

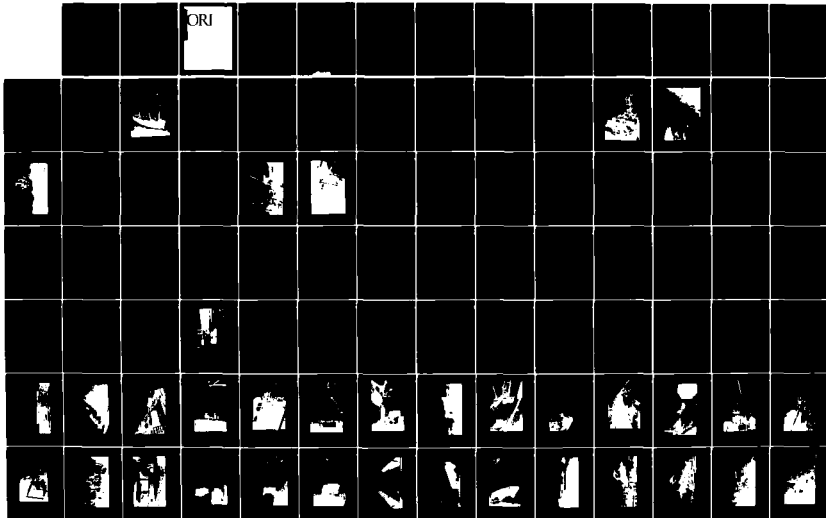
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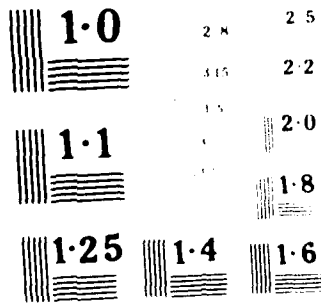
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HEAVY-LIFT BREAKBULK SHIP PRETEST RESULTS OF
THE JOINT LOGISTICS-OVER-THE-SHORE (LOTS)
TEST AND EVALUATION PROGRAM

25 JULY 1977

PREPARED UNDER
CONTRACT NUMBER MDA-903-75-C-0016
FOR THE OFFICE OF THE SECRETARY OF DEFENSE
DEPUTY DIRECTOR (TEST AND EVALUATION)
OFFICE OF THE DIRECTOR, DEFENSE RESEARCH AND ENGINEERING
WASHINGTON, D.C. 20310

REPORT DOCUMENTATION PAGE

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1. GOVT ACCESSION NO.	2. RECIPIENT'S CATALOG NUMBER
3. TYPE OF REPORT & PERIOD COVERED	Final Report Dec 76 - Jun 77
4. PERFORMING ORG. REPORT NUMBER	
5. CONTRACT OR GRANT NUMBER	MNA-903-75-C-0016
6. PROGRAM ELEMENT PROJECT TASK AREA & WORK UNIT NUMBERS	
7. REPORT DATE	25 July 1977
8. NUMBER OF PAGES	133
9. SECURITY CLASS. of this report	Unclassified
10. DECLASSIFICATION/DOWNGRADING SCHEDULE	N/A

Approved for public release; distribution unlimited

By what title is this report covered in the abstract and identify by block number

Breakbulk ship	Container ship	Operating	LACV-30
Land	Container ship	Embarkation	LAPC-LX
Gateway ferry	Frame	Flag vessels	LCU
Container	Lighting	Heavy-lift	Loading
	Deployment	Joint Test	Lighterage

21. ABSTRACT (Include references and identify by block number)

The major objective of the Heavy-Lift Breakbulk Ship Pretest was to determine the capabilities of the Services to use such a ship for deploying selected Logistics-Over-The-Shore (LOTS) equipment to a site where fixed port facilities do not exist. This test was the third of five planned preliminary tests of the Joint LOTS Operational Test and Evaluation Program conducted under the sponsorship of the Deputy Director (Test and Evaluation), Office of the Director, Defense Research and Engineering. The pretest was conducted from anchorages off Sewells Point, Norfolk, Virginia, and Ft. Story, Virginia.

1. Title

2. Author

3. Date

4. Type

5. Period

6. Source

7. Distribution

8. Availability

9. Notes

10. Summary

11. Abstract

The pretest, conducted 1-9 November, 1976, was part of an evaluation program leading to a major LOTS exercise in August, 1977. The heavy-lift ship was needed in order to verify the capabilities for deploying newly procured LOTS equipment assembled in a near ready-to-use configuration. It was anticipated that a LOTS beach and throughput system could be established more rapidly if equipment assembly requirements were minimized. Operational response time would be significantly improved because the detailed disassembly—required for embarkation aboard conventional breakbulk ships, containerships, and most bargeships—would not be required for the heavy-lift breakbulk ship.

A secondary objective, conducting a container-oriented throughput operation, was added to the pretest by the Services. This objective was included for training purposes and for eliminating potential technical problems during the LOTS main test.

The results of the pretest indicated that equipment could be deployed with minimal disassembly and emphasized the continuing need for the heavy-lift breakbulk ship. Anticipated time savings are on the order of 53 hr in deployment of the 300-ton capacity crane with minimum disassembly. This is compared to the time needed for the more detailed disassembly required when only conventional breakbulk ships are available.

The heaviest item loaded was a 1466-class LCU that weighed 180 long tons. A 1644-class LCU was scheduled for loading but lacked an appropriate sling. A recommendation was made that such a sling be included as part of the ship's equipment. Except for the 300-ton crane, all equipment was loaded/unloaded without difficulty. Handling of the 300-ton crane was complicated by the fact that it was rigged incorrectly. Also it had to be placed in the LCU backwards so that the combined center of gravity of the LCU with the crane was far enough aft to be safe and seaworthy. Consequently, after it was backed out of the LCU, the crane had to be turned around on the beach, a move that delayed the crane's operational readiness for several hours.

During the container throughput phase a temporary containership discharge facility (TCDF), an Army 300-ton lifting capacity crane mounted on a DeLong barge, was used by military personnel to unload containers from a ship

For the first time, the use of the new, low G II, proved the concept feasible in a limited way. The test provided an opportunity to evaluate the amount of derating to the crane's rated capacity to use when it is operating on an unstable platform. These findings are expected in a later report to be published by the Army. A crane will be utilized during the LOTS main test.

The crane was used to form a pier at the beach. The DeLong, a 140-ton crane, was beached, picked-up, ramps lowered, and moved to the pier. The pier with the 140-ton crane was used to load containers.

The crane used to load containers was the Army's 300-ton capacity crane. It was used to load containers and used as a crane-on-beach container. The crane was used to load containers and the 140-ton crane on the pier. The crane's inability to reach containers in lighters and the use of the crane's 140-ton capacity were successfully and consistently demonstrated. The newly built, was employed to load containers. The crane was used to load containers, but wave motion and constant movement of the crane with the chassis made this operation too time-consuming. The crane was successfully used to lighter containers at the beach. The crane was used to load containers where a front loader rapidly off-loaded containers from the crane's chassis.

The test verified the Services' capabilities for using heavy and oversized equipment. The crane, because of its weight and size, is the first opportunity in over 4 years. This opportunity provided the experience which will be amplified during the main test.

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ABSTRACT

The primary objective of the heavy-lift Breakbulk Ship Pretest was to determine the feasibility of the Services to use such a ship for deploying equipment to a site where fixed port facilities are not available. This was the third of five planned preliminary tests of the Breakbulk Ship Pretest and Evaluation Program conducted under the direction of the Deputy Director (Test and Evaluation), Office of the Secretary, Department of Defense Engineering. The pretest was conducted from 20 October to 11 November 1976, at Norfolk, Virginia, and Ft. Story, Virginia.

The pretest, conducted 1-11 November, 1976, was part of an evaluation program conducted as part of an exercise in August, 1977. The heavy-lift ship was tested to determine the capabilities for deploying newly procured equipment in a ready-to-use configuration. It was anticipated that a container-oriented throughput system could be established more rapidly at a port where port requirements were minimized. Operational requirements would be significantly improved because the detailed disassembly-requirements for equipment on most conventional breakbulk ships, containerships, and lift barges would not be required for the heavy-lift breakbulk ship.

The primary objective of conducting a container-oriented throughput pretest was to determine the feasibility of the Services. This objective was anticipated to be achieved by eliminating potential technical problems associated with the pretest.

The results of the pretest indicated that equipment could be deployed with minimal disassembly and emphasized the continuing need for the heavy-lift breakbulk ships. Anticipated time savings are on the order of 53 hr in deployment of the lift-capacity crane with minimum disassembly. This is compared to the time needed for the more detailed disassembly required when only conventional breakbulk ships are available.

The heaviest item loaded was a 14ft-class LCU that weighed 180 long tons. A 14ft-class LCU was scheduled for loading but lacked an appropriate sling. A recommendation was made that such a sling be included as part of the ship's equipment. Except for the 300-ton crane, all equipment was loaded/unloaded without difficulty. Handling of the 300-ton crane was complicated by the fact that it was rigged incorrectly. Also it had to be placed in the LCU backwards so that the combined center of gravity of the LCU with the crane was far enough aft to be safe and seaworthy. Consequently, after it was backed out of the LCU, the crane had to be turned around on the beach, a move that reduced the crane's operational readiness for several hours.

During the container throughput phase a temporary containership discharge facility (ICDF), an Army 300-ton lifting capacity crane mounted on a Delong barge, was used by military personnel to unload containers from a ship for the first time. A previous exercise, OLCF II, proved the concept feasible on a larger barge using civilian operators. This pretest provided an opportunity to instrument the crane for an evaluation on the amount of derating to the crane's lifting capacity is necessary when it is operating on an unstable platform. These findings are expected in a later report to be published by a Naval laboratory and will be utilized during the LOTS main test.

A Delong barge was also used to form a pier at the beach. The Delong, with ramps and a 140-ton crane aboard, was beached, jacked-up, ramps lowered, and made operational in approximately 1 1/2 hr. The pier with the 140-ton crane was then used as an unloading facility for containers.

Also tested for the first time was the Army's 300-ton capacity crane which was placed at the high water line and used as a crane-on-beach container unloading facility. Both the 300-ton crane-on-beach and the 140-ton crane on the Delong pier were hampered by an inability to reach containers in lighters at low tide. Amphibians-LAPC-IXs and LAPC-XVs--were successfully and concurrently used during calm seas. A causeway ferry was employed to load containers on milvan chassis at shipside using the ICDF, but wave motion and container alignment difficulties with the chassis made this operation too time-consuming. The causeway ferry was successfully used to lighter containers at low tide and over sandbars to the beach where a frontloader rapidly off-loaded the containers and placed them on milvan chassis.

In summary, the pretest verified the Services' capabilities for using a ready-bulk breakbulk ship to deploy certain LOTS heavy and outsized equipment. The only item not considered feasible, because of its weight and size, is the Delong barge. The pretest also provided the first opportunity in over 4 years to conduct a container throughput exercise. This opportunity provided the experience required by military personnel which will be amplified during the main test.

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I. INTRODUCTION

BACKGROUND

The principal objective of the heavy-lift breakbulk ship pretest was to determine the capabilities of the Services to use a vessel of this type to:

- Deploy heavy and oversized, mission-essential, Logistics-Over-The-Shore (LOTS) equipment to an off-shore site,
- Off-load and transport the equipment to shore in landing craft deployable aboard the ship, and
- Prepare the equipment on the beach for LOTS throughput operations.

A secondary objective, conducting a container-oriented throughput operation, was added to the pretest by the Services for training purposes and for identifying potential unforeseen technical problems during the LOT main test. These objectives were accomplished in an exercise conducted November 1-9, 1976. The test began with the ship at anchorage in Hampton Roads, Virginia, where equipment was loaded and continued off Ft. Story, Virginia, where ship discharge and throughput operations took place.

The heavy-lift breakbulk ship pretest also offered a less obvious but important feature besides verifying the deployability of new equipment. There is rarely an opportunity for deployment of very large and heavy equipment, especially if handling by military personnel is required. The paucity of heavy-lift ships and the cost, difficulty, and infrequency of repositioning oversized, heavy equipment have diminished the familiarity and skill of military personnel in dealing with such equipment. Accordingly, it was found that some "rediscovery" of the special equipment and handling considerations was necessary for supporting this type of operation.

The results of the tests conducted with the test material are presented in the report of the test program. The test program was conducted in the field and the results are presented in the report. The test program was conducted in the field and the results are presented in the report. The test program was conducted in the field and the results are presented in the report.

With the advent of the new equipment, planners have recognized that these items are among the largest and heaviest items in the inventory. For example, the heavy machinery and container handling equipment used in the test all exceed the size and weight of a tank and all have a weight in excess of 10,000 lbs. The test equipment is a key item in the test program and its availability is a critical factor in the test program.

The ship used for the tests was the USNS T-ESB-1 (see figure 1) which was built in 1961 and was rebuilt in 1964 with a stern, heavy lift deck and extra large deck openings. The ship was rebuilt for long term service in the Military Sealift Command fleet. The other ship in the fleet is the USNS T-ESB-2 which was built in 1961 and was rebuilt in 1964 with a stern, heavy lift deck and extra large deck openings. The ship was rebuilt for long term service in the Military Sealift Command fleet. The other ship in the fleet is the USNS T-ESB-3 which was built in 1961 and was rebuilt in 1964 with a stern, heavy lift deck and extra large deck openings. The ship was rebuilt for long term service in the Military Sealift Command fleet.

The test program was conducted in the field and the results are presented in the report. The test program was conducted in the field and the results are presented in the report. The test program was conducted in the field and the results are presented in the report.

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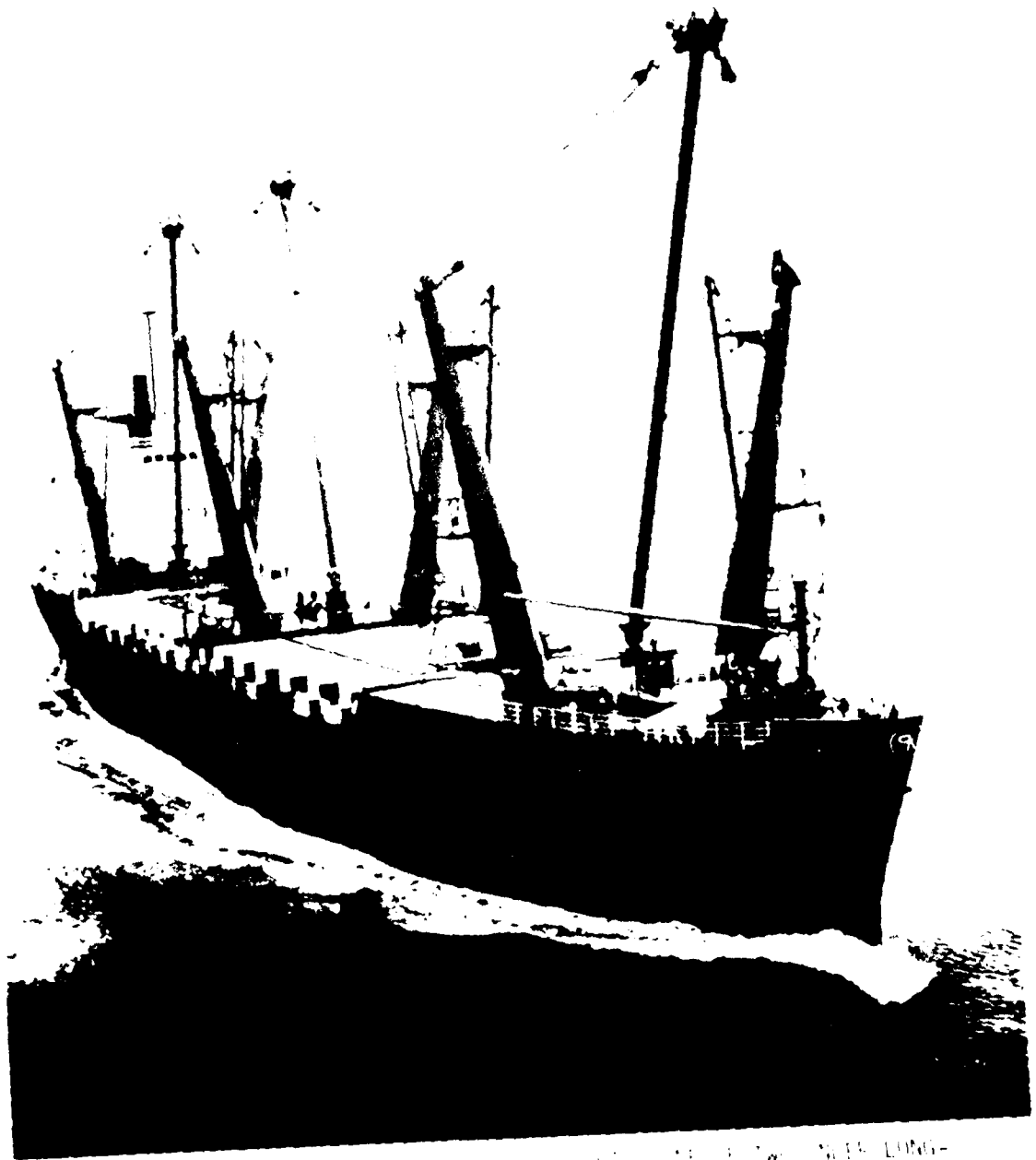


FIGURE 1. A REEFED SCHOONER AT SEA WITH LONG-
LEADERS AND GALLEYS AROUND

heavy items such as 2 MGs, LARC-116s, and locomotives. Second, there are three 120-ton top-stowkin booms, 100 ft in length which permit loading large heavy items in holds 1, 3, and 4. The 120-ton booms can also be paired to work together around the ship a nominal 240-ton lifting capacity, permitting the hoisting of an L-19. A total of four L19s can be stowed on the main deck. Figure 1-11 illustrates the capability for use singly or paired. The general characteristics of the two heavy-lift breakbulk ships are contained in Table 1. Appendix A contains more detailed information on ship characteristics.

TABLE 1
GENERAL CHARACTERISTICS
S.S. TRANSCOLORADO AND S.S. TRANSCOLUMBIA

Type of vessel: Single screw LARC-116 transport converted to breakbulk ship having a heavy-lift capability of 240 tons. Vessel was originally built in 1945 and converted by Newport News Shipbuilding and Drydock Co., Newport News, Virginia in July 1964.	
Length overall	500 ft 10 1/2 in
Length between perpendicular	436 ft 10 in
Breadth molded	71 ft 6 in
Depth to main deck at side molded	40 ft 6 in
Draft to assigned waterline molded	30 ft 4 1/2 in
Displacement in salt water	21,700 tons
Deadweight	11,475 tons
Shaft horsepower - normal	9,100
Continuous sea speed	16 knots
Cargo ship characteristics	
Displacement	11,225 tons
Vertical center of gravity, KG	27.93 ft above keel
Longitudinal center of gravity, LCG	236.94 ft fwd of A-P
Officers and crew	38
Number of cargo holds	5

The TRANSCOLUMBIA's master and chief mate reported that on one occasion the ship had loaded and discharged a 300-ton tugboat.

120' FOR ANCHORAGE WITH
WINDS FROM 45°
AND 130°

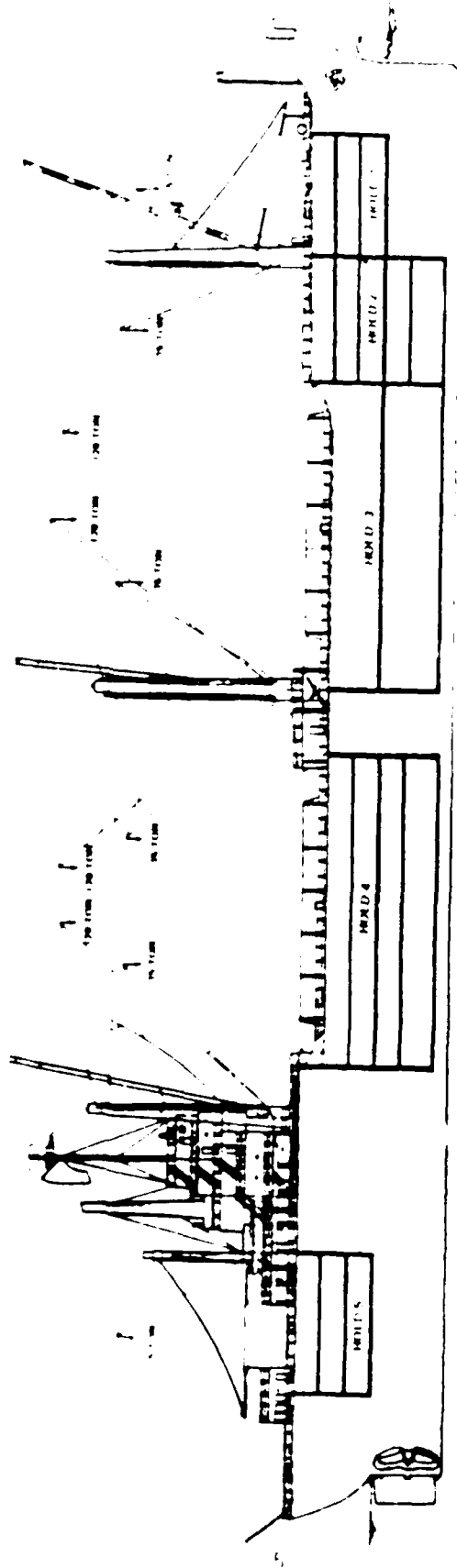


FIGURE 2. HEAVY-LIFT BREAKBULK SHIP PROFILE

1970-1971

The test lifts originally selected for this report were the heaviest and most complex lifts ever attempted on a standardized cargo at a 1000-ton breakbulk ship. These lifts were eliminated, however, for criteria eliminated, namely, the lift was too large to attempt. The characteristics of the test lifts are given in Table 1.

The lifts originally selected for the 1970-1971 test series were not test lifts:

- The heavy lift crane on the vessel could not be made available to conduct the required developmental tests.
- The heavy lift crane on the vessel was considered a redundant lift since its employment was restricted to a cargo of breakbulk cargo which had lesser capabilities.
- A new type of lift crane which had not yet been developed for the project.
- The heavy lift crane on the vessel which was not available.

The heavy lift crane on the vessel is needed to transport the heavy lift cargo to the pier when embarked in a tactically disassembled configuration. A tactical disassembly of the crane is defined as the minimum disassembly necessary for deck stowage. In a tactical disassembly the crane, which was the heavy lift crane, had all sections of the boom - except the boom bases removed - with the counterweights and out-rigger floats. The weight of the crane in weight of the sections (from approximately 150 long tons) was approximately 100 long tons in the test. This is as opposed to the crane being disassembled into components of less than 10 long tons each, which is the time and required 1 to 2 days for reassembly.

The heavy lift crane (145-ton lifting capacity) is smaller and lighter than the heavy lift crane and is a suitable load for an LCM, which has a capacity of approximately 64 short tons and can be deployed on most commercial ships. In the 1970-1971 test the heavy lift crane was loaded into an LCM but loading from a heavy lift breakbulk ship presented different problems, discussed in detail later in this report.

Finally, the heavy lift crane was embarked for the first time in the 1970-1971 test series. The heavy lift breakbulk ship was the only ship tested that had the required capacity (more than 100 long tons) and space available to load and stow the heavy lift crane.

The heavy lift crane in this instance refers to the Army of long pier and the heavy lift breakbulk ship discharge facility (HDF). The latter is a facility with a large crane mounted on it. The crane is positioned alongside a pier ready for unloading operations.

TABLE 2
HEAVY-LIFT SHIP PRETEST PLANNED LOADS

Lifts Planned	Characteristics					Remarks
	Lift Made	Length (Ft)	Width (Ft)	Height (Ft)	Weight LTons	
400 Model (20 ton lifting capacity) crane, tactical disassembly	Yes	57.6	12	13.5	98	
400 Model (14 ton lifting capacity) crane, tactical disassembly	Yes	48.5	11.3	9.4	42	
400 Model	Yes	62.5	26.6	15.3	88	
2400-Class LCL	Yes	119	34	17.8	180	
2400-Class LCL	No	135.3	29	17	151.8	No sling available
400 Model Sideloader	Yes	41	12.5	11.7	64	Top handler removed.
Clark Frontloader	No	30.5	13.2	16.5	69.3	Not received in the inventory. Top handler (60 LTons) removed.
400V-30	No	76.3	33	21.5	27.7	Not available for loading
3 x 25 Causeway Section	No	90	21.3	5.1	60.3	Lift was redundant*
4000-Milvans	19	20	8	8	-	Weights varied by container
4000-Ft Container	1	40	8	8	30	

* See ORI Technical Report No. 1037.

MEASUREMENT AND EVALUATION

During the equipment deployment aspects of the test the most important job was to check the physical feasibility of moving the LOTS equipment with the ship's crane and, once in the objective area, making the equipment available to the lift operations. Thus, observations were concerned with matters of crane clearance, centers of gravity (did the item hang in an appropriate position), proper fit of lift slings with lift points, any pendulation problems due to wind or other factors, and the like. Times required for deployment of the equipment items were measured to support main test planning. Crane cycles and crane throughput data samples were also obtained. The throughput rates found and the factors that influence them were additional inputs to main test planning.

During the ship off-loading measurements were made of the sea state and the motion of the LCI platform. An ancillary test to measure the stresses on the components of the LCI was also conducted. These measurements, made by personnel from the Naval Civil Engineering Laboratory at Port Hueneme, California, will be the subject of a separate Navy report. The results may assist the Joint Test and Evaluation program by establishing better safe working limit criteria for the LCI crane working in this environment.

Finally, observations were made of the way various equipment functioned in the environment and of cargo documentation and control procedures.

III. OPERATIONS

LOADING AND UNLOADING

On-site operations began about 0700 hr November 2, 1976, with the LARC-IX, MBI-1 at anchor off Sewells Point in Hampton Roads. Weather conditions throughout the loading and discharge phases of the pretest were clear with a light-to-calm wind and calm seas at both the Sewells Point anchorage and off Blue Beach, Ft. Story.

Preparations for loading required approximately 3 hr and included the opening of hatches and the loading of dunnage, cargo rigging sets, and the 6250 crane. Most of the test cargo was accomplished using the ship's 120-ton booms which are designed to move very large objects and, hence, move rather slowly. Initially, the first day, only containers and the LARC-IX were loaded before interrupted operations. On most ships round-the-clock operations are desirable but with the heavy-lift ship this is not advisable because of the extraordinarily long booms (100 ft) and the need for the boom operator to constantly watch the line passing through the sheaves at the boom tip. This is particularly true at night since artificial light at the 100-ft distance is inadequate.

The first lift on the second day was the 1466-class 10, which was lifted on the starboard side of Hold No. 4 without difficulty. The 9125 crane subsequently was loaded and stowed in the well deck of the LARC-IX. At hold No. 3 the 6250 crane was loaded on the port side and the sideloader on the starboard side. All lifts were made in a fairly routine fashion except for the 6250 crane which was lifted with a pronounced fore and aft tilt.

