

NATIONAL BUREAU OF STANDARDS MICROCOPY RESOLUTION TEST CHART

Z AD-A156 388

昌

MERRIMACK RIVER BASIN
BENNINGTON, NEW HAMPSHIRE

PAPER MILL DAM NH 00251

STATE NO 22.06

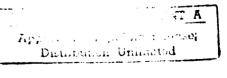
PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM





DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

FEBRUARY 1979



85 06 18 122

UNCLASSIFIED

REPORT DOCUMENTATION F		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NH 00251	AISUS	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subsisse) Paper Mill Dam		INSPECTION REPORT
NATIONAL PROGRAM FOR INSPECTION OF N	ON-FEDERAL	6. PERFORMING ORG. REPORT NUMBER
U.S. ARMY CORPS OF ENGINEERS NEW ENGLAND DIVISION		8. CONTRACT OR GRANT NUMBER(#)
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
DEPT. OF THE ARMY, CORPS OF ENGINEER	S	12. REPORT DATE February 1979
NEW ENGLAND DIVISION, NEDED 424 TRAPELO ROAD, WALTHAM, MA. 02254		13. NUMBER OF PAGES
14. MONITORING AGENCY NAME & ADDRESS(If different	from Controlling Office)	UNCLASSIFIED
		184. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) APPROVAL FOR PURLIC RELEASE. DISTRIB		

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different 'em Report)

18. SUPPLEMENTARY NOTES

Cover program reads: Phase I Inspection Report, National Dam Inspection Program; however, the official title of the program is: National Program for Inspection of Non-Federal Dams; use cover date for date of report.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

DAMS, INSPECTION, DAM SAFETY.

Merrimack River Basin Bennington, New Hampshire Contoocook River

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The dam has a hydraulic height of 13 ft. and is 280 ft. long. It is a run of the river concrete gravity dam with a spillway length of 142 ft. The dam is in fair condition with a few major concerns. It is small in size with a significant hazard classification. A major breach at top of dam would result in the loss of few, if any lives and appreciable property damage.

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.



DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION, CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02154

REPLY TO ATTENTION OF: NEDED

FEB 14 1200

Honorable Hugh J. Gallen Governor of the State of New Hampshire State House Concord, New Hampshire 03301

Dear Governor Gallen:

Inclosed is a copy of the Paper Mill Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Water Resources Board, the cooperating agency for the State of New Hampshire. In addition, a copy of the report has also been furnished the owner, Monadnock Paper Mills, Bennington, New Hampshire.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for your cooperation in carrying out this program.

Sincerely,

Incl As stated MAX B. SCHEIDER
Colonel. Corps of Engineer

Colonel, Corps of Engineers Division Engineer

> PTIC COPY

Allery, V

Unn. Jui t

NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.: NH00251

Name of Dam: Paper Mill Dam

Town: Bennington

County and State: Hillsborough County, New Hampshire

River: Contoocook River
Date of Inspection: November 20, 1978

BRIEF ASSESSMENT

Paper Mill Dam has a hydraulic height of 13 feet, is of varied topwidth, and totals 280 feet long. It is a run-of-the-river concrete gravity dam with a spillway length of 142 feet. The spillway has a 45° inclined downstream face. The head and waste gates are located in the north abutment. The dam spans a reach of the Contoocook River, and is located in south-central New Hampshire. Maximum storage capacity is about 50 acre-feet. Paper Mill Dam is used for industrial process water as well as for hydropower purposes. The pond is about 1140 feet in length with a surface area of about 5 acres.

The dam is in fair condition. Major concerns are: structural stability of the spillway under conditions of the test flood and the deteriorated concrete in the dam and gate structures.

Based on small size and significant hazard classifications in accordance with Corps guidelines, the test flood is 1/4 Probable Maximum Flood (PMF). A test flood outflow of 15,760 cfs (83 csm) would overtop the dam by about 5.2 feet (9.1 feet over spillway crest). The spillway will pass 3,830 cfs or about 24 percent of the test flood. A major breach at top of dam would result in the loss of few, if any lives and appreciable property damage.

The owner, Monadnock Paper Mills, should implement the results of the recommendations and remedial measures given in Sections 7.2 and 7.3 within one year after receipt of this Phase I inspection report.

Warren A. Guinan Project Manager N.H. P.E. 2339 This Phase I Inspection Report on Paper Mill Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgement and practice, and is hereby submitted for approval.

OSEPH W. FENEGAN, JR., MEMBER
Warer Control Branch
Engineering Division

CARNEY M. TERZIAN, MEMBER

Design Branch

Engineering Division

JOSEPH A. MCELROY, CHAIRMAN

Chief, NED Materials Testing Lab.

sert Q. Mr Elroy

Foundations & Materials Branch

Engineering Division

APPROVAL RECOMMENDED:

OE B. FRYAR

Chief, Engineering Division

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

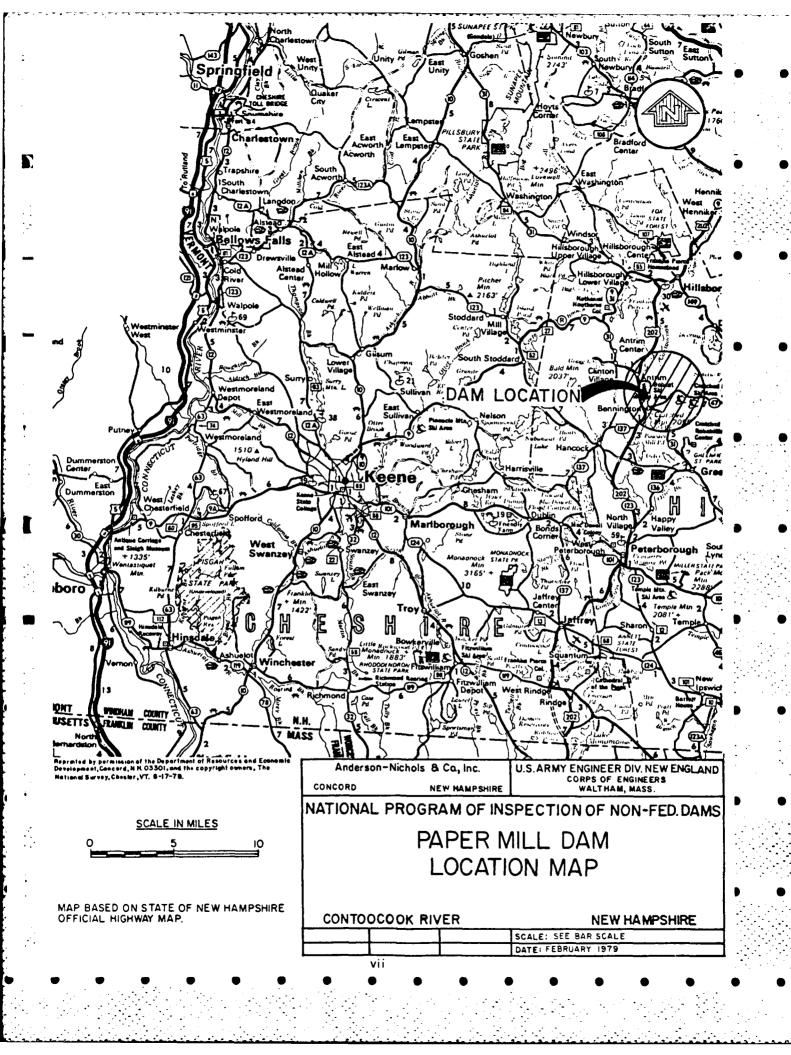
Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

TABLE OF CONTENTS

Title	Page
LETTER OF TRANSMITTAL. BRIEF ASSESSMENT. REVIEW BOARD PAGE. PREFACE. TABLE OF CONTENTS. OVERVIEW PHOTO. LOCATION MAP.	iv v vi vii
REPORT	
Section	
PROJECT INFORMATION	1-1 1-1 1-1 1-3
2 ENGINEERING DATA	2-1 2-1 2-1 2-1 2-1
3 VISUAL INSPECTION	3-1 3-1 3-3
4 OPERATIONAL PROCEDURES	4-1 4-1 4-1 4-1
4.4 Description of Any Warning System in Effect 4.5 Evaluation	4-1 4-1 5-1 5-1
6 STRUCTURAL STABILITY	6-1
6.1 Evaluation of Structural Stability	6-1 7-1 7-1 7-1 7-2 7-2
APPENDICES	- -
Design VISUAL INSPECTION CHECKLIST ENGINEERING DATA	A B C D E



Figure 1 - Overview of Paper Mill Dam.



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT PAPER MILL DAM

SECTION 1 PROJECT INFORMATION

1.1 General

a. Authority. Public Law 92-367, August 8, 1972 authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Anderson-Nichols & Company, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed were issued to Anderson-Nichols under a letter of November 20, 1978 from Max B. Scheider, Colonel, Corps of Engineers. Contract No. DACW33-79-C-0009 has been assigned by the Corps of Engineers for this work.

b. Purpose

- (1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) To encourage and prepare the States to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. <u>Location</u>. Paper Mill Dam is located in Bennington, New Hampshire. The dam is a run-of-the-river dam spanning the Contoocook River approximately 43 miles above its confluence with the Merrimack River in Concord, New Hampshire. The Contoocook River is a major tributary in the Merrimack River Basin. Paper Mill Dam is shown on U.S.G.S. Quadrangle, Hillsboro, New Hampshire with coordinates approximately at N43°00'24", W71°55'36", Hillsborough County, New Hampshire. (See Location Map page vii.)

