



NATIONAL BUREAU OF STANDARDS

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	MERRIMACK RIVER BASIN
	HOLDEN, MASSACHUSETTS
	QUINAPOXET RESERVOIR DAM
	MA 00929
	PHASE I INSPECTION REPORT
NAT	IONAL DAM INSPECTION PROGRAM
	JUN 2 7 1985
NEW F	DEPARTMENT OF THE ARMY ENGLAND DIVISION, CORPS OF ENGINEERS WALTHAM, MASS. 02154
	SEPTEMBER 1980
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DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION, CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02254

REPLY TO ATTENTION OF:

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OCT 2 8 1930

Honorable Edward J. King Governor of the Commonwealth of Massachusetts State House Boston, Massachusetts 02133

Dear Governor King:

Inclosed is a copy of the Quinapoxet Reservoir Dam - MA-00929 Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Department of Environmental Quality Engineering, the cooperating agency for the Commonwealth of Massachusetts. In addition, a copy of the report has also been furnished the owner, the City of Worcester.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Department of Environmental Quality Engineering for your cooperation in carrying out this program.

Sincerely,

Incl As stated

Colonel, Corps of Engineers
 Division Engineer

QUINAPOXET RESERVOIR DAM MA 00929

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MERRIMACK RIVER BASIN HOLDEN, MASSACHUSETTS

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Identification: MA 00929 Name of Dam: QUINAPOXET RESERVOIR DAM Town: TOWN OF HOLDEN County and State: WORCESTER COUNTY Stream: QUINAPOXET RIVER Date of Inspection: 29 MAY 1980

BRIEF ASSESSMENT

Quinapoxet Reservoir Dam is approximately 1,050 feet long including the spillway and has a maximum height of approximately 45 feet. It consists of an earth embankment with riprap wave protection at the upstream face and a loamed and seeded crest and downstream face. The outlet works sluice gate operator stand is near the center of the dam and the spillway is near the right abutment of the dam. A low earth dike, approximately 370 ft. long, is located about 1,000 ft. south of dam.

The facility is considered to be in good condition. Evidence of minor seepage was observed on the downstream slope of the dam adjacent to the left wall of the spillway discharge channel.

Based on the size classification, intermediate, and hazard potential classiffcation, high, in accordance with Corps of Engineers Guidelines, the spillway test flood is the Probable Maximum Flood. Hydraulic analyses indicate that the routed test flood outflow of 12,000 cfs (inflow 12,900 cfs or 650 csm) could be passed with a freeboard of about 2.5 ft. and an unused surcharge-storage of about 785 acre-ft. remaining. The principal spillway capacity with water at top of dam is about 175 percent of the routed test flood outflow.

An investigation is recommended to evaluate the significance of the observed evidence of seepage relative to long-term embankment stability. Recommended remedial measures include the removal of brush from the dam and dike, the restoration and periodic reading of the existing piezometers, the replacement of a flashboard brace, the repairs of a wall joint and the resealing of other wall joints. The Owner should develop a formal maintenance program, operational procedure, and emergency procedures plan and should institute a program of biennial technical inspections. The remedial measures and recommendations should be performed as discussed in Section 7 within two years of receipt of this report by the Owner.

CAMP DRESSER & MCKEE INC.

(Roge, N. Wood

Roget H. Wood Vice President

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This Phase I Inspection Report on Quinapoxet Reservoir Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the <u>Recommended Guidelines for Safety Inspection of</u> <u>Dams</u>, and with good engineering judgment and practice, and is hereby submitted for approval.

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RICHARD DIBUONO, MEMBER Water Control Branch Engineering Division

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ARAMAST MAHTESIAN, MEMBER Geotechnical Engineering Branch Engineering Division

CARNEY M. TERZIAN, CHAIRMAN Design Branch Engineering Division

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APPROVAL RECOMMENDED:

OE B. FRYAR

Chief, Engineering Division

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I Investigations are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the test flood is based on the estimated "probable maximum flood" for the region (greatest reasonably possible storm runoff), or a fraction thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential. TABLE OF CONTENTS

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1. OVERVIEW OF DAM FROM RIGHT ABUTMENT.



2. PROJECT PLAQUE.



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

QUINAPOXET RESERVOIR DAM MA 00929

1.1 General

a. <u>Authority</u> - Public Law 92-367, 8 August 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region.

Camp Dresser & McKee Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Massachusetts. Authorization and notice to proceed was issued to Camp Dresser & McKee Inc. under a letter of 27 March 1979, from Colonel John P. Chandler, Corps of Engineers. Contract No. DACW 33-79-C-0053 has been assigned by the Corps of Engineers for this work. Contract Modification No. P0003, effective 2 May 1980 was subsequently issued by Colonel William E. Hodgson, Jr., Corps of Engineers. Haley and Aldrich, Inc. has been retained by Camp Dresser & McKee Inc. for the soils and geological portions of the work.

- b. <u>Purpose</u> The primary purpose of the investigation is to:
 - Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
 - (2) Encourage and assist the States to initiate quickly effective dam safety programs for non-Federal dams.
 - (3) Update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location - Quinapoxet Reservoir Dam is located on the west side of Princeton Street in the Town of Holden, Massachusetts, as shown on the report's Location Map. The northern half of the reservoir is located in the Town of Princeton, Massachusetts. The dam impounds the waters of South Wachusett Brook to form Quinapoxet Reservoir. The Quinapoxet River flows from the dam to the Wachusett Reservoir, a distance of approximately 7 miles. The coordinates for the dam are 71 degrees-52.8 minutes longitude and 42 degrees-23.3 minutes latitude.

SECTION 6: STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

- a. <u>Visual Observations</u> No evidence of spillway or embankment instability was observed during the site examination. The apparent local seepage is not, at this time, considered significant with respect to embankment stability.
- b. <u>Design and Construction Data Available documents include:</u>
 - "Memorandum on Design of Dam Section" which summarizes stability and seepage analyses;
 - 2) Plans and Specifications;
 - 3) Construction Progress Reports;
 - 4) a "Final Report" summarizing design and construction.

Based on a review of these records, it is considered that the spillway and embankments should have an adequate margin of safety under static conditions.

- c. <u>Operating Records</u> There are no known operating records, other than State and County inspection reports, to aid in evaluation of the stability of the facility. These reports give no indication of any instability.
- d. <u>Post Construction Changes</u> The original facility was modified by the addition of a stone jetty and reconstruction of the spillway flashboards in 1977. This construction is not considered significant relative to the stability of the facility. Also, the piezometers shown on the plans have apparently been cut off or covered.
- e. <u>Seismic Stability</u> Quinapoxet Reservoir is located within Seismic Zone 2 (a moderate risk area) and in accordance with recommended Corps of Engineers Guidelines, does not warrant seismic analysis.

Dam Failure Analysis - Based on the Corps of Engineers Guidelines f. for estimating Dam Failure Hydrographs, and assuming a failure would occur along 40 percent of the mid-height length with water at test flood stage, the dam failure outflow would be approximately 89,500 cfs. The project discharge prior to failure would be 12,000 cfs for a combined dam failure outflow of approximately 101,500 cfs. Flooding downstream of the dam prior to a dam failure due to the 12,000 cfs project discharge would overtop each roadway between the dam and Wachusett Reservoir by 1.5-ft. to 4-ft. depth. One house at State Route 31 would be flooded to about 2-ft. above its sill. As a result of a dam failure, substantial domestic development, including several roadways, would be affected with a resulting "high" hazard. In the area between the dam and State Route 31, Princeton Street and Mill Street would be overtopped by about 13 to 15 ft. One house near Princeton Street would be affected by about 4 ft. of water. About 22 houses would be affected near the Route 31 area. In the area around Wachusett River Street which is located about 3,000 ft. downstream of Route 31, another 14 houses would be affected. The street would be overtopped by about 25 ft. of water. Downstream of Wachusett River Street, one railroad embankment and another roadway would be affected before the flood wave would reach the Thomas Basin of the Wachusett Reservoir where the flood wave would attenuate.

is pumped about 2.5 miles from Quinapoxet Reservoir to Kendall **Reservoir.** The pumps are actuated manually based on water demand and water levels at other reservoirs within the City of Worcester's water supply system. An examination of available records indicated that the highest reservoir level was 0.7 ft. above spillway crest flashboards (El. 733.7 NGVD) on 23 March 1972 as a result of a total of 1.35 inches of rainfall in three days. On 24 January 1979 the reservoir level reached El. 733.5 or 0.5 ft. above spillway crest flashboards, as a result of 6.81 inches of rainfall in seven days. It was noted that about 15 to 25 MGD was being pumped from the reservoir during the period of 20 to 26 January 1979 while little to no water was pumped during March 1972. The August 1955 storm was a significant event in this region but there are no records available relative to the Quinapoxet Reservoir water level. Thus the highest recorded level is 733.7 which indicates a spillway discharge of about 375 cfs.