Off-loading began about 0730 on 4 November after the ship had moved to an anchorage off Blue Beach, Ft. Story. The order for off-loading was the 6250 crane, sideloader, the 40-ft container, the 9125 crane, the 1466-class 10, and the LARC-IX. Only the 6250 crane posed any difficulties and this was

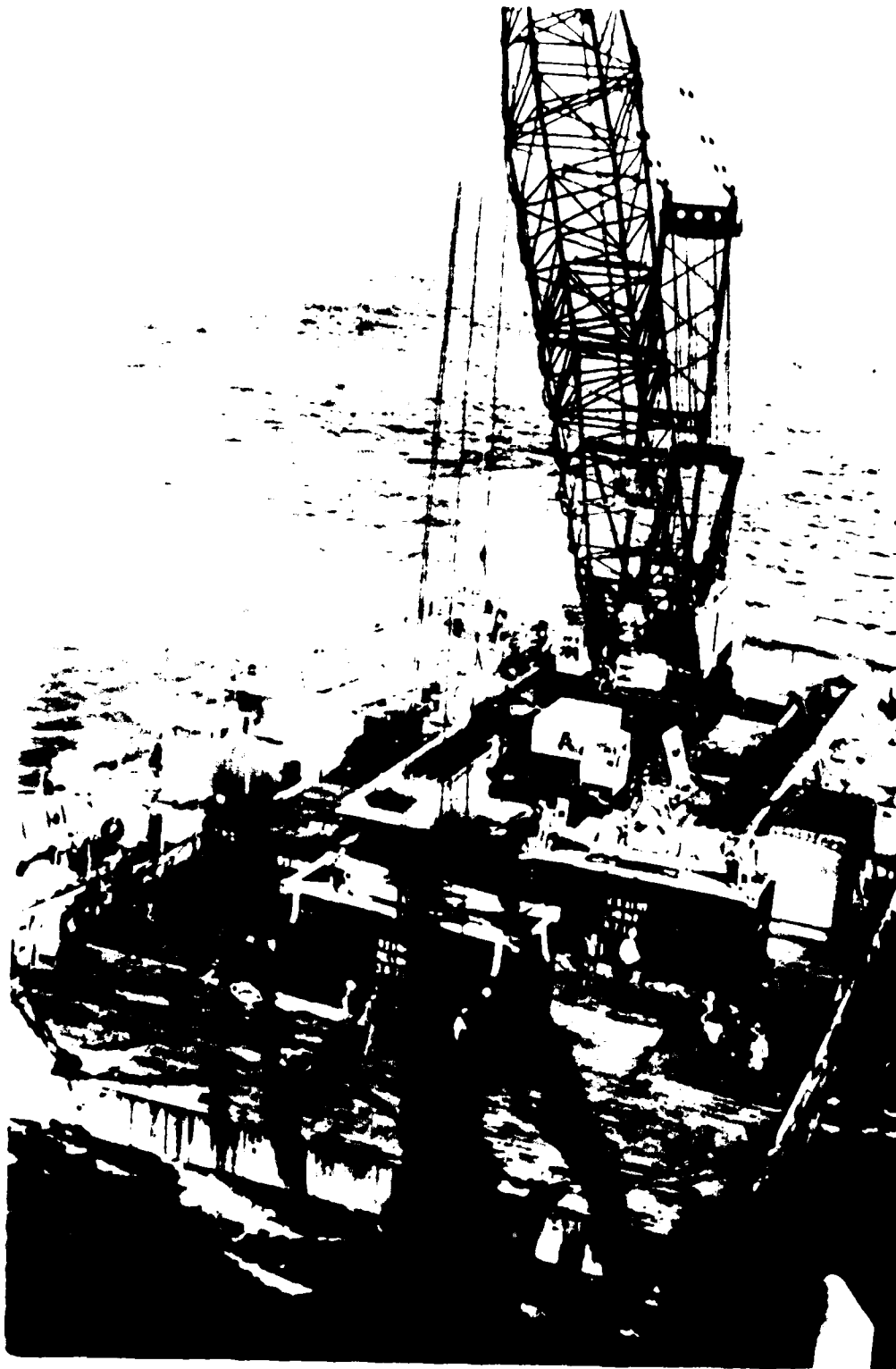


FIGURE 3. TEMPORARY CONTAINERSHIP DISCHARGE FACILITY



TABLE 1
 SUMMARY OF RESULTS OF THE INVESTIGATION

Location	Time	Direction	Speed	Remarks
Main Deck	10:00	Starboard	10 knots	Clear
Between Main Deck and Main Deck 2	10:05	Starboard	10 knots	Clear
Between Main Deck 2 and Main Deck 3	10:10	Starboard	10 knots	Clear
Main Deck 3	10:15	Starboard	10 knots	Clear
Main Deck 4	10:20	Starboard	10 knots	Clear
Main Deck 5	10:25	Starboard	10 knots	Clear
Main Deck 6	10:30	Starboard	10 knots	Clear
Main Deck 7	10:35	Starboard	10 knots	Clear
Main Deck 8	10:40	Starboard	10 knots	Clear
Main Deck 9	10:45	Starboard	10 knots	Clear
Main Deck 10	10:50	Starboard	10 knots	Clear
Main Deck 11	10:55	Starboard	10 knots	Clear
Main Deck 12	11:00	Starboard	10 knots	Clear
Main Deck 13	11:05	Starboard	10 knots	Clear
Main Deck 14	11:10	Starboard	10 knots	Clear
Main Deck 15	11:15	Starboard	10 knots	Clear
Main Deck 16	11:20	Starboard	10 knots	Clear
Main Deck 17	11:25	Starboard	10 knots	Clear
Main Deck 18	11:30	Starboard	10 knots	Clear
Main Deck 19	11:35	Starboard	10 knots	Clear
Main Deck 20	11:40	Starboard	10 knots	Clear
Main Deck 21	11:45	Starboard	10 knots	Clear
Main Deck 22	11:50	Starboard	10 knots	Clear
Main Deck 23	11:55	Starboard	10 knots	Clear
Main Deck 24	12:00	Starboard	10 knots	Clear
Main Deck 25	12:05	Starboard	10 knots	Clear
Main Deck 26	12:10	Starboard	10 knots	Clear
Main Deck 27	12:15	Starboard	10 knots	Clear
Main Deck 28	12:20	Starboard	10 knots	Clear
Main Deck 29	12:25	Starboard	10 knots	Clear
Main Deck 30	12:30	Starboard	10 knots	Clear
Main Deck 31	12:35	Starboard	10 knots	Clear
Main Deck 32	12:40	Starboard	10 knots	Clear
Main Deck 33	12:45	Starboard	10 knots	Clear
Main Deck 34	12:50	Starboard	10 knots	Clear
Main Deck 35	12:55	Starboard	10 knots	Clear
Main Deck 36	1:00	Starboard	10 knots	Clear
Main Deck 37	1:05	Starboard	10 knots	Clear
Main Deck 38	1:10	Starboard	10 knots	Clear
Main Deck 39	1:15	Starboard	10 knots	Clear
Main Deck 40	1:20	Starboard	10 knots	Clear
Main Deck 41	1:25	Starboard	10 knots	Clear
Main Deck 42	1:30	Starboard	10 knots	Clear
Main Deck 43	1:35	Starboard	10 knots	Clear
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Main Deck 45	1:45	Starboard	10 knots	Clear
Main Deck 46	1:50	Starboard	10 knots	Clear
Main Deck 47	1:55	Starboard	10 knots	Clear
Main Deck 48	2:00	Starboard	10 knots	Clear
Main Deck 49	2:05	Starboard	10 knots	Clear
Main Deck 50	2:10	Starboard	10 knots	Clear
Main Deck 51	2:15	Starboard	10 knots	Clear
Main Deck 52	2:20	Starboard	10 knots	Clear
Main Deck 53	2:25	Starboard	10 knots	Clear
Main Deck 54	2:30	Starboard	10 knots	Clear
Main Deck 55	2:35	Starboard	10 knots	Clear
Main Deck 56	2:40	Starboard	10 knots	Clear
Main Deck 57	2:45	Starboard	10 knots	Clear
Main Deck 58	2:50	Starboard	10 knots	Clear
Main Deck 59	2:55	Starboard	10 knots	Clear
Main Deck 60	3:00	Starboard	10 knots	Clear
Main Deck 61	3:05	Starboard	10 knots	Clear
Main Deck 62	3:10	Starboard	10 knots	Clear
Main Deck 63	3:15	Starboard	10 knots	Clear
Main Deck 64	3:20	Starboard	10 knots	Clear
Main Deck 65	3:25	Starboard	10 knots	Clear
Main Deck 66	3:30	Starboard	10 knots	Clear
Main Deck 67	3:35	Starboard	10 knots	Clear
Main Deck 68	3:40	Starboard	10 knots	Clear
Main Deck 69	3:45	Starboard	10 knots	Clear
Main Deck 70	3:50	Starboard	10 knots	Clear
Main Deck 71	3:55	Starboard	10 knots	Clear
Main Deck 72	4:00	Starboard	10 knots	Clear
Main Deck 73	4:05	Starboard	10 knots	Clear
Main Deck 74	4:10	Starboard	10 knots	Clear
Main Deck 75	4:15	Starboard	10 knots	Clear
Main Deck 76	4:20	Starboard	10 knots	Clear
Main Deck 77	4:25	Starboard	10 knots	Clear
Main Deck 78	4:30	Starboard	10 knots	Clear
Main Deck 79	4:35	Starboard	10 knots	Clear
Main Deck 80	4:40	Starboard	10 knots	Clear
Main Deck 81	4:45	Starboard	10 knots	Clear
Main Deck 82	4:50	Starboard	10 knots	Clear
Main Deck 83	4:55	Starboard	10 knots	Clear
Main Deck 84	5:00	Starboard	10 knots	Clear
Main Deck 85	5:05	Starboard	10 knots	Clear
Main Deck 86	5:10	Starboard	10 knots	Clear
Main Deck 87	5:15	Starboard	10 knots	Clear
Main Deck 88	5:20	Starboard	10 knots	Clear
Main Deck 89	5:25	Starboard	10 knots	Clear
Main Deck 90	5:30	Starboard	10 knots	Clear
Main Deck 91	5:35	Starboard	10 knots	Clear
Main Deck 92	5:40	Starboard	10 knots	Clear
Main Deck 93	5:45	Starboard	10 knots	Clear
Main Deck 94	5:50	Starboard	10 knots	Clear
Main Deck 95	5:55	Starboard	10 knots	Clear
Main Deck 96	6:00	Starboard	10 knots	Clear
Main Deck 97	6:05	Starboard	10 knots	Clear
Main Deck 98	6:10	Starboard	10 knots	Clear
Main Deck 99	6:15	Starboard	10 knots	Clear
Main Deck 100	6:20	Starboard	10 knots	Clear



FIGURE 5. ATTACHMENT POINTS TO ADJUST SPREADER BAR FOR CENTERS-
OF-GRAVITY ON 6050 AND 9125 MODELS

was successful, although there were minor delays in inserting the strap under the pins of the lifting frame and also in manhandling the loops of the strap over the cable blocks of the ship's heavy-lift boom.

The smaller crane, the 915, was lifted first. There was a delay while the crane upper was rotated 180 degrees. The boom base was over the crane truck cab in the final configuration. After a test lift the crane was set down again in the LCL and the nylon loop inspected. The lift was then made without any further delays.

The lift of the 6250 crane was the final heavy lift and was the only one that required an on-the-spot decision. The same lifting frame that was used for the smaller crane was used for the 110-ton 6250 crane lift. As the lift started, the lead nosed up. The front wheels were about 3 ft off the deck before the rear wheels began to lift clear. The crane boom, facing the rear, slanted downward toward the ramp of the LCL it was being lifted from. If the lift had continued, the boom presumably would have come in contact with the top edge of the ramp. Experience in the breakbulk ship pretest¹ had shown that even seemingly minor bumps impacting on the tubular frame of the crane boom can cause dents that seriously affect the maximum lift capability of the crane. Thus the possibility of contact had to be minimized.

The way to avoid the problem would have been to re-rig the lift so that it remained level. This would have involved shifting the lift point at the apex of the lift frame from one point to another in the series of holes available. However, such re-rigging would have been time-consuming. A decision was made to continue the lift, but to first lower the LCL ramp so as to provide increased clearance. This was done, and the lift proceeded with the crane at a pronounced slant. As the crane started downward toward the deck of the ship the tilt would have caused the boom base to make contact with timbers on the hatch top before the crane wheels made contact. To avoid this possibility caused a delay of about 15 minutes. The crane was repositioned in such a way that the boom base was located over a gap between the opening of hatch number 3 and the deck house. This allowed the crane wheels to touch before the tip of the boom base. With that problem solved, the lift was completed.

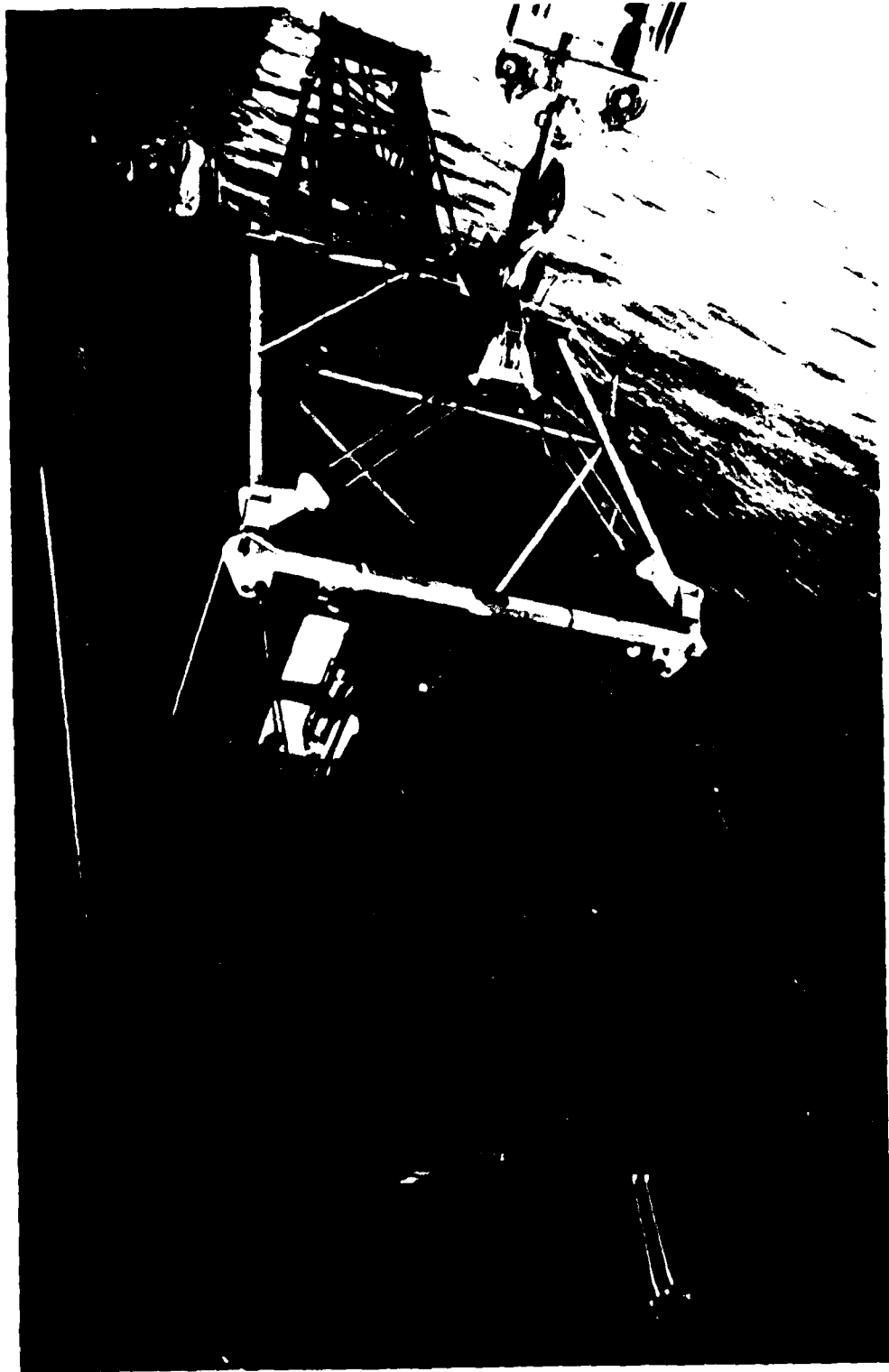
The total time required for the lift, including delays, was 2 hr and 12 minutes. There were three delays: 10 min waiting for the LCL to tie-up in the proper location; 10 min waiting for the LCL to be lowered into malfunctioning; and 15 minutes for the crane to be repositioned. Upon completion of this lift the ship weighed in the yard and was ready to depart.

APPENDIX A

General

The lifting of the heavy lift began at about 10:00 AM, November 4. The weather was clear and calm. There were no problems for the most part the order

operations. Reference is made to the results of the Conventional Breakbulk Ship Pretest of the U.S. Navy's Over-the-Board (OTB) Test and Evaluation Program, NAVY Technical Report TR-137, October 1976.



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9125 Crane

The LCM8 carrying the Army 9125 crane to shore had no difficulty underway despite a pronounced list. The LCM8 grounded on an off-shore sandbar an hour before low tide. A LARC-V from the Naval Beach Group detachment assisted it in backing off. The LCM8 then waited for the tide to come in, and some 6 hr later made a second attempt. Again the LCM8 was stuck on a sandbar. This time cables were passed from bulldozers to the landing craft. With a hard strain on the lines the LCM8 was pulled over the bar and into the deeper water nearer the shore. From there it was successfully beached.

Bulldozers then graded a ramp for the crane to use in coming ashore. Momat was unrolled onto the graded ramp and, some 30 minutes after the LCM8 had been pulled across the sandbar, the crane was ready for moving ashore. In moving out of the LCM8 onto the mat, the crane got hung up on the after end of its carrier. By using an outrigger to jack itself up, the crane freed itself and moved onto the beach with no further difficulty. No difficulty was recorded in assembling the crane's counterweights, attaching the boom sections, and reeving the cables. These operations were accomplished during the night so that the crane was ready for operations before the first landing craft arrived the next day.

Sideloader

The LCU carrying the sideloader also had to be assisted by bulldozers in landing. It came ashore on the same tide as the LCM8 carrying the 9125 crane. After moving ashore out of the LCU, the sideloader overran the Momat matting and got stuck in the sand. Bulldozers assisted and got it back on the Momat. On another occasion it got stuck crossing a narrow gap between Momat strips. This time it used its outriggers to elevate its tires so that beach matting could be placed under them and then it was freed.

CONTAINER THROUGHPUT OPERATIONS

General

In the second phase of the pretest, which involved container throughput operations, the TCCF was used exclusively to discharge containers from hold and deck stowage locations aboard the TRANSCOLUMBIA to various types of lighters, including LCU, LCM8, LARC-XV, LARC-LX, BC barge, and causeway ferry.

Four methods were used to unload containers from lighters:

- 140-ton crane on jacked-up B DeLong to off-load all lighters and load containers on milvan chassis.
- 300-ton crane at the high waterline primarily to off-load LCU and LCM8 craft. It was used to also off-load amphibians and to transfer loaded containers onto milvan chassis.
- 140-ton crane in the marshalling area to unload amphibians.

- Frontloader to off-load containers from a causeway ferry onto milvan chassis.

These subsystem elements were not used concurrently due to the small quantity of test cargo available (20 milvans and 1 40-ft van). Nevertheless, the pretest was the first opportunity in 4 years that a container throughput exercise had been attempted. Data and training on the new Army equipment were needed. It was also the first time in 4 years that a container marshalling area operation was conducted and, although the activities there were relatively slow and simple, the same data and training opportunities existed. Documentation and movements management also played a part in this phase with some limited use of the mobile GPS van.

To be representative of military cargo shipped in containers, the containers were weighted with dummy cargo. Figure 2 shows the weight distribution of the containers used.

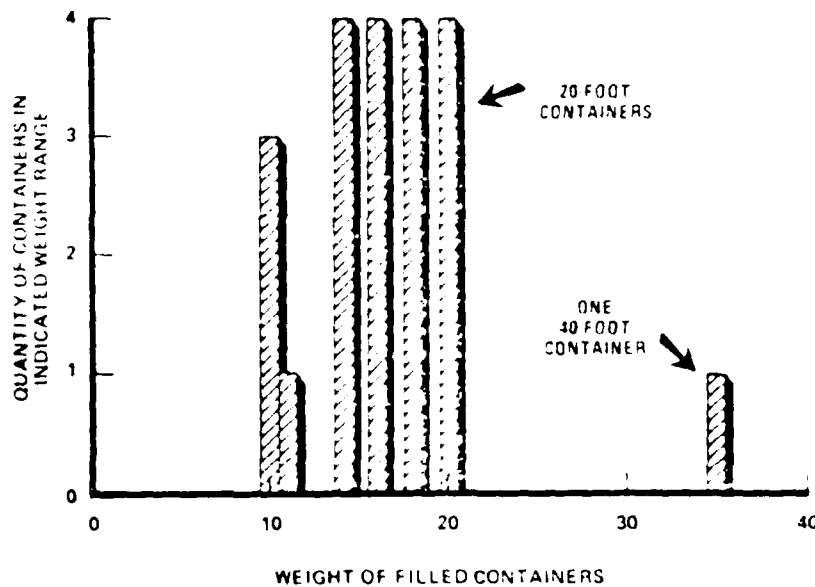


FIGURE 2. DISTRIBUTION OF CONTAINER WEIGHTS (20 and 40-FT)

Temporary Container Discharge Facility

Use of the heavy-lift breakbulk ship as a containership had two of recognized drawbacks. First, there were no cell guides to assist in attachment of the container spreader bar to containers in the hold. As a result, stevedores had to wrestle the spreader bar around over the tops of containers until it could be engaged with the corner fittings. Second, the TDCF had to

made allowances for clear the ship's booms and kingposts. Both of these obstacles tended to slow cycle times. However, the time data gathered provides a good approximate information useful for main test planning.

During the pretest the containers were first completely off-loaded from the ship and reloaded. In some cases a container was backloaded and then without detaching the containers from the spreader bar the container was reloaded in the lighter. These latter iterations were disregarded since they had more training value than data validity. The TCOF working the TRANS-LOG MBRB off-loaded 8 and backloaded 16 containers. When the ship charter period was completed, a LASH barge was used briefly instead. No timings were made of these loading and unloading events. There were considerable periods while working the ship in which the crane was inactive or delayed. When the LASH barge and was operating, a cycle required approximately 10 minutes. Similarly, backloading containers to the ship required approximately 7 minutes each. Further discussion of these times is contained in Section III, Table 6 summarizes the statistics of the TCOF.

TABLE 6
SUMMARY OF TCOF CHARACTERISTICS

TCOF length (boom assembled)	130 ft
TCOF width	60 ft
TCOF weight*	656.2 LTons
boom length	100 ft
boom tip used	Heavy duty
weight of hook blocks (2)	1,450 lb each
hook operation	Double drum
wire	1 inch
hook-part purchase	2 parts per hook
hook actual operation during test	15.3
* includes barge, crane, and crane foundations.	

Crane in Use

Operations with the 6250 crane at the water's edge commenced the afternoon of 7 November. The first day's activities consisted of discharging only five LASHs during a period of approximately 1 1/2 hr. Operations had commenced just 45 minutes after low tide, so it was not possible to land LCUs, LCMs, or barges close enough for the crane to reach them. Therefore, to attain some crane use, amphibians were employed instead.

The next day, there was a morning high tide (0854) so retrograde operations were possible. One L¹ was beached, backloaded with four containers, and retracted in 43 minutes. The average cycle time per container was 10 minutes 43 seconds. Bad weather was being experienced at the beach so the next day was loaded with only two containers before it was retracted after 22 minutes. After that the L² crane practiced loading and unloading (LAC-1) and training. Gusts up to 30 knots were experienced which caused difficulties for rigline handlers.

On the last day of beach operations for the 110-ton crane, approximately 1 hr before high tide, a LASH barge was grounded within the channel's reach and four containers were unloaded at an average rate of 3 3/4 minutes each. The barge was subsequently brought in at low tide and one container was off-loaded.

Delong Pier Operations

The design of the beach unloading system to be exercised was the 110-ton crane on the Delong pier. The Delong with the crane abeam was towed to the pier by tug and positioned at the beach using a MoS. Installation began following a working schedule normally followed a 110-ton crane once the permit is in hand.

The Delong was brought in approximately 1 hr before high tide and approximately 40 minutes later all its caissons (piling) had been lowered. There was no activity the next day and the third day, 7 November, after some work on the piling, the ramps to the Delong were lowered from the Delong to the beach; however, by the end of that day some additional alignment was required and the fourth day was spent aligning the ramps. Then, because a ramp was needed shore side of the 4-ft high Delong ramps, an assault vehicle landing ramp (AHL) ramp was installed. By the end of the day, after approximately 10 hr of activity, spread over 4 days, the Delong pier was ready for operations. Appendix 1 provides a detailed description of the installation process and attendant crane operations.

Operationally the Delong handled approximately 10 containers during the Delong pier stage. The first day of operations was mostly one of practice lifting a retrograde landing craft and once onto a truck. The morning of the next day, 8 November, the hydraulic spreader was found damaged and a manual spreader had to be obtained. Consequently, the opportunity for operations during the high tide period was lost. During the low tide period initially some practice was accomplished by loading and off-loading trucks. Then two LAC-1s were sent with containers to the Delong and these were unloaded onto the pier. One container was later retrograded via a LAC-1.

The next day, 9 November, was more active. In the morning during high tide two L¹s were loaded with three retrograde containers. Then three containers a L² barge were hoisted for off-loading a total of 10 containers. In the afternoon installations replaced landing craft in order that operations could continue during low tide. Two LAC-1s were off-loaded and two others were back-loaded.

The last day, 2 November, the ICBF barge was moved at high tide to the beach and loaded with four containers. At some point the ICBF barge was damaged and required welding a plate over the hole. The welding was done at low tide with the barge grounded and the hole exposed.

4.2.2.2. CAUSEWAY

The causeway ferry was used twice during the operation. The first time was for mobile loading, in which containers were placed on milvan chassis directly on the beach. The second employment a day later called for placing the containers directly on the causeway. The four-section causeway used in both instances was created by two LCMF causeway tender boats.

On 3 November the first operation was begun by loading three milvan trailers at the beach east of the Pelong pier. Bulldozers constructed a sand ramp to the causeway. As soon as the ramp was prepared, three M-54 trucks with the trailers individually proceeded onto the causeway. Each truck-trailer unit was positioned in a separate causeway section. The most seaward section, the one between the two tender boats, was left vacant. None of the vehicles were tied down. The causeway retracted from the beach without difficulty at low tide and proceeded towards the ship.

At 1400 the first milvan was lifted from the deck of the ICBF. After considerable effort to position the container on the platform trailer, the attempt was aborted. The problems were:

- The relative motions of the ICBF and the causeway.
- The twist angle (approximately 45 degrees) needed to properly align the container with the trailer (see Figure 9).
- The limited deck area for line holders.
- The target is small—even when there is no relative motion, as on dry land; it is not easy to position a container directly onto the container fittings of this type of trailer without repeated tries.

The second attempt on a different trailer was successful, requiring only 10 minutes. The first lift attempted had been to a trailer spotted on the causeway well forward of the ICBF crane. The second lift loaded a trailer which offered a better angle to the axis of the boom. (Dotted lines, Figure 9.) The

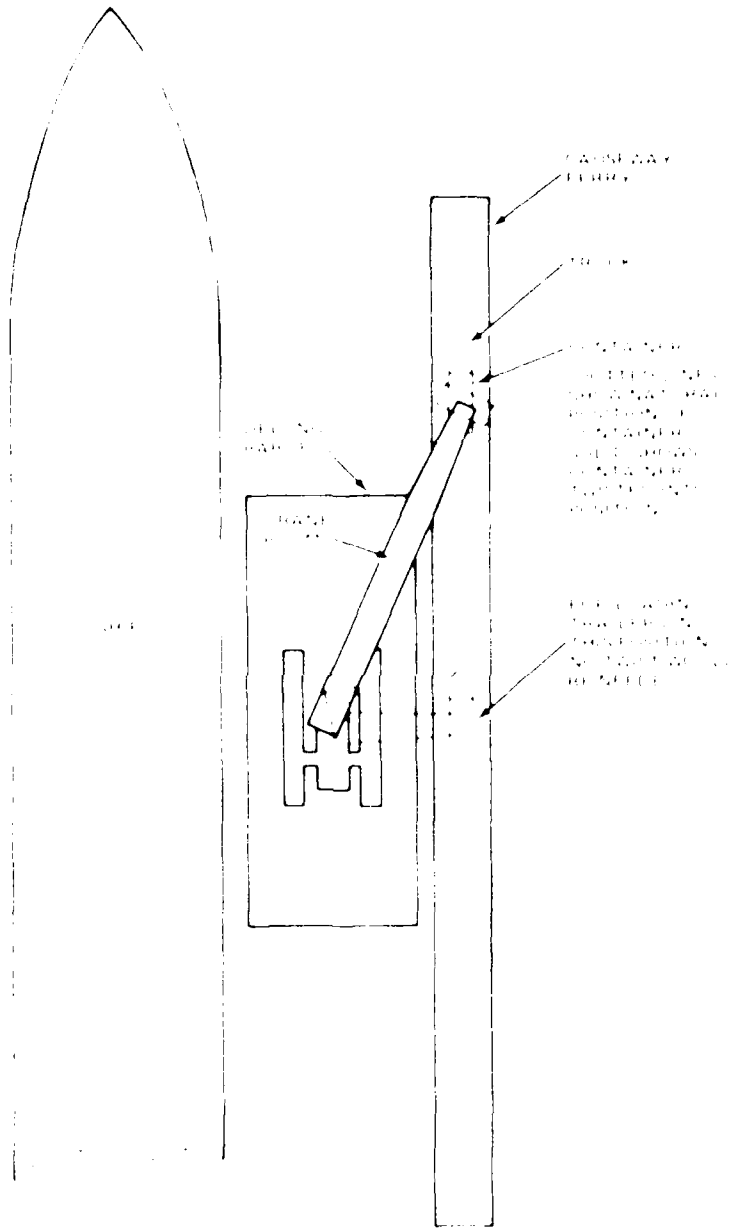


FIG. 1. A perspective view of the assembly shown in FIG. 2. The assembly consists of a pointed member, a rectangular member with a central cutout, a diagonal rod, a nut, a washer, and a vertical plate with a hole. The rod passes through the cutout and the hole, and is secured by the nut and washer.

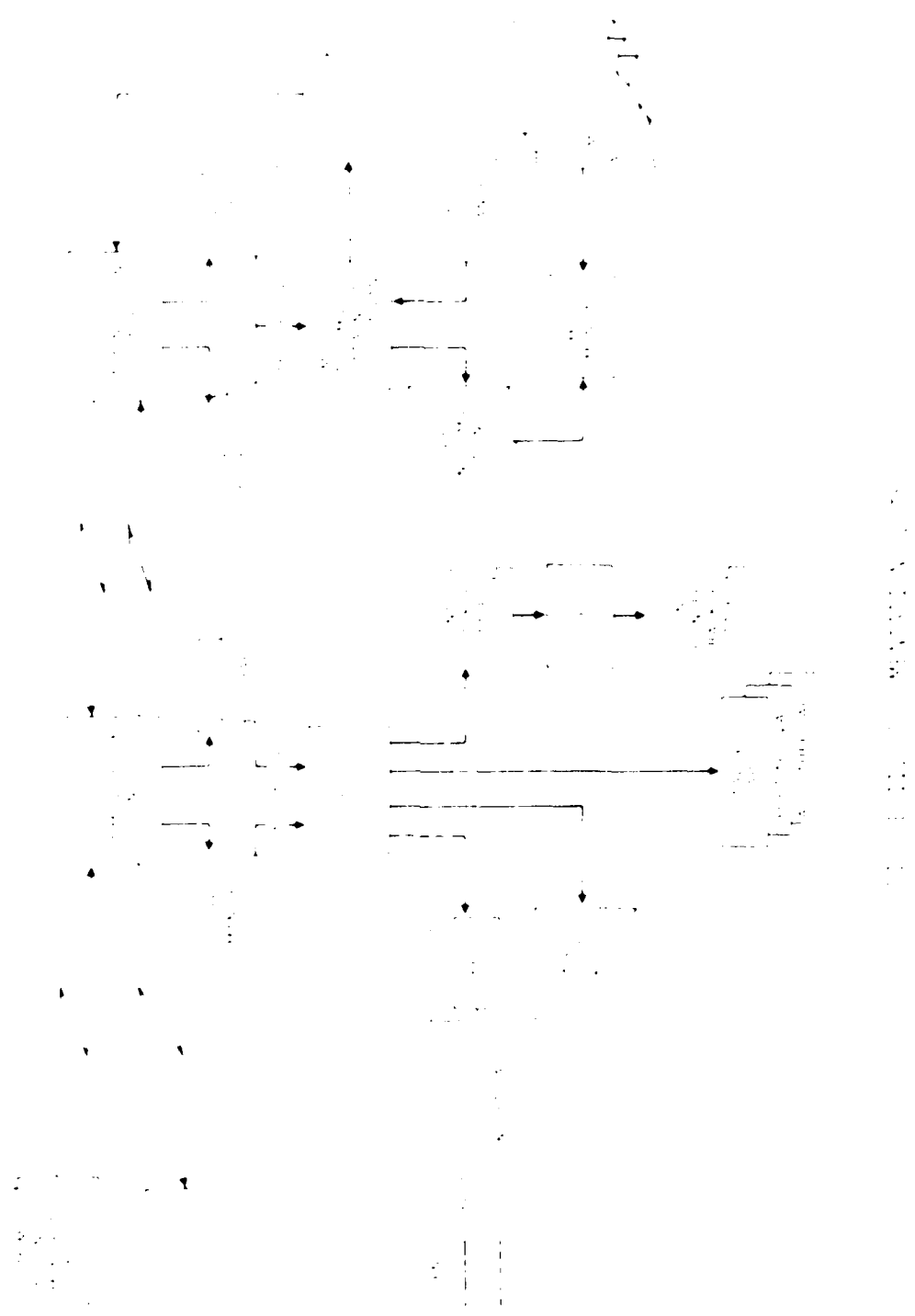


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CONCLUSIONS

The results of the study indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people. The results also indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people. The results also indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people. The results also indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people.