- h. Design and Construction History. One drawing was disclosed of the Paper Mill Dam and Head Gates. This drawing was done by Aberthaw Construction Company in Boston, Massachusetts and dated August 14, 1922. It shows the existence of a previous dam. The drawing indicates that the existing dam was constructed approximately 5.5 feet downstream of the old dam with its crest at the same elevation as the old dam. No details of the previously existing dam were disclosed. This drawing also shows an ogee spillway. Apparently this downstream face was repaired in 1939 and changed to the present straight face inclined at 45°.
- i. Normal Operating Procedures. No written operating procedures were disclosed for Paper Mill Dam. The Contoocook River discharge to the damsite is primarily controlled by the Powder Mill Pond Dam, located approximately 5,600 feet upstream. Before reaching the Paper Mill Dam, the discharge from the Powder Mill Pond also flows over the Monadnock Power Station Dam and the Pierce Power Dam located about 2,100 feet and 1,200 feet upstream, respectively. Monadnock Paper Mills own and control each of these dams. Generally, they operate the Powder Mill Pond Dam to provide sufficient discharge at the Paper Mill Dam for use in power generation and industrial water supply in their paper processing plant.

It is reported that every July the waste gate is opened to release accumulated sediment which has built up behind the dam. This annual opening also permits inspection of the gate and the gate operating facilities.

1.3 Pertinent Data

a. <u>Drainage Area</u>. The drainage area consists of 191 square miles (122,240 acres) of gently rolling terrain.

b. Discharge at Damsite.

- (1) Outlet works waste gate 8'H \times 6'W @ invert elevation 620.6' MSL. Gate capacity at top of dam 710 cfs @ 631.5' MSL. Three head gates 8'H \times 6'W @ invert elevation 620.3' MSL. Capacity is controlled by the turbine capacity which is unknown.
- (2) The maximum discharge at damsite a U.S.G.S. gaging station with a drainage area of 368 square miles is located on the Contoocook River near Henniker, New Hampshire. A maximum discharge of 22,200 cfs was reported at this gaging station during the September 1938 flood. Using this figure, the maximum discharge at damsite can be interpolated to be approximately 12,500 cfs.

- (2) Length of spillway crest pool 1,140
- (3) Length of flood control pool not applicable
- e. Storage (acre-feet)
- (1) Recreation pool not applicable
- (2) Flood control pool not applicable
- (3) Spillway crest pool 25 (approximate)
- (4) Top of dam ~ 50 (approximate)
- (5) Test flood pool 85 (approximate)
- f. Reservoir Surface (acres)
- (1) Recreation pool not applicable
- (2) Flood control pool not applicable
- (3) Spillway crest 5 (approximate)
- (4) Test flood pool 7 (approximate)
- (5) Top of dam 6 (approximate)
- g. Dam
- (1) Type concrete gravity dam
- (2) Length 280'
- (3) Height 19' (structural height)
- (4) Top width varied
- (5) Side slopes upstream face is vertical; down-stream face of spillway is straight but inclined at 45° .
 - (6) Zoning not applicable
 - (7) Impervious core not applicable
 - (8) Cutoff unknown
 - (9) Grout curtain unknown

SECTION 2 ENGINEERING DATA

2.1 Design

No original design data were disclosed for Paper Mill Dam.

2.2 Construction

One drawing prepared by Aberthaw Construction Company, Boston, Massachusetts, was found in the files of the New Hampshire Water Resources Board (NHWRB). This was a drawing of the Paper Mill Dam and Head Gates and was dated August 14, 1922. A copy of this drawing can be seen in Appendix B.

2.3 Operation

No written engineering operational data for power and process water operations have been prepared. Oral instructions have been in effect during the history of the operations. These instructions are transmitted from supervisors to subordinates.

2.4 Evaluation

- a. Availability. Limited engineering data were available for Paper Mill Dam. A search of the files of the NHWRB and direct contact with the owner revealed only a limited amount of recorded information.
- b. Adequacy. Because of the limited amount of detailed data available, the final assessments and recommendations of this investigation are based on the visual inspection and hydrologic and hydraulic calculations.
- c. Validity. The visual inspection is generally consistent with the $\overline{1922}$ drawing by the Aberthaw Construction Company. An ogee spillway crest is shown on this plan; the visual inspection of this dam shows a straight downstream face angled 45°. This change apparently occurred during repairs in 1939.

An earth dike has been constructed north of the roadway to effectively cut off high water from flowing directly into the canal. The dike is approximately 1.7 feet above the roadway and 9.3 feet above the spillway crest. The dike is approximately 190 feet long and 6 feet high. The top of the dike is 9 to 10 feet wide with side slopes of about 3H:1V. The side slopes are wooded and the exposed portion of the dike near the roadway shows a gravel surface which would be susceptible to erosion during high water conditions. (See Appendix C - Figure 4.)

A 12-inch concrete pipe about 20 feet in length extends through this dike. If water should ever pond behind the dike, some discharge could be passed through the pipe into the canal. The inlet to this pipe contains stoplog slots which would provide a means of controlling flow.

On a return visit to the dam on April 19, 1979 it was observed that a piece of the dam crest (approximately 2 cubic feet) had apparently spalled away near the center of the dam. The depression caused by the spalling is reflected in the water surface passing over the crest. (See Appendix C - Figure 15.)

c. Appurtenant Structures. The outlet works and gate-control structures are located at the north abutment. (See Appendix C - Figure 5.) Significant spalling and erosion of the concrete on the downstream side of the gate structure was noted. The presence of bedrock in the discharge channel immediately downstream of the gate structure would indicate that the abutment is on bedrock, which is consistent with design drawings dated 1922 which show the gate structure to be founded on "ledge."

The waste gate is located adjacent to the north abutment of the spillway. The timber gate is manually operated by a mechanism located directly above the opening. At the time of inspection leakage was noted through the timber gate. (See Appendix C - Figure 6.) The downstream concrete wall to the right of the low-level outlet was noted to have deteriorated and spalled from the base to approximately 2 feet up the wall. (See Appendix C - Figure 7.)

The head gates are located adjacent but perpendicular to the waste gate. The leading edges of the head gate inlet structures have also deteriorated and spalled to a depth of approximately 1 - 3 inches. (See Appendix C - Figure 8.) It appeared that some portion of the gate support structures had been recently repaired. The timber gates were inspected in the raised position and found to be in good

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures

Although no written operational procedures have been developed for Paper Mill Dam, Messrs. Gordon Bishop, Chief Engineer and George Edwards, Maintenance Superintendent, are fully familiar with the operational procedures of their four dams, Powder Mill, Monadnock Power, Pierce Power, and Paper Mill, and the appurtenant facilities including the operations for hydropower generation. Mr. Bishop maintains complete records of all maintenance performed including cost records and operates on an annual budget. Each summer maximum releases of water from Powder Mill Dam are made and power is generated for a period such that the Powder Mill Reservoir is drawn down to about two feet below the concrete crest. This procedure provides additional storage enabling the lower three ponds to be drawn down for visual inspection and maintenance, if required. The gates at Powder Mill are then closed and the lower three dams are dry for a week to 10 days. This procedure is usually accomplished in July. Accumulated sediment which has built up behind the dam passes downstream through the waste or power gates (waste gate at Paper Mill). The head gates are operated to provide sufficient discharge into the mill building for use in power generation and industrial process water.

4.2 Maintenance of Dam

Monadnock Paper Mills is responsible for the maintenance of Paper Mill Dam. No written maintenance program has been prepared. Maintenance is performed as required; larger items are budgeted and scheduled for completion annually. Inspection of the upstream face of the dam is accomplished during the drawdown period. Mill maintenance personnel are aware of spalling and loose concrete in the dam face and funds are approved for repairs to be done in September and October 1979.

4.3 Maintenance of Operating Facilities

The annual releasing of sediment through the waste gate enables the testing of the operating facilities to ensure that they are functional.

4.4 Description of Any Warning System in Effect

A gage is located on the downstream face of the road crossing located approximately 2,200 feet downstream of Paper Mill Dam. During floodflow periods (usually occurring each spring) when the water reaches 3 feet on this downstream tailwater gage (0' at gage-598' MSL) a flood watch around the clock is initiated by maintenance personnel. Two men ride up and down the road along the stream to observe conditions. Evacuation of the

SECTION 5 HYDROLOGIC/HYDRAULIC

5.1 Evaluation of Features

- a. General. Paper Mill Dam is a low, run-of-the-river concrete gravity dam which impounds a reservoir of small size. The abutments are concrete and would probably with-stand considerable overtopping before serious damage would result. The dam has 3.9 feet of freeboard available before overtopping would occur on the north abutment. The south abutment is 4.1 feet above spillway crest. The northerly dike has a crest elevation averaging 9.3 feet above spillway crest.
- b. <u>Design Data</u>. No hydrologic or hydraulic design data were disclosed for Paper Mill Dam.
- c. Experience Data. Low flow and flood profiles for the March 1936 and September 1938 floods are shown on the Contoocook River, New Hampshire Plan and Profile, Sheet 5 of 7, February 1939, Revised February 1951, U.S. Engineer Office, Boston, Massachusetts. (See Appendix B.)
- d. <u>Visual Observations</u>. At the time of inspection, no visual evidence was noted of damage to any portions of the concrete structure caused by excessive discharges.
- e. Test Flood Analysis. Paper Mill Dam is classified as being small in size having a hydraulic height of 19 feet and a maximum storage capacity of 50 acre-feet. The dam was determined to have a Significant Hazard classification. Using the Recommended Guidelines for Safety Inspection of Dams, the test flood was determined to be 1/4 Probable Maximum Flood (PMF).

