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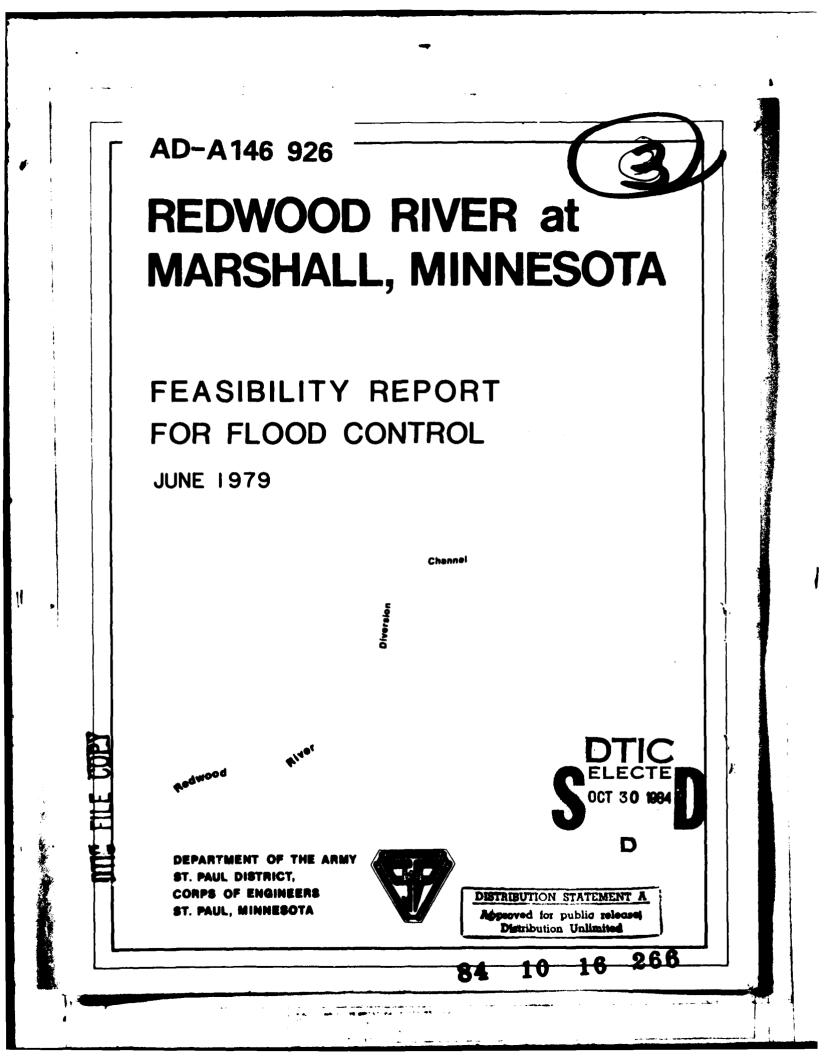
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-works, interior drainage works, aesthetic measures, recreational facilities, and required relocations. The plan also includes revegetation of all disturbed areas. A 133-year degree of flood protection for the City of Marshall and adjacent urbanized areas would be provided.

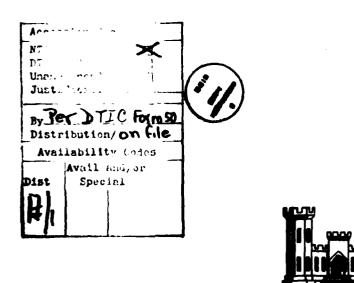
This report consists of a main report and two appendices.

## SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

# FEASIBILITY REPORT FOR FLOOD CONTROL

## REDWOOD RIVER AT MARSHALL, MINNESOTA

UNDER SECTION 216 OF THE FLOOD CONTROL ACT OF 1970, AS AMENDED



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U.S. ARMY ENGINEER DISTRICT, ST. PAUL CORPS OF ENGINEERS SAINT PAUL, MINNESOTA

## SYLLABUS

The purpose of this study was to investigate alternative measures and select a plan for insuring effective operation of the existing flood control project and providing flood protection to new unprotected development. Recurrent flooding of the Redwood River together with damaging overflows into the adjoining Cottonwood River basin has resulted in flood damages and the need for local emergency flood fights.

The selected plan of improvement consists of channel widening, straightening, and bank reshaping measures; levees; an overflow diversion structure with appurtenant control and outlet works, interior drainage works; aesthetic measures; recreational facilities; and required relocations. The plan also includes revegation of all disturbed areas. The plan would provide a 133-year degree of flood protection for the City of Marshall and adjacent urbanized areas.

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Adverse environmental effects resulting from plan implementation would be minimized where possible. Opportunities for environmental enhancement in some areas would be realized. The economic stability and effects of the flood damage reduction benefits resulting from the plan will have favorable impacts on the regional and national economies.

The District Engineer recommends Federal participation in the construction of the additional flood protection and recreational measures at Marshall in accordance with the President's cost sharing policy. The estimated cost to the Federal Government would be \$1,745,100. The estimated combined non-Federal first cost is \$758,900. The benefitcost ratio for the proposed overall project is 1.8.

#### PREFACE

In reviewing this document, it should be specifically noted that completion of this study and report has undergone several years' delay in order to reflect numerous changes in Federal policy, regulations, and procedures. It should be further noted that during this time the city of Marshall has experienced vibrant growth and development, and this high growth rate is anticipated to continue for some time into the future based on currently announced industrial plant and employment expansion plans and new housing expansion trends (averaging about 160 housing units per year over the past 5 years). Information on this vibrant rate of growth in urban development is contained in Appendix I, Section J (See Development Under Existing Conditions).

Since the background information contained in this report on the resources and economy of the study area was leveloped early in the 1970's prior to this vibrant growth rate at Marshall, the future population and projected urban growth rates presented in the main report and various appendixes are now conservative and outdated estimates. Modifying this report to properly reflect existing and future growth rates would not alter the selected flood damage reduction plan or its scale of development. Phase I preconstruction planning will reflect any changed condition. Thus, further delay in completing this study to reflect more appropriate existing and projected future growth rates is not believed warranted at this time or in the best public interest. Proceeding with project authorization, postauthorization planning, and timely construction would best serve the needs of the citizens of Marshall and alleviate the threat, potential for loss of life, and human suffering associated with flooding.

### REDWOOD RIVER AT

## MARSHALL, MINNESOTA

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#### FEASIBILITY REPORT

## FOR FLOOD CONTROL

## THE STUDY AND REPORT

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## REDWOOD RIVER AT MARSHALL, MINNESOTA

FEASIBILITY REPORT

## THE STUDY AND REPORT

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Marshall, Minnesota, the county seat of Lyon County, is located in southwestern Minnesota near the center of the Redwood River Basin. The community occupies both banks of the Redwood River for a distance of about 4.8 miles at a point approximately 68 miles upstream of the river's confluence with the Minnesota River, as shown on plate 1. A federally-constructed flood control project was completed at Marshall in 1963. This project was originally designed for a peak flood flow of 6,500 cfs which had a 114-year frequency of occurrence. After the occurrence of two major floods in a short time span (1957 and 1969), discharge-frequency relationships at Marshall have been revised. Based on the revised discharge-frequency curve, what was originally a 114-year recurrence interval is now a 59-year interval. Because of flocd problems experienced during the record April 1969 flood due to inadequate channel capacity both upstream and downstream of the existing project, the City and County have requested a study to deter-

mine if corrective action is advisable. A discussion of background information, problems and needs, alternative measures considered, and recommended action are discussed in the following report sections.

#### PURPOSE AND AUTHORITY

Authority for this study is provided for in section 216 of the 1970 River and Harbor Act. This section of the Act states:

"The Secretary of the Army, acting through the Chief of Engineers, is authorized to review the operation of projects the construction of which has been completed and which were constructed by the Corps of Engineers in the interest of navigation, flood control, water supply, and related purposes, when found advisable due to significantly changed physical or economic conditions and to report thereon to Congress with recommendations on the advisability of modifying the structures or their operation, and for improving the quality of the environment in the overall public interest."

By resolutions of 6 June 1972 and 3 July 1972 respectively, the Lyon County Board of Commissioners and the City of Marshall requested that the Corps of Engineers review the operation of the existing project to determine the advisability of corrective measures required to upgrade the project and provide protection to unprotected development at Marshall. By letter of December 3, 1975, the City of Marshall requested additional studies of the advisability of

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locally desired recreational facilities in conjunction with the existing and proposed flood control measures.

#### SCOPE OF THE STUDY

The flood control portion of this study principally concerns the adequacy of the existing Corps of Engineers project in providing flood damage reduction in the City of Marshall and adjacent urbanized areas both upstream and downstream of the city. The study area applicable to flood damage reduction and recreational needs includes these reaches in addition to the natural river reach through the city. Any required recreational lands would be limited to lands acquired for the existing and proposed flood control project or immediately adjacent lands purchased entirely at local expense to provide access to considered developments. Investigations were made in sufficient detail to permit selection of the best overall plan from a series of alternatives and establish final project designs and cost estimates. Selection of the recommended plan was made after considering various effects, water and related land resource planning objectives, current planning policies and criteria, and the views of interested agencies and public. Coordination was maintained through the study with the City of Marshall and interested state and Federal agencies.

#### STUDY PARTICIPANTS AND COORDINATION

To assure the acceptability of a plan to the local public, close coordination between Federal, State and local interests has been an important element in this study. Several meetings were held with the City of Marshall to identify the nature and extent of the flood problem and needed recreation facilities and to determine alternative solutions thereto. Coordination was maintained with

the following state and Federal agencies during the study:

- \* Minnesota Department of Natural Resources
- \* Minnesota Pollution Control Central Agency
- \* Minnesota Department of Highways
- \* U.S. Department of the Interior Fish and Wildlife Service
  - Bureau of Outdoor Recreation
  - National Park Service
- \* U.S. Department of Agriculture Soil Conservation Service
- \* U.S. Environmental Protection Agency

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Meetings open to and attended by the public were held with the Marshall City Council on 3 March 1975 and 20 October 1975 to obtain local views on proposed upstream and downstream reach improvements respectively. Pertinent correspondence regarding this coordination effort is attached in Appendix II. On February 1977 a public meeting was held at Marshall to discuss the proposed plan of improvement. A copy of the meeting transcript together with subsequent correspondence received is also contained in Appendix II.

