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DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION, CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02154

REPLY TO ATTENTION OF: NEDED

FEB 1 1 1900

Honorable Hugh J. Gallen Governor of the State of New Hampshire State House Concord, New Hampshire 03301

Dear Governor Gallen:

Inclosed is a copy of the Walker Oliverian Stream Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Water Resources Board, the cooperating agency for the State of New Hampshire. In addition, a copy of the report has also been furnished the owner, Mr. Robert V. Walker, Pike, New Hampshire.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for your cooperation in carrying out this program.

Sincerely,

Incl As stated MAX B. SCHEIDER Colonel, Corps of Engineers Division Engineer

NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.: Name of Dam: Town: County and State: Stream: Date of Inspection:

NH00068 Walker Oliverian Stream Dam Haverhill Grafton County, New Hampshire Oliverian Brook May 8, 1979

BRIEF ASSESSMENT

Walker Oliverian Stream Dam has a hydraulic height of 19 feet, is of varied topwidth, and is 74 feet long. It is a run-of-the-river, split stone and masonry, gravity dam with one inoperable gate and a vertical-drop spillway. The dam spans a reach of Oliverian Brook, and is located in northwestern New Hampshire. Maximum storage capacity is about 20 acre-feet. Walker Oliverian Stream Dam was used for small hydroelectric power generation but now acts only as a stream barrier. The pond ranges from 1700 to 2000 feet in length with a surface area of about 4 acres.

The dam is in poor condition. Of concern is: (1) the stability of the dam under flood conditions with substantial overtopping, and (2) the seepage that is evident over much of the downstream face of the dam.

Based on small size and significant hazard classifications in accordance with Corps guidelines, the test flood is ½ Probable Maximum Flood (PMF). A test flood outflow of 15,150 cfs (500 csm) would overtop the dam by about 10.5 feet (12.5 feet over spillway crest). The spillway will pass 695 cfs or about 5 percent of the test flood. A major breach at top of dam could result in the loss of 1 or 2 lives and appreciable property damage.

The owner, Robert V. Walker, should implement the results of the recommendations and remedial measures given in Sections 7.2 and 7.3 within one year after receipt of this Phase I Inspection Report.

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Warren A. Guinan Project Manager

N.H. P.E. 2339

This Phase I Inspection Report on Walker Oliverian Stream Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the <u>Recommended Guidelines for Safety Inspection of</u> <u>Dans</u>, and with good engineering judgement and practice, and is hereby submitted for approval.

OSEPH W. FEINEGAN, JR., D.DER Wager Control Branch Ingineering Division

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JOSEPH A. MCELROY, MEMBER Foundation & Materials Branch . Engineering Division

Corney 4. Fazian

CARNEY M. "IERZIAN, CHAIRMAN Chief, Structural Section Design Branch Engineering Division

APPROVAL RECONDENDED:

ME B. FR

Chief, Engineering Division

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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 June 1979 Figure 1 - Overview of Walker Oliverian Stream Dam.



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT WALKER OLIVERIAN STREAM DAM

SECTION 1 PROJECT INFORMATION

1.1 General

a. <u>Authority</u>. Public Law 92-367, August 8, 1972 authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Anderson-Nichols & Company, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed were issued to Anderson-Nichols under a letter of March 22, 1979 from John P. Chandler, Colonel, Corps of Engineers. Contract No. DACW33-79-C-0050 has been assigned by the Corps of Engineers for this work.

b. Purpose

(1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.

(2) To encourage and prepare the States to initiate quickly effective dam safety programs for non-Federal dams.

(3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location. Walker Oliverian Stream Dam, also known as Norton Pike Dam, is located in Pike, New Hampshire and is a run-ofthe-river dam spanning Oliverian Brook. After discharging over the dam, Oliverian Brook flows westerly for a distance of 4 miles to its confluence with the Connecticut River. Walker Oliverian Stream Dam is shown on U.S.G.S. Quadrangle, Newbury, N.H. - Vt. with coordinates approximately at N 44^o Ol' 54", W 72^o 00' 31", Grafton County, New Hampshire. (See Location Map page vii.)

b. Description of Dam and Appurtenances. Walker Oliverian Stream Dam is a split-stone, gravity dam on ledge about 74 feet in length and about 19 feet in height. A small gatehouse (8' x 10' x 8') is located atop the northerly abutment. An opening $(3.5'H \times 7'W)$ is located directly below the gatehouse. A gate is located below this but its dimensions could not be determined. The northerly abutment consists of a split stone wall and a concrete gatehouse footing. The split stone wall also acts as a containing wall for the dirt road located just north of the north abutment. The north side of the 20' wide road consists of natural, wooded land sloping upward. The southerly abutment is a concrete extension of the foundation of a mill building which no longer exists.

c. <u>Size Classification</u>. Small (hydraulic height - 19 feet; storage - 20 acre-feet) based on height and storage requirements of < 40 feet and \geq 50 but < 1000 acre-feet, respectively, as given in Recommended Guidelines for Safety Inspection of Dams.

d. <u>Hazard Classification</u>. Significant Hazard. A major breach would probably result in the loss of 1 or 2 lives and appreciable property damage. (See Section 5.1 f.)

e. <u>Ownership</u>. The Walker Oliverian Stream Dam was originally owned by the Norton Pike Company. Ownership was transferred to the Moosilauke Lumber and Bobbin Company sometime during the 1930's. Ownership remained unchanged until about eight years ago when Mr. Robert V. Walker, the current owner, bought the property.

f. Operator. The current owner and operator of the Walker Oliverian Stream Dam is Robert V. Walker, Back Bay Road, Pike, New Hampshire 03780. Phone: 603/989-5670.

g. <u>Purpose of Dam</u>. The dam was constructed to facilitate hydroelectric power generation. The power plant is no longer functional and only the ruins of the power plant and mill building remain.

h. Design and Construction History. No information was disclosed regarding the design and construction of the dam. The dam appears to have been built in the mid or late 1800's.

i. <u>Normal Operational Procedures</u>. No written operational procedures were disclosed for the dam.

1.3 Pertinent Data

a. Drainage Area. The drainage area consists of 30.3 square miles (19,392 acres) of rolling and mountainous, mostly forested terrain. Numerous storage areas are present in the upstream drainage basin.

b. Discharge at Damsite

(1) Outlet works - One "gate opening" at the northerly end of the spillway invert elevation 736.5' MSL. The gate itself is no longer operational and its dimensions are unknown. One penstock opening 4'x4' @ invert elevation 723.0' MSL; silt and debris block all flow through the penstock opening.

(2) The maximum discharge at the damsite is unknown.

