

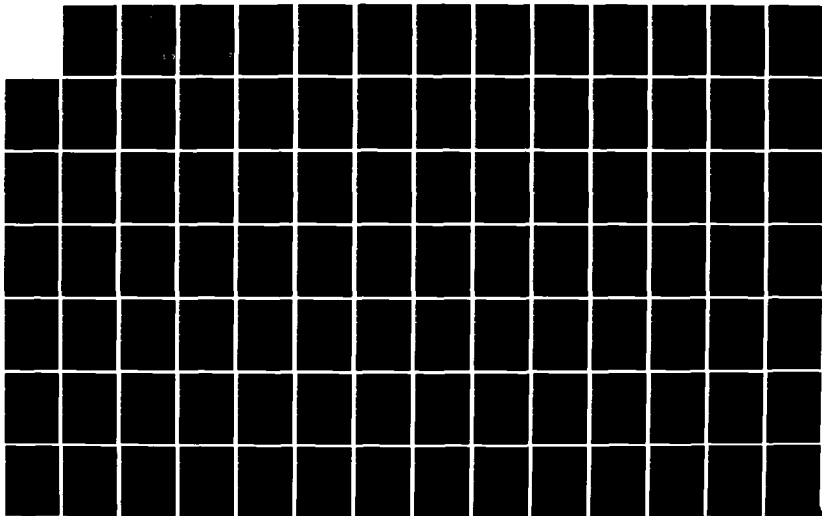
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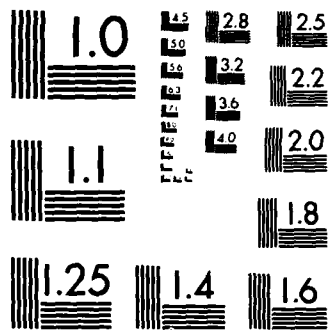
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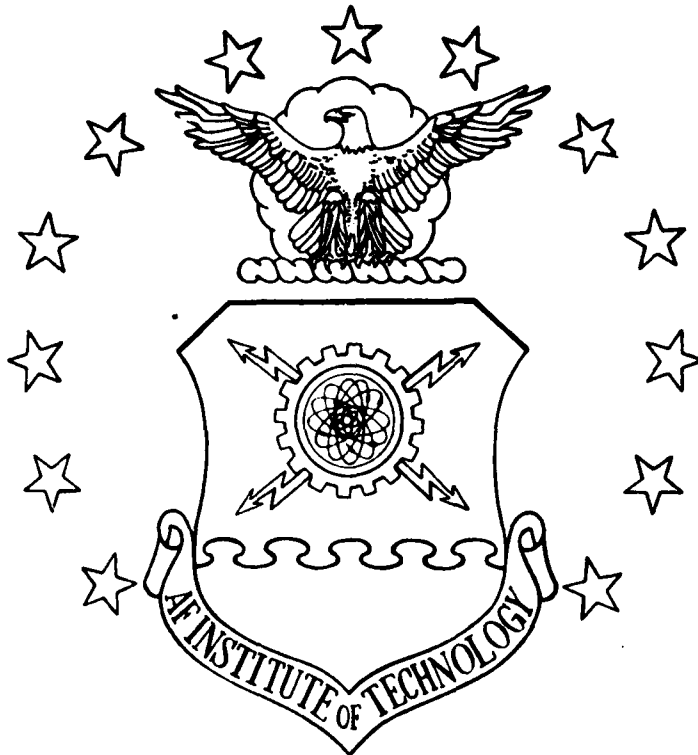
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**HEATING PARAMETER ESTIMATION USING  
COAXIAL THERMOCOUPLE GAGES IN  
WIND TUNNEL TEST ARTICLES**

THESIS

Neil T. Cahoon  
Captain, USAF

AFIT/GAE/AA/84D-3

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**HEATING PARAMETER ESTIMATION USING COAXIAL  
THERMOCOUPLE GAUGES IN WIND TUNNEL  
TEST ARTICLES**

**THESIS**

**Presented to the Faculty of the School of Engineering  
of the Air Force Institute of Technology  
Air University  
In Partial Fulfillment of the  
Requirements for the Degree of  
Master of Science in Aeronautical Engineering**

**Neil T. Cahoon, B.S.E.  
Captain, USAF**

**December 1984**

**Approved for public release; distribution unlimited**

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Also to my wife, Shirley, for the sacrifices she made during the course of this academic experience, I would like to say thanks. She provided immeasurable support and encouragement during my long hours of study.



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### List of Symbols

$A, A', b, d$	Coefficient Matrices ( $i \times i$ )
$c$	Specific Heat
$E$	Residual Error Vector ( $m$ )
$G$	Kalman Gain Vector ( $i$ )
$H$	Thermocouple Location Matrix ( $m \times i$ )
$h_0$	Magnitude of Heat Transfer Coefficient Ratio
$h_s$	Heat Transfer Coefficient Derivative
$\bar{h}$	Heat Transfer Coefficient Ratio
$h_{ref}$	Reference Heat Transfer Coefficient at Zero State
$I$	Identity Matrix
$J_k$	Conditional Information Matrix
$k$	Thermal Conductivity
$L$	Total Number of Spatial Node Points
$P$	Covariance Matrix ( $i \times i$ )
$Q$	Model Error Covariance Matrix ( $i \times i$ )
$q$	Heating Rate
$R_m$	Covariance for $m$ th measurement
$S$	Score Vector ( $k$ )
$S_{i,k}$	Sensitivity Vectors ( $i$ ) for the $k$ th Parameter
$T_{aw}$	Adiabatic Wall Temperature
$t$	Time
$U$	Temperature Vector ( $i$ )

$x$	Spatial Coordinate
$Y$	Thermocouple Measurement Vector
$\alpha$	Angle of Attack
$\epsilon$	Emissivity
$\Theta$	Parameter Vector
$\mu_n$	Measurement Vector at nth Time Point
$\rho$	Density
$\sigma$	Stefan-Boltzmann Constant
$\delta$	Transition Matrix
$\delta_c$	Scaling Parameter for Specific Heat
$\delta_k$	Scaling Parameter for Thermal Conductivity

Superscripts

-	a priori Propagation
+	a posteriori Propagation
*	Parameter Estimate
n	Time Level
s	Iteration Level
T	Transpose

Subscripts

i	Spatial Node Point
k	Number of Model Parameter
m	Number of Thermocouples
o	Freestream Conditions

## Abstract

A heat energy balance is applied to a coaxial thermocouple gage for parameter estimation in wind tunnel test articles. This method can significantly reduce wind tunnel test costs and time. Modifications to the data reduction technique HEATEST (HEATing ESTimation) are made. The program allows for transient test techniques to be used as well as assuming an isothermal wall. A non-linear convective heat transfer coefficient model may also be used. Data is generated to test the new program. Temperature profiles throughout the thermocouple gage were good and were compared with changes in time step, thermocouple length, and number of discrete node points. The estimation of the convective heat transfer coefficient and thermal conductivity were excellent.

**HEATING PARAMETER ESTIMATION USING COAXIAL  
THERMOCOUPLE GAUGES IN WIND TUNNEL  
TEST ARTICLES**

**I. INTRODUCTION**

**1.1 Background**

The determination of heat transfer rates on hypersonic configurations upon reentry is important for the survival of the vehicle. The problem is that the heat rate is not a quantity which may be directly scaled from model tests in wind tunnels. However, the parameters which make up the heat rate equation (thermal conductivity and specific heat, for example) can be scaled from which the heat rate may then be calculated. Wind tunnel heat transfer measurements have traditionally used a thin walled test model fabricated with thermocouples mounted on the inside skin surface. The "thermal model" then yields a heat rate based on temperature measurement from the thermocouple. Another technique uses a coaxial thermocouple gage mounted in a thick skin model. A discussion of the two methods follows.

**The Traditional Thin Skin Model**

The "thermal model" of a traditional wind tunnel thin

skin model assumes that all of the heat penetrates the thin skin via conduction to a standard thermocouple gage mounted on the back face. No lateral conduction is assumed and since the emittance of the steel model is low, radiation is assumed negligible. A typical heat rate measurement data point is acquired by injecting the cooled model into the wind tunnel at a known temperature and time and by measuring the temperature at later times. The model is then removed from the tunnel, cooled, and a change in configuration is made in preparation for the next injection and subsequent data point. There are three very severe limitations associated with this technique (Ref 1). The first is the inability to acquire more than one data point during any one injection. The thermal model simply does not allow for the type of change in configuration or model attitude which can be accomplished using dynamic testing techniques (to be discussed later). Associated with this limitation is the long cooling time between each test which significantly increases the cost per data point for the overall test. A second limitation is the special thin skin model which must be fabricated, further contributing to increased test cost. Finally, the assumption of no lateral conduction through the model may in fact be a poor assumption at some critical locations with large curvature. An alternate type of gage, the coaxial thermocouple, can eliminate these limitations with an overall effect of reducing time and cost.

## A New Application For An Old Thermocouple

The coaxial thermocouple gage is shown in Fig. 1.1. It consists of a constantan (a metal alloy) jacket surrounding a chromel core with a thin layer of insulation separating the two metals. The coaxial gage is mounted in a steel model thick enough so that the thermal pulse is not sensed on the backface (ie. the model wall is considered a semi-infinite slab). The thermocouple surface is formed when the gage is lightly sanded to match the contour of the model. Some gages are available with backface temperature monitoring to assure that the thermal pulse does not reach the backface in any given run so that an analytical integration of the heat equation can be used to determine the heating rate history. The backface temperature information prior to this investigation is not factored into the data reduction process, however.

Operation of the coax gage is based on uniform conduction along the gage length which would necessitate the model be made of a material with similar thermal properties (Ref 3). The thermal properties of stainless steel match very closely with the gage properties, therefore, the presence of the gage is negligible. The matching of thermal properties also enhances accuracy. A coaxial gage which is matched thermally with the model allows an isothermal wall assumption, whereas other gauges such as calorimeters and thin film gages are not thermally matched, and cause a non-isothermal wall. Measured heat transfer can be in error by

$$\begin{aligned}\dot{\{U\}} &= [A]\{U\} + \{b\} + W(t) \\ \{S_k\} &= [A]\{S_k\} + \{d_k\}\end{aligned}\quad (3-1)$$

These equations are solved using a tridiagonal algorithm in subroutine TPS3 for the temperature states, and subroutine SENS for the sensitivity of the temperature to the kth parameter. Propagation of the covariance, P, of the temperature state at each node is accomplished by the approximate difference equation,

$$\begin{aligned}P(t_n^-) &= \phi(\Delta t)P(t_{n-1}^+)\phi^T(\Delta t) \\ &+ \int_{t_{n-1}}^{t_n} \phi(t_n-\lambda)Q\phi^T(t_n-\lambda)d\lambda\end{aligned}\quad (3-2)$$

where  $\phi$  is the transition matrix and where the - and + superscripts are used to denote the expected values before an update (or a priori) and updated (or a posteriori) values, respectively. This calculation is made in subroutine TPSOSP2.

A model of the temperature measurement process must be used for the Kalman filter equations. The measurement equation to identify thermocouple location is,

$$Y(t_n) = H \{U(t_n)\} + \{\mu_n\}\quad (3-3)$$

The updated temperature is calculated by,

$$U(t_n^+) = U(t_n^-) + GE(t_n)\quad (3-4)$$

time. They are found by employing a Kalman filter - a set of recursive equations that optimally combine the propagation of the model equations with measurement updates at each sample time. After the entire temperature - time (state) history has been calculated, a gradient algorithm is used to solve for best estimates of the parameters according to a maximum likelihood criterion.

The second type of estimate consists of the parameters defined in the parameter vector,  $\{\theta\}$ , as given in Equation 2-10. These parameters remain essentially constant throughout a transient maneuver profile such as a pitch sweep and are estimated based on data from the entire maneuver history. The process of estimating states and parameters is then iterated for convergence to some optimal estimate.

The method used to estimate the states and parameters is formulated from stochastic estimation theory and is known as adaptive estimation. A detailed development of the estimation equations is beyond the scope of this thesis and the reader is referred to References 7 and 8 for more detail.

The thermal model equations for temperature and sensitivity have already been written in the matrix stochastic estimation form of Equation 2-12 as,



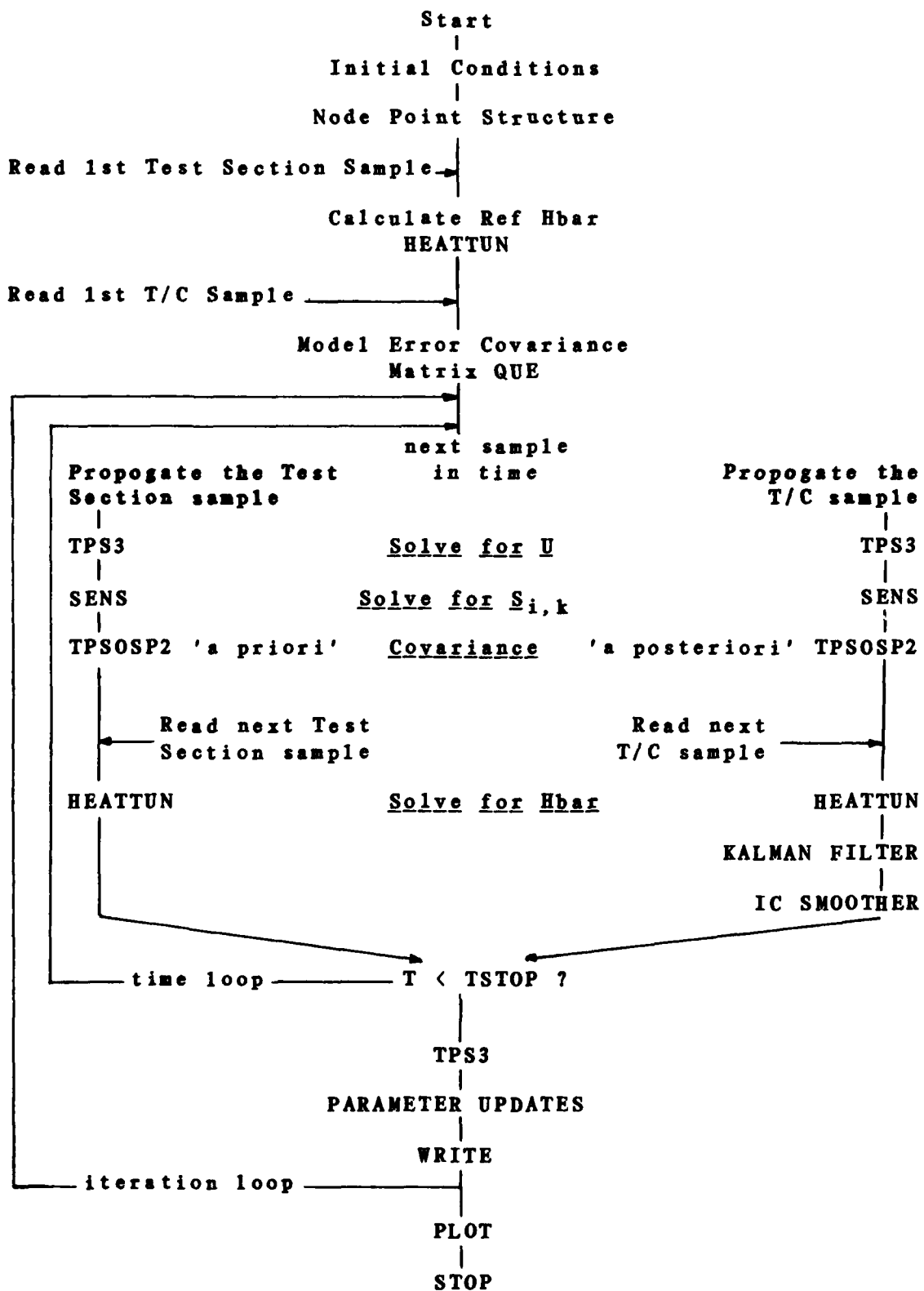


Figure 3.1 HEATEST Algorithm Summary

### III. HEATEST OVERVIEW

The HEATEST program was originally developed to determine and model heat rates from the Space Shuttle Orbiter thermocouple data, hence most of its nomenclature references flight data samples and trajectory samples. The wind tunnel equivalence of the trajectory sample would be the test section conditions at the time of the sample (ie. density, velocity, pressure, etc.). The flight data are the thermocouple measurements from the coaxial gages.

An algorithm summary of the HEATEST program is given in Figure 3.1. The initial conditions for the temperature profile,  $U(t)$ , and the initial covariance,  $P(t)$ , are specified at the start of the wind tunnel test run. Heating model initial parameters, and the initial reference values for the heating model are read in as inputs to the program. Initial sensitivities of the state are specified to be zero. The node point structure throughout the depth of the thermocouple is then calculated from the input of the length of the gage and the number of node points.

Two types of estimates must be made in order to describe the thermodynamic environment in the wind tunnel. The first type are the state estimates, which are defined by each node temperature. These state estimates are not constant since the temperature varies throughout the maneuver, and hence, must be estimated at each node point in

The {b} vector is not used directly for the covariance equation, but is approximated by an error model given by,

$$Q_{\text{error}} = [\bar{h} h_{\text{ref}} (T_{\text{aw}} - U_1) \Delta x / \phi_k k]^2 \quad (2-15)$$



$$[A']\{U_i^n\} + \{b\} = 0 \quad (2-9)$$

where  $[A']$  is an  $n \times n$  tridiagonal matrix of material properties and  $\{U_i^n\}$  is the  $n$ -dimensional column vector of unknown temperature at each node point for each time.

In general, the unknown parameters in this model formulation are the heat transfer coefficient intercept,  $h_0$ , the slopes  $h_{a1}$  and  $h_{a2}$ , and the scaling parameters for specific heat and thermal conductivity,  $\phi_c$  and  $\phi_k$ , respectively. These parameters may be defined as a vector,  $\theta$ , of unknown parameters for use in the system identification scheme as,

$$\theta = \{h_0, h_{a1}, h_{a2}, \phi_c, \phi_k\}^T \quad (2-10)$$

The primary purpose of the heating estimation program is to obtain best estimates of these parameters during transient test maneuvers. To estimate these parameters it is necessary to calculate the model sensitivity to each unknown parameter.

## 2.2 Sensitivity Equations

The derivative of Equation (2-7) with respect to each parameter yields equations of the same form as Equation (2-9) from which the HEATEST program propagates the sensitivity. For example, the sensitivity of the temperature with respect to  $h_0$  would be written as follows,

$$\frac{\partial U}{\partial \theta_1} = \frac{\partial U}{\partial h_0} = S_{h0} = S_{i,1} \quad (2-11)$$

level defined by the superscript  $n$ ,

$$\begin{aligned}(U_1^{n,s+1})^4 &= (U_1^{n,s})^4 + 4(U_1^{n,s})^3[U_1^{n,s+1} - U_1^{n,s}] \\ &= -3(U_1^{n,s})^4 + 4(U_1^{n,s})^3 U_1^{n,s+1}\end{aligned}\quad (2-6)$$

Substituting Equation (2-6) into (2-5) yields,

$$\begin{aligned}\frac{\rho \phi_c \Delta x}{2} \frac{U_1^n - U_1^{n-1}}{\Delta t} &= \frac{-\phi_k k_{1+1/2}}{\Delta x} U_1^n + \frac{\phi_k k_{1+1/2}}{\Delta x} U_2^n \\ &- \epsilon \sigma [-3(U_1^{n,s})^4 + 4(U_1^{n,s})^3 U_1^{n,s+1} - (U_1^n)^4] \\ &+ [h_0 + h_{a1}(\alpha - \alpha_1) + h_{a2}(\alpha - \alpha_2)] h_{ref} (T_{aw} - U_1^{n,s+1})\end{aligned}\quad (2-7)$$

The model equation for the interior node points, ( $i=2,imax$ ), yields,

$$\begin{aligned}\rho \phi_l c \Delta x \frac{U_i^n - U_i^{n-1}}{\Delta t} &= \frac{\phi_k k_{i-1/2}}{\Delta x} U_{i-1} \\ &- \frac{\phi_k (k_{i-1/2} + k_{i+1/2})}{\Delta x} U_i \\ &+ \frac{\phi_k k_{i+1/2}}{\Delta x} U_{i+1}\end{aligned}\quad (2-8)$$

Equations (2-7) and (2-8) can be rearranged into the familiar matrix form,

parameters other than those included in the reference heat transfer coefficient are summarized by the static transfer relation or heat transfer coefficient ratio,  $h_{bar} = h/h_{ref}$ . Here, the ratio is assumed to be piecewise linear with respect to angle of attack as derived from Lagrange Interpolation Theory (Ref 6 and Ref therein).

$$h_{bar} = [h_0 + h_{a1}(\alpha - \alpha_1) + h_{a2}(\alpha - \alpha_2)] \quad (2-4)$$

where  $h_0$  is the magnitude of the heat transfer coefficient,  $h$  at the reference conditions,  $\alpha_1$ , specified by the one subscript. The heating parameters  $h_0$ ,  $h_{a1}$ , and  $h_{a2}$  are considered to be unknown and constant over a prescribed time period, and will be estimated by the HEATEST program. The parameters correspond to a derivative with respect to deflection angle of the model. Thus, for constant step size, the model equation at the surface node, ( $i=1$ ), becomes,

$$\begin{aligned} \frac{\rho \phi_c \Delta x}{2} \frac{U_1^n - U_1^{n-1}}{\Delta t} &= \frac{-\phi_k^{k_{1+1/2}}}{\Delta x} U_1^n \\ &+ \frac{\phi_k^{k_{1+1/2}}}{\Delta x} U_2^n - \epsilon \sigma [(U_1^n)^4 - (U_{\infty}^n)^4] \\ &+ [h_0 + h_{a1}(\alpha - \alpha_1) + h_{a2}(\alpha - \alpha_2)] h_{ref} (T_{aw} - U_1^n) \end{aligned} \quad (2-5)$$

The non-linear radiation term is quasi-linearized on an iteration level defined by the superscript  $s$  and by the time

where

- $\epsilon$  radiative emissivity
- $\sigma$  Stefan Boltzmann constant
- $c$  material Specific Heat
- $\rho$  material density
- $k$  Thermal Conductivity
- $\phi_c$  Specific Heat scaling parameter
- $\phi_k$  Thermal Conductivity scaling parameter

The material specific heat and thermal conductivity are both scaled by the two factors  $\phi_c$  and  $\phi_k$ , respectively, hence the value for  $c$  and  $k$  will remain unchanged. The parameters  $\phi_c$  and  $\phi_k$  will be estimated by the HEATEST program. Coefficients with subscripts which are less than one or greater than  $n$  are zero. The radiation and heat rate terms are also zero except at the surface node. Equation 2-1 includes terms due to conduction from adjacent node points  $k_{i-1/2}/\Delta x_{i-1}$ , surface radiation  $\epsilon\sigma U_i^4$ , and the convective transfer of energy as obtained from the heating model. The resulting system of implicit difference equations must be solved simultaneously.

The heating model for the convective transfer of energy is based on Newton's Law of Cooling,

$$q = h(T_{aw} - T) \quad (2-2)$$

Non-dimensionalizing by a reference heat transfer coefficient,  $h_{ref}$  yields,

$$q = \bar{h} h_{ref} (T_{aw} - U_i) \quad (2-3)$$

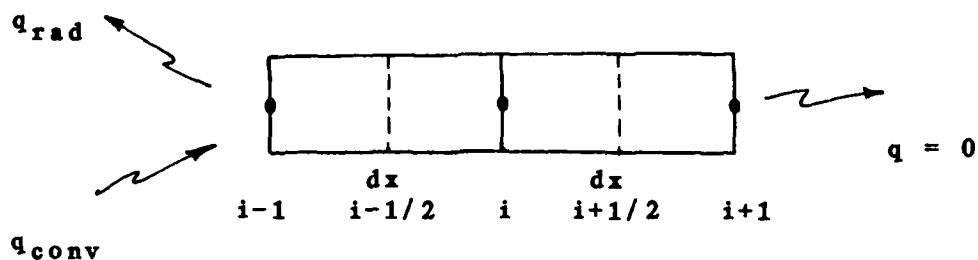
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## II. THE THERMAL MODEL

### 2.1 Temperature Equations

A cross section of the one-dimensional model is given in Figure 1.1 and below as a typical coaxial thermocouple gage.



An energy balance is performed on each element. The thermal conductivity,  $k$ , is taken as an average between each node. Fourier's Law of Heat Conduction throughout the gage, the Stefan-Boltzmann Law for radiation and Newton's Law of Cooling for convection on the surface face yield a system of  $n$  nonlinear differential equations of the form:

$$\begin{aligned}
 & [(\rho_i \phi_c c_i \Delta x_i + \rho_{i-1} \phi_c c_{i-1} \Delta x_{i-1}) / 2] [(U_i^n - U_i^{n-1}) \Delta t] \\
 & = \phi_k [k_{i-1/2} / \Delta x_{i-1}] U_{i-1}^n \\
 & \quad - \phi_k [k_{i-1/2} / \Delta x_{i-1} + k_{i+1/2} / \Delta x_{i+1}] U_i^n \\
 & \quad + \phi_k [k_{i+1/2} / \Delta x_{i+1}] U_{i+1}^n \\
 & \quad - \epsilon \sigma (U_i^4 - U_{i-1}^4) + h_{bar} h_{ref} (T_{aw} - U_i) \quad (2-1)
 \end{aligned}$$

gage using a Kalman filter(Ref 2). The purpose of this investigation is to incorporate the appropriate thermal model equations into the HEATEST program for application to coaxial thermocouple gages as used in the wind tunnel. Two reasons for doing this are, 1) replace the analytical with the semi-infinite assumption, ie. extend the run time or shorten the gage, and, 2) estimate thermal properties. Testing and verification of the modified program is necessary for verification of the validity of the results. Simulated data are generated by an analytical solution, and are processed for testing purposes for which the results are known.

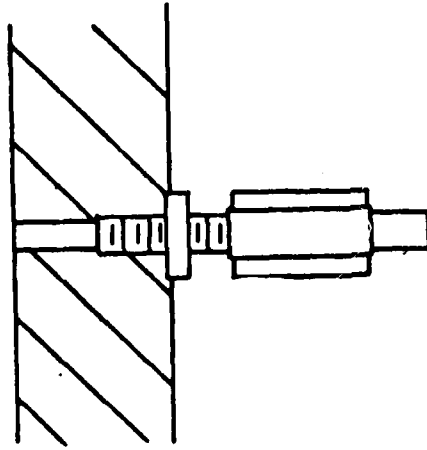
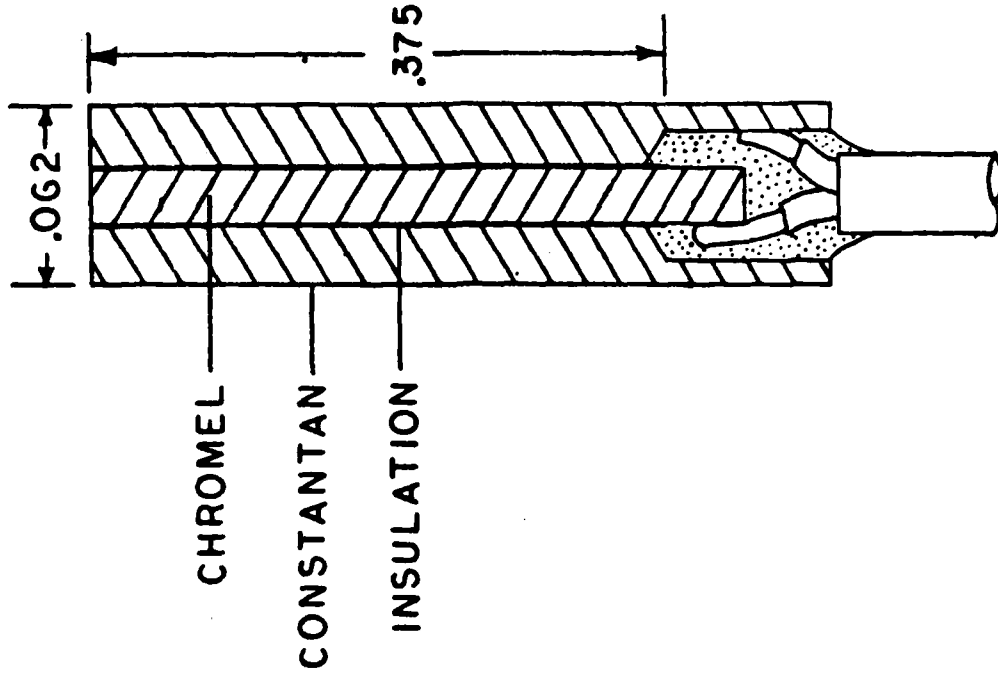
### 1.3 Overview

A development of the pertinent temperature, sensitivity, and covariance equations will be developed for introduction into the HEATEST program in Chapter II. Details in format for programming may be found in Appendix A & B. Chapter III is an overview of the HEATEST algorithm and shows how the equations developed in Chapter II are utilized. Chapter IV outlines the method for testing the program and offers a discussion of the test cases made and results. Finally, conclusions about the validity of the modifications, and suggestions for further improvement are included in Chapter V.

up to 40% because of the non-isothermal (Ref 2). The same rugged model built for pressure measurements can be used for temperature measurements as well, which would further reduce the wind tunnel costs. The data reduction technique, which uses the temperature time history, eliminates the requirement to fix the model configuration or attitude during any one run, hence dynamic testing techniques may be used similar to the flight test technique used for the Space Shuttle Orbiter (Ref 4). The model may be swept in angle of attack, for example, to determine heat rates as a function of angle of attack. All of these attributes along with a short response time and no required calibration (ref Knox) combine to yield the wind tunnel engineer a tool of marked improvement over previous methods.

