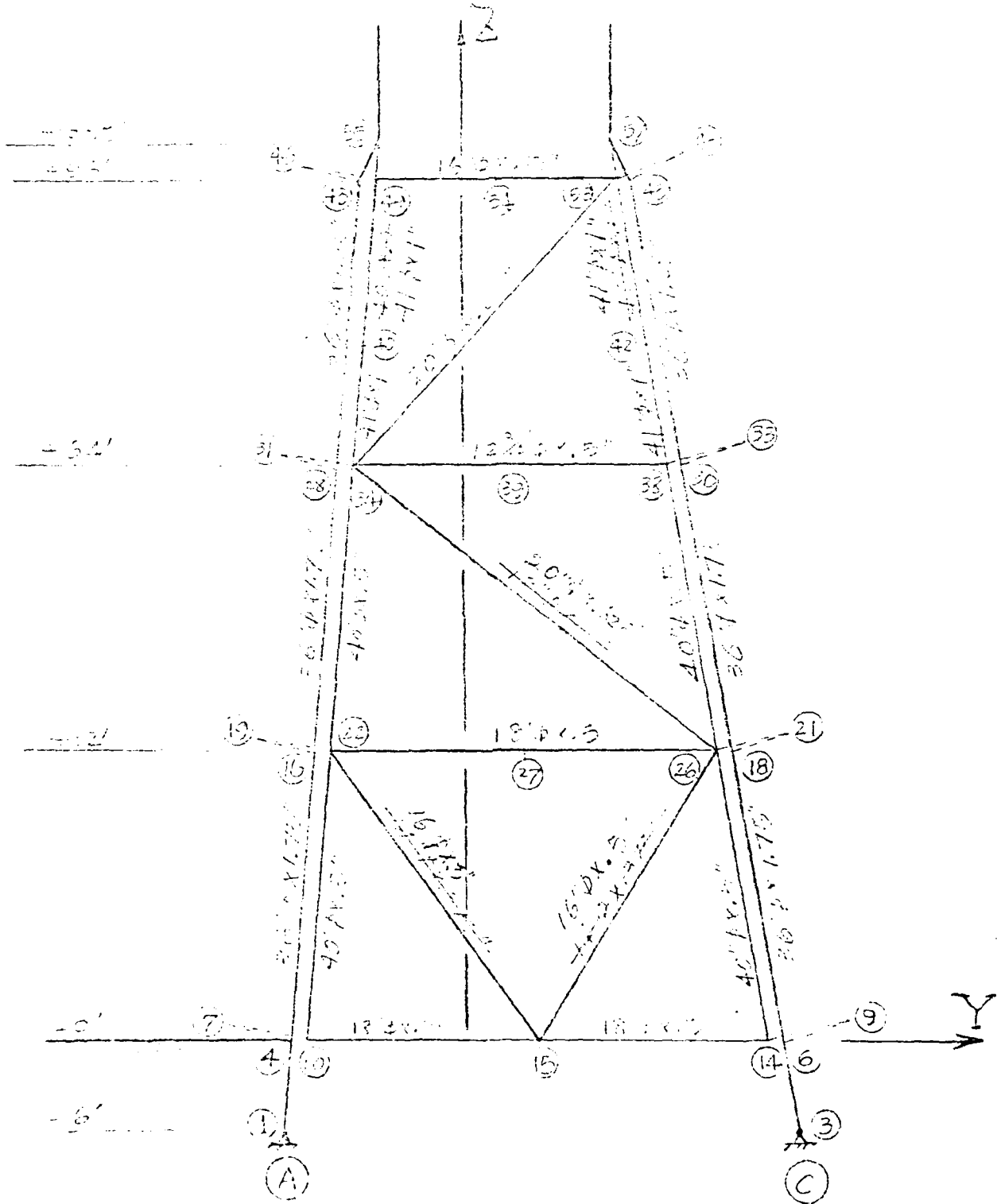
Sheet 1 of 2

By S. Green Civil U.S. NAVY

Station Station 2 Concept Analysis

Date 4-1-76 Job No. 27-724-9B

Calculation Spine Frame Analysis



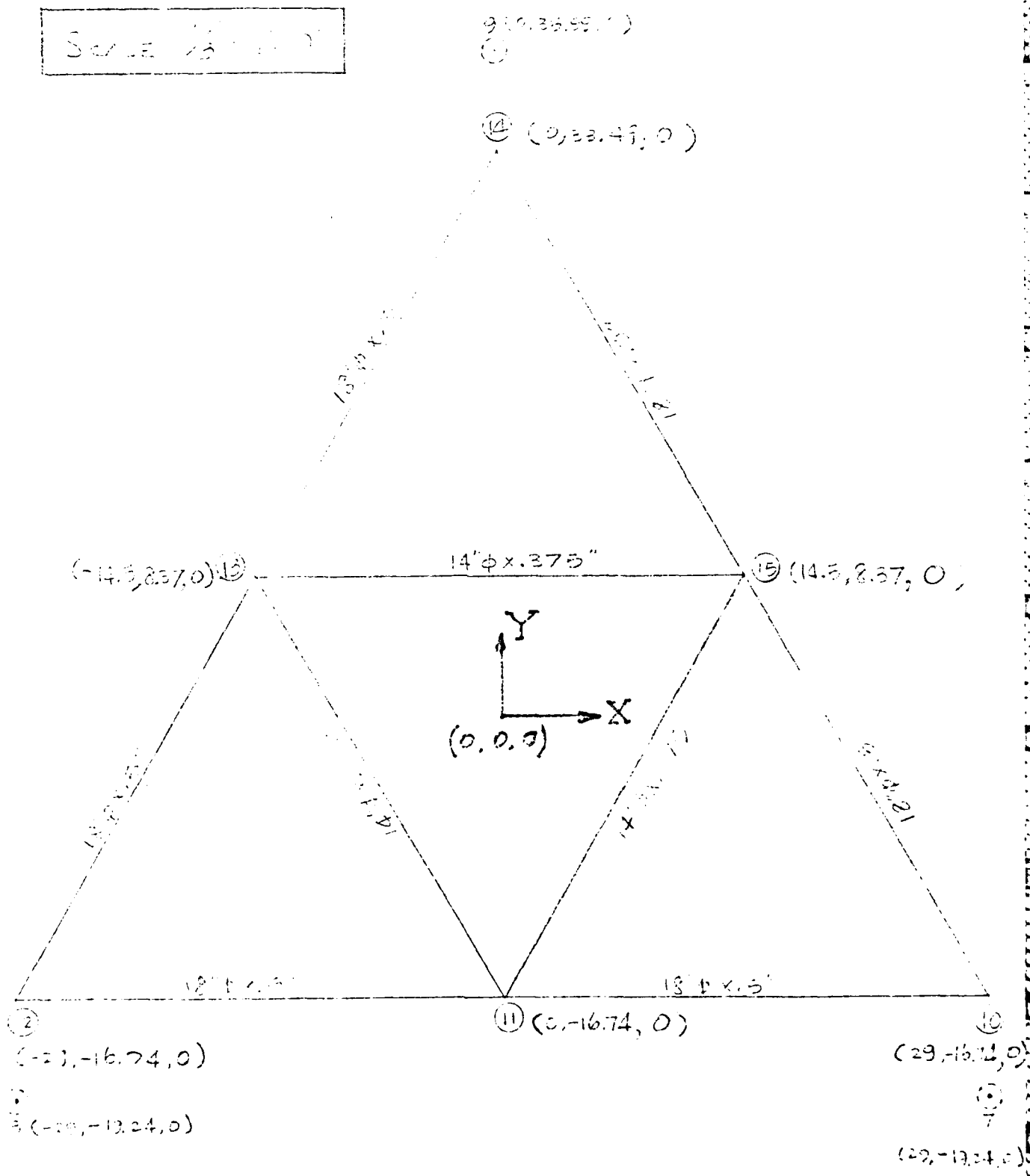
By Client U. I. B. I. Subject Structural Concept Design
 Date 3-26-72 Job No. 27-726-92 Calculation Span Frame Analysis

PLAN

SCALE $\frac{1}{8}'' = 1'-0''$

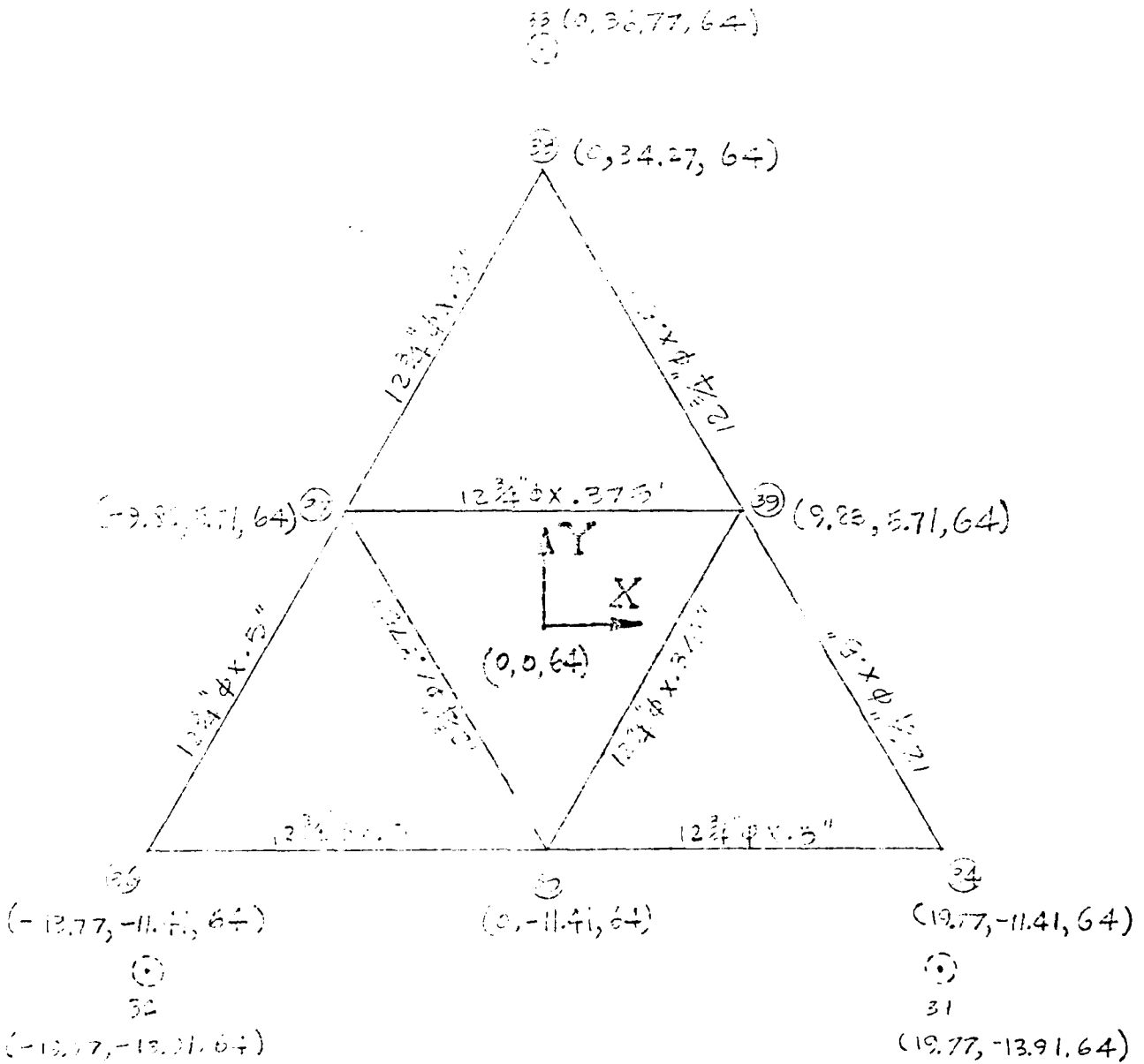
9 (0, 33.99, 0)
 ⑩

⑭ (0, 33.49, 0)

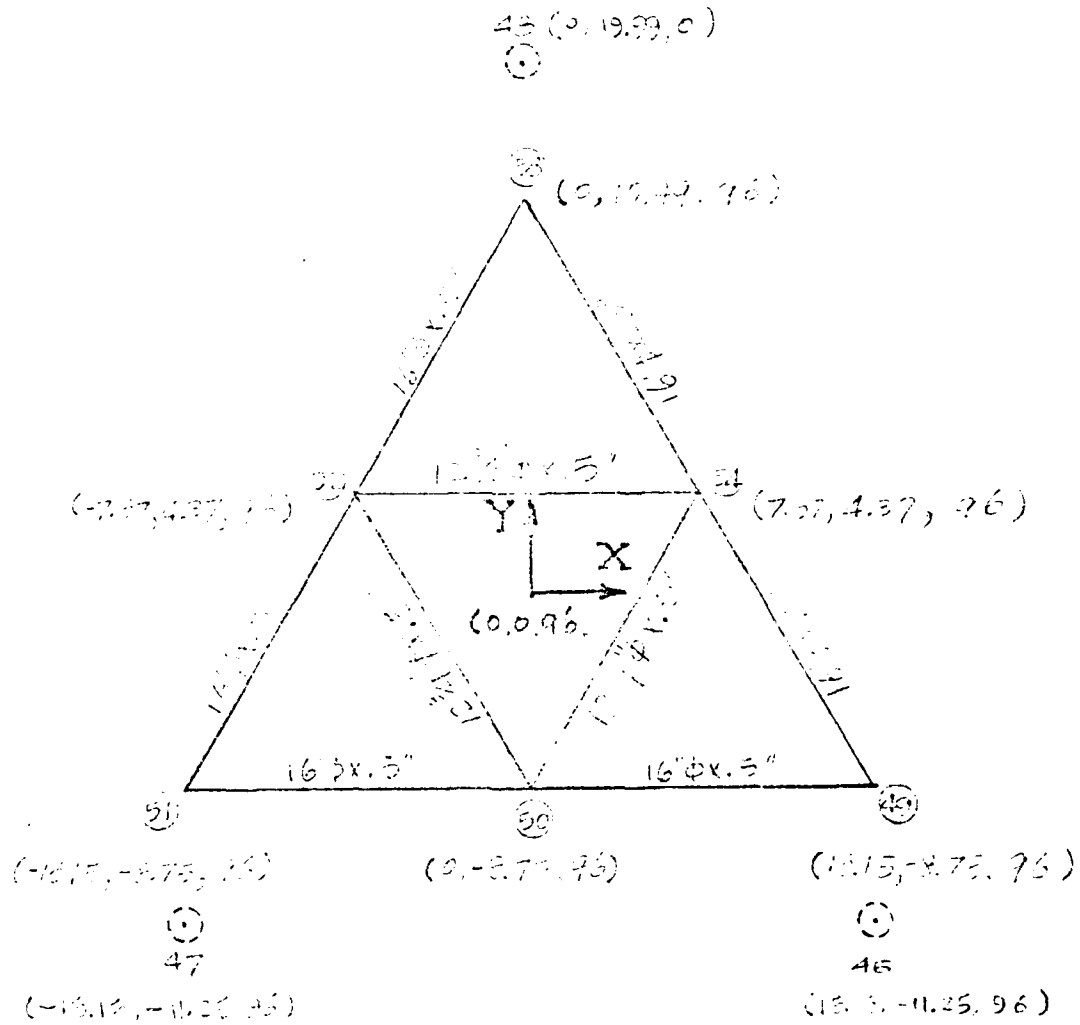


by C. J. [unclear] Date 4-25-76

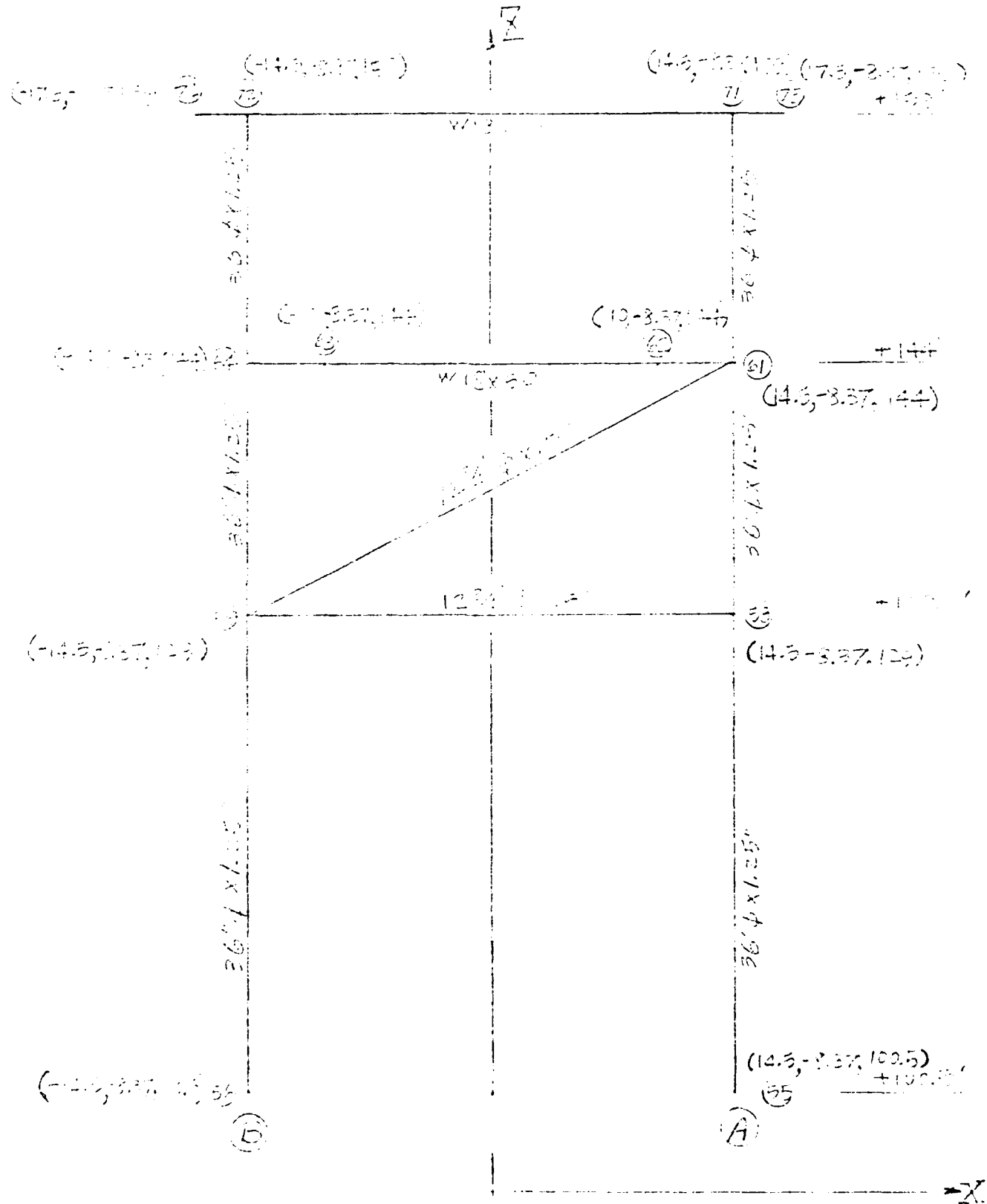
Subject Structural Concept Analysis
Calculation Space Frame Analysis



By C. Ch... Client ... Subject Structure of Concrete
 Date 4-26-73 Job No. ... Calculation Splice Forces



Client U.S. NAVY Subject Structural Concept Analysis
 Date 1-7-92 Job No. 27-10-92 Calculation Space Frame Analysis

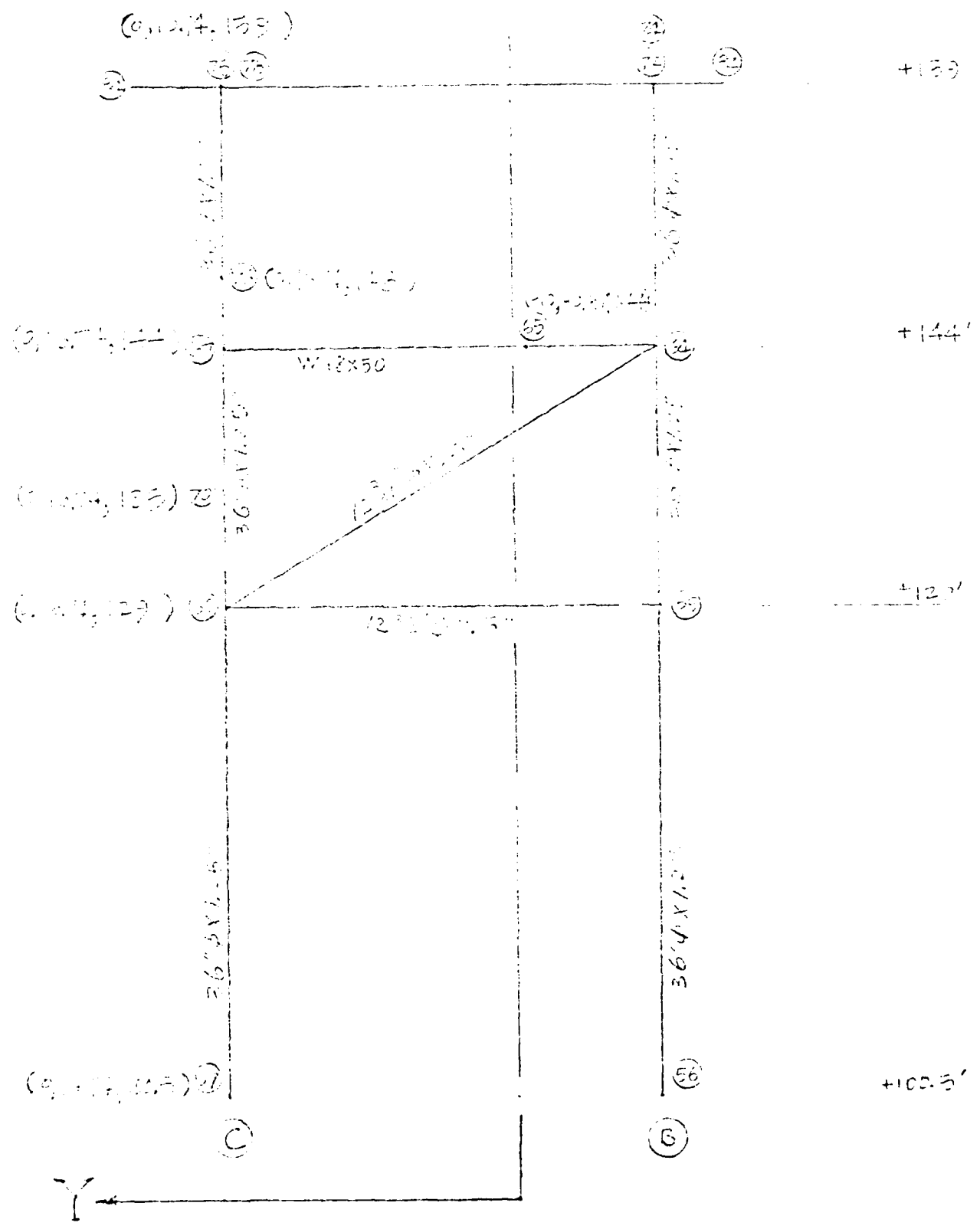


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Sheet 20.12 of 22

By C. J. [unclear] Client U.S. Navy Subject Structural Concept Analysis
Date 4-12-78 Job No 27-771-72 Calculation See Frame Diagram

AZ



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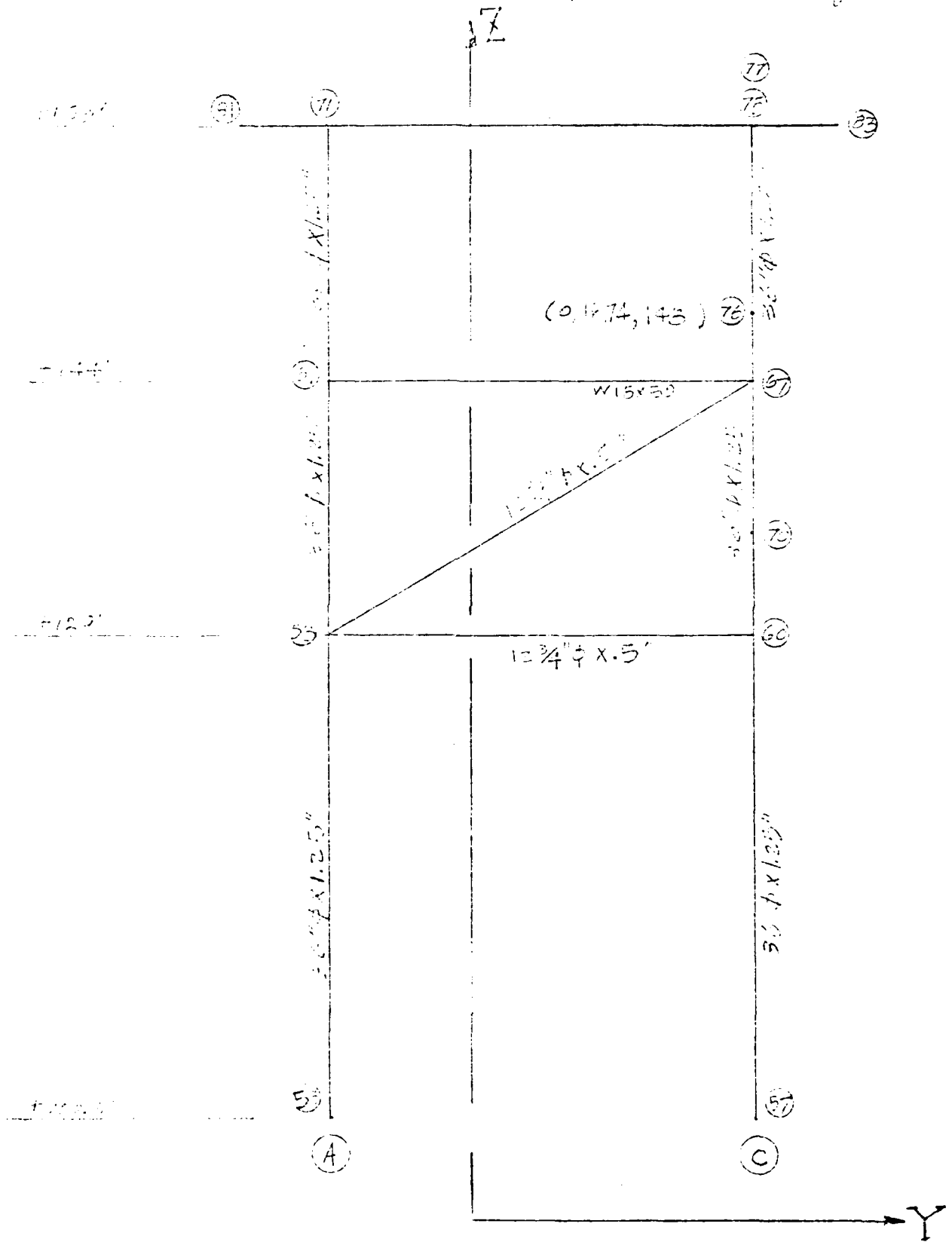
Sheet 12.17 of 22

By C. C. ... Client U.S. NAVY

Subject Structural Concept Analysis

Date 1-27-74 Job No. 27-77-1A

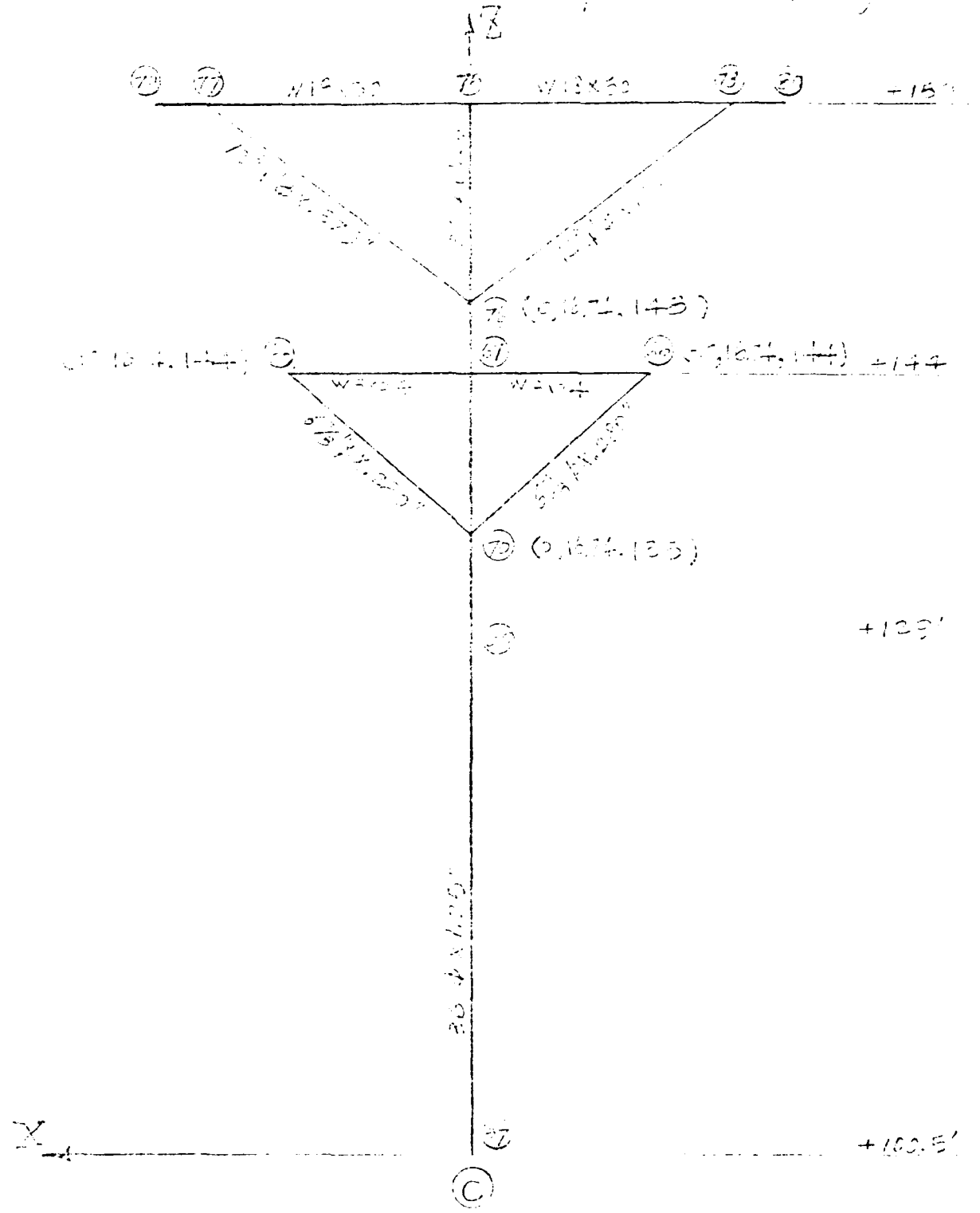
Calculation Space Truss Analysis



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Sheet 15 of 22

By C. [Signature] Client U.S. Navy Subject Structure of [unclear]
 Date 7-2-53 Job No. 27-77-93 Calculation [unclear]

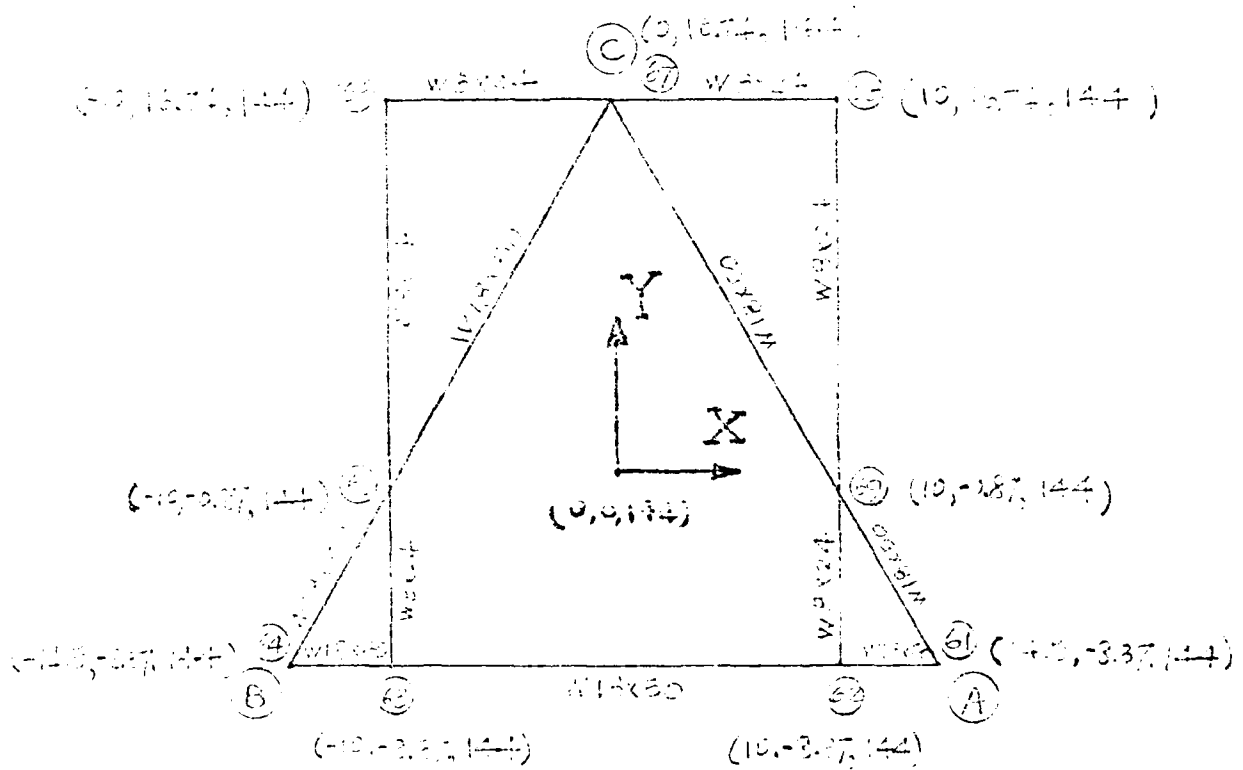


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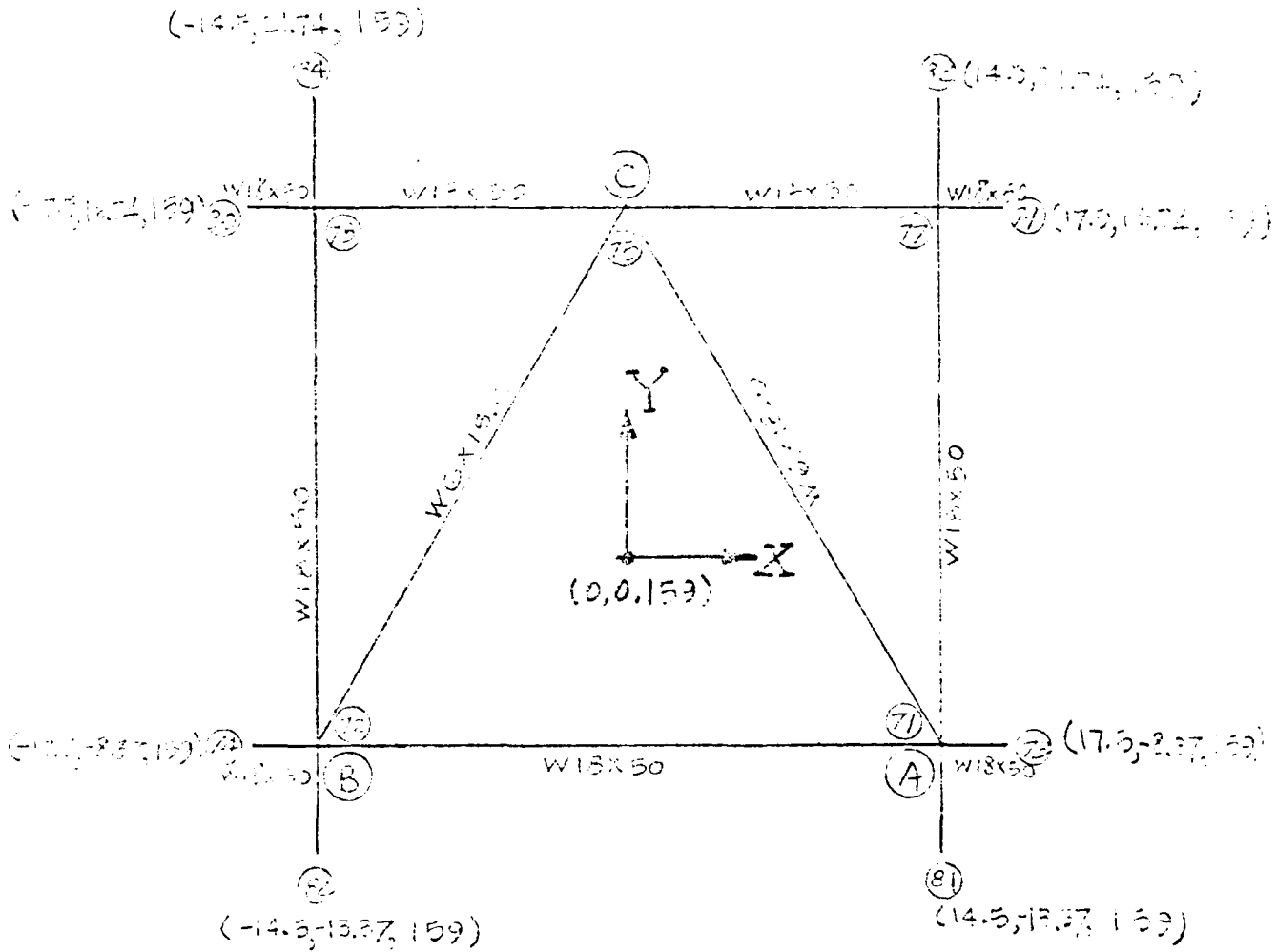
Sheet 11 of 12

By S. S. [unclear] Date 1-25-73
 Object U.S. 1177
 Job No. 1177-73

Subject Struct. Analysis
 Calculation Space Frame Analysis

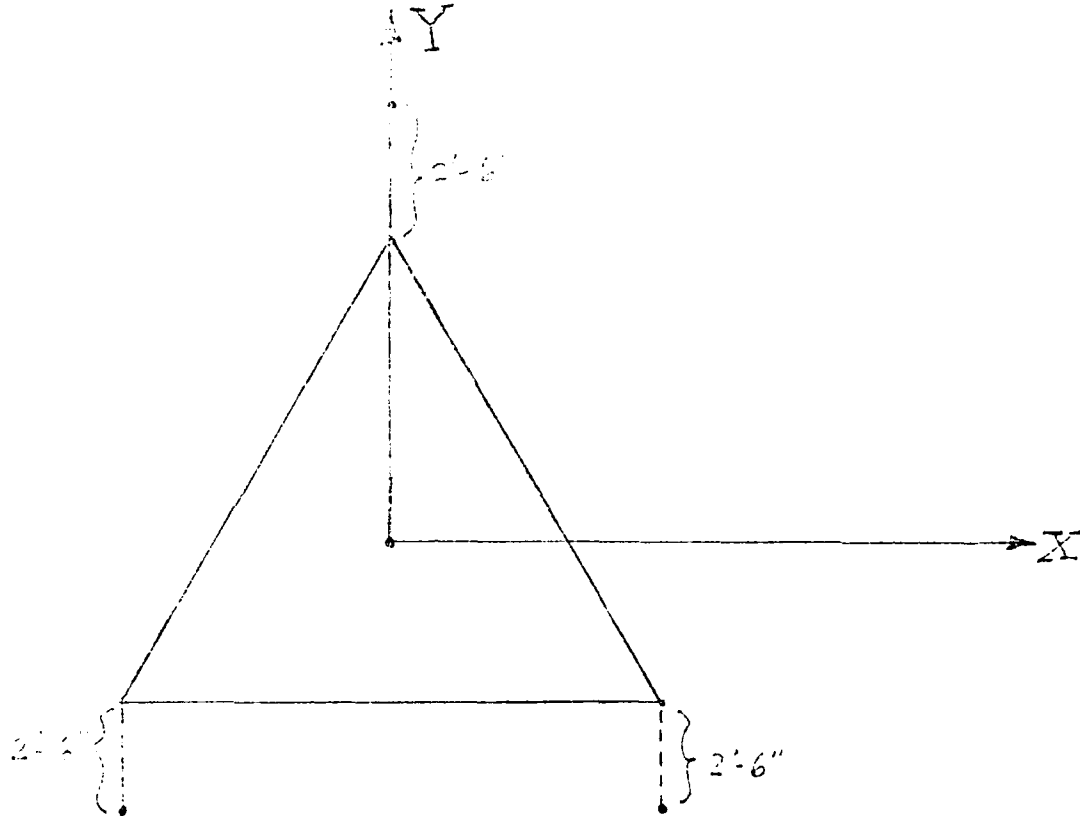


By C. Chen Client U. I. 10Y Subject Structural Design of Analysis
 Date 8-27-14 Job No. 27-111-14 Calculation Spse FEM Analysis

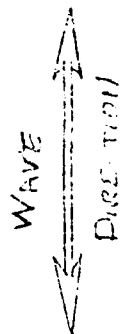


By S. Olson Client US Navy Construction of Concrete Analysis
Date Feb 28 Job No. 270 221 14 Calculation Upper Limb Length

Joint Coordinates for Wishbone Junction Point



Wishbone
Junction
Point



Client Shell Subject Offshore Platform
Date 4-11-72 Job No. E7-711-3 Calculation SP CR

10.3 RESULTS OF ANALYSIS

(i) Loads on Piles

Maximum Tensile Force = 1450 KIPS

Maximum Compressive Force = 1300 KIPS

According to Pile Capacity Curves shown on Page 3-8) for 36" O.D. pipe piles, the proposed 130 ft of penetration is acceptable.

(ii) Member Stresses

Stresses on each structural component are in acceptable range under design environmental conditions.

(iii) Deflections

The maximum deflection at the top deck (E.L. +75'-0" from MLW) is at 6.8 inches under most critical environmental conditions.

SECTION 11
CORROSION PROTECTION

11.1 INTRODUCTION

API Recommendations for corrosion protection serve as the base for selecting the protection methods in this section.

Project: *Offshore Platform Concept Analysis*
 Date: *11/15/77* Job No: *11-77-1/2* Calculation: *Corrosion Protection*

11.2 API RECOMMENDATIONS

CORROSION PROTECTION

2.12 Zone Definition. The surface area of a platform is divided into three zones for corrosion protection considerations. The zones are:

- a. *Splash Zone.* That area extending 6 feet above low lunar tide to 4 feet below low lunar tide.
- b. *Atmospheric Zone.* That area above the splash zone.
- c. *Submerged Zone.* That area below the splash zone.

2.13 Protection in Splash Zone. The splash zone area shall be protected by one of the following methods:

- a. Extra steel in excess of that needed for strength.
- b. *Noncorrosive metallic wrap.*
- c. *Coatings.*

2.14 Protection in Atmospheric Zone. All steel surfaces in the atmospheric zone should be protected against corrosion. Proper surface preparation and application of materials selected will prove most economical. Various paint systems and galvanizing have proved satisfactory. Application procedures should follow the manufacturer's recommendations closely.

2.15 Protection in the Submerged and Buried Zones. One of the following modes of cathodic protection should be used to protect the structure in the submerged zone:

- a. *Sacrificial anodes.*
- b. *Impressed current.*

2.16 Selection of Method to be Used. Either of the systems (or their combination), if properly designed, installed, and maintained will satisfactorily protect the submerged portion of the platform. The proper selection will depend upon due consideration of the requirements imposed by the size of the platform, water depth, connecting pipe lines, availability or nature of electric power, and personnel assignments. Sacrificial anodes may add a significant amount of weight to the structure which must be considered when designing for launching and installation. For impressed current systems, qualified personnel are required to monitor and maintain the system continually, and a continuous source of electrical power is required from the beginning to develop initial polarity and prevent corrosion.

2.17 Current Requirements. The corrosivity of the environment and the current required to achieve complete protection depend on the environmental variables which affect oxygen availability at the steel surface. The most important variables are: (1) water velocity, (2) water depth, (3) water temperature and salinity, and (4) the ability to deposit calcareous deposits on the surface.

The initial minimum current densities recommended for the submerged zone (the total exposed area between the water surface and the bottom) are:

Area	Current Density mA/ft ²
Gulf of Mexico	5-6
West Coast of United States	7-8
Cook Inlet	35-40

These values are adequate if the anodes are properly distributed throughout the submerged zone, and this can generally be achieved with sacrificial anodes. Since the output of impressed current anodes is much higher and their number is less, the distribution is less efficient and these values should be increased by a factor of 1.25-2.0.

In addition to the above, current should be applied for protection of the steel in the soil. The requirement for the soil zone (the total exposed area of the jacket, piles and drive pipe in the soil) is 1-2 mA/ft². The well casing should be protected with the application of an additional 3 amperes per well. Due consideration should be given to the effect of connecting pipelines and risers to the platform.

Project: CREST OFFSHORE
 Date: 4-28-76 Job No. 27-771-73

Subject: Structural Protection
 Calculation: Corrosion Protection

2.03 System Design

a. Sacrificial Anodes. The design of a sacrificial system involves establishing the total weight of alloy required and a distribution which will effectively disperse the current throughout the area to be protected.

1. Total Weight

$$W_t = \frac{I \times N \times 8760}{C}$$

where:

- W_t = Total weight of alloy (lbs)
- I = Total current requirement (amps)
- N = Desired life (years)
- C = Capacity of alloy $\frac{\text{amp-hrs}}{\text{lb}}$

Capacities of some of the more common alloys at loadings of 200-700 mA/ft² are:

Alloy	C
Zinc (Mil-A-18601H)	370
Aluminum-Zinc-Mercury	1250-1200
Aluminum-Zinc-Indium	760-870
Aluminum-Zinc-Tin	420-1130

The differences shown within any one grouping are attributed to variations in both composition and heat treatment offered by the various suppliers.

Note: The anode selected should have a minimum closed circuit driving voltage of 1160 mv.

2. Anode Configuration. Neglecting the effects of any corrosion products, the current which an anode can deliver is a function of the anode/electrolyte resistance, R_a, and the potential difference between the anode and cathode, E. R_a can be determined from a modification of Dwight's formula:

$$R_a = \frac{0.0625 \rho \left(\ln \frac{4L}{r} - 1.0 \right)}{L}$$

where:

- L = length of anode (inches)
- r = equivalent radius (inches)
- ρ = resistivity of electrolyte (ohm-cm) at the anticipated water temperature

For other than cylindrical anode shapes:

$$r = \sqrt{\frac{\text{cross sectional area}}{\pi}}$$

A weight/anode configuration relationship should be selected which will permit the

sacrificial alloy to be consumed over the desired life. This can be expressed as:

$$N = \frac{C \times W_t}{8760 \times E/R_a}$$

It is customary to assume E = 0.250V and to calculate R_a based on the dimensions of the anode at 40% consumption.

3. Location. The anodes should be positioned throughout the platform in relation to the area of steel to be protected. Since the efficiency of most sacrificial alloys is adversely affected when covered with mud, attachment of anodes to structural members at the mud line should be avoided.

4. Method of Attachment. Anodes may be welded to structural members using stand-offs or flush-type pads. If the standoff method is used, a minimum of 12 inches between the anode and adjacent steel should be allowed, and the connections should be designed to withstand the installation loads caused by launching and pile driving and the environmental loads during the life of the anode. The flush-type anode should incorporate a dielectric shield which extends a minimum of 12 inches outward from the perimeter. Tack welding or set screws may be used to establish electrical continuity if a clamp-type connection is used.

b. Impressed Current. The design of an impressed current system involves selecting the anode material, determining the optimum methods of attaching the anodes to the structure, and assuring the reliability of associated electrical hardware (rectifiers, anode lead wire, etc.).

1. Anodes. Unless the system is designed for replacement, the anode material must function for the expected life of the structure. Some materials used at this time and pertinent properties are listed in the following table:

Material	Rate of consumption, lb/A yr	Max. Current Density, A/ft ²	Maximum Potential, Volts
Lead silver alloy	0.1-0.2	15-20	100 +
Lead w/ platinum pins	0.003	15-20	100 +
Platinum over Titanium	0.000013	100 +	8
Platinum over Niobium	0.000013	100 +	40-50
Platinum over Tantalum	0.000013	100 +	200

2. Method of Attachment. Impressed current anodes may be permanently fixed to the structure during construction, run through protective conduits which are installed in the fabrication yard, suspended by their lead wire or by a plastic rope supported on a shielding composition fitting which is screwed or flanged to the protective conduit, or mounted on bottom-supported sleds. The installation must be designed to withstand the environmental forces as well as the

By S. J. [unclear] Date U.S.M.A. [unclear] Subj: Structure of Concentration
 Date 4-27-76 Job No 27 776 94 Calculation Current Protection

special conditions imposed by high electrical potentials and currents. Dielectric shielding material which can withstand the caustic chlorine, high current density environment should be used as a barrier on the steel adjacent to the anode to prevent maldistribution of the protective current.

3. Placement of Anodes. The anodes should be positioned so that all portions of the structure are adequately protected. With the smaller output anodes (30-50 amperes) current "throw" is in the range of 25 to 50 feet while a projection of 60 to 70 feet is possible with the 200 ampere anodes if properly shielded.
4. Conductor. If oil-immersed rectifiers are used, cross-linked polyethylene (XLPE) insulated conductors should be specified, because it will not deteriorate on contact with transformer oil.
5. Rectifier. The rectifier(s) should be sized to deliver the anticipated current output of the anodes; however, some oversizing of the rectifier to permit higher current densities during polarization may be desirable. The rectifier voltage should be adequate to overcome the resistance of platform wiring and anode lead, the anode/electrolyte resistance and the back EMF of the anode.

2.49 Monitoring. Potential surveys should be conducted periodically to assure that the structure is adequately protected. A potential of -0.85 volts with reference to a Cu/CuSO₄ electrode (-0.80 volts Ag/AgCl or +0.25 volts to zinc) is the accepted criterion for protection. The reference cell should be relatively close to the protected steel when the measurements are made. Permanent zinc or Ag/AgCl reference cells can be installed, but polarization of such cells should be checked. Rectifier outputs on impressed current systems should be checked weekly to determine if the rectifiers and anodes are operating satisfactorily. When problems are encountered, immediate steps should be taken to restore protection.

2.50 Record Keeping. When a structure is installed, a cathodic protection system file should be set up at the location responsible for design. This file should contain drawings of the structure showing the position of all anodes. In the case of impressed current systems, the drawings should also show the location of all rectifiers and wiring. This file should also contain a record of all potential surveys, rectifier current/voltage readings, and any repairs made to the system.

W.D. Cline, Client U.S. Navy

Subject: Design of Corrosion Protection

Proj. 4-23-75 Job No. 27-771-1

Calculation: Corrosion Protection

11.3 DESIGN DATA

Zones for Corrosion Protection:

- a) Splash Zone: From 80ft to 34ft above mud-line
(34ft MLW)
- b) Atmospheric Zone: 73ft (above mud-line) and up
- c) Submerged Zone: 0ft to 30ft (above mud-line)
0ft to 130ft (below mud-line)

Current Requirements:

Current Density = 6 mA/24" of surface in water

2 mA/24" of surface in mud zone

Design Life:

15 to 4 yrs

CREST OFFSHORE, INC.

Sheet 1025 of 12

By W. J. ... Client U.S. NAVY Project Structural Conceptual
 Date 1-1-77 Job No. 27-771-01 Calculation Cr. Section Properties

11.4 SUBMERGED ZONE

A. ~~WATER~~ SOILS

MEMBER SIZE	MEMBER LENGTH (SPEC.)	SQ. FT. AREA	NO. REQUIRED	TOTAL AREA	NOTES
	FT	SQ. FT		SQ. FT	
41 1/2 x 1 WT	36'-0"	386.42	3	1,159.26	Jkt Leg
40 1/2 x 3/8 WT	46'-0"	421.71	3	1,445.13	Jkt Leg
40 1/2 x 3/8 WT	58'-0"	273.52	3	219.96	Midline Leg
40 1/2 x 3/8 WT	28'-0"	106.29	3	318.87	
40 1/2 x 3/8 WT	48'-9"	222.73	3	689.19	132' M/L
14 1/2 x 3/8 WT	24'-4"	89.17	3	267.52	"
12 1/2 x 3/8 WT	33'-6"	131.85	3	395.55	64' M/L
10 1/2 x 3/8 WT	19'-0"	63.92	3	197.76	"
6 1/2 x 3/8 WT	40'-2"	168.29	6	1,010.34	0-32' M/L V.
2 1/2 x 6 1/2 WT	64'-3"	235.36	3	356.08	32'-64' M/L V.
20 1/2 x 3/8 WT	23'-3"	123.94	3	371.82	64-81' M/L V.
				7,531.48	

By C. Chou Client U.S. Navy Service Structural Dept. Annapolis
 Date Feb 26 62 Job No. 27-77-12 Calculation Corrosion Protection

(3) Mud Zone

Member SIZE	Member LENGTH	Surface AREA	NO. REQUIRED	TOTAL AREA	NOTES
	FT	SQ. FT		SQ. FT	
2" X 1/2"	150'	1,026.46	5	5,132.33	Piling

TOTAL CURRENT REQUIREMENTS

$$\begin{aligned}
 I &= 6 \times 7,531.43 + 2 \times 5,099.23 \\
 &= 55,368 \text{ m Amps.} \\
 &= 55.4 \text{ Amps.}
 \end{aligned}$$

CAPACITY OF ALLOY

Use $C = 1250 \frac{\text{amp-hrs}}{\text{sq. ft}}$

(ALUMINUM-ZINC-MERCURY)

Client Shell International Subject Structural Concept Development
Date 11/11/82 Job No. 11-25-82 Calculation Case 11-25-82

TOTAL WEIGHT OF TUBES AND ANODES

$$\begin{aligned}
 W &= \frac{11 \times 3760}{1} \\
 &= \frac{55.4 \times 10 \times 3760}{1000} \\
 &= 3,882.4 \text{ lbs}
 \end{aligned}$$

Use 325 lbs anode

$$\text{No. of } n = \frac{3,882.4}{325} = 11.9$$

Use 15 x 325 lbs/anode

4,375#

W.C. Chen Client U.S. 1577 Subject 1577
Date 11/21/92 Job No. 22-777-92 Calculation Surge vs. Protection

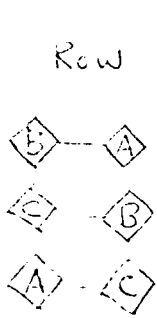
11.5 SPLASH ZONE

Use 0.5 inch extra steel in excess of that needed for strength.

by C. C. [unclear] [unclear] [unclear]
 Date 1/15/75 Job No. 37 [unclear]

Subject [unclear] [unclear] [unclear]
 Calculation [unclear] [unclear]

JACKET ELEVATION



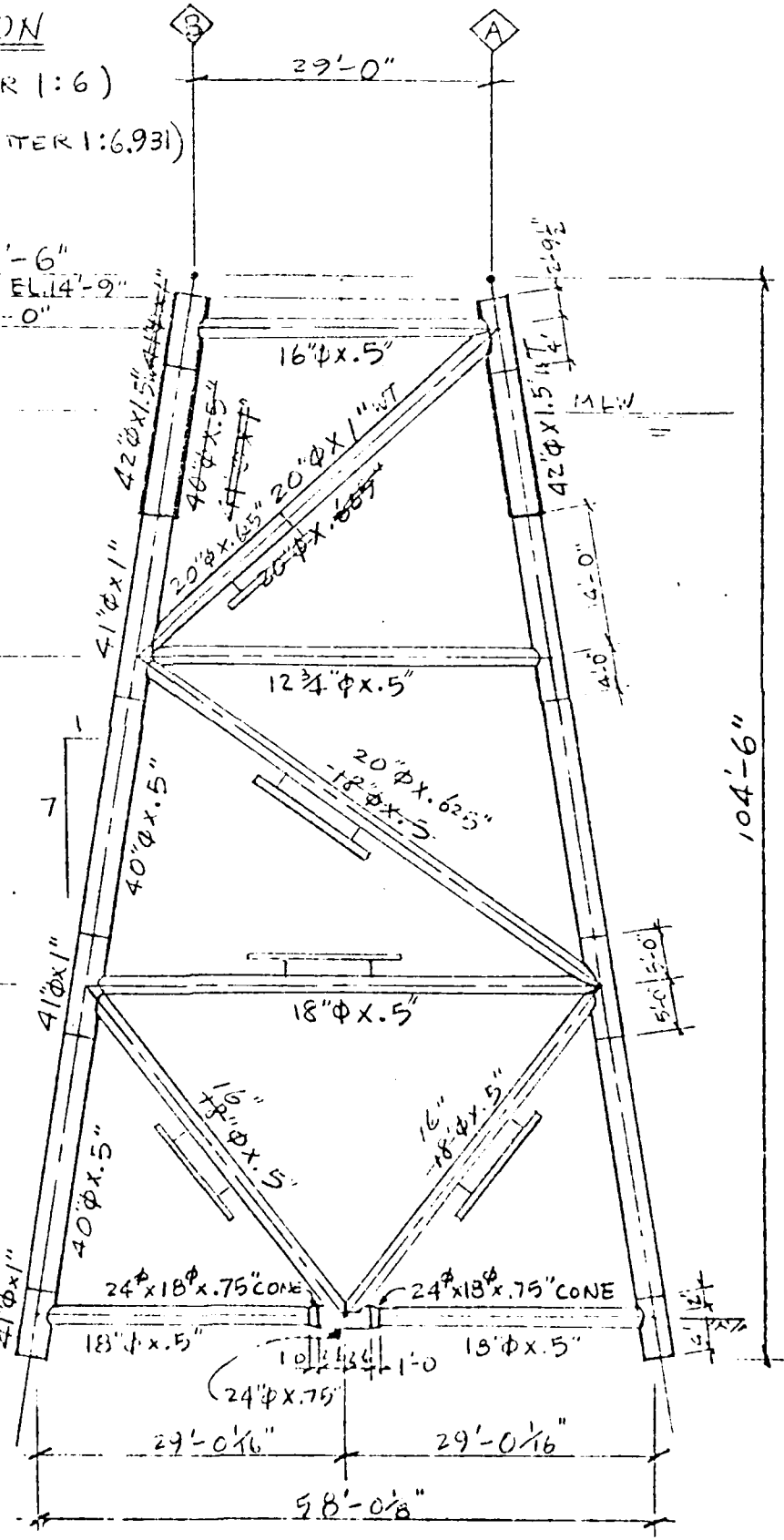
(TRUE BATTER 1:6)
 (APPEARANCE BATTER 1:6.931)

W.P. EL. 16'-6"
 TOP OF JKT. EL. 14'-9"
 ± EL. (+) 12'-0"
 EL. 0'-0"

± EL. (-) 20'-0"

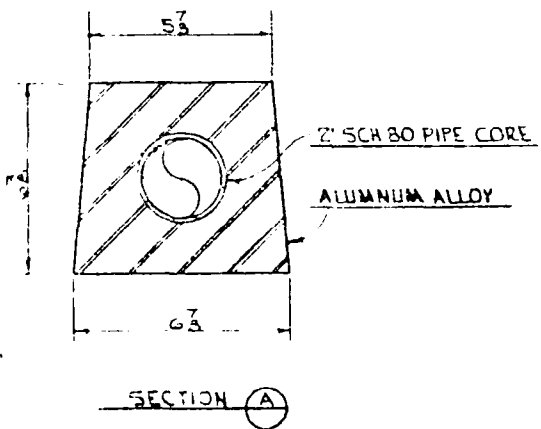
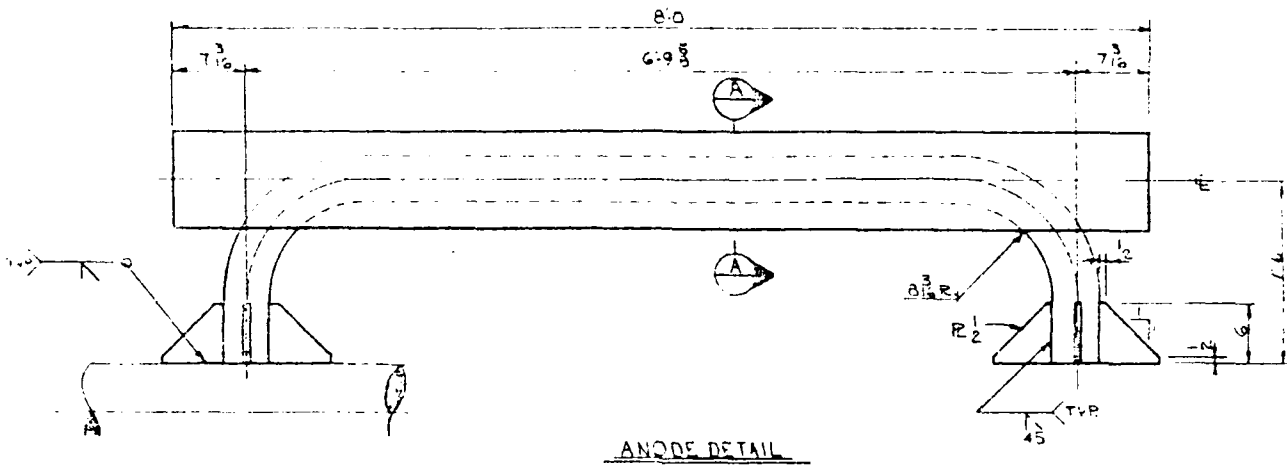
± EL. (-) 52'-0"

Mid Line EL. (-) 84'-0"
 BOT. OF JKT. EL. (-) 83'-0"



SCALE 1/16" = 1'-0"

By C. Chinn Check M. G. HAY Subject Structural Corrosion Analysis
 Date 5-4-72 Job No. 27-521-32 Calculation Corrosion Protection



ANODE WEIGHT LBS EACH

ALUMINUM ALLOY	CORE	TOTAL ANODE
325	43	368

NOTE:
 THE CATHODIC PROTECTION SYSTEM USED ON THIS PLATFORM WAS DESIGNED IN ACCORDANCE WITH PROCEDURES DEFINED BY CATHODIC PROTECTION SERVICE OF HOUSTON, TEXAS. THE ANODES USED SHALL BE OF THE DOW GALVALUM TYPE AS SHOWN ON CATHODIC PROTECTION SERVICE DRAWING S-263.

CREST OFFSHORE, INC.

Sheet 12 of 12

By C. J. ... Client W. J. ... Subject Structural Computations
 Date 4-22-71 Job No. 87-171-1 Calculation Corrosion Protection

11.6 ATMOSPHERIC ZONE

Check and verify corrosion protection for this

MEMBER SIZE	MEMBER LENGTH (Center to Center)	SURFACE AREA	No. REQUIRED	TOTAL AREA	NOTES
	FT	SQ. FT.		SQ. FT.	
4" x 4" WT	20'-9"	128.2	3	684.6	JKT LEG
10" x 8" WT	30'-0"	126.7	3	380.1	JKT BRACES EL. (+) 2'-0"
12" x 8" WT	15'-0"	50.1	3	150.3	"
36" x 12.25" WT	37'-0"	537.2	3	1,611.6	Sup. STR LEG
12" x 8" WT	28'-0"	96.6	3	290.4	BRACES EL. (+) 4'-0"
12" x 8" WT	32'-8"	103.0	3	327.0	"
3" x 3" WT	12'-6"	21.7	2	43.4	BRACES
1" x 1" WT	18'-0"	60.1	2	120.2	"
W18 x 30	20'-0"	150.5	3	478.5	Equip. Deck
1/2" x 24	25'-0"	74.0	2	148.0	"
1/2" x 24	20'-0"	59.2	10	592.0	"
1/4" x 24	20'-0"	500.0	2	1000.0	"

continue.

CREST OFFSHORE, INC.

Sheet 11 of 13

By C. Chivers Client Shell Subject Structural Deck Area
 Date 4-20-70 Job No. 27-621-00 Calculation Structural Deck Area

MEMBER SIZE	MEMBER LENGTH (SQ. FT) FT	SURFACE AREA SQ. FT	NO. REINFORCING	TOTAL AREA SQ. FT	NOTES
215x50	33'-0"	170.6	4	682.4	Top Deck
170x27	33'-0"	128.7	4	515.6	"
112x23	33'-0"	96.3	4	385.2	"
4x3/8x5.2	5'-0"	3.23	57	218.3	"
21' x 2	33'x33'	1,223.0	2	2450.0	"
16' x 2	33'-0"	87.0	2	174.0	"
			TOTAL	10,251.6	

10,251.6 SQ. FT

Stairway *

1,331.

Boat Landing *

743. SQ. FT

12,331 SQ. FT

* Values from deck Pile Structures under separate contract
 Crest Offshore Job No. 27-621-00 to Cubic Corporation.

SECTION 12
WEIGHT TAKEOFF

12.1 INTRODUCTION

Set forth herein is the weight and material list of the major components of the proposed three-pile structure. Boat landing, stairway, safety nets and miscellaneous items are not included in this section.

Client: CalPFA California State Water Structural Concept Analysis
Date: Dec 2/82 Job No: 82-071-3A Calculation: Weight Tables

12.2 MATERIAL LISTING

(A) Summary

The listing provides herein summary material requirements for the proposed three-pile structure including boat landing, stairways and miscellaneous items.

CREST OFFSHORE, INC.

Sheet 20 of 26

Project: Offshore Platform Location: Offshore
 Date: 10/15/75 Drawn by: W. J. Hoff

BILL OF MATERIALS SUMMARY

ACR 3-PILE STRUCTURE - MATERIAL LISTING -- U.S. NAVY -- C. CHRY

NOMINAL DIMENSION	TOTAL LENGTH (FEET)	TOTAL WEIGHT (POUND)
PIPE		
42,000 O.D. X 1,500 WT	63.00	41303.43
41,000 O.D. X 1,000 WT	102.00	43615.71
40,000 O.D. X 0,500 WT	166.64	30260.07
38,000 O.D. X 1,750 WT	300.00	192221.81
35,000 O.D. X 1,500 WT	480.00	265542.75
30,000 O.D. X 1,250 WT	257.00	110051.84
24,000 O.D. X 0,750 WT	21.00	3914.59
20,000 O.D. X 1,000 WT	41.40	8603.85
20,000 O.D. X 0,375 WT	193.80	25087.54
18,000 O.D. X 0,500 WT	299.28	27494.20
15,000 O.D. X 0,500 WT	330.90	27414.55
14,000 O.D. X 0,375 WT	160.14	8746.41
12,750 O.D. X 0,500 WT	349.02	22852.78
12,750 O.D. X 0,375 WT	95.31	4728.21
0,375 O.D. X 0,250 WT	18.00	3-1.86
* SHAPE		
W 18 X 50.00	227.00	11350.00
W 12 X 27.00	140.00	5780.00
W 8 X 24.00	250.00	6000.00
W 6 X 15.50	58.00	899.00
CHANNELS		
C 12 X 25.00	152.00	3800.00
PLATE		
1.000 THICKNESS	4.18	170.81
0.375 THICKNESS	108.16	1656.16
0.250 THICKNESS	1725.07	17609.37

TOTAL WEIGHT 858449.38 LBS

EXCESS PILING TO BE CUT OFF IN FIELD

36" O.D. X 1.75	12.00	7180.
36" O.D. X 1.50	13.00	9900.
36" O.D. X 1.25	39.00	13920.
36" O.D. X 1.00	100.00	25920.
		<u>315920.</u>

LBS

453 TONS

GREST OFFSHORE, INC.

Sheet 6 of 6

Project: Offshore Platform Subject: Material Listing
Drawing No. 22-011-1-1 Calculation: Weight

(B) Material Listing -- Composite

BILL OF MATERIALS SUMMARY
ACMR 3-PILE STRUCTURE MATERIAL LISTING -- PILING U.S. NAVY--O.CHEM

NOMINAL DIMENSION	TOTAL LENGTH (FEET)	TOTAL WEIGHT (POUNDS)
PIPE		
76,000 O.D. X 1,750 WT	300.00	102221.81
56,000 O.D. X 1,500 WT	480.00	265542.75
36,000 O.D. X 1,250 WT	66.00	30647.25

TOTAL WEIGHT 488411.81 LBS

EXCESS PILING TO BE CUT OFF IN FIELD

22" x .425	3 x 1 x 10' x 464 #/ft	= 13,920 #
36" x .75	3 x 2 x 2' x 340 #/ft	= 7,650 #
36" x 1.50	3 x 3 x 2' x 353 #/ft	= 9,954 #
		<u>31,524 #</u>

GRADE POINT

22" x .425	3 x 2 x 3' x 216 #/ft	= 25,920 #
------------	-----------------------	------------

Total	488,412
	31,524
	<u>35,920</u>
	545,856 #

CREST OFFSHORE, INC.

Sheet 12 of 100

By S. Chrya Client U.S. Navy Subject 3-Pile Structure
 Date 4-76 Job No. 42-7111 Calculation Weight Takeoff

Jacket

WORK OF MATERIALS SUMMARY
 4048 3-PILE STRUCTURE MATERIAL LISTING -- JACKET U.S. NAVY--010484

TOTAL WEIGHT (LBS) TOTAL LENGTH (FEET)

PIPE

42,000	0.0	X	1,500	FT	63.56	21523.83
21,000	1.0	X	1,000	FT	102.70	43615.71
60,000	0.0	X	1,500	FT	136.50	30950.87
20,000	0.0	Y	0,750	FT	21.00	3914.59
20,000	0.0	X	1,000	FT	41.40	8208.85
20,000	0.0	X	0,625	FT	105.80	25087.54
15,000	0.0	X	1,500	FT	209.28	27094.20
15,000	0.0	X	0,500	FT	33.40	27414.55
10,000	0.0	X	1,375	FT	160.14	8708.87
12,750	0.0	X	0,500	FT	164.07	10742.81
12,750	0.0	X	0,375	FT	59.31	2982.30

TOTAL WEIGHT 231130.04 LBS

CREST OFFSHORE, INC.

Sheet 13 of 16 for 6
0111

Order No. 0111
 Drawing No. 0111

Subject Deck Base Cap and Anchor
 Calculation Weight Take Off

Material

WITH THE FOLLOWING TOLERANCES: AS SHOWN
 APPROXIMATE BILL OF MATERIAL LISTING -- SUPERSTRENGTH STEEL -- U.S. NAVY -- C, CHEM.
 WEIGHTS AND DIMENSIONS IN POUNDS AND INCHES -- (SEE NOTE 1)

PLATE

36.000" W. x 1.250" T	171.00	7560.00
12.75" W. x 0.500" T	154.25	12105.00
20.250" W. x 0.375" T	34.50	1100.00
10.000" W. x 0.250" T	18.00	570.00

ANGLE

L 18" X 15.00" L	227.00	3305.00
" 12" X 27.00	140.00	3740.00
" 8" X 20.00	250.00	6100.00
" 6" X 15.50	58.00	890.00

CHANNELS

C 12" X 25.00	152.00	3800.00
---------------	--------	---------

PLATE

1.00 THICKNESS	4.18	171.00
0.375 THICKNESS	100.16	1056.16
0.250 THICKNESS	1725.76	17619.37

TOTAL WEIGHT 138907.13 LBS

APPENDIX A
COMPUTER PRINTOUTS

A.1 INTRODUCTION

The computer printouts compiled hereinafter were used, respectively, in the following items:

- (1) Pile Driving Resistance Curves;
- (2) Laterally Loaded Pile Capacity;
- (3) Wave and Wind Loads;
- (4) Space Frame Analysis; and
- (5) Member Weight Takeoff.

A-2 PILE DRIVING RESISTANCE CURVES

File P. 1. 1. 1. Resistance Curves

File Diameter	- 30 in.
Minimum Wall Thickness	- .75 in.
Penetration	- 180 ft.
Hammer	- Vulcan 040
Quake Factor, tip	- .025 in.

6 0 0 0 R E M O T E R A T C H

UNITED COMPUTING 67, APEX/SL, B.0.24

10.19.31. 04/15/76.

JJJJJJJJJJJJ	YY	JJJJJJJJJJJJ	222222222	JJJJJJJJJJJJ	RRRRRRRRRR	EEEEEEEEEEEE
JJJJJJJJJJJJ	YY	JJJJJJJJJJJJ	22222222222	JJJJJJJJJJJJ	RRRRRRRRRRR	EEEEEEEEEEEE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	222222	JJ	RRRRRRRRRR	EEEEEEEE
JJ	YY	JJ	222222	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	22	JJ	RR	EE
JJ	YY	JJ	2222222222	JJJJJJ	RR	EE
JJJJJ	YY	JJJJJ	2222222222	JJJJJ	RR	EE
JJJJJ	YY	JJJJJ	2222222222	JJJJJ	RR	EE

WAVE EQUATION PROGRAM CHECK-HOUSTON UCC.
 MC CLELLAND REPORT DATA FOR CURAC PROJECT.
 MARCH 30, 1976

PROB 1
 30 INCH DIAM PILE-EAST COAST USA.
 180 FT PENETRATION-VULCAN 040 HAMMER.
 0 TIPS, 0.25, MINIMUM WALL THICKNESS=.75 RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE	1
NEW HAMMER DATA OPTION	1
NEW MATERIAL DATA OPTION	1
NEW PILE SECTION DATA OPTION	1
NEW SOIL DATA OPTION	1
SPECIFIED BLOW COUNT OPTION	1
OUTPUT OPTION FOR STRESS	1
HPF FOR STRESS OUTPUT OPTION	275.
ULTIMATE RESISTANCE INCREMENT (TONS)	50.0
MAX BLOWS FOR RESISTANCE-BLOW CURVE (RPF)	300.
SPECIFIED SEGMENT LENGTH (FT)	0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION	VULCAN 040 HAMMER
HAMMER EFFICIENCY	.75
HAMMER ENERGY (FT-LBS)	120000.00
HAMMER EXPLOSIVE FORCE (LBS)	0.00
NUMBER OF HAMMER SEGMENTS	2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	278000.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES =	1		
MATERIAL TYPE	(TOD)	UNIT WT. (PCF)	MODULUS (PST)
1	30.000	490.0	20000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS	5
-------------------------------	---

NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE(FT) 140.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER	
				TOP	BOTTOM
1	1	1.250	30.	0	30
2	1	1.750	95.	30	125
3	1	1.250	40.	125	165
4	1	1.000	40.	165	205
5	1	.750	135.	205	340

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE = JSIDE .15
 POINT DAMPENING RESISTANCE = JPOINT .15
 SOIL SHAKE FOR SIDE = QSIDE .10
 SOIL SHAKE FOR POINT = QPOINT .03

TIP RESISTANCE PERCENTAGE

14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROJ 1 30 INCH DIAM PILE-EAST COAST USA.
 180 FT PENETRATION-VULCAN 600 HAMMER.

RU # 14

QTIP=.025, MINIMUM WALL THICKNESS=.75

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FY	SLACK IN.	WFLIGHT LRS	AREA SQ. IN.	COEF RSTITU	SPR STIFF LRS/IN.
1	0.00	1000.00	4000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	27284469.
3	160.00	0.00	3841.78	112.90	1.00	27284469.
4	150.00	0.00	3841.78	112.90	1.00	27284469.
5	140.00	0.00	3841.78	112.90	1.00	27284469.
6	130.00	0.00	4564.28	155.31	1.00	43460350.
7	121.36	0.00	4564.28	155.31	1.00	43460350.
8	112.73	0.00	4564.28	155.31	1.00	43460350.
9	104.09	0.00	4564.28	155.31	1.00	43460350.
10	95.45	0.00	4564.28	155.31	1.00	43460350.
11	86.82	0.00	4564.28	155.31	1.00	43460350.
12	78.18	0.00	4564.28	155.31	1.00	43460350.
13	69.55	0.00	4564.28	155.31	1.00	43460350.
14	60.91	0.00	4564.28	155.31	1.00	43460350.
15	52.27	0.00	4564.28	155.31	1.00	43460350.
16	43.64	0.00	4564.28	155.31	1.00	43460350.
17	35.00	0.00	3841.78	112.90	1.00	27284469.
18	25.00	0.00	3841.78	112.90	1.00	27284469.
19	15.00	0.00	3841.78	112.90	1.00	27284469.
20	5.00	0.00	3100.15	91.11	1.00	27284469.
21	-5.00	0.00	3100.15	91.11	1.00	22017380.
22	-15.00	0.00	3100.15	91.11	1.00	22017380.
23	-25.00	0.00	3100.15	91.11	1.00	22017380.
24	-35.00	0.00	3100.15	91.11	1.00	22017380.
25	-45.00	0.00	1978.72	68.92	1.00	19739720.
26	-53.44	0.00	1978.72	68.92	1.00	19739720.
27	-61.88	0.00	1978.72	68.92	1.00	19739720.
28	-70.31	0.00	1978.72	68.92	1.00	19739720.
29	-78.75	0.00	1978.72	68.92	1.00	19739720.
30	-87.19	0.00	1978.72	68.92	1.00	19739720.
31	-95.63	0.00	1978.72	68.92	1.00	19739720.
32	-104.06	0.00	1978.72	68.92	1.00	19739720.
33	-112.50	0.00	1978.72	68.92	1.00	19739720.
34	-120.94	0.00	1978.72	68.92	1.00	19739720.
35	-129.39	0.00	1978.72	68.92	1.00	19739720.
36	-137.81	0.00	1978.72	68.92	1.00	19739720.
37	-146.25	0.00	1978.72	68.92	1.00	19739720.
38	-154.69	0.00	1978.72	68.92	1.00	19739720.
39	-163.13	0.00	1978.72	68.92	1.00	19739720.
40	-171.56	1000.00	1978.72	68.92	1.00	19739720.

1 30 INCH DIAM PILE - EAST COAST USA,
 180 FT PENETRATION - VULCAN 600 HAMMER.

QTY = .025, MINIMUM WALL THICKNESS = .75 RU = 14

TABLE 2 - MAXIMUM STRESS DATA

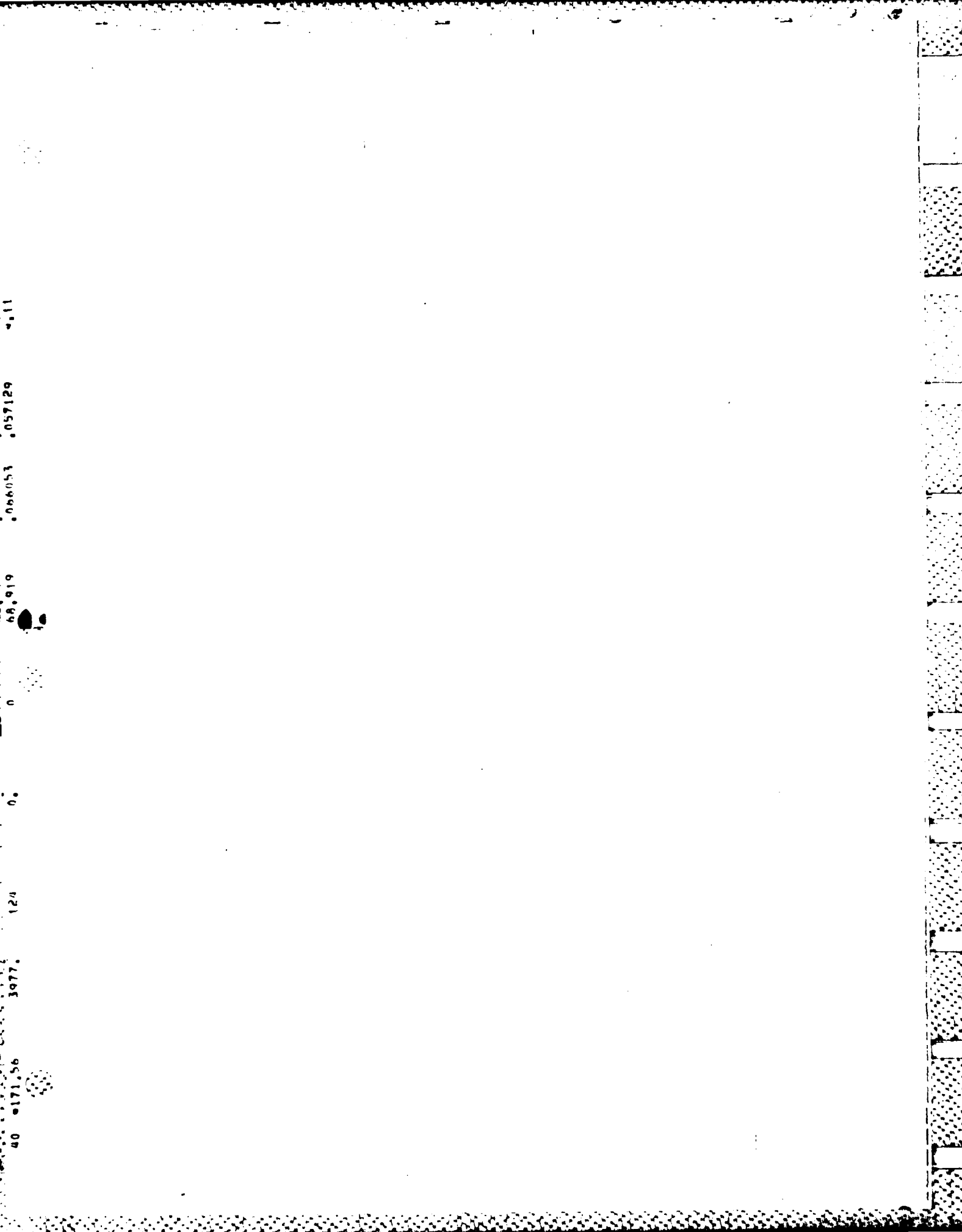
TYP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0411 INCHES

NUMBER OF BLOWN PER FOOT = 292.50

TOTAL INTERVALS = 192

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	1747701	30	0.	158	1,000	1.413143	1.408242	-.66
2	0.00	1528932	42	0.	153	1,000	1.048332	.864676	-2.90
3	160.00	13899.	45	611.	87	112.901	1.075414	.844709	-2.65
4	150.00	14191.	47	1181.	90	112.901	1.071942	.827144	-2.49
5	140.00	14356.	49	1700.	92	112.901	1.065286	.813632	-2.26
6	130.00	10466.	51	1471.	94	155.313	1.055434	.799513	-1.84
7	121.36	10492.	53	1421.	95	155.313	1.047041	.790153	-1.59
8	112.73	10492.	55	1490.	97	155.313	1.036542	.779254	-1.17
9	104.09	10420.	56	1676.	99	155.313	1.024085	.767053	-.95
10	95.45	10261.	58	1572.	100	155.313	1.010084	.756511	-1.19
11	86.82	10053.	60	1354.	102	155.313	.994704	.746731	-1.09
12	78.18	9827.	62	1014.	103	155.313	.978318	.733614	-.57
13	69.55	9570.	64	804.	104	155.313	.961346	.719311	-.66
14	60.91	9282.	66	604.	105	155.313	.944225	.707473	-.93
15	52.27	8957.	68	404.	0	155.313	.929152	.694137	-.20
16	43.64	8698.	71	204.	0	155.313	.922507	.675023	-.98
17	35.00	11757.	74	0.	0	112.901	.917891	.653857	1.21
18	25.00	11523.	76	0.	0	112.901	.908078	.625961	-.13
19	15.00	11270.	79	0.	0	112.901	.894908	.608956	-1.67
20	5.00	11712.	83	0.	0	91.106	.877626	.598529	-2.51
21	5.00	14055.	85	0.	0	91.106	.855801	.589515	-2.75
22	-15.00	14284.	89	0.	0	91.106	.824020	.577108	-2.70
23	-25.00	14526.	92	0.	0	91.106	.787344	.561862	-2.52
24	-35.00	14854.	96	0.	0	91.106	.746063	.543012	-2.28
25	-45.00	19642.	98	0.	0	68.919	.700624	.519998	-2.02
26	-53.44	19475.	101	0.	0	68.919	.648425	.491031	-1.77
27	-61.88	19157.	103	0.	0	68.919	.595229	.459169	-1.55
28	-70.31	18672.	105	0.	0	68.919	.541616	.428704	-1.33
29	-78.75	18047.	108	0.	0	68.919	.488040	.388228	-1.11
30	-87.19	17259.	111	0.	0	68.919	.434532	.350189	-.90
31	-95.63	16372.	114	0.	0	68.919	.381824	.311466	-.79
32	-104.06	15521.	114	0.	0	68.919	.330350	.272728	-.66
33	-112.50	14554.	117	0.	0	68.919	.281906	.234767	-.54
34	-120.94	13273.	118	0.	0	68.919	.237115	.194430	-.46
35	-129.38	11497.	121	0.	0	68.919	.195783	.144530	-.39
36	-137.81	10164.	123	0.	0	68.919	.159137	.133826	-.32
37	-146.25	8378.	124	0.	0	68.919	.127922	.107161	-.27
38	-154.69	6516.	122	0.	0	68.919	.101956	.085266	-.22



111

.057129

.066053

68,919

0

0.

124

3977.

40 171,56

PROR

1 30INCH DIAM PILE-EAST COAST USA,
180FT PENETRATION-VULCAN 640 HAMMER.

QTTP=.025, MINIMUM WALL THICKNESS=.75 HU = 14

TABLE 9 -- RESISTANCE-HLDM CURVE DATA

TTP RESISTANCE PERCENTAGE = 14.00

BLOWS/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS FORCE-TONS	MAX C STRESS LBS/SQ. IN. (N)	SEG LBS/SQ. IN. (N)	MAX T STRESS LBS/SQ. IN. (N)	SEG
2.58	50	23.10	15555.	11674.	30
4.35	100	42.66	16576.	8709.	30
6.45	150	58.66	16833.	6089.	31
9.65	200	71.93	17064.	3915.	11
12.96	250	82.94	17289.	2895.	12
16.24	300	92.08	17512.	1921.	12
19.42	350	99.65	17728.	1760.	9
23.40	400	105.93	17955.	1751.	9
28.51	450	111.15	18146.	1743.	9
35.24	500	115.25	18351.	1734.	9
44.34	550	118.33	18550.	1726.	9
57.11	600	120.64	18743.	1718.	9
75.69	650	121.96	18927.	1709.	9
103.84	700	123.93	19116.	1701.	9
146.99	750	128.93	19299.	1701.	5
205.74	800	133.31	19474.	1701.	5
292.30	850	137.06	19642.	1700.	5
441.84	900	140.57	19804.	1700.	5

PR08

1 30 INCH DIAM PILE - EAST COAST USA,
180 FT PENETRATION - VULCAN 080 HAMMER.

0.2% MINIMUM WALL THICKNESS, 75 HU = 14

TABLE 10 - SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOW PER FOOT	RESISTANCE TONS
144.99	750.
205.74	800.
244.73	826.
297.30	850.

10.17.12SPIL.CM100.T100.			
10.17.12SFL	64	0.000	
10.17.12SAC340NCR0023.2777100CC JH			
10.17.12. 04/15/76.JYJ2JRF			
10.17.12.4FL.40000.		0.000	
10.17.12SFL	3492	0.001	
10.17.12SFL	16384	0.001	
10.17.12.MAP.0FF.			
10.17.13SFL	256	0.001	
10.17.13.GET.PILR(CAR0024)			
10.17.21.READY = PILR			
10.17.21SFL	4096	0.001	0
10.17.21SFL	72	1	
10.17.21.PILR.			
10.17.21SFL00	16384	0.001	
10.17.24SFL01	16384	0.136	190
10.17.24.FL REQUIRED TO LOAD			36370R (1560R)
10.17.24.FL REQUIRED TO EXECUTE			34000R (14336)
10.17.24SFL	16384	0.140	
10.17.3A.END.PILDRI			
10.17.38.COST.	14336	8.779	30
10.17.38SFL			26.4
10.17.39.			
10.17.39.			
10.17.39SFL	12288	8.749	7
10.17.40.EXIT.			
10.17.40SJT00	2368	6.749	5
10.17.40.			
10.17.40.*P.F. PRUS*P.F. ACC *TAPE PRUS* TAPE ACC			

Pile Driving Resistance Curves

Pile Diameter	- 36 in.
Minimum Wall Thickness	- .75 in.
	- 1.25 in.
Penetration	- 200 ft.
Hammer	- Vulcan 040
Quake Factor, tip	- .025 in.
	- .10 in.
	- .30 in.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PILE STRUCTURE
 MC CLELLAND REPORT DATA FOR ACMR 3-PILE STRUCTURE -- MORNING 1
 APRIL 19 1976

PROB
 1

36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 QTYPE, 025, MINIMUM WALL THICKNESS, 75 IN, RU # 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED FLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX FLOWS FOR RESISTANCE-BLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) 0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LRS) 0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WFIGHT (LH)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TUD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE(FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	40.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 STIFF DAMPING RESISTANCE = JSTDF .15
 POINT DAMPING RESISTANCE = JPOINT .15
 SOIL QUAKE FOR SIDE = QSIDE .10
 SOIL QUAKE FOR POINT = QPOINT .03

TIP RESISTANCE PERCENTAGE

14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION == VULCAN 040 HAMMER

OTIPS, 0.25, MINIMUM WALL THICKNESS, 75 IN. RU = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTITU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2512.19	83.06	1.00	22580864.
32	-128.33	0.00	2512.19	83.06	1.00	22580864.
33	-137.78	0.00	2512.19	83.06	1.00	22580864.
34	-146.67	0.00	2512.19	83.06	1.00	22580864.
35	-155.56	0.00	2512.19	83.06	1.00	22580864.
36	-164.44	0.00	2512.19	83.06	1.00	22580864.
37	-173.33	0.00	2512.19	83.06	1.00	22580864.
38	-182.22	0.00	2512.19	83.06	1.00	22580864.
39	-191.11	1000.00	2512.19	83.06	1.00	22580864.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION == VULCAN 020 HAMMER

OTTPS.025, MINIMUM WALL THICKNESS.75 IN. RU = 14

TABLE 6 -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0314 INCHES

NUMBER OF HITS PER FOOT = 377.08

TOTAL INTERVALS = 155

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1781801.	36	0.	86	1.000	1.195696	1.179398	0.72
2	0.00	1481408.	48	0.	0	1.000	.743900	.733771	0.49
3	120.00	10889.	50	0.	0	136.463	.770099	.716667	0.40
4	111.00	10927.	53	0.	0	136.463	.761915	.705719	0.52
5	102.00	11005.	56	0.	0	136.463	.753255	.693367	0.59
6	93.00	11142.	59	0.	0	136.463	.744311	.682629	0.68
7	84.00	11303.	62	0.	0	136.463	.735145	.670450	0.83
8	75.00	11533.	65	0.	0	136.463	.725968	.657722	1.00
9	66.00	11715.	67	0.	0	136.463	.716689	.644401	1.17
10	57.00	11879.	70	0.	0	136.463	.706968	.630581	1.34
11	48.00	12016.	72	0.	0	136.463	.696425	.616248	1.48
12	39.00	12135.	75	0.	0	136.463	.684855	.601551	1.58
13	30.00	10268.	78	0.	0	162.578	.672102	.586582	1.67
14	21.67	10391.	80	0.	0	162.578	.661195	.574680	1.75
15	13.33	10540.	83	0.	0	162.578	.649429	.562380	1.83
16	5.00	10698.	85	0.	0	162.578	.636833	.549547	1.89
17	-3.33	10847.	88	0.	0	162.578	.623334	.536290	1.93
18	-11.67	10844.	90	0.	0	162.578	.608663	.522622	1.97
19	-20.00	10864.	93	0.	0	162.578	.592642	.508247	2.03
20	-28.33	10845.	96	0.	0	162.578	.575210	.493099	2.07
21	-36.67	10749.	98	0.	0	162.578	.556467	.477238	2.11
22	-45.00	10550.	101	0.	0	162.578	.536834	.460492	2.16
23	-53.33	10258.	103	0.	0	162.578	.516758	.442860	2.16
24	-61.67	9994.	107	0.	0	162.578	.496101	.424660	2.16
25	-70.00	11629.	110	0.	0	136.463	.474837	.405811	2.14
26	-78.33	11315.	113	0.	0	136.463	.449487	.382993	2.04
27	-86.67	10807.	114	0.	0	136.463	.423651	.360151	1.95
28	-95.00	10195.	118	0.	0	136.463	.397447	.337332	1.87
29	-103.33	9596.	122	0.	0	136.463	.370251	.314778	1.79
30	-111.67	9137.	124	0.	0	136.463	.342421	.292453	1.69
31	-120.00	14165.	129	0.	0	43.056	.313907	.270606	1.59
32	-128.89	13277.	132	0.	0	43.056	.266434	.233646	1.43
33	-137.78	12117.	133	0.	0	43.056	.222996	.198025	1.26
34	-146.67	10431.	135	0.	0	43.056	.183082	.167047	1.09
35	-155.56	9125.	139	0.	0	43.056	.147975	.138175	0.93
36	-164.44	7426.	141	0.	0	43.056	.117698	.112485	0.72
37	-173.33	5227.	149	0.	0	43.056	.092789	.080000	0.53

056824 056640

MS 056

0

0.

141

4177.

59 0191.011



PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER

QTIP, 0.25, MINIMUM WALL THICKNESS, 7.5 IN. RU = 14

TABLE 9 -- RESISTANCE-R/L/W CURVE DATA

ROWS/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS	FORCE-TONS	MAX C STRESS LRS/SQ. IN. NO.	SEG MAX T STRESS LRS/SQ. IN. NO.	SEG
2.65	50	21.89	13374	31 12495	31
4.09	100	43.15	13888	31 10219	31
6.47	150	57.92	14087	31 8105	31
8.84	200	72.55	14137	31 6203	31
11.86	250	85.35	14205	31 4509	31
14.30	300	96.54	14247	31 2995	31
16.20	350	106.55	14325	31 1640	31
18.42	400	114.91	14373	31 841	32
21.07	450	122.42	14422	31 0	39
24.27	500	128.99	14460	31 0	39
28.16	550	134.72	14495	31 0	39
32.98	600	139.57	14524	31 0	39
39.06	650	143.65	14545	31 0	39
46.47	700	146.96	14557	31 0	39
57.12	750	149.73	14559	31 0	39
70.93	800	151.77	14544	31 0	39
90.24	850	152.82	14517	31 0	39
117.64	900	156.45	14467	31 0	39
156.08	950	161.66	14403	31 0	39
205.31	1000	166.27	14331	31 0	39
273.06	1050	170.01	14253	31 0	39
377.08	1100	173.06	14165	31 0	39

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200FT PENETRATION -- VULCAN 000 HAMMER

GTIPS, 0.25, MINIMUM WALL THICKNESS, 7.75 IN. RU = 14

TABLE 10 -- SPECIFIED BLDG DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PFR FOOT	RESISTANCE TONS
156.08	950.
205.31	1000.
273.06	1050.
295.60	1063.

HAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACHR 3-PILE STRUCTURE -- HOHNG 1
 APRIL 19 1976

PROG 2
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 OTTPS, 10, MINIMUM WALL THICKNESS=.75 IN. 011 = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED RLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPFF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX RLOW'S FOR RESISTANCE-RLOW CURVE (RPFF) 300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TUN)	UNIT WT. (PCF)	MODULUS (PST)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER	
				TOP	BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	80.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE - JSIDE .15
 POINT DAMPING RESISTANCE - JPOINT .15
 SOIL QUAKE FOR SIDE - OSIDE .10
 SOIL QUAKE FOR POINT - OPOINT .10

TIP RESISTANCE PERCENTAGE

35.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 2 34-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN ODO HAMMER

QTIPS, 10-MINIMUM WALL THICKNESS=.75 IN. MU = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF ASTITU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2512.19	83.06	1.00	22580864.
32	-128.33	0.00	2512.19	83.06	1.00	22580864.
33	-136.67	0.00	2512.19	83.06	1.00	22580864.
34	-145.00	0.00	2512.19	83.06	1.00	22580864.
35	-153.33	0.00	2512.19	83.06	1.00	22580864.
36	-161.67	0.00	2512.19	83.06	1.00	22580864.
37	-170.00	0.00	2512.19	83.06	1.00	22580864.
38	-178.33	0.00	2512.19	83.06	1.00	22580864.
39	-186.67	1000.00	2512.19	83.06	1.00	22580864.

PROJ 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER

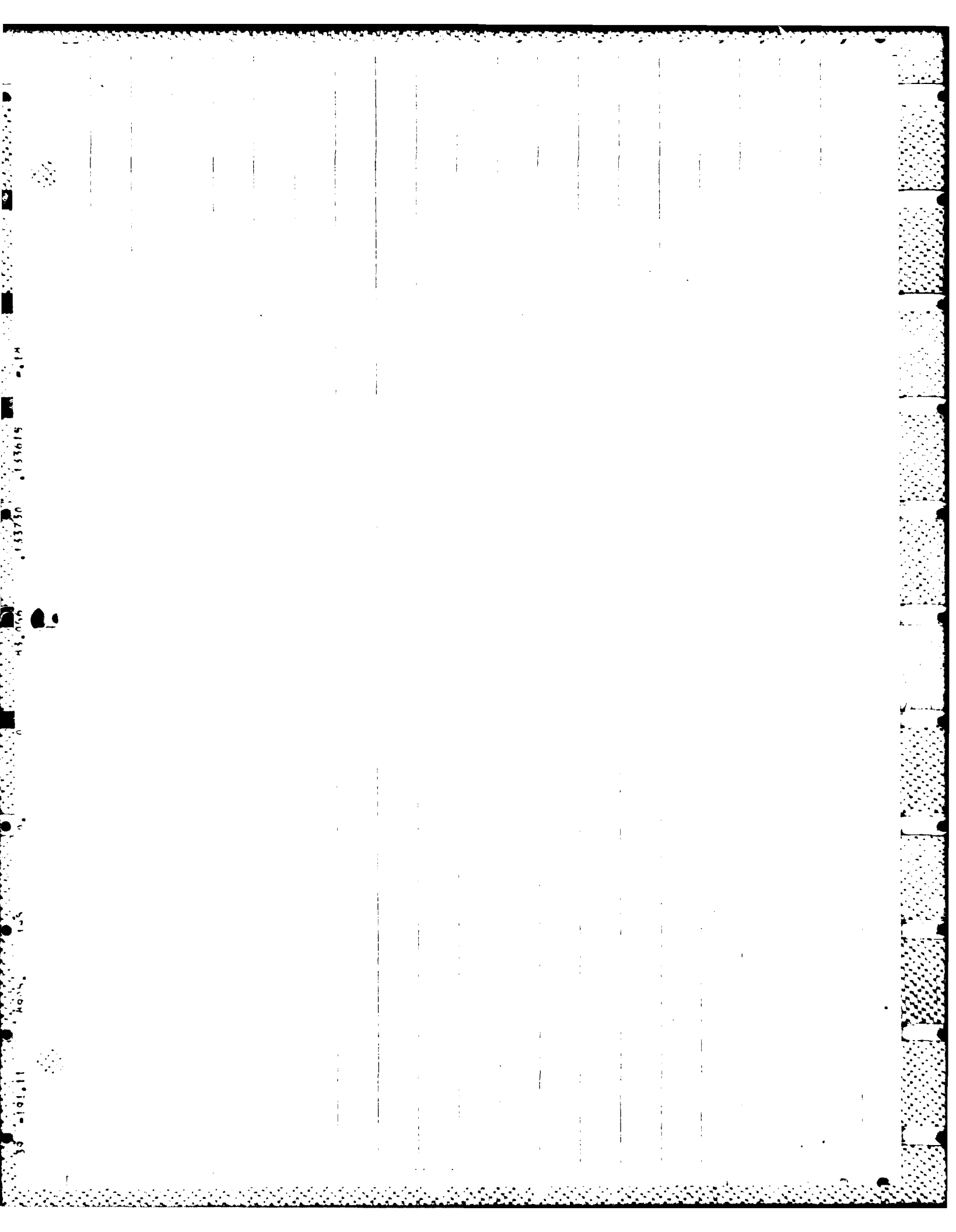
OTIP=10, MINIMUM WALL THICKNESS=.75 IN. HUI = 35

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 35.00

PERMANENT SFT OF PILE = .0337 INCHES
 NUMBER OF BLOWS PER FOOT = 355.77
 TOTAL INTERVALS = 159

SEC	ELEV FT	MAX C STRESS LBS/SQ.IN.	TIME N	MAX T STRESS LBS/SQ.IN.	TIME N	AREA SQ.IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1781801.	36	0.	86	1.000	1.213118	1.195109	-.59
2	0.00	1481808.	48	0.	0	1.000	.800812	.772794	-.08
3	120.00	10889.	50	0.	0	136.463	.787956	.759958	-.03
4	111.00	10927.	53	0.	0	136.463	.779014	.753663	.01
5	102.00	11005.	56	0.	0	136.463	.770689	.746867	.02
6	93.00	11162.	59	0.	0	136.463	.762406	.739543	-.03
7	84.00	11303.	62	0.	0	136.463	.754498	.731682	-.11
8	75.00	11533.	65	0.	0	136.463	.747345	.723369	-.22
9	66.00	11714.	67	0.	0	136.463	.740711	.717459	-.32
10	57.00	11977.	70	0.	0	136.463	.733959	.709953	-.43
11	48.00	12010.	72	0.	0	136.463	.728853	.697092	-.54
12	39.00	12114.	75	0.	0	136.463	.719362	.688063	-.66
13	30.00	10232.	77	0.	0	162.578	.711787	.678687	-.80
14	21.67	10318.	80	0.	0	162.578	.705937	.670957	-.90
15	13.33	10415.	82	0.	0	162.578	.699813	.662794	-.99
16	5.00	10516.	85	0.	0	162.578	.692933	.654224	-1.09
17	-3.33	10567.	87	0.	0	162.578	.685073	.645069	-1.20
18	-11.67	10574.	90	0.	0	162.578	.676191	.635221	-1.31
19	-20.00	10527.	92	0.	0	162.578	.666427	.624660	-1.43
20	-28.33	10478.	95	0.	0	162.578	.656044	.613178	-1.56
21	-36.67	10383.	97	0.	0	162.578	.644988	.600646	-1.69
22	-45.00	10209.	100	0.	0	162.578	.632862	.587026	-1.83
23	-53.33	9941.	102	0.	0	162.578	.620044	.572284	-1.94
24	-61.67	9636.	105	0.	0	162.578	.606305	.556530	-2.01
25	-70.00	11187.	108	0.	0	136.463	.591552	.539987	-2.04
26	-78.33	10902.	111	0.	0	136.463	.573055	.519741	-2.04
27	-86.67	10490.	113	0.	0	136.463	.553398	.499115	-2.01
28	-95.00	10030.	116	0.	0	136.463	.532331	.478149	-1.96
29	-103.33	9635.	120	0.	0	136.463	.509549	.456922	-1.94
30	-111.67	9324.	124	0.	0	136.463	.484986	.435283	-1.91
31	-120.00	14659.	127	0.	0	83.056	.458840	.413292	-1.88
32	-128.69	14258.	132	0.	0	83.056	.412506	.370397	-1.82
33	-137.78	13909.	135	0.	0	83.056	.367685	.335564	-1.68
34	-146.67	13579.	135	0.	0	83.056	.323984	.297846	-1.45
35	-155.56	12552.	138	0.	0	83.056	.281191	.261838	-1.20
36	-164.44	11790.	143	0.	0	83.056	.238792	.227577	-.99
37	-173.33	11267.	145	0.	0	83.056	.190338	.190554	-.73
38	-182.22	10331.	144	0.	0	83.056	.140649	.145309	-.45
39	-191.11	8905.	145	0.	0	83.056	.133730	.133615	-.18



1.14

133615

133730

43,000

0

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1.55

MONS.

39 - 101.11

PROB 2 30-IN. DIAMETER PILES 3-PIEF STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER

QTIP, 10, MINIMUM WALL THICKNESS, .75 IN. RU = 35

TABLE 9 -- RESISTANCE-CURVE DATA

BLOWS/FT.	TOTAL TONS	RESISTANCE DYNAMIC PT	MAX C STRESS	SEG	MAX T STRESS	SEG
		TONS	LBS/SQ. IN. MI.	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	
2.56	500	54.41	15087.	31	12072.	31
4.08	1000	101.75	14104.	31	9414.	31
6.70	1500	142.42	14188.	31	6973.	31
9.42	2000	177.50	14252.	31	4828.	31
13.29	2500	208.12	14304.	31	2942.	31
15.93	3000	234.67	14348.	31	1338.	6
18.41	3500	257.79	14397.	31	387.	12
21.43	4000	277.95	14435.	31	146.	12
25.14	4500	295.50	14473.	31	48.	5
29.84	5000	310.69	14509.	31	0.	39
35.49	5500	323.81	14537.	31	0.	39
43.49	6000	335.24	14568.	31	0.	39
54.77	6500	345.04	14591.	31	0.	39
70.19	7000	352.96	14615.	31	0.	39
93.31	7500	359.27	14631.	31	0.	39
130.74	8000	364.57	14646.	31	0.	39
199.58	8500	368.69	14653.	31	0.	39
355.77	9000	369.81	14659.	31	0.	39

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200FT PENETRATION -- VULCAN OIL MANHOLE

DTTS, 10, MINIMUM WALL THICKNESS = .75 IN. RII = 35

TABLE 10 -- SPECIFIED RII/DATA

TIP RESISTANCE PERCENTAGE = 35.00

RLDS PER FOOT	RESISTANCE TONS
130.74	800.
199.58	850.58
235.38	860.38
242.16	862.16

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAN REPORT DATA FOR ACHM 3-PILE STRUCTURE -- HITTING 1
 APRIL 19 1974

PROG 3
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 OTYPE, 30, MINIMUM WALL THICKNESS, .75 IN. RII = 50

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE	1
NEW HAMMER DATA (OPTION)	1
NEW MATERIAL DATA (OPTION)	1
NEW PILE SECTION DATA (OPTION)	1
NEW SOIL DATA (OPTION)	1
SPECIFIED MINIMUM COUNT (OPTION)	1
OUTPUT OPTION FOR STRESS	1
RPFF FOR STRESS OUTPUT (OPTION)	275.
ULTIMATE RESISTANCE INCREMENT (TONS)	50.0
MAX PILEMS FOR RESISTANCE-CURVE (RPFF)	300.
SPECIFIED SEGMENT LENGTH (FT)	=0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION	VULCAN 040 HAMMER
HAMMER EFFICIENCY	.75
HAMMER ENERGY (FT-LBS)	120000.00
HAMMER EXPLOSIVE FORCE (LHS)	=0.00
NUMBER OF HAMMER SEGMENTS	2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LR)	AREA (SQ IN)	COEFF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	400000.00	1.00	.00	2780000.00
2	1000.00	278000.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TON)	UNIT WT. (PCF)	MODULUS (PST)
1	36.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS = 0

NUMBER OF SECTIONS ABOVE 120.00
 NUMBER OF FREE STANDING PILE(S) 120.00

SECTION NUMBER	MATERIAL TYPE	PILE THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	80.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE = JSIDE .15
 POINT DAMPING RESISTANCE = JPPOINT .15
 SOIL SHAKE FOR SIDE = QSIDE .10
 SOIL SHAKE FOR POINT = QPOINT .30

TIP RESISTANCE PERCENTAGE

50.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

POOR

3 30-IN. DIAMETER PILES 3-PILE STRUCTURE
200FT PENETRATION -- VULCAN OGD HAMMER

QTYP=30, MINIMUM WALL THICKNESS=75 IN. WU = 50

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLV FT	SLACK IN.	WTGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27000.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2512.19	83.06	1.00	22580864.
32	-128.89	0.00	2512.19	83.06	1.00	22580864.
33	-137.78	0.00	2512.19	83.06	1.00	22580864.
34	-146.67	0.00	2512.19	83.06	1.00	22580864.
35	-155.56	0.00	2512.19	83.06	1.00	22580864.
36	-164.44	0.00	2512.19	83.06	1.00	22580864.
37	-173.33	0.00	2512.19	83.06	1.00	22580864.
38	-182.22	0.00	2512.19	83.06	1.00	22580864.
39	-191.11	1000.00	2512.19	83.06	1.00	22580864.

