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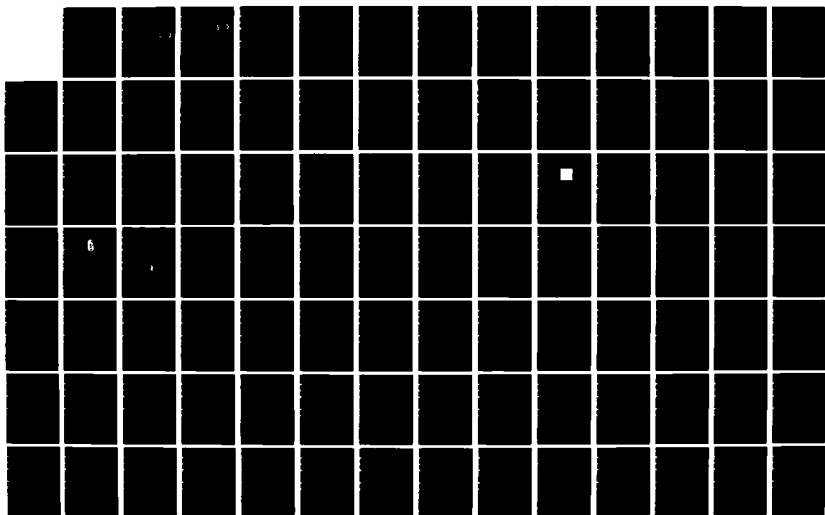
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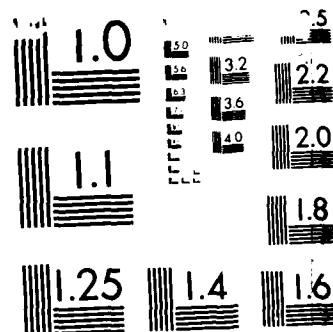
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FOR A MOBILE AUTONOMOUS ROBOT

THESIS

Roland J. Bloom  
Captain, USAF

William J. Ramey, Jr.  
Captain, USAF

AFIT/GA/GE/ENG/85D-33

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FOR A MOBILE AUTONOMOUS ROBOT

THESIS

Presented to the Faculty of the School of Engineering  
of the Air Force Institute of Technology

Air University

In Partial Fulfillment of the  
Requirements for the Degree of  
Master of Science in Astronautical Engineering  
and Electrical Engineering, Respectively

Roland J. Bloom, B.S.A.E  
Captain, USAF

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December 1985

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## Preface

It is only a matter of time until the autonomous mobile robot becomes a reality. The key to achieving this goal lies in the development of a navigation system capable of accurate position determination and intelligent, efficient, collision-free, path planning through the robot's environment. Hopefully, our efforts have provided some advancement toward creating such a robot navigation system.

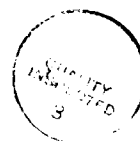
The success of this thesis was a direct result of the endless support provided by several individuals and organizations. A special thanks goes to our thesis advisor Dr. Matthew Kabrisky for having the confidence to turn us loose on this project. Additionally, we would like to thank our sponsor, Tim Anderson of AFMRL; Robert Durham, Orville Wright, Dick Wager, and Stan Bashore of AFIT/ENG; Carl Short and Ron Ruley of AFIT/RMF; Mrs. Allis Moore of AFWAL; Allen Cooper, Berny Swagert, and George Kelsh of King Radio Corporation; Diane White, Ed Freedman, and Cal Watson of Analog Devices Incorporated; Bill Lee and Roger Heilman of Sundstrand Data Control Incorporated; and a generous thanks to King Radio Corporation for their donation of equipment to the project.

We would also like to express our appreciation to Tom Clifford and Bert Schneider for creating the MARRS-1 robot and putting together the robot laboratory. Their efforts made our endeavor possible. In addition, we owe Tom

Clifford a special thanks for his assistance and advice throughout the project.

We would also like to extend our gratitude to Lt. Col. Dan Biezad for his tireless assistance from the very beginning. To him we credit the aquisition of our directional gyro system.

Most of all we wish to acknowledge the many sacrifices made by our wives and children. Without their patience, love, and understanding we could not have completed this thesis.



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## Abstract

A navigation system for a mobile autonomous robot is presented. The navigation system is based upon a directional gyroscope and a single axis accelerometer which enables a robot to navigate independent of wheel optical shaft encoders and other commonly used positioning apparatus. The computer controlled navigation system is capable of providing absolute heading, heading rate (angular velocity), and linear velocity to a user computer. These data from the navigation system (heading and velocity) are used to compute the present location of the robot. In addition, the heading data is used to form a closed loop feedback control system for maintaining the robot on a desired course. The navigation system was designed specifically for application on an existing Air Force Institute of Technology (AFIT) robot; however, it could be easily adapted to any robot system with a standard IEEE RS-232 serial communication interface. Test results are provided which demonstrate the use of closed loop heading control on the AFIT robot and which identify problems associated with the use of an accelerometer system for distance measurement. This thesis includes all schematics, parts lists, software listings, and operating instructions for the navigation system. A new robot world modeling and path planning technique is also presented.

# GYRO AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A MOBILE AUTONOMOUS ROBOT

## I. Introduction

### BACKGROUND

In general, robots fall into three broad categories: fixed arm robots, mobile robots, and mobile autonomous robots. It is important to understand how these three classes of robots differ.

A fixed arm robot is a machine modeled after the human arm and hand. It is capable of armlike movement and has a handlike manipulator, but by itself is incapable of movement from one location to another. Fixed arm robots are by far the largest category of present day robots, encompassing virtually all of the currently available robots. They are used primarily for repetitive manipulative tasks such as industrial assembly line work. Because these robots do not in general possess the ability to move themselves about their environment, they will not be discussed further.

A mobile robot is "a robot mounted on a moveable platform" [11:17]. They are distinguished by their ability to move freely about their environment, but with command and control provided external to the robot. Underwater salvage robots provide an excellent example of mobile robotics. They can move freely about their environment, but are

controlled from a surface vessel by a team of human operators. Since mobile robots are not self controlled, they too will not be discussed further.

A mobile autonomous robot is "a robot acting independently and of its own volition" [11:17]. They are distinguished by their ability to move freely about their environment completely under internal control independent of external machine or human assistance. Mobile autonomous robots have many potential applications, but currently they do not exist outside of research labs. Expansion of this concept is the basis of this thesis.

In recent years, there has been a substantial increase of interest in mobile autonomous robots. A report regarding the First World Conference on Robotics Research, held in early 1985, noted that one of the most actively researched fields was mobile autonomous robots [11:17]. This surge of interest is a direct result of the "microelectronics revolution" which has resulted in today's microprocessors and digital integrated circuits (IC's). Tremendous computational power is now available in very small packages making the internal control required for a mobile autonomous robot feasible.

The potential to develop a mobile autonomous robot has generated many possible applications. Chief among these is the performance of tasks hazardous to human personnel such as fire fighting, bomb disposal, nuclear waste disposal,

underwater salvage and repair, deep sea exploration, chemical production, mining, sentry duty, and military reconaissance and attack missions.

This effort is being led by the Department of Defense (DOD). The Defense Advanced Research Projects Agency (DARPA) currently has a 17 million dollar contract with Martin Marrietta Corporation to develop an autonomous land vehicle [21] and has asked General Dynamics and others for proposals on battlefield robots [13:48]. DARPA is also funding multi-legged mobile robotics research at Ohio State University [13:48].

The Army's General Officer Steering Committee for Artificial Intelligence and Robotics recently issued a report outlining near-term (1980's) robotic systems applications [14]. They include: a light weight robotic vehicle to mount antitank guided missiles, mortars, and small arms; a robotic obstacle/mine breaching tank; a robotic transport and resupply vehicle; a security sentry robot; an explosive ordnance disposal robot; and a robot scout vehicle.

The Air Force Medical Research Laboratory at Wright-Patterson Air Force Base (WPAFB) is currently working on the development of a mobile autonomous robot to service aircraft in a nuclear, biological, or chemical (NBC) contaminated environment. This thesis is an extension of that effort.

All of the above applications require the robot to be

able to perform three primary functions: computation, manipulation, and navigation.

Computation is the robot's ability to make job application related control decisions. For example, an aircraft servicing robot would have to decide which subsystems to test and then which part to replace. In the field of artificial intelligence, this would be called an expert system. Since numerous expert systems of the type required for robotics have already been developed, this function will not be discussed further.

Manipulation is the robot's ability to skillfully handle and move objects in its environment. This function has been well developed and is commercially available in the form of a fixed arm robot. Therefore this function also will not be discussed further.

Navigation is the robot's ability to direct itself toward some destination. This problem has yet to be adequately addressed and is the major impediment to the development of a mobile autonomous robot. Robot navigation is the focus of this thesis.

Navigation requires that the robot be able to follow a given or calculated course of travel making course corrections as necessary. This means the robot must be capable of finding its current location in reference to the desired course. This information is required for steering control feedback in order to accurately follow a given

course.

In addition, the robot must know its starting location and final destination on the same frame of reference as its current location. This will give it the ability to know when it has arrived at the desired location.

Finally, a navigation system must provide a means for recognizing obstacles, both known and unknown. It must allow for course changes to avoid these obstacles and yet still arrive at the destination in a time efficient manner. A robot must be able to deal with a dynamic environment.

Physically, the navigation system is composed of sensors and steering control. The sensor subsystems collect position and obstacle data. the steering control subsystem uses the position and obstacle data to make any necessary course changes. All but the most simple steering control subsystems require many intelligent decisions to be made and therefore require a computer as the controller.

Past research work on mobile robot and mobile autonomous robot navigation has produced vision, embedded wire, beacon, shaft encoder, and sonar based navigation systems, where the environmental data from each system's sensors is interpreted by a computer to control the path of travel.

Vision navigation systems use television cameras to "see" the desired path and obstacles much like a human. Vision systems today are relatively crude in spite of modern

advances in high speed computer systems. They are not capable of interpreting the digital video information fast enough to allow real time navigation.

Dr. Hans Moravec has done considerable research in the area of robotic vision. During his Ph.D. work at Stanford University, he experimented with the "Stanford cart", a mobile robot which he equipped with a video camera [17]. The cart's ultimate achievement was travelling through an obstacle laden area to a goal about 60 feet away. The trip took a total of about five hours. In addition, the cart did no onboard processing of the video images. They were transmitted by radio link to a VAX 780 computer which interpreted the data and issued the resulting steering commands. This reduces the robot to the mobile category as opposed to the mobile autonomous classification.

Dr. Moravec, now a professor at Carnegie Mellon University, is still diligently pursuing his research into creating human like vision for a mobile robot. However, he admits that to reach his goal he needs a computer which is about 1000 times faster than his current computer [9:30]. Present vision systems are not fast enough to allow real time navigation and the computers are not small enough to be built on board the robot for a mobile autonomous system.

Embedded wire systems find the desired path by following wires on or beneath the travel surface like a train on railroad tracks. This system is very simple,



requires little computational ability, and navigation can be done in real time. However, it is not very flexible. Places of travel are limited to where the wire tracks are located and continuity of the wire from start to destination. Obstacle avoidance is impossible without additional sensors and even then would be limited to stopping and waiting for the obstacle to move.

Beacon systems determine the desired path from position reference information broadcast by beacons found near the path of travel. This system is also simple, easy to implement, and provides a real time navigation capability. It suffers from the need to provide beacons in the robots working environment for navigation. Additional sensors are required to provide an obstacle avoidance capability.

Optical shaft encoder systems rely on "dead reckoning" navigation by starting at a known position and moving precise distances as measured by the optical shaft encoder. This is also a relatively simple system, easy to implement, and can be done in real time. It is more flexible than the embedded wire system because it is not limited to following wire tracks, but it suffers from errors in sensor data. The distance moved data must be very accurate or error will be introduced that is cumulative and will eventually result in the robot becoming lost.

Optical shaft encoders have proven to be fairly accurate under ideal conditions. However, several sources

of position error accompany their use. These position errors are unbounded and cumulative. One error source is wheel slippage, resulting in an inaccurate measurement of actual distance traveled.

A second problem lies in knowing the exact circumference of the wheel. The distance traveled by the robot is determined from the number of revolutions made by the wheel; one revolution of wheel travel equals the distance of one circumference in linear travel. As the tire wears out, the error in the measured distance grows larger.

A third problem results from computational errors. This error is most prominent when the robot has negotiated many turns, requiring numerous calculations based on geometric approximations to determine the current location of the robot. After a short period of travel, the robot will begin to stray off course due to an accumulation of error. The performance of optical shaft encoders degrades considerably as the number of maneuvers performed by the robot increases.

A fourth problem with optical shaft encoders results from not having an absolute heading reference. All heading computations from encoder data produce a relative heading to some initial heading. Initial heading of the robot must be externally provided and can itself be a very large error source. In Figure 1.1, the effect of initial heading error is illustrated. Without an accurate initial heading, the robot will eventually become lost. A robot system using

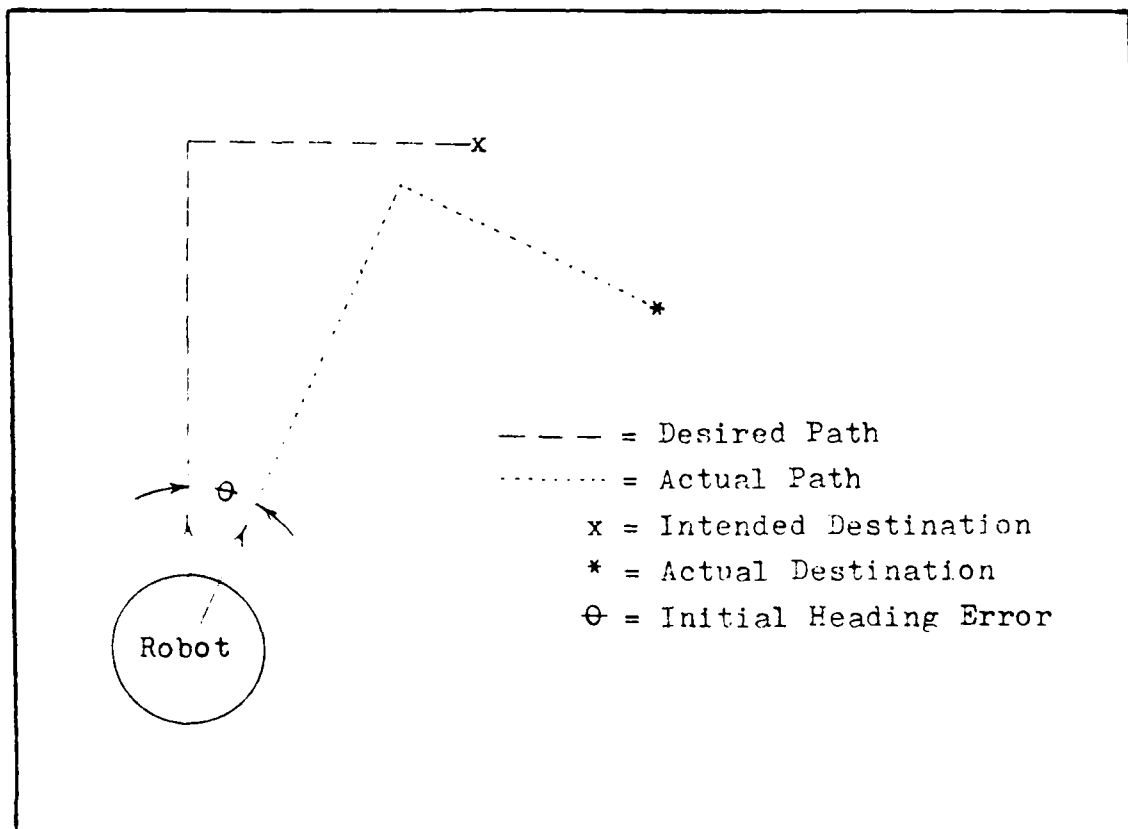


Figure 1.1. Effect of initial heading error.

optical shaft encoders for navigation is highly dependent on this initial heading reference.

Finally, optical shaft encoders offer no means for detecting obstacles. Therefore, additional sensors are required to provide an obstacle avoidance capability. Sonars (ultrasonic ranging units) can be used to complement the optical shaft encoders and together provide position and obstacle detection information. In addition, the sonars can be used to compensate for errors in the encoders by providing range information to known obstructions. In other

words, the sonars can provide a position "fix" so the robot knows its location with respect to its known environment.

Dr. James Crowley [12] is experimenting with just such a system. He uses a focused rotating ultrasonic ranging device to maintain a description of the robots external environment. This description is called a sensor model. The estimated position of the robot, obtained from optical shaft encoders, is compared to the position of the robot determined from the sensor model to create a composite model. This composite model represents an average position of the robot. In this way, Crowley seeks to maintain an accurate estimate of the robots position.

It is not very feasible to use sonars as the only source of navigation data since their range is limited (making navigation through a large open area impossible) and unknown obstacles could be misinterpreted as known obstacles causing the robot to become lost. It is also important to note that sonar data is useless for navigation without an accurate heading reference. A detected object cannot be used as a reference without knowing the direction of the object in the navigation reference frame.

Previous thesis work at the Air Force Institute of Technology (AFIT) has produced a mobile robot, the Mobile Autonomous Robot Research System-1 (MARRS-1), that can map its environment and provide obstacle detection with sonar sensors. It can also measure distance travelled with

optical shaft encoders. In addition, the robot has an onboard computer for dedicated navigation calculations. However, MARRS-1 is not capable of autonomous navigation. The current navigation system can only traverse a course preprogrammed into the drive computer through the robot's keyboard or by use of the teaching pendant. It can only collect, not use for navigation, sonar obstacle information and shaft encoder distance data (as presently programmed). In addition, it is not able to compensate for errors in wheel direction and distance measurements, which may cause MARRS-1 to wander from the programmed course (open loop steering control).

It is obvious that past robot navigation research, both at AFIT and abroad, has not produced an accurate, real time, autonomous, mobile navigation system. A new approach is indicated by the weaknesses and liabilities of past systems. First, an absolute and directly measurable robot heading reference is required. Second, an accurate and preferably non-mechanical method of distance measurement is necessary. Third, an accurate, long distance (5 to 50 feet or more) method of obstacle detection is required. Finally, a navigation algorithm is required that models the sensor data into a real world map and issues robot steering commands based on this mapping.

This thesis attempts to solve these problems by adapting an aircraft directional gyroscope system for the

heading reference, an accelerometer for distance measurement, and sonars for obstacle detection. Robot "world modeling" and path planning is discussed, but not implemented.

#### PROBLEM AND SCOPE

The problem is to design and fabricate a real time, point to point, closed loop, mobile autonomous robot navigation system for the MARRS-1 robot. In addition, it must be capable of detecting and avoiding both previously known and unknown obstacles.

Real time navigation is defined to be navigation at the maximum constant motion travel speed of MARRS-1. Point to point refers to navigation from a given starting point to a given destination and includes in-course obstacle detection and avoidance. Closed loop refers to the ability to detect and correct course errors. Autonomous, in this case, will be broadened to mean needing no external support except power.

Design and fabrication will include: construction of a new third body tier to house the gyro and accelerometer based navigation system (GYRAC); physical and electrical modification of MARRS-1 to allow GYRAC integration; fabrication of a GYRAC control computer; implementation of GYRAC computer software; fabrication of a digital electronic interface between the gyro/accelerometer and GYRAC computer;

integration of the MARRS-1 drive and navigation computers with the GYRAC computer; a simple point to point navigation control program (no obstacle avoidance) to demonstrate course tracking; full testing of all new hardware and compilation of test results; complete schematic diagrams and operating manuals for all new hardware; and fully documented software listings for all operational and test programs.

Obstacle detection and avoidance were not implemented, but are available since this has been demonstrated on a previous thesis [19]. Finally, the design options available were limited by hardware and software restrictions imposed by systems previously added to MARRS-1, limited space internal to the robot, limited time, and insufficient funds.

### Assumptions

Several basic assumptions are necessary for a navigation system based on a directional gyroscope and an accelerometer. This thesis is predicated on the following assumptions:

1. Assume no local disturbances will be present in the earth's magnetic field. This assumption is necessary since the directional gyro output is slaved to a magnetic flux detector for absolute reference to magnetic north.
2. Assume the operational environment of the robot is a perfectly smooth and level surface. This assumption is necessary since a single accelerometer cannot distinguish true acceleration from local gravity. Therefore, any tilt of the accelerometer input axis into the vertical plane will induce an error in measured acceleration.

3. Assume a perfect integrator. An operational amplifier integrator circuit is used to integrate accelerometer output to obtain velocity.
4. Assume velocity of the robot is constant over sample period. This is necessary for simplicity and ease of calculation.
5. Assume sample time is known precisely. Using accelerometer output to ultimately obtain distance traveled by the robot is a time dependent problem.

All the above assumptions, excluding the first, are tied directly to the use of an accelerometer. Each of these assumptions will be addressed again in Chapter V.

#### Evolution and Capability of MARRS-1

The MARRS-1 began as a Heathkit HERO-1 robot. This original HERO-1 has since undergone substantial modification and today bears little resemblance to its former self. Lieutenant Owen [19] was the first to modify the original HERO-1. He added a laser barcode scanner and several Polaroid ultrasonic ranging units to the robot. The scanner was used to determine the location of the robot by reading barcodes taped to the floor. The first step had been taken toward creating an autonomous mobile robot. The HERO-1 could collect useful but limited navigation data on its own.

Follow-on work by Clifford and Schneider [10] was a major leap toward the goal of creating a mobile autonomous robot. Under their thesis effort, the HERO-1 was completely rebuilt. The following is a list of the major modifications performed by Clifford and Schneider:

1. A new main body was fabricated. This new body is 12



sided and consists of two separate levels. The top level can rotate with respect to the lower level.

2. The HERO-1 CPU (MC6808) was upgraded with the addition of a Virtual Devices Inc. MENOS-1 MC6801 CPU board which added RS-232 serial communication capability to the HERO-1.
3. Two dozen Polaroid sonar transducers were attached to the new robot body (one on each segment of the upper and lower body decks).
4. Optical shaft encoders were placed on the two rear wheel shafts and on the front (drive) wheel steering shaft to provide distance moved data.
5. An MC6802 based computer was added to control the optical shaft encoder subsystem and the sonar subsystem. This computer is called the Navigation computer.

The resulting heavily modified HERO-1 was renamed MARRS-1. MARRS-1 was then used to generate sonar range data and wheel distance data. This data was post processed on an external computer to create a composite map of the robot's local environment relative to the robot (whose position was determined from the shaft encoder data). This represents a significant improvement over the capability of the Owen modified HERO-1. However, like Owen's modified HERO-1, the MARRS-1 served only as a collector of navigation data. The actual movement of the robot was controlled by a human operator. MARRS-1 was not yet an autonomous robot, but it possessed the capability to become one.

The capability of the MARRS-1 at the beginning of this thesis can be summarized as follows:

1. All functions of the original HERO-1 still existed, except for the arm [10:III-3]. This capability included programable movement of the robot.

Unfortunately, this programed motion was open loop, resulting in unreliable and nonrepeatable movement. The robot could not follow a straight line path.

2. The laser barcode scanner was removed but all provisions for attaching it (both mechanically and electrically) to the robot still existed.
3. Sonar and optical shaft encoder data could be gathered by the navigation computer and relayed via an RS-232 computer interface to an external computer for storage on a floppy disk. Firmware was resident onboard the Navigation computer to obtain and transmit the data.
4. Four RS-232 computer interface ports were available for use. One port allowed communication with the main CPU (MENOS-1 upgrade board). The other three ports allowed access to the navigation computer.

#### General Approach

Development of a mobile autonomous robot navigation system for the MARRS-1 required a rigorous analysis of past and present robot navigation research literature. Based on this literature search, a new approach to world modeling for mobile autonomous robots was developed.

This new navigation approach required collection of specific types of data. The current systems and sensors on the MARRS-1 were compared against these new requirements and a list of sensors and systems to be constructed were compiled. A prime requisite during this analysis was to limit the data collected so that onboard computers could process the data fast enough to allow real time navigation.

The required sensors and subsystems were built and tested as was the necessary software to drive each subsystem. Modifications were then made to the MARRS-1

system to allow the GYRAC subsystem to be physically, electrically, and functionally (through software) integrated onto the MARRS-1 platform. Navigation system testing was performed and supporting data collected to validate the new navigation system.

Finally, MARRS-1 system software was developed, tested, and support data collected to demonstrate the feasibility of gyro based steering control. Conclusions and recommendations are provided based on testing at each of the various stages.

#### Sequence of Presentation

Chapter One provides a detailed problem background, problem statement and scope, assumptions, evolution of MARRS-1, general approach, and sequence of presentation. Chapter Two covers the GYRAC system design and theory of operation. Chapter Three discusses GYRAC system integration onto the MARRS-1 platform. Chapter Four presents a new mobile autonomous robot navigation theory for world modelling and path planning. Chapter Five discusses testing results and analysis of the various stages of the GYRAC development. Chapter Six gives a system summary and presents conclusions and recommendation. The appendices contain hardware data sheets, schematic diagrams, device layouts, wiring diagrams, connector diagrams, an equipment list, and a parts list. Included are software structure

charts, program listings, collected data tables, and software operating instructions.

## II. GYRAC Design and Theory of Operation

The hardware design goal of this thesis is to create a navigation data system capable of providing absolute heading and velocity data, in binary digital form, to an external computer. Three primary requirements are the basis for this design:

1. A KCS-55A Pictorial Navigation System (produced by King Radio Corp.) was ordered after selection as the best directional gyro system for this project and a QA-1100 accelerometer (produced by Sundstrand Data Control Inc.) was already on hand at AFIT. Therefore, the system must be centered around the KCS-55A Pictorial Navigation System and the QA-1100 accelerometer.
2. The navigation data system must be compatible with the MARRS-1 but also easily transportable to another robot system.
3. The system must be attainable with resources readily available to AFIT.

Since the foundation of the system is a gyro and an accelerometer, the navigation data system will hereafter be referred to as the "GYRAC" system (for gyro and accelerometer system).

### Summary of GYRAC System

A general layout of the GYRAC system can be seen in the block diagram in Figure 2.1. The gyro subsystem provides analog heading information which is then converted to a 12 bit TTL (Transistor Transistor Logic) digital data signal. Angular velocity is a byproduct of this conversion in analog signal form. Thus, the analog angular velocity is digitized

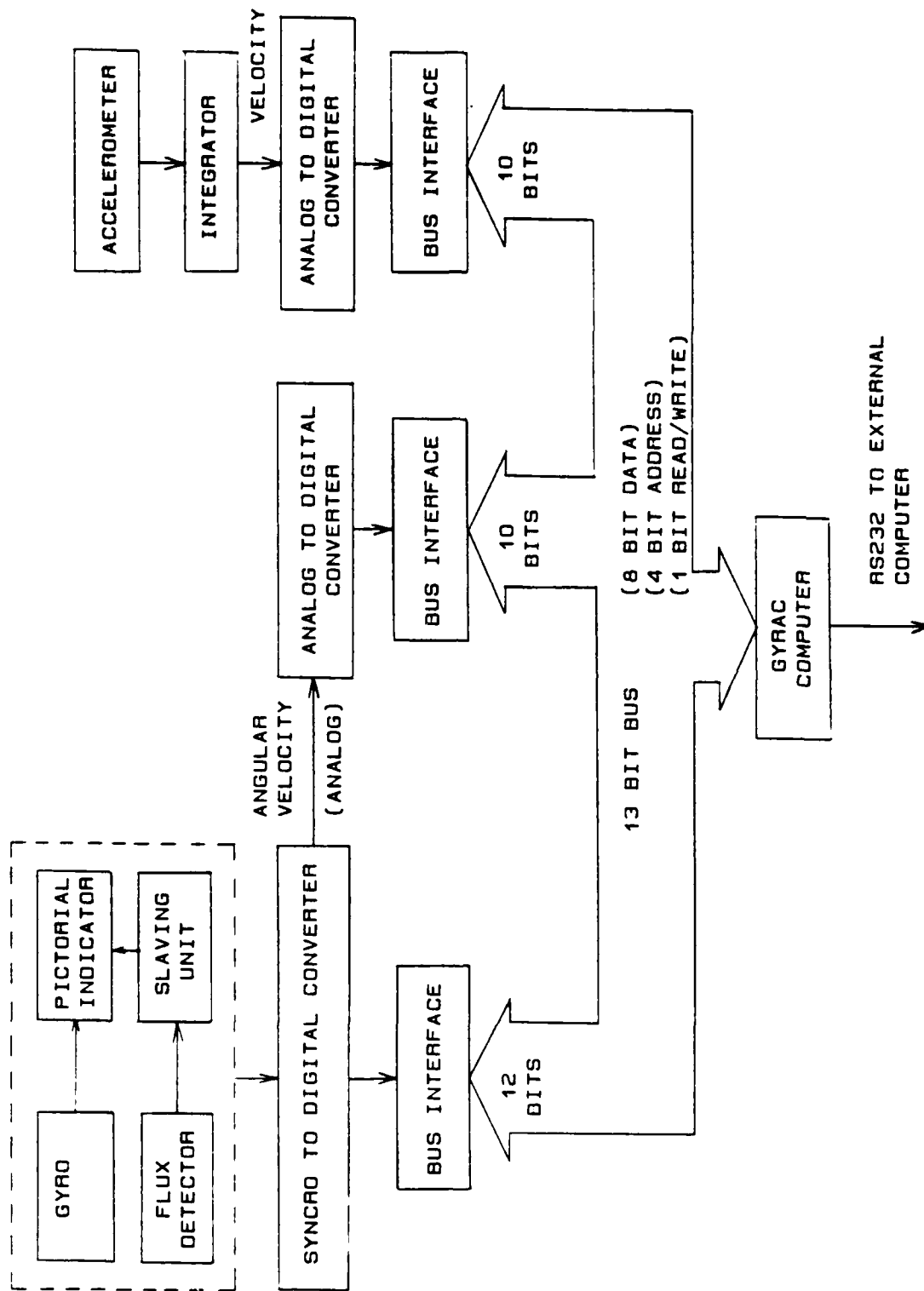


Figure 2.1. GYRAC System Block Diagram

through an analog-to-digital converter resulting in a 10 bit digital data signal. The accelerometer produces an analog signal which is integrated via an operational amplifier circuit and converted to digital TTL data by an analog-to-digital converter. The three digital data signals are connected to a common thirteen wire bus containing eight data lines, four address lines, and a read/write line. This bus serves as a standard sensor interface to the GYRAC computer. The GYRAC computer interprets commands received from an external computer via an RS-232 serial data link and acquires the appropriate sensor data as directed by the external command. The GYRAC computer then performs any necessary preprocessing of the data, converts it to serial format, and transmits it to the external computer via the RS232 link.

#### The Gyro Subsystem.

The gyro subsystem is composed of four major elements: a directional gyro; an indicator unit; a magnetic flux detector; and a slaving unit. The directional gyro provides a gyro stabilized magnetic heading to the indicator. The directional gyro consists of two primary components: the gyro itself and a base assembly, see Figure 2.2.

The gyro is a spinning mass precision gyro with two degrees of freedom, see Figure 2.3. Relative angular displacement is sensed by an optical encoder assembly mounted on the gyro's outer gimbal. Electrical outputs from

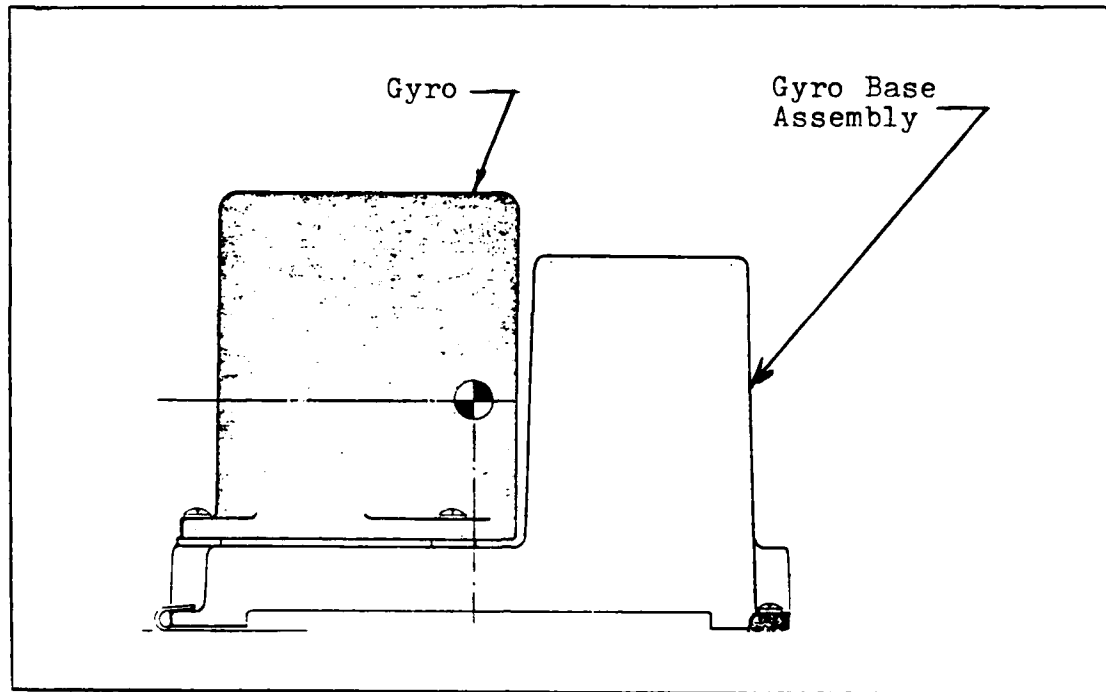


Figure 2.2. Directional Gyro [1:2-11]

the optical encoder are two square waves which are used to drive a stepper motor in the indicator. The gyro base assembly contains the control logic for the gyro and the slaving logic for the indicator. The gyro base also serves as the power supply for the entire gyro subsystem. From the single 28 volts DC input into the gyro base, the following internal voltage supplies are generated: 26 VAC 400 Hz for the gyro spin motor, flux detector excitation, and heading synchro excitation; + and - 15 VDC regulated supply for the analog circuitry in the system; +15 VDC unregulated voltage for the stepper motor in the indicator; and +5 VDC regulated supply for the system digital logic circuitry [3:5-33].



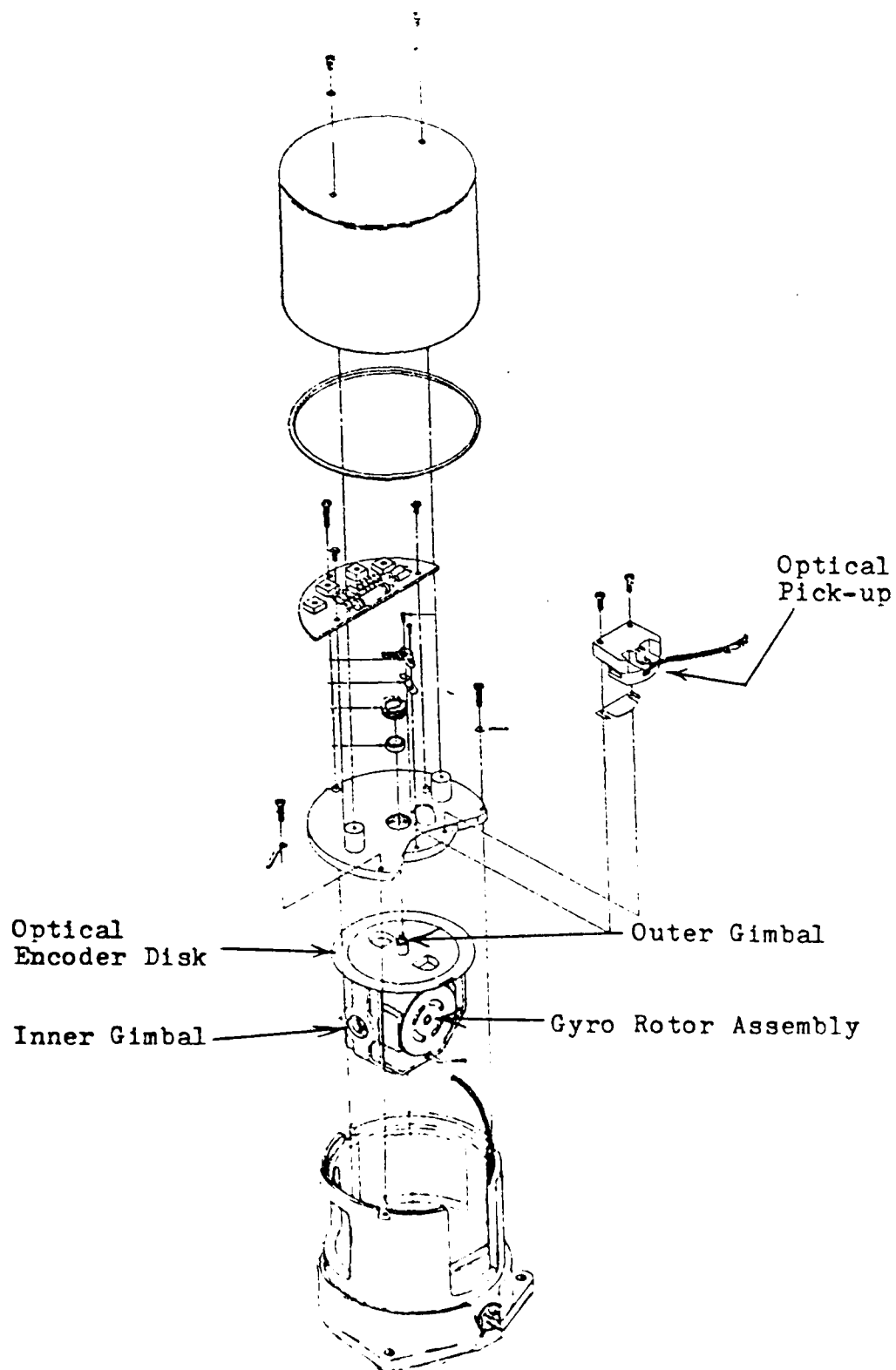


Figure 2.3. Gyro, Exploded View [2:5-33].

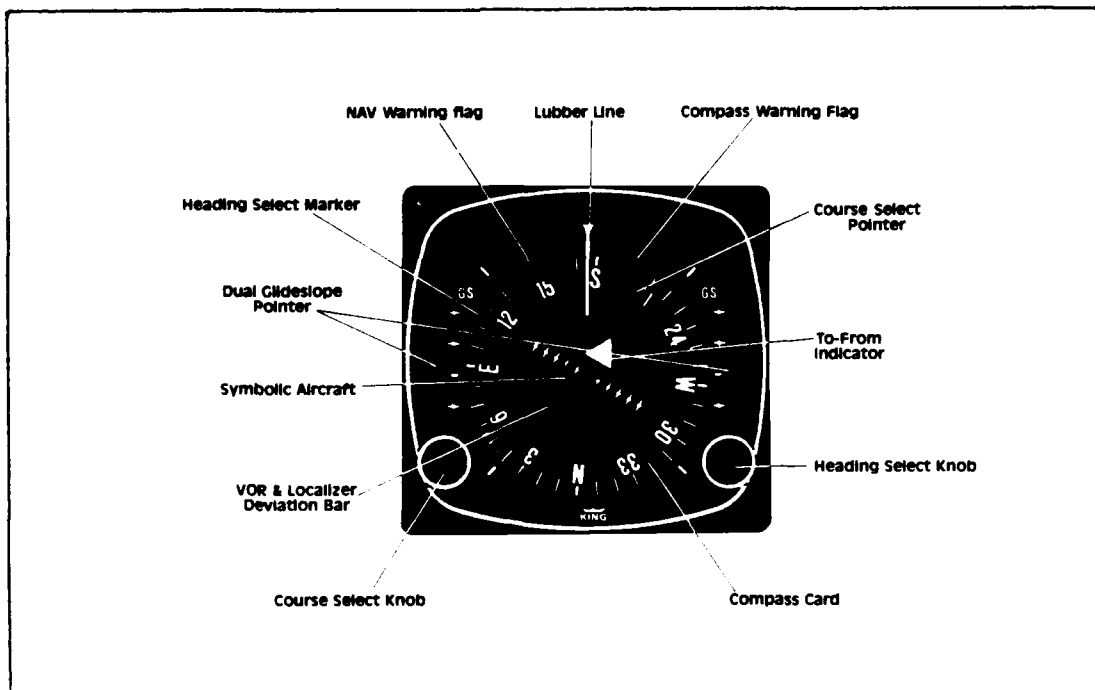


Figure 2.4. The Heading Indicator [1:2-9]

Also, separate regulated grounds are maintained for the analog and digital circuitry. For the GYRAC system, the above mentioned supplies and grounds are routed to a central power distribution panel to provide the necessary power for other GYRAC hardware (see Appendix E).

The indicator is typical of the type seen in the cockpit of small aircraft, as shown in Figure 2.4. A digital stepper motor is used to drive the heading display in response to the signals generated in the directional gyro. The signals from the gyro consist of a two phase excitation drive that is connected to the four stepper motor leads as shown in Figure 2.5. Each time the A or B waveforms (see

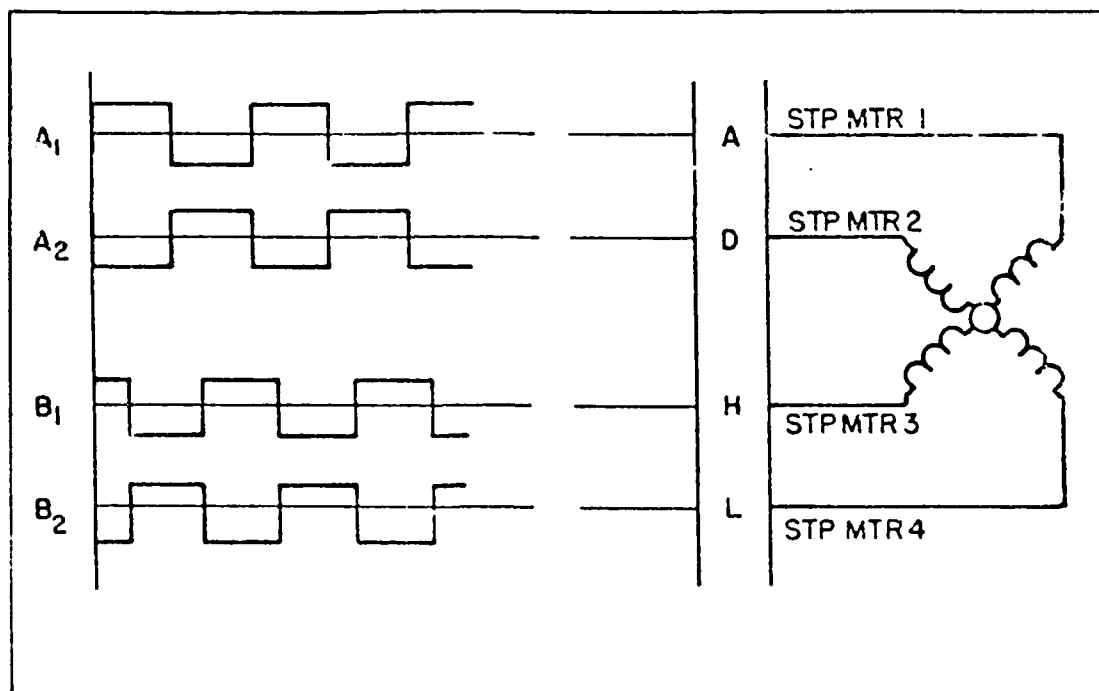


Figure 2.5. Stepper Motor Drive Circuit [2:4-1]

Figure 2.5) change state, the motor shaft moves nine degrees in a direction determined by the previous state of the waveforms. This motion is reduced to a 0.25 degree card rotation by a 36:1 gear train assembly [2:4-1]. Thus, the display card moves in increments of 0.25 degree thereby limiting the resolution of the heading angle to + or - 0.25 degree movement of the indicator display can be tracked by a synchro control transmitter (CX) which is mounted internally on the rear of the compass card shaft (see Figure 2.6). This CX is intended to provide a slaving signal to another display, but can be used to get an absolute electrical representation of heading. This fact is crucial

# Syncro Control Transmitter (CX)

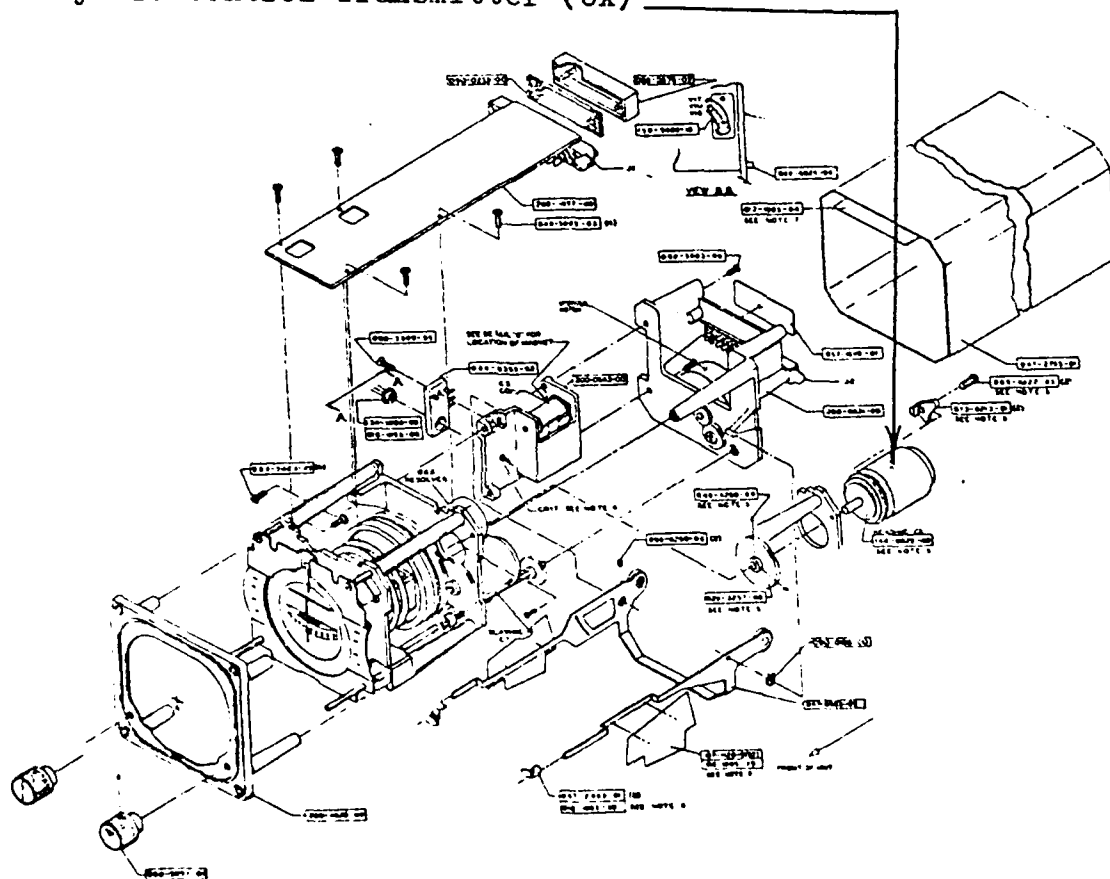


Figure 2.6. Indicator, Exploded View [2:5-5] .

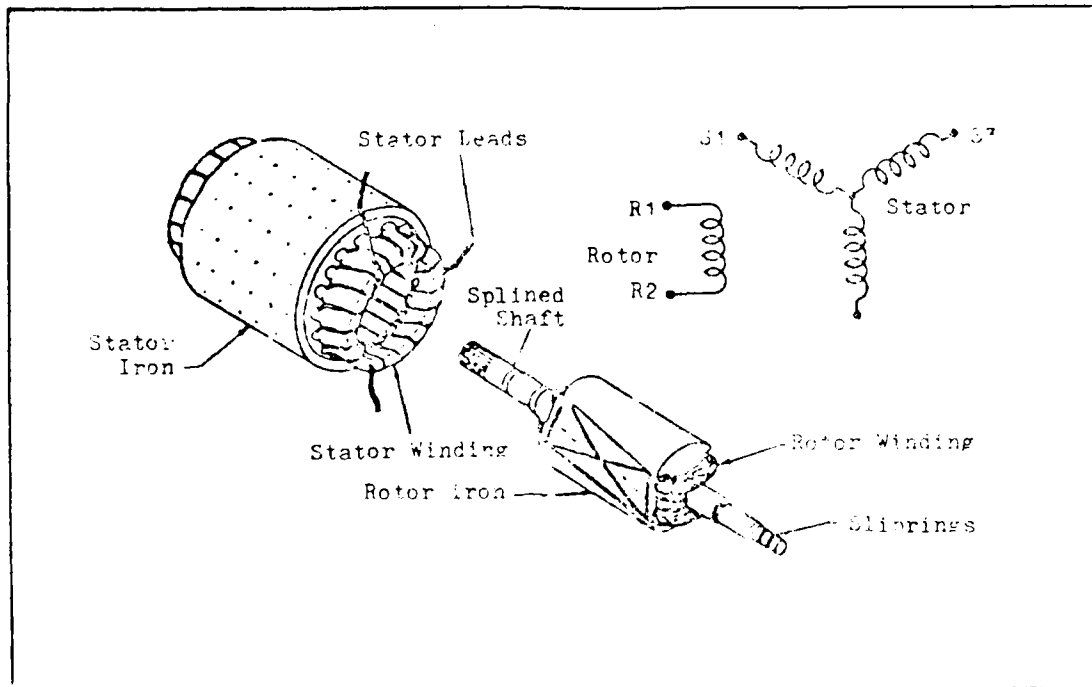


Figure 2.7. Internal Structure of a Syncro Control Transmitter and its electrical representation. [18:2]

to the realization of the GYRAC system. If the rotor of the CX is excited with a reference voltage (AC), then syncro format voltages will appear as output across the S1, S2, and S3 terminals (see Figure 2.7) [18:2]. These voltages are a function of the shaft angle  $\theta$ . For example, if the rotor (which has a single winding) is excited by a reference voltage across R1 and R2 (see Figure 2.7) of the form:

$$A \sin(\omega t)$$

Then the voltages which will appear across the stator

terminals will be:

$$S1 \text{ to } S3 = A \sin(wt) \sin \theta$$

$$S3 \text{ to } S2 = A \sin(wt) \sin( \theta + 120 )$$

$$S2 \text{ to } S1 = A \sin(wt) \sin( \theta + 240 )$$

where  $\theta$  is the shaft angle.

These voltages are known as syncro format voltages [18:2]. A desirable result of the syncro output is that it can be easily converted to a digital signal with a standard syncro-to-digital (S/D) converter. An SDC1700 12 bit S/D converter made by Analog Devices is used (see Appendix A and C) to provide a TTL digital binary representation of the heading angle (shaft angle). The SDC1700 also provides an angular velocity output in analog form which will be converted to digital by an analog-to-digital (A/D) converter. The A/D converter to be used is also produced by Analog Devices and is a 10 bit converter (Part # AD573, see Appendix A and C for detail).

The magnetic flux detector senses the direction of the earth's magnetic field and converts this information to a three-wire syncro format, much like the CX in the indicator. This information is transmitted to the indicator for slaving purposes, see Figure 2.8 for an exploded view of the detector. The flux detector can be oriented so the gyro system displays a heading relative to some artificial North direction. This feature is used to align the GYRAC system

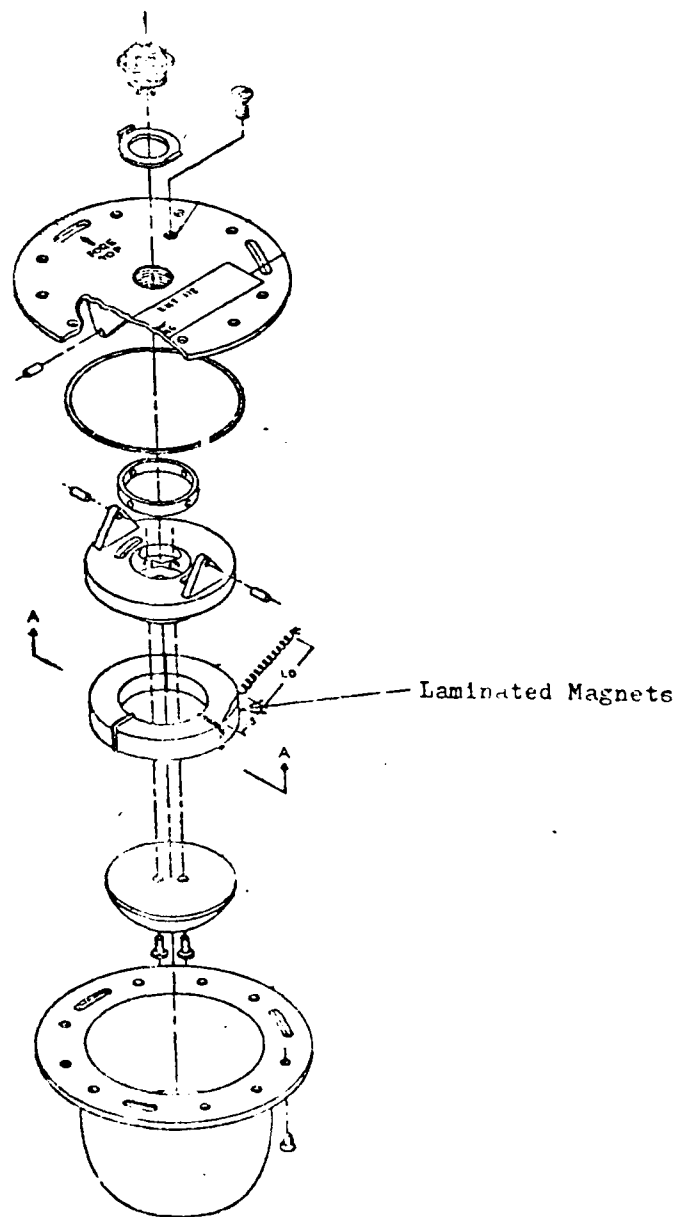


Figure 2.8. Flux Detector, Exploded View [4:5-3] .

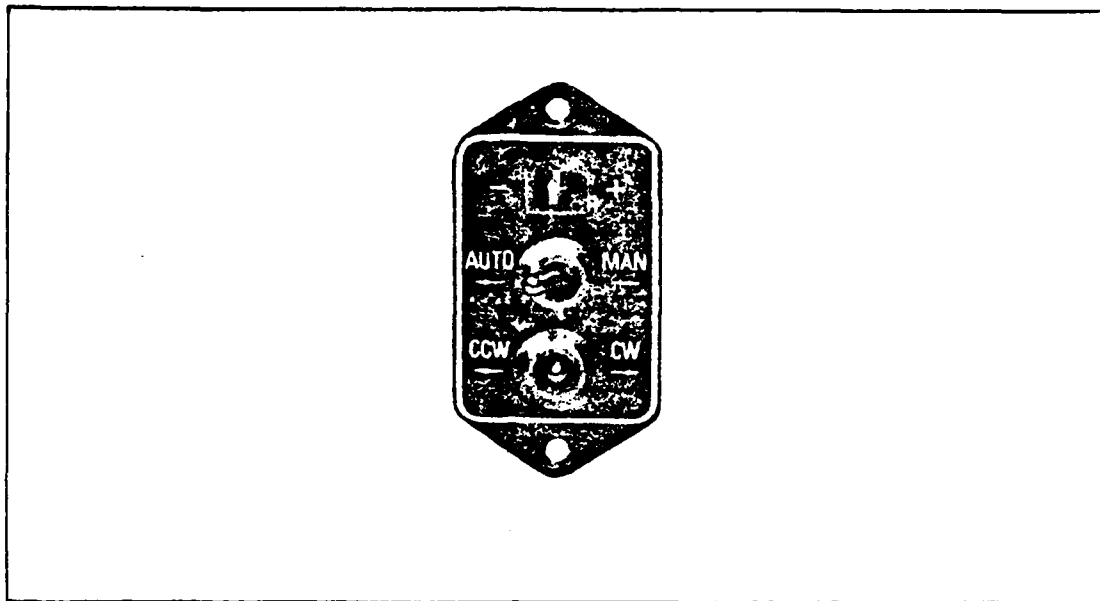


Figure 2.9. Slaving Unit [1:2-19]

with some convenient navigation coordinate system in the test area.

The slaving unit, shown in Figure 2.9, contains a slaving meter, slaving switches, and corrector circuitry which can compensate for the effect of local magnetic disturbances on the flux detector. The meter current is generated in the directional gyro base assembly (slaving logic) and represents the difference between the flux detector sensed heading and the heading displayed on the indicator. The slaving switches allow the gyro system to be operated in either a free-gyro mode (no slaving with the flux detector) or in the slaved mode (automatic slaving with flux detector). There is also a manual slaving switch which



can be used to rotate the display card in the indicator either clockwise or counter-clockwise. In addition to the slaving meter and slave switching functions, the slaving unit also includes a compensation circuit. This circuit causes a shift in the magnetic direction vector and thus can compensate for "hard iron" effects caused by nearby ferrous materials.

#### The Accelerometer Subsystem.

The accelerometer used in this thesis is a QA-1100 servo-type single-axis accelerometer produced by Sundstrand Data Control Incorporated (see Figure 2.10). The sensor, as

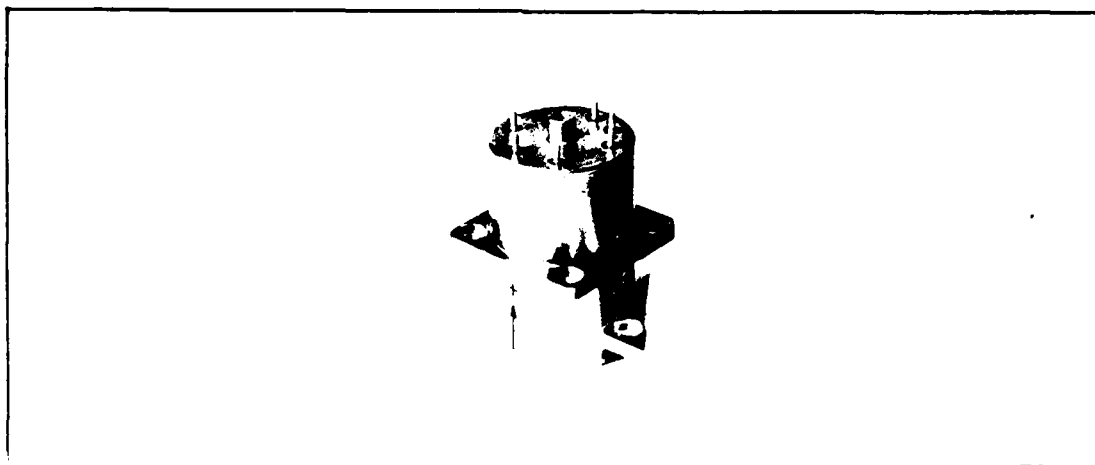


Figure 2.10. The QA-1100 Accelerometer [20]

shown in Figure 2.11, consists of the following key elements [7:1-3]:

1. A proof mass, pendulously supported and ideally constrained so as to allow only one degree of freedom about a well defined axis fixed within the

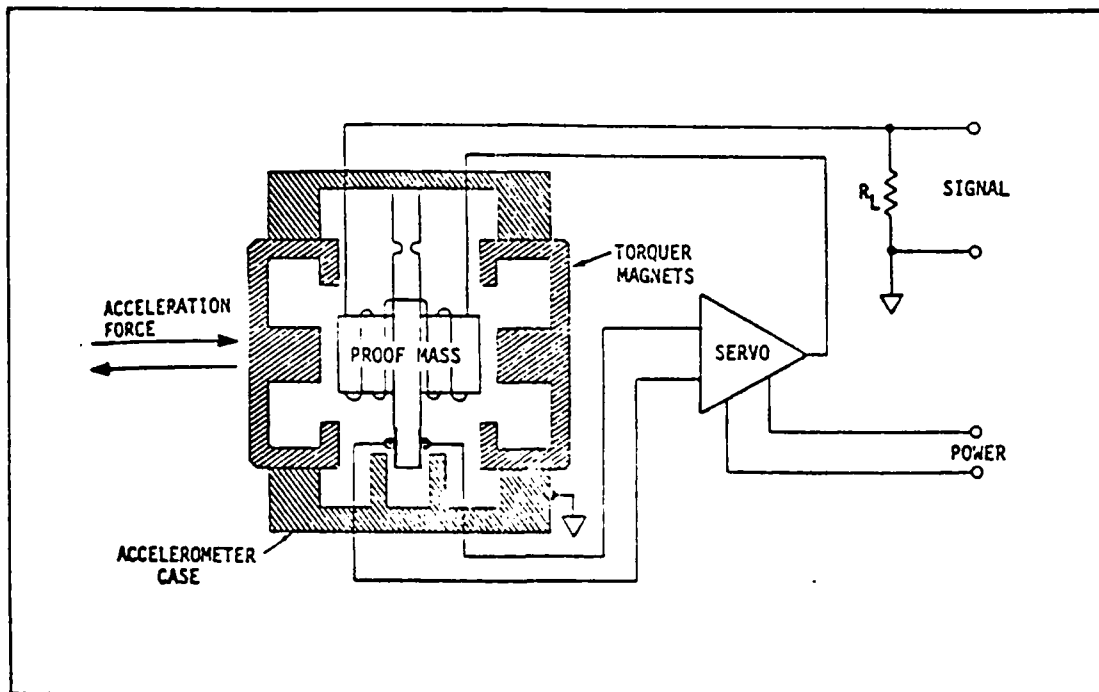


Figure 2.11. Basic Structure of a Servo-Type Accelerometer [7:1-3]

sensor.

2. A pick-off that can sense extremely small displacements of the proof mass.
3. A torquer, which is a coil positioned within a permanent magnetic field and attached to the proof mass, allowing force to be applied to the proof mass in response to a current passed through the coil.
4. A restorer circuit, or servo, that causes an electrical current to flow through the torquer coil in response to a pick-off signal. The resulting electromagnetic force balances the inertial reactive forces.

The basic operation of the accelerometer is that of a linear single axis electro-mechanical device for measuring

acceleration. The operation is based on movement of the proof mass during acceleration. A pickoff senses the displacement of the mass and the servo amplifier develops a current which is supplied through the torque coil to rebalance the proof mass. Thus, the rebalance current is proportional to the sensed acceleration and is a very accurate measure of acceleration. As more acceleration is applied to the accelerometer, the assembly will maintain the proof mass position and rebalance current will increase with increased acceleration until the sensor saturation limit is reached. An exploded view of the actual sensor assembly can be seen in Figure 2.12.

This type of accelerometer does not come with an internal (factory set) load resistor ( $R_L$  in Figure 2.11). Thus, an external load resistor must be provided. This is desirable since the ranging, or sensitivity, of the accelerometer output can be chosen to suit specific applications. The value of the external load resistor is determined by the following formula [7:3-6]:

$$R_L = \frac{\text{voltage sensitivity desired}}{\text{current sensitivity of the accelerometer}}$$

The current sensitivity of the QA-1100 is approximately 1.3mA/g (where g is the acceleration due to gravity). For this thesis, the accelerometer is configured to have a

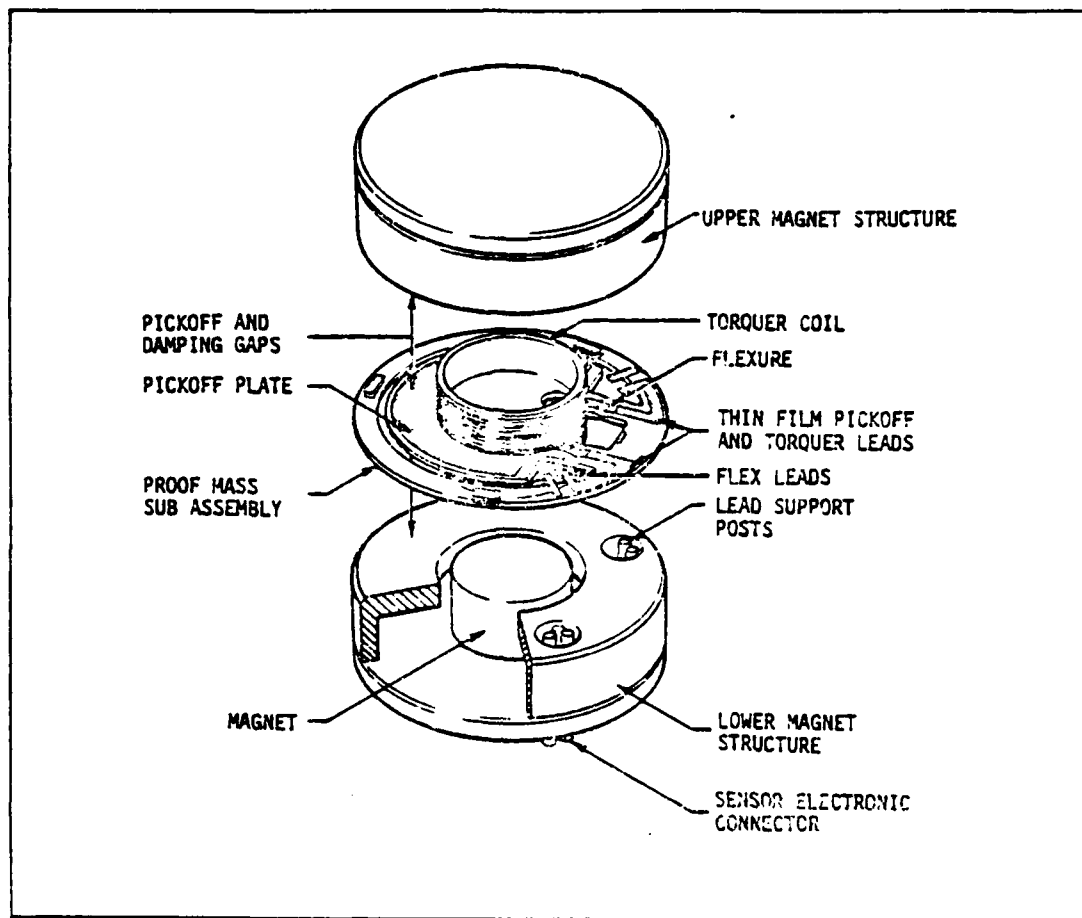


Figure 2.12. QA-1100 Sensor Assembly, Exploded View  
[7:1-4]

sensitivity of 2 volts/g. R consists of a single precision resistor in series with a 10 turn trim-pot for fine tuning of the sensitivity (see Appendix B for schematic detail).

