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CHARTLEY POND DAM MA 00814

# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

**APRIL 1979** 

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Norton, Mass.

Chartley Brook, tributary of the Taunton River

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The dam is a 200 ft. long, 10 high earthfill dam. The dam is small in size with a hazard classlification of high. The overall condition of the dam is fair because the outlet cannot discharge the test flood without overtopping. It is recommended that the owher employ a qualified engineer to perform a detainled hydraulic/hydologic analysis to evaluate the required outlet capacity.

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# DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION. CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM. MASSACHUSETTS 02154

REPLY TO ATTENTION OF:

Honorable Edward J. King Governor of the Commonwealth of Massachusetts State House Boston, Massachusetts 02133

AUG 1 6 1979



#### Dear Governor King:

I am forwarding to you a copy of the Chartley Pond Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Department of Environmental Quality Engineering, the cooperating agency for the Commonwealth of Massachusetts. In addition, a copy of the report has also been furnished the owner, Mr. David Opatha, Director, Town of Norton Conservation Commission, Town Hall, Norton, Massachusetts 02766.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Department of Environmental Quality Engineering for your cooperation in carrying out this program.

Sincerely yours,

Incl
As stated

MAX B. SCHEIDER

Colonel, Corps of Engineers

Division Engineer

CHARTLEY POND DAM
MA 00814

TAUNTON RIVER BASIN
NORTON, MASSACHUSETTS

PHASE I - INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM 1.1

# NATIONAL DAM INSPECTION PROGRAM

### PHASE I INSPECTION REPORT BRIEF ASSESSMENT

Identification No.: MA 00814

Name of Dam: Chartley Pond Dam

Town: Norton

County and State: Bristol County, Massachusetts

Stream: Chartley Brook - Tributary of the Taunton

River

Date of Inspection: December 1, 1978

Chartley Pond Dam is a 200-foot long 10-foot high earthfill dam built in the 1800's. A two-lane paved roadway is the crest of the dam while the downstream face includes a concrete wall and portions of the foundations for two structures. The embankment is in good condition but minor maintenance is required. Water discharges through a small outlet controlled by stop logs. An outlet at the dam for a water wheel is blocked and abandoned. An outlet controlled by removable stop logs functions as the spillway for the dam. Removable stop logs at the time of the inspection were at El 102.7 with an effective width of 6.7 feet. Fixed weirs at the side of the outlet are at El 104 and have a total width of 8.5 feet.

Based on Corps of Engineers' Guidelines, the Dam has been classified as "small" and in the "high" hazard category. Accordingly, a test flood equal to one-half the probable maximum flood (PMF) was used for this analysis. Hydraulic analyses indicate that the outlet can discharge a flow of 170 cfs before overtopping the dam at El 105.6. This discharge represents 14 percent of the outflow test flood discharge of 1,230 cfs. The outflow test flood which crests at El

107.3 will overtop the dam by 1.7 feet. Draining the pond to El 96.5 prior to the outflow test flood will not appreciably reduce the amount of overtopping. The outlet cannot pass the test flood even with all stop logs removed, and overtopping of 1.2 feet will occur.

It is recommended that the Owner employ a qualified consultant to perform a detailed hydraulic/hydologic analysis to evaluate the required outlet capacity. Prior to that study the dam should immediately be drained to minimize the potential overtopping. There are no recommended alternatives.

The overall condition of the dam is fair because the outlet cannot discharge the test flood without overtopping. Accordingly, the recommendations and remedial measures outlined above should be implemented within a period of one year after receipt of this Prase I Inspection report.

OF CONNECTION OF

Edward M. Greco, P.E. Project Manager

Metcalf & Eddy, Inc.

Connecticut Registration No. 08365

Approved by:

Stephen L. Bishop, P.E.

Vice President

Metcalf & Eddy, Inc.

Massachusetts Registration No. 19703

STEPHEN
BISHOP
No. 19703 O

This Phase I Inspection Report on Chartley Pond Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

OSEPH W. FINEGAN, JR., MEMBER
Warer Control Branch
Engineering Division

CARNEY M. TERZIAN, MEMBER

Design Branch

Engineering Division

JOSEPH A. MCELROY, CHAIRMAN

Chief, NED Materials Testing Lab.

Foundations & Materials Branch

Engineering Division

APPROVAL RECOMMENDED:

¥ 1

LUE B. FRYAR

Chief, Engineering Division

#### PREFACE

This report is prepared under guidance contained in Recommended Guidelines for Safety Inspection of Dams, for a Phase I Investigation. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff, or fractions thereof). Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate

condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general conditions and the downstream damage potential.

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# OVERVIEW CHARTLEY POND DAM NORTON, MASSACHUSETTS



NORTON, MASS, GUADRANGLE

NORTON, MASS, GUAD

LOCATION MAP ... CHARTLEY POND DAM

# NATIONAL DAM INSPECTION PROGRAM

#### PHASE I INSPECTION REPORT

#### CHARTLEY POND

#### SECTION 1

#### PROJECT INFORMATION

## 1.1 General

a. Authority. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Metcalf & Eddy, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Massachusetts. Contract No. DACW 33-79-C-0016 dated November 28, 1978 has been assigned by the Corps of Engineers for this work.

# b. Purpose

- (1) Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) Encourage and assist the States to quickly initiate effective dam safety programs for non-Federal dams.
- (3) Update, verify and complete the National Inventory of Dams.

# 1.2 Description of Project

a. Location. The dam is located on Chartley Pond, a tributary of Taunton River in the

Town of Norton, Bristol County, Massachusetts (see Location Map and Drainage Area Map).

Description of Dam and Appurtenances. ley Pond Dam consists of a 200-foot long, 10-foot high earthfill dam. The crest of the dam, consists of South Worcester Street, a twolane city street, and a small parking area for the Sinclair Mfg. Co. The 30-foot wide street is paved and drainage catchbasins located at the edge of the pavement discharge into the outlet conduit. Immediately adjacent to the downstream face of the dam are two multi-story brick and wood frame structures. foundation to the structures form an integral part of the downstream face of the dam. embankment fill between the pavement and the structures is grass covered and generally slopes toward the downstream side. downstream face of the dam consists of a concrete wall between the two structures, separated by the discharge channel. The crest of the dam along the crown of the road varies between Elevation (E1) 105.6 to E1 106.1.

The entrance to the outlet conduit is through a concrete structure covered with a concrete slab. Openings are located along the front and The two openings in the front (upstream) are controlled by 2-inch thick stop logs. Each opening at the time of inspection was 3.35-feet wide and 2.6-feet high from the bottom of the slab to the top of the removable stop logs. The invert of the stop logs were at El 96.5. The fixed openings on the sides are barred and 4.25-feet long by 1.3-feet high. Discharge to the downstream channel is through a dry stone masonry conduit. The conduit has three channels, one of which had no flow because of debris. The two channels which are in operation vary in cross-section. Generally, they are about 3- to 5-feet wide and 5- to 6-feet high although there are some local restrictions in width and height within the channel. The two downstream openings narrow to 3 feet and 3-1/2 feet.