PROJ 5 34-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN DRUM HAMMER

QTPTS. 30, MINIMUM WALL THICKNESS .75 IN. RII = 50

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 50.00

PERMANENT SET OF PILE = .0203 INCHES
 NUMBER OF BLOWS PER FOOT = 500.68
 TOTAL INTERVALS = 162

SEG	FLEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	DMAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	1781801.	36	0.	162	1,000	1.240636	1.233526	12.04
2	0.00	1481408.	48	0.	0	1,000	.828015	.818145	.22
3	120.00	10889.	50	0.	0	136.463	.814294	.808768	.30
4	111.00	10927.	53	0.	0	136.463	.806497	.806497	.38
5	102.00	11005.	56	0.	0	136.463	.803675	.803675	.42
6	93.00	11162.	59	0.	0	136.463	.800235	.800235	.45
7	84.00	11343.	62	0.	0	136.463	.796287	.796287	.44
8	75.00	11532.	65	0.	0	136.463	.791986	.791986	.42
9	66.00	11714.	67	0.	0	136.463	.787506	.787506	.37
10	57.00	11876.	70	0.	0	136.463	.782954	.782954	.29
11	48.00	12006.	72	0.	0	136.463	.778297	.778297	.18
12	39.00	12102.	75	0.	0	136.463	.773462	.773462	.05
13	30.00	12111.	77	0.	0	162.578	.768821	.768357	-.07
14	21.67	12174.	80	0.	0	162.578	.764087	.764159	-.14
15	13.33	12346.	82	0.	0	162.578	.763462	.759657	-.25
16	5.00	12408.	85	0.	0	162.578	.760564	.754753	-.35
17	-3.33	12424.	87	0.	0	162.578	.757123	.749418	-.44
18	-11.67	12388.	89	0.	0	162.578	.753073	.745598	-.54
19	-20.00	12333.	92	0.	0	162.578	.748003	.737194	-.66
20	-28.33	12259.	94	0.	0	162.578	.743068	.730086	-.80
21	-36.67	12164.	97	0.	0	162.578	.737023	.722031	-.96
22	-45.00	12000.	99	0.	0	162.578	.730271	.712847	-1.12
23	-53.33	9744.	101	0.	0	162.578	.722704	.702549	-1.26
24	-61.67	9420.	104	0.	0	162.578	.714197	.691288	-1.34
25	-70.00	10900.	107	0.	0	136.463	.704650	.679288	-1.37
26	-78.33	10495.	109	0.	0	136.463	.692120	.664531	-1.38
27	-86.67	10222.	111	0.	0	136.463	.678116	.649473	-1.38
28	-95.00	9826.	115	0.	0	136.463	.662374	.633997	-1.40
29	-103.33	9504.	118	0.	0	136.463	.644997	.617845	-1.44
30	-111.67	9246.	122	0.	0	136.463	.626165	.600854	-1.50
31	-120.00	13494.	124	0.	0	83.056	.606420	.582926	-1.51
32	-128.89	13494.	126	0.	0	83.056	.572248	.550985	-1.51
33	-137.78	13494.	132	0.	0	83.056	.538100	.518649	-1.48
34	-146.67	13270.	134	0.	0	83.056	.502801	.485735	-1.44
35	-155.56	12767.	135	0.	0	83.056	.466422	.452430	-1.31
36	-164.44	12090.	139	0.	0	83.056	.429269	.419190	-1.11
37	-173.33	11952.	143	0.	0	83.056	.391508	.386115	-.83
38	-182.22	11751.	147	0.	0	83.056	.354822	.351249	-.52

PROB 3 36-IN. DIAMETER PILES TESTS STRUCTURE
 200FT PENETRATION -- VULCAN OGD HAMMER

QTIP=30, MINIMUM WALL THICKNESS=.75 IN. RU = 50

TABLE 9 -- RESISTANCE-HULL CURVE DATA

TIP RESISTANCE PERCENTAGE = 50.00

BLOWS/FT.	TOTAL TONS	RESISTANCE DYNAMIC PT	MAX C STRESS	SEG	MAX T STRESS	SEG
		FORCE-TONS	LBS/SQ. IN. MD.	LBS/SQ. IN. MD.		
2.49	50	77.43	13574.	31	11778.	31
4.16	100	144.24	14214.	31	8846.	31
6.98	150	201.14	14278.	31	6237.	31
10.65	200	250.01	14319.	31	3960.	31
16.12	250	292.27	14363.	31	1994.	31
20.03	300	328.70	14400.	31	944.	12
24.23	350	360.11	14432.	31	742.	12
29.66	400	387.15	14459.	31	545.	12
36.92	450	411.06	14490.	31	355.	12
46.98	500	431.71	14518.	31	172.	11
61.75	550	448.48	14540.	31	82.	3
83.22	600	465.90	14558.	31	9.	3
127.38	650	477.65	14580.	31	0.	39
221.86	700	482.82	14599.	31	0.	39
590.68	750	475.16	14612.	31	0.	59

PROB 3 30-IN. DIAMETER PILES S-PILE STRUCTURE
200T PENETRATION -- VULCAN 040 HAMMER

OTIP=30, MINIMUM WALL THICKNESS=.75 IN. HUI = 50

TABLE 10 -- SPECIFIED MIN. DATA

TIP RESISTANCE PERCENTAGE = 50.00

BLONS PER FOOT	RESISTANCE TONS
327.38	650%
221.86	700%
234.06	704%
279.84	715%

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 MC CLELLAND REPORT DATA FOR ACMR 3-PILE STRUCTURE -- HORING 1
 APRIL 19 1974

PROR
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36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 OTTDS.02%, MINIMUM WALL THICKNESS=1.25 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED BLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPE FOR STRESS OUTPUT OPTION 1
 ULTIMATE RESISTANCE INCREMENT (TONS) 275.
 MAX BLOWMS FOR RESISTANCE=300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COFF OF RESTYTUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TON)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 MC CLELLAND REPORT DATA FOR ACWR 3-PILE STRUCTURE -- WORKING 1
 APRIL 19 1974

PROB 4
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 DTTPS, 025, MINIMUM WALL THICKNESS=1.25 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED ALLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 HPE FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX ALLOWS FOR RESISTANCE-ALLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COEFF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TUN)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 3

NUMBER OF SECTIONS ALLOWED
 NUMBER OF SECTIONS ALLOWED 0
 LENGTH OF FREE STANDING PILE(FT) 120.00
 SECTION NUMBER MATERIAL WALL THICKNESS (IN) LENGTH (FT) STATION NUMBER TOP BOTTOM
 1 1 1.250 90.0 90
 2 1 1.500 100.0 190
 3 1 1.250 130.0 320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE = JSIDE .15
 POINT DAMPING RESISTANCE = JPOINT .15
 SOIL SHAKE FOR SIDE = QSIDE .10
 SOIL SHAKE FOR POINT = QPOINT .03

TIP RESISTANCE
 PERCENTAGE
 14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 4 3/4-IN. DIAMETER PILES 3-PILE STRUCTURE
 POINT PENETRATION == VULCAN 040 HAMMER

QTIPS, 0.25, MINIMUM WALL THICKNESS 1.25 IN. RU = 14

TABLE 7 == PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF	RSTJTIU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60		2780000.
2	0.00	1000.00	27800.00	1.00	.90		36642910.
3	120.00	0.00	4179.19	136.46	1.00		36642910.
4	111.00	0.00	4179.19	136.46	1.00		36642910.
5	102.00	0.00	4179.19	136.46	1.00		36642910.
6	93.00	0.00	4179.19	136.46	1.00		36642910.
7	84.00	0.00	4179.19	136.46	1.00		36642910.
8	75.00	0.00	4179.19	136.46	1.00		36642910.
9	66.00	0.00	4179.19	136.46	1.00		36642910.
10	57.00	0.00	4179.19	136.46	1.00		36642910.
11	48.00	0.00	4179.19	136.46	1.00		36642910.
12	39.00	0.00	4179.19	162.58	1.00		47147562.
13	30.00	0.00	4610.13	162.58	1.00		47147562.
14	21.67	0.00	4610.13	162.58	1.00		47147562.
15	13.33	0.00	4610.13	162.58	1.00		47147562.
16	5.00	0.00	4610.13	162.58	1.00		47147562.
17	-3.33	0.00	4610.13	162.58	1.00		47147562.
18	-11.67	0.00	4610.13	162.58	1.00		47147562.
19	-20.00	0.00	4610.13	162.58	1.00		47147562.
20	-28.33	0.00	4610.13	162.58	1.00		47147562.
21	-36.67	0.00	4610.13	162.58	1.00		47147562.
22	-45.00	0.00	4610.13	162.58	1.00		47147562.
23	-53.33	0.00	4610.13	162.58	1.00		47147562.
24	-61.67	0.00	4610.13	162.58	1.00		47147562.
25	-70.00	0.00	4024.40	136.46	1.00		38052252.
26	-78.67	0.00	4024.40	136.46	1.00		38052252.
27	-87.33	0.00	4024.40	136.46	1.00		38052252.
28	-96.00	0.00	4024.40	136.46	1.00		38052252.
29	-104.67	0.00	4024.40	136.46	1.00		38052252.
30	-113.33	0.00	4024.40	136.46	1.00		38052252.
31	-122.00	0.00	4024.40	136.46	1.00		38052252.
32	-130.67	0.00	4024.40	136.46	1.00		38052252.
33	-139.33	0.00	4024.40	136.46	1.00		38052252.
34	-148.00	0.00	4024.40	136.46	1.00		38052252.
35	-156.67	0.00	4024.40	136.46	1.00		38052252.
36	-165.33	0.00	4024.40	136.46	1.00		38052252.
37	-174.00	0.00	4024.40	136.46	1.00		38052252.
38	-182.67	0.00	4024.40	136.46	1.00		38052252.
39	-191.33	1000.00	4024.40	136.46	1.00		38052252.

PROB 4 30-IN. DIAMETER PILES 5-PTIF STRUCTURE
 POINT PENETRATION -- VULCAN OJO HAMMER

OTTP=0.25, MINIMUM WALL THICKNESS=1.25 IN. RHO = 14

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0374 INCHES

NUMBER OF HITS PER POINT = 321.13

TOTAL INTERVALS = 133

SEC	ELEV FT	MAX C STRESS LBS/90.0 IN.	TIME N	MAX T STRESS LBS/90.0 IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	R (M) IN.	V (M) FT/SEC
1	0.00	1781759.	31	0.	74	1.000	1.146375	1.170335	-1.75
2	0.00	1442024.	41	0.	0	1.000	.774623	.717423	-.65
3	120.00	10884.	43	0.	0	136.463	.760820	.699075	-.72
4	111.00	10924.	46	0.	0	136.463	.752573	.684238	-.82
5	102.00	11003.	48	0.	0	136.463	.743825	.672741	-.94
6	93.00	11161.	51	0.	0	136.463	.734673	.658624	-1.07
7	84.00	11341.	53	0.	0	136.463	.725205	.643946	-1.22
8	75.00	11533.	56	0.	0	136.463	.715450	.628709	-1.40
9	66.00	11716.	58	0.	0	136.463	.705433	.612879	-1.57
10	57.00	11891.	60	0.	0	136.463	.694498	.596519	-1.75
11	48.00	12019.	62	0.	0	136.463	.683424	.579528	-1.91
12	39.00	12137.	65	0.	0	136.463	.670774	.561916	-2.06
13	30.00	10285.	67	0.	0	162.574	.656405	.543687	-2.19
14	21.47	10417.	69	0.	0	162.574	.644714	.529008	-2.24
15	13.33	10583.	72	0.	0	162.574	.631363	.513477	-2.34
16	5.00	10766.	74	0.	0	162.574	.616657	.494324	-2.38
17	-3.33	10896.	74	0.	0	162.574	.600433	.482435	-2.40
18	-11.67	10954.	78	0.	0	162.574	.582759	.466234	-2.39
19	-20.00	10977.	81	0.	0	162.574	.563660	.449612	-2.36
20	-28.33	10959.	83	0.	0	162.574	.543180	.432534	-2.33
21	-36.67	10476.	85	0.	0	162.574	.521364	.414934	-2.30
22	-45.00	10742.	88	0.	0	162.574	.498334	.396665	-2.27
23	-53.33	10577.	90	0.	0	162.574	.474189	.377657	-2.24
24	-61.67	10420.	93	0.	0	162.574	.448491	.357932	-2.21
25	-70.00	12144.	95	0.	0	136.463	.422463	.337563	-2.16
26	-78.67	11419.	98	0.	0	136.463	.390221	.311813	-2.05
27	-87.33	11034.	100	0.	0	136.463	.357682	.285452	-1.93
28	-96.00	10904.	103	0.	0	136.463	.325346	.260290	-1.79
29	-104.67	10474.	106	0.	0	136.463	.293344	.235299	-1.65
30	-113.33	9849.	109	0.	0	136.463	.261414	.210840	-1.51
31	-122.00	9349.	113	0.	0	136.463	.229444	.187534	-1.36
32	-130.67	8955.	115	0.	0	136.463	.197949	.165540	-1.21
33	-139.33	8380.	115	0.	0	136.463	.168331	.145497	-1.10
34	-148.00	7801.	115	0.	0	136.463	.141513	.127034	-.97
35	-156.67	6540.	117	0.	0	136.463	.118536	.110463	-.83
36	-165.33	5549.	118	0.	0	136.463	.100007	.095761	-.64
37	-174.00	4512.	117	0.	0	136.463	.084941	.083091	-.49
38	-182.67	3401.	115	0.	0	136.463	.072798	.071997	-.37
39	-191.33	2299.	113	0.	0	136.463	.062549	.062549	-.25

PORT PENETRATION -- 16-IN. DIAMETER PILES SOFT STRUCTURE
 VULCAN 040 HAMMER

OTYPE, 0.25-MINIMUM WALL THICKNESS 1.25 IN. RUI = 14

TABLE 9 -- RESISTANCE-DYNAMIC CURVE DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLows/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS	DYNAMIC PT TOTAL-TONS	MAX C STRESS LRS/SO. IN.	SEG LRS/SO. IN.	MAX T STRESS LRS/SO. IN.	SEG
2.67	500	192.41	11499.	11	10033.	25
4.17	1000	37.03	12042.	12	8662.	25
6.24	1500	52.96	12092.	12	7338.	25
8.55	2000	67.41	12094.	12	6104.	25
10.80	2500	80.51	12096.	12	4991.	26
13.68	3000	92.40	12098.	12	4116.	8
16.24	3500	103.17	12100.	12	3480.	8
18.14	4000	112.92	12102.	12	2169.	27
20.29	4500	121.74	12104.	12	1361.	28
22.76	5000	129.69	12106.	12	676.	30
25.61	5500	136.85	12108.	12	0.	32
28.94	6000	143.33	12110.	12	0.	39
32.87	6500	149.13	12112.	12	0.	39
37.59	7000	154.24	12114.	12	0.	39
43.30	7500	158.66	12116.	12	0.	39
50.32	8000	162.52	12118.	12	0.	39
59.09	8500	165.87	12120.	12	0.	39
70.25	9000	168.89	12122.	12	0.	39
84.84	9500	171.54	12123.	12	0.	39
103.53	10000	173.00	12125.	12	0.	39
128.55	10500	176.95	12127.	12	0.	39
160.80	11000	181.92	12130.	12	0.	39
199.17	11500	187.09	12132.	12	0.	39
240.96	12000	192.35	12134.	12	0.	39
321.13	12500	197.66	12144.	25	0.	39

PROJ 4 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200FT PENETRATION -- VULCAN ODD HAMMER

QTIP = .025, MINIMUM WALL THICKNESS = 1.25 IN. RU = 14

TABLE 10 -- SPECIFIED ALLOW DATA.

TIP RESISTANCE PERCENTAGE = 14.00

BLINDS PER FOOT	RESISTANCE TONS
128.55	1050.
200.17	1150.
250.96	1200.
321.13	1250.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACOMP 3-PILE STRUCTURE -- HURTING I
 APRIL 19 1976

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36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 TYPE=10,MINIMUM WALL THICKNESS=1.25 IN. MU = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED HILUM COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 1
 ULTIMATE RESISTANCE INCREMENT (TONS) 275.
 MAX RUNS FOR RESISTANCE-CURVE 50.0
 SPECIFIED SEGMENT LENGTH (FT) 300.
 RPF -0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LRS) 0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COFF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2700000.00
2	1000.00	27000.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TON)	UNIT WT. (PCF)	MODULUS (PST)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 3

NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	130.	190	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE = JSIDE .15
 POINT DAMPING RESISTANCE = JPOINT .15
 SOIL QUAKE FOR SIDE = OSIDE .10
 SOIL QUAKE FOR POINT = OPOINT .10

TIP RESISTANCE PERCENTAGE

15.0000

TABLE 6 -- SPECIFIED ALLOW COUNT DATA

NUMBER OF SPECIFIED ALLOW COUNTS 4

ALLOW PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 5 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VOLCAN OGD HAMMER

QTIP=10, MINIMUM WALL THICKNESS=1.25 IN. MU = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELFV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	CHIEF RSTTU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2700000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4024.40	136.46	1.00	38052252.
26	-78.67	0.00	4024.40	136.46	1.00	38052252.
27	-87.33	0.00	4024.40	136.46	1.00	38052252.
28	-96.00	0.00	4024.40	136.46	1.00	38052252.
29	-104.67	0.00	4024.40	136.46	1.00	38052252.
30	-113.33	0.00	4024.40	136.46	1.00	38052252.
31	-122.00	0.00	4024.40	136.46	1.00	38052252.
32	-130.67	0.00	4024.40	136.46	1.00	38052252.
33	-139.33	0.00	4024.40	136.46	1.00	38052252.
34	-148.00	0.00	4024.40	136.46	1.00	38052252.
35	-156.67	0.00	4024.40	136.46	1.00	38052252.
36	-165.33	0.00	4024.40	136.46	1.00	38052252.
37	-174.00	0.00	4024.40	136.46	1.00	38052252.
38	-182.67	0.00	4024.40	136.46	1.00	38052252.
39	-191.33	1000.00	4024.40	136.46	1.00	38052252.

PROG 5 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN OIL MANNER

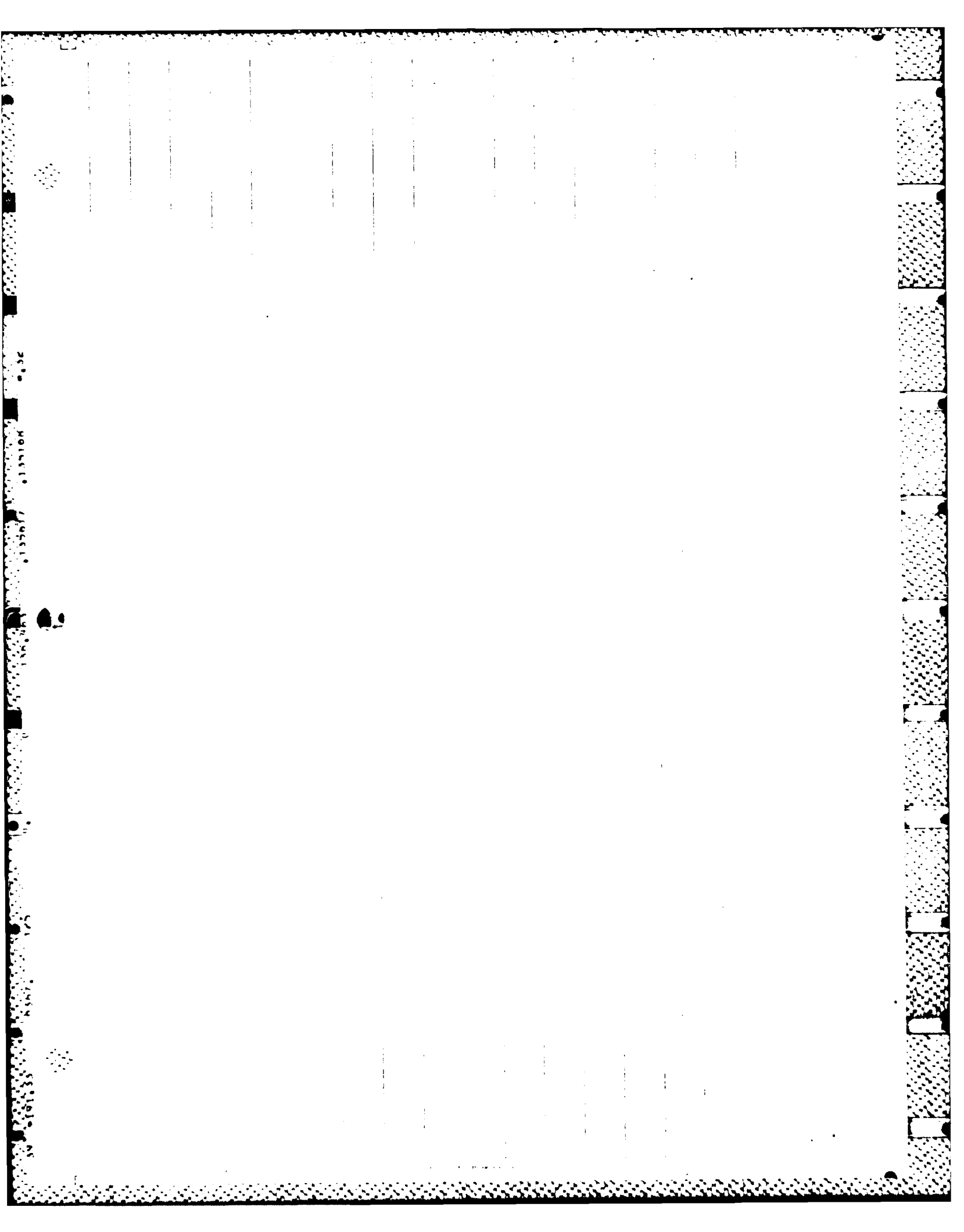
QTTP=10, MINIMUM WALL THICKNESS=1.25 IN. RU = 35

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 35.00

PERMANENT SET OF PILE = .0356 INCHES
 NUMBER OF H/CMS PER FOOT = 336.92
 TOTAL INTERVALS = 137

SEC	ELEV FT	MAX C STRESS LBS/SQ.IN.	TIME H	MAX T STRESS LBS/SQ.IN.	TIME I	AREA SQ.IN.	UMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1781759.	31	0.	74	1,000	1.200510	1.180993	-0.66
2	0.00	1482024.	41	0.	0	1,000	.788225	.752172	-0.30
3	120.00	10488.	43	0.	0	136.463	.774077	.756565	-0.34
4	111.00	10920.	46	0.	0	136.463	.766360	.726966	-0.39
5	102.00	11003.	48	0.	0	136.463	.757970	.716608	-0.47
6	93.00	11161.	51	0.	0	136.463	.749476	.705634	-0.57
7	84.00	11341.	53	0.	0	136.463	.741183	.693901	-0.70
8	75.00	11533.	56	0.	0	136.463	.733225	.681609	-0.84
9	66.00	11715.	58	0.	0	136.463	.725806	.668721	-1.01
10	57.00	11879.	60	0.	0	136.463	.718099	.655258	-1.18
11	48.00	12012.	62	0.	0	136.463	.709893	.641313	-1.35
12	39.00	12117.	64	0.	0	136.463	.701021	.626845	-1.51
13	30.00	10242.	67	0.	0	162.578	.691370	.611863	-1.65
14	21.67	10358.	69	0.	0	162.578	.681052	.599407	-1.73
15	13.33	10450.	71	0.	0	162.578	.673714	.587356	-1.80
16	5.00	10566.	73	0.	0	162.578	.663257	.574608	-1.85
17	-3.33	10635.	75	0.	0	162.578	.651550	.561600	-1.88
18	-11.67	10636.	78	0.	0	162.578	.638581	.548343	-1.89
19	-20.00	10620.	80	0.	0	162.578	.624308	.534857	-1.90
20	-28.33	10573.	82	0.	0	162.578	.608644	.521012	-1.91
21	-36.67	10493.	84	0.	0	162.578	.591736	.506647	-1.94
22	-45.00	10387.	87	0.	0	162.578	.573520	.491593	-1.99
23	-53.33	10274.	90	0.	0	162.578	.554098	.475692	-2.05
24	-61.67	10184.	92	0.	0	162.578	.533648	.458872	-2.08
25	-70.00	11978.	95	0.	0	136.463	.485718	.441301	-2.05
26	-78.67	11795.	97	0.	0	136.463	.449094	.396222	-1.99
27	-87.33	11571.	99	0.	0	136.463	.42716	.373285	-1.91
28	-96.00	11308.	102	0.	0	136.463	.405850	.350297	-1.84
29	-104.67	10998.	104	0.	0	136.463	.377799	.327332	-1.76
30	-113.33	10600.	106	0.	0	136.463	.348465	.304310	-1.70
31	-122.00	10099.	108	0.	0	136.463	.318416	.281138	-1.63
32	-130.67	9787.	113	0.	0	136.463	.288417	.258012	-1.50
33	-139.33	9750.	116	0.	0	136.463	.259263	.235668	-1.28
34	-148.00	9514.	118	0.	0	136.463	.231088	.214599	-1.11
35	-156.67	9056.	117	0.	0	136.463	.203331	.194150	-0.95
36	-165.33	8542.	119	0.	0	136.463	.178446	.174065	-0.76
37	-174.00	7977.	124	0.	0	136.463	.151116	.148516	-0.59
38	-182.67	7450.	121	0.	0	136.463			



PROJ 5 30-IN. DIAMETER PILES 3-PTIE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER

QTTP=10, MINIMUM WALL THICKNESS=1.25 IN. MU = 35

TABLE 9 -- RESISTANCE-HLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 35.00

BLOWS/FT.	RESISTANCE DYNAMIC PT	MAX C STRESS	SFG	MAX T STRESS	SEG
TOTAL TONS	FORCE-TONS	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	
2.54	50%	48.42	11	9883.	25
4.10	100%	92.09	12	8050.	25
6.32	150%	131.44	12	6996.	25
9.05	200%	167.03	12	5478.	25
11.84	250%	199.19	12	4069.	26
15.43	300%	228.29	12	3518.	A
17.91	350%	254.65	12	2437.	A
20.30	400%	278.52	12	1457.	27
23.09	450%	300.11	12	574.	27
26.37	500%	319.61	12	0.	39
30.27	550%	337.19	12	0.	39
35.00	600%	353.01	12	0.	39
40.41	650%	367.51	12	0.	39
48.11	700%	380.14	12	0.	39
57.53	750%	391.78	12	0.	39
69.98	800%	402.04	12	0.	39
87.06	850%	410.80	12	0.	39
111.64	900%	418.11	12	0.	39
140.29	950%	424.68	12	0.	39
212.69	1000%	430.44	12	0.	39
336.92	1050%	434.42	12	0.	39

PRDH 5 3/4 IN. DIAMETER PILES SOFT STRUCTURE
200FT PENETRATION -- VULCAN DRUM HAMMER

OTTP=10, MINIMUM WALL THICKNESS=1.25 IN. RU = 55

TABLE 10 -- SPECIFIC ALLOW DATA

TIP RESISTANCE PERCENTAGE = 35.00

ALOWS PER FOOT	RESISTANCE TONS
149.20	950.
212.60	1000.
243.07	1015.
289.30	1035.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PILE STRUCTURE
 NC CLELLAND REPORT DATA FOR ACR 3-PILE STRUCTURE -- HITTING 1
 APRIL 19 1974

PROB
 6

36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 CTYPE 30, MINIMUM WALL THICKNESS 1.25 IN. RU = 50

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED PLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 1
 ULTIMATE RESISTANCE INCREMENT (TONS) 275.
 MAX PLOWS FOR RESISTANCE CURVE (HPF) 50.0
 SPECIFIED SEGMENT LENGTH (FT) 300.
 -0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) -0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(THD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS = 1

NUMBER OF SECTIONS ALLOWED 0
 LENGTH OF FREE STANDING PIECE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	150.	190	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE • JSTOE .15
 POINT DAMPING RESISTANCE • JPOINT .15
 SOIL QUAKE FOR SIDE • OSIDE .10
 SOIL QUAKE FOR POINT • OPOINT .30

TIP RESISTANCE PERCENTAGE

50.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
500.	25.

P000 200FT PENETRATION -- 50-IN. DIAMETER PILES 3-PILE STRUCTURE
 -- VULCAN ODN HAMMER

OTTP=30, MINIMUM WALL THICKNESS=1.25 IN. QU = 50

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLYV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RS/TTU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	95.00	0.00	4179.19	136.46	1.00	36642910.
7	82.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	44.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-24.33	0.00	4610.13	162.58	1.00	47147562.
21	-30.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-55.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4024.40	136.46	1.00	38052252.
26	-78.67	0.00	4024.40	136.46	1.00	38052252.
27	-87.33	0.00	4024.40	136.46	1.00	38052252.
28	-95.00	0.00	4024.40	136.46	1.00	38052252.
29	-104.67	0.00	4024.40	136.46	1.00	38052252.
30	-113.33	0.00	4024.40	136.46	1.00	38052252.
31	-122.00	0.00	4024.40	136.46	1.00	38052252.
32	-130.67	0.00	4024.40	136.46	1.00	38052252.
33	-139.33	0.00	4024.40	136.46	1.00	38052252.
34	-148.00	0.00	4024.40	136.46	1.00	38052252.
35	-156.67	0.00	4024.40	136.46	1.00	38052252.
36	-165.33	0.00	4024.40	136.46	1.00	38052252.
37	-174.00	0.00	4024.40	136.46	1.00	38052252.
38	-182.67	0.00	4024.40	136.46	1.00	38052252.
39	-191.33	1000.00	4024.40	136.46	1.00	38052252.

PROJ 200 FT PENETRATOR 36 IN. DIAMETER PILES 5-PTIF STRUCTURE
 200 FT PENETRATOR 36 IN. DIAMETER PILES 5-PTIF STRUCTURE

OTITE, 30. MINIMUM WALL THICKNESS=1.25 IN. RU = 50

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 50.00

PERMANENT SET OF PTIF = .0306 INCHES

NUMBER OF BLOWS PER FOOT = 392.41

TOTAL INTERVALS = 141

SEG	ELEV FT	MAX C. STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	ARFA SQ. IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1781750.	31	0.	74	1.000	1.275522	1.205312	-.45
2	0.00	1482020.	41	0.	0	1.000	.812861	.796538	-.09
3	120.00	10888.	43	0.	0	136.463	.799150	.783940	-.10
4	111.00	10920.	46	0.	0	136.463	.791164	.777476	-.13
5	102.00	11003.	48	0.	0	136.463	.782992	.770172	-.17
6	93.00	11161.	51	0.	0	136.463	.775081	.762013	-.24
7	84.00	11341.	53	0.	0	136.463	.767920	.753030	-.32
8	75.00	11535.	56	0.	0	136.463	.762186	.743296	-.43
9	66.00	11715.	58	0.	0	136.463	.757298	.732855	-.54
10	57.00	11878.	60	0.	0	136.463	.752556	.721852	-.68
11	48.00	12008.	62	0.	0	136.463	.747669	.710350	-.82
12	39.00	12105.	64	0.	0	136.463	.742445	.698502	-.96
13	30.00	12164.	67	0.	0	162.578	.736588	.686389	-1.07
14	21.67	12285.	69	0.	0	162.578	.731299	.678837	-1.13
15	13.33	12364.	71	0.	0	162.578	.725213	.667244	-1.17
16	5.00	12438.	73	0.	0	162.578	.718142	.657676	-1.16
17	-3.33	12464.	75	0.	0	162.578	.710017	.648248	-1.13
18	-11.67	12433.	77	0.	0	162.578	.700690	.639032	-1.11
19	-20.00	12381.	79	0.	0	162.578	.690164	.629963	-1.13
20	-28.33	12312.	82	0.	0	162.578	.678440	.620902	-1.13
21	-36.67	12231.	84	0.	0	162.578	.665509	.611485	-1.18
22	-45.00	12132.	86	0.	0	162.578	.651543	.601724	-1.24
23	-53.33	12004.	89	0.	0	162.578	.636555	.591240	-1.29
24	-61.67	11845.	91	0.	0	162.578	.620863	.580255	-1.31
25	-70.00	11616.	94	0.	0	136.463	.604964	.568923	-1.28
26	-78.67	11316.	96	0.	0	136.463	.588655	.554716	-1.23
27	-87.33	11586.	98	0.	0	136.463	.569592	.540502	-1.17
28	-96.00	11436.	101	0.	0	136.463	.552054	.526314	-1.13
29	-104.67	11268.	103	0.	0	136.463	.533602	.511900	-1.14
30	-113.33	10970.	105	0.	0	136.463	.514645	.496806	-1.18
31	-122.00	10556.	108	0.	0	136.463	.495862	.480865	-1.21
32	-130.67	9915.	107	0.	0	136.463	.477755	.464258	-1.18
33	-139.33	9381.	113	0.	0	136.463	.459167	.446923	-1.17
34	-148.00	9251.	116	0.	0	136.463	.439553	.428638	-1.12
35	-156.67	8963.	117	0.	0	136.463	.419005	.409713	-1.00
36	-165.33	8512.	117	0.	0	136.463	.397252	.390606	-.85
37	-174.00	8249.	124	0.	0	136.463	.374728	.371281	-.71
38	-182.67	8100.	127	0.	0	136.463	.352645	.341218	-.52

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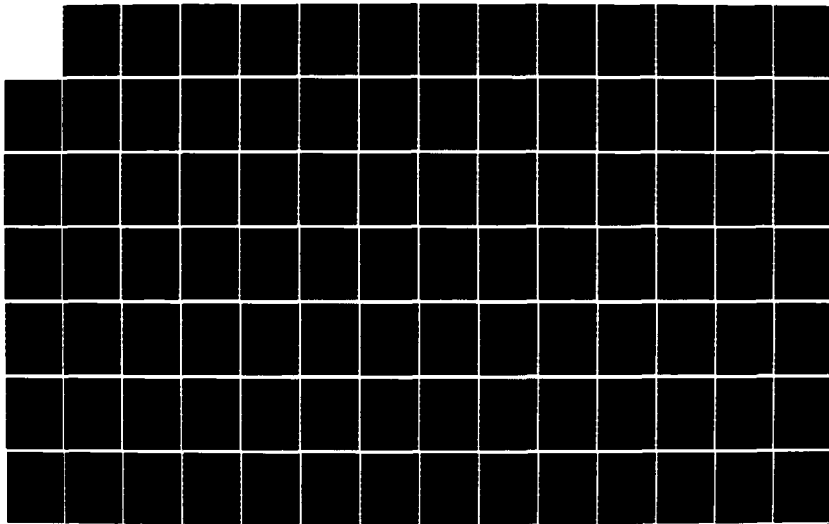
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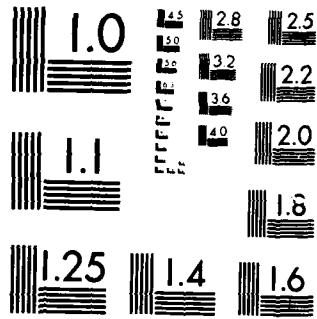
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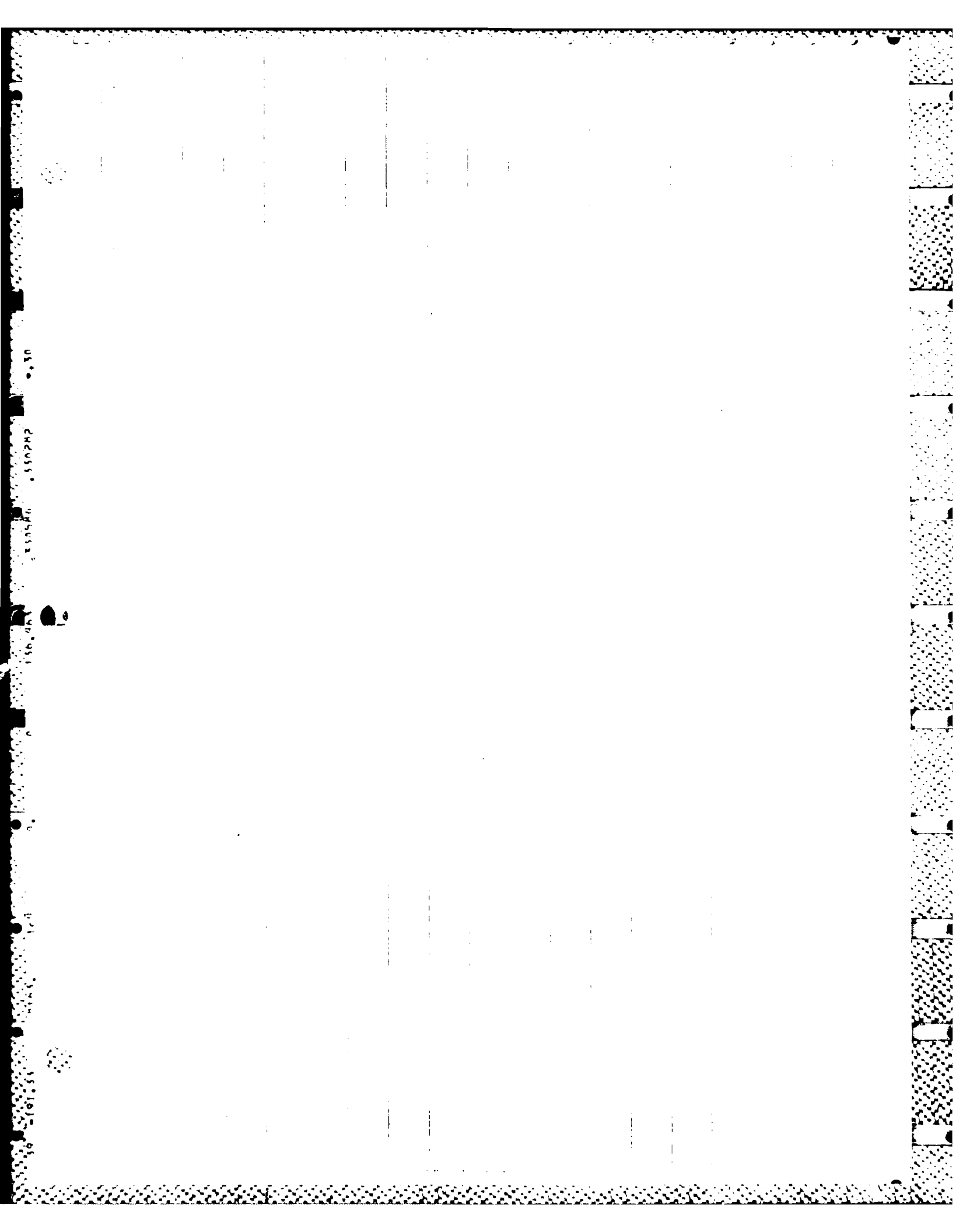
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MICROCOPY RESOLUTION TEST CHART
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PRDA 36-IN. DIAMETER PILES (PILE STRUCTURE)
 200T PENETRATION -- VULCAN 030 HAMMER

OTTE, 30, MINIMUM WALL THICKNESS 1.25 IN. RII = 50

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 50.00		TIP RESISTANCE PERCENTAGE = 50.00		TIP RESISTANCE PERCENTAGE = 50.00		TIP RESISTANCE PERCENTAGE = 50.00	
BLOWS/FT.	RESISTANCE DYNAMIC PT	MAX C STRESS	SEG	MAX T STRESS	SEG	MAX C STRESS	SEG
TOTAL	TOTAL	LR/SQ. IN. MIN.	LR/SQ. IN. MIN.	LR/SQ. IN. MIN.	LR/SQ. IN. MIN.	LR/SQ. IN. MIN.	LR/SQ. IN. MIN.
2.45	50.	69.04	11	11744.	11	9772.	25
4.04	100.	131.11	12	12047.	12	4273.	25
6.55	150.	144.92	12	12049.	12	6750.	25
10.01	200.	237.13	12	12090.	12	5368.	25
13.45	250.	242.53	12	12091.	12	4078.	25
19.36	300.	323.47	12	12042.	12	2955.	9
22.66	350.	360.30	12	12094.	12	2140.	9
26.65	400.	393.66	12	12005.	12	963.	25
31.57	450.	423.97	12	12094.	12	104.	27
37.77	500.	451.44	12	12097.	12	0.	39
45.81	550.	475.95	12	12099.	12	0.	39
56.60	600.	497.54	12	12090.	12	0.	39
71.79	650.	519.05	12	12100.	12	0.	39
94.59	700.	539.55	12	12101.	12	0.	39
132.12	750.	547.64	12	12103.	12	0.	39
204.11	800.	559.94	12	12104.	12	0.	39
392.41	850.	556.99	12	12105.	12	0.	39

FROM 200FT PENETRATION -- 50-IN. DIAMETER PILES 4-PILE STRUCTURE
 -- VULCAN OGD HAMMER
 Q TIP = 30,000 LBS MIN WALL THICKNESS = 1.25 IN. RUI = 50

TABLE 10 -- SPECIFIED MIN. DATA

TIP RESISTANCE PERCENTAGE =	50.00
ALLOW PER FOOT	RESISTANCE TONS
132.12	750
204.11	800
232.69	812
293.00	831

JVJ0JVC. 04/20/76. UNITED COMPUTING* 67. APTX/SI. H.0.24

09.1A.44SPIL.CM100.1000.					
09.1A.44SFL	64	0.000			
09.1A.453AC3400CR0023.27771000C 1M					
09.1A.45.04/20/76.JVJ0JVC					
09.1A.45.HFL.40000.					
09.1A.45SFL	392	0.001			
09.1A.45SFL	14344	0.001			
09.1A.45.WAP.OFF.					
09.1A.45SFL	256	0.001			
09.1A.45.GET.PILR(CR0024)					
09.1A.49.READY = PTLA					
09.18.49SFL	4096	0.002	0	0.	
09.1A.49SFI	72	1			
09.1A.49.PTLA.					
09.1A.49SFL00	16344	0.002			
09.1A.50SFL01	14364	0.144	140	A	
09.1A.50.PL REQUIMED TO LOAD			36370H	(15608)	
09.1A.51.PL REQUIMED TO EXECUTE			34000H	(14336)	
09.1A.51SFL	14344	0.144			
09.19.57.END PTLDR					
09.19.57.COST.					
09.19.57SFL	14336	52.444	16A	1P	
09.19.5A.			SERVICE UNITS=	137.6	
09.19.5A.			JOB COSTS=	34.40	
09.19.58SFL	1228H	52.442	7	5	
09.19.58.EXIT.					
09.19.58SJT00	2368	52.442			
09.19.58.			*FL*	*CPU SEC.	*DISC PRUS* DISC ACC
09.19.58.OP.F.			*PRUS*P.F.	*ACC	*TAPE PRUS* TAPE ACC

Pile Driving Resistance Curves

Pile Diameter	- 30 in.
Minimum Wall Thickness	- .75 in.
	- 1.25 in.
Penetration	- 150 ft.
Hammer	- Vulcan 040
Quake Factor, tip	- .025 in.
	- .10 in.
	- .30 in.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACHR 3-PILE STRUCTURE -- RORING 1
 APRIL 19 1974

PROB
 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTYPE.025, MINIMUM WALL THICKNESS=.75 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED ALLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 BPF FOR STRESS OUTPUT OPTION 1
 ULTIMATE RESISTANCE INCREMENT (TONS) 275.
 MAX BLOWS FOR RESISTANCE-HLOW CURVE (RPF) 50.0
 SPECIFIED SEGMENT LENGTH (FT) 300.
 =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TOD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	20000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	30.	240	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE - JSIDE .15
 POINT DAMPENING RESISTANCE - JPONT .15
 SOIL QUAKE FOR SIDE - OSIDE .10
 SOIL QUAKE FOR POINT - OPOINT .03

TIP RESISTANCE PERCENTAGE

14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 1 3/4-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

QTTPS, 0.25, MINIMUM WALL THICKNESS, 7.5 IN. RU = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLYV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2826.21	83.06	1.00	20071479.
32	-130.00	0.00	2826.21	83.06	1.00	20071479.
33	-140.00	1000.00	2826.21	83.06	1.00	20071479.

PROB 1 36-IN. DIAMETER PILLS 3-PTIF STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

QTIPR, 0.25, MINIMUM WALL THICKNESS, .75 IN. MU = 14

TABLE 8 -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILF = .0367 INCHES

NUMBER OF BLOWS PER FOOT = 327.21

TOTAL INTERVALS = 131

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	1781868.	34	0.	81	1,000	1,171165	1,170179	-.22
2	0.00	1481874.	45	0.	0	1,000	.760521	.702812	-.97
3	120.00	10887.	47	0.	0	136,443	.746588	.681076	-1.14
4	111.00	10926.	50	0.	0	136,443	.738074	.669082	-1.33
5	102.00	11004.	53	0.	0	136,443	.728692	.654424	-1.51
6	93.00	11160.	56	0.	0	136,443	.718454	.639069	-1.67
7	84.00	11341.	58	0.	0	136,443	.707286	.623030	-1.81
8	75.00	11535.	61	0.	0	136,443	.695039	.606445	-1.94
9	66.00	11714.	63	0.	0	136,443	.681653	.589162	-2.07
10	57.00	11884.	66	0.	0	136,443	.666971	.571261	-2.20
11	48.00	12035.	68	0.	0	136,443	.650746	.552548	-2.32
12	39.00	12186.	71	0.	0	136,443	.632767	.53447	-2.45
13	30.00	12341.	74	0.	0	162,578	.612687	.512267	-2.58
14	21.67	12604.	77	0.	0	162,578	.595385	.495080	-2.67
15	13.33	12893.	79	0.	0	162,578	.575340	.476832	-2.74
16	5.00	13215.	82	0.	0	162,578	.553536	.457504	-2.78
17	-3.33	13481.	84	0.	0	162,578	.529821	.437089	-2.77
18	-11.67	13656.	87	0.	0	162,578	.504088	.415795	-2.70
19	-20.00	13756.	90	0.	0	162,578	.477702	.393761	-2.57
20	-28.33	13758.	92	0.	0	162,578	.449681	.371106	-2.40
21	-36.67	13808.	94	0.	0	162,578	.42081	.347969	-2.25
22	-45.00	13806.	97	0.	0	162,578	.389620	.324248	-2.10
23	-53.33	13910.	100	0.	0	162,578	.357667	.300292	-1.93
24	-61.67	13933.	104	0.	0	162,578	.324909	.274236	-1.78
25	-70.00	12185.	106	0.	0	136,443	.291907	.242292	-1.61
26	-78.33	11642.	109	0	0	136,443	.254743	.224633	-1.44
27	-86.67	10633.	110	0	0	136,443	.220241	.198400	-1.25
28	-95.00	9418.	112	0	0	136,443	.186678	.173932	-1.15
29	-103.33	8093.	114	0.	0	136,443	.164276	.151185	-1.01
30	-111.67	6734.	117	0.	0	136,443	.136447	.130587	-.84
31	-120.00	8345.	118	0.	0	136,443	.118065	.112567	-.67
32	-130.00	6226.	120	0.	0	136,443	.084694	.083694	-.50
33	-140.00	4791.	117	0.	0	136,443	.061674	.061513	-.17

PROB 1 30-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER

OTYPE, 0.25-MINIMUM WALL THICKNESS .75 IN. RU = 14

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS/FT.	RESISTANCE DYNAMIC PT	MAX C STRESS	SEG MA T STRESS	SEG
TOTAL-TONS	FORCE-TONS	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	NO.
2.92	50%	19.65	1148A.	12
4.34	100%	37.37	1207B.	11
6.42	150%	53.44	1209A.	10
9.14	200%	68.06	1210Z.	9
11.68	250%	81.36	1210S.	8
15.38	300%	93.45	12109.	8
17.07	350%	104.43	12113.	7
18.98	400%	114.41	12116.	7
21.15	450%	123.51	12120.	21
23.65	500%	131.71	12.23.	45.
26.54	550%	139.10	12127.	0.
29.92	600%	145.74	12131.	0.
33.92	650%	151.52	12135.	0.
38.69	700%	156.58	12140.	0.
44.46	750%	161.01	12144.	0.
51.56	800%	164.90	12148.	0.
60.44	850%	168.21	12153.	0.
71.73	900%	170.68	12157.	0.
86.38	950%	172.13	12161.	0.
105.94	1000%	174.56	12165.	0.
132.05	1050%	179.44	12169.	0.
164.60	1100%	184.89	12174.	0.
204.92	1150%	190.52	12178.	0.
256.51	1200%	195.05	12182.	0.
327.21	1250%	198.96	12186.	0.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

OTTR=025, MINIMUM WALL THICKNESS=75 IN. RU = 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PFR FOOT	RESISTANCE TONS
132.05	1050.
204.92	1150.
256.51	1200.
296.68	1231.

HAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACHR 3-PILE STRUCTURE -- HURTING 1
 APRIL 19 1976

PROB 2
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTIPS, 10, MINIMUM WALL THICKNESS, .75 IN. RU = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED RLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX RLOWs FOR RESISTANCE-RLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (80 IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TOD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	50.	240	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE = JSIDE .15
 POINT DAMPING RESISTANCE = JPDNT .15
 SOIL SHAKE FOR SIDE = OSIDE .10
 SOIL SHAKE FOR POINT = OPNT .10

TIP RESISTANCE PERCENTAGE

35.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 2 150FT PENETRATION -- 48-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN ODO HAMMER

OTTP=10, MINIMUM WALL THICKNESS=.75 IN. RI = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2700000.
2	0.00	1000.00	27400.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4010.13	162.58	1.00	47147562.
14	21.67	0.00	4010.13	162.58	1.00	47147562.
15	13.33	0.00	4010.13	162.58	1.00	47147562.
16	5.00	0.00	4010.13	162.58	1.00	47147562.
17	-3.33	0.00	4010.13	162.58	1.00	47147562.
18	-11.67	0.00	4010.13	162.58	1.00	47147562.
19	-20.00	0.00	4010.13	162.58	1.00	47147562.
20	-28.33	0.00	4010.13	162.58	1.00	47147562.
21	-36.67	0.00	4010.13	162.58	1.00	47147562.
22	-45.00	0.00	4010.13	162.58	1.00	47147562.
23	-53.33	0.00	4010.13	162.58	1.00	47147562.
24	-61.67	0.00	4010.13	162.58	1.00	47147562.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2826.21	83.06	1.00	20071879.
32	-130.00	0.00	2826.21	83.06	1.00	20071879.
33	-140.00	1000.00	2826.21	83.06	1.00	20071879.

PROB 2 36-IN. DIAMETER PILES T-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER

OTYPE=10, MINIMUM WALL THICKNESS=.75 IN. RU = 35

TABLE 6 -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 55.00

PERMANENT SET OF PILE = .0250 INCHES

NUMBER OF BLOWS PER FOOT = 480.92

TOTAL INTERVALS = 135

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	RI	TIME N	AREA SQ. IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1781868.	34	0.	0	1.000	1.000	1.182726	1.179973	-.33
2	0.00	1481874.	45	0.	0	1.000	1.000	.771284	.722784	-.56
3	120.00	10887.	47	0.	0	136.463	136.463	.757458	.705332	-.67
4	111.00	10926.	50	0.	0	136.463	136.463	.749159	.694071	-.80
5	102.00	11004.	53	0.	0	136.463	136.463	.740268	.682530	-.93
6	93.00	11160.	56	0.	0	136.463	136.463	.730862	.670786	-1.04
7	84.00	11341.	58	0.	0	136.463	136.463	.720992	.658660	-1.15
8	75.00	11535.	61	0.	0	136.463	136.463	.710650	.646654	-1.25
9	66.00	11713.	63	0.	0	136.463	136.463	.699831	.634124	-1.35
10	57.00	11881.	66	0.	0	136.463	136.463	.688300	.621157	-1.46
11	48.00	12022.	68	0.	0	136.463	136.463	.675691	.607618	-1.59
12	39.00	12147.	71	0.	0	136.463	136.463	.661726	.593234	-1.73
13	30.00	10303.	73	0.	0	162.578	162.578	.646256	.577842	-1.88
14	21.67	10455.	76	0.	0	162.578	162.578	.632816	.564897	-2.00
15	13.33	10641.	78	0.	0	162.578	162.578	.618012	.550794	-2.10
16	5.00	10851.	81	0.	0	162.578	162.578	.601953	.535559	-2.18
17	-3.33	11007.	83	0.	0	162.578	162.578	.584622	.519332	-2.20
18	-11.67	11092.	86	0.	0	162.578	162.578	.566150	.502285	-2.16
19	-20.00	11155.	89	0.	0	162.578	162.578	.546474	.484615	-2.11
20	-28.33	11132.	91	0.	0	162.578	162.578	.525528	.466299	-2.06
21	-36.67	11030.	93	0.	0	162.578	162.578	.503193	.447276	-1.99
22	-45.00	10810.	96	0.	0	162.578	162.578	.479284	.427583	-1.91
23	-53.33	10487.	98	0.	0	162.578	162.578	.453875	.407340	-1.83
24	-61.67	10190.	102	0.	0	162.578	162.578	.427290	.386498	-1.81
25	-70.00	11795.	106	0.	0	136.463	136.463	.400516	.364961	-1.77
26	-78.53	11551.	108	0.	0	136.463	136.463	.369013	.338745	-1.74
27	-86.67	11273.	109	0.	0	136.463	136.463	.338423	.312195	-1.71
28	-95.00	10800.	112	0.	0	136.463	136.463	.308388	.285612	-1.58
29	-103.53	9658.	114	0.	0	136.463	136.463	.278628	.259776	-1.41
30	-111.67	8934.	118	0.	0	136.463	136.463	.248857	.230794	-1.24
31	-120.00	13671.	123	0.	0	83.056	83.056	.214544	.210714	-1.01
32	-130.00	12207.	123	0.	0	83.056	83.056	.168282	.166026	-.59
33	-140.00	10163.	120	0.	0	83.056	83.056	.124952	.124945	-.16

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION == VULCAN OGD HAMMER

OTIPS, 10, MINIMUM WALL THICKNESS=.75 IN. HUI = 35

TABLE 9 == RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 55.00

BLOWS/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS FORCE-TONS	MAX C STRESS LBS/SQ.IN. NO.	SFG LBS/SQ.IN. NO.	MAX T STRESS LBS/SQ.IN. NO.	SEC
2.91	50	48.98	11702.	8003.	12
4.43	100	92.92	12090.	6900.	11
6.72	150	132.58	12094.	5599.	10
9.71	200	168.42	12097.	4369.	10
12.77	250	200.40	12100.	3276.	9
16.85	300	230.10	12103.	2303.	9
19.01	350	256.67	12106.	1448.	8
21.51	400	280.43	12108.	333.	19
24.44	450	302.44	12111.	0.	33
27.93	500	322.88	12114.	0.	33
32.13	550	340.96	12532.	0.	33
37.26	600	357.18	12978.	0.	33
43.65	650	371.39	13348.	0.	33
51.76	700	383.52	13640.	0.	33
62.32	750	393.41	13809.	0.	33
76.52	800	401.49	13971.	0.	33
96.50	850	408.02	14041.	0.	33
126.36	900	413.66	14076.	0.	33
174.81	950	418.15	14064.	0.	33
264.71	1000	420.31	13941.	0.	33
480.92	1050	422.06	13671.	0.	33

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

GTIP=10, MINIMUM WALL THICKNESS=.75 IN. PU = 55

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 55.00

BLOWS PER FOOT	RESISTANCE TONS
126.36	900.
194.33	964.
244.71	1000.
247.55	1000.

HAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACUM 3-PILE STRUCTURE -- HRRING 1
 APRIL 19 1976

PROB 3
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTIPS, 30. MINIMUM WALL THICKNESS=.75 IN. RUI = 50

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED BLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX BLOWS FOR RESISTANCE INCREMENT (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) 0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) 0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1
 MATERIAL TYPE 1
 (TON) 36.000
 UNIT WT. (PCF) 490.0
 MODULUS (PST) 20000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	50.	240	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE = JSIDE .15
 POINT DAMPENING RESISTANCE = JPOINT .15
 SOIL SHAKE FOR SIDE = SSIDE .10
 SOIL SHAKE FOR POINT = SPOINT .30

TIP RESISTANCE PERCENTAGE

50.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE(FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER	
				TOP	BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	50.	190	240
4	1	.750	50.	240	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE = JSIDE .15
 POINT DAMPENING RESISTANCE = JPONT .15
 SOIL GRADE FOR SIDE = GSIDE .10
 SOIL GRADE FOR POINT = GPPOINT .30

TIP RESISTANCE PERCENTAGE
 50.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 3 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN OUN HAMMER

QTIPs, 30, MINIMUM WALL THICKNESS=.75 IN. MU = 50

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEFF RSTITU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	3869.62	136.46	1.00	39574342.
25	-70.00	0.00	3869.62	136.46	1.00	39574342.
26	-78.33	0.00	3869.62	136.46	1.00	39574342.
27	-86.67	0.00	3869.62	136.46	1.00	39574342.
28	-95.00	0.00	3869.62	136.46	1.00	39574342.
29	-103.33	0.00	3869.62	136.46	1.00	39574342.
30	-111.67	0.00	3869.62	136.46	1.00	39574342.
31	-120.00	0.00	2826.21	83.06	1.00	20071879.
32	-130.00	0.00	2826.21	83.06	1.00	20071879.
33	-140.00	1000.00	2826.21	83.06	1.00	20071879.

PROB 3 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

QTIP = .30, MINIMUM WALL THICKNESS = .75 IN. MU = 50

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 50.00
 PERMANENT SPT OF PILE = .0321 INCHES
 NUMBER OF BLOWS PER FOOT = 373.31
 TOTAL INTERVALS = 140

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	QMAX(M) IN.	D(M) IN.	V(M) FT/SFC
1	0.00	178168.	34	0.	R1	1.000	1.204296	1.198202	-0.03
2	0.00	1481874.	45	0.	0	1.000	.792178	.757744	-0.11
3	120.00	10887.	47	0.	0	136.463	.778429	.742907	-0.15
4	111.00	10926.	50	0.	0	136.463	.770316	.734703	-0.19
5	102.00	11004.	53	0.	0	136.463	.761851	.726570	-0.24
6	93.00	11160.	56	0.	0	136.463	.753274	.718625	-0.30
7	84.00	11341.	58	0.	0	136.463	.744813	.710900	-0.35
8	75.00	11535.	61	0.	0	136.463	.736684	.703425	-0.42
9	66.00	11713.	63	0.	0	136.463	.728938	.696071	-0.48
10	57.00	11878.	66	0.	0	136.463	.720722	.688699	-0.54
11	48.00	12014.	68	0.	0	136.463	.712020	.681221	-0.60
12	39.00	12119.	70	0.	0	136.463	.702830	.673575	-0.66
13	30.00	10248.	73	0.	0	162.578	.692328	.665626	-0.74
14	21.67	10344.	75	0.	0	162.578	.684165	.658099	-0.81
15	13.33	10467.	78	0.	0	162.578	.675058	.651804	-0.89
16	5.00	10589.	80	0.	0	162.578	.666471	.643886	-0.97
17	-3.33	10661.	82	0.	0	162.578	.658982	.635128	-1.03
18	-11.67	10674.	85	0.	0	162.578	.648975	.625606	-1.06
19	-20.00	10660.	87	0.	0	162.578	.636341	.615553	-1.04
20	-28.33	10624.	90	0.	0	162.578	.624882	.605035	-1.07
21	-36.67	10531.	92	0.	0	162.578	.612465	.593864	-1.04
22	-45.00	10347.	95	0.	0	162.578	.598959	.581892	-1.13
23	-53.33	10064.	96	0.	0	162.578	.584568	.568925	-1.20
24	-61.67	9722.	99	0.	0	162.578	.568833	.554682	-1.29
25	-70.00	11123.	101	0.	0	136.463	.554514	.539199	-1.33
26	-78.33	10573.	104	0.	0	136.463	.535578	.519495	-1.37
27	-86.67	10033.	107	0.	0	136.463	.515504	.499735	-1.40
28	-95.00	9661.	111	0.	0	136.463	.494100	.478717	-1.37
29	-103.33	9163.	112	0.	0	136.463	.471344	.457166	-1.26
30	-111.67	8619.	116	0.	0	136.463	.447315	.435561	-1.11
31	-120.00	15495.	122	0.	0	136.463	.422142	.414109	-0.94
32	-130.00	13202.	125	0.	0	136.463	.374954	.372811	-0.60
33	-140.00	12524.	126	0.	0	136.463	.332145	.332117	-0.18

PROB 3 1/2 IN. DIAMETER PILLS TAPPIE STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

OTIP=30, MINIMUM WALL THICKNESS=.75 IN. RU = 50

TABLE 9 -- RESISTANCE-DYNAMIC CURVE DATA

TIP RESISTANCE PERCENTAGE %	50.00	RESISTANCE DYNAMIC PT		MAX C STRESS	SEG	MAX T STRESS	SEG
		TOTAL-TONS	FORCE-TONS	LBS/SQ.IN. (N)	LHS/SQ.IN. (N)	LBS/SQ.IN. (N)	NO.
2.83	50%	69.84		11695.	12	6388.	12
4.56	100%	152.29		12089.	12	6850.	11
7.29	150%	188.76		12092.	12	5380.	10
10.87	200%	239.33		12094.	12	4074.	10
15.07	250%	284.07		12096.	12	2874.	10
21.32	300%	325.63		12098.	12	1837.	6
25.03	350%	358.55		12100.	12	1310.	6
29.59	400%	389.65		12102.	12	908.	5
35.33	450%	417.45		12501.	31	214.	12
42.77	500%	441.95		12907.	31	0.	33
52.73	550%	462.92		13285.	31	0.	33
66.79	600%	480.45		13514.	31	0.	33
87.93	650%	499.22		13641.	31	0.	33
122.85	700%	513.92		13696.	31	0.	33
190.74	750%	524.18		13711.	31	0.	33
373.31	800%	520.10		14645.	31	0.	33

PROB 3 36-IN. DIAMETER PILES TESTED STRUCTURE
150FT PENETRATION -- VULCAN ODD HAMMER

QTIP, 30. MINIMUM WALL THICKNESS, 75 T. MU = 50

TABLE 10 -- SPECIFIED ALLOW DATA

TIP RESISTANCE PERCENTAGE = 50.00

ALOWS PER FOOT	RESISTANCE TONS
144.02	720.
190.74	750.
228.72	766.
294.68	785.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACMH 3-PILE STRUCTURE -- BORING 1
 APRIL 19 1976

PROB 4
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 DTTP, 0.25, MINIMUM WALL THICKNESS 1.25 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED ALLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX ALLOWS FOR RESISTANCE-BLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) 0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) 0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	270000.00
2	1000.00	27000.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1
 MATERIAL TYPE (TUB) UNIT WT. (PCF) MODULUS (PST)
 1 36.000 490.0 29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 3
 NUMBER OF SECTIONS CHANGED 0

NUMBER OF SPITTINGS ALLOWED 120,000
 LENGTH OF FREE STANDING PILE(FT) 0

SECTION NUMBER	MATERIAL TYPE	PILE THICKNESS (IN)	LENGTH (FT)	STATION NUMBER	
				TOP	BOTTOM
1	1	1,250	90	0	90
2	1	1,500	100	90	190
3	1	1,250	40	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE - JSIDE .15
 POINT DAMPING RESISTANCE - JPONT .15
 SOIL SHAKE FOR SIDE .10
 SOIL SHAKE FOR POINT .03

TIP RESISTANCE PERCENTAGE

14,000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150	25
200	25
250	25
300	25

PROB

4 36 IN. DIAMETER PILES 3-PILE STRUCTURE
150 FT PENETRATION -- VULCAN 040 HAMMER

OTTP=0.25, MINIMUM WALL THICKNESS=1.25 IN. RI = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	PLEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTYTH	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.54	1.00	47147562.
14	21.67	0.00	4610.13	162.54	1.00	47147562.
15	13.33	0.00	4610.13	162.54	1.00	47147562.
16	5.00	0.00	4610.13	162.54	1.00	47147562.
17	-3.33	0.00	4610.13	162.54	1.00	47147562.
18	-11.67	0.00	4610.13	162.54	1.00	47147562.
19	-20.00	0.00	4610.13	162.54	1.00	47147562.
20	-28.33	0.00	4610.13	162.54	1.00	47147562.
21	-36.67	0.00	4610.13	162.54	1.00	47147562.
22	-45.00	0.00	4610.13	162.54	1.00	47147562.
23	-53.33	0.00	4610.13	162.54	1.00	47147562.
24	-61.67	0.00	4610.13	162.54	1.00	47147562.
25	-70.00	0.00	4127.59	136.46	1.00	37100946.
26	-78.33	0.00	4127.59	136.46	1.00	37100946.
27	-86.67	0.00	4127.59	136.46	1.00	37100946.
28	-95.00	0.00	4127.59	136.46	1.00	37100946.
29	-103.33	0.00	4127.59	136.46	1.00	37100946.
30	-111.67	0.00	4127.59	136.46	1.00	37100946.
31	-120.00	0.00	4127.59	136.46	1.00	37100946.
32	-128.33	0.00	4127.59	136.46	1.00	37100946.
33	-136.67	1000.00	4127.59	136.46	1.00	37100946.

PROB 150FT PENETRATION 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

QTIPS, 0.25-IN. MINIMUM WALL THICKNESS=1.25 IN. MU = 14

TABLE 4 -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00
 PERMANENT SET OF PILE = .0409 INCHES
 NUMBER OF BLOWS PER FOOT = 293.70
 TOTAL INTERVALS = 118

SEC	FLEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	178205.	31	0.	74	1.000	1.168919	1.168919	-1.21
2	0.00	1481205.	40	0.	0	1.000	.759061	.700713	-1.00
3	120.00	10887.	43	0.	0	136.463	.745125	.680878	-1.18
4	111.00	10925.	45	0.	0	136.463	.736585	.666758	-1.35
5	102.00	11002.	48	0.	0	136.463	.727178	.651949	-1.53
6	93.00	11159.	50	0.	0	136.463	.716851	.636415	-1.70
7	84.00	11339.	53	0.	0	136.463	.705545	.620140	-1.85
8	75.00	11535.	55	0.	0	136.463	.693147	.603197	-1.99
9	66.00	11715.	57	0.	0	136.463	.679523	.585552	-2.13
10	57.00	11881.	59	0.	0	136.463	.664533	.567160	-2.28
11	48.00	12037.	62	0.	0	136.463	.647994	.547895	-2.40
12	39.00	12191.	64	0.	0	136.463	.629681	.527790	-2.50
13	30.00	10388.	67	0.	0	162.578	.609244	.508820	-2.59
14	21.67	10624.	69	0.	0	162.578	.591290	.489635	-2.65
15	13.33	10821.	72	0.	0	162.578	.571330	.471581	-2.69
16	5.00	11260.	74	0.	0	162.578	.549250	.452592	-2.72
17	-3.33	11536.	76	0.	0	162.578	.525099	.432462	-2.74
18	-11.67	11710.	79	0.	0	162.578	.499191	.411198	-2.71
19	-20.00	11796.	81	0.	0	162.578	.471654	.38887	-2.66
20	-28.33	11782.	84	0.	0	162.578	.442871	.365427	-2.54
21	-36.67	11620.	85	0.	0	162.578	.413036	.341272	-2.36
22	-45.00	11341.	88	0.	0	162.578	.382400	.316762	-2.21
23	-53.33	10970.	90	0.	0	162.578	.350978	.291889	-2.02
24	-61.67	10567.	93	0.	0	162.578	.318802	.267114	-1.84
25	-70.00	11996.	96	0.	0	136.463	.285962	.242554	-1.64
26	-78.89	11483.	100	0.	0	136.463	.245032	.212483	-1.40
27	-87.78	10690.	101	0.	0	136.463	.206255	.184065	-1.21
28	-96.67	9579.	102	0.	0	136.463	.170950	.157629	-1.05
29	-105.56	8754.	103	0.	0	136.463	.140442	.133350	-0.85
30	-114.44	6750.	104	0.	0	136.463	.115247	.111757	-0.64
31	-123.33	5289.	104	0.	0	136.463	.094583	.093242	-0.43
32	-132.22	4012.	107	0.	0	136.463	.078492	.078078	-0.20
33	-141.11	3000.	106	0.	0	136.463	.065858	.065834	-0.14

PROB 4 16-IN. DIAMETER PILES (4-PIE STRUCTURE)
 150FT PENETRATION -- VULCAN 040 HAMMER

OTIPS, 0.25, MINIMUM WALL THICKNESS 1.25 IN. RII = 14

TABLE 9 -- RESISTANCE-MIDUM CURVE DATA

TIP RESISTANCE PERCENTAGE = 14.00		HOURS/FT.		RESISTANCE DYNAMIC PT		MAX C STRESS		SFG		MAX T STRESS		SFG	
		TOTAL-TONS FORCE-TONS		LBS/SQ. IN. (NO.)		LBS/SQ. IN. (NO.)		LBS/SQ. IN. (NO.)		LBS/SQ. IN. (NO.)		LBS/SQ. IN. (NO.)	
2.87	50.	19.50	1166R.	12	9012.	25							
4.28	100.	56.77	1705A.	12	7447.	10							
6.31	150.	57.61	12095.	12	6255.	10							
8.99	200.	66.97	12099.	12	5193.	9							
11.41	250.	80.01	12104.	12	4200.	9							
15.09	300.	91.88	12108.	12	3429.	8							
16.73	350.	102.68	12112.	12	2682.	7							
18.57	400.	112.51	12117.	12	1454.	25							
20.65	450.	121.45	12121.	12	715.	25							
23.02	500.	129.60	12125.	12	27.	25							
25.74	550.	137.00	12129.	12	0.	33							
28.49	600.	143.71	12133.	12	0.	33							
32.57	650.	149.75	12137.	12	0.	33							
36.91	700.	155.25	12142.	12	0.	33							
42.08	750.	160.15	12146.	12	0.	33							
48.30	800.	164.41	12150.	12	0.	33							
55.91	850.	168.19	12154.	12	0.	33							
65.34	900.	171.65	12158.	12	0.	33							
77.16	950.	174.54	12162.	12	0.	33							
92.13	1000.	176.71	12166.	12	0.	33							
111.25	1050.	179.33	12170.	12	0.	33							
135.59	1100.	184.52	12174.	12	0.	33							
164.93	1150.	190.14	12179.	12	0.	33							
199.16	1200.	195.90	12183.	12	0.	33							
240.58	1250.	201.72	12187.	12	0.	33							
293.70	1300.	207.45	12191.	12	0.	33							
365.08	1350.	212.75	12195.	12	0.	33							

PROB 4 36-IN. DYNAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

QTIPS, 0.25-MINIMUM WALL THICKNESS 1.25 IN. PU = 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PER FOOT	RESISTANCE TONS
135.59	1100.
199.14	1200.
240.54	1250.
293.70	1300.

NAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACMR 5-PILE STRUCTURE -- RUNNING 1
 APRIL 19 1976

PROB
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36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTYPE, 10-MINIMUM WALL THICKNESS 1.25 IN. MU = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE	1
NEW HAMMER DATA OPTION	1
NEW MATERIAL DATA OPTION	1
NEW PILE SECTION DATA OPTION	1
NEW SOIL DATA OPTION	1
SPECIFIED PLUM COUNT OPTION	1
OUTPUT OPTION FOR STRESS	1
HPF FOR STRESS OUTPUT OPTION	275.
ULTIMATE RESISTANCE INCREMENT (TONS)	50.0
MAX ALLOWS FOR RESISTANCE-BLOW CURVE (RPF)	300.
SPECIFIED SEGMENT LENGTH (FT)	40.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION	VULCAN 040 HAMMER
HAMMER EFFICIENCY	.75
HAMMER ENERGY (FT-LBS)	120000.00
HAMMER EXPLOSIVE FORCE (LBS)	40.00
NUMBER OF HAMMER SEGMENTS	2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LBS / IN)
1	1000.00	40000.00	1.00	.60	2700000.00
2	1000.00	27000.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES	1
MATERIAL TYPE	1
UNIT WT. (PCF)	36.000
MODULUS (PSI)	400.0 20000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 3

NUMBER OF SECTIONS PLACED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	WALL THICKNESS (IN)
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	40.	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE - JSIDE .15
 POINT DAMPING RESISTANCE - JPOINT .15
 SOIL SHAKE FOR SIDE - OSIDE .10
 SOIL SHAKE FOR POINT - OPOINT .10

TIP RESISTANCE PERCENTAGE

35.0000

TABLE 6 -- SPECIFIED ALLOW COUNT DATA

NUMBER OF SPECIFIED ALLOW COUNTS 4

ALLOW PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROJ 5 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN ORO HAMMER

QTIPS, 10, MINIMUM WALL THICKNESS=1.25 IN. MU = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTIII	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	278000.
2	0.00	1000.00	27800.00	1.00	.60	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4127.59	136.46	1.00	37100946.
26	-78.33	0.00	4127.59	136.46	1.00	37100946.
27	-86.67	0.00	4127.59	136.46	1.00	37100946.
28	-95.00	0.00	4127.59	136.46	1.00	37100946.
29	-103.33	0.00	4127.59	136.46	1.00	37100946.
30	-111.67	0.00	4127.59	136.46	1.00	37100946.
31	-120.00	0.00	4127.59	136.46	1.00	37100946.
32	-128.33	0.00	4127.59	136.46	1.00	37100946.
33	-136.67	1000.00	4127.59	136.46	1.00	37100946.

PROB 5 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN ORO HAMMER

QTIP, 10, MINIMUM WALL THICKNESS 1.25 IN. RU = 45

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 35.00

PERMANENT SET OF PILE = .0272 INCHES

NUMBER OF BLOWS PER FOOT = 440.70

TOTAL INTERVALS = 122

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME M	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	1782025.	31	0.	74	1,000	1.180319	1.177411	-.34
2	0.00	1441205.	40	0.	0	1,000	.768810	.718445	-.60
3	120.00	10887.	43	0.	0	136.463	.754977	.740732	-.72
4	111.00	10925.	45	0.	0	136.463	.746664	.649152	-.66
5	102.00	11002.	48	0.	0	136.463	.737731	.677227	-.99
6	93.00	11159.	50	0.	0	136.463	.724234	.644977	-1.12
7	84.00	11339.	53	0.	0	136.463	.718236	.652587	-1.26
8	75.00	11535.	55	0.	0	136.463	.707493	.639304	-1.34
9	66.00	11714.	57	0.	0	136.463	.696564	.625676	-1.53
10	57.00	11874.	59	0.	0	136.463	.684708	.611457	-1.64
11	48.00	12023.	62	0.	0	136.463	.671729	.596672	-1.76
12	39.00	12151.	64	0.	0	136.463	.657402	.581227	-1.86
13	30.00	10309.	66	0.	0	162.578	.641575	.565053	-1.96
14	21.67	10465.	69	0.	0	162.578	.627416	.551405	-2.04
15	13.33	10666.	71	0.	0	162.578	.612567	.537617	-2.14
16	5.00	10845.	73	0.	0	162.578	.595448	.522314	-2.24
17	-3.33	11052.	75	0.	0	162.578	.577622	.505764	-2.34
18	-11.67	11134.	78	0.	0	162.578	.557410	.487499	-2.40
19	-20.00	11140.	80	0.	0	162.578	.536723	.464425	-2.40
20	-28.33	11159.	82	0.	0	162.578	.514496	.444767	-2.37
21	-36.67	11054.	84	0.	0	162.578	.491401	.427415	-2.29
22	-45.00	10885.	87	0.	0	162.578	.467304	.406415	-2.19
23	-53.33	10659.	89	0.	0	162.578	.441404	.384375	-2.07
24	-61.67	10391.	92	0.	0	136.463	.414424	.361495	-1.96
25	-70.00	11913.	94	0.	0	136.463	.386242	.339268	-1.86
26	-78.89	11518.	99	0.	0	136.463	.349000	.310123	-1.75
27	-87.78	11373.	101	0.	0	136.463	.311871	.280753	-1.65
28	-96.67	11008.	103	0.	0	136.463	.275980	.251737	-1.43
29	-105.56	10321.	105	0.	0	136.463	.241657	.224044	-1.20
30	-114.44	9517.	105	0.	0	136.463	.208327	.197440	-.96
31	-123.33	8749.	111	0.	0	136.463	.177245	.172422	-.76
32	-132.22	7912.	110	0.	0	136.463	.150465	.149102	-.48
33	-141.11	6545.	108	0.	0	136.463	.127229	.126893	-.28

PROB 5 36-IN. DIAMETER PILLS TOILE STRUCTURE
 150FT PENETRATION -- VULCAN ODO MACHFR

QTIPS, 10. MINIMUM WALL THICKNESSES 1.25 IN. RU = 35

TABLE 9 -- RESISTANCE-HLUM CURVE DA

BLINDS/FT.	TIP RESISTANCE PERCENTAGE B	RESISTANCE DYNAMIC PT TOTAL-TONS	MAX C STRESS LBS/SQ. IN. MIN.	SEG MAX T STRESS LBS/SQ. IN. MIN.	SEG
2.85	50%	48.14	11673.	12	4781.
4.35	100%	91.51	12087.	12	7342.
6.57	150%	130.66	12091.	12	6015.
9.54	200%	166.04	12094.	12	4817.
12.42	250%	198.09	12097.	12	3782.
16.45	300%	227.18	12101.	12	2910.
18.89	350%	253.42	12104.	12	2225.
20.84	400%	277.65	12107.	12	826.
23.55	450%	299.50	12110.	12	92.
26.73	500%	319.37	12113.	12	0.
30.50	550%	337.41	12117.	12	0.
35.04	600%	353.41	12120.	12	0.
40.57	650%	368.72	12123.	12	0.
47.44	700%	382.29	12126.	12	0.
56.14	750%	394.55	12129.	12	0.
67.39	800%	405.55	12132.	12	0.
82.43	850%	415.29	12136.	12	0.
103.30	900%	423.65	12139.	12	0.
133.92	950%	431.17	12142.	12	0.
181.88	1000%	437.96	12145.	12	0.
265.65	1050%	442.90	12148.	12	0.
440.70	1100%	446.59	12151.	12	0.

PROB 5 30-IN. DIAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN OUN HAMMER

OTPS 10, MINIMUM WALL THICKNESS=1.25 IN. RU = 35

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 35.00

BLOWS PER FOOT	RESISTANCE TONS
133.92	9504
141.88	10004
265.65	10504
289.81	10604

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACHR 3-PILE STRUCTURE -- HONOLULU I
 APRIL 19 1976

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36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTTPS, 30, MINIMUM WALL THICKNESS=1.25 IN. HU = 50

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED ALLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX ALLOWS FOR RESISTANCE-HLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) -0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) -0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LB / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TUN)	UNIT WT. (PCF)	MODULUS (PST)
1	16.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 3
 NUMBER OF SECTIONS CHANGED 0

NUMBER OF SECTIONS CHANGED 0
 NUMBER OF SECTIONS ADDED 0
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	90.	0	90
2	1	1.500	100.	90	190
3	1	1.250	MO.	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE = JSIDE .15
 POINT DAMPING RESISTANCE = JPOINT .15
 SOIL SHAKE FOR SIDE .05IDE .10
 SOIL SHAKE FOR POINT .0POINT .30

TIP RESISTANCE PERCENTAGE

50.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PFH FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 150FT PENETRATION == 3/4-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION == VULCAN ORO HAMMER

OTIPR.30. MINIMUM WALL THICKNESS 1.25 IN. KII = 50

TABLE 7 == PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LRS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	36642910.
3	120.00	0.00	4179.19	136.46	1.00	36642910.
4	111.00	0.00	4179.19	136.46	1.00	36642910.
5	102.00	0.00	4179.19	136.46	1.00	36642910.
6	93.00	0.00	4179.19	136.46	1.00	36642910.
7	84.00	0.00	4179.19	136.46	1.00	36642910.
8	75.00	0.00	4179.19	136.46	1.00	36642910.
9	66.00	0.00	4179.19	136.46	1.00	36642910.
10	57.00	0.00	4179.19	136.46	1.00	36642910.
11	48.00	0.00	4179.19	136.46	1.00	36642910.
12	39.00	0.00	4179.19	136.46	1.00	36642910.
13	30.00	0.00	4610.13	162.54	1.00	47147562.
14	21.67	0.00	4610.13	162.54	1.00	47147562.
15	13.33	0.00	4610.13	162.54	1.00	47147562.
16	5.00	0.00	4610.13	162.54	1.00	47147562.
17	-3.33	0.00	4610.13	162.54	1.00	47147562.
18	-11.67	0.00	4610.13	162.54	1.00	47147562.
19	-20.00	0.00	4610.13	162.54	1.00	47147562.
20	-28.33	0.00	4610.13	162.54	1.00	47147562.
21	-36.67	0.00	4610.13	162.54	1.00	47147562.
22	-45.00	0.00	4610.13	162.54	1.00	47147562.
23	-53.33	0.00	4610.13	162.54	1.00	47147562.
24	-61.67	0.00	4610.13	162.54	1.00	47147562.
25	-70.00	0.00	4127.59	136.46	1.00	37100946.
26	-78.33	0.00	4127.59	136.46	1.00	37100946.
27	-86.67	0.00	4127.59	136.46	1.00	37100946.
28	-95.00	0.00	4127.59	136.46	1.00	37100946.
29	-103.33	0.00	4127.59	136.46	1.00	37100946.
30	-111.67	0.00	4127.59	136.46	1.00	37100946.
31	-120.00	0.00	4127.59	136.46	1.00	37100946.
32	-128.33	0.00	4127.59	136.46	1.00	37100946.
33	-136.67	1000.00	4127.59	136.46	1.00	37100946.

PROB 150FT PENETRATION 30-IN. DIAMETER PILLS 3-PIE STRUCTURE
 0TIP=30, MINIMUM WALL THICKNESS=1.25 IN. WII = 50

TABLE A -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 50.00
 PERMANENT SET OF PILE = .0310 INCHES
 NUMBER OF B.L.S PER FOOT = 187.07
 TOTAL INTERVALS = 127

SEG	ELEV FT	MAX C STRESS LBS/SQ.IN.	TIME N	MAX T STRESS LBS/SQ.IN.	TIME N	ARFA SQ.IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	1782025.	51	0.	74	1.000	1.200689	1.193692	0.47
2	0.00	1481205.	40	0.	0	1.000	.788490	.751702	0.17
3	120.00	10447.	43	0.	0	136.443	.774733	.736381	0.23
4	111.00	10925.	45	0.	0	136.443	.765588	.727523	0.30
5	102.00	11002.	44	0.	0	136.443	.758089	.718477	0.39
6	93.00	11159.	50	0.	0	136.443	.749441	.709262	0.51
7	84.00	11339.	53	0.	0	136.443	.740801	.699872	0.62
8	75.00	11534.	55	0.	0	136.443	.732362	.690351	0.72
9	66.00	11714.	57	0.	0	136.443	.724127	.680755	0.80
10	57.00	11876.	59	0.	0	136.443	.715605	.671018	0.86
11	48.00	12012.	62	0.	0	136.443	.706520	.661316	0.90
12	39.00	12122.	64	0.	0	136.443	.696657	.651619	0.93
13	30.00	10253.	66	0.	0	162.578	.685925	.641809	1.00
14	21.67	10356.	68	0.	0	162.578	.676705	.633780	1.09
15	13.33	10480.	70	0.	0	162.578	.666453	.625063	1.22
16	5.00	10612.	72	0.	0	162.578	.655117	.615441	1.33
17	-3.33	10697.	74	0.	0	162.578	.642765	.604845	1.41
18	-11.67	10714.	77	0.	0	162.578	.629615	.593424	1.44
19	-20.00	10703.	79	0.	0	162.578	.616204	.581452	1.42
20	-28.33	10656.	81	0.	0	162.578	.602695	.569074	1.37
21	-36.67	10568.	84	0.	0	162.578	.588441	.556353	1.31
22	-45.00	10445.	86	0.	0	162.578	.572842	.543321	1.24
23	-53.33	10300.	88	0.	0	162.578	.555894	.529781	1.24
24	-61.67	10116.	90	0.	0	162.578	.537917	.515422	1.30
25	-70.00	11672.	92	0.	0	136.443	.519651	.500183	1.27
26	-78.89	11046.	93	0.	0	136.443	.497122	.480215	1.27
27	-87.78	10473.	99	0.	0	136.443	.474821	.459753	1.24
28	-96.67	10269.	101	0.	0	136.443	.451567	.438516	1.20
29	-105.56	9848.	103	0.	0	136.443	.427771	.414887	1.06
30	-114.44	9219.	103	0.	0	136.443	.403262	.395372	0.89
31	-123.33	8723.	110	0.	0	136.443	.378292	.373979	0.76
32	-132.22	8441.	113	0.	0	136.443	.354322	.352411	0.54
33	-141.11	8195.	115	0.	0	136.443	.331002	.330509	0.37

PROB

150FT PENETRATION -- 5/8 IN. DIAMETER PILES 30PTIF STRUCTURE
VULCANOID HAMMER

TYPE 30, MINIMUM WALL THICKNESS 1.25 IN. RUI = 50

TABLE 9 -- RESISTANCE-HL/IN CURVE DATA

TIP RESISTANCE PERCENTAGE = 50.00

HL/IN	RESISTANCE DYNAMIC PT	MAX C STRESS	SFG	MAX T STRESS	SEG
FT	TOTAL-TONS FORCE-TONS	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	LBS/SQ. IN. NO.	
2.77	50%	11654.	12	8625.	25
4.07	100%	12045.	12	7226.	11
7.14	150%	12088.	12	5823.	10
10.69	200%	12090.	12	4545.	10
14.70	250%	12093.	12	3465.	9
20.57	300%	12095.	12	2481.	9
25.97	350%	12098.	12	1583.	9
28.07	400%	12100.	12	547.	20
33.15	450%	12103.	12	0.	33
39.50	500%	12105.	12	0.	33
47.73	550%	12108.	12	0.	33
58.76	600%	12110.	12	0.	33
74.21	650%	12113.	12	0.	33
97.25	700%	12115.	12	0.	33
134.89	750%	12117.	12	0.	33
206.20	800%	12120.	12	0.	33
387.07	850%	12122.	12	0.	33

PROB 6 36-IN. DIAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

BTIPS, 30, MINIMUM WALL THICKNESS=1.25 IN. RU = 50

TABLE 10 -- SPECIFIED H/L/W DATA

TIP RESISTANCE PERCENTAGE = 50.00

HLOWS PER FOOT	RESISTANCE TONS
136.89	750.
206.20	800.
234.20	812.
294.35	831.

JYJZGR. 04/19/74. *UNITED COMPUTING* 67. APFX/SL. R.0.24

17.52.053PIL,CMI00,T1000.			
17.52.053FL	K4	0.000	
17.52.063AC3400CRR0023,2777100CC)R			
17.52.06.04/19/74.JYJZGR			
17.52.06.WFL,40000.			
17.52.063FL	3392	0.001	
17.52.063FL	16384	0.001	
17.52.06.WAP,DEF.			
17.52.063FL	256	0.001	
17.52.063CET,PILR(CAR0024)			
17.52.10.WEANY - PILR			
17.52.103FL	4096	0.001	0.
17.52.103FL	72	1	
17.52.10.PILR.			
17.52.103FL00	16384	0.002	
17.52.123FL01	16384	0.141	190
17.52.12.FL REQUIRED TO LOAD			363708 (15608)
17.52.12.FL REQUIRED TO EXECUTE			340008 (14336)
17.52.123FL	16384	0.145	
17.53.10.FND PILDM			
17.53.10.COST.	14336	39.007	158
17.53.103FL		SERVICE UNITS	104.6
17.53.11.		JOB COSTS	24.15
17.53.113FL	12288		7
17.53.11.EXIT.			5
17.53.113UT00	2368	39.030	
17.53.11.	*FL*	*CPU SFC.	*DISC PRUS* DISC ACC
17.53.11.	*AP.F.	*PRUS.P.F. ACC	*TAPE PRUS* TAPE ACC

Pile Driving Resistance Curves

Pile Diameter	- 36 in.
Minimum Wall Thickness	- 1.5 in.
Penetration	- 200 ft. - 150 ft.
Hammer	- Vulcan 040
Quake Factor, tip	- .025 in.

HAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACMR 3-PILE STRUCTURE -- HORIZING 1
 APRIL 19 1974

PROB
 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER
 OTIPS.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA (OPTION) 1
 NEW MATERIAL DATA (OPTION) 1
 NEW PILE SECTION DATA (OPTION) 1
 NEW SOIL DATA (OPTION) 1
 SPECIFIED BLOW COUNT (OPTION) 1
 OUTPUT OPTION FOR STRESS 1
 BPF FOR STRESS OUTPUT (OPTION) 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX BLOWS FOR RESISTANCE-BLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2700000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TON)	UNIT WT. (PCF)	MODULUS (PSI)
1	36,000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4

NUMBER OF TIP SECTIONS CHANGED
 NUMBER OF SECTIONS ABOVE
 LENGTH OF SHEET STANDING PILE(S) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	40.	0	40
2	1	1.750	100.	40	140
3	1	1.500	100.	140	240
4	1	1.500	40.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE - JSIDE .15
 POINT DAMPING RESISTANCE - JPOINT .15
 SOIL SHAKE FOR SIDE .10
 SOIL SHAKE FOR POINT .03

TIP RESISTANCE PERCENTAGE

14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB. 1 36 IN. DIAMETER PILES 3-PILE STRUCTURE
 200 FT PENETRATION -- VULCAN ODO HAMMER

QTYPE, 0.75, MINIMUM WALL THICKNESS, 1.5 IN. RU = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT	SLACK IN.	WFIGHT LBS	AREA SQ. IN.	CNCF PSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2780000.
2	0.00	1000.00	27800.00	1.00	.90	32978619.
3	120.00	0.00	4643.54	136.46	1.00	32978619.
4	110.00	0.00	4643.54	136.46	1.00	32978619.
5	100.00	0.00	4643.54	136.46	1.00	32978619.
6	90.00	0.00	4643.54	136.46	1.00	32978619.
7	80.00	0.00	5339.52	188.30	1.00	54608898.
8	71.67	0.00	5339.52	188.30	1.00	54608898.
9	63.33	0.00	5339.52	188.30	1.00	54608898.
10	55.00	0.00	5339.52	188.30	1.00	54608898.
11	46.67	0.00	5339.52	188.30	1.00	54608898.
12	38.33	0.00	5339.52	188.30	1.00	54608898.
13	30.00	0.00	5339.52	188.30	1.00	54608898.
14	21.67	0.00	5339.52	188.30	1.00	54608898.
15	13.33	0.00	5339.52	188.30	1.00	54608898.
16	5.00	0.00	5339.52	188.30	1.00	54608898.
17	-3.33	0.00	5339.52	188.30	1.00	54608898.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4610.13	162.58	1.00	47147562.
26	-78.33	0.00	4610.13	162.58	1.00	47147562.
27	-86.67	0.00	4610.13	162.58	1.00	47147562.
28	-95.00	0.00	4610.13	162.58	1.00	47147562.
29	-103.33	0.00	4610.13	162.58	1.00	47147562.
30	-111.67	0.00	4610.13	162.58	1.00	47147562.
31	-120.00	0.00	4917.48	162.58	1.00	44200839.
32	-128.89	0.00	4917.48	162.58	1.00	44200839.
33	-137.78	0.00	4917.48	162.58	1.00	44200839.
34	-146.67	0.00	4917.48	162.58	1.00	44200839.
35	-155.56	0.00	4917.48	162.58	1.00	44200839.
36	-164.44	0.00	4917.48	162.58	1.00	44200839.
37	-173.33	0.00	4917.48	162.58	1.00	44200839.
38	-182.22	0.00	4917.48	162.58	1.00	44200839.
39	-191.11	1000.00	4917.48	162.58	1.00	44200839.

PROB 1. 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 040 HAMMER

OTPS=.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE B -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0424 INCHES

NUMBER OF HITS PER FOOT = 282.97

TOTAL INTERVALS = 134

SEC	ELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LRS/SQ. IN.	TIME N	AREA SQ. IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1779488	32	0.	134	1.000	1.117019	.670291	-12.04
2	0.00	1624301	43	0.	99	1.000	.690077	.652987	-1.14
3	120.00	12264	46	237.	92	136.463	.669866	.632731	-1.23
4	110.00	12583	48	348.	94	136.463	.659300	.617952	-1.34
5	100.00	12836	50	330.	96	136.463	.654137	.601428	-1.45
6	90.00	13005	52	206.	97	136.463	.652799	.583307	-1.55
7	80.00	9452	54	0.	0	188.300	.652353	.563759	-1.65
8	71.67	9478	56	0.	0	188.300	.651577	.551110	-1.71
9	63.33	9504	59	0.	0	188.300	.649935	.537731	-1.77
10	55.00	9514	61	0.	0	188.300	.647234	.523741	-1.83
11	46.67	9492	63	0.	0	188.300	.643262	.509274	-1.90
12	38.33	9458	65	0.	0	188.300	.637777	.494444	-1.96
13	30.00	9451	67	0.	0	188.300	.630639	.479379	-2.02
14	21.67	9478	70	0.	0	188.300	.621641	.464259	-2.09
15	13.33	9560	72	0.	0	188.300	.610622	.449326	-2.17
16	5.00	9691	75	0.	0	188.300	.597490	.434715	-2.23
17	3.33	9840	77	0.	0	188.300	.582189	.420330	-2.25
18	-11.67	9991	80	0.	0	188.300	.564743	.405992	-2.23
19	-20.00	11679	82	0.	0	162.578	.545450	.391639	-2.22
20	-28.33	11729	85	0.	0	162.578	.521570	.375013	-2.23
21	-36.67	11727	87	0.	0	162.578	.496397	.358359	-2.27
22	-45.00	11663	89	0.	0	162.578	.470262	.341536	-2.31
23	-53.33	11541	92	0.	0	162.578	.443288	.324544	-2.35
24	-61.67	11360	94	0.	0	162.578	.415603	.306580	-2.37
25	-70.00	11118	96	0.	0	162.578	.387686	.288179	-2.34
26	-78.33	10819	99	0.	0	162.578	.359531	.269455	-2.28
27	-86.67	10474	101	0.	0	162.578	.331565	.250550	-2.19
28	-95.00	10048	103	0.	0	162.578	.303940	.231689	-2.04
29	-103.33	9577	106	0.	0	162.578	.276608	.213162	-1.94
30	-111.67	8996	109	0.	0	162.578	.249563	.194712	-1.80
31	-120.00	8468	113	0.	0	162.578	.222412	.176872	-1.65
32	-128.89	8129	115	0.	0	162.578	.193595	.158681	-1.45
33	-137.78	7706	116	0.	0	162.578	.166297	.141771	-1.26
34	-146.67	7015	116	0.	0	162.578	.141454	.125970	-1.05
35	-155.56	6101	119	0.	0	162.578	.119638	.111460	-.86
36	-164.44	5213	119	0.	0	162.578	.102238	.094270	-.64
37	-173.33	4240	119	0.	0	162.578	.084306	.084716	-.46
38	-182.22	3352	117	0.	0	162.578	.076004	.076000	-.27

123 456 789 012 345 678 901 234 567 890

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 000 MAMFED

QTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. MU = 14

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

BLOWS/FT.	TIP RESISTANCE PERCENTAGE	RESISTANCE DYNAMIC PT TOTAL-TONS FORCE-TONS	MAX C STRESS LBS/SQ. IN. NO.	SEG (LBS/SQ. IN. NO.)	SEG MAX T STRESS	SEG
2.74	50%	18.69	12999.	6	9138.	30
4.12	100%	35.91	12999.	6	8346.	29
5.89	150%	51.74	13005.	6	7440.	29
8.04	200%	66.26	13005.	6	6568.	30
10.45	250%	79.61	13005.	6	5778.	30
12.84	300%	91.89	13005.	6	5038.	30
15.60	350%	103.17	13005.	6	4340.	30
18.03	400%	113.55	13005.	6	3675.	30
19.83	450%	123.06	13005.	6	3072.	31
21.86	500%	131.79	13005.	6	2501.	31
24.16	550%	139.76	13005.	6	1946.	31
26.79	600%	147.04	13005.	6	1401.	32
29.82	650%	153.66	13005.	6	918.	32
33.34	700%	159.63	13005.	6	572.	5
37.07	750%	165.03	13005.	6	553.	5
42.35	800%	169.92	13005.	6	534.	5
48.20	850%	174.22	13005.	6	515.	5
55.27	900%	176.03	13005.	6	496.	5
63.96	950%	181.51	13005.	6	478.	5
74.74	1000%	184.68	13005.	6	450.	5
88.30	1050%	187.16	13005.	6	440.	5
105.58	1100%	189.14	13005.	6	422.	5
127.74	1150%	193.30	13005.	6	403.	5
155.67	1200%	198.15	13005.	6	385.	5
188.93	1250%	203.21	13005.	6	370.	4
229.67	1300%	208.40	13005.	6	359.	4
282.97	1350%	213.67	13005.	6	348.	4
357.70	1400%	218.95	13005.	6	337.	4

PROB 1 36 IN. DIAMETER PILES 3-PILE STRUCTURE
200 FT PENETRATION -- VULCAN 040 HAMMER

OTIP, 0.25, MINIMUM WALL THICKNESS 1.5 IN. RII # 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PER FOOT	RESISTANCE TONS
127.74	1150.
184.93	1250.
229.67	1300.
282.97	1350.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACMR 3-PILE STRUCTURE -- HOWING 1
 APRIL 19 1976

PROB 2
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 GTYPE=025, MINIMUM WALL THICKNESS=1.5 IN. RU = 10

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED RLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPP FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX RIGIDS FOR RESISTANCE-FLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) -0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 040 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 120000.00
 HAMMER EXPLOSIVE FORCE (LBS) -0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	HEIGHT (LH)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	40000.00	1.00	.60	2780000.00
2	1000.00	27800.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TON)	UNIT WT. (PCF)	MODULUS (PST)
1	36.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4

NUMBER OF SECTIONS ADDED 9
 LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	40.	0	40
2	1	1.750	50.	40	90
3	1	1.500	100.	90	190
4	1	1.500	40.	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE - JSIDE .15
 POINT DAMPENING RESISTANCE - JPOINT .15
 SOIL SHAKE FOR SIDE - QSIDE .10
 SOIL SHAKE FOR POINT - QPOINT .03

TIP RESISTANCE PERCENTAGE

14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROR 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN ODD HAMMER

QTYPE=.025, MINIMUM WALL THICKNESS=1.5 IN. HUI = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLY FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTITU	SPR STIFF LBS/IN.
1	0.00	1000.00	40000.00	1.00	.60	2740000.
2	0.00	1000.00	27800.00	1.00	.90	32978619.
3	120.00	0.00	4643.54	134.46	1.00	32978619.
4	110.00	0.00	4643.54	134.46	1.00	32978619.
5	100.00	0.00	4643.54	134.46	1.00	32978619.
6	90.00	0.00	4643.54	134.46	1.00	32978619.
7	80.00	0.00	5339.52	188.30	1.00	54606898.
8	71.67	0.00	5339.52	188.30	1.00	54606898.
9	63.33	0.00	5339.52	188.30	1.00	54606898.
10	55.00	0.00	5339.52	188.30	1.00	54606898.
11	46.67	0.00	5339.52	188.30	1.00	54606898.
12	38.33	0.00	5339.52	188.30	1.00	54606898.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4917.48	162.58	1.00	44200839.
25	-70.00	0.00	4917.48	162.58	1.00	44200839.
26	-78.33	0.00	4917.48	162.58	1.00	44200839.
27	-86.67	0.00	4917.48	162.58	1.00	44200839.
28	-95.00	0.00	4917.48	162.58	1.00	44200839.
29	-103.33	0.00	4917.48	162.58	1.00	44200839.
30	-111.67	0.00	4917.48	162.58	1.00	44200839.
31	-120.00	0.00	4917.48	162.58	1.00	44200839.
32	-128.33	0.00	4917.48	162.58	1.00	44200839.
33	-136.67	1000.00	4917.48	162.58	1.00	44200839.

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION == VULCAN 040 HAMMER

QTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. RII = 14

TABLE A == MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0412 INCHES

NUMBER OF BLOWS PER FOOT = 291.61

TOTAL INTERVALS = 121

SEG	FLEV FT	MAX C STRESS LBS/SQ.IN.	TIME N	MAX T STRESS LRS/SQ.IN.	TIME N	AREA SQ.IN.	DHAY(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	1779684	32	0.	69	1.000	1.115633	1.115093	.05
2	0.00	1626289	43	0.	95	1.000	.679655	.666531	.91
3	120.00	12262.	45	202.	88	136.463	.640236	.640256	1.06
4	110.00	12561.	48	167.	89	136.463	.662588	.625135	1.25
5	100.00	12744.	50	0.	0	136.463	.662911	.604161	1.47
6	90.00	12797.	52	0.	0	136.463	.662515	.581699	1.70
7	80.00	9204.	54	0.	0	188.300	.660463	.558170	1.95
8	71.67	9128.	56	0.	0	188.300	.657522	.543192	2.10
9	63.33	9062.	58	0.	0	188.300	.652736	.528122	2.24
10	55.00	9009.	61	0.	0	188.300	.645774	.512539	2.40
11	46.67	9002.	63	0.	0	188.300	.636598	.498855	2.58
12	38.33	9067.	66	0.	0	188.300	.624951	.481158	2.73
13	30.00	10475.	69	0.	0	162.578	.610925	.465192	2.81
14	21.67	10937.	71	0.	0	162.578	.592214	.446209	2.84
15	13.33	11275.	74	0.	0	162.578	.570990	.426615	2.86
16	5.00	11481.	76	0.	0	162.578	.547215	.406700	2.92
17	-3.33	12060.	79	0.	0	162.578	.520862	.386716	3.01
18	-11.67	12303.	81	0.	0	162.578	.492143	.366493	3.04
19	-20.00	12421.	84	0.	0	162.578	.461654	.345454	3.00
20	-28.33	12412.	86	0.	0	162.578	.429661	.324590	2.92
21	-36.67	12280.	88	0.	0	162.578	.396644	.302669	2.72
22	-45.00	12013.	90	0.	0	162.578	.363064	.280485	2.51
23	-53.33	11654.	92	0.	0	162.578	.329372	.257723	2.32
24	-61.67	11161.	95	0.	0	162.578	.295133	.234751	2.10
25	-70.00	10625.	99	0.	0	162.578	.260991	.211728	1.88
26	-78.89	10162.	102	0.	0	162.578	.224734	.187752	1.61
27	-87.78	9547.	103	0.	0	162.578	.190425	.164646	1.38
28	-96.67	8573.	103	0.	0	162.578	.159145	.143193	1.16
29	-105.56	7375.	106	0.	0	162.578	.131784	.123073	.93
30	-114.44	6102.	106	0.	0	162.578	.109486	.105063	.70
31	-123.33	4809.	106	0.	0	162.578	.091445	.084539	.51
32	-132.22	3634.	105	0.	0	162.578	.07369	.076627	.36
33	-141.11	2751.	109	0.	0	162.578	.066152	.065919	.21

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 000 HAMMER

QTIPR.025, MINIMUM WALL THICKNESS=1.5 IN. HU # 14

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TTP RESISTANCE PERCENTAGE = 14.00

BLOWS/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS	DYNAMIC PT FORCE-TONS	MAX C STRESS LRS/SO.IN. NO.	SEG MAX T STRESS LRS/SO.IN. NO.	SEG
3.02	50	18.62	12657.	9365.	14
4.44	100	35.71	12797.	7450.	24
6.20	150	51.58	12797.	6942.	24
8.54	200	65.74	12797.	5993.	24
11.05	250	78.93	12797.	5117.	24
13.56	300	91.06	12797.	4320.	25
16.39	350	102.22	12797.	3593.	25
18.51	400	112.49	12797.	2943.	6
20.36	450	121.93	12797.	2270.	25
22.44	500	130.62	12797.	1658.	25
24.79	550	138.61	12797.	1078.	26
27.46	600	145.90	12797.	556.	27
30.52	650	152.65	12797.	327.	4
34.06	700	158.76	12797.	316.	4
38.17	750	164.29	12797.	305.	4
43.01	800	169.33	12797.	294.	4
48.74	850	173.85	12797.	284.	4
55.60	900	177.88	12797.	273.	4
63.40	950	181.59	12797.	262.	4
74.06	1000	184.97	12797.	251.	4
86.60	1050	187.68	12797.	241.	4
102.21	1100	189.77	12797.	230.	4
121.71	1150	193.82	12797.	225.	3
145.73	1200	199.16	12797.	220.	3
173.28	1250	204.75	12797.	215.	3
205.19	1300	210.45	12797.	211.	3
243.54	1350	216.25	12797.	206.	3
291.61	1400	222.02	12797.	202.	3
354.62	1450	227.82	12797.	197.	3

PROB 2 36-IN. DIAMETER PILES SOPILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

GTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PER FOOT	RESISTANCE TONS
145.73	1200.
205.19	1300.
243.54	1350.
291.61	1400.

