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Cold Regions Research & Engineering Laboratory

# Reverse phase HPLC method for analysis of TNT, RDX, HMX and 2,4-DNT in munitions wastewater



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For conversion of SI metric units to U.S./British customary units of measurement consult ASTM Standard E380, Metric Practice Guide, published by the American Society for Testing and Materials, 1916 Race St., Philadelphia, Pa. 19103.

Cover: Liquid chromatogram of a typical explosive mixture.

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# Reverse phase HPLC method for analysis of TNT, RDX, HMX and 2,4-DNT in munitions wastewater

T.F. Jenkins, C.F. Bauer, D.C. Leggett and C.L. Grant

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| Explosives Test and evaluation<br>HMX TNT<br>Interlaboratory test Water pollution control<br>RDX<br>20 ABSTRACT (Continue on reverse of the increases and identify by block number)<br>An analytical method was developed to determine the concentrations of F<br>wastewater. The method involves dilution of an aqueous sample with an e<br>solvent mixture, filtration through a 0.4-µm polycarbonate membrane and<br>Reverse-phase, high-performance liquid chromatography using an LC-8 col<br>lytes, their degradation products, and impurities expected in wastewater m<br>compositions. An eluent of 50% water, 38% methanol and 12% acetonitri<br>TNT from each other and the potential interferents. The method provided   | IMX, RDX, TNT and 2,4 DNT in munitions<br>equal volume of methanol-acetonitrile<br>I analysis of a 100- $\mu$ L subsample by<br>lumn. Retention times of these four ana-<br>natrices were determined for two eluent<br>ile successfully separated HMX, RDX and<br>d linear calibration curves over a wide range   |
| DN I Statistical tests<br>Explosives Test and evaluation<br>HMX TNT<br>Interlaboratory test Water pollution control<br>RDX<br>ADSTRACT (Continue on reverse state H increasery and identify by block number)<br>An analytical method was developed to determine the concentrations of F<br>wastewater. The method involves dilution of an aqueous sample with an e<br>solvent mixture, filtration through a 0.4-µn polycarbonate membrane and<br>Reverse-phase, high-performance liquid chromatography using an LC-8 col-<br>lytes, their degradation products, and impurities expected in wastewater m<br>compositions. An eluent of 50% water, 38% methanol and 12% acetonitrit<br>TNT from each other and the potential interferents. The method provided<br>of concentrations. Detection limits were conservatively estimated to be 20<br>1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE CONC. | IMX, RDX, TNT and 2,4 DNT in munitions<br>equal volume of methanol-acetonitrile<br>analysis of a 100- $\mu$ L subsample by<br>lumn. Retention times of these four ana-<br>natrices were determined for two eluent<br>ile successfully separated HMX, RDX and<br>d linear calibration curves over a wide range<br>6, 22, 14 and 10 $\mu$ g/L for HMX, RDX, TNT |

### 20. Abstract (cont'd).

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2.4-DNT respectively. Analytical precision was estimated at  $\pm$  3.4, 3.3, 4.4 and 4.6 µg/L. A ruggedness test involving the major manipulative steps in the procedure indicated that use of glass sampling containers, the portion of filtrate chosen for analysis and a carefully measured sample-to-organic-solvent ratio was necessary to obtain consistent analytical results. The method was tested with munition wastewater from several Army ammunition plants and found to perform adequately for load and pack wastewaters, wastewater from HMX/RDX manufacture and contaminated groundwater. An interlaboratory test of the method was conducted with nine participating organizations, including laboratories at four Army ammunition plants, the EPA's Environmental Monitoring and Support Laboratory, three Army research organizations and a university. For the four analytes collectively, the analytical accuracy was within 5%, the intralaboratory precision (repredatbility) was 5 to 9% based on the average of duplicate injections, and the interlaboratory precision (reproducibility) was 7 to 10%. This evaluation excluded about 10% of the data, which were identified as outliers. 

#### PREFACE

This report was prepared by Thomas F. Jenkins and Daniel C. Leggett, Research Chemists, Earth Sciences Branch, Research Division, U.S. Army Cold Regions Research and Engineering Laboratory and Dr. Christopher F. Bauer, Associate Professor, and Dr. Clarence L. Grant, Professor, Chemistry Department, University of New Hampshire (UNH), Durham, New Hampshire.

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6. U.S. Environmental Protection Agency, Environmental Monitoring and Support Laboratory; Dr. D. Forest, analyst/supervisor.

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P. Butler obtained the data for suspended solids, pH and total organic carbon used in the filtration-recovery study.

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### ABBREVIATIONS

| ААР         | Army Ammunition Plant  |
|-------------|--|
| AEHA        | Army Environmental Hygiene Agency  |
| ANOVA       | Analysis of Variance   |
| GC-ECD      | Gas Chromatographic-Electron Capture Detector  |
| GC-FID      | Gas Chromatographic-Flame Ionization Detector  |
| GOCO        | Government-Owned, Contractor-Operated  |
| LCWSI       | Large Caliber Weapons Systems Laboratory (U.S. Army)                                     |
| MS          | Mass spectroscopy  |
| NBS         | National Bureau of Standards   |
| RP-HPLC     | Reverse Phase, High Performance Liquid Chromatography                                    |
| RSD         | Relative Standard Deviation  |
| SARM        | Standard Analytical Reference Materials  |
| TLC         | Thin-Layer Chromatography  |
| USEPA, EMSL | U.S. Environmental Protection Agency, Environmental<br>Monitoring and Support Laboratory |
| UV          | Ultraviolet  |

#### SUMMARY

This report documents the experiments conducted during the development and collaborative testing of a Reverse-Phase, High-Performance Liquid Chromatography (RP-HPLC) method for HMX, RDX, TNT and 2,4-DNT in water. This method utilizes an LC-8 column with an eluent of 50% water, 38% methanol and 12% acetonitrile. Retention times for HMX, RDX, TNT and 2,4-DNT were 3.2, 4.1, 7.0 and 7.8 minutes, respectively, at an eluent flow rate of 1.5 mL/minute. Measurement of the retention times of expected matrix contaminants and degradation products indicated that none would interfere with the determination of HMX, RDX or TNT. The presence of 4-amino-2,6-dinitrotoluene (a microbial degradation product of TNT) 2,4,5-TNT and 2,6-DNT could interfere with 2,4-DNT determination since they all elute within 0.2 minutes of 2,4-DNT.

Water samples were analyzed as follows. A 10-mL aqueous sample was diluted with 10 mL of a mixed solvent composed of 76% methanol 24% acetonitrile (V/V) in a scintillation vial. The sample was capped, shaken and allowed to stand for 15 minutes. The sample was then filtered through a 0.4- $\mu$ m Nuclepore polycarbonate membrane into a second scintillation vial. A 100- $\mu$ L subsample of this solution was then injected into an LC-8 column and eluted with 1.5 mL/minute of 50/38/12% water/methanol/acetonitrile (V/V/V). The column effluent was directed to a fixed wavelength, 254-nm UV detector and the response measured with a digital integrator.

Detector response was linear from the detection limits to 5580  $\mu g/L$  for HMX, 6200  $\mu g/L$  for RDX, 4200  $\mu g/L$  for TNT and 1600  $\mu g/L$  for DNT. The linear range can be extended by use of smaller injection volumes. Using peak height measurements and linear regression analysis, analytical sensitivity was established for HMX, RDX, TNT and 2,4-DNT at  $5.0 \times 10^{-3}$ ,  $6.8 \times 10^{-3}$ ,  $1.1 \times 10^{-2}$  and  $1.4 \times 10^{-2}$  absorbance units per mg/L, respectively, for 100- $\mu$ L injection volumes.

Since removal of suspended solids is necessary to protect expensive HPLC columns, experiments were conducted to assess the degree of loss during filtration by adsorption on various types of filters. Nuclepore 0.4- $\mu$ m polycarbonate membranes were found to be well suited for this application. Dilution of sample with an equal volume of methanol-acetonitrile solution prior to filtration was found to result in quantitative recovery of spikes of 2,4-DNT, TNT and RDX. There were small losses of HMX, which appeared to be proportional to the concretentation of suspended material present in the sample. Even in the worst case tested, over 92% of the spiked HMX was recovered.

Detection limits of this method were obtained by the method of Hubaux and Vos (1970) using data from peak area measurements from a digital integrator. The values of 26  $\mu$ L for HMX, 22  $\mu$ g/L for RDX, 14  $\mu$ g/L for TNT and 10  $\mu$ g/L for 2,4-DNT are considered to be conservative, and are sufficient to meet current and projected discharge limits. Analytical precision was estimated at  $\pm 3.4 \mu$ g/L for HMX,  $\pm 3.3 \mu$ g/L for RDX,  $\pm 4.4 \mu$ g/L for TNT and  $\pm 4.6 \mu$ g/L for DNT at concentrations below 245  $\mu$ g/L, 136  $\mu$ g/L, 77  $\mu$ g/L and 64  $\mu$ g/L respectively.

A ruggedness test was conducted to determine the sensitivity of the method to small deviations in the analytical protocol. The results indicated that use of glass containers rather than polyethylene was desirable, particularly for 2,4-DNT. Accu-

rate 2,4-DNT analysis also required consistency in the filtration procedure, washing the filter with the first 10-mL portion of sample-organic solvent solution and using the second 10-mL portion for analysis. Care was also found to be very important in the volumetric measurements used to dilute the sample with the organic solvent. The solvent strength affected the measured HMX and RDX peak areas over and above the effect expected because of the resulting differences in analyte concentration.

Munitions wastewaters were collected at four Army ammunition plants. These included wastewater from a load and pack facility and an RDX-HMX manufacturing line and also an RDX contaminated groundwater. The method appeared to be adequate for analysis of all three types of matrices.

Results of a collaborative study, where nine laboratories each analyzed four aqueous matrices spiked with the analytes, showed that the overall performance of the RP-HPLC method is very good for the concentration ranges studied. The evidence supporting this evaluation is summarized below:

1. For DNT, RDX and HMX the median "found" concentrations are within 3% of the true values. For TNT the difference is within 5%. Considering that the "true" values themselves are necessarily somewhat uncertain, the overall accuracy is very good.

2. The repeatability, based on duplicate injections of each of two aliquots, is about 7, 9, 15 and 10  $\mu$ g/L for DNT, TNT, RDX and HMX respectively. These values represent percent relative deviations on the order of 5 to 9%. If single injections were used the repeatabilities would be inflated by a factor of 1.414 (square root of 2).

3. Reproducibilities for each analyte are about 6, 21, 40 and 44% greater than repeatabilities for DNT, TNT, RDX and HMX respectively. This gives percent interlaboratory deviations, based on average concentration examined, of about 7% for DNT, RDX and HMX and 10% for TNT. The most likely source of these differences between laboratories is the calibration of the instrumental response.

4. Recoveries of a given analyte were similar regardless of matrix. Overall, DNT and RDX were recovered quantitatively, and TNT and HMX showed small losses of about 5%.

The standard deviation of replication was independent of concentration in the concentration ranges examined in this collaborative study. Because of this, the relative standard deviations for RDX and HMX are better than those of DNT and TNT when in fact RDX and HMX have poorer absolute precisions.

Valid statistical analysis required rejection of about 10% of the individual data values. Even where a substantial number of outliers was identified, the repeatabilities for those analytes most effected (RDX and HMX) grew from 5% relative to only 12% relative when no values were eliminated. This larger relative deviation is still quite acceptable for analysis at the microgram-per-litre level.

At this point we are confident in recommending that this HPLC method be implemented as a means of monitoring munitions plant wastewaters and natural waters for DNT, TNT, RDX and HMX at the submilligram-per-litre level. The accuracy and reproducibility in the analysis of real environmental samples have proven to be adequate for this task.

## **REVERSE PHASE HPLC METHOD FOR ANALYSIS OF TNT, RDX, HMX AND 2,4-DNT IN MUNITIONS WASTEWATER**

T.F. Jenkins, C.F. Bauer, D.C. Leggett and C.L. Grant

## **PART 1. METHOD DEVELOPMENT**

#### **INTRODUCTION**

#### Monitoring requirements

One of the Army's most serious water pollution problems is the disposal of wash waters used to clean equipment and interior surfaces at TNT and RDX manufacturing and demilitarization facilities. It has been estimated that up to a half million gallons (190,000,000 L) of this type of wastewater is generated from a single production line each day (Walsh et al. 1973). Since this washdown process is necessary for safe operation, it is unlikely that this waste stream will be eliminated in the near future.

Current practice is to collect wash water from these processing operations in a holding tank and pump the wastewater through a carbon adsorption column. This procedure is capable of reducing TNT and RDX levels to the low parts-per-billion range. The treated wastewater is then typically discharged to a nearby surface stream. These point discharges are subject to state and federal National Pollution Discharge Elimination System (NPDES) permits, which generally limit the acceptable concentrations of TNT and RDX (2,4,6trinitrotolune and hexahydro-1,3,5-trinitro-1,3,5triazine [see Appendix B]). Carbon adsorption technology can at present meet discharge limitations, but these carbon columns have finite lifetimes. Eventually, breakthrough occurs and regeneration or replacement is necessary.

To satisfy permit requirements and to check on system performance, daily monitoring of wastewater from the carbon adsorption columns is generally necessary during manufacturing. Current monitoring requires separate determinations for TNT and RDX, the two most common explosives used by the U.S. Army.

Additionally, monitoring for HMX (octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazine [see Appendix B]) also an Army explosive and a common impurity in RDX and 2,4-DNT (2,4-dinitrotoluene [see Appendix B])-a low-level impurity in TNTmay also be required in the near future. At present no standard analytical method is available for TNT, RDX or HMX. Hence, individual Army installations have developed their own procedures, which differ widely in their detection limits, specificity and precision. Since 2,4-DNT is one of EPA's priority pollutants, a standard method involving solvent extraction and gas chromatographic analysis has been developed for its determination (Federal Register 1979). No information is available on the suitability of this method for simultaneous determination of TNT, RDX and HMX.

#### Objectives

The first objective of this effort was to choose from among the various alternatives for measurement of TNT, RDX, HMX and 2,4-DNT the method best suited for compliance monitoring requirements at U.S. Army Ammunition Plants (AAP). The method of choice must satisfy the following requirements:

1. It must have detection limits sufficiently low to satisfy current and future monitoring requirements for point discharges.

2. It must be rapid to enable quick remedial ac-

| Installation  | Max. discharge<br>concentrations<br>(mg/L)* | Monitoring<br>requirement | Analytical<br>method       |
|---------------|---|---------------------------|----------------------------|
| Lone Star AAP | TNT, 0.3<br>RDX, 15                         | l grab/day                | Solvent extraction, GC-FID |
| Louisiana AAP | TNT <sup>†</sup> , 2.0                      | 1 composite/day           | Silas Mason Colorimetric   |

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2 composite/mo.

**RD-HPLC** 

RP-HPLC, or GC-FID

RP-HPLC, or GC-ECD

Table 1. Survey of discharge limits and analytical methods at Government-owned, contractor-operated installations in 1981.

Maximum daily average as specified on NPDES permit.

**TNT, 0.5** 

RDX, 15

..

† TNT and nitrobodies.

\*\* None specified on permit.

tion if discharges are found to be in violation of discharge limits.

Iowa AAP

Holston AAP

Radford AAP

3. It should be precise and accurate so that the waste stream can be characterized using a minimum number of replicates.

4. It should be free of interferences from the common contaminants in AAP waste streams, including decomposition products and impurities commonly found in the explosives.

5. It should allow measurement of all four of the analytes in the same procedure since they will often occur together because of the types of formulations typically used in explosives production.

6. It should be as inexpensive as possible to implement, on both an initial capital cost and a per sample basis.

A second objective of this study was to conduct a collaborative test of the developed method to determine how well it works in a variety of laboratories. This was to include several laboratories that support munitions manufacturing operations, where monitoring of discharges for NPDES permit compliance is required.

#### **Possible analytical approaches**

Two parallel approaches were used to assess which analytical methods were best suited for the above analytes in a water matrix. First, a literature search was conducted which identified the methods that had been reported in the open literature as well as in published government reports. The second was by personal site visits to five AAPs and several government laboratories that had extensive experience with these types of analyses.

A summary of some of the most important information from the five AAPs, including their discharge limits, monitoring requirements and the analytical methods in use, is presented in Table 1. Clearly, the discharge limits vary somewhat from site to site primarily because of their location in different states and EPA regions and because of the lack of a nationwide discharge standard. At present both TNT and RDX are limited in most permits but HMX and DNT are not. Analytical approaches in use include a colorimetric method, Reverse-Phase, High-Performance Liquid Chromatography (RP-HPLC), and solvent extraction followed by Gas Chromatographic analysis using either a Flame Ionization Detector (GC-FID) or Electron Capture Detector (GC-ECD). Discussions with analytical chemists at each installation resulted in a consensus that for compliance monitoring, a direct approach such as RP-HPLC was the most desirable if sufficiently low detection limits could be obtained. While it is difficult to predict the discharge limits for these substances that may be set in the future, current research at the U.S. Army Medical Bioengineering Research and Development Laboratory indicates that limits as low as 300  $\mu$ g/L, 920  $\mu$ g/L, 120  $\mu$ g/L and less than 40µg/L for RDX, HMX, DNT and TNT, respectively, are possible.\*

<sup>\*</sup> Personal communication with J. Barkley, U.S. Army Medical Bioengineering Research and Development Laboratory, Fort Detrick, Maryland.

Besides these five APPs, we also consulted Dr. John Walsh at U.S. Army Natick Laboratories and Dr. Richard Bishop from the U.S. Army Environmental Hygiene Agency. Both of these individuals had extensive analytical experience in the determination of the analytes from their research activities. Again the recommendation was RP-HPLC because of the difficulty associated with GC analysis of RDX and HMX, primarily attributable to thermal degradation at the temperatures required to volatilize these substances in the injector. Experience in our own laboratory also indicated that RP-HPLC could successfully be used to determine these four analytes in a single analysis (Leggett, in prep.).

Analytical methods for TNT, RDX, HMX and DNT in water are generally modifications of procedures developed for analysis of the explosives themselves. Yinon and Zitrin (1981) give an extensive review of these methods as they apply to the analysis of intact explosives and post explosion residues.

The approaches that have received attention for trace analysis of these substances in water are:

- 1. Direct colorimetric analysis
- 2. Thin-layer chromatography
- 3. Gas-liquid chromatography with a variety of detectors
- 4. High-performance liquid chromatography, normal and reverse-phase.

#### Colorimetric analysis

The production of characteristic colored products from alkaline hydrolysis of nitroaromatics has been known since the 19th century (Yinon and Zitrin 1981). Application of this concept for the analysis of trace levels of TNT in munitions wastewater was reported by Mudri (1968). In this method a sample of wastewater is diluted with an aqueous sodium sulfite-sodium hydroxide solution. Absorbance measurements at 500 nm are used to detect the extent of color development, which was found to be linearly related to TNT concentrations from less than 1 to 20 ppm. Recovery studies indicated that the procedure was accurate to  $\pm 10\%$ but possible interferences from other nitroaromatics or nitramines were not studied.

Jurinski et al. (1975) reported an automated colorimetric procedure for TNT analysis in wastewaters. In this method, the sample was diluted with 15% KOH and the transmittance at 440 nm measured. They found that the method obeyed Beer's law and was applicable in the 1-80 ppm range. No interference was found for mono- or dinitrotoluenes or RDX; however, other isomers of TNT, TNB (1,3,5-trinitrobenzene [see Appendix B]) and Tetryl (methyl-2,4,6-trinitrophenylnitramine [see Appendix B]) gave positive responses.

A modification of the colorimetric approach for TNT determination has been reported by Heller et al. (1977). A colored reaction product is produced by alkaline hydrolysis and immobilized on a quaternary ammonium ion-exchange resin that had been saturated with a fluorescent dye. The reduction in fluorescence when the immobilized resin is excited with UV radiation is proportional to concentration of TNT. Although it is not suited for precise laboratory determination of TNT, this method offers an approach to detecting breakthrough of TNT from activated carbon treatment columns. This concept has been extended to the development of portable detection tubes (Heller et al. 1982), which detect TNT at concentrations as low as 100  $\mu$ g/L in fresh water. But these tubes are not suitable for RDX, HMX or DNT. None of the reported colorimetric procedures are capable of simultaneous measurement of these four analytes.

#### Thin-layer chromatography

Thin-layer chromatography (TLC) has been evaluated for use in determining some of these analytes in water and sediment. Hoffsommer et al. (1972) describe a method in which TNT and RDX are extracted from sediment with benzene. The solvent is removed by evaporation and the residue is dissolved in a small volume of benzene; this solution is spotted on a TLC plate and developed with a hexane-acetone solution. TNT and RDX appear as dark spots under 254-nm UV light. No data on detection limits, precision or accuracy are presented.

Glover and Hoffsommer (1973) report on the use of TLC to determine HMX and RDX in munitions wastewater. The water solution is extracted with benzene, the extract evaporated to dryness, taken up in acetone and spotted on a silica gel plate. The plates are developed with benzeneacetone and HMX and RDX are separated and detected as dark spots under a 254-nm UV light. Detection limits of 20  $\mu$ g/L are estimated for HMX using this procedure, with analytical accuracy of about  $\pm 10\%$  in the 0.1- to 1.0-mg/L range.

Epstein et al. (1977) have used TLC to qualitatively characterize TNT wastewaters from several AAPs. TLC was very powerful in separating the many individual components, particularly in wastewater from the manufacture of TNT. Quantitation, however, was accomplished by other means. While solvent extraction followed by TLC analysis appears to be sufficiently sensitive, the

semi-quantitative nature of TLC reduces its utility when precise and accurate quantitative analysis is needed.

A method for the determination of TNT in water by conversion to nitrate has been reported by Leggett (1977). Recovery was near 100% for TNT, but potential interference from other nitroaromatics or nitramines was not determined. Therefore, this method does not lend itself to determination of individual components. Since the various substances have different levels of toxicity and thus have different discharge limits, a total analysis is not sufficient.

A method for TNT analysis in water by differential pulse polarography has also been reported (Conley and Mikucki 1976). The potential was swept cathodically, reducing the three nitro groups sequentially at -0.28, -0.45 and -0.61 V versus the standard calomel electrode. Concentrations below 100 ppb can be analyzed directly. No information was presented, however, on whether the presence of RDX, HMX or DNT in the water would interfere with TNT analysis.

#### Gas-liquid chromatography

A number of researchers have reported gas chromatographic procedures for DNT, TNT and RDX. A method by Goerlitz and Law (1975) has been listed as the method of choice for TNT and RDX in water by the National Handbook of Recommended Methods for Water-Data Acquisition (U.S. Dept. of Interior 1977). This method involves four sequential extractions of water with benzene, combination of the extracts, volume reduction to 0.5 mL with a Kuderna-Danish evaporator, column chromatographic clean-up, and analysis of the column eluate using Gas Chromatography with an OV-17 column and an Electron Capture Detector (GC-ECD). The detection limits for this procedure are well below 1  $\mu$ g/L for both TNT and RDX with recovery of 95  $\pm 15\%$  for TNT and 85  $\pm 10\%$  for RDX.

A similar method for DNT has been adopted by the EPA (Federal Register 1979). This procedure includes three sequential extractions with methylene chloride, solvent exchange with toluene, evaporative concentration, cleanup by column chromatography and analysis by GC-ECD using an OV-17 column. A detection limit of  $0.06 \,\mu g/L$  for 2,4-DNT was reported with baseline separation between 2,4- and 2,6-DNT. Experience in our own laboratory and in others has indicated that the DNTs can be separated easily from TNT using GC (Murrmann et al. 1971).

Determination of HMX by GC has also been ac-

complished using a fused silica capillary column coated with OV-101. This is in contrast to earlier reports that RDX could be determined in an HMX matrix with no elution of an HMX peak (Rowe 1967). Personal discussions with a number of experjenced analysts indicate that measurement of HMX by GC methods was difficult because of significant and nonreproducible decomposition at the temperatures required to volatilize the compound. Douse (1981) reported that the peak shape and response for HMX was improved using temperature programming. The lower analytical precision (10%), compared to other analytes, indicates that HMX was probably thermally degrading even in this work. Similar problems were encountered with RDX, which would apparently chromatograph acceptably for long periods and then, for no explainable reason, start erratically decomposing during analysis.

A number of other papers have also presented GC-ECD methods for analysis of DNT, TNT and its microbial metabolites, the aminodinitrotoluenes and diaminonitrotoluenes (Hoffsommer and Rosen 1972, Glover et al. 1977, Hashimoto et al. 1980). These methods differ primarily in the choice of extraction solvent and the specific column used for analysis. Jurinski et al. (1975) and Spanggord et al. (1982) present similar methods using an FID detector rather than ECD.

Krull et al. (1983) address the problem of potential interferences in measurement of various dinitrotoluenes by using ECD and photoionization detectors, and in documenting response ratios. This technique is very valuable for trace analysis of groundwater or surface waters but is probably unnecessary in analysis of the wastewater matrix, particularly following carbon column cleanup. GC/MS methods for unequivocal identification of DNT and TNT and their metabolites have also been reported (Pereira et al. 1979, Weinberg and Hsu 1983).

#### High-performance liquid chromatography

The use of Reverse-Phase, High-Performance Liquid Chromatography (RP-HPLC) for analysis of TNT wastewaters was first reported by Walsh et al. (1973). Walsh was able to separate TNT from 2,4-DNT using a C-18 column with 10:90 V/V acetonitrile/water under isocratic conditions. Direct injection of 10  $\mu$ L of wastewater permitted concentration estimates in the low microgramsper-litre range. No figures of merit with respect to precision, percent recovery or detection limits were provided.

Doali and Juhasz (1974) reported on the use of

normal phase HPLC for the analysis of several explosive formulations. Conditions were provided for the separation of TNT and DNT and also for RDX and HMX, but not for all four in one matrix. Because this paper describes methods suitable for analysis of solid explosive, rather than trace levels in water, no information on detection limits was provided. Since normal phase HPLC typically uses non-polar elution solvents, an extraction step would be required, unlike reverse phase where aqueous solutions can be injected directly.

Stanford (1977) reported a RP-HPLC method that separated 2,4,6-TNT from the various isomers of DNT, and TNT from RDX in water. This method uses a C-18 column and various elution solvents of ethanol/water, acetonitrile/water and methanol/acetonitrile/water. For injections of 100  $\mu$ L, detection limits of 50-250  $\mu$ g/L were reported using a UV detector at 230 nm. Stanford observed a reversal in elution order for TNT and DNT between methanol/water and acetonitrile/ water whict he attributed to a specific interaction between acetonitrile and nitroaromatics.

Stidham (1979) described a RP-HPLC method for the determination of nitramines and TNT from a RDX-HMX manufacturing operation. Using a gradient elution technique and a ternary solvent mixture of methanol/acetonitrile/water, he achieved detection limits of less than 65  $\mu$ g/L with direct injection of 700  $\mu$ L of aqueous sample. A C-8 column was used with UV detection at 230 nm. This method achieves good separation for HMX, RDX and TNT as well as SEX (octahydro-1-(N)-acetyl-3,5,7-trinitro-1,3,5,7-tetrazine [see Appendix B]) and TAX (hexahydro-1-(N)acetyl-3,5-dinitro-1,3,5-triazine [see Appendix B]), two major impurities in RDX-HMX manufacture. Stidham measured UV spectra of TNT, RDX, HMX, TAX and SEX to choose the best wavelength for detection, which generally was in the 240- to 245-nm region for these five compounds. Detailed assessments of analytical precision were presented at concentration ranges from 50 to 10 mg/L. Precision was generally better than 10%. Recovery of spiked samples indicated that the inaccuracy was generally better than  $\pm 10\%$ . Stidham reported that direct injection with RP-HPLC gave superior performance with respect to accuracy and precision compared to methods that required sample extraction or preconcentration by "... avoiding tedious analytical steps and minimizing potential degradation or sample loss."

Bratin et al. (1981) compared the limits of detection obtainable using UV detection at 254 nm versus electrochemical detection with RP-HPLC for HMX, RDX, TNT and DNT. A gold-mercury amperometric detector improved detection limits by factors of 3.5-5.1 at equivalent signal-to-noise ratios. If very low detection limits are required this detector shows great promise; however, it is not currently in common use.

Hoffsommer et al. (1981) compared UV detection at 200 nm versus 254 nm for TNT, RDX, HMX and DNT and found an improvement in detection limits of only about a factor of two. Detection limits of about 200 g/L were found for injection volumes of  $30 \ \mu$ L. Lakings et al. (1981) reported detection limits of 89  $\mu$ g/L for RDX and 50  $\mu$ g/L for TNT and DNT for a similar RP-HPLC method using UV detection at 254 nm and 100- $\mu$ L injection volumes.

An innovative use of electron capture detection with HPLC was reported by Krull et al. (1981). Detection limits are expected to be very low because of the extreme sensitivity of the ECD for nitro-containing aromatics (e.g. TNT, DNT); but because it requires the analyte to be volatilized, it suffers the same problems as GC analysis, i.e., the very low vapor pressures and thermal instability of HMX and RDX. Use of ECD with HPLC is still in the research stage and is not currently in common use.

West<sup>•</sup> has also reported a RP-HPLC method for RDX, TNT and DNT in munitions wastewaters: 500  $\mu$ L of filtered wastewater is injected into an ODS column eluted with 30/70 (V/V) methanol/water, and the column effluent is analyzed by UV at 254 nm. West obtained detection limits of 3  $\mu$ g/L for RDX, 5  $\mu$ g/L for TNT and 7  $\mu$ g/L for DNT. Subsequent discussions with aim indicated that for routine analysis, however, injection volumes should probably be reduced somewhat.

In some subsequent studies within our own laboratory, RP-HPLC has been successfully used to determine TNT, RDX, HMX and DNT in leachate from PVC pipes (Parker et al., in prep.), in soil and sediment extracts (Cragin et al., in prep.), in plant tissue digests<sup>†</sup> and in sorption isotherm experiments with bentonite drilling muds (Leggett and Foley, in prep.)

#### Assessment of alternatives

Of the alternative methods, clearly the two best suited for compliance monitoring are GC-ECD

<sup>•</sup> Personal communication with Dr. J. West, Louisiana AAP. 1982.

<sup>†</sup> Personal communication with D. Leggett and B. Foley, CRREL, 1984.

and RP-HPLC. GC-ECD is particularly attractive because of its sensitivity and selectivity for nitroaromatics and nitramines. Detection limits of better than  $1 \mu g/L$  for all four analytes are achievable using this approach, which will certainly meet all current and projected needs. GC-ECD instrumentation is currently available in most Army and GOCO (government-owned, contractor-operated) installations so little capital cost would be required to implement this method.

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シャクトンストロージングシストレスについて、「日本日本のシャンシント」となったのであるのののです。

GC methods, however, require extraction from the water matrix into a nonpolar organic solvent. Partition coefficients between nonpolar solvents and water for these substances are not very favorable, particularly for RDX and HMX (Leggett and Foley, in prep.), and hence, a number of sequential extractions would be required to approach complete recovery. Following extraction, the solvent must be concentrated by evaporation prior to analysis. This entire procedure is very time consuming, resulting in a turn-around time of at least several hours between delivery of sample to the laboratory and availability of the data. This is clearly not desirable if the values are not within compliance limits and discharge has continued while the analyses are underway. In addition the large number of exacting steps will reduce analytical precision unless very highly trained technicians are available, a situation only rarely true for compliance monitoring activities. GC analysis also requires that the analytes be thermally stable within the injector and analytical column. This is a problem for HMX, which has a very low vapor pressure and is thermally labile, and to a lesser extent for RDX and TNT, which have shown unpredictable thermal instability problems.

**RP-HPLC** is attractive because aqueous solutions can be analyzed directly, without the necessity of solvent extraction. Good detection limits can be obtained without sample preconcentration, because, relative to GC, large volumes can be injected. The ability to analyze aqueous solutions directly allows a turn-around time of 30 minutes or less, which is very desirable for discharge monitoring. HPLC instrumentation is currently available at most AAPs.

Several detection concepts have been reported for these analytes in RP-HPLC. Electro-chemical detectors and ECDs are both very sensitive, but are not readily available or routinely used. Detection by UV is somewhat less sensitive for these analytes, but is available on most HPLC equipment. The most common UV detector is a single wavelength 254-nm detector, although variable wavelength systems are becoming more common. For reliability, however, the 254-nm UV detector is excellent. All four analytes absorb strongly at 254 nm, although their absorptivity is somewhat higher at slightly shorter wavelengths. Most HPLC systems at GOCO and Army installations are equipped with fixed wavelength 254-nm detectors, while only a few are equipped with variable wavelength systems. Detection limits of less than 100  $\mu g/L$  have been reported by several investigators. These values are one-tenth the current discharge limits for TNT and less than one one-hundreth that currently set for RDX.

Several RP columns have been used to provide adequate separation for these four analytes, including C-8, C-18 and CN. The C-8 column can also separate TAX and SEX, the most significant impurities in HMX-RDX manufacture. Generally, the eluents for the analysis of these four compounds have been methanol/water, acetonitrile/ water or a ternary system of methanol/acetonitrile/ water. All seem to provide adequate separation, although the elution order of TNT and DNT is reversed in changing from water/methanol to water/ acetonitrile. In addition, isocratic acetonitrile/ water co-elutes HMX and RDX.

Most HPLC systems currently in use in the Army are not equipped to perform gradient elution. Isocratic conditions have most commonly been used in the past and adequate performance has been achieved. Therefore, it seems desirable to use an isocratic method, if possible, to minimize the necessity for capital expediture for new equipment for compliance monitoring. Isocratic analyses are also faster if a number of samples are to be analyzed.

In summary, we proposed RP-HPLC as the method most desirable for compliance monitoring for these four analytes in munitions wastewater. For initial testing we chose a C-8 column with a methanol/water eluen: under isocratic conditions with UV detection at 254 nm.

#### **EXPERIMENTAL**

#### Instrumentation

All HPLC measurements at CRREL during method development were conducted on two instrumental set-ups. The first is a Perkin Elmer Series 3/LC-65T equipped with a variable wavelength UV detector set at 254 nm and a Rheodyne 7125 sample loop injector. The second utilizes the Perkin Elmer Series 3 pump with a Rheodyne 7125 loop injector and a Spectra-Physics SP8300 fixed 254-nm UV detector. Depending on the experi-

| Participant            | System description   |  |  |  |  |
|------------------------|--|--|--|--|--|
| AEHA                   | Waters Model 6000A pump<br>Waters U6K Universal Injector (100-µL loop)<br>Waters Model 440 absorbance, fixed wavelength 254-nm detector<br>Integrator—HP 3390A   |  |  |  |  |
| USEPA, EMSL            | Waters Model 6000A pump<br>Waters Model M710 WISP autosampler<br>Waters Model 440 UV-254-nm detector<br>Waters Model 721 microprocessor  |  |  |  |  |
| Univ. of New Hampshire | Waters Model 6000 pump<br>Waters Model U6K injector<br>Waters Model 1205 UV-254-nm detector<br>Integrator—HP 3390A   |  |  |  |  |
| CRREL                  | Perkin Elmer Series 3 pump<br>Rheodyne 7125 sample loop injector<br>Spectra-Physics Model SP8300 UV-254-nm detector<br>Integrator—HP 3390A   |  |  |  |  |
| Louisiana AAP          | Perkin Elmer Series 3 pump<br>Perkin Elmer ISS-100 autosampler, sample loop 150 µL.<br>Perkin Elmer UV-VIS variable wavelength detector set at 254 nm<br>Perkin Elmer Sigma 15 Chromatography data station |  |  |  |  |
| lowa AAP               | Waters Model ALC-204 pump<br>Waters Model M710B WISP Autosampler<br>Waters Model 440, UV-254-nm detector<br>Manual peak height determination   |  |  |  |  |
| Holston AAP            | Spectra Physics Model 8700 pump<br>Valco injection valve<br>Perkin Elmer LC75, variable wavelength UV set at 254 nm<br>Spectra Physics SP4000 Integrator   |  |  |  |  |
| Radford AAP            | Dupont 870 pump<br>Rheodyne Model 7120 injection valve<br>LCD UV-3, UV-254-ium detector<br>Spectra Physics SP4000 Integrator   |  |  |  |  |
| LCWSL                  | Spectra Physics 8100 pump<br>Valco injection valve<br>Perkin Elmer Model 250, fixed wavelength 254-nm detector<br>Spectra Physics Model 4100 integrator  |  |  |  |  |

#### Table 2. Instrumentation used by various collaborative test participants.

ment, peak heights were measured manually or peak areas were obtained using HP3390A Integrators. In all cases,  $100 \ \mu$ L of sample was injected via a  $100 \ \mu$ L sample loop. A collaborative test was conducted following method development to assess overall performance of the method. The instruments used by the participants are summarized in Table 2.

All analyses for both method development and the collaborative test were conducted on Supelco 25 cm by 4.6 mm LC-8 columns (5  $\mu$ ). The number of theoretical plates for these columns averaged about 5000. A 2-cm precolumn of LC-8 was frequently used.

#### Chemicals

All analytical standards for TN'f, RDX, HMX, 2,4-DNT, 2,6-DNT, Tetryl and TNB were prepared from Standard Analytical Reference Materials (SARM) obtained from the Armament Research and Development Center, Large Caliber Weapon Systems Laboratory (LCWSL), Energetic Materials Division. SARM quality material from the same batch was supplied to each collaborative test participant for each of the four analytes determined. Standards were dried to constant weight in a vacuum desiccator over dry calcium chloride in the dark.

Standards for the aminodinitrotoluenes, the

diaminonitrotoluenes, SEX and TAX, used for retention time confirmation, were obtained from Dr. David Kaplan at the U.S. Army Natick Laboratories and used without further purification.

Methanol, acetonitrile and water used to prepare the mobile phases for various experiments were Baker HPLC grade solvents. They were combined in the proper proportions and vacuum filtered through a solvent-washed 0.4- $\mu$ m Nuclepore filter to remove particulate matter and to degas the solvent. Fresh mobile phase was prepared daily.

#### **RESULTS AND DISCUSSION**

#### Retention times of major analytes and common impurities

In addition to separating the analytes of interest from one another, the RP-HPLC method must be able to distinguish these analytes from other common components of munitions waste matrices, including impurities in the explosive formulations and decomposition products. It is impossible to test all the wastewaters from the many manufacturing operations over the range of conditions expected. However, several studies have documented the major impurities in these types of wastes. A study conducted by Stidham (1979), for example, identified the types of impurities common to RDX-HMX manufacturing and processing. Stidham found that in addition to RDX and HMX. TAX and SEX were present at concentrations as high as 5.2 and 2.0 mg/L, respectively. No other nitramines were detected. Since wastewater from this process is ultimately disposed of in surface waters, compliance monitoring of this type of wastewater will be required.

Four other compounds, unrelated to nitramines, were also detected by Stidham in cyclohexanone wastes. These substances contain only carbonyland hydroxyl-functionality and would therefore have very low UV absorptivity. Consequently, they would only be detectable at very high concentrations, well above expected levels. Cyclohexanone has a very low UV absorptivity, but because it is used as a recrystallizing solvent for purification of RDX, it could be present in rather large concentration. Thus, it is important for the method to be capable of separating cyclohexanone from the four analytes of interest.

For wastewater from load and pack operations, the waste is primarily generated from washdown of equipment used to melt solid explosives and pour them into shell casings. Thus, any explosive that becomes associated with this waste stream is completely dissolved. The explosive itself and its major impurities and their decomposition products will become important components of the wastewater.

The major impurities in production grade TNT have been identified by a number of investigators as TNB, DNTs and several of the unsymmetrical isomers of TNT. Of the DNTs, the 2,4-isomer is present in the greatest concentration, ranging from 0.06% (Leggett et al. 1977) to 0.72% (Gehring and Shirk 1967). The sum of the other isomers is, at most, present at only about one-third of the concentration of the 2,4-isomer (Leggett et al. 1977). Munitions wastewaters are generally held in collection tanks prior to carbon treatment and ultimate disposal. During the holding period, these wastes are subject to microbial transformation. TNT degrades metabolically under both aerobic and anaerobic conditions (McCormick et al. 1976) by a stepwise reduction of the nitro groups initially forming 4-amino-2,6-dinitrotoluene (4-Am-DNT) and 2-amino-4,6-dinitrotoluene (2-Am-DNT) (see Appendix B). These substances have been detected along with TNT in contaminated groundwater at the Hawthorne Naval Ammunition Depot, Nevada (Pereira et al. 1979). Further reduction of these components results in 2,4-diamino-6-nitrotoluene (2,4 DAm-NT) and 2,6-diamino-4-nitrotoluene (2,6 DAm-NT) (see Appendix B), which are apparently stable to further reduction (Kaplan and Kaplan 1982). Thus, the periodic presence of these amino-containing decomposition products is expected in wastewater from load and pack operations. Any analytical method used for these wastewaters must be able to separate these substances from the major components and also allow quantitation if sufficient concentrations are present.

Spanggord et al. (1982), using capillary GC-MS, have recently reported the identification of 32 different substances in the condensate wastewater from manufacture of TNT using capillary GC-MS. These include mono-, di-, and tri-nitrotoluenes and mono-, di- and tri-nitrobenzenes, several nitro-containing phenols, two nitro-containing benzonitriles, toluene, several aminonitrotoluenes and a couple of more exotic substances. This type of wastewater amounts to a very small portion of the munitions related wastewater and is far too complex for analysis by RP-HPLC using standard columns. No attempt was made to study the elution behavior of these substances.

Experiments were conducted to determine the retention times of major impurities and decompo-

Table 3. Retention times of primary analytes, impurities and decomposition products in two eluents (flow rate of 1.5 mL/minute at 25 °C).

|                  | Retention times (m. |          |  |  |  |  |
|------------------|---------------------|----------|--|--|--|--|
| Substance        | Eluent A*           | Eluent B |  |  |  |  |
| нмх              | 2.69                | 3.15     |  |  |  |  |
| RDX              | 3.94                | 4.15     |  |  |  |  |
| TNT              | 7.15                | 7.45     |  |  |  |  |
| 2-4-DNT          | 8.67                | 8.24     |  |  |  |  |
| SEX              | 2.43                | 2.58     |  |  |  |  |
| TAX              | 2.86                | 2.84     |  |  |  |  |
| TNB              | 4.61                | 4.86     |  |  |  |  |
| Terry            | 6.49                | 7.18     |  |  |  |  |
| 2-Am-DNT         | 8.44                | 7.86     |  |  |  |  |
| 4-Am-DNT         | 8.63                | 8.03     |  |  |  |  |
| 2,4-DAm-NT       | 2.73                | 2.78     |  |  |  |  |
| 2,6-DAm-NT       | 2.57                | 2.63     |  |  |  |  |
| 2,6-DNT          | 8.97                | 8.41     |  |  |  |  |
| 2,4,5-TNT        | 7.50                | 8.11     |  |  |  |  |
| Cyclohexanone    | 3.93                | 3.60     |  |  |  |  |
| Diethylphthalate | 15.26               | 12.61    |  |  |  |  |



\* Eluent A-50% water, 50% methanol.

† Eluent B-50% water, 38% methanol, 12% acetonitrile.

sition products using the LC-8 column with two different eluents: A-50% methanol and 50% water (V/V) and B-38% methanol, 12% acetonitrile and 50% water (V/V/V). The retention times for these substances and the four primary analytes are presented in Table 3.

The elution order for the two eluents is quite similar for the four primary analytes and the group of possible interfering substances. Eluent A separates TNT from 2,4-DNT by about 1.5 minutes compared to 0.8 minutes for eluent B. Eluent A also separates TNT from tetryl more completely, in about 0.7 minutes compared to 0.27 minutes for eluent B. However, eluent A does not separate HMX from SEX or TAX, both significant contaminants in HMX-RDX wastes. In addition, cyclohexanone co-elutes with RDX. Eluent B separates RDX and cyclohexanone by about 0.6 minutes and separates HMX from SEX and TAX by 0.6 and 0.3 minutes, respectively (Fig. 1). In addition, some recent experiments by Gleichauf\* indi-

Figure 1. Chromatogram of HMX, RDX, TNT and 2,4-DNT with and without major contaminants using eluent **B**.

cate that components of natural humic material interfere with HMX when eluent A is used, but are sufficiently separated for quantitation when eluent B is used. Unfortunately, neither eluent separates 2,4-DNT efficiently from the aminodinitrotoluenes or 2,6-DNT. Of the four primary analytes, however, 2,4-DNT is certainly the least important. It is significant only as an impurity in TNT, where it is present at concentrations less than 0.5% of that for TNT.

An eluent of acetonitrile/water was not studied because it is known that HMX and RDX co-elute using this eluent.

Clearly for HMX, RDX and TNT determination, B (38% methanol, 12% acetonitrile and 50% water) is the eluent of choice. Its only drawback is the poor separation of TNT and tetryl; however, tetryl is rarely used at present and its occurrence is only likely in the analysis of wastewater in old disposal lagoons. Since these are being phased out, tetryl should not pose an analytical problem for current or future analyses.

<sup>•</sup>Personal communication with G. Gleichauf, University of New Hampshire, 1984.

#### Linearity tests

To test response linearity, standard solutions of HMX, RDX, TNT and DNT were prepared at eight concentrations ranging from 11-5580, 12-6200, 9-4300 and 6-3200  $\mu$ g/L, respectively. These solutions were diluted with an equal volume of methanol/acetonitrile solution (76/24% V/V) and 100  $\mu$ L was injected into an LC-8 column and eluted with 50/38/12% water/methanol/acetonitrile at 1.5 mL/min. Quantitation was achieved using a fixed wavelength 254-nm detector coupled to both a strip chart recorder and an integrator (Table A1). The retention times were as follows: HMX-3.16 minutes, RDX-4.18 minutes, TNT-7.53 minutes and DNT-8.36 minutes.

Random error variances of the three replicates at each concentration were obtained (Table A1) and tested for homogeneity using Bartlett's test. For HMX, a  $\chi^2$  value of 2.04 was calculated, less than a critical value of 12.59 for  $\alpha = 0.05$  with six degrees of freedom. Thus for HMX, the variances are considered homogeneous over the entire range tested. A similar result was obtained for TN<sup>1</sup>T. The  $\chi^2$  value was calculated to be 10.43, again less than a critical value of 12.59 and the variances are considered homogeneous for TNT as well.

For DNT, the  $\chi^2$  value for the entire range was 15.17, indicating nonhomogeneous variance. Looking at individual variances, however, indicated that the variance for the highest concentration sample was greater than the sum of the variances for the other six concentrations. When Bartlett's test was repeated for the lowest six concentrations, the  $\chi^2$  value dropped to 5.04 and the variances were considered homogeneous within the reduced range.

Use of Bartlett's test for RDX also indicated that the variances were nonhomogeneous. Inspection of individual variance values (Table A1) indicates that this is attributable to two abnormally low variances at intermediate concentrations. Dropping the highest concentration data as was done for DNT will not improve this situation. Since the other five variances appear to be quite similar, we assumed the variances to be sufficiently homogeneous for regression analysis.

Within the regions of homogeneity, peak areas were individually regressed against known concentrations to obtain the best fit linear calibration curves (Table 4). Regression analysis tables were obtained to test whether the linear model adequately describes the data, or more simply, whether the responses were linear with concentration

#### Table 4. Regression analysis for linearity tests.

|                         | Sum of                         | Degrees of               | Mean                       |       |
|-------------------------|--------------------------------|--------------------------|----------------------------|-------|
| Variable                | squares                        | freedom                  | squares                    | F*    |
|                         |                                |                          |                            |       |
|                         | HMX (area) b                   | $= 2631.8, b_1$          | = 337.53                   |       |
| Total                   | 0.12934E+14                    | 21                       |                            |       |
| <i>b</i> ° <sup>†</sup> | 0.46238E + 13                  | 1                        |                            |       |
| <i>b</i> ,••            | 0.83112E + 13                  | 1                        |                            |       |
| L of F <sup>††</sup>    | 0.57030E + 08                  | 5                        | 1.1406E + 7                | 2.36  |
| Error                   | 0.67761E+08                    | 14                       | 4.8401E+6                  |       |
|                         |                                |                          |                            |       |
| -                       | (penk height) b.               |                          | , <i>D</i> , = 4.995E-U    | 10    |
| Total                   | 0.29517E - 02<br>0.11202E - 02 | 21                       |                            |       |
| <i>b</i> 。<br>b,        | 0.11202E = 02<br>0.18204E = 02 | 1                        |                            |       |
| LofF                    | 0.25666E - 05                  | 5                        | 5.1332E - 07               | 0.84  |
| Error                   | 0.85984E - 05                  | 14                       | 6.1417E - 07               | 0.04  |
| Liner                   | 0.033042 - 03                  |                          | 0.14172 07                 |       |
|                         | RDX (area) b                   | $= 6807.0, b_1$          | = 459.62                   |       |
| Total                   | 0.29694E + 14                  | 21                       |                            |       |
| b.                      | 0.10667E + 14                  | 1                        |                            |       |
| b.                      | 0.19026E + 14                  | 1                        |                            |       |
| L of F                  | 0.21270E + 09                  | 5                        | 4.2540E + 7                | 0.10  |
| Error                   | 0.59884E + 09                  | 24                       | 4.2774E + 8                |       |
|                         |                                |                          |                            | ~     |
|                         | (peak height) b.               |                          | , 0, = 0.789E - 0          |       |
| Total                   | 0.66013E - 02                  | 21                       |                            |       |
| <b>b</b> •              | 0.24471E - 02                  | 1                        |                            |       |
| b.<br>Lof E             | 0.41398E - 02<br>0.32312E - 05 | 5                        | 6.4624E - 07               | 0.81  |
| L of F                  | 0.32312E = 03<br>0.11160E = 04 | 14                       | 7.9714E - 07               | 0.01  |
| Error                   | 0.111006-04                    | 14                       | 1.9/142 0/                 |       |
|                         | TNT (area) b                   | = 3580.8, b <sub>1</sub> | = 959.64                   |       |
| Totai                   | 0.61991E+14                    | 21                       |                            |       |
| b.                      | 0.22096E + 14                  | 1                        |                            |       |
| Ь.                      | 0.39895E + 14                  | 1                        |                            |       |
| LofF                    | 0.14631E+09                    | 5                        | 2.9262E + 7                | 1.18  |
| Error                   | 0.34575E+09                    | 14                       | 2.4696E + 7                |       |
|                         |                                |                          |                            |       |
|                         | (peak height) b.               |                          | $b_1 = 1.069 E - 0$        | 13    |
| Total                   | 0.76724E - 02                  | 21                       |                            |       |
| b.                      | 0.27888E - 02                  |                          |                            |       |
| b.                      | 0.48715E - 02                  | 1<br>5                   | 5.113E - 07                | 0.75  |
| LofF                    | 0.25564E - 05<br>0.95943E - 05 | 14                       | 6.85JE - 07                | 0.75  |
| Error                   | 0.93943E - 03                  | 14                       | 0.8552 - 07                |       |
|                         | DNT (area) b                   | • = 2835.5, b,           | - 1266.7                   |       |
| Total                   | 0.59790E + 14                  | 21                       |                            |       |
| b.                      | 0.21293E + 14                  | 1                        |                            |       |
| <i>b</i> ,              | 0.38497E + 14                  | 1                        |                            |       |
| LofF                    | 0.24198E+09                    | 5                        | 4.8396E + 7                | 0.78  |
| Error                   | 0.52928E+09                    | 14                       | 3.7806E + 7                |       |
| -                       |                                |                          |                            |       |
|                         | T (peak height) b.             |                          | $0_1 = 1.358E - 0$         | 5     |
| Total                   | 0.69466E - 02                  | 21                       |                            |       |
| <b>b</b> •              | 0.25152E - 02                  | 1                        |                            |       |
| D.                      | 0.44210E - 02                  | 1                        | 4 4325 07                  | 0,76  |
| L of F                  | 0.22113E - 05                  | 5<br>14                  | 4.423E – 07<br>5.843E – 07 | V. /U |
| Error                   | 0.81805E - 05                  |                          | J.04JE - 0/                |       |
| • Varian                | ce ratio, critical vi          | alue is 2.99 for         | 5 and 14 degrees           | of    |

 Variance ratio, critical value is 2.99 for 5 and 14 degrees of freedom.

† Intercept.

\*\* Slope.

tt Lack of fit.

over the concentration ranges examined (Table 4). In all cases F values comparing lack of fit (L of F) to random error were much lower than 2.99, the critical value for 5 and 14 degrees of freedom at a 95% confidence level. Since L of F is not significant, the responses are adequately described by linear models over the ranges tested.

Variances for manually measured peak height data were not homogeneous over the concentration range tested because of, in part, quantitation error. Quantitation error results from the limited number of significant figures obtainable in manual peak height estimation. Even so, the regression lines obtained for peak heights can be used to describe the sensitivity of this method. For HMX, RDX, TNT and DNT, the sensitivities were  $5.0 \times$  $10^{-3}$ ,  $6.8 \times 10^{-3}$ ,  $1.1 \times 10^{-2}$  and  $1.4 \times 10^{-2}$  absorbance units/ppm, respectively, for 100-µL injection volumes. The noise level, peak to peak, was about 4.1×10<sup>-3</sup> absorbance units. Using a signal-tonoise ratio criterion of 3 to 1, we estimated detection limits of 25, 18, 11 and 9  $\mu$ g/L for HMX, RDX, TNT and 2,4-DNT respectively.

Linearity tests were also conducted using a variable wavelength detector set at 254 nm. Noise levels on the variable wavelength system were much higher. This was reflected in poorer precision and higher detection limits. Thus, where a choice is available, use of a fixed wavelength detector will probably result in better performance, particularly at low concentration.

#### **Filtration** tests

Typical aqueous environmental samples will contain particulates in amounts that are unacceptable for direct injection into an HPLC column. For this reason, we decided that a filtration step was necessary to protect expensive HPLC columns.