## 1.2 OBJECTIVES

A method of analysis to identify the aerothermodynamic flight environment and update the thermal model of the engineering simulation of the Space Shuttle Orbiter was designed by the Air Force Flight Test Center. This method is in the form of a digital computer program called HEATEST (HEATing ESTimation). The program provides a correlation of the heating as well as a heat rate time history. The program integrates numerically instead of relying on some analytical assumption. It satisfies a maximum likelihood criteria for each parameter and obtains best estimates for the temperature at discrete nodes throughout the length of the



MODEL TCS  
COAXIAL PROBE MOUNTED  
IN A METAL WALL

FIGURE 1.1 COAXIAL THERMOCOUPLE GAGE

where

$$G = P(t_n^-)H^T[HP(t_n^-)H^T + R_m]^{-1}$$

$$E = Y(t_n) - HU(t_n^-)$$

The updated sensitivities are calculated by,

$$S_k(t_n^+) = [I-GH]P(t_n^-)[I-GH]^T + GR_mG^T \quad (3-5)$$

The updated covariance is calculated by,

$$P(t_n^+) = [I-GH]P(t_n^-)[I-GH]^T + GR_mG^T \quad (3-6)$$

To alleviate the problem of imprecise initial conditions, a fixed point smoothing algorithm has been added to the HEATEST program. Details of the smoother and its effects in the adaptive estimation scheme may be found in Reference 6.

Finally, the best estimates of the parameters are then estimated at the end of a specified time segment by the gradient algorithm,

$$\theta^* = \theta - [\partial^2 F / \partial \theta^2]^{-1} \partial F / \partial \theta = \theta + J^{-1}S \quad (3-7)$$

where,

$$J_{i,j} = \sum_{n=1}^N S_{i,k}(t_n^-)H^T[HP(t_n^-)H^T + R_m]HS_{i,k}(t_n^-)$$

$$S_k = \sum_{n=1}^N S_{i,k}(t_n^-)H^T[R_m]^{-1}[Y(t_n) - HU(t_n^-)]$$

The matrix J is an approximation for the Jacobian or conditional information matrix and is given in component

form by  $J_{i,k}$ . The score vector,  $S_k$ , is used to approximate the gradient of the likelihood function for a large number of time samples.

Using these equations, best estimates for the temperature time history (states) at each node can be found, as well as the deviation in temperature as provided by the covariance matrix. Also, an estimate of the parameter uncertainty is provided by the Cramer-Rao bound. The Cramer-Rao bound relates the conditional information matrix to the covariance of the parameter estimate.

## IV. RESULTS

### 4.1 Test Procedure

To test the validity of the program modifications, a set of contrived data was generated. Its development assumes that the heat rate due to convection at the surface node is constant and equal to the heat rate due to conduction at the surface. The heat rate due to convection is given by,

$$q = h(T_{aw} - T_w)$$

or

$$q = h_{bar}h_{ref}(T_{aw} - T_w) \quad (4-1)$$

where  $h_{bar}$  is defined as in Equation A-12. The equation for the heat rate due to conduction assuming a one-dimensional, homogenous, semi-infinite solid is as follows (Ref 9),

$$q = \frac{(\rho ck)^{1/2}}{\pi} \int_0^t \frac{dT_w(\tau)}{d\tau} \frac{d\tau}{(t-\tau)^{1/2}} \quad (4-2)$$

where  $t$  = time from start of heating  
 $T(t)$  = surface temperature rise  
 $\tau$  = dummy variable of integration

Equating Equations 4-1 and 4-2 yields,

$$q = \bar{h} h_{ref} (T_{aw} - T_w) = \frac{(\rho c k)^{1/2}}{\mu} \int \frac{dT_w(\tau) d\tau}{(t-\tau)^{1/2}} \quad (4-3)$$

Two different expressions for the derivative of the wall temperature with respect to time were used. The first implied a linear change in temperature with respect to time yielding a constant for  $dT_w/dt$  and the second expression assumes that temperature was a quadratic function of time as shown,

<u>Linear</u>	<u>Quadratic</u>
$T_w = bt + c$	$T_w = at^2 + bt + c$
$\frac{dT_w}{dt} = b$	$\frac{dT_w}{dt} = 2at + b$

Solving Equation 4-3 for  $T_{aw}$  so that  $h$  and  $q$  are constant and after making the indicated substitutions and integrating yields,

Linear assumption

$$T_{aw} = T_w + \frac{2b}{\bar{h} h_{ref}} \sqrt{\frac{\rho c k t}{\pi}} \quad (4-4)$$

Quadratic assumption

$$T_{aw} = T_w + \frac{2}{\bar{h} h_{ref}} \sqrt{\frac{\rho c k t}{\pi}} \left( b + \frac{4at}{3} \right) \quad (4-5)$$



A short computer program was written to produce a temperature-time history in the data tape format for the HEATEST program. For the above equations,  $h_{ref}$  and  $h_{bar}$  (the estimated parameter) were set equal to 1 and the coefficients  $a$ ,  $b$ , and  $c$ , were selected to yield reasonable values for  $T_w$ .

#### 4.2 Test Cases

The reference test case was taken to be a 10 sec. simulated wind tunnel test run using the linear data provided from the previous section. Thermocouple samples and test section samples were provided at the rate of one sample per second. The objective was to examine the rate of convergence of the temperature states and to estimate the first parameter,  $h_0$ . Recall from Section 4.1 that the data was generated to yield a value of one for  $h_0$ . Also of interest, was the validity of the model to the semi-infinite solid assumption (ie. no change in the temperature at the back face node throughout any specified time segment).

The input data is shown in Figure 4.1 and is generated digitally depending upon a desired time step ( $\Delta t$ ). The initial temperature throughout each gage is assigned a value of 60°F. Figure 4.2 shows the input temperature values for a  $\Delta t = 1$  sec. as used in the reference test case.

Figure 4.3 identifies the temperature state at the 2 sec.(lowest curve), 6 sec.(middle curve), and 10 sec.(top curve) times following the first iteration through the

updated HEATEST program. It clearly shows that at the back face node, the semi-infinite solid assumption used to derive the data is violated. This is indicated by the change in backface (node 6) temperature with time. Note also, however, that the temperature gradient at the back nodes (between nodes 5 and 6) is zero due to the adiabatic wall assumption. It should also be pointed out that surface node temperature response to the given input was immediate with no time lag.

Figure 4.4 is similar to Figure 4.3 except the temperature states and parameter estimates have been iterated to convergence, in this case, three times. Overlaying the two figures shows no perceptible difference between them, and the data shows no variations in values until after the second decimal point. In spite of the response of the back face node which would ordinarily invalidate the test, the estimated value for  $h_0$  was .99598, within .4% of the desired value of 1! Several test cases will be compared to this reference by examining changes in time step, thermocouple length, and the number of node points. Also, an examination of the ability of the program to estimate the other parameters, follows.

#### 4.2.1 Changes in Time Step

Figures 4.4, 4.5, and 4.6 show temperature states at 2, 6, and 10 sec. for  $\Delta t$  equal to 1, .5, and .25 sec., respectively. All three curves required three iterations

for convergence. The curves are all similar in shape with almost no perceptible differences. However, if the 10 sec. curves from  $\Delta t = 1$  sec. and  $\Delta t = .25$  sec. are overlaid as in Figure 4.7, a small difference may be noted at the backface nodes indicating that, indeed, a decrease in time step will yield a profile which will more closely approximate the model.

#### 4.2.2 Changes in Thermocouple Length

Changes in thermocouple length offered the most dramatic changes in temperature state as can be seen in Figures 4.8, 4.9, and 4.10 where the lengths range from .1 ft., .05ft., and .025 ft., respectively. The two longer lengths converged within three iterations while the short thermocouple length took four iterations to converge. The extra iteration is most likely due to the large deviation from the model and the large differences in temperature state from one time step to the next. Figure 4.11 compares the temperature state of each thermocouple length after the 10 sec. run. The lowest curve is associated with the longest thermocouple, and the upper curve is associated with the short gage.

#### 4.2.3 Changes in Number of Node Points

For this comparison, a 10 sec. run with 6 node points and a 3 sec. run with 6 node points (Figures 4.12 and 4.13) will be compared with a 10 sec. run with 12 node points and

a 3 sec. run with 12 node points (Figures 4.14 and 4.15). Each of the test runs were converged by the third iteration. At both of the different run times, increasing the number of nodes yielded a solution which more closely approximates the model (ie. the semi-infinite solid at the back face node) and gave correspondingly better estimates for  $h_0$ . The comparison of temperature states is better represented by Figures 4.16 and 4.17 which directly compares 6 nodes and 12 nodes interspersed evenly throughout the .05 ft. long thermocouple for 10 sec. and 3 sec. run times, respectively.

#### 4.2.4 Parameter Estimation

The ability of the algorithm to estimate  $h_0$  has already been discussed. To summarize, even when the output temperature states clearly violate the semi-infinite solid assumption used in generating the data, the estimated values of  $h_0$  remain within 15%. The 15% is a worst case number derived from the short thermocouple using a coarse grid for a long run time. An average deviation which considers all of the test cases evaluated is closer to 3%.

To estimate  $\phi_k$ , an erroneous data value was given for  $K_{data}$ , wherein the program iterated to a value for  $\phi_k$  which, when multiplied by the erroneous  $K_{data}$ , would yield the correct value, ie.  $\phi_k K_{data} = K_{correct}$ . The erroneous  $K_{data}$  which was input into the program was 14% in error of the  $K_{correct}$  value. The value provided by the program for  $\phi_k$  when multiplied by  $K_{data}$  yielded a value within .9% of

the  $K_{\text{correct}}$  value!

The estimate of  $\phi_c$  was not as successful, however. After 6 iterations, the solution was diverging from the expected value. A suspected sign error in the  $\phi_c$  sensitivity calculation is the most likely cause.

The quadratic input data was used as a comparison to the linear data to challenge the algorithm, ie. the more complicated the input the more difficult the estimation process. No direct comparison may be made of temperature, however, since the input data is different. The parameter estimation of  $h_g$  using the quadratic input data was still excellent yielding .1%, while the estimate using linear data was somewhat better at .05%.

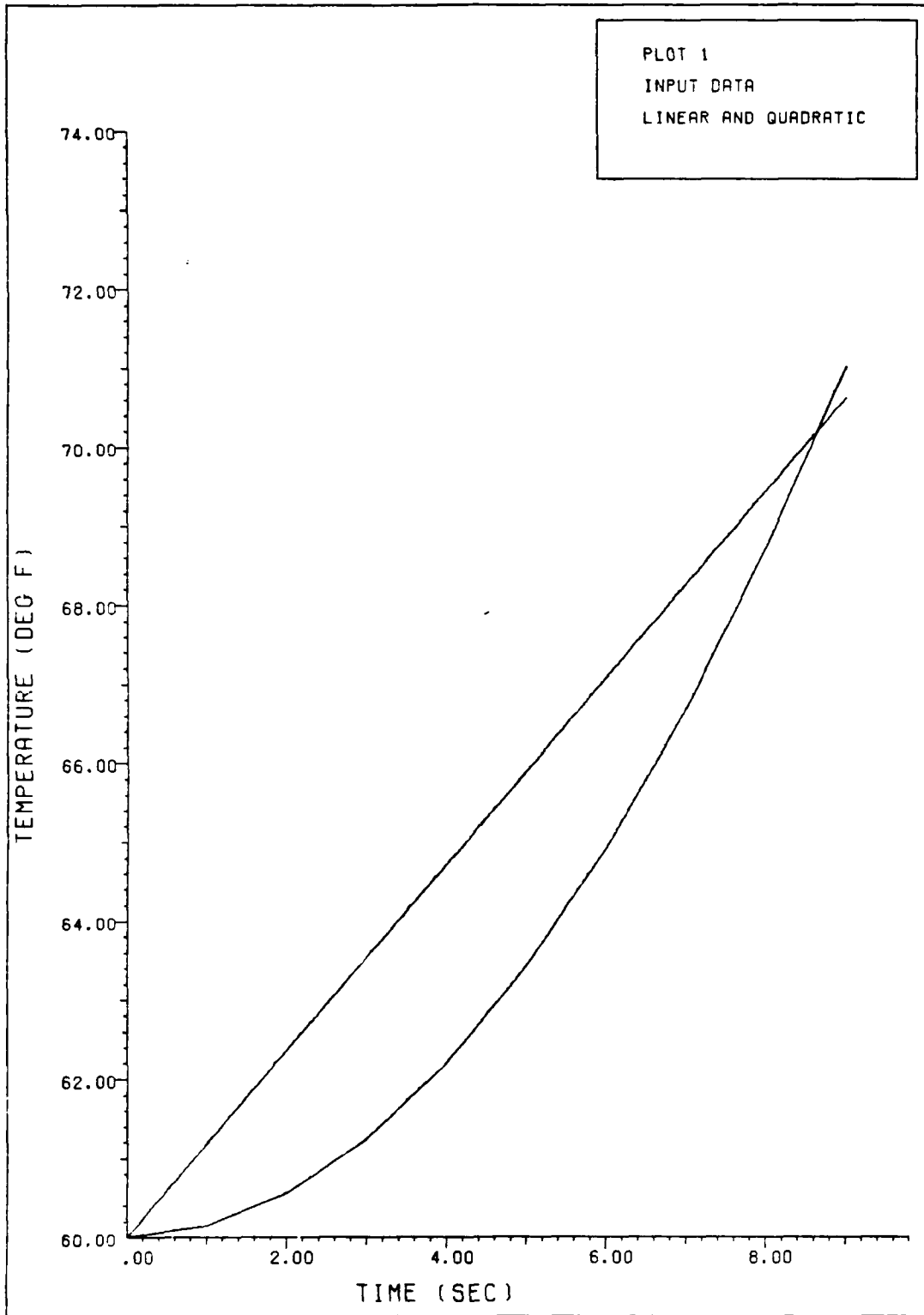


FIGURE 4.1

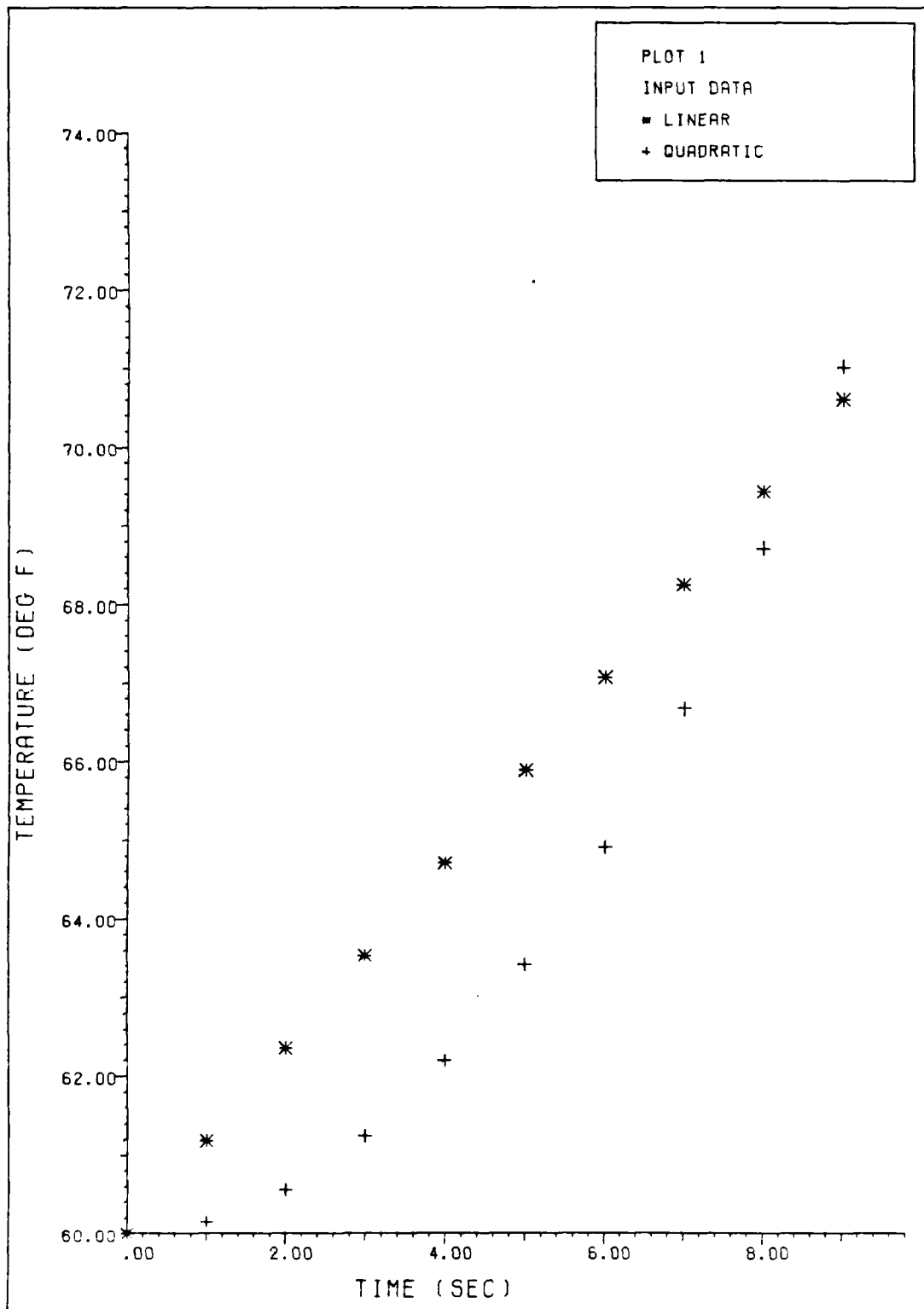


FIGURE 4.2

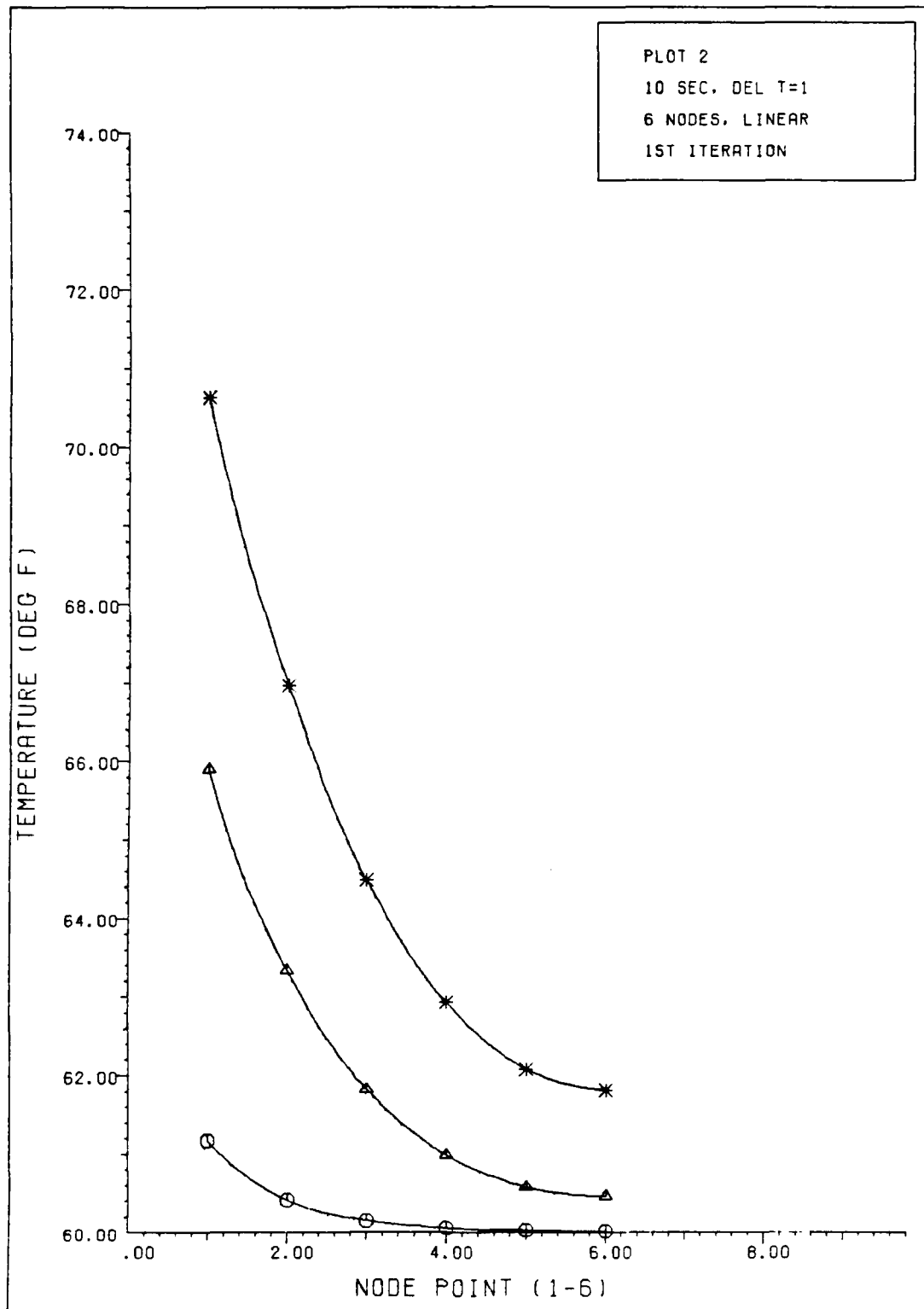


FIGURE 4.3 TEMP VS NODE POINT HISTORY (2,6,10 SEC)



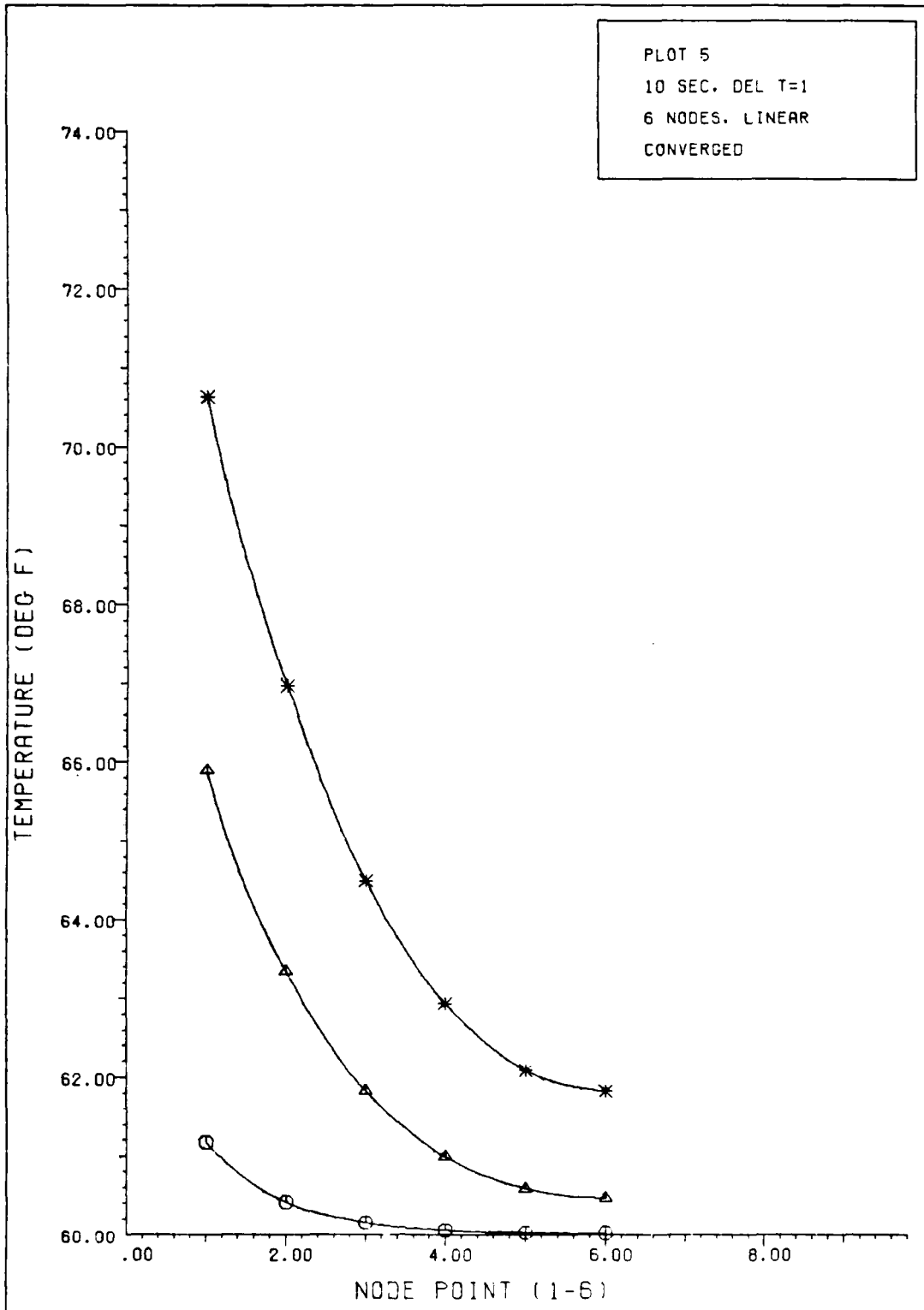


FIGURE 4.4 TEMP VS NODE POINT HISTORY (2.6, 10 SEC)

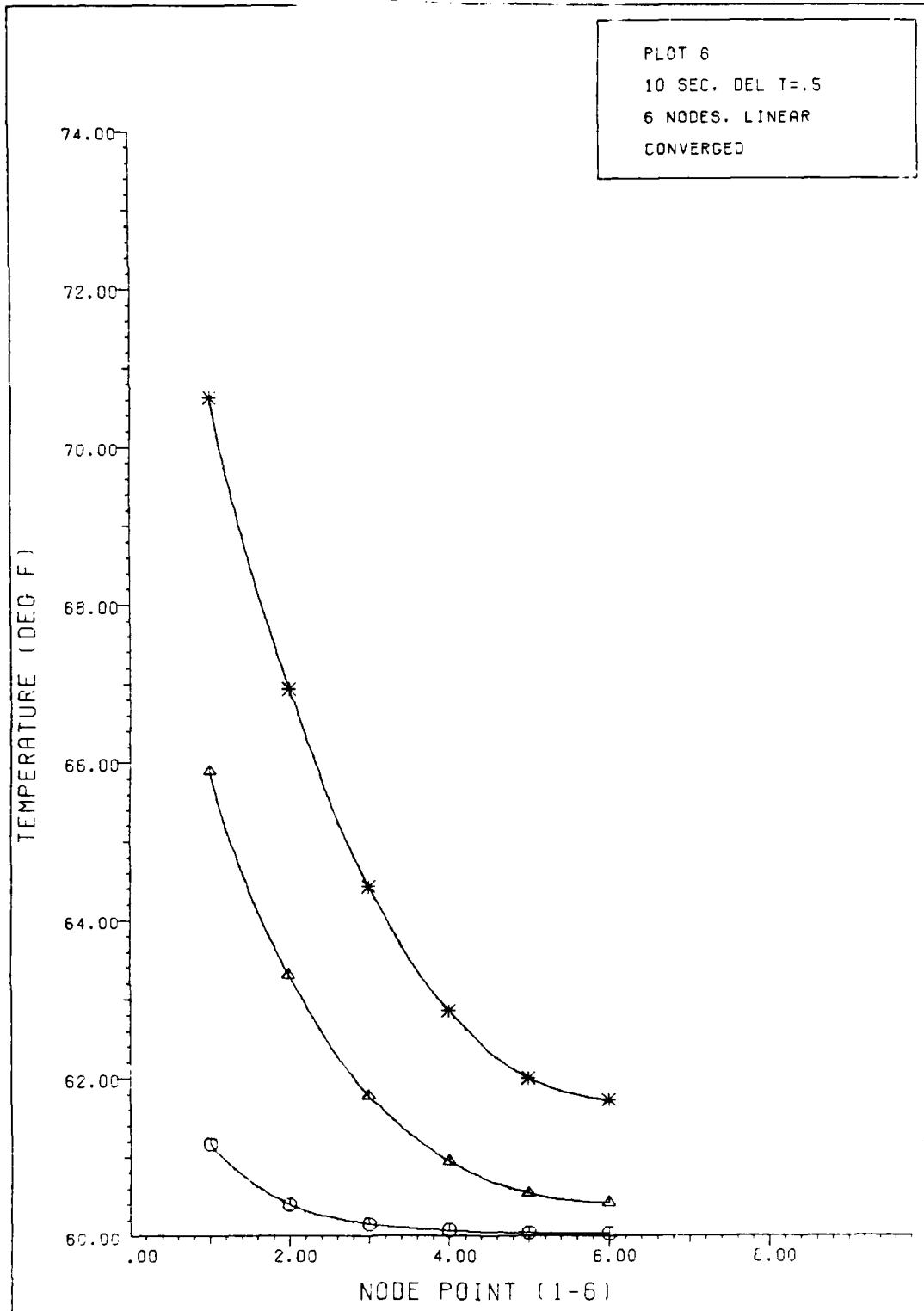


FIGURE 4.5 TEMP VS NODE POINT HISTORY (2.6, 10 SEC)

the utility of the program to be used in wind tunnel runs of much longer duration.