JVJUNCT. 04/20/76. *UNITED COMPUTING* 67. APEX/SI. H.0.24

15.49.56\$PL,CM100,T1000.				
15.49.56\$FL 64	0.000			
15.49.56\$AC3400CRR0023,2777100CC 3H				
15.49.56.04/20/76.JVJUNCT				
15.49.56.FEL,40000.				
15.49.56\$FL 3392	0.000			
15.49.56\$FL 163M4	0.000			
15.49.56.HAP,OFF.				
15.49.57\$EL 256	0.000			
15.49.57.GE7,PILR(CA80024)				
15.50.01.READY PILB				
15.50.01\$FL 4096	0.000	0	0.	
15.50.01\$FI 72	1			
15.50.02.PILH.				
15.50.02\$FL00 163M4	0.000			
15.50.03\$FL01 163M4	0.143	190	7	
15.50.03.FL REQUIRED TO LOAD		363708	(15608)	
15.50.03.FL REQUIRED TO EXECUTE		340008	(14336)	
15.50.03\$FL 163M4	0.147			
15.50.28.END PILDR1				
15.50.28.COST.				
15.50.28\$FL 14336	18.488	59	5	
15.50.29. SERVICE UNITS#	52.4			
15.50.29. JOB COSTS#	13.10			
15.50.29\$FL 12288	18.504	7	5	
15.50.29.EXIT,				
15.50.29\$JT00 2368	18.504			
15.50.29. *FL* *CPU SFC. *DISC PRUS* DISC ACC				
15.50.29. *P.F. PRUS*P.F. ACC *TAPE PRUS* TAPE ACC				

2.6

Pile Driving Resistance Criteria

Pile Diameter	- 36 in.
Minimum Wall Thickness	- 1.5 in.
Penetration	- 200 ft. - 150 ft.
Hammer	- Vulcan 060
Quake Factor, tip	- .025 in.

HAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACMR 3-PILE STRUCTURE -- BORING 1
 APRIL 19 1976

PROG 1
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 060 HAMMER
 QTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED ALLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPA FOR STRESS OUTPUT OPTION 1
 ULTIMATE RESISTANCE INCREMENT (TONS) 275.
 MAX BLOWS FOR RESISTANCE-BLOW CURVE (RPP) 50.0
 SPECIFIED SEGMENT LENGTH (FT) 300.
 -0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 060 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 100000.00
 HAMMER EXPLOSIVE FORCE (LBS) 0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	HEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	60000.00	1.00	.60	3240000.00
2	1000.00	40200.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TOD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

LENGTH OF FREE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	40.	0	40
2	1	1.750	100.	40	140
3	1	1.500	100.	140	240
4	1	1.500	40.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE = JSIDE .15
 POINT DAMPENING RESISTANCE = JPOINT .15
 SOIL SHAKE FOR SIDE = GSTOE .10
 SOIL SHAKE FOR POINT = GPOINT .03

TIP RESISTANCE PERCENTAGE
 14.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 660 HAMMER

QTPR.025, MINIMUM WALL THICKNESS 1.5 IN. RU = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLV FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	60000.00	1.00	.60	3240000.
2	0.00	1000.00	40200.00	1.00	.90	32978619.
3	120.00	0.00	4643.54	136.46	1.00	32978619.
4	110.00	0.00	4643.54	136.46	1.00	32978619.
5	100.00	0.00	4643.54	136.46	1.00	32978619.
6	90.00	0.00	4643.54	136.46	1.00	32978619.
7	80.00	0.00	5339.52	188.30	1.00	54606898.
8	71.67	0.00	5339.52	188.30	1.00	54606898.
9	63.33	0.00	5339.52	188.30	1.00	54606898.
10	55.00	0.00	5339.52	188.30	1.00	54606898.
11	46.67	0.00	5339.52	188.30	1.00	54606898.
12	38.33	0.00	5339.52	188.30	1.00	54606898.
13	30.00	0.00	5339.52	188.30	1.00	54606898.
14	21.67	0.00	5339.52	188.30	1.00	54606898.
15	13.33	0.00	5339.52	188.30	1.00	54606898.
16	5.00	0.00	5339.52	188.30	1.00	54606898.
17	-3.33	0.00	5339.52	188.30	1.00	54606898.
18	-11.67	0.00	5339.52	188.30	1.00	54606898.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4610.13	162.58	1.00	47147562.
26	-78.33	0.00	4610.13	162.58	1.00	47147562.
27	-86.67	0.00	4610.13	162.58	1.00	47147562.
28	-95.00	0.00	4610.13	162.58	1.00	47147562.
29	-103.33	0.00	4610.13	162.58	1.00	47147562.
30	-111.67	0.00	4610.13	162.58	1.00	47147562.
31	-120.00	0.00	4917.48	162.58	1.00	44200839.
32	-128.69	0.00	4917.48	162.58	1.00	44200839.
33	-137.78	0.00	4917.48	162.58	1.00	44200839.
34	-146.67	0.00	4917.48	162.58	1.00	44200839.
35	-155.56	0.00	4917.48	162.58	1.00	44200839.
36	-164.44	0.00	4917.48	162.58	1.00	44200839.
37	-173.33	0.00	4917.48	162.58	1.00	44200839.
38	-182.22	0.00	4917.48	162.58	1.00	44200839.
39	-191.11	1000.00	4917.48	162.58	1.00	44200839.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 000 HAMMER

OTIPS .025, MINIMUM WALL THICKNESS 1.5 IN. RU = 14

TABLE B -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SPT OF PILE = .0027 INCHES
 NUMBER OF BLOW PER FOOT = 280.78
 TOTAL INTERVALS = 141

SEG	FLEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	228172	34	0.	73	1.000	1.46829	1.466484	-2.24
2	0.00	191922A	49	0.	0	1.000	.928824	.925151	-2.55
3	120.00	14413.	51	0.	0	136.443	.895952	.888169	-2.72
4	110.00	14730.	54	0.	0	136.463	.850480	.850480	-2.91
5	100.00	14990.	56	0.	0	136.443	.866103	.829194	-1.10
6	90.00	15141.	58	0.	0	136.443	.860748	.797562	-1.31
7	80.00	11001.	60	0.	0	188.300	.850422	.764868	-1.52
8	71.67	11024.	62	0.	0	188.300	.849518	.744582	-1.66
9	63.33	11031.	64	0.	0	188.300	.843257	.723891	-1.80
10	55.00	11011.	66	0.	0	188.300	.835053	.702927	-1.94
11	46.67	10987.	68	0.	0	188.300	.825922	.681797	-2.07
12	38.33	10992.	71	0.	0	188.300	.814471	.660615	-2.19
13	30.00	11039.	73	0.	0	188.300	.800964	.639482	-2.29
14	21.67	11136.	76	0.	0	188.300	.785286	.618473	-2.34
15	13.33	11286.	78	0.	0	188.300	.767255	.597653	-2.46
16	5.00	11500.	81	0.	0	188.300	.746940	.577094	-2.51
17	-3.33	11735.	84	0.	0	188.300	.724282	.556820	-2.55
18	-11.67	11954.	86	0.	0	188.300	.694382	.536717	-2.57
19	-20.00	14005.	89	0.	0	162.578	.672496	.516558	-2.58
20	-28.33	14085.	91	0.	0	162.578	.639811	.492917	-2.60
21	-36.67	14092.	94	0.	0	162.578	.605876	.468833	-2.59
22	-45.00	14021.	96	0.	0	162.578	.570927	.444249	-2.56
23	-53.33	13466.	98	0.	0	162.578	.535362	.419158	-2.49
24	-61.67	13441.	101	0.	0	162.578	.499336	.393717	-2.37
25	-70.00	13345.	103	0.	0	162.578	.463070	.368013	-2.26
26	-78.33	12976.	106	0.	0	162.578	.427016	.341960	-2.12
27	-86.67	12521.	108	0.	0	162.578	.391131	.315918	-1.96
28	-95.00	11947.	111	0.	0	162.578	.352334	.289890	-1.83
29	-103.33	11374.	114	0.	0	162.578	.319584	.264146	-1.67
30	-111.67	10824.	118	0.	0	162.578	.284327	.238784	-1.53
31	-120.00	10394.	119	0.	0	162.578	.250290	.214284	-1.35
32	-128.89	9941.	119	0.	0	162.578	.215925	.189432	-1.19
33	-137.78	8941.	121	0.	0	162.578	.184344	.166212	-1.05
34	-146.67	7995.	123	0.	0	162.578	.155877	.144630	-2.91
35	-155.56	6898.	125	0.	0	162.578	.131408	.124992	-2.75
36	-164.44	5738.	125	0.	0	162.578	.110729	.107329	-2.60
37	-173.33	4733.	124	0.	0	162.578	.093562	.091840	-2.45
38	-182.22	3794.	126	0.	0	162.578	.079332	.078718	-2.30
39	-191.11	3659.	128	0.	0	162.578	.067738	.067508	-2.20

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 060 HAMMER

QTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 9 -- RESISTANCE=BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS/FT.	RESISTANCE DYNAMIC PT TOTAL-TONS FORCE-TONS	MAX C STRESS LBS/SQ.IN. NO.	SFG LBS/SQ.IN. NO.	MAX T STRESS LBS/SQ.IN. NO.	SFG
2.07	50	20.57	14947.	1000.	28
2.90	100	39.53	15105.	8994.	28
4.00	150	56.99	15141.	7922.	28
5.39	200	73.03	15141.	6919.	28
7.00	250	87.79	15141.	5977.	29
8.74	300	101.37	15141.	5127.	29
10.51	350	113.85	15141.	4333.	29
12.95	400	125.42	15141.	3860.	6
14.14	450	135.88	15141.	3238.	6
15.46	500	145.59	15141.	2371.	6
16.92	550	154.51	15141.	1683.	30
18.56	600	162.72	15141.	1137.	31
20.40	650	170.26	15141.	611.	31
22.48	700	177.19	15141.	109.	32
24.86	750	183.56	15141.	0.	39
27.58	800	189.41	15141.	0.	39
30.72	850	194.77	15141.	0.	39
34.58	900	199.60	15141.	0.	39
38.68	950	203.83	15141.	0.	39
43.79	1000	207.50	15141.	0.	39
49.90	1050	210.77	15141.	0.	39
57.32	1100	213.78	15141.	0.	39
66.41	1150	216.35	15141.	0.	39
77.68	1200	218.20	15141.	0.	39
91.45	1250	219.59	15141.	0.	39
109.77	1300	224.06	15141.	0.	39
132.49	1350	229.16	15141.	0.	39
160.44	1400	234.57	15141.	0.	39
192.99	1450	239.85	15141.	0.	39
231.93	1500	244.49	15141.	0.	39
280.78	1550	248.67	15141.	0.	39
346.41	1600	252.60	15141.	0.	39

PROJ 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200FT PENETRATION -- VULCAN 060 HAMMER

QTIP: .025, MINIMUM WALL THICKNESS: 1.5 IN. RU = 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PER FOOT	RESISTANCE TONS
132.49	1350.
192.99	1450.
231.93	1500.
280.78	1550.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACUR 3-PILE STRUCTURE -- WORKING 1
 APRIL 19 1976

PROB 2
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER
 OTTPE.025, MINIMUM WALL THICKNESS 1.5 IN. RU = 14

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED BLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 RPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX BLOWS FOR RESISTANCE-BLOW CURVE (RPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) =0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 060 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 180000.00
 HAMMER EXPLOSIVE FORCE (LBS) =0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	HEIGHT (LR)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	60000.00	1.00	.60	3200000.00
2	1000.00	40200.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(TOD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4
 NUMBER OF SECTIONS CHANGED 0

NUMBER OF SECTIONS ABOVE 120.00
 LENGTH OF FREE STANDING PILE (FT)

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1,250	40.	0	40
2	1	1,750	50.	40	90
3	1	1,500	100.	90	190
4	1	1,500	40.	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPING RESISTANCE - JSIDE .15
 POINT DAMPING RESISTANCE - JPPOINT .15
 SOIL SHAKE FOR SIDE - OSIDE .10
 SOIL SHAKE FOR POINT - OPOINT .03

TIP RESISTANCE PERCENTAGE

14,000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 040 HAMMER

OTYPE=025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELFV FT	SLACK IN.	WFIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	60000.00	1.00	.60	3240000.
2	0.00	1000.00	40200.00	1.00	.90	32978619.
3	120.00	0.00	4643.54	136.46	1.00	32978619.
4	110.00	0.00	4643.54	136.46	1.00	32978619.
5	100.00	0.00	4643.54	136.46	1.00	32978619.
6	90.00	0.00	4643.54	136.46	1.00	32978619.
7	80.00	0.00	5339.52	188.30	1.00	54606898.
8	71.67	0.00	5339.52	188.30	1.00	54606898.
9	63.33	0.00	5339.52	188.30	1.00	54606898.
10	55.00	0.00	5339.52	188.30	1.00	54606898.
11	46.67	0.00	5339.52	188.30	1.00	54606898.
12	38.33	0.00	5339.52	188.30	1.00	54606898.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4917.48	162.58	1.00	44200839.
26	-78.69	0.00	4917.48	162.58	1.00	44200839.
27	-87.78	0.00	4917.48	162.58	1.00	44200839.
28	-96.67	0.00	4917.48	162.58	1.00	44200839.
29	-105.56	0.00	4917.48	162.58	1.00	44200839.
30	-114.44	0.00	4917.48	162.58	1.00	44200839.
31	-123.33	0.00	4917.48	162.58	1.00	44200839.
32	-132.22	0.00	4917.48	162.58	1.00	44200839.
33	-141.11	1000.00	4917.48	162.58	1.00	44200839.

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN OGN HAMMER

QTIP=.025, MINIMUM WALL THICKNESS=1.5 IN. RU = 14

TABLE 8 -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 14.00

PERMANENT SET OF PILE = .0433 INCHES
 NUMBER OF HITS PER FOOT = 277.24
 TOTAL INTERVALS = 136

SEG	SELEV FT	MAX C STRESS LBS/SQ. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	D MAX (M) IN.	D (M) IN.	V (M) FT/SEC
1	0.00	2281172.	34	0.	74	1.000	1.478018	1.478018	-1.02
2	0.00	1918744.	49	0.	0	1.000	.919705	.889438	-1.52
3	120.00	14390.	51	0.	0	136.443	.891044	.844346	-1.70
4	110.00	14433.	53	0.	0	136.463	.880989	.807410	-1.88
5	100.00	14785.	55	0.	0	136.463	.873315	.768858	-2.06
6	90.00	14820.	57	0.	0	136.463	.868442	.724985	-2.24
7	80.00	10661.	59	0.	0	188.300	.853286	.688132	-2.43
8	71.67	10586.	61	0.	0	188.300	.844471	.663014	-2.54
9	63.33	10528.	64	0.	0	188.300	.833336	.637524	-2.67
10	55.00	10494.	66	0.	0	188.300	.819780	.611782	-2.78
11	46.67	10545.	69	0.	0	188.300	.803615	.585962	-2.89
12	38.33	10719.	72	0.	0	188.300	.784889	.560231	-2.96
13	30.00	12723.	75	0.	0	162.578	.763023	.538816	-2.99
14	21.67	13122.	78	0.	0	162.578	.735179	.506059	-2.99
15	13.33	13600.	81	0.	0	162.578	.704541	.478166	-2.98
16	5.00	14138.	83	0.	0	162.578	.671148	.451200	-2.90
17	-3.33	14618.	86	0.	0	162.578	.635166	.425467	-2.79
18	-11.67	14928.	88	0.	0	162.578	.596826	.400528	-2.70
19	-20.00	15071.	90	0.	0	162.578	.556632	.375786	-2.54
20	-28.33	15051.	92	0.	0	162.578	.515114	.351063	-2.38
21	-36.67	14866.	95	0.	0	162.578	.472482	.325992	-2.18
22	-45.00	14555.	97	0.	0	162.578	.429882	.300649	-2.01
23	-53.33	14090.	100	0.	0	162.578	.385401	.274696	-1.84
24	-61.67	13537.	104	0.	0	162.578	.342021	.248331	-1.72
25	-70.00	12907.	106	0.	0	162.578	.299826	.221730	-1.58
26	-78.69	12145.	107	0.	0	162.578	.256953	.193741	-1.44
27	-87.78	11148.	108	0.	0	162.578	.216935	.166582	-1.32
28	-96.67	9894.	111	0.	0	162.578	.180884	.140916	-1.21
29	-105.56	8543.	112	0.	0	162.578	.148945	.117415	-1.12
30	-114.44	6970.	113	0.	0	162.578	.121881	.096679	-1.04
31	-123.33	5366.	111	0.	0	162.578	.099333	.079401	-.92
32	-132.22	4143.	113	0.	0	162.578	.081680	.066461	-.76
33	-141.11	3154.	114	0.	0	162.578	.068283	.057739	-.58

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN OUN HAMMER

OTYPE 025, MINIMUM WALL THICKNESS 1.5 IN. RU = 14

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS/FT.	RESISTANCE DYNAMIC PT	MAX C STRESS	SEG MAX T STRESS	SEG
TOTAL-TONS FORCE-TONS	LRS/SQ.IN. NO.	LRS/SQ.IN. NO.	LRS/SQ.IN. NO.	
2.24	50	14600	9795	22
3.11	100	14813	8584	22
4.24	150	14820	7380	22
5.70	200	14820	6271	23
7.42	250	14820	5262	23
9.14	300	14820	4673	6
12.23	350	14820	4023	6
13.55	400	14820	3162	6
14.58	450	14820	2300	5
15.03	500	14820	1645	5
17.43	550	14820	1102	4
19.10	600	14820	142	25
20.97	650	14820	0	33
23.08	700	14820	0	33
25.46	750	14820	0	33
28.17	800	14820	0	33
31.28	850	14820	0	33
34.86	900	14820	0	33
39.02	950	14820	0	33
43.90	1000	14820	0	33
49.66	1050	14820	0	33
56.54	1100	14820	0	33
64.82	1150	14820	0	33
74.88	1200	14820	0	33
87.23	1250	14820	0	33
102.46	1300	14820	0	33
121.30	1350	14820	0	33
144.26	1400	14820	0	33
170.24	1450	14820	0	33
200.10	1500	14820	0	33
234.77	1550	14820	0	33
277.24	1600	14820	0	33
330.70	1650	14820	0	33

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
150FT PENETRATION -- VULCAN 040 HAMMER

OTTP=0.025, MINIMUM WALL THICKNESS=1.5 IN. R11 = 14

TABLE 10 -- SPECIFIED BLOW DATA

TIP RESISTANCE PERCENTAGE = 14.00

BLOWS PER FOOT	RESISTANCE TONS
144.26	1400.
200.10	1500.
234.77	1550.
277.24	1600.

JYJ00PZ. 04/20/76. *UNITED COMPUTING* 07. APXY/SL. H.O.24

16.42.21SPIL,CW100,75000.				
16.42.21SFL	64	0.000		
16.42.21SAC3000CRR0023,2777100CC)R				
16.42.21. 04/20/76.JYJ00PZ				
16.42.22.RFL,40000.		0.000		
16.42.22SFL	3592	0.000		
16.42.22SFL	16384	0.000		
16.42.22.WAP,OFF.				
16.42.22SFL	256	0.000		
16.42.22.GET,PILR(CR00024)				
16.42.27.READY * PILB.		0.000	0	0.
16.42.27SFL	4096	0.000		
16.42.27SFL	72	1		
16.42.28.PILH.				
16.42.28SFL00	16384	0.002		
16.42.32SFL01	16384	0.143	190	6
16.42.32SFL REQUIRED TO LOAD			36370R	(15608)
16.42.32SFL REQUIRED TO EXECUTE			30000R	(14336)
16.42.32SFL	16384	0.14R		
16.43.10.END PILDR1				
16.43.10.COST.	14336	22.595	60	5
16.43.10SFL		SERVICE UNITS*	63.0	
16.43.12.		JOB COSTS*	15.74	
16.43.12SFL	12288		7	5
16.43.12.EXIT.				
16.43.12SJT00	236R	22.617		
16.43.12. *FL* *CPU SEC. *DISC PRUS* DISC ACC				
16.43.12. *PRUS*P.F. ACC *TAPE PRUS* TAPE ACC				

Pile Driving Resistance Curves

Pile Diameter	- 36 in.
Minimum Wall Thickness	- 1.5 in.
Penetration	- 200 ft. - 150 ft.
Hammer	- Vulcan 060
Quake Factor, tip	- .10 in.

WAVE EQUATION ANALYSIS FOR 36" DIA. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR AC4R 3-PILE STRUCTURE -- HAMMING 1
 APRIL 19 1976

PROB 1
 36" IN. DIAMETER PILES 3-PILE STRUCTURE
 200 FT PENETRATION -- VULCAN 060 HAMMER
 GPIPE 10 MINIMUM WALL THICKNESS 1.5 IN. RU = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE 1
 NEW HAMMER DATA OPTION 1
 NEW MATERIAL DATA OPTION 1
 NEW PILE SECTION DATA OPTION 1
 NEW SOIL DATA OPTION 1
 SPECIFIED HLOW COUNT OPTION 1
 OUTPUT OPTION FOR STRESS 1
 HPF FOR STRESS OUTPUT OPTION 275.
 ULTIMATE RESISTANCE INCREMENT (TONS) 50.0
 MAX PLUMS FOR RESISTANCE-HLOW CURVE (HPF) 300.
 SPECIFIED SEGMENT LENGTH (FT) --0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION VULCAN 060 HAMMER
 HAMMER EFFICIENCY .75
 HAMMER ENERGY (FT-LBS) 180000.00
 HAMMER EXPLOSIVE FORCE (LBS) --0.00
 NUMBER OF HAMMER SEGMENTS 2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LBS)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	60000.00	1.00	.60	3240000.00
2	1000.00	40200.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES = 1

MATERIAL TYPE	(THD)	UNIT WT. (PCF)	MODULUS (PSI)
1	36.000	490.0	29000000.0

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS 4

NUMBER OF SECTIONS ADDED 0
 LENGTH OF PIPE STANDARD PIPE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER TOP	STATION NUMBER BOTTOM
1	1	1.250	40.	0	40
2	1	1.750	100.	40	140
3	1	1.500	100.	140	240
4	1	1.500	40.	240	320

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE - JSIDE .15
 POINT DAMPENING RESISTANCE - JPPOINT .15
 SOIL SHAKE FOR SIDE - OSIDE .10
 SOIL SHAKE FOR POINT - OPOINT .10

TIP RESISTANCE PERCENTAGE

35.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 060 HAMMER

QTYP=10 ,MINIMUM WALL THICKNESS=1.5 IN. PU = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	ELEV FT.	SLACK IN.	WEIGHT LBS.	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	60000.00	1.00	.60	3240000.
2	0.00	1000.00	40200.00	1.00	.90	32978619.
3	120.00	0.00	4643.54	136.46	1.00	32978619.
4	110.00	0.00	4643.54	136.46	1.00	32978619.
5	100.00	0.00	4643.54	136.46	1.00	32978619.
6	90.00	0.00	4643.54	136.46	1.00	32978619.
7	80.00	0.00	5359.52	188.30	1.00	54606898.
8	71.67	0.00	5359.52	188.30	1.00	54606898.
9	63.33	0.00	5359.52	188.30	1.00	54606898.
10	55.00	0.00	5359.52	188.30	1.00	54606898.
11	46.67	0.00	5359.52	188.30	1.00	54606898.
12	38.33	0.00	5359.52	188.30	1.00	54606898.
13	30.00	0.00	5359.52	188.30	1.00	54606898.
14	21.67	0.00	5359.52	188.30	1.00	54606898.
15	13.33	0.00	5359.52	188.30	1.00	54606898.
16	5.00	0.00	5359.52	188.30	1.00	54606898.
17	-3.33	0.00	5359.52	188.30	1.00	54606898.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4610.13	162.58	1.00	47147562.
26	-78.33	0.00	4610.13	162.58	1.00	47147562.
27	-86.67	0.00	4610.13	162.58	1.00	47147562.
28	-95.00	0.00	4610.13	162.58	1.00	47147562.
29	-103.33	0.00	4610.13	162.58	1.00	47147562.
30	-111.67	0.00	4610.13	162.58	1.00	47147562.
31	-120.00	0.00	4917.48	162.58	1.00	44200839.
32	-128.33	0.00	4917.48	162.58	1.00	44200839.
33	-137.77	0.00	4917.48	162.58	1.00	44200839.
34	-146.67	0.00	4917.48	162.58	1.00	44200839.
35	-155.56	0.00	4917.48	162.58	1.00	44200839.
36	-164.44	0.00	4917.48	162.58	1.00	44200839.
37	-173.33	0.00	4917.48	162.58	1.00	44200839.
38	-182.22	0.00	4917.48	162.58	1.00	44200839.
39	-191.11	1000.00	4917.48	162.58	1.00	44200839.

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200 FT PENETRATION -- VULCAN 060 HAMMER

QTIPS, 10, MINIMUM WALL THICKNESS 1.5 IN. KU = 35

TABLE B -- MAXIMUM STRESS DATA

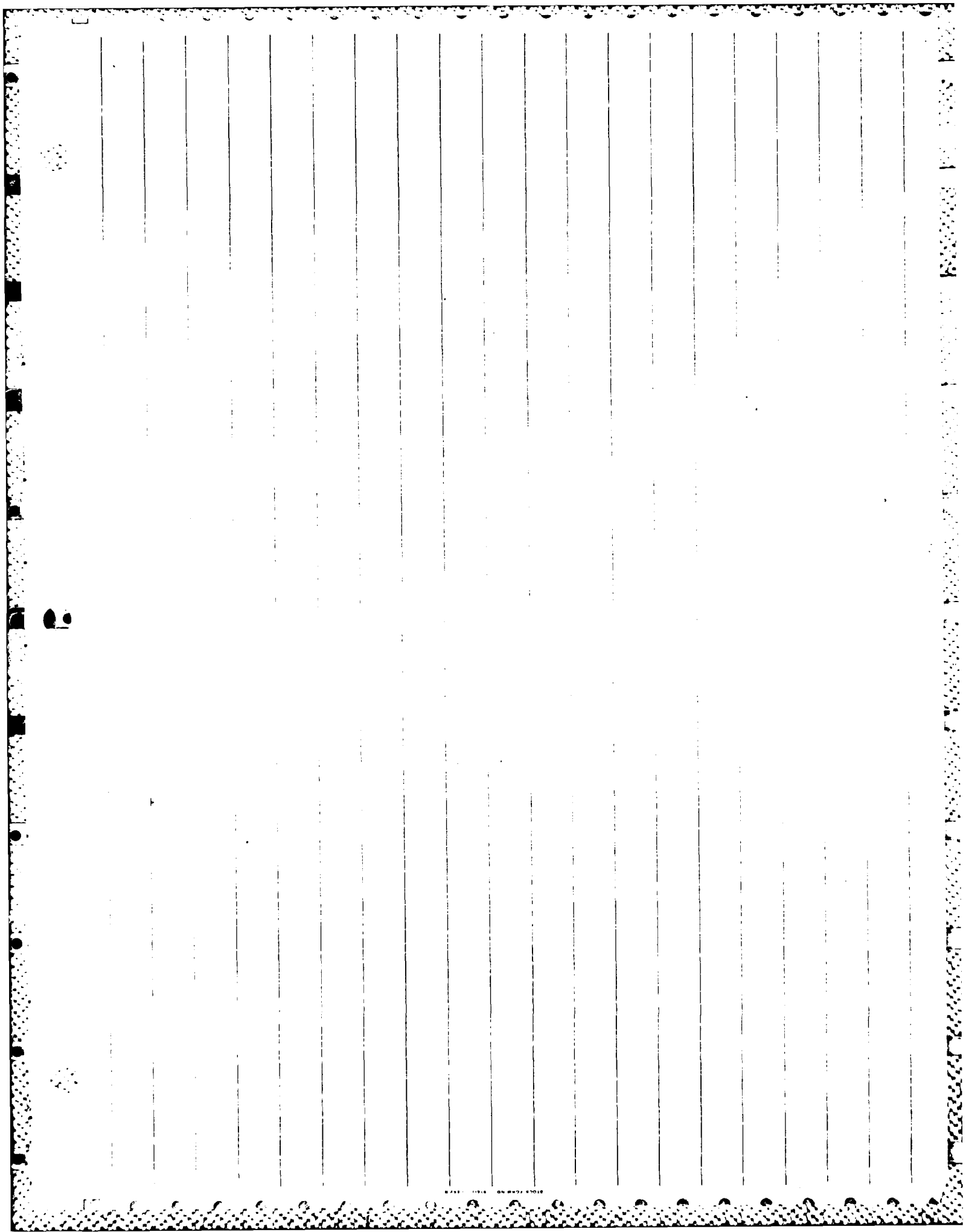
TIP RESISTANCE PERCENTAGE = 35.00

PERMANENT SET OF PILE = .0360 INCHES

NUMBER OF BLOWS PER FOOT = 333.25

TOTAL INTERVALS = 145

SEG	ELEV FT	MAX C STRESS LBS/SG. IN.	TIME N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	DMAX (M) IN.	V (M) FT/SEC
1	0.00	228172.	34	0.	73	1.000	1.486792	1.486708
2	0.00	1919228.	49	0.	0	1.000	.964504	.961827
3	120.00	14413.	51	0.	0	136.463	.933899	.929308
4	110.00	14730.	54	0.	0	136.463	.913054	.905390
5	100.00	14990.	56	0.	0	136.463	.893527	.879821
6	90.00	15141.	58	0.	0	136.463	.882559	.852855
7	80.00	11001.	60	0.	0	188.300	.877403	.824708
8	71.67	11024.	62	0.	0	188.300	.873916	.807084
9	63.33	11028.	64	0.	0	188.300	.869511	.788956
10	55.00	11003.	66	0.	0	188.300	.863949	.770463
11	46.67	10967.	68	0.	0	188.300	.856977	.751757
12	38.33	10945.	70	0.	0	188.300	.848436	.732065
13	30.00	10949.	73	0.	0	188.300	.838179	.714184
14	21.67	10986.	75	0.	0	188.300	.826122	.695541
15	13.33	11060.	78	0.	0	188.300	.812126	.677139
16	5.00	11181.	80	0.	0	188.300	.796199	.658993
17	-3.33	11328.	83	0.	0	188.300	.778336	.641060
18	-11.67	11479.	86	0.	0	188.300	.758587	.623236
19	-20.00	13421.	88	0.	0	162.578	.737108	.605317
20	-28.33	13497.	90	0.	0	162.578	.710840	.584220
21	-36.67	13429.	93	0.	0	162.578	.683440	.562721
22	-45.00	13510.	95	0.	0	162.578	.655023	.540851
23	-53.33	13437.	97	0.	0	162.578	.625787	.518642
24	-61.67	13316.	100	0.	0	162.578	.596111	.496217
25	-70.00	13147.	102	0.	0	162.578	.566120	.473596
26	-78.33	12953.	104	0.	0	162.578	.536143	.450748
27	-86.67	12852.	106	0.	0	162.578	.505704	.427756
28	-95.00	12731.	109	0.	0	162.578	.474638	.404474
29	-103.33	11904.	111	0.	0	162.578	.442548	.380903
30	-111.67	11422.	112	0.	0	162.578	.409845	.356819
31	-120.00	11164.	119	0.	0	162.578	.377000	.332301
32	-128.89	10984.	121	0.	0	162.578	.342531	.305786
33	-137.78	10715.	123	0.	0	162.578	.309196	.279225
34	-146.67	10291.	125	0.	0	162.578	.276540	.253493
35	-155.56	9812.	129	0.	0	162.578	.242777	.228548
36	-164.44	9058.	129	0.	0	162.578	.212768	.204308
37	-173.33	8833.	131	0.	0	162.578	.184550	.180687
38	-182.22	7869.	130	0.	0	162.578	.159182	.157817



PRCB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 200FT PENETRATION -- VULCAN 060 HAMMER

OTYPE, 10 MINIMUM WALL THICKNESS=1.5 IN. HU # 35

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 35.00

BLOWS/FT.	RESISTANCE DYNAMIC PT TOTAL TONS FORCE-TONS	MAX C STRESS LRS/SQ. IN. MIN.	SEG MAX T STRESS LRS/SQ. IN. MIN.	SEG
2.02	50.	14094.	9944.	28
2.89	100.	15141.	8708.	27
4.07	150.	15141.	7564.	28
5.59	200.	15141.	6471.	28
7.43	250.	15141.	5400.	28
9.30	300.	15141.	4484.	28
11.45	350.	15141.	4045.	6
13.98	400.	15141.	3248.	6
15.41	450.	15141.	2206.	6
17.02	500.	15141.	1488.	5
18.83	550.	15141.	717.	30
20.89	600.	15141.	106.	30
23.25	650.	15141.	0.	39
25.94	700.	15141.	0.	39
29.15	750.	15141.	0.	39
32.49	800.	15141.	0.	39
37.34	850.	15141.	0.	39
42.71	900.	15141.	0.	39
49.27	950.	15141.	0.	39
57.45	1000.	15141.	0.	39
67.85	1050.	15141.	0.	39
81.41	1100.	15141.	0.	39
99.68	1150.	15141.	0.	39
125.22	1200.	15141.	0.	39
163.07	1250.	15141.	0.	39
223.76	1300.	15141.	0.	39
333.25	1350.	15141.	0.	39

PROB 1 36-IN. DIAMETER PILES 3-PILE STRUCTURE
200BT PENETRATION -- VULCAN OAD HAMMER

OTIPS.10 , MINIMUM WALL THICKNESS=1.5 IN. RI = 35

TABLE 10 -- SPECIFIED HDM DATA

TIP RESISTANCE PERCENTAGE = 35.00

HDM'S PER FOOT	RESISTANCE TONS
125.22	1200.
223.76	1300.
243.43	1512.
291.94	1335.

WAVE EQUATION ANALYSIS FOR 36-IN. DIAMETER PIPE PILES
 MC CLELLAND REPORT DATA FOR ACRP 3-PILE STRUCTURE -- MORING 1
 APRIL 19 1976

PROB 2
 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 060 HAMMER
 OTIPS, 10, MINIMUM WALL THICKNESS=1.5 IN. RII = 35

TABLE 1 -- PROGRAM CONTROL DATA

PILE TYPE	1
NEW HAMMER DATA OPTION	1
NEW MATERIAL DATA OPTION	1
NEW PILE SECTION DATA OPTION	1
NEW SOIL DATA OPTION	1
SPECIFIED FLOW CURVE OPTION	1
OUTPUT OPTION FOR STRESS	1
RPF FOR STRESS OUTPUT OPTION	275.
ULTIMATE RESISTANCE INCREMENT (TONS)	50.0
MAX ALLOWS FOR RESISTANCE-FLOW CURVE (HPF)	300.
SPECIFIED SEGMENT LENGTH (FT)	-0.00

TABLE 2 -- HAMMER DATA

HAMMER DESCRIPTION	VULCAN 060 HAMMER
HAMMER EFFICIENCY	.75
HAMMER ENERGY (FT-LBS)	180000.00
HAMMER EXPLOSIVE FORCE (LBS)	-0.00
NUMBER OF HAMMER SEGMENTS	2

SEGMENT NUMBER	SLACK (IN)	WEIGHT (LB)	AREA (SQ IN)	COEF OF RESTITUTION	SPRING CONSTANT (LR / IN)
1	1000.00	60000.00	1.00	.60	3240000.00
2	1000.00	40200.00	1.00	.90	0.00

TABLE 3 -- MATERIAL DATA

NUMBER OF MATERIAL TYPES	1
MATERIAL TYPE	1
(TON)	36.000
UNIT WT. (PCF)	490.0
MODULUS (PSI)	29000000.

TABLE 4 -- PILE SECTION DATA

TOTAL NUMBER OF PILE SECTIONS	4
-------------------------------	---

NUMBER OF SECTIONS ADDED 6
 LENGTH OF PIPE STANDING PILE (FT) 120.00

SECTION NUMBER	MATERIAL TYPE	WALL THICKNESS (IN)	LENGTH (FT)	STATION NUMBER	
				TIP	BOTTOM
1	1	1.250	40.	0	40
2	1	1.750	50.	40	90
3	1	1.500	100.	90	190
4	1	1.500	40.	190	270

TABLE 5 -- SOIL DATA

NUMBER OF TIP RESISTANCE PERCENTAGES 1
 SIDE DAMPENING RESISTANCE • JSIDE .15
 POINT DAMPENING RESISTANCE • JPOINT .15
 SOIL SHAKE FOR SIDE • OSIDE .10
 SOIL SHAKE FOR POINT • OPOINT .10

TIP RESISTANCE PERCENTAGE 35.0000

TABLE 6 -- SPECIFIED BLOW COUNT DATA

NUMBER OF SPECIFIED BLOW COUNTS 4

BLOWS PER FOOT	TOLERANCE
150.	25.
200.	25.
250.	25.
300.	25.

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- WULCAN 060 HAM-HP

OTTPR,10 ,MINIMUM WALL THICKNESSE1.5 IN. MU = 35

TABLE 7 -- PILE SEGMENT DATA

SEGMENT	FLY FT	SLACK IN.	WEIGHT LBS	AREA SQ. IN.	COEF RSTTU	SPR STIFF LBS/IN.
1	0.00	1000.00	60000.00	1.00	.60	3240000.
2	0.00	1000.00	40200.00	1.00	.90	32978619.
3	120.00	0.00	4643.50	136.46	1.00	32978619.
4	110.00	0.00	4643.50	136.46	1.00	32978619.
5	100.00	0.00	4643.50	136.46	1.00	32978619.
6	90.00	0.00	4643.50	136.46	1.00	32978619.
7	80.00	0.00	5339.52	188.30	1.00	54606898.
8	71.67	0.00	5339.52	188.30	1.00	54606898.
9	63.33	0.00	5339.52	188.30	1.00	54606898.
10	55.00	0.00	5339.52	188.30	1.00	54606898.
11	46.67	0.00	5339.52	188.30	1.00	54606898.
12	38.33	0.00	5339.52	188.30	1.00	54606898.
13	30.00	0.00	4610.13	162.58	1.00	47147562.
14	21.67	0.00	4610.13	162.58	1.00	47147562.
15	13.33	0.00	4610.13	162.58	1.00	47147562.
16	5.00	0.00	4610.13	162.58	1.00	47147562.
17	-3.33	0.00	4610.13	162.58	1.00	47147562.
18	-11.67	0.00	4610.13	162.58	1.00	47147562.
19	-20.00	0.00	4610.13	162.58	1.00	47147562.
20	-28.33	0.00	4610.13	162.58	1.00	47147562.
21	-36.67	0.00	4610.13	162.58	1.00	47147562.
22	-45.00	0.00	4610.13	162.58	1.00	47147562.
23	-53.33	0.00	4610.13	162.58	1.00	47147562.
24	-61.67	0.00	4610.13	162.58	1.00	47147562.
25	-70.00	0.00	4917.48	162.58	1.00	44200839.
26	-78.33	0.00	4917.48	162.58	1.00	44200839.
27	-86.67	0.00	4917.48	162.58	1.00	44200839.
28	-95.00	0.00	4917.48	162.58	1.00	44200839.
29	-103.33	0.00	4917.48	162.58	1.00	44200839.
30	-111.67	0.00	4917.48	162.58	1.00	44200839.
31	-120.00	0.00	4917.48	162.58	1.00	44200839.
32	-128.33	0.00	4917.48	162.58	1.00	44200839.
33	-136.67	1000.00	4917.48	162.58	1.00	44200839.

PROB 2 36-IN. DIAMETER PILES 3-PILE STRUCTURE
 150FT PENETRATION -- VULCAN OAK HAMMER

QTIPS: 10 .MINIMUM WALL THICKNESS: 1.5 IN. RI = 35

TABLE B -- MAXIMUM STRESS DATA

TIP RESISTANCE PERCENTAGE = 35.00

PERMANENT SET OF PILE = .0412 INCHES
 NUMBER OF BLOWS PER FOOT = 291.15
 TOTAL INTERVALS = 140

SEC	ELEV FT	MAX C. STRESS LBS/SQ. IN.	TYPE N	MAX T STRESS LBS/SQ. IN.	TIME N	AREA SQ. IN.	DMAX(M) IN.	D(M) IN.	V(M) FT/SEC
1	0.00	228177.	34	0.	74	1.000	1.493421	1.493421	-.04
2	0.00	191874.	49	0.	0	1.000	.926801	.926801	1.10
3	120.00	14390.	51	0.	0	136.463	.846652	.846652	1.21
4	110.00	14633.	53	0.	0	136.463	.855108	.855108	1.33
5	100.00	14745.	55	0.	0	136.463	.822221	.822221	1.45
6	90.00	14820.	57	0.	0	136.463	.81894	.81894	1.56
7	80.00	10461.	59	0.	0	148.300	.873053	.873053	1.70
8	71.67	10545.	61	0.	0	148.300	.866136	.866136	1.80
9	63.33	10522.	64	0.	0	148.300	.857402	.857402	1.94
10	55.00	10443.	66	0.	0	148.300	.846647	.846647	2.08
11	46.67	10496.	69	0.	0	148.300	.833858	.833858	2.21
12	38.33	10403.	72	0.	0	148.300	.818795	.818795	2.33
13	30.00	12480.	74	0.	0	162.578	.801580	.801580	2.41
14	21.67	12746.	77	0.	0	162.578	.779347	.779347	2.47
15	13.33	13067.	80	0.	0	162.578	.754865	.754865	2.51
16	5.00	13443.	82	0.	0	162.578	.728178	.728178	2.54
17	-3.33	13746.	84	0.	0	162.578	.699305	.699305	2.53
18	-11.67	14036.	87	0.	0	162.578	.668504	.668504	2.51
19	-20.00	14143.	89	0.	0	162.578	.636184	.636184	2.49
20	-28.33	14230.	91	0.	0	162.578	.602791	.602791	2.48
21	-36.67	14149.	94	0.	0	162.578	.568097	.568097	2.44
22	-45.00	14004.	96	0.	0	162.578	.531446	.531446	2.37
23	-53.33	13714.	98	0.	0	162.578	.494418	.494418	2.26
24	-61.67	13301.	101	0.	0	162.578	.456065	.456065	2.06
25	-70.00	13070.	105	0.	0	162.578	.417424	.417424	1.90
26	-78.49	12844.	108	0.	0	162.578	.376527	.376527	1.76
27	-87.78	12354.	110	0.	0	162.578	.336952	.336952	1.64
28	-96.67	11406.	109	0.	0	162.578	.298417	.298417	1.52
29	-105.56	10942.	112	0.	0	162.578	.260653	.260653	1.42
30	-114.44	10198.	116	0.	0	162.578	.224591	.224591	1.32
31	-123.33	9493.	118	0.	0	162.578	.193105	.193105	1.21
32	-132.22	8549.	117	0.	0	162.578	.165548	.165548	1.06
33	-141.11	6864.	119	0.	0	162.578	.141216	.141216	.89

PROB Z 36-IN. DIAMETER PILES S-PILE STRUCTURE
 150FT PENETRATION -- VULCAN 060 HAMMER

OTIP=10, MINIMUM WALL THICKNESS=1.5 IN. MU = 35

TABLE 9 -- RESISTANCE-BLOW CURVE DATA

TIP RESISTANCE PERCENTAGE = 35.00		BLOWS/FT. RESISTANCE DYNAMIC PT		MAX C STRESS		SEG MAX T STRESS		SEG
TOTAL-TONS FORCE=TONS	RESISTANCE DYNAMIC PT	LBS/SQ. IN. (NO.)	LBS/SQ. IN. (NO.)	LBS/SQ. IN. (NO.)	LBS/SQ. IN. (NO.)	LBS/SQ. IN. (NO.)	LBS/SQ. IN. (NO.)	
50	51.19	14820.	5	9707.	22			
100	98.03	14820.	6	8428.	22			
150	140.85	14820.	6	7148.	22			
200	180.11	14820.	6	5960.	22			
250	216.15	14820.	6	5001.	6			
300	249.25	14820.	6	4329.	6			
350	279.67	14820.	6	3369.	6			
400	307.66	14820.	6	2430.	5			
450	333.43	14820.	6	1789.	5			
500	357.19	14820.	6	1174.	4			
550	379.09	14820.	6	751.	4			
600	399.31	14820.	6	0.	33			
650	417.97	14820.	6	0.	33			
700	435.17	14820.	6	0.	33			
750	450.96	14820.	6	0.	33			
800	465.08	14820.	6	0.	33			
850	478.77	14820.	6	0.	33			
900	490.99	14820.	6	0.	33			
950	502.36	14820.	6	0.	33			
1000	512.77	14820.	6	0.	33			
1050	521.95	14820.	6	0.	33			
1100	530.18	14820.	6	0.	33			
1150	537.31	14820.	6	0.	33			
1200	543.75	14820.	6	0.	33			
1250	549.79	14820.	6	0.	33			
1300	554.63	14820.	6	0.	33			
1350	557.98	14820.	6	0.	33			
1400	562.08	14820.	6	0.	33			

PROB 2 36 IN. DIAMETER PILES 3-PILE STRUCTURE
150 FT PENETRATION -- VULCAN OGD HAMMER

OTTPS, 10, MINIMUM WALL THICKNESS 1.5 IN. RU = 35

TABLE 10 -- SPECIFIED HDW DATA

TYP RESISTANCE PERCENTAGE = 35.00

HLDWS PER FOOT	RESISTANCE TONS
153.96	1250.
205.01	1300.
243.55	1326.
291.15	1350.

1A.08.14SPIL*CM100,71000.				
1A.08.14SF1	44	0.000		
1A.08.15SACS00CARR023,2777100CC 3H				
1A.08.15. 04/20/74. JYJOPNC				
1A.08.15.PFL,40000.				
1A.08.16SF1	5392	0.001		
1A.08.16SF1	16384	0.001		
1A.08.16.PAP,OFF.				
1A.08.16SF1	250	0.001		
1A.08.16.GET,PTLH(CRAG024)				
1A.08.19.READY = PILB	0	0.001	0	0.
1A.08.19SF1	4096			
1A.08.19SF1	72	1		
1A.08.19.PILB.				
1A.08.19SF100 16384	0.001			
1A.08.20SF101 16384	0.139	190		6
1A.08.20.FL REQUIRED TO LOAD			363708 (-15608)	
1A.08.20.FL REQUIRED TO EXECUTE			340008 (14336)	
1A.08.20SF1	16384	0.143		
1A.08.49.END PILDRI				
1A.08.49.CDST.				
1A.08.49SF1	14336	21.092	58	6
1A.08.50.		SERVICE UNITS	59.1	
1A.08.50.		JOB COSTS	14.77	
1A.08.50SF1	12288	21.111	7	5
1A.08.50.FXII.				
1A.08.50SJT00	2368	21.111		
1A.08.50.		*FL* *CPU SEC. *DISC PRUS* DISC ACC		
1A.08.50.*P.F.*PRUS*P.F.*ACC *IAPE PRUS* TAPE ACC				

A-3 LATERALLY LOADED PILE CAPACITY

C. CHERN 00442705 9107 LFC9011 SYS.56

LL	EEEEEEEEEE	CCCCCCCC	9999999999	000000	11	000000	11
LL	EEEEEEEEEE	CCCCCCCC	9999999999	0000000000	111	0000000000	111
LL	EE	CC	99	00	1111	00	1111
LL	EE	CC	99	00	11	00	11
LL	EE	CC	99	00	11	00	11
LL	EEEEEEEE	CC	99	00	11	00	11
LL	EEEEEEEE	CC	9999999999	00	11	00	11
LL	EEEEEEEE	CC	9999999999	00	11	00	11
LL	EE	CC	99	00	11	00	11
LL	EE	CC	99	00	11	00	11
LL	EE	CC	99	00	11	00	11
LL	EEEEEEEEEE	CCCCCCCC	9999999999	0000000000	11111	0000000000	11111
LL	EEEEEEEEEE	CCCCCCCC	9999999999	0000000000	11111	0000000000	11111

JJ	0000000000	HHHHHHHHHH	9999999999	11	000000	7777777777
JJ	0000000000	HHHHHHHHHH	9999999999	111	0000000000	7777777777
JJ	00	HH	99	1111	00	77
JJ	00	HH	99	11	00	77
JJ	00	HH	99	11	00	77
JJ	00	HH	9999999999	11	00	77
JJ	00	HH	9999999999	11	00	77
JJ	00	HH	99	11	00	77
JJ	00	HH	99	11	00	77
JJ	00	HH	99	11	00	77
JJ	0000000000	HHHHHHHHHH	9999999999	11111	0000000000	77
JJ	0000000000	HHHHHHHHHH	9999999999	11111	0000000000	77

SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GGGGGGGGGG
SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GGGGGGGGGG
SS	SS	YY	YY	MM	MM	SS	GG
SS	SS	YY	YY	MM	MM	SS	GG
SS	SS	YY	YY	MM	MM	SS	GG
SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GG
SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GG
SS	SS	YY	YY	MM	MM	SS	GGGG
SS	SS	YY	YY	MM	MM	SS	GGGG
SS	SS	YY	YY	MM	MM	SS	GG
SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GGGGGGGGGG
SS	SSSSSSSSSS	YY	YY	MM	MM	SSSSSSSSSS	GGGGGGGGGG

C. CHERN 00442705 9107 LFC9011 SYS.56

ISV40 JOB ORIGIN FROM GROUP=0027 , DSPSCR , DEVIC=H027AD1, DAS
 //LEC9011 JOB (00042705002777100)LEC27011,IC,CHERN ,PRTY=4,CLASS=A,C

// TIME=(005),REGIN=25AK
 //MATTN LINES=(005,1),CARMS=(00,C)
 //JNLIB DD DS=CPROD,LIR03,DISP=SHR
 // EXEC PGM=STKXCG97
 //PT06F001 DD SYSUTEA
 //PT05F001 DD *

LEC9011 IFF4037 LFC9011 STARTED TIME=18.13.41
 LEC9011 IFF234E D BAH,ASPAH P106F001
 *LEC9011 007 IECASPO BAH IS LEC9011 A ASP10001
 *LEC9011 00K IECASPO 0M2 IS LEC9011
 LEC9011 IFF202E K 0M2=01910701,LEC9011,
 LEC9011 T1=LEC9011 CC=0404705 P=2777100 T J=LEC27011 REC,CHERN ABQ107
 //LFC9011 IFF404J LFC9011 ENDF TIME=18.14.05
 //LFC9011 JOB (00042705002777100)LEC27011,IC,CHERN ,PRTY=4,CLASS=A,*
 // TIME=(005),REGIN=25AK
 //JNLIR DD DS=CPROD,LIR03,DISP=SHR
 // EXEC PGM=STKXCG97

//PT06F001 DD SYSUTEA
 //PT05F001 DD UNIT=(CTC,OFFER),DSDNAM=ASPI0001,
 //DISP=(OLD,DELETE),VOL=SER=019107,DCH=(LRECL=80,RLKSIZE=80,RECFM=F)
 //
 // IFF2357 ALLUC. FOR LFC9011
 // IFF2371 107 ALLOCATED TO JNLIR
 // IFF2371 0AH ALLOCATED TO PT06F001
 // IFF2371 0M2 ALLOCATED TO PT05F001
 // IFF1421 = STEP WAS EXECUTED - COND CODE 0000
 // IFF2851 DCPROD,LIR03 PASSED
 // IFF2851 VOL SER NOS= DC5002. DELETED
 // IFF2851 SYS76113,1M1312,RV001,LFC9011,ASPD001 DELETED
 // IFF2851 VOL SER NOS= ASP6A8.
 // IFF2851 SYS76113,1M1312,RV001,LFC9011,ASPI0001 DELETED
 // IFF2851 VOL SER NOS= 019107.
 // IFF3731 STEP / / START 70113.1813
 // IFF3741 STEP / / STOP 70113.1813 CPU 0M1M 01.33SEC STOR VIRT 100M

PAGES DATA ACQUISITION SYSTEM

* STEP NAME START TIME 18.13.40.80 MAIN CORE RECD 250 K LCS CORE RECD 0 K STEP CPU 00.00.01.33 *
 * PGM NAME STKXCG97 STOP TIME 18.13.58.61 MATTN CORE USED 100 K LCS CORE USED 0 K JOB CPU 00.00.01.33 *
 * DISPATCH PRTY 1 FLAP. TIME 00.00.17.75 MAIN CORE HRRAD 0 K LCS CORE HRRAD 0 K CONDITION CODE 0000 *

EXCP STATISTICS

UNIT	EXCP COUNT	UNIT	EXCP COUNT	UNIT	EXCP COUNT	UNIT	EXCP COUNT
347	0	BAH	424	0M2	42	EXCP TOTAL	470
EXCP STATISTICS							
IEF57411 STEP/DCPR00,LIR03 / TOTAL EXCP 000070							
IEF2851 VOL SER NOS= DC5002.							
IEF3751 JOB /LEC9011 / START 70113.1813							

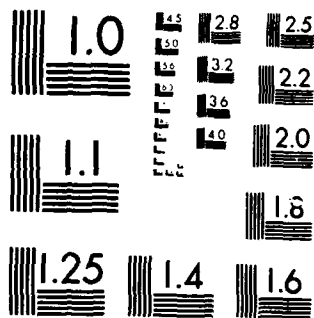
C.CHEMN 00442705 9107 A LFC9011 5106001

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JJ	UU	HH	99	00	11	77
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FF	TTTTTTTTTT	UUUUUUUU	HHHHHHHHHH	FF	FF	11111
FF	TTTTTTTTTT	UUUUUUUU	HHHHHHHHHH	FF	FF	11111

C.CHEMN 00442705 9107 A LFC9011 FT06F001



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

LATERALLY LOADED PILE PROGRAM

HEAD COLUMN ANALYSIS USING RIGID LINK FINITE ELEMENT TECHNIQUES

NUMBER OF PROBLEMS IN SET = 1

GENERAL PROBLEM TITLE = 3-PILE ACRS STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

PROBLEM DESCRIPTION = MULTIPLE CONDITIONS YES, 8KIP NETS727251 P81460KIP TENSION

TABLE 1 - PROGRAM CONTROL DATA FOR PUNCH NO. 1

PRIOR DATA OPTIONS (HOLD = 1) DEF.S. 2 5 4A 4B 5
0 0 0 0 0 0 0

NUMBER OF CARDS INPUT THIS PROBLEM TABLE NUMBER
2 3 4A 4B 5
1 0 2 5 30

LIST OF JOINT STATIONS = 5 10 15 20 30

TABLE 2 - CONSTANTS AND ITERATION CONTROL DATA

NUMBER OF INCREMENTS = 60
CALCULATE STRESSES (YES = 1) (NO = 0) 1
INCREMENT LENGTH = 0.3600 02
MAXIMUM ALLOWABLE DEFLECTION = 0.1000 03
DEFLECTION CONTROL TOLERANCE = 0.1000 02
MODULUS OF ELASTICITY = 0.3000 05
PILE RADIUS = 0.1400 02
STA. AT WHICH FORCES AND DEFLECTIONS SPECIFIED FOR RETENTION = 1

DEFLECTION CLOSURE TOLERANCE LESS THAN 0.001 SUGGESTED

TABLE 3 - SPECIFIED DEFLECTIONS AND SLOPES

STATION	CASE	DEFLECTION	SLOPE
			NONE SPECIFIED

TABLE 04 - PILE PROPERTIES

PROGRAM AUTOMATICALLY AVERAGES MOMENT UP INERTIA
AND AREA VALUES AT CHANGES IN A AND T THUS, T
VALUES FOR TIP AND MIDDLE ELEMENTS ARE HALVED.

FROM STA.	TO STA.	T	A
0	7	0.2770 05	0.1880 03
7	40	0.2420 05	0.1630 03

TABLE OF - PILE LOADINGS

FROM	TO	CONT.	Q	S	T	R	P
0	0	0	0.5180 02	0.0	0.0	0.7330 07	0.0
0	1	1	0.0	0.0	0.0	0.0	0.1460 04
7	1	1	0.0	0.0	0.0	0.0	0.1260 04
33	1	1	0.0	0.0	0.0	0.0	0.8600 03
48	0	0	0.0	0.0	0.0	0.0	0.2000 02

PROGRAM ASSUMES LOADING OF TABLE 48 AND 5 IS APPLIED AS
 CONCENTRATED LOADING AT INCREMENT POINTS. THEORETICAL SPRINGS
 CONNECTING RIGID FINITE ELEMENTS ARE LOCATED AT INCREMENT POINTS.

TABLE 5 - MULTIPLIER LOAD AND SUPPORT CURVES

FROM TO CONT. MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

0 1 -0.3000-01 0.1000-02 2 1

ACTUAL Q-W CURVE POINTS

0 0.3000 04 0.0 -0.3000 04

1 -0.9900 02 -0.9900 02 0.9900 02 0.9900 02

FROM TO CONT. MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

2 1 -0.3000-01 0.1000-02 2 1

ACTUAL Q-W CURVE POINTS

0 0.3000 04 0.0 -0.3000 04

1 -0.9900 02 -0.9900 02 0.9900 02 0.9900 02

FROM TO CONT. MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

3 1 -0.3000-01 0.1000-02 4 1

ACTUAL Q-W CURVE POINTS

0 0.8790 01 0.8790 01 0.8790 01 0.5220 01 0.4320 01 0.3060 01

1 -0.9900 02 -0.2000 02 -0.1130 01 -0.5000 00 -0.3000 00 -0.7000-01 -0.1600-01

2 -0.3060 01 -0.4320 01 -0.5220 01 -0.8790 01 -0.8790 01 -0.8790 01 -0.8790 01

3 0.1600-01 0.7000-01 0.1000-02 0.3000 00 0.5000 00 0.1130 01 0.2000 02 0.9900 02

FROM TO CONT. MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

5 1 -0.3000-01 0.1000-02 4 1

ACTUAL D-W CURVE POINTS

0	0.6900 02	0.4900 02	0.6900 02	0.5560 02	0.4300 02	0.530 02	0.2070 02	0.7980 01
1	-0.0990 02	-0.2000 02	-0.1130 01	-0.5000 00	-0.2900 00	-0.1700 00	-0.6300 01	-0.9000 02
2	-0.7000 01	-0.2070 02	-0.3330 02	-0.4300 02	-0.5560 02	-0.8900 02	-0.6900 02	-0.8900 02
3	0.9000 02	0.6500 01	0.1700 00	0.2900 00	0.5000 00	0.1130 01	0.2000 02	0.9990 02

FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

7 1 -0.5000 01 0.1000 02 4 1

ACTUAL D-W CURVE POINTS

0	0.1870 03	0.1870 03	0.1870 03	0.1170 03	0.9000 02	0.7110 02	0.4560 02	0.2290 02
1	-0.9000 02	-0.2000 02	-0.1130 01	-0.5000 00	-0.3000 00	-0.1800 00	-0.7100 01	-0.1700 01
2	-0.2900 02	-0.4560 02	-0.7110 02	-0.9000 02	-0.1170 03	-0.1870 03	-0.1870 03	-0.1870 03
3	0.1700 01	0.7100 01	0.1800 00	0.3000 00	0.5000 00	0.1130 01	0.2000 02	0.9990 02

FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

9 1 -0.3000 01 0.1000 02 8 1

ACTUAL D-W CURVE POINTS

0	0.2090 03	0.2090 03	0.2090 03	0.1310 03	0.1010 03	0.7880 02	0.4950 02	0.2180 02
1	-0.9990 02	-0.2000 02	-0.1130 01	-0.5000 00	-0.2900 00	-0.1700 00	-0.6600 01	-0.1200 01
2	-0.2180 02	-0.4950 02	-0.7880 02	-0.1010 03	-0.1310 03	-0.2090 03	-0.2090 03	-0.2090 03
3	0.1200 01	0.6600 01	0.1700 00	0.2900 00	0.5000 00	0.1130 01	0.2000 02	0.9990 02

FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

12 1 -0.5000 01 0.1000 02 4 1

ACTUAL D-W CURVE POINTS

0	0.4920 03	0.4920 03	0.4920 03	0.3070 03	0.2420 03	0.1940 03	0.1500 03	0.8970 02
1	-0.9990 02	-0.2000 02	-0.1130 01	-0.5000 00	-0.3000 00	-0.1900 00	-0.9000 01	-0.3800 01
2	-0.8970 02	-0.1500 03	-0.1940 03	-0.2420 03	-0.3070 03	-0.4920 03	-0.4920 03	-0.4920 03

0.38000-01 0.90000-01 0.1900 0 0.5000 00 0.1130 01 0.2000 02 0.9900 03
 FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY
 19 1 -0.3000-01 0.1000-02 8 1

ACTUAL NEW CURVE POINTS

0 0.7650 03 0.7650 03 0.4741 03 0.3377 03 0.3020 03 0.2100 03 0.1400 03
 1 -0.9990 02 -0.2000 02 -0.1130 01 -0.3000 01 -0.1900 00 -0.9000-01 -0.3800-01
 2 -0.1400 03 -0.2100 03 -0.3020 03 -0.4780 03 -0.7650 03 -0.7650 03 -0.7650 03
 3 0.3800-01 0.9000-01 0.1900 00 0.3000 00 0.1130 01 0.2000 02 0.9990 02

FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

20 1 -0.5000-01 0.1000-02 8 1

ACTUAL NEW CURVE POINTS

0 0.1070 04 0.1070 04 0.6660 03 0.5250 03 0.4210 03 0.2920 03 0.1900 03
 1 -0.9990 02 -0.2000 02 -0.1130 01 -0.5000 00 -0.1900 00 -0.9000-01 -0.3800-01
 2 -0.1900 03 -0.2920 03 -0.4210 03 -0.5250 03 -0.6660 03 -0.1070 04 -0.1070 04
 3 0.3800-01 0.9000-01 0.1900 00 0.3000 00 0.1130 01 0.2000 02 0.9990 02

FROM TO CONT. MULTIPLIER MULTIPLIER TOTAL NO. OF POINTS SYMMETRY

49 1 -0.5000-01 0.1000-02 8 1

ACTUAL NEW CURVE POINTS

0 0.1990 04 0.1990 04 0.1250 04 0.9430 03 0.7880 03 0.5470 03 0.3640 03
 1 -0.9990 02 -0.2000 02 -0.1130 01 -0.5000 00 -0.1900 00 -0.9000-01 -0.3800-01
 2 -0.3640 03 -0.5470 03 -0.7880 03 -0.9430 03 -0.1250 04 -0.1990 04 -0.1990 04
 3 0.3800-01 0.9000-01 0.1900 00 0.3000 00 0.1130 01 0.2000 02 0.9990 02

PROBLEM NUMBER = 1

PROBLEM DESCRIPTION = MUDLINE CONDITIONS V=51, BKTP R=7327251 BR1460KTP TENSION

ITERATION MONITOR DATA

ITER. NO.	DIFF. CURVES	NO. STAS. NOT CLOSED	5	10	15	20	30
1	NO	15	0.2490=01	-0.2990=02	0.2120=04	0.1610=04	0.9230=07
2	NO	9	0.4930=01	-0.3670=02	-0.1400=03	0.3530=04	0.1320=06
3	NO	9	0.5510=01	-0.3610=02	-0.1800=03	0.3880=04	0.1350=06
4	NO	9	0.5510=01	-0.3610=02	-0.1800=03	0.3880=04	0.1350=06

RESULTS

STA.	DIST. ALONG PILE	DEPL.	SLOPE	MOMENT	HEAD COLUMN SHEAR	APPLIED NON LINEAR LATERAL LOADING	COMBINED STRESS(MAX.)
0	0.0	0.200	-0.64420-013	-0.4750 04	50.635	0.0	10.854
1	36.000	0.170	-0.81450-013	-0.2930 04	50.535	0.0	9.515
2	72.000	0.147	-0.90140-013	-0.1110 04	50.535	0.0	8.181
3	108.000	0.114	-0.91040-013	0.7150 03	48.209	-4.679	7.773
4	144.000	0.082	-0.84370-013	0.2370 04	30.141	-13.607	8.695
5	180.000	0.053	-0.71600-013	0.3530 04	23.354	-16.351	9.301
6	216.000	0.030	-0.55180-013	0.4050 04	4.149	-20.684	9.484
7	252.000	0.013	-0.37570-013	0.3850 04	-15.071	-18.058	9.833
8	288.000	0.003	-0.21300-013	0.2960 04	-26.317	-4.841	9.838
9	324.000	-0.002	-0.92540-011	0.1430 04	-26.770	3.630	8.977
10	360.000	-0.000	-0.19470-014	0.1030 04	-21.260	7.209	8.216
11	396.000	-0.005	0.16270-014	0.4000 03	-13.939	7.307	7.650
12	432.000	-0.002	0.27140-014	0.3660 02	-7.595	5.716	7.281
13	468.000	-0.001	0.24600-014	-0.1330 03	-2.735	3.611	7.262
14	504.000	-0.001	0.17190-014	-0.1660 03	-0.049	1.774	7.193
15	540.000	-0.000	0.06830-015	-0.1360 03	1.094	0.526	7.076
16	576.000	-0.000	0.41330-015	-0.8760 02	1.277	-0.107	6.946
17	612.000	0.000	0.86240-016	-0.4430 02	1.006	-0.348	6.819
18	648.000	0.000	0.61140-016	-0.1510 02	0.820	-0.381	6.703
19	684.000	0.000	-0.97910-016	0.3160 00	0.290	-0.271	6.598
20	720.000	0.000	-0.82230-016	0.6010 01	0.083	-0.150	6.508
21	756.000	0.000	-0.51670-016	0.6510 01	-0.021	-0.059	6.413
22	792.000	0.000	-0.24470-016	0.0500 01	-0.054	-0.007	6.318
23	828.000	-0.000	-0.76620-017	0.2440 01	-0.049	0.015	6.222
24	864.000	-0.000	0.73920-016	0.0450 00	-0.032	0.019	6.126
25	900.000	-0.000	0.33720-017	0.1170 00	-0.016	0.014	6.031
26	936.000	-0.000	0.31510-017	-0.2060 00	-0.005	0.008	5.937
27	972.000	-0.000	0.20260-017	-0.2460 00	0.000	0.003	5.843
28	1008.000	-0.000	0.06670-018	-0.1790 00	0.002	0.000	5.748
29	1044.000	0.000	0.29120-018	-0.9470-01	0.002	-0.001	5.654
30	1080.000	0.000	-0.29150-019	-0.5450-01	0.001	-0.001	5.559
31	1116.000	0.000	-0.12160-018	-0.2830-02	0.001	-0.001	5.465
32	1152.000	0.000	-0.30790-019	0.8340-02	0.000	-0.000	5.370
33	1188.000	0.000	-0.64900-019	0.6970-02	-0.000	-0.000	5.276
34	1224.000	0.000	-0.27090-019	0.5920-02	-0.000	-0.000	4.933
35	1260.000	-0.000	-0.06590-019	0.2810-02	-0.000	0.000	4.589
36	1296.000	-0.000	0.26260-019	0.8110-03	-0.000	0.000	4.245
37	1332.000	-0.000	0.43720-019	-0.1060-03	-0.000	0.000	3.902
38	1368.000	-0.000	0.32530-019	-0.3060-03	-0.000	0.000	3.558
39	1404.000	-0.000	0.16430-019	-0.2870-03	0.000	0.000	3.215
40	1440.000	0.000	0.57300-011	-0.1600-03	0.000	-0.000	2.871
41	1476.000	0.000	0.25760-012	-0.6670-04	0.000	-0.000	2.528
42	1512.000	0.000	-0.14430-011	-0.7700-04	0.000	-0.000	2.184
43	1548.000	0.000	-0.13660-011	-0.3070-04	0.000	-0.000	1.840
44	1584.000	0.000	-0.40550-012	0.3190-04	-0.000	-0.000	1.497
45	1620.000	-0.000	-0.32530-012	0.7490-05	-0.000	0.000	1.153
46	1656.000	-0.000	-0.58700-013	0.3270-05	-0.000	0.000	0.810
47	1692.000	-0.000	0.45470-013	0.4530-06	-0.000	0.000	0.466
48	1728.000	-0.000	0.04970-013	0.1480-06	-0.000	0.000	0.061
49	1764.000	-0.000	0.65300-013	-0.8190-09	-0.000	0.000	0.000

50	1400.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
51	1450.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
52	1500.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
53	1550.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
54	1600.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
55	1650.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
56	1700.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
57	1750.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
58	1800.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
59	1850.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
60	1900.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

USER SHOULD NOTE THAT SLIP LISTED ABOVE IS RELATIVE TO SLOPE AT BOTTOM OF PILE AND IS NOT THE SLIP RELATIVE TO ORIGINAL PILE DEFLECTION.

USER SHOULD NOTE THAT BEAM COLUMN SHEAR LISTED IS THAT DUE TO BOTH LATERAL AND AXIAL EFFECTS ALSO THAT APPLIED LATERAL LOADING IS TOTAL FOR ONE INCREMENT LENGTH

MEMBERS AND REACTIONS STORED FOR STIFFNESS COEFFICIENT DEVELOPMENT USE

DEFLECTIONS	ROTATIONS	MOMENTS	LATERAL SHEAR	AT STATION
0.174421 00	-0.814550-03	-0.292590 04	0.518130 02	1

USER SHOULD NOTE LATERAL SHEAR ABOVE IS THE SHEAR AT STATION.
SHEAR GIVEN IS PERPENDICULAR TO ORIGINAL UNDEFORMED MEMBER AXIS.

ASP JOB NO. = 9107

DATE = 76.114

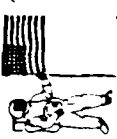
//LFC9011 JOB (000442705002777)OUT(1EC27011),C,CHERN 1,PRINTED,CLASS=,C9107

ELAPSED TIME ON MAIN = 4 = 000.05, START TIME = 18.13.42

DDNAME = SYSMSG PRINTED ON 00027PRT, LINES = 000077
DDNAME = ST06F001 PRINTED ON 00027PRT, LINES = 000428
LINES OUTPUT FOR THIS JOB = 000505

CARDS FROM MAIN FOR THIS JOB = NONE

A-4 WAVE AND WIND LOADS



26	GRUP	RR4	BRACES4	1400	375	2900	1160	3600	2	243	A	A		
27	GRUP	RR5	BRACES5	1275	500	2900	1160	3600	2	342	A	A		
28	GRUP	RR6	BRACES6	1275	375	2900	1160	3600	2	342	A	A		
29	GRUP	RR7	BRACES7	6,625	200	2900	1160	3600	2	314	A	A		
30	GRUP	RR8	WISHMAN			2900	1160	3600	2			01		
31	GRUP	STL	SUSTLEG	3600	1250	2900	1160	3600	1			01		
32	GRUP	RR1	WAX50			2900	1160	3600	1			01		
33	GRUP	RR8	WAX24			2900	1160	3600	1			01		
34	GRUP	RR6	WAX15			2900	1160	3600	1			01		
35	MEMBER		1	4	P10							F	0000	1
36	MEMBER		4	16	P10							F	0000	1
37	MEMBER		16	28	P20							F	0000	1
38	MEMBER		28	43	P20							F	0000	1
39	MEMBER		43	55	P20							F	0000	1
40	MEMBER		55		P10							F	0000	2
41	MEMBER		5	17	P10							F	0000	2
42	MEMBER		17	29	P20							F	0000	2
43	MEMBER		29	44	P20							F	0000	2
44	MEMBER		44	56	P20							F	0000	2
45	MEMBER		56		P10							F	0000	3
46	MEMBER		3	6	P10							F	0000	3
47	MEMBER		6	18	P10							F	0000	3
48	MEMBER		18	30	P20							F	0000	3
49	MEMBER		30	45	P20							F	0000	3
50	MEMBER		45	57	P20							F	0000	3
51	MEMBER		10	22	JL1							F	4100	
52	MEMBER		22	34	JL1							F	4100	
53	MEMBER		34	40	JL2							F	4100	
54	MEMBER		40	49	JL2							F	4100	
55	MEMBER		49	55	JL2							F	4100	
56	MEMBER		12	24	JL1							F	4000	
57	MEMBER		24	36	JL1							F	4000	
58	MEMBER		36	41	JL2							F	4100	
59	MEMBER		41	51	JL2							F	4100	
60	MEMBER		51	56	JL2							F	4100	
61	MEMBER		14	26	JL1							F	4000	
62	MEMBER		26	38	JL1							F	4000	
63	MEMBER		38	42	JL2							F	4100	
64	MEMBER		42	53	JL2							F	4100	
65	MEMBER		53	57	JL2							F	4100	
66	MEMBER		10	11	RR2							F	1800	
67	MEMBER		11	12	RR2							F	1800	
68	MEMBER		12	13	RR2							F	1800	
69	MEMBER		13	14	RR2							F	1800	
70	MEMBER		14	15	RR2							F	1800	
71	MEMBER		15	16	RR2							F	1800	
72	MEMBER		11	13	RR4							F	1400	
73	MEMBER		13	15	RR4							F	1400	
74	MEMBER		15	11	RR4							F	1400	
75	MEMBER		22	23	RR2							F	1800	
76	MEMBER		23	24	RR2							F	1800	
77	MEMBER		24	25	RR2							F	1800	
78	MEMBER		25	26	RR2							F	1800	
79	MEMBER		26	27	RR2							F	1800	
80	MEMBER		27	28	RR2							F	1800	
81	MEMBER		23	25	RR4							F	1400	



82	MEMBER	25	27	ARR	1400
83	MEMBER	27	23	ARR	1400
84	MEMBER	34	35	ARR	1275
85	MEMBER	35	36	ARR	1275
86	MEMBER	36	37	ARR	1275
87	MEMBER	37	38	ARR	1275
88	MEMBER	38	39	ARR	1275
89	MEMBER	39	34	ARR	1275
90	MEMBER	35	37	ARR	1275
91	MEMBER	37	39	ARR	1275
92	MEMBER	39	35	ARR	1600
93	MEMBER	49	50	ARR	1600
94	MEMBER	50	51	ARR	1600
95	MEMBER	51	52	ARR	1600
96	MEMBER	52	53	ARR	1600
97	MEMBER	53	54	ARR	1600
98	MEMBER	54	49	ARR	1600
99	MEMBER	50	52	ARR	1275
100	MEMBER	52	50	ARR	1275
101	MEMBER	54	50	ARR	1600
102	MEMBER	31	22	ARR	1600
103	MEMBER	11	24	ARR	1600
104	MEMBER	13	24	ARR	1600
105	MEMBER	13	26	ARR	1600
106	MEMBER	15	26	ARR	1600
107	MEMBER	15	22	ARR	1600
108	MEMBER	22	34	ARR	2000
109	MEMBER	24	34	ARR	2000
110	MEMBER	24	34	ARR	2000
111	MEMBER	36	49	ARR	2000
112	MEMBER	38	51	ARR	2000
113	MEMBER	34	53	ARR	2000
114	MEMBER	4	7	MAN	F 0000
115	MEMBER	7	10	MAN	F 0000
116	MEMBER	5	8	MAN	F 0000
117	MEMBER	8	12	MAN	F 0000
118	MEMBER	6	9	MAN	F 0000
119	MEMBER	9	14	MAN	F 0000
120	MEMBER	16	19	MAN	F 0000
121	MEMBER	19	22	MAN	F 0000
122	MEMBER	17	20	MAN	F 0000
123	MEMBER	20	24	MAN	F 0000
124	MEMBER	18	21	MAN	F 0000
125	MEMBER	21	26	MAN	F 0000
126	MEMBER	28	31	MAN	F 0000
127	MEMBER	31	34	MAN	F 0000
128	MEMBER	29	32	MAN	F 0000
129	MEMBER	32	36	MAN	F 0000
130	MEMBER	30	35	MAN	F 0000
131	MEMBER	33	38	MAN	F 0000
132	MEMBER	43	45	MAN	F 0000
133	MEMBER	46	49	MAN	F 0000
134	MEMBER	40	47	MAN	F 0000
135	MEMBER	47	51	MAN	F 0000
136	MEMBER	45	48	MAN	F 0000
137	MEMBER	48	53	MAN	F 0000



138 MEMBER	55	5A	STL						3600
139 MEMBER	56	61	STL						3600
140 MEMBER	61	71	STL						3600
141 MEMBER	56	59	STI						3600
142 MEMBER	59	64	STI						3600
143 MEMBER	64	72	STI						3600
144 MEMBER	57	60	STI						3600
145 MEMBER	60	73	STI						3600
146 MEMBER	70	67	STL						3600
147 MEMBER	67	76	STI						3600
148 MEMBER	76	75	STI						3600
149 MEMBER	54	59	RR5						1275
150 MEMBER	59	60	RR5						1275
151 MEMBER	60	58	RR5						1275
152 MEMBER	59	61	RR5						1275
153 MEMBER	60	64	RR5						1275
154 MEMBER	64	67	RR5						1275
155 MEMBER	70	69	RR7						64625
156 MEMBER	70	68	RR7						64625
157 MEMBER	76	77	RR6						1275
158 MEMBER	76	78	RR6						1275
159 MEMBER	61	62	WIA						0000
160 MEMBER	62	63	WIA						0000
161 MEMBER	63	64	WIA						0000
162 MEMBER	64	65	WIA						0000
163 MEMBER	65	67	WIA						0000
164 MEMBER	67	69	WIA						0000
165 MEMBER	69	61	WIA						0000
166 MEMBER	63	65	WIA						0000
167 MEMBER	65	64	WIA						0000
168 MEMBER	66	67	WOB						0000
169 MEMBER	67	68	WOB						0000
170 MEMBER	68	69	WOB						0000
171 MEMBER	69	62	WIA						0000
172 MEMBER	71	73	WIA						0000
173 MEMBER	71	72	WIA						0000
174 MEMBER	72	74	WIA						0000
175 MEMBER	71	61	WIA						0000
176 MEMBER	71	77	WIA						0000
177 MEMBER	77	83	WIA						0000
178 MEMBER	72	82	WIA						0000
179 MEMBER	72	78	WIA						0000
180 MEMBER	74	84	WIA						0000
181 MEMBER	77	79	WIA						0000
182 MEMBER	77	75	WIA						0000
183 MEMBER	75	78	WIA						0000
184 MEMBER	78	80	WIA						0000
185 MEMBER	71	75	WOB						0000
186 MEMBER	72	75	WOB						0000
187 JOINT	1	2987	-1725	-600					
188 JOINT	2	-2987	-1725	-600					
189 JOINT	3	000	3449	-600					
190 JOINT	4	2910	-1684	0					
192 JOINT	5	-2910	-1684	0					
193 JOINT	6	0	3359	0					
					111				PILING A
					111				PILE C A
					111				PILE C C
									MUDLINE
									MUDLINE

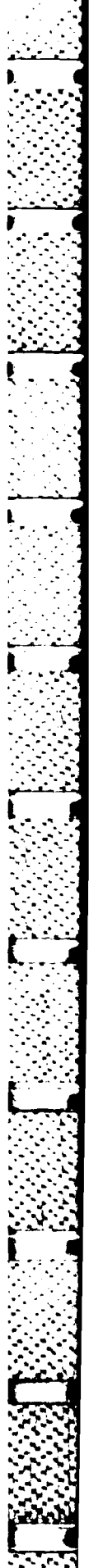


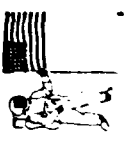


194	JOINT	7	2900	-1924	0	MIDLINE
195	JOINT	8	-2900	-1924	0	MIDLINE
196	JOINT	9	0	3599	0	MIDLINE
197	JOINT	10	2900	-1674	0	MIDLINE
198	JOINT	11	0	-1674	0	MIDLINE
199	JOINT	12	-29	-1674	0	MIDLINE
200	JOINT	13	-1450	837	0	MIDLINE
201	JOINT	14	0	3549	0	MIDLINE
202	JOINT	15	1450	837	0	MIDLINE
203	JOINT	16	2447	-1417	3200	1 LEVEL
204	JOINT	17	-2447	-1417	3200	1 LEVEL
205	JOINT	18	0	2425	3200	1 LEVEL
206	JOINT	19	2434	-1657	3200	1 LEVEL
207	JOINT	20	-2434	-1657	3200	1 LEVEL
208	JOINT	21	0	3065	3200	1 LEVEL
209	JOINT	22	2434	-1407	3200	1 LEVEL
210	JOINT	23	0	-1407	3200	1 LEVEL
211	JOINT	24	-2434	-1407	3200	1 LEVEL
212	JOINT	25	-1219	704	3200	1 LEVEL
213	JOINT	26	0	2815	3200	1 LEVEL
214	JOINT	27	1219	704	3200	1 LEVEL
215	JOINT	28	1987	-1151	6400	2 LEVEL
216	JOINT	29	-1987	-1151	6400	2 LEVEL
217	JOINT	30	0	5437	6400	2 LEVEL
218	JOINT	31	1977	-1391	6400	2 LEVEL
219	JOINT	32	-1977	-1391	6400	2 LEVEL
220	JOINT	33	0	3677	6400	2 LEVEL
221	JOINT	34	1977	-1141	6400	2 LEVEL
222	JOINT	35	0	-1141	6400	2 LEVEL
223	JOINT	36	-1977	-1141	6400	2 LEVEL
224	JOINT	37	-984	571	6400	2 LEVEL
225	JOINT	38	0	3427	6400	2 LEVEL
226	JOINT	39	984	571	6400	2 LEVEL
227	JOINT	40	1774	-1040	7800	HOAT LOG
228	JOINT	41	-1774	-1040	7800	HOAT LOG
229	JOINT	42	0	2880	7800	HOAT LOG
230	JOINT	43	1525	-885	9600	3 LEVEL
231	JOINT	44	-1525	-885	9600	3 LEVEL
232	JOINT	45	0	1759	9600	3 LEVEL
233	JOINT	46	1515	-1125	9600	3 LEVEL
234	JOINT	47	-1515	-1125	9600	3 LEVEL
235	JOINT	48	0	1999	9600	3 LEVEL
236	JOINT	49	1515	-875	9600	3 LEVEL
237	JOINT	50	0	-875	9600	3 LEVEL
238	JOINT	51	-1515	-875	9600	3 LEVEL
239	JOINT	52	-757	437	9600	3 LEVEL
240	JOINT	53	0	1749	9600	3 LEVEL
241	JOINT	54	757	437	9600	3 LEVEL
242	JOINT	55	1450	-837	10050	4P LEVEL
243	JOINT	56	-1450	-837	10050	4P LEVEL
244	JOINT	57	0	1674	10050	4P LEVEL
245	JOINT	58	1450	-837	12900	ST H-ACE
246	JOINT	59	-1450	-837	12900	ST H-ACE
247	JOINT	60	0	1674	12900	ST H-ACE
248	JOINT	61	1450	-837	14400	FOT TRCK
249	JOINT	62	1000	-837	14400	FOT TRCK



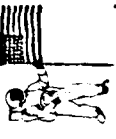
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309	LOAD	Z	34	40	4.73-	05	4.73-	06	GLOR UNITF	WV 0 1
310	LOAD	X	34	40	0.45	1	0.73	44	GLOR UNITF	WV 0 1
311	LOAD	Y	34	40	0.45	04	4.73-	06	GLOR UNITF	WV 0 1
312	LOAD	Z	34	40	0.00	1	6.09	06	GLOR UNITF	WV 0 1
313	LOAD	X	40	49	0.00	84	6.09	06	GLOR UNITF	WV 0 1
314	LOAD	Y	40	49	0.00-	04	6.09-	09	GLOR UNITF	WV 0 1
315	LOAD	Z	40	49	6.09	1	6.09	106	GLOR UNITF	WV 0 1
316	LOAD	X	40	49	6.09-	09	6.09-	09	GLOR UNITF	WV 0 1
317	LOAD	Y	40	49	6.09	96	6.09	09	GLOR UNITF	WV 0 1
318	LOAD	Z	40	49	6.09-	09	6.09-	118	GLOR UNITF	WV 0 1
319	LOAD	X	40	49	12.17	102	6.09	11	GLOR UNITF	WV 0 1
320	LOAD	Y	40	49	12.17	09	6.09-	121	GLOR UNITF	WV 0 1
321	LOAD	Z	49	55	0.00	1	1.52	10	GLOR UNITF	WV 0 1
322	LOAD	X	49	55	0.00	114	1.52	121	GLOR UNITF	WV 0 1
323	LOAD	Y	49	55	0.00-	10	1.52-	10	GLOR UNITF	WV 0 1
324	LOAD	Z	49	55	1.52	1	1.52	125	GLOR UNITF	WV 0 1
325	LOAD	X	49	55	1.52	10	1.52-	10	GLOR UNITF	WV 0 1
326	LOAD	Y	49	55	1.52	10	1.52-	128	GLOR UNITF	WV 0 1
327	LOAD	Z	49	55	3.04	1	1.52	11	GLOR UNITF	WV 0 1
328	LOAD	X	49	55	3.04	125	1.52	11	GLOR UNITF	WV 0 1
329	LOAD	Y	49	55	3.04-	10	1.52-	44	GLOR UNITF	WV 0 1
330	LOAD	Z	49	55	3.04	1	10.81-	04	GLOR UNITF	WV 0 1
331	LOAD	X	12	24	0.00-	47	10.81-	04	GLOR UNITF	WV 0 1
332	LOAD	Y	12	24	0.00	04	10.81-	04	GLOR UNITF	WV 0 1
333	LOAD	Z	12	24	0.00-	3	10.81-	50	GLOR UNITF	WV 0 1
334	LOAD	X	12	24	10.81	48	10.81	04	GLOR UNITF	WV 0 1
335	LOAD	Y	12	24	10.81	04	10.81-	04	GLOR UNITF	WV 0 1
336	LOAD	Z	12	24	10.81-	1	17.41-	53	GLOR UNITF	WV 0 1
337	LOAD	X	12	24	21.63	50	10.81	04	GLOR UNITF	WV 0 1
338	LOAD	Y	12	24	21.63	04	10.81-	04	GLOR UNITF	WV 0 1
339	LOAD	Z	12	24	21.63	1	10.81-	57	GLOR UNITF	WV 0 1
340	LOAD	X	24	36	0.00-	1	10.81-	05	GLOR UNITF	WV 0 1
341	LOAD	Y	24	36	0.00	53	10.81	64	GLOR UNITF	WV 0 1
342	LOAD	Z	24	36	0.00-	04	10.81-	05	GLOR UNITF	WV 0 1
343	LOAD	X	24	36	10.81-	1	10.81-	05	GLOR UNITF	WV 0 1
344	LOAD	Y	24	36	10.81	57	10.81	05	GLOR UNITF	WV 0 1
345	LOAD	Z	24	36	10.81-	05	10.81-	71	GLOR UNITF	WV 0 1
346	LOAD	X	24	36	21.63	64	10.81	06	GLOR UNITF	WV 0 1
347	LOAD	Y	24	36	21.63	05	10.81-	06	GLOR UNITF	WV 0 1
348	LOAD	Z	24	36	21.63-	73	4.73	77	GLOR UNITF	WV 0 1
349	LOAD	X	36	41	0.00-	05	4.73-	05	GLOR UNITF	WV 0 1
350	LOAD	Y	36	41	0.00	77	4.73	42	GLOR UNITF	WV 0 1
351	LOAD	Z	36	41	0.00-	05	4.73-	06	GLOR UNITF	WV 0 1
352	LOAD	X	36	41	4.73-	1	4.73-	44	GLOR UNITF	WV 0 1
353	LOAD	Y	36	41	4.73	77	4.73	06	GLOR UNITF	WV 0 1
354	LOAD	Z	36	41	4.73-	05	4.73-	06	GLOR UNITF	WV 0 1
355	LOAD	X	36	41	9.45-	1	4.73-	44	GLOR UNITF	WV 0 1
356	LOAD	Y	36	41	9.45	42	4.73	06	GLOR UNITF	WV 0 1
357	LOAD	Z	36	41	9.45-	06	4.73-	06	GLOR UNITF	WV 0 1
358	LOAD	X	41	51	0.00-	1	6.09-	06	GLOR UNITF	WV 0 1
359	LOAD	Y	41	51	0.00	84	6.09	06	GLOR UNITF	WV 0 1
360	LOAD	Z	41	51	0.00-	04	6.09-	09	GLOR UNITF	WV 0 1
361	LOAD	X	41	51	6.09-	1	6.09-	1	GLOR UNITF	WV 0 1





362	LOAD	Y	41	51	6.09	96	9.09	101	GLOR UNIF	MV 0 1
363	LOAD	Z	41	51	6.09	09	6.09	09	GLOR UNIF	MV 0 1
364	LOAD	X	41	51	12.17	1	6.09	1	GLOR UNIF	MV 0 1
365	LOAD	Y	41	51	12.17	106	6.09	114	GLOR UNIF	MV 0 1
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367	LOAD	X	51	56	0.00	1	1.52	1	GLOR UNIF	MV 0 1
368	LOAD	Y	51	56	0.00	118	1.52	121	GLOR UNIF	MV 0 1
369	LOAD	Z	51	56	0.00	10	1.52	10	GLOR UNIF	MV 0 1
370	LOAD	X	51	56	1.52	1	1.52	1	GLOR UNIF	MV 0 1
371	LOAD	Y	51	56	1.52	121	1.52	125	GLOR UNIF	MV 0 1
372	LOAD	Z	51	56	1.52	10	1.52	10	GLOR UNIF	MV 0 1
373	LOAD	X	51	56	3.04	1	1.52	1	GLOR UNIF	MV 0 1
374	LOAD	Y	51	56	3.04	125	1.52	128	GLOR UNIF	MV 0 1
375	LOAD	Z	51	56	3.04	10	1.52	11	GLOR UNIF	MV 0 1
376	LOAD	Y	14	26	0.00	50	10.81	51	GLOR UNIF	MV 0 1
377	LOAD	Z	14	26	0.00	08	10.81	08	GLOR UNIF	MV 0 1
378	LOAD	Y	14	26	10.81	51	10.81	53	GLOR UNIF	MV 0 1
379	LOAD	Z	14	26	10.81	04	10.81	09	GLOR UNIF	MV 0 1
380	LOAD	Y	14	26	21.63	53	10.81	56	GLOR UNIF	MV 0 1
381	LOAD	Z	14	26	21.63	09	10.81	09	GLOR UNIF	MV 0 1
382	LOAD	Y	26	38	0.00	55	10.86	59	GLOR UNIF	MV 0 1
383	LOAD	Z	26	38	0.00	11	10.86	11	GLOR UNIF	MV 0 1
384	LOAD	Y	26	38	10.86	59	10.86	64	GLOR UNIF	MV 0 1
385	LOAD	Z	26	38	10.86	11	10.86	12	GLOR UNIF	MV 0 1
386	LOAD	Y	26	38	21.72	64	10.86	70	GLOR UNIF	MV 0 1
387	LOAD	Z	26	38	21.72	12	10.86	13	GLOR UNIF	MV 0 1
388	LOAD	Y	38	42	0.00	65	5.01	69	GLOR UNIF	MV 0 1
389	LOAD	Z	38	42	0.00	25	5.01	27	GLOR UNIF	MV 0 1
390	LOAD	Y	38	42	5.01	69	5.01	73	GLOR UNIF	MV 0 1
391	LOAD	Z	38	42	5.01	27	5.01	29	GLOR UNIF	MV 0 1
392	LOAD	Y	38	42	10.02	73	5.01	78	GLOR UNIF	MV 0 1
393	LOAD	Z	38	42	10.02	29	5.01	31	GLOR UNIF	MV 0 1
394	LOAD	Y	42	53	0.00	65	7.09	71	GLOR UNIF	MV 0 1
395	LOAD	Z	42	53	0.00	41	7.09	45	GLOR UNIF	MV 0 1
396	LOAD	Y	42	53	7.09	71	7.09	74	GLOR UNIF	MV 0 1
397	LOAD	Z	42	53	7.09	45	7.09	49	GLOR UNIF	MV 0 1
398	LOAD	Y	42	53	14.17	79	7.09	84	GLOR UNIF	MV 0 1
399	LOAD	Z	42	53	14.17	49	7.09	55	GLOR UNIF	MV 0 1
400	LOAD	Y	53	57	0.00	120	1.52	123	GLOR UNIF	MV 0 1
401	LOAD	Z	53	57	0.00	20	1.52	20	GLOR UNIF	MV 0 1
402	LOAD	Y	53	57	1.52	123	1.52	124	GLOR UNIF	MV 0 1
403	LOAD	Z	53	57	1.52	20	1.52	21	GLOR UNIF	MV 0 1
404	LOAD	Y	53	57	3.04	126	1.52	129	GLOR UNIF	MV 0 1
405	LOAD	Z	53	57	3.04	21	1.52	21	GLOR UNIF	MV 0 1
406	LOAD	Y	10	11	0.00	21	9.67	21	GLOR UNIF	MV 0 1
407	LOAD	Z	10	11	9.67	21	9.67	21	GLOR UNIF	MV 0 1
408	LOAD	Y	10	11	19.33	21	9.67	21	GLOR UNIF	MV 0 1
409	LOAD	Z	10	11	0.00	21	9.67	21	GLOR UNIF	MV 0 1
410	LOAD	Y	11	12	9.67	21	9.67	21	GLOR UNIF	MV 0 1
411	LOAD	Z	11	12	19.33	21	9.67	21	GLOR UNIF	MV 0 1
412	LOAD	Y	12	13	0.00	09	9.67	09	GLOR UNIF	MV 0 1
413	LOAD	Z	12	13	0.00	05	9.67	05	GLOR UNIF	MV 0 1
414	LOAD	Y	12	13	9.67	09	9.67	10	GLOR UNIF	MV 0 1
415	LOAD	Z	12	13	9.67	05	9.67	06	GLOR UNIF	MV 0 1
416	LOAD	Y	12	13	19.33	10	9.67	10	GLOR UNIF	MV 0 1
417	LOAD	Z	12	13	19.33	06	9.67	06	GLOR UNIF	MV 0 1





418	LOAD	X	13	14	0.00	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
419	LOAD	X	13	14	0.00	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
420	LOAD	X	13	14	9.67	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
421	LOAD	Y	13	14	9.67	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
422	LOAD	X	13	14	19.34	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
423	LOAD	X	13	14	19.34	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
424	LOAD	X	14	15	0.00	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
425	LOAD	Y	14	15	0.00	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
426	LOAD	X	14	15	9.67	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
427	LOAD	Y	14	15	9.67	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
428	LOAD	X	14	15	19.34	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
429	LOAD	Y	14	15	19.34	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
430	LOAD	X	15	16	0.00	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
431	LOAD	Y	15	16	0.00	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
432	LOAD	X	15	16	9.67	10	9.67	10	9.67	GLOR	UNIF	AV	0	1
433	LOAD	Y	15	16	9.67	06	9.67	06	9.67	GLOR	UNIF	AV	0	1
434	LOAD	X	15	16	19.33	09	9.67	09	9.67	GLOR	UNIF	AV	0	1
435	LOAD	Y	15	16	19.33	05	9.67	05	9.67	GLOR	UNIF	AV	0	1
436	LOAD	X	11	13	0.00	07	9.67	07	9.67	GLOR	UNIF	AV	0	1
437	LOAD	Y	11	13	0.00	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
438	LOAD	X	11	13	9.67	07	9.67	07	9.67	GLOR	UNIF	AV	0	1
439	LOAD	Y	11	13	9.67	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
440	LOAD	X	11	13	19.33	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
441	LOAD	Y	11	13	19.33	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
442	LOAD	X	13	15	0.00	18	9.67	18	9.67	GLOR	UNIF	AV	0	1
443	LOAD	Y	13	15	9.67	18	9.67	18	9.67	GLOR	UNIF	AV	0	1
444	LOAD	Y	13	15	19.33	18	9.67	18	9.67	GLOR	UNIF	AV	0	1
445	LOAD	X	15	11	0.00	08	9.67	08	9.67	GLOR	UNIF	AV	0	1
446	LOAD	Y	15	11	0.00	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
447	LOAD	X	15	11	9.67	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
448	LOAD	Y	15	11	9.67	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
449	LOAD	X	15	11	19.33	07	9.67	07	9.67	GLOR	UNIF	AV	0	1
450	LOAD	Y	15	11	19.33	04	9.67	04	9.67	GLOR	UNIF	AV	0	1
451	LOAD	Y	22	23	0.00	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
452	LOAD	Y	22	23	8.13	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
453	LOAD	Y	22	23	16.25	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
454	LOAD	Y	23	24	0.00	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
455	LOAD	Y	23	24	8.13	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
456	LOAD	Y	23	24	16.25	24	8.13	24	8.13	GLOR	UNIF	AV	0	1
457	LOAD	X	24	25	0.00	10	8.13	10	8.13	GLOR	UNIF	AV	0	1
458	LOAD	Y	24	25	0.00	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
459	LOAD	X	24	25	8.13	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
460	LOAD	Y	24	25	8.13	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
461	LOAD	X	24	25	16.25	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
462	LOAD	Y	24	25	16.25	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
463	LOAD	X	25	26	0.00	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
464	LOAD	Y	25	26	0.00	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
465	LOAD	X	25	26	8.13	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
466	LOAD	Y	25	26	8.13	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
467	LOAD	X	25	26	16.25	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
468	LOAD	Y	25	26	16.25	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
469	LOAD	X	26	27	0.00	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
470	LOAD	Y	26	27	0.00	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
471	LOAD	X	26	27	8.13	11	8.13	11	8.13	GLOR	UNIF	AV	0	1
472	LOAD	Y	26	27	8.13	06	8.13	06	8.13	GLOR	UNIF	AV	0	1
473	LOAD	X	26	27	16.25	11	8.13	11	8.13	GLOR	UNIF	AV	0	1



474	LOAD	Y	26	27	16.25	06	8.13	06	GLOR UNIT	WV 0 1
475	LOAD	Y	27	22	0.00	11	8.13	11	GLOR UNIT	WV 0 1
476	LOAD	Y	27	22	0.00	06	8.13	06	GLOR UNIT	WV 0 1
477	LOAD	Y	27	22	8.13	11	8.13	11	GLOR UNIT	WV 0 1
478	LOAD	Y	27	22	8.13	06	8.13	06	GLOR UNIT	WV 0 1
479	LOAD	X	27	22	16.25	11	8.13	11	GLOR UNIT	WV 0 1
480	LOAD	Y	27	22	16.25	06	8.13	06	GLOR UNIT	WV 0 1
481	LOAD	X	23	25	0.00	08	8.13	08	GLOR UNIT	WV 0 1
482	LOAD	X	23	25	0.00	05	8.13	05	GLOR UNIT	WV 0 1
483	LOAD	X	23	25	8.13	04	8.13	04	GLOR UNIT	WV 0 1
484	LOAD	Y	23	25	8.13	05	8.13	05	GLOR UNIT	WV 0 1
485	LOAD	X	23	25	16.25	09	8.13	09	GLOR UNIT	WV 0 1
486	LOAD	X	23	25	16.25	05	8.13	05	GLOR UNIT	WV 0 1
487	LOAD	Y	25	27	0.00	20	8.13	20	GLOR UNIT	WV 0 1
488	LOAD	Y	25	27	8.13	20	8.13	20	GLOR UNIT	WV 0 1
489	LOAD	Y	25	27	16.25	20	8.13	20	GLOR UNIT	WV 0 1
490	LOAD	Y	27	23	0.00	09	8.13	09	GLOR UNIT	WV 0 1
491	LOAD	Y	27	23	0.00	05	8.13	05	GLOR UNIT	WV 0 1
492	LOAD	X	27	23	8.13	09	8.13	09	GLOR UNIT	WV 0 1
493	LOAD	Y	27	23	8.13	05	8.13	05	GLOR UNIT	WV 0 1
494	LOAD	X	27	23	16.25	08	8.13	08	GLOR UNIT	WV 0 1
495	LOAD	Y	27	23	16.25	05	8.13	05	GLOR UNIT	WV 0 1
496	LOAD	Y	34	35	0.00	23	6.59	23	GLOR UNIT	WV 0 1
497	LOAD	Y	34	35	6.59	23	6.59	23	GLOR UNIT	WV 0 1
498	LOAD	Y	34	35	13.18	23	6.59	23	GLOR UNIT	WV 0 1
499	LOAD	Y	35	36	0.00	23	6.59	23	GLOR UNIT	WV 0 1
500	LOAD	Y	35	36	6.59	23	6.59	23	GLOR UNIT	WV 0 1
501	LOAD	Y	35	36	13.18	23	6.59	23	GLOR UNIT	WV 0 1
502	LOAD	X	36	37	0.00	10	6.59	10	GLOR UNIT	WV 0 1
503	LOAD	Y	36	37	0.00	06	6.59	06	GLOR UNIT	WV 0 1
504	LOAD	X	36	37	6.59	10	6.59	10	GLOR UNIT	WV 0 1
505	LOAD	Y	36	37	6.59	06	6.59	06	GLOR UNIT	WV 0 1
506	LOAD	X	36	37	13.18	10	6.59	10	GLOR UNIT	WV 0 1
507	LOAD	Y	36	37	13.18	06	6.59	06	GLOR UNIT	WV 0 1
508	LOAD	X	37	38	0.00	07	10.07	07	GLOR UNIT	WV 0 1
509	LOAD	Y	37	38	0.00	03	10.07	03	GLOR UNIT	WV 0 1
510	LOAD	X	37	38	10.07	07	10.07	07	GLOR UNIT	WV 0 1
511	LOAD	Y	37	38	10.07	03	10.07	03	GLOR UNIT	WV 0 1
512	LOAD	X	37	38	20.15	07	10.07	07	GLOR UNIT	WV 0 1
513	LOAD	Y	37	38	20.15	03	10.07	03	GLOR UNIT	WV 0 1
514	LOAD	X	38	39	0.00	07	10.07	07	GLOR UNIT	WV 0 1
515	LOAD	Y	38	39	0.00	02	10.07	02	GLOR UNIT	WV 0 1
516	LOAD	X	38	39	10.07	07	10.07	07	GLOR UNIT	WV 0 1
517	LOAD	Y	38	39	10.07	03	10.07	03	GLOR UNIT	WV 0 1
518	LOAD	X	38	39	20.15	07	10.07	07	GLOR UNIT	WV 0 1
519	LOAD	Y	38	39	20.15	03	10.07	03	GLOR UNIT	WV 0 1
520	LOAD	X	39	34	0.00	10	6.59	10	GLOR UNIT	WV 0 1
521	LOAD	Y	39	34	0.00	06	6.59	06	GLOR UNIT	WV 0 1
522	LOAD	X	39	34	6.59	10	6.59	10	GLOR UNIT	WV 0 1
523	LOAD	Y	39	34	6.59	06	6.59	06	GLOR UNIT	WV 0 1
524	LOAD	X	39	34	13.18	10	6.59	10	GLOR UNIT	WV 0 1
525	LOAD	Y	39	34	13.18	06	6.59	06	GLOR UNIT	WV 0 1
526	LOAD	X	35	37	0.00	10	6.59	10	GLOR UNIT	WV 0 1
527	LOAD	Y	35	37	0.00	06	6.59	06	GLOR UNIT	WV 0 1
528	LOAD	X	35	37	6.59	10	6.59	10	GLOR UNIT	WV 0 1
529	LOAD	Y	35	37	6.59	06	6.59	06	GLOR UNIT	WV 0 1



530	LOAD	X	35	37	13.1A	10	6.59	10	GLOR UNIT	AV 0 1
531	LOAD	Y	35	37	13.1A	06	6.59	06	GLOR UNIT	AV 0 1
532	LOAD	Y	37	39	0.00	24	6.59	24	GLOR UNIT	AV 0 1
533	LOAD	Y	37	39	6.59	24	6.59	24	GLOR UNIT	AV 0 1
534	LOAD	Y	37	39	13.17	24	6.59	24	GLOR UNIT	AV 0 1
535	LOAD	X	39	35	6.00	10	6.59	10	GLOR UNIT	AV 0 1
536	LOAD	Y	39	35	0.00	06	6.59	06	GLOR UNIT	AV 0 1
537	LOAD	X	39	35	6.59	10	6.59	10	GLOR UNIT	AV 0 1
538	LOAD	Y	39	35	6.59	06	6.59	06	GLOR UNIT	AV 0 1
539	LOAD	X	39	35	13.18	10	6.59	10	GLOR UNIT	AV 0 1
540	LOAD	Y	39	35	13.1A	06	6.59	06	GLOR UNIT	AV 0 1
541	LOAD	Y	49	50	0.00	46	5.05	46	GLOR UNIT	AV 0 1
542	LOAD	Y	49	50	5.05	46	5.05	46	GLOR UNIT	AV 0 1
543	LOAD	Y	49	50	10.10	46	5.05	46	GLOR UNIT	AV 0 1
544	LOAD	Y	50	51	0.00	46	5.05	46	GLOR UNIT	AV 0 1
545	LOAD	Y	50	51	5.05	46	5.05	46	GLOR UNIT	AV 0 1
546	LOAD	Y	50	51	10.10	46	5.05	46	GLOR UNIT	AV 0 1
547	LOAD	X	51	52	0.00	20	5.05	20	GLOR UNIT	AV 0 1
548	LOAD	Y	51	52	0.00	12	5.05	12	GLOR UNIT	AV 0 1
549	LOAD	Y	51	52	5.05	20	5.05	20	GLOR UNIT	AV 0 1
550	LOAD	Y	51	52	5.05	12	5.05	12	GLOR UNIT	AV 0 1
551	LOAD	X	51	52	10.10	21	5.05	21	GLOR UNIT	AV 0 1
552	LOAD	Y	51	52	10.10	12	5.05	12	GLOR UNIT	AV 0 1
553	LOAD	Y	52	53	0.00	21	5.05	21	GLOR UNIT	AV 0 1
554	LOAD	Y	52	53	0.00	12	5.05	12	GLOR UNIT	AV 0 1
555	LOAD	X	52	53	5.05	21	5.05	21	GLOR UNIT	AV 0 1
556	LOAD	Y	52	53	5.05	12	5.05	12	GLOR UNIT	AV 0 1
557	LOAD	X	52	53	10.10	21	5.05	21	GLOR UNIT	AV 0 1
558	LOAD	Y	52	53	10.10	12	5.05	12	GLOR UNIT	AV 0 1
559	LOAD	X	53	54	0.00	21	5.05	21	GLOR UNIT	AV 0 1
560	LOAD	Y	53	54	0.00	12	5.05	12	GLOR UNIT	AV 0 1
561	LOAD	X	53	54	5.05	21	5.05	21	GLOR UNIT	AV 0 1
562	LOAD	Y	53	54	5.05	12	5.05	12	GLOR UNIT	AV 0 1
563	LOAD	X	53	54	10.10	21	5.05	21	GLOR UNIT	AV 0 1
564	LOAD	Y	53	54	10.10	12	5.05	12	GLOR UNIT	AV 0 1
565	LOAD	X	54	49	0.00	21	5.05	21	GLOR UNIT	AV 0 1
566	LOAD	Y	54	49	0.00	12	5.05	12	GLOR UNIT	AV 0 1
567	LOAD	X	54	49	5.05	21	5.05	21	GLOR UNIT	AV 0 1
568	LOAD	Y	54	49	5.05	12	5.05	12	GLOR UNIT	AV 0 1
569	LOAD	X	54	49	10.10	20	5.05	20	GLOR UNIT	AV 0 1
570	LOAD	Y	54	49	10.10	12	5.05	12	GLOR UNIT	AV 0 1
571	LOAD	X	54	49	0.00	16	5.05	16	GLOR UNIT	AV 0 1
572	LOAD	Y	54	49	0.00	09	5.05	09	GLOR UNIT	AV 0 1
573	LOAD	X	54	49	5.05	16	5.05	16	GLOR UNIT	AV 0 1
574	LOAD	Y	54	49	5.05	09	5.05	09	GLOR UNIT	AV 0 1
575	LOAD	X	54	49	10.10	17	5.05	17	GLOR UNIT	AV 0 1
576	LOAD	Y	54	49	10.10	10	5.05	10	GLOR UNIT	AV 0 1
577	LOAD	Y	52	54	0.00	39	5.05	39	GLOR UNIT	AV 0 1
578	LOAD	Y	52	54	5.05	39	5.05	39	GLOR UNIT	AV 0 1
579	LOAD	Y	52	54	10.09	39	5.05	39	GLOR UNIT	AV 0 1
580	LOAD	X	54	50	0.00	17	5.05	17	GLOR UNIT	AV 0 1
581	LOAD	Y	54	50	0.00	10	5.05	10	GLOR UNIT	AV 0 1
582	LOAD	X	54	50	5.05	17	5.05	17	GLOR UNIT	AV 0 1
583	LOAD	Y	54	50	5.05	10	5.05	10	GLOR UNIT	AV 0 1
584	LOAD	X	54	50	10.10	16	5.05	16	GLOR UNIT	AV 0 1
585	LOAD	Y	54	50	10.10	09	5.05	09	GLOR UNIT	AV 0 1