A second outlet, which is apparently clogged with debris or otherwise blocked, is located near the west abutment of the dam. This outlet at one time provided water for power for the building across the street (presently the Balfour Co.). Discharge from the intake flowed through a water wheel within the building and out into the downstream channel. Remnants of the foundation to a gate operating mechanism remain on the intake structure. The valve for the pipe is located within the Balfour Co. building but is owned by the Town of Norton.

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The upstream face of the dam consists of a one-foot thick concrete wall. Vertical cracks, varying in thickness from hairline to about 1/4-inch occur at about 3- to 5-foot intervals along the wall.

A small one-story wood frame building is located adjacent to the east abutment where the dam ties into natural ground. The west abutment consists of natural ground which forms a part of Route 123.

- c. Size Classification. Chartley Pond Dam is classified in the "small" category since it has a maximum height of 10 feet and a maximum storage capacity of about 430 acre-feet.
- d. Hazard Classification. Immediately downstream of the dam are two small factories and a parking area for the Balfour Company. Further downstream along the discharge channel are several small businesses and residences. A failure of the dam could adversely affect people within the downstream buildings. Excessive property damage as well as a loss of life is possible. Accordingly the dam has been placed in the "high" hazard category.
- e. Ownership. The dam is owned by the Town of Norton Conservation Commission. Mr. David Opatka, Director, Town Hall, Norton, Massachusetts, 02766, (617-285-6301) granted permission to enter the property and inspect the dam.
- f. Operators. The dam is operated by personnel from the Town of Norton. The single operating

outlet is regulated by manually adjusting the stop logs. The abandoned outlet reportedly is not operable.

- g. Purpose of Dam. Presently, the water in Chartley Pond is not being used. The dam serves only to form an impoundment to control algae development in the upper pond.
- h. Design and Construction History. No information is available on the design and construction history of the dam.
- i. Normal Operating Procedures. The stop logs at the outlet can be adjusted manually. Some are reportedly removed as soon as possible to lower the reservoir in anticipation of storms. The logs are subsequently replaced to keep the pond from becoming too low. Pool level at the time of the inspection was El 103.2. High pool should not reportedly exceed El 104.5, which is denoted by a steel pin at the outlet structure along the upstream wall.

### 1.3 Pertinent Data

- a. Drainage Area. The approximately 4,333-acres (6.77 square miles) drainage area includes numerous small ponds and swamps mostly in the neighboring Town of Attleboro to the west. An estimated 5 to 10 percent of the drainage area is residential with a portion being in downtown Attleboro. The land area is generally flat. Several gravel pits are noted within the area.
- b. Discharge. Normal discharge is through an outlet channel beneath South Worcester Street where the flow is contained in a dry stone masonry conduit. This conduit discharges into a natural stream adjacent to and between the two factories downstream. Flow eventually discharges into Barrowsville Pond about 1/2 mile downstream. Flow from Barrowsville Pond continues eventually to the Taunton River.

Hydraulic analysis indicates that at the outflow test flood discharge rate of 1,230 cfs with stop logs at El 102.7 the dam will be overtopped by 1.7 feet. Even with all stop logs removed. The dam will be overtopped by 1.2 feet.

- c. Elevation (feet above MSL (Mean Sea Level)). A benchmark was established at El 106.0 on the top of the outlet wall. This elevation was estimated from a United States Geological Survey (USGS) topographic map. All elevations used are based on conditions observed in the field at the time of the inspection. All hydraulic calculations are based on the top of stop logs at El 102.7.
  - (1) Top dam: 105.6 to 106.1
  - (2) Test flood pool: 107.3 (with stop logs at El 102.7)
  - (3) Design surcharge (original design): Unknown
  - (4) Full flood control pool: N/A
  - (5) Recreation pool: 102.7
  - (6) Outlet crest (top of stop logs): 102.7
  - (7) Upstream portal invert diversion tunnel: N/A
  - (8) Streambed at outlet of dam: 96.0
  - (9) Tailwater: N/A

### d. Reservoir

- (1) Length of maximum pool: 6,800 feet
- (2) Length of recreation pool: 6,800 feet
- (3) Length of flood control pool: N/A

# e. Storage (acre-feet)

- (1) Test flood surcharge: 340 at El 107.3
- (2) Top of dam: (upstream face) 430 at El 105.4
- (3) Flood control pool: N/A
- (4) Recreation pool: 230 (Approximate)
- (5) Spillway crest: 230

# f. Reservoir Surface (acres)

- \*(1) Top dam: 74.4
- \*(2) Test flood pool: 74.4
- (3) Flood-control pool: N/A
- (4) Recreation pool: 74.4
- (5) Spillway crest: N/A

# g. Dam

- (1) Type: Earthfill
- (2) Length: 240 feet
- (3) Height: (maximum) 10 feet
- (4) Top width: 75 feet
- (5) Side slopes: Upstream; vertical concrete wall
  Downstream; concrete wall and foundation structures
- (6) Zoning: Unknown
- (7) Impervious core: Unknown
- (8) Cutoff: Unknown
- (9) Grout curtain: Unknown

<sup>\*</sup>Based on the assumption that the surface area will not significantly increase with changes in pond elevation from 102.7 to 107.3.

- i. Spillway. There is no spillway at this site. The outlet conduit discharges normal flows.
- j. Regulating Outlets. Two outlets exist at the dam. Aside from the discharge outlet, a second outlet has not been operated for years according to the Owner and is blocked. The outlet to the dam is controlled by manually operated stop logs. Removal of all the stop logs will substantially lower the reservoir to about El 96.5.

#### SECTION 2

#### ENGINEERING DATA

2.1 General. There are four pages of sketches, and sections of past inspection reports, available for the dam (see pages B-3, B-6, B-10 to B-12). These sketches show views of the outlet structure and intake, and one is a plan of the upstream face of the dam. No other plans, specifications, or computations are available from the Owner, State, or County offices relative to the design, construction, or repair of this dam.

We acknowledge the assistance and cooperation of Mr. David Opatka, Director of the Norton Conservation Commission; and Mr. Larry DeSantos of Sinclair Manufacturing Company.

- 2.2 Construction Records. There are no as-built drawings for the dam.
- 2.3 Operating Records. There are no operating records available, and no daily record is kept of the elevation of the pool or rainfall at the dam site.

# 2.4 Evaluation

- a. Availability. There are no engineering data available.
- b. Adequacy. The lack of detailed hydraulic, structural, and construction data did not allow for a definitive review. Therefore, the evaluation of the adequacy of this dam is based on the visual inspection, past performance history, and engineering judgment.
- c. Validity. Drawings shown in this report are consistent with observed field conditions.