As with any measurement device, the accelerometer has a scale factor and bias error. However, without the use of a centrifuge, these values are very hard to determine to a substantial degree of accuracy. Nonetheless, a tumble test can be performed and has been performed. A tumble test

consists of positioning the accelerometer with the input axis exactly vertical, pointing downward and then upward. The sensor will detect the earth's gravity vector. The two measurements (input axis up and input axis down, referred to as  $V_{OUT}$ ) are then used in the following equation:

$$V_{OUT} = V_{ACT} \times \text{Scale factor} + \text{Bias}$$

Here  $V_{ACT}$  is 2 volts (since 2 volts/g is the sensitivity of the accelerometer). Use of this equation results in two equations and two unknowns (scale factor and bias). Preliminary testing of the accelerometer has resulted in a very small value for bias (about 2 millivolts) and a scale factor of very near unity. Thus, for this thesis, the scale factor is assumed to be equal to one and the bias is assumed to be zero. This assumption will be discussed further in Chapter V under Review of Assumptions.

Accelerometers cannot distinguish between gravity and true acceleration. This fact is a major concern in the GYRAC system and must be accounted for. A special mounting platform has been built for the accelerometer allowing for complete leveling. The accelerometer platform will be initially adjusted until a very near zero reading is established from the accelerometer. However, during movement of the GYRAC system it is highly likely that errors will occur in the accelerometer output due to travel over a non-level surface. This problem is discussed further in Chapter

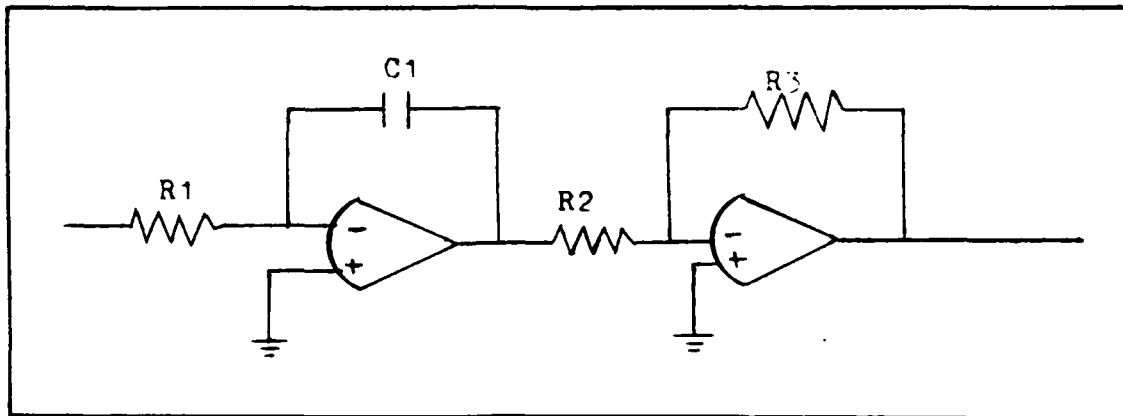


Figure 2.13. Accelerometer Integrator and Scaling Circuit

V under Review of Assumptions.

The output from the accelerometer is connected to an integrator circuit, shown in Figure 2.13. The output, which is velocity, is scaled such that one volt is equal to one foot per second of velocity. This analog voltage is then fed into an A/D converter (another AD573) resulting in a 10 bit binary representation of velocity.

#### GYRAC Computer and Interfacing Subsystem.

Up to this point, the gyro subsystem and the accelerometer subsystem have been discussed. The resulting output of these systems will be in digital form as mentioned earlier. The remaining task is to transmit these signals out to an external computer where they can be used for navigation purposes. This is accomplished through a bi-directional GYRAC sensor bus, the GYRAC computer, and an RS-232 interface. The sensor bus contains eight data lines,

four address lines, and one read/write line. Since the gyro and accelerometer data is all larger than 8 bits, the data from each of these devices must be gathered in two separate parts. This causes timing problems since the S/D and the A/D converters constantly update themselves with the most current measurement. This means that after a data signal is obtained, the value in the converter will change before the second half of the data signal can be transmitted.

This problem was solved by latching the data into a set of tri-state latches. These latches will hold the data as long as necessary, allowing sufficient time to transmit both bytes of the data signal. See Appendix B for more design detail. Also, since each data signal from each converter is divided into two parts, a separate address is used for each part. Thus, six addresses are needed to obtain all the gyro and accelerometer data. A seventh address is used to reset the integrator constant to zero (by discharging the capacitor over the op-amp). This reset is required to insure no initial condition exists on the integrator and can be used to reset the integrator periodically when the GYRAC system is not moving. See Appendix B for detailed design layout of address decoding.

All computer interface devices, the integrator circuit, the A/D converters, the accelerometer load resistor circuit, and a set of 7-segment LED displays are located on a general purpose wire-wrap card. The LED displays are used to read

the heading information coming from the S/D converter and display it in hexadecimal format. This information is used for initial alignment of the flux detector and troubleshooting. A layout of the wire-wrap card and the LED circuitry can be seen in Appendix B.

The GYRAC computer was originally a custom printer interface card built for AFIT, but was modified to its present state. The processor is a 6802 based microprocessor with 1k of ROM and 128 bytes of RAM. A modification was made to add an additional 2K bytes of static RAM to increase the memory capability. The new memory map is detailed in Appendix D. The computer also contains an asynchronous communication interface adapter (ACIA) which converts eight bit parallel data to RS-232 format serial data and handles all handshaking to an external computer. A parallel interface adapter (PIA) is also resident on the computer card which acts as the interface between the GYRAC sensor bus and the GYRAC computer bus. A power modification was also made to the computer to create its necessary + and - 12 volts and -5 volts from the + and - 15 volts available from the gyro base. The GYRAC computer software is present in the 1k EPROM (see Appendix F for program listing) allowing the computer to receive and respond to commands from an external computer via an RS232 serial link. A schematic diagram of the GYRAC computer showing the RAM and power modifications can be seen in Appendix D. Appendix E contains the edge



connector wiring diagrams for all the GYRAC system circuit boards (S/D converter card, interface card, and computer card) showing all interconnecting plugs.

#### GYRAC System - Theory of Operation

The purpose of this section is to provide a clear picture of how the GYRAC system functions as a whole. It is intended to supplement the previous subsystem descriptions. This discussion begins by explaining what occurs on system power-up and ends with a description of how the system responds to a command input. The slaving switch is assumed to be placed into the "slaved" position (representing a full up configuration of the GYRAC). The GYRAC must be stationary upon power-up to allow for stabilization of the flux detector.

Once power has been applied to the system, the rotor (spinning mass) in the gyro begins to rotate. Output from the gyro (the two square waves) is paused while the rotor comes up to operational speed (16,000 rpm). During this same time, a red HDG flag (compass warning flag - see Figure 2.4) is displayed on the indicator face. This red flag is a visual indication that the displayed heading is not valid. While the rotor is coming up to speed, the slaving signal from the magnetic flux detector is allowed to pass to the indicator providing the reference signal for magnetic north. The compass card in the indicator is rotated at the fast slaving rate, 360 deg/min [6], until the reading on the

indicator is in agreement with the magnetic flux detector slaving signal. Once the rotor has reached operational speed, the red HDG flag is removed and the indicated heading is valid. This usually occurs about one to two minutes after power-up. Any robot system using the GYRAC must account for this spin-up and alignment time (perhaps through a timed delay before requesting initial GYRAC data).

The absolute heading of the GYRAC system will be accurately shown on the indicator and on the LED display in 12 bit hexadecimal. Any rotational movement of the GYRAC will be sensed by the gyro which provides the signal to keep the indicator accurately positioned. In addition, the indicator will respond to deviations from the flux detector slaving signal at the slow slaving rate, 3 deg/min [6]. This slow rate is used to prevent the indicator from trying to follow an unstable reading from the flux detector. The flux detector is very sensitive to movement, so its output can only be trusted after it has stabilized. At this point (after the initial alignment), the flux detector signal serves primarily to compensate for gyro errors, such as drift. This particular gyro has proven to be a very accurate and stable reference. The drift rate of this gyro is less than 0.25 deg in 12 hours [8]. For this reason, the slaving signal from the flux detector could be turned off (switch to "free gyro" mode) after initial alignment is obtained.

After the heading data becomes valid, the GYRAC is ready to receive a command input. The firmware operating in the GYRAC computer is continuously checking for an input. Once an input arrives, it is compared to a list of acceptable commands. An acceptable command is a single byte of data in ASCII format representing the capitol letters A to O, see Appendix F for command definitions. If it is a valid command, the firmware program sets the appropriate address on the bus to enable the requested data (be it heading, heading rate, or velocity). The desired data is collected over the data bus (one byte at a time), converted to serial format and transmitted out via the RS-232 interface. The RS-232 interface is a simple three wire interface consisting of transmit data, receive data, and ground. See Appendix E for more detail.

It is important to note that the digital heading output is in a right-handed reference system. That is, the heading angle increases with counter-clockwise robot rotation. This is backwards from the visual indicator unit. The indicator displays increasing heading angle for clockwise rotation. Therefore, the digital output from the GYRAC and the LED displayed heading will not agree with the visual indicator except at 0 and 180 degrees. The GYRAC digital heading output was intentionally made to conform to the more conventional right-handed reference system.

### III. Integration of the GYRAC System onto MARRS-1

#### Structural

The entire GYRAC system is contained in a new third body tier which has been added to the top of the existing MARRS-1 physical structure. It is separated and supported from the lower body tiers by eight 10.0 inch by 3/8 inch diameter threaded and tapped aluminum rods. The all aluminum third tier is 12 sided and 20.5 inches by 20.5 inches by 7.0 inches high and contains two swing down removable-pin hinged doors to allow easy access to internal components. An 18.0 inch U-shaped aluminum tower extends above the third tier to provide support and ferro-magnetic isolation for the gyro's magnetic flux detector.

In addition, four aluminum plates were constructed and attached to the first and second body tiers locking them together into a single rigid body. This was done because the original robot design allows for separate body rotation of the first and second tiers. The GYRAC requires a fixed orientation relative to the entire body and can not tolerate rotation without introducing navigation errors.

#### Electrical

The electrical and mechanical subsystems of the GYRAC are completely isolated and independent of the remainder of MARRS-1. Power for the GYRAC is supplied over an external cable and connects to the body tier via a four pin DIN plug

(see Appendix E for detailed power distribution). All gyro commands and data are passed to and from the GYRAC via a standard three wire RS-232 serial interface. Connection is made on the GYRAC body via a standard RS-232 DB25 cable connector (see Appendix E for pin out details). These are the only two external connections required to operate the GYRAC. It is important to note that both of these connections and system operation is independent of MARRS-1. Therefore the GYRAC could easily be removed from the MARRS-1 structure and mounted on a different platform.

Utilization of the GYRAC system by MARRS-1 for navigation requires communication between three different onboard computers and a single external disk based computer for program transmission and data collection. Figure 3.1 illustrates the required interconnections.

The navigation computer, a Motorola 6802 based system resident in the first body tier, is the navigation system control computer. Its purpose is to collect sensor data from the GYRAC and drive computers, transmit collected data to the external computer, analyze this data and decide how to move, and then issue the appropriate commands to the drive computer.

The GYRAC computer, a Motorola 6802 based system contained in the third body tier, accepts requests for data, formats the data if necessary, and then transmits the requested data.

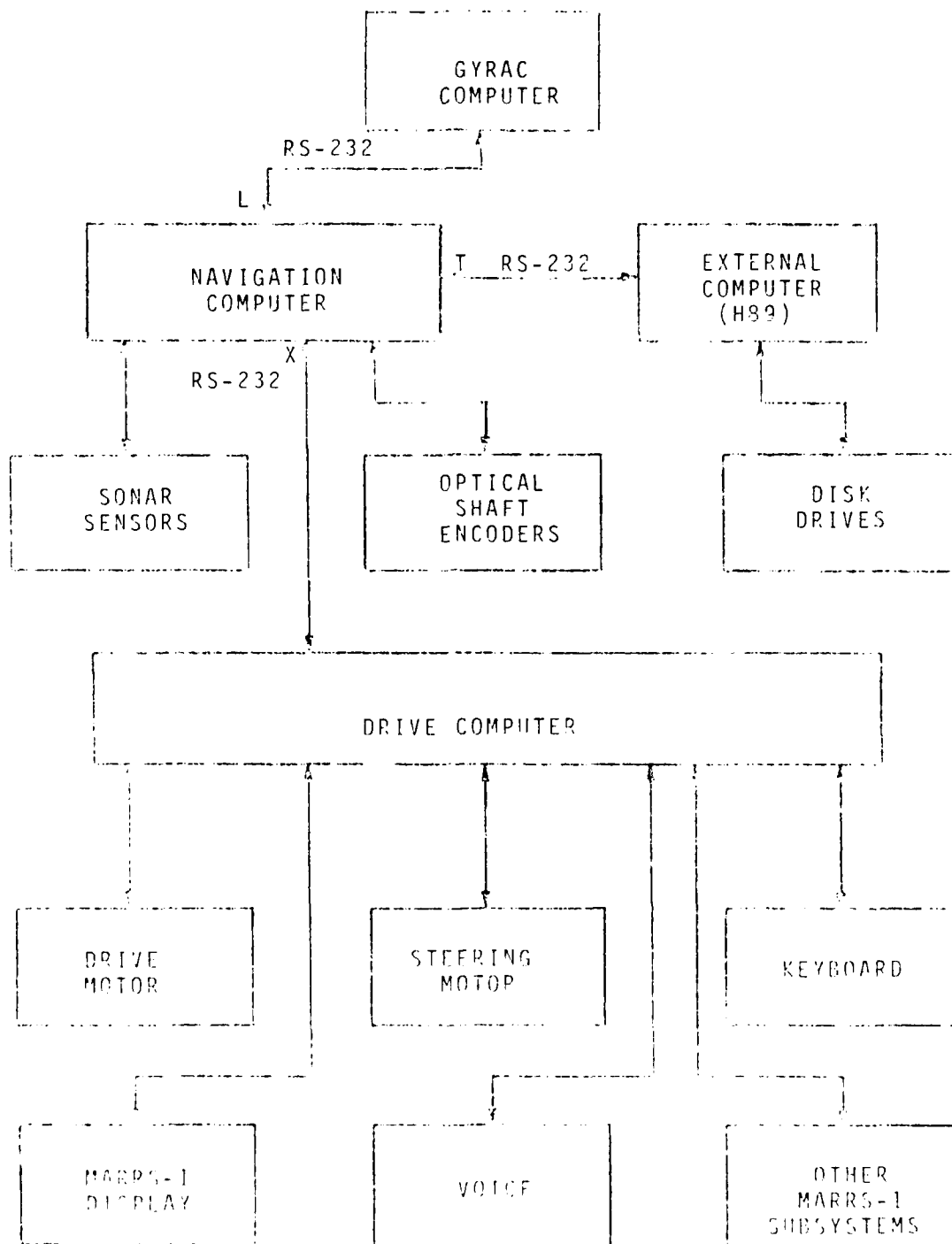


Figure 3.1 MAPRS-1 Computer System

The drive computer, a Motorola 6801 based system by Virtual Devices located in the first body tier, is the main robot computer. It controls all robot sensors and devices except the sonars and optical encoders, which are controlled by the navigation computer and the gyro and accelerometer which are controlled by the GYRAC computer. This computer is able to respond to both requests for data and commands to activate a device. However, as used in this thesis, the drive computer only accepts commands to move the steering wheel and start and stop the main robot drive motor.

The external computer, a Z80 based CP/M system by Heathkit, would not be required in a field deployed operational robot. However, as used in this thesis for data collection, it must be connected in order for the navigation software to function correctly.

All communication between the four computers is done via standard three wire RS-232 serial data links at 9600 baud. A cable is connected between the navigation computer Port X and the drive computer MENOS port. A second cable is connected between the navigation computer Port L and the GYRAC computer. The last cable is connected between the navigation computer Port T and the external computer. All cable connections are made with standard RS-232 DB25 connectors. They are located on the robot's rear lower panel, except the GYRAC connector which is on the back of the third body tier. Notice that all inter-computer

communication must go through the navigation computer.

Port L of the navigation computer was not originally designed to support 9600 baud. Therefore, a modification was made to the navigation computer board to allow Port L to select from one of eight switch selectable baud rates. It is now identical to the layout of Ports X and T [10]. All ports are currently set to 9600 baud.

In addition, the DB25 connector on the lower rear panel was wired in parallel to an existing internal cable to provide both laser barcode communication at 300 baud (original cable) and GYRAC communication at 9600 baud (new connector). Note that both functions can not be used simultaneously.

### Software

The MARRS-1 GYRAC system consists of four different custom software programs which can be run in three different system configurations to provide both test data and MARRS-1 navigation.

The first configuration allows direct communication with the GYRAC computer to allow testing, calibration, and checkout of the GYRAC subsystem. It makes use of the GYRAC program resident in read only memory (ROM) on the GYRAC computer board. An RS-232 cable must be connected between the GYRAC and the external computer. The modem 720 program (M72) is executed on the external computer to provide outside communications capability. Commands are typed on



the external computer's terminal and the corresponding data from the GYRAC is displayed. See Appendix F for complete operating instructions, structure charts, and program listings. Note that not all data is displayed since the GYRAC data is transmitted in a raw eight bit serial format which produces occasional non-printable characters.

The second configuration allows for collection and storage of heading, velocity, and angular velocity data at precise 0.1 second intervals. In addition, time mark data and distance moved from all three wheel's optical shaft encoders is provided. All data is reformatted to printable hexadecimal format which may be displayed on the external computer's terminal, saved to disk, or printed on the printer. It makes use of the GYRAC monitor program, in the GYRAC computer, and the GTEST overlay program, in the navigation computer (see Appendix F and G for GYRAC and GTEST program details). An RS-232 cable connection is required between the GYRAC computer and the navigation computer Port L and between the external computer and the navigation computer Port X. The M72 program is executed on the external computer to provide communication with MARRS-1 to send appropriate commands and receive data. See Appendix G for complete operating instructions, structure charts, and program listings. The MBASIC programs CONVERT and POSITION (see Appendix I) may be run on the saved data to produce a data plot.

The third configuration demonstrates limited mobile autonomous robot navigation (using only heading data) and collection and storage of gyro heading data. The heading data is reformatted to printable hexadecimal format which may be displayed on the external computer's terminal, saved to disk, or printed on the printer. It makes use of the GYRAC monitor program, in the GYRAC computer, the MARRS.NAV program in the drive computer, and the NAV program, in the navigation computer. An RS-232 cable connection is required between the GYRAC computer and the navigation computer Port L, between the navigation computer Port X and the drive computer (MENOS), and between the external computer and the navigation computer Port T. The M72 program is executed on the external computer to provide communication with MARRS-1 to send appropriate commands and receive data. See Appendix H for complete operating instructions, structure charts, and program listings. Note that the NAV and MARRS.NAV software demonstrates a very simple method of navigation and inter-computer communication. They are not intended to form the basis of a field application, but to illustrate gyro functionality.

#### IV. General Robot Navigation Theory

With the recent growth in research in the area of mobile and autonomous robotics, it is only a matter of time before a truly autonomous mobile robot becomes a reality. This robot will possess a navigation system capable of gathering and processing sensory information to accurately determine its location. In addition, the navigation system will also maintain a world model of the robots environment, perform path planning (determine travel routes around known obstructions), and provide for dynamic obstacle avoidance (method of surmounting unknown obstacles). The task of the navigation system will be very complex and its future development is crucial to the realization of a mobile autonomous system.

Two major aspects of the robot navigation problem, world modeling and path planning, will be the topic of this chapter. Dynamic obstacle avoidance is considered beyond the scope of this thesis and will not be covered. First some governing assumptions will be discussed. Second, an overview of several popular approaches to world modeling will be presented. Third, a new world modeling technique will be introduced. Finally, this chapter will conclude with a detailed presentation of path planning based on this new world model.

### ASSUMPTIONS

Since the world model is intended for use by a land based robot (MARRS-1 in particular) which can only move in two dimensions, only a two dimensional "floor plan" type world model will be considered. Robots that could extend or shrink themselves vertically would constitute a special category which is beyond the scope of this paper. For more information on three dimensional modeling and path planning see [15]. This section will also be concerned only with a robot which can be modeled in two dimensions as a circle (consistent with the use of MARRS-1). Some techniques for treating robots of other geometries can be found in [15]. Finally, it is assumed that all locations on the world map can be represented directly in an absolute reference frame.

### PAST APPROACHES

World modeling can be thought of as providing a description (in essence a map) of the robots known operating environment. This information must be expressed in terms that the robot can easily understand and best utilize. Virtually all models to date represent the physical world of the robot in two dimensions using an outline picture method. Two approaches have been used to describe the robots world. One approach has been to model all the obstacles in the robots world. The other approach has been to model the free space or safe areas of travel for the robot. Basically, the choices are to model where the robot can or cannot go.

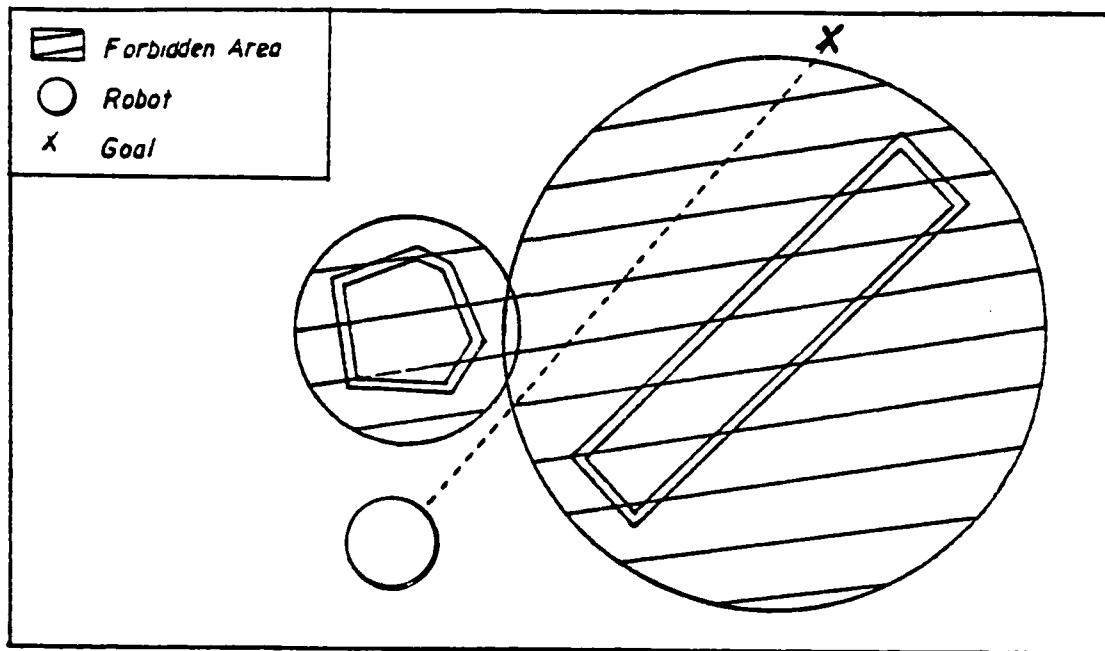


Figure 4.1. Circular approximations of physical objects [16:24]

Moravec [17] proposed modeling all physical obstacles with their enclosing circles. The radii of the enclosing circles could be increased by a small amount to provide a clear area of buffer space surrounding the obstacle. This would help prevent collisions between the robot and the obstacles. The primary drawback of this method is the waste of useful free space (see Figure 4.1).

A better way to model physical objects would be to use straight line polygonal closed surface approximations. The lowest order polygon possible would be the best choice. Lozano-Perez [15] has done considerable work in this area.

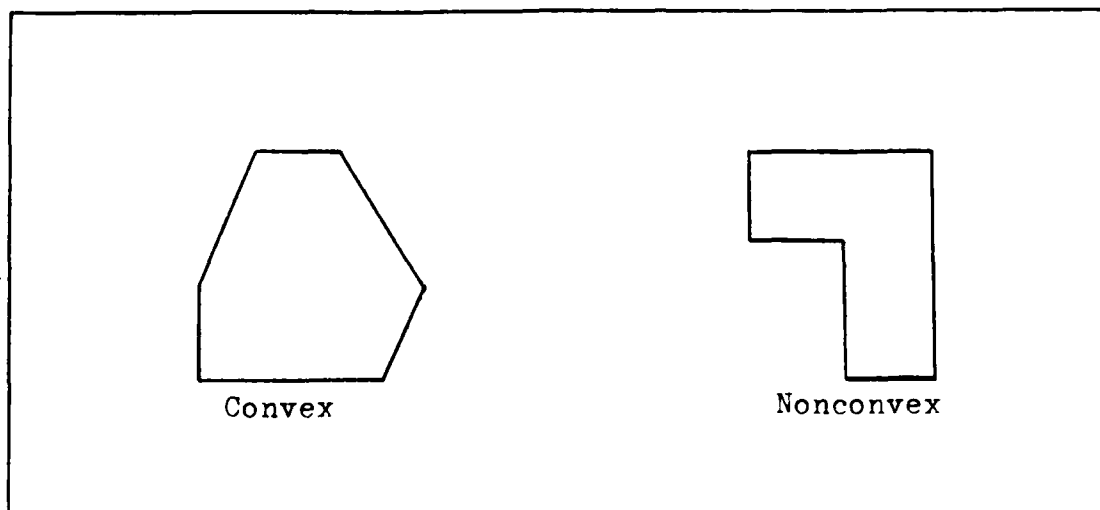


Figure 4.2. Polygon approximations to real world obstacles

He not only chooses to model physical objects as polygons but as convex polygons. A convex polygon is a polygon with no internal angle greater than 180 degrees (see Figure 4.2).

Given that all obstacles are represented as convex polygons, a path can be found around an obstacle by searching for a path around the vertices or corners of the polygon. For example, to go from point A to point B, in Figure 4.3, a path is planned going through each vertice of the polygon obstacle. Only the paths that do not cross the obstacle are considered possible. Either path 1 or 2 could be taken. Both traverse the outside perimeter of the obstacle and result in the shortest paths available. Physical objects such as that shown in Figure 4.2 which are not convex in shape are either modeled as convex anyway or modeled as overlapping convex polygons by Lozano-Perez (see Figure 4.4).

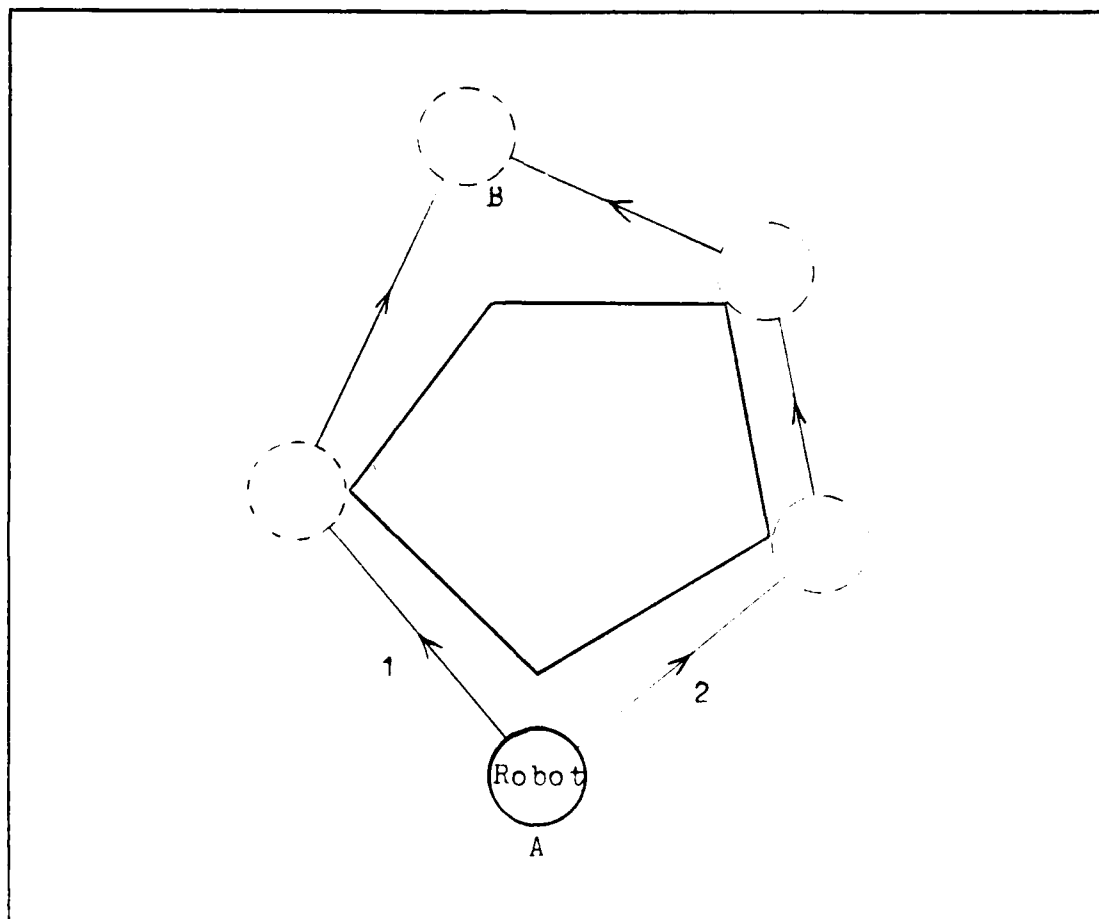


Figure 4.3. Technique of Lozano-Perez for going around an obstacle.

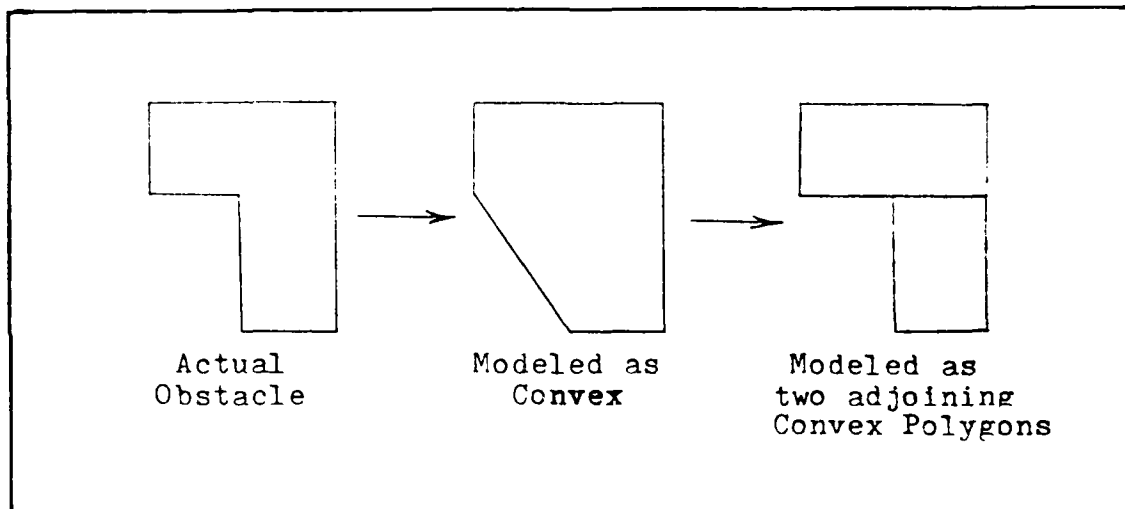


Figure 4.4. Examples of how an obstacle may be modeled using Lozano-Perez technique.

For a circular shaped robot, Lozano-Perez proposes a technique of displacing the vertices of an obstacle by the radius of the robot [15:562]. Thus, the robot can be treated as a point; thereby, greatly simplifying the path finding problem. This technique is illustrated in Figure 4.5. Notice how the robot (now a point) is made to pass through the extended vertices.

The technique of Lozano-Perez has several disadvantages. It can be wasteful of free space and computationally inefficient because physical objects must be modeled as convex polygons. In addition, this technique forces the robot to hug an obstacle as it goes around it. Relatively small errors in the world map or in the navigation data greatly increase the probability of a collision.



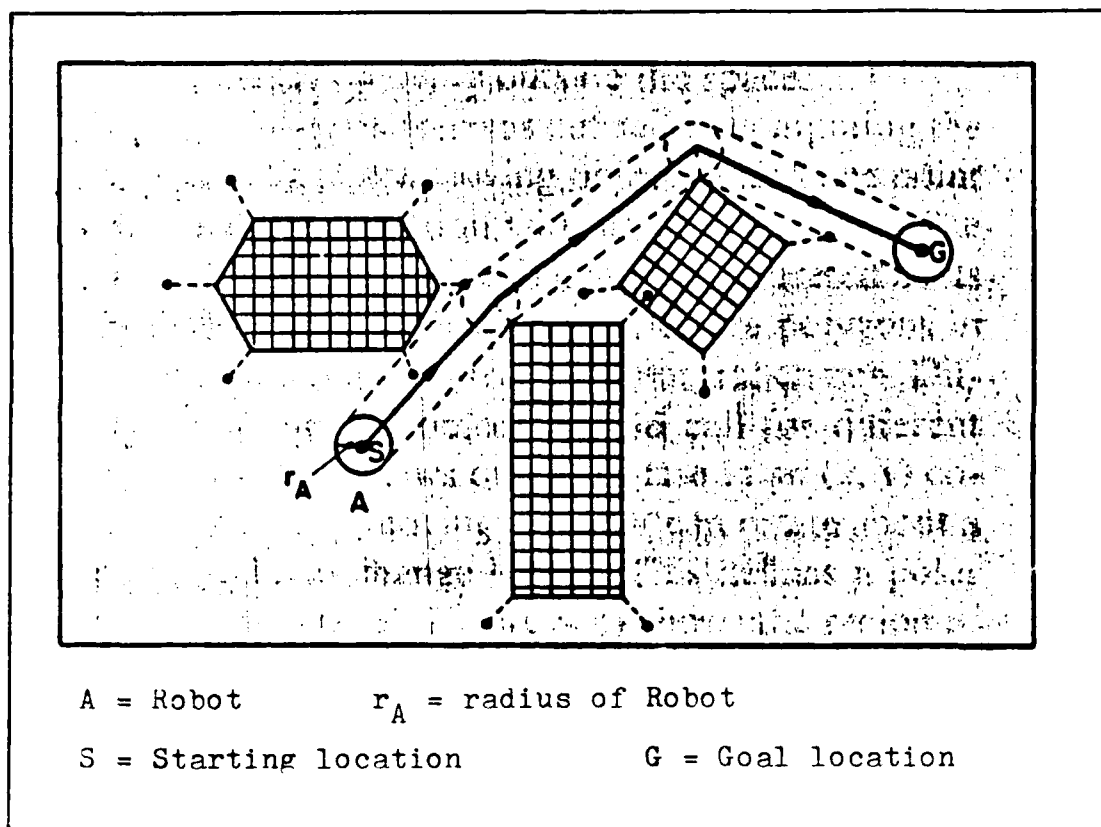


Figure 4.5. Vertices of all obstacles are extended outward so the robot can be treated as a point.  
 [15:562]

Monaghan [16] also proposes using polygon approximations for obstacles, but does not restrict the polygons to convex shapes only. This results in a better representation of the actual shape of an obstacle with a minimum number of total vertices. He also shrinks the robot to a point mass and enlarges the obstacles by a likewise amount by extending the sides of the polygons (remember Lozano-Perez extended the vertices). Monaghan's path finding technique is similar to that of Lozano-Perez where a

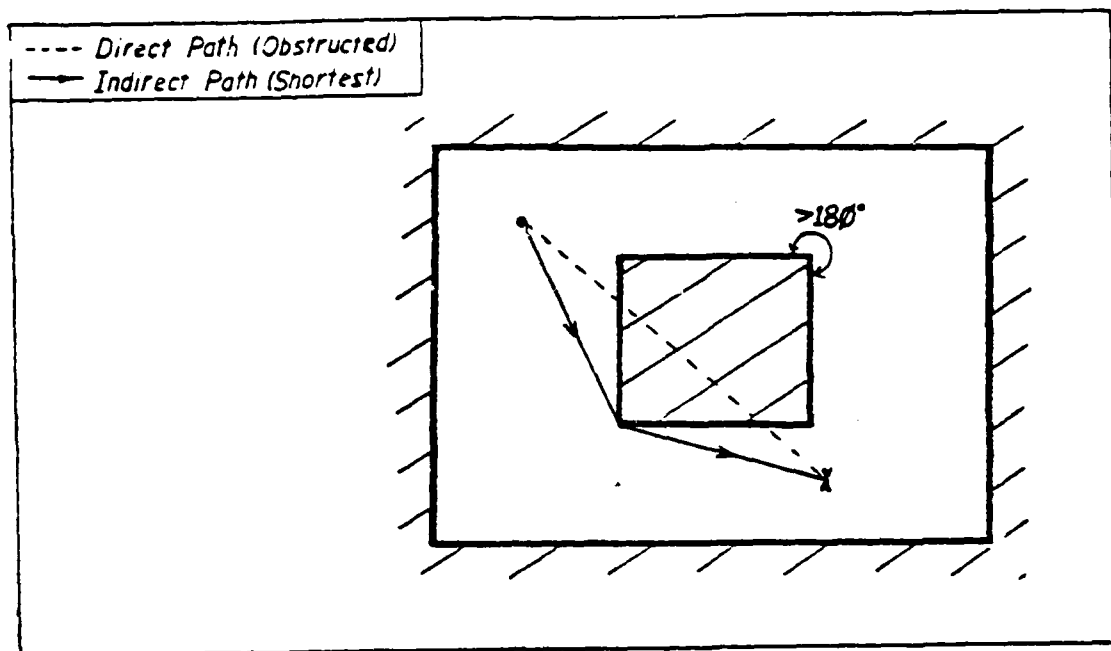


Figure 4.6a. Monaghan's modeling technique [16:47]

search of the vertices of an obstacle is performed to find a way around it. Monaghan's work emphasizes finding the shortest path to the goal point. Thus, a vertex of an obstacle is used as a "way point" as shown in Figure 4.6a. However, an inside corner (resulting from the use of nonconvex obstacles) is never considered as a way point (see Figure 4.6b). This technique does give the shortest path, but it is certainly not the safest (due to possible collision).

So far, the obstacles modeling approach to world modeling has been discussed. We have seen that obstacles may be represented by either their enclosing circle or a polygonal approximation. Another approach to world

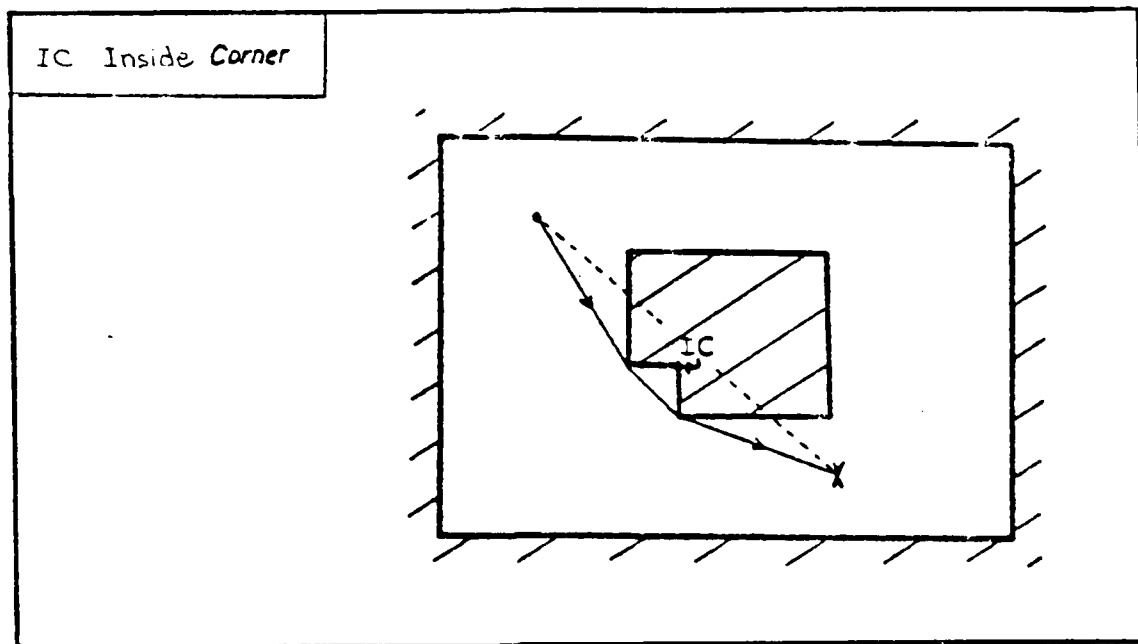


Figure 4.6b. Inside corners are not used as "way points"  
[16:48]

modeling is to model the free space which a robot may occupy.

Brooks describes the free space which a robot may travel as a network of cones [16:25]. Obstacles are polygon shaped and the free space between the faces of these polygons can be formed into generalized cones or "freeways" (see Figure 4.7). The robot is restricted to travel along the center or "spine" of these cones. This technique is less prone to collision since the robot is required to remain at the centerline of free space. The major problem with this method, as pointed out by Monaghan [16:28], is "the difficulty of modeling the map to account for movement

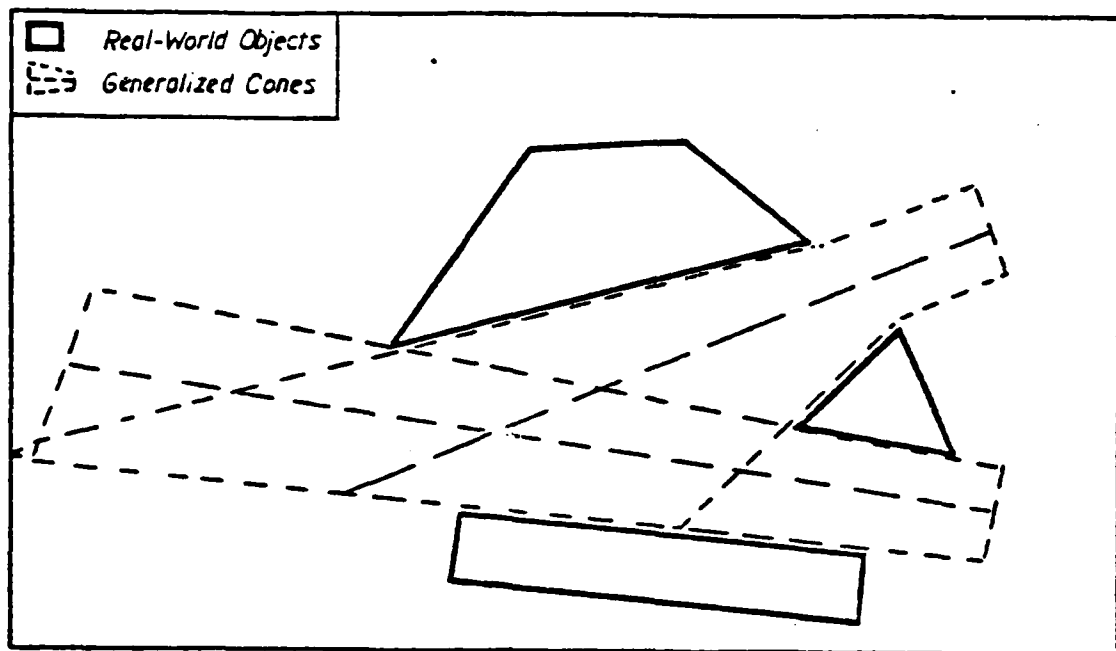


Figure 4.7. Generalized cones form freeways between obstacles [16:27]

of any obstacles. Repositioning a single object could involve comparing each of its faces with all those of every other obstacle to recompute the adjacent free space cones."

Another free space modeling technique directly models the regions through which the robot may travel. This technique is attributed to Crowley [16:28]. Crowley models the free space around objects through a series of convex polygons (see Figure 4.8). It is important to note that any two points within a convex polygon can be connected with an unobstructed line (see Figure 4.9). Thus, movement confined to within the borders of a convex polygon is guaranteed to be collision free. Motion is restricted, however, when it is necessary to travel to other regions (adjacent convex

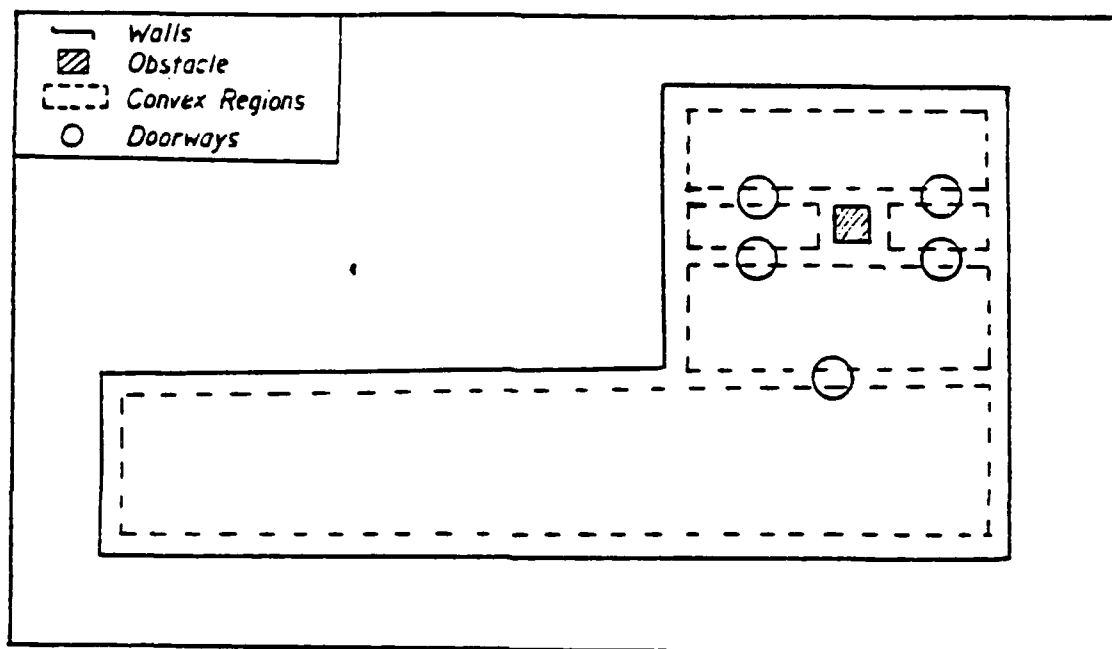


Figure 4.8. Convex regions separated by doorways represent free space [16:29] .

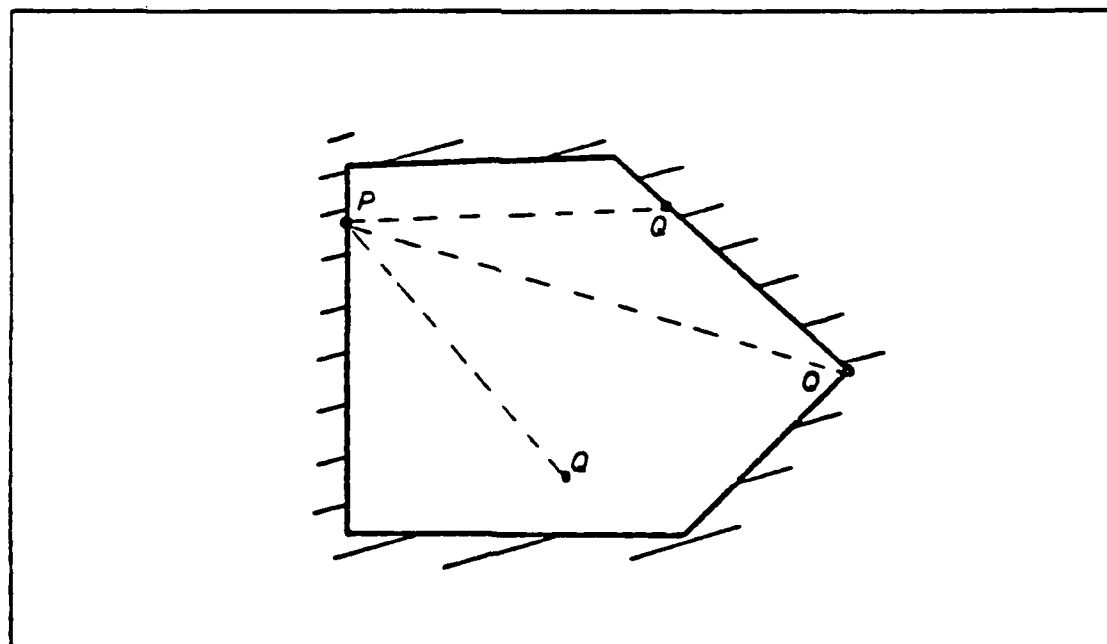


Figure 4.9. Any two points, P and Q, in or on a convex polygon may be connected by an unobstructed straight line [16:45] .

polygons). This can only be done through a defined "doorway" (see Figure 4.8). With this modeling technique, finding a path results in searching the network of doorways and free spaces.

Crowley also treats the robot as a point much the same way Lozano-Perez does. However, while Lozano-Perez enlarges obstacles to account for the robots size, Crowley shrinks his free space by an amount equal to the robot radius. One problem with Crowley's technique can be seen in Figure 4.8. Notice that for just one obstacle, five free space regions must be stored into memory. Also, if an obstacle is moved many free space regions must be recomputed. Crowley's use of doorways, however, is very appealing and will be expounded upon later.

#### A NEW TECHNIQUE

A brief discussion of the current schools of thought for modeling a robot's world has preceded this section. By combining some of these ideas, a better method can be obtained. Consider the following approach:

1. Obstacles will be modeled as polygons (not just convex).
2. The obstacles will be enlarged so the robot can be treated as a point.
3. Abstract safe points will be established such that at least one safe point can be reached from anywhere in the robots environment.

This method is a combination of obstacle modeling and free

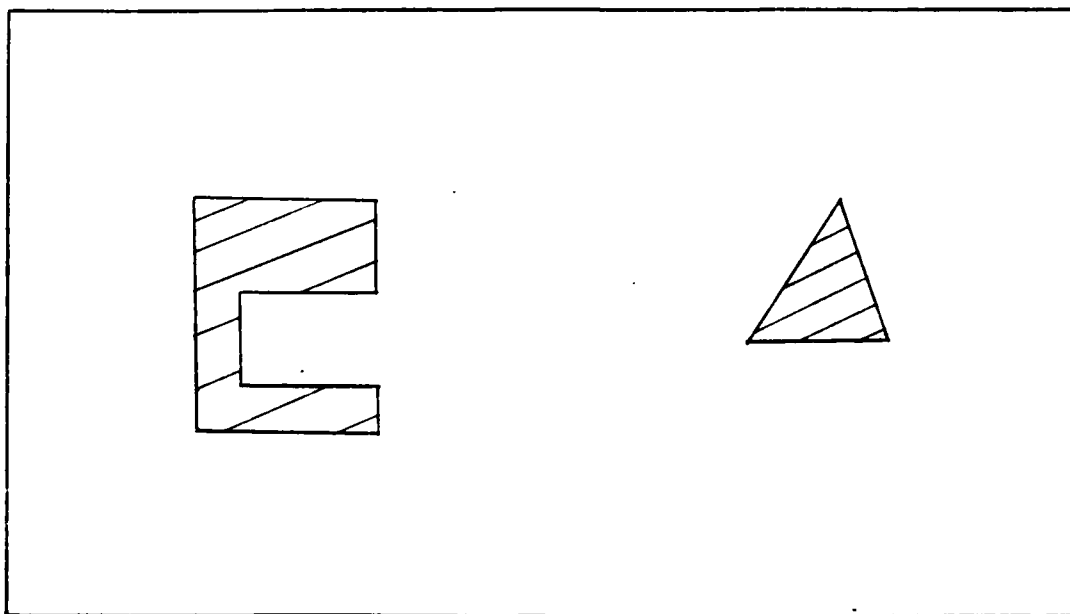


Figure 4.10 Room with two obstacles.

space modeling techniques. For example, in Figure 4.10, a room is depicted with two obstacles. Note that one obstacle is convex in shape and the other is not. Now, a series of doorways can be established much the same way as in Crowley's technique. The free space is divided into adjoining convex polygons as in Figure 4.11. Then, doorways are established between adjacent convex regions. Next, the free space boundaries are removed leaving only the obstacles and the doorways (which are represented as a series of points - see Figure 4.12). These doorway points are called "safe points". If a direct path is obstructed, a search is made of the "safe points" and indirect paths can be obtained as in shown Figure 4.13.

Unlike Crowley's technique, requiring a doorway be used

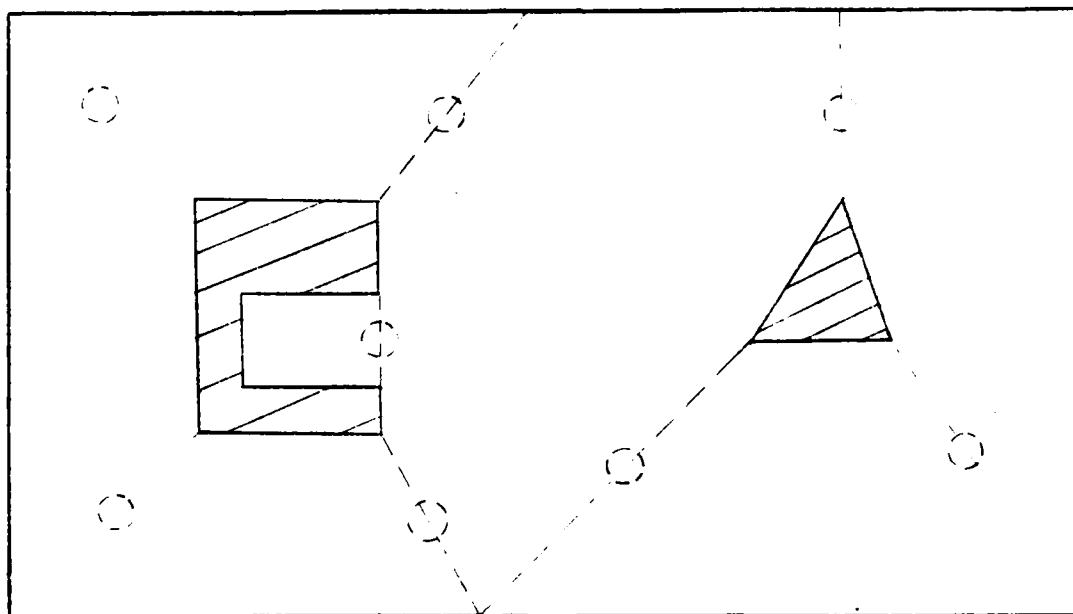


Figure 4.11. Free space is divided into convex regions to define "safe points."

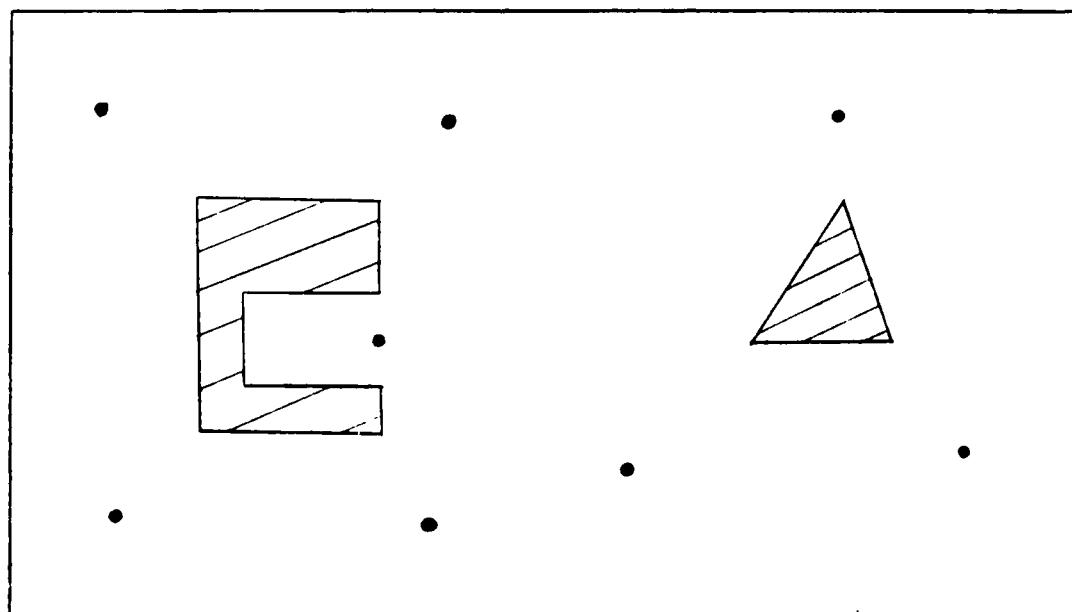


Figure 4.12. Only obstacles and safe points are modeled.



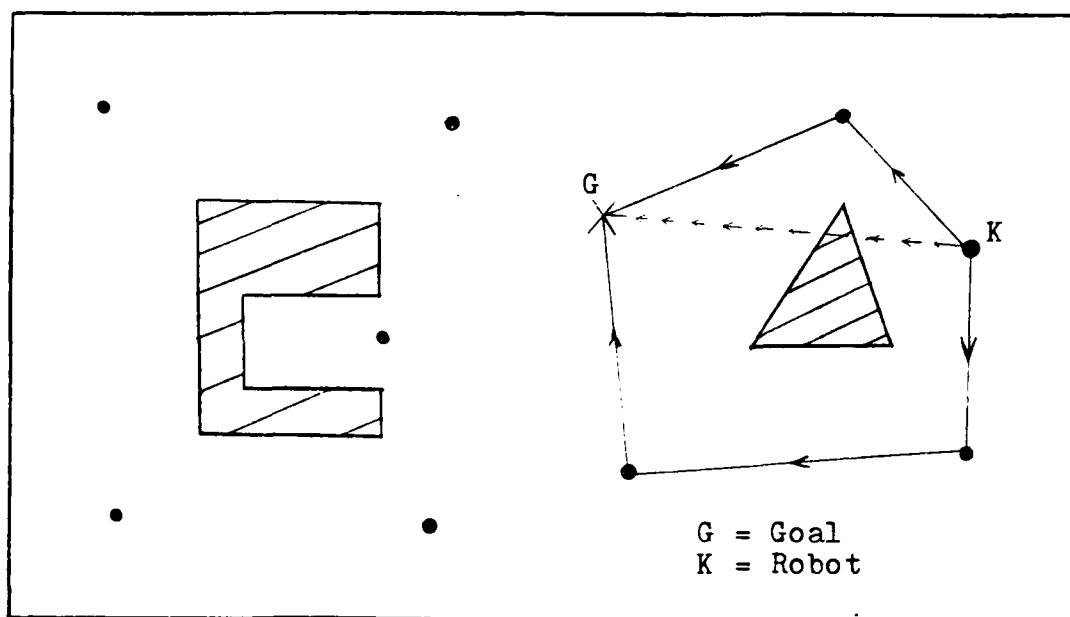


Figure 4.13. Indirect pathways pass through safe points.

as passage between free space regions, this technique uses doorways or safe points only when the goal is obstructed by an obstacle. Direct passage can take place anywhere in the room as long as the pathway is unobstructed.

To avoid having pathways which run very near the side of an obstacle, the free space boundaries must be carefully chosen when establishing safe points. For example, Figure 4.14 shows again the way Crowley separates a room into free space regions. This is a poor choice since it may require sustained travel very near an obstacle or border. Notice how the path to the goal runs parallel to the wall. This increases the chance of collision. As a rule of thumb, free space boundaries should be constructed so they never run parallel to an obstacle face or exterior boundary. Figure

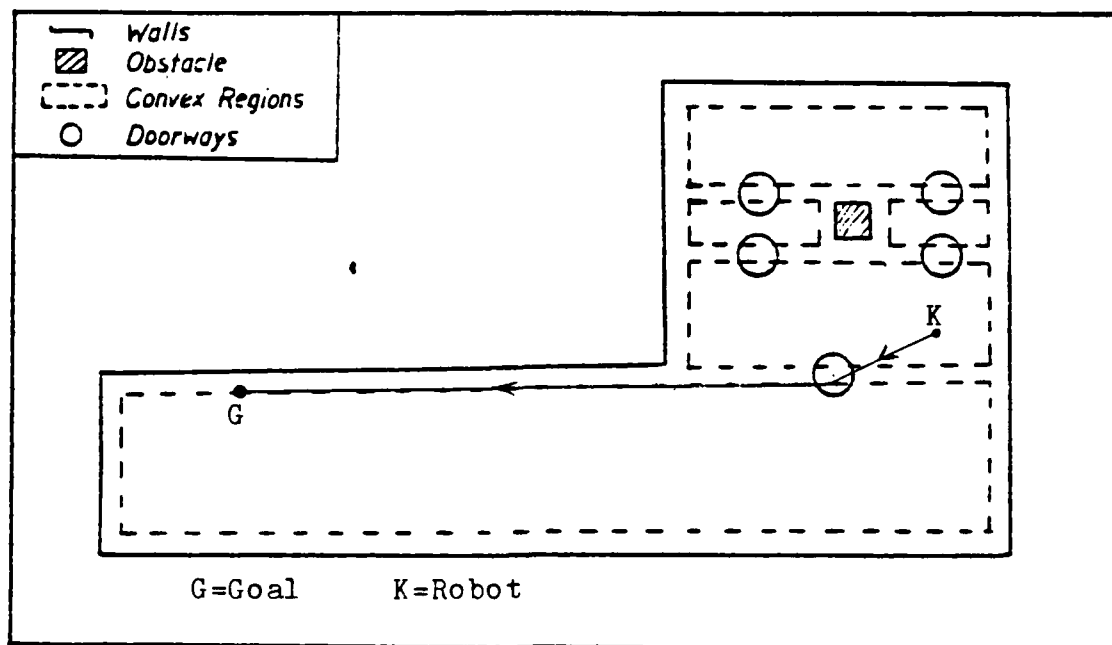


Figure 4.14. Problems occur if free space regions are not chosen correctly.

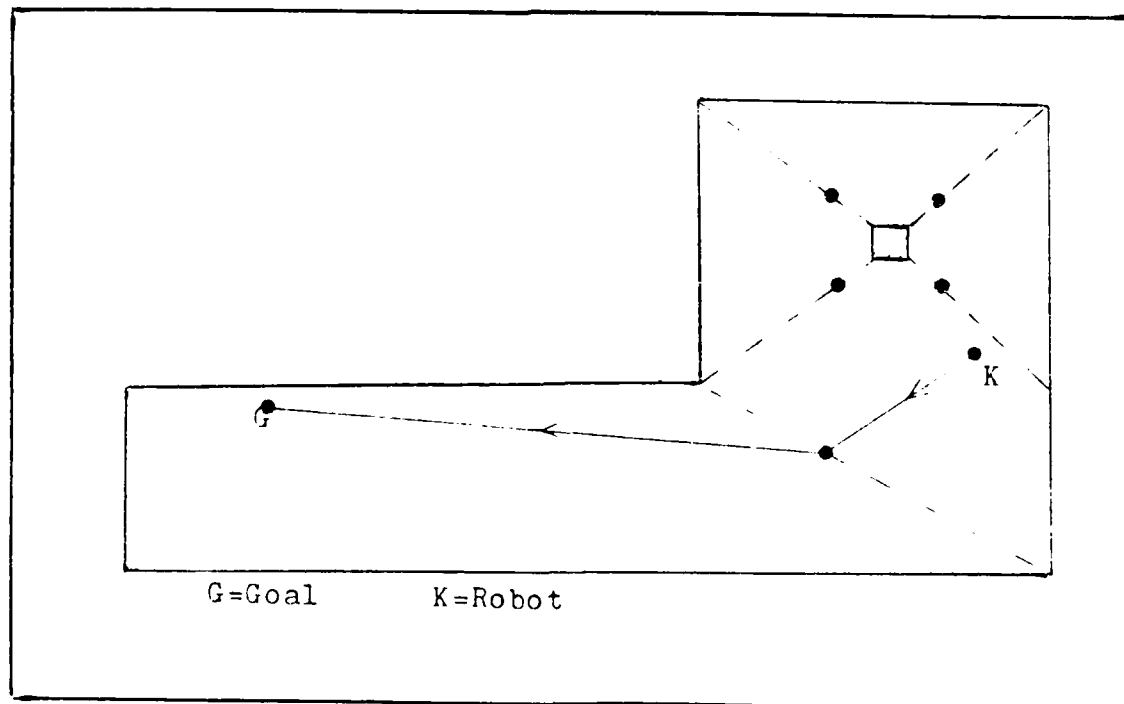


Figure 4.15. Free space regions can be chosen to minimize the probability of collision.