586	LOAD	X	11	22	0.00-	1	13.44-	GLOR UNIT	AV 0 1
587	LOAD	Y	11	22	0.00-	19	13.44-	GLOR UNIT	AV 0 1
588	LOAD	Z	11	22	0.00-	1	13.44-	GLOR UNIT	AV 0 1
589	LOAD	X	11	22	13.44-	1	13.44-	GLOR UNIT	AV 0 1
590	LOAD	Y	11	22	13.44-	19	13.44-	GLOR UNIT	AV 0 1
591	LOAD	Z	11	22	13.44-	1	13.44-	GLOR UNIT	AV 0 1
592	LOAD	X	11	22	26.88-	1	13.44-	GLOR UNIT	AV 0 1
593	LOAD	Y	11	22	26.88-	20	13.44-	GLOR UNIT	AV 0 1
594	LOAD	Z	11	22	26.88-	1	13.44-	GLOR UNIT	AV 0 1
595	LOAD	X	11	24	0.00-	1	13.44-	GLOR UNIT	AV 0 1
596	LOAD	Y	11	24	0.00-	19	13.44-	GLOR UNIT	AV 0 1
597	LOAD	Z	11	24	0.00-	1	13.44-	GLOR UNIT	AV 0 1
598	LOAD	X	11	24	13.44	1	13.44	GLOR UNIT	AV 0 1
599	LOAD	Y	11	24	13.44	19	13.44	GLOR UNIT	AV 0 1
600	LOAD	Z	11	24	13.44-	1	13.44-	GLOR UNIT	AV 0 1
601	LOAD	X	11	24	26.88	1	13.44	GLOR UNIT	AV 0 1
602	LOAD	Y	11	24	26.88	20	13.44	GLOR UNIT	AV 0 1
603	LOAD	Z	11	24	26.88-	1	13.44-	GLOR UNIT	AV 0 1
604	LOAD	X	13	21	0.00-	03	13.44-	GLOR UNIT	AV 0 1
605	LOAD	Y	13	21	0.00-	14	13.44	GLOR UNIT	AV 0 1
606	LOAD	Z	13	21	0.00	09	13.44	GLOR UNIT	AV 0 1
607	LOAD	X	13	24	13.44-	03	13.44-	GLOR UNIT	AV 0 1
608	LOAD	Y	13	24	13.44	14	13.44	GLOR UNIT	AV 0 1
609	LOAD	Z	13	24	13.44	09	13.44	GLOR UNIT	AV 0 1
610	LOAD	X	13	24	26.88-	03	13.44-	GLOR UNIT	AV 0 1
611	LOAD	Y	13	24	26.88	10	13.44	GLOR UNIT	AV 0 1
612	LOAD	Z	13	24	26.88	09	13.44	GLOR UNIT	AV 0 1
613	LOAD	X	13	26	0.00-	04	13.44-	GLOR UNIT	AV 0 1
614	LOAD	Y	13	26	0.00	16	13.44	GLOR UNIT	AV 0 1
615	LOAD	Z	13	26	0.00-	08	13.44-	GLOR UNIT	AV 0 1
616	LOAD	X	13	26	13.44-	04	13.44-	GLOR UNIT	AV 0 1
617	LOAD	Y	13	26	13.44	16	13.44	GLOR UNIT	AV 0 1
618	LOAD	Z	13	26	13.44-	08	13.44-	GLOR UNIT	AV 0 1
619	LOAD	X	13	26	26.88-	04	13.44-	GLOR UNIT	AV 0 1
620	LOAD	Y	13	26	26.88	17	13.44	GLOR UNIT	AV 0 1
621	LOAD	Z	13	26	26.88-	08	13.44-	GLOR UNIT	AV 0 1
622	LOAD	X	15	26	0.00	04	13.44	GLOR UNIT	AV 0 1
623	LOAD	Y	15	26	0.00	16	13.44	GLOR UNIT	AV 0 1
624	LOAD	Z	15	26	0.00-	08	13.44-	GLOR UNIT	AV 0 1
625	LOAD	X	15	26	13.44	04	13.44	GLOR UNIT	AV 0 1
626	LOAD	Y	15	26	13.44	16	13.44	GLOR UNIT	AV 0 1
627	LOAD	Z	15	26	13.44-	08	13.44-	GLOR UNIT	AV 0 1
628	LOAD	X	15	26	26.88	04	13.44	GLOR UNIT	AV 0 1
629	LOAD	Y	15	26	26.88	17	13.44	GLOR UNIT	AV 0 1
630	LOAD	Z	15	26	26.88-	08	13.44-	GLOR UNIT	AV 0 1
631	LOAD	X	15	22	0.00	03	13.44	GLOR UNIT	AV 0 1
632	LOAD	Y	15	22	0.00	14	13.44	GLOR UNIT	AV 0 1
633	LOAD	Z	15	22	0.00	09	13.44	GLOR UNIT	AV 0 1
634	LOAD	X	15	22	13.44	03	13.44	GLOR UNIT	AV 0 1
635	LOAD	Y	15	22	13.44	14	13.44	GLOR UNIT	AV 0 1
636	LOAD	Z	15	22	13.44	09	13.44	GLOR UNIT	AV 0 1
637	LOAD	X	15	22	26.88	03	13.44	GLOR UNIT	AV 0 1
638	LOAD	Y	15	22	26.88	14	13.44	GLOR UNIT	AV 0 1
639	LOAD	Z	15	22	26.88	09	13.44	GLOR UNIT	AV 0 1
640	LOAD	X	22	36	0.00	1	18.20	GLOR UNIT	AV 0 1
641	LOAD	Y	22	36	0.00	27	18.20	GLOR UNIT	AV 0 1





642	LOAD	Z	22	36	0.00=	1	1A.20=	1	GLOR UNIF	MV 0 1
643	LOAD	X	22	36	1A.20	1	1A.20	1	GLOR UNIF	MV 0 1
644	LOAD	Y	22	36	1A.20	29	1A.20	32	GLOR UNIF	MV 0 1
645	LOAD	Z	22	36	1A.20=	1	1A.20=	1	GLOR UNIF	MV 0 1
646	LOAD	X	22	36	3A.39	1	1A.20=	1	GLOR UNIF	MV 0 1
647	LOAD	Y	22	36	3A.39	32	1A.20	36	GLOR UNIF	MV 0 1
648	LOAD	Z	22	36	3A.39=	1	1A.20=	1	GLOR UNIF	MV 0 1
649	LOAD	X	24	3A	0.00=	0A	20.9A=	09	GLOR UNIF	MV 0 1
650	LOAD	Y	24	3A	0.00	11	20.9A	13	GLOR UNIF	MV 0 1
651	LOAD	Z	24	3A	0.00=	10	20.9A=	12	GLOR UNIF	MV 0 1
652	LOAD	X	24	3A	20.9A=	09	20.9A=	17	GLOR UNIF	MV 0 1
653	LOAD	Y	24	3A	20.9A	13	20.9A	14	GLOR UNIF	MV 0 1
654	LOAD	Z	24	3A	20.9A=	12	20.9A=	13	GLOR UNIF	MV 0 1
655	LOAD	X	24	3A	41.93=	10	20.9A=	15	GLOR UNIF	MV 0 1
656	LOAD	Y	24	3A	41.93	14	20.9A	18	GLOR UNIF	MV 0 1
657	LOAD	Z	24	3A	41.93=	13	20.9A=	14	GLOR UNIF	MV 0 1
658	LOAD	X	26	34	1.00	0A	1A.20	0A	GLOR UNIF	MV 0 1
659	LOAD	Y	26	34	0.00	14	1A.20	15	GLOR UNIF	MV 0 1
660	LOAD	Z	26	34	0.00	12	1A.20	13	GLOR UNIF	MV 0 1
661	LOAD	X	26	34	1A.20	0A	1A.20	09	GLOR UNIF	MV 0 1
662	LOAD	Y	26	34	1A.20	15	1A.20	1A	GLOR UNIF	MV 0 1
663	LOAD	Z	26	34	1A.20	13	1A.20	14	GLOR UNIF	MV 0 1
664	LOAD	X	26	34	3A.39	09	1A.20	09	GLOR UNIF	MV 0 1
665	LOAD	Y	26	34	3A.39	16	1A.20	17	GLOR UNIF	MV 0 1
666	LOAD	Z	26	34	3A.39	14	1A.20	15	GLOR UNIF	MV 0 1
667	LOAD	X	36	49	0.00=	1	11.8A=	02	GLOR UNIF	MV 0 1
668	LOAD	Y	36	49	0.00	3A	11.8A	40	GLOR UNIF	MV 0 1
669	LOAD	Z	36	49	0.00=	1	11.8A=	1	GLOR UNIF	MV 0 1
670	LOAD	X	36	49	11.8A=	02	11.8A=	02	GLOR UNIF	MV 0 1
671	LOAD	Y	36	49	11.8A	40	11.8A	40	GLOR UNIF	MV 0 1
672	LOAD	Z	36	49	11.8A=	1	11.8A=	02	GLOR UNIF	MV 0 1
673	LOAD	X	36	49	23.72=	02	11.8A=	02	GLOR UNIF	MV 0 1
674	LOAD	Y	36	49	23.72	44	11.8A	50	GLOR UNIF	MV 0 1
675	LOAD	Z	36	49	23.72=	02	11.8A=	02	GLOR UNIF	MV 0 1
676	LOAD	X	36	49	35.5A=	02	11.8A=	02	GLOR UNIF	MV 0 1
677	LOAD	Y	36	49	35.5A	50	11.8A	5A	GLOR UNIF	MV 0 1
678	LOAD	Z	36	49	35.5A=	02	11.8A=	02	GLOR UNIF	MV 0 1
679	LOAD	X	38	51	0.00=	0A	13.93=	09	GLOR UNIF	MV 0 1
680	LOAD	Y	38	51	0.00	15	13.93	17	GLOR UNIF	MV 0 1
681	LOAD	Z	38	51	0.00	1A	13.93	1A	GLOR UNIF	MV 0 1
682	LOAD	X	38	51	13.93=	09	13.93=	16	GLOR UNIF	MV 0 1
683	LOAD	Y	38	51	13.93	17	13.93	19	GLOR UNIF	MV 0 1
684	LOAD	Z	38	51	13.93	1A	13.93	21	GLOR UNIF	MV 0 1
685	LOAD	X	38	51	27.86=	10	13.93=	11	GLOR UNIF	MV 0 1
686	LOAD	Y	38	51	27.86	19	13.93	21	GLOR UNIF	MV 0 1
687	LOAD	Z	38	51	27.86	21	13.93	23	GLOR UNIF	MV 0 1
688	LOAD	X	38	51	41.79=	11	13.93=	12	GLOR UNIF	MV 0 1
689	LOAD	Y	38	51	41.79	21	13.93	23	GLOR UNIF	MV 0 1
690	LOAD	Z	38	51	41.79	23	13.93	2A	GLOR UNIF	MV 0 1
691	LOAD	X	34	53	0.00	09	9.49	26	GLOR UNIF	MV 0 1
692	LOAD	Y	34	53	0.00	23	9.49	25	GLOR UNIF	MV 0 1
693	LOAD	Z	34	53	0.00=	15	9.49=	16	GLOR UNIF	MV 0 1
694	LOAD	X	34	53	9.49	10	9.49	11	GLOR UNIF	MV 0 1
695	LOAD	Y	34	53	9.49	25	9.49	2A	GLOR UNIF	MV 0 1
696	LOAD	Z	34	53	9.49=	16	9.49=	1A	GLOR UNIF	MV 0 1
697	LOAD	X	34	53	16.97	11	9.49	13	GLOR UNIF	MV 0 1



698	LOAD	Y	34	53	18.97	28	9.49	31	GLOR	UNIF	MV	0	1
699	LOAD	Z	34	53	18.97	18	9.49	20	GLOR	UNIF	MV	0	1
700	LOAD	X	34	53	28.46	13	9.49	14	GLOR	UNIF	MV	0	1
701	LOAD	Y	34	53	28.46	31	9.49	34	GLOR	UNIF	MV	0	1
702	LOAD	Z	34	53	28.46	20	9.49	22	GLOR	UNIF	MV	0	1
703	LOAD	X	34	53	37.95	14	9.49	15	GLOR	UNIF	MV	0	1
704	LOAD	Y	34	53	37.95	34	9.49	34	GLOR	UNIF	MV	0	1
705	LOAD	Z	34	53	37.95	22	9.49	25	GLOR	UNIF	MV	0	1
706	LOAD	Y	55	58	6.00	113	5.70	124	GLOR	UNIF	MV	0	1
707	LOAD	Y	55	58	5.70	126	5.70	141	GLOR	UNIF	MV	0	1
708	LOAD	Y	55	54	11.40	141	5.70	158	GLOR	UNIF	MV	0	1
709	LOAD	Y	55	58	17.10	158	5.70	178	GLOR	UNIF	MV	0	1
710	LOAD	Y	55	58	22.80	174	5.70	202	GLOR	UNIF	MV	0	1
711	LOAD	Y	58	61	0.00	202	4.19	221	GLOR	UNIF	MV	0	1
712	LOAD	Y	58	61	4.19	221	4.19	244	GLOR	UNIF	MV	0	1
713	LOAD	Y	58	61	8.39	244	4.19	270	GLOR	UNIF	MV	0	1
714	LOAD	Y	58	59	0.00	113	5.70	124	GLOR	UNIF	MV	0	1
715	LOAD	Y	56	59	5.70	126	5.70	141	GLOR	UNIF	MV	0	1
716	LOAD	Y	58	59	11.40	141	5.70	158	GLOR	UNIF	MV	0	1
717	LOAD	Y	58	59	17.10	158	5.70	178	GLOR	UNIF	MV	0	1
718	LOAD	Y	58	59	22.80	174	5.70	202	GLOR	UNIF	MV	0	1
719	LOAD	Y	59	64	0.00	202	4.19	221	GLOR	UNIF	MV	0	1
720	LOAD	Y	59	64	4.19	221	4.19	244	GLOR	UNIF	MV	0	1
721	LOAD	Y	59	64	8.39	244	4.19	270	GLOR	UNIF	MV	0	1
722	LOAD	Y	57	60	0.00	116	5.70	129	GLOR	UNIF	MV	0	1
723	LOAD	Y	57	60	5.70	129	5.70	143	GLOR	UNIF	MV	0	1
724	LOAD	Y	57	60	11.40	143	5.70	160	GLOR	UNIF	MV	0	1
725	LOAD	Y	57	60	17.10	160	5.70	180	GLOR	UNIF	MV	0	1
726	LOAD	Y	57	60	22.80	180	5.70	201	GLOR	UNIF	MV	0	1
727	LOAD	Y	60	70	0.00	201	2.00	210	GLOR	UNIF	MV	0	1
728	LOAD	Y	60	70	2.00	210	2.00	220	GLOR	UNIF	MV	0	1
729	LOAD	Y	60	70	4.00	220	2.00	231	GLOR	UNIF	MV	0	1
730	LOAD	Y	70	67	0.00	231	.22	232	GLOR	UNIF	MV	0	1
731	LOAD	Y	70	67	.22	232	.22	233	GLOR	UNIF	MV	0	1
732	LOAD	Y	70	67	.44	233	.22	234	GLOR	UNIF	MV	0	1
733	LOAD	Y	70	67	.67	234	.22	235	GLOR	UNIF	MV	0	1
734	LOAD	Y	70	67	.89	235	.22	237	GLOR	UNIF	MV	0	1
735	LOAD	Y	70	67	1.11	237	.22	238	GLOR	UNIF	MV	0	1
736	LOAD	Y	70	67	1.33	238	.22	239	GLOR	UNIF	MV	0	1
737	LOAD	Y	70	67	1.56	239	.22	241	GLOR	UNIF	MV	0	1
738	LOAD	Y	70	67	1.78	241	.22		GLOR	UNIF	MV	0	1
739	LOAD	Y	58	59	0.00	71	9.67	71	GLOR	UNIF	MV	0	1
740	LOAD	Y	58	59	9.67	71	9.67	71	GLOR	UNIF	MV	0	1
741	LOAD	Y	58	59	19.33	71	9.67	71	GLOR	UNIF	MV	0	1
742	LOAD	X	59	60	0.00	31	9.67	52	GLOR	UNIF	MV	0	1
743	LOAD	Y	59	60	0.00	14	9.67	14	GLOR	UNIF	MV	0	1
744	LOAD	X	59	60	9.67	32	9.67	32	GLOR	UNIF	MV	0	1
745	LOAD	Y	59	60	9.67	14	9.67	14	GLOR	UNIF	MV	0	1
746	LOAD	X	59	60	19.33	32	9.67	31	GLOR	UNIF	MV	0	1
747	LOAD	Y	59	60	19.33	14	9.67	14	GLOR	UNIF	MV	0	1
748	LOAD	X	60	58	0.00	31	9.67	32	GLOR	UNIF	MV	0	1
749	LOAD	Y	60	58	0.00	14	9.67	14	GLOR	UNIF	MV	0	1
750	LOAD	X	60	58	9.67	52	9.67	32	GLOR	UNIF	MV	0	1
751	LOAD	Y	60	58	9.67	14	9.67	14	GLOR	UNIF	MV	0	1
752	LOAD	X	60	58	19.33	32	9.67	31	GLOR	UNIF	MV	0	1
753	LOAD	Y	60	58	19.33	14	9.67	14	GLOR	UNIF	MV	0	1



750	LOAD	Y	59	61	0.00	71	9.13	7A	GLOR	UNIF	WV	0	1
755	LOAD	Y	59	61	9.13	7A	9.13	8A	GLOR	UNIF	WV	0	1
756	LOAD	Y	59	61	10.25	8A	9.13	9A	GLOR	UNIF	WV	0	1
757	LOAD	X	60	64	0.00	24	8.41	27	GLOR	UNIF	WV	0	1
758	LOAD	Y	60	64	0.00	24	8.41	33	GLOR	UNIF	WV	0	1
759	LOAD	Z	60	64	0.00	25	8.41	28	GLOR	UNIF	WV	0	1
760	LOAD	X	60	64	8.41	27	8.41	30	GLOR	UNIF	WV	0	1
761	LOAD	Y	60	64	8.41	33	8.41	36	GLOR	UNIF	WV	0	1
762	LOAD	Z	60	64	8.41	24	8.41	31	GLOR	UNIF	WV	0	1
763	LOAD	X	60	64	10.41	30	8.41	33	GLOR	UNIF	WV	0	1
764	LOAD	Y	60	64	16.81	34	8.41	39	GLOR	UNIF	WV	0	1
765	LOAD	Z	60	64	16.81	31	8.41	34	GLOR	UNIF	WV	0	1
766	LOAD	X	58	67	0.00	24	7.07	27	GLOR	UNIF	WV	0	1
767	LOAD	Y	58	67	0.00	29	7.07	32	GLOR	UNIF	WV	0	1
768	LOAD	Z	58	67	0.00	25	7.07	28	GLOR	UNIF	WV	0	1
769	LOAD	X	58	67	7.07	27	7.07	29	GLOR	UNIF	WV	0	1
770	LOAD	Y	58	67	7.07	32	7.07	35	GLOR	UNIF	WV	0	1
771	LOAD	Z	58	67	7.07	24	7.07	30	GLOR	UNIF	WV	0	1
772	LOAD	X	58	67	14.14	29	7.07	31	GLOR	UNIF	WV	0	1
773	LOAD	Y	58	67	14.14	35	7.07	37	GLOR	UNIF	WV	0	1
774	LOAD	Z	58	67	14.14	30	7.07	32	GLOR	UNIF	WV	0	1
775	LOAD	Y	70	66	0.00	42	.53	43	GLOR	UNIF	WV	0	1
776	LOAD	Y	70	66	.53	43	.53	43	GLOR	UNIF	WV	0	1
777	LOAD	Y	70	66	.66	43	.53	43	GLOR	UNIF	WV	0	1
778	LOAD	Y	70	66	1.00	43	.53	43	GLOR	UNIF	WV	0	1
779	LOAD	Y	70	66	1.53	43	.53	43	GLOR	UNIF	WV	0	1
780	LOAD	Y	70	66	1.66	43	.53	44	GLOR	UNIF	WV	0	1
781	LOAD	Y	70	66	1.99	44	.53	44	GLOR	UNIF	WV	0	1
782	LOAD	Y	70	66	2.33	44	.53	44	GLOR	UNIF	WV	0	1
783	LOAD	Y	70	66	2.66	44	.53	44	GLOR	UNIF	WV	0	1
784	LOAD	Y	70	68	0.00	42	.53	43	GLOR	UNIF	WV	0	1
785	LOAD	Y	70	68	.33	43	.53	43	GLOR	UNIF	WV	0	1
786	LOAD	Y	70	68	.66	43	.53	43	GLOR	UNIF	WV	0	1
787	LOAD	Y	70	68	1.00	43	.53	43	GLOR	UNIF	WV	0	1
788	LOAD	Y	70	68	1.33	43	.53	43	GLOR	UNIF	WV	0	1
789	LOAD	Y	70	68	1.66	43	.53	44	GLOR	UNIF	WV	0	1
790	LOAD	Y	70	68	1.99	44	.53	44	GLOR	UNIF	WV	0	1
791	LOAD	Y	70	68	2.33	44	.53	44	GLOR	UNIF	WV	0	1
792	LOAD	Y	70	68	2.66	44	.53	44	GLOR	UNIF	WV	0	1
793	LOAD	Z	43	55	4.08	345			GLOR	COMC	WN	1	2
794	LOAD	Y	43	55					GLOR	COMC	WN	1	2
795	LOAD	Y	43	55	4.08	345			GLOR	COMC	WN	1	2
796	LOAD	Y	44	56					GLOR	COMC	WN	1	2
797	LOAD	X	44	56	4.07	345			GLOR	COMC	WN	1	2
798	LOAD	Y	45	57					GLOR	COMC	WN	1	2
799	LOAD	Y	45	57	4.08	1111			GLOR	COMC	WN	2	2
800	LOAD	Y	43	55					GLOR	COMC	WN	2	2
801	LOAD	X	43	55	4.08	1111			GLOR	COMC	WN	2	2
802	LOAD	Y	44	56					GLOR	COMC	WN	2	2
803	LOAD	X	44	56	4.07	1111			GLOR	COMC	WN	2	2
804	LOAD	Y	45	57					GLOR	COMC	WN	2	2
805	LOAD	Y	45	57	4.07	1111			GLOR	COMC	WN	2	2
806	LOAD	X	10	22	0.00	1	10.81	1	GLOR	UNIF	WV	0	2
807	LOAD	Y	10	22	0.00	51	10.81	52	GLOR	UNIF	WV	0	2
808	LOAD	Z	10	22	0.00	04	10.81	04	GLOR	UNIF	WV	0	2
809	LOAD	X	10	22	10.81	1	10.81	1	GLOR	UNIF	WV	0	2



A10	LOAD	Y	10	22	10.81	52	10.81	54	GLOR	UNIF	AV	0	2
A11	LOAD	Z	10	22	10.81	04	10.81	04	GLOR	UNIF	AV	0	2
A12	LOAD	Y	10	22	21.63	1	10.81	1	GLOR	UNIF	AV	0	2
A13	LOAD	Y	10	22	21.63	54	10.81	57	GLOR	UNIF	AV	0	2
A14	LOAD	Z	10	22	21.63	04	10.81	05	GLOR	UNIF	AV	0	2
A15	LOAD	Y	22	34	0.00	1	10.81	1	GLOR	UNIF	AV	0	2
A16	LOAD	X	22	34	0.00	57	10.81	62	GLOR	UNIF	AV	0	2
A17	LOAD	Z	22	34	0.00	05	10.81	05	GLOR	UNIF	AV	0	2
A18	LOAD	Y	22	34	10.81	1	10.81	1	GLOR	UNIF	AV	0	2
A19	LOAD	X	22	34	10.81	62	10.81	66	GLOR	UNIF	AV	0	2
A20	LOAD	Z	22	34	10.81	05	10.81	05	GLOR	UNIF	AV	0	2
A21	LOAD	Y	22	34	21.63	68	10.81	74	GLOR	UNIF	AV	0	2
A22	LOAD	X	22	34	21.63	05	10.81	06	GLOR	UNIF	AV	0	2
A23	LOAD	Z	22	34	21.63	05	10.81	06	GLOR	UNIF	AV	0	2
B24	LOAD	X	34	40	0.00	1	4.73	1	GLOR	UNIF	AV	0	2
B25	LOAD	Y	34	40	0.00	78	4.73	82	GLOR	UNIF	AV	0	2
B26	LOAD	Z	34	40	0.00	05	4.73	06	GLOR	UNIF	AV	0	2
B27	LOAD	X	34	40	4.73	1	4.73	1	GLOR	UNIF	AV	0	2
B28	LOAD	Y	34	40	4.73	82	4.73	87	GLOR	UNIF	AV	0	2
B29	LOAD	Z	34	40	4.73	06	4.73	06	GLOR	UNIF	AV	0	2
B30	LOAD	X	34	40	4.73	1	4.73	1	GLOR	UNIF	AV	0	2
B31	LOAD	Y	34	40	4.73	87	4.73	93	GLOR	UNIF	AV	0	2
B32	LOAD	Z	34	40	4.73	06	4.73	06	GLOR	UNIF	AV	0	2
B33	LOAD	X	40	49	0.00	1	6.09	1	GLOR	UNIF	AV	0	2
B34	LOAD	Y	40	49	0.00	92	6.09	101	GLOR	UNIF	AV	0	2
B35	LOAD	Z	40	49	0.00	08	6.09	09	GLOR	UNIF	AV	0	2
B36	LOAD	X	40	49	6.09	1	6.09	1	GLOR	UNIF	AV	0	2
B37	LOAD	Y	40	49	6.09	101	6.09	111	GLOR	UNIF	AV	0	2
B38	LOAD	Z	40	49	6.09	09	6.09	10	GLOR	UNIF	AV	0	2
B39	LOAD	X	40	49	12.17	1	6.09	02	GLOR	UNIF	AV	0	2
B40	LOAD	Y	40	49	12.17	111	6.09	123	GLOR	UNIF	AV	0	2
B41	LOAD	Z	40	49	12.17	10	6.09	11	GLOR	UNIF	AV	0	2
B42	LOAD	X	49	55	0.00	1	1.52	1	GLOR	UNIF	AV	0	2
B43	LOAD	Y	49	55	0.00	123	1.52	124	GLOR	UNIF	AV	0	2
B44	LOAD	Z	49	55	0.00	10	1.52	10	GLOR	UNIF	AV	0	2
B45	LOAD	X	49	55	1.52	1	1.52	1	GLOR	UNIF	AV	0	2
B46	LOAD	Y	49	55	1.52	126	1.52	129	GLOR	UNIF	AV	0	2
B47	LOAD	Z	49	55	1.52	10	1.52	11	GLOR	UNIF	AV	0	2
B48	LOAD	X	49	55	3.04	1	1.52	02	GLOR	UNIF	AV	0	2
B49	LOAD	Y	49	55	3.04	129	1.52	133	GLOR	UNIF	AV	0	2
B50	LOAD	Z	49	55	3.04	11	1.52	11	GLOR	UNIF	AV	0	2
B51	LOAD	X	12	24	0.00	1	10.81	1	GLOR	UNIF	AV	0	2
B52	LOAD	Y	12	24	0.00	51	10.81	52	GLOR	UNIF	AV	0	2
B53	LOAD	Z	12	24	0.00	04	10.81	04	GLOR	UNIF	AV	0	2
B54	LOAD	X	12	24	10.81	1	10.81	1	GLOR	UNIF	AV	0	2
B55	LOAD	Y	12	24	10.81	52	10.81	50	GLOR	UNIF	AV	0	2
B56	LOAD	Z	12	24	10.81	04	10.81	04	GLOR	UNIF	AV	0	2
B57	LOAD	X	12	24	21.63	1	10.81	1	GLOR	UNIF	AV	0	2
B58	LOAD	Y	12	24	21.63	54	10.81	57	GLOR	UNIF	AV	0	2
B59	LOAD	Z	12	24	21.63	04	10.81	05	GLOR	UNIF	AV	0	2
B60	LOAD	X	24	36	0.00	1	10.81	1	GLOR	UNIF	AV	0	2
B61	LOAD	Y	24	36	0.00	57	10.81	62	GLOR	UNIF	AV	0	2
B62	LOAD	Z	24	36	0.00	05	10.81	05	GLOR	UNIF	AV	0	2
B63	LOAD	X	24	36	10.81	1	10.81	1	GLOR	UNIF	AV	0	2
B64	LOAD	Y	24	36	10.81	62	10.81	68	GLOR	UNIF	AV	0	2
B65	LOAD	Z	24	36	10.81	05	10.81	05	GLOR	UNIF	AV	0	2





866	LOAD	X	24	36	21.63	1	10.81	1	10.81	GLOR UNIF	WV 0 2
867	LOAD	Y	24	36	21.63	68	10.81	76	10.81	GLOR UNIF	WV 0 2
868	LOAD	Z	24	36	21.63	05	10.81	06	10.81	GLOR UNIF	WV 0 2
869	LOAD	X	36	41	0.00	1	4.73	1	4.73	GLOR UNIF	WV 0 2
870	LOAD	Y	36	41	0.00	74	4.73	82	4.73	GLOR UNIF	WV 0 2
871	LOAD	Z	36	41	0.00	05	4.73	06	4.73	GLOR UNIF	WV 0 2
872	LOAD	X	36	41	4.73	1	4.73	1	4.73	GLOR UNIF	WV 0 2
873	LOAD	Y	36	41	4.73	82	4.73	87	4.73	GLOR UNIF	WV 0 2
874	LOAD	Z	36	41	4.73	06	4.73	06	4.73	GLOR UNIF	WV 0 2
875	LOAD	X	36	41	9.45	1	4.73	1	4.73	GLOR UNIF	WV 0 2
876	LOAD	Y	36	41	9.45	87	4.73	93	4.73	GLOR UNIF	WV 0 2
877	LOAD	Z	36	41	9.45	06	4.73	06	4.73	GLOR UNIF	WV 0 2
878	LOAD	X	41	51	0.00	1	6.09	1	6.09	GLOR UNIF	WV 0 2
879	LOAD	Y	41	51	0.00	92	6.09	101	6.09	GLOR UNIF	WV 0 2
880	LOAD	Z	41	51	0.00	08	6.09	09	6.09	GLOR UNIF	WV 0 2
881	LOAD	X	41	51	6.09	1	6.09	1	6.09	GLOR UNIF	WV 0 2
882	LOAD	Y	41	51	6.09	101	6.09	111	6.09	GLOR UNIF	WV 0 2
883	LOAD	Z	41	51	6.09	09	6.09	10	6.09	GLOR UNIF	WV 0 2
884	LOAD	X	41	51	12.17	1	6.09	02	6.09	GLOR UNIF	WV 0 2
885	LOAD	Y	41	51	12.17	111	6.09	123	6.09	GLOR UNIF	WV 0 2
886	LOAD	Z	41	51	12.17	10	6.09	11	6.09	GLOR UNIF	WV 0 2
887	LOAD	X	51	56	0.00	1	1.52	1	1.52	GLOR UNIF	WV 0 2
888	LOAD	Y	51	56	0.00	123	1.52	126	1.52	GLOR UNIF	WV 0 2
889	LOAD	Z	51	56	0.00	10	1.52	10	1.52	GLOR UNIF	WV 0 2
890	LOAD	X	51	56	1.52	1	1.52	1	1.52	GLOR UNIF	WV 0 2
891	LOAD	Y	51	56	1.52	126	1.52	129	1.52	GLOR UNIF	WV 0 2
892	LOAD	Z	51	56	1.52	10	1.52	11	1.52	GLOR UNIF	WV 0 2
893	LOAD	X	51	56	3.04	1	1.52	02	1.52	GLOR UNIF	WV 0 2
894	LOAD	Y	51	56	3.04	129	1.52	133	1.52	GLOR UNIF	WV 0 2
895	LOAD	Z	51	56	3.04	11	1.52	11	1.52	GLOR UNIF	WV 0 2
896	LOAD	X	14	26	0.00	39	10.81	41	10.81	GLOR UNIF	WV 0 2
897	LOAD	Y	14	26	0.00	07	10.81	07	10.81	GLOR UNIF	WV 0 2
898	LOAD	Z	14	26	10.81	41	10.81	42	10.81	GLOR UNIF	WV 0 2
899	LOAD	X	14	26	10.81	07	10.81	06	10.81	GLOR UNIF	WV 0 2
900	LOAD	Y	14	26	21.63	42	10.81	46	10.81	GLOR UNIF	WV 0 2
901	LOAD	Z	14	26	21.63	07	10.81	08	10.81	GLOR UNIF	WV 0 2
902	LOAD	X	26	38	0.00	45	10.81	47	10.81	GLOR UNIF	WV 0 2
903	LOAD	Y	26	38	0.00	09	10.81	09	10.81	GLOR UNIF	WV 0 2
904	LOAD	Z	26	38	10.81	47	10.81	51	10.81	GLOR UNIF	WV 0 2
905	LOAD	X	26	38	10.81	09	10.81	10	10.81	GLOR UNIF	WV 0 2
906	LOAD	Y	26	38	21.72	51	10.81	55	10.81	GLOR UNIF	WV 0 2
907	LOAD	Z	26	38	21.72	10	10.81	10	10.81	GLOR UNIF	WV 0 2
908	LOAD	X	38	42	0.00	51	5.01	55	5.01	GLOR UNIF	WV 0 2
909	LOAD	Y	38	42	0.00	20	5.01	21	5.01	GLOR UNIF	WV 0 2
910	LOAD	Z	38	42	5.01	55	5.01	59	5.01	GLOR UNIF	WV 0 2
911	LOAD	X	38	42	5.01	21	5.01	23	5.01	GLOR UNIF	WV 0 2
912	LOAD	Y	38	42	10.02	59	5.01	64	5.01	GLOR UNIF	WV 0 2
913	LOAD	Z	38	42	10.02	23	5.01	25	5.01	GLOR UNIF	WV 0 2
914	LOAD	X	42	53	0.00	53	5.31	58	5.31	GLOR UNIF	WV 0 2
915	LOAD	Y	42	53	0.00	33	5.31	36	5.31	GLOR UNIF	WV 0 2
916	LOAD	Z	42	53	5.31	58	5.31	61	5.31	GLOR UNIF	WV 0 2
917	LOAD	X	42	53	5.31	36	5.31	41	5.31	GLOR UNIF	WV 0 2
918	LOAD	Y	42	53	10.63	64	5.31	70	5.31	GLOR UNIF	WV 0 2
919	LOAD	Z	42	53	10.63	40	5.31	44	5.31	GLOR UNIF	WV 0 2
920	LOAD	X	42	53	15.94	70	5.31	78	5.31	GLOR UNIF	WV 0 2
921	LOAD	Y	42	53	15.94	44	5.31	49	5.31	GLOR UNIF	WV 0 2



922	LOAD	Y	53	57	0.00	106	1.52	109	GL04	UNIF	WV	0	2
923	LOAD	Z	53	57	0.00	18	1.52	18	GL06	UNIF	WV	0	2
924	LOAD	Y	53	57	1.52	109	1.52	113	GL04	UNIF	WV	0	2
925	LOAD	Z	53	57	1.52	18	1.52	19	GL04	UNIF	WV	0	2
926	LOAD	Y	53	57	3.04	113	1.52	116	GL04	UNIF	WV	0	2
927	LOAD	Z	53	57	3.04	19	1.52	19	GL06	UNIF	WV	0	2
928	LOAD	Y	10	11	0.00	23	9.67	23	GL04	UNIF	WV	0	2
929	LOAD	Y	10	11	9.67	23	9.67	23	GL14	UNIF	WV	0	2
930	LOAD	Y	10	11	19.33	23	9.67	23	GL04	UNIF	WV	0	2
931	LOAD	Y	11	12	0.00	23	9.67	23	GL04	UNIF	WV	0	2
932	LOAD	Y	11	12	9.67	23	9.67	23	GL04	UNIF	WV	0	2
933	LOAD	Y	11	12	19.33	23	9.67	23	GL14	UNIF	WV	0	2
934	LOAD	X	12	13	0.00	10	9.67	10	GL04	UNIF	WV	0	2
935	LOAD	Y	12	13	0.00	06	9.67	06	GL06	UNIF	WV	0	2
936	LOAD	X	12	13	9.67	10	9.67	10	GL06	UNIF	WV	0	2
937	LOAD	Y	12	13	9.67	06	9.67	06	GL06	UNIF	WV	0	2
938	LOAD	X	12	13	19.33	19	9.67	00	GL04	UNIF	WV	0	2
939	LOAD	Y	12	13	19.33	06	9.67	05	GL04	UNIF	WV	0	2
940	LOAD	X	13	14	0.00	09	9.67	09	GL04	UNIF	WV	0	2
941	LOAD	Y	13	14	0.00	05	9.67	05	GL04	UNIF	WV	0	2
942	LOAD	X	13	14	9.67	09	9.67	08	GL06	UNIF	WV	0	2
943	LOAD	Y	13	14	9.67	05	9.67	05	GL04	UNIF	WV	0	2
944	LOAD	X	13	14	19.34	08	9.67	08	GL04	UNIF	WV	0	2
945	LOAD	Y	13	14	19.34	05	9.67	05	GL04	UNIF	WV	0	2
946	LOAD	X	14	15	0.00	08	9.67	08	GL04	UNIF	WV	0	2
947	LOAD	Y	14	15	9.67	05	9.67	05	GL04	UNIF	WV	0	2
948	LOAD	X	14	15	9.67	05	9.67	05	GL04	UNIF	WV	0	2
949	LOAD	Y	14	15	9.67	05	9.67	05	GL04	UNIF	WV	0	2
950	LOAD	X	14	15	19.34	09	9.67	09	GL04	UNIF	WV	0	2
951	LOAD	Y	14	15	19.34	05	9.67	05	GL04	UNIF	WV	0	2
952	LOAD	X	15	16	0.00	09	9.67	10	GL04	UNIF	WV	0	2
953	LOAD	Y	15	16	0.00	05	9.67	06	GL04	UNIF	WV	0	2
954	LOAD	X	15	16	9.67	10	9.67	10	GL04	UNIF	WV	0	2
955	LOAD	Y	15	16	9.67	06	9.67	06	GL04	UNIF	WV	0	2
956	LOAD	X	15	16	19.33	10	9.67	10	GL04	UNIF	WV	0	2
957	LOAD	Y	15	16	19.33	06	9.67	06	GL04	UNIF	WV	0	2
958	LOAD	X	11	13	0.00	08	9.67	08	GL04	UNIF	WV	0	2
959	LOAD	Y	11	13	0.00	04	9.67	04	GL04	UNIF	WV	0	2
960	LOAD	X	11	13	9.67	08	9.67	07	GL04	UNIF	WV	0	2
961	LOAD	Y	11	13	9.67	04	9.67	04	GL04	UNIF	WV	0	2
962	LOAD	X	11	13	19.33	07	9.67	07	GL04	UNIF	WV	0	2
963	LOAD	Y	11	13	19.33	04	9.67	04	GL04	UNIF	WV	0	2
964	LOAD	X	13	15	0.00	17	9.67	17	GL04	UNIF	WV	0	2
965	LOAD	Y	13	15	9.67	17	9.67	17	GL04	UNIF	WV	0	2
966	LOAD	X	13	15	19.33	17	9.67	17	GL04	UNIF	WV	0	2
967	LOAD	Y	15	11	0.00	07	9.67	07	GL04	UNIF	WV	0	2
968	LOAD	X	15	11	0.00	04	9.67	04	GL04	UNIF	WV	0	2
969	LOAD	Y	15	11	9.67	07	9.67	07	GL04	UNIF	WV	0	2
970	LOAD	X	15	11	9.67	04	9.67	04	GL04	UNIF	WV	0	2
971	LOAD	Y	15	11	19.33	08	9.67	08	GL04	UNIF	WV	0	2
972	LOAD	X	15	11	19.33	04	9.67	04	GL04	UNIF	WV	0	2
973	LOAD	Y	22	23	0.00	26	8.13	26	GL04	UNIF	WV	0	2
974	LOAD	X	22	23	8.13	26	8.13	26	GL04	UNIF	WV	0	2
975	LOAD	Y	22	23	16.25	26	8.13	26	GL04	UNIF	WV	0	2
976	LOAD	X	23	24	0.00	26	8.13	26	GL04	UNIF	WV	0	2
977	LOAD	Y	23	24	8.13	26	8.13	26	GL04	UNIF	WV	0	2



978	LOAD	Y	23	24	16.25	26	A.13	26	GLOR UNIT	AV	0	2
979	LOAD	X	24	25	6.00	11	A.13	11	GLOR UNIT	AV	0	2
980	LOAD	Y	24	25	0.00	06	A.13	06	GLOR UNIT	AV	0	2
981	LOAD	X	24	25	A.13	11	A.13	11	GLOR UNIT	AV	0	2
982	LOAD	Y	24	25	A.13	06	A.13	06	GLOR UNIT	AV	0	2
983	LOAD	X	24	25	16.25	11	A.13	11	GLOR UNIT	AV	0	2
984	LOAD	Y	24	25	16.25	06	A.13	06	GLOR UNIT	AV	0	2
985	LOAD	X	25	26	0.00	11	A.13	11	GLOR UNIT	AV	0	2
986	LOAD	Y	25	26	0.00	06	A.13	06	GLOR UNIT	AV	0	2
987	LOAD	X	25	26	A.13	10	A.13	10	GLOR UNIT	AV	0	2
988	LOAD	Y	25	26	A.13	06	A.13	06	GLOR UNIT	AV	0	2
989	LOAD	X	25	26	16.25	10	A.13	10	GLOR UNIT	AV	0	2
990	LOAD	Y	25	26	16.25	06	A.13	06	GLOR UNIT	AV	0	2
991	LOAD	X	26	27	0.00	09	A.13	09	GLOR UNIT	AV	0	2
992	LOAD	Y	26	27	0.00	05	A.13	06	GLOR UNIT	AV	0	2
993	LOAD	X	26	27	A.13	10	A.13	10	GLOR UNIT	AV	0	2
994	LOAD	Y	26	27	A.13	06	A.13	06	GLOR UNIT	AV	0	2
995	LOAD	X	26	27	16.25	10	A.13	11	GLOR UNIT	AV	0	2
996	LOAD	Y	26	27	16.25	06	A.13	06	GLOR UNIT	AV	0	2
997	LOAD	X	27	28	0.00	11	A.13	11	GLOR UNIT	AV	0	2
998	LOAD	Y	27	28	0.00	04	A.14	06	GLOR UNIT	AV	0	2
999	LOAD	X	27	28	A.13	11	A.13	11	GLOR UNIT	AV	0	2
1000	LOAD	Y	27	28	A.13	06	A.13	06	GLOR UNIT	AV	0	2
1001	LOAD	X	27	28	16.25	11	A.13	11	GLOR UNIT	AV	0	2
1002	LOAD	Y	27	28	16.25	06	A.13	06	GLOR UNIT	AV	0	2
1003	LOAD	X	28	29	0.00	09	A.13	09	GLOR UNIT	AV	0	2
1004	LOAD	Y	28	29	0.00	05	A.13	05	GLOR UNIT	AV	0	2
1005	LOAD	X	28	29	A.13	09	A.13	04	GLOR UNIT	AV	0	2
1006	LOAD	Y	28	29	A.13	05	A.13	05	GLOR UNIT	AV	0	2
1007	LOAD	X	28	29	16.25	04	A.13	04	GLOR UNIT	AV	0	2
1008	LOAD	Y	28	29	16.25	05	A.13	05	GLOR UNIT	AV	0	2
1009	LOAD	X	28	29	0.00	19	A.13	19	GLOR UNIT	AV	0	2
1010	LOAD	Y	28	29	A.13	19	A.13	19	GLOR UNIT	AV	0	2
1011	LOAD	X	28	29	16.25	19	A.13	19	GLOR UNIT	AV	0	2
1012	LOAD	Y	28	29	0.00	04	A.13	04	GLOR UNIT	AV	0	2
1013	LOAD	X	28	29	0.00	05	A.13	05	GLOR UNIT	AV	0	2
1014	LOAD	Y	28	29	A.13	04	A.13	04	GLOR UNIT	AV	0	2
1015	LOAD	X	28	29	A.13	05	A.13	05	GLOR UNIT	AV	0	2
1016	LOAD	Y	28	29	16.25	09	A.13	09	GLOR UNIT	AV	0	2
1017	LOAD	X	28	29	16.25	05	A.13	05	GLOR UNIT	AV	0	2
1018	LOAD	Y	28	29	0.00	24	A.59	24	GLOR UNIT	AV	0	2
1019	LOAD	X	34	35	0.00	24	A.59	24	GLOR UNIT	AV	0	2
1020	LOAD	Y	34	35	13.14	24	A.59	24	GLOR UNIT	AV	0	2
1021	LOAD	X	35	36	0.00	24	A.59	24	GLOR UNIT	AV	0	2
1022	LOAD	Y	35	36	0.00	24	A.59	24	GLOR UNIT	AV	0	2
1023	LOAD	X	35	36	13.14	10	A.59	10	GLOR UNIT	AV	0	2
1024	LOAD	Y	36	37	0.00	10	A.59	10	GLOR UNIT	AV	0	2
1025	LOAD	X	36	37	0.00	06	A.59	06	GLOR UNIT	AV	0	2
1026	LOAD	Y	36	37	6.59	10	A.59	10	GLOR UNIT	AV	0	2
1027	LOAD	X	36	37	6.59	06	A.59	06	GLOR UNIT	AV	0	2
1028	LOAD	Y	36	37	13.14	10	A.59	10	GLOR UNIT	AV	0	2
1029	LOAD	X	36	37	13.14	09	A.59	06	GLOR UNIT	AV	0	2
1030	LOAD	Y	37	38	0.00	07	10.07	07	GLOR UNIT	AV	0	2
1031	LOAD	X	37	38	0.00	02	10.07	02	GLOR UNIT	AV	0	2
1032	LOAD	Y	37	38	10.07	07	10.07	06	GLOR UNIT	AV	0	2
1033	LOAD	X	37	38	10.07	02	10.07	02	GLOR UNIT	AV	0	2



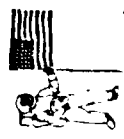


1030	LOAD	X	37	38	20.15	06	10.07	06	10.07	06	GL08 UNIF	WV 0 2
1031	LOAD	Y	37	38	20.15	02	10.07	02	10.07	02	GL08 UNIF	WV 0 2
1032	LOAD	Z	38	39	0.00	06	10.07	06	10.07	06	GL08 UNIF	WV 0 2
1033	LOAD	X	38	39	0.00	02	10.07	02	10.07	02	GL08 UNIF	WV 0 2
1034	LOAD	Y	38	39	16.07	06	10.07	06	10.07	06	GL08 UNIF	WV 0 2
1035	LOAD	Z	38	39	16.07	02	10.07	02	10.07	02	GL08 UNIF	WV 0 2
1036	LOAD	X	39	39	20.15	07	10.07	07	10.07	07	GL08 UNIF	WV 0 2
1037	LOAD	Y	39	39	20.15	02	10.07	02	10.07	02	GL08 UNIF	WV 0 2
1038	LOAD	Z	39	39	0.00	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1039	LOAD	X	39	39	6.59	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1040	LOAD	Y	39	39	6.59	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1041	LOAD	Z	39	39	13.18	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1042	LOAD	X	39	39	13.18	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1043	LOAD	Y	39	39	0.00	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1044	LOAD	Z	39	39	0.00	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1045	LOAD	X	39	39	6.59	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1046	LOAD	Y	39	39	6.59	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1047	LOAD	Z	39	39	13.18	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1048	LOAD	X	39	39	13.18	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1049	LOAD	Y	39	39	0.00	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1050	LOAD	Z	39	39	0.00	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1051	LOAD	X	39	39	6.59	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1052	LOAD	Y	39	39	6.59	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1053	LOAD	Z	39	39	13.18	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1054	LOAD	X	39	39	13.18	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1055	LOAD	Y	39	39	0.00	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1056	LOAD	Z	39	39	6.59	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1057	LOAD	X	39	39	6.59	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1058	LOAD	Y	39	39	0.00	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1059	LOAD	Z	39	39	6.59	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1060	LOAD	X	39	39	6.59	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1061	LOAD	Y	39	39	13.18	10	6.59	10	6.59	10	GL08 UNIF	WV 0 2
1062	LOAD	Z	39	39	13.18	06	6.59	06	6.59	06	GL08 UNIF	WV 0 2
1063	LOAD	X	49	50	6.00	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1064	LOAD	Y	49	50	6.00	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1065	LOAD	Z	49	50	5.05	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1066	LOAD	X	49	50	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1067	LOAD	Y	49	50	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1068	LOAD	Z	49	50	5.05	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1069	LOAD	X	50	51	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1070	LOAD	Y	50	51	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1071	LOAD	Z	50	51	0.00	21	5.05	21	5.05	21	GL08 UNIF	WV 0 2
1072	LOAD	X	51	52	0.00	12	5.05	12	5.05	12	GL08 UNIF	WV 0 2
1073	LOAD	Y	51	52	5.05	21	5.05	21	5.05	21	GL08 UNIF	WV 0 2
1074	LOAD	Z	51	52	5.05	12	5.05	12	5.05	12	GL08 UNIF	WV 0 2
1075	LOAD	X	51	52	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1076	LOAD	Y	51	52	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1077	LOAD	Z	51	52	0.00	12	5.05	12	5.05	12	GL08 UNIF	WV 0 2
1078	LOAD	X	52	53	5.05	20	5.05	20	5.05	20	GL08 UNIF	WV 0 2
1079	LOAD	Y	52	53	5.05	11	5.05	11	5.05	11	GL08 UNIF	WV 0 2
1080	LOAD	Z	52	53	5.05	19	5.05	19	5.05	19	GL08 UNIF	WV 0 2
1081	LOAD	X	52	53	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1082	LOAD	Y	52	53	10.10	04	5.05	04	5.05	04	GL08 UNIF	WV 0 2
1083	LOAD	Z	52	53	0.00	11	5.05	11	5.05	11	GL08 UNIF	WV 0 2
1084	LOAD	X	53	54	5.05	20	5.05	20	5.05	20	GL08 UNIF	WV 0 2
1085	LOAD	Y	53	54	5.05	11	5.05	11	5.05	11	GL08 UNIF	WV 0 2
1086	LOAD	Z	53	54	10.10	20	5.05	20	5.05	20	GL08 UNIF	WV 0 2
1087	LOAD	X	53	54	10.10	11	5.05	11	5.05	11	GL08 UNIF	WV 0 2
1088	LOAD	Y	53	54	0.00	20	5.05	20	5.05	20	GL08 UNIF	WV 0 2
1089	LOAD	Z	53	54	0.00	12	5.05	12	5.05	12	GL08 UNIF	WV 0 2
1090	LOAD	X	54	49	5.05	20	5.05	20	5.05	20	GL08 UNIF	WV 0 2





1090	LOAD	Y	54	49	5.05-	12	5.05-	GLOR	UNIF	WV	0	2
1091	LOAD	X	54	49	10.10-	21	5.05-	GLOR	UNIF	WV	0	2
1092	LOAD	Y	54	49	10.10-	12	5.05-	GLOR	UNIF	WV	0	2
1093	LOAD	X	50	52	0.00-	17	5.05-	GLOR	UNIF	WV	0	2
1094	LOAD	Y	50	52	0.00-	10	5.05-	GLOR	UNIF	WV	0	2
1095	LOAD	Y	50	52	5.05-	16	5.05-	GLOR	UNIF	WV	0	2
1096	LOAD	Y	50	52	5.05-	09	5.05-	GLOR	UNIF	WV	0	2
1097	LOAD	X	50	52	10.10-	16	5.05-	GLOR	UNIF	WV	0	2
1098	LOAD	Y	50	52	10.10-	09	5.05-	GLOR	UNIF	WV	0	2
1099	LOAD	Y	52	54	0.00-	37	5.05-	GLOR	UNIF	WV	0	2
1100	LOAD	Y	52	54	5.05-	37	5.05-	GLOR	UNIF	WV	0	2
1101	LOAD	Y	52	54	10.00-	37	5.05-	GLOR	UNIF	WV	0	2
1102	LOAD	X	54	50	0.00-	16	5.05-	GLOR	UNIF	WV	0	2
1103	LOAD	Y	54	50	0.00-	09	5.05-	GLOR	UNIF	WV	0	2
1104	LOAD	X	54	50	5.05-	16	5.05-	GLOR	UNIF	WV	0	2
1105	LOAD	Y	54	50	5.05-	09	5.15-	GLOR	UNIF	WV	0	2
1106	LOAD	X	54	50	10.10-	16	5.05-	GLOR	UNIF	WV	0	2
1107	LOAD	Y	54	50	10.10-	09	5.05-	GLOR	UNIF	WV	0	2
1108	LOAD	X	11	22	0.00-	1	13.44	GLOR	UNIF	WV	0	2
1109	LOAD	Y	11	22	0.00-	21	13.44	GLOR	UNIF	WV	0	2
1110	LOAD	Z	11	22	0.00-	1	13.44	GLOR	UNIF	WV	0	2
1111	LOAD	X	11	22	13.44	1	13.44	GLOR	UNIF	WV	0	2
1112	LOAD	Y	11	22	13.44	21	13.44	GLOR	UNIF	WV	0	2
1113	LOAD	Z	11	22	13.44	1	13.44	GLOR	UNIF	WV	0	2
1114	LOAD	X	11	22	26.88	1	13.44	GLOR	UNIF	WV	0	2
1115	LOAD	Y	11	22	26.88	22	13.44	GLOR	UNIF	WV	0	2
1116	LOAD	Z	11	22	26.88	1	13.44	GLOR	UNIF	WV	0	2
1117	LOAD	X	11	24	0.00-	1	13.44	GLOR	UNIF	WV	0	2
1118	LOAD	Y	11	24	0.00-	21	13.44	GLOR	UNIF	WV	0	2
1119	LOAD	Z	11	24	0.00	1	13.44	GLOR	UNIF	WV	0	2
1120	LOAD	X	11	24	13.44	1	13.44	GLOR	UNIF	WV	0	2
1121	LOAD	Y	11	24	13.44	21	13.44	GLOR	UNIF	WV	0	2
1122	LOAD	Z	11	24	13.44	1	13.44	GLOR	UNIF	WV	0	2
1123	LOAD	X	11	24	26.88	1	13.44	GLOR	UNIF	WV	0	2
1124	LOAD	Y	11	24	26.88	22	13.44	GLOR	UNIF	WV	0	2
1125	LOAD	Z	11	24	26.88	1	13.44	GLOR	UNIF	WV	0	2
1126	LOAD	X	13	24	0.00	03	13.44	GLOR	UNIF	WV	0	2
1127	LOAD	Y	13	24	0.00-	13	13.44	GLOR	UNIF	WV	0	2
1128	LOAD	Z	13	24	0.00-	08	13.44	GLOR	UNIF	WV	0	2
1129	LOAD	X	13	24	13.44	03	13.44	GLOR	UNIF	WV	0	2
1130	LOAD	Y	13	24	13.44	14	13.44	GLOR	UNIF	WV	0	2
1131	LOAD	Z	13	24	13.44	09	13.44	GLOR	UNIF	WV	0	2
1132	LOAD	X	13	24	26.88	03	13.44	GLOR	UNIF	WV	0	2
1133	LOAD	Y	13	24	26.88	15	13.44	GLOR	UNIF	WV	0	2
1134	LOAD	Z	13	24	26.88	09	13.44	GLOR	UNIF	WV	0	2
1135	LOAD	X	13	26	0.00	03	13.44	GLOR	UNIF	WV	0	2
1136	LOAD	Y	13	26	0.00-	15	13.44	GLOR	UNIF	WV	0	2
1137	LOAD	Z	13	26	0.00	07	13.44	GLOR	UNIF	WV	0	2
1138	LOAD	X	13	26	13.44	03	13.44	GLOR	UNIF	WV	0	2
1139	LOAD	Y	13	26	13.44	14	13.44	GLOR	UNIF	WV	0	2
1140	LOAD	Z	13	26	13.44	07	13.44	GLOR	UNIF	WV	0	2
1141	LOAD	X	13	26	26.88	03	13.44	GLOR	UNIF	WV	0	2
1142	LOAD	Y	13	26	26.88	14	13.44	GLOR	UNIF	WV	0	2
1143	LOAD	Z	13	26	26.88	07	13.44	GLOR	UNIF	WV	0	2
1144	LOAD	X	15	26	0.00-	03	13.44	GLOR	UNIF	WV	0	2
1145	LOAD	Y	15	26	0.00-	15	13.44	GLOR	UNIF	WV	0	2



1146	LOAD Z	15	24	0.00	07	13.44	07	GLOB UNIF	AV	0	2
1147	LOAD X	15	24	13.44	03	13.44	03	GLOB UNIF	AV	0	2
1148	LOAD Y	15	24	13.44	14	13.44	14	GLOB UNIF	AV	0	2
1149	LOAD Z	15	24	13.44	07	13.44	07	GLOB UNIF	AV	0	2
1150	LOAD X	15	24	26.88	03	13.44	03	GLOB UNIF	AV	0	2
1151	LOAD Y	15	24	26.88	14	13.44	14	GLOB UNIF	AV	0	2
1152	LOAD Z	15	24	26.88	07	13.44	07	GLOB UNIF	AV	0	2
1153	LOAD X	15	22	0.00	03	13.44	03	GLOB UNIF	AV	0	2
1154	LOAD Y	15	22	0.00	14	13.44	14	GLOB UNIF	AV	0	2
1155	LOAD Z	15	22	0.00	07	13.44	07	GLOB UNIF	AV	0	2
1156	LOAD X	15	22	13.44	03	13.44	03	GLOB UNIF	AV	0	2
1157	LOAD Y	15	22	13.44	14	13.44	14	GLOB UNIF	AV	0	2
1158	LOAD Z	15	22	13.44	09	13.44	09	GLOB UNIF	AV	0	2
1159	LOAD X	15	22	26.88	03	13.44	03	GLOB UNIF	AV	0	2
1160	LOAD Y	15	22	26.88	15	13.44	15	GLOB UNIF	AV	0	2
1161	LOAD Z	15	22	26.88	09	13.44	09	GLOB UNIF	AV	0	2
1162	LOAD X	22	36	0.00	1	18.20	1	GLOB UNIF	AV	0	2
1163	LOAD Y	22	36	0.00	29	18.20	29	GLOB UNIF	AV	0	2
1164	LOAD Z	22	36	0.00	1	18.20	1	GLOB UNIF	AV	0	2
1165	LOAD X	22	36	18.20	1	18.20	1	GLOB UNIF	AV	0	2
1166	LOAD Y	22	36	18.20	31	18.20	31	GLOB UNIF	AV	0	2
1167	LOAD Z	22	36	18.20	1	18.20	1	GLOB UNIF	AV	0	2
1168	LOAD X	22	36	36.39	1	18.20	1	GLOB UNIF	AV	0	2
1169	LOAD Y	22	36	36.39	34	18.20	34	GLOB UNIF	AV	0	2
1170	LOAD Z	22	36	36.39	1	18.20	1	GLOB UNIF	AV	0	2
1171	LOAD X	24	38	0.00	09	20.96	09	GLOB UNIF	AV	0	2
1172	LOAD Y	24	38	0.00	12	20.96	12	GLOB UNIF	AV	0	2
1173	LOAD Z	24	38	0.00	11	20.96	11	GLOB UNIF	AV	0	2
1174	LOAD X	24	38	20.96	09	20.96	09	GLOB UNIF	AV	0	2
1175	LOAD Y	24	38	20.96	12	20.96	12	GLOB UNIF	AV	0	2
1176	LOAD Z	24	38	20.96	12	20.96	12	GLOB UNIF	AV	0	2
1177	LOAD X	24	38	41.93	09	20.96	09	GLOB UNIF	AV	0	2
1178	LOAD Y	24	38	41.93	12	20.96	12	GLOB UNIF	AV	0	2
1179	LOAD Z	24	38	41.93	12	20.96	12	GLOB UNIF	AV	0	2
1180	LOAD X	26	34	0.00	05	13.65	05	GLOB UNIF	AV	0	2
1181	LOAD Y	26	34	0.00	11	13.65	11	GLOB UNIF	AV	0	2
1182	LOAD Z	26	34	0.00	10	13.65	10	GLOB UNIF	AV	0	2
1183	LOAD X	26	34	13.65	07	13.65	07	GLOB UNIF	AV	0	2
1184	LOAD Y	26	34	13.65	13	13.65	13	GLOB UNIF	AV	0	2
1185	LOAD Z	26	34	13.65	11	13.65	11	GLOB UNIF	AV	0	2
1186	LOAD X	26	34	27.29	04	13.65	04	GLOB UNIF	AV	0	2
1187	LOAD Y	26	34	27.29	14	13.65	14	GLOB UNIF	AV	0	2
1188	LOAD Z	26	34	27.29	13	13.65	13	GLOB UNIF	AV	0	2
1189	LOAD X	26	34	40.94	09	13.65	09	GLOB UNIF	AV	0	2
1190	LOAD Y	26	34	40.94	16	13.65	16	GLOB UNIF	AV	0	2
1191	LOAD Z	26	34	40.94	14	13.65	14	GLOB UNIF	AV	0	2
1192	LOAD X	36	49	0.00	02	11.86	02	GLOB UNIF	AV	0	2
1193	LOAD Y	36	49	0.00	38	11.86	38	GLOB UNIF	AV	0	2
1194	LOAD Z	36	49	0.00	1	11.86	1	GLOB UNIF	AV	0	2
1195	LOAD X	36	49	11.86	02	11.86	02	GLOB UNIF	AV	0	2
1196	LOAD Y	36	49	11.86	42	11.86	42	GLOB UNIF	AV	0	2
1197	LOAD Z	36	49	11.86	02	11.86	02	GLOB UNIF	AV	0	2
1198	LOAD X	36	49	23.72	02	11.86	02	GLOB UNIF	AV	0	2
1199	LOAD Y	36	49	23.72	44	11.86	44	GLOB UNIF	AV	0	2
1200	LOAD Z	36	49	23.72	02	11.86	02	GLOB UNIF	AV	0	2
1201	LOAD X	36	49	45.54	02	11.86	02	GLOB UNIF	AV	0	2





1202	LOAD	Y	36	49	35.5A	53	11.8A	60	GLOR UNIF	MV 0 2
1203	LOAD	Z	34	49	35.5A	02	11.8A	02	GLOR UNIF	MV 0 2
1204	LOAD	X	34	51	0.00	06	9.20	07	GLOR UNIF	MV 0 2
1205	LOAD	Y	34	51	0.00	11	9.20	13	GLOR UNIF	MV 0 2
1206	LOAD	Z	34	51	0.00	13	9.20	15	GLOR UNIF	MV 0 2
1207	LOAD	X	34	51	9.20	07	9.20	04	GLOR UNIF	MV 0 2
1208	LOAD	Y	34	51	9.20	13	9.20	15	GLOR UNIF	MV 0 2
1209	LOAD	Z	34	51	9.20	15	9.20	17	GLOR UNIF	MV 0 2
1210	LOAD	X	34	51	18.57	08	9.20	00	GLOR UNIF	MV 0 2
1211	LOAD	Y	34	51	18.57	15	9.20	17	GLOR UNIF	MV 0 2
1212	LOAD	Z	34	51	18.57	17	9.20	10	GLOR UNIF	MV 0 2
1213	LOAD	X	34	51	27.46	09	9.20	10	GLOR UNIF	MV 0 2
1214	LOAD	Y	34	51	27.46	17	9.20	19	GLOR UNIF	MV 0 2
1215	LOAD	Z	34	51	27.46	19	9.20	21	GLOR UNIF	MV 0 2
1216	LOAD	X	34	51	37.14	10	9.20	11	GLOR UNIF	MV 0 2
1217	LOAD	Y	34	51	37.14	19	9.20	22	GLOR UNIF	MV 0 2
1218	LOAD	Z	34	51	37.14	21	9.20	24	GLOR UNIF	MV 0 2
1219	LOAD	X	34	51	46.43	11	9.20	13	GLOR UNIF	MV 0 2
1220	LOAD	Y	34	51	46.43	22	9.20	24	GLOR UNIF	MV 0 2
1221	LOAD	Z	34	51	46.43	24	9.20	27	GLOR UNIF	MV 0 2
1222	LOAD	X	34	53	0.00	10	15.81	11	GLOR UNIF	MV 0 2
1223	LOAD	Y	34	53	0.00	24	15.81	27	GLOR UNIF	MV 0 2
1224	LOAD	Z	34	53	0.00	16	15.81	17	GLOR UNIF	MV 0 2
1225	LOAD	X	34	53	15.81	11	15.81	12	GLOR UNIF	MV 0 2
1226	LOAD	Y	34	53	15.81	27	15.81	30	GLOR UNIF	MV 0 2
1227	LOAD	Z	34	53	15.81	17	15.81	20	GLOR UNIF	MV 0 2
1228	LOAD	X	34	53	31.62	12	15.81	13	GLOR UNIF	MV 0 2
1229	LOAD	Y	34	53	31.62	30	15.81	33	GLOR UNIF	MV 0 2
1230	LOAD	Z	34	53	31.62	20	15.81	22	GLOR UNIF	MV 0 2
1231	LOAD	X	55	58	0.00	117	5.70	130	GLOR UNIF	MV 0 2
1232	LOAD	Y	55	58	5.70	130	5.70	146	GLOR UNIF	MV 0 2
1233	LOAD	Z	55	58	11.00	146	5.70	163	GLOR UNIF	MV 0 2
1234	LOAD	X	55	58	17.10	163	5.70	185	GLOR UNIF	MV 0 2
1235	LOAD	Y	55	58	22.40	185	5.70	210	GLOR UNIF	MV 0 2
1236	LOAD	Z	58	61	0.00	210	3.97	220	GLOR UNIF	MV 0 2
1237	LOAD	X	58	61	3.97	229	3.97	248	GLOR UNIF	MV 0 2
1238	LOAD	Y	58	61	7.95	248	3.97	275	GLOR UNIF	MV 0 2
1239	LOAD	Z	56	59	0.00	117	5.70	130	GLOR UNIF	MV 0 2
1240	LOAD	X	56	59	5.70	130	5.70	146	GLOR UNIF	MV 0 2
1241	LOAD	Y	56	59	11.40	146	5.70	163	GLOR UNIF	MV 0 2
1242	LOAD	Z	56	59	17.10	163	5.70	185	GLOR UNIF	MV 0 2
1243	LOAD	X	56	59	22.40	185	5.70	210	GLOR UNIF	MV 0 2
1244	LOAD	Y	59	64	0.00	210	3.97	229	GLOR UNIF	MV 0 2
1245	LOAD	Z	59	64	3.97	229	3.97	248	GLOR UNIF	MV 0 2
1246	LOAD	X	59	64	7.95	248	3.97	275	GLOR UNIF	MV 0 2
1247	LOAD	Y	57	60	0.00	104	5.70	114	GLOR UNIF	MV 0 2
1248	LOAD	Z	57	60	5.70	114	5.70	129	GLOR UNIF	MV 0 2
1249	LOAD	X	57	60	11.40	129	5.70	146	GLOR UNIF	MV 0 2
1250	LOAD	Y	57	60	17.10	144	5.70	163	GLOR UNIF	MV 0 2
1251	LOAD	Z	57	60	22.40	163	5.70	185	GLOR UNIF	MV 0 2
1252	LOAD	X	60	70	0.00	183	2.00	192	GLOR UNIF	MV 0 2
1253	LOAD	Y	60	70	2.00	192	2.00	201	GLOR UNIF	MV 0 2
1254	LOAD	Z	60	70	4.00	201	2.00	209	GLOR UNIF	MV 0 2
1255	LOAD	X	70	67	0.00	209	1.35	215	GLOR UNIF	MV 0 2
1256	LOAD	Y	70	67	1.35	215	1.35	223	GLOR UNIF	MV 0 2
1257	LOAD	Z	70	67	2.71	223	1.35	231	GLOR UNIF	MV 0 2



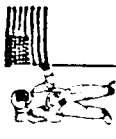
1258	LOAD	Y	58	59	0.00	74	9.67	74	GLOR UNIT	AV 0 2
1259	LOAD	Y	58	59	9.67	74	9.67	74	GLOR UNIT	AV 0 2
1260	LOAD	Y	58	59	19.33	74	9.67	74	GLOR UNIT	AV 0 2
1261	LOAD	X	59	60	0.00	31	9.67	31	GLOR UNIT	AV 0 2
1262	LOAD	X	59	60	0.00	19	9.67	19	GLOR UNIT	AV 0 2
1263	LOAD	X	59	60	9.67	31	9.67	31	GLOR UNIT	AV 0 2
1264	LOAD	Y	59	60	9.67	18	9.67	17	GLOR UNIT	AV 0 2
1265	LOAD	X	59	60	19.33	31	9.67	24	GLOR UNIT	AV 0 2
1266	LOAD	Y	59	60	19.33	17	9.67	16	GLOR UNIT	AV 0 2
1267	LOAD	X	60	58	0.00	28	9.67	30	GLOR UNIT	AV 0 2
1268	LOAD	Y	60	58	0.00	16	9.67	17	GLOR UNIT	AV 0 2
1269	LOAD	X	60	58	9.67	30	9.67	31	GLOR UNIT	AV 0 2
1270	LOAD	Y	60	58	9.67	17	9.67	18	GLOR UNIT	AV 0 2
1271	LOAD	X	60	58	19.33	31	9.67	32	GLOR UNIT	AV 0 2
1272	LOAD	Y	60	58	19.33	18	9.67	19	GLOR UNIT	AV 0 2
1273	LOAD	Y	59	61	0.00	74	8.65	81	GLOR UNIT	AV 0 2
1274	LOAD	Y	59	61	8.65	81	8.65	84	GLOR UNIT	AV 0 2
1275	LOAD	Y	59	61	17.29	88	8.65	97	GLOR UNIT	AV 0 2
1276	LOAD	X	60	64	0.00	22	6.25	25	GLOR UNIT	AV 0 2
1277	LOAD	Y	60	64	0.00	26	6.25	29	GLOR UNIT	AV 0 2
1278	LOAD	Z	60	64	0.00	23	6.25	25	GLOR UNIT	AV 0 2
1279	LOAD	X	60	64	6.25	25	6.25	27	GLOR UNIT	AV 0 2
1280	LOAD	Y	60	64	6.25	29	6.25	32	GLOR UNIT	AV 0 2
1281	LOAD	Z	60	64	6.25	25	6.25	28	GLOR UNIT	AV 0 2
1282	LOAD	X	60	64	12.49	27	6.25	30	GLOR UNIT	AV 0 2
1283	LOAD	Y	60	64	12.49	32	6.25	36	GLOR UNIT	AV 0 2
1284	LOAD	Z	60	64	12.49	28	6.25	31	GLOR UNIT	AV 0 2
1285	LOAD	X	60	64	18.74	30	6.25	33	GLOR UNIT	AV 0 2
1286	LOAD	Y	60	64	18.74	36	6.25	39	GLOR UNIT	AV 0 2
1287	LOAD	Z	60	64	18.74	31	6.25	34	GLOR UNIT	AV 0 2
1288	LOAD	X	58	67	0.00	25	7.69	27	GLOR UNIT	AV 0 2
1289	LOAD	Y	58	67	0.00	31	7.69	32	GLOR UNIT	AV 0 2
1290	LOAD	Z	58	67	0.00	26	7.69	28	GLOR UNIT	AV 0 2
1291	LOAD	X	58	67	7.69	27	7.69	28	GLOR UNIT	AV 0 2
1292	LOAD	Y	58	67	7.69	32	7.69	34	GLOR UNIT	AV 0 2
1293	LOAD	Z	58	67	7.69	24	7.69	29	GLOR UNIT	AV 0 2
1294	LOAD	X	58	67	15.38	28	7.69	30	GLOR UNIT	AV 0 2
1295	LOAD	Y	58	67	15.38	34	7.69	36	GLOR UNIT	AV 0 2
1296	LOAD	Z	58	67	15.38	29	7.69	31	GLOR UNIT	AV 0 2
1297	LOAD	Y	70	66	0.00	38	2.02	40	GLOR UNIT	AV 0 2
1298	LOAD	Y	70	66	2.02	40	2.02	41	GLOR UNIT	AV 0 2
1299	LOAD	Y	70	66	4.04	41	2.02	43	GLOR UNIT	AV 0 2
1300	LOAD	Y	70	68	0.00	38	2.02	40	GLOR UNIT	AV 0 2
1301	LOAD	Y	70	68	2.02	40	2.02	41	GLOR UNIT	AV 0 2
1302	LOAD	Y	70	68	4.04	41	2.02	43	GLOR UNIT	AV 0 2
1303	LOAD	Z	3							
1304	LOAD	Z	1	4	0.00	557	6.06	557	GLOR UNIT	DL 0 3
1305	LOAD	Z	4	16	0.00	557	32.44	557	GLOR UNIT	DL 0 3
1306	LOAD	Z	16	28	0.00	403	32.44	403	GLOR UNIT	DL 0 3
1307	LOAD	Z	28	43	0.00	403	32.44	403	GLOR UNIT	DL 0 3
1308	LOAD	Z	43	55	0.00	403	4.59	403	GLOR UNIT	DL 0 3
1309	LOAD	Z	2	5	0.00	557	6.06	557	GLOR UNIT	DL 0 3
1310	LOAD	Z	5	17	0.00	557	32.44	557	GLOR UNIT	DL 0 3
1311	LOAD	Z	17	29	0.00	403	32.44	403	GLOR UNIT	DL 0 3
1312	LOAD	Z	29	44	0.00	403	32.44	403	GLOR UNIT	DL 0 3
1313	LOAD	Z	44	56	0.00	403	4.59	403	GLOR UNIT	DL 0 3



1314	LOAD	Z	3	6	0.00	.557	6.07			GLOR	UNTF	DL	0	3
1315	LOAD	Z	4	18	0.00	.557	32.44			GLOR	UNTF	DL	0	3
1316	LOAD	Z	18	30	0.00	.403	32.58			GLOR	UNTF	DL	0	3
1317	LOAD	Z	30	45	0.00	.403	36.13			GLOR	UNTF	DL	0	3
1318	LOAD	Z	45	57	0.00	.403	4.58			GLOR	UNTF	DL	0	3
1319	LOAD	Z	10	22	0.00	.183	32.44			GLOR	UNTF	DL	0	3
1320	LOAD	Z	22	34	0.00	.183	32.44			GLOR	UNTF	DL	0	3
1321	LOAD	Z	34	40	0.00	.371	14.26			GLOR	UNTF	DL	0	3
1322	LOAD	Z	40	49	0.00	.371	14.26			GLOR	UNTF	DL	0	3
1323	LOAD	Z	49	55	0.00	.371	4.56			GLOR	UNTF	DL	0	3
1324	LOAD	Z	12	24	0.00	.183	32.44			GLOR	UNTF	DL	0	3
1325	LOAD	Z	24	36	0.00	.183	32.44			GLOR	UNTF	DL	0	3
1326	LOAD	Z	36	41	0.00	.371	14.26			GLOR	UNTF	DL	0	3
1327	LOAD	Z	41	51	0.00	.371	14.26			GLOR	UNTF	DL	0	3
1328	LOAD	Z	51	56	0.00	.371	4.56			GLOR	UNTF	DL	0	3
1329	LOAD	Z	14	26	0.00	.183	32.44			GLOR	UNTF	DL	0	3
1330	LOAD	Z	26	34	0.00	.183	32.58			GLOR	UNTF	DL	0	3
1331	LOAD	Z	34	42	0.00	.371	15.03			GLOR	UNTF	DL	0	3
1332	LOAD	Z	42	53	0.00	.371	21.26			GLOR	UNTF	DL	0	3
1333	LOAD	Z	53	57	0.00	.371	4.56			GLOR	UNTF	DL	0	3
1334	LOAD	Z	10	11	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1335	LOAD	Z	11	12	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1336	LOAD	Z	12	13	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1337	LOAD	Z	13	14	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1338	LOAD	Z	14	15	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1339	LOAD	Z	15	10	1.71	.081	25.58			GLOR	UNTF	DL	0	3
1340	LOAD	Z	11	13	1.41	.047	26.17			GLOR	UNTF	DL	0	3
1341	LOAD	Z	13	15	1.41	.047	26.17			GLOR	UNTF	DL	0	3
1342	LOAD	Z	15	11	1.41	.047	26.17			GLOR	UNTF	DL	0	3
1343	LOAD	Z	22	23	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1344	LOAD	Z	23	24	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1345	LOAD	Z	24	25	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1346	LOAD	Z	25	26	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1347	LOAD	Z	26	27	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1348	LOAD	Z	27	22	1.71	.081	20.96			GLOR	UNTF	DL	0	3
1349	LOAD	Z	23	25	1.41	.047	21.55			GLOR	UNTF	DL	0	3
1350	LOAD	Z	25	27	1.41	.047	21.55			GLOR	UNTF	DL	0	3
1351	LOAD	Z	27	23	1.41	.047	21.55			GLOR	UNTF	DL	0	3
1352	LOAD	Z	34	35	1.71	.057	16.35			GLOR	UNTF	DL	0	3
1353	LOAD	Z	35	36	1.71	.057	16.35			GLOR	UNTF	DL	0	3
1354	LOAD	Z	36	37	1.71	.057	16.35			GLOR	UNTF	DL	0	3
1355	LOAD	Z	37	38	1.71	.057	26.80			GLOR	UNTF	DL	0	3
1356	LOAD	Z	38	39	1.71	.057	26.80			GLOR	UNTF	DL	0	3
1357	LOAD	Z	39	34	1.71	.057	16.35			GLOR	UNTF	DL	0	3
1358	LOAD	Z	35	37	1.71	.043	16.35			GLOR	UNTF	DL	0	3
1359	LOAD	Z	37	39	1.71	.043	16.35			GLOR	UNTF	DL	0	3
1360	LOAD	Z	39	35	1.71	.043	16.35			GLOR	UNTF	DL	0	3
1361	LOAD	Z	49	50	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1362	LOAD	Z	50	51	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1363	LOAD	Z	51	52	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1364	LOAD	Z	52	53	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1365	LOAD	Z	53	54	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1366	LOAD	Z	54	49	1.71	.072	11.73			GLOR	UNTF	DL	0	3
1367	LOAD	Z	50	52	1.71	.057	11.73			GLOR	UNTF	DL	0	3
1368	LOAD	Z	52	54	1.71	.057	11.73			GLOR	UNTF	DL	0	3
1369	LOAD	Z	54	50	1.71	.057	11.73			GLOR	UNTF	DL	0	3



1370	LOAD	Z	11	22	1.71	-.072	34.90	-.072	GLOR UNIF	DL 0 3
1371	LOAD	Z	11	24	1.71	-.072	36.90	-.072	GLOR UNIF	DL 0 3
1372	LOAD	Z	13	24	1.71	-.072	36.89	-.072	GLOR UNIF	DL 0 3
1373	LOAD	Z	13	26	1.71	-.072	36.90	-.072	GLOR UNIF	DL 0 3
1374	LOAD	Z	15	26	1.71	-.072	36.89	-.072	GLOR UNIF	DL 0 3
1375	LOAD	Z	15	22	1.71	-.072	36.89	-.072	GLOR UNIF	DL 0 3
1376	LOAD	Z	22	36	2.42	-.112	44.76	-.112	GLOR UNIF	DL 0 3
1377	LOAD	Z	24	3A	2.42	-.112	50.96	-.112	GLOR UNIF	DL 0 3
1378	LOAD	Z	26	34	2.42	-.112	44.76	-.112	GLOR UNIF	DL 0 3
1379	LOAD	Z	36	49	2.42	-.112	42.61	-.112	GLOR UNIF	DL 0 3
1380	LOAD	Z	38	51	2.42	-.112	51.89	-.112	GLOR UNIF	DL 0 3
1381	LOAD	Z	34	53	2.42	-.112	42.60	-.112	GLOR UNIF	DL 0 3
1382	LOAD	Z	4	7	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1383	LOAD	Z	7	10	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1384	LOAD	Z	5	8	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1385	LOAD	Z	8	12	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1386	LOAD	Z	6	9	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1387	LOAD	Z	9	14	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1388	LOAD	Z	16	19	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1389	LOAD	Z	19	22	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1390	LOAD	Z	17	20	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1391	LOAD	Z	20	24	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1392	LOAD	Z	18	21	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1393	LOAD	Z	21	26	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1394	LOAD	Z	28	31	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1395	LOAD	Z	31	34	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1396	LOAD	Z	29	32	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1397	LOAD	Z	32	36	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1398	LOAD	Z	30	33	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1399	LOAD	Z	33	38	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1400	LOAD	Z	43	46	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1401	LOAD	Z	46	49	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1402	LOAD	Z	44	47	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1403	LOAD	Z	47	51	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1404	LOAD	Z	45	48	0.00	-.148	2.40	-.148	GLOR UNIF	DL 0 3
1405	LOAD	Z	48	53	0.00	-.148	2.50	-.148	GLOR UNIF	DL 0 3
1406	LOAD	Z	55	58	0.00	-.403	23.00	-.403	GLOR UNIF	DL 0 3
1407	LOAD	Z	55	58	23.00	-.464	5.50	-.464	GLOR UNIF	DL 0 3
1408	LOAD	Z	58	61	0.00	-.464	15.00	-.464	GLOR UNIF	DL 0 3
1409	LOAD	Z	61	71	0.00	-.464	15.00	-.464	GLOR UNIF	DL 0 3
1410	LOAD	Z	56	59	0.00	-.403	23.00	-.403	GLOR UNIF	DL 0 3
1411	LOAD	Z	56	59	23.00	-.464	5.50	-.464	GLOR UNIF	DL 0 3
1412	LOAD	Z	59	64	0.00	-.464	15.00	-.464	GLOR UNIF	DL 0 3
1413	LOAD	Z	64	72	0.00	-.464	15.00	-.464	GLOR UNIF	DL 0 3
1414	LOAD	Z	57	60	0.00	-.403	23.00	-.403	GLOR UNIF	DL 0 3
1415	LOAD	Z	57	60	23.00	-.464	5.50	-.464	GLOR UNIF	DL 0 3
1416	LOAD	Z	60	70	0.00	-.464	5.00	-.464	GLOR UNIF	DL 0 3
1417	LOAD	Z	70	67	0.00	-.464	9.00	-.464	GLOR UNIF	DL 0 3
1418	LOAD	Z	67	76	0.00	-.464	4.00	-.464	GLOR UNIF	DL 0 3
1419	LOAD	Z	76	75	0.00	-.464	11.00	-.464	GLOR UNIF	DL 0 3
1420	LOAD	Z	58	59	1.71	-.065	25.58	-.065	GLOR UNIF	DL 0 3
1421	LOAD	Z	59	60	1.71	-.065	25.58	-.065	GLOR UNIF	DL 0 3
1422	LOAD	Z	60	68	1.71	-.065	25.58	-.065	GLOR UNIF	DL 0 3
1423	LOAD	Z	59	61	1.71	-.065	29.23	-.065	GLOR UNIF	DL 0 3
1424	LOAD	Z	60	64	1.71	-.065	29.23	-.065	GLOR UNIF	DL 0 3
1425	LOAD	Z	58	67	1.71	-.065	29.23	-.065	GLOR UNIF	DL 0 3



1426	LOAD Z	70	69	1.59	-0.19	10.27	-0.19	GL08	UNIF	DL	0	3
1427	LOAD Z	70	68	1.59	-0.19	10.27	-0.19	GL08	UNIF	DL	0	3
1428	LOAD Z	76	77	1.71	-0.50	14.78	-0.50	GL08	UNIF	DL	0	3
1429	LOAD Z	76	78	1.71	-0.50	14.78	-0.50	GL08	UNIF	DL	0	3
1430	LOAD Z	61	62	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1431	LOAD Z	62	63	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1432	LOAD Z	63	64	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1433	LOAD Z	64	65	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1434	LOAD Z	65	67	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1435	LOAD Z	67	69	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1436	LOAD Z	69	61	0.00	-0.55	7.50	-0.55	GL08	UNIF	DL	0	3
1437	LOAD Z	63	65	0.00	-0.24	7.50	-0.24	GL08	UNIF	DL	0	3
1438	LOAD Z	65	66	0.00	-0.24	17.61	-0.24	GL08	UNIF	DL	0	3
1439	LOAD Z	66	67	0.00	-0.24	10.00	-0.24	GL08	UNIF	DL	0	3
1440	LOAD Z	67	68	0.00	-0.24	10.00	-0.24	GL08	UNIF	DL	0	3
1441	LOAD Z	68	69	0.00	-0.24	17.61	-0.24	GL08	UNIF	DL	0	3
1442	LOAD Z	69	62	0.00	-0.24	7.50	-0.24	GL08	UNIF	DL	0	3
1443	LOAD Z	71	73	0.00	-0.55	3.00	-0.55	GL08	UNIF	DL	0	3
1444	LOAD Z	71	72	0.00	-0.55	29.00	-0.55	GL08	UNIF	DL	0	3
1445	LOAD Z	72	74	0.00	-0.55	3.00	-0.55	GL08	UNIF	DL	0	3
1446	LOAD Z	71	81	0.00	-0.55	5.00	-0.55	GL08	UNIF	DL	0	3
1447	LOAD Z	71	77	0.00	-0.55	25.11	-0.55	GL08	UNIF	DL	0	3
1448	LOAD Z	77	83	0.00	-0.55	5.00	-0.55	GL08	UNIF	DL	0	3
1449	LOAD Z	72	82	0.00	-0.55	5.00	-0.55	GL08	UNIF	DL	0	3
1450	LOAD Z	72	78	0.00	-0.55	25.11	-0.55	GL08	UNIF	DL	0	3
1451	LOAD Z	78	84	0.00	-0.55	5.00	-0.55	GL08	UNIF	DL	0	3
1452	LOAD Z	77	79	0.00	-0.55	3.00	-0.55	GL08	UNIF	DL	0	3
1453	LOAD Z	77	75	0.00	-0.55	14.50	-0.55	GL08	UNIF	DL	0	3
1454	LOAD Z	75	78	0.00	-0.55	14.50	-0.55	GL08	UNIF	DL	0	3
1455	LOAD Z	78	80	0.00	-0.55	3.00	-0.55	GL08	UNIF	DL	0	3
1456	LOAD Z	71	75	0.00	-0.16	29.00	-0.16	GL08	UNIF	DL	0	3
1457	LOAD Z	72	75	0.00	-0.16	29.00	-0.16	GL08	UNIF	DL	0	3
1458	LOADEN							GL08	C0VC	RUAT	ENG	
1459	LOAD Y	40	49	89	242			GL08	C0VC	RUAT	ENG	
1460	LOAD Y	41	51	89	242			GL08	C0VC	STAIRS		
1461	LOAD Y	55	58	242	406			GL08	C0VC	STAIRS		
1462	LOAD Y	56	59	242	406			GL08	C0VC	STAIRS		
1463	LOADEN							GL08	UNIF	ADD	DEAD	
1464	LOAD Z	61	62		-13			GL08	UNIF	ADD	DEAD	
1465	LOAD Z	62	63		-13			GL08	UNIF	ADD	DEAD	
1466	LOAD Z	63	64		-13			GL08	UNIF	ADD	DEAD	
1467	LOAD Z	64	65		-13			GL08	UNIF	ADD	DEAD	
1468	LOAD Z	65	67		-13			GL08	UNIF	ADD	DEAD	
1469	LOAD Z	67	69		-13			GL08	UNIF	ADD	DEAD	
1470	LOAD Z	69	61		-13			GL08	UNIF	ADD	DEAD	
1471	LOAD Z	61	71	15	-793			GL08	C0VC	ADD	DEAD	
1472	LOAD Z	60	72	15	-793			GL08	C0VC	ADD	DEAD	
1473	LOAD Z	76	75	15	-793			GL08	C0VC	ADD	DEAD	
1474	LOADEN							GL08	UNIF	LIVE	LDS	
1475	LOAD Z	61	62		-86			GL08	UNIF	LIVE	LDS	
1476	LOAD Z	62	63		-86			GL08	UNIF	LIVE	LDS	
1477	LOAD Z	63	64		-86			GL08	UNIF	LIVE	LDS	
1478	LOAD Z	64	65		-86			GL08	UNIF	LIVE	LDS	
1479	LOAD Z	65	67		-86			GL08	UNIF	LIVE	LDS	
1480	LOAD Z	67	69		-86			GL08	UNIF	LIVE	LDS	
1481	LOAD Z	69	61		-86			GL08	UNIF	LIVE	LDS	



JVJOCME 04/27/76 UNITED COMPUTING* 67, APRX/91 4,0,25

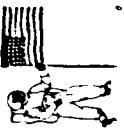
09.53.23	DATAEDT,CM100,1200,PT.				
09.53.23AFL	64	0.000			
09.53.23BAC	3400CR0023,277710GCC 3H				
09.53.23	04/27/76, JVJOCME				
09.53.24SFL	3192	0.000			
09.53.24GET	DATAEDT(LIBRARY)				
09.53.24PFADY	= DATAEDT				
09.53.24GET	TAPE9=S771C1.				
09.53.26	READY = S771C1				
09.53.26AFL	31000.				
09.53.26SFL	4096	0.001	0	0.	
09.53.26SFT	225	2			
09.53.26SFL	12800	0.001			
09.53.26	MAP,OFF.				
09.53.26	REDUCE.				
09.53.26SFL	256	0.003			
09.53.27	DATAEDT.				
09.53.27SFLS	12800	0.003			
09.53.27SFLR	12800	0.004	126	5	
09.53.28SFLR	17400	0.103	4	1	
09.53.28AFL	REQUIRED TO LOAD				
09.53.28AFL	REQUIRED TO EXECUTE				
09.53.28AFL	17400 (M064)				
09.53.32	STOP				
09.53.32	REPLACE, TAPE10=S771C2.				
09.53.34	READY = S771C2				
09.53.34	CUST.				
09.53.34SFL	A064	3.265	870	51.	
09.53.34SFT	212				
09.53.35.	SERVICE UNITS*		14.9		
09.53.35.	JOB COSTS*		3.73		
09.53.35SFL	12288	3.284	7	5	
09.53.35	EXIT.				
09.53.35J700	2368	3.284			
09.53.35.	*FL* *CPU SEC. *DISC PRUS* DISC ACC				
09.53.35.	*P.F. PRUS*P.F. ACC *TAPE PRUS* TAPE ACC				



LINE NO. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92

LINE NO.	DESCRIPTION	UNIT	QTY	PRICE	TOTAL	DATE	STATUS	REMARKS
43	100							
44	90							
45	80							
46	70							
47	60							
48	50							
49	40							
50	30							
51	WIND 1	90	3410	1500	100	173	15	ALL
52	WIND 2	290	3410	1400	100	173	15	ALL
53	END							
54	SFCT							
55	SFCT PTLING1	THU	18410	5536000	2768100			3600 1750
56	SFCT PTLING2	THU	13404	4125024	2062512			3600 1250
57	SFCT IKTLEG1	THU	6205	2420592	1210296			4000 500
58	SFCT IKTLEG2	THU	12504	5020702	2510351			4100 1000
59	SFCT BRACE1	THU	3800	3578784	1789392			2000 625
60	SFCT BRACE2	THU	2700	210632	105316			1800 500
61	SFCT BRACE3	THU	2415	146384	73192			1600 500
62	SFCT BRACE4	THU	1405	70260	35130			1000 375
63	SFCT BRACE5	THU	1920	72720	36360			1275 500
64	SFCT BRACE6	THU	1458	55832	27916			1275 375
65	SFCT BRACE7	THU	558	5430	2715			4625 280
66	SFCT WISBARM	PRY	5000	3000000	3000000			1000
67	SFCT SURTIEG	THU	13404	4125024	2062512			3600 1250
68	SFCT WAX20	WPC	1420	125	176			750 570
69	SFCT WAX20	WPC	704	30	211			650 398
70	SFCT WAX15	WPC	456	11	50			600 269
71	GRID							
72	GRID P10 PTLING1		3600	1750	2900	1160	3600	1
73	GRID P20 PTLING2		3600	1250	2900	1160	3600	1
74	GRID P11 IKTLEG1		4100	1000	2900	1160	3600	1
75	GRID P12 IKTLEG2		4100	1000	2900	1160	3600	1
76	GRID P01 BRACE1		2000	625	2900	1160	3600	2 483 A A
77	GRID P02 BRACE2		1800	500	2900	1160	3600	2 302 R A
78	GRID P03 BRACE3		1600	500	2900	1160	3600	2 302 R A
79	GRID P04 BRACE4		1400	375	2900	1160	3600	2 283 A A
80	GRID P05 BRACE5		1275	500	2900	1160	3600	2 302 R A
81	GRID P06 BRACE6		1275	375	2900	1160	3600	2 302 R A
82	GRID P07 BRACE7		4625	280	2900	1160	3600	2 314 R A
83	GRID WAX PYSURV				2900	1160	3600	2 01
84	GRID ST1 SURTIEG		3600	1250	2900	1160	3600	1 01
85	GRID W18 WAX50				2900	1160	3600	1 01
86	GRID W04 WAX20				2900	1160	3600	1 01
87	GRID W06 WAX15				2900	1160	3600	1 01
88	MEMBER							
89	MEMBER							
90	MEMBER							
91	MEMBER							
92	MEMBER							

F 0000 1
F 0000 1
F 0000 1
F 0000 1



LINE NO. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40

98	MEMBER	43	55	RD	F	0000	1
99	MEMBER	2	5	RD	F	0000	2
95	MEMBER	5	17	RD	F	0000	2
96	MEMBER	17	29	RD	F	0000	2
97	MEMBER	20	44	RD	F	0000	2
98	MEMBER	44	56	RD	F	0000	2
99	MEMBER	3	6	RD	F	0000	3
100	MEMBER	4	18	RD	F	0000	3
101	MEMBER	18	30	RD	F	0000	3
102	MEMBER	30	45	RD	F	0000	3
103	MEMBER	45	57	RD	F	0000	3
104	MEMBER	10	22	RD	F	0000	3
105	MEMBER	22	34	RD	F	0000	3
106	MEMBER	34	40	RD	F	0000	3
107	MEMBER	40	49	RD	F	0000	3
108	MEMBER	49	55	RD	F	0000	3
109	MEMBER	12	24	RD	F	0000	3
110	MEMBER	24	36	RD	F	0000	3
111	MEMBER	36	41	RD	F	0000	3
112	MEMBER	41	51	RD	F	0000	3
113	MEMBER	51	56	RD	F	0000	3
114	MEMBER	14	26	RD	F	0000	3
115	MEMBER	26	38	RD	F	0000	3
116	MEMBER	38	42	RD	F	0000	3
117	MEMBER	42	53	RD	F	0000	3
118	MEMBER	53	57	RD	F	0000	3
119	MEMBER	10	11	RD	F	0000	3
120	MEMBER	11	12	RD	F	0000	3
121	MEMBER	12	13	RD	F	0000	3
122	MEMBER	13	14	RD	F	0000	3
123	MEMBER	14	15	RD	F	0000	3
124	MEMBER	15	16	RD	F	0000	3
125	MEMBER	11	13	RD	F	0000	3
126	MEMBER	13	15	RD	F	0000	3
127	MEMBER	15	11	RD	F	0000	3
128	MEMBER	22	23	RD	F	0000	3
129	MEMBER	23	24	RD	F	0000	3
130	MEMBER	24	25	RD	F	0000	3
131	MEMBER	25	26	RD	F	0000	3
132	MEMBER	26	27	RD	F	0000	3
133	MEMBER	27	28	RD	F	0000	3
134	MEMBER	28	29	RD	F	0000	3
135	MEMBER	29	27	RD	F	0000	3
136	MEMBER	27	23	RD	F	0000	3
137	MEMBER	34	35	RD	F	0000	3
138	MEMBER	35	36	RD	F	0000	3
139	MEMBER	36	37	RD	F	0000	3
140	MEMBER	37	38	RD	F	0000	3
141	MEMBER	38	39	RD	F	0000	3
142	MEMBER	39	30	RD	F	0000	3



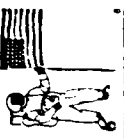
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SEAT PLAN - 2

LINE NO.	1	2	3	4	5	6	7	8
	0	0	0	0	0	0	0	0
	5	5	5	5	5	5	5	5
	0	0	0	0	0	0	0	0

193	MEMBER	61	71	STL					3600
194	MEMBER	56	59	STL					3600
195	MEMBER	59	64	STL					3600
196	MEMBER	64	72	STL					3600
197	MEMBER	57	60	STL					3600
198	MEMBER	60	70	STL					3600
199	MEMBER	70	67	STL					3600
200	MEMBER	67	76	STL					3600
201	MEMBER	76	75	STL					1275
202	MEMBER	54	59	RR5					1275
203	MEMBER	59	60	RR5					1275
204	MEMBER	60	58	RR5					1275
205	MEMBER	50	61	RR5					1275
206	MEMBER	60	64	RR5					1275
207	MEMBER	58	67	RR5					6,625
208	MEMBER	70	68	RR7					6,625
209	MEMBER	76	77	RR4					1275
210	MEMBER	76	78	RR4					1275
211	MEMBER	61	62	W1A					0000
212	MEMBER	62	63	W1A					0000
213	MEMBER	63	64	W1A					0000
214	MEMBER	63	64	W1A					0000
215	MEMBER	64	65	W1A					0000
216	MEMBER	65	67	W1A					0000
217	MEMBER	67	69	W1A					0000
218	MEMBER	69	61	W1B					0000
219	MEMBER	63	65	W0A					0000
220	MEMBER	65	66	W0A					0000
221	MEMBER	66	67	W0A					0000
222	MEMBER	67	68	W0A					0000
223	MEMBER	68	69	W0A					0000
224	MEMBER	69	62	W0A					0000
225	MEMBER	71	73	W1A					0000
226	MEMBER	71	72	W1A					0000
227	MEMBER	72	78	W1A					0000
228	MEMBER	71	71	W1B					0000
229	MEMBER	71	77	W1A					0000
230	MEMBER	77	83	W1A					0000
231	MEMBER	72	82	W1A					0000
232	MEMBER	72	78	W1A					0000
233	MEMBER	78	84	W1A					0000
234	MEMBER	77	79	W1A					0000
235	MEMBER	77	75	W1A					0000
236	MEMBER	75	78	W1A					0000
237	MEMBER	78	80	W1A					0000
238	MEMBER	71	75	W0B					0000
239	MEMBER	72	75	W0B					0000

240	JOINT	1	2987	-1725	-600	111	PTING A
241	JOINT	2	-2987	-1725	-600	111	PTING R



LINE NO. 1 2 3 4 5 6 7 8

LINE NO.	1	2	3	4	5	6	7	8
243	JOINT	3	300	3400	-600			PTLNG C
244	JOINT	4	2910	-1684	0			MIDL TPF
245	JOINT	5	-2910	-1684	0			MIDL TPF
246	JOINT	6	0	3359	0			MIDL TPF
247	JOINT	7	2900	-1920	0			MIDL TPF
248	JOINT	8	-2900	-1920	0			MIDL TPF
249	JOINT	9	0	3599	0			MIDL TPF
250	JOINT	10	2900	-1674	0			MIDL TPF
251	JOINT	11	0	-1674	0			MIDL TPF
252	JOINT	12	-29	-1674	0			MIDL TPF
253	JOINT	13	-1450	R37	0			MIDL TPF
254	JOINT	14	0	3509	0			MIDL TPF
255	JOINT	15	1450	R37	0			MIDL TPF
256	JOINT	16	2047	-1417	3200			1 LEVEL
257	JOINT	17	-2047	-1417	3200			1 LEVEL
258	JOINT	18	0	2825	3200			1 LEVEL
259	JOINT	19	2438	-1657	3200			1 LEVEL
260	JOINT	20	-2438	-1657	3200			1 LEVEL
261	JOINT	21	0	3065	3200			1 LEVEL
262	JOINT	22	2438	-1407	3200			1 LEVEL
263	JOINT	23	0	-1407	3200			1 LEVEL
264	JOINT	24	-2438	-1407	3200			1 LEVEL
265	JOINT	25	-1219	700	3200			1 LEVEL
266	JOINT	26	0	2615	3200			1 LEVEL
267	JOINT	27	1219	700	3200			1 LEVEL
268	JOINT	28	1987	-1151	6400			2 LEVEL
269	JOINT	29	-1987	-1151	6400			2 LEVEL
270	JOINT	30	0	3437	6400			2 LEVEL
271	JOINT	31	1977	-1391	6400			2 LEVEL
272	JOINT	32	-1977	-1391	6400			2 LEVEL
273	JOINT	33	0	3677	6400			2 LEVEL
274	JOINT	34	1977	-1101	6400			2 LEVEL
275	JOINT	35	0	-1101	6400			2 LEVEL
276	JOINT	36	-1977	-1101	6400			2 LEVEL
277	JOINT	37	-988	571	6400			2 LEVEL
278	JOINT	38	0	3427	6400			2 LEVEL
279	JOINT	39	988	571	6400			2 LEVEL
280	JOINT	40	1774	-1040	7800			BOAT LDG
281	JOINT	41	-1774	-1040	7800			BOAT LDG
282	JOINT	42	0	2880	7800			3 LEVEL
283	JOINT	43	1525	-885	9600			3 LEVEL
284	JOINT	44	-1525	-885	9600			3 LEVEL
285	JOINT	45	0	1759	9600			3 LEVEL
286	JOINT	46	1515	-1125	9600			3 LEVEL
287	JOINT	47	-1515	-1125	9600			3 LEVEL
288	JOINT	48	0	1999	9600			3 LEVEL
289	JOINT	49	1515	-875	9600			3 LEVEL
290	JOINT	50	0	-875	9600			3 LEVEL
291	JOINT	51	-1515	-875	9600			3 LEVEL
292	JOINT	52	-757	437	9600			3 LEVEL



PAGE

SEALING

LINE NO. 1 2 3 4 5 6 7 8

293	JOINT	53	0	1749	9600	3 LEVEL
294	JOINT	54	757	437	9600	3 LEVEL
295	JOINT	55	1450	-837	10050	AP LEVEL
296	JOINT	56	-1450	-837	10050	WP LEVEL
297	JOINT	57	0	1674	10050	WP LEVEL
298	JOINT	58	1450	-837	12900	ST BRACE
299	JOINT	59	-1450	-837	12900	ST BRACE
300	JOINT	60	0	1674	12900	ST BRACE
301	JOINT	61	1450	-837	14400	FOT DECK
302	JOINT	62	1000	-837	14400	FOT DECK
303	JOINT	63	-1000	-837	14400	FOT DECK
304	JOINT	64	-1450	-837	14400	FOT DECK
305	JOINT	65	-1000	-837	14400	FOT DECK
306	JOINT	66	-1000	1674	14400	FOT DECK
307	JOINT	67	0	1674	14400	FOT DECK
308	JOINT	68	1000	1674	14400	FOT DECK
309	JOINT	69	1000	-837	14400	FOT DECK
310	JOINT	70	0	1674	13500	BRACE PT
311	JOINT	71	1450	-837	15900	TOP DECK
312	JOINT	72	-1450	-837	15900	TOP DECK
313	JOINT	73	1750	-837	15900	TOP DECK
314	JOINT	74	-1750	-837	15900	TOP DECK
315	JOINT	75	0	1674	15900	TOP DECK
316	JOINT	76	0	1674	14800	BRACE PT
317	JOINT	77	1450	1674	15900	TOP DECK
318	JOINT	78	-1450	1674	15900	TOP DECK
319	JOINT	79	1750	1674	15900	TOP DECK
320	JOINT	80	-1750	1674	15900	TOP DECK
321	JOINT	81	1450	-1337	15900	TOP DECK
322	JOINT	82	-1450	-1337	15900	TOP DECK
323	JOINT	83	1450	2174	15900	TOP DECK
324	JOINT	84	-1450	2174	15900	TOP DECK
325	END					



6-PHASE ACR STRUCTURE -- U.S. NAVY (16-IN. DIAMETER PILING) -- C.CHFRM

INPUT UNITS

....ENGLISH

OUTPUT UNITS

....ENGLISH



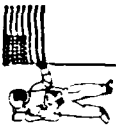
*** WAVE POSITION SUMMARY REPORT ***

WAVE ANGLE = 90.00

LOAD CONDITION 1

TRIAL NO.	DIST. TO CREST FT	PHASE ANGLE DEG	SHEAR KIPS		MOMENT FT-KIPS		RESULT		VERTICAL FORCE KIPS
			X	Y	X	Y	X	Y	
1	-20.0	10.89	1.9	728.9	-60287.	155.	60287.	7.4	
2	-15.0	8.17	-1.9	751.8	-63523.	-164.	63523.	2.5	
3	-10.0	5.45	-2.8	759.7	-64911.	-288.	64912.	4.0	
4	-5.0	2.72	-2.7	757.5	-65027.	-273.	65028.	4.4	
5	0.0	-0.00	-2.2	751.6	-64799.	-193.	64800.	4.2	
6	5.0	-2.72	-1.6	729.0	-62502.	-102.	62502.	3.8	
7	10.0	-5.45	-1.0	709.7	-60429.	-14.	60429.	3.7	





*** I D A D S U M M A R Y R E P O R T ***

WAVE NUMBER = 1

WAVE DIRECTION = 90.000

X SHEAR FORCE = -2.7309 KIPS

Y SHEAR FORCE = 757.4846 KIPS

RESULTANT SHEAR FORCE = 757.4895 KIPS

X MIDLINE MOMENT = -65027.4029 FT-KIPS

Y MIDLINE MOMENT = -273.2350 FT-KIPS

RESULTANT MIDLINE MOMENT = 65028.0670 FT-KIPS

Z VERTICAL FORCE = 4.3589 KIPS

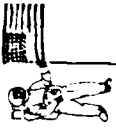


***** WAVE POSITION SUMMARY REPORT *****

LOAD CONDITION 2

WAVE ANGLE = 270.00

TRIAL NO.	DIST. FT	PHASE ANGLE	S H F A R		M U L T I P L I C A T I O N		M O M E N T S		V E R T I C A L F O R C E	
			X	Y	X	Y	X	Y	X	Y
1	-20.0	10.89	-733.7	733.7	60886.	79.	60886.	-1.1		
2	-15.0	8.17	-708.9	708.9	62924.	-120.	62924.	-.4		
3	-10.0	5.45	-761.3	761.3	64825.	-52.	64825.	-.4		
4	-5.0	2.72	-757.1	757.1	64668.	37.	64668.	-.7		
5	0.0	-0.00	-757.1	757.1	65243.	126.	65243.	-.9		
6	5.0	-2.72	-739.4	739.4	63568.	194.	63568.	-.9		
7	10.0	-5.45	-717.2	717.2	61498.	193.	61498.	-.4		



*** I T A D S U M M A R Y R E P O R T ***

WAVE NUMBER = 2

WAVE DIRECTION = 270.000

X SHEAR FORCE = 1.4179 KIPS

Y SHEAR FORCE = -757.1200 KIPS

RESULTANT SHEAR FORCE = 757.1213 KIPS

X MUDDLINE MOMENT = 65243.4242 FT-KIPS

Y MUDDLINE MOMENT = 126.2453 FT-KIPS

RESULTANT MUDDLINE MOMENT = 65243.5463 FT-KIPS

Z VERTICAL FORCE = -.9087 KIPS

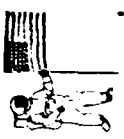
**** DEAD LOAD REPORT ****

LOAD CONDITION 1

MEAN WATER DEPTH = 123.500 FT

STRUCTURE DEAD LOAD =

035.8654 KIPS

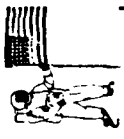


SFAI/040-2
DEVELOPED BY SYSTEMS TECHNOLOGY, INC.
HOUSTON, TEXAS
RELEASE 2 AND 11
MARCH 1976

LINE NO. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42

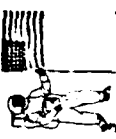
Table with columns for line numbers, descriptions (e.g., SECT, GRUP, MEMBER), and various alphanumeric codes and numbers.