Using the 1/4 PMF, the test flood discharge was determined to be 15,760 cfs. The overtopping analysis indicates that the dam would be overtopped by 5.2 feet during the test flood. The maximum spillway capacity at top of dam is 3,830 cfs which is 24 percent of the test flood discharge. However, because both abutments are concrete, they would probably withstand considerable overtopping before damage. The northerly dike has a crest averaging 9.3 feet above spillway crest and would therefore be on the verge of overtopping during the test flood.

f. Dam Failure Analysis. The impact of failure of Paper Mill Dam at normal flow conditions and at top of dam were assessed using the Guidance of Estimating Downstream

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

- a. <u>Visual Observations</u>. The visual examination indicated the following evidence of potential long-term stability problems:
- (1) Deterioration and erosion of the concrete in the main dam, particularly along the cold joints and at the non-overflow portion at the south abutment of the dam.
- (2) Spalling and erosion of the concrete on the downstream side of the waste gate structure.
- b. <u>Design and Construction Data</u>. A drawing dated 1922 shows the plan of the dam and a typical cross section. The cross section shown on this drawing has an ogee downstream face. No construction data were available.
- c. Operating Records. No operating records pertinent to the structural stability of the dam were available.
- d. Post-Construction Changes. The dam was apparently repaired in 1939, which is apparently the time when the original ogee downstream face was changed to the present straight face inclined at 45° .
- e. <u>Seismic Stability</u>. This dam is located in Seismic Zone No. 2 in accordance with recommended Phase I guidelines does not warrant seismic analysis.

7.3 Remedial Measures

- a. Operating and Maintenance Procedures. The owner should:
- (1) Remove trees and brush for a distance of 25 feet upstream and downstream of the south abutment.
 - (2) Visually inspect the dam once a month.
- (3) Establish a written surveillance and warning program to follow in the event of emergency conditions.
- (4) Engage a Registered Professional Engineer to make a complete technical inspection once every two years.

7.4 Alternatives

None.

APPENDIX A

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST PARTY ORGANIZATION

PROJECT Paper Mill Dam, N.H.	DATE November 20, 1978
	TIME 8:30 AM
	WEATHER Clear, cold (40°F)
	W.S. ELEV. U.S. DN.S. 627.8 618.5
PARTY:	
1. Warren Guinan 6	Leslie Williams
2. Robert Langen 7.	Harold Wilcox (1/3/79)
3. Stephen Gilman 8.	John Falcione (1/3/79)
4. Ronald Hirschfeld 9.	
5. Robert Ojendyk 10.	
PROJECT FEATURE	INSPECTED BY REMARKS
1. Hydrology/Hydraulics	R. Langen
2. Structural	S. Gilman
3. Soils & Geology	R. Hirschfeld
4. Mechanical	H. Wilcox
5	
6	
7	
8	
9	
10	

	CTION CHECKLIST
PROJECT Paper Mill Dam, N.H.	DATE November 20, 1978
PROJECT FEATURE Northern Dike	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DIKE EMBANKMENT	
Crest Elevation	Ranges from 636.6 - 637.7
Current Pool Elevation	Not applicable
Maximum Impoundment to Date	Not applicable
Surface Cracks	None noted
Pavement Condition	Not applicable
Movement or Settlement of Crest	None noted
Lateral Movement	None apparent
Vertical Alignment	Good
Horizontal Alignment	Good
Condition at Abutment and at Concrete Structures	Good at tiein with road abutment
Indications of Movement of Structural Items on Slopes	None visible
Trespassing on Slopes	Foot path visible on dike crest
Sloughing or Erosion of Slopes or Abutments	Slight erosion at south end exposed gravel surface. Slopes wooded.
Rock Slope Protection - Riprap Failures	None
Unusual Movement or Cracking at or Near Toes	None apparent
Unusual Embankment or Down- stream Seepage	None apparent
Piping or Boils	None visible
Foundation Drainage Features	None apparent
Toe Drains	None visible
Instrumentation System	None visible
Vegetation	Grassed crest

PERIODIC INSPE	CTION CHECKLIST
PROJECT Paper Mill Dam, N.H.	DATE November 20, 1978
PROJECT FEATURE Intake Channel &	Structure NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	
a. Approach Channel	Contoocook River
Slope Conditions	Good, vertical concrete sidewalls
Bottom Conditions	Not visible beneath pond level
Rock Slides or Falls	None
Log Boom	See below
Debris	Little
Condition of Concrete Lining	Not visible beneath pond level
Drains or Weep Holes	None apparent
b. Intake Structure	
Condition of Concrete	Concrete in good condition; piers have deteriorated and spalled
Stop Logs and Slots	Good
Logboom - at upstream of intake of boards. This stops floating trastop log was weathered and in poor	onsists of a wood log with vertical h from reaching the intakes. The condition.
Steel trash racks were rusted but	in good condition.
	ļ

PERIODIC INSPECT	TION CHECKLIST
PROJECT Paper Mill Dam, N.H.	DATE November 20, 1978
PROJECT FEATURE Control Tower	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - CONTROL TOWER	
a. Concrete and Structural	
General Condition	Good
Condition of Joints	Good. No evidence of movement
Spalling	1" - 3" on leading edges of gate
Visible Reinforcing	piers None
Rusting or Itaining of Concrete	None visible
Any Seepage or Efflorescence	Little on faces of abutments and
Joint Alignment	piers Good
Unusual Seepage or Leaks in Gate Chamber	None
Cracks	Limited to hair line cracks
Rusting or Corrosion of Steel	Only at embedded elements of steel
b. Mechanical and Electrical	
Air Vents	4 wooden sluice gates. Hand operated wheels. Gates are in
Float Wells	good condition
Crane Hoist	Not applicable Not applicable
Elevator	Not applicable
Hydraulic System	Not applicable
Service Gates	Good condition - operating
Emergency Gates	mechanism - good condition Not applicable
Lightning Protection System	Not applicable
Emergency Power System	Not applicable

Not applicable

Wiring and Lighting System

PERIODIC INSPECTION CHECKLIST

PROJECT Paper Mill Dam, N.H. PROJECT FEATURE Outlet Structure DISCIPLINE	& Channel NAME
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL General Condition of Concrete	Good
Rust or Staining	None visible
Spalling Erosion or Cavitation	Significant deterioration of north wall d/s of low-level outlet at bas
Visible Reinforcing	None visible
Any Seepage or Efflorescence	None visible
Condition at Joints	No apparent movement
Drain holes	None apparent
Channel	
Loose Rock or Trees Overhanging Channel	Some trees and brush adjacent to channel, which is wide.
Condition of Discharge Channel	Good. One log across channel immediately downstream of low-level outlet.

PERIODIC INSPECTION CHECKLIST DATE November 20, 1978 PROJECT Paper Mill Dam, N.H. PROJECT FEATURE Spillway Weir NAME DISCIPLINE _____ AREA EVALUATED CONDITION OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS a. Approach Channel Contoocook River General Condition Good Loose Rock Overhanging Channel None Trees Overhanging Channel Some trees and brush adjacent to channel which is wide - not Floor of Approach Channel visible beneath pond surface b. Weir and Training Walls General Condition of Concrete Fair. Weir has surface erosion 'z" deep and 2" deep at concrete Rust or Staining pour joints. None visible Spalling Some spalling on training walls. See note below. Any Visible Reinforcing None Some on training walls at hairline Any Seepage or Efflorescence cracks Drain Holes None apparent c. Discharge Channel General Condition Good - very rocky Loose Rock Overhanging Channel None Trees Overhanging Channel Some trees and brush adjacent to | channel which is wide. Floor of Channel Bedrock, with some large boulder.

Other Obstructions

frost action.

Four railroad - bridge piers

Note: Left abutment and training wall has spalled 4" deep. One area on d/s face about 4' below u/s water line has seepage through concrete. D/s face spalled from

PERIODIC INSPECTION CHECKLIST

PROJECT Paper Mill Dam, N.H.	DATE November 20, 1978
PROJECT FEATURE Service Bridge	NAME
DISCIPLINE	NAME

Ω

	r		
AREA EVALUATED	CONDITIO	N	
OUTLET WORKS - SERVICE BRIDGE	Over low-level outlet	Over Intake & Bar Rack	
a. Super Structure			
Bearings	None	None	
Anchor Bolts	None	None	
Bridge Seat	None	None	
Longitudinal Members	None	None	
Underside of Deck	Good	Fair	
Secondary Bracing	None	None	
Deck	Conc, good cond.	Some spalling on	
Drainage System	None	east end None	
Railings	Steel-little	Steel-good	
Expansion Joints	corrosion Fair	Fair	
Paint	Fair	Fair	
b. Abutment & Piers			
General Condition of Concrete	Good	Good-Surface laitance	
Alignment of Abutment	Good	gone below water lir	
Approach to Bridge	Not applicable	Not applicable	
Condition of Seat & Backwall	Not applicable	Not applicable	

	1111 Dam	Paper N	PROJECT
PROJECT FEATURE Reservoi	Reservo:	FEATURE	ppo.፣ድርጥ

DATE November 20, 1978

NA R. Langen

	· · · · · · · · · · · · · · · · · · ·
AREA EVALUATED	REMARKS
_	
Stability of Shoreline	Good
Sedimentation	Significant
Changes in Watershed Runoff Potential	None
Upstream Hazards	l restaurant
Downstream Hazards	Monadnock Paper Mill parking lot and maintenance garage; bridge
Alert Facilities	None
Hydrometeorological Gages	None
Operational & Maintenance Regulations	None posted
•	
	-