## 5.2 Recommendations

Actual wind tunnel test data from coaxial gages needs to be analyzed by the program to instill more confidence in the results. This would require that the data tape format be modified to be compatible with the program inputs.

Also, a prescribed model for  $h_{bar}$  as a function of angle of attack needs to be input to determine the ability of the program to estimate the piecewise linear derivatives,  $h_{\alpha 1}$  and  $h_{\alpha 2}$ . The additional input data would then be the wind tunnel model angle of attack at each thermocouple sample time.

Another potential modification to the program would be to use a second order time derivative approximation as opposed to the current first order approximation. It is suspected that the increased accuracy would improve the state estimates particularly for large time gaps in thermocouple data.

The temperature state estimates might be improved by incorporating a variable grid. An exponential grid generation scheme would concentrate node points near the surface where the largest temperature gradients exist.

A final recommendation, would be to make the program more 'user friendly' and to publish documentation much like a users manual.

## V. CONCLUSIONS AND RECOMMENDATIONS

### 5.1 Conclusions

The program works for this simplified test case of known parameters and number of node points. The ability of the program to determine the temperature state appeared very good but definite conclusions cannot be drawn without comparing this data to actual thermocouple data. The ability of the program to estimate the parameters,  $h_0$  and  $\phi_k$  was demonstrated extremely well. Re-examination of the  $\phi_c$  equations must be made before further conclusions may be made about the ability of the program to estimate this parameter. It is theoretically possible, however.

The objective, to validate the use of the modified HEATEST program for use of coaxial thermocouple gages on wind tunnel test articles, has been met for the special case of this analytical model. The program is capable of determining temperature states and estimating parameters with a high degree of accuracy. A note concerning the semi-infinite slab assumption needs to be emphasized. This assumption was made only for the data generation program to yield data for which the analytical solution was known. As mentioned in Chapter 1, some coaxial gages are available with backface temperature monitoring which would also provide another temperature measurement to enhance estimation of  $\phi_k$  and  $\phi_c$ . This feature would greatly enhance

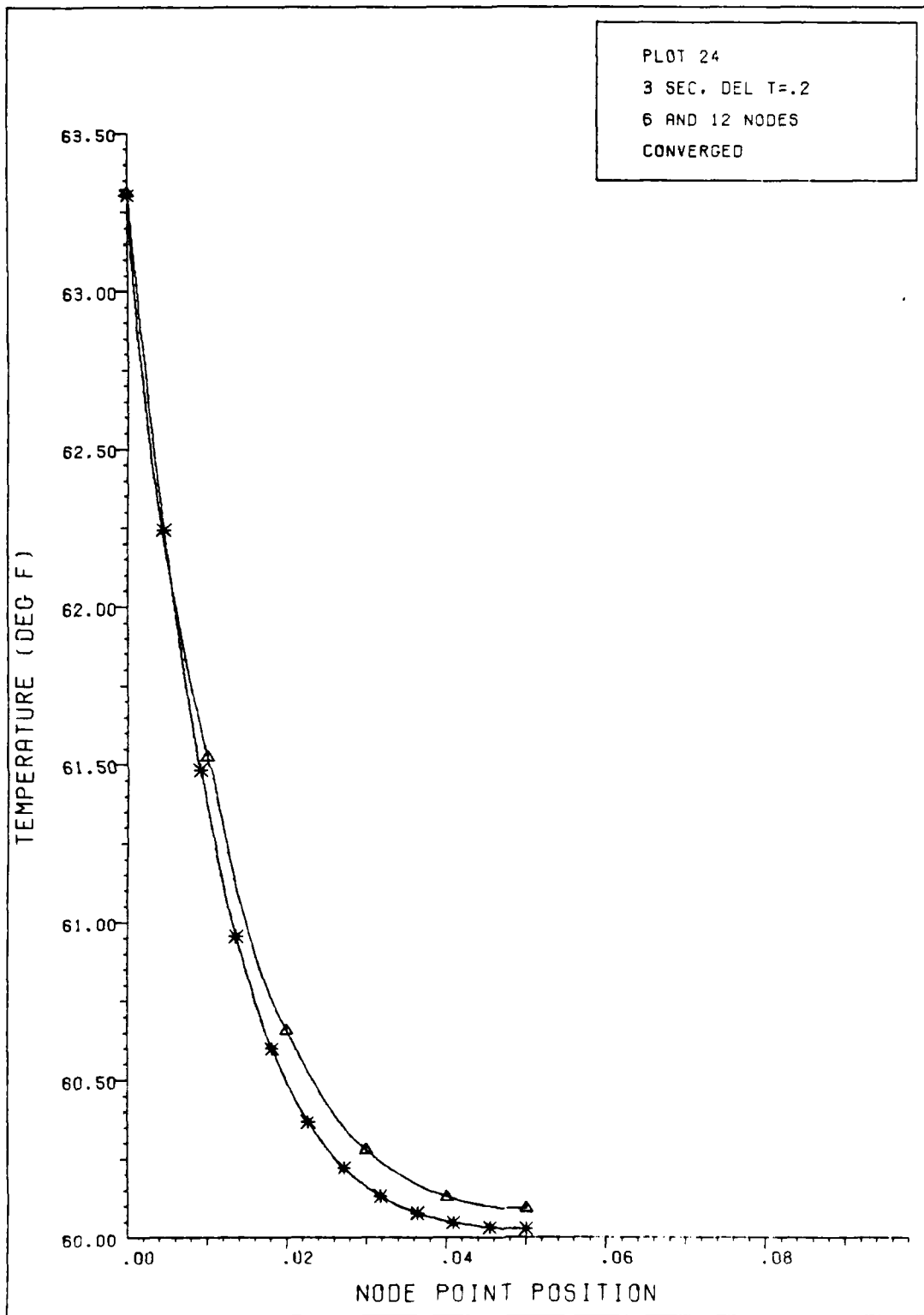


FIGURE 4.17 TEMP VS NODE POS. (6 NODES VS 12 NODES)

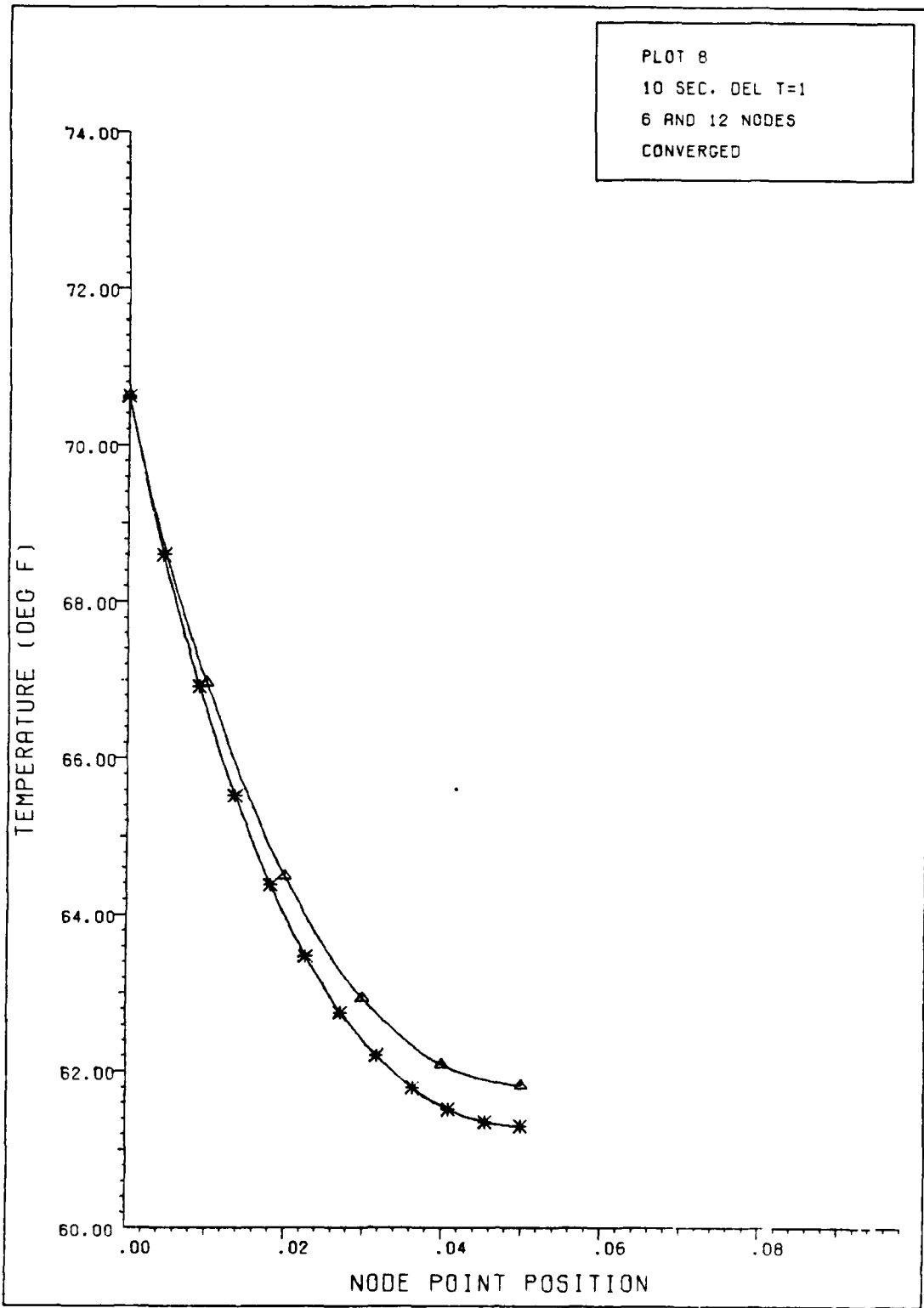


FIGURE 4.16 TEMP VS NODE POS. (6 NODES VS 12 NODES)

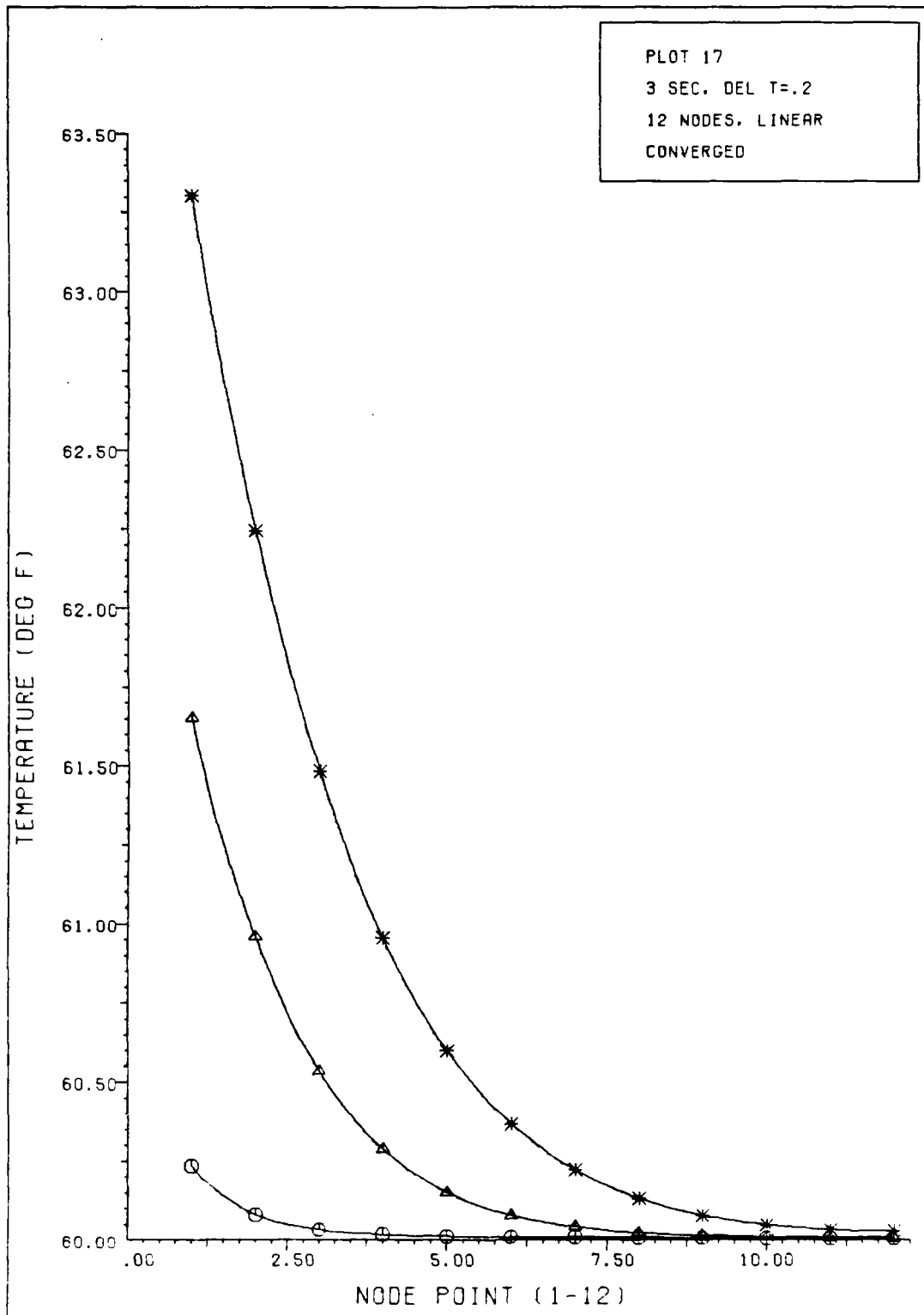


FIGURE 4.15 TEMP VS NODE POINT (.4, 1.6, 3.0 SEC.)

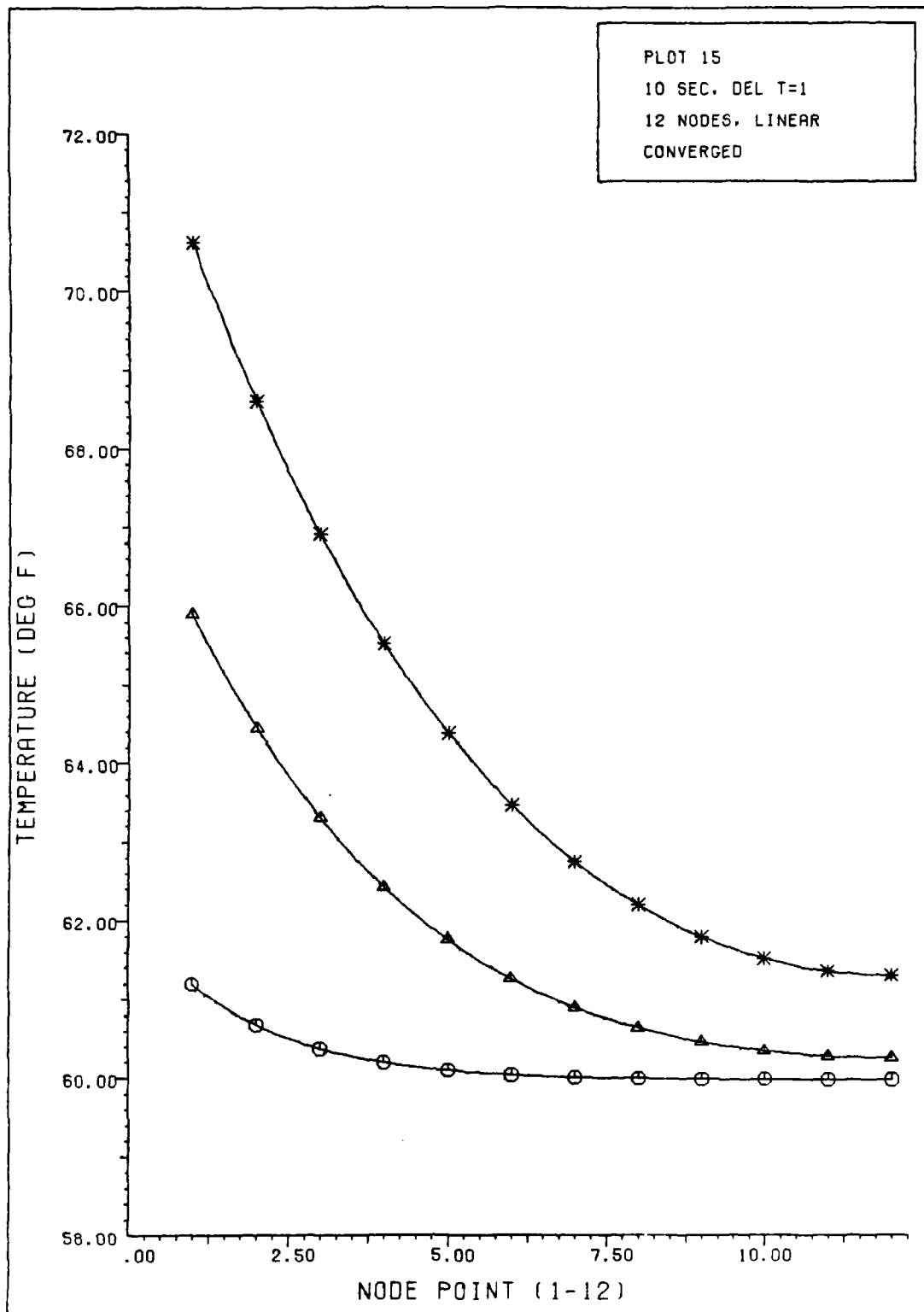


FIGURE 4.14 TEMP VS NODE POINT HISTORY(2.6.10 SEC)



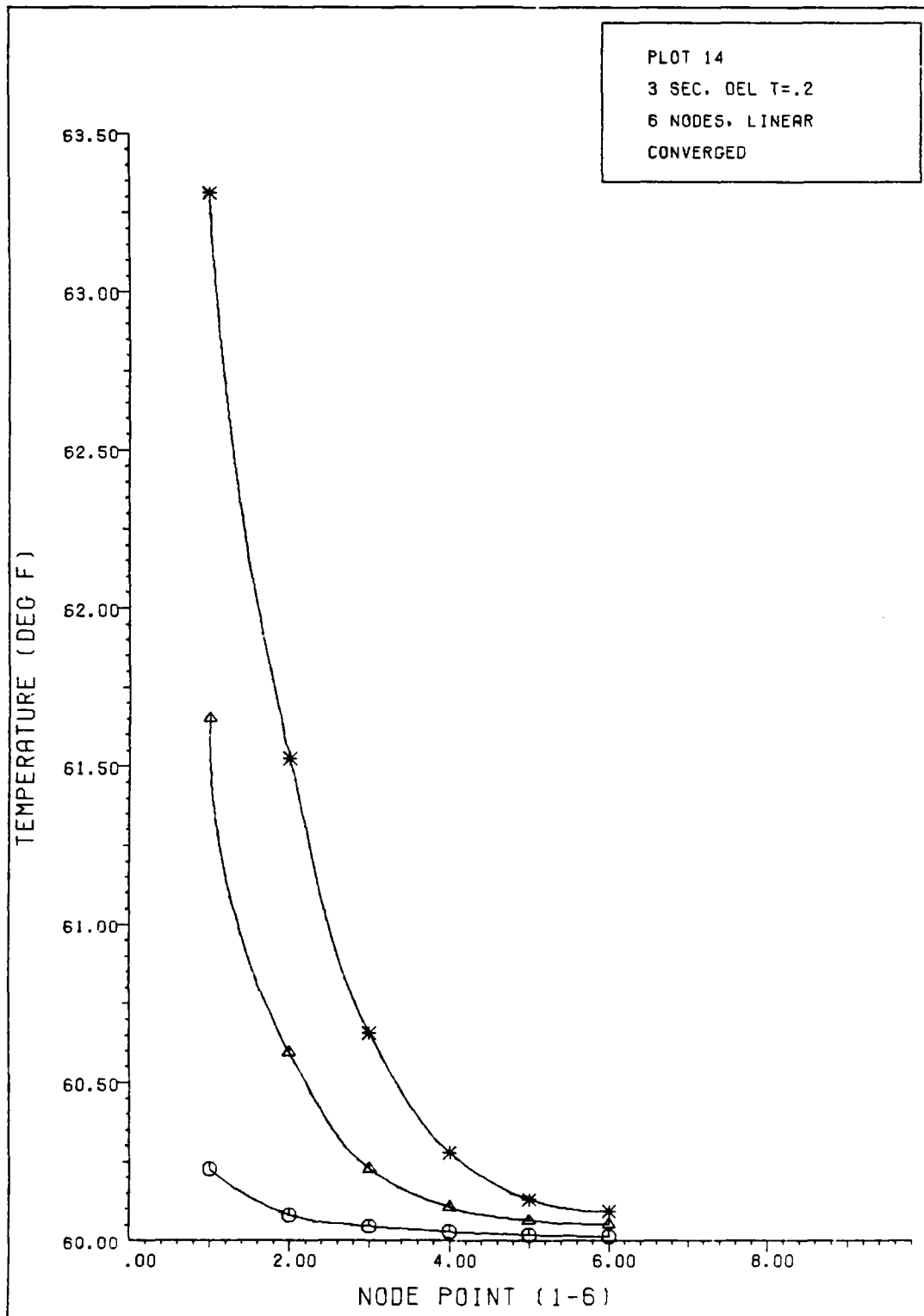


FIGURE 4.13 TEMP VS NODE POINT (.4, 1.6, 3.0 SEC)

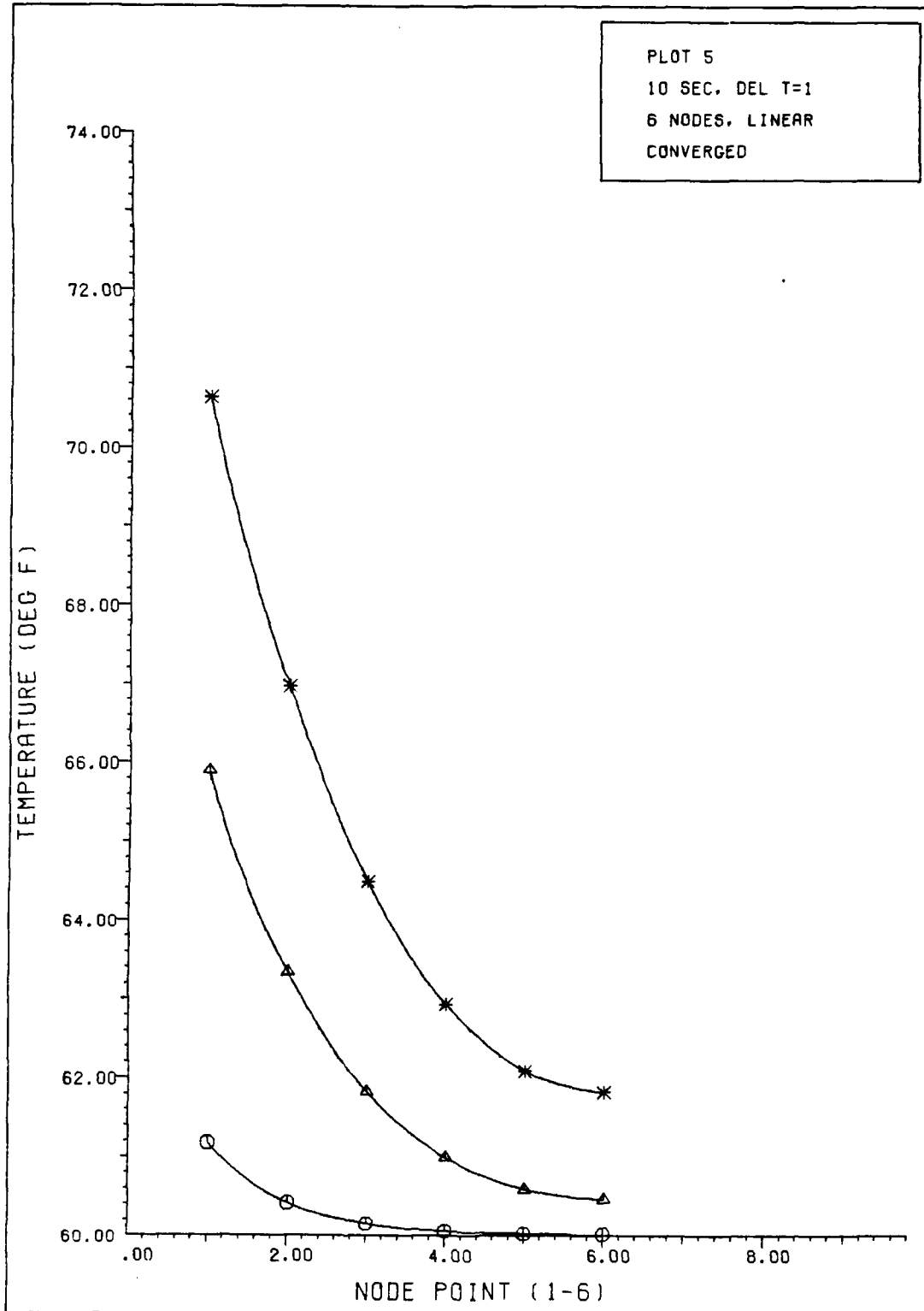


FIGURE 4.12 TEMP VS NODE POINT HISTORY(2.6,10 SEC)