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(3) Ungated spillway capacity @ top of dam - 695 cfs @ 740.0' MSL

(4) Ungated spillway capacity @ test flood elevation -8,340 cfs @ 750.5' MSL

(5) Gated spillway capacity @ top of dam elevation - not applicable

(6) Gated spillway capacity @ test flood elevation - not applicable

(7) Total spillway capacity @ test flood elevation -8,340 cfs @ 750.5' MSL

(8) Total project discharge @ test flood elevation -15,150 cfs @ 750.5' MSL

c. Elevation (ft. above MSL based on USGS Quadrangle)

toe)

- (1) Streambed at centerline of dam 721.3 (at downstream
 - (2) Maximum tailwater unknown
 - (3) Opening invert (under north gatehouse) 736.5
 - (4) Main spillway crest 738.0
 - (5) South spillway crest 737.5
 - (6) Top of dam 740.0
 - (7) Test flood pool 750.5

d. Reservoir (feet)

- (1) Length of maximum pool 2000
- (2) Length of pool at spillway crest 1700
- (3) Length of flood control pool not applicable
- e. Storage (acre-feet)
 - (1) Recreation pool not applicable
 - (2) Flood control pool not applicable
 - (3) Spillway crest pool 16 (approximate)
 - (4) Top of dam pool 20 (approximate)
 - (5) Test flood pool 40 (approximate)

f. Reservoir Surface (acres) (1)Recreation pool - not applicable (2) Flood control pool - not applicable (3) Spillway crest pool - 4 (approximate) (4) Top of dam pool - 5 (approximate) Test flood pool - 10 (approximate) (5) g. Dam (1)Type - split stone and masonry, gravity dam with a broad, flat spillway crest creating a nearly vertical overflow. (2) Length - 74' (3) Height - 19' (structural height) Top width - varied (4) (5) Side Slopes - Upstream: unknown Downstream: vertical face (6) Zoning - unknown Impervious core - unknown (7) (8) Cut-off - unknown (9) Grout curtain - unknown Diversion and Regulating Tunnel - not applicable h. Spillway i. Type - split stone, flat, broad-crested with vertical (1) downstream face. (2) Length of weir - 62'; the southern 9 feet of the spillway is a weir with a crest elevation 0.5 feet lower (737.5' MSL) than that of the main spillway. This portion of the spillway was once part of a mill building foundation. (3) Crest elevation - 738.0' MSL (4) Gates - none (5) U/S Channel - The approach channel to the spillway

(5) U/S Channel - The approach channel to the spillway consists of Oliverian Brook which ranges in width from 75 feet to 125 feet. The banks are lined with brush and some small trees. Silt has accumulated to within approximately 2 feet of the spillway crest.

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(6) D/S Channel - The channel immediately downstream of the dam is approximately 50 feet wide. There are some small trees growing in the middle of the channel immediately downstream of the dam. The channel consists of a vertical, 8' high, cut stone wall on the south side and nearly vertical ledge on the north side extending approximately 300 feet downstream. Channel overbanks are covered with grass and some small trees. Some mill building ruins remain on the south overbank immediately downstream of the dam. Oliverian Brook passes through a concrete, vertical-walled bridge opening under N.H. Route 25 approximately 400 feet downstream of the dam. A developed area located about 4000 feet downstream of the dam on the relatively flat southwestern overbank consists of two mobile homes.

j. <u>Regulating Outlets</u>. A 3.5'H x 7' W opening is located near the north abutment immediately below the gatehouse. The opening invert is at elevation 736.5' MSL; the gate itself is inoperable and its dimensions are unknown.

A penstock opening is located near the south abutment with an invert elevation of 723.0' MSL. The opening has been blocked by debris. The penstock itself is deteriorated and inoperable.

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SECTION 2 ENGINEERING DATA

2.1 Design

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No data were disclosed regarding the design of Walker Oliverian Stream Dam.

2.2 Construction

No data were disclosed regarding the construction of the dam.

2.3 Operation

No operational data were disclosed.

2.4 Evaluation

a. <u>Availability</u>. No engineering data were available for evaluation of Walker Oliverian Stream Dam.

SECTION 3 VISUAL INSPECTION

3.1 Findings

a. <u>General</u>. Walker Oliverian Stream Dam is a low dam which impounds a reservoir of small size. The drainage area above the dam is rolling, mountainous, and heavily wooded. The downstream area is rolling and partially wooded.

Dam. Walker Oliverian Stream Dam is a run-of-theb. river split stone, gravity dam on ledge. (See Appendix C -Figure 2.) The dam has a hydraulic height of 19 feet and totals 74 feet in length. The north abutment consists of a split stone wall and a concrete gatehouse footing. A small gatehouse is located atop the north abutment. (See Appendix C -Figure 3.) The operating mechanism inside appears to have been inactive for many years. An opening 3.5'H X 7'W is located directly below the gatehouse. (See Appendix C - Figure 4.) The dirt road bed is inadequately supported just downstream of the north (See Appendix C - Figure 5.) The spillway crest is abutment. 62 feet in length and its crest is about 17 feet above the downstream toe. (See Appendix C - Figure 6.) The southern end of the crest has been damaged and allows a small amount of outflow below normal crest elevation. (See Appendix C - Figure 7.) It could not be determined if flow over the center portion of the crest was a result of construction or settling of the masonry structure at this point. (See Appendix C - Figure 2.) The southerly abutment is a concrete extension of the foundation of the mill building which no longer exists. (See Appendix C -Figure 7.) The remains of the old penstock, which formerly was located in the mill building, is located about 12 feet left of the southern abutment. (See Appendix C - Figure 8.)

c. Appurtenant Structures. A wooden gatehouse structure is located on the dam near the north abutment and is in poor condition. (See Appendix C - Figure 9.) A badly rusted wheel and gear mechanism in the gatehouse operated a wooden slide gate also in a deteriorated condition. (See Appendix C - Figure 10.) The entire mechanism appears to have been inoperable for quite some time. The cut-stone masonry gate opening and spillway showed evidence of leaking at the joints and those directly underneath the gatehouse seemed to have moved laterally, thereby giving a loose, open-joint appearance. (See Appendix C -Figure 11.) The south spillway appears to have once supported a wooden water-wheel and pit, which have since collapsed into the tailwater pool. (See Appendix C - Figure 8.)

d. Reservoir Area. The approach channel to the spillway consists of Oliverian Brook which ranges in width from 75 feet to 125 feet. The banks are lined with brush and some small trees. (See Appendix C - Figure 12.) Silt has accumulated to within approximately 2 feet of the spillway crest.