4.15 shows the same room only this time with different free space borders. None of the borders are parallel to an obstacle face or exterior boundary. Figure 4.15 also shows the new path for the same starting and goal points as in Figure 4.14. Notice how the path no longer hugs the wall. By using this rule of thumb, safer pathways can be planned.

This new technique offers several significant advantages. By using regular polygons to model obstacles, an accurate representation of the actual physical object can be obtained, wasting little or no free space. Treating the robot as a point precludes having to consider the volume of space occupied by the robot. Using "safe points" to plan paths around obstacles keeps the robot a safe distance from obstructions. Thus, fewer collisions should occur. Above all, this method is simple and requires minimum computer memory.

This technique also has a few disadvantages. It could be argued that not yielding the shortest path is a disadvantage. However, for a robot not under a tight energy or time constraint, the shortest route is not necessarily the best. Safety may be more important. When the world model becomes very complex, some other disadvantages appear. If an obstacle is moved, several safe points may have to be recomputed. Also, as the number of obstacles increases, the number of safe points goes up almost exponentially resulting in heavy computational loading.

### DETAILED PATH PLANNING

World modeling and path planning are highly dependent upon each other. Path planning cannot take place until a world model has been determined and the best world model is one that provides for the best path planning. In the preceding discussion of world modeling, it was necessary to consider path planning in a general sense. For example, the robot must determine if an obstruction lies in its direct path to the goal. How does the robot do this? How does the robot determine the best indirect path if an obstruction exists? Details of path planning will be discussed in the following section which will answer these questions.

The world model is stored in the robots memory as an ordered list of points. All of the points  $(X,Y)$  are relative to the same reference system. Each obstacle is described by an ordered list of its vertices. Also, the vertices of all exterior boundaries are stored (to the robot, exterior boundaries are just more obstacles). Safe points are stored as a separate list of points. Thus, a simple room can be represented as in Figure 4.16.

Assume that the robot is located at  $(17,10)$  and the goal is located at  $(2,11)$  as depicted in Figure 4.16. Notice, that the direct path to the goal is obstructed. This is obvious to us, but how does the robot know this? Before answering this question lets review some geometry. Figure 4.17 shows a line segment connecting the points K and

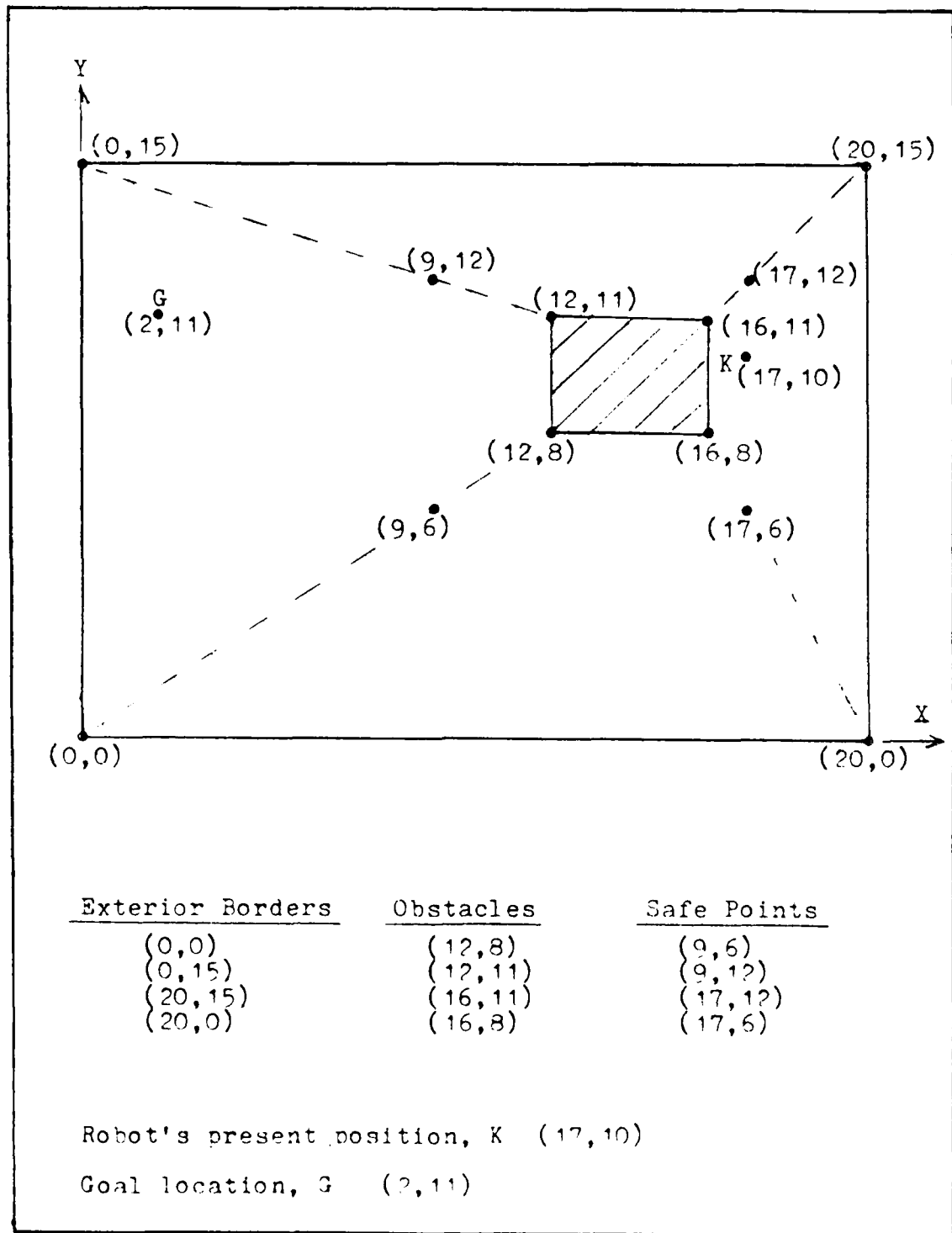


Figure 4.16. Modeling of a room with one obstacle as a set of points.

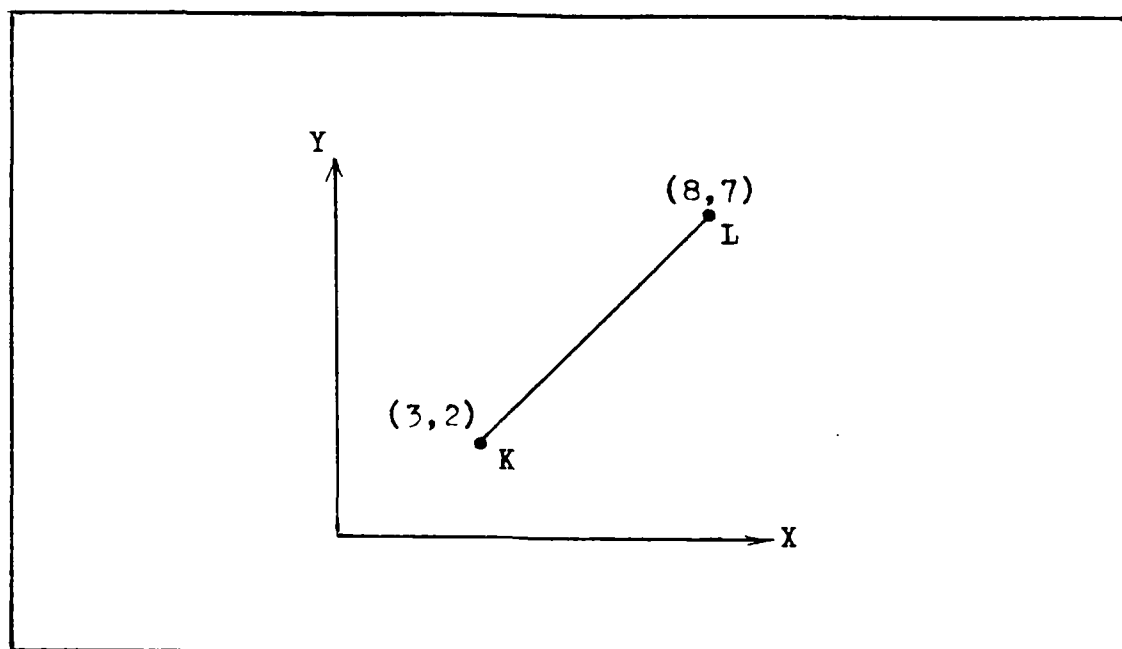


Figure 4.17. Line connecting two points can be represented through parametric equations.

L. This line segment can be represented by the following parametric equations [16:62]:

$$X = X_K + (X_L - X_K)s$$

$$Y = Y_K + (Y_L - Y_K)s \quad (1)$$

Substituting the coordinates of K and L into the parametric equations results in the following expressions:

$$X = 3 + (8 - 3)s$$

$$Y = 2 + (7 - 2)s$$

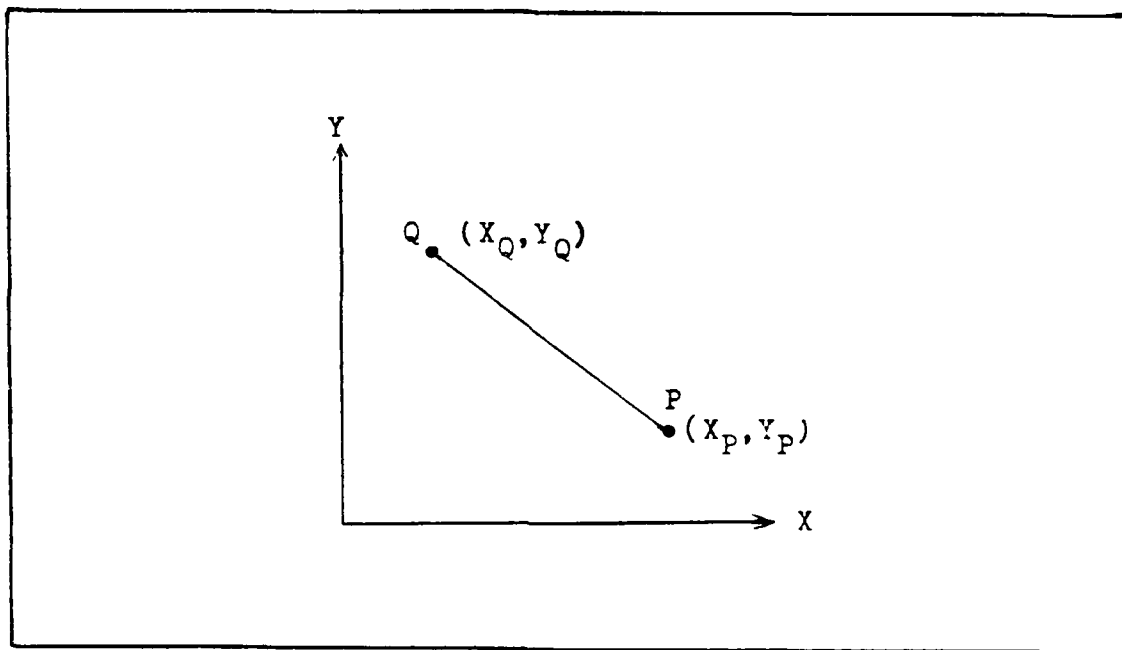


Figure 4.18. Line connecting two arbitrary points.

*Simplifying*

$$X = 3 + 5s$$

$$Y = 2 + 5s$$

$(X,Y)$  obtained from these equations will always lie on the line segment for  $s$  between 0 and 1.

Now consider another set of points  $P$  and  $Q$  as shown in Figure 4.18. Let this line be represented by the following parametric relations

$$X = X_P + (X_Q - X_P)t$$

$$Y = Y_P + (Y_Q - Y_P)t \quad (2)$$

where  $t$  is the parameter in this case. Again, if  $t$  lies between 0 and 1 then  $(X,Y)$  is on the line joining  $P$  and  $Q$ . The parametric relations (1) and (2) can be used to develop a test which can determine if two line segments intersect [3]. Solving the set of equations (1) and (2) simultaneously for the parameters  $s$  and  $t$  results in the following expressions:

$$s = \frac{(X_Q - X_P)(Y_P - Y_K) - (Y_Q - Y_P)(X_P - X_K)}{(X_Q - X_P)(Y_L - Y_K) - (Y_Q - Y_P)(Y_L - X_K)} \quad (3)$$

$$t = \frac{(X_L - X_K)(Y_P - Y_K) - (Y_L - Y_K)(X_P - X_K)}{(X_Q - X_P)(Y_L - Y_K) - (Y_Q - Y_P)(X_L - X_K)}$$

The parameter values,  $s$  and  $t$ , obtained from the above expressions can be used to determine if two lines intersect. Two lines intersect only if both  $s$  and  $t$  take on values between 0 and 1. This test will hereafter be referred to as the parameter test.

To determine if an obstacle lies in the direct path of the robot, the parameter test is performed. The robot's location and the goal point form one set of points ( $K$  and  $L$ ). The vertices ( $P$  and  $Q$ ) of each obstacle are then used, one pair at a time, to determine if an intersection exists. All obstacles or obstacle faces may not need to be checked



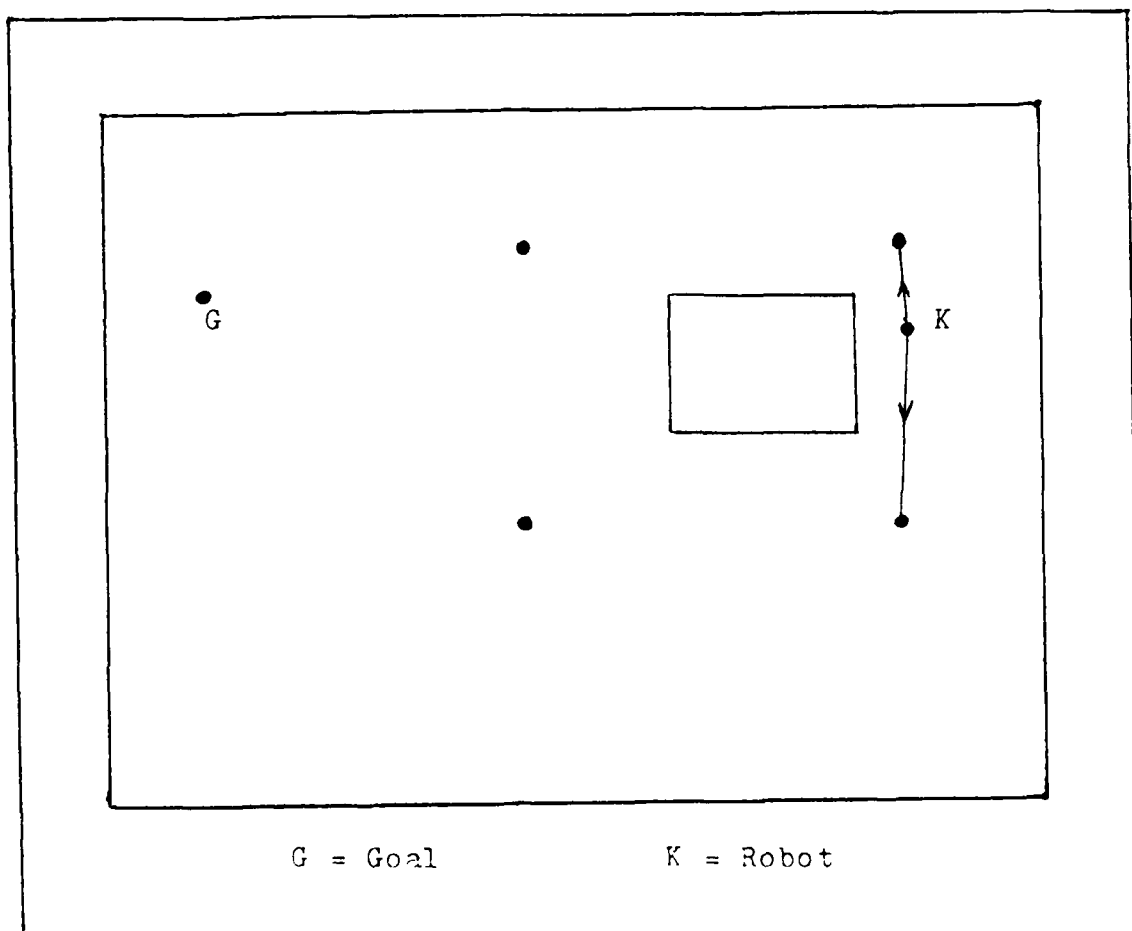


Figure 4.19 Two safe points can be reached through a direct path from the robots present position.

for intersections. No more tests are needed once the first intersection is found. Of course, if no intersections exist then the robot has a clear direct path. If an intersection is found, the robot must determine an indirect path.

To determine an indirect path to the goal point, the robot must perform a search through all the safe points and determine which ones he has direct access to. The parameter test is again used to eliminate the safe points with direct path obstructions. For our example (Figure 4.19), two safe

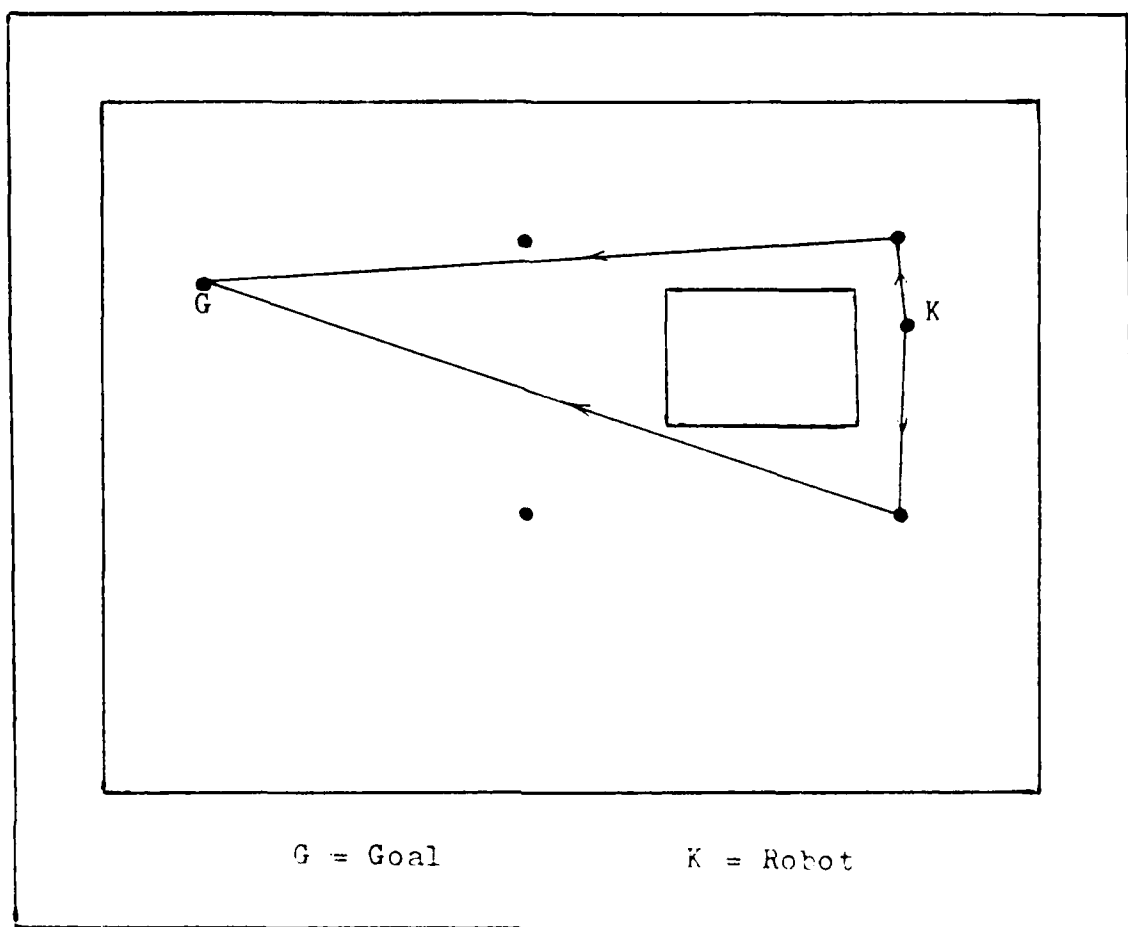


Figure 4.20. Two safe point paths lead to the goal.

points can be reached by a direct path from the robots present location. From each of these reachable safe points, a direct path to the goal is checked for obstacles (again using the parameter test). If no direct paths exist, another safe point must be found. For our example, this is not necessary since the goal can be reached directly from either safe point (see Figure 4.20). However, which path should be taken?

To select the "best" path among several possibilities,

an optimization test is performed. For each possible path, a cost function is maintained. The optimum path is the one with the lowest cost value. The cost function expression is as follows:

$$\begin{aligned} \text{COST} = & \left( \begin{matrix} X \\ K \end{matrix} - \begin{matrix} X \\ P_1 \end{matrix} \right)^2 + \left( \begin{matrix} Y \\ K \end{matrix} - \begin{matrix} Y \\ P_1 \end{matrix} \right)^2 + \left( \begin{matrix} X \\ P_1 \end{matrix} - \begin{matrix} X \\ P_2 \end{matrix} \right)^2 \\ & + \left( \begin{matrix} Y \\ P_1 \end{matrix} - \begin{matrix} Y \\ P_2 \end{matrix} \right)^2 + \dots + \left( \begin{matrix} X \\ P_{n-1} \end{matrix} - \begin{matrix} X \\ P_n \end{matrix} \right)^2 \\ & + \left( \begin{matrix} Y \\ P_{n-1} \end{matrix} - \begin{matrix} Y \\ P_n \end{matrix} \right)^2 + \left( \begin{matrix} X \\ P_n \end{matrix} - \begin{matrix} X \\ G \end{matrix} \right)^2 + \left( \begin{matrix} Y \\ P_n \end{matrix} - \begin{matrix} Y \\ G \end{matrix} \right)^2 \end{aligned}$$

where K = Starting Point  
P = Safe Point  
G = Goal  
n = number of safe points used

This cost function is merely the sum of the distances squared of each leg of the path. Thus, the optimum path is the shortest path.

### CONCLUSION

World modeling and path planning represent only a portion of the general robot navigation problem. However, their importance to the realization of an autonomous mobile robot system should not be taken lightly. Before a robot can begin to move, it must have some knowledge of its environment and it must be able to plan out a collision free route through its environment. This problem has received the recent attention of several researchers. Some of the current

techniques of world modeling have been presented along with a new approach. Path planning, under this new approach, consists of finding an unobstructed pathway to the goal point. Safe points are used only if a direct path does not exist. The details of this path planning have been developed through a simple example.

## V. Testing, Analysis, and Results

The testing of the GYRAC system was divided into three primary phases. The goal of each of these phases is listed below:

- Phase I. Verify the functionality of the GYRAC system.
- Phase II. Determine if the data from the GYRAC can be used to accurately track the location of the robot (MARRS-1) as it moves about the test area.
- Phase III. Demonstrate the capability of MARRS-1 to use GYRAC heading data to follow a programmed heading exercising closed loop steering control.

### Phase I

The primary thrust of this phase was to verify that every part of the GYRAC system operated properly. This turned out to be a tremendous task consuming a substantial portion of the allotted thesis time.

For Phase I testing, the GYRAC was connected to an H89 computer through an RS-232 interface and interrogated via M72 modem software. A logic state analyzer, and oscilloscope (see Appendix L) were used to troubleshoot the GYRAC hardware, firmware and verify correct operation of the GYRAC computer. Excluding the accelerometer subsystem, all hardware and software was eventually verified to function exactly as planned. The accelerometer subsystem could not be completely verified until subjected to motion. However, under static test several problems were encountered.

Output from the accelerometer integrator circuit was continually changing. Within a few minutes after power-up of the GYRAC system, the integrator output would become saturated. Operational amplifier (op amp) integrator circuits of this type, operating normally, eventually integrate into saturation under a constant input. However, the rate at which the output from the GYRAC integrator increased was much faster than anticipated. The input to the integrator (output from the accelerometer) was not constant, due to the extreme sensitivity of the accelerometer to movement, but it was very small (about 0.1mv). Such a small input should not cause saturation of the integrator so rapidly. An identical integrator circuit was breadboarded for testing.

The breadboarded integrator circuit was tested without an input (zero input voltage) and within a few minutes after power up it would integrate into saturation (just like the actual circuit). This was unexpected. After consulting with Analog Devices Corporation, it was discovered that the observed drift rate could be modeled mathematically through the following equation:

$$R = \frac{I_B}{C}$$

where  $R$  = drift rate  
       $I$  = current bias of operational amplifier  
       $B$   
       $C$  = capacitance of integrator feedback

It can be seen from the above equation that in order to decrease the drift rate, it is necessary to decrease the current bias of the op amp or increase the capacitance in the circuit, or both. The AD544 op amp (see Appendix A), manufactured by Analog Devices, was selected as a replacement due to its low current bias of 10 picoamps. Also, the integrator circuit was redesigned to contain a higher capacitance. Both a 200 microfarad and a 2000 microfarad capacitor were ordered. After obtaining the capacitors, they were measured for actual capacitance and resistors were chosen to achieve the appropriate gain for the integrator circuit. The 2000 microfarad capacitor was selected for installation into the GYRAC due to the very low drift rate achieved in the test circuit with this capacitor. The lowest possible drift rate was desired since the input signal to the integrator circuit is also very small.

After installation into the GYRAC, the accelerometer circuit was again tested. The results were much better than originally obtained. However, the output from the integrator was erratic and inconsistent. Through a process of elimination, another problem was found. The active CMOS switch used to reset the integrator (through software) was leaking current into the integrator circuit and charging the

capacitor thereby causing the inconsistent and erratic output. The switch is presently disconnected from the circuit and a manual reset of the integrator must be performed by physically shorting across the capacitor.

At the end of Phase I testing, the accelerometer subsystem appeared to be functioning correctly. The GYRAC system was ready for Phase II.

### Phase II

The objective of Phase II was to collect GYRAC heading and velocity data while the GYRAC was under motion and post process the data to determine the location of the robot (MARRS-1) in the test area. The computed location of the robot could then be compared with the actual location to test the performance of the GYRAC system.

For this phase of testing, the GYRAC was fully integrated with the MARRS-1 test bed. A memory overlay program, GTEST.A, was created to take advantage of firmware already operating inside the NAV computer. Clifford and Schneider had produced NAV computer firmware for collecting data from the various optical shaft encoders and sonars onboard the MARRS-1. [10:B-1] The overlay program replaces Clifford and Schneider routines for gathering sonar data with routines for gathering GYRAC data. See Appendix G for GTEST.A structure charts, program listing, and operating instructions.

All data are received through an H89 computer via M72



modem software and are then stored on floppy disk. The collected data are in exactly the same format as Clifford/Schneider data [10:IV-11] with the GYRAC data in place of the sonar data.

The raw GYRAC data is in hexadecimal format so an MBASIC program called CONVERT (see Appendix I for listing) was created to convert the raw data to integer format. The integer data is then used in another MBASIC program called POSITION (see Appendix I for listing) which computes the position of the robot in the test area based on the GYRAC heading and velocity data and a given initial position. See Appendix J for a sample output from the POSITION program. The computed position is in terms of a cartesian coordinate system centered in a corner of the test area as shown in Figure 5.1. The GYRAC is aligned such that heading is referenced to zero degrees along the x-axis and increases in the counter-clockwise direction, right handed system.

After several test runs with consistent but unusual results, the accelerometer subsystem was again suspect. The computed position of the robot indicated almost no movement, see Figure 5.2. The velocity levels gathered from the GYRAC were much too small. Eventually, it was discovered that the integrator circuit was loading the internal accelerometer restorer circuit (servo), see Figure 2.11. The result was a total changing of the characteristics of the accelerometer. The voltage sensitivity of the accelerometer, 2 volts/g, was

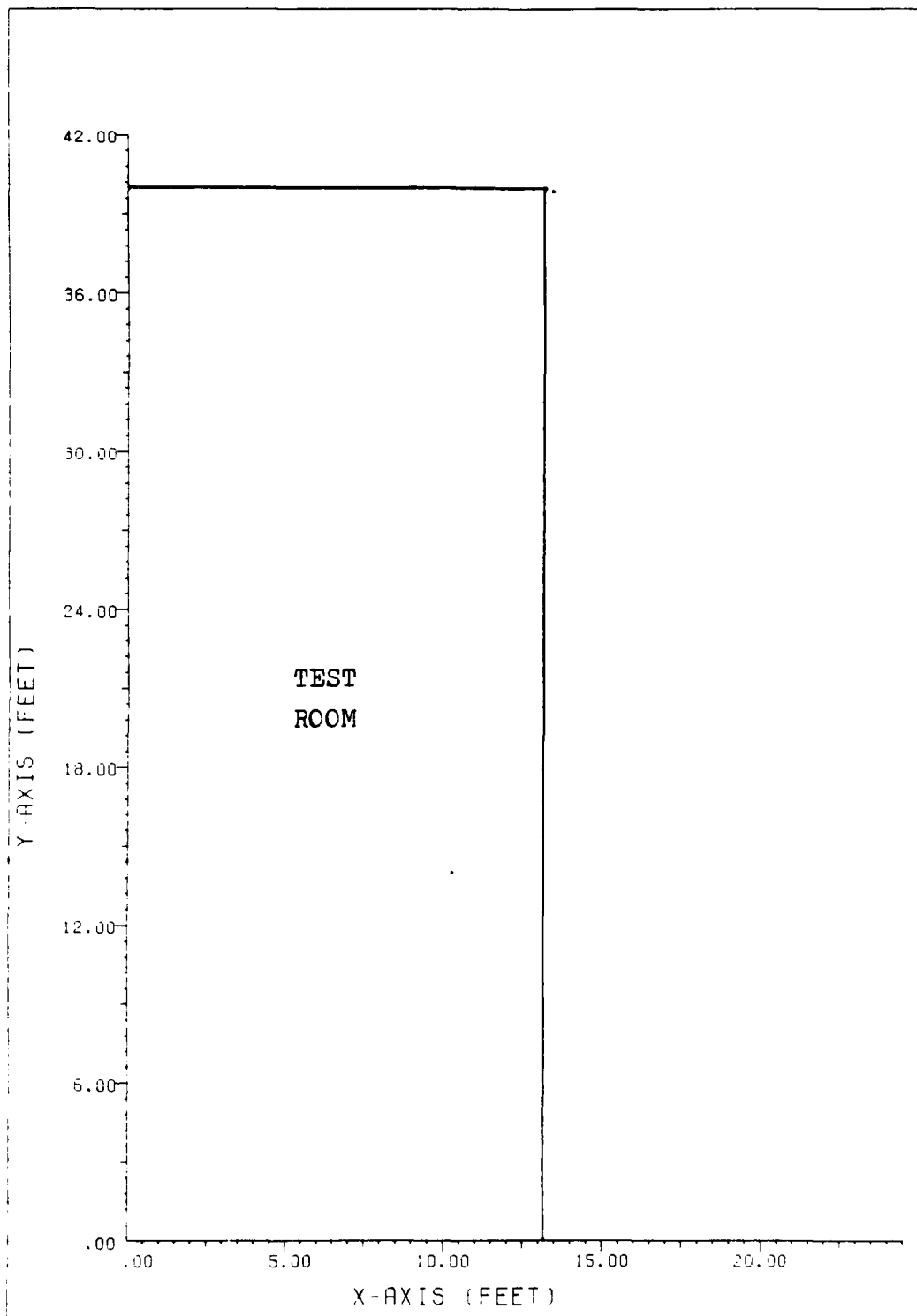


Figure 5.1. Cartesian coordinate system is centered in corner of test area.

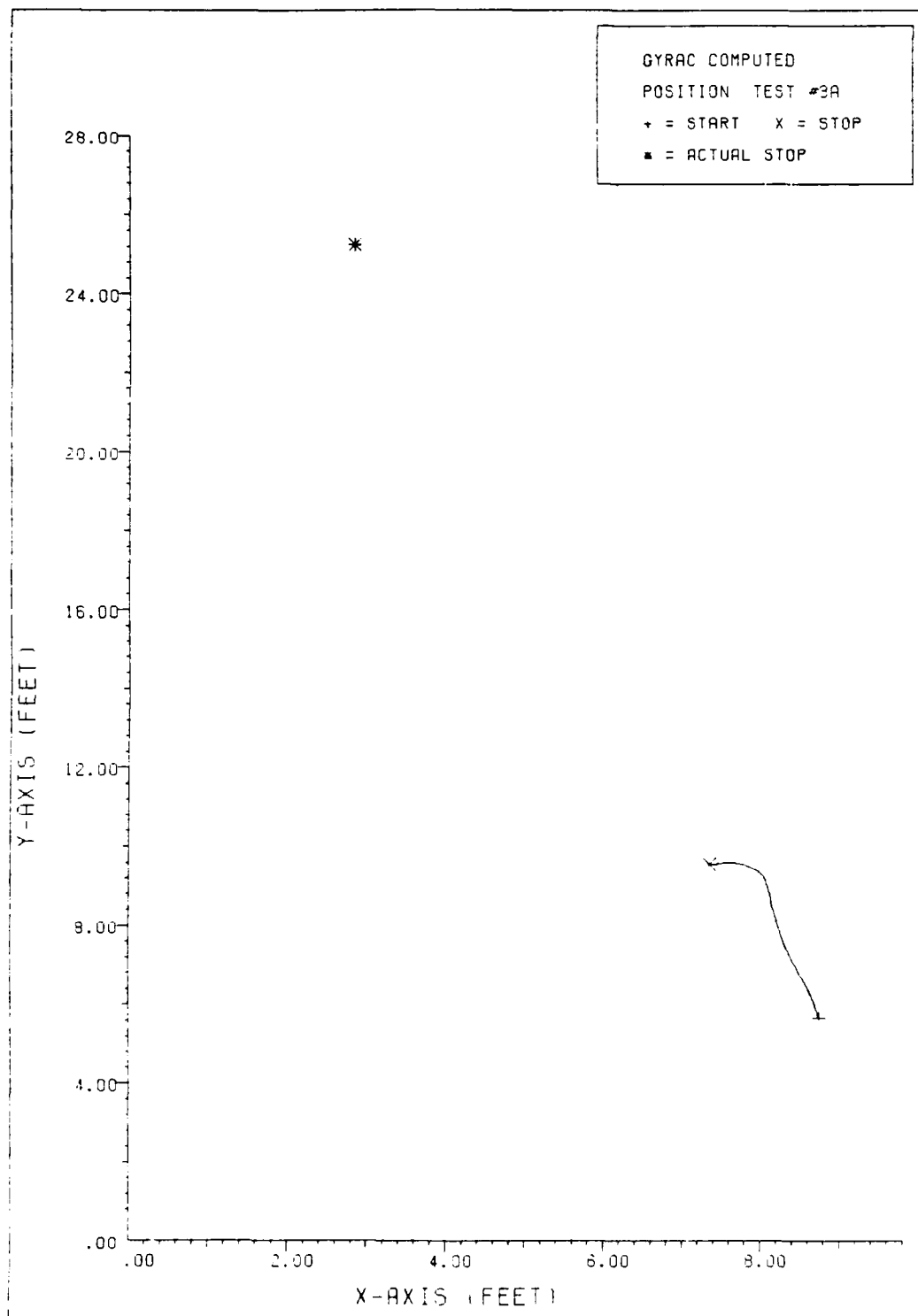


Figure 5.2. GYRAC computed position test using accelerometer sensitivity of  $2v/g$ .

no longer valid. A tumble test of the accelerometer was performed with the accelerometer completely connected to the the rest of the GYRAC, under full electrical load. The new voltage sensitivity was measured to be 0.393 volts/g instead of the 2 volts/g desired. This explained the low velocity levels. However, the accuracy of this newly measured sensitivity was questionable since the total loading effect of the integrator circuit could not be determined. The 0.393volts/g was measured at the load resistor  $R_L$  (see Figure 2.11). Using this new sensitivity, further testing resulted in computed positions that were in error on the high side. The computed location of the robot was always downrange from the actual location, see Figure 5.3. This indicated that the actual sensitivity of the accelerometer must be higher. An average sensitivity value of 0.6volts/g was obtained by comparing test runs using the 2v/g sensitivity with those using the 0.393v/g sensitivity. This 0.6v/g sensitivity resulted in computed positions much closer to the actual positions but still only with "ball park" accuracy, see Figure 5.4. In addition, the results were not consistent, sometimes high and sometimes low, almost random. Another problem had been around from the beginning; the output from the integrator (velocity) would not go back to zero after stopping MARRS-1. These problems indicated a possible error in sensed acceleration.

Several tests were performed with only the

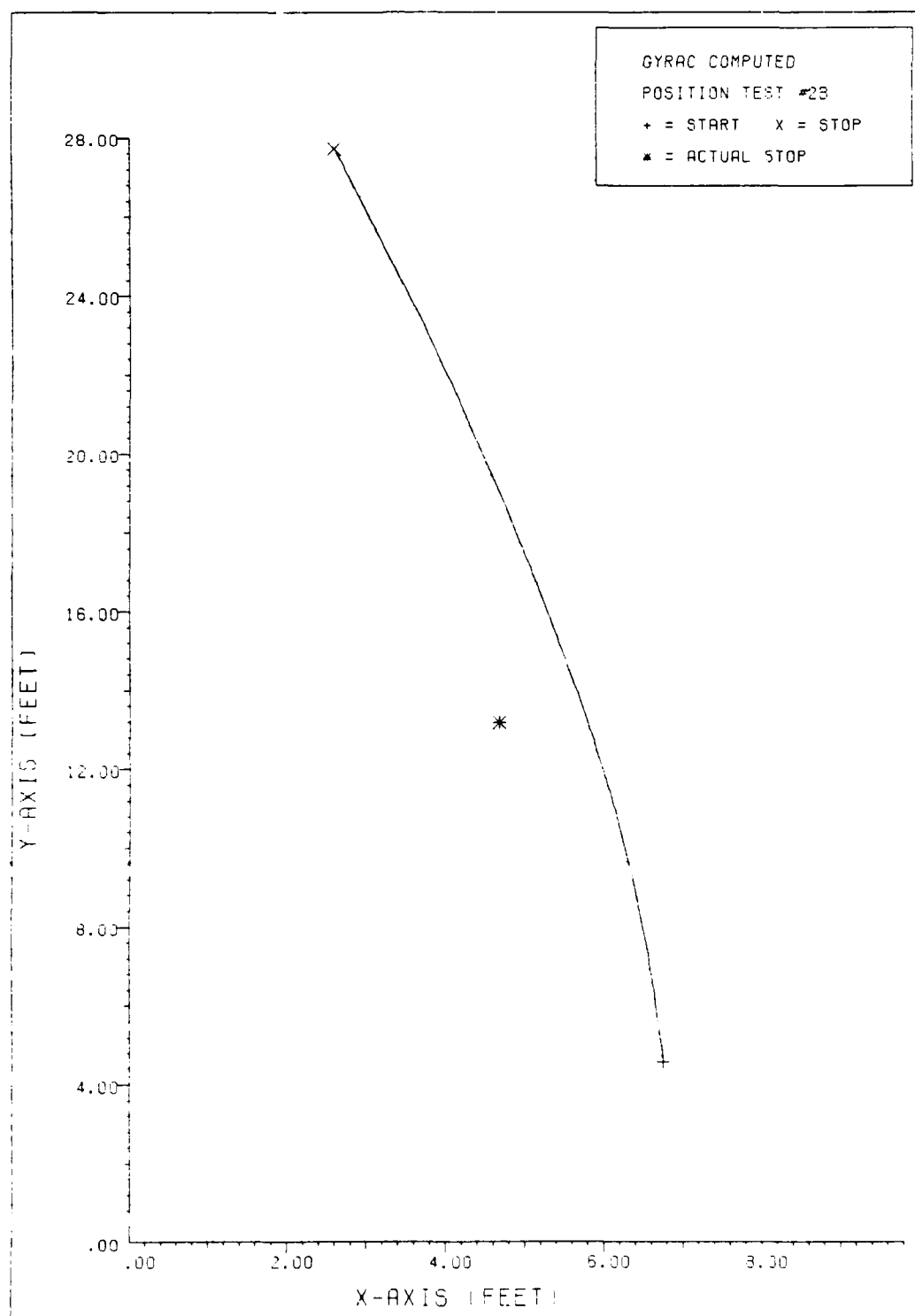


Figure 5.3. GYRAC computed position test using accelerometer sensitivity of  $0.393\text{v/g}$ .

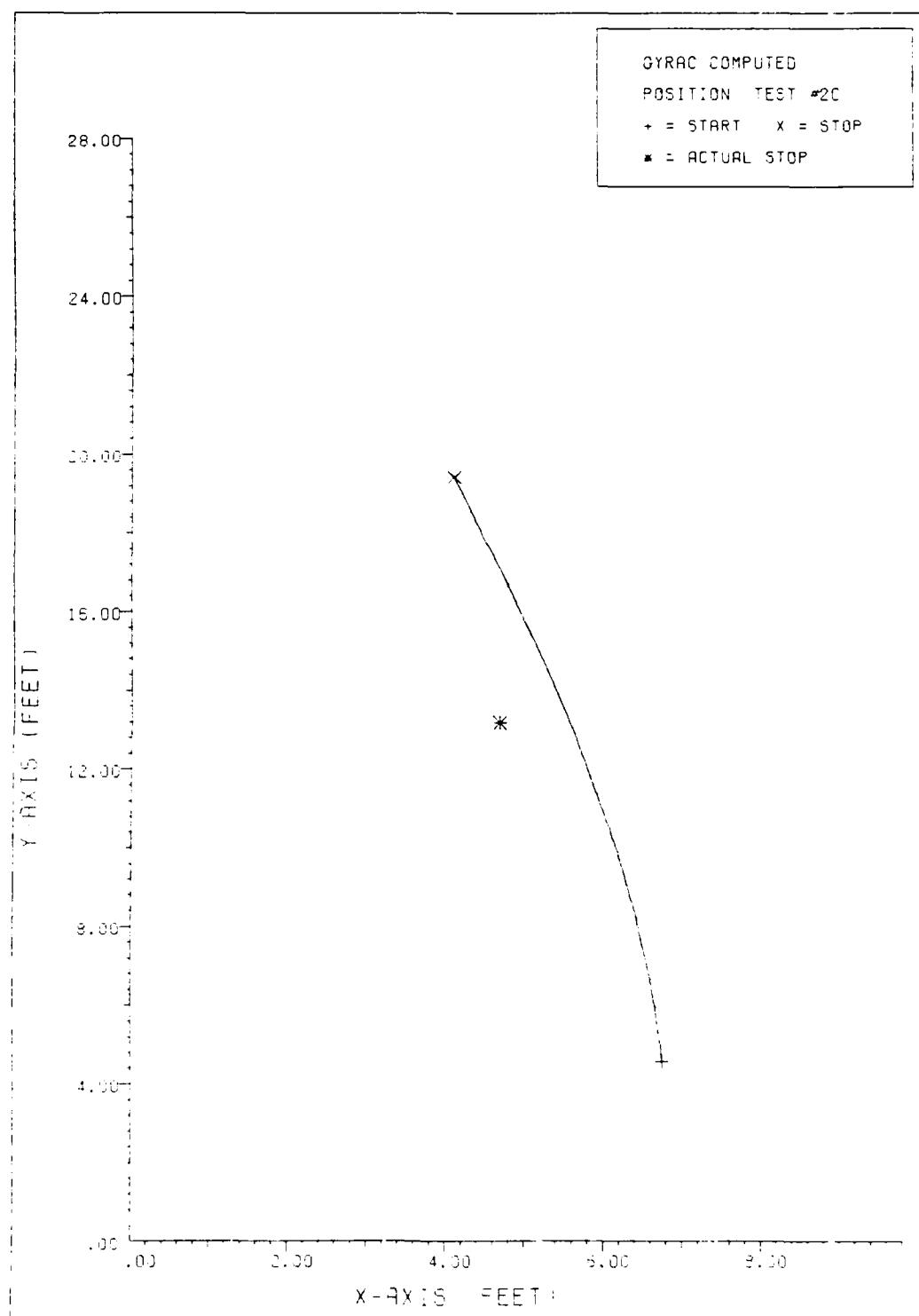


Figure 5.4. GYRAC computed position test using accelerometer sensitivity of 0.6v/g.

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GYRO AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A  
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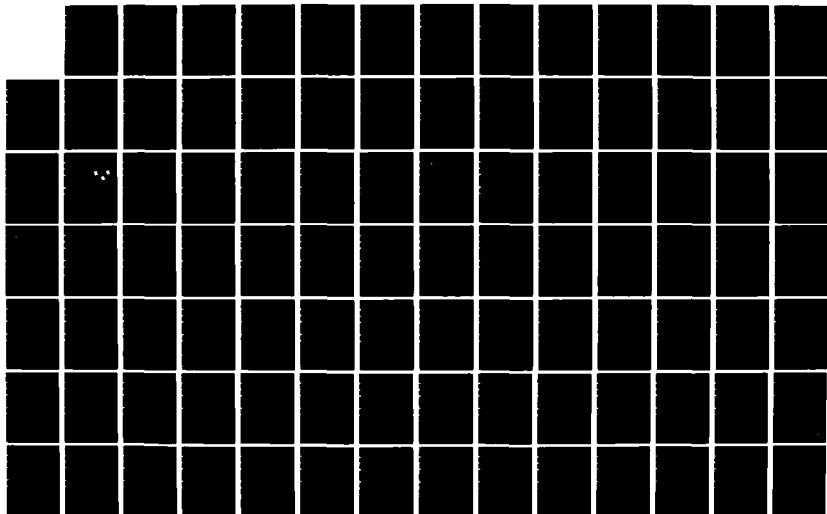
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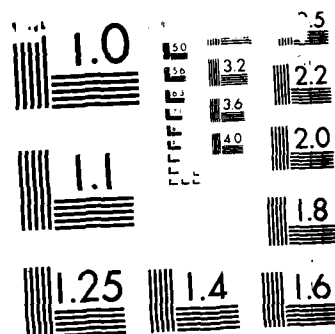
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A



accelerometer in the system. The integrator circuit was completely disconnected and the accelerometer output was connected to a gain circuit which was connected to the A/D converter. Pure acceleration data was obtained to determine the levels of acceleration achieved by the MARRS-1 under normal movement about the test area. These tests were very revealing. Figure 5.5 is a plot of acceleration vs time and illustrates the random nature of the sensed acceleration. It shows that the actual acceleration due to motion sensed by the GYRAC is on the same order of magnitude as the sensed acceleration due to tilt error (sensed gravity). In essence, the signal to noise ratio of the system is about one. The MARRS-1 moves at such a slow speed that the actual acceleration never gets much over the noise level. For example, in Figure 5.5, it is not obvious when the robot began movement and when it stopped. In Figure 5.5, the robot actually started forward movement at 2.3 seconds and was at a complete stop at 13.8 seconds. Thus, the acceleration data from the GYRAC and likewise the velocity data cannot be relied upon without some type of error compensation or a stable platform. The assumption of a perfectly smooth and level surface had been violated.

Due to the results from the acceleration tests, it was not necessary to continue Phase II testing. The accelerometer subsystem could never perform adequately without major modifications. Therefore, the third phase of

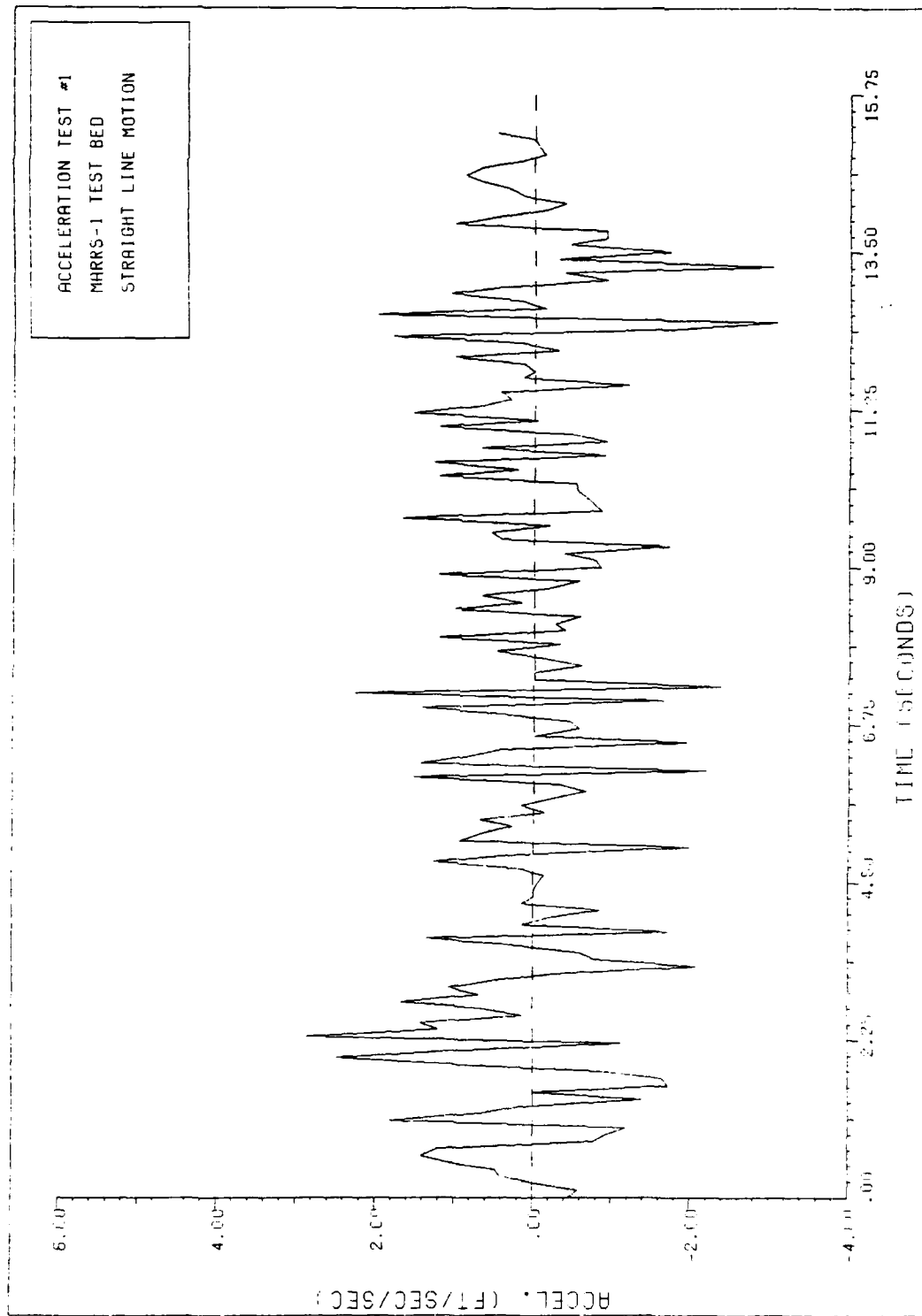


Figure 5.5 Acceleration Test #1.

testing was initiated since it did not require the use of the accelerometer subsystem.

### Phase III

The purpose of Phase III testing was to demonstrate the feasibility of using gyro heading data for closed loop control of the MARRS-1 steering motor. This effort produced a navigation program for the Nav computer that requests heading data from the GYRAC system and issues commands to a control program in the drive computer (see Appendix H for listings, structure charts, and operating instructions for both programs). The robot will rotate in place until locked on the specified heading. It then follows the given heading correcting for course errors as it moves until manually stopped. In addition, at each point where a course correction is considered the heading data is transmitted to an external computer for storage and off line analysis (see Appendix K).

Three problems surfaced during the design and testing of this system. First, a communication execution speed problem; second, a steering motor response problem; and third, a steering over correction problem.

Implementation of this system of navigation routines required communication between four different computers: the Nav, GYRAC, Drive, and external computers. The manner in which these communication links and interfaces were

implemented have a significant impact on the navigation performance.

The link between the GYRAC and the Nav computer is an RS-232 line operating at 9600 baud. As used in this application, one byte commands are issued by the Nav computer and two bytes of heading data are returned by the GYRAC computer. The communication programs at both ends of the link are written in assembly language to make the link perform efficiently and quickly. This link performed without error and did not significantly slow down the navigation process.

The link between the Nav computer and the external computer is very similar to the GYRAC-Nav computer link. It also performed well and did not slow down the navigation process.

However, the link between the Nav computer and the Drive computer, as implemented, slowed down the course correction process. this resulted in impaired navigation performance. Once again, a 9600 baud RS-232 link was used. However, communication over the link does not use single byte commands and is only driven by assembly language communication routines at the Nav computer end.

To simplify implementation, the decision was made to use the existing Drive computer communication interface and assembly language control routines for the steering and drive motors. The Nav computer controls the operation by

sending six bytes of data representing a jump to subroutine command and a specific memory address (ASCII format). Execution of these subroutines by the Drive computer controls the steering and drive motors. Unfortunately, the Drive computer communications software interface requires a small time delay between bytes of data. In addition, each Drive computer motor control subroutine executes a voice command, READY, before returning control of the system back to the communications routine. These two unnecessary time delays limit the Drive computer to at most one command per second which limits the rate at which course corrections can be made.

The command communication problem is further compounded by a slow steering motor response. The steering motor does not move instantly from one position to another. It takes as long as four to five seconds to move 180 degrees. In addition, once the wheel is turned to the desired angle it takes a finite amount of time for this change to produce a measurable course correction. Small changes in wheel direction can produce large changes in robot heading if given sufficient time for movement, but the robot will be off course for this entire time period.

The solution used to alleviate these problems is time delay. Time delays are executed for each steering command to allow the wheel sufficient time to move to the directed position. Small time delays were also added after each

course correction to allow time for the wheel direction change to take effect.

A steering over correction problem occurs when the steering wheel is turned for course corrections. The Nav computer is not able to straighten the steering wheel onto the correct heading before the robot has overshoot the desired course. This causes the robot to oscillate around the given course resulting in an unstable system where the overcorrections become increasingly large.

This problem has several causes. First, the gyro heading data is measured in increments of approximately 0.088 degrees, but the robot can not set a course to this accuracy since the steering stepper motor moves in one degree increments. Therefore, it must alternately switch between two adjacent steering stepper motor settings to follow most headings.

Second, due to irregularities in the floor and an unbalanced weight distribution of the robot platform over its wheels, the robot drifts from a "straight course" even if the steering wheel is locked in the center position.

Third, course corrections are made in one degree increments each time the heading is sampled and found to deviate from the desired course. If a large course correction must be made, many wheel turn commands will be issued causing a sharp wheel angle to be present when the desired heading is detected. The wheel can only be

straightened by many more wheel turn commands in the opposite direction. However, during this time the robot will continue moving in the wrong direction incurring a large overcorrection error.

The overcorrection problem was solved by defining a heading window formed by dropping the least significant four bits of the twelve bit heading reading. This makes the window approximately 1.5 degrees wide with the desired heading located on one of the sixteen possible headings inside the window (unfortunately not centered in the window). Any heading inside the window is defined to be the "correct course". The unstable oscillations are damped by moving the steering wheel to the center position (straight ahead) with a single command as soon as the edge of the heading window is detected. Detected headings within the heading window do not produce a course correction, but allow the robot to continue moving straight ahead (steering wheel centered).

Additional time delays have been provided after each course correction to allow small steering changes more time to take effect. This works well only if the robot begins its movement within or near the heading window. To insure that this always occurs, a rotate-robot-to-heading-window routine is executed before following the directed heading. This aligns the robot's heading within the heading window before forward motion is started.

Figure 5.6 graphically shows the heading data for a 33 foot robot run where the robot's initial heading was within the heading window. No rotation occurred since the initial heading was 88.15 degrees which is inside the heading window. The heading samples are not evenly distributed in time, but occur at course correction decision points. Notice that the robot still oscillates around the given heading, but the oscillations are damped making the navigation system stable. This figure also shows that few detected headings are in the heading window which produces many course corrections and therefore small oscillations around the window.

Figure 5.7 shows a 33 foot robot run where the initial heading was not within the heading window. An initial heading of 66.53 degrees is not shown on the graph since the robot rotated without forward motion to 88.15 degrees which is the first point shown in the figure. Notice that the rotate routine aligned the robot's heading within the heading window. Figure 5.7 also shows the course tracking accuracy that can be obtained when the navigation system "locks on" to a course inside the window.

As in the previous figure, Figure 5.8 does not show the initial heading of 112.67 degrees. The robot automatically aligned itself inside the heading window by rotating to a heading of 87.54 degrees. Notice that a large number of the heading points are again outside the window resulting in



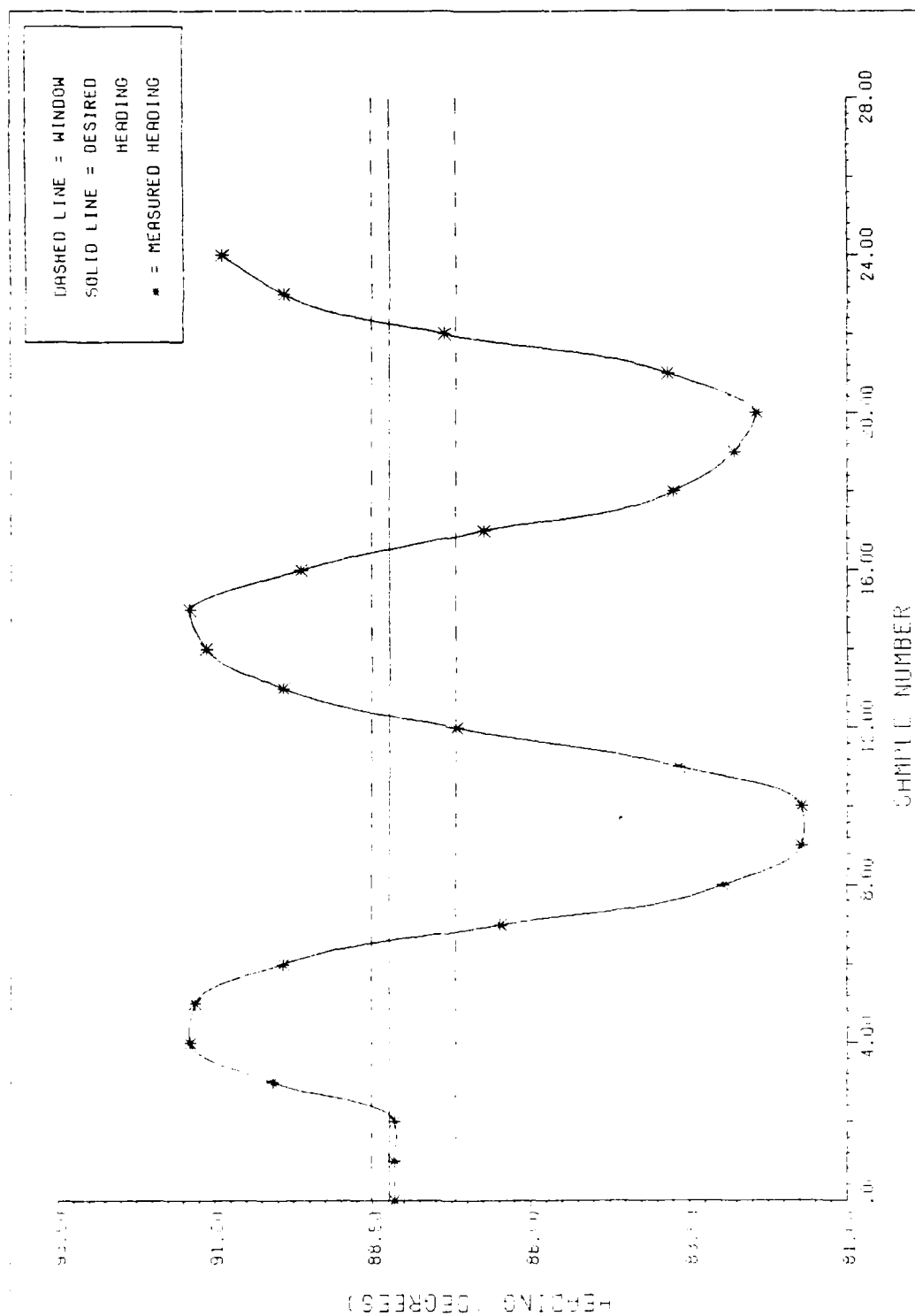


Figure 5.6. GYRAC Navigation Test #1, Automatic control of MARRS-1 Heading.

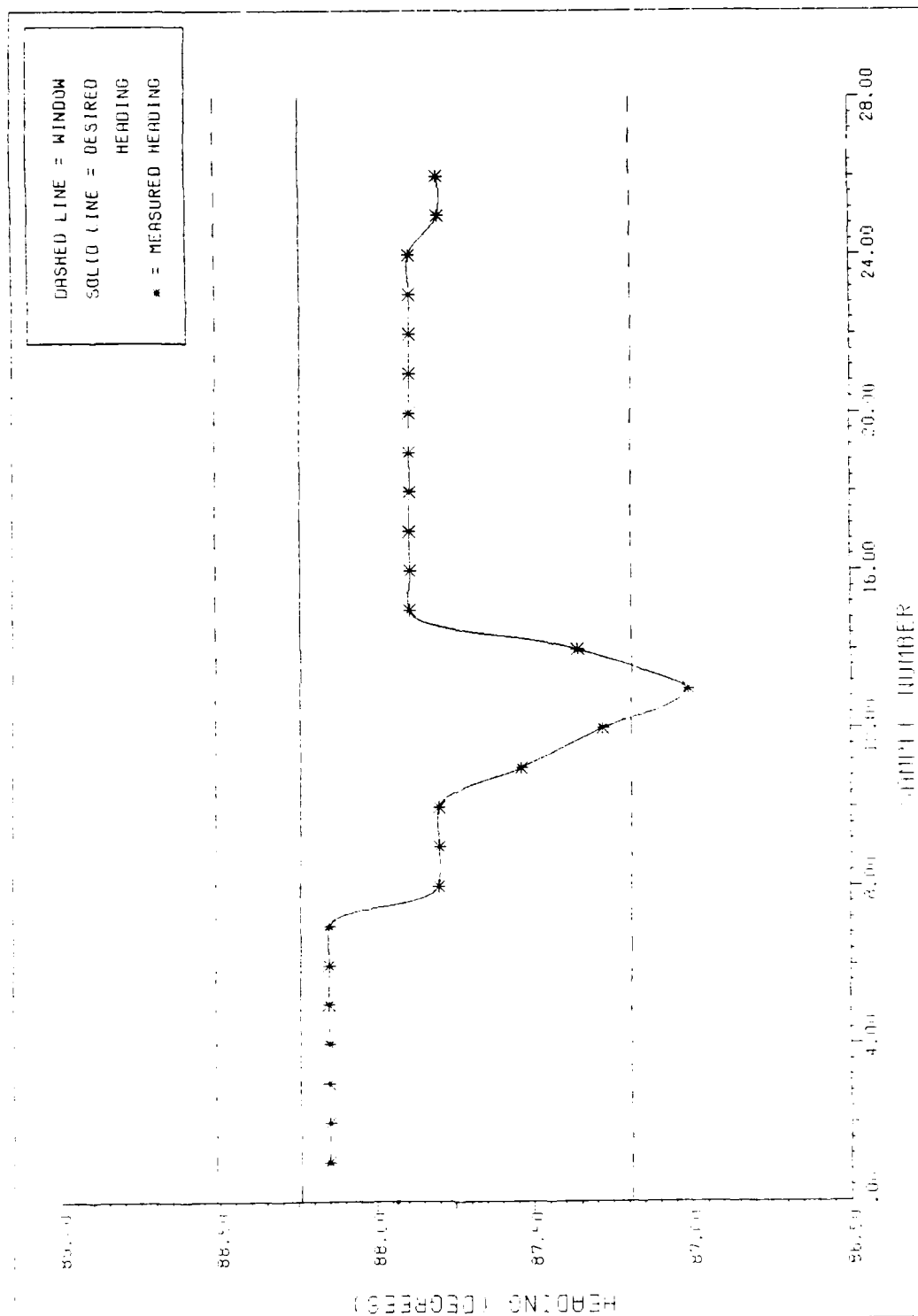


Figure 5.7. GYRAC Navigation Test #2, Automatic Control of MARRS-1 Heading.