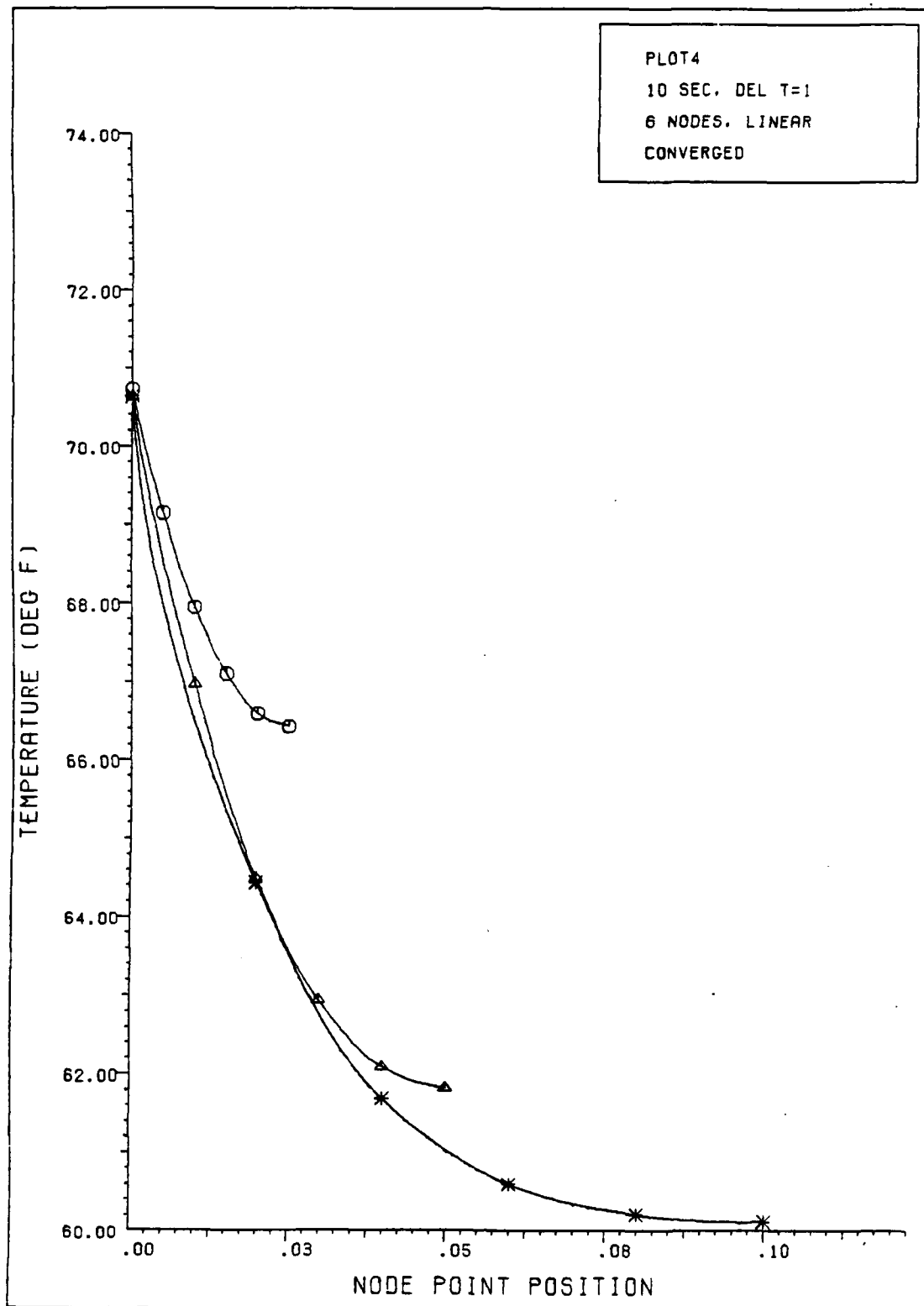


FIGURE 4.11 TEMP VS POS. (T/C LENGTH=.1,.05,.025FT)

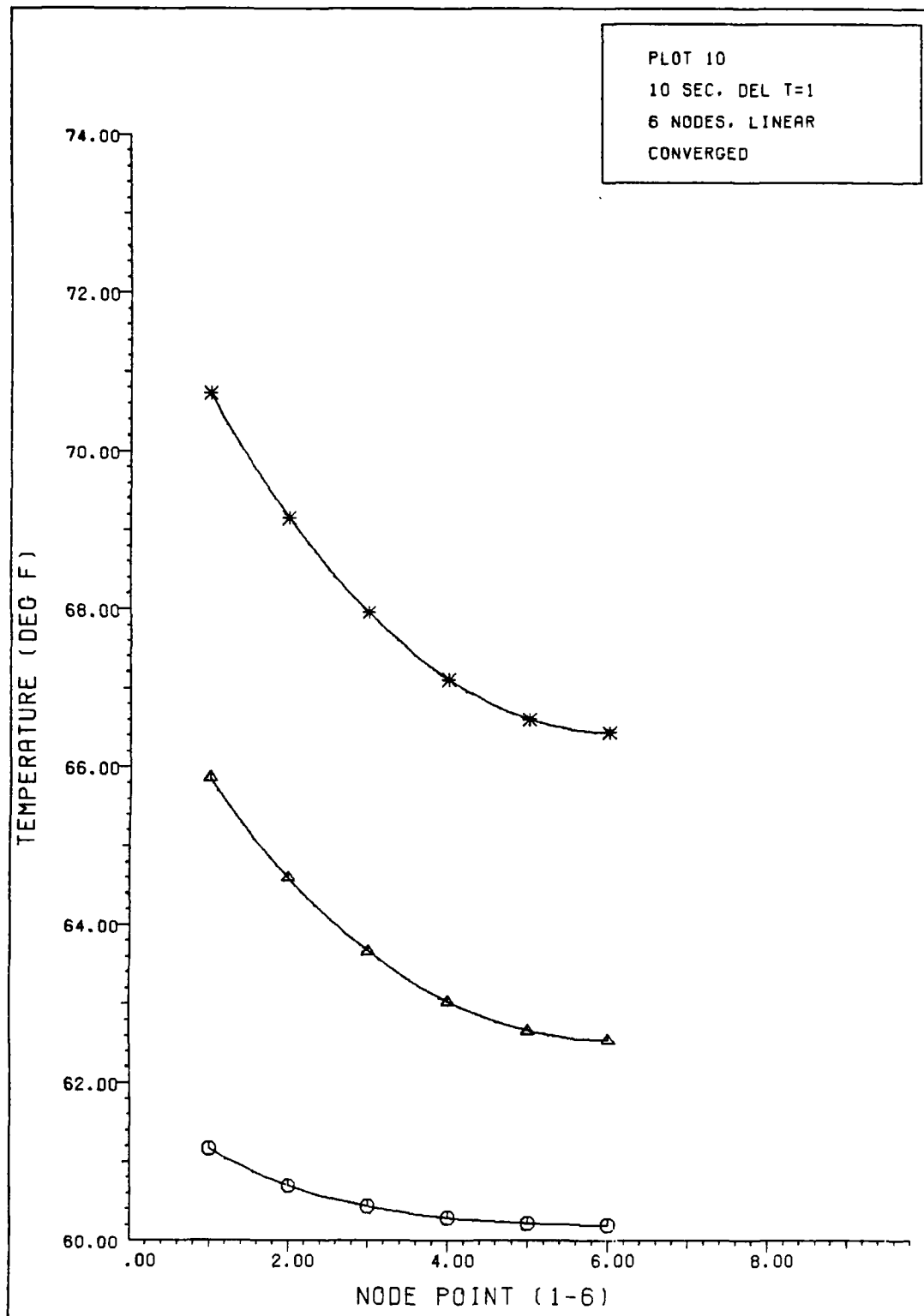


FIGURE 4.10 TEMP VS NODE POINT (T/C LENGTH=.025FT)

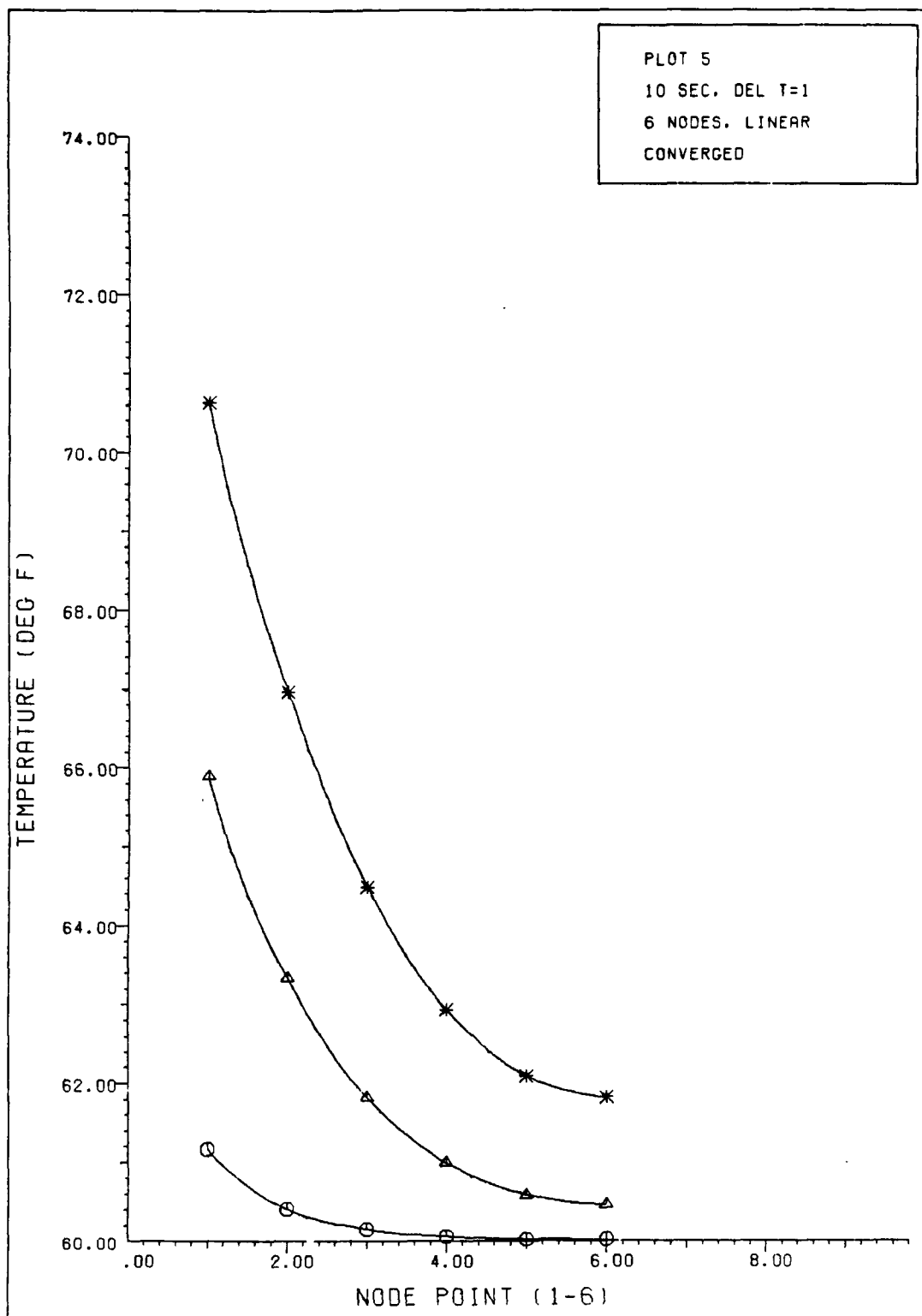


FIGURE 4.9 TEMP VS NODE POINT (T/C LENGTH= .05 FT)

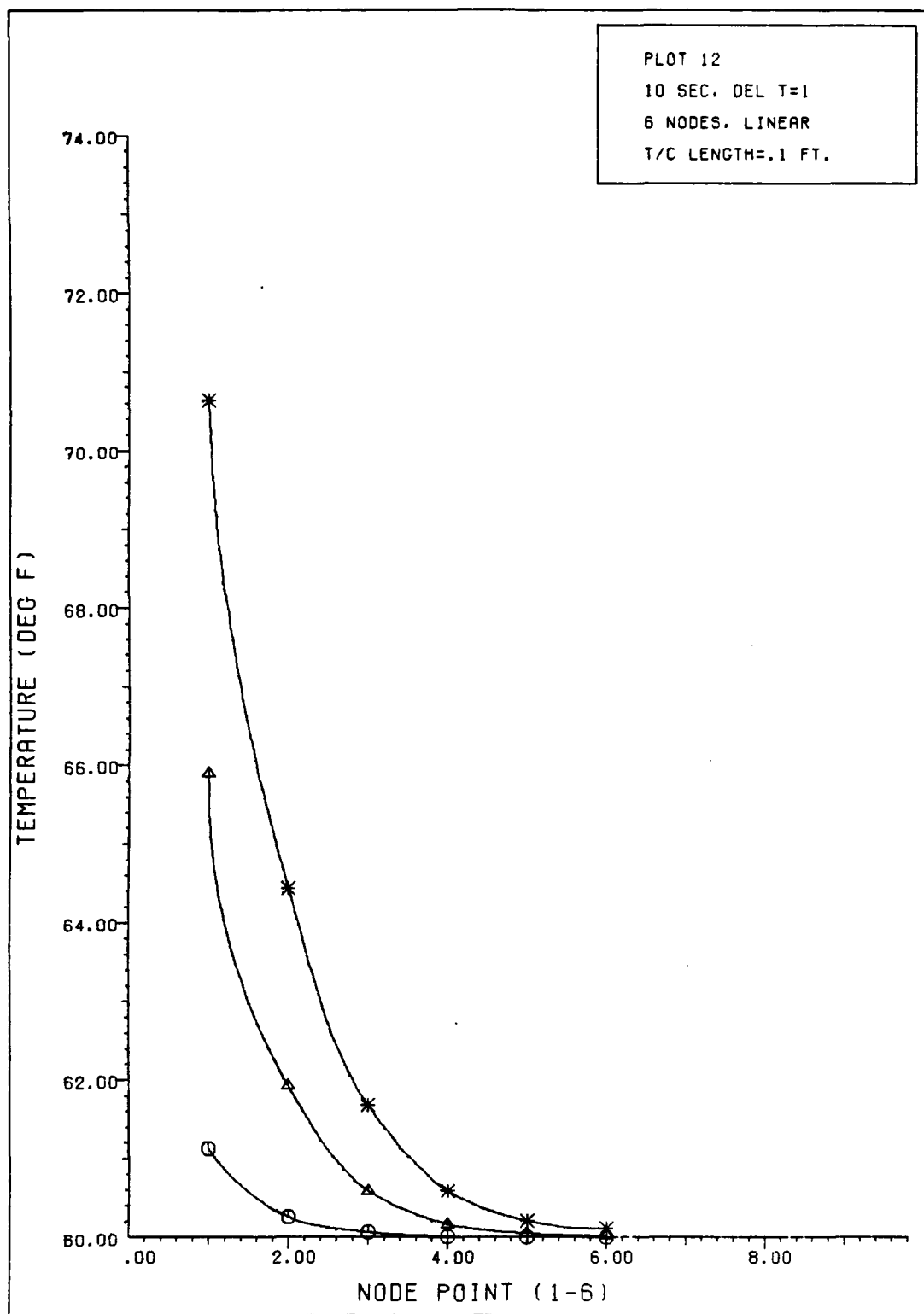


FIGURE 4.8 TEMP VS NODE POINT (T/C LENGTH= .1 FT.)

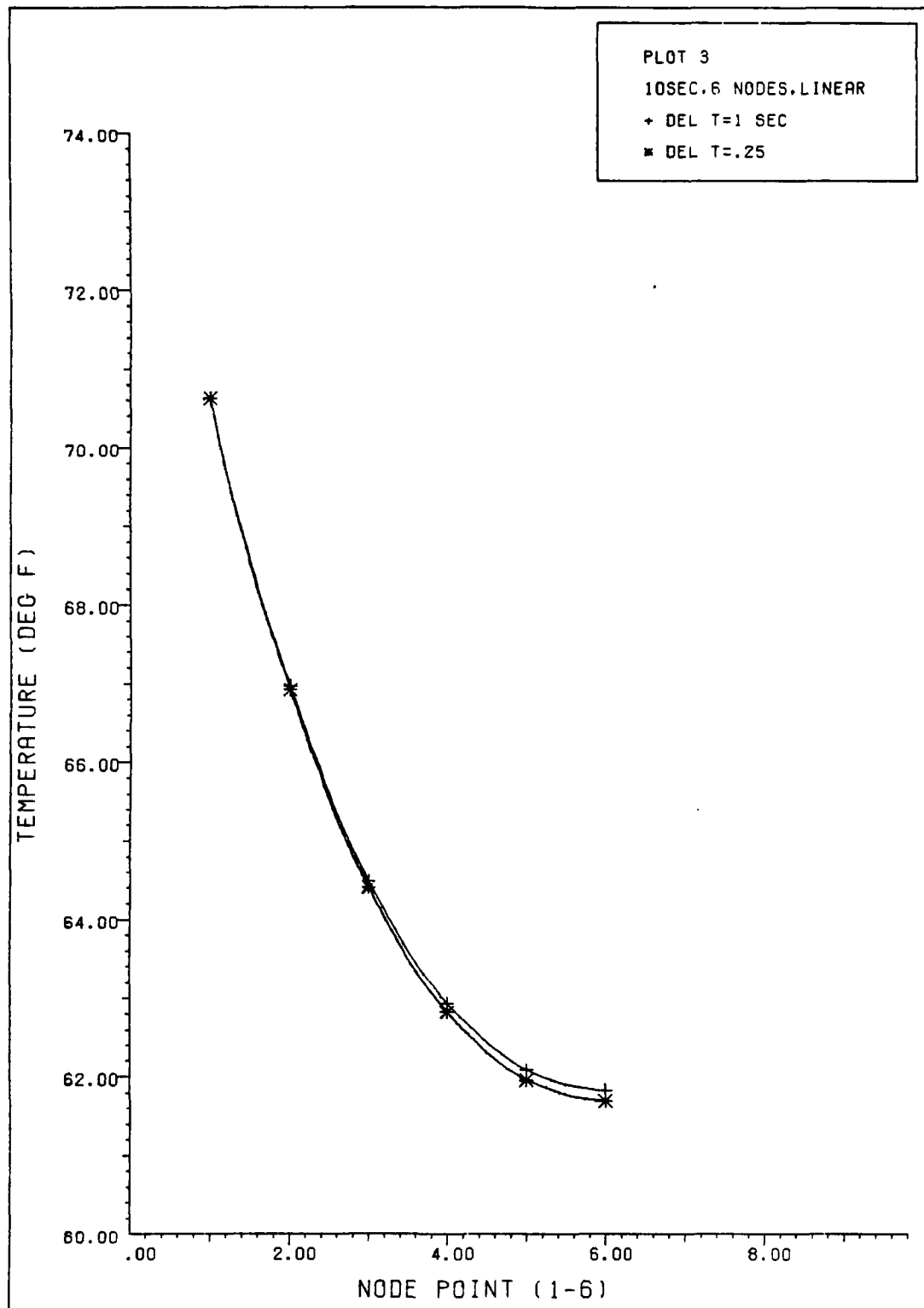


FIGURE 4.7 TEMP VS NODE POINT(DEL T=1 AND .25 SEC)

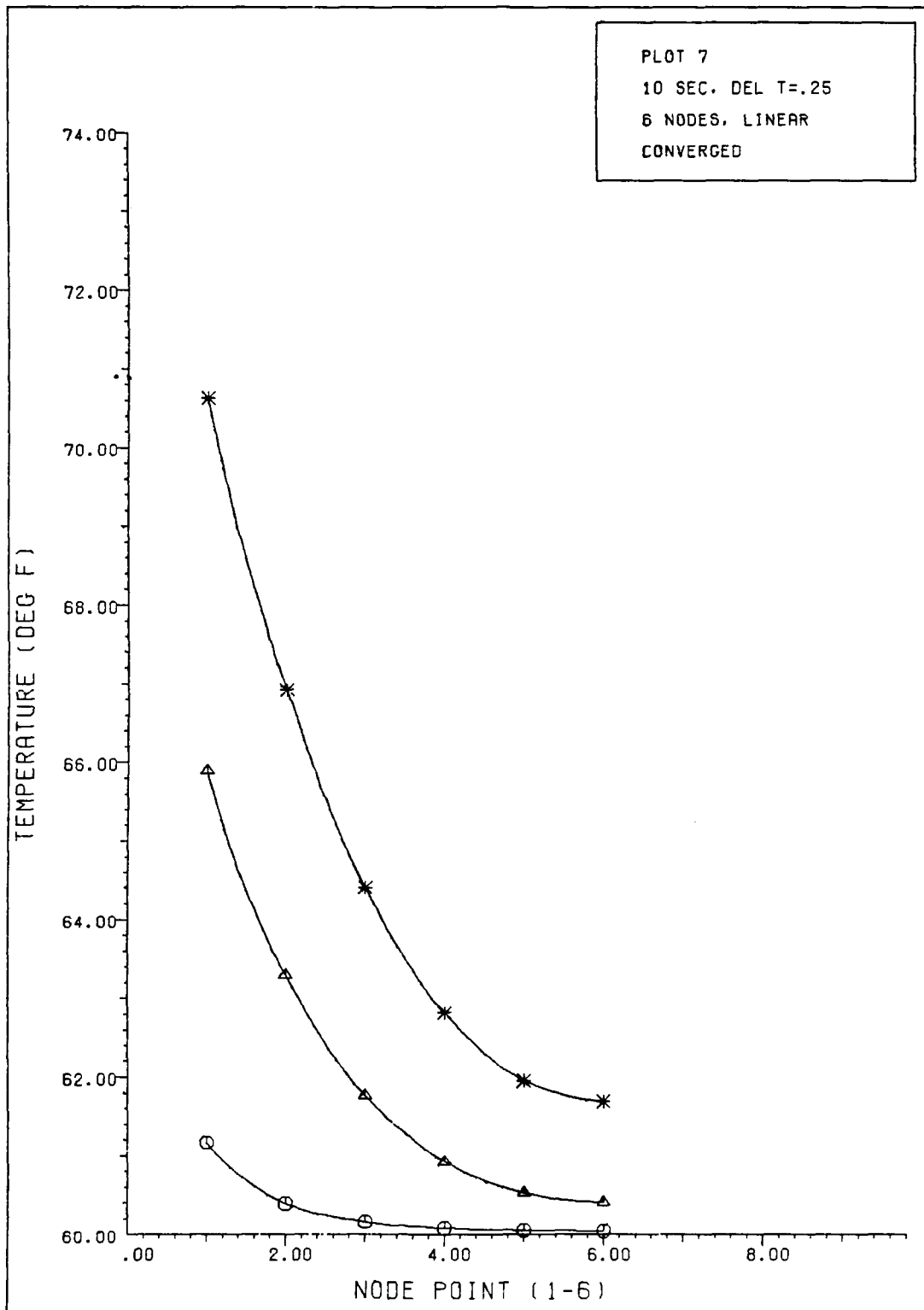
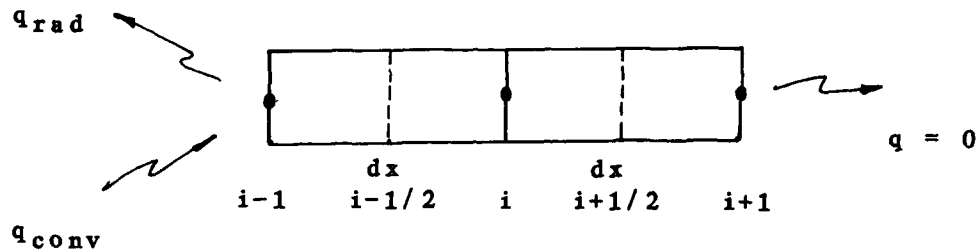


FIGURE 4.6 TEMP VS NODE POINT HISTORY (2.6, 10 SEC)



## APPENDIX A

Derivation of equations using a one-dimensional energy balance formulation are given as follows,



$$\begin{aligned}
 \text{Energy in the left face} &= -k\partial T/\partial x = q_1 \\
 \text{Energy generated within the element} &= q \, dx = 0 \\
 \text{Change in internal energy} &= \rho c(\partial T/\partial \tau) dx \\
 \text{Energy out of right face} &= -k(\partial T/\partial x)_{x+dx} \\
 &= -\left[ \frac{k\partial T}{\partial x} + \frac{\partial}{\partial x} \left( \frac{k\partial T}{\partial x} \right) dx \right]
 \end{aligned}$$

Then, combining the above and using Fourier's Law of Heat Conduction, ie,

energy in left face + energy within the element = change in internal energy + energy out right face  
yields,

$$-\frac{k\partial T}{\partial x} + qdx = \rho c \frac{\partial T}{\partial \tau} dx - \left[ \frac{k\partial T}{\partial x} + \frac{\partial}{\partial x} \left( \frac{k\partial T}{\partial x} \right) dx \right] \quad (A-1)$$

or,

$$\rho c \frac{\partial T}{\partial \tau} = \frac{\partial}{\partial x} \left( \frac{k\partial T}{\partial x} \right) \quad (A-2)$$

or, replacing T by U,

$$\rho c U_t = (k U_x)_x \quad (A-3)$$

or,

$$\rho c U_t = \left[ \frac{k_{i-1/2}}{\Delta x_{i-1/2}} (U_{i-1}^n - U_i^n) - \frac{k_{i+1/2}}{\Delta x_{i+1/2}} (U_i^n - U_{i+1}^n) \right] \frac{1}{\Delta x} \quad (A-4)$$

where  $\Delta X$  may be written as,

$$\Delta x = \frac{\Delta x_{i+1/2} + \Delta x_{i-1/2}}{2}$$

then, writing the time gradient in first order backward difference form and expanding yields,

$$\begin{aligned} \rho c \frac{U_i^n - U_{i-1}^n}{\Delta t} &= \frac{2k_{i-1/2}}{\Delta x_{i-1/2} (\Delta x_{i+1/2} + \Delta x_{i-1/2})} U_{i-1}^n \\ &- \frac{2k_{i-1/2}}{\Delta x_{i-1/2} (\Delta x_{i+1/2} + \Delta x_{i-1/2})} U_i^n \\ &- \frac{2k_{i+1/2}}{\Delta x_{i+1/2} (\Delta x_{i+1/2} + \Delta x_{i-1/2})} U_i^n \\ &+ \frac{2k_{i+1/2}}{\Delta x_{i+1/2} (\Delta x_{i+1/2} + \Delta x_{i-1/2})} U_{i+1}^n \end{aligned} \quad (A-5)$$

then, specifying equal spacing for each node point,

$$\Delta x_{i+1/2} = \Delta x_{i-1/2}$$

and the equation becomes,

$$\rho c \frac{U_i^n - U_i^{n-1}}{\Delta t} = \frac{k_{i-1/2}}{\Delta x^2} U_{i-1}^n - \left( \frac{k_{i-1/2}}{\Delta x^2} + \frac{k_{i+1/2}}{\Delta x^2} \right) U_i^n + \frac{k_{i+1/2}}{\Delta x^2} U_{i+1}^n \quad (\text{A-6})$$

Now, instead of estimating  $c$  and  $k$  directly, define two scaling parameters  $\phi_c$  and  $\phi_k$  such that  $c$  and  $k$  will remain constant. These two parameters are estimated by the HEATEST program.

$$\rho \phi_c c \Delta x \frac{U_i^n - U_i^{n-1}}{\Delta t} = \phi_k \frac{k_{i-1/2}}{\Delta x} U_{i-1}^n - \phi_k \left( \frac{k_{i-1/2}}{\Delta x} + \frac{k_{i+1/2}}{\Delta x} \right) U_i^n + \phi_k \frac{k_{i+1/2}}{\Delta x} U_{i+1}^n \quad (\text{A-7})$$

This equation is applicable at all interior ( $i \neq 1, i \neq i_{\max}$ ) points.

For the back face, assuming a semi-infinite solid,  $i = i_{\max}$  and the equation becomes,

$$\frac{\rho \phi_c c \Delta x}{2} \frac{U_L^n - U_L^{n-1}}{\Delta t} = \frac{\phi_k k_{L-1/2}}{\Delta x} U_{L-1}^n - \frac{\phi_k k_{L-1/2}}{\Delta x} U_L^n \quad (\text{A-8})$$

For the front face, ( $i = 1$ ), the effects of radiation away from and convection toward the solid surface must be accounted for.

The radiation is modeled using the Stefan-Boltzmann Law,

$$q = \epsilon\sigma(U_1^4 - U_{\infty}^4) \quad (A-9)$$

where	$\epsilon$	radiative emissivity
	$\sigma$	Stefan-Boltzmann constant
	$U$	Temperature ( $^{\circ}R$ )

The convective transfer of energy is modeled using Newton's Law of Cooling,

$$q = h(T_{aw} - T_w) \quad (A-10)$$

Non-dimensionalizing by a reference heat transfer coefficient,  $h_{ref}$  yields,

$$q = h_{bar}h_{ref}(T_{aw} - U_1) \quad (A-11)$$

where,  $h_{bar} =$  convective heat transfer coefficient ratio  
 $T_{aw} =$  adiabatic wall temp of test article

The dependance of the heat transfer coefficient on parameters other than those included in the reference heat transfer coefficient are summarized by the static transfer relation or heat transfer coefficient ratio,  $h/h_{ref}$ . Here, the ratio is assumed to be piecewise linear with respect to angle of attack as derived from Lagrange Interpolation Theory (Ref 6),

$$h_{\text{bar}} = h/h_{\text{ref}} = [h_0 + h_{a1}(\alpha - \alpha_1) + h_{a2}(\alpha - \alpha_2)] \quad (\text{A-12})$$

where  $h_0$  is the magnitude of the heat transfer coefficient,  $h$ , at the reference condition specified at  $\alpha_1$ . Combining Equations A-7, A-9, A-11, and A-12 and evaluating at node one yields,

$$\begin{aligned} \frac{\rho \phi_c \Delta x}{2} \frac{U_1^n - U_1^{n-1}}{\Delta t} &= -\frac{\phi_k k_{k+1/2}}{\Delta x} U_1^n \\ &+ \frac{\phi_k k_{k+1/2}}{\Delta x} U_2^n - \epsilon \sigma [(U_1^n)^4 - (U_{\text{db}}^n)^4] \\ &+ [h_0 + h_{a1}(\alpha - \alpha_1) + h_{a2}(\alpha - \alpha_2)] h_{\text{ref}} (T_{\text{aw}} - U_1^n) \end{aligned} \quad (\text{A-13})$$

Using the quasi-linearization as developed in Equation 2-6, the resultant form for determining the temperature time history at each node point is given in Equations 2-7 and 2-8.