- d. <u>Visual Observations</u> The visual inspection of the dam was made on 29 May 1980. At the time, the reservoir level was at spillway crest. The freeboard at the dam was 7.0 ft. but only about 5.0 ft. at a natural swale located about 1,000 ft. to the left of the dam and about 5.5 ft. at the dike located about 1,000 ft. to the right of the dam. The spillway, chute and stilling basin were clear of debris. The outlet works sluice gate was closed and no leakage was oberserved. The Owner's representative opened and closed the sluice gate during the inspection of the dam to demonstrate its operability.
- e. <u>Test Flood Analysis</u> Based on the Corps of Engineers Guidelines, the recommended test flood for the size, intermediate, and hazard potential, high, is the PMF (Probable Maximum Flood). The test flood was estimated using the Corps of Engineers "Guidelines for Estimating Maxmimum Probable Discharge in Phase I Dam Safety Investigations". Based on the watershed terrain being undeveloped with moderate to flat slopes and significant upstream storage, a PMF peak inflow rate of 650 cfs per square mile was selected for the 19.85 sq. mi. drainage area. The resulting peak test flood inflow is approximately 12,900 cfs.

Assuming that the flashboards collapse at design reservoir surcharge elevation 734.0 (1-ft. depth over flashboards) the routed test flood outflow is 12,000 cfs at a stage of 737.5. Neither the dam, dike, or swale to the north of the dam would be overtopped. The depth of water over the spillway would be about 6.5 ft. with the flashboards collapsed. The spillway capacity at the test flood elevation is about 12,000 cfs or 100 percent of the routed test flood outflow. The drain capacity at top of flashboards (elevation 733.0) is approximately 430 cfs.

The tailwater analysis indicates that the downstream spillway channel has the hydraulic capacity to carry 12,000 cfs without overtopping its bank. However, the capacity of the bridge at Princeton Street is less than that of the spillway channel. A discharge of 12,000 cfs would overtop Princeton Street by about 2.2 ft. and would flood the toe of the dam by about 2.5 feet.

SECTION 5: HYDRAULIC/HYDROLOGIC

5.1 Evaluation of Features

- General Quinapoxet Reservoir Dam is an earth embankment located in Holden. Massachusetts and forming a water supply impoundment for the City of Worcester, Massachusetts. The impoundment is fed by South Wachusett Brook and discharges to the Quinapoxet River. The watershed is 19.85 square miles of undeveloped land with flat to moderate slopes and significant upstream storage. At the concrete spillway crest (E1. 731.0 NGVD) the reservoir storage is about 3,424 acre-feet, increasing to 6,174 acre-feet at the top of the dam (El. 740.0 NGVD). The 200 ft. long spillway has facilities for 2 feet of flashboards which are always in place. The length of the dam, including the spillway, is about 1,050 ft. and the overall height of the dam is about 45 ft. The reservoir drain is a 4-ft. square reinforced concrete conduit located near the center of the dam and controlled from a gate operator on its crest. The dam is basically a high spillage-low surcharge project.
- b. <u>Design Data</u> The following hydraulic/hydrologic design data for the dam was obtained from the 14 September 1953 final report on "The Construction of Quinapoxet Reservoir and Appurtenances" by Metcalf and Eddy Engineers, 50 Staniford Street, Boston, MA 02114.

Drainage Area	19.85 sq.mi.
Reservoir capacity	1,200 mil. gal.
Water surface area	285 acres
Spillway length	200 ft.
Spillway crest elev	E1. 731
Height of flashboards	2 ft.
Water surface on collapse of flashboards	El. 734
Design flood at spillway	3,300 Sec ft
Design flood per sq.mi. of drainage area	240 Sec ft.

c. <u>Experience Data</u> - The City of Worcester maintains a record of water levels at the Quinapoxet Reservoir. However, it is difficult to correlate rainfall to spillway discharge because water SECTION 4: OPERATIONAL PROCEDURES

- 4.1 <u>Procedures</u> Water levels are recorded daily and the pumping rates from the reservoir are adjusted accordingly to minimize spillage from the reservoir to the Quinapoxet River.
- 4.2 <u>Maintenance of the Dam</u> There is no established formal maintenance program for this dam. The operator indicated that maintenance is performed on a demand basis. The grass on the slopes is cut once per year and twice per year on the flat areas. The condition of the dike indicates that this structure is not included in this program.
- 4.3 <u>Maintenance of Operating Facilities</u> Two feet of flashboards are maintained year round on the spillway. The reservoir drain is kept normally closed. The gate operator is cranked and greased annually to insure it is kept operable.
- 4.4 <u>Description of Any Warning System in Effect</u> There is no established warning system or emergency preparedness plan in effect for this structure.
- 4.5 <u>Evaluation</u> The dam is currently being operated on a routine basis and maintenance is being performed on the basis of need. The dike should be added to the maintenance work being performed.

The procedures being employed should be compiled in writing and expanded where necessary for ready reference by the operating personnel. It should also contain provisions for the biennial technical inspection of the dam, an emergency preparedness plan and the details of operation of a warning system.

- c. Appurtenant Structures
 - (1) The outlet works is in good condition. The sluice gate was opened slightly during the site examination and then closed as shown in Photos 11 and 12.
 - (2) The dike is also in good condition with no observed evidence of embankment settlement, lateral movement or other major deficiencies. The dike however is covered by tall grass, weeds and a significant amount of brush and small trees as shown in Photos 13 and 14.
- d. <u>Reservoir area</u> The Quinapoxet Reservoir is surrounded by moderately sloped hills which are heavily forested. The shore line of the pond is undeveloped and no structures would be affected by the test flood surcharge.

The side slopes to the pond are moderate and there appears to be no significant potential for landslides into the pond which would create waves that might overtop the dam. No conditions were noted that could result in a sudden increase in sediment load into the pond.

- e. <u>Downstream Channel</u> The Quinapoxet River flows from the dam on a moderate slope to the Wachusett Reservoir. The river crosses a pocket of development around the State Route 31 area, but otherwise flows through undeveloped land.
- 3.2 <u>Evaluation</u> The dam, dike and appurtenant structures are considered to be in good condition, based on the visual examination. The evidence of seepage noted on the downstream slope of the dam is not considered serious at this time. However, changes in the quantity or pattern of seepage could be significant relative to the performance of the dam embankment.

SECTION 3: VISUAL INSPECTION

3.1 Findings

I.

a. <u>General</u> - The Phase I visual examination of Quinapoxet Reservoir Dam was conducted on 29 May 1980.

In general, the earthen embankments, spillway and outlet works were observed to be in good condition. The reservoir level at the time of the site examination was at the top of flashboards Elev. 733.0.

Visual inspection checklists for the site visit are included in Appendix A, prior inspection reports in Appendix B, and selected photographs in Appendix C.

- b. <u>Dam</u> The dam and spillway, Photos 1, 8 and 9 appear to be in generally good condition, based on the visual site examination. No evidence of embankment settlement, lateral movement or other major deficiencies was observed. The following specific items were noted:
 - The crest and downstream slope of the dam have good grass cover as shown in Photos 3 and 4. Some brush and small trees are present in the riprap along the upstream slope as shown in Photo 5.
 - (2) A small amount of clear seepage flow (perhaps 1 to 2 gpm) was observed at the base of the riprapped slope, on the left side, just below the end of the spillway stilling basin as shown in Photo 10. This flow is assumed to be from the blanket drain system.
 - (3) A wet area was observed on the downstream slope of the dam, just below the berm about mid-height and adjacent to the spillway left channel wall. The seepage appears to originate near the location of piezometer P-2 as shown on Sheet 4 of the contract drawings (see Appendix B), although the piezometer itself was not found. The wet area extends roughly 50 ft. along the spillway channel to a point where the seepage flows over the channel wall.
 - (4) No piezometers were found on the dam embankment.
 - (5) One of the flashboard braces near the right end of the spillway is missing as shown in the foreground of Photo 7.
 - (6) The side wall joint immediately downstream of the spillway weir at its right end is exhibiting structural distress in the form of cracking, as shown in Photo 6. The sealant at other joints in the spillway side channel, chute and stilling basin is in need of renewal.

SECTION 2: ENGINEERING DATA

- 2.1 <u>Design Records</u> Design records in the form of construction plans and a final construction report dated September 14, 1953 by Metcalf & Eddy were located. Plans and specifications for Restoration of the Spillway Flashboards and Construction of a Stone Jetty in 1977 were also located.
- 2.2 <u>Construction Records</u> A final construction report described above is available.
- 2.3 <u>Operational Records</u> The City of Worcester maintains records on rainfall, pumpage from the reservoir, and reservoir water levels. Inspection reports by the County and the Division of Waterways, State of Massachusetts, were also located and are included in Appendix B.