#### SECTION 3

#### VISUAL INSPECTION

# 3.1 Findings

- a. General. The Phase I Inspection of the dam at Chartley Pond was performed on December 1, 1978. A copy of the inspection checklist is included in Appendix A. Previous inspections of the dam have been made by others in the past. Records of inspections made in 1959, 1968, 1970, and 1974 are included in Appendix B.
- b. Dam. Chartley Pond Dam is an earthfill dam, the crest of which includes South Worcester Street, a two-lane city street. The crest of the dam is in good condition. The road in this area is a vertical curve with the lowest elevation in the vicinity of the outlet. The pavement is also in good condition. Drainage from the road is collected at each edge in catchbasins which discharge into the outlet channel.

The upstream face of the dam is comprised of a continuous concrete wall (no joints) in fair condition. Minor cracking was noted in regular intervals along the wall. The cracks ranged in size from hairline to about 1/4 inch. The concrete face was pitted and stained. Minor erosion, in the form of small holes, between the wall at the outlet and the embankment was evident.

The downstream wall is constructed of concrete. In several areas along the foot of the wall the concrete was eroded and broken. A leak under the downstream wall, reported in a past inspection report, could not be examined because water was discharging through the channel. It is assumed that the leak still exists. Buildings housing Sinclair Manufacturing and Balfour Company are located on either side of the outlet discharge channels.

The basement of each structure is adjacent to the embankment of the dam. In the past, water from the pond was used at each of these structures. The downstream face appeared in good condition. The earthen portion of the downstream section of the dams was covered with grass except for a small paved parking area.

A depression was observed at the grassed area near the edge of the outlet discharge channel. It appears that soil may have infiltrated through the void in the stone masonry of the discharge conduit.

The abutments of the dam tie into natural ground. The east end continued as South Worcester Street while the west abutment is located at the intersection of South Worcester Street and Route 123.

c. Appurtenant Structures. Two outlets exist at the dam. One, on the west end is an abandoned and blocked intake into the present Balfour Company. The Owner stated that the intake was blocked at the upstream face of the dam and that a valve control located within the Balfour Company Building has not been operated in several years. Discharge from this outlet would flow through the building and into the downstream channel. No other information was available on this outlet.

Discharge through the outlet of the dam is controlled by wooden stop logs. The sides of the outlet structure have two fixed weirs. Removing all of the stop logs will drain the pond. The concrete structure was in good condition. Just to the east of the structure was a steel pin which the Owner stated marked the legal "high water limit" (El 104.5). Staining along the structure and upstream wall indicated the pond level rarely rose above this elevation for long periods of time.

The discharge conduit separates into three channels under the road. The channels were

constructed of dry stone masonry and appeared in satisfactory condition. The channels vary in width. The three channels discharge into two downstream openings, one 3-feet wide by 5.3- feet high and the other 3.5-feet wide by 6.1- feet high. Water passes from these openings into the downstream channel.

- d. Reservoir Area. The area around Chartley Pond is undeveloped, except immediately at the dam. The area consists mostly of flat, swampland. Chartley Pond reportedly resulted from excavating iron ore used at the Old Lennon Forge Iron Works (Balfour Company structure) at the dam. Peckham Street and a railroad track cross the reservoir area.
- e. Downstream Channel. Discharge through the outlet conduit flows between the Balfour Company and Sinclair Manufacturing Company. The flow is contained between stone masonry walls and the foundation of Balfour and Sinclair buildings. About 100 to 200 feet downstream, the area flattens out and discharge is through a shallower natural stream. Small trees line the channel. Eventually flow discharges into the upper reach of Barrowsville Pond about 2,000 feet downstream.
- 3.2 Evaluation. The above findings indicate that the physical condition of the embankment is good. Continued maintenance and the recommendations as listed in Section 7.3 are necessary at this time.

CHARTLEY POND DAM

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#### SECTION 4

#### OPERATING PROCEDURES

- 4.1 Procedures. According to the Owner, the dam is inspected periodically. Generally one 8-inch stop log is reportedly removed, if possible, 2-3 days before imminent storms and replaced when the storm has passed. The stop logs have been removed by unauthorized persons on many occasions and therefore it has been difficult to maintain a high water level.
- Maintenance of the Dam. There is no specific maintenance program for the dam. However, because of its location abutting private property and its use as a roadway, little additional maintenance is required by the Owner.
- 4.3 Maintenance of Operating Facilities. There is no specific maintenance program for the operating facility.
- 4.4 Description of Any Warning System in Effect.
  There is no warning system in effect at this dam.
  However, it is anticipated that abutters would be aware of the water level in the pond and could take appropriate action such as notifying the Owner or other Town authorities.
- Evaluation. There is no regularly scheduled maintenance program. However, the Owner periodically visits the dam. Because of the location and construction of the dam very little maintenance by the Owner is required. A systematic and complete inspection program should be instituted at the dam. Maintenance, as required, should continue to be performed.

#### SECTION 5

#### HYDRAULIC/HYDROLOGIC

# 5.1 Evaluation of Features

General. Drainage to Chartley Pond originates in generally flat swampland in the Towns of Attleboro and Norton. The drainage area consists of about 6.8 square miles of sparsely populated land. An outlet consisting of a small diameter pipe, now abandoned, provided water to a structure occupied by the Balfour Company. Because the control valve for the pipe is downstream from the dam the pipe is always under a hydraulic head. The only other outlet is a conduit and outlet structure which is provided with removable stop logs. Each side of the structure is provided with a fixed level outlet 4.25 feet long which is fitted with a bar rack. The front of the structure was designed for the installation of stop logs which produce a weir 6.7 feet long. At the time of the inspection the stop logs were set at El 102.7. Two fixed weirs are at El 104. Both openings are covered by a concrete slab having a bottom at El 105.3. A high water marker has been installed at El 104.5. capacity of the discharge channels are controlled by two openings which are 3 feet by 5.3 feet and 3.5 feet by 6.1 feet. (See Figures B-1 and B-2).

Overtopping of the upstream wall occurs at about El 105.4. The roadway will be overtopped at about El 105.6. The invert of the upstream side of the two outlets is about El 96.5 which is assumed to be the bottom of the pond. The elevation of the invert of the discharge conduit at the downstream side of the stop logs is El 96.5. The invert at the discharge end is El 95.0. There is no other low level outlet at the dam.

- b. Design Data. There are no hydraulic computations available for the design of this dam.
- c. Experience Data. Hydraulic records are not available for this dam. Detailed information on the past performance of the dam is unknown. The Owner stated he has had difficulty maintaining high water levels because of unauthorized persons removing the stop logs. A past inspection report indicated the Owner was able to maintain a water level which prevented overtopping of the dam in the 1955 (record) flood. However, minor overtopping of the dam has reportedly occurred periodically.
- d. <u>Visual Observation</u>. The outlet structure appears in good condition. Water is impounded by the use of stop logs which could be removed although with some difficulty.
- Test Flood Analysis. The Probable Maximum Flood (PMF) rate was determined to be 400 cfs per square mile. This calculation is based on the average slope of the drainage area of 0.7 percent, the pond-plus-swamp area to drainage area ratio of 29.5 percent, and the U.S. Army Corps of Engineers' guide curves for Maximum Probable Flood Peak Flow Rates (dated December 1977). Applying one-half the full PMF to the 6.77 square miles of drainage area results in a calculated peak flood flow of 1,400 cfs as the inflow test flood. By adjusting the inflow test flood for surcharge storage, the maximum discharge rate was established as 1,230 cfs (182 cfs per square mile), with a water surface at El 107.3. This analysis assumes stop logs placed to El 102.7 and the abandoned outlet closed.