The matrix form for the equations may be found after defining the following,

$$\begin{aligned} \text{RCX}_i &= \rho \phi_c \Delta x & \text{RCX}_1 &= \frac{\text{RCX}_1}{2} & \text{RCX}_L &= \frac{\text{RCX}_L}{2} \\ \text{RM}_i &= \frac{\phi_k k_{i-1/2}}{\Delta x} & \text{RM}_1 &= 0 \\ \text{RP}_i &= \frac{\phi_k k_{i+1/2}}{\Delta x} & \text{RP}_L &= 0 \end{aligned}$$



## APPENDIX B

The derivation of the sensitivity equations. The derivative of Equation 2-7 with respect to each parameter yields equations from which the HEATEST program propagates the sensitivity. A vector of parameters is formed and the sensitivity notation is as shown,

$$\Theta = [h_0, h_{a1}, h_{a2}, \rho_c, \rho_k]^T \quad S_{i,k} = \frac{\partial U}{\partial \Theta_k}$$

$\underline{\hspace{1cm}}$  parameter no  
 $\underline{\hspace{1cm}}$  node point

Defining,  $h_{\text{bar}} = [h_0 + h_{a1}(a-a_1) + (h_{a2}(a-a_2))]$ , the sensitivity equations at node one are,

$$\begin{aligned} \Theta_1: \quad & \frac{\rho \rho_c c \Delta x}{2} \frac{S_{1,1}^n - S_{1,1}^{n-1}}{\Delta t} = \frac{-\rho_k(k_{i+1/2})}{\Delta x} S_{1,1}^n \\ & + \frac{\rho_k(k_{i+1/2})}{\Delta x} S_{2,1}^n - 4\epsilon\sigma(U_1^n)^3 S_{1,1}^n + h_{\text{ref}}(T_{\text{aw}} - U_1^n) \\ & - S_{1,1}^n h_{\text{ref}} h_{\text{bar}} \end{aligned} \quad (\text{B-1})$$

$$\begin{aligned} \Theta_2: \quad & \frac{\rho \rho_c c \Delta x}{2} \frac{S_{1,2}^n - S_{1,2}^{n-1}}{\Delta t} = \frac{-\rho_k(k_{i+1/2})}{\Delta x} S_{1,2}^n \\ & + \frac{\rho_k(k_{i+1/2})}{\Delta x} S_{2,2}^n - 4\epsilon\sigma(U_1^n)^3 S_{1,2}^n \\ & + (a-a_1) h_{\text{ref}}(T_{\text{aw}} - U_1^n) - S_{1,2}^n h_{\text{ref}} h_{\text{bar}} \end{aligned} \quad (\text{B-2})$$

$$\theta_3: \frac{\rho \phi_c c \Delta x}{2} \frac{S_{1,3}^n - S_{1,3}^{n-1}}{\Delta t} = \frac{-\phi_k(k_{i+1/2})}{\Delta x} S_{1,3}^n$$

$$+ \frac{\phi_k(k_{i+1/2})}{\Delta x} S_{2,3}^n - 4\epsilon\sigma(U_1^n)^3 S_{1,3}^n$$

$$+ (\alpha - \alpha_2) h_{ref}(T_{aw} - U_1^n) - S_{1,3}^n h_{ref} h_{bar}$$

(B-3)

$$\theta_4: \frac{S_{1,4}^n - S_{1,4}^{n-1}}{\Delta t} = \frac{-2\phi_k k_{i+1/2}}{\rho \phi_c c \Delta x^2} S_{1,4}^n + \frac{2\phi_k k_{i+1/2}}{\rho \phi_c^2 c \Delta x^2} U_1^n$$

$$+ \frac{2\phi_k k_{i+1/2}}{\rho \phi_c c \Delta x^2} S_{1,4}^n - \frac{2\phi_k k_{i+1/2}}{\rho \phi_c^2 c \Delta x^2} U_2^n$$

$$- \frac{8\epsilon\sigma(U_1^n)^3}{\rho \phi_c c \Delta x} S_{1,4}^n + \frac{2\epsilon\sigma(U_1^4 - U_2^4)}{\rho \phi_c^2 c \Delta x}$$

$$- \frac{2h_{bar} h_{ref}}{\rho \phi_c c \Delta x} S_{1,4}^n - \frac{2h_{bar} h_{ref}(T_{aw} - U_1)}{\rho \phi_c^2 c \Delta x}$$

(B-4)

$$\theta_5: \frac{\rho \phi_c c \Delta x}{2} \frac{S_{1,5}^n - S_{1,5}^{n-1}}{\Delta t} = \frac{-\phi_k k_{i+1/2}}{\Delta x} S_{1,5}^n$$

$$- \frac{k_{i+1/2}}{\Delta x} U_1^n + \frac{\phi_k k_{i+1/2}}{\Delta x} S_{2,5}^n + \frac{k_{i+1/2}}{\Delta x} U_2^n$$

$$- 4\epsilon\sigma U_1^3 S_{1,5} - S_{1,5} h_{ref} h_{bar}$$

(B-5)

The sensitivity equations at the interior node points are as



follows,

$$\theta_i, \quad i = 1, 2, 3$$

$$\begin{aligned} \rho \phi_c c \Delta x \frac{S_{i,k}^n - S_{i,k}^{n-1}}{\Delta t} &= \frac{\phi_k k_{i-1/2}}{\Delta x} S_{i-1,k} \\ &- \frac{\phi_k (k_{i-1/2} + k_{i+1/2})}{\Delta x} S_{i,k} \\ &+ \frac{\phi_k k_{i+1/2}}{\Delta x} S_{i+1,k} \end{aligned}$$

(B-6)

$\theta_4$ :

$$\begin{aligned} \frac{S_{i,4}^n - S_{i,4}^{n-1}}{\Delta t} &= \frac{\phi_k k_{i-1/2}}{\rho \phi_c c \Delta x^2} S_{i-1,4}^n - \frac{\phi_k k_{i-1/2}}{\rho \phi_c^2 c \Delta x^2} U_{i-1}^n \\ &- \frac{\phi_k}{\rho \phi_c c \Delta x} \frac{(k_{i-1/2} + k_{i+1/2})}{\Delta x} S_{i,4}^n \\ &+ \frac{\phi_k}{\rho \phi_c^2 c \Delta x} \frac{(k_{i-1/2} + k_{i+1/2})}{\Delta x} U_i^n + \frac{\phi_k k_{i+1/2}}{\rho \phi_c c \Delta x^2} S_{i+1,4}^n \\ &- \frac{\phi_k k_{i+1/2}}{\rho \phi_c^2 c \Delta x^2} U_{i+1}^n \end{aligned}$$

(B-7)

$\theta_5$ :

$$\begin{aligned} \rho \phi_c c \Delta x \frac{S_{i,5}^n - S_{i,5}^{n-1}}{\Delta t} &= \frac{\phi_k k_{i-1/2}}{\Delta x} S_{i-1,5} \\ &- \frac{\phi_k (k_{i-1/2} + k_{i+1/2})}{\Delta x} S_{i,5} \end{aligned}$$

$$\begin{aligned}
& + \frac{\rho_k k_{i+1/2}}{\Delta x} S_{i+1,5} + \frac{k_{i-1/2}}{\Delta x} U_{i-1} \\
& - \frac{(k_{i-1/2} + k_{i+1/2})}{\Delta x} U_i + \frac{k_{i+1/2}}{\Delta x} U_{i+1}
\end{aligned}$$

(B-8)

The backface equations are of the same form as the node 1 equations without the convection and radiation terms.

If Equations A-14 are used to reduce the equations to the form of Equation 2-9, the sensitivity equations become,

$$[A']\{S_{i,k}\} + \{d_k\} = 0 \quad (B-9)$$

where the [A] matrix for the sensitivity equations is the same as the [A] matrix for the temperature equations, A-15. The {d} vectors for each parameter are listed as follows,

$$\{d\}_1 = \left\{ \begin{array}{l} \left( h_{ref}(T_{aw} - U_1) + \frac{RCX_1}{\Delta t} S_{1,1}^{n-1} \right) / BBB_1 \\ \left( \frac{RCX_i}{\Delta t} S_{i,1}^{n-1} \right) / BBB_i \end{array} \right\}$$

$$\{d\}_2 = \left\{ \begin{array}{l} \left( (\alpha - \alpha_1) h_{ref}(T_{aw} - U_1) + \frac{RCX_1}{\Delta t} S_{1,2}^{n-1} \right) / BBB_1 \\ \left( \frac{RCX_i}{\Delta t} S_{i,2}^{n-1} \right) / BBB_i \end{array} \right\}$$

$$\{d\}3 = \left\{ \begin{array}{l} \left( (\alpha - \alpha_2) h_{ref} (T_{aw} - U_1) + \frac{RCX_1}{\Delta t} S_{1,3}^{n-1} \right) / BBB_1 \\ \left( \frac{RCX_i}{\Delta t} S_{i,3}^{n-1} \right) / BBB_i \end{array} \right\}$$

$$\{d\}4 = \left\{ \begin{array}{l} \left( \frac{-RP_1 (U_2 - U_1) + \epsilon \sigma (U_1^4 - U_2^4) - h_{bar} h_{ref} (T_{aw} - U_1)}{\phi_c} + \frac{RCX_1 S_{i,4}^{n-1}}{\Delta t} \right) / BBB_1 \\ \left( \frac{-RM_i (U_{i-1} - U_i) + RP_i (U_i - U_{i+1}) + RCX_i S_{i,4}}{\phi_c} \right) / BBB_i \end{array} \right\}$$

$$\{d\}5 = \left\{ \begin{array}{l} \left( \frac{RP_1 (U_2 - U_1) + RCX_1 S_{i,5}^{n-1}}{\phi_k} \right) / BBB_1 \\ \left( \frac{RM_i U_{i-1} - (RM_i + RP_i) U_i + RP_i U_{i+1} + RCX_i S_{i,5}^{n-1}}{\phi_k} \right) / BBB_i \end{array} \right\}$$

(B-10)

**APPENDIX C**

The HEATEST program follows.

DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST, PL=5000  
 FTNS. I, ANSI=0, L=OUTS, LO=5/-A.

```

1  PROGRAM HEATEST (INPUT, OUTPUT, TAPE2, TAPE3, TAPE4, TAPES, TAPE8=
2  *OUTPUT, TAPE9, TAPE10, TAPE12, TAPE13, TAPE21, TAPE30)
3
4  C TAPE2 = CALCOMP PLOT FILE
5  C TAPE3 = TEMP ICS
6  C TAPE4 = MANEUVER (BET) FILE
7  C TAPE9 = TEMP IC OUTPUT FILE FROM ADAPTIVE FILTER MODE
8  C TAPE10 = ADAPTIVE TEMPERATURE/STATE ESTIMATE TIME SERIES
9  C TAPE12 = FORMATTED TIME SERIES FOR PLOT
10 C TAPE13 = THERMOCOUPLE MEASUREMENTS
11
12 REAL M1
13 REAL TW1
14 LOGICAL IFICENT, IFPLOT, IFPRINT, IFXFLG
15 COMMON /CFLAG/IFICENT, IFPLOT, IFPRINT
16 COMMON/CTCMMT/NTCT
17 COMMON/COSP/NPTSS, USI(6), PHI(6,6), NPT, PC(6,6), RR,
18 &QD(6,6), QDT(6,6), QUE(6,6), A(6,6), RCX(6), RP(6), RM(6)
19 COMMON/CSENS/SUSI(6,5), UM1(6)
20 LOGICAL FREAD(13)
21 DIMENSION CI(5)
22 LOGICAL FAUTO
23 DIMENSION FAUTO(7)
24 DIMENSION QP(5)
25 COMMON/CPARAM/HO, HALF(2), PHIC, PHIK, ZP, Z, ALPHI(2), KA, S(5),
26 &CIF(5,5), KAF, IFX(5), ACCI(5), IFXSUM, NPAR, DALPHI(2)
27 EQUIVALENCE (HO, QP(1))
28 COMMON/CONTUN/T, TAW1, ALPHA, H, V, RHO, P, TEMP, C, TRAD, RHOG,
29 &TO, TSINK, XFT, DEL, PDEL
30 COMMON/CHEAT/Q, TS, QREF, TW, M1, RENS, HBAR, HREF
31 COMMON/ICTPS2/TINIT(1), ERALOW, E
32 COMMON/CTIME/TSTART, TSTOP, DTPENT, NRPITER, ITPRAM
33 COMMON/CDX/DX(1)
34 COMMON /CONST/ XP1(13)
35 COMMON/CPARAM2/AVERROR, EQUI, UMEAS
36 COMMON /CFPLOT/IFPLOT, TSCALE, TMIN, TAXL, YSCALE, YMIN, YAXL, ASCALE, AMIN
37 *, AAXL
38 COMMON /CSMTH/ UICSM(6,6), PICSM(6,6), UAP(6), PAP(6,6),
39 &SMIC, TSMTH, W(6,6)
40 LOGICAL SMIC
41 COMMON/CKF/K(6), S1(6), J1(6,6), TC(2), NODES(2), KFOPT
42 REAL K, J1
43 COMMON/GPC/NPTPC
44 DIMENSION FLT1(2), FLT2(1)
45 EQUIVALENCE (TAW1, FLT1(1))
46 EQUIVALENCE (REF, ALPH)
47 EQUIVALENCE (TW1, TC(1))
48 DIMENSION TITLE(10)
49 DIMENSION REMARK(10)
50 DIMENSION PLAB1(12), PLAB2(12), NUM(12)
51 DIMENSION VAR(13)
52 DIMENSION PU(2), PE(2), PUF(2), PEF(2)
53 DIMENSION READ(13)
54 DATA NPAR /5/
55 DATA CLAB /1HC/
    
```

OCT10 6  
 OCT10 7  
 FHEATEST2 4  
 FHEATEST2 5  
 FHEATEST2 6  
 FHEATEST2 7  
 FHEATEST2 8  
 FHEATEST2 9  
 FHEATEST2 10  
 FHEATEST2 11  
 FHEATEST2 12  
 FHEATEST2 13  
 UPOCT09 10  
 FHEATEST2 14  
 UPOCT09 11  
 UPAUG16 9  
 UPAUG16 6  
 UPOCT09 5  
 UPAUG16 7  
 FHEATEST2 21  
 UPAUG16 10  
 CPARAM 2  
 OCT10 2  
 UPAUG16 1  
 UPAUG16 2  
 UPAUG16 3  
 UPAUG16 4  
 OCT10 3  
 COMTUN 3  
 UPAUG16 12  
 UPAUG16 13  
 FHEATEST2 30  
 UPAUG16 14  
 HAROLD 1  
 UPOCT09 12  
 FHEATEST2 34  
 FHEATEST2 35  
 UPOCT09 1  
 FCSMTH 4  
 UPAUG16 8  
 FDKF 3  
 FHEATEST2 37  
 UPAUG16 15  
 UPAUG16 16  
 UPAUG16 17  
 UPAUG16 18  
 FHEATEST2 41  
 FHEATEST2 42  
 FHEATEST2 43  
 HAROLD 2  
 UPAUG16 19  
 FHEATEST2 45  
 UPAUG16 20  
 FHEATEST2 47

```

56 DATA LABELX/SHLABEL/
57 DATA DTP/O/
58 DATA ERALOW/.5/
59 DATA KA,KAF,IPE/1,1,1,1/
60 DATA THDEP/.05/
61 DATA NPTSS/6/
62 DATA TRAD/O./
63
64 C READ INPUT DECK DATA
65 C
66 C CALL INPUT
67 C
68 C NODE POINT STRUCTURE
69 C
70 DX(1)=THDEP/NPTSS
71 NODES(1)=1
72 NODES(2)=NPTSS
73
74 C
75 C ENTER OUTER/PARAMETER ESTIMATION ITERATION LOOP
76 C
77 READ(5,3990)ITRJSK,ITCSK,NPTPC,IIC
78 FORMAT(8(18X,12))
79 READ(5,4001)INTERV,IFXFLG
80 FORMAT(6X,14,9X,11,10X,7L1)
81 DELS=(TSTOP-TSTART)/INTERV
82 TSTOPF=TSTOP
83 TSTOP=TSTART+DELS
84 IF(IFXFLG)THEN
85 READ(5,4011,END=4034)NRPITER,IFX,FAUTO,TSTOP,KFOPT,NPTPC
86 FORMAT(4X,11,5X,18I1,10X,7L1/8X,F10.5,5X,11,8X,12)
87 READ(5,4012,END=4034)FREAD,READ
88 FORMAT(3X,13L1,13F8.4)
89 DO 4016 II=1,5
90 IF(FREAD(II))QP(II)=READ(II)
91 DO 4017 I1=1,2
92 IF(FREAD(II))ALPH(II)=READ(II)
93 FORMAT(3X,7L1,7F10.5)
94 GO TO 4033
95 IFXFLG=.FALSE.
96 TSTOP=TSTOPF
97 CONTINUE
98 END IF
99 IF(TSTOP.GT.TSTOPF)TSTOP=TSTOPF
100 IFXSUM=0
101 DO 30 I=1,NPAR
102 IFXSUM=IFXSUM+IFX(I)
103 NRPIT=NRPITER+1
104 DO 198 ITPRAM=1,NRPIT
105 KA=1
106 KAF=1
107 REWIND 3
108 REWIND 4
109 REWIND 10
110 REWIND 13
111 CALL ZERO(S,NPAR,1)
112

```

```

FHEATEST2 48
FHEATEST2 49
FHEATEST2 50
FHEATEST2 52
OCT30 1
UPSEP19 2
UPSEP19 3
FHEATEST2 54
FHEATEST2 55
FHEATEST2 58
FHEATEST2 57
FHEATEST2 58
FHEATEST2 59
UPSEP19 4
OCT24 1
OCT24 2
FHEATEST2 120
FHEATEST2 121
FHEATEST2 122
FHEATEST2 123
FHEATEST2 124
FHEATEST2 125
FHEATEST2 126
FHEATEST2 127
FHEATEST2 128
FHEATEST2 129
FHEATEST2 130
FHEATEST2 131
FHEATEST2 132
FHEATEST2 133
FHEATEST2 134
FHEATEST2 135
UPSEP24 1
UPSEP24 2
FHEATEST2 138
UPSEP19 5
UPSEP19 6
FHEATEST2 141
FHEATEST2 142
FHEATEST2 143
FHEATEST2 144
FHEATEST2 145
FHEATEST2 146
FHEATEST2 147
FHEATEST2 149
FHEATEST2 150
FHEATEST2 151
FHEATEST2 152
FHEATEST2 153
FHEATEST2 154
FHEATEST2 155
FHEATEST2 156
FHEATEST2 157
FHEATEST2 158
FHEATEST2 159
FHEATEST2 160

```

DO=LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,OB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1  SUBROUTINE TPS3(DTT)
2  COMMON /CTCMNT/NTCT
3  COMMON/COMTUN/T,TAW1,ALPHA,H,V,RHD,P,TEMP,C,TRAD,RHOG,
4  &TO,TSINK,XFT,DEL,PDEL
5  COMMON /CHEAT/Q,IS,OREF,TW,M1,RENS,HBAR,HREF
6  COMMON/COSP/NPTSS,USI(6),PHI(6),NPT,PC(6),RR,
7  AQD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
8  COMMON/CSENS/SUSI(6,5),UM1(6)
9  COMMON /ICTPS2/TINIT(1),ERALLOW,E
10 COMMON /CDX/DX(1)
11 REAL M1
12 DIMENSION AAAA(6),CCCC(6),DDDD(6),G(6),W(6)
13 EQUIVALENCE (QD(1,1),AAAA(1)),(QD(1,2),CCCC(1)),(QD(1,3),DDDD(1)),
14 &(QD(1,5),G(1)),(QDT(1,1),W(1))
15 DATA SIG/4.761E-13/
16 DATA MIT/2/
17
18 C SHIFT STORAGE
19 DO 460 I=1,NPTSS
20 UM1(I)=USI(I)
21
22 C FORM TRIANGONAL MATRIX
23
24 DO 511 I=2,NPTSS
25
26   BBB=RCX(I)/DTT+RP(I)+RM(I)
27   AAAA(I)=RM(I)/BBB
28   CCCC(I)=RP(I)/BBB
29   DDDD(I)=RCX(I)*UM1(I)/DTT/BBB
30
31   511 CONTINUE
32
33 C TRIANGONAL SOLUTION
34 DO 540 M=1,MIT
35
36   BBB=RCX(1)/DTT+RP(1)+RM(1)+4.*E*SIG*(USI(1)+460.)***3.+
37   @HBAR*HREF
38   AAAA(1)=RM(1)/BBB
39   CCCC(1)=RP(1)/BBB
40   DDDD(1)=(RCX(1)*UM1(1)/DTT+E*SIG*(3*USI(1)**4+TRAD**4)+HBAR*HREF*
41   &TAW1)/BBB
42   G(1)=DDDD(1)
43   W(1)=-CCCC(1)
44
45 DO 520 I=2,NPTSS
46   W(I)=-CCCC(I)/(1+AAAA(I)*W(I-1))
47   G(I)=(DDDD(I)+AAAA(I)*G(I-1))/(1+AAAA(I)*W(I-1))
48   UNEW =G(NPTSS)
49   UERMX=ABS(UNEW-USI(NPTSS))
50   USI(NPTSS)=UNEW
51   DO 530 L=2,NPTSS
52     I=NPTSS-L+1
53     UNEW=G(I)-W(I)+USI(I+1)
54     UERMX=ABS(UNEW-USI(I))
55     UERMX=AMAX1(UERMX,UERR)
56     USI(I)=UNEW
57
58   530 CONTINUE
59   IF(UERMX.LT.ERALLOW.AND.M.GE.5)GO TO 550
60   540 CONTINUE

```

UPAUG1 11  
 UPAUG1 12  
 OCT10 13  
 COMTUN 14  
 UPAUG1 15  
 UPAUG16 16  
 UPOCT09 17  
 UPAUG16 18  
 UPAUG1 19  
 UPAUG15 20  
 FTFS3 21  
 FTFS3 22  
 UPOCT09 23  
 FTFS3 24  
 FTFS3 25  
 UPAUG1 26  
 UPAUG1 27  
 FTFS3 28  
 FTFS3 29  
 FTFS3 30  
 FTFS3 31  
 FTFS3 32  
 FTFS3 33  
 FTFS3 34  
 FTFS3 35  
 FTFS3 36  
 FTFS3 37  
 FTFS3 38  
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 FTFS3 53  
 FTFS3 54  
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 FTFS3 56  
 FTFS3 57  
 FTFS3 58  
 FTFS3 59  
 FTFS3 60  
 UPSEP12 61  
 FTFS3 62  
 FTFS3 63  
 FTFS3 64  
 FTFS3 65  
 FTFS3 66  
 FTFS3 67  
 FTFS3 68  
 FTFS3 69  
 UPAUG1 70  
 UPAUG1 71  
 UPAUG1 72  
 UPAUG1 73  
 UPAUG1 74  
 UPAUG1 75  
 UPAUG1 76  
 UPAUG1 77  
 UPAUG1 78  
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 UPAUG1 119  
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 UPAUG1 122  
 UPAUG1 123  
 UPAUG1 124  
 UPAUG1 125  
 UPAUG1 126  
 UPAUG1 127  
 UPAUG1 128  
 UPAUG1 129

```

1 56
1 57
1 58
1 59
1 60
1 61
1 62
1 63
1 64
1 65
1 66
1 67
1 68
1 69

RCX(I)=RHOG*PHIC*ZP*DX(I)*.5
RP(I)=PHIK*Z/DX(I)
RM(I)=0.
A(1,1)=-RP(I)/RCX(I)
A(1,2)=RP(I)/RCX(I)
ALINI=-(.4.*E*SIG*(USI(1)+460.))*3.+HBAR*HREF)/RCX(I)
END IF
511 CONTINUE
      A(1,1) = A(1,1)+ALINI
C
C SYSTEM MATRIX COMPLETED
C
      RETURN
      END
UPAUG1      8
UPAUG1      9
FMAKEA2    181
FMAKEA2    182
FMAKEA2    183
OCT30      14
FMAKEA2    185
FMAKEA2    186
FMAKEA2    187
FMAKEA2    193
FMAKEA2    194
FMAKEA2    195
FMAKEA2    196
FMAKEA2    197

```



DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=O,L=OUTS,LO=S/-A.

```

1  SUBROUTINE MAKEA
2  COMMON /CPLCL/IPT,PFAC
3  COMMON/COMTUN/T,TAW1,ALPHA,H,V,RHO,P,TEMP,C,TRAD,RHOG,
4  &TO,TSINK,XFT,DEL,PDEL
5  COMMON /CHEAT/Q,TS,REF,TW,M1,RENS,HBAR,HREF
6  COMMON /ICTPS2/TINIT(1),ERALOW,E
7  COMMON/COSP/NPTSS,USI(6),PHI(6,6),NPT,PC(6,6),RR,
8  &QD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
9  COMMON/CPC/NPTPC
10 LOGICAL FAUTO
11 DIMENSION FAUTO(7)
12 DIMENSION OP(5)
13 COMMON/CPARAM/HO,HALF(2),PHIC,PHIK,ZP,Z,ALPHI(2),KA,S(5),
14 &CIF(5,5),KAF,IFX(5),ACC(5),IFXSUM,NPAR,DALPH(2)
15 EQUIVALENCE (HO,OP(1))
16 COMMON/CKF/K(6),S(6),J1(6,6),TC(2),NODES(2),KFOPT
17 REAL K,J1
18 COMMON /CDX/DX(1)
19 REAL M1
20 COMMON /CTCMMT/NTCT
21 DATA SIG/4.761E-13/
22 DATA E/.3/
23 DATA HREF/1./
24 DATA RHOG/17.10603937/
25 DATA ZP/3.233477/
26 DATA Z/3.054E-3/
27
28 C SET UP LINEARIZED SYSTEM MATRIX, A
29 C
30 CALL ZERO (A(1,1),NPTSS,NPTSS)
31 DO 511 I=1,NPTSS
32 C CURRENT PASS TEMPERATURES
33 C FORM MATRIX
34 C
35 C
36 C I=NPTS
37 IF (I.EQ.NPTSS) THEN
38 RCX(I)=RHOG*PHIC*ZP*DX(1)*.5
39 RM(I)=PHIK*Z/DX(1)
40 RP(I)=0.
41 A(I,I-1)=RM(I)/RCX(I)
42 A(I,I)=-RM(I)/RCX(I)
43
44 C BLOCK B INTERIOR POINTS
45 C
46 ELSE IF ((I.GT.1).AND.(I.LT.NPTSS)) THEN
47 RCX(I)=RHOG*PHIC*ZP*DX(1)
48 RP(I)=PHIK*Z/DX(1)
49 RM(I)=PHIK*Z/DX(1)
50 A(I,I-1)=RM(I)/RCX(I)
51 A(I,I+1)=RP(I)/RCX(I)
52 A(I,I)=-A(I,I-1)-A(I,I+1)
53
54 C SURFACE NODE I=1
55 ELSE IF (I.EQ.1) THEN

```

FMAKEA2 2  
 FMAKEA2 3  
 OCT10 3  
 COMTUN 3  
 UP AUG16 40  
 UP AUG16 41  
 UP OCT09 5  
 FMAKEA2 13  
 CPARAM 2  
 OCT10 2  
 UP AUG16 1  
 UP AUG16 2  
 UP AUG16 3  
 UP AUG16 4  
 UP AUG16 8  
 FDKF 3  
 UP AUG15 2  
 FMAKEA2 18  
 UP AUG16 42  
 UP AUG16 43  
 UP AUG16 44  
 OCT20 4  
 OCT30 11  
 OCT30 12  
 OCT30 13  
 FMAKEA2 44  
 FMAKEA2 45  
 FMAKEA2 46  
 FMAKEA2 47  
 FMAKEA2 48  
 FMAKEA2 57  
 FMAKEA2 58  
 FMAKEA2 59  
 FMAKEA2 94  
 FMAKEA2 95  
 UP AUG1 1  
 UP AUG1 2  
 UP AUG1 3  
 FMAKEA2 104  
 FMAKEA2 105  
 FMAKEA2 106  
 FMAKEA2 125  
 FMAKEA2 128  
 FMAKEA2 128  
 UP AUG1 4  
 UP AUG1 5  
 UP AUG1 6  
 UP AUG1 7  
 FMAKEA2 170  
 FMAKEA2 171  
 FMAKEA2 172  
 FMAKEA2 173  
 FMAKEA2 174  
 FMAKEA2 175



FTNS. I, ANSI=0, L=OUTS, LO=S/-A.