2.4 Evaluation

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- a. <u>Availability</u> The construction plans, final construction report and reservoir operation records are available at the City of Worcester DPW Building, 20 E. Worcester St., Worcester, MA.
- b. <u>Validity</u> The available data was in good agreement with conditions observed during the site examination.
- c. <u>Adequacy</u> The available data, in combination with the visual evaluation described in the following section, is adequate for the purpose of the Phase I investigation.

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i. Spillway (1) Type.....Broad crested side discharge spillway with flashboards, chute and stilling basin (2) Length of weir.....200 ft. (3) Crest elevation a) with flashboards......733.0 b) without flashboards.....731.0 (4) Gates.....None (5) U/S Channel.....Ouinapoxet Reservoir (6) D/S Channel.....Concrete Rectangular channel with varying slope, width and side depth. A 40-ft. long, 8 ft. high concrete impact wall with a 5-ft. V-notch drain forms a stilling basin followed by a riprapped basin prior to the beginning of the Quinapoxet River's natural channel. j. Regulating Outlets Invert: U/S.....702.0 (1)Size: Box Culvert.....4-ft. (2) by 4-ft. Description.....Reinforced concrete box culvert located near the center of the dam. (3) (4) Control Mechanism......Manually operated Sluice gate (4-ft. sq.) with operator stand at crest of dam. Other.....6" dia. gated bypass (5)

around sluice gate

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f. <u>Reservoir Surface</u> (acres)

(1)	Normal pool
(2)	Flood-control poolN/A
(3)	Spillway crest
(4)	Top of dam
(5)	Test flood pool

g. Embankments

h.

	Dam	<u>Dike</u>
(1)	TypeZoned earth Embankment	Earth Embankment
(2)	Length1050 ft.	370 ft.
(3)	Height 45 ft.	7 ft.
(4)	Top width 20 ft.	20 ft.
(5)	Side Slopes, Upstream2H to 1V (upper) 2.5H to 1V (lower	3H to 1V `)
	Downstream2H to 1V	3H to 1V
(6)	Zoning"Impervious" core with "per- vious" shells	None
(7)	Impervious CoreCompacted Glacial Till	None
(8)	CutoffCore extends to rock	None
(9)	Grout curtainNone	None
Dive	rsion and Regulating Tunnel	• None

(5)	Gated	spillway	capacity	at	normal	poo1	elevation	N/A
-----	-------	----------	----------	----	--------	------	-----------	-----

- (6) Gated spillway capacity at test flood elevation.....N/A
- (7) Total spillway capacity at test flood elevation: 12,000 cfs
 @ 737.5 elev.
- (8) Total Project discharge at test flood elevation: 12,000 cfs
 @ 737.5 elev.
- c. Elevation (ft. above NGVD)

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	(1)	Streambed at centerline of dam
	(2)	Test flood tailwater709.7
	(3)	Upstream portal invert diversion tunnelN/A
	(4)	Normal pool733.0
	(5)	Full flood control poolN/A
	(6)	Spillway crest a. with flashboards
		b. without flashboards
	(7)	Design surcharge (Original Design)Unknown
	(8)	Top of dam
	(9)	Test flood surcharge737.5
d.	Leng	th of Reservoir (miles estimated)
	(1)	Normal pool
	(2)	Flood control poolN/A
	(3)	Spillway crest pool
	(4)	Top of daml.7
	(5)	Test flood pool
e.	Stor	age (acre-feet)

(1) Normal pool......3,976

i. <u>Normal Operating Procedure</u> - Maintenance at the dam is performed on a routine basis. There is a caretaker permanently assigned to the City of Worcester's reservoir system who is responsible for the operation and maintenance of the facility. The grass is cut at least once a year and the outlet works manual sluice gate operator is greased and tested each year. Two feet of flashboards are maintained on the spillway crest year round and require no adjustment. A pump station, located on the west bank of the reservoir, is manually regulated to optimize pumpage from Quinapoxet Reservoir to Kendall Reservoir and thus into the City of Worcester's water distribution system.

1.3 Pertinent Data

Elevations given in this report are on National Geodetic Vertical Datum (NGVD) formerly referred to as Mean Sea Level.

- a. <u>Drainage Area</u> The drainage area tributary to the dam site is 19.85 square miles. The watershed is flat and undeveloped except for some scattered houses. The undeveloped land is heavily forested with swampy areas throughout. Muschopauge Pond, which is part of the Quinapoxet Reservoir drainage area, is used as a water supply to the Towns of Rutland and Holden. The Quinapoxet Reservoir accounts for approximately 2 percentage of the total drainage area.
- b. <u>Discharge at Dam Site</u> The City of Worcester takes daily readings of the reservoir water level together with daily pumping rates from the reservoir and daily readings of precipitation. An examination of these records indicates that the reservoir level is kept at top of flashboards (El. 733.0.NGVD) or below, even during periods of high precipitation. The highest recorded reservoir level is El. 733.7, occuring on 23 March 1972, apparently as a result of all other City of Worcester reservoirs being full at the time so that no pumpage was occurring. The precipitation for the period of 21 to 23 March 1972 was 1.35-inches. A reservoir level of El. 733.7 would result in an estimated discharge of 375 cfs.
 - Outlet works size: 4-ft. by 4-ft. reinforced concrete box culvert. Discharge capacity at top of flashboards is approximately 430 cfs.
 - (2) Maximum known flood at damsite: 375 cfs (Est.) on 23 March 1972.
 - (3) Ungated spillway capacity at top of dam: 21,000 cfs @ 740 elev.
 - (4) Ungated spillway capacity at test flood elevation: 12,000 cfs @ 737.5 elev.

lined circular basin under the masonry Princeton Street Bridge and into the original Quinapoxet River bed.

The outlet works consist of a 4-ft. by 4-ft. reinforced concrete box culvert which extends 310-ft. from its intake structure, through a sluice gate chamber, to the spillway stilling basin. The sluice gate chamber and manual gate operator are located near the center of the dam. A gated 6-in. diameter sluice gate bypass is located at the invert of the gate chamber which may be used to maintain a flow in the Quinapoxet River when the reservoir level is below spillway crest and the sluice gate is closed. The outlet works' intake is a reinforced concrete special structure which incorporates a flared inlet with provision for stoplogs.

- c. <u>Size Classification</u> The maximum height of the dam is approximately 45 feet and the estimated total storage capacity at the top of the dam is 6,174 acre-feet. According to guidelines established by the Corps of Engineers, the dam is classified in the intermediate category based on both storage capacity and height.
- d. <u>Hazard Classification</u> The results of the dam failure analysis indicate that about 35 homes would be affected by water depths of 1 to 15 ft. and the potential loss of life would be in excess of 10 persons. Consequently, the dam is classified in the "high" hazard category.
- e. <u>Ownership</u> The dam is owned by the City of Worcester. The owner is represented by Mr. Richard Grant, Assistant Commissioner of Public Works, 20 East Worcester Street, Worcester, MA 01608, tel. (617) 798-8151.
- f. <u>Operator</u> Mr. Kenneth Starbard is assigned responsibility for operation of the dam. His business address is Kendall Reservoir, South Road, Holden, MA 01520, tel. (617) 829-4811.
- g. <u>Purpose of the Dam</u> Quinapoxet Reservoir Dam provides for water supply storage to the City of Worcester. Water from the Quinapoxet Reservoir is pumped to Kendall Reservoir and eventually to the City of Worcester water distribution system. The water which discharges over the spillway enters the Quinapoxet River and becomes part of the Metropolitan District Commission's Water Supply through the Wachusett Reservoir.
- h. Design and Construction History The dam was designed in 1952 and was essentially complete by mid-July 1953. Impoundment of water was started on 6 July 1953. The original facility was modified by the addition of a stone jetty and reconstruction of spillway flashboards in 1977. According to Worcester County records a former dam located approximately 2,400-ft. upstream of the site of the existing facility and which impounded only South Wachusett Brook to form Quinapoxet Pond was destroyed by City on 1 August 1952.

b. <u>Description of Dam and Appurtenances</u> - Quinapoxet Reservoir Dam consists of a zoned earth embankment, with an outlet conduit extending beneath the center of the dam and a concrete spillway structure located at the right abutment. There is also a low earth dike extending across a natural saddle, roughly 1,000 ft. beyond the right abutment of the main dam. The general layout of the dam, dike and appurtenant structures is shown on the location plan included in Appendix C.

The embankment is about 1,050 ft. long (including spillway), has a maximum height of 45 ft., and is 20 ft. wide at the crest. The grass-covered downstream slope is 2H to 1V, with a 6-ft. wide berm at mid-height. The upstream slope is 2H to 1V near the crest and flattens to 2-1/2H to 1V, 17 ft. below the crest. Riprap wave protection extends to the crest on the upstream side.

