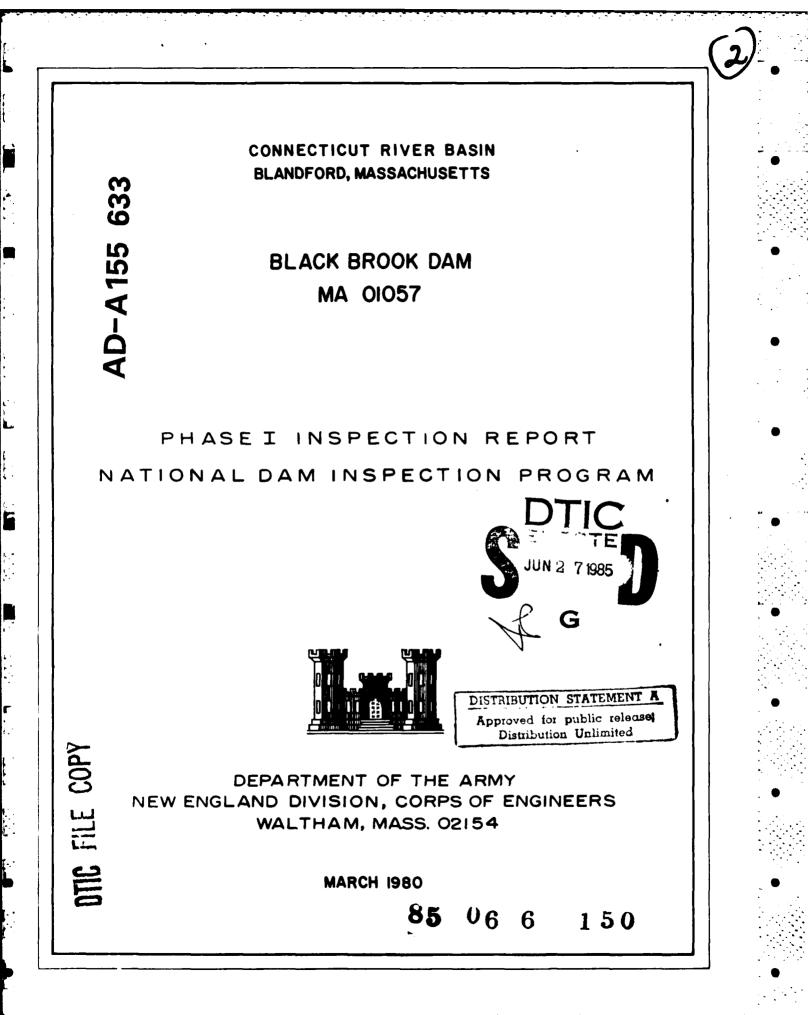
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#### DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION, CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02254

REPLY TO ATTENTION OF:

NEDED

MAR 1 7 1981

Honorable Edward J. King Governor of the Commonwealth of Massachusetts State House Boston, Massachusetts 02133

Dear Governor King:

Inclosed is a copy of the Black Brook Dam (MA-01057) Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

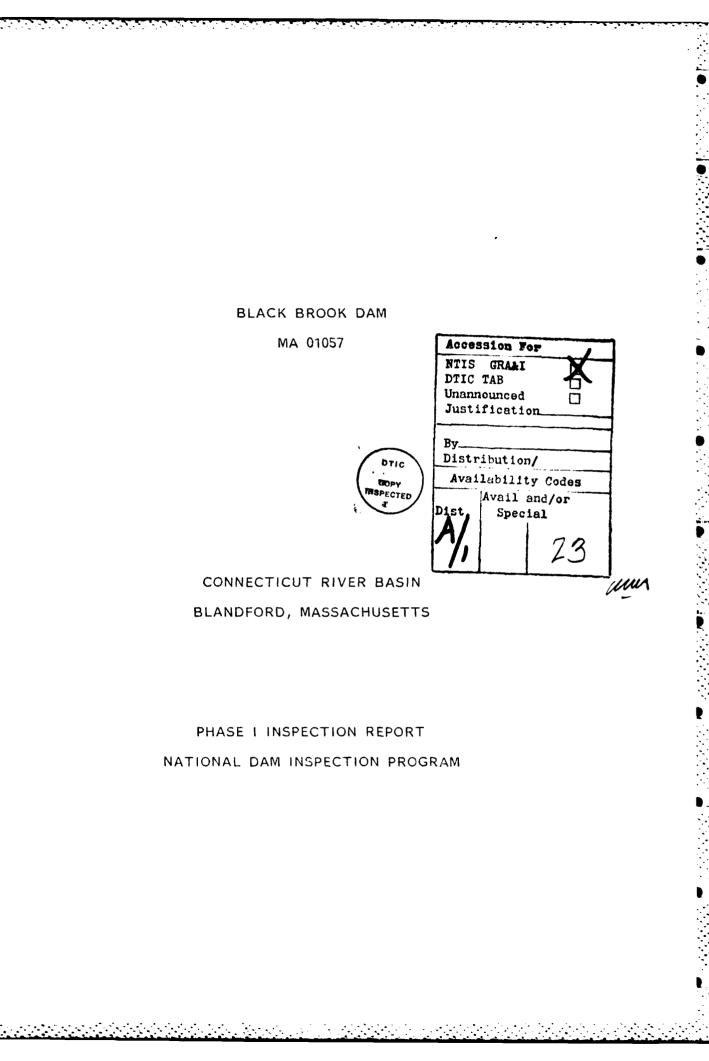
A copy of this report has been forwarded to the Department of Environmental Quality Engineering, the cooperating agency for the Commonwealth of Massachusetts. In addition, a copy of the report has also been furnished the owner, Town of Russell, Russell, MA..

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Department of Environmental Quality Engineering for your cooperation in carrying out this program.

Sincerely, he lette

Incl As stated C. E. EDGÁR, III Colonel, Corps of Engineers Division Engineer



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#### NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.: Mass. D.P.W. No: Name of Dam: Town: County and State: Stream: Date of Inspection:

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MA 01057 1-7-33-8 Black Brook Dam Blandford Hampden County, Massachusetts Black Brook 11/20/79

# BRIEF ASSESSMENT

The Black Brook Dam, is located on Black Brook a tributary to Bradley Brook and the Westfield River and is in the Town of Blandford, Massachusetts. The dam site is approximately 2.6 miles upstream along Bradley Brook and Black Brook from the Town of Russell and is located off of Martin Phelps Road in Blandford. The dam is a multiple purpose water supply and flood protection facility which is owned by the Town of Russell through its Water Commission. It was designed by the U.S. Department of Agriculture, Soil Conservation Service and was completed in 1971. The dam is an earthfill embankment about 1168 feet in length, and 60 feet in height and has a reinforced concrete principal spillway which maintains the water supply pool level and controls the release of stored floodwater, and a 50 foot wide earth and ledge excavated emergency spillway channel in the right abutment.

The dam and appurtenances were found to be in <u>FAIR</u> condition. The visual inspection indicated that silt from under the upstream riprap is being washed out by runoff and wave action to form small deltas in the pond, the trash rack on the riser has been damaged, the toe of the dam is wet along the abutments and the floor of the discharge channel of the emergency spillway is wet. Some maintenance and minor remedial work is required as listed in Section 7.

The test flood for this dam has been determined to be the Probable Maximum Flood (PMF), based on a classification of <u>INTERMEDIATE</u> size and <u>HIGH</u> hazard. The drainage area is 2.3 square miles and the PMF test flood is 5,800 CFS. Routing the test flood through the reservoir, with the initial pool level at the water supply pool elevation, results in a test flood outflow of 2,700 CFS which does not exceed the capacity of the spillways. Pool elevation at test flood conditions is 893 MSL which is 3 feet below the top of dam.

The combined spillways have a capacity of about 5000 CFS with the water level at the top of the dam. This capacity is about 185% of the routed test flood outflow from the reservoir.

Failure of the dam would pose a serious threat to approximately 75 structures, most of which are houses, in the Russell area, one major highway bridge, and one secondary road crossing.

The recommendations for additional investigations and recommended remedial measures as listed in Section 7 should be implemented within one year of receipt of this report by the Owner.

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SANITARY

John W. Powers Massachusetts Registration 23106 This Phase I Inspection Report on Black Brook Dam (MA-01057)

has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the <u>Recommended Guidelines for Safety Inspection of</u> <u>Dams</u>, and with good engineering judgment and practice, and is hereby submitted for approval.

Homman Wathur

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ARAMAST MARTESIAN, MEMBER Geotechnical Engineering Branch Engineering Division

Carney M. Tazis

CARNEY M. TERZIAN, MEMBER Design Branch Engineering Division

mo.

RICHARD DIBUONO, CHAIRMAN Water Control Branch Engineering Division

APPROVAL RECONCENDED:

DE B. FREAR

Chief, Engineering Division

# PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation: however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition, and the downstream damage potential.

The Phase I Investigation does <u>not</u> include an assessment of the need for fences, gates, no-trespassing signs, repairs to existing fences and railings and other items which may be needed to minimize trespass and provide greater security for the facility and safety to the public. An evaluation of the project for compliance with OSHA rules and regulations is also excluded.

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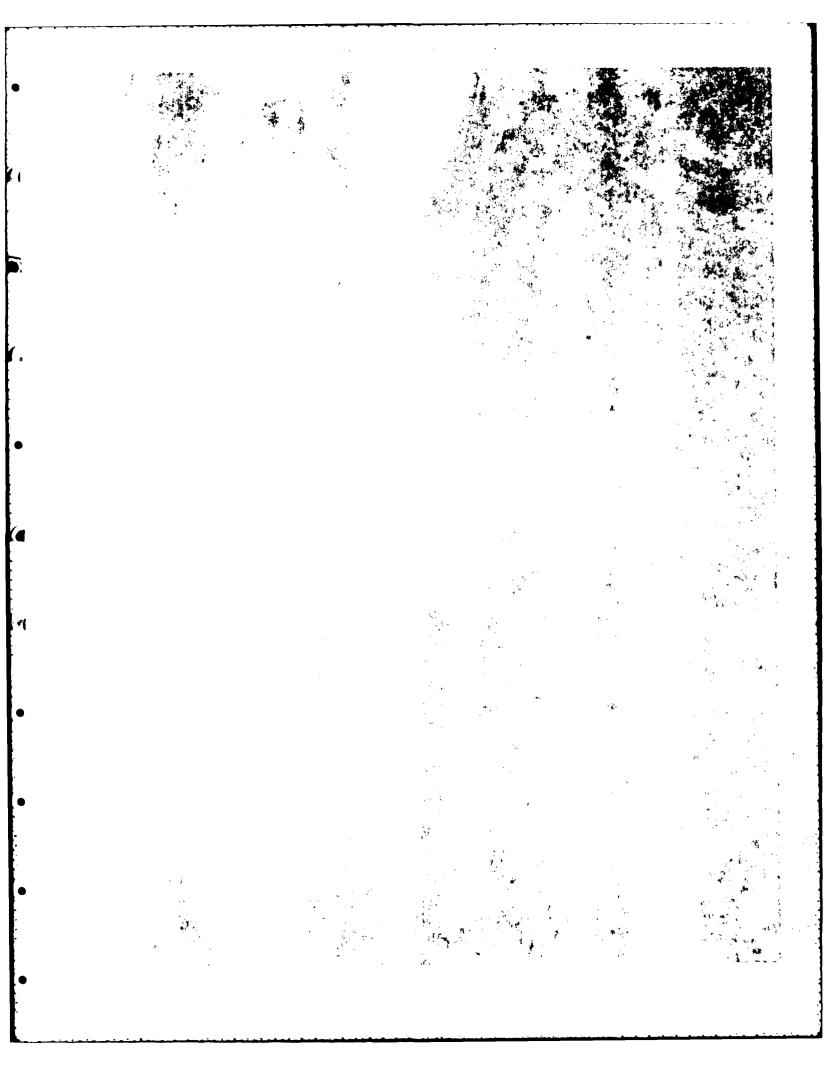
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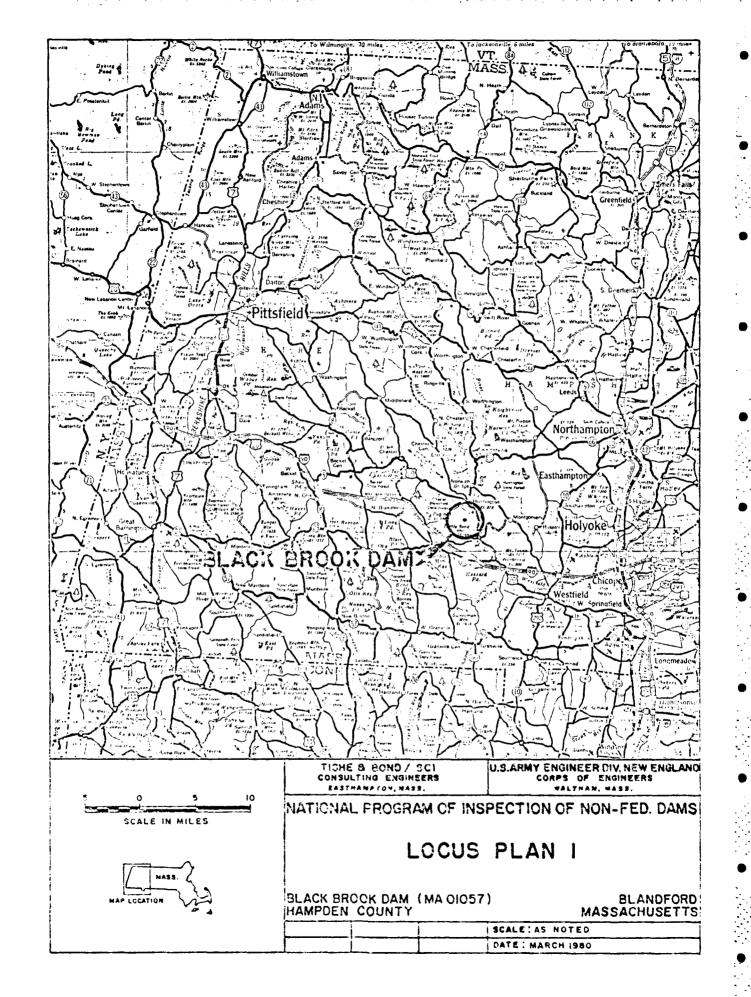
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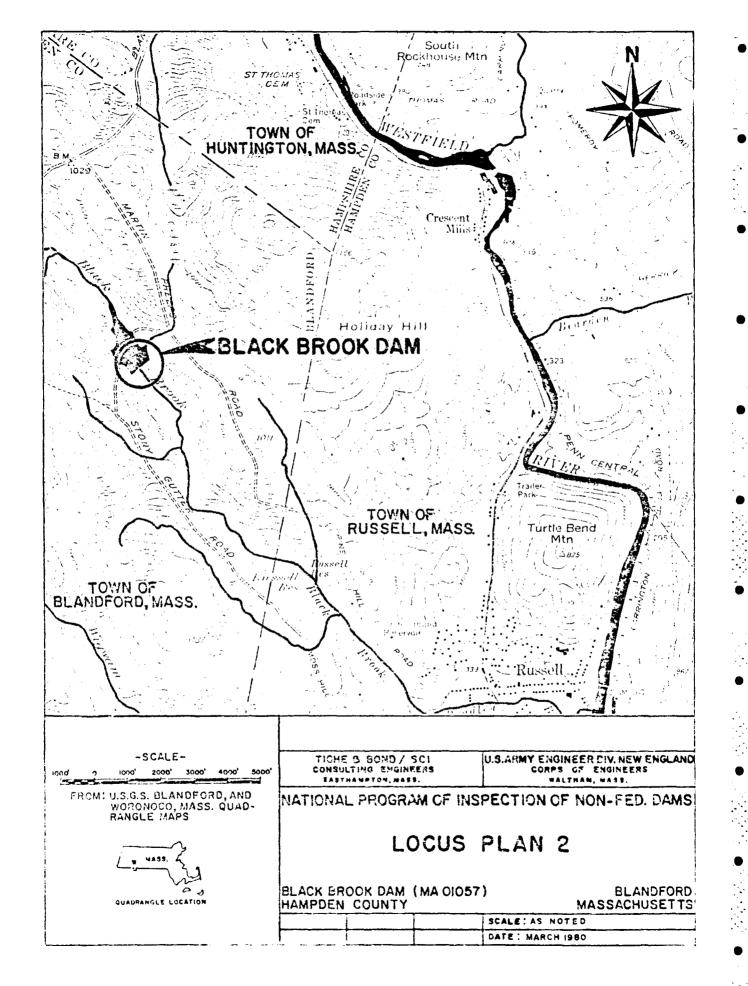
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# NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

#### BLACK BROOK DAM

# SECTION 1

# PROJECT INFORMATION

#### 1.1 General

#### (a) <u>Authority</u>

Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Tighe & Bond/SCI has been retained by the New England Division to inspect and report on selected dams in Massachusetts. Authorization and notice to proceed were issued to Tighe & Bond/SCI under a letter of October 24, 1979 from Colonel William E. Hodgson, Jr., Corps of Engineers. Contract No. DACW-33-80-C-0005 has been assigned by the Corps of Engineers for this work.

# (b) Purpose

1) Perform technical inspection and evaluation of non-federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-federal interests.

2) Encourage and prepare the states to initiate quickly effective dam safety programs for non-federal dams.

3) Update, verify, and complete the National Inventory of Dams.

# (c) Scope

The program provides for the inspection of non-federal dams in the high hazard potential category based upon location of the dams, and those dams in the significant hazard potential category believed to represent an immediate danger based on condition of the dams.

# 1.2 Description of Project

#### (a) Location

The Black Brook Dam is located in the Town of Blandford, Massachusetts, about 2.6 miles upstream from the Town of Russell. The dam is located on Black Brook which is a tributary to Bradley Brook and the Westfield River, respectively. The dam and impoundment is located off of Martin Phelps Road in the Town of Blandford.

The dam is located on the U.S.G.S. Blandford and Woronoco, Mass., quadrangles at latitude N42°-12'-36" and longitude W72°-53'-18". Refer to the location plan, and Appendix B for additional information.

#### (b) Description of Dam & Appurtenances

The dam consists of an earthfill embankment, a principal spillway consisting of a reinforced concrete drop inlet structure having a two stage riser section, a 36-inch diameter reinforced concrete outlet conduit, and a reinforced concrete impact basin at the conduit outlet. An emergency spillway is located in the right abutment and consists of a grass covered earth channel excavated in natural ground and ledge.

#### 1) Embankment (See pages B-1, B-2, B-3 and B-5)

The following information has been taken from the As-Built Drawings dated 1972.

The dam embankment is approximately 1,168 feet long and has a structural height of 60 feet. The upstream slope is 2.5 horizontal on 1 vertical. The downstream slope is 2.5 horizontal on 1 vertical, and the width of the top of dam is 18 feet. The upstream slope surface is covered with dumped riprap to the top of dam; riprap has been placed on the downstream face to elevation 885 MSL.

The embankment material is a silty sand (SM using Unified Soil Classification System) with silty sand comprising the central core, the upstream and downstream outer sections and the downstream toe. A cutoff trench consisting of silty sand is located beneath the embankment along the centerline of the dam.

The top of the dam is covered with grass growth.

2) Principal Spillway (See pages B-7 and B-9)

The principal spillway consists of a reinforced concrete drop inlet structure with a sluice gate controlled inlet pipe at invert elevation 841.0 for the pond drain, an uncontrolled orifice inlet at invert elevation 863.5 for the water supply pool and uncontrolled overflow weirs at elevation 876 for the high stage pond outlet.

The riser structure is 38.2 feet high from the base of the foundation to the top of the structure. The inside dimensions are 3 feet x 9 feet with walls that vary in thickness from 21" to 10". The inside boltom elevation of the riser structure is 340.0. The low stage water supply orifice is

located on the upstream face and measures 26 inches wide x 12 inches high with an invert elevation of 863.5. The high stage overflow weirs are formed by the tops of the riser section walls and have a total length of 18 feet with a crest elevation of 876.0. There are two anti-vortex walls perpendicular to the top of the weir walls with a solid concrete platform bridging the two walls. The sluice gate operator stand is supported on this platform. The anti-vortex walls flare out and up from about elevation 869.5 to 876.0 at a 45° angle. Them the walls are vertical for about 2.1 feet to the surface of the platform. Galvanized angle irons have been bolted between the walls to act as a trash rack.

The sluice gate which controls the 18 inch diameter pond drain is an 18 inch square gate mounted on a 12 inch deep wall thimble. The gate is operated by a rising stem, crank operated, floor stand located on the top of the riser structure.

The pond drain consists of about 40 feet of 18 inch diameter reinforced concrete water pipe with a reinforced concrete inlet structure. This conduit enters the riser structure through the upstream side.

The principal spillway structure has a 36 inch diameter outlet conduit discharging to an impact basin located at the downstream toe of the dam. The 36 inch diameter conduit consists of reinforced concrete pipe with a continuous concrete bedding and six reinforced concrete anti-seep collars. The invert elevation of the outlet pipe is 840.0 at the principal spillway and 836.0 at the impact basing with an overall length of 232.33 feet and a slope of 0.017 ft/ft.

The impact basin is constructed of reinforced concrete and is approximately 18 feet long x 14 feet wide with a reinforced concrete baffle spanning across the flow path to dissipate the energy from the high velocity outlet flow from the  $3\hat{0}$ inch diameter conduit during flood flows.

3) Emergency Spillway (See pages B-4 and B-8)

The emergency spillway consists of a grass covered earth and ledge excavated channel in the right abutment of the dam. The spillway channel has a control section at elevation 887.5 which is 50 feet wide and 30 feet long. A concrete weir 3' wide exists on the downstream edge of the flat control section and extends between the toe of slopes in the spillway. The spillway approach channel, along the centerline, has a section sloping up towards the control section at 2% for about 225 feet, then 1.59% for about 175 feet to the control section. The control section is level at elevation 887.5 for a distance of about 30 feet. The discharge channel slopes downward at 2.5% for about 175 feet and then 2.15% for about 160 feet where it discharges onto original ground downstream of the dam. The side slopes of the spillway excavation are at 2 horizontal to 1 vertical in earth and somewhat steeper where ledge outcrops were encountered. The maximum depth of excavation is at the control section and is about 32 feet. The control section is approximately 8.5 feet below the top of the dam.

# 4) Foundation and Embankment Drainage (See page B-6)

A 4 foot wide trench drain of clean sand and gravel extends into the foundation of the downstream toe. The trench drain extends from the centerline of the principal spillway left about 548 ft. and right about 602 ft., with an 8 inch diameter perforated CMP drain pipe extending the full length of the trench. Both 8 inch diameter trench drain outlet pipes discharge into the impact basin structure at the outlet of the principal spillway.

#### (c) Size Classification

The dam's maximum impoundment (computed to the top of the dam) of about 1620 acre-feet and structural height of 60 feet place it in the INTERMEDIATE size classification.

# (d) Hazard Classification

The hazard potential classification for this dam is <u>HIGH</u> because of the significant potential for loss of human life and property which may occur in the event of a failure. There is a high potential for severely damaging about 75 structures, most of which are houses with attendant probable loss of more than a few lives, as well as one major highway bridge and one secondary road bridge.

#### (e) Ownership

The Black Brook Dam is owned by the Town of Russell acting through its Board of Water Commissioners. The address is as follows:

Town of Russell Board of Water Commissioners Box 164 Russell, Massachusetts

#### (f) Operator

The operation of the Black Brook dam is the responsibility of the Town of Russell acting through its Board of Water Commissioners. The contact person for the Water Commissioners is Mr. Edward Miller. The telephone number is 1-413-862-3276.

# (g) Purpose of Dam

The Black Brook Dam is a multiple-purpose dam which maintains a low level water supply pool and provides flood water storage to reduce downstream flooding from the dam's drainage area. Stored flood water is gradually released through low and high stage inlets of the principal spillway.

# (h) Design and Construction History

The Black Brook Dam was designed by the U.S. Department of Agriculture, Soil Conservation Service. It was completed in the fall of 1971 and has been in operation since that time.

#### (i) Normal Operation Procedure

The Black Brook Dam is normally self regulating with the only controlled outlet being the pond drain. This outlet is operated only as part of infrequent maintenance checks and in the event the Town of Russell requires downstream flow for water supply when the water level is below the low stage inlet.

# 1.3 Pertinent Data

# (a) Drainage Area

The drainage area for the Black Brook Dam covers approximately 2.3 square miles. The drainage area from which Black Brook originates, and the surrounding perimeter areas are primarily mountainous woodland with some open areas. There are no developments within the watershed.

#### (b) Discharge at Dam Site

Normal discharge at the site is via the low and high stage inlets to the principal spillway and through the 36 inch diameter outlet conduit to the downstream channel. If flood flows occur of sufficient magnitude and duration to fill the flood water storage available, then excess flow will be discharged around the dam via the emergency spillway channel.

- 1) Outlet works:
  - a) Pond drain, 18 inch dia., inv. elev. 841.40 NGVD sluice gate controlled, Maximum Capacity 74 CFS.
  - b) low stage inlet orifice, 25 inch wide x 12 inches high, inv. elev. 863.5 NGVD, ungated, Maximum Capacity 67 CFS.

# 2) Maximum known flood at dam site:

It is reported that the highest pond elevation to date was observed during the fall of 1979. During this period the pond elevation was at approximately 868 ft. NGVD. Pond elevation during the March, 1980 flood flows reportedly did not reach elevation 868 ft. NGVD. No discharge flow data or recorded pond elevation data is available.

# 3) Ungated spillway capacity at top of dam

With the water level at the top of the dam (elev. 896 feet NGVD) spillway capacities are as follows:

principal spillway		220 CFS
emergency spillway		4780 CFS
	Total	5000 CFS

# 4) Ungated spillway capacity at test flood elevation

With the water level at the test flood elev. (893 feet NGVD) spillway capacities are as follows:

principal spillway		215 CFS
emergency spillway		2485_CFS
	Total	2700 CFS

5) Gated spillway capacity at normal pool elevation:

None

6) Gated spillway at test flood elevation:

None

7) Total spillway capacity at test flood elevation:

2700 cfs at elev. 893 feet NGVD. (Same as #4)

8) Total project discharge at top of dam:

5000 cfs at elev. 896 feet NGVD. (Same as #3)

9) Total project discharge at test flood elevation:

2700 cfs at elev. 893 feet NGVD.

- (c) Elevation (ft. above MSL)
  - 1) Streambed at toe of dam 336.±

2) Bottom of cutoff - 834±

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- 3) Maximum tailwater Unknown
- 4) Recreation pool Not Applicable
- 5) Normal Water supply pool 863.5
- 6) High stage flood control pool 876.0
- 7) Full flood control pool 887.5
- 8) Emergency spillway crest elevation = 887.5 ungated
- 9) Design surcharge 885.8
- 10) Top of dam 896
- 11) Test flood surcharge 893
- (d) Reservoir (Length in feet)
  - 1) Normal water supply pool 1920 ft±
  - 2) Flood Control pool 4000 ft±
  - 3) Emergency spillway crest pool 4000 ft.±
  - 4) Top of dam 4400 ft±
  - 5) Test flood pool 4300
- (e) Storage (acre-feet)
  - 1) Normal water supply pool 74
  - 2) Flood control pool 942
  - 3) Spillway crest pool
    - a) Low stage crest (water supply pool) 74
    - b) High stage crest 330
    - c) Emergency spillway 942
  - 4) Top of dam 1620
  - 5) Test flood pool 1340

# (f) <u>Reservoir Surface</u> (acres)

- 1) Normal water supply pool 11
- 2) Flood-control pool 69
- 3) Spillway crest
  - a) Low stage crest (water supply pool) 11
  - b) High stage crest 34
  - c) Emerg. spillway crest 69
- 4) Test flood pool 76
- 5) Top of dam 81

# (g) <u>Dam</u>

- 1) Type Earth embankment
- 2) Length 1168 ft±
- 3) Height 60 ft±
- 4) Top Width 18 ft
- 5) Side Slopes 2.5 hor. on 1 vert. both faces.
- 6) Zoning Homogeneous, semi-pervious silty sand
- 7) Impervious Core None
- 8) Cutoff Variable width and depth, semi-pervious silty sand earthfill
- 9) Grout curtain None
- (h) Diversion and Regulating Tunnel

Not applicable

- (i) Spillways
  - 1) Type:

a)	Principal spillway:	Reinforced concrete drop inlet
Ь)	Emergency spillway:	Grass covered, earth and ledge excavated channel with level control section and buried concrete weir

wall

2)	Length of weir:				
	a)	High stage inlet:	2 @ 9 ft. = 18 ft.		
	b)	Emergency spillway:	50 ft.		
(3)	Cres	st Elevation			
	a)	High stage inlet:	876.0		
	b)	Emergency spillway:	877.5		
(4)	Gate	es: None			
(5)	Ups	tream channel:			
	a)	Principal Spillway:	Reservoir		
	b)	Emergency Spillway:	Grass covered earth and ledge excavated channel.		
(6)	Dow	nstream Channel:			
	a)	Principal Spillway:	Riprapped channel 115± ft. to natural stream channel through fairly steep narrow valley		
	b)	Emergency Spillway:	Grass covered, earth and ledge excavated channel to wooded area discharging into natural stream channel downstream of dam		

# (j) Regulating Outlets

The only regulated outlets from the dam consist of a pond drain which is controlled by a manually operated 18 inch square sluice gate and an ungated low stage inlet orifice. The sluice gate is located on the inside face of the pond side wall of the principal spillway riser with its invert at elevation 841.0. The floor stand operator is located on the top of the principal spillway riser. The gate is a Joyce-Cridland, non seating head type, with a rising stem operator having the following identification:

# WJ70-4508 WJ65

The gate is normally in the closed position, and only rarely operated for maintenance checks and to allow water to flow in the stream to the downstream water intake reservoir.

The pertinent data regarding these outlets are as follows:

- a) Pond drain, 18 inch dia., inv. elev. 841.40 NGVD, Maximum capacity 74 CFS, controlled by an 18 inch square sluice gate.
- b) Low stage inlet orifice, 25 inches wide x 12 inches high, inv. elev. 863.5 NGVD, ungated, maximum capacity 67 CFS.

# SECTION 2 - ENGINEERING DATA

# 2.1 Design Data

The design data for the Black brook dam provided by the Soil Conservation Service includes hydrologic and hydraulic computations and summaries, structural calculations, a geological report, soil laboratory test data, a summary of embankment slope stability analysis, and other design information all contained within a "Design Report" dated 1969 and 1970. The design of the dam and appurtenances is based primarily on a number of Soil Conservation Service Publications which are listed in the General Section of the Design Report. Since water supply was one aspect of the project, the Soil Conservation Service, by regulation, contracted for the design of the water supply appurtenances with a private engineering firm. The firm's name is Loewer Sargent and Assoc. of Kensington, MD.

This design data was reviewed and found to be in accordance with good engineering practice. It was used extensively in preparing Section 5 and Appendix D of this report.