A meeting was held with City officials in Marshall on 2 March 1978 to review revised study recommendations based on a review of the draft report by higher Corps authority. On 2 April 1979, a meeting was held with City officials and other interested persons to discuss additional studies of alternative flood barrier alignments made in response to Executive Orders 11988 and 11990. At this same meeting, the City adopted two resolutions indicating its willingness and intent to provide required assurances of local cooperation when and as required for the proposed flood plain management and recreation measures. Copies of these resolutions are also contained in Appendix 2.

#### THE REPORT

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Results of this study are presented in a main report with two appendices. The main report is a brief non-technical presentation with recommendations concerning proposed improvements to alleviate the flood problem at Marshall. Appendix I is a detailed technical report following the same general outline as the main report, but providing greater detail on natural and economic resources, plan formulation, and division of responsibilities for implementing the selected plan. Appendix II contains all pertinent correspondence associated with the study.

#### PRIOR STUDIES AND REPORTS

House Document No. 230, 74th Congress, 1st Session, includes a report submitted by the St. Paul District Engineer on 24 November 1934 concerning water and related land resource problems in the Minnesota River Basin. However, this report did not specifically consider flooding and related problems at Marshall.

House Document 417, 86th Congress, 2nd Session, includes a 25 March 1960 report from the St. Paul District Engineer recommending flood control improvements at Marshall to include clearing and snagging of a 3.1 mile reach of the Redwood River, construction of 2,135 feet of levee, and a floodwater diversion channel at Federal and Non-Federal first costs of \$2,252,000 and \$701,000 respectively, and subject to certain assurances of local cooperation.

A flood plain information report on the Redwood River at Marshall was prepared by Wehrman, Chapman Associates, Inc., Minneapolis, Minnesota under contract to the Corps of Engineers in December, 1974. This report, prepared at the request of the City of Marshall with the endorsement of the Minnesota Department of Natural Resources contains maps, profiles, and cross sections which indicate the extent of flooding which has been experienced and which could occur in the future at Marshall.

A flood insurance report has been prepared for the city by the St. Paul District, Corps of Engineers under contract to the Federal Insurance Administration. This report was completed in August 1976.

## RESOURCES AND ECUNOMY OF THE STUDY AREA

The City of Marshall (1970 population 9,886) is located in southwestern Minnesota and along the Redwood River at mile 68.1 as shown on plates 1 and 2. It is the county seat of Lyon County

and also serves as the retail trade and service center for the surrounding rich agricultural region.

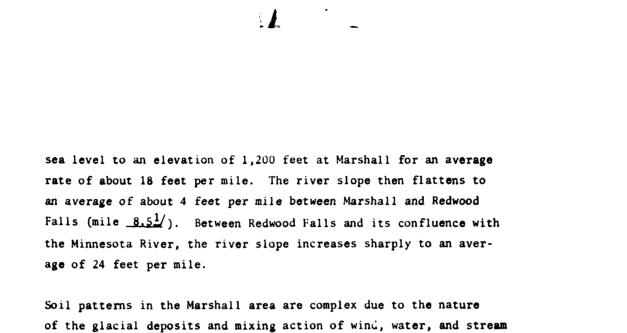
ENVIRONMENTAL SETTING AND NATURAL RESOURCES

Marshall is located along the Redwood River between river miles 66.0 and 70.8. The town lies on the topographic divide between the Redwood and Cottonwood River basins, the Cottonwood River located about 6 miles to the south at its nearest point.

Land use in the study area outside the urbanized area is predominantly agricultural with scattered rural residential and recreation uses. A narrow intermittent fringe of bottomland forest along both river banks provides food, water, and sanctuary for area wildlife. The agricultural lands, which extend to these wooded areas are slowly being lost to expanding residential and other development. Public land use along the flood plain consists of a state roadside park, city-owned right-of-way along the existing floodwater diversion channel, and the Southwest State College at Marshall and three city parks.

The Redwood River rises in Pipestone County and extends downstream along an elongated drainage area of approximately 743 square miles of which 251 square miles are located upstream of Marshall. The river at Marshall is generally less than 40 feet wide with numerous areas of steep, eroding banks and is flanked on both sides by an intermittent but fairly dense strip of tree and understory cover.

The general topography of the basin is that of a rolling upland area. The river drops from an elevation of about 1,850 feet above



of the glacial deposits and mixing action of wind, water, and stream flow. Soils are of recent and glacial origin and consist of alluvial silt, clay, and sand underlain by clayey glacial till or sandy outwash material. The inherent soil fertility is quite high, reflected in high annual agricultural yields during non-drought periods.

The climate of the study area is characteristically continental with wide seasonal variations in temperature. Average mean daily temperatures range from  $74^{\circ}$  in July to  $13^{\circ}$  in January, the coldest month. A rage annual temperature is about  $45^{\circ}$  with recorded extremes of  $-36^{\circ}$  F and  $107^{\circ}$  F. Normal yearly precipitation is about 27 inches with the annual snowfall averaging about 40 inches. High intensity rains of 4 to 5 inches in 24 hours are not uncommon during the spring and summer.

Vegetation in the study area consists of the thin strip of forest and understory cover along the river banks, small isolated plots of native prairie, grasslands on previously tilled cropland, and domesticated plant communities on agricultural and residential areas. Reed canary grass is by far the most abundant grass species found on the river banks. Aquatic vegetation generally consists of several species of attached algae and a few species of aquatic weeds.

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 $<sup>\</sup>frac{1}{A11}$  Redwood River mileages referenced to mile 0.0 at the confluence with the Minnesota River.

The river woodlands provide habitat and a source of food and water for a variety of wildlife. Red fox (<u>Vulpes</u> fulva), raccon (<u>Procyn lotor</u>), mink (<u>Mustela vison</u>), muckrat (<u>Ondatra zibethica</u>), and beaver (<u>Castor canadensis</u>) are common in the area. The woodlands along the river just downstream of Marshall are uniquely important to the local bird population as many species of wading birds are attracted to the sewage disposal ponds located north of Marshall. No significant sport fishery is present in the river at Marshall due to the high turbidity levels and very shallow depths or dry areas during low-flow periods.

Although the Marshall area has experienced substantial Indian and early white settler activity, no evidence of historic Indian, or sites of other historical or archeological interest have been identified in the study area. This finding is supported by a check of the National Register of Historic Places, research done by the State of Minnesota, and an environmental assessment for the Marshall municipal airport by the City Engineer.

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Major recreational resources in Marshall include four municipal parks and a private golf course. Developed public use areas in the immediate study area include the state roadside park located southwest of the community as shown on plate 1, and three city parks as shown on plate 2. Some walking trails are found in the river woodlands but are not publicly owned. Fishing and canoeing activity is minimal due to the very shallow areas and fallen trees and snags in the channel. The City is presently making a study of a bicycle trail system around the city. A portion of this system would utilize existing city-owned diversion channel right-of-way and provide connections to the college and downtown areas.

Two County ditches are located within the study area. These ditches No. 70 and No. 62 are maintained by Lyon County in accordance with

State law. The Redwood River downstream of the State Highway 23 crossing is classified as a judicial ditch.

The existing flood control project at Marshall is located mostly within the City limits and operated and maintained by the City in accordance with local assurances of cooperation previously furnished to the Secretary of the Army. The City has recently adopted a flood plain management program based on the completed flood plain information report. Management of unincorporated flood plain areas adjacent to the city are subject to an existing agreement between the City and Lyon County.

#### HUMAN RESOURCES

The present site of Marshall was settled in 1869. Railroad transportation to the town was initiated in 1872. The city's population has steadily increased to a 1970 population of 9,886, an increase of 48 percent over the 1960 census. Much of this increase was due to annexation by the City and the opening of the Southwest State College at Marshall. The City's population is expected to grow over the next 25 years but at a decreasing rate.

#### DEVELOPMENT AND ECONOMY

Marshall, the county seat of Lyon County, serves as an important regional government, trade and service center. The State college provides various sducational and cultural opportunities for area residents. Much of the agricultural activity around Marshall is

based on the marketing of annual products with three of the largest employers involved in food processing. Farming in the area continues to become more specialized with a decrease in cash crops and an increase in livestock and dairy operations. Median family income for Marshall residents in 1970 was \$9,856 with a per capita income of \$2,840. The Marshall area is served by one major U.S. highway, three State highways, rail freight service, two truck freight lines, bus service, and a charter airplane service.

## PROBLEMS AND NEEDS

The existing federally-constructed flood control project provides protection to much of Marshall during the frequent smaller floods. However, a large portion of the city remains subject to severe damage during major flood periods. The following paragraphs discuss the status of existing improvements, the flood problem and improvements desired by local interests. Additional discussion of study area resource management problems and needs is given in Section C of Appendix I to this report.

STATUS OF EXISTING PLANS AND IMPROVEMENTS

In 1952 the City completed a 1,100-foot long channel cutoff on the Redwood River at mile 67.0. This cutoff together with channel clearing and straightening works by the Corps of Engineers in 1953 reduced flood stages about a foot in the downstream portion of the town. The City was provided additional protection with the completion of the existing diversion project in 1963. This project, constructed by the Corps of Engineers, included channel clearing and snagging, a levee, a 2.4-mile long floodwater diversion channel, channel enlargement along two river reaches, flanking spoil dikes along improved channel reaches, drop structures in the diversion and natural channels, and necessary road, rail and bridge alterations. The project was designed to pass a flow of 6,500 cubic feet per second (cfs) around and through the city with no significant flood damage.