The embankment consists of two zones. The central core zone consists of compacted impervious glacial till which extends to bedrock. The other zone consists of upstream and downstream shells which are composed of clean, well-graded gravel with a sand binder. Sheet 10A of 18 of the contract drawings (included in Appendix B) shows the embankment section as described in the Designer's Final Report. It should be noted that embankment sections on other sheets show a zone of "random material" which was not actually placed. Also, the Designer's Final Report states that excess material from the spillway excavation was spread on the upstream toe.

A horizontal blanket drain is located beneath the downstream portion of the embankment and extends downstream from the middle section of the dam. The drain consists of layers of "selected pervious material" and "washed stone", with a system of collector pipes which discharge collected seepage near the downstream end of the spillway channel. According to available plans, eight (8) piezometers were installed during the original construction to monitor seepage conditions within the embankment.

The dike is a homogeneous earth embankment 370 ft. long, 7 ft. high, and 20 ft. wide at the crest. Side slopes are 3H to 1V upstream and downstream. The dike slopes are grass and brush covered, with no riprap.

The 200 ft. long concrete spillway consists of a 4 ft. wide horizontal crest with a 4H to IV sloped riprap upstream face and a 2.8H to IV sloped concrete downstream face. Two feet of flashboards are maintained on the crest of the dam year round. The flashboards consist of eight (8), 25-ft. long hinged sections which are held in place by special bolts designed to fail when the reservoir has a side channel discharge which conveys the flow to an 8-ft. high, 25' wide channel chute and then to a stilling basin. The stilling basin varies in width from 25 to 40 feet and has side wall heights of up to 20 feet at the end. The stilling basin is formed by a concrete impact wall which incorporates a v-notch drain designed to prevent the formation of ice within the stilling basin. Flow from the stilling basin is channeled by a riprapped SECTION 7: ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

7.1 Dam Assessment

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- <u>Condition</u> Based on the visual examination and review of available records, the dam is considered to be in good condition. While some evidence of local seepage was noted, no conditions which would require urgent remedia! action were observed.
- b. <u>Adequacy of Information</u> The evaluation of the dam has been based on the visual examination, consideration of available documents and past performance, and application of engineering judgement. Generally, the information available or obtained has been adequate for the purposes of the Phase I assessment. However, it is recommended that additional information relative to embankment seepage be obtained as outlined in Section 7.2.
- c. <u>Urgency</u> The recommendations for an additional investigation and remedial measures, outlined in Sections 7.2 and 7.3, respectively, should be undertaken by the Owner within two years after receipt of this report.

7.2 Recommendations

It is recommended that the Owner arrange for the following investigation to be performed by a registered professional engineer experienced in dam design and construction:

 Evaluate the significance of the observed evidence of seepage relative to long-term embankment stability, and assess the need for corrective action. Piezometers should be located and restored to service where possible. Criteria should be established for monitoring of restored piezometers by the Owner. The Owner should implement corrective action as required, based on the results of the evaluation.

7.3 Remedial Measures

- a. <u>Operation and Maintenance Procedures</u> The following remedial work should be undertaken by the Owner:
 - Remove brush from dam and dike. Mow both embankments at least once a year to permit visual inspection.

- (2) Periodic readings should be made on any piezometers that can be restored. This data would provide a useful check of embankment and drainage system performance.
- (3) Replace the missing flashboard brace near the right end of the spillway weir.
- (4) Repair the cracked wall joint immediately downstream of the right end of the spillway weir and reseal other joints in the spillway, chute and stilling basin walls.
- (5) Establish a formal maintenance program and operational procedures for the dam.
- (6) Prepare a formal emergency procedures plan and warning system in cooperation with downstream officials and institute a program of biennial technical inspections.
- 7.4 <u>Alternatives</u> There are no practical alternatives recommended.

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APPENDIX A

INSPECTION CHECKLIST

	Page No.
VISUAL INSPECTION PARTY ORGANIZATION	A-1
VISUAL INSPECTION CHECKLIST	
Embankment: Dam	A-2
Embankment: Uike	A-3
Spillway	A-4
Outlet Works	A-5

VISUAL INSPECT	ION PARTY ORGANIZATION	
NATIONAL DAM	INSPECTION PROGRAM	
AM: Quinapoxet Reservoir Da	n	
ATE: 29 May 1980		
IME: <u>1:00 PM</u>		
EATHER: Sunny		
ATER SURFACE ELEVATION UPSTREA	M: 333 (NGVD)	
TREAM FLOW: Minor (wave action	on and some leakage through flashboards)	
NSPECTION PARTY:		
1Roger H. Wood, CDM	·	
2. <u>Joseph E. Downing, CDM</u>		
3. Joseph R. Araujo, CDM		
4. Douglas G. Gifford. H&A		
5. John Critchfield, H&A		
ROJECT FEATURE	INSPECTED BY REMARKS	
1. <u>Structural/Operations</u>	Roger Wood	
2. Hydraulics/Hydrology	Joseph Downing and Joseph Araujo	
3. Embankments	Douglas Gifford and John Critchfield	
4		
DECENT DUDING INCOROTIONS	,	
RESENT DURING INSPECTION:		
Bruce_Blanchard, Owner	Representative & Operator	
Ζ.		

VISUAL INSPECTION CHECK LIST NATIONAL DAM INSPECTION PROGRAM

DAM: Quinapoxet Reservoir Dam EMBANKMENT: <u>DAM</u>

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DATE: 29 May 1980

CHECK LIST	CONDITION
 Upstream Slope Vegetation Sloughing or Erosion Rock Slope Protection Riprap Failures Animal Burrows 	 1. a. Few saplings among riprap stones. b. None apparent. c. Riprap (cobbles to 2 ft. stones) extends to crest. Good condition. d. None observed.
2. Crest a. Vegetation b. Sloughing or Erosion c. Surface cracks d. Movement or Settlemen	2. a. Grass. b. None observed. c. None observed. t. d. None apparent.
 Downstream Slope Vegetation Sloughing or Erosion Surface Cracks Animal Burrows Movement or Cracking toe Unusual Embankment or Downstream Seepage Piping or Boils Foundation Drainage Fi Toe Drains 	 3. a. Grass. b. None observed. c. None observed. d. None observed. e. None apparent. f. Noted wet area below berm, near spillway. Wet and soggy, no apparent flow Spillway wall also wet. g. None observed. h,i D/S drainage blanket with collection pipe.
 4. General a. Lateral Movement b. Vertical Alignment c. Horizontal Alignment d. Condition at Abutment at Structures e. Indications of Moveme Structural Items f. Trespassing g. Instrumentation System 	 4. a. None apparent. b. Crest appears level except slightly higher near gate valve. c. Good. d. Apparent lateral movement of retaining wall at right end of spillway, with associated backfill settlement. e. See 4d. f. Infrequent, locked gate. g. Piezometers shown on plan but not located in field.

A-2

VISUAL INSPECTION CHECK LIST NATIONAL DAM INSPECTION PROGRAM

DAM: <u>Ouinapoxet Reservoir Dam</u> EMBANKMENT:<u>DIKE</u>

DATE . 29 May 1980

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CHEC	K LIST	CONDITION
1.	Upstream Slope a. Vegetation b. Sloughing or Erosion c. Rock Slope Protection - Riprap Failures d. Animal Burrows	 Grass, weeds, brush. None apparent. No riprap. None observed.
2.	Crest a. Vegetation b. Sloughing or Erosion c. Surface cracks d. Movement or Settlement	2. a. Grass, weeds, brush. b. None observed. c. None observed. d. None apparent.
3.	Downstream Slope a. Vegetation b. Sloughing or Erosion c. Surface Cracks d. Animal Burrows e. Movement or Cracking near toe f. Unusual Embankment or Downstream Seepage g. Piping or Boils h. Foundation Drainage Features i. Toe Drains	 3. a. Brush and trees. b. None observed. c. None observed. d. None observed. e. None apparent. f. Swampy area downstream. g. None observed. h. None. i. None.
4.	 General a. Lateral Movement b. Vertical Alignment c. Horizontal Alignment d. Condition at Abutments and at Structures e. Indications of Movement of Structural Items f. Trespassing g. Instrumentation Systems 	<pre>4. a. None apparent. b. Good. c. Good. d. Good. e. No structural items. f. Infrequent. g. None</pre>

HECK LIST	CONDITION
 Approach Channel a. General Condition b. Obstructions c. Log Boom etc. 	1. a. Good condition. b. None. c. None observed.
 Weir Flashboards Weir Elev. Control (Gate) Vegetation Seepage or Efflorescence Rust or Stains Cracks Condition of Joints Spalls, Voids or Erosion Visible Reinforcement General Struct. Condition 	 2. a. Two feet, brace at right end missing. b. Flashboards only. c. None observed. d. Flow precludes evaluation. e. Flow precludes evaluation. f. None observed. g. Flow precludes evaluation. h. Flow precludes evaluation. i. None observed. j. Good.
 Discharge Channel Apron Stilling Basin Channel Floor Vegetation Seepage Obstructions General Struct. Condition 	 3. a. Good condition. b. Good condition. c. Good conditon. d. None observed. e. None observed. f. All structures clear. g. Good.
 4. Walls a. Wall Location (1) Vegetation (2) Seepage or Efflorescenc (3) Rust or Stains (4) Cracks (5) Condition of Joints (6) Spalls, Voids or Erosio (7) Visible Reinforcement (8) General Struct. Conditi 	 4. a. All Spillway Walls (1) No major condition observed. (2) Efflorescence right side intake wall. (3) None observed. (4) Cracked joint right side D/S of weir. Possible diagonal cracks right side U/S of weir. (5) See (4), a number of joints have no sealant. (6) See (4) for spalls, no major erosion. (7) None observed. (8) Good.

