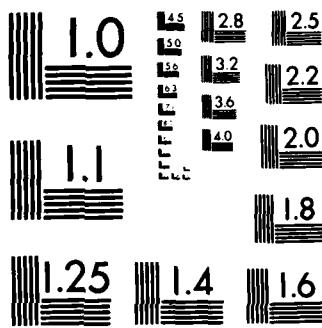


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ESTIMATION OF F-15 PEACETIME  
MAINTENANCE MANPOWER REQUIREMENTS  
USING THE LOGISTICS COMPOSITE MODEL

THESIS

GOR/SM/76D-5

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Abstract

Estimates of the maintenance manpower requirements of a planned F-15 Tactical Fighter Training Wing operating in a peacetime environment were requested by Tactical Air Command. The Logistics Composite Model (LCOM), a computer simulation, was used in conjunction with the Moody Regression and Moody Manpower programs to estimate these requirements. A more efficient method, using statistical tests of hypothesis, was developed for determining steady state in the simulation model. Using this method, steady state conditions were found to exist, in most cases, at the end of the first simulated day. An estimate was made of the autocorrelation present in each set of simulation output data. Then, correcting for this autocorrelation, statistical confidence intervals were constructed for the manpower estimates. By simulating at various levels of flying activity and with various constraints on resource availability, manpower requirements were found to be relatively insensitive to these constraints at low sortie rates and more sensitive at higher sortie rates. The authors suggest that the construction of statistical confidence intervals and the methodology developed in this study for determining steady state should be given serious consideration in future LCOM manpower studies. *Keywords include: 1473*

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ESTIMATION OF F-15 PEACETIME  
MAINTENANCE MANPOWER REQUIREMENTS  
USING THE LOGISTICS COMPOSITE MODEL

THESIS

Presented to the Faculty of the School of Engineering  
of the Air Force Institute of Technology  
Air University  
in Partial Fulfillment of the  
Requirements for the Degree of

Master of Science

by

George DeGovanni, B.S.  
Captain USAF

Donald M. Douglas, B.S.  
Major USAF

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Graduate Operations Research

December 1976



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Preface

This thesis represents the first detailed Logistics Composite Model (LCOM) analysis of United States Air Force (USAF) peacetime flying operations. In the study, we have attempted to shed light on the statistical and sensitivity inferences of the manpower estimation process. Hopefully, our efforts will allow the LCOM community to achieve greater statistical accuracy with LCOM.

We would like to thank our advisor, Colonel Ronald A. Luhks, and reader, Lieutenant Colonel Jon R. Hobbs, for their guidance during these past six months. We especially thank Lieutenant James R. Lowell for his ceaseless efforts and expert technical advice throughout our thesis effort. We also would like to thank Lieutenant Colonel Donald C. Tetmeyer, William D. Moody, and Wayne Jansen for their help with LCOM procedures. Finally, we would like to thank our wives, Mary and Bobbi, without whose help and encouragement this thesis would not have been possible.

George DeGovanni  
Donald M. Douglas

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## Symbols and Abbreviations

AFB	Air Force Base
AFIT	Air Force Institute of Technology
AFM	Air Force Manual
AFSC	Air Force Specialty Code
AGE	Aerospace Ground Equipment
$\alpha$	Type I Error
ASD	Aeronautical Systems Division
ASR	Accomplished Sortie Rate
ATS	Avionic Test Station
AUTO	Automatic
$\beta$	Type II Error
COM	Communications
E	Mutually Exclusive Probability
$E( )$	Expected Value
ECM	Electronic Counter Measures
$E(U)$	Mean Value of Mann-Whitney
FC	Functional Code
FHPM	Flying Hours per Month
G	Nonmutually Exclusive Probability
$H_a$	Statistical Alternate Hypothesis
$H_0$	Statistical Null Hypothesis
INS	Inertial Navigation System
L	Interval or Lag Between Data Points
LCOM	Logistics Composite Model

Symbols and Abbreviations (continued)

LRU	Line Replaceable Unit
M	Direct Manning in Number of Men
MPIP	Maintenance Posture Improvement Program
$M_s$	Manpower Constraint in Number of Men
MSBMA	Mean Sorties Between Maintenance Action
N	Sample Size
NAV	Navigations
NRTS	Not Repairable This Station
P(R)	Probability That R Equals Some Integer Valued Number of Runs
PSR	Performance Summary Report
R	Number of Runs
$\rho$	Autocorrelation Coefficient
$\hat{\rho}$	Estimated Autocorrelation Coefficient
$\hat{\rho}(L)$	Estimated Autocorrelation Coefficient at Lag (L)
$\rho(L)$	Autocorrelation Coefficient at Lag (L)
RPV	Remotely Piloted Vehicle
$\sigma^2$	Population Variance
$S_\mu$	Standard Deviation of the Mean
$S_\mu^2$	Sample Variance of the Mean
TAC	Tactical Air Command
TFTW	Tactical Fighter Training Wing
U	Mann-Whitney Statistic
$\mu$	Population Mean
U.E.	Unit Equipment

Symbols and Abbreviations (continued)

UHF	Ultra High Frequency
USAF	United States Air Force
V(U)	Variance of Mann-Whitney Statistic
W	Mann-Whitney Rank Value
WUC	Work Unit Code
$\bar{X}$	Sample Mean
$x_t$	Output Data Value at Time (t)
Z	Standard Normal Random Variable

## I. INTRODUCTION

Estimation of the maintenance manpower necessary to support desired flying activities in various United States Air Force (USAF) organizations is a continuing problem. As new aircraft enter the inventory and as procedures change, there exists a recurring need for reliable estimates of the maintenance manpower necessary to support desired levels of flying activity efficiently. These estimates aid USAF managers in allocating maintenance manpower to new or existing flying units and insuring combat readiness.

### Background

One method which has been used successfully to estimate these maintenance manpower requirements involves the use of the Logistics Composite Model (LCOM). The LCOM is a USAF computer simulation language designed to model USAF base level aircraft, maintenance, and support functions (Ref 33). Specifically, the model can be used to estimate maintenance manpower requirements for a USAF flying wing at specified levels of flying activity.

Two previous Air Force Institute of Technology (AFIT) theses have addressed LCOM estimation of maintenance manpower requirements: Green and Rumple constructed an LCOM simulation to evaluate the effects of alternative operational, maintenance, and supply policies on remotely piloted vehicle (RPV) maintenance manning (Ref 14:ii). Fritz and Yates used LCOM to simulate the interaction of the RPV, the launch aircraft, and the recovery helicopter (Ref 13:ii).

Tactical Air Command (TAC) used LCOM to estimate maintenance manpower requirements for their F-4, A-7, A-10, F-15, and F-16 aircraft

(Ref 23). However, TAC conducted the majority of these studies using a wartime operational environment and devoted little attention to a peacetime environment. Consequently, TAC suggested that AFIT students consider a peacetime LCOM study as a possible graduate thesis topic (Ref 29) and offered to make available an on-the-scene technical advisor to assist in making such a study meet TAC requirements.

Each of these previous LCOM studies simulated concurrent flying and maintenance activity. That is, aircraft maintenance was performed only on days of scheduled flying operations. In a wartime environment, this practice is acceptable since aircraft missions are scheduled seven days a week. However, this practice has one major drawback: if a high level of flying activity is scheduled, the aircraft maintenance organization may, at times, become overloaded with work. This causes a temporary decrease in flying activity until the maintenance organization clears out the backlogged work.

In a peacetime environment, flying operations are normally scheduled Monday through Friday. During high levels of flying activity, the maintenance organization continues to perform its functions on weekends in order to alleviate backlogged work. In this manner, the maintenance complex can usually keep stride with the weekly flying operations and the day to day level of flying activity remains fairly constant.

In this thesis, the authors use LCOM to model a peacetime flying environment. The model simulates a Monday through Friday flying schedule and a seven day maintenance work week.

#### Thesis Objectives

A need exists to expand F-15 LCOM estimation of maintenance manpower requirements to include the peacetime operational environment

(Ref 29). Furthermore, previous LCOM manpower studies have not emphasized statistical analysis of the output data.

In this thesis, the authors use LCOM to estimate the maintenance manpower requirements for an F-15 Tactical Fighter Training Wing (TFTW) with 72 unit equipment (U.E.) aircraft operating in a peacetime environment. In addition, they construct statistical confidence intervals around the resulting estimates of maintenance manpower requirements. Finally, the authors investigate the sensitivity of manpower requirements to variations in availability of aircraft parts and support equipment.

#### Thesis Scope

The LCOM peacetime environment is determined by TAC Training Syllabus Course Numbers F1500 B,I, and TX (Ref 30) requirements. These publications specify the flying training activity for F-15 pilot upgrade training which is the primary mission of a TFTW. The 58th TFTW located at Luke Air Force Base (AFB), Arizona currently uses these syllabi for all F-15 pilot upgrade training and is the base case for determining the peacetime F-15 LCOM operation and maintenance procedures.

#### Overview

The remainder of the thesis consists of five chapters. The LCOM chapter describes the Logistics Composite Model and Moody Manpower/Regression Programs. The Data Base chapter describes the maintenance and operations data base. The Methodology chapter lays the groundwork for this study's estimation of manpower requirements. The Analysis and Results chapter contains the manpower estimations and describes their sensitivity to variations in aircraft spare parts and support equipment.

Finally, the Conclusions and Recommendations chapter summarizes the thesis findings.

## II. LCOM MANPOWER ESTIMATION

Rather than present a detailed description of the LCOM process, this chapter introduces simplified LCOM concepts which form a basis for the remainder of the thesis. Further detail concerning LCOM can be found in Drake (Ref 7 and 8) and Tetmeyer (Ref 33). The LCOM manpower estimation process uses the Logistics Composite Model, the Moody Regression Program, and the Moody Manpower Program (Ref 7, 8, and 33). The interaction of these computer programs produces a complete basic manning document for a USAF maintenance organization.

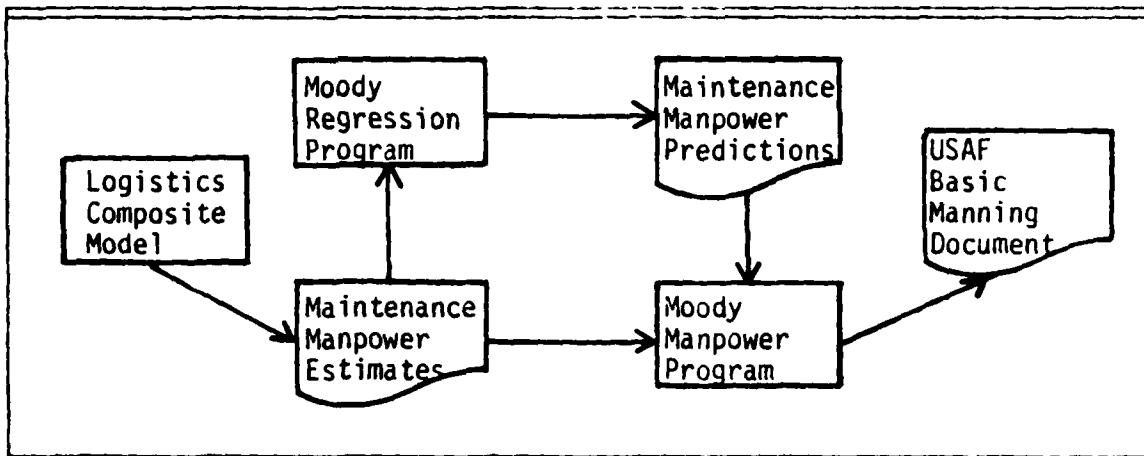


Figure 1. LCOM and Moody Regression/Manpower Program Relationship

Figure 1 depicts the interrelationship of LCOM and the Moody Regression/Manpower Programs. The Logistic Composite Model estimates maintenance manpower requirements for specified levels of flying activity. The Moody Regression Program uses these estimates and regression techniques to predict maintenance manpower requirements for a wide range of flying activity. The Moody Manpower Program uses the LCOM estimates and Regression predictions to produce a complete basic manning document for a USAF

maintenance organization. The following paragraphs describe each program in greater detail.

#### Logistics Composite Model

The LCOM uses three major computer programs to model aircraft flying operations, maintenance functions, and resource constraints. These programs are the preprocessor, main, and postprocessor programs (Ref 7: Chap. 1, p.2). The preprocessor program prepares aircraft operations and maintenance data for the main program. The main program simulates the interaction of aircraft operations, maintenance functions, and resource constraints and provides a statistical summary of the simulation results. The postprocessor program offers additional statistical output data.

Figure 2 illustrates the relationship between the three LCOM programs and the input/output data.

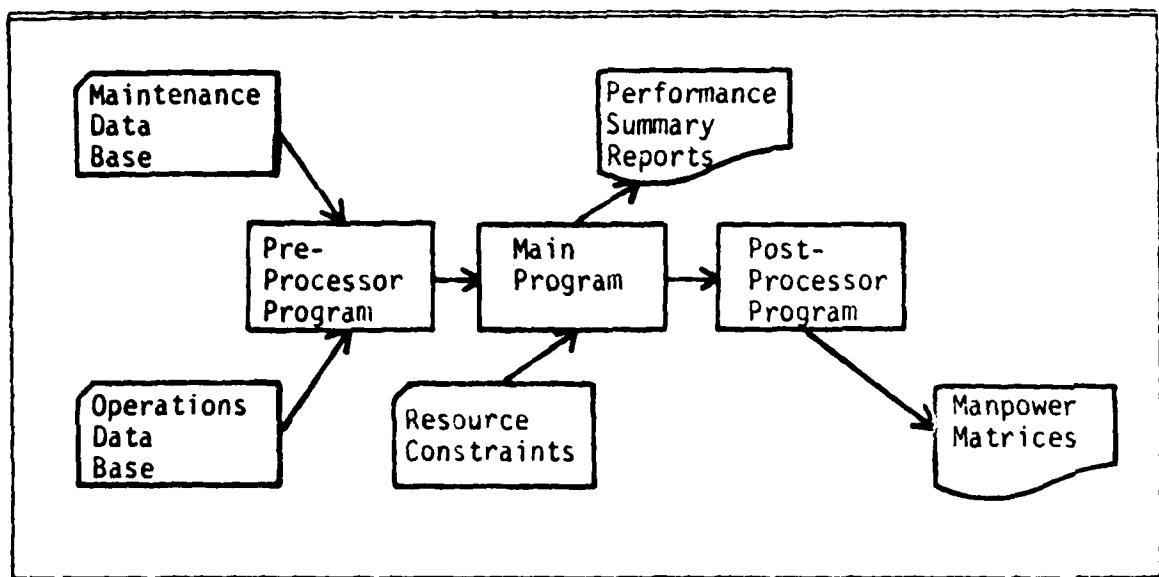


Figure 2. LCOM Program and Data Relationship

The operations and maintenance data bases represent the respective aircraft flying operations and maintenance characteristics. Resource

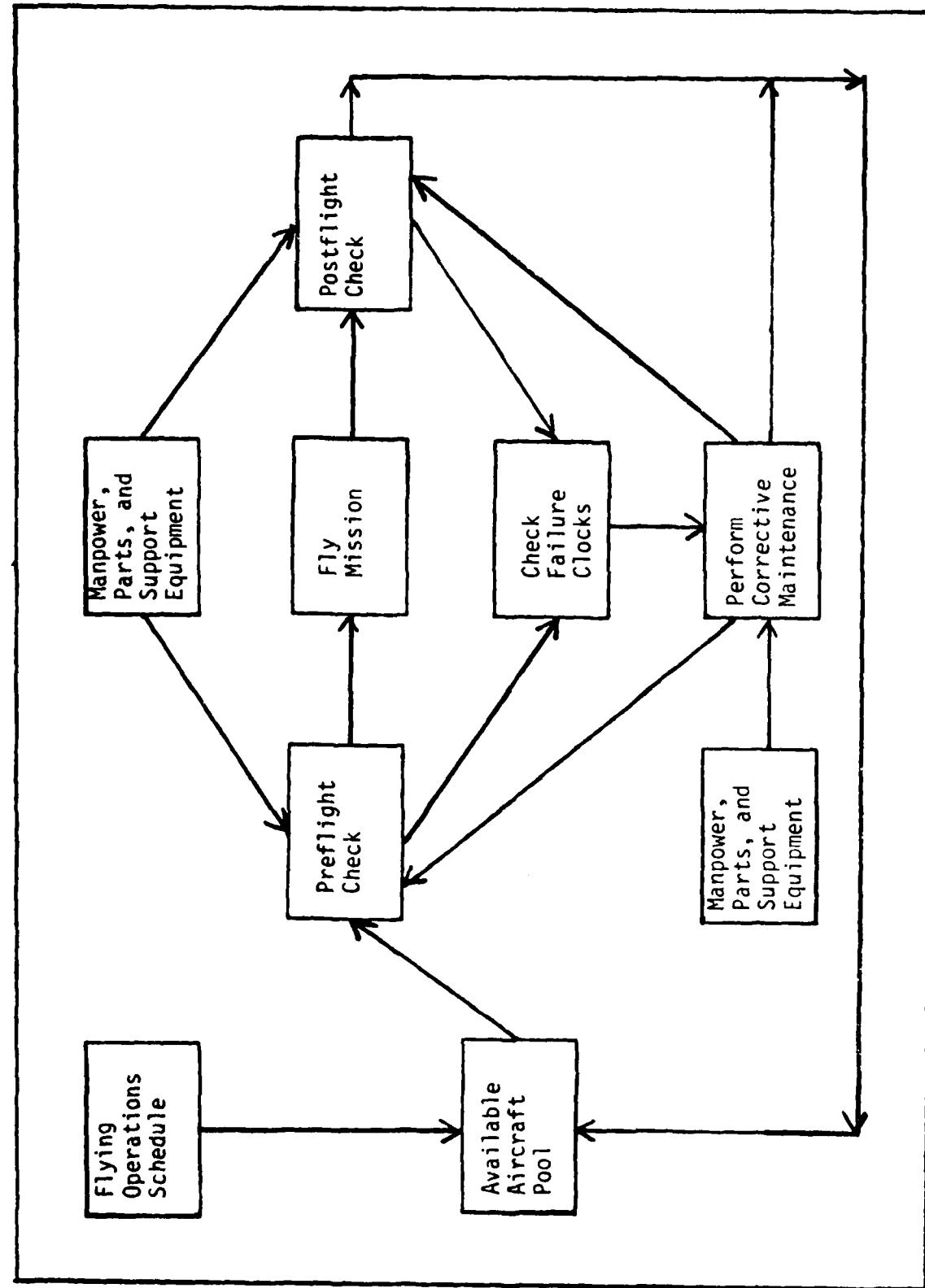
constraints consist of specified quantities of men by Air Force Specialty Code (AFSC), aircraft spare parts, and support equipment. The performance summary reports depict statistical summaries of the simulation results. Finally, the manpower matrices illustrate the daily distribution of manpower requirements (by AFSC).

Figure 3 shows how LCOM uses the flying operations schedule, maintenance functions, and resource constraints to simulate a sequence of maintenance activities. When the flying schedule calls for aircraft to start mission preparation, LCOM designates aircraft from the available aircraft pool for the mission. Each aircraft then processes through the preflight to postflight check blocks.

During this processing, LCOM uses men, spare parts, and support equipment as needed to perform maintenance functions. If all available manpower is already performing aircraft maintenance, LCOM delays the next mission until maintenance manpower is available. If the aircraft are ready for launch at their scheduled takeoff time, the missions fly for the specified mission length and then return for processing through the postflight check block. After postflight, LCOM places the aircraft in the available aircraft pool.

The LCOM also maintains a failure clock on each aircraft subsystem. These clocks use an exponential failure distribution to determine the number of sorties flown until corrective maintenance for their respective subsystems. Since LCOM does not simulate in-flight activity, it checks the failure clocks only during preflight and postflight. If the number of sorties flown equals a particular subsystem's clock value, LCOM lists that component as failed and ceases mission processing. The failed component then processes through the corrective maintenance block and uses

Figure 3. LCOM Simulation of Maintenance Activities



men, spare parts, and support equipment as necessary to perform the corrective maintenance. Upon completion of all corrective maintenance activity, LCOM allows the aircraft to continue with mission processing. However, if corrective maintenance delays an aircraft beyond its scheduled takeoff time, LCOM cancels the corresponding mission and returns the respective aircraft to the available aircraft pool.

The following description of LCOM's preprocessor, main, and post-processor programs more clearly defines the simulation process.

Preprocessor Program. The preprocessor program translates and organizes the maintenance and operations data bases for the main program. During data translation, the program scans the data base for inconsistencies and provides error diagnostic messages for data ambiguities (Ref 7: Chap. II, p.1). In some cases, the program makes computer logic assumptions when it finds minor data errors concerning user intentions and provides a message specifying the data ambiguity and corresponding program assumption. This feature prevents an unnecessary computer abort for minor data errors.

The LCOM maintenance data base consists of a weapon system's scheduled and unscheduled maintenance procedures, major components (parts), component failure frequencies, mean service and repair times, and resource (men, part, support equipment) requirements. This data represents the maintenance environment of an LCOM simulation (Ref 33:30).

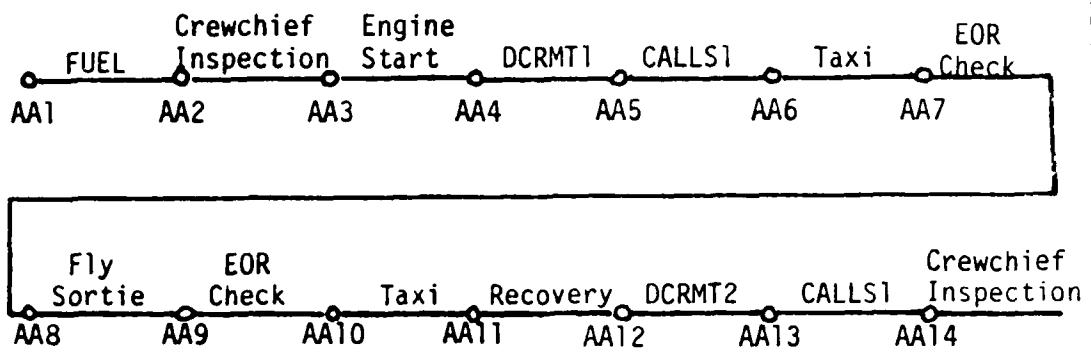
During data base formulation, the user graphically depicts the maintenance environment using LCOM networks (Ref 33:28). These networks define maintenance relationships within the data base. Figure 4 illustrates a simplified LCOM main network and corrective maintenance network for an aircraft mission.

In an LCOM network, tasks represent the scheduled and unscheduled maintenance procedures. These tasks are connected by network nodes (Ref 33:32). For example, nodes AA1/AA2, in Figure 4, define a FUEL task. The user also specifies the men (by Air Force Specialty Code), support equipment, and service or repair time necessary to complete a task. If a task resource is not available, LCOM will delay processing the aircraft mission beyond the guilty task until the constraining resource becomes available. For example, the FUEL task requires two men (AFSC 431X1), one fuel truck, and five minutes.

Every weapon system is composed of many major components or parts. The work unit code (WUC) manual for the particular weapon system numerically defines each of these parts. The LCOM maintains a failure clock for each major component in the maintenance network (Ref 33:36). For example, nodes M1/M2, in Figure 4, define the failure clock for the UHF radio (F63A00). The user assigns each failure clock a failure frequency parameter. He determines this parameter by analyzing failure rates of corresponding real life weapon system components. Mean sorties between maintenance action (MSBMA) is the most common parameter (Ref 33:56). In Figure 4, F63A00 has a MSBMA equal to 10 sorties. At the completion of an aircraft mission, the failure clock for each component in that mission main network advances one sortie.

The LCOM allows the user to specify the percent of time a major component fails before or after mission launch through the use of a clock decrement task (Ref 33:37). Nodes AA4/AA5, in Figure 4, define the clock decrement task prior to launch (DCRMT1) while nodes AA12/AA13 define the clock decrement task after launch (DCRMT2) for the UHF radio.

Main Mission Network:



UHF Radio Corrective Maintenance Network:

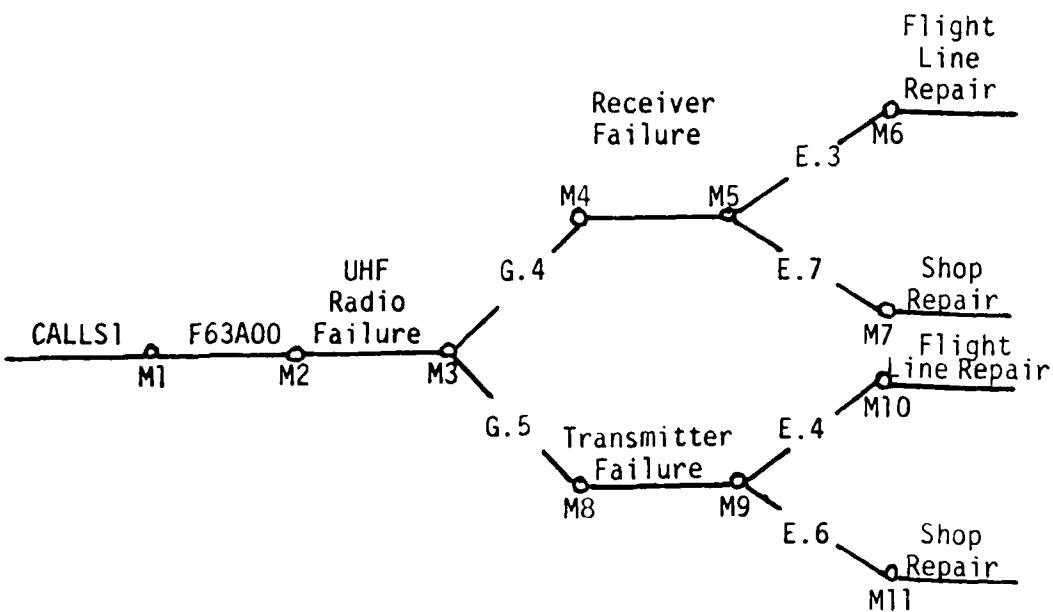


Figure 4. LCOM Maintenance Network

For example, DCRMT1 advances F63A00 three-fourth sortie and DCRMT2 advances F63A00 one-fourth sortie for a one sortie advance of the UHF radio clock by the completion of a processed aircraft mission.

Certain component failures in an LCOM network are not sortie related. In these cases, the failure clock uses a parameter other than MSBMA and the decrement task advances the failure clock by an adjusted amount independent of a sortie. One example is the gun on a tactical aircraft. Periodic gun maintenance is usually based on number of expended ammunition rounds. In this case, the failure clock uses rounds fired as a parameter and the decrement task advances the clock a certain number of rounds each mission sortie.

The LCOM interrogates a failure clock via a Call task (Ref 33:36). Nodes AA5/AA6 and AA13/AA14, in Figure 4, define the Call task (CALLS1) for the UHF radio failure clock (F63A00). Each time LCOM processes a mission through a Call task, the Model checks the corresponding clock to see if it has advanced to its MSBMA parameter. If the clock has advanced to this parameter, LCOM marks that component as failed and stops processing the aircraft mission. At the same time, the model begins processing the failed component through its respective corrective maintenance network. In Figure 4, LCOM processes the UHF radio through the UHF radio corrective maintenance network after F63A00 advances 10 sorties.

Within the corrective maintenance network, LCOM allows the user to specify which subsystem(s) caused the component failure and who fixes the subsystem(s). The model accomplishes this function with G and E probability distributions (Ref 33:62-65).

A G probability is a nonmutually exclusive probability that determines which subsystem(s) caused the component failure. Since the G

probability is nonmutually exclusive, either one or more than one subsystem can cause a component failure. In Figure 4, there exists a .4 probability that the receiver (nodes M4/M5) caused the radio failure, a .5 probability that the transmitter (nodes M8/M9) caused the radio failure, and an inferred .1 probability that both the receiver and transmitter caused the radio failure.

An E probability is a mutually exclusive probability that determines who fixes the broken subsystem(s). Since the E probability is mutually exclusive, Flight Line Repair (node M6) or Shop Repair (node M7), but not both, can fix the receiver. In Figure 4, there exists a .7 probability that Shop Repair fixes the receiver and a .3 probability that Flight Line Repair fixes the receiver.

If Shop Repair fixes the receiver, LCOM immediately generates a new part from supply stock and allows the aircraft mission to continue processing through its main network. After Shop Repair fixes the receiver, LCOM returns the repaired receiver to supply stock.

After constructing the LCOM networks, the user transcribes this information onto LCOM Extended Forms 11 (Ref 33:32-36). He then transfers this data to a computer card deck. This card deck is the completed maintenance data base. Figure A-1 in Appendix A contains a sample LCOM Extended Form 11.

The operations data base consists of the aircraft daily flying and maintenance schedules. These schedules form the operational scenario for an LCOM simulation.

The flying schedule contains the aircraft mission type, number of primary aircraft for each mission, mission takeoff time, mission cancel time, and flight duration. Missions with similar configurations, flight

time, preflight and postflight servicing, and maintenance crew requirements are grouped under a single LCOM mission type (Ref 33:16), since LCOM only simulates ground activity. As far as LCOM is concerned, flight time is that time which an aircraft is unavailable for maintenance.

The maintenance schedule specifies the number of spare aircraft per mission type, missions that fly more than once during the day (preflight to thru-flight), and number of phase inspections and aircraft washes.

The user designs the operational scenario for a specified level of flying activity. This level of activity is usually designated as aircraft sortie rate. Equation (1) defines sortie rate.

$$\text{sortie rate} = \frac{\text{sorties/day}}{\text{aircraft U.E. size}} \quad (1)$$

The U.E. size is the number of authorized aircraft assigned to a unit. Sorties per day may be either scheduled sorties or accomplished sorties. During the planning stage, the user bases the operational scenario on a scheduled aircraft sortie rate. After an LCOM simulation, the user computes an accomplished aircraft sortie rate.

The user records the completed operational scenario onto LCOM Forms 20 (Ref 33:17) prior to transferring the information to a computer card deck. The punched card deck represents the operational data base. Appendix B contains three operational scenarios based on scheduled sortie rates of .43, .74, and 1.0.

Main Program. The main program simulates maintenance and operations data base interaction. During this interaction, the main program uses available resources to prepare scheduled maintenance and flying

activity. The program processes each mission type through its respective main network while simulating all required maintenance tasks.

The preprocessor translated maintenance data base contains unconstrained maintenance manpower, aircraft spare parts, and support equipment. When these resources are left unconstrained, the main program has little difficulty complying with the operations data base's scheduled sortie rate provided sufficient time is allowed between scheduled missions for postflight and preflight maintenance tasks. If resources are constrained, the main program delays mission types, as necessary, when men, spare parts, and/or support equipment are unavailable. If a mission delay exceeds its cancel time, the program cancels the guilty mission. To constrain these resources, the user submits a series of computer cards to the main program prior to simulation. Each card specifies the number of maintenance men by AFSC and work shift, quantity of spare parts by WUC, and/or quantity of support equipment available during the LCOM simulation (Ref 33:123).

After simulation, the main program provides statistical data in the form of Performance Summary Report (PSR). These reports include the number of flying hours, number of sorties requested, number of sorties accomplished, manhours (by AFSC) used, manhour utilization rate (by AFSC), and parts (by WUC) consumed, generated, or backordered (Ref 7, Chap. II, p. 3). The user specifies the interval and number of PSR's desired prior to simulation. Figures C-1 and C-4 in Appendix C contain sample PSR's. The PSR's are used to evaluate the effects of main program simulation. For example, the user can compare scheduled and accomplished sortie rates to determine the effect of resource constraints on the simulation.

Postprocessor Program. The postprocessor program produces manpower matrices for each AFSC. These manpower matrices depict how an AFSC workload varies with the time of day (Ref 33:121). Figures C-2, C-3, C-5, and C-6 in Appendix C contain examples of on-equipment, off-equipment, and backorder matrix printouts for various AFSC's.

These on/off equipment printouts display the number of times during a simulated period that the number of people shown in the leftmost vertical axis are working at the time of day shown on the horizontal axis. This time is in half hour increments.

For instance, the on-equipment matrix for AFSC 326C2, in Appendix C, shows 11 cases in which two people are needed between 0330 and 0400.

The backorder matrices indicate which work shifts require additional personnel in order to increase sorties accomplished.

#### Moody Regression Program

The Moody Regression Program allows the user to estimate maintenance manning requirements for a wide range of flying activity (Ref 33:126). The user provides the program with three sets of LCOM estimated manning requirements (by AFSC) for an operational scenario based on three different scheduled sortie rates. The Moody Regression Program uses this data to compute first and second order regression equations for maintenance manning (by AFSC) as a function of flying hours per month. The program compares these ordered equations for goodness of fit and chooses that equation, for each AFSC, with the best fit. These equations can be used to graphically depict the information as shown in Figure 5.

#### Moody Manpower Program

The Moody Manpower Program produces a complete basic authorization document for a maintenance organization (Ref 33:129). The program

requires a unit's aircraft U.E. size and flying hours per month from the LCOM simulation, regression equations from the Moody Regression Program, the minimum crew size for each AFSC, and the organization's Major Command supervision and overhead requirements. The resultant document defines the organization structure by Air Force Functional Code (FC) and provides manning requirements by AFSC grade level, for each FC.

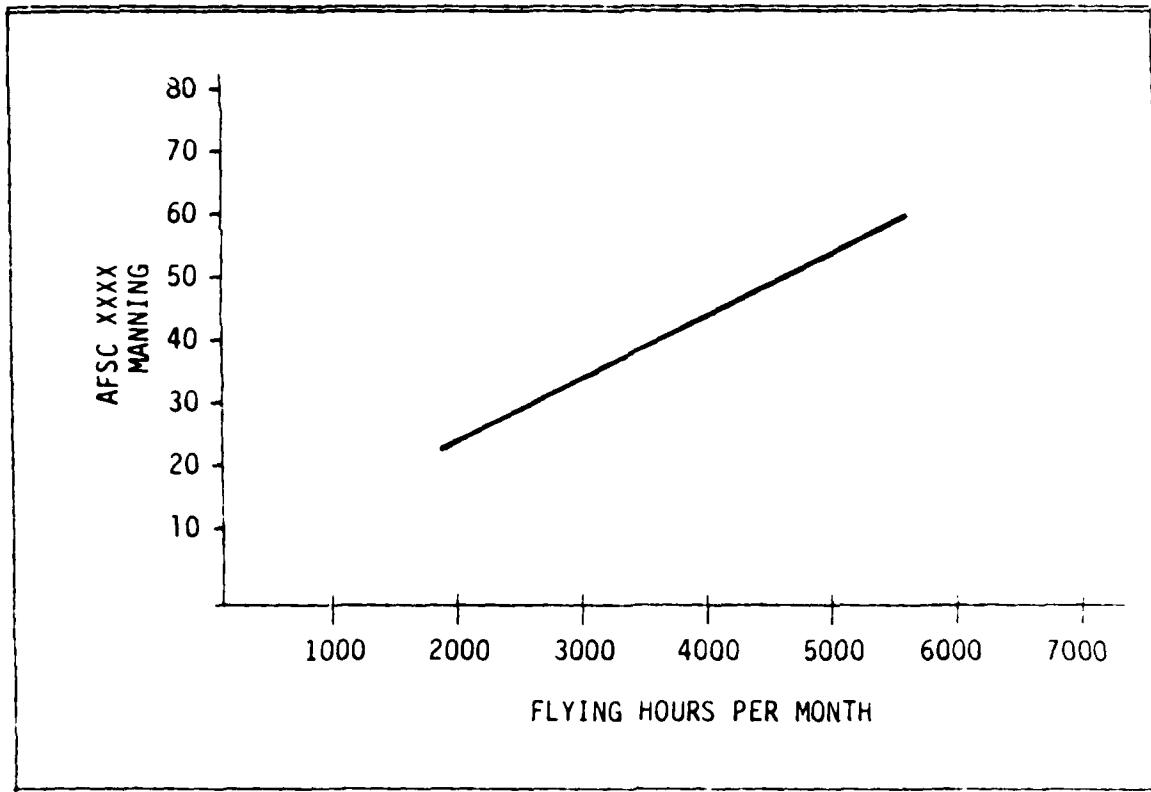


Figure 5. Moody Regression Graph

#### Summary

This chapter established the basic concepts used in the LCOM manpower estimation process. These concepts included the three LCOM programs, the Moody Regression Program, and the Moody Manpower Program. The next

Chapter uses these concepts to describe the F-15 peacetime maintenance data base, operations data base, and resource constraints used in this study.

### III. DATA BASE

This chapter contains a discussion of the maintenance and operations data bases and resource constraints used in the F-15 TFTW peacetime Logistics Composite Model. The description includes pertinent assumptions and the maintenance organization structure.

#### Maintenance Data Base

The maintenance data base is a modified version of maintenance data used in the ASD F-15/F-16 Wartime Study (Ref 5). Revisions include maintenance of TF-15 aircraft and simplified flight line maintenance networks with reduced armament and electronic counter measure requirements. Pages 107 through 149 in Appendix A contain a computer listing of the revised data base. The following paragraphs discuss these revisions in terms of the maintenance organization structure, scheduled and unscheduled maintenance procedures, repair/service times, weapon system components, and failure parameters.

Maintenance Organization Structure. Figure 6 illustrates the maintenance organization structure that supports the LCOM F-15 TFTW. This structure is similar to the 58th TFTW maintenance operation. The LCOM estimates those functional codes (FC's) designated by an "L" in Figure 6; the Moody Manpower Program produces a basic authorization document for all FC's depicted in the organization structure. Table I translates these FC's into AFSC's for LCOM estimated manpower and gives their work descriptions.

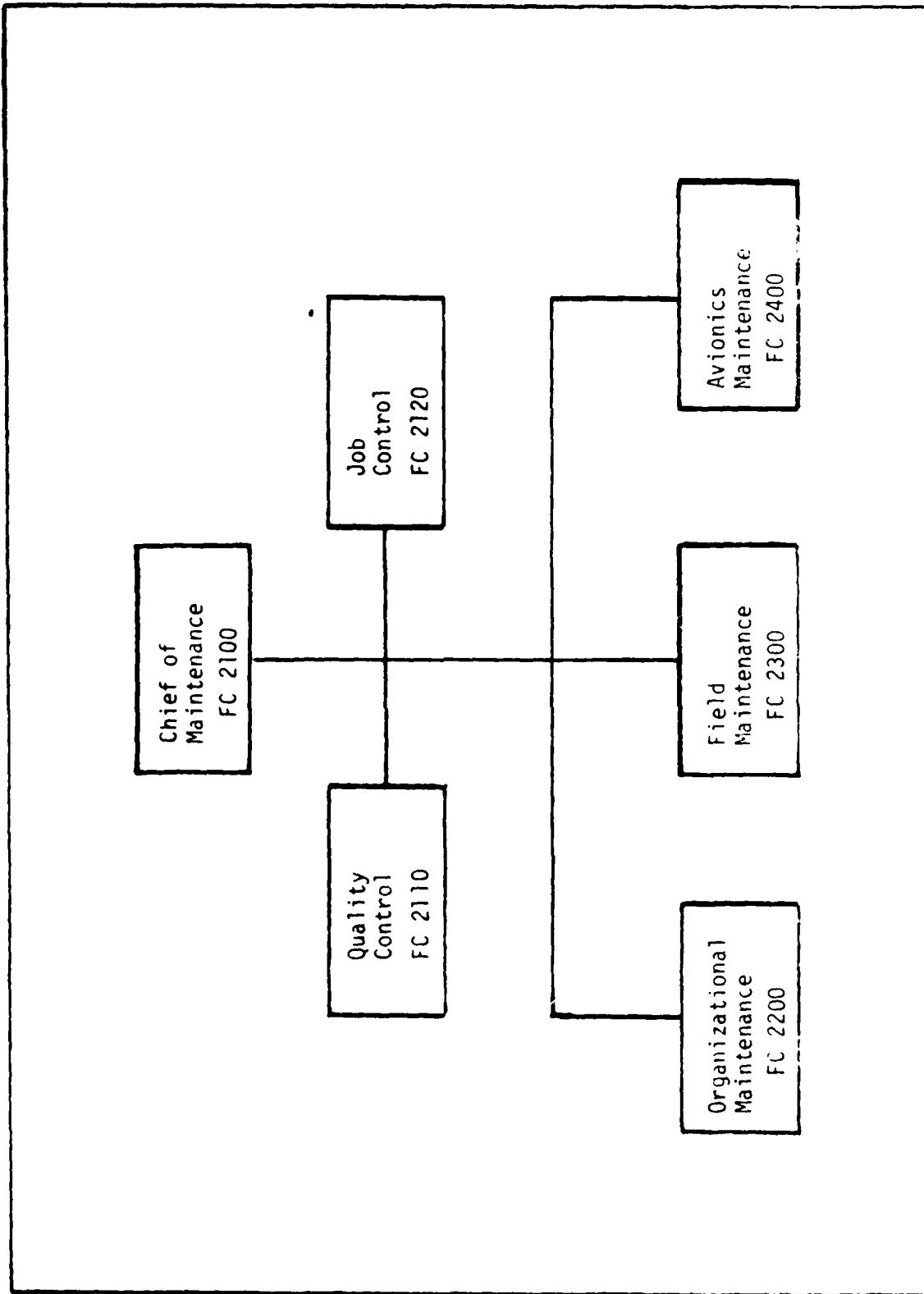


Figure 6. LCOM F-15 TFTW Maintenance Organization Structure

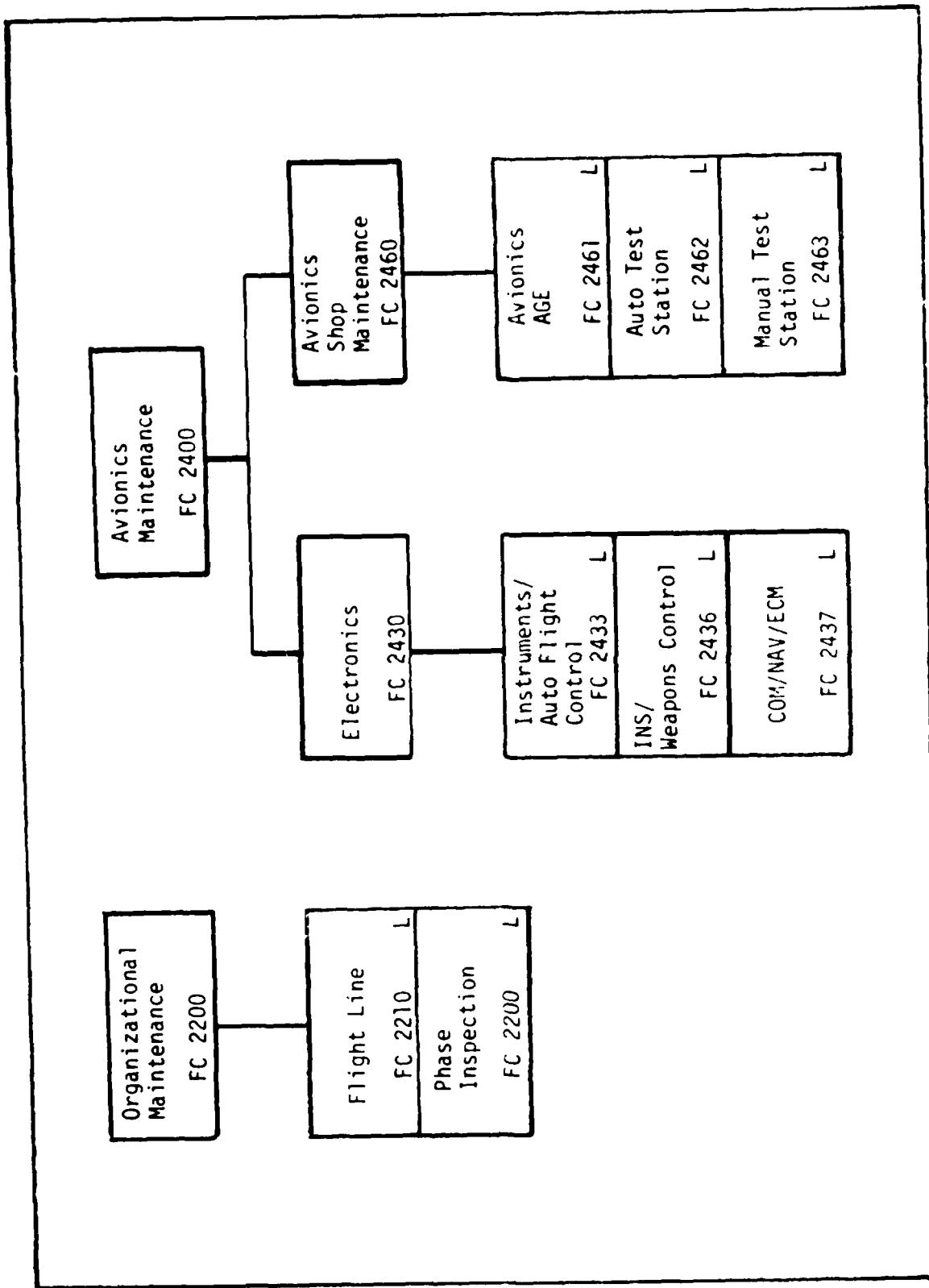


Figure 6. LCOM F-15 TFTW Maintenance Organization Structure (Continued)

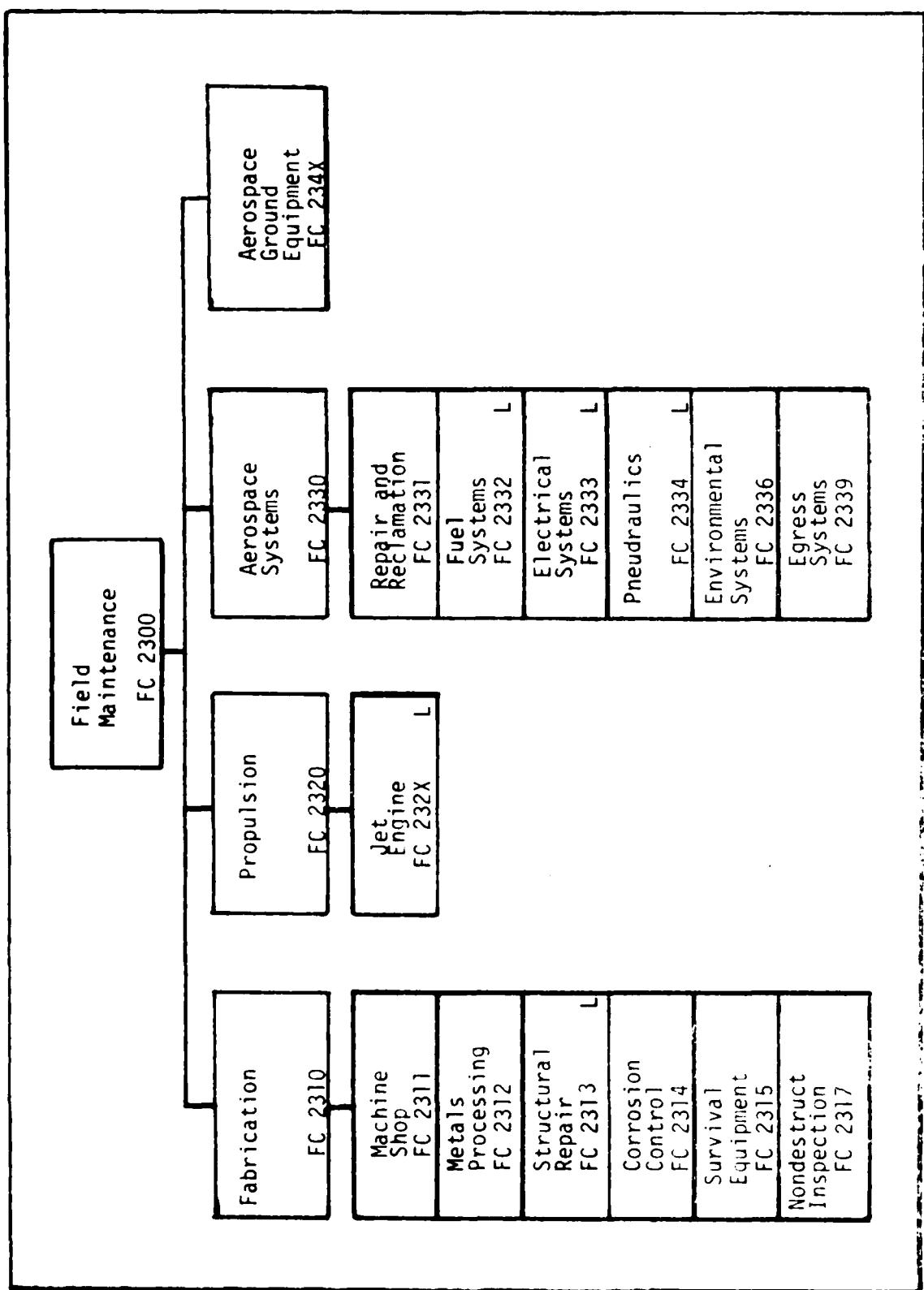


Figure 6. LCOM F-15 TFTW Maintenance Organization Structure (Continued)

Table I  
Function Code to AFSC Translation

FC	WORK DESCRIPTION	AFSC
22XX	Flight Line Crew Chief/ Phase Inspection	431X1
2313	Structural Repair	531X3
232X	Jet Engine Shop/Jet Engine Flight Line/Test Cell	426X2
2332	Fuel Systems	423X3
2333	Electrical Systems	423X0
2334	Pneudraulics	423X4
2336	Environmental Systems	423X1
2339	Egress Systems	423X2
2433	Automatic Flight Control/Instruments	326X2B
2436	Inertial Navigation System/Weapon Control	326X2A
2437	Communications/Navigations/Electronic Counter Measures	326X2C
2462	Automatic Test Station	326X1D
2463	Manual Test Station	326X1C

Scheduled and Unscheduled Maintenance. The wartime data base contained maintenance procedures peculiar to a wartime environment. With the technical assistance of the TAC advisor, the authors deleted wartime procedures and added, when necessary, the appropriate peacetime maintenance functions. The resulting LCOM networks represent those scheduled and unscheduled maintenance procedures performed by the 58th TFTW located at Luke AFB, Arizona. These modifications are based on an operational audit of maintenance procedures at Luke AFB (Ref 22) and TAC coordinated peacetime maintenance assumptions (Ref 16, 17, and 27). These assumptions consist of the following:

- The LCOM simulation models maintenance procedures of a 72 U.E. TFTW operating under TAC Training Syllabus course numbers F1500 B, I, and TX (Ref 30).
- Both F-15A and TF-15A aircraft maintenance are modeled.
- The 20mm gun is loaded with 1,000 rounds of ammunition and reloaded after two DART missions are flown. This is the only "live" ammunition used in the simulation.
- Ground aborted missions are not rescheduled since course flying requirements have a nine percent refly factor in establishing the Flying Training Program.
- The wing maintenance activity is organized per AFM 66-1 (Ref 4) and does not reflect Maintenance Posture Improvement Program (MPIP) reorganization.
- The F-15/TF-15 phase inspection procedures performed by the 58th TFTW at Luke AFB are used in scheduled maintenance networks.

- Not repairable this station (NRTS) components use a 15 day resupply time.
- On/off equipment maintenance is available 24 hours a day and seven days a week.
- On-equipment failure of a component is corrected by a remove and replace task when parts are available.
- Cannibalization is initiated when spare parts are constrained and a removed component cannot be repaired in time to accomplish a mission.
- End-of-runway teams are always available during scheduled flying periods.

Maintenance Repair/Service Time. Maintenance task repair and service times are based on interviews with the respective work center supervisors at Luke AFB, Arizona (Ref 1). The data base listing in Appendix A depicts these times and the respective maintenance tasks.

Weapon System Components. The authors used the F/TF-15A Series Work Unit Code (WUC) Manual to describe all weapon system components (parts) (Ref 36). A WUC is a five character code (11XXX-99XXX) that identifies each weapon system part. The maintenance data base describes each F-15 part at the two-four significant character WUC level. This description is equivalent to the line replaceable unit (LRU) level.

Component Failure Parameters. The maintenance data tape (Ref 1) for the 58th TFTW at Luke AFB, defines failure parameters for components in the corrective maintenance networks. This tape contains maintenance

data for the September 1975 - February 1976 time period and includes 2132 F/TF-15 flying sorties and 2867 flying hours.

Tetmeyer, Moody, and Nichols (Ref 32 and 33) describe the detailed procedures necessary to extract useful maintenance data from this tape. They also illustrate the method to compute the LCOM failure parameters (MSBMA and G/E Probabilities).

The data base listing in Appendix A illustrates the G and E probabilities for each corrective maintenance network. Appendix D contains each component failure clock, its corresponding MSBMA, and decrement value. The decrement values come from the F-15/F-16 Wartime Study (Ref 5).

#### Operations Data Base

The F-15 peacetime operations data base contains the flying training schedule and maintenance wash and phase inspection schedules and supports a 72 U.E. TFTW consisting of 48 single seat (F-15) and 24 tandem seat (TF-15) aircraft. The following TAC coordinated assumptions (Ref 16, 17, and 27) were used during construction of the operational scenarios contained in Appendix B.

- TAC Training Syllabus Course Numbers F1500 B, I, and TX define the unit's flying requirements (Ref 30).

- The modeled TFTW conducts only a conversion and air-to-air training program.

- Flying schedule sortie length and variance are derived from the training syllabi.

-Flying training is not scheduled on weekends or holidays.

-Night flying is scheduled as training requires.

-Aircraft scheduled for morning flights are thru-flighted as required to meet mission requirements.

-Aircraft missions delayed longer than two hours are cancelled.

-Only scheduled and spare mission aircraft are preflighted each day.

-Preflight inspections for each aircraft are completed at least two hours prior to scheduled takeoff.

Flying Schedule. This study uses three flying schedules to obtain scheduled sortie rates of .43, .74, and 1.0. Each schedule contains a 13 percent over schedule for maintenance cancellations and a nine percent over schedule for rescheduled training requirements. The .74 sortie rate establishes the base line flying schedule while the .43 and 1.0 sortie rates allow for decreased or increased demands in F-15 pilots. The schedules use a 65/35 ratio of F-15 versus TF-15 aircraft.

The flying schedules involved two basic mission types: Conversion and Air-Air missions. Conversion missions familiarize the pilot with basic F-15 aircraft performance characteristics. Air-Air missions contain tactical air intercept, combat, and gunnery maneuvers. All three flying schedules are based on a 30/70 ratio of Conversion versus Air-Air missions.

Maintenance Schedule. The maintenance schedule specifies the number of spare aircraft, thru-flights, washes, and phase inspections. In this study, the following conditions apply: 52 percent of scheduled aircraft are thru-flighted each day; airframes receive a wash every 75 hours and a phase inspection every 50 hours; spare aircraft are based on 10 percent of scheduled sorties.

Table II summarizes the daily maintenance requirements for the three operational scenarios used in this study.

Table II  
Daily Maintenance Requirements

	Scheduled Sortie Rate		
	.43	.74	1.0
Scheduled Aircraft	21	35	47
Scheduled Sorties	31	53	72
Spare Aircraft	4	6	8
Hours per Airframe per Month	15	25	33

#### Resource Constraints

During the LCOM simulation, the authors constrain selected spare parts and support equipment to measure the effects on accomplished sortie rate and maintenance manpower. These constraints reflect the quantity of spare parts and support equipment available from base supply stock.

This study uses part supply levels found in the F-15/F-16 Wartime manpower Study (Ref 5:60-64). These quantities reflect the most current information on part levels. Appendix E lists the constrained spare parts by WUC and the corresponding supply quantity.

The only support equipment constrained during simulation are avionic test stations (ATS's). Maintenance personnel use these stations to troubleshoot aircraft avionic components. There are three ATS types in the maintenance data base. Appendix E lists each type, the job description, and constrained quantity.

#### Summary

The F-15 TFTW maintenance and operations data bases and resource constraints were discussed in this chapter. The discussion included pertinent TAC coordinated assumptions and the modeled maintenance organization structure. The next section contains the procedures used in this study to simulate peacetime maintenance and operations data base interaction and analyze the resultant manpower estimates.

#### IV METHODOLOGY

In this chapter, the authors discuss the concepts and procedures employed in the development of manning estimates using the LCOM model, and the analyses of results obtained. Specifically, this includes an explanation of the sequence of simulation runs performed, the use of the resulting data to compute manpower estimates, and the procedures employed to validate the model. Further, the authors discuss the statistical concepts used to define steady state for the model and to construct confidence intervals for the manpower estimates. Finally, the use of the Moody Regression and Moody Manpower Programs to investigate the sensitivity of manning requirements to parts/ATS constraints is explained.

##### Sequence of Simulation Runs

In order to estimate manpower requirements for a particular combination of sortie rate and parts/ATS constraints, a series of LCOM runs was performed as shown in Figure 7. To investigate the sensitivity of manpower requirements to various constraints and sortie rates, this sequence was repeated for each of the nine possible combinations of the three sortie rates (.43, .74, and 1.0) and the three levels of resource constraints (unconstrained parts/ATS, constrained parts and unconstrained ATS, and constrained parts/ATS).

##### Determination of Manpower Requirements

The LCOM determined manpower requirements are based on the total manhours used for each AFSC. After running the model with unconstrained manpower as indicated in Figure 7, it is necessary to constrain the number of men available in the model in order to estimate the actual number

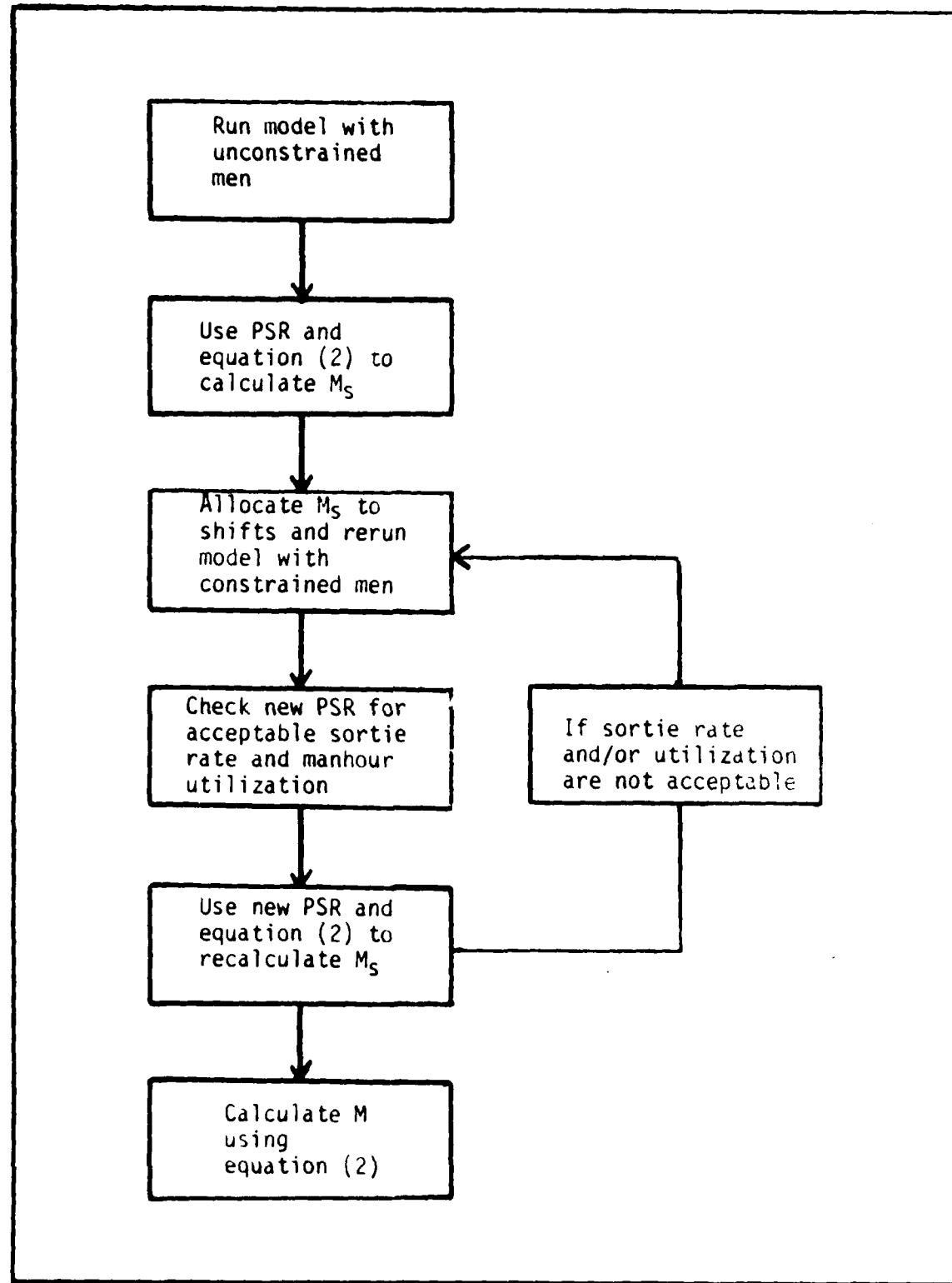


Figure 7. Sequence of Simulation Runs

of men required to support a specified sortie rate. Equation (2) is used to convert each AFSC's total manhours used into these manning constraints.

$$M_S = \frac{\text{Total Manhours Used}}{(\text{Utilization Factor})(\text{Number of Days})(\text{Shift Length})} \quad (2)$$

In this equation, the total manhours used for each AFSC are obtained from the simulation's performance summary report (PSR). The utilization factor is the fraction of manhours available for direct work; in this case, the Air Force standard is 0.6 (Ref 2: Chap. 6, p. 29). Shift length is eight hours. The  $M_S$  then becomes the average number of men available each day for each AFSC (Ref 33:121). This number is allocated over the three shifts using the manpower matrices as a guide. The resulting shift manning is incorporated into the model as a constraint on manpower. Certain AFSC's require a minimum crew size to perform their maintenance functions. In cases where  $M_S$  is less than the daily minimum crew manning, the minimum crew size is assigned to each shift as the constraint on manpower. The simulation is then rerun to determine what change has occurred in the accomplished sortie rate, as defined by equation (1), and to ensure that the resulting manhour utilization rate has not exceeded 0.6. If the accomplished sortie rate and/or manhour utilization rate are unacceptable, the process is repeated as indicated in Figure 7.

The  $M_S$  resulting from this procedure, however, is not the actual number of men required because it does not consider the fact that each individual normally works five days a week, takes leave, and may otherwise be legitimately absent from work. The Air Force standard for actual hours worked per man per month is 144 hours (Ref 3:7-8). Equation (3) is used to convert  $M_S$  into Direct Manning ( $M$ ). Direct Manning

represents the final manpower estimate for each AFSC in the LCOM simulation.

$$M = \frac{M_S(\text{work days/month})(\text{shift length})}{144 \text{ hours/man/month}} \quad (3)$$

#### Model Validation

If a simulation model is to be of use in making predictions, then those predictions must be shown to be correct or at least as good as predictions made using some other method. Emshoff and Sisson state that the best possible evidence of such validity is that the model has made satisfactory predictions in the past (Ref 10:204). In this respect, the general LCOM model has been proven valid by numerous previous studies of other weapons systems and scenarios. There was, however, no direct counterpart to the present study, and for this reason a further investigation of validity was conducted.