APPENDIX B
ENGINEERING DATA

NEW HAMPSHIRE WATER CONTROL COMMISSION DATA ON DAMS IN NEW HAMPSHIRE

	STATE NO
Town Bennington	.: County Hillsooro
Stream Gontoocook	******
Basin-Primary Merrimack River	: Secondary Contoocook River -
Local Name	
Coordinates—Lat43° 00! +2,200	: Long. 71° 55! † 2,800
ENERAL DATA	
Drainage area: Controlled Sq. Mi.: 1	Uncontrolled Sq. Mi.: Total192 Sq. Mi.
Overall length of dam 27.93 ft.: Date of	Construction1922
Height: Stream bed to highest elev12.58.	ft.: Max. Structure .8.08 8.03 5.03 ft.
Cost—Dam	: Reservoir
ESCRIPTION O Gee Face Concrete	
Waste Gates	
Type	******
Number1: Size8	ft. high x
Elevation Invert	: Total Area
Hoist	***************************************
Waste Gates Conduit	
Number: Mater	ials
Size ft.: Length	ft.: Areasq. ft.
Embankment	
Type	***************************************
	. ft.: Min ft.
Top-Width	: Elev ft.
Slopes-Upstream on	: Downstream on
Length-Right of Spillway	: Left of Spillway
Spillway	
Materials of Construction Conci	rete
Length—Total	ft.: Net
Height of permanent section—max 8	ft.: Min ft.
Flashboards—Type Removable V	: Height .2.Ω
	: Top of Flashboard
•	efs.:
Abutments	•
Materials: Concrete.	
Freeboard: Max. 14.5 A 55	ft.: Min
Headworks to Power Devel.—(See "Data on I	
WNER Monachook Paper Mills-	Sanday & Plantitudina II II
1 ilmining Cond, M. 94.	
Canal SOO! to Mill	
Canas Coo to milit	

NEW HAMPSHIRE WATER CONTROL COMMISSION DATA ON WATER POWER DEVELOPMENTS IN NEW HAMPSHIRE

LOCATION								
Town	Benningto	n.		County	Hiller	QXQ	•••••	
Stream	.Cont.cocc	ok.		•••••	•••••	•••••	•••••	
Basin-Prima	rv Merri	mack River		Sec	condary .C	ont pacac	k.Riv.	er
Local Name		Grat . 4	11.9.7.1	••••••	••••••	•	······	
GENERAL DA					•			
Head-Max.		ft.: h n.	ft.:	Ave	3	<u>01</u>		
Date of Con	struction	922		Use of Pov	verI <u>n</u> du	strial	• • • • • • • • • • • • • • • • • • • •	
Pondage		Section 1985	ac. ft.: S	Storage	••••••	,	• • • • • • • • • • • • • • • • • • • •	ac.
DESCRIPTION	ľ		A. 1. 1.			4.4	. •	4 4
Racks	4			(s.)				
Size of Ra	ck Opening			••••••	••••••			المرادا أو
Size of B	Br	pagagaga empagagagaga sa sa sa Tanggagagaga	: 1	Material	••••••	•••••	•••••	
Area: Gre	esc		Sq. Ft.:	Net		•••••••		ps
Head Gates		* 5" ·	,					.*.
Туре	***********	••••••••		••••••	••••••	•••••	••••••	
Number	3	: Size	ft. 1	nigh x	6	•••••	•••••	ft. wi
Elevation	of Invert	7.24		Total Area	4	<u> </u>	••••••	sq.
** * .		•		••••	••••••	•••••		
Penstock Number. Size	1	45 "	.: Material					
Penstock Number . Size Turbines Number .	1	45"	.: Material: Length . : Makers		800	-	************	······································
Penstock Number. Size Turbines Number. Rating H	1 P. per unit .	45 "	.: Material: Length . : Makers	Total Caps	800 acity	8	00	P
Penstock Number . Size Turbines Number . Rating HI Max. Den	1 P. per unit .	45"	.: Material: Length . : Makers	Total Caps	800 acity	8	00	P
Penstock Number . Size Turbines Number . Rating HI Max. Den	P. per unit .	45" per unit	.: Material: Length . : Makers	Total Caps	800 acity		00	B
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type	1 P. per unit . nent C.F.S.,	45" per unit	.: Material: Length . : Makers	Total Caps	800 acity		00	B
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type	1 P. per unit . nent C.F.S.,	45" per unit	.: Material: Length . : Makers	Total Caps	800 acity		00	B
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number .	P. per unit .	45" per unit	.: Material: Length . : Makers	Total Caps	800 acity : Total		00	В с
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make	P. per unit . nent C.F.S.,	45" per unit Lectric D	.: Material: Length . : Makers	Total Caps	acity	<i>8</i>	00	B c
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV	P. per unit . nent C.F.S., General	per unit	.: Material: Length .: Makers	Total Capa	acity	. 1	00	E C C C C C C C C C C C C C C C C C C C
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV	P. per unit . nent C.F.S., General	per unit	.: Material: Length .: Makers	Total Capa	acity	. 1	00	E C C C C C C C C C C C C C C C C C C C
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number . Make Rating KV Exciter Number .	P. per unit . nent C.F.S., General W., per unit	45" per unit Electric D 200	.: Material: Length .: Makers	Total Caps 25 ; Total Caps	acity	. 1 - 2	0 0	В. С
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV Exciter Number Rating-pe	P. per unit. nent C.F.S., General. W., per unit	per unit	.: Material: Length .: Makers	Total Caps 25 ; Total Caps	acity	. 1 - 2	0 0	В. С
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV Exciter Number Rating-pe	P. per unit	per unit	.: Material: Length .: Makers	Total Caps 25 Total Cap Capacity	acity		0 0	K. V
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV Exciter Number Rating-pe OUTPUT—KV 19	P. per unit	per unit Lectric D 200	.: Material: Length .: Makers .: .: .: .: .: .: .: .: .: .: .: .: .:	Total Capa 25 ; Total Capa Capacity	acity		0.0	K. V.
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number . Make Rating KV Exciter Number . Rating-pe OUTPUT—KV 19	P. per unit. nent C.F.S., General. W., per unit r unit	per unit Electric D 200	.: Material: Length .: Makers .: Makers .: Total	Total Caps 25 Total Caps Capacity 19	acity		0 0	K. V.
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV Exciter Number Rating-pe OUTPUT—KV 19 19	P. per unit General W., per unit r unit WHRS	per unit Lectric D. 200.	.: Material: Length .: Makers .: .: .: .: .: .: .: .: .: .: .: .: .:	Total Capa Total Capa	acity		00	K. V.
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number . Make Rating KV Exciter Number . Rating-pe OUTPUT—KV 19 19 19	P. per unit. nent C.F.S., General. W., per unit	per unit Electric D 200	.: Material: Length .: Makers .: Makers .: Total	Total Caps 25; Total Caps Capacity 19 19 19	acity		0 0	K. V.
Penstock Number . Size Turbines Number . Rating HI Max. Den Drive Type Generator Number Make Rating KV Exciter Number . Rating-pe OUTPUT—KV 19 19	P. per unit	per unit Lectric D. 200.	.: Material: Length .: Makers .: Makers .: Total	Total Capa Total Capa	acity		0 0	K. V.

NEW HAMPSHIRE WATER RESOURCES BOARD

QUESTIQ:NAIRE

WATER POWERS OF NEW HALFSHIRE

Monadnock Paper Mills Bennington New Hampshire

Gentlemen:

We raintain in this office a list of the water power installations in New Hampshire. In recent months we have had several inquiries concerning the water power installations in the State and have found that our information is in some cases out of date.

We are, therefore, bringing this information up to date and request your cooperation by filling in the questionnaire below with data on your development, and return it to us in the enclosed stamped envelope.

Very truly yours,

RSH:GMB Enci.

Chief Engineer

Dam No. 22.06: Location: Contobcook River at Semmington

1. Will you please check or correct:

	Our Data	Your Corrections
Drainage Area - Sq.Mi. Head - feet Capacity (Total) Wheel - H.P. Generator - K.W.	192 30 800	

2. Is the power plant now in operation?

3. If not, is the equipment in operable condition?

4. Is the dam in good repair?

B-3

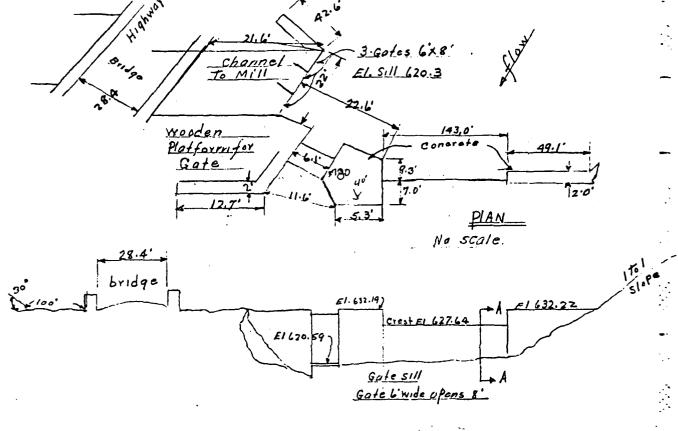
NEW HAMPSHIRE
WATER RESOURCES
BOARD
CONCORD, N. H.

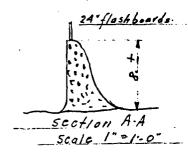
MERRIMACK. Coritoocook Monadnock Paper Mills
COMPUTER G. S. W. CHECKER A.R. FOOT.