A-4

OUTLET WORKS:		
CHECK LIST	CONDITION	
<pre>1. Inlet a. Obstructions b. Channel c. Structure d. Screens e. Stop Logs f. Gates</pre>	1. Not visible, under water.	
2. Control Facility a. Structure b. Screens c. Stop Logs d. Gates e. Conduit f. Seepage or Leaks	2. a. Visible portion in good condition. b. None observed. c. None observed. d. Manual, operational. e. Not visible. f. None observed.	
 Outlet a. Structure b. Erosion or Cavitat c. Obstructions d. Seepage or Leaks 	3. a. Opening in stilling basin wall, good condition. b. None observed. c. None observed.	
 4. Mechanical and Electric a. Crane Hoist b. Hydraulic System c. Service Power d. Emergency Power e. Lighting f. Lightning Protection 	d. None observed. 4. a. Not applicable. b. Not applicable. c. Manually operated. d. Not applicable. e. Not applicable. f. Not applicable.	
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A-5
APPENDIX B

ENGINEERING DATA

DOCUMENTS	Page No.
List of Available Documents	B-1

PRIOR INSPECTION REPORTS

	Tuge no.
Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County	B-2 B-3 B-4 B-5-6 B-7 B-8 B-9 B-10 B-11
	Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County Worcester County

No.	<u>Title</u>	Page No.
1. 2. 3. 4. 5. 6. 7.	Plan of Dam Typical Sections Dam and Spillway Details Miscellaneous Sections & Details Drain Conduit Borings Proposed Stone Jetty and	B-12 B-13 B-14 B-15 B-16 B-17 B-18
	Flashboard Alterations	

* Inspection Reports on former dam located upstream of existing facility are included for their historic and hydrologic content.

LIST OF DOCUMENTS

QUINAPOXET RESERVOIR

DOCUMENT

- I. Complete Set of Design Drawings, and a Final Construction Report.
- Design Drawings, Final Construction Report, and Operating Records.
- Design Drawings and Monthly Construction Reports.
- 4. Plans and Specifications for Restoration of Spillway Flashboards and Construction of a Stone Jetty in 1977.

LOCATION

Metcalf & Eddy Engineers 54 Staniford Street Boston, MA

City of Worcester DPW Building 20 E. Worcester Street Worcester, MA 01608

Worcester County County Court House Worcester, MA Coffin & Richardson 141 Milk Street Boston, MA 02109



· LOCATION Near Princelon T.L. - Quisgooxet Pand - Near Hincoles St. C. C. DOCKET NO. DESCRIPTION OF DAM DESCRIPTION OF WATERSHED Name of Main Stream Type Forth - Impervious Fill Care Quinopoxet Brei " " any other Streams Muschopsige Br. - Bypard Br. -Length 1100'± Top Eky. 740 Length of Watershed Woodwisch Br. - Broaf from Mark Height 35' ± 170x. Width " 20' Thickness top Series hed Is Watershed Cultivated bottom 180' ± 190x. **Downstream Slope Percent in Forests** 2:1 2:1 and 2/2:1 below eler. 723 Steepness of Slope 44 Upstream 200' Too Elex 731, 4'X 4" Drain Conduit Length of Spillway Kind of Soil No. of Acres in Watershed 19.85 50. Mi. 20.7 S.M Size of Gates Location of Gates Water Surface 280 Acres Approx. Center of Length of Reservoir Flashboards used Copocity 1200 Million Gollan Wiath # # Width Flashboards or Gates 00 Max Flow Cu. Ft. per Sec. Metook Dam designed by Eddy out Head or Flashboards-Low Water " constructed by Calenton' Bras Carp 1952-1953 н -High " Year constructed GENERAL REMARKS Twined by City of Norcester Noter Deat. 1436 DAM NO. DECREE NO. TOWN OR CITY Holden PLAN NO. Flood LOCATION Near Princeton T.L. - Quina poxet Pond Near Princeton St. C. DOCKET NO DESCRIPTION OF DAM DESCRIPTION OF RESERVOIR & South Wachusett Brook Name of Main Stream Earth-Dry Walls -Stone Apron-El lo Туре " " any other Streams, Length _300¥ the cord is Longth of Watershed Height 8.4 Width " # Thickness top 8 Is Watershed Cuitivated bottom 16.** . Percent in Forests Dewnstream Slope Kerticial Steepness of Slope 12:1 Upstream Kind of Soil Length of Spillway Depth= 3'5 Length 60'1 No. of Acres in Watershed Size of Gates None Location of Gates Length of Reservoir Flashboards used Yes Width " " Width Flashboards or Gates 8 Max Flow Cu. Ft. per Sec. Dam designed by Head or Flashboards-Low Water " constructed by --High " Year constructed GENERAL REMARKS GENERAL REMARKS Walker, Ice Co., Worcester. 1942* City of Worcester Waler Dept Owned by Inspected: Nov. 18, 19 47 E. Perry Hardy-LON (ag) & Old Dam 21-10 destroyed by City of Inspected: Dec. 7, 1928-L.O. Marden. Warester Aug. 1, 1952, and number was given to New Dom downstre Oct. 5, 1938 - L. H. Spofford Mar. 21, 1939 downstream from of site. top Heas wy Barnes | 8-\$250

B-2

discharge of 12,000 cfs would overtop Princeton Street by about 2.2 ft. and would flood the toe of the dam by about 2.5 feet.

5-2

COUNTY OF WORCESTER MASSACHUSETTS

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COUNTY ENGINEER

Inspection of Dams, Reservoir Dams, and Reservoira.

Inspected by W. O. Li	Indquist	Date 3-27-37	Dam No. 21-10
Town Holden	Locs	uinapoxet.	Pond
Owner		Ūæ	· ; · · · · · · · · · · · · · · · · · ·
Material and Type	•••••••••••••••••••••••••••••••••••••••		······
Dam Designed by	C	Constructed by	Уеаг
SPILLWAY-Length	Feet. Depth	Fect	
El. top Abutment	El. Crest	El. Apron	I. Streambed
Width top Abutment	Width top Crest	Width bottom Spillw	ay
Width Flashboards carried	K	ind Flashboards	
El. Flowline Cleanout Pipe	8	ise and Kind Cleanout Pipe	
Kind of Foundation under S	pillway		
Condition 1 flashboar	d <u>on at prese</u> n	ittimeLogs.andol	drowboatsnertly
blocking flow of w	ater.Large_cra	cks_easterly_abutme	ntwall.
EMBANKMENT-Length o	verallFeet	•	
El. TopE	I. Natural Ground	Width Top	
Width of Bottom		peDownst	ream Slope
Kind of Corewall	•	- 	- rap
Material in Embankment			•
Condition 2. Washouts	should be fil	led in	
no leaks evident.	• Fair condit	10 n. ,	·
GATES		Location	
Size	Kind	El. Flowline	
Condition Open at	present.		
WHEEL Kind	•••••••••••••••••••••••••••••••••••••••	Size Rated	н. Р.
Location		Ave. Head	
Evidence of Leaks in Structur	re		
Recent Renairs and Date			
Topography of Country below	7 Dam		
Tobography or country solor		•••••••••••••••••••••••••••••••••••••••	
Nature of Buildings and Road	is below Dam		
Number of Acres in Pond			Miles
Discharge in Second Feet ner	Square Mile		
Estimated Storage Million Cu	ibic Feet		
second particle transmit of			· · · · · · · · · · · · · · · · · · ·

B-3

WORCESTER COUNTY ENGINEER	
Inspection of Dams, Reservoir Dams, and Re:	servoirs
nspected by L. H. Spofford Date 10-5-38	Dam No. 21-10 .
'ownHoldenLocation Quinapoxet	t Lake
wner Walker Ice Co. Use Impour arth embankment, faced with concrete stone masonry SPILL"AY 70' wide with rock apron. Remains of few	nding y on pond side. flashboard, catwalk
Width top Abut. Width top Crest Width by	EL.ST.Ben Stayed
Vidth flashboards Kind Flashboards	focom openay
El.Flowline Cleanout Pipe Size and Ki	Ind Pipe -+
(ind of Foundation under Spillway	
Condition High water mark was approximately 4'6" c	over crest of
spillway.	
······································	
FLBANKLIENT	
EL. TopEl.Natural GroundV	idth Top
Wiath of BorromUpstream SlopeDow	mstream Slope
Kind of CorewallRipra	p
Material in EmbankmentFoundat	ion
Condition 1 washout about 2 ft. deep x 12' long eas	t end. 1 washout about
12 ft. deep x 10 ft. west end (washed out in 1936	and not repaired)
GATESLocation	
SizeKindEi.Fl	owline
Condition Evidence that flood topped the embankmen	t about a foot
where washout occurred.	
Evidence of Leaks in Structure	
Recent Repairs and Date	
Number Acres in PondDrainage Area : Discharge in Second Feat por Square Mile	in Sq. Miles
Estimated Storage Million Cubia France	
rearmaned proligke WIIIIOU CADIC LEGI	·