#### 2.2 Construction Data

"As Built" record drawings were available for the Black Brook Dam. These drawings have been reviewed and found to show good agreement with the design drawings and visual inspection.

Appendix B contains copies of the important "as built" drawings. These copies have been made from originals provided by the Soil Conservation Service.

# 2.3 Operational Data

The dam is self regulating for flood control purposes, and no operational data is available. Under normal conditions the hydraulics of the principal spillway maintain a low level water supply pool and flood flows are discharged via the high stage overflow weirs of the principle spillway and the emergency spillway.

During periods of low runoff from the watershed, the Town of Russell Water Department may release water from the impoundment in order to augment the flow entering the lower intake reservoir. The 18 inch diameter pond drain and sluice gate must be used for this purpose. There are no other regulating gates to be operated. Information from the Water Department indicated that the pond drain has never been operated for water supply purposes and the present Water Department Superintendent reports that he has never operated the pond drain gate.

#### 2.4 Evaluation of Data

#### (a) Availability

Sufficient data is available to permit an evaluation of the dam when combined with findings of the visual inspection.

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# (b) Adequacy

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There is sufficient design and construction data to permit an assessment of dam safety when combined with the visual inspection, past performance, and sound engineering judgment.

# (c) Validity

Since the observations of the inspection team generally confirm the available data, a satisfactory evaluation for validity is indicated.

# SECTION 3 - VISUAL INSPECTION

#### 3.1 Findings

# (a) <u>General</u>

The Black Brook Dam, No MA 01057, was in <u>FAIR</u> condition at the time of the inspection.

(b) Dam

1) Earth Embankment (See Photos 3, 4, 8 & 9)

The upstream face of the dam embankment showed a surface irregularity in the slope to the right of the spillway riser. Also, fine sand was being eroded from under the riprap at a number of locations at the normal water supply pool water line and was forming small sand deltas at the waterline.

The top of the dam and the downstream face above elevation 885.0 has a heavy grass cover which is well established. There is some evidence of trespassing on the dam by trail motorcycles which have caused minor damage to grassed areas.

The toe of the dam at both the right and left abutments is wet with a slight noticeable movement of water downhill towards the impact basin. No movement of silt was evident, however. The wetness could be caused by ground water seeping from the watershed above the dam since a significant amount of area drains towards the dam.

Small diameter trees were noted growing along the right end of the embankment.

The heavy grass growth on the embankment prevented a thorough inspection of this feature.

(2) Emergency Spillway (See Photos 5 & 6)

The emergency spillway channel is in good condition. There is a considerable amount of wetness downstream of the crest weir wall, but this must be natural ground water. The channel itself was free of debris but significant growth of weeds and grass exists. The channel has been excavated through original ground and ledge.

The channel and side slopes have a heavy grass growth providing good erosion protection where ledge outcrops do not exist.

#### (c) Appurtenant Structures

#### 1) Drop Inlet Principal Spillway (See hotos 1 & 7)

The principal spillway riser was found to be in good condition. The structure appeared to be structurally sound with no visible cracking, spalling, seepage, or efflorescence.

It was noted that one of the trash rack bars was missing and a second was damaged on the left side of the riser.

# 2) Pond Drain Inlet Pipe

At the time of the inspection, the water level was at the normal water supply pool level. Therefore, the inlet pipe and headwall structure were submerged and not visible.

#### 3) Outlet Conduit

The 36 inch diameter conduit was found in good condition. The alignment was good with only a small hydraulic jump in the flow being noted at the third joint in from the impact basin. All visible interior joints were dry above the flow line. The interior of the conduit that was visible is in good condition with no spalling, cracking, or efflorescence.

#### 4) Impact Basin (See Photos 2, 10, 11 & 12)

The impact basin was found to be in good condition with only a few minor shrinkage cracks being visible, and no spalling, or efflorescence. The structure was clear of debris with free unobstructed outflow to the downstream channel.

#### (d) Reservoir Area (See Photo 1)

The shore of the reservoir is generally shallow sloping woodland. It appears stable and in good condition.

#### (e) Downstream Channel (See Photo 2)

The downstream channel is in good condition with only a slight amount of vegetation encroachment. The channel immediately downstream of the dam is unobstructed. Riprap protection of the channel is minimal, but appears to be adequate.

#### 3.2 Evaluation

The dam is generally in <u>FAIR</u> condition with the following deficiencies being noted:

(a) Silt and fine sand is eroding from under the riprap on the upstream face at the water line and wasning into the pond.

- (b) There is a surface irregularity in the upstream slope to the right of the principal spillway.
- (c) The toe of the dam at both the right and left abutments is wet.

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- (d) One of the trash rack bars is missing on the left side of the principal spillway riser.
- (e) Trespassing by wheeled vehicles on the dam and emergency spillway was evident.
- (f) There is a heavy grass growth on the dam embankment.

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# SECTION 4 - OPERATIONAL AND MAINTENANCE PROCEDURES

# 4.1 Operational Procedures

(a) General

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No written operational procedures are available for this dam. The dam is normally self regulating for flood control purposes. The sluice gate on the pond drain is normally in the closed position and is not routinely operated. It is reported that the gate has not been operated since 1974 and is believed to have been operated once prior to 1974 for maintenance purposes.

#### (b) Description of Warning System In Effect

There is no written downstream warning system in effect.

#### 4.2 Maintenance Procedures

(a) General

An annual inspection is made by the Soil Conservation Service and recommendations resulting from this inspection are implemented by the Town of Russell through its Board of Water Commissioners.

Typical maintenance items assigned to the Town of Russell include liming and fertilizing, mowing, clearing of accumulated debris, etc. At the time of this Phase I inspection the embankments and emergency spillway channel were overgrown with a heavy growth of grass. Also, a trash rack bar was missing from the riser.

#### (b) Operational Facilities

The only facility which requires operation is the pond drain sluice gate. This gate may be used to release impounded water to the downstream water supply intake reservoir and also to completely drain the impoundment.

Discussions with a representative of the Town of Russell Water Commissioners indicated that the sluice gate for the pond drain is <u>not</u> routinely operated and it has not been required to release impounded water for water supply purposes. A visual inspection of the gate operator indicated that lubrication is required.

There are no other facilities which require operation.

#### 4.3 Evaluation

The extent of the growth on the dam embankments, and the emergency spillway channel, and the missing and damaged trash rack bar on the riser indicate that improvements are needed in the routine maintenance program. These items should be checked and corrected on a routine, frequent basis. In addition, the sluice gate should be operated at least annually as a minimum and kept well lubricated to prevent corrosion and maintain the operator in an operable condition.

Additional emphasis on routine maintenance will assist the owners in assuring the long term safety of the dam.

A formal, written downstream emergency flood warning system should be developed and put into operation.

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# SECTION 5 - EVALUATION OF HYDRAULIC/ HYDROLOGIC FEATURES

# 5.1 General

Black Brook Dam, No. MA 01057, is a multiple-purpose water supply and floodwater storage facility which was designed by the Soil Conservation Service (SCS), as part of the overall Westfield River flood protection project.

The dam is located on Black Brook in the Town of Blandford, Massachusetts about 2.6 miles upstream along Bradley Brook and Black Brook of the Town of Russell. The dam is about 2.5 miles upstream of its confluence with Bradley Brook and 3 miles upstream of the confluence of Bradley Brook and the Westfield River in the Town of Russell, Massachusetts.

The drainage area upstream of the dam is 2.3 square miles (1485 acres) with a mountainous perimeter and interior from which Black Brook originates.

No development exists in the watershed due to the use of impounded water for water supply. The area is primarily wooded with only a minor amount of open fields.

The dam itself is about 1168 feet long and 60 feet high, and is an earthfill embankment. The facility has a principal spillway which has low and high stage inlets and discharges all normal stream flows via a 36-inch diameter conduit through the dam. An emergency spillway, consisting of a 50 ft. wide earth excavated channel with a grass cover, carries flood flows which exceed the storage capacity of the impoundment around the dam to the downstream channel.

The dam has a sluice gate controlled pond drain which may be used to release impounded water to the downstream water supply intake reservoir and also to completely drain the impoundment.

#### 5.2 Design Data

The hydraulic features of the Black Brook Dam have been designed by the S.C.S. to retard a 100 year frequency storm without discharge occurring in the emergency spillway. The top of the dam elevation was established based on a maximum probable storm as datermined by S.C.S. The design storm for establishing the top of the dam was based on 23.1 inches of rainfall resulting in 18.6 inches of runoff. The peak design inflow is 12,150 CFS and the routed design outflow is 3712 CFS at a pond elevation of 895.90. The calculations included in the SCS Design Report include storage vs. elevation, stage discharge curves for the combined spillways, and routing of the various test floods through the reservoir. These calculations are dated 1969 and 1970.

#### 5.3 Experience Data

No records of flow or stage are known to be available for the Black Brook Dam.

# 5.4 Test Flood Analysis

The selection of the test flood is based on the Corps of Engineers, "Recommended Guidelines for Safety Inspection of Dams," dated November 1976. These guidelines state that dams classified as "Intermediate" in size, and "High" in hazard potential be tested against the "Probable Maximum Flood" (PMF) for the region within which the dam is located.

The determination of the PMF for the Black Brook dam is based on the Corps of Engineers "Preliminary Guidance for Estimating Maximum Probable Discharges in Phase I Dam Safety Investigations" dated March 1978. The Guide curves provided cover drainage areas as small as 2.0 sq. miles.

Graphically, the guidance curve gives a unit discharge of 2,500 cfs per square mile of drainage area which results in a PMF of 5,800 cfs for Black Brook Dam.

The purpose of this Phase I investigation is to assess the dam's overtopping potential and its ability to store and/or discharge the test flood. This requires determing the storage characteristics of the impoundment area and the stage vs. discharge characteristics of the spillway. The SCS design report tabulates all of this data, and our review has determined the information to be substantially correct and valid, therefore, as noted in the computations included in Appendix D, this information has been utilized in performing the test flood analysis.

The test flood has been routed through the reservoir using the iteration process as outlined in the Corps of Engineers, "Preliminary Guidance for Estimating Probable Maximum Discharges in Phase I Dam Safety Inspections." The results of routing the PMF test flood through the reservoir indicate that the storage capacity of the impoundment area will reduce the test flood inflow of 5,800 cfs to a reservoir outflow of approximately 2,700 cfs at a pond elevation of 893 ft. NGVD. This assumes that the level of the water supply (normal pool) pond is at elevation 363.5, which is the invert of the low stage orifice, at the start of the storm, and the entire flood storage volume is available.

The combined spillways have a discharge capacity with the water level at the top of the dam (elev. 896.0 ft. NGVD) of 5,000 cfs. The combined spillways have a capacity of 185% of the routed test flood outflow and a freeboard of 3.0 feet remains to the top of the dam at test flood stage.

#### 5.5 Dam Failure Analysis

A dam failure analysis using the procedures in the Corps of Engineers, "Rule of Thumb Guidance for Estimating Downstream Failure Hydrographs" dated April, 1978, was performed for the Black Brook Dam. The assumed conditions are as follows:

- 1. Water level prior to breach is at test flood elevation.
- 2. Stream flow downstream of dam at time of breach is PMF test flood spillway outflow.

For an assumed breach equal to 40 percent of the dam width computed at half height, the breached width is 272 ft. The resulting dam failure flow using a water elevation of 893 ft. MSL is 207,300 cfs.

The first and second damage areas impacted by the dam failure would be the dam itself and the water supply pipeline for the City of Springfield, Massachusetts just downstream. Prior to the dam failure the flow in the stream would be 2,700 cfs with a stage of 6 feet. After the dam failure the flow would be 206,000 cfs at a stage of 37 feet. There are no houses or other forms of development in the area of the dam, therefore, damage would be confined to the dam structure and appurtenances and to the water supply pipeline for the City of Springfield, Massachusetts.

The third damage area impacted by the dam failure would be the Town of Russell water supply reservoir about 6000' downstream of the Black Brook dam. The reservoir, small in volume, will not add to the flow but would most likely be damaged by the failure. Thus, the Town would loose its water supply. Prior to the failure the dam would most likely withstand the flow and no damage would result.

The fourth area to be impacted would be a culvert and bridge crossing at the intersection of Bradley Brook and State Highway Route 20. Prior to the dam failure the test flood spillway flow would be 2,700 cfs resulting in a river stage of 2 feet. No structures nor the roadway will be flooded by pre-failure flows. After the dam failure the flood flows will be 96,400 cfs and the water level will be 20 feet above the brook bed. This flow will inundate about 16 houses approximately 3 to 5 feet, 1,000 feet of secondary road, 1,000 feet of primary road, and the road bridge at the crossing of Route 20 over Bradley Brook.

The fifth area to be impacted would be a secondary road bridge downstream of the Route 20 crossing. Prior to dam failure the test flood outflow would be 2,700 cfs resulting in a river stage of 24 feet above the brook bed. No structures nor the roadway will be flooded by pre-failure flows. After the dam failure, the flow will be 93,600 cfs and the brook stage will be 21 feet above the brook bed. The flow will flood between 35 to 40 structures, about 10 to 12 feet, two secondary streets totaling about 1500 feet, and a secondary road bridge.

The sixth impact area will be a foot bridge ruins just upstream from the confluence of Bradley Brook with the Westfield River. Prior to the dam failure the test flood flow will be 2,700 cfs and the brook stage will be 6 feet above the brook bed. No structures nor the roadway will be flooded by pre-failure flows. After the dam failure the flow will be 79,100 cfs and the brook stage will be 22 feet above the brook bed. This will inundate about 18 homes and about 1000 feet of secondary street. The seventh and eighth areas to be impacted will be the confluence of the Bradley Brook with the Westfield River and a mill dam downstream. Prior to the dam failure, the river flow will be 2,700 cfs. The river stage will be about elev. 272 feet. After the dam failure the flow in the river will be 70,000 cfs, resulting in a river stage of  $\epsilon$  out elev. 284 at the mill dam. This will flood the railroad tracks, which parallel the river, and the mill structure by about 4 feet.

Downstream of the mill dam, the dam failure flow will be quickly dissipated by the flat slope and broad channel of the Westfield River. The dam failure flow will not constitute a serious damage potential downstream of impact area 8.

		no significant dam- age	After failure poten- tial loss of water supply pipeline	After failure poten- tial loss of water supply dam	After failure 16 houses flooded, 1000 ft. primary road, 1 bridge, 2 culverts	After failure 40 houses flooded, 2 streets totalling 1000 <sup>1</sup> and 1 bridge	After failure 5 houses flooded
NLURE	Stage After Failure FT. (over road)	37	37	31	20 (9.2)	21 (3.5)	21.5 (4.5)
AFTER DAM FAILURE	River Before Failure FT. (over road)	Q	Q	Q	N	2	ω
AM JMPACT BEFORE AND Black Brook Dam 01057	Rates After Eailure CFS	207,300	206,000	127,100	96,400	93,600	79,100
EAM IMPAC	Flow Before Falure CFS	2,700	2,700 k	2,700	2,700 10'	2,700	2,700 ry
PROBABLE DOWNSTRE	Other Damage	0	Pipeline crossing Black Brook	Dam	1 bridge & 2 culverts 1000' second- ary road, 1000' primary road	1 bridge 1500' second- ary road	1 Foot- bridge ruins 1000' secondary road
PROB	No. of Strue tures	0	0	0 bir	16	and- 40	је 18
	Location	1 Dam	2 100' DS Water Supply Pipeline	3 6000° DW Water Supply Reservoir	<sup>0</sup> 4 11,250 <sup>1</sup> DS State Route 20	5 12,250' DS Second- Secondary Road	6 11,250 Footbridge ruins

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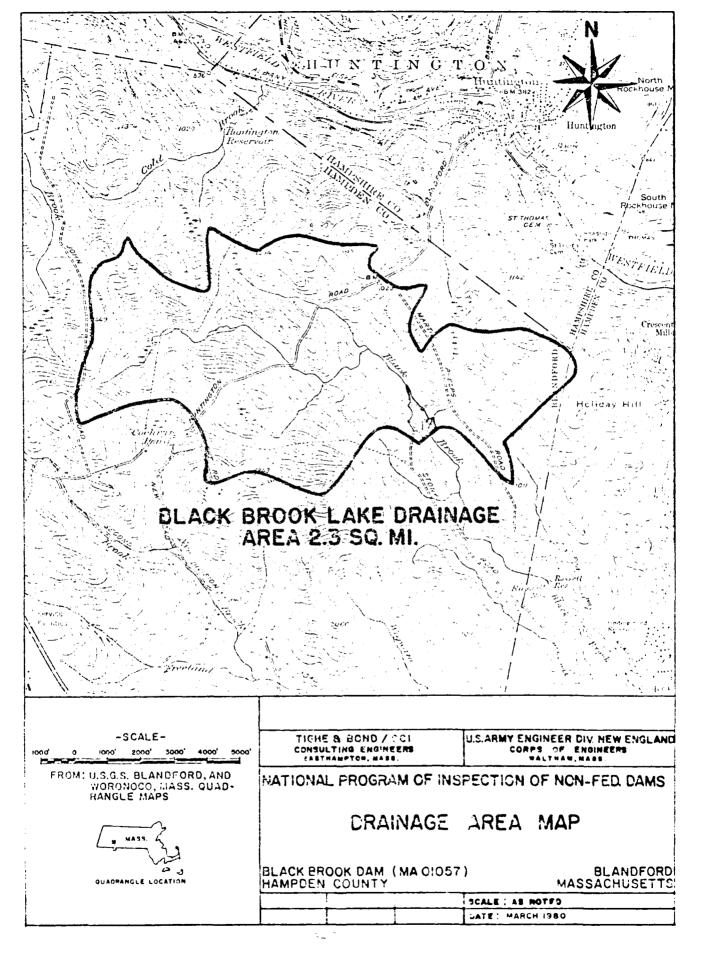
					•. • . • . • .		• • • • • • • • •	
	amaye	l )' RR ‡± fl.						
Comments	No significant damaye	After failure mill structure & 2000' will be flooded 4±						
Comn	signifi	After failure structure & will be flood						
â								
Stage After Failure FT. (over road)	284 MSL	284 MSL (4)						
S								
River Before Failure FT. (over road)	272 MSL	272 MSL						
	27	27						
υ	0	0	0 75±					
Rates After CFS	79,100	70,000	11 13					
			ow low					
Flow Before CFS	2,700	2,700	Pre-failure flow Past failure flow					
	i d		<mark>⊳re-fai</mark> ast fa					
		Dam R R	b y b y					
Other Damage	2 9 9	Mill Dam 2000' RR	floode floode					
			tures tures					
No. of Structures	0		struc struc					
Struc	ance Ver	Dam iver	Total no. of structures flooded Total no. of structures flooded					
	onflue eld Riv	ield R	Total Total					
tion	7 14,300 Confluence w/Westfield River	8 14,600 DS Mill Dam on Westfield River	·					
l. <u>ocation</u>	7 14 w/	8 14 on		5- 6				

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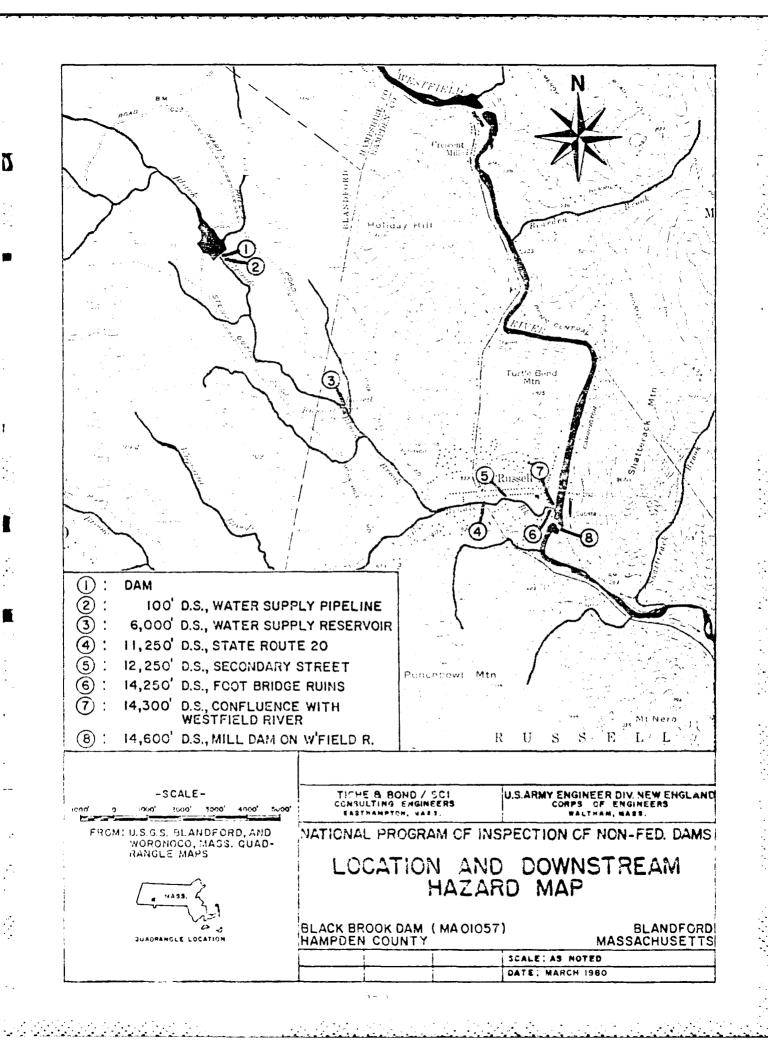
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# SECTION 6 - EVALUATION OF STRUCTURAL STABILITY

## 6.1 Visual Observation

The visual inspection of the dam embankments did identify conditions that warrant further investigation of the slopes. The erosion of silt from under the riprap on the upstream face at the water line is of concern and should be investigated to determine the affect on stability. There is a surface irregularity on the upstream face of the embankment to the right of the principal spillway riser.

The large extent of wetness at the toe of the embankment is also of concern, and should be investigated further to determine what affects, if any, it may have on the downstream toe, slope and foundation stability.

## 6.2 Design and Construction Data

## ) Embankment

Analysis carried out during the design phase included an embankment slope stability analysis by the "Swedish Circle" method. Based on this analysis a 2.5 horizontal to 1 vertical embankment slope was utilized.

# b) Appurtenant Structures

A review of the structural calculations for the design of the principal spillway structure and the outlet conduit revealed that these structures have been designed on the basis of sound engineering practice.

# 6.3 Post Construction Changes

There have been no post construction changes to the dam and appurtenances.

# 6.4 Seismic Stability

The Black Brook Dam is located in seismic zone 1. According to the recommended Corps of Engineers Guidelines, a seismic analysis is not warranted.

# SECTION 7 - ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

#### 7.1 Dam Assessment

# (a) <u>Condition</u>

The dam and its appurtenances are in FAIR condition due to upstream embankment surface irregularity, the wet condition of the downstream toe and the erosion of the silt from under the riprap.

## (b) Adequacy of Information

There is sufficient design and construction data to permit an assessment of dam safety when combined with visual inspection, past performance, and sound engineering judgment.

## (c) Urgency

The recommendations and remedial measures described herein should be implemented by the owner within one year of receipt of this Phase I Inspection Report.

#### 7.2 Recommendations

The recommendations of this Phase I investigation are that the following additional studies be made under the supervision of a qualified registered professional engineer:

(a) Determine the cause of the wet conditions at the toe of the embankment. These conditions should be investigated to determine the effects on the stability of the dam and foundation material, and to determine what corrective measures may be required, which should then be implemented.

(b) Determine the cause of silt erosion from under the riprap on the upstream face and develop and implement corrective measures, if required.

(c) Investigate the cause of the irregularity in the slope of the upstream embankment to the right of the principal spillway and develop and implement corrective measures, if required.

# 7.3 Remedial Measures

The recommendations of this Phase I investigation are that the following remedial and/or maintenance items be carried out:

- (a) Replace and repair trash rack bars.
- (b) Routinely check the upstream embankment for depressions or settlements due to the loss of material from under riprap.

(c) Operate the pond drain sluice gate at least annually as a maintenance check and maintain the operator well lubricated.
(d) Mow the grass cover on the dam embankment and maintain it in mowed condition.
(e) Remove small diameter trees along the right end of the emban

- (e) Remove small diameter trees along the right end of the embankment and maintain an area of at least 20 feet horizontally from each toe clear of trees.
- (f) Discourage trespassing on the dam and embankments by motor vehicles.
- (g) Develop an "Emergency Action Plan" that will include an effective preplanned downstream warning system, locations of emergency equipment, materials and manpower, authorities to contact and potential areas that require evacuation. This Plan should include monitoring the dam during and immediately after periods of heavy rainfall.
- (h) Continue the program of annual technical inspections by a registered professional engineer qualified in dam design and inspection.

# 7.4 Alternatives

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There are no practical alternatives to the above Recommendations and Remedial Measures.

# APPENDIX A

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# VISUAL CHECKLIST

PARTY ORGANIZATION			
PROJECT_Black_Brook_Dam	DATE 11/20/79		
	TEE_ 9:00 A.M.		
	WEATHER Cloudy & Cool		
	W.S. ELEV. <u>863</u> , U.S. <u>836</u> , DN.S.		
PARTY: Tighe & Bond/SCI Hydrologic/			
George McDonnell, P.E., Hydraulic 6.			
2. John Powers, P.E., Project Manager 7			
3. David Lenart, P.E., Civil . 8.			
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	PROJECT Black Brook Dam	DATE	
	PROJECT FEATURE	NAME	
	DISCIPLENE	NAME	<u>.</u>
	AREA EVALUATED	CCNDITIONS	
2	AM EMBANKAENT	·	
	Crest Elevation		-
	Current Pool Elevation	2" over normal w.l.	
	Maximum Impoundment to Date	Appears to be principal SW elev.	
	Surface Cracks	None	
	Favement Condition	Upstream and downstream good	
	Novement or Settlement of Crest	None noted	
	Lateral Movement	None noted	
	Vertical Alignment	Good	
	Horizontal Alignment	Good	
	Condition at Abutment and at Concrete Structures	L&R abutments good None	
	Indications of Movement of Structural Items on Slopes	Slopes down & upstream good	
	Trespassing on Slopes Vegitation on Slopes Sloughing or Erosion of Slopes or Abutments	Some minor tracks of MC Some brush growing in rock fill near toe Erosion of silt from under riprap at water line.	
	Rock Slope Protection - Riprap Failures	Slight irregularity in slope right of spillway	
	Unusual Movement or Cracking at or near Toes	None-toe along R&L abutment is wet but	
	Unusual Embankment or Downstream Seepage	slight flow None - same as above	
	Piping or Boils	None	
	Foundation Dreinage Features	Flow (slight) no sediment	
	Toe Drains	Good - standing water with slight flow	
	Instrumentation System	N/A	

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	CN CHECK LIET	
PROJECT Black Brook Dam	DATE	•
PROJECT FEATURE	14VE	:
DISCIPLIE	NAME	
AREA EVALUATED	CONDITION	}
OUTLET MORKS - SPILLMAY WEIR, APPROACH AND DISCHARGE CHANNELS		
a. Approach Channel		1
General Condition	Good - heavy grass growth	ł
Loose Rock Overhanging Channel	None	
Trees Overhanging Channel	None	
Floor of Approach Channel	Solid and dry	
b. Weir and Training Walls	Good, crest 50' wide at toe of slopes	
General Condition of Concrete	Good	
Pust or Staining	N/A	
Spilling	N/A	
Any Visible Reinforcing	N/A	
Any Seepage or Efflorescence	N/A	
Drain Holes	N/A	
c. Discharge Channel	Good heavy grass growth	
General Condition	Floor wet about 100' downstream of cress	
Looce Rock Overhanging Channel	None	
Trees Overhanging Channel	None	
Floor of Channel	Fírm but wet	ļ
Other Obstructions	None	
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PROFECT Black Brook Dam	DATE	
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PROJECT FEATURE	N4/E	107.1607 <u>6</u>
DISCIPLEKE	NAME	
AREA EVALUATED	CONDITION	
DUILET MORKS - CONTROL TOWER	No access to tower inside	
. Concrete end Structurel	Lower trash rack left missing-one damaged	
General Condition	Good	
Condition of Joints	Good	
Spalling	None	
Visible Reinforcing	None	17 . <u>2</u>
Rusting or Staining of Concrete	None	
Any Seepage or Efflorescence	None	
Joint Alignment	Good	
Unusual Seepage or Leaks in Gate Chamber	None	
Crecks	None	
Rusting or Corrosion of Steel	Ladder has slight rust	
b. Mechanical and Electrical	N/A	
Air Vents	N/A	
Float Wells	N/A	
Crane Hoist	N/A	
Elevator	N/A	
Hydraulic System	N/A	
Service Gates	N/A	
Emergency Gates	Joyce-Cridland 5 Ton Ser W/J70-4508	
Lightning Protoction System	Model MJ65 N/A	
Integency Power System	N/A	l
Wiring and Lighting System in Sate Chamber	N/A Copy available to DTIC does not permit fully legible reproduction	

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FROJECT FEATURE	NAME	1
	NAVE	
APEA EVALUATED	CC::DIFICN	
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHAIDEL		
General Condition of Concrete	Good - plastering done to finish	
Ruot or Staining	None	
Spalling	None	
Erosion or Cavitation	None	}
Visible Reinforcing	None	
Any Seepage or Efflorescence	None	
Condition at Joints	Good	
Drain holes	Good	
Channel	Good	
Loose Rock or Trees Overhanging Channel	None	
Condition of Discharge Channel	Good Pipe alignment good but 3rd joint had hydraulic jump noted. Not visible entirely	
,		
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PROJECTBlack_Brook_Bam	DATE	
PROJECT FENTURE	NAME	
DISCIPLEE	NAVE	
AREA EVALUATED	CONDITION	
UTLET WORMS - TRANSITION AND CONDUTT		•
General Condition of Concrete	Good - access limited - no access to inside	
Rust or Staining on Concrete	None	
Spalling	None	
Erosion or Cavitation	None visible	
Gracking	None visible	
Alignment of Monoliths	None visible	
Alignment of Joints	Good	
Numbering of Monoliths	N/A	
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FROUTER Black Brook Dam	DATE	-
PROJECT FEATURE	NAVE	-
	NANE	
		-
APEA EVALUATED	CCIDITION	
OUTLET MORNE - ETTAKE CHARTEL AND ETTAKE STRUCTURE	· · · · · · · · · · · · · · · · · · ·	
a. Approach Channel		
Slope Conditions		
Bottom Conditions	Notaccessible water level at normal	
Rock Slides or Falls	pool elevation	
Log Boom		
Debris		
Condition of Concrete Lining		
Drains or Weep Holes		
b. Intake Structure		
Condition of Concrete		
Stop Logs and Slots		
	<b>Copy available to DTIC does not</b> <b>permit fully legible reproduction</b>	

PROJECT Black Brook Dam		
PROJECT VEATURE	NAVE	-
DECERE	NAVE	-
AREA EVALUATED	CONDITION	
CUTLET MORMS - SERVICE BRIDGE		
a. Super Structure		
Bearingo		
Ancnor Bolts		
Bridge Seat		
Longitudinal Members		
Under Side of Deck	N/A	
Secondary Bracing		
Deck		
Dreinege System		
Bailings		
Expansion Joints		
Delat		
. Abutment & Piers		
General Condition of Concrete		
Alignment of Abutment		
Approsen to Bridge		
Condition of Seat & Eachwall		• • • •
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# APPENDIX B

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# ENGINEERING DATA

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# APPENDIX B

# ENGINEERING DATA

# 1. Design and Construction Records:

The following records are kept on file by the U.S. Dept. of Agriculture, Soil Conservation Service and may be obtained through their office located on Cottage Street in Amherst, Massachusetts.