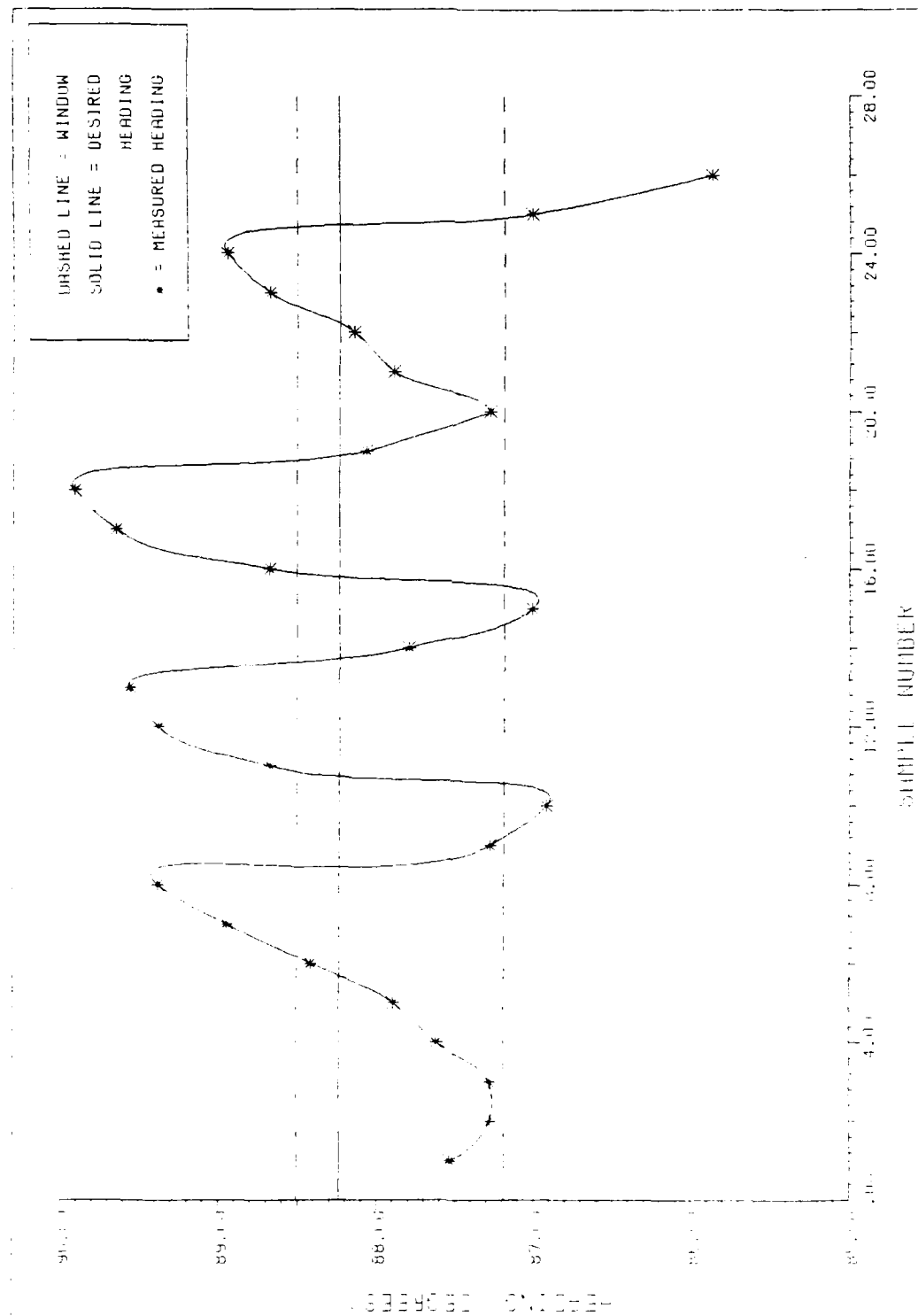


Figure 5.8. GYRAC Navigation Test #3, Automatic Control of MARRS-1 Heading.

course oscillation. However, the oscillations are not as severe as in Figure 5.6.

Careful study of all three figures indicate large oscillations occur when larger wheel angles (from the center position) are used. This causes frequent course changes to be executed because detected headings are not within the heading window. However, because course deviations oscillate around the actual course the mean course was very close to the desired course. The worst case oscillations resulted in movement of plus or minus five inches around the desired heading. No course drift was observed which is supported by a worst case final destination error of five inches. Therefore, feasibility of gyro based robot navigation has been demonstrated.

#### Review of Assumptions

The purpose of this section is to address the validity and impact of each assumption made in Chapter I and Chapter II.

Five governing assumptions were set forth in Chapter I. The first assumption, concerning local magnetic disturbances, proved to be valid. The magnetic flux detector was aligned only once and throughout the testing of the GYRAC, consistent heading information was obtained at all points in the test area.

The second assumption, that of a perfectly smooth and level operating surface, was the nemesis of this thesis. As

mentioned under Phase II testing, the effect of accelerometer tilt error was far greater than anticipated. As a result, the GYRAC velocity data can not be used for navigation.

The validity of the remaining three assumptions (a perfect integrator, constant velocity over sample period, and precisely known sample time), all dealing with the accelerometer subsystem, could not be determined due to the inaccuracy in sensed acceleration. The effect of each of these assumptions is expected to be small given an accurate acceleration measure.

In Chapter II, it was assumed that the bias and scale factor errors would be negligible. The effect of this assumption could not be determined. However, due to the very small acceleration levels involved with the movement of MARRS-1, the bias and scale factor errors could have a significant impact on the accuracy of the sensed acceleration. In this case, they would have to be compensated for.

#### Miscellaneous

The gyro base assembly, which serves as the power source for the entire GYRAC system, was noticed to get extremely warm during operation of the GYRAC. To avoid damage to the base assembly, a separate source of +5 volt power was instituted. A separate external power supply is

used to source the +5 volts and is provided through the same cable as is used for the system +28 volts external supply. This modification greatly reduced the load on the gyro base assembly and corrected the heating problem. The GYRAC power panel diagram in Appendix E has been updated to reflect this change.

## VI. Summary, Conclusions, and Recommendations

### Summary and Conclusions

The purpose of this thesis was to design and fabricate a real time, point to point, closed loop, mobile autonomous robot navigation system for the MARRS-1 robot. Specifically, the thesis was limited to three primary tasks. The first task was to develop the GYRAC system which would be capable of providing heading and velocity data. The second task was to integrate the GYRAC onto the MARRS-1 robot for verification testing, and the third task was to demonstrate autonomous navigation with the MARRS-1/GYRAC system.

Each of the these three parts was completed with the last task being completed to a limited extent. The GYRAC system is a complete and functional unit. However, the velocity data from the GYRAC is not usable for navigation. As mentioned in Chapter V, the true acceleration due to motion rarely, if ever, gets above the tilt error sensed by the accelerometer. This results in an ambiguous acceleration signal and thus an inaccurate velocity signal.

This problem has two major causes; the acceleration actually experienced by the MARRS-1 as it travels across the floor is very small in magnitude and short in duration; and, there is no error compensation in the accelerometer subsystem for gravity induced (tilt) errors. Nothing can be done about the small accelerations experienced by the

MARRS-1, since it is an inherently slow moving robot. Furthermore, speeding up the movement of MARRS-1 would not solve the problem since any flexible robot navigation system must be able to perform well at all reasonable speeds. This means that to make the GYRAC a completely usable system, a method of isolating the accelerometer from gravity tilt error must be incorporated. There are several methods for overcoming this tilt error problem. Several of these are presented in the Recommendations section.

The problems encountered with the accelerometer subsystem should not overshadow the success with the remainder of the GYRAC system. The GYRAC has proven to be a very reliable and accurate source of heading data. This heading data can be used by any robot system with an RS-232 serial interface. In addition, the heading data available from the GYRAC can be with respect to any reference direction and only one alignment along this reference is necessary. Subsequently, the GYRAC need only be powered up and will automatically provide accurate heading data with respect to the aligned reference. This GYRAC heading data could be combined with a separate source of distance measurement, such as wheel optical shaft encoders, to produce a viable navigation system. This could be accomplished on the MARRS-1 through software alone and is discussed further in the Recommendations section.

The GYRAC is completely integrated onto the MARRS-1 and



several tests of the integrated system have been completed verifying the compatibility of the two systems. Numerous software routines were produced allowing for communication between the MARRS-1 and the GYRAC and for data gathering and processing purposes. Complete detail of these programs can be found in Appendices G, H, and I.

The MARRS-1 is not yet capable of autonomous navigation, but a step was made toward that goal. The MARRS-1 can follow a given heading under self control of the steering stepper motor. MARRS-1 can be initially positioned at any heading and under self control it will rotate in place until it is aligned along a programmed heading, straighten out the front wheel, and begin forward movement making steering corrections as it travels in order to maintain its heading. Currently, the MARRS-1 will follow the programmed heading until manually stopped. With the addition of a distance measurement to the control algorithms, the MARRS-1 could be programmed to move autonomously about the test area.

Finally, the importance of robot world modelling and path planning to autonomous navigation should not be taken lightly. Before a robot can begin to move it must have some knowledge of its surroundings and it must be able to plan out collision free and efficient pathways through its environment. Some of the current techniques of world modelling have been presented along with a new approach.

Path planning, under this new approach consists of finding an unobstructed pathway to the goal point. Safe points are used only if a direct path does not exist. The details of this path planning have been developed through a simple example.

### Recommendations

There was not time to accomplish many of the goals optimistically set forth at the beginning of this thesis effort. In addition, throughout the development of the GYRAC system and while working with the MARRS-1 robot, many problems were identified too late to correct and many new ideas were conceived too late to implement. Therefore, the following recommendations are offered as possible extensions of, or improvements to, this thesis:

1. To correct the tilt error problem with the accelerometer subsystem in the GYRAC, some type of error compensation is necessary. For example, two or more accelerometers could be added to the system. These accelerometers would be perpendicular to each other and perpendicular to the existing accelerometer. By aligning one accelerometer along the vertical and the other along the horizontal (but perpendicular to the existing accelerometer), a signal could be generated which would be proportional to the amount of tilt experienced by the platform. This signal could be subtracted from the original

accelerometer signal; thereby, nulling out the tilt error. Perpendicular accelerometer pairs are commercially available through Sundstrand Data Control Incorporated and other manufacturers. In addition, due to the small amount of acceleration actually experienced by the MARRS-1, another single-axis accelerometer should be purchased with much greater sensitivity. This accelerometer would replace the current QA-1100 in the GYRAC. A full scale range of plus or minus one "g" would be sufficient (the QA-1100 has a range of plus or minus 13 "g's") and would result in accelerometer readings which would be less susceptible to bias and scale factor errors. Also, a new integrator circuit should be designed with a much higher impedance to avoid loading the accelerometer internal servo circuit. This is necessary so the sensitivity of the accelerometer will not be effected by the integrator circuit. The new integrator circuit must also be designed with drift rate in mind, as described in Chapter V under Phase I testing.

2. Another possibility for correcting the tilt error problem would be to incorporate a displacement gyro. This gyro could be used to sense small displacement angles of the accelerometer into the vertical. This displacement, or tilt angle, could be used to generate a signal proportional to the amount of accelerometer tilt. This signal could then be used to null out the tilt error.

3. The tilt error problem could also be corrected by

using a stable platform, such as those used in inertial navigation systems (INS), to mount the accelerometer. Only a single axis platform would be required to maintain the accelerometer input axis in the horizontal plane. Taking this suggestion even further, a complete INS could be incorporated on the MARRS-1 or another robot instead of the GYRAC. An INS would provide velocity and direction information sufficient for navigation.

4. The GYRAC heading data could be combined with an external source of displacement data, such as the wheel shaft encoder data on MARRS-1, to produce data suitable for position determination.

5. Tests need to be conducted to compare the accuracy of computing the position of MARRS-1 based on pure wheel shaft data with computed position based on both GYRAC heading and wheel shaft data.

6. More work is necessary to refine the control of the MARRS-1 allowing it to follow a given heading. Reasonably accurate navigation was observed using the relatively simple approached outlined in Chapter V. However, several improvements can be made that should greatly improve performance.

First, the drive computer control programs and communication software should be rewritten in assembly language using single byte ASCII commands. This will eliminate command and communication time delays allowing

faster steering response (hundreds per second as opposed to one per second). This would also allow the heading window to be narrowed which would help reduce oscillations.

This change also requires the command routines of the Nav program to be changed, but nav.a (see Appendix H) has been designed in a three level structure to make changes and additions easy. The bottom level consists of hardware and device dependent routines such as transmit a byte of data to the Drive computer. The middle level of intermediate routines uses the lower level routines to define function primitives such as turn on drive motor at high speed. The top level of commands use the function primitives to form navigation commands such as rotate until locked on the heading window. Therefore, each level is independent of the way lower levels are implemented which limits the effects of changes to within a module.

Second, more intelligent steering control routines should be developed. They should anticipate when to start straightening out the front wheel instead of trying to do it all at once as was done in this thesis. In addition, they should be able to move the steering wheel in increments proportional to the amount of correction needed as opposed to single degree increments per correction. These additions will flatten out the oscillations and provide better navigation accuracy.

7. Once an accurate method of position determination

and of controlling the MARRS-1 is verified, the next step would be to develop the math routines necessary for MARRS-1 to perform the onboard processing required for navigation. The full world model as described in Chapter IV could then be implimented to provide the MARRS-1 with path planning capability.

### Bibliography

1. 006-0111-05. KCS 55/55A Pictorial Navigation System. Installation Manual, King Radio Corporation, Olathe, Kansas, November 1981.
2. 006-5111-05. KI 525 Pictorial Navigation Indicator. Maintenance/Overhaul Manual. King Radio Corporation, Olathe, Kansas, March 1984.
3. 006-5111-05. KG 102 Directional Gyro. Maintenance/Overhaul Manual. King Radio Corporation, Olathe, Kansas, March 1984.
4. 006-5111-05. KMT 112 Magnetic Aximuth Transmitter. Maintenance/Overhaul Manual. King Radio Corporation, Olathe, Kansas, March 1984.
5. 006-5111-05. KA 51Blaving Accessory. Maintenance/Overhaul Manual. King Radio Corporation, Olathe, Kansas, March 1984.
6. 006-8250-04 20K. King KCS 55A Silver Crown Compass System. Specification Sheet. King Radio Corporation, Olathe, Kansas, April 1979.
7. 012-0293-001. Q-Flex Accelerometers. Instruction Manual. Sundstrand Data Control Incorporated, Redmond, Washington, January 1878.
8. Bloom, Capt Roland J., Dyer, Capt Donald D. and Capt Fred Williams. "Lab #3." Laboratory Report. Wright Patterson AFB, OH: EE 6.44, School of Engineering, Air Force Institute of Technology, March 1985.
9. Bortz, A.B. "Moravec's Mobile Robots," Robotics Age, 6: 25-31 (September 1984).
10. Clifford, T. and H. Schneider. Creating a Mobile Autonomous Robot Research System (MARRS). MS thesis. Wright-Patterson AFB, OH: School of Engineering, Air Force Institute of Technology, December 1984. (AFIT/GE/ENG/84D-19)
11. Coleman, Arthur. "Robotics Research: The Next Five Years and Beyond," Robotics Age, 7: 14-19 (Februrary 1985).
12. Crowley, James I. "Navigation for an Intelligent Mobile Robot," IEEE Journal of Robotics and Automation, 1: 31-41 (March 1985).

13. Ebisch, Robert. "Metal Warriors," The Computer & Electronics Graduate, 2: 45-48 (Spring 1985).
14. General Officer Steering Committee for Artificial Intelligence and Robotics. Draft Summary of TRADOC Requirements for Generic Robot Vehicle Systems. 9 April 1985.
15. Lozano-Perez, T. and M. A. Wesley. "An Algorithm for Planning Collision-free Paths Among Polyhedral Obstacles," Communications of the ACM, 22 (10): 560-570 (October 1979).
16. Monaghan, Capt Glen E. Navigation for an Autonomous Mobile Robot. MS thesis. Wright-Patterson AFB, OH: School of Engineering, Air Force Institute of Technology, December 1984. (AFIT/GE/ENG/84D-47)
17. Moravec, Hans P. "The Stanford Cart and the CMU Rover," Proceedings of the IEEE, 71: 872-884. IEEE Press, New York, 1983.
18. O'Donogue, Val. Syncro & Resolver Conversion. Memory Devices Ltd., Surrey, United Kingdom, 1980.
19. Owen, R.J. Environmental Mapping by a Hero-1 Robot Using Sonar and Laser Barcode Scanner. MS thesis. Wright-Patterson AFB, OH: School of Engineering, Air Force Institute of Technology, December 1983. (AFIT/GE/EE/83D-52)
20. Q-Flex Servo Accelerometers. Brochure. Sundstrand Data Control, Incorporated, Redmond Washington, 1978.
21. Tice, Jim. "Autonomous Vehicles Ready for Intelligent Applications," Air Force Times: 18 (29 July 1985).



Vita

Captain Roland J. Bloom was born on 2 December 1958 in Grants, New Mexico. After graduating from White Pine High School, Ely, Nevada in 1977 he entered the United States Air Force Academy in Colorado Springs, Colorado.

Upon graduation from the Academy in May 1981, he received the degree of Bachelor of Science in Astronautical Engineering and was commissioned as a Regular Second Lieutenant of the United States Air Force.

He was assigned to the Peacekeeper Division of the 6595th Missile Test Group at Vandenberg AFB, California. While at Vandenberg AFB, Captain Bloom served as primary Test Controller for the assembly, check-out, and launch preparation of the first four Peacekeeper flight-test missiles.

In May 1984, he entered the Masters's program in Astronautical Engineering at the Air Force Institute of Technology.

Captain Bloom is married to the former Raylene A. Burgess of East Ely, Nevada. They have two children: Jessica and Brandon.

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### Vita

Captain William J. Ramey Jr. was born December 25, 1952 in Great Falls, Montana. He graduated as class Valedictorian in 1971 from Jefferson High School, Boulder, Montana and later that year attended Montana State University. He enlisted in the Air Force in 1974 and became an Honor Graduate of the Cryptographic Equipment Maintenance School at Lackland AFB, Texas, where he was later assigned as an Instructor. He attended San Antonio College pursuing a degree in Electrical Engineering. In 1977, he was selected for the Airman Education and Commissioning Program and attended Texas A&M University where he received a Bachelor of Science degree in Electrical Engineering in 1979. In 1980, he graduated as a Distinguished Graduate from Officer Training School. Upon graduation, he was assigned to the National Security Agency (NSA) as a Computer Engineer and was later certified by NSA as a Senior Cryptologic Engineer. He attended the University of Maryland pursuing a Masters degree in Electrical Engineering. In 1984, Captain Ramey began a Masters program in Electrical Engineering at the Air Force Institute of Technology, Wright Patterson AFB, Ohio.

Captain Ramey is married to the former Elizabeth A. West of Farmingdale, New York. They have three children: Matthew, Joshua, and Katherine.

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## APPENDIX A

SDC 1700 S/D Converter Data Sheet .....	A-2
AD573 A/D Converter Data Sheet .....	A-8
AD544 Operational Amplifier Data Sheet .....	A-15

## SDC 1700 S/D Converter Data Sheet



# Low Profile Synchro/Resolver-to-Digital Converter

## SDC1700/1702/1704 SERIES

### FEATURES

Internal Microtransformers for 60Hz, 400Hz and 2.6kHz

#### References

Low Profile (0.4")

10-, 12- or 14-Bit Resolution for 360°

High Tracking Rates (75 revs/sec)

Voltage Scaling with External Resistors (Unique Feature)

DC Voltage Output Proportional to Angular Velocity

Low Cost

Lightweight 3oz. (85 grams)

MIL Spec/Hi Rel Options Available

### APPLICATIONS

Servo Mechanisms

Retransmission Systems

Coordinate Conversion

Antenna Monitoring

Simulation

Industrial Controls

Fire Control Systems

Machine Tool Control Systems

### GENERAL DESCRIPTION

The SDC1700, SDC1702 and SDC1704 are modular, continuous tracking Synchro/Resolver-to-Digital Converters which employ a type 2 servo loop.

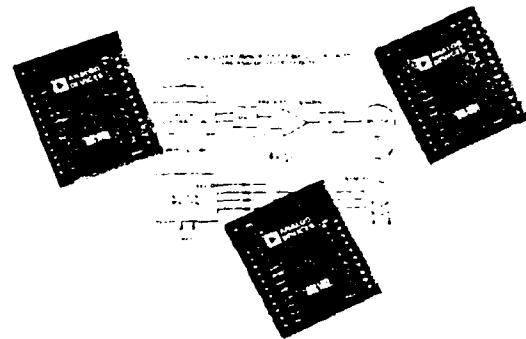
They are intended for use in both Industrial and Military applications.

The input signals can be either 3 wire synchro plus reference or 4 wire resolver plus reference, depending on the option. The outputs will be presented in TTL compatible, parallel natural binary.

One of the outstanding features of the converters is the use of precision Scott T and reference microtransformers. This has made it possible to include the transformers within the module, even on the 60Hz option, and yet still maintain the profile height of 0.4"

Particular attention has been paid in the design, to achieving the highest tracking rates and accelerations possible, compatible with the resolution and carrier frequency used, while at the same time obtaining a high overall accuracy.

When SDC's are used in control loops, it is often useful to have a voltage which is proportional to angular velocity. This voltage is available and has been brought out on all the SDC1700 converters.



Extended temperature range versions of all the converters are available.

### MODELS AVAILABLE

The three Synchro-to-Digital Converters described in this data sheet differ primarily in the areas of resolution, accuracy and dynamic performance as follows:

Model SDC1702XYZ is a 10-bit converter which has an overall accuracy of  $\pm 22$  arc-minutes and a resolution of 21 arc-minutes.

Model SDC1700XYZ is a 12-bit converter with an overall accuracy of  $\pm 8.5$  arc-minutes and a resolution of 5.3 arc-minutes.

Model SDC1704XYZ is a 14-bit converter with an overall accuracy of  $\pm 2.2$  arc-minutes  $\pm 1$ LSB and a resolution of 1.3 arc-minutes.

The XYZ code defines the option thus: (X) signifies the operating temperature range, (Y) signifies the reference frequency, (Z) signifies the input voltage and range, and whether it will accept synchro or resolver format.

More information about the option code is given under the heading of "Ordering Information".

#### NOTE:

For all the standard options, no external transformers are needed with these converters.

# SDC 1700 S/D Converter Data Sheet (continued)

## SPECIFICATIONS (typical @ +25°C unless otherwise noted)

MODELS	SDC1702	SDC1700	SDC1704
ACCURACY <sup>1</sup> (max error)			
50Hz	±22 arc minutes	±8.5 arc minutes	±2.2 arc minutes ±1LSB
400Hz	±22 arc minutes	±8.5 arc minutes	±2.2 arc minutes ±1LSB
2 kHz	±22 arc minutes	±8.5 arc minutes	±2.2 arc minutes ±1LSB
RESOLUTION	10 Bits (1LSB = 21 arc mins)	12 Bits (1LSB = 5.3 arc mins)	14 Bits (1LSB = 1.3 arc mins)
OUTPUT (in Parallel)	10 Bits (Natural Binary)	12 Bits (Natural Binary)	14 Bits (Natural Binary)
SIGNAL AND REFERENCE FREQUENCY	50Hz, 400Hz, 2 kHz	*	*
SIGNAL VOLTAGE (Line-to-Line)			
Low Level	11.8V rms	*	*
High Level	90V rms	*	*
SIGNAL IMPEDANCES			
Low Level	20kΩ (Resistive)	*	*
High Level	200kΩ (Resistive)	*	*
REFERENCE VOLTAGE			
Low Level	26V (11.8V Signal)	*	*
High Level	115V (90V Signal)	*	*
REFERENCE IMPEDANCE			
	270kΩ (115V Signal)	*	*
	56kΩ (26V Reference)	*	*
	(Impedance is Resistive)	*	*
TRANSFORMER ISOLATION	500V dc	*	*
TRACKING RATE (min)			
50Hz	5 Revolutions Per Second	*	500 <sup>2</sup> sec
400Hz	30 Revolutions Per Second	*	12 Revolutions Per Second
2 kHz	75 Revolutions Per Second	*	25 Revolutions Per Second
Accel <sup>2</sup>			
Constant K <sub>A</sub>			
50Hz	1980/sec <sup>2</sup>	*	520/sec <sup>2</sup>
400Hz	110,000/sec <sup>2</sup>	*	30,000/sec <sup>2</sup>
2 kHz	518,000/sec <sup>2</sup>	*	170,000/sec <sup>2</sup>
STEP RESPONSE (179° Step) (For 1LSB Error)			
50Hz	1.5sec	*	*
400Hz	125ms	*	*
2 kHz	50ms	*	*
POWER LINES	±15V @ 25mA ±5% -5V @ 20mA	*	±15V @ 30mA ±5% -5V @ 85mA
POWER DISSIPATION	1.1 Watts	*	1.3 Watts
DATA LOGIC OUTPUT <sup>3</sup> (TTL Compatible)	2 TTL Loads SDC17026VZ 4 TTL Loads SDC17025VZ	2 TTL Loads SDC17006VZ 4 TTL Loads SDC17005VZ	2 TTL Loads on All Options
BUSY LOGIC OUTPUT POSITIVE PULSE (1 TTL Load)			
50Hz	9.0μs	*	9.0μs
400Hz	2.0μs	*	2.0μs
2 kHz	2.0μs	*	1.5μs
MAX DATA TRANSFER TIME			
50Hz	40μs	*	15μs
400Hz	5.0μs	*	1.0μs
2 kHz	1.8μs	*	0.8μs
INHIBIT INPUT (For Inhibit)	Logic 0 <sup>4</sup> (1 TTL Load)	*	Logic 0 <sup>4</sup> (2 TTL Loads)
WARM UP TIME	1 sec to Rated Accuracy	*	*
TEMPERATURE RANGE			
Operating	0 to +70°C Standard -55 to +125°C Extended	*	*
Storage	-55 to +125°C	*	*
DIMENSIONS	0.125" x 2.025" x 0.4"	*	*
	7.4 x 51.8 x 10.2mm	*	*
WEIGHT	1.05 g (0.5 ounce)	*	*

### NOTES

<sup>1</sup> Accuracy same as SDC1702

<sup>2</sup> Test over the appropriate operating temperature range of the option and for 40% rms signal and reference amplitude variation, 50% rms signal and reference harmonic distortion, 0.15% power supply variation and 10% variation in reference frequency.

<sup>3</sup> It is recommended that buffers should be used if the above converters

are required to drive over a distance greater than 6'

<sup>4</sup> The output is correct over the range without notice.

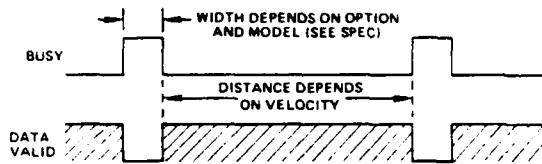
## SDC 1700 S/D Converter Data Sheet (continued)

### DATA TRANSFER (All Models)

The readiness of the converters for data transfer is indicated by the state of the BUSY pin.

The voltage appearing on the BUSY pin consists of a train of pulses, at TTL levels, of length according to the model and option (see specification table). The converter is busy when the BUSY pin is at a TTL "High" level. These pulses correspond to those delivered by the VCO to increment or decrement the up-down counter (see schematic diagram). Thus the pulses will occur for increasing and decreasing counts.

The most suitable time for transferring data is when the BUSY is at a logic "Lo" state, and the times allowable for data transfer are shown in the specification. Even at the maximum speed of the option, these times will be sufficient to transfer data before the next BUSY pulse occurs.



Data Transfer Diagram

### DATA TRANSFER DIAGRAM

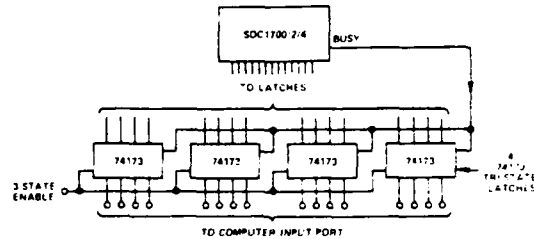
Taking the INHIBIT to a logic "Lo" state prevents the VCO (BUSY) pulses from updating the up-down counter. However, if applied during a BUSY pulse, the INHIBIT will not become effective until the end of the BUSY pulse.

The best method of transferring the data is by applying the INHIBIT (taking it to a logic "Lo" state), waiting for at least the width of a BUSY pulse, transferring the data and releasing the INHIBIT.

Note that sustained application of the INHIBIT opens the internal control loop and the converter may take on appreciable time to recover to full accuracy when the loop is restored.

### INTERFACING WITH A COMPUTER

It is recommended that external latches are used to enable data to be transferred onto a computer data bus. One method is shown in the diagram. Using this method will mean that the latches are constantly updated by the BUSY signal, while at the same time enabling inputs to be made to the computer by means of normal data transfer procedures. The AC1755 mounting card contains these external components.



Suggested External Computer Interface Circuitry

### THEORY OF OPERATION

If the unit is a Synchro-to-Digital Converter, then the 3 wire synchro output will be connected to S1, S2 and S3 on the module and the Scott T transformer pair will convert these signals into resolver format.

$$\begin{aligned} \text{i.e., } V_1 &= K E_0 \sin \omega t \sin \theta \\ V_2 &= K E_0 \sin \omega t \cos \theta \end{aligned}$$

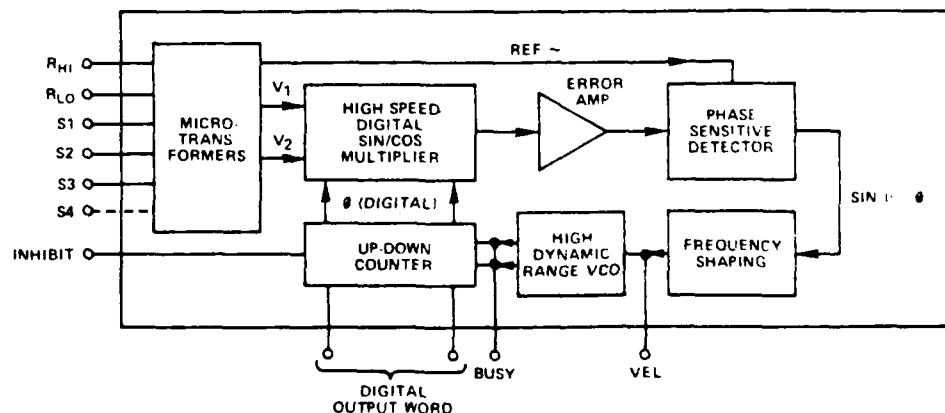
Where  $\theta$  is the angle of the Synchro Shaft

If the unit is a Resolver-to-Digital Converter, then the 4 wire resolver output will be connected to S1, S2, S3 and S4 on the module and the microtransformer will act purely as an isolator.

To understand the conversion process, then assume that the current word state of the up-down counter is  $\phi$

The  $V_1$  is multiplied by  $\cos \phi$  and  $V_2$  is multiplied by  $\sin \phi$  to give

$$\begin{aligned} &K E_0 \sin \omega t \sin \theta \cos \phi \\ \text{and } &K E_0 \sin \omega t \cos \theta \sin \phi \end{aligned}$$



Functional Diagram of the SDC1700.2/4 Converters

## SDC 1700 S/D Converter Data Sheet (continued)

These signals are subtracted by the error amplifier to give:

$$K E_O \sin \omega t (\sin \theta \cos \phi + \cos \theta \sin \phi) \\ \text{or } K E_O \sin \omega t \sin (\theta - \phi)$$

A phase sensitive detector, integrator and Voltage Controlled Oscillator (VCO) form a closed loop system which seeks to null  $\sin (\theta - \phi)$ .

When this is accomplished, the word state of the up-down counter ( $\phi$ ), equals within the rated accuracy of the converter, the synchro shaft angle  $\theta$ .

### CONNECTING THE CONVERTER

The electrical connections to the converter are straightforward. The power lines, which must not be reversed, are  $\pm 15V$  and  $5V$ . They must be connected to the " $\pm 15V$ " and " $5V$ " pins with the common connection to the ground pin GND.

It is suggested that  $0.1\mu F$  and  $0.8\mu F$  capacitors be placed in parallel from  $+15V$  to GND, from  $-15V$  to GND and from  $+5V$  to GND.

The digital output is taken from pins:

- 1 through 10 for the SDC1702
- 1 through 12 for the SDC1700
- 1 through 14 for the SDC1704

Pin 1 represents the MSB in each case. The reference connections are made to pins " $R_{HI}$ " and " $R_{LO}$ ".

In the case of a Synchro, the signals are connected to " $S1$ ", " $S2$ " and " $S3$ " according to the following convention:

$$E_{S1 - S3} = E_{RLO} - R_{HI} \sin \omega t \sin \theta \\ E_{S3 - S2} = E_{RLO} - R_{HI} \sin \omega t \sin (\theta + 120^\circ) \\ E_{S2 - S1} = E_{RLO} - R_{HI} \sin \omega t \sin (\theta + 240^\circ)$$

For a resolver, the signals are connected to " $S1$ ", " $S2$ ", " $S3$ " and " $S4$ " according to the following convention:

$$E_{S1 - S3} = E_{RLO} - R_{HI} \sin \omega t \sin \theta \\ E_{S2 - S4} = E_{RHI} - R_{LO} \sin \omega t \cos \theta$$

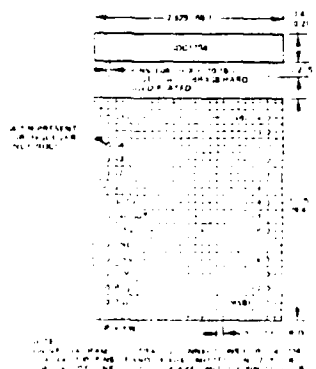
The analog voltage representing velocity is available between " $VEL$ " and " $GND$ ".

The " $BCSY$ " and " $INHIBIT$ " pin (if used), should be connected as described under the heading "Data Transfer".

NOTE: If the INHIBIT pin is used (i.e., driven to 0 volts), the control loop will be opened and a finite time will be required (see spec) for the converter to recover.

### OUTLINE DIMENSIONS AND PIN CONNECTION DIAGRAM

Dimensions are shown in inches and (mm).



MATING SOCKET: CAMBION 450-3388-01-03

### RESISTIVE SCALING OF INPUTS

A unique feature of the SDC1700 series of converters is that the inputs can be resistively scaled to accommodate any range of input signal and reference voltages.

This means that a standard converter can be used with a personality card in systems where a wide range of input and reference voltages are encountered. In addition it should be noted that a 400Hz unit will operate from a 2.6kHz reference. It will however have the velocity and acceleration characteristics as specified for the 400Hz converter. A 60Hz converter will operate from a 400Hz reference and will have the velocity and acceleration characteristics as specified for the 60Hz converter.

To calculate the values of the external scaling resistors for a synchro converter, add  $1.11k\Omega$  in series with  $S1$ ,  $S2$  and  $S3$  per extra volt in the case of the signal, and  $2.2k\Omega$  in the case of the reference. In the case of a resolver converter add  $2.22k\Omega$  per extra volt in series with  $S1$  and  $S2$  for the signal and  $2.2k\Omega$  per extra volt in series with  $R_{HI}$  for the reference.

For example, assume that we have an 11.8 volt line to line signal/26.0 volt reference converter, and we wish to use a 60 volt line to line signal with a 115 volt reference.

Thus in each signal input line, the extra voltage capability required is:

$$60 - 11.8 = 48.2 \text{ volts}$$

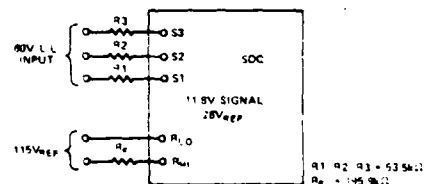
Therefore each resistor needs to have a value of  $48.2 \times 1.11 = 53.5k\Omega$ . In the case of the reference, the extra voltage capability required is:

$$115 - 26.0 = 89 \text{ volts}$$

Therefore the resistor needs to have a value of:

$$89.0 \times 2.2 = 195.8k\Omega$$

Thus the inputs can be scaled as in the diagram below.



NOTE: IN THE CASE OF  $R1$ ,  $R2$  AND  $R3$  THE RATIO ERRORS BETWEEN THE RESISTANCES IS MORE IMPORTANT THAN THE ABSOLUTE RESISTANCE VALUES.

IN GENERAL A 1% RATIO ERROR WILL GIVE RISE TO AN EXTRA INACCURACY OF 17 ARC MINUTES WHILE A RATIO ERROR OF 0.1% WILL GIVE RISE TO AN EXTRA INACCURACY OF 1.7 ARC MINUTES.

THE ABSOLUTE VALUE OF  $R4$  IS NOT CRITICAL.

### BIT WEIGHT TABLE

Bit Number	Weight in Degrees
1 (MSB)	150.0000
2	75.0000
3	45.0000
4	22.5000
5	11.2500
6	5.6250
7	2.8125
8	1.4063
9	0.7031
10 (LSB for SDC1702)	0.3516
11	0.1758
12 (LSB for SDC1700)	0.0879
13	0.0439
14 (LSB for SDC1704)	0.0220

## SDC 1700 S/D Converter Data Sheet (continued)

### VELOCITY PIN

This pin provides a voltage output which is proportional to the angular velocity of the input. The voltage goes negative for an increasing digital angle and goes positive for a decreasing digital angle.

The characteristics of the velocity pin output are given in the table below.

Scaling of Output Voltage for One Full max. Velocity	2Volts (Nominal)
Output Voltage Temp. Coeff.	0.05%/°C of Output
Output Voltage Drift (All Models)	0 to +70°C ±50µV/°C -55°C to +105°C ±100µV/°C
Linearity	0 sec to 800/sec SDC1704 400Hz 1% 0 sec to 100/sec SDC1704 60Hz 1% 0 sec to 800/sec SDC1700/2 400Hz 2% 0 sec to 100/sec SDC1700/2 60Hz 1.5%
Noise (0 to 20Hz)	1600/sec SDC1700/2/4 400Hz 2mV rms 200/sec SDC1700/2/4 60Hz 2mV rms
Impedance (Output)	1Ω
max Current Available	1mA

The velocity voltage can be used in closed loop servo systems for stabilization instead of a tachometer.

The SDC1700/2/4 velocity outputs do not have the disadvantages of being inefficient at low speeds and do not need gearing required by tachometers. In addition, the output is available at no extra cost.

For other velocity output scaling and linearity consult the factory.

Two examples of the use of the velocity pin are shown in the diagram below.

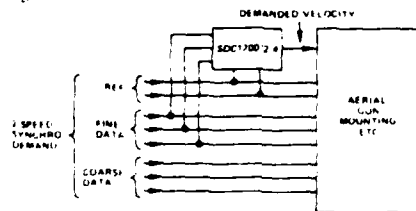


Diagram showing a velocity feed forward application. The SDC is used to produce the demanded velocity from Synchro form inputs.

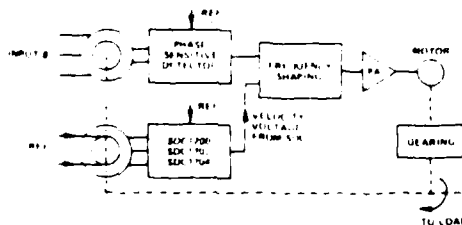
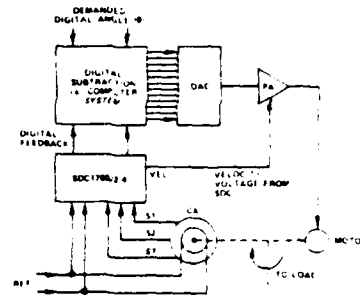


Diagram showing the velocity voltage being used to stabilize an electro-mechanical control loop.

### APPLICATIONS OF SYNCHRO-TO-DIGITAL CONVERTERS

SDCs can be used in a variety of ways in control loops as well as for the conversion of angular data into a form which is readily acceptable to digital displays or computers.

The diagram below shows an SDC being used in a digitally controlled feedback loop.



An SDC Being Used in a Digitally Controlled Feedback Loop

Such loops as shown in the diagram above require the high dynamic performance of the SDC1700 series converters. It should be noted that in this application, the SDC1700 series will replace conventional tachometers and phase sensitive detectors while at the same time provide digital position feedback.

Many synchro systems employ a two speed, geared arrangement utilizing one synchro for the fine shaft and one for the coarse. An example of this type is shown below.

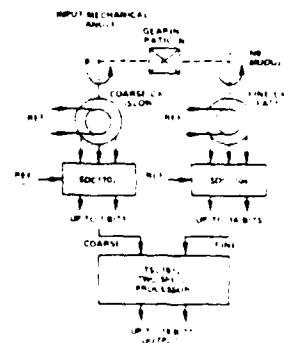


Diagram Showing Coarse-Fine Synchro Processor System

In the above example, two tracking SDC's are being used to provide data for coarse/fine (two speed) data transmission systems.

The TSL1612 is a processor which combines the outputs of two SDC's to provide one output word of up to 19 bits in length.

The TSL1612 is available for any ratio between 2:1 and 36:1 and provides automatic compensation for misalignment of the coarse synchro relative to its shaft. It also corrects for any overlap between the digits of the coarse and fine shafts.



## SDC 1700 S/D Converter Data Sheet (continued)

### MEAN TIME BETWEEN FAILURES (M.T.B.F.)

The estimated mean time between failures is given as follows:

SDC1700/2	174,000 Hours
SDC1704	167,000 Hours

Further information relating to M.T.B.F. and to the quality control and test procedures employed by us can be obtained from the factory on request.

### TRANSFER FUNCTION

The transfer function of the SDC1700/2 and SDC1704, 400Hz versions, is given below.

For the transfer functions of the other models or for a detailed analysis of those given here, please contact us.

#### SDC1700/2 400Hz

$$\frac{\theta_0}{\theta_1} = \frac{8.8 \times 10^7 (1 + 0.8 \times 10^{-3} s)}{s^3 + 8.04 \times 10^2 s^2 + 6.1 \times 10^5 s + 8.8 \times 10^7}$$

#### SDC1704 400Hz

$$\frac{\theta_0}{\theta_1} = \frac{2.95 \times 10^7 (1 + 8.2 \times 10^{-3} s)}{s^3 + 8.05 \times 10^2 s^2 + 1.95 \times 10^5 s + 2.95 \times 10^7}$$

### CARD MOUNTING

All the converters can be mounted on an AC1755 mounting card. This card contains the latches described under the "Data Transfer" heading, which are necessary to transfer the data on to a computer bus system, and sockets for the converter.

The latches have a tri-state output to facilitate ease of use.

The AC1755 also contains facilities for the inclusion of input signal and reference scaling resistors as described under the heading "Resistive Scaling of Inputs".

The card uses a 22/22 0.156" pitch edge connector. The pin out is shown below. If it is not required to use the external latches, they can be jumpered on the board.

#### AC1755 MOUNTING CARD

Dimensions shown in inches and (mm).

First Angle  
Projection

#### EDGE CONNECTIONS AC1755

Pin Number	Function	Pin Number	Function
1	REF 1	17	REF 2
2	REF 3	18	REF 4
3	REF 5	19	REF 6
4	REF 7	20	REF 8
5	REF 9	21	REF 10
6	REF 11	22	REF 12
7	REF 13	23	REF 14
8	REF 15	24	REF 16
9	REF 17	25	REF 18
10	REF 19	26	REF 20
11	REF 21	27	REF 22
12	REF 23	28	REF 24

### ORDERING INFORMATION

Parts should be ordered by the appropriate part number (i.e.,

VOL. II, 13-54 SYNCHRO & RESOLVER CONVERTERS

SDC1700, SDC1702, SDC1704) followed by the appropriate XYZ option code.

If the unit is to be a Resolver-to-Digital Converter, the SDC should be replaced by RDC in the part number.

The XYZ options are as follows:

X signifies the operating temperature range and the options are:

- X = 5 signifies 0 to +70°C (commercial) temperature.
- X = 6 signifies -55°C to +105°C (extended) temperature.

Y signifies the reference frequency and the options are:

- Y = 1 signifies 400Hz
- Y = 2 signifies 60Hz \*
- Y = 4 signifies 2.6kHz

Z signifies the input signal and reference voltages and whether the converter is an SDC or an RDC. The options are:

- Z = 1 signifies synchro, signal 11.8V rms, reference 26V rms
- Z = 2 signifies synchro, signal 90V rms, reference 115V rms
- Z = 3 signifies resolver, signal 11.8V rms, reference 11.8V rms
- Z = 4 signifies resolver, signal 26V rms, reference 26V rms
- Z = 8 signifies resolver, signal 11.8V rms, reference 26V rms

Thus, for example, an SDC1704 with a commercial (0 to +70°C) operating range, using a 400Hz, 26V reference with an 11.8V signal would be ordered as an SDC1704511.

For other than these options, consult the factory.

### CAUTIONS

Do not reverse the power supplies.

Do not connect signal and/or reference inputs to other than S1, S2, S3, S4, R<sub>HI</sub> or R<sub>LO</sub>.

Do not connect signals and/or references to a lower voltage rated converter. (Such as a 115V Synchro into a 26V Converter).

Misconnections as per the above will damage the units and void the warranty.

### OTHER PRODUCTS

The SDC1700/2/4 converters are just a few of the modules and instruments concerned with Synchro and Resolver conversion manufactured by us.

Other products are listed below and technical data is available. If you have any questions about our products or require advice about the use of them for a particular application, please contact our Applications Engineering Department.

### TWO SPEED PROCESSORS

Which utilize the digital outputs of two SDCs in a 2 speed coarse/fine system to produce one combined digital word of up to 19 bits in length. The TSL1612 in particular is available for any ratio between 2:1 and 36:1.

### DIGITAL-TO-SYNCHRO CONVERTERS

Resolutions of between 10 and 14 bits are available.

### BCD OUTPUT SYNCHRO-TO-DIGITAL CONVERTERS

The SBDC1752 and SBDC1753 are converters with a BCD instead of a binary output based upon the SDC1700. They have outputs of 0-360.0 degrees and 0 to 360.0 degrees respectively.

#### \*60Hz Operation

For 60Hz operation, a 60Hz converter can be used with no reduction in accuracy.



## Fast, Complete 10-Bit A/D Converter with Microprocessor Interface

### AD573\*

#### FEATURES

Complete 10-Bit A/D Converter with Reference, Clock  
and Comparator  
Full 8- or 16-Bit Microprocessor Bus Interface  
Fast Successive Approximation Conversion - 20 $\mu$ s  
typ  
No Missing Codes Over Temperature  
Operates on +5V and -12V to -15V Supplies  
Low Cost Monolithic Construction

#### PRODUCT DESCRIPTION

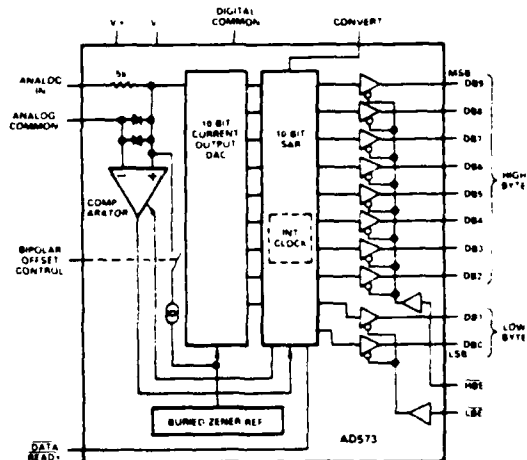
The AD573 is a complete 10-bit successive approximation analog to digital converter consisting of a DAC, voltage reference, clock, comparator, successive approximation register (SAR) and 3 state output buffers—all fabricated on a single chip. No external components are required to perform a full accuracy 10-bit conversion in 20 $\mu$ s.

The AD573 incorporates the most advanced integrated circuit design and processing technology available today. The successive approximation function is implemented with I<sup>2</sup>L integrated injection logic. Laser trimming of the high stability SiCr thin film resistor ladder network at the wafer stage LWT insures high accuracy, which is maintained with a temperature compensated sub-surface Zener reference.

Operating on supplies of +5V and -12V to -15V, the AD573 will accept analog inputs of 0 to +10V or -5V to +5V. The trailing edge of a positive pulse on the CONVERT line initiates the 20 $\mu$ s conversion cycle. DATA READY indicates completion of the conversion. HIGH BYTE ENABLE HBE and LOW BYTE ENABLE LBE control the 8-bit and 2-bit three state output buffers.

The AD573 is available in two versions for the 0 to +70°C temperature range, the AD573J and AD573K. The AD573S guarantees  $\pm 1$ LSB relative accuracy and no missing codes from -55°C to +125°C.

#### AD573 FUNCTIONAL BLOCK DIAGRAM



Two package configurations are offered. All versions are also offered in a 20-pin hermetically sealed ceramic DIP. The AD573J and AD573K are also available in a 20-pin plastic DIP.

#### PRODUCT HIGHLIGHTS

1. The AD573 is a complete 10-bit A/D converter. No external components are required to perform a conversion.
2. The AD573 interfaces to many popular microprocessors without external buffers or peripheral interface adapters. The 10 bits of output data can be read as a 10-bit word or as 8- and 2-bit words.
3. The device offers true 10-bit accuracy and exhibits no missing codes over its entire operating temperature range.
4. The AD573 adapts to either unipolar (0 to +10V) or bipolar (-5V to +5V) analog inputs by simply grounding or opening a single pin.
5. Performance is guaranteed with +5V and -12V or -15V supplies.

\*Protected by U.S. Patent Nos. 3,940,760; 4,213,806; 4,136,349; 4,400,649, and 4,400,690.

# AD573 A/D Converter Data Sheet (continued)

## SPECIFICATIONS

( $T_A = 25^\circ\text{C}$ ,  $V_+ = +5\text{V}$ ,  $V_- = -12\text{V}$  or  $-15\text{V}$ , all voltages measured with respect to digital common, unless otherwise indicated)

Model	AD573J			AD573K			AD573S			Units
	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
RESOLUTION	10			10			10			Bits
RELATIVE ACCURACY <sup>1</sup>	$\pm 1$			$\pm 1.2$			$\pm 1$			LSB
$T_A = T_{min}$ to $T_{max}$	$\pm 1$			$\pm 1.2$			$\pm 1$			LSB
FULL SCALE CALIBRATION <sup>2</sup>	$\pm 2$			$\pm 2$			$\pm 2$			LSB
UNIPOLAR OFFSET	$\pm 1$			$\pm 1.2$			$\pm 1$			LSB
BIPOLAR OFFSET	$\pm 1$			$\pm 1.2$			$\pm 1$			LSB
DIFFERENTIAL NONLINEARITY <sup>3</sup>	10			10			10			Bits
$T_A = T_{min}$ to $T_{max}$	9			10			10			Bits
TEMPERATURE RANGE	0		+70	0		+70	-55		+125	°C
TEMPERATURE COEFFICIENTS <sup>4</sup>										
Unipolar Offset	$\pm 2$			$\pm 1$			$\pm 2$			LSB
Bipolar Offset	$\pm 2$			$\pm 1$			$\pm 2$			LSB
Full Scale Calibration <sup>2</sup>	$\pm 4$			$\pm 2$			$\pm 5$			LSB
POWER SUPPLY REJECTION										
Positive Supply										
+4.5V to +5.5V	$\pm 2$			$\pm 1$			$\pm 2$			LSB
Negative Supply										
-12.5V to -15V	$\pm 2$			$\pm 1$			$\pm 2$			LSB
-12.5V to -11.4V	$\pm 2$			$\pm 1$			$\pm 2$			LSB
ANALOG INPUT IMPEDANCE	3.0	5.0	7.0	3.0	5.0	7.0	3.0	5.0	7.0	k $\Omega$
ANALOG INPUT RANGES										
Unipolar	0		+10	0		+10	0		+10	V
Bipolar	-5		+5	-5		+5	-5		+5	V
OUTPUT CODING										
Unipolar	Positive True Binary			Positive True Binary			Positive True Binary			
Bipolar	Positive True Offset Binary			Positive True Offset Binary			Positive True Offset Binary			
LOGIC OUTPUT										
Output Sink Current										
$V_{OL} = 0.4\text{V max}$ , $T_{min}$ to $T_{max}$	3.2			3.2			3.2			mA
Output Source Current <sup>5</sup>										
$V_{OH} = 2.4\text{V max}$ , $T_{min}$ to $T_{max}$	0.5			0.5			0.5			mA
Output Leakage	$\pm 40$			$\pm 40$			$\pm 40$			$\mu\text{A}$
LOGIC INPUTS										
Input Current	$\pm 100$			$\pm 100$			$\pm 100$			$\mu\text{A}$
Logic "1"	2.0			2.0			2.0			V
Logic "0"	0.8			0.8			0.8			V
CONVERSION TIME										
$T_A = T_{min}$ to $T_{max}$	10	20	30	10	20	30	10	20	30	$\mu\text{s}$
POWER SUPPLY										
$V_+$	+4.5	+5.0	+7.0	+4.5	+5.0	+7.0	+4.5	+5.0	+7.0	V
$V_-$	-11.4	-15	-16.5	-11.4	-15	-16.5	-11.4	-15	-16.5	V
OPERATING CURRENT										
$V_+$	15	25		15	25		15	25		mA
$V_-$	9	15		9	15		9	15		mA
PACKAGE <sup>6</sup>										
Ceramic DIP	D20A			D20A			D20A			
Plastic DIP	N20A			N20A						

### NOTES

Relative accuracy is defined as the deviation of the code transition points from the ideal transfer point on a straight line from the zero to the full scale of the device.

Full scale calibration is guaranteed trimmable to zero with an external 50k potentiometer in place of the 15k fixed resistor.

Full scale is defined as 10 volts minus 1 LSB, or 9.999 volts.

Defined as the resolution for which no missing codes will occur.

Range from -15V to +25V,  $T_A = 25^\circ\text{C}$  to  $T_{max}$  or  $T_{min}$ .

The data output lines have active pull-ups to source 0.5mA. The DATA READY line is open collector with a nominal 6k $\Omega$  internal pull-up resistor.

See Section 19 for package outline information.

Specifications subject to change without notice.

Specifications shown in boldface are tested on all production units at final electrical test. Results from those tests are used to calculate outgoing quality levels. All min and max specifications are guaranteed, although only those shown in boldface are tested on all production units.

## AD573 A/D Converter Data Sheet (continued)

## FUNCTIONAL DESCRIPTION

A block diagram of the AD573 is shown in Figure 1. The positive CONVERT pulse must be at least 500ns wide. DR goes high within 1.5µs after the leading edge of the convert pulse indicating that the internal logic has been reset. The negative edge of the CONVERT pulse initiates the conversion. The internal 10-bit current output DAC is sequenced by the integrated injection logic (I<sup>2</sup>L) successive approximation register (SAR) from its most significant bit to least significant bit to provide an output current which accurately balances the input signal current through the 5kΩ resistor. The comparator determines whether the addition of each successively weighted bit current causes the DAC current sum to be greater or less than the input current; if the sum is more, the bit is turned off. After testing all bits, the SAR contains a 10-bit binary code which accurately represents the input signal to within  $\pm \text{LSB} = 0.05\%$  of full scale.

The SAR drives  $\overline{DR}$  low to indicate that the conversion is complete and that the data is available to the output buffers.  $\overline{HBE}$  and  $\overline{LBE}$  can then be activated to enable the upper 8-bit and lower 2-bit buffers as desired.  $\overline{HBE}$  and  $\overline{LBE}$  should be brought high prior to the next conversion to place the output buffers in the high-impedance state.

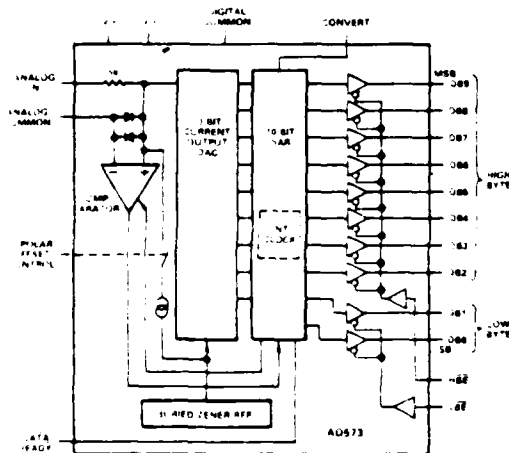


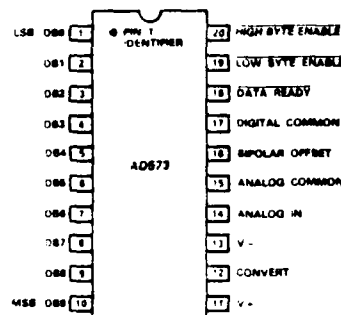
Figure 1 AD573 Functional Block Diagram

The temperature compensated buried Zener reference provides the primary voltage reference to the DAC and ensures excellent stability with both time and temperature. The bipolar offset input controls a switch which allows the positive bipolar offset current, exactly equal to the value of the MSB less  $\pm$ LSB, to be injected into the summing  $\pm$  node of the comparator to offset the DAC output. Thus the nominal 0 to  $\pm$ LSB unipolar input range becomes a  $\pm$ SV to  $\pm$ SV range. The 10 $\Omega$  thin film input resistor is trimmed so that with a full scale input signal, an input current will be generated which exactly matches the DAC input with all bias on.

### UNIPOLAR CONNECTION

The AD573 contains all the active components required to perform a complete A/D conversion. Thus, for many applications, all that is necessary is connection of the power supplies,  $+5V$  and  $+12V$  to  $+15V$ , the analog input and the convert pulse. However, there are some features and special connections which should be considered for achieving optimum performance. The functional pinout is shown in Figure 2.

The standard unipolar 0 to +10V range is obtained by shorting the bipolar offset control pin (pin 16) to digital common (pin 17).



**Figure 2. AD573 Pin Connections**

### Full Scale Calibration

The 5k $\Omega$  thin film input resistor is laser trimmed to produce a current which matches the full scale current of the internal DAC—plus about 0.3%—when an analog input voltage of 9.990 volts  $\pm$  10 volts  $\pm$  1LSB is applied at the input. The input resistor is trimmed in this way so that if a fine trimming potentiometer is inserted in series with the input signal, the input current at the full scale input voltage can be trimmed down to match the DAC full scale current as precisely as desired. However, for many applications the nominal 9.99 volt full scale can be achieved to sufficient accuracy by simply inserting a 15 $\Omega$  resistor in series with the analog input to pin 14. Typical full scale calibration error will then be within  $\pm$  2LSB or  $\pm$  0.2%. If more precise calibration is desired, a 50 $\Omega$  trimmer should be used instead. Set the analog input at 9.990 volts, and set the trimmer so that the output code is just at the transition between 11111111 10 and 11111111 11. Each LSB will then have a weight of 9.76mV. If a nominal full scale of 10.24 volts is desired (which makes the LSB have a weight of exactly 10.00mV), a 100 $\Omega$  resistor and a 100 $\Omega$  trimmer (or a 200 $\Omega$  trimmer with good resolution) should be used. Of course, larger full scale ranges can be arranged by using a larger input resistor, but linearity and full scale temperature coefficient may be compromised if the external resistor becomes a sizeable percentage of 5k $\Omega$ . Figure 3 illustrates the connections required for full scale calibration.

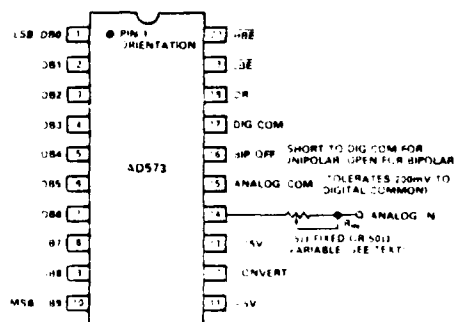


Figure 3 Standard AD573 Connections

### Unipolar Offset Calibration

Since the Unipolar Offset is less than  $\pm 1$  LSB for all versions of the AD573, most applications will not require trimming. Figure 4 illustrates two trimming methods which can be used if greater accuracy is necessary.

## Applying the AD573

Figure 4a shows how the converter zero may be offset by up to  $\pm 3$  bits to correct the device initial offset and/or input signal offsets. As shown, the circuit gives approximately symmetrical adjustment in unipolar mode.

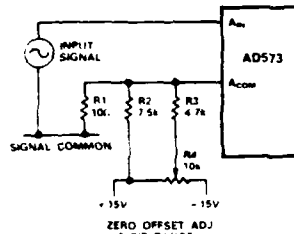


Figure 4a.

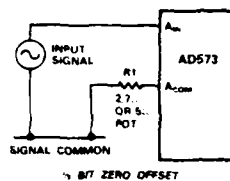


Figure 4b.

Figure 5 shows the nominal transfer curve near zero for an AD573 in unipolar mode. The code transitions are at the edges of the nominal bit weights. In some applications it will be preferable to offset the code transitions so that they fall between the nominal bit weights, as shown in the offset characteristics.

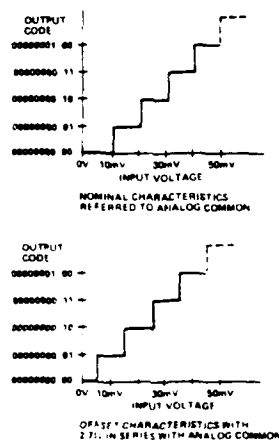


Figure 5. AD573 Transfer Curve - Unipolar Operation (Approximate Bit Weights Shown for Illustration, Nominal Bit Weights = 9.766mV)

This offset can easily be accomplished as shown in Figure 4b. At balance, after a conversion, approximately 2mA flows into the Analog Common terminal. A 2.7k resistor in series with the terminal will result in approximately the desired 1/2 bit offset of the transfer characteristics. The nominal 2mA Analog Common current is not closely controlled in manufacture. If high accuracy is required, a 50k potentiometer, connected as a rheostat, can be used as R1. Additional negative offset range may be obtained by using larger values of R1. Of course, if the zero transition point is changed, the full scale transition point will also move. Thus, if an offset of 1/2 LSB is introduced, full scale trimming as described on the previous page should be done with an analog input of 9.985 volts.

**NOTE:** During a conversion, transient currents from the Analog Common terminal will disturb the offset voltage. Capacitive decoupling should not be used around the offset network. These transients will settle appropriately during a conversion. Capacitive

decoupling will "pump up" and fail to settle resulting in conversion errors. Power supply decoupling, which returns to analog signal common, should go to the signal input side of the resistive offset network.

## BIPOLAR CONNECTION

To obtain the bipolar  $-5V$  to  $+5V$  range with an offset binary output code, the bipolar offset control pin is left open.

A  $-5.000$  volt signal will give a 10-bit code of 00000000 00; an input of 0.000 volts results in an output code of 10000000 00 and  $+4.99$  volts at the input yields the 11111111 11 code. The nominal transfer curve is shown in Figure 6.

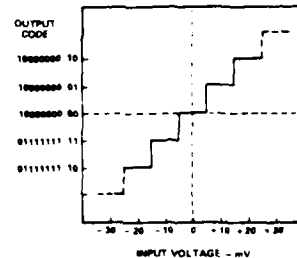


Figure 6. AD573 Transfer Curve - Bipolar Operation

Note that in the bipolar mode, the code transitions are offset 1/2 LSB such that an input voltage of 0 volts  $\pm 5mV$  yields the code representing zero (10000000 00). Each output code is then centered on its nominal input voltage.

## Full Scale Calibration

Full Scale Calibration is accomplished in the same manner as in Unipolar operation except the full scale input voltage is  $+4.985$  volts.

## Negative Full Scale Calibration

The circuit in Figure 4a can also be used in Bipolar operation to offset the input voltage (nominally  $-5V$ ) which results in the 00000000 00 code. R2 should be omitted to obtain a symmetrical range.

The bipolar offset control input is not directly TTL compatible but a TTL interface for logic control can be constructed as shown in Figure 7.

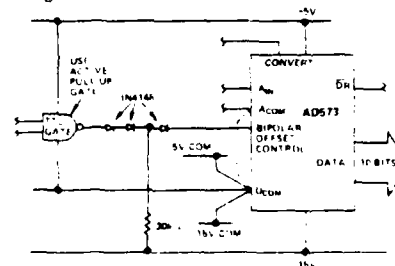


Figure 7. Bipolar Offset Controlled by Logic Gate  
Gate Output = 1 Unipolar 0 - 10V Input Range  
Gate Output = 0 Bipolar  $\pm 5V$  Input Range

## SAMPLE-HOLD AMPLIFIER CONNECTION TO THE AD573

Many situations in high-speed acquisition systems or digitizing rapidly changing signals require a sample-and-hold amplifier (SHA) in front of the A-D converter. The SHA can acquire and hold a

## AD573 A/D Converter Data Sheet (continued)

signal faster than the converter can perform a conversion. A SHA can also be used to accurately define the exact point in time at which the signal is sampled. For the AD573, a SHA can also serve as a high input impedance buffer.

Figure 8 shows the AD573 connected to the AD582 monolithic SHA for high speed signal acquisition. In this configuration, the AD582 will acquire a 10 volt signal in less than 10 $\mu$ s with a droop rate less than 100 $\mu$ V/ms.

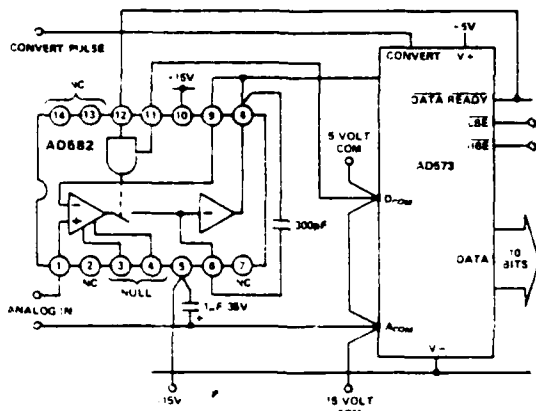


Figure 8. Sample-Hold Interface to the AD573

$\overline{DR}$  goes high after the conversion is initiated to indicate that reset of the SAR is complete. In Figure 8 it is also used to put the AD582 into the hold mode while the AD573 begins its conversion cycle. The AD582 settles to final value well in advance of the first comparator decision inside the AD573.

$\overline{DR}$  goes low when the conversion is complete placing the AD582 back in the sample mode. Configured as shown in Figure 8, the next conversion can be initiated after a 10 $\mu$ s delay to allow for signal acquisition by the AD582.

Observe carefully the ground, supply, and bypass capacitor connections between the two devices. This will minimize ground noise and interference during the conversion cycle.

### GROUNDING CONSIDERATIONS

The AD573 provides separate Analog and Digital Common connections. The circuit will operate properly with as much as  $\pm 200$ mV of common mode voltage between the two commons. This permits more flexible control of system common bussing and digital and analog returns.

In normal operation, the Analog Common terminal may generate transient currents of up to 2mA during a conversion. In addition a static current of about 2mA will flow into Analog Common in the unipolar mode after a conversion is complete. The Analog Common current will be modulated by the variations in input signal.

The absolute maximum voltage rating between the two commons is  $\pm 1$  volt. It is recommended that a parallel pair of back-to-back protection diodes be connected between the commons if they are not connected locally.