F 0000 1
F 0000 1
F 0000 1
F 0000 1
F 0000 2
F 0000 2



SFALPAI-2

LINE NO.	1	2	3	4	5	6	7	8
43	MEMBER	17	29	P20				F 0000 2
44	MEMBER	20	40	P20				F 0000 2
45	MEMBER	44	56	P20				F 0000 2
46	MEMBER	3	6	P10				F 0000 3
47	MEMBER	6	18	P10				F 0000 3
48	MEMBER	18	30	P20				F 0000 3
49	MEMBER	30	45	P20				F 0000 3
50	MEMBER	45	57	P20				F 0000 3
51	MEMBER	10	22	J11				F 4000
52	MEMBER	22	34	J11				F 4000
53	MEMBER	34	40	J12				F 4100
54	MEMBER	40	49	J12				F 4100
55	MEMBER	49	55	J12				F 4000
56	MEMBER	12	24	J11				F 4000
57	MEMBER	24	36	J11				F 4100
58	MEMBER	36	41	J12				F 4100
59	MEMBER	41	51	J12				F 4100
60	MEMBER	51	56	J12				F 4100
61	MEMBER	14	26	J11				F 4000
62	MEMBER	26	38	J11				F 4000
63	MEMBER	38	42	J12				F 4100
64	MEMBER	42	53	J12				F 4100
65	MEMBER	53	57	J12				F 4100
66	MEMBER	10	11	HR2				1800
67	MEMBER	11	12	HR2				1800
68	MEMBER	12	13	HR2				1800
69	MEMBER	13	14	HR2				1800
70	MEMBER	14	15	HR2				1800
71	MEMBER	15	10	HR2				1800
72	MEMBER	11	13	HR4				1400
73	MEMBER	13	15	HR4				1400
74	MEMBER	15	11	HR4				1400
75	MEMBER	22	23	HR2				1800
76	MEMBER	23	24	HR2				1800
77	MEMBER	24	25	HR2				1800
78	MEMBER	25	26	HR2				1800
79	MEMBER	26	27	HR2				1800
80	MEMBER	27	27	HR2				1800
81	MEMBER	23	25	HR4				1400
82	MEMBER	25	27	HR4				1400
83	MEMBER	27	23	HR4				1400
84	MEMBER	34	35	HR5				1275
85	MEMBER	35	36	HR5				1275
86	MEMBER	36	37	HR5				1275
87	MEMBER	37	38	HR5				1275
88	MEMBER	38	39	HR5				1275
89	MEMBER	39	39	HR5				1275
90	MEMBER	35	37	HR6				1275
91	MEMBER	37	39	HR6				1275
92	MEMBER	39	35	HR6				1275



PAGE

SFAL1410-2

LINE NO.	1	2	3	4	5	6	7	8
93	MEMBER	49	50	ARR				1600
94	MEMBER	50	51	ARR				1600
95	MEMBER	51	52	ARR				1600
96	MEMBER	52	53	ARR				1600
97	MEMBER	53	54	ARR				1600
98	MEMBER	54	49	ARR				1600
99	MEMBER	50	52	ARR				1275
100	MEMBER	52	54	ARR				1275
101	MEMBER	54	50	ARR				1600
102	MEMBER	11	22	ARR				1600
103	MEMBER	11	24	ARR				1600
104	MEMBER	13	24	ARR				1600
105	MEMBER	13	26	ARR				1600
106	MEMBER	15	26	ARR				1600
107	MEMBER	15	22	ARR				2000
108	MEMBER	22	36	ARR				2000
109	MEMBER	24	34	ARR				2000
110	MEMBER	24	34	ARR				2000
111	MEMBER	34	49	ARR				2000
112	MEMBER	38	51	BRI				2000
113	MEMBER	34	53	ARR				2000
114	MEMBER	4	7	MAN	1111			F 0000
115	MEMBER	7	10	MAN				F 0000
116	MEMBER	5	8	MAN	1111			F 0000
117	MEMBER	4	12	MAN				F 0000
118	MEMBER	6	9	MAN	1111			F 0000
119	MEMBER	9	14	MAN				F 0000
120	MEMBER	16	19	MAN	1111			F 0000
121	MEMBER	19	22	MAN				F 0000
122	MEMBER	17	20	MAN	1111			F 0000
123	MEMBER	20	24	MAN				F 0000
124	MEMBER	18	21	MAN	1111			F 0000
125	MEMBER	21	26	MAN				F 0000
126	MEMBER	28	31	MAN	1111			F 0000
127	MEMBER	31	34	MAN				F 0000
128	MEMBER	29	32	MAN	1111			F 0000
129	MEMBER	32	36	MAN				F 0000
130	MEMBER	30	33	MAN	1111			F 0000
131	MEMBER	33	38	MAN				F 0000
132	MEMBER	43	46	MAN	1111			F 0000
133	MEMBER	44	49	MAN				F 0000
134	MEMBER	44	47	MAN	1111			F 0000
135	MEMBER	47	51	MAN				F 0000
136	MEMBER	45	48	MAN	1111			F 0000
137	MEMBER	44	53	MAN				F 3600
138	MEMBER	55	58	STL				3400
139	MEMBER	58	61	STL				3400
140	MEMBER	61	71	STL				3400
141	MEMBER	54	59	STL				3400
142	MEMBER	59	64	STL				3400



PAGE

SPALMAN-2

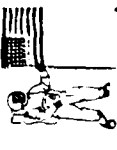
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	5	0	5	0	5	0	5	0
	0	5	0	5	0	5	0	5
	0	5	0	5	0	5	0	5

143	MEMBER	64	72	STL					3600
144	MEMBER	57	60	STL					3600
145	MEMBER	60	70	STL					3600
146	MEMBER	70	67	STL					3600
147	MEMBER	67	74	STL					3600
148	MEMBER	74	75	STL					1275
149	MEMBER	54	59	RRS					1275
150	MEMBER	59	60	RRS					1275
151	MEMBER	60	54	RRS					1275
152	MEMBER	59	61	RRS					1275
153	MEMBER	60	64	RRS					1275
154	MEMBER	54	67	RRS					1275
155	MEMBER	70	66	RR7					6,625
156	MEMBER	70	64	RR7					6,625
157	MEMBER	76	77	RR6					1275
158	MEMBER	74	74	RR6					1275
159	MEMBER	61	62	W1A					0000
160	MEMBER	62	63	W1A					0000
161	MEMBER	63	64	W1A					0000
162	MEMBER	64	65	W1A					0000
163	MEMBER	65	67	W1A					0000
164	MEMBER	67	69	W1A					0000
165	MEMBER	69	61	W1A					0000
166	MEMBER	63	65	W0A					0000
167	MEMBER	65	64	W0A					0000
168	MEMBER	64	67	W0A					0000
169	MEMBER	67	68	W0A					0000
170	MEMBER	68	69	W0A					0000
171	MEMBER	60	62	W0A					0000
172	MEMBER	71	73	W1A					0000
173	MEMBER	71	72	W1A					0000
174	MEMBER	72	70	W1A					0000
175	MEMBER	71	81	W1A					0000
176	MEMBER	71	77	W1A					0000
177	MEMBER	77	83	W1A					0000
178	MEMBER	72	82	W1A					0000
179	MEMBER	72	74	W1A					0000
180	MEMBER	74	80	W1A					0000
181	MEMBER	77	79	W1A					0000
182	MEMBER	77	75	W1A					0000
183	MEMBER	75	78	W1A					0000
184	MEMBER	74	80	W1A					0000
185	MEMBER	71	75	W06					0000
186	MEMBER	72	75	W06					0000
187	JOINT								
188	JOINT	1	2987	-1725	-600			PTING A	
189	JOINT	2	2987	-1725	-600			PTING B	
190	JOINT	3	000	3449	-600			PTING C	
191	JOINT	4	2910	-1684	0			MIDLINF	
192	JOINT	5	2910	-1684	0			MIDLINF	



LINE NO. 1 2 3 4 5 6 7 8

193	JOINT	6	0	3350	0	MUDLINE
194	JOINT	7	2900	-1924	0	MUDLINE
195	JOINT	8	-2000	-1924	0	MUDLINE
196	JOINT	9	0	3599	0	MUDLINE
197	JOINT	10	2900	-1674	0	MUDLINE
198	JOINT	11	0	-1674	0	MUDLINE
199	JOINT	12	-20	-1674	0	MUDLINE
200	JOINT	13	-1450	R37	0	MUDLINE
201	JOINT	14	0	3549	0	MUDLINE
202	JOINT	15	1450	R37	0	MUDLINE
203	JOINT	16	2047	-1417	3200	1 LEVEL
204	JOINT	17	-2047	-1417	3200	1 LEVEL
205	JOINT	18	0	2825	3200	1 LEVEL
206	JOINT	19	2438	-1657	3200	1 LEVEL
207	JOINT	20	-2438	-1657	3200	1 LEVEL
208	JOINT	21	0	3065	3200	1 LEVEL
209	JOINT	22	2438	-1407	3200	1 LEVEL
210	JOINT	23	0	-1407	3200	1 LEVEL
211	JOINT	24	-2438	-1407	3200	1 LEVEL
212	JOINT	25	-1219	704	3200	1 LEVEL
213	JOINT	26	0	2815	3200	1 LEVEL
214	JOINT	27	1219	704	3200	1 LEVEL
215	JOINT	28	1987	-1151	6400	2 LEVEL
216	JOINT	29	-1987	-1151	6400	2 LEVEL
217	JOINT	30	0	3437	6400	2 LEVEL
218	JOINT	31	1977	-1391	6400	2 LEVEL
219	JOINT	32	-1977	-1391	6400	2 LEVEL
220	JOINT	33	0	3677	6400	2 LEVEL
221	JOINT	34	1977	-1141	6400	2 LEVEL
222	JOINT	35	0	-1141	6400	2 LEVEL
223	JOINT	36	-1977	-1141	6400	2 LEVEL
224	JOINT	37	-988	571	6400	2 LEVEL
225	JOINT	38	0	3427	6400	2 LEVEL
226	JOINT	39	968	571	6400	2 LEVEL
227	JOINT	40	1774	-1040	7800	MUD LOG
228	JOINT	41	-1774	-1040	7800	MUD LOG
229	JOINT	42	0	2880	7800	3 LEVEL
230	JOINT	43	1525	-885	9600	3 LEVEL
231	JOINT	44	-1525	-885	9600	3 LEVEL
232	JOINT	45	0	1759	9600	3 LEVEL
233	JOINT	46	1515	-1125	9600	3 LEVEL
234	JOINT	47	-1515	-1125	9600	3 LEVEL
235	JOINT	48	0	1949	9600	3 LEVEL
236	JOINT	49	1515	-875	9600	3 LEVEL
237	JOINT	50	0	-875	9600	3 LEVEL
238	JOINT	51	-1515	-875	9600	3 LEVEL
239	JOINT	52	-757	437	9600	3 LEVEL
240	JOINT	53	0	1749	9600	3 LEVEL
241	JOINT	54	757	437	9600	3 LEVEL
242	JOINT	55	1450	-837	10050	MP LEVEL



SFALDAD-2

LINE NO. 1..... 2..... 3..... 4..... 5..... 6..... 7..... 8

245	JOINT	59	-1450	-837	10050	WP LEVEL
246	JOINT	57	0	1674	10050	WP LEVEL
245	JOINT	58	1450	-837	12900	ST HRACE
246	JOINT	59	-1450	-837	12900	ST HRACE
247	JOINT	60	0	1674	12900	FOT DECK
248	JOINT	61	1450	-837	14400	FOT DECK
249	JOINT	62	1000	-837	14400	FOT DECK
250	JOINT	63	-1000	-837	14400	FOT DECK
251	JOINT	64	-1450	-837	14400	FOT DECK
252	JOINT	65	-1000	-887	14400	FOT DECK
253	JOINT	66	-1000	1674	14400	FOT DECK
254	JOINT	67	0	1674	14400	FOT DECK
255	JOINT	68	1000	1674	14400	FOT DECK
256	JOINT	69	1000	-887	14400	HRACE PT
257	JOINT	70	0	1674	13500	TOP DECK
258	JOINT	71	1450	-837	15900	TOP DECK
259	JOINT	72	-1450	-837	15900	TOP DECK
260	JOINT	73	1750	-837	15900	TOP DECK
261	JOINT	74	-1750	-837	15900	TOP DECK
262	JOINT	75	0	1674	15900	HRACE PT
263	JOINT	76	0	1674	14800	TOP DECK
264	JOINT	77	1450	1674	15900	TOP DECK
265	JOINT	78	-1450	1674	15900	TOP DECK
266	JOINT	79	1750	1674	15900	TOP DECK
267	JOINT	80	-1750	1674	15900	TOP DECK
268	JOINT	81	1450	-1337	15900	TOP DECK
269	JOINT	82	-1450	-1337	15900	TOP DECK
270	JOINT	83	1450	2174	15900	TOP DECK
271	JOINT	84	-1450	2174	15900	TOP DECK
272	LOAD					
273	LOADCN	1				
274	LOAD X	43	55	4.08	345	GLOR CONC
275	LOAD Y	43	55			GLOR MOMT
276	LOAD X	44	56	4.08	345	GLOR CONC
277	LOAD Y	44	56			GLOR MOMT
278	LOAD X	45	57	4.07	345	GLOR CONC
279	LOAD Y	45	57			GLOR MOMT
280	LOAD X	43	55	4.08	1111	GLOR CONC
281	LOAD Y	43	55			GLOR MOMT
282	LOAD X	44	56	4.08	1111	GLOR CONC
283	LOAD Y	44	56			GLOR MOMT
284	LOAD X	45	57	4.07	1111	GLOR CONC
285	LOAD Y	45	57			GLOR MOMT
286	LOAD X	10	22	0.00	1	GLOR UNTE
287	LOAD Y	10	22	0.00	48	GLOR UNTE
288	LOAD Z	10	22	0.00	04	GLOR UNTE
289	LOAD X	10	22	10.81	1	GLOR UNTE
290	LOAD Y	10	22	10.81	48	GLOR UNTE
291	LOAD Z	10	22	10.81	04	GLOR UNTE
292	LOAD X	10	22	21.63	1	GLOR UNTE



SFALOAD=2

LINE NO. 1 1 1 2 2 3 3 4 4 5 5 6 6 7 7 A

293	LOAD Y	10	22	21.63	50	10.41	53	GLOR UNITF	WV 0 1
294	LOAD Z	10	22	21.63	04	10.41	04	GLOR UNITF	WV 0 1
295	LOAD X	22	34	0.00	1	10.41	1	GLOR UNITF	WV 0 1
296	LOAD Y	22	34	0.00	53	10.41	57	GLOR UNITF	WV 0 1
297	LOAD Z	22	34	0.00	04	10.41	05	GLOR UNITF	WV 0 1
298	LOAD X	22	34	10.41	1	10.41	1	GLOR UNITF	WV 0 1
299	LOAD Y	22	34	10.41	57	10.41	60	GLOR UNITF	WV 0 1
300	LOAD Z	22	34	10.41	05	10.41	05	GLOR UNITF	WV 0 1
301	LOAD X	22	34	21.63	1	10.41	1	GLOR UNITF	WV 0 1
302	LOAD Y	22	34	21.63	64	10.41	71	GLOR UNITF	WV 0 1
303	LOAD Z	22	34	21.63	05	10.41	04	GLOR UNITF	WV 0 1
304	LOAD X	34	40	0.00	1	4.73	1	GLOR UNITF	WV 0 1
305	LOAD Y	34	40	0.00	73	4.73	77	GLOR UNITF	WV 0 1
306	LOAD Z	34	40	0.00	05	4.73	05	GLOR UNITF	WV 0 1
307	LOAD X	34	40	4.73	1	4.73	1	GLOR UNITF	WV 0 1
308	LOAD Y	34	40	4.73	77	4.73	82	GLOR UNITF	WV 0 1
309	LOAD Z	34	40	4.73	05	4.73	06	GLOR UNITF	WV 0 1
310	LOAD X	34	40	9.45	1	4.73	1	GLOR UNITF	WV 0 1
311	LOAD Y	34	40	9.45	82	4.73	88	GLOR UNITF	WV 0 1
312	LOAD Z	34	40	9.45	06	4.73	06	GLOR UNITF	WV 0 1
313	LOAD X	40	49	0.00	1	6.09	1	GLOR UNITF	WV 0 1
314	LOAD Y	40	49	0.00	88	6.09	90	GLOR UNITF	WV 0 1
315	LOAD Z	40	49	0.00	08	6.09	09	GLOR UNITF	WV 0 1
316	LOAD X	40	49	6.09	1	6.09	1	GLOR UNITF	WV 0 1
317	LOAD Y	40	49	6.09	96	6.09	106	GLOR UNITF	WV 0 1
318	LOAD Z	40	49	6.09	09	6.09	09	GLOR UNITF	WV 0 1
319	LOAD X	40	49	12.17	1	6.09	1	GLOR UNITF	WV 0 1
320	LOAD Y	40	49	12.17	106	6.09	118	GLOR UNITF	WV 0 1
321	LOAD Z	40	49	12.17	09	6.09	11	GLOR UNITF	WV 0 1
322	LOAD X	49	55	0.00	1	1.52	1	GLOR UNITF	WV 0 1
323	LOAD Y	49	55	0.00	118	1.52	121	GLOR UNITF	WV 0 1
324	LOAD Z	49	55	0.00	10	1.52	10	GLOR UNITF	WV 0 1
325	LOAD X	49	55	1.52	1	1.52	1	GLOR UNITF	WV 0 1
326	LOAD Y	49	55	1.52	121	1.52	125	GLOR UNITF	WV 0 1
327	LOAD Z	49	55	1.52	10	1.52	10	GLOR UNITF	WV 0 1
328	LOAD X	49	55	3.04	1	1.52	1	GLOR UNITF	WV 0 1
329	LOAD Y	49	55	3.04	125	1.52	124	GLOR UNITF	WV 0 1
330	LOAD Z	49	55	3.04	10	1.52	11	GLOR UNITF	WV 0 1
331	LOAD X	12	24	0.00	1	10.41	1	GLOR UNITF	WV 0 1
332	LOAD Y	12	24	0.00	47	10.41	48	GLOR UNITF	WV 0 1
333	LOAD Z	12	24	0.00	04	10.41	04	GLOR UNITF	WV 0 1
334	LOAD X	12	24	10.41	1	10.41	1	GLOR UNITF	WV 0 1
335	LOAD Y	12	24	10.41	48	10.41	50	GLOR UNITF	WV 0 1
336	LOAD Z	12	24	10.41	04	10.41	04	GLOR UNITF	WV 0 1
337	LOAD X	12	24	21.63	1	10.41	1	GLOR UNITF	WV 0 1
338	LOAD Y	12	24	21.63	50	10.41	53	GLOR UNITF	WV 0 1
339	LOAD Z	12	24	21.63	04	10.41	04	GLOR UNITF	WV 0 1
340	LOAD X	24	36	0.00	1	10.41	1	GLOR UNITF	WV 0 1
341	LOAD Y	24	36	0.00	53	10.41	57	GLOR UNITF	WV 0 1
342	LOAD Z	24	36	0.00	04	10.41	05	GLOR UNITF	WV 0 1



REAR UNIT-2

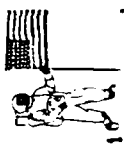
LINE NO.	1	2	3	4	5	6	7	8
343	LOAD X	24	36	10.41	1	GLOR	UNTE	01
344	LOAD Y	24	36	10.41	60	GLOR	UNTE	01
345	LOAD Z	24	36	10.41	05	GLOR	UNTE	01
346	LOAD X	24	36	21.63	1	GLOR	UNTE	01
347	LOAD Y	24	36	21.63	64	GLOR	UNTE	01
348	LOAD Z	24	36	21.63	05	GLOR	UNTE	01
349	LOAD X	36	41	0.00	1	GLOR	UNTE	01
350	LOAD Y	36	41	0.00	73	GLOR	UNTE	01
351	LOAD Z	36	41	0.00	05	GLOR	UNTE	01
352	LOAD X	36	41	4.73	1	GLOR	UNTE	01
353	LOAD Y	36	41	4.73	77	GLOR	UNTE	01
354	LOAD Z	36	41	4.73	06	GLOR	UNTE	01
355	LOAD X	36	41	9.45	1	GLOR	UNTE	01
356	LOAD Y	36	41	9.45	82	GLOR	UNTE	01
357	LOAD Z	36	41	9.45	06	GLOR	UNTE	01
358	LOAD X	41	51	0.00	1	GLOR	UNTE	01
359	LOAD Y	41	51	0.00	88	GLOR	UNTE	01
360	LOAD Z	41	51	0.00	09	GLOR	UNTE	01
361	LOAD X	41	51	6.09	1	GLOR	UNTE	01
362	LOAD Y	41	51	6.09	104	GLOR	UNTE	01
363	LOAD Z	41	51	6.09	09	GLOR	UNTE	01
364	LOAD X	41	51	12.17	1	GLOR	UNTE	01
365	LOAD Y	41	51	12.17	104	GLOR	UNTE	01
366	LOAD Z	41	51	12.17	09	GLOR	UNTE	01
367	LOAD X	51	56	0.00	1	GLOR	UNTE	01
368	LOAD Y	51	56	0.00	118	GLOR	UNTE	01
369	LOAD Z	51	56	0.00	10	GLOR	UNTE	01
370	LOAD X	51	56	1.52	1	GLOR	UNTE	01
371	LOAD Y	51	56	1.52	121	GLOR	UNTE	01
372	LOAD Z	51	56	1.52	10	GLOR	UNTE	01
373	LOAD X	51	56	3.04	1	GLOR	UNTE	01
374	LOAD Y	51	56	3.04	125	GLOR	UNTE	01
375	LOAD Z	51	56	3.04	11	GLOR	UNTE	01
376	LOAD X	14	26	0.00	50	GLOR	UNTE	01
377	LOAD Y	14	26	0.00	08	GLOR	UNTE	01
378	LOAD Z	14	26	10.41	51	GLOR	UNTE	01
379	LOAD X	14	26	10.41	08	GLOR	UNTE	01
380	LOAD Y	14	26	21.63	53	GLOR	UNTE	01
381	LOAD Z	14	26	21.63	09	GLOR	UNTE	01
382	LOAD X	26	38	0.00	55	GLOR	UNTE	01
383	LOAD Y	26	38	0.00	11	GLOR	UNTE	01
384	LOAD Z	26	38	10.46	59	GLOR	UNTE	01
385	LOAD X	26	38	10.46	11	GLOR	UNTE	01
386	LOAD Y	26	38	21.72	60	GLOR	UNTE	01
387	LOAD Z	26	38	21.72	12	GLOR	UNTE	01
388	LOAD X	38	42	0.00	65	GLOR	UNTE	01
389	LOAD Y	38	42	0.00	25	GLOR	UNTE	01
390	LOAD Z	38	42	5.01	69	GLOR	UNTE	01
391	LOAD X	38	42	5.01	27	GLOR	UNTE	01
392	LOAD Y	38	42	10.02	73	GLOR	UNTE	01



SEALING-2

LINE NO. 1 2 3 4 5 6 7 8

393	LOAD Z	34	42	10.02	29	5.01	51	GLOR UNTE	VV 0 1
394	LOAD Y	42	53	0.00	65	7.09	71	GLOR UNTE	VV 0 1
395	LOAD Z	42	53	0.00	41	7.09	45	GLOR UNTE	VV 0 1
396	LOAD Y	42	53	7.09	71	7.09	79	GLOR UNTE	VV 0 1
397	LOAD Z	42	53	7.09	45	7.09	49	GLOR UNTE	VV 0 1
398	LOAD Y	42	53	14.17	79	7.09	84	GLOR UNTE	VV 0 1
399	LOAD Z	42	53	14.17	49	7.09	55	GLOR UNTE	VV 0 1
400	LOAD Y	53	57	0.00	120	1.52	123	GLOR UNTE	VV 0 1
401	LOAD Z	53	57	0.00	20	1.52	26	GLOR UNTE	VV 0 1
402	LOAD Y	53	57	1.52	123	1.52	124	GLOR UNTE	VV 0 1
403	LOAD Z	53	57	1.52	20	1.52	21	GLOR UNTE	VV 0 1
404	LOAD Y	53	57	3.04	126	1.52	129	GLOR UNTE	VV 0 1
405	LOAD Z	53	57	3.04	21	1.52	21	GLOR UNTE	VV 0 1
406	LOAD Y	10	11	0.00	21	9.67	21	GLOR UNTE	VV 0 1
407	LOAD X	10	11	9.67	21	9.67	21	GLOR UNTE	VV 0 1
408	LOAD Y	10	11	19.33	21	9.67	21	GLOR UNTE	VV 0 1
409	LOAD Z	11	12	0.00	21	9.67	21	GLOR UNTE	VV 0 1
410	LOAD Y	11	12	9.67	21	9.67	21	GLOR UNTE	VV 0 1
411	LOAD X	11	12	19.33	21	9.67	21	GLOR UNTE	VV 0 1
412	LOAD Z	12	13	0.00	09	9.67	09	GLOR UNTE	VV 0 1
413	LOAD Y	12	13	0.00	05	9.67	05	GLOR UNTE	VV 0 1
414	LOAD X	12	13	9.67	09	9.67	16	GLOR UNTE	VV 0 1
415	LOAD Y	12	13	9.67	05	9.67	06	GLOR UNTE	VV 0 1
416	LOAD X	12	13	19.33	10	9.67	10	GLOR UNTE	VV 0 1
417	LOAD Y	12	13	19.33	06	9.67	06	GLOR UNTE	VV 0 1
418	LOAD X	13	14	0.00	10	9.67	10	GLOR UNTE	VV 0 1
419	LOAD Y	13	14	0.00	06	9.67	06	GLOR UNTE	VV 0 1
420	LOAD X	13	14	9.67	10	9.67	10	GLOR UNTE	VV 0 1
421	LOAD Y	13	14	9.67	06	9.67	06	GLOR UNTE	VV 0 1
422	LOAD X	13	14	19.34	10	9.67	10	GLOR UNTE	VV 0 1
423	LOAD Y	13	14	19.34	06	9.67	06	GLOR UNTE	VV 0 1
424	LOAD X	14	15	0.00	10	9.67	10	GLOR UNTE	VV 0 1
425	LOAD Y	14	15	0.00	06	9.67	06	GLOR UNTE	VV 0 1
426	LOAD X	14	15	9.67	10	9.67	10	GLOR UNTE	VV 0 1
427	LOAD Y	14	15	9.67	06	9.67	06	GLOR UNTE	VV 0 1
428	LOAD X	14	15	19.34	10	9.67	10	GLOR UNTE	VV 0 1
429	LOAD Y	14	15	19.34	06	9.67	06	GLOR UNTE	VV 0 1
430	LOAD X	15	16	0.00	10	9.67	10	GLOR UNTE	VV 0 1
431	LOAD Y	15	16	0.00	06	9.67	06	GLOR UNTE	VV 0 1
432	LOAD X	15	16	9.67	10	9.67	10	GLOR UNTE	VV 0 1
433	LOAD Y	15	16	9.67	06	9.67	06	GLOR UNTE	VV 0 1
434	LOAD X	15	16	19.33	09	9.67	09	GLOR UNTE	VV 0 1
435	LOAD Y	15	16	19.33	05	9.67	05	GLOR UNTE	VV 0 1
436	LOAD X	15	16	0.00	07	9.67	07	GLOR UNTE	VV 0 1
437	LOAD Y	15	16	0.00	04	9.67	04	GLOR UNTE	VV 0 1
438	LOAD X	15	16	9.67	07	9.67	07	GLOR UNTE	VV 0 1
439	LOAD Y	15	16	9.67	04	9.67	04	GLOR UNTE	VV 0 1
440	LOAD X	15	16	19.33	04	9.67	04	GLOR UNTE	VV 0 1
441	LOAD Y	15	16	19.33	04	9.67	04	GLOR UNTE	VV 0 1
442	LOAD X	15	16	0.00	14	9.67	14	GLOR UNTE	VV 0 1



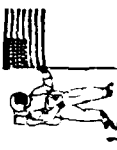
SEATTLE-2

LINE NO.	1	2	3	4	5	6	7	8
443	LOAD Y	13	15	9.67	1A	9.67	1P	GLOR UNTF
444	LOAD Y	13	15	9.67	1A	9.67	1A	GLOR UNTF
445	LOAD X	15	11	0.00	0A	9.67	0P	GLOR UNTF
446	LOAD Y	15	11	0.00	0A	9.67	0A	GLOR UNTF
447	LOAD Y	15	11	9.67	0A	9.67	07	GLOR UNTF
448	LOAD Y	15	11	9.67	0A	9.67	0A	GLOR UNTF
449	LOAD X	15	11	19.33	07	9.67	07	GLOR UNTF
450	LOAD Y	15	11	19.33	0A	9.67	0A	GLOR UNTF
451	LOAD Y	22	23	0.00	2A	8.13	2A	GLOR UNTF
452	LOAD Y	22	23	8.13	2A	8.13	2A	GLOR UNTF
453	LOAD Y	22	23	16.25	2A	8.13	2A	GLOR UNTF
454	LOAD Y	23	24	0.00	2A	8.13	2A	GLOR UNTF
455	LOAD Y	23	24	8.13	2A	8.13	2A	GLOR UNTF
456	LOAD Y	23	24	16.25	2A	8.13	2A	GLOR UNTF
457	LOAD X	24	25	0.00	10	8.13	11	GLOR UNTF
458	LOAD Y	24	25	0.00	0A	8.13	0A	GLOR UNTF
459	LOAD X	24	25	8.13	11	8.13	11	GLOR UNTF
460	LOAD Y	24	25	8.13	0A	8.13	0A	GLOR UNTF
461	LOAD X	24	25	16.25	11	8.13	11	GLOR UNTF
462	LOAD X	25	26	16.25	0A	8.13	0A	GLOR UNTF
463	LOAD X	25	26	0.00	11	8.13	11	GLOR UNTF
464	LOAD Y	25	26	0.00	0A	8.13	0A	GLOR UNTF
465	LOAD X	25	26	8.13	11	8.13	11	GLOR UNTF
466	LOAD Y	25	26	8.13	0A	8.13	0A	GLOR UNTF
467	LOAD X	25	26	16.25	11	8.13	11	GLOR UNTF
468	LOAD Y	25	26	16.25	0A	8.13	0A	GLOR UNTF
469	LOAD X	26	27	0.00	11	8.13	11	GLOR UNTF
470	LOAD Y	26	27	0.00	0A	8.13	0A	GLOR UNTF
471	LOAD X	26	27	8.13	11	8.13	11	GLOR UNTF
472	LOAD Y	26	27	8.13	0A	8.13	0A	GLOR UNTF
473	LOAD X	26	27	16.25	11	8.13	11	GLOR UNTF
474	LOAD Y	26	27	16.25	0A	8.13	0A	GLOR UNTF
475	LOAD X	27	28	0.00	11	8.13	11	GLOR UNTF
476	LOAD Y	27	28	0.00	0A	8.13	0A	GLOR UNTF
477	LOAD X	27	28	8.13	11	8.13	11	GLOR UNTF
478	LOAD Y	27	28	8.13	0A	8.13	0A	GLOR UNTF
479	LOAD X	27	28	16.25	11	8.13	11	GLOR UNTF
480	LOAD Y	27	28	16.25	0A	8.13	0A	GLOR UNTF
481	LOAD X	28	29	0.00	0A	8.13	0A	GLOR UNTF
482	LOAD Y	28	29	0.00	05	8.13	05	GLOR UNTF
483	LOAD X	28	29	8.13	0A	8.13	0A	GLOR UNTF
484	LOAD Y	28	29	8.13	05	8.13	05	GLOR UNTF
485	LOAD X	28	29	16.25	09	8.13	09	GLOR UNTF
486	LOAD Y	28	29	16.25	05	8.13	05	GLOR UNTF
487	LOAD Y	25	27	0.00	20	8.13	20	GLOR UNTF
488	LOAD Y	25	27	8.13	20	8.13	20	GLOR UNTF
489	LOAD Y	25	27	16.25	20	8.13	20	GLOR UNTF
490	LOAD X	27	28	0.00	09	8.13	09	GLOR UNTF
491	LOAD Y	27	28	0.00	05	8.13	05	GLOR UNTF
492	LOAD X	27	28	8.13	09	8.13	09	GLOR UNTF



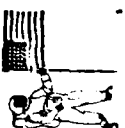
SEAL GAU-2

LINE NO.	1	2	3	4	5	6	7	8
493	LOAD Y	27 23	8.13	05	8.13	04	GLOR UNITE	WV 0 1
494	LOAD X	27 23	16.25	08	8.13	08	GLOR UNITE	WV 0 1
495	LOAD Y	27 23	16.25	05	8.13	05	GLOR UNITE	WV 0 1
496	LOAD Y	34 35	0.00	23	6.59	23	GLOR UNITE	WV 0 1
497	LOAD Y	34 35	6.59	23	6.59	23	GLOR UNITE	WV 0 1
498	LOAD Y	34 35	13.18	23	6.59	23	GLOR UNITE	WV 0 1
499	LOAD Y	35 36	0.00	23	6.59	23	GLOR UNITE	WV 0 1
500	LOAD Y	35 36	6.59	23	6.59	23	GLOR UNITE	WV 0 1
501	LOAD Y	35 36	13.18	23	6.59	23	GLOR UNITE	WV 0 1
502	LOAD X	36 37	0.00	10	6.59	10	GLOR UNITE	WV 0 1
503	LOAD Y	36 37	0.00	06	6.59	06	GLOR UNITE	WV 0 1
504	LOAD X	36 37	6.59	10	6.59	10	GLOR UNITE	WV 0 1
505	LOAD Y	36 37	13.18	10	6.59	10	GLOR UNITE	WV 0 1
506	LOAD X	36 37	13.18	06	6.59	06	GLOR UNITE	WV 0 1
507	LOAD Y	36 37	0.00	07	10.07	07	GLOR UNITE	WV 0 1
508	LOAD X	37 38	0.00	03	10.07	03	GLOR UNITE	WV 0 1
509	LOAD Y	37 38	0.00	07	10.07	07	GLOR UNITE	WV 0 1
510	LOAD X	37 38	10.07	07	10.07	07	GLOR UNITE	WV 0 1
511	LOAD Y	37 38	10.07	03	10.07	03	GLOR UNITE	WV 0 1
512	LOAD X	37 38	20.15	07	10.07	07	GLOR UNITE	WV 0 1
513	LOAD Y	37 38	20.15	03	10.07	03	GLOR UNITE	WV 0 1
514	LOAD X	38 39	0.00	07	10.07	07	GLOR UNITE	WV 0 1
515	LOAD Y	38 39	0.00	02	10.07	02	GLOR UNITE	WV 0 1
516	LOAD X	38 39	10.07	07	10.07	07	GLOR UNITE	WV 0 1
517	LOAD Y	38 39	10.07	03	10.07	03	GLOR UNITE	WV 0 1
518	LOAD X	38 39	20.15	07	10.07	07	GLOR UNITE	WV 0 1
519	LOAD Y	38 39	20.15	03	10.07	03	GLOR UNITE	WV 0 1
520	LOAD X	39 34	0.00	10	6.59	10	GLOR UNITE	WV 0 1
521	LOAD Y	39 34	0.00	06	6.59	06	GLOR UNITE	WV 0 1
522	LOAD X	39 34	6.59	10	6.59	10	GLOR UNITE	WV 0 1
523	LOAD Y	39 34	6.59	06	6.59	06	GLOR UNITE	WV 0 1
524	LOAD X	39 34	13.18	10	6.59	10	GLOR UNITE	WV 0 1
525	LOAD Y	39 34	13.18	06	6.59	06	GLOR UNITE	WV 0 1
526	LOAD X	35 37	0.00	10	6.59	10	GLOR UNITE	WV 0 1
527	LOAD Y	35 37	0.00	06	6.59	06	GLOR UNITE	WV 0 1
528	LOAD X	35 37	6.59	10	6.59	10	GLOR UNITE	WV 0 1
529	LOAD Y	35 37	6.59	06	6.59	06	GLOR UNITE	WV 0 1
530	LOAD X	35 37	13.18	10	6.59	10	GLOR UNITE	WV 0 1
531	LOAD Y	35 37	13.18	06	6.59	06	GLOR UNITE	WV 0 1
532	LOAD X	37 39	0.00	24	6.59	24	GLOR UNITE	WV 0 1
533	LOAD Y	37 39	6.59	24	6.59	24	GLOR UNITE	WV 0 1
534	LOAD X	37 39	13.17	24	6.59	24	GLOR UNITE	WV 0 1
535	LOAD Y	39 35	0.00	10	6.59	10	GLOR UNITE	WV 0 1
536	LOAD X	39 35	0.00	06	6.59	06	GLOR UNITE	WV 0 1
537	LOAD X	39 35	6.59	10	6.59	10	GLOR UNITE	WV 0 1
538	LOAD Y	39 35	6.59	06	6.59	06	GLOR UNITE	WV 0 1
539	LOAD X	39 35	13.18	10	6.59	10	GLOR UNITE	WV 0 1
540	LOAD Y	39 35	13.18	06	6.59	06	GLOR UNITE	WV 0 1
541	LOAD X	40 50	0.00	46	5.05	46	GLOR UNITE	WV 0 1
542	LOAD Y	40 50	5.05	46	5.05	46	GLOR UNITE	WV 0 1



SEAL 1111-2

LINE NO.	1	2	3	4	5	6	7	8
543	LOAD Y	49	50	10.10	46	5.05	GLOR UNTF	WV 0 1
544	LOAD Y	50	51	0.00	46	5.05	GLOR UNTF	WV 0 1
545	LOAD Y	50	51	5.05	46	5.05	GLOR UNTF	WV 0 1
546	LOAD Y	50	51	10.10	46	5.05	GLOR UNTF	WV 0 1
547	LOAD X	51	52	0.00	20	5.05	GLOR UNTF	WV 0 1
548	LOAD Y	51	52	0.00	12	5.05	GLOR UNTF	WV 0 1
549	LOAD X	51	52	5.05	21	5.05	GLOR UNTF	WV 0 1
550	LOAD Y	51	52	5.05	12	5.05	GLOR UNTF	WV 0 1
551	LOAD X	51	52	10.10	21	5.05	GLOR UNTF	WV 0 1
552	LOAD Y	51	52	10.10	12	5.05	GLOR UNTF	WV 0 1
553	LOAD X	52	53	0.00	21	5.05	GLOR UNTF	WV 0 1
554	LOAD Y	52	53	0.00	12	5.05	GLOR UNTF	WV 0 1
555	LOAD X	52	53	5.05	21	5.05	GLOR UNTF	WV 0 1
556	LOAD Y	52	53	5.05	12	5.05	GLOR UNTF	WV 0 1
557	LOAD X	52	53	10.10	21	5.05	GLOR UNTF	WV 0 1
558	LOAD Y	52	53	10.10	12	5.05	GLOR UNTF	WV 0 1
559	LOAD X	53	54	0.00	21	5.05	GLOR UNTF	WV 0 1
560	LOAD Y	53	54	0.00	12	5.05	GLOR UNTF	WV 0 1
561	LOAD X	53	54	5.05	21	5.05	GLOR UNTF	WV 0 1
562	LOAD Y	53	54	5.05	12	5.05	GLOR UNTF	WV 0 1
563	LOAD X	53	54	10.10	21	5.05	GLOR UNTF	WV 0 1
564	LOAD Y	53	54	10.10	12	5.05	GLOR UNTF	WV 0 1
565	LOAD X	54	49	0.00	21	5.05	GLOR UNTF	WV 0 1
566	LOAD Y	54	49	0.00	12	5.05	GLOR UNTF	WV 0 1
567	LOAD X	54	49	5.05	21	5.05	GLOR UNTF	WV 0 1
568	LOAD Y	54	49	5.05	12	5.05	GLOR UNTF	WV 0 1
569	LOAD X	54	49	10.10	20	5.05	GLOR UNTF	WV 0 1
570	LOAD Y	54	49	10.10	12	5.05	GLOR UNTF	WV 0 1
571	LOAD X	50	52	0.00	16	5.05	GLOR UNTF	WV 0 1
572	LOAD Y	50	52	0.00	09	5.05	GLOR UNTF	WV 0 1
573	LOAD X	50	52	5.05	16	5.05	GLOR UNTF	WV 0 1
574	LOAD Y	50	52	5.05	09	5.05	GLOR UNTF	WV 0 1
575	LOAD X	50	52	10.10	17	5.05	GLOR UNTF	WV 0 1
576	LOAD Y	50	52	10.10	10	5.05	GLOR UNTF	WV 0 1
577	LOAD X	52	54	0.00	39	5.05	GLOR UNTF	WV 0 1
578	LOAD Y	52	54	5.05	39	5.05	GLOR UNTF	WV 0 1
579	LOAD X	52	54	10.09	39	5.05	GLOR UNTF	WV 0 1
580	LOAD Y	50	50	0.00	17	5.05	GLOR UNTF	WV 0 1
581	LOAD X	54	50	0.00	10	5.05	GLOR UNTF	WV 0 1
582	LOAD Y	54	50	5.05	17	5.05	GLOR UNTF	WV 0 1
583	LOAD X	54	50	5.05	09	5.05	GLOR UNTF	WV 0 1
584	LOAD Y	54	50	10.10	16	5.05	GLOR UNTF	WV 0 1
585	LOAD X	54	50	10.10	09	5.05	GLOR UNTF	WV 0 1
586	LOAD Y	11	22	0.00	1	13.44	GLOR UNTF	WV 0 1
587	LOAD X	11	22	0.00	19	13.44	GLOR UNTF	WV 0 1
588	LOAD Z	11	22	0.00	1	13.44	GLOR UNTF	WV 0 1
589	LOAD Y	11	22	13.44	1	13.44	GLOR UNTF	WV 0 1
590	LOAD X	11	22	13.44	19	13.44	GLOR UNTF	WV 0 1
591	LOAD Z	11	22	13.44	1	13.44	GLOR UNTF	WV 0 1
592	LOAD X	11	22	26.88	1	13.44	GLOR UNTF	WV 0 1



SEALING

LINE NO. 1 1 2 3 4 5 6 7 8

593	LOAD Y	11	22	26.88	20	13.44	21	GLOR UNIT	WV 0 1
594	LOAD Z	11	22	26.88	1	13.44	1	GLOR UNIT	WV 0 1
595	LOAD X	11	24	0.00	1	13.44	1	GLOR UNIT	WV 0 1
596	LOAD Y	11	24	0.00	19	13.44	19	GLOR UNIT	WV 0 1
597	LOAD Z	11	24	0.00	1	13.44	1	GLOR UNIT	WV 0 1
598	LOAD X	11	24	13.44	1	13.44	1	GLOR UNIT	WV 0 1
599	LOAD Y	11	24	13.44	19	13.44	20	GLOR UNIT	WV 0 1
600	LOAD Z	11	24	13.44	1	13.44	1	GLOR UNIT	WV 0 1
601	LOAD X	11	24	26.88	1	13.44	1	GLOR UNIT	WV 0 1
602	LOAD Y	11	24	26.88	20	13.44	21	GLOR UNIT	WV 0 1
603	LOAD Z	11	24	26.88	1	13.44	1	GLOR UNIT	WV 0 1
604	LOAD X	13	24	0.00	03	13.44	05	GLOR UNIT	WV 0 1
605	LOAD Y	13	24	0.00	14	13.44	14	GLOR UNIT	WV 0 1
606	LOAD Z	13	24	0.00	09	13.44	09	GLOR UNIT	WV 0 1
607	LOAD X	13	24	13.44	03	13.44	03	GLOR UNIT	WV 0 1
608	LOAD Y	13	24	13.44	14	13.44	14	GLOR UNIT	WV 0 1
609	LOAD Z	13	24	13.44	09	13.44	09	GLOR UNIT	WV 0 1
610	LOAD X	13	24	26.88	03	13.44	03	GLOR UNIT	WV 0 1
611	LOAD Y	13	24	26.88	14	13.44	15	GLOR UNIT	WV 0 1
612	LOAD Z	13	24	26.88	09	13.44	09	GLOR UNIT	WV 0 1
613	LOAD X	13	26	0.00	04	13.44	04	GLOR UNIT	WV 0 1
614	LOAD Y	13	26	0.00	16	13.44	16	GLOR UNIT	WV 0 1
615	LOAD Z	13	26	0.00	08	13.44	08	GLOR UNIT	WV 0 1
616	LOAD X	13	26	13.44	04	13.44	04	GLOR UNIT	WV 0 1
617	LOAD Y	13	26	13.44	16	13.44	17	GLOR UNIT	WV 0 1
618	LOAD Z	13	26	13.44	08	13.44	08	GLOR UNIT	WV 0 1
619	LOAD X	13	26	26.88	04	13.44	04	GLOR UNIT	WV 0 1
620	LOAD Y	13	26	26.88	17	13.44	17	GLOR UNIT	WV 0 1
621	LOAD Z	13	26	26.88	08	13.44	09	GLOR UNIT	WV 0 1
622	LOAD X	15	26	0.00	04	13.44	04	GLOR UNIT	WV 0 1
623	LOAD Y	15	26	0.00	16	13.44	16	GLOR UNIT	WV 0 1
624	LOAD Z	15	26	0.00	08	13.44	08	GLOR UNIT	WV 0 1
625	LOAD X	15	26	13.44	04	13.44	04	GLOR UNIT	WV 0 1
626	LOAD Y	15	26	13.44	16	13.44	17	GLOR UNIT	WV 0 1
627	LOAD Z	15	26	13.44	08	13.44	08	GLOR UNIT	WV 0 1
628	LOAD X	15	26	26.88	04	13.44	04	GLOR UNIT	WV 0 1
629	LOAD Y	15	26	26.88	17	13.44	17	GLOR UNIT	WV 0 1
630	LOAD Z	15	26	26.88	08	13.44	09	GLOR UNIT	WV 0 1
631	LOAD X	15	22	0.00	03	13.44	03	GLOR UNIT	WV 0 1
632	LOAD Y	15	22	0.00	14	13.44	14	GLOR UNIT	WV 0 1
633	LOAD Z	15	22	0.00	09	13.44	09	GLOR UNIT	WV 0 1
634	LOAD X	15	22	13.44	03	13.44	03	GLOR UNIT	WV 0 1
635	LOAD Y	15	22	13.44	14	13.44	14	GLOR UNIT	WV 0 1
636	LOAD Z	15	22	13.44	09	13.44	09	GLOR UNIT	WV 0 1
637	LOAD X	15	22	26.88	03	13.44	03	GLOR UNIT	WV 0 1
638	LOAD Y	15	22	26.88	14	13.44	15	GLOR UNIT	WV 0 1
639	LOAD Z	15	22	26.88	09	13.44	09	GLOR UNIT	WV 0 1
640	LOAD X	22	36	0.00	1	18.20	1	GLOR UNIT	WV 0 1
641	LOAD Y	22	36	0.00	27	18.20	29	GLOR UNIT	WV 0 1
642	LOAD Z	22	36	0.00	1	18.20	1	GLOR UNIT	WV 0 1



SEALED-2

LINE NO.	1	2	3	4	5	6	7	8
643	LOAD X	22	36	18.20	1	18.20	GLOR UNTF	WV 0 1
644	LOAD Y	22	36	18.20	29	18.20	GLOR UNTF	WV 0 1
645	LOAD Z	22	36	18.20	32	18.20	GLOR UNTF	WV 0 1
646	LOAD X	22	36	36.39	1	18.20	GLOR UNTF	WV 0 1
647	LOAD Y	22	36	36.39	32	18.20	GLOR UNTF	WV 0 1
648	LOAD Z	22	36	36.39	1	18.20	GLOR UNTF	WV 0 1
649	LOAD X	20	38	0.00	08	20.96	GLOR UNTF	WV 0 1
650	LOAD Y	20	38	0.00	11	20.96	GLOR UNTF	WV 0 1
651	LOAD Z	20	38	0.00	10	20.96	GLOR UNTF	WV 0 1
652	LOAD X	24	38	20.96	09	20.96	GLOR UNTF	WV 0 1
653	LOAD Y	24	38	20.96	13	20.96	GLOR UNTF	WV 0 1
654	LOAD Z	24	38	20.96	12	20.96	GLOR UNTF	WV 0 1
655	LOAD X	24	38	41.93	14	20.96	GLOR UNTF	WV 0 1
656	LOAD Y	24	38	41.93	13	20.96	GLOR UNTF	WV 0 1
657	LOAD Z	24	38	41.93	08	18.20	GLOR UNTF	WV 0 1
658	LOAD X	26	34	0.00	14	18.20	GLOR UNTF	WV 0 1
659	LOAD Y	26	34	0.00	12	18.20	GLOR UNTF	WV 0 1
660	LOAD Z	26	34	0.00	08	18.20	GLOR UNTF	WV 0 1
661	LOAD X	26	34	18.20	08	18.20	GLOR UNTF	WV 0 1
662	LOAD Y	26	34	18.20	15	18.20	GLOR UNTF	WV 0 1
663	LOAD Z	26	34	18.20	13	18.20	GLOR UNTF	WV 0 1
664	LOAD X	26	34	36.39	09	18.20	GLOR UNTF	WV 0 1
665	LOAD Y	26	34	36.39	16	18.20	GLOR UNTF	WV 0 1
666	LOAD Z	26	34	36.39	14	18.20	GLOR UNTF	WV 0 1
667	LOAD X	36	49	0.00	1	11.86	GLOR UNTF	WV 0 1
668	LOAD Y	36	49	0.00	36	11.86	GLOR UNTF	WV 0 1
669	LOAD Z	36	49	0.00	1	11.86	GLOR UNTF	WV 0 1
670	LOAD X	36	49	11.86	02	11.86	GLOR UNTF	WV 0 1
671	LOAD Y	36	49	11.86	40	11.86	GLOR UNTF	WV 0 1
672	LOAD Z	36	49	11.86	02	11.86	GLOR UNTF	WV 0 1
673	LOAD X	36	49	23.72	02	11.86	GLOR UNTF	WV 0 1
674	LOAD Y	36	49	23.72	40	11.86	GLOR UNTF	WV 0 1
675	LOAD Z	36	49	23.72	02	11.86	GLOR UNTF	WV 0 1
676	LOAD X	36	49	35.58	02	11.86	GLOR UNTF	WV 0 1
677	LOAD Y	36	49	35.58	50	11.86	GLOR UNTF	WV 0 1
678	LOAD Z	36	49	35.58	02	11.86	GLOR UNTF	WV 0 1
679	LOAD X	38	51	0.00	08	15.93	GLOR UNTF	WV 0 1
680	LOAD Y	38	51	0.00	15	13.93	GLOR UNTF	WV 0 1
681	LOAD Z	38	51	0.00	16	13.93	GLOR UNTF	WV 0 1
682	LOAD X	38	51	13.93	09	13.93	GLOR UNTF	WV 0 1
683	LOAD Y	38	51	13.93	17	13.93	GLOR UNTF	WV 0 1
684	LOAD Z	38	51	13.93	18	13.93	GLOR UNTF	WV 0 1
685	LOAD X	38	51	27.86	10	13.93	GLOR UNTF	WV 0 1
686	LOAD Y	38	51	27.86	19	13.93	GLOR UNTF	WV 0 1
687	LOAD Z	38	51	27.86	21	13.93	GLOR UNTF	WV 0 1
688	LOAD X	38	51	41.79	21	13.93	GLOR UNTF	WV 0 1
689	LOAD Y	38	51	41.79	21	13.93	GLOR UNTF	WV 0 1
690	LOAD Z	38	51	41.79	23	13.93	GLOR UNTF	WV 0 1
691	LOAD X	38	51	0.00	09	9.49	GLOR UNTF	WV 0 1
692	LOAD Y	38	51	0.00	23	9.49	GLOR UNTF	WV 0 1



SFALOAD=2

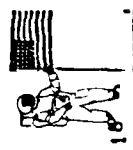
LTME NO. 1 2 3 4 5 6 7 8

693	LOAD Z	34	53	0.00	15	9.49	14	GLOR UNTE	MV 0 1
694	LOAD Y	34	53	9.49	10	9.49	11	GLOR UNTE	MV 0 1
695	LOAD Y	34	53	9.49	25	9.49	24	GLOR UNTE	MV 0 1
696	LOAD Z	34	53	9.49	16	9.49	14	GLOR UNTE	MV 0 1
697	LOAD X	34	53	14.97	11	9.49	13	GLOR UNTE	MV 0 1
698	LOAD Y	34	53	14.97	24	9.49	31	GLOR UNTE	MV 0 1
699	LOAD Z	34	53	14.97	14	9.49	20	GLOR UNTE	MV 0 1
700	LOAD X	34	53	24.46	13	9.49	14	GLOR UNTE	MV 0 1
701	LOAD Y	34	53	24.46	31	9.49	34	GLOR UNTE	MV 0 1
702	LOAD Z	34	53	24.46	20	9.49	22	GLOR UNTE	MV 0 1
703	LOAD X	34	53	37.95	14	9.49	15	GLOR UNTE	MV 0 1
704	LOAD Y	34	53	37.95	34	9.49	38	GLOR UNTE	MV 0 1
705	LOAD Z	34	53	37.95	22	9.49	25	GLOR UNTE	MV 0 1
706	LOAD Y	55	58	0.00	113	5.70	126	GLOR UNTE	MV 0 1
707	LOAD Y	55	58	5.70	126	5.70	141	GLOR UNTE	MV 0 1
708	LOAD Y	55	58	11.40	141	5.70	154	GLOR UNTE	MV 0 1
709	LOAD Y	55	58	17.10	154	5.70	174	GLOR UNTE	MV 0 1
710	LOAD Y	55	58	22.80	174	5.70	202	GLOR UNTE	MV 0 1
711	LOAD Y	58	61	0.00	202	4.19	221	GLOR UNTE	MV 0 1
712	LOAD Y	58	61	4.19	221	4.19	240	GLOR UNTE	MV 0 1
713	LOAD Y	58	61	8.39	240	4.19	270	GLOR UNTE	MV 0 1
714	LOAD Y	58	59	0.00	113	5.70	126	GLOR UNTE	MV 0 1
715	LOAD Y	58	59	5.70	126	5.70	141	GLOR UNTE	MV 0 1
716	LOAD Y	58	59	11.40	141	5.70	154	GLOR UNTE	MV 0 1
717	LOAD Y	58	59	17.10	154	5.70	174	GLOR UNTE	MV 0 1
718	LOAD Y	58	59	22.80	174	5.70	202	GLOR UNTE	MV 0 1
719	LOAD Y	59	64	0.00	202	4.19	221	GLOR UNTE	MV 0 1
720	LOAD Y	59	64	4.19	221	4.19	244	GLOR UNTE	MV 0 1
721	LOAD Y	59	60	8.39	244	4.19	270	GLOR UNTE	MV 0 1
722	LOAD Y	57	60	0.00	114	5.70	143	GLOR UNTE	MV 0 1
723	LOAD Y	57	60	5.70	129	5.70	160	GLOR UNTE	MV 0 1
724	LOAD Y	57	60	11.40	143	5.70	176	GLOR UNTE	MV 0 1
725	LOAD Y	57	60	17.10	160	5.70	190	GLOR UNTE	MV 0 1
726	LOAD Y	57	60	22.80	180	5.70	201	GLOR UNTE	MV 0 1
727	LOAD Y	60	70	0.00	201	2.00	210	GLOR UNTE	MV 0 1
728	LOAD Y	60	70	2.00	210	2.00	220	GLOR UNTE	MV 0 1
729	LOAD Y	60	70	4.00	220	2.00	231	GLOR UNTE	MV 0 1
730	LOAD Y	70	67	0.00	231	.22	232	GLOR UNTE	MV 0 1
731	LOAD Y	70	67	.22	232	.22	233	GLOR UNTE	MV 0 1
732	LOAD Y	70	67	.44	233	.22	234	GLOR UNTE	MV 0 1
733	LOAD Y	70	67	.67	234	.22	235	GLOR UNTE	MV 0 1
734	LOAD Y	70	67	.89	235	.22	237	GLOR UNTE	MV 0 1
735	LOAD Y	70	67	1.11	237	.22	238	GLOR UNTE	MV 0 1
736	LOAD Y	70	67	1.33	238	.22	239	GLOR UNTE	MV 0 1
737	LOAD Y	70	67	1.56	239	.22	241	GLOR UNTE	MV 0 1
738	LOAD Y	70	67	1.78	241	.22	241	GLOR UNTE	MV 0 1
739	LOAD Y	58	59	0.00	71	9.67	71	GLOR UNTE	MV 0 1
740	LOAD Y	58	59	9.67	71	9.67	71	GLOR UNTE	MV 0 1
741	LOAD Y	58	59	19.33	71	9.67	71	GLOR UNTE	MV 0 1
742	LOAD X	59	60	0.00	31	9.67	32	GLOR UNTE	MV 0 1



SEALHAT-2

LINE NO.	1	2	3	4	5	6	7	8	
743	LOAD Y	59	60	0.00	18	9.67	18	GLOR UNTF	AV 0 1
744	LOAD X	50	60	9.67	32	9.67	32	GLOR UNTF	AV 0 1
745	LOAD Y	59	60	9.67	18	9.67	18	GLOR UNTF	AV 0 1
746	LOAD X	59	60	19.33	32	9.67	31	GLOR UNTF	AV 0 1
747	LOAD Y	59	60	19.33	18	9.67	18	GLOR UNTF	AV 0 1
748	LOAD X	60	58	0.00	18	9.67	18	GLOR UNTF	AV 0 1
749	LOAD Y	60	58	0.00	18	9.67	18	GLOR UNTF	AV 0 1
750	LOAD X	60	58	9.67	32	9.67	32	GLOR UNTF	AV 0 1
751	LOAD Y	60	58	9.67	18	9.67	18	GLOR UNTF	AV 0 1
752	LOAD X	60	58	19.33	32	9.67	31	GLOR UNTF	AV 0 1
753	LOAD Y	60	58	19.33	18	9.67	18	GLOR UNTF	AV 0 1
754	LOAD X	59	61	0.00	71	9.13	71	GLOR UNTF	AV 0 1
755	LOAD Y	59	61	9.13	78	9.13	86	GLOR UNTF	AV 0 1
756	LOAD X	59	61	18.25	86	9.13	95	GLOR UNTF	AV 0 1
757	LOAD Y	60	64	0.00	24	8.41	27	GLOR UNTF	AV 0 1
758	LOAD X	60	64	0.00	29	8.41	33	GLOR UNTF	AV 0 1
759	LOAD Z	60	64	0.00	25	8.41	20	GLOR UNTF	AV 0 1
760	LOAD X	60	64	8.41	27	8.41	30	GLOR UNTF	AV 0 1
761	LOAD Y	60	64	8.41	33	8.41	36	GLOR UNTF	AV 0 1
762	LOAD Z	60	64	8.41	28	8.41	31	GLOR UNTF	AV 0 1
763	LOAD X	60	64	16.81	30	8.41	33	GLOR UNTF	AV 0 1
764	LOAD Y	60	64	16.81	36	8.41	39	GLOR UNTF	AV 0 1
765	LOAD Z	60	64	16.81	31	8.41	34	GLOR UNTF	AV 0 1
766	LOAD X	58	67	0.00	24	7.07	27	GLOR UNTF	AV 0 1
767	LOAD Y	58	67	0.00	29	7.07	32	GLOR UNTF	AV 0 1
768	LOAD Z	58	67	0.00	25	7.07	28	GLOR UNTF	AV 0 1
769	LOAD X	58	67	7.07	27	7.07	29	GLOR UNTF	AV 0 1
770	LOAD Y	58	67	7.07	32	7.07	35	GLOR UNTF	AV 0 1
771	LOAD Z	58	67	7.07	28	7.07	30	GLOR UNTF	AV 0 1
772	LOAD X	58	67	14.14	29	7.07	31	GLOR UNTF	AV 0 1
773	LOAD Y	58	67	14.14	35	7.07	37	GLOR UNTF	AV 0 1
774	LOAD Z	58	67	14.14	30	7.07	32	GLOR UNTF	AV 0 1
775	LOAD X	70	66	0.00	42	.33	43	GLOR UNTF	AV 0 1
776	LOAD Y	70	66	.33	43	.33	43	GLOR UNTF	AV 0 1
777	LOAD Z	70	66	.66	43	.33	43	GLOR UNTF	AV 0 1
778	LOAD X	70	66	1.00	43	.55	43	GLOR UNTF	AV 0 1
779	LOAD Y	70	66	1.33	43	.33	43	GLOR UNTF	AV 0 1
780	LOAD Z	70	66	1.66	43	.33	44	GLOR UNTF	AV 0 1
781	LOAD X	70	66	1.99	44	.33	44	GLOR UNTF	AV 0 1
782	LOAD Y	70	66	2.33	44	.33	44	GLOR UNTF	AV 0 1
783	LOAD Z	70	66	2.66	44	.33	44	GLOR UNTF	AV 0 1
784	LOAD X	70	66	0.00	42	.55	43	GLOR UNTF	AV 0 1
785	LOAD Y	70	66	.33	43	.33	43	GLOR UNTF	AV 0 1
786	LOAD Z	70	66	.66	43	.33	43	GLOR UNTF	AV 0 1
787	LOAD X	70	66	1.00	43	.55	43	GLOR UNTF	AV 0 1
788	LOAD Y	70	66	1.33	43	.55	43	GLOR UNTF	AV 0 1
789	LOAD Z	70	66	1.66	43	.55	44	GLOR UNTF	AV 0 1
790	LOAD X	70	66	1.99	44	.55	44	GLOR UNTF	AV 0 1
791	LOAD Y	70	66	2.33	44	.55	44	GLOR UNTF	AV 0 1
792	LOAD Z	70	66	2.66	44	.55	44	GLOR UNTF	AV 0 1



SEALOAD=2

LINE NO. 1 1 1 2 2 3 3 4 4 5 5 6 6 7 7 8

A43	LOAD Y	49	55	0.00	123	1.52	124	GLOR	UNTF	WV	0	2
A44	LOAD Z	49	55	0.00	10	1.52	10	GLOR	UNTF	WV	0	2
A45	LOAD X	49	55	1.52	1	1.52	1	GLOR	UNTF	WV	0	2
A46	LOAD Y	49	55	1.52	126	1.52	129	GLOR	UNTF	WV	0	2
A47	LOAD Z	49	55	1.52	10	1.52	11	GLOR	UNTF	WV	0	2
A48	LOAD X	49	55	3.04	1	1.52	12	GLOR	UNTF	WV	0	2
A49	LOAD Y	49	55	3.04	129	1.52	133	GLOR	UNTF	WV	0	2
A50	LOAD Z	49	55	3.04	11	1.52	11	GLOR	UNTF	WV	0	2
A51	LOAD X	12	24	0.00	1	10.81	1	GLOR	UNTF	WV	0	2
A52	LOAD Y	12	24	0.00	51	10.81	52	GLOR	UNTF	WV	0	2
A53	LOAD Z	12	24	0.00	04	10.81	04	GLOR	UNTF	WV	0	2
A54	LOAD X	12	24	10.81	1	10.81	1	GLOR	UNTF	WV	0	2
A55	LOAD Y	12	24	10.81	52	10.81	54	GLOR	UNTF	WV	0	2
A56	LOAD Z	12	24	10.81	04	10.81	04	GLOR	UNTF	WV	0	2
A57	LOAD X	12	24	21.63	1	10.81	1	GLOR	UNTF	WV	0	2
A58	LOAD Y	12	24	21.63	54	10.81	57	GLOR	UNTF	WV	0	2
A59	LOAD Z	12	24	21.63	04	10.81	05	GLOR	UNTF	WV	0	2
A60	LOAD X	24	36	0.00	1	10.81	1	GLOR	UNTF	WV	0	2
A61	LOAD Y	24	36	0.00	57	10.81	62	GLOR	UNTF	WV	0	2
A62	LOAD Z	24	36	0.00	05	10.81	05	GLOR	UNTF	WV	0	2
A63	LOAD X	24	36	10.81	1	10.81	1	GLOR	UNTF	WV	0	2
A64	LOAD Y	24	36	10.81	62	10.81	64	GLOR	UNTF	WV	0	2
A65	LOAD Z	24	36	10.81	05	10.81	05	GLOR	UNTF	WV	0	2
A66	LOAD X	24	36	21.63	1	10.81	1	GLOR	UNTF	WV	0	2
A67	LOAD Y	24	36	21.63	64	10.81	74	GLOR	UNTF	WV	0	2
A68	LOAD Z	24	36	21.63	05	10.81	06	GLOR	UNTF	WV	0	2
A69	LOAD X	36	48	0.00	1	4.73	1	GLOR	UNTF	WV	0	2
A70	LOAD Y	36	48	0.00	74	4.73	82	GLOR	UNTF	WV	0	2
A71	LOAD Z	36	48	0.00	05	4.73	06	GLOR	UNTF	WV	0	2
A72	LOAD X	36	48	4.73	1	4.73	1	GLOR	UNTF	WV	0	2
A73	LOAD Y	36	48	4.73	82	4.73	87	GLOR	UNTF	WV	0	2
A74	LOAD Z	36	48	4.73	06	4.73	06	GLOR	UNTF	WV	0	2
A75	LOAD X	36	48	9.45	1	4.73	1	GLOR	UNTF	WV	0	2
A76	LOAD Y	36	48	9.45	87	4.73	93	GLOR	UNTF	WV	0	2
A77	LOAD Z	36	48	9.45	06	4.73	06	GLOR	UNTF	WV	0	2
A78	LOAD X	48	56	0.00	1	6.09	1	GLOR	UNTF	WV	0	2
A79	LOAD Y	48	56	0.00	92	6.09	101	GLOR	UNTF	WV	0	2
A80	LOAD Z	48	56	0.00	08	6.09	09	GLOR	UNTF	WV	0	2
A81	LOAD X	48	56	6.09	1	6.09	1	GLOR	UNTF	WV	0	2
A82	LOAD Y	48	56	6.09	101	6.09	111	GLOR	UNTF	WV	0	2
A83	LOAD Z	48	56	6.09	09	6.09	10	GLOR	UNTF	WV	0	2
A84	LOAD X	48	56	12.17	1	6.09	02	GLOR	UNTF	WV	0	2
A85	LOAD Y	48	56	12.17	111	6.09	123	GLOR	UNTF	WV	0	2
A86	LOAD Z	48	56	12.17	10	6.09	11	GLOR	UNTF	WV	0	2
A87	LOAD X	56	64	0.00	1	1.52	1	GLOR	UNTF	WV	0	2
A88	LOAD Y	56	64	0.00	123	1.52	124	GLOR	UNTF	WV	0	2
A89	LOAD Z	56	64	0.00	10	1.52	10	GLOR	UNTF	WV	0	2
A90	LOAD X	56	64	1.52	1	1.52	1	GLOR	UNTF	WV	0	2
A91	LOAD Y	56	64	1.52	126	1.52	129	GLOR	UNTF	WV	0	2
A92	LOAD Z	56	64	1.52	10	1.52	11	GLOR	UNTF	WV	0	2



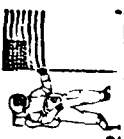
SFAI 010102

LINE NO.	1	2	3	4	5	6	7	8		
893	LOAD	Y	51	54	3,004	1	1,52	02	GLOR UNITF	WV 0 2
894	LOAD	Y	51	56	3,004	129	1,52	133	GLOR UNITF	WV 0 2
895	LOAD	Z	51	5A	3,004	11	1,52	11	GLOR UNITF	WV 0 2
896	LOAD	Y	14	26	0,00	59	10,81	41	GLOR UNITF	WV 0 2
897	LOAD	Z	14	2A	0,00	07	10,81	07	GLOR UNITF	WV 0 2
898	LOAD	Y	14	2A	10,81	41	10,81	42	GLOR UNITF	WV 0 2
899	LOAD	Z	14	2A	10,81	07	10,81	07	GLOR UNITF	WV 0 2
900	LOAD	Y	14	2A	21,63	42	10,81	44	GLOR UNITF	WV 0 2
901	LOAD	Z	14	2A	21,63	07	10,81	0A	GLOR UNITF	WV 0 2
902	LOAD	Y	2A	3A	0,00	45	10,86	47	GLOR UNITF	WV 0 2
903	LOAD	Z	2A	3A	0,00	09	10,86	09	GLOR UNITF	WV 0 2
904	LOAD	Y	2A	3A	10,86	47	10,86	51	GLOR UNITF	WV 0 2
905	LOAD	Z	2A	3A	10,86	09	10,86	10	GLOR UNITF	WV 0 2
906	LOAD	Y	26	3A	21,72	51	10,86	55	GLOR UNITF	WV 0 2
907	LOAD	Z	26	3A	21,72	10	10,86	10	GLOR UNITF	WV 0 2
908	LOAD	Y	3A	42	0,00	51	5,01	55	GLOR UNITF	WV 0 2
909	LOAD	Z	3A	42	0,00	20	5,01	21	GLOR UNITF	WV 0 2
910	LOAD	Y	3A	42	5,01	55	5,01	50	GLOR UNITF	WV 0 2
911	LOAD	Z	3A	42	5,01	21	5,01	23	GLOR UNITF	WV 0 2
912	LOAD	Y	3A	42	10,02	59	5,01	60	GLOR UNITF	WV 0 2
913	LOAD	Z	3A	42	10,02	23	5,01	25	GLOR UNITF	WV 0 2
914	LOAD	Y	42	53	0,00	53	5,31	5A	GLOR UNITF	WV 0 2
915	LOAD	Z	42	53	0,00	33	5,31	36	GLOR UNITF	WV 0 2
916	LOAD	Y	42	53	5,31	5A	5,31	60	GLOR UNITF	WV 0 2
917	LOAD	Z	42	53	5,31	36	5,31	40	GLOR UNITF	WV 0 2
918	LOAD	Y	42	53	10,63	60	5,31	70	GLOR UNITF	WV 0 2
919	LOAD	Z	42	53	10,63	40	5,31	44	GLOR UNITF	WV 0 2
920	LOAD	Y	42	53	15,94	70	5,31	7A	GLOR UNITF	WV 0 2
921	LOAD	Z	42	53	15,94	34	5,31	49	GLOR UNITF	WV 0 2
922	LOAD	Y	53	57	0,00	106	1,52	109	GLOR UNITF	WV 0 2
923	LOAD	Z	53	57	0,00	1A	1,52	1A	GLOR UNITF	WV 0 2
924	LOAD	Y	53	57	1,52	109	1,52	113	GLOR UNITF	WV 0 2
925	LOAD	Z	53	57	1,52	18	1,52	19	GLOR UNITF	WV 0 2
926	LOAD	Y	53	57	3,04	113	1,52	11A	GLOR UNITF	WV 0 2
927	LOAD	Z	53	57	3,04	19	1,52	19	GLOR UNITF	WV 0 2
928	LOAD	Y	10	11	0,00	23	9,67	23	GLOR UNITF	WV 0 2
929	LOAD	Z	10	11	9,67	23	9,67	23	GLOR UNITF	WV 0 2
930	LOAD	Y	10	11	19,33	23	9,67	23	GLOR UNITF	WV 0 2
931	LOAD	Z	10	11	0,00	23	9,67	23	GLOR UNITF	WV 0 2
932	LOAD	Y	11	12	9,67	23	9,67	23	GLOR UNITF	WV 0 2
933	LOAD	Z	11	12	19,33	23	9,67	23	GLOR UNITF	WV 0 2
934	LOAD	Y	12	13	0,00	10	9,67	10	GLOR UNITF	WV 0 2
935	LOAD	Z	12	13	0,00	06	9,67	06	GLOR UNITF	WV 0 2
936	LOAD	Y	12	13	9,67	10	9,67	10	GLOR UNITF	WV 0 2
937	LOAD	Z	12	13	9,67	06	9,67	06	GLOR UNITF	WV 0 2
938	LOAD	Y	12	13	19,33	10	9,67	09	GLOR UNITF	WV 0 2
939	LOAD	Z	12	13	19,33	06	9,67	05	GLOR UNITF	WV 0 2
940	LOAD	Y	13	14	0,00	09	9,67	0A	GLOR UNITF	WV 0 2
941	LOAD	Z	13	14	0,00	05	9,67	05	GLOR UNITF	WV 0 2
942	LOAD	Y	13	14	9,67	09	9,67	0A	GLOR UNITF	WV 0 2



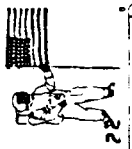
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LINE NO.	1	2	3	4	5	6	7	8					
903	LOAD	Y	13	14	0.67	05	9.67	05	GLOR	UNTF	WV	0	2
904	LOAD	X	13	14	19.34	0A	9.67	0A	GLOR	UNTF	WV	0	2
905	LOAD	Y	13	14	19.30	05	9.67	05	GLOR	UNTF	WV	0	2
906	LOAD	X	14	15	0.00	0A	9.67	0A	GLOR	UNTF	WV	0	2
907	LOAD	Y	14	15	0.00	05	9.67	05	GLOR	UNTF	WV	0	2
908	LOAD	X	14	15	9.67	0A	9.67	0A	GLOR	UNTF	WV	0	2
909	LOAD	Y	14	15	9.67	05	9.67	05	GLOR	UNTF	WV	0	2
950	LOAD	X	14	15	19.34	09	9.67	09	GLOR	UNTF	WV	0	2
951	LOAD	Y	14	15	19.34	05	9.67	05	GLOR	UNTF	WV	0	2
952	LOAD	X	15	10	0.00	09	9.67	10	GLOR	UNTF	WV	0	2
953	LOAD	Y	15	10	0.00	05	9.67	10	GLOR	UNTF	WV	0	2
954	LOAD	X	15	10	9.67	10	9.67	10	GLOR	UNTF	WV	0	2
955	LOAD	Y	15	10	9.67	0A	9.67	10	GLOR	UNTF	WV	0	2
956	LOAD	X	15	10	9.67	0A	9.67	10	GLOR	UNTF	WV	0	2
957	LOAD	Y	15	10	19.33	0A	9.67	10	GLOR	UNTF	WV	0	2
958	LOAD	X	15	10	19.33	06	9.67	10	GLOR	UNTF	WV	0	2
959	LOAD	Y	11	13	0.00	0A	9.67	0A	GLOR	UNTF	WV	0	2
960	LOAD	X	11	13	9.67	0A	9.67	0A	GLOR	UNTF	WV	0	2
961	LOAD	Y	11	13	9.67	0A	9.67	0A	GLOR	UNTF	WV	0	2
962	LOAD	X	11	13	19.33	07	9.67	07	GLOR	UNTF	WV	0	2
963	LOAD	Y	11	13	19.33	04	9.67	04	GLOR	UNTF	WV	0	2
964	LOAD	X	13	15	0.00	17	9.67	17	GLOR	UNTF	WV	0	2
965	LOAD	Y	13	15	9.67	17	9.67	17	GLOR	UNTF	WV	0	2
966	LOAD	X	13	15	19.53	17	9.67	17	GLOR	UNTF	WV	0	2
967	LOAD	Y	14	11	0.00	07	9.67	07	GLOR	UNTF	WV	0	2
968	LOAD	X	15	11	0.00	04	9.67	04	GLOR	UNTF	WV	0	2
969	LOAD	Y	15	11	9.67	07	9.67	07	GLOR	UNTF	WV	0	2
970	LOAD	X	15	11	9.67	04	9.67	04	GLOR	UNTF	WV	0	2
971	LOAD	Y	15	11	19.33	0A	9.67	0A	GLOR	UNTF	WV	0	2
972	LOAD	X	15	11	19.33	0A	9.67	0A	GLOR	UNTF	WV	0	2
973	LOAD	Y	22	23	0.00	26	8.13	26	GLOR	UNTF	WV	0	2
974	LOAD	X	22	23	8.13	26	8.13	26	GLOR	UNTF	WV	0	2
975	LOAD	Y	22	23	14.25	26	8.13	26	GLOR	UNTF	WV	0	2
976	LOAD	X	23	24	0.00	26	8.13	26	GLOR	UNTF	WV	0	2
977	LOAD	Y	23	24	8.13	26	8.13	26	GLOR	UNTF	WV	0	2
978	LOAD	X	23	24	14.25	26	8.13	26	GLOR	UNTF	WV	0	2
979	LOAD	Y	24	25	0.00	11	8.13	11	GLOR	UNTF	WV	0	2
980	LOAD	X	24	25	0.00	06	8.13	06	GLOR	UNTF	WV	0	2
981	LOAD	Y	24	25	8.13	11	8.13	11	GLOR	UNTF	WV	0	2
982	LOAD	X	24	25	8.13	06	8.13	06	GLOR	UNTF	WV	0	2
983	LOAD	Y	24	25	14.25	11	8.13	11	GLOR	UNTF	WV	0	2
984	LOAD	X	24	25	14.25	06	8.13	06	GLOR	UNTF	WV	0	2
985	LOAD	Y	25	26	0.00	11	8.13	11	GLOR	UNTF	WV	0	2
986	LOAD	X	25	26	0.00	06	8.13	06	GLOR	UNTF	WV	0	2
987	LOAD	Y	25	26	8.13	11	8.13	11	GLOR	UNTF	WV	0	2
988	LOAD	X	25	26	8.13	06	8.13	06	GLOR	UNTF	WV	0	2
989	LOAD	Y	25	26	14.25	11	8.13	11	GLOR	UNTF	WV	0	2
990	LOAD	X	25	26	14.25	06	8.13	06	GLOR	UNTF	WV	0	2
991	LOAD	Y	26	27	0.00	0A	8.13	10	GLOR	UNTF	WV	0	2
992	LOAD	X	26	27	0.00	05	8.13	06	GLOR	UNTF	WV	0	2



SPALHAD=2

LINE NO.	1	2	3	4	5	6	7	8	
993	LOAD X	24	27	A.13=	10	A.13=	10	GLOR UNTF	MV 0 2
994	LOAD Y	24	27	A.13=	04	A.13=	04	GLOR UNTF	MV 0 2
995	LOAD X	24	27	16.25=	10	A.13=	11	GLOR UNTF	MV 0 2
996	LOAD Y	24	27	16.25=	06	A.13=	06	GLOR UNTF	MV 0 2
997	LOAD X	27	22	0.00=	11	A.13=	11	GLOR UNTF	MV 0 2
998	LOAD Y	27	22	0.00=	04	A.13=	04	GLOR UNTF	MV 0 2
999	LOAD X	27	22	A.13=	11	A.13=	11	GLOR UNTF	MV 0 2
1000	LOAD Y	27	22	A.13=	06	A.13=	06	GLOR UNTF	MV 0 2
1001	LOAD X	27	22	16.25=	11	A.13=	11	GLOR UNTF	MV 0 2
1002	LOAD Y	27	22	16.25=	06	A.13=	06	GLOR UNTF	MV 0 2
1003	LOAD X	23	25	0.00=	09	A.13=	09	GLOR UNTF	MV 0 2
1004	LOAD Y	23	25	0.00=	05	A.13=	05	GLOR UNTF	MV 0 2
1005	LOAD X	23	25	A.13=	09	A.13=	08	GLOR UNTF	MV 0 2
1006	LOAD Y	23	25	A.13=	05	A.13=	05	GLOR UNTF	MV 0 2
1007	LOAD X	23	25	16.25=	08	A.13=	08	GLOR UNTF	MV 0 2
1008	LOAD Y	23	25	16.25=	05	A.13=	05	GLOR UNTF	MV 0 2
1009	LOAD X	25	27	0.00=	19	A.13=	19	GLOR UNTF	MV 0 2
1010	LOAD Y	25	27	A.13=	19	A.13=	19	GLOR UNTF	MV 0 2
1011	LOAD X	25	27	16.25=	19	A.13=	19	GLOR UNTF	MV 0 2
1012	LOAD Y	27	23	0.00=	08	A.13=	08	GLOR UNTF	MV 0 2
1013	LOAD X	27	23	0.00=	05	A.13=	05	GLOR UNTF	MV 0 2
1014	LOAD Y	27	23	A.13=	08	A.13=	09	GLOR UNTF	MV 0 2
1015	LOAD X	27	23	A.13=	05	A.13=	05	GLOR UNTF	MV 0 2
1016	LOAD Y	27	23	16.25=	09	A.13=	09	GLOR UNTF	MV 0 2
1017	LOAD X	27	23	16.25=	05	A.13=	05	GLOR UNTF	MV 0 2
1018	LOAD Y	34	35	0.00=	24	A.59=	24	GLOR UNTF	MV 0 2
1019	LOAD X	34	35	6.59=	24	6.59=	24	GLOR UNTF	MV 0 2
1020	LOAD Y	34	35	13.18=	24	6.59=	24	GLOR UNTF	MV 0 2
1021	LOAD X	35	36	0.00=	24	6.59=	24	GLOR UNTF	MV 0 2
1022	LOAD Y	35	36	A.59=	24	A.59=	24	GLOR UNTF	MV 0 2
1023	LOAD X	35	36	13.18=	24	6.59=	24	GLOR UNTF	MV 0 2
1024	LOAD Y	36	37	0.00=	10	6.59=	10	GLOR UNTF	MV 0 2
1025	LOAD X	36	37	0.00=	06	6.59=	06	GLOR UNTF	MV 0 2
1026	LOAD Y	36	37	6.59=	10	6.59=	10	GLOR UNTF	MV 0 2
1027	LOAD X	36	37	6.59=	06	6.59=	06	GLOR UNTF	MV 0 2
1028	LOAD Y	36	37	13.18=	10	6.59=	10	GLOR UNTF	MV 0 2
1029	LOAD X	36	37	13.18=	06	6.59=	06	GLOR UNTF	MV 0 2
1030	LOAD Y	37	38	0.00=	07	10.07=	07	GLOR UNTF	MV 0 2
1031	LOAD X	37	38	0.00=	02	10.07=	02	GLOR UNTF	MV 0 2
1032	LOAD Y	37	38	10.07=	07	10.07=	06	GLOR UNTF	MV 0 2
1033	LOAD X	37	38	10.07=	02	10.07=	02	GLOR UNTF	MV 0 2
1034	LOAD Y	37	38	20.15=	06	10.07=	06	GLOR UNTF	MV 0 2
1035	LOAD X	37	38	20.15=	02	10.07=	02	GLOR UNTF	MV 0 2
1036	LOAD Y	38	39	0.00=	06	10.07=	06	GLOR UNTF	MV 0 2
1037	LOAD X	38	39	0.00=	02	10.07=	02	GLOR UNTF	MV 0 2
1038	LOAD Y	38	39	10.07=	06	10.07=	07	GLOR UNTF	MV 0 2
1039	LOAD X	38	39	10.07=	02	10.07=	02	GLOR UNTF	MV 0 2
1040	LOAD Y	38	39	20.15=	07	10.07=	07	GLOR UNTF	MV 0 2
1041	LOAD X	38	39	20.15=	02	10.07=	02	GLOR UNTF	MV 0 2
1042	LOAD Y	39	38	0.00=	10	6.59=	10	GLOR UNTF	MV 0 2



SPAL 111111

LINE NO.	1	2	3	4	5	6	7	8	
1043	LOAD Y	39	34	0.00	06	6.59	04	GLOR UNTF	WV 0 2
1044	LOAD X	39	34	6.59	10	6.59	10	GLOR UNTF	WV 0 2
1045	LOAD Y	39	34	6.59	06	6.59	06	GLOR UNTF	WV 0 2
1046	LOAD X	39	34	13.18	10	6.59	10	GLOR UNTF	WV 0 2
1047	LOAD Y	39	34	13.18	06	6.59	06	GLOR UNTF	WV 0 2
1048	LOAD X	35	37	0.00	10	6.59	10	GLOR UNTF	WV 0 2
1049	LOAD Y	35	37	0.00	06	6.59	06	GLOR UNTF	WV 0 2
1050	LOAD X	35	37	6.59	10	6.59	10	GLOR UNTF	WV 0 2
1051	LOAD Y	35	37	6.59	06	6.59	06	GLOR UNTF	WV 0 2
1052	LOAD X	35	37	13.18	10	6.59	10	GLOR UNTF	WV 0 2
1053	LOAD Y	35	37	13.18	06	6.59	06	GLOR UNTF	WV 0 2
1054	LOAD X	37	39	0.00	23	6.59	23	GLOR UNTF	WV 0 2
1055	LOAD Y	37	39	6.59	23	6.59	23	GLOR UNTF	WV 0 2
1056	LOAD X	37	39	13.17	23	6.59	23	GLOR UNTF	WV 0 2
1057	LOAD Y	39	35	0.00	10	6.59	10	GLOR UNTF	WV 0 2
1058	LOAD X	39	35	0.00	06	6.59	06	GLOR UNTF	WV 0 2
1059	LOAD Y	39	35	6.59	10	6.59	10	GLOR UNTF	WV 0 2
1060	LOAD X	39	35	6.59	06	6.59	06	GLOR UNTF	WV 0 2
1061	LOAD Y	39	35	13.18	10	6.59	10	GLOR UNTF	WV 0 2
1062	LOAD X	39	35	13.18	06	6.59	06	GLOR UNTF	WV 0 2
1063	LOAD Y	49	50	0.00	48	5.05	48	GLOR UNTF	WV 0 2
1064	LOAD X	49	50	5.05	48	5.05	48	GLOR UNTF	WV 0 2
1065	LOAD Y	49	50	10.10	48	5.05	48	GLOR UNTF	WV 0 2
1066	LOAD X	50	51	0.00	48	5.05	48	GLOR UNTF	WV 0 2
1067	LOAD Y	50	51	5.05	48	5.05	48	GLOR UNTF	WV 0 2
1068	LOAD X	50	51	10.10	48	5.05	48	GLOR UNTF	WV 0 2
1069	LOAD Y	51	52	0.00	21	5.05	21	GLOR UNTF	WV 0 2
1070	LOAD X	51	52	0.00	12	5.05	12	GLOR UNTF	WV 0 2
1071	LOAD Y	51	52	5.05	21	5.05	21	GLOR UNTF	WV 0 2
1072	LOAD X	51	52	5.05	12	5.05	12	GLOR UNTF	WV 0 2
1073	LOAD Y	51	52	10.10	20	5.05	20	GLOR UNTF	WV 0 2
1074	LOAD X	51	52	10.10	12	5.05	12	GLOR UNTF	WV 0 2
1075	LOAD Y	52	53	0.00	20	5.05	20	GLOR UNTF	WV 0 2
1076	LOAD X	52	53	0.00	12	5.05	12	GLOR UNTF	WV 0 2
1077	LOAD Y	52	53	5.05	20	5.05	20	GLOR UNTF	WV 0 2
1078	LOAD X	52	53	5.05	11	5.05	11	GLOR UNTF	WV 0 2
1079	LOAD Y	52	53	10.10	19	5.05	19	GLOR UNTF	WV 0 2
1080	LOAD X	52	53	10.10	11	5.05	11	GLOR UNTF	WV 0 2
1081	LOAD Y	53	54	0.00	18	5.05	18	GLOR UNTF	WV 0 2
1082	LOAD X	53	54	0.00	11	5.05	11	GLOR UNTF	WV 0 2
1083	LOAD Y	53	54	5.05	19	5.05	19	GLOR UNTF	WV 0 2
1084	LOAD X	53	54	5.05	11	5.05	11	GLOR UNTF	WV 0 2
1085	LOAD Y	53	54	10.10	20	5.05	20	GLOR UNTF	WV 0 2
1086	LOAD X	53	54	10.10	11	5.05	11	GLOR UNTF	WV 0 2
1087	LOAD Y	54	49	0.00	20	5.05	20	GLOR UNTF	WV 0 2
1088	LOAD X	54	49	0.00	12	5.05	12	GLOR UNTF	WV 0 2
1089	LOAD Y	54	49	5.05	20	5.05	20	GLOR UNTF	WV 0 2
1090	LOAD X	54	49	5.05	12	5.05	12	GLOR UNTF	WV 0 2
1091	LOAD Y	54	49	10.10	21	5.05	21	GLOR UNTF	WV 0 2
1092	LOAD X	54	49	10.10	12	5.05	12	GLOR UNTF	WV 0 2

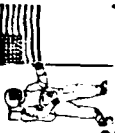
SFA111A1-2

LINE	A	1	2	3	4	5	6	7	8
1093	LOAD X	50	52	0.00	17	5.05	16	GLOR UNTE	WV 0 2
1094	LOAD Y	50	52	0.00	17	5.05	06	GLOR UNTE	WV 0 2
1095	LOAD X	50	52	5.05	16	5.05	16	GLOR UNTE	WV 0 2
1096	LOAD Y	50	52	5.05	09	5.05	09	GLOR UNTE	WV 0 2
1097	LOAD X	50	52	10.10	16	5.05	16	GLOR UNTE	WV 0 2
1098	LOAD Y	50	52	10.10	02	5.05	02	GLOR UNTE	WV 0 2
1099	LOAD X	52	54	0.00	37	5.05	37	GLOR UNTE	WV 0 2
1100	LOAD Y	52	54	5.05	37	5.05	37	GLOR UNTE	WV 0 2
1101	LOAD X	54	50	0.00	16	5.05	16	GLOR UNTE	WV 0 2
1102	LOAD Y	54	50	0.00	16	5.05	09	GLOR UNTE	WV 0 2
1103	LOAD X	54	50	0.00	16	5.05	16	GLOR UNTE	WV 0 2
1104	LOAD Y	54	50	5.05	16	5.05	16	GLOR UNTE	WV 0 2
1105	LOAD X	54	50	5.05	09	5.05	09	GLOR UNTE	WV 0 2
1106	LOAD Y	54	50	10.10	16	5.05	17	GLOR UNTE	WV 0 2
1107	LOAD X	54	50	10.10	09	5.05	10	GLOR UNTE	WV 0 2
1108	LOAD Y	11	22	0.00	1	13.44	1	GLOR UNTE	WV 0 2
1109	LOAD X	11	22	0.00	21	13.44	21	GLOR UNTE	WV 0 2
1110	LOAD Y	11	22	0.00	1	13.44	1	GLOR UNTE	WV 0 2
1111	LOAD X	11	22	13.44	1	13.44	1	GLOR UNTE	WV 0 2
1112	LOAD Y	11	22	13.44	21	13.44	22	GLOR UNTE	WV 0 2
1113	LOAD X	11	22	13.44	1	13.44	1	GLOR UNTE	WV 0 2
1114	LOAD Y	11	22	26.88	1	13.44	1	GLOR UNTE	WV 0 2
1115	LOAD X	11	22	26.88	22	13.44	23	GLOR UNTE	WV 0 2
1116	LOAD Y	11	22	26.88	1	13.44	1	GLOR UNTE	WV 0 2
1117	LOAD X	11	24	0.00	1	13.44	1	GLOR UNTE	WV 0 2
1118	LOAD Y	11	24	0.00	21	13.44	21	GLOR UNTE	WV 0 2
1119	LOAD X	11	24	0.00	1	13.44	1	GLOR UNTE	WV 0 2
1120	LOAD Y	11	24	13.44	1	13.44	1	GLOR UNTE	WV 0 2
1121	LOAD X	11	24	13.44	21	13.44	22	GLOR UNTE	WV 0 2
1122	LOAD Y	11	24	13.44	1	13.44	1	GLOR UNTE	WV 0 2
1123	LOAD X	11	24	26.88	1	13.44	1	GLOR UNTE	WV 0 2
1124	LOAD Y	11	24	26.88	22	13.44	23	GLOR UNTE	WV 0 2
1125	LOAD X	11	24	26.88	1	13.44	1	GLOR UNTE	WV 0 2
1126	LOAD Y	11	24	0.00	03	13.44	03	GLOR UNTE	WV 0 2
1127	LOAD X	11	24	0.00	13	13.44	14	GLOR UNTE	WV 0 2
1128	LOAD Y	11	24	0.00	08	13.44	09	GLOR UNTE	WV 0 2
1129	LOAD X	13	24	15.44	03	13.44	03	GLOR UNTE	WV 0 2
1130	LOAD Y	13	24	13.44	14	13.44	15	GLOR UNTE	WV 0 2
1131	LOAD X	13	24	13.44	09	13.44	09	GLOR UNTE	WV 0 2
1132	LOAD Y	13	24	26.88	03	13.44	03	GLOR UNTE	WV 0 2
1133	LOAD X	13	24	26.88	15	13.44	16	GLOR UNTE	WV 0 2
1134	LOAD Y	13	24	26.88	09	13.44	10	GLOR UNTE	WV 0 2
1135	LOAD X	13	26	0.00	03	13.44	03	GLOR UNTE	WV 0 2
1136	LOAD Y	13	26	0.00	14	13.44	14	GLOR UNTE	WV 0 2
1137	LOAD X	13	26	0.00	07	13.44	07	GLOR UNTE	WV 0 2
1138	LOAD Y	13	26	13.44	03	13.44	03	GLOR UNTE	WV 0 2
1139	LOAD X	13	26	13.44	14	13.44	14	GLOR UNTE	WV 0 2
1140	LOAD Y	13	26	13.44	07	13.44	07	GLOR UNTE	WV 0 2
1141	LOAD X	13	26	26.88	03	13.44	03	GLOR UNTE	WV 0 2
1142	LOAD Y	13	26	26.88	14	13.44	14	GLOR UNTE	WV 0 2



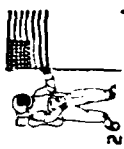
SEAL LOAD=2

LINE NO.	1	2	3	4	5	6	7	A			
1143	LOAD Z	13	26	26.48	07	13.44	07	GLOR UNTE	AV	0	2
1144	LOAD X	15	26	0.00	03	13.44	03	GLOR UNTE	AV	0	2
1145	LOAD Y	15	26	0.00	14	13.44	14	GLOR UNTE	AV	0	2
1146	LOAD Z	15	26	0.00	07	13.44	07	GLOR UNTE	AV	0	2
1147	LOAD X	15	26	13.44	03	13.44	03	GLOR UNTE	AV	0	2
1148	LOAD Y	15	26	13.44	14	13.44	14	GLOR UNTE	AV	0	2
1149	LOAD Z	15	26	13.44	07	13.44	07	GLOR UNTE	AV	0	2
1151	LOAD X	15	26	26.48	03	13.44	03	GLOR UNTE	AV	0	2
1151	LOAD Y	15	26	26.48	14	13.44	14	GLOR UNTE	AV	0	2
1152	LOAD Z	15	26	26.48	07	13.44	07	GLOR UNTE	AV	0	2
1153	LOAD X	15	22	0.00	03	13.44	03	GLOR UNTE	AV	0	2
1154	LOAD Y	15	22	0.00	14	13.44	14	GLOR UNTE	AV	0	2
1155	LOAD Z	15	22	0.00	07	13.44	07	GLOR UNTE	AV	0	2
1156	LOAD X	15	22	13.44	03	13.44	03	GLOR UNTE	AV	0	2
1157	LOAD Y	15	22	13.44	14	13.44	14	GLOR UNTE	AV	0	2
1158	LOAD Z	15	22	13.44	07	13.44	07	GLOR UNTE	AV	0	2
1159	LOAD X	15	22	26.48	09	13.44	09	GLOR UNTE	AV	0	2
1160	LOAD Y	15	22	26.48	15	13.44	15	GLOR UNTE	AV	0	2
1161	LOAD Z	15	22	26.48	09	13.44	09	GLOR UNTE	AV	0	2
1162	LOAD X	22	36	0.00	1	18.20	1	GLOR UNTE	AV	0	2
1163	LOAD Y	22	36	0.00	29	18.20	29	GLOR UNTE	AV	0	2
1164	LOAD Z	22	36	0.00	1	18.20	1	GLOR UNTE	AV	0	2
1165	LOAD X	22	36	18.20	1	18.20	1	GLOR UNTE	AV	0	2
1166	LOAD Y	22	36	18.20	31	18.20	31	GLOR UNTE	AV	0	2
1167	LOAD Z	22	36	18.20	1	18.20	1	GLOR UNTE	AV	0	2
1168	LOAD X	22	36	36.39	1	18.20	1	GLOR UNTE	AV	0	2
1169	LOAD Y	22	36	36.39	34	18.20	34	GLOR UNTE	AV	0	2
1170	LOAD Z	22	36	36.39	1	18.20	1	GLOR UNTE	AV	0	2
1171	LOAD X	24	38	0.00	09	20.96	09	GLOR UNTE	AV	0	2
1172	LOAD Y	24	38	0.00	12	20.96	12	GLOR UNTE	AV	0	2
1173	LOAD Z	24	38	0.00	11	20.96	11	GLOR UNTE	AV	0	2
1174	LOAD X	24	38	20.96	09	20.96	09	GLOR UNTE	AV	0	2
1175	LOAD Y	24	38	20.96	12	20.96	12	GLOR UNTE	AV	0	2
1176	LOAD Z	24	38	20.96	12	20.96	12	GLOR UNTE	AV	0	2
1177	LOAD X	24	38	41.93	09	20.96	09	GLOR UNTE	AV	0	2
1178	LOAD Y	24	38	41.93	12	20.96	12	GLOR UNTE	AV	0	2
1179	LOAD Z	24	38	41.93	12	20.96	11	GLOR UNTE	AV	0	2
1180	LOAD X	26	34	0.00	06	13.65	07	GLOR UNTE	AV	0	2
1181	LOAD Y	26	34	0.00	11	13.65	13	GLOR UNTE	AV	0	2
1182	LOAD Z	26	34	0.00	10	13.65	11	GLOR UNTE	AV	0	2
1183	LOAD X	26	34	13.65	07	13.65	08	GLOR UNTE	AV	0	2
1184	LOAD Y	26	34	13.65	13	13.65	14	GLOR UNTE	AV	0	2
1185	LOAD Z	26	34	13.65	11	13.65	13	GLOR UNTE	AV	0	2
1186	LOAD X	26	34	27.29	08	13.65	09	GLOR UNTE	AV	0	2
1187	LOAD Y	26	34	27.29	14	13.65	16	GLOR UNTE	AV	0	2
1188	LOAD Z	26	34	27.29	13	13.65	14	GLOR UNTE	AV	0	2
1189	LOAD X	26	34	40.00	09	13.65	10	GLOR UNTE	AV	0	2
1190	LOAD Y	26	34	40.00	16	13.65	16	GLOR UNTE	AV	0	2
1191	LOAD Z	26	34	40.00	14	13.65	16	GLOR UNTE	AV	0	2
1192	LOAD X	34	49	0.00	02	11.24	02	GLOR UNTE	AV	0	2



SEALING-2

LINE NO.	1	2	3	4	5	6	7	8	
1193	LOAD Y	34	49	0.00	34	11.46	42	GLOR UNIT	WV 0 2
1194	LOAD X	34	49	0.00	1	11.46	02	GLOR UNIT	WV 0 2
1195	LOAD X	34	49	11.46	02	11.46	02	GLOR UNIT	WV 0 2
1196	LOAD Y	34	49	11.46	42	11.46	44	GLOR UNIT	WV 0 2
1197	LOAD X	34	49	11.46	02	11.46	02	GLOR UNIT	WV 0 2
1198	LOAD X	34	49	23.72	02	11.46	02	GLOR UNIT	WV 0 2
1199	LOAD Y	34	49	23.72	44	11.46	53	GLOR UNIT	WV 0 2
1200	LOAD Z	34	49	23.72	02	11.46	02	GLOR UNIT	WV 0 2
1201	LOAD X	34	49	35.58	02	11.46	02	GLOR UNIT	WV 0 2
1202	LOAD X	34	49	35.58	53	11.46	00	GLOR UNIT	WV 0 2
1203	LOAD Z	34	49	35.58	02	11.46	02	GLOR UNIT	WV 0 2
1204	LOAD X	34	51	0.00	06	9.29	07	GLOR UNIT	WV 0 2
1205	LOAD Y	34	51	0.00	11	9.29	13	GLOR UNIT	WV 0 2
1206	LOAD Z	34	51	0.00	13	9.29	15	GLOR UNIT	WV 0 2
1207	LOAD X	34	51	9.29	07	9.29	04	GLOR UNIT	WV 0 2
1208	LOAD Y	34	51	9.29	13	9.29	15	GLOR UNIT	WV 0 2
1209	LOAD Z	34	51	9.29	15	9.29	17	GLOR UNIT	WV 0 2
1210	LOAD X	34	51	18.57	04	9.29	06	GLOR UNIT	WV 0 2
1211	LOAD Y	34	51	18.57	15	9.29	17	GLOR UNIT	WV 0 2
1212	LOAD Z	34	51	18.57	17	9.29	19	GLOR UNIT	WV 0 2
1213	LOAD X	34	51	27.46	09	9.29	10	GLOR UNIT	WV 0 2
1214	LOAD Y	34	51	27.46	17	9.29	19	GLOR UNIT	WV 0 2
1215	LOAD Z	34	51	27.46	19	9.29	21	GLOR UNIT	WV 0 2
1216	LOAD X	34	51	37.14	10	9.29	11	GLOR UNIT	WV 0 2
1217	LOAD Y	34	51	37.14	19	9.29	22	GLOR UNIT	WV 0 2
1218	LOAD Z	34	51	37.14	21	9.29	24	GLOR UNIT	WV 0 2
1219	LOAD X	34	51	46.43	11	9.29	13	GLOR UNIT	WV 0 2
1220	LOAD Y	34	51	46.43	22	9.29	24	GLOR UNIT	WV 0 2
1221	LOAD Z	34	51	46.43	24	9.29	27	GLOR UNIT	WV 0 2
1222	LOAD X	34	53	0.00	10	15.81	11	GLOR UNIT	WV 0 2
1223	LOAD Y	34	53	0.00	24	15.81	27	GLOR UNIT	WV 0 2
1224	LOAD Z	34	53	0.00	16	15.81	17	GLOR UNIT	WV 0 2
1225	LOAD X	34	53	15.81	11	15.81	12	GLOR UNIT	WV 0 2
1226	LOAD Y	34	53	15.81	27	15.81	30	GLOR UNIT	WV 0 2
1227	LOAD Z	34	53	15.81	17	15.81	20	GLOR UNIT	WV 0 2
1228	LOAD X	34	53	31.62	12	15.81	13	GLOR UNIT	WV 0 2
1229	LOAD Y	34	53	31.62	30	15.81	33	GLOR UNIT	WV 0 2
1230	LOAD Z	34	53	31.62	20	15.81	22	GLOR UNIT	WV 0 2
1231	LOAD X	55	58	0.00	117	5.70	130	GLOR UNIT	WV 0 2
1232	LOAD Y	55	58	5.70	150	5.70	146	GLOR UNIT	WV 0 2
1233	LOAD Z	55	58	11.40	144	5.70	143	GLOR UNIT	WV 0 2
1234	LOAD X	55	58	17.10	163	5.70	145	GLOR UNIT	WV 0 2
1235	LOAD Y	55	58	22.80	185	5.70	210	GLOR UNIT	WV 0 2
1236	LOAD Z	55	61	0.00	210	5.97	229	GLOR UNIT	WV 0 2
1237	LOAD X	55	61	3.97	229	3.97	248	GLOR UNIT	WV 0 2
1238	LOAD Y	55	61	7.95	248	3.97	275	GLOR UNIT	WV 0 2
1239	LOAD Z	55	61	0.00	117	5.70	130	GLOR UNIT	WV 0 2
1240	LOAD X	56	59	5.70	150	5.70	146	GLOR UNIT	WV 0 2
1241	LOAD Y	56	59	11.40	146	5.70	143	GLOR UNIT	WV 0 2
1242	LOAD Z	56	59	17.10	163	5.70	145	GLOR UNIT	WV 0 2