Design records include the following:

construction drawings construction specifications construction revisions design criteria layout hydraulic design foundation and embankment design geology report soil testing report structural computations quantity estimates inspector's notes seeding schedule

Construction records include the following:

inspector's and engineer's diaries soil testing reports concrete testing reports material certifications equipment guarantees correspondence quantities pay estimates "as built" drawings

# 2. Inspection Reports (Appended)

Date

Inspecting Agency

9/21/78	See Listing On Report
5/18/77	11
6/9/77	н
5/11/77	11
5/24/76	н
6/4/75	11
6/2/75	11
7/15/74	10
9/17/73	ii
3/28/73	

# 3. "As Built" Drawings (Appended)

# <u>Page No.</u>

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# Description

B-1	Cover Sheet
B-2	Plan of Site
B-3	Plan of Dam Site
B-4	Plan of Emergency Spillway
B-5	Typical Section
B-6	Foundation Drainage Details
B-7	Principal Spillway - Plan & Profile
B-8	Emergency Spillway Drain - Plan & Profile
B-9	Riser Details
B-10	Conduit Details
B-11	Reservoir Drain Details
B-12	Impact Basin Details
B-12	Impact Basin Details
B-13-16	Log of Test Holes

التخانا بالمسلك Soil Conse. Mation Sarvice SOLE CONSERVATION ~SEVICE ICH 4 Whatle, St Hodley / 171,01035-OPFEATION AND MUNTFULNCE FROM UN-/ S-10 32. MASSACHUSFTETS · and Site Really, FK 4/3, Black Bir Date op. oring local Organization Toward Respect the feration and Maintenance Inspection Record day showed a need for certain maintenance and regar work. This and other maintenance ha bee: completed as follows: Prel - 2 April to Maintenance Performed by: (contributed nC Inbor, Force Account, Contract, Etc.) Cests Completed Item Bo. TOWN OF ROSSELL WATCH DENT. By The Town of 100.00 10-1-28 NORR WAS DONE BY BUSSEN HURLONY PUPT TOWN OF RUSSEI WINTER DEDT. 14 4.30-919 Town of RUSSCH WARR DUPT. Ś Town of Russell WATCH DEAT 7 TOWN of RUSSell WHITE DENT. r 82000 RETARKS: Depresentative . Perresentative Report due: Annually struction: ters. WK; FeEA (if lean involved) · . . Spor or

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<u>vr-</u>	ef Inspectio	<u>n</u> : Speci Annu3	$\frac{\operatorname{conv} K \ S. \ H C}{\operatorname{Structure Operation}}$ $1 \ \overline{X}$ on: Town of Russell		tory X
re	sent for Inspe archie/7.55 L	ction:Pot	nich Shackey Ten With Beardy Unin A.		
	ITEM	Uondi- tion * (S or U)	··· ••··· •• •• •• •• •• •• •• •• •• ••	Esti- materi Costs	Agreed Date Repairs to be complete
•	Vegetation	S	Gelerally excelle_T. Now grass areas in emerconcy	250	july'79
•	Fences	S	Do not men crownietch		
•	Principal Spillway	S			
•	Emergency Spillway	S	Removie down trop and pile of weed Cut small trep encreasing al entran	\$ 50	Dec. 15
•	Ambankment & Riprop	S	Prevent werdy promith from encreating on dike	100	Dec. 15- 78
•	Reserveir Area	S	, ,		
	Gates and Valves	S	Operate and lubricate art equipment at least once a yes	#50	Nov. 15.
•	Outlet Channels	S			
••	Ctructure Preinaço Cutleta	.S	Remore plant growth in tor drain outlet.	\$10	Nov 15 7
ĵ.	Artuss Rd.	S			) ; ;
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	Article (1997)		Copy aveil a consection of the	TC	all the states of the states o

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2 OMM INSPECTION RECORD CHECT LIST terms to be checked at time of inspection may include, but not be limited to, the Mlewing: 6. Reservoir Area Verefation Undesirable venetative growth a. Reed for cutting &/or spraying a. Cut or fallen trees Need for reseeding, fertilizing, liming ò. b. Slash and other debris Evidence of winter injury, insect с. c. d. Erosion of banks damage, disease. d. Need for mowing and removal of excess 7. Gates and Valves mowed vegetation. a. Damage by debris, ice freezing, e. Other rust or corrosion Fendes 8. Channels a. Loose or damaged posts Sedimentation a. b. Bank cutting b. Loose or broken wires Accumulated debris in fence c. Debris accumulation с. d. Condition of riprap or other d. Condition of gates and cables works of improvement Frincipal Spillway (1) Undermining Obstructions in spillway а. (2) Damage or deterioration b. Condition of outlet and riser (3) Adjacent channel scouring (1) Signs of seepage e. Adjacent property damage (2) Separation of joints (3) Cracks, breaks, or deterioration 9. Structure Prainage Outle's of concrete Drainage outlet pipes a. (4) Differential settlement (1) Clean or dirty water Sediment level in relation to the top (2) Rodent guard attached c. of riser and functioning Scour at outlet d. (3) Pipes free flowing, no obstructions Condition of trash racks е. (4) Evidence of seepage Emergency Spillway (a) Adjacent to pipes Erosion а. (b) Lower 1/3 downstream b. Sedimentation slope & flood plain c. Weeds, logs, or other obstructions, Rock toe drains b. reducing channel capacity (1) Free draining into still-Deposition or sloughing d. ing basin or collection e. Drainage problems channels f. Seeps (2) Clean or dirty water Emmankment and Riprop 10. Access Roads a. Settlement or cracking Safety Hazards 11. b. Erosion 12. Sirns c. Leakere 13. Vandalism d. Rodent, wildlifs, or livestock damage e. Wave damage

Consinuea)

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contion: Sponsore: Mass. Div. of Mater Resources, Full (if loan involved), SCS

MA\_AS\_ TRIAL 3/22/76 U.S.Department of Agriculture Soil Conservation Service

OPERATION AND MAINTENANCE RECORD

Project BLITDLEY BROOK W/S -BLACK SROC Date 5/18/77

Sponsoring Local Organization Town of RUSSELL

The Operation and Maintenance Inspection Record dated 5/34/76showed a need for certain maintenance and repair jobs. These jobs have been completed as follows:

C.W

-77

Agreed to Item No.	Maintenance Performed by: (Contributed Labor, Force Account, Contract, Etc.)	Actual Costs	Date Completed
1	4,500 LAS- FERTILIZER 5-10-10,	# 350,00	SerT. 30, 1576
3	TRASH REMOVED FROM TRACK RACK	125.00	5501. 20. 1976
4	DEBRIS REMOVED	50,00	Sept - 30. 1576
5	LOGS + DEBRIG REMOVED.	100.00	5-17-30, 1876
6	DEBRIS REMOVED	50.00	full . Je 1576
10.	DITCHING CONSTRUCTED	100.00	CAH 30, 1576

REMARKS:

SCS Representative District Conservationist

Distribution: Mass.DWR;FmHA (if loan involved)

and a statter

SLO Representatives Chairman, Wate Board

Report due: Annually Nov. 1

9 Cott	tage Street, Amherst, Massachusetts	
		Date: June 3, 1976
SUBJECT	T: AS - Distribution of Operation a (PL 566)	nd Maintenance Inspection Report/s
20: 1	<ol> <li>Charles Kennedy (3 copies) Director and Chief Engineer Division of Water Resources Mass. Dept. of Environmental Mgt. 100 Combridge Street Boston, MA 02202</li> </ol>	SPONSORS: Chairman, Hampden Cons. District c/o Hadley SCS Chairman, Board of Selectmen, Town Hall, Russell, MA 01071
Ż	2. <u>Soil Conservation Service</u> District Conservationist/s W. Warren	Chairman, Board of Selectmen Town Hall, Blandford, MA 01008
	Project Engineer J. Elnsmar State Administrative Officer (file copy) State Conservation Engineer	Mrs. Florence Pomeroy P.O. Box 85 Russell, MA 01071
	Mods Hill Rd. Fublic Wor Fussell, MA 01071 Mr. Edward Miller	rks Dept, Town Hall, Russell, MA 01071
	Water Commission Town Hall; Russell, MA	
	Water Commission	
for the	Water Commission Town Hall; Russell, MA and are reports of the CSM inspection	held in theBradley_Brook
for the <u>s</u>	Water Commission Town Hall; Russell, MA and are reports of the OSM inspection we sites listed below:	held in the <u>Bradley Brook</u> (watershed)
for the <u>s</u>	Water Commission Town Hall; Russell, MA and are reports of the CSM inspection as sites listed below: <u>Site</u>	held in the <u>Bradley Brook</u> (watershed) <u>Date Inspection Performed</u>
for the <u>s</u>	Water Commission Town Hall; Russell, MA and are reports of the CSM inspection as sites listed below: <u>Site</u>	held in the <u>Bradley Brook</u> (watershed) <u>Date Inspection Performed</u>

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Accession

# UNITED STATES DEPARTMENT OF AGFICULTURE

# SOIL CONSERVATION SERVICE

i

29 Cottage Street, Arherst, Macsachusetts

## Date: June 9, 1977

SUBJECT: AS - Distribution of Operation and Maintenance Inspection Report/s (PL 566)

- TO: 1. Charles Kennedy (3 cepies) Director and Chief Engineer Division of Water Resources Mass. Dept. of Environmental Mgt. Boston, MA 02202
  - 2. Soil Concervation Service District Conservationist/s W. Warren Project Engineer J. Elasmar State Administrative Officer/ (file copy) State Conservation Engineer

SPCHGORS: Chairman, Hampden Cons. District c/o Hadley SC3

Chairman, Board of Selectmen Town Hall, Russell, MA 01071

Chairman, Board of Selectmen Town Hall, Blandford, MA 01008

Mrs. Florence Pomeroy P. O. Box 35 Russell, MA 01071

Attendees:

Mr. Ernest Castro Moss Hill Rd. Russell, MA 01071 Mr. Charles Kenyon, Highway Foreman Public Works Dept. Town Hall, Russell, MA 01071

Mr. Edward Miller Water Commission Town Hall, Russell, MA

Enclosed are reports of the O&M inspection held in the Bradley Brook Watershed for the sites listed below:

# Site

Date Inspection Performed

Black Prook

5/11/77

Cincerely,

Dr. Fonjanin Icour Ebate Conservationist

1 Enclosure



/22	/76		INSPECTION RECORD Soil C	ept. of Agr Conservation	Service
'ro	ject_BRH	OLEY	BROOK WHTERSHED Inspection I	)ate///	77
Site	Name/No	BLACK			
<u>rype</u>	e of Inspecti	<u>on</u> : S <sub>I</sub>	DecialStructure Operation:	Satisfacto	ry 🔀
			mual 🔀	Unsatisfac	tory 🔄
Spoi	nsoring Local	Organiz	ation: TOWN GF RUSSELL		
		ection:	trouble Alunker		WMF.Warren
for	- flormor	Coust	Inguare .		
	ITEM	Condi- tion *	Maintenance & Needed Repairs	Esti- mated	Agreed Date Repairs to
		S or U			be Complet
1.	Vegetation	S	Excellent rond. t Top dress velch 300L Arel 0-20-20; topdiess grass with 300Lb/	5/#250	
		5	Arel 0-20-20; topdiess grass with 300L 10-10-10. Seed rued canary grass in small or tas.	·of X	
2.	Fences	S	OFTAS.		
3.	Principal	S			
	Spillway				
4.	Emergency	C	Remove growth Top scope, and	75.00	
	Spillway	) >	Andr.	13.	
<u> </u>	Embankment		Pour a defau + utiter 1 1 D.	/	
	& Riprap	S.	Remove delves tou U/station for this	250.00	
		· · · ·	have have have been and		
6.	Reservoir Area	S	Kenove growth from superio		
7.	Gates or	15			
	Valves				
8.	Outlet		Remore bush and cat tails	100.00	
	Channels	S		100-0	
9.	Structure				
	Drainnge	S		1	
	Cutleta		The D.C Contract		
10.	Access Rd.	5	Koad Cooki you		
11.	· · · · · · · · · · · · · · · · · · ·	1			
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(Listrict Conservationist) Geroject Engineer)

(Report due, annually: July 1)

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E

(SLO Representative)

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	e Name/No		Decial Structure Operation:	Satisfacto	ory L-
	nsoring Local	A	nnual	Unsatisfad	
Pre	sent for Insp	ection:	Obrilio Tranfal Higher	in tin	
	0, 10 . (-)	Jall.	- Enver F. J. Constrand Jimes / 70	- 12- 7-3	
	ITEM	Condi- tion * S or U		Esti- mated Costs	Agreed Date Repairs to be Complete
1.	Vegetation	S	Excellent condition, Topdress annually Crime Vetch 200 Lb per Dire 0-20-20 Conversional and Lb per Dire 0-20-20 Conversional and Lb per 20-00 10-10-10	125pr- acre	Sept 30 1570
2.	Fences	5			
3.	Principal Spillway	S	Remove eletin from trash rack	500	,.
4.	Emergency Spillway	5	Remove delses from month of spelling	180,00	, (
5.	Emcankment & Riprap	S.	Rinere Logo valles along ups for Ripsof Locks good Fill PIS chatment genter with 2" stones	320,00	1
6.	Reservoir Area	5	Jemore buch for evige of port open	50.00	
7.	Gates or Valves	.5			
8.	Outlet Channels	5			
9.	Structure Drainage Outlets	.S			
10.	Access Rd.	S	Town time placed grand or word. Had some children	16000	, <b>.</b>
11.					
	ArnS:(over)	<u></u>	<b>S</b> = Untisfactory; U = Unsatisfact <b>Copy dyn<sup>31</sup></b> pennut <sup>(1)</sup>	•	-7 TIC <sup>5</sup> - 1175
<u>2.</u>	(1-in -)-) x	Engin	st) (Project Engineer)		

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# June 4, 1975

# ETFORT OF ANNUAL INCREDICH

# BLACK BROCK SITE

BRADLEY BROOK WATERSHED

On June 2, 1975, the following met at Black Brook Cite in the Town of Blandford, Massachusetts for the purpose of conducting the annual inspection.

Frank LaDembard Edward Miller Don Lambert Fevin Maguire Ken Wood William F. Warren James J. Elasmar Supt., Water Department-Town of Russell Water Commission-Town of Russell Hampden Conservation Semiester District Water Resources Commission-Doston Water Resources Commission-Doston Soil Conservation Service-Nadley Soil Conservation Service-Ctis

# General.

The Town of Russell is responsible for the operation and maintenance of this site.

#### Structural Conditions and Recommendations

- 1. Remove logs and debris U/S toe of dam and from edges of permanent pool.
- 2. Remove debris from trash rack.
- 3. Trash rack bar broken at high stage.
- 4. Repair Entrance Gate.
- 5. Cutlet end of 3.C. wet, repair tire tracks.(6" perforated under drain in place)
- 6. Fill D/S abutment gutter with 2" stone.

Tubmitted by:

Jane Home

James J. Elastar Freject Ingineer Otis, Ma.

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# ANNUAL INSPECTION BLACK BROOK SITE

## Agronomic Conditions and Recommendations

Agronomic conditions in general are excellent. Dike slopes and most other areas are covered with a very fine stand of crownvetch with some fescue. As recommended last year mowing was discontinued with no detrimental effects discernible. Some areas of this soil in the borrow areas and on the left of the stone gutter have a somewhat thin cover of fescue but it is better than last year. A wet area of the emergency spillway is without vegetative cover. Small eroded areas of the downstream side of the dike (noted last year) were filled with soil, fertilized and seeded.

Topdress crownvetch with 300 lb. per acre 0-20-20 or equal.

Topdress grass in borrow areas, etc. with 300 lb. per acre 10-10-10. This is more critical than the vetch.

Sow Reed Canary Grass at the rate of 1 lb. per 1000 square feet in the bare wet area of the emergency spillway.

Diversion berms on the access road have been worn down and are to be rebuilt.

Submitted by

William Dome

William F. Warren District Conservationist Hadley

DISTRIFUTION OF T DLEY BROOK OWM PEDORT: . INSPECTION HELD 6/2/75

Attendees:

Mr. Frank LaRombard, Superintendent Water Dept. Town Hall Russell, MA 01071

Mr. Edward Miller Water Commission Town Hall Russell, MA 01071

> Mr. Donald Lambert, Chairman Hampden Conservation District c/o SCS office in Hadley also cc to his home: Moulton Hill Rd. Monson 01057

Division of Water Resources:

K. Maguire
K. Wood
Div. of Water Resources
100 Cambridge St.
Boston, MA 02202

William Warren, DC, SCS, Hadley

James Elasmar, Project Engr,SCS, Otis

Always Mrc. Florence Pomeroy P. O. Box 85 Russell, M. 01071

State office SCS, Amherst, MA

C. Currin/ENN FILE A. Verdi/Dion with originals

Town of Pussell responsible for OAM (except Freeland Site)

Co-Spensor of watershed

Also to C.Kennedy

## 7/15/74

#### REPORT OF ANNUAL INSPECTION

#### BRADLEY BROOK WATERSHED

On June 24, 1974, the following met at the Black Brook Site in the Town of Blanford, Massachusetts for the purpose of conducting the annual inspection.

Frank LaBombard	Supt. of Water Department, Town of Russell
William Mikuski	Chairman, Board of Selectmen - Russell
Kevin Maguire	Water Resources Commission - Boston
William Warre <b>n</b>	Soil Conservation Service - Hadley
William Annable	Soil Conservation Service - Amherst
James Elasmar	Soil Conservation Service - Otis
George Greenleaf	Soil Conservation Service - Otis

#### GENERAL

The Town of Russell is responsible for the operation and maintenance of this site.

# STRUCTURAL CONDITIONS AND RECOMMENDATIONS

Logs should be removed from the upstream slope of the dam and from the edges of the permanent pool. Large field stones should be placed in eroded outlet section to prevent future erosion. Diversion ditches at the northern and southern construction access road should be deepened so that water will flow east of the road. A small area on the west slope of the emergency spillway has slipped; however this does not seem critical and will be watched for future erosion. The condition of the concrete looks good. The repairs at the borrow area look very good. Eroded lower end of dry channel just north of the riprapped brook near the dam should be shaped and lined with large field stone.

## AGRONOMIC CONDITIONS AND RECOMMENDATIONS

Vegetation generally is in very good condition although some areas of exposed subsoil show nutrient deficiencies in the yellow thin condition of the grass. Topdress crownvetch annually with 300 lb. 0-20-20 and grasses with 300 lb. 10-10-10 or equal per acre. Galled spot on downstream side, west end, of dam should be repacked with loam, fertilized and seeded. Mowing of crownvetch is not necessary and not recommended unless in the future bruch begins to encroach.

Submitted by,

James J. Elasmar Project Engineer William F. Warren District Conservationist

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-Atta K. D. Cash

UNITED STATES DEFARTMENT OF AGRICULTURE Soil Conservation Service Amherst, Massachusetts 01002

## September 17, 1973

# REFORT OF ANNUAL INSPECTION Bradley Brook Watersned

On August 29, 1973, the following met at the Black Brook Site, Bradley Brook Watershed, in the Town of Russell, Massachusetts, for the purpose of conducting the annual inspection of the Black Brook Site:

Mrs. Florence B. Pomeroy	Water and Conservation Commissions
Mr. Frank LaBombard	Superintendent, Water Department
Mr. James J. Elasmar	Soil Conservation Service

Mr. William Warren, District Conservationist, made a review of the site on 8/1/73.

#### GENERAL

The Town of Russell is responsible for the operation and maintenance of this site.

# STRUCTURAL CONDITION AND RECOMMENDATION

Logs and other debris should be removed from the upstream slope of the dam. Weeds growing between the rocks on the upstream riprapped slope should be sprayed to kill the growth. Remove dead trees from the edges of the permanent pool. The condition of the concrete and the riprap at the outlet channel looks good.

It was noted that the town of Russell has filled in eroded ditches north and south of the riprapped waterway. The area south of the waterway was filled with earth and seeded. The eroded ditch north of the waterway was filled with 3" - 4" stone and looks very good. It is recommended that large stones be placed at the steep outlet section to prevent future erosion.

#### VEGETATIVE CONDITIONS AND RECOMMENDATIONS

The grass and legume cover has made remarkable development after a slow start in the spring of 1972. Dike slopes above the rock riprap are a solid heavy growth of Crown Vetch. Other areas are predominantly fescues, somewhat "thin" and nitrogen-starved in the borrow areas, good to excellent elsewhere including the emergency spillway bottom and slopes.

Mow and rake the heavy fescue stands in August or September. Topdress "thin" fescue grass stands in birrow areas with 500 lbs. 10-10-10, or equal, per acre. Other fescue areas should be topdressed with 300 lbs. 10-10-10 per acre. At least 25% of the nitrogen should be derived from an organic source. The Crown Vetch should be topdresse with 300 lbs. of 0-20-20, or equal, per acre.

Concurred in:

ancer Matune

Donald L. Basinger 6 State Concervation Engineer

cc: U. Kannedy, DWR (3) -- <u>1 for DFW</u> U. Elaomar D. Basinger W. Warren (5) C. Moustakis A. Verdi (2) D. Stockwell MNG file

(hristop

Christopher G. Houstakie / State Resource Conservationist UNITED STATES DEPARTMENT OF AG...CULTURE Soil Conservation Service 29 Cottage Street Amherst, Massachusetts 01002

REVISED Aug. 28, 1972

# REPORT OF ANNUAL INSPECTION Bradley Brook Watershed

On July 25, 1972, the following met at the Black Brook Site, Bradley Brook Watershed, in the Town of Russell, Massachusetts, for the purpose of conducting the annual inspection of the Black Brook Site:

Mrs. Florence B. Pomeroy	Water and Conservation Commissions
Mr. Gerald R. Pomeroy	Town Moderator
Mr. Vernon A. Shattuck	Selectman, Town of Russell
Mr. Edward Miller	Selectman, Town of Russell
Mr. Frank LaBombard	Superintendent, Water Department
Mr. Gregory T. Buteau	Soil Conservation Service
Mr. James J. Elasmar	Soil Conservation Service

Mr. William Warren, District Conservationist, made a review of the site on June 10, 1972.

Heavy and continuous rains this spring caused erosion damage on dormant seeded areas and washed out the left bank of the stone waterway. Some soil slips occurred on cut slopes in the borrow area. Erosion was noted along the bottom of the diversion ditch located above the emergency spillway and on the downstream face of the dam. Erosion from the barricades at Martin Phelps Road and from the south end of the borrow area toward the riprapped waterway has occurred. The general appearance of the vegetative cover looks good in spite of a late start this spring. Crown vetch is coming along quite well.

Since the scheduled inspection, SCS has made additional studies of the site and is preparing a proposal for repair of the areas damaged by erosion. This proposal will be submitted to the Town for consideration at a later date.

A dead tree on the upstream side of the dam, right of the riser, should be removed. Debris along the upstream toe of the dam and along the permanent pool should also be removed.

The entire site should be topdressed with fertilizer by the town as soon as possible. Topdress all vegetated areas that are not scheduled for repairs. A map is attached showing areas to be topdressed and application rates. A sample contract is attached for town reference, if they plan to contract for this work. This work is maintenance and is the responsibility of the Town.

Submitted by:

James Elasmar/wmb Project Engineer

William Warren District Conservationist

2 Attachments

cc: C. Kennedy, DWR (3) --1 for DPW
J. Elasmar D. Basinger
W. Warren (5) C. Moustakis
A. Verdi (2) D. Stockwell
ENG file

RIPRODUCED AT GOVERNMENT EXPENSE

# BRADLEY BROOK WATERSHED PROJECT BLACK BROOK MULTIPLE-PURPOSE DAM WATER SUPPLY AND FLOOD PREVENTION

DRAINAGE AREA		1485	ACRES
TOTAL STORAGE		942	ACRE FEET
FLOODWATER RETARDING STORAGE		864	ACRE FEET
RUSSELL WATER SUPPLY	·.	74	ACRE FEET
SURFACE AREA		11	ACRES
HEIGHT OF DAM	• • •	56	FEET
VOLUME OF FILL	20	00,000	CUBIC YARDS

# BUILT UNDER THE WATERSHED PROTECTION AND

### FLOOD PREVENTION ACT

by

TOWN OF RUSSELL

and

## MASSACHUSETTS WATER RESOURCES COMMISSION

BLACK BR.

and HAMPDEN CONSERVATION DISTRICT

### with the assistance of

## SOIL CONSERVATION SERVICE

#### of the

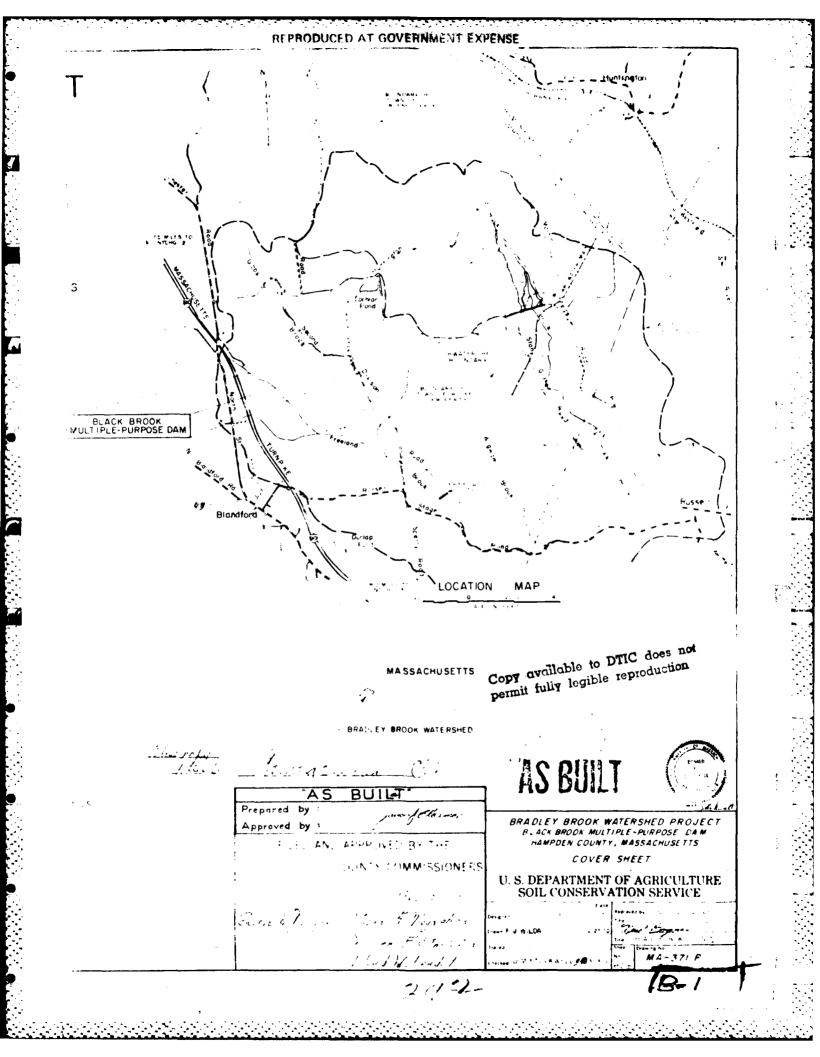
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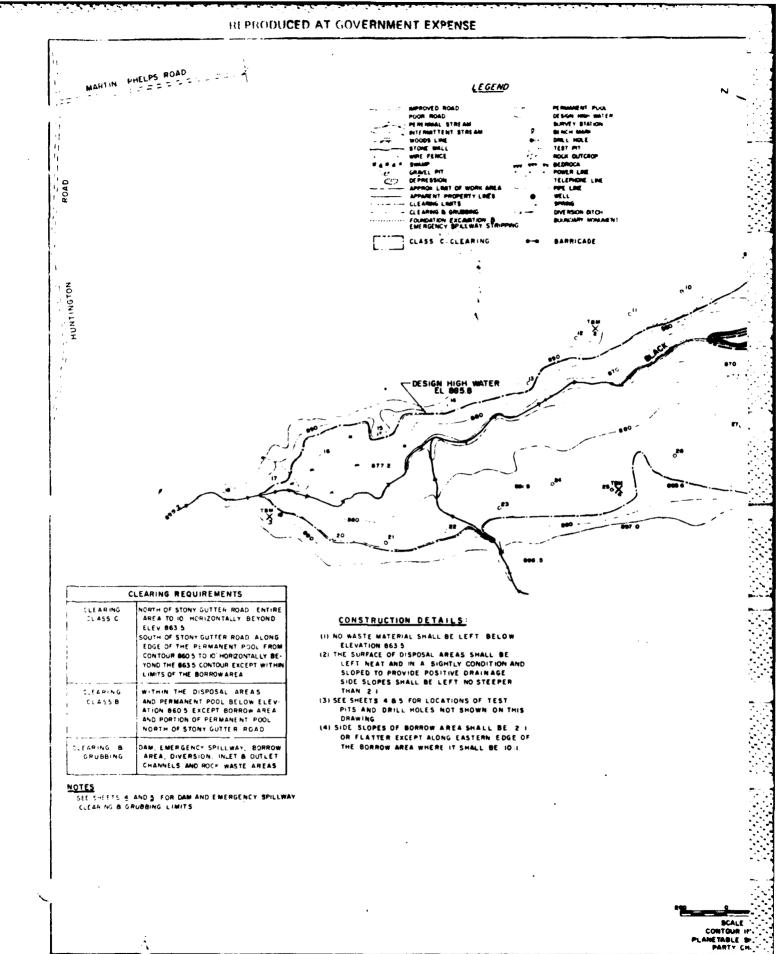
## INDEX