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It should be noted that this type of exercise was well received by the planners and participants. In general, these were areas which required an experience in order to. For example, difficulties were experienced by divers in entering the water and teachers over the beach and in the field. The results of the study indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people. The results also indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people. The results also indicate that the capability to deliver a force equivalent to 10% of the maximum voluntary contraction is possible for a group of 1000 people.

This position proved to be in error—the pins should have been at the other end. As the lift began the error became all too evident. The center of gravity of the crane assembly began to swing to a position under the suspension point, with the crane at a strong tilt. (See sketch, Figure 12.)

The tilt, however, was accommodated in the loading phase, although it did create some delay. While the ship was underway or prior to the initiation of ship unloading, the lifting frame should have been modified. The decision not to correct the location of the pins resulted in additional delays during off-loading operations.

Comparison of Crane Readiness Times for Different Assembly Configurations

The disassembly of the 300-ton capacity crane to a tactical configuration for deployment takes less time than an administrative (detailed) disassembly would for deployment on a ship with a less capable boom. This, of course, is also true for crane reassembly once the crane has been shipped to the objective area. Table 7 illustrates the differences in deployment times for the two disassembly operations. The table is based upon judgments regarding which delays are typical of real operations, which operations can be done concurrently, and the like.

In the test the 6250 crane was made ready from its minimum disassembly configuration in a shorter period than required when fully disassembled as in previous pretests. The turnaround of the crane on the beach makes a precise comparison of the times for the two get-ready operations difficult. Even after subtracting administrative delays, it is not possible to make an exact comparison.

The comparison shown in Table 7, then, should be interpreted as showing a general order of magnitude of difference in the times that could be expected between the two assembly operations, if two otherwise similar operations are compared. The table indicates what times were included and excluded in the comparison.

Looked at in total, the savings in time by moving the crane in its minimum disassembly configuration is about 2 days. This difference depends on the assumptions made. These assumptions concern such matters as:

- Whether the loading bottleneck will be the heavy crane (in effect, Table 7 does assume this);
- The order of unloading from the ship (the components for the 9125 and 6250 cranes are assumed to have priority for unloading); and
- Whether the assembly of the 9125 crane could be done concurrently with the discharge of the 6250 crane components from the ship (as assumed in Table 7).

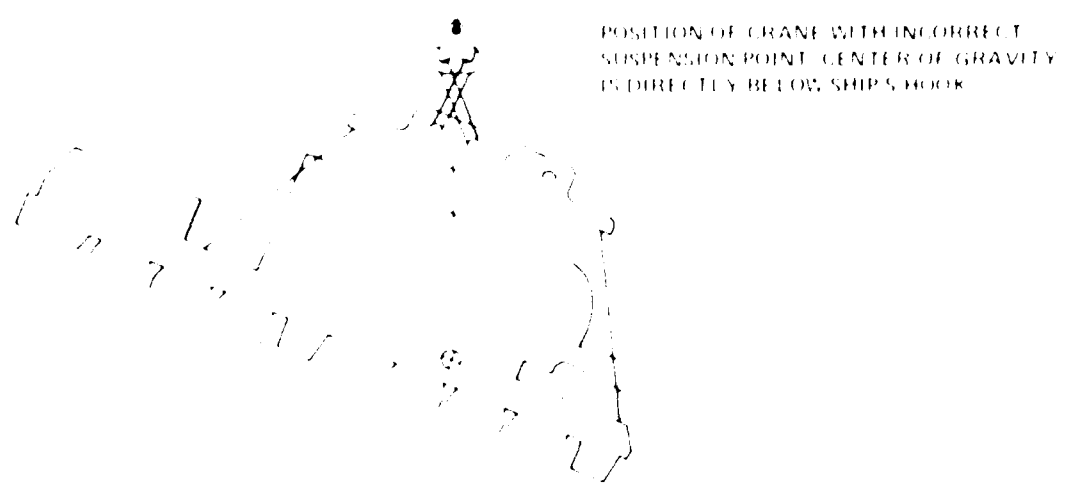
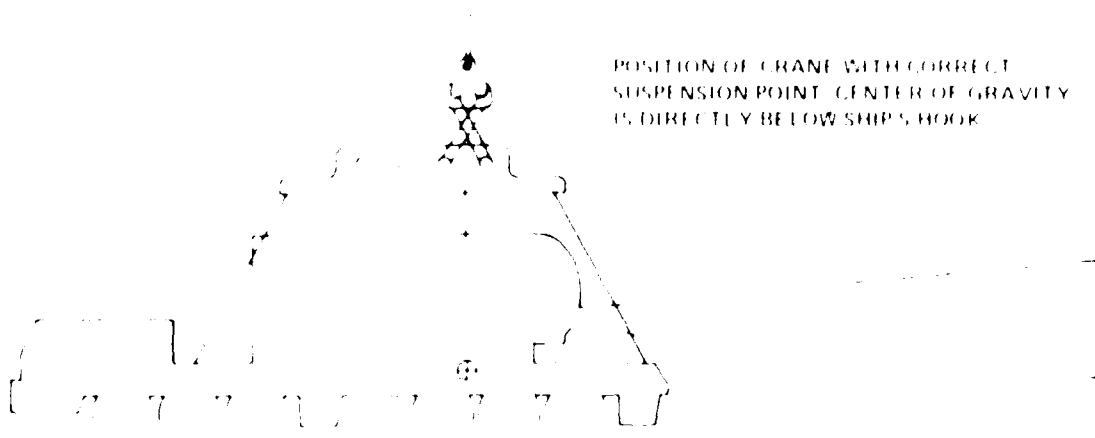


FIGURE 1. SCHEMATIC SHOWING CRANE TILT
 Tilt resulted from incorrect selection of holes
 in top member of hoist rig.
 (Not to scale.)

TABLE 1
 MINIMUM TIME TIMES FOR DEPLOYING HEAVY CRANE

Administrative, Disassembled (250 (as in previous pretest))		Minimum Disassembly (as in Heavy-Lift Ship pretest)	
Disassembly and Loading Times			
Disassembly and mobile loading (as reported on 411-11) 42 hr		Partial disassembly and mobile loading of booms and ctrwts. 11 hr	
Transit time to port not counted		Transit time	0
Loading times counterweights, booms, etc. 27 hr		Single heavy lift	1 hr
Loading times counterweights, booms, etc. 27 hr		Counterweights, booms, etc.	2.7 hr
	89.4 hr		16.7 hr
Off-loading times (at objective area)			
Off-loading needed to assist disassembly 1.5 hr		Off-loading assembled crane	1.5 hr
Booms 1.5 hr			
Counterweights 1.5 hr			
Monitor Total off-loading	4.5 hr		4.5 hr
Movement to shore			
Transit time for last boat; free transit time with 100 lb component with off-loading 1.0 hr		Ship-to-shore transit time	1.0 hr
Transfer time at shoreline, time on the last boat; free to walk to component with off-loading 1.0 hr		Transfer time	1.0 hr
	2.0 hr		2.0 hr
Assembly times (based on best estimates)			
Reassemble 9125 crane 13 hr		Install operator's module	1 hr
Reassemble 6250 crane 20 hr		Assemble booms and counter- weights	3 hr
	33 hr		4 hr
	34.4 hr		11.7 hr
Difference attributable to degree of disassembly 11.3 hr			

Even if the assumptions listed are not realized in a contingency and the listed components of the deployment times are different from those shown in the table, it is judged that there would still be a definite advantage. This advantage would be in the order of two days if the more fully assembled crane configuration is possible for deployment. This advantage is gained by the use of a heavy-lift ship that can load and discharge the crane (tactically disassembled) and the type lighter needed to transport the 6250 crane (in its more nearly operational configuration) to shore.

The decision on which configuration to use in moving the 6250 crane will be dictated by the shipping available. Assuming that in a future emergency heavy-lift ships will have other cargo competing for sea transport, a comparison like that shown above would be of value in making a decision on shipping allocations. In either case, if shipments must be delayed until an appropriate estimate of combat capability has been established in the objective area.

One of the major allocation considerations are the lesser risks in the transport of the heavier, fully assembled crane versus the risks of reassembly if it after it has been detail-stripped. Detail stripping is necessary to permit the crane being carried on a ship that can load and off-load components weighing only 10,000 tons or less. The detailed disassembly and reassembly includes the need for more highly skilled and experienced personnel and still carries the risk of not being able to assemble those fitting components that might have been damaged in transit.

Moving Cranes Ashore from Ship

Transit of the cranes from the ship to the vicinity of the beach from their respective lighters, the LCC and the LMC, presented no problem. But lighters close to the beach presented real difficulties at low tide and some problems even at high tide. Thus, the sandbars were a considerably delaying factor in landing in the operations at Green Beach, Ft. Story. For the lighters amphibians are, of course, an answer to sandbars and the beach gradient problems. However, during the deployment phase and ship-to-ship movement, even the largest amphibious vehicle (the LARC-11) is not capable of lightering either crane. In any case, these vehicles are in short supply and are themselves difficult to deploy. Thus, for deployment with landing craft, beach gradient and sandbar problems appear to need further study, in the light of the potential problems they present to equipment deployment, especially LMC equipment.

CONCLUSIONS AND RECOMMENDATIONS

The use of the heavy-lift ship to deploy 140t-class LCCs was reaffirmed as a tried and proven procedure during the pretest. However, the Navy's new 1646-class LC which had been scheduled for loading was not because neither the ship nor the Navy had the necessary sling. As part of the charter agreement the ship is required to carry other LC slings but no requirement has been levied for carrying a sling needed for this type landing craft. Since this is the predominant LC in the Navy and the older Army LCCs will be phased out in favor of a craft similar to the Navy's, this shortcoming should be rectified.

From the point of view of the best use of the heavy-lift ship as a resource with severe limitations on the total quantities of equipment it can carry, its lift capability is still most important. MCR has 16 ships that can carry LMs, causeway sections, and, potentially, BC barges, but it has only these two ships that can carry four LMs each. An LC is necessary for carrying a fully-assembled crane and it has a greater container lightering capacity that is relatively unhindered in improved beach operations. It also has capabilities to operate longer in heavy weather than other types of landing craft.

CAUSEWAY FERRY BEACHING

The causeway ferry was the only non-amphibian lighter in the pretest that was able to function at any desired stage of the tide and could cross sandbars that hindered other landing craft. The reason for this is the shallow draft of the causeway, particularly its shoreward end when left unloaded. The shallow draft permits a close approach to the beach and its light weight forward permits the shore end to be pushed up on the sand toward dry land. The section at the shore end is, thus, literally a causeway leading out to the cargo-carrying sections of the ferry which remain in deeper water. The total length of the four-section ferry used was 460 ft, although additional sections can be added increasing the length.

The operation in which the causeway was loaded with containers placed with trailers on the beach athwartship was in the overall more efficient than the operation in which the containers were placed on military chassis. This was because much greater accuracy was required to land the containers on the military chassis, which proved to be difficult and time consuming.

For the operation without trailers the containers were placed directly on the causeway. The possible disadvantage is that loaded in this manner there is a greater chance the containers are likely to get wet in other than a calm sea. Also, the containers had to be positioned athwartship for unloading by a front loader on the beach. This required tagline handlers to turn the suspended containers 90 degrees or more. This was accomplished, however, without great difficulty, since the containers are 16 ft long and the causeway is 21 ft wide, there is little room along the edge of the causeway for tagline handlers to maneuver the swaying containers.

For unloading the ferry on shore the front loader was very effective. It was only one unit was slow since the same front loader was also used to position each container on a trailer. The five containers were unloaded in just over 1 hr, or approximately 68 minutes each. If two front loaders had been available this time could have been greatly reduced. An empty loader could move onto the causeway immediately after its predecessor left with a load. Another way to reduce the causeway unloading time, at the expense of some double handling and possible truck delay, would be to have the single front loader drop each container at a point near the causeway until it was unloaded. Then the front loader would load trailers until another loaded causeway ferry was beached.

The causeway ferry provides a beaching capability where landing craft are not able to function. Its use should be considered by the JIC in its lightering mix during periods of the main test when landing craft are unable to beach.

CONFIDENTIAL - SECURITY INFORMATION - UNCLASSIFIED

The purpose of the following report is to provide information to military personnel who are interested in the results of the tests. It is expected that the test results were useful in planning the future test and in general concepts for the development of the test at this time with a view to further development.

The information reported in this report is based on the results of the tests conducted at the test site. The results of the tests are reported in the report which is available to the public. The results of the tests are reported in the report which is available to the public. The results of the tests are reported in the report which is available to the public.

The following information is provided for your information.

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THE UNIVERSITY OF MICHIGAN

The first part of the report deals with the general situation of the country and the position of the various groups of the population. It is followed by a detailed description of the economic situation and the results of the various surveys conducted during the year. The report then discusses the social and cultural conditions of the country and the progress of the various reforms. The final part of the report contains a summary of the main findings and a list of recommendations.

The report is divided into four main parts. The first part deals with the general situation of the country and the position of the various groups of the population. The second part describes the economic situation and the results of the various surveys conducted during the year. The third part discusses the social and cultural conditions of the country and the progress of the various reforms. The final part contains a summary of the main findings and a list of recommendations.

The report is written in a clear and concise style and is well organized. It provides a comprehensive overview of the country and its various aspects. The data presented is accurate and reliable. The report is a valuable source of information for anyone interested in the country and its development.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that this is essential for ensuring transparency and accountability in the organization's operations.

2. The second part of the document outlines the various methods and tools used to collect and analyze data. It highlights the need for consistent and reliable data collection processes to support effective decision-making.

3. The third part of the document focuses on the role of technology in data management and analysis. It discusses how modern software solutions can streamline data collection, storage, and reporting, thereby improving efficiency and accuracy.

4. The fourth part of the document addresses the challenges associated with data management, such as data quality, security, and privacy. It provides strategies to mitigate these risks and ensure that data is used responsibly and ethically.

5. The fifth part of the document discusses the importance of data governance and the establishment of clear policies and procedures. It stresses that a strong governance framework is necessary to ensure that data is managed in a consistent and compliant manner.

6. The sixth part of the document explores the role of data in strategic planning and performance management. It explains how data-driven insights can help organizations identify trends, opportunities, and areas for improvement.

7. The seventh part of the document discusses the importance of data literacy and training for all employees. It emphasizes that having a data-driven culture is essential for maximizing the value of data and driving organizational success.

8. The eighth part of the document provides a summary of the key points discussed and offers recommendations for further action. It encourages organizations to continuously monitor and improve their data management practices to stay competitive in a data-driven world.

THE HISTORY OF THE UNITED STATES

The first part of the history of the United States is the discovery of the continent by Christopher Columbus in 1492. This event led to the establishment of the first permanent European settlements in North America.

The second part of the history is the period of the American Revolution, which began in 1775 and ended in 1783. This period was marked by the struggle for independence from British rule and the signing of the Declaration of Independence in 1776.

The third part of the history is the period of the early republic, which began in 1789 with the signing of the Constitution and the election of George Washington as the first president.

The fourth part of the history is the period of the westward expansion, which began in the early 19th century and continued until the mid-19th century. This period was marked by the discovery of gold in California and the settlement of the western frontier.

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Table A-1
 SUMMARY OF DATA

Deck heights	
Deck height at upper deck	10.0
Deck height	10.0
Deck height	10.0
Deck height	10.0
Deck height	10.0
Deck height	10.0

Deck	Deck heights				
	Deck height	Deck height	Deck height	Deck height	Deck height
Deck 1	10.0	10.0	10.0	10.0	10.0
Deck 2	10.0	10.0	10.0	10.0	10.0

- Maximum height of the deck 10.0
- Maximum height of the deck 10.0
- Maximum height of the deck 10.0
- Maximum height of the deck 10.0

SECRET

NAVY REPORT - ON THE OPERATION OF THE "SANDY"

DATA, Nov. 11, 1944

The test runs of the belined large pier beam (1000 tons) were before the start of the test. The large, with standard equipment, were well in a fully equipped position, was towed to the working site of the beach, 1000 tons, by the "SANDY" (see figure 1). At the start of the test, the barge was pulled ashore with a single line from the "SANDY" and a heavy breeze failed with the test. The barge is pulled out with the ropeward and about at the high water line. Two full zero attempts since the large is then ashore, but were unsuccessful. The cable to the "SANDY" is zero parted. The large was then pulled to the spot with a single line.

The following equipment was used on the large pier beam (1000 tons):

- one 2000 ton crawler crane
- one 100 ton derrick
- two trailers, one in air compressor, the other a generator
- assorted lashing equipment
- two sewers, 1000 (10 ft x 10 ft x 10 ft)

A rough calculation shows that the average draft was 1000 tons.



FIGURE B.1.1. B BELONG PIER ENROUTE TO RED BEACH

After a day with no activity (November 2), work began on positioning the ramps. Small track steel plating, mounted on rail-ties, was positioned in front of the barge on the beach to act as a foundation for the beach end of the ramp when the ramp had been winched off the barge. Concurrently, a metal lip at the shore edge of the barge was burned off with an acetylene torch to facilitate off-loading the ramp. Holes were cut in the ramps for cable hooks so that each ramp could be winched off with two bulldozers.

During the operation one bulldozer winched a little faster than the other, causing some side motion of the first ramp. As a result, the cable hole on the right side was distorted and the line came loose. A new hook-up was made to an existing clewline and the ramp was winched off the barge without further incident. The ramp was pulled to a position with one end on the beach and the other still overlapping the barge platform by approximately 10 ft.

The beach area was again graded and the beach end foundation timbers were re-aligned. The second ramp was winched off the barge. Alignment with the left ramp was assisted by an additional bulldozer. The winching this time took only 20 minutes. (Lessons learned on the first ramp were evident during the winching operation on the second.)

Next the beach was raised further on its caissons to allow a better angle for the ramps. The pier supports or beams. The supports, or ledges, are located on the vertical face of the barge end. They are at a sufficient distance below the barge deck so that when the ramps are in place, its top is flush with the barge deck.

The life-lift crane then lifted the barge end of the left ramp. At the same time two bulldozers began pulling the beach end of the ramp until the barge end was clear of the barge platform. The crane then lowered the ramp on to the support ledge. The ramp was then secured. This operation took only 5 minutes each for both ramps. An additional bulldozer was used to push the right ramp against the left. When both ramps were in place, the right side at the beach end was approximately 1 ft higher than the left. This was the situation when activities ceased at the end of the working day.

The next morning, November 4, two 15-ton cranes attempted to lift the beach end of the left ramp in order to shore it up to the height of the right side. The weight of the ramp was estimated at 25 tons. By lifting only one end, the total lift was only about 12 1/2 tons. Two attempts to lift the ramp were unsuccessful and the 15-ton cranes were secured. However, two bulldozers, working in unison, were able to lift the end of the ramp. Shoring was installed and proper horizontal alignment achieved.

As the left ramps were properly positioned and secured to the pier, a sand ramp was constructed by two bulldozers. Immediately thereafter, an Assault Vehicle Landing Bridge (ALB) positioned its scissored landing bridge over the sand ramp to the pier ramps. No problems were encountered with the ALB. Total time for the ALB operation was 4 minutes.

A final beach grading was completed at 1600 and the pier was ready for operations. Total elapsed working time for the ramp emplacement was

the following information regarding the location of the bridge and the bridge itself was obtained from the following sources:

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- [Faded text]
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The first part of the report deals with the general situation of the country. It is a very interesting and detailed account of the country's history and present state. The author has done a great deal of research and his work is well worth reading. The second part of the report deals with the political situation. It is a very interesting and detailed account of the country's political system and the role of the government. The author has done a great deal of research and his work is well worth reading. The third part of the report deals with the economic situation. It is a very interesting and detailed account of the country's economic system and the role of the government. The author has done a great deal of research and his work is well worth reading.

The fourth part of the report deals with the social situation. It is a very interesting and detailed account of the country's social system and the role of the government. The author has done a great deal of research and his work is well worth reading. The fifth part of the report deals with the cultural situation. It is a very interesting and detailed account of the country's cultural system and the role of the government. The author has done a great deal of research and his work is well worth reading.

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The eighth part of the report deals with the conclusion. It is a very interesting and detailed account of the country's future and the role of the government. The author has done a great deal of research and his work is well worth reading. The ninth part of the report deals with the appendix. It is a very interesting and detailed account of the country's future and the role of the government. The author has done a great deal of research and his work is well worth reading.

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All operations ceased during a lunch break between 1145 and 1155. During this time, the LAFS barge was at quayside. Two milvans were on the pier waiting to be shifted to the marshalling area. These milvans were ultimately shifted to the quayside after the pier approximately 4 hr after being released from the pier.

After the lunch break, operations consisted of two loaded LAFSs docking and disdocking, one LAFS was on the pier. Two additional milvans were then loaded into these LAFSs after which operations were resumed.

Early in the afternoon, however, the ALE scissor ramp was removed. Heavy gear, including the battens, were substituted, together with Morat for the scissor ramp. At this time seas were rough with wave heights estimated to be 10 ft with winds of 20 knots.

The LAFSs were on the pier but because of the surf conditions, operations were not successful. The shaft would ground out whenever it made contact with the seabed. Unsuccessful attempts to lift the milvan out of the LAFS were made. All other operations were postponed.

Operations resumed at the pier at 1159 after some difficulty with the scissor ramp. The scissor ramp and the LAFS departed. Operations were called off the pier due to the rough wind and seas.

At 1200, two LAFSs and four milvans were rapidly loaded into a LAFS barge. Heavy containers had been prepositioned on the pier before the barge moored at the quayside. After the barge was loaded, two LAFSs arrived.

One was empty with one container and the other was empty. The container was lifted, returned to the pier, and then three times. Average cycle time was 5 minutes.

Operations were resumed during the lunch break. At 1400 a LAFS barge arrived at the pier for welding repairs. The repairs continued throughout the remainder of the day. A 1 ft x 1 ft plate was welded over a hole inflicted above the waterline. This operation took up one whole side of the pier and restricted operations operations to the other side.

During the remainder of the day, four LAFSs were loaded with containers. There were no apparent difficulties.

APPENDIX C

TEMPORARY CONTAINERSHIP DISCHARGE FACILITY (TCDF)

GENERAL

The heavy-lift Breakbulk Ship Pretest helped provide data on crane capabilities and limitations in the important area of Temporary Containership Discharge Facility (TCDF) operations. This pretest was the first opportunity to use the Army's CW-4050 (300-ton lifting capacity) crane on a floating B-landing barge for the discharge of containers from the holds of a ship. In addition, it was the first time military operators were used to conduct TCDF-containership operations. Although there were some artificialities due to the lack of container cell guides, the need to top the crane boom to clear the barge beams and kingposts, and the limited opportunity for establishing a rhythmic unloading, valuable data and insights were gained.

DISCUSSION

As of this report, it is uncertain what capacity load can be safely lifted by a mobile crane mounted on a floating platform when the crane (and platform) moves in response to waves or to the load. That is, when waves are moving the platform, different kinds of stresses occur in the crane from those experienced on solid ground. Accordingly, the crane lift capability is reduced to allow for such extra or different stresses; in other words, the crane must be derated for operations in a seaway. It is possible that the point may be reached where the crane on the barge cannot safely hoist the heaviest loads. In that case, in attempting a lift there is the possibility of a catastrophic failure to some component of the crane.

Table 1
Summary of the results of the first round of the
questionnaire on the Merit System, 1971-1972

Question	Yes	No	Don't know
1. The Merit System is a fair way to select and promote government employees.	65%	25%	10%
2. The Merit System is a fair way to pay government employees.	60%	30%	10%
3. The Merit System is a fair way to discipline government employees.	55%	35%	10%
4. The Merit System is a fair way to evaluate government employees.	60%	30%	10%
5. The Merit System is a fair way to train government employees.	55%	35%	10%
6. The Merit System is a fair way to provide benefits to government employees.	50%	40%	10%
7. The Merit System is a fair way to provide a career ladder for government employees.	55%	35%	10%
8. The Merit System is a fair way to provide a pension plan for government employees.	50%	40%	10%
9. The Merit System is a fair way to provide a health insurance plan for government employees.	55%	35%	10%
10. The Merit System is a fair way to provide a life insurance plan for government employees.	50%	40%	10%

The above table shows the results of the first round of the questionnaire on the Merit System, 1971-1972. The questions were asked of a representative sample of government employees. The results show that a majority of government employees believe that the Merit System is a fair way to select and promote, pay, discipline, evaluate, train, provide benefits, provide a career ladder, and provide a pension plan for government employees. However, a smaller majority believe that the Merit System is a fair way to provide a health insurance plan and a life insurance plan for government employees.

Figure 10 illustrates the clearances and reach dimensions that will be used in the pretest in which the heavy-lift ship was acting as a substitute for a containership. A reach to the centerline of the ship is necessary to move hatch covers on many containerships. The designers of containerships, in general, follow the rule that a hatch cover can be no heavier than the heaviest container to be lifted from the holds of that ship. This limits the heavy-lift requirement to a maximum of 10,000 lb or the equivalent weight of a heavy-lift container and that of a spreader bar needed to lift it. In ships with only 20-ft containers hatch covers weigh considerably less but a factor of safety is applied to approximating the maximum requirement.

The heavy-lift ship has a beam of 110 ft. Half of this distance, the reach to the ship's centerline, added to the tender between the barge and the ship and the lift beam of the crane produce a crane reach requirement of 110 ft to centerline per the hatch of the heavy-lift breakbulk ship. This distance is 110 ft greater in Figure 10. It may be noted from Table 11 that, under the heavy-lift current generation scale for this distance, a hatch cover weighing 10,000 lb cannot be lifted. In fact, there is a 15,000 lb lifting requirement for 110 ft reach (see state no. 1). This is approximately the lift and reach needed in the pretest for the type ship chartered by the Coast Guard for this study. In fact, there are only seas and a relatively light spreader bar available for this study.

In wider containerships (most have beams of approximately 95 ft), the reach will have to be greater. It is not variable for ships this wide that a heavy-lift crane on the centerline, the reach would have to be at least 110 ft to reach centerline (centerline center) the crane would not be able to lift a 10,000 lb hatch cover. A crane designed for 20-ft containers with a lift capacity of 10,000 lb, the lift would be within the limits of the derated crane.

APPENDIX A - TABLE 11 - LIFTING CAPACITY

The heavy-lift breakbulk ship pretest was conducted using a 10-ft lift beam on the crane. The tender is 100 ft, the crane, the core of weights and the lift capacity of the crane is reduced. However, there are other instances that would require a reach to the use of a longer beam. One factor to be considered in the pretest is the requirements, ship stability, and trees and

The limited reach of the 10-ft crane used in the pretest will, generally, prevent lifting directly those containers from hatches directly perpendicular to the barge, especially with respect to those containers near the centerline. It is not probable that a reach only to the centerline of the containership will necessitate frequent repositioning in order to place the lift beam over the barge near the centerline within the barge's lifting hatch.

Crane reach to containership containership type chartered for study, with a lift beam of 10 ft. The center of gravity for the hatch cover is within 10 ft of the ship's centerline. Therefore, the reach will be 110 ft, well within the 110 ft sea state lift capacity.

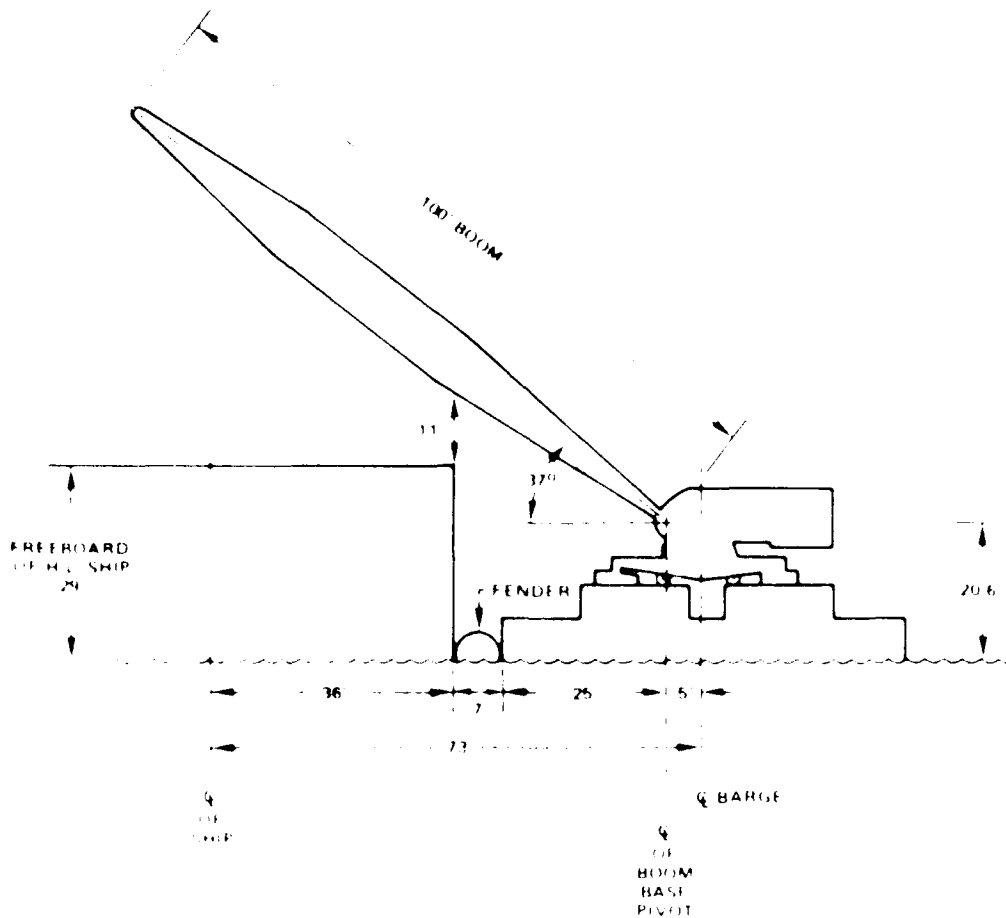


FIGURE 6.1. CLEARANCE AND REACH DIMENSIONS FOR 6050 LB CRANE
 mounted with mast-top relation, using heavy-lift ship, pretest.