The City presently has a flood plain management program in effect with floodway recently having been designated for the area. Adjacent flood plain reaches upstream and downstream of the City limits are subject to Lyon County flood plain management regulations for unincorporated areas.

#### THE FLOOD PROBLEM

The City of Marshall remains subject to severe flood damage during major flood periods. The existing project was designed to pass a peak flood flow of 6,500 cfs around and through the City without any significant flood damages. Updated frequency-discharge relationships indicate that the 114-year frequency of occurrence originally associated with this discharge is now a 59-year recurrence interval. Based on these updated relationships, a 100-year recurrence interval corresponds to a peak discharge of 8,200 cfs or a discharge close to the 8,090 cfs which occurred during the April 1969 flood.

The existing diversion channel has sufficient capacity to pass the original design discharged of 6,500 cfs without any problems. However, the existing channels upstream and downstream of the project have insufficient capacity to pass the design flood into or away from the project. Channel capacity

along both reaches is limited by extensive debris, vegetative growth, inadequate flow area, and numerous sharp meanders. Thus, as evidenced during the April 1969, the actual level of protection afforded the City is against a flood having a recurrence interval of about once in 16 years (point at which flood flows would overtop CSAH 7 and flow into Marshall).

Overbank flows along the upstream reach commence at the wayside park at a flow of about 2,500 cfs. At a discharge of 6,500 cfs most of the land area upstream of County State Aid Highway 7 (CSAH 7) (plate 1) would be flooded. At a discharge greater than 3,500 cfs, floodwaters would cross over CSAH 7 and re-enter the river after passing through the western part of the town. At the peak Redwood River discharge of 8,090 cfs at the Highway 23 wayside park during the 1969 flood, approximately 1,400 cfs initially overtopped Highway 23 and flowed into the Cottonwood basin. The construction of an emergency levee along CSAH 7 during the flood to prevent overflows into the town resulted in inundation damages to upstream farmlands. Subsequent breaching of Highway 23 to relieve pressure on the emergency levee and remove the retained floodwaters allowed an additional 1,106 cfs to flow into the Cottonwood causing inundation and erosion damages to two farm properties located south of the highway. At the height of the flood only 5,590 cfs reached the existing diversion structure. Without the emergency raise of CSAH 7, approximately 1,090 cfs would have flowed over CSAH 7 into the City causing extensive damage.

Insufficient downstream reach channel capacity was also demonstrated during the 1969 flood when extensive emergency measures were required to protect downstream development against a peak downstream discharge of 5,590 cfs (8090 - 2500). It is expected that a much greater damage potential would occur in the event of the revised downstream 100-year discharge of 6,700 cfs.

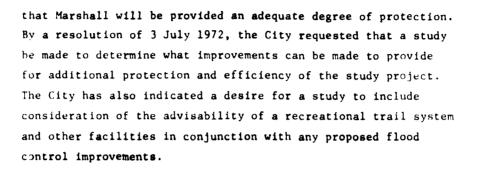
Based on a review of the existing project's performance during the 1969 flood, it is obvious that without additional measures upstream and downstream of the project, the project cannot function as intended. These additional improvements are needed to pass the design flood both into and away from the diversion project without damaging overbank flows.

## RECREATIONAL AND OTHER RELATED RESOURCE NEEDS

During the course of this study, the City has indicated a growing need for a city-wide recreational trail system. A recent survey by the City indicates that local residents place a high priority on the need for such a system. A perimeter trail system utilizing city pwned diversion channel right-of-way is in the initial planning stage by the City. Local interests also desired improvements to a generally undeveloped softball complex on the diversion channel right-of-way, cross-country ski facilities, river bank improvements in the interest of public safety at two city parks, expanded picnicking facilities at a third park, an off-road vehicle track, and nature education and quiet areas.

#### IMPROVEMENTS DESIRED

The primary improvements sought by the City are the additional measures to insure effective operation of the existing project and protect presently unprotected development immediately downstream of the existing project. By a resolution of 6 June 1972, Lyon County requested that the Corps review the operation of the existing project and required modifications be made thereto to insure



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## FORMULATING A PLAN

The actual damages and problems experienced during the April 1969 flood and the present potential for even greater flood damages emphasize the need for additional flood control measures at Marshall.

The purpose of these formulation studies is to review the operation of the existing flood control project at Marshall with the intent of identifying solutions that meet the study objectives identified early in this study. These specific objectives are:

Reduce damages from flooding along the Redwood River at
 Marshall during the period 1980 to 2030.

• Contribute to water and winter recreation needs for Marshall during the period 1980 to 2030.

• Contribute to the riverine woodland and wetland areas within the City of Marshall for ecological, diversity, and aesthetic purposes during the period 1980 to 2030.

A detailed discussion of planning objectives and criteria is given in Section D of Appendix I to this report.

In formulating a plan, consideration must be given to both structural and non-structural solutions giving due consideration to economic, environmental and social well-being factors. Preservation

and enhancement of study area natural, cultural and recreational resources are also considered.

#### FORMULATION AND EVALUATION CRITERIA.

In the formulation of alternative plans, two major objectives relating to Federal participation in water and related hand resource programs have been considered.

- \* Enhance national economic development by increasing the value of the Nation's output of goods and services and improving economic efficiency.
- \* Enhance the quality of the environment by the management, conservation, preservation, creation, restoration or improvement of the quality of natural and cultural resources.

To meet these objectives, each alternative is analyzed on a "with" or "without" project basis and is developed using a variety of technical, economic, and environmental criteria. Consideration is also given to the effects of all plans considered on regional development and social well-being of the affected people.

#### TECHNICAL CRITERIA

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Technical data such as hydraulic and soils parameters, design requirements, and results of other studies made for project designs and cost estimates are prepared and evaluated according to Corps of Engineers regulations and accepted professional practice. Both general criteria applicable to any project and criteria specific to the Marshall area were considered in formulating a plan.

<u>General Technical Criteria</u> require that the degree of protection be the maximum practical level of protection, or the Standard project flood level, if feasible. The plan must be complete within itself, technically feasible, and be generally in concert with water and related land resource programs of other interested agencies.

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Specific Technical Criteria require that controlled overflow into the Cottonwood River basin commence at a Redwood River discharge of approximately 6,500 cfs. Approximately 50 percent of the Redwood River flow in excess of 6,500 cfs would be diverted into the Cottonwood River basin. For interior drainage designs, these criteria require that any ponding or pumping facilities be designed to minimize adverse economic, environmental, and social well-being effects in affected areas.

#### ECONOMIC CRITERIA

The selected plan to insure effective operation of the existing project must be economically justified with a benefit to cost ratio greater than unity. Annual costs and benefits are based on a 50-year economic life, and interest rate of 6 7/8 percent and price levels and conditions existing in October 1977.

#### ENVIRONMENTAL AND OTHER CONSIDERATIONS

Environmental, recreational, and other planning criteria involve consideration of the public health and safety, social well-being, and quality of life of the local residents, as well as general public acceptance of the project. Environmental planning criteria require that preservation or enhancement of area environmental resources be given equal consideration with economic efficiency in developing and evaluating alternative solutions.

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Social well-being factors considered in this study include: possible loss of life and hazards to health and safety of area residents; preservation and enhancement of social, cultural, historical, and aesthetic values in the area; air, noise, and water pollution; injurious displacement of people and businesses; adverse employment effects; and disruption of desirable community and regional growth.

The plan must fit integrally into an overall plan for water and related land resources management and development for the Upper Mississippi River basin.

#### POSSIBLE SOLUTIONS

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Flood damage reduction solutions considered in this study pertain only to additional measures needed to assure effective operation of the existing project and to providing flood protection to downstream development not presently protected by the existing project. Both structural and non-structural solutions and combinations of both were considered in selecting a plan of improvement. In addition to these solutions, the consequences of doing nothing to alleviate the recurring flood problem is considered as a base from which to measure the impacts of positive alternative solutions.

No Public Action - Plan 1

This alternative represents the "without" project or base condition and provides for continuance of the existing situation at Marshall without any further local, State or Federal action to provide additional measures to assure effective operation of the existing

project. The existing situation relating to flooding at Marshall is represented by the existing federally-constructed project, flood warnings by the National Weather Service Forecast office in Minneapolis of impending Redwood River flood occurrences, related emergency flood fight and supporting disaster relief activities by the City and other government agencies, the required purchase of flood insurance to obtain federally-supported financing for building in flood prone areas, and flood plain management regulations recently adopted by the City of Marshall. It is recognized that flood warnings, if timely and accurate, tend to mitigate flood losses and are essential to public safety.

With this alternative (see table 1), a large portion of the highly developed central part of the city and agricultural lands adjacent to the city would remain vulnerable to extensive flood damages during major floods without major flood fighting efforts. No further public action would thus perpetuate the continued burden on the City in terms of human suffering, hazards to public health and safety and the required inefficient commitment of local financial and manpower resources. This course of action does little in terms of permanent flood damage reduction and is clearly unacceptable to the City. Therefore, this alternative was not considered further except as the base condition against which the other alternatives are compared. Only the continuance of flood warnings, the enforcement of local flood plain management, and flood insurance programs will be considered further but as supplements to other alternatives. With this alternative, average annual flood damages of \$352,685 could be expected to periodically recur.

Permanent Evacuation - Plan 2

Permanent evacuation would solve the residual flood problem at Marshall but would require the relocation of most developments in

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the city including over 1,100 residences, over 200 businesses, and several churches and schools. Roadways and utilities would remain as needed to serve adjacent flood-free areas and the evacuated areas which would be converted to open-space recreational and other public use areas. The displacement of existing development in addition to being totally uneconomic is considered impractical and totally unacceptable to local interests and therefore is not considered further.

Permanent evacuation of the downstream reach was considered not as an alternative to the existing project, but rather as a complement to it relative to evacuation of new unprotected development. Evacuation of this new development would involve the removal and relocation of eight new residences, 32 mobile homes, three apartment buildings of 33 units each, four apartment buildings with eight basement level units affected in each, and seven large buildings on the college campus. Total first costs for this alternative are estimated at \$20,000,000. Comparison of average annual costs and benefits of \$1,526,300 and \$379,900 respectively indicate an unfavorable 0.3 benefit-cost ratio as shown on table 1.