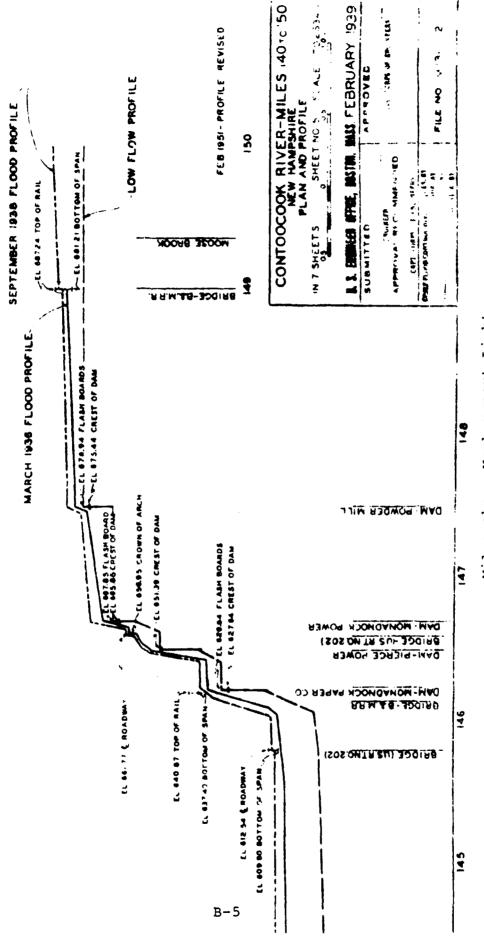
COMPUTER G. S. W. CHECKER A.R. FOOT.

Channel To Mill Great G. S.

Channel To Mill Great G. S.







Miles above Newburyport Light

NEW HAMPSHIRE WATER RESOURCES BOARD

INVENTORY OF DAMS AND WATER FOWER DEVELOPMENTS

<u>PAM</u>	<i>F</i>
BASTY Merrimack	NO. X 22.06 /182 PA
RIVER (ntoocook-	NO. X 22.06 /60 PROVIDE TO 146.3 D.A.SQ. MIL/192 4
TOWN Bennmaton	OWNER MECEN CLE Paper Mills Vust
TOWN Bennington LOVAL NAME OF DAM	
BUILT /922 DESCRIPTION	Concrete Courty
POND ERLY-AGRES DRAW	DOWN FOR FOND CAPACITY-ACRE FT.
ात-संक्रीतार्थ वर प्रस्ति पर पर पर प्रस्ति है।	12.58 MAX. MIN.
OVERALL LENGTH OF DAM-FT. 279	3. MAX.FLOOD HEIGHT ABOVE CREST-FT. 627.64 LOGAL GAGE
PERMANENT CREST ELEV. U.S.G.S'.	627.64 LOJAL GAGE
TAILMATER ELEV.U.3.F.S.	
SPILLWAY LENGTHS-FT. //4/wrs.	143 AE FREEDCARD-FT. 4.5 WRB. 4.5CH
FLASHBOARDS-TYPE, HEIGHT FROVE	CRINT 2.0 A &
WASTE GATES-NC. WIDTH MAK. OF	
	7.05' Waste
3 6.0 . 8.0	7.24' to wheel chausel
REMARKS 4I MORIMON H	19: Water 629.64
Driginal plans by Aberthow Co	Boston, Mass.
PS COMM, SAYS dam 10'h	194 200 1chg, Spillmay 1501/049 2
Condition good.	, , , , , , , , , , , , , , , , , , ,
	· · · · · · · · · · · · · · · · · · ·
	2014
	ASSUMED C = 3.9
	ASSUMED C = 3.9 43.53
PCWER DEVELOPMENT	ASSUMED C = 3.9
POWER DEVELOPMENT RATED HEAD C.F.	ASSUMED C = 3.9
PCWER DEVELOPMENT	ASSUMED C = 3.9
POWER DEVELOPMENT RATED HEAD C.F.	ASSUMED C = 3.9
POWER DEVELOPMENT RATED HEAD C.F.	ASSUMED C = 3.9
PCWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL	ASSUMED C = 3.9 3. GATE - KW MAKE
POWER DEVELOPMENT RATED HEAD C.F.	S. GATE - EW MAKE 700KW 45 Poducy Hunt porez Tox
PCWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL	ASSUMED C = 3.9 3. GATE - KW MAKE
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL ### ### ### #######################	S. GATE - EW MAKE 700KW 45 Poducy Hunt porez Tox
POWER DEVELOPMENT RATED HEAD C.F. UNITS NO. HP FEET FULL Scorified 30	S. GATE - EW MAKE 700KW 45 Poducy Hunt porez Tox
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL ### ### ### #######################	S. GATE - EW MAKE 700KW 45 Poducy Hunt porez Tox
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL ### ### ###########################	S. GATE - KW MAKE POOKW 45 Poducy Hunt horiz Top GE.DC-250V rch 1936-Flood by Wir B
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL Abouted 30 USE Power for Paper Mill. REMARKS Surveyed during MA Marinuum head 5.544 disea	S. GATE - KW MAKE POOKW 45 Peducy Hunt herez Tee GE.DC-250V TCh 1936-Fleed by Wir B Fange 10:000 CAS 52 CAS / 12 mi
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL Accompanying Sketch Copy	S. GATE - KW MAKE POOKW 45 Peducy Hunt herez Tes GE.DC-250V TCh 1936-Fleed by Wir B Ange 10.000c 45 52 c.45 /2 mi ed from Army Engineer's Field vote:
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL Fower for Paper Mill. REMARKS Surveyed during MA	S. GATE - KW MAKE POOKW 45 Peducy Hunt herez Tes GE.DC-250V Teh 1936-Fleed by Wir B Ange 10.000c 45 52 c.45 /2 mi ed from Army Engineer's Field note:
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL Fower for Paper Mill. REMARKS Surveyed during MA	S. GATE - KW MAKE POOKW 45 Peducy Hunt herez Tes GE.DC-250V TCh 1936-Fleed by Wir B Ange 10.000c 45 52 c.45 /2 mi ed from Army Engineer's Field vote:
POWER DEVELOPMENT RATED HEAD C.F. UNITS MO. HP FEET FULL Fower for Paper Mill. REMARKS Surveyed during MA	S. GATE - KW MAKE POOKW 45 Peducy Hunt herez Tes GE.DC-250V Teh 1936-Fleed by Wir B Ange 10.000c 45 52 c.45 /2 mi ed from Army Engineer's Field note:

TATE 1925125 C.

DAKS AND THEIR LOCATIONS IN TOWN OF Bennington

	Location River, Brook, Pond or Lake	on ind or Lake	Condition Ruins or Operable	Owner Monadonock Paper Mills	Owner's Address Bennington
٦.	v rowder Mill Dam	Lake	Concrete		
ج	Monadnock Power Station Dam	River	r	£	r
پر	Pierce Power Station Dam	River	£	£	t
Ž.	4V6 Paper Mill Dam	River	t	E	-
5. 6. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	Three Dams on two Town Water work	a on two brooks Ass.	Uperable	Town of Bennington	
€.	Lake George		Non-operable	Monadnock Paper Mills	Ŧ
9.			1 5/2 mone	The state of the s	C.
10.			ROUTE THE COMMENTER THE COMMEN		
11.			T.C. IIPT	9	Celusia.
.12.			Seyer B		
13.			10.00	-	

Town No. 4-5 Town Pennington No. 150
Data by
Owner
River or Stream Contoccook River
Public Utility
Wheel Capacity H. P. 130 { Primary H. P. 90% time }
Type of Construction Concrete
Height 14 Operating Head 14 ft.
Length
Would Failure of Dam do Harm! Yes
Present Condition Fair Date 1922 LWB Good 1925

PAPER MILL DAM

Town No6
Data by L. W. 3 File
Owner
River or Stream Contoocook River
Public Utility No Drainage area 184 sq. mi.
Wheel Capacity H. P
Type of Construction Concrete
Height10ft. Operating Head30ft.
Length 200 ft. Spillway Length (No. 1) 150 ft. (No. 2) ft.
Would Failure of Dam do Harmi. No.
Present Condition Pair Date 1972
m. LVB Good

NEW HAMPSHIRE WATER RESOURCES BCARD State House Annex Concord, N. H.

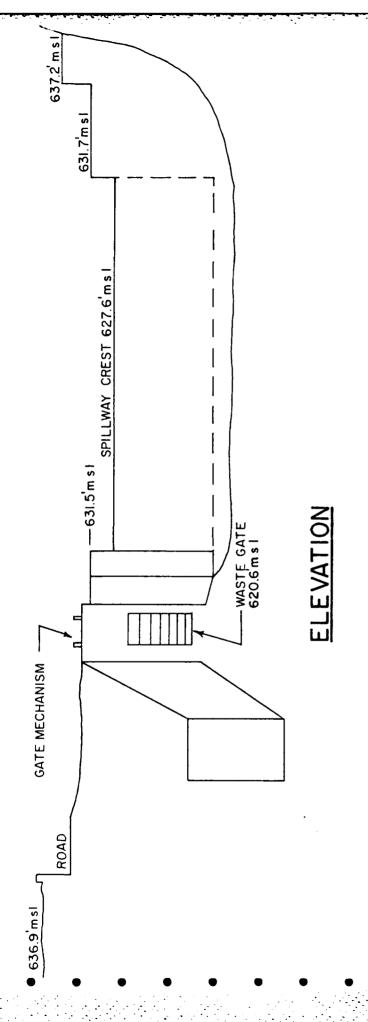
December 4, 1961

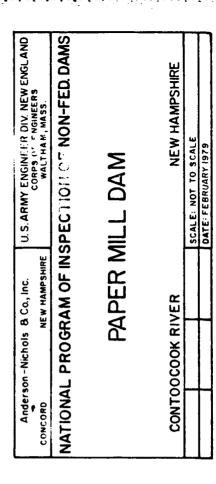
Monadnock Paper Co, Bennington, N.H.