Downstream Channel. The channel immediately downstream e. of the dam is approximately 50 feet wide. There are some small trees growing in the middle of the channel immediately downstream of the dam. The channel consists of a vertical, 8' high, cutstone wall on the south side and nearly vertical ledge on the north side extending approximately 300 feet downstream. Channel overbanks are covered with grass and some small trees. Some mill building ruins remain on the south overbank immediately downstream of the dam. Oliverian Brook passes through a concrete, vertical-walled bridge opening under N.H. Route 25 approximately 400 feet downstream of the dam. (See Appendix C - Figure 13.) A developed area located about 4000 feet downstream of the dam on the relatively flat southwestern overbank consists of two mobile homes.

3.2 Evaluation

Based on visual inspection, the Walker Oliverian Stream Dam is in poor condition.

Seepage through the masonry joints over the entire face of the dam poses a stability problem and should be monitored.

The deteriorated condition of the gatehouse structure, gate operating mechanism, and especially the gate is of increasing concern and could potentially cause the dam to breach at this location.

It could not be determined at the time of the inspection if flow below the normal crest elevation of the dam was a result of construction or caused by settlement of the masonry structure. (See Appendix C - Figure 2.)

Trees growing on both abutments and undermining of the gravel road on the north abutment immediately downstream of the dam do not appear to pose any immediate threat to the stability of the dam.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures

No written operational procedures were disclosed for Walker Oliverian Stream Dam. This small dam has served only as a stream barrier for many years.

4.2 Maintenance of Dam

Robert V. Walker is responsible for maintenance of Walker Oliverian Stream Dam.

4.3 Maintenance of Operating Facilities

It appears that little maintenance has been performed on the dam and appurtenances for many years.

4.4 Description of Any Warning System in Effect

No written warning system was disclosed for Walker Oliverian Stream Dam.

4.5 Evaluation

The current operational procedures were evaluated as poor. This evaluation is due to the observed condition of the dam and the fact that no written procedures were disclosed.



SECTION 5 HYDROLOGIC/HYDRAULIC

5.1 Evaluation of Features

a. <u>General</u>. Walker Oliverian Stream Dam is a low, run-ofthe-river, split stone and mortar, gravity dam that impounds a reservoir of small size. The total length of the dam is 74 feet, 62 feet of which consists of the main, vertical-drop spillway. The top of dam is 2 feet above the spillway crest. Because the dam is of split stone and masonry in poor condition, large overtopping would likely result in a breach.

b. Design Data. No hydrologic design data were found.

c. Experience Data. No data were disclosed concerning flood heights, flood damage, or discharges at the dam.

d. <u>Visual Observations</u>. The main spillway is still intact but seepage is evident in several places on the downstream face.

e. <u>Test Flood Analysis</u>. Walker Oliverian Stream Dam is classified as small, having a hydraulic height of 19 feet and a maximum storage capacity of 20 acre-feet. This small reservoir contains runoff from a 30.3 square mile drainage area, characterized by rolling and mountainous, mostly forested terrain. Due to large upstream storage reservoir a csm value was obtained between the "Rolling" and "Flat and Coastal" curves. Using a csm value of 1,000, a Probable Maximum Flood (PMF) of 30,300 cfs was obtained. The Recommended Guidelines for Safety Inspection of Dams dictated use of ½ the PMF.

Using $\frac{1}{2}$ PMF, the test flood discharge was determined to be 15,150 cfs. The overtopping analysis indicates that the dam would be overtopped by 10.5 feet during the test flood. The maximum spillway capacity at top of dam is 695 cfs, which is only 5% of the test flood discharge.

f. Dam Failure Analysis. The impact of failure of the dam at top of dam was assessed using the Guidance for Estimating Downstream Dam Failure Hydrographs issued by the Corps of Engineers. The analysis covered the reach extending from the dam to a developed area consisting of two mobile homes on the south bank of Oliverian Brook approximately 4,000 feet downstream. A breach at top of dam would increase the stage 3.2 feet above the already high flood water surface elevation, damaging the trailers downstream. The potential for loss of life is minimal (estimated to be 1 or 2 lives). Therefore, Walker Oliverian Stream Dam was classified Significant Hazard.

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SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. <u>Visual Observations</u>. The downstream face of the dam seems to have maintained a nearly vertical alignment. There appears to be minor seepage over the entire downstream face of the dam through the masonry joints. It could not be determined if flow over the center portion of the high water crest indicates settling of the masonry dam structure or is a result of construction. The visual examination indicates the following evidence of potential problems:

(1) Seepage through the cut masonry joints

(2) Possible movement of the south abutment

(3) Undermining of the gravel road on the north abutment immediately downstream of the dam

(4) Deterioration of the gatehouse structure and gate

(5) Trees growing on both abutments

In addition, the crumbling condition of the old mill structures on the south abutment, trees and stone rubble in the tailwater pool and the collapsed wooden water wheel pit near the south abutment.

b. <u>Design and Construction Data</u>. No design and construction data were disclosed.

c. Operating Records. No operating records pertinent to the structural stability of the dam were disclosed.

d. <u>Post-Construction Changes</u>. No record of post-construction changes were found.

e. <u>Seismic Stability</u>. This dam is located in Seismic Zone 2 and in accordance with the Phase I guidelines does not warrant seismic analysis.

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SECTION 7

ASSESSMENT, RECOMMENDATIONS, AND REMEDIAL MEASURES

7.1 Dam Assessment

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a. <u>Condition</u>. The visual inspection indicates that the Walker Oliverian Stream Dam is in poor condition. The major problems which, if not corrected, could lead to structural instability are:

(1) Seepage through the cut masonry joints

(2) Possible movement of the south abutment

(3) Undermining of the gravel road on the north abutment immediately downstream of the dam

(4) Deterioration of the gatehouse structure and gate.

(5) Trees growing on both abutments.

The crumbling condition of the old mill structures on the south abutment, trees and stone rubble in the tailwater pool, and the collapsed wooden water wheel pit near the south abutment are further indications of the poor condition of this dam.

b. Adequacy of Information. The information available is such that the assessment of the condition of the dam must be based primarily on the visual inspection. The visual inspection is adequate to identify problems noted in 7.1a. above and to assess the general condition of the dam.

c. <u>Urgency</u>. The recommendation in 7.2 below and remedial measures recommended in 7.3 below should be implemented by the owner within one year after receipt of this Phase I report.

d. <u>Need for Additional Information</u>. The information obtained and the visual inspection are adequate for purposes of this evaluation.