A longer reach could also be beneficial in helping ship stability. This would result when the TCF is capable of reaching across the ship's centerline to unload containers. Thus, with only one TCF or CCF working this would help the ship maintain a more even keel during the unloading process than if all the containers were first removed from one side and then the other.

Another factor to be considered is the freeboard of the ship. For a container ship with a freeboard greater than the heavy-lift breakbulk ship, a longer boom would be required. This is illustrated in figure 6.1.

With the range of weights and vessel characteristics now known, more detailed planning for the configuration and operation of the crane crane on the breakbulk type TCF can be done.

APPENDIX

APPENDIX I - SUMMARY OF INVESTIGATION REPORT



FIGURE 1. S.S. TRANSCALUMBIAN (TYPE 1000). The S.S. TRANSCALUMBIAN, one of two heavy-lift breakbulk ships under long-term charter to the Ministry of Defense, was used in October 1975 for the first time in the Persian Gulf. The primary objective of the exercise was to load 1000 heavy and out-sized equipment and harbor stores at the ship at anchor in the Persian Gulf and distribute it ashore for the conduct of the exercise. The ship is shown in the foreground.



The photograph shows a large, dark, rectangular structure, possibly a building or a large container, situated on a light-colored, textured ground. The structure has a prominent vertical support or staircase on its side. The image is heavily stylized with deep shadows and bright highlights.





FIGURE 3.4. 40-FT CONTAINER. One 40-ft container was included in the load to provide data and experience in handling a 40-ft container which weighed 14,700 lbs.



FIGURE 1.5. DECK PREPARED. Lunnage was laid on deck in preparation for the heaviest lift made in the LIFT pretest program, a 140t-class Army L₁. Each of the two heavy-lift ships (the only heavy-lift ships currently in the U.S. flag fleet) can carry four of these large landing craft. A 164t-class L₁ could not be lifted because neither the ship nor the Navy had the necessary sling.



FIGURE 1-6. BOOM MARRIAGE. To lift the 180-long ton LCU, a boom marriage of two 100-ton capacity booms was made. This gives the ship a 200-ton capacity, although reportedly the ship has lifted and carried a 250-ton tug.



FIGURE 1. LIFTED WITH EASE. The LCU lift, although infrequently accomplished, was made with relative ease. Military personnel acted as stevedores but the ship's company operated all machinery and directed the technical aspects of the lift.



FIGURE 1. (MAY 1977) LIFE RAFTS. During the LC, lift the ship did experience nearly an 8-degree
list. However, the ship was designed to take a maximum of a 10-degree list during loading. A counter-
balancing system is used for heavy lifts.

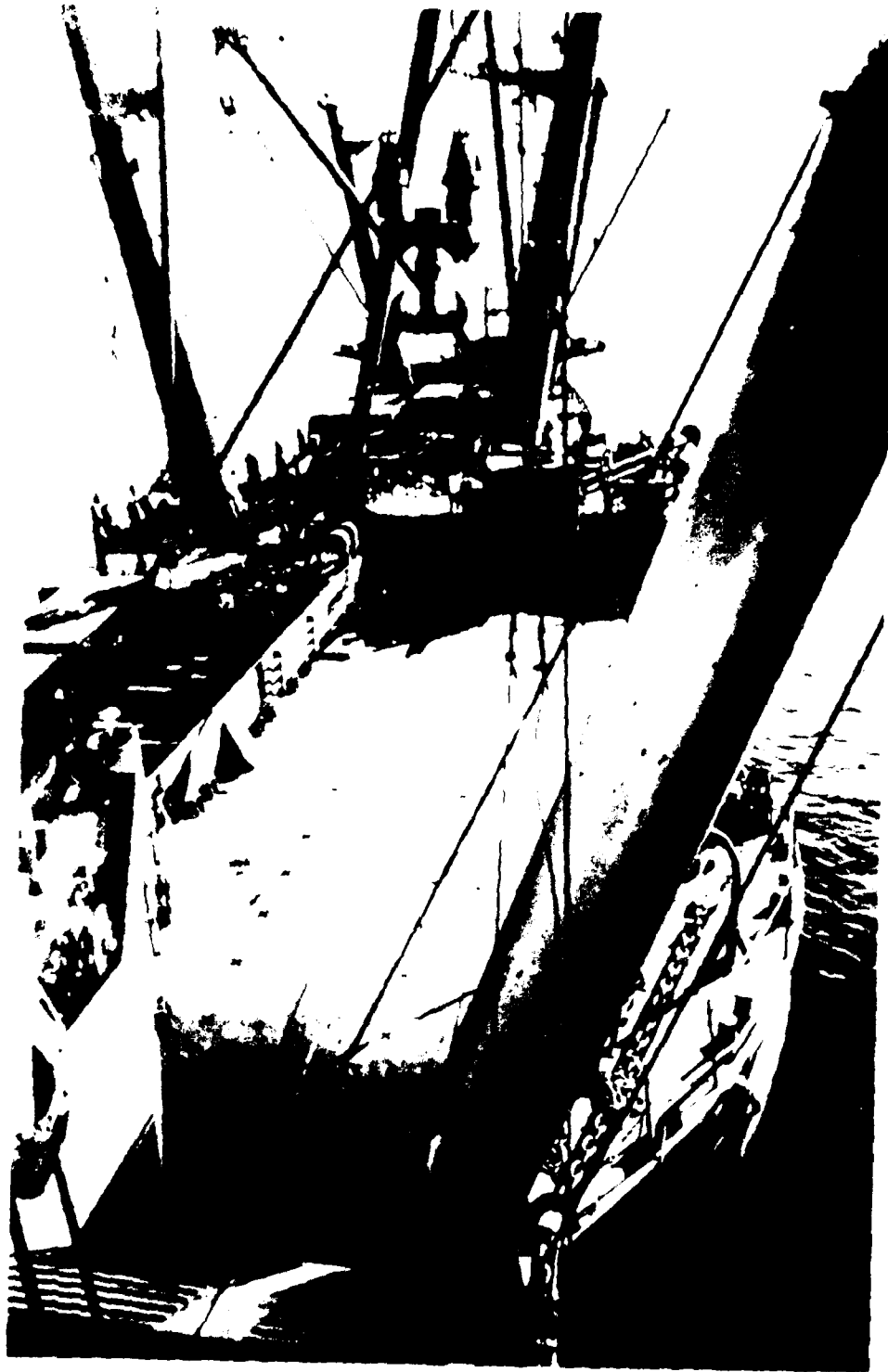
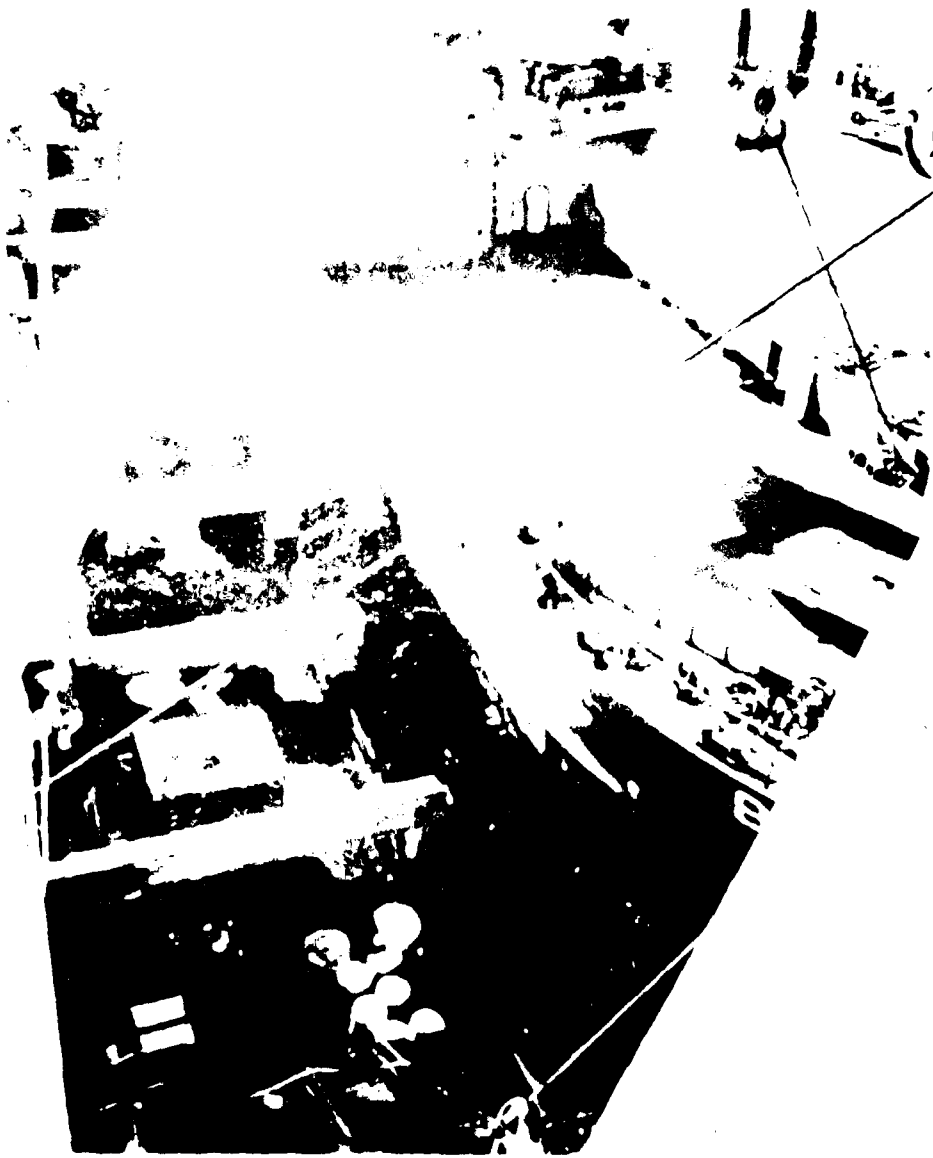


FIGURE 1. SPECIAL PREPARATIONS REQUIRED. No special preparations are required to remove the 10^4 for lifting. In this case the 10^4 mast was lowered to a lower deck level, but this proved to be unnecessary.



... ..
... ..
... ..
... ..



The above photograph shows the rigging of the ship, which is a complex system of ropes and pulleys. The rigging is used to hoist and lower the sails and other equipment on the ship. The photograph is a high-contrast, black and white image, which emphasizes the geometric shapes and textures of the rigging. The rigging is a key component of a ship's structure, and it is essential for the ship's operation. The photograph provides a detailed view of the rigging, showing the intricate details of the ropes and pulleys. The rigging is a testament to the skill and craftsmanship of the ship's crew, and it is a vital part of the ship's heritage.



The structure is the hull of a ship, showing the complex arrangement of plates and beams. The person in the upper right corner is looking towards the camera.

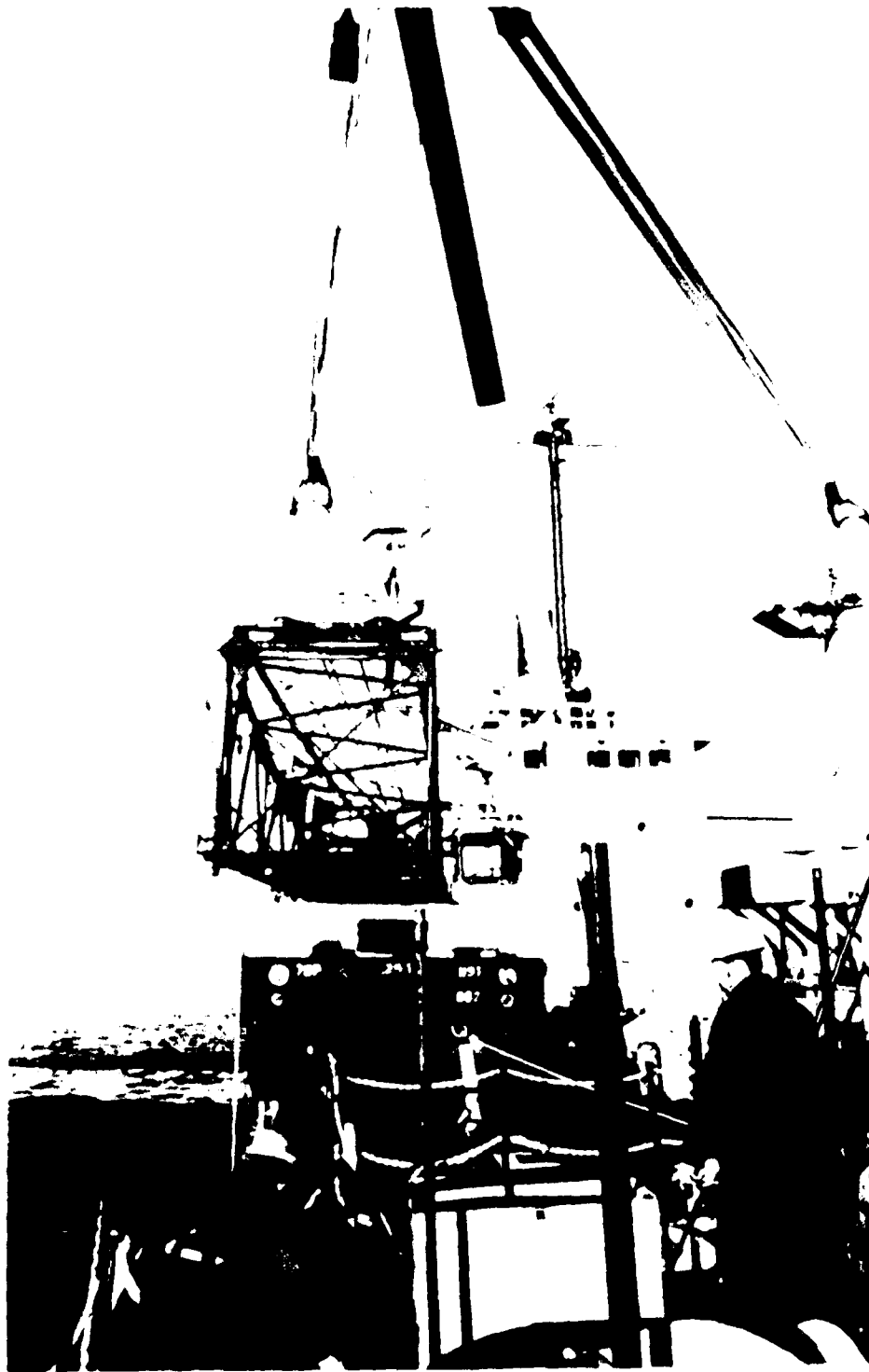


FIGURE 1. CRANE LIFTING THE HULL. In fitting the 14-ft. plate into the hull, the crane is 100 ft. long, which is 10% ft. long, but more than adequate to handle the hull's weight.

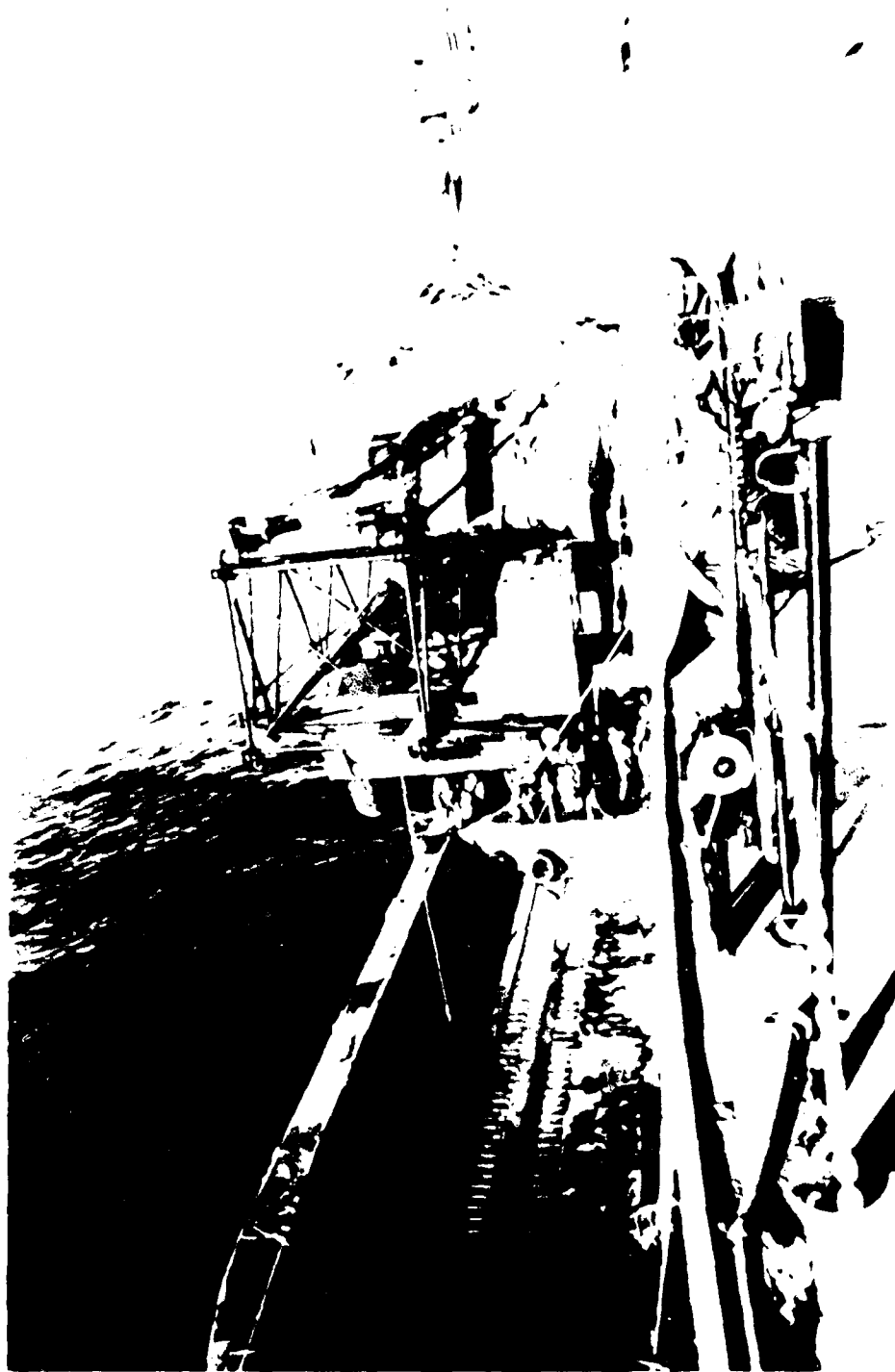
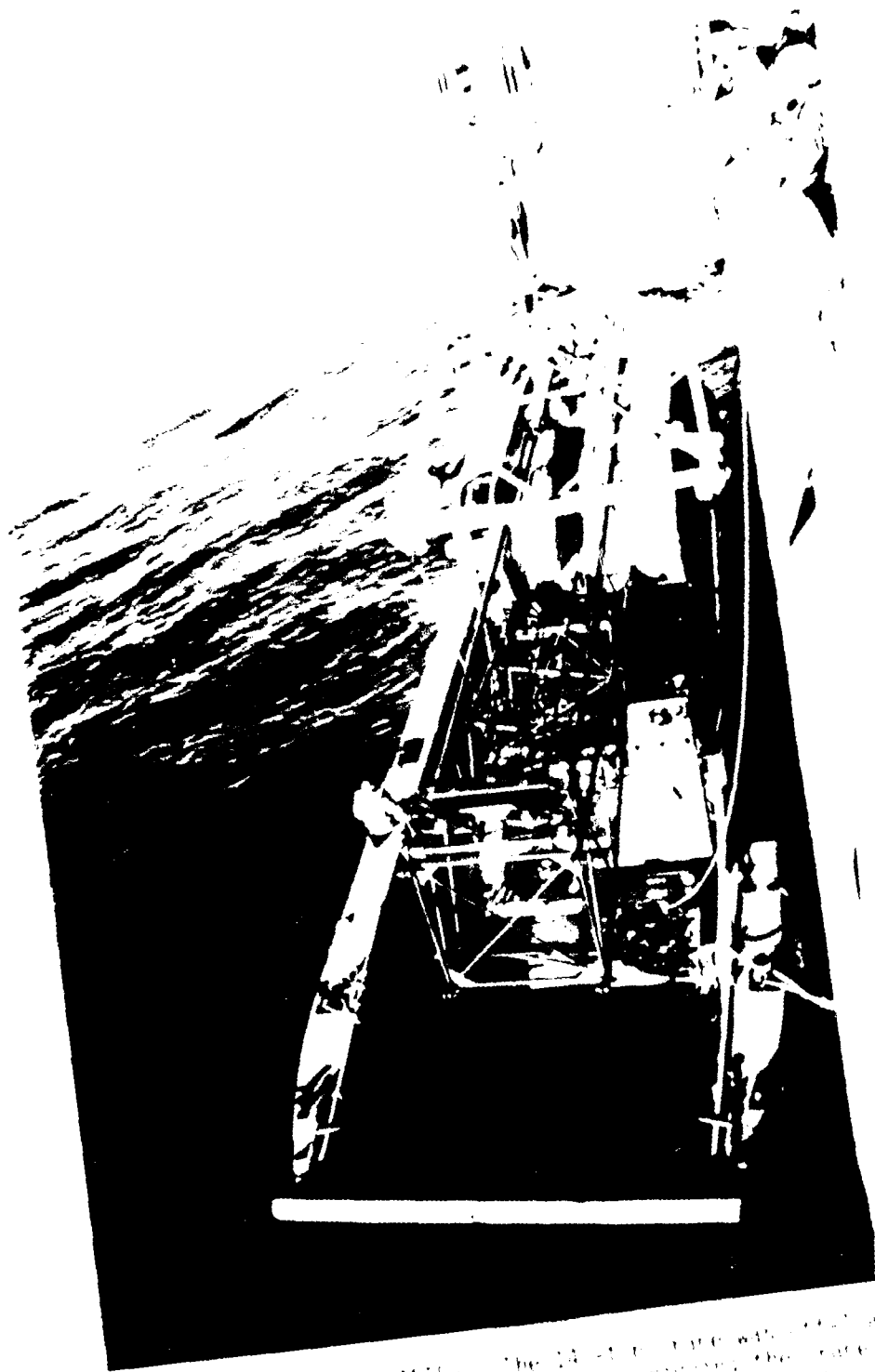
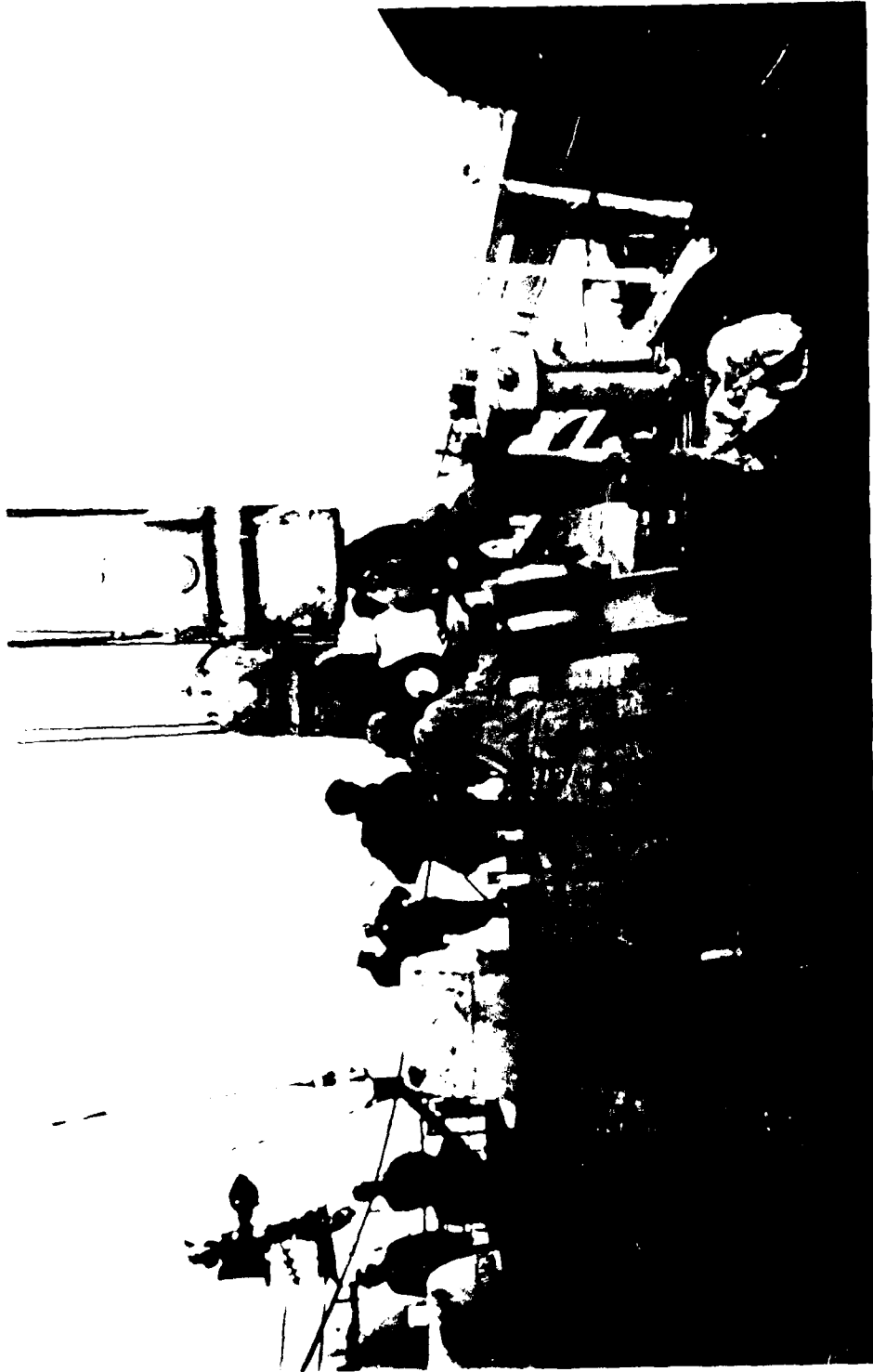


Fig. 1. The case of a machine for drilling holes in the ground. The machine is a vertical one, and it is used for drilling holes in the ground. The machine is a vertical one, and it is used for drilling holes in the ground. The machine is a vertical one, and it is used for drilling holes in the ground.