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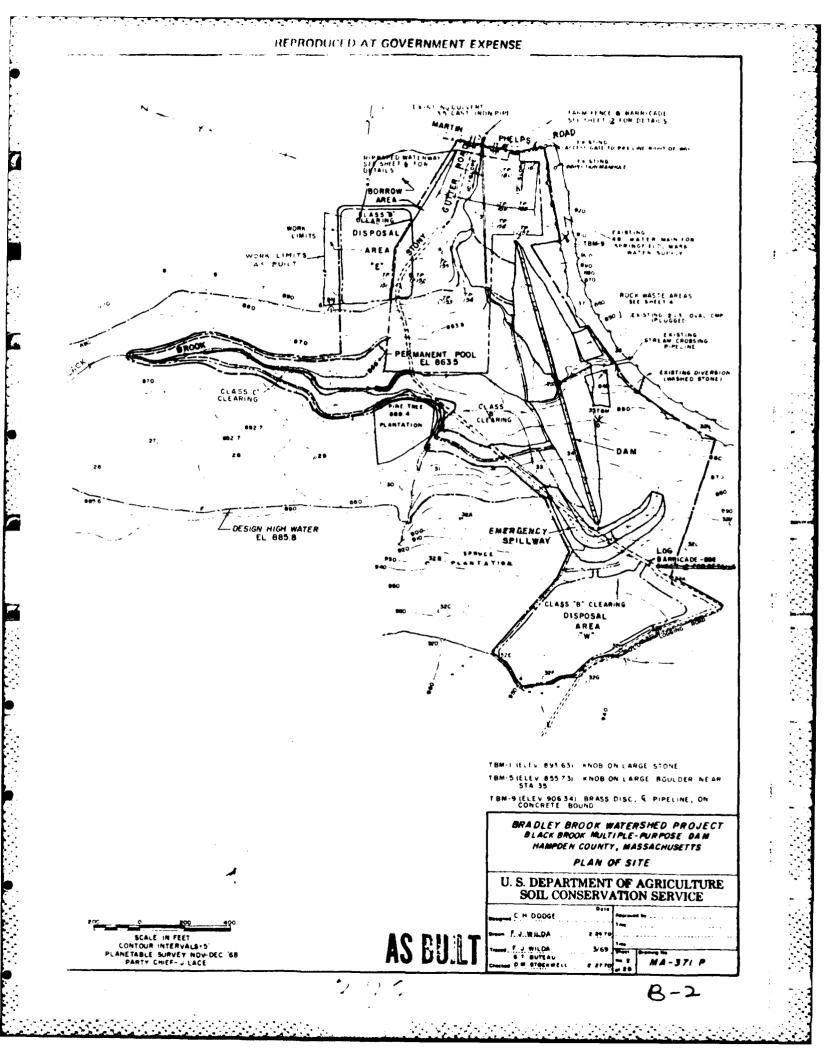
SHEET 28- STABILIZATION OF STRUCTURES

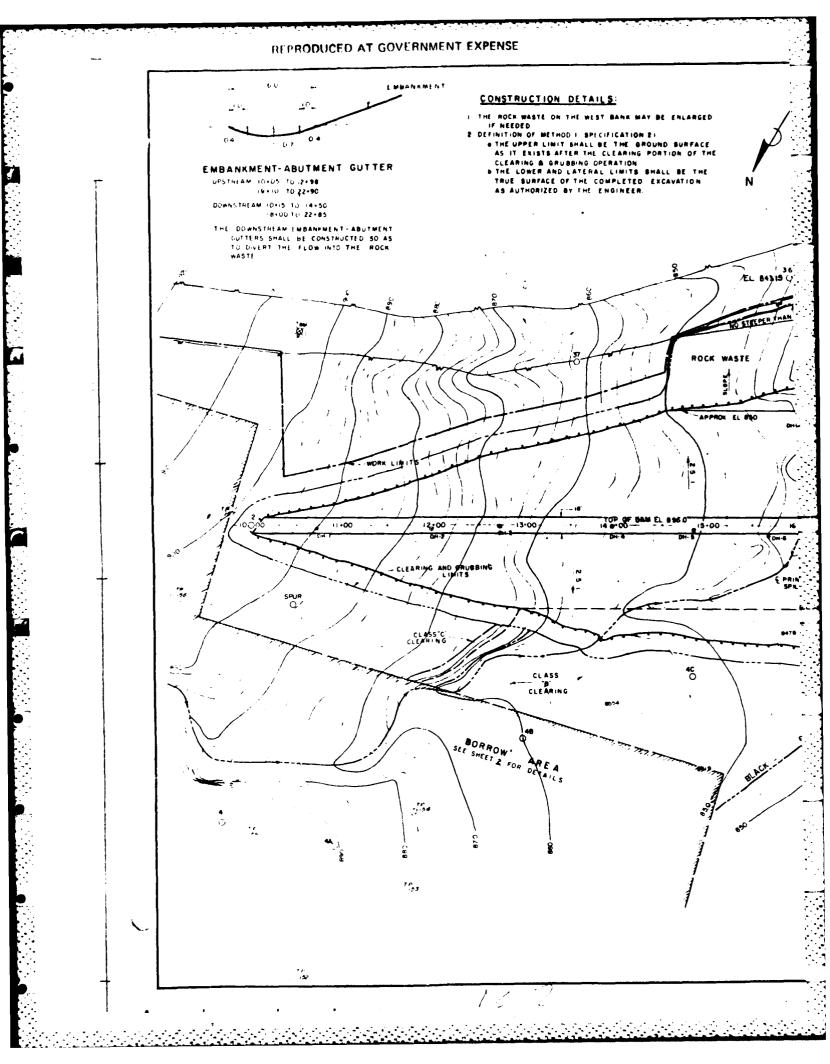


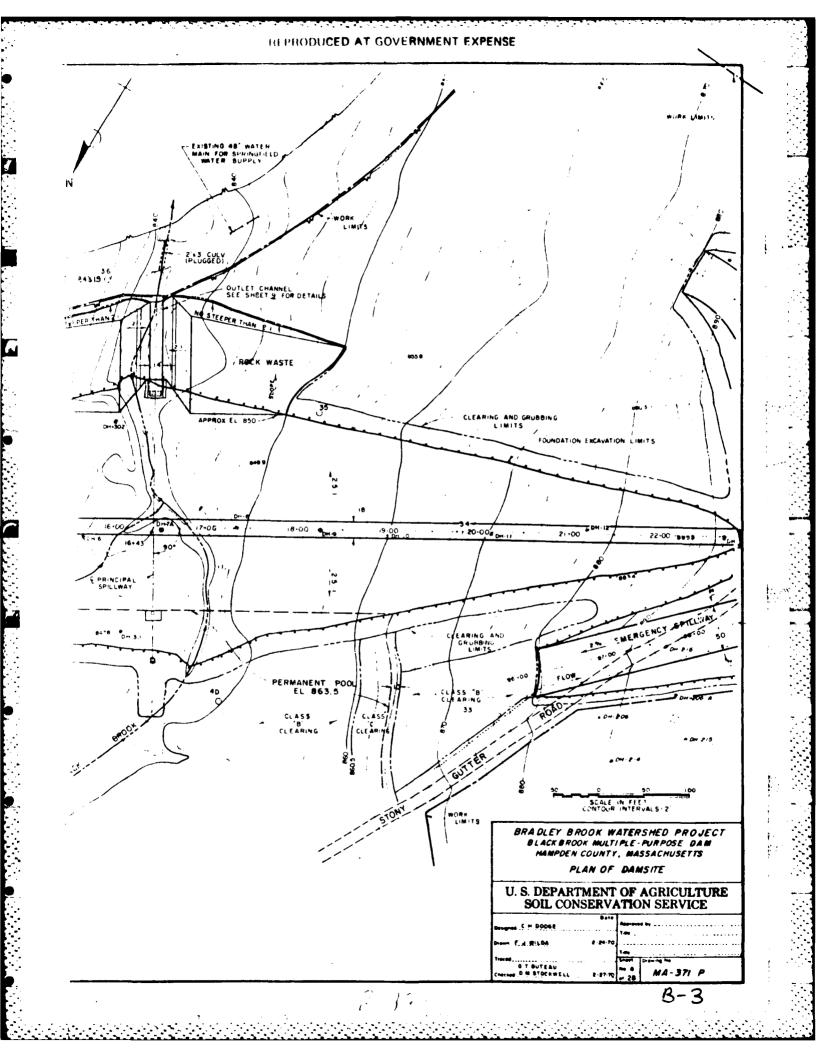


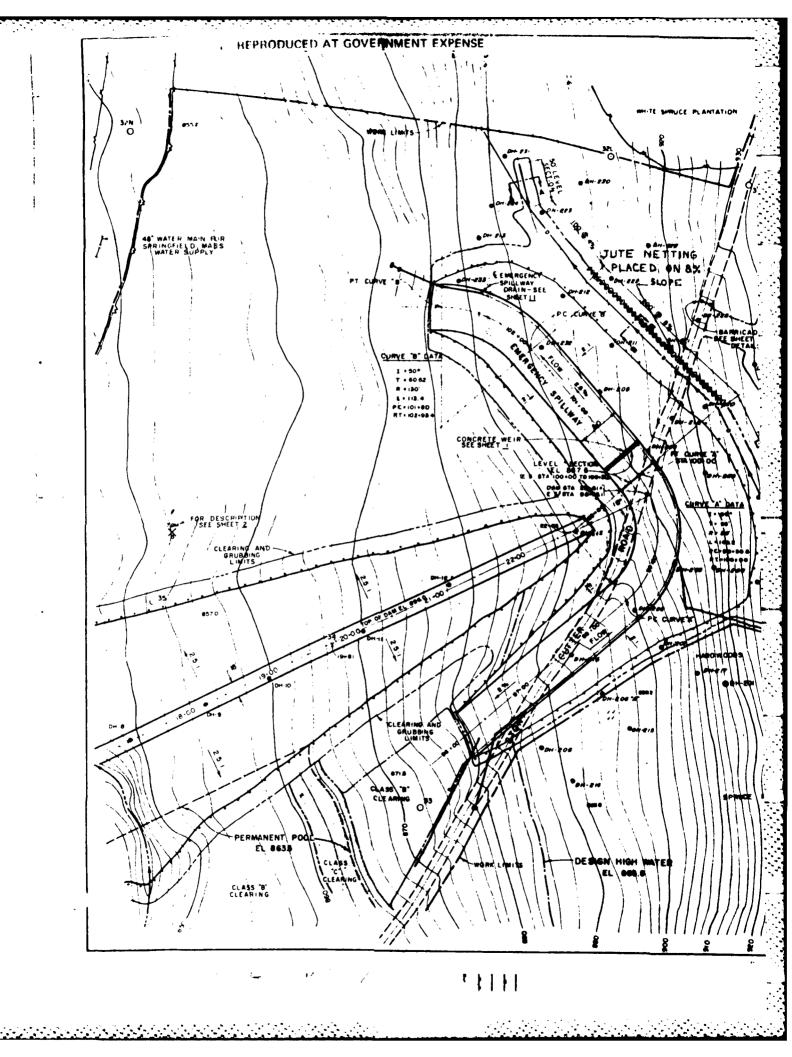
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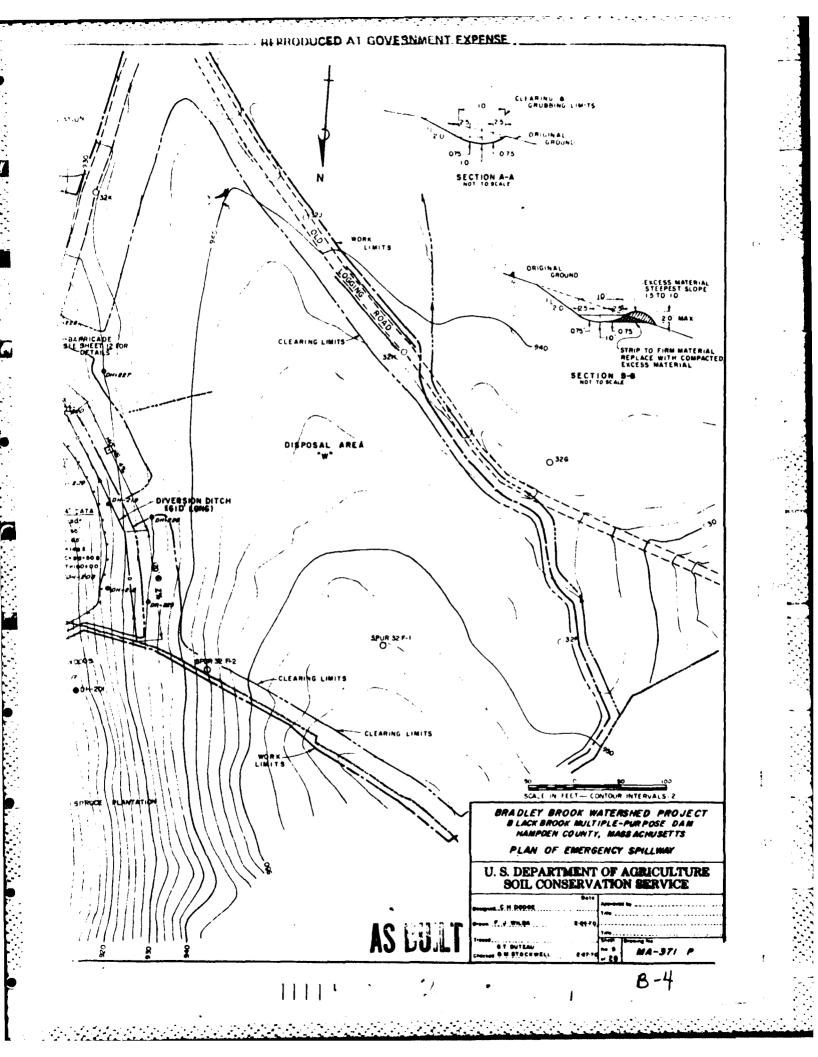
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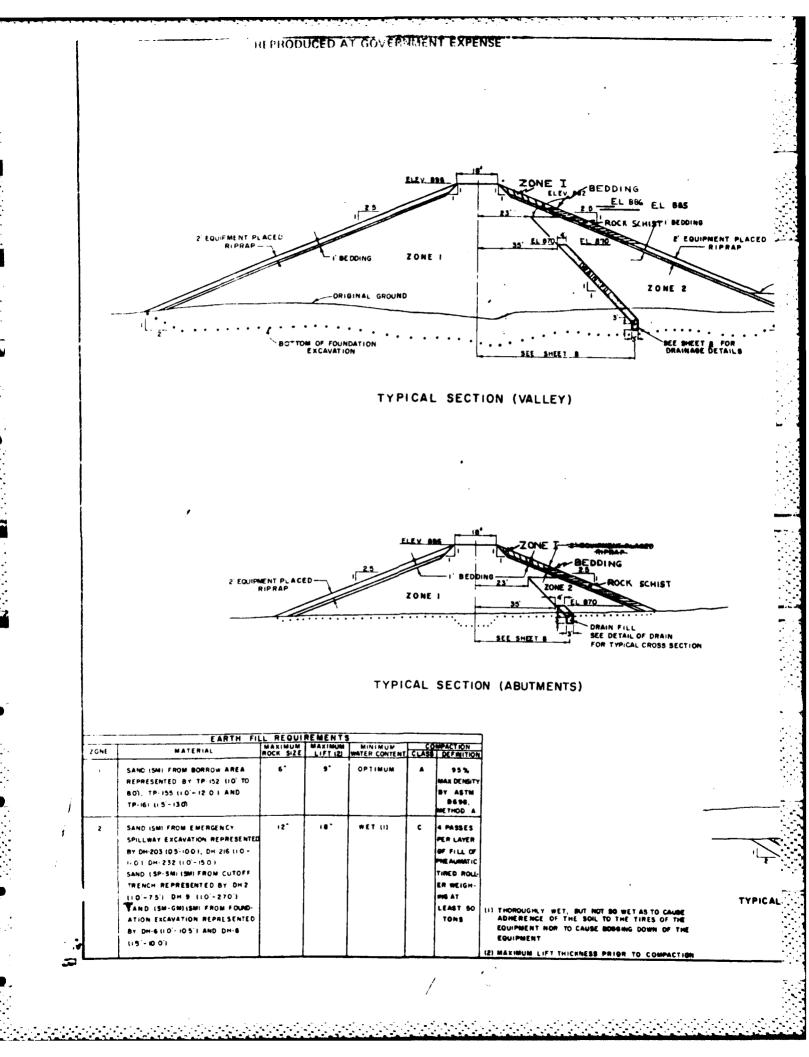