7.2. Recommendations

The owner should engage a Registered Professional Engineer to design remedial measures for elimination of the seepage along the downstream face of the dam and restore the regulating gate and gatehouse to an operable condition. 7.3 Remedial Measures

a. Operating and Maintenance Procedures

(1) Seepage through the masonry joints on the downstream face of the dam should be monitored on a monthly basis.

(2) Movements of the south abutment should be monitored on a monthly basis.

(3) Erosion underneath the cantilevered portion of the gravel roadway on the north abutment should be repaired and checked for future erosion.

(4) The north and south abutments including portions immediately downstream, the tailwater pool should be cleared and maintained free of brush, trees and rubble.

(5) Establish a surveillance program for use during and immediately following periods of heavy rainfall and also a warning program to follow in case of emergency conditions.

(6) Have the dam inspected by a Registered Professional Engineer once every year.

7.4 Alternatives

If the owner should determine that the expense of the repairs and upkeep are too great, recommend that the dam be removed under the direction of a Registered Professional Engineer.

APPENDIX A

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION PARTY ORGANIS	CHECKLIST ZATION	
PROJECT <u>Walker Oliverian Stream</u> Dam	DATE <u>May 8, 1979</u> TIME <u>11:30 AM</u> WEATHER <u>Clear, warm</u> W.S. ELEV. U.S. DN.S. <u>738</u> 722	
Warren Guinan 6 2. Stephen Gilman 7.	Pattu Kesavan Ronald Hirschfeld	
Robert Ojendyk 8 John Regan 9 Gerry Blanchette		
PROJECT FEATURE	INSPECTED BY REMARKS W. Guinan/J. Regan	
<u>Structural Stability</u> <u>Soils and Geology</u>	S, Gilman R. Hirschfeld	
)		
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A-1		

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PERIODIC INSP	PECTION CHECKLIST	• 1. 1.
PROJECT Walker Oliverian Stream	Dam DATE May 8, 1979	
PROJECT FEATURE Approach_Chann	nel NAME	
DISCIPLINE	NAME	
AREA EVALUATED	CONDITION	•
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE		
a. Approach Channel		
Slope Conditions	Good	
Bottom Conditions	Not visible beneath water surface	
Rock Slides or Falls	None	-
Log Boom	Not visible	
Debris	None	
Condition of Concrete Lining	Not applicable	
Drains or Weep Holes	None	
b. Intake Structure		
Condition of Concrete		
Stop Logs and Slots	Not applicable	
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PROJECT Walker Oliverian Stream	Dam DATE May 8, 1979
PROJECT PRAMURE Gatebouse & Mech	
PROJECT FEATURE <u>Outchouse</u> a ricen	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - CONTROL TOWER	Wooden gatehouse
a. Concrete and Structural	
General Condition	poor; deteriorated
Condition of Joints	
Spalling	
Visible Reinforcing	
Rusting or Staining of Concrete	
Any Seepage or Efflorescen	Ce
Joint Alignment	
Unusual Seepage or Leaks in Gate Chamber	n Not visible
Cracks	
Rusting or Corrosion of Steel	
b. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	
Hydraulic System	Nachanical sate on north side
Service Gates	of dam not operable; gate sub-
Emergency Gates	merged. Wheel and gear mechanism is badly rusted.
Emorgency Dover System	
Wiring and Lighting Suprem	
arting and Digiting System	
 	A- 3

PERIODIC INSPE	ECTION CHECKLIST	
PROJECT Walker Oliverian Stream	Dam DATE May 8, 1979	-
PROJECT FEATURE Outlet Channel	NAME	
DISCIPLINE	NAME	
AREA EVALUATED	CONDITION	
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL		
General Condition of Concrete		
Rust or Staining		••••
Spalling		
Erosion or Cavitation		
Visible Reinforcing		
Any Seepage or Efflorescence	Leaking at joints	
Condition at Joints	Leaking at joints; masonry appears	an Para
Drain holes	to have moved laterally. None	•••
Channel		
Loose Rock or Trees Overhanging Channel	Many trees overhanging channel	
Condition of Discharge Channel	Fair; rocky with some trees growing in channel just below dam.	
		68 1
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PERIODIC INSPE	CTION CHECKLIST	
PROJECT Walker Oliverian Stream	DATE May 8, 1979	
PROJECT FEATURE Spillway	NAME	
DISCIPLINE	NAME	•
AREA EVALUATED	CONDITION	
OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS		
a. Approach Channel		
General Condition	Good	ē
Loose Rock Overhanging Channel	None	
Trees Overhanging Channel	Some, but channel is moderately	
Floor of Approach Channel	wide Not visible beneath water surface	
b. Weir and Training Walls		
General Condition of Concrete		
Rust or Staining		■ The Theorem
Spalling		
Any Visible Reinforcing		
Any Seepage or Efflorescence		Ave
Drain Holes	None	
c. Discharge Channel		
General Condition	Fair	
Loose Rock Overhanging Channel	Dry stone masonry retaining walls	Y
Trees Overhanging Channel	support road fill on north side of channel	
Floor of Channel	Many trees overhanging channel Bedrock	
Other Obstructions	None	
		•

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PROJECT Walker Oliverian	Stream Dam DATE May 8, 1979
PROJECT FEATURE Reservoi	r NAME
AREA EVALUATED	REMARKS
Stability of Shoreline	Fair
Sedimentation	Some
Changes in Watershed Runoff Potential	None
Upstream Hazards	None
Downstream Hazards	N.H. Route 25 bridge, several homes about 1 mile downstream
Alert Facilities	None
Hydrometeorological Gages	None
Operational & Maintenance Regulations	None
,	

۰. <u>.</u> • APPENDIX B

ENGINEERING DATA

N. H. WALLR RESCURCES BOARD Concord, N. H. 03301	•••
DAM SAFERY INSPECTION FEFORT FORM	
Dam Number: 112.02.	• •
Inspected by: <u>SCB</u> Date: <u>24 July 1974</u>	
.ocal name of dam or water body:	
Waer: Address:	• •
Wher was/was not interviewed during inspection. Unainage Area: <u>317dal 20.4000</u> sq. mi. Stream: <u>010000000</u>	
Fond Area:Acre, StorageAc-Ft. Nex. Head 15 Ft.	• •
Foundation: Type, Seepage present at toe - Yes No,	
Spillway: Type Over Elaw, Freeboard over perm. crest: 3.	
Wiath 40't, Flashboard height Nono,	
Max. Capacityc.f.s.	
Embankmeat: Type, CoverWidth,	
Upstream slope to 1; Downstream slopeto 1	
abutments: Type Court Stone, Condition: Good, Fair, Poor	
Jates or Pond Drain: Size <u>6×7</u> Capacity Type <u>Cate</u>	
Lifting apparatusOperational condition ? No	
Changes since construction or last inspection:	
Downstreem development: V 400' To NH# 2.5	
This dam would would not be a menace if it failed.	•
Suggested reinspection date:	
Remarks:	
	• •
n 1	
B-1	
	• • •

NEW HAMPSHIRE WATER RESOURCES BOARD

QUESTIONNAIRE

WATER POWER DEVELOPMENTS IN NEW HAMPSHIRE

Monsilande the of Bottin Co WRA N. H.