A first-time model, such as the one under consideration here, cannot be validated completely until the system it represents actually comes into existence. Until that time, the model's validity can only be evaluated in terms of credibility. Emshoff and Sisson suggest that such validation consists of debugging the program, checking that key subsystem models predict their part of the world well (using historical data), and that knowledgeable individuals agree to the reasonableness of the model structure and output or face validity (Ref 10:206). The authors used these criteria in conjunction with a more detailed debugging procedure, recommended by Tetmeyer, to develop the following validation procedure (Ref 33:111, 113).

A 28 day unconstrained simulation was run, with complete diagnostics, and the output checked to insure that: all phases and scheduled

inspections were accomplished as well as a high percentage of scheduled sorties, there were no unsatisfied demands for personnel, the number of repairable generations for each item in the shop repair summary was equal to the number of units demanded for the same item in the supply summary, and, finally, there were no cannibalizations, supply backorders or unsatisfied demands (anything else would have indicated a data error) (Ref 33:113).

Next, a 28 day simulation was run with each of the three flying schedules. In each case, all unscheduled maintenance was removed from the model, thus preventing any equipment or aircraft breakdowns. In each case, all scheduled sorties were in fact accomplished, demonstrating the feasibility of the flying scenarios.

Finally, the MSBMA assigned from historical data to each failure clock was compared to the MSBMA actually observed during a 28 day run of the simulation. In most cases the variation was low; those few cases that did show a large variation in MSBMA had a large assigned MSBMA (the failure should seldom occur). In these cases small numerical differences between observed and predicted numbers of failures resulted in large changes in MSBMA. In light of the negative exponential distribution of failures in the model, and the short time span of the test simulation, variations of this sort were not unexpected. Further, as noted by Emshoff and Sisson, variations in the distribution of infrequent events are not normally significant when the model is intended to predict the behavior of some larger system (Ref 10:205). Consequently, the authors saw no reason to doubt the validity of the model based on its stochastic behavior.

The model was also tested for face validity. Emshoff and Sisson state that face validity exists when knowledgeable individuals agree to the reasonableness of the model structure and output (Ref 10:204). In this case, Lowell and Moody examined the model and output and found it, in their opinion, to be reasonable (Ref 24).

### Steady State

In any simulation model, one of the important questions the researcher must answer is, "How long must the simulation be run until the parameters of interest (in this study sortie rate and manhours used) reach typical values for the system, or steady state?" Steady state, of course, is a relative condition depending on the specific parameters being considered and the degree of accuracy desired from the simulation. For instance, the time series output of a hypothetical simulation might appear like that shown in Figure 8.

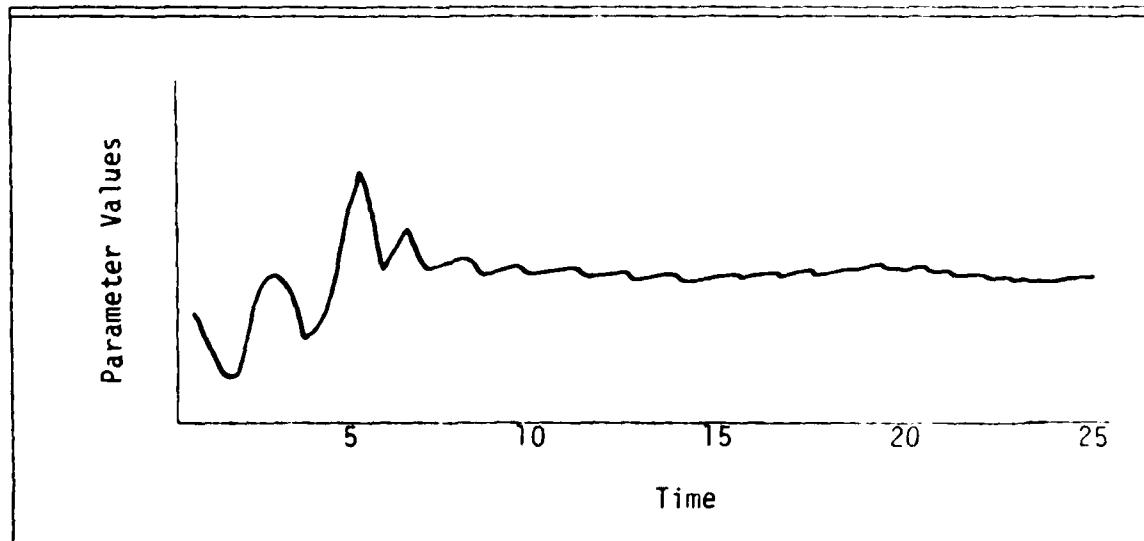


Figure 8. Type I Hypothetical Steady State Behavior

In this particular hypothetical example, after time period 10 the value of the output parameter is reasonably constant. In such a situation, the user could confidently accept data after that time as being typical of the system being modeled.

Unfortunately, many simulations do not exhibit the type of behavior just described. The values of output parameters may increase or decrease over time, indicating that they do not have a typical value within the system being simulated. Another possibility is that the value of the output may fluctuate considerably from one observation to the next; yet, in viewing such data over time the individual data points show no particular trends; but instead, appear to be randomly distributed about some central value. Such a case is illustrated in Figure 9. A closer

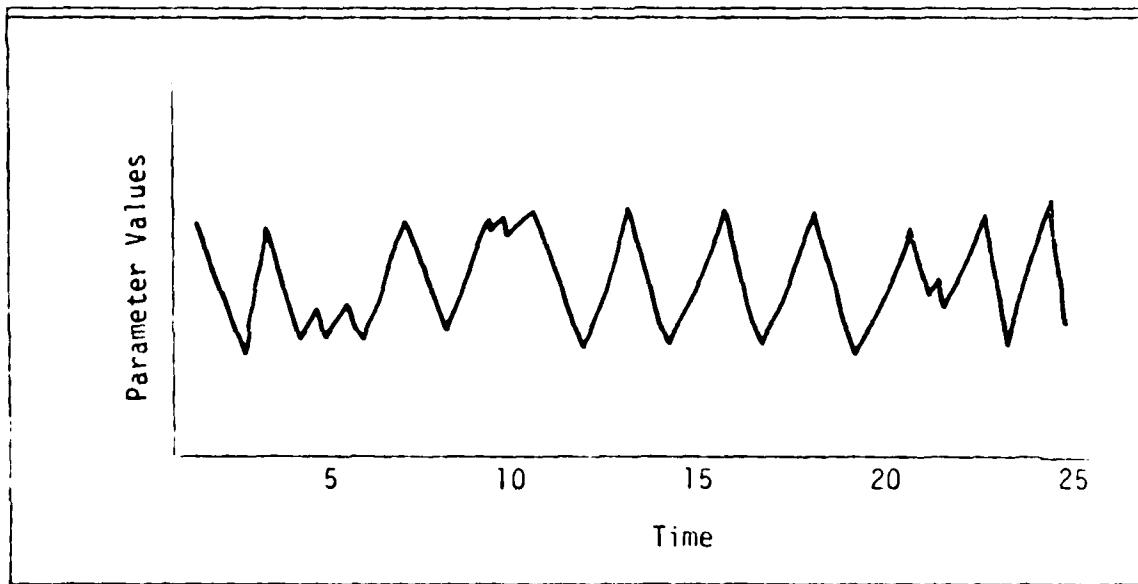


Figure 9. Type II Hypothetical Steady State Behavior

examination of the two situations depicted in Figures 8 and 9 reveals that the graph in Figure 8 after period 10, is actually similar to the situation depicted in Figure 9 except for the amplitude of the fluctuations.

### Some Criteria for Steady State

Tetmeyer states in his discussion of the LCOM model that steady state is reached when successive thirty day manhour totals for each AFSC do not vary more than five percent (Ref 33:112). Of course, this is just another way of stating how much error the user is willing to accept.

As noted by Conway:

"...it is also important to recognize that equilibrium is a limiting condition which may be approached but never actually attained. This means that there is no single point in the execution of a simulation experiment beyond which the system is in equilibrium. The difference between the temporal and limiting distribution presumably decreases with time and one seeks a point beyond which he is willing to neglect the error that is made by considering the system to be in equilibrium" (Ref 6).

Emshoff and Sisson mention a procedure similar to that used by Tetmeyer, but go on to discuss other methods which the authors of this study felt were possibly more appropriate (Ref 10:192). Specifically, they state that steady state has been reached when successive output values vary randomly about some typical value; or similarly, when successive observations of the time series output are statistically indistinguishable (Ref 10:190).

The procedure described by Tetmeyer for identifying steady state is in common usage among LCOM practitioners. In an effort to reduce computer running time, the authors elected to investigate the feasibility of determining steady state by comparing probability distributions as suggested by Emshoff and Sisson.

Student's T Test. Student's T test is a very powerful statistical test which can be used to compare the means of two populations. Such

a test might be used to indicate if the mean values of the simulation output over two adjacent time periods were statistically indistinguishable (Ref 25:343). This, in turn, would indicate that the simulation was in steady state. To use the test, however, one must be able to assume that the sample data is from at least a near normal or mound shaped probability distribution (Ref 12:169).

Since, in this study, the flying scenario calls for no flying on Saturday or Sunday, the distribution of manhours used per day is bimodal in nature. Consequently, the authors felt an assumption of normality was not warranted.

It is important to point out, nevertheless, that in other experiments having a continuous flying schedule, such as a wartime model or a peacetime scenario as described by Tetmeyer, the T test might be an appropriate tool (Ref 33:126-127). For a further discussion of the T test, the reader is referred to any elementary text on parametric statistics.

The Man-Whitney U Test. The Mann-Whitney U test is a nonparametric statistical test designed to indicate if two independent random samples can reasonably be expected to have come from different probability distributions, or if the two are stochastically indistinguishable. The primary advantage of this test is its applicability regardless of the probability distribution of the data to be tested (Ref 28: 116).

Use of the U Test in Determining Steady State. In light of the distribution-free nature of the Mann-Whitney test, it was tested as an indicator of steady state on the simulation runs which had constrained

manpower. The first fourteen days of simulation output were compared to the remainder of the data from each run; a two week segment was chosen to provide sufficient data for meaningful application of the test, and also to avoid bias which would have resulted if proportionately more Saturdays and Sundays (nonflying days) were included in one of the samples than in the other. The null hypothesis ( $H_0$ ) was defined to be:

$H_0$ : The two samples come from the same probability distribution.

If  $H_0$  is not rejected, then the test is not able to distinguish between the two samples, and the authors considered steady state to exist at the beginning of the first sample. The alternate hypothesis ( $H_a$ ) was defined as:

$H_a$ : The two samples do not come from the same probability distribution.

When  $H_a$  is accepted, a significant difference exists between the two samples indicating that steady state has not been reached at the beginning of the first sample. In such instances, the authors threw out data from the first part of the time series (in increments of seven days) until the test indicated that steady state had been reached.

Application of the Mann-Whitney test involves first, computing the value of the  $U$  statistic for the two samples being compared.  $U$  is defined as the smaller of

$$U = N_1 N_2 \frac{N_1(N_1 + 1)}{2} - W_1 \quad (4)$$

or  $U = N_1 N_2 \frac{N_2(N_2 + 1)}{2} - W_2$  (5)

where  $N_1$  and  $N_2$  are the sample sizes of the two time periods being compared, and  $W_1$  and  $W_2$  are obtained by ranking the  $(N_1 + N_2)$  data points from one to  $(N_1 + N_2)$  and summing these ranks for each group. Then, for  $N_1$  and  $N_2$  greater than ten.

$$Z = \frac{U - E(U)}{\sqrt{V(U)}}$$
 (6)

where  $Z$  is the standard normal random variable,  $E(U)$  is the expected value of the  $U$  statistic

$$E(U) = \frac{N_1 N_2}{2}$$
 (7)

and  $V(U)$  is the variance of the  $U$  statistic.

$$V(U) = \frac{N_1 N_2 (N_1 + N_2 + 1)}{12}$$
 (8)

(Ref 25:535-538).

If  $H_0$  is true then

$$P(|Z| \leq Z_{\alpha/2}) = \alpha$$
 (9)

where  $\alpha/2$  is equal to the integral of the standard normal distribution function from  $Z_{\alpha/2}$  to  $\infty$  (Ref 25:276). It can then be said with probability  $(1 - \alpha)$  that if the absolute value of  $Z$ , from equation (6), is greater than or equal to  $Z_{\alpha/2}$  then  $H_0$  is not true.

The Runs Test. The Runs Test was used to identify steady state for simulation runs with unconstrained manpower. This test is a distribution

free statistical test which can be used to guard against nonrandomness in a time series. Such nonrandomness may be related to either trends or periodicities in the data. As noted earlier in this paper, one criteria for steady state in a simulation is randomness of the output data about some central value. To use the test, the time series is separated into observations above the mean and observations below the mean. A run is defined as a series of observations all above or all below the mean. Given the number of data points above the mean ( $N_1$ ), the number of points below the mean ( $N_2$ ), and the number of runs ( $R$ ); it is possible to compute the probability of observing  $R$  or fewer runs assuming the sequence is in fact random. These probabilities are commonly tabulated and can be used in testing various hypotheses (Ref 25:542-547).

Application of Runs Test in Determining Steady State. In using the Runs Test as an indicator of steady state, the authors aggregated the daily manhour totals by weeks. Too few runs, in a statistical sense, were taken as an indication of a trend in the data. The null and alternate hypotheses were defined as follows:

$H_0$ : There is no trend in the data--steady state is assumed to exist over the entire time series.

$H_a$ : There is a trend in the data--steady state does not exist over the entire time series.

The rejection region was defined to be  $R$  such that  $P(R) \leq .1$ . As with the Mann-Whitney Test, if  $H_0$  was rejected with the original data set, the data set was reduced until  $H_0$  was no longer rejected.

Type I and Type II Errors. When using any statistical test of hypothesis, the experimenter must be aware of the errors that can be made in accepting or rejecting  $H_0$ . The probability of rejecting  $H_0$  when  $H_0$  is in fact true is termed the Type I error and is denoted by  $\alpha$ . The authors chose the relatively large value of 0.1 for  $\alpha$ , so that the Type II error ( $\beta$ ), defined as the probability of accepting  $H_0$  when actually  $H_a$  is true, would not be too large. Mendenhall and Shaeffer note that as  $\alpha$  increases  $\beta$  will decrease (Ref 25:330). Even so, with the relatively small sample sizes involved in this study,  $\beta$  will be quite large. The authors, however, do not consider this serious since the intention is not to "prove" that the null hypothesis is true, but only to detect any significant deviation from that hypothesis.

#### Confidence Intervals

The mean value for manhours used, from the simulation output, is merely an estimate of the true mean for the system being modeled. The accuracy of this estimate is affected by the analyst's decision on when steady state exists, the number of data points used in the estimate ( $N$ ), and the variance of the sample data ( $S^2$ ). When considering the accuracy of such an estimate, the analyst is led to the consideration of statistical confidence intervals.

If the sample data is composed of independent random variables, the sample mean will possess a normal distribution for sample sizes larger than thirty (Ref 25:270). Then, the statistic

$$Z = \frac{(\bar{X} - \mu)}{\sqrt{S_{\bar{x}}^2}} \quad (10)$$

where  $\mu$  = the population mean

$\bar{X}$  = the sample mean

$S_{\mu}^2$  = the sample variance of the mean ( $\frac{S^2}{N}$ )

$S_{\mu}$  = the sample standard deviation of the mean ( $\sqrt{S_{\mu}^2}$ )

As before,  $Z$  is the standard normal random variable with zero mean and variance equal to one. From equation (10) can be constructed the following confidence interval:

$$\mu = \bar{X} \pm Z_{\alpha/2} S_{\mu} \quad (11)$$

where  $Z_{\alpha/2}$  is such that the integral of the standard normal density function from  $Z_{\alpha/2}$  to  $\infty$  is equal to  $\alpha/2$ . It can now be stated with probability  $(1 - \alpha)$  that the true population mean is contained in the interval given in equation (11) (Ref 25:276-277).

Autocorrelation. In many simulation models, the parameter values for separate observations are not independent; they are affected in some way by those values that precede them. For instance, in the LCOM model used in this study, high work loads on one day may carry over into the next day causing the man hours used on both days to be high. This type of dependence is called autocorrelation. The autocorrelation coefficient,  $\rho$ , where  $\rho$  is as defined by equation (12), is a measure of this dependency. If man hours used on any particular day is assumed to be normally distributed,  $\rho$  equal zero implies independence, and  $\rho$  equal one implies complete dependence (Ref 35:70).

$$\rho(L) = \frac{E((X_t - \bar{X})(X_{t+L} - \bar{X}))}{\sigma^2} \quad (12)$$

where  $E$  = expected value  
 $x_t$  = output value at time ( $t$ )  
 $\bar{x}$  = sample mean  
 $\sigma^2$  = population variance  
 $L$  = interval or lag between data points to be tested for dependence (Ref 10:194-199).

Given only a sample from the entire population, it is not possible to compute  $\rho(L)$ . However, an estimate,  $\hat{\rho}(L)$  is available as follows.

$$\hat{\rho}(L) = \frac{\sum_{t=1}^{N-L} (x_t - \bar{x})(x_{t+L} - \bar{x})}{\sum_{t=1}^N (x_t - \bar{x})^2} \quad (13)$$

Correcting for Autocorrelation. The procedure developed previously for constructing confidence intervals employed an estimate of the variance of the mean,  $S_\mu^2$ , based on an assumption of independence. If autocorrelation is present, then, the procedure for constructing confidence intervals must be modified.

One possibility is to examine  $\hat{\rho}(L)$ . If a value of  $(L)$  can be found such that  $\hat{\rho}(L) = 0$ , then the data can be combined or blocked into intervals of length  $(L)$ . The mean values for these blocks will now be independent, and as such can be used to construct confidence intervals as previously described (Ref 10:199-200).

A second possibility is to correct the variance of the mean ( $S_\mu^2$ ) by using the following relationship.

$$\text{Corrected } S_\mu^2 = S_\mu^2 [1 + 2 \sum_{L=1}^{N-1} \left(1 - \frac{L}{N}\right) \hat{\rho}(L)] \quad (14)$$

The reader should note that when  $\rho(L) = 0$ , the above reduces to the form used in the previous development of confidence intervals (Ref 10:199).

### Sensitivity Analysis

The Moody Regression Program, discussed in Chapter II, was used to develop a relationship between direct manning requirements and flying hours per month. A regression equation was developed for each AFSC with constrained manpower only, constrained manpower and parts, and constrained manpower, parts and ATS. These equations were then plotted to demonstrate the sensitivity of manning requirements, for each AFSC, to various sortie rates and parts/ATS constraints.

The primary inputs to the Regression Program consist of flying hours per month and final direct manning ( $M$  from equation (3)) rounded in accordance with AFM 25-5 (Ref 2:7-8). Manning for some LCOM shred-outs is combined under a single AFSC as shown in Appendix A. Further, direct manning for some LCOM shred-outs cannot be properly estimated using LCOM hours from the PSR. For instance, the End of Runway Crew requires very few LCOM hours in the model. In reality though, the positions must be manned during all flying operations. Direct manning in this case was estimated using the following relationship (Ref 3:2-4).

$$M = \frac{(\text{crew size})(\text{work days/wk})(\text{hrs/day})(4.348 \text{ wks/mo})}{144 \text{ hours/man/month}} \quad (15)$$

Direct manning for these LCOM shred-outs was combined under the appropriate AFSC in the Regression Program.

### Developing a Manning Document

The final step in obtaining an estimate of required manpower involves the use of the Moody Manpower Program. Up until this point only

direct manning has been discussed; that is, no consideration has been given to the fact that there is a requirement for supervisory and other overhead personnel in the maintenance organization being modeled. The Moody Manpower Program converts the results of the final simulation runs and the Moody Regression runs into a completed manning document, which reflects the total maintenance manning, by AFSC and work center, necessary to support the organization under study at a specified sortie rate and with specified constraints on parts/ATS.

In this study the authors used the Moody Manpower Program to develop estimates for total required manning, and also to demonstrate the sensitivity of total manning to parts/ATS constraints.

#### Summary

This chapter has included a discussion of the concepts and procedures used by the authors in accomplishing the objectives of this study. In the next chapter the authors demonstrate the methodology discussed here and present the results.

## V. ANALYSIS AND RESULTS

The analysis and results of the F-15 peacetime LCOM study are documented in this chapter. The analysis section investigates the simulation's steady state conditions and autocorrelation functions. The results section consists of maintenance manpower estimates for each AFSC listed in Table I of Chapter III, statistical confidence intervals for these estimates, manpower sensitivity to variations in spare parts and ATS, and a complete basic manning document for the modeled F-15 TFTW.

### Analysis

Simulation analysis consisted of graphical and statistical interpretation of accomplished aircraft sortie rate, AFSC manhours used, and AFSC autocorrelation coefficients. The authors used the procedures discussed in Chapter IV to analyze these variables. The simulation run length during this analysis consisted of 98 simulation days including weekends; this period is equivalent to 14 seven day weeks.

Steady State. The authors conducted steady state analysis on both unconstrained and constrained manpower simulations. During the unconstrained manpower simulations, PSR's were requested every seven days. The authors used daily PSR's for the constrained manpower simulations.

The authors chose a seven day data period for unconstrained manpower simulations due to a fundamental seven day cycle in the LCOM statistical output. This cycle was caused primarily by the peacetime operational scenarios; the five day flying and seven day maintenance schedule resulted in an appreciable decrease in manhours used for most AFSC's during the weekends. The accumulation of output data into seven day intervals smoothed this cyclic pattern and simplified the steady state

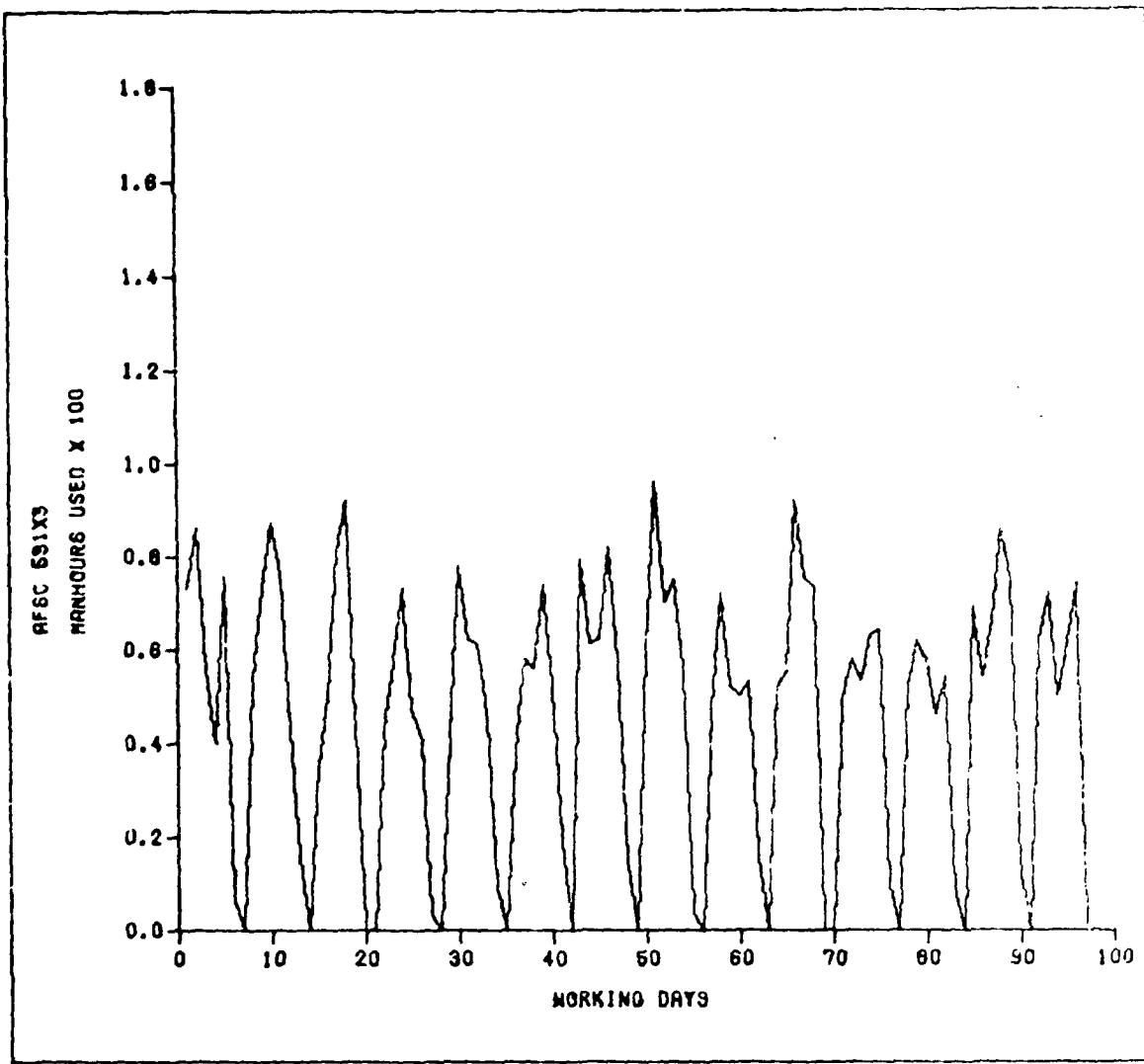


Figure 10. AFSC 531X3 (Structural Repair) Daily Manhours Used

analysis. For example, Figure 10 graphically depicts the daily manhours used for AFSC 531X3 (Structural Repair) over the 98 day simulation period based on unconstrained parts/ATS at a .74 scheduled sortie rate. The graph illustrates the seven day cyclic pattern caused by decreased manhours used during weekends. Figure 11 contains the weekly manhours used for the same AFSC with identical simulation conditions. The graph, in this case, clearly represents steady state conditions throughout the

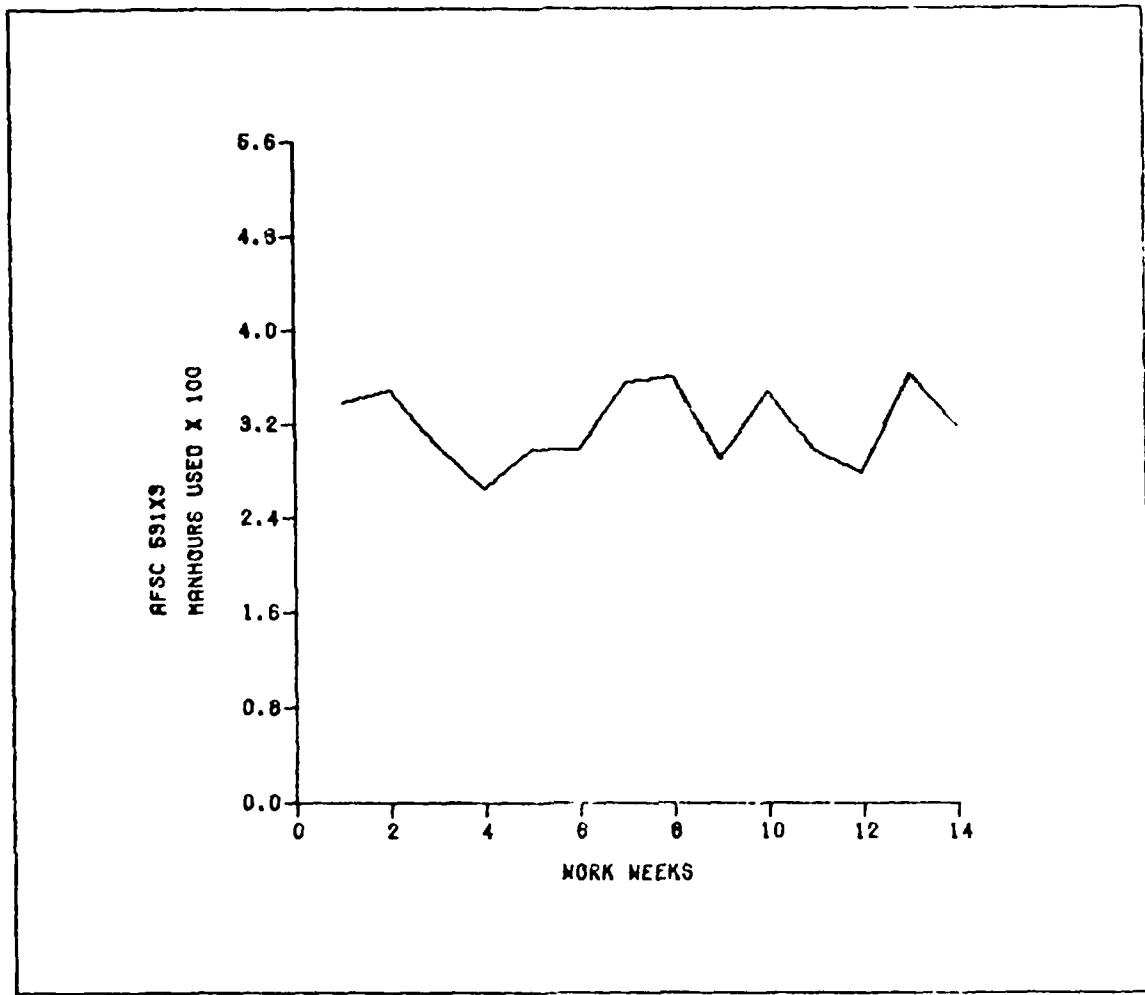


Figure 11. AFSC 531X3 (Structural Repair) Weekly Manhours Used

14 week period; additionally, the Runs test described in Chapter IV indicated no trends in this weekly data. All AFSC's except AFSC 423X3 (Fuel Systems) exhibited similar graphical and statistical steady state conditions throughout the 98 day unconstrained manpower simulations.

AFSC 423X3 was the only manpower statistic to exhibit nonsteady state conditions during the unconstrained manpower simulations. This AFSC exhibited an unstable condition during the constrained parts/ATS simulation at a .43 scheduled sortie rate. Figure 12 graphically

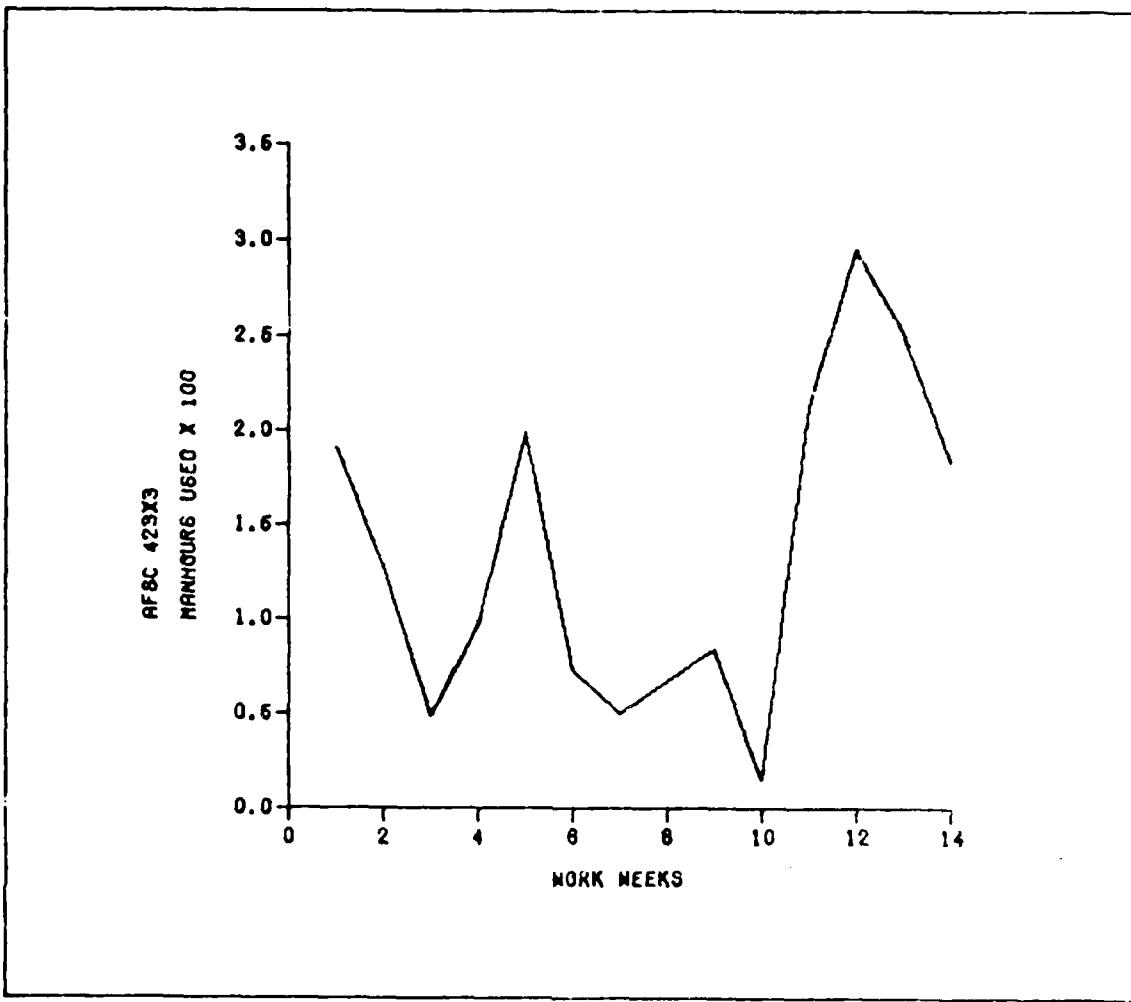


Figure 12. AFSC 423X3 (Fuel Systems) Weekly Manhours Used

illustrates this AFSC's instability in manhours used. The increase in manhours used during the eleventh through thirteenth weeks is especially noteworthy. This demand indicates a backlog of work during the latter portion of the simulation period. The authors, therefore, constrained manpower for this AFSC using the average daily manhours used during the eleventh through thirteenth weeks. This method of constraining manpower has two advantages: first, manpower is allocated to the constrained manpower simulation based on peak workloads as described by Tetmeyer (Ref 33:119); second, if peak workloads are not considered during the

manpower constraint process, the constrained manpower simulation's PSR will indicate manhour utilization for the AFSC in question greater than 60 percent and an additional constrained manpower simulation will be necessary to reduce this utilization below 60 percent.

Table III  
AFSC 531X3 Manpower Constraint Calculation

Source	Calculation
Equation (2)	$M_S = \frac{(0-98 \text{ Day PSR})}{(\text{Utilization Factor})(\text{Number of Days})(\text{Shift Length})}$ $= \frac{4445}{(.6)(98)(8)}$ $= 9.449 \approx 10 \text{ Men}$

Since all other AFSC's exhibited steady state conditions during the entire simulation period, the authors constrained manpower for these AFSC's using equation (2) from Chapter IV and the respective AFSC manhours used contained in the 0-98 day cumulative PSR. Table III illustrates the calculation of the manpower constraint for AFSC 531X3 (Structural Repair) using equation (2) and the respective manhours used in Figure C-1 of Appendix C. It should be noted that all manpower constraints are rounded to the next highest integer value during input to the main LCOM program.

During the constrained manpower simulations, the authors used a modified version of LCOM (Ref:19) which provided daily PSR's containing

only operations and personnel data. The elimination of shop repair and supply data from the PSR's appreciably reduced the amount of unneeded computer output during these simulations. Daily manhours used data was required in order to accurately compute the autocorrelation coefficients and statistical confidence intervals discussed later in the chapter; the daily data permits large sample size statistical analysis and increases the statistical confidence in the output data.

Figure 13 graphically illustrates the daily manhours used for AFSC 431X1 (Flight Line Crew Chief) for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. This graph indicates two major points: first, the seven day cycle of manhours used is very evident; second, the underlying steady state nature of the data throughout the 98 day simulation period is visible. Because steady state conditions are more difficult to detect in the daily manhours used data, the Mann-Whitney Test described in Chapter IV was used to verify output stability. The test indicated no statistical differences in the data contained in Figure 13.

All AFSC's except those listed in Table IV exhibited similar steady state conditions during the entire 98 day constrained manpower simulation period. For those AFSC's in Table IV, the Mann-Whitney test initially indicated instability in the data. The test was, therefore, reapplied to these AFSC's after eliminating the first seven days of data. In most cases, the reduced data set passed the test. In other cases, the first 14 days of data had to be eliminated before the reduced data set would pass the Mann-Whitney test. Table IV indicates each AFSC and its respective usable data sub-set. These data subsets were used to verify

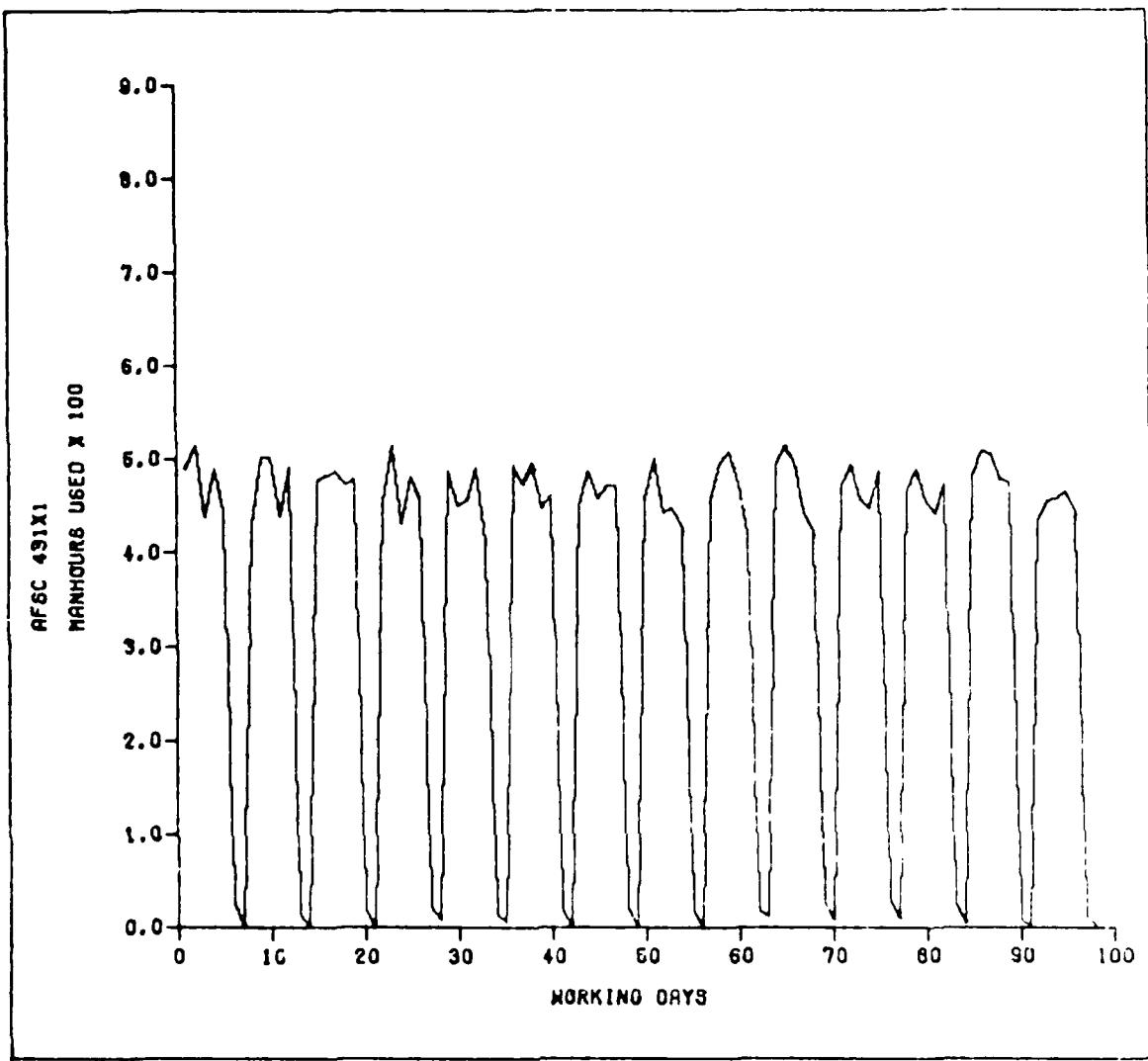


Figure 13. AFSC 431X1 (Flight Line Crew Chief) Daily Manhours used

manhour utilization, calculate manpower estimates, and compute confidence intervals for the AFSC's listed in Table IV.

The authors also analyzed accomplished aircraft sortie rate for the constrained manpower simulations. If this sortie rate exhibits steady state conditions, then the modeled F-15 TFTW can satisfy TAC training syllabi requirements on a routine basis.

Table IV  
LCOM AFSC's That Exhibited Initial Transient Conditions

Constraint Type	Scheduled Sortie Rate	AFSC	Usable Simulation Period
Unconstrained Parts/ATS	1.0	326X2A (COM/ NAV/ ECM)	Last 91 Days
Constrained Parts/ Unconstrained ATS	1.0	423X3 (Fuel Systems)	Last 84 Days
Constrained Parts/ Constrained ATS	1.0	326X1D (Automatic Test Station)	Last 91 Days
	1.0	326X2A (Inertial Navigation System)	Last 91 Days
	1.0	431X1 (Phase Inspection)	Last 91 Days
	.74	426X2 (Jet Engine)	Last 84 Days

Figure 14 depicts the accomplished aircraft sortie rate for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. The graph excludes weekends due to the undefined nature of sortie rate for nonflying days. In Figure 14, accomplished sortie rate exhibits a steady state condition throughout the 70 flying days. The Mann-Whitney test also verified steady state conditions in the data. Accomplished sortie rates

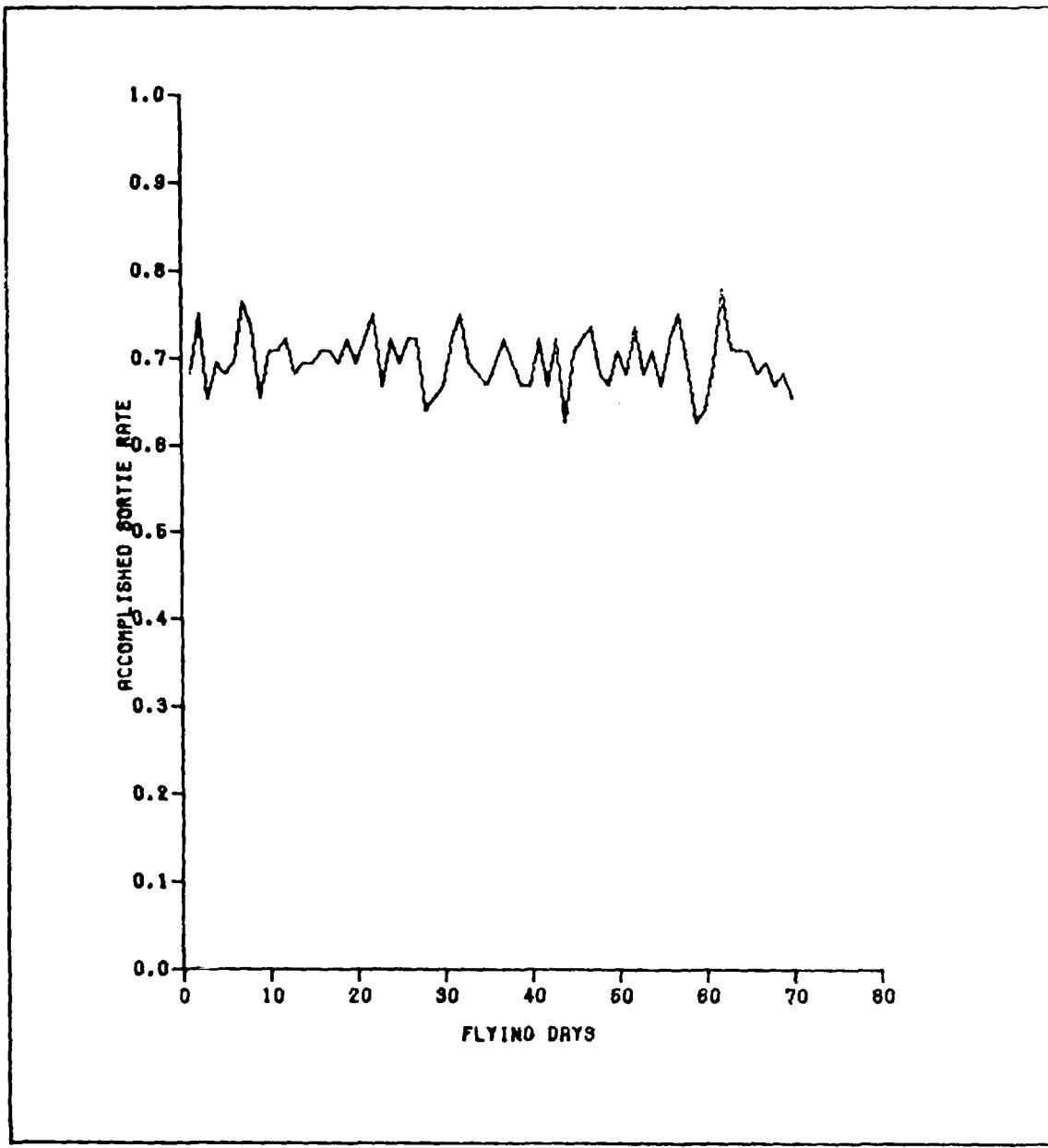


Figure 14. Accomplished Aircraft Sortie Rate for Constrained Manpower and Unconstrained Parts/ATS Simulation at .74 Scheduled Sortie Rate

for each of the nine combinations of parts/ATS constraints and scheduled sortie rates exhibited similar steady state conditions. These steady state conditions indicate that the modeled F-15 TFTW can routinely meet syllabi training requirements.

Autocorrelation. The authors conducted the autocorrelation analysis on the constrained manpower simulations. The autocorrelation coefficients ( $\hat{\rho}(L)$ ) were estimated for each AFSC using the respective manhours used and equation (13) found in Chapter IV; the lag (L) between daily observations was incremented to include a one through 97 day lag. For those AFSC's listed in Table IV,  $\hat{\rho}(L)$  was estimated for the corresponding reduced data sets. The analysis consisted of both graphical and statistical interpretation of the autocorrelation function.

Figure 15 graphically illustrates the autocorrelation function versus the lag in days for AFSC 431X1 (Flight Line Crew Chief) for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. This graph indicates two major points: first, the seven day cyclic nature of the function caused by the reduced manhour demands on weekends is clearly evident; second, multiple lags of seven days are highly correlated. The high correlation of manhours used on multiple seven day lags is due to the seven day cyclic nature of the simulation data. This functional form of autocorrelation coefficients prevents the grouping of manhours used into blocks of independent observations. The authors, therefore chose to use the estimated correlation coefficients and equation (14) to correct the variance of daily manhour observations during the computation of manpower statistical confidence intervals.

AFSC 423X3 (Fuel Systems) was the only AFSC to exhibit a more desirable autocorrelation function. The reason for this unique difference was that the fuel systems shop did not show a routine decrease in manhours used each weekend. This resulted in an absence of the seven day cycle. Figure 16 illustrates the graphical nature of the autocorrelation function for this AFSC. In the graph, lags of 15 or more days indicate

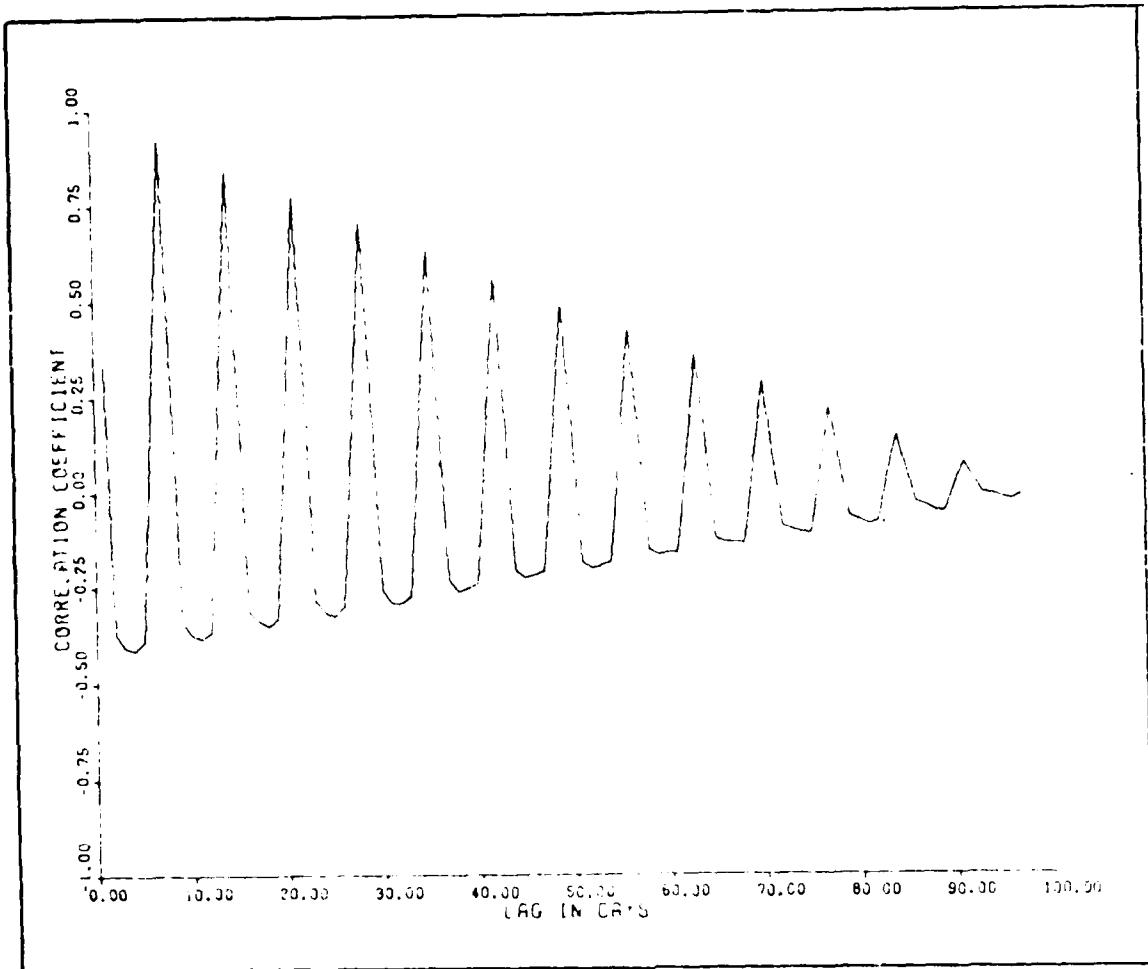


Figure 15. AFSC 431X1 (Flight Line Crew Chief) Autocorrelation Function

a  $\hat{\rho}(L)$  close to zero. As a result, manhours used contained on cumulative 15 day PSR's would be statistically independent and could be treated as independent observations during the calculation of statistical confidence intervals. The type of autocorrelation function illustrated in Figure 16 is often found in an LCOM simulation where maintenance and flying activity operate concurrently. Concurrent maintenance and flying activity do not produce the cyclic output data that is found in this study. In particular, wartime LCOM simulations contain the functional form illustrated in Figure 16.

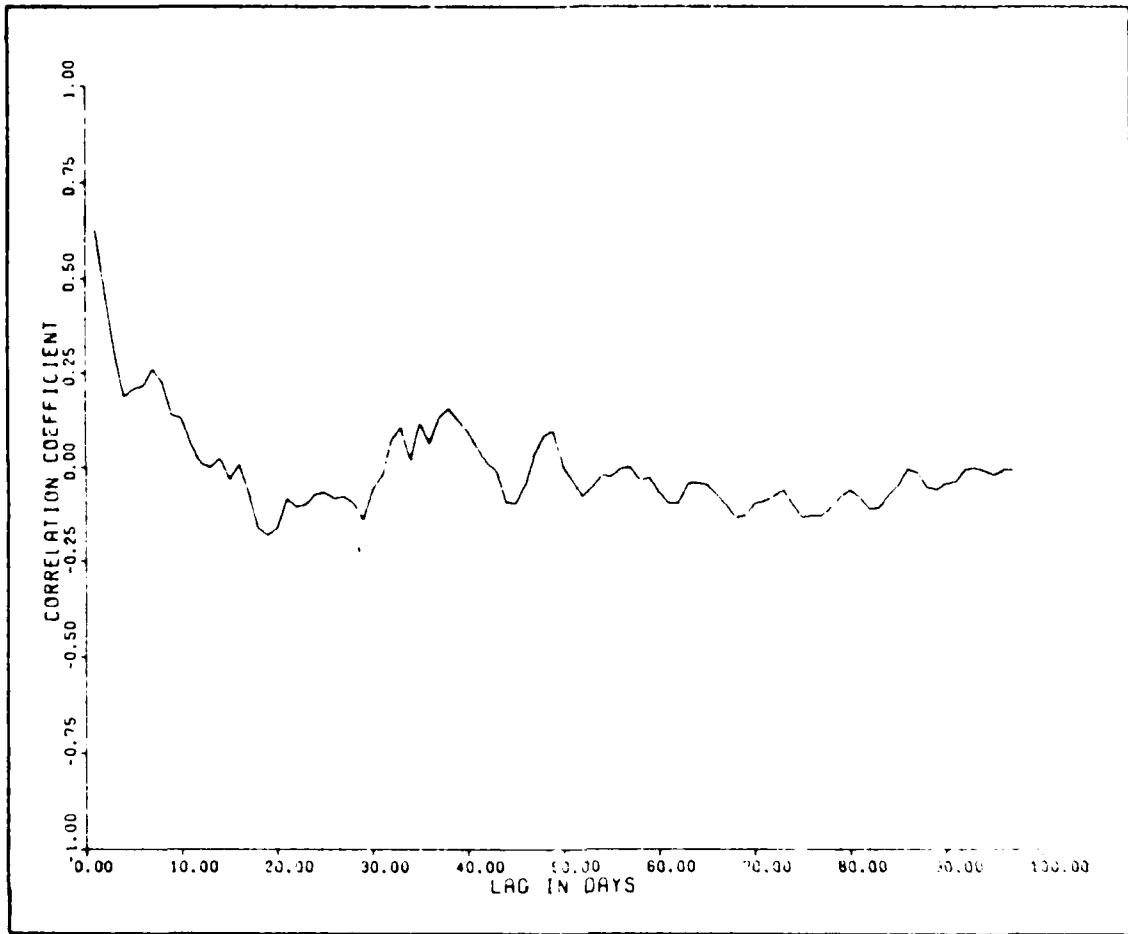


Figure 16. AFSC 423X3 (Fuel Systems) Autocorrelation Function

Because the majority of AFSC's in this study exhibited autocorrelation functions similar to Figure 15, the variance of daily manhours used for each AFSC including AFSC 423X3 was corrected using equation (13). These corrected variances were used during calculation of the manpower confidence intervals.

#### Results

The results of the F-15 TFTW LCOM simulation contain the direct manning estimations ( $M$ ) for each AFSC contained in Table I of Chapter III,

95 percent confidence intervals for these estimates, and sensitivity of M to constrained parts and constrained parts/ATS. The final output of these estimates is a USAF basic manning document for the F-15 TFTW based on unconstrained parts and ATS.

Direct Manning. The average daily manhours used from the final constrained manpower simulations are applied to equations (1) and (2) from Chapter IV to calculate the direct manning for each AFSC listed in Table I. Direct Manning is then converted to whole men according to AFM 25-5 standards (Ref 2:Chap. 6, p. 29). During the calculation of M, the AFM 25-5 standard of 30.44 work days per month is applied to equation (2). Table V illustrates the computation of direct manning for AFSC 531X3 (Structural Repair) for the unconstrained parts/ATS simulation at .74 scheduled sortie rate.

Table V  
AFSC 531X3 Direct Manning Computation

Source	Calculation
Equation (1)	$M_S = \frac{\text{Average Daily Manhours Used}}{(\text{Utilization Factor})(\text{Shift Length})}$ $= \frac{(40.44)}{(.6)(8)}$ $= 8.425$
Equation (2)	$M = \frac{M_S (\text{Workdays}/\text{Mo})(\text{Shift Length})}{144 \text{ Hours/Man/Month}}$ $= \frac{(8.425)(30.44)(8)}{144}$ $= 14.248$
AFM 25-5	Direct Manning = 14 Men

Confidence Intervals. Confidence intervals for direct manning are computed using equations (1), (2), (11), and (14) found in Chapter IV. The computation is a six step process: first, estimate the sample variance of daily manhours used (Ref 25:268); second, use equation (14) to calculate the corrected sample variance of daily manhours used; third, convert the corrected sample variance into a standard deviation of daily manhours used; fourth use equations (1) and (2) to transform the standard deviation of daily manhours used into a direct manning standard deviation; fifth, use equation (11) to develop 95 percent confidence intervals for direct manning; finally, convert the confidence intervals into integer values in accordance with AFM 25-5 (Ref 2: Chap. 6, p. 29).

Table VI illustrates the computation of a 95 percent confidence interval for the direct manning of AFSC 531X3 based on unconstrained parts/ATS at a .74 scheduled sortie rate. In these calculations, N equals the number of steady state days simulated. In all cases, except those AFSC's listed in Table IV, N equals 98.

The procedures contained in Tables V and VI were used to compute each AFSC's direct manning and confidence intervals for the three constraint types (unconstrained parts/ATS, constrained parts/unconstrained ATS, and constrained parts/ATS) and scheduled sortie rates (.43, .74, and 1.0). The direct manning for the End of Runway Crew was separately calculated using equation (15) found in Chapter IV and added to the direct manning estimate and confidence interval of AFSC 431X1 (Flight Line Crew Chief). This calculation is illustrated in Table VII.

Table VI  
AFSC 531X3 Confidence Interval Computation

Source	Calculation
Sample Variance of Daily Manhours Used	$S_{\mu}^2 = 5.526$
Equation (14)	$\begin{aligned} \text{Corrected } S_{\mu}^2 &= S_{\mu}^2 [1 + 2 \sum_{L=1}^{N-1} (1 - \frac{L}{N}) \hat{\rho}(L)] \\ &= 5.256 [1 + 2 \sum_{L=1}^{97} (1 - \frac{L}{98}) \hat{\rho}(L)] \\ &= .507 \end{aligned}$
Convert Variance to Standard Deviation	$\begin{aligned} \text{Average Daily Manhours Used} &= \sqrt{.507} \\ \text{Standard Deviation} &= .712 \end{aligned}$
Equation (1)	$\begin{aligned} M_S \text{ Standard Deviation} &= \frac{\text{Average Daily Manhours Used Standard Deviation}}{\text{Utilization Factor} \times \text{Shift Length}} \\ &= \frac{(.712)}{(.6)(8)} \\ &= .148 \end{aligned}$
Equation (2)	$\begin{aligned} M \text{ Standard Deviation} &= \frac{(M_S \text{ Standard Deviation})(\text{Work Days/Mo})(\text{Shift Length})}{(144 \text{ Hours/Man/Month})} \\ &= \frac{(.148)(30.44)(8)}{144} \\ &= .250 \end{aligned}$

Table VI. (Continued)  
AFSC 531X3 Confidence Interval Computation

Source	Calculation
Equation (11)	$\begin{aligned} \text{95% Confidence Interval} &= M \pm (Z_{\alpha/2}) \left( \frac{\text{M Standard Deviation}}{\sqrt{N}} \right) \\ &= 14.248 \pm (1.96)(.250) \\ &= 14.248 \pm .49 \\ &= (13.758, 14.738) \end{aligned}$
AFM 25-5	$\begin{aligned} \text{95% Confidence Interval for } M &= (13, 14) \text{ Men} \end{aligned}$

Table VII  
End of Runway Crew Direct Manning Computation

Source	Computation
Equation (15)	$\begin{aligned} M &= \frac{(\text{Crew Size})(\text{Workdays per Month})}{144 \text{ Hours/Man/Month}} (\text{Hours per Day})(\text{4.348 Weeks per Month}) \\ &= \frac{(3)(5)(16)(4.348)}{144} \\ &= 7.25 \end{aligned}$
AFM 25-5	Direct Manning = 7 Men

Direct Manning Sensitivity. This section illustrates both graphically and statistically the sensitivity of direct manning estimates to each of the three simulation constraint types and scheduled sortie rates. The authors used the Moody Regression Program to develop a regression equation for each constraint type comparing AFSC direct manning with flying hours per month (FHPM). The accomplished sortie rate (ASR) corresponding to the simulation's scheduled sortie rate was converted into FHPM for the purpose of this comparison. Table VIII depicts the resulting ASR and FHPM for the three constraint types and scheduled sortie rates.