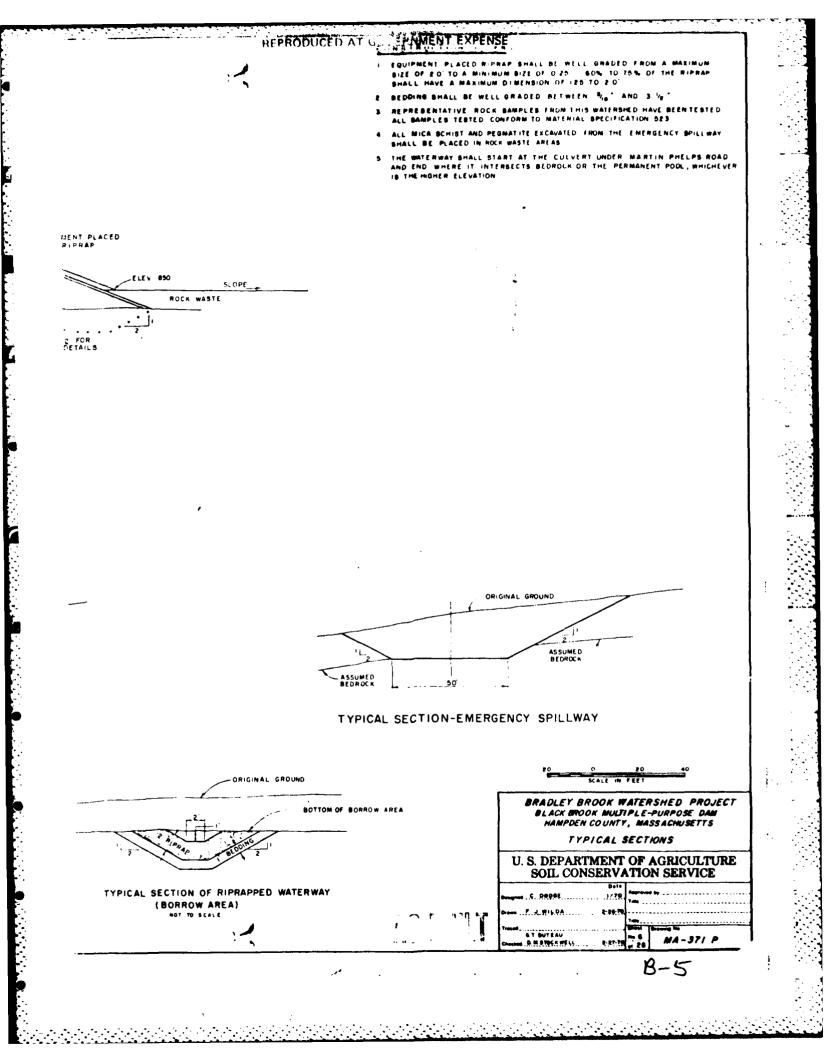


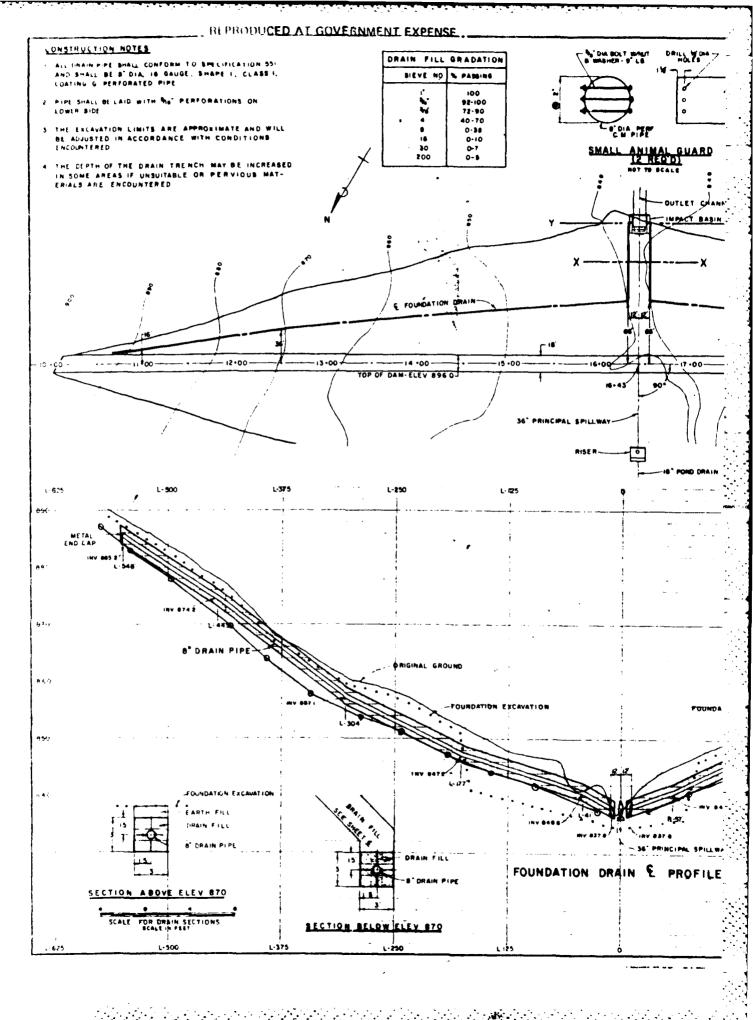


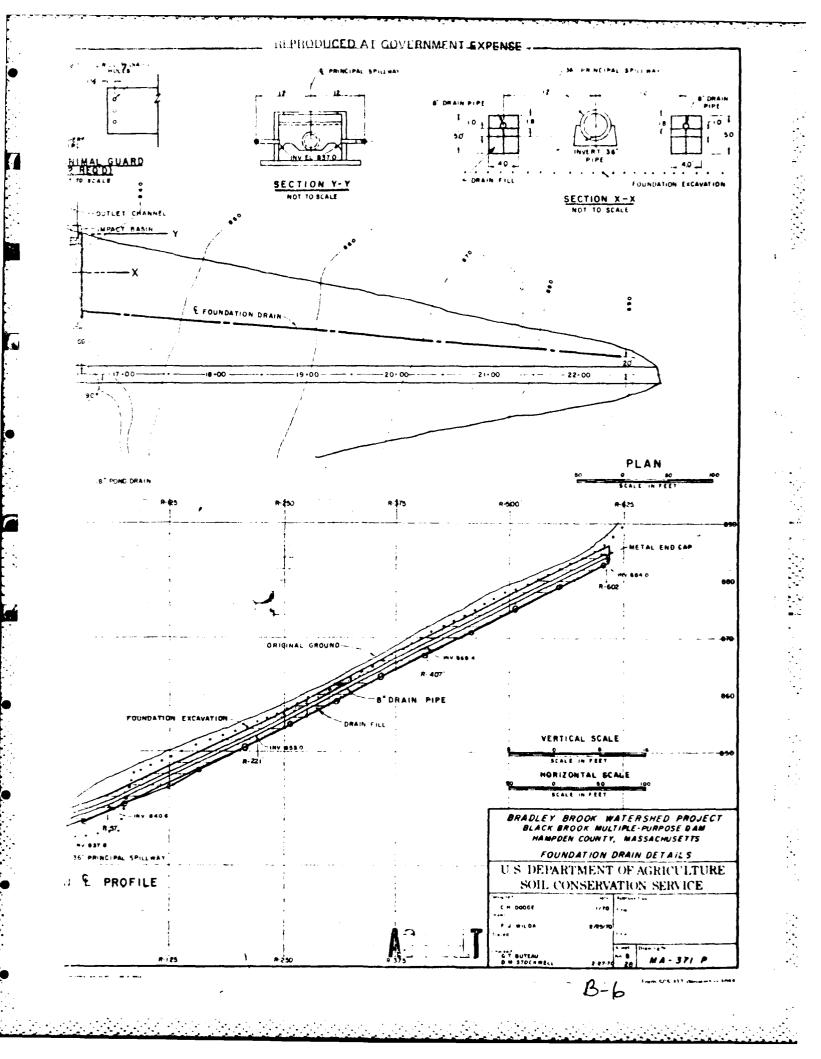




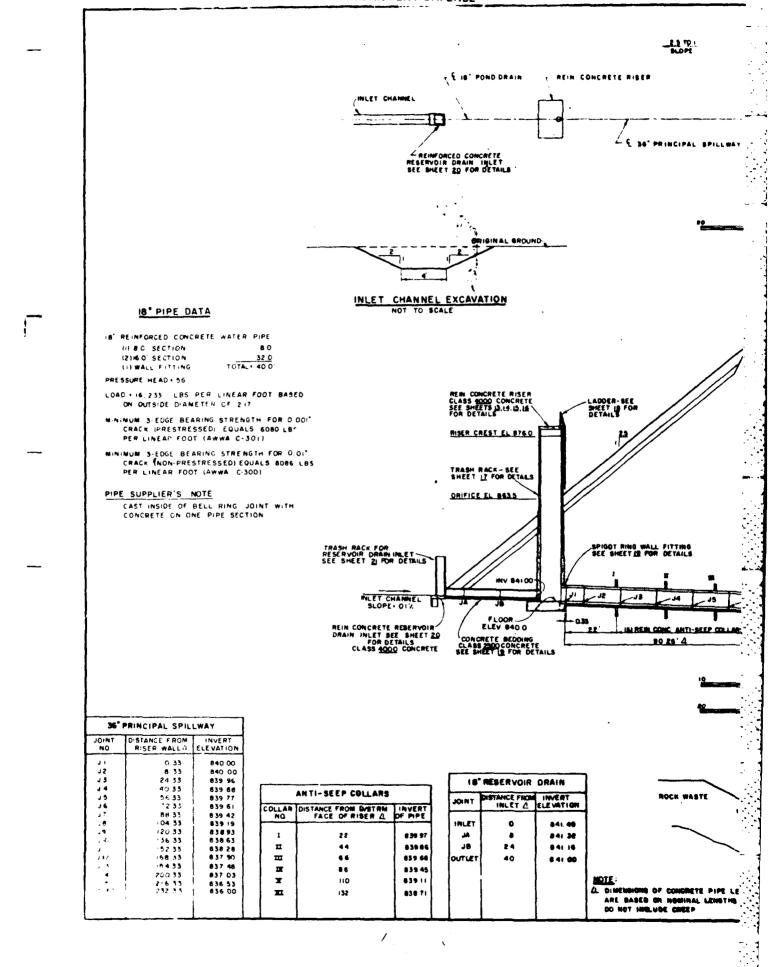








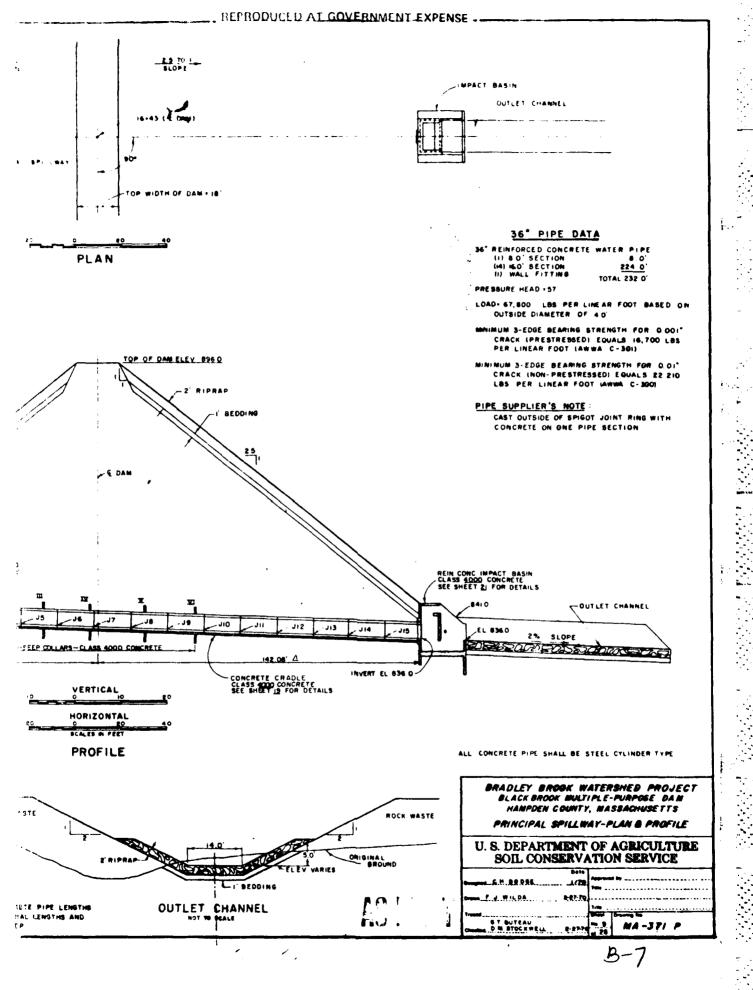
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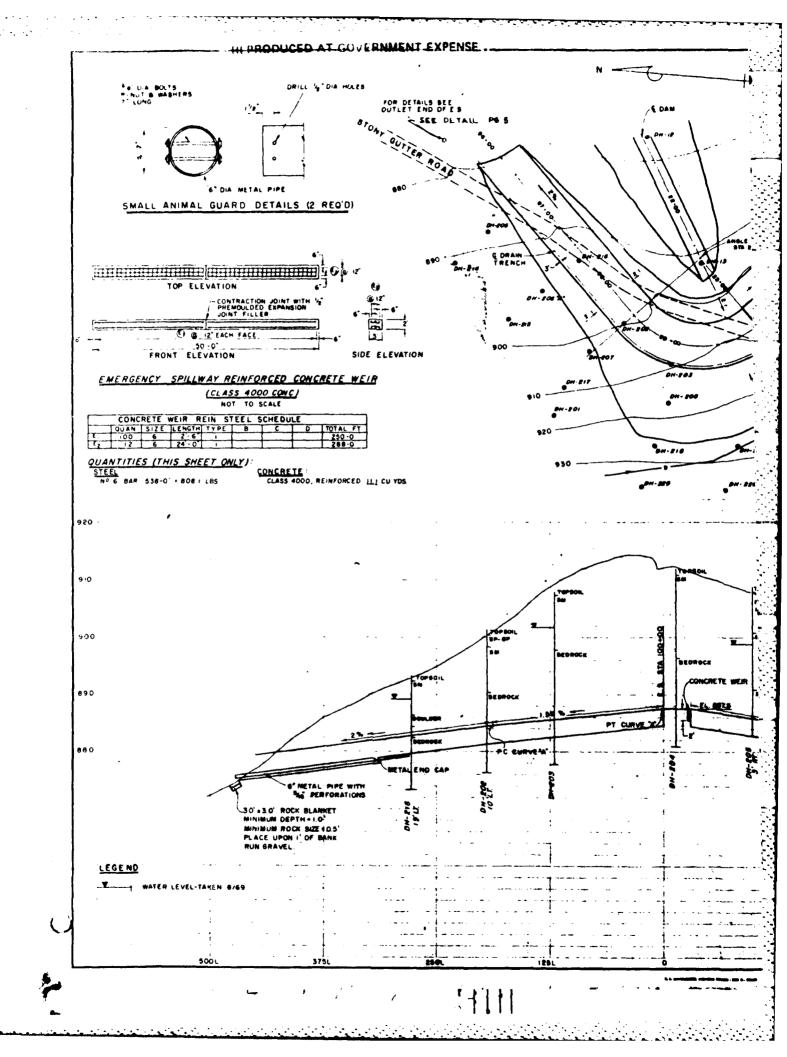
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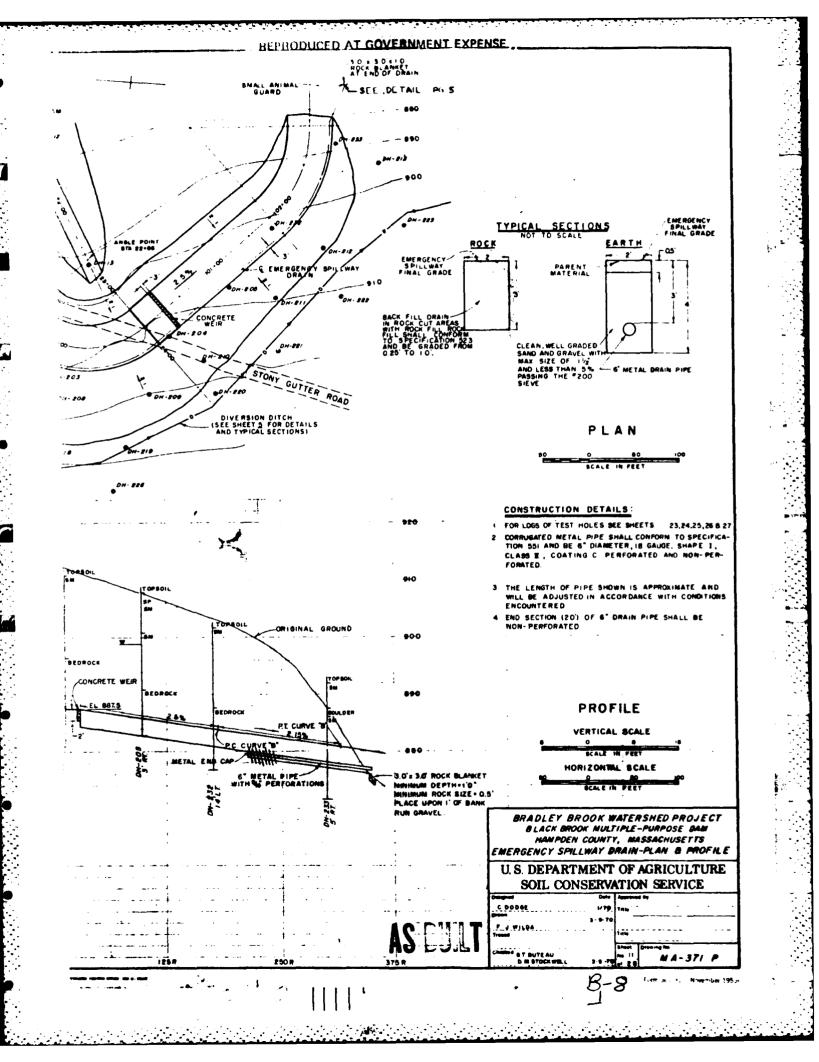
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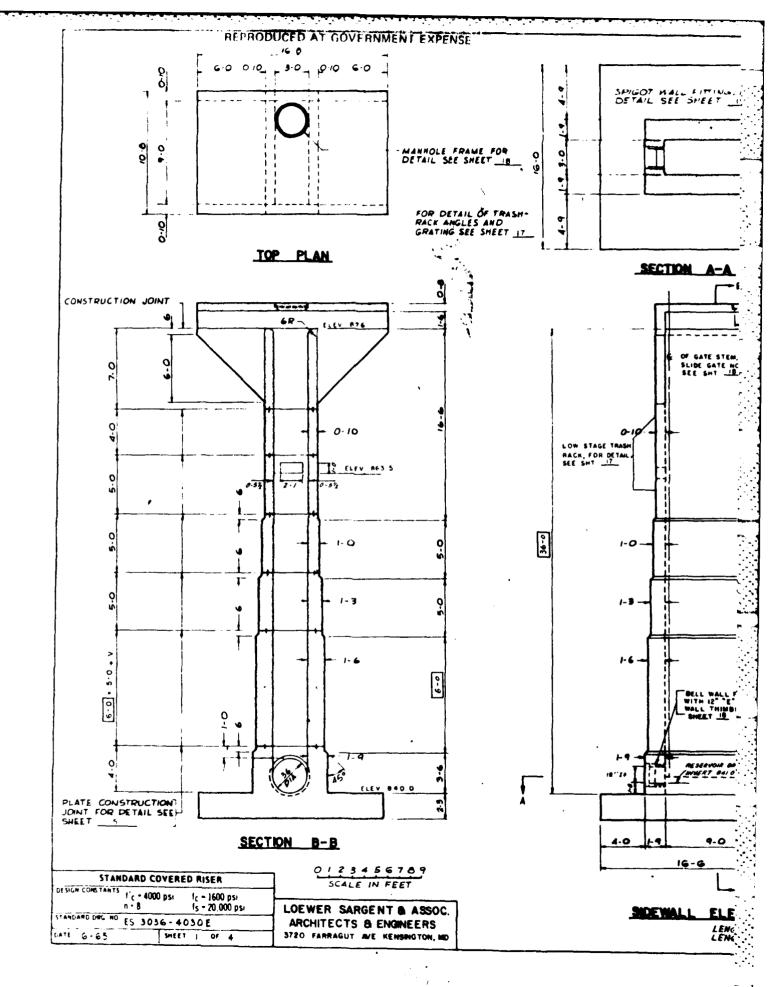
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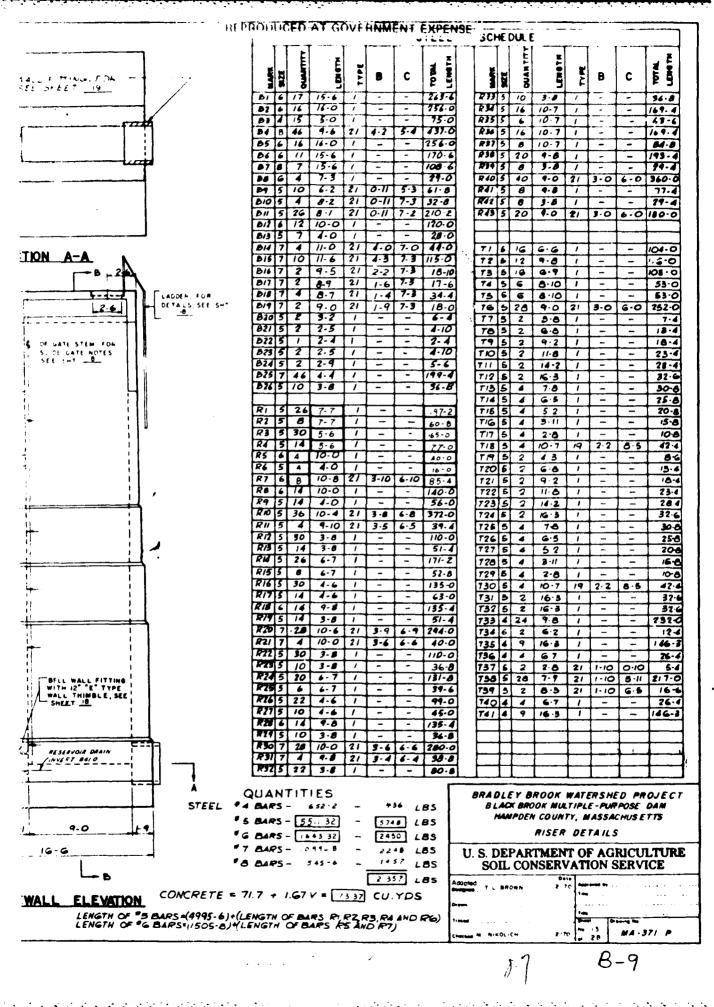


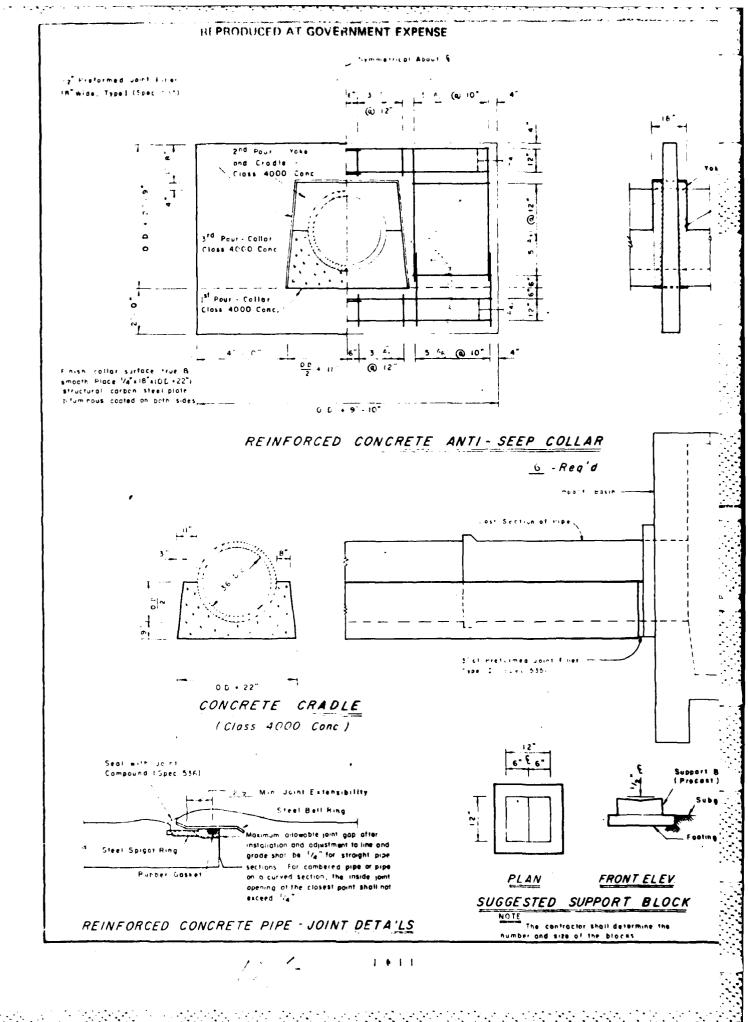
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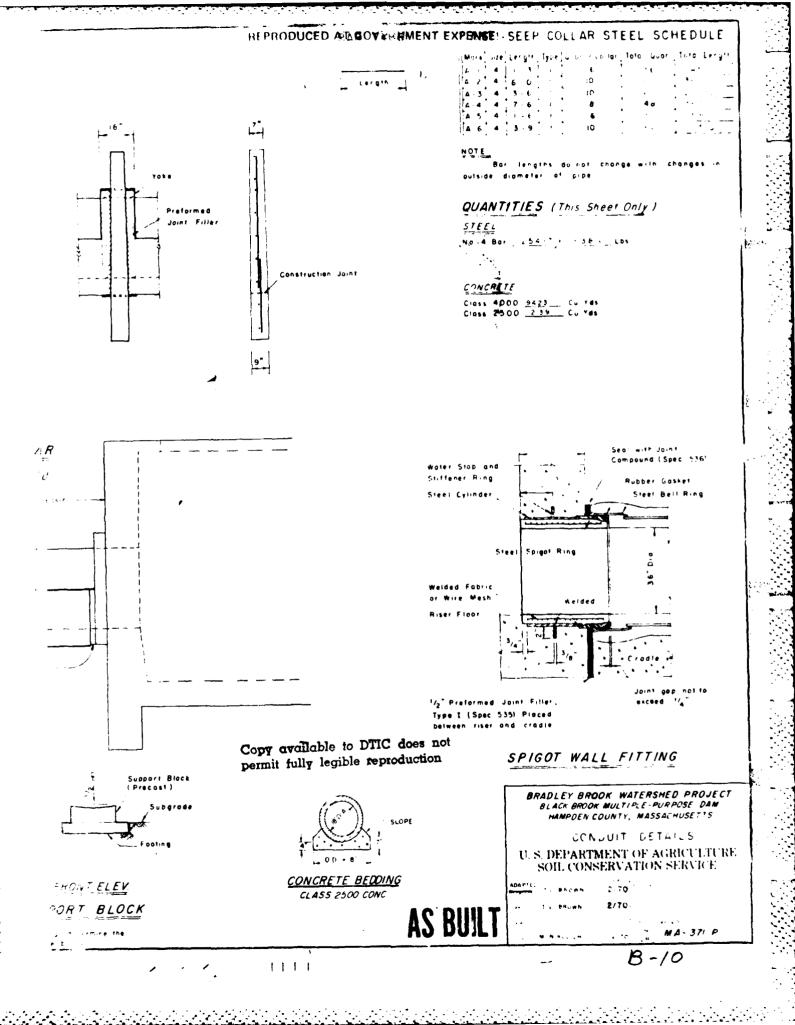


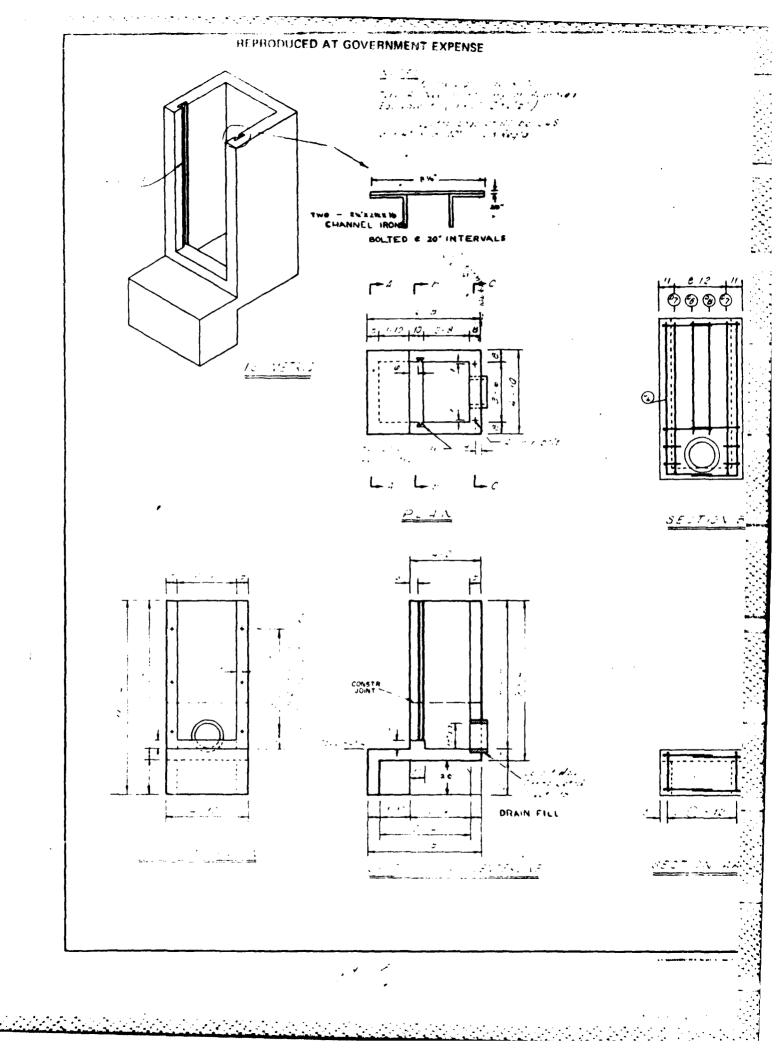


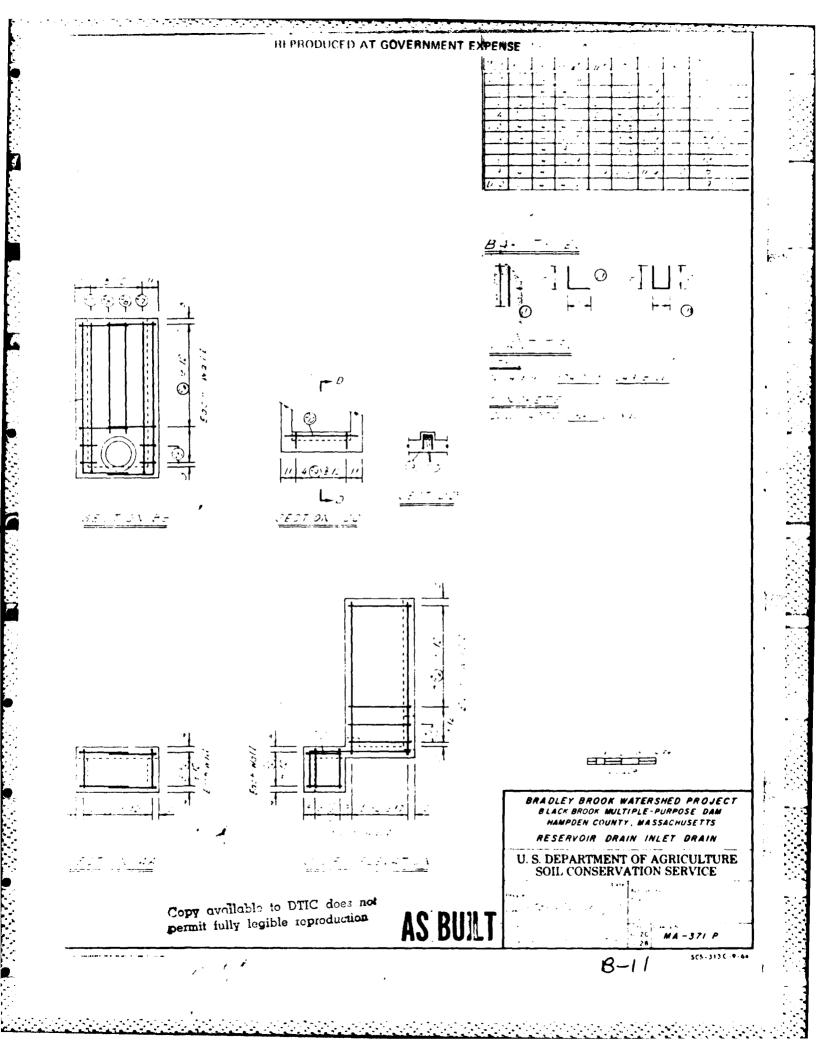


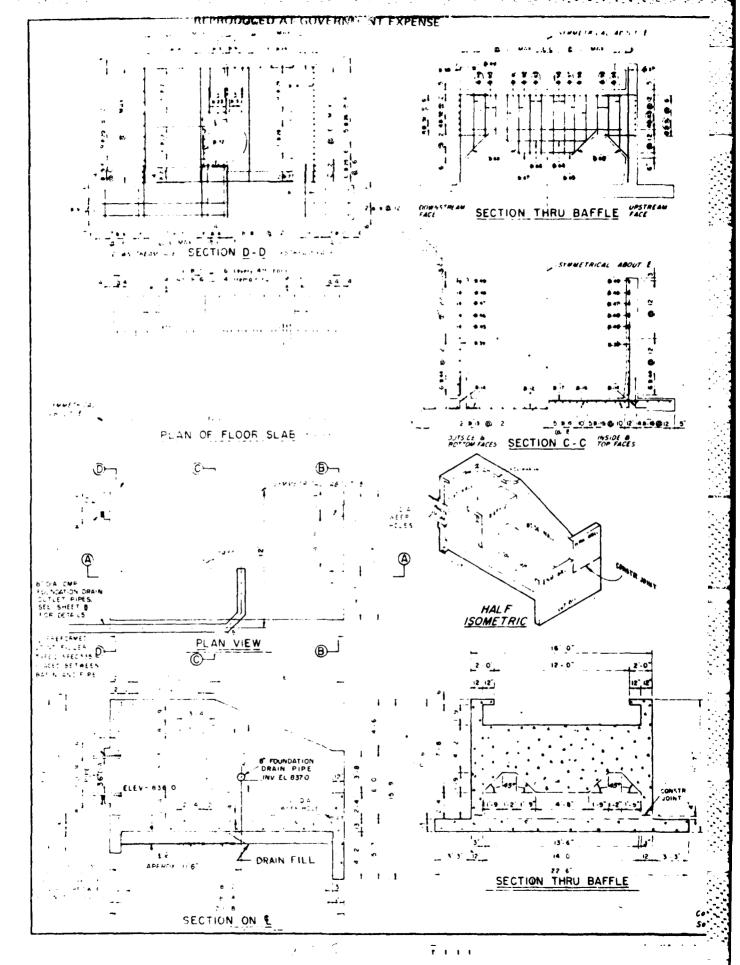




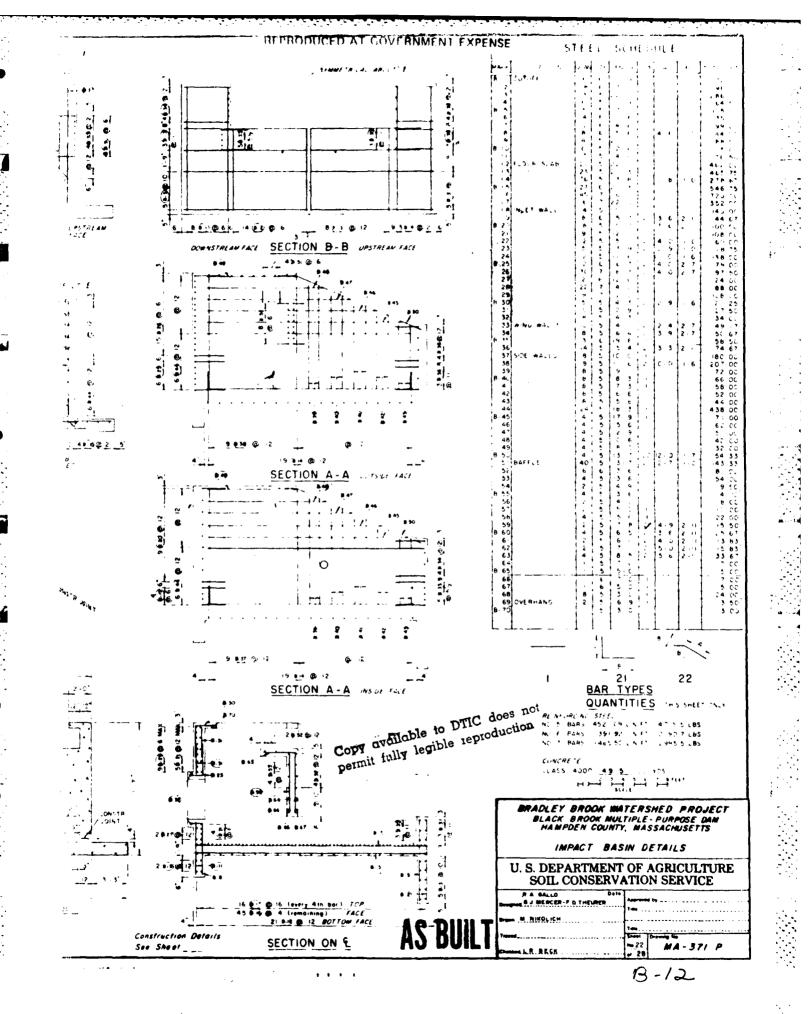








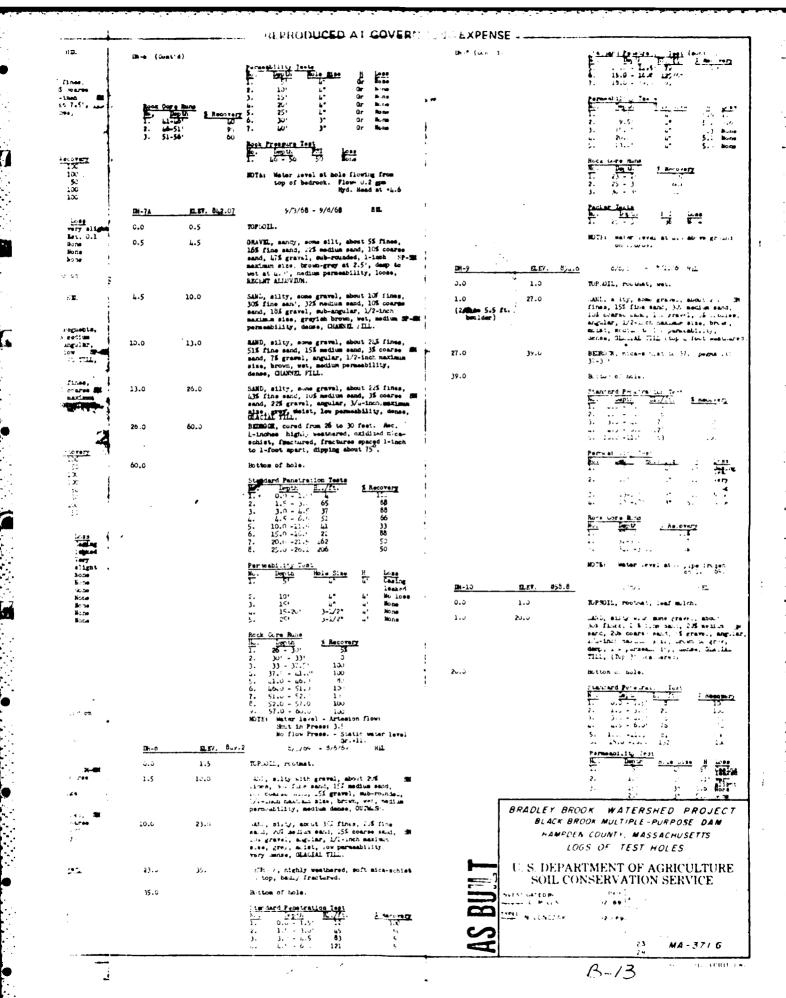
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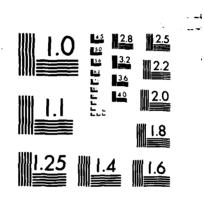
$\frac{1}{12} \qquad \frac{1}{12} $	(iost	<b>.</b>	H.	/18/67	- 8/1	8/11/6v	۔ ھىدھ		19771231919 <u>Mil</u>	ED AL GOVE	REPRODUC	به بر میتوند. و بر ف از	ð.~	AP.	
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Description         Description <thdescription< th=""> <thdescription< th=""></thdescription<></thdescription<>			1			of hole.	30 Mot		<b>2</b> 0.0						1.5
L.         D.0         F. 200         F. 200 <thf. 200<="" th="">         F. 200         <thf. 200<="" th=""></thf.></thf.>		Đ	50 100	<u>к</u> . е.	11 66 66 100	Impth           0.0         - 1.5           1.5         - 3.0           3.0         - 4.5           7.5         - 9.0           0.0         -11.5	2. 2. 3. 4. 5.		•	100 100 58 100 50 100	Si         Ft.           Si         Ft.           1.0'         45          5'         75          0'         75          5         120/6"          5         121	Landara Penetri           Landara Penetri           Low         Landara           Low         Landara           Low         Landara           Low         Landara           Low         Landara           Landara         Landara           Landara <thlandara< th="">           Landara&lt;</thlandara<>			
Image: Note of the state of the st		0.0	very alleged	<b>HH</b> 5.1	Jeye eri	Top sh	<u>1.</u>				.5 130	. 20.0 - 21.	:		
Local and products of 0/5/6/         Ref         Ref         Local and products of 0/5/6/         Ref         Ref         Local and products of 0/5/6/         Ref         Ref <thref< th="">         Ref         Ref         <thref<< td=""><td>-</td><td>0.9</td><td>None None None f</td><td>. 5.3 5.1</td><td>).</td><td>15' 15-20' Mater level</td><td>3. 4.</td><td><b>)</b> (* 1970) 1970 - J. 1970 - J.</td><td></td><td>.5 Very slight Let. 0.1 .3 None</td><td>Hola 5180 3-1/2* 3-1/2* 3-1/2*</td><td><u>k. 1.6512.</u> </td><td></td><td></td><td></td></thref<<></thref<>	-	0.9	None None None f	. 5.3 5.1	).	15' 15-20' Mater level	3. 4.	<b>)</b> (* 1970) 1970 - J. 1970 - J.		.5 Very slight Let. 0.1 .3 None	Hola 5180 3-1/2* 3-1/2* 3-1/2*	<u>k. 1.6512.</u> 			
Line         Line <thline< th="">         Line         Line         <thl< td=""><td>÷</td><td><u>ل</u>ه.</td><td>HEL (</td><td>0/69</td><td>- \$/10/5</td><td></td><td>4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</td><td>N.ST.</td><td>794 - K</td><td></td><td></td><td></td><td></td><td></td><td></td></thl<></thline<>	÷	<u>ل</u> ه.	HEL (	0/69	- \$/10/5		4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	N.ST.	794 - K						
C:         E.T.         CH12/0 - CH12/0 HE         H.0           1:         Th CH1, revear.         H.0         3.5         Second and the framework in the framework										ground on 5/15/69	wei at 3.9' below	uffi materia			
100         100 Autor,	•		fregenate,	and rook	e gravel (	ailty, some	. SAND,			HJZ.					<u></u>
atom, 070k H TRUAL.     9.5     D.3     D.4.5		10.	ingular,	155 gravel, own, moist,	and, 155 198, brown Des, WEAT	25% coarse in maximum si ability, den	send, 1-inc perme			Carse sand, Aximum Sise,	ilty, aboit 10% : nedium mand, 25% -round, 3/u-inch	AND, gravel, s line sand, 35% r D% gravel, sub-			
11/2       11/2	I.	ນ.	Ж воагов 🜉 🥐	um sand, 20	OS medium	ine sand, 20	258 1	5.5ط	9.5	eability,	ndium to low per TERRAJE.	prown, mulst, ne lense, OUTWALH 1			
Action of noise.         Decision Provide Noise. <thdecision noise.<="" provide="" th=""> <thdecision noise.<="" provide="" td=""><td></td><td>26.</td><td></td><td></td><td><del>.</del></td><td>AL TILL.</td><td>OLACI</td><td>57.0</td><td>15.5</td><td>Carse sand, SM</td><td>nedium sand, 15% Jular, 1/3-inch m Sist, los permeabl</td><td>ine sand, 20% r b. gravel, Angulive-bruwn, mos</td><td></td><td>21.5</td><td></td></thdecision></thdecision>		26.			<del>.</del>	AL TILL.	OLACI	57.0	15.5	Carse sand, SM	nedium sand, 15% Jular, 1/3-inch m Sist, los permeabl	ine sand, 20% r b. gravel, Angulive-bruwn, mos		21.5	
B::         B:: <td></td> <td></td> <td>Becomer 4</td> <td></td> <td>Lion Test</td> <td>ard Penetrat</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td>• Þ</td>			Becomer 4		Lion Test	ard Penetrat						-			• Þ
Person Uliv: Trait         Dist         Dist <thdist< th="">         Dist         Dist<td>· ·</td><td><b>6</b>0.</td><td>50 100 50 50 100</td><td>7 1 8 5 5</td><td>60/6 137 118 118 115 100 120/6</td><td>1.5 - 2.5 4.5 - 6.0 10.0 - 11.5 15.0 - 16.5 20.0 - 21.5 35.0 - 36.5 42.0 - 43.0</td><td>1. 2. 3. 5. 5. 7. 8.</td><td></td><td></td><td>10. 50 130 10. 50</td><td><u>B1./ft</u>. .5' <u>6</u> .0' <u>32</u> .0' <u>50/6</u> .0' <u>5</u> .5' <u>5'</u></td><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td></td><td></td><td></td></thdist<>	· ·	<b>6</b> 0.	50 100 50 50 100	7 1 8 5 5	60/6 137 118 118 115 100 120/6	1.5 - 2.5 4.5 - 6.0 10.0 - 11.5 15.0 - 16.5 20.0 - 21.5 35.0 - 36.5 42.0 - 43.0	1. 2. 3. 5. 5. 7. 8.			10. 50 130 10. 50	<u>B1./ft</u> . .5' <u>6</u> .0' <u>32</u> .0' <u>50/6</u> .0' <u>5</u> .5' <u>5'</u>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
1       b/12/69       c/11/69       HEL       6.       40°       3-1/2° 0       Bose          1       TOP-DIL, leaf muich.       5.       40°       3-1/2° 0       Bose          1       TOP-DIL, leaf muich.       5.       40°       3-1/2° 0       Bose          1       TOP-DIL, leaf muich.       5.       40°       3-1/2° 0       Bose          1       SAME, pressin, score stl., about 75 fines, 25-30       Same       1       5.       5.       1       5.       1       5.       1       5.       1       5.       1       5.       1       1       5.       1       1       1       5.       1       1       1       1       1       1       5.       1.			Identified I dentified I dent	4" 5. 4" 5. 3-1/2" 5. 3-1/2" 5. 3-1/2" 5.	<u>Holo</u> 1" 1" 1" 1" 1" 1" 1"	Dep th 5' 10' 15' 20' 25' 30	2. 3. 5. 6.			Long O.y gpm None None	131 <u>Rele State</u> 3-1/2" 5-3 3-1/2" 5-4 3-1/2" 5-5	<b>Correct 11119</b> Ter <b>1.</b> <u>201</u> <b>1.</b> 107 <b>3.</b> 157 <b>4.</b> 207			
<ul> <li>NANG, gravel, some slit, about 75 fines, 2.3 fine sand, 35 meile, sand, 20 course S-ST search, 15 gravel, routed, 1/2-inch maximum stre, brown, darp, nexturn-hap permeability, dense, TANALE 1200ETL.</li> <li>ANG, s.ty, about 5.6 fines, 255 fine sand, 2.4 moiler sand, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, ST sequers, 1/2 course sand, 1/2 course sand, 2/2 gravel, sequers, sequers, sequers, sequers, sequers, sequers, 1/2 course sand, 1/2 course sand 1/2 course san</li></ul>			) Hoan	3-1/2" 0	.ر	40'	ő.			HEL					<u>n - :</u>
11:1       1.4%, s.t.t., sbott i.i fines, 255 fine sand, 2 is moilum sand, 155 coarse sand, 155 gravel, mi acquiar, 1/2-inth maximum sise, gray, moist, .ous processitily, wary dense, discill Till.       Acc / Login       Discillation for the set of t			:		52.0	145.5 - 4 147.0 - 5	1. 2.			OS compe SP-SH . ch maximum	ione sili, about 30% measur sand, 1, rounded, 1/2- sp, conternigh [	GANE, gravel, so CM fine sanu, j Galu, 136 gravel Dize, brown, dar			•
argular, 1/2-thin fractions size, gray moist, the prince of the set of the s		t		loss		Lepth	Жо.			fine sand, 155 gravel mar i	out 2.5 fines, 2	AND, sliting abo		21.(	
Bit to of mile.       Bit of mile.       Bit of mile.       Bit of mile.       Bit of mile.       Mile       Bit of mile.       Mile					level at h	i Materle				rey, moist,	ich maximum sise,	ngular, 1/2-ind			
Interform     Interform     Interform     Interform       No.     South     Birlin     Birlin     Birlin       No.     Birlin     Birlin     Birlin     Birlin       Birlin     Birlin     Birlin     Birlin     Birlin       Birlin     Birli			•	* 15 1 40			au -			1		all the second second ex			
<pre>1. 1 5.00 60 100 10 10.5 SAMD, gravel, silty, about 20% fines, median and, 10% search , 1.5 11% fine sand, 10% gravel, methods and 10% fine sand, 10% search , 1.5 11% fine sand, 10% search , 10% search , 10% fine sand, 10% search , 10% search , 10% fine sand, 10% search , 10% sear</pre>	<u>98-0</u>		anagin .	G/ 3/ GY						A Recovery	B1./ft.	ta dard Printer			
1.1       1.1       1.0       1.5       fine sand, 10% measure and, 10% grave, measure and 10% grave,	<b>0.</b> 0		nes, <b>31-61</b>	back 20% fi	11 <b>4</b> , aba.	gravel, al	SAND			100	3.0° 6¢	i. i. • ;			
I.      5.7 Nume     10.5     10.0     andly, solidy solid general, and the send, 25% concrete     10.0       3.        10.0     15% fine send, 7% solid sendum as and 7% solid sendum as and 7% send	1.5	• •	inch parada-	Funded, 1- mi, medium ALIFUIM.	I, BUD-F.4 FOMR, Wet, WALLEF ALL	4:5 gravel min sive, br by, looss, 8	sand mari bili			100 . <u>Loss</u>	1151 121 1151 121 Hole Size	n 2. no 21 Permenti ni in ini Permenti ni ini ini			
	10.0		10h mari-	lium sand, 2 Liar, 1/3-1.1 Lou purnsab	258 modiu 1, angula damp, 10 CIAL TILL	fine sand, 7 , 105 gravel sise, gray, dense, GLAG	155 sand Muli Vary			7 Nume 3 None 1 None	3-17.1	. 2			
	<b>13.</b> 0		No cat #9/7		ation Tes BL./IL.	dard Penetre	Star M.	: 6. J	1.1.0						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35.0		100 100 50 100 50 50 100	/6"	13 177 125 200/6" 53	1.5 - 3.0 3.0 - 4.5 4.5 - 5.0 10.0 -10.5 33.5 -35.0	2. 3. 5. 6.			loes not de si -	gible repr	available fully log	Copy perni		