Gentlemen:

We maintain in this office a list of the water power installations in New Hampshire and are frequently receiving inquiries concerning these installations. We are, therefore, bringing this information up to date, and request your cooperation by filling in the questionnaire below with data on your development and return it to us in the enclosed stamped envelope.

If the ownership has changed, will you please forward this questionnaire to the present owners.

Very truly yours.

cting Chairman

Brook Location Howhiel Dam No. //202 River et Olinn

1. Will you please check or correct:

Your Our Data Corrections 16 Head - feet Capacity Wheel - H.P. Generator - K.W. 2. Is the power plant in operation? يتها لآي 3. If not, is the equipment in operable condition? 4. Is the dam in good repair? ____ * 1000 \sim Signed: B-2



Oliverian Stream Haverhill, N. H.

May 21, 1946

This dam was inspected on above date. Hr. Eichhorn, manager of the Moosilauke Lumber and Bobbin Company was contacted. He stated that repairs were made in 1942 which consisted of <u>concretion</u> the south and of the dam. This section was weakened during the 1936 Flood. The only part of the dam that appeared to be in poor repair at the time of the inspection was the gate section. The gate is inoperable and the masonry around the gate structure shows signs of disintegration, probably due somewhat to frost action as well as high water. This was called to Mr. Eichhorn's attention and he stated that he would attempt to get it remained in the next few years.

The dam is not being operated for power, all of the penstock and associated structures were destroyed by fire. The only being made of the present pond is as a source of ice and, Mr. Bichhorn stated, the ice company contributed to the regain of the dam.

Locnard R. Frost Engineer

B-3
Form E80

NEW HAMPSHIRE WATER RESOURCES BOARD

QUESTIONNAIRE

WATER POWERS OF NEW HAMPSHIRE

THEFE & DOBRIN Morton Pike

New Hampshire

Gentlemen:

We maintain in this office a list of the water power installations in New Hampshire. In recent months we have had several inquiries concerning the water power installations in the State and have found that our information is in some cases out of data.

We are, therefore, bringing this information up to date and request your cooperation by filling in the questionnaire below with data on your development, and return it to us in the enclosed stamped envelope.

Very truly yours,

Lingtin

RECEIVED

FINE

JUL 131942 NORTON PIKE CO.

RSH: GMB Encl.

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Richard S. Holmgren Chief Engineer

Dam No. Location: Oliverian Streamiver at Haverhill 112.02

1. Will you please check or correct:

		Our Data	Your Corrections]	
	Drainage Area - Sq.Mi. Head - feet Capacity Wheel - H.P. Generator - K.W.	31 (16)	B-ann		
2.	Is the power plant now	in operation	13 - 20		
3.	If not, is the equipment	t in operabl	e condition?	no	
4.	Is the dam in good repa	ir?	- tad	slapp	Lance Gistle
Dat C	. July 14/47	igned) B-4	E TANK	HER 3 33	MAN O

NEW HAMPSHIRE WATER CONTROL COMMISSION DATA ON DAMS IN NEW HAMPSHIRE

DATA ON DAM	MS IN NEW HAMPSHIRE	
LOCATION	STATE NO /112	02)
Town Haverhill /	· County Grafton	3
Stroom Oliverian Stroom		***********************
Desig Deine Copp B /	Decenden Oliverian Stream (
Basin-Primary		
Local Name 44° 001 \approx 11 600	- 72° 001 - 2 000	••••••
Coordinates—Lat44		•••••••
SENERAL DATA		
Drainage area: Controlled	: Uncontrolled	Sq. M1.
Overall length of dam	f Construction	
Height: Stream bed to highest elev	ft.: Max. Structure	fl.
Cost—Dam	Reservoir	•••••
DESCRIPTION Gravity- Split S	tone on Ledge 🗸	
Waste Gates		
Type	A. 1	••••••
Number: Size	it. high x	. ft. wide
Elevation Invert	: Total Area	sq. ft.
Hoist	•••••••••••••••••••••••••••••••••••••••	••••••
Waste Gates Conduit		
Number: Mat	erials	
Sizeft.: Length	ft.: Area	sq. ft.
Embankment		
Туре	•••••••••••••••••••••••••••••••••••••••	•••••
Height-Max	ft.: Min	ft.
TopWidth	: Elev.	ft.
Slopes—Upstream on		•••••
Length-Right of Spillway	: Left of Spillway	••••••••••••••••
Spillway		
Materials of Construction		
LengthTotal	ft.: Net	ft.
Height of permanent section-Max	ft.: Min	ft.
Flashboards-Type	: Height	ft.
Elevation-Permanent Crest	: Top of Flashboard	
Flood Capacity cf	s.:	
Abutments		
Materials:	•	
Freeboard: Max	ft.: Min	ft.
Headworks to Power Devel.—(See "Data	on Power Development")	
DWNER	Pike N H	
REMARKS Musilanie Lumbe		
Rob	bin to.	
	C- J	
	Г , Л	,
Tabulation By AAN&RLT	113 Date December 12, 1938. 7,	114/42
		•