Movement of the apartment and college buildings would be physically impossible, leaving razing the only alternative. Even the temporary loss of the buildings from the State Regional College campus would place a severe and adverse economic, educational, and social impact on the community, region, and state. Permanent evacuation of the new development is totally unacceptable to all concerned interests and therefore not considered further.

Partial Evacuation and Flood Proofing - Plan 3

This alternative (table 1) would involve partial evacuation of selected downstream reach flood prone structures together with flood proofing measures to remaining residential, commercial, and public 19

structures in both reaches. Evacuated areas would be managed as flood damage-free areas in accordance with local flood plain management regulations that are in effect for the City.

Partial evacuation measures would involve the relocation of all residential structures subject to flood depths greater than 3 feet and any structure not considered suitable for flood proofing. With this alternative, 30 residences, 5 commercial structures, and the trailer court in the downstream reach would be relocated out of the 100-year flood plain.

Floodproofing measures would include structural changes and landscaping measures. Structural changes to the basement level apartment units would include sealing of doorways, windows, and other openings, sealing and bracing of basements, and in some cases, provision of floor drain standpipes. Structural changes to the college buildings would include these same measures plus the construction of bulkheads in interconnecting equipment tunnels and placement of valve closures in drain pipes running between and from the buildings. Sealing of the ground level windows and other openings could probably be accomplished but only with the remaining threat of extensive damage and possible health and safety hazards in the event of failure of any one closure. Seepage into these units would likely be a problem during major flood periods. Assuming effective bulkhead and valve closures, water damage to the college buildings would be minimized. However, extensive electrical failures would still be possible due to electrical shorting of cables, switches and connections in the cableways.

This plan would significantly reduce potential flood damages but only at excessive economic and social well-being costs as shown on table 1. The removal of the much needed residential and apartment housing from areas presently zoned and developed for this purpose would have a major adverse long-term effect on regional education-

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al opportunities and established community patterns. Local interests clearly do not favor a major rearrangement of area housing and indicate a preference for a more positive method of flood protection for the college campus. Further, it is accepted State policy that permanently habitable space below the regulatory flood elevation should not be flood proofed. Similarly, evacuation and floodproofing in the upstream reach would be totally infeasible since nearly all of the core city would be affected.

Upstream Reservoir Storage - Plan 4

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Reservoir storage was also considered as a possible solution to Marshall's flood problem. The only practical site from a technical standpoint is located in Camden State Park, about 8 miles upstream of Marshall. Earlier studies made in support of the existing project and recent preliminary review studies show that a single large reservoir would probably have sufficient storage capacity but would be economically infeasible and environmentally unacceptable. Estimated average annual costs and benefits of \$1,523,500 and \$339,900 respectively indicate an unfavorable benefit-cost ratio of 0.2 as shown on table 1. A reservoir in this regionally important park would result in extensive forest resource losses, the loss of several miles of canoe stream and stream fishery and major aesthetic alterations.

A system of small reservoirs on headwater tributary streams presently under consideration to solve agricultural flooding would be located too far upstream and have too little storage volume to provide the desired level of flood protection for the City of Marshall. Thus, for these reasons, upstream storage via a single large reservoir or a system of small tributary reservoirs is dropped from further consideration. FLOOD BARRIER AND CHANNEL WORK ALTERNATIVES - UPSTREAM REACH

Both flood barriers and channel works were considered as additional upstream reach measures to permit efficient operation of the existing project as designed. It became clear very early in the study that because of inadequate channel capacity and topographic and other constraints, neither levees or channel works alone would achieve the desired solutions. As described in the earlier report paragraphs on technical criteria, overflows of the Redwood River occur naturally during major flood periods in the vicinity of the Highway 23wayside park. Hydraulic studies subsequent to the 1969 flood indicate that approximately 50 percent of these overflows would have entered the Cottonwood River basin under natural (pre-existing project) conditions. To avoid any major hydraulic changes to the existing flood flow pattern at Marshall, all upstream structural alternatives provide for continuance of these overflows via diversion works at the wayside park.

COMBINED LEVEE - CHANNEL WORKS - PLAN 5U

This alternative would enable operation of the existing project to provide a 100-year degree of protection with the construction of levees, channel widening, bank protection, and clearing and snagging measures along the Redwood River between the existing diversion structure (mile 70.2) and the upstream study limit (mile 73.8). An overflow structure with attendant outlet channel and culvert works would be located at the wayside park. The 540-foot long overflow structure would divert approximately 50 percent of flood overflows in excess of the present design discharge of 6,500 cfs, or a maximum Another modification (5U-mod. 3) including a 700-foot long cut-off along with the 600-foot long cut-off would further reduce the channel length and provide a slight reduction in levee heights. As the increased total project first costs of about \$250,000 would clearly not be commensurate with the minor benefits gained, this modification is not considered further.

Modification (5U-mod. 4 or Executive Order 11988 Plan) would eliminate all right bank levees downstream of those required to maintain proper operation of the overflow structure. This modification would also require that State Highway 23 and CSAH 7 be raised to suitable elevations such that they would act as flood barriers. This would create an approximately 80 acre triangular ponding area which would keep flood flows from bypassing the diversion structure and flooding Marshall. Due to the additional costs that would be incurred due to the purchase of necessary lands and costs of required road raises, this modification would be economically infeasible and thus was not considered further. Detailed discussion of this alternative including analysis of substitute levees in lieu of the road raises is given in Section J of Appendix I to this report.

Two alternatives were considered to the proposed overflow structure along the right channel bank at the wayside park. The first would involve lowering of State Highway 23 in the vicinity of the wayside park to permit unimpeded overflow into the Cottonwood River basin. Downstream channel improvements would be limited to insure required river stages at the park (overflow area). However, limiting the channel measures would likely result in severe downstream bank erosion and potential levee damages. In view of these adverse effects along with possible damage to the highway, traffic disruptions, and potential overflow inundation damages to farm properties, this modification was not considered further.

The second alternative to the proposed river bank overflow structure would involve using the existing Highway 23 embankment as a

of 850 cfs at the 100-year Redwood River flow of 8,200 cfs.

The plan would also provide for minor interior drainage measures, relocation of two structures, and utility relocations. Plan impacts and total first costs of about \$1.7 million are shown on table 1. The plan would accomplish the desired improvement generally in accordance with the desires of local interests. Thus, it is carried forward for further impact analysis and possible combination with downstream improvements to develop a total plan for the area.

Several minor modifications to plan 5U were considered with a view towards modifying the effects of the considered levees and overflow structure. One modification (5U-mod.1) suggested by local interests would involve realignment of the right bank levee to permit flood-free use of a 10-acre river meander area located just upstream of CSAH 7. Although this modification would increase total plan 5U first costs by about \$160,000, it is carried forward for further impact and trade-off analysis at the request of local interests.

Another modification (5U-mod.2) would substitute a 600-foot long cut-off channel in lieu of a 4-foot high levee across the river meander. This cut-off channel would reduce the natural channel length by 1,900 feet and result in a slight lowering of the levees. This modification, with reduced main channel works and bank protection needs, would provide a net saving of about \$50,000 in total first costs, exclusive of financial losses to the property owner and a flood-free access. Utilization of the 10-acre area would be hindered as access across the channel would be affected by backwater in the cut-off channel every one to two years. As this modification is of questionable economic merit and lacks local support, it is not considered further.

controlled overflow wier together with raising of a driveway east of the park to confine overflows to the park area. This plan, together with considered downstream channel improvements would actually result in lesser overflows into the Cottonwood Basin and corresponding increased downstream flows through Marshall. Further, any changed downstream channel conditions with related back water stage effects at the park overflow area would make overflow control questionable. In view of these problems, potential highway embankment damages, and traffic disruptions, this modification was not considered further.

FLOODWATER DIVERSION CHANNEL - PLAN 6U

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Consideration was given at the request of local officials to a flood-water diversion channel between the CSAH 7 bridge and the Burlington Northern Railroad Bridge. This 4,200 foot-long channel with a 200-foot top width would pass about 60 percent of the design 100-year flood flow. In addition to extensive realigning and widening of the natural channel at the downstream confluence, extensive bank protection and levee works would still be required. Seven acres of forested land would be required for this plan. Greatly increased total first costs of about \$3.4 million and other plan impacts are shown on table 1. This plan would accomplish the desired flood damage reduction along the upstream reach but at a substantially higher economic and environmental costs than plan 5U. However, it is carried forward for further impact and trade-off analysis at the request of local interests. A modification of this plan providing additional by-pass channel capacity was also considered but dropped as added benefits did not compare favorably with increased project first costs.

#### STRUCTURAL AFTERNATIVES - DOWNSTREAM REACH

Alternative downstream reach structural measures considered as possible solutions together with the previously discussed upstream works include channel works, levees, combined leveechannel works, and combined levee-highway works as discussed in the following paragraphs. An itemized breakdown of economic, social, and environmental impacts for these alternatives is shown on table 1.

### CHANNEL IMPROVEMENTS ONLY - PLAN 7D

Downstream reach channel improvements to provide a 100-year degree of protection to bottom land cropland and scattered rural farmsteads was quickly found to be both technically and economically infeasible. Thus, channel improvements were considered only in the context of improving the operation of the existing project and reducing flood damages to unprotected urban development.

Considered channel improvements would include channel widening between river miles 64.63 and 66.3 and a 1,300-foot long channel cutoff between 65.47 and 65.94. Clearing and snagging would be accomplished along the entire reach downstream to the State Highway 23 bridge (mile 58.3). Riprap bank protection would be provided at two bends to prevent erosion of channel banks and possible damage to County Road 67. Estimated total first costs would be \$303,000.