An experiment was conducted to assess which types of filters could be used to remove particulates without adversely affecting .he ability to analyze for trace levels of the four analytes by RP-HPLC. The following types of filter materials were tested with pink water and lagoon water from Louisiana AAP: glass fibre, polyvinyl chloride, polycarbonate and cellulose acetate-nitrate. The results of this study are presented in detail elsewhere (Leggett, in prep.). In general, use of cellulose-ester membranes was not recommended because of loss of the analytes, presumably by sorption on the membrane surface. The extent of loss was inversely related to the rate of filtration. No losses were encountered using polycarbonate filter materials nor with plastic syringes or polycarbonate filter holders, nor was anything leached at concentrations that interferred with the HPLC analysis. Subsequent work has indicated that disposable PTFE filter membranes are also acceptable for this application.

Another concern was whether absorption of analytes on natural particulates could bind significant amounts, with losses as the particulates were removed by filtration. It has been argued on the basis of octanol-water partition coefficients (see Table 6) that significant loss by this mechanism was unlikely, but it was not possible to be certain without experimental evidence (Leggett, in prep.). In addition, because of the slow rate of dissolution in water, small particles of the solid explosives could be removed by filtration. Since it was our goal to develop a method that would determine the total amount of material in the discharge, both in solution and associated with the particulate phase, we decided to dilute the aqueous samples one to one with methanol or methanol-acetonitrile prior to filtration. We feel that this procedure is desirable because 1) it further lessens the possible loss of analyte by adsorption on filters, particularly if filter media other than polycarbonate are used; 2) it would enhance desorption from natural particulates prior to their removal by filtration; and 3) it would increase the rate of dissolution of small particles of solid explosive.

To test the adequacy of this procedure, an experiment was conducted to see whether measurable amounts of the four analytes would be sorbed by particulates in various types of waters. We used five different types of water in the study: 1) Connecticut River water collected at Hanover, New Hampshire; 2) Hanover, New Hampshire, tapwater; 3) groundwater from a deep well in Canaan, New Hampshire; 4) water from a stagnant pond in Lebanon, New Hampshire; and 5) Milli-Q water. Total suspended solids (TSS), pH and total organic carbon (TOC) were determined on aliquots of each water (Table 5). Three replicate samples of

Table 5. Total suspended solids, pH and total organic carbon in waters used for recovery study.

| Sample            | TSS<br>(mg/L) | рН  | TOC<br>(mg/L) |
|-------------------|---------------|-----|---------------|
| Milli-Q           | < 0.1         | 4.4 | < 0.1         |
| Groundwater       | 0.2           | 7.1 | 0.7           |
| Tapwater          | 1.1           | 5.8 | 3.2           |
| Connecticut River | 1.7           | 7.8 | 4.3           |
| Pond water        | 4.2           | 7.9 | 10.2          |

᠆ᢣᠧ᠊ᡏᠯ᠆ᡆᠻᢆᠣᢜᠲᢄ᠊ᢐᠧᢆ᠕ᢦᢢ᠆ᡚ᠊ᢦᡫ᠂ᢣᡷᡔᡥ᠆ᡊᡣᢣᡭᢛᢣᡄ᠆ᡄᠮ᠇ᡵᢥᠲᡥᡵᢜᡆᢜ᠂ᢞ᠂ᡐᡯᡪᢥᡵᡘᠯᡵᡘᠮᡳᡬᡀᠻᡵᡘᢜᢘᢜᢘᠱᢘᠱᡳᡧᢋ᠋᠂ᠺᠼ᠆ᡧᡯᡧᠮ᠆ᢦᡘᢘᡯᢘᢜᢘᡏᢛᠮᡟᢠᠱ

| Table 6. Physical constants for TNT | F, RDX, HMX and DNT. |
|-------------------------------------|----------------------|
|-------------------------------------|----------------------|

|           | Meltii<br>poin | • | Solubil    | ity   |      |   | Vapor press                    | ure at 20°C |
|-----------|----------------|---|------------|-------|------|---|--------------------------------|-------------|
| Substance | (°C)           | · | (mg/L at . | 24°C) | Kow  | • | lorr                           | Pascul      |
| TNT       | 80.1           | a | 136        | d     | 45.0 | d | 1.3×10* e                      | 1.7×10-     |
| RDX       | 203.5          | b | 43         | d     | 7.65 | d | 1.0×10** f                     | 1.3 × 10"   |
| HMX       | 280.0          | b | 5.0        | -     | 1.38 | d | -                              | -           |
| DNT       | 70.0           | h | 180        | d     | 75.2 | d | 2 <u>× 10<sup>-4</sup> g</u> _ | 3 × 10-1    |

\*Octanol-water partition coefficient.

a-Jenkins et al. (1973).

b-Stidham (1979).

c-Glover and Hoffsommer (1973).

d-Leggett (unpubl.)

e-Leggett (1977).

f-Coates et al. (1970).

g-Leggett et al. (1977).

h-Dean (1979).

500 mL of each type of water were autoclaved for 1 hour at 121 °C, cooled to room temperature and spiked with stock solutions of HMX, RDX, TNT and DNT in methanol.

Each sample of spiked water was stirred for 1 hour and allowed to stand overnight in the dark. A 10-mL subsample was removed with a volumetric pipet and placed in a 20-mL scintillation vial, 10 mL of methanol was added, and the samples were shaken and allowed to stand at least 15 minutes. Each sample was then filtered through a 0.4- $\mu$ m Nuclepore polycarbonate membrane into a clean scintillation vial. Processed samples were analyzed in duplicate by injection of 100  $\mu$ l into a LC-8 HPLC column followed by elution with 1.5 mL/minute of 50% water, 38% methanol and 12% acetonitrile. The Milli-Q water was also analyzed in duplicate without filtration. The results of these analyses are presented in Table A2.

An analysis of variance test of these data was done, considering the duplicate analyses of three replicate samples as six total replicates since the variance for analytical replicates was about the same magnitude as that for replicate samples. The results indicated that there was no significant difference in analyte concentrations (at the 95% confidence level) between any of the five types of filtered water or the unfiltered Milli-Q water for TNT, RDX or DNT. This indicates that for these analytes, the addition of methanol prior to filtration eliminates any sorption on particulates or filter membranes. For HMX, however, a significant difference at the 95% confidence level was found, with an F ratio of 5.92 compared to a table value of 2.53.A Duncan's Multiple Range test revealed that the Connecticut River water and the pond

water were the two samples that differed significantly from the unfiltered Milli-Q water. These were also the two samples that had the highest total suspended solids and total organic carbon (Table 5). The mean values of the river and pond for HMX were 60.8 and 58.4  $\mu$ g/L, respectively, compared to a mean value of 63.2  $\mu$ g/L, for the unfiltered Milli-O water. It seems likely that adsorption of HMX on particulates and removal by filtration is not completely eliminated by dilution with methanol or that some irreversible chemisorption has occurred. Octanol-water partition coefficients have been used to simulate the nonspecific partitioning of hydrophobic organics between water and soil or sediments (Karickhoff et al. 1979). Since HMX has an octanol-water partition coefficient of 1.38, lower than those for the other three analytes (Table 6), if physical adsorption is responsible for loss, it must be due to some specific adsorption sites that are active for it because of its particular size or shape. Even so, only about 7.5% and 3.8% of the HMX was lost for the pond water and river water, compared to the unfiltered Milli-O water. Thus dilution of the sample with an equal volume of methanol seems desirable to minimize sorptive losses on filters and particulates.

In some recent experiments, Gleichauf<sup>\*</sup> compared the recovery of TNT spiked into solutions containing soluble and particulate humic acid at concentrations up to 20 mg/L. When these solutions were equilibrated with an equal volume of

<sup>•</sup> Personal communication with G. Gleichauf, University of New Hampshire, 1984.



Figure 2. Examples of chromalograms for HMX, RDX, TNT and 2,4-DNT at several analyte concentrations.

methanol prior to filtration, complete recovery of TNT was observed using this HPLC method with equilibration times as short as 15 minutes. If the solutions were filtered without the addition of the organic modifier, only about 80% of the spiked TNT was recovered. Thus, addition of the organic modifier can reduce analyte loss during filtration, presumably by removal of TNT sorbed on the surface of particulate humic acid prior to removal of the particulate on the filter.

#### **Detection limit determination**

A study was conducted to establish the detection limits of this RP-HPLC method for the four analytes in a common distilled water matrix. The study was configured as specified in the U.S. Army Toxic and Hazardous Materials Agency Quality Assurance Program (USATHAMA 1982), which is based on a method by Hubaux and Vos (1970). In this approach, detection limits were assumed for each analyte and standards were prepared at 0.5, 1, 1.5, 2, 5, 10 and 20\* times these values. The estimated detection limits were 25, 27, 15 and 13  $\mu$ g/L, for HMX, RDX, TNT and 2,4-DNT, respectively, close to the detection limits estimated from signal-to-noise ratio measurements in the linearity tests described earlier. Aqueous standards at each of these seven levels were prepared in quadruplicate on each of four days and analyzed in random order as described below. The results are shown in Table A3. Figure 2 shows three example chromatograms.

Analyses were conducted by diluting 10 mL of each sample with 10 mL of a solution that was 76% methanol and 24% acetonitrile (V/V), allowing the solution to stand at least 15 minutes and filtering it through a 0.4-µm Nuclepore polycarbonate filter. The first 10 mL portion of filtrate was discarded and the second 10 mL portion was saved for analysis. Samples were analyzed by filling a 100- $\mu$ L sample loop to capacity, injecting into an LC-8 column maintained at 25  $\pm 1^{\circ}$ C and eluting with a mobile phase of 50% water, 38% methanol and 12% acetonitrile (V/V/V) at 1.5 mL/minute. Retention times were 3.1, 4.1, 7.3 and 8.1 minutes for HMX, RDX, TNT and DNT, respectively. A fixed wavelength 254-nm detector was used, with the output attached to a digital integrator.

To determine detection limits for each analyte, first the mean and variance were obtained for the integrator readings at each concentration (Table 7). Bartlett's test was used to determine over what concentration ranges the variances were homogeneous. For HMX, Bartlett's test gave a  $\chi^2$  value of 18.23 when all the data were used, relative to a critical value f 12.59. When the data for the highest concentration were eliminated, the  $\chi^2$  value dropped to 6.23 compared to a critical value of 11.07. Thus in this range the variance was accepted as homogeneous at the 95% confidence level. For DNT, an analogous situation was found. Inclusion of all the data resulted in a significant  $\chi^2$ 

These two concentration levels are not specified in the USATHAMA Quality Assurance Program, but were included in this analysis.

value while eliminating the two highest concentrations resulted in a  $\chi^2$  value of 0.99 compared to a critical value of 9.49. Thus within the range of the five lowest standards, we considered the variance homogeneous.

For RDX and TNT, on the other hand, Bartlett's tests, using the data for all seven and the lowest six standards, all resulted in significant  $\chi^2$ values at the 95% confidence level. The  $\chi^2$  values for the lowest five standards were also barely significant in both cases, but there seemed to be no direct relationship between variance and concentration in this range. Therefore, for the purposes of the estimation of detection limits, the variances were considered homogeneous in this range. For HMX, variances were considered homogeneous over the concentration range 12.55-245.1  $\mu g/L$ . For RDX, TNT and 2,4-DNT, the homogeneous ranges were 13.63-136.31, 7.72-77.2 and 6.4-64.0  $\mu g/L$  respectively.

Using the data within these ranges, we regressed the known concentrations against the 16 individual integrator readings for each analyte at each concentration; the best fit linear equations obtained are presented in Table 8. Regression analysis tables were obtained for these data to test whether the assumption of a linear relationship between concentration and response was justified. In all cases the linear model adequately described the data at the 95% confidence level.

Confidence limits about the regression lines were determined at the 90% confidence level. The d<sub>x</sub> : tion limit was obtained from the value of X (the target concentration) corresponding to the point on the lower confidence limit curve where the value of Y (integrator units) equals the value of Y on the upper confidence limit curve at X = 0(Hubaux and Vos 1970). This is shown graphically for HMX in Figure 3. The detection limits for HMX, RDX, TNT and DNT obtained in this manner were 26, 22, 14 and 10 respectively.

The random error variances obtained at each concentration can also be used to define analytical precision. For HMX, within the region of homogeneous variance, the average variance was about  $7.3 \times 10^{\circ}$  integrator units and hence the standard deviation was about  $2.7 \times 10^{\circ}$ . When this was converted to concentration units using the regression line, the analytical precision in the concentration range  $12-245 \ \mu g/L$  was estimated at  $\pm 3.4 \ \mu g/L$ . Above  $245 \ \mu g/L$ , the relative standard deviation is probably constant at about  $\pm 2\%$ . In a similar manner, the analytical precision for RDX was estimated at  $\pm 3.3 \ \mu g/L$  in the 13-136  $\mu g/L$  concentration range, for TNT at  $4.4 \ \mu g/L$  in the 7-77

## Table 7. Variance analysis at measured concentrations for detection limit test.

|         |               |               |                          | Bartlett |
|---------|---------------|---------------|--------------------------|----------|
|         | Concentration | Integra       | 1851                     |          |
| Analyte | (µg/L)        | Mean          | Variance                 | <u></u>  |
| нмх     | 12.55         | 5.111         | 4.85 × 10°               |          |
|         | 24.51         | 10,690        | 5.18×10*                 |          |
|         | 36.76         | 13.881        | $4.20 \times 10^{\circ}$ |          |
|         | 49.02         | 20,220        | 8.67 × 10*               |          |
|         | 122.05        | 44,168        | 1.11 × 10°               |          |
|         | 245.1         | 88,135        | 1.00 × 10'               | 6.23     |
|         | 490.2         | 179,720       | 2.47 × 10°               | 18.231   |
| RDX     | 13.63         | 7,265         | 4.24 × 104               |          |
|         | 27.26         | 14,707        | 8.87 × 10*               |          |
|         | 40.89         | 21,084        | 6.20 × 10*               |          |
|         | 54.52         | 27,990        | 2.09 × 10'               |          |
|         | 136.3         | 65,707        | 9.57 × 10*               | 10.82    |
|         | 272.6         | 130,669       | 2.08 × 10*               | 14.691   |
|         | 545.2         | 263,501       | 4.76 × 10°               | 31.261   |
| TNT     | 7,72          | 6,718         | 1.24 × 10°               |          |
|         | 15.44         | 15,987        | 1.09 × 10*               |          |
|         | 23.16         | 23,612        | 4.25 × 10'               |          |
|         | 30.88         | 31,315        | 1.17 × 10'               |          |
|         | 77.2          | 77,309        | $1.82 \times 10^{\circ}$ | 10.84    |
|         | 154.4         | 155,133       | 6.63 × 10°               | 22.87    |
|         | 308.8         | 308,734       | 1.64 × 10'               | 52.32    |
| DNT     | 6.40          | <b>6,</b> 071 | 1.93 × 10'               |          |
|         | 12.80         | 15,9          | $1.84 \times 10^{10}$    |          |
|         | 19.20         | 24,854        | 2.80 × 10'               |          |
|         | 25.60         | 34,192        | 2.25 × 10°               |          |
|         | 64.0          | 85,156        | $1.84 \times 10^{\circ}$ | 0.99     |
|         | 128.0         | 171,249       | 8.86 × 10'               |          |
|         | 256.0         | 336 551       | 3.96 × 10'               | 17.50    |

• Critical  $\chi^2$  values ( $\alpha = 0.05$ ) are 12.59 when data for all seven concentrations are used, 11.07 when the highest concentration is dropped and 9.49 when the data for the two highest concentrations are dropped.

† Variances are significant at the 95% confidence level.

# Table 8. Regression equations for detection limit tests (in the form: Peak area $= b_0 + b_1$ [concentration]).

|         | Corcentration<br>range |        |        |
|---------|------------------------|--------|--------|
| Analyte | (µg/L)                 | b•     | Ъ,     |
| нмх     | 12.55-245.1            | 2631.8 | 337.53 |
| RDX     | 13.63-272.6            | 6807.0 | 459.62 |
| TNT     | 7.72- 77.2             | 3580.8 | 959.64 |
| 2,4 DNT | 6.40- 64.0             | 2835.5 | 1266.7 |



Figure 3. Detection limit determination for HMX.

 $\mu$ g/L range and for DNT at 4.6  $\mu$ g/L in the 6-64  $\mu$ g/L range. At higher concentrations, relative standard deviation is estimated at  $\pm 2\%$  for RDX and  $\pm 4\%$  for TNT and DNT.

#### Ruggedness test

When a published analytical method is selected for use, it is often difficult to reproduce the levels of performance obtained by the original investigator. The originator of the method was meticulous in reproducing the many individual steps required. While some of these steps are called out in detail in the published method, many others may not be. Although these steps may be common practice in the originator's laboratory, they may not be elsewhere, and strict adherence to procedural details may be critical in the outcome of analytical determinations.

A method that has been used to help assess the sensitivity of analytical methods to small deviations in test protocols is called a "ruggedness test" (Youden and Steiner 1975). To conduct such a test, the originator of a method carefully scrutinizes every step involved in the procedure to identify variables, such as composition of containers, types of filters and holders, storage conditions, temperatures, holding times, etc. Consideration is given, using experience and chemical intuition, as to whether deviations in a specific step could modify the analytical result. An experiment is then designed to test small variations in those steps that seem likely to result in analytical deviations.

For the RP-HPLC method under investigation, the method was studied carefully and four specific aspects were selected as being the most likely areas where small deviations in procedure could produce significant changes in results. These variables are designated  $X_1-X_4$ :  $X_1$ , use of plastic rather than glass vials for sample storage;  $X_2$ , during filtration, use of the first 10-mL portion of filtrate rather than the second 10 mL as specified;  $X_3$ , determination of whether the 15-minute holding time after dilution with methanol was more or less effective than a much longer (4-hour) holding time; and  $X_4$ , how critical the volume ratio of sample to methanol was in determining peak areas for the four analytes.

To conduct this experiment, a 2<sup>4</sup> factorial design was used. The factors, levels tested, and design and interaction matrices in coded units are presented in Tables A4 and A5. The 16 individual trials and analytical standards were analyzed in random order in duplicate. The test solution contained the following approximate concentrations: HMX-202  $\mu$ g/L, RDX-131  $\mu$ g/L, TNT-177  $\mu$ g/L and DNT-96  $\mu$ g/L.

Analysis was conducted in a 25 cm by 4 mm LC-8 column using a mobile phase of 50% methanol and 50% water at 1.5 mL/minute. Injections were made by filling a  $100-\mu$ L sample loop to capacity with the filtered sample or standard. Quantitation of each peak was made using a variable wavelength UV detector set at 254 nm, and peak ateas were measured using a digital integrator. Retention times for HMX, RDX, TNT and DNT were 2.6, 3.8, 6.7 and 8.2 minutes respectively.

We constructed calibration curves for the four standards run in duplicate using least squares linear regression analysis with and without an intercept. An F-ratio test was conducted to determine whether the true intercepts were equal to zero for each analyte. In all cases, the hypothesis of zero intercept could not be rejected at the 95% confidence level and the model with a zero intercept was accepted as the proper calibration curve. Using these models, we converted peak areas for individual trials to concentrations (Table 9). The following estimates of relative standard deviation were obtained from these 16 sets of duplicate analyses: 10.7% for HMX, 6.5% for RDX, 6.2% for TNT and 9.5% for 2,4-DNT.

The data in Table 9 were evaluated by analysis of variance techniques (Table A6). A summary of the effects for all four analytes is presented in Table 10.

Variable  $X_1$  is significant only for 2,4-DNT where the samples stored in glass gave a higher average concentration than the samples stored in polyethylene. Of the four analytes, DNT has the highest octanol-water partition coefficient and,

Table 9. Duplicate concentration values  $(\mu g/L)^*$  for trials in the ruggedness test.

| Trial | H/      | НМХ     |         | HMX RDX |         | DX      |         | NT      | 2,4-DNT |  |
|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--|
| 1     | 145.168 | 150.439 | 116.680 | 104.814 | 158.849 | 153.894 | 89.413  | 87.093  |         |  |
| 2     | 229.971 | 210.516 | 158.191 | 147.957 | 199.183 | 203.885 | 131.903 | 130.816 |         |  |
| 3     | 315.186 | 333.983 | 126.885 | 131.402 | 190.567 | 204.919 | 103.302 | 86.663  |         |  |
| 4     | 129.717 | 146.785 | 122.668 | 119.178 | 120.180 | 150.541 | 89.934  | 66.533  |         |  |
| 5     | 243.024 | 233.021 | 139.573 | 126.348 | 201.818 | 192.011 | 110.314 | 125.308 |         |  |
| 6     | 141.500 | 178.869 | 128.817 | 111.820 | 169.579 | 165.918 | 87.286  | 87.800  |         |  |
| 7     | 183.772 | 170.126 | 145.881 | 113.694 | 158.928 | 155,164 | 90.615  | 86.573  |         |  |
| 8     | 211.514 | 246.641 | 141.376 | 142.570 | 213.203 | 188.184 | 105.600 | 114.588 |         |  |
| 9     | 195.495 | 256.575 | 137.557 | 143.220 | 205.274 | 207.088 | 98.225  | 113.778 |         |  |
| 10    | 161.946 | 152.550 | 117.080 | 114.011 | 124.220 | 161.263 | 87.864  | 69.457  |         |  |
| 11    | 146.774 | 189.100 | 122.646 | 121.794 | 162.092 | 157,153 | 67.021  | 91.245  |         |  |
| 12    | 237.584 | 185.207 | 144.085 | 137.380 | 199.822 | 177.911 | 114.730 | 103.719 |         |  |
| 13    | 208.300 | 173.637 | 127.027 | 120.125 | 166.040 | 167.102 | 85.647  | 78.719  |         |  |
| 14    | 238.640 | 243.794 | 153.350 | 140.139 | 200.200 | 196.895 | 108.958 | 98.000  |         |  |
| 15    | 241.290 | 216.503 | 156.969 | 146.139 | 202.212 | 203.167 | 98.700  | 96.700  |         |  |
| 16    | 166.529 | 193.062 | 127.124 | 116.924 | 161.855 | 162.131 | 81.500  | 78.687  |         |  |

 Concentration are not really known to six significant figures but the values were retained since the statistical analysis was performed without rounding off the values to three significant figures.

Table 10. Effects of variations in sample handling on results for HMX, RDX, TNT and 2,4-DNT in water by HPLC.

Effects were estimated in a 2° factorial experiment—bold face values are significant at the 95% confidence level.

ī

|                               | Effects: Concentration differences<br>(µg/L) <sup>†</sup> |        |        |         |  |  |  |  |  |
|-------------------------------|---|--------|--------|---------|--|--|--|--|--|
| Variable*                     | НМХ   | RDX    | TNT    | 2,4-DNT |  |  |  |  |  |
| х.                            | + 3.95  | - 2.98 | - 1.35 | + 7.66  |  |  |  |  |  |
| X,                            | - 9.40  | - 1.88 | + 3.70 | + 7.27  |  |  |  |  |  |
| х,                            | - 6.45  | - 4.52 | - 7.60 | - 0.07  |  |  |  |  |  |
| X.**                          | + 75.0  | - 21.4 | - 43.6 | - 25.9  |  |  |  |  |  |
| x.x,                          | - 16.3  | + 0.69 | + 4.23 | + 6.00  |  |  |  |  |  |
| X,X,                          | +13.1   | + 1.73 | - 0.25 | 2.73    |  |  |  |  |  |
| x.x.                          | - 22.1  | + 2.59 | - 1.50 | - 2.02  |  |  |  |  |  |
| X <sub>1</sub> X <sub>1</sub> | - 13.3  | + 3.56 | + 2.61 | + 3.38  |  |  |  |  |  |
| X,X.                          | + 7.71  | - 4.32 | + 0.40 | - 4.62  |  |  |  |  |  |
| x,x,                          | - 16.7  | - 2.05 | - 6.47 | - 3.46  |  |  |  |  |  |
| X,X,X,                        | - 8.43  | + 4.50 | + 1.86 | + 6.55  |  |  |  |  |  |
| x.x,x.                        | + 14.3  | - 4.33 | + 7.52 | - 4.16  |  |  |  |  |  |
| x.x.x.                        | - 14.5  | - 4.38 | - 2.22 | + 1.44  |  |  |  |  |  |
| x,x,x.                        | + 14.4  | - 5.79 | - 4.65 | - 1.26  |  |  |  |  |  |
| X,X,X,X,                      | + 20.5  | - 2.62 | + 5.33 | - 3.14  |  |  |  |  |  |

- X<sub>1</sub> = Two-day sample storage in glass (+1 level) and in polyethylene bottles (-1 level).
- X<sub>1</sub> = Pirst 10-mL filtrate from 0.4-μm Nuclepore (+1 level) and second 10-mL portion (-1 level).
- X, = Standing 15 minutes before filtering MeOH/H<sub>3</sub>O solution (+1 level) and 4 hours standing (-1 level), both in glass vials.
- X<sub>4</sub> = 8/10 sample-to-MeOH volume ratio (+1 level) and 10/8 sample-to-MeOH ratio (+1 level).
- † Average concentration for each compound was: HMX = 202 μg/L, RDX = 131 μg/L. TNT = 177 μg/L, and 2.4-DNT = 95.8 μg/L.
- \*\* See text for explanation of large effect of variable X...

hence, is the substance most prone to adsorbing or partitioning into an organic surface such as polyethylene by non-specific or hydrophobic mechanisms.

Variable  $X_2$  is also significant only for 2,4-DNT where the first 10 mL of filtrate appears to have a higher concentration than the second 10 mL. The reason for this effect is unclear and seems to be in the opposite direction one might expect if there was adsorption in the filter membrane.

Variable  $X_3$  was not found to be significant for any of the four analytes. Thus a 15-minute standing time seems sufficient after dilution with methanol, at least when the analyte was present as a dissolved species. Variable  $X_4$ , the volume ratio of sample to methanol, was found to be significant for all four analytes. This was expected since the actual concentration of the +1 coded trials was 25% lower than that for the -1 coded trials. The raw data were not adjusted for this effect because of concerns about adverse effects on error estimates. Consequently, it is necessary to examine the size of the effects in comparison to the expected values. For this purpose, the average concentrations were calculated for both coded levels and the +1 coded levels were multiplied by 1.25 to account for the expected 25% differences. An adjusted sum of squares was also calculated using the corrected concentrations and new F ratios were estimated based on the original error mean squares. The results of these calculations are displayed in Table 11. Clearly, the sample-to-methanol ratio exhibits a substantial effect on the results for HMX even

Table 11. Further analysis of the effect of sample/methanol ratio by adjusting for volume differences.

| НМХ    | RDX   |  | 2,4-DNT   |
|--------|---|--|---|
| 239.9  | 142.1                                       | 199.1  | 108.7   |
| 164.9  | 120.6                                       | 155.6  | 82.8  |
| - 45.5 | - 17.8                                      | - 28.0   | - 31.2  |
| 206.1  | 150.8                                       | 194.4  | 103.5   |
| - 16.4 | + 5.8                                       | - 2.4  | - 5.0   |
| 19.7*  | 8.45*                                       | i.46   | 2.62  |
|        | 239.9<br>164.9<br>- 45.5<br>206.1<br>- 16.4 | 239.9 142.1<br>164.9 120.6<br>-45.5 -17.8<br>206.1 150.8<br>-16.4 +5.8 | 239.9       142.1       199.1         164.9       120.6       155.6         -45.5       -17.8       -28.0         206.1       150.8       194.4         -16.4       +5.8       -2.4 |

Table 12. Results of methanol/water ratio test, concentration in  $\mu g/L$ .

| Sample | НМХ    | RDX   | TNT   | DNT   |
|--------|--------|-------|-------|-------|
| 1 (1)  | \$22.0 | 289.0 | 94.8  | 129.8 |
| (2)    | 495.9  | 294.5 | 94.5  | 124.2 |
| 2 (1)  | 496.9  | 292.3 | 97.3  | 95.7  |
| (2)    | 506.8  | 292.5 | 95.0  | 127.6 |
| 3 (1)  | 495.8  | 285.5 | 94.3  | 128.6 |
| (2)    | 493.0  | 291.7 | 92.6  | 124.9 |
| 4 (1)  | 488.0  | 286.2 | 92.6  | 128.0 |
| (2)    | 503.0  | 297.4 | 89.5  | 126.2 |
| 5 (1)  | 490.8  | 291.6 | 94.0  | 127.5 |
| (2)    | 507.5  | 290.7 | 88.4  | 125.1 |
| 6 (1)  | 472.4  | 271.8 | 95,9  | 125.3 |
| (2)    | 480.7  | 284.5 | 97.9  | 123.8 |
| 7 (1)  | 473.1  | 276.2 | 94.9  | 123.3 |
| (2)    | 441.3  | 265.3 | 94.5  | 118.1 |
| 8 (1)  | 455.9  | 280.8 | 97.4  | 100.0 |
| (2)    | 478.8  | 273.1 | 82.9  | 120.1 |
| 9 (1)  | 478.5  | 276.2 | 94.5  | 123.2 |
| (2)    | 475.3  | 276.1 | 93.6  | 120.0 |
| 10 (1) | 466.4  | 277.7 | 101.2 | 94.5  |
| (2)    | 471.1  | 277.2 | 91.4  | 122.6 |

after volume corrections are applied. A smaller but significant effect is also in evidence for RDX, which elutes second, but no significant effect is noted for TNT or 2,4-DNT. Further testing of this effect is desirable when the actual analyte concentrations are equivalent in two cases. However, it appears that proper maintenance of this sampleto-methanol ratio is essential for reliable results.

The results of the ruggedness test indicate that it is important to be very specific with regard to the types of containers and the portion of filtrate chosen foi analysis. It also appears that sample-tomethanol ratio is important over and above the obvious effect on the resulting concentration in the final solution.

#### Solvent strength test

To test further the effect of various sample-tomethanol ratios in the solution injected into the HPLC, two standards were prepared, one in water and one in methanol, but both with equal concentrations of HMX, RDX, TNT and DNT. Five replicate 10-mL portions of the methanol standard were each diluted with 8 mL of water (samples 1-5). Five replicates of the water were diluted in a like manner with methanol (samples 6-10). These 10 samples thus had equivalent concentrations of the four analytes, but five had a 10/8 methanolto-water ratio and five had an 8/10 methanol-towater ratio.

The 10 samples were analyzed randomly in duplicate (Table 12). A variance ratio (F) test on the two solvent types indicated no significant difference in random error for any of the four analytes at the 95% confidence level. Therefore, the variances were pooled for both types of samples for a given analyte and a t-test was run to compare treatment means. The calculated t values were 32.9, 7.3, 0.7 and 1.4 for HMX, RDX, TNT and DNT, respectively, while the t-table value is 2.101 for the 95% confidence level. Thus, there again is a significant difference in the peak areas for HMX and to a lesser degree for RDX but not for TNT and DNT. This result confirms that found earlier for the effect of variable  $X_{4}$  in the ruggedness test for all four analytes after adjustment was made for actual concentration differences. Therefore, it is important to ensure that the solvent strengths of samples and standards are carefully matched or inaccurate results for HMX and RDX will result. The reason for this is uncertain but may be due to differences in absorptivities of these substances in solvents of varying composition, which would be the most significant for substances eluting early in the chromatogram, like HMX.

# Methanol-water equilibrium times with river water

In the ruggedness test, two contact times (15 minutes and 4 hours) between methanol addition

| Rever water, concentrations in $\mu g/L$ . |                       |       |               |        |      |            |  |  |  |  |
|--|-----------------------|-------|---------------|--------|------|------------|--|--|--|--|
|  | _                     | τντ   |               |        |      |            |  |  |  |  |
| Sample                                     | 15 min                | 4 hr  | Difference    | 15 min | 4 hr | Difference |  |  |  |  |
| 1  | 106.4                 | 105.8 | + 0. <b>6</b> | 75.ó   | 75.9 | -0.3       |  |  |  |  |
| 2  | 99.2                  | 101.3 | - 2.1         | 78.8   | 81.0 | - 2.2      |  |  |  |  |
| 3  | 100.0                 | 102.2 | - 2.2         | 74.7   | 75.5 | - 0.8      |  |  |  |  |
|  | <b>~~</b> <i>&lt;</i> |       |               |        |      |            |  |  |  |  |

Table 13. Results of equilibration time study with Connecticut Diver water concentrations in us/I

| umpie |                | <u> </u> | Dijerence              | <u></u> | • nr           | DUJerence              |  |  |
|-------|----------------|----------|------------------------|---------|----------------|------------------------|--|--|
|       |                |          |                        |         |                |                        |  |  |
| 1     | 106.4          | 105.8    | + 0. <b>6</b>          | 75.6    | 75.9           | - 0.3                  |  |  |
| 2     | 99.2           | 101.3    | - 2.1                  | 78.8    | 81.0           | - 2.2                  |  |  |
| 3     | 100.0          | 102.2    | - 2.2                  | 74.7    | 75.5           | ~ 0.8                  |  |  |
| 4     | 99.6           | 96.3     | +3.3                   | 75.0    | 80.3           | - 5.3                  |  |  |
| 5     | 105.7          | 107.9    | - 2.2                  | 76.6    | 78.4           | -1.8                   |  |  |
| 6     | 97.8           | 94.1     | + 3.7                  | 76.1    | 72.3           | + 3.8                  |  |  |
| 7     | 102.5          | 106.2    | - 3.7                  | 80.5    | 78.6           | + 1.9                  |  |  |
| 8     | 52.2           | 55.8     | - 3.6                  | 74.5    | 74.3           | + 0.2                  |  |  |
|       |                |          | $\overline{X} = -0.78$ |         |                | $\overline{X} = -0.56$ |  |  |
|       |                |          | <i>S</i> = 2.72        |         |                | S = 2.74               |  |  |
|       | ( value = 0.81 |          |                        |         | / value = 0.58 |                        |  |  |
|       | 1.95           | (df = 7) | = 2.365                | 1.95    | (df = 7)       | = 2.365                |  |  |

and filtration were tested; no significant differences were found in analyte concentration for a distilled water matrix. It is possible, however, that in a natural water sample, a significant amount of these analytes might be adsorbed to natural particulate matter. If so, it seems that addition of methanol should desorb at least a portion of this material, but the process could be rate limited and a longer contact time could be useful.

To test the role of adsorption, a sample of Connecticut River water was collected, spiked with TNT and RDX and divided into eight subsamples. Typical levels of suspended solids for this water are 2-3 mg/L. Four subsamples were stored in glass and four in plastic for 9 days. Then, two 10-mL portions of the water in each bottle were withdrawn. One was mixed with 10 mL of methanol, allowed to stand 15 minutes and filtered through a 0.4-µm Nucleopore polycarbonate filter. The second aliquot was mixed with methanol and allowed to stand for 4 hours prior to filtering.

A 100-µL portion of each filtered sample was injected into a LC-8 column and eluted with a mobile phase of 38% methanol, 12% acetonitrile and 50% water. Peak areas were obtained for RDX (4.2 minutes) and TNT (7.3 minutes) (Table 13).

A paired 1-test was conducted on these data. The results indicated that there was no significant difference at the 95% confidence level for either TNT or RDX. This agrees with the result obtained in the ruggedness test for this variable for these two substances and indicates that a 15-minute equilibration time is sufficient for natural waters containing low levels of natural particulate matter.

#### Analysis of real munitions wastes

In our discussion of the RP-HPLC method thus far, we have considered only synthetic samples; aqueous samples prepared by spiking distilled water or several natural water matrices with low levels of TNT, RDX, HMX and DNT. To test the method with a variety of real munitions wastes, samples were collected at Louisiana AAP. Iowa AAP, Holston AAP and Milan AAP.

The initial samples were collected at the Louisiana AAP from two different sources. The first was wastewater from a load and pack operation following activated carbon treatment. The second was from an old lagoon, once used for disposal of load and pack wastewater prior to use of the carbon treatment process. Figure 4 is an example of the chromatograms obtained. These samples were analyzed in the usual manner using a mobile phase of 50/50% methanol/water. The concentrations of TNT, RDX and HMX found in these samples are presented in Table 14.

Clearly, the wastewater samples following the carbon treatment represent the simpler matrix with well-defined peaks only for TNT, RDX and HMX. No significant interferences are apparent in this matrix. The lagoon water sample, on the other hand, has several other peaks in addition to those for TNT, RDX and HMX. For the most part, they are well separated from the analytes of interest.

At Milan AAP, groundwater from a contaminated water supply well was sampled and analyzed as described above (Fig. 5). A peak for RDX was observed at a retention time of 3.97 minutes, with a peak area corresponding to an aqueous concentration of 70  $\mu$ g/L. No analytical problems were



Figure 4. Chromatogram for disposal pond at Louisiana Army Ammunition Plant.



Figure 5. Examples of chromatograms for two samples of contaminated groundwater at Milan Army Ammunition Plant.

| Table | 14. | Analy | sis of | munition   | westes  | from   | Louisiana, |
|-------|-----|-------|--------|------------|---------|--------|------------|
| Milan | and | lowa  | AAP    | s, concent | rations | in µg/ | ′L.        |

| Sample                   | нмх   | RDX    | TNT    | DNT |
|--------------------------|-------|--------|--------|-----|
| Louisiana                |       |        |        |     |
| Load and pack wastewater | 289   | 2,430  | 19     | < 0 |
| Lagoon water             | 1,652 | 6,280  | 1,314  | 915 |
| Milan                    |       |        |        |     |
| Water supply well        | < d   | 70     | < d    | < d |
| lows wasiewater          |       |        |        |     |
| Before carbon column     | 4,600 | 19,700 | 51,300 | < d |
| After one carbon column  | 606   | 586    | 128    | < d |
| After two carbon columns | < d   | < d    | < d    | < d |

d---detection limits are estimated at about 26  $\mu$ g/L for HMX, 22  $\mu$ g/L for RDX, 14  $\mu$ g/L for TNT, and 10  $\mu$ g/L for DNT.

encountered and the method appeared to function well for this type of water matrix.

At Iowa AAP, samples were collected from a waste stream produced from melt and pour operations for loading of artillery shells. Three types of samples were collected: wastewater prior to carbon treatment, wastewater following treatment with one carbon column and wastewater following treatment with two carbon columns. Analyses of these samples were conducted as usual, using a mobile phase of water/methanol/acetonitrile in a ratio of 50:38:12. Retention times for HMX, RDX, TNT and DNT standards were 3.4, 4.4, 7.4 and 8.3 minutes, respectively. Chromatograms obtained are shown in Figure 6 and quantitative results results are presented in Table 14. The method seemed to work very well for these samples. Concentration of these analytes in the wastewater prior to carbon treatment was quite high (=60 mg/L for TNT) and injection volumes between 2  $\mu$ L and 100  $\mu$ L were tried. The results demonstrated that the concentrations obtained were independent of sample volume when the volumes were properly considered in calculations.



Figure 6. Chromatograms for treatment sequence at Iowa Army Ammunition Plant.

The lowa sample before carbon treatment and after the first carbon column had an additional peak just after TNT but too early for DNT. A peak in this region had been observed in samples containing TNT that were held at room temperature for several days. This peak is probably a microbial degradation product of TNT, perhaps one of the isomers of aminodinitrotoluene.

A sample of wastewater from an RDX-HMX manufacturing operation at Holston AAP was also subjected to this analytical procedure. Large peaks for HMX and RDX were found along with several other very early eluting peaks. The concentrations of HMX and RDX were found to be about 3.0 and 27.4 mg/L respectively. Two of the early eluting peaks are thought to be SEX and TAX, two known impurities in RDX-HMX manufacturing.

#### Preparations for collaborative test

It appears that the RP-HPLC method is suitable for use in compliance monitoring at Army and GOCO installations, based on CRREL research. In order to determine how well this method works in a variety of other laboratories, a collaborative test of the method was conducted. A number of laboratoric, were contacted and nine agreed to participate. Seven of these were within the Army system including four ammunition plants and three research laboratories. The other two were a university and the USEPA Environmental Monitoring and Support Laboratory. Thus the nine laboratories included some rather diverse participants in both background and experience with this type of analysis.

The broad strategy for conducting the collaborative test was as follows: a set of water matrices was to be chosen and sent to each participant along with a set of solutions containing the four analytes with which the matrices were to be spiked. The matrices were to represent some of the types of water that might be analyzed by this method and were to be stabilized as much as possible to retard chemical or microbiological modifications during storage. The spiking solutions were to be made up in methanol and were to represent various concentration ranges. Preparation of the samples and the beginning of the test were to be coordinated to minimize the storage times and, hence, the chances for deterioration.

Since the bulk of the study was to be based on the spiking of aqueous matrices with a methanolbased stock solution, it was necessary to ensure that evaporation of this volatile solvent during shipment and storage was eliminated. To do so we planned to store the methanol solutions in flame sealed glass ampules. A study was conducted to determine whether this procedure resulted in any measurable change in concentration of the four analytes in a methanol stock solution. A stock solution of HMX, RDX, TNT and DNT in methanol was prepared at about 330, 250, 100 and 125  $\mu$ g/L respectively. Approximately 10 mL of this solution was poured into four glass ampules. (The glass ampules were 1.8 cm in diameter with a capacity of about 10 mL, obtained from OIC, College Station, Texas.) One ampule was sealed immediately using the methane-oxygen flame from an OIC Purging and Sealing Module of an organic carbon analyzer. The neck of the other three ampules were covered with aluminum foil and they were placed in a freezer for 30 minutes. They were then removed and quickly sealed while cold.

The methanol solutions in the four ampules were analyzed as follows. A volume of solution was withdrawn from the ampule and mixed with

| Table  | 15. I | Results  | of | flame | sealing | test, | mean | con- |
|--------|-------|----------|----|-------|---------|-------|------|------|
| centra | tions | ; in µg∕ | L. | *     |         |       |      |      |

| Sample                | НМ    | <u>x</u> | RDX   |   | TNT   | DNT      |  |
|-----------------------|-------|----------|-------|---|-------|----------|--|
| Ampule 1 <sup>†</sup> | 339.4 | att      | 250.7 | b | 104.6 | 129.6 ab |  |
| Ampule 2              | 341.4 | a        | 252.2 | ь | 107.7 | 125.5 c  |  |
| Ampule 3              | 341.2 | а        | 258.8 | a | 105.9 | 132.5 ab |  |
| Ampule 4              | 340.2 | 8        | 259.6 | 8 | 109.0 | 133.7 a  |  |
| Stock**               | 329.5 | Ь        | 247.5 | Ь | 100.8 | 127.5 bc |  |

Mean of three replicates.

1 Ampule 1 was sealed immediately; the other three ampules were cooled in a freezer for 30 minutes prior to sealing.

\*\* Same solution used in ampules but not flame sealed.

†† Values with different letters are considered significantly different from each other at the 95% confidence level using Duncan's multiple range test.

an equal volume of HPLC grade water. A  $100-\mu L$  volume of each was injected in triplicate into a LC-8 column and eluted with 1.5 mL/minute of 50:38:12% water/methanol/acetonitrile. Quantitation was obtained by comparison of the peak areas to that obtained when the same methanol stock solution was analyzed in a like manner but without flame sealing. The results are presented in Table 15.

For HMX, the four sealed ampules were significantly higher in concentration at the 95% confidence level than the unsealed stock solution by about 3%. For RDX, two of the sealed ampules were significantly higher than the other two and the unsealed stock. The average ampule concentration was again about 3% higher than the unsealed stock solution. For TNT, there was more variability in the replicates, which resulted in no significant difference between any of the ampules and the unsealed stock. For DNT, there were significant differences among the ampules, with ampule 2 being lower then the other three. This result is caused by one very low value in the three replicates. Even so, the average concentration of the ampules is again about 3% higher than the unsealed stock.

If the result for DNT in ampule 2 is ignored, the mean values for the stock solution are lower than the mean for any of the ampules for all analytes.

The value for ampule 1 is next lowest in all cases. Recall that ampule 1 was sealed immediately and not allowed to stand in the freezer for 30 minutes prior to sealing as were the others. It appears that a small amount of methanol evaporated during the 30 minutes the ampules were cooled in the freezer, resulting in a slight but measurable increase in concentration for all four analytes. Since the ampule that was sealed immediately was only significantly different from the unsealed stock for one analyte, it appears that the major portion of the evaporation did not occur during the sealing process itself, but rather in the standing. Since the vapor pressure of methanol is reduced from about 112 torr (14.9 kPa) at 25° C to only 28 torr (3.7 kPa) at 0°C, the majority of the evaporation probably occurred while the solution was cooling rather than after it reached the final temperature. Thus ampules 2, 3 and 4 were not significantly different from each other even though they were sealed several minutes apart, resulting in slightly different standing periods.

In conclusion, it appeared that sealing the methanol solutions in glass ampules could be used to ensure that evaporation did not cause the collaborative 'est participants to receive spiking solutions that differed in analyte concentrations. In addition, if the solutions were cooled in the freezer before the ampules were filled, the small amount of evaporation that was observed could be reduced to insignificant levels. A test of the long-term stability of methanol solutions of these analytes was also conducted. A solution was prepared with HMX, RDX, TNT and DNT concentrations of 279, 310, 215 and 160  $\mu g/L$ . It was sealed as described above, except that a capped flask of the solution was cooled in the refrigerator prior to being placed in a glass ampule and flame-sealed. This solution was allowed to stand in the refrigerator in the dark for 5 months. It was then opened and analyzed using RP-HPLC with a LC-8 column and the ternary eluent described earlier. The mean determined concentrations of three replicates for HMX, RDX, TNT and DNT were 273, 316, 212 and 163  $\mu$ g/L, respectively. Clearly these analytes were stable in methanol solution over this 5-month period.

## **PART 2. COLLABORATIVE TEST**

#### **PROTOCOL STRATEGY**

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A number of important decisions were made in setting up the analytical protocol for the collaborative test. Since the rationale behind these decisions is not obvious in many cases, a discussion was considered helpful. The following comments are presented in roughly the same sequence as the procedural steps in the protocol (Appendix C).

The style of the protocol is that of a very detailed recipe. In fact, it is so detailed as to be insulting to any competent analyst because it ignores his or her judgment in even the most trivial matters. There is an excellent reason for this approach, namely the need to focus attention on the performance of the test method alone. Consequently, it was necessary to eliminate or control unknown sources of experimental error by requiring strict adherence to the protocol. The protocol itself explains to the analyst the reasons for such rigidness. All deviations from the procedure had to be cleared with Tom Jenkins at CRREL. For similar reasons, the collaborative test was to be handled by a single analyst in each laboratory. Different analysts certainly perform with different levels of skill; having multiple analysts would only reduce our ability to derive useful information from statistical evaluation of the data.

The standards and water matrices shipped from CRREL and the standards prepared within each laboratory had to be stored in the dark and at a temperature of around 4°C. These measures were necessary to prevent photochemical or biological degradation of the analyte species in these materials, and to reduce solvent evaporation from standards that were used throughout the study. Some of these solutions were more susceptible to changes than others. For example, biological activity is completely inhibited in methanol solutions but not in aqueous ones. The *Preparation of Aqueous Matrices* section below discusses other precautions taken to minimize this problem.

The instrumentation required for the HPLC method and also the collaborative study were not

the ultimate in state of the art quality. Rather, the method was constructed around routine instruments that most laboratories were likely to have already, especially the AAPs, which will be using this method routinely to test their wastewater purification systems. We chose isocratic liquid chromatography using a single-wavelength UV absorption detector and a digital electronic integrator. Quantitation using electronically integrated peak areas was required because other approaches to area measurement are much more labor intensive. It was unlikely that the HPLC method would be accepted as a standard method if an integrator were not used. The reagent solutions were prepared as follows:

1. The sample modifier was 76% methanol and 24% acetronitrile (V/V). An equal volume of this solvent was added to each aqueous sample. The mixture was prepared using volumetric pipettes rather than volumetric flasks to minimize systematic differences with the mobile phase because of volume contraction. Dilution of the samples with this solvent, rather than with methanol alone, eliminates a negative peak that elutes just before HMX and results in unpredictable integration.

2. The HPLC mobile phase was 50% water, 38% methanol and 12% acetonitrile (V/V/V). Graduated cylinders were used to prepare this solvent. It also had to be prepared daily because bacterial growth was not insignificant even with so much methanol present. A substantial bacterial population clogged the inlet filters of the HPLC. An additional reason for daily preparation was that selective evaporation of one of the solvent components was possible. This would lead to a systematic change in the retention volumes of the analytes as the solvent composition changed. For storing the column after use, pure methanol was used. This fully inhibits bacterial activity.

3. Individual-analyte stock, combined-analyte working stock and working standards were prepared as follows. First, working standard concentrations were selected in the range of concentrations of interest for the collaborative study. Then, stock standard concentrations and dilution factors were chosen to minimize the number of transfers necessary to prepare the working standards and to minimize the errors introduced by volumetric tolerances. To dissolve the SARM solids, methanol was adequate for DNT and TNT, but not for RDX and HMX, which needed 40% acetonitrile. This difference in solvent composition had a negligible effect on the working standards. Creation of the combined-analyte stock entailed a 40-fold dilution with methanol of the RDX and HMX stock solutions. Thus, this combined stock contained only 1% acetonitrile. The next dilution down to the working standards further reduced this level.

Each aqueous matrix was spiked at low, medium and high levels. The particular levels were selected to cover the range of concentations likely to be found in treated munitions wastewaters and in contaminated natural waters: about 30 to 500  $\mu$ g/L. This range extends roughly from 20 to 30 times the detection limits estimated, in the method development phase, by the Hubaux and Vos (1970) method. Having analytical results from three concentration levels permits evaluation of accuracy and precision near to and far from the detection limits. Actually, spikes of four different concentrations were used. Two of these spike levels, either the highest two or the middle two, were close in value-no more different from each other than a factor of 1.15. These two spikes together represented the high or medium concentration level respectively. The other two spikes were set off by factors of at least 0.3 and as much as 2 or more. For example, for matrix B the DNT analyte spike levels were 61.4, 76.8, 115 and 128  $\mu$ g/L; for RDX the levels were 74.3, 248, 273 and 372  $\mu$ g/L. For DNT, the two high values are together the high range; for RDX, the two middle values are the medium range.

The purpose of having two closely spaced concentrations is so that our chosen statistical evaluation method, called the Youden two-sample chart, can be applied to the data. This method displays graphically the relative magnitudes of systematic and random errors that exist in the method.

The analytical work was divided into two segments: establishment of statistical control of the procedure and analysis of the spiked water matrices. During the first segment the analyst certified that the HPLC column was performing within its specifications, established working curves for each of the four analytes, and analyzed a test sample whose composition was specified by CRREL. If the results were acceptable, the analyst could proceed with the analysis of the spiked water matrices. Since these working curves would be the basis for all other measurements, the characteristics of these curves had to be well established using linear regression statistics. Theoretically, the UV detector response should be linear in concentration and have a zero intercept. Previous experience at CRREL in developing the HPLC method had shown that in practice this behavior did take place. Consequently, the laboratories participating in this study were expected to be able to achieve the same results. The advantages of linearity and a zero intercept are simplified daily calibration and significant time savings.

To construct the working curves, chromatograms of the four working standards and the blank were obtained in duplicate. The 10 injections were sequer randomly, a necessary prerequisite for value valuation. Unweighted linear regression analysis was applied to the data, using models with and without a zero intercept. Since many analytical chemists are not familiar with proper curve fitting procedures, step-by-step instructions were provided in the protocol. First, the model with an intercept was tested to determine whether it was adequately fit by a straight line. Existence of significant lack of fit required taking steps to ascertain the source of the nonlinearity and to correct it. After successful completion of this task, the regression line was tested to determine whether it passed through the origin. Again, action might have had to be taken to achieve this. The responses of the two blank samples were not included in the regression analysis because "zero" values force the fitted curve toward the origin. Omission of these data represent taking a conservative approach toward fitting the lines. The blanks were analyzed only to see whether significant contamination existed in the reagents.

An unweighted least squares approach was used instead of a weighted approach, which may be considered more generally appropriate, because the former was easier to carry out. Experiments at CRREL found that in the lower concentration ranges of the HPLC method the variances are homogeneous. This means that the weighted and unweighted approaches are equivalent for the concentration levels of interest.

The water matrices chosen for study were representative of waters for which the HPLC method was devised. The matrices were:

A. Final effluent from an AAP pink water treatment facility. It contained no detectable ana-

lytes and was spiked with TNT and RDX.

B. Distilled or deionized water from each participating laboratory's supply. Exact methods of preparation for these matrices are discussed in the *Preparation of Aqueous Matrices* section.

C. Uncontaminated well water from Canaan, New Hampshire. No detectable analytes were present and it was spiked with DNT and HMX.

D. Contaminated well water from an AAP site that contained RDX.

The ampule solutions used for spiking the water matrices were prepared and labeled in a manner that avoided creating a predictable pattern that an analyst might discern. The concentrations were not identical for every matrix nor were they sequenced to match their labels for each matrix—if such a precaution were not observed and an analyst discovered the pattern, subsequent samples could no longer be considered independent because the analyst's subjective judgment might influence how these later samples were handled.

The sequence in which the matrices were analyzed was randomized. All of the analyses on a given matrix had to be done in a single working day. This avoided the problem of day-to-day variability associated with remaking standards and recalibration. Four aliquots of the matrix were taken. Each was spiked using a different ampule spike solution. Another aliquot of the matrix was taken as the unspiked sample. Each of these solutions was processed in duplicate following the procedure described in the protocol. Then each of the processed samples was to be injected onto the HPLC column in duplicate. This meant a total of 20 chromatograms had to be obtained in addition to those necessary for establishing the working curve for that day (at least eight). More than an 8-hour day would have been necessary for completing all these tasks. To alleviate the time crunch, daily calibration was performed by preparation and analysis of only the highest concentration standard instead of all of the standards.

Relying on the response of a single standard seems somewhat risky. In this particular case the decision can be justified because the fundamental relationship between the response of the UV absorption detector and concentration of the analytes is well understood and is well controlled by the instrumentation. Furthermore, each participating laboratory would have already established that their instrument's response was linear and through the origin. Extensive experience at CRREL with the HPLC method has indicated that a linear response is to be expected. Hence, there was no need to verify this condition every day of the interlaboratory study. Instead, a singlestandard calibration approach was taken.