NEW HAMPSHIRE WATER CONTROL COMMISSION

CATION					AT DAM NO.(1	12.02)
Cown	verhill		: Co	unty	Grafton	شده در و به ۲۰۰۰ ع م از مواد مرو ۲ موهد موجود مواد مواد مواد م
tream	Oliverian	Stream	******			******
Basin-Primary	<u> </u>	nn R	******	: Secondar	yOliverian S	tream
Local Name		· · · · · · · · · · · · · · · · · · ·	، ، ، که بردو بود. ۲۰۰۰ ۰۰ د د		•	الم من يعد إن مع من غير . الم يون الم
NERAL DAT				• • • • • • • • • • • • • • • • • • •		
Head-Max:	ft.	: M in	ft.: A v			
Date of Const	ruction		: Us	e of Power	2	لاير. در اير در ايروندي در در
Pondage			c. ft.: Stor	age		ac. ft.
SCRIPTION		(1) A transformed and the second sec second second sec				
Racks		an a				
Size of Rac	k Opening		a ay berta da angan 1996 - Anganan 1996 - Anganan			and the standard stands in the standard standard standard standard standard standard standard standard standard Standard standard stand Standard standard sta
Size of Bar			: Mat	erial		2
Area: Gross	1.1284.14 ⁴ 1.1	S State Contraction S	a.Ft.: Ne			en ft
Head Gates	sister. Zister.					
Type		· · · · · · · · · · · · · · · · · · ·			•••	
Numher	• • •	Size	ft high	· ····	•••••••••••••••••	
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Hoist				·····		
Penstock				•		· ·
Number		м	aterial		•	
Size			Length			
Turbines						
Number	2	•]	Makers	unknown	n (not used)	
Rating HP.	per unit		: То	tal Capacity	······	an a
Max. Deme	nt C.F.S. per	unit		: Tot	a)	efe
Drive	and the second s					······ ···· ··· ··· ··· ··· ··· ··· ··
Tyne				•	۲۰۰۰ کې د ۲۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰۰	
Consistent	••••••••••••••••••••••••••••••••••••••			•••••••••••••••••		
Number						
Male	····	******	••••••	**********	***************************************	***************************************
Dating 1/11		•			•••••••••••••••••••••••••••••••••••••••	
Raung KW.	, per unit	· · · · · · · · · · · · · · · · · · ·	······ , 10	har Capacity.	••••••••••••••	
EXC'IEF	•	n gan an a	· .		1 1	
Number	·····	: Маке . 	. .	•••	•	•••••
Kaung-per			Total Ca	pacity	•••••••••••	K. W.
JIPUT-KWI	HKS		•	10		
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NNER	Vorton Pil	e-0 0		Pik	e N H	

		Form EIA 484j	
			• •
PUBLIC SERVICE COMMISSION OF NEW TAX		T 5700	
TOWN	TOWN	STATE	
EAVERHILL.	NO. 2	NO. //2.07	• •
DRAINAGE	POND		
AREA 31 Sq. Mi.	AREA FOUNDATION		
MATERIALS OF	NATURE OF Ledge	······································	
PURPOSE POWER-CONSERVATION-DOMESTIC-RECE	REATION-TRANSPORTATION-PUBLIC	עדונודט	
HEIGHTS, TOP OF DAM TO BED OF STREAM 181	TOP OF DAM TO SPILLWAY CRESTS 31	· · · · · · · · · · · · · · · · · · ·	
SPILLWAYS, LENGTHS DEPTHS BELOW TOP OF DAM ADDITOX, 401	<u> </u>	LENGTH OF DAM 25' ADDrox.	
FLASHBOARDS TYPE, HEIGHT ABOVE CREST		7	• •
OPERATING HEAD CREST TO N. T. W. ADDEDX. 161	TOP OF FLASHBOARDS TO N. T. W.	6	
WHEELS, NUMBER KINDS & H. P. 2 Theels - not used			
GENERATORS, NUMBER KINDS & K. W.			
H. P. 90 P. C. TIME 100 P. C. EFF.	H. P. 75 P. C. TIME 100 P. C. EFF.	·	
REFERENCES, CASES, PLANS, INSPECTIONS			
REMARKS			
CONDITION: GOOD			. • •
MENACE: Yes. Will be subject to periodic	: inspection.		•
			•
	·:		
To the Public Service Com	mission:		
made July 17, 1336, according to notificatio for same is enclosed.	on to owner dated June 23	, 1386, and bill	
	D. Waldo White Chief Engineer		• •
August 6, 1936 Copy to Owner			
в-7			
			• •

NEW HAMPSHIRE WATER RESOURCES BOARD INVENDORY OF DAMS AND WATER POWER DEVELOPMENTS DAM BASIN Connecticut NO. 2 - - I-5302 RIVER Oliverian Stream MILES FROM MOUTH 4.05 D.A.SQ.MI. 31 TOWN Haverhill OWNER Norton Pike, NH. LONAL NAME OF DAM DESCRIPTION Gravity - Split Stone on Ledge BUILT POND CAPACILY ACRE FT. DRANDOWN FT. POND AREA-AGRES HEIGHT-TOP TO BED OF STREAM-FT. MAX. FLOOD HEIGHT ABOVE CREST-FT. OVERALL LENGTH OF DAM-FT 2. MAX.FLOOD HEIGHT ABOVE CREST-FT. PERMANENT CREST ELEV.U.S. G.S. LOJAL GAGE MAX. MIN. ELEV.U.S.G.S. LOCAL GAGE TAILWATER SPILLWAY LENGTHS -FT. 40+ FLASHBOARDS-TYPE, HEIGHT ABOVE CREST FREEBOARD-FT. Nono WASTE GATES-NO. WIDTH MAX. OPENING DEPTH SILL BELCW CREST REMARKS Condition Good ME ANTO COMMER FIRST & Mouth Olivarian Stream 247.85 mi from kooth Connecticut R. PCWER DEVELOPMENT RATED HEAD C.F.S. NO. HP FULL GATE KW MAKE UNITS FEET 2 100 USE Power REMARKS Mendes wheels not in 1150 B-8 7/17/34

7449	an tha that an				
TOWN NO.1,2	TownHaverh	ill , J. F	No <u>54</u>	. PAGE NO	
NAME OF COMPAN	v Pike Manuf	acturing	Company		
HOME ADDRESS	Pike, N. H.	•••••			
DRAINAGE AREA.	33. 50. м	I. HEAD	16 FT.		
RIVER Oliver	ian Brook	RATE SEC. FT	. PER SQ. MI. 90% TIM	= QQQ	•••••
		RESOURC	ES		
10 8 C	ENTRAL STATIONS		FOR ISOLATED I	NOUSTRIA'_ PLA	NTS
WHEEL CAP, H. P.	WHEEL CAP, H. P. PRIMARY H. P.		WHEEL CAP. H. P.	PRIMARY H.	P. 90% TIME
			100	33.5	<i>i</i> 9
		USES			
FOR CENTRA	AL STATIONS		FOR ISOLATED INDUS	RIAL PLANTS	· ·
K. V. A. CAPACITY	ANNUAL KW. H. OUTPUT	K. V. A. CAPA	CITY PROD. AND CONS	H. ANNU	AL KW. H.

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APPENDIX C

PHOTOGRAPHS









May 8, 1979

Figure 2 - Looking northeast at downstream face of dam. Note water trickling over crest at center of photo.

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May 8, 1979 Figure 3 - Looking northwest at upstream face of dam.



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Figure 4 - Looking upstream at gatehouse and opening. Note ledge on north bank at left.