Hydraulic analysis indicates that the outlet can discharge 150 cfs at El 105.4 which is the elevation of the top of the upstream wall of the dam. At this elevation water begins to spill onto the roadway and crest of the dam.

At the maximum discharge rate of 1,230 cfs at El 107.3 the roadway and low area on the crest

of the dam (El 105.6) would be overtopped by 1.7 feet. At El 105.6 the outlet would be discharging 170 cfs or 14 percent of the test flood.

The impact of permanently removing all the stop logs (to El 96.5) was evaluated. Under these conditions, the outlet conduit would pass 37 percent of the test flood before overtopping at El 105.6. Overtopping would be 1.2 feet at El 106.8.

Completely draining the pond prior to the test flood has little effect on preventing over-topping under the test flood. Prior inspection reports also indicate the dam has inadequate outlet capacities.

Historical information and past inspection reports indicate the dam was not overtopped in the 1955 (record) flood. The Owner states that the dam has been overtopped in several instances because stop logs were not removed sufficiently ahead of time. During the times the dam was overtopped the road remained passable to trucks. No damage to the dam or adjacent structures occurred.

With the water surface at El 102.7 (present top of stop logs), no inflow, and the removal of 1 foot of stop logs the dam could be lowered 1 foot in about four days. Under the same condition, if 4 feet of stop logs were removed, the pond could be lowered 1 foot in about 12 hours.

Dam Failure Analysis. Assuming a failure of the dam with the water surface at El 105.6, which is the lowest elevation on the crest of the roadway and dam, the peak discharge flood flow would be about 1,100 cfs. At El 105.6, the spillway would be discharging 170 cfs which would produce a 4-foot depth of flow. Failure of the dam would produce a total depth of 7.8 feet in the channel. It is probable that the resulting flood wave could have a severe impact on the Sinclair Manufacture and Balfour Co. buildings immediately downstream as well as several businesses and a few residences further downstream. The approximate flood impact area is shown on the location map, page iv.

#### SECTION 6

#### STRUCTURAL STABILITY

# 6.1 Evaluation of Structural Stability

a. Visual Observations The evaluation of the structural stability of Chartley Pond Dam is based on the visual inspection conducted on December 1, 1978. A detailed discussion of the visual inspection appears in Section 3. Based on this inspection the dam is considered to be in good condition except for the outlet which cannot pass the test flood.

Except for increasing the capacity of the outlet, only minor maintenance and regular inspections are required to assure continued performance of the dam.

b. Design and Construction Data. Discussion with the Owner and State personnel indicate there are no available plans, specifications or computations on the design, or construction of the original dam.

Information does not appear to exist on the type, shear strength, and permeability of the soil and/or rock materials of the embankment.

- c. Operating Records. There is no instrumentation of any type in Chartley Pond Dam, and no instrumentation was ever reported installed in this dam. The performance of this dam under prior loading can only be inferred from physical evidence at the site.
- d. <u>Post-Construction Changes</u>. There are no asbuilt drawings available for Chartley Pond Dam.
- e. Seismic Stability. The dam is located in Seismic Zone No. 2, and in accordance with recommended Phase I guidelines, does not warrant seismic analysis at this time.

#### SECTION 7

# ASSESSMENT, RECOMMENDATIONS, AND REMEDIAL MEASURES

### 7.1 Dam Assessment

a. Condition. Based upon a visual inspection of the site and limited operational or maintenance information, there are minor deficiencies which should be corrected to assure continued performance of the dam. Generally, the dam is considered to be in fair condition since the outlet cannot discharge the test flood without overtopping the dam.

Hydraulic analysis indicate that the outlet can discharge 170 cfs with the water surface at El 105.6 which is the low point on the crest of the roadway. An outflow test flood of 1,230 cfs (one-half PMF) at El 107.3 will overtop the dam by 1.7 feet. This analysis was based on stop logs positioned to El 102.7. Even if all the stop logs were removed the dam would still be overtopped during the test flood.

- b. Adequacy. The lack of detailed design and construction data did not allow for a definitive review. Therefore, the evaluation of the adequacy of this dam is based primarily on visual inspection, past performance, and engineering judgment.
- c. <u>Urgency</u>. The recommendations and remedial measures should be implemented by the Owner within one year after receipt of this Phase I Inspection Report.
- d. Need for Additional Investigation. Additional investigations to further assess the adequacy of the outlet are outlined below in Section 7.2 Recommendations.

7.2 Recommendations. It is recommended that the Owner employ a qualified consultant to perform a detailed hydraulic/hydrologic analysis for the purpose of increasing the outlet capacity.

Recommendations on repairs and maintenance procedures are outlined below under Section 7.3 Remedial Measures.

# 7.3 Remedial Measures.

- a. Operating and Maintenance Procedures. The overall condition of both the dam and appurtenant structures appear to be in fair condition because of the small spillway capacity. It is recommended that the following specific maintenance or actions be performed:
  - (1) Until such time as when the hydraulic analysis and evaluation has been completed and recommendations incorporated, all the stop logs should be removed and the pond drained to minimizing potential overtopping.
  - (2) Fill holes near the downstream wall and at the outlet.
  - (3) Investigate the condition of the blocked outlet.
  - (4) Implement a systematic program of maintenance inspections. As a minimum the inspection program should consist of a bi-monthly (every two months) inspection of the dam and appurtenances, supplemented by additional inspections during and after severe storms. All repairs and maintenance should be undertaken in accordance with all applicable State regulations.
  - (5) Technical inspection of this dam should be continued on a bi-ennial (every two years) basis.

- (6) Institute a definite plan for surveillance and a warning system during periods of unusually heavy rains and/or runoff.
- 7.4 Alternatives. There are no recommended alternatives.