These channel works would provide only a minor reduction in flood damages to flood-prone urban development. The upstream portion of these works would, however, mitigate the slightly increased river stages due to increased flows from the upstream reach works. In view of the limited benefits, and the potential adverse environmental effects,

particularly in regard to transient birdlife, occasionally utilizing the nearby river bottom woods, channel improvements were not considered further except in combination with downstream levee works.

### HIGHWAY ALIGHMENT LEVEE - PLAN 8D

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This alternative would include a 7,600-foot long levee extending a considered highway alignment (approved system route FAS 6072) from high ground near 5th Street and Hudson Avenue to high ground near the Highway 23 embankment. Also included would be a 450-foot long levee along the right channel bank upstream of the downstream confluence with the diversion channel and a low 200-foot long levee to bridge another low right channel bank area. Other works would include a 7-acre interior drainage ponding area with attendant ditch and outlet works and a temporary sandbag closure across 4th Street (County 67). These plan measures would result in more efficient operation of the existing project and provide a adequate degree of protection to presently unprotected downstream reach development.

Estimated total first costs of \$347,600 and other plan impacts are shown on table 1. Since this plan provides the desired degree of flood damage reduction, is incrementally feasible as indicated by a 2.5 benefit-cost ratio, and is generally acceptable to local interests, it is carried forward for detailed impact and trade-off analysis.

#### COMBINED HIGHWAY-LEVEE - PLAN 9D

This alternative was considered at the request of the City, which in conjunction with Lyon County, is considering a possible highway by-pass around the northern part of the city. This by-pass around

the west and north sides of Marshall would include approved routes FAU 5764 and FAS 6072. Route FAS 6072 would extend from the vicinity of the junction of the diversion channel and natural river (mile 66.1) easterly to U.S. Highway 23 as shown on plate 1. This plan would include a combined highway-levee embankment along much the same alignment as for plan 8D. Required flood control measures would be similar to those of plan 8D but excluding the 200-foot long levee and sandbag closure. The Federal first costs for flood control would be limited to the equivalent levee cross-section required together with the 400-foot levee and needed interior drainage works. As this alternative is favor is to the City, it is also carried forward for additional impact and trade-off analysis.

COMBINED LEVEE-CHANNEL WORKS - PLAN 10D

Consideration was given to combined levee-channel measures to further reduce flood stages and required embankment heights. This plan would include channel works (Plan 7D) together with the highway alignment levee (Plan 8D) and reduce required levee heights by about one-half foot. Interior drainage requirements would be the same as for plan 8D. Construction of the channel widening measures would require removal of an existing right bank levee and replacement of the 200-foot long levee with an 850-foot long levee of slightly higher height. Total plan first costs of \$580,800 and other plan impacts are shown on table 1. Average annual incremental first costs for the channel works of \$22,000 when compared with incremental average annual benefits of \$11,400 indicates that addition of the channel work is not economically feasible. Further, this alternative would have a greater adverse effect in terms of vegetative and habitat losses due to channel bank clearing and reshaping.

EXECUTIVE ORDER 11988 AND EXECUTIVE ORDER 11990 ALTERNATIVES

Additional alternatives prepared in response to Executive Orders 11988 and 11990 are presented in Section J of Appendix I to this report.

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| SPERMENTELSE SLEAR APPOLLA  |  | forestay take at your development site  | Possible same of tag  | ;   | <u>14 0</u>  | 13.1   | 1.1  | 4,6  | • •   | 2.4   |
| Winterstal other Affertes   |  | Anna biganang sito<br>Anna biganang sito  | Possibly some at new<br>development site  |   |  | He trees sflected -  |  |  |   |   |
| HATOPPA SEED, Affected  | -  | State Callege   | Brate Ceilege   |   |  |  |  |  |   |   |
|   | plaza migulations  | forere intgrang ad-<br>offect on Local<br>returnity pottore. Loss<br>of regionol offectional<br>facility  | Severe shert-com ad-<br>verse attest during ra-<br>laceting of 46 fickly<br>unsta.  | ····· Presarvan<br>and cuity<br>flooding.   | ion of stiblished community devolu-<br>ril pattorna due to increased ofers.  |  |  | Hajor benetje al offect dan<br>demogen along danmetredi rea  |   | f flood   |
| timisdist. ftimmfigs  | Long trom bahedits<br>To strong and<br>"iperial habitst<br>Ant to restlicted<br>Genelogiant with flood<br>plane regulation   | ung-toth behaftst to blologis<br>ethics the project anno. Jud<br>totses in othey areas where pr   | al andaristica<br>Cardinad payeesatt<br>Guidents releesta   | Conversit<br>Derpesta<br>ettimmit<br>hapezer  | on of Tobustary reduction is<br>al to assessive times along reduced<br>ast due to reaches, sing vith a<br>changer. Jorgers, forgerigry of<br>an benchisk forme.                                    | a biotis popula.<br>chamel and loves<br>unor long-torn<br>sinterion.offects        | <ul> <li>When I long-term advance<br/>offerts on advance and<br/>riporism tabling due to<br/>obsend Undification.</li> </ul> | Reduced hob.tot for opined on<br>and conti memory for the of the<br>gained offer in presention tiller<br>land.   | ar birds differ intg-<br>a to- aquatic and<br>d farm- to alammaj<br>habitat for<br>soil differ<br>area for is   | turn admyte diffects to<br>6 riperian habitet den<br>Redifications. Befored<br>rapiend game bises and<br>ls. Nort of the required<br>reports to the furnished |

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TABLE 1 -- COMPARISON OF ALTERNATIVE MANS CONSIDERED (CONTINU

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|   |  | ENTIRE ST  | JOY AREA   | -  | UPSTR   |
|---|--|--|--|--|---|
|   | PLAN 1   | PLAN :   | PLAN 3   | PLAN 4   | PLAN 10   |
| PLANTO OBJE TIVE ENEXTED  | ha<br>Public Action  | Permanent<br>Evacuation  | Partial Evacuation<br>and Floodproofing_                                   | lipstream  | Combined Levee<br>Channel Works   |
| 117 - 154 (Heurish States) - 2017 - 2017                        |  |  |  |  |   |
| Ecosystem stimut  |  |  |  |  |   |
| . e (e * 1)   | ant spole to residen-<br>tial development over a<br>long period of time and<br>in accordance with exist- | for agri, purposes. Pote<br>timi for the loss of up<br>to 200 ic, of cropiand 5<br>native vegetation if res  | tilled cropland or va-<br>cant lands. Increased<br>ogen-space areas.       | eral acres of fure r and<br>understors inver change<br>to aquatic vegetation in<br>and around reservoir in<br>State Park.<br>Likely conversion if<br>present limited them  | <pre>icres of mixed for<br/>ind understorw jow<br/>Loss of terrestial<br/>aquatic vegetation<br/>long riprapped cha-<br/>bank<br/> Winor iong-tei<br/>nabitat, short</pre>      |
| en de ator a compositor   | Presentation of existing<br>aquatic and riparian habi<br>rat due to flood plain<br>regulations.          | ing wildlife habi  | enhancement of exist<br>rat. Undetermined loss<br>at at redeveloped areas. | fisherv to lake fi nerv.<br>Loss of valuable game<br>and other small marmul<br>habitar.  | due to increst<br>struction. Per<br>labitat. Perm<br>cropland.  |
| kestret   | samenhat improved over<br>time:  | Major gain in open<br>space, park, and green<br>belt area,   | Moderate gain in open-<br>space, park,and green-<br>beit area.             |  | Permanent visu<br>impaired acces<br>where levees p<br>lots.   |
| Threatened ( condargered pesses                                 | No Effect  | No Known Effect  | No Known Effect  | Not Evaluated  | No KRE  |
| Aze Quality<br>Mater Quality                                    | Yu Lifect<br>Cont:Ruod decrease due<br>to unchecked channel<br>bank erosiun.                             | relocation and reco  | nd sir quality during<br>instruction period.                               | Short-term (4-5 vri in-<br>crease in smoke, dust,<br>and combustion products;<br>during reservoir clear-<br>ing & project constructi<br>Possible slow degrada-<br>tion of lake water qual-<br>ity over project life. | and combustion<br>project consti-<br>on.<br>Major increase<br>ing and shortly<br>term improvemen  |
|   |  |  |  | Beneficial effect at Mar<br>shall due to reduced sed   |   |
| Noise Gevel strest  | No Effect  |  | ase in noise levels duri<br>, and reconstruction per                       |  | ase during constru-   |
| lrreversible lo <b>mp</b> itments of<br>Rescuries to Buture Use | Vone   | Puel, materials, and<br>land for demolition<br>and reconstruction at<br>new site.  | Fuel, meterials, and<br>land for floodproofing                             | Several acres of forest-   | t.<br>it.<br>ion of   |
| Man-wade resources  | No significant effect  | Permanent removal of<br>hundreds of reside ,<br>and business structures  | Partial removal of most<br>prerely flood prone<br>itructures.              | Permanent loss of<br>state park facilities<br>in the reservoir area.   | One house wou:<br>located a shor<br>Four other won<br>somewhat affec<br>the close pro:<br>considered fl.<br>Other flood pr<br>would be sign:<br>susceptible to<br>flood damage. |
| Natural resources   | Continued streambank<br>eresion, high turbidity  | Some portion of evacuat<br>area could revert to a<br>near natural state. So<br>natural grass could be<br>adversely affected by<br>relocated development. | effects to natural   | Permanent loss of<br>males of free-flowing<br>a stream due to innumda-<br>tion by reservoir.   | Permanent los:<br>about 4.2 acru<br>of woodland.  |

1/federal first cost for flood control works same as for plan 7D. To now unprotected development unly.