SEALING

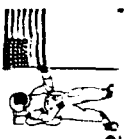
LINE NO.	1	2	3	4	5	6	7	8	
1243	LOAD V	54	50	22.80	185	5.70	210	GLOR UNTE	AV 0 2
1244	LOAD V	50	64	0.00	210	3.97	220	GLOR UNTE	AV 0 2
1245	LOAD V	50	60	3.97	220	3.97	248	GLOR UNTE	AV 0 2
1246	LOAD V	59	60	7.95	248	3.97	275	GLOR UNTE	AV 0 2
1247	LOAD V	57	60	0.00	104	5.70	114	GLOR UNTE	AV 0 2
1248	LOAD V	57	60	5.70	114	5.70	120	GLOR UNTE	AV 0 2
1249	LOAD V	57	60	11.40	120	5.70	144	GLOR UNTE	AV 0 2
1250	LOAD V	57	60	17.10	144	5.70	163	GLOR UNTE	AV 0 2
1251	LOAD V	57	60	22.80	163	5.70	183	GLOR UNTE	AV 0 2
1252	LOAD V	60	70	0.00	183	2.00	192	GLOR UNTE	AV 0 2
1253	LOAD V	60	70	2.00	192	2.00	201	GLOR UNTE	AV 0 2
1254	LOAD V	60	70	4.00	201	2.00	209	GLOR UNTE	AV 0 2
1255	LOAD V	70	67	0.00	209	1.35	215	GLOR UNTE	AV 0 2
1256	LOAD V	70	67	1.35	215	1.35	223	GLOR UNTE	AV 0 2
1257	LOAD V	70	67	2.71	223	1.35	231	GLOR UNTE	AV 0 2
1258	LOAD V	58	59	0.00	74	9.67	74	GLOR UNTE	AV 0 2
1259	LOAD V	58	59	9.67	74	9.67	74	GLOR UNTE	AV 0 2
1260	LOAD V	58	59	19.33	74	9.67	74	GLOR UNTE	AV 0 2
1261	LOAD V	50	60	0.00	32	9.67	31	GLOR UNTE	AV 0 2
1262	LOAD V	50	60	0.00	31	9.67	18	GLOR UNTE	AV 0 2
1263	LOAD V	59	60	9.67	31	9.67	30	GLOR UNTE	AV 0 2
1264	LOAD V	50	60	9.67	18	9.67	17	GLOR UNTE	AV 0 2
1265	LOAD V	50	60	19.33	30	9.67	28	GLOR UNTE	AV 0 2
1266	LOAD V	50	60	19.33	17	9.67	16	GLOR UNTE	AV 0 2
1267	LOAD V	60	58	0.00	28	9.67	30	GLOR UNTE	AV 0 2
1268	LOAD V	60	58	0.00	16	9.67	17	GLOR UNTE	AV 0 2
1269	LOAD V	60	58	9.67	30	9.67	31	GLOR UNTE	AV 0 2
1270	LOAD V	60	58	9.67	17	9.67	18	GLOR UNTE	AV 0 2
1271	LOAD V	60	58	19.33	31	9.67	32	GLOR UNTE	AV 0 2
1272	LOAD V	60	58	19.33	18	9.67	10	GLOR UNTE	AV 0 2
1273	LOAD V	59	61	0.00	74	8.65	61	GLOR UNTE	AV 0 2
1274	LOAD V	59	61	8.65	81	8.65	88	GLOR UNTE	AV 0 2
1275	LOAD V	60	64	0.00	88	8.65	97	GLOR UNTE	AV 0 2
1276	LOAD V	60	64	0.00	22	6.25	25	GLOR UNTE	AV 0 2
1277	LOAD V	60	64	0.00	26	6.25	29	GLOR UNTE	AV 0 2
1278	LOAD V	60	64	0.00	23	6.25	25	GLOR UNTE	AV 0 2
1279	LOAD V	60	64	6.25	25	6.25	27	GLOR UNTE	AV 0 2
1280	LOAD V	60	64	6.25	29	6.25	32	GLOR UNTE	AV 0 2
1281	LOAD Z	60	64	5.25	25	6.25	28	GLOR UNTE	AV 0 2
1282	LOAD Z	60	64	12.49	27	6.25	30	GLOR UNTE	AV 0 2
1283	LOAD V	60	60	12.49	32	6.25	34	GLOR UNTE	AV 0 2
1284	LOAD Z	60	64	12.49	28	6.25	31	GLOR UNTE	AV 0 2
1285	LOAD X	60	64	18.74	30	6.25	33	GLOR UNTE	AV 0 2
1286	LOAD Y	60	64	18.74	36	6.25	50	GLOR UNTE	AV 0 2
1287	LOAD Z	60	64	18.74	31	6.25	50	GLOR UNTE	AV 0 2
1288	LOAD X	58	67	0.00	25	7.69	27	GLOR UNTE	AV 0 2
1289	LOAD Y	58	67	0.00	50	7.69	52	GLOR UNTE	AV 0 2
1290	LOAD Z	58	67	0.00	26	7.69	28	GLOR UNTE	AV 0 2
1291	LOAD X	58	67	7.69	27	7.69	28	GLOR UNTE	AV 0 2
1292	LOAD Y	58	67	7.69	32	7.69	34	GLOR UNTE	AV 0 2



SPACED=2

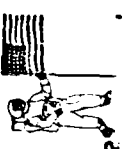
LINE NO. 1 2 3 4 5 6 7 A

1293	LOAD Z	58	67	7,490	2A	7,49	29	GLOR UNITF	AV	0	2
1294	LOAD X	5A	67	15,34	2A	7,49	30	GLOR UNITF	AV	0	2
1295	LOAD Y	5A	67	15,34	3A	7,49	34	GLOR UNITF	AV	0	2
1296	LOAD Z	5A	67	15,34	20	7,49	51	GLOR UNITF	AV	0	2
1297	LOAD Y	70	66	2,02	3A	2,02	40	GLOR UNITF	AV	0	2
1298	LOAD Y	70	66	2,02	40	2,02	43	GLOR UNITF	AV	0	2
1299	LOAD Y	70	66	2,02	41	2,02	43	GLOR UNITF	AV	0	2
1300	LOAD Y	70	66	2,02	3A	2,02	40	GLOR UNITF	AV	0	2
1301	LOAD Y	70	66	2,02	40	2,02	41	GLOR UNITF	AV	0	2
1302	LOAD Y	70	66	2,02	41	2,02	43	GLOR UNITF	AV	0	2
1303	LOADCN	3									
1304	LOAD Z	1	4	0,00	557	6,06	557	GLOR UNITF	DL	0	3
1305	LOAD Z	4	16	0,00	557	32,44	557	GLOR UNITF	DL	0	3
1306	LOAD Z	16	28	0,00	403	32,44	403	GLOR UNITF	DL	0	3
1307	LOAD Z	28	43	0,00	403	32,44	403	GLOR UNITF	DL	0	3
1308	LOAD Z	43	55	0,00	403	4,59	403	GLOR UNITF	DL	0	3
1309	LOAD Z	2	5	0,00	557	6,06	557	GLOR UNITF	DL	0	3
1310	LOAD Z	5	17	0,00	557	32,44	557	GLOR UNITF	DL	0	3
1311	LOAD Z	17	29	0,00	403	32,44	403	GLOR UNITF	DL	0	3
1312	LOAD Z	29	40	0,00	403	32,44	403	GLOR UNITF	DL	0	3
1313	LOAD Z	40	56	0,00	403	4,59	403	GLOR UNITF	DL	0	3
1314	LOAD Z	3	6	0,00	557	6,06	557	GLOR UNITF	DL	0	3
1315	LOAD Z	6	18	0,00	557	32,44	557	GLOR UNITF	DL	0	3
1316	LOAD Z	18	30	0,00	403	32,44	403	GLOR UNITF	DL	0	3
1317	LOAD Z	30	45	0,00	403	36,13	403	GLOR UNITF	DL	0	3
1318	LOAD Z	45	57	0,00	403	4,58	403	GLOR UNITF	DL	0	3
1319	LOAD Z	10	22	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1320	LOAD Z	22	34	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1321	LOAD Z	34	40	0,00	371	14,14	371	GLOR UNITF	DL	0	3
1322	LOAD Z	40	49	0,00	371	18,26	371	GLOR UNITF	DL	0	3
1323	LOAD Z	49	55	0,00	371	4,56	371	GLOR UNITF	DL	0	3
1324	LOAD Z	12	20	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1325	LOAD Z	20	36	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1326	LOAD Z	36	41	0,00	371	14,14	371	GLOR UNITF	DL	0	3
1327	LOAD Z	41	51	0,00	371	18,26	371	GLOR UNITF	DL	0	3
1328	LOAD Z	51	56	0,00	371	4,56	371	GLOR UNITF	DL	0	3
1329	LOAD Z	14	26	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1330	LOAD Z	26	38	0,00	143	32,44	143	GLOR UNITF	DL	0	3
1331	LOAD Z	38	42	0,00	371	15,03	371	GLOR UNITF	DL	0	3
1332	LOAD Z	42	53	0,00	371	21,26	371	GLOR UNITF	DL	0	3
1333	LOAD Z	53	57	0,00	371	4,56	371	GLOR UNITF	DL	0	3
1334	LOAD Z	10	11	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1335	LOAD Z	11	12	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1336	LOAD Z	12	13	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1337	LOAD Z	13	14	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1338	LOAD Z	14	15	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1339	LOAD Z	15	16	1,71	041	25,58	041	GLOR UNITF	DL	0	3
1340	LOAD Z	11	13	1,41	047	26,17	047	GLOR UNITF	DL	0	3
1341	LOAD Z	13	15	1,41	047	26,17	047	GLOR UNITF	DL	0	3
1342	LOAD Z	15	11	1,41	047	26,17	047	GLOR UNITF	DL	0	3



SEAL 100-2

LINE NO.	1	2	3	4	5	6	7	8
1343	LOAD Z	22	23	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1344	LOAD Z	23	24	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1345	LOAD Z	24	25	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1346	LOAD Z	25	26	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1347	LOAD Z	26	27	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1348	LOAD Z	27	28	1.71	-.041	20.96	GLOR UNITF	DL 0 3
1349	LOAD Z	28	29	1.71	-.047	21.55	GLOR UNITF	DL 0 3
1350	LOAD Z	29	30	1.71	-.047	21.55	GLOR UNITF	DL 0 3
1351	LOAD Z	30	31	1.71	-.047	21.55	GLOR UNITF	DL 0 3
1352	LOAD Z	31	32	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1353	LOAD Z	32	33	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1354	LOAD Z	33	34	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1355	LOAD Z	34	35	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1356	LOAD Z	35	36	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1357	LOAD Z	36	37	1.71	-.057	16.35	GLOR UNITF	DL 0 3
1358	LOAD Z	37	38	1.71	-.043	16.35	GLOR UNITF	DL 0 3
1359	LOAD Z	38	39	1.71	-.043	16.35	GLOR UNITF	DL 0 3
1360	LOAD Z	39	40	1.71	-.043	16.35	GLOR UNITF	DL 0 3
1361	LOAD Z	40	41	1.71	-.072	11.73	GLOR UNITF	DL 0 3
1362	LOAD Z	41	42	1.71	-.072	11.73	GLOR UNITF	DL 0 3
1363	LOAD Z	42	43	1.71	-.072	11.73	GLOR UNITF	DL 0 3
1364	LOAD Z	43	44	1.71	-.072	11.73	GLOR UNITF	DL 0 3
1365	LOAD Z	44	45	1.71	-.072	11.73	GLOR UNITF	DL 0 3
1366	LOAD Z	45	46	1.71	-.057	11.73	GLOR UNITF	DL 0 3
1367	LOAD Z	46	47	1.71	-.057	11.73	GLOR UNITF	DL 0 3
1368	LOAD Z	47	48	1.71	-.057	11.73	GLOR UNITF	DL 0 3
1369	LOAD Z	48	49	1.71	-.057	11.73	GLOR UNITF	DL 0 3
1370	LOAD Z	49	50	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1371	LOAD Z	50	51	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1372	LOAD Z	51	52	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1373	LOAD Z	52	53	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1374	LOAD Z	53	54	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1375	LOAD Z	54	55	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1376	LOAD Z	55	56	1.71	-.072	36.90	GLOR UNITF	DL 0 3
1377	LOAD Z	56	57	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1378	LOAD Z	57	58	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1379	LOAD Z	58	59	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1380	LOAD Z	59	60	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1381	LOAD Z	60	61	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1382	LOAD Z	61	62	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1383	LOAD Z	62	63	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1384	LOAD Z	63	64	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1385	LOAD Z	64	65	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1386	LOAD Z	65	66	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1387	LOAD Z	66	67	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1388	LOAD Z	67	68	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1389	LOAD Z	68	69	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1390	LOAD Z	69	70	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1391	LOAD Z	70	71	2.42	-.112	49.76	GLOR UNITF	DL 0 3
1392	LOAD Z	71	72	2.42	-.112	49.76	GLOR UNITF	DL 0 3



SEALING-2

LINE NO.	1	2	3	4	5	6	7	8
1393	LOAD Z	21	24	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1394	LOAD Z	28	31	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1395	LOAD Z	31	34	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1396	LOAD Z	29	32	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1397	LOAD Z	32	36	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1398	LOAD Z	30	33	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1399	LOAD Z	34	34	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1400	LOAD Z	43	46	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1401	LOAD Z	44	49	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1402	LOAD Z	44	47	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1403	LOAD Z	47	51	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1404	LOAD Z	45	48	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1405	LOAD Z	48	53	0.00	0.148	2.50	GLOR UNITF	DL 0 3
1406	LOAD Z	55	58	0.00	0.403	23.00	GLOR UNITF	DL 0 3
1407	LOAD Z	55	58	23.00	0.464	5.50	GLOR UNITF	DL 0 3
1408	LOAD Z	54	61	0.00	0.464	15.00	GLOR UNITF	DL 0 3
1409	LOAD Z	61	71	0.00	0.464	15.00	GLOR UNITF	DL 0 3
1410	LOAD Z	56	59	0.00	0.403	23.00	GLOR UNITF	DL 0 3
1411	LOAD Z	56	59	23.00	0.464	5.50	GLOR UNITF	DL 0 3
1412	LOAD Z	50	60	0.00	0.464	15.00	GLOR UNITF	DL 0 3
1413	LOAD Z	64	72	0.00	0.464	15.00	GLOR UNITF	DL 0 3
1414	LOAD Z	57	60	0.00	0.403	23.00	GLOR UNITF	DL 0 3
1415	LOAD Z	57	60	23.00	0.464	5.50	GLOR UNITF	DL 0 3
1416	LOAD Z	60	70	0.00	0.464	6.00	GLOR UNITF	DL 0 3
1417	LOAD Z	70	67	0.00	0.464	9.00	GLOR UNITF	DL 0 3
1418	LOAD Z	67	76	0.00	0.464	4.00	GLOR UNITF	DL 0 3
1419	LOAD Z	76	75	0.00	0.464	11.00	GLOR UNITF	DL 0 3
1420	LOAD Z	58	50	1.71	0.065	25.58	GLOR UNITF	DL 0 3
1421	LOAD Z	59	60	1.71	0.065	25.58	GLOR UNITF	DL 0 3
1422	LOAD Z	60	58	1.71	0.065	25.58	GLOR UNITF	DL 0 3
1423	LOAD Z	59	61	1.71	0.065	29.23	GLOR UNITF	DL 0 3
1424	LOAD Z	60	64	1.71	0.065	29.23	GLOR UNITF	DL 0 3
1425	LOAD Z	58	67	1.71	0.065	29.23	GLOR UNITF	DL 0 3
1426	LOAD Z	70	66	1.59	0.019	10.27	GLOR UNITF	DL 0 3
1427	LOAD Z	70	68	1.59	0.019	10.27	GLOR UNITF	DL 0 3
1428	LOAD Z	76	77	1.71	0.050	14.78	GLOR UNITF	DL 0 3
1429	LOAD Z	74	78	1.71	0.050	14.78	GLOR UNITF	DL 0 3
1430	LOAD Z	61	62	0.00	0.055	4.50	GLOR UNITF	DL 0 3
1431	LOAD Z	62	63	0.00	0.055	20.00	GLOR UNITF	DL 0 3
1432	LOAD Z	63	64	0.00	0.055	4.50	GLOR UNITF	DL 0 3
1433	LOAD Z	64	65	0.00	0.055	8.75	GLOR UNITF	DL 0 3
1434	LOAD Z	65	67	0.00	0.055	20.25	GLOR UNITF	DL 0 3
1435	LOAD Z	67	69	0.00	0.055	20.25	GLOR UNITF	DL 0 3
1436	LOAD Z	69	61	0.00	0.055	8.75	GLOR UNITF	DL 0 3
1437	LOAD Z	63	65	0.00	0.024	7.50	GLOR UNITF	DL 0 3
1438	LOAD Z	65	66	0.00	0.024	17.61	GLOR UNITF	DL 0 3
1439	LOAD Z	66	67	0.00	0.024	10.00	GLOR UNITF	DL 0 3
1440	LOAD Z	67	68	0.00	0.024	10.00	GLOR UNITF	DL 0 3
1441	LOAD Z	68	69	0.00	0.024	17.61	GLOR UNITF	DL 0 3
1442	LOAD Z	69	62	0.00	0.024	7.50	GLOR UNITF	DL 0 3



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LINE NO.	1	2	3	4	5	6	7	8
1443	LOAD Z	71	73	0.00	-.055	3.00	-.055	DL 0 3
1444	LOAD Z	71	72	0.00	-.055	29.00	-.055	GLOR UNTF
1445	LOAD Z	72	74	0.00	-.055	3.00	-.055	DL 0 3
1446	LOAD Z	71	81	0.00	-.055	5.00	-.055	GLOR UNTF
1447	LOAD Z	71	77	0.00	-.055	25.11	-.055	DL 0 3
1448	LOAD Z	77	83	0.00	-.055	5.00	-.055	GLOR UNTF
1449	LOAD Z	72	82	0.00	-.055	5.00	-.055	DL 0 3
1450	LOAD Z	72	78	0.00	-.055	25.11	-.055	GLOR UNTF
1451	LOAD Z	78	84	0.00	-.055	5.00	-.055	DL 0 3
1452	LOAD Z	77	79	0.00	-.055	3.00	-.055	GLOR UNTF
1453	LOAD Z	77	75	0.00	-.055	14.50	-.055	DL 0 3
1454	LOAD Z	75	78	0.00	-.055	14.50	-.055	GLOR UNTF
1455	LOAD Z	78	80	0.00	-.055	3.00	-.055	DL 0 3
1456	LOAD Z	71	75	0.00	-.016	29.00	-.016	GLOR UNTF
1457	LOAD Z	72	75	0.00	-.016	29.00	-.016	DL 0 3
1458	END							

NO. OF WARNING ERRORS = 67

NO. OF FATAL ERRORS = 0

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 1 JSE 1 JES 4

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 2 JSE 4 JES 16

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 3 JSE 16 JES 28

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 4 JSE 28 JES 43

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 5 JSE 43 JES 55

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 6 JSE 2 JES 5

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 7 JSE 5 JES 17

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 8 JSE 17 JES 29

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 9 JSE 29 JES 44

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 10 JSE 44 JES 56

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.



MEMBERS 11 JSE 3 JES 4

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 12 JSE 6 JES 18

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 13 JSE 18 JES 60

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 14 JSE 30 JES 45

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 15 JSE 45 JES 57

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 19 JSE 4 JES 7

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 20 JSE 7 JES 10

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 21 JSE 5 JES 8

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 22 JSE 8 JES 12

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 23 JSE 6 JES 9

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 24 JSE 9 JES 14

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 25 JSE 14 JES 19

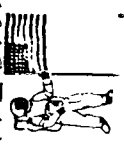
*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 26 JSE 19 JES 22

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBERS 27 JSE 17 JES 20

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.



*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 88 JSB 20 JEB 24

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 89 JSB 18 JEB 21

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 90 JSB 21 JEB 26

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 91 JSB 28 JEB 31

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 92 JSB 31 JEB 34

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 93 JSB 29 JEB 32

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 94 JSB 32 JEB 36

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 95 JSB 30 JEB 33

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 96 JSB 33 JEB 38

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 97 JSB 43 JEB 46

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 98 JSB 46 JEB 49

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 99 JSB 44 JEB 47

*** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.
 MEMBERS 100 JSB 47 JEB 51



MEMBER 101 JS= 45 JF= 48
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 102 JS= 48 JF= 51
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 124 JS= 61 JF= 62
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 125 JS= 62 JF= 63
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 126 JS= 63 JF= 64
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 127 JS= 64 JF= 65
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 128 JS= 65 JF= 67
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 129 JS= 67 JF= 69
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 130 JS= 69 JF= 61
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 131 JS= 63 JF= 65
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 132 JS= 65 JF= 66
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 133 JS= 66 JF= 67
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 134 JS= 67 JF= 68
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 135 JS= 66 JF= 67
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.



MEMBER 135 JS# 69 JF# 69
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 136 JS# 69 JF# 62
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 137 JS# 71 JF# 73
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 138 JS# 71 JF# 72
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 139 JS# 72 JF# 74
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 140 JS# 71 JF# 81
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 141 JS# 71 JF# 77
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 142 JS# 77 JF# 83
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

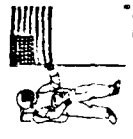
MEMBER 143 JS# 72 JF# 82
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 144 JS# 72 JF# 78
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 145 JS# 78 JF# 80
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 146 JS# 77 JF# 79
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 147 JS# 77 JF# 75
 *** WARNING NO. SL. 7 ***
 THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.



MEMBER 148 JSB 75 IFE 7A

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 149 JSB 7A JFB 40

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 150 JSB 71 JFB 75

*** WARNING NO. SL. 7 ***
THE MEMBER BELOW HAS A DIAMETER = 0 AND HAS BEEN SKIPPED.

MEMBER 151 JSB 72 IFE 75

AD-A164 421

STRUCTURAL CONCEPT ANALYSIS REPORT FOR THE EAST COAST
AIR COMBAT MANEUVER. (U) CREST ENGINEERING INC TULSA OK
MAY 76 27-771-92-APP-C CHES/NAVFAC-FPO-7601-APP-C
N62477-76-C-0179

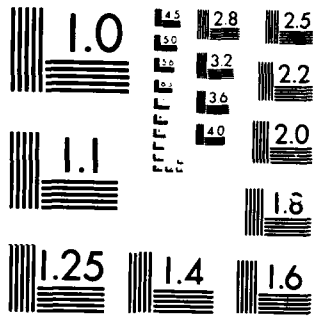
6/7

UNCLASSIFIED

F/G 13/13

NL

The table consists of 10 columns and 10 rows. The top row contains 10 blacked-out cells. The remaining 9 rows each contain 9 blacked-out cells, with the first cell in each row being empty. This layout suggests a table with 10 columns and 10 rows, where the top row and the first column (excluding the top cell) are redacted.



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A



JVJZCF. 04/26/76. UNLIMITED COMPUTING AT 7. 0000/51. H.0.25

17.16.55	SEALOAD.CM100.7500.PT.				
17.16.50	SL AU	0.000			
17.16.50	SAC3000CAR0025.2777100CC 3H				
17.16.50	04/26/76.JVJZCF				
17.16.51	FL 3302	0.001			
17.16.51	GET.TAPE26=SPFILE(THRARY)				
17.16.52	READY = SPFILE				
17.16.52	GET.SL2(THRARY)				
17.17.02	READY = SL2				
17.17.02	WFL130000				
17.17.02	FL 4096	0.001	0	0.	
17.17.02	SL 934	2			
17.17.02	SL2				
17.17.02	FLS 45056	0.001			
17.17.04	SLA 45056	0.400	413	16	
17.17.04	FL REQUIRED TO LOAD		73660R	(30640)	
17.17.04	FL REQUIRED TO EXECUTE		63600R	(26496)	
17.17.05	FL 45056	0.400			
17.17.06	SSC SSL2 START SEALOAD				
17.17.32	SSC SSL2 STMP SEALOAD				
17.17.32	STUP				
17.17.32	SSH* 45056	10.514	2015	177.	
17.17.32	SL 30	2			
17.17.32	REPLACE.TAPE9=8771C1.				
17.17.34	READY = 8771C1				
17.17.34	CONST.				
17.17.34	FL 4096	10.514	0	0.	
17.17.34	SL 208	1			
17.17.35	SERVICE UNITS=	46.2			
17.17.35	JOB COSTER	11.55			
17.17.35	FL 1228	10.537	9	5	
17.17.35	EXIT.				
17.17.35	JT00 2368	10.537			
17.17.35	FL* CPU SEC.				
17.17.35	PRUS*P.F. ACC				
17.17.35	PRUS* TAPE ACC				

A-5 SPACE FRAME ANALYSIS



 * STHAAL
 * A SYMFEROM TECHNOLOGY, INC. DEVELOPMENT *
 * RELEASE 6 1100 12 *
 * MARCH 1976 *

DATE 04/27/76

30PTLE ADMR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHEEN

PROGRAM OPTIONS

THE FOLLOWING OPTIONS HAVE BEEN REQUESTED FOR THIS ANALYSIS.

INPUTCARD PLUS DATA FILE INPUT

INPUT UNITSENGLISH

OUTPUT UNITSENGLISH

EXECUTIONUNITY CHECK
UNITY CHECKS COMPUTED BY AMERICAN INSTITUTE OF
 STEEL CONSTRUCTION 1969 CODE, SECTIONS 1.5, 1.6,
 LOCAL BUCKLING STRESS OF TUBULAR MEMBERS INVE-
 TIGATED BY COLUMN RESEARCH COUNCIL METHOD.
 RESULTS INVALID FOR A514 STEEL.

.....NO. OF SEGMENTS 1
VARBL MEMR, SEGMENTS/SECT 1

LOADNO. BASIC LOAD CONDS. 6
NO. COMBINED LOAD CONDS. 2

REPORTTABUL FCHL AND GROUP PRIP PRINT
JOINT DEFLECTIONS PRINT
GROUP AND UN CHK SUMMARY PRINT
MEMBER STRESS REPORT NO. 1 PRINT
MEMBER STRESS REPORT NO. 2 PRINT
MEMBER STRESS REPORT NO. 3 PRINT
REACTION FORCES AND MOMTS PRINT
EQUILIBRIUM CHECK PRINT

EQUILIBRIUM CHECK POST VALUES
FORCES 100.00 LR
MOMENTS 100.00 IN-LB



COMPUTER PRINT

PAGE 1
DATE 04/27/76

JOINT AND STRUCTURE ANALYSIS (SHEET PLATED BULGING) - C. P. HERR
TENSILE STRENGTH OF WELD DISCONTINUITIES

GRP	M/S	JOINT THICK IN.	WT IN.	ND IN.	AX T.P.	TX IN.	IV IN.	IZ IN.	FY PSI	KV	KZ	SHEAR AREA IN ²	INPUT SEC LFN FT.
*** E = 29000000.0 PSI, G = 11600000.0 PSI ***													
P10	1	0.00	1.750	36.00	144.30	55360.00	27683.00	27683.00	36.0	1.0	1.0	188.30	-0.00
P20	1	0.00	1.250	36.00	136.46	41250.28	20625.14	20625.14	36.0	1.0	1.0	136.46	-0.00
JL1	1	0.00	1.500	40.00	62.05	24205.92	12102.96	12102.96	36.0	1.0	1.0	62.05	-0.00
JL2	1	0.00	1.000	41.00	125.04	50297.02	25148.51	25148.51	36.0	1.0	1.0	125.04	-0.00
AR1	2	4.83	0.625	21.00	58.00	3574.04	1787.02	1787.02	36.0	0.8	0.8	38.04	-0.00
AR2	2	3.42	0.500	14.00	27.49	2106.32	1053.16	1053.16	36.0	0.8	0.8	27.49	-0.00
AR3	2	3.42	0.375	14.00	24.55	1463.86	731.93	731.93	36.0	0.8	0.8	24.55	-0.00
AR4	2	2.83	0.500	14.00	16.05	745.60	372.80	372.80	36.0	0.8	0.8	16.05	-0.00
AR5	2	3.42	0.500	12.75	19.24	723.28	361.64	361.64	36.0	0.8	0.8	19.24	-0.00
AR6	2	3.42	0.375	12.75	14.54	548.42	274.21	274.21	36.0	0.8	0.8	14.54	-0.00
AR7	2	3.18	0.240	6.63	5.58	54.30	28.15	28.15	36.0	0.8	0.8	5.58	-0.00
STL	1	0.00	1.250	36.00	136.46	41250.28	20625.14	20625.14	36.0	1.0	1.0	136.46	-0.00

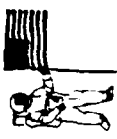


STRASS - GROUP PROPERTIES REPORT

PAGE 2
DATE 04/27/74

3-PILE ACHD STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHEMERN
WIDE FLANGE/WIDE FLANGE COMPACT MEMBER PROPERTIES

GRP	W/S	JOINT THICK FT.	FLANGE THICK IN.		FLANGE WIDTH IN.		WEB THICK IN.	RADIUS IN.		DEPTH IN.	AX IN2	IX IN4	IV IN4	IZ IN4	FY KSI	KZ	IB FT.	SEC LEN FT.	INPUT
			IN.	IN.	IN.	IN.													
*** E = 29000000.0 PSI, G = 11600000.0 PSI ***																			
W1A	1	0.00	.570	.358	7.50	.500	18.00	16.20	1.25	802.00	40.20	36.0	1.0	1.0	1.0	1.0	.01	0.00	
W08	1	0.00	.398	.245	6.50	.500	7.93	7.06	.34	62.50	18.20	36.0	1.0	1.0	1.0	1.0	.01	0.00	
W06	1	0.00	.269	.255	6.00	.500	6.00	4.56	.11	30.10	9.67	36.0	1.0	1.0	1.0	1.0	.01	0.00	



STRAUSS - GROUP PROPERTIES REPORT

PAGE 3
DATE 08/27/76

3-PILE ACWR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- P.C.M.H.M.
PHYSIC SECTION MEMBERS

GRP	W/S	JOINT THICK FT.	Z-DPTH IN.	V-DPTH IN.	AX IN2	IX IN4	IY IN4	IZ IN4	KY KSI	KZ	INPUT SEC LEN FT.
WRN	2	0.00	10.00	5.00	50.00	30000.00	30000.00	30000.00	36.0	1.0	0.00

*** E = 29000000.0 PSI, G = 11600000.0 PSI ***



STATE OUTPUT DATA

TOPIF ACMR STRUCTURE -- U.S. NAVY (SABIT), DIAMETER PILING) -- C. CHERN

LINE NO. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49

LINE NO.	DESCRIPTION	QTY	UNIT	PRICE	TOTAL	DATE	STATUS
1	SFCT PILING1	TUR	18830	5536000	2768300	2768300	3600 1750
2	SFCT PILING2	TUR	13646	4125028	2062514	2062514	3600 1250
3	SFCT JKTIFG1	TUR	6205	2420592	1210296	1210296	4000 500
4	SFCT JKTIFG2	TUR	12566	5029702	2514851	2514851	4100 1000
5	SFCT RHAFCS1	TUR	3804	357808	178704	178704	2000 625
6	SFCT RHAFCS2	TUR	2749	210432	105316	105316	1800 500
7	SFCT RHAFCS3	TUR	2435	196386	73193	73193	1600 500
8	SFCT RHAFCS4	TUR	1605	70560	37280	37280	1400 375
9	SFCT RHAFCS5	TUR	1924	72328	36164	36164	1275 500
10	SFCT RHAFCS6	TUR	1458	55892	27941	27941	1275 375
11	SFCT RHAFCS7	TUR	558	2815	2815	2815	6.625 280
12	SFCT WTSWHIN	PRY	5000	3000000	3000000	3000000	1000
13	SFCT SUSTLEG	TUR	13646	4125028	2062514	2062514	3600 1250
14	SFCT WXP24	WFC	1620	125	80200	80200	750 570
15	SFCT WXP24	WFC	706	34	8250	1820	650 398
16	SFCT WXP24	WFC	456	11	3010	967	600 269
17	GRUP P10	PILING1	3600	1750	2900	1160	3600 1
18	GRUP P20	PILING2	3600	1250	2900	1160	3600 1
19	GRUP J11	JKTIFG1	4000	500	2900	1160	3600 1
20	GRUP J12	JKTIFG2	4100	1000	2900	1160	3600 1
21	GRUP RH1	RHAFCS1	2000	625	2900	1160	3600 2 483 8 A
22	GRUP RH2	RHAFCS2	1800	500	2900	1160	3600 2 342 A 8
23	GRUP RH3	RHAFCS3	1600	500	2900	1160	3600 2 342 A A
24	GRUP RH4	RHAFCS4	1400	375	2900	1160	3600 2 283 A A
25	GRUP RH5	RHAFCS5	1275	500	2900	1160	3600 2 342 A A
26	GRUP RH6	RHAFCS6	1275	375	2900	1160	3600 2 342 A A
27	GRUP RH7	RHAFCS7	6.625	280	2900	1160	3600 2 318 8 8
28	GRUP WXP24	WXSUSLEG	3600	1250	2900	1160	3600 2
29	GRUP WXP24	WXSUSLEG	3600	1250	2900	1160	3600 1
30	GRUP WXP24	WXP24	3600	1250	2900	1160	3600 1
31	GRUP WXP24	WXP24	3600	1250	2900	1160	3600 1
32	GRUP WXP24	WXP24	3600	1250	2900	1160	3600 1
33	GRUP WXP24	WXP24	3600	1250	2900	1160	3600 1
34	MEMBER						
35	MEMBER	1	4	P10			0.000 1
36	MEMBER	4	16	P10			0.000 1
37	MEMBER	16	28	P20			0.000 1
38	MEMBER	28	43	P20			0.000 1
39	MEMBER	43	55	P20			0.000 1
40	MEMBER	55	17	P10			0.000 2
41	MEMBER	17	29	P20			0.000 2
42	MEMBER	29	44	P20			0.000 2
43	MEMBER	44	56	P20			0.000 2
44	MEMBER	56	6	P10			0.000 3
45	MEMBER	6	18	P10			0.000 3
46	MEMBER	18	30	P20			0.000 3
47	MEMBER	30	45	P20			0.000 3

SYSTEM INPUT DATA

MEMBER AC-4 STRUCTURE -- U.S. NAVY (46-TH DIA-ETPM PILING) -- C.CHEEN

LINE NO.	MEMBER	1	2	3	4	5	6	7	8
50	MEMBER	45	57	P20					F 0000 3
51	MEMBER	10	22	J11					F 4000
52	MEMBER	22	34	J11					F 4000
53	MEMBER	34	40	J12					F 4100
54	MEMBER	40	49	J12					F 4100
55	MEMBER	49	55	J12					F 4100
56	MEMBER	12	24	J11					F 4000
57	MEMBER	24	36	J11					F 4000
58	MEMBER	34	41	J12					F 4100
59	MEMBER	41	51	J12					F 4100
60	MEMBER	51	56	J12					F 4100
61	MEMBER	14	26	J11					F 4000
62	MEMBER	26	34	J11					F 4000
63	MEMBER	34	42	J12					F 4100
64	MEMBER	42	53	J12					F 4100
65	MEMBER	53	57	J12					F 4100
66	MEMBER	10	11	HR2					1800
67	MEMBER	11	12	HR2					1800
68	MEMBER	12	13	HR2					1800
69	MEMBER	13	14	HR2					1800
70	MEMBER	14	15	HR2					1800
71	MEMBER	15	10	RR2					1800
72	MEMBER	11	13	RR4					1400
73	MEMBER	13	15	RR4					1400
74	MEMBER	15	11	RR4					1400
75	MEMBER	22	23	HR2					1800
76	MEMBER	23	24	RR2					1800
77	MEMBER	24	25	HR2					1800
78	MEMBER	25	26	HR2					1800
79	MEMBER	26	27	HR2					1800
80	MEMBER	27	22	HR2					1800
81	MEMBER	23	25	RR4					1400
82	MEMBER	25	27	RR4					1400
83	MEMBER	27	23	RR4					1400
84	MEMBER	34	35	RR5					1275
85	MEMBER	35	36	RR5					1275
86	MEMBER	36	37	RR5					1275
87	MEMBER	37	38	RR5					1275
88	MEMBER	38	39	RR5					1275
89	MEMBER	39	34	RR5					1275
90	MEMBER	35	37	RR6					1275
91	MEMBER	37	39	RR6					1275
92	MEMBER	39	35	RR6					1275
93	MEMBER	49	50	RR3					1600
94	MEMBER	50	51	RR3					1600
95	MEMBER	51	52	RR3					1600
96	MEMBER	52	53	RR3					1600
97	MEMBER	53	54	RR3					1600
98	MEMBER	54	49	RR3					1600



OPTIC AC R STRUCTURE -- (S. NAV (30-17), DIAMETER PILING) -- C. CHERN

LINE NO. 1 2 3 4 5 6 7 8

09	MEMBER	50	52	ARS								1275
100	MEMBER	52	54	ARS								1275
101	MEMBER	54	50	ARS								1600
102	MEMBER	11	22	ARS								1600
103	MEMBER	11	24	ARS								1600
104	MEMBER	13	24	ARS								1600
105	MEMBER	13	26	ARS								1600
106	MEMBER	15	26	ARS								1600
107	MEMBER	15	22	ARS								2000
108	MEMBER	22	36	ARI								2000
109	MEMBER	24	38	ARI								2000
110	MEMBER	26	34	ARI								2000
111	MEMBER	36	49	ARI								2000
112	MEMBER	34	51	ARI								2000
113	MEMBER	34	53	ARI								2000
114	MEMBER	4	7	MAN	1111							F 0000
115	MEMBER	7	10	MAN								F 0000
116	MEMBER	5	8	MAN	1111							F 0000
117	MEMBER	6	12	MAN								F 0000
118	MEMBER	6	9	MAN	1111							F 0000
119	MEMBER	9	14	MAN								F 0000
120	MEMBER	16	19	MAN	1111							F 0000
121	MEMBER	19	22	MAN								F 0000
122	MEMBER	17	20	MAN	1111							F 0000
123	MEMBER	20	24	MAN								F 0000
124	MEMBER	18	21	MAN	1111							F 0000
125	MEMBER	21	26	MAN								F 0000
126	MEMBER	28	31	MAN	1111							F 0000
127	MEMBER	31	34	MAN								F 0000
128	MEMBER	29	32	MAN	1111							F 0000
129	MEMBER	32	36	MAN								F 0000
130	MEMBER	30	33	MAN	1111							F 0000
131	MEMBER	33	38	MAN								F 0000
132	MEMBER	43	46	MAN	1111							F 0000
133	MEMBER	46	49	MAN								F 0000
134	MEMBER	44	47	MAN	1111							F 0000
135	MEMBER	47	51	MAN								F 0000
136	MEMBER	45	48	MAN	1111							F 0000
137	MEMBER	48	53	MAN								F 0000
138	MEMBER	55	58	STL								3600
139	MEMBER	58	61	STL								3600
140	MEMBER	61	71	STL								3600
141	MEMBER	56	50	STL								5600
142	MEMBER	59	64	STL								3600
143	MEMBER	64	72	STL								3600
144	MEMBER	57	60	STL								3600
145	MEMBER	60	70	STL								5600
146	MEMBER	70	67	STL								3600
147	MEMBER	67	76	STL								3600



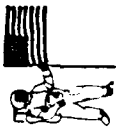
STATUS REPORT DATA

PAGE 4
DATE 04/27/76

(PILING ACH STRUCTURE -- U.S. NAVY (30-11), DIAMETER PILING) -- C,CHERN

LINE NO. 1 2 3 4 5 6 7 8 9

148	MEMBER	74	75	STI								3600
149	MEMBER	54	59	HD5								1275
150	MEMBER	50	60	HD5								1275
151	MEMBER	60	58	HD5								1275
152	MEMBER	59	61	HD5								1275
153	MEMBER	60	60	HD5								1275
154	MEMBER	54	67	HD5								6,625
155	MEMBER	70	66	HD7								6,625
156	MEMBER	70	64	HD7								1275
157	MEMBER	74	77	HD6								1275
158	MEMBER	74	78	HD6								0000
159	MEMBER	61	62	A1A								0000
160	MEMBER	62	63	A1A								0000
161	MEMBER	63	64	A1A								0000
162	MEMBER	64	65	A1A								0000
163	MEMBER	65	67	A1A								0000
164	MEMBER	67	69	A1A								0000
165	MEMBER	69	61	A1B								0000
166	MEMBER	63	65	A0R								0000
167	MEMBER	65	66	A0R								0000
168	MEMBER	66	67	A0A								0000
169	MEMBER	67	68	A0B								0000
170	MEMBER	68	69	A0B								0000
171	MEMBER	69	62	A0R								0000
172	MEMBER	71	73	A1A								0000
173	MEMBER	71	72	A1A								0000
174	MEMBER	72	70	A1A								0000
175	MEMBER	71	81	A1A								0000
176	MEMBER	71	77	A1B								0000
177	MEMBER	77	83	A1A								0000
178	MEMBER	72	82	A1A								0000
179	MEMBER	72	74	A1A								0000
180	MEMBER	74	84	A1B								0000
181	MEMBER	77	79	A1B								0000
182	MEMBER	77	75	A1A								0000
183	MEMBER	75	74	A1A								0000
184	MEMBER	78	80	A1A								0000
185	MEMBER	71	75	A1B								0000
186	MEMBER	72	75	A0B								0000
187	JOINT											
188	JOINT	1	2987	-1725	-600							
189	JOINT	2	-2987	-1725	-600			111		PILING A		
190	JOINT	3	000	3489	-600			111		PILING B		
191	JOINT	4	2910	-1684	0			111		PILING C		
192	JOINT	5	-2910	0	0					MULTIPLE		
193	JOINT	6	0	3559	0					MULTIPLE		
194	JOINT	7	2900	-1924	0					MULTIPLE		
195	JOINT	8	-2900	-1924	0					MULTIPLE		
196	JOINT	9	0	3599	0					MULTIPLE		



TRIPLE ARCH STRUCTURE -- U.S. NAVY (SMITH DIAMETER PILING) -- C. CHERRY

LINE NO. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58

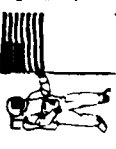
197	JOINT	10	2000	-1674	0	MUDLINE
198	JOINT	11	0	-1674	0	MUDLINE
199	JOINT	12	-29	-1674	0	MUDLINE
200	JOINT	13	-1450	837	0	MUDLINE
201	JOINT	14	0	3349	0	MUDLINE
202	JOINT	15	1450	837	0	MUDLINE
203	JOINT	16	2447	-1417	3200	1 LEVEL
204	JOINT	17	-2447	-1417	3200	1 LEVEL
205	JOINT	18	0	2425	3200	1 LEVEL
206	JOINT	19	2438	-1657	3200	1 LEVEL
207	JOINT	20	-2438	-1657	3200	1 LEVEL
208	JOINT	21	0	5665	3200	1 LEVEL
209	JOINT	22	2438	-1407	3200	1 LEVEL
210	JOINT	23	0	-1407	3200	1 LEVEL
211	JOINT	24	-2438	-1407	3200	1 LEVEL
212	JOINT	25	-1219	704	3200	1 LEVEL
213	JOINT	26	0	2815	3200	1 LEVEL
214	JOINT	27	1219	704	3200	1 LEVEL
215	JOINT	28	1947	-1151	6400	2 LEVEL
216	JOINT	29	-1947	-1151	6400	2 LEVEL
217	JOINT	30	0	3457	6400	2 LEVEL
218	JOINT	31	1977	-1391	6400	2 LEVEL
219	JOINT	32	-1977	-1391	6400	2 LEVEL
220	JOINT	33	0	3677	6400	2 LEVEL
221	JOINT	34	1977	-1141	6400	2 LEVEL
222	JOINT	35	0	-1141	6400	2 LEVEL
223	JOINT	36	-1977	-1141	6400	2 LEVEL
224	JOINT	37	-988	571	6400	2 LEVEL
225	JOINT	38	0	3427	5400	2 LEVEL
226	JOINT	39	988	571	6400	2 LEVEL
227	JOINT	40	1774	-1040	7800	ROAT LOG
228	JOINT	41	-1774	-1040	7800	ROAT LOG
229	JOINT	42	0	2880	7800	ROAT LOG
230	JOINT	43	1525	-885	9600	3 LEVEL
231	JOINT	44	-1525	-885	9600	3 LEVEL
232	JOINT	45	0	1759	9600	3 LEVEL
233	JOINT	46	1515	-1125	9600	3 LEVEL
234	JOINT	47	-1515	-1125	9600	3 LEVEL
235	JOINT	48	0	1999	9600	3 LEVEL
236	JOINT	49	1515	-875	9600	3 LEVEL
237	JOINT	50	0	-875	9600	3 LEVEL
238	JOINT	51	-1515	-875	9600	3 LEVEL
239	JOINT	52	-757	457	9600	3 LEVEL
240	JOINT	53	0	1749	9600	3 LEVEL
241	JOINT	54	757	457	9600	3 LEVEL
242	JOINT	55	1450	-837	10050	WP LEVEL
243	JOINT	56	-1450	-837	10050	WP LEVEL
244	JOINT	57	0	1674	10050	WP LEVEL
245	JOINT	58	1450	-837	12900	ST HRACE



3-MILE ACROSS STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

LINE NO. 1...5...0...1...2...3...4...5...6...7...8

246	JOINT	59	-1450	-837	12900			ST BRACE	
247	JOINT	60	0	1674	12900			ST BRACE	
248	JOINT	61	1450	-837	14400			FOT DECK	
249	JOINT	62	1000	-837	14400			FOT DECK	
250	JOINT	63	-1000	-837	14400			FOT DECK	
251	JOINT	64	-1450	-837	14400			FOT DECK	
252	JOINT	65	-1000	-837	14400			FOT DECK	
253	JOINT	66	-1000	1674	14400			FOT DECK	
254	JOINT	67	0	1674	14400			FOT DECK	
255	JOINT	68	1000	1674	14400			FOT DECK	
256	JOINT	69	1000	-837	14400			FOT DECK	
257	JOINT	70	0	1674	13500			BRACE PT	
258	JOINT	71	1450	-837	15900			TOP DECK	
259	JOINT	72	-1450	-837	15900			TOP DECK	
260	JOINT	73	1750	-837	15900			TOP DECK	
261	JOINT	74	-1750	-837	15900			TOP DECK	
262	JOINT	75	0	1674	15900			TOP DECK	
263	JOINT	76	0	1674	14800			BRACE PT	
264	JOINT	77	1450	1674	15900			TOP DECK	
265	JOINT	78	-1450	1674	15900			TOP DECK	
266	JOINT	79	1750	1674	15900			TOP DECK	
267	JOINT	80	-1750	1674	15900			TOP DECK	
268	JOINT	81	1450	-1337	15900			TOP DECK	
269	JOINT	82	-1450	-1337	15900			TOP DECK	
270	JOINT	83	1450	2174	15900			TOP DECK	
271	JOINT	84	-1450	2174	15900			TOP DECK	
272	LOAD								
273	LOADCN	1							
274	LOAD Y	43	55	4.08	345			GLOR COMC	WN 1 1
275	LOAD X	43	55			4.08=244106		GLOR MOMT	WN 1 1
276	LOAD Y	44	56	4.08	345			GLOR COMC	WN 1 1
277	LOAD X	44	56			4.08=244106		GLOR MOMT	WN 1 1
278	LOAD Y	45	57	4.07	345			GLOR COMC	WN 1 1
279	LOAD X	45	57			4.07=244106		GLOR MOMT	WN 1 1
280	LOAD Y	43	55	4.08	1111			GLOR COMC	WN 2 1
281	LOAD X	43	55			4.08=653247		GLOR MOMT	WN 2 1
282	LOAD Y	44	56	4.08	1111			GLOR COMC	WN 2 1
283	LOAD X	44	56			4.08=653247		GLOR MOMT	WN 2 1
284	LOAD Y	45	57	4.07	1111			GLOR COMC	WN 2 1
285	LOAD X	45	57			4.07=653247		GLOR MOMT	WN 2 1
286	LOAD X	10	22	0.00	1	10.81		GLOR UNIF	WV 0 1
287	LOAD Y	10	22	0.00	47	10.81		GLOR UNIF	WV 0 1
288	LOAD Z	10	22	0.00	34	10.81		GLOR UNIF	WV 0 1
289	LOAD X	10	22	10.81	1	10.81		GLOR UNIF	WV 0 1
290	LOAD Y	10	22	10.81	48	10.81		GLOR UNIF	WV 0 1
291	LOAD Z	10	22	10.81	34	10.81		GLOR UNIF	WV 0 1
292	LOAD X	10	22	21.63	1	10.81		GLOR UNIF	WV 0 1
293	LOAD Y	10	22	21.63	50	10.81		GLOR UNIF	WV 0 1
294	LOAD Z	10	22	21.63	34	10.81		GLOR UNIF	WV 0 1

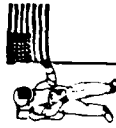


STAMP INPUT DATA

3-PILE 60-DR STRUCTURE -- U.S. NAVY (\$6-IN. DIAMETER PILING) -- C.CHERN

LINE NO. 1 2 3 4 5 6 7 8
...0...5...0...5...0...5...0...5...0...5...0...5...0...5...0...5...0

295	LOAD X	22	34	0.00	1	10.81	1						GLOR UNIF	WV 0 1
296	LOAD Y	22	34	0.00	53	10.81	57						GLOR UNIF	WV 0 1
297	LOAD Z	22	34	0.00	04	10.81	05						GLOR UNIF	WV 0 1
298	LOAD X	22	34	10.81	1	10.81	1						GLOR UNIF	WV 0 1
299	LOAD Y	22	34	10.81	57	10.81	64						GLOR UNIF	WV 0 1
300	LOAD Z	22	34	10.81	05	10.81	05						GLOR UNIF	WV 0 1
301	LOAD X	22	34	21.63	1	10.81	71						GLOR UNIF	WV 0 1
302	LOAD Y	22	34	21.63	64	10.81	04						GLOR UNIF	WV 0 1
303	LOAD Z	22	34	21.63	05	10.81	01						GLOR UNIF	WV 0 1
304	LOAD X	34	40	0.00	1	4.73	77						GLOR UNIF	WV 0 1
305	LOAD Y	34	40	0.00	73	4.73	05						GLOR UNIF	WV 0 1
306	LOAD Z	34	40	0.00	05	4.73	05						GLOR UNIF	WV 0 1
307	LOAD X	34	40	4.73	1	4.73	1						GLOR UNIF	WV 0 1
308	LOAD Y	34	40	4.73	77	4.73	82						GLOR UNIF	WV 0 1
309	LOAD Z	34	40	4.73	05	4.73	06						GLOR UNIF	WV 0 1
310	LOAD X	34	40	9.45	1	4.73	1						GLOR UNIF	WV 0 1
311	LOAD Y	34	40	9.45	82	4.73	88						GLOR UNIF	WV 0 1
312	LOAD Z	34	40	9.45	06	4.73	06						GLOR UNIF	WV 0 1
313	LOAD X	40	49	0.00	1	6.09	1						GLOR UNIF	WV 0 1
314	LOAD Y	40	49	0.00	88	6.09	96						GLOR UNIF	WV 0 1
315	LOAD Z	40	49	0.00	04	6.09	09						GLOR UNIF	WV 0 1
316	LOAD X	40	49	6.09	1	6.09	1						GLOR UNIF	WV 0 1
317	LOAD Y	40	49	6.09	96	6.09	106						GLOR UNIF	WV 0 1
318	LOAD Z	40	49	6.09	09	6.09	09						GLOR UNIF	WV 0 1
319	LOAD X	40	49	12.17	1	6.09	1						GLOR UNIF	WV 0 1
320	LOAD Y	40	49	12.17	106	6.09	118						GLOR UNIF	WV 0 1
321	LOAD Z	40	49	12.17	09	6.09	11						GLOR UNIF	WV 0 1
322	LOAD X	49	55	0.00	1	1.52	1						GLOR UNIF	WV 0 1
323	LOAD Y	49	55	0.00	118	1.52	121						GLOR UNIF	WV 0 1
324	LOAD Z	49	55	0.00	10	1.52	10						GLOR UNIF	WV 0 1
325	LOAD X	49	55	1.52	1	1.52	1						GLOR UNIF	WV 0 1
326	LOAD Y	49	55	1.52	121	1.52	125						GLOR UNIF	WV 0 1
327	LOAD Z	49	55	1.52	10	1.52	10						GLOR UNIF	WV 0 1
328	LOAD X	49	55	3.04	1	1.52	1						GLOR UNIF	WV 0 1
329	LOAD Y	49	55	3.04	125	1.52	128						GLOR UNIF	WV 0 1
330	LOAD Z	49	55	3.04	10	1.52	11						GLOR UNIF	WV 0 1
331	LOAD X	12	24	0.00	1	10.81	1						GLOR UNIF	WV 0 1
332	LOAD Y	12	24	0.00	47	10.81	49						GLOR UNIF	WV 0 1
333	LOAD Z	12	24	0.00	01	10.81	04						GLOR UNIF	WV 0 1
334	LOAD X	12	24	10.81	1	10.81	1						GLOR UNIF	WV 0 1
335	LOAD Y	12	24	10.81	48	10.81	50						GLOR UNIF	WV 0 1
336	LOAD Z	12	24	10.81	04	10.81	04						GLOR UNIF	WV 0 1
337	LOAD X	12	24	21.63	1	10.81	1						GLOR UNIF	WV 0 1
338	LOAD Y	12	24	21.63	50	10.81	53						GLOR UNIF	WV 0 1
339	LOAD Z	12	24	21.63	04	10.81	04						GLOR UNIF	WV 0 1
340	LOAD X	24	36	0.00	1	10.81	1						GLOR UNIF	WV 0 1
341	LOAD Y	24	36	0.00	53	10.81	57						GLOR UNIF	WV 0 1
342	LOAD Z	24	36	0.00	04	10.81	05						GLOR UNIF	WV 0 1
343	LOAD X	24	36	10.81	1	10.81	1						GLOR UNIF	WV 0 1



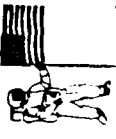
STRAS INPUT DATA

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DATE 04/27/76

3-PILE ACR STRUCTURE -- U.S. NAVY (40-IN. DIAMETER PILING) -- C.CHERN

LINE NO. 1 2 3 4 5 6 7 8

344	LOAD Y	24	36	10.81	57	10.81	64	GLOR UNIF	WV 0 1
345	LOAD Z	24	36	10.81	05	10.81	05	GLOR UNIF	WV 0 1
346	LOAD X	24	36	21.63	1	10.81	1	GLOR UNIF	WV 0 1
347	LOAD Y	24	36	21.63	64	10.81	71	GLOR UNIF	WV 0 1
348	LOAD Z	24	36	21.63	05	10.81	06	GLOR UNIF	WV 0 1
349	LOAD X	36	41	0.00	1	4.73	1	GLOR UNIF	WV 0 1
350	LOAD Y	36	41	0.00	73	4.73	77	GLOR UNIF	WV 0 1
351	LOAD Z	36	41	0.00	05	4.73	05	GLOR UNIF	WV 0 1
352	LOAD X	36	41	4.73	1	4.73	1	GLOR UNIF	WV 0 1
353	LOAD Y	36	41	4.73	77	4.73	82	GLOR UNIF	WV 0 1
354	LOAD Z	36	41	4.73	05	4.73	06	GLOR UNIF	WV 0 1
355	LOAD X	36	41	9.45	1	4.73	1	GLOR UNIF	WV 0 1
356	LOAD Y	36	41	9.45	82	4.73	88	GLOR UNIF	WV 0 1
357	LOAD Z	36	41	9.45	06	4.73	06	GLOR UNIF	WV 0 1
358	LOAD X	41	51	0.00	1	6.09	1	GLOR UNIF	WV 0 1
359	LOAD Y	41	51	0.00	88	6.09	96	GLOR UNIF	WV 0 1
360	LOAD Z	41	51	0.00	08	6.09	09	GLOR UNIF	WV 0 1
361	LOAD X	41	51	6.09	1	6.09	1	GLOR UNIF	WV 0 1
362	LOAD Y	41	51	6.09	96	6.09	106	GLOR UNIF	WV 0 1
363	LOAD Z	41	51	6.09	09	6.09	09	GLOR UNIF	WV 0 1
364	LOAD X	41	51	12.17	1	6.09	1	GLOR UNIF	WV 0 1
365	LOAD Y	41	51	12.17	106	6.09	118	GLOR UNIF	WV 0 1
366	LOAD Z	41	51	12.17	09	6.09	11	GLOR UNIF	WV 0 1
367	LOAD X	51	56	0.00	1	1.52	1	GLOR UNIF	WV 0 1
368	LOAD Y	51	56	0.00	118	1.52	121	GLOR UNIF	WV 0 1
369	LOAD Z	51	56	0.00	10	1.52	10	GLOR UNIF	WV 0 1
370	LOAD X	51	56	1.52	1	1.52	1	GLOR UNIF	WV 0 1
371	LOAD Y	51	56	1.52	121	1.52	124	GLOR UNIF	WV 0 1
372	LOAD Z	51	56	1.52	10	1.52	10	GLOR UNIF	WV 0 1
373	LOAD X	51	56	3.04	1	1.52	1	GLOR UNIF	WV 0 1
374	LOAD Y	51	56	3.04	124	1.52	128	GLOR UNIF	WV 0 1
375	LOAD Z	51	56	3.04	10	1.52	11	GLOR UNIF	WV 0 1
376	LOAD X	14	26	0.00	50	10.81	51	GLOR UNIF	WV 0 1
377	LOAD Y	14	26	0.00	08	10.81	08	GLOR UNIF	WV 0 1
378	LOAD Z	14	26	10.81	51	10.81	53	GLOR UNIF	WV 0 1
379	LOAD X	14	26	10.81	08	10.81	09	GLOR UNIF	WV 0 1
380	LOAD Y	14	26	21.63	53	10.81	56	GLOR UNIF	WV 0 1
381	LOAD Z	14	26	21.63	09	10.81	09	GLOR UNIF	WV 0 1
382	LOAD X	26	38	0.00	55	10.81	50	GLOR UNIF	WV 0 1
383	LOAD Y	26	38	0.00	11	10.81	11	GLOR UNIF	WV 0 1
384	LOAD Z	26	38	10.81	59	10.81	61	GLOR UNIF	WV 0 1
385	LOAD X	26	38	10.81	11	10.81	12	GLOR UNIF	WV 0 1
386	LOAD Y	26	38	21.72	61	10.81	70	GLOR UNIF	WV 0 1
387	LOAD Z	26	38	21.72	12	10.81	13	GLOR UNIF	WV 0 1
388	LOAD X	38	42	0.00	65	5.01	69	GLOR UNIF	WV 0 1
389	LOAD Y	38	42	0.00	25	5.01	27	GLOR UNIF	WV 0 1
390	LOAD Z	38	42	5.01	69	5.01	73	GLOR UNIF	WV 0 1
391	LOAD X	38	42	5.01	27	5.01	29	GLOR UNIF	WV 0 1
392	LOAD Y	38	42	10.02	73	5.01	78	GLOR UNIF	WV 0 1

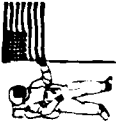


STEP TOP OUT DATA

3-PILE ACHR STRUCTURE -- U.S. NAVY (56-IN. DIAMETER PILING) -- C.CHEMN

LINE NO. 1.....2.....3.....4.....5.....6.....7.....8

LINE NO.	1	2	3	4	5	6	7	8
393	LOAD Z	38	42	10.02	29	5.01	GLOR UNTF	WV 0 1
394	LOAD Y	42	53	0.00	65	7.09	GLOR UNTF	WV 0 1
395	LOAD Z	42	53	0.00	41	7.09	GLOR UNTF	WV 0 1
396	LOAD Y	42	53	7.09	71	7.09	GLOR UNTF	WV 0 1
397	LOAD Z	42	53	7.09	45	7.09	GLOR UNTF	WV 0 1
398	LOAD Y	42	53	14.17	79	7.09	GLOR UNTF	WV 0 1
399	LOAD Z	42	53	14.17	09	7.09	GLOR UNTF	WV 0 1
400	LOAD Y	53	57	0.00	120	1.52	GLOR UNTF	WV 0 1
401	LOAD Z	53	57	0.00	20	1.52	GLOR UNTF	WV 0 1
402	LOAD Y	53	57	1.52	125	1.52	GLOR UNTF	WV 0 1
403	LOAD Z	53	57	1.52	20	1.52	GLOR UNTF	WV 0 1
404	LOAD Y	53	57	3.04	126	1.52	GLOR UNTF	WV 0 1
405	LOAD Z	53	57	3.04	21	1.52	GLOR UNTF	WV 0 1
406	LOAD Y	10	11	0.00	21	9.67	GLOR UNTF	WV 0 1
407	LOAD Z	10	11	9.67	21	9.67	GLOR UNTF	WV 0 1
408	LOAD Y	10	11	19.35	21	9.67	GLOR UNTF	WV 0 1
409	LOAD Z	11	12	0.00	21	9.67	GLOR UNTF	WV 0 1
410	LOAD Y	11	12	9.67	21	9.67	GLOR UNTF	WV 0 1
411	LOAD Z	11	12	19.35	21	9.67	GLOR UNTF	WV 0 1
412	LOAD Y	12	13	0.00	09	9.67	GLOR UNTF	WV 0 1
413	LOAD Z	12	13	0.00	05	9.67	GLOR UNTF	WV 0 1
414	LOAD Y	12	13	9.67	09	9.67	GLOR UNTF	WV 0 1
415	LOAD Z	12	13	9.67	05	9.67	GLOR UNTF	WV 0 1
416	LOAD Y	12	13	19.35	10	9.67	GLOR UNTF	WV 0 1
417	LOAD Z	12	13	19.35	06	9.67	GLOR UNTF	WV 0 1
418	LOAD Y	13	14	0.00	10	9.67	GLOR UNTF	WV 0 1
419	LOAD Z	13	14	0.00	06	9.67	GLOR UNTF	WV 0 1
420	LOAD Y	13	14	9.67	10	9.67	GLOR UNTF	WV 0 1
421	LOAD Z	13	14	9.67	06	9.67	GLOR UNTF	WV 0 1
422	LOAD Y	13	14	19.35	10	9.67	GLOR UNTF	WV 0 1
423	LOAD Z	13	14	19.35	06	9.67	GLOR UNTF	WV 0 1
424	LOAD Y	14	15	0.00	10	9.67	GLOR UNTF	WV 0 1
425	LOAD Z	14	15	0.00	06	9.67	GLOR UNTF	WV 0 1
426	LOAD Y	14	15	9.67	10	9.67	GLOR UNTF	WV 0 1
427	LOAD Z	14	15	9.67	06	9.67	GLOR UNTF	WV 0 1
428	LOAD Y	14	15	19.35	10	9.67	GLOR UNTF	WV 0 1
429	LOAD Z	14	15	19.35	06	9.67	GLOR UNTF	WV 0 1
430	LOAD Y	15	16	0.00	10	9.67	GLOR UNTF	WV 0 1
431	LOAD Z	15	16	0.00	06	9.67	GLOR UNTF	WV 0 1
432	LOAD Y	15	16	9.67	10	9.67	GLOR UNTF	WV 0 1
433	LOAD Z	15	16	9.67	06	9.67	GLOR UNTF	WV 0 1
434	LOAD Y	15	16	19.35	09	9.67	GLOR UNTF	WV 0 1
435	LOAD Z	15	16	19.35	05	9.67	GLOR UNTF	WV 0 1
436	LOAD Y	11	13	0.00	07	9.67	GLOR UNTF	WV 0 1
437	LOAD Z	11	13	0.00	09	9.67	GLOR UNTF	WV 0 1
438	LOAD Y	11	13	9.67	07	9.67	GLOR UNTF	WV 0 1
439	LOAD Z	11	13	9.67	09	9.67	GLOR UNTF	WV 0 1
440	LOAD Y	11	13	19.35	08	9.67	GLOR UNTF	WV 0 1
441	LOAD Z	11	13	19.35	08	9.67	GLOR UNTF	WV 0 1



STANDARD INPUT DATA

TYPE ACMR STRUCTURE -- U.S. NAVY (16-IN. DIAMETER PILING) -- C. CHERN

LINE NO. 1...5...0...1...1...2...2...3...3...4...4...5...5...6...6...7...7...8...8...0

442	LOAD Y	13	15	0.00	1A	9.67	1A	GLOR UNIF	WV 0 1
443	LOAD Y	13	15	9.67	1A	9.67	1A	GLOR UNIF	WV 0 1
444	LOAD Y	13	15	19.33	1A	9.67	1A	GLOR UNIF	WV 0 1
445	LOAD X	15	11	0.00	0A	9.67	0A	GLOR UNIF	WV 0 1
446	LOAD X	15	11	0.00	0A	9.67	0A	GLOR UNIF	WV 0 1
447	LOAD X	15	11	9.67	0A	9.67	0A	GLOR UNIF	WV 0 1
448	LOAD Y	15	11	9.67	0A	9.67	0A	GLOR UNIF	WV 0 1
449	LOAD X	15	11	19.33	0A	9.67	0A	GLOR UNIF	WV 0 1
450	LOAD Y	15	11	19.33	0A	9.67	0A	GLOR UNIF	WV 0 1
451	LOAD Y	22	23	0.00	2A	8.13	2A	GLOR UNIF	WV 0 1
452	LOAD Y	22	23	8.13	2A	8.13	2A	GLOR UNIF	WV 0 1
453	LOAD Y	22	23	16.25	2A	8.13	2A	GLOR UNIF	WV 0 1
454	LOAD Y	23	24	0.00	2A	8.13	2A	GLOR UNIF	WV 0 1
455	LOAD Y	23	24	8.13	2A	8.13	2A	GLOR UNIF	WV 0 1
456	LOAD Y	23	24	16.25	2A	8.13	2A	GLOR UNIF	WV 0 1
457	LOAD X	24	25	0.00	10	8.13	11	GLOR UNIF	WV 0 1
458	LOAD X	24	25	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
459	LOAD X	24	25	8.13	11	8.13	11	GLOR UNIF	WV 0 1
460	LOAD X	24	25	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
461	LOAD X	24	25	16.25	11	8.13	11	GLOR UNIF	WV 0 1
462	LOAD X	24	25	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
463	LOAD X	25	26	0.00	11	8.13	11	GLOR UNIF	WV 0 1
464	LOAD X	25	26	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
465	LOAD X	25	26	8.13	11	8.13	11	GLOR UNIF	WV 0 1
466	LOAD X	25	26	8.13	0A	8.13	0A	GLOR UNIF	WV 0 1
467	LOAD X	25	26	16.25	11	8.13	11	GLOR UNIF	WV 0 1
468	LOAD X	25	26	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
469	LOAD X	26	27	0.00	11	8.13	11	GLOR UNIF	WV 0 1
470	LOAD X	26	27	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
471	LOAD X	26	27	8.13	11	8.13	11	GLOR UNIF	WV 0 1
472	LOAD X	26	27	8.13	0A	8.13	0A	GLOR UNIF	WV 0 1
473	LOAD X	26	27	16.25	11	8.13	11	GLOR UNIF	WV 0 1
474	LOAD X	26	27	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
475	LOAD X	27	22	0.00	11	8.13	11	GLOR UNIF	WV 0 1
476	LOAD X	27	22	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
477	LOAD X	27	22	8.13	11	8.13	11	GLOR UNIF	WV 0 1
478	LOAD X	27	22	8.13	0A	8.13	0A	GLOR UNIF	WV 0 1
479	LOAD X	27	22	16.25	11	8.13	11	GLOR UNIF	WV 0 1
480	LOAD X	27	22	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
481	LOAD X	23	25	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
482	LOAD X	23	25	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1
483	LOAD X	23	25	8.13	0A	8.13	0A	GLOR UNIF	WV 0 1
484	LOAD X	23	25	8.13	0A	8.13	0A	GLOR UNIF	WV 0 1
485	LOAD X	23	25	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
486	LOAD X	23	25	16.25	0A	8.13	0A	GLOR UNIF	WV 0 1
487	LOAD X	25	27	0.00	20	8.13	20	GLOR UNIF	WV 0 1
488	LOAD X	25	27	8.13	20	8.13	20	GLOR UNIF	WV 0 1
489	LOAD X	25	27	16.25	20	8.13	20	GLOR UNIF	WV 0 1
490	LOAD X	27	23	0.00	0A	8.13	0A	GLOR UNIF	WV 0 1



STAR INPUT DATA

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3-PILE ACHR STRUCTURE -- U.S. NAVY (36-IN. DIA-FTW PILING) -- C.C.M.H

LINE NO. 1..... 2..... 3..... 4..... 5..... 6..... 7..... 8.....

491	LOAD Y	27	23	0.00	05	8.13	05	GLOR	UNIF	MV	0	1
492	LOAD X	27	23	8.13	05	8.13	04	GLOR	UNIF	MV	0	1
493	LOAD Y	27	23	8.13	05	8.13	05	GLOR	UNIF	MV	0	1
494	LOAD X	27	23	16.25	04	8.13	04	GLOR	UNIF	MV	0	1
495	LOAD Y	27	23	16.25	05	8.13	05	GLOR	UNIF	MV	0	1
496	LOAD X	34	35	0.00	23	6.59	23	GLOR	UNIF	MV	0	1
497	LOAD Y	34	35	6.59	23	6.59	23	GLOR	UNIF	MV	0	1
498	LOAD X	34	35	13.18	23	6.59	23	GLOR	UNIF	MV	0	1
499	LOAD Y	35	36	0.00	23	6.59	23	GLOR	UNIF	MV	0	1
500	LOAD X	35	36	6.59	23	6.59	23	GLOR	UNIF	MV	0	1
501	LOAD Y	35	36	13.18	23	6.59	23	GLOR	UNIF	MV	0	1
502	LOAD X	36	37	0.00	10	6.59	10	GLOR	UNIF	MV	0	1
503	LOAD Y	36	37	0.00	06	6.59	06	GLOR	UNIF	MV	0	1
504	LOAD X	36	37	6.59	10	6.59	06	GLOR	UNIF	MV	0	1
505	LOAD Y	36	37	6.59	06	6.59	06	GLOR	UNIF	MV	0	1
506	LOAD X	36	37	13.18	10	6.59	10	GLOR	UNIF	MV	0	1
507	LOAD Y	36	37	13.18	06	6.59	06	GLOR	UNIF	MV	0	1
508	LOAD X	37	38	0.00	07	10.07	07	GLOR	UNIF	MV	0	1
509	LOAD Y	37	38	0.00	03	10.07	03	GLOR	UNIF	MV	0	1
510	LOAD X	37	38	10.07	07	10.07	07	GLOR	UNIF	MV	0	1
511	LOAD Y	37	38	10.07	03	10.07	03	GLOR	UNIF	MV	0	1
512	LOAD X	37	38	20.15	07	10.07	07	GLOR	UNIF	MV	0	1
513	LOAD Y	37	38	20.15	03	10.07	02	GLOR	UNIF	MV	0	1
514	LOAD X	38	39	0.00	07	10.07	07	GLOR	UNIF	MV	0	1
515	LOAD Y	38	39	0.00	02	10.07	03	GLOR	UNIF	MV	0	1
516	LOAD X	38	39	10.07	07	10.07	07	GLOR	UNIF	MV	0	1
517	LOAD Y	38	39	10.07	03	10.07	03	GLOR	UNIF	MV	0	1
518	LOAD X	38	39	20.15	07	10.07	07	GLOR	UNIF	MV	0	1
519	LOAD Y	38	39	20.15	03	10.07	03	GLOR	UNIF	MV	0	1
520	LOAD X	39	34	0.00	10	6.59	10	GLOR	UNIF	MV	0	1
521	LOAD Y	39	34	0.00	06	6.59	06	GLOR	UNIF	MV	0	1
522	LOAD X	39	34	6.59	10	6.59	10	GLOR	UNIF	MV	0	1
523	LOAD Y	39	34	6.59	06	6.59	06	GLOR	UNIF	MV	0	1
524	LOAD X	39	34	13.18	10	6.59	10	GLOR	UNIF	MV	0	1
525	LOAD Y	39	34	13.18	06	6.59	06	GLOR	UNIF	MV	0	1
526	LOAD X	35	37	0.00	10	6.59	10	GLOR	UNIF	MV	0	1
527	LOAD Y	35	37	0.00	06	6.59	06	GLOR	UNIF	MV	0	1
528	LOAD X	35	37	6.59	10	6.59	10	GLOR	UNIF	MV	0	1
529	LOAD Y	35	37	6.59	06	6.59	06	GLOR	UNIF	MV	0	1
530	LOAD X	35	37	13.18	10	6.59	10	GLOR	UNIF	MV	0	1
531	LOAD Y	35	37	13.18	06	6.59	06	GLOR	UNIF	MV	0	1
532	LOAD X	37	39	0.00	24	6.59	24	GLOR	UNIF	MV	0	1
533	LOAD Y	37	39	6.59	24	6.59	24	GLOR	UNIF	MV	0	1
534	LOAD X	37	39	13.17	24	6.59	24	GLOR	UNIF	MV	0	1
535	LOAD Y	39	35	0.00	10	6.59	10	GLOR	UNIF	MV	0	1
536	LOAD X	39	35	0.00	06	6.59	06	GLOR	UNIF	MV	0	1
537	LOAD Y	39	35	6.59	10	6.59	10	GLOR	UNIF	MV	0	1
538	LOAD X	39	35	6.59	06	6.59	06	GLOR	UNIF	MV	0	1
539	LOAD Y	39	35	13.18	10	6.59	10	GLOR	UNIF	MV	0	1



SYSTEM INPUT DATA

3-PTILE ARCH STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHEM.

LINE NO.	1	2	3	4	5	6	7	8		
540	LOAD Y	39	35	13.18	06	0.59			GLOR UNIT	AV 0 1
541	LOAD Y	49	50	0.00	46	5.05			GLOR UNIT	AV 0 1
542	LOAD Y	49	50	5.05	46	5.05			GLOR UNIT	AV 0 1
543	LOAD Y	49	50	10.10	46	5.05			GLOR UNIT	AV 0 1
544	LOAD Y	50	51	0.00	46	5.05			GLOR UNIT	AV 0 1
545	LOAD Y	50	51	5.05	46	5.05			GLOR UNIT	AV 0 1
546	LOAD Y	50	51	10.10	46	5.05			GLOR UNIT	AV 0 1
547	LOAD Y	51	52	0.00	20	5.05			GLOR UNIT	AV 0 1
548	LOAD Y	51	52	0.00	12	5.05			GLOR UNIT	AV 0 1
549	LOAD X	51	52	5.05	20	5.05			GLOR UNIT	AV 0 1
550	LOAD X	51	52	5.05	12	5.05			GLOR UNIT	AV 0 1
551	LOAD X	51	52	10.10	21	5.05			GLOR UNIT	AV 0 1
552	LOAD Y	51	52	10.10	12	5.05			GLOR UNIT	AV 0 1
553	LOAD X	52	53	0.00	21	5.05			GLOR UNIT	AV 0 1
554	LOAD X	52	53	0.00	12	5.05			GLOR UNIT	AV 0 1
555	LOAD X	52	53	5.05	21	5.05			GLOR UNIT	AV 0 1
556	LOAD Y	52	53	5.05	12	5.05			GLOR UNIT	AV 0 1
557	LOAD X	52	53	10.10	21	5.05			GLOR UNIT	AV 0 1
558	LOAD Y	52	53	10.10	12	5.05			GLOR UNIT	AV 0 1
559	LOAD X	53	54	0.00	21	5.05			GLOR UNIT	AV 0 1
560	LOAD Y	53	54	0.00	12	5.05			GLOR UNIT	AV 0 1
561	LOAD X	53	54	5.05	21	5.05			GLOR UNIT	AV 0 1
562	LOAD Y	53	54	5.05	12	5.05			GLOR UNIT	AV 0 1
563	LOAD X	53	54	10.10	21	5.05			GLOR UNIT	AV 0 1
564	LOAD Y	53	54	10.10	12	5.05			GLOR UNIT	AV 0 1
565	LOAD X	54	49	0.00	21	5.05			GLOR UNIT	AV 0 1
566	LOAD Y	54	49	0.00	12	5.05			GLOR UNIT	AV 0 1
567	LOAD X	54	49	5.05	21	5.05			GLOR UNIT	AV 0 1
568	LOAD Y	54	49	5.05	12	5.05			GLOR UNIT	AV 0 1
569	LOAD X	54	49	10.10	20	5.05			GLOR UNIT	AV 0 1
570	LOAD Y	54	49	10.10	12	5.05			GLOR UNIT	AV 0 1
571	LOAD X	50	52	0.00	16	5.05			GLOR UNIT	AV 0 1
572	LOAD Y	50	52	0.00	09	5.05			GLOR UNIT	AV 0 1
573	LOAD X	50	52	5.05	16	5.05			GLOR UNIT	AV 0 1
574	LOAD Y	50	52	5.05	09	5.05			GLOR UNIT	AV 0 1
575	LOAD X	50	52	10.10	17	5.05			GLOR UNIT	AV 0 1
576	LOAD Y	50	52	10.10	10	5.05			GLOR UNIT	AV 0 1
577	LOAD X	52	54	0.00	39	5.05			GLOR UNIT	AV 0 1
578	LOAD Y	52	54	5.05	39	5.05			GLOR UNIT	AV 0 1
579	LOAD X	52	54	10.09	39	5.05			GLOR UNIT	AV 0 1
580	LOAD Y	54	50	0.00	17	5.05			GLOR UNIT	AV 0 1
581	LOAD X	54	50	0.00	10	5.05			GLOR UNIT	AV 0 1
582	LOAD X	54	50	5.05	17	5.05			GLOR UNIT	AV 0 1
583	LOAD Y	54	50	5.05	10	5.05			GLOR UNIT	AV 0 1
584	LOAD X	54	50	10.10	16	5.05			GLOR UNIT	AV 0 1
585	LOAD Y	54	50	10.10	09	5.05			GLOR UNIT	AV 0 1
586	LOAD X	11	22	0.00	1	13.44			GLOR UNIT	AV 0 1
587	LOAD Y	11	22	0.00	19	13.44			GLOR UNIT	AV 0 1
588	LOAD Z	11	22	0.00	1	13.44			GLOR UNIT	AV 0 1



STATE INPUT DATA

SEPTILE ACAP STRUCTURE -- U.S. NAVY (36-1) DIAMETER PILING -- C.CHERN

LINE NO.	1	2	3	4	5	6	7	8													
589	LOAD X	11	22	13.44	1	15.44				GLOR	UNTF								MV	0	1
590	LOAD Y	11	22	13.44	10	15.44				GLOR	UNTF								MV	0	1
591	LOAD Z	11	22	13.44	1	15.44				GLOR	UNTF								MV	0	1
592	LOAD X	11	22	26.88	1	13.44				GLOR	UNTF								MV	0	1
593	LOAD Y	11	22	26.88	20	15.44				GLOR	UNTF								MV	0	1
594	LOAD Z	11	22	26.88	1	13.44				GLOR	UNTF								MV	0	1
595	LOAD X	11	24	0.00	19	13.44				GLOR	UNTF								MV	0	1
596	LOAD Y	11	24	0.00	19	13.44				GLOR	UNTF								MV	0	1
597	LOAD Z	11	24	0.00	1	15.44				GLOR	UNTF								MV	0	1
598	LOAD X	11	24	13.44	1	13.44				GLOR	UNTF								MV	0	1
599	LOAD Y	11	24	13.44	19	13.44				GLOR	UNTF								MV	0	1
600	LOAD Z	11	24	13.44	1	13.44				GLOR	UNTF								MV	0	1
601	LOAD X	11	24	26.88	1	13.44				GLOR	UNTF								MV	0	1
602	LOAD Y	11	24	26.88	20	13.44				GLOR	UNTF								MV	0	1
603	LOAD Z	11	24	26.88	1	13.44				GLOR	UNTF								MV	0	1
604	LOAD X	13	24	0.00	03	13.44				GLOR	UNTF								MV	0	1
605	LOAD Y	13	24	0.00	14	13.44				GLOR	UNTF								MV	0	1
606	LOAD Z	13	24	0.00	09	13.44				GLOR	UNTF								MV	0	1
607	LOAD X	13	24	13.44	03	13.44				GLOR	UNTF								MV	0	1
608	LOAD Y	13	24	13.44	14	13.44				GLOR	UNTF								MV	0	1
609	LOAD Z	13	24	13.44	09	13.44				GLOR	UNTF								MV	0	1
610	LOAD X	13	24	26.88	03	13.44				GLOR	UNTF								MV	0	1
611	LOAD Y	13	24	26.88	14	13.44				GLOR	UNTF								MV	0	1
612	LOAD Z	13	24	26.88	09	13.44				GLOR	UNTF								MV	0	1
613	LOAD X	13	26	0.00	04	13.44				GLOR	UNTF								MV	0	1
614	LOAD Y	13	26	0.00	16	13.44				GLOR	UNTF								MV	0	1
615	LOAD Z	13	26	0.00	08	13.44				GLOR	UNTF								MV	0	1
616	LOAD X	13	26	13.44	04	13.44				GLOR	UNTF								MV	0	1
617	LOAD Y	13	26	13.44	16	13.44				GLOR	UNTF								MV	0	1
618	LOAD Z	13	26	13.44	08	13.44				GLOR	UNTF								MV	0	1
619	LOAD X	13	26	26.88	04	13.44				GLOR	UNTF								MV	0	1
620	LOAD Y	13	26	26.88	17	13.44				GLOR	UNTF								MV	0	1
621	LOAD Z	13	26	26.88	08	13.44				GLOR	UNTF								MV	0	1
622	LOAD X	15	26	0.00	04	13.44				GLOR	UNTF								MV	0	1
623	LOAD Y	15	26	0.00	16	13.44				GLOR	UNTF								MV	0	1
624	LOAD Z	15	26	0.00	08	13.44				GLOR	UNTF								MV	0	1
625	LOAD X	15	26	13.44	04	13.44				GLOR	UNTF								MV	0	1
626	LOAD Y	15	26	13.44	16	13.44				GLOR	UNTF								MV	0	1
627	LOAD Z	15	26	13.44	08	13.44				GLOR	UNTF								MV	0	1
628	LOAD X	15	26	26.88	04	13.44				GLOR	UNTF								MV	0	1
629	LOAD Y	15	26	26.88	17	13.44				GLOR	UNTF								MV	0	1
630	LOAD Z	15	26	26.88	08	13.44				GLOR	UNTF								MV	0	1
631	LOAD X	15	22	0.00	03	13.44				GLOR	UNTF								MV	0	1
632	LOAD Y	15	22	0.00	14	13.44				GLOR	UNTF								MV	0	1
633	LOAD Z	15	22	0.00	09	13.44				GLOR	UNTF								MV	0	1
634	LOAD X	15	22	13.44	03	13.44				GLOR	UNTF								MV	0	1
635	LOAD Y	15	22	13.44	14	13.44				GLOR	UNTF								MV	0	1
636	LOAD Z	15	22	13.44	09	13.44				GLOR	UNTF								MV	0	1
637	LOAD X	15	22	26.88	03	13.44				GLOR	UNTF								MV	0	1



STAKE TYPOT DATA

3-PILE ACNR STRUCTURE -- U.S. NAV (36-IN. DIAMETER PILING) -- C.CHERN

LINE NO. 1 2 3 4 5 6 7 A
 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000

638	LOAD Y	15	22	26.88	14	13.44	15	GLOR UNTF	MV 0 1
639	LOAD Z	15	22	26.88	09	13.44	09	GLOR UNTF	MV 0 1
640	LOAD X	22	34	0.00	1	18.20	1	GLOR UNTF	MV 0 1
641	LOAD Y	22	36	0.00	27	18.20	29	GLOR UNTF	MV 0 1
642	LOAD Z	22	36	0.00	1	18.20	1	GLOR UNTF	MV 0 1
643	LOAD X	22	36	18.20	1	18.20	32	GLOR UNTF	MV 0 1
644	LOAD Y	22	36	18.20	29	18.20	1	GLOR UNTF	MV 0 1
645	LOAD Z	22	36	18.20	1	18.20	1	GLOR UNTF	MV 0 1
646	LOAD X	22	36	36.39	1	18.20	1	GLOR UNTF	MV 0 1
647	LOAD Y	22	36	36.39	32	18.20	36	GLOR UNTF	MV 0 1
648	LOAD Z	22	36	36.39	1	18.20	1	GLOR UNTF	MV 0 1
649	LOAD X	24	38	0.00	08	20.96	09	GLOR UNTF	MV 0 1
650	LOAD Y	24	38	0.00	11	20.96	15	GLOR UNTF	MV 0 1
651	LOAD Z	24	38	0.00	10	20.96	12	GLOR UNTF	MV 0 1
652	LOAD X	24	38	20.96	09	20.96	10	GLOR UNTF	MV 0 1
653	LOAD Y	24	38	20.96	15	20.96	14	GLOR UNTF	MV 0 1
654	LOAD Z	24	38	20.96	12	20.96	13	GLOR UNTF	MV 0 1
655	LOAD X	24	38	41.93	10	20.96	11	GLOR UNTF	MV 0 1
656	LOAD Y	24	38	41.93	14	20.96	15	GLOR UNTF	MV 0 1
657	LOAD Z	24	38	41.93	13	20.96	10	GLOR UNTF	MV 0 1
658	LOAD X	26	34	0.00	08	18.20	08	GLOR UNTF	MV 0 1
659	LOAD Y	26	34	0.00	14	18.20	15	GLOR UNTF	MV 0 1
660	LOAD Z	26	34	0.00	12	18.20	13	GLOR UNTF	MV 0 1
661	LOAD X	26	34	18.20	08	18.20	09	GLOR UNTF	MV 0 1
662	LOAD Y	26	34	18.20	15	18.20	14	GLOR UNTF	MV 0 1
663	LOAD Z	26	34	18.20	13	18.20	10	GLOR UNTF	MV 0 1
664	LOAD X	26	34	36.39	09	18.20	09	GLOR UNTF	MV 0 1
665	LOAD Y	26	34	36.39	16	18.20	17	GLOR UNTF	MV 0 1
666	LOAD Z	26	34	36.39	14	18.20	15	GLOR UNTF	MV 0 1
667	LOAD X	36	49	0.00	1	11.86	02	GLOR UNTF	MV 0 1
668	LOAD Y	36	49	0.00	34	11.86	40	GLOR UNTF	MV 0 1
669	LOAD Z	36	49	0.00	1	11.86	1	GLOR UNTF	MV 0 1
670	LOAD X	36	49	11.86	02	11.86	02	GLOR UNTF	MV 0 1
671	LOAD Y	36	49	11.86	40	11.86	44	GLOR UNTF	MV 0 1
672	LOAD Z	36	49	11.86	1	11.86	02	GLOR UNTF	MV 0 1
673	LOAD X	36	49	23.72	02	11.86	50	GLOR UNTF	MV 0 1
674	LOAD Y	36	49	23.72	40	11.86	50	GLOR UNTF	MV 0 1
675	LOAD Z	36	49	23.72	02	11.86	02	GLOR UNTF	MV 0 1
676	LOAD X	36	49	35.54	02	11.86	02	GLOR UNTF	MV 0 1
677	LOAD Y	36	49	35.54	50	11.86	54	GLOR UNTF	MV 0 1
678	LOAD Z	36	49	35.54	02	11.86	02	GLOR UNTF	MV 0 1
679	LOAD X	38	51	0.00	08	13.93	09	GLOR UNTF	MV 0 1
680	LOAD Y	38	51	0.00	15	13.93	17	GLOR UNTF	MV 0 1
681	LOAD Z	38	51	0.00	16	13.93	14	GLOR UNTF	MV 0 1
682	LOAD X	38	51	13.93	09	13.93	10	GLOR UNTF	MV 0 1
683	LOAD Y	38	51	13.93	17	13.93	19	GLOR UNTF	MV 0 1
684	LOAD Z	38	51	13.93	18	13.93	21	GLOR UNTF	MV 0 1
685	LOAD X	38	51	27.86	10	13.93	11	GLOR UNTF	MV 0 1
686	LOAD Y	38	51	27.86	19	13.93	21	GLOR UNTF	MV 0 1



PILE ACR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- F. CHFR

LINE NO.	1	2	3	4	5	6	7	8
687	LOAD Z	3A	51	27.86	21	13.94	GLOR UNIF	WV 0 1
688	LOAD X	3A	51	41.79	12	13.93	GLOR UNIF	WV 0 1
689	LOAD Y	3A	51	41.79	21	13.93	GLOR UNIF	WV 0 1
690	LOAD Z	3A	51	0.00	23	9.49	GLOR UNIF	WV 0 1
691	LOAD X	3A	53	0.00	09	9.49	GLOR UNIF	WV 0 1
692	LOAD Y	3A	53	0.00	23	9.49	GLOR UNIF	WV 0 1
693	LOAD Z	3A	53	0.00	15	9.49	GLOR UNIF	WV 0 1
694	LOAD X	3A	53	9.49	10	9.49	GLOR UNIF	WV 0 1
695	LOAD Y	3A	53	9.49	25	9.49	GLOR UNIF	WV 0 1
696	LOAD Z	3A	53	9.49	16	9.49	GLOR UNIF	WV 0 1
697	LOAD X	3A	53	18.97	11	9.49	GLOR UNIF	WV 0 1
698	LOAD Y	3A	53	18.97	28	9.49	GLOR UNIF	WV 0 1
699	LOAD Z	3A	53	18.97	18	9.49	GLOR UNIF	WV 0 1
700	LOAD X	3A	53	28.46	13	9.49	GLOR UNIF	WV 0 1
701	LOAD Y	3A	53	28.46	31	9.49	GLOR UNIF	WV 0 1
702	LOAD Z	3A	53	28.46	20	9.49	GLOR UNIF	WV 0 1
703	LOAD X	3A	53	37.95	14	9.49	GLOR UNIF	WV 0 1
704	LOAD Y	3A	53	37.95	34	9.49	GLOR UNIF	WV 0 1
705	LOAD Z	3A	53	37.95	22	9.49	GLOR UNIF	WV 0 1
706	LOAD X	55	58	0.00	113	5.70	GLOR UNIF	WV 0 1
707	LOAD Y	55	58	5.70	126	5.70	GLOR UNIF	WV 0 1
708	LOAD Z	55	58	11.40	141	5.70	GLOR UNIF	WV 0 1
709	LOAD X	55	58	17.10	158	5.70	GLOR UNIF	WV 0 1
710	LOAD Y	55	58	22.80	178	5.70	GLOR UNIF	WV 0 1
711	LOAD Z	58	61	0.00	202	4.19	GLOR UNIF	WV 0 1
712	LOAD X	58	61	4.19	221	4.19	GLOR UNIF	WV 0 1
713	LOAD Y	58	61	8.39	244	4.19	GLOR UNIF	WV 0 1
714	LOAD Z	56	59	0.00	113	5.70	GLOR UNIF	WV 0 1
715	LOAD X	56	59	5.70	126	5.70	GLOR UNIF	WV 0 1
716	LOAD Y	56	59	11.40	141	5.70	GLOR UNIF	WV 0 1
717	LOAD Z	56	59	17.10	158	5.70	GLOR UNIF	WV 0 1
718	LOAD X	56	59	22.80	178	5.70	GLOR UNIF	WV 0 1
719	LOAD Y	59	64	0.00	202	4.19	GLOR UNIF	WV 0 1
720	LOAD Z	59	64	4.19	221	4.19	GLOR UNIF	WV 0 1
721	LOAD X	59	64	8.39	244	4.19	GLOR UNIF	WV 0 1
722	LOAD Y	57	60	0.00	116	5.70	GLOR UNIF	WV 0 1
723	LOAD Z	57	60	5.70	129	5.70	GLOR UNIF	WV 0 1
724	LOAD X	57	60	11.40	143	5.70	GLOR UNIF	WV 0 1
725	LOAD Y	57	60	17.10	160	5.70	GLOR UNIF	WV 0 1
726	LOAD Z	57	60	22.80	180	5.70	GLOR UNIF	WV 0 1
727	LOAD X	60	70	0.00	201	2.00	GLOR UNIF	WV 0 1
728	LOAD Y	60	70	2.00	210	2.00	GLOR UNIF	WV 0 1
729	LOAD Z	60	70	4.00	220	2.00	GLOR UNIF	WV 0 1
730	LOAD X	70	67	0.00	231	.22	GLOR UNIF	WV 0 1
731	LOAD Y	70	67	.44	232	.22	GLOR UNIF	WV 0 1
732	LOAD Z	70	67	.67	233	.22	GLOR UNIF	WV 0 1
733	LOAD X	70	67	.89	234	.22	GLOR UNIF	WV 0 1
734	LOAD Y	70	67	1.11	235	.22	GLOR UNIF	WV 0 1
735	LOAD Z	70	67	1.11	237	.22	GLOR UNIF	WV 0 1



STRUT OUTPUT DATA

PILE ACMR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

LINE NO. 1 2 3 4 5 6 7 8

736	LOAD Y	70	67	1.33	238	.22	230	GLOR UNIF	AV 0 1
737	LOAD Y	70	67	1.56	259	.22	241	GLOR UNIF	AV 0 1
738	LOAD Y	70	67	1.78	241	.22		GLOR UNIF	AV 0 1
739	LOAD Y	58	59	0.00	71	9.67	71	GLOR UNIF	AV 0 1
740	LOAD Y	58	59	9.67	71	9.67	71	GLOR UNIF	AV 0 1
741	LOAD Y	58	59	19.33	71	9.67	71	GLOR UNIF	AV 0 1
742	LOAD X	59	60	0.00	31	9.67	32	GLOR UNIF	AV 0 1
743	LOAD X	59	60	0.00	18	9.67	18	GLOR UNIF	AV 0 1
744	LOAD X	59	60	9.67	32	9.67	32	GLOR UNIF	AV 0 1
745	LOAD X	59	60	9.67	18	9.67	18	GLOR UNIF	AV 0 1
746	LOAD X	59	60	19.33	32	9.67	31	GLOR UNIF	AV 0 1
747	LOAD X	59	60	19.33	18	9.67	18	GLOR UNIF	AV 0 1
748	LOAD X	60	58	0.00	31	9.67	32	GLOR UNIF	AV 0 1
749	LOAD X	60	58	0.00	18	9.67	18	GLOR UNIF	AV 0 1
750	LOAD X	60	58	9.67	32	9.67	32	GLOR UNIF	AV 0 1
751	LOAD X	60	58	9.67	18	9.67	18	GLOR UNIF	AV 0 1
752	LOAD X	60	58	19.33	32	9.67	31	GLOR UNIF	AV 0 1
753	LOAD X	60	58	19.33	18	9.67	18	GLOR UNIF	AV 0 1
754	LOAD Y	59	61	0.00	71	9.13	74	GLOR UNIF	AV 0 1
755	LOAD Y	59	61	9.13	74	9.13	66	GLOR UNIF	AV 0 1
756	LOAD Y	59	61	18.25	66	9.13	95	GLOR UNIF	AV 0 1
757	LOAD X	60	64	0.00	24	8.41	27	GLOR UNIF	AV 0 1
758	LOAD X	60	64	0.00	29	8.41	33	GLOR UNIF	AV 0 1
759	LOAD Z	60	64	0.00	25	8.41	28	GLOR UNIF	AV 0 1
760	LOAD X	60	64	8.41	27	8.41	30	GLOR UNIF	AV 0 1
761	LOAD Y	60	64	8.41	33	8.41	36	GLOR UNIF	AV 0 1
762	LOAD Z	60	64	8.41	28	8.41	31	GLOR UNIF	AV 0 1
763	LOAD X	60	64	16.81	30	8.41	35	GLOR UNIF	AV 0 1
764	LOAD Y	60	64	16.81	36	8.41	39	GLOR UNIF	AV 0 1
765	LOAD Z	60	64	16.81	31	8.41	34	GLOR UNIF	AV 0 1
766	LOAD X	58	67	0.00	24	7.07	27	GLOR UNIF	AV 0 1
767	LOAD X	58	67	0.00	29	7.07	32	GLOR UNIF	AV 0 1
768	LOAD Z	58	67	0.00	25	7.07	28	GLOR UNIF	AV 0 1
769	LOAD X	58	67	7.07	27	7.07	29	GLOR UNIF	AV 0 1
770	LOAD Y	58	67	7.07	32	7.07	35	GLOR UNIF	AV 0 1
771	LOAD Z	58	67	7.07	28	7.07	30	GLOR UNIF	AV 0 1
772	LOAD X	58	67	14.14	29	7.07	31	GLOR UNIF	AV 0 1
773	LOAD Y	58	67	14.14	35	7.07	37	GLOR UNIF	AV 0 1
774	LOAD Z	58	67	14.14	30	7.07	32	GLOR UNIF	AV 0 1
775	LOAD Y	70	66	0.00	42	.33	43	GLOR UNIF	AV 0 1
776	LOAD Y	70	66	.33	43	.33	43	GLOR UNIF	AV 0 1
777	LOAD Y	70	66	.00	43	.33	43	GLOR UNIF	AV 0 1
778	LOAD Y	70	66	1.00	43	.55	43	GLOR UNIF	AV 0 1
779	LOAD Y	70	66	1.33	43	.55	43	GLOR UNIF	AV 0 1
780	LOAD Y	70	66	1.66	43	.55	44	GLOR UNIF	AV 0 1
781	LOAD Y	70	66	1.99	44	.33	44	GLOR UNIF	AV 0 1
782	LOAD Y	70	66	2.33	44	.55	44	GLOR UNIF	AV 0 1
783	LOAD Y	70	66	2.66	44	.33	43	GLOR UNIF	AV 0 1
784	LOAD Y	70	66	0.00	42	.33	43	GLOR UNIF	AV 0 1



STATE THERM DATA

3-PTILE ACVR STRUCTURE -- U.S. NAVY (38-INT. DIAMETER PILING) -- C,CHERN

LINE NO.	1	2	3	4	5	6	7	8	
785	LOAD Y	70	68	.33	43	.33	43	GLOR UNTF	WV 0 1
786	LOAD Y	70	68	.66	43	.33	43	GLOR UNTF	WV 0 1
787	LOAD Y	70	68	1.00	43	.33	43	GLOR UNTF	WV 0 1
788	LOAD Y	70	68	1.33	43	.33	43	GLOR UNTF	WV 0 1
789	LOAD Y	70	68	1.66	43	.33	44	GLOR UNTF	WV 0 1
790	LOAD Y	70	68	1.99	44	.33	44	GLOR UNTF	WV 0 1
791	LOAD Y	70	68	2.33	44	.33	44	GLOR UNTF	WV 0 1
792	LOAD Y	70	68	2.66	44	.33	44	GLOR UNTF	WV 0 1
793	TRANCN	2							
794	LOAD Y	43	55	4.08=	345			GLOR CONC	WN 1 2
795	LOAD X	43	55					GLOR MOMT	WN 1 2
796	LOAD Y	44	56	4.08=	345			GLOR CONC	WN 1 2
797	LOAD X	44	56					GLOR MOMT	WN 1 2
798	LOAD Y	45	57	4.07=	345			GLOR CONC	WN 1 2
799	LOAD X	45	57					GLOR MOMT	WN 1 2
800	LOAD Y	43	55	4.08=	1111			GLOR CONC	WN 2 2
801	LOAD X	43	55					GLOR MOMT	WN 2 2
802	LOAD Y	44	56	4.06=	1111			GLOR CONC	WN 2 2
803	LOAD X	44	56					GLOR MOMT	WN 2 2
804	LOAD Y	45	57	4.07=	1111			GLOR CONC	WN 2 2
805	LOAD X	45	57					GLOR MOMT	WN 2 2
806	LOAD X	10	22	0.00=	1	10.81=	1	GLOR UNTF	WV 0 2
807	LOAD Y	10	22	0.00=	51	10.81=	52	GLOR UNTF	WV 0 2
808	LOAD Z	10	22	0.00=	04	10.81=	04	GLOR UNTF	WV 0 2
809	LOAD X	10	22	10.81=	1	10.81=	1	GLOR UNTF	WV 0 2
810	LOAD Y	10	22	10.81=	52	10.81=	54	GLOR UNTF	WV 0 2
811	LOAD Z	10	22	10.81=	04	10.81=	04	GLOR UNTF	WV 0 2
812	LOAD X	10	22	21.63=	1	10.81=	1	GLOR UNTF	WV 0 2
813	LOAD Y	10	22	21.63=	54	10.81=	57	GLOR UNTF	WV 0 2
814	LOAD Z	10	22	21.63=	04	10.81=	05	GLOR UNTF	WV 0 2
815	LOAD X	22	34	0.00=	1	10.81=	1	GLOR UNTF	WV 0 2
816	LOAD Y	22	34	0.00=	57	10.81=	62	GLOR UNTF	WV 0 2
817	LOAD Z	22	34	0.00=	05	10.81=	05	GLOR UNTF	WV 0 2
818	LOAD X	22	34	10.81=	1	10.81=	1	GLOR UNTF	WV 0 2
819	LOAD Y	22	34	10.81=	62	10.81=	68	GLOR UNTF	WV 0 2
820	LOAD Z	22	34	10.81=	05	10.81=	05	GLOR UNTF	WV 0 2
821	LOAD X	22	34	21.63=	1	10.81=	1	GLOR UNTF	WV 0 2
822	LOAD Y	22	34	21.63=	68	10.81=	74	GLOR UNTF	WV 0 2
823	LOAD Z	22	34	21.63=	05	10.81=	04	GLOR UNTF	WV 0 2
824	LOAD X	34	40	0.00=	1	4.73=	1	GLOR UNTF	WV 0 2
825	LOAD Y	34	40	0.00=	78	4.73=	82	GLOR UNTF	WV 0 2
826	LOAD Z	34	40	0.00=	05	4.73=	06	GLOR UNTF	WV 0 2
827	LOAD X	34	40	4.73=	1	4.73=	1	GLOR UNTF	WV 0 2
828	LOAD Y	34	40	4.73=	82	4.73=	87	GLOR UNTF	WV 0 2
829	LOAD Z	34	40	4.73=	06	4.73=	04	GLOR UNTF	WV 0 2
830	LOAD X	34	40	9.45=	1	4.73=	1	GLOR UNTF	WV 0 2
831	LOAD Y	34	40	9.45=	87	4.73=	93	GLOR UNTF	WV 0 2
832	LOAD Z	34	40	9.45=	06	4.73=	06	GLOR UNTF	WV 0 2
833	LOAD X	40	48	0.00=	1	6.04=	1	GLOR UNTF	WV 0 2



SYSTEM INPUT DATA

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3-PILE ACPM STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

LTNE NU, 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000

R34	LOAD Y	40	49	0.00	92	6.09	101	GLOR UNIF	WV 0 2
R35	LOAD Z	40	49	0.00	08	6.09	09	GLOR UNIF	WV 0 2
R36	LOAD X	40	49	6.09	1	6.09	1	GLOR UNIF	WV 0 2
R37	LOAD Y	40	49	6.09	101	6.09	111	GLOR UNIF	WV 0 2
R38	LOAD Z	40	49	6.09	09	6.09	10	GLOR UNIF	WV 0 2
R39	LOAD X	40	49	12.17	1	6.09	02	GLOR UNIF	WV 0 2
R40	LOAD Y	40	49	12.17	111	6.09	123	GLOR UNIF	WV 0 2
R41	LOAD Z	40	49	12.17	10	6.09	11	GLOR UNIF	WV 0 2
R42	LOAD X	49	55	0.00	1	1.52	1	GLOR UNIF	WV 0 2
R43	LOAD Y	49	55	0.00	123	1.52	126	GLOR UNIF	WV 0 2
R44	LOAD Z	49	55	0.00	10	1.52	10	GLOR UNIF	WV 0 2
R45	LOAD X	49	55	1.52	1	1.52	1	GLOR UNIF	WV 0 2
R46	LOAD Y	49	55	1.52	126	1.52	129	GLOR UNIF	WV 0 2
R47	LOAD Z	49	55	1.52	10	1.52	11	GLOR UNIF	WV 0 2
R48	LOAD X	49	55	3.04	1	1.52	02	GLOR UNIF	WV 0 2
R49	LOAD Y	49	55	3.04	129	1.52	133	GLOR UNIF	WV 0 2
R50	LOAD Z	49	55	3.04	11	1.52	11	GLOR UNIF	WV 0 2
R51	LOAD X	12	24	0.00	1	10.81	1	GLOR UNIF	WV 0 2
R52	LOAD Y	12	24	0.00	51	10.81	52	GLOR UNIF	WV 0 2
R53	LOAD Z	12	24	0.00	04	10.81	04	GLOR UNIF	WV 0 2
R54	LOAD X	12	24	10.81	1	10.81	1	GLOR UNIF	WV 0 2
R55	LOAD Y	12	24	10.81	52	10.81	54	GLOR UNIF	WV 0 2
R56	LOAD Z	12	24	10.81	04	10.81	04	GLOR UNIF	WV 0 2
R57	LOAD X	12	24	21.63	1	10.81	1	GLOR UNIF	WV 0 2
R58	LOAD Y	12	24	21.63	54	10.81	57	GLOR UNIF	WV 0 2
R59	LOAD Z	12	24	21.63	04	10.81	05	GLOR UNIF	WV 0 2
R60	LOAD X	24	36	0.00	1	10.81	1	GLOR UNIF	WV 0 2
R61	LOAD Y	24	36	0.00	57	10.81	62	GLOR UNIF	WV 0 2
R62	LOAD Z	24	36	0.00	05	10.81	05	GLOR UNIF	WV 0 2
R63	LOAD X	24	36	10.81	1	10.81	1	GLOR UNIF	WV 0 2
R64	LOAD Y	24	36	10.81	62	10.81	64	GLOR UNIF	WV 0 2
R65	LOAD Z	24	36	10.81	05	10.81	05	GLOR UNIF	WV 0 2
R66	LOAD X	24	36	21.63	1	10.81	1	GLOR UNIF	WV 0 2
R67	LOAD Y	24	36	21.63	64	10.81	76	GLOR UNIF	WV 0 2
R68	LOAD Z	24	36	21.63	05	10.81	06	GLOR UNIF	WV 0 2
R69	LOAD X	36	41	0.00	1	4.73	1	GLOR UNIF	WV 0 2
R70	LOAD Y	36	41	0.00	78	4.73	82	GLOR UNIF	WV 0 2
R71	LOAD Z	36	41	0.00	05	4.73	06	GLOR UNIF	WV 0 2
R72	LOAD X	36	41	4.73	1	4.73	1	GLOR UNIF	WV 0 2
R73	LOAD Y	36	41	4.73	82	4.73	87	GLOR UNIF	WV 0 2
R74	LOAD Z	36	41	4.73	06	4.73	06	GLOR UNIF	WV 0 2
R75	LOAD X	36	41	9.45	1	4.73	1	GLOR UNIF	WV 0 2
R76	LOAD Y	36	41	9.45	87	4.73	93	GLOR UNIF	WV 0 2
R77	LOAD Z	36	41	9.45	06	4.73	06	GLOR UNIF	WV 0 2
R78	LOAD X	41	51	0.00	1	6.09	1	GLOR UNIF	WV 0 2
R79	LOAD Y	41	51	0.00	92	6.09	101	GLOR UNIF	WV 0 2
R80	LOAD Z	41	51	0.00	08	6.09	09	GLOR UNIF	WV 0 2
R81	LOAD X	41	51	6.09	1	6.09	1	GLOR UNIF	WV 0 2
R82	LOAD Y	41	51	6.09	101	6.09	111	GLOR UNIF	WV 0 2



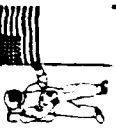
STRAN INPUT DATA

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3-PILE AC4R STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

LTNE NO. 1 2 3 4 5 6 7 8
1 1 1 1 1 1 1 1
5 5 5 5 5 5 5 5
0 0 0 0 0 0 0 0
2 2 2 2 2 2 2 2
5 5 5 5 5 5 5 5
0 0 0 0 0 0 0 0
3 3 3 3 3 3 3 3
5 5 5 5 5 5 5 5
0 0 0 0 0 0 0 0
4 4 4 4 4 4 4 4
5 5 5 5 5 5 5 5
0 0 0 0 0 0 0 0
6 6 6 6 6 6 6 6
7 7 7 7 7 7 7 7
8 8 8 8 8 8 8 8
0 0 0 0 0 0 0 0
5 5 5 5 5 5 5 5
0 0 0 0 0 0 0 0