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mille 2 Stores WORCESTER COUNTY ENGINEER Inspection of Dams, Reservoir Dams, and Reservoirs Date 11 (1 2) 39 Dam No. 21-10 ispected by In Location Jumpor mer malken see Co-Use gring SPILLWAY L.top abutment_____El.Crest____El.Apron___El.Ct.Bed____ ldth top Abut._____Width top Crest_____Width bottom Sp.way_____ ldth flashboards ("top log. Kind Flashboards L.Flowline Cleanout Pipe _____Size and Kind Pipe_____ Ind of Foundation under Spillway___ milition fair - County abutmente have been crache mo areat Marina FLBANJENT . Top _____El.Natural Ground _____ Width Top Lith of Borrom_____Upstream Slope____Downstream Slope____ ind of Corewall Piprap aterial in Embankment Earth Foundation sudition Poor - no repairs have been made to was 1938 7 Wood! - see patoler 1938 inspec Location cast end of a cillion JATES DAM- of ize 3 wil x 3 2 40 organiz Kind El.Flowline andition Water is remme three organiz about 3' deep - open min vidence of Leaks in Structure Moli- on and going my ecent Repairs and Date MMM Cored umber Acres in Pond_____Drainage Area in Sq. Miles_____ ischarge in Second Feet per Square Mile_____ stimated Storage Million Cubic Feet

B-5

APPENDIX C

SELECTED PHOTOGRAPHS OF PROJECT

LOCATI	<u>ON PLAN</u>	Page No.
Loc	ation of Photographs	C-1
PHOTOG	RAPHS	
No.	Title	
1.	Overview of Dam from Right Abutment	iv
2.	Project Plaque	iv
3.	View of Dam and Spillway Downstream	C-2
	Channel from Left Abutment	
4.	Downstream Face of Dam from Right	C-2
	Abutment Showing Spillway Downstream	
-	Channel in Foreground	
5.	Crest and Upstream Face of Dam from	C-3
c	Left Abutment	
0. 7	view of Right Side of Spillway	C-3
/.	view of Spillway and Spillway Left Abutment	C-4
ö.	Spillway Downstream Channel with Princeton	C-4
0	Street Bridge shown at end of Spillway Channel	
9.	View of Spillway Downstream Channel from	C-5
10	Princeton Street Bridge	
10.	Seepage at Riprap to the Left of the Stilling	C-5
11	Basin Sill	
11.	Reservoir Drain Gate Operator on Dam Crest	C-6
12.	Photo of Reservoir Drain Outlet at Spillway	C-6
13	Unatrian Face of Dike from its Left Abutment	C 7
14.	Crest of Dike from Left Abutment	
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NN Holden DAM NO	21-10 New
CATION Why side of Princeton St. STREAM _ Quin.	poxet River
"Quingposet Reservoir." WORCESTER COUNTY ENGINEERING DEPAR WORCESTER, MASSACHUSETTS	TMENT
DAM INSPECTION REP.	<u>PRT</u>
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pected by Date Date	June 1. 1965.
e of Dam <u>Generate - Earth</u> Condition	a lever
LLWAY	
shboards in Place Recent Re	pairs
dition bord (Point is fall to top	of boards)
airs Needed	
Dam constructed in 1952 - 1953	
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:	County Engineer

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OCATION Quinapexet Res-	STREAM
WORCESTER COUNTY EN Worcester,	GINEERING DE PARTMENT MASSACHUSET1'S
DAM INSPEC: Burequ of Water	TION REPORT
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AKS	
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	DATE: May 25, 1960
	P.J. mane
	County Engineer

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OWN	Holden	DAM NO.	21-12
OCATION Caste	ry side Princeton	34 STREAM	Quimaros 6 - Parer
	WORCESTER COUN WORCES	تعذريم TY ENGINEERING DE TER, MASSACHUSETT	PARTMENT S
	DAM INSP	ECTION RE	PORT
wned by	City of Marcaster	Place	ter Papt. Use Matters
nspected by _		Date	054.13 1955
ype of Dam	Earth and con	condi	tion <u>6000</u>
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TOWN_Holden

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DAM	ND.	21	-01

LOCATION Auria poxet

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BTREAM

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WORCESTER COUNTY ENGINEERING DEPARTMENT WORCESTER, MASSACHUSETTS

DAM INSPECTION REPORT

	More. Water	Dep/ PLACE	Worce	ester	USE 140	soph
	LOM	DATE	Oct.	12, 1950		,
TYPE OF DAM	Earth. Store &	Conc. Spi	linen	CONDITION	6-1-1	•

SPILLWAY

FLASHBOAR	DS IN	PLACE	 RECENT	REPAIRS	
CONDITION	•••		 		
REPAIRS NEI	EDED	•••••••••••••••••••••••••••••••••••••••	 		 ••••••

EMBANKMENT_

RECENT REPAIRS

GATES

RECENT REPAIRS
REPAIRS NEEDED

LEAKS

HOW SERIOUS

DATE Oct. 12, 17,50

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B-8

TOWN Holden		DAM NO. 21-40	
Quinapoxet	Pond	8TREAM	
WORD	ESTER COUNTY ENGINEERI	NG DEPARTMENT	
	WORCESTER, MASSACHU	SETTS	
	DAM INSPECTION R	EPORT	
DWNED BY Worcester	Water Dept. PLACE Worces	ster use storage	
INSPECTED BY E. PETTY-	Hardy-Marden DATE No	v.18,1947	
TYPE OF DAM Earth-s	tone and concrete	CONDITION	
	·		•
SPILLWAY			
FLASHBOARDS IN PL	ACE 18" RECEI	NT REPAIRS 1942	
CONDITION	Good -new apro	n 1942	
REPAIRS NEEDED	New catwalk stringer s belo	w catwalk top-reduce area	
spillway.			••• .
			•
RECENT REPAIRS	none	·····	
	good		
REPAIRS NEEDED	none		• • •
			•
GATES	none		•
RECENT REPAIRS	none		
CONDITION	good		· ·
REPAIRS NEEDED	none	······································	•
LEAKS			•
HOW BERIOUS	Seepage to east of spillway	y-not hazardous.	
		Feb.10.1948	
	DAT		
		Pa head	-
		COUNTY ENDINEER	
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3. VIEW OF DAM AND SPILLWAY DOWNSTREAM CHANNEL FROM LEFT ABUTMENT.



4. DOWNSTREAM FACE OF DAM FROM RIGHT ABUTMENT SHOWING SPILLWAY DOWNSTREAM CHANNEL IN FOREGROUND.



5. CREST AND UPSTREAM FACE OF DAM FROM LEFT ABUTMENT.



6. VIEW OF RIGHT SIDE OF SPILLWAY.

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7. VIEW OF SPILLWAY AND SPILLWAY LEFT ABUTMENT.

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8. SPILLWAY DOWNSTREAM CHANNEL WITH PRINCETON STREET BRIDGE SHOWN AT END OF SPILLWAY CHANNEL.