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AD-A1	55 633	NAT Bla	IONAL Ick Bri Nem Ei	PROGR OOK DA NGLAND	AM FOR M (MA DIV	R INSPE 0(U) MAR 80	CTION CORP	OF NO 5 OF E	N-FEDE Ngines	RAL DA	ins Than	2/	2
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17h	1												
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						_							



MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

2	prv.	с. с. н. 11 буна.	Be-2 or an	<u>B-B</u>	and the second	101. 1
	1.	RP2011, proceed, case most	~ <b>.</b>	و.ب	RPUIL.	
••	2	SANL, B.IL	J.5	9.0	SAND, stilly, even organic, element uit Elemen, 315 filme seur, 205 metrus eend,	
		abul 2.3 unt a, 3.5 Can maid, 1.4 adi a said, R cuares sand, 1.5			65 overse and, 20 gravel, 3/ Lost. Realman Alar, brown, colet, met.an. 37-68	
		graves, aug lar, 3du-the earts. alte, drums to gre, at , teel, wist.			permeability, io ee, THULLCE DEFUSITE.	15.5
		ande, Julius perioditizza vor- Laide, Hauzai III (neo voro i in	<b>,</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	aust .	QRAVE, and with race fragmente, down (\$ final, )\$ fine raid, 108 metion dand,	
			(11.5 to 12.5	ported, )	70% source send, 60% gravel, angular, 1-inch maximu, e.s., brown, deep, 67-68	ieu.5
8.00		Build 1 0			montum permethill'y, very donne	
		Stan and Ponetrat. on Tout- By Luph E./It. & A covery	24.5	30-0	BEIRDER, miss schiet, top 4 feet highly menument and fractures.	. ډر
		2	ە. س	·.	introm of pole.	•
		ن. يكتب (1.0 – ريي			Jundard Peneuralling Thata	
		je instalije ibu Du Portalije Teeto			L. Input H.//L. & Account	
		Loss Loss Chief Size			2. 1.5 -3.0° 3, 200 3. 3.0° 4.5° 56 86	
		د معنی کر در معنی کر د کر در معنی کر در معنی ک	•	•.	u. 4.5-5.5 111/6" 66 5. 13.6-11.5' 100/3" 200	
		3. <u>1.</u> 3-1/2" 10:00			6. 15,0-16.3 137/8" 100	
		2.: 3* None		4	Permandellity Tools No. Dopto No.1. Star. 1 1000	
•	ELFV.	1-1 a/_1-5, - 8/23/5+ (p		4	A. 5" - 5" Casing Junior	
<u>ir-d</u>		TUPSUL, rouses, fine-grained		4	2. 10 <sup>1</sup> 2".18" Gr. 15.1 Gr. 3. 10-15 <sup>1</sup> -1/2" Gr. 15.1 Gr. (. 12-30) 3" Gr. 2-mr.	
		Bog Heite		1	4. 17-30* 3* 87* 7977 slight	
		LAND, Siley suby gravely boulders, SN about 21 lines, 255 fine serve 215			Ruck Core Aune	٥.
					No. Depth Recovery	1.
		elta, bruch vo grej al 1 fest, molst, 100 permatility, deuse, GLACIAL TILL			2. 17-21' 100 3. 21-25' 100	
		(weat rud in top a foot).			li. 25-3. 100 HOTEs Mater lovel at 20-01below ground	
12	8	BELADUK, was required in carschist,			en 9/11/68	6.
		Busine of the last	<u>DH-202</u>	LET. 901.		•••
		Landar Peneiration Test	3.0	1.0	TOPSOLL, rootmat.	
			1.0	3.0	SAND, gravel, about is fines, 20% fine sand, 20% medium sand, 20% section sand, 20% sectors	
		3.   35   50 3.   35   132			405 gravel, subsounded, 3/4-10th meximum size, brown, sale, so in parmonbility,	18.
RUCE ST		Person's 1157 Testa Austria de Siger de Loss	• •		Redius dense, OFTMA.: TERACE	26.
	h & hur our	Au ingit Hote State Loss Very stught	3.0	11.0	SAME, silty, some gravel, shout 30% fines, . 15% fine eand, 20% medium send, 20% comment	••••
		2 1.2 hone			sand, 15% gravel, angular, 1/2-indu and i maximum eise, gray-brown, moist low	
		3. 101 31 5.5 None 	11.0	<b></b>	permembility, very dense, GLACIAL TILL.	
'ā -	<u> </u>	······································	11.0	25.0	(top 3') fractures app of 2" to 8" aparts	
	• J	TUPBOIL, ruothat, ira: mulet.	25.0		Botton of hole.	
•		CALD, sity with gravel and mach, St :	23.0		Standard Passyntics Test	
(		about 2.1 fires, 30k fine same, str. a section word, by coerse same, 5% gravely			Ro. Daptio H.// L Ance Page 1. 0.0 - 1 2 100	
		argular, 1/2-inch maximum aise, brown, W 1, jos permospility, denne,			2, 1,5 - 3,0' 22 100 3, 3,0 - 4,5' 62 100 f	
		VERTIERED GLACIAL TILL.			س. 10، 32 10، س. 10	
••	2	BEDNO.X, rca-echist.			Rock Core Bane R Conth & According 1. 11-15	<u>興</u> . 0.0
<b>2</b> 5.		ສະພະເຕັກອະຈະ			2. 15-16 100	1.0
		Stature Penetration Teste No. Lepth Bir/fi. & Recover			3. 10-23 80	
		2. i.j j.v. 10 00			HOTE: Mater lovel at - pipe fromm 12/5/80-	•
		00 مىلە - ئىز بر 01 - 60 - ئىز بىر بى	<b>21-2</b> 03	<b>51.07</b> , 907	<u>-8</u> 8/6/69 #2.	
		Periodo 1117 Teste No. 1510 doin Size o Long	0.0	0.5	70P 5011.	19.0
		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	0.5	10.0	SAND, dlity, ame gravel, about 155 fines, 1 155 fine sudd, 335 measur mend, 255 conten	•
		Z, 1.º! 3-1/2" 5.3 № № 3. 1.º 3-1/2" Δr. None			rand, 15% graval, sub-routied, ./C-insh	
		Res. C. r. Reta			to notive personality, dense, didili	
		1. 1. 17 10.	10.0	30.0	BERNOR - wice setiet - moderately fractasted	
		1, 1,-2, ,J ,, 21,-2, €0			fractures a indus to 1. inches sport, and ; fractures dipping W, some harissetal.	
		BOCK Pressure Toss	30.0		Notion of hole.	
		No. Dett. P51 Loss	Book C		Standard Poststettion Tons	
			1.	10-12" # Accover	Z 1. 0.0 - 1.5 3 100	٥.
		and loss not	<b>j.</b> .	12-16" 75 16-19" 80	2.         2.         3.0         3.2         80         1           3.         3.0         - 4.5         70         100         45	1.
		available to DTIC does not	4. 5.	19-24' 100 24-29' 100	k. u.> = 6.0 00 66 i HOTE: Matur loval at <u>6 fact Jac</u> ley ground	
	Copy	available to Diffe doubten it fully legible reproduction	<b>3</b> 1-201	29-30' 100 E.T. 911	66 WWW7.	
	perm	II treat	0.0	1.0	TOPSOIL, rootmat.	
					والكرافي والمتحد والمتحد والمتحد والمحمول والمحمول والمحمول والمحمول والمحمول والمحمول والمحمول والمحمول والمحمو	

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,	Marine (Constat)		REPRODUCED AT GOVERS	-		
	Main Contral	E.C.				1
	<b>å</b> • 5	11.55	SAN, silty with grownal, about 2000 2016 Junes, 3026 Eine annal, dy6 an tium, ,	11-U	2	BRANCE, projection, consideration And Alica, well there is the terms of
			sant, 15% coarse send, 15% grave., sub-angular, 3/u-inch sanisms size,			aparts from the second states and an aparts from the second states and
_			brow 's grey, same low personblikty, dense, DLACIAL TILL, weathered in	21.J		Button of the second se
- 69			Sig L Jeet.			
. L	15-5	20.4	BRIGUER, pormatite, monthy inidepar			Stendard Pointaniso Test
4 <b>4</b> ,			and mica; for frastures, molt.			
P-08	N.5	41.0	BRINDE, mice semist, highly fractured, frectures 2-13-inches			ر ۲۰۰۰ میز از ایجاد ۲۷۷ (۱۰۰۰ ماله می
			spart, most fractures dipping about /u sume hurisontal.			ال ال الم الم الم الم الم
4	ن. {ر		Buttom of hole.			Buck Care Russ
	,					De Lore Auto De Lore & Nacovery J. 1817 - 2017 Jul
			Standard Penetration <u>A.</u> <u>Depth</u> <u>EL./ft</u> . <u>E Recovery</u> 1. 0.0 + 1.5 13 130		•	2. <b>36.</b> 2. 21. 5
z			).≤ <b>- 3.0 - 11 - 10</b> 0			MUTSE Mater Level Liesing at euroses B- +0 SPL
7			j. 3			sone as a sector de
			5. 10.0 +10.5 103/6" 100	•		
			Non Core Rune	Di-207	ELEV. *	8/1/6+ - 8/6/69 HEL
			1. 15.5-10 205	0.0	2 20	TOPSDIL, P vinei.
ļ			2- 18-23 205 3- 23-26 455	1.J cored bea	3 1	SAND, s.117, some grave, about SN
			4+ 26+31 <b>506</b>	7 50 9	1. fent	35a fines, 2 8 .: ne ease, 158 mediu- dend, 105 course sand, 158 gravel,
0296			HOTE: Mater level at pipe frozen on 12/5/69,		•	angular, 1-inc' maximum sizu, groy,
F1	DH-205	ELEV. 90~.0			τ,	damp, low part watering, very sample, GLACEAL YILL.
			· · · · · · · · · · · · · · · · · · ·	10 U	27.5	BEDROCK, mice-schist, tap 6 :t.
	0.0	1.0	TOPSULL, root.at.			badly continered, rotten, signly fractured, fractures 2 to 3 instes
	1.0	5.0	SAND, gravel, silty, about 105 fines, - 20% fire sand, 35% medium sand, 20%			apart, dipping 70°.
			coarse sand, 15% gravel, sub-rounded, 1/2-inch maximum sise, brown, moist	27.5		Bottom e; hole.
:4			medium permembility, loose glacial			Standard Penetration Test
: <b>4</b>	• >	N	outwash, TERRACE DEPOLITS. SP-CEL			No. Deput B1./it. & Becover 1 0.0 - 1.: 2 100
	6.3	10.0	SAND, silty with gravel, about 25% ; fines, 25% fine sand, 15% medius dat ;			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
			sand, 20% cuarse sand, 20% gravel, angular,1/2-inch magimum sise, brown			بد، (ز ۵۰۵ - ۲۰۰۰ س
, ,			to grey, moist, low permeability, very danse, GLACIAL TILL.			Burn Came B. ca
	18.0	26.0				Rock Core R. 65 No. Dec 22. 1. 20.0 - 1.0 - 37
7. 7-0 <b>7</b>			BEIROCK - mica-schist - badly weathered - poor rucomery			2. 20.0 - 20.0 - 20.
	20.0		Bester of here.			3 2000 - 2510 05 4. 2560 - 2160 100
57 9 4 SH :	,		Standard Penetration Test			NOTE: Whier at 10.5 below
			Ho. Decth H1./1: SRecovery 1	-		RUTE: Milar at 10.5 Decon
			2. 1.5 - 3.0 80 100	<b>.</b>		
ered			3. 3.0 - 4.5 - 4. 90 4. 4.5 - 5.5 97/6" 50	<u>04-200</u>	<u> </u>	8/7/69 - 8/8/59 - <del>8</del> 2
ntal.			3. 10.0 -11.5 BO 100	J.J	1.0	TOPSOIL, PROVINGL.
			Ack Core Runs No. Depth <u>S Recovery</u> 1. 18-21' Jok	15	10.0	HAND, silvy, some gravel, about SH JUE rimes, 20% fine and, 10% medium
2			1. 18-21 308 2. 21-251 205			send, 256 coarse - va, 108 gravel, espaine, 4/2-inc. matural size,
			NOTE: Water level at 10,0' below			brown to grey, swist, low permutat-
			ground on 8/12/69			lity, dense, BLACIAL THL.
				13.0	17.0	BERNOCK, mace-script, ball: inclured 2 to 3 inches spart, most insciumes
	DH-200	ELEV. 589.1	7/31/69 - 8/1/69 Hal			dipping 7- , some norisenie.
	0.0	1.0	TUPSOIL, rootaat.	17.0	60.0	SCINCE, purstite, mostly felipper
	1.0 3 to L' cored boulder	19.0	CAND, slity, about 25% fines, 25%			and mice Slightly fractures, fractures 0 to 3 feet quart.
i/ <b>69.</b>	004 A987		coarse sand, 105 gravel, angular,	د.دما	•	Bottom of nois.
			1/2-inch maximum size, brown to figrey, moist, low permeability, very			Standard Penetration Test
			dense, QLACIAL TILL.			to. Lopus Bi./ft. S Recovery
•	19.0	•	REFUSAL, Bottom of hole.			1. 0.0 + 2. · · 3 202 2. 1.5 + 3. 0 · · · · · · · · · · · · · · · · · ·
AP00			Clanding Penetration Test			3. 3.0 = 4.01 00 0 4. 4.5 = 0.01 23 0
: <b>#</b>			Ko. Depth B1.//t. / Recovery			
<b>101.</b>			2.         1.5         3.0         1.0 <sup>6</sup> 1.00            3.         4.0         5.4         111         100			1
			4. 10.0 -11.5 158 100 .			
c taured			5. 15.0 -16.5 152 100 6. 18.0 -19.0 125/6" 50 ,		BRADLEY BROO	K WATER SHED PROJECT
80 <b>61</b>			MOTE: Water level at 10.0 below	}	BLACK BROOM	MULTIPLE-PURPOSE DAM
			ground on t/u/69.	ł	HAMPDEN C	OUNTY, MASSACHUSETTS
	IH-2064	B.SV. 895.7		ł	LOGS	OF TEST HOLES
9 <b>7</b>	u.o	1.0	TOPSOIL, rootmat	ت المحمد ا	IS DEDADTS	ENT OF ACRICUITURE
	1.0	11.5	SAME, gravel, silty, about 105 fines,		SOIL CONS	AENT OF AGRICULTURE
			10% files sand, 25% modium sand, 30% conres sand, 25% gravel, sub-angular,		SULL CONS	ENVATION SERVICE
hau c			1-inch maximum size, brown to gray,		D MILLS	12/ 6 4
•			damp, modium to low permanbility, dragt medium danas, diacital Till, ventioned		D N LONCZAK	12/60
			to 3.5'.			
						MA-3716
						F 28,
			-			R-14 NEW GLANDREE LAND
:			· · ·			$\smile$ $\cdot$ $\prime$

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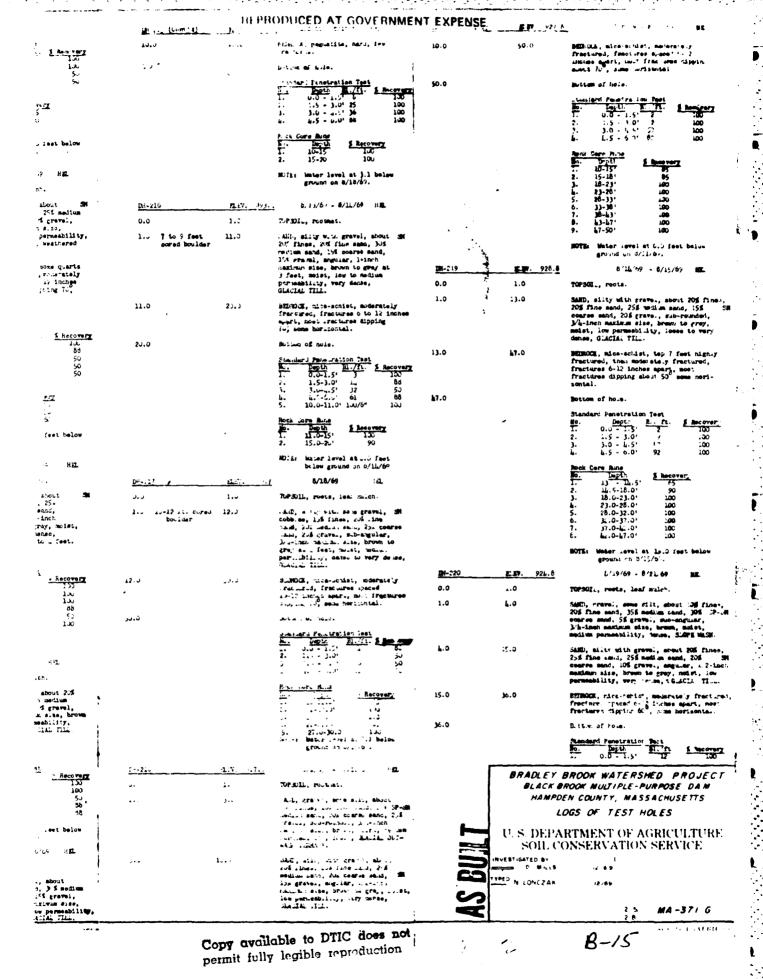
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Hof Constan	BLEV. DAY		1-211 (Gent) 42	2
-		Aure with Anne Ar Ling Lin & Accestery 1. 10.0 - 15.0 LSS		Prevident Personation fort
				1. 0.0 - 1.5 - 100
		2. 15.0 = 14.6 208 3. 19.0 = 23.0 008		2. 1.5 - 3.0' 5 1.00 3. 3.0 - 4.5' 67 50
		4. 23.0 - 20.0 1005 5. 26.0 - 31.0 1005		4. 4.5 - 5.5° 100/6° 50
		6. 31.0 - 36.0 95\$ 7. 36.0 - 38.0 1005		Bork Core Buse
		7. 30.0 - 30.0 100£ 7. 30.0 - 1.00. 100£		Nu. David. S Recovery
		HOTE: Maxim level at 8 feet bolds ground ou with 0 -		2. 20 + 201 90 3. 82 + 301 80
and the second s	En .2	≟ 8/18/69 - 8/19/69 MML		HDTS: When lovel of 6.6 feet below ground on 5/12/69.
0.0	1.0	TOPHOLL, roote, loaf m.lch.	•	·····
1	3.0	SANI, gravel, some allt, about	<u>194-212</u>	
		105 fines, 255 fine sand, 205 SP-EN ' medium said, 30% cuerse sand,	0.0 1.0	TOP 1011, roots, leaf mileh.
		155 gravel, sub-rounded, 1/4-inob	1.0 15.0	LAND, silly with gravel, shout
		nazirus eise, brown, moist, medium perveability, loose, GinCIAL OUTHACH	(8 to 10.5 bostors)	20% fines, 25% fine sand, 25% medium sand, 20% coarse sand, 10% gravel,
		TERRICE.	•	angular, 3/4-inch maximum size, brown to gray, moist, low permeability,
	1.J.J	AND, silty with gravel, about at 23. fines, 25% fine sand, 25% medium -		very dates, GLACIAL TILL, weathered in top 5 feet.
		sand, 20% coarse sand, 10% gravel,	-	
		angular, 1/2-inch maximum aise, brown to gray, moist low permeability,	15.0 28.0	BEEROCK, mice-schist with some quarts seems 3 to 6 inches thick moderately
		very dense, QLACIAL TILL (weathered)	-	iractured, Fractures 6 to 12 inches spart. Host fractures disping 70,
44.2	37	BEDHOCK - mice-schist, top 3 fest		sum herisontal.
		highly vestered, meanately fractured, fractures o to 12 inches	26.0	soutons of hole.
		apar., inschures dipping 70°.		Standard Penetration Test
<b>5</b>		Bottom of hole.	•	Ro. Depth B1./II. E Accovery I. 0.2 - 1.5' 4 100
		Stanuard Penetration Test		2. 1,5 - 3.0' 24 55
		No. Lepth E1./ft. <u>5 Recovery</u> 1. U.U = 1.5' 2 1005	•	3. 3.0 - 4.5 46 50 4. 4.5 - 6.3 84 50
		1. 1.5 - 3.0 <sup>1</sup> 9 1005 3. 3.0 - 4.5 <sup>1</sup> 66 605		2. 11.0 -12.5" 94 50
		4. 10.0 -11.5' 96 865		Acca Core Buns
		1. 25.0 - 26.0" 125/5" 885		No. Both & Recovery
		Both core Autor No. Deptr. <u>1 Recovery</u> 1. 10-17 95		2. 20-23* 50 3. 23-28* 60
		1. 16-17 <u>95</u> 2. 17-20 65		
		3. 20-25 95		NDTL: Mater level at 4.6 feet below ground on 8/23/69.
		4. 25-29 95 5. 2y+3 <b>8</b> 03		-
		J. 32-37 .J.	DH-213 B.EV. 8-1.4	8/11/65 - 8/15/69 HEL
	•	NOTE: Natur lavel at 3.1 below ground	0.0 1.0	TOPSCIL, roots, loaf milch.
		on 0/15/67.	1.0 7.5-9.5 cored 16.5	JLVE, silty with gravel, about 🕮
<u>3-2.</u>	ELEV. 916.7	8/8/69 - 8/11/69 Kg	boul der	25% fines, 20% fine send, 25% medium send, 15% source send,
	1.0	NFSULL, rootant.		1:1 gravel, angular, 1/2-inch
<b>4</b> • 0	17.;	SAUL, Filty with gravel, about 25%		pariment else, byown to gray, moist, lou permeshility, very dense,
•	,	lines, 30% fine sand, 30% medium - 300		GLACIAL TILL, weathered to & Seet.
		sain, 52 coarse sand, 15 gravel, angular, 1/7-inch maximus size,	16.5	Bottem of hole.
		brive to gray at 1 feet, note, low purneability, danse, REAJAL TILL,		taniate Prestration Inth
		Westnered in top 9 feet.		$\frac{1}{1} = \frac{1}{0.0 - 1} \frac{1}{10} = \frac{1}{2} \frac{1}{10} \frac{1}{10} = \frac{1}{10} \frac{1}{10} \frac{1}{10} = \frac{1}{10} \frac{1}{10} \frac{1}{10} \frac{1}{10} = \frac{1}{10} \frac{1}{1$
1.0	ن. در	Bullow, mica-schiat momentaly fractured		2. 1.5 - 3.0° 6 100 3. 3.0 - 4.5° 34 100
		Crattures spared o to 12 inches spart		
		horizonta.		- 10-0 -11-0* 29 50 ∧. 15:0 -16-5* 14 100
		botthe of hole.		W/TLI to water swatting.
		taking Penetration Test		
		h. Depts Harrit. A Recovery	DH-214 MLEV. 57	./15/69 = 8/18/69 Has.
		2. 2.5 - 3.5 - 32 - 2.5 - 5	0.0 1.0	TUPSDIL, roots, losf mish.
		3. 3.0 - 4.1 by 53 58 4.1 4.5 - 5.4 110 of marken 1.0		.ARL, ally with gravel, about 205
		4. 10.5 +10.07 120 100 6. 10.0 +10.7 170 5.	1.0 11.5	fines, 255 fine semi, 255 medium 👘
				sand. 246 course sand, 136 gravel, arguiar, 3/4-1000 maximum sise, brown
		Roce Gore Runs		- gruy, mulat, low permembility, conce to very dense, discipal TILL.
		$\begin{array}{cccccccccccccccccccccccccccccccccccc$		weathered to & feet,
		3. 22.5 - 27.5 40 	11.5	Stilms of hulo.
		Muite among level at 1 (At be) w		Landard Penetration Test
		erowand or 5.1.16+,		S. Leput. H., Tt. S Accover T. 0.5 - 1.5' 5 100
3	ELK	u/12/o - s/11/69 Sta		2. <b>i.</b> = 3. 1 10 <b>i</b> €0
•••	1.0	ToPAIL, month, etc.		3. 3.0 - 4.1°/ 3- 50. u. u.S. 6.01 70 56
• •	17.2	LANL, s.ltr, som gravel, about 205 🛛 🗰		5. 10.0 -11. <sup>64</sup> 118 98 1
		Lines, 5.5 line sand, 3.7. medium manu, . 1 6 coarse sand, 10% erav 1, argular,		Will unter level at in , foot below
		Warthe maximum size, brown to gray		ground on 3, 14/64.
		at u.4 feet, wet, medium permeability, 100se, 3LACIAL TILL.	<u>E41-215</u> ELEY. 12-14	8/15/69 - 5/14/69 HEL
• ••	3010	Bills . Bica-schist, moderately free -	0.0 1	TOPHOIL, Poots.
		THEFT, TRACHARDS STATE	1 13	AND, silty, with gravel, about
		a, and, must inactained disping 7.	,	155 fines, 205 fire send, 315 medium sani, 200 coarse sand, 155 gravel.
		notion of hole.		sub-rounded, Mu-inch maximum size, brown to gray, moist, low personality,
				dense to very solet, low persentity,