Figure 5 - Looking northeast at dirt roadbed stability pinning.



May 8, 1979 Figure 6 - Looking north-south across spillway crest.



May 8, 1979 Figure 7 - Looking upstream at southerly half of spillway. C-4



May 8, 1979

Figure 8 - Closeup looking upstream at old penstock opening at left. Note deterioration of south abutment wall (right-center).



May 8, 1979

Figure 9 - Looking at the upstream face of the deteriorated wooden gatehouse.



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May 8, 1979 Figure 10 - View of the rusted wheel and gear mechanism in the gatehouse.



Figure 11 - Closeup looking upstream through gatehouse opening.



May 8, 1979 Figure 12 - Looking upstream into reservoir from north abutment.



May 8, 1979

Figure 13 - Looking at State Route 25 crossing located about 400 feet downstream of the dam.

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS



HUDROLOGY J HUDRAULIES 16 WALLER OLIVERIAN STREAM DAM AFSI 9Jun 79 D1: 30.3 mi Size Classification : Small Hazard Classification : - Dignificant Test Flord : 1/2 PMF Calculate PMF using "Preliminary Buidance for Estimating Maximum Protable Discharges in Phase I Dam Safety Investigations," March 1978. bpe of valley floor is = 24 ft/mi. Due to the existence of a large westheam storage area, a curve located appreximately 1/2-way between the "Flat and Coastal" and "Rolling" curves was used to letermine the CSM value for PMF. @ DA = 30.3 mi², a CSM value of 1000 was obtained. : PMF discharge = 20.3 mi² × 1000 CSM = 30,300 cfs = 30,300 cfs 1/2 PMF (Test Flood) = 15,150 cfs Develop a dam discharge rating curve using the wein cross-section shown on paye D-5. Assumptions *C = 3.0 (average value used for all wells) Top of both abutment @ Elev. 740.0 MSL Normal storage = 16 acre-feet DA = 30.3 mi² * King & Bruter Handbook was used to determine proper 'c' values. Use wein equation, Q=CLH#, to develop dam discharge nating curve... and Mitice equation Q=CAVZgh

. '				
Trial M	Jo. Water Suf Elevatin	are <u>Discharge(cf</u>	2/16 5)	
-	736.5	0		
2	737.5	$Q = 3(7) I^{3/2} = ZO$	معنی در مع	
	738.0	$Q = 3(7) 1.5^{3/2} + 3(9)0.5$	572 = 50	
4 Top	p dom 740.0	$Q = 3(7)3.5^{3/2} + 3(9)2.5^{3/2} = 695$	₹ ₂ + 5	i I ●
5	742.0	Q = (0.8)(24.5)(12(32.2)3)(9)(4.5)(24.5)(12(32.2)3)(9)(4.5)(2.5)(2.5)(2.5)(2.5)(2.5)(2.5)(2.5)(2	(15) + (15) +	
<u>6</u> Top	rood 743.0	$Q = (0.9)(24.5)(\sqrt{44 \times 4.75}) + 3(53)(5.0)^{\frac{1}{2}} + 3(10)3.$ 3(52)(5.0) ^{3/2} = 2	$73(9)5.5^{3/2}+$ $0^{3/2}+$ 7ZO	
	745.0	$Q = (0.8)(24.5)(44.4 \times 6.75)(4.4 \times 6.75)(4.75)(4.4 \times 6.75)(4.4 \times$)+ 7.0) $^{3/2}$ + 2.0) $^{3/2}$ +	
·····	· · · ·	$3(22(2.0))^{2} = 4,80^{2}$	15	
<u> </u>	748.0	$Q \cdot (0.8) (24.5) (444 \times 9.75)$ 3(9) (10.5) = + 3(53) (10) 3(10) (8.0) = + 3(15) (5.0)	+) ² +) ³ /2 +	
······································	· · · · .	$3(10)(5.0)^{1/2} + 3(10)(5)$ $3(20)(5.0)^{3/2} + 3(12)(7)$)*2+)*2=9,630	
		•• • • •	• • • • • • • • • • • • • • • • • • •	
· · · · ·		D-3		

3/16 Trial No Water Surface Distance (45) 9 Q = (0.3)(24.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(14.5)(15.5)(14.5)(15.5)(14.5)(15.5)(14.5)(15.5)(15.5)(14.5)(15.5)(752.0 $3(15)(9)^{1/2} + 3(\frac{1}{2}36)(9)^{1/2} + 3(\frac{1}{2}36)(9)^{1/2} + 3(12)(11)^{1/2} = 18,715$ Use the above trials to establish a discharge rating surve Test Flood = 15,150 cts Test Flood Elevation = 750.5' MSL Walker Oliverian Stream Dans would be over spillway about 10.5 feet (12.5 feet over spillway arest) during the test flood! Spillway capacity @ top of dance is 695 cts which is about 5 pucent of The test fissed discharge. D-4





6/16 DUWINSTREAM CHANNIEL KATING LURVE ARM 5Jun 79 Purpose: Check flow-carrying capacity of channel immediately downstriam of dam. Use cross section 200 ft. Jourstream of sam (see P.D-9). Develop a discharge rating curve using the Manning Equation : Q' = 1.49 ALZ's 542 where n = composite channel rougniess confficient A = area of section (++2) K= nyoraulic radius (Et) S= slope of reach length of reach = 400 \$ft. elevation @ 4/5 toc of dans = 721.3 invest elevation & thilge = 718.7 510pe = 0.006 composite n = 0.05 The trials below reject to the downstream channel CACSS Section shown on p. D-9. Trial No. Stage (ft) Discharge A = 2(50) = 100 ft WP= 50+4 = 54 ft R = A/WP = 100/54 = 1.85 H Q=1.49 (100)(1.55)2/3 (0.006) 1/2 = 350 cfs * Surveying data did not provide a staram invert elevation 200 ft. d/s of the dam. The staram invert at N.H. Koule 25 was used when calculating the slope l of the striam was at the subject cross section.