# APPENDIX A PERIODIC INSPECTION CHECKLIST

### PERIODIC INSPECTION

#### PARTY ORGANIZATION

PROJECT_	CHARTLEY POND DAM		DATE DEC. 1, 1978	-
			TIME 8 AM - 12 Noon	<u>n</u>
			WEATHER Clear, co	Īq
			W.S. ELEV.103.21	U.SDN.S
PARTY:			Assumed benchmark El. outlet structure	106 at
1	R. Weber	6.		
2	C. Sweet			
3	W. Checchi	8.		<del></del>
4	H. Lord			
5	L. Branagan			
	PROJECT FEATURE		INSPECTED BY	
1	Dam		Weber/Branagan	
2	Spillway		Weber/Branagan	
3				

page 1 of 5

PROJECT CHARTLEY POND DAM	DATE Dec. 1. 1978
PROJECT FEATURE Dam	NAME_R Weber
DISCIPLINE Geotechnical	NAME
AREA EVALUATED	CONDITIONS
DAM EMBANKMENT	
Crest Elevation	Elevation varies from El. 105.6 to El. 106.1
Current Pool Elevation	E1. 102.7
Maximum Impoundment to Date	Unknown
Surface Cracks	None visible
Pavement Condition	Excellant
Movement or Settlement of Crest	None visible
Lateral Movement	None visible
Vertical Alignment	Sag curve
Horizontal Alignment	Straight
Condition at Abutment and at Concrete Structures	Good-ties into natural ground and roadway
Indications of Movement of Structural Items on Slopes	None visible
Trespassing on Slopes	Roadway
Sloughing or Erosion of Slopes or Abutments	Erosion at outlet headwall-minor depression in crest at outlet conduit discharge end
Rock Slope Protection - Riprap Failures	Concrete wall forms upstream face
Unusual Movement or Cracking at or near Toes	None visible
Unusual Embankment or Downstream Seepage	None visible
Piping or Boils	None visible
Foundation Drainage Features	Unknown
Toe Drains	Unknown
Instrumentation System	Unknown
	page 2 of 5

DATE DEC. 1, 1978
NAME R. Weber
NAME
CONDITION
None
Submerged
None visible
None
None visible
Unknown
Unknown
Unknown
Unknown

PROJECT CHARTLEY POND DAM	DATE Dec. 1, 1978				
PROJECT FEATURE Dam	NAME R. Weber				
DISCIPLINE Geotechnical	NAME				
AREA EVALUATED	CONDITION				
OUTLET WORKS - TRANSITION AND CONDUIT	Conduit formed by dry stone masonry- good condition				
General Condition of Concrete	Boot concision				
Rust or Staining on Concrete	Not applicable				
Spalling	Not applicable				
Erosion or Cavitation	Not applicable				
Cracking	Not applicable				
Alignment of Monoliths	Good-no masonry out of place				
Alignment of Joints	Not applicable				
Numbering of Monoliths	Not applicable				

PROJECT CHARTLEY POND DAM	DATE Dec. 1, 1978
PROJECT FEATURE Outlet	NAME R. Weber/L. Branagan
DISCIPLINE Geotechnical/Hydraulics	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL	Generally good-some erosion at water line Periodic cracks (hairline to ½")
General Condition of Concrete	
Rust or Staining	Moderate staining below water line
Spalling	None visible
Erosion or Cavitation	None visible upstream-slight
Visible Reinforcing	None visible
Any Seepage or Efflorescence	None visible
Condition at Joints	Fair
Drain Holes	None visible
Channel	
Loose Rock or Trees Over-	None overhanging but small trees and boulder within channel

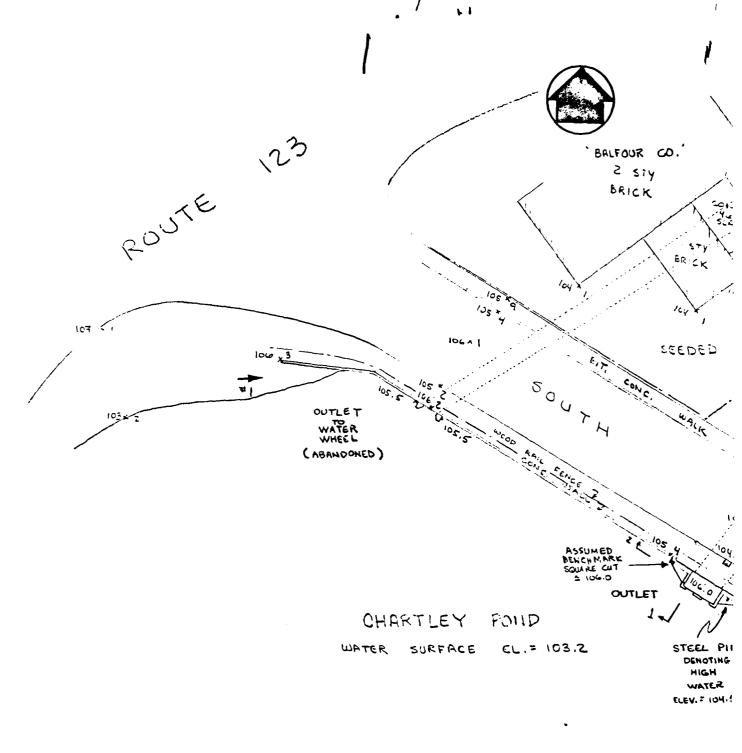
Fair

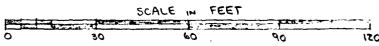
Condition of Discharge Channel

#### APPENDIX B

# PLANS OF DAM AND PREVIOUS INSPECTION REPORTS

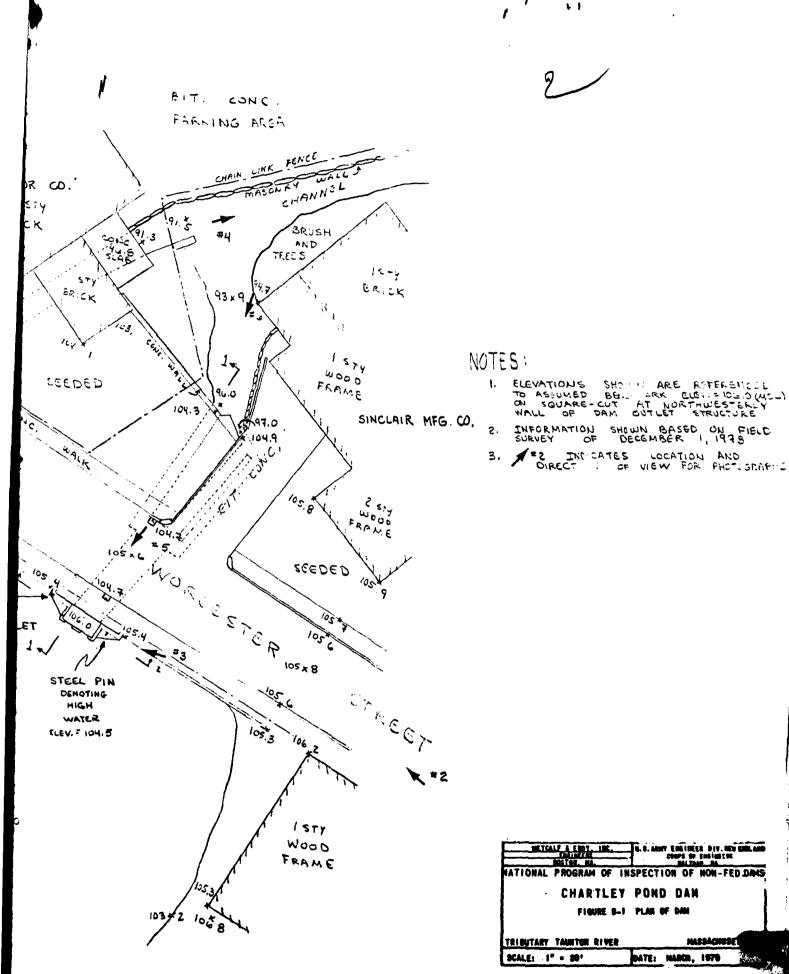
	Page
Figure B-1, Plan of Dam	B-1
Figure B-2, Sections Through Dam	B-2
Previous Inspections	B-3