### CONTROL AND TIMING OF THE AD573

The operation of the AD573 is controlled by three inputs: CONVERT,  $\overline{HBE}$  and  $\overline{LBE}$ .

#### Starting a Conversion

The conversion cycle is initiated by a positive-going CONVERT

pulse at least 500ns wide. The rising edge of this pulse resets the internal logic, clears the result of the previous conversion, and sets  $\overline{DR}$  high. The falling edge of CONVERT begins the conversion cycle. When conversion is completed  $\overline{DR}$  returns low. During the conversion cycle,  $\overline{HBE}$  and  $\overline{LBE}$  should be held high. If  $\overline{HBE}$  or  $\overline{LBE}$  goes low during a conversion, the data output buffers will be enabled and intermediate conversion results will be present on the data output pins. This may cause bus conflicts if other devices in a system are trying to use the bus.

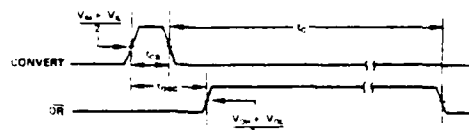


Figure 9. Convert Timing

#### Reading the Data

The three-state data output buffers are enabled by  $\overline{HBE}$  and  $\overline{LBE}$ . Access time of these buffers is typically 150ns (250 maximum). The Data outputs remain valid until 50ns after the enable signal returns high, and are completely into the high-impedance state 100ns later.

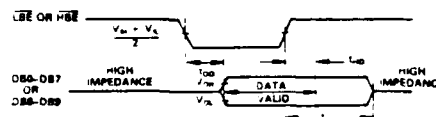


Figure 10. Read Timing

### TIMING SPECIFICATIONS (All grades, $T_A = T_{max} - T_{min}$ )

Parameter	Symbol	Min	Typ	Max	Units
CONVERT Pulse Width	$t_{CS}$	500	—	—	ns
$\overline{DR}$ Delay from CONVERT	$t_{DSC}$	—	1	1.5	$\mu$ s
Conversion Time	$t_C$	10	20	30	$\mu$ s
Data Access Time	$t_{DD}$	0	150	250	ns
Data Valid after $\overline{HBE}$ , $\overline{LBE}$					
High	$t_{HD}$	50	—	—	ns
Output Float Delay	$t_{HL}$	—	100	200	ns

### MICROPROCESSOR INTERFACE CONSIDERATIONS - GENERAL

When an analog-to-digital converter like the AD573 is interfaced to a microprocessor, several details of the interface must be considered. First, a signal to start the converter must be generated; then an appropriate delay period must be allowed to pass before valid conversion data may be read. In most applications, the AD573 can interface to a microprocessor system with little or no external logic.

The most popular control signal configuration consists of decoding the address assigned to the AD573, then gating this signal with the system's  $\overline{WR}$  signal to generate the CONVERT pulse, and gating it with RD to enable the output buffers. The use of a memory address and memory  $\overline{WR}$  and RD signals denotes "memory-mapped" I/O interfacing, while the use of a separate I/O address space denotes "isolated I/O" interfacing. In 8-bit bus systems, the 10-bit AD573 will occupy two locations when data is to be read, therefore, two usually consecutive addresses must be decoded. One of the addresses can also be used as the address which produces the CONVERT signal during  $\overline{WR}$  operations.

Figure 11 shows a generalized diagram of the control logic for

# AD573 A/D Converter Data Sheet (continued)

## Interfacing to the AD573

an AD573 interfaced to an 8-bit data bus, where two addresses (ADC ADDR and ADC ADDR + 1) have been decoded. ADC ADDR starts the converter when written to; the actual data being written to the converter does not matter and contains the high byte data during read operations. ADC ADDR + 1 performs no function during write operations, but contains the low byte data during read operations.

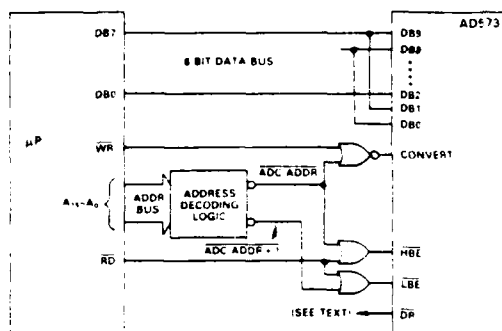


Figure 11. General AD573 Interface to 8-Bit Microprocessor

In systems where this read-write interface is used, at least 30 microseconds (the maximum conversion time) must be allowed to pass between starting a conversion and reading the results. This delay or "timeout" period can be implemented in a short software routine such as a countdown loop, enough dummy instructions to consume 30 microseconds, or enough actual useful instructions to consume the required time. In tightly-timed systems, the DR line may be read through an external three-state buffer to determine precisely when a conversion is complete. Higher-speed systems may choose to use DR to signal an interrupt to the processor at the end of a conversion.

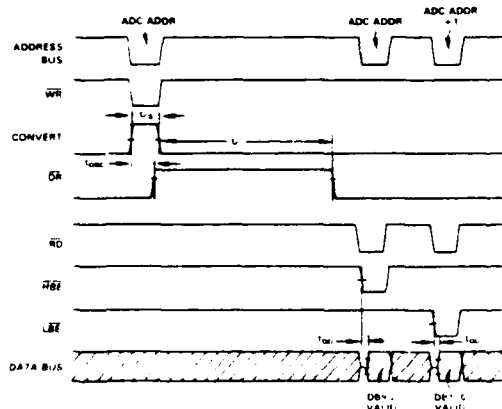


Figure 12. Typical AD573 Interface Timing Diagram

### CONVERT Pulse Generation

The AD573 is tested with a CONVERT pulse width of 500ns and will typically operate with a pulse as short as 300ns. However, some microprocessors produce active WR pulses which are shorter than this. Either of the circuits shown in Figure 13 can be used to generate an adequate CONVERT pulse for the AD573.

In both circuits, the short low-going WR pulse sets the CONVERT line high through a flip-flop. The rising edge of DR, which signifies that the internal logic has been reset, resets the flip-flop and brings CONVERT low, which starts the conversion.

Note that  $t_{DSC}$  is slightly longer when the result of the previous conversion contains a logic 1 on the LSB. This means that the actual CONVERT pulse generated by the circuits in Figure 13 will vary slightly in width.

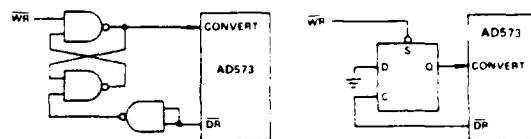


Figure 13a. Using 74LS00 Figure 13b. Using 1 74LS74

### Output Data Format

The AD573 output data is presented in a left-justified format. The 8 MSBs (DB9-DB2, pins 10 through 3) are enabled by HBE (pin 20) and the 2 LSBs (DB1, DB0 - pins 2 and 1) are enabled by LBE (pin 19). This allows simple interface to 8-bit system buses by overlapping the 2 MSBs and the 2 LSBs. The organization of the data is shown in Figure 14.

When the least significant bits are read, LBE brought low, the six remaining bits of the byte will contain meaningless data. These unwanted bits can be masked by logically ANDing the byte with 11000000 (C0 hex), which forces the 6 lower bits to logic 0 while preserving the two most significant bits of the byte.

Note that it is not possible to reconfigure the AD573 for right justified data.

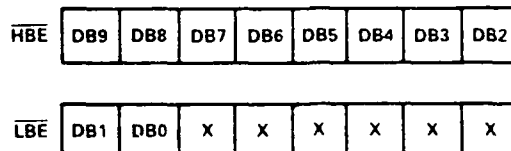


Figure 14. AD573 Output Data Format

In systems where all 10 bits are desired at the same time, HBE and LBE may be tied together. This is useful in interfacing to 16-bit bus systems. The resulting 10-bit word can then be placed at the high end of the 16-bit bus for left justification or at the low end for right justification.

It is also possible to use the AD573 in a "stand-alone" mode, where the output data buffers are automatically enabled at the end of a conversion cycle. In this mode, the DR output is wired to the HBE and LBE inputs. The outputs thus are forced into the high-impedance state during the conversion period, and valid data becomes available approximately 500ns after the DR signal goes low at the end of the conversion. The 500ns delay allows propagation of the least significant bit through the internal logic.

This mode is particularly useful for bench-testing of the AD573, and in applications where dedicated I/O ports of peripheral interface adapter chips are available.

## AD573 A/D Converter Data Sheet (continued)

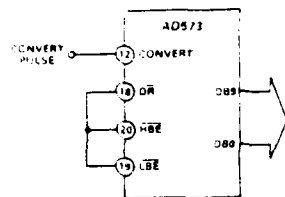


Figure 15. AD573 in "Stand-Alone" Mode  
(Output Data Valid 500ns After DR Goes Low)

### Apple II Microcomputer Interface

The AD573 can provide a flexible, low-cost analog interface for the popular Apple II microcomputer. The Apple II, based on a 1MHz 6502 microprocessor, meets all timing requirements for the AD573. Only a few TTL gates are required to decode the signals available on the Apple II's peripheral connector. The recommended connections are shown in Figure 16.

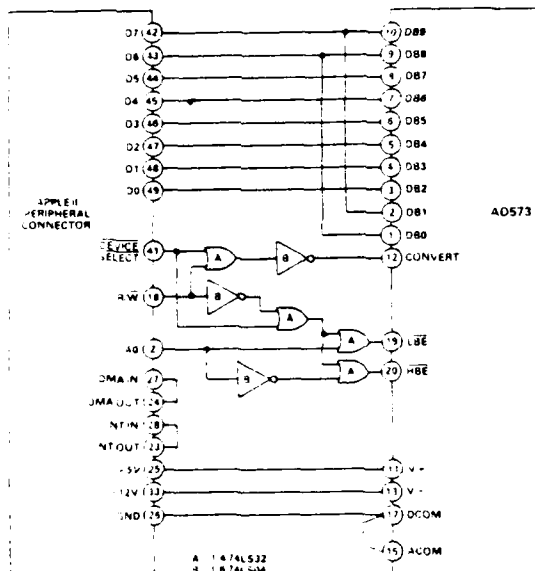


Figure 16. AD573 Interface to Apple II

The BASIC routine listed here will operate the AD573 circuit shown in Figure 16. The conversion is started by POKEing to the location which contains the AD573. The relatively slow execution speed of BASIC eliminates the need for a delay routine between starting and reading the converter. This routine assumes that the AD573 is connected for a  $\pm 5$  volt input range. Variable I represents the integer value from 0 to 1023 read from the AD573. Variable V represents the actual value of the input signal in volts.

```
100 PRINT "WHICH SLOT IS THE A/D IN? INPUT S
110 A = 49280 + 16*S
120 POKE A,0
130 L = PEEK A : H = PEEK A + 1
140 I = 4*H + INT L/64
150 V = (I/1024)*10-5
160 PRINT "THE INPUT SIGNAL IS "V" VOLTS."
```

It is also possible to write a faster-executing assembly-language routine to control the AD573. Such a routine will require a

delay between starting and reading the converter. This can be easily implemented by calling the Apple's WAIT subroutine which resides at location 3FCA8, after loading the accumulator with a number greater than or equal to two.

### 8085-Series Microprocessor Interface

The AD573 can also be used with 8085-series microprocessors. These processors use separate control signals for RD and WR, as opposed to the single  $R/\bar{W}$  control signal used in the 6800/6500 series processors.

There are two constraints related to operation of the AD573 with 8085-series processors. The first problem is the width of the CONVERT pulse. The circuit shown in Figure 17, essentially the same as that shown in Figure 13, will produce a wide enough CONVERT pulse when the 8085 is running at 5MHz. For 8085 systems running at slower clock rates (3MHz), the flip-flop-based circuit can be eliminated since the  $\bar{WR}$  pulse will be approximately 500ns wide.

The other consideration is the access time of the AD573's three-state output data buffers, which is 250ns maximum. It may be necessary to insert wait states during RD operations from the AD573. This will not be a problem in systems using memories with comparable access times, since wait states will have already been provided in the basic system design.

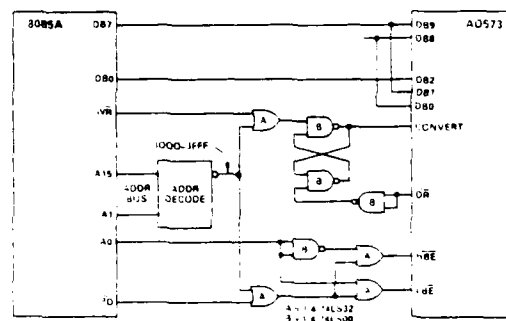


Figure 17. AD573-8085A Interface Connections

The following assembly-language subroutine can be used to control an AD573 residing at memory locations 3000<sub>H</sub> and 3001<sub>H</sub>. The 10 bits of data are returned left-justified in the DE register pair.

```
ADC: LXI H,3000 ;LOAD HL WITH AD573 ADDRESS
      MOV M,A ;START CONVERSION
      MVI B,06 ;LOAD DELAY PERIOD
      LOOP: DCR B ;DELAY LOOP
            JNZ LOOP
            MOV A,M ;READ LOW BYTE
            ANI 00 ;MASK LOWER 6 BITS
            MOV E,A ;STORE CLEAN LOW BYTE IN E
            INR L ;LOAD HIGH BYTE ADDRESS
            MOV D,M ;MOVE HIGH BYTE TO D
            RET ;EXIT
```



# AD544 Operational Amplifier Data Sheet



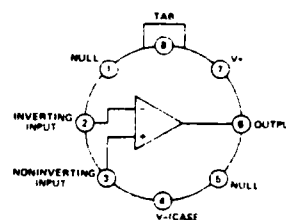
## High Speed Implanted FET-Input Op Amp

### AD544

#### FEATURES

Low Bias Current: 25pA max, warmed-up  
Low Offset Voltage: 500 $\mu$ V max  
Low Offset Voltage Drift: 5 $\mu$ V/ $^{\circ}$ C max  
Low Input Voltage Noise: 2 $\mu$ V p-p  
Low Quiescent Current: 2.5mA max  
High Slew Rate: 13V/ $\mu$ s  
Fast Settling to  $\pm 0.01\%$ : 3 $\mu$ s  
Low Total Harmonic Distortion: 0.0015% at 1kHz

#### AD544 FUNCTIONAL BLOCK DIAGRAM



TO-99  
TOP VIEW

#### PRODUCT DESCRIPTION

The AD544 is a high speed monolithic FET-input operational amplifier fabricated with the most advanced bipolar, JFET and laser trimming technologies. The AD544 offers bias currents significantly lower than currently available monolithic FET-input devices: 25pA max, warmed-up for the AD544K and L, 50pA max for the AD544J. In addition, the offset voltage is laser trimmed to less than 0.5mV on the AD544L and 1.0mV on the AD544K utilizing Analog's laser-wafer-trimming (LWT) process. When combined with the AD544's low offset voltage drift (5 $\mu$ V/ $^{\circ}$ C max for "L", 10 $\mu$ V/ $^{\circ}$ C max for "K"), these features offer the user IC performance truly superior to existing FET-input op amps—and at low, monolithic pricing.

The key technology required for monolithic JFET-input op amps is the ion-implanted JFET. Ion-implantation (as opposed to diffusion) permits the fabrication of precision, matched JFET's on a monolithic bipolar chip. Analog Devices optimizes the process to produce bias currents lower than other popular FET-input op amps and specifies each device for the maximum value at either input in the fully warmed-up condition. Additional benefits of this optimization include low voltage noise (2 $\mu$ V p-p, 0.1–10Hz), and low quiescent current.

The AD544 is recommended for any operational amplifier application requiring excellent ac and dc performance at low cost. The 2MHz bandwidth and low offset of the AD544 make it an excellent choice as an output amplifier for current output D/A Converters such as the AD7541, 12-Bit CMOS DAC. High common mode rejection (80dB, min on the "K" and "L" versions) and open-loop gain ensures better than "12-bit" linearity in high impedance buffer applications.

The AD544 is available in four versions, the "J", "K" and "L" are specified over the 0 to +70 $^{\circ}$ C temperature range and the "S" over the -55 $^{\circ}$ C to +125 $^{\circ}$ C operating temperature range. All devices are packaged in the hermetically-sealed, TO-99 metal can.

#### PRODUCT HIGHLIGHTS

1. Improved bipolar and JFET processing on the AD544 results in the lowest bias current available in a high speed monolithic FET op amp.
2. Analog Devices, unlike some manufacturers, specifies each device for the maximum bias current at either input in the warmed-up condition, thus assuring the user that the AD544 will meet its published specifications in actual use.
3. Laser-wafer-trimming reduces offset voltage to as low as 0.5mV max (AD544L), thus eliminating the need for external nulling in many situations.
4. If offset nulling is required, the additional offset voltage drift induced will be minimal. (In some devices, offset voltage drift can increase an additional 3 $\mu$ V/ $^{\circ}$ C per mV of offset nulled.)
5. Low voltage noise (2 $\mu$ V, p-p), and low offset voltage drift (5 $\mu$ V/ $^{\circ}$ C) enhance the AD544's performance as a precision op amp.
6. The high slew rate (13.0V/ $\mu$ s) and fast settling time to 0.01% (3.0 $\mu$ s) make the AD544 ideal for D/A, A/D, sample-and-hold circuits and high speed integrators.
7. Low harmonic distortion (0.0015%) makes the AD544 an ideal choice for audio applications.

# AD544 Operational Amplifier Data Sheet (continued)

## SPECIFICATIONS ( $\alpha + 25^{\circ}\text{C}$ and $V_s = \pm 15\text{V}$ dc)

Model	AD544J			AD544K			AD544L			AD544S			Units
	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
OPEN LOOP GAIN <sup>1</sup> $V_O = \pm 10\text{V}$ , $R_L \geq 2\text{k}\Omega$ $T_{\text{min}}$ to $T_{\text{max}}$ , $R_L = 2\text{k}\Omega$	30,000 20,000			50,000 40,000			50,000 40,000			50,000 20,000			V/V V/V
OUTPUT CHARACTERISTICS													
Voltage ( $R_L = 2\text{k}\Omega$ , $T_{\text{min}}$ to $T_{\text{max}}$ )	$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		V
Voltage ( $R_L = 10\text{k}\Omega$ , $T_{\text{min}}$ to $T_{\text{max}}$ )	$\pm 12$	$\pm 13$		$\pm 12$	$\pm 13$		$\pm 12$	$\pm 13$		$\pm 12$	$\pm 13$		V
Short Circuit Current		25			25			25			25		mA
FREQUENCY RESPONSE													
Unity Gain Small Signal		2.0			2.0			2.0			2.0		MHz
Full-Power Response		200			200			200			200		kHz
Slew Rate, Unity Gain	8.0	13.0		8.0	13.0		8.0	13.0		8.0	13.0		V/ $\mu\text{s}$
Settling Time to 0.01%		3.0			3.0			3.0			3.0		$\mu\text{s}$
Total Harmonic Distortion		0.0025			0.0025			0.0025			0.0025		%
INPUT OFFSET VOLTAGE <sup>2</sup>													
Initial Offset			2.0			1.0			0.5			1.0	mV
Input Offset Voltage vs. Temp. or $T_{\text{min}}$ to $T_{\text{max}}$			20			10			5			15	$\mu\text{V}/^{\circ}\text{C}$
Input Offset Voltage vs. Supply, $T_{\text{min}}$ to $T_{\text{max}}$			200			100			100			100	$\mu\text{V}/\text{V}$
INPUT BIAS CURRENT <sup>3</sup>													
Either Input		10	50		10	25		10	25		10	25	pA
Offset Current		5			2			2			2		pA
INPUT IMPEDANCE													
Differential <sup>4</sup>		$10^{12/6}$			$10^{12/6}$			$10^{12/6}$			$10^{12/6}$		M $\Omega$ pF
Common Mode		$10^{12/3}$			$10^{12/3}$			$10^{12/3}$			$10^{12/3}$		M $\Omega$ pF
INPUT VOLTAGE RANGE													
Differential		$\pm 20$			$\pm 20$			$\pm 20$			$\pm 20$		V
Common Mode	$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		V
Common Mode Rejection		74			80			80			80		dB
INPUT NOISE													
Voltage 0.1Hz to 10Hz		2			2			2			2		$\mu\text{V p-p}$
$f = 10\text{Hz}$		35			35			35			35		nV/ $\sqrt{\text{Hz}}$
$f = 100\text{Hz}$		22			22			22			22		nV/ $\sqrt{\text{Hz}}$
$f = 1\text{kHz}$		18			18			18			18		nV/ $\sqrt{\text{Hz}}$
$f = 10\text{kHz}$		16			16			16			16		nV/ $\sqrt{\text{Hz}}$
POWER SUPPLY													
Rated Performance		$\pm 15$			$\pm 15$			$\pm 15$			$\pm 15$		V
Operating	$\pm 5$		$\pm 18$	$\pm 5$		$\pm 18$	$\pm 5$		$\pm 18$	$\pm 5$		$\pm 18$	V
Quiescent Current		1.8	2.5		1.8	2.5		1.8	2.5		1.8	2.5	mA
TEMPERATURE RANGE													
Operating, Rated Performance	0		+70	0		+70	0		+70	-55		+125	$^{\circ}\text{C}$
Storage	-65		+150	-65		+150	-65		+150	-65		+150	$^{\circ}\text{C}$
PACKAGE <sup>5</sup>													
TO-99 Style (H08B)	AD544JH			AD544KH			AD544LH			AD544SH			

### NOTES

<sup>1</sup>Open Loop Gain is specified with  $V_O$  both nulled and unnullled.  
<sup>2</sup>Input Offset Voltage specifications are guaranteed after 5 minutes of operation at  $T_A = +25^{\circ}\text{C}$ .

<sup>3</sup>Bias Current specifications are guaranteed at maximum at either input after 5 minutes of operation at  $T_A = +25^{\circ}\text{C}$ . For higher temperatures, the current doubles every  $10^{\circ}\text{C}$ .

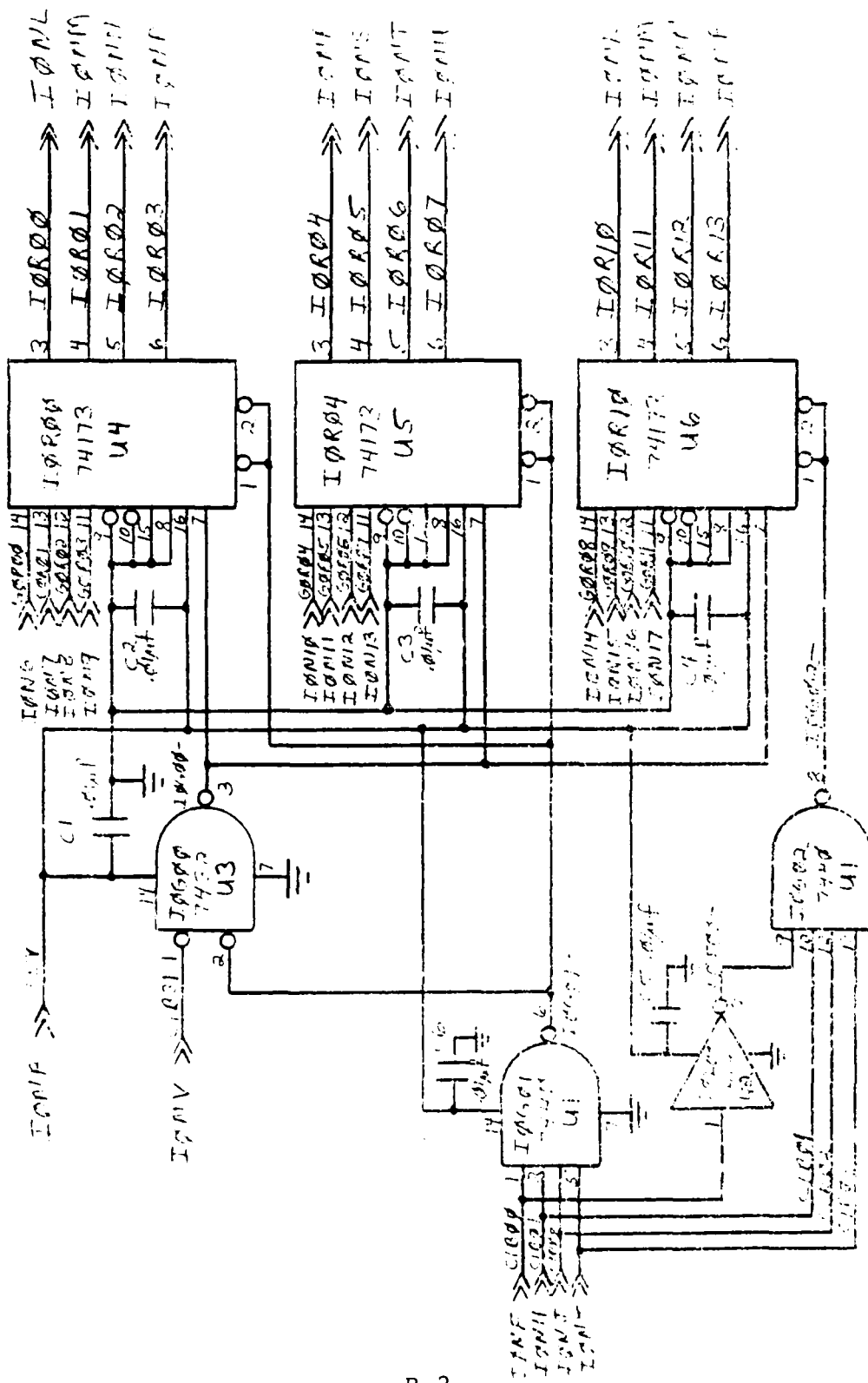
<sup>4</sup>Defined as voltage between inputs, such that neither exceeds  $\pm 10\text{V}$  from ground.

<sup>5</sup>See Section 19 for package outline information.  
Specifications subject to change without notice.

Specifications shown in boldface are tested on all production units at final electrical test. Results from those tests are used to calculate outgoing quality levels. All min and max specifications are guaranteed, although only those shown in boldface are tested on all production units.

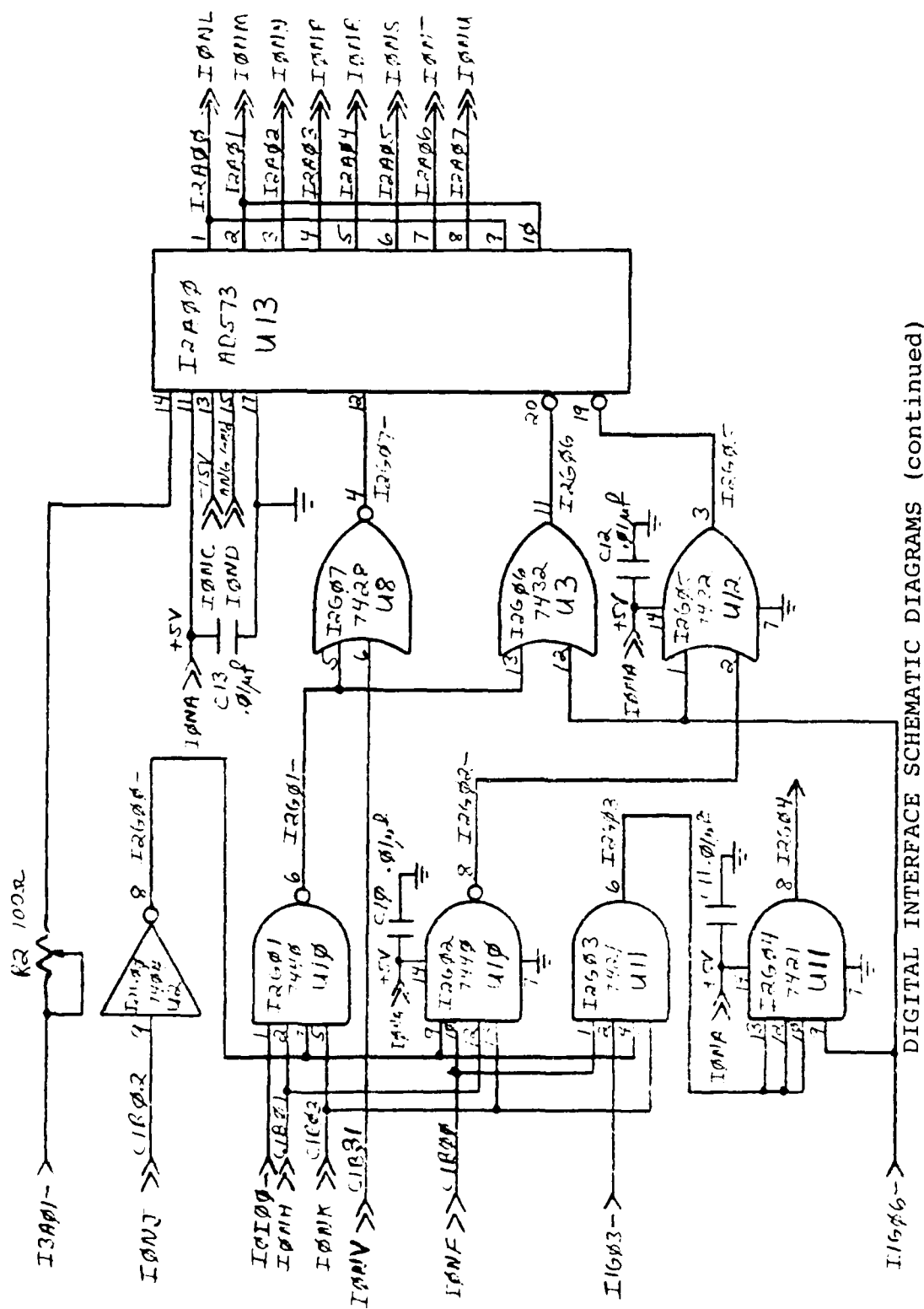
## APPENDIX B

Digital Interface Schematic Diagrams .....	B-2
Circuit Card I: Digital Interface Parts List .....	B-7
Digital Interface Device Layout .....	B-10

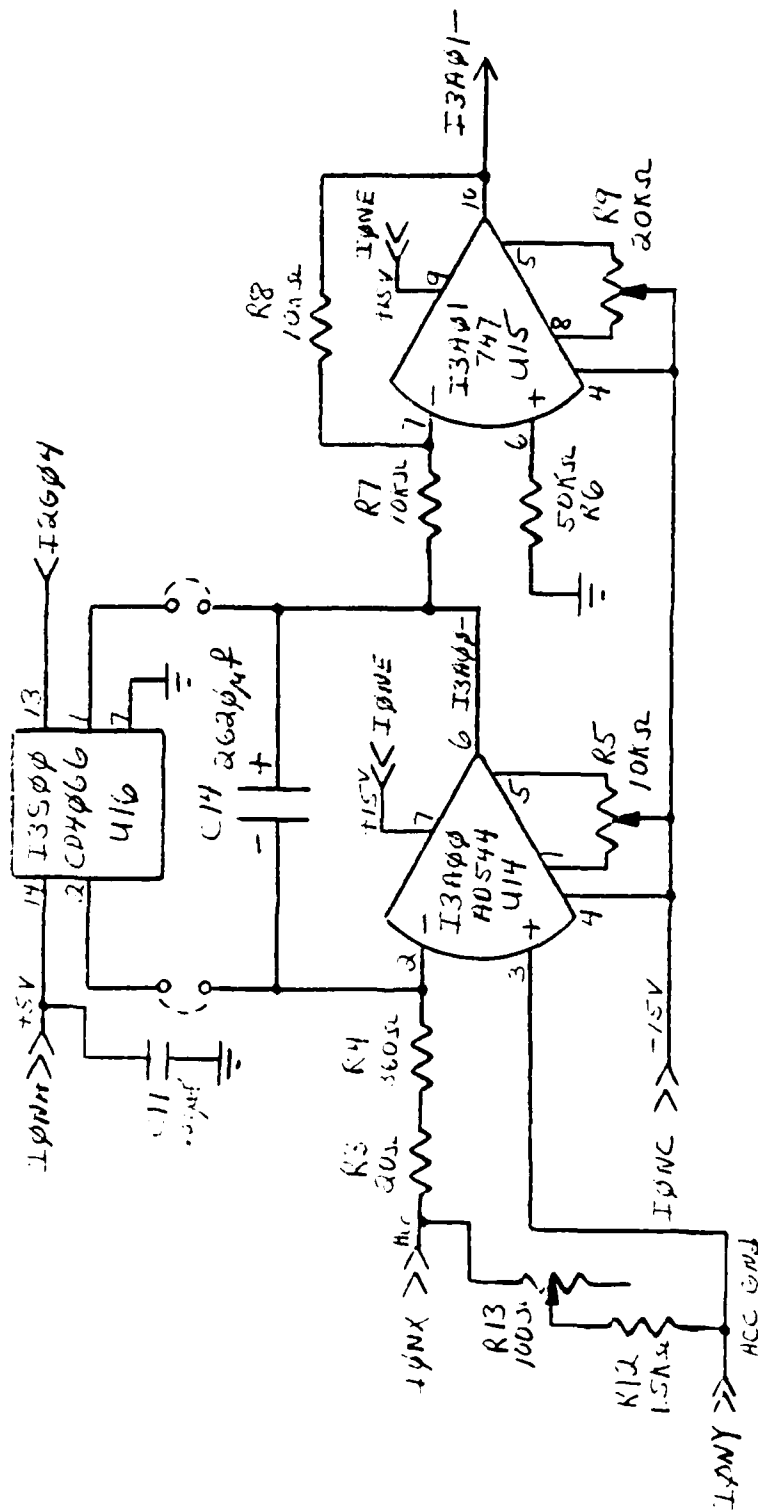


DIGITAL INTERFACE SCHEMATIC DIAGRAMS

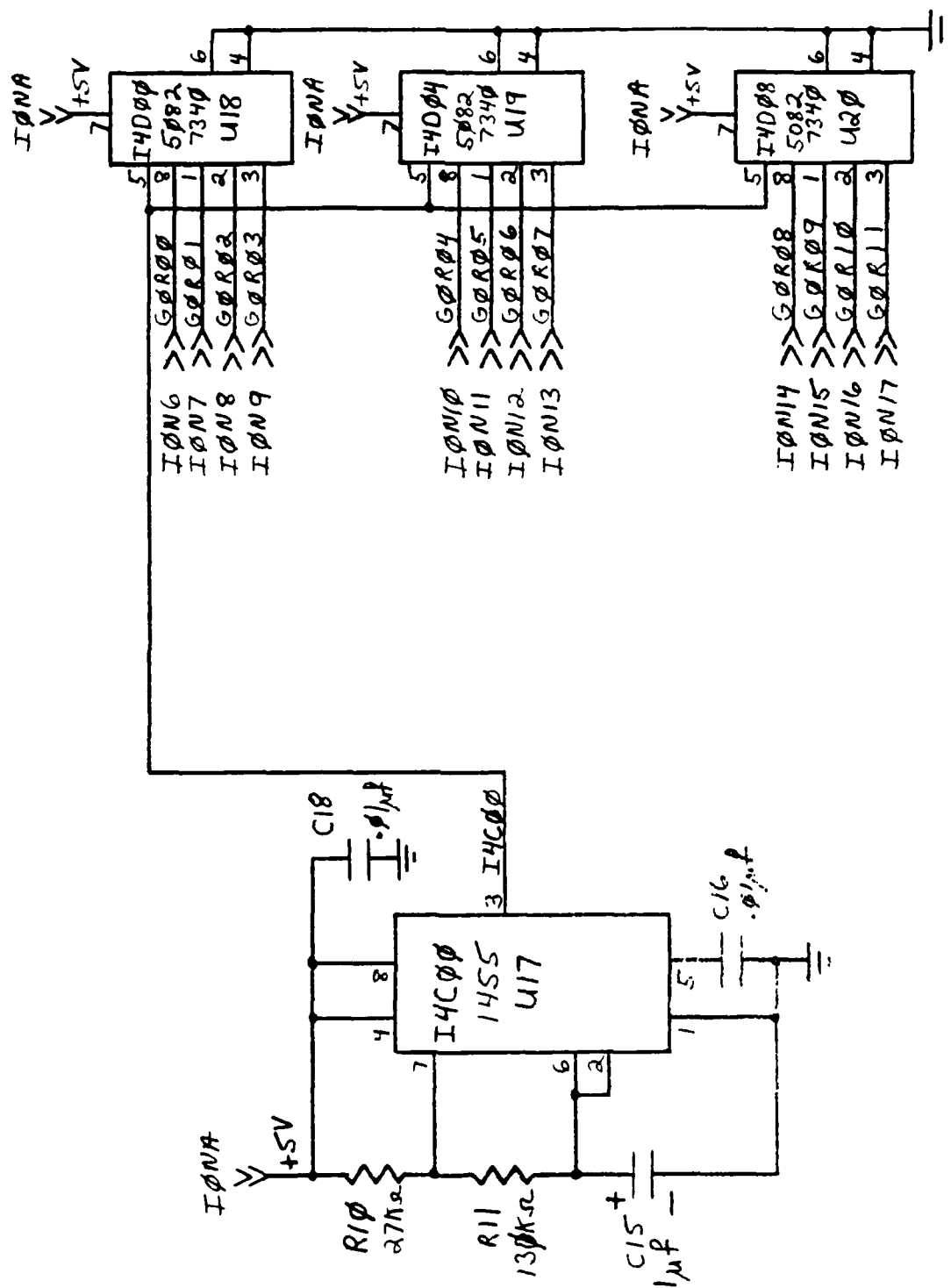




DIGITAL INTERFACE SCHEMATIC DIAGRAMS (continued)



DIGITAL INTERFACE SCHEMATIC DIAGRAMS (continued)



DIGITAL INTERFACE SCHEMATIC DIAGRAMS (continued)



Circuit Card I: Digital Interface  
Parts List

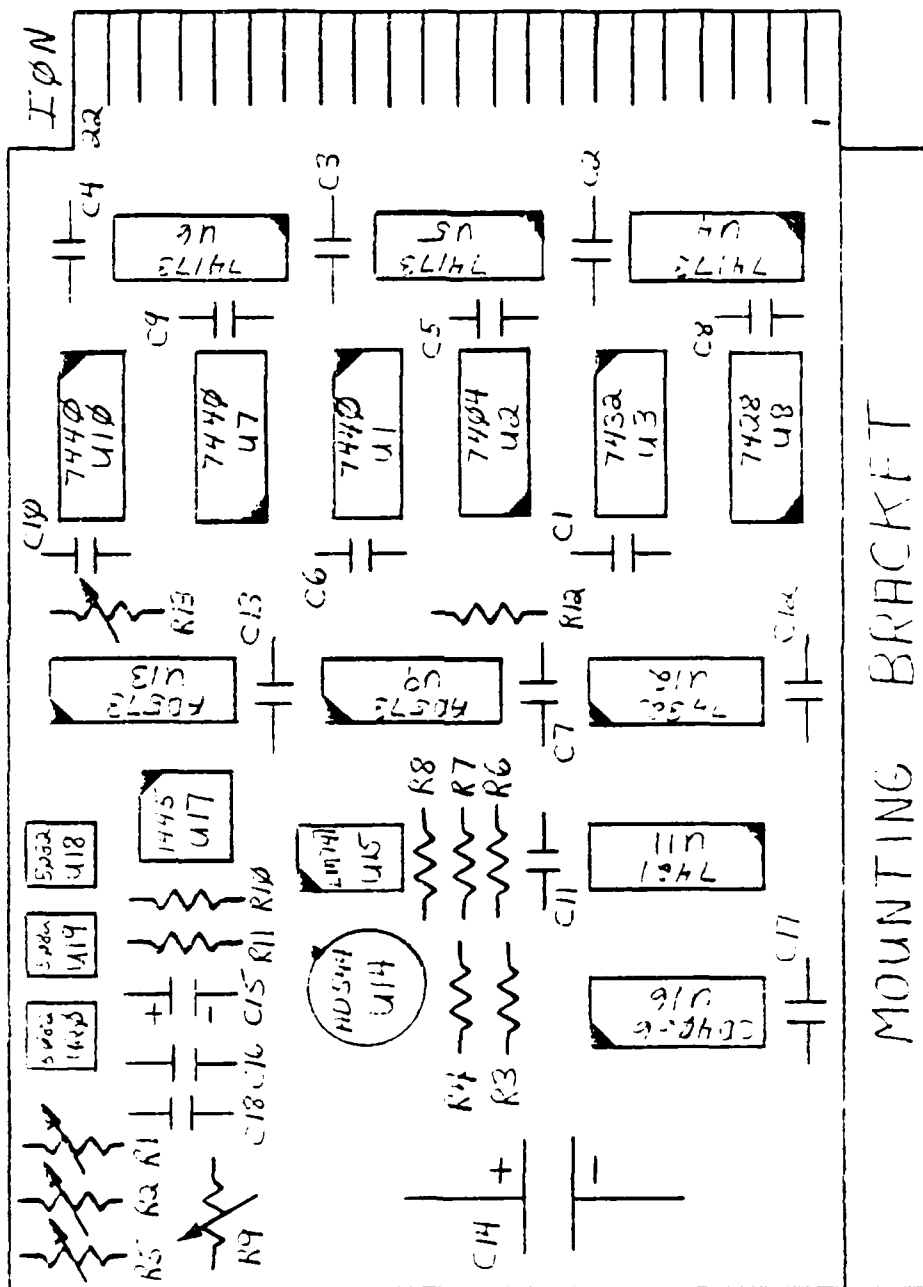
Part Number	Type	Schematic Reference #
7440	Dual 4-Input Positive NAND Buffers	U1 U7 U10
7404	Hex Inverters	U2
7432	Quadruple 2-Input Positive-OR Gates	U3 U12
74173	4-Bit D-Type Register With 3-State Outputs	U4 U5 U6
7428	Quadruple 2-Input Positive-NOR Gates	U8
AD 573	10-Bit Analog to Digital Converter	U9 U13
7421	Dual 4-Input Positive AND Gates	U11
AD 544	Precision Operational Amplifier	U14
LM 747	Dual Operational Amplifiers	U15
CD 4066	Quad Bilateral Switch	U16
1445	Dual Monostable Multivibrator	U17

Circuit Card I: Digital Interface  
Parts List (Continued)

Part Number	Type	Schematic Reference #
5082/7340	Single Digit HEX LED Display with Latches and Driver	U18 U19 U20
100	Variable Resistor (Ohms)	R1 R2 R13
20	Resistor (Ohms)	R3
360	Resistor (Ohms)	R4
10K	Variable Resistor (Ohms)	R5
50K	Resistor (Ohms)	R6
10K	Resistor (Ohms)	R7 R8
20K	Variable Resistor (Ohms)	R9
27K	Resistor (Ohms)	R10
130K	Resistor (Ohms)	R11
1.5K	Resistor (Ohms)	R12

Circuit Card I: Digital Interface  
Parts List (Continued)

Part Number	Type	Schematic Reference #
0.01 Micro	Capacitor (Farads)	C1
		C2
		C3
		C4
		C5
		C6
		C7
		C8
		C9
		C10
		C11
		C12
		C13
		C16
		C17
		C18
2220 Micro	Capacitor (Farads)	C14
1.0	Capacitor (Farads)	C15

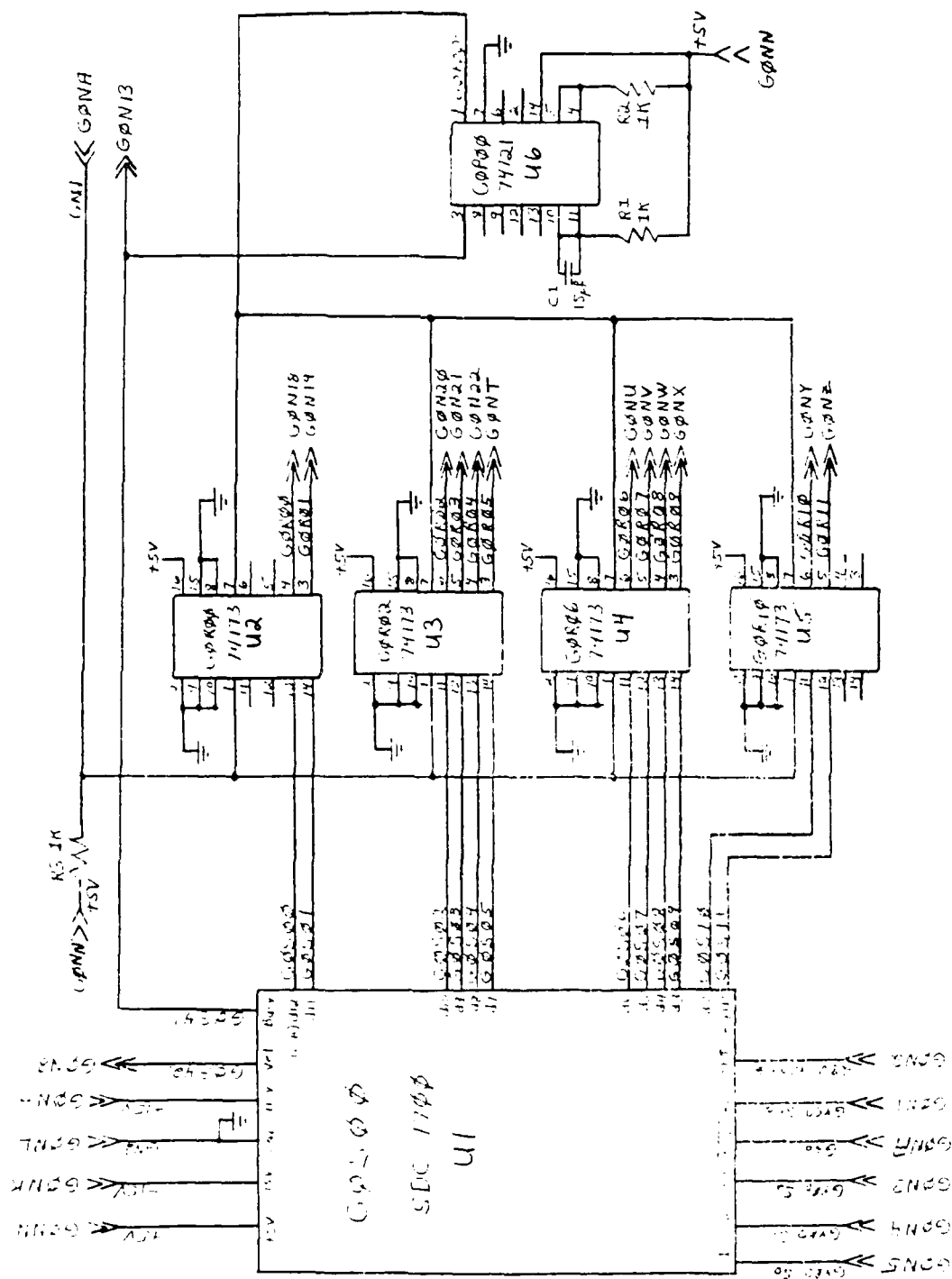


MOUNTING BRACKET

DIGITAL INTERFACE DEVICE LAYOUT

## APPENDIX C

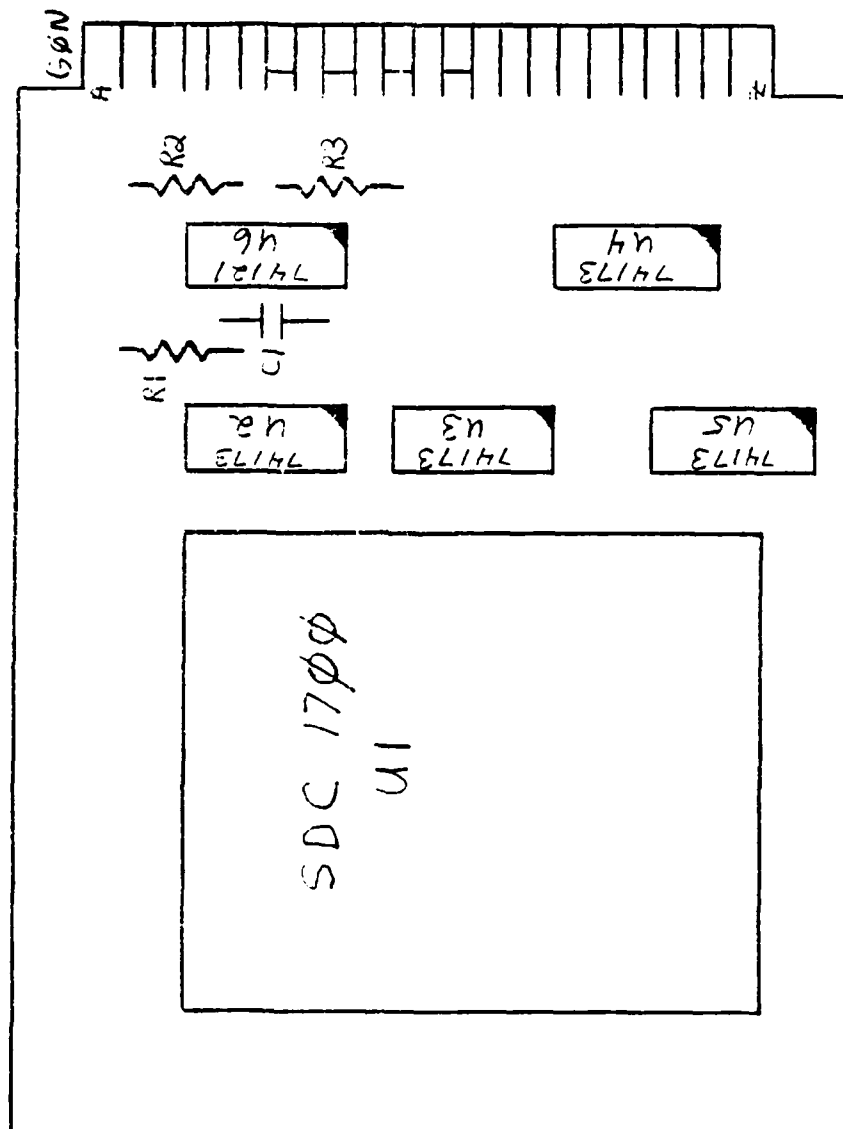
Syncro to Digital Schematic Diagram .....	C-2
Circuit Card G: Syncro to Digital Parts List .....	C-3
Syncro to Digital Device Layout .....	C-4



SYNCR0 TO DIGITAL SCHEMATIC DIAGRAM

Circuit Card G: Syncro to Digital  
Parts List

Part Number	Type	Schematic Reference #
SDC 1700	Syncro to Digital Converter	U1
74173	4-Bit D-Type Register With 3-State Outputs	U2 U3 U4 U5
74121	Monostable Multivibrator	U6
1K	Resistor (Ohms)	R1 R2 R3
15 pico	Capacitor (Farads)	C1

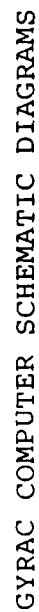


SYNCHRO TO DIGITAL DEVICE LAYOUT



## APPENDIX D

GYRAC Computer Schematic Diagrams .....	D-2
Circuit Card C: Computer Controller Parts List .....	D-4
GYRAC Computer Memory Map .....	D-7
GYRAC Computer Device Layout .....	D-9





# Circuit Card C: Computer Controller Parts List

Part Number	Type	Schematic Reference #
MC6802	Microprocessor with Clock and 128 Bytes RAM (CPU)	U1
74138	3-8 Line Decoders- Multiplexers	U2
2708	1024 x 8 bit U.V. Erasable PROM	U3
MC6840	Programmable Timer Module (PTM)	U4
MC6850	Asynchronous Communications Interface Adapter (ACIA)	U5
MC6821	Peripheral Interface Adapter (PIA)	U6
1489	Quad Line Receiver	U7
1488	Quad Line Driver	U8
7414	Hex Schmitt-Trigger Inverters	U9
MC7905CT	Negative 5 Volt Voltage Regulator	U10
SK3592	Positive 12 Volt Voltage Regulator	U11

Circuit Card C: Computer Controller  
Parts List (Continued)

Part Number	Type	Schematic Reference #
MC7912CT	Negative 12 Volt Voltage Regulator	U12
MB8416A	CMOS 2048 x 8 Byte Static RAM	U13
1N914	Signal Diode	D1
3579.545 KC	Crystal Oscillator	X1
3K	Resistor (Ohms)	R1
10K	Resistor (Ohms)	R2
1K	Resistor (Ohms)	R3
2.7K	Resistor (Ohms)	R4
22 Pico	Capacitor (Farads)	C1 C2
0.01 Micro	Capacitor (Farads)	C3 C4 C5 C6 C7 C15 C16 C18 C19 C20
100 Micro	Capacitor (Farads) 50 WVDC	C8

Circuit Card C: Computer Controller  
Parts List (Continued)

Part Number	Type	Schematic Reference #
10 Micro	Capacitor (Farads)	C9
	50 WVDC	C10
		C11
		C17
0.001 Micro	Capacitor (Farads)	C12
		C13
		C14

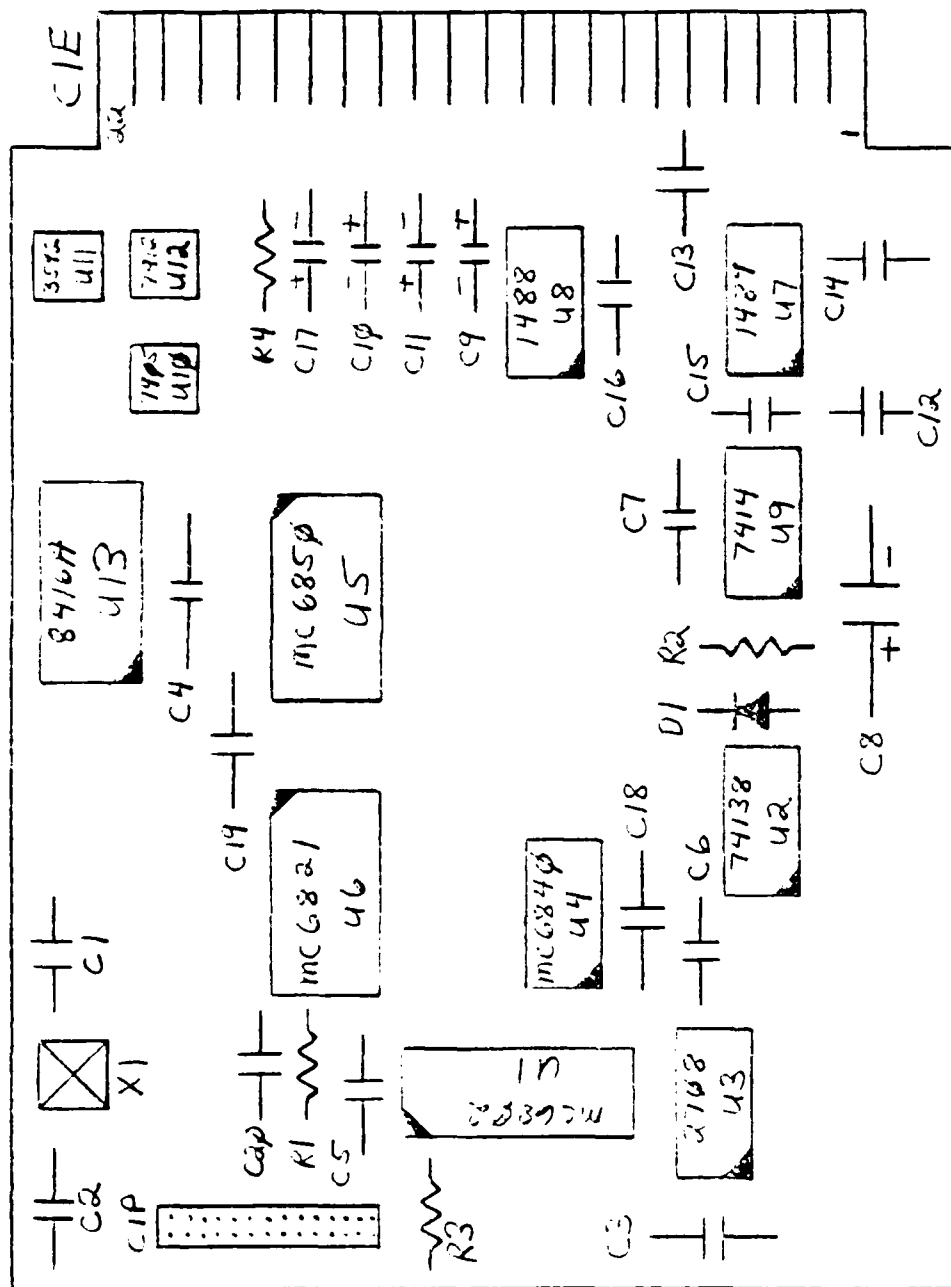
# GYRAC COMPUTER MEMORY MAP

ADDRESS (HEX)	DEVICE
0000 to 007F	0128 Bytes of on Processor Scratchpad RAM
6000 to 67FF	2048 Bytes of RAM (Alternate Addresses 7000-77FF)
8000	PIA Data Direction/Peripheral Register A (Alternate Address 9000)
8001	PIA Control Register A (Alternate Address 9001)
8002	PIA Data Direction/Peripheral Register B (Alternate Address 9002)
8003	PIA Control Register B (Alternate Address 9003)
A000	ACIA Control/Status Register (Alternate Address B000)
A001	ACIA TX Data/RX Data Register (Alternate Address B001)
C000	PTM Write Control Register #3/#1 (Alternate Address D000)
C001	PTM Write Control #2/Status Registers (Alternate Address D001)
C002	PTM MSB Buffer #1 Register/Timer #1 Counter (Alternate Address D002)
C003	PTM Timer #1 Latches/LSB Buffer #1 Register (Alternate Address D003)
C004	PTM MSB Buffer #2 Register/Timer #2 Counter (Alternate Address D004)
C005	PTM timer #2 Latches/LSB Buffer #2 Register (Alternate Address D005)

# GYRAC COMPUTER MEMORY MAP (continued)

ADDRESS (HEX)	DEVICE
C0060	PTM MSB Buffer #3 Register/Timer #3 Counter (Alternate Address D006)
C007	PTM Timer #3 Latches/LSB Buffer #3 Register (Alternate Address D007)
E000 to E3FF	1024 Bytes of GYRAC Control Program in EPROM (Alternate Addresses F000-F3FF)
E3FE to E3FF	Address of Reset Vector
E3FC to E3FD	Address of Non-maskable Interrupt Vector
E3FA to E3FB	Address of Software Interrupt Vector
E3F8 to E3F9	Address of Interrupt Vector



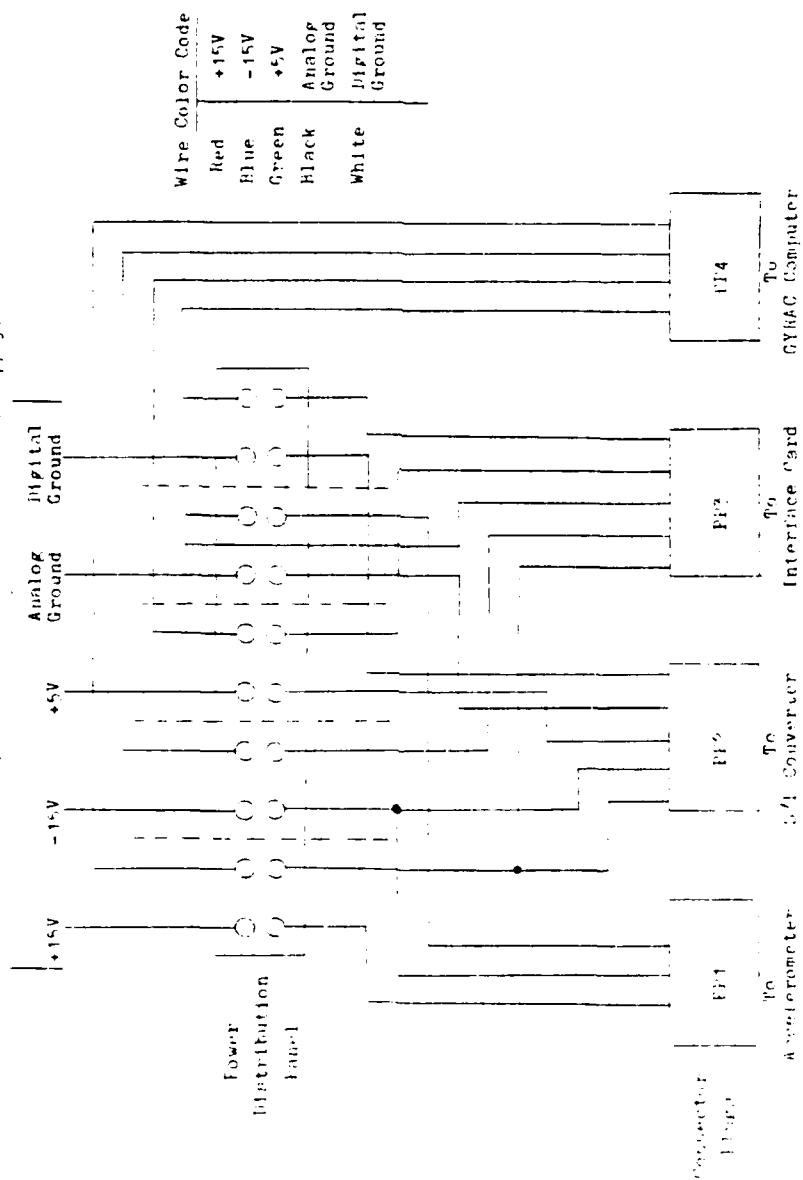


GYRAC COMPUTER DEVICE LAYOUT

## APPENDIX E

GYRAC Power Panel .....	E-2
GON: Syncro to Digital Edge Connector .....	E-3
C1P: GYRAC Computer Sensor Bus Connector .....	E-4
C1E: GYRAC Computer Edge Connector .....	E-5
ION: Digital Interface Edge Connector .....	E-6
H89 to GYRAC RS-232 Cable .....	E-7
H89 to NAV T or Drive Computer RS-232 Cable .....	E-8
GYRAC to NAV L Computer RS-232 Cable .....	E-9
Drive Computer to NAV X RS-232 Cable .....	E-10
GYRAC Wiring Harness .....	E-11

From Gyro Base Assembly (except +5V in from External Supply)



# GYRAC POWER PANEL

GON: Syncro to Digital Edge Connector

Pin Number	Signal Name	Description
GON1	None	GYRO Base Ground
GON2	None	GYRO Base 28 Volts 400 Hertz
GON3	None	GYRO Indicator S2
GON4	None	GYRO Indicator S1
GON5	None	GYRO Indicator S0
GON6		Unused
GON8	GOS42	Angular Velocity Analog Signal
GON13	GOS41	S to D Busy Signal (unused)
GON15		Unused
GON16		Unused
GON17		Unused
GON18	GOR00	D0 Data Bit
GON19	GOR01	D1 Data Bit
GON20	GOR02	D2 Data Bit
GON21	GOR03	D3 Data Bit
GON22	GOR04	D4 Data Bit
GONA	None	Digital Ground
GONF	None	+15 Volts DC
GONH	None	+15 Volts DC
GONJ	None	-15 Volts DC
GONK	None	-15 Volts DC
GONL	None	Analog Ground
GONM	None	Analog Ground
GONN	None	+5 Volts DC
GONP	None	+5 Volts DC
GONT	GOR05	D5 Data Bit
GONU	GOR06	D6 Data Bit
GONV	GOR07	D7 Data Bit
GONW	GOR08	D8 Data Bit
GONX	GOR09	D9 Data Bit
GONY	GOR10	D10 Data Bit
GONZ	GOR11	D11 Data Bit

# C1P: GYRAC Computer Sensor Bus Connector

Pin Number	Signal Name	Description
C1P1		Unused
C1P2		Unused
C1P3		Unused
C1P4		Unused
C1P5		Unused
C1P6		Unused
C1P7		Unused
C1P8		Unused
C1P9		Unused
C1P10		Unused
C1P11		Unused
C1P12		Unused
C1P13		Unused
C1P14		Unused
C1P15		Unused
C1P16	C1B10	Reserved (unused)
C1P17	None	+5 Volts (thru pullup resistor)
C1P18	C1B11	Reserved (unused)
C1P19	C1B30	Interrupt In (unused)
C1P20		Unused
C1P21	C1B31	Read/Write Out
C1P22	None	+5 Volts (thru pullup resistor)
C1P23	C1B03	A3 Sensor Address Bit
C1P24	C1B01	A1 Sensor Address Bit
C1P25	C1B25	D5 Sensor Data Bus
C1P26	C1B23	D3 Sensor Data Bus
C1P27	C1B21	D1 Sensor Data Bus
C1P28	C1B27	D7 Sensor Data Bus
C1P29	C1B26	D6 Sensor Data Bus
C1P30	C1B20	D0 Sensor Data Bus
C1P31	C1B22	D2 Sensor Data Bus
C1P32	C1B24	D4 Sensor Data Bus
C1P33	None	+5 Volts (thru pullup resistor)
C1P34	C1B00	A0 Sensor Address Bit
C1P35	C1B02	A2 Sensor Address Bit
C1P36	None	+5 Volts (thru pullup resistor)
C1P37	None	Digital Ground
C1P38	None	Digital Ground
C1P39	None	Digital Ground
C1P40	None	Digital Ground