7/16 AFG Trial No. Stage (FH) Discharge **FJun**Pa 2 A=5(50)=250 H" 5 WP= 50+10= 60 ft R = A/WP = 250/60 = 4.17 H $\varphi = \frac{1.49}{0.05} (250) (4.17)^{4/3} (0.006)^{1/2}$ = 1500 cfs ろ B $A = B(50) = 100 \text{ ft}^2$ WP = 150+16 = 66 ft R= A/WP = 400/66=6.06 ft $Q = \frac{1.49}{0.05} (400)(6.06)^{2/3} (0.006)^{1/2}$ = 3070 cfs A = 10(50) + 1/2(2)(6) 4 10 $+ \frac{1}{2}(2)(4) = 510 + 2$ WP= 66 + 7/sin 18,4° + 1/sin 26.6° = 76.8 ft. R= A/WP= 510/76, B= 5.34 ft Q=1,49 (510) (5,34) 2/3 (0.106 /2 0.05 = 3600 cfs A = 12(50) + 1/2(4)(12)ち 12 $+ \frac{1}{2}(4)(8) = 640 \mu^{2}$ WP = 66 + 4/3in 18.4° + 4/sin 26.6° = 87.6 ft R= A/WP= 640/87.6=7.31 ft Q = 1.49 (640) (7.31) 43 (0.306) 1/2 0.05 = Fifico cfs D-8





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10/16

Rev. ad the 18 Jul 79

BREACH ANALUSIS

-Puspose: Determine sugree of sinkstream hazered. Assume: Ted elevation = 740.0 (rop of both doutments) Upstriam riverbed elevation = 726.0* due to silt build-up. $Q_{\mathbf{p}} = 9/27 \quad W_{\mathbf{b}} \sqrt{9} \cdot 10^{3/2} \quad where \quad iV_{\mathbf{b}} = breach \quad width \\ q = 32.2 \quad f4/sec^2 \\ q_{\mathbf{b}} = pool \; c/cv, - u/s \; nives bed \; c/cv,$ Wh= 0.4(74)=30ft; Yo= 740.0-726.0=14 ft. _ Qp, = \$\frac{1}{27}(30)(\frac{1}{32.2})(14)^{\frac{1}{2}} = 2,640 cfs Additional flow over dam during breach ... $Q = CLH^{3/2} = 3.0 (74-30)(2)^{3/2} = 373 cfs$ Total Encach q = 2,640 + 373 = 3013 cfs Antecedent Discharge (Qa) = flow over dam before breach R = 100 cfs (see rating curve on p. D-6)

* Sketch of my near section shows a high silt elevation. In the count of a breach, it is assumed that most of the silt would be washed downstream.

D-11

BREACH	ANALISI: (CONIT.	11/16 Rev. affi 18 Jul 79	
llee a ty adjaciant too fat naturg ca	pical choos suct to two (2) m seconstacam e crue using tué	for of the stream channel object houses located approximately fifte sam. Develop a discharge Manning Equation:	
$Q = 1.49 + \frac{49}{n} + \frac{1.49}{r_1} + \frac{1.49}{r_1}$	$4R^{42} 5^{12} = \frac{1.42}{5.72} (0.0)$ $being 1 + f(5) + 5$ $being 1 + f(5) + 5$	$\frac{2}{400} = \frac{721.3 - 640.0}{4000} = 0.02 \text{; } n=0.05$ $\frac{4000}{4000}$ $\frac{2}{12} = 4.21$ $\frac{2}{100000000000000000000000000000000000$	
Trial No.	-2/a.je (f+.)	Disconge	من م
/	2	$A = 2(20) = 40 H^{2}$ WH = 20 + 4 = 24 H R = A/100 = 40/24 = 1.7 H $R = 4.21(40)(17)^{73} = 240 c/s$	
2	Γ.	$\begin{array}{l} 4 & (1,2) + 3(1/2) = 105 \ ft^2 \\ (1+2) + 20 + 2 + 4.2 = 31.2 \ ft \\ 105 \ ft = 2.4 \ ft \\ 4.21 \ (105) \ ft = 4.4 \ ft \\ 4.21 \ (105) \ ft = 4.2 = 1000 \ ct \end{array}$	
Ř	7	$A = 7(2) + 5^{2}(12) + 2(100)(1/2) = 353 ft^{2}$ WP = 27 + 200 + 7.1 = 234.1 ft K = 957 (134.1 = 1.51 ft) $Q = 4.21(353)(1.1)^{43} = 1956 cfc$	
4	Ĵ	$\begin{array}{l} A=9(20)+7^{2}(12)+4^{2}(100)(12)=1005, 11^{2}\\ NP=27+000+9.9=436.9 \ 11\\ R=1006/436.9=2.3 \ 14\\ Q=4.21, 1005, 110, 13=7,372 \ cfs \end{array}$	
		D-12	

Rev. at STAT BREACH PALALYSIS (CONT) IBJUL 79 Discharge Trial No. Stave (ft) $A = 10, 5/20 + (8, 5)^{2}(1/2) + (5, 5)^{2}(100)(1/2)$ 10.5 ち = 1759 ft2 WP= 27 + 550 + 12 = 589 ft R = 1759/089 = 3.0 Q=4,21 (175,9)(3.0)2/3 - 15,403 - 15 $A = \frac{12(20)}{10^{2}(12)} + \frac{10^{2}(12)}{100}(1/2)$ 12 = 2740 1.12 WP= 27 + 700 + 14.1 = 741.1 ft R = 2740/741.1 = 3.7 ft $Q = 4.21(2740)(3.7)^{3/8} = 27,593 \text{ cfs}$ Breach at top of Juin - elevation 740.0 MEL

12/16

Total tincoch G = 3013 cfs (see p. D-11) Stage = 7.6 feet @ 3013 fs (see dis hazard nating curve) Anicedent discrimine = 700 cf (see f. D-11) Stage = 4.4 feet @ 700 cfs (see dis hazard nating curve) Therefore, stage increase at dis instand area will be: 7.6-4.4 = 3.2 feet





15/16 AFSM MANNEDIS OF BRIDGE OPENING (401 DIS OF DALL) 17 Jun 19 N.H. Rite. 25 Low chord el. 734.2 Lev. affit 18 Jul 79 Trivert el. 716.7 - - - - - - -----Bogulard: Discharge capacity of Lisidge opening (raximum The we creating backwater) des Manning Equation: G = 1.49 AK 2/3 51/2 where A = 15.5 (50) = 175 ft2 WP- ED+2(12.5) +81 H. R = A/WP = 775/81 = 4.6 ft. 5 = 0.02 , n= 0.03* $G = \frac{1.49}{2.03} (775) (9.6)^{2/3} (0.02)^{1/2} = 94,558 \text{ cfs}$ 10 10 >>> 2810 (Total Breach G), co of a bridge are negligible in the in a concl walls beneath bridge. D-16



CONMUSION - HARAKE ISTER ANT MA

Walker Oliverian Fineria Dam is a significant harand dam. Twe (2) mobile homis are located on the south ore bank close to Oliverian Barok about 4000 feet de motion of the dam. Approximable damage to these atoms in motion right of a bacach at top of dam accurred. Loss of one or two lives would be possible.


APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

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