Triplicates of newly made working standard of high concentration were obtained. The mean peak areas for the four analytes were compared with the confidence intervals around the working curves previously established. Detailed instructions for carrying out this comparison were given. If no differences were found, the analyses could begin. A significant difference would indicate either systematic error in preparation of the standard or instrumental response drift. To distinguish between these two possibilities, a second set of triplicates then were run using another newly made high standard. The mean of this set was tested against the working curve. If a difference still existed, another statistical test was performed-a t-test for equivalence between the two sets of triplicates. If this last test indicated no difference, then nothing was wrong with the way the standard had been prepared and instrumental response drift was suspected. The analyst could then proceed with analysis of the spiked water samples. If the t-test indicated a difference, then either the instrument was subject to strong short-term drift or noise or there was insufficient reproducibility in the analyst's technique of solution preparation. At this point, CRREL would have had to be consulted.

Once the analysis had been shown to be under statistical control on that day, the spiked solutions could be prepared and analyzed. As stated above there were 20 separate aqueous samples to be analyzed. Five replicates of the high concentration working standard prepared that day were also analyzed. These 25 analyses were done in random sequence. The day's working curve for each analyte was based on the mean response of the five replicates of the standard and assuming a zero intercept.

#### PREPARATION OF METHANOL SOLUTIONS

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Standard Analytical Reference Materials (from LCWSL) of TNT, RDX, HMX and DNT were dried in a vacuum dessicator until successive weights did not differ by greater than 0.2 mg (approximately 24 hours). A sample of each solid (about 100 mg) was carefully weighed out on weighing paper to the nearest 0.01 mg, transferred to individual volumetric flasks and diluted to volume with a solution of 90% methanol/10% aceto-
Table 16. Concentrations (mg/L) of HMX, RDX, TNT and DNT in ampules supplied to each participant.

| Solution  | НМХ   | RDX   | TNT   | DNT   |
|-----------|-------|-------|-------|-------|
| Test      | 27.85 | 30.98 | 21.46 | 16.01 |
| A1 and D4 | 4.46  | 9.91  | 3.43  | 5.12  |
| A2 and D3 | 13.37 | 19.82 | 10.30 | 8.96  |
| A3 and D2 | 14.70 | 22.30 | 11.67 | 10.24 |
| A4 and D1 | 22.28 | 49.56 | 17.16 | 12.80 |
| B1 and C4 | 6.68  | 7.43  | 5.15  | 6.14  |
| B2 and C3 | 22.28 | 24.78 | 13.73 | 11.52 |
| B3 and C2 | 24.51 | 27.26 | 15.44 | 12.80 |
| B4 and C1 | 33.42 | 37.17 | 8.58  | 7.68  |

nitrile. The concentrations of HMX, RDX, TNT and DNT in these stock standards were 111.40, 123.92, 85.83 and 64.04 mg/L respectively.

The spiking and test solutions for the collaborative study were prepared from these four stock standards by combining various volumes of each using volumetric pipettes and diluting to volume with methanol in ground-glass-stoppered volumetric flasks. To further prevent loss of methanol by evaporation, the tops of the stoppers were carefully wrapped with Parafilm. For the test solution, 25 mL of each stock standard was used with no additional dilution. For the eight spiking solutions, the volumes of individual stock solutions used varied from 10 to 100 mL. The concentrations of the four analytes in the resulting solutions are presented in Table 16.

These solutions were cooled overnight in a refrigerator and then approximately 5 mL was dispensed into individual ampules using an automatic pipet that was cleaned carefully with methanol before use and between individual solutions. These ampules were labeled as shown in Table 16. It should be noted that two types of ampules with different labels were filled from the same solution. For example, the contents of ampules labeled A1 and D4 were identical, although the participents in the collaborative test were not informed of this.

A set of sealed ampules consisting of one test solution, 16 ampules labeled A1-A4, B1-B4, C1-C4 and D1-D4, and an empty ampule were placed in a square plastic container. The outside of the ampules were packed with paper towels so they wouldn't break during shipment. The ampule sets were stored in a refrigerator in the dark overnight.

# Table 17. Concentrations $(\mu g/L)$ of analytes in aqueous matrices.

| Matrix   | НМХ | RDX  | TNT  | <u>DNT</u> |
|----------|-----|------|------|------------|
| A        | _   | 55.6 | 38.1 | ~          |
| B•       | -   |      | -    |            |
| С        | 124 | ~    | -    | 71.7       |
| <u>D</u> |     | 112  | _    |            |
|          |     |      |      |            |

Distilled or deionized water from each location.

#### PREPARATION OF AQUEOUS MATRICES

Matrix A was prepared on 2 September from water collected earlier at the Iowa AAP. This water was collected from the effluent of the second carbon column from a pink water treatment line. This carbon column had just been placed in operation and analysis of the water indicated that the concentrations of HMX, RDX, TNT and DNT were below detection limits.

This water and sufficient well water to bring the volume to 18 L were combined and sterilized by autoclaving in a 23-L (5-gal.) glass jug for  $2\frac{1}{2}$  hours at 127 °C. The jug was cooled and spiked with 8 mL of the TNT stock solution and 20 mL of a 50-mg/L RDX solution to recreate concentrations of these analytes found at Iowa AAP in effluent from the first carbon column. The pH of the solution was reduced to approximately 5.5 with 1 N HCl to inhibit hydrolysis reactions. The concentration of the analytes in solution are shown in Table 17.

We autoclaved 15 1-L glass bottles as described above, cooled and filled them with the above solution and labeled them "Matrix A." These bottles were immediately placed in a refrigerator in the dark until shipment. Sample bottles for the other two matrices were prepared and stored the same way.

Matrix C was prepared on 2 September from well water collected in Canaan, New Hampshire. We autoclaved 18 L of this water for  $2\frac{1}{2}$  hours at 127 °C, cooled it and spiked it with 20 mL of the DNT and HMX stock solutions. The resulting concentrations of these analytes are presented in Table 17. The pH of this solution was also adjusted to 5.5 with 1 N HCl.

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|               | Samples  | Matrix analyzed |           |        |        |  |  |
|---------------|----------|-----------------|-----------|--------|--------|--|--|
| Laboratory    | received | A               | B         | Ċ      | D      |  |  |
| USEPA, EMSL   | 9 Sep    | 16 Sep          | 22 Sep    | 21 Sep | 20 Sep |  |  |
| AEHA          | 7 Sep    | 15 Sep          | 16 Sep    | i4 Sep | 13 Sep |  |  |
| CRREL         | 6 Sep    | 27 Sep          | 21 Sep    | 26 Sep | 22 Sep |  |  |
| UNH           | 6 Sep    | 26 Sep          | 28 Sep    | 21 Sep | 27 Sep |  |  |
| LCWSL         | 6 Sep    | 18 Oct          | 14 Oct    | 17 Oct | 19 Oct |  |  |
| Iowa AAP      | 10 Sep   | 18 Oct          | 14 Oct    | 11 Oct | 16 Oct |  |  |
| Louisiana AAP | 7 Sep    | 29 Sep          | 27 Sep    | 28 Sep | 30 Sep |  |  |
| Holston AAP   | 8 Sep    | 22 Nov          | 30 Nov    | 1 Dec  | 29 Nov |  |  |
| Radford AAP   | 7 Sep    | 12 Oct          | 14,18 Oct | 12 Oct | 14 Oct |  |  |

Table 18. Timetable for receipt of samples and analysis of aqueous matrices.

Matrix D was prepared on 1 September from contaminated well water from the Milan AAP. Upon analysis, this water had an RDX concentration of about 72  $\mu$ g/L, while the concentration of the other analytes was below detection limits. Since our experience indicated that RDX is destroyed when the water is autoclaved, this solution was not subjected to this procedure but was mixed with autoclaved well water to obtain a sufficient volume for the test. A small amount of the RDX stock solution was added to increase the concentration of RDX above 100  $\mu$ g/L (Table 17). Since the solution was not sterile, it was reduced to pH 3.5 with 1 N HCl to prolong its stability.

#### SHIPMENT OF SAMPLES

Samples were shipped to the various participants on 6 September 1983. All samples were kept on ice in the dark during shipment. The samples that went to Louisiana AAP were shipped by air freight and were received the following day (Table 18). Samples to all other locations were delivered by car and care was taken to keep the samples cold during transit. Samples arrived at the various locations between 6 and 10 September (Table 18).

#### SUMMARY OF PROTOCOL FOR COLLABORATIVE STUDY

The protocol (Appendix C) consisted of a detailed procedure that the participating laboratories were required to follow explicitly. Strict adherence was essential in order for the statistical analysis of results to provide unbiased estimates of method performance. The reasoning behind this is that unknown sources of random or systematic error had to be eliminated insofar as possible. Any deviations from the protocol had to be cleared by CRREL.

A single analyst in each laboratory was responsible for all aspects of this study, from receipt of materials through data analysis. All efforts were to be documented in duplicate in a project notebook. Detailed instructions concerning the following items were given:

- 1. Inspection of materials received from CRREL.
- 2. Storage of these materials.
- 3. Required instrumentation and settings.
- 4. Hardware and glassware-types and cleaning.
- 5. Chemical reagents.
- 6. Preparation and storage of HPLC mobile phase and calibration standards.
- 7. Conditioning of HPLC column and test of its performance.
- 8. Practice run through analytical procedure using a test sample.
- Spiking and analysis of water matrices (four matrices at four spike concentration levels).
- 10. Data calculations and reporting.

The analytical work was done in two steps. The analyst first spent some time becoming familiar with the procedures. During this period working curves for each of the four analytes were prepared and steps taken to establish that they were linear and passed through the origin. A test sample whose composition was specified by CRREL was analyzed. If the results were acceptable, the analyst could procede with the analysis of the collaborative test samples. These statistical procedures and their rationale were described thoroughly in the protocol.

The second portion of the work consisted of analysis of the four water matrices; three of these were provided by CRREL and the fourth was the laboratory's own reagent-grade water. These matrices were analyzed directly and after spiking with standard analyte solutions. Four different spiking solutions were provided. Each contained all four analytes. All of the work associated with a given water matrix could be performed in a single workday; the chronological order for matrix analysis was random. The daily procedure consisted of the following:

1. The most concentrated stat dard was analyzed and its response was statistically compared with the previously established working curves.

2. Barring unresolved discrepancies in the first step, the spiked matrix samples were prepared: four separate spiked samples and one unspiked sample.

3. Each of these solutions was processed in duplicate and each of these twin processed samples was injected in duplicate onto the HPLC column (20 total injections) along with five replicates of the highest standard; the injection sequence was random.

4. The day's working curve for each analyte was based on the mean response of the five replicates of the highest standard, assuming a zero intercept.

5. The concentrations for the 20 injections of spiked and unspiked water samples were calculated.

#### STATISTICAL ANALYSIS

#### Rationale

A primary goal of this collaborative study was to assess the capability of the HPLC method to determine DNT, TNT, RDX and HMX concentrations under typical environmental conditions. The performance characteristics evaluated were accuracy, repeatability (precision within individual laboratories ), and reproducibility (precision between laboratories) (Youden and Steiner 1975). A number of standard statistical tests were applied to the data to extract these summary characteristics (Youden and Steiner 1975). It must be emphasized that, although these calculations may seem straightforward, it is often necessary to apply chemical intuition to assist in making reasonable decisions.

The sequence of tasks was roughly: inspection of raw data and construction of Youden two-sample plots to obtain a "feel" for overall performance, rejection of extreme values (outliers), analysis of variance to extract estimates of precision,

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and regression analysis to evaluate overall accuracy. Most calculations were made using the computer program MINITAB, which is available on one of the mainframe computers at the University of New Hampshire.

The nine participating laboratories reported data in a uniform format using a form provided with the collaborative test protocol. For each laboratory there were 320 individual concentration values in micrograms per litre (four analytes  $\times$ four aqueous matrices × five analyte concentration levels per matrix  $\times$  two aliquots processed per spiked solution × two injections per aliquot). These data sets are collected in Table A7. After loading this information into a computer file, it was proofread scrupulously to correct transcription errors. Individual laboratories were identified only by number to avoid potential bias where value judgment was required. All laboratories followed the required analytical protocol except for laboratory 7; consequently, this one was rejected. By requiring adherence to the protocol we assured that every laboratory would have the same general sources of variation. Since laboratory 7 followed its own protocol, its results were subject to different sources of error; therefore, laboratory 7's data set and that of the other laboratories are not comparable.

An initial impression of analytical performance can be gleaned from inspection of the results of the test sample analysis, which had been a prerequisite for carrying out the water sample analyses. Table 19 lists individual results, means, standard deviations and actual concentrations. The differences between the mean determined concentrations and the actual values is quite small: less than

Table 19. Determination of test sample composition, concentrations in  $\mu g/L$ .

| Laboratory         | DNT            | TNT   | RDX   | НМХ   |
|--------------------|----------------|-------|-------|-------|
|                    | 167.0          | 210 7 | 104 7 | 769.4 |
| 1                  | 157.0          | 210.7 | 304.7 | 268.4 |
| 2                  | 162.0          | 217.0 | 315.0 | 275.0 |
| 3                  | 156.6          | 212.9 | 336.1 | 237.8 |
| 4                  | 1 <b>60</b> .0 | 220.7 | 306.6 | 270.3 |
| 5                  | 152.1          | 220.6 | 315.5 | 249.2 |
| 6                  | 148.0          | 193.0 | 265.0 | 256.0 |
| 7                  | 190.3          | 279.5 | 336.0 | 288.9 |
| 8                  | 164.0          | 187.0 | 321.0 | 259.0 |
| 9                  | 155.9          | 208.6 | 311.4 | 278.1 |
| Mean               | 160.7          | 216.7 | 312.4 | 264.7 |
| Actual value       | 160            | 215   | 310   | 279   |
| Standard deviation | 12.1           | 26.3  | 21.1  | 15.8  |
| % RSD              | 7.8            | 7.0   | 4.1   | 3.2   |

1% for all analytes but HMX, for which the difference is still less than 5%. The relative standard deviations are not unreasonably large. It must be recognized that these values represent the relative performance across the laboratories; consequently, we may expect large scatter.

Detailed inspection for gross errors was the next step. This was aided by calculation of the mean concentration for each set of four replicate analyses on each sample. (Henceforth, the word "sample" will refer specifically to the solutions from which the two aliquots were withdrawn for processing. Thus, the "four replicates" represent the two aliquots, each of which was injected into the HPLC in duplicate.) These means were compared with the concentrations that should have been found (henceforth called the "true" values), given the concentrations of the added spiking solutions and the amount of analyte already present in each matrix. This comparison was made by looking simultaneously at the results of all the participants for a given sample and analyte (see Table A8). In addition, each set of four replicates was inspected for internal consistency. Any datum that seemed to be dimparate from its group was checked against the original lab notebook. Only two out of about 30 suspect values were resolved in this manner. Transcription errors were the cause. In one case we found that two data columns in a laboratory's report had been mislabeled. Although this inspection approach did find some errors, it is clearly very inefficient.

A comment regarding the definition of "true value" is in order. Spiking solutions were propared using SARM solids. The quality of these standards is not as good as NBS primary reference materials, but the assays are certified to be within 98 mole %. As far as the collaborative test is concerned, the assay of these standards should not affect the evaluation of interlaboratory precision because the SARM sent to each collaborating laboratory was prepared from the same batch. There could be a small effect on accuracy because the SARM used for the spiking solutions was from a different batch than the SARM distributed to the collaborators.

For 11 of the 16 analyte-matrix combinations, diluted solutions of SARM were added to a material in which no analyte was already present. In this case the accuracy can be affected only by the propagation of error through the SARM assays and volumetric measurement tolerances (assuming no errors in manipulation). For the remaining five analyte-matrix combinations (DNT matrix C, TNT matrix A, RDX matrices A and D, HMX matrix C), analyte was already present. These existing levels were determined at CRREL by the HPLC method that is under scrutiny in this collaborative study Because of the added errors inherent in analytical measurement, the "true values" derived in these five cases are subject to a larger degree of uncertainty.

#### Youden two-sample plots

To aid further with inspection of the results and to begin to consider the problem of outliers. Youden two-sample plots were constructed for each analyte (Fig. 7). A Youden plot (Youden and Steiner 1975) concisely summarizes the relative amount of systematic error between laboratories in comparison to the amount of random error in the method and also indicates the relative accuracy of the results. In these diagrams, the reported concentrations for two of the spiked solutions are plotter' against each other. The two solutions involved were those two that were purposely made similar to each other in concentration. (See Protocol Strategy section for details.) In order to display these plots in an easily digestible fashion, the data were contracted to permit display of all matrices on a single set of axes: the values plotted were the means of the four replicate determinations, normalized to the true values (Table A9). Eight points were excluded because they were so far off from the expected value and from the other measured values in that data set.

Each plot contains a large amount of information. The higher concentration spike was plotted versus the lower concentration in all cases. The origin of the solid axes locates the medians for the entire data set for that analyte. The shortened dashed axis locates the true values, which after normalization equal (1.0, 1.0). The medians have been used here instead of means because the former are not affected greatly by the few outlying points. Table 20 lists the median values. Both the tabulated values and the Youden plots show that the overall accuracy is quite good, the disparity being 3% or less for DNT, RDX and HMX, and less than 5% for TNT. The shapes of the Youden plot for DNT and TNT hug the 45° line. This indi-

#### Table 20. Grand medians for each analyte.

| Analyte | Low spike (range)   | High spike (range)  |  |  |  |
|---------|---------------------|---------------------|--|--|--|
| DNT     | 0.970 (0.719-1.094) | 0.982 (0.753-1.068) |  |  |  |
| TNT     | 0.957 (0.567-1.180) | 0.955 (0.798-1.072) |  |  |  |
| RDX     | 1.017 (0.601-1.293) | 1.030 (0.875-1.268) |  |  |  |
| нмх     | 0.990 (0.593-1.272) | 0.983 (0.854-1.167) |  |  |  |



Figure 7. Youden two-sample plots.

cates that systematic error between laboratories is larger than the method's random error. For RDX and HMX, the pattern is more circular, indicating that random and systematic errors are more nearly equivalent. Note that the relative amount of systematic error, as shown by the spread of points

along the 45° line, is roughly the same for all analytes but that the random error, as shown by the straight-line distances to the 45° line, is larger for RDX and HMX than for DNT and TNT. The most likely source of the systematic error is the calibration procedure. 

|        |         | Quadra |    |       |      |       |
|--------|---------|--------|----|-------|------|-------|
| Matrix | Analyte | (++)   | () | (+ -) | (-+) | Bias? |
| A      | DNT     | 3      | 3  | 2     | 0    |       |
|        | TNT     | 0      | 7  | 0     | 1    | Low   |
|        | RDX     | 3      | 3  | 0     | 2    |       |
|        | нмх     | 1      | 3  | 2     | 2    | High  |
| В      | DNT     | 2      | 5  | 0     | 1    | Low   |
|        | TNT     | 5      | 2  | 1     | 0    | High* |
|        | RDX     | 2      | 2  | 2     | 1    | -     |
|        | НМХ     | 2      | 2  | 0     | 3    |       |
| С      | DNT     | 4      | 2  | 0     | 1    | High* |
|        | TNT     | 4      | 4  | 0     | 0    | _     |
|        | RDX     | 2      | 3  | 1     | 2    |       |
|        | HMX     | 3      | 4  | 1     | 0    |       |
| D      | DNT     | 3      | 2  | 1     | 1    |       |
|        | TNT     | 5      | 1  | 0     | ł    | High* |
|        | RDX     | 4      | 2  | 1     | 0    | High* |
|        | НМХ     | 4      | 1  | 1     | 1    | High  |

Table 21. Number of laboratories that fail into each quadrant of the Youden plots for individual matrices.

Biased with respect to data medians but not to "true" values.

Method performance for each matrix may be estimated by counting the number of laboratories that fall into each quadrant of the Youden plots (Table 21). By comparing the relative number of points in quadrant I (+ +) vs quadrant III (--), one can identify where bias exists for particular analytes and particular matrices. The only clear cases of low bias are for TNT and HMX in matrix A (treated pink water) and DNT in matrix B (laboratory water) and of high bias for HMX in matrix D (RDX-contaminated ground ster). Several other combinations are biased with respect to the grand medians, but are instead clustered around the true values. Hence, we did not consider these data to be outliers. The total number of points in the (+ +) and (- -) quadrants compared to the (+ -) and (- +) clearly supports the statement that the major errors are systematic rather than random. Of course, we must remember that only the most extreme outliers have been eliminated from the data at this point.

#### **Rejection of outliers**

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More sophisticated statistical methods had to be applied at this point to help us decide whether outliers existed and whether or not to reject them. There is a need to be cautious about wielding these methods, as Youden suggests (Youden and Steiner 1975): Our task is that of presenting a realistic picture of the population of laboratories. This last objective has to be balanced against the distortion of the picture that would occur from keeping a result so out of line that the estimate of error does not mirror the real merit of the analytical method... The inclusion in the statistical analysis of even one or two points emphatically apart from the main pattern considerably increases the estimates of standard deviation...obtained. The danger is that a really promising analytical method may fail to receive a positive recommendation for adoption because of a lapse by one or two collaborators.

The particular reasons for excluding outliers are 1) that the HPLC method is being tested here, not the individual laboratories, 2) there is no other way to find mistakes that are not obvious by inspection, and 3) analysis of variance assumes homogeneity in the data set variance.

Lastly, it is inevitable that a data set this large will contain some outliers. Inspection found many instances of suspect values that could not be rejected or corrected by reference to the laboratory notebooks. The collaborators should be commended for their honesty in reporting data that they could have censored had they observed apparently errant values. Rejection of outliers is more safely done with reference to the entire population of analytical results rather than with reference to the results within a single laboratory.

The particular statistical tests applied are described in detail in Youden and Steiner (1975). The

tests were applied in the following sequence: ranking test on laboratories, Dixon's range test on individual data values, range test for homogeneity of variance among laboratories, and Cochran's test for homogeneity of variance between replicates. For these calculations, a single analytical datum is defined as the average result on duplicate injections from a given vial. Only the results of these tests in terms of outliers rejected will be discussed here.

#### Ranking test

The ranking test for laboratories was applied to the collection of means of the four replicated determinations on each spiked sample (Table A8). For each different sample, laboratories were ranked according to their reported concentrations. These rankings were then summed across all the samples. The distribution of total scores was compared to limiting scores expected for the case of completely random errors. Any laboratory having a score outside these limits indicates systematic error. Only one data set could be eliminated without ambiguity: RDX for laboratory 5. In several other instances, the ranking test indicated systematic error, but inspection of the data led us to decide not to reject them because only a few of the concentration values were extreme. These could be eliminated on an individual basis instead of by eliminating the entire laboratory, which would be throwing away many valid data points.

#### Dixon's test

Next, Dixon's test was used to uncover individual stray data. To apply this test and in preparation for the analysis of variance, we decided to define one "analytical value" as the average of the responses for the two duplicate injections from the same aliquot sample. This reduced the number of apparent replicates per sample to two instead of four. Although averaging eliminates information on the variability between duplicate injections of the same sample, it mimics the probable approach that most analysts would take in practice, namely to base their quantitative result on the average of (at least) two injections instead of just one injection.

Dixon's test is sensitive to values that lie outside the range expected in the case of randomly distributed results. When an individual datum was flagged for rejection, its duplicate was also rejected. (Recall that each datum here represents an analytical measurement of one of two duplicate aliquots removed from each sample.) In order to maintain balance in the data sets, we chose this procedure rather than the alternative of filling in for the rejected datum by calculating an expected value. Table 22 lists the numbers of pairs of values that

|  | Number rejected |     |     |     |  |  |
|--|-----------------|-----|-----|-----|--|--|
| l.aboratory  | DNT             | TNT | TDX | НМХ |  |  |
|  |                 |     |     |     |  |  |
| 1  | 3               | 1   | 1   | 1   |  |  |
| 2  | 0               | 0   | 1   | 2   |  |  |
| 3  | 2               | 1   | 1   | 1   |  |  |
| 4  | 0               | 0   | 0   | 0   |  |  |
| 5  | 1               | 2   | 18* | 2   |  |  |
| 6  | 0               | 1   | 6   | 171 |  |  |
| 8  | 5               | 5   | 6   | 171 |  |  |
| 9  | Ó               | 0   | Ó   | 0   |  |  |
| Total rejected   | 11              | 10  | 33  | 40  |  |  |
| Number per laboratory before rejection                 | 17              | 17  | 18  | 17  |  |  |
| Total pairs before rejection                           | 136             | 136 | 144 | 136 |  |  |
| Percent rejected                                       | 8               | 7   | 23  | 29  |  |  |
| Percent rejected disregarding<br>rejected laboratories | 8               | 7   | 12  | 6   |  |  |

Table 22. Catalogue of aliquot pairs rejected on basis of Dixon's test.

\* Entire laboratory rejected via laboratory rank test.

† Entire laboratory rejected because at least half of individuals were outliers.

were rejected. The relative number of outliers for each analyte is between 6 and 12% when excluded laboratories are not considered part of the total. This does not represent a significant loss to the data set and seems to be typical for collaborative studies (Horwitz 1982).

In some of these cases we observed that the results for all four analytes in a given sample were identified as outliers and that the amount of deviation was similar in magnitude and direction. This is a clear indication of mishandling of the sample during processing, such as erroneous use of volumetric glassware.

Note that only those samples with non-zero concentration levels were considered. Specifically, 3 out of the 20 samples (four matrices  $\times$  five spike levels) contained no DNT, TNT or HMX, and two contained no RDX. These samples were not included because in most cases laboratories reported duplicate "0.0" concentrations. Since the variance here is zero, the within laboratory variance would be decreased in the analysis of variance tests because of addition of degrees of freedom without concommitant increase in the sum of squares. Hence, inclusion of these data falsely sensitizes the tests for homogeneity of variance and the analysis of variance.

#### Range lest

We found the variance among laboratories to be homogeneous by using a range test based on the sums of the data for the duplicate aliquots. A range was calculated for laboratories within each sample. The maximum range was compared with the sum of all the ranges. Only RDX failed this comparison. Although dropping one sample did result in passing the test, we decided that this was undesirable since a large number of values had already been eliminated by previous tests. Furthermore, analysis of variance is a robust test—it can handle a small amount of heterogeneity without risk.

#### Cochran's test

Finally, Cochran's test compares the maximum variance between the duplicate aliquots with respect to the total sum of squares of duplicates. The results were that DNT and TNT were homogeneous after rejection of the pairs of outliers identified by Dixon's test and that RDX and HMX were slightly heterogeneous. No data, however, were excluded from the latter two analytes because too many values had to be dropped to pass the test. This artificially contracts the variance to levels that are not realistic. Relative to DNT and TNT, RDX and HMX should have larger random error components as indicated by the Youden plots.

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Table A10 lists the entire data set, showing which values were rejected using the statistical evaluations described above.

#### Analysis of variance

Since outliers had been rejected and the data sets were now adequately homogeneous, analysis of variance (ANOVA) was carried out to separate individual contributions to the overall variance (Table 23). Several items in Table 23 must be explained. The degrees of freedom change for each analyte for two reasons: different numbers of rejected outliers and different numbers of samples (17 or 18). Note that for all analytes the laboratories are significantly different from each other. Frankly, we expected this result since the vast majority of collaborative studies show this trend (Youden and Steiner 1975). Furthermore, it is reasonable to expect more variability among several laboratories than within any given laboratory. For RDX and HMX, the laboratory-sample interaction is also significant, indicating an inconsistent bias among laboratories. The size of this effect is much smaller than the consistent laboratory bias, however.

This table also shows the grand average of the measured concentrations, the standard deviation of replication (the within-laboratory standard deviation or the repeatability), and the percent Relative Standard Deviation (RSD). These last values are all between 5 and 9%. The reason that the percent RSDs for RDX and HMX are lower than those of the other analytes is that the average concentrations measured for RDX and HMX were two to three times greater than those for TNT and DNT. Since previous studies at CRREL, as well as this study, have demonstrated that the variance in this concentration range is independent of concentration, the RSD must decrease with increasing concentration.

To demonstrate the effect on ANOVA of not rejecting outliers, the uncensored data set for RDX and HMX was subjected to ANOVA. This is shown in Table 24. The tangible result of ignoring outliers is that all mean square values are larger. Specifically, the interaction between laboratories and samples becomes much stronger, and the standard deviation of replication and the % RSD increase by factors of about 2.5. These values seem uncharacteristically large and give the impression that the HPLC method cannot be expected to achieve precisions better than 12%. The uncen-

#### Table 23. Analysis of variance.

|              | SS               | DF        | MS      | F      | SS             | DF       | MS       | F      |
|--------------|------------------|-----------|---------|--------|----------------|----------|----------|--------|
|              | DNT              |           |         |        |                | ۲ř       | T        |        |
| Total        | 3,300,508        | 250       |         |        | 3,474,037      | 252      |          |        |
| CF           | 2,848,709        | 1         |         |        | 2,869,867      | 1        |          |        |
| Labs         | 1,385.69         | 7         | 197.96  | 3.76•  | 6,279.94       | 7        | 897.13   | 10.76* |
| Samples      | 438,125          | 16        |         |        | \$75,532       | 16       |          |        |
| Replicates   | 6,574.84         | 125       | 52.60   |        | 10,500.64      | 126      | 83.33    |        |
| Interaction  | 5,713.47         | 101       | 56.57   | 1.08†  | 11,857.42      | 102      | 116.25   | 1.391  |
| Lab × sample |                  |           |         |        |                |          |          |        |
|              | Gra. 1 Avera     | ge = 10   | 6.75    |        | Grand Avera    | ge = 10  | 6.72     |        |
|              | Std. dev. of r   | eplicatio | on =    |        | Std. dev. of r | eplicati | on =     |        |
|              | Replica          | te MS :   | = 7.25  |        | Replica        | ie MS    | = 9.13   |        |
|              | % RSD ≈ 6.       | 79        |         |        | % RSD = 8.     | 55       |          |        |
|              | RDX              |           |         |        |                | HN       | 4X       |        |
| Total        | 21,591,195       | 222       |         |        | 10,253,207     | 192      |          |        |
| CF           | 16,815,188       | 1         |         |        | 7.883.430      | 1        |          |        |
| Labs         | 30,045           | 6         | 5,007.5 | 22.8 • | 7,525.31       | 5        | 1,505.06 | 14.34* |
| Samples      | 4,688,011        | 17        |         |        | 2,333,177      | 16       |          |        |
| Replicates   | 24,326.27        | 111       | 219.2   |        | 10,075.24      | 96       | 104.95   |        |
| Interaction  | 33,624.73        | 86        | 391.0   | 1.78*  | 18,999.45      | 74       | 256.75   | 2.45*  |
| Lab × sample |                  |           |         |        |                |          |          |        |
|              | Grand Avera      | ge = 21   | 75.22   |        | Grand Avera    | ge = 20  | 2.63     |        |
|              | Std. dev. of a   | replicati | 0n =    |        | Std. dev. of r | eplicati | on =     |        |
|              | √ <b>Replice</b> | ite MS    | = 14.8  |        | Replica        |          |          |        |
|              | % RSD = 5        | 38        |         |        | % RSD = 5.     | 06       |          |        |

\*Significant at 0.99 probability.

† Not significant.

|              | <u>SS</u>    | DF        | MS        | F      | \$5          | DF     | MS        | F      |
|--------------|--------------|-----------|-----------|--------|--------------|--------|-----------|--------|
|              | RD)          | (         |           |        |              | H      | мх        |        |
| Total        | 30,478,680   | 288       |           |        | 15,911,994   | 272    |           |        |
| CF           | 23,686,095   | 1         |           |        | 12,012,847   | 1      |           |        |
| Labs         | 143,535      | 7         | 20,503.57 | 17.7 • | 88,077.3     | 7      | 12,582.46 | 20.8 • |
| Samples      | 6,097,818    | 17        |           |        | 3,303,801    | 16     |           |        |
| Replicates   | 167,219      | 144       | 1,161.24  |        | 82,211.3     | 136    | 604.5     |        |
| Interaction  | 384,033      | 119       | 3,227.17  | 2.78*  | 425,057.4    | 112    | 3,795.1ó  | 6.28*  |
| Lab × sample |              |           |           |        |              |        |           |        |
|              | Grand Avera  | age = 2i  | 86.78     |        | Grand Avera  | ge = 2 | 10.15     |        |
|              | Std. dev. of | replicati | on =      |        | Std. dev. of | -      |           |        |
|              | Replic       | ate MS    | = 34.1    |        | Replice      | ite MS | = 24.59   |        |
|              | % RSD = 1    | 1.9       |           |        | 7 RSD = 1    | 1.7    |           |        |

Table 24. Analysis of variance for uncensored RDX and HMX data.

\*Significant at 0.99 probability.

| Table | 25.  | Repeatability | and | reproducibility | of | HPLC |
|-------|------|---------------|-----|-----------------|----|------|
| metho | d (4 | g/L).         |     |                 |    |      |

| Analyte | Repeatability | % RSD | Reproducibility | % RSD |
|---------|---------------|-------|-----------------|-------|
| DNT     | 7.25          | 6.8   | 7.66            | 7.2   |
| TNT     | 9.13          | 8.6   | 11.08           | 10.4  |
| RDX     | 14.80         | 5.4   | 20.80           | 7.6   |
| HMX     | 10.25         | 5.1   | 14.75           | 7.3   |

sored data sets for DNT and TNT were not subjected to ANOVA because there were so few outliers that the changes would have been minimal.

Next, the variance was segregated according to its sources, in particular, so we could calculate the reproducibility (between laboratory variance). This is accomplished easily using the mean square values from the ANOVA tables. The results are listed in Table 25.

The repeatability values in Table 25 represent the standard deviation to be expected for a single determination (based on duplicate injections) by the HPLC method when compared with all other results within one laboratory. The reproducibility values represent the standard deviation to be expected for a single determination by the HPLC method when compared with all other results from many laboratories. As expected, the reproducibility is the larger of the two values, although the magnitude of this difference is not unusually large. It should be recognized that the inclusion of values considered to be outliers would produce a greater increase in the reproducibility estimate than in the repeatability estimate. The reason for this expectation is that most outliers were identified according to their magnitude with respect to the rest of the data set (which contributes to reproducibility) and not according to the amount of variation between duplicates (which contributes to repeatability).

#### **Regression** analysis

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The last task was to evaluate accuracy by linear least squares regression analysis of "found" concentrations (y) plotted versus "true concentrations" (x). A perfectly accurate method should have an intercept of 0 and a slope of 1.00. Regression equations were determined for each of the four analytes in each of the four matrices using the data after rejection of outliers. The 16 equations are given in Table 26. Clearly, all slopes are quite close to the theoretically expected value of 1.00. Intercepts will be considered below.

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For each analyte, an analysis of variance was conducted according to the procedure described in Volk (1958) to test the hypothesis that the slopes for the four matrices were homogeneous. Another way of saying this is accepting the hypothesis means that the amount of deviation removed by fitting individual least squares lines for each matrix, over that removed by using a pooled slope for all four matrices together, is not statistically significant. As shown in Table 27, the hypothesis of homogeneity could not be rejected at the 95% confidence level for any of the analytes. In fact, the largest F ratio found was 1.74 for DNT, with a value of 2.65 required for rejection of the hypothesis. Based on these analysis, we concluded that each analyte could be represented by a single fitted curve regardless of sample matrix. These pooled equations are in Table 28.

Table 28 also shows the least squares equations for the model through the origin, i.e., the model in which the intercept is required to be zero. An Ftest as described by Youden (1951) was employed to test the hypothesis that the intercepts were equal to zero. For DNT and TNT, it was not possible to reject the hypothesis so we concluded that the model through the origin was the best one to describe the data. For RDX and HMX, the zero intercept hypothesis was rejected and equations with both intercept and slope were deemed best. Appropriate confidence intervals were calculated for the slopes, as shown in Table 29.

To interpret these results for the pooled data, we must remember that the regressions were of "found" concentration versus "true" concentration. Thus, a perfectly accurate method should have an intercept of 0.00 and a slope of 1.00. The intercepts for DNT and TNT have been shown above to be equivalent to 0. In the case of DNT, the slope of the fitted model, 0.986, is extremely close to the theoretically expected value. The small difference may arise from the fact that the SARM used to prepare the spiking solutions at CRREL was from a different batch than the SARM dis-

Table 26. Linear least squares regression equations for each matrix and each analyte (x and y are in  $\mu g/L$ ).

|          | DNT                | TNT                 |
|----------|--------------------|---------------------|
| Matrix A | y = 1.28 + 0.979x  | y = -8.26 + 0.964x  |
| B        | y = 3.20 + 0.909x  | y = -0.729 + 0.973x |
| С        | y = 1.14 + 0.998x  | y = -3.18 + 0.970x  |
| D        | y = 3.12 + 0.942x  | y = 3.14 + 0.960x   |
|          | RDX                | НМХ                 |
| Matrix A | y = 8.75 + 0.997x  | y = 1.93 + 0.959x   |
| 8        | y = 4.03 + 1.01x   | y = 8.69 + 0.978x   |
| С        | y = -0.803 + 1.00x | y = 6.88 + 0.951x   |
| D        | y = 8.49 + 0.984x  | y = 15.3 + 0.933x   |

 Table 27. Analysis of variance test for homogeneity of slopes.

| Source of<br>variation | <b>SS</b> | đ٢        | MS     | F     |
|------------------------|-----------|-----------|--------|-------|
|                        |           | · · · · · |        |       |
| DNT: Between slopes    | 321.5     | 3         | 107.17 | 1.74• |
| Error                  | 14,915.5  | 242       | 61.63  |       |
| TNT: Between slopes    | 15.3      | 3         | 5.1    | 0.041 |
| Error                  | 29,266.7  | 244       | 119.9  |       |
| RDX: Between slopes    | 471       | 3         | 157    | 0.37  |
| Error                  | 91,054    | 214       | 425.5  |       |
| HMX: Between slopes    | 311       | 3         | 103.7  | 0.51  |
| Error:                 | 37,773    | 184       | 205.3  |       |

•  $F_{0.95}(3,242) = 2.65.$ 

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† Any F value below 1 is not significant.

tributed to the collaborators. Since SARM assays are certified to be at least 98 mole %, this 2% uncertainty could account for the observed slope being slightly less than 1.00. The largest deviation expected from SARM assay inaccuracy is 2.8% as calculated by propagation of errors test (mean square of the 2% inaccuracy for each SARM batch).

For TNT, the slope of 0.944 cannot be attributed to SARM assay differences alone. This means that as a whole the collaborators recovered only 94.4% of the TNT. The reason for this low recovery is probably related to the fact that TNT is susceptible to decomposition by chemical, photochemical and microbial action. This happened despite steps taken during the preparation of matrices and spiking solutions and in the storage of these materials to try to minimize such losses.

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#### Table 28. Linear least squares regression equations for each analyte over all matrices.

|     | Model with intercept | Model through origin |
|-----|----------------------|----------------------|
| DNT | y = -2.15 + 1.00x    | y = -0.986x          |
| TNT | y = -0.798 + 0.950x  | y = 0.944x           |
| RDX | y = 5.82 + 0.996x    | y = 0.996x           |
| HMX | y = 8.36 + 0.955x    | y = 0.987x           |

\* These models are the accepted ones.

Table 29. Confidence intervals (95%) for intercepts of accepted models  $(\mu g/L)$ .

| DNT ±0.0088 | TNT ±0.0116  |
|-------------|--------------|
| RDX ±0.0186 | HMX ± 0.0183 |

In the case of RDX, the slope of 0.996 indicates nearly quantitative recovery, but a small positive intercept of 5.8  $\mu$ g/L is found. This intercept could arise either because negative curvature exists in the plot of "found" versus "true," which would tend to cause the fitted linear model to have a smaller slope and larger intercept, or because a small positive bias exists. An inspection of the residuals from the regression analysis showed no indication of curvature; therefore, the bias appears to be real.

Finally for HMX, both the intercept and slope depart from theory but not by a large amount. The small positive intercept represents a rea! bias since inspection of the regression residuals indicates no curvature in the relationship. The slope value indicates a small loss of HMX, more than can be accounted for by SARM assay errors.

Clearly, the results indicate very good accuracy considering that eight laboratories were represented and all concentrations were below 1 mg/L.

### CONCLUSIONS

Given the inevitable errors associated with the quantitative determination of trace level organic compounds in natural waters, the overall performance of the HPLC method for DNT, TNT, RDX and HMX is very good for the concentration ranges studied. The evidence supporting this evaluation is summarized below:

1. For DNT, RDX and HMX the median

"found" concentrations are within 3% of the "true" values. For TNT the difference is within 5%. Considering that the true values themselves are somewhat uncertain, the overall accuracy is very good.

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2. The repeatability, based on duplicate injections of each of two aliquots, is about  $\pm 7$ , 9, 15 and 10  $\mu$ g/L for DNT, TNT, RDX and HMX respectively. These values represent percent relative deviations on the order of 5 to 9%. If single injections were used, the repeatabilities would be inflated by a factor of 1.414 (square root of 2).

3. Reproducibilities for each analyte are about  $\pm 6$ , 21, 40 and 44% greater than repeatabilities for DNT, TNT, RDX and HMX respectively. This gives percent interlaboratory deviations, based on average concentration examined, of about 7% for DNT, RDX and HMX, and 10% for TNT. The most likely source of these differences between laboratories is the calibration of the instrumental response.

4. Recoveries of a given analyte were similar regardless of matrix. Overall, DNT and RDX were recovered quantitatively, and TNT and HMX showed small losses of about 5%.

We found that the standard deviation of replication was independent of concentration in the concentration ranges examined in this collaborative study. This observation confirms a similar finding from Part 1 of this report. Thus the relative standard deviations (RSD) for RDX and HMX are better than those of DNT and TNT when in fact RDX and HMX have poorer absolute precisions. This is clearly shown by the Youden plots, in which RDX and HMX have a much larger degree of scatter than DNT and TNT.

Valid statistical analysis required rejection of about 10% of the individual data values. This was not done blindly but with the aid of chemical intuition and with the view that the method, and not the individual laboratories, was being evaluated. Even where substantial number of outliers we e identified, the repeatabilities for those analytes most affected (RDX and HMX) grew from 5% relative to only 12% relative when no values were eliminated. This larger RSD is still quite acceptable for analysis at the microgram-per-litre level.

In order to put the performance of this method in perspective, it is instructive to compare the results of this collaborative study with others dealing with measurement of trace level constituents. Horwitz (1982) has discussed the interrelationship between interlaboratory reproducibility and concentration of analyte. Using data from over 150

independent collaborative studies, he found a clear logarithmic relationship between percent relative standard deviation of reproducibility and concentration of analyte. The reproducibility roughly doubles for each decrease of concentration of two orders of magnitude. Furthermore, this trend is independent of analyte or of analytical method. For the concentration levels measured by the HPLC method in this study, the expected reproducibility according to E prwitz is about 20%. Reproducibilities of 7 to 10% were actually found. The difference is most likely attributable to the fact that the samples distributed to the collaborating laboratories were homogeneous whereas many of the studies cited by Horwitz involved heterogeneous materials

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At this point we are confident in recommending that this HPLC method be implemented for monitoring munitions plant wastewaters and natural waters for DNT, TNT, RDX and HMX at the submilligram-per-litre levei. The accuracy and reproducibility in the analysis of real environmental samples have proven to be adequate for this task. The instrumental response was calibrated daily by using a single high standard in order to make as much time available for analysis of real samples as possible. This single-standard approach can be implemented efficiently by means of quality control charts.

#### LITERATURE CITED

Bratin, K., P.T. Kissinger, R.C. Briner and C.S. Bruntlett (1981) Determination of nitro aromatic, nitramine, and nitrate ester explosive compounds in explosive mixtures and gunshot residue by liquid chromatography and reductive electrochemical detection. Analytica Chimica Acta, 130: 295-311.

**Coates, A.D., A. Freedman and L.P. Kuhn (1970)** Characteristics of certain military explosives. Aberdeen Proving Ground, Maryland: Ballistic Research Laboratories Report No. 1507.

Conley, K.A. and W.J. Mikucki (1976) Migration of explosives and chlorinated pesticide in a simulated sanitary landfill. USA Construction Engineering Research Laboratory, Technical Report N-8.

Cragin, J.H., D.C. Leggett, B.T. Foley and P.W. Schumacher (In prep.) TNT, RDX and HMX in soils and sediments: Analytical techniques and drying losses. USA Cold Regions Research and Engineering Laboratory, CRREL Special Report.

the state of the second st

0-1-27-37-27-07-02-02-02-02-02-

Dean, J.A. (1979) Lange's Handbook of Chemistry. New York: McGraw-Hill.

**Doali, J.A. and A.A. Juhasz** (1974) Application of high speed liquid chromatography to the qualitative analysis of compounds of propellant and explosive interest. *Journal of Chromatographic Science*, 12: 15-56.

**Douse, J.M.F.** (1981) Trace analysis of explosives at the low picogram level by silica capillary column gas-liquid chromatography with electron capture detection. *Journal of Chromatography*, **208:** 8-88.

**Epstein, J., H.Z. Sommer and B.E. Hackley** (1977) Environmental quality standards research in wastewater of Army ammunition plants. Chemical Systems Laboratory Report ARCSL-TR-77025.

Federal Register (1979) Nitroaromatics and isophorone method 609. 44(233), Monday, December 3, pp. 69510-69513.

Gehring, D.G. and J.E. Shirk (1967) Separation and determination of trinitrotoluene isomers by gas chromatography. *Analytical Chemistry*, 39: 1315-1318.

Glover, D.J. and J.C. Hoffsommer (1973) Thin layer chromatographic analysis of HMX in water. Bulletin of Environmental Contamination and Toxicology, 10: 302-304.

Giover, D.J., J.C. Hoffsommer and D.A. Kubose (1977) Analysis of mixtures of 2-amino-4,6-dinitrotoluene, 4-amino-2,6-dinitrotoluene, 2,4-diamino-6-nitrotoluene, and 2,6-diamino-4-nitrotoluene. Analytical Chimica Acta, 88: 381-384.

Goerlitz, D.F. and L.M. Law (1975) Gas chromatographic method for the analysis of TNT and RDX explosives contaminating water and soilcore material. U.S. Geological Survey, Open File Report No. 75-182.

Hashimoto, A., H. Sakino, E. Yamagami and S. Tateishi (1980) Determination of diritrotoluene isomers in sea water and industrial effluent by high-resolution electron-capture gas chromatography with a glass capillary column. *Analyst*, 105: 787-793.

Heller, C.A., R.R. McBride and M.A. Ronning (1977) Detection of trinitrotoluene in water by fluorescent ion-exchange resins. *Analytical Chemistry*, 49: 2251-2253.

Heller, C.A., S.R. Grenyl and E.D. Erickson (1982) Field detection of 2,4,6-trinitrotoluene in water by ion-exchange resins. *Analytical Chemistry*, 54: 286-289.

Hoffsommer, J.C. and J.M. Rosen (1972) Analysis of explosives in sea water. Bulletin of Environ-

nin wider and the contract

mental Contamination and Toxicology, 7: 177-181.

Hoffsommer, J.C., D.J. Glover and J.M. Rosen (1972) Analysis of explosives in sea water and in ocean floor sediment and fauna. Naval Ordnance Laboratory Report 72-215.

Hoffsommer, J.C., D.A. Kubose and D.J. Glover (1981) Microanalysis of selected energetic nitro compounds by gas/liquid chromatography. Naval Surface Weapons Center TR 80-535.

Horwitz, W. (1982) Evaluation of analytical methods used for regulation of food and drugs. *Analytical Chemistry*, 54: 67A-76A.

Hubaux, A. and G. Vos (1970) Decision and detection limits for linear calibration curves. *Analytical Chemistry*, 42: 849-855.

Jenkins, T.F., R.P. Murrmann and D.C. Leggett (1973) Mass spectra of isomers of trinitrotoluene. Journal of Chemical and Engineering Data, 18: 438-439.

Jurinski, N.B., G.E. Podolak and H.L. Hess (1975) Comparison of analytical methods for trace quantities of 2,4,6-trinitrotoluene. American Industrial Hygiene Association Journal, pp. 497-502.

Kapian, D.L. and A.M. Kapian (1982) Thermophilic biotransformations of 2,4,6-trinitrotoluene under simulated composting conditions. *Applied* and Environmental Microbiology, 44: 757-760.

Karickhoff, S.W., D.S. Brown and T.A. Scott (1979) Sorption of hydrophobic pollutants on natural sediments. *Water Research*, 13: 241-248.

Krull, I.S., E.A. Davis, C. Santasania, S. Kraus, A. Basch and Y. Bamgerger (1981) Trace analysis of explosives by HPLC-electron capture detection (HPLC-ECD). Analytical Letters, 14: 1363-1376. Krull, I.S., M. Swartz, R. Hilliard, K.H. Xie and J.N. Driscoll (1983) Trace analysis for organic nitrocompounds by gas chromatography-electroncapture/photoionization detection methods. Journal of Chromatography, 260: 347-362.

Lakings, D.B., R.J. Baker and M.V. Crook (1981) Precision and accuracy assessment of the HPLC analytical technique for the determination of DNP, RDX, TNB, DNB, 2,4-DNT, TNT, Tetryl and DPA. Midwest Research Institute Technical Report No. 1. Aberdeen Proving Ground, Maryland: U.S. Army Toxic and Hazardous Materials Agency.

Leggett, D.C. (1977) Determination of 2,4,6-trinitrotoluene in water by conversion to nitrate. Analytical Chemistry, 49: 880.

Leggett, D.C. (In prep.) Filtration and analysis of water for TNT, RDX and HMX by HPLC. USA

Cold Regions Research and Engineering Laboratory, CRREL Special Report.

Leggett, D.C. and B.T. Foley (In prep.) Sorption of military explosives (TNT, DNT, TDX and HMX) on bentonite drilling muds: Effects on groundwater analysis. USA Cold Regions Research and Engineering Laboratory, CRREL Special Report.

Leggett, D.C., T.F. Jenkins and R.P. Murrmann (1977) Composition of vapors evolved from military TNT as influenced by temperature, solid composition, age and source. USA Cold Regions Research and Engineering Laboratory, CRREL Special Report 77-16.

McCormick, N.G., F.E. Fecherry and H.S. Levinson (1976) Microbial transformation of 2,4,6-trinitrotoluene and other nitro aromatics compounds. *Applied and Environmental Microbiol*ogy, 31: 949-958.

Mudri, S.S. (1968) A simple method for determination of TNT in TNT wastes. *Environmental Health*, 10: 35-39.

Murrmann, R.P., T.F. Jenkins and D.C. Leggett (1971) Composition and mass spectra of impurities in military grade TNT vapor. USA Cold Regions Research and Engineering Laboratory, CRREL Special Report 158.

**Parker, L.V., T.F. Jenkins and B.T. Foley** (In prep.) The suitability of polyvinyl chloride pipe for monitoring TNT, RDX, HMX and DNT in groundwater. USA Cold Regions Research and Engineering Laboratory, Special Report.

Pereira, W.E., D.C. Short, D.B. Manigold and P.K. Roscio (1979) Isolation and characterization of TNT and its metabolites in groundwater by gas chromatograph-mass spectrometer-computer techniques. Bulletin of Environmental Contamination and Toxicology, 21: 554-562.

Rowe, M.L. (1967) Determination of hexahydro-1,3,5-trinitro-S-triazine in octahydro-1,3,5,7,tetranitro-S-tetrazine by gas chromatography. Journal of Gas Chromatography, October, pp. 531-533. Spanggord, R.J., B.W. Gibson, R.G. Keck, D.W. Thomas and J.J. Barkley (1982) Effluent analyses of wastewater generated in the manufacture of 2, 4,6-trinitrotoluene. 1. Characterization study. Environmental Science and Technology, 16: 229-232.

Stanford, T.B. (1977) The determination of tetryl and 2,3-, 2,4-, 2,5-, 2,6-, 3,4- and 3,5-dinitrotoluene using high performance liquid chromatography. Contract Report DAMD-17-74-C-4123 to U.S. Army Medical Research and Development Command. Columbus: Battelle Laboratories.

Stidham, B.R. (1979) Analysis of wastewater for organic compounds unique to RDX/HMX manufacturing and processing. Final Engineering Report for Contract DAAA-09-78-C-3000 to U.S. Army Medical Research and Development Command. Kingsport, Tennessee: Holston Defense Corporation.

USATHAMA (1982) Sampling and chemical analysis quality assurance program for U.S. Army Toxic and Hazardous Materials Agency, Aberdeen Proving Ground, Maryland.

U.S. Department of Interior (1977) National handbook of recommended methods for water-data acquisition. Reston, Virginia.

Volk, W. (1958) Applied Statistics for Engineers. New York: McGraw-Hill.

Walsh, J.T., R.C. Chalk and C.M. Merritt (1973) Studies of munition wastes. *Analytical Chemistry*, 45: 1215-1220.

Weinberg, D.S. and J.P. Hsu (1983) Comparison of gas chromatographic and gas chromatographic/ mass spectrometric techniques for the analysis of TNT and related nitroaromatics. Journal of High Resolution Chromatography and Chromatography Communications, 6: 404-418.

Yinon, J. and S. Zitrin (1981) The Analysis of Explosives. Vol. 3. Pergamon Series in Analytical Chemistry. Oxford: Pergamon Press.

Youden, W.J. and E.H. Steiner (1975) Statistical Manual of the Association of Official Analytical Chemists. Statistical Techniques for Collaborative Tests. Arlington, Virginia: AOAC.

Youden, W.J. (1951) Statistical Methods for Chemists. New York: Wiley.