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Jan Harris

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## WIN OF ALTERNATIVE "L"

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|   |   | H INLY  |  | LOW ISTREAM RE  |  | <b>A</b> 1. (A1  |
|---|---|---|--|---|--|--|
| PLW 4   | ·· · · · -  | PLAN NI   | Plan "D  | Plan 9D   | PLAN 9D  | Plan 100   |
|   | nd ted Tever<br>Carrel Motat  | Floodwater<br>Diversion (hannel)  | Channel<br>Improvements  | Highway Alignment<br>Levre  | Combined Highway<br>Levee  | Combined Lever<br>Thannel Works  |
| rtal acres of forest services<br>understors cover scharges<br>to aquatic vegetat or<br>and around reservest   | <ul> <li>toward formest: a<br/>operators over 3<br/>torerrestual and g<br/>or evenation a 3<br/>compared hannel 4</li> </ul>  | emporary loss of<br>round cover along<br>evens until respeding  | Temporary loss <sup>[4]</sup> to 5<br>yearsy of ground cover,<br>shrubs along 2 miles of<br>river oank. Permanent<br>loss of mature tree-<br>along river in the vi-<br>cinity of channel mod-<br>ilications.   | 4.5 scres of upland<br>grasses, forms, shrubs   | Temporary loss of about<br>4.1 acres of native<br>grasses, shrubs and a<br>few scattered trees               | Temporary vegetative<br>ground cover losses<br>along levee streas<br>Permanent loss along<br>riprapped channel<br>bank areas   |
| isels conversion of<br>opecant limited stream<br>Likners to lake fishers<br>alses f valuable game<br>and other small marma-<br>satitat.   | un tat short term -<br>un to horeand stra<br>tokato n. Permanent  | se effect on riparian<br>2 scason, advers, effect<br>am turbidity during con-<br>loss of wooled wild life<br>ove of 15.8 acres of tilled. | Tempurary and long term<br>term lisruption or smul<br>mammal habitat along re-<br>worked river banks and<br>nel cutoff. Short term<br>effect on insuted area<br>due to increased turbid<br>porary moverse effect to<br>birdlife utilizing wood<br>river as a resting place |   | n of small manmal nab-<br>s of 19 acres of tiller  | Short-term adverse<br>effect to stream fish<br>erv and other aquatic<br>life due to increased<br>turbidity and sedi-<br>mentations. Long-term (o<br>of small mammal habitat<br>the vicinity of channel<br>modifications. |
| Maior Visual and o hro<br>hanges in existing<br>State Pars with orma<br>lion of a large late.   | romanent cional char<br>moleces access to pr<br>where levers bass the<br>off.   |   | Long-term changes in areas where channelizat. takes place.   | ີ່ Moderate Visual ເ<br>ນວກ of levee and ື່,ບ   | hange to natural setting<br>aure ponding area.   | with completion  |
| Not Evaluated   | 'vo known effi  | ict.  | No Effect  | No effect   | No effect  | Na effect  |
| Short term (4-5 yr: i)<br>crease in smoke, dus?,<br>and combustion product<br>during reservoir clear-<br>ing & project construction.  | Short term (2 vrs.) and combustion production production  | t levels during   | Slight increase in<br>two-season constru   | n fust and combustion pro<br>action period.   | ducts during and for a s   | nort time after  |
| Possible slow degrada-<br>tion of lake water qual-<br>it, over project life.<br>Deneficial effect at Mar-<br>shall due to reduced sedi  | -Major increase in str-<br>ing and shortly after<br>term improvement due<br>stabilization.  | construction. Long  | Major increase in stream<br>turbidity levels during<br>construction period.  |   | No effect  | Significant increase in<br>stream turbidity and<br>sedimentation during<br>and shortly after chan-<br>nel construction work  |
| Ment loads.<br>M.<br>od Temporary increase  | during construction of  | eriad   | Tem  | porary increase during co   | nstruction period  | •••••••  |
| Several acres of forest<br>edistate park land and<br>fast flowing stream lost<br>to reservoir development<br>Materials for construction<br>outpackment, access road an<br>maintenance facilities. | during constru  | es expended   | Energy resources used<br>for construction.   | <ul> <li> Energy resources a<br/>project constructi</li> </ul>  |  | sed for  |
| Permanent loss of<br>state park facilities<br>in the reservoir area   | One house would be r<br>located a short dist<br>Four other would be<br>somewhat affected by<br>the close proximity<br>considered flood bar<br>Other flood prome st<br>would be significant<br>susceptible to recur<br>flood damage. | ance.<br>of<br>riers.<br>ructures<br>iy less  | No significant effect<br>other than raising and<br>widening one bridge.  | Major beneficial<br>effect to college<br>complex with<br>increased level<br>of flood protect-<br>ion. | A considered feeder hij<br>could be effiliently<br>integrated with the con<br>sidered levee embank-<br>ment. |  |
| Permanent less of<br>males of free-flowing<br>a stream due to immunda-<br>tion by reserveif.  | Permanent loss of about 4.2 scres of woodland.  | Permanent loss of<br>about 7 acres of<br>forested area.   | Permanent loss of<br>about 0.10 acres of<br>channel bank woodlands.  | No significant effect to<br>natural resources.  | o Same as Plan 80  | Same as Plan 80  |

### ALTERNATIVES CONSIDERED FURTHER

Of the upstream reach alternatives considered, only the combinedlevee channel works plan (5U) and the floodwater diversion channel plan were considered for detailed impact analysis. A minor modification of plan 5U to include protection of an additional 10-acre area via realignment of the project levee was also carried forward. This impact analysis clearly showed that of the two basic plans (plans 5U and 6U), plan 5U provides the most cost effective solution and is the least aesthetically and environmentally disruptive. Further analysis also indicates that protection of the 10-acre meander area would be technically feasible, locally acceptable but economically unjustified.

Of the downstream reach alternatives considered, the highway alignment levee (plan &D) and the combined highway-levee (plan 9D) were examined further. In addition, limited channel widening measures are also considered with both plans. Both plans would be technically and economically feasible from a flood damage reduction standpoint. The combined highway-levee plan would require about 20 more acres of cropland and result in slightly higher vegetative and habitat losses. Although initially suggested by the City as a possible efficient combination of projects, it is believed that the required planning and designs for the highway would not be completed in time to achieve a combined project assuming approval and normal Federal funding of any recommended flood control works. Since the proposed levee follows the proposed highway alignment, it could later be incorporated into the proposed highway without major modifications of the flood control project features.

### CONTRIBUTIONS OF ALTERNATIVES TO MATIONAL OBJECTIVES

To achieve a balanced plan for flood control while maintaining and enhancing the natural environment, separate plans were developed. The first optimizes national economic efficiency while the second provides for achieving the principal flood damage reduction objective while emphasizing the environmental quality objective. These separate plans were then analyzed via a trade-off analysis of plan impacts to achieve a compromise or selected plan.

National Economic Development (NED) Plan - The NED plan, from a national viewpoint, must reflect the best return on any investment of economic resources. From the foregoing analysis, the NED plan for the upstream reach would be plan 50 incorporating levees, overflow diversion works and channel improvement measures. Similarly for the downstream reach, plan 80 together with limited channel widening measures provides the most economical method of obtaining effective operation of the existing project and providing a 100year degree of protection to unprotected urban development. Thus, for the entrie project area, the overall NED plan would include plan 50 together with plan 80 and accompanying channel works.

Environmental Quality (EQ) Plan - Since all the alternatives considered were formulated based on satisfying the specific flood damage reduction objective, and the EQ plan must also satisfy this objective, the EQ plan will, with relatively minor alteration, be among the alternatives considered. Working within the context of a framework environmental quality objective plan, which was initially least disruptive to the environment, measures were added incrementally to develop the most acceptable and environmentally beneficial plan.

From an analysis of the alternatives considered further for flood damage reduction, it was determined that the overall EQ plan would include:

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For the upstream reach -- Plan 5U incorporating added measures including relocation and reshaping of the flood barriers at nearby residences to minimize adverse aesthetic effects, tree and shrub plantings at selected locations along the levees and surface treatment of the overflow weir to blend it into the park setting. Also included would be the controlled disposal of waste excavation, trees, brush and debris, deletion of clearing and snagging measures other than at riprapped or widened channel areas; and management of residual flood plain areas.

For the downstream reach - Plan 8D together with channel widening measures, tree and shrub plantings, and flood plain management measures for residual unprotected areas is selected as the EQ plan as well as the NED plan for the downstream reach since it would have no significant adverse effect on the natural and cultural setting while still satisfying the flood damage reduction alternatives.

Both the NED and EQ plans would also include a recreational trail system and related facilities along the rights-of-way needed for flood control measures. The proposed trail and other facilities are desired by local interests no matter what type of flood control measures are considered.

# SELECTING A PLAN

Of the alternatives considered, all but one total plan for Marshall have been eliminated. The selected plan reflects only minor tradeoffs from the NED plans and in this instance, is also the EQ plan.

In summary, the Selected Plan includes: upstream reach plan 5U without the major clearing and snagging measures but including the levee reshaping, relocations, aesthetic measures, and management of residual flood plain areas; downstream reach plan 8D with accompanying channel widening and flood plain management measures and recreational measures along both reaches. The characteristics of the selected plan have been evaluated according to the Federal Water Resource Council's planning objectives. A summary of selected characteristics for the selected and EQ plan, along with similar ones for the NED plan is given in table 2. A detailed account of plan characteristics for the selected plan is given in table D-4 of Section D of Appendix 1.

The selected plan provides the most cost-effective solution for assuring effective operation of the existing project and provides the most feasible means of flood protection to unprotected downstream reach urbanized development. Of the viable solutions considered in terms of flood control, the selected plan would result in the least adverse environmental impact in terms of required lands, vegetative losses and related effects on fish and wildlife habitat. Minimal (one family) displacement of people would occur. In this one instance, a house would be moved only a short distance on the same property. Thus, the environmental quality and social wellbeing objectives are best satisfied with this plan. Local interests have indicated at various meetings that the selected plan is acceptable. For these reasons, a total area plan incorporating the modified upstream reach plan 5U as described in the preceeding paragraph together with downstream reach plan 8D (also described in preceeding paragraph) and various recreational facilities is selected for detailed designs and recommendation.