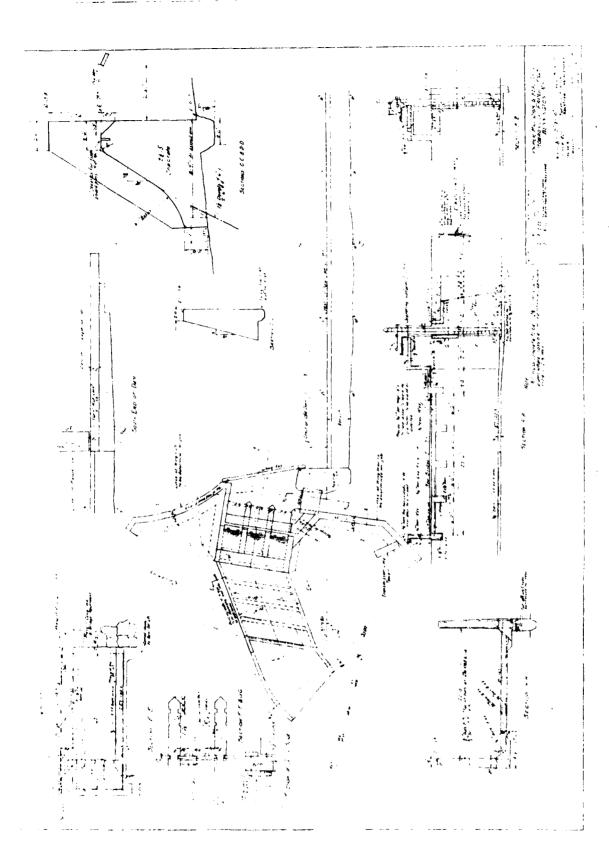
Dear Sir:

To bring our records of hydro-electric power installations up to date, we are requesting you to furnish the following information on your generators in use at the present time:

__ reported as _____160 __KW in 1951 presently using KW generators. 240 K7 in 1051 ales: presently using_ ___KV generators. 450 KM in 1057 also: presently using KV generators Monachock Station 1-120 KUA - (== 03) Pince station 1- 220 KUA 17 = - (== 00) / -- (22.06) Will Will Wheel 1-750 KUA Francis C. Woode Francis C. Moore Giore whals & generators and an in good condition and produce pour when water is available. Civil Engineer MuBullail Power Engineer







APPENDIX C

PHOTOGRAPHS

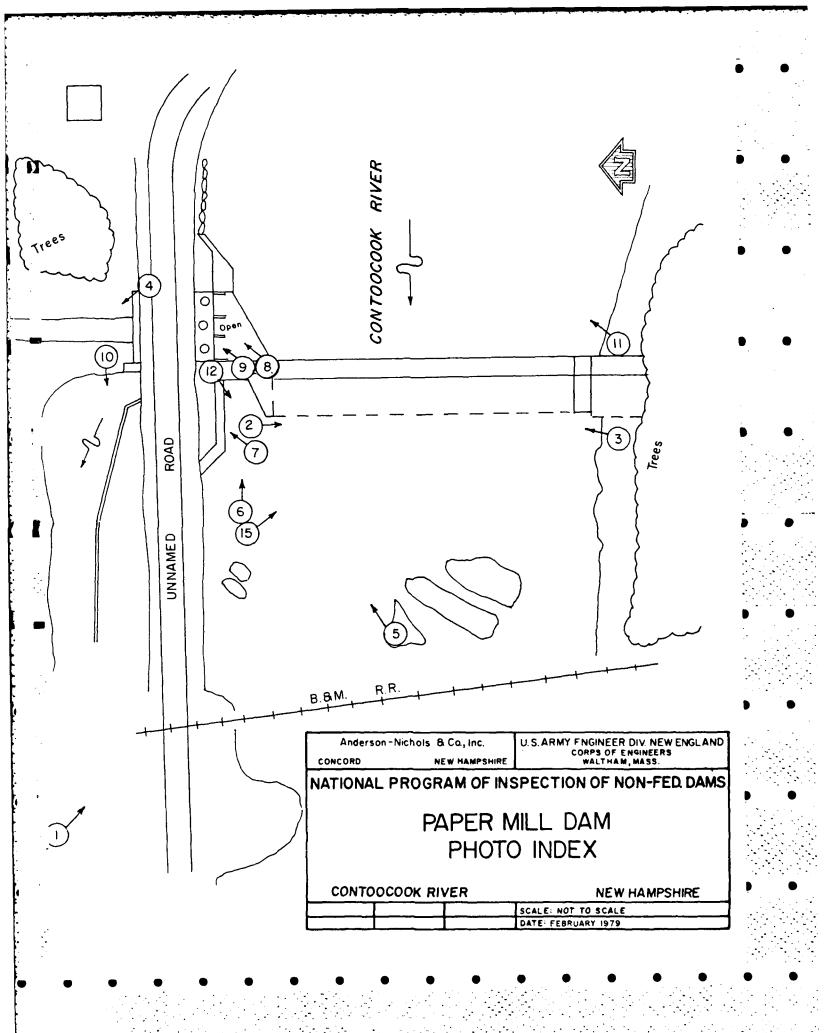




Figure 2 - Looking south along the upract of fact of the spillson. Not a booking to the south of the south of



Figure 3 - Looking at the south abutment adjacent to the spillway. Note the spilling of the concrete.



Figure 4 - looking at the upstream face of the northerly dike. Note the gravel crest.



Figure 5 - Ties of the tests without the the wind to contain the last state of the last

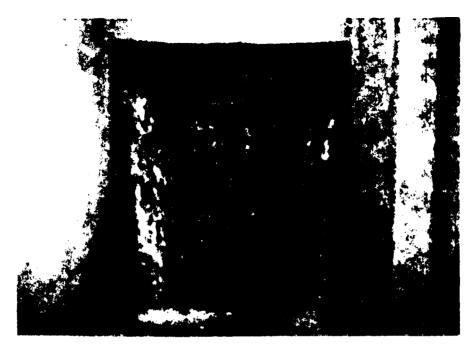


Figure 6 - tinw of the timber rate in the waste of a contract to the norm that a contract the specific specifi

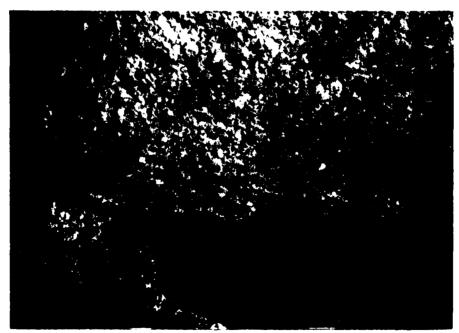


Figure 7 - View of the deteriorated and spelled transfer at the hane of the worte bluice.



Figure 3 - View of the trash racks and head gates.
Note the spalling of the piers.

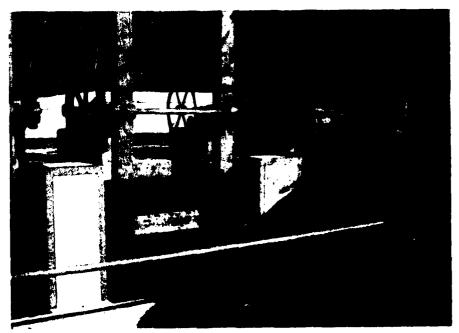


Figure 9 - Looking north at the timber head dates and the operating mechanisms.



Figure 10 - View of the canal which feeds discharge into the mill building for use in power generation and process water.

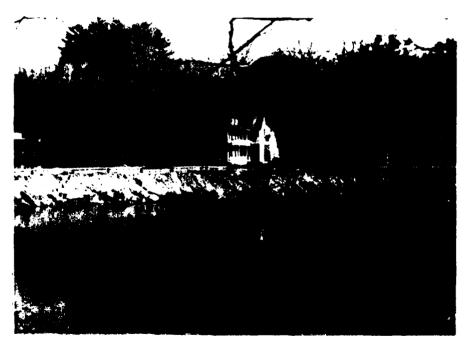


Figure 11 - Looking at the house/restaurant located on the north bank of the approach channel.



Figure 12 - Looking at the railroad bridge located about 200 feet downstream of the dam.



Figure 13 - View of Monadneck Paper Mills located on the east bank of the discharge channel about 1000 feet below the dam.

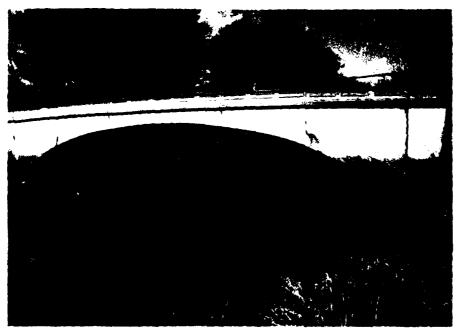


Figure 14 - View of the upstream face of the road crossing located approximately 2,200 feet downstream of the dam.