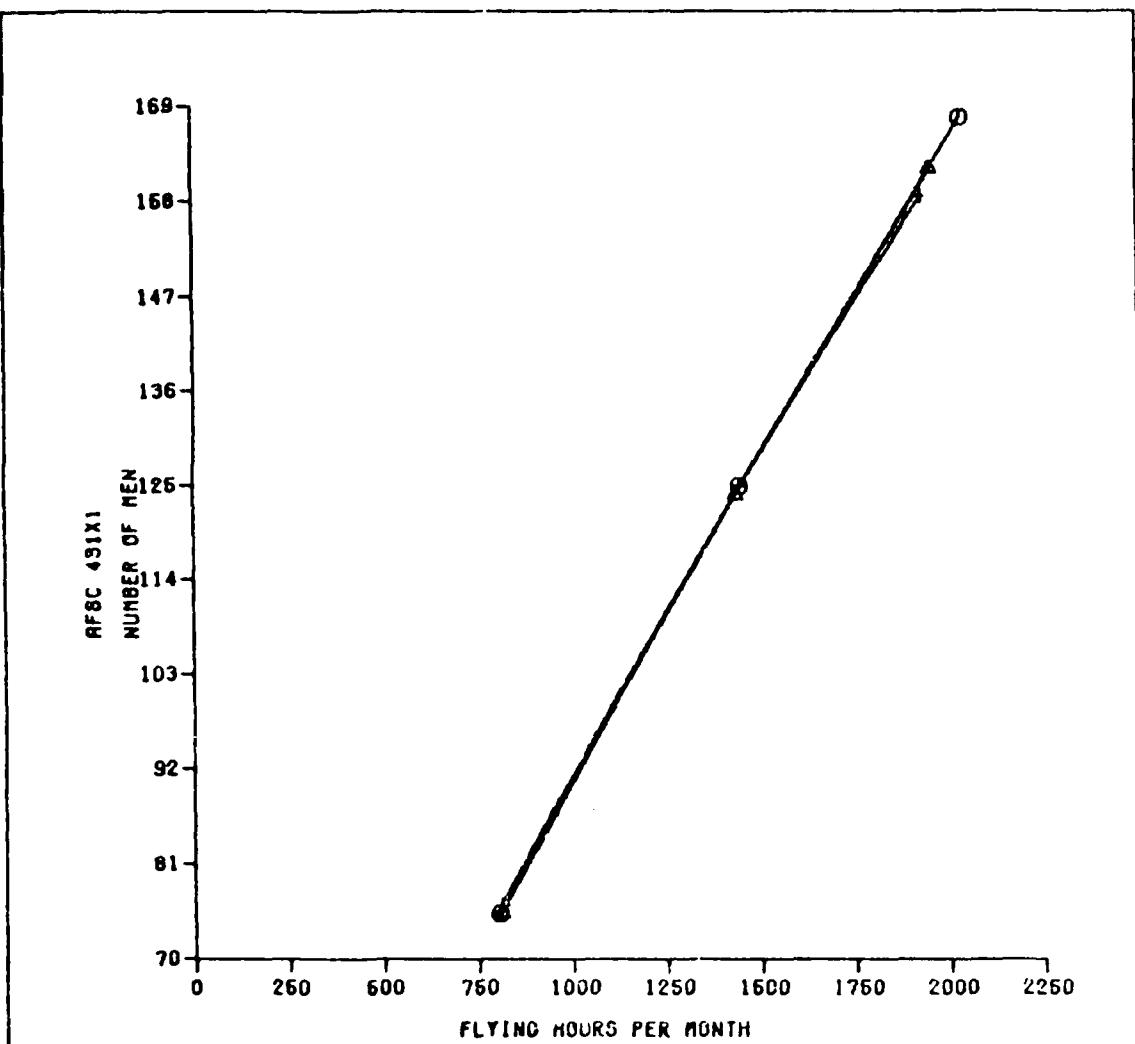
Table VIII

Accomplished Sortie Rate (ASR) and Flying Hours per Month (FHPM) versus Constraint Type and Scheduled Sortie Rate

Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
Unconstrained Parts/ Unconstrained ATS	.404 ASR 806 FHPM	.697 ASR 1444 FHPM	.955 ASR 2037 FHPM
Constrained Parts/ Unconstrained ATS	.406 ASR 809 FHPM	.692 ASR 1433 FHPM	.916 ASR 1954 FHPM
Constrained Parts/ Constrained ATS	.406 ASR 808 FHPM	.698 ASR 1446 FHPM	.904 ASR 1930 FHPM

Figures 17 through 30 depict the direct manning for those AFSC's listed in Table I. These figures use the Moody Regression equations to graphically illustrate the sensitivity of direct manning to constraint type and flying hours per month. The figures also depict in tabular form the direct manning and 95 percent confidence intervals corresponding to each constraint type and scheduled sortie rate.

Table VIII and Figures 17 through 30 summarize the relationships between scheduled sortie rate, flying hours per month, accomplished sortie rate, and direct manning. For example, AFSC 431X1 (Flight Line Crew Chief) in Figure 17 requires 76 direct men with a 95 percent confidence interval of (74-78) to achieve 806 FHPM and a .404 ASR based on unconstrained parts/ATS and a .43 scheduled sortie rate.



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	76 (74-78)	124 (120-128)	168 (163-172)
△ - Constrained Parts/ Unconstrained ATS	76 (74-79)	123 (119-127)	162 (157-167)
+ - Constrained Parts/ Constrained ATS	77 (75-79)	124 (119-128)	159 (149-169)

Figure 17. AFSC 431X1 (Flight Line Crew Chief) Direct Manning

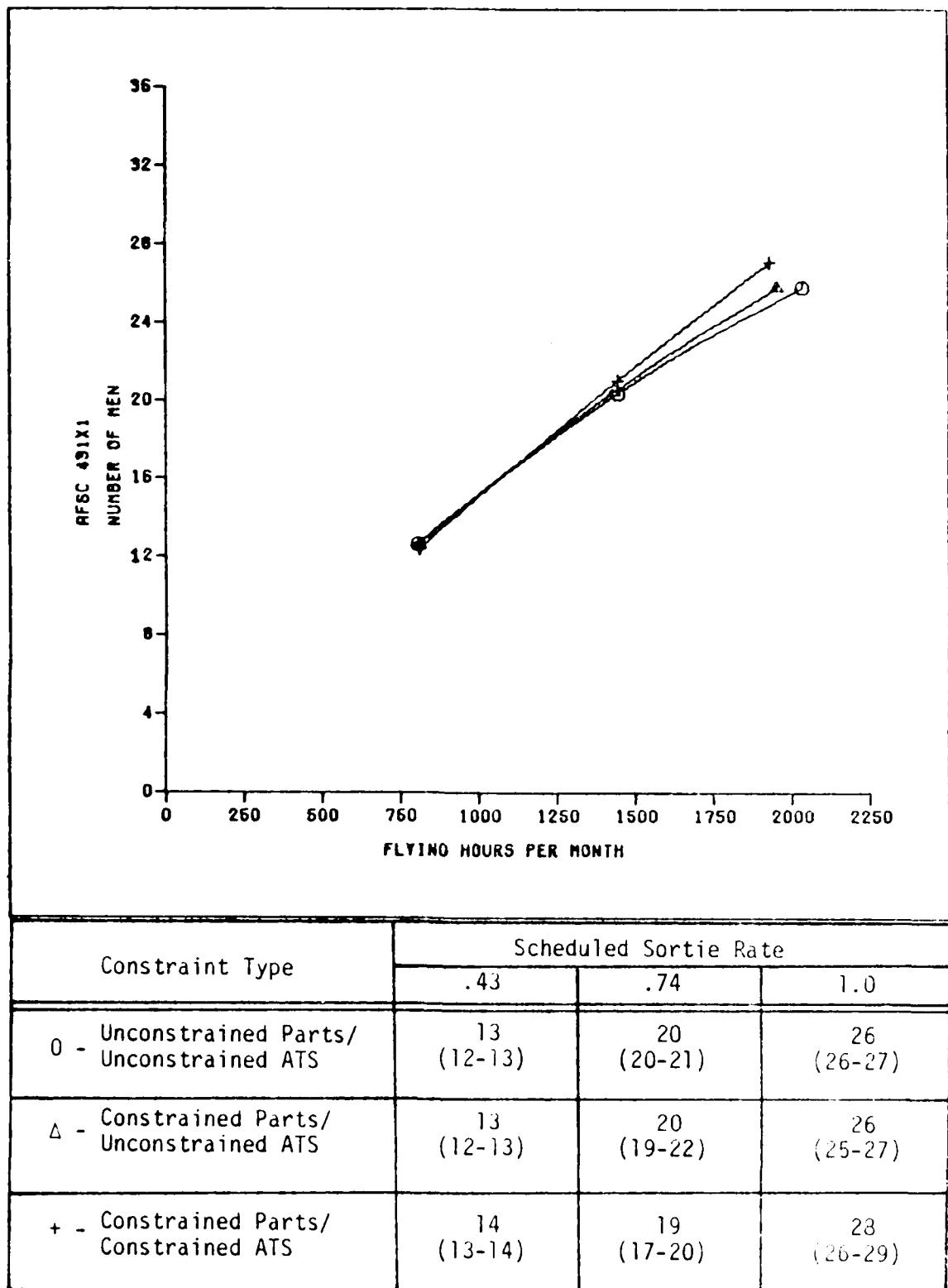
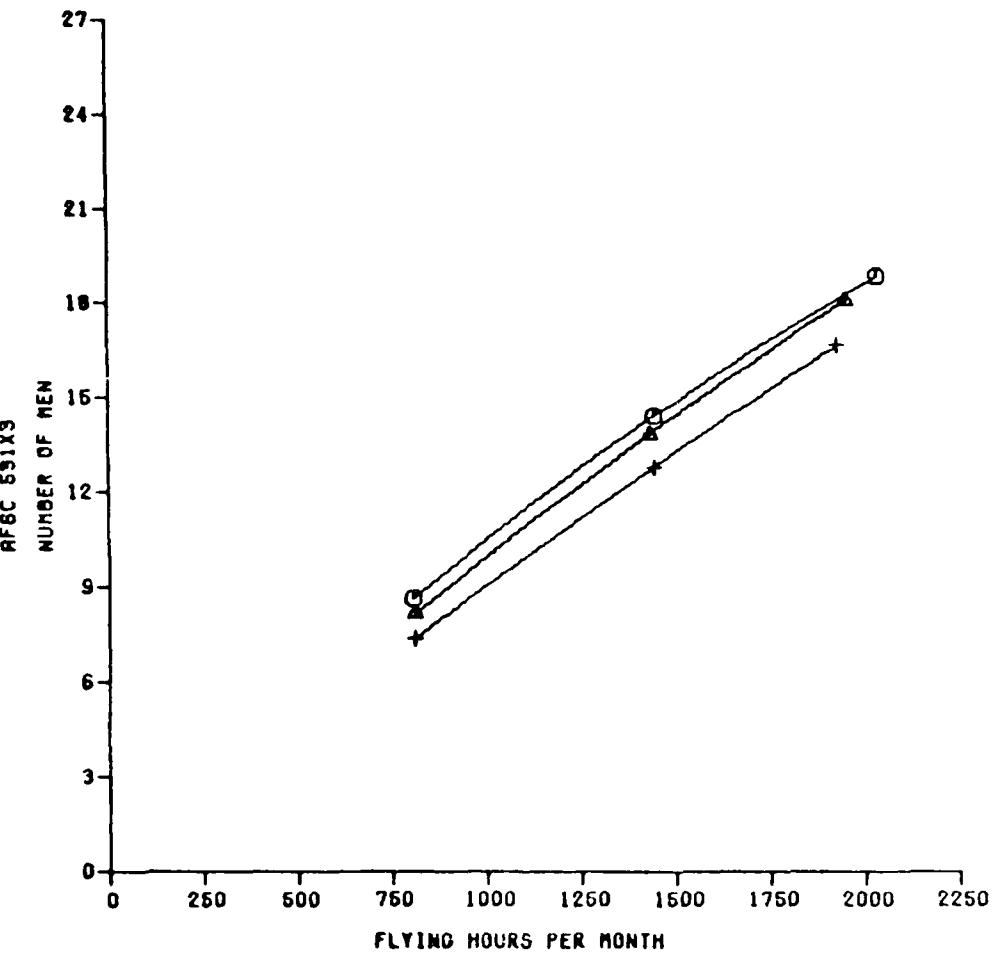
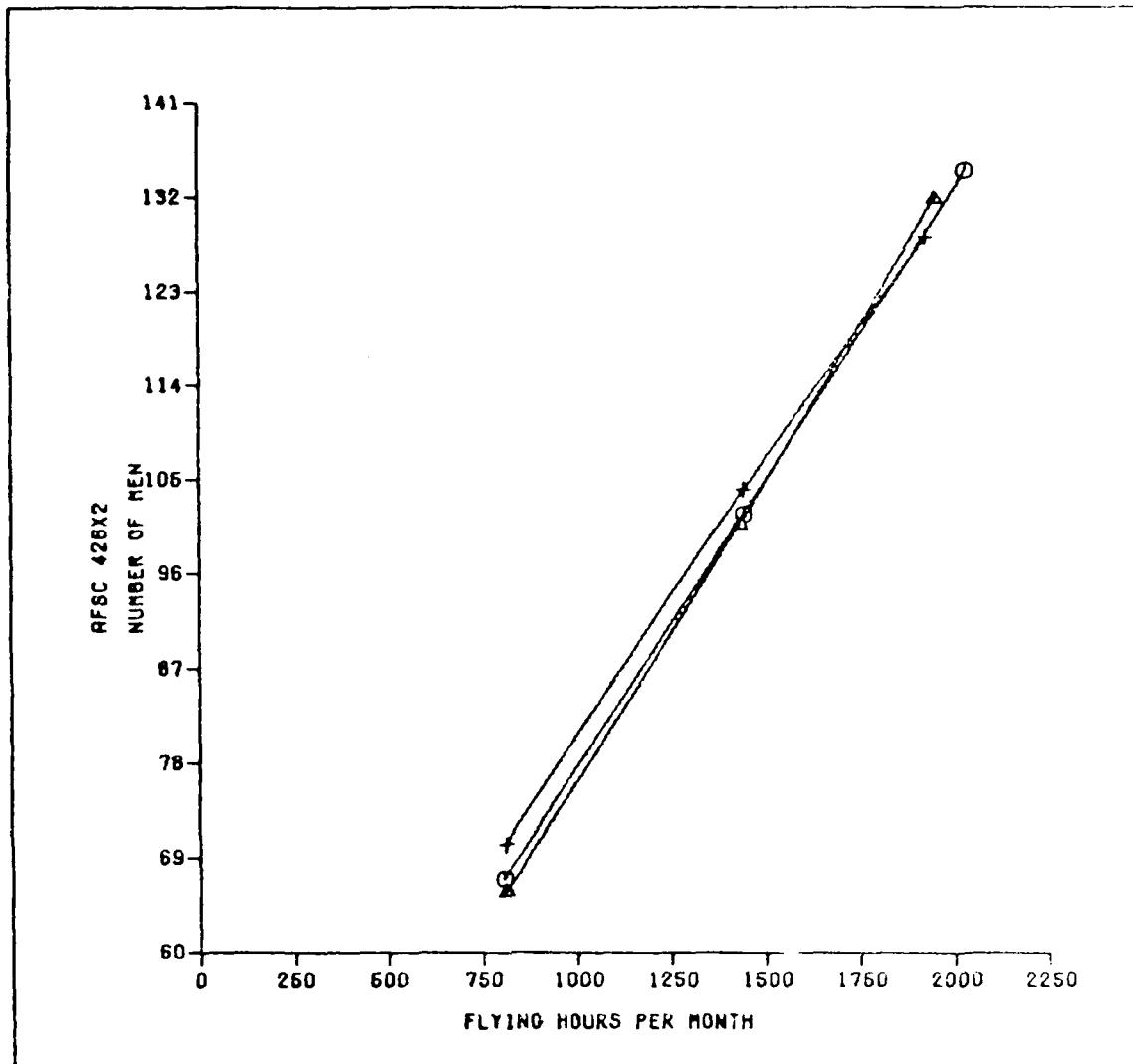


Figure 18. AFSC 431X1 (Phase Inspection) Direct Manning



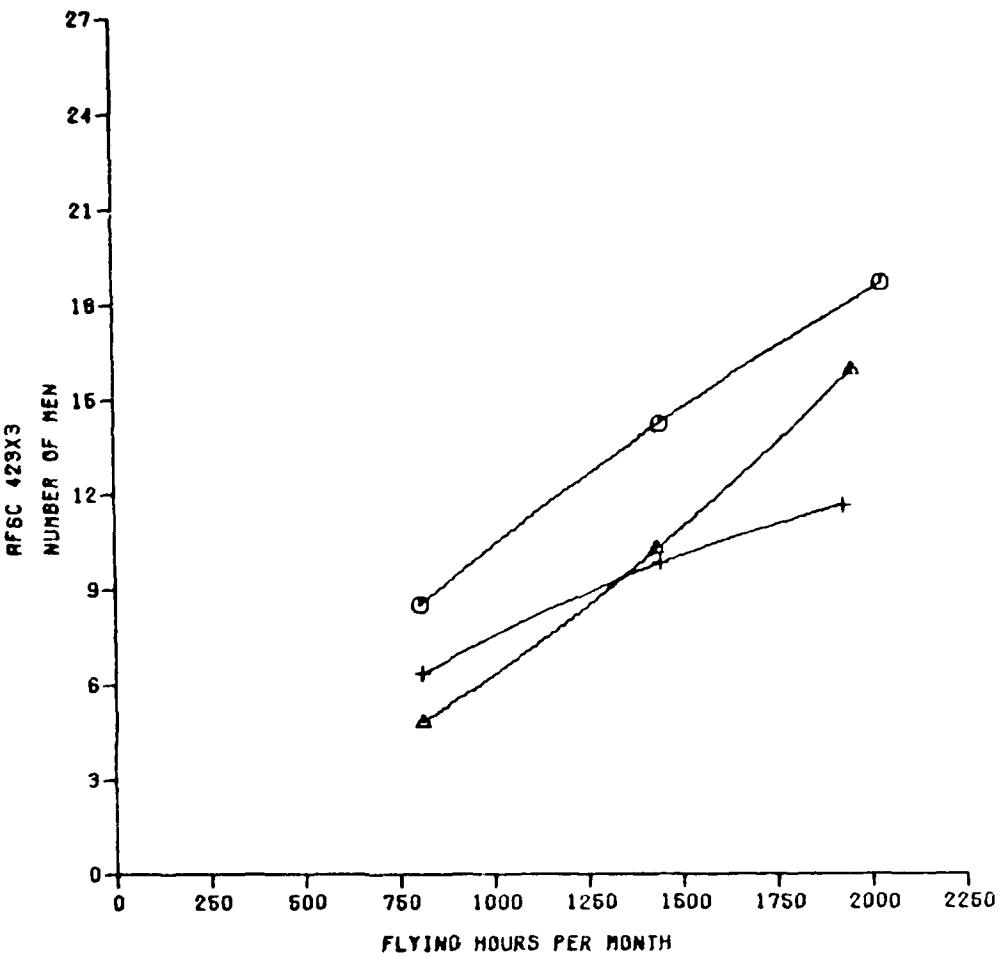
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	9 (8-9)	14 (13-14)	19 (18-20)
△ - Constrained Parts/ Unconstrained ATS	8 (8-9)	14 (13-14)	18 (17-19)
+ - Constrained Parts/ Constrained ATS	8 (8-9)	12 (12-13)	17 (16-19)

Figure 19. AFSC 531X3 (Structural Repair) Direct Manning



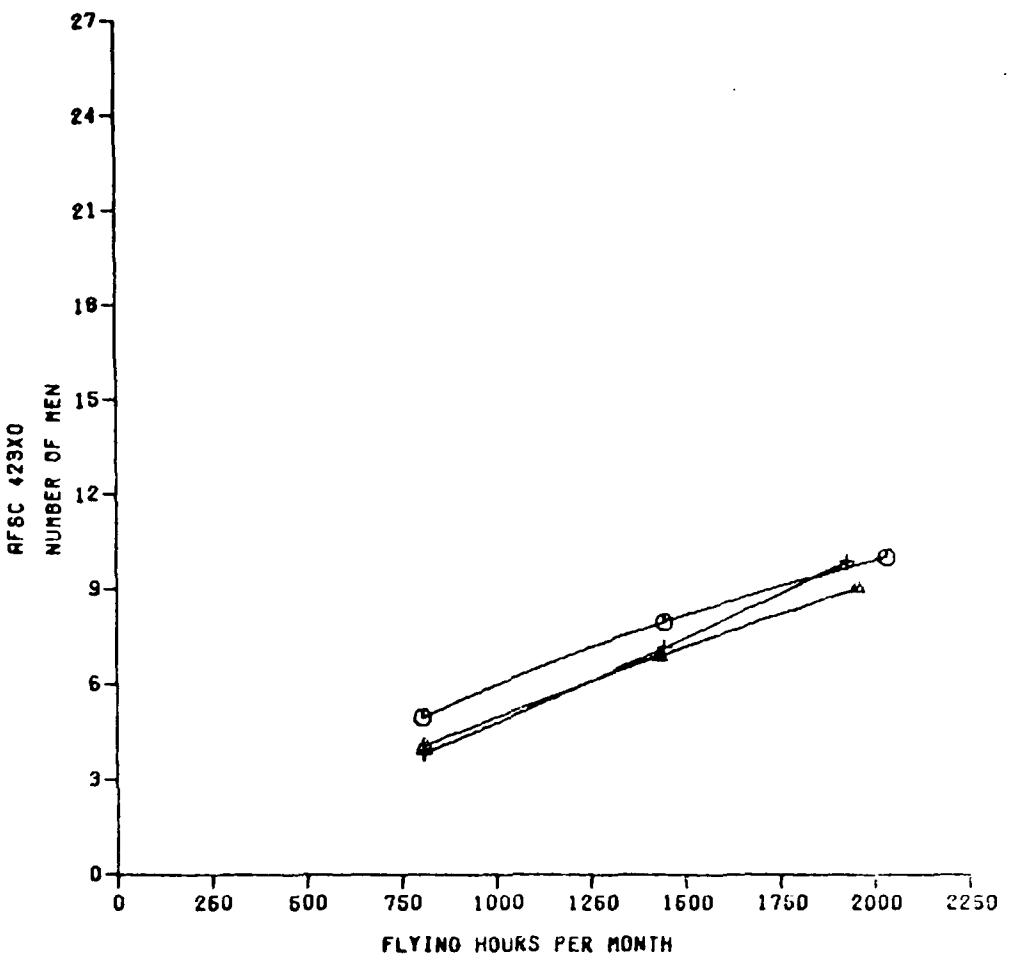
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	66 (64-68)	103 (94-112)	134 (120-142)
△ - Constrained Parts/ Unconstrained ATS	68 (65-70)	90 (82-107)	133 (128-139)
+ - Constrained Parts/ Constrained ATS	68 (65-72)	107 (101-112)	137 (127-147)

Figure 20. AFSC 426X2 (Jet Engine) Direct Training



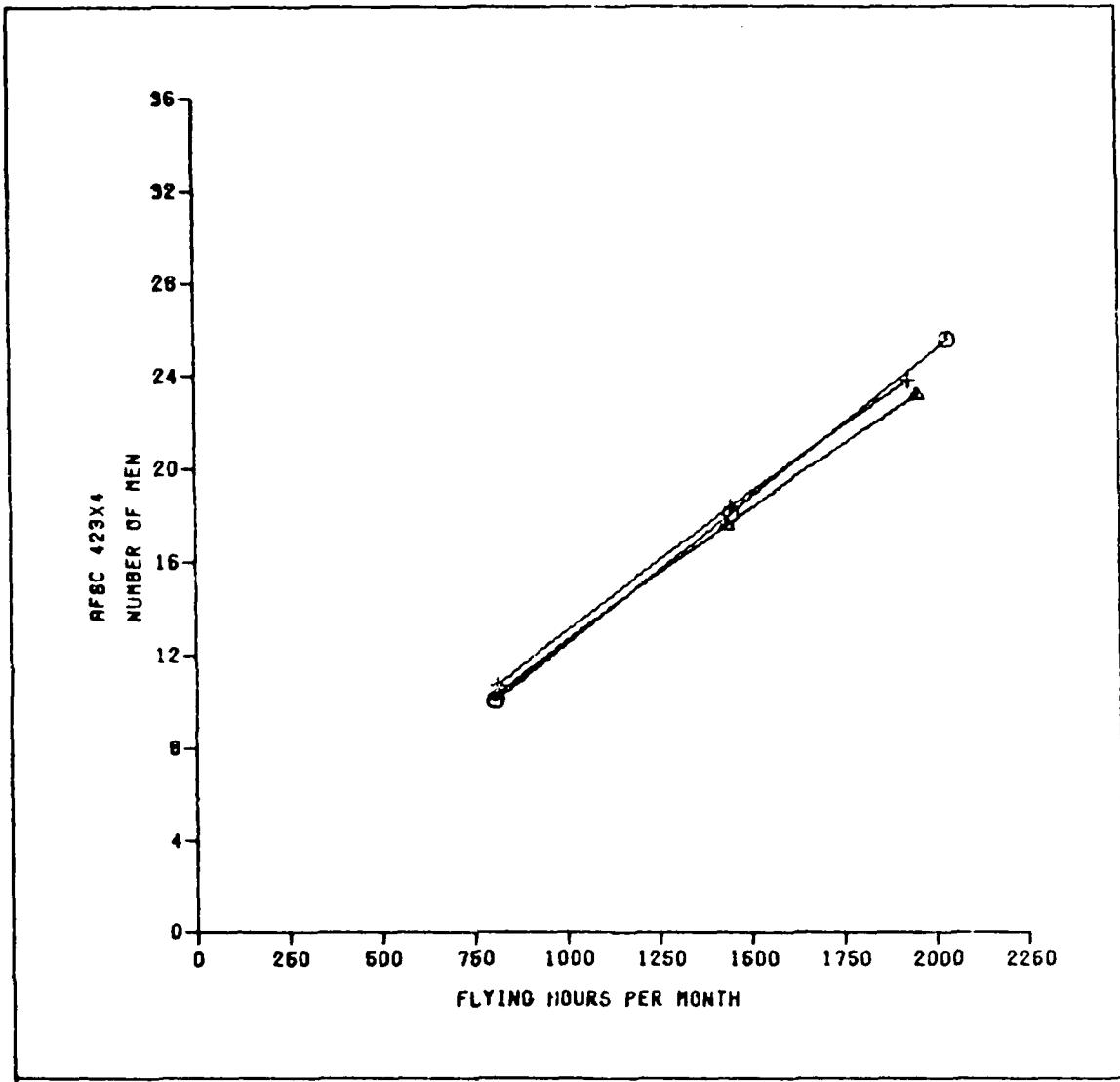
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
○ - Unconstrained Parts/ Unconstrained ATS	7 (5-9)	16 (14-17)	18 (16-19)
△ - Constrained Parts/ Unconstrained ATS	5 (5-6)	10 (10-11)	16 (15-18)
+ - Constrained Parts/ Constrained ATS	7 (6-8)	9 (8-9)	12 (11-13)

Figure 21. AFSC 423X3 (Fuel Systems) Direct Manning



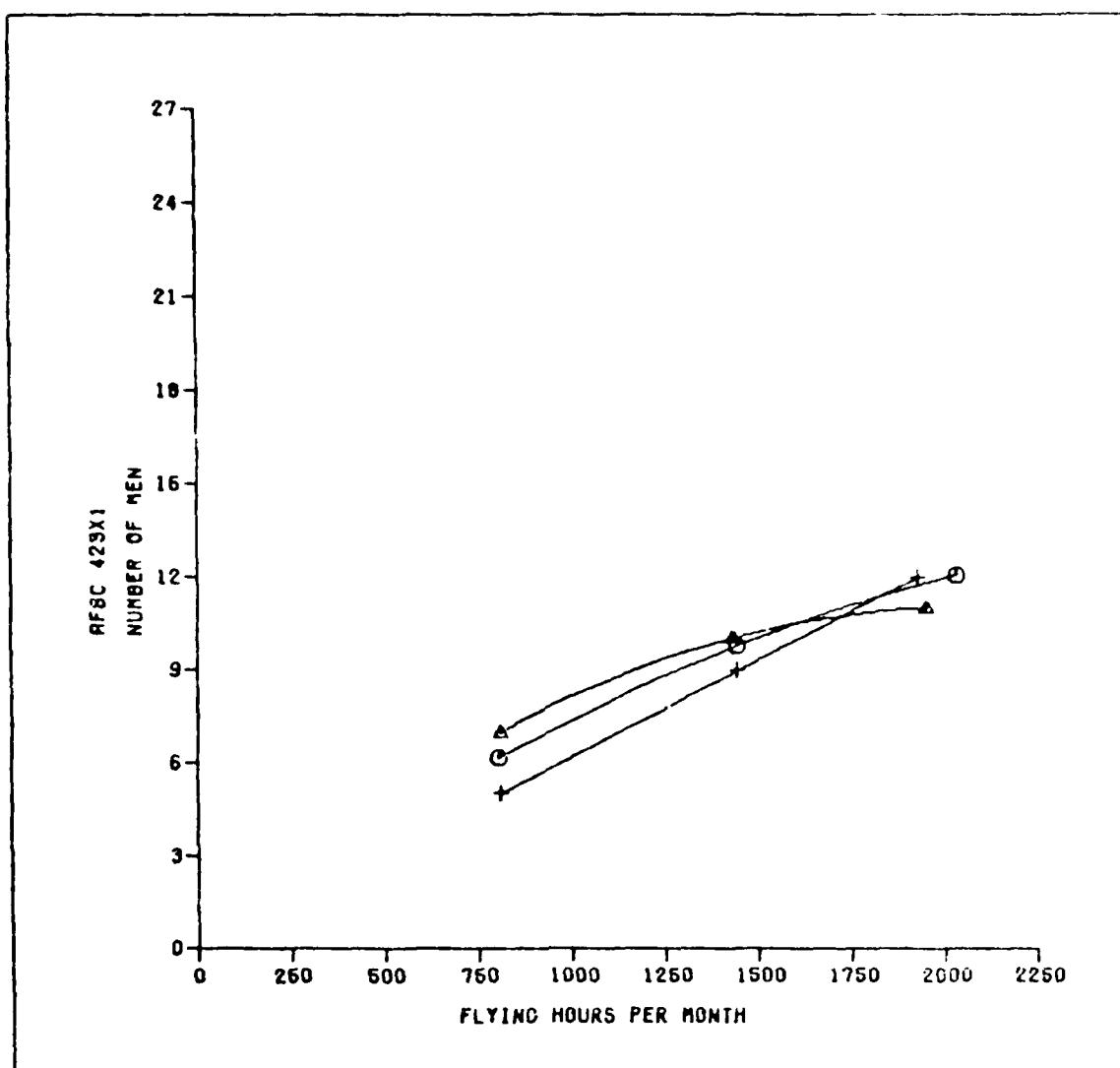
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	5 (5-5)	8 (7-8)	10 (9-10)
△ - Constrained Parts/ Unconstrained ATS	4 (4-5)	7 (6-7)	9 (9-10)
+ - Constrained Parts/ Constrained ATS	4 (4-4)	7 (7-7)	10 (9-10)

Figure 22. AFSC 423X0 (Electrical Systems) Direct Manning



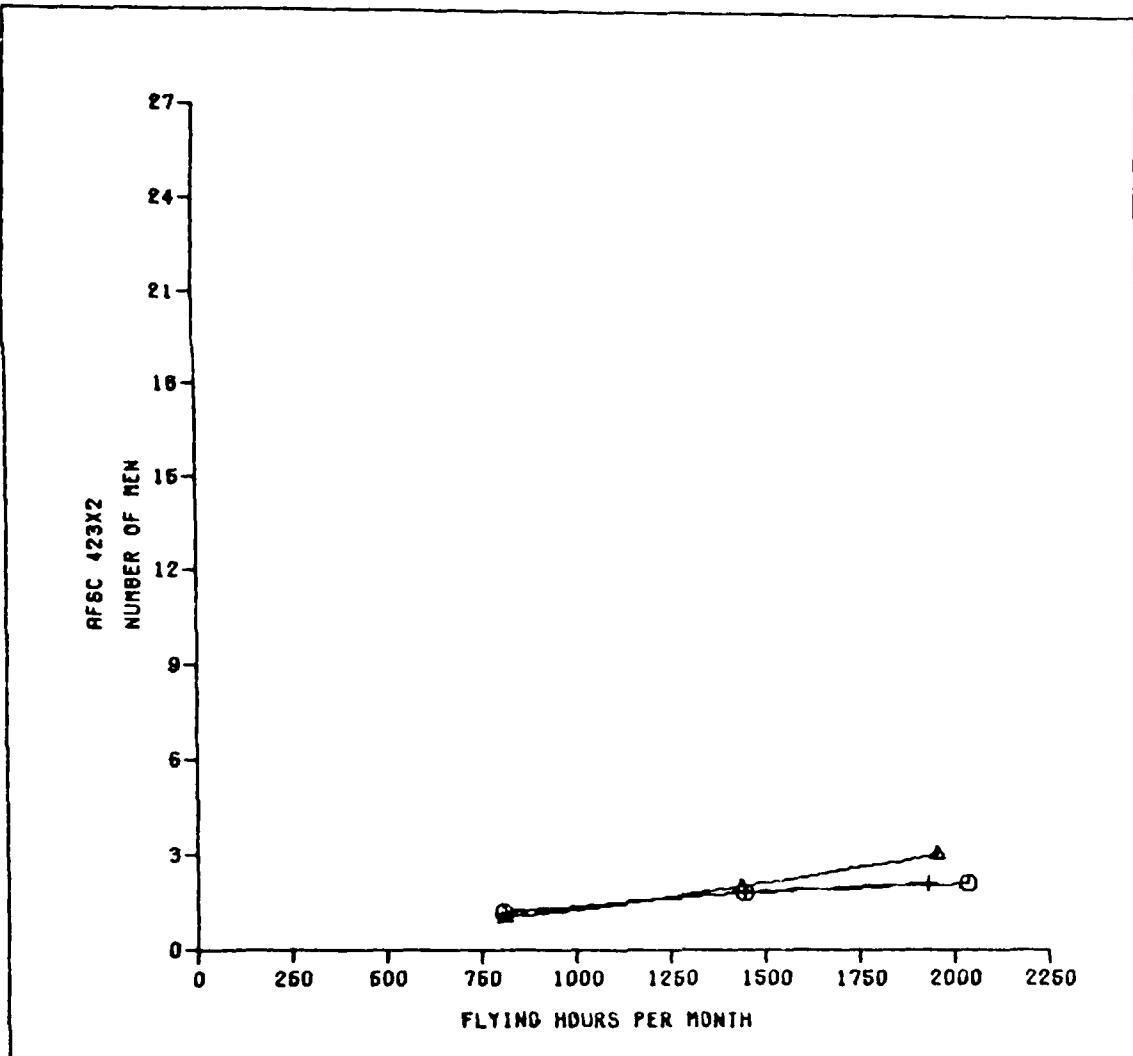
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	11 (10-11)	17 (16-19)	26 (25-27)
△ - Constrained Parts/ Unconstrained ATS	10 (9-11)	18 (17-19)	23 (22-24)
+ - Constrained Parts/ Constrained ATS	11 (10-11)	18 (18-19)	24 (22-25)

Figure 23. AFSC 423X4 (Pneudraulics) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
○ - Unconstrained Parts/ Unconstrained ATS	6 (5-6)	10 (9-10)	12 (12-13)
△ - Constrained Parts/ Unconstrained ATS	7 (7-7)	10 (9-11)	11 (10-11)
+ - Constrained Parts/ Constrained ATS	5 (5-5)	9 (9-9)	12 (11-13)

Figure 24. AFSC 423X1 (Environmental Systems) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	1 (1-2)	2 (2-2)	2 (2-3)
Δ - Constrained Parts/ Unconstrained ATS	1 (1-1)	2 (2-2)	3 (2-3)
+ - Constrained Parts/ Constrained ATS	1 (1-2)	2 (1-2)	2 (2-3)

Figure 25. AFSC 423X2 (Egress Systems) Direct Manning

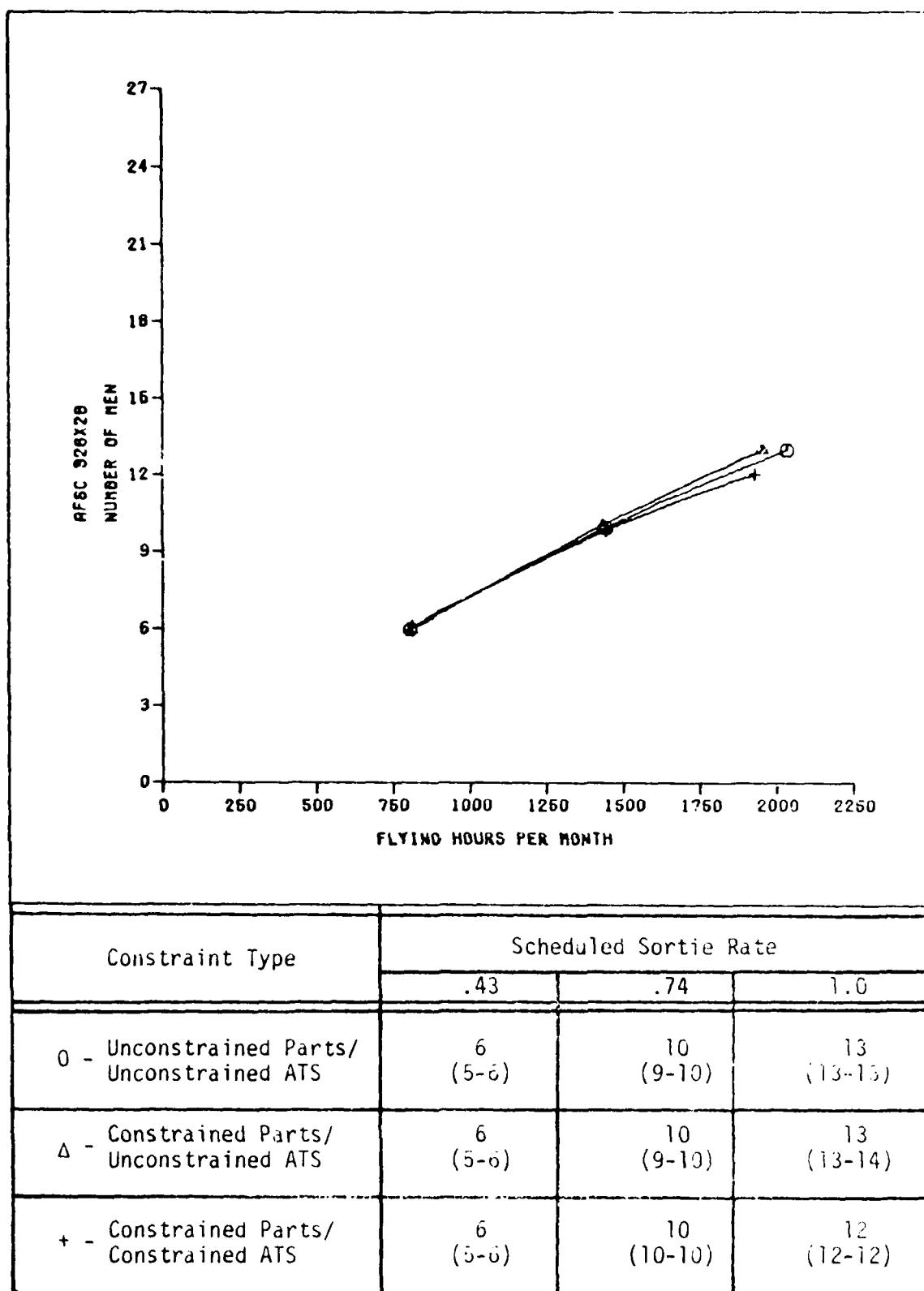
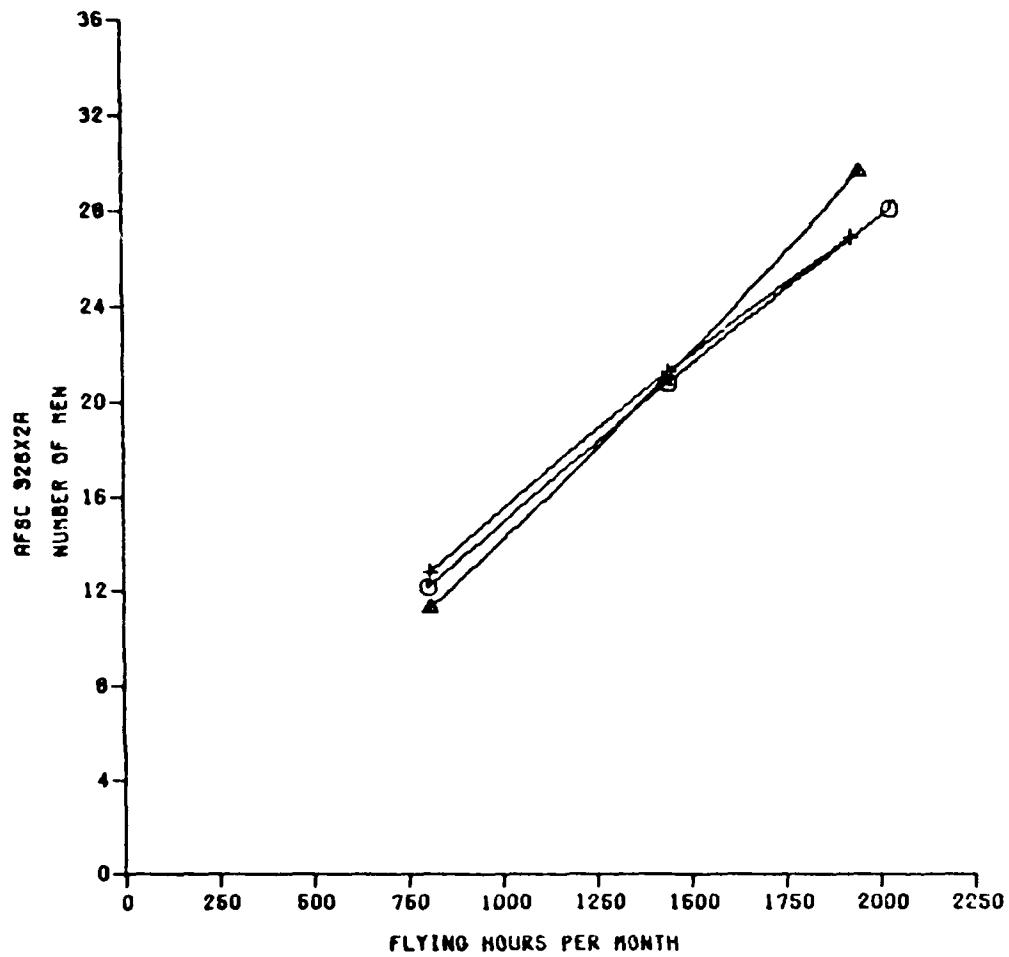
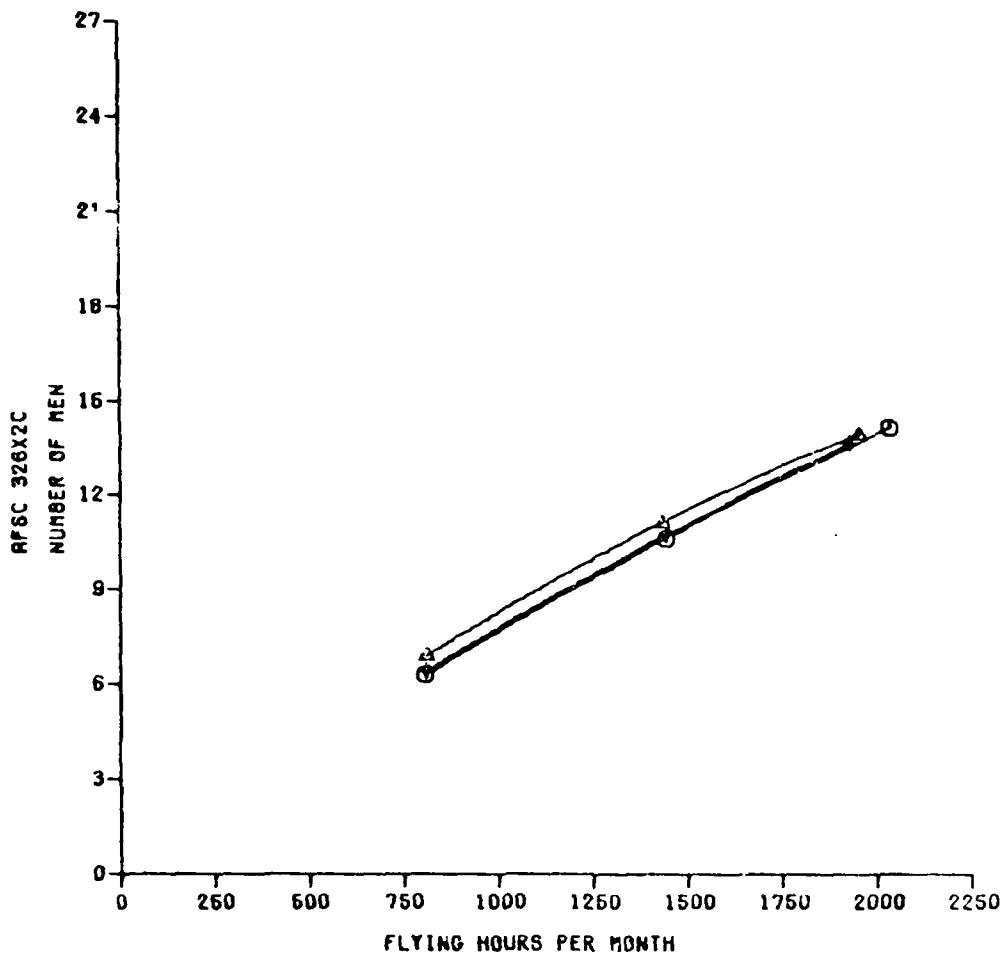


Figure 26. AFSC 326X2B (Automatic Flight Control/Instrument) Direct Manning



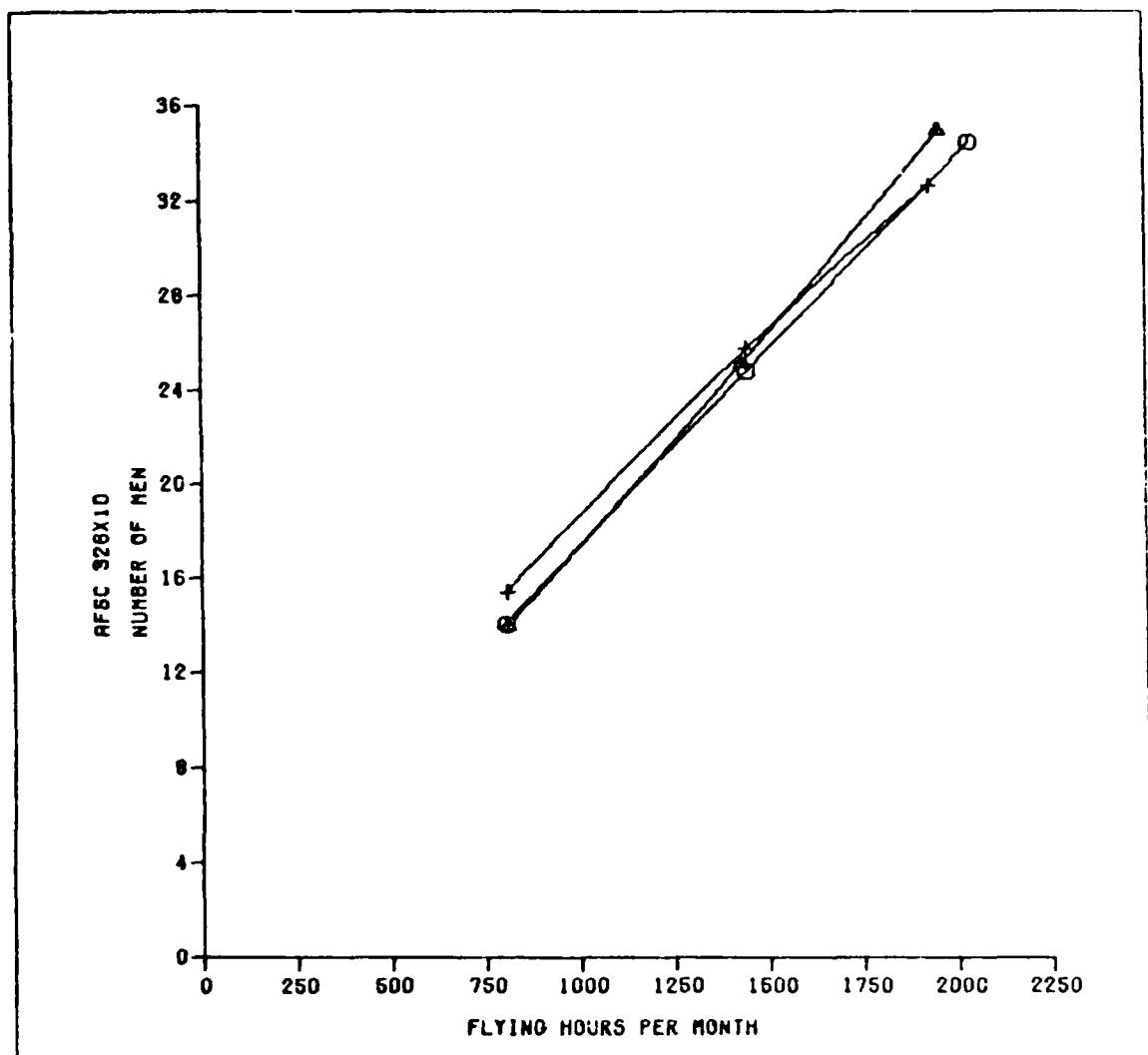
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
○ - Unconstrained Parts/ Unconstrained ATS	12 (11-12)	21 (21-22)	28 (28-29)
△ - Constrained Parts/ Unconstrained ATS	12 (12-12)	20 (19-21)	30 (29-31)
+ - Constrained Parts/ Constrained ATS	13 (12-13)	21 (20-22)	27 (25-30)

Figure 27. AFSC 326X2A (Inertial Navigation System/Weapon Control)  
Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	6 (6-7)	11 (10-11)	14 (13-14)
Δ - Constrained Parts/ Unconstrained ATS	7 (6-7)	11 (10-11)	14 (14-15)
+ - Constrained Parts/ Constrained ATS	7 (6-7)	10 (10-11)	14 (13-15)

Figure 28. AFSC 326X2C (Communications/Navigations/Electronic Counter Measures) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	13 (13-14)	26 (24-27)	34 (33-36)
△ - Constrained Parts/ Unconstrained ATS	14 (13-15)	25 (23-27)	35 (34-37)
+ - Constrained Parts/ Constrained ATS	16 (15-16)	25 (25-26)	33 (32-34)

Figure 29. AFSC 326X1D (Automatic Test Station) Direct Manning

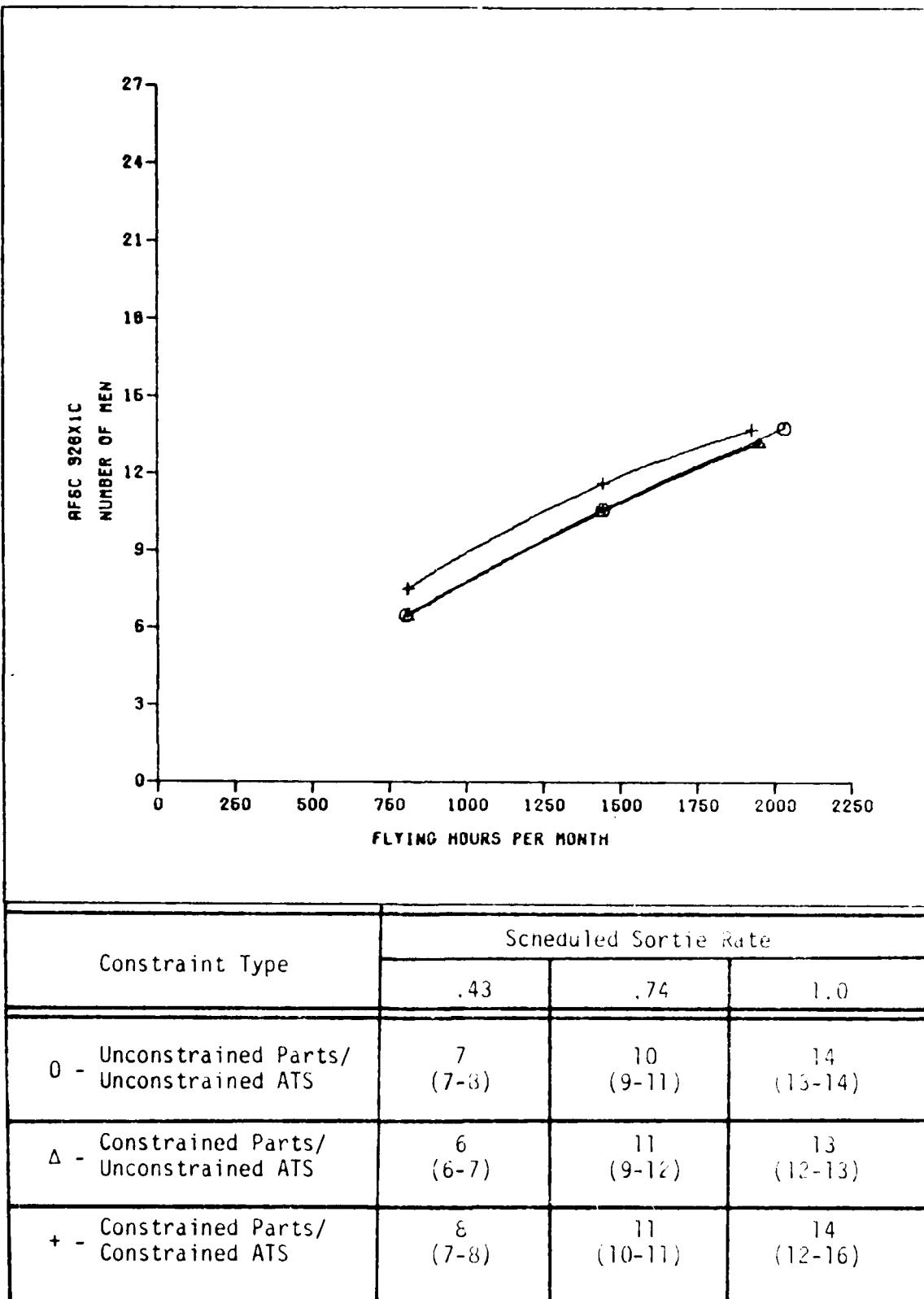
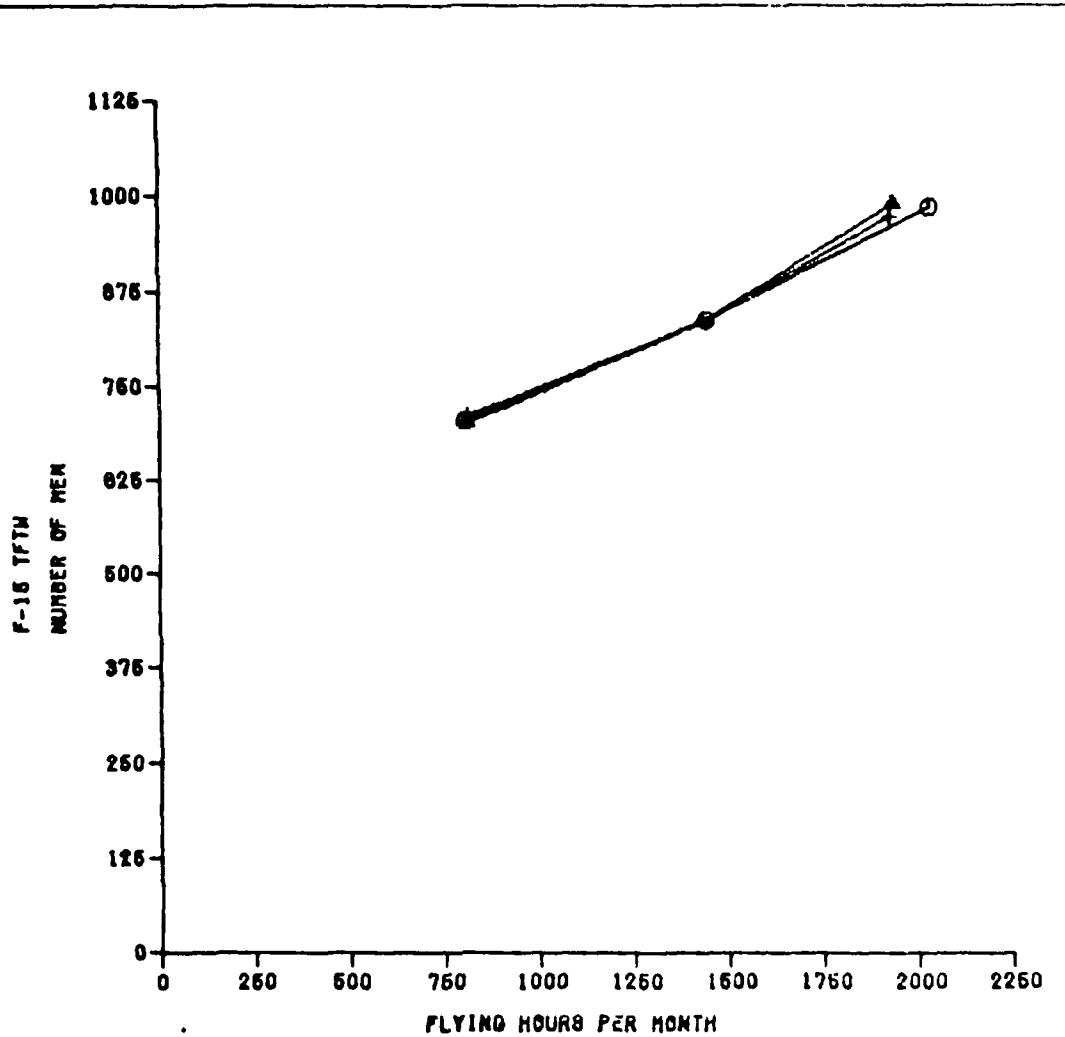


Figure 30. AFSC 326X1C (Manual Test Station) Direct Manning

Manning Document. The authors used the Moody Manpower Program to develop a complete basic manning document for the maintenance organization depicted in Figure 6 of Chapter III. Additionally, the program was used to determine the total maintenance manning requirements for each constraint type and scheduled sortie rate. The Moody Manpower Program considers each AFSC's minimum crew manning during the development of total manning requirements. If direct manning estimates are below the respective minimum crew manning, the program uses the minimum crew manning to determine total manning requirements. Since the LCOM networks define minimum crew requirements for each maintenance task, AFSC minimum crew manning remains constant for each constraint type and scheduled sortie rate. Table IX depicts the minimum crew manning for each AFSC. Figure 31 indicates the sensitivity of the F-15 TFTW's total manning requirements to constraint type and scheduled sortie rate. Figure 32 illustrates the basic manning document for unconstrained parts/ATS at a .74 scheduled sortie rate.

Table IX  
AFSC Minimum Crew Manning

AFSC	Work Description	Minimum Crew Manning
431X1	Flight Line Crew Chief	31
431X1	Phase Inspection	24
531X3	Structural Repair	10
426X2	Jet Engine	48
423X3	Fuel Systems	10
423X0	Electrical Systems	10
423X4	Pneudraulics	10
423X1	Environmental Systems	10
423X2	Egress Systems	10
326X2B	Automatic Flight Control/Instruments	10
326X2A	Inertial Navigation System/Weapon Control	10
326X2C	Communications/Navigations/Electronic Counter Measures	10
326X1D	Automatic Test Station	10
326X1C	Manual Test Station	10



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	705	837	984
Δ - Constrained Parts/ Unconstrained ATS	703	834	990
+ - Constrained Parts/ Constrained ATS	710	836	973

Figure 31. F-15 TFTW Total Manning Requirements

F15 TFTW MANNING DOCUMENT

**CHIEF OF MAINTENANCE**

F/C	DESC.	OSC	AFSC	GRADE	RQMT
-240000	CHIEF OF MAINT	JN	4095	COL	1
210000	CHIEF OF MAINT	JN	4016	LTC	1
210030	CHIEF OF MAINT	JN	43191	CMS	1
213000	CHIEF OF MAINT	JN	43171C	HSG	1
-218000	CHIEF OF MAINT	JN	70490	CIV	1
					6
218000	CHIEF OF MAINT	JND	70270	HSG	1
-210000	CHIEF OF MAINT	JND	70250	SSG	2
210000	CHIEF OF MAINT	JND	70250	SGT	3
-213000	CHIEF OF MAINT	JND	70230	A1C	1
					7
216020	CHIEF OF MAINT TNG MSG	JNB	75193	SMS	1
-240000	CHIEF OF MAINT TNG MSG	JNB	76172	SSG	1
210000	CHIEF OF MAINT TNG MSG	JNB	75132	SSG	1
					3
210000	CHIEF OF MAINT PROD ANAL	JNA	39170A	HSG	1
210000	CHIEF OF MAINT PROD ANAL	JNA	39150A	SSG	1
-218000	CHIEF OF MAINT PROD ANAL	JNA	39150A	SGT	1
					3
218000	QUALITY CONT ADM	JND	70250	CIV	2
					2
-218000	PROGRAMS/MOBILITY	JNC	66170	HSG	2
					2
211000	QUALITY CONT FCF	JNHA	4024	OPT	2
-244000	QUALITY CONT	JNHA	43171C	SSG	1
					3
211000	QUALITY CONT I O DEST	JNHCD	43151C	SSG	2
					2
-211000	QUALITY CONT	JNH	4016	LTC	1
211000	QUALITY CONT	JNH	43191	CMS	1
					2

Figure 32. F-15 TFTW Manning Document

RD-A156 540

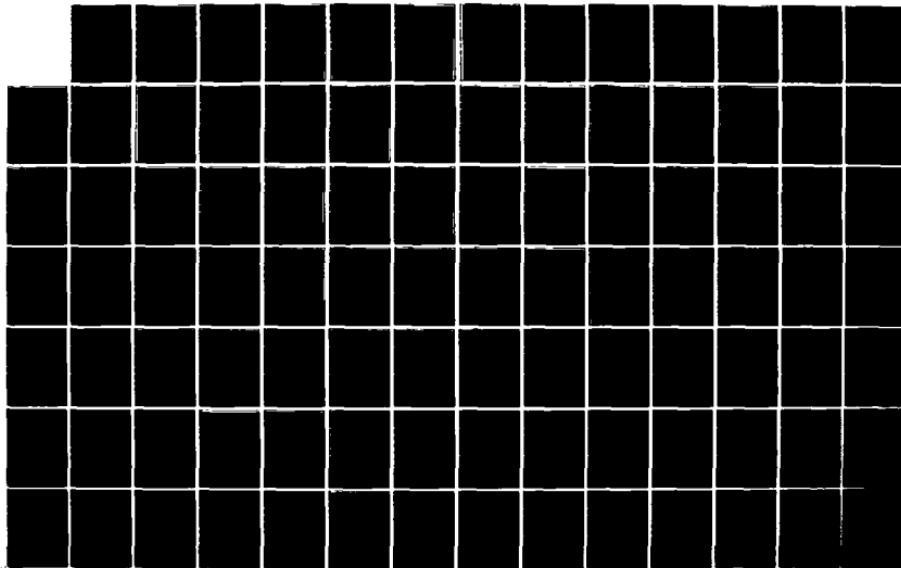
ESTIMATION OF F-15 PEACETIME MAINTENANCE MANPOWER  
REQUIREMENTS USING THE (U) AIR FORCE INST OF TECH  
WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI.