9. VIEW OF SPILLWAY DOWNSTREAM CHANNEL FROM PRINCETON STREET BRIDGE. NOTE SILL AND V-NOTCH DRAIN IN FOREGROUND.



10. SEEPAGE AT RIPRAP TO THE LEFT OF THE STILLING BASIN SILL.



11. RESERVOIR DRAIN GATE OPERATOR ON DAM CREST. PUMP HOUSE IS VISIBLE ON FAR SIDE OF RESERVOIR.



12. PHOTO OF RESERVOIR DRAIN OUTLET AT SPILLWAY CHANNEL. STILLING BASIN TAKEN DURING TEST OPERATION OF DRAIN.



13. UPSTREAM FACE OF DIKE FROM ITS LEFT ABUTMENT.



14. CREST OF DIKE FROM LEFT ABUTMENT. NOTE TREES GROWING ON THE DOWNSTREAM FACE.

APPENDIX D

HYDRAULIC AND HYDROLOGIC COMPUTATIONS

FIGURES	Page No.
Drainage Area Map Dam Failure Impact Area Map	D-1 D-2
COMPUTATIONS	
Elevations; Surface Areas, Pool Storage Volumes;	D-3
Stage-Discharge Relationship	D - 4
Stage-Discharge Relationship and Storage-Elevation Curves	D-5
Surcharge-Storage Routing; Outlet Works Capacity,	D-6
and lailwater Analysis	D-7
Dam Fatture Analysis	0-7





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JOB NO. 380-6-RT-24 COMPUTED BY Joe H SER & MCKEE CLIENT _______ PROJECT Dani Safety Insp. DATE CHECKED. 7/25/80 DATE 6-20-80 DETAIL Quina poxet Reservoir CHECKED BY JED PAGE NO. ____ - 7

ELEVATIONS

All elevations based on National Vertical Geodetic Datum (NGVD) Concrete Spillway Crest W/flashboards 739.0; W/out flashboards 731.0 Top of Dam Top of Dike (Located to the right of the dam) 738.5 Top of Swale on Princeton Street (Located to the left of the dam) Toe of Dome natural ground @ end of spillway channel near Princeton Street 695.0

SURFACE AREAS

Drainage Area = 12,705 acres \approx 19.85 square variles (from ME Reservoir Surface Areas: @E1. 731.0 \approx 267 acres (from 1953 Metcolf & Eddy Report) @ E1. 733.0 \approx 285 acres @ E1. 740.0 \approx 343 acres (Determined by CDM) @ E1. 750.0 \approx 428 acres "

POOL STORAGE VOLUMES

 $\begin{array}{l} & & \text{Spillway (rest El. 731.0, storage = 3424 acre-feet (from MyEreport)} \\ & & \text{El. 733.0, storage = 3424 + } \left(\frac{267+285}{2} \right) = 3976 acre-feet \\ & & \text{El. 740.0, storage = 3976 + } \left(\frac{285+343}{2} \right) 7 = 6174 acre-feet (Top of Dam) \\ & & & \text{El. 750.0, storage = } 6174 + \left(\frac{343+428}{2} \right) 10 = 10,029 acre-feet \\ \end{array}$

TEST FLOOD DETERMINATION

Based on an hydraulic height of 45 feet and a storage at top of dam (El. 740.6) of 6,174 acre-feet the size classification is INTERNEDIATE, according to COE quidelines.

The dam failure analysis on pages 5-7 indicates a HIGH hazard classification.

Therefore, based on COE guidelines, the test flood is the PMF.

JOB NO. 380-6-KT-24 COMPUTED BY Joe H. SSER & MCKEE CLIENT _____ COE PROJECT Dam Safety Inspection DATE CHECKED 7/25/80 DATE 6-20-80 DETAIL QUING POX et Reservoir CHECKED BY JED PAGE NO. 2-The drainage area is undeveloped, except for some scattered houses throughout the drainage area. It is heavily forested with swampy areas scattered throughout (. Muschopauge Pond, Beated northeast of Quinapoxet Reservoir, is part of the drainage area to Quinapoxet Reservoir but serves as a water supply Rutland and Holden. Therefore, relative to safe (yield the drainage area to Muschopauge Pond (378 abres: 0.59 sq. miles) is independent of the D.H. to Quinapoxet Res. But relative to the test flood it will only set to attenuate the peak flow. It is further assumed that no water will be pumped from the Quinapoxet Reservoir during the test flood period Based on the drainage area characteristics described above, the peak test flood inflow to Quinapoxet Reservoir is based on the flat and coastal " curve of the NED Corps of Engineers "Preliminary Guidance for Estimating Maximum Probable Discharges in Phase I Dam Safety Investigations ". :. PMF = 650 csm x 19.85 sg. Mi = 12,900 cfs STAGE-DISCHARGE RELATIONSHIP Reservoir Water Spillway Discharge Length = 200 ft surface Ekrotion C-volue H-ft Discharge, Cfs (NEVD) Zero (assumes drain pipe) to be closed 733.0 * 733.5 3.3 0,5 233 734.0** 3.4;3.2 |; 3 4 680;3326 3.4 5,440 735.0 5 6 3.5 736.0 7,826 737.0 3.6 10,580 7 138.0 3.7 13,700 NOTES: * The concrete spillway crest is at elevation 731.0, however, normal operation is to keep 2-feet of flashboards along the length of the spillway year-round.