### APPENDIX A: DATA

# Method development

# Table A1. Analytical results of linearity tests.

|               | HOOL                     |  |               | -<br>FEDX                          |  |
|---------------|--------------------------|--|---------------|------------------------------------|--|
| Concentration | Paak Aree<br>(Integrator | Peak height<br>(absorbance                     | Concentration | Peat area<br>(Integrator           | Peak height<br>(absor bance                    |
| (ug/L)        | units)                   | units)   | (10/0         | units)                             | units)   |
| 22.3          | 9707                     | 1.46x10-4                                      | 24, e         | 17222                              | 2.17=10-4                                      |
|               | 12872                    | 1,50x10""                                      |               | 23376                              | 3,19x10**                                      |
|               | 9463                     | 1,48x10-4                                      |               | 146.58                             | 2.19m10-4                                      |
|               | 7=10681                  |  |               | T=18412                            |  |
|               | 0 <sup>2</sup> =3,6 2E6  |  |               | o <sup>2</sup> 2.02€7              |  |
| 55.8          | 21720                    | 3.05×10-4                                      | 62.0          | 30051                              | 4.06=10-4                                      |
|               | 28074                    | 5.01+10-4                                      |               | 31804                              | 4.13+10-4                                      |
|               | 2.370                    | 3,13=10-4                                      |               | 30837                              | 4,10x10**                                      |
|               | 7=23721                  |  |               | ¥-30897                            |  |
|               | σ <sup>2</sup> =1,4Ξ7    |  |               | 0~1.7 IES                          |  |
| 111,6         | 39035                    | 5.00x10-4                                      | 124.0         | 61334                              | 8.52+10  |
|               | 35474                    | 5 91=10-4                                      |               | 58965                              | 8,22×10*4                                      |
|               | 41373                    | 6,00x10-4                                      |               | 60696                              | 8.48x 10""                                     |
|               | Y=38627                  |  |               | Y=60352                            |  |
|               | 0 <sup>2</sup> -8.82E6   |  |               | o <sup>2</sup> -1.50E6             |  |
| 558           | 187470                   | 3.29x10-3                                      | 620           | 288580                             | 4.74x10-3                                      |
|               | 191470                   | 3.23x10-3                                      |               | 289080                             | 4,65=10-3                                      |
|               | 192390<br>Te190443       | 3,18x10-3                                      |               | 305970                             | 4.65x10*3                                      |
|               | σ <sup>2</sup> =6,84€6   |  |               | 7-294543<br>0 <sup>2</sup> -9.80E7 |  |
|               |                          |  |               | 0.44.8027                          |  |
| 1116          | 379810                   | 6.30x10-3                                      | 1240          | 591220                             | 9.29+10-3                                      |
|               | 378210<br>379800         | 6.46±10-3<br>6.46±10-3                         |               | 574470<br>584170                   | 9,22×10-3<br>9,34×10+3                         |
|               | T=379273                 | 0,00010  |               | T= 583287                          | *.J*X IV                                       |
|               | 02-8.48E5                |  |               | 0 <sup>2</sup> 7 07E7              |  |
| 2232          | 752980                   | 1,26x10+2                                      | 2480          | 1146000                            | 1.81×10-2                                      |
|               | 7 5 5 9 0 0              | 1,27×10+2                                      |               | 1144400                            | 1.01×10-2                                      |
|               | 756130                   | 1,28x10-2                                      |               | 1148700                            | 1.83×10+2                                      |
|               | ¥=755003                 |  |               | Y-1146367                          |  |
|               | σ <sup>2</sup> ≈3,0€6    |  |               | ~1,0 K1                            |  |
| 5580          | 1883800                  | 2.60x10-2                                      | 6200          | 2846200                            | 3, 95× 10-2                                    |
|               | 1869700                  | 2.86=10-2                                      |               | 2854600                            | 4.32=10-2                                      |
|               | 1890100                  | 2,86×10-2                                      |               | 2864500                            | 4.31x10-2                                      |
|               | T= 1886533               |  |               | Y-2855100                          |  |
|               | 02-1.04E7                |  |               | 0 <sup>2</sup> -8,39E7             |  |
| 17.2          | 22386                    | 2.00x10*4                                      | 12.8          | 18044                              | 1,80x10-4                                      |
|               | 18883                    | 1,79=10-4                                      |               | 16891                              | 1.75×10-4                                      |
|               | 20296                    | 1.97x10-4                                      |               | 25403                              | 2.17×10-4                                      |
|               | Y=20522                  |  |               | Y+20113                            |  |
|               | o <sup>2</sup> =3,11E6   |  |               | 0 <sup>2</sup> -2.13E7             |  |
| 43.0          | 384 34                   | 4.28x10-4                                      | 32.0          | 44425                              | 4,01x10 <sup>-4</sup>                          |
|               | 42977                    | 4.23=10-4                                      |               | 38845                              | 5,98x10 <sup>-4</sup><br>5,89x10 <sup>-4</sup> |
|               | 46234                    | 4.09x10-4                                      |               | 34601                              | 3,89x10-*                                      |
|               | T=4 2548                 |  |               | T-39290                            |  |
|               | <sup>2</sup> •1,5∑7      |  |               | o <sup>2</sup> •2.4 € 7            |  |
| 86,0          | 84853                    | 8.85.10  | 64.0          | 84288                              | 8.76×10-4                                      |
|               | 98201<br>86431           | 8_66x10 <sup>-4</sup><br>8_78x10 <sup>-4</sup> |               | 85186<br>92984                     | 8.07x10 <sup>-4</sup><br>8.23x10 <sup>-4</sup> |
|               | T-89828                  | 0. / 0X 1V                                     |               | 92984<br>Y+87486                   | 0.4 34 10                                      |
|               | 0 <sup>2</sup> -3,3267   |  |               | 0 <sup>2</sup> •2.29E7             |  |
|               | 0-93,34E/                |  |               | 0 -4.29E/                          |  |

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|               | TNT  |   |               | 2,4-0HT  | ~   |
|---------------|--|---|---------------|--|---|
| Concentration | Pask eres<br>(Integrator<br>Units)                                   | Peek height<br>(absorbance<br>un(15)                                    | Concentration | Peak erea<br>(Integrator<br>units)   | Peak haight<br>(absorbance<br><u>units)</u>                                 |
| 430           | 411360<br>413900<br>414770<br>T=d13343<br>σ <sup>2</sup> =3,1€6      | 4.93x10~3<br>4.94x10~3<br>4.67x10~3                                     | 320           | 403880<br>405520<br>405930<br>Y=403113<br>g <sup>2</sup> =1,1656             | 4,57x10*3<br>4,61x10 <sup>-3</sup><br>4,41x10 <sup>-3</sup>                 |
| 860           | 826690<br>825590<br>834460<br>7-828910<br>0 <sup>2</sup> =2,3467     | 9,60x10 <sup>-3</sup><br>9,68x10 <sup>-3</sup><br>9,62x10 <sup>-3</sup> | 6 40          | 815160<br>608080<br>815120<br>Tr-812787<br>0 <sup>2</sup> =1.6657            | 9,06x10 <sup>-3</sup><br>9,17x10 <sup>-3</sup><br>9,09x10 <sup>-3</sup>     |
| 1720          | 1650600<br>1659900<br>1655800<br>T=1655433<br>σ <sup>2</sup> =2,17Ε7 | 1.92x10 <sup>-2</sup><br>1.92x10 <sup>-2</sup><br>1.93x10 <sup>-2</sup> | 1280          | 1625300<br>1628200<br>1633200<br><u>Y=162896</u> 7<br>g <sup>2</sup> =1,5527 | 1.81x10 <sup>-2</sup><br>1.83x10 <sup>-2</sup><br>1.84x10 <sup>-2</sup>     |
| 4300          | 4119300<br>4134800<br>4135200<br>T+4129767<br>0 <sup>2</sup> -8,2287 | 4,30x10 <sup>-2</sup><br>4,67x10 <sup>-2</sup><br>4,67x10 <sup>-2</sup> | 3200          | 4041100<br>4055100<br>4055400<br>Te4054867<br>2-1.8668                       | 4, 10x 10 <sup>-2</sup><br>4,44x 10 <sup>-2</sup><br>4,45x 10 <sup>-2</sup> |

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|  | Pask ares  | Peek N   | elaht   |   |  |  | <u>4-ONT</u><br>Ik erea   | Peak haige  |
|--|--|--|---|---|--|--|---|---|
| Concentret II  |  | (epeor   | bence   |   | (ja/L)   | on (in   | regrator<br>(n)(ta)   | (absorbani<br>units)  |
| 430  | 411360<br>413900   | 4,93x<br>4,94x   | 10-3  |   | 320  |  | 03880<br>05520  | 4,57x10*<br>4,61x10*  |
|  | 414770   | 4.67×  | 10-3  |   |  | 4  | 05930   | 4,41±10-  |
|  | T=013343<br>0 <sup>2</sup> -3,1€6  |  |   |   |  |  | 403110  |   |
|  | -  |  |   |   |  | •  |   | 9,06×10-  |
| 860  | 826690<br>825590   | 9,60x<br>9,68x   | 10-3  |   | 640  | 6  | 15160   | 9.17.10-  |
|  | 834460<br>7-828910   | 9,62   | 10-3  |   |  |  | 15120<br>812787   | 9,09x10   |
|  | 7-828910<br>02-2,3467  |  |   |   |  |  | 812787<br>1.66E7  |   |
| 1720   | 1650600  | 1,921  | 10-2  |   | 1280   |  | 25500   | 1,81x10-  |
| 1729   | 1699900  | 1,92)<br>1,92)<br>1,93)  | 10-2  |   |  | 16   | 28200   | 1,83x10"<br>1,83x10"<br>1,84x10"  |
|  | 1655800<br>7+1655433   | 1.63   |   |   |  |  | 53200<br>1628967  | '.84x10"  |
|  | σ <sup>2</sup> =2.17E7   |  |   |   |  |  | 1.5%7   |   |
| 4 300  | 4119300  | 4,30   | 10-2  |   | 3200   |  | 41100   | 4,10x10"  |
| - 200  | 4134800  | 4,67,  | 10-2  |   |  | 40   | 55100<br>68400  | 4,44x10"<br>4,45x10"  |
|  | ¥155200<br>¥+4129767   | 4,0 A  |   |   |  | _  | 4034867   | 1.12410   |
|  | 2-8.22E7   |  |   |   |  |  | 1.8668  |   |
|  |  |  |   |   |  |  |   |   |
|  |  |  |   |   | icate  |  |   |   |
| Sæ   | pte  | <u>A</u>   | <u> </u>  |   | lcate<br>2B  |  | <u> </u>  | Maan  |
| <u>San</u>   | apte   | <u> </u>   | <u>1</u> 9  | A   | 2  |  | <u> </u>  | Maan.   |
| MI   | 11-0   | <u>A</u> 61, 7   | <u>9</u><br>65.3  | A   | 28   | <u>A</u><br>63, 3  | <u>8</u><br>63, 3   | 63, 2   |
| Mi<br>(ui<br>Mi  | -Q<br>    tored)<br>    -Q   | 61,7<br>61,1   | 65.3  | A<br>61.7<br>64.2   | 2B<br>B<br>63, 3<br>63, 9  | 65, 3<br>68, 1   | 63, 3<br>63, 9  | 63, 2<br>64, 1  |
| M)<br>(ur<br>Gre   | ill-Q<br>htlitered)  | 61,7<br>61,1<br>62,5<br>60,6   | 63.3<br>63.3<br>54.4<br>64,4  | A<br>61.7<br>64.2<br>62.5<br>61.1   | 2<br>  | 63, 3<br>68, 1<br>66, 9<br>58, 9   | 63, 3<br>63, 9<br>61, 1<br>63,6   | 63, 2<br>64, 1<br>63,6<br>61, 9   |
| Mi<br>(ur<br>Bi<br>Taj<br>Cou  | 111-Q<br>1111-Q<br>1111-Q<br>Sundwater<br>Seater   | 61,7<br>61,1<br>62,5   | 65, 3<br>63, 3<br>64,4  | A<br>61,7<br>64,2<br>62,5   | 2B<br>   | 63, 3<br>68, 1<br>68, 9  | 63, 3<br>63, 9<br>61, 1   | 63,2<br>64,1<br>63,6  |
| Mi<br>(ur<br>Bi<br>Taj<br>Cou  | ill-Q<br>htlitered)<br>lli-Q<br>sundwater<br>swater<br>nn, River   | 61,7<br>61,1<br>62,5<br>60,6<br>61,1   | 63.3<br>63.3<br>54.4<br>64,4<br>39,7  | A<br>61,7<br>64,2<br>52,5<br>61,1<br>61,7<br>57,8   | 2<br>  | 63, 3<br>68, 1<br>66, 9<br>58, 9<br>64,4   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9   | 63, 2<br>64, 1<br>63,6<br>61, 9<br>60,8   |
| Mi<br>(ur<br>Mi<br>Gre<br>Taj<br>Po<br>Mi  | ill-Q<br>htlitered)<br>lll-Q<br>sundester<br>noseter<br>no, River<br>nd water<br>lll-Q   | 61,7<br>61,1<br>62,5<br>60,6<br>61,1   | 63.3<br>63.3<br>54.4<br>64,4<br>39,7  | A<br>61,7<br>64,2<br>52,5<br>61,1<br>61,7<br>57,8   | 2<br>B<br>B<br>B<br>B<br>B<br>C<br>B<br>B<br>B<br>C<br>B<br>C<br>B<br>C<br>C<br>B<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C   | 63, 3<br>68, 1<br>66, 9<br>58, 9<br>64,4   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9   | 63, 2<br>64, 1<br>63,6<br>61, 9<br>60,8   |
| MI<br>(ur<br>Grc<br>Taj<br>Coc<br>Po<br>MI<br>(ur<br>MI<br>(ur<br>MI   | 111-Q<br>httl:tered)<br>li1-Q<br>how deater<br>how River<br>how ater<br>li1-Q<br>httl:tered)<br>li1-Q  | 61,7<br>61,1<br>62,9<br>60,6<br>61,1<br>58,1<br>47,3<br>49,2   | 65.3<br>63.3<br>64.4<br>64.4<br>39.7<br>35.6<br>49.3<br>49.3  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.5  | 2<br>8<br>63.3<br>63.9<br>64.4<br>62.5<br>61.1<br>60.6<br>0x<br>50.0<br>47.6   | 63, 3<br>68, 1<br>66, 9<br>58, 9<br>64, 4<br>36, 1<br>49, 5<br>52, 4   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>48, 8  | 63, 2<br>64, 1<br>63, 6<br>61, 9<br>60, 8<br>58, 4<br>48, 3<br>49, 1  |
| MI<br>(ur<br>Gri<br>Co<br>Po<br>MI<br>(ur<br>MI<br>Gri   | (11-Q)<br>httltered)<br>(11-Q)<br>sundester<br>sundester<br>nn, River<br>nd water<br>(11-Q)<br>httl:Q<br>httl:Q  | 61,7<br>61,1<br>62,3<br>60,6<br>61,1<br>58,1<br>47,3   | 63.3<br>63.3<br>64.4<br>64.4<br>39.7<br>35.6  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47_5  | 2<br>8<br>63.3<br>63.9<br>64.6<br>62.5<br>61.1<br>60.6<br>00x<br>50.0  | 61, 3<br>68, 1<br>66, 9<br>58, 9<br>64, 4<br>36, 1<br>49, 5  | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 7<br>45, 8   | 63, 2<br>64, 1<br>63, 6<br>51, 9<br>60, 8<br>38, 4<br>48, 3   |
| MI<br>(ur<br>Mi)<br>Cro<br>Taj<br>Cor<br>Po<br>Po<br>Mi<br>(ur<br>Ni<br>Ger<br>Taj<br>Cor  | (11-Q)<br>hilitered)<br>liliQ<br>sundwater<br>sundwater<br>nd water<br>liliQ<br>hilitered)<br>liliQ<br>sundwater<br>sundwater<br>sumstar<br>n, River   | 61,7<br>61,1<br>62,5<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,8<br>44,9<br>48,8   | 65.3<br>63.3<br>64.4<br>64.4<br>99.7<br>33.6<br>49.3<br>49.2<br>46.6<br>50.8<br>47.1  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.5<br>47.3<br>47.3<br>47.3<br>45.1<br>45.8  | 2<br>8<br>63.3<br>63.9<br>64.4<br>62.5<br>61.1<br>60.6<br>0x<br>50.0<br>47.6<br>49.2<br>49.3<br>47.8   | 63, 3<br>68, 1<br>66, 9<br>58, 9<br>64, 4<br>36, 1<br>49, 5<br>52, 4<br>45, 6<br>47, 3<br>49, 0  | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 8<br>46, 1<br>49, 0<br>43, 9  | 63, 2<br>64, 1<br>63, 6<br>51, 9<br>60, 8<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1   |
| MI<br>(ur<br>Mi)<br>Cro<br>Taj<br>Cor<br>Po<br>Po<br>Mi<br>(ur<br>Ni<br>Ger<br>Taj<br>Cor  | (11-Q)<br>httlseed)<br>Lit-Q<br>booster<br>booster<br>hd water<br>hd water<br>httlseed)<br>Lit-Q<br>httlseed)<br>Lit-Q<br>booter<br>booter<br>booter   | 61,7<br>61,1<br>62,5<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,5<br>49,2<br>47,8   | 63.3<br>63.3<br>64.4<br>64.4<br>59.7<br>35.6<br>49.3<br>49.3<br>49.2<br>46.6<br>50.8  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.3<br>47.5<br>47.3<br>47.8<br>46.1<br>45.8<br>46.3  | 2<br>80x<br>63.3<br>63.9<br>64.4<br>62.5<br>61.1<br>60.6<br>10x<br>50.0<br>47.6<br>49.2<br>49.5<br>47.8<br>47.1  | 63, 3<br>68, 1<br>66, 9<br>58, 9<br>64, 4<br>36, 1<br>49, 5<br>52, 4<br>45, 6<br>47, 3   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 1<br>49, 0  | 63, 2<br>64, 1<br>63, 6<br>61, 9<br>60, 6<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0  |
| MI<br>(ut<br>Mi<br>Gr<br>Taj<br>Cot<br>Po<br>Mi<br>(ut<br>Mi<br>Gr<br>Taj<br>Gr<br>Cot   | (11-Q)<br>httltpred)<br>111-Q<br>bundwater<br>buster<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://www.<br>http://wwww.<br>http://wwww.<br>http://wwww.<br>http://wwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwww   | 61,7<br>62,3<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9   | 63.3<br>64.4<br>64.4<br>59.7<br>55.6<br>49.3<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>47.5<br>47.5<br>47.5<br>47.3<br>47.8<br>46.1<br>45.8<br>48.3   | 2<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B  | 63.3<br>68.1<br>66.9<br>58.9<br>64.4<br>36.1<br>49.5<br>52.4<br>45.6<br>47.5<br>49.0<br>47.1   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 1<br>49, 0<br>45, 9<br>46, 1  | 63, 2<br>64, 1<br>63, 6<br>61, 9<br>60, 8<br>58, 4<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0   |
| MI<br>(ur<br>Mi<br>Cri<br>Taj<br>Coi<br>Poi<br>Mi<br>(ur<br>Mi<br>Gri<br>Taj<br>Coi<br>Poi<br>Al<br>(ur<br>(ur)  | 111-Q<br>hill-pred)<br>lill-Q<br>boster<br>boster<br>hd water<br>111-Q<br>hill-Q<br>boster<br>hn, River<br>hd water<br>boster<br>hd water<br>boster<br>hd water<br>hill-Q<br>hill-Q<br>hill-Q<br>hill-Q  | 61,7<br>61,1<br>62,3<br>60,6<br>61,1<br>38,1<br>47,3<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9<br>28,9   | 63, 3<br>63, 3<br>64, 4<br>59, 7<br>55, 6<br>49, 3<br>49, 2<br>46, 6<br>50, 8<br>47, 1<br>49, 2<br>30, 7  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.3<br>47.5<br>47.3<br>47.5<br>47.3<br>47.5<br>17.8<br>46.1<br>5.8<br>46.1<br>5.8<br>46.3<br>T<br>50.6   | 2<br>83.3<br>63.9<br>64.4<br>62.5<br>61.1<br>60.6<br>10x<br>50.0<br>47.6<br>49.2<br>49.3<br>47.8<br>47.1<br>NT<br>28.4   | 63.3<br>68.1<br>66.9<br>58.9<br>64.4<br>36.1<br>49.5<br>52.4<br>45.6<br>47.3<br>49.0<br>47.1<br>30,7   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>36, 9<br>61, 1<br>45, 8<br>45, 8<br>46, 8<br>46, 1<br>49, 0<br>43, 9<br>46, 1<br>28, 1  | 63, 2<br>64, 1<br>63, 6<br>51, 9<br>60, 6<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6   |
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| MI<br>(ur<br>Mi)<br>Cri<br>Taj<br>Co<br>Po<br>Mi<br>(ur<br>Mi)<br>Gri<br>Co<br>Po<br>Mi)<br>(ur<br>Taj<br>Co<br>Po<br>Mi)<br>(ur<br>Taj<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co  | (11-Q)<br>httltpred)<br>httltpred)<br>undester<br>paster<br>hn, River<br>nd water<br>httltp<br>httltpred)<br>httltpred)<br>httl<br>hd water<br>hd water<br>hd water<br>hd water<br>hd water<br>hd water  | 61,7<br>61,1<br>62,5<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9<br>28,9<br>28,9<br>28,9<br>28,9   | 63, 3<br>64, 4<br>64, 4<br>59, 7<br>55, 6<br>49, 3<br>49, 2<br>46, 6<br>50, 8<br>47, 1<br>49, 2<br>30, 7<br>29, 9<br>29, 7  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.3<br>47.3<br>47.3<br>47.8<br>46.1<br>45.8<br>48.3<br>7<br>30.6<br>29.9<br>29.0   | 2<br>80X<br>63.3<br>63.9<br>64.4<br>62.5<br>50.0<br>47.6<br>49.2<br>49.3<br>47.6<br>47.2<br>49.3<br>47.8<br>47.1<br>10X<br>20.4<br>27.4<br>29.5  | 63.3<br>68.1<br>66.9<br>58.9<br>64.4<br>36.1<br>49.5<br>52.4<br>45.6<br>47.5<br>49.0<br>47.1<br>30,7<br>29.9<br>32.1   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 1<br>49, 0<br>45, 9<br>46, 1<br>28, 1<br>27, 0<br>28, 0  | 63, 2<br>64, 1<br>63, 6<br>61, 9<br>60, 8<br>58, 4<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>28, 8<br>29, 8  |
| MI<br>(ur<br>Mi)<br>Cri<br>Taj<br>Co<br>Po<br>Mi<br>(ur<br>Mi)<br>Gri<br>Co<br>Po<br>Mi)<br>(ur<br>Taj<br>Co<br>Po<br>Mi)<br>(ur<br>Taj<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co<br>Co  | <pre>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-</pre>  | 61,7<br>61,1<br>62,5<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9   | 63, 3<br>63, 3<br>64, 4<br>64, 4<br>59, 7<br>35, 6<br>49, 3<br>49, 2<br>46, 6<br>50, 8<br>47, 1<br>49, 2<br>30, 7<br>29, 9<br>29, 7<br>28, 4<br>29, 0   | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5  | 2<br>8<br>63.3<br>63.9<br>64.4<br>62.5<br>61.1<br>60.6<br>10x<br>50.0<br>47.6<br>49.2<br>49.5<br>47.6<br>49.2<br>49.5<br>47.8<br>47.1<br>NT<br>28.4<br>27.4<br>29.5<br>28.5<br>30.7                              | 65.3<br>68.1<br>66.9<br>58.9<br>64.4<br>26.1<br>49.5<br>52.4<br>45.6<br>47.5<br>49.0<br>47.1<br>30,7<br>29.9<br>32.1<br>28.3<br>27.3   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 1<br>49, 0<br>43, 9<br>46, 1<br>28, 1<br>27, 0<br>28, 0<br>29, 0<br>27, 3   | 63, 2<br>64, 1<br>65, 6<br>61, 9<br>60, 6<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>26, 8<br>29, 8<br>28, 7<br>28, 1   |
| MI<br>(ur<br>Mi)<br>Gri<br>Coi<br>Poi<br>Mi<br>(ur<br>Mi)<br>Gri<br>Tai<br>Coi<br>Poi<br>Mi)<br>(ur<br>Mi)<br>Gri<br>Tai<br>Coi<br>Poi<br>Poi<br>Poi<br>Poi<br>Poi<br>Poi<br>Poi<br>Poi<br>Poi<br>P  | <pre>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-Q<br/>())-</pre>  | 61,7<br>61,1<br>62,5<br>60,6<br>61,1<br>58,1<br>47,5<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9   | 63, 3<br>63, 3<br>64, 4<br>64, 4<br>59, 7<br>35, 6<br>49, 3<br>49, 2<br>46, 6<br>50, 8<br>47, 1<br>49, 2<br>30, 7<br>29, 9<br>29, 7<br>28, 4<br>29, 0   | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5<br>47.5  | 2<br>80X<br>63.3<br>63.9<br>64.4<br>62.5<br>21.1<br>60.6<br>10X<br>50.0<br>47.6<br>49.2<br>49.5<br>47.8<br>47.1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1        | 65.3<br>68.1<br>66.9<br>58.9<br>64.4<br>26.1<br>49.5<br>52.4<br>45.6<br>47.5<br>49.0<br>47.1<br>30,7<br>29.9<br>32.1<br>28.3<br>27.3   | 63, 3<br>63, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 1<br>49, 0<br>43, 9<br>46, 1<br>28, 1<br>27, 0<br>28, 0<br>29, 0<br>27, 3   | 63, 2<br>64, 1<br>65, 6<br>61, 9<br>60, 6<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>26, 8<br>29, 8<br>28, 7<br>28, 1   |
| MI<br>(ur<br>MI)<br>Crc<br>Taj<br>Coc<br>Po<br>MI<br>(ur<br>MI)<br>Grc<br>Taj<br>Co<br>Po<br>MI<br>(ur<br>MI)<br>Grc<br>Taj<br>Co<br>Po<br>MI<br>(ur<br>MI)<br>Grc<br>Taj<br>Co<br>Po<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>Po<br>(ur<br>MI)<br>(ur<br>MI)<br>Coc<br>Po<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur<br>MI)<br>(ur)<br>(ur)<br>(ur)<br>(ur)<br>(ur)<br>(ur)<br>(ur)<br>(ur 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1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>28, 8<br>29, 8<br>29, 8<br>29, 1<br>28, 7<br>28, 7<br>28, 7  |
| MI<br>(ur<br>Mi)<br>Gra<br>Taj<br>Cor<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gra<br>Taj<br>Cor<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gra<br>Cor<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gra<br>Taj<br>Gra<br>Taj<br>Gra<br>Cor<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gra<br>Cor<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Scra<br>Po<br>Mi)<br>(ur<br>Scra<br>Scra<br>Scra<br>Scra<br>Po<br>(ur<br>Scra<br>Scra<br>Scra<br>Scra<br>Scra<br>Scra<br>Scra<br>Scr   | <pre>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(11-Q)<br/>(</pre>  | 61, 7<br>61, 1<br>62, 5<br>60, 6<br>61, 1<br>58, 1<br>47, 5<br>49, 2<br>47, 8<br>44, 9<br>48, 8<br>43, 9<br>28, 9<br>28, 9<br>28, 9<br>28, 6<br>30, 7<br>27, 5<br>28, 4<br>36, 7<br>37, 7<br>36, 6<br>37, 2<br>35, 0<br>37, 2  | 63.3<br>63.3<br>64.4<br>59.7<br>33.6<br>49.3<br>49.2<br>46.6<br>30.8<br>47.1<br>49.2<br>49.2<br>49.2<br>49.2<br>49.2<br>49.2<br>49.2<br>49.2  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.5<br>47.5<br>47.5<br>47.3<br>47.8<br>46.1<br>45.8<br>46.3<br>7.3<br>30.6<br>29.9<br>29.0<br>29.6<br>27.2<br>26.1<br>57.3<br>37.3<br>37.3<br>37.3                           | 2<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B<br>- B  | 65.3<br>68.1<br>66.9<br>58.9<br>64.4<br>36.1<br>49.5<br>52.4<br>45.6<br>47.5<br>49.0<br>47.1<br>30,7<br>29.9<br>32.1<br>28.3<br>27.3<br>30,7<br>38.2<br>36.5<br>36.2                 | 63, 3<br>65, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 8<br>46, 1<br>49, 0<br>45, 9<br>46, 1<br>28, 1<br>27, 0<br>28, 0<br>29, 0<br>27, 3<br>27, 0<br>35, 3<br>35, 7<br>36, 0                                     | 63, 2<br>64, 1<br>65, 6<br>61, 9<br>60, 8<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>28, 8<br>29, 8<br>29, 7<br>28, 1<br>28, 7<br>28, 7<br>28, 1<br>28, 7<br>36, 9<br>36, 1<br>37, 0          |
| MI<br>(ur<br>Mi)<br>Cri<br>Taj<br>Coi<br>Po<br>Mi<br>(ur<br>Mi)<br>(ur<br>Mi)<br>Gri<br>Taj<br>Coi<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gri<br>Taj<br>Coi<br>Po<br>Mi)<br>(ur<br>Mi)<br>Gri<br>Taj<br>Coi<br>Po<br>Mi)<br>(ur<br>Mi)<br>Coi<br>Po<br>Po<br>Mi)<br>Coi<br>Po<br>Po<br>Mi)<br>Coi<br>Po<br>Po<br>Mi)<br>Coi<br>Po<br>Po<br>Mi)<br>Coi<br>Po<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Coi<br>Po<br>Mi)<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Coi<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Coi<br>Coi<br>Po<br>Coi<br>Po<br>Coi<br>Coi<br>Coi<br>Coi<br>Coi<br>Coi<br>Coi<br>Coi<br>Coi<br>Co | <pre>iii-Q iiii-Q iii-Q i</pre>   | 61,7<br>61,1<br>62,3<br>60,6<br>61,1<br>38,1<br>47,3<br>49,2<br>47,8<br>44,9<br>48,8<br>43,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28,9<br>28   | 63.3<br>63.3<br>64.4<br>59.7<br>53.6<br>49.3<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2<br>46.6<br>50.8<br>47.1<br>49.2<br>46.4<br>45.3<br>30.7<br>29.9<br>29.7<br>28.4<br>29.0<br>28.1<br>36.4<br>35.4<br>37.9<br>36.4  | A<br>61.7<br>64.2<br>52.5<br>61.1<br>61.7<br>57.8<br>R<br>47.3<br>47.3<br>47.3<br>47.3<br>47.3<br>47.3<br>47.3<br>47.3  | 2<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8   | 63.3<br>66.1<br>66.9<br>58.9<br>64.4<br>26.1<br>49.5<br>52.4<br>43.6<br>47.3<br>49.0<br>47.1<br>30,7<br>29.9<br>32.1<br>28.5<br>27.3<br>30,7<br>38.2<br>36.5<br>36.2<br>37.3<br>36.6 | 63, 3<br>65, 9<br>61, 1<br>63, 6<br>56, 9<br>61, 1<br>45, 8<br>46, 1<br>49, 0<br>43, 9<br>46, 1<br>28, 1<br>28, 1<br>27, 0<br>28, 0<br>27, 3<br>27, 0<br>28, 0<br>29, 0<br>27, 3<br>35, 3<br>35, 7<br>36, 0<br>38, 1<br>35, 6 | 63, 2<br>64, 1<br>65, 6<br>61, 9<br>60, 6<br>58, 4<br>48, 3<br>49, 1<br>47, 2<br>48, 0<br>47, 1<br>47, 0<br>29, 6<br>26, 8<br>29, 6<br>26, 8<br>29, 8<br>28, 7<br>28, 1<br>28, 7<br>36, 9<br>36, 1<br>37, 0<br>36, 8<br>33, 8 |
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| Table A | <b>A</b> 3. | Detection | limit | test. |
|---------|-------------|-----------|-------|-------|
|---------|-------------|-----------|-------|-------|

|               |               |                    |                  | Ta               | ble A3.          | Detection limi | t test.       |                         |                  |                               |                  |
|---------------|---------------|--------------------|------------------|------------------|------------------|----------------|---------------|-------------------------|------------------|-------------------------------|------------------|
|               | Concentration | <u> </u>           |                  | ror Units        |                  |                | Concentration |                         |                  | or Units                      |                  |
| <u>Sample</u> | (µg/L)        | Day 1              | Dey 2            | Cay 3            | Day 4            | Sample         | (10/1)        | Dey 1                   | Day 2            | Day 3                         | Day 4            |
|               |               |                    | H                | 1X               |                  |                |               |                         | TN               | it.                           |                  |
| 0.5 X         | 12,55         | 5470<br>516 i      | 8226<br>5058     | 4944<br>1813     | 4122             | 0.5 ×          | 7,72          | 8886<br>5427            | 12670            | 13149<br>9332                 | 5511<br>6706     |
|               |               | 6189               | 7961             | 4050             | 4808             |                |               | 4447                    | 4587             | 3968                          | 2969             |
| ١x            | 24.51         | 10021<br>9799      | 4073<br>12199    | 3557<br>9832     | 2583             | 1 x            | 15.44         | 6869<br>8884            | 3116<br>13679    | 4217                          | 4 1 57<br>1604 6 |
| • •           | 14.51         | 14258              | 8571             | 10183            | 9320             | • •            |               | 13899                   | 15892            | 10961                         | 16144            |
|               |               | 13953              | 13774<br>10334   | 13393<br>10390   | 6363<br>3518     |                |               | 14 <b>58</b> 4<br>17651 | 20064<br>20083   | 14178<br>13784                | 20390            |
| 1.5 X         | 36,76         | 15296              | 12994            | 15573            | 238              | 1,5 K          | 23,16         | 29895                   | 25004            | 10295                         | 2035             |
|               |               | 17054              | 14227            | 10658            | 4442             |                |               | 26544                   | 19894            | 31070                         | 2445             |
|               |               | 16339<br>9807      | 12928<br>13714   | 14201<br>15450   | 15416<br>11574   |                |               | 21521<br>33471          | 23618<br>12961   | 2632 <sup>-</sup><br>24289    | 3130<br>1739     |
| 2 X           | 49.02         | :9857              | 17974            | 15054            | 7 Z^             | 2 x            | 30,88         | 29535                   | 28555            | 26822                         | 3206             |
|               |               | 22153              | 17988            | 15671            | ۰۰۰<br>۵۰        |                |               | 29180<br>30844          | 35802<br>30918   | 25531<br>26888                | 3126             |
|               |               | 19578              | 22953            | 24956            | 23106            |                |               | 30389                   | 37674            | 35908                         | 3539             |
| 5 X           | 122.55        | 39900<br>40092     | 46717<br>44212   | 46132<br>48049   | 44799<br>40623   | 5 x            | 17.2          | 50861<br>77016          | 72409<br>75697   | 84584<br>77560                | 71905            |
|               |               | 39996              | 44835            | 52438            | 43555            |                |               | 82260                   | 73255            | 60177                         | 7379             |
| 10 ж          | 243.1         | 4 3064<br>8 58 1 7 | 44413<br>86432   | 42379<br>92414   | 45404<br>85057   | 10 X           | 154_4         | 74898<br>169020         | 84961<br>154840  | 75760<br>144850               | 7237             |
|               | 2-3.1         | 89839              | 88957            | 91065            | 91337            |                |               | 172710                  | 156130           | 151150                        | 14746            |
|               |               | 86705<br>78953     | 88328<br>89659   | 87972<br>89836   | 86766<br>90021   |                |               | 155010                  | 153930<br>155490 | 154660                        | 15710            |
| 20 x          | 490.2         | 191920             | 174210           | 174200           | 180610           | 20 ×           | 308.3         | 301420                  | 304960           | 309680                        | 30645            |
|               |               | 178900             | 178450           | 176330<br>176480 | 171750<br>177980 |                |               | 352540<br>304590        | 313790<br>311760 | 307150<br>304600              | 29604            |
|               |               | 179720             | 172130           | 175120           | 176620           |                |               | 305020                  | 298090           | 306560                        | 31590            |
|               |               |                    | R                | OX               |                  |                |               |                         | 04               | vt                            |                  |
| ū, 5 x        | 13.63         | 10827              | 9102             | 4283             | 9332             | 0.5 X          |               | 2356                    | 4361             | 3544                          | 181              |
| 0.7 -         | 17.07         | 7998               | 4725             | 6632             | 5926             | 0.7 *          | 6.4           | 2072                    | 2098             | 8431                          | 432              |
|               |               | 8052               | 8229             | 6022             | 6513             |                |               | 1 3 5 0 2               | 5590             | 6398                          | 453<br>1277      |
| 1 X           | 27.26         | 10021<br>13539     | 4005             | 7169<br>11374    | 5609<br>12974    | l x            | 12,8          | 15304                   | 2081<br>11652    | 7941<br>17582                 | 7 39             |
|               |               | 13811              | 16999            | 16627            | 14896            |                |               | 19140                   | 9834             | 18771                         | 1507             |
|               |               | 16864              | 21338<br>19639   | 15723<br>16487   | 11115            |                |               | 18950<br>20966          | 10123<br>16286   | 16074<br>15826                | 1842<br>2309     |
| 1,5 X         | 40.89         | 23896              | 18606            | 20011            | 18122            | 1.5 X          | 19.2          | 29875                   | 26739            | 24828                         | 2963             |
|               |               | 27645<br>22253     | 20954<br>23802   | 20042<br>20306   | 21994            |                |               | 24341<br>27416          | 2686 2<br>29507  | 26147<br>27307                | 2647             |
|               |               | 22042              | 19091            | 20540            | 19704            |                |               | 106 36                  | 13846            | 29633                         | 2425             |
| 2 ×           | 54.92         | 23414<br>24933     | 25853<br>27443   | 22073<br>22480   | 28472<br>39795   | 2 X            | 25,6          | 29654<br>30818          | 39336<br>34449   | 327 <b>35</b><br>27855        | 3128             |
|               |               | 31127              | 27310            | 35456            | 27864            |                |               | 38308                   | 39463            | 2 50 39                       | 3313             |
| 5 x           | 136.3         | 29914<br>65160     | 27636<br>64177   | 27861<br>66898   | 26234<br>63175   | 5 x            | 64.0          | 35157<br>87897          | 38000            | 43303<br>85665                | 54 50<br>88 94   |
|               |               | 65584              | 70117            | 61318            | 69453            | <i>·</i> ·     | <b>.</b> •    | 03164                   | 82577            | 85145                         | 8441             |
|               |               | 62131<br>64665     | 70842<br>68595   | 63691<br>62503   | 62227<br>68770   |                |               | 91657<br>85272          | 83519<br>87709   | 87978<br>85275                | 8919<br>7288     |
| 10 x          | 2 72.6        | 130950             | 132570           | 130050           | 130990           | 10 X           | 128.0         | 167080                  | 169940           | 171370                        | 16441            |
|               |               | 131900<br>129140   | 132880<br>130580 | 139980<br>133520 | 129980<br>127210 |                |               | 196730<br>169810        | 173250<br>172310 | 1693 <del>5</del> 0<br>167050 | 16796<br>1801    |
|               |               | 116250             | 130380           | 133520           | 132070           |                |               | 149740                  | 172680           | 176820                        | 17114            |
| 20 x          | 545.2         | 283470<br>268770   | 257350<br>260470 | 260890           | 268830<br>254050 | 20 ×           | 256,0         | 340380                  | 329940           | 334030                        | 33332            |
|               |               |                    | 200-10           | 264420           | 624070           |                |               | 352540                  | 333430           | 342800                        | 32588            |
|               |               | 260400             | 263800           | 266370           | 267990           |                |               | 3 366 20                | 337820           | 337970                        | 33471            |

Table A4. Factors employed in  $2^4$  factorial experiment to test the ruggedness of HPLC determination of HMX, RDX, TNT and 2, 4-DNT in aqueous samples.

|  | <u>Co</u>   | dad levels         |
|--|-------------|--------------------|
| Factors  | (+)         | (-)                |
| x1 • Sample storage (2 days)                               | Glass vials | Polvethylana vials |
| X2 = Portion of filtrate from<br>0.4 um nuclepore filter   | First 10 aL | Second 10 mL       |
| X3 + Equilibration time with<br>methance before filtration | 15 ninutes  | 4 hours            |
| X <sub>10</sub> = Yolume catlo of sample-to-methanol       | 8/10        | 10/8               |

# Table A5. Design and interaction matrices in coded units.

| Tr la: | <u>x, x, x, x,</u> | ×1 ×1 ×1 ×2 ×2 ×3<br>×2 ×3 ×4 ×3 ×4 ×4 | x <sub>1</sub> x <sub>1</sub> x <sub>1</sub> x <sub>2</sub> x <sub>1</sub><br>x <sub>2</sub> x <sub>2</sub> x <sub>3</sub> x <sub>3</sub> x <sub>2</sub><br>x <sub>3</sub> x <sub>6</sub> x <sub>6</sub> x <sub>6</sub> x <sub>6</sub> x <sub>3</sub><br> |
|--------|--------------------|--|---|
| 1      | +1 +1 +1 +1        | +  +  +  +  +  +                       | *1 *1 *1 *1 *1  |
| 2      | +1 +1 +1 -1        | *  *  =  *  *  *  *                    | *1 -1 -1 -1 -1  |
| 3      | 1 -1 +1 -1         | -  +1 -1 -1 +1 -1                      | -1 +1 -1 +1 +1  |
| 4      | +1 +1 +1 +1        | -1 +1 +1 -1 -1 +1                      | -1 -1 +1 -1 -1  |
| 5      | +1 +1 =1 =1        | +1 +1 +1 +1 +1 +1                      | -1 -1 +1 +1 +1  |
| 6      | +1 +1 -1 +1        | +1 +1 +1 +1 +1 +1                      | -1 +1 +1 +1 +1  |
| 7      | +1 -1 -1 +1        | -1 -1 +1 +1 -1 -1                      | +1 +1 +1 +1 +1  |
| 8      | +1 -1 -1 -1        | -1 -1 -1 +1 +1 +1                      | +1 +1 +1 +1 -1  |
| 9      | -1 +1 +1 -1        | -1 -1 +1 +1 +1 +1 -1                   | -1 +1 +1 -1 +1  |
| 10     | -1 +1 +1 +1        | -1 -1 -1 +1 +1 +1                      | +1 +1 +1 +1 +1  |
| 4.1    | -1 +1 +1 +1        | +1 -1 -1 -1 +1 +1                      | +1 +1 +1 +1 +1  |
| 12     | -1 -1 +1 -1        | +1 -1 +1 -1 +1 -1                      | +1 +1 +1 +1 -1  |
| 13     | -1 +1 -1 +1        | -1 +1 -1 -1 +1 -1                      | +1 -1 +1 -1 +1  |
| 14     | -1 +1 -1 -1        | -1 +1 +1 -1 -1 +1                      | +1 +1 -1 +1 -1  |
| 15     | •1 •1 •1 •1        | +  +1 +1 +1 +1 +1                      | -1 -1 -1 -1 +1  |
| 16     | -1 -1 -1 +1        | + + + - + + - 1 - 1 - 1                | -1+1+1+1-1  |

|--|

Table A6. Analysis of variance for ruggedness test. The complete experimental design appears in Tables A4 and A5 and the results are in Table 9.

| Verlebie                      | Et (ect<br>(us/L) | Sun of      | Degrees<br>of freedow | Noan<br>squares | <u></u> |
|-------------------------------|-------------------|-------------|-----------------------|-----------------|---------|
|                               |                   | 2           | .,4-DNT               |                 |         |
| Total                         |                   | 1385447.000 | 32                    |                 |         |
| C.F.**                        | 202,413           | 1311072,000 | 1                     |                 |         |
| x <sub>1</sub>                | +3,953            | 124,994     | t                     | Same as 5,5,    | 0.27    |
| x2                            | -9.396            | 706,222     | 1                     | •               | 1.92    |
| x <sub>3</sub>                | -6,451            | \$32,949    | 1                     |                 | 0,72    |
| x                             | -75.04            | 45052, 515  | 1                     |                 | 97.0*   |
| x1x2                          | -16,256           | 2114,125    | 1                     |                 | 4,550   |
| x <sub>1</sub> x <sub>3</sub> | +13,114           | 1375,764    | 1                     | •               | 2.96    |
| x <sub>1</sub> x              | -22,143           | 3922,544    | 1                     |                 | 8.44    |
| x2x3                          | -13,314           | 1418,048    | 1                     | •               | 3.05    |
| x <sub>2</sub> x              | +7,713            | 475,938     | 1                     | •               | 1.02    |
| x <sub>2</sub> x              | -16,713           | 2510.038    | 1                     |                 | 5,40*   |
| x1x2x3                        | -8,428            | 568,266     | 1                     |                 | 1,22    |
| x1x2x                         | +14,333           | 1643, 364   | 1                     | -               | 3, 54   |
| x1x3x                         | -14,489           | 1679.391    | 1                     | •               | 3,61    |
| X2X3X                         | +14,428           | 1665, 222   | 1                     |                 | 3, 58   |
| ×1×2×3×4                      | +20,473           | 3353,191    | 1                     | -               | 7,220   |
| Error                         |                   | 7434,02     | 16                    | 464,676         | •       |

Standard Deviation (5,) based on duplicates is equal to Verror HS = 21,55

for the entire experiment, the percent relative standard deviation (\$ ASD) is given by

 $\$ RSD = \frac{\$_V (100)}{grand mean} = \frac{(21, 99)(100)}{202,413} = 10,75$ 

ROX

| Totel   |         | 558395,000 | 32  |              |        |
|---|---------|------------|-----|--------------|--------|
| c./.**  | 131,397 | 552150.000 | 1   |              |        |
| ×1  | -2,982  | 71,156     | 1   | Same as 5,5, | 0.99   |
| ×2  | -1,875  | 20,136     | 1   | -            | 0,39   |
| ×3  | -4,521  | 163,479    | 1   | -            | 2_26   |
| x   | -21,429 | 3673, 531  | 1   | •            | 50, 9° |
| ×1×2  | +0,693  | 3,830      | 1   | •            | 0.05   |
| xix3  | +1,733  | 24,016     | 1   | •            | 0,33   |
| ×1×4  | +2,585  | 53,447     | 1   | -            | 0,75   |
| x2×3  | +3,559  | 101,350    | 1   | -            | 1,40   |
| x 2 x 4   | -4,517  | 149,062    | 1   |              | 2.06   |
| x jx  | -2,047  | 33, 524    | 1   | -            | 0,48   |
| ×1×2×3  | +4,500  | 161,976    | 1   | •            | 2,24   |
| x1x2x   | -4,323  | 149,619    | 1   | •            | 2.07   |
| x1x3x4  | -4,383  | 153.672    | 1   | •            | 2,13   |
| ×2×3×4  | -5,795  | 268,448    | - I | •            | 3,71   |
| X <sub>1</sub> X <sub>2</sub> X <sub>3</sub> X <sub>4</sub> | -2,520  | 54,905     | 1   | •            | 0,76   |
| trear   |         | 1155.02    | 16  | 72,189       |        |

Standard Deviation (S.) bases on duplicates is equal to derror #5 = 0.50

For the entire experiment, the S relative standard deviation (S RSD) is given by

| \$ R\$D + | grand reen | • <u>(0,50)(100)</u><br>151,357 | • | 6,475 |
|-----------|------------|---------------------------------|---|-------|
|           |            |                                 |   |       |

(1,16) = 4,49; an P value in the table above which exceeds 4,49 is significant at the 95 probability invel,

\*\*C.5. \* Correction factor  $(\frac{(IV)^2}{n})$ . The difference between the total and C.f. is the total corrected sum of squares.