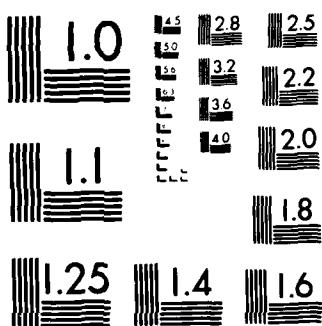
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NL





MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS 1963 A

211000	QUALITY CONT	JNHB	42375	MSG	1
211000	QUALITY CONT	JNHR	42375	TSG	2
211000	QUALITY CONT	JNHR	46272	MSG	1
211000	QUALITY CONT	JNHB	46272	TSG	4
211000	QUALITY CONT	JNHB	43171C	MSG	2
211000	QUALITY CONT	JNHB	43171C	TSG	4
211000	QUALITY CONT	JNHR	43151C	SSG	1
211000	QUALITY CONT	JNHB	46270	MSG	1
211000	QUALITY CONT	JNHB	46270	TSG	1
211000	QUALITY CONT	JNHB	46170	MSG	1
211000	QUALITY CONT	JNHR	46170	TSG	1
211000	QUALITY CONT	JNHS	32672A	MSG	1
211000	QUALITY CONT	JNHR	32672A	TSG	1
211000	QUALITY CONT	JNHB	32672B	TSG	1
211000	QUALITY CONT	JNHR	32672C	MSG	1
211000	QUALITY CONT	JNHB	32672C	TSG	2

25

212000	MAINT CONT	JNI	4016	LTC	1
212000	MAINT CONT	JNI	4024	CPT	1
212000	MAINT CONT	JNI	39290	CMS	1
212000	MAINT CONT	JNI	70250	SSG	1

4

212000	MAINT CONT J03 CNTL	JNIA	63191	SMS	1
212000	MAINT CONT J08 CNTL	JNIA	43171C	MSG	2
212000	MAINT CONT J09 CNTL	JNIA	43171C	TSG	6
212000	MAINT CONT J09 CNTL	JNIA	43151C	SSG	7
212000	MAINT CONT J09 CNTL	JNIA	43151C	SGT	8
212000	MAINT CONT J09 CNTL	JNIA	42355	SSG	2
212000	MAINT CONT J09 CNTL	JNIA	42355	SGT	2
212000	MAINT CONT J09 CNTL	JNIA	32672A	MSG	1
212000	MAINT CONT J09 CNTL	JNIA	32652A	SSG	1
212000	MAINT CONT J09 CNTL	JNIA	32652A	SGT	1
212000	MAINT CONT J09 CNTL	JNIA	46270	MSG	1
212000	MAINT CONT J09 CNTL	JNIA	46270	TSG	1
212000	MAINT CONT J09 CNTL	JNIA	46250	SSG	1
212000	MAINT CONT J09 CNTL	JNIA	46250	SGT	1

35

212000	MAINT CONT PLANS/SCH/002	JNIR	32672A	MSG	1
212000	MAINT CONT PLANS/SCH/002	JNIR	32672B	TSG	1
212000	MAINT CONT PLANS/SCH/002	JNIR	43171C	TSG	3
212000	MAINT CONT PLANS/SCH/002	JNIR	39230	SSG	6
212000	MAINT CONT PLANS/SCH/002	JNIR	39230	SGT	2
212000	MAINT CONT PLANS/SCH/002	JNIR	39270	MSG	2
212000	MAINT CONT PLANS/SCH/002	JNIR	39270	TSG	4
212000	MAINT CONT PLANS/SCH/002	JNIR	39290	SMS	1
212000	MAINT CONT PLANS/SCH/002	JNIR	70250	SGT	1
212000	MAINT CONT PLANS/SCH/002	JNIR	43171C	TSG	2
212000	MAINT CONT PLANS/SCH/002	JNIR	43161C	SSG	1
212000	MAINT CONT PLANS/SCH/002	JNIR	39270	MSG	1
212000	MAINT CONT PLANS/SCH/002	JNIR	39230	SSG	1

26

212000	MAINT CONT MAT CONT	JNIC	6424A	CPT	1
212000	MAINT CONT MAT CONT	JNIC	64570	MSG	1
212000	MAINT CONT MAT CONT	JNIC	70250	SGT	1

3

212000	MAINT CONT MAT CONT	JNICA	64570	TSG	4
212000	MAINT CONT MAT CONT	JNICA	64550	SSG	4
212000	MAINT CONT MAT CONT	JNICA	64550	SGT	5
212000	MAINT CONT MAT CONT	JNICA	64530	AIC	3

16

212000	MAINT CONT MAT CONT	JNICB	39270	MSG	3
212000	MAINT CONT MAT CONT	JNICB	39230	SSG	6
212000	MAINT CONT MAT CONT	JNICB	39230	SGT	6
212000	MAINT CONT MAT CONT	JNICB	39270	TSG	3

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Figure 32. F-15 TFTW Manning Document (continued)

**ORGANIZA. MAINTENANCE SQUADRON**

--F/C	DESC.	OSC	AFSC	GRADE	RQMT.
223000	ORGANIZ. MAINT S2	AA	4016	MAJ	1
-223000	ORGANIZ. MAINT S2	AA	44016	LTC	1
220000	ORGANIZ. MAINT S2	AA	70250	SSG	1
-220000	ORGANIZ. MAINT S2	AA	70230	A1C	1
220000	ORGANIZ. MAINT S2	AA	43191	CMS	1
					5
-226000	UNIT ADMIN	AU	7034	CPT	1
220000	UNIT ADMIN	AU	70250	SSG	1
-220000	UNIT ADMIN	AU	70230	A1C	2
220000	UNIT ADMIN	AU	10090	MSG	1
					5
-221000	FLIGHT LINE SUPV	MLH	4024	CPT	1
221000	FLIGHT LINE SUPV	MLH	70230	A1C	1
-221000	FLIGHT LINE SUPV	MLH	4024	LT	4
221000	FLIGHT LINE SUPV	MLH	43191	SMS	1
-221000	FLIGHT LINE CMF	MLH	43171C	MSG	1
221000	FLIGHT LINE CMF	MLH	43171C	MSG	1
-221000	FLIGHT LINE CMF	MLH	43171C	MSG	4
221000	FLIGHT LINE CMF	MLH	43171C	TSG	20
-221000	FLIGHT LINE EXPEDITOR	MLH	43171C	TSG	4
221000	FLIGHT LINE CMF	MLH	43151C	SSG	4
-221000	FLIGHT LINE INSPECTOR	MLH	43191	SMS	1
221000	FLIGHT LINE GO SUPP EDP	MLH	43171C	MSG	1
-221000	FLIGHT LINE BENCH STOCK	MLH	43151C	SSG	1
221000	FLIGHT LINE BENCH STOCK	MLH	43151C	SGT	2
-221000	FLIGHT LINE JBB EQUIP	MLH	43171C	TSG	1
221000	FLIGHT LINE JBB EQUIP	MLH	43151C	SSG	1
-221000	FLIGHT LINE JBB EQUIP	MLH	43151C	SGT	1
221000	FLIGHT LINE JBB EQUIP	MLH	43131C	A1C	1
-221000	FLIGHT LINE	MLH	43191	SMS	1
221000	FLIGHT LINE	MLH	43191	MSG	1
-221000	FLIGHT LINE	MLH	43171C	MSG	4
221000	FLIGHT LINE	MLH	43171C	TSG	1
-221000	FLIGHT LINE	MLH	43171C	SSG	5
221000	FLIGHT LINE	MLH	43151C	SSG	19
-221000	FLIGHT LINE	MLH	43151C	SGT	41
221000	FLIGHT LINE	MLH	43151C	A1C	10
-221000	FLIGHT LINE	MLH	43181C	A1C	41
					176
222000	PHASE	MLI	431	71CMSSG	1
-222000	PHASE	MLI	431	71CTSG	4
222000	PHASE	MLI	431	71CSSG	1
-222000	PHASE	MLI	431	51CSSG	4
222000	PHASE	MLI	431	51CSGT	8
-222000	PHASE	MLI	431	51CA1C	2
222000	PHASE	MLI	431	31CA1C	7

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Figure 32. F-15 TFTW Manning Document (continued)

FIELD MAINTENANCE SQUADRON

F/C	DESC.	OSC	AFSC	GRADE	RQNT
230000	FIELD MAINT S7	AA	6015	MAJ	1
230000	FIELD MAINT S9	AA	A4015	CFC	1
230000	FIELD MAINT SD	AA	70250	SSG	1
230000	FIELD MAINT SD	AA	42692	CMS	1
230000	FIELD MAINT S7	AA	70230	A1C	1
					5
230000	UNIT ADMIN	AU	7034	CPT	1
230000	UNIT ADMIN	AU	70250	SSG	1
230000	UNIT ADMIN	AU	70230	A1C	1
230000	UNIT ADMIN	AU	10090	MSG	1
					6
231000	FABRICATION	MKH	63195	SMS	1
					7
231100	MACHINE SHOP	MKHA	53150	SSG	2
231100	MACHINE SHOP	MKHA	53150	SGT	2
231100	MACHINE SHOP	MKHA	53150	A1C	1
231100	MACHINE SHOP	MKHA	53130	A1C	1
					8
231200	METAL PROCESSING	MKHB	53151	SSG	2
231200	METAL PROCESSING	MKHB	63151	SGT	2
231200	METAL PROCESSING	MKHB	53131	A1C	2
					9
231300	STRUT REPAIR	MKHC	63173	SSG	1
231300	STRUT REPAIR	MKHC	53153	SSG	2
231300	STRUT REPAIR	MKHC	53153	SGT	5
231300	STRUT REPAIR	MKHC	53153	A1C	1
231300	STRUT REPAIR	MKHC	53133	A1C	5
					10
231400	CORROSION CONTROL	MKHF	53154	SSG	1
231400	CORROSION CONTROL	MKHF	53154	SGT	2
231400	CORROSION CONTROL	MKHF	53154	A1C	3
231400	CORROSION CONTROL	MKHF	63134	A1C	2
					11
231500	SURVIVAL EQUIPMENT	MKHF	58271	TSG	1
231500	SURVIVAL EQUIPMENT	MKHF	58251	SSG	2
231500	SURVIVAL EQUIPMENT	MKHF	5A241	SGT	2
231500	SURVIVAL EQUIPMENT	MKHF	58231	A1C	2
231500	SURVIVAL EQUIPMENT	MKHF	58250	SSG	1
231500	SURVIVAL EQUIPMENT	MKHF	58250	SGT	1
231500	SURVIVAL EQUIPMENT	MKHF	5A230	A1C	1
					12
231700	NON-DESTRUCTIVE INSPECTION	MKHG	53175	CIV	1
231700	NON-DESTRUCTIVE INSPECTION	MKHG	53175	TSG	1
231700	NON-DESTRUCTIVE INSPECTION	MKHG	53155	SSG	2
231700	NON-DESTRUCTIVE INSPECTION	MKHG	53155	SGT	2
231700	NON-DESTRUCTIVE INSPECTION	MKHG	53135	A1C	2
					13
232100	PROPELLION	MKE	4826	LT	1
232000	PROPELLION	MKE	45292	CMS	1
232700	WRENCH STOCK/TOOL R4	MKE	42672	TSG	1
232800	WRENCH STOCK/TOOL R4	MKE	42652	SSG	1
232800	WRENCH STOCK/TOOL R4	MKE	42652	SGT	1
232800	WRENCH STOCK/TOOL R4	MKE	42632	A1C	1
					14

Figure 32. F-15 TFTW Manning Document (continued)

232300	JET ENGINE	MKIC	42672	MSG	2
232300	JET ENGINE	MKIC	42672	TSG	2
232300	JET ENGINE	MKIC	42672	SSG	4
232300	JET ENGINE	MKIC	42652	SSG	16
232300	JET ENGINE	MKIC	42652	SGT	34
232300	JET ENGINE	MKIC	42652	AIC	8
232300	JET ENGINE	MKIC	42632	AIC	35
					101
233000	AEROSPACE SYSTEMS	MKJ	4024	LT	1
233000	AEROSPACE SYSTEMS	MKJ	70250	SGT	1
233000	AEROSPACE SYSTEMS	MKJ	42396	SMS	1
					3
233100	REPAIR AND RECLAMATION	MKJA	43171C	MSG	2
233100	REPAIR AND RECLAMATION	MKJA	43171C	TSG	3
233100	REPAIR AND RECLAMATION	MKJA	43151C	SSG	6
233100	REPAIR AND RECLAMATION	MKJA	43151C	SGT	6
233100	REPAIR AND RECLAMATION	MKJA	43131C	AIC	5
					22
233200	FUEL SYSTEMS	MKJB	42373	SSG	1
233200	FUEL SYSTEMS	MKJB	42353	SSG	2
233200	FUEL SYSTEMS	MKJB	42153	SGT	5
233200	FUEL SYSTEMS	MKJB	42353	AIC	1
233200	FUEL SYSTEMS	MKJB	42333	AIC	5
					14
233300	ELECTRICAL SYSTEMS	MKJC	42370	SSG	1
233300	ELECTRICAL SYSTEMS	MKJC	42350	SSG	2
233300	ELECTRICAL SYSTEMS	MKJC	42350	SGT	1
233300	ELECTRICAL SYSTEMS	MKJC	42350	AIC	1
233300	ELECTRICAL SYSTEMS	MKJC	42330	AIC	3
					10
233400	PNEUMAULICS	MKJD	42374	SSG	1
233400	PNEUMAULICS	MKJD	42354	SSG	3
233400	PNEUMAULICS	MKJD	42354	SGT	6
233400	PNEUMAULICS	MKJD	42354	AIC	1
233400	PNEUMAULICS	MKJD	42334	AIC	7
					18
233600	ENVIRONMENTAL SYSTEMS	MKJF	42351	SSG	2
233600	ENVIRONMENTAL SYSTEMS	MKJF	42361	SGT	1
233600	ENVIRONMENTAL SYSTEMS	MKJF	42351	AIC	1
233600	ENVIRONMENTAL SYSTEMS	MKJF	42331	AIC	4
					10
233900	EGRESS SYSTEMS	MKJI	42352	SSG	2
233900	EGRESS SYSTEMS	MKJI	42352	SGT	3
233900	EGRESS SYSTEMS	MKJI	42352	AIC	1
233900	EGRESS SYSTEMS	MKJB	42332	AIC	4
					10
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	MSG	2
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	TSG	2
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	SSG	4
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	SSG	15
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	SGT	33
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	AIC	8
234000	AEROSPACE GROUND EQUIPMENT	MKK	42335	AIC	36
					98

Figure 32. F-15 TFTW Manning Document (continued)

AVIONICS COMMAND SQUADRON

F/C	DESC.	OSC	AFSC	GRADE	RQMT
248000	AVIONICS SQ	AA	A6096	LTC	1
248000	AVIONICS-SQ	AA	4016	MAJ	1
248000	AVIONICS SQ	AA	32090	CMS	1
248000	AVIONICS SQ	AA	70250	SSG	1
248000	AVIONICS SQ	AA	70230	A1C	1
248000	AVIONICS SQ	AA	4024	CPT	1
					6
240000	UNIT ADMIN	AU	7034	CPT	1
240000	UNIT ADMIN	AU	10090	MSG	1
240000	UNIT ADMIN	AU	70250	SSG	1
240000	UNIT ADMIN	AU	70230	A1C	1
					4
243800	ELECTRONICS	HJO	4026	CPT	1
243800	ELECTRONICS	HJO	32622C	MSG	1
					2
243300	AUT FLT CON & INST SUPV	HJO	32692	SMS	1
243300	AUT FLT CON & INST	HJO	32652B	SSG	2
243300	AUT FLT CON & INST	HJO	32652B	SGT	3
243300	AUT FLT CON & INST	HJO	32652B	A1C	1
243300	AUT FLT CON & INST	HJO	32632A	A1C	4
					11
243600	WEAP CON & INER NV SJ <sup>2</sup> V	HJOA	32692	SMS	1
243600	WEAP CON & INER NV	HJOA	32672A	MSG	1
243600	WEAP CON & INER NV	HJOA	32672A	TSG	1
243600	WEAP CON & INER NV	HJOA	32672A	SSG	1
243600	WEAP CON & INER-NV	HJOA	32652A	SSG	3
243600	WEAP CON & INER NV	HJOA	32652A	SGT	7
243600	WEAP CON & INER NV	HJOA	32652A	A1C	1
243600	WEAP CON & INER NV	HJOA	32632A	A1C	6
					21
243700	COMM NV & PEN AIDS	HJOC	32652C	SSG	1
243700	COMM NV & PEN AIDS	HJOC	32652C	SGT	3
243700	COMM NV & PEN AIDS	HJOC	32652C	A1C	1
243700	COMM NV & PEN AIDS	HJOC	32632C	A1C	5
					10
246000	AVN SHOP MAINT	HJP	4024	CPT	1
246000	AVN SHOP MAINT	HJP	32692	MSG	1
					2

Figure 32. F-15 TFTW Manning Document (continued)

246100	AVN AGE	MJPA	32670R	MSG	1
246100	AVN AGE	MJPA	32670B	TSG	1
246100	AVN AGE	MJPA	32670H	SSG	1
246100	AVN AGE	MJPA	32650R	SSG	6
246100	AVN AGE	MJPA	32650H	SGT	9
246100	AVN AGE	MJPA	32650B	A1C	2
246100	AVN AGE	MJPA	32670B	A1C	8

26

246200	AUTO TST STN SUPV	MJPB	32692	SMS	1
246200	AUTO TST STN	MJPA	326710	MSG	1
246200	AUTO TST STN	MJPB	326710	TSG	1
246200	AUTO TST STN	MJPA	326710	SSG	1
246200	AUTO TST STN	MJPB	326510	SSG	6
246200	AUTO TST STN	MJPA	326510	SGT	6
246200	AUTO TST STN	MJPB	326510	A1C	2
246200	AUTO TST STN	MJPB	326310	A1C	7

26

246300	MAN TST STN	MJPC	32651C	SSG	1
246300	MAN TST STN	MJPC	32651C	SGT	3
246300	MAN TST STN	MJPC	32651C	A1C	1
246300	MAN TST STN	MJPC	32631C	A1C	6

10

#### SUMMARY OF WHOLE WING

COL	1
LTC	6
MAJ	3
CPT	11
LT	3

**TOTAL** 24

**GIV** 4

CMS	6
SMS	12
MSG	5
MSG	46
TSG	89
SSG	23
SSG	146
SGT	227
A1C	47
A1C	208

**TOTAL** 890

Figure 32. F-15 TFTW Manning Document (continued)

### Summary

This chapter contains a discussion of the analysis and results of the F-15 TFTW LCOM simulation. The analysis section contains a graphical and statistical interpretation of the simulation's steady state conditions and autocorrelation coefficients. The results consist of direct manning estimates for each AFSC listed in Table I, their respective 95 percent confidence intervals, the sensitivity of these estimates to variations in parts and ATS, and a USAF basic manning document for the F-15 TFTW. The Conclusion and Recommendation Chapter summarizes the results and makes recommendations concerning the thesis findings.

## VI. CONCLUSIONS AND RECOMMENDATIONS

As stated in Chapter I, this thesis had three major objectives: first, use LCOM to estimate the maintenance manpower requirements for a 72 U.E. F-15 TFTW; second, construct statistical confidence intervals for these manpower estimates; third, investigate the sensitivity of maintenance manpower requirements to variations in the availability of aircraft spare parts and support equipment. The authors accomplished these objectives and presented their analysis and results in Chapter V. Figures 17 through 30 illustrate each AFSC's direct manning requirements, confidence intervals, and sensitivity to constraint type and scheduled sortie rate. Figure 31 depicts the total manning requirements for a 72 U.E. F-15 TFTW and the sensitivity of these requirements to constraint type and scheduled sortie rate. Finally, Figure 32 contains a basic manning document for a 72 U.E. F-15 TFTW based on unconstrained parts/ATS and a .74 scheduled sortie rate.

### Conclusions

This thesis has allowed the authors to develop several noteworthy conclusions concerning LCOM manpower estimation, in general, and the peacetime model used in this study. They feel that these developments will enable greater statistical accuracy in LCOM manpower estimates and, therefore, further enhance LCOM's position in the manpower community.

Steady State. In this study, the authors developed a more efficient procedure for determining steady state conditions in an LCOM computer simulation. The procedure involved graphical and statistical analysis of daily and weekly AFSC manhour totals as described in Chapters IV and V.

Using this technique, the authors found that the F-15 TFTW model used in this thesis exhibited steady state conditions throughout the 98 day simulation period. In those isolated instances found in Table IV of Chapter V where individual AFSC's indicated transient behavior, this behavior disappeared after the first or second week into the simulation period. As a result, output data for the entire simulation period was used to estimate maintenance manpower requirements. When contrasted with the more common procedure of discarding the first 30 days in an LCOM simulation (Ref 33:114-115), the procedure used in this study more efficiently utilizes computer run time and allows equally accurate results. When one considers that this study required more than 25 computer runs, the overall savings in computer time is significant.

Autocorrelation. The study used autocorrelation analysis to develop 95 percent statistical confidence intervals for AFSC direct manning estimates. The procedure allowed the authors to estimate maintenance manpower requirements with a very high degree of statistical accuracy. Based on this procedure, all AFSC's except two indicated a five percent or less variability in direct manning estimates; AFSC's 426X2 (Jet Engine) and 423X3 (Fuel Systems) indicated an eight percent and nine percent, respectively, variability in direct manning estimates. Such accuracy lends confidence to the LCOM manpower estimation process.

Model Validity. In order to verify these procedures, the authors compared the LCOM direct manning estimates and corresponding statistical confidence intervals contained in Chapter V with estimates from three other LCOM simulation strategies. Table X illustrates this comparison using four sets of manning estimates based on unconstrained parts/ATS

Table X  
Comparison of Simulation Strategies

AFSC	Simulation Strategy			
	1	2	3	4
431X1 (Flight Line Crew Chief)	124(120-128)	124	124	125
431X1 (Phase Inspection)	20(20-21)	21	20	20
531X3	14(13-14)	13	13	13
426X2	103(94-112)	97	107	97
423X3	16(14-17)	13	13	11
423X0	8(7-8)	7	7	8
423X4	17(16-19)	18	18	18
423X1	10(9-10)	9	10	8
423X2	2(2-2)	2	2	2
326X2B	10(9-10)	9	9	10
326X2A	21(21-22)	21	21	20
326X2C	11(10-11)	10	11	11
326X1D	26(24-27)	25	25	24
326X1C	10(9-11)	10	11	11
ASR	.697	.694	.708	.692
<b>Strategy 1 - 98 day simulation with 5 day flying schedule and 7 day maintenance schedule.</b>				
<b>Strategy 2 - 196 day simulation with 5 day flying schedule and 7 day maintenance schedule.</b>				
<b>Strategy 3 - 100 day simulation with 5 day flying schedule and 5 day maintenance schedule.</b>				
<b>Strategy 4 - 98 day simulation with 5 day flying schedule, 7 day maintenance schedule, and different random number seeds.</b>				

and a .74 scheduled sortie rate. In this table, Strategy 1 reflects the methodology and results contained in Chapters IV and V, respectively.

The direct manning estimates from Strategy 2 were obtained using methodology similar to Strategy 1 except the simulation period consisted of 196 days and the manning estimates were based solely on the last 98 simulated days. The reason for doubling the simulation period was to determine if the authors' assertions concerning the peacetime model's steady state behavior were, in fact, correct. Since the direct manning estimates obtained from Strategy 2 were similar to the corresponding Strategy 1 estimates, the authors concluded that longer computer run times did not significantly affect the F-15 TFTW direct manning estimates. This comparison confirmed their steady state analysis of the peacetime model.

In Strategy 3, the direct manning estimates were based on a 100 day simulation period with a concurrent five day flying and maintenance work week. Such a scenario eliminated weekends from the maintenance schedule and eliminated the opportunity to perform backlogged maintenance work on nonflying days. During the computation of direct manning under this strategy, 20.99 work days per month replaced 30.44 work days per month in Equation (3) of Chapter IV (Ref 2:Chap. 6, p. 29). Although the manning estimates from this strategy were similar to those of Strategy 1, the authors concluded that higher scheduled sortie rates, and/or more severe parts/ATS constraints would cause bottlenecks in the maintenance work flow and produce erratic day-to-day manhours used data. Such data would cause transient behavior at the beginning of the simulation period and would require longer computer run times in order to achieve steady state conditions. Since actual peacetime operations routinely schedule flying

and maintenance activity Monday through Friday and permit weekend maintenance activity to alleviate backlogged work, a scenario based on a five day flying and seven day maintenance work week is a logical simulation strategy for peacetime LCOM studies. Such a strategy reflects peacetime operations in that maintenance manpower only works on weekends when there exists a work demand and permits efficient LCOM estimation of peacetime maintenance manpower over a wide range of flying activity levels and aircraft part/ATS constraints.

The direct manning estimates from Strategy 4 were obtained using methodology identical to Strategy 1 and different random number seeds in the LCOM main program. The change in random number seeds created an independent replication of direct manning estimates; the slight differences in AFSC manning estimates between Strategies 1 and 4 are a normal occurrence in replicated data. At the same time, this small variability in AFSC direct manning between the two replications supported the internal validity of the F-15 TFTW model used in this study and reinforced the authors' confidence in the F-15 peacetime model (Ref 10:204).

It should be noted that the AFSC 423X3 (Fuel Systems) direct manning estimate in Strategies 2, 3, and 4 did not fall within the respective Strategy 1 confidence interval. Additionally, the Strategy 4 estimates for AFSC's 423X1 (Environmental Systems) and 326X2A (Inertial Navigation System/Weapon Control) did not lie within the corresponding Strategy 1 confidence intervals. The authors found these deviations interesting but not disconcerting. The authors expected isolated deviations in direct manning estimates for two reasons: first, when direct manning estimates are rounded to integer values in accordance with AFM 25-5 standards, two estimates such as 8.61 and 8.62 become eight and nine,

respectively; second, some variability in replicated data is to be expected. The comparison of simulation Strategy 1 with Strategies 2, 3, and 4 was intended to illustrate, in a general sense, that the authors methodology was valid. The authors could not completely explain the lower estimates for AFSC 423X3 in Strategies 2, 3, and 4. However, they do not feel that the deviation of these estimates from the Strategy 1 estimates was reason to question the overall validity of Strategy 1. If there had existed consistent deviations among a majority of the AFSC estimates in Strategies 2, 3, and 4 when compared to Strategy 1, the authors would have questioned the validity of their methodology. However, in general, just the opposite is true. The majority of estimates in Strategies 2, 3, and 4 agreed closely with the results of Strategy 1. Thus, the authors believe the comparison of simulation strategies supports, in a general sense, the validity of their methodology.

Manning Sensitivity. It is apparent from Figure 31 in Chapter V that F-15 TFTW total manning requirements were relatively insensitive to the constrained parts and ATS contained in Appendix E. Although total manning requirements indicated a slight sensitivity to parts and ATS constraints at the 1.0 scheduled sortie rate, these constraints had little effect on total manning requirements at the lower scheduled flying activity levels. The authors concluded that at and below a .74 scheduled sortie rate the spare part and ATS constraints contained in Appendix E were sufficient to support the daily flying activity.

At the 1.0 scheduled sortie rate, the spare parts and ATS constraints could not support the daily flying activity. As a result, the constrained parts simulation required additional manpower to repair and/or cannibalize aircraft parts while the constrained parts/ATS simulation

required less manpower because a limited number of men could perform ATS functions. As Table VIII in Chapter V indicates, these constraints also had a noticeable effect on accomplished sortie rate (ASR) and flying hours per month (FHPM). The authors concluded that more severe part and ATS constraints would have similar effects on the lower flying activity levels.

Individual AFSC manning showed no particular trend in sensitivity to constraint type. The AFSC 423X3 (Fuel Systems) in Figure 21 was the most sensitive estimate while AFSC 431X1 (Flight Line Crew Chief) displayed the least sensitivity. In most cases, the AFSC direct manning confidence intervals for the .43 and .74 scheduled sortie rates contained two or more constraint type manning estimates. The authors, therefore, concluded that, since the modeled F-15 TFTW conducts its routine flying training in the .43 and .74 scheduled sortie rate range, direct manning sensitivity to aircraft spare part and ATS constraints contained in Appendix E was statistically insignificant.

#### Recommendations

As a result of this study, the authors have gained an indepth understanding of the LCOM manpower estimation process. They believe this experience qualifies them to make several recommendations concerning future LCOM studies.

The authors recommend that the LCOM postprocessor program be modified to provide time series plots of AFSC manhours used. These plots would be similar to the graphs illustrated in Figures 10 through 13 in Chapter V. This capability would allow LCOM users to efficiently determine the steady state behavior of their simulation model. Tetmeyer

(Ref 31) agreed that such a capability would benefit the LCOM community; Drake (Ref 29) confirmed the feasibility of such a modification. The authors, therefore, recommend that the new version of LCOM (LCOM II) incorporate this feature.

It is recommended that LCOM peacetime studies use a five day flying and seven day maintenance work week. This type of scenario reflects actual peacetime operations and permits efficient LCOM estimation of maintenance manpower over a wide range of flying activity levels.

Finally, the authors recommend that the LCOM community use the methodology described in Chapter IV to develop statistical confidence intervals for manning estimates. This procedure adds statistical reliability to the LCOM estimates and provides decision makers with a realistic perspective of manpower requirements.

#### Future Work

The accomplishment of the authors stated objectives represent the conclusion of this thesis effort. However, the authors feel that future LCOM studies should investigate the interaction of peacetime manning estimates with a wartime environment. For example, the peacetime manning estimates derived from this thesis should be incorporated into the F-15 wartime model in order to measure the effect on accomplished sortie rate and manhour utilization rate. Such an effort would realistically portray the conversion of a peacetime flying organization into a wartime operation and give the decision maker direction in determining potential operational problem areas.

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APPENDIX A

F-15 TFTW DATA BASE

## APPENDIX A

### F-15 TFTW DATA BASE

1. This appendix contains a computer listing of the F-15 peacetime maintenance data base. The data base is listed in LCOM Extended Form 11 format on pages 107 through 149. The data base organization corresponds to the LCOM Extended Form 11 column headings illustrated in Figure A-1. Maintenance manpower defined in the data base networks is available 24 hours a day and seven days a week. Tetmeyer (Ref 33) describes in further detail the mechanics of the LCOM Extended Form 11.

Figure A-1. LCOM Extended Form 11

2. The networks include the following coding conventions.

a. ACTION CODES:

F - Failure Clock.

T - Troubleshoot On-aircraft.

X - Work to Facilitate Maintenance (Access, Preparation, etc.).

A - Get and Hookup Aircraft Ground Equipment.

R - Remove/Replace LRU.

M - Repair On-aircraft.

V - Verify Systems Works.

W - Check and Repair In-shop.

K - Check OK in Shop.

N - Check and NRTS/Condemn.

J - Aircraft Handling.

B - Loading/Downloading.

G - Fueling.

H - Flightline Inspection/Service.

P - Phase Inspection.

C - Call Section (Reference to a sub-network).

Q - Draw LRU from Supply.

D - Decrement a Failure Clock.

Z - Fly Sortie.

b. Task names for unscheduled maintenance use the appropriate LRU work unit code (WUC). Task names for general aircraft servicing and support tasks are mnemonic abbreviations of the task description. For example, the task of reloading the gun is named LDGUN, and the task of servicing liquid oxygen is named LOXSV.

c. LCOM SELECTION MODES:

- A - Non-Mutually Exclusive Probability.
- C - Call Section Reference to a Sub-network.
- D - Task Done in Indicated Order.
- E - Mutually Exclusive Probability.
- F - Task Done if Indicated Failure Occurs.
- G - Relative Probability, Non-Mutually Exclusive.
- H - Task Not Done if Indicated Failure Occurs.
- I - Task Done Only if Cannibalization is Required.
- X - Task Done When Failure Occurs in Subsequent Tasks.
- S - Sortie (Externally Scheduled).

3. Task resource names are the Air Force Specialty Codes (AFSC's) of maintenance personnel, or mnemonic abbreviations for ground support equipment. For example, LXCART indicates a liquid oxygen service cart, and D60 indicates an M32-60 Ground Power Unit. The fourth (skill level) digit of the Air Force Specialty Code is replaced by an X, except in cases where a further shredout is necessary. Table A-I depicts each AFSC whose manpower was estimated by LCOM, the corresponding LCOM shredout, and the work description.

Table A-I  
LCOM AFSC Shredout Used in F-15 Data Base

AFSC	LCOM Shredout	Work Description
326X1D	326A1	Automatic Test Station
326X2A	326A2	Inertial Navigation System/Weapon Control
326X1C	326B1	Manual Test Station
326X2B	326B2	Automatic Flight Control/Instruments
326X2C	326C2	Communications/Navigation/Electronic Counter Measures
423X0	423X0	Electrical Systems
423X1	422X1	Environmental Systems
423X2	422X2	Egress Systems
423X3	424X0	Fuel Systems
423X4	421X2	Pneudraulics
426X2	432X0	Jet Engine Shop/Jet Engine Flight Line
	432T0	Jet Engine Test Cell
431X1	431X1	Flight Line Crew Chief
	431P1	Phase Inspection
531X3	531X3	Structural Repair

JGF19101275 X-12		25	02 1 00 1 17	DBASE
4			MAIN NETWORKS FOR F15 TFW OPERATION	DBASE
4			THIS IS AN UPDATE OF THE F15 STUDY	DBASE
H			ACCOMPLISHED OCTOBER 1975. THE	DBASE
H			CLOCKS HAVE BEEN CHANGED TO REFLECT	DBASE
4			ACTUAL LUKE AFC O-TS FROM THE PERIOD	DBASE
H			SEP 75 THRU FEB 76. THE PHASE AND	DBASE
H			ENGINE NETWORKS HAVE BEEN CHANGED	DBASE
H			GEASSTICALLY. THE PHASE A-DEUCE TEC	DBASE
H			AND AFLC AND LOCMES SUPPORT THE NEW	DBASE
4			100 HOUR PHASE INSPECTION THAT WAS	DBASE
H			SUGGESTED BY SIGHT SURVEY. THE ENGINE MODELS	DBASE
H			HAD TO BE RE-NETWORKED TO REFLECT THIS.	DBASE
H			ALL NETWORK CHANGES HAVE BEEN MATCHED, GEAR	DBASE
4			UNDER THE DIRECTION OF THE SYSTEMS MAINTENANCE	DBASE
4			AND ALL SIMULATION WILL BE DONE	DBASE
H			AS AN ASIT THIS IS TOPIT.	DBASE
H		00010	PREFLIGHT DUMMY SORTIE	DBASE
JG11 Z-100	3	00110 31		DBASE
JG11 008MT3	3	00110 31		DBASE
CALPRE 014433 JG11 3	3	00110 31		DBASE
JG11 CALPU JG11 3	3	00110 31		DBASE
JG11 MPPAGE	3	00110 31	5 29L 1060	DBASE
JG11 MPPFT	3	00110 31	17 29L 1-31X1	DBASE
CALPRE H10X3V	3	00110 31	5 29L 2-31X1 ILUART	DBASE
CALPRE 0074T3	3	00110 31		DBASE
	4	00110	CHANGE MALFUNC ECM PSD	DBASE
CALEGN 00PMG2	3	00110 31		DBASE
JG11 CALPU JG11 3	3	00110 31		DBASE
JG11 3E2M10	3	00110 31	11 1L 332F02 14J1	DBASE
JG11 3E2M43	3	00110 31	5 1L 1060	DBASE
	4	00110	PFCSCO AND INSPECTION OF GUN	DBASE
CLGUW1 BLGUN	3	00110 31	4 1L 3-62X1	DBASE
CLGUW1 HKGUN	3	00110 31	4 2L 2-62X2	DBASE
	4	00010	DOWNLOAD AIM9 FOR ENGINE MAINT 15 77	DBASE
CALEG2 MISSIL CALEG1 X	3	00010 31	7 1L 4-62Z1	DBASE
CALJK2 MISSIL CALJK1 X	3	00010 31	DOWNLOAD AIM9 FOR JACKING 15 77	DBASE
	4	00010	DOWNLOAD AIM9 FOR UNMNT 15 77	DBASE
CALLS2 MISSIL CALLS1 X	3	00010 31		DBASE
	4	00010	AIR-AIR TNG FIRST TO TURN	DBASE
AA1 CALPZ 4A12	3	00110 31		DBASE
AA2 H2FM 4A13	3	00110 31	5 29L 3462Z0	DBASE
AA3 H1UNCH 4A14	3	00110 31	3 29L 1-31X1	DBASE
AA4 HSTPT2 4A15	3	00110 31	5 29L 2-31X1	DBASE
AA5 00RMT1 4A16	3	00110 31		DBASE
AA6 CALEG2 4A17	3	00110 31		DBASE
AA7 CALJK2 4A18	3	00110 31		DBASE
AA8 CALLOM 4A19	3	00110 31		DBASE
AA9 CALFL1 4A11	3	00110 31		DBASE
AA10 JTAKI 4A11	3	00110 31	2 10L	DBASE
AA11 HEUFGD 4A12	3	00110 31	1 10L 3431X1 3462Z0	DBASE
AA12 720000 4-13	3	00110 31		DBASE
AA13 HEGFIN 4A14	3	00110 31	1 1L 2462Z0	DBASE
AA14 00RMT2 4A15	3	00110 31		DBASE
AA15 00RMT3 4A16	3	00110 31	5 29L 2-31X1	DBASE
AA16 HTPRU1 4A17	3	00110 31	3 29L 1-31X1	DBASE
AA16 HTPRU2 4A18	3	00110 31	3 29L 1431X1	DBASE
AA17 CALEG1 4A17	3	00010 31		DBASE
AA17 CALJK1 4A18	3	00010 31		DBASE

A818	CALLS1	A819	C	J8C10	31		DBASE	64
A819	OLGUM1		C	J8C10	31		DBASE	65
				J8C10	31		DBASE	66
				J8C10	31		DBASE	67
A821	MUNCH	A822	C	J8C10	31	AIR-AIR TAG TURN TO TURN	DBASE	68
A822	MSTRT2	A823	C	J8C10	31		DBASE	69
A823	OLGUM1	A824	C	J8C10	31		DBASE	70
A824	CALJK2	A825	C	J8C10	31		DBASE	71
A825	CALJK2	A826	C	J8C10	31		DBASE	72
A826	CALLOM	A827	C	J8C10	31		DBASE	73
A827	CALLS1	A828	C	J8C10	31		DBASE	74
A828	JTAXI	A829	C	J8C10	31		DBASE	75
A829	HEOPT2	A830	C	J8C10	31		DBASE	76
A830	Z-1-3	A831	S	J8C10	31		DBASE	77
A831	HEOPT2	A832	C	J8C10	31		DBASE	78
A832	HTAXI	A833	C	J8C10	31		DBASE	79
A833	DCEMT2	A834	C	J8C10	31		DBASE	80
A834	DCEMT2	A835	C	J8C10	31		DBASE	81
A835	HTH-EU1	A836	C	J8C10	31		DBASE	82
A836	HTH-EU2	A837	C	J8C10	31		DBASE	83
A837	JALE31	A838	C	J8C10	31		DBASE	84
A838	CALJK1	A839	C	J8C10	31		DBASE	85
A839	CALLS1	A840	C	J8C10	31		DBASE	86
A840	CALUM1		C	J8C10	31		DBASE	87
				J8C10	31	AIR-AIR TAG TURN TO LAST	DBASE	88
A841	MUNCH	A842	C	J8C10	31		DBASE	89
A842	MSTRT2	A843	C	J8C10	31		DBASE	90
A843	DCEMT2	A844	C	J8C10	31		DBASE	91
A844	CALJK2	A845	C	J8C10	31		DBASE	92
A845	CALJK2	A846	C	J8C10	31		DBASE	93
A846	CALLOM	A847	C	J8C10	31		DBASE	94
A847	CALLS1	A848	C	J8C10	31		DBASE	95
A848	HTAXI	A849	C	J8C10	31		DBASE	96
A849	HEOPT2	A850	C	J8C10	31		DBASE	97
A850	Z-1-3	A851	S	J8C10	31		DBASE	98
A851	HEOPT2	A852	C	J8C10	31		DBASE	99
A852	DCEMT2	A853	C	J8C10	31		DBASE	100
A853	DCEMT2	A854	C	J8C10	31		DBASE	101
A854	HTAXI	A855	C	J8C10	31		DBASE	102
A855	GASF13	A856	C	J8C10	31		DBASE	103
A856	DARM	A857	C	J8C10	31		DBASE	104
A857	HEOPT2	A858	C	J8C10	31		DBASE	105
A858	HTAXI	A859	C	J8C10	31		DBASE	106
A859	Z-1-3	A860	C	J8C10	31		DBASE	107
A860	HEOPT2	A861	C	J8C10	31		DBASE	108
A861	Z-1-3	A862	S	J8C10	31		DBASE	109
A862	CALJK1	A863	C	J8C10	31		DBASE	110
A863	OLGUM1		C	J8C10	31		DBASE	111
				J8C10	31	AIR-AIR FIRST TO LAST	DBASE	111
A864	CALPRE	A865	C	J8C10	31		DBASE	112
A865	MACH	A866	C	J8C10	31		DBASE	113
A866	MUNCH	A867	C	J8C10	31		DBASE	114
A867	MSTRT2	A868	C	J8C10	31		DBASE	115
A868	DCEMT2	A869	C	J8C10	31		DBASE	116
A869	DCEMT2	A870	C	J8C10	31		DBASE	117
A870	CALJK2	A871	C	J8C10	31		DBASE	118
A871	CALJK2	A872	C	J8C10	31		DBASE	119
A872	CALLOM	A873	C	J8C10	31		DBASE	120
A873	CALLS1	A874	C	J8C10	31		DBASE	121
A874	JTAXI	A875	C	J8C10	31		DBASE	122
A875	HEOPT2	A876	C	J8C10	31		DBASE	123
A876	Z-1-3	A877	C	J8C10	31		DBASE	124
A877	HEOPT2	A878	C	J8C10	31		DBASE	125
A878	Z-1-3	A879	C	J8C10	31		DBASE	126
A879	HEOPT2	A880	C	J8C10	31		DBASE	127
A880	Z-1-3	A881	C	J8C10	31		DBASE	128
A881	HEOPT2	A882	C	J8C10	31		DBASE	129

BB117	HPOST1	0	00010	31	DBASE	130	
BB117	HPOST2	0	00010	31	DBASE	131	
BB117	SALEG1	44114	0	00010	31	DBASE	132
BB113	SALJK1	44119	-	00010	31	DBASE	133
BB113	SALLS1	44120	0	00010	31	DBASE	134
BB113	SALGU1	-	-	00010	31	DBASE	135
		4	00010	CONVERSION TNG MISSION FIRST TO TURN	00010	136	
CON1	SALLEP1	CON12	0	00010	31	DBASE	137
CON2	MJUN14	CON13	0	00010	31	DBASE	138
CON1	HST-T1	CON14	25	00010	31	DBASE	139
CON3	HST-T2	CON1	75	00010	31	DBASE	140
CON1	DT-T1	-	-	00010	31	DBASE	141
CON1	SALEG2	CON45	0	00010	31	DBASE	142
CON5	ZL-JK1	CON46	0	00010	31	DBASE	143
CON6	CALLD1	CON47	0	00010	31	DBASE	144
CON7	SALLS1	CON48	0	00010	31	DBASE	145
CON8	JT-XI	CON49	0	00010	31	DBASE	146
CON9	MEGPG1	CON50	0	00010	31	DBASE	147
CON11	ZL-JK1	CON51	0	00010	31	DBASE	148
CON11	MEGRIN	CON52	0	00010	31	DBASE	149
CON11	DCR-T2	-	-	00010	31	DBASE	150
CON12	MTAXI	CON53	0	00010	31	DBASE	151
CON13	SALJK1	CON54	0	00010	31	DBASE	152
CON14	MTHRU1	-	-	00010	31	DBASE	153
CON14	MTHRU2	0	00010	31	DBASE	154	
CON15	SALEG1	CON55	0	00010	31	DBASE	155
CON15	SALJK1	CON56	0	00010	31	DBASE	156
CON15	ZALLS1	-	-	00010	31	DBASE	157
		1	00010	CONVERSION TNG MISSION TURN TO LAST	00010	158	
CON1	MJUNCH	CON57	0	00010	31	DBASE	159
CON11	HST-T1	CON58	25	00010	31	DBASE	160
CON11	HST-T2	CON59	75	00010	31	DBASE	161
CON32	DCR-T1	-	-	00010	31	DBASE	162
CON32	SALEG2	CON60	0	00010	31	DBASE	163
CON33	CALLD1	CON61	0	00010	31	DBASE	164
CON4	SALLM1	CON62	0	00010	31	DBASE	165
CON35	SALLS1	CON63	0	00010	31	DBASE	166
CON35	JTAXI	CON64	0	00010	31	DBASE	167
CON37	MEGPG1	CON65	0	00010	31	DBASE	168
CON38	ZL-JK1	CON66	0	00010	31	DBASE	169
CON39	MEGRIN	CON67	0	00010	31	DBASE	170
CON39	DCR-T2	-	-	00010	31	DBASE	171
CON41	MTAXI	CON68	0	00010	31	DBASE	172
CON41	GASF11	CON69	0	00010	31	DBASE	173
CON42	HPOST1	-	-	00010	31	DBASE	174
CON42	HPOST2	0	00010	31	DBASE	175	
CON42	SALEG1	CON70	0	00010	31	DBASE	176
CON43	SALJK1	CON71	0	00010	31	DBASE	177
CON44	SALLS1	-	-	00010	31	DBASE	178
		4	00010	CONVERSION TNG MISSION TURN TO TURN	00010	179	
CON1	MJUNCH	CON72	0	00010	31	DBASE	180
CON1	HST-T1	CON73	25	00010	31	DBASE	181
CON1	HST-T2	CON72	75	00010	31	DBASE	182
CON2	DCR-T1	-	-	00010	31	DBASE	183
CON2	SALEG2	CON73	0	00010	31	DBASE	184
CON3	CALLD1	CON74	0	00010	31	DBASE	185
CON4	SALLM1	CON75	0	00010	31	DBASE	186
CON5	SALLS1	CON76	0	00010	31	DBASE	187
CON6	JTAXI	CON77	0	00010	31	DBASE	188
CON7	MEGRIN	CON78	0	00010	31	DBASE	189
CON8	ZL-JK1	CON59	0	00010	31	DBASE	190
CON8	MEGPG1	CON60	0	00010	31	DBASE	191
CON8	DCR-T2	-	-	00010	31	DBASE	192
CON1	MTAXI	CON61	0	00010	31	DBASE	193
CON1	GASF11	CON62	0	00010	31	DBASE	194
CON62	MTHRU1	-	-	00010	31	DBASE	195

CON62	WTMPU2	0	66010	31	OBASE	196	
CON62	CALEG1 CON62	0	66011	31	OBASE	197	
CON63	SALUKI CCN164	0	66012	31	OBASE	198	
CON6-	CALLS1	0	66013	31	OBASE	199	
CON112	CALPSE CCN101	0	66014	31	OBASE	200	
CON112	MUNTA CCN102	0	66015	31	OBASE	201	
CON112	MSTRT2 CON113 E	75	66016	31	OBASE	202	
CON112	MSTRT1 CON113 E	25	66017	31	OBASE	203	
CON113	DC2HT1	0	66018	31	OBASE	204	
CON113	DC2HT2 CON114	0	66019	31	OBASE	205	
CON113	DC2LX2 CON115	0	66020	31	OBASE	206	
CON113	DC2LX3 CON115	0	66021	31	OBASE	207	
CON113	CALLE1 CON117	0	66022	31	OBASE	208	
CON117	ITAX1 CON118	0	66023	31	OBASE	213	
CON115	ME2RD CON119	0	66024	31	OBASE	210	
CON115	ZI1 CON119	0	66025	31	OBASE	211	
CON111	MEOPIN CON111	0	66026	31	OBASE	212	
CON111	DC2HT2	0	66027	31	OBASE	213	
CON111	DC2LX1 CON112	0	66028	31	OBASE	214	
CON112	GAFF1 CON113	0	66029	31	OBASE	215	
CON113	HPST1	0	66030	31	OBASE	216	
CON113	HPST2	0	66031	31	OBASE	217	
CON113	CALEG1 CON114	0	66032	31	OBASE	218	
CON113	DC2LX1 CON115	0	66033	31	OBASE	219	
CON115	CALLE1	0	66034	31	OBASE	219	
CON115	CALLS1	0	66035	31	OBASE	220	
SCHEDULED WASH TODAY							
JU103	ZI1 JU104 S	0	66036	11	OBASE	221	
JU103	DC2HT2	0	66037	31	OBASE	222	
JU104	JTOMC JU105	0	66038	32	4 29L 5-31X1	OBASE	224
JU105	JPRE2 JU106	0	66039	32	10 29L 1431X1 1TUG	OBASE	225
JU105	JWASH1 JU107	0	66040	32	30 29L 3431X1 1WRACK	OBASE	226
JU107	J22 JU108	0	66041	32	25 29L 1531X-	OBASE	227
JU107	JLUB	0	66042	32	10 29L 1-31X1	OBASE	228
JU109	JTOMA2	0	66043	32	10 29L 1-31X1	OBASE	229
CTANK HANG CENTERLINE EXTERNAL TANK							
TANK1	FTANK TANK1	0	1337	CTANK 31	OBASE	230	
TANK1	DMHGT TANK2	0	CTANK 31	15 29L 3431X1	OBASE	231	
TANK2	DC2HT2 TANK3	0	CTANK 31	OBASE	232		
TANK3	CALPSE TANK4	0	CTANK 31	OBASE	233		
TANK4	DC2HT2 TANK5	0	CTANK 31	4 29L 2432Z0	OBASE	235	
TANK5	GASF15	0	CTANK 31	OBASE	236		
F-15 PHASE INFO FROM TEST ATKINS AND SSGT SOUNDS AT LUKE AFB ARIZ APRIL 75							
4					OBASE	237	
4					OBASE	238	
4					OBASE	239	
4					OBASE	240	
4					OBASE	241	
4					OBASE	242	
PHASE	DC2HT2 PHASE 1	0	PHASE 32		OBASE	243	
PHASE	DC2HT2	0	PHASE 32		OBASE	244	
PHASE	DC2HT2 F-14SE	0	PHASE 32		OBASE	245	
PHASE	DC2HT2	0	PHASE 32		OBASE	246	
PHASE	DTANK PHASE1	0	PHASE 32	5 29L 3431X1	OBASE	247	
PHASE	HANGAR PHASE3	0	PHASE 32	5 29L 1431X1	OBASE	248	
PHASE	ZI1 PHASE1	0	PHASE 32		OBASE	249	
PHASE	FPH4S1 PHASE1	0	PHASE 32		OBASE	250	
PHASE	FPH4S1 PHASE1	0	PHASE 32	8 29L 5-31X1	OBASE	251	
PHASE	FPH4S3 PHASE1	0	PHASE 32	8 29L 5-31X1	OBASE	252	
PHASE	FPH4S5 PHASE1	0	PHASE 32	8 29L 5-31X1	OBASE	253	
PHASE	FPH4S5 FPH4S1	0	PHASE 32	8 29L 5-31X1	OBASE	254	
PHASE	FPH4S5 PHASE1	0	PHASE 32	4 29L 5-31X1	OBASE	255	
PHASE	FPH4S5 PHASE2	0	PHASE 32	3 29L 2-31X1	OBASE	256	
PHASE	FPH4S4	0	PHASE 32	5 29L 1531X1	OBASE	257	
PHASE	OPEN PHASE3	0	PHASE 32		OBASE	258	
PHASE	PJACK PHASE3	0	PHASE 32	5 29L 4-31X1	OBASE	259	
PHASE	PJACK PHASE3	0	PHASE 32	10 29L 2431P1 1421X2	OBASE	260	
PHASE	PJACK PHASE3	0	PHASE 32		OBASE	261	

PHB.26	33PFC1	PHB.07	S	PHASE	32	OBASE	262
PHB.17	PJ143	PHB.13	S	PHASE	32	OBASE	263
PHB.17	PDC	PHB.04	S	PHASE	32	OBASE	264
PHB.13	CFIG	PHB.19	S	PHASE	32	OBASE	265
PHB.16	CPAN	PHB.11	S	PHASE	32	OBASE	266
PHB.11	PTCH	PHB.11	S	PHASE	32	OBASE	267
PHB.11	P42I	PHB.12	S	PHASE	32	OBASE	268
PHB.12	P42I	PHB.13	S	PHASE	32	OBASE	269
PHB.12	PDU43	PHB.13	S	PHASE	32	OBASE	270
PHB.13	PTCHD			PHASE	32	OBASE	271
CPAN	PPAN1			PHASE	32	OBASE	272
CPAN	PPAN2			PHASE	32	OBASE	273
CPAN	PPAN3			PHASE	32	OBASE	274
CPAN	PPAN4			PHASE	32	OBASE	275
CSPEC1	LOCK1			PHASE	32	OBASE	276
CSPEC1	CLUB1			PHASE	32	OBASE	277
CSPEC1	PINST1			PHASE	32	OBASE	278
CSPEC1	PF101			PHASE	32	OBASE	279
CSPEC1	PF102			PHASE	32	OBASE	280
CSPEC1	PF103			PHASE	32	OBASE	281
CLUB1	LJ31			PHASE	32	OBASE	282
CLUB1	LJ32			PHASE	32	OBASE	283
CLUB1	LJ31			PHASE	32	OBASE	284
CLUB1	LJ32			PHASE	32	OBASE	285
CLUB1	LJ31			PHASE	32	OBASE	286
CLUB1	LJ32			PHASE	32	OBASE	287
CLUB1	LJ31			PHASE	32	OBASE	288
CLUB1	LJ32			PHASE	32	OBASE	289
CLUB1	LJ31			PHASE	32	OBASE	290
CLUB1	LJ32			PHASE	32	OBASE	291
CLUB1	LJ31			PHASE	32	OBASE	292
CLUB1	LJ32			PHASE	32	OBASE	293
CLUB1	LJ31			PHASE	32	OBASE	294
CLUB1	LJ32			PHASE	32	OBASE	295
CLUB1	LJ31			PHASE	32	OBASE	296
CLUB1	LJ32			PHASE	32	OBASE	297
CLUB1	LJ31			PHASE	32	OBASE	298
CLUB1	LJ32			PHASE	32	OBASE	299
CLUB1	LJ31			PHASE	32	OBASE	300
CLUB1	LJ32			PHASE	32	OBASE	301
CLUB1	LJ31			PHASE	32	OBASE	302
CLUB1	LJ32			PHASE	32	OBASE	303
CLUB1	LJ31			PHASE	32	OBASE	304
CLUB1	LJ32			PHASE	32	OBASE	305
CFIX	PFIX1			PHASE	32	OBASE	306
CFIX	PFIX2			PHASE	32	OBASE	307
CFIX	PFIX3			PHASE	32	OBASE	308
CLOCK1	LOCK1			PHASE	32	OBASE	309
CLOCK1	LOCK2			PHASE	32	OBASE	310
CLOCK1	LOCK2			PHASE	32	OBASE	311
CLOCK1	LOCK3			PHASE	32	OBASE	312
CLOCK1	LOCK3			PHASE	32	OBASE	313
CLOCK1	LOCK1			PHASE	32	OBASE	314
CLOCK1	LOCK1			PHASE	32	OBASE	315
CLOCK1	LOCK2			PHASE	32	OBASE	316
CLOCK1	LOCK-			PHASE	32	OBASE	317
CLOCK1	LOCK-			PHASE	32	OBASE	318
CLOCK1	LOCK5			PHASE	32	OBASE	319
CLOCK1	LOCK1			PHASE	32	OBASE	320
PHB.01	PSAFE	PHB.02	S	PHASE	32	OBASE	321
PHB.02	CPAN	PHB.03	S	PHASE	32	OBASE	322
PHB.03	CSPEC2	PHB.05	S	PHASE	32	OBASE	323
PHB.05	PDU43	PHB.06	S	PHASE	32	OBASE	324
PHB.06	PTC	PHB.06	S	PHASE	32	OBASE	325
PHB.06	CFIX	PHB.07	S	PHASE	32	OBASE	326
PHB.07	CPAN	PHB.08	S	PHASE	32	OBASE	327

PHB36 T3WGT	0	PHASE 32	5 29L 5431X1	DBASE 320
CSPEC2 P110T2	1	PHASE 32	1 29L 232532	DBASE 329
CSPEC2 PF/C1	3	PHASE 32		DBASE 330
CSPEC2 PHB37 PHE37	3	PHASE 32	11 29L 4-6277	DBASE 331
PHB39 SWAP1 PHB313	3	PHASE 32	11 29L 2-02X7	DBASE 332
PHB37 C1E257	1	PHASE 32	21 29L 4-6277	DBASE 333
CSPEC2 CL00K2	3	PHASE 32		DBASE 334
CSPEC2 PE-S22	1	PHASE 32	11 29L 1422X1	DBASE 335
CSPEC2 PHB22	3	PHASE 32	15 29L 1421X2	DBASE 336
CSPEC2 P15S	2	PHASE 32	11 29L 1432X2	DBASE 337
CSPEC2 CL132	2	PHASE 32		DBASE 338
CLU32 LJ31	1	PHASE 32		DBASE 339
CLU32 LJ31	0	PHASE 32		DBASE 340
CLU32 LJ31	2	PHASE 32		DBASE 341
CLU32 LJ31	0	PHASE 32		DBASE 342
CLU32 LJ31	2	PHASE 32		DBASE 343
CLU32 LJ31	3	PHASE 32		DBASE 344
CLU32 LJ31	2	PHASE 32		DBASE 345
CLU32 LJ31	3	PHASE 32		DBASE 346
CLU32 LJ31	2	PHASE 32		DBASE 347
CL00K2 LJ00K2	3	PHASE 32		DBASE 348
CLOCK2 LJ00K2	2	PHASE 32		DBASE 349
CLOCK2 LJ00K2	3	PHASE 32		DBASE 350
CLOCK2 LJ00K2	1	PHASE 32		DBASE 351
CLOCK2 LJ00K2	3	PHASE 32	10 29L 2431P1	DBASE 352
CLOCK2 LJ00K2	2	PHASE 32		DBASE 353
CLOCK2 LJ00K2	3	PHASE 32		DBASE 354
P1C12 PS4FE PHB312	2	PHASE 32		DBASE 355
PMC.12 CPIN PHB313	3	PHASE 32		DBASE 356
PMC.17 PECK P-CAN	2	PHASE 32	5 29L 143101 243101	DBASE 357
PMC.13 CSPEC3 PHB315	3	PHASE 32		DBASE 358
PMC.15 P73 PHB315	2	PHASE 32		DBASE 359
PMC.15 P73 PHB315	2	PHASE 32		DBASE 360
PMC.14 CFIV PHB317	2	PHASE 32		DBASE 361
PMC.17 CPIN PHB319	3	PHASE 32		DBASE 362
PMC.18 T3WGT	1	PHASE 32		DBASE 363
CSPEC3 PHB37 PHB33	3	PHASE 32	11 29L 3-6270	DBASE 364
PMC.15 SWAP2 PHB312	2	PHASE 32	11 29L 2432X0	DBASE 365
PMC.11 P4E259	3	PHASE 32	11 29L 3-6222	DBASE 366
CSPEC2 CL00K3	2	PHASE 32		DBASE 367
CSPEC2 CL00K3	3	PHASE 32		DBASE 368
CSPEC2 PEV32	1	PHASE 32	35 29L 1432X0	DBASE 369
CSPEC2 PDUH1 PHB311	3	PHASE 32		DBASE 370
PMC.11 PEV32	1	51 PHASE 32	5 29L 1-67X0	DBASE 371
PMC.11 PEV32	1	51 PHASE 32	21 29L 1-67X0	DBASE 372
CSPEC2 PEV32	4	51 PHASE 32	11 29L 2422X1	DBASE 373
CLOCK3 LJ00K3	3	PHASE 32		DBASE 374
CLOCK3 LJ00K3	3	PHASE 32		DBASE 375
CLOCK3 LJ00K3	2	PHASE 32		DBASE 376
CLOCK3 LJ00K3	2	PHASE 32	11 29L 1431P1	DBASE 377
CLOCK3 LJ00K7	3	PHASE 32		DBASE 378
CLOCK3 LJ00K7	2	PHASE 32		DBASE 379
CLU33 LJ31	3	PHASE 32		DBASE 380
CLU33 LJ31	2	PHASE 32		DBASE 381
CLU33 LJ32	3	PHASE 32		DBASE 382
CLU33 LJ32	2	PHASE 32		DBASE 383
CLU33 LJ32	3	PHASE 32		DBASE 384
CLU33 LJ32	2	PHASE 32		DBASE 385
CLU33 LJ32	3	PHASE 32		DBASE 386
CLU33 LJ32	2	PHASE 32		DBASE 387
CLU33 LJ32	3	PHASE 32		DBASE 388
CLU33 LJ32	2	PHASE 32		DBASE 389
PMC.12 CPIN PHB313	2	PHASE 32		DBASE 390
PMC.13 P4E259 PHB314	3	PHASE 32		DBASE 391

PH0101	SE-CAN PH0105	0	PHASE	32	16 29L 3-3101	094SE	394	
PH0102	SE-CAN PH0105	0	PHASE	32		094SE	395	
PH0103	SE-CAN PH0107	0	PHASE	32		094SE	396	
PH0104	PILOT CAN	0	PHASE	32		094SE	397	
PH0105	PILOT CAN	0	PHASE	32		094SE	398	
PH0106	PILOT CAN	0	PHASE	32		094SE	399	
PH0107	TJACUT	0	PHASE	32		094SE	400	
CSPE2-	CLOCK	0	PHASE	32		094SE	401	
CSPE3-	CLOCK	0	PHASE	32		094SE	402	
CSPE4-	CLOCK	0	PHASE	32		094SE	403	
CSPE5-	CLOCK	0	PHASE	32		094SE	404	
CSPE6-	CLOCK	0	PHASE	32	16 29L 1422X1	094SE	405	
CSPE7-	CLOCK	0	PHASE	32	16 29L 1421X2	094SE	406	
CSPE8-	CLOCK	0	PHASE	32	16 29L 1-23X0	094SE	407	
CSPE9-	CLOCK	0	PHASE	32	16 29L 1-32X0	094SE	408	
CLOCK-	CLOCK	0	PHASE	32		094SE	409	
CLOCK-	CLOCK	0	PHASE	32		094SE	410	
CLOCK-	CLOCK	0	PHASE	32		094SE	411	
CLOCK-	CLOCK	0	PHASE	32		094SE	412	
CLOCK-	CLOCK	0	PHASE	32		094SE	413	
CLOCK-	CLOCK	0	PHASE	32		094SE	414	
CLOCK-	CLOCK	0	PHASE	32		094SE	415	
CLUE+	LJ32	0	PHASE	32		094SE	416	
CLUE+	LJ32	0	PHASE	32		094SE	417	
CLUE+	LJ31	0	PHASE	32		094SE	418	
CLUE+	LJ31	0	PHASE	32		094SE	419	
CLUE+	LJ31	0	PHASE	32		094SE	420	
CLUE+	LJ31	0	PHASE	32		094SE	421	
CLUE+	LJ31	0	PHASE	32		094SE	422	
CLUE+	LJ31	0	PHASE	32		094SE	423	
CLUE+	LJ31	0	PHASE	32		094SE	424	
CLUE+	LJ31	0	PHASE	32		094SE	425	
CLUE+	LJ31	0	PHASE	32		094SE	426	
CLUE+	LJ31	0	PHASE	32		094SE	427	
CLUE+	LJ31	0	PHASE	32		094SE	428	
CLUE+	LJ31	0	PHASE	32		094SE	429	
CLUE+	LJ31	0	PHASE	32		094SE	430	
CCANP#	F7F	PH0111	H	PHASE	32		094SE	431
CCANP#	F7F	PH0111	H	PHASE	32		094SE	432
PH0111	E3E55	PH0112	0	PHASE	32	35 29L 2422X2	094SE	433
PH0112	E3E55	PH0113	0	PHASE	32	35 29L 2422X2	094SE	434
PH0113	E3E55	PH0114	0	PHASE	32	5 29L 1422X2	094SE	435
PH0114	E3E55	PH0105	0	PHASE	32	35 29L 2-22X2	094SE	436
PH0115	E3E55	PH0105	0	PHASE	32	35 29L 1-31P1	094SE	437
PH0221	E3E552	PH0222	0	PHASE	32	15 29L 2-22Y2	094SE	438
PH0222	E3E55	PH0223	0	PHASE	32	15 29L 2422X2	094SE	439
PH0223	E3E55	PH0224	0	PHASE	32	2 29L 1422X2	094SE	440
PH0224	E3E55	PH0225	0	PHASE	32	15 29L 2422X2	094SE	441
PH0225	E3E55	0	PHASE	32	18 29L 1431P1	094SE	442	
110.1	1	S11PA	P44P ACTUATORS TCI			094SE	443	
S11P	F311P1	S11P2	F	39.	S11PA 31	094SE	444	
S11P	F311P4	S11P2	0	S11PA	31	70 29L 1421X2	094SE	445
S11P2	F311P4	0	S11PA	31	10 29L 2421X2	094SE	446	
S11P2	J11P1	J11P3	0	S11PA	31		094SE	447
13M01	1	S13M0	WHEEL SPEED SENSOR TCI			094SE	448	
S13M1	F313M0	S13M1	F	150	S13M0 31	094SE	449	
S13M1	J313M0	S13M2	0	S13M0	31		094SE	450
S13M2	J313M0	S13M3	0	S13M0	31		094SE	451
S13M3	F313M0	I43MCA	0	S13M0	31	23 29L 2423X0	094SE	452
I43MCA	J11M01	0	S13M0	31	3 29L 1423X0	094SE	453	
I43M01	Q13M01	0	S13M0	31	5 29L 2423X0	094SE	454	
1-G01	4	S14G0	AILERON SERVOCYL TCI			094SE	455	
S14G1	F314G0	S14G1	F	39.	S14G0 31	094SE	456	
S14G1	Q314G0	S14G2	0	S14G0	31		094SE	457
S14G2	Q314G0	S14G3	0	S14G0	31		094SE	458
S14G3	CALGP1	S14G5	C	S14G0	31		094SE	459