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Direity     Diffy:     (-3):       1.00     1.00       2     (     1.00       2     (     1.00       2     (     1.00       2     (     1.00       2     (     1.00       2     (     1.00       2     (     1.00        3.01     1.00        3.01     1.00        3.01     1.00        3.01     1.00	RUPSOIL, route. AND, silty with gravel, about 205 is which are send, 25% modium SN send, 20% coarse send, 10% gravel, angular, Nu-inch matrixm sites, haven to gray, moist, low perseability, dense, to wary dense, GLACIAL TILL. Matter Person 100 perseability, dense, to wary dense, GLACIAL TILL. Matter Person 100 perseability, dense, to wary dense, GLACIAL TILL. Matter Person 100 person to the send of the send of the send to the send of the send of the send to the send of the send of the send to the send of the send of the send of the send to the send of the send of the send of the send of the send NOTE: Matter level not recorded.	87-0       10.0       MMDULE, miss-setters, marg.         80-0       Buttom of turbs.         Promoters       Promoters       Promoters         1.0       0.0       -1.51       0.1         1.0       0.0       -1.51       0.1       100         1.0       0.0       -1.51       0.1       100         1.0       0.0       -1.51       0.1       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       -1.51       0.0       0.0         1.0       0.0       0.0       0.0       0.0         1.0       0.0       0.0       0.0       0.0         1.0       0.0       0.0       0.0       0.0         1.0       0.0       0.0       0.0       0.0         1.0       0.0       <	0.0 9.0 9.152 0.0 1.0 8.0 1.0 8.0 8.0 1.0 8.0 0.0 1.0
. L.u 	L.       L.       L./Li.       L. Monthmark         1       1       1       17       86         1       1       17       86         1       1       17       86         1       1       10       17       86         1       1       10       10       10         1       1       1       90       100         Rece. were Ring       L. Bacovart       100       10         1       1       1       100       100         1       1       1       100       100         1       1       1       100       100         1       1       1       100       11         1       1       1       100       11         1       1       1.00       11       100         1       1       1       1       100         1       1       1       100       11         1       1       1       100       1         1       1       1       1       100 <th>Plandari Prostivi Proti       Processing         1       0.0 - 1.5       100         3. 3.9 - 6.5       70       80         4. 6.00 - 7.5       100       80         5. 7.6 - 8.0       35       50         6. 10.0 - 21.5       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         8. 20.0 - 21.5       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100      <t< th=""><th>22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0</th></t<></th>	Plandari Prostivi Proti       Processing         1       0.0 - 1.5       100         3. 3.9 - 6.5       70       80         4. 6.00 - 7.5       100       80         5. 7.6 - 8.0       35       50         6. 10.0 - 21.5       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         7. 15.0 - 15.2       100       100         8. 20.0 - 21.5       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 15.0 - 15.2       100       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100         1. 200       1.5       100 <t< th=""><th>22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0</th></t<>	22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0
. L.u 	2 1 3.0. 17 86 3. 3.0 - 3.7. 50 100 3. 3.0 - 3.7. 50 100 4 $a_{11} = 5.7. 106/6^{4}$ 50 5 $1000 = 31.0^{4}$ 98 100 <b>Recevers Amme</b> <b>Recevers Am</b>	Back Core Ruge       Smacrowski         2.       1.0       -1.5       100         3.       3.0       -1.5       100         3.       3.0       -1.5       100         3.       3.0       -1.5       100         3.       3.0       -1.5       100         3.       -1.5       -1.5       100         3.       -1.5       -2.5       100         7.       -2.5       -2.5       100         7.       -3.5       -2.5       100         7.       -3.5       -2.5       100         7.       -2.5       -2.5       100         7.       -2.5       -2.5       100         7.       -2.5       -2.5       100         1       -20       -2.5       100         2       -20       -2.5       100         3       -35       -35       -5.5         1       -20       -2.5       5         2       -20       -2.5       50         2       -2.5       -3.5       55         1       -2.5       -3.5       50         2       -	22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0
. L.u . L.u 7.0 2 	) $j_{10} = a_{11}^{1/2}$ 50 100 $a_{11} = a_{12}^{1/2}$ 106/6* 50 $a_{12} = a_{12}^{1/2}$ 106 <b>Rece were Rung</b> <b>No.</b> Easily 20 100 <b>Rece were Rung</b> <b>No.</b> Easily 20 <b>Constant</b> $a_{11} = a_{12}^{1/2}$ 100 <b>ROTE: Mater level not recorded.</b> 2 $b_{1/06}$ HEL <b>TOPSOLL, rotts.</b> AUL, silty vit, gravel, about 205 10 were 25 fine and, 25% modium SH sand, 20% coarse and, 10% gravel, angular Muriach matimum size, brown to gray, moist, low persephility, dames, to wary dames, CLAILE THL. Rettor of hole: <b>Lide.Ler. Perstruct 10.</b> Thet <b>Lide.Ler. Perstruct 10.</b> The <b>Lide.Ler. Perstruct 10.</b> The <b>Lide.Ler. Perstruct 10.</b> The <b>Lide.Ler. Perstruct 10.</b> The <b>Lide.Ler. Perstruct 10.</b> The second set. <b>Lide.Ler. 10.</b> Silt, mice-schist, about <b>Lide.Ler. Perstruct 10.</b> The second set. <b>Lide.Ler. 10.</b> Silt, mice-schist, about <b>Lide.Ler. 10.</b> Silt, silt. Mice-schist, about <b>Lide.Ler. 10.</b> Silt, silt. Mice-schist, about <b>Lide.Ler. 10.</b> Silt, silt. <b>Lide.Ter.</b> <b>AUD.</b> Silt, some gravel, about 25t fines, <b>Lid.Ler. Silt. Struct 10.</b> Silt. <b>Lide.Ler. 10.</b> Silt. Silt. Silt. Silt. <b>Lide.Ler. 10.</b> Silt. Silt. Silt. Silt. <b>Lide.Ler. 10.</b> Silt. Silt. Silt. Silt. Silt. <b>Lide.Ler. 10.</b> Silt. Silt. Silt. Silt. Silt. <b>Lide.Ler. 10.</b> Silt.	2.       1.5 - 3.40°       36       100         3.       3.5 - 1.5 - 70       80       80         4.       6.0 - 7.5 + 43       80         5.       7.5 - 9.0 - 335       50         6.       3.1.0 - 1.2 : 51       100         7.       3.5 - 3.5 : 200       200         7.       3.5 - 3.5 : 200       200         7.       3.5 - 3.5 : 200       200         7.       3.5 : 3.5 : 200       200         7.       3.5 : 30       100         Permendentilisty Perce         1.       200       3.5 : 50         3.       15'       3.5 : 50         3.       15'       3.5 : 50         3.       15'       3.5 : 50         3.       3.5 : 400       30         3.       3.5 : 400       30         3.       3.5 : 400       35         Perckar Tonta         1.       21:-7 = 40.70         3.5 : 400       3.5          5.5          5.5          5.5          5.5          5.5	22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0
. L.u . L.u 7.0 2 	$\frac{10.0-11.0}{10}  y_{0}  100$ Rect with Rung $\frac{1}{10}  \frac{1}{10}  \frac{1}{10}  \frac{1}{10}  \frac{1}{10}$ $\frac{1}{10}  \frac{1}{10}  \frac{1}{10}  \frac{1}{10}  \frac{1}{10}$ $\frac{1}{10}  \frac{1}{10}  \frac{1}{$	3.       3.3 - 3.5 - 1.5 - 70       80         1.       6.0 - 7.5 + 8.0       30       50         5.       7.5 - 8.0       30       50         6.       20.0 - 22.5 : 207/2*       0       100         Permedbility Parts         1.       1.5 : 20.0 : 25.2 : 127/2*       0         2.       10°       4*       5.4 : 200         2.       10°       4*       5.4 : 200         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       15'       3*       5.5 : 50         3.       3.5 : 40       55'         3.5 : 40       55'         3.5 : 40       55'         3.5 : 40       55'         3.5 : 40       55'         3.5 : 40       55'         3.5 : 40       55'         3.5 : 40'       55'         3.5 : 40'       5'	22-152 0.0 0.0 0.0 1.0 8.0 72-151 0.0
. L.u 	Description       2 Anson versus         1       10         2       17         2       17         2       17         2       17         2       17         2       17         2       2         3       22         2       2         MOTE:       Mator level not recorded.         2       5'/00         MOTE:       Mator level not recorded.         2       5'/00         MUL, silty with gravel, about 20%         13       2.5 fine end, 25% motion         angular, Murick maximum gise, brown         to gray, moint, low pressbility, dense,         to yary dones, CLAILI THL.         Matter of hole.         Liter.ar. Penetration Test         5	5.       7.6 - 9.0 - 136       50         6.       11.0 - 12.5*       100         7.       15.0 - 15.2*       107/2*       0         8.       20.0 - 21.5*       90       100         Presentility Parts         1.       5       100         2.       10°       4*       5.4       100         1.       5       100       1.00       1.00         2.       10°       4*       5.4       1.00         3.       15'       3*       5.5       1.00         1.       15'       3*       5.5       1.00         3.       15'       3*       5.5       1.00         1.       2.7       50'       3'       1.00         1.       2.7       50'       55       1.00         2.       30 - 55'       95       3.35 - 40       95         1.       2.1.       2.1.       1.00       5       1.00         1.       2.1.       2.1.       1.0       35       1.00         1.       2.1.       2.1.       1.0       1.0       1.0       1.0         1.       2.1.       2.1.       <	<b>8.0</b> <b>37-153</b> 0.0 1.0 <b>8.0</b> <b>77-154</b> 0.0
. L.u 	2. $17 - 22^{-1}$ 100 3. $22 - 20^{-1}$ 100 HOTE: Mater level not resorded. 2. $5^{-1}/0^{-1}$ HE. TUPSUL, rute. AUL, silty with gravel, about 20% 51 - 7. 25 fine and, 25% modium SH angular, Mu-inch maximum give, brown to gray, molet, low persobility, dense, to yray dense, CLAIMI THL. Mather dense, Mather dense, 26 for the dense, Mather dense, 26 for the dense dense dense dense dense. AND, gravel, will mather dense dense dense. the dense, VALLY MILLY dense to the dense dense, VALLY MILLY MAX. CAND, silty, some gravel, about 25t fines, the formed dense dense dense dense dense dense dense dense. CAND, silty, some gravel, about 25t fines, the formed dense	7.       15.0 - 15.2 *       100         9.       20.0 - 21.5 *       90       100         9.       20.0 - 21.5 *       90       100         9.       20.0 - 21.5 *       90       100         9.       20.0 - 21.5 *       90       100         9.       101       101       101       100         9.       100       100       100       100         1.       101       101       101       100       100         1.       101       101       101       101       100       100         1.       101       101       100       100       100       100         1.       101       100       101       100       100       401         1.       101       100       Neuron       101       100       100	<b>8.0</b> <b>37-153</b> 0.0 1.0 <b>8.0</b> <b>77-154</b> 0.0
. L.u 	). $22 - 26$ 100 NOTE: Mater level not recorded. 2 $5^{\prime}/66$ HE TOPSDIL, rote. AUD, slity with gravel, about 20% is = 0.25 fine each, 25% median SH such 20% coarse sand, 10% gravel, angular Mu-inch matrixm size, brown to gray, noist, low persechility, dense, to vary dense, GALIAL THL. Better of hole. <u>104.147. Penetration Test</u> <u>105.167.157.100</u> <u>100</u> 3.32.57.25 for 100 3.32.57.25 for 100 1.1.5.10.100 3.32.57.25 for 100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.10.100 1.1.5.1000 1.1.5.1000 1.1.5.1000 1.1.5.1000 1.1.5.	Permenentility Parts         1	<b>8.0</b> <b>37-153</b> 0.0 1.0 <b>8.0</b> <b>77-154</b> 0.0
- 2.J ( to 7.3 2.a.) cored bder) 	$\frac{b'_{1.2}/c_{2}}{B} \qquad HE  FUPSDLL, route. AUL, silty with gravel, about 20% is +1.25 fine eard, 25% modian SM and, 20% coarse sand, 10% gravel, angular, Mu-inch matimum size, haven to gray, moist, low perseability, dense, to vary dense, (EATIAL TILL. Bettor of hole.                   $	Image         Image         Image         Image           2.         101         4*         5.3         Image           3.         15'         3*         5.5         Image           3.         100         3*         5.5         Image           3.         10'         3*         30'         30'         30'           3.         3.5         40'         35'         Image         Image           1.         21'         30'         35'         Image         Image           1.         21'         10''''''''''''''''''''''''''''''''''''	۵.0 <b>37-153</b> 0.0 1.0 <b>8</b> .0 <b>77-154</b> 0.0
- 2.J ( to 7.3 2.a.) cored bder) 	RUPSDIL, rowis.AUL, silty with gravel, about 20%is = 25% fine each, 25% modiansandiar, 25% coarse each, 10% gravel,sandiar, Wu-inch mairium size, havento gray, moist, low perseability, dense,to wary dense, GANIAL TIL.Matter of hole.Size.Lar. Penetration Test $h_{-}$ <	2.       10 <sup>1</sup> k <sup>+</sup> 5.4       regr         3.       15 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         4.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         5.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         5.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         1.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         2.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         1.       20 <sup>1</sup> 3 <sup>2</sup> 5.5       hem         2.       20 <sup>2</sup> 3 <sup>2</sup> 5.5       55         2.       30 <sup>2</sup> 3.5       55       55         Pecker Tests       5.1       5.5       hem         1.       21 <sup>2</sup> 10 <sup>2</sup> 3.5       hem         BOTE       hater Loral at ground Loral on 4/6/66       hem       100 4.5         BOTE       hater Loral at ground Loral on 4/6/66       hem       101 4.5         1.       9 <sup>1</sup> Stream channet       401 4.5 <sup>1</sup> 1.       9 <sup>1</sup> Stream channet       401 4.5 <sup>1</sup>	8.0 <u>79-153</u> 0.0 1.0 8.0 <u>79-154</u> 0.0
. ( w 7.0 244). corea bder)       	All, silty with gravel, about 20% is $r^{-2}$ . 25% fine each, 25% modium SN sand, 20% coarse each, 10% gravel, angular, Mu-inch mains sites, haven to gray, moist, low perseability, dense, to wary dense, GALIAI TIL. Better of hole. <u>Site Let Penetration Test</u> <u>A. 2010</u> , <u>B. /It</u> <u>i Recovery</u> <u>I. 1.5 - 1.5' 2 100</u> <u>I. 1.5 - 1.5' 2 100</u> <u>J. 1.5' - 1.5' 5 50</u> <u>. 2010</u> , <u>1.5' 5 50</u> <u>. 2010</u> , <u>1.5' 6 50</u> <u>. 2010</u> , <u>1.5' 5 50</u> <u>. 2010</u> , <u>1.5' 72 50</u> NOTE: Water level not recorded. <u>D. 1' 10.5' 100</u> <u>Note: Water level not recorded.</u> <u>TOP.011</u> , roournt. <u>AND</u> , gravel, milt, mica-schist, about <u>10% (J. 1.5' 6.5) sectium SP-SN</u> cand, 30% coarse sanz, 25% gravel, mub-rounded, <u>Mu-icc</u> maximum site, hrown, moist, white perseability, dense to ver, dense, VALLY ALUY TUN. <u>CANU</u> , silty, some gravel, about 25% fines, <u> fine sand</u> , <u> solut</u> spirability.	1.       15'       3'       5.5       home         1.       20'       3'       5.5       home         5.       20'       3'       5.5       home         1.       20'       3'       5.5       home         1.       20'       3'       5.5       home         1.       20'       3'       5'       5'         1.       20'       3'       5'       5'         1.       20'       3'       5'       5'         2.       3'       3'       5'       5'         2.       3'       3'       5'       5'         3.       3'       4''       5''       5''         1.       22''       3'''       5''''''       5''''''''''''''''''''''''''''''''''''	<u>27-153</u> 0.0 1.0 8.0 <u>77-154</u> 0.0
( u fr. cored bder)       	13 -*. 255 fine send, 255 mediam SH and, 205 coarse and, 105 greesi, angular, Mu-inch maximum gise, brown to gray, moist, low persephility, dense, to wary dose, GLAIMI THL. Action of hole. <u>itsular. Penetration Test</u> <u>b. 100 and States</u> <u>itsular. Penetration Test</u> <u>itsular. Penetration Test</u> <u>itsular. 100 and States</u> <u>itsular. 100 and States</u> <u>itsular. 100 and States</u> <u>itsular. 100 and States</u> <b>NOTL: Mater level not recorded</b> . <u>105 (Dires, 105 fine each; 255 gravel, shout 105 (Dires, 101 fine each; 255 fines,, sine each, 0.55 median SP-SH cands, Silty, some gravel, about 255 fines,, sine each; conservel, angular, 1/7-insch cantist, site, gravel, moist, penetability, dense to ver, dense, Vally Ally Fally Filly Silty, some gravel, apout 255 fines,, sine each; conservel, angular, 1/7-insch cantist, site, gravel, moist, penetability, dense to ver, dense, vally fill filly fill</u>	L.       20'       3"       5.5       Nome         South State       South State       South State       South State       South State         Back Core Runge       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State       South State       South State       South State         South State       South State	<u>27-153</u> 0.0 1.0 8.0 <u>77-154</u> 0.0
- <u>. ELFY</u>	<pre>send, 20% coarse sand, 10% grees!, angular, Mu-inch maximum sites, herem to gray, moist, low permeability, danse, to wary danse, CLAIMI THL. Maximum site, CLAIMI THL. Maximum site, CLAIMI THL. Maximum site, State State in the same site state same site same in the same site same same site same site same in the same same site same site same site same same site same same site same site same site same same site same same site same site same site same same same same same site same site same site same site same same site same same site same same site same same same same same same same sam</pre>	Back Core Russ         S Process           1         21         20         50           2         30         35         55           3         35         40         55           Packar Tents         F.1         50         55           1         21         50         55           Packar Tents         F.1         50         55           BOTEs         No.or 2010         55         50           BOTEs         No.or 2010         101         101         101           1         94         Stream channel: 401         45%           Portice         101         199         Retering in 501         595	<u>27-153</u> 0.0 1.0 8.0 <u>77-154</u> 0.0
3.; 1019 . 32.J	to gray, moist, low perseability, dense, to vary dense, GLAIAI TILL. Exton of hole.	Image: 1	<u>27-153</u> 0.0 1.0 8.0 <u>77-154</u> 0.0
3.; .· 1015 . 32.J	Exiten of hole. $\frac{5142.1427. Penetration Test}{5$	2. 30 - 35 3. 35 - 40 95 Packar Tents 1. 20.5 Jo 55 Both BOTEs Notor Level at ground Level on 8/6/66 BOTEs Notor Level at ground Level on 8/6/66 10/16 10/16 10/	0.0 1.0 8.0 <u>77-154</u> 0.0
3.; .· 1015 . 32.J	List Lar.         Penetration Test           h.         Logits         B./ft         1 Recovery           1         1.0         1.0         1.0           3         1.0         1.00         1.00           3         1.0         1.00         1.00           3         1.0         1.00         1.00	Packar Tents       Full       Full       Full         1:       22:::=       0:0.0.55       Bome         BOTE:       Nator Level at ground Level on &/6/66         TES:       Nator Level on &/6/66	0.0 1.0 8.0 <u>77-154</u> 0.0
3.; .· 1015 . 32.J	h         Desite         D./ft         i Accovery           1         1.5'         100         100           3         1.5'         20         100           3         1.5'         20         50            1.5'         20         50            1.5'         20         50            1.5'         3         100           1         1.5'         3         100           1         1.5'         3         100           7.         20.0         -21.5'         72         50           MOTH< Mater level not recorded.	TEAT HOLE NUMBERING SYSTEM Lenter 1000 Street at ground Level on AVE/55 TEAT HOLE NUMBERING SYSTEM Lentering of dam 1 94 Street news 501 45% Praticulare 101 199 Reter news 501 555	0.0 1.0 8.0 <u>77-154</u> 0.0
ريو د. درمان . يورون	<ul> <li>1.5 - 3.0' 8 100</li> <li>3</li></ul>	1. 27.5 - 60.0 35 Home HOTER National as ground Loval on 6/6/69.  TESTING ENUMBERING System Lentering of dam 1. 94 Stream channel 401 494 Portugues 101 199 Retering to 501 599	2.0 8.0 <u>77-154</u> 0.0
رید در این ۱۹۹۶ ، ۱۹۹۶ .		TENT KOLE NUMBERING SYSTEM Lementing of dam 1. 94. Stream channel: 401.494 Portice area 101.199. Reter wers 501.599	8.0 <u>77-154</u> 0.0
رید در این ۱۹۹۶ ، ۱۹۹۶ .	<ul> <li>1110.51 Ji. 100</li> <li>7. 20.0 -21.51 Ji. 100</li> <li>7. 20.0 -21.51 72 50</li> <li>NOTL: Mater Level not recorded.</li> <li>7/31/07 - 0/4/69 HEL</li> <li>TOP.01L, rootmat.</li> <li>AND, gravel, silt, mice-schist, about 105 firms, 201 firms sand, 205 medium SP-SW cande, 30% corder sam., 25% gravel, mub-rowindow Mutart. maximum site, herown, soist, weitus partsellity, dense to ver, dense, Valley Ally TUN.</li> <li>CAND, Silty, sone gravel, angular, 1/7-ised course samd, 10% gravel, mutart, 15% firms, coist, gravel, soist 25% fines, curves and, 10% gravel, angular, 1/7-ised course samd, 10% gravel, angular, 1/7-ised course samd, log gravel, angular, 1/7-ised</li> </ul>	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	<u>₽-154</u> 0.0
رید در این ۱۹۹۶ ، ۱۹۹۶ .	NOTH Mater level not recorded. (1) 7/31/07 - 0/1/69 HEL TOP.OLL, rootnat. AND, gravel, slit, mice-achist, about 105 films, 104 films sant, 255 medium SP-SW cand, 305 coarse sant, 255 gravel, sub-rounded, Mu-inct maximum size, brown, moist, wellum permeability, dense to ver, dense, ValLEY all/WTUM. CAN, slity, some gravel, about 255 filmes, films sand, baneutm sand, 205 SH coarse sand, 1.5 gravel, angular, 1/7-ineh cantal a size, grav, moist, low permeability,	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	<u>₽-154</u> 0.0
رید در این ۱۹۹۶ ، ۱۹۹۶ .	1/31/07 - 6/4/69 HEL TOP.011, rootnet. 	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	<u>₽-154</u> 0.0
رید در این ۱۹۹۶ ، ۱۹۹۶ .	TOP.011, rootnet. AMD, gravel, silt, mice-schist, about LUS (Lies, 201 fine sani, 25% medium SP-BH cand, 30% coarse san., 25% gravel, sub-rounded, Mu-iact. maximum sile, brown, solist, wellum partneability, dense to ver, dense, ValLEY ALLUYTUM. CANU, Silty, some gravel, about 25% fines, fine sand, angular, 1/7-ised cuarse sand, 1.5 gravel, angular, 1/7-ised cuarse sand, 1.5 gravel, angular, 1/7-ised	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	<u>₽-154</u> 0.0
۰۰۰ نامه د. ۲	AND, gravel, silt, aica-achist, about LUS (Lnes, LUI (Ins sani, 205 medium SP-SM cand, 30% coarse san., 205 gravel, sub-runied, Mu-iact. maximum sis, brown, soist, wellus parteability, dense to ver, dense, ValLEY ALLUYUM. CAND, Silty, sone gravel, about 255 fines, . 5 fine sand, .0% medium sand, 208 SM cuarse sand, L0% gravel, angular, 1/7-isem calls, silts, grav, solet, low permeability,	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	0.0
. 32.J <sup>°</sup>	135 Lines, 135 Line sent, 255 medium SP-BW cand, 335 course sand, 255 gravel, sub-rownled, Mu-iact maximum size, brown, moist, writes partneshility, dense to ver, dense, VaLLSY ALLUVTUM. (AND, Silty, sone gravel, about 255 fines,, 5 fine sand, 136 medium sand, 235 fines,, 5 fine sand, 136 gravel, angular, 17-imem rantin, size, grav, solet, low permeability.	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	0.0
. 32.3	<pre>sub-rounded, Musicat maximum size, brown, motet, weitum permeability, dense to ver, dense, VALDY SUDVING. UAND, silty, some gravel, about 255 fines, U.S fine sand, U.S medium sand, 205 SH course sand, U.S gravel, angular, 1/2-inch routing size, gray, moles, low permeability.</pre>	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	
. 32.3	<pre>ver, dense, VallEY AlliVTUR. (AND, Silly, some gravel, about 255 fines, (.+ fine eard, 10% mealum eard, 208 SH cuarse eard, los gravel, angular, 1/2-inch rattar size, gray, solet, low permeability,</pre>	Lenferline of dam 1. 9%. Stream channes: 401. 49%. Printiw area 101. 199. Reter weis, 501. 599.	1.0
. 32.3		Relation area 101 199 Relief mells 501 599	
العهم ا	cuarse saud, lui gravel, angular, 1/2-inch maximum size, gray, moist, low permeability,	, t. unigency spiritually 201, 299 601, 699	
	WERV JEDAN, (RATE: TV:	enterime of outlet structure 301 399 701 799	
الافضيف الم	and a second provide the second s	UNIFIED SOIL CLASSIFICATION SYSTEM SYMBOLS	
	BiBOE, mice-schist, weathered in top	GW Well graded gravels, gravel sand misturas	12.0
	Both of hole.	GP Ponthy graded gravels GM Stity gravels gravel sand silt mintures	
	isindar. Peretration Test	GC Clavey gravets, gravet sand clay mistures SW Well graded sands, sand gravet mistures	<b>IP-155</b>
	A LOUIS BALLAN ARCOVERY	SP Poorly graded sands M Sits sand	0.0
	2	SC Clayey sands, sand clay mistures	1.3
	L	ML Sitts with liquid limit of 50 or less MH Sitts with insued limit above 50	
	لىكى 10.1 - 10.1 دىرى مەر	CL Clays with legand lense of 50 or less CH Clays with legand lense source 50	
	Per tab if Talis Loss ar Repth Mile its N Loss ar Rose	Critical Constraints and the second s	
	ar Nose 2 ar Idey	com - congarine solts and crays to reliable him fields of NU	12.0
	alight. Or Nous		
	- P - Der Honw - 2 - E Der Hone		17-156
	Or Thu		0.0
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	Without the second of 5/5/6 a	17 a	<b>T</b> 7
in	t <b>−</b> α ο δ + − <u>−</u>	Permit and the control of the contro	0.0
	WP.016, C. Jost	<u>,                                    </u>	1.5
· ···	AND, grave, sume allt, about of fines, and line sand, 3.6 maint sand, 2.5 coarse	<u>వ</u> ్తి	
	sad, d'é grave, seb-ruinded, l-inch iP-SH action 0.5 s, brown, wet, medium to high	7	
	hamlaab	63	1.0
• •	cancy warely note gravely about 15% fines, 198 June saudy 15% mentan sandy 15% coarse		1,.0

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HEPRODUCTO AT COVERNMENT EXPENSE - 12 .21. 0. 1-25 11. LV. 1.1.1 12/1/65 H. TT-151 S.F. 11 E. SDPSDL remarked, and, aller, about 205 fines, 405 fine and, 115 medium and, 155 searce ease, 206 grave, sul-angular, 12-insh maximum bis, alive, demp, 200 permeability, demos GLACIA, TELL, slout 205 plus 6-inst. inst. P##11. ... υ.υ ۵.۵ 9.0 1.0 1 .... ...... **10 e**. 100 100 88 86 50 100 0 100 .... 1 9.0 Autom of pit. 14.0 r• 🗭 temple 159.2 - 3 feet to ly seet 12/1/69 H KL R.W. 14.5 F-1W 12/1/69 X 17-152 E.SV. 891.6 1.U TUP SOIL. 0.0 1.0 TOP SOIL. 0.01 L Loss AALD, rill, with gravel, shoul 205 iind, u.S. Live sawi, 200 medium rani, JR 15 Lores sawi, 155 pravel, euh-servier, u-righ maimum size, size, asyo, asyo, lee pursesh.it, unter, ALACEAL TILL, she t 155 plus 6-iver size. datD, elity, about 3.5 (ince, idd fine eand, 15% medium eard, 15% eearse send, 10% gravel, sub-angular 15-ince marinam size, red-brown to elive at 3 feat, damy, lou person-bility, dense, dialattil Til, mout 15% plue 6-imch eise. 13.0 1.0 8.0 1.0 a very 5 home Mctton of pit 13.0 MORACIL. 5.0 No Sample. No Sample. R.W. rivey :2/./04 d 🖬 🗸 77-162 B.W. 179.8 12/1/69 н£. 17-153 1.5 107-1011. J.J SAMD, silty with grave, about 27. fire, uS live said, 205 conjectant, SM 105 coarse pand, 10 gravel, sub-scriet, in-inco marine suce, cite, and p, ice perceptity, dense, GLATAI TILL, abo 155 plus court ite. 1.0 TOP SOIL. 0.3 1.5 13.0 SAMD, silty, about 205 fines, 405 fine wand, 155 medium sand, 155 coarse 1.0 **b.**0 31 01 2/6/65 SABD, silt, about VN ince, dD fine and, 158 medium sand, 158 ocarse sand, 108 gravel, sub-angular, 26-inch maximum siss, red-brown to olive at SM 3 feet, damp, leu persability, damae, Olicial Till, about 158 plus 6-imm hotton of pit. 13.0 ..... comple 161.1 -- 3 feat to .3 fuet 8.0 NUMBER OF Sample 153.1 -- 3 feet to 0 feet. MOTHE Samplas above 3 feet are not Lasan beckupe of Japanese Beetle guarantire. 12/1/69 X2. ELEV. 679.2 1-15 0.0 1.0 TOPSOTL. SAND, silty, shout 20% fines, 40% fine and, 15% medium sand, 15% course sand, 10% graval, sub-megular, 20-imen & mariaum size, rad-brown to slive at 3 feet, damp, lev permashility, dense, GLACIAL THL, about 12% plus 6-imeh COMPACTION CURVES STANDARD PROCTORS 12.0 1.0 49 121 594 121 594 12 694 12 794 SM SAMPLE FROM TP 156. 3' TO 12' 130 1 .1... ÷. 125 -Bottom of pit. DAY DENSITY 12.0 K NO . 2 120-No Semple. 5 TP-155 BLEV. Jug.8 12/1/69 H.B. 115 1.0 TOP-JOIL. 0.0 110-SAUD, silty with gravel and cobbins, about 20% fines, 40% fine send, 20% and angular, 18-insh maximum sits, olive, damp, 180 paramebility, dense, OlaCIAL TILL, about 10% pius 6-inch size. . ---4.3 12.0 į 502 B 10 12 14 16 18 20 MOISTURE CONTENT, PER CENT OF DRY WEIGHT Bottom of pit. 12.0 SM SAMPLE FROM TP 161, 3' TO 13' Sample 155.1 -- 3 feet to 12 feet. 135 -(Q. 130 -17-156 ELEV 874.7 12/1/69 HEL St. Carion 0.0 1.0 TOPSOIL. :25 NC: Stars' SAMD, silty, with gravel and sobbles, about 2% lines, 40% fins send, 20% - 30 Redux each, 10% serves seni, 10% gravel, a.gu.ar, lu-inch maximum siss, olive, darp, lew personabilit, sense, olixe, III., about 15% plus 6-inch size. \* 1.0 12.0 120 ł ...**Š** 3 õ ,15. Bottom of pit. 12.0 B IC IZ 4 16 18 NOISTURE CONTENT, PERCENT OF DRI WE GM No somple. BRADLEY BROOK WATERSHED PROJECT TP- ... 12/1/65 REL BLACK BROOK MULTIPLE-PURPOSE DAM HAMPDEN COUNTY, MASSACHUSETTS د. ب 1.0 TUP.DIL. LOGS OF TEST HOLES SAND, siley with gravel, about 20% fines, and fine sand, 20% gravel, argular, low fourse sense, 10% gravel, argular, iowinth machana sise, siles, asay, iow permeability, demes, MACIAL TILL, about 15%, plus 6-inch size. 13.0 1.00 U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE NVESTIGATED BY 12/88 13.0 Botton of pit. TYPED N LONCZAR Sample 1571 - 3 feet to 12 feet 2/69 R MA - 371 6 -16 8 STATISTICS PROFESSION