| All of the set of th   | $t_{1}$ $t_{1}$ $t_{2}$ $t_{2}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{2}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{2}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{2}$ $t_{2}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{1}$ $t_{2}$ $t_{1}$ $t_{2}$ $t_{1}$ $t$  | Table A                         | 6 (cont'a                  | 1). Analysis  | of varian                     | ice for rugged                           | ness test.      |  |
|--|--|---------------------------------|----------------------------|---|-------------------------------|--|-----------------|--|
| $\frac{1}{12} \frac{1}{12} \frac$   | $\frac{1}{2} \frac{1}{2} \frac{1}$   |                                 |                            |   |                               |  |                 |  |
| $\begin{aligned} \frac{1023703,000}{54} & \frac{32}{54} & \frac{1}{520} & \frac{1023703,000}{14,000} & \frac{1}{54} & \frac{1}{520} & \frac{1}{54} & \frac{1}{520} & \frac{1}{540} & \frac{1}{5200,249} & \frac{1}{160} & \frac{1}{5200,249} & \frac{1}{1600,21} & \frac{1}{1600,2$   | $\begin{aligned} \frac{1023703,000}{54} & \frac{32}{1} & \frac{1}{1},00534,000} & \frac{1}{1} & \frac{1}{1},00534,000} & \frac{1}{1},00534,$   | Varlebie                        | ( <u>16</u> /L)            | Equeros   | of freedom                    | squeres                                  | <i></i>         |  |
| $C_{1,2}^{(2)} = (17,252) (100314,000) 1 \\ S_{2}^{(2)} = (1,250) (1,250) 1 \\ S_{3}^{(2)} = (1,250) (1,250) 1 \\ S_{4}^{(2)} = (1,250) (1,250) (1,250) 1 \\ S_{4}^{(2)} = (1,250) (1,250$   | $C_{1,4}^{-1} = (17,3)^{-1} (1003)^{-1} ($   |                                 |                            |   | TNT                           |  |                 |  |
| $ \begin{aligned} x_{3} &= -1,300 & 14,300 & 1 & Same at 5,5. & 0,12 \\ x_{3} &= -3,540 & 100,407 & 1 & - 5,52 \\ x_{4} &= -3,540 & 130,0140 & 1 & - 125,1 \\ x_{4} &= -3,540 & 130,0140 & 1 & - 11,10 \\ x_{4} &= -1,300 & 16,002 & 1 & - 0,15 \\ x_{4} &= -1,300 & 16,002 & 1 & - 0,15 \\ x_{4} &= -1,300 & 16,002 & 1 & - 0,15 \\ x_{4} &= -1,300 & 16,002 & 1 & - 0,15 \\ x_{4} &= -1,300 & 16,002 & 1 & - 0,15 \\ x_{4} &= -1,221 & 15,22 & 1 & - 0,11 \\ x_{4} &= -1,221 & 15,22 & 1 & - 0,11 \\ x_{4} &= -1,221 & 15,22 & 1 & - 0,13 \\ x_{4} &= -1,222 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 15,224 & 1 & - 0,12 \\ x_{4} &= -1,221 & 1,227,11 & 1 & - 1,43 \\ x_{4} &= -1,481 & 127,11 & 1 & - 1,43 \\ x_{4} &= -1,481 & 127,11 & 1 & 120,400 \\ x_{4} &= -1,2481 & 227,420 & 1 & - 1,28 \\ x_{4} &= -1,2481 & 227,420 & 1 & - 0,20 \\ x_{4} &= -1,2481 & 227,420 & 1 & - 0,20 \\ x_{4} &= -1,2481 & 227,420 & 1 & - 0,20 \\ x_{4} &= -1,2481 & - 1,22 \\ x_{4} &= -1,2481 & - 1,22 \\ x_{4} &= -1,248 & 1 & - 0,20 \\ x_{4} &= -2,248 & 23,244 & 1 & - 0,23 \\ x_{4} &= -2,248 & 23,275 & 1 & - 0,40 \\ x_{4} &= -2,248 & 1 & - 3,322 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 1,22 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &= -2,248 & 1 & - 0,23 \\ x_{4} &=$  | $ \begin{aligned} x_{3} &= -1,350 & 14,353 & 1 & Some at 5,5. & 0,12 \\ x_{3} &= -3,340 & 100,467 & 1 & - 5,52 \\ x_{4} &= -5,340 & 1320,240 & 1 & - 125,1 \\ x_{4}^{2} &= -4,232 & 143,279 & 1 & - 1,19 \\ x_{4}^{2} &= -4,232 & 143,279 & 1 & - 0,13 \\ x_{4}^{2} &= -4,232 & 143,279 & 1 & - 0,13 \\ x_{4}^{2} &= -4,030 & 1,002 & 1 & - 0,13 \\ x_{4}^{2} &= -4,030 & 1,022 & 1 & - 0,13 \\ x_{4}^{2} &= -4,040 & 1,022 & 1 & - 0,13 \\ x_{4}^{2} &= -4,040 & 1,022 & 1 & - 0,13 \\ x_{4}^{2} &= -4,040 & 1,022 & 1 & - 0,13 \\ x_{4}^{2} &= -4,040 & 1,022 & 1 & - 0,13 \\ x_{4}^{2} &= -4,040 & 1,022 & 1 & - 0,12 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & - 1,03 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & - 1,03 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & - 1,03 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & - 1,03 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & - 1,03 \\ x_{4}^{2} &= -4,040 & 12,711 & 1 & 100 \\ x_{4}^{2} &= -7,240 & 0,032 & 1 & - 3,177 \\ x_{4}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{4}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,240 & 0,030 & 1 & - 3,177 \\ x_{5}^{2} &= -7,244 & 0,171 & 1 & 0,23 \\ x_{5}^{2} &= -7,244 & 0,170 & 1 & - 0,23 \\ x_{5}^{2} &= -7,244 & 0,160 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,160 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,160 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,160 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 1,10 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 0,27 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 0,27 \\ x_{5}^{2} &= -7,244 & 0,100 & 1 & - 0,27 \\ x_{5}^{2} &= -1,237 & 12,052 & 1 & - 0,15 \\ x_{5}^{2} &= -1,242 & 100 & 13,474 & 1 & - 1,10 \\ x_{5}^{2} &= -1,242 & 100 & 13,474 & 1 & - 1,10 \\ x_{5}^{2} &= -1,242 & 100 & 13,474 & 1 & - 1,10 \\ x_{5}^{2} &= -1,242 & 100 & 13,474 & 1 & - 0,20 \\ x_{5}^{2}$   |                                 |                            |   |                               |  |                 |  |
| $ \frac{1}{3} - \frac{1}{7}, \frac{1}{7},$   | $\frac{1}{3} - \frac{1}{7}, $   |                                 |                            |   |                               | Same as 5.5.                             | 0.12            |  |
| $\begin{aligned} \int_{1}^{2} \frac{-43}{2} \frac{-43}{2} \frac{13200}{2} \frac{240}{2} \frac{1}{1} \frac{1}{1$  | $\begin{aligned} \int_{1}^{2} \frac{-45}{2} \frac{-45}{2} \frac{11200}{2} \frac{240}{2} \frac{1}{2} \frac{1}{2$  | ×2                              |                            |   |                               | :  |                 |  |
| $\frac{1}{2}\frac{1}{2} = -\frac{1}{2}1$       | $\frac{1}{2}\frac{1}{2}, \frac{1}{2}, \frac{1}{2}1$   | ^)<br>X_                        |                            |   |                               |  |                 |  |
| $\frac{1}{2}$ | $\begin{aligned} \sum_{q=1}^{n} \sum_$  | ×1×2                            |                            |   |                               |  |                 |  |
| $\frac{1}{2} \frac{1}{2} \frac{1}$   | $\begin{aligned} \sum_{q=1}^{n} (0, 403) & 1, 302 & 1 & 1 & 0, 011 \\ \sum_{q=1}^{n} (0, 403) & 1, 202 & 1, 202 & 1, 202 & 0, 213 \\ \sum_{q=1}^{n} (0, 1, 5, 122 & 423, 223 & 1 & 0, 123 \\ \sum_{q=1}^{n} (0, 1, 5, 122 & 122, 223 & 1 & 0, 123 \\ \sum_{q=1}^{n} (0, 1, 5, 123 & 122, 223 & 16 & 120, 600 \\ \end{bmatrix} \\ \text{Stendard Deviation } (S_q 1 based on duplicates is equal to ferror HS = 11.0 \\ \text{For the entire coperiment, the Siralative stendard deviation (SRD) is given by \\ \sum_{q=1}^{n} (1, 1, 5, 123 & 1233, 40 & 120 & 120 \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1, 1) & \text{Seese as 5, 5, 5, 13} \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1) & \text{Seese as 5, 5, 5, 13} \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1) & \text{Seese as 5, 5, 5, 13} \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1) & \text{Seese as 5, 5, 5, 13} \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1, 1) & \text{Seese as 5, 5, 5, 13} \\ \sum_{q=1}^{n} (1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1$   | x 1x 3<br>x 1x.                 |                            |   |                               |  |                 |  |
| $\frac{1}{2} \frac{1}{2} \frac{1}$   | $\frac{1}{2} \frac{1}{2} \frac{1}$   | x2x3                            | +2,610                     | 54,481  |                               |  | 0.45            |  |
| $\frac{1}{2}\frac{1}{2}\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\frac{1}{2$     | $\frac{1}{2}\frac{1}{2}\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\frac{1}{2$ | ×2×4<br>x . x .                 |                            |   | •                             |  |                 |  |
| $\frac{1}{2}\frac{1}{2}\frac{1}{2}, -\frac{2}{2}, -\frac{1}{2}, -$   | $\frac{1}{2}\frac{1}{2}\frac{1}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{1}{2}, -$   | ~3~4<br>×1×2×3                  | +:_860                     | 27.679  |                               |  | 0.23            |  |
| $\frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} - \frac{1}{2} - \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} - \frac{1}{2} \frac{1}{2$   | $\frac{1}{2}\frac{1}{2}\frac{1}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{2}{2}, -\frac{1}{2}, -$   | x <sub>1</sub> x <sub>2</sub> x | +7.522                     | 452,629   |                               |  | 3.75            |  |
| $\frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{227}{220} \frac{1}{16} \frac{1}{100,000} = \frac{1}{1,00}$ Standard Daviation (S <sub>1</sub> ) based on duplicates is equal to $\sqrt{40 \text{ row is}} = \frac{11.0}{100}$ .<br>For the entire organization (S <sub>1</sub> ) based on duplicates is equal to $\sqrt{40 \text{ row is}} = \frac{11.0}{100}$ .<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>Tore:<br>$\frac{1}{2,4-001}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}{2,1-000}$<br>$\frac{1}$   | $\frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{227}{220} \frac{1}{10} \frac{1}{100} \frac{1}{100,000}$ Standard Daviation (S <sub>1</sub> ) based on dupitates is equal to $\sqrt{krror M3} = \frac{11.0}{100}$ .<br>For the entire experiment, the S relative standard deviation (SABD) is given by<br>$\frac{1}{2,4-001} \frac{1}{2,4-001} \frac{1}{100} \frac{1}{1000} + \frac{1}{1000} \frac{1}{1000} + 6.205$ $\frac{7,4-001}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{1000} + 6.205$ $\frac{7,4-001}{1000} \frac{1}{1000} 1$   |                                 |                            |   | •                             |  |                 |  |
| Standard Deviation (S <sub>x</sub> ) based on duplicates is equal to <i>form</i> MS = <u>11,0</u><br>for the entire operiment, the S relative standard deviation (S ASD) is<br>given by<br>$S_{RSD} = \frac{4}{grand man} + \frac{(11,0)}{177,352} + 6,305$<br>$Z_{1,4}^{4,001}$<br>Tore:<br>$S_{RSD} = \frac{4}{grand man} + \frac{(11,0)}{177,352} + 6,305$<br>$Z_{1,5}^{4,001} + \frac{11}{2},000 + 1$<br>$S_{1,5}^{4,001} + \frac{11}{2},000 + 16$<br>$S_{1,5}^{4,001} + \frac{11}{2},000 + 100 + 100$<br>$S_{1,5}^{4,001} + \frac{11}{2},000 + 100 + 100 + 1000$  | Standard Deviation ( $\xi_{y}$ ) based on duplicates is equal to form $MS = 11.0$<br>for the entire operiment, the S relative standard deviation (S ABD) is<br>given by<br>$f = 850 + \frac{4}{grand man} + \frac{(11.0)}{177.352} + 6.205$<br>$Z_{1}^{4.001}$<br>Tore:<br>$Z_{1}^{4.001}$<br>Tore:<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{2}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.001}$<br>$Z_{1}^{4.$   | ~?~?~<br>X1X2X3X4               |                            | 227.420   | -                             |  |                 |  |
| For the entries observed then, the S relative standard deviation (S RSD) is<br>given by:<br>$g_{RSD} = \frac{4}{g^2 end mean} = \frac{(11,0) (100)}{177,352} = 6,205$ $Z_{1} = \frac{1}{72,352} = 6,205$ $Z_{1} = \frac{1}{72,40} = \frac{1}{72,352} = 6,205$ $Z_{1} = \frac{1}{72,40} = \frac{1}{72,352} = \frac{1}{72$   | For the entries owner least, the S relative standard deviation (S RSD) is<br>given by:<br>$\begin{aligned} s_{RSD} = \frac{s_{y}^{-1} (100)}{grand mean} = \frac{(11,0) (100)}{177,352} + 6,205 \\ \hline \\ r_{y} + QMT \\ \hline \\ r_{y} + QMT \\ \hline \\ r_{y} + QMS \\ \hline \\ r$  | Error                           |                            | 1932_94   | 16                            | 120.609                                  |                 |  |
| For the antire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$g_{RSD} = \frac{4}{grand man} + \frac{(11_{4}0) (100)}{177,352} + 6,205$ $\frac{7}{2} + \frac{100}{177,352} + 6,205$ $\frac{7}{2} + \frac{100}{2} + \frac{100}{2} + \frac{100}{177,352} + 6,205$ $\frac{7}{2} + \frac{100}{2} + \frac{1000}{2} + \frac{100}{2} + $   | For the antire experiment, the S relative standard deviation (S RSD 1s<br>given by<br>$g_{RSD} = \frac{4}{grand mean} + \frac{(11,0) \cdot (100)}{(177,352)} + 6,205$ $Z_{1} + C_{2} $   |                                 |                            |   |                               |  | _               |  |
| given by<br>$f_{R3D} = \frac{4}{grand man} + \frac{(11,0)}{177,352} + 6,205$ $r_{4} = \frac{1}{2} + \frac{100}{177,352} + 6,205$ $r_{4} = \frac{1}{2} + \frac{100}{177,352} + 6,205$ $r_{4} = \frac{1}{2} + \frac{100}{177,352} + + \frac{1000}{177,352} + \frac{100}{177,352} + \frac{100}{177,3$   | given by<br>$f_{R3D} = \frac{4}{grand man} + \frac{(11,0) + (100)}{177,352} + 6,205$ $2,4-001$ Torei 00,778 29354,000 12<br>1 + 1 + 7,265 + 69,711 + 1 + 1000 + 5,5, 3,135 + 10,011 + 10,001 + 10,001 + 10,000 + 10,001 + 10   | Stenderd (                      | Deviation (                | Sy) based on du   | plicates is (                 | equal to Verror HI                       | i = <u>11_0</u> |  |
| given by<br>$f_{RSD} = \frac{4}{grand man} + \frac{(11,0)}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{(11,0)}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{111,01}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{111}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{111}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{111}{177,352} + 6,205$ $r_{4} = \frac{9}{27 and man} + \frac{111}{177,352} + 6,205$ $r_{4} = \frac{1}{27 and man} + \frac{1}{27 and$   | given by<br>$f_{R3D} = \frac{4}{grand man} + \frac{(11,0) + (100)}{177,352} + 6,205$ $r_{4} = \frac{1}{2} + \frac{100}{2} + \frac{1}{2} + \frac{100}{177,352} + 6,205$ $r_{4} = \frac{1}{2} + \frac{100}{2} + \frac{1}{2} + \frac{100}{2} + \frac{100}{2} + \frac{1}{2} +$   | for the e                       | ntire omper                | iment, the \$ re  | lative stand                  | ard deviation (\$ A                      | 150) 18         |  |
| $\frac{1}{2} \frac{1}{2} \frac{1}$   | $\frac{1}{2} \frac{1}{2} \frac{1}$   |                                 |                            |   |                               |  |                 |  |
| Tore: 302434,000 32<br>C,F,** 95,778 295548,000 1<br>x1 *7,645 495,711 1 Same at 5,5, 5,75*<br>x2 *7,268 0,038 1 - 0,01<br>x4, -22,482 3958,972 1 * 65,46*<br>x1x2 *5,998 287,656 1 - 3,52<br>x1x3 *2,754 59,817 1 * 0,40<br>x2x3 *2,754 99,817 1 * 0,40<br>x1x4 *4,621 170,825 1 * 2,09<br>x1x5 * -4,621 170,825 1 * 2,00<br>x1x5 * -4,621 170,825 1 * 2,00<br>x1x5 * -4,642 1 170,825 1 * 2,00<br>x1x5 * -4,640 134,474 1 * 1,70<br>x1x5 * -4,640 134,474 1 * 0,20<br>x1x5 * -4,257 12,652 1 * 0,20<br>x1x5 * -4,257 12,653 1 * 0,20<br>x1x5 * -4,257 12,658 16 * 0,20<br>x1x5 * -4,257 12,658 16 * 0,20<br>x1x5 * -4,257 12,658 16 * 0,20<br>x15 * -4,257 12,658 16 * 0,20<br>x15 * -4,257 12,658 16 * 0,20<br>* -4,257 * 0,20<br>* -4,25  | Tore: 302434,000 32<br>C,F,** 95,778 293548,000 1<br>x1 +7,645 495,711 1 Same at 5.5, 5,73*<br>x2 -7,768 0,038 1 - (0,01<br>x4 -22,882 3338,972 1 - 65,6*<br>x1x2 -2,982 293548,972 1 - 63,6*<br>x1x2 -2,982 297,558 1 - 3,52<br>x1x3 -2,734 59,817 1 - 0,40<br>x2x3 -2,734 99,817 1 - 0,40<br>x2x3 -2,734 99,817 1 - 0,40<br>x2x4 -4,621 170,622 1 - 1,18<br>x1x2 -4,642 1 170,622 1 - 2,09<br>x1x2 -4,640 138,474 1 - 1,17<br>x1x2 -4,640 138,474 1 - 1,70<br>x1x2 -4,640 138,474 1 - 0,20<br>x1x2x4 -4,180 138,474 1 - 0,20<br>x1x2x4 -1,257 12,652 1 - 0,20<br>x1x2x4 -4,180 138,474 1 - 0,20<br>x1x2x4 -4,180 -4,475 18,480 -1 48,490<br>x1x2x4 -4,490 138,474 1 - 0,297<br>x1x2x4 -4,490 1  |                                 |                            | \$ RSD •  |                               | <u>0) (100)</u> = 6,201<br>7,352 = 6,201 | ٤               |  |
| C.F.** 93,778 293348,000 1<br>$x_1 + 7,643 = 409,711 1 3 are as 5,5, 3,75*  x_2 - 7,264 0,038 1 - 5,17*  x_3 - 0,099 0,038 1 - 0,001  x_4 - 29,882 93384,972 1 - 65,64  x_1x_2 - 29,882 - 3334,972 1 - 0,600  x_1x_3 - 2,024 32,775 1 - 0,600  x_2x_3 - 2,024 32,775 1 - 0,600  x_2x_3 - 4,621 170,423 1 - 1,12  x_2x_4 - 4,621 170,423 1 - 1,18  x_1x_2x_4 - 4,621 170,423 1 - 4,200  x_1x_2x_4 - 4,620 138,474 1 - 1,70  x_1x_2x_4 - 4,160 138,474 1 - 0,200  x_2x_3x_4 - 1,227 12,632 1 - 0,200  x_1x_2x_4 - 1,227 12,632 1 - 0,207  From 1300,89 16 81,681  Standard Devlation ($x_1) based on duplicates is equal to ferror MS = 9,04  For the antire apperiment, the S relative stenderd deviation ($R50) is given by  \frac{$x_40}{x_1} - \frac{$x_10}{x_1} + \frac{$x_10}{x_1} + $x_10} - \frac{$(100)}{95,778} - 9,455 $  | $C_{r}^{r} e^{e} = 93,778 = 293588,000 + 1 = 5,5,5 = 3,139 = 3,179 = $   | Total                           |                            |   |                               |  |                 |  |
| $\frac{x_{2}}{x_{3}} = -7.268 \qquad 0.038 \qquad 1 \qquad = \qquad 2.17^{n}$ $\frac{x_{3}}{x_{3}} = -2.069 \qquad 0.038 \qquad 1 \qquad = \qquad 0.001$ $\frac{x_{4}}{x_{4}} = -23.82 \qquad 5338.972 \qquad 1 \qquad = \qquad 63.6^{n}$ $\frac{x_{1}x_{2}}{x_{1}x_{2}} = -3.969 \qquad 287.858 \qquad 1 \qquad = \qquad 3.52$ $\frac{x_{1}x_{3}}{x_{1}x_{4}} = -2.024 \qquad 32.775 \qquad 1 \qquad = \qquad 0.40$ $\frac{x_{2}x_{3}}{x_{3}x_{4}} = -2.044 \qquad 32.775 \qquad 1 \qquad = \qquad 0.40$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -2.464 \qquad 53.998 \qquad 1 \qquad = \qquad 1.12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -3.464 \qquad 93.998 \qquad 1 \qquad = \qquad 1.18$ $\frac{x_{1}x_{2}x_{3}}{x_{3}x_{4}} = -3.464 \qquad 93.998 \qquad 1 \qquad = \qquad 1.18$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{2}x_{4}} = -4.621 \qquad 170.825 \qquad 1 \qquad = \qquad 1.70$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{2}x_{4}} = -4.621 \qquad 170.825 \qquad 1 \qquad = \qquad 1.70$ $\frac{x_{1}x_{2}x_{3}}{x_{3}x_{4}} = -4.621 \qquad 170.825 \qquad 1 \qquad = \qquad 1.70$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{2}x_{4}} = -4.160 \qquad 138.474 \qquad 1 \qquad = \qquad 0.70$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{2}x_{4}} = -1.237 \qquad 12.632 \qquad 1 \qquad = \qquad 0.97$ $\frac{x_{1}x_{2}x_{3}}{x_{1}x_{2}x_{3}x_{4}} = -1.237 \qquad 12.632 \qquad 1 \qquad = \qquad 0.97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1.237 \qquad 12.632 \qquad 1 \qquad = \qquad 0.97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -3.160 \qquad 138.474 \qquad 1 \qquad = \qquad 0.97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{3}x_{4}} = -3.161 \qquad 76.914 \qquad 1 \qquad = \qquad 0.97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -3.160 \qquad 136.69 \qquad 16 \qquad 81.681$ $\frac{37anderd}{avar} faveries is equal to \sqrt{xrerot} MS = 9.04 \frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{2}x_{3}}{x_{1}x_{3}x_{4}} = -3.161 \qquad 9.047 \frac{x_{1}x_{3}}{x_{1}x_{4}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{4}x_{4}}{x_{5}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{4}x_{4}}{x_{4}x_{5}x_{4}} = -3.600 \qquad 13.601 \frac{x_{1}x_{4}x_{4}}{x_{5}x_{4}} = -3.600 \frac{x_{1}x_{3}}{x_{1}x_{4}} = -3.160 \qquad 13.601 \frac{x_{1}x_{4}}{x_{5}x_{4}} = -3.600 \qquad 13.600 \qquad 13.600 \qquad 13.600 \qquad 13.600 \qquad 13.600 $  | $\frac{x_{2}}{x_{3}} = -7,268 \qquad 0.038 \qquad 1 \qquad = \qquad 9.179$ $\frac{x_{3}}{x_{3}} = -2,069 \qquad 0.038 \qquad 1 \qquad = \qquad 60.01$ $\frac{x_{4}}{x_{5}} = -23,829 \qquad 538,672 \qquad 1 \qquad = \qquad 63,69$ $\frac{x_{1}x_{2}}{x_{5}} = -3,998 \qquad 287,838 \qquad 1 \qquad = \qquad 3.92$ $\frac{x_{1}x_{3}}{x_{1}x_{3}} = -2,024 \qquad 32,775 \qquad 1 \qquad = \qquad 0.40$ $\frac{x_{2}x_{3}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 170,825 \qquad 1 \qquad = \qquad 1,12$ $\frac{x_{3}x_{4}}{x_{3}x_{4}} = -4,621 \qquad 130,874 \qquad 1 \qquad = \qquad 0,20$ $\frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,20$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{3}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}x_{4}} = -1,100$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{3}x_{4}}{x_{1}x_{4}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}} = -1,237 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{2}x_{3}}{x_{1}x_{4}} = -3,439 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{2}}{x_{1}x_{4}} = -3,439 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{4}}{x_{4}} = -3,439 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{4}}{x_{4}} = -3,439 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{4}}{x_{4}} = -3,449 \qquad 1 \qquad = \qquad 0,97$ $\frac{x_{1}x_{4}}{x_{4}} = -3,449 \qquad 1 \qquad = \qquad 0,459$ $\frac{x_{1}}{x_{4}} = -3,449 \qquad 1 \qquad = \qquad 0,459$ $\frac{x_{1}}{x_{4}}$  |                                 | 95.778                     |   |                               |  |                 |  |
| $\frac{x_{3}}{x_{1}} = -0.069  0.038  1 \qquad -  <0.01$ $\frac{x_{4}}{x_{1}} = -23.882  9338.972  1 \qquad -  & 63.69$ $\frac{x_{1}}{x_{1}} = -2.734  59.817  1 \qquad -  & 0.73$ $\frac{x_{1}}{x_{1}} = -2.024  32.775  1 \qquad -  & 0.40$ $\frac{x_{2}}{x_{3}} = -3.984  91.498  1 \qquad -  & 1.12$ $\frac{x_{2}}{x_{4}} = -4.621  170.822  1 \qquad -  & 2.09$ $\frac{x_{3}}{x_{4}} = -4.621  170.822  1 \qquad -  & 2.09$ $\frac{x_{3}}{x_{4}} = -4.621  170.822  1 \qquad -  & 4.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  133.069  1 \qquad -  & 4.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  133.069  1 \qquad -  & 4.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  133.069  1 \qquad -  & 0.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  133.069  1 \qquad -  & 0.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  138.074  1 \qquad -  & 0.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  136.484  1 \qquad -  & 0.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  136.484  1 \qquad -  & 0.20$ $\frac{x_{1}}{x_{4}} = \frac{x_{4}}{2.0}  136.49  16  81.681$ Standard Devlation $(\frac{x_{1}}{y})$ based on dualicates is equal to $\sqrt{Error HS} = 9.04$ For the antire experiment, the S relative standard deviation (S RSD) is given by $\frac{S RSU = \frac{x_{1}(1007)}{0.000} + \frac{(9.04)(100)}{93.778} + 9.455$ $\frac{e^{x_{1}}}{9.9} (1,16) + 4.491$ an F value in the table above unich exceeds 4.49 is algoriticant at the 995 probability level. $\frac{e^{x_{1}}}{e^{y_{1}}} = 1.9 \text{ total corrected sum of squares.}$  | $\frac{x_{3}}{x_{1}} = -0.069  0.038  1 \qquad =  <0.01$ $\frac{x_{4}}{x_{1}} = -25.982  3538.972  1 \qquad =  65.69$ $\frac{x_{1}x_{2}}{x_{1}x_{3}} = -2.734  59.817  1 \qquad =  0.73$ $\frac{x_{1}x_{3}}{x_{1}x_{4}} = -2.024  32.775  1 \qquad =  0.40$ $\frac{x_{2}x_{3}}{x_{2}x_{4}} = -4.621  170.622  1 \qquad =  2.09$ $\frac{x_{3}x_{4}}{x_{1}x_{3}} = -5.464  99.998  1 \qquad =  1.12$ $\frac{x_{4}x_{4}}{x_{1}x_{3}} = -6.621  170.622  1 \qquad =  2.09$ $\frac{x_{3}x_{4}}{x_{1}x_{3}} = -6.621  170.622  1 \qquad =  2.09$ $\frac{x_{3}x_{4}}{x_{1}x_{3}} = -6.621  170.622  1 \qquad =  2.09$ $\frac{x_{3}x_{4}}{x_{1}x_{3}} = -6.621  138.674  1 \qquad =  1.70$ $\frac{x_{1}x_{2}x_{4}}{x_{1}x_{3}} = -6.160  138.674  1 \qquad =  1.70$ $\frac{x_{1}x_{2}x_{4}}{x_{1}x_{3}} = -6.160  138.674  1 \qquad =  0.20$ $\frac{x_{1}x_{2}x_{4}}{x_{1}x_{3}} = -6.160  138.644  1 \qquad =  0.20$ $\frac{x_{1}x_{2}x_{4}}{x_{1}x_{4}} = -5.141  70.632  1 \qquad =  0.15$ $\frac{x_{1}x_{2}x_{4}}{x_{1}x_{3}} = -5.141  70.632  1 \qquad =  0.97$ For the antire asperiment, the \$ \$relative standerd deviation (\$ \$R30) is given by $\frac{$ R30 = \frac{x_{1}(100)}{0x_{3}nd magn} = \frac{(9.04)(100)}{93.738} = 9.455$ <sup>97</sup> 0.1,16) = 4.491 an F value in the table above which exceeds 4.49 is algorithmat at the 995 probability is val. <sup>97</sup> 0.1,16) = 4.491 an F value in the table above which exceeds 4.49 is algorithmat at the 995 probability is val.   | ×1                              | +7,663                     |   |                               | Same as 5,5,                             |                 |  |
| $ \frac{1}{3} \frac{1}{3} \frac{-23}{3} \frac{233}{3} \frac{272}{3} \frac{1}{3} \frac{1}{$   | $ \frac{1}{3} \frac{-23,887}{12} = \frac{3336,972}{1336} = \frac{1}{1} = \frac{69,66}{3,52} \\ \frac{1}{3} \frac{1}{3} = \frac{2,734}{2,734} = \frac{39,817}{39,817} = \frac{1}{1} = \frac{0,73}{0,40} \\ \frac{1}{3} \frac{1}{3} \frac{1}{3} = \frac{-2,024}{2,324} = \frac{32,775}{1,75} = \frac{1}{1} = \frac{0,40}{0,40} \\ \frac{1}{3} \frac{1}{3} \frac{1}{4} = \frac{-2,024}{4,21} = \frac{32,775}{1,0622} = \frac{1}{1} = \frac{-2,00}{2,00} \\ \frac{1}{3} \frac{1}{3} \frac{1}{4} = \frac{-3,464}{2,11} = \frac{9,998}{1,0620} = \frac{1}{1} = \frac{-4,20}{4,10} \\ \frac{1}{3} \frac{1}{3} \frac{1}{3} \frac{1}{3} = \frac{-3,464}{3,1060} = \frac{13,6874}{1} = \frac{-1,16}{1,10} \\ \frac{1}{3} \frac{1}{3} \frac{1}{3} \frac{1}{3} \frac{1}{3} = \frac{-4,20}{3,10} \\ \frac{1}{3} \frac$  | *2<br>*-                        |                            |   |                               | -  |                 |  |
| $ \frac{x}{12} + \frac{x}{2} + $   | $x_{1}x_{2} + s_{5} + 900 = 207, 650 + 1 + - 0, 352$ $x_{1}x_{4} - 2, 074 + 39, 617 + 1 + 0, 400$ $x_{1}x_{4} - 2, 074 + 32, 775 + 1 + 0, 400$ $x_{2}x_{3} + s_{5} + 304 + 91, 498 + 1 + 1, 12$ $x_{2}x_{4} - 4, 621 + 170, 625 + 1 + 2, 09$ $x_{3}x_{4} - 3, 644 + 95, 998 + 1 + 1, 18$ $x_{1}x_{2}x_{3} + 6, 540 + 343, 089 + 1 + 0, 170$ $x_{1}x_{2}x_{3}x_{4} + -4, 640 + 138, 474 + 1 + 1, 170$ $x_{1}x_{2}x_{3}x_{4} + -4, 640 + 138, 474 + 1 + 0, 170$ $x_{1}x_{2}x_{3}x_{4} + -4, 257 + 12, 652 + 1 + 0, 15$ $x_{1}x_{2}x_{3}x_{4} + -4, 257 + 12, 652 + 1 + 0, 15$ $x_{1}x_{2}x_{3}x_{4} + -4, 257 + 12, 652 + 1 + 0, 15$ $x_{1}x_{2}x_{3}x_{4} + -4, 257 + 12, 652 + 1 + 0, 15$ $x_{1}x_{3}x_{3}x_{4} + -5, 141 + 74, 914 + 1 + 0, 977$ For the antire experiment, the \$relative standard deviation (\$ R\$0) is given by $\frac{$x R$U} = \frac{$x_{1} (1007)}{$x_{1}a_{1}x_{1}a_{2}} + \frac{($x_{1}007)}{93, 778} + 9, 455$ $\frac{$x_{1}(1,16) + 4, 491 \text{ on } F \text{ value in the table above which exceeds 4, 49 is a ignificant at the 955 probability level.$ $\frac{$x_{1}(1,16) + 4, 491 \text{ on } F \text{ value in the table above which exceeds 4, 49 is a ignificant at the 955 probability level.$ $\frac{$x_{1}(1,16) + 1000}{C_{1}x_{1}x_{2}x_{3}x_{4}} + 5000 + 1$  | X,                              |                            |   |                               | -  |                 |  |
| $ \frac{x_{1}x_{2}}{x_{2}x_{3}} + \frac{-2}{3},024 \qquad 32,773 \qquad 1 \qquad = \qquad 0,40 \\ x_{2}x_{3} + \frac{-2}{3},024 \qquad 91,498 \qquad 1 \qquad = \qquad 1,12 \\ x_{2}x_{3} - \frac{-4}{4},621 \qquad 170,625 \qquad 1 \qquad = \qquad 2,09 \\ x_{3}x_{4} - \frac{-4}{3},644 \qquad 93,998 \qquad 1 \qquad = \qquad 1,18 \\ x_{1}x_{2}x_{3} + \frac{-4}{3},646 \qquad 343,089 \qquad 1 \qquad = \qquad 4,20 \\ x_{1}x_{2}x_{3} + \frac{-4}{3},260 \qquad 13,474 \qquad 1 \qquad = \qquad 1,70 \\ x_{1}x_{2}x_{3} + \frac{-4}{3},277 \qquad 12,632 \qquad 1 \qquad = \qquad 0,20 \\ x_{2}^{2}x_{3}x_{4} + \frac{-1}{3},277 \qquad 12,632 \qquad 1 \qquad = \qquad 0,20 \\ x_{2}^{2}x_{3}x_{4} + \frac{-1}{3},277 \qquad 12,632 \qquad 1 \qquad = \qquad 0,97 \\ Error \qquad 1306,89 \qquad 16 \qquad 81,681 \\ \hline $ Standard Deviation (\$_{y}\$) besed on dupicates is equal to $\sqrt{Error H3} = \frac{9,04}{9,04} \\ For the antire experiment, the $ relative standard deviation ($ R30) is given by \\ \hline \qquad \qquad$   | $ \frac{x_{1}x_{0}}{x_{2}x_{3}} + \frac{-2}{3}, \frac{224}{3} + \frac{32}{3}, \frac{773}{3} + \frac{1}{3} + \frac{-2}{3}, \frac{204}{3} + \frac{32}{3}, \frac{773}{3} + \frac{1}{3} + \frac{-2}{3}, \frac{204}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{2}{3}, \frac{1}{3} + \frac{-2}{3}, \frac{2}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3}, \frac{1}{3} + \frac{1}{3}, \frac$   | ×1×2                            |                            |   |                               | •  |                 |  |
| $\frac{1}{3}$ | A 34   | *1*3<br>*.*.                    |                            |   | -                             | 2  |                 |  |
| $\frac{1}{3}$ | A 34   | ×2×3                            |                            | 91,498  | ī                             | •  |                 |  |
| $x_{1}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{2}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 0,97$ Error 1306,89 16 81,681  Standard Deviation (S <sub>y</sub> ) based on duplicates is equal to $\sqrt{Error MS} = 9,04$ For the antire experiment, the S relative standard deviation (S RSO) is given by $\frac{S RSU}{r^{2} r_{2} r_{3}^{2} (1007)} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{9}{r^{2}} \cdot 99 (1,16) = 4,491 \text{ an F value in the table above which exceeds 4,49 is algorithment at the 935 probability level. $ **C.F. • Correction factor $\left(\frac{(1y)^{2}}{r}\right)$ . The difference between the total and C.F. is the total corrected sum of squares.   | $x_{1}^{2}y_{1}^{2}$ , $e_{1}^{2}4y_{2}^{2}$ , $e_{1}^{2}2y_{3}^{2}$ , $e_{1}^{2}2y_{3}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{4}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{$  | ×2×+                            |                            |   |                               | •  |                 |  |
| $x_{1}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{2}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 0,97$ Error 1306,89 16 81,681  Standard Deviation (S <sub>y</sub> ) based on duplicates is equal to $\sqrt{Error MS} = 9,04$ For the antire experiment, the S relative standard deviation (S RSO) is given by $\frac{S RSU}{r^{2} r_{2} r_{3}^{2} (1007)} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{9}{r^{2}} \cdot 99 (1,16) = 4,491 \text{ an F value in the table above which exceeds 4,49 is algorithment at the 935 probability level. $ **C.F. • Correction factor $\left(\frac{(1y)^{2}}{r}\right)$ . The difference between the total and C.F. is the total corrected sum of squares.   | $x_{1}^{2}y_{1}^{2}$ , $e_{1}^{2}4y_{2}^{2}$ , $e_{1}^{2}2y_{3}^{2}$ , $e_{1}^{2}2y_{3}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{4}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{$  | 1314<br>X,X,X,                  |                            |   |                               |  |                 |  |
| $x_{1}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{2}^{1} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 1,237$ $\frac{1}{2} x_{1}^{2} y_{1}^{2} y_{1} = 0,97$ Error 1306,89 16 81,681  Standard Deviation (S <sub>y</sub> ) based on duplicates is equal to $\sqrt{Error MS} = 9,04$ For the antire experiment, the S relative standard deviation (S RSO) is given by $\frac{S RSU}{r^{2} r_{2} r_{3}^{2} (1007)} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{9}{r^{2}} \cdot 99 (1,16) = 4,491 \text{ an F value in the table above which exceeds 4,49 is algorithment at the 935 probability level. $ **C.F. • Correction factor $\left(\frac{(1y)^{2}}{r}\right)$ . The difference between the total and C.F. is the total corrected sum of squares.   | $x_{1}^{2}y_{1}^{2}$ , $e_{1}^{2}4y_{2}^{2}$ , $e_{1}^{2}2y_{3}^{2}$ , $e_{1}^{2}2y_{3}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{4}^{2}y_{4}^{2}$ , $e_{1}^{2}2y_{4}^{2}y_{$  | x1x2x6                          |                            |   |                               |  |                 |  |
| $\frac{x_1^2 x_2^2 x_4}{8rc\sigma} = -5.141 \qquad 78.914 \qquad 1 \qquad = \qquad 0.97$<br>Error $1306.89 \qquad 16 \qquad 81.681$ Standard Davlation (S <sub>V</sub> ) based on duplicates is equal to $\sqrt{8rc\sigma} + 85 = 9.04$<br>For the antire experiment, the S relative standard deviation (S RSO) is<br>given by $\frac{S - 850}{\sigma^2 and maan} = \frac{(9.04) (100)}{95.778} + 9.455$ $\frac{9}{7} \cdot 99 (1,16) + 4.49; an F value in the table above which exceeds 4.49 is algorithment at the 955 probability level. \frac{190}{C_{s}F_{s}} + Correction factor (\frac{(10)^{2}}{n}). The difference between the total and C_{s}F_{s} is the total corrected sum of squares.$  | $x_1^{2}x_2^{2}x_{4}^{2} = -5.141  76.914  1  =  0.97$<br>Error $1306.89  16  81.681$<br>Standard Deviation $(S_{y})$ based on dualicates is equal to $\sqrt{Error MS} = 9.04$<br>For the antire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$\frac{S RSD}{Grand mean} = \frac{(9.04)(100)}{95.778} = 9.455$ $\frac{9.9}{3}(1,16) = 4.493 \text{ an F value in the table above which exceeds 4.49 is algorificant at the 995 probability level. \frac{FC_{x}F_{x}}{r} = C_{x}rection factor \left(\frac{(D_{y})^{2}}{r}\right), \text{ The difference between the total and C_{x}F_{x} is the total corrected sum of squares,}$  | ^1^3*4                          |                            |   |                               |  |                 |  |
| Error 1306.89 16 81.681<br>Standard Deviation (S <sub>v</sub> ) based on duplicates is equal to $\sqrt{Error HS} = 9.04$<br>For the antire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$S RSD = \frac{S_v (100)}{07gnd mean} = \frac{(9.04) (100)}{95,778} = 9.455$<br><sup>47</sup> .99 (1,16) = 4.49; an F value in the table above which exceeds 4.49 is<br>algorithment at the 995 probability level.<br><sup>46</sup> C.F. = Currection factor $\left(\frac{(Dv)^2}{n}\right)$ . The difference between the total and<br>C.F. is the total corrected sum of squares.  | Error 1306,89 16 81,681<br>Standard Deviation (S <sub>v</sub> ) based on dusticates is equal to $\sqrt{Error HS} = 9.04$<br>For the antire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$\frac{S RSD = \frac{S_v (1007)}{07 gnd mean} = \frac{(S_v 04) (100)}{93,778} = 9.425$<br><sup>47</sup> .99 (1,16) = 4.49; an F value in the table above which exceeds 4.49 is<br>algorithms to the 995 probability level.<br><sup>46</sup> C.F. = Currection factor $\left(\frac{(10x)^2}{n}\right)$ . The difference between the total and<br>C.F. is the total corrected sum of squares.   | *2*3*6<br>X.X.X.X.X.            |                            |   |                               |  |                 |  |
| For the entire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$\frac{g RSD = \frac{s_y (100)}{07g ng eqen} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{s_y g}{1,16} = 4,49; an F value in the table above which exceeds 4,49 isalgorithment at the 995 probability level. \frac{s_y C_y F}{n} = C_y F_z + C_y C_z + C_$   | For the entire experience, the S relative stenderd deviation (S RSD) is<br>given by<br>$\frac{g RSD = \frac{s_y (1007)}{0 T g n d mean} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{97}{s} \frac{99}{s} (1,16) = 4,49; an F value in the table above which exceeds 4,49 isalgorithment at the 995 probability level. \frac{g RC_z F_z}{r} = C_z F_z is the total corrected sum of squares.$  | trror                           |                            |   |                               |  |                 |  |
| For the entire experiment, the S relative standard deviation (S RSD) is<br>given by<br>$\frac{g RSD = \frac{s_y (100)}{07g ng eqen} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{s_y g}{1,16} = 4,49; an F value in the table above which exceeds 4,49 isalgorithment at the 995 probability level. \frac{s_y C_y F}{n} = C_y F_z + C_y C_z + C_$   | For the entire experience, the S relative stenderd deviation (S RSD) is<br>given by<br>$\frac{g RSD = \frac{s_y (1007)}{0 T g n d mean} = \frac{(9,04) (100)}{95,778} = 9,455$ $\frac{97}{s} \frac{99}{s} (1,16) = 4,49; an F value in the table above which exceeds 4,49 isalgorithment at the 995 probability level. \frac{g RC_z F_z}{r} = C_z F_z is the total corrected sum of squares.$  |                                 |                            |   |                               |  |                 |  |
| given by<br>$\frac{s}{g} \frac{1007}{grand maan} = \frac{(9_004)(100)}{95,778} = 9,455$<br><sup>67</sup> ,95 (1,16) = 4,49; an F value in the table above which exceeds 4,49 is<br>algorificant at the 955 probability level.<br><sup>66</sup> C.F. = Currection factor $\frac{(10)^2}{n}$ . The difference between the total and<br>C.F. is the total corrected sum of squares.   | given by<br>$\frac{s}{r_{grid}} = \frac{s}{r_{grid}} \frac{(100)}{95,778} = 9,455$ $\frac{s}{r_{grid}} \frac{(1,16)}{95} = 4,49; \text{ an } F \text{ value in the table above which exceeds 4,49 is algorithment at the 955 probability level.}$ $\frac{s}{r_{grid}} = \frac{s}{r_{grid}} \frac{(1,16)}{r_{grid}} = \frac{s}{r_{grid}} \frac{(1,16)}{r_{grid}} = \frac{1}{r_{grid}} = \frac{1}{r_{grid}} \frac{(1,16)}{r_{grid}} = \frac{1}{r_{grid}} (1,16$   | Standard (                      | Deviation (                | L) based on du  | elicetes is a                 | equal to Vertor HI                       | - +,04          |  |
| $\frac{s}{97} \frac{(1,16)}{99} = \frac{s}{97} \frac{(100)}{99 \frac{1}{97} \frac{100}{95} \frac{9}{95} \frac{(100)}{95} = 9.455}$<br><sup>97</sup> .99 (1,16) = 4.49; an F value in the table above which exceeds 4.49 is algorithment of the 995 probability level.<br><sup>97</sup> c.F. = Currection factor $\frac{(10)^2}{n}$ . The difference between the total and C.F. is the total corrected sum of squares.  | $\frac{s}{97} \frac{(1,16)}{99} = \frac{s}{97} \frac{(100)}{99,00} = \frac{(3,04)(100)}{93,778} = 9,455$ $\frac{97}{99} \frac{(1,16)}{99} = 4,49; an F value in the table above which exceeds 4.49 is algorithment at the 995 probability level. \frac{4\pi C_{s}F_{s}}{r} = C_{s}rsction factor \left(\frac{(10)^{2}}{r}\right), \text{ The difference between the total and } C_{s}F_{s} is the total corrected sum of squares.$   |                                 | tire exper                 | imont, the \$ re  | iative stande                 | ord deviation (\$ R                      | \$0) f#         |  |
| $\frac{g_{RSU} = \frac{Y}{GT gnd} \frac{g}{gg} = \frac{g_{RS}(4)}{gg} = \frac{g_{RS}(4)}{$   | $\frac{g}{dT} \frac{g}{dT} \frac$   | given by                        |                            |   |                               |  |                 |  |
| <sup>er</sup> , <sup>99</sup> (1,16) • 4,49; an F value in the table above which exceeds 4,49 is<br>algorithment at the 995 probability level.<br><sup>en</sup> C.F. • Currection factor $\left(\frac{(Dy)^2}{n}\right)$ . The difference between the total and<br>C.F. is the total corrected sum of squares.   | <sup>er</sup> .93 (1,16) • 4,49; an F value in the table above which exceeds 4,49 is<br>algorithment at the 955 probability level.<br><sup>en</sup> C.F. • Correction factor $\left(\frac{(D_F)^2}{n}\right)$ . The difference between the total and<br>C.F. is the total corrected sum of squares.  |                                 | 1                          | 8 (10)  | 07 (9,04                      | <u>4) (100)</u> • 9,451                  | 1               |  |
| **C.F. • Currection factor $\left(\frac{(D_r)^2}{n}\right)_r$ . The difference between the total and C.F. is the total corrected sum of squares,   | **C.F. • Currection factor $\left(\frac{(D_{T})^2}{n}\right)_{r}$ . The difference between the total and C.F. is the total corrected sum of squares.   |                                 |                            | grand m   | en 9                          | 5,118                                    |                 |  |
| C.F. is the total corrected sum of squares,  | C.F. is the total corrected sum of squares,  | ** .99 (1,1<br>.99 sign         | 16) = 4,49;<br>lificant at | an F value in t<br>the 955 probabi                        | the table aim<br>Fifty level, | ave which exceeds                        | 4.49 /8         |  |
| C.F. is the total corrected sum of squares,  | C.F. is the total corrected sum of squares,  | **C.F. + 0                      | Correction (               | factor $\left(\frac{(\underline{D}_{Y})^{2}}{n}\right)$ . | The differ                    | once hotveen the t                       | otel and        |  |
| 44   | 44   | c                               | .F, is the                 | totel correcte  | d sum of squi                 | or es,                                   |                 |  |
| 44   | 44   |                                 |                            |   |                               |  |                 |  |
|  |  |                                 |                            | 4   | 14                            |  |                 |  |
|  |  |                                 |                            |   |                               |  |                 |  |

| Total                         |         | 302434,000 | 32 |              |         |
|-------------------------------|---------|------------|----|--------------|---------|
| C.F.**                        | 95,778  | 293548,000 | 1  |              |         |
| <b>4</b> 1                    | +7,663  | 469,711    | 1  | Same as 5,5, | 5,75*   |
| x2                            | +7,268  | 0,038      | 1  | -            | 9,170   |
| x3                            | -0,069  | 0.038      | 1  | -            | <0.01   |
| x                             | -25.802 | 5358,972   | 1  |              | 6 9. 6* |
| x <sub>1</sub> x <sub>2</sub> | +5,998  | 287,638    | 1  | •            | 3,92    |
| xixi                          | -2,734  | 59.817     | 1  |              | 0.73    |
| x <sub>1</sub> x <sub>4</sub> | -2.024  | 32,775     | 1  | •            | 0.40    |
| ×2×3                          | +3,384  | 91,498     | T  | •            | 1, 12   |
| X2X4                          | -4,621  | 170,625    | ,  | •            | 2,09    |
| ×3×4                          | -3,464  | 95,998     | 1  | •            | 1,18    |
| x1x2x3                        | +6,540  | 343,089    | 1  | •            | 4,20    |
| X1X2X                         | -4,160  | 138,474    | ł  | •            | 1,70    |
| x1x3x4                        | +1,442  | 16,644     | 1  | -            | 0,20    |
| ×2×3×6                        | -1,297  | 12,632     | I  | -            | Ú, 15   |
| x1x2x3x4                      | -5,141  | 76,914     | 1  | •            | 0,97    |
| trror                         |         | 1306,89    | 16 | \$ 1, 68 t   |         |

| \$ RSU = + + <u>(9,04) (100)</u> = 9,455 |
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# Collaborative test

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Table A7. Concentrations of DNT, TNT, RDX, and HMX ( $\mu g/L$ ) reported by laboratories participating in collaborative test of HPLC method. (First set of four columns list identification indices for the other columns; remaining columns are also in sets of four-four analytes per hiporatory.)

|                   |          |              |             | •••      |
|-------------------|----------|--------------|-------------|----------|
| - PRINT<br>COLUMN |          |              |             |          |
| COUNT             | NATRIX   | SEIRE        | VIAL        | INJECTN  |
| BOW               | 80       | 80           | 80          | 80       |
| 1                 | 1. = A   | •            |             |          |
| 2                 | 1,       | 0. = u<br>0. | inspiked 1. | 1.       |
| 3                 | 1.       | ŏ.           | 1.          | 2.       |
| 4                 | 1,       | o.           | 2.          | 1.       |
| 5                 | 1.       | 1.           | 1.          | 2.       |
| 7                 | 1.       | 1.           | 1.          | 1.       |
| 8                 | 1.<br>1. | 1.           | 2.          | 1.       |
| 9                 | 1.       | 1.           | 2.          | 2.       |
| 10                | 1.       | 2.           | 1.          | 1.       |
| 11                | 1.       | 2.           | 1.          | 2.       |
| 12                | 1.       | 2.           | 2.          | 1.       |
| 13<br>14          | 1.       | 3.           | 2.<br>1.    | 2.       |
| 15                | 1.       | 3.           | 1.          | 1.       |
| 16                | 1.       | 3.           | 2.          | 2.       |
| 17                | 1.<br>1. | з.           | 2.          | 1.<br>2. |
| 18                | 1.       | 4.           | 1.          | 1.       |
| 19                | Ϊ,       | 4.<br>4.     | 1.          | 2.       |
| 20                | 1.       | 4.           | 2.          | 1.       |
| 21                | 2        | ō.           | 2.          | 2.       |
| 22<br>23          | 2        | 0.           | 1.          | 1.       |
| 24                | 2.       | 0.           | 2,          | 2.       |
| 25                | Ζ.       | 0.           | 2.          | 1.<br>2. |
| 26                | 2.2.     | 1.           | <u>ī</u> .  | 1.       |
| 27                | 2.       | 1.           | 1.          | 2.       |
| 28                | 2.       | 1.<br>1.     | 2.          | 1,       |
| 29                | 2.       | 2.           | 2.          | 2.       |
| 30                | 2.       | 2.           | 1.<br>1.    | 1.       |
| 31<br>32          | 2.       | 2.           | 2.          | 2.       |
| 33                | 2.       | 2.           | 2.          | 1.       |
| 34                | 2.<br>2, | з.           | 1.          | 2.       |
| 35                | 2, 2,    | 3.           | 1.          | 2.       |
| 36                | 2,       | 3.           | 2.          | 1.       |
| 37                | 2.       | 3.<br>4.     | 2.          | 2.       |
| 38                | 2.       | 4,           | 1.          | 1.       |
| 39<br>40          | 2.       | 4.           | 1.          | 2.       |
| 41                | 2.       | 4.           | 2.          | 1.       |
| 42                | 3. = C   | 0.           | 1.          | 2.       |
| 43                | 3.<br>3. | 0.           | 1.          | 1.<br>2. |
| 44                | 3.       | 0.           | 2.          | 1.       |
| 45                | 3.       | 0.<br>1.     | 2.          | 2.       |
| 46                | 3.       | 1.           | 1.          | 1.       |
| 47                | 3.       | 1.           | 1.          | 2.       |
| 48<br>49          | 3.       | 1.           | 2.          | 1.       |
| 50                | 3.       | 2.           | 1.          | 2.       |
| ~ ~               | 3,       | 2.           | 1.          | 1.       |
|                   |          |              |             | 2.       |



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Table A7 (cont'd) Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

| · · · · · ·    |                    |                    |                    |                  |
|----------------|--------------------|--------------------|--------------------|------------------|
| 51             | 3.                 | 2.                 | 2.<br>2.           | 1.<br>2.         |
| 52             | 3.                 | 2.                 | 1.                 | 1.               |
| \$3            | 3.                 | 3.                 | 1.                 | 2.               |
| 54             | 3.                 | 3.                 | 2.                 | 1.               |
| 55             | 3.                 | 3.                 | 2.                 | 2.               |
| 56             | 3.                 | 4.                 | 1.                 | 1.               |
| 57             | 3.                 | 4.                 | 1.                 | 2.               |
| 58             | 3.<br>3.           | 4.                 | 2.                 | 1.               |
| 59             | 3.                 | 4                  | 2.                 | 2.               |
| 60<br>61       | 4 D                | 0.                 | 1.                 | 2.               |
| 62             | 4.                 | 0.                 | 1.<br>2.           | 1.               |
| 63             | 4.                 | 0.                 | 2.                 | 2.               |
| 64             | 4.                 | 0.                 | 1.                 | 1,               |
| 65             | 4.                 | 1.                 | 1.                 | 2.               |
| 66             | 4.                 | 1.                 | 2.                 | 1.               |
| 67             | μ.                 | 1.                 | 2.                 | 2.               |
| 68             | 4,<br>4,           | 2.                 | 1.                 | 1.               |
| 69             | 4.                 | 2.                 | 1.                 | 2.               |
| 70<br>71       | 4.                 | 2.                 | 2.                 | 2.               |
| 72             | 4.                 | 2.                 | 2.                 | ĩ.               |
| 73             | 4.                 | 3.                 | 1.                 | 2.               |
| 74             | 4.                 | 3.                 | 2.                 | 1.               |
| 75             | 4.                 | 3.<br>3.           | 2.                 | 2.               |
| 76             | 4.                 | J.<br>4.           | 1.                 | 1.               |
| 77             | 4.                 | 4.                 | 1.                 | 2.               |
| 78             | 4                  | 4.                 | 2.                 | 1.               |
| 79<br>80       | 4.                 | 4.                 | 2.                 | 2.               |
|                | T C10-C13          |                    |                    | HMX LAB1         |
| PRIN<br>COLUMN | DNT LAB1           | THT LART           | REI LABI           | 80               |
| COUNT          | 80                 | 80                 | 80                 |                  |
| ROW            |                    |                    | 54,900             | 0.000            |
| 1              | 0.000              | 29.800<br>27.230   | 50.500             | 0.000            |
| 2              | 0.000              | 27.400             | 58,100             | 0.000            |
| 3              | 0.000<br>0.000     | 32.300             | 58,400             | 0.000            |
| ц<br>Б         | 42.500             | 63,900             | 149.900            | 35.800<br>36.800 |
| 5<br>6         | 48.300             | 66.900             | 151.600            | 32,300           |
| 7              | 50.000             | 62.800             | 145.500            | 37.700           |
| 8              | 46.900             | 60.300             | 247.200            | 116.100          |
| 9              | P4.300             | 133,300<br>131,100 | 257.600            | 131.300          |
| 10             | 87.900             | 129.400            | 244,300            | 119.700          |
| 11             | 03,507<br>£7,800   | 135.800            | 252.700            | 129.000          |
| 12             | \$2.100            | 142.000            | 273.300            | 131.700          |
| 13<br>14       | 90.577             | 143.500            | 260.200            | 127.200          |
| 15             | \$6.400            | 143.600            | 273.300<br>304.100 | 129.600          |
| 16             | \$5.300            | 147.600            | 555,500            | 202.800          |
| 17             | 124.300            | 203.900<br>157.600 | \$39.500           | 269.200          |
| 18             | 125.300            | 205.500            | 544,600            | 208.300          |
| 19             | 126.600<br>125.700 | 202.370            | 558.600            | 2 03.800         |
| 20             | 0.000              | 0.000              | 0.000              | 0.000            |
| 21             | 0.000              | 0.000              | 0.000              | 0.000            |
| 2 2<br>2 3     | 0.000              | 0.000              | 0.000              | 0.000            |
| 24             | 0.000              | C.000              | 0.00.<br>61,200    | 61,000           |
| 25             | 48.900             | 47,300             | 01,444             |                  |
|                |                    |                    |                    |                  |



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# Table A7 (cont'd).

| 26     | 52.700     | 43.500   | 62.300   | 64.100   |
|--------|------------|----------|----------|----------|
| 27     | 48.300     | 47.100   | 72.000   | 60.900   |
| 28     | 52.000     | 39.600   | 68.800   | 57.700   |
| 29     | 83.100     | 121.700  | 274.900  | 222.600  |
| 30     | 87.800     | 121.600  | 265.100  | 212.000  |
| 31     | 138.300    | 177.100  | 248.800  | 211.900  |
| 32     | 85.300     | 121.200  | 251.900  | 214.200  |
| 33     | 100.200    | 133.900  | 287.800  | 232.500  |
| 34     | \$7.800    | 137.800  | 271,800  | 234.900  |
| 35     | 162.400    | 157.300  | 280.100  | 232.100  |
| 36     | \$8.900    | 135.300  | 261.800  | 229.200  |
| 37     | 63.000     | 86°COO   | 376.700  | 312.400  |
| 38     | 58.400     | 77.200   | 375.100  | 313.300  |
| 39     | 61.100     | 77.000   | 374.600  | 320.700  |
| 40     | 64.300     | 76.700   | 382.800  | 315.800  |
| 41     | 56.300     | C.COO    | 0.000    | 113.400  |
| 42     | 58.700     | 0.000    | 0.000    | 118.800  |
| 43     | 52.700     | 0.000    | 0.000    | 116.400  |
| 44     | 54.900     | 0.000    | 0.000    | 116.500  |
| 45     | 140.700    | 63.900   | 379,400  | 446.200  |
| 46     | 134.500    | 67.500   | 417.200  | 440.700  |
| 47     | 147.400    | 85.200   | 377.000  | 430.500  |
| 48     | 141.400    | 62.200   | 383.100  | 436.600  |
| 49     | 204.200    | 157.300  | 279.600  | 347.900  |
| 50     | 235.700    | 191.300  | 238.000  | 362.200  |
| 51     | 206.100    | 152.600  | 234.500  | 357.300  |
| 52     | 191.000    | 111.500  | 284.100  | 353.500  |
| 53     | 185.700    | 132.900  | 243.900  | 337.700  |
| 54     | 183.800    | 132.600  | 212.900  | 330.000  |
| 55     | 196.100    | 142.300  | 257.600  | 333.300  |
| 56     | 184.700    | 134.900  | 212.000  | 330.000  |
| 57     | 127.700    | 37.300   | 74.700   | 180.300  |
| 58     | 131.000    | 35.400   | 67.200   | 182,700  |
| 59     | 129.600    | 40.800   | 54.000   | 173.000  |
| 60     | 120.400    | 35.900   | 70.700   | 180.900  |
| 61     | 0.000      | C.000    | 95.700   | 0.000    |
| 62     | C.000      | 0.000    | 109.400  | 0.000    |
| 63     | 0.000      | 0.000    | 90.800   | 0.000    |
| 64     | 0.000      | 0.000    | 113.300  | 0.000    |
| 65     | 123.400    | 173.500  | 570.600  | 205.100  |
| 66     | 121.300    | 170,000  | 595.400  | 204.900  |
| 67     | 139.000    | 154.300  | 557.000  | 203.100  |
| 68     | 154.500    | 135.800  | 569,300  | 206.600  |
| 69     | 63,990     | 105.500  | 325.300  | 136.500  |
| 70     | 107.400    | 126.000  | 324,700  | 136.800  |
| 71     | 64.000     | 99.500   | 336.300  | 137.700  |
| 72     | 104.900    | 126.400  | 322,800  | 131.300  |
| 73     | 178.000    | 2(6.300  | 463.100  | 260.900  |
| 74     | 174.600    | 206.600  | 481.300  | 246.700  |
| 75     | 180.700    | 205.800  | 490.700  | 251.800  |
| 76     | 173.100    | 198.900  | 466.400  | 233.300  |
| 77     | 40.900     | 22.400   | 197.400  | 39.700   |
| 78     | 35.500     | 24.600   | 208.500  | 38.100   |
| 79     | 45.600     | 31.100   | 199.300  | 47.100   |
| 80     | 35.300     | 18.900   | 177.900  | 38.800   |
|        |            |          |          |          |
|        |            |          |          |          |
|        | NT C20-C23 |          |          |          |
| COLUMN |            | TNT LAB2 | RDX LAB2 | HMX LAB2 |
| COUNT  | 80         | 80       | 80       | 80       |
| BOW    | 0 000      | 37 000   | 100 000  | A AAA    |
| 1      | 0.000      | 37.000   | 158.900  | 0.000    |
| 2      | 0.000      | 30.900   | 202,100  | 0.000    |