```

1 SUBROUTINE QUEMAT
2 DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000
3 FTNS. I, ANSI=0, L=OUTS, LO=S/-A.
4
5 SUBROUTINE QUEMAT
6 COMMON /CONST/ XP1(13)
7 LOGICAL IFICENT,IFPLOT,IFPRINT
8 COMMON /CFIAG/IFICENT,IFPLOT,IFPRINT
9 COMMON/COMTUN/I,TAH1,ALPHA,H,V,RHO,P,TEMP,C,TRAD,RHOG,
10 &TO,TSINK,XFT,DEL,PDEL
11 COMMON /CICWMT/NTCT
12 COMMON /CDX/DX(1)
13 COMMON/COSP/NPTSS,USI(6),PHI(6,6),NPT,PC(6,6),RR,
14 &QD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
15 COMMON /ICTPS2/TINIT(1),ERALOW,E
16 COMMON/CSENS/SUSI(6,5),UM1(6)
17 COMMON/CKF/K(6),S1(6),J1(6,6),TC(2),NODES(2),KFOPT
18 REAL K,J1
19 COMMON /CICSTAT/TR,SDIC,SDME,SDMEA,SDBN
20 COMMON /CHEAT/Q,TS,QREF,TW,M1,RENS,HBAR,HREF
21 REAL M1
22 DIMENSION R(6,6)
23 EQUIVALENCE (QD(1,1),R(1,1))
24
25 C RR = SDMEA
26
27 C MATRIX OF SPACIAL CORRELATIONS, R
28 C SPACIAL CORRELATIONS IN RSI MUST ALLOW FOR VARIABLE NODE STRUCTURE
29 DO 200 I=1,NPTSS
30 SUMR=0.
31 DO 200 J=I,NPTSS
32 XP=SUMR/TR
33 XP=ABS(XP)
34 IF(I.EQ.1)XP1(J)=XP*TR
35 IF(XP.GT.100.)XP=100.
36 R(I,J)=EXP(-XP)
37 IF(ABS(RP(J)).LT.1.E-8)GO TO 200
38 SUMR=SUMR+RPX(J)/RP(J)
39 R(J,I)=R(I,J)
40 PRINT*,XP1=',(XP1(I),I=1,NPTSS)
41
42 C MODEL ERROR MATRIX, QUE
43
44 RC=SQRT(ABS((RCX(1)+RCX(2))*5))
45 QER=(HBAR*HREF*(TAW1-USI(1))/(RM(1)+RP(1))/2)**2
46 DO 221 I = 1, NPTSS
47
48 WHILE I.EQ.1 ADD BOUNDARY NOISE DUE TO HEAT TERMS
49 IF (I.EQ.1) THEN
50 QUE(I,I)=((SDBN*QER)**2+(SDME*QER)**2)/2
51 ELSE
52 QUE(I,I) = (SDME*QER)**2.
53 END IF
54 END WHILE
55
56 IF (I.EQ.NPTSS) GO TO 222
57 IP1 = I+1
58 DO 221 J = IP1,NPTSS
59
60 C

```

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55

2 HAROLD  
28 UPOCT09  
23 UPOCT09  
24 OCT10  
3 COMTUN  
35 UPAUG16  
38 UPAUG16  
6 UPAUG16  
5 UPOCT09  
37 UPAUG16  
7 UPAUG16  
8 UPAUG16  
3 FDKF  
15 FQUE  
38 UPAUG16  
17 FQUE  
7 UPOCT09  
19 FQUE  
20 FQUE  
21 FQUE  
22 FQUE  
23 FQUE  
24 FQUE  
25 FQUE  
28 FQUE  
27 OCT30  
9 FQUE  
29 HAROLD  
29 FQUE  
30 FQUE  
31 FQUE  
32 FQUE  
33 FQUE  
34 FQUE  
30 HAROLD  
35 FQUE  
36 FQUE  
37 FQUE  
38 FQUE  
10 OCT10  
40 FQUE  
41 FQUE  
42 FQUE  
43 FQUE  
10 OCT30  
45 FQUE  
46 FQUE  
47 FQUE  
48 FQUE  
48 FQUE  
50 FQUE  
51 FQUE  
52 FQUE  
53 FQUE

```

56 C
57 C READ CALCOMP PLOT SPECIFICATIONS
58 C
59 READ(5,1000)IPLOT
60 READ(5,2000)TSCALE,TMIN,TAXL
61 READ(5,2000)YSCALE,YMIN,YAXL
62 READ(5,2000)ASCALE,AMIN,AXL
63 1000 FORMAT(10X,12.7(3X,12))
64 C
65 C READ TIMES
66 C
67 C START-STOP TIMES / PRINT TIME STEP
68 READ(5,2000)TSTART,TSTOP,DTPEM
69 C DATA FOR I.C. SMOOTHER
70 READ(5,100)SMIC,ISMTH
71 100 FORMAT(8X,11.8X,F10.5)
72 C # OF ITERATIONS/FIX=0 FIXES PARAMETER/AUTO FLAG FOR REFERENCE
73 READ(5,2010)NRPITER,IFX,FAUTO,KFOPT
74 C NEWTON-RAPHSON ACCELERATION PARAMETERS(O)ACC(2)
75 READ(5,2015)ACC
76 C HEATING MODEL INITIAL PARAMETERS
77 READ(5,2020)(QP(II),II=1,NPAR)
78 C INITIAL REFERENCE VALUES FOR HEATING MODEL
79 READ(5,2030)ALPH
80 2010 FORMAT(5X,12.3X,5I11.5X,7L1.8X,11)
81 2015 FORMAT(5X,8F5.2/5X,8F5.2)
82 2020 FORMAT(10X,8F8.4/28X,5F8.4)
83 2030 FORMAT(10X,7F8.4)
84 RETURN
85 END

```

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FINPUT 129
FINPUT 130
FINPUT 131
FINPUT 132
FINPUT 133
FINPUT 134
FINPUT 135
FINPUT 140
FINPUT 142
FINPUT 143
FINPUT 144
FINPUT 145
FINPUT 146
CHUCK 34
UPSEP24 3
CHUCK 36
FINPUT 147
FINPUT 148
FINPUT 149
FINPUT 150
FINPUT 151
UPSEP24 4
FINPUT 153
UPSEP24 5
OCT10 8
FINPUT 156
FINPUT 157
FINPUT 158
FINPUT 159
FINPUT 160

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```

1  SUBROUTINE IC
2  LOGICAL IFICENT,IFPLOT,IFPRINT
3  COMMON /CFLAG/IFICENT,IFPLOT,IFPRINT
4  COMMON /CTCWMT/NTCT
5  COMMON /CDX/DX(1)
6  COMMON/COSP/NPTSS,USI(6),PHI(6,6),NPT,PC(6,6),RR,
7  &QD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
8  COMMON /ICTPSZ/TINIT(1),ERALLOW,E
9  COMMON/CSNS/SUSI(6,5),UM1(6)
10 COMMON/CKF/K(6),S1(6),J1(6,6),TC(2),NODES(2),KFPT
11 REAL K,J1
12 COMMON /CICSTAT/TR,SDIC,SDME,SDMEA,SDBN
13 COMMON /CHEAT/Q,TS,OREF,TW,M1,RENS,HBAR,HREF
14 REAL M1
15 DIMENSION R(6,6)
16 EQUIVALENCE (QD(1,1),R(1,1))
17
18 C INITIAL SENSITIVITIES
19 C
20 RR = SDMEA
21
22 C MATRIX OF SPACIAL CORRELATIONS, R
23 C
24 C SPACIAL CORRELATIONS IN RSI MUST ALLOW FOR VARIABLE NODE STRUCTURE
25 DO 200 I=1,NPTSS
26 SUMR=0.
27 DO 200 J=I,NPTSS
28 XP=SUMR/TR
29 XP=ABS(XP)
30 IF(XP.GT.100.)XP=100.
31 R(I,J)=EXP(-XP)
32 IF(ABS(RP(J)).LT.1.E-8)GO TO 200
33 SUMR=SUMR+RCX(J)/RP(J)
34 R(J,I)=R(I,J)
35 C
36 C COVARIANCE MATRIX OF TEMP ICS, PC
37 C
38 DO 210 I = 1,NPTSS
39 PC(I,I) = (SDIC*USI(I))**2.
40 IF (I.EQ.NPTSS) GO TO 211
41 IP1 = I+1
42 DO 210 J = IP1,NPTSS
43 PC(I,J) = USI(I)*USI(J)*SDIC**2.*R(I,J)
44 PC(J,I) = PC(I,J)
45 210 CONTINUE
46 RETURN
47 END

```

FIC 2  
 UPOCT09 21  
 UPOCT09 22  
 UPAUG16 31  
 UPAUG16 32  
 UPAUG16 6  
 UPOCT09 5  
 UPAUG16 33  
 UPAUG16 7  
 UPAUG16 8  
 FDKF 3  
 FIC 15  
 UPAUG16 34  
 FIC 17  
 UPOCT09 7  
 FIC 19  
 FIC 20  
 FIC 21  
 FIC 22  
 FIC 23  
 FIC 24  
 FIC 25  
 FIC 26  
 FIC 27  
 FIC 28  
 FIC 29  
 FIC 30  
 DCT30 8  
 FIC 32  
 FIC 33  
 FIC 34  
 FIC 35  
 FIC 36  
 FIC 37  
 FIC 38  
 FIC 39  
 FIC 40  
 FIC 41  
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 FIC 44  
 FIC 45  
 FIC 46  
 FIC 47  
 FIC 48  
 FIC 49  
 FIC 50

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56 C
57 C READ CALCOMP PLOT SPECIFICATIONS
58 C
59 READ(5,1000)IPILOT
60 READ(5,2000)TSCALE,TMIN,TAXL
61 READ(5,2000)YSCALE,YMIN,YAXL
62 READ(5,2000)ASCAL,AMIN,AAXL
63 FORMAT(10X,12,7(3X,12))
64 C
65 C READ TIMES
66 C
67 C START-STOP TIMES / PRINT TIME STEP
68 READ(5,2000)TSTART,TSTOP,DTPEM
69 C DATA FOR I.C. SMOOTHER
70 READ(5,100)SMIC,TSMTH
71 FORMAT(6X,11,8X,F10.5)
72 C # OF ITERATIONS/FIX=0 FIXES PARAMETER/AUTO FLAG FOR REFERENCE
73 READ(5,2010)NRPITER,IFX,FAUTO,KFOPT
74 C NEWTON-RAPHSON ACCELERATION PARAMETERS(O)ACC(2)
75 READ(5,2015)ACC
76 C HEATING MODEL INITIAL PARAMETERS
77 READ(5,2020)(QP(II),II=1,NPAR)
78 C INITIAL REFERENCE VALUES FOR HEATING MODEL
79 READ(5,2030)ALPH
80 FORMAT(5X,12,3X,5I11,5X,7L11,8X,11)
81 2015 FORMAT(5X,8F5.2/5X,8F5.2)
82 2020 FORMAT(10X,8F8.4/28X,5F8.4)
83 2030 FORMAT(10X,7F8.4)
84 RETURN
85 END

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129 FINPUT
130 FINPUT
131 FINPUT
132 FINPUT
133 FINPUT
134 FINPUT
135 FINPUT
140 FINPUT
142 FINPUT
143 FINPUT
144 FINPUT
145 FINPUT
146 FINPUT
34 CHUCK
3 UPSEP24
36 CHUCK
147 FINPUT
148 FINPUT
149 FINPUT
150 FINPUT
151 FINPUT
4 UPSEP24
153 FINPUT
5 UPSEP24
8 OCT10
156 FINPUT
157 FINPUT
158 FINPUT
159 FINPUT
160 FINPUT

```

DD=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE INPUT
2 LOGICAL IFICENT,IFPLOT,IFPRINT
3 CHARACTER *30 VEH,FLTDT,TMANV,CTPT
4 COMMON /CFLAG/IFICENT,IFPLOT,IFPRINT
5 COMMON/CTCMMT/NTCT
6 COMMON/CTIME/TSTART,TSTOP,DTPEENT,NRPITER,ITPRAM
7 COMMON/ICTPS2/TINIT(1),ERALOW,E
8 COMMON/CDX/DX(1)
9 LOGICAL FAUTO
10 DIMENSION FAUTO(7)
11 DIMENSION QP(5)
12 COMMON/CPARAM/HO,HALF(2),PHIC,PHIK,ZP,Z,ALPH(2),KA,S(5),
13 &CIF(S,5),KAF,IFX(5),ACC(5),IFXSUM,NPAR,DALPH(2)
14 EQUIVALENCE (HO,QP(1))
15 COMMON/CKF/K(6),S1(6),J1(6,6),TC(2),NODES(2),KFOPT
16 REAL K,J1
17 COMMON /CSMTH/ UICSM(6),PICSM(6,6),UAP(6),PAP(6,6),
18 &SMIC,TSMTH,W(6,6)
19 LOGICAL SMC
20 COMMON /CCOM/VEH,FLTDT,TMANV,CTPT
21 COMMON /CICSTAT/TR,SDIC,SDME,SDMEA,SDBN
22 COMMON /CFPLOT/IPLOT,TSCALE,TMIN,TAXL,YSCALE,YMIN,YAXL,ASCALE,AMIN
23 * ,AAXL
24
25 C READ VEHICLE/MANEUVER UNIQUES
26
27 C
28 READ(5,3000)VEH
29 FORMAT(A30)
30 READ(5,3000)FLTDT
31 READ(5,3000)TMANV
32 READ(5,3000)CTPT
33
34 C
35 READ(5,1000)NTCT
36
37 C IFICENT = T ICS FROM DISK / F CONSTANT ICS FROM CARDS
38 C IFPLOT = T CREATE CALCOMP / F NO PLOT FILE
39 C IFPRINT = T PRINT TIME SERIES / F NO TEMP TIME SERIES OUTPUT
40
41 C
42 READ(5,4000)IFICENT
43 FORMAT(8(9X,L1))
44 READ(5,4000)IFPLOT
45 READ(5,4000)IFPRINT
46 READ(5,4000)IFPRINT
47
48 C
49 READ(5,2000)F10,F10.5,(3(5X,F10.5)/10X,F10.5,3(5X,F10.5))
50
51 C
52 READ IN INITIAL TEMPERATURES (USED IF IFICENT = F)
53
54 C
55 READ(5,2000)TINIT
56
57 C
58 READ(5,2000)TINIT
59
60 C
61 INITIAL COVARIANCE AND ERROR STATISTICS
62
63 C
64 READ(5,2001)TR,SDIC,SDME,SDMEA
65 READ(5,2001)SDBN
66
67 C
68 2001 FORMAT(10X,F10.5,3(5X,F10.5))
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1 341 PRINT *, 'T, USI=', TLEST, (USI(II), II=1, NPTSS)
1 342 REWIND 3
1 343 TSTART=TSTOP
1 344 GO TO 4
1 345 END IF
346 REWIND 3
347 WRITE(3) USI, PC, SUSI
348 PRINT *, 'T, USI=', TLEST, (USI(II), II=1, NPTSS)
349 IF(IFPLOT) CALL FPLOT
350 C
351 C PLOT CALCOMP FILE FROM TAPE12
352 C
353 STOP 'END-OF-FILE ENCOUNTERED ON INPUT TAPE IN HEATEST'
354 END
355
FHEATEST2 450
FHEATEST2 451
FHEATEST2 452
FHEATEST2 453
FHEATEST2 454
FHEATEST2 455
FHEATEST2 456
FHEATEST2 457
CHUCK 32
FHEATEST2 459
FHEATEST2 460
FHEATEST2 461
FHEATEST2 462
FHEATEST2 463
FHEATEST2 464

```



```

1 284 IF(NLAB.EQ.0)GO TO 120
1 285 24 CONTINUE
1 286 GO TO 100
1 287 END IF
1 288
1 289 C PROPAGATION TO TSTOP
1 290 C
1 291 120 DELT=TSTOP-TLEST
1 292 CALL TPS3(DELT)
1 293 TLEST=TSTOP
1 294 C WRITE SMOOTHED I.CS TO TAPE3
1 295 IF(SMIC)THEN
1 296 REWIND (3)
1 297 WRITE(3) UICSM,PICSM,SUSI
1 298 REWIND (3)
1 299 IIC=1
1 300 ENDIF
1 301
1 302 C EXIT TEMPERATURE/STATE ESTIMATION LOOP
1 303 C
1 304 IF(ITPRAM.LE.NRPITER.OR.NRPITER.EQ.0) THEN
1 305 C UPDATE PARAMETER ESTIMATES - LIST RESULTS
1 306 C
1 307 CALL PAREST
1 308 IT=1
1 309 DO 197 II=1,NPAR
1 310 IF(IFX(II).EQ.0)THEN
1 311 CI(II)=0.
1 312 GO TO 197
1 313 END IF
1 314 CI(II)=SQRT(ABS(CIF(IT,IT)))
1 315 IT=II+1
1 316
1 317 197 CONTINUE
1 318 IF(ITPRAM.EQ.1)WRITE(6,3079)
1 319 FORMAT(/,1X,'ITER',T18,'HALPH1',T30,'HALPH2',T42,'PHIC',
1 320 &'T54','PHIK',T66,'ZP',T76,'Z',T88,'ALPHA1',T100,
1 321 &'ALPHA2',T112,'ALPHA3',T18,'QBETA',T18,'QLOGRE',T30,'QDELE',T42
1 322 &,'QDELEBF',T54,'QMACH',T66,'PHIKB',T1X,'(CRAMER-RAO BOUND)')
1 323 WRITE(6,3080)ITPRAM,(QP(I),I=1,10),(CI(I),I=1,10),
1 324 &(QP(I),I=11,16),(CI(I),I=11,16)
1 325 3080 FORMAT(1X,12,2X,10(F8.5,4X)/5X,10(1X,(' ',E8.2,')',1X)/
1 326 &5X,6(F8.5,4X)/5X,6(1X,(' ',E8.2,')',1X))
1 327 WRITE(6,3081)AVERAGE
1 328 3081 FORMAT(1X,'AVERAGE ERROR=',E12.5/)
1 329 C
1 330 END IF
1 331 198 CONTINUE
1 332 IIC=1
1 333 C
1 334 C
1 335 IF(SMIC) GO TO 998
1 336 IF(TSTOP.LT.TSTOPF-1.E-6)THEN
1 337 C RESET INITIAL CONDITIONS WITH FOLLOWING DATA TO DISK
1 338 C
1 339 REWIND 3
1 340 WRITE(3)USI,PC,SUSI

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FHEATEST2 342  
FHEATEST2 343  
FHEATEST2 344  
FHEATEST2 345  
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FHEATEST2 347  
FHEATEST2 348  
FHEATEST2 349  
FHEATEST2 350  
FHEATEST2 351  
CHUCK 23  
CHUCK 24  
CHUCK 27  
CHUCK 28  
CHUCK 29  
HAROLD 26  
CHUCK 30  
FHEATEST2 352  
FHEATEST2 353  
FHEATEST2 354  
FHEATEST2 355  
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FHEATEST2 358  
FHEATEST2 359  
FHEATEST2 360  
FHEATEST2 361  
FHEATEST2 362  
FHEATEST2 363  
FHEATEST2 364  
FHEATEST2 365  
FHEATEST2 366  
FHEATEST2 367  
FHEATEST2 368  
FHEATEST2 371  
OCT30 6  
OCT30 7  
FHEATEST2 374  
FHEATEST2 375  
FHEATEST2 376  
FHEATEST2 377  
FHEATEST2 378  
FHEATEST2 379  
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FHEATEST2 381  
FHEATEST2 382  
FHEATEST2 383  
FHEATEST2 384  
FHEATEST2 385  
FHEATEST2 397  
FHEATEST2 444  
CHUCK1 1  
FHEATEST2 445  
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FHEATEST2 448  
FHEATEST2 449

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C SAVE A PRIORI VALUES
DO 27 I=1,NPTSS
  UAP(I)=USI(I)
DO 27 J=1,NPTSS
  PAP(I,J)=PC(I,J)
C
DO 25 I=1,NTCT
  PU(I)=USI(NODES(I))
  PE(I)=SQRT(ABS(PC(NODES(I),NODES(I))))
25 CALL KF
  E1 = SQRT(ABS(PC(1,1)))
DO 26 I=1,NTCT
  PUF(I)=USI(NODES(I))
  PEF(I)=SQRT(ABS(PC(NODES(I),NODES(I))))
26 WRITE(9,99)I,PU(1),PE(1),PUF(1),PEF(1),TC(1)
99 FORMAT(1X,F5.2,3X,2(3X,F9.5,3X,'( ',E8.2,' )'),5X,F9.5)
98 WRITE(9,98)(USI(I),I=1,NPTSS)
98 FORMAT(11,B(F8.5,3X))
C INITIALIZE SMOOTHER
IF(ICOUNT.EQ.0)THEN
  DO 1000 I=1,NPTSS
    UICSM(I)=USI(I)
  DO 1000 J=1,NPTSS
    PICSM(I,J)=PC(I,J)
    W(I,J)=PC(I,J)
1000 W(I,J)=PC(I,J)
  ENDIF
C SMOOTH I.C.'S
TSMTH=TLEST
IF(SMIC)THEN
  IF(ICOUNT.NE.0)THEN
    CALL FPSM(TSTART)
  DO 510 IM=1,NPTSS
    VAR(IM)=SQRT(ABS(PICSM(IM,IM)))
510 VAR(IM)=SQRT(ABS(PICSM(IM,IM)))
  ENDIF
  ENDIF
C WRITE APOSTERIORI STATE ESTIMATE TO TAPE10/TAPE12
C
IF(ITPRAM.GT.NRPITER) THEN
  IF(IFPRINT)WRITE(10)1,TLEST,USI(1),E1,EQUI,PU,PE,PUF,PEF,TC.
  & Q,REF,ALPHA,BETA,RENS,DELE,DELBF,M1
  & M1
  IF(IFPLOT)WRITE(12,3095)TLEST,USI(1),EQUI,PU(1),TC(1),
  & ALPHA,BETA,RENS,DELE,DELBF,M1,QN
  TRITE=TLEST
  END IF
  DTP = 0.
C
  ICOUNT= 1
C KF UPDATE COMPLETE - SET UP FOR NEXT PROPAGATION INTERVAL
C
C UPDATE THERMAL PROPERTIES/A MATRIX BASED ON UPDATED STATES
C NOTE! PROPERTIES MAY NEED UPDATED MORE OFTEN IF TC SAMPLE RATE IS LOW
C
  CALL MAKEA
  READ NEXT THERMOCOUPLE SAMPLE
  DO 24 II=1,ITCSK
  READ(13,END=999)NLAB,TUPDT,(TC(I),I=1,NTCT)

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CHUCK 11
CHUCK 12
CHUCK 13
CHUCK 14
CHUCK 15
CHUCK 16
FHEATEST2 312
FHEATEST2 313
FHEATEST2 314
FHEATEST2 315
FHEATEST2 316
FHEATEST2 317
FHEATEST2 318
FHEATEST2 319
OCT30 2
OCT30 3
OCT30 4
OCT30 5
HAROLD 10
HAROLD 11
HAROLD 12
HAROLD 13
HAROLD 14
HAROLD 15
HAROLD 16
HAROLD 17
HAROLD 18
CHUCK 17
CHUCK 18
HAROLD 19
HAROLD 20
HAROLD 21
HAROLD 22
CHUCK 21
CHUCK 22
FHEATEST2 320
FHEATEST2 321
FHEATEST2 322
FHEATEST2 323
FHEATEST2 324
UPCOTO9 16
FHEATEST2 325
FHEATEST2 328
FHEATEST2 329
FHEATEST2 330
FHEATEST2 331
FHEATEST2 332
FHEATEST2 333
HAROLD 25
FHEATEST2 334
FHEATEST2 335
FHEATEST2 336
FHEATEST2 337
FHEATEST2 338
FHEATEST2 339
FHEATEST2 340
UPAUG24 1

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170 DO 500 IM=1,NPTSS
171 UICSM(IM)=USI(IM)
172 VAR(IM)=SORT(ABS(PC(IM,IM)))
173 PRINT*, 'UIC= ',(UICSM(IM),IM=1,NPTSS)
174 PRINT*, 'VAR= ',(VAR(IM),IM=1,NPTSS)
175 ICOUNT=0
176
177 C PROPAGATION TO TRAJECTORY SAMPLE TIME/TIMES
178
179 100 IF(T.LT.TUPDT.AND.T.LT.TSTOP)THEN
180 DELT=T-TLEST
181 CALL TPS3(DELT)
182 CALL SENS(DELT)
183 CALL TPSOSP2(DELT)
184 TLEST=T
185 DTP=DTP+DELT
186
187 C
188 C WHEN DTP.GE.DTPENT THEN WRITE TEMP/STATE ESTIMATES TO TAPE10/TAPE12
189 C
190 IF ((DTP.GE.DTPENT).AND.(ITPRAM.GT.NRPITER)) THEN
191 DTP = 0.
192 IF(IFPRINT)WRITE(6)O,TLEST,USI(1),TC(1),HBAR,HREF,ALPHA,TO
193 IF(IFPRINT)WRITE(10)O,TLEST,USI(1),EQUI,USI(NODES(1)),Q,
194 &QREF,ALPHA,BETA,RENS,DELE,DELBF,M1
195 IF(IFPLOT)WRITE(12,3055)TLEST,USI(1),EQUI,USI(NODES(1)),TC(1),
196 ALPHA,BETA,RENS,DELE,DELBF,M1,QN
197 3055 FORMAT(BE13.7)
198 TRITE=TLEST
199 END IF
200
201 C READ NEXT TRAJECTORY SAMPLE
202 DO 22 I1=1,ITRJSK
203 READ(4,END=999)NLAB,T,(FLT1(I),I=1,NLAB)
204 IF(NLAB.EQ.0)T=TSTOP
205 22 CONTINUE
206 CALL HEATTUN
207 GO TO 100
208 END IF
209
210 C PROPAGATION TO THERMOCOUPLE SAMPLE TIME/TIMES
211 C
212 IF(TUPDT.LE.TSTOP)THEN
213 DELT=TUPDT-TLEST
214 CALL TPS3(DELT)
215 CALL SENS(DELT)
216 CALL TPSOSP2(DELT)
217 TLEST=TUPDT
218 DTP=DTP+DELT
219 IF(TUPDT.GE.T)THEN
220 DO 23 I1=1,ITRJSK
221 READ(4,END=999)NLAB,T,(FLT1(I),I=1,NLAB)
222 IF(NLAB.EQ.0)T=TSTOP
223 23 CONTINUE
224 CALL HEATTUN
225 END IF
226
227 C KALMAN UPDATES
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113 CALL ZERO(CIF,NPAR,NPAR)
114 IF(IIC.EQ.O)CALL ZERO(SUSI,NPTSS,NPAR)
115
116 C READ C & B FILE LABEL ON TRAJ TAPE
117 C
118 READ(4)C,LIC,ITAIL,TITLE,ITEST,FLT,DFLT,DREQ,DCOM
119 33 IF(EOF(4).NE.O.)CALL EXIT
120 IF(C.NE.CLAB)CALL EXIT
121 READ(4)LABEL,NRSECT,NREM,(REMARK(I),I=1,NREM),NLAB,
122 *(PLAB1(I),PLAB2(I),NUM(I),I=1,NLAB)
123 IF(LABEL.NE.LABELX)CALL EXIT
124
125 C READ C & B FILE LABEL ON THE T/C MEAS TAPE
126 C
127 7 READ(13)C,LIC,ITAIL,TITLE,ITEST,FLT,DFLT,DREQ,DCOM
128 44 IF(EOF(13).NE.O.)CALL EXIT
129 IF(C.NE.CLAB)CALL EXIT
130 READ(13)LABEL,NRSECT,NREM,(REMARK(I),I=1,NREM),NLAB,
131 *(PLAB1(I),PLAB2(I),NUM(I),I=1,NLAB)
132 IF(LABEL.NE.LABELX)CALL EXIT
133
134 C SET TEMPERATURE INITIAL CONDITIONS
135 C
136 IF(IIC.EQ.O)THEN
137 C INITIAL TEMPERATURES
138 C
139 DO 403 I=1,NPTSS
140 403 USI(I)=TINIT(I)
141 IF(IFICENT)THEN
142 READ(3)USI
143 END IF
144 IF(IIC.NE.O)THEN
145 REWIND 3
146 READ(3)USI,PC,SUSI
147 REWIND 3
148 END IF
149 EQUI=USI(1)
150
151 C INITIALIZE SMOOTHER
152 C INITIALIZE PARAMETERS AT TSTART
153 DTP=0
154 TLEST=TSTART
155 C READ FIRST TRAJECTORY SAMPLE
156 10 READ(4,END=999)NLAB,T,(FLT1(I),I=1,NLAB)
157 IF(NLAB.EQ.O)GO TO 999
158 IF(T.LT.TSTART)GO TO 10
159 C CALCULATE REFERENCE HEATING
160 CALL HEATTUN
161 C READ FIRST THERMOCOUPLE SAMPLES AND LOCAL PRESSURE
162 20 READ(13,END=999)NLAB,TUPDT,(TC(I),I=1,NTCT)
163 IF(NLAB.EQ.O)GO TO 999
164 IF(TUPDT.LT.TSTART)GO TO 20
165 C INITIALIZE THERMAL PROPERTIES/A MATRIX
166 CALL MAKEA
167 IF(IIC.EQ.O)CALL IC
168 CALL QUEMAT
169 C
170
171 FHEATEST2 161
172 FHEATEST2 162
173 FHEATEST2 163
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271 FHEATEST2 261

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```
56 IF(UERMX.GT.ERALDW)WRITE(6,1000)ERALDW,N.T,UERMX,USI(1)
57   FORMAT(1X,15HMAX ERROR TEMP~,E12.6,2X,12,2X,4(E12.6,1X))
58   CONTINUE
59   RETURN
60   END
130 FTPS3
131 FTPS3
132 FTPS3
133 FTPS3
134 FTPS3
```



```

58 IF(IP, EQ. 4) THEN
59 DDD(1)=DDD(1)-RP(1)*(USI(2)-USI(1))-(HBAR*HREF*(TAW1-
60 &USI(1))+E*SIG*((USI(1)+460.)*4-TRAD**4))/PHIC
61 DO 533 I=2, NPTSS-1
62 DDD(I)=DDD(I)-(RM(I)*(USI(I-1)-USI(I))+RP(I)*(USI(I)-USI(
63 &I+1)))/PHIC
64 DDD(NPTSS)=DDD(NPTSS)+RM(NPTSS)*(USI(NPTSS-1)-USI(NPTSS))/PHIC
65 END IF
66 C SENSITIVITY FOR CONDUCTIVITY FACTOR PHIK
67 IF(IP, EQ. 5) THEN
68 DDD(1)=DDD(1)+RP(1)*(USI(2)-USI(1))/PHIK
69 DO 534 I=2, NPTSS-1
70 DDD(I)=DDD(I)+(RM(I)*USI(I-1)-(RM(I)+RP(I))*USI(I)+RP(I)
71 &*USI(I+1))/PHIK
72 DDD(NPTSS)=DDD(NPTSS)+RM(NPTSS)*(USI(NPTSS-1)-USI(NPTSS))/PHIK
73 END IF
74 DO 535 I=1, NPTSS
75 AAA(I)=AA(I)/BB(I)
76 CCC(I)=CC(I)/BB(I)
77 DDD(I)=DDD(I)/BB(I)
78 C
79 C TRIAGONAL SOLUTION
80 C ELIMINATION STEP
81 G(1)=DDD(1)
82 W(1)=-CCC(1)
83 DO 536 I=2, NPTSS
84 W(I)=-CCC(I)/(1.+AAA(I)*W(I-1))
85 G(I)=(DDD(I)+AAA(I)*G(I-1))/(1.+AAA(I)*W(I-1))
86 C BACKWARD SUBSTITUTION
87 SUSI(NPTSS, IP)=G(NPTSS)
88 DO 537 L=2, NPTSS
89 I=NPTSS-L+1
90 SUSI(I, IP)=G(I)-W(I)*SUSI(I+1, IP)
91 CONTINUE
92 RETURN
93 END

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UPAUG1 37  
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FSENS3 124  
FSENS3 125  
FSENS3 126

DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1  SUBROUTINE PAREST
2  LOGICAL FAUTO
3  DIMENSION FAUTO(7)
4  DIMENSION QP(5)
5  COMMON/CPARAM/HO,HALF(2),PHIC,PHIK,ZP,Z,ALPH(2),KA,S(5),
6  &CIF(5,5),KAF,IFX(5),ACC(5),IFXSUM,NPAR,DALPH(2)
7  EQUIVALENCE (HO,QP(1))
8  COMMON/ICTPS2/TINIT(1),ERALOW,E
9  COMMON/CDX/DX(1)
10 COMMON/CTIME/TSTART,TSTOP,DTPTENT,NRPITER,ITPRAM
11 COMMON/MAIN2/IMA2
12 DIMENSION CIFI(6,6)
13 DATA KIN,KOUT/5,6/
14 IMA2=16
15 NR=IFXSUM
16 IF(NR.EQ.1)THEN
17 CIF(1,1)=1./CIF(1,1)
18 GO TO 20
19 END IF
20
21 C INVERT CONDITIONAL INFORMATION MATRIX,CIF
22 CALL GMINV(NR,NR,CIF,CIFI,MR,1)
23 DO 15 IR=1,NR
24 DO 15 IC=1,NR
25 CIF(IR,IC)=CIFI(IR,IC)
26 IT=1
27 DO 29 IP=1,NPAR
28 IF(IFX(IP),EQ.0)GO TO 29
29 JT=1
30 DO 28 JP=1,NPAR
31 IF(IFX(JP),EQ.0)GO TO 28
32 QP(IP)=QP(IP)+CIF(IT,JT)*S(JT)
33 JT=JT+1
34 CONTINUE
35 IT=IT+1
36 CONTINUE
37 RETURN
38 END
    
```