** The spillway flash boards are designed to collapse when the reservoir water level reaches El. 734.0±

D-4



D-5

$\frac{SUPPONTANE GE - STORAGE ROUTING}{Real Test Flood Inflow, Gp = 12,900 cfs; Surcharge El. = 737,75}{Real Test Flood Inflow, Gp = 12,900 cfs; Surcharge El. = 737,75} STOR, = Surcharge Starge = 1495ac ft × 124ft = 1.412 inchesDrainage AreaOutflow, Gp, = Op(i - store) = 12,700(1 - 1412) = 11,940 cfs - El. 737,45STOR2 = (400 × 12)/12, 705 = 1.321 · in; STORAUG = (1.412+1.322)/2=1.367 · in.Gp2 = 12,900 (1 - (1.367/19)) = 11,970, say 12,000 cfs - FEI. 737,45: Real Laflow = 12,700 cfsRouted Post Outflow = 12,000 cfs E Surcharge El. = 737,5 NGVDORAIN CAPACITY @ spillway creatQ = CAVZ9H where E = 0.60, A = 4x4 = 1632.ftH = based on water surface Espillway Creat, El. 733.0 = 733.702 = 31 ftControl Section is at Princeton St. BridgeCrifice flow, Q: 0.7 (370) KeI.H = 2078 H85Elsore - spillway creatChannel flow over Rosdway 2 1.49 AR^{46} (0.01) = Q2WSE Orifice Flow Channel Flow Tok/DistanceTO II is go to 11 (300 cfs)Channel flow over Rosdway 2 1.49 AR^{46} (0.01) = Q2WSE Orifice Flow Channel FlowTO II is Sofo Teli 3:24 B280 (6.930): @ the routed test flood outflow of 12000 cfs thietail water elevation is about 709.7 or about 2.2 fedover the roadway. Thus, the spillway downstream channel$	a na sea anna an sea anna a	<u>20-8</u> 0
Peak Test Flood Inflow, Qp = 12,900 efs; Surcharge El. = 139,75 STOR, = Surcharge Storage = 14953cft × 12"/ft = 1.4/2 inches Draimage Area Outflow, Qp, = Qp(1- <u>STOR</u>) = 12,900(1- <u>1412</u>) = 11,940 cfs \rightarrow El. 737,45 STOR ₂ = (1400 × 12)/12,705 = 1.322-in; STOR _{PUG} = (1.412+1.322)/2=.1367-in. Op ₂ = 12,900 (1 - (1.367/19)) = 11,970, say 12,000 cfs \rightarrow El. 737,45 Reat Inflow = 12,900 cfs Routed Rost Outflow = 12,000 cfs C Surcharge El. = 737.5 NGVD ORAIN CAPACITY C spillway crest Q = CA/29H where C = 0.60, A = 4x4 = 1639.ft H = based on auster surface C spillway Crest, El. 733.0 = 733 702 = 31 ft Q = 0.60 (16)/64.4 (31 = 430 cfs TAILWATER ANALY 515 Channel fbu over Roadway 2 1.89 AR ⁴⁵ (0.01) ^{0.5} Channel fbu over Roadway 2 1.89 AR ⁴⁵ (0.01) ^{0.5} Channel fbu over Roadway 2 1.89 AR ⁴⁵ (0.01) ^{0.5} Q = 13 7490 311 1.45 1980 9,470 T11 15 8050 761 3.24 8280 (6.320) : Q thie routed test flood outflow of 12,000 cfs thie tailway Compared Tailes of Surface of Sufface of Surface of Surface of Sufface of S	ARGE-STORAGE ROUTING	
$STOR_{+} = Surcharge Starge = \frac{14953c.ft \times 12^{4}ft}{12,705 ocres} = 1.4/2 inches$ $Dutflow, Qp_{+} = Qp_{+}(1 - \frac{570R_{+}}{12}) = 12,900(1 - \frac{1412}{19}) = 11,940 cfs \rightarrow El. 737,455$ $StOR_{2} = (400 \times 12)/12,705 = 1.322 - in ; 5TOR_{AUG} = (1.412 + l.322)/2 = 1.367 - in.$ $Sp_{2} = 12,900 (1 - (1.367/19)) = 11,970, say 12,000 cfs \rightarrow El. 737,455$ $:: Reat Inflow = 12,900 cfs$ $Routed Rost Outflow = 12,000 cfs & Surcharge El. = 737.5 NGWD$ $ORAIN CAPWCITY & spillway crest$ $Q = CH/29H where & C = 0.60; H = 4x4 = 1639.ft$ $H \ge based on woter surface & spillway Crest, El. 733.0 = 733.4702 = 31 ft$ $Q = 0.60 (16)\sqrt{k4.4}(31 = 430 ofs$ $TAIL WATER ANALY 515$ $Control Section is at Rincetow St. Bridge = 16.698/5 Channel flow our Rosdway 2.1.69 R R^{45} (0.01)^{6} = Q_{2}$ $WSE Orifice Flow Channel Flow Channel Flow Channel Flow Of 13,000 cfs (0.01)^{6} = Q_{2}$ $WSE Orifice Flow Channel Flow Of 12,000 cfs (0.01)^{6} = 0.60$ $WSE Orifice Flow Channel Flow Of 13,000 cfs (0.01)^{6} = 0.60$ $WSE Orifice Flow Channel Flow of 12,000 cfs (0.01)^{6} = 0.2$ $WSE Orifice Flow Channel Flow Of 12,000 cfs (0.01)^{6} = 0.2$ $WSE Orifice Flow Channel Flow Of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice Flow Channel Flow Of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice Flow Channel Flow Of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow flow of 13,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow flow of 13,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow Of 13,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of how flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,000 cfs (0.00)^{6} = 0.60$ $WSE Orifice flow of flow of 12,0$	st Flood Inflow, Qp = 12,900 efs ; Surcharge El. = 737.73	۲
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$\begin{aligned} & 5TOR_{2} = (400 \times 1/2)/12, 705 = 1.322 - in; 5TOR_{AVG} = (1.412 + 1.322)/2 = 1.367 - in. \\ & Sp_{2} = 12,900 (1 - (1.367/19)) = 11,970, say 12,000 cfs + El. 737,45 \\ & Reat Inflow = 12,900 cfs \\ & Routed Post Outflow = 12,000 cfs & Surcharge El. = 737.5 NGVD \\ \hline SRAIN CAPHOLITY @ spillway oreit \\ & Q = CA/29H \\ & where & & & & & & & & & & & & & & & & & & $	$Q_{p_1} = Q_p(1 - \frac{5TOR_1}{19}) = 12,900(1 - \frac{1.412}{19}) = 11,940 cfs \rightarrow El. $	737.45
$\begin{aligned} & P_{P_{2}} = 12,900 \left(1 - (1.367/19) \right) = 11,970, say 12,000 cfs + El. 737,45 \\ & Peak Inflow = 12,900 cfs \\ & Routed Peak Outflow = 12,000 cfs & Surcharge El. = 737.5 NGVD \\ \hline PRAIN CAPHOITY & spillway crest \\ & Q = CA/2gH & where & l = 0.60, A = 4x4 = 16.39.ft \\ & H > based on water surface & spillway Crest, El. 733.0 \\ & = 733 \cdot 702 = 31.ft \\ \hline Q = 0.60 \left(16 \right) fel.4 (31 = 430 cfs \\ \hline TALLWATER ANALY 515 \\ Control Section is at Princetou st. Bridge \\ & Crifice flow, Q = 0.7 (370) Fel.4H = 2078 H^{0.5} \\ & Crifice flow, Q = 0.7 (370) Fel.4H = 2078 H^{0.5} \\ \hline Channel flow over Roadway = 1.49 AR^{1/5} (0.01)^{0.5} = Q_2 \\ \hline DOB \\ \hline USE \\ \hline TO9 \\ 13 \\ \hline TO9 \\ 14 \\ \hline 15 \\ \hline D0 \\ \hline 11 \\ 15 \\ \hline D1 \\ \hline 15 \\ \hline D1 \\ \hline 11 \\ \hline 15 \\ \hline D1 \\ \hline 15 \\ 15 \\$	(1400 x12)/12,705 = 1.322-in; STORAUG=(1.412+1.322)/2=1.30	67-in.
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JOB NO. 380-6-RT-24 COMPUTED BY OF H CLIENT COE CAMP DRESSER & McKEE PROJECT Dam Safety InspectionDATE CHECKED 7/25/80 DETAIL Quinapoxet Reservoir CHECKED BY JED P DATE 6-20-20 PAGE NO 5-7 DAM FAILURE ANALYSIS a. Project Discharge Prior to Dam Failure. Assume WSE @ routed peak test flood surcharge, El. 737.5 (NGVD) . Q= 12,000 cfs, which would overtop each street on the downstream channel (Quina poxet River) all the way to its point of discharge at the Wachusett Reservoir. The depth of water over each roadway would vary from 1.5 to about 4ft@ River St. One house at state Route 31 would be affected by water about 2 feet above its sill. b. Project Discharge After Dam Failure, WSE = 737.5 Q2= 8/27 (9) 12 Wo (4) 1.5 where g = 32.2 ft/sec ~ Wb= width of failure section Assume got of the mid-her. Longth would fail = 480×0.4 = 192ft 16 = height of failure section = WSE - Toe of Dam El : Q2= 8/27 (32,2) 1/2 (192) (42.5) .5 = 737.5 - 695 = 42.5 ft * 89, 500 cfs Total Failure Flow & Qp = 89,500 + 12,000 = 101,500 say <u>100,000cfs</u> Determine the impact of @ 100,000 cfs discharge on the downstream area. <u>Reach 1</u> - Dan to Princeton Street immediately Disofdom The section geometry was described on page 4 in the Tailwater Analysis Stage-Discharge relationship Total Ficus Channel Flow Orifice Flow WSE 9,500 51,000 60,500 717 97,800 108,400 10,600 722 : WSE @ Princeton St would be 721 = or 13.5 ft above the roadway and over 4-ft above the sill house on the right downstream bank.

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$\frac{5tage - Vischarge Kelotionship:}{WSE} Orifice Flow Channel flow Total Discharge (cfs) 584.8 11,300 15,000 26,300 589.8 12,500 27,900 40,400 594.8 13,600 45,150 58,750 \frac{VSE}{5400} \frac{Surfice Area}{(ac)} \frac{Total Shrage}{(ac-f+)} \frac{Awil Surcharge Storage}{(ac-f+)} (Busene in SSE Q:12 560 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 $. /	0. 4	0//		El. 557.8(FIS Report)
$ \frac{WSE}{S84.8} = \frac{0rifice Flow}{11,300} = \frac{Channel flow}{15,000} = \frac{100}{26,300} = \frac{100}{27,900} = \frac{100}{40,400} = \frac{100}{40,400} = \frac{100}{45,150} = \frac{100}{58,750} = \frac{100}{58,750} = \frac{100}{100} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{210} = \frac{100}{210} = \frac{100}{210} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{210} = \frac{100}{100} = \frac{100}{210} = \frac{100}{100} $	<u>5tage</u>	- Vische	orge Kelationshi	<u>p:</u> 40,4	
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	WSE	Orifice Flow	Channel flow	Total Discharge
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		584.8	11,300	15.000	26,300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		589.8	12,500	27.900	40.400
$\frac{5tor \partial ge}{MSE} = \frac{3urfsce Ares}{(2c)} = \frac{75/3}{54r \circ ge} = \frac{4usil Surcharge Storage}{(2c-ft)} = \frac{5torage}{(2c-ft)} = 5tor$	•	596.8	13 600	45 150	58 750
$\begin{array}{c c} \underline{Storage} \\ \underline{WSE} \\ \underline{SC} \\ 560 \\ 570 \\ 580 \\ 580 \\ 590 \\ 590 \\ 590 \\ 590 \\ 600 \\ \hline \end{array} \\ \begin{array}{c} 3urfice \ Area \\ Total \ Storage \\ Total \ Storage \\ (ac-f+) \\$, ,	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Store	ae			
WSE Surfice Area Total Storage Awail. Surcharge Storage (Asseme in an analysis) 560 0 (ac) (ac-ft) (ac-ft) (ac-ft) use and analysis 560 0	51010	<u> </u>			
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$)C	Jurpice Hred	10131 2400 390 HVBil. Jul	courge storage (Hoseme init.
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JOF NO. 380-6-KT-24 COMPUTED BY. CLIENT COE PROJECT Dam Safety Inspection DATE CHECKED 7/25/80 DATE 6-20-80 DETAIL Quine for Et Reservoir PAGE NO _____7 CHECKED BY____ Capeok dam foilure outflow of 100,000 cfs, WSE = 606 t before routed out flow = 100,000 (1 - Storoge in Resch) = 100,000 (1 - 2506) = 51,500. Storage in Res.) = 100,000 (1 - 2506) = 51,500. C Q= 51,500 cfs, WSE 2 5931; Storage = 1476 \$ Aug Storage = 19912cfi routed outflow = 100,000 (1-1991) = 61,400 ofs say outflow 2 61,500 cfs; corresponding WSE = 595,5 of about 262 feet over the roadway. About 14 houses would be affected by woher depths of 1 to 15 fut. Downstroom of River Street, the area is undeveloped, except for a comple of roadways which would be over topped. The flood wave would attenuate in this area and dissipate into the Wachusett Reservoir. In conclusion of the aforegoing analysis, the hazard resulting from a dam failure would be "HIGH" hazord

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APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

NOT AVAILABLE AT THIS TIME

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