# C1E: GYRAC Computer Edge Connector

Pin Number	Signal Name	Description
C1E1	None	Digital Ground
C1E2	C1G01-	Tx Data Out (active low)
C1E3	None	Rx Data In (active low)
C1E4	C1G00-	Ready to Send
C1E5	None	+5 Volts DC Out
C1E6		Unused
C1E7		Unused
C1E8	None	+5 Volts DC Out
C1E9		Unused
C1E10	None	Power On Reset (active low)
C1E11		Unused
C1E12	None	+15 Volts DC In
C1E13		Unused
C1E14	None	-12 Volts DC Out
C1E15		Unused
C1E16	None	+12 Volts DC Out
C1E17		Unused
C1E18	None	-5 Volts DC Out
C1E19		Unused
C1E20		Unused
C1E21	None	-15 Volts DC In
C1E22		Unused
C1EA	None	Digital Ground
C1EB		Unused
C1EC		Unused
C1ED		Unused
C1EE		Unused
C1EF		Unused
C1EH	None	Unused
C1EJ		Unused
C1EK		Unused
C1EL		Unused
C1EM		Unused
C1EN		Unused
C1EP		Unused
C1ER		Unused
C1ES		Unused
C1ET		Unused
C1EU		Unused
C1EV		Unused
C1EW		Unused
C1EX	None	+5 Volts (thru pullup resistor)
C1EY		Unused
C1EZ	None	+5 Volts DC In

# ION: Digital Interface Edge Connector

Pin Number	Signal Name	Description
ION1		Unused
ION2		Unused
ION3		Unused
ION4		Unused
ION5		Unused
ION6	GOR00	S/D D0 Data Bit
ION7	GOR01	S/D D1 Data Bit
ION8	GOR02	S/D D2 Data Bit
ION9	GOR03	S/D D3 Data Bit
ION10	GOR04	S/D D4 Data Bit
ION11	GOR05	S/D D5 Data Bit
ION12	GOR06	S/D D6 Data Bit
ION13	GOR07	S/D D7 Data Bit
ION14	GOR08	S/D D8 Data Bit
ION15	GOR09	S/D D9 Data Bit
ION16	GOR10	S/D D10 Data Bit
ION17	GOR11	S/D D11 Data Bit
ION18		Reserved
ION19		Reserved
ION20		Reserved
ION21		Reserved
ION22		Reserved
IONA	None	+5 Volts DC
IONB	None	Digital Ground
IONC	None	-15 Volts DC
IOND	None	Analog Ground
IONE	None	+15 Volts DC
IONF	C1B00	A0 Address Bit
IONH	C1B01	A1 Address Bit
IONJ	C1B02	A2 Address Bit
IONK	C1B03	A3 Address Bit
IONL	Bus	D0 Data Bit
IONM	Bus	D1 Data Bit
IONN	Bus	D2 Data Bit
IONP	Bus	D3 Data Bit
IONR	Bus	D4 Data Bit
IONS	Bus	D5 Data Bit
IONT	Bus	D6 Data Bit
IONU	Bus	D7 Data Bit
IONV	C1B31	Read/Write Control Line
IONW	GOS42	Angular Velocity Analog Signal
IONX	None	Acceleration Analog Signal
IONY	None	Acceleration Ground
IONZ		Unused

# H89 to GYRAC RS-232 Cable

89 Connector Pin Number	Signal Description	GYRAC Connector Pin Number
2	Tx Data	2
3	Rx Data	3
7	Ground	7



# H89 to Nav T or Drive Computer RS-232 Cable

Nav T/Drive Computer		
H89 Connector Pin Number	Signal Description	Connector Pin Number
2	Tx Data	3
3	Rx Data	2
7	Ground	7

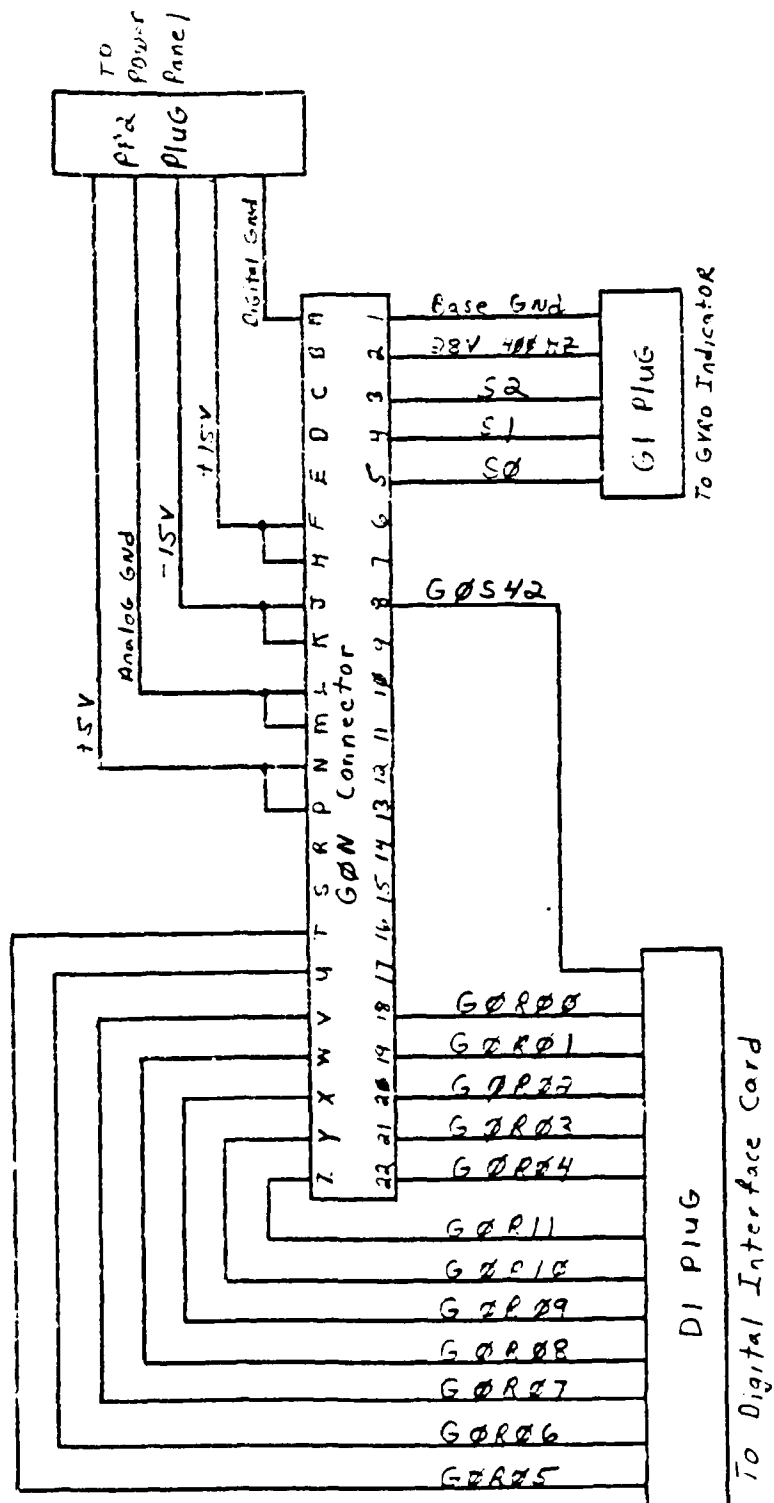
GYRAC to Nav L Computer RS-232 Cable

GYRAC Connector Pin Number	Signal Description	Nav L Connector Pin Number
2	Tx Data	3
3	Rx Data	2
7	Ground	7

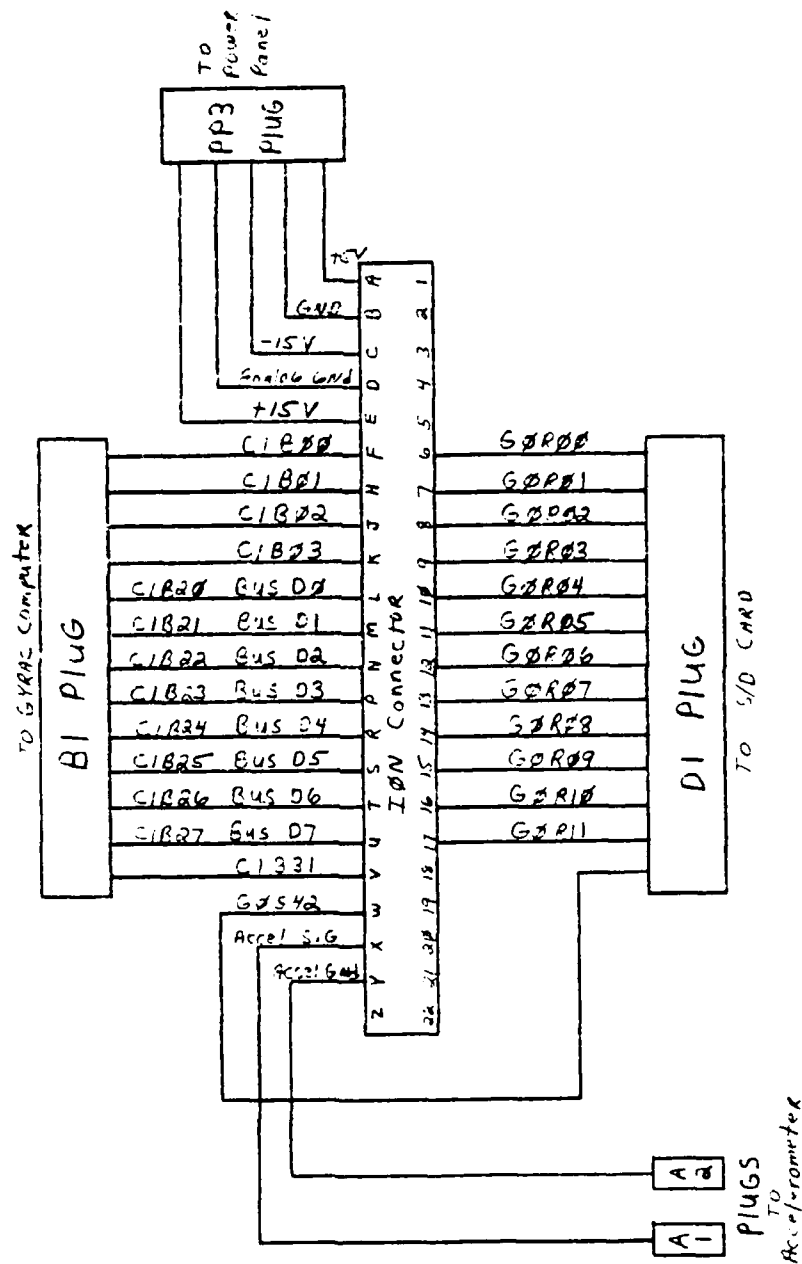
# Drive Computer to Nav X RS-232 Cable

Drive Computer Connector Pin Number	Signal Description	Nav X Connector Pin Number
---	-----------------------	-------------------------------

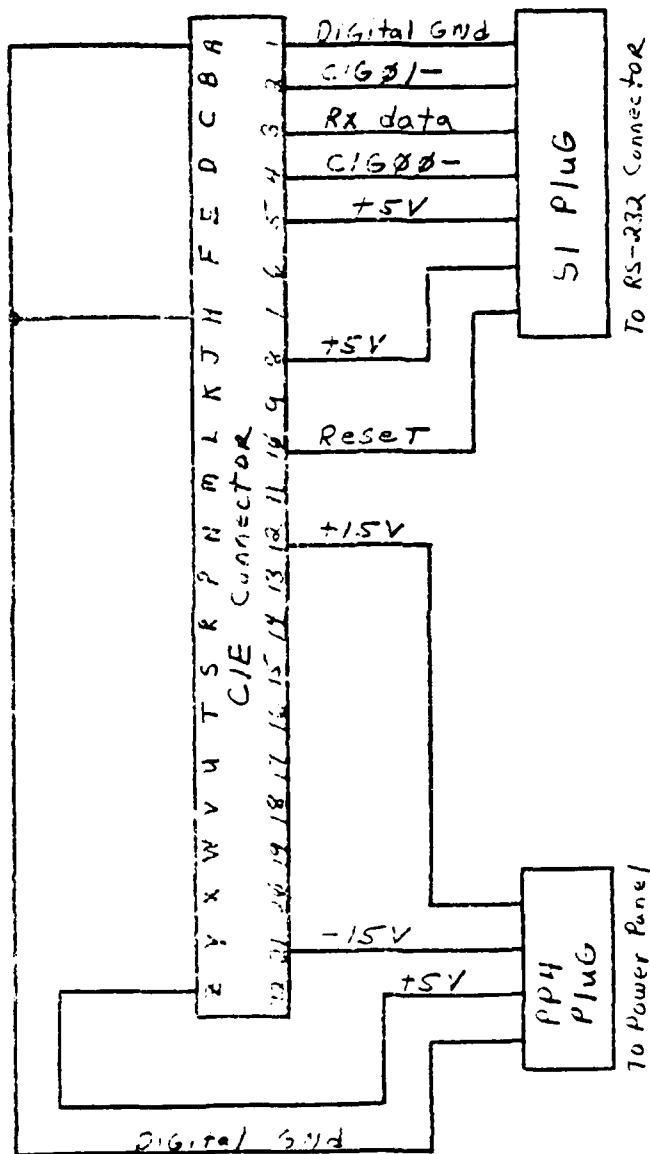
2	Tx Data	3
3	Rx Data	2
7	Ground	7



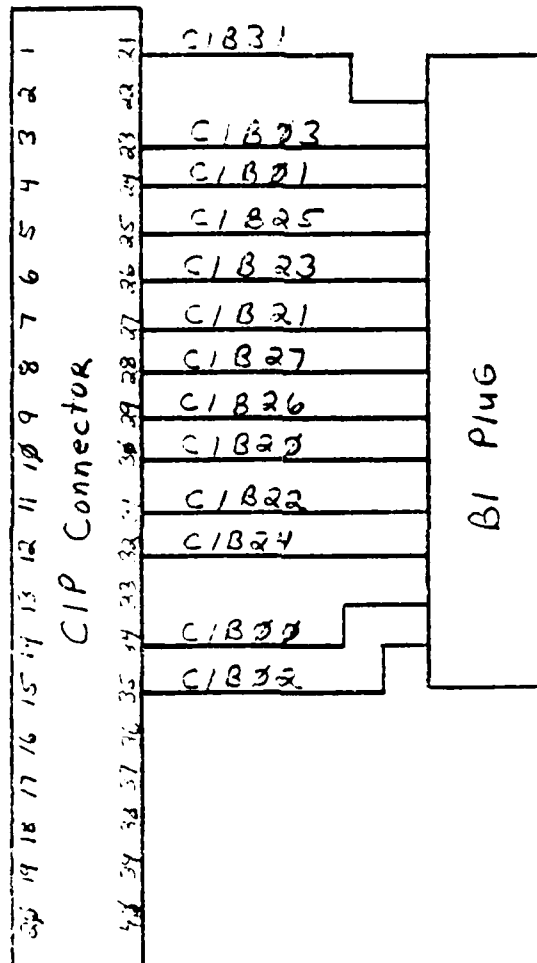
GYRAC WIRING HARNESS



GYRAC WIRING HARNESS (continued)



GYRAC WIRING HARNESS (continued)

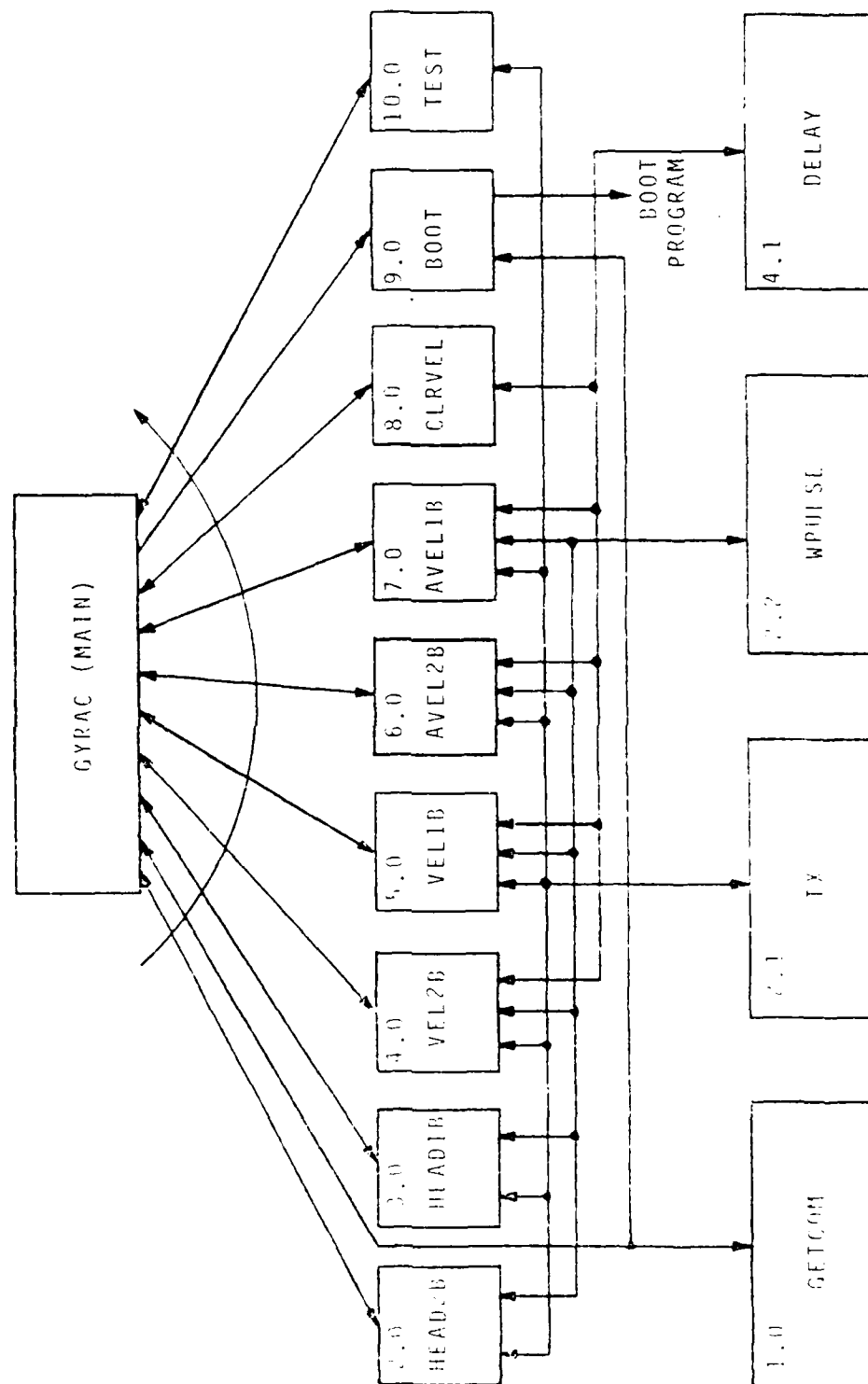


GYRAC WIRING HARNESS (continued)

## APPENDIX F

GYRAC.A Structure Chart .....	F-2
GYRAC.A Program Listing .....	F-3
GYRAC.A Operating Instructions .....	F-21





GYRAC.A STRUCTURE CHART

## GYRAC.A PROGRAM LISTING

```
DATE: 06-18-79
TIME: 11:11
TITLE: D FRC CONTROL PROGRAM
PROGRAMMER: RA41A
COMPILER: IBM XL C WILSON G. TAYLOR
SUBJECT: DFR AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A
MOBILE AUTONAVIGATOR THESES
OPERATING SYSTEM: IBM OS/VS M VLS41 MAGNOLIA MICROSYSTEMS INC
LANGUAGE: REXX ASSEMBLER V1.1 VIRTUAL SERVICES 1974
NOTE: This program is assembled and then burned into an EPROM
for operation and control of the D FRC subsystem.
CONTENTS: main
          getin
          readit
          writt
          calcl
          evalb
          averib
          averlt
          linvel
          boot
          test
          on
          pulse
          delay
FUNCTIONS: This program provides an RS-100 test, a RA41 boot
loader, the capability to read 1 or 2 types of
heading, angular velocity, and velocity and transmit
the data over an RS-100 interface, and can clear the
velocity to start in the Accelerometer Subsystem.
```

[illegible]

## GYRAC.A PROGRAM LISTING (continued)

0000	pinio	equ	10000H	;Timer module I/O address 0 pin or later
0001	staco	equ	17000H	;Initial stack pointer
0002	read	equ	1000H	;FPGA read port address
0003	write	equ	1004H	;FPGA write port address
0004	otctrl	equ	1004H	;OT 1 way to be written, use enable block
0005				;General OT mode, continuous operating mode, output enabled
0006	psctrl	equ	40000H	;Timer divide count to 5 = (2000000-1)/5
0007	addrreset	equ	1000H	;Give ACIA token pin to 147,148 Hz
0008	addradd	equ	1500H	;Reset ACIA command
0009				;Divide by 10 module, 8 bits data plus 1 stop bit, all interrupts disabled
0010	txreg	equ	0000H	;ACIA transmit data register empty
0011	rxreg	equ	0000H	;ACIA receive data register full
0012	headaddl	equ	0000H	;Address of GSRAC heading low byte
0013	headaddh	equ	0004H	;Address of GSRAC heading high byte
0014	veladdl	equ	0008H	;Address of GSRAC velocity low byte
0015	veladdh	equ	000CH	;Address of GSRAC velocity high byte
0016	avevel1	equ	0010H	;Address of GSRAC ang vel low byte
0017	avevelh	equ	0014H	;Address of GSRAC ang vel high byte
0018	velclear	equ	0000H	;Address of GSRAC vel clear device
0019	temp	equ	00000H	;Address of RAM scratch pad
0020	rambot	equ	00000H	;Address of bottom of 21 ram block
0021	blockb	equ	00000H	;Address of number of blocks of data
0022	bytes	equ	00000H	;Address of number of bytes in a block
0023	char	equ	00000H	;Address of current ASCII character
0024	charcnt	equ	00000H	;Address of current character count
0025	del	equ	0500H	;Timing delay loop variable

Address	Hex	Asm	Comment
0000		begin	Beginning of main program
0001	0F	init	Disable interrupts
0002	0E 07 FF	lis	#stack
			Initialize stack pointer to top of RAM
0004	4F	liara	Put zero in A reg
0005	17 00 01	staa	Clear AIA control register A
0006	07 00 01	staa	Clear AIA control register B
0007	17 00 01	staa	Make AIA port B an input port
0008	07	liara	
0009	07 00 00	staa	Make AIA port A an output port
0010	07 00	liara	#read
0011	07 00 01	staa	Prepare port A for data out & read
0012	07 00 00	staa	Prepare port B for data input
0013	07 00 01	staa	
0014	07 00 01	staa	
0015	07 00 00	staa	
0016	07 00 00	staa	
0017	07 00 00	staa	
0018	07 00 00	staa	
0019	07 00 00	staa	
0020	07 00 00	staa	
0021	07 00 00	staa	
0022	07 00 00	staa	
0023	07 00 00	staa	
0024	07 00 00	staa	
0025	07 00 00	staa	
0026	07 00 00	staa	
0027	07 00 00	staa	
0028	07 00 00	staa	
0029	07 00 00	staa	
0030	07 00 00	staa	
0031	07 00 00	staa	
0032	07 00 00	staa	
0033	07 00 00	staa	
0034	07 00 00	staa	
0035	07 00 00	staa	
0036	07 00 00	staa	
0037	07 00 00	staa	
0038	07 00 00	staa	
0039	07 00 00	staa	
0040	07 00 00	staa	
0041	07 00 00	staa	
0042	07 00 00	staa	
0043	07 00 00	staa	
0044	07 00 00	staa	
0045	07 00 00	staa	
0046	07 00 00	staa	
0047	07 00 00	staa	
0048	07 00 00	staa	
0049	07 00 00	staa	
0050	07 00 00	staa	
0051	07 00 00	staa	
0052	07 00 00	staa	
0053	07 00 00	staa	
0054	07 00 00	staa	
0055	07 00 00	staa	
0056	07 00 00	staa	
0057	07 00 00	staa	
0058	07 00 00	staa	
0059	07 00 00	staa	
0060	07 00 00	staa	
0061	07 00 00	staa	
0062	07 00 00	staa	
0063	07 00 00	staa	
0064	07 00 00	staa	
0065	07 00 00	staa	
0066	07 00 00	staa	
0067	07 00 00	staa	
0068	07 00 00	staa	
0069	07 00 00	staa	
0070	07 00 00	staa	
0071	07 00 00	staa	
0072	07 00 00	staa	
0073	07 00 00	staa	
0074	07 00 00	staa	
0075	07 00 00	staa	
0076	07 00 00	staa	
0077	07 00 00	staa	
0078	07 00 00	staa	
0079	07 00 00	staa	
0080	07 00 00	staa	
0081	07 00 00	staa	
0082	07 00 00	staa	
0083	07 00 00	staa	
0084	07 00 00	staa	
0085	07 00 00	staa	
0086	07 00 00	staa	
0087	07 00 00	staa	
0088	07 00 00	staa	
0089	07 00 00	staa	
0090	07 00 00	staa	
0091	0		

# GYRAC.A PROGRAM LISTING (continued)

B 40	01 40	1000	#0000	IFB command I in B register
B 41	01 41	1001	#0001	IFB command I in A register?
B 42	01 42	1002	#0002	IFB yes go execute command I
B 43	01 43	1003	#0003	IFB command J in B register
B 44	01 44	1004	#0004	IFB command J in A register?
B 45	01 45	1005	#0005	IFB yes go execute command J
B 46	01 46	1006	#0006	IFB command K in B register
B 47	01 47	1007	#0007	IFB command K in A register?
B 48	01 48	1008	#0008	IFB yes go execute command K
B 49	01 49	1009	#0009	IFB command L in B register
B 50	01 50	1010	#0010	IFB command L in A register?
B 51	01 51	1011	#0011	IFB yes go execute command L
B 52	01 52	1012	#0012	IFB command M in B register
B 53	01 53	1013	#0013	IFB command M in A register?
B 54	01 54	1014	#0014	IFB yes go execute command M
B 55	01 55	1015	#0015	IFB command N in B register
B 56	01 56	1016	#0016	IFB command N in A register?
B 57	01 57	1017	#0017	IFB yes go execute command N
B 58	01 58	1018	#0018	IFB command O in B register
B 59	01 59	1019	#0019	IFB command O in A register?
B 60	01 60	1020	#0020	IFB yes go execute command O
B 61	01 61	1021	#0021	IFB command P in B register
B 62	01 62	1022	#0022	IFB command P in A register?
B 63	01 63	1023	#0023	IFB yes go execute command P
B 64	01 64	1024	#0024	IFB command Q in B register
B 65	01 65	1025	#0025	IFB command Q in A register?
B 66	01 66	1026	#0026	IFB yes go execute command Q
B 67	01 67	1027	#0027	IFB command R in B register
B 68	01 68	1028	#0028	IFB command R in A register?
B 69	01 69	1029	#0029	IFB yes go execute command R
B 70	01 70	1030	#0030	IFB command S in B register
B 71	01 71	1031	#0031	IFB command S in A register?
B 72	01 72	1032	#0032	IFB yes go execute command S
B 73	01 73	1033	#0033	IFB command T in B register
B 74	01 74	1034	#0034	IFB command T in A register?
B 75	01 75	1035	#0035	IFB yes go execute command T
B 76	01 76	1036	#0036	IFB command U in B register
B 77	01 77	1037	#0037	IFB command U in A register?
B 78	01 78	1038	#0038	IFB yes go execute command U
B 79	01 79	1039	#0039	IFB command V in B register
B 80	01 80	1040	#0040	IFB command V in A register?
B 81	01 81	1041	#0041	IFB yes go execute command V
B 82	01 82	1042	#0042	IFB command W in B register
B 83	01 83	1043	#0043	IFB command W in A register?
B 84	01 84	1044	#0044	IFB yes go execute command W
B 85	01 85	1045	#0045	IFB command X in B register
B 86	01 86	1046	#0046	IFB command X in A register?
B 87	01 87	1047	#0047	IFB yes go execute command X
B 88	01 88	1048	#0048	IFB command Y in B register
B 89	01 89	1049	#0049	IFB command Y in A register?
B 90	01 90	1050	#0050	IFB yes go execute command Y
B 91	01 91	1051	#0051	IFB command Z in B register
B 92	01 92	1052	#0052	IFB command Z in A register?
B 93	01 93	1053	#0053	IFB yes go execute command Z
B 94	01 94	1054	#0054	IFB command A in B register
B 95	01 95	1055	#0055	IFB command A in A register?
B 96	01 96	1056	#0056	IFB yes go execute command A
B 97	01 97	1057	#0057	IFB command B in B register
B 98	01 98	1058	#0058	IFB command B in A register?
B 99	01 99	1059	#0059	IFB yes go execute command B
B 100	01 100	1060	#0060	IFB command C in B register
B 101	01 101	1061	#0061	IFB command C in A register?
B 102	01 102	1062	#0062	IFB yes go execute command C
B 103	01 103	1063	#0063	IFB command D in B register
B 104	01 104	1064	#0064	IFB command D in A register?
B 105	01 105	1065	#0065	IFB yes go execute command D
B 106	01 106	1066	#0066	IFB command E in B register
B 107	01 107	1067	#0067	IFB command E in A register?
B 108	01 108	1068	#0068	IFB yes go execute command E
B 109	01 109	1069	#0069	IFB command F in B register
B 110	01 110	1070	#0070	IFB command F in A register?
B 111	01 111	1071	#0071	IFB yes go execute command F
B 112	01 112	1072	#0072	IFB command G in B register
B 113	01 113	1073	#0073	IFB command G in A register?
B 114	01 114	1074	#0074	IFB yes go execute command G
B 115	01 115	1075	#0075	IFB command H in B register
B 116	01 116	1076	#0076	IFB command H in A register?
B 117	01 117	1077	#0077	IFB yes go execute command H
B 118	01 118	1078	#0078	IFB command I in B register
B 119	01 119	1079	#0079	IFB command I in A register?
B 120	01 120	1080	#0080	IFB yes go execute command I
B 121	01 121	1081	#0081	IFB command J in B register
B 122	01 122	1082	#0082	IFB command J in A register?
B 123	01 123	1083	#0083	IFB yes go execute command J
B 124	01 124	1084	#0084	IFB command K in B register
B 125	01 125	1085	#0085	IFB command K in A register?
B 126	01 126	1086	#0086	IFB yes go execute command K
B 127	01 127	1087	#0087	IFB command L in B register
B 128	01 128	1088	#0088	IFB command L in A register?
B 129	01 129	1089	#0089	IFB yes go execute command L
B 130	01 130	1090	#0090	IFB command M in B register
B 131	01 131	1091	#0091	IFB command M in A register?
B 132	01 132	1092	#0092	IFB yes go execute command M
B 133	01 133	1093	#0093	IFB command N in B register
B 134	01 134	1094	#0094	IFB command N in A register?
B 135	01 135	1095	#0095	IFB yes go execute command N
B 136	01 136	1096	#0096	IFB command O in B register
B 137	01 137	1097	#0097	IFB command O in A register?
B 138	01 138	1098	#0098	IFB yes go execute command O
B 139	01 139	1099	#0099	IFB command P in B register
B 140	01 140	1100	#0100	IFB command P in A register?
B 141	01 141	1101	#0101	IFB yes go execute command P
B 142	01 142	1102	#0102	IFB command Q in B register
B 143	01 143	1103	#0103	IFB command Q in A register?
B 144	01 144	1104	#0104	IFB yes go execute command Q
B 145	01 145	1105	#0105	IFB command R in B register
B 146	01 146	1106	#0106	IFB command R in A register?
B 147	01 147	1107	#0107	IFB yes go execute command R
B 148	01 148	1108	#0108	IFB command S in B register
B 149	01 149	1109	#0109	IFB command S in A register?
B 150	01 150	1110	#0110	IFB yes go execute command S
B 151	01 151	1111	#0111	IFB command T in B register
B 152	01 152	1112	#0112	IFB command T in A register?
B 153	01 153	1113	#0113	IFB yes go execute command T
B 154	01 154	1114	#0114	IFB command U in B register
B 155	01 155	1115	#0115	IFB command U in A register?
B 156	01 156	1116	#0116	IFB yes go execute command U
B 157	01 157	1117	#0117	IFB command V in B register
B 158	01 158	1118	#0118	IFB command V in A register?
B 159	01 159	1119	#0119	IFB yes go execute command V
B 160	01 160	1120	#0120	IFB command W in B register
B 161	01 161	1121	#0121	IFB command W in A register?
B 162	01 162	1122	#0122	IFB yes go execute command W
B 163	01 163	1123	#0123	IFB command X in B register
B 164	01 164	1124	#0124	IFB command X in A register?
B 165	01 165	1125	#0125	IFB yes go execute command X
B 166	01 166	1126	#0126	IFB command Y in B register
B 167	01 167	1127	#0127	IFB command Y in A register?
B 168	01 168	1128	#0128	IFB yes go execute command Y
B 169	01 169	1129	#0129	IFB command Z in B register
B 170	01 170	1130	#0130	IFB command Z in A register?
B 171	01 171	1131	#0131	IFB yes go execute command Z
B 172	01 172	1132	#0132	IFB command A in B register
B 173	01 173	1133	#0133	IFB command A in A register?
B 174	01 174	1134	#0134	IFB yes go execute command A
B 175	01 175	1135	#0135	IFB command B in B register
B 176	01 176	1136	#0136	IFB command B in A register?
B 177	01 177	1137	#0137	IFB yes go execute command B
B 178	01 178	1138	#0138	IFB command C in B register
B 179	01 179	1139	#0139	IFB command C in A register?
B 180	01 180	1140	#0140	IFB yes go execute command C
B 181	01 181	1141	#0141	IFB command D in B register
B 182	01 182	1142	#0142	IFB command D in A register?
B 183	01 183	1143	#0143	IFB yes go execute command D
B 184	01 184	1144	#0144	IFB command E in B register
B 185	01 185	1145	#0145	IFB command E in A register?
B 186	01 186	1146	#0146	IFB yes go execute command E
B 187	01 187	1147	#0147	IFB command F in B register
B 188	01 188	1148	#0148	IFB command F in A register?
B 189	01 189	1149	#0149	IFB yes go execute command F
B 190	01 190	1150	#0150	IFB command G in B register
B 191	01 191	1151	#0151	IFB command G in A register?
B 192	01 192	1152	#0152	IFB yes go execute command G
B 193	01 193	1153	#0153	IFB command H in B register
B 194	01 194	1154	#0154	IFB command H in A register?
B 195	01 195	1155	#0155	IFB yes go execute command H
B 196	01 196	1156	#0156	IFB command I in B register
B 197	01 197	1157	#0157	IFB command I in A register?
B 198	01 198	1158	#0158	IFB yes go execute command I
B 199	01 199	1159	#0159	IFB command J in B register
B 200	01 200	1160	#0160	IFB command J in A register?
B 201	01 201	1161	#0161	IFB yes go execute command J
B 202	01 202	1162	#0162	IFB command K in B register
B 203	01 203	1163	#0163	IFB command K in A register?
B 204	01 204	1164	#0164	IFB yes go execute command K
B 205	01 205	1165	#0165	IFB command L in B register
B 206	01 206	1166	#0166	IFB command L in A register?
B 207	01 207	1167	#0167	IFB yes go execute command L
B 208	01 208	1168	#0168	IFB command M in B register
B 209	01 209	1169	#0169	IFB command M in A register?
B 210	01 210	1170	#0170	IFB yes go execute command M
B 211	01 211	1171	#0171	IFB command N in B register
B 212	01 212	1172	#0172	IFB command N in A register?
B 213	01 213	1173	#0173	IFB yes go execute command N
B 214	01 214	1174	#0174	IFB command O in B register
B 215	01 215	1175	#0175	IFB command O in A register?
B 216	01 216	1176	#0176	IFB yes go execute command O
B 217	01 217	1177	#0177	IFB command P in B register
B 218	01 218	1178	#0178	IFB command P in A register?
B 219	01 219	1179	#0179	IFB yes go execute command P
B 220	01 220	1180	#0180	IFB command Q in B register
B 221	01 221	1181	#0181	IFB command Q in A register?
B 222	01 222	1182	#0182	IFB yes go execute command Q
B 223	01 223	1183	#0183	IFB command R in B register
B 224	01 224	1184	#0184	IFB command R in A register?
B 225	01 225	1185	#0185	IFB yes go execute command R
B 226	01 226	1186	#0186	IFB command S in B register
B 227	01 227	1187	#0187	IFB command S in A register?
B 228	01 228	1188	#0188	IFB yes go execute command S
B 229	01 229	1189	#0189	IFB command T in B register
B 230	01 230	1190	#0190	IFB command T in A register?
B 231	01 231	1191	#0191	IFB yes go execute command T
B 232	01 232	1192	#0192	IFB command U in B register
B 233	01 233	1193	#0193	IFB command U in A register?
B 234	01 234	1194	#0194	IFB yes go execute command U
B 235	01 235	1195	#0195	IFB command V in B register
B 236	01 236	1196	#0196	IFB command V in A register?
B 237	01 237	1197	#0197	IFB yes go execute command V
B 238	01 238	1198	#0198	IFB command W in B register
B 239	01 239	1199	#0199	IFB command W in A register?
B 240				

# GYRAC.A PROGRAM LISTING (continued)

```

B017 10 B1 17      jsr    avel1b    ;Read and T: 1 byte of ang vel
B018 7E B1 17      jmp     input    ;Get next command

B01E 00 B0 FA cmdD jsr    head1b    ;Read and T: 2 bytes of heading
B01F 7E B0 FA      jmp     input    ;Get next command

B044 10 B1 11 cmdD jsr    head1b    ;Read and T: 1 byte of heading
B045 7E B0 10      jmp     input    ;Get next command

B04A 10 B1 41 cmdE jsr    vel1b     ;Read and T: 2 bytes of velocity
B04B 7E B0 36      jmp     input    ;Get next command

B010 00 B1 74 cmdF jsr    vel1b     ;Read and T: 1 byte of velocity
B011 7E B0 36      jmp     input    ;Get next command

B056 00 B1 10 cmdG jsr    dirvel    ;Clear velocity constant
B057 7E B0 36      jmp     input    ;Get next command

B061 00 B1 36 cmdH jsr    avel2b    ;Read and T: 2 bytes of ang vel
B062 7E B0 36      jmp     input    ;Get next command

B06C 00 B1 09 cmdI jsr    avel1b    ;Read and T: 1 byte of ang vel
B06D 7E B0 16      jmp     input    ;Get next command

B013 00 B0 FA cmdJ jsr    head2b    ;Read and T: 2 bytes of heading
B014 10 B1 41      jsr    vel1b     ;Read and T: 2 bytes of velocity
B015 7E B0 36      jmp     input    ;Get next command

B001 00 B1 19 cmdK jsr    head1b    ;Read and T: 1 byte of heading
B004 10 B1 74      jsr    vel1b     ;Read and T: 1 byte of velocity
B007 7E B0 10      jmp     input    ;Get next command

B00A 7E B0 06 cmdL jmp     init     ;Reset and re-initialize GYRAC

B000 7E B1 E2 cmdM jmp     boot     ;Load Raw heading from RS-232 & execute

B1E0 00 B1 6C cmdN jsr    test     ;If printable char to RS-232
B1E1 7E B0 31      jmp     input    ;Get next command

B0E1 00 B1 10 cmdO jsr    head1b    ;Read and T: 1 byte of heading
B0E2 10 B1 41      jsr    vel1b     ;Read and T: 2 bytes of velocity
B0E3 7E B0 16      jmp     input    ;Get next command

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 5/10/85
VERSION: 1.0
NAME: getcom
MODULE NUMBER: 1.0
DESCRIPTION: This module reads an Asci: byte from the ACIA
and places it in the A register. It will loop
indefinitely until a byte is read.
RAISED VARIABLES: None
RETURN: Asci: command byte in the A register
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAME JR.
HISTORY: NONE

```

```

BDEF 04 A0 00 getcom ldaa aciastat ;Get ACIA (PS-232) status
BDEF 04 01 andra ;Is receive data register full
BDEF 07 00 beq getcom ;If no loop to getcom
BDEF 05 A0 01 ldaa aciadata ;Else read command byte from ACIA
BDEF 07 01 rts

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 05/15/82
VERSION: 1.1
NAME: head2b
MODULE NUMBER: 204
DESCRIPTION: This module sends a write pulse to the gyro heading data register to latch the data, reads two bytes of heading data, and sends the data, high byte first, to the ACIA (53-132) output. Only the least significant 12 bits of the data is significant.
PASSED VARIABLES: None
RETURNS: Two bytes of heading data written to ACIA (53-132)
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: tp, wpulse
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 original
        Version 1.1 change heading data format

```

```

E0FA 36 0F head2b ldaa #headaddl ;Get address of LSB of heading
E0FC 87 30 00 staa piadataA ;Write LSB heading address to GYRAC
E0FE 80 ED 23 ;sr wpulse ;Send GYRAC write pulse to latch data
E100 85 0E ldaa #headaddh ;Get address of MSB of heading
E102 87 30 00 staa piadataA ;Write MSB heading address to GYRAC
E104 85 38 02 ldsb piadataB ;Read MSB of heading from GYRAC
E106 80 ED 1F ;sr tp ;Send MSB of heading to ACIA
E108 36 0F ldaa #headaddl ;Get address of LSB of heading
E10A 87 30 00 staa piadataA ;Write LSB heading address to GYRAC
E10C 85 38 02 ldsb piadataB ;Read LSB of heading from GYRAC
E10E 80 ED 1F ;sr tp ;Send LSB of heading to ACIA
E110 39 rts

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 05/14/85
VERSION: 1.0
NAME: GA
MODULE NUMBER: 2.1
DESCRIPTION: This module tests the status of the ACIA for an
             empty transmit data register in an indefinite
             loop until found and then the data in the B
             register is sent to the ACIA RS-232 output.
PARM VARIABLES: Input data byte in the B register
RETURN: Data byte output to ACIA
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: readit
                  readb
                  vll2b
                  vll1b
                  ave10c
                  ave11c
AUTHOR: CAPT WILLIAM J. SAMEY JR.
HISTORY: NONE

```

```

E210 16 00 00 00      10aa  acrststat  ;Read ACIA (RS-232) status
E211 17 02          10ab  *done      ;Is ACIA transmit data register empty?
E212 18 00          10ac  *x         ;If no, loop to 16 and recheck status
E213 19 00 00 00      10ad  acrddata  ;Else transmit data in B reg to ACIA
E214 20 00 00 00      10ae  rts

```



# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 10/10/85
VERSION: 1.1
NAME: wpulse
MODULE NUMBER: 0.1
DESCRIPTION: This module sends a write pulse to the GYRAC.
PULSED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: 0
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: head0b
                  head1b
                  head2b
                  head3b
                  head4b
                  head5b
AUTHOR: CAPT WILLIAM H. RAMEY JR.
HISTORY: NONE

```

```

8223 06 14 wpulse 1dab #write :Get GYRAC write command
8225 F7 30 01 stab piactr1A :Send GYRAC write level to latch data
8228 06 10 1dab #read :Get GYRAC read command
8229 F7 30 01 stab piactr1A :Send GYRAC read level to form a pulse
8230 39

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 05/16/85
VERSION: 1.1
NAME: headb
MODULE NUMBER: 0.0
DESCRIPTION: This module sends a write pulse to the gyro
             heading data register to latch the data, reads
             the bytes of heading data, adjusts the data to
             form a byte of the 8 most significant bits, and
             sends this byte of heading data to the ACIA
             (RS-232) output.
RAISED VARIABLES: None
RETURN: One byte of heading data written to ACIA (RS-232)
GLOBAL VARIABLES USED: temp
GLOBAL VARIABLES CHANGED: temp
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: tcr
             upulse
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 original
         Version 1.1 change heading data format

```

```

E119 56 0F headb ldaa #headadd1 ;Get address of LSB of heading
E11B 57 50 00 staa piadataA ;Write address of LSB of head to GYRAC
E11E 5D E2 03 jsr upulse ;Send GYRAC write pulse to latch data
E121 56 4E ldaa #headaddh ;Get address of MSB of heading
E123 57 50 00 staa piadataA ;Write address of MSB of head to GYRAC
E126 58 50 02 ldab piadataB ;Read MSB of heading data
E129 59 aslb ;Move lower 4 bits to upper 4 bits
E12A 59 aslb ;and shift 4 bytes into the lower
E12B 59 aslb ;4 bits--i.e. 00000000. This will
E12C 59 aslb ;form the MS nibble of the heading byte
E12E 56 0F ldaa #headaddl ;Get address of LSB of heading
E12F 57 50 00 staa piadataA ;Write address of LSB of head to GYRAC
E132 58 50 02 ldab piadataB ;Read LSB of heading data
E135 44 lraa ;Move upper 4 bits to lower 4 bits
E136 44 lraa ;and shift 4 bytes into the upper
E137 44 lraa ;4 bits--i.e. 00000000. This will
E138 44 lraa ;form the LB nibble of the heading byte
E139 57 00 staa temp ;Save the LB nibble of the heading
E13C 5A 00 erat temp ;Form 8 bits of heading (1 byte)
E13D 5D E2 13 jsr tcr ;Output 1 byte of heading to ACIA
E140 39 rts

```

GYRAC.A PROGRAM LISTING (continued)

```

DATE: 04/01/97
VERSION: 1.1
NAME: vel1
MODULE NUMBER: 1.0
DESCRIPTION: This module sends a write pulse to the AD7894
              velocity data register to latch the data, reads
              the bytes of velocity data, generates and sends
              the data, MID first, to the ASCII RS-232C output.
              Only the least significant 10 bits of the data is
              significant.
PAUSED VARIABLE: None
RETURN: Two bytes of velocity data written to ASCII (RG-200)
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTER USED: A, C
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: to
                  pulse
                  delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 Original
          Version 1.1 change velocity data format

```

E141	36	0A	ve12b	ldaa	#veladdr	:Get address of MSB of velocity
E142	07	80	00	staa	piadataA	:Write MSB velocity address to GPRAC
E143	00	ED	01	lsrc	iculse	:Send GPRAC write pulse to latch data
E149	00	ED	0E	lsrc	delay	:Allow for A to D conversion time
E140	01	39	02	ldat	piadataA	:Read MSB of heading from GPRAC
E14F	07	80		staa	temp	:Save raw MSB of data
E151	94			lsrcb		:Form correct MSB
E152	94			lsrcb		
E153	94			lsrcb		
E154	94			lsrcb		
E155	94			lsrcb		
E156	94			lsrcb		
E157	00	ED	10	lsrc	hi	:Send MSB of heading to ADC
E158	08	10		ldaa	#veladdr1	:Get address of LSB of velocity
E159	07	80	00	staa	piadataA	:Write LSB velocity address to GPRAC
E15A	00	ED	02	ldat	piadataA	:Read LSB of velocity from GPRAC
E15B	94			lsrcb		:Adjust raw LSB to correct format
E15C	94			lsrcb		
E15D	94			lsrcb		
E15E	94			lsrcb		
E15F	94			lsrcb		
E160	94			lsrcb		
E161	94			lsrcb		
E162	94			lsrcb		
E163	94			lsrcb		
E164	94			lsrcb		
E165	94			lsrcb		
E166	94			lsrcb		
E167	94			lsrcb		
E168	94			lsrcb		
E169	94			lsrcb		
E16A	94			lsrcb		
E16B	94			lsrcb		
E16C	94			lsrcb		
E16D	94			lsrcb		
E16E	94			lsrcb		
E16F	94			lsrcb		
E170	94			lsrcb		
E171	94			lsrcb		
E172	94			lsrcb		
E173	94			lsrcb		
E174	94			lsrcb		
E175	94			lsrcb		
E176	94			lsrcb		
E177	94			lsrcb		
E178	94			lsrcb		
E179	94			lsrcb		
E17A	94			lsrcb		
E17B	94			lsrcb		
E17C	94			lsrcb		
E17D	94			lsrcb		
E17E	94			lsrcb		
E17F	94			lsrcb		
E180	94			lsrcb		
E181	94			lsrcb		
E182	94			lsrcb		
E183	94			lsrcb		
E184	94			lsrcb		
E185	94			lsrcb		
E186	94			lsrcb		
E187	94			lsrcb		
E188	94			lsrcb		
E189	94			lsrcb		
E18A	94			lsrcb		
E18B	94			lsrcb		
E18C	94			lsrcb		
E18D	94			lsrcb		
E18E	94			lsrcb		
E18F	94			lsrcb		
E190	94			lsrcb		
E191	94			lsrcb		
E192	94			lsrcb		
E193	94			lsrcb		
E194	94			lsrcb		</

GYRAC.A PROGRAM LISTING (continued)

```
DATE: 04-01-82
VERSION: 1.1
NAME: delay
MIDDLE MODULE: 4.1
CALCULATION:  $\frac{1}{1000} \times 1000 \text{ provides a time delay } = 1.0174 \times 10^{-3}$ 
              (1000/1000) in seconds.
PAUSED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A
FILES READ: None
FILES WRITTEN: None
MIDDLE CALLED: None
CALLING MODULES: void
                void
                a void
                a void
                void
                void
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: NONE
```

```

E11E      36 05      delay      ldaa      *tbl1      ;Get time delay variable
E12E      01              next      bcc      done      ;if done, go to done
E13E      44              decb      delay      ;if not done, decrement delay
E14E      08 00              bne      next      ;if not done, do another loop delay
E15E      07              rts

;-----
;-----
E17E      00              org      vector
E18E      00 00 00 00      fdb      begin, begin, begin, begin      ;set up vector table
E19E      00 00 00 00

;-----
E40E      END

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 01-12-87
VERSION: 1.1
NAME: velib
MODULE NUMBER: 5.0
DESCRIPTION: This module sends a write pulse to the Gyrac
             velocity data register to latch the data, reads
             the MSB of heading data, and sends this byte of
             velocity data to the ACIA (RS-232) output.
PASSED VARIABLES: None
RETURNS: One byte of velocity data (latched to ACIA (RS-232))
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: pulse
                delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 original
         Version 1.1 change velocity data format

```

```

B174  00 00  velib  ldaa  #veladdh  ;Get address of MSB of velocity
B175  17 00 00     staa  piadataA    ;Write address of MSB of vel to GYRAC
B176  00 00 00     jsr   mpulse      ;Send GYRAC write pulse to latch data
B177  00 00 00     jsr   delay        ;Allow for A to D conversion time
B178  00 00 00     load  piadataB    ;Read MSB of velocity data
B179  00 00 00     st    bx          ;Output 1 byte of velocity to ACIA
B180  00 00 00     rts

```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 11/21/85
VERSION: 1.1
NAME: ave101
MODULE NUMBER: 0.0
DESCRIPTION: This module sends a write pulse to the gyro
angular velocity data register to latch the data,
reads two bytes of ang vel data, reformats and
sends the data, MSB first, to the AQIA (A3-100)
output. Only the least significant 10 bits of
the data is significant.
PASSED VARIABLES: None
RETURNS: Two bytes of angular velocity data written to AQIA
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED:
    module
    delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 original
        Version 1.1 change angular velocity data format
    
```

```

E101 06 00 ave101: ldaa #ave1addh ;Get address of MSB of ang vel
E102 07 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E103 08 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E104 09 00 00 lsr #delay ;Allow for A to D conversion time
E105 0A 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E106 0B 00 stob temp ;Save raw MSB of data
E107 0C 04 lart ;Form correct MSB of data
E108 0D 04 lart
E109 0E 04 lart
E110 0F 04 lart
E111 10 04 lart
E112 11 04 lart
E113 12 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E114 13 00 ldaa #ave1addl ;Get address of LSB of ang vel
E115 14 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E116 15 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E117 16 04 lart ;Adjust raw LSB to correct format
E118 17 04 lart
E119 18 04 lart
E120 19 04 lart
E121 1A 04 lart
E122 1B 04 lart
E123 1C 00 ldaa temp ;Get raw MSB of data
E124 1D 04 asr 4 ;Adjust raw MSB to correct L/D format
E125 1E 04 lart
E126 1F 04 lart
E127 20 04 staa temp ;Store corrected L/D to AQIA
E128 21 00 ldaa #ave1addh ;Get address of MSB of ang vel
E129 22 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E130 23 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E131 24 00 00 lsr #delay ;Allow for A to D conversion time
E132 25 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E133 26 00 stob temp ;Save raw MSB of data
E134 27 04 lart ;Form correct MSB of data
E135 28 04 lart
E136 29 04 lart
E137 2A 04 lart
E138 2B 04 lart
E139 2C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E140 2D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E141 2E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E142 2F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E143 30 04 lart ;Adjust raw LSB to correct format
E144 31 04 lart
E145 32 04 lart
E146 33 04 lart
E147 34 04 lart
E148 35 04 lart
E149 36 00 ldaa temp ;Get raw MSB of data
E150 37 04 asr 4 ;Adjust raw MSB to correct L/D format
E151 38 04 lart
E152 39 04 lart
E153 3A 04 staa temp ;Store corrected L/D to AQIA
E154 3B 00 ldaa #ave1addh ;Get address of MSB of ang vel
E155 3C 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E156 3D 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E157 3E 00 00 lsr #delay ;Allow for A to D conversion time
E158 3F 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E159 40 00 stob temp ;Save raw MSB of data
E160 41 04 lart ;Form correct MSB of data
E161 42 04 lart
E162 43 04 lart
E163 44 04 lart
E164 45 04 lart
E165 46 04 lart
E166 47 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E167 48 00 ldaa #ave1addl ;Get address of LSB of ang vel
E168 49 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E169 4A 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E170 4B 04 lart ;Adjust raw LSB to correct format
E171 4C 04 lart
E172 4D 04 lart
E173 4E 04 lart
E174 4F 04 lart
E175 50 04 lart
E176 51 00 ldaa temp ;Get raw MSB of data
E177 52 04 asr 4 ;Adjust raw MSB to correct L/D format
E178 53 04 lart
E179 54 04 lart
E180 55 04 staa temp ;Store corrected L/D to AQIA
E181 56 00 ldaa #ave1addh ;Get address of MSB of ang vel
E182 57 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E183 58 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E184 59 00 00 lsr #delay ;Allow for A to D conversion time
E185 5A 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E186 5B 00 stob temp ;Save raw MSB of data
E187 5C 04 lart ;Form correct MSB of data
E188 5D 04 lart
E189 5E 04 lart
E190 5F 04 lart
E191 60 04 lart
E192 61 04 lart
E193 62 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E194 63 00 ldaa #ave1addl ;Get address of LSB of ang vel
E195 64 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E196 65 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E197 66 04 lart ;Adjust raw LSB to correct format
E198 67 04 lart
E199 68 04 lart
E200 69 04 lart
E201 6A 04 lart
E202 6B 04 lart
E203 6C 00 ldaa temp ;Get raw MSB of data
E204 6D 04 asr 4 ;Adjust raw MSB to correct L/D format
E205 6E 04 lart
E206 6F 04 lart
E207 70 04 staa temp ;Store corrected L/D to AQIA
E208 71 00 ldaa #ave1addh ;Get address of MSB of ang vel
E209 72 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E210 73 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E211 74 00 00 lsr #delay ;Allow for A to D conversion time
E212 75 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E213 76 00 stob temp ;Save raw MSB of data
E214 77 04 lart ;Form correct MSB of data
E215 78 04 lart
E216 79 04 lart
E217 7A 04 lart
E218 7B 04 lart
E219 7C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E220 7D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E221 7E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E222 7F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E223 80 04 lart ;Adjust raw LSB to correct format
E224 81 04 lart
E225 82 04 lart
E226 83 04 lart
E227 84 04 lart
E228 85 04 lart
E229 86 00 ldaa temp ;Get raw MSB of data
E230 87 04 asr 4 ;Adjust raw MSB to correct L/D format
E231 88 04 lart
E232 89 04 lart
E233 8A 04 staa temp ;Store corrected L/D to AQIA
E234 8B 00 ldaa #ave1addh ;Get address of MSB of ang vel
E235 8C 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E236 8D 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E237 8E 00 00 lsr #delay ;Allow for A to D conversion time
E238 8F 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E239 90 00 stob temp ;Save raw MSB of data
E240 91 04 lart ;Form correct MSB of data
E241 92 04 lart
E242 93 04 lart
E243 94 04 lart
E244 95 04 lart
E245 96 04 lart
E246 97 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E247 98 00 ldaa #ave1addl ;Get address of LSB of ang vel
E248 99 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E249 9A 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E250 9B 04 lart ;Adjust raw LSB to correct format
E251 9C 04 lart
E252 9D 04 lart
E253 9E 04 lart
E254 9F 04 lart
E255 A0 04 lart
E256 A1 00 ldaa temp ;Get raw MSB of data
E257 A2 04 asr 4 ;Adjust raw MSB to correct L/D format
E258 A3 04 lart
E259 A4 04 lart
E260 A5 04 staa temp ;Store corrected L/D to AQIA
E261 A6 00 ldaa #ave1addh ;Get address of MSB of ang vel
E262 A7 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E263 A8 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E264 A9 00 00 lsr #delay ;Allow for A to D conversion time
E265 AA 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E266 AB 00 stob temp ;Save raw MSB of data
E267 AC 04 lart ;Form correct MSB of data
E268 AD 04 lart
E269 AE 04 lart
E270 AF 04 lart
E271 B0 04 lart
E272 B1 04 lart
E273 B2 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E274 B3 00 ldaa #ave1addl ;Get address of LSB of ang vel
E275 B4 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E276 B5 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E277 B6 04 lart ;Adjust raw LSB to correct format
E278 B7 04 lart
E279 B8 04 lart
E280 B9 04 lart
E281 BA 04 lart
E282 BB 04 lart
E283 BC 00 ldaa temp ;Get raw MSB of data
E284 BD 04 asr 4 ;Adjust raw MSB to correct L/D format
E285 BE 04 lart
E286 BF 04 lart
E287 C0 04 staa temp ;Store corrected L/D to AQIA
E288 C1 00 ldaa #ave1addh ;Get address of MSB of ang vel
E289 C2 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E290 C3 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E291 C4 00 00 lsr #delay ;Allow for A to D conversion time
E292 C5 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E293 C6 00 stob temp ;Save raw MSB of data
E294 C7 04 lart ;Form correct MSB of data
E295 C8 04 lart
E296 C9 04 lart
E297 CA 04 lart
E298 CB 04 lart
E299 CC ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E300 CD 00 ldaa #ave1addl ;Get address of LSB of ang vel
E301 CE 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E302 CF 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E303 D0 04 lart ;Adjust raw LSB to correct format
E304 D1 04 lart
E305 D2 04 lart
E306 D3 04 lart
E307 D4 04 lart
E308 D5 04 lart
E309 D6 00 ldaa temp ;Get raw MSB of data
E310 D7 04 asr 4 ;Adjust raw MSB to correct L/D format
E311 D8 04 lart
E312 D9 04 lart
E313 DA 04 staa temp ;Store corrected L/D to AQIA
E314 DB 00 ldaa #ave1addh ;Get address of MSB of ang vel
E315 DC 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E316 DD 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E317 DE 00 00 lsr #delay ;Allow for A to D conversion time
E318 DF 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E319 E0 00 stob temp ;Save raw MSB of data
E320 E1 04 lart ;Form correct MSB of data
E321 E2 04 lart
E322 E3 04 lart
E323 E4 04 lart
E324 E5 04 lart
E325 E6 04 lart
E326 E7 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E327 E8 00 ldaa #ave1addl ;Get address of LSB of ang vel
E328 E9 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E329 EA 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E330 EB 04 lart ;Adjust raw LSB to correct format
E331 EC 04 lart
E332 ED 04 lart
E333 EE 04 lart
E334 EF 04 lart
E335 F0 04 lart
E336 F1 00 ldaa temp ;Get raw MSB of data
E337 F2 04 asr 4 ;Adjust raw MSB to correct L/D format
E338 F3 04 lart
E339 F4 04 lart
E340 F5 04 staa temp ;Store corrected L/D to AQIA
E341 F6 00 ldaa #ave1addh ;Get address of MSB of ang vel
E342 F7 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E343 F8 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E344 F9 00 00 lsr #delay ;Allow for A to D conversion time
E345 FA 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E346 FB 00 stob temp ;Save raw MSB of data
E347 FC 04 lart ;Form correct MSB of data
E348 FD 04 lart
E349 FE 04 lart
E350 FF 04 lart
E351 00 04 lart
E352 01 04 lart
E353 02 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E354 03 00 ldaa #ave1addl ;Get address of LSB of ang vel
E355 04 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E356 05 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E357 06 04 lart ;Adjust raw LSB to correct format
E358 07 04 lart
E359 08 04 lart
E360 09 04 lart
E361 0A 04 lart
E362 0B 04 lart
E363 0C 00 ldaa temp ;Get raw MSB of data
E364 0D 04 asr 4 ;Adjust raw MSB to correct L/D format
E365 0E 04 lart
E366 0F 04 lart
E367 10 04 staa temp ;Store corrected L/D to AQIA
E368 11 00 ldaa #ave1addh ;Get address of MSB of ang vel
E369 12 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E370 13 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E371 14 00 00 lsr #delay ;Allow for A to D conversion time
E372 15 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E373 16 00 stob temp ;Save raw MSB of data
E374 17 04 lart ;Form correct MSB of data
E375 18 04 lart
E376 19 04 lart
E377 1A 04 lart
E378 1B 04 lart
E379 1C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E380 1D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E381 1E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E382 1F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E383 20 04 lart ;Adjust raw LSB to correct format
E384 21 04 lart
E385 22 04 lart
E386 23 04 lart
E387 24 04 lart
E388 25 04 lart
E389 26 00 ldaa temp ;Get raw MSB of data
E390 27 04 asr 4 ;Adjust raw MSB to correct L/D format
E391 28 04 lart
E392 29 04 lart
E393 2A 04 staa temp ;Store corrected L/D to AQIA
E394 2B 00 ldaa #ave1addh ;Get address of MSB of ang vel
E395 2C 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E396 2D 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E397 2E 00 00 lsr #delay ;Allow for A to D conversion time
E398 2F 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E399 30 00 stob temp ;Save raw MSB of data
E400 31 04 lart ;Form correct MSB of data
E401 32 04 lart
E402 33 04 lart
E403 34 04 lart
E404 35 04 lart
E405 36 04 lart
E406 37 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E407 38 00 ldaa #ave1addl ;Get address of LSB of ang vel
E408 39 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E409 3A 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E410 3B 04 lart ;Adjust raw LSB to correct format
E411 3C 04 lart
E412 3D 04 lart
E413 3E 04 lart
E414 3F 04 lart
E415 40 04 lart
E416 41 00 ldaa temp ;Get raw MSB of data
E417 42 04 asr 4 ;Adjust raw MSB to correct L/D format
E418 43 04 lart
E419 44 04 lart
E420 45 04 staa temp ;Store corrected L/D to AQIA
E421 46 00 ldaa #ave1addh ;Get address of MSB of ang vel
E422 47 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E423 48 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E424 49 00 00 lsr #delay ;Allow for A to D conversion time
E425 4A 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E426 4B 00 stob temp ;Save raw MSB of data
E427 4C 04 lart ;Form correct MSB of data
E428 4D 04 lart
E429 4E 04 lart
E430 4F 04 lart
E431 50 04 lart
E432 51 04 lart
E433 52 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E434 53 00 ldaa #ave1addl ;Get address of LSB of ang vel
E435 54 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E436 55 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E437 56 04 lart ;Adjust raw LSB to correct format
E438 57 04 lart
E439 58 04 lart
E440 59 04 lart
E441 5A 04 lart
E442 5B 04 lart
E443 5C 00 ldaa temp ;Get raw MSB of data
E444 5D 04 asr 4 ;Adjust raw MSB to correct L/D format
E445 5E 04 lart
E446 5F 04 lart
E447 60 04 staa temp ;Store corrected L/D to AQIA
E448 61 00 ldaa #ave1addh ;Get address of MSB of ang vel
E449 62 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E450 63 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E451 64 00 00 lsr #delay ;Allow for A to D conversion time
E452 65 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E453 66 00 stob temp ;Save raw MSB of data
E454 67 04 lart ;Form correct MSB of data
E455 68 04 lart
E456 69 04 lart
E457 6A 04 lart
E458 6B 04 lart
E459 6C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E460 6D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E461 6E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E462 6F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E463 70 04 lart ;Adjust raw LSB to correct format
E464 71 04 lart
E465 72 04 lart
E466 73 04 lart
E467 74 04 lart
E468 75 04 lart
E469 76 00 ldaa temp ;Get raw MSB of data
E470 77 04 asr 4 ;Adjust raw MSB to correct L/D format
E471 78 04 lart
E472 79 04 lart
E473 7A 04 staa temp ;Store corrected L/D to AQIA
E474 7B 00 ldaa #ave1addh ;Get address of MSB of ang vel
E475 7C 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E476 7D 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E477 7E 00 00 lsr #delay ;Allow for A to D conversion time
E478 7F 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E479 80 00 stob temp ;Save raw MSB of data
E480 81 04 lart ;Form correct MSB of data
E481 82 04 lart
E482 83 04 lart
E483 84 04 lart
E484 85 04 lart
E485 86 04 lart
E486 87 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E487 88 00 ldaa #ave1addl ;Get address of LSB of ang vel
E488 89 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E489 8A 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E490 8B 04 lart ;Adjust raw LSB to correct format
E491 8C 04 lart
E492 8D 04 lart
E493 8E 04 lart
E494 8F 04 lart
E495 90 04 lart
E496 91 00 ldaa temp ;Get raw MSB of data
E497 92 04 asr 4 ;Adjust raw MSB to correct L/D format
E498 93 04 lart
E499 94 04 lart
E500 95 04 staa temp ;Store corrected L/D to AQIA
E501 96 00 ldaa #ave1addh ;Get address of MSB of ang vel
E502 97 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E503 98 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E504 99 00 00 lsr #delay ;Allow for A to D conversion time
E505 9A 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E506 9B 00 stob temp ;Save raw MSB of data
E507 9C 04 lart ;Form correct MSB of data
E508 9D 04 lart
E509 9E 04 lart
E510 9F 04 lart
E511 A0 04 lart
E512 A1 04 lart
E513 A2 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E514 A3 00 ldaa #ave1addl ;Get address of LSB of ang vel
E515 A4 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E516 A5 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E517 A6 04 lart ;Adjust raw LSB to correct format
E518 A7 04 lart
E519 A8 04 lart
E520 A9 04 lart
E521 AA 04 lart
E522 AB 04 lart
E523 AC 00 ldaa temp ;Get raw MSB of data
E524 AD 04 asr 4 ;Adjust raw MSB to correct L/D format
E525 AE 04 lart
E526 AF 04 lart
E527 B0 04 staa temp ;Store corrected L/D to AQIA
E528 B1 00 ldaa #ave1addh ;Get address of MSB of ang vel
E529 B2 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E530 B3 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E531 B4 00 00 lsr #delay ;Allow for A to D conversion time
E532 B5 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E533 B6 00 stob temp ;Save raw MSB of data
E534 B7 04 lart ;Form correct MSB of data
E535 B8 04 lart
E536 B9 04 lart
E537 BA 04 lart
E538 BB 04 lart
E539 BC ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E540 BD 00 ldaa #ave1addl ;Get address of LSB of ang vel
E541 BE 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E542 BF 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E543 C0 04 lart ;Adjust raw LSB to correct format
E544 C1 04 lart
E545 C2 04 lart
E546 C3 04 lart
E547 C4 04 lart
E548 C5 04 lart
E549 C6 00 ldaa temp ;Get raw MSB of data
E550 C7 04 asr 4 ;Adjust raw MSB to correct L/D format
E551 C8 04 lart
E552 C9 04 lart
E553 CA 04 staa temp ;Store corrected L/D to AQIA
E554 CB 00 ldaa #ave1addh ;Get address of MSB of ang vel
E555 CC 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E556 CD 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E557 CE 00 00 lsr #delay ;Allow for A to D conversion time
E558 CF 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E559 D0 00 stob temp ;Save raw MSB of data
E560 D1 04 lart ;Form correct MSB of data
E561 D2 04 lart
E562 D3 04 lart
E563 D4 04 lart
E564 D5 04 lart
E565 D6 04 lart
E566 D7 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E567 D8 00 ldaa #ave1addl ;Get address of LSB of ang vel
E568 D9 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E569 DA 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E570 DB 04 lart ;Adjust raw LSB to correct format
E571 DC 04 lart
E572 DD 04 lart
E573 DE 04 lart
E574 DF 04 lart
E575 E0 04 lart
E576 E1 00 ldaa temp ;Get raw MSB of data
E577 E2 04 asr 4 ;Adjust raw MSB to correct L/D format
E578 E3 04 lart
E579 E4 04 lart
E580 E5 04 staa temp ;Store corrected L/D to AQIA
E581 E6 00 ldaa #ave1addh ;Get address of MSB of ang vel
E582 E7 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E583 E8 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E584 E9 00 00 lsr #delay ;Allow for A to D conversion time
E585 EA 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E586 EB 00 stob temp ;Save raw MSB of data
E587 EC 04 lart ;Form correct MSB of data
E588 ED 04 lart
E589 EE 04 lart
E590 EF 04 lart
E591 F0 04 lart
E592 F1 04 lart
E593 F2 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E594 F3 00 ldaa #ave1addl ;Get address of LSB of ang vel
E595 F4 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E596 F5 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E597 F6 04 lart ;Adjust raw LSB to correct format
E598 F7 04 lart
E599 F8 04 lart
E600 F9 04 lart
E601 FA 04 lart
E602 FB 04 lart
E603 FC 00 ldaa temp ;Get raw MSB of data
E604 FD 04 asr 4 ;Adjust raw MSB to correct L/D format
E605 FE 04 lart
E606 FF 04 lart
E607 00 04 staa temp ;Store corrected L/D to AQIA
E608 01 00 ldaa #ave1addh ;Get address of MSB of ang vel
E609 02 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E610 03 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E611 04 00 00 lsr #delay ;Allow for A to D conversion time
E612 05 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E613 06 00 stob temp ;Save raw MSB of data
E614 07 04 lart ;Form correct MSB of data
E615 08 04 lart
E616 09 04 lart
E617 0A 04 lart
E618 0B 04 lart
E619 0C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E620 0D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E621 0E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E622 0F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E623 10 04 lart ;Adjust raw LSB to correct format
E624 11 04 lart
E625 12 04 lart
E626 13 04 lart
E627 14 04 lart
E628 15 04 lart
E629 16 00 ldaa temp ;Get raw MSB of data
E630 17 04 asr 4 ;Adjust raw MSB to correct L/D format
E631 18 04 lart
E632 19 04 lart
E633 1A 04 staa temp ;Store corrected L/D to AQIA
E634 1B 00 ldaa #ave1addh ;Get address of MSB of ang vel
E635 1C 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E636 1D 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E637 1E 00 00 lsr #delay ;Allow for A to D conversion time
E638 1F 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E639 20 00 stob temp ;Save raw MSB of data
E640 21 04 lart ;Form correct MSB of data
E641 22 04 lart
E642 23 04 lart
E643 24 04 lart
E644 25 04 lart
E645 26 04 lart
E646 27 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E647 28 00 ldaa #ave1addl ;Get address of LSB of ang vel
E648 29 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E649 2A 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E650 2B 04 lart ;Adjust raw LSB to correct format
E651 2C 04 lart
E652 2D 04 lart
E653 2E 04 lart
E654 2F 04 lart
E655 30 04 lart
E656 31 00 ldaa temp ;Get raw MSB of data
E657 32 04 asr 4 ;Adjust raw MSB to correct L/D format
E658 33 04 lart
E659 34 04 lart
E660 35 04 staa temp ;Store corrected L/D to AQIA
E661 36 00 ldaa #ave1addh ;Get address of MSB of ang vel
E662 37 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E663 38 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E664 39 00 00 lsr #delay ;Allow for A to D conversion time
E665 3A 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E666 3B 00 stob temp ;Save raw MSB of data
E667 3C 04 lart ;Form correct MSB of data
E668 3D 04 lart
E669 3E 04 lart
E670 3F 04 lart
E671 40 04 lart
E672 41 04 lart
E673 42 ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E674 43 00 ldaa #ave1addl ;Get address of LSB of ang vel
E675 44 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E676 45 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E677 46 04 lart ;Adjust raw LSB to correct format
E678 47 04 lart
E679 48 04 lart
E680 49 04 lart
E681 4A 04 lart
E682 4B 04 lart
E683 4C 00 ldaa temp ;Get raw MSB of data
E684 4D 04 asr 4 ;Adjust raw MSB to correct L/D format
E685 4E 04 lart
E686 4F 04 lart
E687 50 04 staa temp ;Store corrected L/D to AQIA
E688 51 00 ldaa #ave1addh ;Get address of MSB of ang vel
E689 52 10 00 staa #ave1addh ;Write MSB ang vel address to GYRAC
E690 53 02 00 lsr #pulse ;Send GYRAC write pulse to latch data
E691 54 00 00 lsr #delay ;Allow for A to D conversion time
E692 55 10 01 ldat #addata0 ;Read MSB of ang vel from GYRAC
E693 56 00 stob temp ;Save raw MSB of data
E694 57 04 lart ;Form correct MSB of data
E695 58 04 lart
E696 59 04 lart
E697 5A 04 lart
E698 5B 04 lart
E699 5C ED 03 lsr 3 ;Send MSB of ang vel to AQIA
E700 5D 00 ldaa #ave1addl ;Get address of LSB of ang vel
E701 5E 10 00 staa #ave1addl ;Write LSB ang vel address to GYRAC
E702 5F 10 01 ldat #addata1 ;Read LSB of ang vel from GYRAC
E7
```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 11/17/88
VERSION: 1.1
AUTHOR: ave11b
MODULE NUMBER: 7.3
DESCRIPTION: This module sends a write pulse to the gyro
angular velocity data register to latch the data,
reads the MSB of ang vel data, and sends this
byte of ang vel data to the ACIA (PS-012) output.