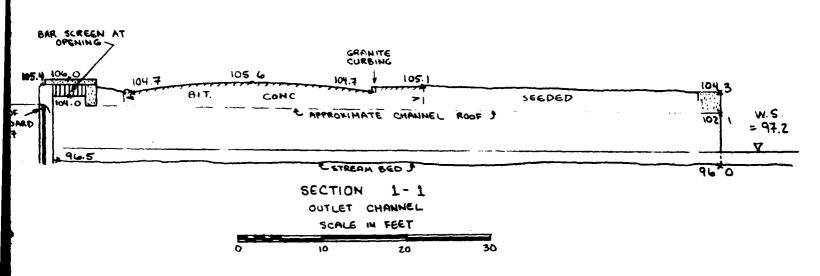


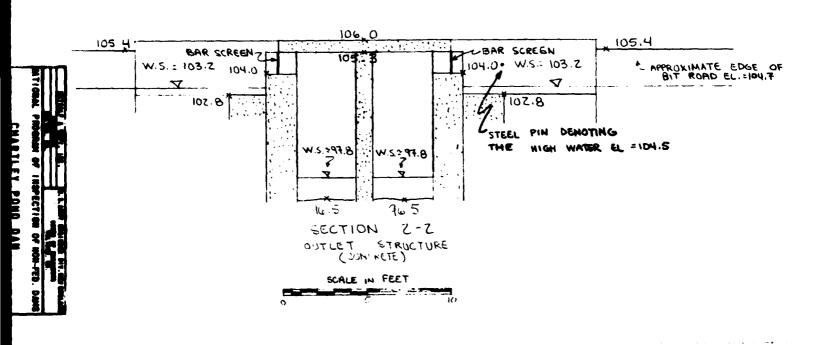


METCALF & EDDY, INC.

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1.1

# BRISTOCKOUNTY, MASS. DATA SHEET B INSPECTION FORM FOR DAMS

en Borton	Date of Inspection 1/6/59
a 80.	Inspected By JR - MA
Chartley Pond	Organization Hapfes, Mariling & Bushanas, It
	turdy Mill, South Morecator Street
Reference: Uptress of 616 S	(Planned - to use pend as
	heat exchange-Sinclair opposed to elimination of dan)
ner of hem Sinclair Mig. Pr	metion of Dam / Hose at present
leads nor Biv. of Vatorusva, Mans. BPV)	
sinage Area <u>1.2 Mg. Mis</u> Churucter jor Fleed a 2100 efs reduced to 500 efs	by evailable storage especity
ood of Record (date) 1955 pt Pleed p 700	scharge (or high pater el.)
meral Description of Dam and Discharge	
Earth - 2 Sluiceways - manually v Northerly Allice shetreeted by de	therem stoplege. bris
Dometroom channel is inadequate.	
timated Discharge Capacity: 350 efs (5'	head, 14' off. length)
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wood	Gone walls
100	
	50'E 18 1
Sa worcesfor SA 30	
	A' 1 2 2 2 3 1 8' 1
CHARILEY	Y POND E TEL
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	(obstructed) B-B
marks and Recommendations: Recommendations	
Discharge Snovisione images	
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BRISTOL COUNTY, MASS. No-1 Dam No. Norton Town: INSPECTION REPORT & DATA FOR DAMS Stream: PREPARED FOR THE BRISTOL COUNTY COMMISSIONERS Chartley Pond Pond: BY HAYDEN, HARDING & EUCHANAN, INC., EOSTON, MASS. Date: 1-6-59 Sinclair Mfg. - So. Worcester Street

(Planned to use pond as heat exchange JHR - RMB CONDITION RATING His Address: Structural: Function of Dam: Sinclair onnosed to elimination of dam Hydraulic: esenilocation & Access: Unstream of Old Sturdy Mill. South Worcester Street General: Fair Tat. 41 57 00 Long. 71 13 40 Norton PRIORITY: Prainage Area: 6.2sq.mi.;Ponds: ac. : Res. Gdam: KINISON-COLBY FLOODS Character of B.A.: flat. swampy Minor: stimated 350 cfs (5 head, 14' eff, length) Major: 2100 \* cfs Discharge Rare: cfs Meximm: Capacity: cfs General Description of Dem and Discharge Control: Farth - 2 sluiceways manually withdrawn stonlogs. Northerly sluice obstructed by debris Downstream channel is anadequate. Sketch (Not to Scale): ycons walls Unto 50. Worcester CHARILEY POND 8 - B Remarks and Recommendations: Reconstruction proposed in House #3270 Discharge provisions inadequate, Downstream channel inadequate. Owner has, however, been able to maintain pond elevation during all floods of 1955 (record year) Recommend new spillway, Channel widening downstream. Floods per Div. of Waterways, Mass. DPW) \* reduced to 500 cfs by available storage capacity Design Flood : 700 cfs (per House #3270) Nate Comment Same Condition Dam No.

B-4

CHARTLEY POND DAM

. 1

# BRISTOL COUNTY, MASS. INSPECTION REPORT FOR DAMS

DAM NO. No - 1
TOWN: Norton

١.

PREPARED FO BY UNIVERS INSPECTION DATE	REMARKS & RECOMMENDATIONS	<del></del>
3-24-70	Southerly sluice is topped by 8". Some erosion of the concrete and stone wall downstream of southerly sluice has occurred. Flanking on northerly side of downstream wall. Northerly sluice is still blocked; should be claimed to relieve flow through southerly sluice. Discharge provisions inadequate. Downstream channel beyond buildings is in good condition.	
	•	
		•

Supplement to original report and data by Hayden, Harding & Buchanan, Inc.

DAM NO. No - 1

chartley fond Wall 8 29-74 6-3-218-1 DETAIL CONC. DAM. DETAIL CONC. DAM B' 1490 - 2+17.5 SIDE VIEW

of Deeds	INSPECTI Date of Prev	Contract  Norten M  Town Stal	-3-74
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B. Is there a stoage impoundment in the	area or flood pla	in downstrea	e of dam which	n could accomm	plate the
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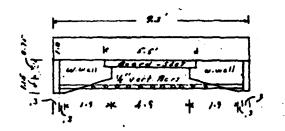
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"HARTIEY POND. NORTON 6-3-218-1 BK 17916 (120, 121) itenstone B 1190 Top VIEW 1 1 SCALE I'- 4'

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Front Yiew

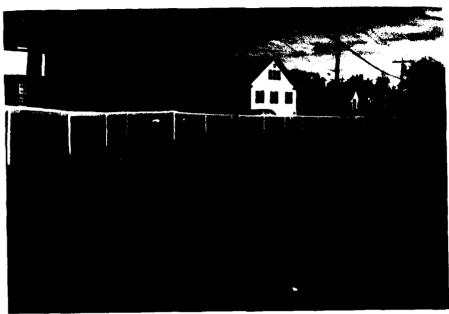


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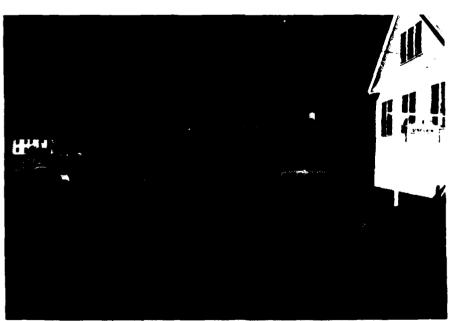
chartley Fond - Norton So Worcester St.