# Table 2 - System of Accounts

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# Summary Comparison of Alternatives

|    |                           | NED Plan  | EQ and Selected Plan   |
|----|---------------------------|---|--|
| 1. | Plan Data                 |   |  |
|    | Structures                | Levees, channel<br>works, overflow<br>weir, culvert<br>works, ponding<br>area.  | Levee, channel works,<br>overflow weir, culvert<br>works, ponding area,<br>aesthetic measures. |
|    | Additional land           | 119.8 acres   | 119.8 acres  |
|    | Non-structural components | Management of resi-<br>dual flood plain<br>areas.   | Management of resi-<br>dual flood plain<br>areas.  |
| 2. | NED <sup>1/</sup>         |   |  |
|    | Beneficial (Ann.Benefits) | \$260,800   | \$260,800  |
|    | Adverse (Ann.Costs) 2/    | 156,300   | $160,600^{3/}$   |
|    | Net (Benefits)            | 106,300   | 100,200  |
| 3. | EQ                        |   |  |
|    | Water quality             | Temporary increase<br>in turbidity long-<br>term decrease.  | Temporary increase<br>in turbidity. Long-<br>term decrease.                                    |
|    | Recreation and open space | Added recreational<br>opportunities with<br>trail system and<br>other facilities.   | Additional recrea-<br>tional opportunities<br>with trail system<br>and other facilities.       |
| 4. | R.D.                      |   |  |
|    | Project area              | Beneficial effect<br>with protection of<br>regional State Col-<br>lege facilities and<br>improved prospects<br>for Marshall's stand<br>ings as regional tra<br>and service center |  |

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fulle 2. System of A country (continued)

Summery Congarn on of Alternatives

SED Plan

FQ and Selected Plan

5. SWB

Relaced flood risk

Reduced flood dame. Same as NED Plan ages to public, commercial, and residential development.

 $\frac{1}{2}$ /Present condition flood damage reduction benefits only.  $\frac{1}{2}$ /Excludes annual costs for purchase of floodway lands as purchase  $\frac{3}{2}$ /would be common to all upstream reach structural alternatives.  $\frac{3}{2}$ /Increased costs for levee widening and landscaping measures.

# SCALE OF DEVELOPMENT

To deter the optimum level of protection, annual costs and benefits were evaluated for the 50 year, 100 year, 100 year, 200 year, and 100 year those levels. In optimum relationship between average uncould note and benefits exists for a bid year level of protection. A consistivity analysis of interest rates varying over time versus benefit cost ratios for various levels of protection was made to determine the limits of economic feasibility. This analysis (see "ection D of Apiendix I) indicated that the maximum feasible level of protection or benefit-cost ratio greater than 1.0 would be about the 150 year level at an 8 3/8 percent interest rate. Provision of the added increment of protection between the 133-year and 150-year flood levels would result in significantly increased total Federal and non-Federal first costs of  $\phi(0,000)$ .

Provision of a standard project level of protection would require major additional works including road and driveway raises and the relocation of numerous residents and businesses in the downtown

area to accommodate needed flood barriers and interior drainage works. An SPF level of protection is clearly infeasible as indicated by a 0.7 benefit-cost ratio.

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With an assumed levee failure at the SPF flow, several hundred commercial and residential structures would be adversely affected in the city. However, as nearly all proposed levees along both study reaches would be relatively low (4 to 5 feet average height) and overbank velocities would be less than one foot per second, the potential for loss of life is not considered great. To assure that no SPF level flows would overtop flood barriers and enter the city, two feet of freeboard above the SPF flood level would be provided along the right bank levee between the existing diversion structure (mile 70.5) and proposed overflow works at the State Highway 23 wayside park.

After review of the draft feasibility report, the City has stated (See April 1978 letter from City in Appendix 2) that a SPF level of protection would be unrealistic and unacceptable. By letter of 21 February 1979 (See Appendix 2) the City also indicates that "the ... 133-year level of protection would still be a most acceptable level of protection" and that"... the additional work and cost involved do not warrant the relatively small degree of additional protection..." between the 133-year and 150-year flood levels. Thus, based on the optimization and sensitivity analysis, consideration of the impact of a SPF levee failure, and views of the City, a 133-year degree of protection is selected as the appropriate level for project designs and estimates.

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# THE SELECTED PLAN

This section of the report describes the plan of improvement as selected in the previous section on plan formulation. In addition to the basic plan description, all meaningful effects, both beneficial and adverse, are identified and discussed. Pertinent information concerning design, construction, and operation and maintenance is also presented to provide the reader with a broader understanding of the technical aspects involved in plan implementation.

### PLAN DESCRIPTION

The plan of improvement to provide additional measures to assure effective operation of the existing project and to provide protection to unprotected downstream reach urbanized development are discussed separately for the upstream and downstream study reaches. Also discussed briefly are the proposed recreational facilities. The general plan of improvement is shown on plates 1 and 2.

Upstream reach improvements would consist of levees, channel improvements, a gabion channel drop structure, an overflow diversion structure with attendant outlet channel and culvert works, road raises, two temporary sandbag closures, minor interior drainage works, relocation of structures and utilities, aesthetic treatment measures, and management of residual flood plain areas in accordance with adopted flood plain management regulations. Preservation of the 71.1 acre area upstream of CSAH 7 as project floodway is required to prevent encroachments in the area which would increase flood stages with possible adverse effects to the right bank levee and impaired operation of the overflow works.

Upstream reach levees would include a 2,260-foot long levee extending along the left bank from the existing diversion structure to the Burlington Northern Railroad embankment. Levee heights would range from 4 to 7 feet for an average of 5 feet. A 1,660-foot long levee with an average height of 4 feet would extend along the left overbank from the proposed gabion control upstream to high ground as shown on plate 1. The left bank levee would have a 10-foot top width and 1 on 3 side slopes except at the riverside residences located just upstream of CSAH 7. At this location the landward levee slope would be variable or warped as needed to blend it into the adjacent setting.

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Right bank levees would include a 6,350-foot long levee with an average height of 5.5 feet extending from the existing diversion structure upstream to the State Highway 23 embankment at the wayside park. This love would provide 2 feet of freeboard over the SPF flood level to preclude overtopping of the levee during flows exceeding the design flood level. Right bank levee works would also include a short levee and road raise extending from the proposed overflow diversion to high ground as shown on plate 1. A 45-foot long temporary sandbag closure at the upstream terminus of this levee would provide free-board to contain the 133-year flood with 3 feet of freeboard. A 100-foot long temporary sandbag closure would be provided as needed across Highway 23 at the east end of the wayside park to prevent SPF level flows from leaving the park area. Proposed channel improvements would include realignment of the channel for a distance of about 500 feet to alleviate the sharp river bend just upstream

of the CSAH 7 bridge Other channel works would include about 3,300 feet of channel widening along three river reaches to obtain bottom widths ranging from 45 to 55 feet as required. Reshaping and riprapping of channel bends would be accomplished as shown on plate 1. Reshaped channel banks not riprapped would be topsoiled and seeded. Abandoned car bodies and other large debris would be removed from the channel. Riprap would be placed over the entire channel cross-section at the CSAH 7 bridge to protect the bridge piers.

The proposed 540-foot long overflow diversion structure would divert approximately one-half the Redwood River flood flows in excess of 6,500 cfs (about 850 cfs at 100-year flood flow) into the Cottonwood River basin via the diversion overflow channel. A 6-foot high gabion channel control structure would be located immediately downstream of the overflow structure as shown on plate 1. This structure, together with the 1,660-foot contining left overbank levee would insure proper river stage control over the overflow weir.

The proposed 2,140-foot long overflow channel with required culvert works through the Highway 23 embankment would carry the excess Redwood River overflows into the Cottonwood basin. This channel, with a 20-foot bottom width and side slopes ranging from 1 on 4 to 1 on b would accommodate up to 50 percent of the excess river flow over 6,500 cfs or a peak flow of 1260 cfs at the design 133-year Redwood River flood flow

Required upstream reach interior drainage works would include the flap-gating of two double culverts through the Burlington Northern Railroad embankment, extension of a 36-inch highway roadside drainage system through the right bank levee works, the placement of one

gated and one ungated culvert through two driveways, and the relocation of one driveway culvert. In addition, minor landscaping measures would be accomplished at one right bank levee location to eliminate a small natural ponding area.

The proposed channel works would involve the excavation of about 61,125 cubic yards of material. Of this amount, 44,590 cubic yards would be utilized as levee fill. Two small left bank spoil areas (.7 acres total) would accommodate about 4,520 cubic yards. The remaining 12,015 cubic yards would be placed on the city-owned spoil disposal area adjacent to the existing diversion channel for later re-use.

The proposed upstream reach flood control improvements would require the acquisition of an estimated 99.5 acres of land and temporary construction easements at selected locations. Of these lands 71.1 acres would be flood plain lands located upstream of CSAH 7 and acquired for project floodway purposes. Necessary relocations would include the relocation of one house a short distance on the same property, five utility poles, 550 feet of farm fencing and the temporary relocation and replacement of 700 feet of buried utility cable. A temporary by-pass would be constructed across the median to permit two-way traffic on State Highway 23 during placement of the overflow channel culverts.

Proposed <u>downstream reach improvements</u> would include levee works, channel widening, interior drainage measures, and proposed management of residual flood plain areas as shown on plate 1. Required levee works would include a 7,670-foot long levee with an average height of about S feet extending from high ground near Highway 23 upstream to high ground near 5th Street and Hudson Avenue as shown on plate 2. A 100-foot long temporary sandbag closure would be required at the County 67 levee crossing to provide a 3-foot freeboard

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over the 135 year flood level. All, included would be a 450-foot long levee of 4-foot average height along the natural channel right bank upstream of the downstream confluence with the existing diversion channel. An B60 foot long levee with an average height of 5 feet would replace an existing right channel bank spoil levee removed by the needed charged withing all how on plate 1.