# Table A7 (cont'd). Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

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| 3         | 0.000              | 26.200  | 76.400  | 0.000   |
|-----------|--------------------|---------|---------|---------|
| 4         | 0.000              | 33,000  | 113.800 | 0.000   |
| 5         | 46.900             | 64.400  | 159.100 | 46.300  |
| 6         | 48.000             | 67.300  | 163.600 | 33.400  |
| 7         | 52.400             | 73.200  | 163.800 | 45.000  |
| 8         | 46.300             | 67.600  | 158.100 | 48.900  |
| 9         | P6.900             | 129.100 | 267.900 | 129,100 |
| 10        | 86.200             | 134.300 | 266.900 | 126,100 |
| 11        | 85.500             | 138.300 | 264.200 | 129.100 |
| 12        | 89,100             | 138.200 | 256.700 | 135.400 |
| 13        | 106.410            | 157.800 | 292.900 | 147.200 |
| 14        | 108.900            | 165.000 | 283.400 | 145,400 |
| 15        | 102.900            | 151.700 | 301.500 | 143.100 |
| 16        | 97.400             | 152.400 | 295.400 |         |
| 17        | 121.300            | 207.100 | 574.700 | 137.000 |
| 18        | 125.200            | 208.000 | 570.900 | 225.300 |
| 19        | 131.100            | 203.000 | 553.000 | 237.400 |
| 20        | 124.100            | 207.400 |         | 222.300 |
| 21        | 0.000              |         | 545.400 | 222.800 |
| 22        |                    | 0.000   | 0.000   | 0.000   |
| 23        | C.000              | 0.000   | 0.000   | 0.000   |
|           | 0.000              | C.COO   | 0.000   | 0.000   |
| 24        |                    | 0.000   | 0.000   | 0.000   |
| 25        | 64.100             | 53.900  | 71.100  | 73.800  |
| 26        | 62.900             | 54.100  | 69.000  | 77.700  |
| 27        | 62.600             | 54.700  | 76.400  | 123.700 |
| 28        | 62.100             | 49.600  | 79.100  | 186.700 |
| 29        | 116.000            | 142.200 | 262.500 | 286.000 |
| 30        | 116.300            | 138.000 | 264.900 | 229.100 |
| 31        | 112.400            | 135.300 | 254.100 | 223.000 |
| 32        | 114.100            | 125.900 | 245.100 | 233.200 |
| 33        | 127.270            | 157.100 | 280.500 | 243.400 |
| 34        | 126.100            | 153.900 | 259.300 | 230.600 |
| 35        | 128.900            | 156.700 | 272.200 | 331.300 |
| 36        | 128.400            | 156.500 | 268.700 | 236.100 |
| 37        | 79.200             | 90.700  | 374.500 | 423.600 |
| 38        | 78.600             | 90.000  | 367.800 | 328.600 |
| 39        | 75.500             | £4.700  | 373.100 | 316.500 |
| 40        | 76.000             | e5.300  | 364.100 | 343.400 |
| 41        | 72.000             | 0.000   | 0.000   | 128.200 |
| 42        | 72.400             | 0.000   | 0.000   | 114.700 |
| 43        | 71.200             | C.C00   | 0.000   | 125.000 |
| 44        | 77.000             | 0.000   | 0.000   | 128.100 |
| 45        | 153.400            | 90.800  | 380.500 | 446.500 |
| 46        | 150.000            | 86.800  | 379.300 | 452.200 |
| 47<br>48  | 147.200<br>151.200 | 82.500  | 374.100 | 461.000 |
| 49        |                    | 88.800  | 399.800 | 453.300 |
| 50        | 198.800            | 155.000 | 274.600 | 359.900 |
|           | 199.700            | 149.900 | 291.900 | 368.800 |
| 51<br>52  | 202.000            | 157.700 | 288.000 | 365.900 |
|           | 189.900            | 150.100 | 275.000 | 337.700 |
| 53        | 154.100            | 146.700 | 259.300 | 350.400 |
| 54        | 183.200            | 136.200 | 257.100 | 342.900 |
| 55        | 193.500            | 136.200 | 264.400 | 491.700 |
| 56        | 186.300            | 140.000 | 262.700 | 354.800 |
| 57        | 133.500            | 51,400  | 76.100  | 193.400 |
| 59        | 135.400            | 50.000  | 74.200  | 198.300 |
| 59        | 139.000            | 54.600  | 78.800  | 201.800 |
| 60        | 136.370            | 53.800  | 76.600  | 189.700 |
| 61        | 0.000              | 0.000   | 174.900 | 0.000   |
| 62        | 0.000              | 0.000   | 122.500 | 0.000   |
| 63<br>61  | 0.000              | 0.000   | 117.700 | 0.000   |
| 64<br>K C | 0.000              | 0.000   | 130.200 | 0.000   |
| 65        | 123.400            | 177.900 | E24.200 | 229.900 |
| 66        | 121.300            | 165.800 | 614.200 | 223,500 |

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# Tab's A7 (cont'd).

|        |                | 14( + /L/ (evii | · • .            |          |
|--------|----------------|-----------------|------------------|----------|
| 67     | 119 200        | 162 000         | F02 600          | 200 100  |
|        | 118.300        | 162.400         | 593.500          | 200.100  |
| 68     | 128.600        | 174,400         | 634.400          | 222.600  |
| 69     | 99.500         | 120.800         | 344,900          | 166.100  |
| 70     | 101.000        | 113.900         | 366,300          | 164,300  |
| 71     | 99.600         | 113.900         | 349.100          | 164.200  |
| 72     | 103.400        | 121.100         | 357.800          | 160.400  |
| 73     | 86.400         | 102.000         |                  | 134.800  |
|        |                |                 | 326.800          |          |
| 74     | 86.400         | 99.200          | 314,400          | 140.670  |
| 75     | 84.700         | 102.800         | 337.200          | 131.900  |
| 76     | 86.900         | 101.700         | 324.900          | 135,200  |
| 77     | 53.100         | 35.200          | 219.300          | 46.300   |
| 78     | 48.600         | 31.800          | 312.800          | 73.500   |
| 79     | 46.900         | 34.400          |                  |          |
|        | 48.500         |                 | 228.500          | 64.800   |
| 80     | 40.500         | 32.700          | 227.200          | 50.700   |
|        |                |                 |                  |          |
|        |                |                 |                  |          |
| PRIM   | T C30-C33      |                 |                  |          |
| COLUMN | DNT LAB3       | TNT IAP3        | BCX LAB3         | HMX LAB3 |
| COUNT  | 80             | 80              | 80               | 80       |
|        | 00             | 0 <b>V</b>      | αv               | 00       |
| BOW    |                | 20 (00          | 74 4 44          |          |
| 1      | 0.000          | 29.600          | 76.600           | 0.000    |
| 2      | c.000          | 19.200          | 90.300           | 0.000    |
| 3      | 0.000          | 28.000          | 74.200           | 0.000    |
| 4      | 0.000          | 18.200          | 58.100           | 0.000    |
| 5      | 56.000         | 41.900          | 181.500          | 53,100   |
| 6      | 48.400         | 49.100          | 183.600          | 53.200   |
|        |                |                 |                  |          |
| 7      | 50.300         | 81.300          | 160.900          | 58.200   |
| 8      | 52.700         | 67.300          | 169.900          | 51.200   |
| 9      | 107.600        | 124.700         | 278.400          | 128.600  |
| 10     | 97.800         | 131.400         | 247.200          | 140.400  |
| 11     | 81.500         | 120.600         | 278.000          | 154,200  |
| 12     | 74.500         | 87.600          | 237,900          | 104.600  |
|        |                |                 |                  |          |
| 13     | \$3.500        | 123.700         | 310.000          | 153.200  |
| 14     | 102.800        | 146.000         | 301.400          | 120.700  |
| 15     | <b>53.5</b> 00 | 138.300         | 285.700          | 144,600  |
| 16     | 107.900        | 152.900         | 292.900          | 136.700  |
| 17     | 139.600        | 187.200         | 539.900          | 210.600  |
| 18     | 127.900        | 166.800         | 609.700          | 221.900  |
| 19     | 172.400        | 196.800         | 566,400          | 252.100  |
| 20     | 180.300        | 223.800         |                  |          |
|        |                |                 | 586.200          | 205.400  |
| 21     | 0.000          | 0.000           | 0.000            | 0.000    |
| 22     | 0.000          | 0.000           | 0.000            | 0.000    |
| 2.3    | 0.000          | 0.000           | 0.000            | 0.000    |
| 24     | 0.000          | C.COO           | 0.000            | 0.000    |
| 25     | 52.200         | 71,600          | 106,800          | 87.600   |
| 26     | 60.100         | 51.400          | \$8.600          | 97.300   |
| 27     | 53,900         | 38.100          | 87.800           | 56.500   |
| 28     | 62.500         | 34 100          |                  |          |
|        |                | 31.100          | 84.000           | 87.500   |
| 29     | \$8.200        | 103.900         | 230.300          | 191.600  |
| 30     | 107.300        | 117.200         | 2 <b>60.</b> 700 | 200.700  |
| 31     | 88,400         | 117,300         | 276.100          | 221.500  |
| 32     | 68.400         | 153.300         | 213.900          | 196.300  |
| 33     | 105.100        | 153,100         | 318,200          | 275.500  |
| 34     | 1 6. 400       | 124.700         | 277.100          | 300.700  |
| 35     |                |                 |                  |          |
|        | 122.200        | 139.200         | 314,600          | 228.900  |
| 36     | 117.600        | 135.400         | 307.100          | 331.300  |
| 37     | 71.800         | 95.100          | 384.800          | 328.300  |
| 38     | 56.900         | 67.000          | 460.400          | 298.900  |
| 39     | 72.700         | 76.700          | 391.900          | 323.100  |
| 40     | 59.600         | 90.800          | 355.900          | 341.800  |
| 41     | 69.200         | 0.000           | 0.000            | 86.400   |
| 42     |                |                 |                  |          |
|        | 82.300         | 0.000           | 0.000            | 152.000  |
| 43     | 70.400         | 0.000           | 0.000            | 107.300  |
| 44     | 68.900         | C.000           | 0.000            | 111.200  |
| 45     | 165.900        | 74.100          | 377,900          | 434.900  |
| 46     | 137.900        | 72.900          | 363.000          | 381.500  |
|        |                |                 |                  |          |

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Table A7 (cont'd). Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

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| •   | •  | • • •   |   |   |
|---|--|---|---|---|
| . 7   | 154 600  | 00 (00  |   | 1 06 700  |
| 47  | 154,600  | 82.600  | 400.400   | 406.700   |
| 48  | 148.200  | 85.900  | 363.500   | 402.300   |
| 49  | 198.000  | 124.400   | 297.200   | 333.600   |
| 50  | 203.400  | 142.700   | 297.800   | 335.600   |
| 51  | 207.700  | 130.500   | 285.300   | 334.300   |
| 52  | 213.400  | 156.600   | 297.000   | 395.300   |
| 53  | 132.600  | 85.600  | 145.500   | 245.500   |
| 54  | 137.900  | 80.700  | 168.400   | 243.300   |
| 55  | 129.600  | 70,900  | 141.400   | 243.300   |
| 56  | 135.100  | 73.300  | 141.400   | 242.200   |
| 57  | 134.400  | 59.700  | 76.700  | 173.700   |
| 58  | 132.500  | 57.700  | 81.400  | 191.600   |
| 59  | 137.100  | 71.900  | 100.500   | 210.500   |
| 60  | 138.400  | 52.200  | 70.700  | 196.900   |
|   |  | 0.000   | 137.400   | 0.000   |
| 61  | 0.000  |   |   | 0.000   |
| 62  | 0.000  | 0.000   | 129.700   |   |
| 63  | 0.000  | 0.000   | 120.100   | 0.000   |
| 64  | 0.000  | 0.000   | 151.900   | 0.000   |
| 65  | 126.600  | 175.500   | 676.000   | 224.800   |
| 66  | 140.900  | 184.900   | 709.100   | 247.900   |
| 67  | 114.800  | 167.400   | 647.000   | 232.400   |
| 68  | 133.200  | 184.800   | 674.200   | 235.100   |
| 69  | 115.500  | 116.300   | 374.300   | 157.800   |
| 70  | 101.000  | 116,100   | 339.300   | 134.800   |
| 71  | 108.100  | 120.800   | 378.200   | 166.900   |
| 72  | 104.900  | 107.400   | 376.700   | 166.200   |
| 73  | 54.400   | 87.400  | 371.100   | 159.200   |
| 74  | \$4.800  | 115.200   | 356.900   | 155.900   |
| 75  | 79.000   | 121.200   | 336.100   | 213.600   |
|   | 99.000   | 112.100   | 367.500   | 153.300   |
| 76<br>77  |  | 33.000  |   |   |
|   | 55.100   | 33.000  | 223.100   | 46.000  |
|   |  |   | 250 300   | C 0 0 0 0   |
| 78  | 47.600   | 35.500  | 250.700   | 50.000  |
| 78<br>79  | 47.600<br>47.300   | 35.500<br>34.200  | 233.500   | 61.700  |
| 78  | 47.600   | 35.500  |   |   |
| 78<br>79<br>80<br>PRI   | 47.600<br>47.300<br>63.200<br>NT C40-C43   | 35.500<br>34.200<br>25.800  | 233.500<br>260,300  | 61.700<br>40.700  |
| 78<br>79<br>80<br>PRI<br>COLUNN   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4   | 35.500<br>34.200<br>25.800<br>TNT LAB4  | 233.500<br>260.300<br>REX LAB4  | 61.700<br>40.700<br>HNI LAB4  |
| 78<br>79<br>80<br>PRI<br>COLUNN<br>COUNT  | 47.600<br>47.300<br>63.200<br>NT C40-C43   | 35.500<br>34.200<br>25.800  | 233.500<br>260,300  | 61.700<br>40.700  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW  | 47.600<br>47.300<br>63.200<br>VI C40-C43<br>DNI LAB4<br>80   | 35.500<br>34.200<br>25.800<br>TNT LAB4  | 233.500<br>260.300<br>REX LAB4<br>80  | 61.700<br>40.700<br>HMI LAB4<br>80  |
| 78<br>79<br>80<br>PRI<br>COLUNN<br>COUNT<br>ROW<br>1  | 47.600<br>47.300<br>63.200<br>VI C40-C43<br>DNI LAB4<br>80<br>0.000  | 35.500<br>34.200<br>25.800<br>TNT LAB4  | 233.500<br>260.300<br>REX LAB4  | 61.700<br>40.700<br>HNI LAB4  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2  | 47.600<br>47.300<br>63.200<br>VI C40-C43<br>DNI LAB4<br>80   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900  | 61.700<br>40.700<br>HMI LAB4<br>80  |
| 78<br>79<br>80<br>PRI<br>COLUNN<br>COUNT<br>ROW<br>1  | 47.600<br>47.300<br>63.200<br>VI C40-C43<br>DNI LAB4<br>80<br>0.000  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900  | 61.700<br>40.700<br>HNI LAB4<br>80<br>0.000   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4  | 47.600<br>47.300<br>63.200<br>VI C40-C43<br>DNI LAB4<br>80<br>0.000<br>0.000   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000  | 61.700<br>40.700<br>HME LAB4<br>80<br>0.000<br>0.000  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4  | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>36.700<br>35.100<br>34.800<br>29.600<br>69.300  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900  | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4  | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000  | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>36.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000   | 61.700<br>40.700<br>HNI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>48.900  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>36.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>70.500  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700   | 61.700<br>40.700<br>HNI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8  | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>50.700   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700<br>160.900  | 61.700<br>40.700<br>HNI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800   |
| 78<br>79<br>80<br>COLUNY<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9   | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>55.100<br>55.100<br>50.700<br>97.200   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700<br>160.900<br>270.800   | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600  |
| 78<br>79<br>80<br>COLUNN<br>COLUNN<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10  | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>50.700<br>97.200<br>88.500  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>63.900<br>163.000<br>159.300<br>165.700<br>160.900<br>270.800<br>249.100  | 61.700<br>40.700<br>HME LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100   |
| 78<br>79<br>80<br>COLUNY<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11   | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>50.700<br>97.200<br>88.500<br>88.500<br>88.200  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>270.800<br>249.100<br>255.500   | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12   | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>50.700<br>97.200<br>88.500<br>88.500<br>88.200<br>85.200  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>160.900<br>270.800<br>249.100<br>255.500<br>252.300   | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>97.200<br>88.500<br>88.500<br>88.200<br>89.200<br>99.700  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>70.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>160.900<br>270.800<br>249.100<br>255.500<br>255.500<br>252.300<br>282.300   | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200  |
| 78<br>79<br>80<br>COLUNM<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>97.200<br>88.500<br>88.500<br>88.500<br>85.200<br>99.700<br>100.400   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>160.909<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>296.600  | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900   |
| 78<br>79<br>80<br>COLUNM<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15   | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>88.500<br>88.500<br>88.500<br>88.200<br>99.700<br>100.400<br>102.300  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>144.400   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700<br>160.900<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>296.600<br>287.000   | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900  |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16                                     | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>55.200<br>88.500<br>88.200<br>85.200<br>97.700<br>1C0.400<br>1C2.300<br>58.600  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>70.100<br>70.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.200  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700<br>160.900<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>282.300<br>283.500  | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17                               | 47.600<br>47.300<br>63.200<br>NT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>55.200<br>88.500<br>85.200<br>85.200<br>85.200<br>97.700<br>1C0.400<br>1C2.300<br>58.600<br>122.400   | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>70.100<br>70.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.200<br>141.200<br>157.600  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>159.300<br>165.700<br>160.909<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>296.600<br>283.500<br>550.600  | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000  |
| 78<br>79<br>80<br>COLUNY<br>COUNY<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18                         | 47.600<br>47.300<br>63.200<br>WT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>0.000<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>97.200<br>88.500<br>88.500<br>88.200<br>99.700<br>1C2.400<br>122.400<br>128.200  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>70.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.200<br>157.600<br>2C9.400  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>296.600<br>287.000<br>283.500<br>559.300  | 61.700<br>40.700<br>HNI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19                   | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>88.500<br>88.200<br>85.200<br>97.200<br>88.500<br>85.200<br>97.200<br>88.500<br>85.200<br>1C0.400<br>1C2.300<br>58.600<br>122.400<br>128.200<br>127.700 | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>144.400<br>141.200<br>157.600<br>2C9.400<br>2C1.700   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>163.000<br>165.700<br>165.700<br>165.700<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>296.600<br>283.500<br>550.600<br>559.300<br>544.000  | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>147.800<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100        |
| 78<br>79<br>80<br>COLUNY<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20             | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>88.500<br>88.200<br>85.200<br>97.200<br>88.500<br>85.200<br>97.200<br>88.500<br>85.200<br>122.400<br>128.200<br>127.700<br>122.400            | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>144.400<br>141.200<br>157.600<br>2C9.400<br>2C1.700<br>206.600  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>287.000<br>283.500<br>550.600<br>559.300<br>542.200   | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100<br>226.600                   |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20<br>21       | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.200<br>88.500<br>88.200<br>85.200<br>99.700<br>1C0.400<br>1C2.300<br>58.600<br>122.400<br>127.700<br>122.400<br>0.000  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>141.200<br>157.600<br>2C9.400<br>2C1.700<br>206.600<br>C.000  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>282.300<br>296.600<br>283.500<br>550.600<br>559.300<br>544.000<br>542.200<br>0.000                                | 61.700<br>40.700<br>HMX LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100<br>226.600<br>0.900          |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20<br>21<br>22 | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.100<br>88.500<br>88.200<br>85.200<br>97.200<br>88.500<br>85.200<br>97.200<br>88.500<br>85.200<br>122.400<br>128.200<br>127.700<br>122.400            | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>144.400<br>141.200<br>157.600<br>2C9.400<br>2C1.700<br>206.600  | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>270.800<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>287.000<br>283.500<br>550.600<br>559.300<br>542.200   | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100<br>226.600<br>0.900<br>0.000 |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20<br>21       | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.200<br>88.500<br>88.200<br>85.200<br>99.700<br>1C0.400<br>1C2.300<br>58.600<br>122.400<br>127.700<br>122.400<br>0.000  | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>129.600<br>129.600<br>129.600<br>129.600<br>129.600<br>135.300<br>141.000<br>141.200<br>157.600<br>2C9.400<br>2C1.700<br>206.600<br>C.000<br>C.000<br>C.000 | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>282.300<br>296.600<br>283.500<br>550.600<br>559.300<br>544.000<br>542.200<br>0.000                                | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100<br>226.600<br>0.000<br>0.000 |
| 78<br>79<br>80<br>COLUNN<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20<br>21<br>22 | 47.600<br>47.300<br>63.200<br>VT C40-C43<br>DNT LAB4<br>80<br>0.000<br>0.000<br>0.000<br>56.000<br>39.200<br>55.100<br>55.100<br>55.100<br>55.100<br>55.200<br>88.500<br>88.200<br>85.200<br>99.700<br>1C0.400<br>1C2.300<br>58.600<br>122.400<br>127.700<br>122.400<br>0.000                                | 35.500<br>34.200<br>25.800<br>TNT LAB4<br>80<br>3C.700<br>35.100<br>34.800<br>29.600<br>69.300<br>70.100<br>7C.500<br>71.700<br>14C.400<br>129.600<br>120.000<br>135.300<br>141.000<br>141.300<br>141.200<br>157.600<br>2C9.400<br>2C1.700<br>206.600<br>C.000<br>0.000   | 233.500<br>260.300<br>REX LAB4<br>80<br>56.900<br>55.900<br>63.900<br>61.000<br>163.000<br>165.700<br>165.700<br>165.700<br>165.700<br>249.100<br>255.500<br>252.300<br>282.300<br>282.300<br>296.600<br>287.000<br>283.500<br>550.600<br>559.300<br>550.600<br>559.300<br>544.000<br>542.200<br>0.000<br>0.000 | 61.700<br>40.700<br>HMI LAB4<br>80<br>0.000<br>0.000<br>0.000<br>48.900<br>53.000<br>34.000<br>51.800<br>140.600<br>131.100<br>147.800<br>124.100<br>136.200<br>142.900<br>139.900<br>143.600<br>228.000<br>227.100<br>220.100<br>226.600<br>0.900<br>0.000 |

# Table A7 (cont'd).

| 25     | 63.500      | 49.100   | 77.300   | 69.700   |
|--------|-------------|----------|----------|----------|
| 26     | 64,900      | 52.400   | 71.000   | 63.400   |
|        |             |          |          |          |
| 27     | 56.500      | 48.600   | 72.200   | 61.900   |
| 28     | 57.200      | 51.100   | 77.100   | 71.100   |
| 29     | 110.000     | 136.800  | 242.700  | 214.800  |
| 30     | 110.900     | 133.100  | 245.000  | 226.600  |
| 31     |             | 133.500  | 246.400  | 211.100  |
|        | 112.100     |          |          | 211.100  |
| 32     | 91.200      | 139.700  | 232.300  | 217.800  |
| 33     | 130.600     | 147.200  | 283.500  | 248.900  |
| 34     | 125.700     | 136.800  | 263.000  | 247.700  |
| 35     | 132,200     | 150.100  | 274.300  | 244.300  |
| 36     | 127.300     | 150.700  | 272.100  | 232.400  |
|        |             |          | 375.600  | 325.200  |
| 37     | 84.800      | 81.900   |          | -        |
| 38     | 76.800      | 90.200   | 396.100  | 344.300  |
| 39     | 76.200      | 90.100   | 391.300  | 323.200  |
| 40     | 60.800      | £7.200   | 370.700  | 324.000  |
| 41     | 80.000      | 0.000    | 0.000    | 125.900  |
| 42     | 72.900      | 0.000    | 0.000    | 128.900  |
|        |             |          |          |          |
| 43     | 70.600      | 0.000    | 0.000    | 127.700  |
| 44     | 74.600      | C.COO    | 0.000    | 127.700  |
| 45     | 148.800     | 88.400   | 378.100  | 460.400  |
| 46     | 150.500     | 85.300   | 368.400  | 460.900  |
| 47     | 151.800     | 87.400   | 374.700  | 459.500  |
|        |             |          |          |          |
| 48     | 149.900     | 73.400   | 373.100  | 469.300  |
| 49     | 201.600     | 152.400  | 277.500  | 367.900  |
| 50     | 199.800     | 153.800  | 275.900  | 375.900  |
| 51     | 197.800     | 154.500  | 275.000  | 367.900  |
| 52     | 203.200     | 159.200  | 285.800  | 368.200  |
| 53     | 180.200     | 135.900  | 253.000  | 347.600  |
| 54     | 187.300     | 137.300  | 250.900  | 347.000  |
| 55     | 181.400     | 135.000  | 252.000  | 343.900  |
|        |             |          |          |          |
| 56     | 186.400     | 135.800  | 251.300  | 339.600  |
| 57     | 134,400     | 52.600   | 81.400   | 199.200  |
| 58     | 134.200     | 45.700   | 83.000   | 189.500  |
| 59     | 130.200     | 43.600   | 91.200   | 197.000  |
| 60     | 136.500     | 49.200   | 88.100   | 191.400  |
| 61     | 0.000       | 0.000    | 112.600  | 0.000    |
|        |             |          |          |          |
| 62     | C.000       | 0.000    | 121.000  | 0.000    |
| 63     | 0.000       | 0.000    | 125.000  | 0.000    |
| 64     | 0.000       | C-000    | 120.600  | 0.000    |
| 65     | 136.100     | 178.700  | 611.000  | 225.300  |
| 66     | 123.300     | 167.100  | 608.900  | 221.600  |
| 67     | 94.100      | 166.700  | 612.800  | 218.900  |
| 68     | 125.500     | 165.400  | 605.000  | 220.800  |
|        |             |          | 347.200  | 151.800  |
| 69     | 105,700     | 103.900  |          |          |
| 70     | 106.800     | 108.400  | 348.200  | 154.300  |
| 71     | 103.300     | 114.400  | 346.800  | 146.100  |
| 72     | 97.900      | 126.000  | 357.200  | 151.300  |
| 73     | 88,700      | 107.500  | 315.700  | 145.700  |
| 74     | 88.900      | 104.900  | 319.200  | 147.300  |
| 75     | 86.600      |          | 314.900  | 145.000  |
|        |             | 109.600  |          |          |
| 76     | 94.000      | 106.800  | 313.800  | 132.000  |
| 77     | 47.000      | 38.400   | 223.200  | 52.500   |
| 78     | 51.500      | 38.500   | 226.100  | 71.400   |
| 79     | 58.300      | 39.000   | 227.400  | 39.200   |
| 80     | 49.500      | 34.000   | 224.600  | 56.400   |
|        | 42          |          |          |          |
|        |             |          |          |          |
|        |             |          |          |          |
|        | INT C50-C53 |          |          | awy time |
| COLUNY |             | THT LAES | REX LABS | SHX LABS |
| COUNT  | 90          | 80       | 80       | 80       |
| ROW    |             |          |          |          |
| 1      | 0.000       | 30.700   | 111.800  | 0.000    |
| 2      | 0.000       | 80.400   | 89.800   | 0.000    |
| 3      | 0.000       | 40.300   | 226.900  | 0.000    |
| ũ      | 0.000       | 35.900   | 93.800   | 0.000    |
|        |             |          | 2.24 000 | 31000    |

| repo     | rted by laboratories | participating in ( | collaborative test | of HPLC method     |
|----------|----------------------|--------------------|--------------------|--------------------|
| 5        | 66.800               | 64.800             | 331.100            | 36.300             |
| 6        | 71.800               | 84.200             | 412.600            | 86.300             |
| 7        | 42.900               | 89.900             | 288.200            | 49.200             |
| 8        | 66.500               | 83.400             | 278.500            | 17.800             |
| 9        | 82.200               | 135.700            | 196.100            | 144.000            |
| 10       | 65.500               | 114.000            | 247.000            | 143,300            |
| 11       | 76.300               | 153.300            | 240.500            | 147.200            |
| 12       | \$7.600              | 129.500            | 339.200            | 127.800            |
| 13       | 110.300              | 118.400            | 343.500            | 95.700             |
| 14       | 95.600               | 164.700            | 402.800            | 132.800            |
| 15       | 82.500               | 162.100            | 318.400            | 164.500            |
| 16       | 92.000               | 133.100            | 289.800            | 167.000            |
| 17       | 127.700              | 212.100            | 692.800            | 219.900            |
| 18       | 110,400              | 186.000            | 647.600            | 238.100            |
| 19       | 139.700              | 166.400            | 683.200            | 131.200            |
| 20       | 143.400              | 230.200            | 572.800            | 209.200            |
| 21       | 0.000                | 6.000              | 0.000              | 0.000              |
| 22       | C.000                | 0.000              | 0.000              | 0.000              |
| 23       | 0.000                | 0.000              | 0.000              | 0.000              |
| 24       | 2,000                | 0.000              | 0.000              | 0.000              |
| 25       | , )00                | 46.900             | 160.100            | 112.000            |
| 26       | 100                  | 83.600             | 200.100            | 79.700             |
| 27       | 70.400               | 72.800             | 125.100            | 89.700             |
| 28       | 75.200               | 83.300             | 197.100            | 98.700             |
| 29       | 65.200               | 144.500            | 258.100            | 267.700            |
| 30       | 126.600              | 165.900            | 268.800            | 220.500            |
| 31       | 122.700              | 149.600            | 304.600            | 222.600            |
| 32<br>33 | 10C.700<br>113.800   | 139.100<br>137.800 | 317.200            | 290.300            |
| 34       |                      |                    | 262.700<br>311.900 | 244.500            |
| 35       | 115.700<br>128.000   | 155.200<br>150.900 | 433.300            | 284.900<br>228.300 |
| 36       | 121.500              | 163.000            | 336.700            | 253.100            |
| 37       | 87.490               | 93.800             | 458.900            | 340.000            |
| 38       | 71.200               | 86.400             | 387.900            | 401.700            |
| 39       | 75.600               | 101.900            | 448.100            | 338.000            |
| 40       | 74.500               | 114, 100           | 424.900            | 352.800            |
| 41       | 93.500               | C.000              | 0.000              | 144.000            |
| 42       | 75.300               | 0.000`             | 0.000              | 250.500            |
| 43       | 77.500               | 0.000              | 0.000              | 188.400            |
| 44       | 78.900               | 0.000              | 0.000              | 63,100             |
| 45       | 167.100              | 136.400            | 389.000            | 404.100            |
| 46       | 174.400              | 68.600             | 399.500            | 440.200            |
| 47       | 167.100              | 79.600             | 433.000            | 419.900            |
| 48       | 134.900              | 109.800            | 651.600            | 441.200            |
| 49       | 197.400              | 145.700            | 222.000            | 382.700            |
| 50       | 189,800              | -54.000            | <b>427.90</b> 0    | 333.500            |
| 51       | 198.500              | 142.000            | 378.900            | 326.500            |
| 52       | 208.400              | 145.200            | 356.000            | 385.200            |
| 53       | 184.400              | 152.800            | 270.400            | 288.900            |
| 54       | 185.900              | 136.500            | 318.500            | 339.200            |
| 55       | 212.000              | 157. 20            | 273.900            | 297.300            |
| 56       | 185.000              | 14                 | 260.900            | 357.400            |
| 57       | 1 19. 100            | 57 300             | 228.900            | 226.200            |
| 58       | 141.900              | 61.500             | 97.000             | 220.700            |
| 59<br>60 | 126.300              | 39.500             | 118.800            | 349.800            |
|          | 139.700              | 45.900             | 109.200            | 203.100            |
| 61<br>62 | 0.000<br>0.000       | C.000              | 219.400            | 0.000              |
| 62<br>63 | 0.000                | 0.000<br>0.000     | 175.800<br>297.700 | 6.000              |
| 63<br>64 | 0.000                | 0.000              | 147.400            | 0.000<br>0.000     |
| 65       | 107.900              | 172.000            | 581.000            | 194.400            |
| 66       | 107.900              | 164.100            | 704.300            | 275.800            |
|          |                      |                    | 1041340            | # 7 J 8 U V V      |

Table A7 (cont'd) Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

# Table A7 (cont'd).

| 67<br>68<br>69<br>70<br>71<br>72<br>73<br>74<br>75<br>76<br>77<br>80 | 140,400<br>119,100<br>97,100<br>93,000<br>101,300<br>105,300<br>79,400<br>78,600<br>88,400<br>125,500<br>55,700<br>73,200<br>38,200<br>44,800 | 167.800 $155.700$ $130.800$ $116.700$ $126.000$ $128.400$ $109.400$ $114.700$ $127.200$ $134.700$ $48.700$ $45.300$ $39.900$ $35.300$ | 681.700<br>607.600<br>393.000<br>432.800<br>350.400<br>429.700<br>287.100<br>438.400<br>444.700<br>373.100<br>270.400<br>263.800<br>413.100<br>266.900 | 257.700<br>209.800<br>181.900<br>142.400<br>114.100<br>138.400<br>174.900<br>120.000<br>140.800<br>75.100<br>78.900<br>77.800<br>94.400 |
|--|---|---|--|---|
| PRI  |   |   |  |   |
| COLUMN   | DNT LAB6<br>80  | TNT LAE6<br>80  | RII LAB6<br>80   | ANI LAB6<br>80  |
| BOW  | 00  |   | 0 <b>v</b>   | 80  |
| 1  | 0.000   | 0.000   | 92.200   | 0.000   |
| 2<br>3   | 0.000<br>0.000  | 0.000   | 143.100  | 0.000   |
| 4  | 0.000   | 0.000<br>0.000  | 79.000<br>126.400  | 0.000<br>0.000  |
| 5  | 45.200  | 29.700  | 211.200  | 79.200  |
| 6<br>7   | 48.900  | 35.600  | 225.500  | 68.600  |
| 8  | 38.500<br>52.500  | 30.200<br>37.500  | 161.800<br>18 <u>8</u> .400  | 62.200<br>83.200  |
| 9  | 92.100  | 117.800   | 340.400  | 174.000   |
| 10   | 99.600  | 110.000   | 333.500  | 166.800   |
| 11<br>12   | 108.000<br>52.500   | 159.300<br>1C5.200  | 339.300  | 181.500   |
| 13   | 101.800   | 119.300   | 300.700<br>301.700   | 158.400<br>163.600  |
| 14   | 102.200   | 122.200   | 337.700  | 157.200   |
| 15   | 117.200   | 134.300   | 330.200  | 170.600   |
| 16<br>17   | 114.400<br>136.200  | 118.800<br>185.000  | 340.500<br>584.800   | 178.400   |
| 18   | 132.500   | 179.400   | 533.300  | 219.600<br>217.000  |
| 19   | 136.600   | 181.200   | 614.400  | 226,600   |
| 20<br>21   | 127.700   | 172.200   | 537.200  | 203.700   |
| 22   | 0.000   | 0.000<br>C.000  | 0.000<br>0.000   | 0.000<br>0.000  |
| 23   | 0.000   | 0.000   | 0.000  | 0.000   |
| 24   | 0.000   | 0.000   | 67.200   | 0.000   |
| 25<br>26   | 55.100<br>66.800  | 46.500<br>44.900  | 271.500<br>269.100   | 182.800   |
| 27   | 54.000  | 52.600  | 81.400   | 192.800<br>135.700  |
| 28   | 59.000  | £4.100  | 95.200   | 136.700   |
| 29<br>30   | 114.000<br>105.300  | 133.000   | 441.900  | 410.600   |
| 31   | 112.000   | 142.400<br>139.700  | 453.300<br>276.300   | 6C2.200<br>543.200  |
| 32   | 107.900   | 122.100   | 272.500  | 592.700   |
| 33   | 121.800   | 151.200   | 691.900  | 569.200   |
| 34<br>35   | 121.600<br>122.000  | 158.200<br>148.700  | 659.100  | 556.300   |
| 36   | 130.900   | 146.700   | 350.400<br>340.000   | 49 <b>3.6</b> 00<br>492 <b>.</b> 300  |
| 37   | 68.400  | e5.300  | 538.900  | 478.400   |
| 38<br>39   | 69.300  | 75.900  | 527.600  | 474.400   |
| 40   | 66.600<br>75.800  | 77.200<br>66.60 <b>0</b>  | 632.900<br>651.600   | 512.900<br>502.600  |
| 41   | 62.100  | 0.000   | 0.000  | 148.400   |

| reported | i vy lavoratories p | a deipatuig ni co  |                    |                    |
|----------|---------------------|--------------------|--------------------|--------------------|
| 42       | 73,700              | C.000              | 0.000              | 107.400            |
| 43       | 72.400              | 0.000              | 0.000              | 107.400            |
| 44       | 62.100              | 0.000              | 0.000              | 90.100             |
| 45       | 135.600             | 57.600             | 317.100            | 445.100            |
| 46       | 143.500             | 66.700             | 345.900            | 403.700            |
| 47       | 146.800             | 77.200             | 342.700            | 470.400            |
| 48       | 148.100             | 68.200             | 342.000            | 523.500            |
| 49       | 200.900             | 137.000            | 242.700            | 4CB.200            |
| 50       | 194,000             | 126.100            | 249.600            | 334.600            |
| 51       | 193.300             | 147.900            | 259.200            | 4 CS . 7 0 0       |
| 52       | 189.100             | 130.400            | 253.900            | 430.900            |
| 53       | 180.000             | 117.200            | 240.600            | 325.000            |
| 54       | 171.900             | 114.800            | 225.400            | 388,600            |
| 55       | 184.300             | 123.200            | 236.900            | 335.100            |
| 56       | 175.200             | 133.400            | 238,500            | 453.100            |
| 57       | 122.500             | 39.100             | 76.200             | 273.200            |
| 58       | 136.600             | 42.500             | 59.000             | 232.700            |
| 59       | 123.700             | 42.500             | 68.900             | 166.000            |
| 60       | 126.400             | 54.400             | 73.900             | 179.200            |
| 61       | 0.000               | C.C00              | 100.700            | 0.000              |
| 62       | C.000               | 0.000              | 95.700             | 0.000              |
| 63       | 0.000               | 0.000              | 97.400             | 0.000              |
| 64       | 0.000               | 0.000              | 92.000             | 0.000              |
| 65       | 120.400             | 160.600            | 553.900            | 194.300            |
| 66       | 121.600             | 167.000            | 543.100            | 186,900            |
| 67       | 122.100             | 160.500            | 574.400            | 201.000            |
| 68<br>69 | 719.100<br>101.700  | 156.300<br>166.700 | 544.200<br>320.600 | 185,200<br>130,400 |
| 70       | 105.200             | 106.200            | 287.700            | 128.               |
| 71       | 102.100             | 116.200            | 297.600            | 140.5              |
| 72       | 87.500              | 119.100            | 295.100            | 144 3              |
| 73       | 83.400              | 86.000             | 253.600            | 92 321             |
| 74       | 85.230              | 97,400             | 278.600            | •                  |
| 75       | 85.900              | 93.900             | 273.400            | 1                  |
| 76       | 84.500              | 91,500             | 282.200            | · ·                |
| 77       | 46.200              | 22.900             | 183.000            | J00                |
| 78       | 48.800              | 26.600             | 196.600            | 0.000              |
| 79       | 46.700              | 31.800             | 187.600            | 0.000              |
| 80       | 52.800              | 27.600             | 188.100            | 0.000              |
|          |                     |                    |                    |                    |
| 081      | INT C70-C73         |                    |                    |                    |
|          | DNT LAB7            | TNI LAB7           | RDX LAB7           | HMX LAB7           |
| COUNT    | 80                  | 80                 | 80                 | 80                 |
| ROW      |                     |                    |                    |                    |
| 1        | 0.000               | 53.900             | 55.200             | 0.000              |
| 2        | 0.000               | 40.400             | 61.500             | 0.000              |
| 3        | 0.000               | 32.400             | 69.200             | 0.000              |
| 4        | 0.000               | 49.200             | 67.500             | 0.000              |
| 5        | 66.800              | 93.800             | 288.900            | 0.000              |
| 6        | 84.000              | 102.200            | 463.300            | 0.000              |
| 7        | 39.200              | 86.700             | 154.000            | 137.700            |
| 8        | 72.800              | 91.600             | 155.800            | 0.000              |
| 9        | 99.100              | 167.600            | 248.100            | 370.300            |
| 10***    | 104.000             | 164,900            | 262.700            | 392.800            |
| 12       | 111.600             | 176.100            | 498.700            | 272.300            |
| 13       | 126.900             | 187.500            | 267.900            | 419.200            |
| 14       | 128.500             | 175.800            | 280.000            | 371.100            |
| 15       | 123.500             | 186.300            | 704.700            | 325,700            |
| 16       | 119.400             | 189.600            | 278.700            | 388.400            |
| 17       | 153.200             | 252.100            | £35.400            | 336.400            |
| 18       | 157.900             | 283.200            | 554.800            | 452.100            |
| 19       | 149.400             | 261.600            | 554.700            | 453.900            |
|          |                     |                    |                    |                    |

Table A7 (cont'd). Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

### Table A7 (cont'd).

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|          |                  | Table A/ (con    | (u).               |                  |
|----------|------------------|------------------|--------------------|------------------|
| 20       | 158.300          | 254.700          | 551.300            | 434.000          |
| 21       | 0.000            | 0.000            | 0.000              | 0.000            |
| 22       | 0.000            | 0.000            | 0.000              | 0.000            |
| 23       | 0.000            | 0.000            | 0.000              | 0.000            |
| 24       | 0.000            | 0.000            | 0.000              | 0.000            |
| 25       | 73.100           | 63.100           | 88.700             | 80.100           |
| 26       | 72,300           | 61.900           | 94.100             | 96.800           |
| 27       | 66.500           | 61.500           | 102.000            | 94.700           |
| 28       | 74.600           | 63.700           | 83.200             | 85.400           |
| 29       | 137.800          | 171.900          | 237.100            | 158.500          |
| 30       | 138.800          | 168.100          | 263.500            | 201.700          |
| 31       | 132.000          | 165.300          | 279.000            | 245.200          |
| 32       | 139.200          | 172.400          | 267.500            | 248.000          |
| 33       | 141.000          | 172.700          | 271.500            | 229.300          |
| 34       | 160.200          | 190.900          | 294.100            | 265,900          |
| 35       | 159.900          | 196.000          | 297.700            | 255.200          |
| 36       | 154.000          | 189.400          | 292.500            | 282.300          |
| 37       | 104.800          | 111.600          | 428.100            | 382.300          |
| 38       | 97.400           | 112.900          | 415.700            | 401.300          |
| 39       | 88.600           | 100.100          | 396.900            | 374.500          |
| 40       | 94,900           | 113.100          | 378.700            | 352.300          |
| 41       | 77.100           | C.000            | 0.000              | 230.900          |
| 42       | 73.500           | 0.000            | 0.000              | 307.200          |
| 43       | 71.200           | 0.000            | 0.000              | 304.100          |
| 44       | 76.400           | 0.000            | 0.000              | 309.200          |
| 45       | 167.500          | 108.400          | 360.200            | 661.700          |
| 46       | 170.700          | 102.400          | 379.700            | 664.400          |
| 47       | 169.800          | 129.100          | 376.700            | 645.300          |
| 48       | 160.800          | 101.900          | 373.100            | 654,000          |
| 49       | 231.300          | 200.000          | 258.500            | 596.200          |
| 50       | 235,500          | 196.300          | 281.600            | 590,300          |
| 51       | 231.400          | 190.900          | 275.900            | 577.600          |
| 52       | 228.100          | 190.600          | 282.000            | 572.900          |
| 53       | 215.900          | 171.900          | 258.600            | 555.900          |
| 54       | 216.600          | 172.300          | 258.300            | 588.000          |
| 55       | 224.800          | 174.100          | 236.100            | 547.300          |
| 56       | 214.200          | 176,700          | 242.100            | 536,300          |
| 57       | 157.100          | 64.400           | 76.600             | 386.400          |
| 58       | 161.200          | 67.200           | 74.900             | 373.100          |
| 59       | 115.300          | 70.200           | 67.700             | 379.100          |
| 60       | 162.900          | 64.500           | 71.900             | 370,100          |
| 61       | 0.000            | 0.000            | 126.500            | 0.000            |
| 62       | 0.000            | 0.000            | 129,300            | 0.000            |
| 63       | 0.000            | 0.000            | 120.400            | 0.000            |
| 64       | 0.000            | 0.000            | 114.400            | 0.000            |
| 65       | 212.400          | 251.100          | 611.500            | 192.300          |
| 66       | 172.400          | 246.300          | 856,900            | 451,800          |
| 67       | 156.100          | 219.200          | 720.800            | 432.300          |
| 68       | 160.000          | 225.500          | 623.400            | 241.500          |
| 69       | 123.800          | 148.300          | 329.400            | 145.700          |
| 70       | 134.500          | 152,500          | 590.100            | 400.000          |
| 71       | 126.900          | 144.000          | 332.600            | 157_000          |
| 72       | 122.800          | 146.000          | 333,700            | 154.000          |
| 73       | 114.000          | 133.600          | 574.900            | 381.700          |
| 74       | 106.800          | 135,500          | 328.400            | 133.000          |
| 75       | 100.200          | 136.700          | 330.900            | 135.200          |
| 76       | 97.500           | 121.600          | 320,800            | 145.300          |
| 77       | 69.700<br>60.100 | 46.400           | 216.500<br>216.000 | 53.300<br>54.700 |
| 78<br>79 | 64.100           | 48.900<br>43.200 | 225.600            | 56.200           |
| 80       | 36.400<br>56.100 | 44.900           | 208.100            | 110.900          |
| 90       | 30.100           | 440700           | 200.100            | 114.700          |

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fable A7 (cont'd). Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

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| DB       | INT C80-C83        |                    |                    |                             |
|----------|--------------------|--------------------|--------------------|-----------------------------|
| COLUM    |                    | THT LAE8           | RCK LAB8           | HNX LABS                    |
| COUNT    | 60                 | 90                 | 80                 | 80                          |
| ROW      | 77                 | 12 700             | 70 000             |                             |
| 1<br>2   | 77.100<br>C.000    | 17.700<br>157.100  | 72.800<br>0.000    | 0.000<br>0.000              |
| 3        | 0.000              | 56.200             | 0.000              | 0.000                       |
| ų        | 0.000              | 0.000              | 0.000              | 0.000                       |
| 5        | \$8.300            | 39.300             | 83.800             | 0.000                       |
| 6        | 49.000             | \$7.200            | 140.400            | 33.800                      |
| 7        | 65.300             | 91.400             | 140.600            | 205.800                     |
| 8<br>9   | 31.100<br>113.900  | 44.100<br>185.500  | 115.800<br>286.300 | 0.000<br>146.100            |
| 10       | 55.800             | 73.800             | 270.100            | 55.300                      |
| 11       | 59.200             | 90.400             | 206.000            | 75.300                      |
| 12       | 65.000             | 113.500            | 191.700            | 41.300                      |
| 13       | 61.200             | 152.400            | 263.800            | 110.600                     |
| 14       | 84.300             | 137.700            | 270.600            | 152.500                     |
| 15<br>16 | 77.400<br>84.500   | 184.900<br>88.100  | 258.900<br>321.100 | 81.700<br>258.400           |
| 17       | 165.800            | 158.500            | 604.200            | 517.800                     |
| 18       | 113.100            | 222.100            | 549.900            | 176.800                     |
| 19       | 141.800            | 202.700            | 640.100            | 251.500                     |
| 20       | 103.100            | 167.600            | 491.400            | 178.600                     |
| 21       | 0.000              | 0.000              | 0.000              | 0.000                       |
| 22<br>23 | 0.000              | C.000<br>0.000     | 0.000<br>0.000     | 0.000                       |
| 24       | 0.000              | 0.000              | 0.000              | 82.700                      |
| 25       | 61.600             | 47,100             | 49.300             | 0.000                       |
| 26       | 87.700             | 20.700             | 204.400            | 96.200                      |
| 27       | 53.500             | 49.700             | 50.400             | 123.700                     |
| 28<br>29 | 59.200<br>82.700   | 34.300<br>139,100  | 81.600<br>351,900  | 153.800<br>181.200          |
| 30       | 94.800             | 156.900            | 243-800            | 153.800                     |
| 31       | 87.600             | 113.800            | 364.200            | 241.500                     |
| 32       | 124.400            | 109.000            | 221.000            | 123.700                     |
| 32       | 138.400            | 197.800            | 307.200            | 229.800                     |
| 34       | 99.800             | 110.300            | 346.000            | 168.700                     |
| 35<br>36 | 106,400<br>139.700 | 146.600<br>113.300 | 253.000<br>290.900 | 330.500<br>241.100          |
| 37       | 49.900             | 64.900             | 404.600            | 421.700                     |
| 38       | 111.100            | 104.000            | 319.100            | 320.800                     |
| 39       | 46.100             | 63.300             | 358.700            | 279.700                     |
| 40       | 89.600             | 203.700            | 368.300            | 276.700                     |
| 41<br>42 | 89.100<br>57.100   | C.000<br>12.600    | 0.000<br>0.000     | 174.400<br>98.400           |
| 43       | 34.000             | 0.000              | 0.000              | 101.100                     |
| 44       | 58.800             | 0.000              | 0.000              | 81.700                      |
| 45       | 169.300            | 91.300             | 353.200            | 475.900                     |
| 46       | 147.900            | 32.600             | 336.100            | 377.900                     |
| 47<br>48 | 127.900<br>114.200 | 66.100<br>20.900   | 386.500<br>554.500 | 4 <b>44.6</b> 00<br>365.700 |
| 49       | 181.700            | 113.000            | 337.600            | 302.400                     |
| 50       | 183.600            | 130.400            | 233.700            | 304.300                     |
| 51       | 192.700            | 152.600            | 310.000            | 350.100                     |
| 52       | 222.500            | 175.000            | 298.700            | 303,400                     |
| 53<br>54 | 158.400<br>164.600 | 125.500<br>96.400  | 230.300<br>256.400 | 306.900<br>252.100          |
| 54<br>55 | 192.700            | 122.300            | 199.100            | 369.200                     |
| 56       | 173,500            | 116,500            | 183.700            | 276.600                     |
| 57       | 142.200            | 63.800             | 148.300            | 195.600                     |
| 58       | 131.700            | 63.200             | 36.700             | 118.400                     |
| 59       | 95.300             | 51.000             | 57.100             | 109.600                     |
| 60       | 80.100             | 132.200            | 35,600             | 174.200                     |

Table A7 (cont'd).

|          |                    | Table A/ (co       | ni uj.             |                    |
|----------|--------------------|--------------------|--------------------|--------------------|
| 61       | 0.000              | 0.000              | 118.500            | 0.000              |
| 62       | 0.000              | 0.000              | 127.300            | 0,000              |
| 63       | 0.000              | 0.000              | 238.000            | 0.000              |
| 64       | 0.000              | 0.000              | 148.300            | 0.000              |
| 65       | 152.400            | 125.200            | 720.300            | 318.700            |
| 66       | 105,100            | 97.500             | 710,900            | 268.400            |
| 67       | 89.600             | 101.500            | 611.600            | 204.500            |
| 68       | 129,100            | 113.900            | 581,300            | 313.600            |
| 69       | 81.500             | 86.600             | 287.400            | 122.800            |
| 70       | 84.200             | 106.400            | 297.600            | 176.200            |
| 71       | 116.800            | 106.100            | 310.200            | 154.700            |
| 72       | 85,500             | 99.800             | 277.500            | 232.500            |
| 73       | 71.300             | E4.900             | 349.000            | 82.800             |
| 74       | 48.500             | 62.300             | 319.800            | 171.600            |
| 75       | 143.800            | 119.400            | 391.800            | 131.800            |
| 76       | 55.800             | 89.000             | 281.900            | 89.300             |
| 77<br>78 | 53.300             | 37.800<br>22.900   | 216.900<br>167.800 | 0.000              |
| 79       | 19.900             | 36.700             | 244.100            | 0.000              |
| 80       | 17.700             | 58.800             | 181.500            | 222.900<br>134.800 |
| 00       | 17.700             | 301000             | 101.300            | 134.000            |
|          |                    |                    |                    |                    |
| PRI      | NT C90-C93         |                    |                    |                    |
| COLUMN   |                    | THT LAR9           | REI LAB9           | HEX LAB9           |
| COUNT    | 80                 | 80                 | 80                 | 80                 |
| ROW      |                    |                    |                    |                    |
| 1        | J.000              | 16.400             | 57.400             | 0.000              |
| 2        | 0.000              | 16.400             | 58.900             | 0.000              |
| 3<br>4   | 0.000              | 17.300             | 58.900             | 0.000              |
| 5        | 0.000<br>49.800    | 16.400<br>49,100   | 57.400<br>157.400  | 0,000              |
| 6        | 51.300             | 45.100             | 154.500            | 41.500<br>45.100   |
| 7        | 49.000             | 49.100             | 156.000            | 45.100             |
| 8        | 49.800             | 50.000             | 154.500            | 45.100             |
| 9        | 86,600             | 114.500            | 254.600            | 135.400            |
| 10       | 87.300             | 115.500            | 256.000            | 131.800            |
| 11       | 88.100             | 117.400            | 254,600            | 133.600            |
| 12       | 87.300             | 115.500            | 257.500            | 130.000            |
| 13       | 58.800             | 127.000            | 278.100            | 148.100            |
| 14       | 98.170             | 128.000            | 279.600            | 142.700            |
| 15       | 100.400            | 129.000            | 278.100            | 142.700            |
| 16       | 58.800             | 129.000            | 278.100            | 144.500            |
| 17<br>18 | 124.100<br>124.100 | 181.900<br>180.900 | 548.900<br>550.300 | 222.100<br>220.300 |
| 19       | 124.900            | 182.900            | 550.300            | 220.300            |
| 20       | 125.600            | 181.900            | 548.900            | 222.100            |
| 21       | 0.000              | 0.000              | 0.000              | 0.000              |
| 22       | 0.000              | 0.000              | 0.000              | 0.000              |
| 23       | 0.000              | 0.000              | 0.000              | 0.000              |
| 24       | C.000              | 0.000              | 0.000              | 0.000              |
| 25       | 60.400             | 49.600             | 75.600             | 66.200             |
| 26       | 61.200             | 50.600             | 75.600             | 66.200             |
| 27       | 61.200             | 52.500             | 74.100             | 64.300             |
| 28       | 61.900             | 51.600             | 75.600             | 66.200             |
| 29<br>30 | 114.600<br>111.500 | 136.200<br>133.300 | 250.400<br>246.000 | 220.500            |
| 31       | 117.700            | 139.100            | 256.400            | 216,800<br>226,000 |
| 32       | 115.300            | 136.200            | 249.000            | 218.700            |
| 33       | 125.400            | 150.800            | 271.200            | 238.900            |
| 34       | 126.200            | 149.800            | 266.700            | 238.900            |
| 35       | 124.600            | 149.800            | 268.200            | 238.900            |
| 36       | 127.000            | 151.800            | 272.700            | 240.700            |
| 37       | 75.900             | 84.600             | 370.500            | 325.200            |
| 38       | 75.100             | 82.700             | 367.500            | 323.400            |
| 39       | 77.400             | 84.600             | 379.400            | 332.600            |
| 40       | 75.900             | 83.700             | 369.000            | 323.400            |

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Table A7 (cont'd) Concentrations of DNT, TNT, RDX, and HMX ( $\mu$ g/L) reported by laboratories participating in collaborative test of HPLC method.