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APPENDIX C **PHOTOGRAPHS** 



NO. 1 VIEW OF UPSTREAM FACE



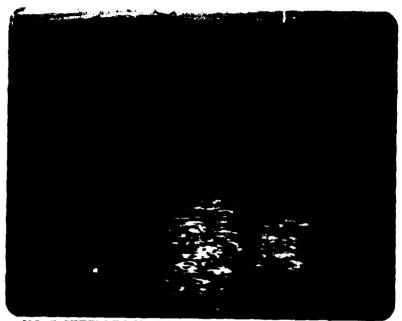
NO. 2 VIEW OF ROADWAY ACROSS CREST OF DAM



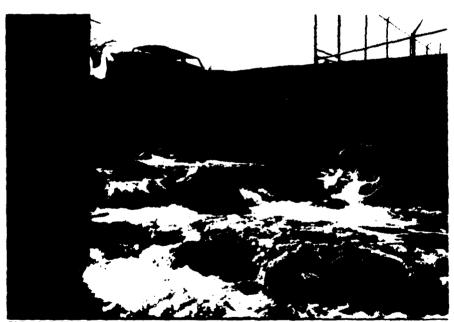
NO. 3 VIEW OF OUTLET STRUCTURE



NO. 4 VIEW OF DOWNSTREAM CHANNEL



NO. 5 VIEW OF DISCHARGE CONDUIT THROUGH DAM



NO. 6 VIEW OF OUTLET AND DOWNSTREAM DISCHARGE CHANNEL

#### APPENDIX D

# HYDROLOGIC AND HYDRAULIC COMPUTATIONS

					Page
Figure	D-1,	Drainage	Area	Map	D-1
Computa	ations	3			D-2

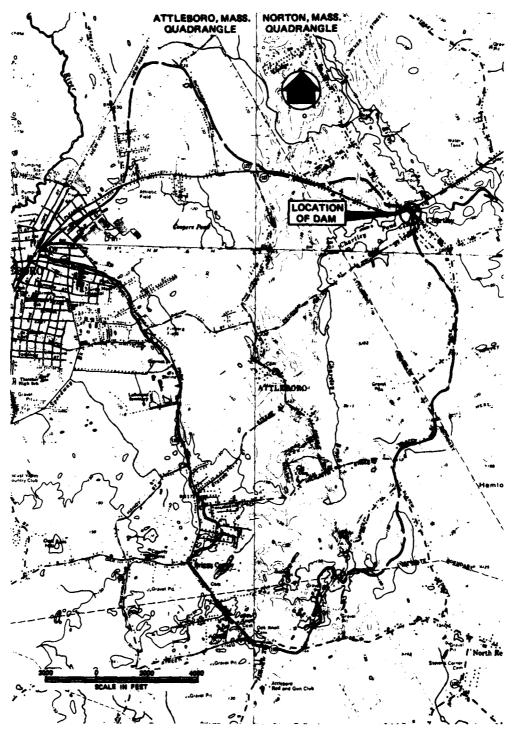


FIG. D-1 DRAINAGE AREA MAP -- CHARTLEY POND

Project			Non Fed. Dan		6191	Poge	1 0 6
Subject	50	stol Ca	onty, Mass.	Comptd. By	LEB	Date : /	(12/79
Detail _	CI	HARTLEY	POND	Ck'd. By	RPV	Date	133139
I			Storage			lows	
	2-	Swamp(s Tota	Area: 0.17 ) Area: 11+11 I Area Pond	7+,26+,05+,100 E(s) É Swamp	o, <b>56 4,</b> 08+ 04 o(s) ;	+.59+.23+./	0.16 mi <sup>2</sup> 5 = 1.84 m 2.00 m
!	<u></u>	- To Ponds	Swamps =	6.77 - 29	1.5%-+		
	3	173-103	=,007	} <u>Sa</u> y	Ave Slope	= 0.7%	i
	Val Fla Size	ues the f t & Coasta : Class: 5m	Curves for Rail and all stazerd	ta was est. takun ed <b>40</b> .Pot.: High	mated to	be below.	,
	5-	Test Flo	od Inflow	= 2 (400)	6.77 =	1400 cfs	
	/a	Dan 1 5 to					
-	•	Pond Sto		0.12 .	: 1 0	lan 102	-
	•	Based	d avea 18 on a Const	t over	through	en 103.	
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**v** 1

# Discharge Relations

### A - Spillway

2-3.35 wide stoplog weirs "Zerisk crestel. 102.7 for Q, 2-4.25 wide fixed weirs with crest el. 104 for Q. Both of above are covered by slab with both el 105.3± Say; all of above become orifices for pond elou > 106 Use "Hydro Tables" williams & Hosen, for weir flow (p=30) Use Q = 6, A Vigh for orifice flow "Co=0.61 [85: Vii i 54.11"]

Pond El.	103	104	105	104	107	108	109	106
Q,	4	3D '	80	130	150	170	190	120
$Q_2$		-	30	80	80	100	110	60
£ Q.	4	30	110 Weir	210	230	270	300	180
- 4,			Weir		0	rifice		

B - Crest Flow
Use 8=2.55 H"5 [Ref.: V.T.Chow "Open Chan Hydr" pg 52]
Crown of So. Worce sten St controls: 130@105.7= £ 110@106.1=

Pond El.	106	107	108
Φ,	50	490	1160
Q,	-	240	730
10	50	730	1890

# C - Culvert Capacity - as pipe

1@ 3.0 mide x 5.3' hi - 90'long - Elev. & outlet 100.6 ± 1@ 3.5! wide x 6.1'hi - 80' long Elev & outlet 100.6 ±

Avail. Hd. = Ho = Entloss + Exitless + Friet. & = [0.5+1.0+0.5] = 24

```
Ent. Water El.
                     103
                              104
                                         105
                                                        By Inspection, culvert capacity will not control discharge, under pipe flow control.
                                         4.4
                              10,5
                                         11.9
                      8.4
                             167
                                        183
                     140
                                         254
                            224
   ٤q,
                                        443
                             311
```

# Discharge Relations - cont.

#### D - Low Level Outlet

1-Assume Partial Removal of Spillung Stoplogs to new crest elev. 101.7 with pond at elev. 102.7.
Initial disch. = 2(3.35)(3.35cfs/ft.) = 22 cfs

Time to lower poud 1' = (0.12+0.02) 43560(640) = 98 hours -tolong?