S16G6	CALTU	S1+G5	3	S16G6	71			OBASE	46:
S16G6	PS16G6	T6-G6	0	S16G6	71	25 29L 2-62X2 1062	1TU22A	OBASE	461
			4	S23J1	31	514K 30XSCOPE 3TMN PHASES 25 77		OBASE	462
S23J1	F3271	S23J1	2	S23J1	71			OBASE	463
S23J1	VS23M1		0	S23J1	31	46 29L 2432X0		OBASE	464
			27M	S23J1		MAIN FUEL PUMP T71 15 77		OBASE	465
S23J1	F323M1	S23M1	F	S23M1	31			OBASE	466
S23J1	PS23M1	S23M1	0	S23M1	31	25 29L 2432X0		OBASE	467
S23J2	VS23M2	S23M2	0	S23M2	31	5 29L 3-32X0		OBASE	468
			27M	S23M2		LOX 6 DAY LEAK CHK		OBASE	469
S67J1	F3+71	S+7L1	F	S67J1	31			OBASE	470
S67J1	VS+71	S+7L1	0	S67J1	31	5 29L 1-32X1		OBASE	471
			4	S7EJ0		RACKS/LAUNCHERS TCI WHEN FIRED		OBASE	472
S75J1	F3751	S751	F	S751	31			OBASE	473
S75J2	VS24M3	S7512	0	S7503	31			OBASE	474
S75J2	F41501	S7512	0	S7511	31			OBASE	475
S75J3	VS75F4	S7514	0	S7503	31			OBASE	476
S7EJ1	VS7522	S7522	0	S7511	31			OBASE	477
			4	S75J1		ARM SYST CK WITH SP TEST EO		OBASE	478
S7EJ4	VS751	S751	0	S7511	31	25 29L 3-62X0 1061	1TU472	OBASE	479
			4	SGUN		F15 GUN SCHEDULED INSPECTIONS		OBASE	480
JGUW1	FSGUN	JGUW1	F	SGUN1	32			OBASE	481
JGUW1	DSGUN1	JGUW1	0	SGUN1	32			OBASE	482
JGUW2	DSGUN2	JGUW2	0	SGUN1	32			OBASE	483
JGUW2	DSGUN2	JGUW2	0	SGUN1	32			OBASE	484
			4	SGUN1		F15 15.01 RIG INSP REQUIREMENTS SGUN1		OBASE	485
JGUW3	VS7511	JGUW3	0	SGUN1	32	25 29L 3-62X1 1061	105	OBASE	486
JGUW3	VS5512	JGUW3	0	SGUN1	32	25 29L 2-62X0 1050	105	OBASE	487
JGUW3	VS5512	JGUW3	0	SGUN1	32	F15 15.01 RIG INSP REQUIREMENTS SGUN2		OBASE	488
JGUW4	VS5513	JGUW4	0	SGUN1	32	115 29L 3-62X1 1061	105	OBASE	489
JGUW4	VS5513	JGUW4	0	SGUN1	32	F15 25.01 RIG INSP REQUIREMENTS SGUN1		OBASE	490
JGUW5	FSGUN1	JGUW5	F	SGUN1	32			OBASE	491
JGUW5	DSGUN1	JGUW5	0	SGUN1	32			OBASE	492
			4	SGUN1		F15 15.01 RIG INSP REQUIREMENTS SGUN2		OBASE	493
JGUW6	VS5514	JGUW6	0	SGUN1	32	41 29L 2-62X1 1061	105	OBASE	494
			4	11A33		FWD FUS		OBASE	495
			4	11A33		F4E 111A 3 C D DATA USED		OBASE	496
			4	11A33		MSG DICELLO LUKE PH 2733 VERIFIED		OBASE	497
			4	11A33		EXPECT OVERALL NSPM AS F+E		OBASE	498
			4	11A33		SCREWS B1 DUE TO OVER TORQUE		OBASE	499
			4	11A33		PANELS CRACKING		OBASE	500
			4	11A33		BOOM CAP FAILING DRAUGS ON LANDING		OBASE	501
			4	11A33		CONSTANT REPAIRS DRG POC		OBASE	502
			4	11A33		F15 MS34A 22		OBASE	503
			4	11A33		FWD FUSELAGE F15		OBASE	504
A1AJ1	F11AJ1	A1AJ1	F	11AJ0	21			OBASE	504
A1AJ1	PS11AJ1	A1AJ1	0	11AJ0	21	22 29L 2431X1		OBASE	505
A1AJ1	M11AJ1	A1AJ1	0	11AJ0	21	19 29L 1431X1		OBASE	506
A1AJ1	F11AJ2	A1AJ2	0	11AJ0	21	16 29L 1531X1		OBASE	507
A1AJ2	M11AJ1	A1AJ1	0	11AJ0	21	18 29L 1531X1		OBASE	508
A1AJ2	SHDF	S11AJ0	0	11AJ0	21			OBASE	509
S11AJ0	L11AJ1	I11AJ1	0	11AJ0	21			OBASE	510
			4	11AJ0		FARING MOUTLE BLAST		OBASE	511
I11AJ1	M11AJ1	I11AJ1	E	11AJ0	23	25 29L 2531X3		OBASE	512
I11AJ1	M11AJ1	I11AJ1	0	11AJ0	23	25 29L 1531X3		OBASE	513
I11AJ1	M11AJ2	I11AJ2	E	11AJ0	23	46 29L 1531X3 146221		OBASE	514
I11AJ1	M11AJ2	I11AJ2	0	11AJ0	21			OBASE	515
S11AJ0	L11AJ2	I11AJ2	0	11AJ0	23			OBASE	516
			4	11AJ0		ACCEES OCORS		OBASE	517
I11AJ2	M11AJ2	I11AJ2	E	11AJ0	23	37 29L 1531X3		OBASE	518
I11AJ2	M11AJ2	I11AJ2	0	11AJ0	23	35 29L 1531X3		OBASE	519
I11AJ2	Q11AJ2	I11AJ2	0	11AJ0	21			OBASE	520
			4	11AJ0		CENTER FUSELAGE		OBASE	521
			4	11AJ0		F4E 111F 6 H DATA USED		OBASE	522
			4	11AJ0		F15 MS34A 22		OBASE	523
			4	11AJ0		THIS APEARS MS34A WILL FFGS GET WORSE		OBASE	524
			4	11AJ0		CTR FUSELAGE F15		OBASE	525

A10C1	F110J1	A10D1	F	6	110J1	21			DPAE	526
A10J1	F110J1	A10C1	E	62	110J1	21	22 29L 1531X1		DPAE	527
A10C1	M110J1		E	12	110J1	21	12 29L 1531X1		DPAE	528
A10J1	M110J1		E	55	110J1	21	14 29L 2531X3		DPAE	529
A10J1	M110J1		E	46	110J1	21	16 29L 1531X1		DPAE	530
A10J1	S10F	S410C1	J		110J1	23			DPAE	531
S410C1	L110A1	I110C1	C	14-67	110J1	23			DPAE	532
	L110A1		4		110J1	23	CTR FUSELAGE		DPAE	533
I410C1	4110A1		E	95	110J1	23	34 29L 2531X3		DPAE	534
I410C1	M110C1		E	CS	110J1	23	15 29L 1531X3		DPAE	535
I410C1	M110C1		J		110J1	21			DPAE	536
S410C1	L110C1	I410C1	C	-5161	110J1	23			DPAE	537
	L110G1		4		110G1		ACCESS DOORS		DPAE	538
I410C1	M110G1		E	11	110G1	23	17 29L 1531X1		DPAE	539
I410C1	M110G1		E	63	110G1	23	34 29L 2531X3		DPAE	540
I410C1	M110G1		E	37	110G1	23	16 29L 1531X3		DPAE	541
I410C1	Q110G1		C		110G1	21			DPAE	542
			4		110G1		AFT FUSELAGE		DPAE	543
			4		110G1	F-E 111K L			DPAE	544
			4		110G1	F15 MS3MA 9			DPAE	545
			4		110G1	AFT FUSELAGE F15			DPAE	546
A1GJ1	F11GJ1	A1GJ1	F	F	110G1	21			DPAE	547
A1GJ1	R11GJ1	A1GJ2	E	CS	110G1	21	28 29L 2531X1		DPAE	548
A1GJ1	M11GJ1		E	5-	110G1	21	8 29L 1531X1		DPAE	549
A1GJ1	M11GJ1		E	45	110G1	21	10 29L 1531X1		DPAE	550
A1GJ1	M11GJ1		E	43	110G1	21	16 29L 2531X3		DPAE	551
A1GJ2	SHOP	S11GJ1	C		110G1	23			DPAE	552
S41GJ1	L11GJ1	I41GJ1	C	-1635	110G1	23			DPAE	553
	L11GJ1		4		110G1	23	AFT FUSELAGE		DPAE	554
I41GJ1	M11GJ1		E	24	110G1	23	23 29L 1531X1		DPAE	555
I41GJ1	M11GJ1		E	67	110G1	23	25 29L 1531X3		DPAE	556
I41GJ1	M11GJ1		E	CS	110G1	23	26 29L 1531X1		DPAE	557
I41GJ1	Q11GJ1		E		110G1	21			DPAE	558
S41GJ1	L11GJ1	I41GJ1	C	20122	110G1	23			DPAE	559
	L11GJ1		4		110G1		ACCESS DOORS		DPAE	560
I41GJ1	M11GJ1		C	110G1	23	19 29L 2531X3		DPAE	561	
I41GJ1	Q11GJ1		C	110G1	21			DPAE	562	
			4		11KJ1		WING ASSY F15		DPAE	563
			4		11KJ1		CRACKS IN WINGS SKIN BEING LOOKED		DPAE	564
			4		11KJ1		INTO PW ENGINEERS		DPAE	565
			4		11KJ1	F-E 112 USED FOR CO-PASIFIABILITY			DPAE	566
			4		11KJ1	MSGT DUCOLLO LUKE 3-FET VOL PH2787			DPAE	567
			4		11KJ1	F15 DATA SHOWS 33 MS3MA AUG75			DPAE	568
			4		11KJ1	WING ASSY F15			DPAE	569
A1KJ1	F11KJ1	A1KJ1	F	2	11KJ1	21			DPAE	570
A1KJ1	D11KJ1	A1KJ1	E	15	11KJ1	21			DPAE	571
A1KJ1	M11KJ1		E	30	11KJ1	21	120 29L 2424X0		DPAE	572
A1KJ1	M11KJ1		E	70	11KJ1	21	29 29L 2424X0		DPAE	573
A1KJ1	R11KJ1	A1KJ2	E	21	11KJ1	21	93 29L 4431C1		DPAE	574
A1KJ1	R11KJ1	A1KJ2	E	22	11KJ1	21	25 29L 1-31X1		DPAE	575
A1KJ1	M11KJ1		E	92	11KJ1	21	10 29L 1531X3		DPAE	576
A1KJ1	M11KJ2		E	41	11KJ1	21	18 29L 2531X3		DPAE	577
A1KJ2	SHOP	S11KJ1	C		11KJ1	23			DPAE	578
S41KJ1	L11KJ1	I41KJ1	C	-1655	11KJ1	23			DPAE	579
	L11KJ1		4		11KJ1		LEADING EDGE TRAILING EDGE		DPAE	580
I41KJ1	M11KJ1		E	66	11KJ1	23	23 29L 1531X3		DPAE	581
I41KJ1	M11KJ2		E	54	11KJ1	23	15 29L 2531X3		DPAE	582
I41KJ1	Q11KJ1		E	11-01	11KJ1	21	95 29L 4431C1		DPAE	583
S41KJ1	L11KJ1	I41KJ1	C	0019	11KJ1	23			DPAE	584
	L11KJ1		4		11KJ1		WING ACCESS PROVISIONS		DPAE	585
I41KJ1	M11KJ1		C	11KJ1	23	18 29L 2424X3		DPAE	586	
I41KJ1	Q11KJ1		E	11KJ1	21	28 29L 1431X1		DPAE	587	
			4		11P00		AIR INDUCTION SYS IS EXPECTED TO		DPAE	588
			4		11P00		HAVE HIGHER FAIL RATE THAN F15		DPAE	589
			H		11P00		REASON IS MORE CYLINDERS & SERVOS		DPAE	590
			4		11P00		F15 DATA SHOWS 18 MS3MA AUG75		DPAE	591

			H	11000	F4E 113 DATA USED 90 43PM	DBASE	592
			M	11010	A COMPOSITE OF F4E A F4F FOR SHOP	DBASE	593
				11010	AIR INSUCTION SYS F15	DBASE	594
				11010		DBASE	595
A1P01	E1P01	A1P01	E	22 11010 21		DBASE	596
A1P01	R1P01	E1P02	E	02 11010 21	29 29L 2326X2	DBASE	597
A1P01	R1P01	E1P02	E	03 11010 21	30 29L 2326X2	DBASE	598
A1P01	R1P01	E1P02	E	04 11010 21	31 29L 2326X2	DBASE	599
A1P01	R1P01	E1P02	E	05 11010 21	32 29L 2326X2	DBASE	600
A1P01	R1P01	E1P02	E	06 11010 21	33 29L 2326X2	DBASE	601
A1P01	R1P01	E1P02	E	07 11010 21	34 29L 2326X2	DBASE	602
A1P01	R1P01	E1P02	E	08 11010 21	35 29L 2326X2	DBASE	603
A1P01	R1P01	E1P02	E	09 11010 21	36 29L 2326X2	DBASE	604
A1P01	R1P01	E1P02	E	10 11010 21	37 29L 2326X2	DBASE	605
A1P01	R1P01	E1P02	E	11 11010 21	38 29L 2326X2	DBASE	606
A1P01	R1P01	E1P02	E	12 11010 21	39 29L 2326X2	DBASE	607
A1P01	R1P01	E1P02	E	13 11010 21	40 29L 2326X2	DBASE	608
A1P01	R1P01	E1P02	E	14 11010 21	41 29L 2326X2	DBASE	609
A1P01	R1P01	E1P02	E	15 11010 21	42 29L 2326X2	DBASE	610
A1P01	R1P01	E1P02	E	16 11010 21	43 29L 2326X2	DBASE	611
A1P01	R1P01	E1P02	E	17 11010 21	44 29L 2326X2	DBASE	612
A1P01	R1P01	E1P02	E	18 11010 21	45 29L 2326X2	DBASE	613
A1P01	R1P01	E1P02	E	19 11010 21	46 29L 2326X2	DBASE	614
A1P01	R1P01	E1P02	E	20 11010 21	47 29L 2326X2	DBASE	615
A1P01	R1P01	E1P02	E	21 11010 21	48 29L 2326X2	DBASE	616
A1P01	R1P01	E1P02	E	22 11010 21	49 29L 2326X2	DBASE	617
			H	12A00	F-E 121 DATA USED	DBASE	618
			M	12A00	F4E 45PM 21	DBASE	619
			M	12A00	MSG DICELLO LUKE PH 2793 SHEETMOL	DBASE	620
			M	12A00	TSG SWEEP LUKE 19G PH 2466	DBASE	621
			M	12A00	COCKPIT FURNISHINGS F15	DBASE	622
A2A01	F12A01	A2A01	F	102 12A00 21		DBASE	623
A2A01	F12A01	A2A01	F	05 12A00 21	11 29L 1431X1	DBASE	624
A2A01	F12A01	A2A01	F	07 12A00 21	12 29L 1431X1	DBASE	625
A2A01	F12A01	A2A01	F	08 12A00 21	13 29L 1431X1	DBASE	626
A2A01	F12A01	A2A01	F	09 12A00 21	14 29L 1431X1	DBASE	627
A2A01	F12A01	A2A01	F	10 12A00 21	15 29L 1431X1	DBASE	628
A2A01	F12A01	A2A01	F	11 12A00 21	16 29L 1431X1	DBASE	629
A2A01	F12A01	A2A01	F	12 12A00 21	17 29L 1431X1	DBASE	630
A2A01	F12A01	A2A01	F	13 12A00 21	18 29L 1431X1	DBASE	631
A2A01	F12A01	A2A01	F	14 12A00 21	19 29L 1431X1	DBASE	632
A2A01	F12A01	A2A01	F	15 12A00 21	20 29L 1431X1	DBASE	633
A2A01	F12A01	A2A01	F	16 12A00 21	GLARE SHIELD INS PAN FWD CREW LH RH C	DBASE	634
A2A01	F12A01	A2A01	F	17 12A00 21	19 29L 1531X3	DBASE	635
A2A01	F12A01	A2A01	F	18 12A00 21		DBASE	636
			H	12A00	EJECTION SEAT	DBASE	637
			M	12A00	A7D 123 DATA USED	DBASE	638
			M	12A00	ASSUME NO SEAT REMOVAL EXCEPT SCHED	DBASE	639
			M	12A00	NO ITEM TO SHOP ITEM FAILING A7D IS	DBASE	640
			M	12A00	NOT ON F15 F15 MS31A -22	DBASE	641
			H	12F00	TSG JENSEN LUKE PH 2325 EXPRESS	DBASE	642
			H	12F00	SSG SCHNEIDER EDWARD EXPRESS	DBASE	643
			H	12F00	MSG GREGORY LUKE PH 2325 EXPRESS VER	DBASE	644
			H	12F00	MSG MILLER LUKE PH 2325 EXPRESS	DBASE	645
			M	12E00	EJECTION SEAT F15	DBASE	646
A2B01	F12B01	A2B01	F	125 12E00 21		DBASE	647
A2B01	F12B01	A2B01	F	126 12E00 21		DBASE	648
A2B01	F12B01	A2B01	F	127 12E00 21		DBASE	649
A2B01	F12B01	A2B01	F	128 12E00 21		DBASE	650
A2B01	F12B01	A2B01	F	129 12E00 21		DBASE	651
A2B01	F12B01	A2B01	F	130 12E00 21		DBASE	652
A2B01	F12B01	A2B01	F	131 12E00 21		DBASE	653
			H	12C00	CANOPY	DBASE	654
			H	12C00	F4E 123 DATA USED	DBASE	655
			H	12C00	V12C01 IS PRES OK	DBASE	656
			H	12C00	HYD OPERATED CANOPY	DBASE	657

4	12030	MSG DICELLO LUKE PH 2793 SHEET NOL	DBASE	659
4	12030	TSG JENSEN LUKE EGRESS	DBASE	659
4	12031	SSG SCHNEIDER EDWARDS EGRESS	DBASE	660
4	12031	F12014 CANOPY MUCH LARGER THAN	DBASE	661
4	12031	F12014 CANOPY IS 5MS WLL = DOUBLE F4E	DBASE	662
4	12031	CANOPY MAT 2PCES FROM ACCUM	DBASE	663
4	12031	AFTER THAT A HANG PUMP UP OF HYD RULE	DBASE	664
4	12031	F12031 MS3MA +2	DBASE	665
4	12031	CANOPY ASSY F15	DBASE	666
A2C12	12031	42001 2	DBASE	667
A2C12	12031	12031 21	DBASE	668
S2C11	12031	12031 21	DBASE	669
A2C13	12031	42012 2	DBASE	670
A2C13	12031	12031 21	DBASE	671
A2C13	12031	12031 21	DBASE	672
A2C13	12031	12031 21	DBASE	673
A2C13	12031	12031 21	DBASE	674
A2C13	12031	12031 21	DBASE	675
A2C13	12031	12031 21	DBASE	676
A2C13	12031	12031 21	DBASE	677
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A2C12	12031	12031 21	DBASE	680
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A2C12	12031	12031 21	DBASE	683
A2C12	12031	12031 21	DBASE	684
S2C11	12031	12031 21	DBASE	685
L1203	4	12030 CANOPY PARTS	DBASE	686
I12C11	12031	12031 23	DBASE	687
I12C11	12031	12031 23	DBASE	688
I12C11	12031	12031 23	DBASE	689
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I12C11	12031	12031 23	DBASE	702
I12C11	12031	12031 23	DBASE	703
A3A12	F13A12	A3A12 21	DBASE	704
A3A12	02P4H7	A3A01 2	DBASE	705
A3A12	02P4H7	A3A02 2	DBASE	706
A3A12	CALGPJ	A3A02 2	DBASE	707
A3A12	CALTTJ	A3A02 2	DBASE	708
A3A12	02P4H7	A3A02 2	DBASE	709
A3A12	02P4H7	A3A02 2	DBASE	710
A3A12	02P4H7	A3A02 2	DBASE	711
A3A12	CALTTJ	A3A02 2	DBASE	712
A3A12	02P4H7	A3A02 2	DBASE	713
A3A12	02P4H7	A3A02 2	DBASE	714
A3A12	CALGPJ	A3A02 2	DBASE	715
A3A12	CALTTJ	A3A02 2	DBASE	716
A3A12	R13A12	A3A02 21	DBASE	717
A3A12	R13A12	A3A02 21	DBASE	718
A3A12	R13A12	A3A02 21	DBASE	719
A3A12	R13A12	A3A02 21	DBASE	720
A3A12	R13A12	A3A02 21	DBASE	721
A3A12	R13A12	A3A02 21	DBASE	722
A3A12	R13A12	A3A02 21	DBASE	723

A3A31 413A13	E	05 13A02 21	16 29L 1431Y1	DBASE 724	
A3A31 413A13	E	27 17A01 21	17 29L 2531Y3	DBASE 725	
A3A32 VJACK	D	13A05 21	17 29L 4431Y1 1360	DBASE 726	
A3A33 VJACK	D	13A05 21		DBASE 727	
A3A34 VJACK	D	13A06 21		DBASE 728	
A3A35 VJACK	D	13A06 21	15 29L 2431X1 1261	DBASE 729	
A3A36 VJACK	D	13A06 21		DBASE 729	
A3A37 V13A43	D	13A06 21		DBASE 730	
A3A38 SHOP	S	13A06 21		DBASE 731	
S43A01 L13A01 23A01 6	-137	13A06 23		DBASE 732	
A3A39 13A01	H	13A06	MAIN LG MECH COMPTIS 13A1 THRU 13A6	DBASE 733	
I3A391 V13A01	E	57 13A06 23	15 29L 2-21X2	DBASE 734	
I3A391 V13A01	E	25 17A01 23	15 29L 2531Y3	DBASE 735	
I3A391 <13A01	E	25 13A06 23	21 29L 1531Y1	DBASE 736	
I3A391 213A01	I	13A06 21	24 29L 2-21Y2	DBASE 737	
S43A01 L13A01 23A01 G	1761	13A06 23		DBASE 738	
A3A391 13A01	H	13A06	UPLATCH MECH ETC 13A1	DBASE 739	
I3A391 N13A01	E	67 13A06 23	16 29L 1531X1	DBASE 740	
I3A391 N13A01	E	63 17A01 23	17 29L 2531Y1	DBASE 741	
I3A391 213A01	D	13A06 21		DBASE 742	
	H	13A06	NOSE GEAR TO INCLUDE STEERING	DBASE 743	
	H	13A06	F4E 135 DATA USED	DBASE 744	
	H	13A06	V TASK APE FOR JACKING / RETRACT OK	DBASE 745	
	H	13A06	F15 MS241 49	DBASE 746	
	H	13A06	HOSE RELENT TIME APE	DBASE 747	
	H	13A06	SHIMMY PROBLEM STARTING	DBASE 748	
	H	13A06	NOSE LG / STEER F15	DBASE 749	
A3B11 F13B1 A3B11	E	26 13B01 21		DBASE 750	
A3B11 D23A07	E	15 13B01 21		DBASE 751	
A3B11 D23A07	E	15 13B01 21		DBASE 752	
A3B11 D23A07	E	15 13B01 21		DBASE 753	
A3B11 D23A07	E	15 13B01 21		DBASE 754	
A3B11 D23A07	E	15 13B01 21		DBASE 755	
A3B11 D23A07	E	15 13B01 21		DBASE 756	
A3B11 D23A07	E	15 13B01 21		DBASE 757	
A3B11 D23A07	E	15 13B01 21		DBASE 758	
A3B11 D23A07	E	15 13B01 21		DBASE 759	
A3B11 D23A07	E	15 13B01 21		DBASE 760	
A3B11 D23A07	E	15 13B01 21		DBASE 761	
A3B11 D23A07	E	15 13B01 21		DBASE 762	
A3B11 D23A07	E	15 13B01 21		DBASE 763	
A3B11 D23A07	E	15 13B01 21	39 29L 2421X2 1351	1TU228	DBASE 764
A3B11 D23A07	E	15 13B01 21	20 29L 2-23X3 1350	1TU229	DBASE 765
A3B11 D23A07	E	15 13B01 21	11 29L 1-3-Y1 1350	1TU229	DBASE 766
A3B11 D23A07	E	15 13B01 21	13 29L 2421Y2	DBASE 767	
A3B11 D23A07	E	15 13B01 21	14 29L 1531Y3	DBASE 768	
A3B11 D23A07	E	02 13B01 21	15 29L 1-31X1	DBASE 769	
A3B11 D23A07	E	3 13B01 21	13 29L 2531Y3	DBASE 770	
A3B11 V13B1	D	13B01 21	15 29L 2-31Y1	DBASE 771	
A3B11 V13B1	D	3 13B01 21	13 29L 2423X0	DBASE 771	
A3B11 V13B1	D	13B01 21		DBASE 772	
A3B11 V13B1	D	13B01 21		DBASE 773	
A3B11 V13B1	D	13B01 21		DBASE 774	
A3B11 V13B1	D	13B01 21		DBASE 775	
A3B11 V13B1	D	13B01 21		DBASE 776	
A3B11 V13B1	D	13B01 21		DBASE 777	
A3B11 V13B1	D	13B01 21		DBASE 778	
A3B11 V13B1	D	13B01 21		DBASE 779	
S43B01 S43B01	S	13B01 21		DBASE 780	
S43B01 L13B1 113B01	D	13B01 21		DBASE 781	
L13B01	H	13B01	NOSE GEAR / STEP COMPTIS	DBASE 782	
I43B01 V13B1	E	03 13B01 23	16 29L 2421X2	DBASE 783	
I43B01 V13B1	E	76 13B01 23	13 29L 1-21Y2	DBASE 784	
I43B01 V13B1	E	07 13B01 23	10 29L 1531Y3	DBASE 785	
I43B01 <13B1	E	13 13B01 23	15 24L 2532X0	DBASE 786	
I43B01 213B01	I	13B01 21	39 29L 2423X0	DBASE 785	
	H	13C01	ARRESTING HOOK SYS	DBASE 786	
	H	13C01	F4E 135XX DATA USED	DBASE 787	
	H	13C01	F15MS3MA NO FAILURE	DBASE 788	
	H	13C01	ARREST HOOK SYS F15	DBASE 789	

A3C01	F13C03	A3C01	F	16-	13C04	21			DBASE	791
A3C01	M13C01	A3C02	E	4-	13C04	21	33 29L 2421X2		DBASE	791
A3C01	M13C01			12	13C04	21	16 29L 2421X2		DBASE	792
A3C01	M13C01			6-	13C04	21	16 29L 2423X0		DBASE	793
A3C01	M13C01	A3C02	E	64	13C04	21	32 29L 1-31X1		DBASE	794
A3C01	M13C01			15	13C04	21	13 29L 1-31Y1		DBASE	795
A3C01	M13C01			2-	13C04	21	19 29L 1531X0		DBASE	796
A3C01	M13C01			22	13C04	21	16 29L 2531X3		DBASE	797
A3C01	S-2P	S43C03	D		13C04	23			DBASE	798
S43C03	L13C01	A3C04	G	121	13C04	23			DBASE	799
	L13C04			4	13C04		ARRESTING HOOK ASY		DBASE	800
I43C01	M13C01			5-	13C04	*23	67 29L 2421X2		DBASE	801
I43C01	M13C01			31	13C04	*23	19 29L 1-31X2		DBASE	802
I43C01	M13C01			15	13C04	*23	13 29L 1531X0		DBASE	803
I43C01	M13C01				13C04	21	33 29L 2421X2		DBASE	804
SAC01	L13C01	I13C01	G	156	13C04	23			DBASE	805
	L13C04			1	13C04		DAMPER ASY		DBASE	806
I43C01	M13C01			32	13C04	*23	21 29L 1531X3		DBASE	807
I43C01	M13C01			63	13C04	*23	21 29L 1531X1		DBASE	808
I43C01	M13C01				13C04	21	32 29L 1431Y1		DBASE	809
	L13C04			4	13C04		NCC		DBASE	810
SAC01	L13C01	I13C01	G	127	13C04	23			DBASE	811
I43C01	M13C01			3	13C04	*23	22 29L 1531X3		DBASE	812
I43C01	M13C01			2	13C04	21			DBASE	813
				4	13C04		BRAKE SYS		DBASE	814
				4	13C04		F-2 1341 1344 DATA USED		DBASE	815
				4	13C04		INCLUDES JACKING AS NECESSARY		DBASE	816
				4	13C04		F15 M58MA 155		DBASE	817
				4	13C04		BRAKE SYS F15		DBASE	818
A3D01	F13D03	A3D01	F	66	13D04	21			DBASE	819
23D01	224-07	A3D01	E	63	13D04	21			DBASE	820
A3D01	224-07	A3D02	D		13D04	21			DBASE	821
-3033	CALGPJ	A3D03	C		13D04	21			DBASE	822
A3D01	CALTPJ	A3D03	C		13D04	21			DBASE	823
A3D01	224-07	A3D03	E	2-	13D04	21			DBASE	824
A3D01	224-07	A3D04	D		13D04	21			DBASE	825
A3D01	CALGPJ	A3D03	C		13D04	21			DBASE	826
A3D01	CALTPU	A3D04	D		13D04	21			DBASE	827
A3D01	M13D01			16	13D04	21			DBASE	828
A3D01	M13D01			17	13D04	21	10 29L 1531Y3		DBASE	829
A3D01	M13D01	A3D04	D		13D04	21	16 29L 2-31X1 1060	1TU228	DBASE	830
A3D01	V13D01				13D04	21			DBASE	831
A3D01	V13D02			16	13D04	21	25 29L 2-21X2 1060	1TU228	DBASE	832
A3D01	V13D01	A3D02	E	6-	13D04	21	4- 29L 2-21X2 1061	1TU228	DBASE	833
A3D01	V13D01	A3D03	C		13D04	21			DBASE	834
A3D01	SHOP	S13D01	D		13D04	21			DBASE	835
S43D01	L13D03	I13D04	D		13D04	21			DBASE	836
	L13D04			4	13D04		BRAKE COMPTS		DBASE	837
I43D01	M13D01			5	13D04	*23	11 29L 1531X1		DBASE	838
I43D01	M13D01			16	13D04	*23	12 29L 1531X1		DBASE	839
I43D01	M13D01			77	13D04	*23	51 29L 1-31Y1 1531X1		DBASE	840
I43D01	M13D02			3	13D04	21			DBASE	841
				4	13F03		LANDING CNTL / WARNING / EMERG SYS		DBASE	842
				4	13F03		F-2 1341 DATA USED FOR F15 17E / 15F		DBASE	843
				4	13F03		F15 M58MA 155		DBASE	844
				4	13F03		LNG CNTL WARN / EMERG SYS F15		DBASE	845
A3F01	F13F03	A3F01	F	174	13F03	21			DBASE	846
A3F01	224-07	A3F04	D		13F03	21			DBASE	847
A3F01	CALGPJ	A3F03	C		13F03	21			DBASE	848
A3F01	CALTPJ	A3F03	C		13F03	21	23 29L 2-21X2 1060		DBASE	849
A3F01	M13F04	A3F02	E	2-	13F03	21	12 29L 1531X3		DBASE	850
A3F01	M13F04			17	13F03	21	18 29L 2-21X2 1060		DBASE	851
A3F01	R13F01	A3F03	E	14	13F03	21	22 29L 2-21X2 1060		DBASE	852
A3F01	R13F01			27	13F03	21	16 29L 1423X0 1060		DBASE	853
A3F01	J13F02	A3F03	E	22	13F03	21	11 29L 4-31X1		DBASE	854
A3F04	R13F02			2	13F03	21	46 29L 2-21X2 1060		DBASE	855

A3F13	R:3F11	3	13	13F13	21	17	29L	232622	1360	DBASE	856	
A3F12	V:3F11	3	13	F12	21	11	29L	2-23X2	1361	DBASE	857	
A3F13	V:3F12	3	1.	13F12	21	15	29L	1-31X1	1360	DBASE	853	
A3F13	S4DF	3	13	F13	21					DBASE	853	
S43F13	L:3F13	3	13F13	23						DBASE	860	
	L13F13	4	13F13							DBASE	854	
I13F13	N:3F13	3	13F13	*23	12	29L	2-21X2		DBASE	862		
I13F13	O:3F13	3	13F13	21					DBASE	867		
	M:	4	13H0C						DBASE	864		
	M:	4	13H0C						DBASE	855		
	M:	4	13H0C						DBASE	856		
	M:	4	13H0C						DBASE	867		
A3H03	F:3M13	A3H04	F	237	13H03	21				DBASE	858	
A3H04	V:3M13	A3H05	3	13H04	21	31	29L	2-23X2	1-31X1	1421X2	DBASE	853
A3H05	R:3M12	3	13H05	21	34	29L	2-21X2			DBASE	871	
A3H05	S:3M12	3	13H05	21	31	29L	2-21X2			DBASE	871	
A3H02	R:3M12	3	13H02	21	14	29L	2-23X2			DBASE	872	
A3H02	S:3M12	3	13H02	21	12	29L	2-23X2			DBASE	873	
A3H02	S4DP	S13H02	3	13H02	23					DBASE	874	
S43H02	L:3M12	A3H01	2	13H02	23					DBASE	875	
L13H02	4	13H02								DBASE	876	
I13H02	N:3M12	3	13H02	*23	10	29L	1-23X2		DBASE	877		
I13H02	O:3M12	3	13H02	21	14	29L	2-23X2		DBASE	878		
	M:	4	13H02						DBASE	879		
	M:	4	13H02						DBASE	879		
	M:	4	13H02						DBASE	879		
A3J01	F:3J01	A3J02	F	19	13J01	21				DBASE	845	
A3J01	R:3J01	A3J02	3	13J02	21	69	29L	2-31X1		DBASE	846	
A3J02	S:3J02	S13J01	3	13J02	21					DBASE	847	
S43J01	L:3J01	I13J01	3	13J02	23					DBASE	848	
L13J01	4	13J02								DBASE	849	
I13J01	N:3J02	3	13J02	*23	62	29L	1-31Y1		DBASE	850		
I13J01	O:3J02	3	13J02	*23	12	29L	1-31Y1		DBASE	851		
I13J01	P:3J02	3	13J02	23	20	29L	2-31Y1		DBASE	852		
I13J01	Q:3J02	3	13J02	21	5	29L	2-31Y1		DBASE	852		
	M:	4	14AA0							DBASE	844	
	M:	4	14AA0							DBASE	845	
	M:	4	14AA0							DBASE	846	
	M:	4	14AA0							DBASE	847	
	M:	4	14AA0							DBASE	848	
	M:	4	14AA0							DBASE	849	
	M:	4	14AA0							DBASE	850	
	M:	4	14AA0							DBASE	851	
	M:	4	14AA0							DBASE	852	
	M:	4	14AA0							DBASE	853	
	M:	4	14AA0							DBASE	854	
	M:	4	14AA0							DBASE	855	
A4A01	F:4A01	A4A01	F	93	14A01	21				DBASE	905	
A4A01	D:4A01	A4A02	3	14A01	21					DBASE	906	
A4A02	D:4A01	A4A02	2	14A01	21					DBASE	917	
A4A03	S4DF	A4A03	3	14A01	21					DBASE	918	
A4A03	21-4A2	21-4A2	2	14A01	21					DBASE	919	
A4A03	21-4A2	21-4A2	3	14A01	21					DBASE	920	
A4A03	21-4A2	21-4A2	0	14A01	21	23	29L	2-23X2	1Dc2	1TU228	DBASE	911
A4A03	21-4A2	21-4A2	3	14A01	21	52	29L	2-23X2	1Dc2		DBASE	911
A4A03	21-4A2	21-4A2	3	14A01	21	15	29L	2-23X2	1Dc2	1TU228	DBASE	912
A4A03	21-4A2	21-4A2	2	14A01	21	13	29L	2-23X2	1Dc2	1TU228	DBASE	913
A4A03	S4DF	S4A03	3	14A01	23					DBASE	914	
S4A03	L:4A03	I14A03	3	14A01	23					DBASE	915	
L14A03	4	14A01								DBASE	916	
I14A03	N:4A03	3	14A01	*23	54	29L	1-43X2			DBASE	917	
I14A03	O:4A03	I14A03	3	14A01	*23	11	29L	1-32X1		DBASE	918	
I14A03	P:4A03	I14A03	3	14A01	*23	36	G			DBASE	919	
I14A03	Q:4A03	I14A03	3	14A01	21	15	29L	2-23X2		DBASE	920	
I14A03	R:4A03	I14A03	4	14A01	21	15	29L	2-23X2		DBASE	921	

			14E30	NO COMPARABILITY		OBASE	922
			14E31	TSGT FOOLE LUKE		OBASE	923
			14E32	TSGT FULTON EDWARDS		OBASE	924
			14E33	F15 MSEMMA 420		OBASE	925
			14E34	PITCH & ROLL CHANNEL ASY F15		OBASE	926
			14E35	F1-53, A-431 F 711 14E31 21		OBASE	927
			14E36	54 29L 2421X2		OBASE	928
			14E37	46 29L 1-21Y2 232632 24701 1050		OBASE	929
			14E38	SHAF S44W8 3		OBASE	930
			14E39	11-031 A-431 2		OBASE	931
			14E40	11-033		OBASE	932
			14E41	14E30 PITCH & ROLL CHANNEL ASY		OBASE	933
			14E42	14E31 21 54 29L 1-21Y2		OBASE	934
			14E43	14E30 21 54 29L 2-21X2		OBASE	935
			14E44	STAR SYS DATA		OBASE	936
			14E45	F111F 14E30 + 37% L+HAB + 14E33 C 3D		OBASE	937
			14E46	F4E 1-3-1 FOR APG 1 1% OF SHEET VOL		OBASE	938
			14E47	F15 MSEMMA 420		OBASE	939
			14E48	STAR SYS F15		OBASE	940
			14E49	F14C30 A-331 F 152 14C31 21		OBASE	941
			14E50	1-031 21		OBASE	942
			14E51	14E31 21		OBASE	943
			14E52	14E31 21		OBASE	944
			14E53	14E31 21		OBASE	945
			14E54	56 14E31 21 26 29L 2-31Y1 1050 1TU225		OBASE	946
			14E55	24 14E31 21 7 29L 1-031X1 1050 1TU226		OBASE	947
			14E56	15 14E31 21 20 29L 2326P2 1050 1TU226		OBASE	948
			14E57	21 14E31 21 57 29L 2421X2 1TU226		OBASE	949
			14E58	SA-031 23		OBASE	950
			14E59	14E31 23		OBASE	951
			14E60	STAR SYS		OBASE	952
			14E61	14E30*23 15 29L 2421X2		OBASE	953
			14E62	14E31 21 36 29L 2421X1		OBASE	954
			14E63	RUDDER		OBASE	955
			14E64	F111F 14E30 23X F4E 1-2 C 3 14E33		OBASE	956
			14E65	F4E 14E30		OBASE	957
			14E66	F15 MSEMMA 32		OBASE	958
			14E67	FUDGER F15		OBASE	959
			14E68	F1-031 44D1 F 21 14E31 21		OBASE	960
			14E69	14E31 21		OBASE	961
			14E70	14E31 21		OBASE	962
			14E71	14E31 21		OBASE	963
			14E72	14E31 21		OBASE	964
			14E73	26 14E31 21 35 29L 2421X1 1050 1TU226		OBASE	965
			14E74	61 14E31 21 30 29L 2421X2 1050 1TU226		OBASE	966
			14E75	14E31 21 32 29L 1431X1		OBASE	967
			14E76	15 14E31 21 26 29L 2326P2 1050 1TU226		OBASE	968
			14E77	32 14E31 21 26 29L 2421X1		OBASE	969
			14E78	SA-031 23		OBASE	970
			14E79	14E31 23		OBASE	971
			14E80	RUDDER COMPTO		OBASE	972
			14E81	14E31 23 16 29L 2421X2		OBASE	973
			14E82	14E31 23 16 29L 2421X2		OBASE	974
			14E83	21 14E31 21 37 29L 2421X2		OBASE	975
			14E84	SPEED BRAKE 3		OBASE	976
			14E85	F4E 14E30 CFS 14E32 DATA JCS		OBASE	977
			14E86	F15 MSEMMA 21		OBASE	978
			14E87	SPEED BRAKE SYS F15		OBASE	979
			14E88	F1-031 A-031 F 67 14E31 21		OBASE	980
			14E89	14E31 21		OBASE	981
			14E90	14E31 21		OBASE	982
			14E91	14E31 21		OBASE	983
			14E92	14E31 21		OBASE	984
			14E93	14E31 21 16 29L 2421X2 1050 1TU226		OBASE	985
			14E94	56 14E31 21 16 29L 2421X2 1050 1TU226		OBASE	986
			14E95	17 14E31 21 17 29L 2423X1 1050 1TU226		OBASE	987
			14E96	05 14E31 21 11 29L 2423X2 1050 1TU226		OBASE	988

A6E33	21-E2	A6E02	E	69	14E00	21	36 29L 2431X1 1060	1TU229	D BASE	988
A6E17	41-E2			69	14E00	21	12 29L 1531X1 1060	1TU228	D BASE	989
A6E10	41-E3			69	14E00	21	21 29L 2531X3 1060	1TU228	D BASE	990
A6E32	V1-E2		O	14	14E01	21	10 29L 2421X2 1060	1TU228	D BASE	991
A6E17	SHOP		S1-E2	1	14E01	21			D BASE	992
SA4E1	L1-E4			1215	14E00	23			D BASE	993
IA6E1	21-E2			1	14E00	23	36 29L 2421X2 1060		D BASE	994
IA6E1	41-E2			59	14E00	23	5 29L 2531X3		D BASE	995
IA6E1	41-E3			67	14E00	23	14 29L 1531X3		D BASE	996
IA6E1	01-E2			3	14E00	21			D BASE	997
IA6E1	11-E2			14E00	21				D BASE	998
IA6E1	11-E3			14E00	21				D BASE	999
IA6E1	11-E4			14E00	21				D BASE	1000
IA6E1	11-E5			14E00	21				D BASE	1001
IA6E1	11-E6			14E00	21				D BASE	1002
IA6E1	11-E7			14E00	21				D BASE	1003
IA6E1	11-E8			14E00	21				D BASE	1004
IA6E1	11-E9			14E00	21				D BASE	1005
IA6E1	11-E10			14E00	21				D BASE	1006
IA6E1	11-E11			14E00	21				D BASE	1007
IA6E1	11-E12			14E00	21				D BASE	1008
IA6E1	11-E13			14E00	21				D BASE	1009
IA6E1	11-E14			14E00	21				D BASE	1010
IA6E1	11-E15			14E00	21				D BASE	1011
IA6E1	11-E16			14E00	21				D BASE	1012
IA6E1	11-E17			14E00	21				D BASE	1013
IA6E1	11-E18			14E00	21				D BASE	1014
IA6E1	11-E19			14E00	21				D BASE	1015
IA6E1	11-E20			14E00	21				D BASE	1016
IA6E1	11-E21			14E00	21				D BASE	1017
IA6E1	11-E22			14E00	21				D BASE	1018
IA6E1	11-E23			14E00	21				D BASE	1019
IA6E1	11-E24			14E00	21				D BASE	1020
IA6E1	11-E25			14E00	21				D BASE	1021
IA6E1	11-E26			14E00	21				D BASE	1022
IA6E1	11-E27			14E00	21				D BASE	1023
IA6E1	11-E28			14E00	21				D BASE	1024
IA6E1	11-E29			14E00	21				D BASE	1025
IA6E1	11-E30			14E00	21				D BASE	1026
IA6E1	11-E31			14E00	21				D BASE	1027
IA6E1	11-E32			14E00	21				D BASE	1028
IA6E1	11-E33			14E00	21				D BASE	1029
IA6E1	11-E34			14E00	21				D BASE	1030
IA6E1	11-E35			14E00	21				D BASE	1031
IA6E1	11-E36			14E00	21				D BASE	1032
IA6E1	11-E37			14E00	21				D BASE	1033
IA6E1	11-E38			14E00	21				D BASE	1034
IA6E1	11-E39			14E00	21				D BASE	1035
IA6E1	11-E40			14E00	21				D BASE	1036
IA6E1	11-E41			14E00	21				D BASE	1037
IA6E1	11-E42			14E00	21				D BASE	1038
IA6E1	11-E43			14E00	21				D BASE	1039
IA6E1	11-E44			14E00	21				D BASE	1040
IA6E1	11-E45			14E00	21				D BASE	1041
IA6E1	11-E46			14E00	21				D BASE	1042
IA6E1	11-E47			14E00	21				D BASE	1043
IA6E1	11-E48			14E00	21				D BASE	1044
IA6E1	11-E49			14E00	21				D BASE	1045
IA6E1	11-E50			14E00	21				D BASE	1046
IA6E1	11-E51			14E00	21				D BASE	1047
IA6E1	11-E52			14E00	21				D BASE	1048
IA6E1	11-E53			14E00	21				D BASE	1049
IA6E1	11-E54			14E00	21				D BASE	1050
IA6E1	11-E55			14E00	21				D BASE	1051
IA6E1	11-E56			14E00	21				D BASE	1052
IA6E1	11-E57			14E00	21				D BASE	1053

83664	023P4M 83326	0	23100 21	3 29L 1431X1	08ASE 1054
		4	23100	023P4D INSTALL OR REMOVE ACFT FROM PACORASE	1055
83673	023P4D 83326	0	23100 21	3 29L 3-32X0 1431X1	08ASE 1056
		4	23100	T23001 TROUBLESHOOT, FIX, TRIM, AND LEAKDRASE	1057
		4	23100	NO PARTS REPLACEMENT	08ASE 1058
83673	T23001 83326	0	23100 21	30 29L 3-32X0 1431X1	08ASE 1059
		4	23100	M23001 MINOR REPAIR WITH PART CHANGES	08ASE 1060
		4	23100	ON TRIM PAD	08ASE 1061
83673	423P4M 83326	0	23100 21	5 29L 3-32X0 1431X1	08ASE 1062
83673	V23004 83326	0	23100 21		08ASE 1063
83673	023P4D 83326	0	23100 21		08ASE 1064
83673	023P4D 83326	0	23100 21		08ASE 1065
83674	023T04	0	23100 21		08ASE 1066
		4	23100	C23LFK ENGINE LEAK CHECK	08ASE 1067
83675	023LEK 83326	0	23100 21	5 29L 2432X0 1431X1	08ASE 1068
83675	E402 S3326	0	23100 21		08ASE 1069
83675	023P4D 83326	0	23100 21		08ASE 1070
83675	023T04 83326	0	23100 21		08ASE 1071
		4	23100	M23001 MINOR REPAIR WITH PART CHANGE	08ASE 1072
		4	23100	ON FLIGHT LINE	08ASE 1073
83676	423001 83326	0	9 23100 21	10 29L 2432X0	08ASE 1074
83676	V23004 83326	0	23100 21		08ASE 1075
83676	023LEK	0	23100 21		08ASE 1076
83676	SHP 83326	0	23100 21		08ASE 1077
83677	023P4M 83326	0	23100 21		08ASE 1078
83677	423001 83326	0	23100 21	15 29L 4-32X0	08ASE 1079
83677	023T04 83326	0	23100 21	15 29L 4-32X0	08ASE 1080
83677	023LEK 83326	0	23100 21		08ASE 1081
83678	T3001 S3326	0	23100 21		08ASE 1082
83678	023P4M	0	9 23100 21		08ASE 1083
83678	023T04 83326	0	10 23100 21		08ASE 1084
		4	23100	ENGINE IN SHOP AND TEST CELL	08ASE 1085
83679	023T04 S3326	0	23100 23	15 29L 3-32X0 1430X0	08ASE 1086
		4	23100	DTOM23 TOW ENGINE TO TEST CELL	08ASE 1087
83680	DTOM23 S3326	0	23100 23	1 29L 2432T0	08ASE 1088
83680	E402 S3326	0	7 23100 23		08ASE 1089
		4	23100	C23T01 CONNECT AND DISCONNECT TEST CELLS	08ASE 1090
83681	023T04 S3326	0	23100 23	9 29L 5-32T0	08ASE 1091
		4	23100	T23002 TROUBLESHOOT AND TRIM TEST CELL	08ASE 1092
83681	T23002 S3326	0	23100 23	5 29L 4-32T0	08ASE 1093
		4	23100	T23003 TFEWD AND SWAP TEST CELL	08ASE 1094
83682	T23003 S3326	0	6 23100 23	5 29L 4-32T0	08ASE 1095
83682	023T04 S3326	0	23100 23		08ASE 1096
83682	023T04 S3326	0	23100 23		08ASE 1097
83682	SHP S3326	0	23100 23		08ASE 1098
83682	DTOM23 S3326	0	23100 23		08ASE 1099
		4	23100	W23001 FINAL SHOP WORK GOOD ENGINE OUT	08ASE 1100
83683	423001	0	23100 23	40 29L 4-32X0	08ASE 1101
83683	DTOM23 S3326	0	23100 23		08ASE 1102
		4	23100	W23001 ENGINE SHOP WORK	08ASE 1103
83684	W23001 S3326	0	23100 23	50 29L 4-32X0	08ASE 1104
		4	23100	H23002 ENGINE SHOP WORK	08ASE 1105
83685	W23002 S3326	0	9 23100 23	60 29L 5-32X0	08ASE 1106
		4	23100	H23003 ENGINE SHOP WORK	08ASE 1107
83685	W23003 S3326	0	11 23100 23	320 29L 4-32X0	08ASE 1108
L23A10		4	23100	C3 INLET MAN MODULE	08ASE 1109
S93686	L23A10 S3326	0	15 23100 23		08ASE 1110
93687	W23A10	0	27 23100 23	40 29L 3432Y0	08ASE 1111
93687	W23A10	0	27 23100 23	22 29L 1431X1	08ASE 1112
93687	W23A10	0	55 23100 23	5 29L 2432T0	08ASE 1113
83688	W23A10	0	84 23100 23	5 29L 2432T0	08ASE 1114
83688	Q23A10	0	23100 21		08ASE 1115
L23A10		4	23100 23	CURE ENGINE MODULE	08ASE 1116
S93689	L23A10 S3326	0	13 23100 23		08ASE 1117
83690	423001	0	12 23100 23	13 29L 1430X0	08ASE 1118
83690	K23000	0	15 23100 23	18 29L 1432X0	08ASE 1119

8300J	N239J	E	73	23000*23	5 29L 1432XC	OBASE 1123
839J	1	O239J	2	23100 21		OBASE 1124
L23C	1	4	23030 23	FAN DRIVE TURBINE MODULE		OBASE 1122
S93J	L23C	1	37000	7 10.45 23 23		OBASE 1123
9300J	M23C	E	60	23000*23	9 29L 1432XC	OBASE 1124
9100J	K23C	E	1	23100*23	10 29L 1432XC	OBASE 1125
9300J	N23C	E	51	23000*23	11 29L 1432XC	OBASE 1126
9300J	O23C	1	23030 21			OBASE 1127
L23F	1	4		AUGMENTOR DUCT AND NOZZLE MODULE		OBASE 1123
S93J	L23F	1	37000	6 1257 23 23		OBASE 1129
83F0J	M23F	E	13	23000*23	12 29L 1432XC	OBASE 1131
93F0J	N23F	E	13	23000*23	13 29L 1432XC	OBASE 1132
93F0J	O23F	2	4	23000*23	14 29L 1531X3	OBASE 1133
93F0J	P23F	2	72	23000*23	5 29L 1432XC	OBASE 1133
93F0J	Q23F	3	0	23030 21		OBASE 1134
L23G	1	4		SEAPROXY MODULE		OBASE 1135
S93J	L23G	1	37000	5 1122 23 23		OBASE 1136
9300J	M23G	E	77	23000*23	5 29L 1432XC	OBASE 1137
9300J	K23G	E	11	23000*23	5 29L 1432XC	OBASE 1138
9300J	N23G	E	55	23000*23	11 29L 1432XC	OBASE 1139
9300J	O23G	1	23030 21			OBASE 1140
L23H	1	4	23030	FUEL SYSTEM		OBASE 1141
S93J	L23H	1	37000	5 1338 23 23		OBASE 1142
93M	M23H	2	27	23000*23	11 29L 1432XC	OBASE 1143
93M	N23H	2	3	23000 21		OBASE 1144
L23I	1	4	23030	OIL SYSTEM		OBASE 1145
S93J	L23I	1	37000	5 11375 23 23		OBASE 1146
93M	M23I	2	27	23000*23	6 29L 1432XC	OBASE 1147
93J	N23I	2	3	23000 21		OBASE 1148
L23K	1	4	23030	ELECTRICAL SYSTEM		OBASE 1149
S93J	L23K	1	37000	5 11235 23 23		OBASE 1150
93K	M23K	2	27	23000*23	6 29L 1432XC	OBASE 1151
93K	N23K	2	3	23000 21		OBASE 1152
L23P	1	4	23030	AUGMENTOR NOZZLE ACTUATION SYSTEM		OBASE 1153
S93J	L23P	1	37000	5 11469 23 23		OBASE 1154
93P	M23P	2	27	23000*23	6 29L 1432XC	OBASE 1155
93P	N23P	2	3	23000 21		OBASE 1156
L23Q	1	4	23030	MISC COMPONENTS		OBASE 1157
S93J	L23Q	1	37000	5 12215 23 23		OBASE 1158
93Q	M23Q	2	30	23000*23	31 29L 1531X1	OBASE 1159
93Q	N23Q	2	70	23000*23	5 29L 1432XC	OBASE 1160
93Q	O23Q	2	27	23000 21		OBASE 1161
L23R	1	4	23030	ENGINE INSTRUMENTS		OBASE 1162
S93J	L23R	1	37000	42 23100 21		OBASE 1163
93R	M23R	2	30	23100 21		OBASE 1164
93R	N23R	2	31	23100 21		OBASE 1165
93R	O23R	2	27	23100 21		OBASE 1166
R23100	S3100	E	29	23100 21	3 29L 232632	OBASE 1167
R23100	T3100	E	29	23100 21	20 29L 2431X1	OBASE 1167
R23100	U3100	E	12	23100 21	20 29L 2432XC	OBASE 1168
R23100	V3100	E	12	23100 21	16 29L 232632	OBASE 1169
R23100	W3100	E	13	23100 21	17 29L 1-31X1 1432XC	OBASE 1170
R23100	X3100	E	13	23100 21	15 29L 1531X0	OBASE 1171
R23100	Y3100	E	9	23100 21	22 29L 1432XC	OBASE 1172
R23100	Z3100	E	23	23100 21		OBASE 1173
S3100	R23100	2	23	23100 23	13 29L 132632	OBASE 1174
S3100	S23100	2	35	23100*23	10 29L 172632	OBASE 1175
S3100	T23100	2	23	23100*23	5 29L 1432XC	OBASE 1176
S3100	U23100	2	23	23100 21	8 29L 232632	OBASE 1177
24AJ0	1	4	24000	JET FUEL STARTER		OBASE 1178
24AJ0	2	4	24000	F15 JET FUEL STARTER		OBASE 1179
24AJ0	3	4	24000	Y24AJ0 SHCP REPAIR		OBASE 1180
24AJ0	4	4	24000	Y24TST TEST CELL SJW		OBASE 1181
24AJ0	5	4	24000	TSGT FETTER-4500 ENG PH 2734		OBASE 1182
24AJ0	6	4	24000	TSST GOESMAN ENG PH 2978		OBASE 1183
24AJ0	7	4	24000	JET FUEL STARTER F45		OBASE 1184
86A0J	F24AJ0	1	46	24AJ0 21		OBASE 1185

86A31	00394H7	86A31	0	26A0	21	DBASE 1136		
86A31	C-1	TIU	86A31	2	26A0	21	DBASE 1137	
3-A-3	T264-3	3-A-212	3	26A0	21	DBASE 1138		
36A12	52-502	0	26A0	21	3-29L 1-32X1	DBASE 1139		
36A2	52-4-1	A	1	26A0	21	6-29L 2-31X1	DBASE 1140	
36A2	52-4-1	36A13	5	5	26A0	21	33-29L 2432X1 1TJ223	DBASE 1141
36A2	52-4-1	36A13	5	22	26A0	21	17-29L 2-21X2 1TJ225	DBASE 1142
56A12	52-4-1	36A13	5	23	26A0	21	15-29L 2-32X1 1TJ226	DBASE 1143
96A32	Y2-4-1	3-A-64	3	26A0	21	24-29L 1-32X1	DBASE 1144	
26A13	02-4-6	1	1	26A0	21	33-29L 2432X1	DBASE 1145	
3-A-3	Y2-4-1	36A13	5	26A0	21	11-29L 2-32X1	DBASE 1146	
66A12	52-4-1	52-4-1	2	26A0	23	DBASE 1147		
S9-21	L2-1-1	I2-4-10	0	26A0	23	DBASE 1148		
12-A-1	4	26A0	23	JFS SYS		DBASE 1149		
I36A31	N2-4A13	0	26A0	23	15-29L 1432X0	DBASE 1200		
4	26A0	ACC OF GEARBOXES				DBASE 1201		
4	26A0	F15 DATA USED				DBASE 1202		
H	26A0	NO WAY TO TEST AMADS				DBASE 1203		
4	26A0	NEW PTC SHAFT SEAL IS WORKING				DBASE 1204		
4	26A0	MSBMA ADJ FROM 25 TO 75 FOR COFFEE-				DBASE 1205		
4	26A0	TIVE ACTIONS				DBASE 1206		
4	26A0	ACC DR GEAR-BOX F15				DBASE 1207		
3-A-3	F2-511	3-A-31	5	26A0	21	DBASE 1208		
3-A-3	72-7407	3-A-31	2	26A0	21	DBASE 1209		
36A31	PANEL	3	26A0	21	5-29L 1431X1	DBASE 1211		
36A32	53-1601	3-9-3	1	26A0	21	DBASE 1211		
36A33	32-5-1	3-8-2	5	26A0	21	26-29L 2431X1	DBASE 1212	
36A33	**263-1	21	26A0	21	24-29L 2432X1 1TJ223	DBASE 1213		
66A33	42-5-1	36A13	5	26A0	21	10-29L 1431X1	DBASE 1214	
9-3-3	2249	26A13	5	53	26A0	21	23-29L 2432X0 1TJ223	DBASE 1215
36A32	5HJP	53-3-1	5	26A0	23	DBASE 1216		
S9-21	L2-3-1	I2-4-10	3	26A0	23	DBASE 1217		
12-A-1	4	26A0	ACC OF GEARBOX			DBASE 1218		
I36A31	N2-3-1	0	26A0	23	16-29L 1-32X1	DBASE 1219		
I36A31	02-3-1	0	26A0	21	23-29L 2432X1	DBASE 1220		
4	26A0	JFS STARTING SYS				DBASE 1221		
4	26A0	NO COMPATIBILITY AVAILABLE				DBASE 1222		
4	26A0	USED FILE DATA				DBASE 1223		
H	26A0	JFS START SYS F15				DBASE 1224		
96D17	F240-1	36A31	F	355	26A0	21	DBASE 1225	
36D12	F240-1	36A31	D	26A0	21	14-29L 2421X2 1TJ225 1431X1	DBASE 1226	
36D12	5HJP	594003	0	26A0	23	DBASE 1227		
S9-21	L2-0-1	I2-4-10	0	26A0	23	DBASE 1228		
12-A-1	4	26A0	JFS START SYS			DBASE 1229		
I36D12	N2-3-1	0	26A0	23	22-29L 2-21X2	DBASE 1230		
I36D12	02-3-1	0	26A0	21	DBASE 1231			
4	26A0	ENV CONN SYS				DBASE 1232		
4	26A0	MSG DEVLAELICK LUKE FNU FH 2791				DBASE 1233		
4	26A0	SSG JAMES EDWARDS ENV				DBASE 1234		
4	26A0	F15 DATA USED				DBASE 1235		
4	26A0	ENV CONN SYS F15				DBASE 1236		
D1A12	F-1A11	D1A12	F	2	26A0	21	DBASE 1237	
D1A12	X-1A13	D1A12	D	26A0	21	13-29L 2422X1 1431X1	DBASE 1238	
D1A12	T-1A13	D1A13	D	26A0	21	24-29L 2422X1	DBASE 1239	
D1A13	R-1A13	D1A12	E	23	26A0	21	26-29L 2422X1	DBASE 1240
D1A13	M-1A13	E	5	26A0	21	27-29L 1422X1	DBASE 1241	
D1A13	R-1A13	E	6	26A0	21	62-29L 2421X2	DBASE 1242	
D1A13	SHOP	SD1A13	0	41A0	23	DBASE 1243		
SD1A13	L-1A13	I01A13	G	00952	41A0	23	DBASE 1244	
L-1A13	4	41A0	23	BLEED / SERVICE AIR		DBASE 1245		
I01A13	N-1A13	0	41A0	23	16-29L 1-22X1	DBASE 1246		
I01A13	O-1A13	0	41A0	21		DBASE 1247		
SD1A13	L-1A13	I01A13	G	0023	41A0	23	DBASE 1248	
L-1A13	4	41A0	23	AVN EDP COOLING		DBASE 1249		
I01A13	K-1A13	0	41A0	23	20-29L 1-22X1	DBASE 1250		
I01A13	Q-1A13	0	41A0	21		DBASE 1251		