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# APPENDIX C

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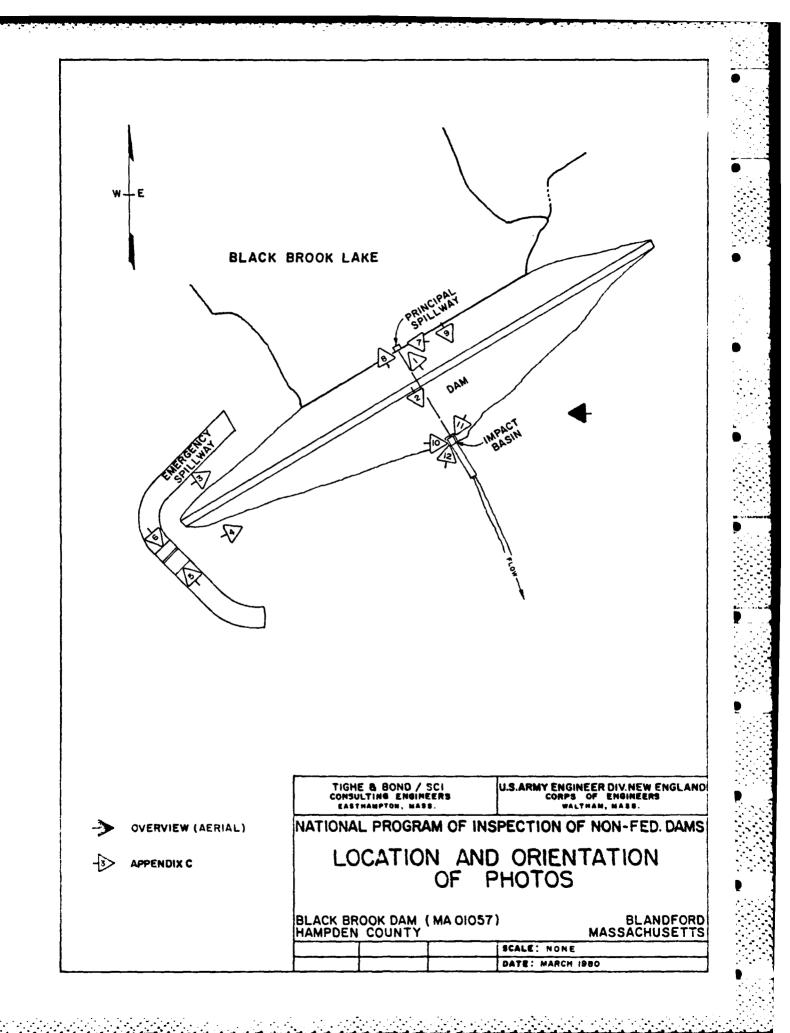
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## PHOTOGRAPHS

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#### Photo 1

Overview of impoundment and principle spillway



#### Photo 2

# Overview of impact basin and downstream channel

#### 796 <u>L. 3</u>

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electicy of updican selections of dam from expression channel of pressioner suilly on eight wide of dam



>>> End of downstroop Endroms of dom com >>>>> contemponey spill->>>> training wall







#### Photo 5

Overvise of sepress channel of emergency spillway from dischase channel

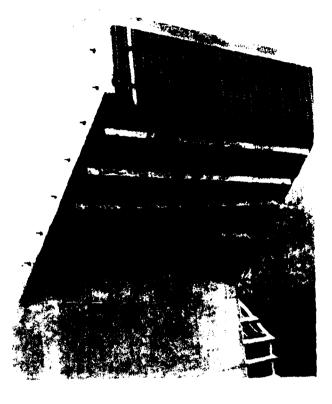


#### Photo 6

Overview of discharge channel of emergency spillway looking downstream from a point just below crest of spillway

#### Photo 7

View of left side or principle spillway. Note trash rack damage and missing bar.



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icw of silt that has washed of from under ribrap on upless embankment at normal of elevation.





Photo 9

View of silt material used for bodding riprap on upstream side of embankment



#### Photo 10

View of left foundation drain at impact basin. Note flow and buildup of slime.

hote 11

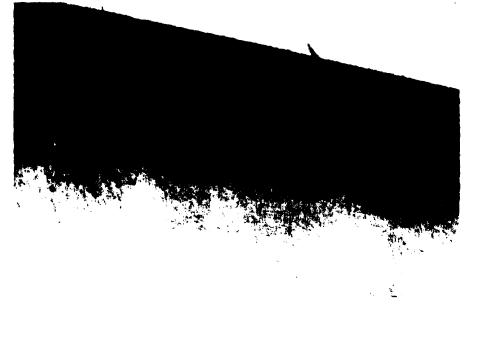
iew of right foundation drain t impact basin. Note flow nd buildup of slime

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NO 12

ew of underside of impact basin orhang. Note cracks and effloscence.



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#### APPENDIX D

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OUTLINE OF DRAINAGE AREA AND COMPUTATIONS

#### APPENDIX D

#### OUTLINE OF DRAINAGE AREA AND HYDRAULIC COMPUTATIONS

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Computations	Page No.
Drainage Area Map	D-1
Hazard Location Map	D-2
Size Classification, Hazard Potential, and Test Flood Determination	D-3
Flood Routing, PMF	D-9
Dam Failure Analysis	D-11

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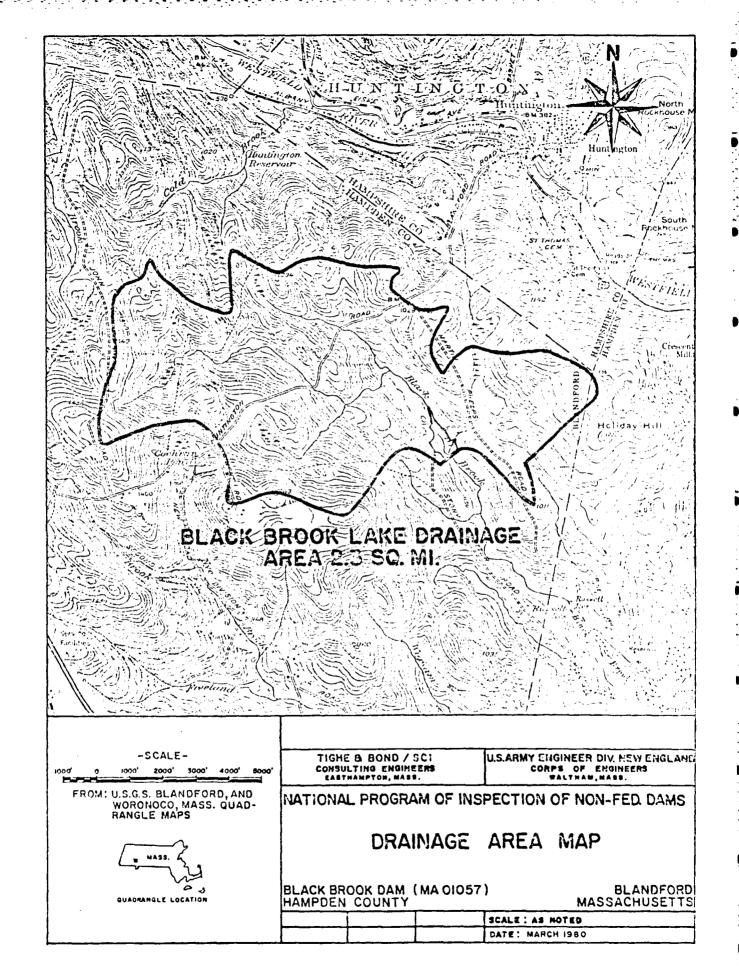
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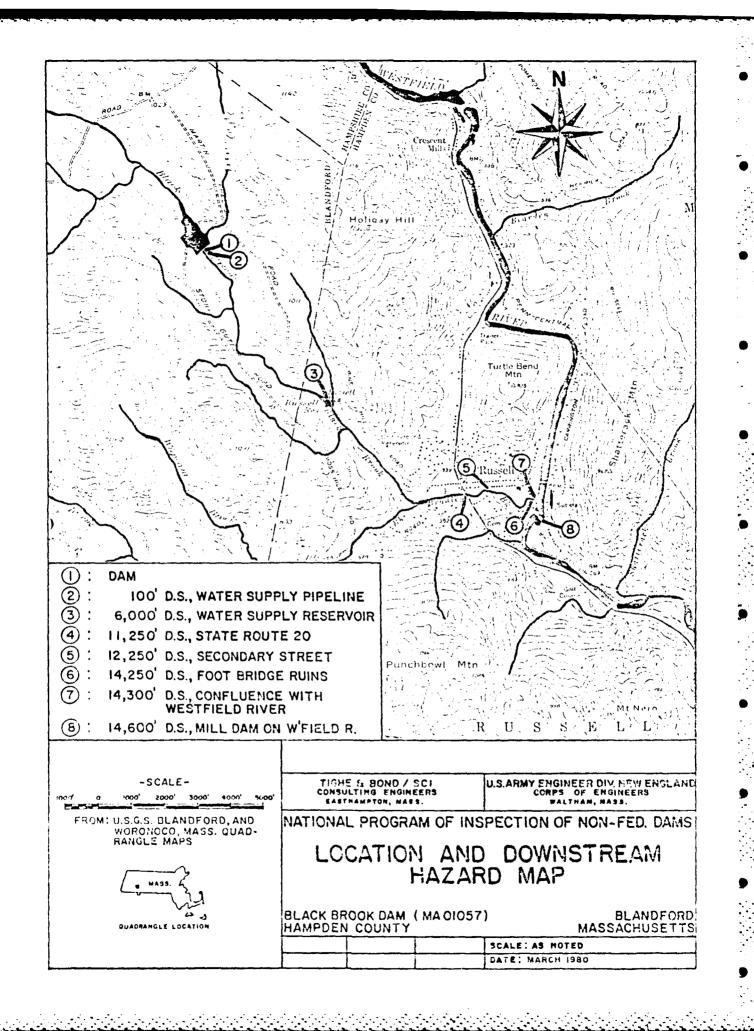
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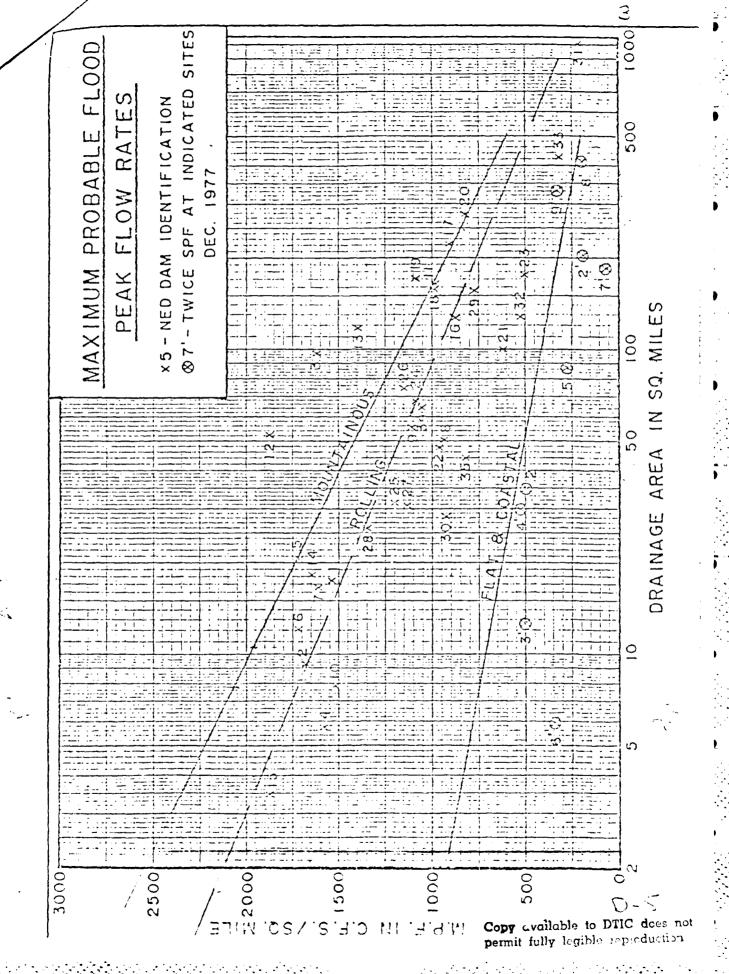
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and the second s 7/23/30 Torret an Mol Black Brook Dam Decision Frence - 23 SM 1) Size Chainfier Man = Dan 2.5 Tee - 833.7 Helt of don 623 62.3 11 > 40 but < 100 . Intersclution Storage at Tim of Dam - 1620 AF 1022AT > 1000AF 604 2 50 000 . Intermediate Horard Prin -2) in the particular from more when . available to DTIC does not a how two in a her and • Copy permit D-3

a martine star 2/23/33 Moe Moe Area in bein is mountanous -bere france is a Mountainon surve 1 Ľ from COE Pril Goud For Fil PUE OLECHAN Oper Company and = 2:00 c2. /th DIL-3720 - 73 = 5750045 use Tarange Copy available to DTIC does not permit fully legible reproduction D-4



And Carl Sugar 19 1 in the Ur. Comp Contendo Moe Spilling ord Conduct Retiry The principal iplicity has a rearmin one setting an Black which is 2-1" on and Not mys Alou -1. 95 here had stege wer the comment of the minute of the the internet of the second Have 37 have a tom 13 A 3's  $\phi$  convince price extended Ale the free free the place to ale magazer here The state of the hest brow excepted and the more all the state in the summer The Spill was is so' will .+ the treeall i de l'an mer a flat conte de la plane planetare 3507 and have a bound converse war and the second sec available to DTIC fully learbl and the second Ccpy 

Live on Dr. ange the state of the second state of the 2/23/2 Limp- Coursey Mile There exists an 18' received drein from the draw structure in the recordon to the bac st the reson The following spillway and conduct cating - formation was taken from the hydroutic section of the design filler For the Black Drook Dan Like, other Sei releases. The following information mus toten from the follow and technical relations. and we have compared the the Spilling Stage - Discharge Data a come to a come 902 370 المراجع 25.1 400 1.200 1 200 -0000 D-7 Copy available to DTIC does not permit fully legible reproduction

in the second contraction of the ZIZAZZ Conp. Conciles Mor Receiver Pouting Europe error to pass (Opi) 5500 cm chuitin = 896.5± Corcherge Should and 896.56± · - 863.50 33.00 From SCL Storigt - Elivetion Come in hydrolic en y office of Drug. Till Star = 896.50 = 1690 AF Volume = 1612 AE 1612-15 1.09 0- 13" Sites of the 200 5300 - 13 1: 1831 <fs Eucheury etc. In Don = 892.07 1-1-1- 1280 AF 1212 AC - 0 92 0 - 9.3 · · · · ·  $\frac{13}{12} = \frac{13}{12} = 230\% c_{-1}$ Copy available to DTIC does not permit fully legible reproduction

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HANDROWEL FRANCE AND MIC REVISED R. OHD 2/2:182 Spilling Part Ender Erg Er. Conduct Ξĩ Dan Total П 887 T 20-. T LC 204.5 Be U 209.9 200 409.9 89.10 213.0 1100 - 13/3.0 5600 3755 9580 1.555 6731 a over de - CLH% C=33 H-Q 397 - 375554 General in Low Street Only : Level Rein Standard Barris Strategie the prove of the second Copy available to DTIC does not permit fully legible reproduction D-5

1. S. 1. 2129180 3 Course Courselly, Mos Store 1282.7F = 0.86 or 10.3" Qp4: 5000(1-10.2)= QDA. 2655 (2. Contrary 7 200 - 892. -1111 1221 - 220 - 2 592.5 - 1300 AF 362 T - 78 FF Vol.... 1222 20 1222 0.83 01 9.9" Store and store i. Dans a not be contopped Stage will be at 393 and discharge will be 2000 215

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D - 1 c

Mou BLACK BASIK DAM DAM FALLORD ANALYSIS Gai - 4/27 1/2 19 1/2 W: Mid noight & Dam = (3161 334/2 = 555 Long h across river to original ground at Elev. 865 ises facel trasces) = 692' 19+60 - 12-92 = 577. 112 there \$123 682' We = 40% 40% 272' You Mar to sor Sand at Genderay Test Elegan 643 المعانة تو The state of the set of the state of - 59' 1. (n = \$27(272)/2=2) 00 = 207 203 de DAN FULLIFE RESTING Or any straight of Trans and 2.2 of met. South and Tost a list = Phile Manterias and Fridd and the strange State State Long to the State State State State The For and Fire Disposed 5 207 200 +20

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Moe BLACK FRÜK PAM 4/13/19) DAM EAILURE FIRST REACH : DAM TO RUSSELL RES. Length: 41; 3.312 = 4.15" 12.22 # 3000 Lengeh & Marin 2.50" (2700) = 6700 K. Styre 5= (3:4 - 620)/6700 0.032 H/H n= 0.04 Valley Me Sertium. 4 4 4 A= 13/+ 4/2 y2+ 3/2 y= = 13/+3/2 117: 4.121+ 2.241 - 12 = 6.251+13 K. A/WP = 1-1+ -12 8 6-201 - 13 40 2-10-10/2 = + 2 = 6.6+6 AR 23 1= 5; R=2.99; Q= 1,7240.5; A= 1254 1= 1. R= 5.44, Q = 8,216 - 5, d = 40. 1= 30, R= 14.94.0 - 120, 9550 = 3010 = 25 Y= 40; R= 19.67; - 251, 523. 2; 4= 520 7 21 5. 16 150 10 10.000 222100 Q cis. Be er - tollare 1= 27 2 -: 1= 6.2; A= 177 : 1= 11 + 3100 = 27. 4. 4. Array 1: June 2 - 2: 7, 1 1000 y= 37, 1, 1- 490, 1= 450 4350 4350 4350 4350 4350 4350 On - in 1 - 100 - 2000 - 2000 - 200 - 200 - 1355 1 = 200+ 193, 455 100 - 360 45. م من من المحتاج الذي المحتاج الموادية المراجع الذي المستقبة <del>المستقبة المحتاج المحتاج المراجع المراجع المراجع ا</del>لم م من من من الصري الأسليكي الأراكي الأراكي المراكي المراكي المراكي المراكي المراكي المراكي المراكي الم Copy available to DTIC does not permit fully legible reproduction D-12

Day Fizzz Hydranics Mie BLACK BROOK 24:41 REACHER Rossell Res. to Stage Brink Reach Longth: 1.55" 2782 - 4200' Stope: (020-343)/4200 - 0.065 Valley X-section: same as reach 1; n= 0.040 MPF 2 Anni 4: Drainage Areq: Dam = 2.3 59.mi 1.87 4.17 59.00i Dim to Stugetrank G=1430/n 5" AR " = 9.4714 AR "'S Y=5'; R= 2.491; Q= 2,498 ds; A= 125 = , V= 12.1 date Y=10'; R= 5.435; G= 11,712 dis; A= 400 = , V= 38.6 date Y=20; R= 14.94; Q= 172.276 date 2,15 = , 100 date R=14.94; 2=172.276(2), A= 40) = 1 = 289. AC. 4. R=18.94; 2=172.276(2), A= 300 = V= 289. AC. 4. R=18.576; C=18.5 C. Y=20) R=12941 2=172 276020 A = 2000 = V= 289. AC.H. Y=25; R=10.576; S=103, 541045; A= 2125 = V= 205 AC.H. Y=20; R=10.205; R=62, 337045; A= 140; = ; V=135 AC.H. 30 -25 2 = --눈 × 2 ? 150, 20 % 736 -50,000 100,000 0 1 20 day 42 212 1. 3 2:2 Eline Francis : OF 2700 cFr & Con John Vield Ac. Th = 2777 + 724 245 = 127 20 gran He Long Me Oglaman F 220 パック イイエン・シットウエル Copy available to DTIC does not V=2812-14 permit fully legible reproduction 12-13

REVERSES CHD Mes BLACK EROSK DAM D.3M FAILURE SILFANCHES KEACH 3, Stage Brook Confluence to Westfield River 4225' Keach ling the 1.49 (271) = 51226 : 1343- 11.31 4 88 2 3.222 11 n= 1.03 ; Valley X-Section: 600 Y < 10: A = 28 Y 2/2 - 101 + 60176 - 421 - 101 Y = Y-10, A = 4+00 + 25/72 + 870 / 4 34 52 = 4410 + 2704 + 145 / " G. 11.053 MJE / 31 A Mile - 7.2970 A. Rive Y = 5% R. - 2.55% 2 15,4200 A= 125 7 V=103 AC.K. Y = 10, R = 5.258, S = 95,230 (4), A = 4420 = , V=424 AC.H. Y = 3', R = 1.575, 2 = 44,10 - 6, A = 4.17=, V = 33 AC.H.  $\begin{array}{c} & & & \\ &$ 124: ---12. . 1.1.1.1 · · · · · · / · · · Ours 2 2 162 330 12 - 2 Entra Fulling Q= 2,700 crs ; 4=2.3' ; V= 37 ac. 14 a) the Follows Rep = 2,00+105,00=103,000 ; 1= 10.4 ; V= 440 ad it  $\mathcal{D}_{p-7} = -2750 + 102370 \left(1 - \frac{440-37}{1307}\right) = 2750 + 73,900 = 76,600$ he de la verster de late Nerve - there was a first second NOT = 2.700+105.000 - 1000 = 070+70,400 = 73,100 cr 6 - - -Copy available to DTIC does not permit fully legible reproduction D - 14

CHE REMAINS 7/9/20 DAW interest Alger maller More Elisten States The HAZAKO A. Roll- I was been der and Ele ( X-2002 Mar - 6201 Strand Stranger 1 12 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 - 51/2 A. 2 (T r=) + hw = 2 T 2 ( " 65 (245) = 2 ( 13) - 215 ( 241) = Assidence marked a communication of the state 200 1 Alin Contra 4,= 2,700 CFS 2700 CFS < 6,370 CFS Coperity · applie contraction by settions day and alt: Fairing : 96,2=108,000-23,20 (100) = 96,400 CP3. Elen Onen Rom = 26400 - 6370 = 90,000 cro H= ( 92000/3(200) = 13.7' Data at Eiser = 3/3 (15.7') = 9.2 ' V-1 = 10 = = = = = = = Copy available to BIIC does not permit i "y legifile i Fredretten

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OHD REVISIONS 7/9/50 Satisf Starke departures M. BLACK 22 MZ JAM HAZARD Secondary Store over Bradley Brook 1 200° 1 55° 1 200° 1 5.3 Bridge section: 9.7 A = 25 × 417 = 5 St ca. 4. hannel versely & 22 lps=4 As some heart to deconcrete on private of So A Y MAR AMAS SUM POR MORANAS SUM (2004) = 14, 20, 24. Ex-10 day - 1 war Q = 2,700 cts. 2700 CFS < 14,100 CFS Especity · asper contribé les attions channel ajeter Fairline : Grz = 79,100 + 28, 200 (2002) = 93,600 cm Filmer Que Road = 93,600 - 14,100 = 79,500 crs.  $H = (79, 5\infty/3(1035))^{2/3} = 0.7'$ Dapati, of Fring = = = = = (8.7) = 5.3 V= = 13= FPS. Copy available to DTIC doss not permit tuiny legible reproduction

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	DAM STATISTICS HUMAN MIC SLADA STATISTICS
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	Champell Japanery : nº 1822 (2012) A: 194+ 5/212 201 Ang Sta AR 12 : 7,215 - 15 - 15
-	$\mathcal{Y} = \langle \mathcal{T} \rangle \langle \mathcal{P} \sim \mathcal{X} \rangle \langle \mathcal{Y} \rangle \langle \mathcal{X} \sim \mathcal{I} \rangle \langle \mathcal{P} \mathcal{P} \mathcal{P} \mathcal{P} \rangle \langle \mathcal{P} \rangle \langle \mathcal{P} \sim \mathcal{T} $
	Free 18 - 19 18 - 79,100 - 22,121 = 56,600 CF3
े. की र	the second will be brought would be set
	( clatter = J. Claud) + = 56,600 / 4=7.2
	Y= 22, P= 1.22 1 42, 110 212 , 1 - 107=
Ľ	Friend 1 79,100 - 4 1 = 36,930 CFS
	1 33.000 / 1 = 56 Y=13+5 L=20L
	He coil ; knows i se serve stat a say the
	Filmer Dist. Browning = 79,100-32,700 = 41,400 (200)
▲	$H = \left(\frac{4}{3} \left(\frac{1}{3} \left(\frac{1}{3}\right)^{2}\right)^{2} = 6.2^{2} \qquad f = 15 + 6.2 = 21.2^{2}$
۰.	$f = 21.5 \pm 1$
	Destate and wording = 3/2 (21-1-15)= 4.3
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ONS REVISIONS TISTS the state 3220 Dam DATE THEY E Style - Marine Wroth the survey Elforthe Eval 1 Error de mager at Westfield Bleer 535 above Samer Dam 102 100 277 11-12 = 125  $\frac{1}{1}$ 269.7.122 250: M.L -- , (0:51 100 Q=14341, 2" + K"== 3.1574.1 2 "= V= 27.5 m  $\begin{array}{l} V = 2\, V_{1} \, (z = 13, 276), \, \hat{U} = 172, 000 + 00, \, \mathcal{A} = 3, 564 \stackrel{\text{d}}{=} (1, 2 + 347), \, W = 340 \\ V = 35', \, \mathcal{U} = 23.013', \, \hat{U} = 298, 430 \, \mathrm{cm}, \, \mathcal{A} = 3, 008 \stackrel{\text{d}}{=} (V = 32, 4.45) \\ Y = 45', \, \mathcal{R} = 28.610, \, \hat{\mathcal{R}} = 505, 460 \, \mathrm{ch} + \mathrm{ch}, \, \mathcal{I} = 5^{10}, \, \mathcal{V} = 37.445 \\ \mathcal{V} = 45', \, \mathcal{R} = 28.610, \, \hat{\mathcal{R}} = 505, 460 \, \mathrm{ch} + \mathrm{ch}, \, \mathcal{I} = 1.276^{-5}, \, \mathcal{V} = 37.445 \\ \mathcal{V} = 4', \, \mathcal{R} = 25.335', \, \mathcal{R} = 3145', \, \mathrm{ch} = 1.276^{-5}, \, \mathrm{V} = 35.45 \\ \mathcal{V} = 17', \, \mathcal{R} = 12.355', \, \mathcal{R} = 61, \, 552\,\mathrm{ch} + \mathrm{ch}, \, \mathcal{I} = 2, \, 234^{-5}, \, \mathrm{V} = 21.45 \end{array}$ Husself Down leveth = Forth Assume and the provides erest at the 269.7 9 below top it wer something section 500 ling. L. 500, Conto La 200, 123.4 130(1-7)% ×' V H O H=1.0 A H=H.7 13 37,300 7,400 Gy arak  $Q_{i}$ 13' 44, 100 39 34 158,000 143,100 55,700 352.400 2 144.250 50.000 19.3.19 5,120 2,222 52-0 Copy available to DTIC door not permit fully legible reproduction P - 15

CHO REVISORS TRA DAM FALLUES HYDELANCS Moe ELACKERSUK DAN Westricht Kiver Erects Ering Dand Silder Æ Q = 2,700 CPS Stage = Elev. 272.2 ± MBL After Dam Fuilare 2, = 79,100 crs 5/300 = Ebr. 284.4= M.7.1 Eternize observe dama - Yo ditter and de gette Staria 222 × 10,111× (284-272 /3(1121)) = 202 ac. ft  $f_{1,17} = 2,700 - 76,400 \left(1 - \frac{202}{1350}\right) = 2700 + 65,000 = 67,700 CFS.$ 5 tag 2 = Eler. 284.0 Flori stays is 4= above R.R. tracks é mille etrustres. Downtream of the same the plane forme fine with the publicity attenuation and not contrate a singer hayard Copy available to DTIC does not permit fully legible reproduction D-19

#### APPENDIX E

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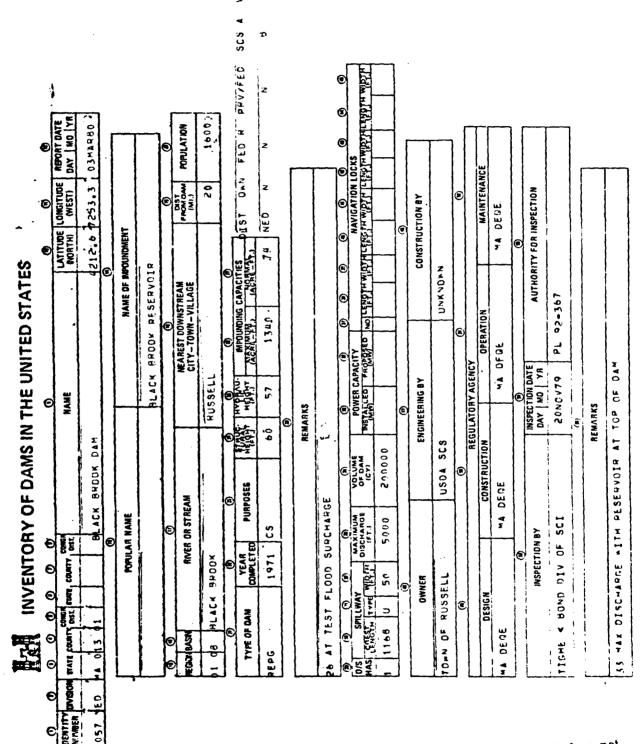
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#### INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS



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