PAIRED VARIABLES: None
RETURNS: One byte of ang vel data written to ACIA (PS-012)
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED:
    wpulse
    delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM D. RAMEY JR.
HISTORY: Version 1.0 original
        Version 1.1 change angular velocity data format
    
```

```

B107 36 30 ave11b 10aa #ave1addn ;Get address of MSB of ang vel
B108 37 30 00 staa #lacdataA ;Write address of MSB of ave1 to DACR1
B109 38 31 20 .sr wpulse ;Send GYRAC write pulse to latch data
B101 39 31 20 .sr delay ;Allow for A to D conversion time
B104 40 30 00 .lsl #dat #ladataB ;Read MSB of angular velocity data
B107 41 31 10 .jsr tx ;Output 1 byte of ang vel to ACIA
B108 42 31 00 .rts
    
```

# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 04/06/85
VERSION: 1.1
NAME: c1rvel
MODULE NUMBER: 1.0
DESCRIPTION: This module clears, sets R on the integration
              constant on the acceleration integrator. This is
              equivalent to zero velocity, initial condition.
              PLACING THE ADDRESS in the GYRAC address bus
              and sending a write pulse, clears the velocity
              constant. The address and write level must be
              REMOVED to stop clearing the constant.
PASSED VARIABLES: None
RETURNS: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. FAMEY JR.
HISTORY: Version 1.0 original
         Version 1.1 add delay subroutine

```

```

0101 26 09 c1rvel 10aa #vconsadd ;Get address of vel const clear device
0102 27 09 00 staa piadataA ;Start clearing velocity constant
0103 05 24 10ab #write ;Get write command
0104 27 09 01 stab piactrlA ;Send GYRAC write level to start clear
0105 0D E2 1E jsr delay ;Allow time for capacitor to discharge
0106 11 10 10ab #read ;Get read command
0107 27 09 01 stab piactrlA ;Send GYRAC read level to stop clear
0108 1F 00 00 c1ra ;Clear
0109 27 09 00 staa piadataA ;Stop clearing velocity constant
0110 17 00 00 rts

```



AD-A164 036 GYRO AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A  
MOBILE AUTONOMOUS RO. (U) AIR FORCE INST OF TECH  
WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI.

GYRO AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A  
MOBILE AUTONOMOUS RO. (U) AIR FORCE INST OF TECH  
WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI.

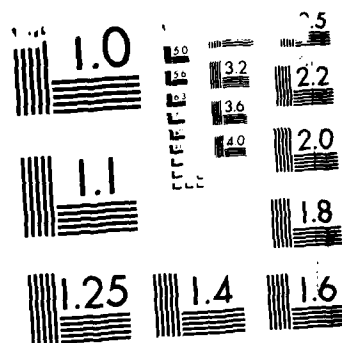
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F/G 17/7

**ML:**[illegible]



MICROCOPY RESOLUTION TEST CHART  
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# GYRAC.A PROGRAM LISTING (continued)

```

DATE: 05/10/85
VERSION: 1.0
NAME: boot
MODULE NUMBER: 0.0
DESCRIPTION: This module will read a program from the ACIA
              (RS-232) serial port, load it into RAM memory,
              and then execute the program just loaded. This
              program does an unconditional jump to the loaded
              program.
PASSED VARIABLES: None
RETURNS: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, X
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: getcom
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: NONE

```

```

E1E2 50 E0 EF boot    jsr    getcom    ;Get the number of blocks to load
E1E3 17 01          staa   blocks    ;Save # of blocks in memory
E1E7 50 E0 EF        jsr    getcom    ;Get the number of bytes in a block
E1EA 07 02          staa   bytes     ;Save # of bytes in a block in memory
E1EC FE 60 00        ldw    rambot    ;Load pointer to RAM memory
E1EF 05 02          ldab   bytes     ;Get number of bytes
E1F1 50 E0 EF bytloop jsr    getcom    ;Get byte of data
E1F4 A7 00          staa   0,x       ;Load data byte into RAM
E1F6 0E            incw           ;Increment to next RAM pointer
E1F7 5A            decb           ;Decrement block byte count
E1F8 01 F7         bne    bytloop    ;If byte count not 0, get next byte
E1FA 7A 00 01       dec    blocks    ;Else block done, decrement blk count
E1FD 26 F0         bne    blkloop    ;If all block are not done, do another
E1FF 7E 60 00       jno    rambot    ;Else go execute loaded program

```

# GYRAC.A PROGRAM LISTING (continued)

```

*****
DATE: 05/10/85
VERSION: 1.0
NAME: test
MODULE NUMBER: 1019
DESCRIPTION: This module will in command send to the ACIA
              (PS-222) output 10 printable ASCII characters.
              It will then return control to the calling
              program.
PASSED VARIABLES: None
RETURNS: 25 characters to ACIA
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: tx
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: NONE
*****

E002 16 21      test      ldab    #21H      ;Get first ASCII character
E004 07 03      stab      char      ;Save character in memory
E006 16 0D      ldaa      #99      ;Get number of characters to be sent
E008 07 04      staa      charcnt   ;Save character count
E00A 01 03      charloop  ldab      char      ;Get next ASCII character
E00C 0D 02 13    jsr       tx        ;Send ASCII character
E00E 70 06 03    inc      char      ;Increment to next ASCII character
E010 7A 09 04    dec      charcnt   ;Decrement character count
E012 16 03      bne      charloop  ;If all characters have not been sent
E014 00 00      ;go send the next one
E016 00 00      ;Else return to calling program
E017 09

```

## GYRAC.A PROGRAM LISTING (continued)

[illegible]

## GYRAC.A OPERATING INSTRUCTIONS

STEP 1: Power up the H89 computer system. Place the System disk in Drive A and the gyro program disk in Drive B. Boot the system (type "B 29") and change the mode of Drive B to single sided double density (type "mode B:ss,dd"). Change the working drive to Drive B (type "B:").

STEP 2: Connect the H89 to GYRAC RS-232 cable between the H89 DCE connector and the MARRS-1 GYRAC Computer connector. Connect the external power cable to the GYRAC and turn on the power supplies. Flip the GYRAC power switch to the on position and press the GYRAC computer reset button. Flip the gyro control switch to the slaved mode for automatic tracking or the free mode for manual heading changes.

STEP 3: Load and run the M72 modem program on the H89 by typing "M72". When this program is running type "T" to enter the M72 Terminal mode. Set the H89 keyboard caps lock on.

STEP 4: Commands may now be issued to the GYRAC. They consist of single character capital letters from A thru O inclusive. The resulting hexadecimal data, as detailed below, is displayed (if it is printable) on the CRT. NOTE: Not all data returned is printable, so some results may not be displayed. Repeat STEP 4 as often as desired.

COMMAND	RESULT
A	Two bytes of heading data (12 valid bits) Two bytes of velocity data (10 valid bits) Two bytes of angular velocity data (10 valid bits)
B	One byte of heading data (8 valid bits) One byte of velocity data (8 valid bits) One byte of angular velocity data (8 valid bits)
C	Two bytes of heading data (12 valid bits)
D	One byte of heading data (8 valid bits)
E	Two bytes of velocity data (10 valid bits)
F	One byte of velocity data (8 valid bits)
G	Clear velocity constant (no data returned)

# GYRAC.A OPERATING INSTRUCTIONS (continued)

COMMAND	RESULT
H	Two bytes of angular velocity data (10 valid bits)
I	One byte of angular velocity data (8 valid bits)
J	Two bytes of heading data (12 valid bits) Two bytes of velocity data (10 valid bits)
K	One byte of heading data (8 valid bits) One byte of velocity data (8 valid bits)
L	Soft reset of GYRAC computer (no data returned)
M	Boot load a program from the H89 into RAM and then execute to loaded program. No data is returned unless the user program sends it. Control is not automatically returned to the GYRAC control program, but is at the mercy of the boot program.
N	Returns 93 printable ASCII characters This tests the communications link
O	One byte of heading data (8 valid bits) Two bytes of velocity data (10 valid bits)

STEP 6: Shutdown all systems. Type "control shift " followed by "control E" to exit Terminal mode. To exit M72, type "CPM". Remove both disks from the drives and turn off the power to the H89 system. Turn off power to the GYRAC and external power supplies.

NOTE: All references to "control" and "shift" in the H89 command lines refer to the control and shift keys and not the words control and shift. It is assumed that the robot has been "pointed" to the desired initial heading before testing commences or that the gyro free mode will be used to vary the heading.

## APPENDIX G

GTEST.A Structure Chart .....	G-2
GTEST.A Test Program Overlay .....	G-3
GTEST.A Operating Instructions .....	G-11



PUTD  
OVERLAY

PUTC  
OVERLAY

PUTB  
OVERLAY

# GTEST.A TEST PROGRAM OVERLAY

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```

DATE: 7-10-75
VERSION: 1.1
TITLE: G-RAC DATA COLLECTION PROGRAM
FILENAME: GTEST.A
COORDINATOR: CAPT WILLIAM J. RAMEL, JR.
PROJECT: GYRO AND NOODLE METER BASED NAVIGATION SYSTEM FOR A
        MOBILE AUTONOMOUS ROBOT (THEMIS)
OPERATING SYSTEM: DEANCOLE X86M V1.0AL MAGNOLIA MICROSYSTEM 1000
LANGUAGE: RISC-A ASSEMBLER V1.1 VIRTUAL DEVICES 1984
USE: This program is assembled and then transferred to the
     robot's navigation computer via an RS-232 link. It must
     be loaded into the nav computer using MOD in terminal (T)
     mode with the following command: L,CEFA,03E9 followed by
     transmitting the file gtest.hex. All of the original
     commands still work: G to begin transmitting data or H9,
     P to pause data Tx, C to resume data Tx, and Q to
     abort the nav computer. Each time the nav computer is
     rebooted (warm or cold) the gtest.hex file must be
     reloaded in order to send gyro data.

CONTENTS: putb
          putc
          puts

FUNCTION: This program overlays three existing subroutines in
         the nav computer's RAM memory to allow the nav
         computer to request data from the G-RAC (over an
         RS-232 link) and then transmit the G-RAC's data
         to an external computer over an RS-232 link. It
         replaces the subroutines that send sonar S, C, and
         D data with subroutines that send velocity, heading,
         and angular velocity respectively. The data is
         represented as four hexadecimal digits.
    
```

0000	begin	0100	0100	start address of the main func
0001	beginb	0101	0101	start address of the head b in
0002	beginh	0102	0102	start address of the head h in
0003	beginv	0103	0103	start address of the head v in
0004	begina	0104	0104	G-RAC command-- to all 4 bytes
0005	beginb	0105	0105	G-RAC command-- to all 4 bytes
0006	beginh	0106	0106	G-RAC command-- to heading 2 bytes
0007	beginv	0107	0107	G-RAC command-- to heading 2 bytes
0008	begina	0108	0108	G-RAC command-- to angular velocity 4 bytes
0009	beginb	0109	0109	G-RAC command-- to angular velocity 4 bytes
000A	beginh	010A	010A	G-RAC command-- to heading 2 bytes
000B	beginv	010B	010B	G-RAC command-- to heading 2 bytes
000C	begina	010C	010C	G-RAC command-- to angular velocity 4 bytes
000D	beginb	010D	010D	G-RAC command-- to angular velocity 4 bytes
000E	beginh	010E	010E	G-RAC command-- to heading 2 bytes
000F	beginv	010F	010F	G-RAC command-- to heading 2 bytes
0010	begina	0110	0110	G-RAC command-- to angular velocity 4 bytes
0011	beginb	0111	0111	G-RAC command-- to angular velocity 4 bytes
0012	beginh	0112	0112	G-RAC command-- to heading 2 bytes
0013	beginv	0113	0113	G-RAC command-- to heading 2 bytes
0014	begina	0114	0114	G-RAC command-- to angular velocity 4 bytes
0015	beginb	0115	0115	G-RAC command-- to angular velocity 4 bytes
0016	beginh	0116	0116	G-RAC command-- to heading 2 bytes
0017	beginv	0117	0117	G-RAC command-- to heading 2 bytes
0018	begina	0118	0118	G-RAC command-- to angular velocity 4 bytes
0019	beginb	0119	0119	G-RAC command-- to angular velocity 4 bytes
001A	beginh	011A	011A	G-RAC command-- to heading 2 bytes
001B	beginv	011B	011B	G-RAC command-- to heading 2 bytes
001C	begina	011C	011C	G-RAC command-- to angular velocity 4 bytes
001D	beginb	011D	011D	G-RAC command-- to angular velocity 4 bytes
001E	beginh	011E	011E	G-RAC command-- to heading 2 bytes
001F	beginv	011F	011F	G-RAC command-- to heading 2 bytes
0020	begina	0120	0120	G-RAC command-- to angular velocity 4 bytes
0021	beginb	0121	0121	G-RAC command-- to angular velocity 4 bytes
0022	beginh	0122	0122	G-RAC command-- to heading 2 bytes
0023	beginv	0123	0123	G-RAC command-- to heading 2 bytes
0024	begina	0124	0124	G-RAC command-- to angular velocity 4 bytes
0025	beginb	0125	0125	G-RAC command-- to angular velocity 4 bytes
0026	beginh	0126	0126	G-RAC command-- to heading 2 bytes
0027	beginv	0127	0127	G-RAC command-- to heading 2 bytes
0028	begina	0128	0128	G-RAC command-- to angular velocity 4 bytes
0029	beginb	0129	0129	G-RAC command-- to angular velocity 4 bytes
002A	beginh	012A	012A	G-RAC command-- to heading 2 bytes
002B	beginv	012B	012B	G-RAC command-- to heading 2 bytes
002C	begina	012C	012C	G-RAC command-- to angular velocity 4 bytes
002D	beginb	012D	012D	G-RAC command-- to angular velocity 4 bytes
002E	beginh	012E	012E	G-RAC command-- to heading 2 bytes
002F	beginv	012F	012F	G-RAC command-- to heading 2 bytes
0030	begina	0130	0130	G-RAC command-- to angular velocity 4 bytes
0031	beginb	0131	0131	G-RAC command-- to angular velocity 4 bytes
0032	beginh	0132	0132	G-RAC command-- to heading 2 bytes
0033	beginv	0133	0133	G-RAC command-- to heading 2 bytes
0034	begina	0134	0134	G-RAC command-- to angular velocity 4 bytes
0035	beginb	0135	0135	G-RAC command-- to angular velocity 4 bytes
0036	beginh	0136	0136	G-RAC command-- to heading 2 bytes
0037	beginv	0137	0137	G-RAC command-- to heading 2 bytes
0038	begina	0138	0138	G-RAC command-- to angular velocity 4 bytes
0039	beginb	0139	0139	G-RAC command-- to angular velocity 4 bytes
003A	beginh	013A	013A	G-RAC command-- to heading 2 bytes
003B	beginv	013B	013B	G-RAC command-- to heading 2 bytes
003C	begina	013C	013C	G-RAC command-- to angular velocity 4 bytes
003D	beginb	013D	013D	G-RAC command-- to angular velocity 4 bytes
003E	beginh	013E	013E	G-RAC command-- to heading 2 bytes
003F	beginv	013F	013F	G-RAC command-- to heading 2 bytes
0040	begina	0140	0140	G-RAC command-- to angular velocity 4 bytes
0041	beginb	0141	0141	G-RAC command-- to angular velocity 4 bytes
0042	beginh	0142	0142	G-RAC command-- to heading 2 bytes
0043	beginv	0143	0143	G-RAC command-- to heading 2 bytes
0044	begina	0144	0144	G-RAC command-- to angular velocity 4 bytes
0045	beginb	0145	0145	G-RAC command-- to angular velocity 4 bytes
0046	beginh	0146	0146	G-RAC command-- to heading 2 bytes
0047	beginv	0147	0147	G-RAC command-- to heading 2 bytes
0048	begina	0148	0148	G-RAC command-- to angular velocity 4 bytes
0049	beginb	0149	0149	G-RAC command-- to angular velocity 4 bytes
004A	beginh	014A	014A	G-RAC command-- to heading 2 bytes
004B	beginv	014B	014B	G-RAC command-- to heading 2 bytes
004C	begina	014C	014C	G-RAC command-- to angular velocity 4 bytes
004D	beginb	014D	014D	G-RAC command-- to angular velocity 4 bytes
004E	beginh	014E	014E	G-RAC command-- to heading 2 bytes
004F	beginv	014F	014F	G-RAC command-- to heading 2 bytes
0050	begina	0150	0150	G-RAC command-- to angular velocity 4 bytes
0051	beginb	0151	0151	G-RAC command-- to angular velocity 4 bytes
0052	beginh	0152	0152	G-RAC command-- to heading 2 bytes
0053	beginv	0153	0153	G-RAC command-- to heading 2 bytes
0054	begina	0154	0154	G-RAC command-- to angular velocity 4 bytes
0055	beginb	0155	0155	G-RAC command-- to angular velocity 4 bytes
0056	beginh	0156	0156	G-RAC command-- to heading 2 bytes
0057	beginv	0157	0157	G-RAC command-- to heading 2 bytes
0058	begina	0158	0158	G-RAC command-- to angular velocity 4 bytes
0059	beginb	0159	0159	G-RAC command-- to angular velocity 4 bytes
005A	beginh	015A	015A	G-RAC command-- to heading 2 bytes
005B	beginv	015B	015B	G-RAC command-- to heading 2 bytes
005C	begina	015C	015C	G-RAC command-- to angular velocity 4 bytes
005D	beginb	015D	015D	G-RAC command-- to angular velocity 4 bytes
005E	beginh	015E	015E	G-RAC command-- to heading 2 bytes
005F	beginv	015F	015F	G-RAC command-- to heading 2 bytes
0060	begina	0160	0160	G-RAC command-- to angular velocity 4 bytes
0061	beginb	0161	0161	G-RAC command-- to angular velocity 4 bytes
0062	beginh	0162	0162	G-RAC command-- to heading 2 bytes
0063	beginv	0163	0163	G-RAC command-- to heading 2 bytes
0064	begina	0164	0164	G-RAC command-- to angular velocity 4 bytes
0065	beginb	0165	0165	G-RAC command-- to angular velocity 4 bytes
0066	beginh	0166	0166	G-RAC command-- to heading 2 bytes
0067	beginv	0167	0167	G-RAC command-- to heading 2 bytes
0068	begina	0168	0168	G-RAC command-- to angular velocity 4 bytes
0069	beginb	0169	0169	G-RAC command-- to angular velocity 4 bytes
006A	beginh	016A	016A	G-RAC command-- to heading 2 bytes
006B	beginv	016B	016B	G-RAC command-- to heading 2 bytes
006C	begina	016C	016C	G-RAC command-- to angular velocity 4 bytes
006D	beginb	016D	016D	G-RAC command-- to angular velocity 4 bytes
006E	beginh	016E	016E	G-RAC command-- to heading 2 bytes
006F	beginv	016F	016F	G-RAC command-- to heading 2 bytes
0070	begina	0170	0170	G-RAC command-- to angular velocity 4 bytes
0071	beginb	0171	0171	G-RAC command-- to angular velocity 4 bytes
0072	beginh	0172	0172	G-RAC command-- to heading 2 bytes
0073	beginv	0173	0173	G-RAC command-- to heading 2 bytes
0074	begina	0174	0174	G-RAC command-- to angular velocity 4 bytes
0075	beginb	0175	0175	G-RAC command-- to angular velocity 4 bytes
0076	beginh	0176	0176	G-RAC command-- to heading 2 bytes
0077	beginv	0177	0177	G-RAC command-- to heading 2 bytes
0078	begina	0178	0178	G-RAC command-- to angular velocity 4 bytes
0079	beginb	0179	0179	G-RAC command-- to angular velocity 4 bytes
007A	beginh	017A	017A	G-RAC command-- to heading 2 bytes
007B	beginv	017B	017B	G-RAC command-- to heading 2 bytes
007C	begina	017C	017C	G-RAC command-- to angular velocity 4 bytes
007D	beginb	017D	017D	G-RAC command-- to angular velocity 4 bytes
007E	beginh	017E	017E	G-RAC command-- to heading 2 bytes
007F	beginv	017F	017F	G-RAC command-- to heading 2 bytes
0080	begina	0180	0180	G-RAC command-- to angular velocity 4 bytes
0081	beginb	0181	0181	G-RAC command-- to angular velocity 4 bytes
0082	beginh	0182	0182	G-RAC command-- to heading 2 bytes
0083	beginv	0183	0183	G-RAC command-- to heading 2 bytes
0084	begina	0184	0184	G-RAC command-- to angular velocity 4 bytes
0085	beginb	0185	0185	G-RAC command-- to angular velocity 4 bytes
0086	beginh	0186	0186	G-RAC command-- to heading 2 bytes
0087	beginv	0187	0187	G-RAC command-- to heading 2 bytes
0088	begina	0188	0188	G-RAC command-- to angular velocity 4 bytes
0089	beginb	0189	0189	G-RAC command-- to angular velocity 4 bytes
008A	beginh	018A	018A	G-RAC command-- to heading 2 bytes
008B	beginv	018B	018B	G-RAC command-- to heading 2 bytes
008C	begina	018C	018C	G-RAC command-- to angular velocity 4 bytes
008D	beginb	018D	018D	G-RAC command-- to angular velocity 4 bytes
008E	beginh	018E	018E	G-RAC command-- to heading 2 bytes
008F	beginv	018F	018F	G-RAC command-- to heading 2 bytes
0090	begina	0190	0190	G-RAC command-- to angular velocity 4 bytes
0091	beginb	0191	0191	G-RAC command-- to angular velocity 4 bytes
0092	beginh	0192	0192	G-RAC command-- to heading 2 bytes
0093	beginv	0193	0193	G-RAC command-- to heading 2 bytes
0094	begina	0194	0194	G-RAC command-- to angular velocity 4 bytes
0095	beginb	0195	0195	G-RAC command-- to angular velocity 4 bytes
0096	beginh	0196	0196	G-RAC command-- to heading 2 bytes
0097	beginv	0197	0197	G-RAC command-- to heading 2 bytes
0098	begina	0198	0198	G-RAC command-- to angular velocity 4 bytes
0099	beginb	0199	0199	G-RAC command-- to angular velocity 4 bytes
009A	beginh	019A	019A	G-RAC command-- to heading 2 bytes
009B	beginv	019B	019B	G-RAC command-- to heading 2 bytes
009C	begina	019C	019C	G-RAC command-- to angular velocity 4 bytes
009D	beginb	019D	019D	G-RAC command-- to angular velocity 4 bytes
009E	beginh	019E	019E	G-RAC command-- to heading 2 bytes
009F	beginv	019F	019F	G-RAC command-- to heading 2 bytes
00A0	begina	01A0	01A0	G-RAC command-- to angular velocity 4 bytes
00A1	beginb	01A1	01A1	G-RAC command-- to angular velocity 4 bytes
00A2	beginh	01A2	01A2	G-RAC command-- to heading 2 bytes
00A3	beginv	01A3	01A3	G-RAC command-- to heading 2 bytes
00A4	begina	01A4	01A4	G-RAC command-- to angular velocity 4 bytes
00A5	beginb	01A5	01A5	G-RAC command-- to angular velocity 4 bytes
00A6	beginh	01A6	01A6	G-RAC command-- to heading 2 bytes
00A7	beginv	01A7	01A7	G-RAC command-- to heading 2 bytes
00A8	begina	01A8	01A8	G-RAC command-- to angular velocity 4 bytes
00A9	beginb	01A9	01A9	G-RAC command-- to angular velocity 4 bytes
00AA	beginh	01AA	01AA	G-RAC command-- to heading 2 bytes
00AB	beginv	01AB	01AB	G-RAC command-- to heading 2 bytes
00AC	begina	01AC	01AC	G-RAC command-- to angular velocity 4 bytes
00AD	beginb	01AD	01AD	G-RAC command-- to angular velocity 4 bytes
00AE	beginh	01AE	01AE	G-RAC command-- to heading 2 bytes
00AF	beginv	01AF	01AF	G-RAC command-- to heading 2 bytes
00B0	begina	01B0	01B0	G-RAC command-- to angular velocity 4 bytes
00B1	beginb	01B1	01B1	G-RAC command-- to angular velocity 4 bytes
00B2	beginh	01B2	01B2	G-RAC command-- to heading 2 bytes
00B3	beginv	01B3	01B3	G-RAC command-- to heading 2 bytes
00B4	begina	01B4	01B4	G-RAC command-- to angular velocity 4 bytes
00B5	beginb	01B5	01B5	G-RAC command-- to angular velocity 4 bytes
00B6	beginh	01B6	01B6	G-RAC command-- to heading 2 bytes
00B7	beginv	01B7	01B7	G-RAC command-- to heading 2 bytes
00B8	begina	01B8	01B8	G-RAC command-- to angular velocity 4 bytes
00B9	beginb	01B9	01B9	G-RAC command-- to angular velocity 4 bytes
00BA	beginh	01BA	01BA	G-RAC command-- to heading 2 bytes
00BB	beginv	01BB	01BB	G-RAC command-- to heading 2 bytes
00BC	begina	01BC	01BC	G-RAC command-- to angular velocity 4 bytes
00BD	beginb	01BD	01BD	G-RAC command-- to angular velocity 4 bytes
00BE	beginh	01BE	01BE	G-RAC command-- to heading 2 bytes
00BF	beginv	01BF	01BF	G-RAC command-- to heading 2 bytes
00C0	begina	01C0	01C0	G-RAC command-- to angular velocity 4 bytes
00C1	beginb	01C1	01C1	G-RAC command-- to angular velocity 4 bytes
00C2	beginh	01C2	01C2	G-RAC command-- to heading 2 bytes
00C3	beginv	01C3	01C3	G-RAC command

```
GTEST.A TEST PROGRAM OVERLAY (continued)
```

```
DATE: 12/19/84
VERSION: 1.0
NAME: JLT
MODULE NUMBER: 1.0
DESCRIPTION: This module reads 80 bytes of velocity data from
the O RAC, converts it to four 'isobaric'
characters and stores the characters in the output
buffer.
PARCEL VARIABLES: None
RETURN: Four hex velocity characters in the data buffer.
LOCAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, C, X
FILES READ: None
FILES WRITTEN: None
MODULE CALLED: OUTBUF
CALLING MODULES: JLTEND
AUTHOR: CAPT WILLIAM L. RAMEY JR.
HISTORY: NONE
```

```

0100 00 00 40 outb      out beginv      ;Start of putb subroutine
0101 00 00      outb      out #intreading ;Point to velocity data buffer
0102 00 00      outb      out #0000      ;Get GPRAC 2 byte vel command
0103 00 00 10 outb      out acia1stat    ;Get GPRAC ACIA status
0104 00 00      outb      out #tdre      ;Is transmit data register?
0105 00 00 11      outb      out txb       ;If no loop to txb and recheck status
0106 00 00 11      outb      out acia1data ;Else send GPRAC command

0107 00 00 10 outb      out acia1stat    ;Get GPRAC ACIA status
0108 00 00      outb      out #rdrf      ;Is receive data register full?
0109 00 00      outb      out rxb       ;If no loop to rxb & recheck status
0110 00 00 11      outb      out acia1data ;Else get the LED of velocity data
0111 00 00 50      outb      out putline   ;Convert data to hex & save in buffer

0112 00 00 10 outb      out acia1stat    ;Get GPRAC ACIA status
0113 00 00      outb      out #rdrf      ;Is receive data register full?
0114 00 00      outb      out rxb       ;If no loop to rxb & recheck status
0115 00 00 11      outb      out acia1data ;Else get the LED of velocity data
0116 00 00 50      outb      out putline   ;Convert data to hex & save in buffer

0117 00      outb      out
0118 00      outb      out
0119 00      outb      out
0120 00      outb      out
0121 00      outb      out
0122 00      outb      out
0123 00      outb      out
0124 00      outb      out
0125 00      outb      out
0126 00      outb      out
0127 00      outb      out
0128 00      outb      out
0129 00      outb      out
0130 00      outb      out
0131 00      outb      out
0132 00      outb      out
0133 00      outb      out
0134 00      outb      out
0135 00      outb      out
0136 00      outb      out
0137 00      outb      out
0138 00      outb      out
0139 00      outb      out
0140 00      outb      out
0141 00      outb      out
0142 00      outb      out
0143 00      outb      out
0144 00      outb      out
0145 00      outb      out
0146 00      outb      out
0147 00      outb      out
0148 00      outb      out
0149 00      outb      out
0150 00      outb      out
0151 00      outb      out
0152 00      outb      out
0153 00      outb      out
0154 00      outb      out
0155 00      outb      out
0156 00      outb      out
0157 00      outb      out
0158 00      outb      out
0159 00      outb      out
0160 00      outb      out
0161 00      outb      out
0162 00      outb      out
0163 00      outb      out
0164 00      outb      out
0165 00      outb      out
0166 00      outb      out
0167 00      outb      out
0168 00      outb      out
0169 00      outb      out
0170 00      outb      out
0171 00      outb      out
0172 00      outb      out
0173 00      outb      out
0174 00      outb      out
0175 00      outb      out
0176 00      outb      out
0177 00      outb      out
0178 00      outb      out
0179 00      outb      out
0180 00      outb      out
0181 00      outb      out
0182 00      outb      out
0183 00      outb      out
0184 00      outb      out
0185 00      outb      out
0186 00      outb      out
0187 00      outb      out
0188 00      outb      out
0189 00      outb      out
0190 00      outb      out
0191 00      outb      out
0192 00      outb      out
0193 00      outb      out
0194 00      outb      out
0195 00      outb      out
0196 00      outb      out
0197 00      outb      out
0198 00      outb      out
0199 00      outb      out
0200 00      outb      out
0201 00      outb      out
0202 00      outb      out
0203 00      outb      out
0204 00      outb      out
0205 00      outb      out
0206 00      outb      out
0207 00      outb      out
0208 00      outb      out
0209 00      outb      out
0210 00      outb      out
0211 00      outb      out
0212 00      outb      out
0213 00      outb      out
0214 00      outb      out
0215 00      outb      out
0216 00      outb      out
0217 00      outb      out
0218 00      outb      out
0219 00      outb      out
0220 00      outb      out
0221 00      outb      out
0222 00      outb      out
0223 00      outb      out
0224 00      outb      out
0225 00      outb      out
0226 00      outb      out
0227 00      outb      out
0228 00      outb      out
0229 00      outb      out
0230 00      outb      out
0231 00      outb      out
0232 00      outb      out
0233 00      outb      out
0234 00      outb      out
0235 00      outb      out
0236 00      outb      out
0237 00      outb      out
0238 00      outb      out
0239 00      outb      out
0240 00      outb      out
0241 00      outb      out
0242 00      outb      out
0243 00      outb      out
0244 00      outb      out
0245 00      outb      out
0246 00      outb      out
0247 00      outb      out
0248 00      outb      out
0249 00      outb      out
0250 00      outb      out
0251 00      outb      out
0252 00      outb      out
0253 00      outb      out
0254 00      outb      out
0255 00      outb      out
0256 00      outb      out
0257 00      outb      out
0258 00      outb      out
0259 00      outb      out
0260 00      outb      out
0261 00      outb      out
0262 00      outb      out
0263 00      outb      out
0264 00      outb      out
0265 00      outb      out
0266 00      outb      out
0267 00      outb      out
0268 00      outb      out
0269 00      outb      out
0270 00      outb      out
0271 00      outb      out
0272 00      outb      out
0273 00      outb      out
0274 00      outb      out
0275 00      outb      out
0276 00      outb      out
0277 00      outb      out
0278 00      outb      out
0279 00      outb      out
0280 00      outb      out
0281 00      outb      out
0282 00      outb      out
0283 00      outb      out
0284 00      outb      out
0285 00      outb      out
0286 00      outb      out
0287 00      outb      out
0288 00      outb      out
0289 00      outb      out
0290 00      outb      out
0291 00      outb      out
0292 00      outb      out
0293 00      outb      out
0294 00      outb      out
0295 00      outb      out
0296 00      outb      out
0297 00      outb      out
0298 00      outb      out
0299 00      outb      out
0300 00      outb      out
0301 00      outb      out
0302 00      outb      out
0303 00      outb      out
0304 00      outb      out
0305 00      outb      out
0306 00      outb      out
0307 00      outb      out
0308 00      outb      out
0309 00      outb      out
0310 00      outb      out
0311 00      outb      out
0312 00      outb      out
0313 00      outb      out
0314 00      outb      out
0315 00      outb      out
0316 00      outb      out
0317 00      outb      out
0318 00      outb      out
0319 00      outb      out
0320 00      outb      out
0321 00      outb      out
0322 00      outb      out
0323 00      outb      out
0324 00      outb      out
0325 00      outb      out
0326 00      outb      out
0327 00      outb      out
0328 00      outb      out
0329 00      outb      out
0330 00      outb      out
0331 00      outb      out
0332 00      outb      out
0333 00      outb      out
0334 00      outb      out
0335 00      outb      out
0336 00      outb      out
0337 00      outb      out
0338 00      outb      out
0339 00      outb      out
0340 00      outb      out
0341 00      outb      out
0342 00      outb      out
0343 00      outb      out
0344 00      outb      out
0345 00      outb      out
0346 00      outb      out
0347 00      outb      out
0348 00      outb      out
0349 00      outb      out
0350 00      outb      out
0351 00      outb      out
0352 00      outb      out
0353 00      outb      out
0354 00      outb      out
0355 00      outb      out
0356 00      outb      out
0357 00      outb      out
0358 00      outb      out
0359 00      outb      out
0360 00      outb      out
0361 00      outb      out
0362 00      outb      out
0363 00      outb      out
0364 00      outb      out
0365 00      outb      out
0366 00      outb      out
0367 00      outb      out
0368 00      outb      out
0369 00      outb      out
0370 00      outb      out
0371 00      outb      out
0372 00      outb      out
0373 00      outb      out
0374 00      outb      out
0375 00      outb      out
0376 00      outb      out
0377 00      outb      out
0378 00      outb      out
0379 00      outb      out
0380 00      outb      out
0381 00      outb      out
0382 00      outb      out
0383 00      outb      out
0384 00      outb      out
0385 00      outb      out
0386 00      outb      out
0387 00      outb      out
0388 00      outb      out
0389 00      outb      out
0390 00      outb      out
0391 00      outb      out
0392
```

# GTEST.A TEST PROGRAM OVERLAY (continued)

0107	01	000
0108	01	000
0109	01	000
0110	01	000
0111	01	000
0112	01	000
0113	01	000
0114	01	000
0115	01	000
0116	01	000
0117	01	000
0118	01	000
0119	01	000
0120	01	000
0121	01	000
0122	01	000
0123	01	000
0124	01	000
0125	01	000
0126	01	000
0127	01	000
0128	01	000
0129	01	000
0130	01	000
0131	01	000
0132	01	000
0133	01	000
0134	01	000
0135	01	000
0136	01	000
0137	01	000
0138	01	000
0139	01	000
0140	01	000
0141	01	000
0142	01	000
0143	01	000
0144	01	000
0145	01	000
0146	01	000
0147	01	000
0148	01	000
0149	01	000
0150	01	000

# GTEST.A TEST PROGRAM OVERLAY (continued)

```

DATE: 12/11/85
VERSION: 1.1
NAME: gtest
MODULE NUMBER: 1
DESCRIPTION: This module reads two bytes of heading data from
the GVRAC, converts it to four hexadecimal
characters and places the characters in the output
buffer. The most significant nibble is masked
out.
RAISED VARIABLES: None
RETURNS: Four hex heading characters in the data buffer.
GLOBAL VARIABLES USED: None
LOCAL VARIABLES CHANGED: None
REGISTERS USED: A, D, X
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: putchex
CALLING MODULES: tend
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: Version 1.0 original program
Version 1.1 add mask to MS nibble of the heading

```

```

004A 0E 25 50 auto    ld  #incheading ;Point to heading data buffer
004C 03 43          ldab #comd    ;Get GVRAC 2 byte heading command
004E 05 08 10 tvc    ldab acialstat ;Get GVRAC ACIA status
0050 34 62          anda #tdre    ;Is transmit data reg empty?
0052 27 F2          beq tvc      ;If no loop to tvc and recheck status
0054 F7 02 11       stab acialdata ;Else send GVRAC command
0056

0059 04 08 10 auto    ldab acialstat ;Get GVRAC ACIA status
005B 34 61          anda #drf     ;Is receive data register full?
005D 27 F2          beq nchk      ;If no loop to nchk & recheck status
005F 04 08 11       ldab acialdata ;Else get the MSB of heading data
0061 34 0F          anda #mask    ;Mask out most significant nibble
0063 20 02 50       jsr outchex  ;Convert data to hex & save in buffer
0065

0068 04 08 10 auto    ldab acialstat ;Get GVRAC ACIA status
006A 34 61          anda #drf     ;Is receive data register full?
006C 27 F2          beq nchk      ;If no loop to nchk & recheck status
006E 04 08 11       ldab acialdata ;Else get the LSB of heading data
0070 20 02 50       jsr outchex  ;Convert data to hex & save in buffer
0072

0074 01          nop
0076 01          nop
0078 01          nop
007A 01          nop
007C 01          nop
007E 01          nop
0080 01          nop
0082 01          nop
0084 01          nop
0086 01          nop
0088 01          nop
008A 01          nop
008C 01          nop
008E 01          nop
0090 01          nop
0092 01          nop
0094 01          nop
0096 01          nop
0098 01          nop
009A 01          nop
009C 01          nop
009E 01          nop
00A0 01          nop
00A2 01          nop
00A4 01          nop
00A6 01          nop
00A8 01          nop
00AA 01          nop
00AC 01          nop
00AE 01          nop
00B0 01          nop
00B2 01          nop
00B4 01          nop
00B6 01          nop
00B8 01          nop
00BA 01          nop
00BC 01          nop
00BE 01          nop
00C0 01          nop
00C2 01          nop
00C4 01          nop
00C6 01          nop
00C8 01          nop
00CA 01          nop
00CC 01          nop
00CE 01          nop
00D0 01          nop
00D2 01          nop
00D4 01          nop
00D6 01          nop
00D8 01          nop
00DA 01          nop
00DC 01          nop
00DE 01          nop
00E0 01          nop
00E2 01          nop
00E4 01          nop
00E6 01          nop
00E8 01          nop
00EA 01          nop
00EC 01          nop
00EE 01          nop
00F0 01          nop
00F2 01          nop
00F4 01          nop
00F6 01          nop
00F8 01          nop
00FA 01          nop
00FC 01          nop
00FE 01          nop

```

# GTEST.A TEST PROGRAM OVERLAY (continued)

0007	01	nop
0008	01	nop
0009	01	nop
000A	01	nop
000B	01	nop
000C	01	nop
000D	01	nop
000E	01	nop
000F	01	nop
0010	01	nop
0011	01	nop
0012	01	nop
0013	01	nop
0014	01	nop
0015	01	nop
0016	01	nop
0017	01	nop
0018	01	nop
0019	01	nop

# GTEST.A TEST PROGRAM OVERLAY (continued)

```

*****
DATE: 07 17 85
VERSION: 1.0
NAME: gtest
MODULE NUMBER: 1.0
DESCRIPTION: This module reads two bytes of ang velocity data
             from the GVRAC, converts it to four hexadecimal
             characters and places the characters in the output
             buffer.
PASSED VARIABLES: None
RETURNS: Four hex ang velocity characters in the data buffer.
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, D, X
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: puthex
CALLING MODULES: send
AUTHOR: CAPT WILLIAM O. RAMEY JR.
HISTORY: NONE
*****

000A 0E 05 5A puts      ldx #Indreading ;Point to ang velocity data buffer
000D 03 48             ldab #comH      ;Get GVRAC 2 byte ang vel command
000F 05 00 10 bnd       lraa acialstat ;Get GVRAC ACIA status
0012 04 02             anda #tdre     ;Is transmit data reg empty?
0014 17 F0             beq bnd        ;If no loop to bnd and recheck status
0016 07 00 11          stab acialdata ;Else send GVRAC command

0019 05 00 10 rndr      lraa acialstat ;Get GVRAC ACIA status
001B 04 01             anda #ndrf     ;Is receive data register full?
001D 17 F0             beq rndm       ;If no loop to rndm & recheck status
001F 05 00 11          lraa acialdata ;Else get the MSB of ang velocity data
0021 1D 02 53          jsr put2hex    ;Convert data to hex & save in buffer

0024 05 00 10 rndl      lraa acialstat ;Get GVRAC ACIA status
0026 04 01             anda #ndrf     ;Is receive data register full?
0028 17 F0             beq rndl       ;If no loop to rndl & recheck status
002A 05 00 11          lraa acialdata ;Else get the LSB of ang velocity data
002C 1D 02 53          jsr put2hex    ;Convert data to hex & save in buffer
002E 17             rts
002F 01             rts
0030 01             rts
0031 01             rts
0032 01             rts
0033 01             rts
0034 01             rts
0035 01             rts
0036 01             rts
0037 01             rts
0038 01             rts
0039 01             rts
003A 01             rts
003B 01             rts
003C 01             rts
003D 01             rts
003E 01             rts
003F 01             rts
0040 01             rts
0041 01             rts
0042 01             rts
0043 01             rts
0044 01             rts
0045 01             rts
0046 01             rts
0047 01             rts
0048 01             rts
0049 01             rts
004A 01             rts
004B 01             rts
004C 01             rts
004D 01             rts
004E 01             rts
004F 01             rts
0050 01             rts
0051 01             rts
0052 01             rts
0053 01             rts
0054 01             rts
0055 01             rts
0056 01             rts
0057 01             rts
0058 01             rts
0059 01             rts
005A 01             rts
005B 01             rts
005C 01             rts
005D 01             rts
005E 01             rts
005F 01             rts
0060 01             rts
0061 01             rts
0062 01             rts
0063 01             rts
0064 01             rts
0065 01             rts
0066 01             rts
0067 01             rts
0068 01             rts
0069 01             rts
006A 01             rts
006B 01             rts
006C 01             rts
006D 01             rts
006E 01             rts
006F 01             rts
0070 01             rts
0071 01             rts
0072 01             rts
0073 01             rts
0074 01             rts
0075 01             rts
0076 01             rts
0077 01             rts
0078 01             rts
0079 01             rts
007A 01             rts
007B 01             rts
007C 01             rts
007D 01             rts
007E 01             rts
007F 01             rts
0080 01             rts
0081 01             rts
0082 01             rts
0083 01             rts
0084 01             rts
0085 01             rts
0086 01             rts
0087 01             rts
0088 01             rts
0089 01             rts
008A 01             rts
008B 01             rts
008C 01             rts
008D 01             rts
008E 01             rts
008F 01             rts
0090 01             rts
0091 01             rts
0092 01             rts
0093 01             rts
0094 01             rts
0095 01             rts
0096 01             rts
0097 01             rts
0098 01             rts
0099 01             rts
009A 01             rts
009B 01             rts
009C 01             rts
009D 01             rts
009E 01             rts
009F 01             rts
00A0 01             rts
00A1 01             rts
00A2 01             rts
00A3 01             rts
00A4 01             rts
00A5 01             rts
00A6 01             rts
00A7 01             rts
00A8 01             rts
00A9 01             rts
00AA 01             rts
00AB 01             rts
00AC 01             rts
00AD 01             rts
00AE 01             rts
00AF 01             rts
00B0 01             rts
00B1 01             rts
00B2 01             rts
00B3 01             rts
00B4 01             rts
00B5 01             rts
00B6 01             rts
00B7 01             rts
00B8 01             rts
00B9 01             rts
00BA 01             rts
00BB 01             rts
00BC 01             rts
00BD 01             rts
00BE 01             rts
00BF 01             rts
00C0 01             rts
00C1 01             rts
00C2 01             rts
00C3 01             rts
00C4 01             rts
00C5 01             rts
00C6 01             rts
00C7 01             rts
00C8 01             rts
00C9 01             rts
00CA 01             rts
00CB 01             rts
00CC 01             rts
00CD 01             rts
00CE 01             rts
00CF 01             rts
00D0 01             rts
00D1 01             rts
00D2 01             rts
00D3 01             rts
00D4 01             rts
00D5 01             rts
00D6 01             rts
00D7 01             rts
00D8 01             rts
00D9 01             rts
00DA 01             rts
00DB 01             rts
00DC 01             rts
00DD 01             rts
00DE 01             rts
00DF 01             rts
00E0 01             rts
00E1 01             rts
00E2 01             rts
00E3 01             rts
00E4 01             rts
00E5 01             rts
00E6 01             rts
00E7 01             rts
00E8 01             rts
00E9 01             rts
00EA 01             rts
00EB 01             rts
00EC 01             rts
00ED 01             rts
00EE 01             rts
00EF 01             rts
00F0 01             rts
00F1 01             rts
00F2 01             rts
00F3 01             rts
00F4 01             rts
00F5 01             rts
00F6 01             rts
00F7 01             rts
00F8 01             rts
00F9 01             rts
00FA 01             rts
00FB 01             rts
00FC 01             rts
00FD 01             rts
00FE 01             rts
00FF 01             rts

```

GTEST.A TEST PROGRAM OVERLAY (continued)

03D8	01	nop
03D9	01	nop
03DA	01	nop
03DB	01	nop
03DC	01	nop
03DD	01	nop
03DE	01	nop
03DF	01	nop
03E0	01	nop
03E1	01	nop
03E2	01	nop
03E3	01	nop
03E4	01	nop
03E5	01	nop
03E6	01	nop
03E7	01	nop
03E8	01	nop
03E9	01	nop

03EA	END
------	-----



# GTEST.A TEST PROGRAM OVERLAY (continued)

area1dat	0011	area1ata	0010	test1da	001A	test1at	001A
area1v	001A	area1a	0011	test1d	001A	test1v	001A
area2	0044	area2a	0045	test2d	0041	test2v	0041
area3	0040	area3a	0040	test3d	0040	test3v	0040
area4	0040	area4a	0040	test4d	0040	test4v	0040
area5	0040	area5a	0040	test5d	0040	test5v	0040
area6	0040	area6a	0040	test6d	0040	test6v	0040
area7	0040	area7a	0040	test7d	0040	test7v	0040
area8	0040	area8a	0040	test8d	0040	test8v	0040
area9	0040	area9a	0040	test9d	0040	test9v	0040
area10	0040	area10a	0040	test10d	0040	test10v	0040
area11	0040	area11a	0040	test11d	0040	test11v	0040
area12	0040	area12a	0040	test12d	0040	test12v	0040
area13	0040	area13a	0040	test13d	0040	test13v	0040
area14	0040	area14a	0040	test14d	0040	test14v	0040
area15	0040	area15a	0040	test15d	0040	test15v	0040
area16	0040	area16a	0040	test16d	0040	test16v	0040
area17	0040	area17a	0040	test17d	0040	test17v	0040
area18	0040	area18a	0040	test18d	0040	test18v	0040
area19	0040	area19a	0040	test19d	0040	test19v	0040
area20	0040	area20a	0040	test20d	0040	test20v	0040
area21	0040	area21a	0040	test21d	0040	test21v	0040
area22	0040	area22a	0040	test22d	0040	test22v	0040
area23	0040	area23a	0040	test23d	0040	test23v	0040
area24	0040	area24a	0040	test24d	0040	test24v	0040
area25	0040	area25a	0040	test25d	0040	test25v	0040
area26	0040	area26a	0040	test26d	0040	test26v	0040
area27	0040	area27a	0040	test27d	0040	test27v	0040
area28	0040	area28a	0040	test28d	0040	test28v	0040
area29	0040	area29a	0040	test29d	0040	test29v	0040
area30	0040	area30a	0040	test30d	0040	test30v	0040
area31	0040	area31a	0040	test31d	0040	test31v	0040
area32	0040	area32a	0040	test32d	0040	test32v	0040
area33	0040	area33a	0040	test33d	0040	test33v	0040
area34	0040	area34a	0040	test34d	0040	test34v	0040
area35	0040	area35a	0040	test35d	0040	test35v	0040
area36	0040	area36a	0040	test36d	0040	test36v	0040
area37	0040	area37a	0040	test37d	0040	test37v	0040
area38	0040	area38a	0040	test38d	0040	test38v	0040
area39	0040	area39a	0040	test39d	0040	test39v	0040
area40	0040	area40a	0040	test40d	0040	test40v	0040
area41	0040	area41a	0040	test41d	0040	test41v	0040
area42	0040	area42a	0040	test42d	0040	test42v	0040
area43	0040	area43a	0040	test43d	0040	test43v	0040
area44	0040	area44a	0040	test44d	0040	test44v	0040
area45	0040	area45a	0040	test45d	0040	test45v	0040
area46	0040	area46a	0040	test46d	0040	test46v	0040
area47	0040	area47a	0040	test47d	0040	test47v	0040
area48	0040	area48a	0040	test48d	0040	test48v	0040
area49	0040	area49a	0040	test49d	0040	test49v	0040
area50	0040	area50a	0040	test50d	0040	test50v	0040
area51	0040	area51a	0040	test51d	0040	test51v	0040
area52	0040	area52a	0040	test52d	0040	test52v	0040
area53	0040	area53a	0040	test53d	0040	test53v	0040
area54	0040	area54a	0040	test54d	0040	test54v	0040
area55	0040	area55a	0040	test55d	0040	test55v	0040
area56	0040	area56a	0040	test56d	0040	test56v	0040
area57	0040	area57a	0040	test57d	0040	test57v	0040
area58	0040	area58a	0040	test58d	0040	test58v	0040
area59	0040	area59a	0040	test59d	0040	test59v	0040
area60	0040	area60a	0040	test60d	0040	test60v	0040
area61	0040	area61a	0040	test61d	0040	test61v	0040
area62	0040	area62a	0040	test62d	0040	test62v	0040
area63	0040	area63a	0040	test63d	0040	test63v	0040
area64	0040	area64a	0040	test64d	0040	test64v	0040
area65	0040	area65a	0040	test65d	0040	test65v	0040
area66	0040	area66a	0040	test66d	0040	test66v	0040
area67	0040	area67a	0040	test67d	0040	test67v	0040
area68	0040	area68a	0040	test68d	0040	test68v	0040
area69	0040	area69a	0040	test69d	0040	test69v	0040
area70	0040	area70a	0040	test70d	0040	test70v	0040
area71	0040	area71a	0040	test71d	0040	test71v	0040
area72	0040	area72a	0040	test72d	0040	test72v	0040
area73	0040	area73a	0040	test73d	0040	test73v	0040
area74	0040	area74a	0040	test74d	0040	test74v	0040
area75	0040	area75a	0040	test75d	0040	test75v	0040
area76	0040	area76a	0040	test76d	0040	test76v	0040
area77	0040	area77a	0040	test77d	0040	test77v	0040
area78	0040	area78a	0040	test78d	0040	test78v	0040
area79	0040	area79a	0040	test79d	0040	test79v	0040
area80	0040	area80a	0040	test80d	0040	test80v	0040
area81	0040	area81a	0040	test81d	0040	test81v	0040
area82	0040	area82a	0040	test82d	0040	test82v	0040
area83	0040	area83a	0040	test83d	0040	test83v	0040
area84	0040	area84a	0040	test84d	0040	test84v	0040
area85	0040	area85a	0040	test85d	0040	test85v	0040
area86	0040	area86a	0040	test86d	0040	test86v	0040
area87	0040	area87a	0040	test87d	0040	test87v	0040
area88	0040	area88a	0040	test88d	0040	test88v	0040
area89	0040	area89a	0040	test89d	0040	test89v	0040
area90	0040	area90a	0040	test90d	0040	test90v	0040
area91	0040	area91a	0040	test91d	0040	test91v	0040
area92	0040	area92a	0040	test92d	0040	test92v	0040
area93	0040	area93a	0040	test93d	0040	test93v	0040
area94	0040	area94a	0040	test94d	0040	test94v	0040
area95	0040	area95a	0040	test95d	0040	test95v	0040
area96	0040	area96a	0040	test96d	0040	test96v	0040
area97	0040	area97a	0040	test97d	0040	test97v	0040
area98	0040	area98a	0040	test98d	0040	test98v	0040
area99	0040	area99a	0040	test99d	0040	test99v	0040
area100	0040	area100a	0040	test100d	0040	test100v	0040

## GTEST.A OPERATING INSTRUCTIONS

STEP 1: Power up the H89 computer system. Place the System disk in Drive A and the gyro program disk in Drive B. Boot the system (type "B 29") and change the mode of Drive B to single sided double density (type "mode B:ss,dd"). Change the working drive to Drive B (type "B:").

STEP 2: Power up the MARRS-1 Robot. Make sure the batteries are fully charged and the charger power line is connected and turned on. Press both the system reset key on the keypad and the Nav computer reset button.

STEP 3: Load and run the M72 modem program on the H89 by typing "M72". When this program is running type "SPD" to change the transmission time delays. When prompted for time delays reply with a "1" for both character and line delay times. Set the H89 keyboard caps lock on.

STEP 4: Connect the H89 to Robot RS-232 cable between the H89 DCE connector and the MARRS-1 Nav T connector. Connect the GYRAC to Nav Computer RS-232 cable between the GYRAC connector and the Nav L connector on MARRS-1. Connect the teaching pendant cable to MARRS-1. Connect the external power cable to the GYRAC and turn on the power supplies. Flip the GYRAC power switch to the on position and press the GYRAC computer reset button. Flip the gyro control switch to the slaved mode.

STEP 5: Load and transmit the GTEST.HEX file to the robot's navigation computer. This is done by typing "L,02FA,03E9" to load the file at Nav computer memory address 02FA (HEX). Next type "T filename". This will place the CRT in terminal mode and create an input buffer to store incoming data in disk file filename. Follow this by typing "control shift " then "control T" and "GTEST.HEX" to transmit the program file to the Nav computer. Reply with Yes when asked for time delays. The program data will be displayed as it is transmitted. If an error is made in STEP 5, the navigation reset button must be pressed and the entire step done over.

STEP 6: Begin program execution. First type "control shift " and then "control Y" to open the input data buffer. Now type "C" to begin program execution. Next steer the robot using the teaching pendant (MARRS-1 manual mode, 4) along the desired course. During program execution the robot will send optical shaft encoder data, heading data, angular velocity data, and velocity data at 0.1 second time

## GTEST.A OPERATING INSTRUCTIONS (continued)

intervals to the H89 computer. This data will be displayed on the CRT and stored in the input buffer.

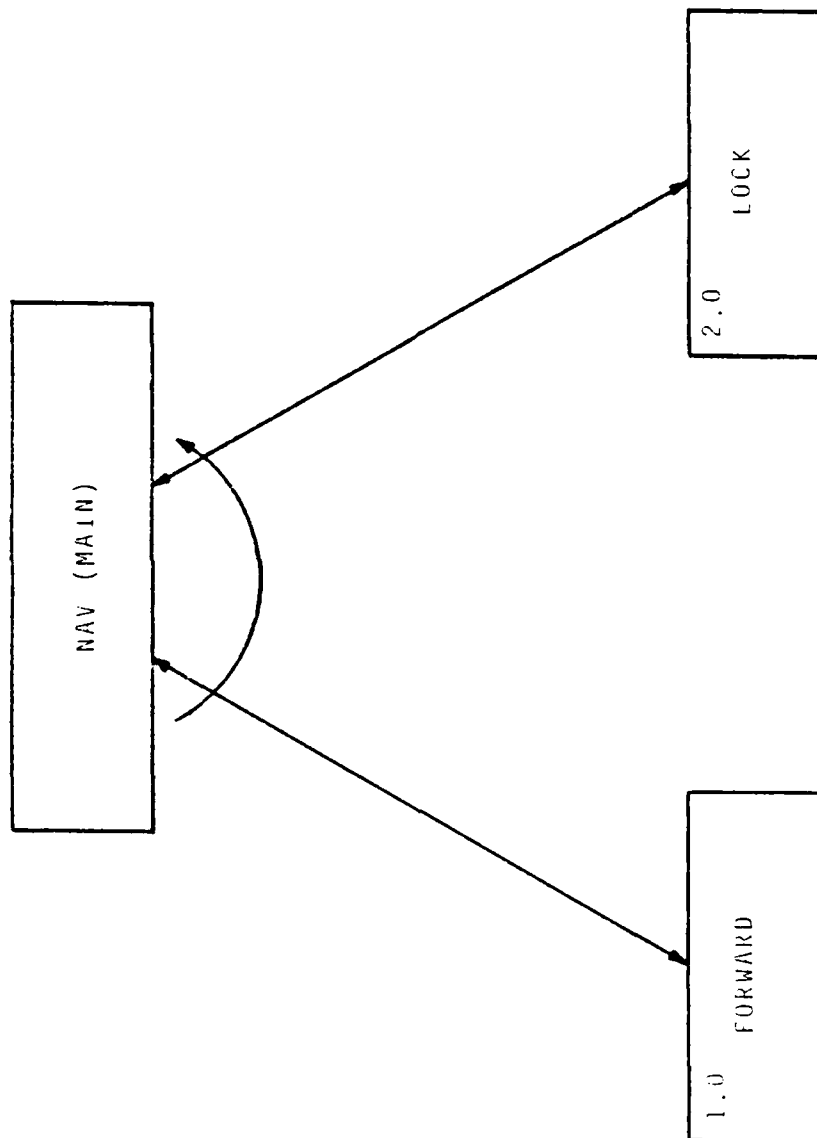
STEP 7: When the robot run is completed (i.e. you have manually stopped it with the MARRS-1 system reset button) the data stored in the input buffer may be written to disk. To do this press the Nav Computer reset button on MARRS-1 and/or type "control C" on the H89. Next type "control shift " followed by "control E". Now type "WRT" to save the data to disk ("del" may also be typed to dump buffered data). If additional runs are required continue with STEP 5 and press all three MARRS-1 reset buttons.

STEP 8: Shutdown all systems. To exit M72, type "CPM". Remove both disks from the drives and turn off the power to the H89 system. Turn off power to the robot, GYRAC, and external power supplies.

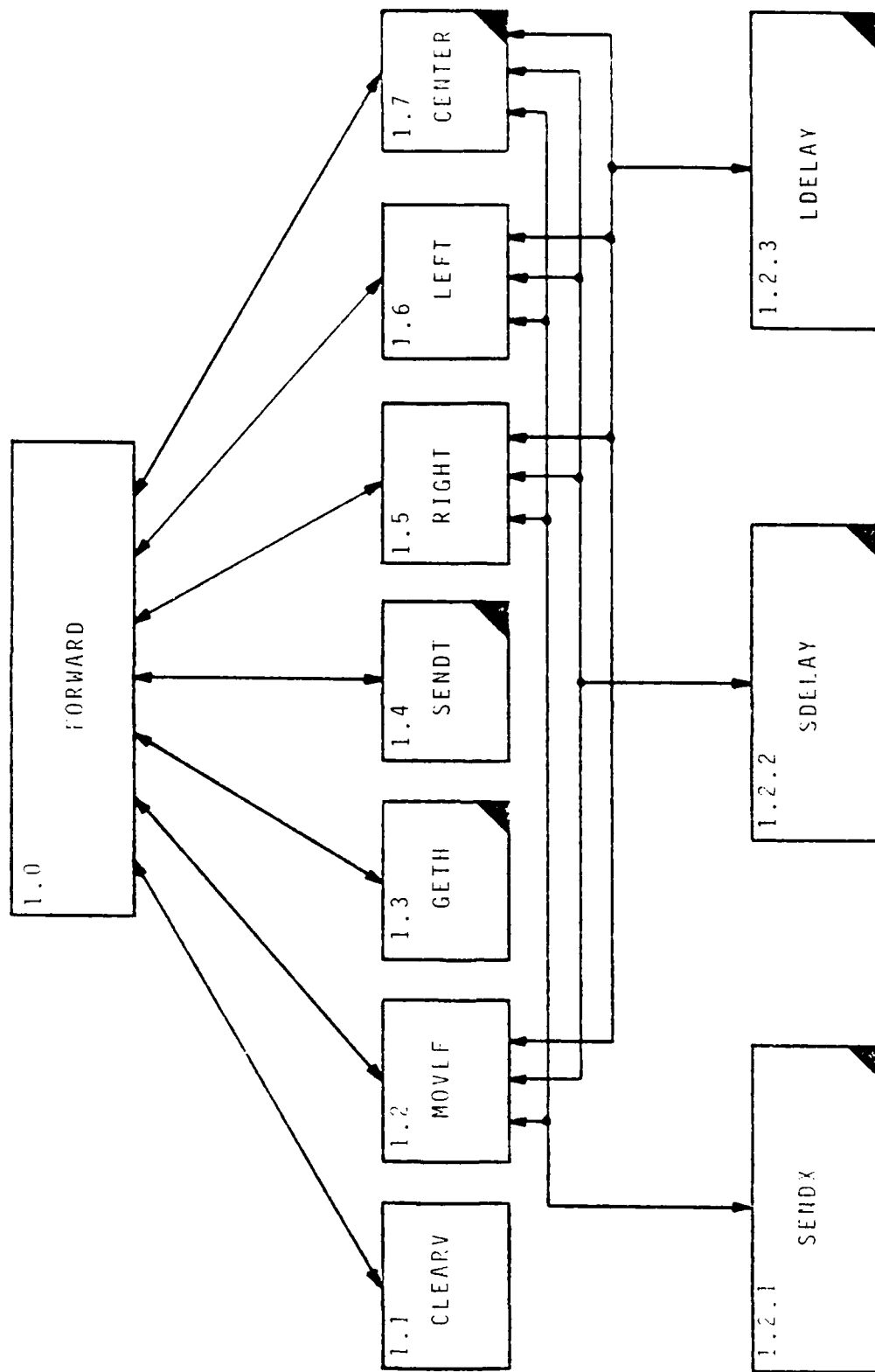
NOTE: All references to "control" and "shift" in the H89 command lines refer to the control and shift keys and not the words control and shift. Care must be taken to ensure the various cables to MARRS-1 do not become tangled during movement. In addition, it is assumed that the robot has been "pointed" to the desired initial heading before movement commences. The actual direction of travel is human controlled from the teaching pendant. Also, the GTEST.HEX program must be loaded each time a run is attempted, since the program is cleared on navigation computer reset or by a "control C" in M72 Terminal mode.

## APPENDIX H

NAV.A Structure Charts .....	H-2
NAV.A Program Listing .....	H-5
MARRS.NAV Program Listing .....	H-26
NAV.A Operating Instructions .....	H-27

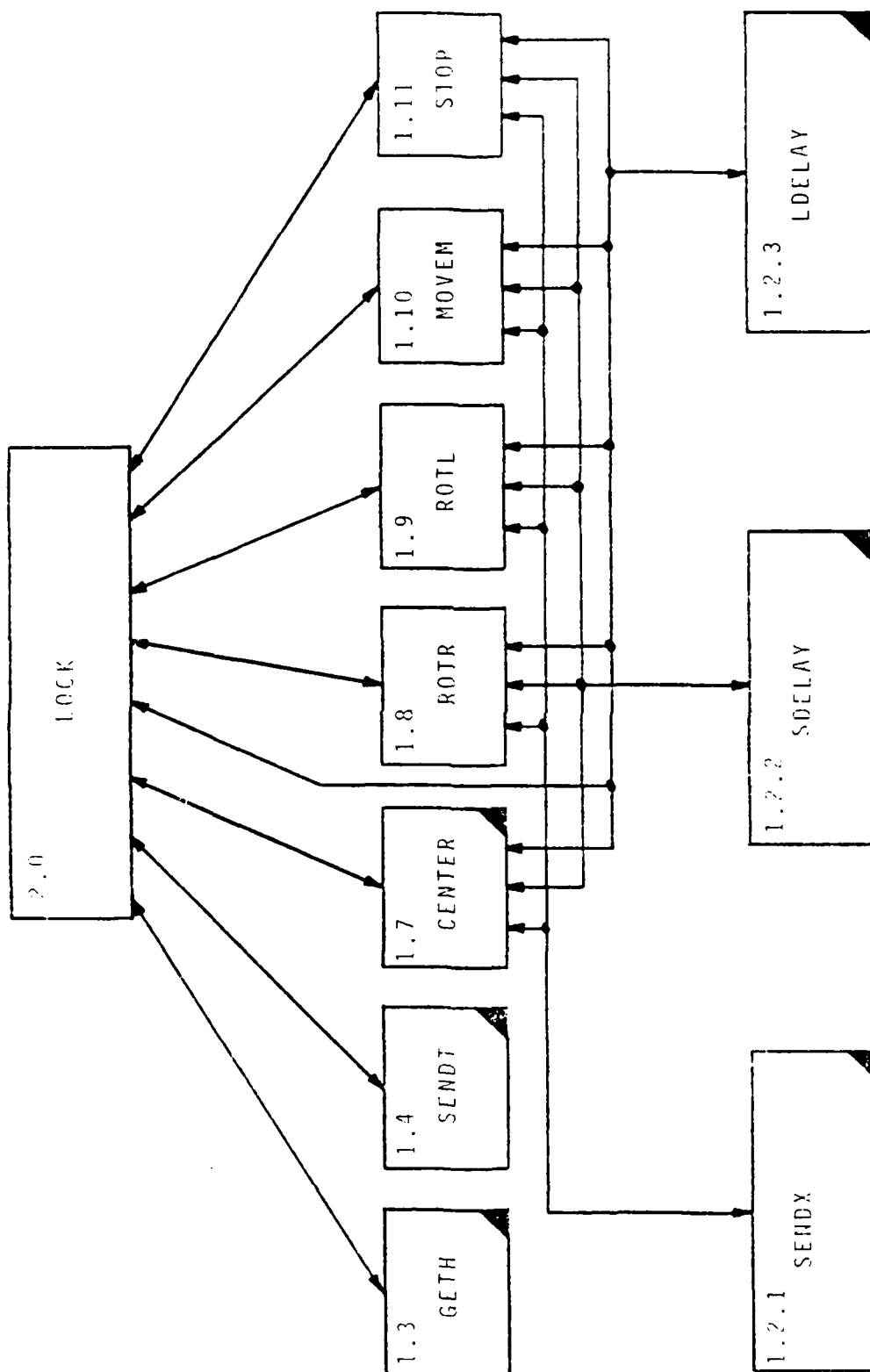


NAV.A STRUCTURE CHARTS



H-3

NAV.A STRUCTURE CHARTS (continued)



H-4

NAV.A STRUCTURE CHARTS (continued)

# NAV.A PROGRAM LISTING

NAV.A PROGRAM LISTING  
 NAV.A PROGRAM LISTING  
 NAV.A PROGRAM LISTING  
 NAV.A PROGRAM LISTING  
 NAV.A PROGRAM LISTING

```

DATE: 19/12/85
VERSION: 1.4
TITLE: NAVIGATION AND HEADING DATA COLLECTION PROGRAM
FILENAME: NAV.A
COORDINATOR: CAPT WILLIAM J. FAMEL JR.
PROJECT: GYRO AND ACCELEROMETER BASED NAVIGATION SYSTEM FOR A
        MOBILE AUTONOMOUS ROBOT (THESIS)
OPERATING SYSTEM: IBM PC/XT/AT V2.142 MAGNOLIA MICROSYSTEM 1980
LANGUAGE: RISC-A ASSEMBLER V1.1 VIRTUAL DEVICE 1984
USE: This program is assembled and then transferred to the
     robot's navigation computer via an RS-232 link (This must
     be preceded by loading the file MAPRS.NAV to the drive
     computer (MENOS) using MTD in Term mode). NAV.HEX can
     be loaded into the nav computer using MTD in terminal (T)
     mode with the following commands: L,1000,1000 followed by
     transmitting the file NAV.HEX. The heading of travel
     is gheadm, gheadn, and gheadl which are set at assembly
     time and therefore fixed in NAV.HEX.