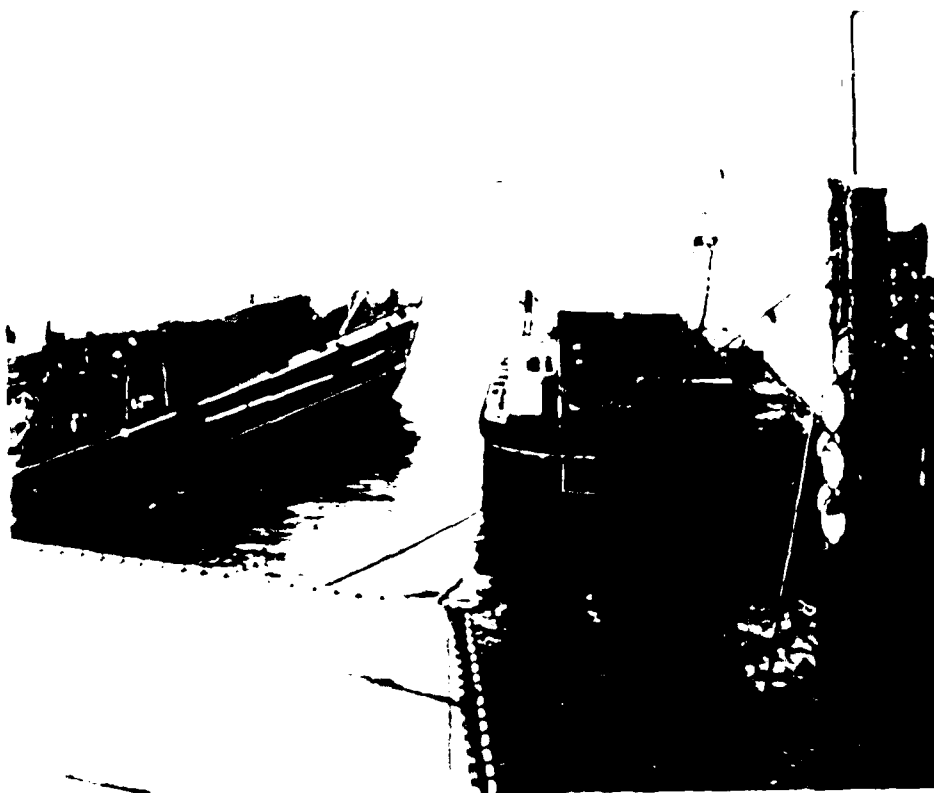
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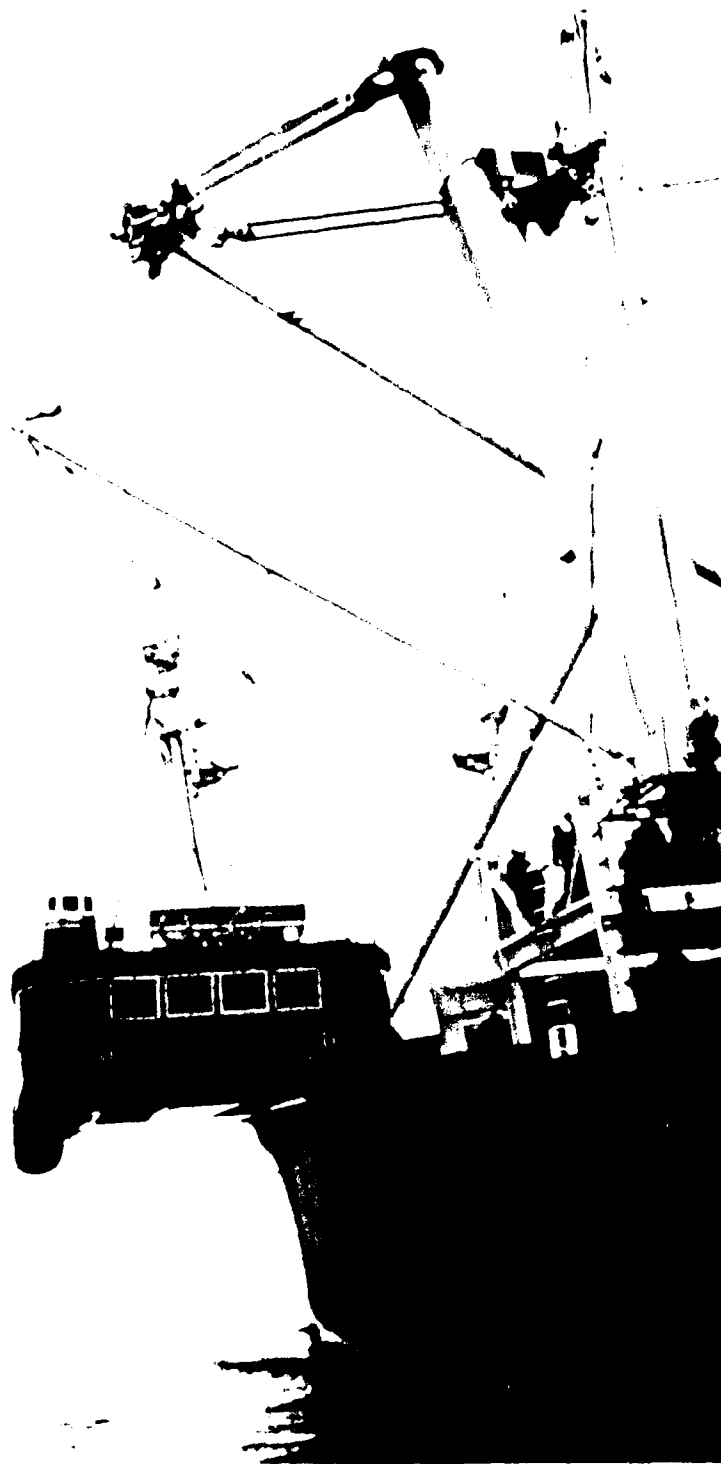
WAG-41 crew members are seen on the deck of the ship during a mission. The image is a high-contrast, black and white photograph showing a group of people on a ship's deck. The scene appears to be a busy deck area with various equipment and structures visible.



The above view provides a perspective of the existing structure. The structure has a minimum clearance of 10 feet and a clearance to the top of structure of 10 feet.



10. A large, rectangular object, possibly a piece of machinery or a container, is being hoisted or moved by a crane or derrick. The object is suspended by cables and is positioned vertically. The background is bright and overexposed, suggesting an outdoor setting.



U.S. NAVY. U.S. MIN. 111. The structure shown in the photograph is a crane used for lifting heavy loads. The crane was used to lift the 100-ton weight of the 100-ton weight.

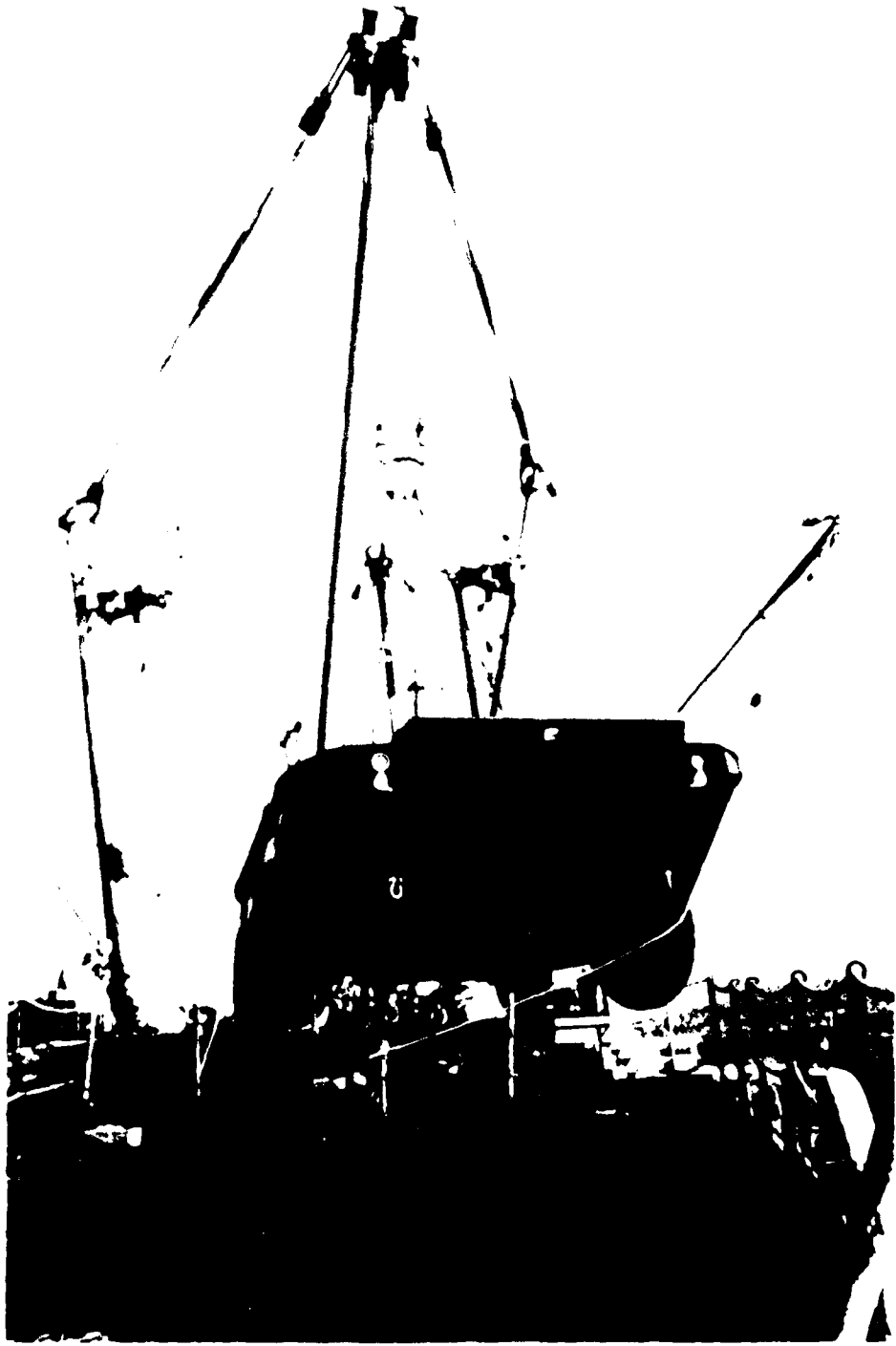
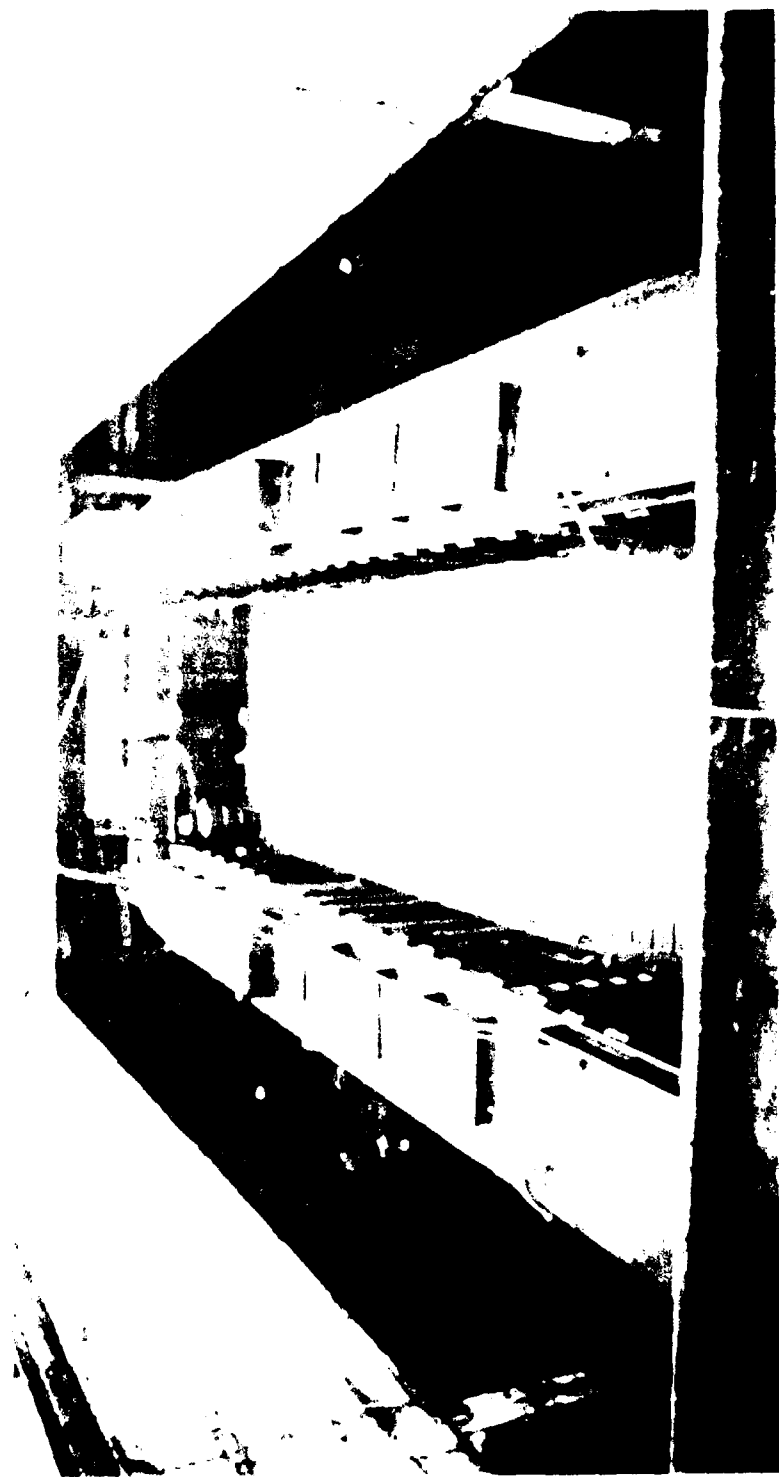


FIGURE 10. OVERHEAD CLEARANCE WITH 1400 PPM. No overhead clearance problems were experienced by the 1400-ton crane winches; the 20.5-m high (LAP-1) across the deck and over the rail.





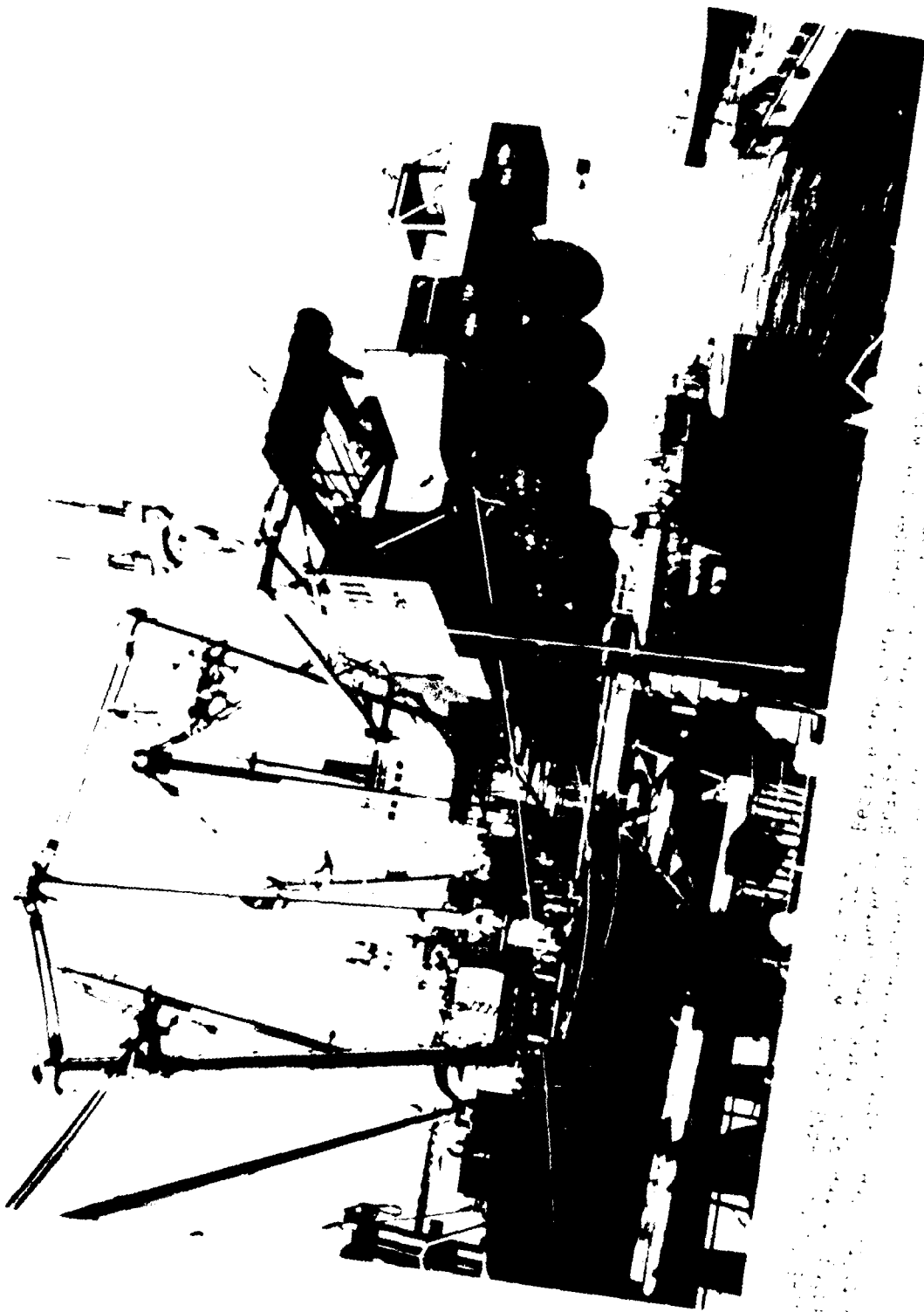
The photograph shows a large, dark, cylindrical object, possibly a piece of machinery or a container, mounted on a structure. The object is oriented vertically and appears to be secured by a horizontal band or cable. The background is bright and overexposed, showing faint outlines of structural elements and possibly other equipment. The image is framed by a thick black border.

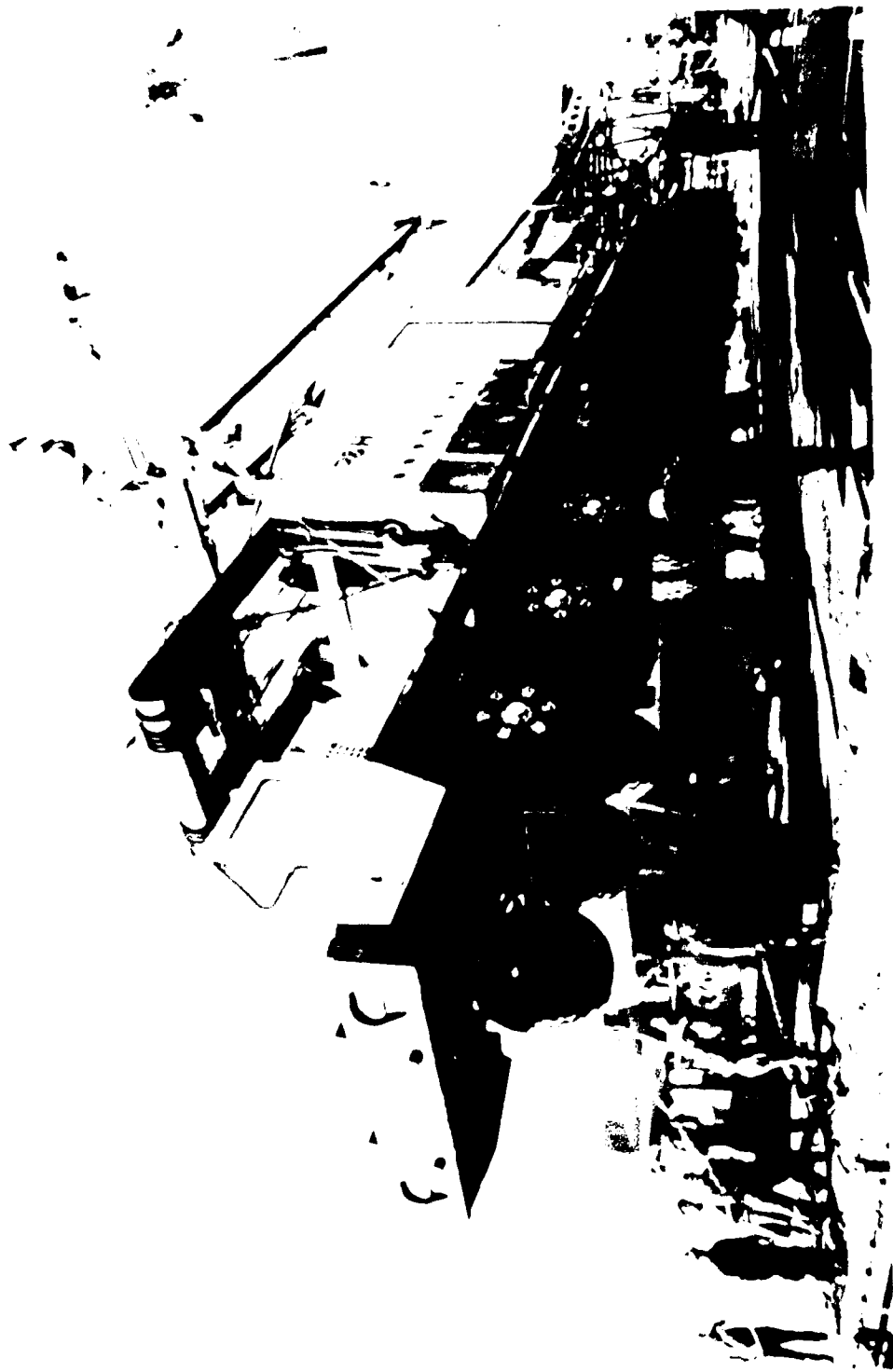


FIGURE 1. Aerial view of the MV-19. Approximately one-third of the 16-minute test time was spent hoisting the MV-19 and another the amphibious landing was completed in the remaining time.



The photograph shows a large, dark, vertical structure, possibly a ship's hull or a large building, with a complex, lighter-colored structure on top. The image is heavily shadowed and lacks fine detail.







...the vessel was ...



A person standing on the deck of a boat, looking towards the camera. The image is high-contrast and grainy.

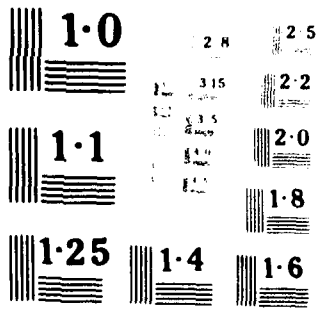




FIGURE D.29. SIDELOADER EASY LIFT. Compared to the other equipment embarked the sideloader went aboard relatively easily. It weighs 64 long tons and is 41 ft long, 12.5 ft wide, and 11.7 ft high.

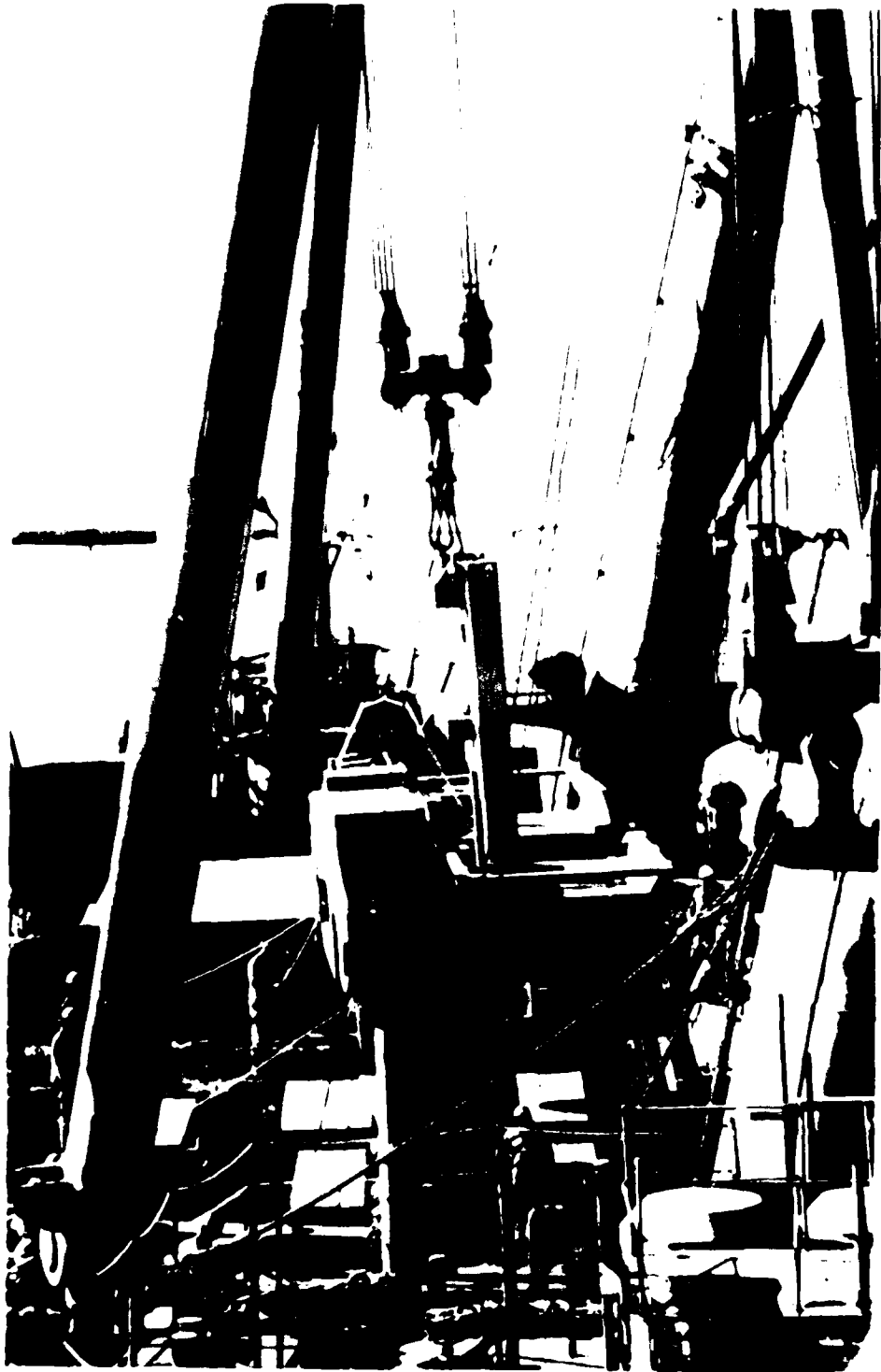


FIGURE D.30. SIDELOADER DECK-STOWED. The sideloader could have been stowed in a hold but to reduce loading time so that other events could be accomplished, it was deck-stowed. Its loading time was only 27 minutes, including rigging time.

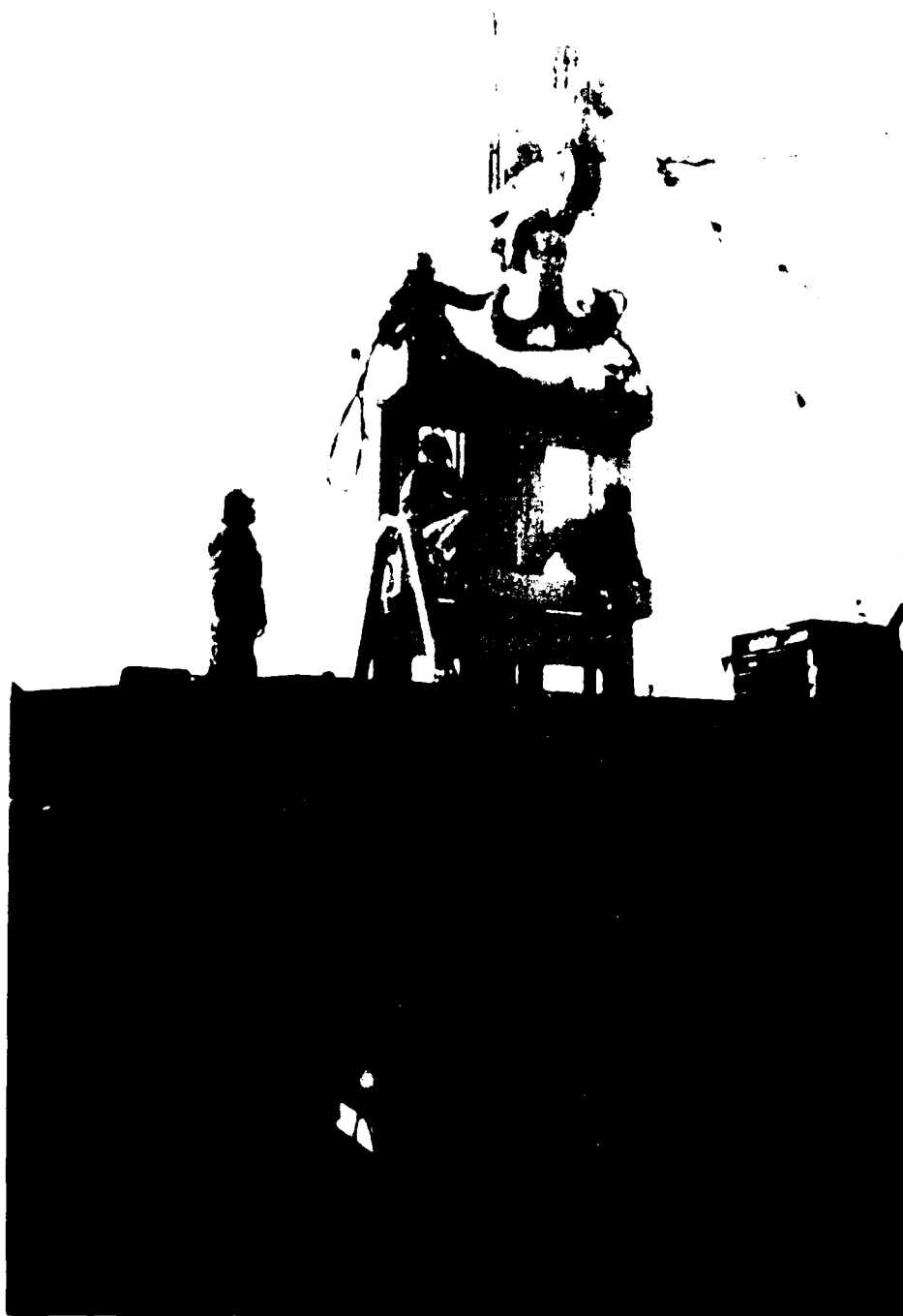


FIGURE 1.41. STEEL BEAM BEING LIFTED BY CRANE. The crane loader for lifting it is necessary to climb at least and attach to the hook. The attach and detach the chokers on the hook required a total of 10 minutes for the loading cycle and 9 minutes during off-loading.