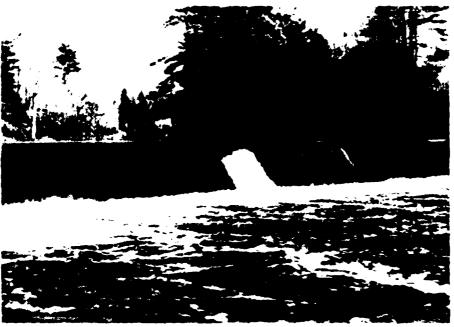
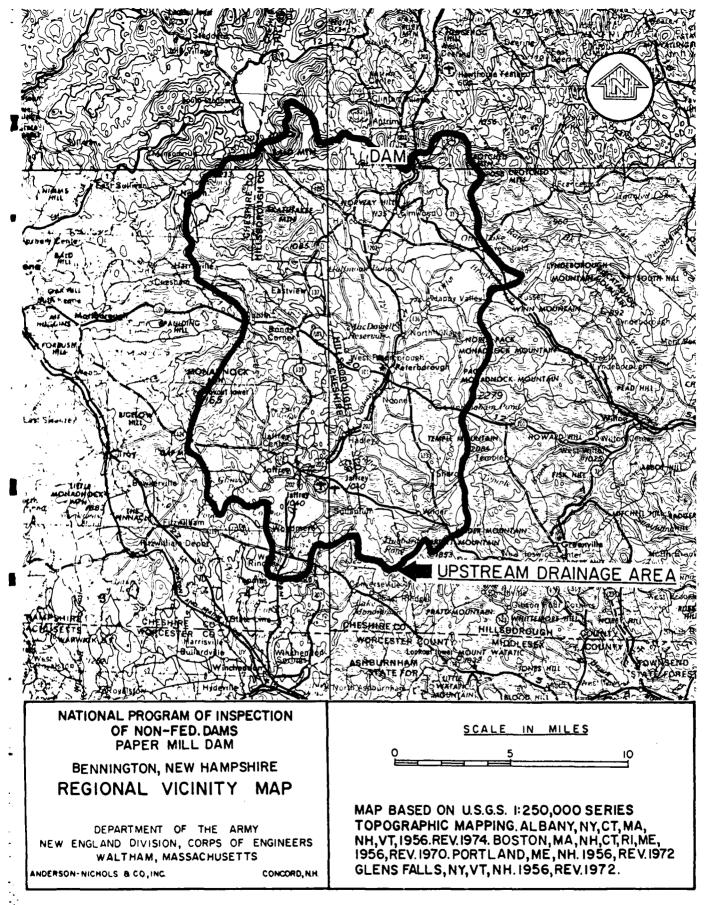


Figure 15 - View of the eroded section of the dam crest.

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS



Determine discharge rating curve for the dam using, the weir equation Q = CLH3/2, where the 'c' for the dam spillway crest is 3.5, c' over abstracts is 3.2, and c' over dike at right abstraction 2.8. (Assuming no tailwater)

Trial #1 @ 627.60 Spillway Crest

Q = O CFS

Trial # 2 0 6 2 8 . 0 Q = 3.5 (142 \(0.4 \) 3/2 = 126 cfs

Trial #3 0629.0 Q-3.5(142)(1,4)3/2=823 cfs

Trial # 4 @ 630.0 Q=3.5(142\(2.4)^3/2=1848 cfs

Trial # 5 @ 631.5 maximum pool (right abut.)
Q = 3.5(142\(\chi 3.9\))^3/z = 3828 cfs

Trial ± 6 © 631.7 left lower abstruent $Q = 3.5(142)(4.1)^{3/2} + 3.2(7.8)(0.2)^{3/2}$ = 4126 + 2 = 4128 cfs

Trial #7 @ 633.0 $Q = 3.5(142)(5.4)^{3/2} + 3.2(7.8)(1.5)^{3/2} + 3.2(35)(1.3)^{3/2}$ = 6237 + 46 + 166 = 6449 cfs

Trial #8 @ 635.0 $Q = 3.5(142)(7.4)^{3/2} + 3.2(7.8)(3.5)^{3/2} + 3.2(35)(3.3)^{3/2}$ = 10,005 + 163 + 671 = 10,839 cfs

* King & Broter - Figure 5-16, Table 5-13

Trial #9 @ 636.6 low pt. right dike $Q = 3.5(142)(9.0)^{3/2} + 3.2(7.8)(5.1)^{3/2} + 3.2(35)(4.9)^{3/2} + 3.2(4.5)(1.3)^{3/2} + 3.2(38)(1.4)^{3/2} + 3.2(55)(1.56)^{3/2} = 13419 + 287 + 1215 + 21 + 201 + 129 = 15.272 cfs$

Trial #10 @ 637.0 Stone wall

Q = 3.5(142)9.4) $\frac{3}{2}$ +3.2(7.8)(5.5) $\frac{3}{2}$ +

3.2(35)(5.3) $\frac{3}{2}$ +3.2(3.0)(0.74) $\frac{3}{2}$ +

3.2(7.8)(5.5) $\frac{3}{2}$ +3.2(38)(1.0) $\frac{3}{2}$ +

3.2(25)(1.76) $\frac{3}{2}$ +2.8(170)(0.3) $\frac{3}{2}$ = 14323+322+1367+6+322+

294+187+78

= 16900 cfs

Use the above trials to develop a discharge rating curve for Paper Mill Dam.

					=								4		ià⁻
•			1								· · · · · · · · · · · · · · · · · · ·				000 81
											· · · · ·			:::1	-
			17:00										- : !-		000191
•) ()					
								- :		0					(4,000
-					\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\			1-4-4	- X	130					!
				* * * * * * * * * * * * * * * * * * * *											0 28 N
!	4			- : :					(-)	0)	4				10
				1 - 1 - 1						C/201					
2										Disc 2/5/79					8000 1986 1986
				++											3
-		12		1 1 1							****				184
		1 1											t		C C
					1	1 -1-1-1		11	7			1 1 1	5		. 0
				-				1	1.1.1.1			, 1).67	1	- 4
			4-4-4							1.1.2/ 1.1.2/ 1.1.2/			Spilling		000
			1			1		1.1.1		1		1	9.12		7
		1	1				· · ·		1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1		1				92
•	•	•			W.	7 GC	St.),-,5_	2	170	イヨー	=		•	•

PEPER Mill Dam

BREACH ANALYSIS - to determine

DENTATION hozard classification. Do

Dreach first at ormal Flow using

Water Resources Data For New

Hampshire and Vermont Water Year

976, U.S. Geological Survey Water
1976, U.S. Geological Survey Water
976, U.S. Geological Survey Water
9776, U.S. G

Qp, = %7 Wo Vo yo 3/2

Wb = breach width

g = 32.7 ffsec

yo = Pool elev. - u/s river bed

628.5' or 0.9' over spillway crest. Upstream
river bed shown on plants \$619.

© Paper Mill Dam $Wb = 142 \times 0.4 = 56.8' \approx 57'$ Yo = 628.5 - 619 = 9.5BREACH © NORMAL FLOW

From above equation: Q = 2806 GL

Q over dam other than breached area: $Q = 3.5 \times 95 \times 0.9\% = 254$ G

Total Breach Q (DRINKL) = 2806+254 = 3060 cfs

Use a typical cross section along the downstream reach from the dam to the road crossing at Monadnock Mills and establish a rating curve using the following Mannings Equation:

Length of reach = 2400' Elev. @ d/s toe = 617 Elev. @ end reach = 600 Slope = 0.007 Composite 'n' = 0.09

Trial # 1 Assume stage of 5'

Trial #2 Assume stage of 10'

Area = $\frac{1}{2}10(100 + 250)$ = $\frac{1750}{1750}$ WP = $\frac{1}{2}$ $\frac{1752}{1752}$ $\frac{1752}{1752}$ $\frac{1752}{1752}$ $\frac{1752}{1752}$

 $Q = \frac{1.49}{.09} \cdot 1750 \cdot 6.972^{3/3} \cdot .007^{1/2}$ Q = 8903 CFS

Trial # 3 Assume stars of 3' Area = 1/2 3(100+148) = 367.5 Up = 100+15+30-145 R=367.55-2.5345

 $Q = \frac{1.49}{1.09} \cdot 367.5 \cdot 2.5345^{3} \cdot .007^{1/2}$ $Q = 949 \quad \text{Cfs}$

Trial # 4 Assume stace of 7'
Area = 127 (100 + 205)
= 1067.5 ft2
WP = 100 + 36 + 70 = 206
P = 1067.5 = 5.182

 $Q = \frac{1.49}{1.05} \cdot 1067.5 \cdot 5.182^{3} \cdot .007^{2}$ = $\frac{4457}{100} \cdot \frac{1}{100} \cdot \frac{1}{10$

Use the above trials to establish a downstream x-section rating curve.

Total Brearly Q = 3060 cfs Stage = 5.7 feet

Antecedent discharge = 3.5.142.0.932 = 424 cfs Stage = 1.7 feet

in Increase in stage caused by breach @ normal flow would be & 4 feet.

Breach @ top of dam - 631.5'MSL Qp, = 3/27 Wb/g yo3/2 = 3/27.57 × 12.53/2

= 4236 cfs Q over don other than breached area: Q - CLH3/2

=35.85.3.9^{3/2}

= 2291 cfs

Total breach Q = 6527 Cfs

Stage @ 6527 = 8.5 feet

Outrodont discharge 3838 cfs = stare 6.2 feet.

Thurace in charge caused by Breach

Thorace in charge caused by Breach

Thorace in charge caused by Breach

On top of dom would be 2.3 feet.

CONCLUSIONS: Breach at top of dams would produce the worst drunstream damane. The breach at nomes flow conditions would stay in bank. Because of the abready with tailwater conditions at flow at top of dams and their the increase in the operation and their the increase in the acoster damant. Loops of life would be less, if any appreciable property and appreciable property. I among a portion to the maintenance of any and a portion to the maintenance.