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| 41 | 71.600  | C.000   | 0.000   | 125.500 |
|----|---------|---------|---------|---------|
| 42 | 72.300  | 0.000   | 0.000   | 130.800 |
| 43 | 72.300  | 0.000   | 0.000   | 132.600 |
| 44 | 70.800  | 0.000   | 0.000   | 125.500 |
| 45 | 147.000 | 78.400  | 374.600 | 454.400 |
| 46 | 150.900 | B0.300  | 386.300 | 470.300 |
| 47 | 147.800 | 79.300  | 380.500 | 456.200 |
| 48 | 146.200 | 76.400  | 376.100 | 456.200 |
|    |         |         |         |         |
| 49 | 198.600 | 140.300 | 276.600 | 369.500 |
| 50 | 201.700 | 142.200 | 281.000 | 373.100 |
| 51 | 199.400 | 143.200 | 278.000 | 366.000 |
| 52 | 198.600 | 142.200 | 273.600 | 369.500 |
| 53 | 186.300 | 126.800 | 253.100 | 346.500 |
| 54 | 186.300 | 126.800 | 254.600 | 350.100 |
| 55 | 185.500 | 125.800 | 253.100 | 343.000 |
| 56 | 183.200 | 124.800 | 250.200 | 344.800 |
| 57 | 133.900 | 48.400  | 76.100  | 194.500 |
| 58 | 134.700 | 48.400  | 76.100  | 198.000 |
| 59 | 131.600 | 46.400  | 74.600  | 194.500 |
| 60 | 130.800 | 45.500  | 74.600  | 192.700 |
| 61 | 0.000   | C.000   | 111.000 | 0.000   |
| 62 | 0.000   | 0.000   | 114.000 | 0.000   |
| 63 | 0.000   | 0.000   | 114.000 | 0.000   |
| 64 | 0.000   | 0.000   | 114.000 | 0.000   |
| 65 | 125.700 | 170.400 | 613.000 | 225.500 |
| 66 | 124.900 | 167.500 | 615.900 | 225.500 |
| 67 | 121.800 | 164.500 | 584,800 | 220.000 |
| 68 | 126,400 | 169.400 | 610.000 | 223.700 |
| 69 | 99.300  | 116.500 | 336.100 | 148.500 |
| 70 | 101.600 | 116.500 | 342.000 | 150.300 |
| 71 |         |         |         |         |
|    | 101.600 | 116.500 | 339.100 | 150.300 |
| 72 | 101.600 | 116.500 | 340.500 | 152.200 |
| 73 | 87.700  | 100.900 | 313.900 | 135.700 |
| 74 | 87.700  | 100.900 | 315.400 | 137.500 |
| 75 | 89.200  | 102.800 | 315.400 | 139.300 |
| 76 | 86.100  | 100.900 | 310,900 | 135.700 |
| 77 | 50.400  | 36.200  | 214.700 | 51.300  |
| 78 | 50.400  | 35.300  | 217.600 | 51.300  |
| 79 | 50.400  | 34.300  | 213.200 | 51.300  |
| 80 | 50,400  | 35,300  | 216.200 | 49.500  |

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Table A8. Mean concentrations ( $\mu g/L$ ) for each set of four replicate determinations on each sample.

| - PRI  | NT C3- | C8    |         |         |         |          |         |
|--------|--------|-------|---------|---------|---------|----------|---------|
| COLUEN |        | LAB   | SPIKE O | SPIKE 1 | SPIKE 2 | SPIKE 3  | SPIKE 4 |
| CODNT  |        | 160   | 160     | 160     | 160     | 160      | 160     |
| ROF    |        |       |         |         |         |          |         |
| A      | DNT    | 1.    | 0.000   | 48.425  | 36,000  | 93.575   | 125.630 |
| 2      |        | 2.    | 0.000   | 48.400  | 86.925  | 103.900  | 125.430 |
| 3      |        | 3.    | 0.000   | 51.850  | 90.350  | 99.425   | 155.050 |
| ų.     |        | 4,    | C.000   | 50,250  | 90.775  | 100.250  | 125.180 |
| 5      |        | 5.    | 0.000   | 62.000  | 80.400  | 95.100   | 130.300 |
| 6      |        | 6.    | 0.000   | 46.275  | 98.050  | 106.900  | 133.250 |
| 7      |        | 7.    | 0.000   | 65.700  | 104.900 | 124.570  | 154.700 |
| 8      |        | 8.    | 19.275  | 60.925  | 83.475  | 76.850   | 130,950 |
| 9      |        | 9.    | 0.000   | 49.975  | 87.325  | 99.025   | 124.680 |
| 10     |        | 10. = |         | 51,200  | 89.600  | 102,000  | 128,000 |
| 11     | TNT    | 1.    | 29.175  | 61.975  | 132.400 | 144, 180 | 202.330 |
| 12     |        | 2.    | 31.775  | 68.125  | 134,980 | 156.730  | 207.550 |
| 13     |        | 3.    | 23.750  | 59,900  | 116.070 | 140.230  | 193.650 |
| 14     |        | 4.    | 32.550  | 70.400  | 131.330 | 141,580  | 203.830 |
| 15     |        | 5.    | 46.825  | 80.575  | 133.130 | 144.580  | 203.680 |

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# Table A8 (cont'd).

| 16       |   |       | 6.               | 0.000                  | 34,250             | 123.070                   | 123.650                   | 179,450                   |
|----------|---|-------|------------------|------------------------|--------------------|---------------------------|---------------------------|---------------------------|
| 17       |   |       | 7.               | 43.975                 | 92.075             | 169,530                   | 185.800                   | 262.900                   |
| 18       |   |       | 8,               | 67.750                 | 68.000             | 115.800                   | 140.770                   | 197.730                   |
| 19       |   |       | 9.               | 16.625                 | 49.325             | 115.730                   | 128.250                   | 181.900                   |
| 20       |   |       | 10.              | mean= 38.100           | 72.400             | 141.000                   | 155.000                   | 210.000                   |
| 21       |   | RDX   | ٦.               | 55.475                 | 148.950            | 250.450                   | 277.720                   | 549.550                   |
| 22       |   |       | 2.               | 147.800                | 161.150            | 263.930                   | 291.300                   | 561.000                   |
| 23       |   |       | 3.               | 74.800                 | 173.980            | 260.380                   | 297.500                   | 575.550                   |
| 24       |   |       | 4.               | 59.425                 | 62.230             | 256.920                   | 287.350                   | 549.030                   |
| 25       |   |       | - <b>5</b> .     | 130.580                | 327.600            | 255.700                   | 338.630                   | 649.100                   |
| 26       |   |       | 6.               | 110.180                | 196.730            | 328.480                   | 327.530                   | 567.430                   |
| 27       |   |       | 7.               |                        | 265.500            | 336.500                   | 382.830                   | 574.050                   |
| 28<br>29 |   |       | 8.               | 18.200                 | 120.150            | 238,520                   | 278.600                   | 571.400                   |
| 30       |   |       | 9.               | 58.150<br>mean= 55.600 | 155.600            | 255.680                   | 278.470                   | 549.600                   |
| 31       |   | 10.07 |                  |                        | 35.650             | <u>254,000</u><br>124.020 | 127.300                   | <u>551.000</u><br>205.770 |
| 32       |   | HMX   | 1.               |                        | 43,650             | 129.680                   | 143.180                   | 226.950                   |
| 33       |   |       | 3.               | C.000                  | 53.925             | 131.950                   | 138.800                   | 222.500                   |
| 34       |   |       | 4.               | 0.000                  | 46.925             | 135.900                   | 14(.650                   | 225.450                   |
| 35       |   |       | 5.               | 0.000                  | 47.400             | 140.580                   | 140.000                   | 199.600                   |
| 36       |   |       | 6.               | 0.000                  | 73,300             | 170.170                   | 167.450                   | 216.730                   |
| 37       |   |       | 7.               | 0.000                  | 34.425             | 345.330                   | 376.100                   | 419,100                   |
| 38       |   |       | 8.               | 0.000                  | 59,900             | 79.500                    | 150.800                   | 281.170                   |
| 39       |   |       | 9.               |                        | 44.200             | 132.700                   | 144.500                   | 221.200                   |
| 40       |   |       | 10.              | mean= 0,000            | 44.600             | 134,000                   | 147.000                   | 223,000                   |
| 41       | B | DNT   | 1.               | C.COO                  | 50.475             | 98.625                    | 114.820                   | 61.700                    |
| 42       |   |       | 2.               | 0.000                  | 62.925             | 114.700                   | 127.650                   | 77.325                    |
| 43       |   |       | 3.               | 0.000                  | 57.175             | 90.575                    | 112.820                   | 65.250                    |
| 44       |   |       | 4.               | 0.000                  | 60,525             | 106.050                   | 128.950                   | 74.650                    |
| 45       |   |       | 5.               | C.000                  | 67.150             | 1 C3. 800                 | 119.750                   | 77,175                    |
| 46       |   |       | 6.               | 0.000                  | 58,475             | 109.800                   | 124.070                   | 70.025                    |
| 47       |   |       | 7.               | 0.000                  | 71.625             | 136.950                   | 153.770                   | 96.425                    |
| 48       |   |       | 8.               | 0.000                  | 65.500             | 97.375                    | 121.070                   | 74.175                    |
| 49<br>50 |   |       | . 9.             | 0.000                  | 61.175             | 114.780                   | 125.800                   | 76.075                    |
| 51       |   | TNT   | <u>10.</u><br>1. | 0.000                  | <u> </u>           | 115.000                   | <u>128,000</u><br>151.070 | 76,800                    |
| 52       |   |       | 2.               | 0.000                  | 53.075             | 135.350                   | 156.050                   | 87.675                    |
| ร์วั     |   |       | 3.               | C.COO                  | 48.050             | 122.930                   | 138.100                   | 82.400                    |
| 54       |   |       | 4,               | 0.000                  | 50,300             | 135.770                   | 146.200                   | 87.350                    |
| 55       |   |       | 5.               | 0.000                  | 71.650             | 149.770                   | 151.730                   | 99.100                    |
| 56       |   |       | 6,               | 0.000                  | 49,525             | 134.300                   | 151.200                   | 76.250                    |
| 57       |   |       | 7.               | 0.000                  | 62.550             | 169.420                   | 187.250                   | 109.430                   |
| 58       |   |       | 8,               | 0.000                  | 37.950             | 129.700                   | 142.000                   | 108.980                   |
| 59       |   |       | 9,               | 0.000                  | 51.075             | 135.200                   | 150.550                   | 83,900                    |
| 60       |   |       | 10.              | mean- C.000            | 51.500             | 137.000                   | 154.000                   | 85.800                    |
| 61       |   | RDX   | 1.               | 0.000                  | 66.200             | 260.170                   | 275.380                   | 377.300                   |
| 62       |   |       | 2.               |                        | 73.900             | 256.650                   | 270.170                   | 369.880                   |
| 63       |   |       | 3.               | 0.000                  | 94,300             | 245.250                   | 304.250                   | 398.250                   |
| 64       |   |       | 4.<br>E          | 0.000                  | 74,400             | 241.600                   | 273.220                   | 383.420                   |
| 65<br>66 |   |       | 5,               | 0.000<br>16.800        | 170.600<br>179.300 | 287.170                   | 336.150                   | 429,950                   |
| 67       |   |       | 6.<br>7.         |                        | 92.000             | 361.000<br>261.780        | 510.550<br>288.950        | 587.750                   |
| 68       |   |       | /•<br>9•         | 0.000                  | 96.425             | 295.230                   | 299.280                   | 404.850<br>362.670        |
| 69       |   |       | 9,               | 0.000                  | 75.225             | 250.450                   | 265.700                   | 371.600                   |
| 70       |   |       | 10.              |                        | 74.300             | 248.000                   | 273.000                   | 372.000                   |
| 71       |   | нмх.  | 1.               | 0.000                  | 60.925             | 215.180                   | 232.180                   | 315.550                   |
| 72       |   | 1015  | 2.               | C.000                  | 115.480            | 242.830                   | 260.350                   | 353.030                   |
| 73       |   |       | 3.               | 0.000                  | 79.725             | 202.520                   | 284.100                   | 323.030                   |
| 74       |   |       | 4.               |                        | 66.525             | 217.580                   | 243.330                   | 329.170                   |
| 75       |   |       | 5,               | 0.000                  | 95.025             | 250.270                   | 252.700                   | 358,130                   |
| 76       |   |       | 6.               |                        | 162.000            | 537.170                   | 527.850                   | 492.080                   |
| 77       |   |       | 7,               | 0.000                  | 89.250             | 223, 350                  | 258.170                   | 377.600                   |
| 78       |   |       | 8.               | 20.675                 | 93.425             | 175.050                   | 242.520                   | 324.730                   |
| 79       |   |       | 9.               | 0.000                  | 65,725             | 220.500                   | 235.350                   | 326,150                   |
| 80       | ~ | -     | 10,              | man- C.COO             | 66.800             | 223.000                   | 245.000                   | 334.000                   |
| 81       | С | DNT ' | 1,               | 55.650                 | 141.000            | 209.250                   | 187,580                   | 127,180                   |
| 82       |   |       | 2.               |                        | 150.450            | 197.600                   | 189.270                   | 136.050                   |
| 83       |   |       | 3.               | 72.700                 | 151.650            | 205.630                   | 133.600                   | 135.600                   |
| 84       |   |       | 4.               | 74.525                 | 150.250            | 200.600                   | 183.830                   | 133.830                   |
|          |   |       |                  |                        |                    |                           |                           |                           |

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| Table A8 (cont'd). | Mean concentrations $(\mu g/L)$ for each set of four replicate determinations on |
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| each sample.       | •  |

| 85         |      | 5.   | 81.300            | 160.880            | 198.520            | 191.830            | 131.750            |
|------------|------|--|-------------------|--------------------|--------------------|--------------------|--------------------|
| 86         |      | 6.   |                   | 143.500            | 194.330            | 177.850            | 127.300            |
| 87         |      | 7.   | 74.550            | 167.200            | 231.580            | 217.880            | 149,130            |
| 88         |      | 8.   | 59.750            | 139.820            | 195.130            | 172.300            | 109.830            |
| 89         |      | 9.   |                   | 147.980            | 199.580            | 185.330            | 132.750            |
| 90         | _    | 10,  | mean• 71.100      | 148.000            | 199.000            | 186.000            | 125.000            |
| 91         | TN   | IT 1.  | 0.000             | 69.700             | +153, 170          | 135.670            | 37.350             |
| 92         |      | 2.   | C.000             | 87.225             | 153.180            | 135.780            | 52.450             |
| 93         |      | 3.   | 0.000             | 78.875             | 138.550            | 77.E25             | 60.375             |
| 94         |      | 4.   |                   | 83.625             | 154.980            | 136.000            | 47.775             |
| 95         |      | 5.   |                   | 98.600             | 146.730            | 145.520            | 51.075             |
| 96         |      | 6.   |                   | 67.425             | 135.350            | 122.150            | 44.625             |
| 97         |      | 7.   |                   | 110.450            | 194.450            | 173.750            | 66.575             |
| 98         |      | θ.   |                   | 52.725             | 142.750            | 115.180            | 77.550             |
| 99         |      | 9.   |                   | 78.600             | 141.980            | 126.050            | 47.175             |
| 100        |      | <u>10</u>  | nean- 0.000       | 85.800             | 154.000            | 137.000            | 51.500             |
| 101        | RD   |  |                   | 389.170            | 259.050            | 231.600            | 66.650             |
| 10.2       |      | 2.   |                   | 383.550            | 282.380            | 260.880            | 76.425             |
| 103        |      | 3.   |                   | 376.200            | 294.330            | 145.170            | 82.325             |
| 104        |      | 4.   |                   | 373.580            | 278.550            | 251.800            | 85.925             |
| 105        |      | 5.   | 0.000             | 468.280            | 346.200            | 280.530            | 138.480            |
| 106        |      | <u>6</u> .   |                   | 336.920            | 251.350            | 235.350            | 69.500             |
| 107        |      | 7.   | 0.000             | 372.420            | 274,500            | 248.770            | 72.775             |
| 108        |      | 8.   | 0.000             | 407.580            | 295.000            | 217.380            | 69.425             |
| 109<br>110 |      | 9.<br>10.  |                   | 379.380            | 277.300            | 252.750            | 75.350             |
| 111        | HM   | the second s |                   | 371.000            | 273.000            | 248.000            | 74.300             |
| 112        |      | 2.   |                   | 438.500<br>453.250 | 355.230            | 332,750            | 179.230            |
| 113        |      | 3.   | 114.230           | 406.350            | 358.080<br>349.700 | 384.950<br>243.580 | 195.800<br>193.180 |
| 114        |      | 4  |                   | 462.530            | 369.980            | 344.530            | 194.270            |
| 115        |      | 5.   |                   | 426.350            | 356.980            | 320.700            | 249.950            |
| 116        |      | 6.   | 113.320           | 460.670            | 394.850            | 375.450            | 212.780            |
| 117        |      | 7.   | 287.850           | 656,350            | 584,250            | 556.880            | 377.170            |
| 118        |      | 8.   | 113.900           | 416.030            | 315.050            | 301.200            | 149.450            |
| 119        |      | 9.   | 128.600           | 459.280            | 369.530            | 346.100            | 194.930            |
| 120        |      | 10.  | mean= 124,000     | 458.000            | 369,000            | 347.000            | 191.000            |
| 121        | D DN |  |                   | 134.550            | 85.050             | 176.600            | 39.325             |
| 122        |      | 2.   |                   | 122.900            | 100.880            | 86.100             | 49.275             |
| 123        |      | 3.   |                   | 128.880            | 107.380            | 91.800             | 53.300             |
| 124        |      | 4.   | 0.000             | 119.750            | 103.400            | 85.550             | 51.575             |
| 125        |      | 5.   | 0.000             | 118.820            | 99.175             | 92.975             | 52.975             |
| 126        |      | 6.   | 0.000             | 120.800            | 99.125             | 84.750             | 48,625             |
| 127        |      | 7.   | C.000             | 175.230            | 127.000            | 104.630            | 56.575             |
| 128        |      | 8.   | 0.000             | 119.050            | 92.000             | 75.650             | 22.725             |
| 129        |      | 9.   |                   | 124.700            | 101.030            | 87.675             | 50.400             |
| 130        |      | 10.  | <b>Desn</b> 0.000 | 128.000            | 102.000            | 85.600             | 51.200             |
| 131        | TN   |  |                   | 158.400            | 114.350            | 204.400            | 24.250             |
| 132        |      | 2.   |                   | 170.130            | 117.430            | 101.430            | 34.525             |
| 133        |      | 3.   | 0.000             | 178,150            | 115.150            | 108.980            | 32.125             |
| 134        |      | 4.   | 0.000             | 169.480            | 113.180            | 107.200            | 37.475             |
| 135        |      | 5.   | C.000             | 164.900            | 125.470            | 121.500            | 42.300             |
| 136        |      | 6.   |                   | 161.100            | 112.050            | 92.200             | 27.225             |
| 137        |      | 7.   |                   | 235.520            | 147.700            | 131.850            | 45.850             |
| 138        |      | 8.   |                   | 109.520            | 98.225             | 88.900             | 49.050             |
| 139        |      | 9.<br>10.  |                   | 167.950            | 116.500            | 101.380            | 35.275<br>34.300   |
| 140        |      |  |                   | 172,000            | 117,000            | 103,000            | 195.770            |
| 141<br>142 | RD   | x 1.<br>2.   |                   | 573.080            | 327.280<br>354.530 | 475.380<br>325.630 | 246.950            |
| 143        |      | 3.   | 134.770           | 676.570            | 367.130            | 357.900            | 240.930            |
| 144        |      | 4.   | 119.800           | 609.430            | 349.850            | 315.900            | 225,330            |
| 145        |      | 5.   |                   | £43.650            | 401.480            | 385.830            | 288.550            |
| 146        |      | 6.   | 96.450            | 553.900            | 300.250            | 271,950            | 188.830            |
| 147        |      | 7.   | 122.650           | 703.150            | 396.450            | 388.750            | 216.530            |
| 148        |      | 8.   | 158.020           | 656.030            | 293.170            | 335.630            | 202.580            |
| 149        |      | 9.   |                   | 605.930            | 339.420            | 313.900            | 215.430            |
| 150        |      | 10.  | men=111.600       | 607.000            | 335.000            | 305.800            | 211.000            |
|            |      |  |                   |                    |                    |                    |                    |
Table A8 (coat'd).

| 151 | HMX 1.    | C.000 | 204.930 | 135.580 | 246.180 | 40.925 |
|-----|-----------|-------|---------|---------|---------|--------|
| 152 | 2.        | 0.000 | 219.020 | 163.750 | 135,630 | 58.825 |
| 153 | 3.        | C.000 | 235.050 | 156.420 | 170.500 | 49.600 |
| 154 | 4.        | 0.000 | 221.650 | 150.880 | 142.500 | 54,875 |
| 155 | 5.        | 0.000 | 234.420 | 136.920 | 143.520 | 81.550 |
| 156 | 6.        | 0.000 | 191.850 | 135.800 | 113.730 | 0.000  |
| 157 | 7.        | 0.000 | 329.470 | 214.180 | 198.800 | 68.775 |
| 158 | 8.        | 0.000 | 276.300 | 171.550 | 116.680 | 89.425 |
| 159 | 9.        | 0.000 | 223.680 | 150.330 | 137.050 | 50.850 |
| 160 | 10, mean= | 0.000 | 223.000 | 147.000 | 134.000 | 44.600 |

Table A9. Spike 2 and spike 3 concentrations (from Table A8) normalized to means (column headings indicate matrix by first letter, analyte by next three, and spike number by last number; outliers are marked by asterisk\*). 10.00

| COLUMN<br>COUNT<br>ROW | BADNT2<br>8 | BACNTJ<br>B | RBDNT2<br>8 | BBDWT3<br>8   |
|------------------------|-------------|-------------|-------------|---------------|
| 1                      | 0.95982     | 0.51740     | C.857609    | 0.89703       |
| 2                      | 0.97015     | 1.01863     | C.997391    | 0,99727       |
| 3                      | 1.00837     | 0.97475     | 0.787609    | 0.88141       |
| 4                      | 1.01311     | C.98284     | 0.922174    | 1.00742       |
| 5                      | 0.89732     | 0.93235     | 0.902609    | 0,93555       |
| 6                      | 1.09431     | 1.06765     | 0.954783    | 0.96930       |
| 7                      | 0.93164     | 0.75343     | 0.846739    | 0,94586       |
| 8                      | 0.97461     | C.97083     | 0.998087    | 0.98281       |
| - PRIM                 | T C21C22C31 | C 32        |             |               |
| COLUNN                 | RCDNT2      | RCDNT3      | RDCNT2      | B D DNT 3     |
| COUNT                  | 8           | 8           | 8           | 8             |
| BOW                    |             |             |             |               |
| 1                      | 1.05151     | 1.00849     | 0.83382     | 1.97098 *     |
| 2                      | 0.99296     | 1,01758     | 0,98902     | 0.96094       |
| 3                      | 1.03332     | C.71935     | 1.05275     | 1.02455       |
| 4                      | 1,00804     | 0.98833     | 1.01373     | 0.99944       |
| 5                      | 0.99759     | 1.03134     | 0.97230     | 1.03767       |
| 6                      | 0.97653     | 0.95618     | 0.97181     | 0.94587       |
| 7                      | 0.98055     | C.92634     | C.90196     | 0.89118       |
| 8                      | 1.00291     | 0.99640     | 0.39049     | 0.97852       |
| PRIM                   | T C3C4C13C1 | 4           |             |               |
| COLUMN                 | RATNT2      | BATHTS      | RBINT2      | <b>RBTNT3</b> |
| COUNT                  | 8           | 8           | 8           | 8             |
| BOW                    |             |             |             |               |
| 1                      | 0.939007    | 0.93019     | 0.98832     | 0.98097       |
| 2                      | 0.957305    | 1.01116     | 0.98796     | 1.01331       |
| 3                      | 0.823191    | 0.90471     | 0.89730     | 0.89675       |
| 4                      | 0.931418    | 0.91600     | 0.99102     | C.94935       |
| 5                      | 0.944184    | 0.93277     | 1.09321     | 0.98526       |
| 6                      | 0.872837    | 0.79774     | 0.98029     | 0.98182       |
| 7                      | 0.821277    | 0.90819     | 0.94672     | 0.92208       |
| 8                      | 0.820780    | 0.82742     | 0.99416     | 0,97760       |

Table A9 (cont'd). Spike 2 and spike 3 concentrations (from Table A8) normalized to means.

| - PRIN<br>COLUMN<br>COUNT<br>BOW  | FCTNT2<br>8                 | BCINT3<br>8       | RDTNT2<br>8     | FDTNT3<br>8          |
|-----------------------------------|-----------------------------|-------------------|-----------------|----------------------|
| 1                                 | 0.99461                     | C. 9029           | 0.97735         | 1.98447 *            |
| 2                                 | 0.99468                     | 1.02C29           | 1.00368         | 0.98476              |
| 3                                 | 0.89968                     | 0.56661           | 0.98419         | 1.05806              |
| 4                                 | 1.00636                     | 0.99270           | 0.96735         | 1.04078              |
| 5                                 | 0.95279                     | 1.06219           | 1.07239         | 1.17961              |
| 6                                 | 0.87890                     | 0.89161           | 0.95769         | 0.89515              |
| 7                                 | 0.92695                     | 0.84073           | 0.83953         | 0.86311              |
| 8                                 | 0.92195                     | 0.92007           | 0.99573         | 0.98427              |
| PRIN<br>COLUMN<br>COUNT<br>ROW    | T C5C6C15C16<br>BARDX2<br>8 | BARDX 3<br>8      | RBRDX2<br>8     | R BR D X 3<br>8      |
| 1                                 | 0.98602                     | 0.99541           | 1.04907         | 1.00872              |
| 2                                 | 1.03909                     | 1.05125           | 1.03488         | 0.98963              |
| 3                                 | 1.02512                     | 1.C6631           | C.98891         | 1.11447              |
| 4                                 | 1.01150                     | 1.02993           | 0.97419         | 1.00081              |
| 5                                 | 1.00669                     | 1.21373           | 1.15794         | 1.23132              |
| 6                                 | 1.29323                     | 1.17394           | 1.45565 #       | 1.87015 *            |
| 7                                 | 0.93906                     | C.S5657           | 1.19044         | 1.09626              |
| 8                                 | 1.00661                     | 0.99810           | 1.00988         | 0.98791              |
| - PRIN<br>COLUMN<br>COUNT<br>ROW  | T C25C26C35C<br>RCRDX2<br>8 | 36<br>RCPDX3<br>8 | RDRDX2<br>8     | RDRDX3<br>8          |
| 1                                 | 0.94890                     | 0.93387           | C.97696         | 1.53447 *            |
| 2                                 | 1.03436                     | 1.05154           | 1.05830         | 1.05174              |
| 3                                 | 1.07813                     | 0.60149           | 1.09591         | 1.15526              |
| 4                                 | 1.02033                     | 1.01532           | 1.04433         | 1.01969              |
| 5                                 | 1.26813                     | 1.13278           | 1.19845         | 1.24542              |
| 6                                 | 0.92070                     | 0.94899           | 0.89627         | 0.67782              |
| 7                                 | 1.08059                     | 0.87653           | 0.87513         | 1.08338              |
| 8                                 | 1.01575                     | 1.C1915           | 1.01319         | 1.01323              |
| PRIN<br>COLURN<br>COUNT<br>BOW    | T C7C9C17C18<br>RAH5X2<br>8 | R PHNX3<br>8      | RB A412<br>8    | RBH <b>ax 3</b><br>8 |
| 1                                 | 0.92552                     | C.86599           | 0.96493         | 0.94767              |
| 2                                 | 0.96776                     | O.97401           | 1.08892         | 1.06265              |
| 3                                 | 0.98470                     | O.94422           | C.9C816         | 1.15959              |
| 4                                 | 1.01418                     | O.95680           | 0.97570         | 0.99318              |
| 5                                 | 1.04910                     | O.95238           | 4.12229         | 1.03143              |
| 6                                 | 1.26993                     | 1.13912           | 2.4C883         | 2.15449              |
| 7                                 | 0.59328                     | 1.02585           | 0.78498         | 0.98988              |
| 8                                 | 0.99030                     | O.98299           | 0.98879         | 0.97694              |
| - PRINT<br>COLUMN<br>COUNT<br>ROW | C C27C28C37C<br>RCHMX2<br>8 | 38<br>RCPNI3<br>8 | RD # # ¥ 2<br>8 | RDAM X3<br>8         |
| 1                                 | 0.96268                     | 0.95853           | 0.92231         | 1.85209 *            |
| 2                                 | 0.97041                     | 1.10937           | 1.11395         | 1.01216              |
| 3                                 | 0.94770                     | 0.70196           | 1.06408         | 1.27239              |
| 4                                 | 1.00266                     | 0.99288           | 1.02639         | 1.06343              |
| 5                                 | 0.96743                     | 0.92421           | 0.93143         | 1.07104              |
| 6                                 | 1.07005                     | 1.00199           | 0.92381         | 0.84873              |
| 7                                 | 0.85379                     | 0.86801           | 1.16701         | 0.88716              |
| 8                                 | 1.00144                     | 0.99741           | 1.02265         | 1.02276              |

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Table A10. Concentrations  $(\mu g/L)$  of aliquots taken from each sample (average of injection duplicate results). Outliers indicated by asterisk<sup>\*</sup>; table is organized into subgroups by matrix; columns represent different spike levels and within each spike level are the two duplicate results for each aliquot from sample; rows are segregated by analyte and then by laboratory.

| MATRIX | A |
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| COLU             |  | C41<br>35                | C 4 2<br>35         | C43<br>35            | C44<br>35            | C45<br>35           |
|------------------|--|--------------------------|---------------------|----------------------|----------------------|---------------------|
| ROW              |  |                          |                     |                      |                      |                     |
| 1                | 1.000  | 1.000                    | 1.000               | 1.000                | 1.000                | 1.000               |
| 2                | spike 0.000<br>1,000   | C_COO<br>2.000           | 1.000               | 1.000                | 2.003                | 2.000               |
| DNT S            | 146 1 0.000  | 0.000                    | 48.400              | 48.450               | 86.350               | 85.650              |
| DNT 5<br>6       | $   \begin{array}{cccc}     2 & 0.000 \\     3 & 0.000   \end{array} $ | 0.000<br>0.000           | 47.450 52.200       | 49.350<br>51.500     | 86.550<br>102.700    | 87.300<br>78.000    |
| 7                | 4 0.000  | 0.000                    | 47.600              | 52.900               | 92.650               | 88.700              |
| 8                | 5 0.000  | 0.000                    | 69.300              | 54.700               | 73.850               | 96.950              |
| 9<br>10          | 6 0.0C0<br>8 38.550 *  | 0.000<br>0.000           | 47.050              | 45.500<br>48.200     | 95.850<br>84.850     | 100.250             |
| 11               | 9 0.000  | 0.000                    | 50.550              | 49,400               | 86,950               | 87.700              |
| 12               | 28.500   | 29.850                   | 62.400              | 61.550               | 132.200              | 132.600             |
| NT 13            | 33.950<br>24.400   | 29.600<br>23.100         | 65.850<br>45.500    | 70.400<br>74.300     | 131.700              | 138.250<br>104.100  |
| 15               | 32.900   | 32.200                   | 69.700              | 71.100               | 135.000              | 127.650             |
| 16               | 55.550   | 38.100                   | 74.500              | 86,650               | 124.850              | 141.400             |
| 17               | 0.000 *  | 0.000 *                  | 34.650              | 33.850               | 113.900              | 132.250             |
| 18<br>19         | 107.400 *<br>16.400  | 28.100 *<br>16.850       | 68.250              | 67.750<br>49.550     | 129.650              | 101.950             |
| 20               | \$2.700  | 58.250                   | 150.750             | 146.950              | 252.400              | 248.500             |
| DX 21            | 200.500 *  | 95.100 *                 | 161.350             | 160.950              | 267.400              | 260.450             |
| 2 2<br>2 3       | 83.450<br>56.400   | 66.150<br>62.450         | 182.550             | 165.400<br>163.300   | 262.800<br>255.950   | 257.950<br>253.900  |
| 24               | 10.800 *   | 160.350 *                | 371.850*            | 283.350 *            | 221.550 *            | 289.850             |
| 25               | 117.650  | 102.700                  | 218,350             | 175.100              | 33€.950 *            | 320.000             |
| 26<br>27         | 36.400 *<br>58.150   | C_000 *<br><u>58,150</u> | 112.100             | 128.200              | 278.200 *<br>255.300 | 198.850             |
| 28               | 0.000  | 0.000                    | 36.300              | 35.000               | 123.700              | 124.350             |
| MX 29            | 0.000  | 0.000                    | 39.850              | 47.450               | 127.600              | 131.750             |
| 30<br>31         | 0.000<br>0.000   | 0.000<br>0.000           | 53.150              | 54.700<br>42.900     | 134.500<br>135.850   | 129.400<br>135.950  |
| 32               | C.000  | 0.000                    | 61.300              | 33.500               | 143.650              | 137.500             |
| 33               | 0,000  | 0.000                    | 73,900 *            | 72.700 *             | 170.400 *            | 169.950             |
| 34<br>35         | 0.000  | 0.000                    | 16.900 *<br>43.300  | 102.900 *<br>45.100  | 10C_700 *<br>133.600 | 58.300 ·<br>131.800 |
| P                | RINT C46-C49   |                          | ,                   |                      |                      |                     |
| CCLU             |  | C47                      | C48                 | C49                  |                      |                     |
| COUN<br>ROW<br>1 | T 35<br>1.000  | 35                       | 35                  | 35                   |                      |                     |
|                  | spike 3.000  | 1.000<br>3.000           | 4.000               | 1.000<br>4.000       |                      |                     |
| 3                | 1.000  | 2.000                    | 1.000               | 2.000                |                      |                     |
| NT 5             |  | 95.850                   | 125,100             | 126.150              |                      |                     |
| NI 5             | 98.150   | 100.150<br>1CC.700       | 123.250<br>133.750* | 127.600<br>176.350 * |                      |                     |
| 7                | 100.050  | 100.450                  | 125,300             | 125.050              |                      |                     |
| 8<br>9           | 102.950<br>102.000   | 87.230<br>115.800        | 119.050             | 141.550              |                      |                     |
| 10               | 72.750 *   | 80.950 *                 | 134.350             | 132.150<br>122.450   |                      |                     |
| 11               | 98.450   | 99,600                   | 124.100             | 125,250              |                      |                     |
| 12               | 142.750  | 145.600                  | 200,750             | 2 03.900             |                      |                     |
| NT 13            | 161.400<br>134.850   | 152.050<br>145.60C       | 207.550             | 207.550<br>210.300   |                      |                     |
| 15               | 141,150  | 142.800                  | 203.500             | 204.150              |                      |                     |
| 16               | 141.550  | 147.600                  | 199.050             | 208.300              |                      |                     |
| 17               | 120.750  | 126.550                  | 182,200             | 176.700              |                      |                     |
| 18               | 145.050  | 136.500                  | 210.300             | 185.150              |                      |                     |

# Table A10 (cont'd). Concentrations ( $\mu g/L$ ) of aliquots taken from each sample.

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| м      | ATRIX A        |                      |                      |                     |                     |                      |                    |
|--------|----------------|----------------------|----------------------|---------------------|---------------------|----------------------|--------------------|
|        | 20             | 266.750              | 288.700              | £47.500             | 551.600             |                      |                    |
| RDX    |                | 288.150              | 298.450              | 572.800             | 549.200             |                      |                    |
| I.U.A. | 22             | 305.700              | 285.300              | 574.800             | 576.300             |                      |                    |
|        | 23             | 289.450              | 285.250              | 554.950             | 543.100             |                      |                    |
|        | 24             | 373.150 *            | 304.100 *            | 670.200*            | 628.000 *           |                      |                    |
|        | 25<br>26       | 319.700 *<br>267.200 | 335.350 *<br>290.000 | 559.050<br>577.050  | 575.800<br>565.750  |                      |                    |
|        | 27             | 278,850              | 278.100              | 549.600             | 549.600             |                      |                    |
|        | 28             | 126.200              | 128.400              | 205.500             | 206.050             |                      |                    |
| HMX    | 29             | 146.300              | 140.050              | 231.350             | 222.550             |                      |                    |
|        | 30<br>31       | 136.950              | 140.650              | 216.250<br>227.550  | 228.750<br>223.350  |                      |                    |
|        | 32             | 114.250              | 165.750              | 229.000             | 170.200             |                      |                    |
|        | 33             | 160.400 *            | 174.500*             | 218.300*            | 215.150 *           |                      |                    |
|        | 34             | 131.550 *            | 170.050*             | 347.300*            | 215.050 *           |                      |                    |
|        | 35             | 145.400              | 143.600              | 221.200             | 221.200             |                      |                    |
| н      | MATRIX I       | 3                    |                      |                     |                     |                      |                    |
| C      | OLUMN          | C>0                  | C51                  | C52                 | C53                 | C54                  | C55                |
|        | DUNT           | 35                   | 35                   | 35                  | 35                  | 35                   | 35                 |
| RC     | D∎             |                      |                      |                     |                     |                      |                    |
|        | 1              | 2.                   | 2.0000               | 2.000               | 2.000               | 2.000                | 2.000              |
|        | 2 sp:<br>3     | 1ke 0.               | 0.0000               | 1.000               | 1.000               | 2.000                | 2.000              |
|        | 4              | 0.                   | C.C000               | 50.800              | 50.150              | 85.450               | 111.800            |
| DNT    | 5              | ο.                   | 0.0000               | 63.500              | 62.350              | 116,150              | 113.250            |
|        | 6              | 0.                   | 0.0000               | 56.150              | 58.200              | 102.750              | 78.400             |
|        | 7              | 0.                   | 0.0000               | 64.200              | 56.850              | 110.450              | 101.650            |
|        | 8<br>9         | 0.<br>0.             | 0.0000               | 61.500<br>60.950    | 72.800<br>56.000    | 95.900<br>105.650    | 111.700<br>109.950 |
|        | 10             | 0.                   | 0.0000               | 74.650              | 56.350              | 80.750               | 106.000            |
|        | 11             | 0.                   | 0.0000               | 60.800              | 61.550              | 113.050              | 116.500            |
|        | 12             | 0.                   | C.0000               | 45.600              | 43.350              | 121.650              | 149.150            |
|        | 13             | 0.                   | 0.0000               | 54.000              | 52.150              | 140.100              | 130.600            |
|        | 14<br>15       | 0.<br>0.             | 0.0000               | 61.500<br>50.750    | 34.600<br>49.850    | 110.550<br>134.950   | 135.300            |
|        | 16             | 0.                   | C.0000               | 65.250*             | 78.050 *            | 155.200 +            | 144.350            |
|        | 17             | ō.                   | C 0000               | 45.700              | 53.350              | 137.700              | 130.900            |
|        | 18             | 0.                   | 0.0000               | 33.900              | 42.000              | 148.000              | 111.400            |
|        | 19             | ` <u>`</u> _         | <u> </u>             | 50.100              | 52.050              | 134.750              | 137.650            |
|        | 20             | •                    | 0.0000               | 62.000<br>70.050    | 70.400              | 270.000              | 250.350            |
|        | 21<br>22       | 0.<br>0.             | 0.0000               | 102.700             | 85.900              | 245.500              | 245.000            |
|        | 23             | Ő.                   | 0.0000               | 74.150              | 79.650              | 243,850              | 239.350            |
|        | 24             | 0.                   | 0.0000               | 180,100 *           | 161.100 *           | 263.450*             | 310.900            |
|        | 25             | 0.                   | 33.6000*             | 270.300 *           | 88.300 *            | 447.600*             | 274.400            |
|        | 26             | 0.                   | 0.0000               | 126.850 *           | 66.000 *<br>74.850  | 297, £50<br>248, 200 | 292.600<br>252.700 |
|        | 27             | <u>0.</u><br>0.      | 0.0000               | 62.550              | 59.300              | 217.300              | 213.050            |
|        | 29             | 0.                   | 0.0000               | 75.750 *            | 155.200 *           | 257.550              | 228.100            |
|        | 30             | э.                   | 0.0000               | 87.450              | 72.000              | 196,150              | 208.900            |
|        | 31             | 0.                   | C.C000               | 66.550              | 66.500              | 220.700              | 214.450            |
|        | 32             | 0.                   | 0.0000               | 95.850<br>187.800 * | 94.200<br>136.200 * | 244,100<br>506,400*  | 256,450<br>567,950 |
|        | 33<br>34       | 0.<br>0.             | 41.3500 *            | 48.100 *            | 138.750 *           | 167.500*             | 182.600            |
|        | 35             | 2.                   | C.CO00               | 66.200              | 65.250              | 218.650              | 222.350            |
|        |                |                      |                      |                     |                     |                      |                    |
|        | •• <i>•</i> •  | <b>65</b> (          | ~E 7                 | <b>65 1</b>         | <b>c</b> to         |                      |                    |
|        | OLUNN<br>ODN:P | C56<br>35            | c57<br>35            | C58<br>35           | C59<br>35           |                      |                    |
|        | OUNT<br>OW     | 57                   | ی ر                  | 1                   |                     |                      |                    |
|        | 1              | 2.000                | 2.000                | 2.000               | 2.000               |                      |                    |
|        | 2              | 3.000                | 3.000                | 4.000               | 4.000               |                      |                    |
|        | )              | 1,000                | 2.000                | 1.000               | 2.000               |                      |                    |

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| MATRIX  | Б  |  |   |  |  |   |
|---|--|--|---|--|--|---|
| 4   | \$9.000 *  | 130,650 *  | 60.700  | 62.700   |  |   |
| DNT 5   | 126.650  | 128.650  | 78.900  | 75.750   |  |   |
| 6<br>7  | 105.750<br>128.150   | 119.900<br>129.750   | 64.350<br>80,800  | 66.150<br>68.500   |  |   |
| 8   | 114.750  | 124.750  | 79.300  | 75.050   |  |   |
| 9   | 121.700  | 126.450  | 68.850  | 71.200   |  |   |
| 10  | 119.100  | 123.050  | 80.500  | 67.850   |  |   |
| $-\frac{11}{12}$  | 125.800  | 125.800  | 75.500  | <u>76.650</u><br>76.850  |  |   |
| TNT 13  | 155.500  | 156.600  | 90.350  | 85.000   |  |   |
| 14  | 138.900  | 137.300  | B1.050  | 83.750   |  |   |
| 15  | 142.000  | 150.400  | 86.050  | 88.650   |  |   |
| 16<br>17  | 146.500<br>154.700   | 156.950<br>147.700   | 90.100  | 108.100  |  |   |
| 18  | 154.050  | 129.950  | 84.450 *  | 71.900<br>133.500 ±  |  |   |
| 19  | 150.300  | 150.800  | 83.650  | 84.150   |  |   |
| 20  | 279.800  | 270.950  | 375.900   | 378.700  |  |   |
| RDX 21<br>22  | 269.900  | 270.450  | 371.150   | 368.600  |  |   |
| 23  | 297.650<br>273.250   | 310.050<br>273.200   | 422.600   | 373.900<br>381.000   |  |   |
| 24  | 287.300 *  | 385.000 *  | 423.400 *   | 436.500 *  |  |   |
| 25  | 675.500 *  | 345.600 *  | 533.250 *   | 642.250 ×  |  |   |
| 26  | 326.600  | 271.950  | 361.850   | 363.500  |  |   |
| <u> </u>  | <u>268,950</u><br>233.700  | 230.650  | 369.000   | 374.200  |  |   |
| 15-0X 29  | 237.000  | 283.700  | 312.850   | 318.250<br>329.950   |  |   |
| 30  | 288.100  | 280.100  | 313.600   | 332.450  |  |   |
| 31  | 248.300  | 238.350  | 334.750   | 323.600  |  |   |
| 32<br>33  | 264.700<br>562.750 ±   | 24C.700<br>492.950 *   | 370.850   | 345.400  |  |   |
|   | JOZ - /JV -  | 442.470.4  | 476.400 *   | 507.750 *  |  |   |
|   |  |  |   |  |  |   |
| 34<br>35<br>Matrix  | 199.250 *<br>238.900   | 265.800 *<br>239.800   | 371.250 <b>*</b><br>324.300   | 278.200 #<br>328.000   |  |   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65   | 265.800 +  | 371.250 *   | 278.200 *  | C64<br>35  |   |
| 34<br>35<br>MATRIX<br>PR<br>Columi<br>Count<br>Row  | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35  | 265.800 +<br>239.800<br>C61<br>35  | C62<br>35   | 278.200 *<br>328.000<br>C63<br>35  | 35   | 39  |
| 34<br>35<br>MATRIX<br>— PR<br>COLUNI<br>COUNT<br>ROW<br>1   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000   | 265.800 *<br>239.800<br>C61<br>35<br>3.000   | C62<br>3.000  | 278.200 *<br>328.000<br>C63<br>35<br>3.000   | 35<br>3.000  | 3.000   |
| 34<br>35<br>MATRIX<br>— PR<br>COLUNI<br>COUNT<br>ROW<br>1   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35  | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000   | C62<br>35   | 278.200 *<br>328.000<br>C63<br>35  | 35   | 3:<br>3.000<br>2.000  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>spike C.000<br>1.000<br>57.500   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800   | C62<br>35<br>3.000<br>1.000<br>137.600  | 278.200 *<br>328.000<br>C63<br>35<br>3.000<br>1.000<br>2.000<br>144.400  | 35<br>3.000<br>2.000<br><u>1.000</u><br>215.550  | 3:<br>3.000<br>2.000<br>2.000   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>J<br>DNT 5   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>spike C.000<br>1.000<br>57.500<br>72.200   | 265.800 +<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700   | 278.200 +<br>328.000<br>c63<br>35<br>3.000<br>1.000<br>2.000<br>144.400<br>149.200   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250  | 3.000<br>2.000<br>2.000<br>198.550<br>195.950   |
| 34<br>35<br>MATRIX<br>  | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>M C60<br>35<br>3.000<br>spike C.000<br>1.000<br>57.500<br>72.200<br>75.750   | 265.800 +<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900  | 278.200 +<br>328.000<br>c63<br>35<br>3.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400  | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700   | 3:000<br>2:000<br>2:000<br>198:550<br>195:950<br>210:550  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>J<br>DNT 5   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>spike C.000<br>1.000<br>57.500<br>72.200   | 265.800 +<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100   | C62<br>35<br>3.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000<br>1.000   | 278.200 +<br>328.000<br>c63<br>35<br>3.000<br>1.000<br>2.000<br>144.400<br>149.200   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250  | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>splke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550  | 278.200 *<br>328.000<br>C63<br>35<br>3,000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>150.850<br>151.000 *<br>147.450   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>20C.700<br>20C.700<br>193.600<br>197.450  | 3.000<br>2.000<br>198.550<br>210.550<br>200.500<br>203.450<br>191.200   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>splke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*  | 278.200 *<br>328.000<br>C63<br>35<br>3,000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.800<br>151.000 *<br>147.450<br>121.050 *   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>200.700<br>193.600<br>197.450<br>182.650   | 3.000<br>2.000<br>198.550<br>210.550<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600   |
| 34<br>35<br>MATRIX<br>PR<br>COLUMI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>sp1ke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950   | 278.200 *<br>328.000<br>C63<br>35<br>3.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>150.850<br>151.000 *<br>147.450<br>121.050 *<br>147.000  | 35<br>3.000<br>2.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150  | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>199.000  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>spike C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550<br>0.000  | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700   | 278.200 *<br>328.000<br>C63<br>35<br>3,000<br>1.000<br>2,000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700   | 35<br>3.000<br>2.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>199.000  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>1<br>2<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>TNT 13<br>14  | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>sp1ke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550   | C62<br>35<br>3.000<br>1.000<br>137.600<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950   | 278.200 *<br>328.000<br>C63<br>35<br>3,000<br>1.000<br>2,000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.600 *<br>151.000 *<br>147.850<br>121.050 *<br>147.000  | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>199.000<br>132.050   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>splke C.000<br>1.000<br>57.500<br>75.750<br>75.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000   | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.700<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>88.800<br>73.500<br>86.850   | 278.200 +<br>328.000<br>   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450<br>133.550<br>153.100   | 3.000<br>2.000<br>198.550<br>210.550<br>200.500<br>203.450<br>191.200<br>199.000<br>132.050<br>153.900<br>143.550   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>sp1ke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000  | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000   | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>88.800<br>73.500<br>86.850<br>102.500  | 278.200 +<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>84.250<br>80.400<br>94.700  | 35<br>3.000<br>2.000<br>1.000<br>219.550<br>200.700<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>107.450<br>182.650<br>174.300<br>152.450<br>133.550<br>153.100<br>145.850  | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>199.000<br>132.050<br>153.900<br>143.550<br>143.600   |
| 34<br>35<br>MATRIX<br>PR<br>COLUN<br>COUNT<br>ROW<br>1<br>2<br>3<br>  | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>spike C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000   | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>72.600<br>72.600<br>72.600<br>72.50<br>46.400<br>71.550<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.000000<br>0.00000000                                      | C62<br>35<br>3,000<br>1,000<br>1,000<br>137,600<br>151,700<br>151,900<br>149,650<br>170,750*<br>139,550<br>158,600*<br>148,950<br>65,700<br>86,800<br>73,500<br>86,850<br>102,500<br>62,150   | 278.200 *<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>80.400<br>94.700<br>72.700   | 35<br>3.000<br>2.000<br>215.550<br>199.250<br>20C.700<br>20C.700<br>193.600<br>197.450<br>182.650<br>20C.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.850<br>131.550   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>199.000<br>132.050<br>153.900<br>143.550<br>156.850<br>143.600   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>4<br>0NT 5<br>6<br>7<br>8<br>9<br>10<br>10<br>11<br>7<br>10<br>11<br>12<br>11<br>11<br>15<br>16<br>17<br>18<br>19  | 199.250 *<br>238.900 *<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>sp1ke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000  | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>78.200<br>67.250<br>46.400<br>71.550<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000   | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>88.800<br>73.500<br>86.850<br>102.500  | 278.200 +<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>84.250<br>80.400<br>94.700  | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.650<br>131.550<br>121.700  | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>132.050<br>143.550<br>143.550<br>143.550<br>143.600<br>139.150<br>163.800  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>PR<br>0<br>0<br>0<br>1<br>1<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>PR<br>COLUNI<br>ROW<br>7<br>9<br>10<br>11<br>11<br>15<br>16<br>17<br>18<br>19<br>20  | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*  | 2 £ 5 . 80 0 *<br>2 3 9 . 80 0<br>C 6 1<br>3 5<br>3 . 00 0<br>0 . 00 0<br>2 . 00 0<br>7 . 00 0<br>6 9 . 6 5 0<br>7 2 . 6 0 0<br>7 8 . 20 0<br>6 7 . 25 0<br>4 6 . 40 0<br>7 1 . 5 5 0<br>0 . 00 0  | 371.250 *<br>324.300<br>C62<br>35<br>3.000<br>1.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.700<br>151.500<br>149.650<br>170.750 *<br>139.550<br>158.600 *<br>148.950<br>65.700<br>86.800<br>73.500<br>86.850<br>102.500<br>62.150<br>61.950<br>79.350<br>398.300   | 278.200 *<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>151.400<br>121.050<br>121.050<br>147.000<br>73.700<br>85.650<br>84.250<br>80.400<br>94.700<br>72.700<br>43.500       | 35<br>3.000<br>2.000<br>215.550<br>199.250<br>20C.700<br>20C.700<br>193.600<br>197.450<br>182.650<br>20C.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.850<br>131.550   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>203.50<br>203.450<br>191.200<br>207.600<br>132.050<br>143.550<br>143.550<br>143.550<br>143.550<br>143.600<br>139.150<br>163.800<br>142.700   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>PR<br>0<br>0<br>0<br>1<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>PR<br>COLUNI<br>ROW<br>7<br>12<br>PR<br>COLUNI<br>ROW<br>7<br>12<br>PR<br>1<br>2<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>- | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*  | 2 £ 5 . 80 0 *<br>2 3 9 . 80 0<br>2 3 9 . 80 0   | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.700<br>159.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>88.800<br>73.500<br>86.850<br>102.500<br>62.150<br>61.950<br>79.350<br>398.300<br>380.150  | 278.200 *<br>328.000<br>C63<br>35<br>3.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>80.400<br>94.700<br>72.700<br>43.500<br>77.850<br>380.050<br>366.950                         | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.850<br>131.550<br>121.700<br>141.250<br>255.800<br>283.250   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>191.200<br>199.000<br>132.050<br>143.550<br>143.600<br>143.600<br>143.600<br>143.800<br>143.800<br>259.300<br>281.500   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>splke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.00000000                                    | 2 £ 5 . 80 0 *<br>2 3 9 . 80 0<br>2 3 9 . 80 0<br>3 . 000<br>0 . 000<br>2 . 000<br>5 3 . 800<br>7 4 . 100<br>6 9 . 6 50<br>7 2 . 600<br>7 8 . 200<br>6 7 . 2 50<br>4 6 . 400<br>7 1 . 5 50<br>0 . 000<br>0 | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>86.800<br>73.500<br>86.850<br>102.500<br>62.150<br>61.950<br>79.350<br>398.300<br>380.150<br>370.450   | 278.200 *<br>328.000   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.650<br>131.550<br>121.700<br>141.250<br>255.600<br>297.500   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>203.450<br>191.200<br>207.600<br>199.000<br>132.050<br>153.900<br>143.550<br>143.550<br>143.600<br>139.150<br>163.800<br>259.300<br>281.500<br>291.150   |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>PR<br>0<br>0<br>0<br>1<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>PR<br>COLUNI<br>ROW<br>7<br>12<br>PR<br>COLUNI<br>ROW<br>7<br>12<br>PR<br>1<br>2<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>PR<br>COLUNI<br>ROW<br>7<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>PR<br>- | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*  | 2 £ 5 . 80 0 *<br>2 3 9 . 80 0   | C62<br>35<br>3,000<br>1,000<br>1,000<br>137,600<br>151,700<br>151,700<br>151,900<br>149,650<br>170,750*<br>139,550<br>158,600*<br>148,950<br>65,700<br>88,800<br>73,500<br>86,850<br>102,500<br>62,150<br>61,950<br>79,350<br>398,300<br>380,150<br>370,450<br>373,250  | 278.200<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>84.250<br>80.400<br>94.705<br>72.700<br>43.500<br>77.850<br>380.050<br>381.950<br>373.900    | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>20C.700<br>20C.700<br>193.600<br>197.450<br>182.650<br>20C.150<br>174.300<br>152.450<br>133.550<br>133.550<br>131.550<br>121.700<br>141.250<br>283.250<br>297.500<br>276.700  | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>199.000<br>132.050<br>153.900<br>143.550<br>156.850<br>143.600<br>143.600<br>259.300<br>281.500<br>281.500<br>280.400  |
| 34<br>35<br>MATRIX<br>PR<br>COLUNI<br>COUNT<br>ROW<br>1<br>2<br>3<br>   | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*  | 2 £ 5 . 80 0 *<br>2 3 9 . 80 0<br>2 3 9 . 80 0<br>3 . 000<br>0 . 000<br>2 . 000<br>5 3 . 800<br>7 4 . 100<br>6 9 . 6 50<br>7 2 . 600<br>7 8 . 200<br>6 7 . 2 50<br>4 6 . 400<br>7 1 . 5 50<br>0 . 000<br>0 | C62<br>35<br>3.000<br>1.000<br>1.000<br>137.600<br>151.700<br>151.700<br>151.900<br>149.650<br>170.750*<br>139.550<br>158.600*<br>148.950<br>65.700<br>86.800<br>73.500<br>86.850<br>102.500<br>62.150<br>61.950<br>79.350<br>398.300<br>380.150<br>370.450   | 278.200 *<br>328.000   | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>200.700<br>193.600<br>197.450<br>182.650<br>200.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.650<br>131.550<br>121.700<br>141.250<br>255.600<br>297.500   | 3.000<br>2.000<br>198.550<br>195.950<br>210.550<br>200.500<br>203.450<br>191.200<br>207.600<br>132.050<br>153.900<br>143.550<br>143.600<br>143.600<br>143.500<br>259.300<br>259.300<br>281.500<br>281.500<br>281.500<br>281.500   |
| 34<br>35<br>MATRIX<br>PR<br>COLUN<br>COUNT<br>ROW<br>1<br>2<br>3<br>  | 199.250 *<br>238.900<br>C<br>INT C60-C65<br>N C60<br>35<br>3.000<br>splke C.000<br>1.000<br>57.500<br>72.200<br>75.750<br>76.450<br>84.400<br>67.900<br>73.100<br>71.950<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.00000000 | 265.800 *<br>239.800<br>C61<br>35<br>3.000<br>0.000<br>2.000<br>53.800<br>74.100<br>69.650<br>72.600<br>72.600<br>72.600<br>72.600<br>72.600<br>72.50<br>46.400<br>71.550<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.0000000<br>0.00000000  | C62<br>35<br>3,000<br>1,000<br>1,000<br>137,600<br>151,700<br>151,900<br>151,900<br>151,900<br>151,900<br>151,900<br>151,900<br>151,900<br>151,900<br>151,900<br>158,600*<br>148,950<br>65,700<br>88,800<br>73,500<br>86,850<br>102,500<br>62,150<br>61,950<br>79,350<br>398,300<br>380,150<br>370,450<br>373,250<br>394,250* | 278.200 *<br>328.000<br>328.000<br>1.000<br>2.000<br>144.400<br>149.200<br>151.400<br>151.400<br>151.400<br>151.400<br>151.000 *<br>147.450<br>121.050 *<br>147.000<br>73.700<br>85.650<br>80.400<br>94.700<br>72.700<br>43.500<br>77.850<br>380.050<br>380.050<br>381.950<br>373.900<br>542.300 * | 35<br>3.000<br>2.000<br>1.000<br>215.550<br>199.250<br>20C.700<br>193.600<br>193.600<br>193.600<br>195.450<br>182.650<br>20C.150<br>174.300<br>152.450<br>133.550<br>153.100<br>145.650<br>131.550<br>121.700<br>141.250<br>255.600<br>283.250<br>297.500<br>276.700<br>324.550* | C65<br>35<br>3.000<br>2.000<br>198.550<br>195.950<br>203.450<br>191.200<br>203.450<br>191.200<br>132.050<br>153.900<br>143.500<br>143.600<br>143.600<br>143.600<br>259.300<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>281.500<br>200<br>281.500<br>281.500<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200 |

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# Table A10 (cont'd). Concentrations ( $\mu g/L$ ) of aliquots taken from each sample.