883	LOAD Z	41	51	6.09	09	6.09	10	GLOR UNIF	MV 0 2
884	LOAD X	41	51	12.17	1	2.09	02	GLOR UNIF	MV 0 2
885	LOAD Y	41	51	12.17	111	6.09	123	GLOR UNIF	MV 0 2
886	LOAD Z	41	51	12.17	10	6.09	11	GLOR UNIF	MV 0 2
887	LOAD X	51	56	0.00	1	1.52	1	GLOR UNIF	MV 0 2
888	LOAD Y	51	56	0.00	123	1.52	126	GLOR UNIF	MV 0 2
889	LOAD Z	51	56	0.00	10	1.52	10	GLOR UNIF	MV 0 2
890	LOAD X	51	56	1.52	1	1.52	1	GLOR UNIF	MV 0 2
891	LOAD Y	51	56	1.52	126	1.52	129	GLOR UNIF	MV 0 2
892	LOAD Z	51	56	1.52	10	1.52	11	GLOR UNIF	MV 0 2
893	LOAD X	51	56	3.04	1	1.52	02	GLOR UNIF	MV 0 2
894	LOAD Y	51	56	3.04	129	1.52	133	GLOR UNIF	MV 0 2
895	LOAD Z	51	56	3.04	11	1.52	11	GLOR UNIF	MV 0 2
896	LOAD X	14	26	0.00	39	10.81	41	GLOR UNIF	MV 0 2
897	LOAD Y	14	26	0.00	07	10.81	07	GLOR UNIF	MV 0 2
898	LOAD Z	14	26	10.81	41	10.81	42	GLOR UNIF	MV 0 2
899	LOAD X	14	26	10.81	07	10.81	07	GLOR UNIF	MV 0 2
900	LOAD Y	14	26	21.63	42	10.81	46	GLOR UNIF	MV 0 2
901	LOAD Z	14	26	21.63	07	10.81	08	GLOR UNIF	MV 0 2
902	LOAD X	26	38	0.00	45	10.86	47	GLOR UNIF	MV 0 2
903	LOAD Y	26	38	0.00	09	10.86	09	GLOR UNIF	MV 0 2
904	LOAD Z	26	38	10.86	47	10.86	51	GLOR UNIF	MV 0 2
905	LOAD X	26	38	10.86	09	10.86	10	GLOR UNIF	MV 0 2
906	LOAD Y	26	38	21.72	51	10.86	55	GLOR UNIF	MV 0 2
907	LOAD Z	26	38	21.72	10	10.86	10	GLOR UNIF	MV 0 2
908	LOAD X	38	42	0.00	51	5.01	55	GLOR UNIF	MV 0 2
909	LOAD Y	38	42	0.00	20	5.01	21	GLOR UNIF	MV 0 2
910	LOAD Z	38	42	5.01	55	5.01	59	GLOR UNIF	MV 0 2
911	LOAD X	38	42	5.01	21	5.01	23	GLOR UNIF	MV 0 2
912	LOAD Y	38	42	10.02	59	5.01	64	GLOR UNIF	MV 0 2
913	LOAD Z	38	42	10.02	23	5.01	25	GLOR UNIF	MV 0 2
914	LOAD X	42	53	0.00	53	5.31	54	GLOR UNIF	MV 0 2
915	LOAD Y	42	53	0.00	53	5.31	56	GLOR UNIF	MV 0 2
916	LOAD Z	42	53	5.31	54	5.31	64	GLOR UNIF	MV 0 2
917	LOAD X	42	53	5.31	56	5.31	60	GLOR UNIF	MV 0 2
918	LOAD Y	42	53	10.63	64	5.31	70	GLOR UNIF	MV 0 2
919	LOAD Z	42	53	10.63	60	5.31	60	GLOR UNIF	MV 0 2
920	LOAD X	42	53	15.94	70	5.31	74	GLOR UNIF	MV 0 2
921	LOAD Y	42	53	15.94	64	5.31	69	GLOR UNIF	MV 0 2
922	LOAD Z	42	53	0.00	106	1.52	109	GLOR UNIF	MV 0 2
923	LOAD X	53	57	0.00	14	1.52	14	GLOR UNIF	MV 0 2
924	LOAD Y	53	57	1.52	109	1.52	113	GLOR UNIF	MV 0 2
925	LOAD Z	53	57	1.52	14	1.52	14	GLOR UNIF	MV 0 2
926	LOAD X	53	57	3.04	113	1.52	116	GLOR UNIF	MV 0 2
927	LOAD Y	53	57	3.04	19	1.52	19	GLOR UNIF	MV 0 2
928	LOAD Z	53	57	0.00	23	9.67	23	GLOR UNIF	MV 0 2
929	LOAD X	10	11	0.00	23	9.67	23	GLOR UNIF	MV 0 2
930	LOAD Y	10	11	19.33	23	9.67	23	GLOR UNIF	MV 0 2
931	LOAD Z	10	11	0.00	23	9.67	23	GLOR UNIF	MV 0 2



STA T I P I T I A

PILE AND STRUCTURE -- U.S. NAVY (30-T, DIAPHRAGM PILING) -- C. CHERA

LINE NO.	1	2	3	4	5	6	7	8	
932	LOAD Y	11	12	9.67	23	9.67	23	GLOR UNTF	AV 0 2
933	LOAD X	11	12	19.33	23	9.67	23	GLOR UNTF	AV 0 2
934	LOAD Y	12	13	0.00	10	9.67	10	GLOR UNTF	AV 0 2
935	LOAD X	12	13	0.00	06	9.67	06	GLOR UNTF	AV 0 2
936	LOAD Y	12	13	9.67	10	9.67	10	GLOR UNTF	AV 0 2
937	LOAD X	12	13	9.67	06	9.67	06	GLOR UNTF	AV 0 2
938	LOAD Y	12	13	19.55	10	9.67	09	GLOR UNTF	AV 0 2
939	LOAD X	12	13	19.55	06	9.67	05	GLOR UNTF	AV 0 2
940	LOAD Y	13	14	0.00	09	9.67	09	GLOR UNTF	AV 0 2
941	LOAD X	13	14	0.00	05	9.67	05	GLOR UNTF	AV 0 2
942	LOAD Y	13	14	9.67	09	9.67	09	GLOR UNTF	AV 0 2
943	LOAD X	13	14	9.67	05	9.67	05	GLOR UNTF	AV 0 2
944	LOAD Y	13	14	19.54	09	9.67	09	GLOR UNTF	AV 0 2
945	LOAD X	13	14	19.54	05	9.67	05	GLOR UNTF	AV 0 2
946	LOAD Y	14	15	0.00	09	9.67	09	GLOR UNTF	AV 0 2
947	LOAD X	14	15	0.00	05	9.67	05	GLOR UNTF	AV 0 2
948	LOAD Y	14	15	9.67	09	9.67	09	GLOR UNTF	AV 0 2
949	LOAD X	14	15	9.67	05	9.67	05	GLOR UNTF	AV 0 2
950	LOAD Y	14	15	19.34	09	9.67	09	GLOR UNTF	AV 0 2
951	LOAD X	14	15	19.34	05	9.67	05	GLOR UNTF	AV 0 2
952	LOAD Y	15	10	0.00	09	9.67	10	GLOR UNTF	AV 0 2
953	LOAD X	15	10	0.00	06	9.67	06	GLOR UNTF	AV 0 2
954	LOAD Y	15	10	9.67	10	9.67	10	GLOR UNTF	AV 0 2
955	LOAD X	15	10	9.67	06	9.67	06	GLOR UNTF	AV 0 2
956	LOAD Y	15	10	19.53	10	9.67	10	GLOR UNTF	AV 0 2
957	LOAD X	15	10	19.53	06	9.67	06	GLOR UNTF	AV 0 2
958	LOAD Y	11	13	0.00	08	9.67	08	GLOR UNTF	AV 0 2
959	LOAD X	11	13	0.00	04	9.67	04	GLOR UNTF	AV 0 2
960	LOAD Y	11	13	9.67	08	9.67	07	GLOR UNTF	AV 0 2
961	LOAD X	11	13	9.67	04	9.67	04	GLOR UNTF	AV 0 2
962	LOAD Y	11	13	19.33	07	9.67	07	GLOR UNTF	AV 0 2
963	LOAD X	11	13	19.33	04	9.67	04	GLOR UNTF	AV 0 2
964	LOAD Y	13	15	0.00	17	9.67	17	GLOR UNTF	AV 0 2
965	LOAD X	13	15	9.67	17	9.67	17	GLOR UNTF	AV 0 2
966	LOAD Y	13	15	19.55	17	9.67	17	GLOR UNTF	AV 0 2
967	LOAD X	13	15	0.00	07	9.67	07	GLOR UNTF	AV 0 2
968	LOAD Y	15	11	0.00	04	9.67	04	GLOR UNTF	AV 0 2
969	LOAD X	15	11	9.67	07	9.67	07	GLOR UNTF	AV 0 2
970	LOAD Y	15	11	9.67	04	9.67	04	GLOR UNTF	AV 0 2
971	LOAD X	15	11	19.33	09	9.67	09	GLOR UNTF	AV 0 2
972	LOAD Y	15	11	19.33	04	9.67	04	GLOR UNTF	AV 0 2
973	LOAD X	22	23	0.00	26	8.15	26	GLOR UNTF	AV 0 2
974	LOAD Y	22	23	8.15	26	8.15	26	GLOR UNTF	AV 0 2
975	LOAD X	22	23	16.25	26	8.15	26	GLOR UNTF	AV 0 2
976	LOAD Y	23	24	0.00	26	8.15	26	GLOR UNTF	AV 0 2
977	LOAD X	23	24	8.15	26	8.15	26	GLOR UNTF	AV 0 2
978	LOAD Y	23	24	16.25	26	8.15	26	GLOR UNTF	AV 0 2
979	LOAD X	24	25	0.00	11	8.15	11	GLOR UNTF	AV 0 2
980	LOAD Y	24	25	0.00	06	8.15	06	GLOR UNTF	AV 0 2

STRAN INPUT DATA

SOPILE ACMR STRUCTURE -- U.S. NAVY (36-14, DIAMETER PILING) -- C.CHEMN

LINE NO.	1	2	3	4	5	6	7	8	
981	LOAD X	24	25	A.13	11	A.13	11	GLOR UNTF	AV 0 2
982	LOAD Y	24	25	A.13	06	A.13	06	GLOR UNTF	AV 0 2
983	LOAD X	24	25	16.25	11	A.13	11	GLOR UNTF	AV 0 2
984	LOAD Y	24	25	16.25	06	A.13	06	GLOR UNTF	AV 0 2
985	LOAD X	25	26	0.00	11	A.13	10	GLOR UNTF	AV 0 2
986	LOAD Y	25	26	0.00	06	A.13	06	GLOR UNTF	AV 0 2
987	LOAD X	25	26	A.13	10	A.13	10	GLOR UNTF	AV 0 2
988	LOAD Y	25	26	A.13	06	A.13	06	GLOR UNTF	AV 0 2
989	LOAD X	25	26	16.25	10	A.13	09	GLOR UNTF	AV 0 2
990	LOAD Y	25	26	16.25	06	A.13	05	GLOR UNTF	AV 0 2
991	LOAD X	26	27	0.00	09	A.13	10	GLOR UNTF	AV 0 2
992	LOAD Y	26	27	0.00	05	A.13	06	GLOR UNTF	AV 0 2
993	LOAD X	26	27	A.13	10	A.13	10	GLOR UNTF	AV 0 2
994	LOAD Y	26	27	A.13	06	A.13	06	GLOR UNTF	AV 0 2
995	LOAD X	26	27	16.25	10	A.13	11	GLOR UNTF	AV 0 2
996	LOAD Y	26	27	16.25	06	A.13	06	GLOR UNTF	AV 0 2
997	LOAD X	27	22	0.00	11	A.13	11	GLOR UNTF	AV 0 2
998	LOAD Y	27	22	0.00	06	A.13	06	GLOR UNTF	AV 0 2
999	LOAD X	27	22	A.13	11	A.13	11	GLOR UNTF	AV 0 2
1000	LOAD Y	27	22	A.13	06	A.13	06	GLOR UNTF	AV 0 2
1001	LOAD X	27	22	16.25	11	A.13	11	GLOR UNTF	AV 0 2
1002	LOAD Y	27	22	16.25	06	A.13	06	GLOR UNTF	AV 0 2
1003	LOAD X	23	25	0.00	09	A.13	09	GLOR UNTF	AV 0 2
1004	LOAD Y	23	25	0.00	05	A.13	05	GLOR UNTF	AV 0 2
1005	LOAD X	23	25	A.13	09	A.13	08	GLOR UNTF	AV 0 2
1006	LOAD Y	23	25	A.13	05	A.13	05	GLOR UNTF	AV 0 2
1007	LOAD X	23	25	16.25	08	A.13	08	GLOR UNTF	AV 0 2
1008	LOAD Y	23	25	16.25	05	A.13	05	GLOR UNTF	AV 0 2
1009	LOAD X	25	27	0.00	19	A.13	19	GLOR UNTF	AV 0 2
1010	LOAD Y	25	27	A.13	19	A.13	19	GLOR UNTF	AV 0 2
1011	LOAD X	25	27	16.25	19	A.13	19	GLOR UNTF	AV 0 2
1012	LOAD Y	27	23	0.00	08	A.13	08	GLOR UNTF	AV 0 2
1013	LOAD X	27	23	0.00	05	A.13	05	GLOR UNTF	AV 0 2
1014	LOAD Y	27	23	A.13	08	A.13	09	GLOR UNTF	AV 0 2
1015	LOAD X	27	23	A.13	05	A.13	05	GLOR UNTF	AV 0 2
1016	LOAD Y	27	23	16.25	09	A.13	09	GLOR UNTF	AV 0 2
1017	LOAD X	27	23	16.25	05	A.13	05	GLOR UNTF	AV 0 2
1018	LOAD Y	34	35	0.00	24	6.59	24	GLOR UNTF	AV 0 2
1019	LOAD X	34	35	6.59	24	6.59	24	GLOR UNTF	AV 0 2
1020	LOAD Y	34	35	13.18	24	6.59	24	GLOR UNTF	AV 0 2
1021	LOAD X	35	36	0.00	24	6.59	24	GLOR UNTF	AV 0 2
1022	LOAD Y	35	36	6.59	24	6.59	24	GLOR UNTF	AV 0 2
1023	LOAD X	35	36	13.14	24	6.59	24	GLOR UNTF	AV 0 2
1024	LOAD Y	36	37	0.00	10	6.59	10	GLOR UNTF	AV 0 2
1025	LOAD X	36	37	0.00	06	6.59	06	GLOR UNTF	AV 0 2
1026	LOAD Y	36	37	6.59	10	6.59	10	GLOR UNTF	AV 0 2
1027	LOAD X	36	37	6.59	06	6.59	06	GLOR UNTF	AV 0 2
1028	LOAD Y	36	37	13.14	10	6.59	10	GLOR UNTF	AV 0 2
1029	LOAD X	36	37	13.14	06	6.59	06	GLOR UNTF	AV 0 2



STAT OUTPUT DATA

30711 ACMR STRUCTURE -- U.S. NAVY (16-IN. DIAMETER PILING) -- C.CHEMN

LINE NO.	1	2	3	4	5	6	7	8
1030	LOAD X	37	3A	0.00	07	10.07	GLOR UNIF	MV 0 2
1031	LOAD Y	37	3A	0.00	02	10.07	GLOR UNIF	MV 0 2
1032	LOAD X	37	3A	10.07	06	10.07	GLOR UNIF	MV 0 2
1033	LOAD Y	37	3A	10.07	02	10.07	GLOR UNIF	MV 0 2
1034	LOAD X	37	3A	20.15	06	10.07	GLOR UNIF	MV 0 2
1035	LOAD Y	37	3A	20.15	02	10.07	GLOR UNIF	MV 0 2
1036	LOAD X	3A	39	0.00	06	10.07	GLOR UNIF	MV 0 2
1037	LOAD Y	3A	39	0.00	02	10.07	GLOR UNIF	MV 0 2
1038	LOAD X	3A	39	10.07	06	10.07	GLOR UNIF	MV 0 2
1039	LOAD Y	3A	39	10.07	02	10.07	GLOR UNIF	MV 0 2
1040	LOAD X	3A	39	20.15	07	10.07	GLOR UNIF	MV 0 2
1041	LOAD Y	3A	39	20.15	02	10.07	GLOR UNIF	MV 0 2
1042	LOAD X	39	34	0.00	10	6.59	GLOR UNIF	MV 0 2
1043	LOAD Y	39	34	0.00	06	6.59	GLOR UNIF	MV 0 2
1044	LOAD X	39	34	6.59	10	6.59	GLOR UNIF	MV 0 2
1045	LOAD Y	39	34	6.59	06	6.59	GLOR UNIF	MV 0 2
1046	LOAD X	39	34	13.18	10	6.59	GLOR UNIF	MV 0 2
1047	LOAD Y	39	34	13.18	06	6.59	GLOR UNIF	MV 0 2
1048	LOAD X	35	37	0.00	10	6.59	GLOR UNIF	MV 0 2
1049	LOAD Y	35	37	0.00	06	6.59	GLOR UNIF	MV 0 2
1050	LOAD X	35	37	6.59	10	6.59	GLOR UNIF	MV 0 2
1051	LOAD Y	35	37	6.59	06	6.59	GLOR UNIF	MV 0 2
1052	LOAD X	35	37	13.18	10	6.59	GLOR UNIF	MV 0 2
1053	LOAD Y	35	37	13.18	06	6.59	GLOR UNIF	MV 0 2
1054	LOAD X	37	39	0.00	23	6.59	GLOR UNIF	MV 0 2
1055	LOAD Y	37	39	0.00	23	6.59	GLOR UNIF	MV 0 2
1056	LOAD X	37	39	13.17	23	6.59	GLOR UNIF	MV 0 2
1057	LOAD Y	39	35	0.00	10	6.59	GLOR UNIF	MV 0 2
1058	LOAD X	39	35	0.00	06	6.59	GLOR UNIF	MV 0 2
1059	LOAD Y	39	35	6.59	10	6.59	GLOR UNIF	MV 0 2
1060	LOAD X	39	35	6.59	06	6.59	GLOR UNIF	MV 0 2
1061	LOAD X	39	35	13.18	10	6.59	GLOR UNIF	MV 0 2
1062	LOAD Y	39	35	13.18	06	6.59	GLOR UNIF	MV 0 2
1063	LOAD Y	49	50	0.00	48	5.05	GLOR UNIF	MV 0 2
1064	LOAD Y	49	50	5.05	48	5.05	GLOR UNIF	MV 0 2
1065	LOAD Y	49	50	10.10	48	5.05	GLOR UNIF	MV 0 2
1066	LOAD Y	50	51	0.00	48	5.05	GLOR UNIF	MV 0 2
1067	LOAD Y	50	51	5.05	48	5.05	GLOR UNIF	MV 0 2
1068	LOAD Y	50	51	10.10	48	5.05	GLOR UNIF	MV 0 2
1069	LOAD X	51	52	0.00	21	5.05	GLOR UNIF	MV 0 2
1070	LOAD X	51	52	0.00	12	5.05	GLOR UNIF	MV 0 2
1071	LOAD X	51	52	5.05	21	5.05	GLOR UNIF	MV 0 2
1072	LOAD Y	51	52	5.05	12	5.05	GLOR UNIF	MV 0 2
1073	LOAD X	51	52	10.10	20	5.05	GLOR UNIF	MV 0 2
1074	LOAD Y	51	52	10.10	12	5.05	GLOR UNIF	MV 0 2
1075	LOAD X	52	53	0.00	20	5.05	GLOR UNIF	MV 0 2
1076	LOAD Y	52	53	0.00	12	5.05	GLOR UNIF	MV 0 2
1077	LOAD X	52	53	5.05	19	5.05	GLOR UNIF	MV 0 2
1078	LOAD Y	52	53	5.05	11	5.05	GLOR UNIF	MV 0 2



3-PHASE AC VR STRUCTURE -- U.S. NAVY (30-INS. DIAMETER PILING) -- C. CHERN

LINE NO. 1...5.....0.....5.....0.....2.....3.....5.....4.....5.....5.....6.....7.....8.....

1079	LOAD X	52	53	10.10	49	5.05	14	GLOR UNIF	MV 0 2
1080	LOAD Y	52	53	10.10	11	5.05	14	GLOR UNIF	MV 0 2
1081	LOAD X	53	54	0.00	14	5.05	19	GLOR UNIF	MV 0 2
1082	LOAD Y	53	54	0.00	11	5.05	19	GLOR UNIF	MV 0 2
1083	LOAD X	53	54	5.05	19	5.05	20	GLOR UNIF	MV 0 2
1084	LOAD Y	53	54	5.05	11	5.05	11	GLOR UNIF	MV 0 2
1085	LOAD X	53	54	10.10	20	5.05	20	GLOR UNIF	MV 0 2
1086	LOAD Y	53	54	10.10	11	5.05	12	GLOR UNIF	MV 0 2
1087	LOAD X	54	49	0.00	20	5.05	20	GLOR UNIF	MV 0 2
1088	LOAD Y	54	49	0.00	12	5.05	12	GLOR UNIF	MV 0 2
1089	LOAD X	54	49	5.05	21	5.05	21	GLOR UNIF	MV 0 2
1090	LOAD Y	54	49	5.05	12	5.05	12	GLOR UNIF	MV 0 2
1091	LOAD X	54	49	10.10	21	5.05	21	GLOR UNIF	MV 0 2
1092	LOAD Y	54	49	10.10	12	5.05	12	GLOR UNIF	MV 0 2
1093	LOAD X	50	52	0.00	17	5.05	16	GLOR UNIF	MV 0 2
1094	LOAD Y	50	52	0.00	10	5.05	09	GLOR UNIF	MV 0 2
1095	LOAD X	50	52	5.05	16	5.05	16	GLOR UNIF	MV 0 2
1096	LOAD Y	50	52	5.05	09	5.05	09	GLOR UNIF	MV 0 2
1097	LOAD X	50	52	10.10	16	5.05	16	GLOR UNIF	MV 0 2
1098	LOAD Y	50	52	10.10	09	5.05	09	GLOR UNIF	MV 0 2
1099	LOAD X	52	54	0.00	37	5.05	37	GLOR UNIF	MV 0 2
1100	LOAD Y	52	54	5.05	37	5.05	37	GLOR UNIF	MV 0 2
1101	LOAD X	52	54	10.09	16	5.05	16	GLOR UNIF	MV 0 2
1102	LOAD Y	54	50	0.00	16	5.05	16	GLOR UNIF	MV 0 2
1103	LOAD X	54	50	0.00	09	5.05	09	GLOR UNIF	MV 0 2
1104	LOAD Y	54	50	5.05	16	5.05	16	GLOR UNIF	MV 0 2
1105	LOAD X	54	50	5.05	09	5.05	09	GLOR UNIF	MV 0 2
1106	LOAD Y	54	50	10.10	16	5.05	17	GLOR UNIF	MV 0 2
1107	LOAD X	54	50	10.10	09	5.05	10	GLOR UNIF	MV 0 2
1108	LOAD Y	11	22	0.00	1	13.44	1	GLOR UNIF	MV 0 2
1109	LOAD X	11	22	0.00	21	13.44	21	GLOR UNIF	MV 0 2
1110	LOAD Y	11	22	0.00	1	13.44	1	GLOR UNIF	MV 0 2
1111	LOAD X	11	22	13.44	1	13.44	1	GLOR UNIF	MV 0 2
1112	LOAD Y	11	22	13.44	21	13.44	22	GLOR UNIF	MV 0 2
1113	LOAD X	11	22	13.44	1	13.44	1	GLOR UNIF	MV 0 2
1114	LOAD Y	11	22	26.88	1	13.44	1	GLOR UNIF	MV 0 2
1115	LOAD X	11	22	26.88	23	13.44	23	GLOR UNIF	MV 0 2
1116	LOAD Y	11	22	26.88	1	13.44	1	GLOR UNIF	MV 0 2
1117	LOAD X	11	24	0.00	1	13.44	1	GLOR UNIF	MV 0 2
1118	LOAD Y	11	24	0.00	21	13.44	21	GLOR UNIF	MV 0 2
1119	LOAD X	11	24	0.00	1	13.44	1	GLOR UNIF	MV 0 2
1120	LOAD Y	11	24	13.44	1	13.44	1	GLOR UNIF	MV 0 2
1121	LOAD X	11	24	13.44	21	13.44	22	GLOR UNIF	MV 0 2
1122	LOAD Y	11	24	13.44	1	13.44	1	GLOR UNIF	MV 0 2
1123	LOAD X	11	24	26.88	1	13.44	1	GLOR UNIF	MV 0 2
1124	LOAD Y	11	24	26.88	23	13.44	23	GLOR UNIF	MV 0 2
1125	LOAD X	11	24	26.88	1	13.44	1	GLOR UNIF	MV 0 2
1126	LOAD Y	13	24	0.00	03	13.44	03	GLOR UNIF	MV 0 2
1127	LOAD X	13	24	0.00	13	13.44	14	GLOR UNIF	MV 0 2



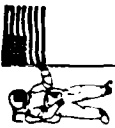


STRATAPUT DATA

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DATE 04/27/76

SOPILE ACBR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHEMN

LINE NO.	1	2	3	4	5	6	7	8							
1128	LOAD Z	13	24	0.00	08	13.04			09					GLOR UNIF	MV 0 2
1129	LOAD X	13	24	13.44	03	13.44			13					GLOR UNIF	MV 0 2
1130	LOAD Y	13	24	13.44	14	13.44			15					GLOR UNIF	MV 0 2
1131	LOAD Z	13	24	13.44	09	13.44			09					GLOR UNIF	MV 0 2
1132	LOAD X	13	24	26.88	03	13.44			03					GLOR UNIF	MV 0 2
1133	LOAD Y	13	24	26.88	15	13.44			16					GLOR UNIF	MV 0 2
1134	LOAD Z	13	24	26.88	09	13.44			10					GLOR UNIF	MV 0 2
1135	LOAD X	13	26	0.00	03	13.44			03					GLOR UNIF	MV 0 2
1136	LOAD Y	13	26	0.00	15	13.44			14					GLOR UNIF	MV 0 2
1137	LOAD Z	13	26	0.00	07	13.44			07					GLOR UNIF	MV 0 2
1138	LOAD X	13	26	13.44	03	13.44			03					GLOR UNIF	MV 0 2
1139	LOAD Y	13	26	13.44	14	13.44			14					GLOR UNIF	MV 0 2
1140	LOAD Z	13	26	13.44	07	13.44			07					GLOR UNIF	MV 0 2
1141	LOAD X	13	26	26.88	03	13.44			03					GLOR UNIF	MV 0 2
1142	LOAD Y	13	26	26.88	14	13.44			14					GLOR UNIF	MV 0 2
1143	LOAD Z	13	26	26.88	07	13.44			07					GLOR UNIF	MV 0 2
1144	LOAD X	15	26	0.00	03	13.44			03					GLOR UNIF	MV 0 2
1145	LOAD Y	15	26	0.00	15	13.44			14					GLOR UNIF	MV 0 2
1146	LOAD Z	15	26	0.00	07	13.44			07					GLOR UNIF	MV 0 2
1147	LOAD X	15	26	13.44	03	13.44			03					GLOR UNIF	MV 0 2
1148	LOAD Y	15	26	13.44	14	13.44			14					GLOR UNIF	MV 0 2
1149	LOAD Z	15	26	13.44	07	13.44			07					GLOR UNIF	MV 0 2
1150	LOAD X	15	26	26.88	03	13.44			03					GLOR UNIF	MV 0 2
1151	LOAD Y	15	26	26.88	14	13.44			14					GLOR UNIF	MV 0 2
1152	LOAD Z	15	26	26.88	07	13.44			07					GLOR UNIF	MV 0 2
1153	LOAD X	15	22	0.00	03	13.44			03					GLOR UNIF	MV 0 2
1154	LOAD Y	15	22	0.00	13	13.44			14					GLOR UNIF	MV 0 2
1155	LOAD Z	15	22	0.00	08	13.44			09					GLOR UNIF	MV 0 2
1156	LOAD X	15	22	13.44	03	13.44			03					GLOR UNIF	MV 0 2
1157	LOAD Y	15	22	13.44	14	13.44			15					GLOR UNIF	MV 0 2
1158	LOAD Z	15	22	13.44	09	13.44			09					GLOR UNIF	MV 0 2
1159	LOAD X	15	22	26.88	03	13.44			03					GLOR UNIF	MV 0 2
1160	LOAD Y	15	22	26.88	15	13.44			16					GLOR UNIF	MV 0 2
1161	LOAD Z	15	22	26.88	09	13.44			10					GLOR UNIF	MV 0 2
1162	LOAD X	22	36	0.00	1	18.20			1					GLOR UNIF	MV 0 2
1163	LOAD Y	22	36	0.00	29	18.20			31					GLOR UNIF	MV 0 2
1164	LOAD Z	22	36	0.00	1	18.20			1					GLOR UNIF	MV 0 2
1165	LOAD X	22	36	18.20	1	18.20			1					GLOR UNIF	MV 0 2
1166	LOAD Y	22	36	18.20	31	18.20			50					GLOR UNIF	MV 0 2
1167	LOAD Z	22	36	18.20	1	18.20			1					GLOR UNIF	MV 0 2
1168	LOAD X	22	36	36.39	1	18.20			1					GLOR UNIF	MV 0 2
1169	LOAD Y	22	36	36.39	34	18.20			34					GLOR UNIF	MV 0 2
1170	LOAD Z	22	36	36.39	1	18.20			1					GLOR UNIF	MV 0 2
1171	LOAD X	24	38	0.00	09	20.96			09					GLOR UNIF	MV 0 2
1172	LOAD Y	24	38	0.00	12	20.96			12					GLOR UNIF	MV 0 2
1173	LOAD Z	24	38	0.00	11	20.96			12					GLOR UNIF	MV 0 2
1174	LOAD X	24	38	20.96	09	20.96			09					GLOR UNIF	MV 0 2
1175	LOAD Y	24	38	20.96	12	20.96			12					GLOR UNIF	MV 0 2
1176	LOAD Z	24	38	20.96	12	20.96			12					GLOR UNIF	MV 0 2



TOPPLE ACWR STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. CHERN

LINE NO.	1	2	3	4	5	6	7	8
1177	LOAD X	24	34	41.93	09	20.96	GLOR UNIF	MV 0 2
1178	LOAD Y	24	34	41.93	12	20.96	GLOR UNIF	MV 0 2
1179	LOAD Z	24	34	41.93	11	20.96	GLOR UNIF	MV 0 2
1180	LOAD X	26	34	0.00	06	13.65	GLOR UNIF	MV 0 2
1181	LOAD Y	26	34	0.00	11	13.65	GLOR UNIF	MV 0 2
1182	LOAD Z	26	34	0.00	10	13.65	GLOR UNIF	MV 0 2
1183	LOAD X	26	34	13.65	07	13.65	GLOR UNIF	MV 0 2
1184	LOAD Y	26	34	13.65	13	13.65	GLOR UNIF	MV 0 2
1185	LOAD Z	26	34	13.65	11	13.65	GLOR UNIF	MV 0 2
1186	LOAD X	26	34	27.29	08	13.65	GLOR UNIF	MV 0 2
1187	LOAD Y	26	34	27.29	14	13.65	GLOR UNIF	MV 0 2
1188	LOAD Z	26	34	27.29	13	13.65	GLOR UNIF	MV 0 2
1189	LOAD X	26	34	40.91	09	13.65	GLOR UNIF	MV 0 2
1190	LOAD Y	26	34	40.91	16	13.65	GLOR UNIF	MV 0 2
1191	LOAD Z	26	34	40.91	14	13.65	GLOR UNIF	MV 0 2
1192	LOAD X	36	49	0.00	02	11.86	GLOR UNIF	MV 0 2
1193	LOAD Y	36	49	0.00	5A	11.86	GLOR UNIF	MV 0 2
1194	LOAD Z	36	49	0.00	1	11.86	GLOR UNIF	MV 0 2
1195	LOAD X	36	49	11.86	02	11.86	GLOR UNIF	MV 0 2
1196	LOAD Y	36	49	11.86	42	11.86	GLOR UNIF	MV 0 2
1197	LOAD Z	36	49	11.86	02	11.86	GLOR UNIF	MV 0 2
1198	LOAD X	36	49	23.72	02	11.86	GLOR UNIF	MV 0 2
1199	LOAD Y	36	49	23.72	46	11.86	GLOR UNIF	MV 0 2
1200	LOAD Z	36	49	23.72	02	11.86	GLOR UNIF	MV 0 2
1201	LOAD X	36	49	35.54	02	11.86	GLOR UNIF	MV 0 2
1202	LOAD Y	36	49	35.54	53	11.86	GLOR UNIF	MV 0 2
1203	LOAD Z	36	49	35.54	02	11.86	GLOR UNIF	MV 0 2
1204	LOAD X	34	51	0.00	06	9.29	GLOR UNIF	MV 0 2
1205	LOAD Y	34	51	0.00	11	9.29	GLOR UNIF	MV 0 2
1206	LOAD Z	34	51	0.00	13	9.29	GLOR UNIF	MV 0 2
1207	LOAD X	34	51	9.29	07	9.29	GLOR UNIF	MV 0 2
1208	LOAD Y	34	51	9.29	13	9.29	GLOR UNIF	MV 0 2
1209	LOAD Z	34	51	9.29	15	9.29	GLOR UNIF	MV 0 2
1210	LOAD X	34	51	18.57	08	9.29	GLOR UNIF	MV 0 2
1211	LOAD Y	34	51	18.57	15	9.29	GLOR UNIF	MV 0 2
1212	LOAD Z	34	51	18.57	17	9.29	GLOR UNIF	MV 0 2
1213	LOAD X	34	51	27.86	10	9.29	GLOR UNIF	MV 0 2
1214	LOAD Y	34	51	27.86	19	9.29	GLOR UNIF	MV 0 2
1215	LOAD Z	34	51	27.86	21	9.29	GLOR UNIF	MV 0 2
1216	LOAD X	34	51	37.14	10	9.29	GLOR UNIF	MV 0 2
1217	LOAD Y	34	51	37.14	19	9.29	GLOR UNIF	MV 0 2
1218	LOAD Z	34	51	37.14	22	9.29	GLOR UNIF	MV 0 2
1219	LOAD X	34	51	46.43	11	9.29	GLOR UNIF	MV 0 2
1220	LOAD Y	34	51	46.43	22	9.29	GLOR UNIF	MV 0 2
1221	LOAD Z	34	51	46.43	24	9.29	GLOR UNIF	MV 0 2
1222	LOAD X	34	53	0.00	10	15.81	GLOR UNIF	MV 0 2
1223	LOAD Y	34	53	0.00	24	15.81	GLOR UNIF	MV 0 2
1224	LOAD Z	34	53	0.00	16	15.81	GLOR UNIF	MV 0 2
1225	LOAD X	34	53	15.81	11	15.81	GLOR UNIF	MV 0 2



STRUCTURE DATA

30PILF ACMR STRUCTURE -- U.S. NAVY (ADPT. DIAMETER PILING) -- C. CHERN

LINE NO.	1	2	3	4	5	6	7	8	
1226	LOAD Y	34	53	15.81	27	15.81	30	GLOR UNIF	WV 0 2
1227	LOAD Z	34	53	15.81	17	15.81	20	GLOR UNIF	WV 0 2
1228	LOAD X	34	53	31.62	12	15.81	13	GLOR UNIF	WV 0 2
1229	LOAD Y	34	53	31.62	30	15.81	33	GLOR UNIF	WV 0 2
1230	LOAD Z	34	53	31.62	20	15.81	22	GLOR UNIF	WV 0 2
1231	LOAD Y	55	54	0.00	117	5.70	150	GLOR UNIF	WV 0 2
1232	LOAD Y	55	54	5.70	130	5.70	144	GLOR UNIF	WV 0 2
1233	LOAD Y	55	54	11.40	146	5.70	163	GLOR UNIF	WV 0 2
1234	LOAD Y	55	54	17.10	163	5.70	185	GLOR UNIF	WV 0 2
1235	LOAD Y	55	54	22.80	185	5.70	210	GLOR UNIF	WV 0 2
1236	LOAD Y	58	61	0.00	210	3.97	229	GLOR UNIF	WV 0 2
1237	LOAD Y	58	61	3.97	229	3.97	248	GLOR UNIF	WV 0 2
1238	LOAD Y	58	61	7.95	248	3.97	275	GLOR UNIF	WV 0 2
1239	LOAD Y	56	59	0.00	117	5.70	150	GLOR UNIF	WV 0 2
1240	LOAD Y	56	59	5.70	130	5.70	144	GLOR UNIF	WV 0 2
1241	LOAD Y	56	59	11.40	146	5.70	163	GLOR UNIF	WV 0 2
1242	LOAD Y	56	59	17.10	163	5.70	185	GLOR UNIF	WV 0 2
1243	LOAD Y	56	59	22.80	185	5.70	210	GLOR UNIF	WV 0 2
1244	LOAD Y	59	64	0.00	210	3.97	229	GLOR UNIF	WV 0 2
1245	LOAD Y	59	64	3.97	229	3.97	248	GLOR UNIF	WV 0 2
1246	LOAD Y	59	64	7.95	248	3.97	275	GLOR UNIF	WV 0 2
1247	LOAD Y	57	60	0.00	104	5.70	116	GLOR UNIF	WV 0 2
1248	LOAD Y	57	60	5.70	116	5.70	129	GLOR UNIF	WV 0 2
1249	LOAD Y	57	60	11.40	129	5.70	144	GLOR UNIF	WV 0 2
1250	LOAD Y	57	60	17.10	144	5.70	163	GLOR UNIF	WV 0 2
1251	LOAD Y	57	60	22.80	163	5.70	183	GLOR UNIF	WV 0 2
1252	LOAD Y	60	70	0.00	183	2.00	192	GLOR UNIF	WV 0 2
1253	LOAD Y	60	70	2.00	192	2.00	201	GLOR UNIF	WV 0 2
1254	LOAD Y	60	70	4.00	201	2.00	209	GLOR UNIF	WV 0 2
1255	LOAD Y	70	67	0.00	209	1.35	215	GLOR UNIF	WV 0 2
1256	LOAD Y	70	67	1.35	215	1.35	223	GLOR UNIF	WV 0 2
1257	LOAD Y	70	67	2.71	223	1.35	231	GLOR UNIF	WV 0 2
1258	LOAD Y	58	59	0.00	74	9.67	74	GLOR UNIF	WV 0 2
1259	LOAD Y	58	59	9.67	74	9.67	74	GLOR UNIF	WV 0 2
1260	LOAD Y	58	59	19.33	74	9.67	74	GLOR UNIF	WV 0 2
1261	LOAD X	59	60	0.00	32	9.67	31	GLOR UNIF	WV 0 2
1262	LOAD Y	59	60	0.00	19	9.67	14	GLOR UNIF	WV 0 2
1263	LOAD X	59	60	9.67	31	9.67	30	GLOR UNIF	WV 0 2
1264	LOAD X	59	60	9.67	18	9.67	17	GLOR UNIF	WV 0 2
1265	LOAD X	59	60	19.33	30	9.67	28	GLOR UNIF	WV 0 2
1266	LOAD Y	59	60	19.33	17	9.67	16	GLOR UNIF	WV 0 2
1267	LOAD X	60	58	0.00	28	9.67	30	GLOR UNIF	WV 0 2
1268	LOAD X	60	58	0.00	16	9.67	17	GLOR UNIF	WV 0 2
1269	LOAD X	60	58	9.67	30	9.67	31	GLOR UNIF	WV 0 2
1270	LOAD Y	60	58	9.67	17	9.67	18	GLOR UNIF	WV 0 2
1271	LOAD X	60	58	19.33	31	9.67	32	GLOR UNIF	WV 0 2
1272	LOAD Y	60	58	19.33	18	9.67	19	GLOR UNIF	WV 0 2
1273	LOAD Y	59	61	0.00	74	8.65	81	GLOR UNIF	WV 0 2
1274	LOAD Y	59	61	8.65	81	8.65	88	GLOR UNIF	WV 0 2



3-PILE ACHR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

LINE NO.	1	2	3	4	5	6	7	8
1275	LOAD Y	59	61	17.29	RA	8.65	GLOR UNTF	WV 0 2
1276	LOAD X	60	64	0.00	22	6.25	GLOR UNTF	WV 0 2
1277	LOAD Y	60	64	0.00	24	6.25	GLOR UNTF	WV 0 2
1278	LOAD Z	60	64	0.00	23	6.25	GLOR UNTF	WV 0 2
1279	LOAD X	60	64	6.25	25	6.25	GLOR UNTF	WV 0 2
1280	LOAD Y	60	64	6.25	29	6.25	GLOR UNTF	WV 0 2
1281	LOAD Z	60	64	6.25	25	6.25	GLOR UNTF	WV 0 2
1282	LOAD X	60	64	12.49	27	6.25	GLOR UNTF	WV 0 2
1283	LOAD Y	60	64	12.49	32	6.25	GLOR UNTF	WV 0 2
1284	LOAD Z	60	64	12.49	28	6.25	GLOR UNTF	WV 0 2
1285	LOAD X	60	64	18.74	30	6.25	GLOR UNTF	WV 0 2
1286	LOAD Y	60	64	18.74	36	6.25	GLOR UNTF	WV 0 2
1287	LOAD Z	60	64	18.74	31	6.25	GLOR UNTF	WV 0 2
1288	LOAD X	58	67	0.00	25	7.69	GLOR UNTF	WV 0 2
1289	LOAD Y	58	67	0.00	30	7.69	GLOR UNTF	WV 0 2
1290	LOAD Z	58	67	0.00	26	7.69	GLOR UNTF	WV 0 2
1291	LOAD X	58	67	7.69	27	7.69	GLOR UNTF	WV 0 2
1292	LOAD Y	58	67	7.69	32	7.69	GLOR UNTF	WV 0 2
1293	LOAD Z	58	67	7.69	28	7.69	GLOR UNTF	WV 0 2
1294	LOAD X	58	67	15.38	29	7.69	GLOR UNTF	WV 0 2
1295	LOAD Y	58	67	15.38	34	7.69	GLOR UNTF	WV 0 2
1296	LOAD Z	58	67	15.38	31	7.69	GLOR UNTF	WV 0 2
1297	LOAD X	70	66	0.00	38	2.02	GLOR UNTF	WV 0 2
1298	LOAD Y	70	66	2.02	40	2.02	GLOR UNTF	WV 0 2
1299	LOAD Z	70	66	4.04	41	2.02	GLOR UNTF	WV 0 2
1300	LOAD X	70	68	0.00	38	2.02	GLOR UNTF	WV 0 2
1301	LOAD Y	70	68	2.02	40	2.02	GLOR UNTF	WV 0 2
1302	LOAD Z	70	68	4.04	41	2.02	GLOR UNTF	WV 0 2
1303	LOADCN	3						
1304	LOAD Z	1	4	0.00	557	6.06	GLOR UNTF	DL 0 3
1305	LOAD Z	4	16	0.00	557	32.44	GLOR UNTF	DL 0 3
1306	LOAD Z	16	28	0.00	403	32.44	GLOR UNTF	DL 0 3
1307	LOAD Z	28	43	0.00	403	32.44	GLOR UNTF	DL 0 3
1308	LOAD Z	43	55	0.00	403	4.59	GLOR UNTF	DL 0 3
1309	LOAD Z	2	5	0.00	557	6.06	GLOR UNTF	DL 0 3
1310	LOAD Z	5	17	0.00	557	32.44	GLOR UNTF	DL 0 3
1311	LOAD Z	17	29	0.00	403	32.44	GLOR UNTF	DL 0 3
1312	LOAD Z	29	44	0.00	403	32.44	GLOR UNTF	DL 0 3
1313	LOAD Z	44	56	0.00	403	4.59	GLOR UNTF	DL 0 3
1314	LOAD Z	3	6	0.00	557	6.06	GLOR UNTF	DL 0 3
1315	LOAD Z	6	18	0.00	557	32.44	GLOR UNTF	DL 0 3
1316	LOAD Z	18	30	0.00	403	32.44	GLOR UNTF	DL 0 3
1317	LOAD Z	30	45	0.00	403	36.13	GLOR UNTF	DL 0 3
1318	LOAD Z	45	57	0.00	403	4.54	GLOR UNTF	DL 0 3
1319	LOAD Z	10	22	0.00	183	32.44	GLOR UNTF	DL 0 3
1320	LOAD Z	22	34	0.00	183	32.44	GLOR UNTF	DL 0 3
1321	LOAD Z	34	40	0.00	371	14.18	GLOR UNTF	DL 0 3
1322	LOAD Z	40	49	0.00	371	18.26	GLOR UNTF	DL 0 3
1323	LOAD Z	49	55	0.00	371	4.56	GLOR UNTF	DL 0 3

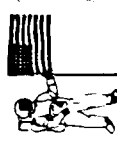


STATE INPUT DATA

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3-PTILE AC-BR STRUCTURE -- U.S. NAVY (30-IN. DIAMETER PILING) -- C.CHERN

LINE NO.	1	2	3	4	5	6	7	8	9	10	UNIT	DL
1324	LOAD Z	12	24	0.00	-.143	32.40	-.143				GLOR UNTF	DL 0 3
1325	LOAD Z	24	36	0.00	-.143	32.40	-.143				GLOR UNTF	DL 0 3
1326	LOAD Z	36	48	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1327	LOAD Z	48	60	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1328	LOAD Z	60	72	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1329	LOAD Z	72	84	0.00	-.143	32.40	-.143				GLOR UNTF	DL 0 3
1330	LOAD Z	84	96	0.00	-.143	32.40	-.143				GLOR UNTF	DL 0 3
1331	LOAD Z	96	108	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1332	LOAD Z	108	120	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1333	LOAD Z	120	132	0.00	-.371	14.24	-.371				GLOR UNTF	DL 0 3
1334	LOAD Z	132	144	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1335	LOAD Z	144	156	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1336	LOAD Z	156	168	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1337	LOAD Z	168	180	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1338	LOAD Z	180	192	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1339	LOAD Z	192	204	1.71	-.041	25.54	-.041				GLOR UNTF	DL 0 3
1340	LOAD Z	204	216	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1341	LOAD Z	216	228	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1342	LOAD Z	228	240	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1343	LOAD Z	240	252	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1344	LOAD Z	252	264	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1345	LOAD Z	264	276	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1346	LOAD Z	276	288	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1347	LOAD Z	288	300	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1348	LOAD Z	300	312	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1349	LOAD Z	312	324	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1350	LOAD Z	324	336	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1351	LOAD Z	336	348	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1352	LOAD Z	348	360	1.41	-.047	26.17	-.047				GLOR UNTF	DL 0 3
1353	LOAD Z	360	372	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1354	LOAD Z	372	384	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1355	LOAD Z	384	396	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1356	LOAD Z	396	408	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1357	LOAD Z	408	420	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1358	LOAD Z	420	432	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1359	LOAD Z	432	444	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1360	LOAD Z	444	456	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1361	LOAD Z	456	468	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1362	LOAD Z	468	480	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1363	LOAD Z	480	492	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1364	LOAD Z	492	504	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1365	LOAD Z	504	516	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1366	LOAD Z	516	528	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1367	LOAD Z	528	540	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1368	LOAD Z	540	552	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1369	LOAD Z	552	564	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1370	LOAD Z	564	576	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1371	LOAD Z	576	588	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3
1372	LOAD Z	588	600	1.71	-.041	20.96	-.041				GLOR UNTF	DL 0 3



STRAS INPUT DATA

30PILE ACMR STRUCTURE -- U.S. NAVY (40-74) DIAPHRAGM PTLTAG -- C. CHERN

LINE NO.	1	2	3	4	5	6	7	8	9	10	UNITF				
1373	LOAD	Z	13	26	1.71	.072	36.90	.072			GLOR	UNITF	DL	0	3
1374	LOAD	Z	15	26	1.71	.072	36.90	.072			GLOR	UNITF	DL	0	3
1375	LOAD	Z	15	22	1.71	.072	36.89	.072			GLOR	UNITF	DL	0	3
1376	LOAD	Z	22	38	2.42	.112	49.76	.112			GLOR	UNITF	DL	0	3
1377	LOAD	Z	24	38	2.42	.112	58.06	.112			GLOR	UNITF	DL	0	3
1378	LOAD	Z	24	34	2.42	.112	49.76	.112			GLOR	UNITF	DL	0	3
1379	LOAD	Z	36	49	2.42	.112	42.61	.112			GLOR	UNITF	DL	0	3
1380	LOAD	Z	38	51	2.42	.112	50.89	.112			GLOR	UNITF	DL	0	3
1381	LOAD	Z	34	53	2.42	.112	42.60	.112			GLOR	UNITF	DL	0	3
1382	LOAD	Z	4	7	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1383	LOAD	Z	7	10	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1384	LOAD	Z	5	8	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1385	LOAD	Z	8	12	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1386	LOAD	Z	6	9	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1387	LOAD	Z	9	14	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1388	LOAD	Z	16	19	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1389	LOAD	Z	19	22	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1390	LOAD	Z	17	20	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1391	LOAD	Z	20	24	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1392	LOAD	Z	18	21	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1393	LOAD	Z	21	26	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1394	LOAD	Z	28	31	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1395	LOAD	Z	31	34	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1396	LOAD	Z	29	32	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1397	LOAD	Z	32	36	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1398	LOAD	Z	30	33	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1399	LOAD	Z	33	38	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1400	LOAD	Z	43	46	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1401	LOAD	Z	46	49	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1402	LOAD	Z	44	47	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1403	LOAD	Z	47	51	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1404	LOAD	Z	45	48	0.00	.000	2.00	.000			GLOR	UNITF	DL	0	3
1405	LOAD	Z	48	53	0.00	.000	2.50	.000			GLOR	UNITF	DL	0	3
1406	LOAD	Z	55	54	0.00	.003	23.00	.003			GLOR	UNITF	DL	0	3
1407	LOAD	Z	55	58	25.00	.000	5.50	.000			GLOR	UNITF	DL	0	3
1408	LOAD	Z	58	61	0.00	.000	15.00	.000			GLOR	UNITF	DL	0	3
1409	LOAD	Z	61	71	0.00	.000	15.00	.000			GLOR	UNITF	DL	0	3
1410	LOAD	Z	54	59	0.00	.003	23.00	.003			GLOR	UNITF	DL	0	3
1411	LOAD	Z	56	59	23.00	.000	5.50	.000			GLOR	UNITF	DL	0	3
1412	LOAD	Z	59	64	0.00	.000	15.00	.000			GLOR	UNITF	DL	0	3
1413	LOAD	Z	64	72	0.00	.000	15.00	.000			GLOR	UNITF	DL	0	3
1414	LOAD	Z	57	60	0.00	.003	23.00	.003			GLOR	UNITF	DL	0	3
1415	LOAD	Z	57	60	23.00	.000	5.50	.000			GLOR	UNITF	DL	0	3
1416	LOAD	Z	60	70	0.00	.000	9.00	.000			GLOR	UNITF	DL	0	3
1417	LOAD	Z	70	67	0.00	.000	9.00	.000			GLOR	UNITF	DL	0	3
1418	LOAD	Z	67	76	0.00	.000	4.00	.000			GLOR	UNITF	DL	0	3
1419	LOAD	Z	76	75	0.00	.000	11.00	.000			GLOR	UNITF	DL	0	3
1420	LOAD	Z	58	59	1.71	.065	25.58	.065			GLOR	UNITF	DL	0	3
1421	LOAD	Z	59	60	1.71	.065	25.58	.065			GLOR	UNITF	DL	0	3



30PILE ACMR STRUCTURE -- U.S. NAVY (36-I. DIAFTER PILING) -- C. CMERN

LINE NO. 1... 2... 3... 4... 5... 6... 7... 8

1422	LOAD Z	60	58	1.71	0.065	25.58	0.065	GLOR UNIF	DL 0 3
1423	LOAD Z	59	61	1.71	0.065	29.23	0.065	GLOR UNIF	DL 0 3
1424	LOAD Z	60	64	1.71	0.065	29.23	0.065	GLOR UNIF	DL 0 3
1425	LOAD Z	58	67	1.71	0.065	29.23	0.065	GLOR UNIF	DL 0 3
1426	LOAD Z	70	66	1.59	0.019	10.27	0.019	GLOR UNIF	DL 0 3
1427	LOAD Z	70	68	1.59	0.019	10.27	0.019	GLOR UNIF	DL 0 3
1428	LOAD Z	76	77	1.71	0.050	14.74	0.050	GLOR UNIF	DL 0 3
1429	LOAD Z	76	78	1.71	0.050	14.74	0.050	GLOR UNIF	DL 0 3
1430	LOAD Z	61	62	0.00	0.055	4.50	0.055	GLOR UNIF	DL 0 3
1431	LOAD Z	62	63	0.00	0.055	20.00	0.055	GLOR UNIF	DL 0 3
1432	LOAD Z	63	64	0.00	0.055	4.50	0.055	GLOR UNIF	DL 0 3
1433	LOAD Z	64	65	0.00	0.055	8.75	0.055	GLOR UNIF	DL 0 3
1434	LOAD Z	65	67	0.00	0.055	20.25	0.055	GLOR UNIF	DL 0 3
1435	LOAD Z	67	69	0.00	0.055	20.25	0.055	GLOR UNIF	DL 0 3
1436	LOAD Z	69	61	0.00	0.055	8.75	0.055	GLOR UNIF	DL 0 3
1437	LOAD Z	63	65	0.00	0.024	7.50	0.024	GLOR UNIF	DL 0 3
1438	LOAD Z	65	66	0.00	0.024	17.61	0.024	GLOR UNIF	DL 0 3
1439	LOAD Z	66	67	0.00	0.024	10.00	0.024	GLOR UNIF	DL 0 3
1440	LOAD Z	67	68	0.00	0.024	10.00	0.024	GLOR UNIF	DL 0 3
1441	LOAD Z	68	69	0.00	0.024	17.61	0.024	GLOR UNIF	DL 0 3
1442	LOAD Z	69	62	0.00	0.024	7.50	0.024	GLOR UNIF	DL 0 3
1443	LOAD Z	71	73	0.00	0.055	3.00	0.055	GLOR UNIF	DL 0 3
1444	LOAD Z	71	72	0.00	0.055	29.00	0.055	GLOR UNIF	DL 0 3
1445	LOAD Z	72	74	0.00	0.055	3.00	0.055	GLOR UNIF	DL 0 3
1446	LOAD Z	71	81	0.00	0.055	5.00	0.055	GLOR UNIF	DL 0 3
1447	LOAD Z	71	77	0.00	0.055	25.11	0.055	GLOR UNIF	DL 0 3
1448	LOAD Z	77	83	0.00	0.055	5.00	0.055	GLOR UNIF	DL 0 3
1449	LOAD Z	72	82	0.00	0.055	5.00	0.055	GLOR UNIF	DL 0 3
1450	LOAD Z	72	78	0.00	0.055	25.11	0.055	GLOR UNIF	DL 0 3
1451	LOAD Z	78	84	0.00	0.055	5.00	0.055	GLOR UNIF	DL 0 3
1452	LOAD Z	77	79	0.00	0.055	3.00	0.055	GLOR UNIF	DL 0 3
1453	LOAD Z	77	75	0.00	0.055	14.50	0.055	GLOR UNIF	DL 0 3
1454	LOAD Z	75	78	0.00	0.055	14.50	0.055	GLOR UNIF	DL 0 3
1455	LOAD Z	78	80	0.00	0.055	3.00	0.055	GLOR UNIF	DL 0 3
1456	LOAD Z	71	75	0.00	0.016	29.00	0.016	GLOR UNIF	DL 0 3
1457	LOAD Z	72	75	0.00	0.016	29.00	0.016	GLOR UNIF	DL 0 3
1458	LOADCN	4							
1459	LOAD Y	40	49	89	242			GLOR CONC	HOAT LNG
1460	LOAD Y	41	51	89	242			GLOR CONC	HOAT LNG
1461	LOAD Y	55	58	242	406			GLOR CONC	STAIRS
1462	LOAD Y	56	59	242	406			GLOR CONC	STAIRS
1463	LOADCN	5							
1464	LOAD Z	61	62		-13			GLOR UNIF	ADD DEAD
1465	LOAD Z	62	63		-13			GLOR UNIF	ADD DEAD
1466	LOAD Z	63	64		-13			GLOR UNIF	ADD DEAD
1467	LOAD Z	64	65		-13			GLOR UNIF	ADD DEAD
1468	LOAD Z	65	67		-13			GLOR UNIF	ADD DEAD
1469	LOAD Z	67	69		-13			GLOR UNIF	ADD DEAD
1470	LOAD Z	69	61		-13			GLOR UNIF	ADD DEAD



STAY DEFLECTIONS AND ROTATIONS

PAGE 1
DATE 04/27/76

LOAD CONDITION NO. 1
S-PILE ARCH STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

JOINT NUMBER	X	DEFLECTION IN INCHES	Z	X	ROTATION IN RADIANS	Y	Z	REMARKS
1	0.00000	0.00000	0.00000	.00437	-.00079	-.00091		
2	0.00000	0.00000	0.00000	.00456	-.00043	.00101		
3	0.00000	0.00000	0.00000	.00500	-.00065	.00047		
4	.05329	.51334	.01898	.00394	-.00077	-.00086		
5	.03533	.52816	.00871	.00415	-.00045	.00096		
6	.04145	.34606	.03331	.00431	-.00065	.00047		
7	.96415	.35424	.23043	.00262	-.00063	-.00086		
8	.83222	.24750	.52287	.00297	.00021	.00096		
9	.97180	.55101	.45048	.00224	.00003	.00047		
10	.93833	.35729	.15196	.00262	.00063	-.00086		
11	.90151	.44294	.31612	.00324	.00034	.00007		
12	.86699	.30040	.43344	.00297	.00021	.00096		
13	.93522	.41510	.23492	.00239	-.00027	.00018		
14	.95779	.35617	.78328	.00224	.00003	.00046		
15	.92154	.44754	.29163	.00224	.00082	-.00008		
16	.29041	1.36297	.09161	.00220	.00053	.00070		
17	.24264	1.44661	.02342	.00223	-.00051	.00074		
18	.24229	1.30623	.09657	.00247	-.00055	.00059		
19	.73731	1.37886	.17583	.00257	.00033	-.00072		
20	.75246	1.42675	.40551	.00264	.00045	.00075		
21	.91751	1.31360	.71756	.00314	.00114	.00059		
22	.71554	1.37796	.09876	.00257	.00033	-.00073		
23	.74542	1.36513	.22114	.00196	.00039	.00007		
24	.77506	1.42598	.52635	.00264	.00045	.00076		
25	.77783	1.34196	.13204	.00137	-.00014	.00004		
26	.89962	1.32128	.00319	.00319	.00014	.00060		
27	.76976	1.37423	.22420	.00125	.00074	.00026		
28	.40823	2.27734	.11675	.00175	-.00016	.00045		
29	.41704	2.29648	.00165	.00150	.00027	.00057		
30	.44444	2.44937	.25768	.00168	.00024	.00060		
31	.61276	2.28683	.00865	.00102	.00043	-.00046		
32	.56957	2.29104	.18895	.00131	.00055	.00058		
33	.82109	2.43271	.70191	.00015	.00083	.00060		
34	.59896	2.28783	.00611	.00142	.00043	-.00046		
35	.59980	2.35953	.06688	.00160	.00023	.00001		
36	.58712	2.29199	.10978	.00131	.00055	.00059		
37	.61524	2.33308	.23098	.00166	.00042	.00053		
38	.80310	2.41535	.69756	.00015	.00083	.00060		
39	.59943	2.37249	.31712	.00143	.00024	.00019		
40	.51042	2.53343	.02831	.00163	.00050	.00035		
41	.50924	2.51677	.10284	.00146	.00047	.00042		
42	.60023	2.40528	.64627	.00096	.00099	.00073		
43	.38555	3.09363	.11367	.00340	.00032	.00045		
44	.43480	3.04198	.00596	.00367	.00020	.00049		
45	.31630	2.94582	.15463	.00392	.00034	.00058		
46	.40521	3.09401	.01520	.00384	.00045	.00046		
47	.42068	3.04224	.13092	.00373	.00031	.00050		
48	.50010	2.98996	.51399	.00415	.00059	.00058		



STERN - JET DEFLECTIONS AND ROTATIONS

PAGE 2
DATE 04/27/76

LOAD CONDITION NO. 1 SPTLE ACMR STRUCTURE -- U.S. NAVY (3A-JP, DIAMETER PILING) -- C. CHERN

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	X	Y	Z	X	Y	Z	REMARKS
49	-.59126	3.09350	-.10064	-.00584	.00045	-.00047	
50	-.01281	3.03520	-.00700	-.00160	.00031	-.00015	
51	-.03577	3.04190	-.01900	-.00373	.00031	-.00051	
52	-.00200	3.03425	-.07588	-.00043	.00045	-.00045	
53	-.32251	2.99427	-.14962	-.00415	.00059	-.00059	
54	-.19670	3.02245	-.15053	-.00030	.00147	-.00016	
55	-.36534	3.32410	-.12579	-.00467	.00037	-.00051	
56	-.42260	3.27200	-.01165	-.00458	.00031	-.00056	
57	-.29003	3.23364	-.13143	-.00490	.00042	-.00056	
58	-.27433	5.04007	-.11881	-.00511	.00036	-.00144	
59	-.26202	4.99027	-.00347	-.00304	.00030	-.00156	
60	-.20643	5.02591	-.14587	-.00299	.00025	-.00026	
61	-.20049	5.33761	-.11880	-.00075	.00039	-.00159	
62	-.20397	5.33441	-.09812	-.00048	.00038	-.00039	
63	-.21967	5.35489	-.01519	-.00054	.00030	-.00109	
64	-.22517	5.27982	-.00035	-.00081	.00027	-.00161	
65	-.32843	5.35506	-.05852	-.00037	.00009	-.00046	
66	-.15944	5.35495	-.11648	-.00036	.00030	-.00102	
67	-.15934	5.28675	-.10981	-.00068	.00021	-.00031	
68	-.15953	5.33290	-.17888	-.00028	.00026	-.00028	
69	-.17107	5.33293	-.13628	-.00031	.00058	-.00060	
70	-.18750	5.18412	-.10745	-.00151	.00028	-.00028	
71	-.14195	5.40790	-.11879	-.00053	.00029	-.00158	
72	-.14751	5.42605	-.00030	-.00081	.00049	-.00160	
73	-.14195	5.39104	-.12931	-.00053	.00029	-.00158	
74	-.14751	5.36916	-.01811	-.00081	.00049	-.00160	
75	-.13683	5.42647	-.10983	-.00082	.00008	-.00030	
76	-.15064	5.32119	-.10983	-.00075	.00015	-.00031	
77	-.13661	5.40792	-.16883	-.00007	.00011	-.00043	
78	-.13707	5.42608	-.13258	-.00034	.00010	-.00039	
79	-.13661	5.46335	-.17290	-.00007	.00011	-.00043	
80	-.13707	5.44039	-.12809	-.00030	.00010	-.00039	
81	-.23673	5.40790	-.08873	-.00053	.00029	-.00158	
82	-.05173	5.42605	-.00915	-.00081	.00009	-.00160	
83	-.16232	5.40792	-.17299	-.00007	.00011	-.00043	
84	-.11390	5.42608	-.15315	-.00034	.00010	-.00039	



STRAIN - JOINT DEFLECTIONS AND ROTATIONS

PAGE 3
DATE 04/27/76

LOAD CONDITION NO. 2

3-PILE ACHR STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - CACHERN

REMARKS

7

ROTATION IN RADIANS

7

7

DEFLECTION IN INCHES

7

JOINT NUMBER

JOINT NUMBER	DEFLECTION IN INCHES	ROTATION IN RADIANS	REMARKS
1	0.00000	0.00000	0.00000
2	0.00000	0.00000	0.00000
3	0.00000	0.00000	0.00000
4	0.04042	0.31212	0.00042
5	0.22500	0.52902	0.00225
6	0.27850	0.30493	0.00278
7	0.71370	0.54310	0.00713
8	0.58634	0.50472	0.00586
9	0.69747	0.54986	0.00697
10	0.64534	0.50614	0.00645
11	0.64906	0.42285	0.00649
12	0.61441	0.51165	0.00614
13	0.67246	0.42000	0.00672
14	0.64534	0.55500	0.00645
15	0.65903	0.44090	0.00659
16	0.21187	0.55924	0.00211
17	0.14499	0.54301	0.00144
18	0.15971	0.50041	0.00159
19	0.26400	0.37117	0.00264
20	0.40040	0.43009	0.00400
21	0.68475	0.31142	0.00684
22	0.50210	0.36927	0.00502
23	0.53240	0.36552	0.00532
24	0.62446	0.43831	0.00624
25	0.55584	0.54724	0.00555
26	0.66855	0.31954	0.00668
27	0.54757	0.36904	0.00547
28	0.28294	0.27101	0.00282
29	0.24304	0.30841	0.00243
30	0.30174	0.45044	0.00301
31	0.40077	0.27456	0.00400
32	0.39632	0.30503	0.00396
33	0.18661	0.45416	0.00186
34	0.42501	0.31048	0.00425
35	0.41599	0.25617	0.00415
36	0.41323	0.30599	0.00413
37	0.43153	0.34040	0.00431
38	0.60245	0.241674	0.00602
39	0.41547	0.30495	0.00415
40	0.55514	0.27115	0.00555
41	0.54284	0.25296	0.00542
42	0.42185	0.40454	0.00421
43	0.25123	0.50123	0.00251
44	0.30144	0.365715	0.00301
45	0.16844	0.299020	0.00168
46	0.27207	0.50216	0.00272
47	0.24764	0.30577	0.00247
48	0.18757	0.299433	0.00187



STRAN • JOINT DEFLECTIONS AND ROTATIONS

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LOAD CONDITION NO. 2

3-PILE ACW STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

JOINT NUMBR / REFLECTION IN INCHES / ROTATION IN RADIANS / MARKS

X Y X Y

49	.25593	-3.09171	.04171	.00388	.00037	.00054
50	.27796	-3.03876	.00706	.00170	.00020	.00010
51	.30140	-3.05701	.00034	.00377	.00023	.00046
52	.25964	-3.04399	.08574	.00045	.00096	.00051
53	.17215	-2.99864	.19645	.00418	.00054	.00052
54	.25430	-3.02387	.14221	.00029	.00158	.00019
55	.23359	-3.32937	.10753	.00471	.00031	.00059
56	.29211	-3.28465	.03012	.00460	.00025	.00051
57	.14257	-3.23984	.13232	.00494	.00039	.00049
58	.16983	-5.05454	.10053	.00313	.00027	.00153
59	.15720	-5.03620	.02234	.00314	.00021	.00152
60	.07301	-5.05627	.10706	.00306	.00017	.00019
61	.11448	-5.35314	.10054	.00076	.00020	.00168
62	.11791	-5.35926	.08551	.00048	.00027	.00019
63	.13338	-5.40720	.02818	.00654	.00020	.00112
64	.13682	-5.33110	.01842	.00083	.00016	.00156
65	.24230	-5.60743	.07283	.00040	.00006	.00040
66	.04031	-5.40755	.12774	.00019	.00022	.00095
67	.04022	-5.32253	.15105	.00068	.00013	.00025
68	.04022	-5.35806	.16981	.00013	.00017	.00006
69	.06995	-5.35780	.12460	.00035	.00052	.00015
70	.05925	-5.21451	.14845	.00155	.00020	.00022
71	.07450	-5.46343	.10052	.00053	.00019	.00166
72	.08015	-5.48174	.01839	.00083	.00039	.00155
73	.07450	-5.40358	.10734	.00053	.00019	.00166
74	.08015	-5.42608	.00445	.00083	.00039	.00155
75	.03445	-5.46143	.15106	.00042	.00001	.00024
76	.03587	-5.35681	.15106	.00074	.00004	.00025
77	.03424	-5.46348	.15368	.00008	.00002	.00029
78	.03471	-5.48157	.15020	.00033	.00001	.00053
79	.03424	-5.47394	.15043	.00008	.00002	.00029
80	.03471	-5.50008	.14998	.00033	.00001	.00053
81	.17034	-5.46343	.06848	.00033	.00001	.00053
82	.01263	-5.48174	.03163	.00003	.00019	.00166
83	.05168	-5.46348	.15838	.00008	.00002	.00029
84	.00319	-5.48157	.17017	.00033	.00001	.00053



STAIR - TOWER DEFLECTIONS AND ROTATIONS

LOAD CONDITION NO. 3
SOPILE ACW STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. CHERN

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	X	Y	Z	X	Y	Z	REMARKS
1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
4	0.2103	0.00000	0.00000	0.00000	0.00000	0.00000	
5	0.2695	0.0242	0.0551	0.00000	0.00000	0.00000	
6	0.0140	0.0239	0.00000	0.00000	0.00000	0.00000	
7	0.4533	0.0202	0.3497	0.00000	0.00000	0.00000	
8	0.4523	0.0306	0.5067	0.00000	0.00000	0.00000	
9	0.4828	0.0187	0.6942	0.00000	0.00000	0.00000	
10	0.4539	0.0206	0.4015	0.00000	0.00000	0.00000	
11	0.4476	0.0091	0.0403	0.00000	0.00000	0.00000	
12	0.4423	0.0302	0.5110	0.00000	0.00000	0.00000	
13	0.4724	0.0041	0.6874	0.00000	0.00000	0.00000	
14	0.4925	0.0181	0.7000	0.00000	0.00000	0.00000	
15	0.4707	0.0219	0.5909	0.00000	0.00000	0.00000	
16	0.4032	0.0174	0.2749	0.00000	0.00000	0.00000	
17	0.3727	0.0289	0.3305	0.00000	0.00000	0.00000	
18	0.0940	0.0755	0.1124	0.00000	0.00000	0.00000	
19	0.3770	0.0440	0.3475	0.00000	0.00000	0.00000	
20	0.3858	0.0252	0.4611	0.00000	0.00000	0.00000	
21	0.3750	0.0040	0.6452	0.00000	0.00000	0.00000	
22	0.3423	0.0437	0.4130	0.00000	0.00000	0.00000	
23	0.3471	0.0477	0.1400	0.00000	0.00000	0.00000	
24	0.3917	0.0222	0.0597	0.00000	0.00000	0.00000	
25	0.4112	0.0606	0.1615	0.00000	0.00000	0.00000	
26	0.3443	0.0928	0.6689	0.00000	0.00000	0.00000	
27	0.4115	0.1335	0.1520	0.00000	0.00000	0.00000	
28	0.0655	0.0405	0.3581	0.00000	0.00000	0.00000	
29	0.1193	0.0600	0.0434	0.00000	0.00000	0.00000	
30	0.1076	0.0482	0.3523	0.00000	0.00000	0.00000	
31	0.3381	0.0387	0.3492	0.00000	0.00000	0.00000	
32	0.3639	0.0657	0.0726	0.00000	0.00000	0.00000	
33	0.1340	0.0328	0.0624	0.00000	0.00000	0.00000	
34	0.3466	0.0387	0.3787	0.00000	0.00000	0.00000	
35	0.3617	0.0607	0.1004	0.00000	0.00000	0.00000	
36	0.3666	0.0659	0.0460	0.00000	0.00000	0.00000	
37	0.3805	0.0563	0.2470	0.00000	0.00000	0.00000	
38	0.1562	0.0168	0.0817	0.00000	0.00000	0.00000	
39	0.3909	0.0594	0.2437	0.00000	0.00000	0.00000	
40	0.2856	0.0538	0.3760	0.00000	0.00000	0.00000	
41	0.3711	0.0150	0.0736	0.00000	0.00000	0.00000	
42	0.1462	0.0434	0.2201	0.00000	0.00000	0.00000	
43	0.2094	0.0747	0.3399	0.00000	0.00000	0.00000	
44	0.3175	0.0724	0.0244	0.00000	0.00000	0.00000	
45	0.3021	0.0512	0.0604	0.00000	0.00000	0.00000	
46	0.2380	0.0733	0.3506	0.00000	0.00000	0.00000	
47	0.2824	0.0670	0.0260	0.00000	0.00000	0.00000	
48	0.2826	0.0559	0.0584	0.00000	0.00000	0.00000	



STRAIN - JOINT DEFLECTIONS AND ROTATIONS

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DATE 04/27/76

LOAD CONDITION NO. 3

SPLIT ARCH STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. CHERN

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

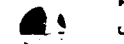
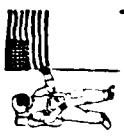
JOINT NUMBER	X	Y	Z	X	Y	Z	REMARKS
49	.02465	.05732	-.03560	.00002	-.00002	-.00003	
50	.02669	.05776	-.03721	.00011	-.00002	-.00002	
51	.02869	.06094	-.04016	.00005	-.00004	-.00002	
52	.02970	.06136	-.04005	.00003	-.00004	-.00003	
53	.03007	.05600	-.05405	.00004	-.00007	-.00006	
54	.02971	.05805	-.04494	.00005	-.00008	-.00002	
55	.02431	.05400	-.04002	.00002	-.00002	-.00003	
56	.02637	.04962	-.04315	.00005	-.00006	-.00001	
57	.03172	.05761	-.05712	.00004	-.00007	-.00004	
58	.01878	.07122	-.03731	.00006	-.00003	-.00004	
59	.01762	.04434	-.04554	.00005	-.00001	-.00002	
60	.02954	.07762	-.05989	.00004	-.00002	-.00003	
61	.01402	.04218	-.03802	.00007	-.00003	-.00004	
62	.01407	.04409	-.04165	.00012	-.00009	-.00004	
63	.01431	.04280	-.04722	.00012	-.00004	-.00004	
64	.01436	.04472	-.04624	.00007	-.00002	-.00003	
65	.01763	.04279	-.05439	.00016	-.00003	-.00004	
66	.02488	.04276	-.04429	.00015	-.00002	-.00009	
67	.02510	.04860	-.06677	.00006	-.00002	-.00002	
68	.02533	.04450	-.05437	.00016	-.00007	-.00001	
69	.01780	.04450	-.05275	.00016	-.00002	-.00005	
70	.02776	.04201	-.04029	.00006	-.00003	-.00002	
71	.00952	.04958	-.03828	.00007	-.00003	-.00004	
72	.00986	.10732	-.04653	.00007	-.00002	-.00003	
73	.00952	.09326	-.03736	.00007	-.00003	-.00004	
74	.00986	.10824	-.04737	.00007	-.00002	-.00003	
75	.02082	.10006	-.06105	.00007	-.00002	-.00002	
76	.02394	.09148	-.06091	.00006	-.00002	-.00002	
77	.02154	.09459	-.05096	.00001	-.00003	-.00002	
78	.02004	.10729	-.06830	.00000	-.00002	-.00009	
79	.02154	.09388	-.05893	.00001	-.00003	-.00002	
80	.02004	.11039	-.06901	.00000	-.00002	-.00009	
81	.00732	.09458	-.03017	.00007	-.00003	-.00004	
82	.00833	.10732	-.04234	.00007	-.00002	-.00003	
83	.02277	.09459	-.05983	.00000	-.00003	-.00002	
84	.02524	.10729	-.06874	.00001	-.00002	-.00009	



LOAD CONDITION NO. 4 / SP-PILE ACW STRUCTURE -- U.S. NAVY (S&IN, STAFFER PILING) -- C.C.MFR.

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	X	Z	Y	X	Y	Z	REMARKS
1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
4	0.00077	0.05173	0.00000	0.00000	0.00000	0.00000	
5	0.00302	0.05799	0.00000	0.00000	0.00000	0.00000	
6	0.00253	0.05707	0.00000	0.00000	0.00000	0.00000	
7	0.01381	0.07825	0.00000	0.00000	0.00000	0.00000	
8	0.02140	0.05913	0.00000	0.00000	0.00000	0.00000	
9	0.02231	0.05780	0.00000	0.00000	0.00000	0.00000	
10	0.01325	0.05192	0.00000	0.00000	0.00000	0.00000	
11	0.01837	0.06261	0.00000	0.00000	0.00000	0.00000	
12	0.02321	0.05952	0.00000	0.00000	0.00000	0.00000	
13	0.02161	0.07112	0.00000	0.00000	0.00000	0.00000	
14	0.02394	0.05856	0.00000	0.00000	0.00000	0.00000	
15	0.02121	0.06785	0.00000	0.00000	0.00000	0.00000	
16	0.01364	0.05054	0.00000	0.00000	0.00000	0.00000	
17	0.01119	0.02810	0.00000	0.00000	0.00000	0.00000	
18	0.01694	0.02568	0.00000	0.00000	0.00000	0.00000	
19	0.02474	0.02081	0.00000	0.00000	0.00000	0.00000	
20	0.01071	0.02897	0.00000	0.00000	0.00000	0.00000	
21	0.03006	0.02756	0.00000	0.00000	0.00000	0.00000	
22	0.02300	0.02300	0.00000	0.00000	0.00000	0.00000	
23	0.01853	0.025581	0.00000	0.00000	0.00000	0.00000	
24	0.01413	0.024084	0.00000	0.00000	0.00000	0.00000	
25	0.02044	0.025708	0.00000	0.00000	0.00000	0.00000	
26	0.00041	0.024930	0.00000	0.00000	0.00000	0.00000	
27	0.02032	0.025470	0.00000	0.00000	0.00000	0.00000	
28	0.01863	0.025905	0.00000	0.00000	0.00000	0.00000	
29	0.01055	0.02527	0.00000	0.00000	0.00000	0.00000	
30	0.02113	0.02096	0.00000	0.00000	0.00000	0.00000	
31	0.01984	0.02008	0.00000	0.00000	0.00000	0.00000	
32	0.01262	0.02552	0.00000	0.00000	0.00000	0.00000	
33	0.01091	0.02129	0.00000	0.00000	0.00000	0.00000	
34	0.01561	0.02026	0.00000	0.00000	0.00000	0.00000	
35	0.01791	0.02042	0.00000	0.00000	0.00000	0.00000	
36	0.01895	0.02569	0.00000	0.00000	0.00000	0.00000	
37	0.01953	0.02162	0.00000	0.00000	0.00000	0.00000	
38	0.00760	0.02747	0.00000	0.00000	0.00000	0.00000	
39	0.02205	0.02217	0.00000	0.00000	0.00000	0.00000	
40	0.02094	0.02699	0.00000	0.00000	0.00000	0.00000	
41	0.01643	0.02415	0.00000	0.00000	0.00000	0.00000	
42	0.01723	0.02084	0.00000	0.00000	0.00000	0.00000	
43	0.02439	0.02463	0.00000	0.00000	0.00000	0.00000	
44	0.01562	0.02576	0.00000	0.00000	0.00000	0.00000	
45	0.02207	0.03269	0.00000	0.00000	0.00000	0.00000	
46	0.03455	0.02040	0.00000	0.00000	0.00000	0.00000	
47	0.00712	0.02560	0.00000	0.00000	0.00000	0.00000	
48	0.04929	0.03327	0.00000	0.00000	0.00000	0.00000	



STRAN - JOINT DEFLECTIONS AND ROTATIONS

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LOAD CONDITION NO. 4

SPILE ACOR STRUCTURE -- U.S. NAVY (36-IN. DIAPETER PILING) -- CACHERN

JOINT NUMBER / X Y Z / ROTATION IN RADIANS / X Y Z / REMARKS

49	.02852	.66019	-.00494	-.00040	.00005	.00020
50	.02176	.64384	.00103	-.00038	-.00001	.00001
51	.01469	.65651	-.01081	-.00042	.00002	.00025
52	.02893	.64769	.02504	.00004	.00027	.00010
53	.05146	.63407	-.04445	-.00090	.00006	.00007
54	.02863	.64007	.02574	.00004	.00024	.00008
55	.03019	.71011	-.01087	-.00104	.00020	.00020
56	.01470	.70475	-.01479	-.00103	.00001	.00025
57	.05482	.68533	-.03191	-.00105	.00004	.00007
58	.02459	1.14777	-.00927	-.00070	.00002	.00016
59	.02419	1.14564	-.01506	-.00069	.00002	.00020
60	.04721	1.13910	-.03524	-.00081	.00005	.00004
61	.02174	1.21286	-.00927	-.00017	.00002	.00017
62	.02101	1.19495	-.01011	-.00011	.00001	.00024
63	.01761	1.20052	-.01272	-.00012	.00002	.00002
64	.01684	1.20844	-.01419	-.00016	.00003	.00019
65	.02176	1.20671	-.02286	-.00010	-.00004	.00003
66	.03667	1.20671	-.04305	-.00012	.00005	.00003
67	.03669	1.20583	-.03604	-.00016	.00007	.00003
68	.03664	1.19664	-.02817	-.00006	.00006	.00014
69	.00224	1.19667	-.01904	-.00007	.00002	.00011
70	.04357	1.18077	-.03557	-.00039	.00005	.00003
71	.01673	1.23466	-.00927	-.00013	.00003	.00016
72	.01574	1.23730	-.01414	-.00017	.00001	.00019
73	.01673	1.24454	-.00410	-.00013	.00003	.00016
74	.01574	1.24399	-.01590	-.00017	.00001	.00019
75	.02059	1.23605	-.03604	-.00014	.00010	.00003
76	.03292	1.21362	-.03604	-.00017	.00008	.00003
77	.02064	1.23464	-.02002	-.00002	.00009	.00006
78	.02057	1.23727	-.05245	-.00012	.00009	.00003
79	.02064	1.24077	-.01674	-.00002	.00009	.00006
80	.02057	1.23840	-.05582	-.00012	.00009	.00003
81	.02660	1.23866	-.00141	-.00013	.00005	.00016
82	.00463	1.23730	-.00375	-.00017	.00001	.00019
83	.01709	1.23864	-.02100	-.00002	.00009	.00006
84	.02245	1.23727	-.05947	-.00012	.00009	.00003



STRAIN - JOINT DEFLECTIONS AND ROTATIONS

LOAD CONDITION NO. 5 30-TON, (30-TON) DIAMETER PILING) - C. CHERN

DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	DEFLECTION IN INCHES	ROTATION IN RADIANS	REMARKS
1	0.00000	0.00000	
2	0.00000	0.00000	
3	0.00000	0.00000	
4	0.00053	0.00000	
5	0.00032	0.00010	
6	0.00004	0.00014	
7	0.0145	0.00275	
8	0.0144	0.0262	
9	0.0153	0.0334	
10	0.0146	0.0280	
11	0.0146	0.0278	
12	0.0146	0.0291	
13	0.0157	0.0396	
14	0.0166	0.0404	
15	0.0157	0.0342	
16	0.0236	0.0485	
17	0.0106	0.0162	
18	0.0021	0.0077	
19	0.0146	0.0274	
20	0.0131	0.0282	
21	0.0087	0.0422	
22	0.0089	0.0247	
23	0.0140	0.0289	
24	0.0132	0.0302	
25	0.0149	0.0349	
26	0.0104	0.0393	
27	0.0149	0.0296	
28	0.0256	0.0174	
29	0.0044	0.0214	
30	0.0117	0.0279	
31	0.0155	0.0292	
32	0.0142	0.0341	
33	0.0167	0.0461	
34	0.0157	0.0304	
35	0.0157	0.0312	
36	0.0145	0.0346	
37	0.0162	0.0354	
38	0.0142	0.0457	
39	0.0180	0.0370	
40	0.0165	0.0367	
41	0.0112	0.0346	
42	0.0102	0.0464	
43	0.0100	0.0350	
44	0.0142	0.0420	
45	0.0014	0.0334	
46	0.0106	0.0307	
47	0.0137	0.0351	
48	0.0010	0.0326	



LOAD CONDITION NO. 5 3-PT LFCR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.C. WERN

JOINT NUMBER	DEFLECTION IN INCHES			ROTATION IN RADIANS			REMARKS
	X	Y	Z	X	Y	Z	
49	.00104	.00453	.00523	.00001	.00001	.00000	
50	.00122	.00394	.00394	.00001	.00000	.00000	
51	.00130	.00419	.00354	.00000	.00001	.00000	
52	.00084	.00377	.00509	.00001	.00000	.00000	
53	.00014	.00344	.00550	.00001	.00000	.00000	
54	.00084	.00417	.00509	.00001	.00001	.00000	
55	.00069	.00482	.00533	.00001	.00001	.00000	
56	.00170	.00426	.00359	.00000	.00001	.00000	
57	.00019	.00294	.00564	.00001	.00000	.00001	
58	.00115	.00564	.00415	.00000	.00000	.00000	
59	.00109	.00403	.00445	.00000	.00000	.00000	
60	.00032	.00479	.00644	.00001	.00000	.00001	
61	.00109	.00694	.00360	.00001	.00001	.00000	
62	.00104	.00683	.00764	.00005	.00007	.00001	
63	.00104	.00514	.00726	.00004	.00004	.00000	
64	.00103	.00492	.00489	.00001	.00000	.00000	
65	.00069	.00514	.01313	.00003	.00015	.00001	
66	.00074	.00513	.00700	.00005	.00000	.00000	
67	.00077	.00600	.00492	.00000	.00000	.00001	
68	.00077	.00683	.00630	.00003	.00000	.00001	
69	.00084	.00683	.01075	.00001	.00010	.00000	
70	.00050	.00547	.00686	.00001	.00000	.00001	
71	.00084	.00843	.00446	.00001	.00000	.00000	
72	.00097	.00613	.00525	.00001	.00000	.00000	
73	.00084	.00651	.00494	.00001	.00000	.00000	
74	.00097	.00608	.00534	.00001	.00000	.00000	
75	.00115	.00692	.00724	.00001	.00000	.00000	
76	.00084	.00612	.00702	.00000	.00000	.00001	
77	.00115	.00843	.00664	.00001	.00000	.00001	
78	.00115	.00613	.00734	.00001	.00000	.00000	
79	.00115	.00840	.00654	.00001	.00000	.00000	
80	.00115	.00599	.00734	.00001	.00000	.00000	
81	.00097	.00843	.00452	.00001	.00000	.00000	
82	.00105	.00613	.00491	.00001	.00000	.00000	
83	.00176	.00843	.00699	.00001	.00000	.00001	
84	.00139	.00613	.00784	.00001	.00000	.00000	

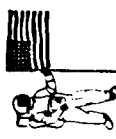


STRAIN - TENSION TESTS AND ROTATIONS

LOAD CONDITION NO. 6 SOLE ACMR STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. CHERN

JOINT NUMBER / DEFECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	X	Y	Z	Y	Z	Y	Z	REMARKS
1	0.00000	0.00000	0.00000	0.0000	0.0000	0.0000	0.0000	
2	0.00000	0.00000	0.00000	0.0000	0.0000	0.0000	0.0000	
3	0.00000	0.00000	0.00000	0.0000	0.0000	0.0000	0.0000	
4	0.00295	0.0024	0.0033	0.0000	0.0000	0.0000	0.0000	
5	0.0167	0.0034	0.0054	0.0001	0.0000	0.0000	0.0000	
6	0.0017	0.0028	0.0077	0.0001	0.0000	0.0000	0.0000	
7	0.0011	0.0049	0.0076	0.0001	0.0000	0.0000	0.0000	
8	0.0098	0.0082	0.0552	0.0002	0.0000	0.0000	0.0000	
9	0.0064	0.0026	0.0162	0.0001	0.0000	0.0000	0.0000	
10	0.00918	0.0050	0.0500	0.0000	0.0000	0.0000	0.0000	
11	0.00918	0.0017	0.0509	0.0000	0.0000	0.0000	0.0000	
12	0.00917	0.0082	0.0599	0.0000	0.0000	0.0000	0.0000	
13	0.0082	0.0049	0.0557	0.0000	0.0000	0.0000	0.0000	
14	0.0036	0.0024	0.02193	0.0000	0.0000	0.0000	0.0000	
15	0.0080	0.0014	0.0146	0.0000	0.0000	0.0000	0.0000	
16	0.0326	0.0061	0.0315	0.0000	0.0000	0.0000	0.0000	
17	0.00541	0.0079	0.0061	0.0000	0.0000	0.0000	0.0000	
18	0.0074	0.0267	0.0041	0.0000	0.0000	0.0000	0.0000	
19	0.0098	0.0077	0.0072	0.0000	0.0000	0.0000	0.0000	
20	0.0015	0.0029	0.0545	0.0000	0.0000	0.0000	0.0000	
21	0.00580	0.0290	0.0291	0.0000	0.0000	0.0000	0.0000	
22	0.00912	0.0076	0.0545	0.0000	0.0000	0.0000	0.0000	
23	0.0066	0.0509	0.0568	0.0000	0.0000	0.0000	0.0000	
24	0.00820	0.0028	0.0656	0.0000	0.0000	0.0000	0.0000	
25	0.00917	0.0054	0.01902	0.0000	0.0000	0.0000	0.0000	
26	0.00675	0.0033	0.0333	0.0000	0.0000	0.0000	0.0000	
27	0.0020	0.0078	0.0598	0.0000	0.0000	0.0000	0.0000	
28	0.01455	0.01651	0.0953	0.0000	0.0000	0.0000	0.0000	
29	0.0182	0.0204	0.1170	0.0000	0.0000	0.0000	0.0000	
30	0.00504	0.03158	0.1512	0.0000	0.0000	0.0000	0.0000	
31	0.00928	0.01674	0.1571	0.0000	0.0000	0.0000	0.0000	
32	0.00858	0.02349	0.1866	0.0000	0.0000	0.0000	0.0000	
33	0.00815	0.03088	0.2508	0.0000	0.0000	0.0000	0.0000	
34	0.00937	0.0175	0.1838	0.0000	0.0000	0.0000	0.0000	
35	0.00934	0.0288	0.1596	0.0000	0.0000	0.0000	0.0000	
36	0.0070	0.0251	0.1442	0.0000	0.0000	0.0000	0.0000	
37	0.00970	0.0204	0.2041	0.0000	0.0000	0.0000	0.0000	
38	0.00670	0.03016	0.2082	0.0000	0.0000	0.0000	0.0000	
39	0.01068	0.02522	0.2005	0.0000	0.0000	0.0000	0.0000	
40	0.00973	0.01997	0.1854	0.0000	0.0000	0.0000	0.0000	
41	0.00683	0.02336	0.1888	0.0000	0.0000	0.0000	0.0000	
42	0.00471	0.02761	0.2539	0.0000	0.0000	0.0000	0.0000	
43	0.00609	0.02665	0.1861	0.0000	0.0000	0.0000	0.0000	
44	0.00835	0.02244	0.1855	0.0000	0.0000	0.0000	0.0000	
45	0.01147	0.01835	0.2043	0.0000	0.0000	0.0000	0.0000	
46	0.00643	0.02461	0.1855	0.0000	0.0000	0.0000	0.0000	
47	0.00812	0.02280	0.1915	0.0000	0.0000	0.0000	0.0000	
48	0.00818	0.01861	0.0858	0.0000	0.0000	0.0000	0.0000	

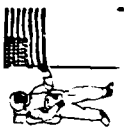


STANLEY DEFLECTIONS AND ROTATIONS

LOAD CONDITION NO. 6 3-PILE ACH STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	DEFLECTION IN INCHES	ROTATION IN RADIANS	REMARKS
49	.00632	.00000	
50	.00728	.00001	
51	.00822	.00003	
52	.00546	.00002	
53	.01148	.00004	
54	.00546	.00002	
55	.00437	.00003	
56	.00491	.00001	
57	.01505	.00004	
58	.00675	.00002	
59	.00628	.00002	
60	.00113	.00001	
61	.00610	.00004	
62	.00605	.00002	
63	.00586	.00004	
64	.00582	.00002	
65	.00412	.00005	
66	.00360	.00003	
67	.00354	.00001	
68	.00351	.00001	
69	.00483	.00008	
70	.00209	.00002	
71	.00441	.00001	
72	.00522	.00002	
73	.00441	.00001	
74	.00522	.00002	
75	.00550	.00004	
76	.00412	.00001	
77	.00549	.00005	
78	.00551	.00001	
79	.00549	.00002	
80	.00551	.00001	
81	.00506	.00001	
82	.00563	.00001	
83	.00877	.00005	
84	.00638	.00001	



STAIN - JOINT DEFLECTIONS AND ROTATIONS

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LOAD CONDITION NO. 7

3-PILE AC-W STRUCTURE - U.S. NAVY (36-IN. DIAPHRAGM PILING) - C. CHERN

JOINT NUMBER /-----DEFLECTION IN INCHES-----/ /-----ROTATION IN RADIANS-----/ /-----MARKS-----/

JOINT NUMBER	DEFLECTION IN INCHES	ROTATION IN RADIANS	MARKS
1	0.0000	0.0000	0.0098
2	0.0000	0.0000	0.0098
3	0.0000	0.0000	0.0044
4	0.2030	0.1415	0.0092
5	0.4612	0.0713	0.0092
6	0.2668	0.0012	0.0044
7	0.7466	0.3872	0.0092
8	0.6096	0.2841	0.0092
9	0.7253	0.9534	0.0044
10	0.7189	0.4020	0.0092
11	0.6791	0.5177	0.0092
12	0.6730	0.4409	0.0092
13	0.7008	0.5102	0.0016
14	0.7123	0.4903	0.0043
15	0.6846	0.4542	0.0067
16	0.6884	0.5106	0.0071
17	0.2900	0.0530	0.0063
18	0.5194	0.1232	0.0056
19	0.5078	0.2263	0.0056
20	0.6958	0.3125	0.0072
21	0.7261	0.4833	0.0064
22	0.5185	0.0560	0.0056
23	0.5398	0.2219	0.0074
24	0.5881	0.4236	0.0014
25	0.5780	0.3951	0.0065
26	0.7022	0.2405	0.0062
27	0.5690	0.6906	0.0063
28	0.2035	0.0490	0.0057
29	0.4011	0.0646	0.0027
30	0.2902	0.1410	0.0035
31	0.4562	0.2809	0.0034
32	0.2151	0.1550	0.0035
33	0.6125	0.2461	0.0036
34	0.4563	0.9668	0.0036
35	0.3582	0.2363	0.0004
36	0.4324	0.1805	0.0037
37	0.4517	0.6455	0.0051
38	0.6225	0.7875	0.0057
39	0.4373	0.2452	0.0026
40	0.3603	0.0407	0.0021
41	0.5708	0.1359	0.0015
42	0.2022	0.7203	0.0068
43	0.2474	0.0508	0.0029
44	0.3212	0.1496	0.0021
45	0.3542	0.1359	0.0051
46	0.2630	0.0326	0.0030
47	0.3113	0.1726	0.0022
48	0.1644	0.3225	0.0052



STRAIN - JOINT DEFLECTIONS AND ROTATIONS

LOAD CONDITION NO. 7 30PILE ACHM STRUCTURE -- U.S. NAVY (36-IN. PLATEPIER PILING) -- C-CMFR

JOINT NUMBER / DEFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	DEFLECTION IN INCHES	ROTATION IN RADIANS	REMARKS
49	25311	0.0025	0.00786
50	28411	0.5515	0.0197
51	31679	0.3655	0.0024
52	26128	0.3769	0.0127
53	15091	0.57314	0.0058
54	25626	0.60212	0.0194
55	22841	0.97584	0.0033
56	30549	0.92052	0.0030
57	11966	0.86462	0.0041
58	16517	0.62544	0.0024
59	15193	0.69347	0.0020
60	05506	0.11297	0.0014
61	10780	0.47688	0.0030
62	11204	0.46479	0.0044
63	13111	0.51578	0.0006
64	13537	0.43790	0.0015
65	23886	0.51622	0.0032
66	02773	0.51637	0.0050
67	02786	0.43377	0.0078
68	02810	0.46341	0.0018
69	08644	0.46314	0.0025
70	04314	0.31181	0.0018
71	06823	0.59909	0.0054
72	07520	0.60550	0.0042
73	06823	0.54640	0.0054
74	07520	0.55574	0.0094
75	03553	0.59109	0.0092
76	02605	0.47283	0.0084
77	03404	0.59910	0.0010
78	03305	0.60543	0.0007
79	03404	0.61204	0.0004
80	03305	0.62251	0.0004
81	15603	0.59009	0.0014
82	00788	0.0788	0.0042
83	05560	0.60559	0.0093
84	00459	0.60910	0.0009
		0.60543	0.0045

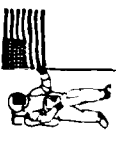


STRAIN EFFECTORS AND ROTATIONS

LOAD CONDITION NO. A 3-PT. LCR STRUCTURE -- (U.S. NAVY (36-IN. DIAMETER PILING)) -- C. CHERN

JOINT / REFLECTION IN INCHES / ROTATION IN RADIANS / REMARKS

JOINT NUMBER	X	Y	Z	X	Y	Z	REMARKS
1	0.00000	0.00000	0.00000	-.00105	-.00105	-.00000	
2	0.00000	0.00000	0.00000	-.00005	-.00005	-.00002	
3	0.00000	0.00000	0.00000	-.00061	-.00061	-.00059	
4	-.07201	-.36560	-.02560	-.00103	-.00103	-.00084	
5	-.00734	-.38901	-.01721	-.00007	-.00007	-.00086	
6	-.03774	-.40087	-.03453	-.00061	-.00061	-.00059	
7	-.09445	-.40315	-.25220	-.00066	-.00066	-.00085	
8	-.76299	-.36065	-.53055	-.00016	-.00016	-.00086	
9	-.09004	-.40063	-.112627	-.00011	-.00011	-.00059	
10	-.06905	-.40657	-.15700	-.00060	-.00060	-.00085	
11	-.02774	-.51150	-.31084	-.00036	-.00036	-.00006	
12	-.78092	-.36391	-.42615	-.00016	-.00016	-.00086	
13	-.05496	-.48720	-.40133	-.00021	-.00021	-.00014	
14	-.07256	-.41264	-.16083	-.00011	-.00011	-.00054	
15	-.04190	-.51304	-.41931	-.00065	-.00065	-.00012	
16	-.07483	-.16382	-.12995	-.00056	-.00056	-.00066	
17	-.10064	-.17671	-.07340	-.00036	-.00036	-.00061	
18	-.21088	-.15622	-.09511	-.00052	-.00052	-.00074	
19	-.06439	-.16052	-.18641	-.00023	-.00023	-.00068	
20	-.09371	-.174597	-.06361	-.00050	-.00050	-.00061	
21	-.07637	-.15710	-.07071	-.00004	-.00004	-.00075	
22	-.04374	-.08748	-.00324	-.00023	-.00023	-.00070	
23	-.07811	-.10443	-.10443	-.00036	-.00036	-.00015	
24	-.71224	-.174303	-.30114	-.00050	-.00050	-.00062	
25	-.70562	-.162142	-.35825	-.00017	-.00017	-.00002	
26	-.05381	-.158381	-.05489	-.00004	-.00004	-.00076	
27	-.09759	-.160791	-.43117	-.00004	-.00004	-.00024	
28	-.03903	-.200489	-.17101	-.00012	-.00012	-.00034	
29	-.28973	-.245903	-.07262	-.00047	-.00047	-.00034	
30	-.41936	-.305653	-.37532	-.00020	-.00020	-.00083	
31	-.04025	-.201060	-.03021	-.00042	-.00042	-.00035	
32	-.51054	-.205094	-.14607	-.00055	-.00055	-.00035	
33	-.02843	-.303345	-.95717	-.00045	-.00045	-.00083	
34	-.03774	-.201180	-.02604	-.00042	-.00042	-.00035	
35	-.02446	-.202745	-.07723	-.00016	-.00016	-.00006	
36	-.02137	-.205210	-.09181	-.00055	-.00055	-.00037	
37	-.04634	-.209879	-.07391	-.00082	-.00082	-.00062	
38	-.00334	-.301022	-.95431	-.00084	-.00084	-.00084	
39	-.02581	-.200050	-.05275	-.00012	-.00012	-.00026	
40	-.04949	-.3014846	-.07196	-.00052	-.00052	-.00018	
41	-.04736	-.315006	-.03753	-.00040	-.00040	-.00015	
42	-.07210	-.298228	-.09064	-.00110	-.00110	-.00094	
43	-.32413	-.304092	-.17417	-.00142	-.00142	-.00127	
44	-.07960	-.307307	-.07210	-.00009	-.00009	-.00022	
45	-.23241	-.309510	-.28709	-.00039	-.00039	-.00074	
46	-.03937	-.304049	-.01914	-.00044	-.00044	-.00024	
47	-.03753	-.307277	-.07931	-.00028	-.00028	-.00023	
48	-.26244	-.307006	-.47402	-.00048	-.00048	-.00077	

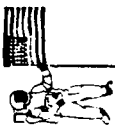


S.I.R.A. - JUNIY DEFLECTIONS AND RADIANS

LOAD CONDITION NO. B 3-PILE ACRB STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - CACHER

JOINT NUMBER /-----X----- DEFECTION IN INCHES-----Z----- /-----X----- ROTATION IN RADIANS-----Z----- /-----X----- REMARKS-----Z-----

49	-.33073	5.84038	-.16188	-.00044	-.00029	
50	-.35586	5.76247	-.08885	-.00026	-.00015	
51	-.38278	3.79229	-.05881	-.00024	-.00024	
52	-.33702	3.76756	-.20179	-.00105	-.00058	
53	-.23936	3.70679	-.32828	-.00068	-.00077	
54	-.33202	5.74414	-.27597	-.00184	-.00024	
55	-.30578	4.12901	-.19247	-.00039	-.00034	
56	-.37911	4.07383	-.08119	-.00027	-.00029	
57	-.20161	3.99547	-.25676	-.00047	-.00074	
58	-.22376	6.29517	-.19199	-.00033	-.00130	
59	-.21294	6.24653	-.09275	-.00026	-.00135	
60	-.13110	6.27309	-.28270	-.00014	-.00036	
61	-.15750	6.27702	-.19555	-.00030	-.00145	
62	-.16175	6.65903	-.20249	-.00039	-.00064	
63	-.18085	6.68740	-.12469	-.00045	-.00111	
64	-.18512	6.61290	-.09164	-.00024	-.00141	
65	-.10227	6.68761	-.28888	-.00097	-.00042	
66	-.10187	6.61973	-.23331	-.00026	-.00118	
67	-.10159	6.65775	-.29110	-.00010	-.00040	
68	-.14527	6.65775	-.30650	-.00019	-.00040	
69	-.11044	6.65778	-.28356	-.00018	-.00008	
70	-.11895	6.48225	-.28015	-.00024	-.00038	
71	-.11568	6.83496	-.19801	-.00024	-.00144	
72	-.11044	6.81132	-.09409	-.00006	-.00139	
73	-.11044	6.78315	-.23660	-.00024	-.00144	
74	-.11568	6.76117	-.07765	-.00046	-.00139	
75	-.10206	6.80710	-.29370	-.00005	-.00039	
76	-.09873	6.65539	-.29194	-.00003	-.00040	
77	-.10103	6.83095	-.29182	-.00003	-.00053	
78	-.10309	6.81110	-.30067	-.00001	-.00049	
79	-.10103	6.85413	-.29082	-.00003	-.00053	
80	-.10309	6.82857	-.30119	-.00002	-.00049	
81	-.19674	6.83496	-.15148	-.00024	-.00124	
82	-.05209	6.81132	-.02852	-.00046	-.00139	
83	-.13298	6.83495	-.29893	-.00003	-.00053	
84	-.07398	6.81110	-.33167	-.00001	-.00049	



STATION - REACTION FORCES AND MOMENTS

PAGE 1
DATE 04/27/76

LOAD CONDITION NO. 1
SOPILE ACMR STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. MEPA

JOINT NUMBER / FORCE IN KIPS / MOMENT IN IN-KIPS / REMARKS

JOINT NUMBER	FORCE IN KIPS	MOMENT IN IN-KIPS	REMARKS
1	91.6651	174.3208	0.0000
2	89.5588	164.8297	0.0000
3	7353	412.0781	0.0000
TOTAL	2.8417	756.2286	0.0000



STRACTION REACTION FORCES AND MOMENTS

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LOAD CONDITION NO. 2
SAMPLE AREA STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.C.F.P.