SD1A3L L-1642	ID1A02 S	30357 61830 23		D9ASE 1252
1A1A1	1	61A31	C2FH COMPT COOL / PLES	D9ASE 1251
ID1E32 K-1842	E	25 41A31*23	25 29L 2-22X1	D9ASE 1254
ID1E32 K-1842	E	25 41A31*23	5 29L 2-22X1	D9ASE 1255
ID1E32 K-1842	O	61A31 21		D9ASE 1256
	4	42A31	ELECT PHM PWD	D9ASE 1257
	4	42A01	F4E 426 FOR 42406 2373 / 41 FOR	D9ASE 1258
	4	42A01	42A03 422 F01 42AF3 41 X1 421 F05	D9ASE 1259
	4	42A30	42C01 423 FOR 42B01 / 306	D9ASE 1260
	4	42A31	471 42C01 3 G 7 9 F02 42E01	D9ASE 1261
	4	42A00	F15 MS3MA 36	D9ASE 1262
	4	42A31	SIG CLVEMN LUKE ELEC	D9ASE 1263
	H	42A00	SIG SMITH EWHA-DS ELECT	D9ASE 1264
	H	42A31	SIG SMH LUKE PH 2473 ELECT 952	D9ASE 1265
	H	42A30	ELECT PWD F15	D9ASE 1266
02A31 C-2A1	O2A11	E	67 42A31 21	D9ASE 1267
02A01 DC-MGP	O2A04	O	42A31 21	D9ASE 1268
02A11 C-2A1	O2A12	E	25 42A31 21	D9ASE 1269
02A12 C-2A1	O2A12	E	25 42A31 21	D9ASE 1270
02A03 K-2A1	O2A11	E	26 42A31 21	D9ASE 1271
02A03 K-2A1	O2A11	E	38 42A00 21	D9ASE 1272
02A02 SHOP SD2A01	O	42A00 23	D9ASE 1273	
SD2A1 L-2A1	O2A31	O	42A31 23	D9ASE 1274
L-2A1	4	42A31	ELECT PWD SYSTEMS	D9ASE 1275
122A1 H-2A1	E	51 42A31*23	56 29L 2-23X1	D9ASE 1276
122A1 K-2A1	E	69 42A31*23	66 29L 2-23X1	D9ASE 1277
122A1 H-2A1	E	41 42A31*23	19 29L 2-23X1	D9ASE 1278
122A1 Q-2A1	O	42A03 21		D9ASE 1279
	4	44A01	EXTERIOR LIGHTING	D9ASE 1280
	4	44F00	F4E 441 DATA USED	D9ASE 1281
	4	44A01	F15 MS3MA 14WUST2	D9ASE 1282
	4	44A00	EXT LIGHTING F15	D9ASE 1283
04E11 F-4A1	O2A11	E	3 42A31 21	D9ASE 1284
04E31 DC-HGP	O2A14	O	44A31 21	D9ASE 1285
04E12 K-2A1	O2A13	O	44A31 21	D9ASE 1286
04E13 T-4A1	O2A12	E	13 44A31 21	D9ASE 1287
04E12 F-4A1	O2A03	O	44A31 21	D9ASE 1288
04E13 V-4A1	O2A14	O	44A01 21	D9ASE 1289
04E12 M-4A1	O2A11	E	44A31 21	D9ASE 1290
04E13 F-4A1	O2A11	E	44A31 21	D9ASE 1291
04E10 F-4A1	O2A04	E	21 44A31 21	D9ASE 1292
04E12 M-4A1	O2A11	E	05 44A31 21	D9ASE 1293
04E12 M-4A2	O2A11	E	10 44A00 21	D9ASE 1294
04E12 M-4A2	O2A11	E	12 44A31 21	D9ASE 1295
04E12 SHOP SD-2A1	O	44A31 23	D9ASE 1296	
SD2A1 L-2A1	O2A11	O	44A00 23	D9ASE 1297
L-2A1	4	44A33	EXT LIGHTING	D9ASE 1298
122A1 H-2A1	E	67 44A31*23	15 29L 2-23X3	D9ASE 1299
122A1 N-2A1	E	33 44A31*23	10 29L 2-23X3	D9ASE 1300
122A1 Q-2A1	O	44A31 21		D9ASE 1301
	H	44B03	INTERIOR LIGHTS	D9ASE 1302
	4	44F00	F4E 441 DATA USED	D9ASE 1303
	H	44B01	F15 MS3MA NO FAILURE	D9ASE 1304
	4	44B01	INTERIOR LSH F15	D9ASE 1305
04B11 F-4A1	O2A11	F	267 44B01 21	D9ASE 1306
04P31 DC-HGP	O2A04	O	44B01 21	D9ASE 1307
04B14 L-2A1	O2A13	O	44B01 21	D9ASE 1308
04B12 M-4A1	O2A13	E	57 44B01 21	D9ASE 1309
04B13 T-4A1	O2A16	E	03 44B01 21	D9ASE 1310
04B12 M-4A2	O2A12	E	01 44B01 21	D9ASE 1311
04B13 F-4A1	O2A11	E	37 44B01 21	D9ASE 1312
04B12 M-4A1	O2A11	E	52 44B01 21	D9ASE 1313
04B14 SHOP SD-2A1	O	44B01 23	D9ASE 1314	
SD2A1 L-2A1	O2A03	O	44B00 23	D9ASE 1315
L-2A1	4	44B00	INTERIOR LIGHTS	D9ASE 1316
104B01 K-4A1	E	05 44B00*23	19 29L 2-23X3	D9ASE 1317

					DBASE 1339
					DBASE 1340
					DBASE 1341
					DBASE 1342
					DBASE 1343
					DBASE 1344
					DBASE 1345
					DBASE 1346
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					DBASE 1349
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					DBASE 1364
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					DBASE 1377
					DBASE 1378
					DBASE 1379
					DBASE 1380
					DBASE 1381
					DBASE 1382
					DBASE 1383

L+5C10	4	45000	NO 2 HYD SYS FWR	D9ASE 1334
I0521: 45011	2	45000*21	26 29L 2-21X2	D9ASE 1335
I0521: <45011	3	45000*23	15 29L 1421X2	D9ASE 1336
I0521: M-5C11	2	45000*23	15 29L 1421X2	D9ASE 1337
I0521: Q-5C11	1	45000 21	29 29L 2-21X2	D9ASE 1338
	4	45000	UTILITY HYD SYS	D9ASE 1339
	M	45000	F43 4513 F11F 43AE4 P FCR 4500E /	D9ASE 1330
	M	45010	LELFO	D9ASE 1331
	M	45000	F13 MS34A 31	D9ASE 1332
	M	45000	EXPECT FD T2 9E 4035E UNLESS AMAC SYS	D9ASE 1333
	M	45001	PROBLEMS CORRECTED	D9ASE 1334
	M	45000	UTILITY HYD SYS F13	D9ASE 1335
05C11: F+5C11 D9C11	5	23 45000 21		D9ASE 1336
05C11: 15C11 75C11		5 29L 21		D9ASE 1337
05C14 CALT-J 05C13	3	45000 21		D9ASE 1338
05C12 R-5C11 05C13	5	26 45000 21	34 29L 2-21X2 1TU22	D9ASE 1339
05C19 M-5C11	3	67 45000 21	18 29L 2-21X2 1TU22	D9ASE 1401
05C19 R-5C11	2	67 45000 21	8 29L 2-21X2 1TU22	D9ASE 1401
05C13 M-5C11	3	61 45000 21	7 29L 2-21X2 1TU22	D9ASE 1402
05C13 R-5C11	2	61 45000 21	12 29L 2-21X2 1TU22	D9ASE 1402
05C15 R-5C11	3	62 45000 21	16 29L 2-31C1 1TU22	D9ASE 1403
05C13 M-5C11	3	62 45000 21	16 29L 1531X1 1TU22	D9ASE 1403
05C13 S40P 30500	3	45000 23		D9ASE 1404
05C11 L-5C11 75C11	2	45000 23		D9ASE 1407
L+5C10	4	45000	UTILITY HYD SYS	D9ASE 1413
I05C11 M-5C11	3	32 45000*23	26 29L 2-21X2	D9ASE 1419
I05C11 <5C11	2	67 45000*23	15 29L 1421X2	D9ASE 1420
I05C11 45C11	2	59 45000*23	15 29L 1421X2	D9ASE 1421
I05C11 K-5C11	3	63 45000*23	13 29L 2536X2	D9ASE 1422
I05C11 Q-5C11	1	45000 21	27 29L 2-21X2	D9ASE 1423
	4	46400	INTERNAL FUEL SYS	D9ASE 1424
	M	46400	F43 4513 DATA USED	D9ASE 1425
	4	46400	TSS POOLE LUKE INST	D9ASE 1426
	4	46400	MSG WILLIAMS LUKE FUEL	D9ASE 1427
	4	46400	SSG PRIN LUKE FUEL	D9ASE 1428
	M	46400	F43 MS34C 115	D9ASE 1429
	4	46400	INTERNAL FUEL SYS F13	D9ASE 1420
05A11 F+5A11 D9A11	5	32 45000 21		D9ASE 1421
05A11 3044Y 05A12	3	56 45000 21		D9ASE 1422
05A12 TFUEL 05A13	2	45000 21	5 29L 3431X1	D9ASE 1423
05A13 DFUEL 05A14	3	46400 21	26 29L 3+31X1	D9ASE 1424
05A13 R-5A11	2	30 46400 21	120 29L 2-21X2	D9ASE 1425
05A15 R-5A12 05A15	3	51 46400 21	67 29L 2-21X2	D9ASE 1426
05A15 R-5A11 05A15	2	51 46400 21	720 29L 2424X1	D9ASE 1427
05A11 05A16 05A15	3	44 46400 21		D9ASE 1428
05A15 M-5A11	3	32 46400 21	61 29L 2-31X1	D9ASE 1429
05A15 M-5A12	2	33 46400 21	10 29L 1531X1	D9ASE 1430
05A15 R-5A12 05A17	2	34 46400 21	51 29L 2-31X1	D9ASE 1431
05A15 DUMMY 05A17	3	46400 21		D9ASE 1432
05A15 34SF15 2635E	2	46400 21		D9ASE 1433
05A15 R-5A13	3	46400 21	5 29L 2424X1 1431X1	D9ASE 1434
05A17 SMDFP SCALZ	2	46400 21		D9ASE 1435
S55A11: L-5A11 05A11	3	46400 23		D9ASE 1436
	4	46400	INTERNAL FUEL SYS	D9ASE 1437
I05A11 M-5A11	3	31 46400*23	26 29L 2-21X2	D9ASE 1438
I05A11 R-5A11	2	30 46400*23	27 29L 1-2-11	D9ASE 1439
I05A11 M-5A11	3	47 46400*23	5 29L 1531X1	D9ASE 1440
I05A11 R-5A12	2	43 46400*23	12 29L 1531X1	D9ASE 1441
I05A11 R-5A13	3	47 46400*23	25 29L 1-31X1	D9ASE 1442
I05A11 K-5A11	2	41 46400*23	15 29L 2-31X1	D9ASE 1443
I05A11 R-5A11	3	43 46400 21		D9ASE 1444
	4	46400	THE FOL IS -XT WG TANK NTW	D9ASE 1445
	4	46400	F43 452 DATA USED	D9ASE 1446
	M	46400	50% LOTS FASTER THAN F-E TANKS	D9ASE 1447
	M	46400	F13 MS34A 31	D9ASE 1448
	4	46400	EXTERNAL FULL SYS F15	D9ASE 1449

06811	F+68.1	06911	F	35F	4681L	21	OBASE 1451		
26811	222407	0681A	E	6-	4671	21	OBASE 1451		
0681A	CALGPJ	06813	C	-6800	21	OBASE 1452			
26812	T+68.1	06814	D	-6E00	21	OBASE 1453			
06814	R+68.1	06813	D	4681C	21	OBASE 1454			
06811	R+68.1	06813	E	7-	4671	21	OBASE 1455		
06811	R+68.1	06813	E	0-	4671	21	OBASE 1456		
06811	R+68.1	06813	E	1-	4671	21	OBASE 1457		
06811	R+68.1	06813	E	17	4671	21	OBASE 1458		
06811	R+68.1	06813	E	18	4671	21	OBASE 1459		
06813	SHOP	SD6811	D	-6E00	21	OBASE 1459			
SD6811	L+68.1	I26803	D	46800	23	OBASE 1460			
SD6811	L+68.1	I26803	D	46800	23	OBASE 1461			
4	-6E00	EXTERNAL WG TANKS							
I26811	R+68.1	21	-6E00	*23	81	29L	2+24X3	OBASE 1462	
I26811	R+68.1	21	4681C	*23	34	29L	2424X3	OBASE 1463	
I26811	R+68.1	21	5-	4681C	*23	16	29L	1424X3	OBASE 1464
I26811	R+68.1	21	03	46800	*23	23	29L	2531X3	OBASE 1465
I26811	R+68.1	21	02	46800	*23	09	29L	1531X1	OBASE 1466
I26811	R+68.1	21	0-	4681C	*23	21	29L	2531X3	OBASE 1467
I26811	R+68.1	21	1-	4681C	*23	03	29L	2536X3	OBASE 1468
I26811	R+68.1	21	-6E00	21				OBASE 1469	
4	-6E00	REFUEL NTHK						OBASE 1470	
4	-6E00	FUE 4631 DATA USED						OBASE 1471	
4	-6E00	F15 MSBMA NO FAILURE						OBASE 1472	
4	-6E00	REFUEL SYS F15						OBASE 1473	
06011	F+60.1	06011	F	32F	46000	21	OBASE 1474		
26011	222407	06014	D	46000	21	OBASE 1475			
26014	CALGPJ	06009	C	-6E00	21	OBASE 1476			
26012	222407	06000	D	46000	21	OBASE 1477			
26010	CALT13	06010	C	-6E00	21	OBASE 1478			
26010	T+60.1	06012	E	1-	46000	21	OBASE 1479		
26012	R+60.1	06003	D	-6E00	21	OBASE 1480			
26013	V+60.1	06003	D	-6E00	21	OBASE 1481			
26010	R+60.1	06012	E	5-	46000	21	OBASE 1482		
26013	R+60.1	06012	E	15	46000	21	OBASE 1483		
26013	R+60.1	06012	E	25	46000	21	OBASE 1484		
26010	R+60.1	06004	E	1-	46000	21	OBASE 1485		
26010	V+60.1	06011	D	-6E00	21	OBASE 1486			
26010	R+60.1	06014	E	5-	46000	21	OBASE 1487		
26012	R+60.1	06012	E	3-	46000	21	OBASE 1488		
26014	SHOP	SD6003	D	46000	23	OBASE 1489			
SD6003	L+60.1	I26000	D	46000	23	OBASE 1489			
L+6003	4	46000	AIR REFUEL SYS					OBASE 1490	
I26011	R+60.1	29	-6E00	*23	15	29L	1531X1	OBASE 1491	
I26011	R+60.1	29	-6E00	*23	15	29L	1421X2	OBASE 1492	
I26000	R+60.1	62	-6E00	*23	16	29L	1424X0	OBASE 1493	
I26016	R+60.1	5	46000	21	46000	21	OBASE 1494		
4	-6E00	FUEL CCNT & WING INDICATING SYS						OBASE 1495	
4	-6E00	F4E +64						OBASE 1496	
4	-6E00	FUEL CONT & WING INDICATING SYS F15						OBASE 1497	
06E11	F+6E11	06E11	F	32	46E14	21	OBASE 1498		
26E11	222407	06E11	D	46E10	21	OBASE 1499			
06E11	CALGPJ	06E13	C	-6E00	21	OBASE 1500			
26E13	T+6E11	06E13	D	46E00	21	OBASE 1501			
06E13	R+6E12	06E02	E	97	-6E00	21	OBASE 1502		
06E13	R+6E12	06E02	E	3	46E00	21	OBASE 1503		
06E12	SHOP	SD6E13	D	-6E00	23	OBASE 1504			
SD6E02	L+6E02	I26E03	D	-6E00	23	OBASE 1505			
L+6E13	4	-6E00	FUEL CONT & WING INO SYS					OBASE 1506	
I26E01	N+6E01	51	46E00	*23	13	29L	1+24X0	OBASE 1507	
I26E01	K+6E01	16	46E00	*23	25	29L	232621	OBASE 1508	
I26E01	N+6E01	3-	46E00	*23	10	29L	232631	OBASE 1509	
I26E03	Q+6E03	0	46E00	21				OBASE 1510	
4	47A00	THE FOL IS LOX NTHK						OBASE 1511	
H	47A00	F11F -7A DATA USED						OBASE 1512	
H	47A00	LOX F15						OBASE 1513	
07A01	F+7A01	07A01	F	63	47A00	21	OBASE 1514		
07A01	R+7A00	07A02	E	47	47A00	21	OBASE 1515		

07A1	R-7A1	07A2	E	12	47A06	21	15	29L	132632	OBASE 1516
07A1	R-7A2	07A2	E	2	47A11	21	14	29L	1-31X1	OBASE 1517
07A1	M-7A1	07A3	E	3	47A03	21	9	29L	2422X1	OBASE 1519
07A1	M-7A1		E	3	47A01	21	10	29L	232622	OBASE 1519
07A13	V-7A13		D	6	47A05	21	05	29L	2422X1	OBASE 1521
07A13	V-7A13		D	6	47A05	21	5	29L	1-31X1	OBASE 1521
07A12	S-7D12	SD7A03	D	4	47A03	23				OBASE 1522
SD7A12	L-7A12	X-7A01	D	4	47A04	23				OBASE 1523
L-7A03			A	4	47A00	LCX SYS				OBASE 1524
SD7A11	M-7A11		E	11	47A01	23	31	29L	2-22X1	OBASE 1525
SD7A11	M-7A11		E	89	47A01	23	17	29L	1-23X1	OBASE 1526
SD7A11	M-7A11		I	47A24	21	5	29L	2-31X1	OBASE 1527	
			A	4	49A00	FIRE DETECT & WARNING SYS				OBASE 1528
			A	4	49A01	FIRE & FAIRING DATA USE2				OBASE 1529
			H	49A03	FIRE DETECT & WARNING ENG & AMMO BAY				OBASE 1530	
09A21	F-9A21	09A21	F	95	49A01	21				OBASE 1531
09A21	F-9A21	09A21	F	95	49A01	21	24	29L	2423XC	OBASE 1532
09A22	B-9A22	09A22	F	66	49A01	21	13	29L	2423YC	OBASE 1532
09A22	B-9A22	09A22	F	33	49A01	21	09	29L	1-23X0	OBASE 1534
09A22	B-9A22	09A22	F	09	49A01	21	1	29L	1-31X1	OBASE 1535
09A22	B-9A22	09A22	F	17	49A01	21	06	29L	2-31X1	OBASE 1536
09A23	V-9A23	09A23	D	49A01	21	09	29L	1-23X1	OBASE 1537	
09A24	V-9A24	09A24	D	49A01	21				OBASE 1538	
09A24	V-9A24	09A24	D	4	51A01	THIS IS LAUNCH FOR 5110 APR8				OBASE 1539
E1L11	F-51L11	E1L11	E	15	51L10	21				OBASE 1540
E1L11	F-51L11	E1L11	E	15	51L10	21	4	29L	1-25L2	OBASE 1541
E1L11	RE1L11	IE1L11	E	15	51L10	21	2	29L	1326L2	OBASE 1542
E1L11	RE1L11	IE1L11	E	15	51L10	21	2	29L	1326L2	OBASE 1543
E1L11	RE1L11	IE1L11	E	15	51L10	21	3	29L	1326L2	OBASE 1544
E1L11	RE1L11	IE1L11	E	15	51L10	21	3	29L	1326L2	OBASE 1545
E1L11	RE1L11	IE1L11	E	15	51L10	21	3	29L	1326L2	OBASE 1546
E1L11	RE1L11	IE1L11	E	15	51L10	21	3	29L	1326L2	OBASE 1547
E1L11	RE1L11	IE1L11	E	4	51A01	VERIFIED BY TS POOL USE F15 DATA				OBASE 1548
E1A01	F-51A01	E1A01	F	5	51A01	21				OBASE 1549
E1A01	D-51A01	E1A01	D	51A01	21					OBASE 1550
E1A01	D-51A01	E1A01	D	51A01	21					OBASE 1551
E1A02	51A02	E1A02	D	75	51A01	21	15	29L	2326P2 1067 1C5	OBASE 1552
E1A02	51A02	E1A02	D	25	51A01	21	15	29L	2326P2 1-31X1 1C5	OBASE 1553
E1A03	SHOP	SE1A03	D	51A01	23					OBASE 1554
E1A03	51A03	IE1A03	D	10549	51A01	23				OBASE 1555
E1A03	51A03	IE1A03	D	51A01	21	10	29L	2326B2 1063 1C5	OBASE 1556	
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1557
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1558
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1559
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1560
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1561
E1A03	51A03	IE1A03	D	51A01	21	10	29L	2326B2 1063 1C5	OBASE 1562	
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1563
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1564
E1A03	51A03	IE1A03	D	51A01	23	15	29L	1326A1 1PTS2+	OBASE 1565	
E1A03	N51A03	IE1A03	D	90	51A01	23	5	29L	1326A1 1PTS2+	OBASE 1566
E1A03	N51A03	IE1A03	D	10238	51A01	23				OBASE 1567
E1A03	N51A03	IE1A03	D	51A01	23	4	51A01	F15 AIRSPEED INO 51A03 G FROM F15	OBASE 1568	
E1A03	K51A03	IE1A03	D	10	51A01	23	22	29L	1326A1	OBASE 1569
E1A03	N51A03	IE1A03	D	90	51A01	23	10	29L	1326A1	OBASE 1570
E1A03	N51A03	IE1A03	D	51A01	21	10	29L	2326B2 1060 1C5	OBASE 1571	
E1A03	51A03	IE1A03	D	51A01	23					OBASE 1572
E1A03	51A03	IE1A03	D	51A01	23	1	51A01	F15 VERTICAL SPEED INO 51A03 G NO DATE	OBASE 1573	
E1A03	K51A03	IE1A03	D	10	51A01	23	10	29L	1326A1	OBASE 1574
E1A03	N51A03	IE1A03	D	90	51A01	23	15	29L	1326A1	OBASE 1575
E1A03	Q51A03	IE1A03	D	51A01	21	10	29L	2326B2 1060 1C5	OBASE 1576	
E1A03	L51A03	IE1A03	D	10119	51A01	23				OBASE 1577
E1A03	51A03	IE1A03	D	51A01	23	4	51A01	F15 STAB AIRSPEED INO 51A03 G FROM F15	OBASE 1578	
E1A03	Q51A03	IE1A03	D	51A01	21	20	29L	2326B2 1060 1C5	OBASE 1579	
E1A03	Q51A03	IE1A03	D	51A01	23					OBASE 1580
E1A03	C51A03	IE1A03	D	51A01	23					OBASE 1581

IE1AG2 NS1AGG	E	9	51A00 23	10 29L 1326A1 1PTS2	DBASE 1532
IE1AG2 KS1AG	E	1	51A00 23	5 29L 1326A1 1PTS2	DBASE 1533
SE1AJ3 L51AH3 IE1AH3	G	11169	51A00 23		DBASE 1534
	M	51A00	F15 PRESSURE ALTIMETER 51AH3 G-F111F	DBASE 1535	
IE1AH3 051AH3	I	51A00 21	10 29L 232632 1060 105	DBASE 1586	
IE1AH3 051AH3 IE1AH3	O	51A00*23		DBASE 1537	
IE1AH3 051AH3 IE1AH2	C	51A00 23		DBASE 1538	
IE1AH3 KS1AH3	E	1	51A00 23	10 29L 1326A1 1PTS1	DBASE 1539
IE1AH3 NS1AH3	E	9	51A00 23	5 29L 1326A1 1PTS1	DBASE 1540
SE1AJ3 L51AH3 IE1AH3	G	11169	51A00 23		DBASE 1591
	M	51A00	F15 STBY GYFO ING G FRM F5E	DBASE 1592	
IE1AJ3 051AJ3	I	51A00 21	10 29L 232632 1060 105	DBASE 1597	
IE1AJ3 051AJ3 IE1AJ3	O	51A00*23		DBASE 1598	
IE1AJ3 051AJ3 IE1AJ2	C	51A00 23		DBASE 1599	
IE1AJ3 KS1AJ3	E	1	51A00 23	10 29L 1326A1 1PTS1P	DBASE 1596
IE1AJ3 NS1AJ3	E	9	51A00 23	5 29L 1326A1 1PTS1C	DBASE 1597
SE1AJ3 L51AJ3 IE1AJ3	G	11169	51A00 23		DBASE 1593
	M	51A00	F15 ALTITUDE ING 51AJ3 G FROM F.E.	DBASE 1593	
IE1AK3 K51AK3	E	1	51A00*23	10 29L 1326B1	DBASE 1600
IE1AK3 NS1AK3	E	9	51A00*23	5 29L 1326B1	DBASE 1601
IE1AK3 051AK3	I	51A00 21	10 29L 232632 1060 105	DBASE 1602	
SE1AJ3 L51AJ3 IE1AJ3	G	11169	51A00 23		DBASE 1613
	M	51A00	F15 ANGLE OF ATTACK ING 51AK3 G NO DATA	DBASE 1604	
IE1AL3 K51AL3	E	1	51A00*23	10 29L 1326B1	DBASE 1605
IE1AL3 NS1AL3	E	9	51A00*23	5 29L 1326B1	DBASE 1606
IE1AL3 051AL3	I	51A00 21	10 29L 232632 1060 105	DBASE 1607	
SE1AJ3 L51AJ3 IE1AJ3	G	11169	51A00 23		DBASE 1603
	M	51A00	F15 ACCELEROMETER ING 51AM3 G FROM F4E	DBASE 1609	
IE1AM3 051AM3	I	51A00 21	10 29L 232632 1060 105	DBASE 1610	
IE1AM3 051AM3 IE1AM3	O	51A00*23		DBASE 1611	
IE1AM3 051AM3 IE1AM2	C	51A00 23		DBASE 1612	
IE1AM3 K51AM3	E	1	51A00 23	10 29L 1326A1 1PTS25	DBASE 1613
IE1AM3 NS1AM3	E	9	51A00 23	5 29L 1326A1 1PTS25	DBASE 1614
	M	51E00	F111F AND F4E DATA USED	DBASE 1615	
	M	51E00	VERIFIED BY TS POOL IF PROBE FIXED	DBASE 1616	
	M	51E00	F15 AIR DATA SYS 51E00 F15=43	DBASE 1617	
E1EJ3 F51EJ3 E1EJ3	E	51	51E00 21		DBASE 1618
E1EJ3 051EJ3 F1EJ3	O	51E00 21		DBASE 1619	
E1EJ3 CALGP3 E1EJ3	C	51E00 21		DBASE 1620	
E1EJ3 K51EJ3 E1EJ3	E	6	51E00 21	10 29L 232632 1060 105	DBASE 1621
E1EJ3 R51EJ3 E1EJ3	E	4	51E00 21	10 29L 1431X1 1060 105	DBASE 1622
E1EJ3 SHP SE1EJ3	O	51E00 23		DBASE 1623	
SE1EJ3 L51EJ3 IE1EJ3	G	11190	51E00 23		DBASE 1624
	M	51E00	USED FOR G SELECT WORK AROUND	DBASE 1625	
	M	51E00	F111F 523244 FOR E SEL AND TIMES	DBASE 1626	
	M	51E00	F15 AIR DATA COMPUTER 51E00 F1E DATA	DBASE 1627	
IE1EA3 051EA3	I	51E00 21	10 29L 232632 1060 105	DBASE 1628	
IE1EA3 051EA3 IE1EA3	O	51E00*23		DBASE 1629	
IE1EA3 051EA3 IE1EA2	C	51E00 23		DBASE 1630	
IE1EA2 K51EA3	E	42	51E00 23	10 29L 1326A1 1PTS25 1TSC	DBASE 1631
IE1EA2 K51EA3	E	9	51E00 23	45 29L 1326A1 1PTS25 1TSC	DBASE 1632
IE1EA2 K51EA3	E	49	51E00 23	89 29L 1326A1 1PTS25 1TSC	DBASE 1633
SE1EA3 L51EA3 IE1EA3	G	11190	51E00 23		DBASE 1634
	M	51E00	F4E 51380 DATA USED	DBASE 1635	
	M	51E00	F15 ANGLE OF ATTACK TRANS 51E00	DBASE 1636	
IE1ED3 K51ED3	E	10	51E00*23	10 29L 1326B1	DBASE 1637
IE1ED3 NS1ED3	E	9	51E00*23	5 29L 1326B1	DBASE 1638
IE1ED3 051ED3	I	51E00 21	10 29L 232632 1060 105	DBASE 1639	
	M	51E00	VERIFIED BY TS POOL SUGEST NO SWING	DBASE 1640	
	M	51E00	F15 STBY COMPASS 51MBC F111F USED	DBASE 1641	
E1M03 F51M03 E1M03	E	426	51M00 21		DBASE 1642
E1M03 051M03 E1M03	O	51M00 21		DBASE 1643	
E1M03 CALGP3 E1M03	C	51M00 21		DBASE 1644	
E1M03 K51M03 E1M03	E	62	51M00 21	10 29L 232632 1060 105	DBASE 1645
E1M03 R51M03 E1M03	E	40	51M00 21	10 29L 1431X1 1060 105	DBASE 1646
E1M03 SHP SE1M03	O	51M00 23		DBASE 1647	

SE1M3C	L51M8J	IE1M9J	C	51M00 23	D <sub>BASE</sub> 1648
			4	51M00 F111F DATA USED	D <sub>BASE</sub> 1649
			4	51M00 F13 STBY COMPASS 51M9J	D <sub>BASE</sub> 1650
IE1M3C	051M8J	I	51M00 21	45 29L 232682 1060 105	D <sub>BASE</sub> 1651
IE1M3C	051M9C	0	51M00 23		D <sub>BASE</sub> 1652
			4	51M00 VERIFIED BY TS PCOLE SET CLOCK=75	D <sub>BASE</sub> 1653
			4	51M00 F13 INDICATOR SET 5.0NG F13=20	D <sub>BASE</sub> 1654
E1N1J	551M12	E1N1J	F	27 51M00 21	D <sub>BASE</sub> 1655
E1N1J	051M67	E1N1C	J	51M00 21	D <sub>BASE</sub> 1656
E1N1J	551M67	E1N1C	J	51M00 21	D <sub>BASE</sub> 1657
E1N1J	551M12	E1N1C	J	26 51M00 21 20 29L 232682 1060 105	D <sub>BASE</sub> 1658
E1N1J	551M12	E1N1C	J	13 51M00 21 13 29L 1-31X1 1060 105	D <sub>BASE</sub> 1659
E1N1J	551M12	E1N1C	J	52 51M00 21 10 29L 232682 1060 105	D <sub>BASE</sub> 1660
E1N1J	551M12	E1N1C	J	51M00 21	D <sub>BASE</sub> 1661
SE1M3C	L51M8J	IE1M9J	G	51M00 23	D <sub>BASE</sub> 1662
			4	51M00 F SEL AND TIMES FM TS BOUCHARD	D <sub>BASE</sub> 1663
			4	51M00 F15 HORIZ SITUATION IND 51M9J G=F15	D <sub>BASE</sub> 1664
IE1M3C	051M8J	-	51M00 21	15 29L 232682 1060 105	D <sub>BASE</sub> 1665
IE1M3C	051M8J	IE1M9J	J	51M00 23	D <sub>BASE</sub> 1666
IE1M3C	051M8J	IE1M9J	J	51M00 23	D <sub>BASE</sub> 1667
IE1M3C	051M8J	IE1M9J	J	17 51M00 23 21 29L 1326A1 1PTS41 1TSD	D <sub>BASE</sub> 1668
IE1M3C	051M8J	IE1M9J	J	9 51M00 23 21 29L 1326A1 1PTS41 1TSD	D <sub>BASE</sub> 1669
SE1M3C	L51M8J	IE1M9J	S	13595 51M00 23	D <sub>BASE</sub> 1670
			4	51M00 TIMES FM F111F 51M9J	D <sub>BASE</sub> 1671
			4	51M00 THIS IS WORK AROUND	D <sub>BASE</sub> 1672
			4	51M00 F15 FLT DIRECTOR ADAPTER 51M9J G=F15	D <sub>BASE</sub> 1673
IE1M3C	051M8J	I	51M00 21	15 29L 232682 1060 105	D <sub>BASE</sub> 1674
IE1M3C	051M8J	IE1M9J	I	51M00 23	D <sub>BASE</sub> 1675
IE1M3C	051M8J	IE1M9J	I	51M00 23	D <sub>BASE</sub> 1676
IE1M3C	051M8J	IE1M9J	I	1 51M00 23 25 29L 1326A1 1PTS42 1TSD	D <sub>BASE</sub> 1677
IE1M3C	051M8J	IE1M9J	I	97 51M00 23 26 29L 1326A1 1PTS42 1TSD	D <sub>BASE</sub> 1678
			4	52A00 DATA 52A4F+52A4G+52A4H USED FOR HSB-A	D <sub>BASE</sub> 1679
			4	52A00 F15 DATA AUG-75 MS3MA -20 CK A70	D <sub>BASE</sub> 1680
			4	52A00 VERIFIED BY TS PCOLE	D <sub>BASE</sub> 1681
			4	52A00 F15 AUTO FLT CONT SET ASW38 F111F	D <sub>BASE</sub> 1682
E2A1J	F52A1J	E2A1J	F	35 52A00 21	D <sub>BASE</sub> 1683
E2A1J	052A1J	E2A1J	J	52A00 21	D <sub>BASE</sub> 1684
E2A1J	052A1J	E2A1J	J	52A00 21	D <sub>BASE</sub> 1685
E2A1J	052A1J	E2A1J	J	74 52A00 21 26 29L 232682 1060 1TU228	D <sub>BASE</sub> 1686
E2A1J	052A1J	E2A1J	J	5 52A00 21 15 29L 1-31X1	D <sub>BASE</sub> 1687
E2A1J	052A1J	E2A1J	J	12 52A00 21 15 29L 1-31X1 1060 1TU228	D <sub>BASE</sub> 1688
E2A1J	052A1J	E2A1J	J	17 52A00 21 17 29L 232682 1060 1TU228	D <sub>BASE</sub> 1689
E2A1J	052A1J	E2A1J	J	52A00 23	D <sub>BASE</sub> 1690
SE2A1J	L52A1J	IE2A1J	G	52A00 23	D <sub>BASE</sub> 1691
			4	52A00 TS BOUCHARD-THIS IS PRESENTLY WORK	D <sub>BASE</sub> 1692
			4	52A00 AROUND ITEM COULD NOT GIVE ESTIMATES	D <sub>BASE</sub> 1693
			4	52A00 F15 PITCH FLT CONT COMPUTER 52A4C	D <sub>BASE</sub> 1694
IE2A1J	052A1J	-	52A00 21	25 29L 232682 1060 1TU228	D <sub>BASE</sub> 1695
IE2A1J	052A1J	IE2A1J	I	52A00 21	D <sub>BASE</sub> 1696
IE2A1J	052A1J	IE2A1J	I	52A00 21	D <sub>BASE</sub> 1697
IE2A1J	052A1J	IE2A1J	I	33 52A00 23 23 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1698
IE2A1J	052A1J	IE2A1J	I	34 52A00 23 25 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1699
IE2A1J	052A1J	IE2A1J	I	33 52A00 23 46 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1700
SE2A1J	L52A1J	IE2A1J	G	52A00 23	D <sub>BASE</sub> 1701
			4	52A00 TS BOUCHARD-WORK AROUND	D <sub>BASE</sub> 1702
			4	52A00 F15 ROLL-YAW FLT CONT COMPUTER E2A3J	D <sub>BASE</sub> 1703
IE2A1J	052A1J	I	52A00 21	25 29L 232682 1060 1TU228	D <sub>BASE</sub> 1704
IE2A1J	052A1J	IE2A1J	I	52A00 21	D <sub>BASE</sub> 1705
IE2A1J	052A1J	IE2A1J	I	52A00 23	D <sub>BASE</sub> 1706
IE2A1J	052A1J	IE2A1J	I	37 52A00 23 46 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1707
IE2A1J	052A1J	IE2A1J	I	32 52A00 23 23 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1708
IE2A1J	052A1J	IE2A1J	I	34 52A00 23 25 29L 1326A1 1PTS12 1TSC	D <sub>BASE</sub> 1709
SE2A1J	L52A1J	IE2A1J	G	52A00 23	D <sub>BASE</sub> 1710
			4	52A00 TS BOUCHARD GAVE TIME ESTIMATES BUT	D <sub>BASE</sub> 1711
			4	52A00 WAS UNSURE OF E SELECT AND W TASK	D <sub>BASE</sub> 1712
			4	52A00 USED F111F FOR THESE	D <sub>BASE</sub> 1713

IE2A7	032AC0	I	52A00	F15 RATE SENSOR ASSY 52AC0 G=F111F	OBASE 1714	
IE2A8	032AC0	I	52A01	21 25 29L 232682 1060 1TU228	OBASE 1715	
IE2A9	032AC0	I	52A02	*23	OBASE 1716	
IE2A10	032AC0	I	52A03	23	OBASE 1717	
IE2A11	032AC0	I	52A04	23	OBASE 1718	
IE2A12	032AC0	E	43	52A05 23 20 29L 132641 1PTS4 1TSC	OBASE 1719	
IE2A13	032AC0	E	31	52A06 23 20 29L 132641 1PTS4 1TSC	OBASE 1719	
IE2A14	032AC0	E	27	52A07 23 20 29L 132641 1PTS4 1TSC	OBASE 1720	
SE2A1	L32A11	I	52A08	23	OBASE 1721	
IE2A15	032AL0	I	52A09	TS ECOUGHAD LAVE TIME ESTIMATES G=F111D F1CE 1722	OBASE 1722	
IE2A16	032AL0	I	52A10	F15 ACCELEROMETER SENSOR ASSY 52ALL	OBASE 1723	
IE2A17	032AL0	I	52A11	21 25 29L 232682 1061 1TU228	OBASE 1724	
IE2A18	032AL0	I	52A12	*23	OBASE 1725	
IE2A19	032AL0	I	52A13	23	OBASE 1726	
IE2A20	032AL0	I	52A14	21 25 29L 132641 1PTS27 1TSC	OBASE 1727	
IE2A21	032AL0	E	21	52A15 23 20 29L 132641 1PTS27 1TSC	OBASE 1728	
IE2A22	032AL0	E	77	52A16 23 20 29L 132641 1PTS27 1TSC	OBASE 1729	
SE2A23	L32A11	I	52A17	23	OBASE 1730	
IE2A24	032AM0	I	52A18	TS ECOUGHAD COULD NOT EST-ING W TASK	OBASE 1731	
IE2A25	032AM0	I	52A19	F15 DYNAMIC PRESSURE SENSOR 52AM0	OBASE 1732	
IE2A26	032AM0	I	52A20	21 30 29L 232682 1060 1TU228	OBASE 1733	
IE2A27	032AM0	I	52A21	*23	OBASE 1734	
IE2A28	032AM0	I	52A22	23	OBASE 1735	
IE2A29	032AM0	E	15	52A23 23 5 29L 132641 1PTS17 1TSC	OBASE 1736	
IE2A30	032AM0	E	9	52A24 23 5 29L 132641 1PTS17 1TSC	OBASE 1737	
IE2A31	032AM0	E	42	FSLL0 21	THIS IS LAUNCH FOR 55L05 AREA	OBASE 1738
IE2A32	032AM0	I	55L05	21 3 29L 1326L2	OBASE 1739	
IE2A33	032AM0	I	55L06	THREE IS NO COMP EQUIP F15 DATA USED	OBASE 1740	
IE2A34	032AM0	I	55L07	THIS IS NETWORK FOR 517 ON F15 55A01	OBASE 1741	
IE2A35	032AM0	I	55L08	21	OBASE 1742	
IE2A36	032AM0	I	55L09	21	OBASE 1743	
IE2A37	032AM0	I	55L10	21	OBASE 1744	
IE2A38	032AM0	I	55L11	21	OBASE 1745	
IE2A39	032AM0	E	95	55A01 21 20 29L 232632 1060 105	OBASE 1746	
IE2A40	032AM0	E	5	55A02 21 20 29L 232682 1060 105	OBASE 1747	
IE2A41	032AM0	I	55A03	21	OBASE 1748	
IE2A42	032AM0	I	55A04	21	OBASE 1749	
IE2A43	032AM0	I	55A05	21	VERIFIED BY TS OBERLY	OBASE 1750
IE2A44	032AM0	I	55A06	21	OBASE 1751	
IE2A45	032AM0	E	15	55A07 *23 25 29L 132681	OBASE 1752	
IE2A46	032AM0	E	9	55A08 *23 20 29L 1326P1	OBASE 1753	
IE2A47	032AM0	I	55A09	21 20 29L 232632 1060 105	OBASE 1754	
IE2A48	032AM0	I	55A10	21	OBASE 1755	
IE2A49	032AM0	I	55A11	21	VERIFIED BY TS OBERLEY	OBASE 1756
IE2A50	032AM0	I	55A12	21	OBASE 1757	
IE2A51	032AM0	E	65	55A00 *23 40 29L 132681	OBASE 1758	
IE2A52	032AM0	I	55A13	21 30 29L 132681	OBASE 1759	
IE2A53	032AM0	E	25	55A04 *23 30 29L 132681	OBASE 1760	
IE2A54	032AM0	I	55A14	21 10 29L 232682 1061 105	OBASE 1761	
IE2A55	032AM0	I	55A15	21	F111F 55A01 AND 55A04 ARE USED AS COMPOUNDED	OBASE 1762
IE2A56	032AM0	I	55A16	21	THIS IS NETWORK FOR F15 SIG DATA PC-OFG 105	OBASE 1763
IE2A57	032AM0	E	65	55A05 21	OBASE 1764	
IE2A58	032AM0	I	55A17	21	OBASE 1765	
IE2A59	032AM0	I	55A18	21	OBASE 1766	
IE2A60	032AM0	E	55A19	21 10 29L 232632 1060 105	OBASE 1767	
IE2A61	032AM0	I	55A20	21	OBASE 1768	
IE2A62	032AM0	I	55A21	21	OBASE 1769	
IE2A63	032AM0	I	55A22	21	SELECT AND TASK TIME ESTIMATES GIVEN	OBASE 1770
IE2A64	032AM0	I	55A23	21	BY TSGT ROBERTS 01-04 514-23	OBASE 1771
IE2A65	032AM0	I	55A24	21	F15 SIG DATA RECORDER FROM F15 DATA	OBASE 1772
IE2A66	032AM0	I	55A25	21 240 29L 2326P2	OBASE 1773	
IE2A67	032AM0	I	55A26	21	OBASE 1774	
IE2A68	032AM0	I	55A27	21	OBASE 1775	
IE2A69	032AM0	E	30	55A28 21 20 29L 232641 1PTS3 1TSC	OBASE 1776	
IE2A70	032AM0	E	30	55A29 21 00 29L 232641 1PTS3 1TSC	OBASE 1777	
IE2A71	032AM0	E	4	55A30 21 00 29L 232641 1PTS3 1TSC	OBASE 1778	
IE2A72	032AM0	I	55A31	21	OBASE 1779	

		55300	VERIFIED BY TS BOUCHARD	DBASE 1780
		55300	F15 CASSETTE FROM F111F 55AAA DATA	DBASE 1781
IES8E1	0553E1	I	55PJJ 21 24 29L 232692	DBASE 1782
IES8E1	0553E1	I	55C00 23	DBASE 1783
		55C00	F111F SEACO USED F15 MSBMA=213	DBASE 1784
		55C00	VERIFIED BY TS POOLE 2733	DBASE 1785
		55C00	F15 ACCELEROMETER COUNTER 55CC0	DBASE 1786
ESC01	E55C1	F	75 55C10 21	DBASE 1787
ESC01	D55H7	E55C1	55C00 21	DBASE 1788
ESC01	C5LG91	E55C1	55C11 21	DBASE 1789
ESC12	R55C13	E55C13	97 55C00 21 13 29L 232692 1060 105	DBASE 1790
		55C00	E SELECT FROM F15 DATA	DBASE 1791
ESC12	455C13	E	3 55C00 21 10 29L 232692 1060 105	DBASE 1792
ESC12	SM7P	E55C13	55C12 23	DBASE 1793
SE5C01	L55C43	IESCA1	3 .357 55C00 23	DBASE 1794
		55C00	F15 DATA USED NO F111F SHOT DATA	DBASE 1795
		55C00	TASK TIME EST BY TS BOUCHARD	DBASE 1796
		55C00	DIGITAL READOUT ELECT COUNTERS 55C00	DBASE 1797
IESCA1	255C13	I	55C00 21 20 29L 232692 1060 105	DBASE 1798
IESCA1	255C14	IESCA1	55C110 21	DBASE 1799
IESCA1	055C14	E55C12	55C10 23	DBASE 1800
IESCA1	155C12	E55C12	5 55C00 23 40 29L 1326A1 1PTS19 1TSC	DBASE 1801
IESCA2	K55C12	E	2 55C00 23 25 29L 1326A1 1PTS19 1TSC	DBASE 1812
IESCA2	155C12	E	92 55C00 23 25 29L 1326A1 1PTS19 1TSC	DBASE 1843
SE5C01	L55C31	IESCA2	5 01119 55C00 23	DBASE 1854
		55C00	F15 DATA USED NO F111F DATA AVAIL	DBASE 1855
		55C00	NO W TASK TIME EST BY TS BOUCHARD	DBASE 1856
		55C00	LINEAR ELECT ACCELEROMETER 55C00	DBASE 1857
IESC3	Q55C32	I	55C00 21 20 29L 232692 1060 105	DBASE 1858
IESC3	055C32	IESCA2	55C110 23	DBASE 1803
IESC3	C55C32	IESCA2	55C00 23	DBASE 1810
IESC3	N55C32	IESCA2	87 55C00 23 12 29L 1326A1 1PTS16 1TSC	DBASE 1811
IESC3	K55C32	IESCA2	19 55C00 23 10 29L 1326A1 1PTS16 1TSC	DBASE 1812
		57101	THIS IS LAUNCH FOR 5700 AREA	DBASE 1813
EPL11	F57L11	E57L01	71 57L10 21	DBASE 1814
EPL11	57L11	E57L01	57L10 21 2 29L 1326L2	DBASE 1815
		57A00	THIS IS NETWORK FOR F15 CENTRAL	DBASE 1816
		57A00	COMPUTER 57A00 THERE IS NO COMP	DBASE 1817
		57A00	DATA F15 DATA USED	DBASE 1818
		57A00	VERIFIED BY TS FAY	DBASE 1819
		57A00	F15 CENTRAL COMPUTER	DBASE 1820
E7A11	F57A11	E7A11	21 57A00 21	DBASE 1821
E7A11	D57H7	E7A11	57A00 21	DBASE 1822
E7A11	C5LG91	E7A11	57A00 21	DBASE 1823
E7A12	R57A01	E7A03	17 51A11 21 8 29L 2326A2 1050 105 1431X1	DBASE 1824
E7A12	M57A01	E	83 57A00 21 10 29L 2326A2 1060 105	DBASE 1825
E7A13	SM7P	SE7A01	57A00 23	DBASE 1826
SE7A01	L57A01	E7A01	57A00 23	DBASE 1827
		57A00	WORK AP JUNO	DBASE 1828
		57A00	F15 57A00 CENT COMP F15 DATA USED	DBASE 1829
IE7A01	Q57A01	I	57A00 21 8 29L 2326A2	DBASE 1830
IE7A01	D57A01	IE7A01	57A00 23	DBASE 1831
IE7A01	C57A01	IE7A02	57A00 23	DBASE 1832
IE7A02	H57-11	E	65 57A00 23 45 29L 1326A1 1PTS21 1TSC	DBASE 1833
IE7A02	N57-11	E	29 57A00 23 35 29L 1326A1 1PTS21 1TSC	DBASE 1834
IE7A02	K57-11	E	6 57A00 23 29 29L 1326A1 1PTS21 1TSC	DBASE 1835
		63L00	THIS IS LAUNCH FOR 6310 AREA	DBASE 1836
F3L11	F63L01	F3L01	12 63L00 21	DBASE 1837
F3L11	RF3A03	F3L01	39 63L00 21 1 29L 1326L2	DBASE 1838
F3L11	RF3A03	F3L01	39 63L00 21 2 29L 1326L2	DBASE 1839
F3L11	RF3A03	F3L01	62 63L00 21 1 29L 1326L2	DBASE 1840
F3L11	RF3A03	F3L01	62 63L00 21 3 29L 1326L2	DBASE 1841
		62A00	COMP DATA FROM F111F AND 17D USED	DBASE 1842
		63A00	VERIFIED BY TSGT FIELD 7303	DBASE 1843
		63A00	THIS NETWORK IS FOR THE 63A AREA F15	DBASE 1844
		63A00	UHF COMM SET AFC 1w9 F15	DBASE 1845

F3A11	F6343	F3A01 F	27	63200	21	DBASE 1346	
F3A11	00-107	F3A01 2	27	63410	21	OBASE 1347	
F3A14	C4LGPJ	F3002 3	63200	21	DBASE 1348		
F3A12	63310	F3A03 E	56	63210	21	DBASE 1349	
F3A12	63310		69	63210	21	13 29L 232602 1060 105	
F3A13	SMDF	SF3A01 7	63210	23	12 29L 232602 1060 105		
SF3A01	L63401	IF3401 3	2335	63400	23	DBASE 1450	
			1	63400	COMP F111F 63400	DBASE 1451	
			4	63400	F15 UHF RT 63400	DBASE 1452	
IF3401	W63401	IF3401 3	77	63210	23	DBASE 1453	
IF3401	K63401		11	63210	23	DBASE 1454	
IF3401	M63401		13	63210	23	DBASE 1455	
IF3401	263401		1	63210	21	DBASE 1456	
IF3401	263401		4	63210	21	12 29L 232602	
IF3401	W63401		4	63210	HC3-LA1 INDICATES THE LEAK CHECK	DBASE 1457	
IF3401	W63401		3	63400	23	DBASE 1458	
SF3A01	L63401	IF3401 3	1067	63400	23	DBASE 1459	
			4	63400	COMP A70 63400	DBASE 1460	
			4	63400	W63401 DATA REFLECTED AT PRECENT FIX	DBASE 1461	
			4	63400	EXPERIENCE AND CAPABILITY WILL MAKE A	DBASE 1462	
			4	63400	65 PRECENT REPAIRS POSSIBLE	DBASE 1463	
			4	63400	F15 UHF BACKUP RECEIVER	DBASE 1464	
IF3401	W63401		89	63210	23	DBASE 1465	
IF3401	N63401		15	63210	23	DBASE 1466	
IF3401	O63401		21	63210	21	DBASE 1467	
			4	63400	THEFE IS NO DATA FOR SECURE VOICE OR	DBASE 1468	
			4	63400	IN-SHOP ANTENNA REPAIR	DBASE 1469	
			4	63400	THIS NETWORK IS FOR THE 639 AREA F15	DBASE 1470	
			4	63400	IT COVERS ALL CONTROL PANELS	DBASE 1471	
			H	63700	334F DATA FROM F111F AND F46	DBASE 1472	
			4	63700	VERIFIED BY TEST FIELD 7318	DBASE 1473	
			4	63300	INTEG CNI CONT SET F15	DBASE 1474	
F3211	F63801	F3901 F	25	63200	21	DBASE 1475	
F3211	00-107	F3901 3	63200	21	DBASE 1476		
F3211	C4LGPJ	F3902 2	63200	21	DBASE 1477		
F3211	63350	F3903 E	56	63300	21	DBASE 1478	
F3211	M63350		45	63300	21	16 29L 232602 1060 105	
F3211	N63350		4	15	63300	21	12 29L 2431X1
F3211	S40P	SF3201 3	63200	23	DBASE 1479		
SF3201	L63300	IF3201 3	13203	63300	23	DBASE 1480	
			1	63300	670 AREA FOR SHOP WORK VERIFIED BY	DBASE 1481	
			4	63300	TEST OFFERLY 7322	DBASE 1482	
			4	63200	ADDED N63300 AND ADJ E SELECT MODES	DBASE 1483	
			4	63200		DBASE 1484	
IF3201	W63300		71	63200	23	DBASE 1485	
IF3201	K63300		15	63200	23	DBASE 1486	
IF3201	N63300		15	63200	23	DBASE 1487	
IF3201	Q63300		I	63200	21	20 29L 232602 1060 105	
SF3201	L63300	IF3201 3	13202	63200	23	DBASE 1488	
			4	63200	ADDED N63300 AND ADJ E SELECT MODES	DBASE 1489	
			H	63200		DBASE 1490	
IF3201	W63300		75	63200	23	15 29L 132691	
IF3201	K63300		15	63200	23	DBASE 1491	
IF3201	N63300		10	63200	23	10 29L 132691	
IF3201	Q63300		I	63200	21	10 29L 232602	
			4	63200	F15 CNI CONTROL USED 63400 AND 64000	DBASE 1492	
			4	63200	F4CH F111F AS COMP	DBASE 1493	
			4	63200	F15 NAVATIS COPY USED 7100A AND 7100AC	DBASE 1494	
			H	63200	F4CH F111F AS COMP	DBASE 1495	
			4	63200		DBASE 1496	
'SF3201	L63300	IF3201 3	13160	63200	23	DBASE 1497	
			1	63200	F15 IFF USED 65400 FROM F111F AS COMP	DBASE 1498	
IF3201	W63300		64	63200	23	15 29L 132691	
IF3201	K63300		15	63200	23	DBASE 1499	
IF3201	N63300		16	63200	23	10 29L 132691	
IF3201	Q63300		63200	71	12 29L 232602	DBASE 1500	
SF3201	L63300	IF3201 3	13167	63200	23	DBASE 1501	

4	63000	F15 MAIN COMM CONTROL USED 67A9C AND	DBASE 1912		
M	63001	ADDED N63EM1 AND ADJ SELE SELECT MODES	DBASE 1913		
4	63002	660AO FROM F121 AS COMM	DBASE 1914		
M	63003		DBASE 1915		
IF3941	463SM3	E 35 63000*23 15 29L 132691	DBASE 1916		
IF3941	X63SM3	E 35 63001*23 15 29L 132691	DBASE 1917		
IF3941	463SM3	E 24 63000*23 15 29L 132691	DBASE 1918		
IF3941	X63SM3	E 24 63001*23 15 29L 132691	DBASE 1919		
SF3941	L63SM3	IF3941 G 3595 63001*23		DBASE 1920	
		ADDED K63EM1 AND N63EM1 AND ADJ SELECT MODES	DBASE 1921		
		M 63002 MODES	DBASE 1922		
		M 63003	DBASE 1923		
IF3942	W63SM3	E 80 63000*23 15 29L 132691	DBASE 1924		
IF3942	X63SM3	E 15 63001*23 15 29L 132691	DBASE 1925		
IF3942	463SM3	E 15 63000*23 15 29L 132691	DBASE 1926		
IF3942	X63SM3	E 15 63001*23 15 29L 132691	DBASE 1927		
		4 63002 THE AAI COMM BK1 IS F15 DATA USED	DBASE 1928		
		5EL12 THIS IS LAUNCH F15 29L AREA	DBASE 1929		
FSL11	F55L11	F55L11 E 63 65L01 21		DBASE 1930	
FSL11	REF55L11	IF55L11 65L01 21		DBASE 1931	
		4 65A00 F111F 65A10-65ACF IS USED AS COMM	DBASE 1932		
		4 65A01 VERIFIED BY TSGT FIELD	DBASE 1933		
		M 65A02 THIS IS IFF TRANSPONDER APX131 FOR F150	DBASE 1934		
FS5A11	F55A11	F55A11 E 47 65L01 21		DBASE 1935	
FS5A11	00RMG7	F55A11 65A00 21		DBASE 1936	
FS5A11	00LG01	F55A11 65L01 21		DBASE 1937	
FS5A12	F55A12	F55A12 E 90 65A00 21 18 29L 232602 1060 105		DBASE 1938	
FS5A12	455A12	E 15 65A00 21 18 29L 232602 1060 105		DBASE 1939	
FS5A12	455A12	E 20 65A00 21 20 29L 1431X1		DBASE 1940	
FS5A12	X55A12	E 20 65A00 21		DBASE 1941	
SF5A12	L65A12	IF55A12 65A00 23		DBASE 1942	
SF5A12	IF55A12	65A00 23		DBASE 1943	
		4 65A10 THREE IS 10 DATA TO INDICATE 65A00	DBASE 1944		
		H 65A00 WORK EITHER F15 OR COMM ACFT	DBASE 1945		
		4 65A01 VERIFIED SHCP WORK WITH TSGT OBERLEY	DBASE 1946		
		4 65A02 PH#7312	DBASE 1947		
		4 65A03 F15 RX/TX F111F 65A00 AS COMM	DBASE 1948		
IF55A13	465A13	E 70 65A00*23 16L 29L 132691		DBASE 1949	
IF55A13	X65A13	E 5 65A00*23 70 29L 132691		DBASE 1950	
IF55A13	465A13	E 25 65A00*23 00 29L 132691		DBASE 1951	
IF55A13	X65A13	E 25 65A00*23 15 29L 232602		DBASE 1952	
		4 65A00 THIS IS NETWORK FOR AAI IFF F15 DATA	DBASE 1953		
		H 65A01 USED AS COMM DATA NOT AVAILABLE	DBASE 1954		
		4 65A02 AAI IFF	DBASE 1955		
F55A13	F55A13	F55A13 E 5 65A00 21		DBASE 1956	
F55A13	00RMG7	F55A13 65A00 21		DBASE 1957	
F55A13	00LG01	F55A13 65A00 21		DBASE 1958	
F55A13	455A13	F55A13 E 70 65A00 21 25 29L 232602 1060 105		DBASE 1959	
F55A13	X55A13	F55A13 65A00 21 7 29L 232602 1060 105		DBASE 1960	
F55A13	455A13	E 30 65A00 21 17 29L 232602 1060 105		DBASE 1961	
F55A13	X55A13	E 30 65A00 21 18 29L 232602 1060 105		DBASE 1962	
F55A13	SHCP	SF55A13 65A00 23		DBASE 1963	
SF55A13	455A13	IF55A13 65A00 23		DBASE 1964	
		4 65A00 F15 AAI RT860/APX75 F15 DATA USE4	DBASE 1965		
		4 65A01 ADJEC X55A13 AND AII SELECT MODES	DBASE 1966		
		H 65A00 VERIFIED SHCP WORK WITH TSGT OBERLEY	DBASE 1967		
		4 65A00 PH#7312	DBASE 1968		
		4 65A00 SGT OBERLEY GAVE BEST ESTIMATES OF	DBASE 1969		
		H 65A00 TASK TIME REQUIREMENTS ALL CREW SIZES	DBASE 1970		
		H 65A00 ARE 1	DBASE 1971		
		H 65A00 F15 AAI RT860/APX75	DBASE 1972		
IF55A14	455A14	E 71 65A00*23 100 29L 132691		DBASE 1973	
IF55A14	X55A14	E 5 65A00*23 45 29L 132691		DBASE 1974	
IF55A14	465A14	E 24 65A00*23 40 29L 132691		DBASE 1975	
IF55A14	X65A14	E 24 65A00*23 23 29L 232602		DBASE 1976	
SF55A14	LOGSMC	IF55A14 65A00*23		DBASE 1977	
		4 65A00 F15 AAI TARGET PROCESSOR F15 DATA USE00	DBASE 1978		