MATRIX C

| 28<br>HAX 29<br>J0<br>31<br>32<br>33<br>34<br>J5 | 116.100<br>121.450<br>119.200<br>127.400<br>197.250 *<br>127.90J *<br>136.400 *<br>128.150 | 116,450<br>126,550<br>109,250<br>127,700<br>125,750 *<br>98,750 *<br>91,400 *<br>129,050 | 443,450<br>449.350<br>408.200<br>460.650<br>422.150<br>424.400 *<br>426.900 *<br>462.350 | 433.550<br>457.150<br>404.500<br>430.550<br>496.950<br>405.150 *<br>456.200 | 355.050<br>364.350<br>334.600<br>371.900<br>355.100<br>371.400 +<br>303.350 +<br>371.300 | 355.400<br>351.800<br>364.800<br>368.050<br>355.850<br>419.300 *<br>326.750 *<br>367.750 |
|--|--|--|--|---|--|--|
|  | PINT C66-C69   |  |  |   |  |  |
| COLU   |  | C67<br>35  | C68<br>35  | C 6 9<br>3 5  |  |  |
| ROW  | 3 444  |  | l .  |   |  |  |
| 1  | 3.000<br>SPIKE 3.000   | 3.000<br>3.000   | 3.000  | 3.000   |  |  |
| _3_  | 1.000  | 2,000  | 1,000  | 2.000   |  |  |
| DNT 5  | 184,750<br>188,650   | 190.400  | 123.350  | 125.000   |  |  |
| 6  | 135.250 *  | 189,900<br>132,350 *   | 134.450<br>133.450   | 137.650<br>137.750  |  |  |
| 7  | 183.750  | 183.900  | 134.300  | 133.350   |  |  |
| 8<br>9   | 185.150  | 198.500  | 130.500  | 133.000   |  |  |
| 10   | 175.950<br>161.500   | 179.750<br>183.100   | 129,550<br>136.950 *   | 125.050<br>82.700 *   |  |  |
| 11   | 126.300  | 184,350  | 134.300  | _131.200  |  |  |
| 12<br>TNT 13                                     | 132.750  | 138.600  | 36.350   | 38.350  |  |  |
| 14   | 141.450<br>E3.150 *  | 138,100<br>72,100 *  | 50.700<br>58.700   | 54.200<br>62.050  |  |  |
| 15   | 136,600  | 135.400  | 49.150   | 45.400  |  |  |
| 16   | 144.650  | 146,400  | 59.450   | 42.700  |  |  |
| 17<br>18   | 116.000<br>11C.950   | 128.300<br>119.400   | 40.800   | 48.450  |  |  |
| 19   | 126,800  | 125.300  | 63.500 *<br>48.400_  | 91.600 *<br>45.950  |  |  |
| 20   | 228.400  | 234.800  | 70.950   | 62.350  |  |  |
| RDX 21   | 258.200  | 263.550  | 75.150   | 77.700  |  |  |
| 22<br>23   | 156.950 *<br>251.950   | 141.400 *<br>251.650   | 79.050<br>82.200   | 85.600<br>89.650  |  |  |
| 24   | 294.450 *  | 267.400 *  | 162.950 *  | 114.000 *   |  |  |
| 25   | 233.000  | 237.700  | 67.600   | 71.400  |  |  |
| 26<br>27   | 243.350<br>253.850   | 191.400<br>251.650   | 92.500   | 46.350  |  |  |
| 28   | 333.850  | 331.650  | 181.500  | 176.950   |  |  |
| HMX 29   | 346,650 *  | 423.250 *  | 195.850  | 195.750   |  |  |
| 30<br>31   | 244.400 *<br>347.300   | 242.750 *  | 182.650  | 2 C3 . 700  |  |  |
| 32   | 314.050  | 327.350  | 194,350<br>223,450 *   | 194.200<br>276.450 *  |  |  |
| 33   | 356.800 *  | 394.100 ×  | 252,950 ×  | 172.600 ×   |  |  |
| 34<br>35   | 279.500 *<br>348.300   | 322.900 *<br>343.900   | 157.000 *  | 141.900 *   |  |  |
| MATRIX D   | 340,300  | 343.900  | 196.250  | 193.600   |  |  |
| COLUM  | IN C70   | <b>c</b> 71  | C 72   | <b>C73</b>  | c7.  |  |
| COUNT  |  | 35   | 35   | C73<br>35   | C74<br>35  | C75<br>35  |
| ro u   |  | - 1  |  | •••   |  | 33   |
| 1  | 4.300<br>spike C.000   | 4.000  | 4.000  | 4.000   | 4.000  | 4.000  |
| 23   | spike 0.000<br>1.000   | C.000<br>2.000   | 1.000  | 1.000   | 2.000  | 2.000  |
| 4  | 0.000  | 0.000  | 122.350  | 146.750   | 85.650   | 84.450   |
| DNT 5<br>6                                       | 0.000<br>0.000   | 0.000  | 122,350<br>1 <b>33</b> ,750  | 123.450   | 100.250  | 101.500  |
| 7  | 0.000  | C.000<br>0.000   | 129.700  | 124.000   | 10€.250<br>10€.250   | 106.500<br>100.550   |
| 8  | 0.000  | C.000  | 107.900  | 129.750   | 95.050   | 103.300  |
| 9  | 0,000  | C.000  | 121.000  | 120.600   | 103.450  | 94.800   |

# Table A10 (cont'd).

MATRIX D

|     | 10              | 0.000                | C.000                | 128.750                   | 109.350                   | 82.850                    | 101.150                   |
|-----|-----------------|----------------------|----------------------|---------------------------|---------------------------|---------------------------|---------------------------|
|     | $\frac{11}{12}$ | 0.000                | 0.000                | 125.300                   | 124.100                   | 100.450                   | 101.600                   |
|     |                 | 0.000                | C.000<br>0.000       | 171.750                   | 145.050                   | 115.750<br>117.350        | 112.950                   |
| TNT | 14              | 0.000                | c.coo                | 180.200                   | 176.100                   | 116.200                   | 114.100                   |
|     | 15              | 0.000                | 0.000                | 172.900                   | 166.050                   | 106.150                   | 120.200                   |
|     | 16              | 000.0                | C.000                | 168.050                   | 161.750                   | 123.750                   | 127.200                   |
|     | 17              | 0.000                | C.000                | 163.800                   | 158.400                   | 106.450                   | 117.650                   |
| TNT | 18<br>19        | 0.000<br>0.000       | 0.000                | 111.350 *                 | 107.700 *                 | 93.500 *                  | 102.950                   |
|     | 20              | 102.550              | 102.050              | <u>168.950</u><br>583.000 | <u>166.950</u><br>563.150 | <u>116.500</u><br>325.000 | <u>116.500</u><br>329.550 |
| RDX | 21              | 148.700              | 123.950              | 619.200                   | 613.950                   | 355.600                   | 353.450                   |
|     | 22              | 133.550              | 136.000              | 692.550                   | 660.600                   | 356.800                   | 377.450                   |
|     | 23              | 116,800              | 122.800              | 609.950                   | 6 C8.900                  | 347.700                   | 352.000                   |
|     | 24              | 157.600 +            | 222.550 *            | 642.650 *                 | 644.650 *                 | 412.500 *                 | 390.050                   |
|     | 25<br>26        | 98.200<br>122.900 *  | 54.700<br>193.150 ·  | 548.500                   | 559.300                   | 304.150                   | 296.350                   |
|     | 27              | 112.500              | 193.150 *<br>114.000 | 715.600 *                 | 596.450 *<br>597.400      | 292.500<br>339.050        | 293.850<br>339.800        |
|     | 28              | 0.000                | 0.000                | 205.000                   | 204.850                   | 136.650                   | 134.500                   |
| HMX | 29              | 0.000                | C.000                | 226.700                   | 211.350                   | 165.200                   | 162.300                   |
|     | 30              | 0.000                | 0.000                | 236.350                   | 233.750                   | 146.300                   | 166,550                   |
|     | 31              | 0.000                | C.000                | 223.450                   | 219.850                   | 153.050                   | 148.700                   |
|     | 32<br>33        | 0.000                | 0.000<br>C.000       | 235.100                   | 233.750                   | 145.600                   | 128.250                   |
|     | 34              | 0.000                | 0.000                | 190.600 ±<br>293.550 ±    | 193.100 *<br>259.050 *    | 125.250 *<br>145.500 *    | 142.350<br>193.600        |
|     | 35              | 0.000                | 0.000                | 225.500                   | 221.850                   | 149.400                   | 151.250                   |
|     |                 |                      |                      |                           |                           |                           |                           |
|     |                 |                      |                      |                           |                           |                           |                           |
|     | COLUNI          |                      | C77                  | C78                       | C79                       |                           |                           |
|     | ROW             | 35                   | 35                   | 35                        | 35                        |                           |                           |
|     | 1               | 4.000                | 4.000                | 4.000                     | 4.000                     |                           |                           |
|     | 2               | spike 3.000          | 3.000                | 4.000.                    | 4.000                     |                           |                           |
|     | 3               | 1.000                | 2.000                | 1.000                     | 2.000                     |                           |                           |
| DNT | 4               | 176.300 *            | 176.900 *            | 38.200 *                  | 40.450 *                  |                           |                           |
| 01  | 5<br>6          | 86.400<br>94.600     | 85.800<br>89.000     | 50.850<br>51.350          | 47.700                    |                           |                           |
|     | 7               | 88.800               | 90.300               | 49.250                    | 55.250<br>53.900          |                           |                           |
|     | 8               | 79.000               | 106.950              | 64.450                    | 41.500                    |                           |                           |
|     | 9               | 84.300               | 85.200               | 47,500                    | 49.750                    |                           |                           |
|     | 10              | 59.900 *             | 99.800 *             | 26.650 *                  | 18.800 *                  |                           |                           |
|     | $\frac{11}{12}$ | <u>87.700</u>        | 87.650               | 50.400                    | 50.400                    |                           |                           |
| TNT | 13              | 206.450 *<br>100.600 | 2C2.350 *<br>102.250 | 23.500<br>35.500          | 25.000<br>33.550          |                           |                           |
|     | 14              | 101.300              | 116.650              | 34.250                    | 30.000                    |                           |                           |
|     | 15              | 106.200              | 108.200              | 38,450                    | 36.500                    |                           |                           |
|     | 16              | 112.050              | 130.950              | 47.000                    | 37.600                    |                           |                           |
|     | 17              | <b>\$1.700</b>       | 92.700               | 24.750                    | 29.700                    |                           |                           |
|     | 18<br>19        | 73.600               | 104.200<br>101.850   | 30.350<br>35.750          | 67.750<br>34.800          |                           |                           |
|     | 20              | 472.200 +            | 478.550 *            | 202.950                   | 188.600                   |                           |                           |
| RDX | 21              | 320.600              | 331.050              | 266.050                   | 227.850                   |                           |                           |
|     | 22              | 364.000              | 351.800              | 236.900                   | 246.900                   |                           |                           |
|     | 23              | 317.450              | 314.350              | 224.650                   | 226.000                   |                           |                           |
|     | 24              | 362.750 *            | 408.900 *            | 267.100 *                 | 310.000 *                 |                           |                           |
|     | 25<br>26        | 266.100<br>334.400   | 277.800              | 189.800                   | 187.850                   |                           |                           |
|     | 27              | 314,650              | 336.850<br>313.150   | 192.350                   | 212.800                   |                           |                           |
|     | 28              | 253.800 *            | 242.550 *            | 38.900                    | 42.950                    |                           |                           |
|     | 29              | 137.700              | 133.550              | 59,900                    | 57.750                    |                           |                           |
| hmx |                 | 157.550              | 183.450              | 48.000                    | 51.200                    |                           |                           |
| HMX | 30              |                      |                      |                           |                           |                           |                           |
| HMX | 31              | 146.500              | 138.500              | 61.950                    | 47.800                    |                           |                           |
| HMX | 31<br>32        | 146.500<br>156.650   | 138.500<br>130.400   | 77.000                    | 86.100                    |                           |                           |
| HMX | 31              | 146.500              | 138.500              |                           |                           |                           |                           |

# APPENDIX B: CHEMICAL STRUCTURES











Figure B5. SEX







Figure B4. 2, 4-DNT



Figure B6. TAX

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Figure B7. 2 Am-DNT.



Figure B9 7 6 DNT



Figure B8. 4 Am-DNT



Figure B10. 2, 4, 5-TN7



Figure B11. 2, 4-DAmNT



Figure B12. 2, 6-DAmNT

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Figure B15, Cyclohexanone

APPENDIX C: PROTOCOL FOR INTERLABORATORY STUDY OF A REVERSE PHASE HPLC METHOD FOR THE DETERMINATION OF 2, 4-DNT, TNT, RDX, AND HMX IN MUNITIONS WASTEWATER. (This appendix exactly reproduces the protocol sent to the participating laboratories.)

#### I. INTRODUCTION

### A. Objective

The goal of this study is to assess the capabilities of this HPLC method for the determination of 2,4-DNT, TNT, RDX and HMX\* in the wastewater from munitions manufacturing and processing facilities and in groundwater.

#### B. Overview

Reverse phase HPLC will be used to determine the levels of the four analytes in four natural and waste water samples, and in these samples spiked with various amounts of standards. Strict adherence to the analytical protocol is essential in order for the statistical analysis of results to provide unbiased estimates of method performance. Bias in the intralaboratory precision can lead to the conclusion that laboratories differ systematically when they really do not. For instance, bias is introduced by discarding selected results and repeating analyses on an arbitrary basis.

Careful attention to detail is necessary to assure proper evaluation of the capabilities of the method for two reasons. Participation in this study represents the investment of a large amount of time and money by the organizers and the participating laboratories. Furthermore, if this method develops into a national regulatory method, a biased evaluation has much greater financial implications than just the cost of this interlaboratory study.

#### **II.** PREPARATIONS

A. Analyst

One analyst will be selected by the lab manager to be responsible for all aspects of this study, including receipt of materials through data

<sup>\* 2,4-</sup>DNT: 2,4-dinitrotoluene, henceforth referred to simply as DNT TNT: 2,4,6-trinitrotoluene

RDX: 1,3,5-trinitro -1,3,5-triazacyclohexane

HMX: 1,3,5,7-tetranitro -1,3,5,7-tetraazacyclooctane

analysis. There are several places where unsolved problems may call a halt to the protocol and require contacting Tom Jenkins\* at CRREL. Further work cannot be performed until the problem is solved. The analyst, with the help of supervisors, should make reasonable attempts to resolve problems before calling.

#### B. Record Keeping

One notebook should be used exclusively for this study and should be labeled appropriately. Carbon or photo copies of notebook pages should be made. The original notebook must be submitted with the analytical report; the lab retains the copy. Complete documentation of experimental work and calculations is essential to help trace the sources of problems that may be discovered after data are returned to the coordinating laboratory.

C. Receipt of materials

The following materials will be shipped from CRREL:

Three 1-L bottles, each of which contains a different water sample typical of the sample type to which this method will be applied; shipped in ice water.

16 sealed glass ampules containing approximately 5 mL of mixed standards of the four analytes in methanol.

Two sealed glass ampules containing specified concentrations of the four analytes in methanol.

Two sealed glass ampules that are empty.

The following standard materials shipped from LCWSL:

Four vials of SARM\*\*: two each of DNT and TNT, 200 mg neat, and two each of RDX and HMX, 200 mg under isopropanol.

Arrangements should be made to notify the analyst immediately when these materials arrive. Upon receipt, the analyst will log each container into the project notebook. Each entry should contain identification number, name, date of arrival, and description of condition. Inspect each

<sup>\*(</sup>Commercial 603-646-4385, Autovon 684-4385, FTS 836-4385) \*\* Standard Analytical Reference Materials

container for damage. Broken, cracked, or leaking containers should be reported immediately to Tom Jenkins at CRREL, who will send replacements.

D. Storage of Materials

Water samples and ampules must be stored in the dark in a refrigerator or coldroom (temperature around 4°C, not below 0°C) immediately after receipt. The S/RMs should be stored in a freezer (< 0°C).

#### III. ANALYSIS

#### A. Overview

The analytical work will be performed in two steps. The analyst first will spend some time becoming familiar with the test procedure. During this period working curves for each of the four analytes will be prepared and steps will be taken to establish that they are linear and pass through the origin. Then a sample whose composition is specified (provided by CRREL) will be analyzed. This experience should help to uncover potential systematic errors and allow the analyst to correct the causes. If uncorrected, these errors could cause a laboratory's results to be excluded from the statistical analysis at the end of the study.

The second portion of the work consists of analysis of four water samples; three of these will be provided by CRREL and the fourth is to be the laboratory's own reagent-grade water (distilled or deionized). These samples represent a range of matrices to which the HPLC method being tested should be applicable. Some amount of the four analytes (DNT, TNT, RDX, HMX) may be present. These matrices will be analyzed directly and after spiking with standard analyte solutions. Four separate spiking experiments will be performed for each matrix.

#### B. Experimental

#### 1. Instrumentation

Chromatograph: The HPLC instrument should consist of a single high pressure pump and a 254-nm fixed wavelength ultraviolet absorption detector. If a fixed wavelength detector is not available, then a multiwavelength detector set to 254 nm may be used. A complete description of the instrument will be requested in the report.

Strip chart recorder: Full scale capacity should be compatible with the UV detector used. The trace is necessary to provide permanent record of experimental results. Computer storage of chromatograms is permissible if that is standard practice for the laboratory. These records should be retained by the participating laboratories unless requested by the coordinating laboratory. Integrator: Calculates peak areas; may be a stand-alone digital integrator or computer-controlled integrator; mechanical or analog integrators may not be substituted without authorization.

Sample loop injector: Nominal 100-µL volume; syringe injection of 100 µL into a larger loop is not permissible without authorization.

2. Operating Parameters

<u>Column</u>: LC8 (Supelco) reverse phase,  $25 \text{ cm} \times 4.6 \text{ mm}$ ; shipped from CRREL filled with methanol/water. Until this study has been completed, the column may not be used for any other purpose.

<u>Column temperature</u>: Room temperature; record hourly during analysis  $(\pm 1^{\circ}C)$ .

Solvent system: 50% water, 38% methanol, 12% acetonitrile by volume. Prepare using graduated cylinders, not volumetric flasks (because of solution contraction upon mixing). Prepare as a large batch (750 mL to 1000 mL), then vacuum filter through a solvent-washed  $0.4-\mu m$  Nuclepore filter to remove particulate matter and to degas the solvent. Fresh solvent should be prepared daily.

Flow rate: 1.5 mL/min.

Detector: 254 nm

Integrator: Threshold set low enough to avoid negative intercept in working curve and high enough to avoid positive intercept (see section III. E).

Recorder: 0.2 in./min chart speed

3. Hardware/glassware

HPLC syringe: Any liquid-tight syringe of capacity 0.5 to 1.0 mL (e.g. Hamilton 750).

Filtration device: Nuclepore syringe filter, 25 mm diameter.

Filter: (.4 µm Nuclepore polycarbonate, 25 mm diameter

Sample filtration syringe: 25 mL, glass or polyethylene (e.g. Plastipak; Becton, Dickinson and Co.; available through laboratory supply company; sterile -- no further cleaning necessary).

Volumetric flasks and pipets: Glass, class A or B; make sure condition is good (e.g. pipet tips not broken).

Scintillation vials: 20-mL glass with polyethylene cap insert (not aluminum); can be purchased from laboratory supply company (sterile; no further cleaning necessary).

<u>Cleaning of volumetric glassware</u>: Soak overnight in detergent, scrub briefly, rinse well with hot tap water, rinse with reagent-grade acetone, rinse with deionized water, oven dry at 105°C; rinse with appropriate solution before filling.

Reagents: Water, methanol, acetonitrile -- all HPLC grade.

Methanol-acetonitrile mixture: A solution consisting of 76% methanol and 24% acetonitrile is prepared and used throughout this method as a diluent for all water samples. This mixture is prepared using graduated cylinders rather than volumetric flasks to minimize systematic differences with the mobile phase because of volume contraction. Dilution with this mixture, rather than methanol alone, eliminates a negative peak which elutes just prior to HMX and results in unpredictable integration.

#### C. Calibration Standards

1. Individual Stock Standards for DNT, TNT, RDX, and HMX. These solutions must be used for the entire study.

For each material:

a. Vacuum dry SARMs at ambient temperature to constant weight (within 1 mg); a vacuum desiccator or vacuum oven attached to a water aspirator or vacuum pump will suffice. For RDX and HMX, remove most of the isopropanol by means of a Pasteur pipet, air dry for several hours, then vacuum dry. Store dried SARMs in a desiccator over dry calcium chloride or Drierite and place in the dark when not in use.

b. Accurately weigh about 0.1 g of each dried SARM onto weighing paper (e.g. VWR or Fisher-brand "Weighing Paper"); transfer carefully into separate 250-mL volumetric flasks. Reweigh weighing paper. Record mass to 0.1 mg.

c. For DNT and TNT dissolve and dilute to volume with methanol. For HMX and RDX, add 100 mL of acetonitrile to dissolve, then fill to volume with methanol.

d. Wrap the stoppered joint with Parafilm. This is an added protection against evaporation.

e. Calculate concentrations exactly in mg/L and label flasks.

f. Store in refrigerator at about 4°C (not below 0°C).

2. Combined-Analyte Working Stock Standard

a. Remove the stock standards from the refrigerator and allow to warm to room temperature (at least 30 min, but not overnight).

b. Invert flasks several times to mix.

c. Into a 1000-mL volumetric flask, pipet 10.0 mL each of DNT and TNT stock solutions and 25.0 mL each of RDX and HMX stock solutions. Dilute to volume with methanol. This standard will be about 4.0 mg/L in DNT and TNT and 10.0 mg/L in RDX and HMX.

d. Calculate the concentrations exactly in mg/L, label the flask, and date it.

e. Wrap the stoppered joint with Parafilm and store the flask in refrigerator when not in use. This standard may be used for one week from the date of preparation and then a fresh one must be prepared.

3. Working Standards

a. To be prepared fresh on each analysis day as instructed.

b. Remove the combined-analyte working stock standard from the refrigerator and allow to warm to room temperature (at least 30 min, but not overnight).

c. Invert flask several times to mix.

d. Transfer 2.00, 5.00, 10.00 and 20.0 mL by pipet into four 250-mL volumetric flasks, respectively.

e. Fill to mark with methanol/acetonitrile mixture. Stopper and invert ten times to mix.

f. Calculate the concentrations exactly in  $\mu g/L$ , label the flasks and date them.

4. Injected Standards

a. For each standard, pipet 10.0 mL into a scintillation vial.

b. Add 10.0 mL of HPLC grade water by means of a pipet.

c. Affix cap and shake to mix.

d. Prepare blank by combining 10.0 mL of methanol/acetonitrile mixture with 10.0 mL of water in vial. Affix cap and mix.

e. Label all vials appropriately.

The solutions that result represent the following concentrations in a 10.0-mL aqueous sample:

| Aliquot volume of      | Approximate concentrations (µg/L) |                 |  |  |
|------------------------|-----------------------------------|-----------------|--|--|
| combined standard (mL) | For DNT and TNT                   | For RDX and HMX |  |  |
| 2                      | 32                                | 80              |  |  |
| 5                      | 80                                | 200             |  |  |
| 10                     | 160                               | 400             |  |  |
| 20                     | 320                               | 800             |  |  |

Note that these values represent the concentrations before addition of the water. (The actual concentrations are half as large.) This can be done because the samples are treated similarly: a one-to-one dilution is made by adding 10.0 mL of methanol/acetonitrile mixture to 10.0 mL of aqueous sample. Thus, the analytical results derived from the working curve need not be corrected for this extra dilution.

The 10.0 mL methanol-acetonitrile/10.0 mL water mixtures are made in scintillation vials rather than in volumetric flasks because a slight volume contraction occurs. This might cause a systematic error because the standards would be diluted with water to volume and the samples diluted with the organic solvent to volume. Volume contraction therefore would lead to the samples being slightly richer in the organic solvent than the standards. Care must be taken in this step to pipet these 10-mL volumes accurately since experience has indicated that a significant error at this stage is compounded when peak areas are measured.

#### D. HPLC Procedure

#### 1. Initial Conditioning

The HPLC column is new. Consequently, conditioning with the mobile phase and a test of performance are required before putting the column to work. This test may be performed the same day as the preliminary experiments (see Section III. E) but must be performed first.

a. Conditioning: Pollow the procedure below (section III. D.2) for instrument warm-up, except pass at least 30 void volumes (about 60 mL) of mobile phase through the column. Continue until the UV detector baseline is level when set to its greatest sensitivity.

b. Performance test (calculation of plate number).

(1) Take a 1-mL aliquot from the combined-analyte working stock standard and dilute to 100 mL in a volumetric flask with mathanol/acetonitrile.

(2) Use the proper sample injection procedure described in section III.D.3 below to obtain a chromatogram. All four analytes should elute within 10 minutes. Use the conditions described in section III.B.2 above, but select a chart speed that spreads the peaks out abnormally wide (such that widths at half height are at least 2.0 cm). Measure the peak width at half height to the closest millimetre.

(3) Calculate the number of plates (N) on the column from each peak using the equation

$$N = 5.54 \left(\frac{t_{r}}{t_{0.5}}\right)^{2}$$

where  $t_r$  is the retention time and  $t_{0.5}$  is the width of the peak at half height, both in minutes.

(4) Average the results for all four analytes.

(5) If the average value is less than 3,000 plates, carefully recheck the calculation. If there is no error, allow another 30 void volumes of mobile phase to wash through the column and repeat the experiment. If the calculated value of N still does not exceed 3,000, the column is not performing up to its specification. If used it may invalidate results from this laboratory. Notify Tom Jenkins at CRREL immediately if this occurs. 

#### 2. Normal Warm-Up Procedure

a. Turn on all electronic equipment and allow to warm-up for at least 30 min.

b. Pass at least 15 void volumes of mobile phase through the column (20 min at 1.5 mL/min) and continue until the UV detector baseline is level when set to its greatest sensitivity.

c. Make certain the pumps are not experiencing vapor lock as indicated by large pressure fluctuations.

d. Check system thoroughly for leaks.

3. Sample Injection Procedure

a. Fill the analytical syringe with methanol/acetonitrile and discharge into a waste beaker.

b. Repeat twice more to remove traces of previous sample.

c. Rinse syringe three times with the sample.

d. Fill syringe with sample to at least 500  $\mu$ L and inject most of this through sample loop, avoid introducing air bubbles. Overfilling the loop in this manner assures that the sample injected is not diluted by solvent in the loop.

#### E. Preliminary Experiments

Before beginning the analyses of the water samples, the analyst should become familiar with the analytical procedure. For this purpose an ampule containing the four analytes has been included as a test sample. This sample should be prepared by transferring a 1.00-mL aliquot of the ampule solution using a volumetric pipet into a 100-mL volumetric flask and diluting to volume with methanol/acetonitrile. This solution may be used up to three days after preparation. A 10.0-mL aliquot of this solution is transferred to a scintillation vial and 10.0 mL of HPLC-grade water is added. Cap tightly and shake.

Test HPLC column plate number specification, if not already done (see section III.D.1). Otherwise, follow the instrument warm-up and column conditioning instructions (see section II.D.2).

Prepare the working standards and blank as specified in sections III.C.3 and III.C.4. Using the procedure described in section III.D.3, inject each standard and blank into the HPLC at least once. Ascertain the detector range that provides sizeable but on-scale peaks so that a good chromatographic record results. Make certain that integration is occurring properly.

Next proceed as if the test material were a real sample to be analyzed.

1. Carefully prepare working curves for the four analytes (see section 4 below). These curves will be the basis of all of the remaining quantitative work; consequently, it is essential that systematic errors be avoided.

2. Carry the test sample through filtration (see section III.F.5 steps c to e) and analysis (see section III.D.3) at least three times and as many more times as is necessary to become accustomed to the procedure.

3. From the last two injections of test sample, determine the concentrations of all four analytes in the test sample using the working curves. Compare results with the specified values. The mean determined values should be within 15% of the specified values. If not, attempt to resolve discrepancies and then process another 10-mL aliquot of the solution in the 1-L flask. If all four analytes are within 15% of the specified values, proceed to section F; if not\_contact Tom Jenkins.

#### Construction of Working Curve

a. Obtain chromatograms of the four working standards and blank in duplicate (10 injections total). Sequence the injections randomly (see Appendix A).

b. Plot peak area versus concentration for each of the four analytes. Do not average the duplicates before plotting. Inspect the plot for gross deviations from linearity -- a set of duplicates wildly off line, or a large degree of curvature. Preliminary work has demonstrated that the analytical response is linear from 10 ug/L to 20 mg/L for DNT and TNT and 25 ug/L to 50 mg/L for RDX and HMX. Significant deviation from linearity is evidence for systematic bias. Whereas it is possible to make analytical determinations with a nonlinear working curve, it is preferable that the systematic error be found and corrected before beginning the interlaboratory test measurements. Once gross errors have been corrected and the plot looks reasonably linear, more rigorous statistical tests must be applied. (If obvious curvature still exists and you have the appropriate computational facilities, inspect the residuals as an aid in diagnosing the problem; otherwise, contact Tom Jenkins).

c. Calculate the regression analysis tables for each analyte using both the model through the origin and the model with an intercept (see Appendix B).

d. Test the model with an intercept for lack of fit for each analyte (see Appendix B). (Comparison of correlation coefficients alone is insufficient.)

- If a significant lack of fit exists for any of the analytes, plot the regression line on top of the data points. Inspect for wild points or curvature. (If you have the appropriate computational facilities, inspect the regression residuals.) Try to resolve the source of nonlinearity. If the problem cannot be resolved, contact Tom Jenkins.

e. Test the hypothesis that the intercept equals zero (see Appendix B).

- It is highly desirable to achieve a calibration that has a zero intercept because this simplifies the daily calibration routine. Thus for daily analysis instead of constructing a complete working curve, it is necessary only to run several replicates of the most concentrated standard.
- If it is found that an intercept is not zero, the most likely reason is that the integrator "zero" has been set too high (negative intercept) or too low (positive intercept). Adjust the integrator and repeat steps a through d. If this repetition fails to provide zero intercepts, search for other

causes. If the problem cannot be resolved, contact lom Jenkins.

F. Analysis of Water Samples

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For each of the four water samples, all of the analyses must be performed on a single day. The sequence in which the matrices must be analyzed is given in Appendix C. Analysis of duplicates is an important part of this study. Sometimes duplicates will appear to be quite different in their response and there will be a strong inclination to discard a response and obtain a new one. Please do not do so, unless there is certainty that a systematic error has been made. Rejection of such data tends to make the within-lab reproducibility artificially good. This increases the sensitivity of statistical tests for differences between laboratories. Thus, significant differences may be found where no differences actually exist.

- Remove matrix and its corresponding four ampules and the combined-analyte working stock standard from refrigerator and allow to warm to room temperature (at least 30 min., but not overnight). Note that the ampules are keyed to be used with a specific matrix (e.g., ampules Al through A4 go with matrix A).
- 2. Warm up instrument and condition HPLC column (see section III.D.2).
- 3. Calibration

If linear working curves with zero intercepts were obtained during the preliminary experiments, daily calibration only requires analysis of the most concentrated working standard. Proceed as follows:

a. Prepare the most concentrated working standard from the combined-analyte stock standard (see section III.C.3).

b. Prepare one vial of this standard for injection (see section III.C.4  $\underline{a}$  to  $\underline{c}$  and  $\underline{e}$ ). Keep this vial tightly capped when not in use.

c. Obtain chromacograms of this standard in triplicate (see section III.D.3).

d. Calculate the mean and standard deviation of the peak areas for each of the four constituents.

e. For each analyte, compare this mean with the response expected from the working curves already established (see Appendix D).

f. If the test indicates no differences for any of the analytes, skip to instruction 4.

g. If the test is significant for any of the analytes, there may be a systematic preparation error, or instrumental response has drifted. To distinguish between these possibilities, carefully repeat steps a through e.

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h. If the tests against the working curves (Appendix D) still indicate significant difference, test for equivalence between the two sets of triplicates run today (see Appendix E).

1. If the test in  $\underline{h}$  indicates no difference, skip to instruction 4.

j. If the test in h indicates significant difference, either the instrument is subject to strong short term drift or noise or there is insufficient reproducibility in the analyst's technique of solution preparation. Call Tom Jenkins before proceeding further.

4. Proceeding one ampule at a time (to avoid solvent evaporation):

a. Open ampule carefully by filing and breaking at neck.

b. Transfer entire contents of ampule (about 5 mL) into a scintillation vial. Immediately pipet 1.00 mL of this solution into a 100-mL volumetric flask. Fill to volume with the water sample. Invert 10 times to mix. This solution will be referred to as the "spiked sample."

c. Label this flask, indicating the ID number of the ampule from which the solution came.

d. Repeat steps a through c for the other three ampules.

e. Prepare the unspiked sample by repeating steps b and c, except begin with 1.00 mL of methanol instead of ampule solution.

5. Five solutions in 100-mL volumetrics are in hand. From each solution, two 10.0-mL aliquots will be taken, processed as below, and injected in duplicate into the HPLC instrument. In addition, the standard prepared in step <u>3b</u> above will be injected five times. Consequently, a total of 25 injections will be made. The sequence of processing and injection must be randomized. Determine the order of injection of samples (see Appendix F). Then proceed through the following steps:

a. When the injection sequence calls for injection of standard or for the second injection of a sample, skip to step f.

b. Pipet 10.0 mL of the sample from its 100-mL volumetric flask into a scintillation vial. Add 10.0 mL of methanol/acetonitrile solution by pipet. Attach cap tightly. Shake vigorously. Let stand for at least 15 minutes before filtration (during this waiting period, the next samples in the sequence should be processed to avoid losing time later). The organic solvent is added for two reasons: (1) to help desorb analyte from the surfaces of particulates and dissolve small particles of analyte that could be present, and (2) to provide a sample compatible with the HPLC mobile phase.

c. Load new Nuclepore filter into filter holder.

d. Rinse 25-mL filtration syringe with methanol/acetonitrile solution then fill to about 10 mL with sample. Filter sample and discard this filtrate.

e. Fill syringe with remaining sample. Filter into a new scintillation vial. This solution will be analyzed. Label vial appropriately.

f. Using proper procedure (see section III.D.3), inject this solution into the HPLC.

g. Repeat steps a through f for each sample in the proper sequence.

- G. Data Analysis
  - 1. Determine working curves for each of the four analytes: a. Calculate the mean peak area  $(\overline{y})$  for the five replicates of the standard.

b. Solve the equation  $\overline{y}/x_{\rm HI} = b_1$  where  $x_{\rm HI}$  is the known concentration of the highest standard and  $b_1$  is the slope of the working curve.

- 2. Substitute the value for the slope into the working curve equation  $y = b_1 x$ . Calculate the concentrations (x) for the 20 injections of spiked and unspiked water samples using individual peak areas (y).
- H. Reporting of Results

An example of the format for reporting results is given in Appendix G.

#### APPENDIX A

# Random Injection Sequence for Working Curve

The samples consist of a blank and four standards, each of which will be injected in duplicate (1 and 2). The sequence of injection of these 10 trials must be random. Use computer generated random numbers, random number tables, or pull slips of paper numbered 1 to 10 from a hat. Record the resulting sequence in the following table and in the notebook, then use this table to keep track of the order of injections.

#### Standard Concentration

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| nominal) |   |   |
|----------|---|---|
| RDX, HMX | Replicate   | Sequence  |
|          |   |   |
| 0        | 1   |   |
| 0        | 2   |   |
| 80       | 1   |   |
| 80       | 2   |   |
| 200      | 1   |   |
| 200      | 2   |   |
| 400      | 1   |   |
| 400      | 2   |   |
| 800      | 1   |   |
| 800      | 2   |   |
|          | RDX,HMX<br>0<br>0<br>80<br>80<br>200<br>200<br>200<br>400<br>400<br>800 | RDX, HMXReplicate010280180220012002400140028001 |

#### APPENDIX B

#### Regression Analysis\*

Previous testing has demonstrated (see section III.E for details) that chromatographic peak area (y) should be a linear function of analyte concentration (x). Two models may be tested, the model through the origin:  $y = b_1x$ , and the model with an intercept:  $y = b_0 + b_1x$ . The coefficients for these models can be calculated as follows:

For model through origin:

$$b_1 = \frac{\Sigma x y}{\Sigma x^2}$$
  $b_0 = 0$ 

For model with intercept:

$$b_1 = \frac{\sum xy - \frac{\sum x \sum y}{n}}{\sum x^2 - \frac{(\sum x)^2}{n}}$$

$$b_0 = \overline{y} - b_1 \overline{x}$$

where  $\overline{y}$  and  $\overline{x}$  represent respective mean values, a is the number of data points, and y is the value of y predicted by the regression equation.\*\*

Regression analysis tables are used to determine whether the data fit the linear models well enough and which linear model is more applicable. The tables must be calculated as follows:

#### Table for Model with Intercept

|                      | Sum of squares<br>(SS)  | Degrees of<br>freedom<br>(df) | Mean<br>square<br>(MS) | F-ratio<br>(F)     |
|----------------------|---|-------------------------------|------------------------|--------------------|
| Residual             | $\Sigma y^{2} - \frac{(\Sigma y)^{2}}{n} - b_{1}^{2} \Sigma x^{2} - \frac{(\Sigma x)^{2}}{n}$ | 6                             | resid. SS<br>6         |                    |
| Error                | $\frac{\Sigma d^2}{2}$  | 4                             | SS error<br>4          |                    |
| Lack of fit<br>(LOF) | Residual SS - Error SS  | 2                             | SS LOF                 | MS LOF<br>MS error |

\*Do not round off intermediate numbers in calculations. Carry through at least six digits to avoid round off errors, even though in the final results less than six digits will be significant.

\*\*The two replicate analyses of the blank (zero sualyte) are not used to obtain regression equations.

where n is the number of data points and d is the difference between the peak areas of duplicates. For the model through the origin, the table is:

|                      | Sum of squares<br>(SS)                           | Degrees of<br>freedom<br>(df) | Mean<br>square<br>(MS) | F-ratio<br>(F)     |
|----------------------|--|-------------------------------|------------------------|--------------------|
| Residual             | $\Sigma y^2 - \frac{(\Sigma x y)^2}{\Sigma x^2}$ | 7                             | resid. SS<br>7         |                    |
| Error                | $\frac{\Sigma d^2}{2}$                           | 4                             | <u>SS error</u><br>4   |                    |
| Lack of fit<br>(LOF) | Residual SS - Error SS                           | 3                             | SS LOF                 | MS LOF<br>MS error |

# Table for Model through Origin

Test for lack of fit: For the model with an intercept, the critical value is  $F_{.95}(2,4) = 6.94$ . If the F-ratio calculated in the right-hand column of the regression analysis table exceeds the critical value, there is a significant lack of fit; i.e., the working curve is not linear. Steps as suggested in the text must be taken to correct this problem. If the calculated value is less than 6.94, the linear model is satisfactory. It is not necessary to test the model through the origin.

After establishing linearity, the intercept must be tested to determine whether it is significantly different from zero. Calculate the F ratio:

## F= (resid. SS for model through origin)-(resid. SS of model with intercept) (residual SS of model with intercept) 6

where the 'residual SS" are in the tables. This can be done only after LOF has been shown to be insignificant. The critical value is  $F_{.95}$  (1,6) = 5.99. If the calculated value exceeds the critical value, the intercept is significantly different from zero. Steps as suggested in the text must be taken to correct this problem. If the problem cannot be resolved, contact Tom Jenkins. If the calculated value is less than 5.99, the intercept is zero.

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#### APPENDIX C

Determination of Chronological Order for Water Sample Analyses

Four water matrices are to be analyzed: three are provided by CRREL (A,B,C) and the fourth must be the participating laboratory's distilled or deionized water supply (D). Randomly select the sequence in which these four samples must be studied by means of computer-generated random numbers, random number tables, or pulling slips of paper numbers 1 to 4 out of a hat.

#### APPENDIX D

Daily check of instrument calibration is achieved by measuring the detector responses for the four analytes in the most concentrated standard. This is performed before beginning the analysis of a number of samples.

The statistical test is based on comparing the mean of triplicate peak area measurements of the standard with the confidence intervals around the working curve which was established during the preliminary experiments. The equations used to perform the comparison are as follows:

$$s_{yp} = \frac{(n_{wc} - 1) s_{wc}^{2} + (n - 1) s^{2}}{(n_{wc} - 1) + (n - 1)}$$
(1)

$$PI = y_{HI} \pm t_{CRIT} + \frac{x_{HI}^2}{\Sigma x^2} \Big)^{1/2}$$
(2)

$$t_{CRIT} = t_{.95} (df = 9) = 2.26$$
 (3)

where

- n = 3, the number of data points in set to be compared with working curve
- n<sub>WC</sub> = 8, the number of measurements used to calculate working curve
  - s = standard deviation of triplicates
- swc = square root of residual mean square from regression analysis
  table for model-through-origin,
- $s_{vp}$  = pooled standard deviation
- **PI** = prediction interval
- $y_{HT}$  = peak area predicted for high standard by working curve
- $x_{HT}$  = known concentration of high standard
- $\Sigma x^2$  = summation over all of the standard concentrations squared (remember that each is used twice; value should be about 1,692,800 for HMX)
- df = degrees of freedom, equals 9; 7 for working curve, 2 for

Notes on use:

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a. Standard deviations of triplicates are most easily calculated by means of:

s = 
$$\left(\frac{\sum y^2 - \frac{(\sum y)^2}{n}}{n-1}\right)^{1/2}$$

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b. Example:

(1) Given: slope = 2.5 concentration = 800 µg/L HMX

s<sub>wc</sub> = 20

 $y_{HI} = 2.5 \times 800 = 2000.$ 

(2) At start of day, 3 replicates are run. Mean area is  $\overline{y} = 1960$  with s = 7.

(3) Use equation 1:

$$s_{yp} = \left(\frac{7(20)^2 + 2(7)^2}{7 + 2}\right)^{1/2} = 17.944$$

(4) Use equation 2:

PI = 2000 ± 2.26(17.944) 
$$\left(\frac{1}{3} + \frac{800^2}{1,692,800}\right)^{1/2}$$

Thus  $PI = 2000 \pm 34.2 = [1965.8 - 2034.2]$ 

(5) Is the mean of the triplicates within the PI? No, since prediction interval is [1965.8 - 2034.2] and  $\overline{y}$  = 1960 is outside interval.

# APPENDIX E

# Comparison of Two Sets of Triplicate Standards

Use the following equations:

$$S_{yp} = \sqrt{s_1^2 + s_2^2}$$
 (1)

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$$t = \frac{(n)^{1/2} |\overline{y}_1 - \overline{y}_2|}{(2)^{1/2} s_{yp}}$$
(2)

$$t_{05} (df = 4) = 2.78$$
 (3)

where

 $\overline{y}_1$  and  $\overline{y}_2$  = means of the two sets of triplicates s<sub>1</sub> and s<sub>2</sub> = corresponding standard deviations n = 3

if t < t.95, then the hypothesis that  $\overline{y}_1 = \overline{y}_2$  is accepted.

#### APPENDIX F

Random Injection Sequence for Analyses of Spiked Water Matrices

The solutions to be analyzed on a given day consist of: a pair of unspiked samples, four pairs of spiked samples, each pair spiked from a different ampule, and a high-concentration standard. The water samples will be injected twice each into the HPLC; the standard, five times. The sequence of 20 sample injections for each water matrix must be random with the standards being injected at fixed points in this sequence (see table below). Use computer generated random numbers, random number tables, or pull slips of paper number 1 to 20 out of a hat. Record the results in table below, and also in the notebook. Repeat the random selection procedure for each matrix.

| •                  |                | Sequence                            |
|--------------------|----------------|-------------------------------------|
| Sample             | Replicate      | Matrix A Matrix B Martix C Martix D |
| Standard           | $\overline{1}$ | First                               |
| Standard           | 2              | between 5th and 6th positions       |
| Standard           | 3              | between 10th and 11th positions     |
| Standard           | 4              | between 15th and 16th positions     |
| Standard           | 5              | Last                                |
| lst vial, unspiked | 1              |                                     |
| · ·                | 2              |                                     |
| 2nd vial, unspiked | 1              |                                     |
|                    | 2              |                                     |
| lst vial, spike l  | 1              |                                     |
|                    | 2              |                                     |
| 2nd "ial, spike 1  | 1              |                                     |
|                    | 2              |                                     |
| lst vial, spike 2  | 1              |                                     |
|                    | 2              |                                     |
| 2nd vial, spike 2  | 1              |                                     |
|                    | 2              |                                     |
| lst vial, spike 3  | 1              |                                     |
|                    | 2              |                                     |
| 2nd vial, spike 3  | 1              |                                     |
|                    | 2              |                                     |
| lst vial, spike 4  | 1              |                                     |
|                    | 2              |                                     |
| 2nd vial, spike 4  | 1              |                                     |
|                    | 2              |                                     |

### APPENDIX G Format of Final Report

FINAL REPORT on HPLC Determination of Ordinance Materials in Water

Sponsor Laboratory: USACRREL

Participating Laboratory:

Laboratory Manager: Analyst:

Checklist of items to be included in report:

laboratory manager's profile of analyst

original project notebook

complete capcription of HPLC instrument and integrator

**Preliminary Experiments** 

A. Plate count of HPLC column:

B. Masses of SARM solid taken for stock standards:

| DNT | <br>g |
|-----|-------|
| TNT | <br>8 |
| RDX | <br>8 |
| HMX | g     |

C. Working curves, in the form: (area) =  $b_1$  (concentration)

DNT: TNT: RDX: HMX:

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D. Analysis of test sample composition; do not correct for 1000-fold dilution; report as  $\mu g/L$ 

DNT: TNT: RDX: HMX:

E. Retention times of analytes in test sample (min) DNT: TNT: RDX: HMX:

| Analytical Results<br>Matrix Type: | Date of             | Analys | is:      |            |                |         |            |
|------------------------------------|---------------------|--------|----------|------------|----------------|---------|------------|
|                                    |                     | DNT    | 1        | INT        | RDX            |         | MX         |
| Working Curve Slopes               |                     |        |          |            |                |         |            |
| Sample Analyses:                   | Replicate<br>number |        | Determin | <u>ned</u> | Concentrations | ( µg/L) | <u>)</u> * |
| unspiked matrix, vial l            | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| unspiked matrix, vial 2            | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 1, vial l                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 2, vial 2                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 2, vial l                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 2, vial 2                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 3, vial l                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 3, vial 2                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 4, vial l                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |
| spike 4, vial 2                    | 1                   |        |          |            |                |         |            |
|                                    | 2                   |        |          |            |                |         |            |

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Jenkins, T.F.

Reverse phase HPLC method for analysis of TNT, RDX, HMX and 2,4-DNT in munitions wastewater / by T.F. Jenkins, C.F. Bauer, D.C. Leggett and C.L. Grant. Hanover, N.H.: Cold Regions Research and Engineering Laboratory; Springfield, Va.: available from National Technical Information Service, 1984.

ix, 106 p., illus.; 28 cm. (CRREL Report 84-29.) Bibliography: p. 36.

1. DNT. 2. Explosives. 3. HMX. 4. Interlaboratory test. 5. RDX. 6. Statistical tests. 7. Test and evaluation. 8. TNT. 8. Water pollution control. I. Bauer, C.F. II. Leggett, D.C. III. Grant, G.L. IV. United States. Army. Corps of Engineers. V. Cold Regions Research and Engineering Laboratory, Hanover, N.H. VI. Series: CRREL Report 84-29.