FPAREST 2  
 CPARAM 2  
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 UPAUG16 1  
 UPAUG16 2  
 UPAUG16 3  
 UPAUG16 4  
 UPSEP24 7  
 UPSEP24 8  
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 UPSEP24 9  
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 UPSEP24 10  
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 FPAREST 42



74/855 OPT=0,ROUND= A/ S/ M/ -D, -DS FTN 5,1+587  
 DO=LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE KF
2 LOGICAL IFICENT, IFPLOT, IFPRINT
3 COMMON /CSMTH/ UICSM(6), PICSM(6,6), UAP(6), PAR(6,6),
4 &SMIC, TSMTH, W(6,6)
5 COMMON /CFLAG/IFICENT, IFPLOT, IFPRINT
6 COMMON /CTCMNT/NTCT
7 COMMON /CPC/NPTPC
8 LOGICAL FAUTO
9 DIMENSION FAUTO(7)
10 DIMENSION QP(5)
11 COMMON/CPARAM/HO, HALF(2), P4IC, PHIK, ZP, Z, ALPH(2), KA, S(5),
12 &CIF(5,5), KAF, IFX(5), ACC(5), IFXSUM, NPAR, DALPH(2)
13 EQUIVALENCE (HO, QP(1))
14 COMMON /ICTPSZ/TINIT(1), ERALOW, E
15 COMMON /CDX/DX(1)
16 COMMON/CSENS/SUSI(6,5), UM1(6)
17 COMMON/COSP/NPTSS, USI(6), PHI(6,6), NPT_PC(6,6), RR,
18 &QD(6,6), QDT(6,6), QUE(6,6), A(6,6), RCX(6), RP(6), RM(6)
19 COMMON/CTIME/TSTART, TSTOP, DTENT, NRPITER, ITPRAM
20 COMMON/CPARAM2/AVERROR, EQUI, UMEAS
21 COMMON/CKF/K(6), S1(6), J1(6,6), TC(2), NODES(2), KFOPT
22 REAL K, J1
23 COMMON /MAIN1/INP, IPVT(6), WORK(6)
24 INP=6
25
26 SDMEA=RR
27
28 C THE FOLLOWING CONTROL CONSTRUCT SORTS KF UPDATE ITERATIONS
29 C REQUIRED BY VECTOR UPDATES AS SPECIFIED IN THE INPUT DECK
30 C
31 DO 98 I=1, NPTSS
32 DO 5 IIT=1, NTCT
33 IF(I.EQ.NODES(IIT)) THEN
34 NODE=NODES(IIT)
35 UMEAS=TC(IIT)
36 GO TO 10
37 END IF
38 CONTINUE
39 GO TO 98
40 ERROR=UMEAS-UAP(NODE)
41
42 IF(KAF.EQ.1) AVERROR=ERROR
43 AVERROR=((KAF-1)*AVERROR+ERROR)/KAF
44 KAF=KAF+1
45
46 C SCORE RUNNING SUMS FOR JACOBIAN OF LIKELIHOOD FN. S.
47 C AND CONDITIONAL INFORMATION MATRIX, CIF
48 C
49 R=(SDMEA*UMEAS)**2.
50
51 DO 26 KO=1, NPAR
52 S1(KO)=SUSI(NODE, KO)*IFX(KO)*ERROR/(PC(NODE, NODE)+R)
53 DO 25 L=1, NPAR
54 J1(KO, L)=-SUSI(NODE, KO)*IFX(KO)*IFX(L)*SUSI(NODE, L)/(PC(NODE, NODE)+
55 *R)
    
```

FKFSUM 2  
 FKFSUM 3  
 OCT10 11  
 OCT10 12  
 UPOCT09 25  
 UPSEP24 12  
 FKFSUM 8  
 CPARAM 2  
 OCT10 2  
 OCT10 2  
 UPAUG16 1  
 UPAUG16 2  
 UPAUG16 3  
 UPAUG16 4  
 UPAUG24 3  
 UPAUG24 4  
 UPAUG16 7  
 UPAUG16 6  
 UPOCT09 5  
 FKFSUM 16  
 UPOCT09 26  
 UPAUG16 8  
 FDKF 3  
 OCT10 4  
 OCT10 5  
 FKFSUM 21  
 FKFSUM 22  
 FKFSUM 23  
 FKFSUM 24  
 FKFSUM 25  
 FKFSUM 26  
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 FKFSUM 36  
 FKFSUM 37  
 HAROLD 38  
 FKFSUM 39  
 FKFSUM 40  
 FKFSUM 41  
 FKFSUM 42  
 FKFSUM 43  
 FKFSUM 44  
 FKFSUM 45  
 FKFSUM 46  
 FKFSUM 47  
 FKFSUM 48  
 FKFSUM 49  
 FKFSUM 50  
 FKFSUM 51  
 FKFSUM 52  
 FKFSUM 53

```

56 CONTINUE
57 IT=1
58 DO 29 IP=1,NPAR
59 IF(IFX(IP).EQ.0)GO TO 29
60 S(IT)=S1(IP)+S(IT)
61 JT=1
62 DO 28 JP=1,NPAR
63 IF(IFX(JP).EQ.0)GO TO 28
64 CIF(IT,JT)=J1(IP,JP)+CIF(IT,JT)
65 JT=JT+1
66 CONTINUE
67 IT=IT+1
68 CONTINUE
69
70 C COMPUTE KALMAN GAIN, K
71 C
72 DO 30 IK=1,NPTSS
73 K(IK)=PAP(IK,MODE)/(PAP(NODE,MODE)+R)
74 C IF KOPT=1 UPDATE
75 C IF KOPT=2 UPDATE EXCEPT ON LAST ITERATION(ITPRAM-NRPIITER)
76 C IF KOPT=3 DO NOT UPDATE
77 C IF KOPT=4 UPDATE COVARIANCE AND SENSITIVITY ONLY
78 C IF KOPT=5 ONLY UPDATE TEMP ON LAST ITERATION
79 C IF KOPT=8 ONLY UPDATE ON LAST ITERATION
80 GO TO(101,102,103,104,101,101)KFOPT
81
82
83 C STATE UPDATE
84
85 101 IF(KFOPT.GE.6.AND.ITPRAM.LE.NRPIITER)GO TO 103
86 IF(KFOPT.EQ.5.AND.ITPRAM.LE.NRPIITER)GO TO 104
87 DO 40 IO=1,NPTSS
88 USI(IO)=USI(IO)+K(IO)*(UMEAS-UAP(NODE))
89
90 C SENSITIVITY UPDATE
91 C
92 104 CONTINUE
93 DO 35 IP=1,NPAR
94 DO 35 L=1,NPTSS
95 35 SUSI(L,IP)=SUSI(L,IP)-K(L)*SUSI(NODE,IP)
96
97 C COVARIANCE UPDATE, PC - JOSEPH FORM
98 NPTSS=NPTC
99
100 CALL ZERO(QD(1,1),NPTSS,NPTSS)
101 DO 50 IC=1,NPTSS
102 QD(IC,IC) = 1.0
103 QD(IC,MODE) = QD(IC,MODE)-K(IC)
104 CALL MAT4(NPTSS,NPTSS,PC(1,1),QD(1,1),QD(1,1))
105 CALL MAT4(NPTSS,1,R,K(1),QD(1,1))
106 DO 55 IPC=1,NPTSS
107 DO 55 JPC=1,NPTSS
108 PC(IPC,JPC) = QD(IPC,JPC)+QD(IPC,JPC)
109 NPTSS=INP
110 98 CONTINUE
111 103 CONTINUE
112 RETURN

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FKFSUM 54  
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FKFSUM 100  
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FKFSUM 110

113

END

FKFSUM 111

DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS.I,ANSI=O,L=OUTS,L0=S/-A.

```

1  SUBROUTINE FPSM(TSTART)
2  COMMON /CONST/ XP1(13)
3  COMMON /CTCHMT/NTCT
4  COMMON /CSMTH/ UICSM(6),PICSM(6,6),UAP(6),PAP(6,6),
5  &SMIC,TSMTH,W(6,6)
6  LOGICAL SMIC
7  COMMON/COSP/NPTSS,USI(6),PHI(6,6),NPT,PC(6,6),RR,
8  &QD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
9  COMMON/CKF/K(6),S1(6),J1(6,6),TC(2),NODES(2),KFOPT
10 REAL K,J1
11 DIMENSION RINV(8,8),HTR(6,8),SFP(6,6),GAIN(6),
12 &WRK1(6,6),WRK2(6,6)
13 COMMON /MAIN1/INP,IPVT(6),WORK(6)
14 INP=6
15
16 C THIS ROUTINE IS A FIXED POINT SMOOTHER ALGORITHM
17 C
18 CALL ZERO(SFP,NPTSS,NPTSS)
19 DO 10 I=1,NTCT
20 SFP(NODES(I),NODES(I))=1./((RR+TC(I))**2).
21
22 C FORM I-SP AND FIND PHIT
23 CALL MMUL(SFP,PC,NPTSS,NPTSS,NPTSS,WRK1)
24 DO 30 I=1,NPTSS
25 DO 30 J=1,NPTSS
26 WRK1(I,J)=-WRK1(I,J)
27 IF(I.EQ.J)WRK1(I,J)=1.0+WRK1(I,J)
28 WRK2(I,J)=PHI(J,I)
29 DO 35 I=1,NPTSS
30 DO 35 J=1,NPTSS
31 PHI(I,J)=WRK2(I,J)
32
33 C FORM W=W*PHIT*(I-SP)
34 CALL MMUL(PHI,WRK1,NPTSS,NPTSS,NPTSS,WRK2)
35 CALL MMUL(W,WRK2,NPTSS,NPTSS,NPTSS,WRK1)
36 DO 40 I=1,NPTSS
37 DO 40 J=1,NPTSS
38 W(I,J)=WRK1(I,J)
39
40 C SOLVE FOR COVARIANCE -- P=P-W(S*PAP*S + S)WTRAN
41 CALL MMUL(PAP,SFP,NPTSS,NPTSS,NPTSS,WRK1)
42 CALL MMUL(SFP,WRK1,NPTSS,NPTSS,NPTSS,WRK2)
43 DO 50 I=1,NPTSS
44 DO 50 J=1,NPTSS
45 WRK1(I,J)=WRK2(I,J)+SFP(I,J)
46 CALL TRI(NPTSS,WRK1,W,PHI,WRK2,NPTSS)
47 DO 60 I=1,NPTSS
48 DO 60 J=1,NPTSS
49 PICSM(I,J)=PICSM(I,J) - WRK2(I,J)
50
51 C SOLVE FOR SMOOTHED STATE (SCALAR UPDATES)
52 DO 150 I=1,NPTSS
53 DO 110 ITT=1,NTCT
54 IF(I.EQ.NODES(ITT))THEN
55 NODE=NODES(ITT)
56

```

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    UMEAS=TC(IJT)
    GO TO 120
    ENDIF
110 CONTINUE
    GO TO 150
120 R=(RR*UMEAS)**2.
C
C COMPUTE GAIN
    DO 121 IJ=1,NPTSS
121 GAIN(IJ)=W(IJ,NODE)/R
C
C UPDATE
    DO 125 IO=1,NPTSS
    TCONST=TSTART+XP1(IO)
    IF(TSMTH .GT. TCONST) GO TO 125
    UICSM(IO)=UICSM(IO)+GAIN(IO)*(UMEAS-UAP(NODE))
125 CONTINUE
150 RETURN
    END
FPSMIC 57
FPSMIC 58
FPSMIC 59
FPSMIC 60
FPSMIC 61
FPSMIC 62
FPSMIC 63
FPSMIC 64
FPSMIC 65
FPSMIC 66
FPSMIC 67
FPSMIC 68
FPSMIC 69
HAROLD 50
HAROLD 51
HAROLD 52
HAROLD 53
FPSMIC 71
FPSMIC 72
FPSMIC 73

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SUBROUTINE MULT(X, Y, N, Z, N2)  
DIMENSION X(N2, N2), Y(N2, N2), Z(N2, N2)  
DO 20 I=1, N  
DO 20 J=1, N  
Z(I, J)=0.  
DO 20 K=1, N  
20 Z(I, J)=Z(I, J)+X(I, K)*Y(K, J)  
RETURN  
END
```

MULT  
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MULT



```

1  SUBROUTINE FUNCT(R,S,T,F,MM)
2  DIMENSION T(MM,MM),F(MM,MM)
3  INTEGER R,S
4  REAL EXP
5  DO 10 I=R,S
6  THE IF-BLOCK GIVES 14-DIGIT ACCURACY WITHOUT UNDERFLOW
7  IF( T(I,I) .LT. -43.) THEN
8  F(I,I)=0.
9  ELSE
10 F(I,I)=EXP( T(I,I) )
11 END IF
12 CONTINUE
13 PROCESS THE KTH SUPERDIAGONAL
14 N=S-R+1
15 NN=N-1
16 NN = NUMBER OF SUPERDIAGONALS IN THE BLOCK
17 IF(NN .EQ. 0) RETURN
18 DO 13 K=1,NN
19 LL=S-K
20 DO 12 I=R,LL
21 DIFF=T(I,I)-T(I+K,I+K)
22 IF(ABS(DIFF) .EQ. 0.0) GO TO 14
23 G=T(I,I+K)*(F(I,I)-F(I+K,I+K))
24 KK=K-1
25 IF(KK .EQ. 0) GO TO 12
26 IF(KK .EQ. 1) KK
27 DO 11 M=1,KK
28 G=G+(F(I,I+M)*T(I+M,I+K)-T(I,I+K-M)*F(I+K-M,I+K))
29 F(I,I+K)=G/DIFF
30 CONTINUE
31 RETURN
32 MM=MM
33 RETURN
34 END
  
```



74/855 OPT=0 ROUND=A/S/M/D DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST. PL=5000  
COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST. PL=5000  
PRINT OUTS LO=S/-A.

2 HOR  
3 QHR  
4 QHR  
5 QHR  
6 QHR  
7 QHR  
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56 QHR

SUBROUTINE HOR(IGH,H,Z,IERR,N2)  
INTEGER I,J,K,L,M,N,EN,II,JJ,LL,MM,NA,NM,NN,N2,  
X IGH,ITS,LOW,MP2,ENM2,IERR,MINO  
REAL H(N2,N2),Z(N2,N2)  
REAL P,Q,R,S,T,W,X,Y,RA,SA,VI,VR,ZZ,NORM  
REAL MACHEP, SORT, ABS, SIGN, REAL, AIMAG  
LOGICAL NOTLAS  
COMPLEX Z3,CMLPX

MACHEP IS A PARAMETER THAT SPECIFIES PRECISION

MACHEP=0.000000000001  
NM-IGH  
N-IGH  
LOW= 1  
IERR= 0  
NORM= 0.  
K= 1

COMPUTE MATRIX NORM

DO 50 I = 1,N  
DO 40 J = K,N  
K = I  
NORM = NORM + ABS(H(I,J))

50 CONTINUE

EN = IGH

T = 0.0

\*\*\* SEARCH FOR NEXT EIGENVALUES\*\*\*

60 IF(EN.LT. LOW) GO TO 1001

ITS = 0

NA = EN - 1

ENM2 = NA - 1

\*\*\*LOOK FOR SINGLE SMALL SUB-DIAGONAL ELEMENT

FOR L=EN STEP -1 UNTIL LOW DO \*\*\*

70 DO 80 LL = LOW, EN

L = EN + LOW - LL

IF(L.EQ. LOW) GO TO 100

S = ABS(H(L-1,L-1)) + ABS(H(L,L))

IF(S.EQ. 0.0) S = NORM

IF(ABS(H(L,L-1)) .LE. MACHEP \* S) GO TO 100

80 CONTINUE

\*\*\* FORM SHIFT \*\*\*

100 X = H(EN,EN)

IF(L.EQ. EN) GO TO 270

Y = H(NA,NA)

W = H(EN,NA) \* H(NA,EN)

IF(L.EQ. NA) GO TO 280

IF(ITS.EQ. 30) GO TO 1000

IF(ITS.NE. 10 .AND. ITS.NE. 20) GO TO 130

\*\*\* FORM EXCEPTIONAL SHIFT \*\*\*

T = T + X

DO 120 I = LOW,EN

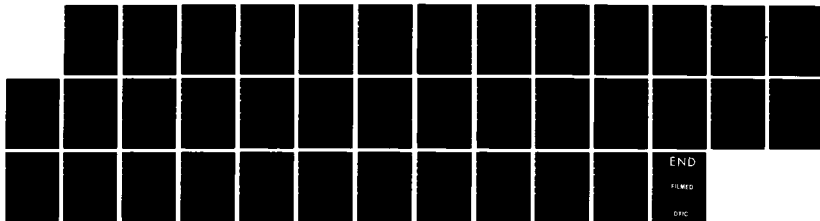
120 H(I,I) = H(I,I) - X

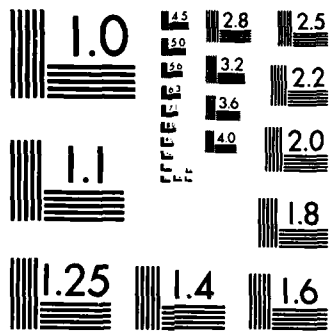
S = ABS(H(EN,NA)) + ABS(H(NA,ENM2))

X = 0.75 \* S



AD-A153 039 HEATING PARAMETER ESTIMATION USING COAXIAL THERMOCOUPLE 2/2  
GAGES IN WIND TUN. (U) AIR FORCE INST OF TECH  
WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI... N T CARNOON  
UNCLASSIFIED DEC 84 AFIT/GAE/AA/84D-3 F/G 9/2 NL





MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

```

113 H(K+1,J) = H(K+1,J) - P * Y
114 H(K,J) = H(K,J) - P * X
115
116 CONTINUE
117 J = MINO(EN,K+3)
118
119 *** COLUMN MODIFICATION ***
120 DO 230 I = 1, J
121 P = X * H(I,K) + Y * H(I,K+1)
122 IF( .NOT. NOTLAS) GO TO 220
123 P = P + ZZ * H(I,K+2)
124 H(I,K+2) = H(I,K+2) - P * R
125 H(I,K+1) = H(I,K+1) - P * Q
126 H(I,K) = H(I,K) - P
127
128 *** ACCUMULATE TRANSFORMATIONS ***
129 DO 250 I = LOW, IGH
130 P = X * Z(I,K) + Y * Z(I,K+1)
131 IF( .NOT. NOTLAS) GO TO 240
132 P = P + ZZ * Z(I,K+2)
133 Z(I,K+2) = Z(I,K+2) - P * R
134 Z(I,K+1) = Z(I,K+1) - P * Q
135 Z(I,K) = Z(I,K) - P
136
137 CONTINUE
138
139 GO TO 70
140
141 *** ONE ROOT FOUND ***
142 H(EN,EN) = X + T
143 EN = NA
144
145 *** TWO ROOTS FOUND ***
146 GO TO 60
147 P = (Y - X) / 2.0
148 Q = P * P + W
149 ZZ = SQRT(ABS(Q))
150 H(EN,EN) = X + T
151 X = H(EN,EN)
152 H(NA,NA) = Y + T
153 IF(Q .LT. 0.0) GO TO 320
154 *** REAL PAIR ***
155 ZZ = P + SIGN(ZZ,P)
156 X = H(EN,NA)
157 S = ABS(X) + ABS(ZZ)
158 P = X / S
159 Q = ZZ / S
160 R = SQRT(P * P + Q * Q)
161 P = P / R
162 Q = Q / R
163
164 *** ROW MODIFICATION ***
165 DO 280 J = NA, N
166 ZZ = H(NA,J)
167 H(NA,J) = Q * ZZ + P * H(EN,J)
168 H(EN,J) = Q * H(EN,J) - P * ZZ
169
170 CONTINUE
171
172 *** COLUMN MODIFICATION ***
173 DO 300 I = 1, EN
174 ZZ = H(I,NA)
175 H(I,NA) = Q * ZZ + P * H(I,EN)
176 H(I,EN) = Q * H(I,EN) - P * ZZ
177
178 CONTINUE
179
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SUBROUTINE HQR

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C *** ACCUMULATE TRANSFORMATIONS ***
DO 310 I = LOW, IGH
  ZZ = Z(I,NA)
  Z(I,NA) = Q*ZZ + P*Z(I,EN)
  Z(I,EN) = Q*Z(I,EN) - P*ZZ
310 CONTINUE
GO TO 330
C *** COMPLEX PAIR ***
320 CONTINUE
330 EN = ENW2
GO TO 60
C * SET ERROR - NO CONVERGENCE TO EIGENVALUE AFTER 30 ITERATIONS
1000 IERR = EN
1001 RETURN
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 68 SGEFA

30 CALL SAXPY(N-K,T,A(K+1,K),1,A(K+1,J),1)  
 CONTINUE  
 40 GO TO 50  
 CONTINUE  
 50 INFO= K  
 CONTINUE  
 60 CONTINUE  
 70 CONTINUE  
 IPVT(N)= N  
 IF(A(N,N) .EQ. 0.0E0) INFO= N  
 RETURN  
 END