2-Assume Partial Removed of Stoplags to new crest elev.
of 98.7 with pond at elev 102.7 [say bot. 2' silted up]
Initial disch. = 2(3.35)(26.75 cfs/4) = 176 cfs

Time to lower pond 1 = .14 (4150) 640

1/2 (176) 3600 = 12.3 hours

# (III) Crest Flow Conditions

# A - Stoplogs in as Found

Pond El. under Test Flood - 107.30 L.P. on Crest (street crown) - 105.57

Max. Crest Flow = 2.55 (1.73) = 5.80 cf s / ft
Under Critical Flow conditions.

4 = 1.01 ft V2 = 5.71 fps.

# B'- Stoplogs removed

Max. depth on crest = 106.8 = 105.57 = 1.23'

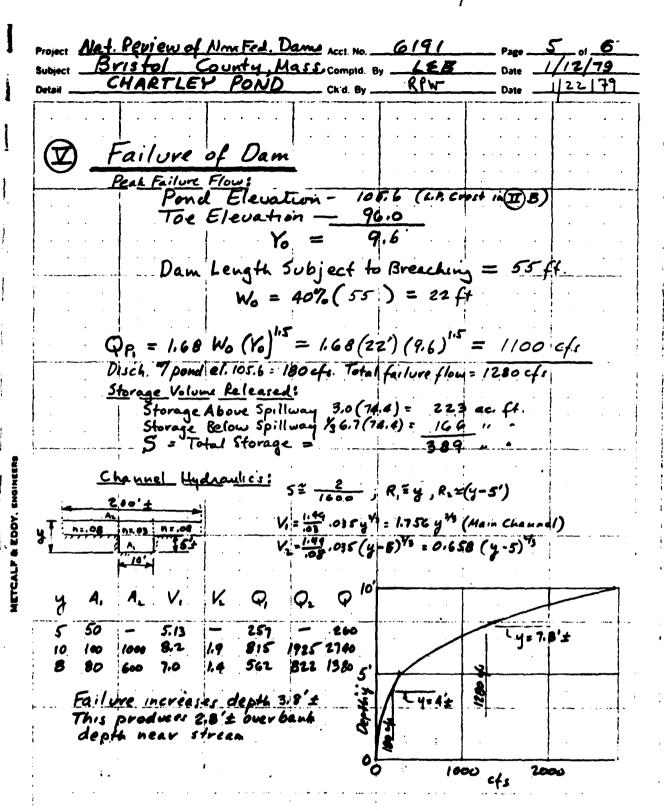
Max. Crest Flow = 2.55(1.23)"5 = 3.5 efs/ft,

As Critical Flow" ye = 0.72 ft.

Ve = 4.86 fp.

Net. Review of NonFed. Dams Acct. No. 6191 Bristol County, Mast. Comptd. By CHARTLEY POND Reu 4/2/79 - Lear 1/22/79 Discharge, Storage & Storage Function us Bond Elev. 8-8 10/ 8-Fre-5.L.in #lements /2/11 A"TEQ4= 1230 c.fs. 50 121 00 1 = N Note: a P Discharge El. 8 -106. 03 \$ 20 11. B test 1. \$5 6.5.m. ₹0-0 101 63 3 ANOd STEN'

D-5



Time to Drain!

43560 (389)
3600(1)(1100) = 8.6 Hours, or 513 minutes

Project Nah. Review of Non Fed Dams Acct. No. 6191

Subject Brishel County, Mass. Comptd. By LES Date 3/2/79

Detail CHARTLEY POND Ck'd. By RPW Date 3/5/79

# VI) Special Discharge Relation

Purpose: Determine effect of removal of all or major number of stoplogs

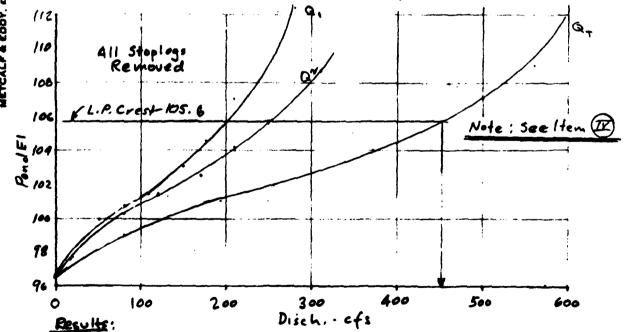
## A - Calc. Culvert Capacity under Inlet Control

Ref.: V.T. Chow Open Chan. Hydr. Fig. 17-29

Culvert #1 - 3.0 wide x 5,3 high } Pata based on Culvert #2 - 3,5 wide x 6,1 high } outlet conditions Invert E1, 96.5

4/4 0.6 0.8: 1.0 1.25 1.5 3,0 48 37 16.5 50 69 9/ 80 145 50 110 170 103.1 99.7 104.5 107.1. BWEL. 100.7 101.8

60 72 89 120 48 80 170 210 250 150 310 420 · 101.4 102.6 104.1 105,7 1087, 114.8 Pond El. 100.2



All stoplage removed; initial pond elev. 96.5; storage to low point -105.6 Storage Depth -9.1; T.F. out = 1400 - 36.6 (9.1) = 1069 efs. Dam would Mar. discharge at pond elev. 105.7 = 450 + Jover top

D-7

#### APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

INVENTORY OF DAMS IN THE UNITED STATES STATE ICENTITY DIVESON STATE COUNTY DIST STATE COUNTY DIST. LATITUDE LONGITUDE REPURT DATE (NORTH) (WEST) DAY MO YR 7113.6 17APR79 POPULAR NAME NAME OF IMPOUNDMENT (8) (6), DIST FROM DAI NEAREST DOWNSTREAM LEGION BASIN RIVER OR STREAM POPULATION CITY-TOWN-VILLAGE NURTON 9869 TR-THREEMILE RIVER (#) (D)
IMPOUNDING CAPACITIES HYPRAU HERGHT YEAR TYPE OF DAM PURPOSES MAXIMUM NORMAC COMPLETED 28 356 Te REMARKS >>=NATE APPROXIMATE (i) POWER CAPACITY 0/8 SPILLWAY NAVIGATION LOCKS CASTH TYPE WATH LENGTH WIDTH LENGTH WIDTH LENGTH WIDTH LENGTH WIDTH 6700 (1) · ENGINEERING BY OWNER CONSTRUCTION BY UNKNOAN UNKNOWN TOWN OF NORTON ❷ CONSTRUCTION OPERATION DESIGN MAINTENANCE MOBE MONE NOSE THE F (9) INSPECTION DATE INSPECTION BY **AUTHORITY FOR INSPECTION** DAY | MO | YR 010FC78 PUBLIC LAN 92-367 METCALE AND EDRY THE. (3) REMARKS

**I** 