IF5E4U	0552H2	I	65900	21	23 29L 2326C2	DBASE 1978	
IF5341	0552H2	I	65900	23	65900 23	DBASE 1979	
IF5341	0552H2	I	65900	23	65900 23	DBASE 1981	
IF5342	0552H2	E	32	65900 23	71 29L 1326A1 1PTSA 1TSD	DBASE 1981	
IF5P42	N55BH2	E	67	65900 23	15 29L 2326A1 1PTSA 1TSD	DBASE 1982	
				71000	THIS IS LAUNCH FOR 71000 ASEA	DBASE 1983	
G13J	F71L1	G13J1	F	71000	21	DBASE 1984	
G13J1	R71L1	I	15	71000 21	4 29L 2326L2	DBASE 1985	
G13J1	R71L2	I	75	71000 21	3 29L 2326L2	DBASE 1986	
G13J1	R71L3	I	21	71000 21	2 29L 2326L2	DBASE 1987	
			4	71000	770 WAS GIVEN AS COMPARABLE BUT THIS	DBASE 1988	
			H	71000	SYSTEM SHOULD BE MUCH BETTER THE 770	DBASE 1989	
			H	71000	ENGINEER'S SUBSYSTEM COULD NOT ESTIMATE CHARGE	DBASE 1990	
			H	71000	HOW MUCH ENERGY WOULD GO INTO 770	DBASE 1991	
			H	71000	73FA1+73GB1+73FD1+73FF1+77FC1 THE LAST ONE	DBASE 1992	
			H	71000	BEING FOR THE INS UNIT END F15 71400 DBASE 1993	DBASE 1993	
			H	71000	VERIFIED BY TSGT RAY 470 17 F15=1	DBASE 1994	
			H	71000	THIS IS NETWORK FOR F15 THE 71000	DBASE 1995	
G1A3J	F71A1	G1A3J1	F	13	71000 21	DBASE 1996	
G1A3J	R71A1	I	71000	21	-	DBASE 1997	
G1A3J	CALGPJ	G1A3J2	C	71000	21	DBASE 1998	
G1A3J	R71A2	G1A3J3	E	8-	71000 21	17 29L 2326A2 1060 105	DBASE 1999
G1A3J	R71A3	E	16	71000 21	22 29L 2326A2 1060 105	DBASE 2000	
G1A3J	R71A4	A	21	71000 21	19 29L 2326A2	DBASE 2001	
G1A3J	SHP	SG1A3J	D	71000	23	DBASE 2002	
SG1A3J	L71AK1	IG1A3J	G	13136	71000 23	DBASE 2003	
			4	71000	F15 INS UNIT USED AND 73FA1+73FD1+	DBASE 2004	
			H	71000	73FF1+73GC1 THE F15 HAS EVERYTHING IN	DBASE 2005	
			H	71000	ONE UNIT E SELECT AND TIMES AND	DBASE 2006	
			H	71000	VERIFIED BY TS POUCHARD WORK AROUND	DBASE 2007	
			H	71000	E SEL AND TIMES FM 470	DBASE 2008	
			H	71000	F15 INS UNIT	DBASE 2009	
IG1A3J	Q71AK1	I	71000	21	10 29L 2326A2 1060 105	DBASE 2010	
IG1A3J	Q71AK1	IG1A3J1	C	71000	23	DBASE 2011	
IG1A3J	Q71AK1	IG1A3J2	C	71000	23	DBASE 2012	
IG1A3J	W71AK1	E	4-	71000	23	96 29L 1T26A1 1PTSA 1TSD	DBASE 2013
IG1A3J	K71AK1	E	20	71000	23	75 29L 1326A1 1PTSA 1TSD	DBASE 2014
IG1A3J	K71AK1	E	28	71000	23	58 29L 1326A1 1PTSA 1TSD	DBASE 2015
SG1A3J	L71AK1	IG1A3J	G	13136	71000 23	DBASE 2016	
			4	71000	F15 INS CONT-ING 470 77FC1 DATA USED	DBASE 2017	
			H	71000	E SELECT AND TASK TIMES AND DATA	DBASE 2018	
			H	71000	VERIFIED BY TS POUCHARD WORK AROUND	DBASE 2019	
			H	71000	F15 INS CONT	DBASE 2020	
IG1A3J	Q71AK1	I	71000	21	10 29L 2326A2 1060 105	DBASE 2021	
IG1A3J	Q71AK1	IG1A3J1	C	71000	23	DBASE 2022	
IG1A3J	Q71AK1	IG1A3J2	C	71000	23	DBASE 2023	
IG1A3J	W71AK1	E	54	71000	23	46 29L 1326A1 1PTSA 1TSD	DBASE 2024
IG1A3J	K71AK1	E	21	71000	23	10 29L 1326A1 1PTSA 1TSD	DBASE 2025
IG1A3J	W71AK1	E	23	71000	23	10 29L 1326A1 1PTSD 1TSD	DBASE 2026
			4	71000	F15 71000 DATA USED	DBASE 2027	
			H	71000	VERIFIED BY TSGT FIELD	DBASE 2028	
			H	71000	THIS IS NETWORK FOR F15 ACF 71000	DBASE 2029	
G13J	F71B1	G13J1	F	3-5	71000 21	DBASE 2030	
G13J1	R71B1	I	71000	21	-	DBASE 2031	
G13J1	CALGPJ	G13J2	C	71000	21	DBASE 2032	
G13J2	R71B1	G13J3	E	85	71000 21	25 29L 2326C2 1060 105	DBASE 2033
G13J2	R71B1	E	15	71000	21	20 29L 2326C2 1060 105 1411X1	DBASE 2034
			4	71000	THREE IS NO SIGNIFICANT SHAP DATA FOR	DBASE 2035	
			H	71000	THIS SUBSYSTEM DATA BY TS POUCHARD	DBASE 2036	
			H	71000	THIS IS NETWORK FOR F15 ACF 71000	DBASE 2037	
G13J3	L71B1	IG13J1	J	71000	23	DBASE 2038	
IG1A3J	W71B1	E	71	71000	23	30 29L 1326B1	DBASE 2039
IG1A3J	K71B1	E	20	71000	23	20 29L 1326B1	DBASE 2040
IG1A3J	W71B1	E	15	71000	23	20 29L 1326B1	DBASE 2041
IG1A3J	Q71B1	I	71000	21	20 29L 2326C2 1060 105	DBASE 2042	
			4	71000	F11F 71000 DATA USED F15 MSE4A 1060 DBASE 2043	DBASE 2043	

			71C00	VERIFIED BY TSGT FIELD		DBASE 2044
			71C01	THIS IS NETWORK FOR F15 ILS 71CAB		DBASE 2145
G1C01	F71C01	G1C01	F	333 71C01 21		DBASE 2146
G1C01	722107	G1C01	T	71C01 21		DBASE 2147
G1C01	34LGPJ	G1C02	S	71C01 21		DBASE 2148
G1C02	971C01	G1C01	E	31 71C00 21	21 29L 232682 1050 105	DBASE 2149
G1C02	M71C03	E	11 71C01 21	14 29L 232682 1050 105	1431X1 DBASE 2051	
G1C03	S40P	SG1C01	T	71C01 21		DBASE 2151
SG1C03	L71C02	IG1C03	D	71C01 23		DBASE 2052
			71C04	F15 ILS FC/F 71CAB USED F111F 71C02		DBASE 2152
			71C05	VERIFIED BY TS OBERLY		DBASE 2153
			71C06	F15 ILS FC/D		DBASE 2153
IG1C04	M71C03	E	75 71C00*23	30 29L 132681		DBASE 2056
IG1C04	K71C03	E	15 71C01*23	24 29L 132681		DBASE 2157
IG1C04	N71C03	E	14 71C00*23	20 29L 132681		DBASE 2158
IG1C04	O71C03	I	71C01 21	1 29L 232682 1050 105	DBASE 2159	
			71C06	F111F 71340 DATA USED F15 MS341 76		DBASE 2159
			71C07	VERIFIED BY TSGT FIELD 443 37 FOR F111D DBASE 2053		
			71C08	THIS IS NETWORK FOR F15 TACAN 71D04		DBASE 2053
G1D01	F71D01	G1D01	F	55 71D01 21		DBASE 2152
G1D01	002457	G1D04	D	71D01 21		DBASE 2164
G1D01	211521	G1D02	S	71D01 21		DBASE 2155
G1D02	R71D03	E	92 71D00 21	23 29L 232682 1050 105		DBASE 2092
G1D02	M71D03	E	71D01 21	15 29L 232682 1050 105	1431X1 DBASE 2157	
G1D03	S40P	SG1D01	D	71D00 23		DBASE 2163
SG1D01	L71D01	IG1D01	T	71D01 23		DBASE 2152
			71D00	F15 TACAN RCVF 71D01 F111F 71D00 USED		DBASE 2171
			71D01	F15 TACAN RCVF		DBASE 2171
IG1D04	M71D03	E	82 71D00*23	20 29L 132681		DBASE 2172
IG1D04	K71D03	E	15 71D01*23	15 29L 132681		DBASE 2177
IG1D04	N71D03	E	5 71D00*23	15 29L 132681		DBASE 2177
IG1D04	O71D03	I	71D01 21	20 29L 232682 1050 105	DBASE 2177	
			71F01	THIS IS NETWORK FOR F15 ATTITUDE		DBASE 2150
			71F02	IMG PEF F111F F15 DATA USED F15 21		DBASE 2150
			71F02	VERIFIED BY TS POOLE		DBASE 2151
			71F03	ATTITUDE/HEADING REF		DBASE 2151
G1F01	F71F01	G1F01	F	52 71F01 21		DBASE 2151
G1F01	002457	G1F04	D	71F00 21		DBASE 2151
G1F02	34LGPJ	G1F02	S	71F01 21		DBASE 2152
G1F02	R71F03	E	56 71F01 21	31 29L 232682 1050 105		DBASE 2157
G1F02	M71F03	E	71F01 21	18 29L 232682 1050 105		DBASE 2157
G1F02	H71F03	I	25 71F01 21	18 29L 1431X1		DBASE 2145
G1F03	S40P	SG1F01	D	71F02 23		DBASE 2155
SG1F01	L71F01	IG1F01	T	10465 71F01 23		DBASE 2157
			71F00	F15 ELEC-CONT 4MP 7-FA: F111F 51CCC		DBASE 2153
			71F00	DATA USED WORK AROUND		DBASE 2153
			71F00	VERIFIED BY TS BOULHARD		DBASE 2190
			71F00	F15 ELEC-CONT 4MP		DBASE 2191
IG1F04	O71F03	I	71F00 21	15 29L 232682 1050 105		DBASE 2140
IG1F04	Q71F03	IG1F01	T	71F01*23		DBASE 2157
IG1F04	C71F01	IG1F02	S	71F01 23		DBASE 2154
IG1F12	A71F03	E	55 71F00 23	40 29L 132681 1PTS14 1TSC		DBASE 2159
IG1F12	K71F03	E	13 71F00 23	30 29L 132681 1PTS14 1TSC		DBASE 2159
IG1F12	N71F03	E	27 71F00 23	36 29L 132681 1PTS14 1TSC		DBASE 2159
SG1F01	L71F03	IG1F03	D	71F01 23		DBASE 2153
			71F01	F15 CTRPLACEMENT GYRO F111F 51CAC DATA DBASE 2034		
			71F00	USED FOR RATE & SELECT AND TASK TIMES DBASE 2100		
			71F00	VERIFIED BY TS BOULHARD		DBASE 2101
			71F00	F15 DISPLACEMENT GYRO		DBASE 2102
IG1F03	O71F03	I	71F01 21	15 29L 222682 1050 105		DBASE 2103
SG1F01	L71F03	IG1F03	T	10499 71F00 23		DBASE 2104
IG1F03	O71F03	IG1F01	D	71F00*23		DBASE 2104
IG1F03	C71F03	IG1F02	S	71F00 23		DBASE 2105
IG1F02	K71F03	E	11 71F00 23	71 29L 132681 1PTS14 1TSC		DBASE 2107
IG1F02	N71F03	E	96 71F00 23	70 29L 132681 1PTS14 1TSC		DBASE 2108
			71F00	F15 COMPASS CONT F111F 51CAC DATA USED DBASE 2109		

		F15 RADAR AND TASK TIMES GIVEN				
						2113
						DBASE 2111
						DBASE 2112
						DBASE 2113
						DBASE 2114
						DBASE 2115
						DBASE 2116
						DBASE 2117
						DBASE 2118
						DBASE 2119
						DBASE 2120
						DBASE 2121
						DBASE 2122
						DBASE 2123
						DBASE 2124
						DBASE 2125
						DBASE 2126
						DBASE 2127
						DBASE 2128
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						DBASE 2167
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						DBASE 2169
						DBASE 2170
						DBASE 2171
						DBASE 2172
						DBASE 2173
						DBASE 2174
						DBASE 2175

IG4F31 N7-F33	E	52	74F00*23	90	29L	232681	DBASE 2176
IG4F31 N7-F33	E	2	74F11*23	51	29L	232681	DBASE 2177
IG4F41 N7-F43	E	46	74F11*23	52	29L	232681	DBASE 2178
IG4F51 N7-F53	-	74F00	21	31	29L	232682 1050	DBASE 2179
SG4F31 L7-F33 IG4FC1 G 16531	7-F33	23					DBASE 2191
	4	74F11	F15 PARAP 73VCC 74FC1 USED FILE 71V1	DBASE 2191			
	M	74F00	IS COMP S SELECT IS 1/3 OF F111F DATA	DBASE 2192			
	M	74F00	F15 USED S SELECT TIME ESTIMATES BY DBASE 2193				
	M	74F00	TS BOUCHARD	DBASE 2194			
	M	74F00	F15 PARAP 73VCC	DBASE 2195			
IG4F31 N7-F33	I	74F00	21	10	29L	232682 1050	DBASE 2196
IG4F31 N7-F33 IG4FC1	I	74F11	21	10	29L	232682 1050	DBASE 2197
IG4F31 N7-F33 IG4FC2 G	74F00	23					DBASE 2198
IG4F32 N7-F33	E	72	74F11	23	59	29L 1326A1 1PTS31 1TSM	DBASE 2199
IG4F32 N7-F33	E	16	74F11	23	30	29L 1326A1 1PTS31 1TSM	DBASE 2199
IG4F32 N7-F33	E	11	74F11	23	21	29L 1326A1 1PTS31 1TSM	DBASE 2191
SG4F31 L7-F33 [G4F31] G 16531	74F00	23					DBASE 2192
	4	74F11	F15 RD FREQ OSC 74F11 USED FILE	DBASE 2193			
	M	74F00	73VAC 4S COMP S SELECT IS 1/3 OF	DBASE 2194			
	M	74F00	F15 F DATA	DBASE 2195			
	M	74F00	AND VERIFIED BY TS BOUCHARD	DBASE 2196			
	M	74F00	F15 RD FREQ OSC	DBASE 2197			
IG4F31 N7-F33	E	74F00	21	10	29L	232682 1050	DBASE 2198
IG4F31 N7-F33 74F11	E	74F11	21	10	29L	232682 1050	DBASE 2199
IG4F31 N7-F33 IG4FC2	I	74F00	23				DBASE 2200
IG4F32 N7-F33	E	72	74F11	23	55	29L 1326A1 1PTS31 1TSM	DBASE 2201
IG4F32 N7-F33	E	13	74F11	23	40	29L 1326A1 1PTS31 1TSM	DBASE 2202
IG4F32 N7-F33	E	15	7-F11	23	40	29L 1326A1 1PTS31 1TSM	DBASE 2203
	M	74F00	F15 ANT 74F11 F111F 73VAC DATA USED	DBASE 2204			
	M	74F11	VERIFIED BY TS BOUCHARD F111 TIME USE	DBASE 2205			
	M	74F00	F15 ANT	DBASE 2206			
SG4F31 L7-F33 74F11	74F00	23					DBASE 2207
IG4F31 N7-F33	E	67	74F11*23	60	29L	232681	DBASE 2208
IG4F31 N7-F33	E	16	74F00*23	30	29L	232681	DBASE 2209
IG4F31 N7-F33	E	17	74F00*23	46	29L	232681	DBASE 2210
IG4F31 N7-F33	E	7-F11	21	35	29L	232682 1050	DBASE 2211
SG4F31 L7-F33 IG4FF1 G 1691	74F11	23					DBASE 2212
	M	74F11	F15 PARAP TGT PROCESSOR 74FF1 F111F	DBASE 2213			
	M	74F00	73VCC DATA USED WORK AROUND	DBASE 2214			
	M	74F11	VERIFIED BY TS BOUCHARD	DBASE 2215			
	M	74F00	F15 RADAR TGT PROCESSOR	DBASE 2216			
IG4F31 N7-F33	-	74F00	21	10	29L	232682 1050	DBASE 2217
IG4F31 N7-F33 IG4FF1 G	7-F33	23					DBASE 2218
IG4F31 N7-F33 74F11	I	74F11	23				DBASE 2219
IG4F32 N7-F33	E	59	74F11	23	81	29L 1326A1 1PTS43 1TSM	DBASE 2220
IG4F32 N7-F33	E	26	74F11	23	45	29L 1326A1 1PTS43 1TSM	DBASE 2221
IG4F32 N7-F33	E	17	74F00	23	45	29L 1326A1 1PTS43 1TSM	DBASE 2222
SG4F31 L7-F33 74F11	74F11	23					DBASE 2223
	M	74F00	VERIFIED BY WORK AROUND	DBASE 2224			
	M	74F11	F15 DATA PROCESSOR 74F00 F15 DATA	DBASE 2225			
IG4F31 N7-F33	I	74F00	21	10	29L	232682 1050	DBASE 2226
IG4F31 N7-F33 74F00	I	74F11	23				DBASE 2227
IG4F31 N7-F33 IG4FC2 G	74F00	23					DBASE 2228
IG4F32 N7-F33	E	71	74F11	23	69	29L 1326A1 1PTS32 1TSM	DBASE 2229
IG4F32 N7-F33	E	12	74F00	23	40	29L 1326A1 1PTS32 1TSM	DBASE 2230
IG4F32 N7-F33	E	6	74F00	23	40	29L 1326A1 1PTS32 1TSM	DBASE 2231
SG4F31 L7-F33 IG4FS1 G 16519	74F11	23					DBASE 2232
	M	74F11	VERIFIED BY WORK AROUND	DBASE 2233			
	M	74F00	F15 ANALOG PROCESSOR 74FS1 F15 DATA	DBASE 2234			
IG4F31 N7-F33	E	7-F33	21	10	29L	232682 1050	DBASE 2235
IG4F31 N7-F33 74FS1	I	74F11	23				DBASE 2236
IG4F31 N7-F33 74FS2	I	74F00	23				DBASE 2237
IG4F32 N7-F33	E	43	74F11	23	90	29L 1326A1 1PTS33 1TSM	DBASE 2238
IG4F32 N7-F33	E	17	74F00	23	64	29L 1326A1 1PTS33 1TSM	DBASE 2239
IG4F32 N7-F33	E	47	74F00	23	64	29L 1326A1 1PTS33 1TSM	DBASE 2240
SG4F31 L7-F33 IG4FK1 G 16119	74F11	23					DBASE 2241

4	74F30	F15 RADAR SET CONT 74FK1 F111F.	DBASE 2242
H	74F30	VERIFIED BY TS BOUCHARD	DBASE 2243
4	74F30	F15 R-CAP SET CONT	DBASE 2244
I	74F30	11 74F30 23 26 29L 132631	DBASE 2245
I	74F30	IG6FK1 07-FK1	DBASE 2246
I	74F30	IG6FK1 07-FK1	DBASE 2247
S64F30 L7-FH1 IG-FH1	3 1786 74F30 23		DBASE 2248
4	74F30	F15 PWR SUPPLY 74-FH1 F15 DATA G SELECT	DBASE 2249
H	74F30	TIMES AND E SELECT GIVEN BY TS BOUCHARD	DBASE 2250
H	74F30	F15 PWR SUPPLY 74-FH1	DBASE 2251
I	57 74F30 23	36 29L 132631	DBASE 2252
I	26 74F30 23	01 29L 132631	DBASE 2253
I	11 74F30 23	12 29L 132631	DBASE 2254
I	74F30 21	13 29L 132632 1050 105	DBASE 2255
4	74J30	F15 INDICATOR GROUP 470 73AE0+73EB1	DBASE 2256
4	74J30	USED F15 153113	DBASE 2257
H	74J30	VERIFIED BY TSGT FAY	DBASE 2258
H	74J30	F15 INDICATOR GROUP	DBASE 2259
G4J1 07-J1 G4J1 1	36 7-J00 21		DBASE 2260
G4J1 07-J1 G4J1 0	7-J00 21		DBASE 2261
G4J1 07-J1 G4J1 0	7-J00 21		DBASE 2262
G4J1 07-J1 G4J1 1	57 74J00 21	20 29L 132632 1050 105	DBASE 2263
G4J2 07-J2 G4J2 1	27 74J00 21	12 29L 132632 1050 105	DBASE 2264
G4J3 07-J3 G4J3 2	74J00 23		DBASE 2265
S64J30 L7-J30 IG-J30	3 2263 74J00 23		DBASE 2266
4	74J30	F15 MULT TWO AND 73AE0 DATA USED	DBASE 2267
H	74J30	VERIFIED BY TS BOUCHARD	DBASE 2268
4	74J30	F15 MULT TWO	DBASE 2269
IG-J30 07-J30	7-J00 21	20 29L 132632 1050 105	DBASE 2270
I	74J30 23		DBASE 2271
IG-J30 07-J30 IG-J30	74J00 23		DBASE 2272
IG-J30 07-J30	7-J00 23	13 29L 132631 1PTS46 1TS0	DBASE 2273
IG-J30 07-J30	16 74J00 23	15 29L 132631 1PTS46 1TS0	DBASE 2274
I	74J00 23	15 29L 132631 1PTS46 1TS0	DBASE 2275
S64J30 L7-J30 IG-J30	3 2263 74J00 23		DBASE 2276
4	74J30	F15 SIG PROCESSOR 74J00 470 73EB1	DBASE 2277
4	74J30	DATA USED WORK AROUND	DBASE 2278
H	74J30	VERIFIED BY TS BOUCHARD	DBASE 2279
4	74J30	F15 SIG PROCESSOR	DBASE 2280
I	74J00 21	8 29L 132632 1050 105	DBASE 2281
IG-J30 07-J30 IG-J30	74J30 23		DBASE 2282
I	74J00 21		DBASE 2283
I	74J30 23		DBASE 2284
I	57 74J30 23	66 29L 132641 1PTS37 1TS0	DBASE 2285
I	21 74J30 23	41 29L 132641 1PTS37 1TS0	DBASE 2286
I	23 74J30 23	41 29L 132641 1PTS37 1TS0	DBASE 2287
4	74K00	F15 HMD NETWORK 470 73FA1+73EB1 DATA	DBASE 2288
4	74K00	USED F15 MODEMA 15 470 13 UCE F15	DBASE 2289
4	74K00	VERIFIED BY TEST RAY	DBASE 2290
4	74K00	F15 HMD	DBASE 2291
G-KC1 F7-K1 G-KC1	13 74K00 21		DBASE 2292
G-KC1 05-MG7 G-KC1	74K00 21		DBASE 2293
G-KC1 05-MG7 G-KC1	74K00 21		DBASE 2294
G-KC2 07-K2 G-KC2	74K00 21		DBASE 2295
G-KC2 07-K2 G-KC2	74K00 21		DBASE 2296
G-KC2 07-K2 G-KC2	74K00 21		DBASE 2297
G-KC2 07-K2 G-KC2	74K00 21		DBASE 2298
G-KC2 07-K2 G-KC2	74K00 21		DBASE 2299
I	74K00 21	8 29L 132642 1050 105	DBASE 2300
I	74K00 21	10 29L 132642 1050 105	DBASE 2301
I	74K00 21	14 31X1	DBASE 2302
I	74K00 23		DBASE 2303
I	74K00 23		DBASE 2304
I	74K00 23		DBASE 2305
I	57 74K00 23	66 29L 132641 1PTS36 1TS0	DBASE 2306
I	21 74K00 23	41 29L 132641 1PTS36 1TS0	DBASE 2307
I	23 74K00 23	20 29L 132681	DBASE 2308

S66K3: L7-KA3 IG-KA3 G 13357 74K00 23  
 1 74K00 F15 HMD DISP UNIT 7-KA3 A7D 73E81 DATA 047AD2ASE 2313  
 4 74K00 USED WORK ARROUND DBASE 2313  
 1 74K01 VERIFIED BY TS BOUCHARD DBASE 2313  
 4 74K01 F15 HMD DISP UNIT DBASE 2313  
 1 74K11 21 CC 29L 2326-2 1020 105 DBASE 2313  
 IS6K3: 07-KE3 IG-KA3 74K11\*23 DBASE 2314  
 IS6K3: 07-KE3 IG-KA3 74K11 23 DBASE 2315  
 IS6K42 07-KA3 E 63 74K01 23 53 29L 1326A1 1PT541 1TSD DBASE 2316  
 IS6K42 07-KA3 E 19 74K11 23 26 29L 1326A1 1PT541 1TSD DBASE 2317  
 IS6K42 07-KA3 E 19 74K01 23 25 29L 1326A1 1PT541 1TSD DBASE 2318  
 SG6K3: 17-KE3 IG-KE3 74K00 23 DBASE 2319  
 4 74K00 VERIFIED BY TS OBERLEY DBASE 2320  
 4 74K00 F15 CAMEFA 7-KF1 FILE DATA USED DBASE 2321  
 IS6KE3: 17-KE3 E 7L 74K00\*23 3L 29L 1326F1 DBASE 2322  
 IS6KE3: 17-KE3 E 25 74K11\*23 25 29L 1326F1 DBASE 2323  
 IS6KE3: 17-KE3 E 5 74K11\*23 2L 29L 1326F1 DBASE 2324  
 IS6KE3: 17-KE3 74K11 21 15 29L 2326-2 1020 105 DBASE 2325  
 4 75F00 VERIFIED BY MS GIBEL YOU 2937/2364 DBASE 2326  
 4 75F00 F15 FAU12 30MB PACK A7D 75AKC DATA DBASE 2327  
 GS6F1: F75F00 GSF1 E 107 75F00 21 DBASE 2328  
 GS6F1: 075F00 GSF1 75F00 21 DBASE 2329  
 GS6F1: 075F00 GSF1 75F00 21 DBASE 2330  
 GS6F1: 075F00 31 75F00 21 15 29L 2462Y1 1060 105 DBASE 2331  
 GS6F1: 075F00 E 69 75F00 21 11 29L 2462Y0 1060 105 DBASE 2332  
 GS6F1: 075F00 SG6F1 75F00 21 DBASE 2333  
 SG6F1: L75F00 IG6F00 75F00 23 DBASE 2334  
 4 75F00 VERIFIED BY MS GIBEL YOU DBASE 2335  
 4 75F00 F15 FAU12 A7D CAT USED DBASE 2336  
 IS6F1: 075F00 E 87 75F00\*23 35 29L 2462Y1 DBASE 2337  
 IS6F1: 075F00 E 3 75F00\*23 6 29L 2462Y3 DBASE 2338  
 IS6F1: 075F00 E 10 75F00\*23 1 29L 2462Y1 DBASE 2339  
 IS6F1: 075F00 75F00 21 13 29L 2462Y0 1060 105 DBASE 2340  
 4 75F00 VERIFIED BY MS GIBEL YOU DBASE 2341  
 4 75F00 F15 IN30420 PYLON 750A3 A7D 75BP3 DATA DBASE 2342  
 GS6F1: F750A3 G6F01 E 152 75000 21 DBASE 2343  
 GS6F1: 0750A3 G6F01 75000 21 DBASE 2344  
 GS6F1: 0750A3 G6F01 75000 21 DBASE 2345  
 GS6F1: 0750A3 E 1 75000 21 9 29L 3462Y1 1424X1 1061 105 DBASE 2346  
 GS6F1: 0750A3 E 24 75000 21 23 29L 1531X3 DBASE 2347  
 GS6F1: 0750A3 57 75000 21 1 29L 1531X1 DBASE 2348  
 4 75001 VERIFIED BY MS GIBEL YOU DBASE 2349  
 4 75001 F15 AFM LAUNCHERS NETWORK FILE AND A7D DBASE 2350  
 GS6F1: F750A3 G6F01 E 51 75F00 21 DBASE 2351  
 GS6F1: 0750A3 G6F01 75000 21 DBASE 2352  
 GS6F1: 0750A3 0750A3 75000 21 DBASE 2353  
 GS6F1: 0750A3 G6F01 75000 21 DBASE 2354  
 GS6F1: 0750A3 29 75000 21 24 29L 3462Y1 1060 105 DBASE 2355  
 GS6F1: 0750A3 21 75000 21 10 29L 2462Y0 1060 DBASE 2356  
 GS6F1: 0750A3 21 75000 21 10 29L 1531X1 1060 DBASE 2357  
 GS6F1: 0750A3 26 75000 21 19 29L 1531X1 DBASE 2358  
 GS6F1: 0750A3 7 75000 21 20 29L 2431X1 DBASE 2359  
 GS6F1: 0750A3 SHMP SG6F00 75F00 23 DBASE 2360  
 SG6F1: L750A3 IG6F00 1216 75F00 23 DBASE 2361  
 175001 4 75F00 VERIFIED BY MS GIBEL YOU DBASE 2361  
 L75001 4 75001 F15 AIM7 LAU FILE DATA USED DBASE 2362  
 IS6F1: 0750A3 96 75F00\*23 15 29L 2462Y0 DBASE 2363  
 IS6F1: 0750A3 9 75F00\*23 9 29L 1531X3 DBASE 2364  
 IS6F1: 0750A3 E 5 75F00\*23 10 29L 2462Y1 DBASE 2365  
 IS6F1: 0750A3 1 75001 21 25 29L 3462Y1 1060 105 DBASE 2366  
 SG6F1: 0750A3 0750A3 75F00 23 DBASE 2367  
 L75001 4 75001 VERIFIED BY MS GIBEL YOU DBASE 2368  
 L75001 4 75F00 F15 AIM9 LAU A7D 75AKC DATA USED DBASE 2369  
 IS6F1: 0750A3 95 75F00\*23 15 29L 2462Y1 DBASE 2370  
 IS6F1: 0750A3 2 75F00\*23 3 29L 1531X3 DBASE 2371  
 IS6F1: 0750A3 3 75F00\*23 15 29L 2462Y1 DBASE 2372  
 IS6F1: 0750A3 75000 21 20 29L 3462Y1 1060 105 DBASE 2373

M	7500J	VERIFIED BY MS GIBELYCU 2977/2464	DBASE 2374
M	7500J	F15 M60 NETWORK A70 75400 DATA USED	DBASE 2375
G5C11 F75C1J G5C11 F	135 7500J 21		DBASE 2376
G5C11 75M67 G5C11 J	7500J 21		DBASE 2377
G5C12 CALGPJ G5C12 C	7500J 21		DBASE 2378
G5C12 75C1J	7500J 21 15 29L 3462YC 1060 105		DBASE 2379
1	7500J PANEL WILL FAIL 10K AS OFTEN AS A70		DBASE 2380
4	7500J VERIFIED BY MS GIBELYCU		DBASE 2381
M	75M0J F15 4591 29L 75 15 21		DBASE 2382
M	75M0J F15 AFM COUNT SET AMG 27 A70 74CA0 USE0		DBASE 2383
G5M11 F75M1J G5M11 F	213 75M0J 21		DBASE 2384
G5M11 75M67 G5M11 J	75M0J 21		DBASE 2385
G5M12 CALGPJ G5M12 C	75M0J 21		DBASE 2386
G5M12 75C1J G5M12 F	90 75M0J 21 25 29L 2462YC 1060 105		DBASE 2387
G5M12 75M67 G5M12 C	2 75M0J 21 16 29L 2462YC 1060 105		DBASE 2388
GEM11 S40P SG5M11 J	75M0J 23		DBASE 2389
SG5M11 L75M1J IG5M11 S	9107 75M0J 23		DBASE 2390
4	75M0J ESTIMATES BY WORK AROUND		DBASE 2391
IG5M11 75M0J	75M0J 21 25 29L 2462YC 1060 105		DBASE 2392
IG5M11 75M0J IG5M11 J	75M0J 23		DBASE 2393
IG5M11 75M11 IG5M11 C	75M0J 23		DBASE 2394
IG5M12 75M11 IG5M12 C	75M0J 23		DBASE 2395
IG5M12 475M0J	21 75M0J 23 25 29L 1326A1 1PTS45 1TS0		DBASE 2396
IG5M12 75M0J	30 75M0J 23 16 29L 1726A1 1PTS45 1TS0		DBASE 2397
IG5M12 75M0J	51 75M0J 23 18 29L 1326A1 1PTS45 1TS0		DBASE 2398
SG5M11 L75M0J IG5M0J S	9107 75M0J 23		DBASE 2399
4	75M0J ESTIMATES BY WORK AROUND		DBASE 2400
M	75M0J F15 CONVERTER PROGRAMMER 75M0C		DBASE 2401
IG5M01 75M0J	I 75M0J 21 15 29L 2462YC 1060 105		DBASE 2402
IG5M01 75M0C IG5M01 J	75M0J 23		DBASE 2403
IG5M01 75M0C IG5M01 C	75M0J 23		DBASE 2404
IG5M02 75M0J	E 20 75M0J 23 51 29L 1326A1 1PTS44 1TS0		DBASE 2405
IG5M02 75M0C	E 31 75M0J 23 46 29L 1326A1 1PTS44 1TS0		DBASE 2406
IG5M02 75M0C	E 51 75M0J 23 46 29L 1326A1 1PTS44 1TS0		DBASE 2407
4	75M0J VERIFIED BY SURGEINK ONLY ONCE 4 ATTIO		DBASE 2408
4	75M0J F15 DATA=56 MCATA=4 1706=12 F111F=17		DBASE 2409
4	75M0J F15 M61A1 GUN NETWORK 75M0J		DBASE 2410
G5H11 F75H1J G5H11 F	21000 75M0J 21		DBASE 2411
G5H11 75M67 G5H11 J	75M0J 21		DBASE 2412
G5H11 CALGPJ G5H11 C	75M0J 21		DBASE 2413
G5H12 75H1J G5H12 E	61 75M0J 21 46 29L 2462X2 1060 1TU229		DBASE 2414
G5H12 75M12	4 17 75M0J 21 14 29L 2462X1 1501X3		DBASE 2415
G5H12 75H1J	E 12 75M0J 21 21 29L 2462X2 1060 1TU224		DBASE 2416
G5H12 75H1J G5H12 E	87 75M0J 21 30 29L 3462X0 1060 105		DBASE 2417
G5H12 75H1J	E 11 75M0J 21 16 29L 2462X0 1060 105		DBASE 2418
G5H12 75H1J	4 16 75M0J 21 13 29L 3462X0 1060 105		DBASE 2419
G5H13 S40P SG5H11 J	75M0J 23		DBASE 2420
4	75M0J F15 M61A1 GUN 75M0J		DBASE 2421
SG5M11 L75M0J IG5M0J S	1246 75M0J 23		DBASE 2422
IG5M11 75M0J	E 86 75M0J 23 30 29L 2462YC		DBASE 2423
IG5M01 K75H0J	E 5 75M0J 23 26 29L 2462X0		DBASE 2424
IG5M01 75M0J	E 9 75M0J 23 30 29L 2462YC		DBASE 2425
IG5M01 75M0J	I 75M0J 21 60 29L 3462X2 1060 105		DBASE 2426
SG5M11 L75M0J IG5M0J S	16317 75M0J 23		DBASE 2427
4	75M0J F15 CPU ASSY 75M0C		DBASE 2428
IG5M01 K75H0J	E 77 75M0J 23 39 29L 2462X0		DBASE 2429
IG5M01 K75H0J	E 23 75M0J 23 23 29L 2462X0		DBASE 2430
IG5M01 75M0J	I 75M0J 21 60 29L 3462X0 1060 105		DBASE 2431
SG5M11 L75M0J IG5M0J S	16167 75M0J 23		DBASE 2432
4	75M0J F15 CONVEYOR SVS 75M0J		DBASE 2433
IG5M11 75H0J	S 75M0J 23 30 29L 2462X0		DBASE 2434
IG5M11 75H0J	I 75M0J 21 120 29L 3462YC 1060		DBASE 2435
SG5M11 L75M0J IG5M0J S	16192 75M0J 23		DBASE 2436
4	75M0J F15 HYD COMP GUN 75M0J		DBASE 2437
IG5M01 K75M0J	D 75M0J 23 13 29L 2462X2		DBASE 2438
IG5M01 K75M0J	I 75M0J 21 30 29L 2462X2		DBASE 2439

F15 ALR 56 NETWORK								
G6A1	F76M1	G6A1	E	10	76A01	21		OBASE 2441
G6A1J1	03EMG7	G6A0M	J		76A0G	21		OBASE 2442
G6A1J1	03LG71	G6A0U	J		76A1	21		OBASE 2443
G6A1J2	075A1		E	75	76A1U	21	10 29L 2326C2 106J	105
G6A1J2	075F1	G6A1	E	25	76A1U	21		OBASE 2444
G6A1J4	075A1	G6A1	E	11	76A1C	21	12 29L 2326C2 106J	105
G6A1J4	075A2	G6A1	E	61	76A1U	21	12 29L 2326C2 106J	105
				4	76G10			OBASE 2445
								OBASE 2446
G6G1	F76G1	G6G1	E	25	76G11	21		OBASE 2447
G6G1J1	03EMG7	G6G1A	J		76G10	21		OBASE 2448
G6G1J1	03LG71	G6G1U	J		76G11	21		OBASE 2449
G6G1J2	075G1	G6G1	J	0	76G11	21	8 29L 2326C2 106J	105
G6G1J2	075G1	G6G1	J	4	76H10		F15 ALR 56	OBASE 2450
G6H1	F76H1	G6H1	E	12	76H1U	21		OBASE 2451
G6H1J1	075H1	G6H1A	J		76H11	21		OBASE 2452
G6H1J2	0ALG71	G6H1C	J		76H11	21		OBASE 2453
G6H1J2	075H1	G6H1	J	65	76H1U	21	10 29L 2326C2 106J	105
G6H1J2	075H1	G6H1	J	1	76H1P	21	10 29L 2326C2 106J	105
G6H1J2	075H1	G6H1	J	2	76H1U	21	10 29L 2326C2 106J	105
G6H1J2	075H1	G6H1	J	1	76H1U	21	15 29L 2326C2 106J	105
G6H1J2	075H1	G6H1	J	4	06211		M32-E1 AGE DESPATCH	OBASE 2454
CALGP1	A0601	A0601	J		06101	21	3 29L 1421A3 1060	OBASE 2455
A0601	A0601	A0601	J		06101	21		OBASE 2456
A0601	A0601	A0601	J	6	06100	21	5 29L 1421A3 1060	OBASE 2457
A0601	A0601	A0601	J	4	06101	21		OBASE 2458
				4	TTU01		HYDRAULIC MULE AGE DESPATCH	OBASE 2459
					TTU01	21	3 29L 1421A3 1TU223	OBASE 2460
ATTU01	TTTU01	ATTU01	J	5	TTU01	21		OBASE 2461
ATTU01	TTTU01	ATTU01	J	5	TTU01	21	5 29L 1421A3 1TU223	OBASE 2462
ATTU01	TTTU01	ATTU01	J	5	TTU01	21		OBASE 2463
ATTU01	TTTU01	ATTU01	J	5	TTU01	21		OBASE 2464
				4	TEST0		T/S FOR COMPUTERS	OBASE 2465
C51A1C	PTSNK	S1AHC1	E	16	TEST0	23		OBASE 2466
C51A1C	PTSNK		E	34	TEST0	23		OBASE 2467
S1AHC1	LPTSI	S1AHC2	J		TEST0	23		OBASE 2468
S1AHC1	LPTSI	S1AHC2	J	4	TEST0		LEU S1AHC T/S	OBASE 2469
S1AHC2	LPTSI	S1AHC3	J		TEST0	23	14 29L	OBASE 2470
S1AHC2	LPTSI	S1AHC3	J		TEST0	23		OBASE 2471
C51A4C	CTSC		J		TEST0	23		OBASE 2472
C51A5C	PTSN	S1AHC1	E	16	TEST0	23		OBASE 2473
C51A5C	PTSN	S1AHC1	E	64	TEST0	23		OBASE 2474
C51A6C	PTSN		J		TEST0	23		OBASE 2475
C51A6C	PTSN		J		TEST0	23		OBASE 2476
S1AG11	LPTSI	S1AGC2	J		TEST0	23		OBASE 2477
S1AG11	LPTSI	S1AGC2	J	4	TEST0		LEU S1AGC T/S	OBASE 2478
S1AG12	PTTS2	S1AGC3	J		TEST0	23	14 29L	OBASE 2479
S1AG12	PTTS2	S1AGC3	J	7	TEST0	23		OBASE 2480
C55B3C	PTSNK	S53B0C1	E	69	TEST0	23		OBASE 2481
C55B2C	PTTS2		J	91	TEST0	23		OBASE 2482
C55B2C	PTTS2		J		TEST0	23		OBASE 2483
C55B2C	PTTS2		J		TEST0	23		OBASE 2484
S53BC1	LPTSI	S53B0C2	J		TEST0	23		OBASE 2485
S53BC1	LPTSI	S53B0C2	J	4	TEST0		LEU S53B0C T/S	OBASE 2486
S53AC12	PTTS3	S53B0L3	J		TEST0	23	12 29L	OBASE 2487
S53AC12	PTTS3	S53B0L3	J		TEST0	23		OBASE 2488
C55C1C	GPTSI		J		TEST0	23		OBASE 2489
C55C1C	GPTSI		J		TEST0	23		OBASE 2490
C55C1C	GPTSI		J	21	TEST0	23		OBASE 2491
C32A3	PTSIK		J	79	TEST0	23		OBASE 2492
C32A3	PTSIK		J		TEST0	23		OBASE 2493
S2AC0J1	LPTSI	S2AC0C2	J		TEST0	23		OBASE 2494
S2AC0J1	LPTSI	S2AC0C2	J	4	TEST0		LEU S2AC0C T/S	OBASE 2495
S2AC0J2	PTTS4	S2AC0C3	J		TEST0	23	13 29L	OBASE 2496
S2AC0J2	PTTS4	S2AC0C3	J	7	TEST0	23		OBASE 2497
C41AAU	PTSN	41AAU1	E	16	TEST0	23		OBASE 2498
C41AAU	PTSN	41AAU1	E	64	TEST0	23		OBASE 2499
C41AAU	CTSC	41AAU2	J		TEST0	23		OBASE 2500
41AAU1	LPTSI	41AAU2	J		TEST0	23		OBASE 2501
41AAU2	LPTSI	41AAU2	J	4	TEST0		LEU 41AAU TAS	OBASE 2502
41AAU2	LPTSI	41AAU2	J		TEST0	23	14 29L	OBASE 2503
41AAU2	LPTSI	41AAU3	J		TEST0	23		OBASE 2504
41AAU2	LPTSI	41AAU3	J		TEST0	23		OBASE 2505

61A3J3	GPTSS	3	TESTC 23	DBASE 2536
71A3C	PTSN < 71AKU	3	TESTC 23	DBASE 2517
671E6	PTSLK	3	TESTC 23	DBASE 2503
671E5	LPTSC	3	TESTC 23	DBASE 2509
71AKC3	LPTSC 71AKC2	3	TESTC 23	DBASE 2510
12734		4	TESTC LRU 71AKC T/S	DBASE 2511
71AKC2	QPTS5	3	TESTC 23	DBASE 2512
71AKC3	GPTSC	3	TESTC 23	DBASE 2513
671F6	PTSN < 71FEC1	3	TESTC 23	DBASE 2514
671F5	PTSLK	3	TESTC 23	DBASE 2515
671F4	CTSC	3	TESTC 23	DBASE 2516
71FEC1	LPTSC 71FEC2	3	TESTC 23	DBASE 2517
12737		4	TESTC LRU 71FEC T/S	DBASE 2518
71FEC2	QPTS7	3	TESTC 23	DBASE 2519
71FEC3	GPTST	3	TESTC 23	DBASE 2520
674E3	PTSN < 7-E3C2	3	TESTC 23	DBASE 2521
674E3	PTSLK	3	TESTC 23	DBASE 2522
674E3	CTSC	3	TESTC 23	DBASE 2523
74E3J1	LPTSC 7-E3C2	3	TESTC 23	DBASE 2524
12731		4	TESTC LRU 7-E3C T/S	DBASE 2525
74E3J2	QPTS3	3	TESTC 23	DBASE 2526
74E3J3	GPT3	3	TESTC 23	DBASE 2527
671E5	PTSN < 71AE52	3	TESTC 23	DBASE 2528
671E5	PTSLK	3	TESTC 23	DBASE 2529
671E5	CTSC	3	TESTC 23	DBASE 2530
71AE51	LPTSC 71AE52	3	TESTC 23	DBASE 2531
12733		4	TESTC LRU 71AE5 T/S	DBASE 2532
71AE52	QPTS3	3	TESTC 23	DBASE 2533
71AE53	GPT3	3	TESTC 23	DBASE 2534
651A1	PTSLK < 51A1C1	3	TESTC 23	DBASE 2535
651A1	PTSLK	3	TESTC 23	DBASE 2536
651A1	CTSC	3	TESTC 23	DBASE 2537
51AJ31	LPTSC 51AJ32	3	TESTC 23	DBASE 2538
12731		4	TESTC LRU 51AJ3 T/S	DBASE 2539
51AJ32	QPTS3	3	TESTC 23	DBASE 2540
51AJ33	GPT3	3	TESTC 23	DBASE 2541
652A3	PTSN < 52A3C1	3	TESTC 23	DBASE 2542
652A3	PTSLK	3	TESTC 23	DBASE 2543
652A3	CTSC	3	TESTC 23	DBASE 2544
52A3J1	LPTSC 52A3C2	3	TESTC 23	DBASE 2545
12731		4	TESTC LRU 52A3C T/S	DBASE 2546
52A3J2	QPTS11	3	TESTC 23	DBASE 2547
52A3J3	GPT511	3	TESTC 23	DBASE 2548
652A3	PTSN < 52AA51	3	TESTC 23	DBASE 2549
652A3	PTSLK	3	TESTC 23	DBASE 2550
652A3	CTSC	3	TESTC 23	DBASE 2551
52AA51	LPTSC 52AA52	3	TESTC 23	DBASE 2552
12732		4	TESTC LRU 52AA5 T/S	DBASE 2553
52AA52	QPTS12	3	TESTC 23	DBASE 2554
52AA53	GPT512	3	TESTC 23	DBASE 2555
649CA1	PTSNK 49CAA1	3	TESTC 23	DBASE 2556
649CA1	PTSLK	3	TESTC 23	DBASE 2557
649CA1	CTSC	3	TESTC 23	DBASE 2558
49CAA1	PTSL3 49CAA2	3	TESTC 23	DBASE 2559
12733		4	TESTC LRU 49CAA T/S	DBASE 2560
49CAA2	QPTS13	3	TESTC 23	DBASE 2561
49CAA3	GPT513	3	TESTC 23	DBASE 2562
671FA1	PTSN < 71FAC1	3	TESTC 23	DBASE 2563
671FA1	PTSLK	3	TESTC 23	DBASE 2564
671FA1	CTSC	3	TESTC 23	DBASE 2565
71FAC1	LPTSC 71FAC2	3	TESTC 23	DBASE 2566
12731		4	TESTC LRU 71FAC T/S	DBASE 2567
71FAC2	QPTS14	3	TESTC 23	DBASE 2568
71FAC3	GPT514	3	TESTC 23	DBASE 2569
611FDC	PTSLK 11P0U1	3	TESTC 23	DBASE 2571
611FDC	PTSLK	3	TESTC 23	DBASE 2571

C11P03	CTSC	3	TESTC 23	DBASE 2572
11P011	LPT515	11P012	TESTC 23	DBASE 2573
LPT515	4	TESTC LRU 21P01 T/S	DBASE 2574	
11P012	GPTS15	11P013	TESTC 23	DBASE 2575
11P013	GPTS15	3	TESTC 23	DBASE 2576
C55C1	PTSN < 55C01	14	TESTC 23	DBASE 2577
C55C3	PTSK	82	TESTC 23	DBASE 2578
C55C3	CTSC	TESTC 23	DBASE 2579	
55C91	LPT515	55C92	TESTC 23	DBASE 2580
LPT515	4	TESTC LRU 55C91 T/S	DBASE 2581	
55C92	GPTS15	55C93	TESTC 23	DBASE 2582
55C93	LPT515	2	TESTC 23	DBASE 2583
C52A41	PTSN < 52A41	16	TESTC 23	DBASE 2584
C52A41	PTSK	4	TESTC 23	DBASE 2585
C52A41	CTSC	TESTC 23	DBASE 2586	
52A41	LPT517	52A412	TESTC 23	DBASE 2587
LPT517	4	TESTC LRU 52A41 T/S	DBASE 2588	
52A412	GPTS17	52A413	TESTC 23	DBASE 2589
52A413	GPTS17	3	TESTC 23	DBASE 2590
C71F31	PTSN < 71F31	15	TESTC 23	DBASE 2591
C71F31	PTSK	4	TESTC 23	DBASE 2592
C71F31	CTSC	TESTC 23	DBASE 2593	
71F31	LPT515	71F312	TESTC 23	DBASE 2594
LPT514	4	TESTC LRU 71F31 T/S	DBASE 2595	
71F312	GPTS13	71F313	TESTC 23	DBASE 2596
71F313	GPTS13	2	TESTC 23	DBASE 2597
C55C41	PTSN < 55C41	15	TESTC 23	DBASE 2598
C55C41	PTSK	4	TESTC 23	DBASE 2599
C55C41	CTSC	TESTC 23	DBASE 2600	
55C41	LPT519	55C412	TESTC 23	DBASE 2601
LPT519	4	TESTC LRU 55C41 T/S	DBASE 2602	
55C412	GPTS19	55C413	TESTC 23	DBASE 2603
55C413	GPTS19	3	TESTC 23	DBASE 2604
C57A41	PTSN < 57A41	30	TESTC 23	DBASE 2605
C57A41	PTSK	64	TESTC 23	DBASE 2606
C57A41	CTSC	TESTC 23	DBASE 2607	
57A41	LPT521	57A412	TESTC 23	DBASE 2608
LPT521	4	TESTC LRU 57A41 T/S	DBASE 2609	
57A412	GPTS21	57A413	TESTC 23	DBASE 2610
57A413	GPTS21	2	TESTC 23	DBASE 2611
C61A40	PTSN < 61A40	20	TESTC 23	DBASE 2612
C61A40	PTSK	8	TESTC 23	DBASE 2613
C61A40	CTSC	TESTC 23	DBASE 2614	
61A40	LPT522	61A402	TESTC 23	DBASE 2615
LPT522	4	TESTC LRU 61A40 T/S	DBASE 2616	
61A402	GPTS22	61A403	TESTC 23	DBASE 2617
61A403	GPTS22	3	TESTC 23	DBASE 2618
C61A40	PTSN < 61A40	20	TESTC 23	DBASE 2619
C61A40	PTSK	40	TESTC 23	DBASE 2620
C61A40	CTSC	TESTC 23	DBASE 2621	
61A40	LPT523	61A402	TESTC 23	DBASE 2622
LPT523	4	TESTC LRU 61A40 T/S	DBASE 2623	
61A402	GPTS23	61A403	TESTC 23	DBASE 2624
61A403	GPTS23	2	TESTC 23	DBASE 2625
C51A01	PTSN < 51A01	22	TESTC 23	DBASE 2626
C51A01	PTSK	72	TESTC 23	DBASE 2627
C51A01	CTSC	TESTC 23	DBASE 2628	
51A01	LPT524	51A02	TESTC 23	DBASE 2629
LPT524	4	TESTC LRU 51A01 T/S	DBASE 2630	
51A02	GPTS24	51A03	TESTC 23	DBASE 2631
51A03	GPTS24	3	TESTC 23	DBASE 2632
C51E41	PTSN < 51E41	33	TESTC 23	DBASE 2633
C51E41	PTSK	67	TESTC 23	DBASE 2634
C51E41	CTSC	TESTC 23	DBASE 2635	
51E41	LPT525	51E42	TESTC 23	DBASE 2636
LPT525	4	TESTC LRU 51E41 T/S	DBASE 2637	

S1E6J2	GPTS23	S1E4E3	0	TESTO 23	12 29L	DBASE 2638
S1E7J2	GPTS23	0	TESTO 23	TESTO 23	DBASE 2639	
C913J1	PTSN X	S1AM61	E	16 TESTO 23		DBASE 2640
C913J4	PTSK	0	TESTO 23	TESTO 23	DBASE 2641	
C912J4	CTSC	0	TESTO 23	TESTO 23	DBASE 2642	
S1AM12	LPTS23	S1AM62	0	TESTO 23	TESTO 23	DBASE 2643
	LPTS26	4	TESTO	LPU S1AM62 T/S		DBASE 2644
S1AM12	GPTS23	S1AM62	0	TESTO 23	14 29L	DBASE 2645
S1AM13	GPTS26	0	TESTO 23	TESTO 23	DBASE 2646	
C928J1	PTSN X	S2AL11	E	17 TESTO 23		DBASE 2647
C926J1	PTSK	0	TESTO 23	TESTO 23	DBASE 2648	
C928J2	CTSC	0	TESTO 23	TESTO 23	DBASE 2649	
S2AL12	LPTS27	S2AL12	0	TESTO 23		DBASE 2650
S2AL12	GPTS27	S2AL13	0	TESTO 23		DBASE 2651
S2AL13	GPTS27	0	TESTO 23	TESTO 23	DBASE 2652	
	LPTS31	4	TESTH	T/S FOR MICROWAVE EQUIP		DBASE 2653
C74FJ1	PTSN X	7-FJ11	E	36 TESTH 23		DBASE 2654
C74FJ1	PTSK	0	6-	TESTH 23		DBASE 2655
C74FJ1	CTS	0	TESTH 23	TESTH 23	DBASE 2656	
7-FJ11	LPTS31	7-FJ12	0	TESTH 23		DBASE 2657
	LPTS31	4	TESTH	LRU 7-FJ11 T/S		DBASE 2658
7-FJ12	GPTS31	7-FJ13	0	TESTH 23	15 29L	DBASE 2659
7-FJ13	GPTS31	0	TESTH 23	TESTH 23	DBASE 2660	
C74FJ2	PTSN X	7-FJ21	E	36 TESTH 23		DBASE 2661
C74FJ2	PTSK	0	6-	TESTH 23		DBASE 2662
C74FJ2	CTS	0	TESTH 23	TESTH 23	DBASE 2663	
7-FJ21	LPTS31	7-FJ22	0	TESTH 23		DBASE 2664
	LPTS31	4	TESTH	LPU 7-FJ21 T/S		DBASE 2665
7-FJ22	GPTS31	7-FJ23	0	TESTH 23	15 29L	DBASE 2666
7-FC12	GPTS31	0	TESTH 23	TESTH 23	DBASE 2667	
C74FJ2	PTSN X	7-FD61	E	6-	TESTH 23	DBASE 2668
C74FJ2	PTSK	0	9-	TESTH 23		DBASE 2669
C74FJ2	CTS	0	TESTH 23	TESTH 23	DBASE 2670	
7-FD61	LPTS32	7-FD62	0	TESTH 23		DBASE 2671
	LPTS32	4	TESTH	LRU 7-FD61 T/S		DBASE 2672
7-FD62	GPTS32	7-FD63	0	TESTH 23	25 29L	DBASE 2673
7-FD63	GPTS32	0	TESTH 23	TESTH 23	DBASE 2674	
C74FJ3	PTSN X	7-FS01	E	17 TESTH 23		DBASE 2675
C74FJ3	PTSK	0	8-	TESTH 23		DBASE 2676
C74FJ3	CTS	0	TESTH 23	TESTH 23	DBASE 2677	
7-FS01	LPTS33	7-FS02	0	TESTH 23		DBASE 2678
	LPTS32	4	TESTH	LRU 7-FS01 T/S		DBASE 2679
7-FS02	GPTS33	7-FS03	0	TESTH 23	14 29L	DBASE 2680
7-FS03	GPTS33	0	TESTH 23	TESTH 23	DBASE 2681	
C76CA1	PTSN X	76CA11	E	16 TESTH 23		DBASE 2682
C76CA1	PTSK	0	9-	TESTH 23		DBASE 2683
C76CA1	CTS	0	TESTH 23	TESTH 23	DBASE 2684	
76CA11	LPTS3-	76CA02	0	TESTH 23		DBASE 2685
	LPTS3-	4	TESTH	LPU 76CA1 T/S		DBASE 2686
76CA12	GPTS3-	76CA03	0	TESTH 23	25 29L	DBASE 2687
76CA13	GPTS34	0	TESTH 23	TESTH 23	DBASE 2688	
	LPTS3-	4	TESTO	T/S FOR DISPLAYS		DBASE 2689
C13H41	PTSN X	13H411	E	17 TESTO 23		DBASE 2690
C13H41	PTSK	0	9-	TESTO 23		DBASE 2691
C13H41	CTS	0	TESTO 23	TESTO 23	DBASE 2692	
13H411	LPTS35	13H402	0	TESTO 23		DBASE 2693
	LPTS35	4	TESTO	LRU 13H41 T/S		DBASE 2694
13H412	GPTS35	13H403	0	TESTO 23	13 29L	DBASE 2695
13H413	GPTS35	0	TESTO 23	TESTO 23	DBASE 2696	
C74KJ1	PTSN X	74KC01	E	30 TESTO 23		DBASE 2697
C74KJ1	PTSK	0	6-	TESTO 23		DBASE 2698
C74KJ1	CTS	0	TESTO 23	TESTO 23	DBASE 2699	
74KC01	LPTS36	74KC02	0	TESTO 23		DBASE 2700
	LPTS36	4	TESTO	LRU 74KC01 T/S		DBASE 2701
74KC02	GPTS36	74KC03	0	TESTO 23	12 29L	DBASE 2702
74KC03	GPTS36	0	TESTO 23	TESTO 23	DBASE 2703	

C74J31	PTSN< 7-JC61	E	19	TESTO 23	DBASE 2704
C74J31	PTSK	E	91	TESTO 23	DBASE 2705
C74J32	GPTS30	E	TESTO 23	DBASE 2706	
Z41C21	LPTS37	Z41C22	E	TESTO 23	DBASE 2707
	LPTS37	4	TESTO	LRU 7-JC1 T/S	DBASE 2708
Z41C22	GPTS37	Z41C23	E	TESTO 23	DBASE 2709
Z41C23	PTSN< Z41M1	E	1	TESTO 23	DBASE 2710
C63M1	PTSK	E	91	TESTO 23	DBASE 2711
C63M1	CTSO	E	TESTO 23	DBASE 2712	
653M11	LPTS39	653M62	E	TESTO 23	DBASE 2713
	LPTS39	1	TESTO	LRU 653M62 T/S	DBASE 2714
653M62	GPTS39	653M63	E	TESTO 23	DBASE 2715
653M7	GPTS39	E	TESTO 23	DBASE 2716	
664B2A	PTSN< 663FA1	E	16	TESTO 23	DBASE 2717
C66B2A	PTSK	E	96	TESTO 23	DBASE 2718
C66B2A	CTSO	E	TESTO 23	DBASE 2719	
669FA1	LPTS39	669FA2	E	TESTO 23	DBASE 2720
	LPTS39	4	TESTO	LRU 669FA1 T/S	DBASE 2721
669FA2	GPTS39	669FA3	E	TESTO 23	DBASE 2722
669FA3	GPTS39	E	TESTO 23	DBASE 2723	
C51N11	PTSN< 51N11	E	12	TESTO 23	DBASE 2724
C51N11	PTSK	E	63	TESTO 23	DBASE 2725
C51N11	CTSO	E	TESTO 23	DBASE 2726	
S1N421	LPTS42	S1N422	E	TESTO 23	DBASE 2727
	LPTS42	1	TESTO	LRU S1N421 T/S	DBASE 2728
S1N422	GPTS42	S1N423	E	TESTO 23	DBASE 2729
S1N423	GPTS42	E	TESTO 23	DBASE 2730	
C74K41	PTSN< 7-K41	E	24	TESTO 23	DBASE 2731
C74K41	PTSK	E	76	TESTO 23	DBASE 2732
C74K41	CTSO	E	TESTO 23	DBASE 2733	
Z41K41	LPTS41	Z41K42	E	TESTO 23	DBASE 2734
	LPTS41	4	TESTO	LRU Z41K41 T/S	DBASE 2735
Z41K42	GPTS41	Z41K43	E	TESTO 23	DBASE 2736
Z41K43	GPTS41	E	TESTO 23	DBASE 2737	
C51N31	PTSN< S1N31	E	32	TESTO 23	DBASE 2738
C51N31	PTSK	E	68	TESTO 23	DBASE 2739
C51N31	CTSO	E	TESTO 23	DBASE 2740	
S1N311	LPTS42	S1N312	E	TESTO 23	DBASE 2741
	LPTS42	1	TESTO	LRU S1N311 T/S	DBASE 2742
S1N312	GPTS42	S1N313	E	TESTO 23	DBASE 2743
S1N313	GPTS42	E	TESTO 23	DBASE 2744	
C74FF1	PTSN< 7-FF1	E	19	TESTO 23	DBASE 2745
C74FF1	PTSK	E	91	TESTO 23	DBASE 2746
C74FF2	CTSO	E	TESTO 23	DBASE 2747	
Z41FF1	LPTS41	Z41FF2	E	TESTO 23	DBASE 2748
	LPTS41	1	TESTO	LRU Z41FF1 T/S	DBASE 2749
Z41FF2	GPTS41	Z41FF3	E	TESTO 23	DBASE 2750
Z41FF3	GPTS41	E	TESTO 23	DBASE 2751	
Z75MC1	PTSN< 75MC1	E	16	TESTO 23	DBASE 2752
C75MC1	PTSK	E	91	TESTO 23	DBASE 2753
C75MC1	CTSO	E	TESTO 23	DBASE 2754	
Z75MC1	LPTS41	Z75MC2	E	TESTO 23	DBASE 2755
	LPTS41	1	TESTO	LRU Z75MC1 T/S	DBASE 2756
Z75MC2	GPTS41	Z75MC3	E	TESTO 23	DBASE 2757
Z75MC3	GPTS41	E	TESTO 23	DBASE 2758	
C75MC1	PTSN< 75MC1	E	39	TESTO 23	DBASE 2759
C75MC1	PTSK	E	91	TESTO 23	DBASE 2760
C75MC1	CTSO	E	TESTO 23	DBASE 2761	
Z75MC1	LPTS41	Z75MC2	E	TESTO 23	DBASE 2762
	LPTS41	1	TESTO	LRU Z75MC1 T/S	DBASE 2763
Z75MC2	GPTS41	Z75MC3	E	TESTO 23	DBASE 2764
Z75MC3	GPTS41	E	TESTO 23	DBASE 2765	
C75MC1	PTSN< 75MC1	E	37	TESTO 23	DBASE 2766
C75MC1	PTSK	E	63	TESTO 23	DBASE 2767
C75MC1	CTSO	E	TESTO 23	DBASE 2768	

76J411 LOTS46	76J412 C	TESTD 23	DBASE 2770
LOTS-6	4	TESTD LFU 76JA T/S	DBASE 2771
76J412 DOTS-6	76J413 3	TESTD 23 13 29L	DBASE 2772
76J412 GOTS-3	0	TESTD 22	DBASE 2773
	4	TSC TSC TEST STATION	DBASE 2774
CTS0 DUMTS0	CTS01 0	TSC 23 11 C 1TSC	DBASE 2775
CTS01 DCMTS0	CTS01 0	TSC 23	DBASE 2776
TS01 FTSC	TS02 0	65 TSC 23	DBASE 2777
TS02 GTSC	TS03 0	TSC 23 53 29L	DBASE 2778
TS03 GTSC	0	TSC *23	DBASE 2779
	4	TSM TSM TEST STATION	DBASE 2780
TS04 DUMTSM	TS041 0	TSM 23 11 C 1TSM	DBASE 2781
CTS11 DCMTS1	TS01 0	TSM 23	DBASE 2782
TS01 FTSM	TS02 0	EZ TSM 23	DBASE 2783
TS02 GTSM	TS03 0	TSM 23 50 29L	DBASE 2784
TS03 GTSM	0	TSM *23	DBASE 2785
	4	TS0 TSO TEST STATION	DBASE 2786
CTS0 DUMTS0	CTS01 0	TS0 23 11 C 1TS0	DBASE 2787
CTS01 DCMTS0	CTS01 0	TS0 23	DBASE 2788
TS01 FTSO	TS02 0	EZ TS0 23	DBASE 2789
TS02 GTSO	TS03 0	TS0 23 50 29L	DBASE 2790
TS03 GTSO	0	TS0 *23	DBASE 2791

APPENDIX B

F-15 TFTW OPERATIONS DATA FILE

APPENDIX B

F-15 TFTW OPERATIONS DATA FILE

1. The operational scenarios contained in this appendix use scheduled aircraft sortie rates of .43, .74, and 1.0. Each scenario schedules aircraft flying and maintenance activity Monday through Friday. The same schedule is repeated each week during the simulation.
2. Explanation of Aircraft Mission Names:
  - a. PFLTF and PFLTTF are dummy missions that make a specified number of corresponding F-15 and TF-15 aircraft unavailable each day.
  - b. AAXX designates Air-Air Missions. The third character defines aircraft type: one is a TF-15 and two is an F-15. The fourth character defines the type of aircraft processing and number of times an aircraft flies each day: one is preflight to thruflight, two is thruflight to thruflight, three is thruflight to postflight, and four is preflight to postflight.
  - c. CONVXX designates conversion missions. The fifth character defines the aircraft type: one is a TF-15 and two is an F-15. The sixth character defines the type of aircraft processing and number of times an aircraft flies each day: one is preflight to thruflight, two is thruflight to postflight, three is thruflight to thruflight, and four is preflight to postflight.
  - d. PHASF and PHASTF are F-15 and TF-15 aircraft scheduled for Phase Inspection.
  - e. WASHF and WASHTF are F-15 and TF-15 aircraft scheduled for Washing and Corrosion Control Inspection.