56  
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1 SUBROUTINE SGEDI 74/855 OPT=0,ROUND= A/ S/ M/-D -DB FTN 5.1+587
2 DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST, PL=5000
3 FTNS, I, ANSI=O, L=OUTS, LO=S/-A.
4
5 SUBROUTINE SGEDI(A,LDA,N,IPVT,WORK)
6 INTEGER LDA,N,IPVT(1)
7 REAL A(LDA,1),WORK(1)
8
9 SGEDI COMPUTES INVERSE OF MATRIX A USING
10 FACTORS COMPUTED BY SGEFA.
11
12 ON ENTRY:
13 A: THE OUTPUT FROM SGEFA, REAL(LDA,N)
14 LDA: THE LEADING DIMENSION OF ARRAY A
15 N: THE ORDER OF MATRIX A
16 IPVT: THE PIVOT VECTOR FROM SGEFA, INTEGER(N)
17 WORK: WORK VECTOR, CONTENTS DESTROYED, REAL(N)
18
19 ON RETURN:
20 A: INVERSE OF THE ORIGINAL MATRIX
21
22 ERROR CONDITION: A DIVISION BY ZERO WILL OCCUR IF THE
23 INPUT FACTOR CONTAINS A ZERO ON THE DIAGONAL.
24 IT WILL NOT OCCUR IF SGEFA HAS SET INFO=0
25
26 THIS IS FROM LINPACK USER'S GUIDE, VERSION 08/14/78
27 REAL T
28 INTEGER I,J,K,KB, KP1,L,NM1
29
30 COMPUTE INVERSE
31 DO 100 K=1,N
32 A(K,K)= 1.OEO/A(K,K)
33 T= -A(K,K)
34 CALL SSCAL(K-1,T,A(1,K),1)
35 KP1= K+1
36 IF(N .LT. KP1) GO TO 80
37 DO 80 J=KP1,N
38 T= A(K,J)
39 CALL SAXPY(K,T,A(1,K),1,A(1,J),1)
40
41 80 CONTINUE
42 90 CONTINUE
43 100 CONTINUE
44
45 C FORM INVERSE(U)*INVERSE(L)
46 NM1= N-1
47 IF(NM1 .LT. 1) GO TO 140
48 DO 130 KB=1,NM1
49 K= N-KB
50 KP1= K+1
51 DO 110 I=KP1,N
52 WORK(I)= A(I,K)
53 A(I,K)= O.OEO
54
55 110 CONTINUE
56
57 120 CALL SAXPY(N,T,A(1,J),1,A(1,K),1)
58 CONTINUE
59 L= IPVT(K)
60
61 SGEDI
62 SGEDI
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61

IF(L .NE. K) CALL SSWAP(N,A(1,K),1,A(1,L),1)  
130 CONTINUE  
140 CONTINUE  
RETURN  
END

SGEDI 57  
SGEDI 58  
SGEDI 59  
SGEDI 60  
SGEDI 61



DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,OB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE SAXPY(N,SA,SX,INCX,SY,INCY)
2   CONSTANT TIMES A VECTOR PLUS A VECTOR.
3   USES UNROLLED LOOP FOR INCREMENTS= 1.
4   FROM LINPACK USER'S GUIDE, VERSION 03/11/78
5   REAL SX(1),SY(1),SA
6   INTEGER I,INCX,INCY,IX,IY,M,MP1,N
7   IF(N.LE.0) RETURN
8   IF(SA.EQ.0.0) RETURN
9   IF(INCX.EQ.1.AND.INCY.EQ.1) GO TO 20
10
11  C CODE FOR UNEQUAL INCREMENTS OR FOR
12  C EQUAL INCREMENTS NOT EQUAL TO 1
13  C
14  IX= 1
15  IY= 1
16  IF(INCX.LT.0) IX= (-N+1)*INCX + 1
17  IF(INCY.LT.0) IY= (-N+1)*INCY + 1
18  DO 10 I=1,N
19  SY(IY)= SY(IY)+ SA*SX(IX)
20  IX= IX+INCX
21  IY= IY+INCY
22  CONTINUE
23  RETURN
24
25  C CODE FOR BOTH INCREMENTS EQUAL TO 1
26  C CLEAN-UP LOOP
27  C
28  20 M=MOD(N,4)
29  IF(M.EQ.0) GO TO 40
30  DO 30 I=1,M
31  SY(I)= SY(I)+ SA*SX(I)
32  CONTINUE
33  IF(N.LT.4) RETURN
34  40 MP1= M+1
35  DO 50 I=MP1,N,4
36  SY(I)= SY(I)+ SA*SX(I)
37  SY(I+1)= SY(I+1)+ SA*SX(I+1)
38  SY(I+2)= SY(I+2)+ SA*SX(I+2)
39  SY(I+3)= SY(I+3)+ SA*SX(I+3)
40  CONTINUE
41  RETURN
42  END

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 SAXPY 3  
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 SAXPY 41

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1 SUBROUTINE SSCAL
2 DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-T8/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000
3 FTNS.I,ANSI=0,L=OUTS,LO=S/-A.
4
5 SUBROUTINE SSCAL(N,SA,SX,INCX)
6 SCALES A VECTOR BY A CONSTANT.
7 USES UNROLLED LOOPS FOR INCREMENT EQUAL TO 1.
8 LINPACK USER'S GUIDE,VERSION 03/11/78
9
10 REAL SA,SX(1)
11 INTEGER I,INCX,M,MP1,N,NINCX
12 IF(N.LE.0) RETURN
13 IF(INCX.EQ.1) GO TO 20
14
15 C
16 C CODE FOR INCREMENT NOT EQUAL TO 1
17 NINCX= N*INCX
18 DO 10 I=1,NINCX,INCX
19 SX(I)= SA*SX(I)
20 10 CONTINUE
21 RETURN
22
23 C
24 C CODE FOR INCREMENT EQUAL TO 1.
25 CLEAN-UP LOOP
26 20 M= MOD(N,5)
27 IF(M.EQ.0) GO TO 40
28 DO 30 I=1,M
29 SX(I)= SA*SX(I)
30 CONTINUE
31 40 MP1= M+1
32 DO 50 I=MP1,N,5
33 SX(I)= SA*SX(I)
34 SX(I+1)= SA*SX(I+1)
35 SX(I+2)= SA*SX(I+2)
36 SX(I+3)= SA*SX(I+3)
37 SX(I+4)= SA*SX(I+4)
38 50 CONTINUE
39 RETURN
40 END

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1  SUBROUTINE SSWAP
2  DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST, PL=5000
3  FTNS, I, ANSI=0, L=OUTS, LO=S/-A.
4
5  C SUBROUTINE SSWAP(N, SX, INCX, SY, INCY)
6  C INTERCHANGES TWO VECTORS.
7  C USES UNROLLED LOOPS FOR INCREMENTS EQUAL TO 1.
8  C LINPACK USER'S GUIDE, VERSION 03/11/78
9
10 REAL SX(1), SY(1), STEMP
11 INTEGER I, INCX, INCY, IX, IY, M, MP1, N
12 IF(N .LE. 0) RETURN
13 IF(INCX .EQ. 1 .AND. INCY .EQ. 1) GO TO 20
14
15 C CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS NOT EQUAL TO 1
16 IX= 1
17 IY= 1
18 IF(INCX .LT. 0) IX= (-N+1)*INCX+1
19 IF(INCY .LT. 0) IY= (-N+1)*INCY+1
20 DO 10 I=1, N
21 STEMP= SX(IX)
22 SX(IX)= SY(IY)
23 SY(IY)= STEMP
24 IX= IX+INCX
25 IY= IY+INCY
26 10 CONTINUE
27 RETURN
28
29 C CODE FOR BOTH INCREMENTS EQUAL TO 1.
30 CLEAN-UP LOOP
31 DO 30 I=1, M
32 STEMP= SX(I)
33 SX(I)= SY(I)
34 SY(I)= STEMP
35 30 CONTINUE
36 IF(N .LT. 3) RETURN
37 DO 50 I=MP1, N, 3
38 STEMP= SX(I)
39 SX(I)= SY(I)
40 SY(I)= STEMP
41 STEMP= SX(I+1)
42 SX(I+1)= SY(I+1)
43 SY(I+1)= STEMP
44 STEMP= SX(I+2)
45 SX(I+2)= SY(I+2)
46 SY(I+2)= STEMP
47 50 CONTINUE
48 RETURN
49 END

```





```

1  SUBROUTINE FLYNES(M,TSCALE,TMIN,I,ASCALE,AMIN,AVL,HT,ISKIP,NCHAR)
2  DIMENSION U(12)
3  EQUIVALENCE (T,U(1))
4  DATA IUNIT/12/
5  REVIND IUNIT
6  II=0
7  1000 READ(IUNIT,1000,END=190)U
8  1000 FORMAT(6E13.7)
9  XO=(U(M)-TMIN)/TSCALE
10 YO=(U(I)-AMIN)/ASCALE+AYL
11 II=II+1
12 III=((II/ISKIP))*ISKIP
13 IF(II.NE.III)GO TO 100
14 CALL SYMBOL(XO,YO,HT,NCHAR,0...-1)
15 GO TO 100
16 CONTINUE
17 RETURN
18 END
19 FLYNES
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29 FLYNES
    
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56 C START PLOT SEQUENCE
57 HT=.07
58 CALL PLOT(4.,.5,-3)
59
60 C
61 YLAB="T2(DEG F)"
62 TLAB="TIME(SEC)"
63 CALL AXIS(0.,0.,TLAB,-10,TAXL,0.,TMIN,TSCALE)
64 CALL AXIS(0.,0.,YLAB,10,YAXL,90.,YMIN,YSCALE)
65 C 4 IN CALL POINTS TO 4TH VARIABLE IN READ,Y
66 CALL FLINE(1,TSCALE,TMIN,4,YSCALE,YMIN,0.)
67 C 5 POINTS TO Z
68 CALL FLINES(1,TSCALE,TMIN,5,YSCALE,YMIN,0.,HT,1,3)
69 C PLOT DEPENDENT VARIABLE
70 AYL=YAXL+1.
71 ALAB="ALPHA(DEG)"
72 CALL AXIS(0.,AYL,ALAB,10,AXL,90.,AMIN,ASCALE)
73 C 6 POINTS TO A
74 CALL FLINE(1,TSCALE,TMIN,6,ASCALE,AMIN,AYL)
75 C
76 C
77 C NEXT PLOT SEQUENCE
78 AXO=TAXL+2.
79 CALL PLOT(AXO,0.,-3)
80 YLAB=" Q/QREF "
81 YAXL=10.
82 YSCALE=.1
83 YMIN=0.
84 IFOX(1)=IFX(4)
85 DO 32 I=2,6
86 IFOX(I)=IFX(I+9)
87 CONTINUE
88
89 DO 200 I=1,6
90 IF(IFOX(I).EQ.0)GO TO 200
91 DATA XL/"ALPHA(DEG)","BETA(DEG)","LOG(RE)"
92 &"DELE(DEG)" " "DELBF(DEG)" " MACH "
93 DATA XXL/5.,6.,4.,4.,5.,5./
94 DATA XSC/5.,1.,1.,5.,5.,5./
95 DATA XM/20.,-3.,5.,-10.,0.,0./
96 CALL AXIS(0.,0.,YLAB,10,YAXL,90.,YMIN,YSCALE)
97 CALL AXIS(0.,0.,XL(I),-10,XXL(I),0.,XM(I),XSC(I))
98 C I+5 POINTS TO ALPHA / 12 POINTS TO Q/QREF
99 IPT=I+5
100 CALL FLINE(IPT,XSC(I),XM(I),12,YSCALE,YMIN,0.)
101 CALL PLOT(AXO,0.,-3)
102 CONTINUE
103 CALL PLOTE(N)
104 RETURN
105 END

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DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1  SUBROUTINE FPLOT
2  COMMON/CFPLOT/IPLOT,TSCALE,TMIN,TAXL,YSCALE,YMIN,YAXL,
3  SSCALE,AMIN,AAXL
4  DIMENSION XL(6),XXL(6),XSC(6),XM(6)
5  DIMENSION IFOX(6)
6  DIMENSION DUM(1024)
7  LOGICAL FAUTO
8  DIMENSION FAUTO(7)
9  DIMENSION QP(5)
10 COMMON/CPARAM/HO,HALF(2),PHIC,PHIK,ZP,Z,ALPH(2),KA,S(5),
11 &CIF(5.5),KAF,IFX(5),ACC(5),IFXSUM,NPAR,DALPH(2),
12 EQUIVALENCE (HO,QP(1))
13 C INITIALIZE PLOTS AND WRITE PLOT FILE TO UNIT 2
14 CALL PLOTS(DUM,1024,2)
15 CALL FACTOR(.787402)
16 DATA IUNIT/12/
17 REWIND IUNIT
18 C FIND MAX AND MINS FOR SCALING
19 DATA TMN,TMX,YMN,YM/1.E7,0.,5000.,-460./
20 DATA AMN,AMX/25.,45./
21 C READ T,USI1,EQUI,USI2,UNEAS,ALPHA
22 100 READ(IUNIT,1000,END=190)T,U,V,Y,Z,A,B,R,DE,DB,DM,OM
23 1000 FORMAT(6E13.7)
24 TMN=AMIN1(TMN,T)
25 TMX=AMAX1(TMX,T)
26 YMN=AMIN1(YMN,U,V,Y,Z)
27 YMX=AMAX1(YMX,U,V,Y,Z)
28 AMN=AMIN1(AMN,A)
29 AMX=AMAX1(AMX,A)
30 GO TO 100
31
32 190 CONTINUE
33 IF(IPLOT.GT.0)GO TO 195
34 C DEFAULT TIME AXIS LENGTH = 4 INCHES
35 TAXL=4.
36 TSCALE=IFIX(((TMX-TMN)/TAXL)+.999)
37 TMIN=TMN
38 C DEFAULT Y AXIS LENGTH = 4 INCHES
39 YAXL=4
40 DYMIN=25.
41 YSCALE=DYMIN*IFIX((YMX-YMN)/DYMIN/YAXL+1.899)
42 YMIN=YSCALE*IFIX(YMN/YSCALE)
43 C DEFAULT A AXIS LENGTH = 2 INCHES
44 AAXL=2.
45 DAMIN=5
46 ASCALE=DAMIN*IFIX((AMX-AMN)/DAMIN/AAXL+1.899)
47 AMIN=ASCALE*IFIX(AMN/ASCALE)
48 195 CONTINUE
49 C SCALE TIME USING INPUT TSCALE ONLY
50 C PUT IN NEGATIVE OR ZERO FOR TMIN AND TAXL
51 IF(TAXL.GT.0)GO TO 198
52 TMIN=TMN
53 TAXL=IFIX((TMX-TMN)/TSCALE+.999)
54 198 CONTINUE
55 C
    
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DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST, PL=5000  
FTNS, I, ANSI=0, L=OUTS, LO=S/-A.

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SUBROUTINE MSCALE (N1, N2, A, X, B)  
  DIMENSION A(1), B(1)  
  COMMON /MAIN1/ NDIM  
  DIMENSION IRAY(6)  
  DATA IRAY/6* -0/  
  IRAY(4)=0  
  JEND=N2*NDIM  
  DO 1 I=1, N1  
  CALL SYSTEMC(144, IRAY)  
  DO 1 IJ=1, JEND, NDIM  
  B(IJ)=X*A(IJ)  
  RETURN  
  END  
  
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SUBROUTINE MAUL 74/855 OPT=0,ROUND=A/S/M/-D,-DS FYN 5.1+587  
DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE MAUL(X,Y,N1,N2,N3,Z)
2 DIMENSION X(1),Y(1),Z(1)
3 COMMON/MAIN1/NDIM
4 NEND3=NDIM*N3
5 NEND2=NDIM*N2
6 DO 1 I=1,N1
7 DO 1 J=I,NEND3,NDIM
8 TM=0.
9 K=I
10 KK=J-I
11 KK=KK+1
12 TM=TM+X(K)*Y(KK)
13 K=K+NDIM
14 IF(K.LE.NEND2) GO TO 5
15 Z(J)=TM
16 RETURN
17 END

```

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SUBROUTINE MAT4 74/855 OPT=0,ROUND= A/ S/ M/-D,-DS FPN 5.1+587  
DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000  
FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```
1 SUBROUTINE MAT4 (N1,N2,X,Y,Z)
2 Z=XY* X=X* IS NZXN2, Y IS N1XN2. Z IS N1XN1
3 DIMENSION X(1), Y(1), Z(1)
4 COMMON /MAIN1/ NDIM
5 CALL MMUL (Y,X,N1,N2,N2,Z)
6 DO 3 I=1,N1
7 IM1=I-1
8 II=IM1+NDIM
9 JJ=I+II
10 DO 2 J=1,N1
11 TEMP=0.
12 KK=J
13 DO 1 K=1,N2,NDIM
14 TEMP=TEMP+Y(K)*Z(KK)
15 1 KK=KK+NDIM
16 Z(JJ)=TEMP
17 2 JJ=JJ+NDIM
18 JJ=I
19 K=II+1
20 KK=II+IM1
21 DO 3 J=K,KK
22 Z(JJ)=Z(J)
23 JJ=JJ+NDIM
24 3 CONTINUE
25 RETURN
26 END
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SUBROUTINE TRANS(A,N,X)  
 DIMENSION A(1),X(1)  
 COMMON/MAIN1/NDIM  
 DO 10 I=1,N  
 DO 10 J=1,N  
 II=I+NDIM\*(J-1)  
 JJ=J+NDIM\*(I-1)  
 A(II)=X(JJ)  
 RETURN  
 END

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60 CONTINUE  
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100 CONTINUE  
RETURN  
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747855 OPT=0,ROUND= A/ S/ M/-D -DS  
 DD=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000  
 FTNS, I, ANSI=0, L=OUTS, LO=S/-A.

```

1 SUBROUTINE SGTSL
2 DD=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000
3 FTNS, I, ANSI=0, L=OUTS, LO=S/-A.
4
5 SUBROUTINE SGTSL(N,C,D,E,B,INFO)
6 INTEGER N,INFO
7 REAL C(1),E(1),B(1),D(1)
8
9 C SGTSL GIVEN A GENERAL TRIDIAGONAL MATRIX AND A RIGHT HAND
10 C SIDE WILL FIND THE SOLUTION - SEE THE LINPAC USER'S GUIDE
11
12 INTEGER K,KB,KP1,NM1,NM2
13 REAL T
14 INFO=0
15 C(1)=D(1)
16 NM1=N-1
17 IF(NM1.LT.1)GO TO 40
18 D(1)=E(1)
19 E(1)=O.OEO
20 E(N)=O.OEO
21 DO 30 K=1,NM1
22 KP1=K+1
23 IF(ABS(C(KP1)).LT.ABS(C(K)))GO TO 10
24 T=C(KP1)
25 C(KP1)=C(K)
26 C(K)=T
27 T=D(KP1)
28 D(KP1)=D(K)
29 D(K)=T
30 T=E(KP1)
31 E(KP1)=E(K)
32 E(K)=T
33 T=B(KP1)
34 B(KP1)=B(K)
35 B(K)=T
36 CONTINUE
37 IF(C(N).NE.O.OEO)GO TO 20
38 INFO=K
39 GO TO 100
40 CONTINUE
41 T=C(KP1)/C(K)
42 C(KP1)=D(KP1)+T*D(K)
43 D(KP1)=E(KP1)+T*E(K)
44 E(KP1)=O.OEO
45 B(KP1)=B(KP1)+T*B(K)
46 CONTINUE
47 IF(C(N).NE.O.OEO)GO TO 50
48 INFO=N
49 GO TO 90
50 CONTINUE
51 NM2=N-2
52 B(N)=B(N)/C(N)
53 IF(N.EQ.1)GO TO 80
54 B(NM1)=(B(NM1)-D(NM1)*B(N))/C(NM1)
55 IF(NM2.LT.1)GO TO 70
56 DO 60 KB=1,NM2
57 K=NM2-KB+1
58 B(K)=(B(K)-D(K)*B(K+1)-E(K)*B(K+2))/C(K)
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DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000  
FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE INTEG(N,A,T,QUE,PHI,QQ,QDT,N2)
2 DIMENSION A(N2,N2),QUE(N2,N2),PHI(N2,N2),QQ(N2,N2),QDT(N2,N2)
3 T2=-T*0.5
4 CALL MEXP(N,A(1,1),T2,PHI(1,1),QQ(1,1),QDT(1,1),N2)
5 CALL TRI(N,QUE(1,1),PHI(1,1),QQ(1,1),QDT(1,1),N2)
6 CALL MSCALE(N,N,QDT(1,1),4.0,QDT(1,1))
7 CALL MULT(PHI(1,1),PHI(1,1),N,A(1,1),N2)
8 CALL TRI(N,QUE(1,1),A(1,1),QQ(1,1),PHI(1,1),N2)
9 DO 10 I=1,N
10 DO 10 J=1,N
11 QDT(I,J)= QUE(I,J)+ QDT(I,J)+ PHI(I,J)
12 T6=T/6.0
13 CALL MSCALE(N,N,QDT(1,1),T6,QDT(1,1))
14 RETURN
15 END

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1 SUBROUTINE HEATTUN  
 2 DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS= USER/-FIXED,DB=-TB/-SB/-SL/ ER/-ID/-PMD/-ST,PL=5000  
 3 FTNS. I, ANSI=0, L=OUTS, LO=S/-A.  
 4  
 5 SUBROUTINE HEATTUN  
 6 COMMON/CHEAT/Q,TS,QREF,TW,M1,RENS,HBAR,HREF  
 7 COMMON/COMTUN/T,TAW1,ALPHA,H.V,RHO,P,TEMP,C,TRAD,RHOG,  
 8 &TO,TSINK,XFT,DEL,PDEL  
 9 LOGICAL FAUTO  
 10 DIMENSION FAUTO(7)  
 11 DIMENSION QP(5)  
 12 COMMON/CPARAM/HO,HALF(2),PHIC,PHIK,ZP,Z,ALPH(2),KA,S(5),  
 13 &CIF(5,5),KAF,IFX(5),ACC(5),IFXSUM,NPAR,DALPH(2)  
 14 EQUIVALENCE (HO,QP(1))  
 15 COMMON/ICTPS2/TINIT(1),ERALLOW,E  
 16 COMMON/CDX/DX(1)  
 17 DATA HREF/1./

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DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
 FTNS,I,ANSI=0,L=OUTS,LO=S/-A.

```

1 SUBROUTINE TPSOSP2(DT)
2 COMMON/COSP/NPTSS,USI(6),PHI(6,6),NPT,PC(6,6),RR,
3 &QD(6,6),QDT(6,6),QUE(6,6),A(6,6),RCX(6),RP(6),RM(6)
4 COMMON/COPT/N,IOA(8),IOB(8),IOC(8),IOFACE(8),IOD(8)
5 COMMON/CPC/NPTPC
6 COMMON /MAINT/INP,IPVT(6),WORK(6)
7 INP=6
8 IF(DT .LE. 0.) GO TO 999
9 T=DT
10 CALL INTEG(NPTPC,A,I,QUE,PHI,QD,QDT,NPTSS)
11 CALL SGEFA(A(1,1),NPTSS,NPTPC,IPVT(1))
12 CALL SGEDI(A(1,1),NPTSS,NPTPC,IPVT(1),WORK(1))
13 CALL MAT4(NPTPC,NPTPC,QDT(1,1),A(1,1),QD(1,1))
14 CALL MAT4(NPTPC,NPTPC,PC(1,1),A(1,1),QDT(1,1))
15 DO 20 I=1,NPTPC
16 DO 20 J=1,NPTPC
17 PHI(I,J)=A(I,J)
18 PC(I,J)=QDT(I,J)+QD(I,J)
19 999 RETURN
20 END
    
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SUBROUTINE EQUATE (NR, NC, A, B)  
DIMENSION A(1), B(1)  
COMMON /MAIN1/ NDIM  
NN=NC*NDIM  
NR1=NR-1  
DO 1 J=1, NN, NDIM  
II=J+NR1  
DO 1 IJ=J, II  
A(IJ)=B(IJ)  
1 CONTINUE  
RETURN  
END
```

```

1 SUBROUTINE GMINV
2 DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/-SL/
3 FTNS. I. ANSI=0. L=OUTS. LO=S/-A.
4
5 SUBROUTINE GMINV (NR, NC, A, U, MR, MT)
6 DIMENSION A(1), U(1), S(30)
7 COMMON /MAINZ/ NDIM
8 COMMON /INDJ/ KIN, KOUT
9 NDIM1=NDIM+1
10 TOL=1. E-14
11 ADV=1. E-24
12 MR=NC
13 NRM1=NR-1
14 TOL1=0.
15 JJ=1
16 DO 1 J=1, NC
17 S(J)=DOT(NR, A(JJ), A(JJ))
18 IF (S(J).GT. TOL1) TOL1=S(J)
19
20 1 JJ=JJ+NDIM
21 TOL1=ADV*TOL1
22 ADV=TOL1
23 JJ=1
24 DO 14 J=1, NC
25 FAC=S(J)
26 JM1=J-1
27 JRM=JJ+NRM1
28 JCM=JJ+JM1
29 DO 2 I=JJ, JCM
30 U(I)=0.
31 U(JCM)=1.0
32 IF (J.EQ.1) GO TO 5
33 KK=1
34 DO 3 K=1, JM1
35 IF (S(K).EQ.1.0) GO TO 3
36 TEMP=-DOT(NR, A(JJ), A(KK))
37 CALL VADD (K, TEMP, U(JJ), U(KK))
38 3 KK=KK+NDIM
39 DO 4 L=1, 2
40 KK=1
41 DO 4 K=1, JM1
42 IF (S(K).EQ.0.) GO TO 4
43 TEMP=-DOT(NR, A(JJ), A(KK))
44 CALL VADD (NR, TEMP, A(JJ), A(KK))
45 CALL VADD (K, TEMP, U(JJ), U(KK))
46 4 KK=KK+NDIM
47 TOL1=TOL+FAC+ADV
48 FAC=DOT(NR, A(JJ), A(JJ))
49 5 IF (FAC.GT. TOL1) GO TO 9
50 DO 6 I=JJ, JRM
51 A(I)=0.
52 S(J)=0.
53 KK=1
54 IF (S(K).EQ.0.) KK=KK+NDIM
55 IF (S(K).EQ.0.) GO TO 8
56 DO 7 K=1, JM1
57 TEMP=-DOT(K, U(KK), U(JJ))
58 CALL VADD (NR, TEMP, A(JJ), A(KK))
59 7 KK=KK+NDIM
60 8 FAC=DOT(J, U(JJ), U(JJ))

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56 MR=MR-1
57 GO TO 11
58 9 S(J)=1.0
59 KK=1
60 DO 10 K=1,JM1
61 IF (S(K).EQ.1.) GO TO 10
62 TEMP=-DOT(NR,A(JJ),A(KK))
63 CALL VADO (K,TEMP,U(JJ),U(KK))
64 KK=KK+NDIM
65 10 FAC=1./SQRT(FAC)
66 DO 12 I=JJ,JRH
67 A(I)=A(I)*FAC
68 DO 13 I=JJ,JCM
69 U(I)=U(I)*FAC
70 JJ=JJ+NDIM
71 IF (MR.EQ.NR.OR.MR.EQ.NC) GO TO 15
72 IF (MT.NE.O) WRITE (KOUT,19) NR,NC,MR
73 15 NEND=NC+NDIM
74 JJ=1
75 DO 18 J=1,NC
76 DO 16 I=1,NR
77 II=I-J
78 S(I)=0.
79 DO 16 KK=JJ,NEND,NDIM
80 S(I)=S(I)+A(II+KK)*U(KK)
81 II=J
82 DO 17 I=1,NR
83 U(II)=S(I)
84 17 II=II+NDIM
85 18 JJ=JJ+NDIM
86 RETURN
87 19 FORMAT (13,1HX,12.8H M: RANK,12)
88 END

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1 FUNCTION DOT (NR, A, B)
2 DIMENSION A(1), B(1)
3 DOT=0.
4 DO 1 I=1, NR
5 DOT=DOT+A(I)+B(I)
6 RETURN
7 END
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SUBROUTINE VADD (N,C1,A,B)  
DIMENSION A(1), B(1)  
DO 1 I=1,N  
1 A(I)=A(I)+C1*B(I)  
RETURN  
END
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DO=-LONG/-OT,ARG=-COMMON/-FIXED,CS=USER/-FIXED,DB=-TB/-SB/-SL/ER/-ID/-PMD/-ST,PL=5000  
FTNS.I,ANSI=0,L=OUTS,LO=S/-A.

```
1 SUBROUTINE VADD (N,C1,A,B)
2 DIMENSION A(1), B(1)
3 DO 1 I=1,N
4 1 A(I)=A(I)+C1*B(I)
5 RETURN
6 END
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## VITA

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A heat energy balance is applied to a coaxial thermocouple gage for parameter estimation in wind tunnel test articles. This method can significantly reduce wind tunnel test costs and time. Modifications to the data reduction program HEATEST (HEATING ESTIMATION) are made. The program allows for transient test techniques to be used as well as assuming an isothermal wall. A non-linear convective heat transfer coefficient model may also be used. Data is generated to test the new program. Temperature profiles throughout the thermocouple gage were good and were compared with changes in time step, thermocouple length, and number of discrete node points. The estimation of the convective heat transfer coefficient and thermal conductivity were excellent.

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