JOINT NUMBER	FORCE IN KIIPS		MOMENT IN KIIPS		REMARKS
	F-X	F-Y	M-X	M-Y	
1	-91.3341	173.4954	670.1794	0.0000	
2	90.2140	170.1944	669.0216	0.0000	
3	-5.770	412.0387	-1338.5127	0.0000	
TOTAL	-1.6971	755.7285	1.1887	0.0000	

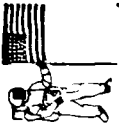


STRAIN REACTION PILES AND MOMENTS

PAGE 3
DATE 04/27/76

LOAD CONDITION NO. 3
3-PILE ARCH STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

JOINT NUMBER	F _{OX}	F _{OY}	F _{OZ}	M _{OX}	M _{OY}	M _{OZ}	REMARKS
1	-16.8822	12.3568	139.7968	0.0000	0.0000	0.0000	
2	16.8817	12.3559	100.4115	0.0000	0.0000	0.0000	
3	.0004	-24.7128	155.6416	0.0000	0.0000	0.0000	
TOTAL	0.0000	0.0000	435.8499	0.0000	0.0000	0.0000	



STRAN - REACTION FORCES AND MOMENTS

LOAD CONDITION NO. 4

3-PILE ACMR STRUCTURE - U.S. NAVY (36-IN. DIAMETER PILING) - C. CHERN

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DATE 04/27/76

JOINT NUMBER	FORCE IN KIPS F _X	F _Y	F _Z	MOMENT IN IN-KIPS M _X	M _Y	M _Z	REMARKS
1	20.2022	-27.1789	-145.9515	0.0000	0.0000	0.0000	
2	-20.2074	-27.1879	-145.9515	0.0000	0.0000	0.0000	
3	0.0052	-75.2532	291.9051	0.0000	0.0000	0.0000	
TOTAL	0.0000	-129.6000	-0.0000	0.0000	0.0000	0.0000	



STRAP REACTION FORCES AND MOMENTS

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DATE 04/27/76

LOAD CONDITION NO. 5 3-PILE ACWR STRUCTURE -- U.S. NAVY (34-IN. DIAMETER PILING) -- C. CHERN

JOINT NUMBER /-----FORCE IN KIPS-----/-----MOMENT IN IN-KIPS-----/-----REMARKS-----/

	F=X	F=Y	F=Z	M=X	M=Y	M=Z
1	-1.4087	.9283	9.8075	0.0000	0.0000	0.0000
2	1.4083	.8276	9.8251	0.0000	0.0000	0.0000
3	.0004	-1.6559	9.8141	0.0000	0.0000	0.0000
TOTAL	-.0000	.0000	29.4447	0.0000	0.0000	0.0000



STRAIN REACTION FORCES AND MOMENTS

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DATE 04/27/76

LOAD CONDITION NO. 6

30PILF ACWP STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHERN

JOINT NUMBER	F=V	F=Z	M=V	M=Z	REMARKS
1	7.6499	53.2513	0.0000	0.0000	
2	7.6485	53.3550	0.0000	0.0000	
3	.0014	53.2917	0.0000	0.0000	
TOTAL	15.2998	159.8980	0.0000	0.0000	



STRAVE - REFACTORS FORCES AND MOMENTS

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DATE 04/27/76

LOAD CONDITION NO. 7

PILE ACWR STRUCTURE -- U.S. NAVY (30FTN. DIAMETER PILING) -- C.C.MERN

JOINT NUMBER / FORCE IN KIIPS / F=Z / MAX / MIN / REMARKS

JOINT NUMBER	FORCE IN KIIPS	F=Z	MAX	MIN	REMARKS
1	213,8594	966,0357	0.0000	0.0000	
2	210,5659	965,2077	0.0000	0.0000	
3	460,9032	1066,7601	0.0000	0.0000	
TOTAL	885,3285	466,4833	0.0000	0.0000	



STRAV - REACTING FORCES AND MOMENTS

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DATE 04/27/76

LOAD CONDITION NO. 8 301LF ACW STRUCTURE -- U.S. NAVY (301N, DIAPHR PILING) -- C.CHERN

JOINT NUMBER /-----FORCE IN KIPS-----/-----MOMENT IN IN-KIPS-----/-----MARKS-----/

	FOR	FOR	MAY	MAY
1	85.9265	0.0000	0.0000	0.0000
2	-83.8277	0.0000	0.0000	0.0000
3	.7428	0.0000	0.0000	0.0000
TOTAL	2.8417	0.0000	0.0000	0.0000

143.8174 614.8088
 -179.3392 608.0144
 -522.6720 1843.6201
 -885.8286 620.7594



STRAN GROUP SUMMARY REPORT

PAGE 1
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30716 ACNR STRUCTURE -- (SOUTH, DIAMETER PILING) -- C. CHERN

MEMBER GROUP	MEMBER NO.	U. CK	CN.	LD.	MEMBER NO.	U. CK	CN.	LD.	MEMBER NO.	U. CK	CN.	LD.	NUMBER OF MEMBERS IN GROUP		
													WITH	WITH	WITH
													UNITY CK	UNITY CK	UNITY CK
													GT.	GT.	LT.
P10	30	1.00	8	18	18	.99	H	11	4	.57	7	6	0	1	0
WRN	33	1.06	8	34	34	1.06	H	21	26	.48	4	24	0	2	22
RR2	25	.80	8	24	25	.65	7	15	10	.49	7	12	0	0	10
JL1	26	1.45	8	36	36	.49	7	22	34	.36	7	6	1	1	5
RRU	15	.24	7	11	13	.22	7	15	15	.19	8	6	0	0	6
RR3	53	1.36	8	54	49	1.24	7	13	26	.90	7	12	1	2	4
P20	30	1.54	8	45	57	1.45	H	18	30	1.19	8	9	2	3	2
RR1	34	1.19	7	26	34	.94	H	34	51	.94	8	6	0	1	2
RR5	60	1.18	8	58	67	1.13	7	59	60	.85	8	15	0	2	7
JL2	42	1.25	8	38	42	1.24	8	53	57	1.22	8	9	0	3	2
RR6	37	.19	H	39	35	.15	H	35	37	.15	8	5	0	0	5
STL	57	.93	8	60	70	.85	H	56	59	.77	7	11	0	0	4
RR8	67	1.01	31	65	67	.99	7	61	62	.96	8	20	1	1	15
RR4	69	.22	H	63	65	.21	H	66	67	.14	7	6	0	0	6
BR7	70	.30	2	70	68	.25	2					2	0	0	2
RR06	71	1.46	8	72	75	.44	7					2	1	1	1

TOTAL MEMBERS 151 6 17 93



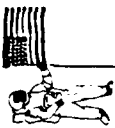
STRAN UNITY CHECK SUMMARY REPORT

PAGE 1
DATE 04/27/76

3-PILE ACMR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. BERN

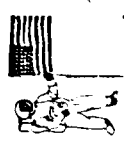
THE FOLLOWING HIGHEST UNITY CHECKS G.T. 1.00
/---FIRST HIGHEST---/---SEC'D HIGHEST---/---THIRD HIGHEST---/

MEMBER NUMBER	MEMBER GROUP ID	UNITY LD. CHECK CN.	UNITY LD. CHECK CN.	UNITY LD. CHECK CN.
67	K18	1.31	1.07	1.38
30	P20	1.50	1.35	1.17
71	K06	1.44	1.44	1.24
45	P20	1.45	1.32	1.14
26	J11	1.45	1.20	1.09
53	B03	1.50	1.27	1.07
42	J12	1.25	1.12	1.08
38	J12	1.24	1.12	1.08
54	H03	1.24	1.17	1.08
53	J12	1.22	1.10	1.05
54	H01	1.19	1.03	1.00
18	P20	1.19	1.08	1.07
60	H05	1.14	1.02	1.07
58	H05	1.13	1.01	1.03
30	K03	1.06	1.01	1.07
33	H01	1.06	1.01	1.07
30	P10	1.00	1.00	1.00



3-DILF ACAR STRUCTURE -- (S. NAVY (360°), DIAPHRAGM PILING) -- C. CHERN

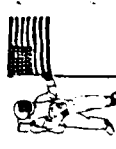
MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITY CK	UNITY CHECK COMPONENT VALUES			LOAD COMP	DIST FROM	FORCE		TORSION		MEMBER ACTION		MOMENT		COMBINED LO	
			AXIAL	V-AXIS	Z-AXIS			FX	FY	IN-KIPS	OUT-KIPS	IN-KIPS	OUT-KIPS	UNITY CK	UNITY CK	UNITY CK	UNITY CK
1	4 P10-01	.565	.242	.041	.202	7	6.1	-.943.59	-.00	5392.70	-9294.67	.466	8	.450	1		
2	5 P10-01	.554	.242	.078	.234	7	6.1	-.942.41	.00	5219.00	9121.31	.455	8	.451	2		
3	6 P10-01	1.001	.467	.534	.000	4	4.1	-1847.41	-.00	17739.53	54.08	.496	7	.799	1		
4	7 W4N-01	.156	.156	.000	.000	7	2.4	168.53	0.00	5.12	59.79	.154	8	.137	1		
4	16 P10-01	.563	.234	.091	.233	7	0.0	-.972.78	106.56	5700.52	-9117.07	.464	8	.448	1		
5	8 W4N-01	.150	.149	.000	.000	7	2.4	161.44	0.00	5.12	-103.39	.146	8	.131	1		
5	17 P10-01	.556	.239	.087	.230	7	0.0	-.972.07	-.60.66	5521.13	4957.22	.453	8	.439	2		
6	9 W4N-01	.270	.269	.000	.001	4	2.4	240.17	0.00	5.11	-223.34	.262	7	.232	1		
6	18 P10-01	.990	.456	.534	.000	8	0.0	-1453.41	219.41	17739.53	94.84	.485	7	.790	1		
7	10 W4N-01	.157	.156	.000	.000	7	2.5	168.38	-.21	11.09	-150.69	.154	8	.137	1		
7	12 W4N-01	.150	.150	.000	.000	7	2.5	161.30	.21	11.09	94.23	.146	8	.131	2		
9	14 W4N-01	.270	.269	.000	.001	4	2.5	290.17	-.00	11.09	-223.34	.262	7	.232	1		
10	11 W4N-01	.235	.174	.009	.046	4	29.0	-.94.63	54.66	65.93	-146.11	.235	7	.219	1		
15	10 W4N-01	.490	.346	.133	.089	4	29.0	-.162.52	.80	382.14	111.70	.453	8	.410	2		
10	22 J11-01	.107	.006	.089	.012	4	32.4	7.56	88.42	1244.45	-454.49	.070	2	.067	1		
11	12 W4N-01	.218	.168	.032	.018	4	29.0	-.88.94	-22.64	114.26	-86.62	.218	7	.211	1		
11	13 W4N-01	.214	.162	.025	.014	7	0.0	10.21	28.10	208.60	66.73	.192	2	.189	8		
15	11 W4N-01	.244	.025	.199	.020	7	29.0	4.55	-24.56	239.74	74.76	.213	2	.209	1		
11	22 W4N-01	.200	.014	.005	.141	4	40.3	7.56	-6.50	57.66	362.02	.147	7	.147	2		
11	24 W4N-01	.142	.019	.005	.154	7	40.3	9.90	-4.95	54.06	317.76	.174	2	.173	8		
12	13 W4N-01	.461	.325	.131	.005	7	0.0	-.171.03	11.16	371.19	69.40	.341	2	.370	8		
12	24 W4N-01	.072	.006	.065	.001	4	32.4	4.14	-131.56	452.30	48.65	.040	3	.032	2		
13	14 W4N-01	.474	.318	.056	.104	4	29.0	-.168.09	11.39	262.53	359.72	.403	7	.401	1		
13	15 W4N-01	.778	.625	.250	.092	4	29.0	17.07	4.62	46.68	131.01	.141	2	.190	7		
13	26 W4N-01	.905	.615	.133	.051	4	0.0	-.258.56	5.25	-203.46	-143.43	.708	1	.685	7		
14	15 W4N-01	.405	.311	.093	.157	7	00.3	-.254.37	-9.62	322.45	-350.04	.436	8	.424	2		
14	26 W4N-01	.249	.008	.238	.003	4	32.4	10.70	107.72	-3134.36	327.19	.230	7	.194	1		
15	22 W4N-01	.806	.635	.169	.003	4	40.3	-.262.57	-13.74	-275.48	33.23	.746	1	.720	7		
15	26 W4N-01	.876	.635	.131	.110	7	00.3	-.262.05	-19.19	-244.41	263.84	.403	8	.399	2		
16	19 W4N-01	.051	.049	.000	.002	4	2.4	52.92	0.00	5.12	-460.25	.047	7	.042	1		
16	24 W4N-01	.493	.350	.107	.107	4	32.4	-.945.43	-359.76	2002.40	-3441.91	.349	4	.377	2		
17	20 W4N-01	.043	.042	.000	.001	4	2.4	45.35	0.00	5.12	216.36	.039	7	.035	2		
17	29 W4N-01	.490	.349	.111	.124	7	32.4	-.944.54	159.49	1047.33	3759.62	.394	4	.373	2		
18	21 W4N-01	.480	.479	.000	.001	4	2.4	517.67	0.00	5.11	166.11	.343	7	.347	2		
18	30 W4N-01	1.184	.677	.510	.001	4	32.6	-.1430.41	174.44	-13512.01	-601.91	.977	7	.872	1		
19	22 W4N-01	.051	.144	.000	.002	4	2.5	-.52.87	-.19	11.09	-519.74	.047	7	.042	1		
20	24 W4N-01	.043	.042	.000	.001	4	2.5	-.45.32	.19	11.09	267.34	.039	7	.035	2		
21	26 W4N-01	.481	.480	.000	.001	4	2.5	-.517.67	-.00	11.09	166.11	.342	7	.346	2		
22	23 W4N-01	.524	.161	.037	.126	7	24.4	-.95.74	73.47	-196.45	362.57	.304	4	.284	2		
27	22 W4N-01	.491	.141	.214	.042	7	24.4	-.45.76	13.56	601.94	265.79	.283	2	.276	1		
22	34 J11-01	.345	.156	.153	.055	7	32.4	-.32.70	-150.95	2337.11	-1400.59	.296	4	.290	1		
22	36 W4N-01	.346	.104	.056	.205	4	0.0	-.65.16	362.34	-860.24	416.74	.332	4	.305	2		
23	24 W4N-01	.342	.160	.033	.149	7	0.0	-.94.92	-74.45	-194.66	416.74	.332	4	.305	2		
23	25 W4N-01	.113	.020	.022	.071	4	24.4	-.6.11	-29.03	52.24	-93.42	.101	1	.100	2		
27	23 W4N-01	.110	.021	.045	.044	7	24.4	-.24.12	-72.56	74.56	71.49	.102	4	.097	1		
24	25 W4N-01	.655	.392	.197	.060	7	0.0	233.05	53.34	574.26	331.75	.651	8	.532	1		
24	36 J11-01	.490	.333	.097	.060	7	32.4	446.61	53.34	1607.52	1263.73	.460	4	.395	1		



3-PILE CAPR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C.CHEMN

UNIT CHCK / CONTROLLING MEMBER ACIDIOUS / -NEXT I.D. HIGH CASES = /

MEMBER NO.	GROUP ID	MAXIMUM CONTAINED UNITY CK	COMPONENT VALUES			LOAD COND NO.	DIST FROM FAIRPT	FORCE FX	TORSION		MOMENT MZ	IN-KIPS		CONTAINED LD	
			AXIAL	Y-AXIS	Z-AXIS				MX	MY		UNITY CK	UNITY CK		
24	38 RR1-01	.902	.690	.012	.200	7	0.0	-599.12	-60.21	-121.63	-499.27	.825	2	.800	8
25	26 RR2-01	.803	.535	.255	.012	8	24.4	-290.67	-84.11	718.88	158.89	.535	1	.523	2
26	27 RR4-01	.170	.137	.021	.112	8	24.4	12.77	4.55	61.30	140.92	.165	7	.164	2
25	27 RR2-01	.411	.104	.506	.002	8	0.0	61.59	59.35	774.86	59.92	.255	2	.255	1
26	34 RR1-01	.979	.789	.054	.136	8	0.0	-493.77	-13.13	266.52	421.49	.814	1	.788	7
26	38 JL1-01	1.409	.573	.859	.016	8	32.4	768.61	167.21	-11338.52	-1566.59	1.204	7	1.087	1
28	31 WBN-01	.355	.054	.000	.001	8	2.4	-58.19	0.00	5.12	-163.84	.054	7	.046	1
28	43 P20-01	.782	.315	.066	.401	7	32.4	-928.57	-549.49	-4352.58	10707.52	.697	8	.628	2
29	32 WBN-01	.053	.052	.000	.001	8	2.4	-55.92	0.00	5.12	372.78	.052	7	.045	2
29	44 P20-01	.788	.315	.112	.361	7	32.4	-927.54	593.48	-5698.93	-10250.58	.717	8	.640	2
30	33 WBN-01	1.061	1.060	.000	.000	8	2.4	-1142.13	0.00	5.11	144.66	.873	7	.780	2
30	45 P20-01	1.536	.745	.790	.001	8	36.1	-1947.21	-366.25	-20215.36	834.58	1.351	7	1.168	1
31	34 WBN-01	.055	.054	.000	.001	8	0.0	58.14	.21	-5.12	-163.84	.054	7	.046	2
32	36 WBN-01	.053	.052	.000	.001	8	0.0	55.87	.21	-5.12	372.78	.052	7	.045	2
33	38 WBN-01	1.058	1.058	.000	.001	8	2.5	1142.13	.00	11.09	144.66	.875	7	.782	2
34	35 RR5-01	.265	.081	.100	.084	8	0.0	-30.34	22.61	166.03	-151.65	.186	7	.133	1
39	34 RR5-01	.791	.597	.188	.007	8	19.8	248.04	-3.82	233.87	44.19	.593	7	.511	2
34	40 JL2-01	.462	.295	.030	.137	7	18.2	801.70	-687.97	-1871.85	4013.28	.412	8	.335	2
34	53 RR1-01	1.189	.677	.402	.110	7	47.4	-449.40	-150.14	-1479.22	773.07	1.032	8	1.001	2
35	36 RR5-01	.167	.019	.101	.047	7	19.8	8.05	-8.35	150.00	102.13	.145	8	.105	3
35	37 RR6-01	.146	.088	.007	.051	8	0.0	-25.08	13.87	19.19	-51.68	.120	1	.117	7
39	35 RR6-01	.149	.061	.011	.076	8	19.8	19.32	-7.64	29.35	-77.02	.117	7	.113	2
36	37 RR5-01	.530	.158	.170	.062	8	0.0	65.73	-4.68	209.32	-23.86	.280	7	.287	2
36	41 JL2-01	.343	.196	.024	.124	7	14.2	531.20	834.06	-1578.49	-3581.65	.313	8	.286	2
36	49 RR1-01	.7465	.073	.001	.391	7	47.4	-48.74	194.18	69.05	-1509.51	.449	8	.424	2
37	38 RR5-01	.309	.107	.188	.044	7	36.2	-36.10	-26.49	239.02	-64.24	.182	8	.152	2
37	39 RR6-01	.146	.116	.032	.068	8	19.8	36.61	-5.60	-12.24	65.14	.174	7	.170	2
38	39 RR5-01	.782	.527	.231	.023	7	0.0	-177.48	2.55	273.62	-86.95	.668	8	.603	2
38	42 JL2-01	1.216	.490	.755	.000	8	15.0	1330.99	157.12	-2009.54	106.64	1.120	7	.978	2
38	51 RR1-01	.938	.540	.510	.088	8	55.7	-334.83	81.92	-1114.85	-594.30	.911	7	.875	1
40	49 JL2-01	.855	.299	.160	.389	7	18.3	811.22	-664.76	-8058.85	12324.74	.855	8	.675	2
41	51 JL2-01	.786	.199	.149	.438	7	18.3	540.79	832.78	-7823.83	-13431.62	.773	8	.623	2
42	53 JL2-01	1.289	.494	.755	.000	8	0.0	1340.80	314.71	-2008.54	130.45	1.324	7	.981	2
43	46 WBN-01	.024	.023	.000	.001	8	2.4	24.71	0.00	5.12	-297.55	.021	1	.021	7
43	55 P20-01	.779	.315	.083	.381	7	0.0	-929.41	-1184.27	-4847.30	10404.46	.694	8	.626	2
44	47 WBN-01	.022	.021	.000	.001	8	2.4	23.19	0.00	5.12	222.62	.017	2	.016	1
44	56 P20-01	.785	.315	.132	.339	7	0.0	-927.43	1115.42	-6170.45	-9882.03	.716	8	.639	2
45	48 WBN-01	.266	.266	.000	.001	8	2.4	246.41	0.00	5.11	194.05	.205	7	.194	1
45	57 P20-01	1.452	.634	.816	.002	8	0.0	-1869.13	-298.19	-20215.36	668.96	1.320	7	1.137	2
46	49 WBN-01	.024	.023	.000	.001	8	2.5	-24.69	.21	11.09	-328.22	.021	1	.021	7
47	51 WBN-01	.023	.022	.000	.001	8	2.5	-23.17	.21	11.09	251.54	.017	2	.016	1
48	53 WBN-01	.267	.266	.000	.001	8	2.5	-286.41	.20	11.04	194.05	.205	7	.194	1
49	50 RR3-01	.450	.229	.041	.180	7	15.1	-120.42	255.51	-187.62	593.81	.394	8	.369	2
49	55 RR3-01	1.238	.552	.646	.041	7	15.2	240.25	117.23	-1315.50	330.70	1.170	8	.746	2
50	51 RR3-01	.452	.201	.054	.452	7	0.0	773.62	-978.45	-9642.70	14399.50	.906	8	.354	2
50	52 RR5-01	.223	.035	.177	.010	7	0.0	-126.93	-239.78	-200.71	314.65	.378	8	.354	2
54	50 RR5-01	.177	.005	.170	.002	7	15.1	14.71	116.92	223.25	52.23	.210	8	.184	1
								1.41	-124.10	209.50	-22.92	.160	8	.145	2



STRUCTURE STRESS REPORT

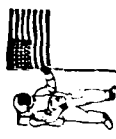
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3-PILE ACMR STRUCTURE -- U.S. NAVY (36-17), DIAPHRAGM PILING) -- C. CHERN

CONTROLLING MEMBER ACTIONS / MOMENT IN-KIPS / MOMENT IN-KIPS / COMBINED LD COMBINED LD

MEMBER NO.	GROUP TO	MAXIMUM COMBINED UNITY CK	UNITY CHECK COMPONENT VALUES		LOAD COMB NO.	DIST FROM PILE (FT)	FORCE FX KIPS	TORSION MX IN-KIPS	MOMENT MY IN-KIPS	MOMENT MZ IN-KIPS	COMBINED LD			
			AXIAL	Z-AXIS							UNITY CK	LD		
51	52 HR3-01	.798	.109	.683	7	0.0	-54.54	-116.59	1355.27	130.14	.614	2	.606	1
51	56 JL2-01	.984	.280	.194	7	0.0	760.43	1052.73	-9798.55	-15941.85	.933	A	.777	2
52	53 HR3-01	.876	.030	.687	M	15.1	-14.88	-114.71	1508.75	725.02	.839	7	.707	2
52	54 HR5-01	.245	.037	.095	M	0.0	15.38	-9.07	180.45	213.64	.256	7	.236	2
53	54 HR3-01	1.364	.607	.679	M	0.0	-319.14	151.47	1418.66	-479.83	1.270	7	1.089	2
53	57 JL2-01	1.215	.566	.634	M	4.6	1537.23	26.43	-16995.69	-2615.06	1.104	7	.949	2
55	58 STL-01	.727	.048	.676	7	28.5	-151.18	1360.46	-16768.54	-1159.97	.663	M	.507	2
56	59 STL-01	.775	.052	.712	7	28.5	-141.48	-1484.24	-17757.37	2259.05	.708	A	.605	2
57	60 STL-01	.930	.107	.822	M	28.5	-294.02	-528.01	20351.02	476.01	.882	7	.698	2
58	59 HR5-01	.508	.051	.004	M	29.0	21.23	-20	52.63	557.83	.491	A	.490	2
60	58 HR5-01	.834	.304	.421	M	0.0	-103.82	-3.48	601.22	306.12	.769	7	.633	1
58	61 STL-01	.674	.029	.643	M	0.0	-81.67	-399.25	15940.62	873.89	.667	7	.526	2
58	67 HR5-01	1.135	.665	.275	7	32.6	-217.02	16.05	-553.25	296.34	1.005	2	.927	8
59	60 HR5-01	.854	.248	.571	M	29.0	105.14	-3.55	541.27	462.23	.820	7	.760	2
59	61 HR5-01	.840	.012	.004	M	0.0	-4.05	-27.92	61.07	-766.97	.634	2	.626	8
59	64 STL-01	.761	.047	.706	M	0.0	-134.07	-149.43	-17569.49	1845.98	.704	A	.600	2
60	64 HR5-01	1.177	.653	.002	M	0.0	-213.10	-18.35	28.98	-519.79	1.017	1	.967	7
60	70 STL-01	.850	.066	.784	M	0.0	-140.98	98.20	19413.15	667.75	.820	7	.646	2
61	62 HR-01	.959	.106	.250	M	0.0	36.97	-0.00	530.08	139.70	.748	7	.645	1
69	61 HR-01	.739	.375	.082	M	8.7	-102.00	-0.00	202.79	-62.38	.683	7	.626	1
61	71 STL-01	.093	.020	.070	M	0.0	-57.53	32.84	1763.14	-371.27	.079	7	.061	2
62	65 HR-01	.556	.358	.003	M	20.0	-37.33	-0.00	6.21	-34.04	.447	2	.295	8
69	62 HR-01	.216	.030	.000	M	7.5	-3.74	-0.00	22.48	209.1	.205	1	.205	8
63	64 HR-01	.352	.106	.206	M	4.5	37.10	-0.08	435.41	-9.29	.225	7	.177	2
63	65 HR-01	.206	.005	.656	M	7.5	.82	-0.00	27.83	-17.47	.184	2	.183	7
64	65 HR-01	.395	.229	.121	M	0.0	-62.29	0.00	300.07	-10.75	.391	A	.329	2
64	72 STL-01	.084	.006	.002	M	0.0	-17.83	35.59	268.86	-1906.69	.077	8	.062	2
65	66 HR-01	.141	.002	.018	M	121	-15	-0.01	8.80	14.60	.133	A	.124	2
65	67 HR-01	.945	.818	.012	M	0.0	-62.81	-0.00	30.15	-36.83	.797	2	.602	8
66	67 HR-01	.145	.001	.021	M	122	.22	.01	10.16	-14.42	.133	2	.105	1
70	66 HR7-01	.298	.001	.000	M	0.0	.09	7.27	-1.96	54.26	.286	7	.140	8
67	68 HR-01	.073	.003	.002	M	10.0	40	-0.01	-1.13	81.30	.056	2	.072	1
67	69 HR-01	.312	.037	.275	M	0.0	-105.40	108.52	648.09	10.74	1.070	1	.377	7
70	69 HR-01	.559	.065	.485	M	0.0	-186.93	-64.64	12287.38	34.32	.526	7	.426	2
67	76 STL-01	.004	.021	.037	M	0.0	-62.38	-64.64	-1447.21	-1070.51	.066	7	.054	2
68	69 HR-01	.072	.001	.023	M	0.0	-0.03	-5.51	11.96	-5.65	.049	7	.044	1
70	68 HR7-01	.255	.000	.000	M	2	.00	-9.42	84.35	-46.72	.247	7	.085	8
71	72 HR-01	.266	.190	.034	M	29.0	-9.42	-0.00	2.97	-4.12	.211	2	.093	8
71	73 HR-01	.001	.000	.001	M	0.0	-0.00	-0.00	2.97	-0.00	.001	A	.001	3
71	75 HR-01	1.463	.902	.057	M	0.0	-10.76	-0.01	168.55	-17.25	.156	1	.235	7
71	77 HR-01	.153	.000	.079	M	0.0	-0.01	-0.01	168.55	-17.25	.156	1	.134	2
71	81 HR-01	.004	.000	.004	M	0.0	-0.00	-0.00	8.25	.00	.004	7	.004	3
72	74 HR-01	.001	.000	.001	M	0.0	-0.00	-0.00	2.97	.00	.001	7	.001	3
72	75 HR-01	.441	.264	.086	M	0.0	-5.15	.00	21.45	5.46	.240	2	.152	8
72	78 HR-01	.169	.001	.078	M	0.0	-0.25	.02	164.35	21.00	.152	2	.148	1
72	82 HR-01	.004	.000	.004	M	0.0	-0.00	-0.00	8.25	.00	.004	7	.004	3
76	75 STL-01	.071	.019	.034	M	0.0	-55.55	-18.71	-1039.55	-765.36	.048	7	.039	2
77	75 HR-01	.074	.008	.014	M	14.5	2.79	.04	38.11	11.22	.052	2	.052	7

Error in Synercom Program

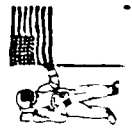


STRUT MEMBER STRESS REPORT

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PILE ACHR STRUCTURE -- U.S. NAVY (36-1), BIAFTER PILING) -- C.CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITY CK	UNITY CHECK COMPONENT VALUES			LOAD COND	DIST FROM END(FT)	FORCE		TORSION		MEMBER ACTIONS		MOMENT		COMBINED LD			
			AVIAL	Y-AXIS	Z-AXIS			FX	FY	MX	MY	IN-KIPS	IN-KIPS	LD	CK	UNITY	CK	UNITY	CK
75	78 W1R-01	.038	.000	.029	H	14.5	2.79					.42			-6.82	.037	7	.032	2
76	77 RR6-01	.047	.005	.051	H	14.2	-3.18			23.36		11.98			-31.43	.033	7	.027	3
76	78 RR6-01	.076	.013	.052	H	0.0	-3.72			-27.35		25.79			-54.54	.051	7	.049	2
77	79 W1R-01	.001	.001	.000	H	0.0	.00			.00		2.97			.00	.001	7	.001	3
77	83 W1R-01	.004	.004	.000	H	0.0	.00			.00		8.25			.00	.004	7	.004	3
78	80 W1R-01	.001	.001	.000	H	0.0	.00			.00		2.97			.00	.001	7	.001	3
78	84 W1R-01	.004	.004	.000	H	0.0	.00			.00		8.25			.00	.004	7	.004	3



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3071F ACMR STRUCTURE -- U.S. NAVY (66-IN. DIAMETER PILING) -- C. CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED LOAD UNITS CK (COND ENDFEET)	DIST FROM	FORCE FX	TORSION TX	MOMENT MY	IN-KIPS	Z-AXIS SHEAR UNITS CK	LD V-Axis CN	LD KLY/RY CN	LD V-Axis SHEAR UNITS CK	LD KLY/RY HIGH UNITS CK	NEXT HIGH UNITS CK
1	4 P10-01	.565	7 6.1	-985.59	-1.00	5592.70	.055	7	.055	7	6.0	6.0	.466
2	5 P10-01	.558	7 6.1	-982.41	.00	5210.00	.053	7	.053	7	6.0	6.0	.455
3	6 P10-01	1.001	8 6.1	-1497.41	-2.00	17739.53	.090	A	.090	A	6.0	6.0	.696
4	7 HRN-01	.156	7 2.4	184.53	.00	5.12	.000	A	.000	A	1.2	1.2	.154
5	8 HRN-01	.150	7 2.4	-972.78	100.56	5700.62	.018	7	.015	7	32.1	32.1	.464
6	9 HRN-01	.556	7 0.0	181.44	.00	5.12	.000	A	.000	A	1.2	1.2	.146
7	10 HRN-01	.270	8 2.4	-972.07	-0.00	5521.13	.014	7	.013	7	32.1	32.1	.453
8	11 HRN-01	.990	8 0.0	29.17	.00	5.11	.000	A	0.000	A	1.2	1.2	.262
9	12 HRN-01	.157	7 2.5	-1853.41	219.41	17759.53	.037	A	.032	A	32.1	32.1	.685
10	13 HRN-01	.150	7 2.5	-184.38	-.21	11.09	.001	A	.010	7	1.2	1.2	.154
11	14 HRN-01	.270	8 2.5	-281.17	.21	11.09	.001	A	.000	7	1.2	1.2	.146
12	15 HRN-01	.235	A 29.0	-94.63	50.66	11.09	.001	7	.000	A	1.2	1.2	.262
13	16 HRN-01	.490	7 29.0	-182.52	.80	382.14	.022	A	.025	2	39.7	39.7	.235
14	17 HRN-01	.107	A 32.4	7.56	88.42	1244.45	.023	A	.015	8	39.7	39.7	.433
15	18 HRN-01	.218	A 29.0	-84.94	-22.60	114.26	.025	2	.017	A	27.9	27.9	.070
16	19 HRN-01	.218	7 0.0	10.21	26.10	206.60	.025	2	.027	2	39.7	39.7	.218
17	20 HRN-01	.240	7 29.0	4.55	-24.36	259.78	.041	7	.025	7	52.1	52.1	.192
18	21 HRN-01	.200	A 40.3	7.56	-0.50	57.66	.020	7	.017	7	64.6	64.6	.213
19	22 HRN-01	.182	7 40.3	9.90	-4.95	317.36	.017	7	.015	7	64.6	64.6	.187
20	23 HRN-01	.461	7 0.0	-171.43	11.15	371.19	.013	7	.010	A	39.7	39.7	.381
21	24 HRN-01	.072	A 32.4	4.14	-131.56	852.30	.026	7	.018	A	27.9	27.9	.040
22	25 HRN-01	.078	8 29.0	-164.09	11.39	262.53	.025	7	.015	7	39.7	39.7	.003
23	26 HRN-01	.193	A 29.0	17.47	4.62	96.68	.018	A	.015	A	52.1	52.1	.191
24	27 HRN-01	.278	A 0.0	-284.56	5.25	-203.46	.015	2	.013	2	64.6	64.6	.208
25	28 HRN-01	.905	7 40.3	-254.57	-9.62	-322.45	.020	1	.018	A	64.6	64.6	.836
26	29 HRN-01	.405	8 0.0	-164.09	-44.25	260.17	.041	7	.023	7	39.7	39.7	.342
27	30 HRN-01	.249	A 32.4	10.70	107.72	-3134.36	.029	A	.023	A	27.9	27.9	.250
28	31 HRN-01	.806	8 40.3	-282.57	-13.74	-275.48	.022	2	.017	7	64.6	64.6	.746
29	32 HRN-01	.876	7 40.3	-262.45	-19.19	-288.41	.039	A	.027	A	64.6	64.6	.803
30	33 HRN-01	.051	A 2.4	52.91	0.00	5.12	.000	A	.021	A	1.2	1.2	.047
31	34 HRN-01	.093	7 32.4	-945.83	-350.76	2002.60	.032	A	.021	A	31.7	31.7	.399
32	35 HRN-01	.043	A 2.4	45.35	0.00	5.12	.000	A	.000	A	1.2	1.2	.039
33	36 HRN-01	.480	7 32.4	-984.54	159.49	1087.33	.018	A	.013	A	31.7	31.7	.394
34	37 HRN-01	.480	A 2.4	517.67	0.00	5.11	.000	A	0.000	A	1.2	1.2	.047
35	38 HRN-01	1.188	8 32.4	-1830.41	176.48	-13512.01	.042	A	.037	A	31.8	31.8	.977
36	39 HRN-01	.051	A 2.5	-52.87	-.19	11.09	.001	A	.003	A	1.2	1.2	.047
37	40 HRN-01	.043	A 2.5	-45.32	.19	11.09	.001	A	.002	A	1.2	1.2	.039
38	41 HRN-01	.481	7 24.0	-917.97	.00	11.09	.001	7	.000	2	1.2	1.2	.582
39	42 HRN-01	.324	7 24.0	-95.72	73.47	-196.05	.056	7	.035	7	32.5	32.5	.308
40	43 HRN-01	.401	7 24.0	-83.76	13.56	603.94	.033	A	.020	A	32.5	32.5	.283
41	44 HRN-01	.365	7 32.4	200.14	-15.95	2337.11	.040	7	.027	7	27.9	27.9	.206
42	45 HRN-01	.346	A 0.0	-95.16	-32.70	362.54	.029	A	.023	A	69.7	69.7	.302
43	46 HRN-01	.342	7 0.0	-94.92	-74.85	-190.66	.059	7	.036	7	32.5	32.5	.332
44	47 HRN-01	.113	A 24.0	-6.11	52.28	52.28	.045	A	.026	A	42.9	42.9	.101
45	48 HRN-01	.110	7 24.0	-24.12	-24.12	72.56	.041	A	.026	A	42.9	42.9	.102
46	49 HRN-01	.655	7 0.0	233.05	.50	574.26	.026	A	.014	A	52.5	52.5	.651
47	50 HRN-01	.400	7 32.4	446.61	53.58	1607.52	.025	7	.022	7	27.9	27.9	.460



S T R A N G E T H E R S T R E S S R E P O R T P. O. 2

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3-PILE ACMR STRUCTURE -- U.S. NAVY (36-1) DIAPHRAGM PILING -- C. CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITS CK	DIST FROM	FORCE FX	TORSION TX	MEMBER ACTIONS		Z-AXIS		LD Y-AXIS		NEXT HIGH UNLCK.			
						MOMENT MY	IN-KIPS	SHEAR	UNITY CK	LD CN	SHEAR	UNITY CK	LD KLYRY	KLZARZ	LD CN
24	38 RR1-01	.902	7 0.0	-399.12	-80.21	-121.63	-99.27	.051	A	.034	A	81.3	81.3	.625	2
25	26 RR2-01	.803	A 24.4	-280.67	-84.11	718.88	154.89	.061	A	.036	A	32.5	32.5	.535	1
25	27 RR4-01	.170	A 24.4	12.77	4.55	61.30	140.92	.017	A	.014	A	42.9	42.9	.165	7
26	27 RR2-01	.411	A 0.0	61.55	59.35	774.86	50.92	.046	A	.029	A	32.5	32.5	.255	2
26	34 RR1-01	.079	A 0.0	-893.77	-13.13	266.52	421.49	.018	A	.017	A	69.7	69.7	.814	1
26	38 JL1-01	1.049	A 32.6	768.61	167.21	-11338.52	-1560.59	.080	A	.070	A	28.0	28.0	1.204	7
28	31 RRN-01	.055	A 2.4	-58.19	0.00	5.12	-163.84	.000	A	.000	A	1.2	1.2	.054	7
28	32 RRN-01	.782	7 32.4	-924.57	-509.49	-4552.58	10707.52	.054	A	.037	A	31.7	31.7	.697	7
29	44 P20-01	.053	A 2.4	-55.92	0.00	5.12	572.78	.000	A	.000	A	1.2	1.2	.052	7
29	44 P20-01	.786	7 32.4	-927.54	593.08	-5694.93	-10230.58	.057	A	.039	A	31.7	31.7	.717	8
30	33 RRN-01	1.061	A 2.4	-1142.13	0.00	5.11	144.66	.000	A	0.000	A	1.2	1.2	.873	7
30	45 P20-01	1.536	A 36.1	-1987.21	-366.25	-20215.36	434.58	.064	A	.052	A	35.3	35.3	1.351	7
31	34 RRN-01	.055	A 0.0	58.14	-.21	-5.12	-163.84	.001	A	.003	A	1.2	1.2	.054	7
32	36 RRN-01	.053	A 0.0	55.87	.21	-5.12	372.78	.001	A	.003	A	1.2	1.2	.075	7
33	38 RRN-01	1.058	A 2.5	1142.13	-.00	11.09	144.66	.001	A	.009	A	36.2	36.2	1.86	7
34	35 RR5-01	.265	A 0.0	-36.34	22.01	166.43	-151.85	.040	A	.026	A	36.2	36.2	.593	7
39	34 RR5-01	.791	A 19.8	248.04	-3.82	253.87	44.19	.013	A	.010	A	36.2	36.2	.412	8
34	40 JL2-01	.462	7 14.2	401.70	-687.97	-1871.45	4013.28	.062	A	.043	A	12.0	12.0	1.032	8
34	53 RR1-01	1.189	7 47.4	-409.00	-150.14	-1479.22	773.07	.066	A	.056	A	59.7	59.7	1.145	8
35	36 RR5-01	.167	7 19.8	4.05	18.35	150.00	102.14	.048	A	.029	A	36.2	36.2	.145	8
35	37 RR6-01	.146	A 0.0	-25.08	13.87	19.19	-51.68	.029	A	.018	A	35.8	35.8	1.20	1
39	35 RR4-01	.149	A 19.8	19.32	-7.84	29.35	-27.42	.020	A	.013	A	35.8	35.8	.117	7
36	37 RR5-01	.330	A 0.0	65.73	-4.68	209.32	-23.86	.016	A	.012	A	36.2	36.2	.280	7
36	41 JL2-01	.343	7 14.2	531.20	834.06	-1574.69	-3581.65	.070	A	.052	A	59.7	59.7	.513	8
36	49 RR1-01	.465	7 47.4	-48.74	194.14	64.05	-1509.51	.100	A	.062	A	59.7	59.7	.409	8
37	38 RR5-01	1.509	7 30.2	-36.19	-26.49	239.62	-64.24	.039	A	.023	A	59.3	59.3	.182	8
37	39 RR6-01	.186	A 19.8	36.61	-5.60	-12.24	65.14	.020	A	.016	A	35.8	35.8	1.174	7
38	39 RR5-01	.782	7 0.0	-177.48	2.55	273.62	-66.95	.011	A	.009	A	59.3	59.3	.668	8
38	42 JL2-01	1.268	A 15.0	1330.99	157.12	-20009.54	106.64	.106	A	.103	A	12.7	12.7	1.120	7
38	51 RR1-01	.938	A 55.7	-334.63	41.92	-1114.45	-594.30	.056	A	.039	A	71.3	71.3	.911	7
40	49 JL2-01	.855	7 18.5	411.22	-684.76	-8050.85	12824.74	.078	A	.059	A	15.5	15.5	.835	8
41	51 JL2-01	.746	7 18.5	541.79	432.74	-7823.83	-13431.62	.091	A	.066	A	15.5	15.5	.773	8
42	53 JL2-01	1.249	A 0.0	1340.00	114.71	-20009.54	130.45	.048	A	.045	A	18.0	18.0	1.124	7
43	46 RRN-01	.024	A 2.4	24.71	0.00	5.12	-297.35	.000	A	.000	A	1.2	1.2	.021	1
43	55 P20-01	.779	7 0.0	-929.41	-1184.27	-4847.30	10404.46	.093	A	.057	A	4.5	4.5	.694	2
44	47 RRN-01	.022	A 2.4	23.19	0.00	5.12	222.62	.000	A	.000	A	1.2	1.2	.017	2
44	56 P20-01	.745	7 0.0	-927.43	1115.42	-6170.45	-6782.03	.094	A	.060	A	4.5	4.5	.716	8
45	48 RRN-01	.266	A 2.4	286.81	6.00	5.11	104.45	.000	A	0.000	A	1.2	1.2	.205	7
45	57 P20-01	1.452	A 0.0	-1869.13	-296.19	-20215.36	868.96	.134	A	.125	A	4.5	4.5	1.320	7
46	49 RRN-01	.024	A 2.5	-24.69	-.21	11.09	-528.22	.001	A	.001	A	1.2	1.2	.021	1
47	51 RR1-01	.023	A 2.5	-23.17	-.00	11.09	251.58	.001	A	.001	A	1.2	1.2	.021	2
48	53 RRN-01	.267	A 2.5	-266.81	-.00	11.09	194.95	.001	A	.000	A	1.2	1.2	.205	7
49	50 RR3-01	.450	7 15.1	-121.42	255.51	-147.42	593.81	.215	A	.118	A	20.5	20.5	.394	8
49	49 RR3-01	1.238	7 15.2	291.25	117.25	1315.50	530.70	.116	A	.071	A	20.5	20.5	1.170	8
49	55 JL2-01	.939	7 0.0	773.63	-978.45	-9642.70	14399.50	.141	A	.113	A	3.9	3.9	.906	8
50	51 RR3-01	.432	7 0.0	-126.93	-230.78	-204.71	318.65	.109	A	.079	A	20.5	20.5	.378	8
50	52 RR5-01	.223	7 0.0	14.71	116.92	223.25	52.23	.151	A	.079	A	26.0	26.0	.210	8
50	50 RR5-01	.177	7 15.1	1.91	-124.10	209.50	-22.92	.160	A	.084	A	26.0	26.0	.160	8

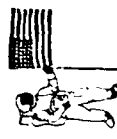


PILE ACMR STRUCTURE -- U.S. NAVY (36-IN. DIA AFTER PILING) -- C. GERNI

MEMBER NO.	GROUP ID	MAXIMUM COMBINED LOAD FROM UNITY CK (KIP) END (FT)	DIST FROM END (FT)	FORCE FX	TORSION NY	MOMENT MY	SPHER ACTIONS	MOMENT MZ	IN-KIPS	2-AXIS SHEAR CN	LD CN	V-AXIS SHEAR CN	LD CN	KL/VARY	ML/Z/R7	HIGH	LD	NEXT HIGH INJ. CK.
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51	52	AR3-01	7	0.0	-50.54	-116.59	1355.27	130.14	.114	A	.069	A	.069	20.5	20.5	.614	2	.614
51	56	JL2-01	7	0.0	760.43	1052.64	-9798.55	-15901.65	.108	A	.118	A	.118	3.9	3.9	.933	A	.933
52	53	AR3-01	A	15.1	-14.86	-114.71	1506.75	725.02	.122	A	.078	A	.078	20.5	20.5	.839	7	.839
52	54	AR5-01	A	0.0	15.38	-9.07	180.45	213.64	.026	B	.020	B	.020	26.0	26.0	.256	7	.256
53	54	AR3-01	A	0.0	-319.14	151.47	-1416.66	-479.63	.145	A	.088	A	.088	20.5	20.5	1.270	7	1.270
53	57	JL2-01	A	4.6	1537.23	26.41	-14995.60	-2015.06	.101	A	.100	A	.100	3.9	3.9	1.104	7	1.104
55	58	STL-01	7	28.5	-131.18	1361.48	-16761.54	-1159.97	.142	7	.101	7	.101	27.8	27.8	.663	A	.663
56	59	STL-01	7	28.5	-141.48	-1088.24	-17757.57	2259.05	.154	7	.109	7	.109	27.8	27.8	.708	A	.708
57	60	STL-01	A	28.5	-294.02	-528.01	20351.02	476.61	.096	A	.080	A	.080	27.8	27.8	.882	A	.882
58	59	AR5-01	7	29.0	21.23	-.20	52.63	557.83	.039	A	.027	A	.027	56.6	56.6	.491	A	.491
60	58	AR5-01	A	0.0	-103.82	-3.48	601.22	306.12	.029	A	.027	A	.027	56.6	56.6	.491	7	.491
58	61	STL-01	A	0.0	-81.67	-399.25	15940.62	873.89	.071	A	.059	A	.059	14.6	14.6	.667	7	.667
59	60	AR5-01	7	32.6	-103.14	10.05	-353.25	296.54	.045	A	.036	A	.036	68.7	68.7	1.005	2	1.005
59	61	AR5-01	7	0.0	-4.05	-27.92	61.07	-766.97	.082	7	.065	7	.065	68.7	68.7	.634	2	.634
59	64	STL-01	7	0.0	-134.07	-149.43	-17569.49	1845.98	.066	A	.059	A	.059	14.6	14.6	.704	A	.704
60	64	AR5-01	A	0.0	-213.10	-18.55	28.98	-519.79	.050	A	.031	A	.031	68.7	68.7	1.017	1	1.017
60	70	STL-01	A	0.0	-190.98	98.20	19413.15	667.75	.065	7	.060	7	.060	5.9	5.9	.820	7	.820
61	62	W1H-01	A	0.0	36.97	-.00	530.08	139.70	.106	A	.028	A	.028	7.7	34.3	.748	7	.748
69	61	W1R-01	A	R7	-102.00	-.09	202.79	-62.38	.057	A	.006	A	.006	14.9	66.6	.683	7	.683
61	71	STL-01	A	0.0	-57.53	32.84	1763.14	-371.27	.007	A	.006	A	.006	14.6	14.6	.079	7	.079
62	63	W1H-01	7	20.0	-37.53	-.00	6.21	-34.04	.076	A	.002	A	.002	7	34.1	152.4	2	.447
69	92	W0R-01	A	7.5	-3.74	.01	-.02	22.48	.012	A	.006	A	.006	1	26.3	56.1	1	.209
63	64	W1R-01	A	4.5	37.10	-.08	455.41	-9.29	.074	A	.006	A	.006	7	7.7	34.3	1	.225
63	65	W0R-01	A	7.5	-.82	.01	-27.83	-17.47	.014	A	.005	A	.005	2	26.3	56.1	2	.184
64	65	W1R-01	7	0.0	-62.29	-.00	300.47	-10.75	.092	A	.003	A	.003	7	14.9	66.6	1	.591
64	72	STL-01	7	0.0	-17.83	35.59	268.86	-1406.69	.008	7	.007	7	.007	14.6	14.6	.077	A	.077
65	66	W0R-01	7	0.0	-.15	-.01	8.80	14.60	.014	A	.002	A	.002	7	61.8	131.6	1	.133
65	67	W1R-01	7	0.0	-62.81	-.00	30.15	-36.83	.079	A	.002	A	.002	34.5	154.3	.797	2	.797
66	67	W0R-01	7	10.0	-.22	.01	10.16	-14.82	.009	7	.003	7	.003	35.1	74.7	.133	2	.133
70	66	AR7-01	2	0.0	.09	7.27	-.96	54.56	.101	A	.058	A	.058	43.9	43.9	.286	7	.286
67	68	W0R-01	7	10.0	-.40	-.01	-1.13	8.30	.007	A	.002	A	.002	7	55.1	74.7	1	.056
67	69	W1R-01	A	0.0	-105.40	-.02	649.06	-10.73	.115	A	.001	A	.001	34.5	154.3	1.070	1	1.070
70	67	STL-01	A	0.0	-186.93	108.51	12247.38	34.52	.072	7	.067	7	.067	8.8	8.8	.526	7	.526
67	76	STL-01	A	0.0	-62.59	-64.64	-1447.21	-1070.51	.009	A	.007	A	.007	3.9	3.9	.066	7	.066
68	69	W0R-01	A	0.0	-.03	.01	11.98	-5.65	.012	A	.001	A	.001	61.8	131.6	.049	7	.049
70	68	AR7-01	2	0.0	-.44	-.04	84.55	-46.72	.063	A	.041	A	.041	43.9	43.9	.247	7	.247
71	72	W1R-01	7	29.0	-9.42	-.01	2.97	-9.12	.010	7	.000	A	.000	49.5	220.9	.211	2	.211
71	73	W1R-01	7	0.0	-.00	-.00	2.05	-.00	.002	A	.000	A	.000	5.1	28.9	.001	A	.001
71	75	W0R-01	A	0.0	-10.76	-.00	7.05	4.10	.014	A	.000	A	.000	135.4	238.9	.878	1	.878
71	77	W1R-01	7	0.0	-.01	.01	166.55	-17.23	.014	7	.001	A	.001	42.8	191.3	.136	1	.136
71	81	W1R-01	A	0.0	-.00	-.00	8.25	-.00	.003	A	.000	A	.000	7	8.8	.004	7	.004
72	74	W1R-01	A	0.0	-.00	-.00	2.97	-.00	.002	A	.000	A	.000	5.1	28.9	.001	7	.001
72	75	W0R-01	7	0.0	-3.15	-.00	21.45	5.46	.014	A	.001	A	.001	135.4	238.9	.290	2	.290
72	78	W1R-01	7	0.0	-.25	.02	164.55	21.00	.014	7	.001	A	.001	42.8	191.3	.152	2	.152
72	82	W1R-01	A	0.0	-.00	-.00	8.25	-.00	.003	7	.000	A	.000	7	8.5	.004	7	.004
76	75	STL-01	A	0.0	-55.55	-18.71	-1039.55	-765.36	.006	A	.006	A	.006	10.7	10.7	.048	7	.048
77	75	W1R-01	A	14.5	2.79	.08	38.11	11.22	.008	A	.001	A	.001	24.7	110.5	.052	2	.052

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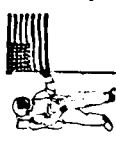


STRAIN GAGE STRESS REPORT NO. 2

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DATE 04/27/76

TEST PIECE ACWR STRUCTURE - U.S. NAVY (ASST. DIAMETER PILING) - C. CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED LOAD UNITS CK COND END(FT)	DIST FROM	FORCE		TORSION		CONTROLLING MEMBER ACTIONS		Z-Axis		LD V-Axis		NEXT LD HIGH UN. CK.	
				FX	FY	FX	FY	MOYENT IN-KIPS	MOYENT IN-KIPS	SMEAR CN	SMEAR CN	LD KLY/RZ	LD KLY/RZ	LD HIGH UN. CK.	LD HIGH UN. CK.
75	78 W18-01	.014	A 14.5	2.70	.05	.42	.42	-6.42	.007	7	.000	1	24.7	110.5	.037
76	77 W18-01	.007	A 18.2	-3.18	23.56	11.94	11.94	-31.43	.039	A	.020	A	32.4	32.4	.033
76	78 W18-01	.076	A 0.0	-1.72	-27.35	25.79	25.79	-54.34	.046	A	.020	A	32.4	32.4	.051
77	79 W18-01	.001	A 0.0	.00	.00	2.97	2.97	.00	.002	A	.000	7	5.1	22.9	.001
77	83 W18-01	.004	A 0.0	.00	.00	8.25	8.25	.00	.003	7	.000	7	8.5	38.1	.004
78	80 W18-01	.001	A 0.0	.00	.00	2.97	2.97	.00	.002	7	.000	A	5.1	22.9	.001
78	84 W18-01	.004	A 0.0	.00	.00	8.25	8.25	.00	.003	3	.000	A	8.5	38.1	.004



S T R A W M E M B E R S T R E S S R E P O R T N O . 3

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PILE ACWR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERRA

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITS CK	LOAD COND NO.	DIST FROM END(FT)	AXIAL STRESS KSI	REINFORCING STRESS Y KSI	Z KSI	SHEAR FORCE FV KIPS	KLY/RY KLZ/RZ KIPS	SECOND-HIGHEST		THIRD-HIGHEST			
										UNITY CHECK	COND	UNITY CHECK	COND		
1	4 P10-01	.565	7	6.1	-5.22	-6.99	0.00	127.75	74.36	6.0	6.0	.466	A	.450	1
2	5 P10-01	.558	7	6.1	-5.22	-6.83	0.00	-125.37	71.97	6.0	6.0	.455	A	.441	2
3	6 P10-01	1.001	A	6.1	-10.08	-11.53	0.00	.74	245.91	6.0	6.0	.496	7	.799	1
4	7 P10-01	.156	7	2.4	3.37	-6.99	0.00	.00	.36	1.2	1.2	.154	A	.157	1
5	8 P10-01	.563	7	2.4	3.23	.00	.01	.00	.36	32.1	32.1	.464	A	.451	1
6	9 P10-01	.556	7	1.0	-5.16	-6.84	0.00	24.98	-18.46	32.1	32.1	.453	A	.439	2
7	10 P10-01	.270	A	2.4	5.80	.00	.02	.00	.36	1.2	1.2	.262	7	.232	1
8	11 P10-01	.990	A	0.0	-9.84	-11.53	0.00	-7.74	-73.57	32.1	32.1	.445	7	.790	1
9	12 P10-01	.157	7	2.5	3.37	.00	.01	7.02	.73	1.2	1.2	.154	A	.137	1
10	13 P10-01	.150	7	2.5	-5.23	.00	.01	-6.72	.73	1.2	1.2	.146	A	.131	2
11	14 P10-01	.270	A	2.5	-5.80	.00	.02	.00	.73	1.2	1.2	.262	7	.232	1
12	15 P10-01	.235	A	29.0	-3.44	-1.37	0.00	3.33	.86	39.7	39.7	.235	7	.219	1
13	16 P10-01	.400	7	29.0	-6.64	-3.40	0.00	.91	2.58	39.7	39.7	.433	A	.410	2
14	17 P10-01	.107	A	32.4	.12	2.19	0.00	7.94	7.50	27.9	27.9	.070	2	.067	1
15	18 P10-01	.218	A	29.0	-3.24	-1.23	0.00	2.94	1.21	39.7	39.7	.218	7	.211	1
16	19 P10-01	.218	7	0.0	.64	4.08	0.00	1.25	-1.53	52.1	52.1	.192	2	.189	8
17	20 P10-01	.244	7	29.0	.53	4.73	0.00	-1.31	1.66	52.1	52.1	.213	2	.209	1
18	21 P10-01	.200	A	40.3	.51	4.01	0.00	-8.40	1.00	64.6	64.6	.187	7	.187	2
19	22 P10-01	.182	7	40.3	.41	3.52	0.00	-4.45	.50	64.6	64.6	.178	2	.173	8
20	23 P10-01	.461	7	0.0	-6.24	-5.23	0.00	-1.14	-2.30	39.7	39.7	.381	2	.370	8
21	24 P10-01	.472	A	32.4	.13	1.42	0.00	7.02	6.49	27.9	27.9	.400	3	.332	2
22	25 P10-01	.478	A	29.0	-6.11	-3.81	0.00	-2.97	2.20	39.7	39.7	.403	7	.401	7
23	26 P10-01	.193	A	29.0	1.09	3.07	0.00	-2.55	.79	52.1	52.1	.191	2	.190	7
24	27 P10-01	.778	A	0.0	-10.62	-2.72	0.00	-1.83	2.14	64.6	64.6	.708	1	.685	7
25	28 P10-01	.905	7	40.3	-10.45	-5.20	0.00	2.81	-2.19	64.6	64.6	.836	A	.824	2
26	29 P10-01	.405	A	0.0	-5.27	-2.24	0.00	1.66	-1.94	39.7	39.7	.342	7	.340	2
27	30 P10-01	.209	A	32.4	.17	5.21	0.00	-1.87	-15.26	27.9	27.9	.230	7	.194	1
28	31 P10-01	.806	A	40.3	-10.78	-3.63	0.00	-1.37	-2.49	64.6	64.6	.746	1	.720	7
29	32 P10-01	.876	7	40.3	-10.78	-4.27	0.00	-2.99	-2.00	64.6	64.6	.803	A	.799	2
30	33 P10-01	.051	A	2.4	1.06	.00	.04	14.19	9.55	31.7	31.7	.047	7	.042	1
31	34 P10-01	.493	7	52.4	-6.93	-3.48	0.00	.00	.36	1.2	1.2	.390	A	.377	2
32	35 P10-01	.043	A	2.4	.91	.00	.02	-11.48	.36	1.2	1.2	.039	7	.035	2
33	36 P10-01	.490	A	2.4	10.35	.00	.11	.00	6.65	31.7	31.7	.394	A	.373	2
34	37 P10-01	.490	A	2.4	-13.41	-3.40	0.00	.00	.36	1.2	1.2	.363	7	.347	2
35	38 P10-01	1.188	A	52.6	-13.41	-11.80	0.00	.74	-59.73	31.8	31.8	.977	7	.872	1
36	39 P10-01	.051	A	2.5	-1.06	.00	.02	1.98	.73	1.2	1.2	.047	7	.042	1
37	40 P10-01	.043	A	2.5	-9.1	.00	.04	-1.70	.73	1.2	1.2	.039	7	.035	2
38	41 P10-01	.481	A	2.5	-10.35	.00	.01	.00	.73	1.2	1.2	.382	7	.346	2
39	42 P10-01	.324	7	24.4	-3.48	-5.53	0.00	-5.02	.80	32.5	32.5	.308	A	.288	2
40	43 P10-01	.305	7	24.4	-3.05	-5.62	0.00	.00	3.56	32.5	32.5	.283	A	.274	1
41	44 P10-01	.365	7	32.4	5.37	4.51	0.00	-4.38	5.42	27.9	27.9	.296	A	.296	1
42	45 P10-01	.306	A	0.0	-1.71	-5.22	0.00	-4.25	-2.47	69.7	69.7	.302	7	.298	1
43	46 P10-01	.342	7	0.0	-3.45	-3.95	1.00	5.52	.74	52.5	52.5	.532	A	.505	2
44	47 P10-01	.113	A	24.4	-6.38	-2.02	0.00	1.51	.84	42.9	42.9	.101	1	.100	2
45	48 P10-01	.110	7	24.4	.06	1.92	0.00	-1.21	.78	42.9	42.9	.097	8	.097	1
46	49 P10-01	.655	7	0.0	8.48	5.67	0.00	.80	-3.39	52.5	52.5	.651	A	.652	1
47	50 P10-01	.400	7	52.4	7.20	5.38	0.00	5.87	2.16	27.9	27.9	.460	A	.395	1

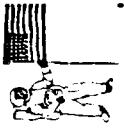


S T R U C T U R E M E M B E R S T R E S S R E P O R T N O . 3

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DATE 04/27/76

3-PILE CAP AND STRUCTURE -- U.S. NAVY (30-IN. DIAMETER PILING) -- C. CHAFIN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNIT/CHECK	LOAD COND NO.	DIST FROM END(FT)	AXIAL STRESS KSI	BENDING STRESS Y KSI	TORSIONAL STRESS Z KSI	SHEAR FORCE FV KIPS	FZ KIPS	KLYARY KLZARZ	SECOND-HIGHEST		THIRD-HIGHEST	
											UNITY CHECK	LOAD COND	UNITY CHECK	LOAD COND
24	38 BR1-01	.902	7	0.0	-10.49	-2.88	0.00	-4.31	1.72	81.3	.825	2	.800	8
25	26 BR2-01	.803	A	24.4	-10.57	-6.29	0.00	-1.58	3.49	32.5	.535	1	.523	2
25	27 BR4-01	.170	A	24.4	.00	2.89	0.00	-2.52	.52	42.9	.165	7	.164	2
26	27 BR2-01	.411	A	0.0	2.24	6.64	0.00	1.77	-4.03	32.5	.255	2	.255	1
26	34 BR1-01	.979	A	0.0	-12.94	-2.79	0.00	4.11	1.11	69.7	.814	1	.784	7
26	3A JL1-01	1.409	A	32.6	12.59	18.91	0.00	4.44	-32.47	28.0	1.204	7	1.087	2
28	31 BRN-01	.055	A	2.4	-1.14	.00	.01	.00	.56	1.2	.054	7	.046	1
29	43 P20-01	.782	7	32.4	-0.40	-10.09	0.00	-36.44	-15.23	31.7	.697	8	.624	2
29	32 WKN-01	.053	A	2.4	-1.12	.00	.03	.00	.54	1.2	.052	7	.045	2
29	44 P20-01	.784	7	32.4	-6.40	-10.22	0.00	36.08	-16.34	31.7	.717	8	.640	2
30	33 BRN-01	1.061	A	2.4	-22.80	.00	.01	0.00	.36	1.2	.873	7	.780	2
30	45 P20-01	1.534	A	36.1	-14.56	-17.66	0.00	-2.74	-74.41	35.3	1.351	7	1.168	1
31	34 BRN-01	.055	A	0.0	1.14	.00	.01	-2.42	.36	1.2	.054	7	.046	2
32	36 WKN-01	.053	A	0.0	1.12	.00	.03	2.33	.36	1.2	.052	7	.045	2
33	38 WKN-01	1.054	A	2.5	22.44	.00	.01	.00	.73	1.2	.875	7	.782	2
34	35 HR5-01	.265	A	0.0	-1.58	-3.07	0.00	-2.91	-1.59	36.2	.186	7	.183	1
39	34 HR5-01	.791	A	19.4	12.49	4.20	0.00	-1.18	1.93	36.2	.593	7	.511	2
34	40 JL2-01	.462	7	14.2	6.58	3.61	0.00	-36.32	-19.13	12.0	.412	8	.375	2
34	53 BR1-01	1.180	7	47.4	-11.41	-9.34	0.00	-6.64	-7.40	59.7	1.032	8	1.001	2
35	36 HR5-01	.167	7	19.8	.42	3.20	0.00	-2.60	1.45	36.2	.145	8	.105	3
35	37 HR6-01	.146	A	0.0	-1.72	-1.26	0.00	-1.40	.50	35.8	.120	1	.117	7
39	35 BR6-01	.149	A	19.8	1.33	1.89	0.00	1.48	.44	35.8	.117	7	.113	2
36	37 HR5-01	.330	A	0.0	3.42	3.71	0.00	.47	-1.77	36.2	.280	7	.247	2
36	41 JL2-01	.343	7	14.2	4.23	3.19	0.00	38.42	-16.85	12.0	.313	8	.286	2
36	49 BR1-01	.465	7	47.4	-1.28	-8.06	0.00	13.23	1.00	59.7	.449	8	.424	2
37	38 BR5-01	.309	7	30.2	-1.88	-4.36	0.00	.90	1.65	59.3	.182	8	.152	2
37	39 BR6-01	.186	A	19.8	2.51	1.51	0.00	-2.34	.38	35.8	.174	7	.170	2
38	39 BR5-01	.242	7	0.0	-9.22	-5.04	0.00	-1.26	-1.75	59.3	.668	8	.603	2
38	42 JL2-01	1.246	A	15.0	10.59	16.31	0.00	11.50	-178.15	12.7	1.120	7	.978	2
34	51 BR1-01	.938	A	55.7	-8.80	-7.07	0.00	4.61	-6.16	71.3	.911	7	.875	1
40	49 JL2-01	.855	7	18.3	9.46	12.00	0.00	-57.56	-37.44	15.5	.835	8	.675	2
41	51 JL2-01	.786	7	18.3	4.50	12.67	0.00	64.44	-37.91	15.5	.773	8	.623	2
42	53 JL2-01	1.249	A	0.0	10.67	16.31	0.00	11.50	74.43	18.0	1.124	7	.981	2
43	46 WKN-01	.024	A	2.4	.49	.00	.02	.00	.36	1.2	.021	1	.021	7
43	55 P20-01	.779	7	0.0	-9.81	-10.02	0.00	-24.32	-30.57	4.5	.694	8	.626	2
44	47 BRN-01	.022	A	2.4	.46	.00	.02	.00	.36	1.2	.017	2	.016	1
44	56 P20-01	.785	7	0.0	-6.40	-10.17	0.00	32.11	-40.31	4.5	.716	8	.639	2
45	48 BRN-01	.266	A	2.4	5.74	.00	.02	0.00	.56	1.2	.205	7	.194	1
45	57 P20-01	1.452	A	0.0	-13.70	-17.66	0.00	-7.40	227.19	4.5	1.320	7	1.137	2
46	49 BRP-01	.024	A	2.5	.49	.00	.03	1.03	.73	1.2	.021	1	.021	7
47	51 BRN-01	.023	A	2.5	.46	.00	.02	.97	.73	1.2	.017	2	.016	1
48	53 BRN-01	.267	A	2.5	-5.74	.00	.02	-7.34	.56	1.2	.205	7	.194	1
49	50 BR3-01	.450	7	15.1	-4.95	-4.77	0.00	-7.34	-1.48	20.5	.390	8	.369	2
50	49 BR3-01	1.234	7	15.2	14.63	14.63	0.00	-2.33	8.11	20.5	1.170	8	.982	2
49	55 JL2-01	.939	7	0.0	6.16	14.15	0.00	133.03	56.41	3.9	.906	8	.746	2
50	51 BR3-01	.432	7	0.0	-5.21	-4.12	0.00	6.14	-2.01	20.5	.378	8	.354	2
50	52 BR5-01	.223	7	0.0	.76	4.04	0.00	1.07	-1.73	26.0	.210	8	.184	1
54	50 BR5-01	.177	7	15.1	.10	3.72	0.00	-0.95	1.77	26.0	.160	8	.145	2



PILE CAP STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITS CK NO.	LOAD COND NO.	DIST FROM END(FT)	AXIAL STRESS KSI	BENDING STRESS Y KSI	Z KSI	SHEAR FORCE		FZ KIPS	KLY/RVY KLZ/PZ	SECOND-HIGHEST LOAD COND		HIGHEST UNIT CHECK	THRD-HIGHEST UNIT CHECK
								FV KIPS	KIPX			UNIT CHECK	COND		
51	52 BR3-01	.79R	7	0.0	-2.24	-14.86	0.00	.83	-8.52	20.5	20.5	.614	2	.606	1
51	56 JL2-01	.98R	7	0.0	6.05	15.25	0.00	-14.89	68.17	3.9	3.9	.933	8	.777	2
52	53 AR3-01	.87R	A	15.1	-1.61	-14.28	0.00	-7.44	9.65	20.5	20.5	.859	7	.707	2
52	54 AR5-01	.265	A	0.0	.60	4.63	0.00	4.11	.35	26.0	26.0	.256	7	.236	2
53	54 AR3-01	1.364	A	0.0	-13.11	-16.35	0.00	-2.75	-9.24	20.5	20.5	1.270	7	1.069	2
53	57 JL2-01	1.215	A	4.6	12.23	14.02	0.00	-5.43	-179.59	3.9	3.9	1.104	7	.949	2
55	54 STL-01	.727	7	28.5	-1.96	-14.67	0.00	7.38	-31.66	27.8	27.8	.653	6	.567	2
56	59 STL-01	.775	7	28.5	-1.04	-15.62	0.00	-12.27	-58.50	27.8	27.8	.704	8	.605	2
57	60 STL-01	.930	A	28.5	-2.15	-17.77	0.00	-6.17	81.82	27.8	27.8	.842	7	.694	2
58	59 AR5-01	.508	A	29.0	1.10	4.88	0.00	-10.83	.84	56.6	56.6	.491	8	.490	2
60	58 AR5-01	.834	A	0.0	-5.40	-11.89	0.00	5.56	-3.96	56.6	56.6	.769	7	.633	1
58	61 STL-01	.674	A	0.0	-6.00	-13.93	0.00	10.77	-61.01	14.6	14.6	.667	7	.526	2
58	67 AR5-01	1.133	7	32.6	-11.28	-8.13	0.00	-3.44	-2.89	64.7	64.7	1.005	2	.927	8
59	60 BR5-01	.850	A	29.0	5.34	13.09	0.00	-6.34	3.86	56.6	56.6	.820	7	.760	2
59	61 AR5-01	.600	7	0.0	-1.21	-11.56	0.00	-13.13	.46	64.7	64.7	.634	2	.624	8
59	64 STL-01	.781	7	0.0	-1.98	-15.42	0.00	18.40	78.29	14.6	14.6	.704	8	.600	2
60	64 AR5-01	1.177	A	0.0	-11.08	-9.18	0.00	-7.12	3.03	64.7	64.7	1.017	1	.967	7
60	70 STL-01	.850	A	0.0	-1.40	-16.95	0.00	8.82	-93.40	5.9	5.9	.820	7	.646	2
61	62 W1A-01	.959	A	0.0	2.28	5.95	13.03	3.50	-9.85	7.7	34.3	.748	7	.645	1
69	61 W1R-01	.730	A	8.7	-6.30	2.28	-5.82	.86	5.26	14.9	66.6	.683	7	.626	1
61	71 STL-01	.953	A	0.0	-4.2	-11.57	0.00	-1.77	-9.34	14.6	14.6	.079	7	.061	2
62	63 W1R-01	.556	7	20.0	-2.30	.67	-3.18	.26	.94	34.1	152.4	.447	2	.295	8
69	62 W1R-01	.216	A	7.5	.53	-6.00	4.01	-4.3	.32	26.3	56.1	.209	1	.205	7
61	64 W1R-01	.352	A	4.5	2.29	4.89	-8.7	5.8	6.64	7.7	30.3	.225	7	.177	2
63	65 W1R-01	.206	A	7.5	-1.32	-1.34	-3.0	.30	.22	26.3	56.1	.144	2	.183	7
64	65 W1A-01	.395	7	0.0	-3.45	3.37	-1.00	-4.1	-3.21	14.9	66.6	.591	8	.329	2
64	72 STL-01	.844	7	0.0	-1.15	-1.68	0.00	-11.10	-2.46	14.6	14.6	.077	8	.062	2
65	66 W1R-01	.141	7	0.0	-2.02	.42	2.61	.11	.24	61.8	131.6	.133	8	.124	2
65	67 W1R-01	.145	7	0.0	-3.88	.30	-2.05	.30	-1.71	30.5	150.3	.797	2	.602	8
66	67 W1R-01	.298	7	10.0	.05	6.42	0.00	2.18	.01	43.9	43.9	.244	7	.140	8
70	66 BR7-01	.023	2	0.0	.02	6.42	0.00	-1.10	.09	35.1	74.7	.056	2	.022	1
67	68 W1R-01	.023	A	0.0	-0.51	7.28	1.40	.18	-10.65	34.5	154.5	1.070	1	.577	7
67	67 STL-01	.559	A	0.0	-1.37	-10.69	0.00	8.73	-108.85	8.8	8.8	.526	7	.426	2
67	76 STL-01	.094	A	0.0	-0.46	-1.57	0.00	-6.00	8.65	3.9	3.9	.066	7	.054	2
68	69 W1R-01	.072	A	0.0	.00	5.50	-1.61	.05	.33	61.8	131.6	.049	7	.044	1
70	68 BR7-01	.255	2	0.0	.00	5.50	0.00	-2.15	.00	43.9	43.9	.247	7	.085	8
71	72 W1R-01	.266	7	29.0	-5.8	.95	-8.5	.00	.43	49.5	220.9	.211	2	.093	8
71	73 W1R-01	.001	7	0.0	-0.0	.03	-0.0	.00	.19	135.4	238.9	.874	1	.235	7
71	75 W1R-01	1.463	A	0.0	-2.36	1.87	1.27	.62	-1.32	42.8	191.3	.136	1	.134	2
71	77 W1R-01	.153	7	0.0	-0.0	1.87	-1.01	.00	.28	8.5	38.1	.004	7	.004	3
71	81 W1R-01	.004	A	0.0	-0.0	.09	0.00	.00	.17	5.1	22.9	.001	7	.001	3
72	74 W1A-01	.001	A	0.0	.03	.03	0.00	.03	.27	135.4	238.9	.290	2	.152	8
72	75 W1B-01	.441	7	0.0	-6.9	2.14	1.69	.00	-1.30	42.8	191.3	.152	2	.148	1
72	78 W1A-01	.149	7	0.0	1.2	1.24	1.46	.00	.27	8.5	38.1	.004	7	.004	3
72	82 W1R-01	.004	A	0.0	-0.0	.09	0.00	.00	.15	10.7	10.7	.048	7	.039	2
76	75 STL-01	.071	A	0.0	-4.1	-1.13	0.00	-6.00	.67	20.7	110.5	.052	2	.052	7
77	75 W1B-01	.074	A	14.5	.17	.43	1.05	.14	.67	20.7	110.5	.052	2	.052	7

5.400
1.400
101.312

Error in Spreader Program



STRAIN GAGE MEASUREMENT STRESS REPORT

PAGE 4
DATE 04/27/76

PILE ACWR STRUCTURE -- U.S. NAVY (36-IN. DIAMETER PILING) -- C. CHERN

MEMBER NO.	GROUP ID	MAXIMUM COMBINED UNITS CK NO.	LOAD COND	DIST FROM END(FT)	AXIAL STRESS KSI	RESULTING STRESS		SHEAR FORCE		PZ KIPS	KLY/RV KLY/RZ	SECOND-HIGHEST		THIRD-HIGHEST	
						Y KSI	Z KSI	FV KIPS	UNITY CHECK			L/AD COND	UNITY CHECK	LOAD COND	
75	78 W1R-01	.034	A	14.5	.17	.00	.64	.01	.33	24.7	110.5	.037	7	.032	2
76	77 BR6-01	.047	A	14.2	-.22	-.77	0.00	.14	.31	32.4	32.4	.055	7	.027	3
76	78 BR6-01	.076	A	0.0	-.25	-1.57	0.00	-.36	.40	32.4	32.4	.051	7	.049	2
77	74 W1R-01	.001	A	0.0	.00	.03	-.00	-.00	.17	5.1	22.9	.001	7	.001	3
77	83 W1R-01	.004	A	0.0	.00	.09	-.00	-.00	.27	8.5	38.1	.004	7	.004	3
78	80 W1P-01	.001	A	0.0	.00	.03	-.00	-.00	.16	5.1	22.9	.001	7	.001	3
78	84 W1R-01	.004	A	0.0	.00	.09	-.00	-.00	.27	8.5	38.1	.004	7	.004	3



10.02.24. BACKWARD SUBSTITUTION
 10.02.24. MOUNTING DEFLECTIONS
 10.02.56. MOUNTING FORCES
 10.00.09. COMPUTING UNITY CHECK
 10.00.15. COMPUTING FOURTH TERM
 10.00.21. ASC STOP STRAN
 10.00.23. STIP
 10.00.23SM* 61000 20.355 22561 3410.
 10.00.23SFI 30 2
 10.00.23.COST. 61000 26.355
 10.00.24. SERVICE UNITS= 214.2
 10.00.24. JOB COSTS= 53.55
 10.00.24SFI 17248 26.375 5
 10.00.24.FXIT. 2368 26.375
 10.00.24SJT00 2368 *DISC PRUS* DISC ACC
 10.00.24. *FL* *CPU SEC. *DISC PRUS* TAPE ACC
 10.00.24.*P.F. PRUS*P.F. ACC *TAPE PRUS* TAPE ACC

A-6 MEMBER WEIGHT TAKEOFF



15940 JOB URTIM FROM GR00000027 , NSPEC , MVIC=0027001, 0A4
 //LEC9016 JOB (0004215500277100P16C27A16), CMERR , PRTY=4, CLASS=, C

// TIME(005,00), REGTIME=250K
 // MAIN LINES(010, 1), CARDS(006, C)
 // JDLIB DD DS=DCPRD0, LIB=, DISR=SRH
 // EXEC DD=LEFC27010
 // FT06F001 DD SVS=UTEA
 // IE15F001 DD *

LEC9016 IEF001 LEC9016 STARTED TIME=10,59,56
 LFC0016 IFF24F D 6A3, ASP083
 *LFC9016 *42 IFCASPO 683 IS LFC9016 A FT06F001
 *LFC9016 *43 IFCASPO 684 IS LFC9016 ASPI0001

LFC0016 IFC20F K 6A4, 017076, 01, LFC9016
 LEC9016 TIMEFC9016 CC=00002705 P=2777100 P JALFC27A16 IFCERRA AB7978
 LEC9016 IEF401 LEC9016 EXEC TIME=11,00,17
 //LEFC9016 JOB (0004270500277100P16C27A16), CMERR , PRTY=4, CLASS=, *

// TIME(005,00), REGTIME=250K
 // JDLIB DD DS=DCPRD0, LIB=, DISR=SRH
 // EXEC DD=LEFC27010
 // FT06F001 DD SVS=UTEA
 // IE15F001 DD *

// TIME(005,00), REGTIME=250K
 // JDLIB DD DS=DCPRD0, LIB=, DISR=SRH
 // EXEC DD=LEFC27010
 // FT06F001 DD SVS=UTEA
 // IE15F001 DD *

IEF2301 ALLOC. FLX LEC9016
 IEF2371 104 ALLOCATED TO JDLIB
 IEF2371 6A3 ALLOCATED TO FT06F001
 IEF2371 684 ALLOCATED TO FT06F001
 IEF1421 * STEP WAS EXECUTED = COND COND 0000
 IEF2A51 DCPRD0, LIB=6
 IEF2A51 VOL SER NOS= 041002
 IEF2A51 SYSTAL24, T105932, 00001, LFC9016, ASP0A001 DELTFD
 IEF2A51 VOL SER NOS= ASP0A01
 IEF2A51 SYSTAL24, T105932, 00001, LFC9016, ASP10001 DELTFD
 IEF2A51 VOL SER NOS= 017076
 IEF3731 STEP / / START 76124, 1059
 IEF3741 STEP / / STOP 76124, 1100 CPU 0MIN 00.32SEC STOR VIRT 232K

PAGES DATA ACQUISITION SYSTEM
 * * * * *
 * STEP NAME START TIME 10,59,53,41 VIRT COND RECD 250 K LCS CORE USED 0 K STEP CPU 00,00,00,32 *
 * PGM NAME LEC27A16 STOP TIME 11,00,17,35 VIRT COND USED 232 K LCS CORE USED 0 K JOB CPU 00,00,00,32 *
 * DISPATCH PROT 1 ELAP. TIME 00,00,23,94 VIRT COND RECD 0 K LCS CORE RECD 0 K CONDITON CODE 0000 *
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UNIT	EXCP COUNT	UNIT	EXCP COUNT	UNIT	EXCP COUNT	UNIT	EXCP COUNT	UNIT	EXCP COUNT
404	0	6A3	235	6A4	45	27A	278		
							EXCP TOTAL		
							278		
IEF3741 STEP / / TOTAL EXCP 00027A REPT									
IEF2A51 DCPRD0, LIB=6									
IEF2A51 VOL SER NOS= 041002									
IEF3741 JOB / LFC9016 / START 76124, 1059									

LIST OF BOAT DATA -- ACAD 3-BOTLE SIZE CTIME MATERIAL LIST G -- U.S. NAVY -- F. CHERRY

QTY	UNIT	PRICE	AMOUNT	WEIGHT	DESCRIPTION
1		36,000	1,500	0.0	PTING
1		36,000	1,750	0.0	PTING
1		36,000	1,250	0.0	PTING
1		41,000	1,000	0.0	JACKET LFG JOINT CAN
1		41,000	1,000	0.0	JACKET LFG JOINT CAN
1		42,000	1,500	0.0	JACKET LFG SPLASH 7/4
1		40,000	0,500	0.0	JACKET LFG
1		40,000	0,500	0.0	JACKET LFG
1		24,000	0,750	0.0	JACKET BRACE JT CAN
1		14,000	0,500	0.0	JKT HORIZ. BRACE 1ST
1		10,000	0,375	0.0	JKT VERT. BRACE 1ST
1		16,000	0,500	0.0	JKT VERT. BRACE 1ST
1		18,000	0,500	0.0	JKT HORIZ. BRACE 2ND
1		14,000	0,375	0.0	JKT VERT. BRACE 2ND
1		20,000	0,625	0.0	JKT VERT. BRACE 2ND
1		12,750	0,500	0.0	JKT HORIZ. BRACE 3RD
1		12,750	0,375	0.0	JKT VERT. BRACE 3RD
1		20,000	0,625	0.0	JKT VERT. BRACE 3RD
1		20,000	1,000	0.0	JKT VERT. BRACE 3RD
1		16,000	0,500	0.0	JKT HORIZ. BRACE 4TH
1		12,750	0,500	0.0	JKT HORIZ. BRACE 4TH
1		36,000	1,250	0.0	SUPER-STRUCTURE LEGS
1		12,750	0,500	0.0	SUPER-STRUCTURE BRAC
1		12,750	0,500	0.0	SUPER-STRUCTURE BRAC
1		12,750	0,375	0.0	SUPER-STRUCTURE BRAC
1		6,625	0,280	0.0	EQUIPMENT DECK
2		16,000	50,000	0.0	EQUIPMENT DECK
2		8,000	24,000	0.0	EQUIPMENT DECK
2		8,000	24,000	0.0	EQUIPMENT DECK
3		20,000	25,000	0,250	TOP DECK
2		18,000	50,000	0.0	TOP DECK
2		12,000	27,000	0.0	TOP DECK
2		6,000	15,500	0.0	TOP DECK
6		12,000	25,000	0.0	TOP DECK
6		12,000	25,000	0.0	TOP DECK
3		0,330	5,750	0,375	TOP DECK
3		35,000	35,000	0,250	TOP DECK
3		0,420	0,830	1,000	SHIMS

AC-9 3-PILE STRUCTURE MATERIAL LISTING -- J.S. LAVY -- C. CHERN

PIPE	NOMINAL DIMENSION (IN. X IN.)	QUANTITY	MEMBER LENGTH (FT)	TOTAL LENGTH (FT)	TOTAL WEIGHT (POUNDS)
	42.000 O.D. X 1.500 AT	3	21.20	63.60	41303.4
	41.000 O.D. X 1.000 AT	3	14.00	42.00	23090.7
	41.000 O.D. X 1.000 AT	3	16.00	48.00	12828.2
	41.000 O.D. X 1.000 AT	3	6.00	18.00	7696.0
	40.000 O.D. X 0.500 AT	3	25.40	76.32	16113.4
	40.000 O.D. X 1.500 AT	3	23.40	70.32	10840.6
	36.000 O.D. X 1.750 AT	3	50.00	150.00	96110.9
	36.000 O.D. X 1.500 AT	3	160.00	480.00	265542.8
	36.000 O.D. X 1.250 AT	3	57.00	171.00	79004.2
	36.000 O.D. X 1.250 AT	3	22.00	66.00	36647.3
	24.000 O.D. X 0.750 AT	3	7.00	21.00	3914.6
	20.000 O.D. X 1.000 AT	3	13.86	41.58	8004.9
	20.000 O.D. X 0.625 AT	3	54.60	163.80	21204.0
	20.000 O.D. X 0.625 AT	3	10.00	30.00	3843.5
	18.000 O.D. X 0.500 AT	6	25.50	153.00	14311.4
	18.000 O.D. X 0.500 AT	6	24.50	146.28	13682.8
	16.000 O.D. X 1.500 AT	6	40.00	240.00	19443.6
	16.000 O.D. X 0.500 AT	6	15.15	90.90	7530.9
	14.000 O.D. X 0.375 AT	3	29.00	87.00	4751.9
	14.000 O.D. X 0.375 AT	3	24.54	73.62	3994.9
	12.750 O.D. X 0.500 AT	3	32.05	97.95	6413.5
	12.750 O.D. X 0.500 AT	3	29.00	87.00	5096.5
	12.750 O.D. X 0.500 AT	6	19.77	118.62	7766.9
	12.750 O.D. X 0.500 AT	3	15.15	45.45	2975.9
	12.750 O.D. X 0.375 AT	3	19.77	59.31	2942.3
	12.750 O.D. X 0.375 AT	2	17.10	34.20	1745.9
	6.625 O.D. X 0.250 AT	2	6.10	12.20	541.9

TOTAL WEIGHT OF PIPE MEMBERS = 717073.1

ACMR 3-PILE STRUCTURE MATERIAL LISTING -- U.S. NAVY -- C. CHERN

W SHAPE

NOMINAL DIMENSION	QUANTITY	MEMBER LENGTH (FT)	TOTAL LENGTH (FT)	TOTAL WEIGHT (POUNDS)
18 X 50,00	4	55,00	140,00	7000,0
18 X 50,00	5	29,00	47,00	435,0
12 X 27,00	4	35,00	140,00	5700,0
18 X 27,00	2	25,00	50,00	1200,0
18 X 24,00	10	20,00	200,00	4000,0
6 X 15,50	2	27,00	58,00	899,0

TOTAL WEIGHT OF W-SHAPE MEMBERS = 22029,0

ACMP 3-PILE STRUCTURE MATERIAL LISTING -- U.S. NAVY -- C. CHERN

PLATE	APPROXIMATE DIMENSIONS (FT X FT X IN)	QUANTITY	TOTAL AREA (SQ. FT)	TOTAL WEIGHT (POUNDS)
	0.42 X 0.41 X 1.000	12	4.18	170.8
	0.33 X 5.75 X 0.575	57	108.16	1656.2
	35.00 X 35.00 X 0.250	1	1225.00	12505.2
	20.00 X 25.00 X 0.250	1	500.00	5104.2
TOTAL WEIGHT OF PLATES			19456.3	

ACMR 3-PILE STRUCTURE MATERIAL LISTING -- U.S. NAVY -- C. CHEN

CHANNELS

NOMINAL DIMENSION	QUANTITY	MEMBER LENGTH (FT)	TOTAL LENGTH (FT)	TOTAL WEIGHT (POUNDS)
C 12 X 25.00	4	35.00	140.00	3500.0
C 12 X 25.00	4	3.00	12.00	300.0
TOTAL WEIGHT OF CHANNELS				3800.0

TOTAL WEIGHT = 742334.4

62

BILL OF MATERIALS SUMMARY
ACMR 3-PILE STRUCTURE MATERIAL LISTING -- U.S. NAVY -- G. CHERN

RISE	MINIMAL DIMENSIONS	TOTAL LENGTH (FEET)	TOTAL WEIGHT (POUNDS)
	42,000 0.0. X 1,500 WT	65.00	43305.43
	41,000 0.0. X 1,000 AT	102.00	43015.71
	40,000 0.0. X 0,500 WT	140.60	50960.07
	38,000 0.0. X 1,750 WT	150.00	96110.08
	36,000 0.0. X 1,500 AT	480.00	265542.75
	34,000 0.0. X 1,250 AT	237.00	110351.04
	24,000 0.0. X 0,750 WT	21.00	3012.59
	20,000 0.0. X 1,000 AT	41.40	8408.65
	20,000 0.0. X 0,625 WT	193.00	25047.54
	14,000 0.0. X 0,500 AT	299.24	27000.20
	14,000 0.0. X 0,500 WT	330.90	27410.55
	14,000 0.0. X 0,375 AT	160.14	6746.41
	12,750 0.0. X 0,500 AT	339.12	22452.74
	12,750 0.0. X 0,375 AT	95.31	1728.21
	6,625 0.0. X 0,280 WT	18.00	341.86

* SHAPE

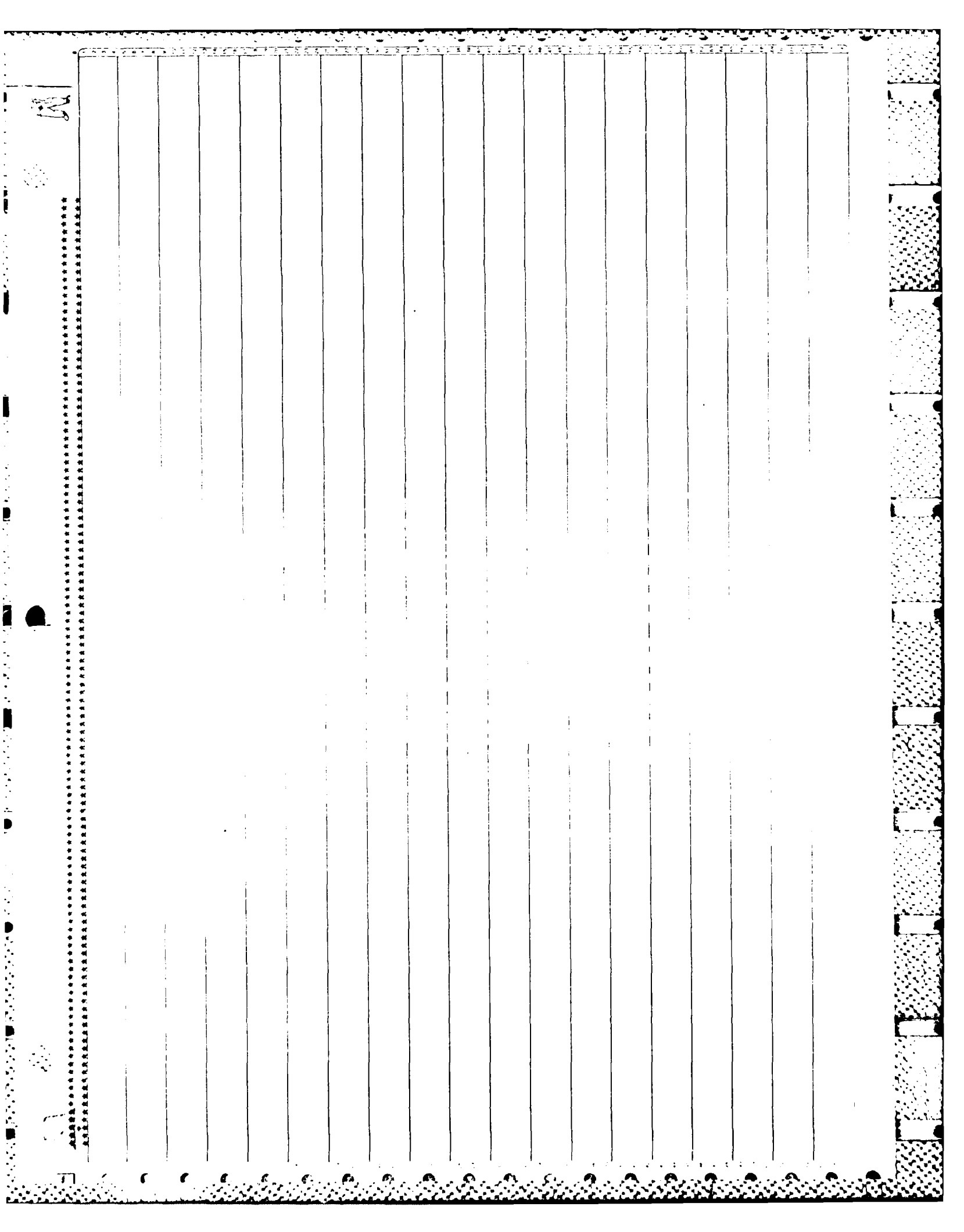
	X 18 X 50.00	227.00	11350.00
	" 12 X 27.00	140.00	5780.00



BILL OF MATERIALS SUMMARY
 ACNR SHIPLE STRUCTURE MATERIAL LISTING -- U.S. NAVY -- C. CHERN

2	8 X 24.00	250.00	0	11.00
2	6 X 15.50	50.00	0	499.00
CHANNELS				
C	12 X 25.00	152.00		\$400.00
PLATE				
	1.000 THICKNESS	4.14		170.81
	0.375 THICKNESS	108.14		1656.14
	0.250 THICKNESS	1725.00		17609.47

TOTAL WEIGHT 762334.00 LBS





ASP JOB NO. = 7978

DATE = 76.124

/ALEC9016 JOB (0044270502777100PLEC27616),ICMERN 1,PTYER,C1ASSE,C7978

ELAPSED TIME ON MAIN = A = 000.00, START TIME = 10.59.53

DDNAME = SYSMSG PRINTED ON RM027PRI, LINES = 000077
DDNAME = FT00F001 PRINTED ON RM027PRI, LINES = 000235
LINES OUTPUT FOR THIS JOB = 000312

CARDS FROM MAIN FOR THIS JOB = NONE



PAGES DATA AND REPORT SYSTEM

1 JRA LOG NUMBER = LFC0116 74120 17.15.03

2 OPERATOR = CHEV

3 ACCTG DATA 000027050277710101FC27A16

4 JOHNAME LFC016

5 SYSTEM ID 5R - 5R

DATE	05/03/76	76.124	INITIATION TIME	17.15.25.20
END TIME	00.00.00.96		TERMINATION TIME	17.15.46.13
PRIORITY	02		ELAPSED TIME	00.00.20.93
CLASS	A		COMPLETION STATUS	0000

6 *****

AD-A164 421

STRUCTURAL CONCEPT ANALYSIS REPORT FOR THE EAST COAST
AIR COMBAT MANEUVER. (U) CREST ENGINEERING INC TULSA OK
MAY 76 27-771-92-APP-C CHES/NAVFAC-FPO-7601-APP-C
N62477-76-C-8179

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UNCLASSIFIED

F/G 13/13

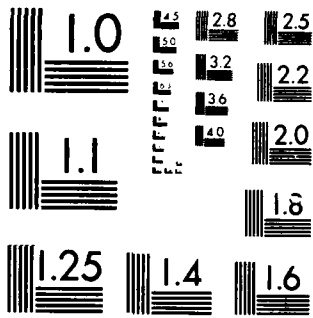
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FBI/DOJ

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DPIC



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963-A

15. Avenue C, 10005

LIST OF DATA -- 3000 -- 3000 -- 3000 -- 3000

1	50,000	1,500	0.0	100,000	511.100
1	50,000	1,750	0.0	50,000	511.100
1	50,000	1,250	0.0	100,000	511.100

AC-9 3-DITE STRUCTURE MATERIAL LISTING -- BILLY G. ...

PIPE

QUANTITY	DESCRIPTION	UNIT PRICE	TOTAL PRICE	TOTAL WEIGHT (POUNDS)
3	36,000 D.P. X 1,750 FT	5.00	150,000	96110.0
3	36,000 D.P. X 1,500 FT	17.00	510,000	205542.4
3	36,000 D.P. X 1,250 FT	22.00	810,000	31667.3

TOTAL WEIGHT OF PIPE MEMBERS = 592300.0

TOTAL WEIGHT = 302300.9

BILL OF MATERIALS SUMMARY
 ACME SUPPLY STRUCTURE MATERIAL LISTING -- PIPE -- U.S. ADV--CUMERS

APPROXIMATE TOTAL WEIGHT (LBS)

PIPE

36,000 O.D. X 1.750 WT	15,000	9450.00
36,000 O.D. X 1.500 WT	480,000	288000.75
36,000 O.D. X 1.250 WT	66,000	33007.25

TOTAL WEIGHT 302100.00 LBS

JACKET LEG JOINT CA	5.000	1.000	0.00	3	5.000	JACKET LEG JOINT CA
JACKET LEG JOINT CA	10.000	1.000	0.00	5	10.000	JACKET LEG JOINT CA
JACKET LEG JOINT CA	15.000	1.000	0.00	5	15.000	JACKET LEG JOINT CA
JACKET LEG SPLASH 7	21.230	1.500	0.00	5	21.230	JACKET LEG SPLASH 7
JACKET LEG	25.100	1.500	0.00	5	25.100	JACKET LEG
JACKET LEG	28.000	1.500	0.00	5	28.000	JACKET LEG
JACKET HRACE IT CA	7.000	0.750	0.00	5	7.000	JACKET HRACE IT CA
1ST HURT. BRACE 1ST	35.500	0.500	0.00	5	35.500	1ST HURT. BRACE 1ST
1ST HURT. BRACE 1ST	39.000	0.500	0.00	5	39.000	1ST HURT. BRACE 1ST
1ST HURT. BRACE 1ST	42.500	0.500	0.00	5	42.500	1ST HURT. BRACE 1ST
1ST HURT. BRACE 2ND	21.300	0.500	0.00	5	21.300	1ST HURT. BRACE 2ND
1ST HURT. BRACE 2ND	21.300	0.500	0.00	5	21.300	1ST HURT. BRACE 2ND
1ST HURT. BRACE 2ND	52.600	0.500	0.00	5	52.600	1ST HURT. BRACE 2ND
1ST HURT. BRACE 3RD	19.770	0.500	0.00	5	19.770	1ST HURT. BRACE 3RD
1ST HURT. BRACE 3RD	19.770	0.500	0.00	5	19.770	1ST HURT. BRACE 3RD
1ST HURT. BRACE 3RD	15.000	0.500	0.00	5	15.000	1ST HURT. BRACE 3RD
1ST HURT. BRACE 4TH	15.150	0.500	0.00	5	15.150	1ST HURT. BRACE 4TH
1ST HURT. BRACE 4TH	15.150	0.500	0.00	5	15.150	1ST HURT. BRACE 4TH

CRESE BROS. CO.
701 SA. WILSON

CREATED: T. APR 11 1974
ADDPFID: FPM 1975

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ACUR 3-DICE STRUCTURE MATERIAL TITANUM -- TACUFT

U.S. NAVY - C. CHEP*

ACME TABLE STRUCTURE MATERIAL LISTING -- 100-SET

PIPE

QUANTITY	UNIT	DESCRIPTION	PRICE PER UNIT	TOTAL PRICE	QUANTITY	UNIT	DESCRIPTION	PRICE PER UNIT	TOTAL PRICE
42,000	0.00	X 1.500 FT	21.20	884.40	63.00			1335.60	
51,000	0.00	X 1.000 FT	14.00	714.00	54.00			756.00	
41,000	0.00	X 1.000 FT	14.00	574.00	30.00			420.00	
41,000	0.00	X 1.000 FT	14.00	574.00	14.00			196.00	
30,000	0.00	X 0.500 FT	25.40	762.00	74.32			1885.66	
40,000	0.00	X 0.500 FT	25.40	1016.00	74.32			1885.66	
20,000	0.00	X 0.750 FT	13.00	260.00	21.00			270.60	
20,000	0.00	X 1.000 FT	14.00	280.00	41.00			574.00	
20,000	0.00	X 0.625 FT	14.00	280.00	143.00			2004.00	
14,000	0.00	X 0.500 FT	25.40	355.60	31.00			783.40	
14,000	0.00	X 0.500 FT	25.40	355.60	153.00			3845.40	
14,000	0.00	X 0.500 FT	24.50	343.00	146.26			3577.86	
15,000	0.00	X 0.500 FT	41.00	615.00	240.00			9840.00	
14,000	0.00	X 0.575 FT	15.00	210.00	67.00			1009.00	
14,000	0.00	X 0.575 FT	20.00	280.00	47.00			946.00	
12,750	0.00	X 0.500 FT	19.77	252.00	73.14			1366.00	
12,750	0.00	X 0.500 FT	15.15	193.00	114.62			1746.00	
12,750	0.00	X 0.575 FT	15.15	193.00	45.45			687.00	
12,750	0.00	X 0.575 FT	19.77	252.00	50.31			992.31	

TOTAL PRICE & TIME MEMBERS = 241131.0

TOTAL PRICE = 241131.0

LIST OF MATERIALS SUMMARY
 ACQU 300116 STEEL PIPE MATERIAL LISTING - 100011 - U.S. AIR FORCE, 1965

UNITAL QUANTITY TOTAL HEIGHT (FEET)

PIPE	UNITAL QUANTITY	TOTAL HEIGHT (FEET)	WEIGHT (LBS)
42,000 0.0	X 1.500 AT	63.00	115,500
41,000 0.0	X 1.000 AT	102.00	186,000
39,000 0.0	X 0.500 AT	146.50	263,700
29,000 0.0	X 0.750 AT	21.00	380,000
20,000 0.0	X 1.000 AT	41.00	738,000
20,000 0.0	X 0.625 AT	193.00	351,000
14,000 0.0	X 0.500 AT	209.00	380,000
14,000 0.0	X 0.500 AT	330.00	594,000
10,000 0.0	X 1.375 AT	160.00	290,000
12,750 0.0	X 0.500 AT	164.00	297,000
12,750 0.0	X 0.575 AT	59.50	108,000

TOTAL HEIGHT 25110.00 LBS

NO	X	Y	Z	DEPTH	STATUS	DESCRIPTION
1	500.000	100.000	100.000	0.00	0	SURF--STR--CIRCF--LEGS
2	12.750	20.000	30.000	0.00	3	SURF--STR--CIRCF--BRAC
3	12.750	30.000	40.000	0.00	3	SURF--STR--CIRCF--BRAC
4	12.750	40.000	50.000	0.00	3	SURF--STR--CIRCF--BRAC
5	12.750	50.000	60.000	0.00	3	SURF--STR--CIRCF--BRAC
6	18.000	20.000	20.000	0.00	3	SURF--STR--CIRCF--BRAC
7	40.000	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
8	20.000	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
9	27.000	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
10	15.500	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
11	25.000	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
12	25.000	20.000	20.000	0.00	3	FLAT--DECK--T--DECK
13	5.750	0.000	0.000	0.00	57	TIP--DECK
14	0.000	0.000	0.000	0.00	57	TIP--DECK
15	5.750	0.000	0.000	0.00	57	TIP--DECK
16	0.000	0.000	0.000	0.00	57	TIP--DECK
17	5.750	0.000	0.000	0.00	57	TIP--DECK
18	0.000	0.000	0.000	0.00	57	TIP--DECK
19	5.750	0.000	0.000	0.00	57	TIP--DECK
20	0.000	0.000	0.000	0.00	57	TIP--DECK
21	5.750	0.000	0.000	0.00	57	TIP--DECK
22	0.000	0.000	0.000	0.00	57	TIP--DECK
23	5.750	0.000	0.000	0.00	57	TIP--DECK
24	0.000	0.000	0.000	0.00	57	TIP--DECK
25	5.750	0.000	0.000	0.00	57	TIP--DECK
26	0.000	0.000	0.000	0.00	57	TIP--DECK
27	5.750	0.000	0.000	0.00	57	TIP--DECK
28	0.000	0.000	0.000	0.00	57	TIP--DECK
29	5.750	0.000	0.000	0.00	57	TIP--DECK
30	0.000	0.000	0.000	0.00	57	TIP--DECK
31	5.750	0.000	0.000	0.00	57	TIP--DECK
32	0.000	0.000	0.000	0.00	57	TIP--DECK
33	5.750	0.000	0.000	0.00	57	TIP--DECK
34	0.000	0.000	0.000	0.00	57	TIP--DECK
35	5.750	0.000	0.000	0.00	57	TIP--DECK
36	0.000	0.000	0.000	0.00	57	TIP--DECK
37	5.750	0.000	0.000	0.00	57	TIP--DECK
38	0.000	0.000	0.000	0.00	57	TIP--DECK
39	5.750	0.000	0.000	0.00	57	TIP--DECK
40	0.000	0.000	0.000	0.00	57	TIP--DECK
41	5.750	0.000	0.000	0.00	57	TIP--DECK
42	0.000	0.000	0.000	0.00	57	TIP--DECK
43	5.750	0.000	0.000	0.00	57	TIP--DECK
44	0.000	0.000	0.000	0.00	57	TIP--DECK
45	5.750	0.000	0.000	0.00	57	TIP--DECK
46	0.000	0.000	0.000	0.00	57	TIP--DECK
47	5.750	0.000	0.000	0.00	57	TIP--DECK
48	0.000	0.000	0.000	0.00	57	TIP--DECK
49	5.750	0.000	0.000	0.00	57	TIP--DECK
50	0.000	0.000	0.000	0.00	57	TIP--DECK
51	5.750	0.000	0.000	0.00	57	TIP--DECK
52	0.000	0.000	0.000	0.00	57	TIP--DECK
53	5.750	0.000	0.000	0.00	57	TIP--DECK
54	0.000	0.000	0.000	0.00	57	TIP--DECK
55	5.750	0.000	0.000	0.00	57	TIP--DECK
56	0.000	0.000	0.000	0.00	57	TIP--DECK

ACQU 3-011F STRUCTURE MATERIAL LISTING -- SCHEDULE 40S -- U.S. NAVY--F. FORM

PIPE

QTY	DESCRIPTION	QTY	WEIGHT (LB)	TOTAL WEIGHT (LB)	TOTAL PRICE (\$)
36,000	0.00 X 1.250 FT	3	57.00	171.00	79000.2
12,750	0.00 X 1.500 FT	3	50.25	150.75	6013.5
12,750	0.00 X 1.500 FT	3	20.00	60.00	5046.5
12,750	0.00 X 1.575 FT	2	18.00	36.00	1745.0
16,625	0.00 X 1.250 FT	2	9.00	18.00	301.0

TOTAL WEIGHT OF PIPE MEMBERS = 93601.8

ACME TRIPLE STRIKE OF MATERIAL LISTING -- SUBJECT CODE: 15. 40X-C. CUPR

SHAPE

NO.	SHAPE	UNIT PRICE	QUANTITY	WEIGHT (LBS)	LENGTH (FT)	TOTAL WEIGHT (POUNDS)
1	18 X 53.00	55.00	10	100.00	705.00	
2	18 X 53.00	25.00	15	147.00	4350.00	
3	12 X 27.00	55.00	10	132.00	4700.00	
4	18 X 24.00	25.00	10	50.00	1200.00	
5	18 X 20.00	20.00	10	200.00	4000.00	
6	6 X 15.50	20.00	2	50.00	400.00	

TOTAL WEIGHT OF AVAILABLE MEMBERS 22029.00

ACME TABLE STRUCTURE SPECIAL LISTING -- SUPERSEDES ALL PREVIOUS ORDERS

PLATE

ORIGINAL DIMENSIONS (FT X FT X TH)	QUANTITY	TOTAL AREA (SQ. FT.)	TOTAL WEIGHT (POUNDS)
3.42 X 6.85 X 1.00	12	23.16	170.4
3.33 X 5.75 X 1.375	57	19.14	1656.2
35.00 X 35.00 X 1.250	1	1225.00	12500.2
20.00 X 25.00 X 1.25	1	500.00	5100.2
		TOTAL WEIGHT OF PLATES =	19956.8

ALUMINUM TUBING MATERIAL LISTING -- 5 PERCENT OF U.S. ALUMINUM

CHANNELS

NOMINAL DIMENSIONS	QUANTITY	WEIGHT (LBS)	LENGTH (FT)	TOTAL WEIGHT (POUNDS)
C 12 X 25.00	4	35.00	140.00	3500.00
F 12 X 25.00	3	35.00	12.00	307.50

TOTAL WEIGHT OF CHANNELS = 3807.50

TOTAL WEIGHT = 3807.50

UNIT OF MATERIALS QUANTITY
 APPROXIMATE SIZE GROUP MATERIAL LISTING -- SUBJECT: (T. 01) 301 AVENUE (CHER)

QUANTITY (LBS) T. 01 (LBS) T. 01 (LBS)

PIPE

36.000 6.0" X 1.250 AT	171.00	19104.10
12.750 6.0" X 0.500 AT	184.05	12100.97
12.750 6.0" X 0.375 AT	36.00	1785.32
6.625 6.0" X 0.250 AT	18.00	301.26

* SHAPE

W 18 X 57.00	227.00	11350.00
W 12 X 27.00	100.00	3780.00
C 8 X 24.00	250.00	6000.00
C 6 X 15.50	59.00	1000.00

CHANNELS

C 12 X 25.00	152.00	3400.00
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WILLIAMS MATERIALS COMPANY
ACQUA SERVICE SUPPLY MATERIAL LISTING - SUBSIDIARY OF WILLIAMS COMPANY

PLATE

1.000 THICKNESS	4.18	17,041
0.575 THICKNESS	104.14	1,456.10
0.250 THICKNESS	1725.10	17,600.87

TOTAL WEIGHT 18347.14 LBS

ASP JOB NO. = 0221

DATE = 76.124

//LFC0016 JOB (00442705002777100000) (FC0016) (FC0016) (LFC0016) (LFC0016) (LFC0016) (LFC0016)

PLEASE TYPE THE MESSAGE = 000,42. START TIME = 17.18.00

LOGOFF = SYSMSG
MESSAGE = STOPJOB
LINES OUTPUT FOR THIS JOB = 000055
PRINTED ON 00027921, LINES = 000077

CLASS FROM WAIT FOR THIS JOB IS FULL

END

FILMED

4-86

DTIC