			1		- 1				9	<u>-</u> .	9/11		
			1						77			 <u>.</u> .	C
			\						5				ì .
									Rat	+ 1	1		00
								1.1.1.1	707	; }-			Ċ
			1					3	(359)		1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		200,
								P	7				7£
						1-1-1-1		- 2		ļ.	1-1-1-1		ξ
				+ +			+ + + + + + + + + + + + + + + + + + + +		1 3 6	<u> </u>			3
) 0 0 0 0 0	130 Q	72			ر ن د ن د کا
					7								
				1					1				6
- !		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \							
						+					 		0.
				4 ·					1.71				† .
	: : : - :			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			1 - 2	 \ 					200
		1											,
													. 0001
	1 ,					I : II		:					-1

	 1		<u> : : ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; </u>	1	<u> </u>	D-11	<u> </u>	<u> </u>	9 9	1	0		-]
												1	.1 %
	 					-							
												11	8
- · :													.
· · · · · · · · · · · · · · · · · · ·	 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					1-1-1-1-1							000
• • • • • • • • • • • • • • • • • • •	 1-1-1-											1 1 1 1	Š
	T		; ;] ;					1-1-4-					Q
	1												0
	 ++										1-1-1-1		
								1 1 1	111111111111111111111111111111111111111				001
	 · · · ·				· · · · · ·								
													82
	· · · · · · · · · · · · · · · · · · ·								300	\ <u>\</u>	2/5/19		
									<u> </u>	Hazar	2		300
					-1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		.7\			70×	3		
.,									Dair	1-00 20 20	1 - 1		400
			<u>1</u>							0 0 0 1			
		1 - 1 - 2								ζ	<i>i</i> /		~

GATE CAPACITIES

Determine approximate gata capacities at top of dam - 6:1.5' Mar

Waste Gate

6'W x 8' H Invert - 620.6' MSL Centerline - 624.6' MSL

Q = CAVZgh ORIFICE EQUATION

Q=(0.7)(48)(V64.4.6.9) Q=708 3710 CFS

Head Gates

is controlled by the head gates capacity in the plant which is unknown.

APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

INVENTORY OF DAMS IN THE UNITED STATES

1 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	155	1410	1400	144.0	1 4 1.0 5	1410	1 5 1 1 2 5 1	1	1		144.0 a 145.4 a 145.	14 (10)	14 11 12 2 2 2 2 2 1 1 2 1 2 1 2 2 2 2
NAME OF IMPOUNDMENT NAME OF IMPOUNDMENT NAME OF IMPOUNDMENT NAME OF IMPOUNDMENT NAME OF IMPOUNDING CAPACITIES NAME	NAME OF IMPOUNDMENT (ii) (iii)	NAME OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDING CAPACITIES CACINE OF IMPOUNDING CAPACITIES CACI	NAME OF IMPOUNDMENT CONTINUE OF IMPOUNDING CAPACITIES CACHE OF IMPOUNDING CAPACITIES C	NAME OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDMENT CONTINUE OF IMPOUNDING CAPACITIES CACHE OF IMPOUNDING CAPACIT	NAME OF IMPOUNDMENT NAME OF IMPOUNDMENT NEAREST DOWNSTREAM NEW ONLY NOW	NAME OF INPOUNDMENT CITY CITY	NAME OF IMPOUNDMENT 190	NAME OF IMPOUNDMENT Construction BY Constr	NAME OF IMPOUNDMENT CONSTRUCTION BY COPERATION CO	NAME OF IMPOUNDMENT (ii) (iii)	NAME OF IMPOUNDMENT 19 19 19 19 19 19 19 1	NAME OF IMPOUNDMENT NAME OF IMPOUNDMENT	NAME OF INPOUNDMENT
NAME OF IMPOUNDMENT	NAME OF IMPOUNDMENT	NEAREST DOWNSTREAM CONTINUED CONTINU	NEAREST DOWNSTREAM	NEAREST DOWNSTREAM	NAME OF IMPOUNDMENT CONTINUE	NAME OF IMPOUNDMENT (1) (1) (1) (2) (3) (4)	NAME OF IMPOUNDMENT	NAME OF IMPOUNDMENT	NAME OF IMPOUNDMENT	NAME OF IMPOUNDMENT	TOTAL	NAME OF IMPOUNDMENT 10 10 10 10 10 10 10 1	NAME OF IMPOUNDMENT
O UK 2 T V F P O O O O O O O O O	TEST DOWNSTREAM	NEAREST DOWNSTREAM CONTINUED CONTINU	NEAREST DOWNSTREAM CONT.	NEAREST CONNSTREAM CONSTREAM CONSTRAIN CONSTRA	NEAREST DOWNSTREAM	NEAREST OWNSTREAM CONSTRUCTION CONSTRUCTION	TO DIK 2 TV F D	C OPERATION C C C C C C C C C	TO DE STAFE CONSTRUCTION CONST	TO DE 17 V F P TO DE 1 TO DE 1	AREST CON ARENT CON AREST CON AREST CON ARENT CON AREN	AREST CON ASTATE AND ASTA	TOWN - 2 TV F D
TEST DOWNSTREAM FROWDOW POPULATION POP	TEST DOWNSTREAM FROWING TO P. S.9 PROUNDING CAPACITIES PROUNDING CAPACITIES PROUNDING CAPACITIES P. S.9 P. S	NEAREST DOWNSTREAM COST	NEAREST DOWNSTREAM FROM CANDAM FORULATION	NEAREST DOWNSTREAM FROM CONTINUED	NEAREST DOWNSTREAM COUST COUNTY	NEAREST DOWNSTREAM FROM CONSTRUCTION CITY - TOWN - VILLAGE FROM COMMANDAM FORULATION CITY - TOWN - VILLAGE CONSTRUCTION BY CITY - TOWN - VILLAGE CITY - CITY	AREST DOWNSTREAM	AREST DOWNSTREAM 1 TOWN - VILLAGE (A)	AREST DOWNSTREAM FROWSTREAM POPULATION (**)	AREST DOWNSTREAM FROM POPULATION (**)	AREST DOWNSTREAM FROWSTREAM POPULATION (*)	AREST DOWNSTREAM FROM CANADAM POPULATION 1.7 - TOWN - VILLAGE 0 0.59	AMEST DOWNSTREAM FROM FR
TEST DOWNSTREAM FROWDOW POPULATION FROWING THE FROWDOW POPULATION FROWING THE FROW POPULATION FROW PETER FROM PETER FROM PETER FROM PETER FROM PETER FROW PETER FROM PETER F	TEST DOWNSTREAM FROWDOM POPULATION	NEAREST DOWNSTREAM ERONGAM POPULATION	NEAREST DOWNSTREAM ERONS POPULATION	NEAREST DOWNSTREAM ERONSAM POPULATION	NEAREST DOWNSTREAM ENOUGH FROM POPULATION	NEAREST DOWNSTREAM FROM FORULATION	AREST DOWNSTREAM FROM POPULATION	TOWN - VILLAGE	The townstream The construction The construct	The townstream The	The townstream The control The control	The townstream The construction The construct	ATEST DOWNSTREAM FROM CANADAM POPULATION (3)
(a) (b) (b) (c) (c) (c) (d) (d) (d) (d) (d) (d) (d) (d) (d) (d	(3) (ACURANTES 151 NEW FED & PHV/FED (ACURANTES) 151 NEW FED (ACURANTES) 151 NEW FED	11 S S S S S S S S S S S S S S S S S S	11 So 22-25 E 2 1 - 3 2 4 5 5 6 5 5 5 5 5 7 5 7 8 8 8 8 8 8 8 8 8 8 8 8	11 So So So So So So So	(A) (A) (A) (B) (B) (B) (B) (B) (B) (B) (B) (B) (B	MOUNDING CAPACITIES	MCOUNTRING CAPACITIES	(A)	(A)	MOUNTOURDING CAPACITIES	(%) (%) (%) (%) (%) (%) (%) (%)	(A)	10 659 10 659 10 10 10 10 10 10 10 1
MACHINE CAPACITIES 151 DES FED & PHV/FED	(Achter 1)	(A)	(%) (%) (MC) (MC) (MC) (MC)	(A) (A) (A) (B) (B) (B) (B) (B) (B) (B) (B) (B) (B	(a) (b) (c) (c)	(ACATALUS) CAPACITIES (ACATALUS) (ACATACITIES So	(%)	(A) IMPOUNDING CAPACITIES (A)	(%) (%)	(%) (%) (%) (%) (%) (%) (%) (%) (%) (%)	(A)	(%) MYOUTHOING CAPACITIES 1 S 1	(A) IMPOUNDING CAPACITIES (A)
MACHINIONG CAPACITIES 151 DES FED & PRYFED	MACHEMAN AND MACHE TO A PROFED OF SO	HEAD INFOLUTIONG CAPACITIES HEAT (ACATAMET) CACACAMET 2 3151 DE FED 9 PRV/FED 13 SA	14 (Achtemen) (Achtemen) 25 FF N N N N N N N N N N N N N N N N N N	HEAD MANUAL CAPACITIES 1.4 (ACRIMINAL CACREMET) CACREMET ST. N.			IMPOUNDING CAPACITIES	IMPOUNDING CAPACITIES	IMPOUNDING CAPACITIES	IMPOUNDING CAPACITIES			IMPOUNDING CAPACITIES
	2 2 5 3 4 5 6	5. Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	25 N N N N N N N N N N N N N N N N N N N	7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7	118 SO	So	0 12: 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(#)	ODERICA COLORER	S	SO	SO	0 OPER (10 to
VE 3 22-SE D. (a) VE CAPACITY LED PROGNIN ED.	VE 3 22-3E D TRECAPACITY VER CAPACITY LED PROGNED	APACITY PHOUSE	APACITY PROCESSED			Stra C.	(a)	(ii) Anti-tra C	OPERATION	(9) (9) (9) (9)	OPERATION AUTHORITY FOR IN	OPERATION AUTHORITY FOR IN 12 92-357	OPERATION AUTHORITY FOR IN PL 92-35/7
PAGIN	PACITY PROJECT	PACITY PHCK (V. V.) E D	PACITY PHON WOLD				(8)	OPERATION	OPERATION	OPERATION	OPERATION (8) AUTHORITY FOR IN	OPERATION AUTHORITY FOR IN 12 92-351	OPERATION (b) AUTHORITY FOR IN

HEPRODUCED / TISCHERNIEW LENGINSS

FILMED

8-85

DTIC