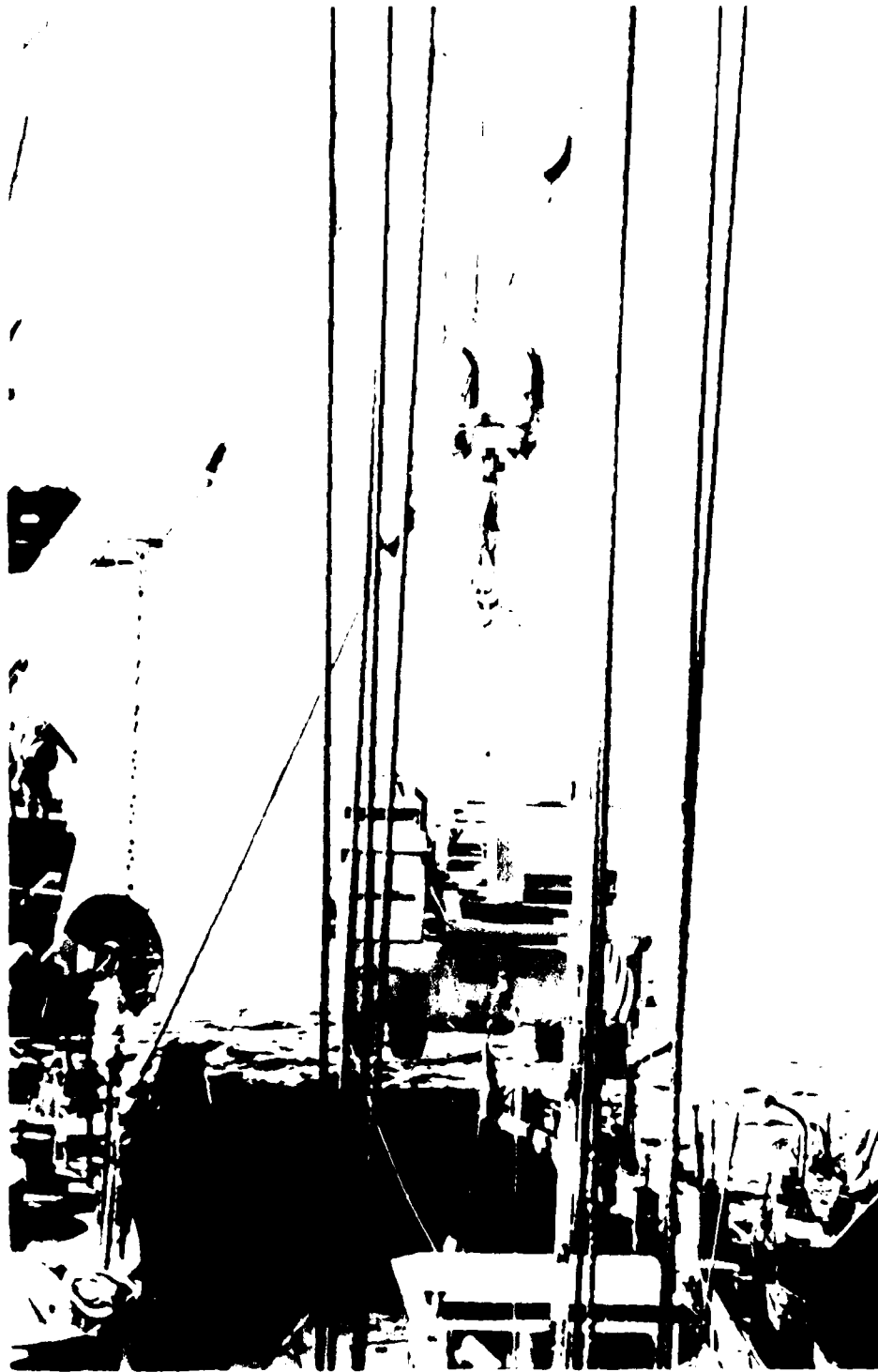


FIGURE D.32. SIDELOADER PLACED IN LCU. No difficulties were experienced off-loading the sideloader into an LCU. The sea state was relatively calm and the wind was light.

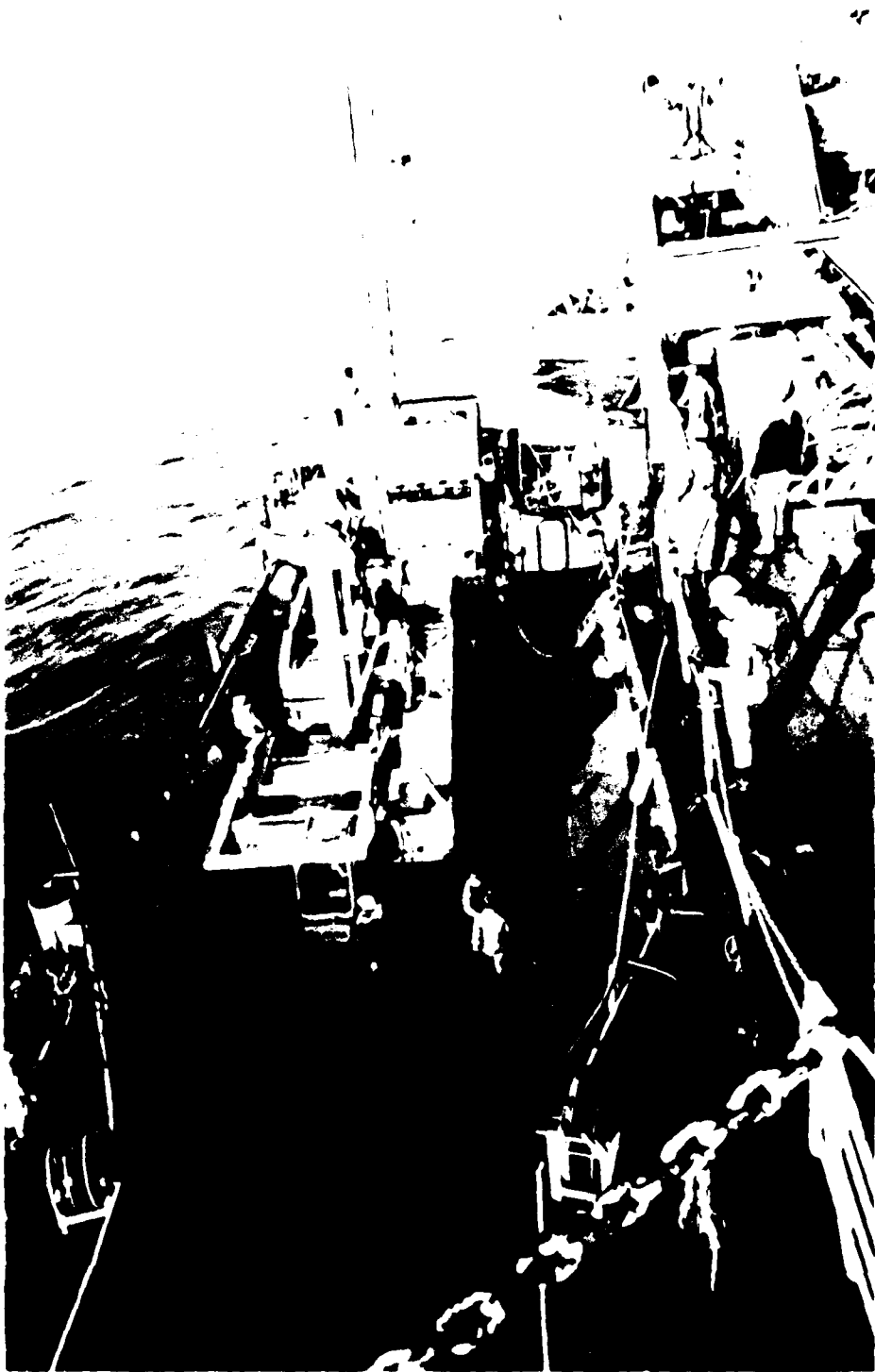


FIGURE 10. OFF-LOADING TIME 34 MINUTES. The side-loader lift was the fastest one made. It took 34 minutes to off-load the side-loader, including time to hoist and cast off the LCU.



FIGURE D.34. TCOF TOWED TO PRETEST SITE. Once the deployment cargo had been off-loaded, the TCOF was positioned alongside the ship so that containers could be off-loaded and throughput events could begin.

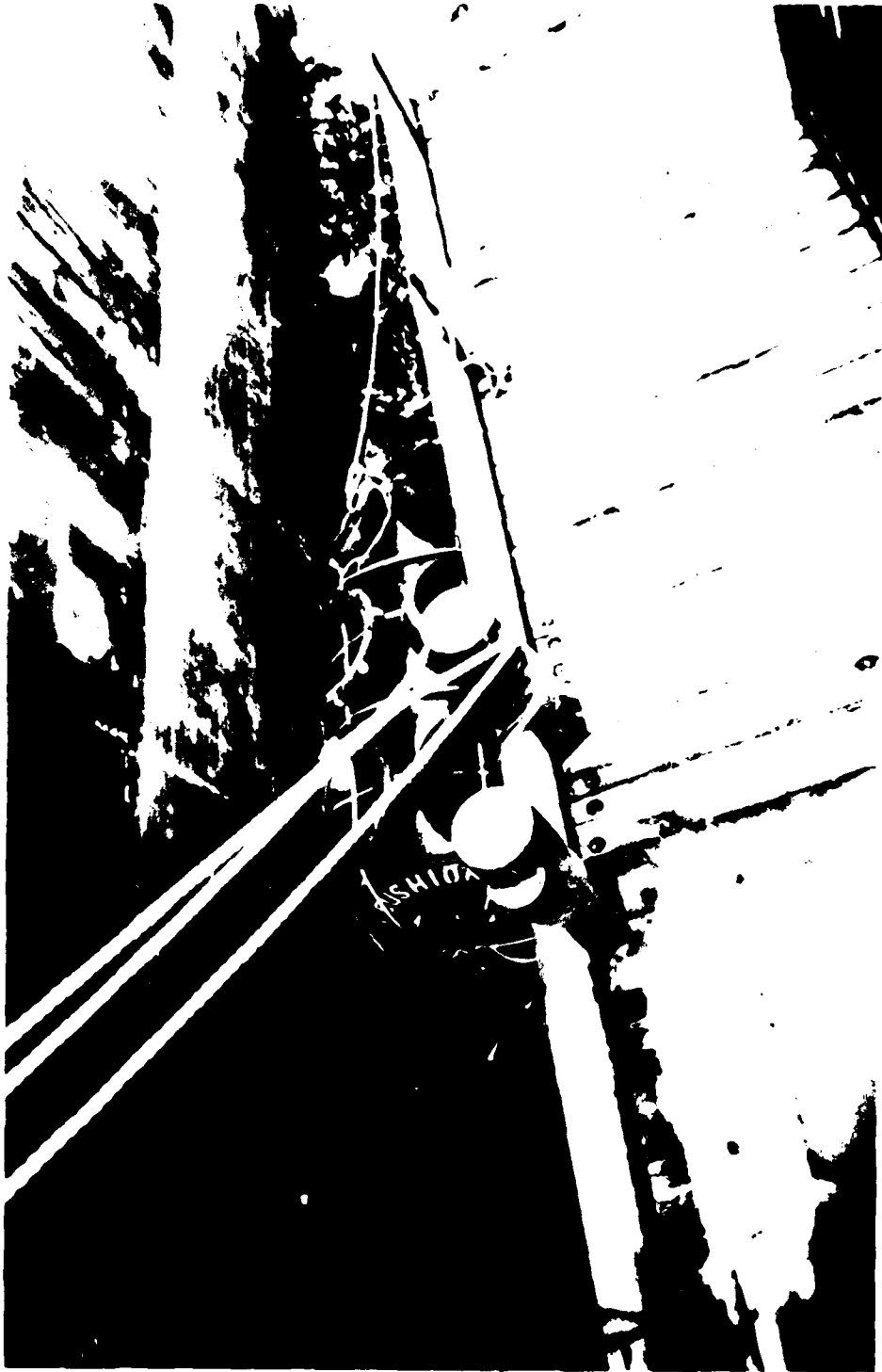


FIGURE D.35. FENDERS USED. Two special inflated fenders, one of which is shown above, were used to separate the TCOF from the ship.



FIGURE 1. CRANEWAY AT THE BOW. After the initial load of containers had been discharged the TCCF was moved to the bow of the ship. Later, when the TCCF had swung into the gap at the bow shown in the photo above, the container spreader had to be turned further to line up with the containers. This was difficult because a two-point attachment was used between the crane and the spreader bar.

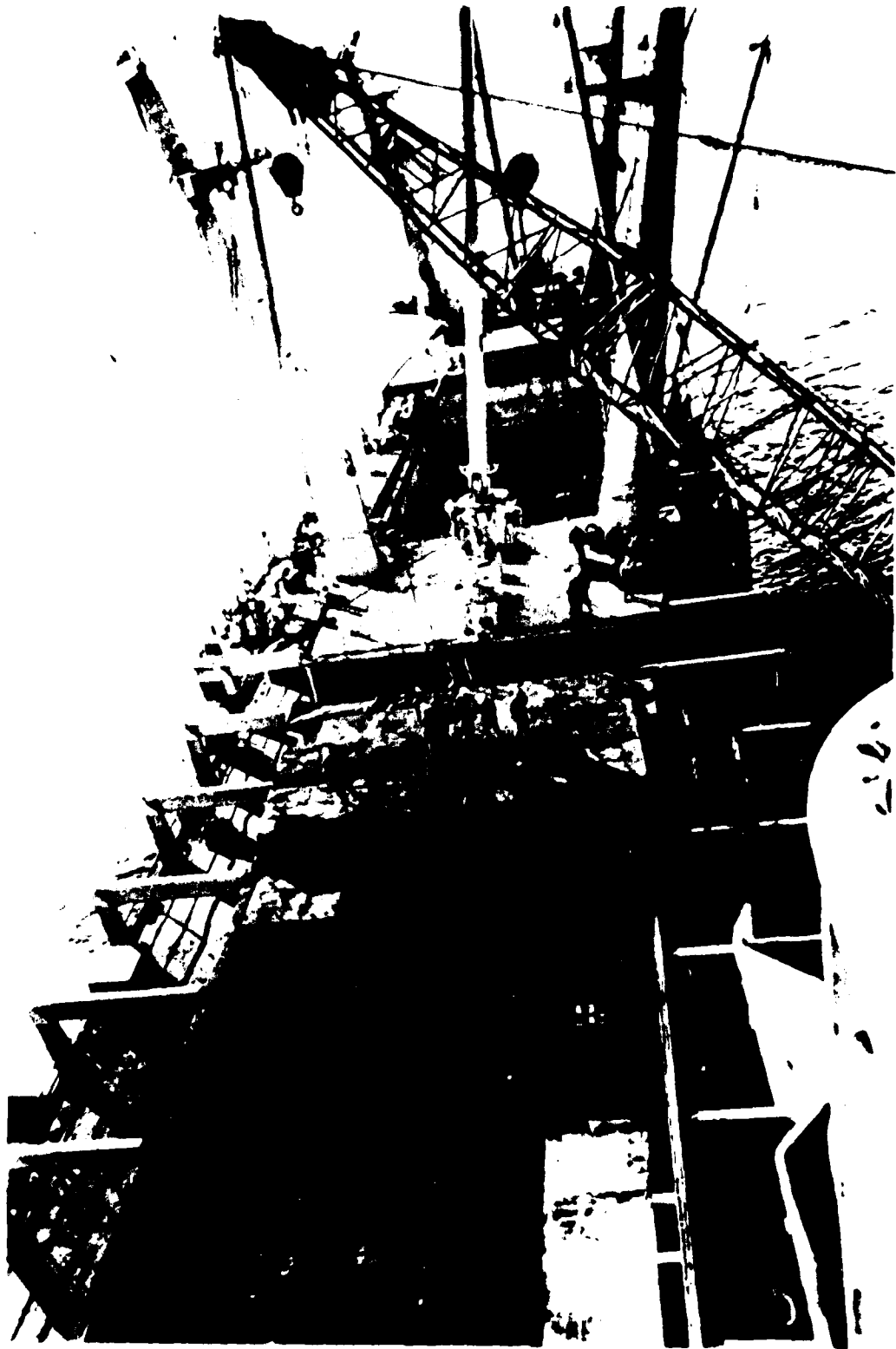


FIGURE D.37. TCDF OPENS HATCH. To gain experience and crane data on hatch square opening, the TCDF was used to remove the 5-ton sections of the hatch cover.

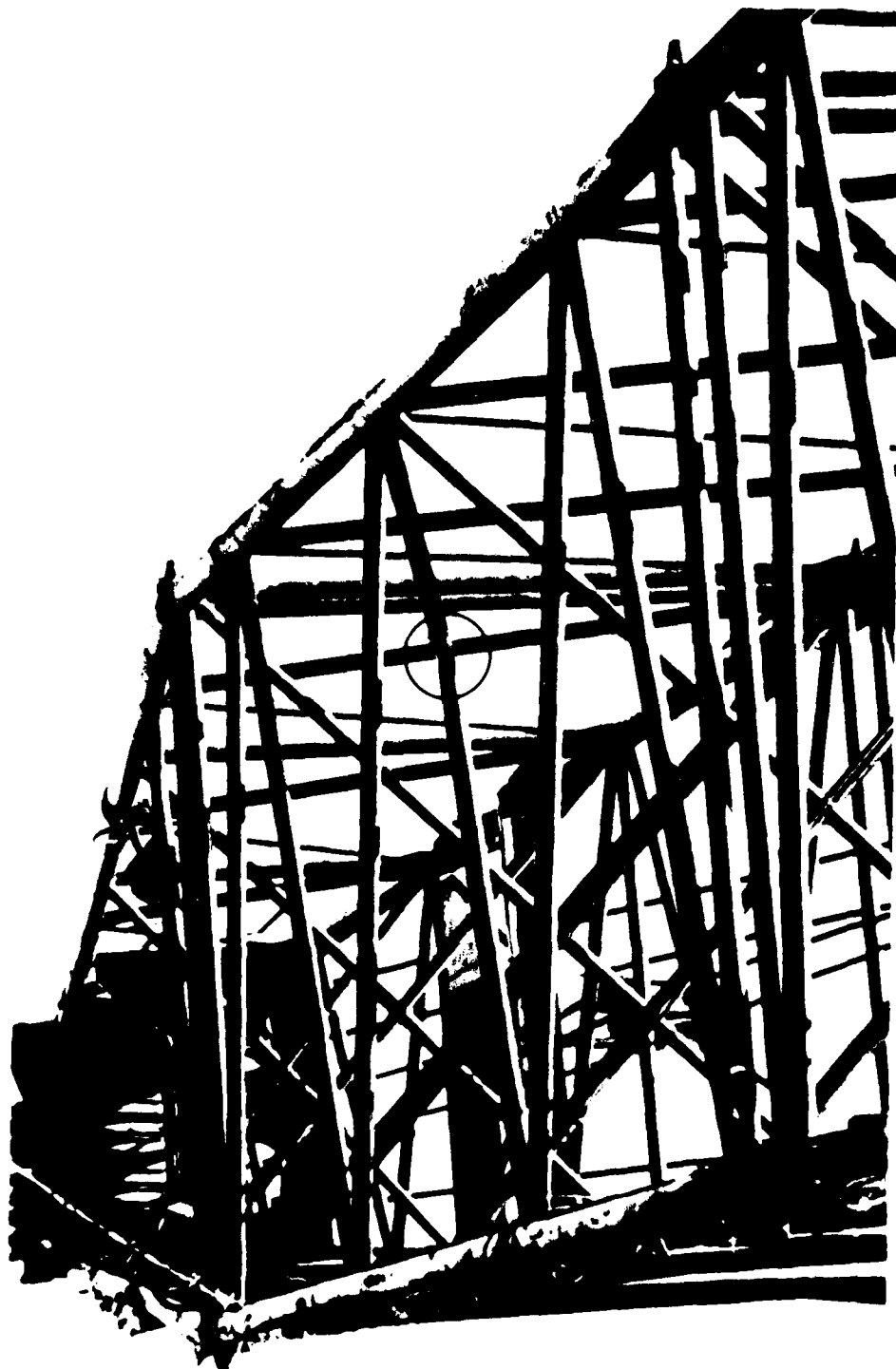


FIGURE D.38. BLOCK DENTS CRANE BOOM. On the first full day of container unloading the sea state caused the crane's block to pendulate during a break in the unloading. The heavy block struck the boom's tubing with sufficient force to seriously dent it.

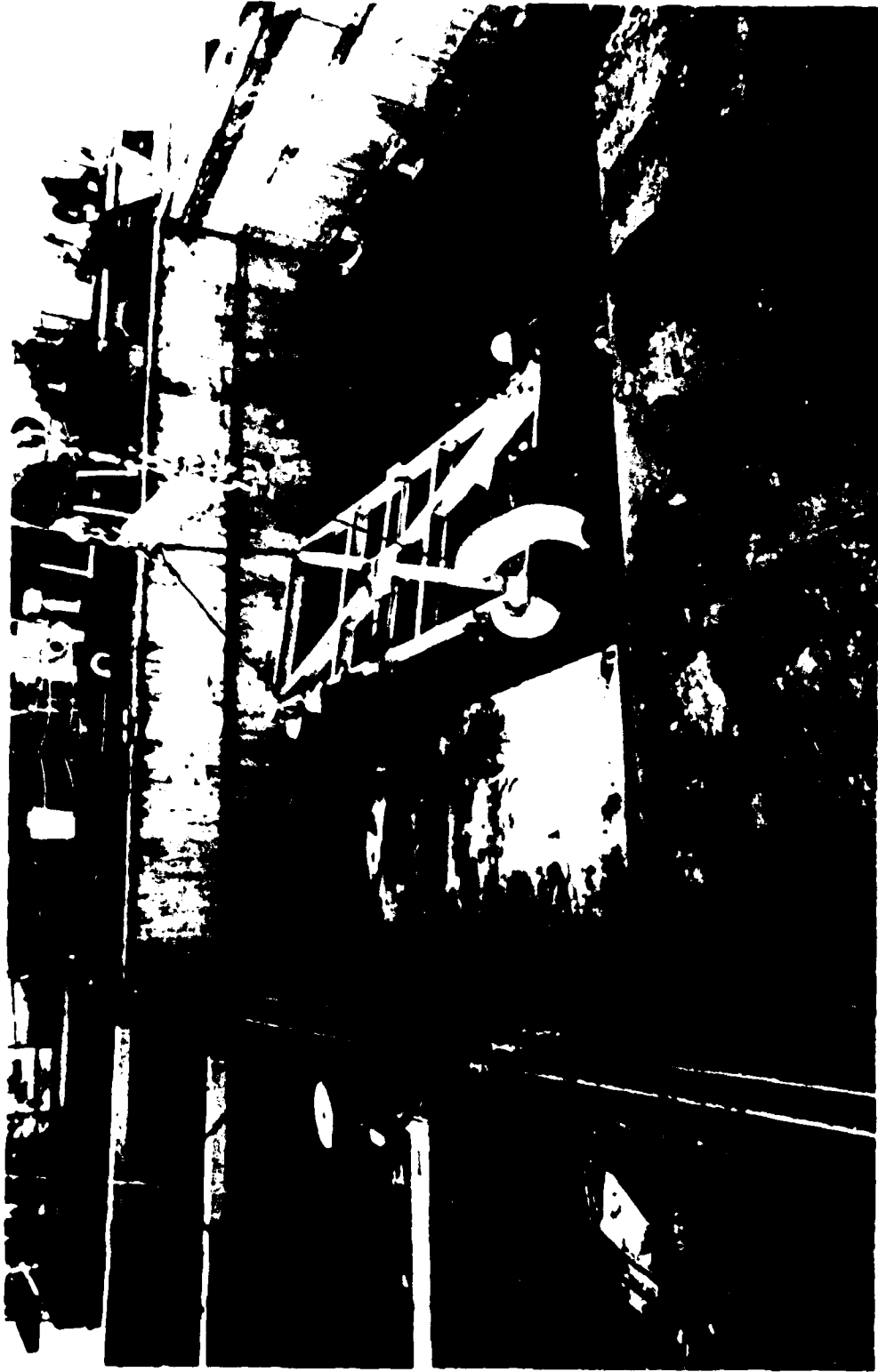


FIGURE C.39. POSITIONING SPREADER BOOM. Without cell guides it was necessary to position the spreader bar manually in the hold. In the boom was not at a 90-degree angle to the container axis, delays and difficulties in attaching the spreader bar were experienced.



FIGURE 2-40. BOW TORSION. Once the container was attached the crane had to top up as well as raise the hook in order to clear the ship's booms and kingposts. This adds delays to cycle times that would not be typical of operations on the clear deck of a container ship.

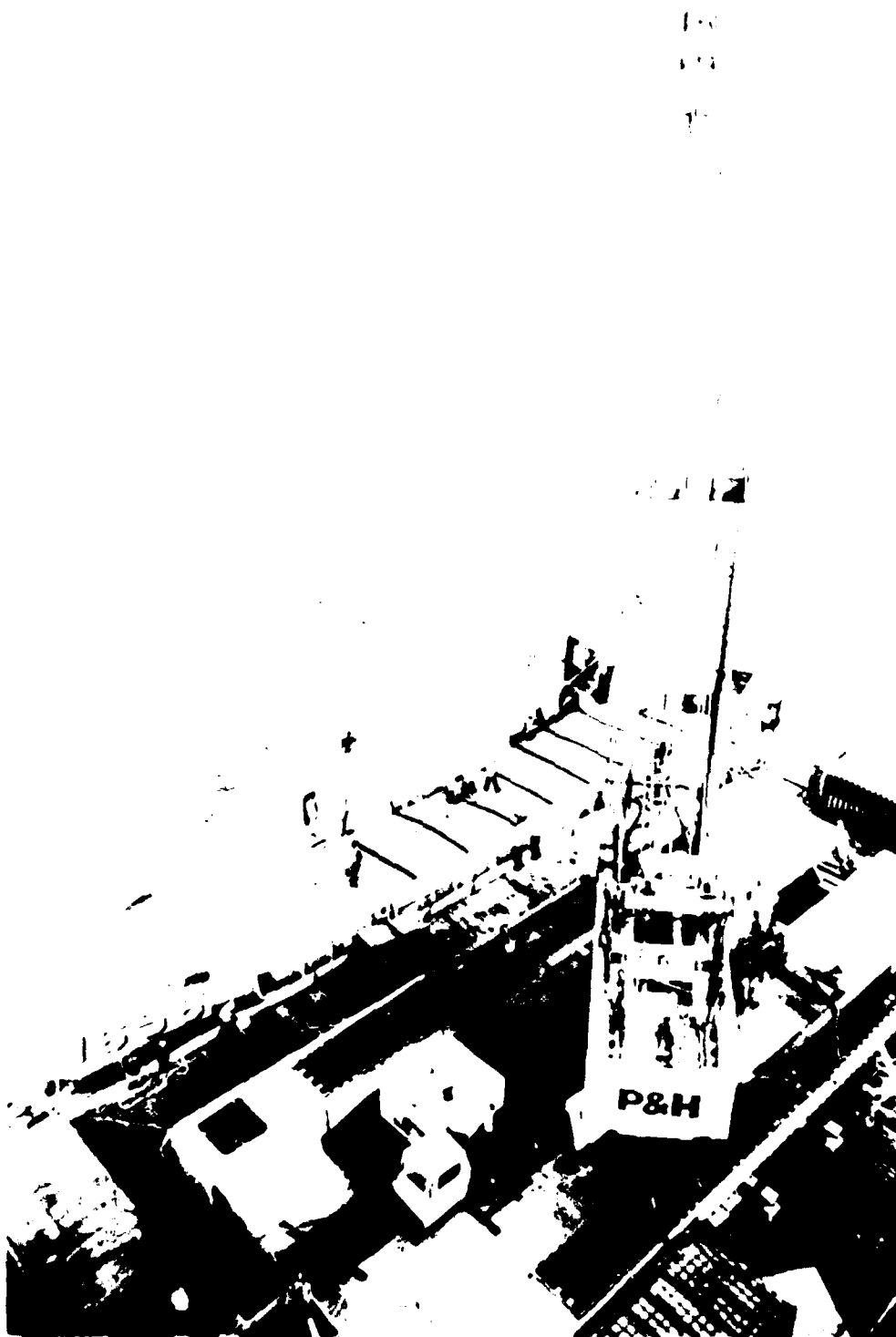


FIGURE D.41. LCU USED FIRE HOSE. To cushion the impact of containers being lowered, a problem when there is a sea state, fire hose was used on the deck of this LCU.



FIGURE D.42. LCU LIGHTLY LOADED. Normally an LCU would be loaded with four containers but because of the limited number of containers available, capacity loading was not practiced.



FIGURE D.43. MOBILE LOADING TIME-CONSUMING. One method of minimizing handling at the beach is to place trailers on a causeway ferry and load the trailers shipside. However, because of the motion of the seas and the need for close alignment during loading, it required approximately an hour to load just two of three trailers and it became apparent that the method was too time consuming.

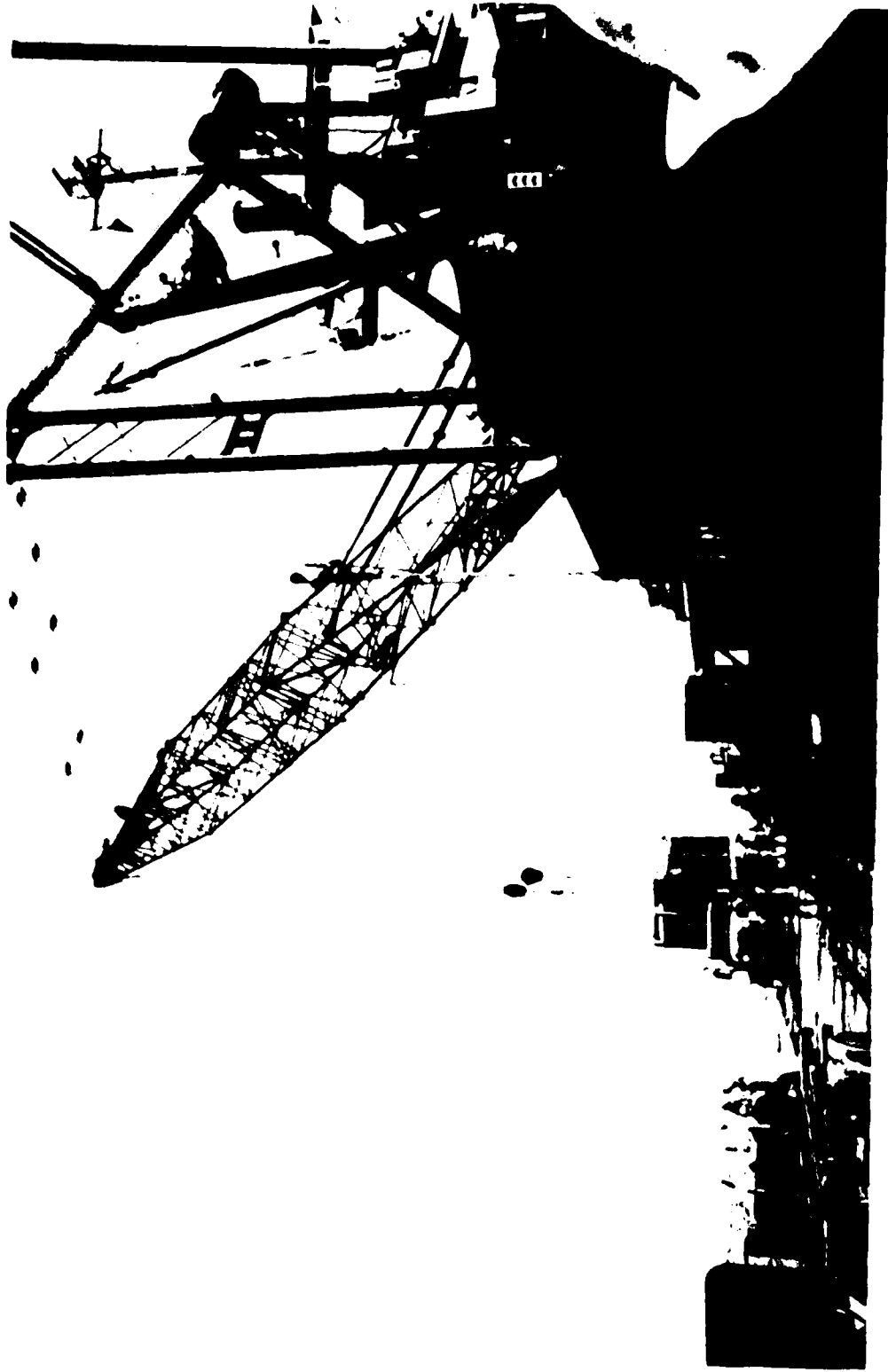


FIGURE D.44. SPREADER BAR NOT ALIGNED. With a two-point spreader bar attachment and automatic taglines, the spreader bar and container were nearly always perpendicular to the boom, while the trailer chassis was not. This necessitated man-handling the container and/or its winch in a position that would permit lowering the trailer corner fittings.