3. Explanation of Column Headings:

- a. TIME - Daily simulation time when an aircraft begins mission processing.
- b. MISSION - Mission name.
- c. A/C TYPE - self explanatory.
- d. SCHED - number of aircraft scheduled for a given mission.
- e. MIN - minimum number of aircraft required to fly a given mission.
- f. SPARE - identifies preparation of spare aircraft for a given mission. If the spare is not used for the mission it is designated for, it then becomes a spare for the next mission.
- g. PRIORITY - LCOM peculiar code that allows an order of importance to mission scheduling.
- h. TAKEOFF - scheduled takeoff time 24 hour clock.
- i. LATENESS - time remaining after scheduled takeoff time before mission cancellation.
- j. SORTIE LENGTH - sortie length in hours and minutes.

.43 OPERATIONAL SCENARIO

DAY 1

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	A221	F15	2	2	1	2	500	2+ 0
114	CONV21	F15	2	2	1	2	545	2+ 0
130	CONV21	TF15	2	2	1	2	600	2+ 0
144	A211	TF15	1	1	0	2	615	2+ 0
215	A216	TF15	2	2	0	2	665	2+ 0
229	A221	F15	1	1	0	2	700	2+ 0
329	A216	TF15	1	1	0	2	800	2+ 0
349	A226	F15	3	3	0	2	820	2+ 0
388	CONV26	F15	2	2	0	2	930	2+ 0
649	A226	F15	1	1	0	2	1120	2+ 0
649	A216	TF15	2	2	0	2	1120	2+ 0
730	CONV12	TF15	1	1	0	2	1200	2+ 0
761	WASHF	F15	1	1	0	2	800	5+ 0
761	PHASF	TF15	1	1	0	2	800	5+ 0
759	PELTTF	TF15	16	2	0	3	1200	6+ 0
759	PELTF	F15	31	2	0	3	1200	6+ 0
1009	A226	F15	2	2	0	2	1440	2+ 0
1030	A213	TF15	1	1	0	2	1500	2+ 0
1059	A223	F15	2	2	0	2	1530	2+ 0
1230	A223	F15	1	1	0	2	1700	2+ 0
1300	CONV12	TF15	1	1	0	2	1730	2+ 0
1315	CONV22	F15	2	2	0	2	1745	2+ 0

DAY 2

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
59	A211	TF15	2	2	1	2	530	2+ 0
144	CONV21	F15	2	2	1	2	615	2+ 0
229	CONV26	F15	2	2	0	2	700	2+ 0
245	A216	TF15	2	2	0	2	715	2+ 0
400	A221	F15	1	1	0	2	730	2+ 0
430	A221	F15	2	2	0	2	900	2+ 0
430	A216	TF15	1	1	0	2	900	2+ 0
510	CONV11	TF15	1	1	1	2	940	2+ 0
614	CONV22	F15	2	2	0	2	1045	2+ 0
620	A226	F15	2	2	0	2	1050	2+ 0
645	A224	F15	2	2	0	2	1115	2+ 0
730	WASHF	F15	1	1	0	2	800	5+ 0
736	A224	F15	2	2	0	2	1200	2+ 1
736	A216	TF15	1	1	0	2	1200	2+ 0
761	PHASF	F15	1	1	0	2	800	5+ 0
800	PELTTF	TF15	16	2	0	3	1200	6+ 0
800	PELYTF	TF15	31	2	0	3	1200	6+ 0
929	A223	F15	2	2	0	2	1300	2+ 0
1100	CONV12	TF15	1	1	0	2	1530	2+ 0
1310	A227	F15	1	1	0	2	1740	2+ 0
1310	A213	TF15	2	2	0	2	1740	2+ 0
1600	CONV14	TF15	1	1	0	2	2030	2+ 0

DAY 3

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	A221	F15	2	2	1	2	500	2+ 0
100	CONV11	TF15	1	1	0	2	530	2+ 0
186	CONV21	F15	2	2	1	2	535	2+ 0
142	A211	TF15	2	2	1	2	615	2+ 0
215	A216	TF15	1	1	0	2	665	2+ 0
230	A221	F15	1	1	0	2	700	2+ 0
329	A216	TF15	1	1	0	2	800	2+ 0
350	A226	F15	3	3	0	2	820	2+ 0
430	A221	F15	1	1	1	2	900	2+ 1
459	CONV24	F15	3	1	0	2	930	2+ 0
557	A222	F15	2	2	0	2	1030	2+ 0
667	A224	F15	1	1	0	2	1120	2+ 0
650	A216	TF15	1	1	0	2	1120	2+ 0
700	CONV14	TF15	1	1	0	2	1130	2+ 0
730	WASHF	F15	1	1	0	2	800	5+ 0
730	CONV12	TF15	1	1	0	2	1200	2+ 0
761	PHASF	F15	1	1	0	2	800	5+ 0
759	PELTTF	TF15	16	2	0	3	1200	6+ 0
763	PELYTF	TF15	29	2	0	3	1200	6+ 0
1010	A224	F15	1	1	0	2	1440	2+ 0
1030	A213	TF15	2	2	0	2	1500	2+ 0
1229	A223	F15	2	2	0	2	1700	2+ 0
1314	CONV22	F15	1	1	0	2	1745	2+ 0
1330	CONV22	F15	1	1	0	2	1800	2+ 0
1345	A223	F15	2	2	0	2	1815	2+ 0

DAY 4

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
100	AA211	TF15	1	1	1	2	530	2+ 0
145	CONV21	F15	3	3	1	2	615	2+ 0
149	AA21	F15	2	2	1	2	620	2+ 0
248	CONV26	F15	1	1	0	2	710	2+ 0
264	AA14	TF15	2	2	0	2	715	2+ 0
308	AA21	F15	3	3	0	2	730	2+ 0
329	AA14	TF15	1	1	0	2	800	2+ 0
408	CONV14	TF15	2	2	1	2	830	2+ 0
430	AA21	F15	2	2	0	2	900	2+ 0
430	AA14	TF15	1	1	0	2	900	2+ 0
645	AA24	F15	1	1	0	2	1115	2+ 0
730	MASHTF	F15	1	1	0	2	800	5+ 0
741	PHASF	F15	1	1	0	2	800	5+ 0
759	PFLTF	F15	31	2	0	3	1200	6+ 0
759	PFLTTF	TF15	14	2	0	3	1200	6+ 0
830	AA23	F15	3	3	0	2	1300	2+ 0
900	AA24	F15	1	1	0	2	1330	2+ 0
900	AA14	TF15	1	1	0	2	1330	2+ 0
919	CONV22	F15	3	3	0	2	1350	2+ 0
1245	AA21	F15	2	2	0	2	1715	2+ 0
1310	AA23	F15	1	1	0	2	1740	2+ 0
1310	AA13	TF15	1	1	0	2	1740	2+ 0
1330	AA23	F15	1	1	0	2	1800	2+ 0

DAY 5

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
30	AA21	F15	2	2	1	2	500	2+ 0
59	CONV11	TF15	1	1	0	2	530	2+ 0
162	AA11	TF15	3	3	1	2	615	2+ 0
200	CONV14	TF15	1	1	0	2	630	2+ 0
229	AA21	F15	2	2	1	2	700	2+ 0
308	CONV21	F15	3	3	1	2	730	2+ 0
350	AA24	F15	3	3	0	2	820	2+ 0
500	CONV24	F15	1	1	0	2	930	2+ 0
529	AA26	F15	2	2	0	2	1000	2+ 0
667	AA26	F15	1	1	0	2	1120	2+ 0
690	AA14	TF15	1	1	0	2	1120	2+ 0
730	MASHTF	TF15	1	1	0	2	800	5+ 0
730	CONV12	TF15	1	1	0	2	1200	2+ 0
742	PHASTF	TF15	1	1	0	2	800	5+ 0
800	PFLTF	F15	30	2	0	3	1200	6+ 0
800	PFLTTF	TF15	15	2	0	3	1200	6+ 0
1010	AA24	F15	1	1	0	2	1440	2+ 0
1030	AA13	TF15	3	3	0	2	1500	2+ 0
1100	AA23	F15	2	2	0	2	1530	2+ 0
1230	AA23	F15	2	2	0	2	1700	2+ 0
1315	CONV22	F15	3	3	0	2	1765	2+ 0

.74 OPERATIONAL SCENARIO

DAY 1

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)	PRIORITY	TAKEOFF	LATENESS	TO-TIE LENGTH
129	REFI	F15	2	2	1	2	2+
160	CONV11	TF15	1	1	6	2	51
126	CONV21	TF15	2	2	2	2	49
130	CONV11	TF15	2	2	1	2	60
145	REFI	TF15	1	1	2	2	61
159	CONV14	TF15	4	2	2	2	630
219	REFI	TF15	2	2	0	2	64
236	4421	F15	1	3	0	2	703
329	REFI	TF15	1	1	2	2	71
350	4426	F15	3	3	1	2	821
400	4421	TF15	2	2	0	2	833
614	4421	F15	2	2	0	2	845
659	CONV26	TF15	2	2	0	2	93
531	4424	F15	2	2	1	2	1011
800	4422	TF15	2	2	0	2	1013
656	4424	F15	1	1	0	2	1126
690	4423	TF15	2	1	0	2	1127
716	CONV11	TF15	1	1	0	2	117
730	443MF	TF15	1	1	2	2	93
731	CONV14	TF15	1	1	0	2	1203
761	4425	TF15	2	1	2	2	97
762	4425TF	TF15	2	1	2	2	98
759	44LTTF	TF15	6	2	2	3	221
759	44LTTF	TF15	1	2	2	3	222
1069	4424	F15	3	3	0	2	1461
1071	4423	TF15	2	2	1	2	147
1059	4423	F15	2	2	0	2	1531
1139	4423	TF15	3	3	0	2	1613
1229	4423	F15	2	2	1	2	171
1300	CONV12	TF15	2	1	2	2	177
1314	CONV12	F15	2	2	0	2	1745
1645	4423	F15	2	2	0	2	2115

DAY 2

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)	PRIORITY	TAKEOFF	LATENESS	TO-TIE LENGTH
180	4421	F15	2	2	1	2	57
131	CONV21	TF15	2	2	2	2	60
145	CONV21	F15	2	2	1	2	615
151	4421	TF15	2	2	2	2	63
230	CONV24	F15	2	2	1	2	71
268	4424	TF15	2	2	2	2	719
301	4421	F15	3	3	1	2	77
349	4421	TF15	2	2	0	2	919
436	4421	F15	1	1	0	2	936
438	4425	TF15	2	1	2	2	938
569	CONV11	TF15	2	2	1	2	941
680	CONV12	TF15	2	2	1	2	980
615	CONV22	F15	2	2	1	2	1045
629	4424	TF15	2	2	2	2	1059
645	4424	F15	2	2	1	2	1115
700	4423	TF15	2	2	2	2	1129
730	445MF	F15	1	1	0	2	93
730	4424	TF15	2	2	1	2	121
761	4425TF	TF15	1	1	1	2	131
762	445MF	TF15	1	1	0	2	141
761	445MF	F15	1	1	0	2	146
759	44LTTF	TF15	18	2	2	3	12
759	44LTTF	TF15	6	2	0	3	12
837	4423	F15	2	3	1	2	132
900	4424	F15	1	1	0	2	1331
900	4424	TF15	1	1	0	2	134
1065	CONV22	F15	2	2	2	2	1515
1059	CONV12	TF15	2	2	2	2	159
1130	CONV24	F15	2	2	1	2	161
1239	CONV24	TF15	1	1	2	2	171
1239	CONV12	TF15	1	1	2	2	171
1300	4423	TF15	2	2	0	2	176
1309	4423	F15	1	1	0	2	176
1309	4423	TF15	1	1	0	2	177
1331	4423	F15	2	2	0	2	18
1063	CONV12	TF15	2	2	0	2	201
1631	CONV12	TF15	2	2	0	2	201

TIME	MISSION	A/C TYPE	SCHED (H:M:S)	SPARES	PRIORITY	TAKEOFF	LATENESS	SOFTIE LENGTH
38	4821	F15	2 2 1	2	9	20	+	1+2
59	CONV11	TF15	1 1 0	2	52	20	+	1+5
109	CONV21	F15	2 2 0	2	93	20	+	1+22
130	CONV11	TF15	2 2 1	2	60	20	+	1+26
162	4821	TF15	4 1 0	2	62	20	+	20
200	CONV14	TF15	6 2 1	2	63	20	+	1+1
215	4821	TF15	2 2 0	2	64	20	+	20
229	4821	F15	3 3 0	2	71	20	+	1+19
330	4818	TF15	1 1 0	2	90	20	+	0+7
349	4821	F15	3 3 0	2	82	20	+	1+15
437	4821	F15	3 3 0	2	91	20	+	20
500	CONV24	F15	2 2 0	2	93	20	+	1+21
529	4821	F15	2 2 0	2	101	20	+	1+2
557	4822	F15	2 2 0	2	103	20	+	1+21
647	4828	F15	2 2 0	2	112	20	+	1+9
669	4814	TF15	1 1 0	2	112	20	+	0+53
689	CONV14	TF15	1 1 0	2	113	20	+	1+4
730	48SHF	F15	1 1 0	2	81	50	+	20 5
736	CONV22	TF15	1 1 0	2	120	20	+	20 3
736	CONV24	F15	2 2 0	2	125	20	+	1+13
781	2FL52	F15	1 1 0	2	90	50	+	20 6
781	2FL52	F15	1 1 0	2	80	50	+	20 5
781	2FL52	F15	1 1 0	2	91	20	+	20 6
800	2FLTTF	TF15	7 2 0	3	121	60	+	12+1
801	2FLTT	TF15	2 2 0	3	122	50	+	20 4
801	4814	TF15	1 1 0	2	123	20	+	0+3
1059	ST24	F15	2 3 0	2	166	20	+	1+2
1130	4813	TF15	1 1 0	2	150	20	+	1+ 9
1231	4823	F15	2 2 0	2	171	20	+	20
1259	CONV12	TF15	2 2 0	2	173	20	+	1+22
1315	CONV22	F15	2 2 0	2	178	20	+	20 8
1333	CONV22	F15	2 2 0	2	180	20	+	1+33
1366	4823	F15	2 2 0	2	181	20	+	20 9
1666	4823	F15	2 2 0	2	211	20	+	20 24

DAY 6

TIME	MISSION	A/C TYPE	SCHED (H:M:S)	SPARES	PRIORITY	TAKEOFF	LATENESS	SOFTIE LENGTH
59	4821	F15	2 2 1	2	93	20	+	20
130	CONV11	TF15	2 2 1	2	61	20	+	1+34
166	CONV21	F15	2 2 0	2	81	20	+	1+22
156	4821	F15	2 2 1	2	62	20	+	1+ 3
239	CONV24	F15	2 2 0	2	71	20	+	1+29
245	4814	TF15	2 2 0	2	715	20	+	1+16
301	4821	F15	3 3 0	2	73	20	+	20 7
330	4814	TF15	2 2 1	2	81	20	+	1+ 3
359	CONV14	TF15	2 2 0	2	83	20	+	20 14
430	4821	F15	1 1 0	2	95	20	+	1+ 9
430	4821	TF15	2 2 0	2	96	20	+	20 21
601	CONV14	TF15	2 2 0	2	113	20	+	1+25
669	4823	F15	2 2 0	2	114	20	+	20 9
689	4822	F15	2 2 0	2	115	20	+	1+49
709	4822	F15	2 2 0	2	116	20	+	20 2
731	4854T	TF15	1 1 0	2	91	50	+	20 6
731	4854T	F15	1 1 0	2	92	50	+	20 9
730	4821	F15	2 2 0	2	121	20	+	1+53
901	4821	TF15	2 2 0	2	122	50	+	12+1
830	2FLTTF	TF15	7 2 0	3	120	60	+	12+1
829	4829	F15	9 9 0	2	121	20	+	1+4
845	CONV24	F15	2 2 0	2	131	20	+	1+27
901	4821	F15	1 1 0	2	132	20	+	20 9
901	4814	TF15	1 1 0	2	133	20	+	1+ 5
921	CONV22	F15	2 2 0	2	134	20	+	20 2
1100	4821	F15	2 2 0	2	153	20	+	1+19
1240	CONV24	F15	2 2 0	2	171	20	+	1+57
1241	CONV12	TF15	1 1 0	2	171	20	+	1+1
1259	4823	F15	2 2 0	2	172	20	+	20 16
1309	4821	F15	1 1 0	2	174	20	+	1+17
1369	4823	F15	2 2 0	2	175	20	+	20 9
1331	4821	F15	2 2 0	2	181	20	+	1+53
1399	CONV14	TF15	2 2 0	2	203	20	+	20 9
1630	CONV12	TF15	2 2 0	2	210	20	+	1+ 7

DAY 8

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)	PRIORITY	TAKEOFF	LATENESS	SOARIE LENGTH
30	4A21	TF19	2	2	2	2+	2+9
59	CONV11	TF15	1	1	2	2+	1+25
130	CONV11	TF15	2	2	2	2+	1+27
162	4A11	TF15	1	1	2	2+	1+2
200	CONV14	TF19	2	2	2	2+	2+9
215	4A11	TF15	2	2	2	2+	2+13
229	4A21	TF19	3	3	2	2+	1+19
303	CONV21	TF15	2	2	2	2+	1+44
330	4A24	TF19	2	2	2	2+	1+4
369	4A24	TF15	3	3	2	2+	1+ 6
399	4A22	TF19	2	2	2	2+	1+ 9
415	4A21	TF15	2	2	2	2+	1+ 5
500	CONV20	TF15	2	2	2	2+	2+19
529	4A24	TF15	2	2	2	2+	1+52
557	4A22	TF19	2	2	2	2+	2+19
647	4A24	TF15	1	1	2	2+	1+ 3
669	4A14	TF19	2	2	2	2+	2+53
695	CONV14	TF15	1	1	2	2+	1+18
730	465MTP	TF19	2	2	2	2+	2+ 9
731	CONV13	TF15	1	1	2	2+	1+32
760	4A21	TF19	22	2	2	2+	12+3
900	46LTTF	TF15	6	2	2	2+	12+ 3
1009	4A24	TF19	3	3	2	2+	2+12
1030	4A13	TF15	1	1	2	2+	1+56
1111	4A22	TF19	2	2	2	2+	2+14
1179	4A23	TF15	3	3	2	2+	1+ 3
1231	4A22	TF19	2	2	2	2+	1+2
1253	CONV12	TF15	1	1	2	2+	1+23
1315	CONV22	TF15	2	2	2	2+	2+17
1646	4A23	TF15	2	2	2	2+	2+ 4

## 1.0 OPERATIONAL SCENARIO

DAY 1

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	AA21	F15	2	2	1	2	500	2+ 0
59	PHASF	F15	1	1	0	2	820	5+ 0
59	PHASF	F15	1	1	0	2	800	5+ 0
59	PHASTF	TF15	1	1	0	2	800	5+ 0
59	WASHF	F15	1	1	0	2	800	5+ 0
108	CONV11	TF15	1	1	0	2	530	2+ 0
109	AA11	TF15	2	2	1	2	540	2+ 0
109	AA21	F15	2	2	0	2	540	2+ 0
116	CONV21	F15	2	2	1	2	545	2+ 0
130	CONV11	TF15	2	2	1	2	610	2+ 0
146	AA21	F15	2	2	0	2	615	2+ 0
146	AA11	TF15	1	1	0	2	615	0+59
159	CONV16	TF15	4	2	1	2	630	2+ 0
219	AA16	TF15	2	2	0	2	645	2+ 0
229	AA21	F15	1	3	0	2	700	2+ 0
239	CONV11	TF15	1	1	0	2	710	2+ 0
308	CONV26	F15	2	2	1	2	730	2+ 0
314	CONV21	F15	1	1	0	2	745	2+ 0
329	AA16	TF15	1	1	0	2	800	2+ 0
349	AA26	F15	3	3	1	2	820	2+ 0
359	AA21	F15	2	2	0	2	830	2+ 0
419	AA21	F15	2	2	0	2	845	2+ 0
363	CONV26	F15	2	2	0	2	930	2+ 0
529	AA24	F15	2	2	0	2	1010	2+ 0
545	AA26	F15	1	1	0	2	1015	2+ 0
545	AA16	TF15	1	1	0	2	1015	2+ 0
688	AA22	F15	2	2	0	2	1030	2+ 0
689	AA26	F15	1	1	0	2	1120	2+ 0
689	AA16	TF15	1	1	0	2	1120	0+52
708	CONV16	TF15	1	1	0	2	1130	2+ 0
715	AA23	F15	2	2	0	2	1145	2+ 0
725	A613	TF15	2	2	0	2	1155	2+ 0
736	CONV12	TF15	1	1	0	2	1200	2+ 0
759	PFLTF	TF15	3	2	0	3	1200	6+ 0
759	PFLTF	F15	11	2	0	3	1200	12+ 0
829	AA23	F15	2	2	0	2	1300	2+ 0
1059	AA26	F15	3	3	0	2	1440	2+ 0
1030	AA13	TF15	2	2	0	2	1500	2+ 0
1344	CONV22	F15	1	1	0	2	1515	2+ 0
1059	AA23	F15	2	2	0	2	1530	2+ 0
1129	CONV12	TF15	1	1	0	2	1545	2+ 0
1139	AA23	F15	3	3	0	2	1610	2+ 0
1236	AA23	F15	2	2	0	2	1700	2+ 0
1308	CONV12	TF15	1	1	0	2	1730	2+ 0
1315	CONV22	F15	2	2	0	2	1745	2+ 0
1665	AA23	F15	2	2	0	2	2115	2+ 0

## DAY 2

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
59	AA21	F15	2	2	1	2	530	2+ 0
108	MASHF	F15	1	1	0	2	600	5+ 0
100	PHASTF	TF15	1	1	0	2	610	5+ 0
108	PHASF	F15	1	1	0	2	610	5+ 0
108	PHASF	F15	1	1	0	2	600	5+ 0
118	CONV24	F15	1	1	1	2	540	2+ 0
111	CONV24	F15	1	1	0	2	542	2+ 0
115	CONV24	F15	1	1	0	2	545	2+ 0
130	CONV11	TF15	2	2	1	2	600	2+ 0
144	CONV21	F15	2	2	1	2	615	2+ 0
158	AA21	F15	2	2	1	2	623	2+ 0
210	CONV11	TF15	1	1	0	2	643	2+ 0
229	CONV24	F15	2	2	0	2	700	2+ 0
245	AA14	TF15	2	2	1	2	715	2+ 0
300	AA21	F15	3	3	0	2	730	2+ 0
345	AA21	F15	2	2	0	2	815	2+ 0
359	AA26	F15	2	1	0	2	830	2+ 0
359	AA14	TF15	1	1	0	2	830	2+ 0
415	AA24	F15	1	1	0	2	845	2+ 0
415	AA14	TF15	1	1	0	2	845	2+ 0
436	AA21	F15	1	1	0	2	900	2+ 0
430	AA14	TF15	1	1	0	2	930	2+ 0
510	CONV11	TF15	2	2	0	2	940	2+ 0
529	AA21	F15	2	1	0	2	1000	2+ 0
529	AA11	TF15	1	1	0	2	1033	2+ 0
600	CONV11	TF15	2	2	0	2	1033	2+ 0
614	CONV22	F15	2	2	0	2	1045	2+ 0
620	AA24	F15	2	2	0	2	1050	2+ 0
645	AA26	F15	2	2	0	2	1115	2+ 0
659	AA23	F15	2	2	0	2	1130	2+ 0
730	AA24	F15	2	2	0	2	1200	2+ 0
800	PFLTF	TF15	5	2	0	3	1200	6+ 0
808	PFLTF	F15	9	2	0	3	1200	6+ 0
829	AA23	F15	3	3	0	2	1330	2+ 0
901	AA26	F15	1	1	0	2	1330	2+ 0
900	AA14	TF15	1	1	0	2	1330	2+ 0
930	CONV12	TF15	1	1	0	2	1400	2+ 0
1344	CONV22	F15	2	2	0	2	1515	2+ 0
1100	CONV12	TF15	2	2	0	2	1530	2+ 0
1129	CONV24	F15	2	2	0	2	1600	2+ 0
1240	CONV24	F15	1	1	0	2	1710	2+ 0
1240	CONV12	TF15	1	1	0	2	1713	2+ 0
1300	AA23	F15	2	2	0	2	1730	2+ 0
1310	AA23	F15	1	1	0	2	1743	2+ 0
1318	AA13	TF15	1	1	0	2	1740	2+ 0
1330	AA23	F15	2	2	0	2	1800	2+ 0
1400	AA23	F15	2	2	0	2	1830	2+ 0
1440	AA13	TF15	1	1	0	2	1833	2+ 0
1600	CONV14	TF15	2	2	0	2	2030	2+ 0
1630	CONV12	TF15	2	2	0	2	2100	2+ 0

DAY	J	TIME	MISSION	A/C	TYPE	SCHED (MIN) (SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29		AA21	F15	2	2	1	2	500	2+ 0	1+ 1
59		NASHTF	TF15	1	1	0	2	600	5+ 0	2+ 6
59		PHASF	F15	1	1	0	2	800	5+ 0	2+ 5
59		PHASF	F15	1	1	0	2	800	5+ 0	2+ 6
59		PHASTF	TF15	1	1	0	2	800	5+ 0	2+ 6
59		NASHF	F15	1	1	0	2	800	5+ 0	2+ 5
100		CONV12	TF15	1	1	0	2	933	2+ 0	1+19
106		CONV21	F15	2	2	0	2	935	2+ 0	1+17
130		CONV11	TF15	2	2	1	2	603	2+ 0	1+23
142		AA31	TF15	1	1	0	2	615	2+ 0	1+ 9
159		CONV14	TF15	4	2	1	2	630	2+ 0	1+59
215		AA16	TF15	2	2	0	2	645	2+ 0	2+28
230		AA21	F15	3	3	0	2	700	2+ 0	1+23
244		AA26	F15	2	2	0	2	715	2+ 0	1+12
244		AA11	TF15	1	1	0	2	715	2+ 0	1+ 2
250		CONV21	F15	1	1	1	2	720	2+ 0	1+30
308		CONV21	F15	1	1	0	2	730	2+ 0	1+12
315		AA21	F15	2	2	1	2	745	2+ 0	2+14
329		AA11	TF15	1	1	0	2	803	2+ 0	2+25
356		AA26	F15	3	3	0	2	820	2+ 0	1+ 3
430		AA21	F15	3	3	0	2	933	2+ 0	0+50
459		CONV24	F15	2	2	0	2	933	2+ 0	1+35
530		AA26	F15	2	2	0	2	1033	2+ 0	0+54
530		CONV24	F15	1	1	0	2	1030	2+ 0	1+22
557		AA22	F15	2	2	0	2	1030	2+ 0	1+ 6
667		AA26	F15	1	1	0	2	1123	2+ 0	0+55
653		AA16	TF15	1	1	0	2	1123	2+ 0	0+57
708		CONV14	TF15	1	1	0	2	1133	2+ 0	1+15
730		CONV12	TF15	1	1	0	2	1200	2+ 0	1+23
735		CONV23	F15	2	2	0	2	1205	2+ 0	1+36
759		MPLTF	TF15	3	2	0	3	1200	6+ 0	12+ 0
759		MPLTF	F15	9	2	0	3	1200	6+ 0	12+ 0
759		AA16	TF15	1	1	0	2	1230	2+ 0	1+ 1
830		AA12	TF15	1	1	1	2	1300	2+ 0	1+10
830		AA26	F15	1	1	0	2	1300	2+ 0	1+14
1316		AA26	F15	3	3	0	2	1443	2+ 0	1+15
1830		AA13	TF15	1	1	0	2	1503	2+ 0	1+11
1130		CONV22	F15	1	1	0	2	1600	2+ 0	1+27
1140		CONV22	F15	1	1	0	2	1610	2+ 0	1+23
1200		AA26	F15	2	1	0	2	1633	2+ 0	0+56
1200		AA13	TF15	1	1	0	2	1630	2+ 0	1+ 2
1229		AA23	F15	2	2	0	2	1700	2+ 0	1+ 7
1300		CONV12	TF15	2	2	0	2	1730	2+ 0	1+25
1314		CONV22	F15	2	2	0	2	1745	2+ 0	1+23
1336		CONV22	F15	2	2	0	2	1800	2+ 0	1+36
1345		AA23	F15	2	2	0	2	1815	2+ 0	1+ 9
1630		AA23	F15	2	1	0	2	1900	2+ 0	0+55
1630		AA13	TF15	1	1	0	2	1900	2+ 0	0+52
1645		AA23	F15	2	2	0	2	2115	2+ 0	2+ 9

DAY 6

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
59	MASHF	TF15	1	1	0	2	800	2+ 0
59	MASHF	F15	1	1	0	2	800	2+ 0
59	PHASF	F15	1	1	0	2	800	2+ 0
59	PHASTF	TF15	1	1	0	2	800	2+ 0
100	AA21	F15	2	2	1	2	530	2+ 0
130	CONV11	TF15	2	2	1	2	600	2+ 0
139	AA21	F15	2	2	0	2	610	2+ 0
139	AA11	TF15	1	1	0	2	610	2+ 0
145	CONV21	F15	2	2	1	2	615	2+ 0
149	AA21	F15	2	2	1	2	620	2+ 0
240	CONV24	F15	2	2	0	2	710	2+ 0
244	AA14	TF15	2	2	1	2	715	2+ 0
303	AA21	F15	3	3	0	2	730	2+ 0
319	CONV21	F15	1	1	0	2	745	2+ 0
329	AA16	TF15	2	2	1	2	800	2+ 0
345	AA21	F15	1	1	1	2	815	2+ 0
345	AA16	TF15	1	1	0	2	815	2+ 0
400	CONV14	TF15	2	2	0	2	830	2+ 0
430	AA21	F15	1	1	0	2	900	2+ 0
438	AA14	TF15	1	1	0	2	900	2+ 0
445	CONV11	TF15	1	1	0	2	915	2+ 0
459	CONV21	F15	1	1	0	2	930	2+ 0
630	CONV11	TF15	2	2	0	2	1030	2+ 0
645	AA26	F15	2	2	0	2	1115	2+ 0
708	AA22	F15	2	2	0	2	1130	2+ 0
710	AA22	F15	2	2	0	2	1140	2+ 0
730	AA24	F15	2	2	0	2	1200	2+ 0
759	PFLTF	F15	11	2	0	3	1200	6+ 0
759	PFLTF	TF15	2	2	0	3	1200	6+ 0
830	AA23	F15	3	3	0	2	1300	2+ 0
844	CONV24	F15	2	2	0	2	1315	2+ 0
908	AA24	F15	1	1	0	2	1330	2+ 0
908	AA14	TF15	1	1	0	2	1330	2+ 0
919	CONV22	F15	2	2	0	2	1350	2+ 0
929	AA13	TF15	1	1	0	2	1410	2+ 0
929	AA24	F15	2	1	0	2	1440	2+ 0
1030	AA24	F15	1	1	0	2	1500	2+ 0
1030	AA23	F15	1	1	0	2	1500	2+ 0
1159	AA26	F15	2	2	0	2	1530	2+ 0
1130	AA23	F15	2	2	0	2	1600	2+ 0
1246	CONV24	F15	1	1	0	2	1710	2+ 0
1248	CONV12	TF15	1	1	0	2	1710	2+ 0
1249	AA23	F15	2	2	0	2	1725	2+ 0
1310	AA23	F15	1	1	0	2	1740	2+ 0
1316	AA13	TF15	1	1	0	2	1740	2+ 0
1330	AA23	F15	2	2	0	2	1800	2+ 0
1500	CONV22	F15	1	1	0	2	1930	2+ 0
1515	CONV12	TF15	1	1	0	2	1945	2+ 0
1529	CONV22	F15	1	1	0	2	2000	2+ 0
1600	CONV14	TF15	2	2	0	2	2030	2+ 0
1638	CONV12	TF15	2	2	0	2	2100	2+ 0

## DAY 5

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
30	AA21	TF15	2	2	1	2	500	2+ 0
59	CONV11	TF15	1	1	0	2	530	2+ 0
100	PHASF	TF15	1	1	0	2	600	5+ 0
108	WASHF	TF15	1	1	0	2	600	5+ 0
140	WASHTF	TF15	2	1	0	2	610	5+ 0
130	CONV11	TF15	2	2	1	2	600	2+ 0
162	AA11	TF15	1	1	0	2	615	2+ 0
200	CONV14	TF15	3	2	1	2	630	2+ 0
215	AA16	TF15	2	2	0	2	645	2+ 0
229	AA21	TF15	3	3	1	2	700	2+ 0
300	CONV21	TF15	2	2	1	2	730	2+ 0
316	AA21	TF15	2	2	1	2	745	2+ 0
314	AA11	TF15	1	1	1	2	745	2+ 0
330	AA14	TF15	1	1	0	2	800	2+ 0
350	AA24	TF15	3	3	1	2	820	2+ 0
359	AA21	TF15	2	2	0	2	830	2+ 0
415	AA21	TF15	2	2	0	2	845	2+ 0
430	AA21	TF15	3	2	0	2	900	2+ 0
430	AA11	TF15	1	1	0	2	900	2+ 0
500	CONV24	TF15	2	2	0	2	930	2+ 0
515	CONV21	TF15	1	1	0	2	945	2+ 0
529	AA26	TF15	2	2	0	2	1000	2+ 0
545	CONV11	TF15	1	1	0	2	1015	2+ 0
557	AA22	TF15	2	2	0	2	1030	2+ 0
647	AA24	TF15	1	1	0	2	1120	2+ 0
650	AA16	TF15	3	1	0	2	1120	2+ 0
655	CONV14	TF15	1	1	0	2	1130	2+ 0
730	CONV12	TF15	1	1	0	2	1200	2+ 0
800	PFLTF	TF15	1	2	0	3	1200	6+ 0
800	PFLTF	TF15	3	2	0	3	1200	6+ 0
929	CONV22	TF15	1	1	0	2	1300	2+ 0
935	CONV24	TF15	1	1	0	2	1335	2+ 0
1010	AA26	TF15	3	3	0	2	1440	2+ 0
1030	AA13	TF15	1	1	0	2	1500	2+ 0
1340	AA23	TF15	3	2	0	2	1510	2+ 0
1343	AA16	TF15	1	1	0	2	1510	2+ 0
1100	AA23	TF15	2	2	0	2	1530	2+ 0
1140	AA23	TF15	3	3	0	2	1610	2+ 0
1230	AA23	TF15	2	2	0	2	1730	2+ 0
1259	CONV12	TF15	1	1	0	2	1730	2+ 0
1315	CONV22	TF15	2	2	0	2	1745	2+ 0
1344	AA23	TF15	2	1	0	2	1815	2+ 0
1366	AA13	TF15	2	1	0	2	1815	2+ 0
1429	CONV12	TF15	1	1	0	2	1900	2+ 0
1500	CONV24	TF15	1	1	0	2	1930	2+ 0
1644	AA23	TF15	2	2	0	2	2115	2+ 0
								2+37

APPENDIX C

PERFORMANCE SUMMARY REPORTS AND MATRICES

## APPENDIX C

### PERFORMANCE SUMMARY REPORTS AND MATRICES

Performance Summary Reports (PSR's) and on/off equipment manpower and backorder matrices are illustrated in this appendix. These statistics reflect the results of the F-15 peacetime simulation based on unconstrained parts, unconstrained avionic test stations, and a .74 scheduled sortie rate. Figures C-1, C-2, and C-3 describe the results of the unconstrained manpower simulation. Figures C-4, C-5, and C-6 contain output statistics for the constrained manpower simulation. Drake (Ref 7 and 8) describes in detail the statistical output of an LCOM simulation.

**RUN NUMBER: 80CPN**      **PERFORMANCE SUMMARY**      **PERIOD: 0900Z 06 NOV TO 0800Z**

OPERATIONS		TOTAL	CRUISE	CONTINENTAL	AATP	PHASE	PHASER	WASHIP	WASHIP	PERCENT
1	NUMBER OF TESTINGS PERIOD	2152.0	1.6	0.0	436.00	0.00	350.00	66.30	26.00	70.00
2	NUMBER OF TESTINGS PERIOD	22.5	2.0	0.0	626.00	0.00	369.00	62.00	26.00	70.00
3	PCT TESTS APPROVED	97.00	93.00	90.00	99.71	100.00	100.00	100.00	100.00	100.00
4	NUMBER OF TESTS REQUESTED	2.5	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
5	NUMBER OF TESTS ISSUED	5.6	0.0	0.0	7.00	15.00	86.00	62.00	26.00	70.00
6	PERCENT TESTS ISSUED	92.6	0.0	0.0	99.55	100.00	96.00	62.00	26.00	70.00
7	Avg. TCRF	Total	41.5	31.5	31.5	31.5	31.5	31.5	31.5	31.5
8	NUMBER OF AIRCRAFT AIRTIME (HRS)	72.7	40.0	26.0	0.00	0.00	0.00	0.00	0.00	0.00
9	NUMBER OF AIRCRAFT DAYS AVAIL.	7156.1	7156.1	7156.1	2352.11	0.00	0.00	0.00	0.00	0.00
10	PCT TESTS CRITICAL ALERT	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
11	PCT UNARMED WEAPONS	43.25	15.00	15.00	15.00	15.00	15.00	15.00	15.00	15.00
12	PCT SIGHTED WEAPONS	23.75	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
13	PCT LOSS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
14	PCT SERVICEABLE MAINT.	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15	Avg. Platform Turnaround Time	7.9	6.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
16	Avg. P.O. OR SIGHTED WEAPONS	7.41	6.01	6.01	6.01	6.01	6.01	6.01	6.01	6.01
17	PERSONNEL	Total	32642	32642	32642	32642	32642	32642	32642	32642
18	MANHOURS (AVERAGE) (HR)	1271.0	47.0	6.0	471.00	0.00	471.00	0.00	471.00	0.00
19	MANHOURS AVAIL (HR)	1270.0	47.0	6.0	471.00	0.00	471.00	0.00	471.00	0.00
20	PERCENT UTILIZATON	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
21	PCT USEFUL MANHOURS	117.0	70.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
22	PCT CRITICAL WEAPONS	0.5	1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00
23	PCT USEFUL MANHOURS	14567.0	14567.0	14567.0	3156.00	0.00	11764.00	1930.00	1930.00	1930.00
24	PCT AVAILABLE (HR)	14567.0	14567.0	14567.0	14567.00	14567.00	14567.00	14567.00	14567.00	14567.00
25	PCT 40% USEFUL	150.0	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
26	PCT 75% USEFUL	112.5	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
27	PCT PCT USEFUL	0.0	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
28	PCT PCT USEFUL	0.0	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
29	OVER TIME MANHOURS USED (HR)	0.0	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00
30	MANDUSS PER FLIGHT HOUR	6.67	6.22	0.0	0.00	0.00	0.00	0.00	0.00	0.00
31	MOST FATALISMS PER 1000 HRS. STEMS	0.0	3.01	1.07	3.03	0.01	4.02	0.01	5.02	5.03

Figure C-1. Unconstrained Simulation Performance Summary Report

M A Y T H I R T Y - F O U R T H P E R I O D																				
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	
21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	
41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	
61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	
81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	
101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	
121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	
141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	
161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	
181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	

TODAY'S TASKS = 60 AVERAGE DAYS = 2.0		SAT EQUIPMENT	
AVG. ITEM. SOTKIN = 1.5666211		695.533677 ON EQUIPMENT MANPOWER MATRIX FOR WORK CENTER 326C2 THIS MATRIX COVERS 31 DAYS OF SIMULATION DATA	
0		0	
•	0	0	0
25	0	0	0
•	0	0	0
•	0	0	0
2P	0	0	0
•	0	0	0
•	0	0	0
150	0	0	0
•	0	0	0
•	0	0	0
0	2	1.1	1
•	2	1	1
10	2	1	1
•	2	1	1
4	1.1	1	1
•	4	1	1
16	1	1	1
50	10	1.1	1.1
•	10	2.2	2.3
37	2.2	1.2	1.2
•	37	1.1	1.1
239	514	1517	12 9 9 9 7 6
•	239	514	1111 12 9 9 9 7 6
42A	42A	1112	569 569 569 569 569 569
•	42A	42A	1516 2210 2210 2210 2210 2210
42A	42A	42A	2724 2724 2724 2724 2724 2724
•	42A	42A	191A 1922 1922 1922 1922 1922
C	1	1	1
•	1	2	3
AVE WKR/HR	.9	.6	.5
ST. DEV/HR	.8	.6	.5
TOTAL HOURS = 1629.2 AVE HOURS/DAY = 32.6 ST. DEV/DAY = .30.6			
TOTAL TASKS PERFORMED = 587 AVE TASK TIME = 1.6 ST. DEV = 1.1			
TOTAL REQUIRED MANNING = 10.64			
SHIFT NUMBER	1	2	3
START HOURLY STOP HOUR	0	8 / 16	16 / 24
DIRECT MANNING/TOTAL MANNING INFFECTIVE	1.52 / 2.56	6.93 / 11.55	4.65 / 7.75
MAXIMUM CREWSIZE PER JOB	2	2	2

Figure C-2. AFSC 326X2C on-Equipment Unconstrained Manpower Matrix

YEARS, TASKS =		60	172		
AVERAGE STIDES =		1,682,791	19,461,860		
AVG TIME, SORTIM =		2.912023	339.305908		
OFF EQUIPMENT MANPOWER MATRIX FOR WORK CENTER 531X3 THIS MATRIX COVERS 60 DAYS OF SIMULATION DATA					
0	0	0	0	0	0
25	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
25	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
15	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
10	0	0	0	0	0
0	0	0	0	0	0
0	2	1	1	1	1
0	2	1	1	1	1
0	4	1	1	1	1
50	4	2	2	2	2
0	36	2	2	2	2
1	1	1	1	1	1
0	37	1	1	1	1
9	9	8	7	7	7
0	169	911	910	909	908
0	240	76	75	74	73
4443	4242	4542	4642	4643	4644
0	1	2	2	2	2
AVE MK/HR	.6	.6	.6	.6	.6
ST DEV/HR	2.0	2.0	2.0	2.0	2.0
TOTAL TASKS PERFORMED =	172	AVE TASK TIME =	2.0	AVE ST DEV =	1.4
TOTAL REQUIRED MANNING =	4.57				
SHIFT NUMBER	1	2	3	4	5
START HOUR-STOP HOUR	6 / 0	9 / 16	16 / 24		
DIRECT MANNING/TOTAL MANN (DIRECT) = .60	1.000 / 2.035	1.000 / 3.113	2.000 / 3.333		
MAXIMUM CREWSIZE PER JOB	2	2	2		

Figure C-3. AFSC 531X3 off-Equipment Unconstrained Manpower Matrix

UN NUMBER: 9400UN		PERFORMANCE SUMMARY										
AFFECTED FUNCTIONS		INITIAL	CONVF	CLNVT	AVF	AVTF	PHASEF	PHASVF	WASHF	WASHVF	PFLTF	PFLTV
1. NUMBER OF MISSIONS ACCOMPLISHED	23325.00	318.00	1346.00	917.00	350.00	96.00	52.00	56.00	26.00	70.00	72.00	
2. PERCENT ACCOMPLISHED	22427.00	427.00	179.00	427.00	346.00	64.00	62.00	56.00	26.00	70.00	70.00	
3. NUMBER ACCOMPLISHED	335.00	—	90.50	39.00	93.95	90.00	100.00	100.00	100.00	100.00	100.00	
4. NUMBER OF SERVICES PROVIDED	5096.	96.00	96.00	96.00	96.00	96.00	96.00	96.00	96.00	96.00	96.00	
5. NUMBER ACCOMPLISHED	5134.00	571.00	771.00	1910.00	440.00	84.00	42.00	56.00	26.00	1616.00	946.00	
6. PERCENT ACCOMPLISHED	42.16	96.31	743.00	1735.00	546.00	65.00	52.00	56.00	26.00	162.00	633.00	
AIRCRAFT		IC1AL	F15	TF15	...	...	...	...	...	...	...	
7. NUMBER OF AIRCRAFT AUTH. IN FCR	72.00	46.00	24.00	0.00	—	—	—	—	—	—	—	
8. NUMBER OF AIRCRAFT/DAYS APPROX.	7056.00	716.00	2352.00	0.00	—	—	—	—	—	—	—	
9. PCT SPARES TIME MAINTAIN	13.40	13.00	12.50	1.00	—	—	—	—	—	—	—	
10. PCT UNPLanned MAINTENANCE	16.76	16.17	16.60	1.00	—	—	—	—	—	—	—	
11. PCT SPARES MAINTENANCE	23.41	21.80	20.61	0.00	—	—	—	—	—	—	—	
12. PCT KIPS	0.00	0.00	0.00	0.00	—	—	—	—	—	—	—	
13. PCT SERVICE & MSEN. REPAIR	8.57	8.27	9.31	0.00	—	—	—	—	—	—	—	
14. PCT CREDIBLYNALLY REPAIR	16.14	19.79	10.85	1.00	—	—	—	—	—	—	—	
15. AVG. STICK SHIFT TURNABOUT TIME	5.75	9.62	9.90	0.00	—	—	—	—	—	—	—	
16. AVG. NO. OF SOFTWARE A/S. /DAY	6.74	6.75	6.72	0.00	—	—	—	—	—	—	—	
PERSONNEL		IC1AL	32641	32642	324F1	326n2	326C2	326L2	321n3	321n2	322x1	322x2
17. PERSONnel IN AUTHORIZED F100	35171.00	133.00	1.97	56.00	47.00	56.00	47.00	47.00	101.00	47.00	47.00	
18. PERSONNEL AVAILABLE F100	35171.00	133.00	1.97	56.00	47.00	56.00	47.00	47.00	101.00	47.00	47.00	
19. PERCENT UTILIZATION	1.97	55.49	55.77	52.90	59.00	57.91	60.00	60.00	69.45	59.00	59.00	
20. PERSONNEL USED F100	12255.01	73.96	61.21	20.05	20.00	20.05	20.05	20.05	23.93	57.60	27.78	
21. PCT UNPLanned MAINTENANCE	65.03	110.00	99.34	1.00	97.64	100.00	100.00	100.00	66.12	93.50	25.46	
22. PCT SPARES MAINTENANCE	34.77	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
23. NUMBER OF P-HD WORKED	1439.00	1400.00	33.00	0.00	106.00	186.00	19.00	19.00	19.00	1470.00	252.00	
24. PCT AVAILABLE EQUIPMENT	73.24	1.74	32.24	47.14	17.76	36.75	10.00	10.00	51.00	37.91	97.56	
25. PCT AVAILABLE EQUIPMENT	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
26. PCT F-04, BY FUNCTION	6.28	0.00	1.27	1.25	1.26	0.37	0.00	0.00	0.41	0.00	0.00	
27. PCT PROV. BY PREFERENCE	1.12	6.00	1.44	1.99	7.34	2.2	0.00	0.00	11.35	3.00	0.00	
28. PCT F-04'S NOT USED	19.27	46.26	65.73	55.58	73.66	61.27	0.00	0.00	35.18	17.46	2.38	
29. OVERTIME PAYMENTS USED F100	2.12	6.06	0.34	0.73	1.01	0.00	0.00	0.00	0.18	0.00	0.00	
30. MAXIMUM PER FLIGHT HOUR	5.45	7.32	0.27	0.13	0.12	0.12	0.12	0.12	0.22	0.12	0.12	
31. MOST FREQ OCCURRED FEARS. TICPS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

Figure C-4. Constrained Simulation Performance Summary Report

P E R S O N N E L		10181	4238	4244	4701	43151	43191	43211	43221	43231	43241
17	MANHOURS AUTHORIZED (11J)	3517.03	67.04	36.07	47.00	117.6	55.00	67.07	67.05	67.06	67.05
18	MANHOURS AVAILABLE (11J)	3517.03	67.04	36.07	47.00	117.6	56.00	67.07	67.05	67.06	67.05
19	PERCENT UTILIZATION	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
20	MANHOURS USED (11L)	1255.51	21.06	45.11	67.03	57.02	57.02	52.35	52.35	52.35	52.35
21	PCT US-MTC, MAINTENANCE	65.23	66.35	1.07	46.21	50.02	31.67	10.57	79.12	21.09	7.77
22	PCT SW-MTC, MAINTENANCE	34.77	34.75	1.07	46.21	50.02	31.67	10.57	1.07	92.36	1.07
23	NUMBER OF PFM DEMANDED	1019.91	1165.75	56.07	11.79	1.07	26.07	1.07	1.07	1.07	1.07
24	PCT AVAILABLE EQUIPMENT	71.24	66.06	56.76	1.07	29.02	25.07	57.01	57.01	57.01	57.01
25	PCT AVAILABLE PERSONNEL	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07
26	PCT FFCV. BY EQUIPMENT	6.35	1.59	1.86	1.07	1.07	1.07	1.07	1.07	1.07	1.07
27	PCT FFCV. BY PERSONNEL	1.12	3.15	3.11	1.07	1.07	1.07	1.07	1.07	1.07	1.07
28	PCT DEMANDS NOT SATIS.	49.27	49.30	46.6	5.07	73.69	16.37	0.07	16.37	0.07	0.07
29	OVERTIME PERSONNEL USED (11L)	2.12	6.7	1.07	1.07	1.07	1.07	0.57	1.07	1.07	1.07
30	MANHOURS PFS FLYING HOUR	5.46	6.19	6.2	1.07	1.07	1.07	1.45	1.07	1.07	1.07
31	POST TRAILLESORT FFFTS. ITTEM	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07
TOTAL		46271	53192	51181	53194	53195	53196	53197	53198	53199	53190
37	MANHOURS AUTHORIZED (11G)	3517.03	67.04	47.00	47.00	21.57	78.07	23.52	23.52	23.52	23.52
38	MANHOURS AVAILABLE (11G)	3517.03	67.04	47.00	47.00	21.57	78.07	23.52	23.52	23.52	23.52
39	PERCENT UTILIZATION	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
40	MANHOURS USED (11G)	1255.51	63.59	6.07	7.07	7.07	7.07	9.07	9.07	9.07	9.07
41	PCT US-MTC, MAINTENANCE	65.23	2.95	97.13	1.07	1.07	1.07	1.07	1.07	1.07	1.07
42	PCT SW-MTC, MAINTENANCE	34.77	97.05	2.97	1.07	1.07	1.07	1.07	1.07	1.07	1.07
43	NUMBER OF PFM DEMANDED	1039.91	27826.00	81.17	2.07	216.00	84.07	88.35	15.30	15.30	15.30
44	PCT AVAILABLE EQUIPMENT	71.24	1.11	79.53	2.76	47.26	66.9	92.27	1.07	1.07	1.07
45	PCT AVAILABLE PERSONNEL	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07	1.07
46	PCT FFCV. BY EQUIPMENT	6.39	4.16	1.12	1.07	1.07	1.07	2.67	0.07	0.07	0.07
47	PCT FFCV. BY PERSONNEL	1.12	0.10	1.12	1.07	1.07	1.07	11.61	0.07	0.07	0.07
48	PCT DEMANDS NOT SATIS.	49.27	0.10	19.27	0.07	46.27	16.32	13.1	47.73	0.07	0.07
49	OVERTIME PERSONNEL USED (11G)	2.12	0.17	0.17	0.07	0.15	0.07	0.07	0.07	0.07	0.07
50	MANHOURS PFS FLYING HOUR	5.49	6.28	6.28	1.07	0.17	0.07	0.02	0.02	0.02	0.02
51	POST TRAILLESORT PERS. ITTEM	1.07	9.73	10.77	10.72	10.73	10.73	10.73	10.73	10.73	10.73

Figure C-4. Constrained Simulation Performance Summary Report (continued)

- DAYS OF STSRS =		60		STCQ		THIS MATRIX COVERS		60 DAYS OF SITUATION DATA					
ON EQUIPMENT BACKORDER		MATRIX FOR WORK CENTER 326C2											
3													
25													
6													
5													
4													
3													
2													
1													
0													
- 1		1 1		1 1		1 1		1 1					
0 9		1		1		1		1					
15	11	1 1		1	1	1		1	1				
14	1	1 2	2	1	1	1	1	1	1				
21	1 2	2		1	1	1		1	1				
16	1 1	3 1	1 1 1 2	2 2	2	5		1	1				
16	2	1 1 2	1 2	2 7	1 1	1 1	2 2	1	1				
11	6 4	3 2	4 6	3 2	1	1	1	1	1				
76	1	1 1 2	3 1	1 1 1	1	1	1	1	1				
93	1	1 2	3 1	1 1 1	1	1	1	1	1				
139	5 3	2 3	3 1	1 2	2	1 2	1 2	1 2	1 2				
171	6 5	2 1	2 2	2 2	2 2	3 1	4 3	5 6	5 6				
56	3 7	6 3	3 2	2 2	2 2	3 1	4 3	5 7	5 7				
206	5 5	6 5	4 6	3 4	3 5	3 5	4 6	5 7	5 7				
336	3 3	3 6 3	4 5	3 2	2 1	2 2	3 7	4 7	4 7				
442	4 7	4 5 5	7 5	6 7	6 7	5 5	6 3	7 5	7 5				
479	1	1 1 2	2 2	3 2	4 2	3 2	4 3	5 3	5 3				
2923	2626	2626	303	3636	3345	3637	3632	2336	2225				
1	2	3	4	6	7	8	9	10	11				
AVE OL/H2	3.4	3.6	3.6	2.6	2.3	2.0	1.8	1.7	1.6				
ST DEV/H2	6.3	7.1	6.2	5.5	5.2	4.6	5.3	4.7	4.0				
TOTAL TASKS 8/0 FCF LACK OF MNTPWR = 565 AVE TASKS P/0 / DAY = 6.48 STD DEV / DAY = 24.19 TOTAL HRS OF DELAY = 2036.75													
TOTAL MEN E/D = 728 AVE CREW = 876 / TSK = 1.76 STD DEV = .55 AVE CREW SIZE REQUEST = 2.0 AVE DELAY AFTER TASK = 5.57													
TOTAL REQUIRED PLANNING = 1.70													
SHIFT NUMBER	1	2	3	4	5	6	7	8	9				
STAFF MCU-STOP HOUR	6	8	8	8	8	8	8	8	8				
EFFECT PLANNING/TOTAL PLANNING INFECTION %	7.15	7.11	7.03	7.01	7.01	7.01	7.01	7.01	7.01				
PARTITION CREWSIZE PER JOB	2	1	1	1	1	1	1	1	1				

Figure C-5. AFSC 326X2C on-Equipment Constrained Manpower Backorder Matrix

Figure C-6. AFSC 531X3 off-Equipment Constrained Manpower Backorder Matrix

APPENDIX D

FAILURE CLOCKS

## APPENDIX D

### FAILURE CLOCKS

This appendix lists the LCOM failure clocks, the respective mean sorties between maintenance action (MSBMA), the decrement tasks, and the decrement values. The MSBMA's are in aircraft sorties unless otherwise specified. DCRMT1, DCRMT2, and DCRMT5 are located in the main flight line networks. DCRMT1 advances the failure clocks prior to a mission launch while DCRMT2 and DCRMT5 advance the clocks after launch. All other decrement tasks are located in the phase and/or corrective maintenance networks.

The cumulative decrement values corresponding to certain failure clocks listed in Table D-I do not equal one. This apparent inconsistency is corrected in respective corrective maintenance network. Tetmeyer (Ref 33) describes in detail the procedures used in designing the corrective maintenance networks and decrementing the corresponding failure clocks.

Table D-I  
Failure Clocks

LCOM CLOCK	MSBMA	DECREMENT	
		DCRMT1	DCRMT2
F11A00	18	.02	.98
F11D00	6	.02	.98
F11G00	8	.02	.98
F11K00	20	.02	.98
F11P00	22	.02	.98
F12A00	102	.02	.98
F12B00	125	.02	.98
F12C00	25	.02	.98
F13A00	11	.09	.91
F13B00	26	.09	.91
F13C00	164	.09	.91
F13D00	65	.09	.91
F13F00	178	.09	.91
F13H00	237	.09	.91
F13J00	19	.09	.91
F14AA0	93	.05	.95
F14AB0	711	.05	.95
F14C00	152	.05	.95
F14D00	21	.05	.95
F14E00	67	.05	.95
F14G00	533	.05	.95
F14H00	426	.05	.95
F23000	5	.06	.94
F23100	42	.06	.94
F24A00	44	.14	.86
F24B00	26	.14	.86
F24D00	355	.14	.86
F27000	5	.06	.94
F41A00	20	.05	.95
F42A00	67	.16	.84
F44A00	20	.09	.91
F44B00	267	.09	.91
F44E00	305	.09	.91
F45A00	112	.07	.93
F45B00	133	.07	.93
F45C00	23	.07	.93
F46A00	32	.06	.94
F46B00	355	.06	.94
F46D00	305	.06	.94
F46E00	32	.06	.94
F47A00	63	.10	.90
F49A00	85	.06	.94
F51A00	50		.95
F51E00	51		.95
F51L00	15	.05	
F51M00	426		.95
F51N00	27		.95

Table D-I. Failure Clocks (continued)

LCOM CLOCK	MSBMA	DECREMENT	
		DCRMT1	DCRMT2
F52A00	35	.19	.81
F55A00	237		.99
F55B00	65		.99
F55C00	76		.99
F55L00	420	.01	
F57A00	21		.87
F57L00	70	.13	
F63A00	27		.91
F63B00	25		.91
F63L00	12	.09	
F65A00	142		.98
F65B00	58		.98
F65L00	69	.02	
F71A00	13		.93
F71B00	305		.93
F71C00	533		.93
F71D00	55		.93
F71F00	52		.93
F71L00	8	.07	
F74E00	164		.93
F74F00	4		.93
F74J00	36		.93
F74K00	18		.93
F74L00	6	.07	
F75B00	51		1.00
F75C00	185		1.00
F75D00	152		1.00
F75F00	107		1.00
F75M00	213		1.00
F76A00	18	.11	.89
F76G00	250	.11	.89
F76H00	12		1.00
FCTANK	1333		1.00
FS11PA	590		1.00
FS13HC	1500		1.00
FS14GC	590		1.00
FS2300	33		1.00
FS23HA	89		1.00
		DCRMT3	
FS4700	60	1.00	
FS7500	30	1.00	

Table D-I. Failure Clocks (continued)

LCOM CLOCK	MSBMA	DECREMENT		
F75H00 FSCGUN FSGUNO	20000 rounds 15000 rounds 25000 rounds	<u>DCRMT5</u>		
FD6000	9	<u>DCRMG2</u>	<u>DCRMG3</u>	<u>DCRMG7</u>
FTTU00	5	<u>DCRMH7</u>		
FTSC	65 demands	<u>DCRMTA</u>		
FTSD	65 demands	<u>DCRMTB</u>		
FTSM	65 demands	<u>DCRMTC</u>		
HF	1	<u>DCRMF</u>		
HTF	1	<u>DCRMF</u>		

APPENDIX E

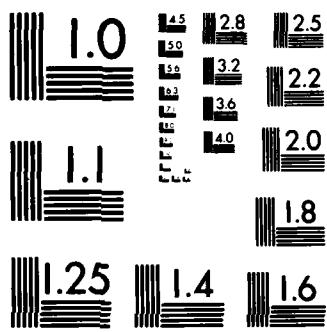
SPARE PART AND AVIONIC TEST STATION CONSTRAINTS

Table E-I. Spare Part Constraints

Work Unit Code	Constrained Quantity	Work Unit Code	Constrained Quantity
13CA0	11	52AB0	7
14AA0	8	52AC0	14
14AB0	1	52AL0	8
23000	37	52AM0	10
24AA0	14	55AC0	3
24B00	31	55AD0	4
51AD0	16	55BC0	5
51AE0	23	55BE0	3
51AF0	11	55CA0	6
51AG0	14	55CBG	33
51AH0	14	57AA0	6
51AK0	18	63AG0	11
51AL0	14	63BC0	14
51AM0	9	63BD0	8
51EA0	4	63BF0	8
51ED0	9	63BH0	7
51NA0	6	65AA0	8
51NB0	10	65BH0	8
52AA0	7	71AE0	14

AD-A156 540      ESTIMATION OF F-15 PEACETIME MAINTENANCE MANPOWER  
                  REQUIREMENTS USING THE (U) AIR FORCE INST OF TECH  
                  WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI.  
UNCLASSIFIED      G DEGOVANNI ET AL DEC 76 AFIT/GOR/SM/76D-5 F/G 5/9      313  
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MICROCOPY RESOLUTION TEST CHART  
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Table E-I. Spare Part Constraints (Continued)

Work Unit Code	Constrained Quantity	Work Unit Code	Constrained Quantity
71AK0	20	74FK0	16
71BDO	6	74FQ0	12
71CA0	7	74FS0	13
71FA0	9	74FU0	11
71FB0	10	74JA0	12
71FC0	11	74JC0	11
71FE0	9	74KA0	7
74EBO	12	74KC0	8
74FA0	14	74KE0	7
74FC0	16	75BB0	5
74FF0	14	75HE0	7
74FH0	16	75MA0	7
74FJ0	14	75MC0	5

Table E-II  
Avionic Test Station Constraints

Avionic Test Station	Job Description	Constrained Quality
TSC	Analog/Digital Computer Test Station	2
TSD	Analog/Visual Computer Test Station	2
TSM	Microwave Frequency Test Station	2

VITA

George DeGovanni was born on 4 January 1947 in Philadelphia, Pennsylvania. He graduated from the United States Air Force Academy in June 1968 with a Bachelor of Science in Mathematics. He completed Undergraduate Pilot Training at Moody AFB, Georgia in August 1969. He then flew combat missions in Vietnam as an OV-10 Forward Air Controller attached to the 20th Tactical Air Support Squadron until April 1971. Upon return to the United States, DeGovanni was assigned to the 14th Pilot Training Wing, Columbus Air Force Base, Mississippi, as a T-38 Instructor Pilot/Flight Examiner. In May 1975, he entered the Air Force Institute of Technology.

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## VITA

Donald Michael Douglas was born on 23 January, 1943 in Mt. Carmel, Illinois. After graduating from high school there in 1961, he attended the United States Air Force Academy from which he received the degree of Bachelor of Basic Science and a commission in the United States Air Force in 1965. He completed pilot training in September, 1966 and served as a KC-135 pilot with the 301st Air Refueling Wing, Lockbourne Air Force Base, Ohio. After completing rotary wing conversion training in May, 1969, he served with the 809th Combat Support Group, F. E. Warren Air Force Base, Wyoming as a UH-1F pilot. During 1970 and 1971 he flew as a UH-1P and UH-1N gunship flight examiner with the 20th Special Operations Squadron, RVN. He then served as an instructor pilot and Wing Chief of UH-1N Standardization in the 1550th AircREW Training and Test Wing, Hill Air Force Base, Utah until entering the School of Engineering, Air Force Institute of Technology, in May 1975.

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