CONTENTS: forward
          lock
          clearv
          movev
          getch
          sendt
          sendn
          rght
          left
          center
          rctr
          rot
          movev
          stop
          sdelay
          ldelay

FUNCTION: This program allows the nav computer to request data
         from the GYRA1 (over an RS-232 link), transmit GYRA1
         heading data to an external computer over an RS-232
         link, and steer the robot along a specified heading.
  
```

```

1000      begin      equ 01000H      ;Starting address of nav program
1001      gheadm      equ 010H        ;MSB 16 nibble given heading in hex
1002      gheadn      equ 00EH        ;LSB 16 nibble given heading in hex
1003      gheadl      equ 00H         ;USE 16 nibble given heading in hex
1004      ghead      equ 010H         ;GPRAC command-- to all 2 bytes
1005      gheadm      equ 010H         ;GPRAC command-- to heading 2 bytes
1006      gheadn      equ 010H         ;GPRAC command-- to heading 1 byte
1007      gheadl      equ 010H         ;GPRAC command-- to velocity 2 bytes
1008      gheadm      equ 010H         ;GPRAC command-- to velocity 1 byte
1009      gheadn      equ 010H         ;GPRAC command-- clear velocity
1010      gheadl      equ 010H         ;GPRAC command-- to heading 2 bytes
1011      gheadm      equ 010H         ;GPRAC command-- to heading 1 byte
1012      gheadn      equ 010H         ;GPRAC command-- to heading 2 bytes
1013      gheadl      equ 010H         ;GPRAC command-- to heading 1 byte
1014      gheadm      equ 010H         ;GPRAC command-- heading system
1015      gheadn      equ 010H         ;GPRAC command-- to heading 2 bytes
1016      gheadl      equ 010H         ;GPRAC command-- heading 1 byte
1017      gheadm      equ 010H         ;GPRAC command-- to heading 2 bytes
  
```



# NAV.A PROGRAM LISTING (continued)

1000	aciatstat	equ	00000000	;ACIA serial port status & control reg
1001	aciatdata	equ	00000000	;ACIA serial port data register
1002	aciatstat	equ	00000000	;MENUB serial port status & control reg
1003	aciatdata	equ	00000000	;MENUB serial port data register
1004	aciatstat	equ	00000000	;TERMINAL serial port status & control reg
1005	aciatdata	equ	00000000	;TERMINAL serial port data register
1006	tdre	equ	00000000	;ACIA transmit data register (000)
1007	rdre	equ	00000000	;ACIA receive data register (001)
1008	rdre	equ	00000000	;MEO mask for heading data
1009				
1010	00 10 40 main	lfr	begin	;Starting Address of nav program
1011	00 10 40	lfr	look	;Rotate robot until facing given head
1012	00 10 40	lfr	forward	;Move forward along given heading
1013	00 10 40	lfr	main	

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# NAV.A PROGRAM LISTING (continued)

```

DATE: 10/12/65
VERSION: 1.1
NAME: forward
MODULE NUMBER: 1.1
DESCRIPTION: This module will steer the robot along a given
            heading (ghead000, ghead01, & ghead1).
PASSED VARIABLES: None
RETURNING: None
GLOBAL VARIABLES USED: ghead0, ghead1
GLOBAL VARIABLES CHANGED: ghead0, ghead1
REGISTERS USED: A, D
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: clearv
                center
                movef
                beth
                sendt
                right
                left
CALLING MODULES: main
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: None

```

```

1003 00 10 A2 forward jsr clearv      ;Clear GVARC velocity constant
1004 00 14 05         jsr center      ;Center the steering wheel
1005 00 10 AF         jsr movef       ;Start drive motor fast speed

1011 00 10 E5 forward jsr beth        ;Get D-RAC heading
1012 00 11 0F         jsr sendt      ;Send heading to external computer
1013 00 13 03         ldaa ghead0     ;Get MSB of current heading
1014 01 00           cmpa #ghead0m   ;If given & current heading are equal
1015 01 07           beq 1100m        ;Then test LSB MS nibble of heading
1016 01 10           bcl left         ;Else if current & given head turn left
1017 00 11 10         jsr right       ;Else turn right
1018 00 00           bra forward      ;Go get next heading update

1025 01 13 07 loutbm ldaa ghead1     ;Get LSB of current heading
1026 04           lsr               ;Use only the MS nibble
1027 04           lsr
1028 04           lsr
1029 04           lsr
1030 01 1E           cmpa #ghead1     ;If current&given test LSB LSH of head
1031 01 07           beq 1100m        ;Else if current & given head turn left
1032 01 0A           bcl left         ;Else turn right
1033 00 11 10         jsr right       ;Else turn right
1034 00 00           bra forward      ;Go get next heading update

1041 00 10 A2 loutb jsr center        ;Center steering wheel
1042 01 05           bra 1100m

1049 01 11 17 left   jsr left         ;Turn left
1050 01 01           bra 1100m        ;Go get next heading update
1051 01 00           bra 1100m

```

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# NAV.A PROGRAM LISTING (continued)

```

NAME: 00000005
VERSION: 1.0
NAME: clearv
FILE NUMBER: 1.1
DESCRIPTION: This module clears the GPR velocity constants.
RAISED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, D
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: forward
AUTHOR: CAPT WILLIAM C. RAMEY JR.
HISTORY: None

```

```

1000 00 47      clearv      1000 #0000      :Get GPRAC clear vel command
1004 04 01 10 00v      1004 acia1stat :Get GPRAC ACIA status
1007 04 01      acia #0000 :Is transmit data reg empty
1009 17 00      seq 00v      :If no rescheck status
1010 07 00 11      stop acia1data :Else send GPRAC clear vel command
1015 00          rts

```

THE FOLLOWING  
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 PAGES

# NAV.A PROGRAM LISTING (continued)

```

DATE: 11/10/65
VERSION: 1.1
UNIT: 11
MODULE NUMBER: 111
DESCRIPTION: This module sends a drive motor fast
              command sequence to the drive computer (MENDR).
PASSED VARIABLES: None
RETURNED: None
LOCAL VARIABLES USED: None
LOCAL VARIABLES CHANGED: None
REGISTERED USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: send, sdelay, delay
CALLING MODULES: forward
AUTHOR: CART WILLIAM L. KAMEY JR.
HISTORY: None
    
```

1047	11 41	movef	load # A	;send to drive computer (MENDR)
1051	ED 13 10		;sr send	;start drive motor fast cont command
1054	ED 11 43		;sr sdelay	;sequence
1057	11 44		load # D1	
1059	ED 13 10		;sr send	
1060	ED 11 43		;sr sdelay	
1067	11 39		load # B	
1071	ED 13 10		;sr send	
1074	ED 11 43		;sr sdelay	
1077	11 31		load # 1	
1079	ED 11 10		;sr send	
1080	ED 11 43		;sr sdelay	
1085	11 30		load # B	
1089	ED 13 10		;sr send	
1094	ED 11 43		;sr sdelay	
1097	11 30		load # A	
1100	ED 11 10		;sr send	
1101	ED 11 43		;sr sdelay	
1103	11 11 50		sr delay	
1105	11 11 50		sr delay	
1106	11 11 50		res	

# NAV.A PROGRAM LISTING (continued)

```

DATE: 05/04/86
VERSION: 1.0
NAME: send
MODULE NUMBER: 1.1.1
DESCRIPTION: This module sends a type of data to the drive
              and then MENOS over an RS-232 link.
PARAMETER VARIABLES: Output data (passed in C reg)
RETURN: None
LOCAL VARIABLES USED: None
LOCAL VARIABLES CHANGED: None
REGISTERS USED: A, D
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: None, right, left, center, rotate, stop
AUTHOR: CAPT WILLIAM L. RAMEY JR.
EDITOR: None
    
```

```

1100 01 00 00 send 10aa acia stat ;Get MENOS ACIA status
1101 04 00      acia #dore ;Is transmit data reg empty
1102 07 00      reg send ;If no recheck status
1103 0A 00 00      stat acia data ;Else send data to MENOS
1104 0D 00      rts
    
```

# NAV.A PROGRAM LISTING (continued)

```

DATE: 08/11/05
VERSION: 1.0
NAME: sdelay
MODULE NUMBER: 1.0.1
DESCRIPTION: This module provides for a short fixed time delay
PASTED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, D
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: Move, Right, Left, Center, Rotate, Stop
AUTHOR: CAPT WILLIAM C. FAME, JR.
HISTORY: None

```

```

1040 17      sdelay  tshb      ;Save registers
1041 18      psha
1042 19      ldsa #ifH      ;Execute fixed time delay
1043 0A FF      sd1      ldsb #ifH
1044 01      sd2      bnp
1045 0A      sb      dsb
1046 0A      bne sd2
1047 0A      dsca
1048 0A      bne sd1
1049 0A      jsr      ;Restore registers
1050 0A      dsb
1051 0A      rts

```

# NAV.A PROGRAM LISTING (continued)

```

.....
DATE: 08/11/87
VERSION: 1.0
NAME: delay
MODULE NUMBER: 1.0.0
DESCRIPTION: This module provides a fixed long time delay
POISED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
LOCAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: move, right, left, center, rotate, stop, lock
AUTHOR: DART WILLIAM J. RAMEY JR.
HISTORY: None
.....

0040 07      delay      pshb          ;Save registers
0041 08          psha
0042 09 09      lsl      lsl      ;Execute time delay
0043 10 FF      ldi      lsl      #0xFF
0044 11          pop
0045 12          lslb
0046 13 00      tne      lsl
0047 14 00      decb
0048 15 00      tne      lsl
0049 16          popa
0050 17          pushb
0051 18          rts

0052          break      rts 1
0053          break      rts 1
0054          END

```

## NAV.A PROGRAM LISTING (continued)

[illegible][illegible]



# NAV.A PROGRAM LISTING (continued)

```

DATE: 10/10/17
VERSION: 1.0
NAME: send
MODULE NUMBER: 1.4
DESCRIPTION: This module sends two bytes of heading data
             represented as four ASCII hex characters to an
             external terminal.
PASSED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: cheadm, cheadl
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: None
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: None
CALLING MODULES: forward, loop
AUTHOR: CAPT WILLIAM J. RAHEY JR.
HISTORY: None

```

```

1107 00 10 00 send 1dab cheadm ;Get MSD of current heading
1110 04 00 1srb ;Convert upper nibble of MSD to ASCII
1111 04 00 1srb
1112 04 00 1srb
1113 04 00 1srb
1114 04 0F andb #FH
1115 00 00 addb #00H
1116 01 00 chrb #00H
1117 00 00 01s sl
1118 00 00 addb #00H
1119 00 00 01s sl
1120 00 00 01s sl
1121 04 00 1dab cheadl ;Get LSD of current heading
1122 04 00 1srb ;Convert lower nibble of LSD to ASCII
1123 04 00 1srb
1124 04 00 1srb
1125 04 00 1srb
1126 04 0F andb #FH
1127 00 00 addb #00H
1128 01 00 chrb #00H
1129 00 00 01s sl
1130 00 00 addb #00H
1131 00 00 01s sl
1132 00 00 01s sl
1133 04 00 1dab cheadl ;Get MSD of current heading
1134 04 00 1srb ;Convert upper nibble of MSD to ASCII
1135 04 00 1srb
1136 04 00 1srb
1137 04 00 1srb
1138 04 0F andb #FH
1139 00 00 addb #00H
1140 01 00 chrb #00H
1141 00 00 01s sl
1142 00 00 addb #00H
1143 00 00 01s sl
1144 00 00 01s sl
1145 04 00 1dab cheadl ;Get LSD of current heading
1146 04 00 1srb ;Convert lower nibble of LSD to ASCII
1147 04 00 1srb
1148 04 00 1srb
1149 04 00 1srb
1150 04 0F andb #FH
1151 00 00 addb #00H
1152 01 00 chrb #00H
1153 00 00 01s sl
1154 00 00 addb #00H
1155 00 00 01s sl
1156 00 00 01s sl
1157 04 00 1dab cheadl ;Get MSD of current heading
1158 04 00 1srb ;Convert upper nibble of MSD to ASCII
1159 04 00 1srb
1160 04 00 1srb
1161 04 00 1srb
1162 04 0F andb #FH
1163 00 00 addb #00H
1164 01 00 chrb #00H
1165 00 00 01s sl
1166 00 00 addb #00H
1167 00 00 01s sl
1168 00 00 01s sl
1169 04 00 1dab cheadl ;Get LSD of current heading
1170 04 00 1srb ;Convert lower nibble of LSD to ASCII
1171 04 00 1srb
1172 04 00 1srb
1173 04 00 1srb
1174 04 0F andb #FH
1175 00 00 addb #00H
1176 01 00 chrb #00H
1177 00 00 01s sl
1178 00 00 addb #00H
1179 00 00 01s sl
1180 00 00 01s sl

```

# NAV.A PROGRAM LISTING (continued)

```

1150  P 10 45      ldat #oadl      :Get LID of current heading
1151  Q4 15        addr #01H      :Insert lower nibble of LID to ASCII
1152  R0 10        addr #00H
1153  R1 17        addr #01H
1154  R2 10        cba $4
1155  R3 10        addr #07H
1156  R4 10 00 45  ldaa astatstat :Get terminal ASCII status
1157  R5 10        anda #tdre     :Is transmit data reg empty
1158  R6 10        bcc $4         :If no receive status
1159  R7 10 01      staa astatdata :Else send data

1171  R1 10        ldat #00H      :Get carriage return
1172  R2 10 00 45  ldaa astatstat :Get terminal ASCII status
1173  R3 10        anda #tdre     :Is transmit data reg empty
1174  R4 10        bcc $4         :If no receive status
1175  R5 10 01      staa astatdata :Else send data

1177  R1 00        ldat #0AH      :Get line feed
1178  R2 10 00 45  ldaa astatstat :Get terminal ASCII status
1179  R3 10        anda #tdre     :Is transmit data reg empty
1180  R4 10        bcc $5         :If no receive status
1181  R5 10 01      staa astatdata :Else send data

1182  R6 20        rts

```

# NAV.A PROGRAM LISTING (continued)

```

DATE: 08/14/55
VERSION: 1.0
NAME: right
MODULE NUMBER: 1.5
DESCRIPTION: This module sends a right turn relative mode
            command sequence to the drive computer (MENDS).
PASSED VARIABLES: None
RETURNS: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: delay, delay, send
CALLING MODULES: forward
AUTHOR: CAPT WILLIAM J. RAMEY JR.
HISTORY: None
    
```

1131	08 41	right	ldab # A1	;Send to drive computer (MENDS)
1132	00 13 10		jsr sendx	right turn continuous command
1131	00 13 48		jsr delay	;sequence
1134	08 44		ldab # D1	
1136	00 13 10		jsr sendx	
1137	00 13 48		jsr delay	
1130	08 36		ldab # D1	
1135	00 13 10		jsr sendx	
1141	00 13 48		jsr delay	
1144	08 31		ldab # D1	
1145	00 13 10		jsr sendx	
1149	00 13 48		jsr delay	
1140	08 34		ldab # A1	
1145	00 13 10		jsr sendx	
1151	00 13 48		jsr delay	
1154	08 33		ldab # D1	
1155	00 13 10		jsr sendx	
1159	00 13 48		jsr delay	
1161	00 13 58		jsr delay	
1162	00 13 58		jsr delay	
1163	00 13 58		jsr delay	
1164	00 13 58		jsr delay	
1165	00 13 58		jsr delay	

# NAV.A PROGRAM LISTING (continued)

```

DATE: 10/17/85
VERSION: 1.0
NAME: Left
MODULE NUMBER: 1.3
DESCRIPTION: This module sends a left turn relative mode
              command sequence to the driver computer (MENDS)
RAISED VARIABLES: None
RETURN: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: sdelay, delay, sendn
CALLING MODULES: forward
AUTHOR: CAPT WILLIAM D. RAMEY JR.
HISTORY: None

```

1109	16 41	Left	ldab #1A	!Send to drive computer (MENDS)
1111	20 13 3D		jsr sendn	!left turn continuous command
110E	20 13 4B		jsr sdelay	!sequence
1101	16 44		ldab #1D	
1103	20 13 1D		jsr sendn	
1101	20 13 4B		jsr sdelay	
1107	06 50		ldab #1E	
110D	20 13 3D		jsr sendn	
110E	20 13 4B		jsr sdelay	
1101	01 31		ldab #11	
1101	20 13 1D		jsr sendn	
1101	20 13 4B		jsr sdelay	
1107	01 30		ldab #10	
1101	20 13 1D		jsr sendn	
110E	20 13 4B		jsr sdelay	
1107	01 34		ldab #14	
1101	20 13 1D		jsr sendn	
1101	20 13 4B		jsr sdelay	
1107	01 32 50		jsr delay	
1107	01 31 50		jsr delay	
1107	01 31 50		jsr delay	
1107	01 31 50		jsr delay	
1107	01 31 50		jsr delay	

# NAV.A PROGRAM LISTING (continued)

```

DATE: 10/1/65
VERSION: 1.1
NAME: center
MODULE NUMBER: 117
DESCRIPTION: This module sends a center steering motor
              drive sequence to the drive computer (MEND).
PARAMETER VARIABLES: None
RETURNS: None
GLOBAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, D
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: send, sdelay, delay
CALLING MODULES: forward, back
AUTHOR: CAPT WILLIAM W. RAMELBERG
EDITOR: None
    
```

```

1205 00 41 center 1dat #A1 ;Send to drive computer (MEND)
1206 00 13 00 ;sr send ;center steering motor command
1207 00 13 48 ;sr sdelay ;sequence

1215 00 44 1dab #D1
1216 00 13 00 ;sr send
1217 00 13 48 ;sr sdelay

1225 00 40 1dab #B1
1226 00 13 00 ;sr send
1227 00 13 48 ;sr sdelay

1235 00 41 1dab #F1
1236 00 13 00 ;sr send
1237 00 13 48 ;sr sdelay

1245 00 40 1dab #A1
1246 00 13 00 ;sr send
1247 00 13 48 ;sr sdelay

1255 00 40 1dab #E1
1256 00 13 00 ;sr send
1257 00 13 48 ;sr sdelay

1265 00 10 58 ;sr delay
1266 00 10 58 ;sr delay

1275 00 10 58 ;sr delay
1276 00 10 58 ;sr delay
1277 00 10 58 ;sr delay
    
```

## NAV.A PROGRAM LISTING (continued)

```

DATE: 1981-05-15
TIME: 11:11
NAME: Bob
CIRCLE NUMBER: 100
DESCRIPTION: This circle will issue the command sequence to
cause the steering drive to have an the initial
steering right when the drive ratio is turned
on.
PAGED VARIABLES: None
RETURN: None
LOCAL VARIABLES USED: None
LOCAL VARIABLES CHANGED: None
REGISTERS USED: A, B
PUSH READ: None
PUSH WRITE: None
CIRCLES CALLED: send, delay, delay,
CALLING CIRCLES: None
NOTES: CAPT WILLIAM J. RAMEY JR.
EDITOR: None

```

[illegible]

## NAV.A PROGRAM LISTING (continued)

```

: DATE: 04-02-85
: TIME: 11:4
: NAME: test
: MODULE NUMBER: 1.0
: DESCRIPTION: This module will issue the command sequence to
: raise the steering wheel to give to the robot
: will rotate left when the drive motor is turned
: on.
: GLOBAL VARIABLES: None
: RETURN: None
: GLOBAL VARIABLES USED: None
: GLOBAL VARIABLES CHANGED: None
: REGISTERS USED: A, B
: FILES READ: None
: FILES WRITTEN: None
: MODULES CALLED: send, delay, delay
: CALLING MODULES: 1001
: AUTHOR: CAPT WILLIAM J. RAMEY JR.
: HISTORY: None

```

1239	00 41	net1	load #A1	;Send to drive computer (MEMO3)
1240	00 10 10		usr send	turn 90 deg left steering wheel
1241	00 10 40		usr delay	;command sequence
1242	00 44		load #C1	
1243	00 10 10		usr send	
1244	00 10 40		usr delay	
1245	00 10		load #10	
1246	00 10 10		usr send	
1247	00 10 40		usr delay	
1248	00 11		load #11	
1249	00 10 10		usr send	
1250	00 10 40		usr delay	
1251	00 11		load #1	
1252	00 10 10		usr send	
1253	00 11 40		usr delay	
1254	00 4		load #F	
1255	00 11 10		usr send	
1256	00 10 40		usr delay	
1257	00 11 40		usr delay	
1258	00 11 10		usr delay	
1259	00 11 10		usr delay	
1260	00 11 10		usr delay	
1261	00 11 10		usr delay	
1262	00 11 10		usr delay	
1263	00 11 10		usr delay	
1264	00 11 10		usr delay	
1265	00 11 10		usr delay	
1266	00 11 10		usr delay	
1267	00 11 10		usr delay	
1268	00 11 10		usr delay	
1269	00 11 10		usr delay	
1270	00 11 10		usr delay	
1271	00 11 10		usr delay	
1272	00 11 10		usr delay	
1273	00 11 10		usr delay	
1274	00 11 10		usr delay	
1275	00 11 10		usr delay	
1276	00 11 10		usr delay	
1277	00 11 10		usr delay	
1278	00 11 10		usr delay	
1279	00 11 10		usr delay	
1280	00 11 10		usr delay	
1281	00 11 10		usr delay	
1282	00 11 10		usr delay	
1283	00 11 10		usr delay	
1284	00 11 10		usr delay	
1285	00 11 10		usr delay	
1286	00 11 10		usr delay	
1287	00 11 10		usr delay	
1288	00 11 10		usr delay	
1289	00 11 10		usr delay	
1290	00 11 10		usr delay	
1291	00 11 10		usr delay	
1292	00 11 10		usr delay	
1293	00 11 10		usr delay	
1294	00 11 10		usr delay	
1295	00 11 10		usr delay	
1296	00 11 10		usr delay	
1297	00 11 10		usr delay	
1298	00 11 10		usr delay	
1299	00 11 10		usr delay	
1300	00 11 10		usr delay	
1301	00 11 10		usr delay	
1302	00 11 10		usr delay	
1303	00 11 10		usr delay	
1304	00 11 10		usr delay	
1305	00 11 10		usr delay	
1306	00 11 10		usr delay	
1307	00 11 10		usr delay	
1308	00 11 10		usr delay	
1309	00 11 10		usr delay	
1310	00 11 10		usr delay	
1311	00 11 10		usr delay	
1312	00 11 10		usr delay	
1313	00 11 10		usr delay	
1314	00 11 10		usr delay	
1315	00 11 10		usr delay	
1316	00 11 10		usr delay	
1317	00 11 10		usr delay	
1318	00 11 10		usr delay	
1319	00 11 10		usr delay	
1320	00 11 10		usr delay	
1321	00 11 10		usr delay	

# NAV.A PROGRAM LISTING (continued)

```

DATE: 0612 85
VERSION: 1.0
NAME: NAV.A
MODULE NUMBER: 1.0
DESCRIPTION: This module will issue the command sequence to
             cause the drive motor to turn on at 90 deg speed.
CALLED VARIABLES: None
RETURNS: None
LOCAL VARIABLES USED: None
GLOBAL VARIABLES CHANGED: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: send, delay, delay
CALLING MODULES: none
AUTHOR: CAPT WILLIAM D. RAMEY JR.
HISTORY: None
    
```

```

1007 00 41 00000000 movem 00ab # 01 ;Send to drive computer (MENGE)
1008 00 13 00 jsr send ;turn 90 deg steering motor command
1009 00 13 40 jsr delay ;sequence

1007 00 44 00000000 ldat # 01
1008 00 13 00 jsr send
1009 00 13 40 jsr delay

1007 00 20 00000000 ldat # 01
1008 00 13 00 jsr send
1009 00 13 40 jsr delay

1007 00 01 00000000 ldat # 1
1008 00 13 00 jsr send
1009 00 13 40 jsr delay

1007 00 01 00000000 ldat # 1
1008 00 13 00 jsr send
1009 00 13 40 jsr delay

1007 00 42 00000000 ldat # 01
1008 00 13 00 jsr send
1009 00 13 40 jsr delay

1007 00 10 00000000 jsr delay
1008 00 13 00 jsr delay
1009 00 13 40 rts
    
```



# NAV.A PROGRAM LISTING (continued)

```

DATE: 07 11 15
VERSION: 1.1
NAME: stop
MODULE NUMBER: 1.11
DESCRIPTION: This module sends the command sequence to stop
the drive and steering motors.
PASSED VARIABLES: None
RETURNS: None
GLOBAL VARIABLES USED: None
LOCAL VARIABLES IN scope: None
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: send, sdelay, delay
CALLING MODULES: lock
AUTHOR: CAPT WILLIAM D. RAMEY JR.
HISTORY: None

```

```

1006 06 41 stop      1tab #1A1      1send to drive computer (MENOS)
1008 00 13 00      1sr send      1stop steering and drive motor command
1009 00 13 40      1sr sdelay     1sequence
1010 06 44          1tab #01
1011 00 13 00      1sr send
1013 00 13 40      1sr sdelay
1014 06 38          1tab #0
1015 00 13 00      1sr send
1016 00 10 40      1sr sdelay
1017 06 31          1tab #11
1018 00 13 00      1sr send
1020 00 13 40      1sr sdelay
1021 06 21          1tab #11
1022 00 13 00      1sr send
1023 00 13 40      1sr sdelay
1024 06 10          1tab #01
1025 00 13 00      1sr send
1026 00 13 40      1sr sdelay
1027 06 11 50      1sr delay
1028 00 11 50      1sr delay
1029 00

```

# NAV.A PROGRAM LISTING (continued)

```

DATE: 12/12/66
VERSION: 1.0
NAME: 1001
MODULE NUMBER: 1.0
DESCRIPTION: This module will initiate the robot until it is
              within 1.5 degrees of the given heading.
PASSED VARIABLES: None
RETURNS: None
LOCAL VARIABLES USED: cheadn, cheadl
LOCAL VARIABLES CHANGED: cheadn, cheadl
REGISTERS USED: A, B
FILES READ: None
FILES WRITTEN: None
MODULES CALLED: center
                 moveh
                 geth
                 sendt
                 rctt
                 rctf
                 stop
                 delay
CALLING MODULES: main
AUTHOR: CAPT WILLIAM G. RAMEY JR.
DISTRIB: None

```

```

1042  00 17 00 1001  jsr  geth      ;Get G FAC heading
1043  00 11 07      jsr  sendt     ;Send heading to external computer
1044  00 10 00      ldaa  cheadn    ;Get MSB of current heading
1045  01 03      cmpa  #theadm     ;If given & current heading are equal
1046  07 07      beq   1044        ;Then test LSB MSB of heading
1047  00 17      bnl  1001        ;Else if current & given are left
1048  00 11 40      jsr  rctt      ;Else move steering wheel 40 right
1049  00 17      bra  1005

1050  00 10 07 1001  ldaa  cheadl    ;Get LSB of current heading
1051  01 04      lsra             ;Use only the MS nibble
1052  01 04      lsra
1053  01 04      lsra
1054  01 03      cmpa  #theadl     ;If current heading = given heading
1055  07 07      beq   1001        ;Then then move forward
1056  00 17      bnl  1001        ;Else if current & given head to left
1057  00 11 40      jsr  rctf      ;Else move steering wheel 40 left
1058  00 17      bra  1005

1059  00 10 07 1001  jsr  rctf      ;Move steering wheel 40 left
1060  00 17      bra  1005

1061  00 10 00 1001  jsr  moveh     ;Start move with no speed
1062  01 07 00 1001  jsr  geth      ;Get G FAC heading
1063  01 07 00 1001  ldaa  cheadn    ;Get MSB of current heading
1064  01 03      cmpa  #theadm     ;If given & current heading are equal
1065  07 07      beq   1001        ;Then test LSB MSB of heading
1066  00 17      bnl  1001        ;Else go get next heading

```

# NAV.A PROGRAM LISTING (continued)

1071	05 11 19 10012	1000 ahead1	test 010 re current heading
1072	44	1000	use only the M nibble
1073	44	1000	
1074	44	1000	
1075	44	1000	
1076	11 0E	0000 ahead1	if current heading = given heading
1077	17 00	0000	then stop rotating
1078	10 07	0000	else go get next heading update
1079	10 12 05 10000	0000	pitch drive motor
1080	10 12 05	0000	center steering wheel
1081	10 12 05	0000	
1082	10 12 05	0000	
1083	10 12 05	0000	
1084	10 12 05	0000	
1085	10 12 05	0000	
1086	10 12 05	0000	
1087	10 12 05	0000	
1088	10 12 05	0000	
1089	10 12 05	0000	
1090	10 12 05	0000	
1091	10 12 05	0000	
1092	10 12 05	0000	
1093	10 12 05	0000	
1094	10 12 05	0000	
1095	10 12 05	0000	
1096	10 12 05	0000	
1097	10 12 05	0000	
1098	10 12 05	0000	
1099	10 12 05	0000	
1100	10 12 05	0000	
1101	10 12 05	0000	
1102	10 12 05	0000	
1103	10 12 05	0000	
1104	10 12 05	0000	
1105	10 12 05	0000	
1106	10 12 05	0000	
1107	10 12 05	0000	
1108	10 12 05	0000	
1109	10 12 05	0000	
1110	10 12 05	0000	
1111	10 12 05	0000	
1112	10 12 05	0000	
1113	10 12 05	0000	
1114	10 12 05	0000	
1115	10 12 05	0000	
1116	10 12 05	0000	
1117	10 12 05	0000	
1118	10 12 05	0000	
1119	10 12 05	0000	
1120	10 12 05	0000	
1121	10 12 05	0000	
1122	10 12 05	0000	
1123	10 12 05	0000	
1124	10 12 05	0000	
1125	10 12 05	0000	
1126	10 12 05	0000	
1127	10 12 05	0000	
1128	10 12 05	0000	
1129	10 12 05	0000	
1130	10 12 05	0000	
1131	10 12 05	0000	
1132	10 12 05	0000	
1133	10 12 05	0000	
1134	10 12 05	0000	
1135	10 12 05	0000	
1136	10 12 05	0000	
1137	10 12 05	0000	
1138	10 12 05	0000	
1139	10 12 05	0000	
1140	10 12 05	0000	
1141	10 12 05	0000	
1142	10 12 05	0000	
1143	10 12 05	0000	
1144	10 12 05	0000	
1145	10 12 05	0000	
1146	10 12 05	0000	
1147	10 12 05	0000	
1148	10 12 05	0000	
1149	10 12 05	0000	
1150	10 12 05	0000	
1151	10 12 05	0000	
1152	10 12 05	0000	
1153	10 12 05	0000	
1154	10 12 05	0000	
1155	10 12 05	0000	
1156	10 12 05	0000	
1157	10 12 05	0000	
1158	10 12 05	0000	
1159	10 12 05	0000	
1160	10 12 05	0000	
1161	10 12 05	0000	
1162	10 12 05	0000	
1163	10 12 05	0000	
1164	10 12 05	0000	
1165	10 12 05	0000	
1166	10 12 05	0000	
1167	10 12 05	0000	
1168	10 12 05	0000	
1169	10 12 05	0000	
1170	10 12 05	0000	
1171	10 12 05	0000	
1172	10 12 05	0000	
1173	10 12 05	0000	
1174	10 12 05	0000	
1175	10 12 05	0000	
1176	10 12 05	0000	
1177	10 12 05	0000	
1178	10 12 05	0000	
1179	10 12 05	0000	
1180	10 12 05	0000	
1181	10 12 05	0000	
1182	10 12 05	0000	
1183	10 12 05	0000	
1184	10 12 05	0000	
1185	10 12 05	0000	
1186	10 12 05	0000	
1187	10 12 05	0000	
1188	10 12 05	0000	
1189	10 12 05	0000	
1190	10 12 05	0000	
1191	10 12 05	0000	
1192	10 12 05	0000	
1193	10 12 05	0000	
1194	10 12 05	0000	
1195	10 12 05	0000	
1196	10 12 05	0000	
1197	10 12 05	0000	
1198	10 12 05	0000	
1199	10 12 05	0000	

## NAV.A PROGRAM LISTING (continued)

[illegible]

# MARRS.NAV PROGRAM LISTING

Address (HEX)	Instruction Code (HEX)	Comment
NONE	AA	Put MARRS-1 into
NONE	01	Instruction Input
NONE	00	Mode at Address 0100
0000	CC	Start Drive Motor
0101	1B	Forward at Fast
0102	FF	Speed (movef)
0103	3A	
0004	03	Turn Steering Motor
0105	DC	One Increment to the
0106	EC	Left (left)
0107	01	
0108	3A	
0009	03	Turn Steering Motor
010A	DC	One Increment to the
010B	E8	RIGHT (right)
010C	01	
010D	3A	
010E	03	Turn Steering Motor
010F	CC	to the Center,
0110	E8	straight, Position
0111	49	(center)
0112	3A	
0113	03	Turn Steering Motor
0114	CC	to the Full Right
0115	E8	Position (rotr)
0116	90	
0117	3A	
0118	02	Stop all Motor
0119	03	Movement (stop)
011A	3A	
010B	CC	Start Drive Motor
010C	13	Forward at Medium
010D	FF	Speed (movem)
010E	3A	
011F	03	Turn Steering Motor
0120	CC	to the Full Left
0121	EC	Position (rotl)
0122	00	
0123	3A	
NONE	R	Reset to Input Mode

## NAV.A OPERATING INSTRUCTIONS

STEP 1: Power up the H89 computer system. Place the System disk in Drive A and the gyro program disk in Drive B. Boot the system (type "B 29") and change the mode of Drive B to single sided double density (type "mode B:ss,dd"). Change the working drive to Drive B (type "B:").

STEP 2: Connect the H89 to Robot RS-232 cable between the H89 DCE connector and the MARRS-1 Drive Computer (MENOS) connector. Power up the MARRS-1 Robot. Make sure the batteries are fully charged and the charger power line is connected and turned on. Press both the system reset key on the keypad and the Nav computer reset button.

STEP 3: Load and run the M72 modem program on the H89 by typing "M72". When this program is running type "SPD" to change the transmission time delays. When prompted for time delays reply with a "1" for both character and line delay times. Set the H89 keyboard caps lock on.

STEP 4: Load and transmit the MARRS.NAV file to the robot's Drive computer. This is done by typing "T" to enter the M72 Terminal mode. Next type "control shift " followed by "control T" and then "MARRS.NAV" to send the program file. When asked if time delays are desired, answer Yes. The file will be displayed as it is being transmitted. When it is finished you will see the data stop and hear the robot say "READY". Type "control shift " followed by "control T" to return to the M72 command mode. This entire step can be skipped if the program is hand keyed directly into MARRS-1 via the onboard keypad (which is the recommended way since it avoids moving cables). NOTE: MARRS-1 system resets do not erase this program.

STEP 5: Connect the H89 to Robot RS-232 cable between the H89 DCE connector and the MARRS-1 Nav T connector. Connect the Drive Computer to Nav Computer RS-232 cable between the Drive Computer connector and the Nav X connector on MARRS-1. Connect the GYRAC to Nav Computer RS-232 cable between the GYRAC connector and the Nav L connector on MARRS-1. Connect the external power cable to the GYRAC and turn on the power supplies. Flip the GYRAC power switch to the on position and press the GYRAC computer reset button. Flip the gyro control switch to the slaved mode.

STEP 6: Load and transmit the NAV.HEX file to the robot's navigation computer. This is done by typing "L,1000,1369"

## NAV.A OPERATING INSTRUCTIONS (continued)

to load the file at Nav computer memory address 1000 (HEX). Next type "T filename". This will place the CRT in terminal mode and create an input buffer to store incoming data in disk file filename. Follow this by typing "control shift " then "control T" and "NAV.HEX" to transmit the program file to the Nav computer. Reply with Yes when asked for time delays. The program data will again be displayed as it is transmitted. If an error is made in STEP 6, the navigation reset button must be pressed and the entire step done over.

STEP 7: Begin program execution. First type "control shift " and then "control Y" to open the input data buffer. Now type "G,1000" to begin program execution. During execution time the robot will send to the H89 two bytes of heading data each time it considers a course change. This data will be displayed on the CRT and stored in the input buffer.

STEP 8: When the robot run is completed (i.e. you have manually stopped it with the MARRS-1 system reset button) the data stored in the input buffer may be written to disk. To do this press the Nav Computer reset button on MARRS-1. Next type "control shift " followed by "control E". Now type "WRT" to save the data to disk ("del" may also be typed to dump buffered data). If additional runs are required continue with STEP 6 and press all three reset buttons on MARRS-1.

STEP 9: Shutdown all systems. To exit M72, type "CPM". Remove both disks from the drives and turn off the power to the H89 system. Turn off power to the robot, GYRAC, and external power supplies.

NOTE: All references to "control" and "shift" in the H89 command lines refer to the control and shift keys and not the words control and shift. Care must be taken to ensure the various cables to MARRS-1 do not become tangled during movement. In addition, it is assumed that the robot has been "pointed" to the desired initial heading before movement commences. The actual direction of travel is set into the NAV.A program at assembly time. Also, the NAV.HEX program must be loaded each time a run is attempted, since the program is cleared on navigation computer reset.

## APPENDIX I

CONVERT.BAS Program Listing .....	I-2
POSITION.BAS Program Listing .....	I-4



# CONVERT.BAS PROGRAM LISTING

```

REM*****
REM*
REM*   DATE:  30SEP85
REM*   VERSION: 1.0
REM*   TITLE:  CONVERT
REM*   FILENAME: CONVERT.BAS
REM*   AUTHOR:  CAPT ROLAND J. BLOOM
REM*   PROJECT: GYRO AND ACCELEROMETER BASED NAVIGATION
REM*             SYSTEM FOR A MOBILE AUTONOMOUS ROBOT
REM*             (THESIS)
REM*   OPERATING SYSTEM:  Z89/Z90 CP/M V2.242 MAGNOLIA
REM*                     MICROSYSTEM  1982
REM*   LANGUAGE:  MBASIC
REM*   USE:  This program is used to convert raw hex-
REM*         adecimal data obtained from the NAV computer
REM*         into integer data.  The whole data string
REM*         is read and converted to integer format.
REM*         The program interactively asks for the name
REM*         of the hex data file and asks for the name
REM*         of the file where the integer data is to be
REM*         stored.
REM*
REM*****
REM*
REM*               MAIN   PROGRAM
REM*
REM*****
REM*
10 PRINT "INPUT THE NAME OF THE HEX DATA FILE TO CONVERT"
20 INPUT "INCLUDE THE DISK DRIVE AND ENCLOSE IN QUOTES",READFILE$
30 PRINT " "
40 PRINT "INPUT THE NAME OF THE FILE TO STORE THE INTEGER DATA"
50 INPUT "INCLUDE THE DISK DRIVE AND ENCLOSE IN QUOTES",PRINTFILE$
60 OPEN "I",#1,READFILE$
70 OPEN "O",#2,PRINTFILE$
REM*
REM*   A DATA  STRING IS READ AND THEN EACH DATA SEGMENT IS
REM*   CONVERTED AND STORED ON DISK
REM*
80 INPUT#1,DATALINE$
90 IF EOF(1) THEN END
100 WORD$ = MID$(DATALINE$,3,4)
110 GOSUB 300
120 PRINT#2,VALUE%," ";
130 FOR I% = 11 TO 26 STEP 5
140 WORD$ = MID$(DATALINE$,I%,4)
150 GOSUB 300
160 GOSUB 450

```

# CONVERT.BAS PROGRAM LISTING (continued)

```

170 NEXT I%
180 FOR I% = 40 TO 47 STEP 7
190 WORD$ = MID$(DATALINE$, I%, 4)
200 GOSUB 300
210 GOSUB 450
220 NEXT I%
230 GOTO 80
REM*****
REM*
REM*          SUBROUTINES    FOLLOW
REM*
REM*****
REM*
REM*  THIS SUBROUTINE CONVERTS THE HEX VALUE TO INTEGER
REM*
300 VALUE% = 0
310 FOR J = 2 TO 4
320 CHAR$ = MID$(WORD$, J%, 1)
330 DIGIT = VAL(CHAR$)
340 IF CHAR$ = "A" THEN DIGIT = 10
350 IF CHAR$ = "B" THEN DIGIT = 11
360 IF CHAR$ = "C" THEN DIGIT = 12
370 IF CHAR$ = "D" THEN DIGIT = 13
380 IF CHAR$ = "E" THEN DIGIT = 14
390 IF CHAR$ = "F" THEN DIGIT = 15
400 VALUE% = VALUE% * 16 + DIGIT
410 NEXT J%
420 RETURN
REM*
REM*  THIS SUBROUTINE STORES THE INTEGER VALUES ON DISK
REM*
450 IF I% = 47 GOTO 480
460 PRINT#2, VALUE%, ", ";
470 GOTO 490
480 PRINT#2, VALUE%
490 RETURN

```

# POSITION.BAS PROGRAM LISTING

```

REM*****
REM*
REM*   DATE:  30SEP85
REM*   VERSION: 1.0
REM*   TITLE:  POSITION
REM*   FILENAME: POSITION.BAS
REM*   AUTHOR:  CAPT ROLAND J. BLOOM
REM*   PROJECT: GYRO AND ACCELEROMETER BASED NAVIGATION
REM*             SYSTEM FOR A MOBILE AUTONOMOUS ROBOT
REM*             (THESIS)
REM*   OPERATING SYSTEM:  Z89/Z90 CP/M V2.242 MAGNOLIA
REM*                     MICROSYSTEM  1982
REM*   LANGUAGE:  MBASIC
REM*   USE:  This program is used to compute the position
REM*         of the MARRS-1 robot based on heading and
REM*         velocity data from the GYRAC.  The raw data
REM*         from the NAV computer (which gathers the
REM*         GYRAC data) must first be converted to
REM*         integer format by the CONVERT program.
REM*         The computed position will be in terms of
REM*         x and y coordinates.  An initial (x,y)
REM*         position is provided to the program
REM*         interactively.  Program output is sent
REM*         to the printer where time, x-coordinate
REM*         and y-coordinate are printed.
REM*
REM*****
REM*
REM*               DEFINITION OF VARIABLES
REM*
REM*****
REM*
REM*           X = X-COORDINATE
REM*           Y = Y-COORDINATE
REM*           DELTAX = INCREMENT OF MOVEMENT IN X-DIRECTION
REM*           DELTAY = INCREMENT OF MOVEMENT IN Y-DIRECTION
REM*           DISTANCE = LINEAR DISTANCE TRAVELLED IN T SECONDS
REM*           T = 0.1 SECONDS (WHICH IS THE SAMPLE TIME)
REM*           HEADING = THE HEADING OF THE ROBOT IN DEGREES
REM*           VELOCITY = THE VELOCITY OF THE ROBOT (FT/SEC)
REM*           WEIGHT = WEIGHT OF EACH BIT OF VELOCITY,
REM*                   1024 BITS REPRESENT 10 VOLTS
REM*                   THEREFORE WEIGHT = 0.00977 VOLTS/BIT
REM*           CONV = CONVERSION FACTOR FOR CONVERTING THE
REM*                   VELOCITY MEASUREMENT FROM VOLTS TO
REM*                   FT/SEC.  THIS VALUE IS BASED ON LOCAL
REM*                   ACCELERATION DUE TO GRAVITY OF 32.174
REM*                   FT/S/S/G AND THE SENSITIVITY OF THE
REM*                   ACCELEROMETER (VOLTS/G).

```

POSITION.BAS PROGRAM LISTING (continued)

```

REM*          GF = GAIN FACTOR. THIS IS THE GAIN IN THE      *
REM*          INTEGRATOR CIRCUIT.                            *
REM*          TIME = TIME OF MEASUREMENT (SECONDS)           *
REM*          RAWTIME = INTEGER VALUE OF TIME. THIS VALUE IS  *
REM*          A FACTOR OF 10 TIMES THE REAL TIME.            *
REM*          RAWVEL = INTEGER VALUE FOR VELOCITY (BITS)      *
REM*          RAWHEAD = INTEGER VALUE FOR HEADING (BITS)      *
REM*          LEFTREV = REVERSE WHEEL COUNTS FROM OPTICAL     *
REM*          SHAFT ENCODER ON LEFT REAR WHEEL.               *
REM*          LEFTFOR = FORWARD WHEEL COUNTS FROM OPTICAL     *
REM*          SHAFT ENCODER ON LEFT REAR WHEEL.               *
REM*          RIGHTREV = REVERSE WHEEL COUNTS FROM OPTICAL    *
REM*          SHAFT ENCODER ON RIGHT REAR WHEEL.              *
REM*          RIGHTFOR = FORWARD WHEEL COUNTS FROM OPTICAL    *
REM*          SHAFT ENCODER ON RIGHT REAR WHEEL.              *
REM*
REM*          NOTE - WHEEL COUNTS ARE NOT USED BY THIS        *
REM*          PROGRAM BUT COULD BE INCORPORATED                *
REM*          TO PROVIDE A SEPARATE POSITION                     *
REM*          CALCULATION.                                     *
REM*
REM*****
REM*
REM*          MAIN PROGRAM FOLLOWS                             *
REM*
REM*****
10 INPUT "INPUT THE NAME OF THE DATA FILE(INCLUDE DISK DRIVE)",
    FILE$
20 OPEN "I",#1,FILE$
30 WEIGHT = 0.00977
33 CONV = 32.174/0.6
37 GF = 1/19.7
39 T = 0.1
40 INPUT "INPUT THE INITIAL POSITION (X,Y) IN FEET,XO,YO
50 X = XO
60 Y = YO
70 INPUT "INPUT THE TEST DESIGNATION",TEST$
80 LPRINT TEST$
90 LPRINT " "
100 LPRINT "          POSITION"
110 LPRINT " TIME(SEC)          X(FT)          Y(FT)"
120 LPRINT "*****          *****          *****"
130 LPRINT " "
140 INPUT#1,RAWTIME,LEFTREV,LEFTFOR,RIGHTREV,RIGHTFOR,RAWVEL,
    RAWHEAD
150 IF EOF(1) THEN END

```

POSITION.BAS PROGRAM LISTING (continued)

```
160 TIME = RAWTIME * 0.1
165 PRINT TIME
170 VELOCITY = (RAWVEL - 512) * WEIGHT * CONV * GF
180 HEADING = RAWHEAD * 0.001534
190 DISTANCE = VELOCITY * T
200 DELTAX = DISTANCE * COS(HEADING)
210 DELTAY = DISTANCE * SIN(HEADING)
220 X = X + DELTAX
230 Y = Y + DELTAY
240 LPRINT USING "    ###.##    ##.##    ##.##";TIME,X,Y
250 GOTO 140
```

APPENDIX J

Phase II Sample Test Data..... J-2

# GYRAC Phase II Sample Test Data

TEST #2B (SENSITIVITY = 0.393)

TIME(SEC)	POSITION	
	X(FT)	Y(FT)
0.0	6.75	4.58
0.1	6.75	4.58
0.2	6.75	4.58
0.3	6.75	4.59
0.4	6.75	4.59
0.5	6.75	4.59
0.6	6.75	4.59
0.7	6.75	4.59
0.8	6.75	4.60
0.9	6.75	4.60
1.0	6.75	4.60
1.1	6.75	4.60
1.2	6.75	4.60
1.3	6.75	4.61
1.4	6.75	4.61
1.5	6.75	4.61
1.6	6.75	4.61
1.7	6.75	4.62
1.8	6.75	4.62
1.9	6.75	4.62
2.0	6.75	4.64
2.1	6.75	4.65
2.2	6.75	4.66
2.3	6.74	4.67
2.4	6.74	4.68
2.5	6.74	4.69
2.6	6.74	4.70
2.7	6.74	4.70
2.8	6.74	4.71
2.9	6.74	4.72
3.0	6.74	4.73
3.1	6.74	4.74
3.2	6.74	4.75
3.3	6.74	4.76
3.4	6.74	4.77
3.5	6.74	4.78
3.6	6.74	4.79
3.7	6.73	4.80
3.8	6.73	4.81
3.9	6.73	4.82
4.0	6.73	4.83
4.1	6.73	4.84
4.2	6.73	4.85

## APPENDIX K

### Phase III Test Data

Gyro Navigation Test Run Number 1 ..... K-2  
Gyro Navigation Test Run Number 2 ..... K-3  
Gyro Navigation Test Run Number 3 ..... K-4



# GYRO NAVIGATION TEST RUN NUMBER 1

Given: 33 Foot Course  
 Heading of 3EC (hex) = 1004 (integer) = 88.2421875  
 (degrees)

Steering Window: 3E0 to 3EF (Hex)  
 992 to 1007 (integer)  
 87.1875 to 88.50585938 (Degrees)

Measured: Heading at each course change decision point

HEADING (Hex)	HEADING (Integer)	HEADING (Degrees)	DEVIATION (Integer)	DEVIATION (Degrees)
3EB	1003	88.15429688	- 1	-0.087890625
3EB	1003	88.15429688	- 1	-0.087890625
3EB	1003	88.15429688	- 1	-0.087890625
401	1025	90.08789063	+21	+1.845703125
410	1040	91.40625	+36	+3.1640625
40F	1039	91.31835938	+35	+3.076171875
3FF	1023	89.91210938	+19	+1.669921875
3D8	984	86.484375	-20	-1.7578125
3B0	944	82.96875	-60	-5.2734375
3A2	930	81.73828125	-74	-6.50390625
3A2	930	81.73828125	-74	-6.50390625
3B8	952	83.671875	-52	-4.5703125
3E0	992	87.1875	-12	-1.0546875
3FF	1023	89.91210938	+19	+1.669921875
40D	1037	91.14257813	+33	+2.900390625
410	1040	91.40625	+36	+3.1640625
3FC	1020	89.6484375	+16	+1.40625
3DB	987	86.74804688	-17	-1.494140625
3B9	953	83.75976563	-51	-4.482421875
3AE	942	82.79296875	-62	-5.44921875
3AA	938	82.44140625	-66	-5.80078125
3BA	954	83.84765625	-50	-4.39453125
3E2	994	87.36328125	-10	-0.87890625
3FF	1023	89.91210938	+19	+1.669921875
40A	1034	90.87890625	+30	+2.63671875

# GYRO NAVIGATION TEST RUN NUMBER 2

Given: 33 Foot Course  
Heading of 3EC (hex) = 1004 (integer) = 88.2421875  
(degrees)

Steering Window: 3E0 to 3EF (Hex)  
992 to 1007 (Integer)  
87.1875 to 88.50585938 (Degrees)

Measured: Heading at each course change decision point

HEADING (Hex)	HEADING (Integer)	HEADING (Degrees)	DEVIATION (Integer)	DEVIATION (Degrees)
2F5	757	66.53320313	-247	-21.70898438
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3EB	1003	88.15429688	- 1	- 0.087890625
3E7	999	87.80273438	- 5	- 0.439454125
3E7	999	87.80273438	- 5	- 0.439454125
3E7	999	87.80273438	- 5	- 0.439454125
3E4	996	87.5390625	- 8	- 0.703125
3E1	993	87.27539063	- 11	- 0.966796875
3DE	990	87.01171875	- 14	- 1.23046875
3E2	994	87.36328125	- 10	- 0.87890625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E8	1000	87.890625	- 4	- 0.3515625
3E7	999	87.80273438	- 5	- 0.439454125
3E7	999	87.80273438	- 5	- 0.439454125

# GYRO NAVIGATION TEST RUN NUMBER 3

Given: 33 Foot Course  
 Heading of 3EC (hex) = 1004 (integer) = 88.2421875  
 (degrees)

Steering Window: 3e0 to 3EF (Hex)  
 992 to 1007 (Integer)  
 87.1875 to 88.50585938 (Degrees)

Measured: Heading at each course change decision point

HEADING (Hex)	HeADING (Integer)	HEADING (Degrees)	DEVIATION (Integer)	DEVIATION (Degrees)
502	1282	112.6757813	+278	+24.43359375
3E4	996	87.5390625	- 8	- 0.703125
3E1	993	87.27539063	- 11	- 0.966796875
3E1	993	87.27539063	- 11	- 0.966796875
3E5	997	87.62695313	- 7	- 0.615234375
3E8	1000	87.890625	- 4	- 0.3515625
3EE	1006	88.41796875	+ 2	+ 0.17578125
3F4	1012	88.9453125	+ 8	+ 0.703125
3F9	1017	89.38476563	+ 13	+ 1.142578125
3E1	993	87.27539063	- 11	- 0.966796875
3DB	989	86.92382813	- 15	- 1.318359375
3F1	1009	88.68164063	+ 5	+ 0.439453125
3F9	1017	89.38476563	+ 13	+ 1.142578125
3FB	1019	89.56054688	+ 15	+ 1.318359375
3E7	999	87.80273438	- 5	- 0.439454125
3DE	990	87.01171875	- 14	- 1.23046875
3F1	1009	88.68164063	+ 5	+ 0.439453125
3FC	1020	89.6484375	+ 16	+ 1.40625
3FF	1023	89.91210938	+ 19	+ 1.669921875
3EA	1002	88.06640625	- 2	- 0.017578125
3E1	993	87.27539063	- 11	- 0.966796875
3E8	1000	87.890625	- 4	- 0.3515625
3EB	1003	88.15429688	- 1	- 0.087890625
3F1	1009	88.68164063	+ 5	+ 0.439453125
3F4	1012	88.9453125	+ 8	+ 0.703125
3DE	990	87.01171875	- 14	- 1.23046875
3D2	977	85.86914063	- 27	- 2.373046875

APPENDIX L

Lab Equipment, Computer Hardware, and Software ..... L-2

LAB EQUIPMENT, COMPUTER, HARDWARE, and SOFTWARE

LAB EQUIPMENT

Quantity	Description
1	AFIT Mobile Robotics Laboratory
1	AFIT MARRS-1 Robot
1	1607 Eldorado Frequency Counter
1	186 Wavetek Waveform Generator
1	1610A Hewlitt Packard Logic State Analyzer
1	465M Tektronics Oscilloscope
1	3466A Hewlitt Packard Digital Multimeter
1	M-15 Trygon Power Supply
1	M-36 Trygon Power Supply
1	6C3000 Powertec Power Supply
1	S-10 Bytek EEPROM Programmer
1	S-52 Ultra Violet Products EEPROM Eraser

COMPUTER HARDWARE

Quantity	Description
1	MARRS-1 Navigation Computer
1	MARRS-1 Drive Computer
1	MARRS-1 GYRAC Computer
1	Heath H89 Computer
1	Heath H27 Eight Inch Dual Disk Drive System
1	Heath H125 Dot Matrix Printer

LAB EQUIPMENT, COMPUTER, HARDWARE, and SOFTWARE (continued)

COMPUTER SOFTWARE

Quantity	Description
1	Wordmaster Word Processor
1	Wordstar Word Processor
1	Virtual Devices Robo A 6802 Cross Assembler
1	Modem 720 Communication Program
1	CP/M Operating System
1	MBASIC Compiler
1	MARRS-1 Drive Computer ROM Software
1	MARRS-1 Navigation Computer ROM Software

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<p>A navigation system for a mobile autonomous robot is presented. The navigation system is based upon a directional gyroscope and a single axis accelerometer which enables a robot to navigate independent of wheel optical shaft encoders and other commonly used positioning apparatus. The computer controlled navigation system is capable of providing absolute heading, heading rate (angular velocity), and linear velocity to a user computer. These data from the navigation system (heading and velocity) are used to compute the present location of the robot. In addition, the heading data is used to form a closed loop feedback control system for maintaining the robot on a desired course. The navigation system was designed</p>					
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Block 11. Gyro and Accelerometer Based Navigation System for a Mobile Autonomous Robot

Block 19. (continued) specifically for application on an existing Air Force Institute of Technology (AFIT) robot; however, it could be easily adapted to any robot system with a standard IEEE RS-232 serial communication interface. Test results are provided which demonstrate the use of closed loop heading control on the AFIT robot and which identify problems associated with the use of an accelerometer system for distance measurement. This thesis includes all schematics, parts lists, software listings, and operating instructions for the navigation system. A new robot world modeling and path planning technique is also presented. (746000) F



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