FIGURE D.45. ALIGNMENT DIFFICULT. Aligning the container with the trailer required from 4-6 personnel to force the container into position so it would engage the corner fittings. Because the procedure was so time-consuming one trailer returned to the beach without being loaded.

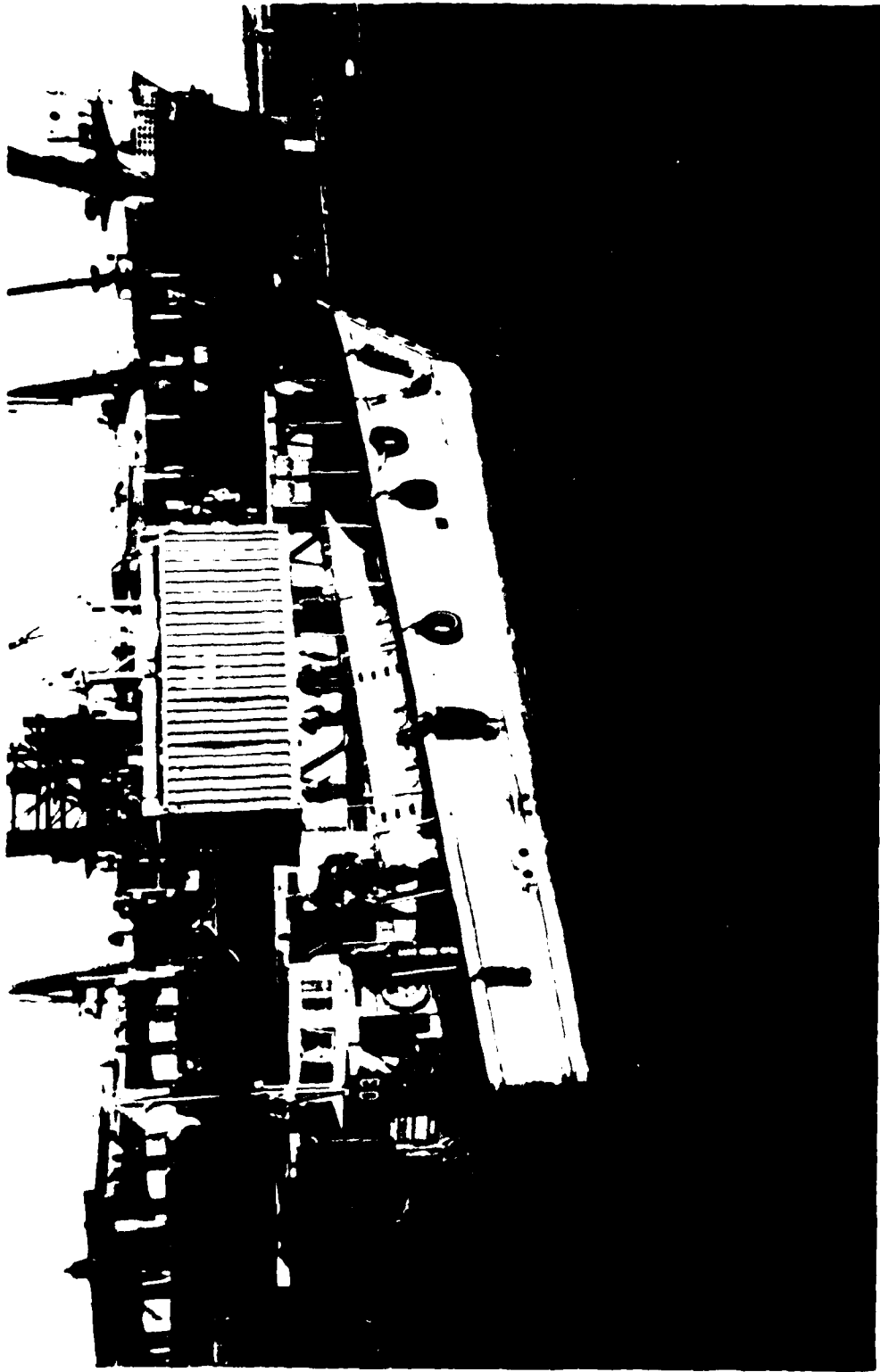


FIGURE D.46. LCM8s USED. LCM8 landing craft received extensive use in the pretest and had better beaching capabilities than LCUs, although both were unable to beach close enough to shore cranes at low tide.

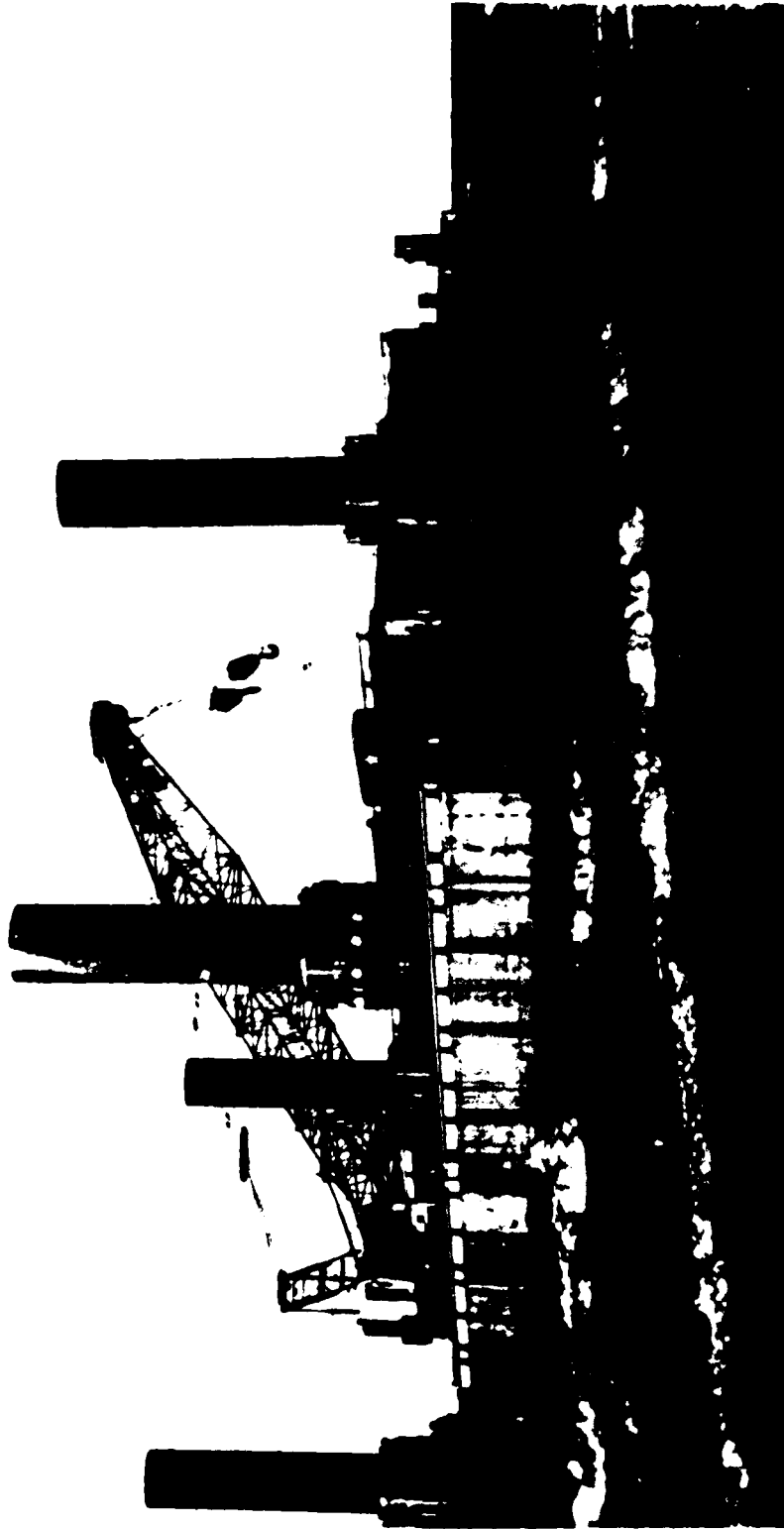


FIGURE D.47. DELONG PIER POSITIONED. To improve shoreside unloading capabilities a 140-ton crane was positioned on a Delong barge and towed to the objective area. The Delong was beached using two LCMs. Later the Delong was jacked-up out of the water on its pilings and ramps were added so that trucks could drive from the beach onto the pier.



FIGURE D.48. LCU RETRACTS. An LCU is shown above retracting from the DeLong pier after unloading at high tide.



PLATE 2-49. WIDE BEACH. Because of the gentle beach gradient and the fact that a single sealong does not extend far enough seaward, landing craft were stranded at low tide. At low tide only amphibians could be unloaded.



FIGURE 50. FAW 44-BEEM. Truck drivers experienced difficulty backing their trailers up the ramp so a rough terrain forklift, which has articulated steering, was tried. The above 44B ramp connects onto the 44B ramp. The 44B ramp was subsequently replaced by a sand ramp.

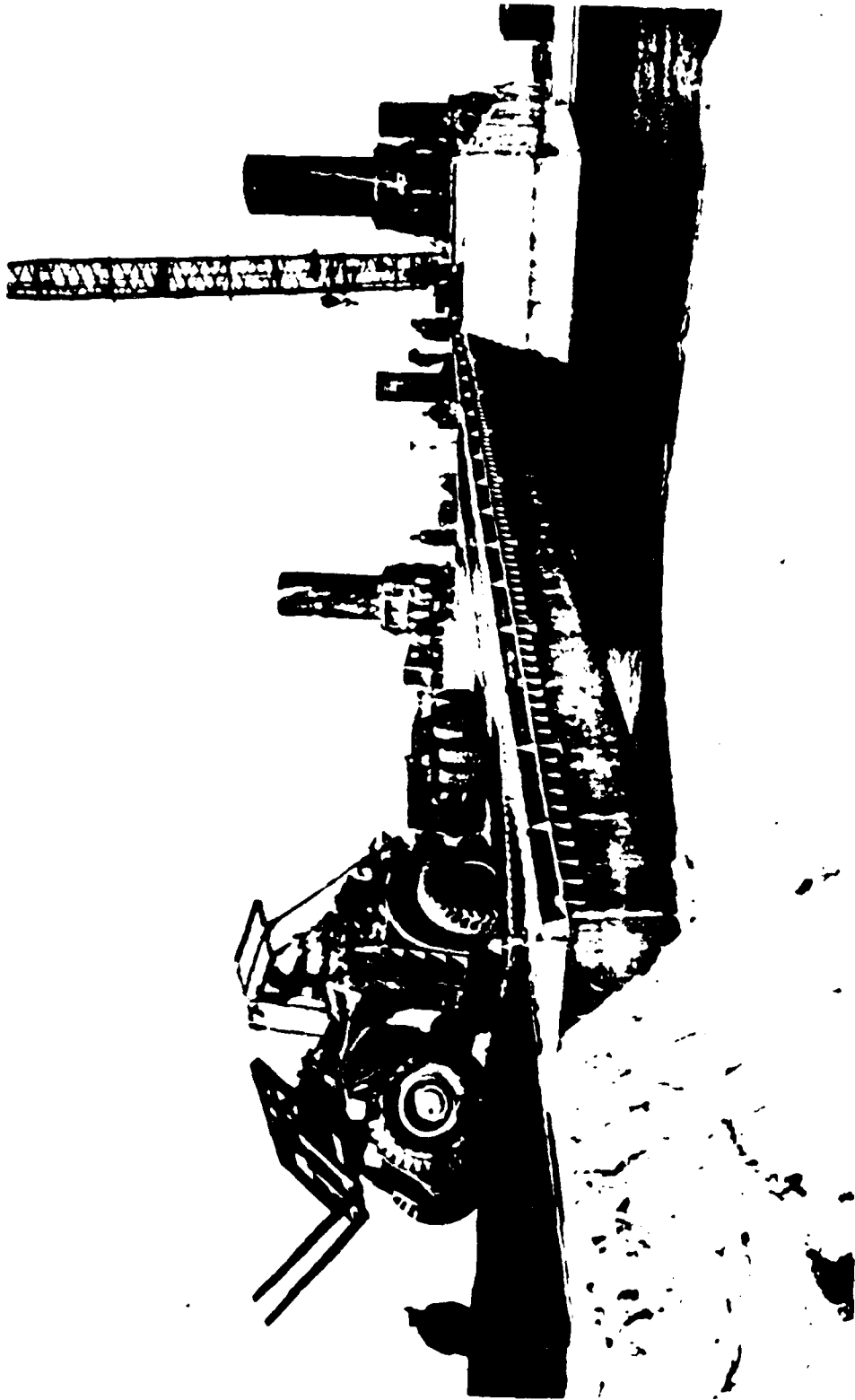


FIGURE D.51. CRANE DELAYED. Until the trailer was positioned under the crane, operations were choked. With experience drivers were able to more rapidly back their trailers up the ramp.

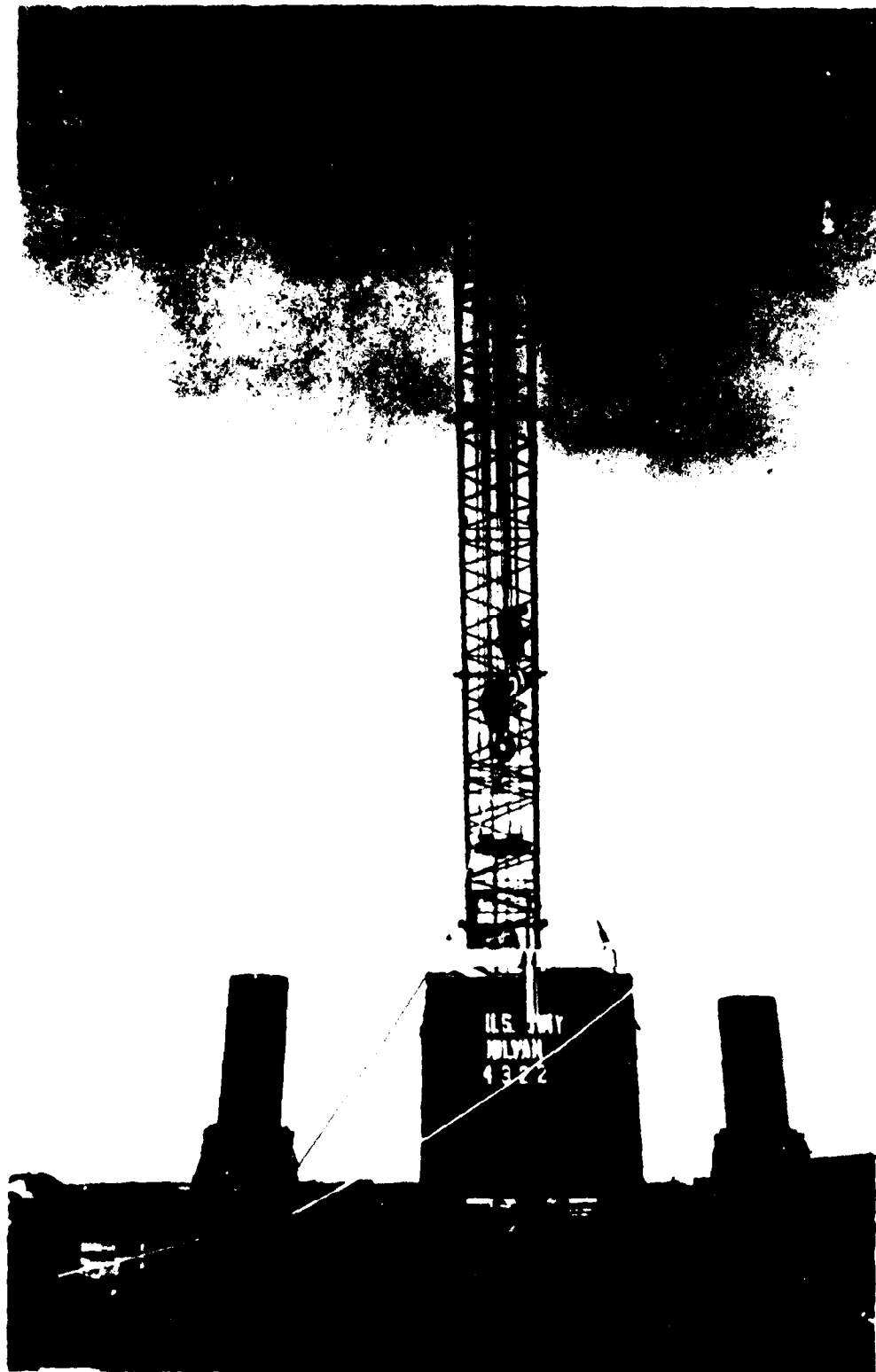


FIGURE 1. CRANE IN POSITION. Once the milvan chassis was on the
ground, the crane was hoisted.



11-11-68. W. M. Smith's photograph. A high speed jet engine boat that easily exceeds the
10000 rpm.



0-54. A view from the beach north of the tower. The tower is the structure in the foreground. The structure in the background is the tower. The structure in the foreground is the tower. The structure in the background is the tower.

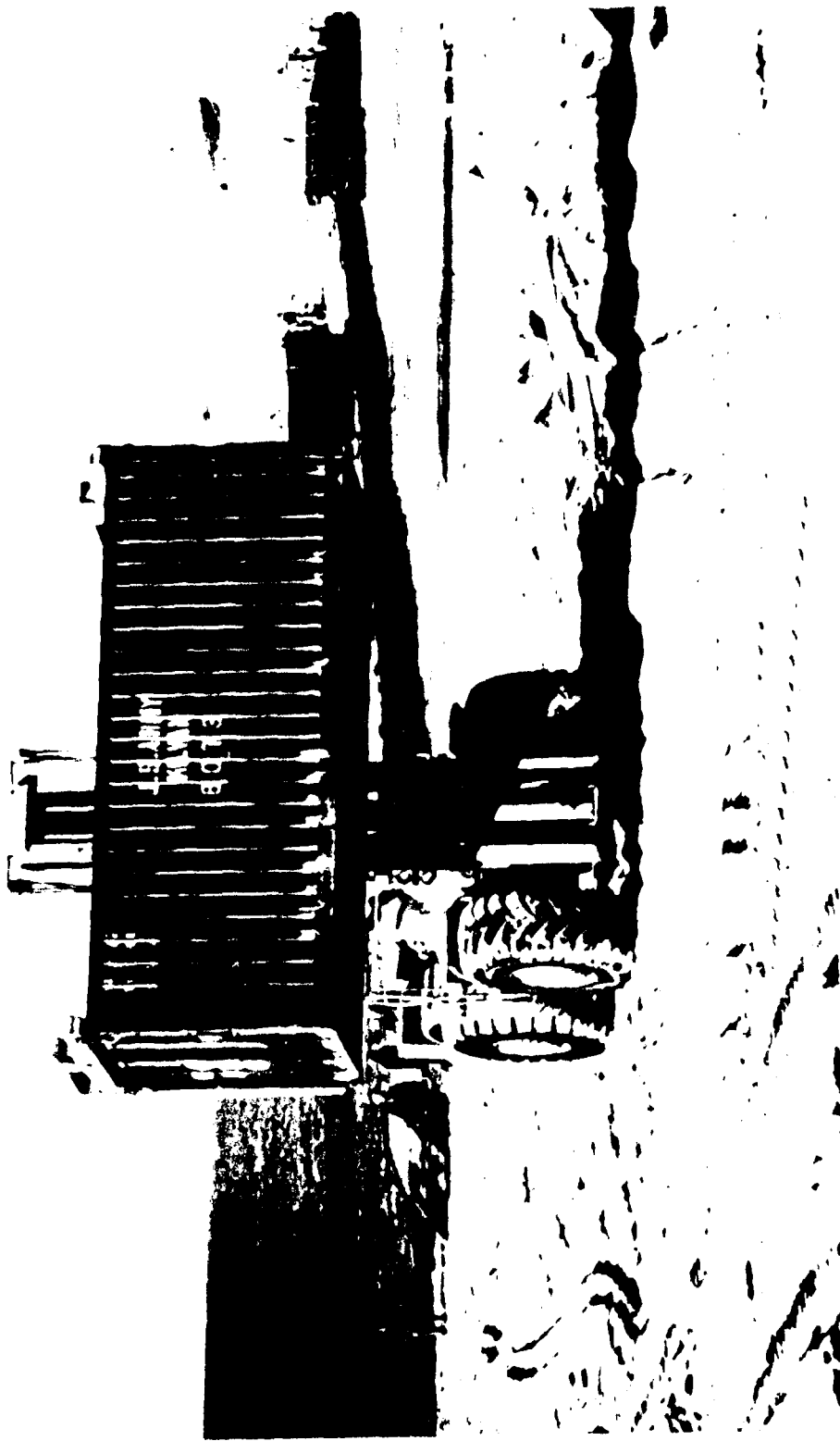
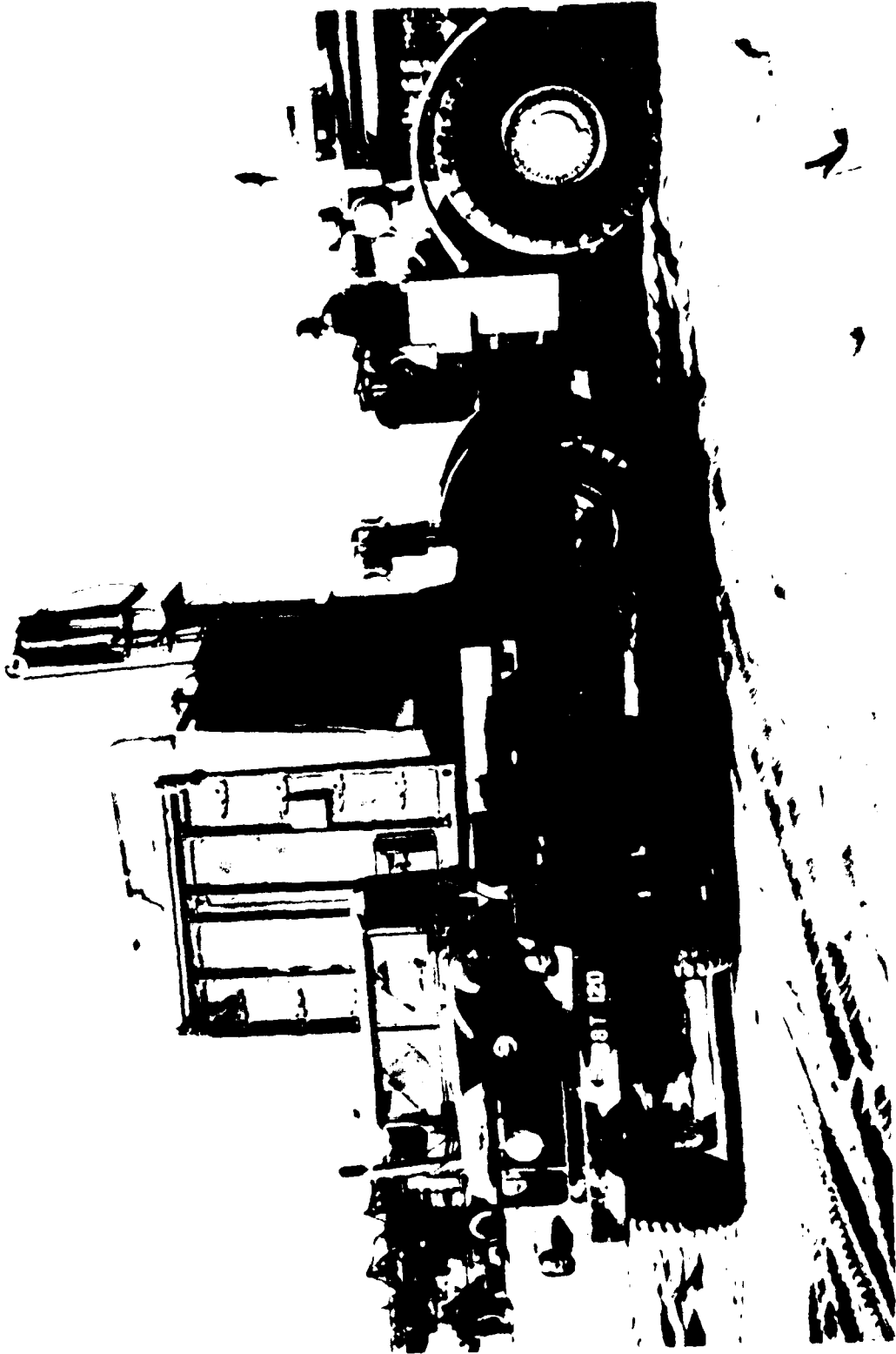


FIG. 1. The vehicle is a military tank. The large front door carries a 14-ton container. The
the container carries the equipment for the tank. The container was necessary.



On 10/26, 1966, the 1st Air Division, 4th Air Division, was loaded above by the front loader. The tire container was lifted on the causeway and the tire was loaded onto the chassis required approximately 4 minutes.



U.S. Army tank crew members are shown in the driver's compartment of a tank during a training exercise. The tank is equipped with a radio and other communication equipment.

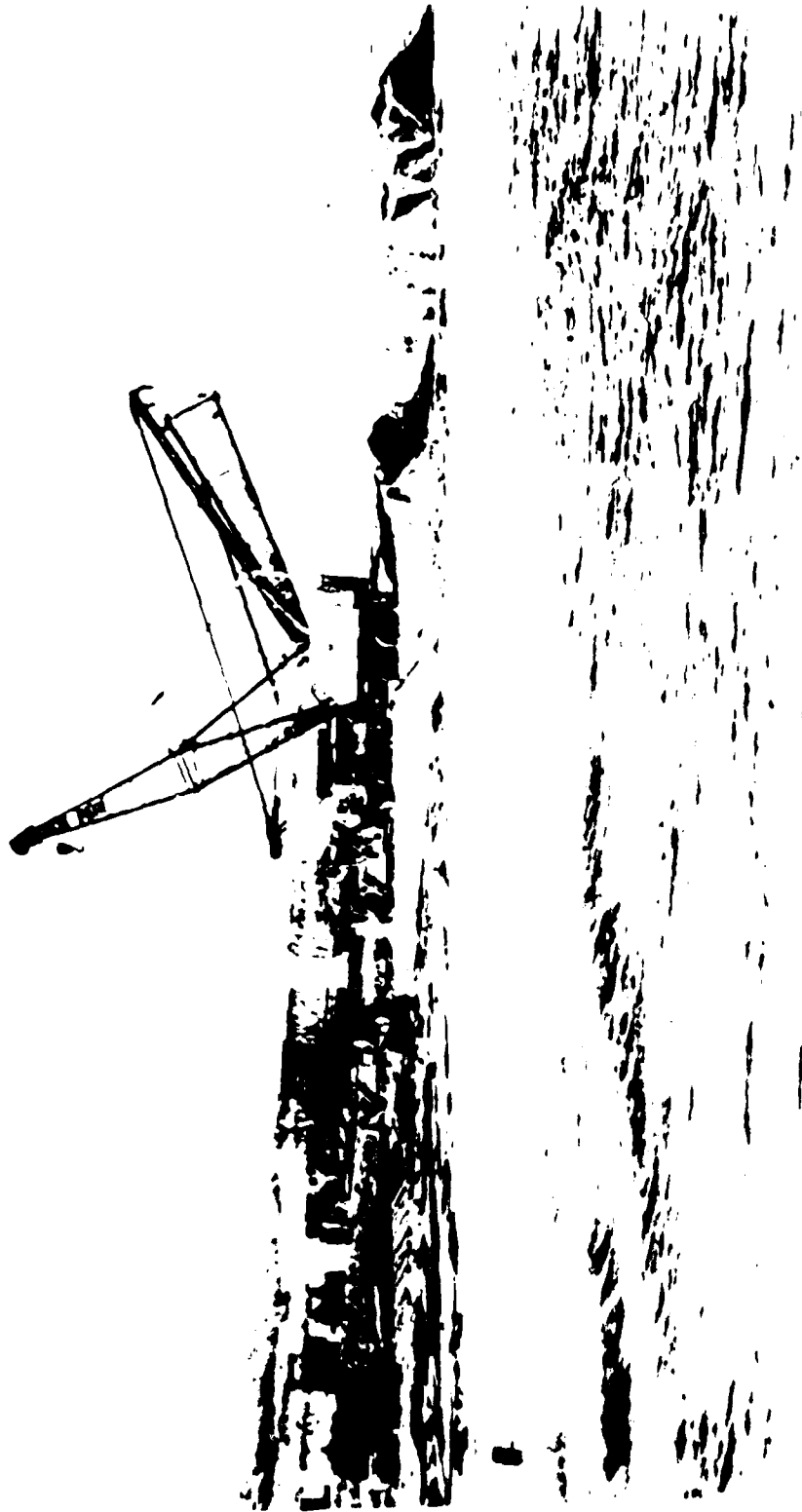


FIGURE 1. The BEACH CRANE ASSEMBLY BEING LIFTED. Since the 300-ton crane was landed and turned around, its assembly could be completed. It required 3 days before being operational, although no night operations were conducted and 200 man-hours were spent reversing the crane due to the necessity of rotating the crane 180 degrees.

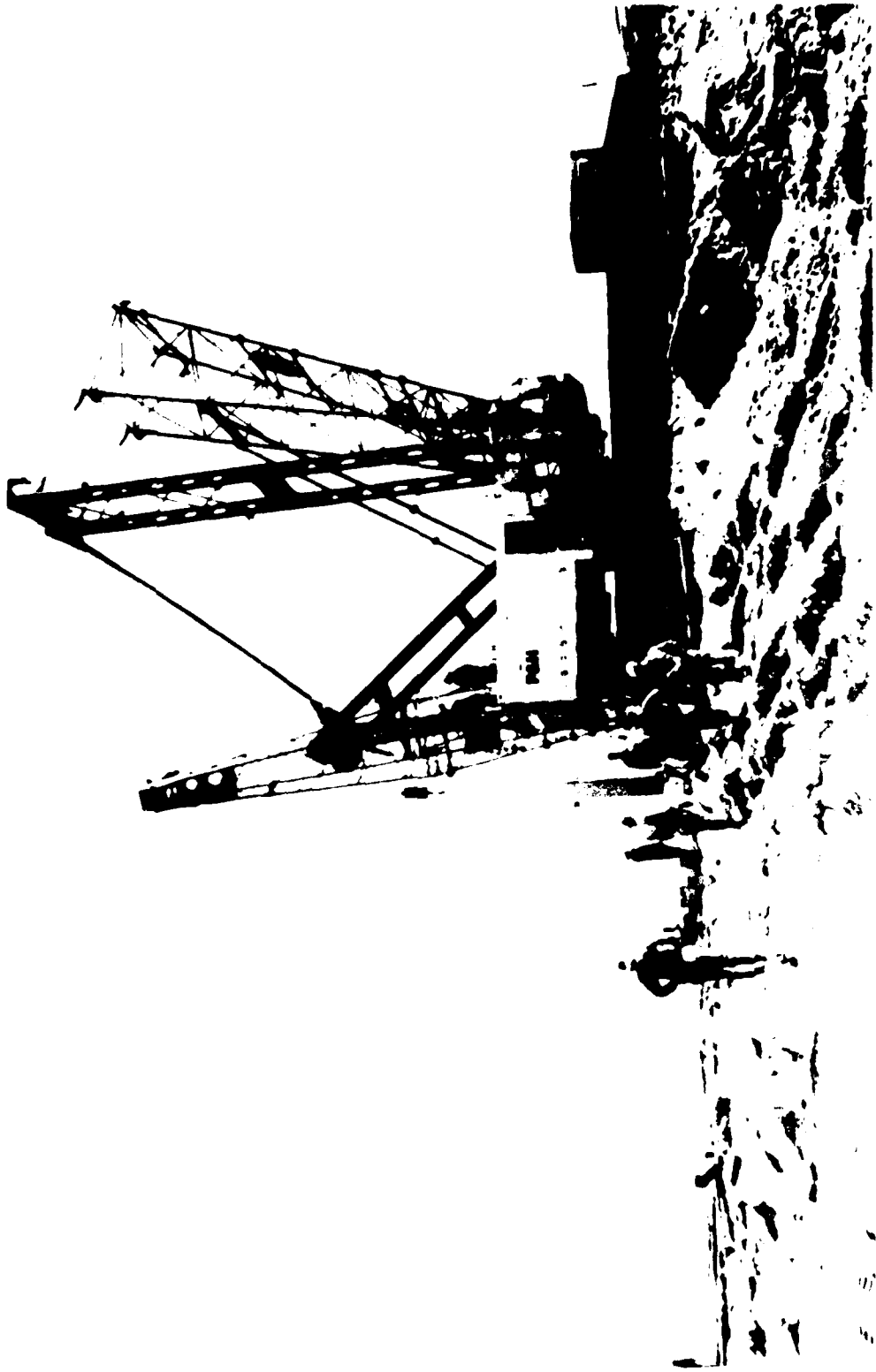


FIGURE D.59. 140-TON CRANE ASSISTS. To recover time lost in turning the 300-ton crane, a 140-ton crane assisted in reassembly. Normally, the 300-ton crane can make itself operational without assistance.

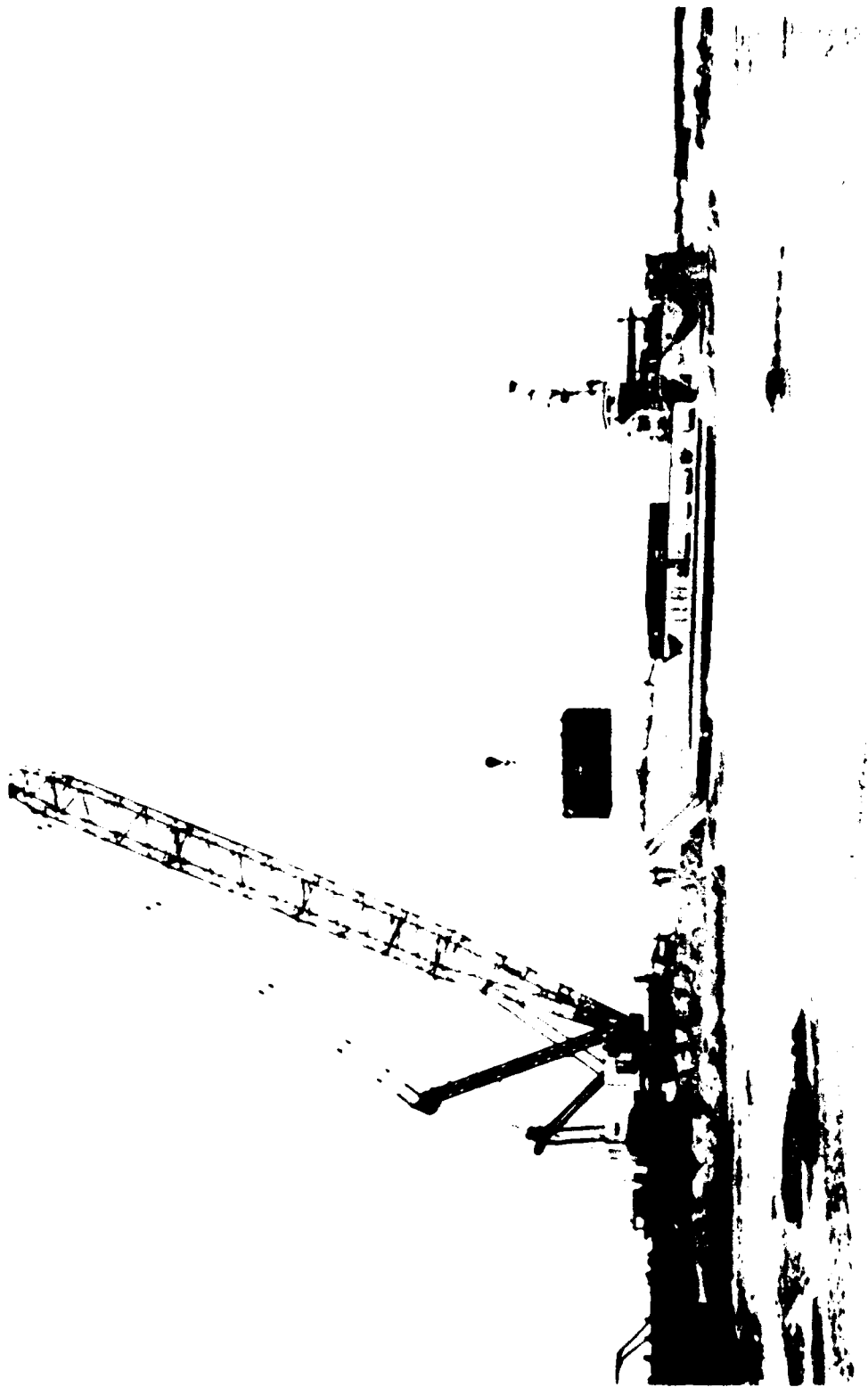


FIGURE D.60. HIGH TIDE OPERATIONS. At high tide landing craft were able to beach within reaching distance of the beach crane and were unloaded without difficulty.



FIGURE 1. Bulldozer at the site of the new terminal. The bulldozer was used to clear the site for dispatch to the manufacturing site.



THE
THE CRANE'S BOON
TO READILY MOVE ACROSS THE SAND AND FOLLOW THE TIDE CUT.



FIGURE 3.63. CHATTILL SPECIFICATIONS. In an effort to keep the beach crane operational a channel was pressed seaward of the crane by bulldozers.

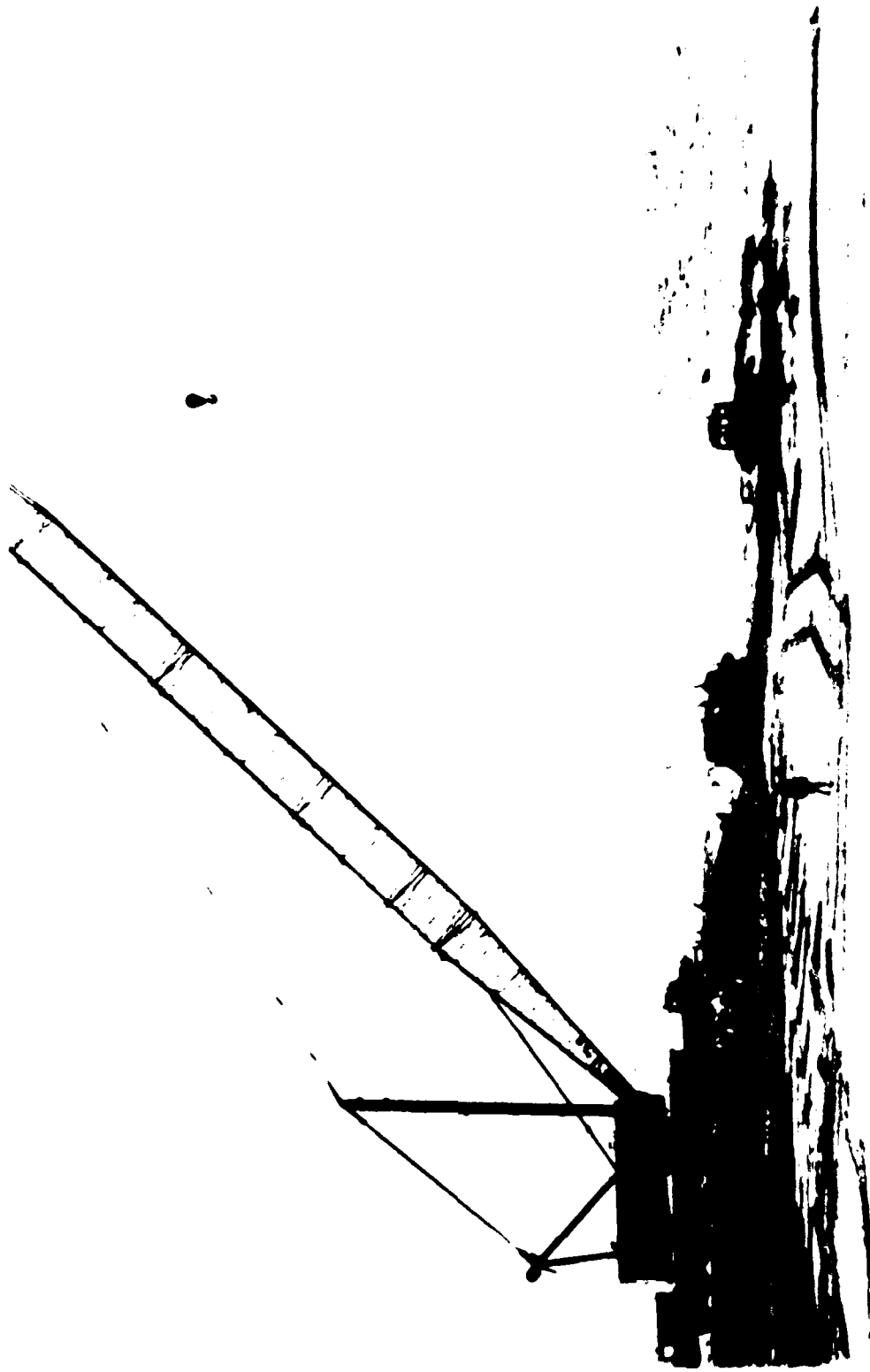


FIGURE D-64. CHANNEL NOT DEEP ENOUGH. After approximately 15 hr of dredging, it was apparent that a channel deep enough could not be excavated. The above photo was taken about 30 minutes before low tide.



D-65

FIGURE D.65. ROUGH WEATHER EXPERIENCED. Another problem was encountered when the surf and winds increased. The sand ramp upon which the crane had been placed began to erode and had to be repaired at high tide by dozers.

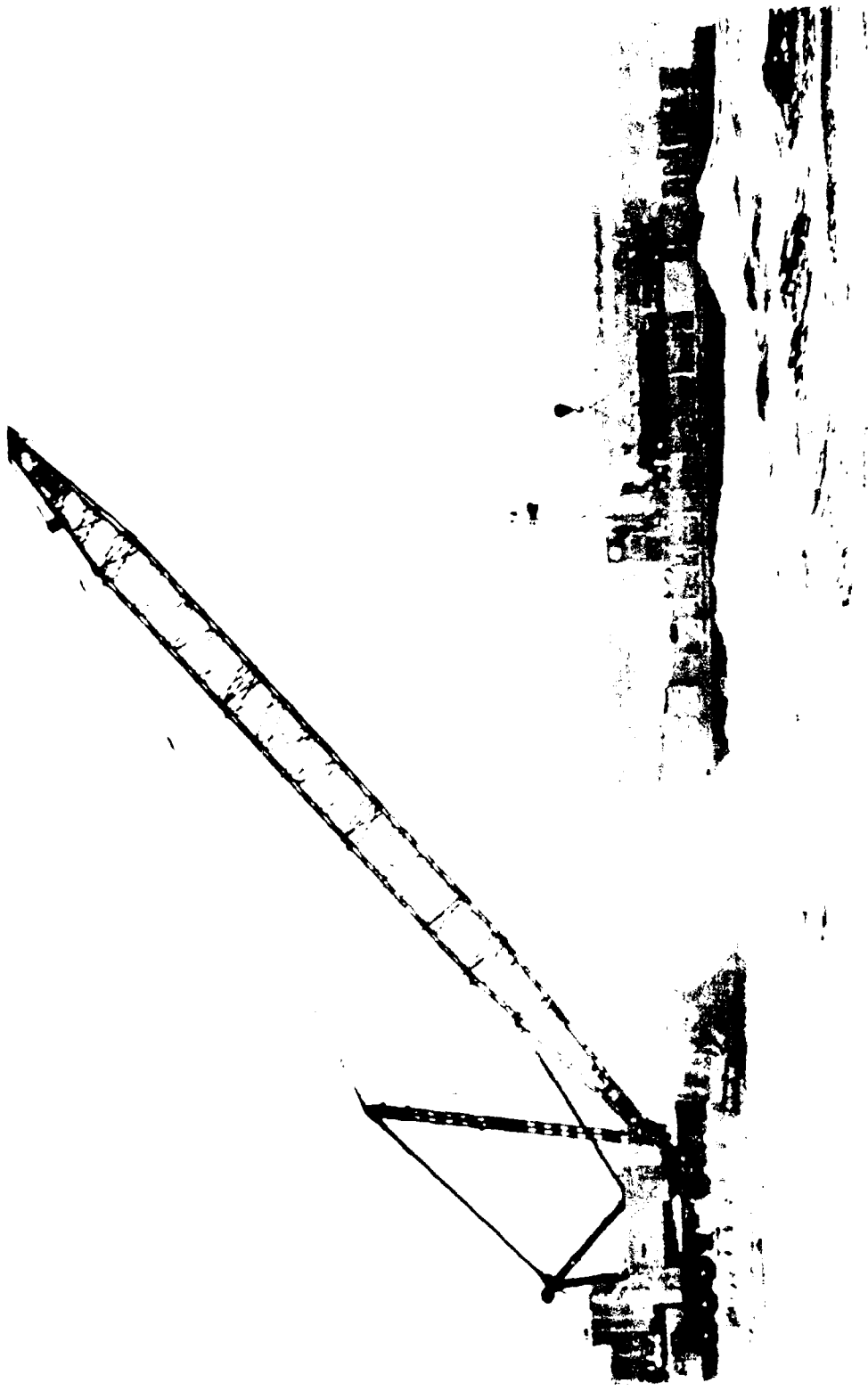
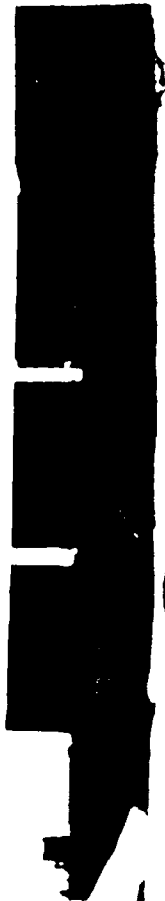
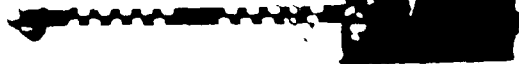
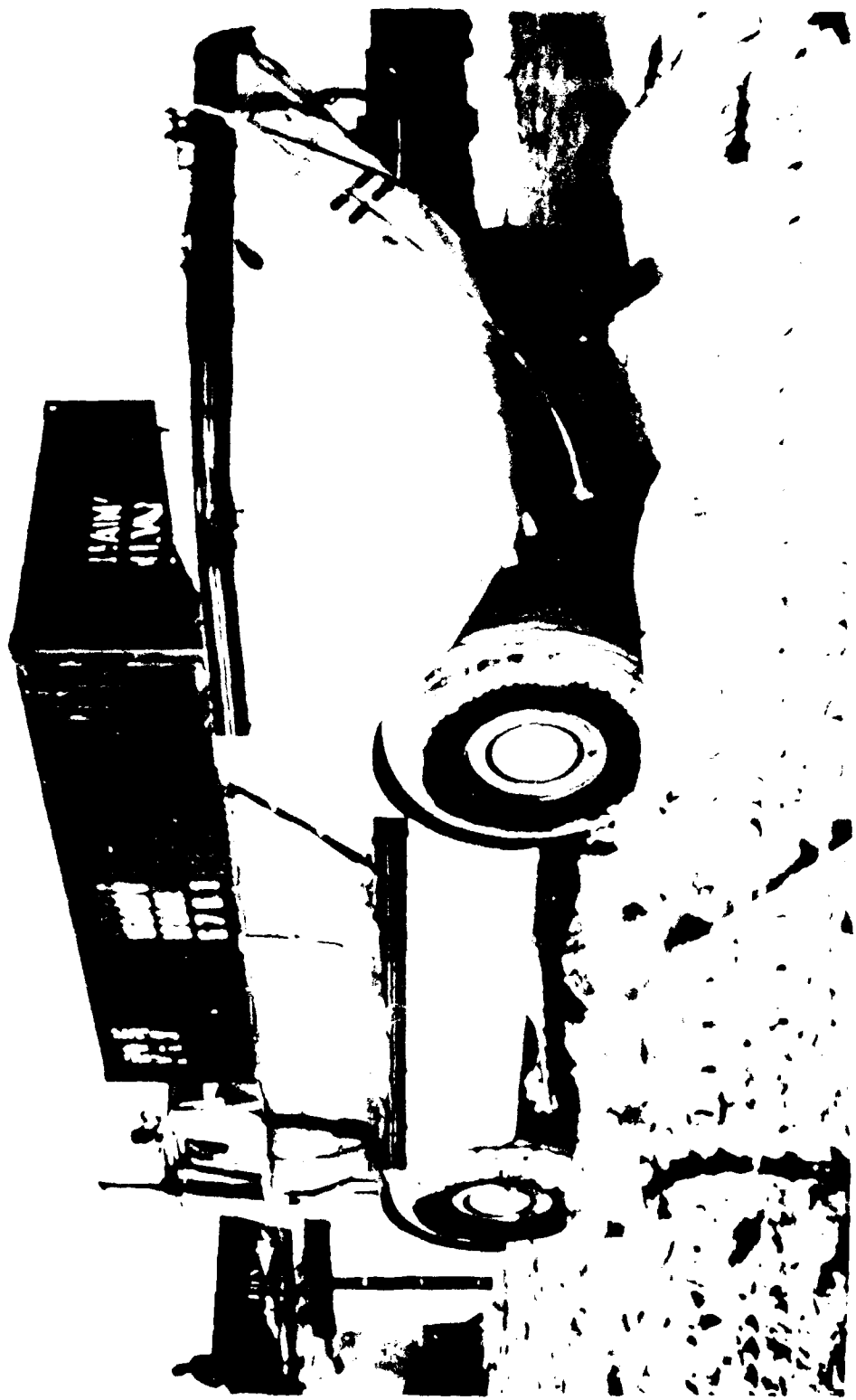


FIGURE 1.66. SOME CONTAINERS AT ALEP. Some container unloading was possible before the heavy weather required cessation of operations.



On 11/16/67, a bullet was recovered from the scene of the shooting. The bullet was found in the area of the building. The bullet was found in the area of the building. The bullet was found in the area of the building.





... (left) ... (right) ... the ...
used. A side-loader ...
military chassis, was more often used by off-lead artillery.

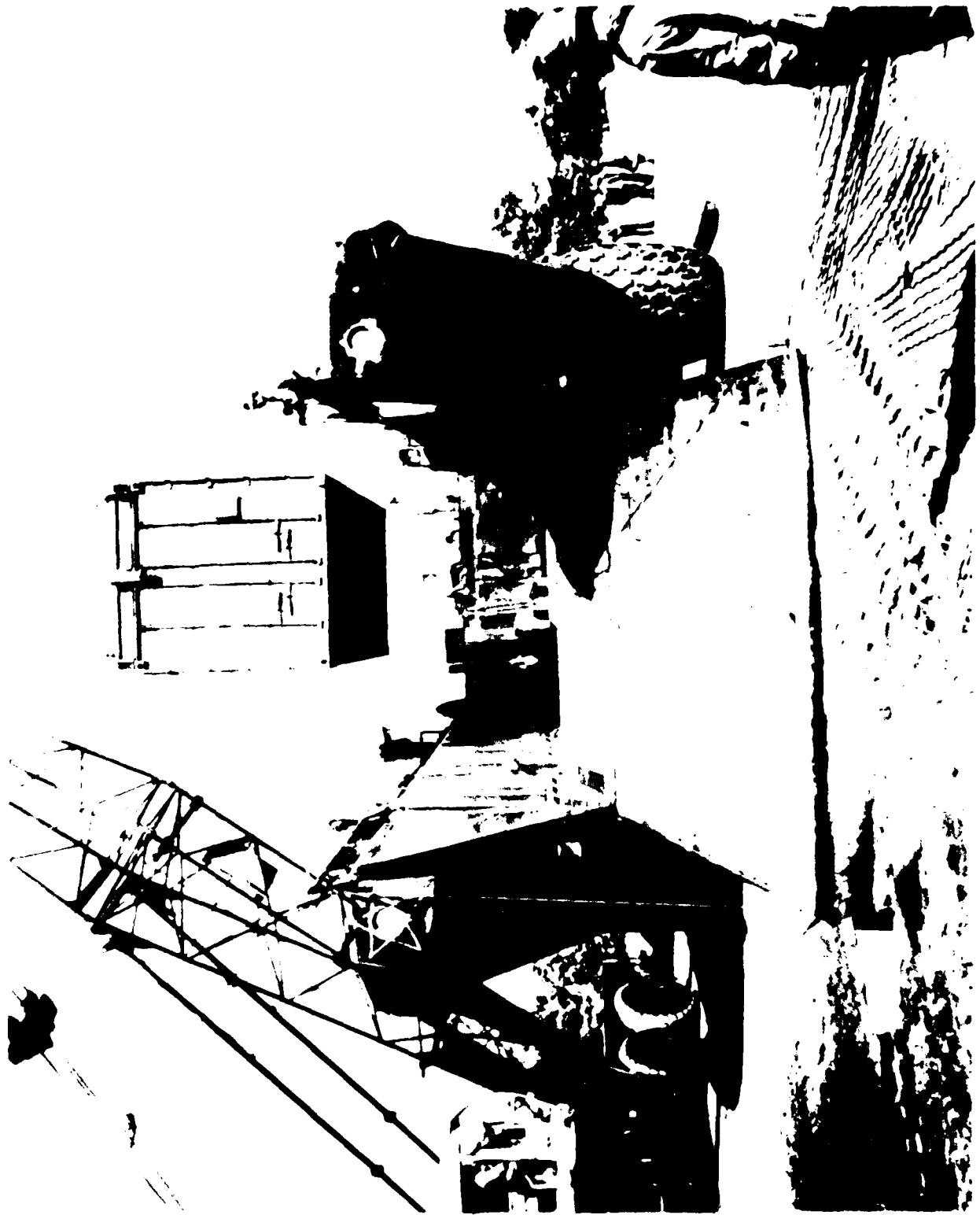


FIGURE 8.79. LARGELY UNOCCUPIED. A CRANE IS UNLOADING AT THE RECHARGING SITE BY A BATTERY CHARGE.



FIGURE D.71. FRONTLOADER CLEARS CONTAINER. Since a vehicle was unloaded a frontloader above a
sideloader was used to clear the discharge point.

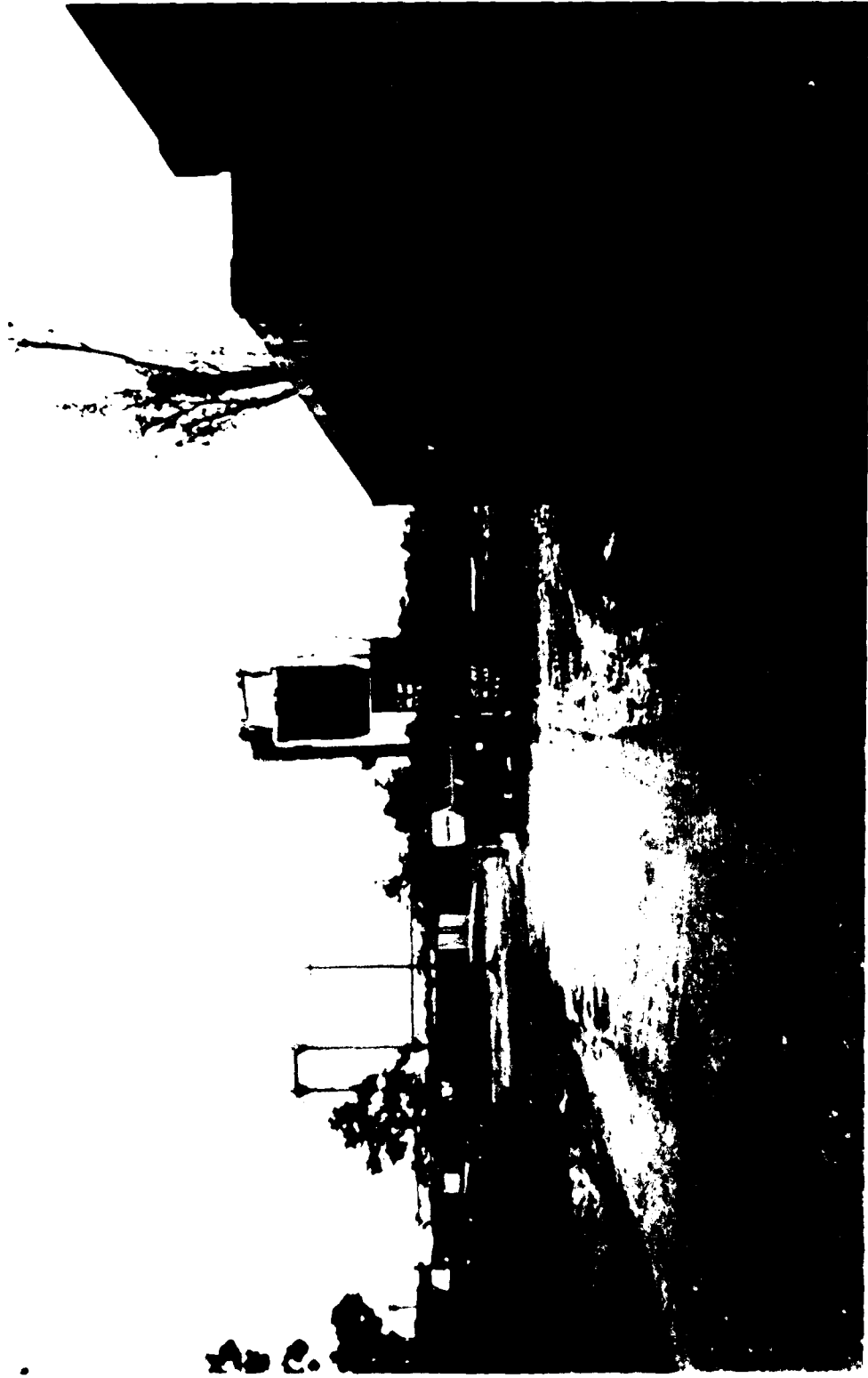


FIGURE D.72. SIDELOADER SAVES SPACE. A side loader (above) is used in the marshalling area to stack a fully-loaded container. Two and three high stacking saves marshalling area storage space. The side loader operates only on hard surfaces.

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