Froposed charned works would consider a decomposed the channel of the right back only to a monomoul bottom width of so feet for a distance of 1,350 feet extending downstream trop the downstream confluence of the existing diversion channel (while 66.1) as shown on plate 1. The reshaped channel bank would have a 1 on 3 side slope and be riprapped its entire length to insure protection of the adjacent levee.

Proposed downstream interior drainage works would consist of a 7acre ponding area, a 5,280-foot long collector ditch along the toe of the levee, and a 24-inch diameter drainage pipe together with needed outlet control works at its junction with County ditch 62.

Of the 54,100 cubic yards of material excavated from the ponding area and channel works, 34,100 cubic yards would be used for levee fill. An additional 9,400 cubic yards would be used to regrade a low area long the levee as shown on plate 1. The remaining spoil would be placed on vacant municipal property for later reuse by local interests.

The proposed downstream measures would require an estimated 20.3 acres of land and temporary access easements to construction areas. The channel and adjacent levee works would require relocation of six utility poles.

All levee crowns and levee and channel side slopes, and other disturbed areas would be reseeded with grass species such as sweet clover that provides cover for area wildlife. Trees and shrubs would be planted at selected locations to enhance the project area aesthetic setting. These plantings, together with the irregular or warped landward levee slopes would help blend the levees into the natural setting.

Proposed recreational improvements would include approximately 5.2 miles of combined walking-biking trail with rest areas and trail head facilities, and about 5.7 miles of cross-country ski trail. Local interest would provide at their expense a total of 0.9 miles of connecting trails prior to or concurrent with the construction of any authorized trail improvements. Other measures would also include limited picnicking facilities on project lands near Justice Park and the softball complex north of State Highway 19. Other facilities to be provided by local interests at their own expense would include development of a quiet area with trails in the wooded area upstream of CSAH 7 and an improved canoe access at the Highway 23 roadside park. Detailed discussion regarding lands, management and cost-sharing responsibilities is given on page 3 of this report and pages G-2, G-3, and G-34 in Section G of Appendix I. The proposed recreational facilities are shown on plate 2.

### EVALUATED ACCOMPLISHMENTS

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The principal accomplishment resulting from the selected plan of improvement would be the enhanced operation of the existing flood control project and the protection of unprotected downstream reach development located immediately adjacent to the presently protected area. The selected plan would provide a 133-year degree of flood protection to the Marshall area. The proposed works would result in an

85 percent reduction in average annual flood dimages to new development and significantly reduce the need for the present and periodic inefficient commitment of local material, financial and manpower resources during major flood occurrences. The alleviation of flood damages would not only enhance the area economy but would improve the safety and well-being of the affected people and preserve intact long established community patterns. The proposed recreational facilities would partially satisfy present and projected facility needs in the Marshall area. Thus, the selected plan accomplishes the study purpose and the desired improvement as expressed by local interests.

#### EFFECT ON THE ENVIRONMENT

The proposed downstream reach works would provide protection to about 85 acres of agricultural land adjacent to the city. Protection from flooding would likely facilitate the eventual conversion of this land to residential development as this area is presently zoned. A total of 119.8 acres of land would be converted to flood control uses. An additional 120 acres of vacant or agricultural land in the reach upstream of the City would also be afforded protection. Protection of these undeveloped lands is soley due to the selection of the most cost-efficient flood barrier alignments. Under existing conditions, the 205 acres of undeveloped flood plain lands can be developed in accordance with State flood plain management criteria by placement of fill to an elevation of one foot above the 100-year flood level. The selected project would not require fill for the development of this area. However, it is recognized that the proposed alignment may accelerate future development of this area.

Construction of the proposed channel works would have adverse shortterm effects on stream water quality, fish, and aquatic biota via increases in turbidity and sedimentation during and for a short time after construction. However, the stabilization of presently eroding channel bank areas would in the long-term reduce turbidity and sedimentation resulting in improved water quality.

The permanent loss of 4.2 acres of woodland would result in associated population losses of small mammals and song birds. Increased noise levels during construction would have unsettling effects on area wildlife. The loss of about 30 mature shade trees at four residences would result in adverse aesthetic impacts to the affected residences and loss of cover to area song birds. The loss of grassy vegetation along the reworked channel banks would also contribute to the permanent loss of small mammal and song bird habitat. The acquisition and designation of 71.1 acres of flood plain lands upstream of CSAH 7 as project floodway would preserve the natural characteristics of that area and maintain wildlife habitat in its current state.

The revegetation of all disturbed areas with cover species would mitigate the ground cover losses. Tree and shrub plantings and sculptured levee sections in the vicinity of affected residences would aid in blending the levees into the adjoining topography and setting. The proposed invee and overflow structure in the park would result in marked aesthetic changes including a slightly impaired view of the natural river setting. In effect, no park area would be lost as the project features would be open to park pedestrian traffic.

### OTHER EFFECTS

Placement of the culverts throughout the State Highway 23 embankment would inconvenience vehicular traffic for about a month. Picnicking and other uses of the wayside park would effectively be eliminated for about one summer season, due to increased noise levels and movement of machinery. Similarly, two driveways would be temporarily affected by road raises and movement of construction equipment. Access to two farm properties would be permanently affected by the levee and channel works.

The proposed works would require the relocation of one permanent residence a short distance on the same property. Noise, dust and pollutant levels would be noticeable during the construction period. The proposed works would not require the displacement of any businesses. In turn, they would enhance community conesion, likely increase protected property values and related tax benefits to the community. Preservation of established community patterns would help maintain Marshall's position as a regionally important trade and farm service center.

### DESIGN

Design of the remedial measures necessary to obtain effective operation of the existing project is based on the need for the maximum practical degree of protection and compatibility with State and local flood plain management regulations.

The existing project is designed to pass a peak discharge of 6,500 cubic feet per second (cfs) which originally had a recurrence interval of about once in 114 years - Kowever, revised frequency-discharge relationships indicate that a flow of 6,500 cfs now has an expected recurrence interval of about once in 59 years. Similarly, a flood with a 1% chance of occurring in any given year (100 year flood) is estimated to have a peak discharge of 8,200 cfs. The hydraulic design of the selected plan is based on providing protection against the 133year Redwood River flood flow.

Although the existing project was designed to pass a flood flow of 6,500 cfs, it was evident during the April 1969 flood (peak discharge of 8,090 cfs) that the design flow was not able to reach the

existing project. Studies also indicate that, without the April 1969 emergency works, overflows over CSAH 7 that commence at a Redwood River flow of about 3,500 cfs would have re-entered the natural channel downstream of the existing diversion structure and caused extensive damage. This zero damage discharge corresponds to a flood frequency of once in about 16 years. Hydraulic studies indicate that of the 8,200 cfs 1% chance flood flow, approximately 1,500 cfs would overflow the State Highway 23 embankment in the vicinity of the wayside park. Approximately 1,090 cfs would flow over CSAH 7 and re-enter the Redwood River downstream of the existing diversion structure. The remaining 5,610 cfs reaching the existing diversion project would combine downstream of Marshall with the re-entering 1,090 cfs overbank flow to give a peak 100year downstream reach discharge of 6,700 cfs.

Hydraulic studies indicate that approximately one-half of the April 1969 flood overflows would have entered the Cottonwood basin were it not for the flood emergency measures undertaken. Thus, to not aggravate either the Cottonwood basin flood problems or downstream Redwood River flood problems over those presently experienced, the design of the proposed overflow diversion structure is based on a near-equal division of overflows for a peak 133-year overflow discharge of approximately 1,260 cfs into the Cottonwood River basin.

Design of the re-shaped channel slopes and levee side slopes is based on the need to prevent slope failure under both peak flood and sudden draw-down conditions. Riprap bank and pier protection is designed in accordance with Corps standards to withstand shear forces created by peak channel velocities.

Structural designs were made in accordance with Corps design criteria. Structural items include the culvert headwalls and gate well for the ponding area discharge conduit.

### CONSTRUCTION

Construction of the project would be accomplished in two construction seasons Required levee fill would be obtained from the channel and ponding area excavation. Topsoil, stripped from channel bank, ponding area, and levee foundations would be stockpiled for later replacement over disturbed areas. Additional topsoil needs would be met from local sources. Riprap would be obtained from the established quarry at Granite Falls, Minnesota. Bedding and other aggregate would be obtained from local suppliers. Concrete and other culvert needs can easily be met from regional sources. Colvert flapgates and associated hardware would likely be obtained through suppliers in the Minneapolis-St. Paul area

The construction works would be closely monitored to minimize stream, air, and noise pollution Applicable guide specifications on environmental protection would be incorporated in any project plans and specifications to minimize pollution. These provisions would include landscape protection, debris burning, erosion control, dust and noise control, and discharges into streams. Plans and specifications will also include the specific type, size, and mix of ground cover, trees, and shrubs required for the project. Also included will be the identification and proper disposition of any buried artifacts uncovered during construction. Government inspectors would be present to monitor construction, and adherence to environmental protection and other project specifications

### OPERATION AND MAINTENANCE

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Operation of the project during a flood emergency would include erection of two temporary sandbag closures (three for an SPF level flood) and operation of the gated control structure at the outlet of the ponding area. Maintenance of the project would include mowing of designated levee, ditch, and channel areas; riprap adjustments or replacements; repair of any severely eroded channel bank areas; periodic inspection of culverts and flapgates; and periodic removal of collected sediment, debris, etc. from the overflow channel, collector ditch and ponding area. Also included would be the maintenance of the proposed recreational facilities. Required mowing would be timed so that the ground cover would be of maximum benefit to wildlife.

# ECONOMICS OF THE SELECTED PLAN

This section of the report presents the economic aspects of the selected plan for the City of Marshall. Included are pertinent details of the flood damage evaluation, benefit analysis, cost estimates and project justification.

#### METHODOLOGY

To determine the economic justification of the proposed project, the merits of the upstream remedial measures and downstream reach measures to protect new development were evaluated separately. Proposed upstream and downstream reach measures were justified on the basis of related annual benefits exceeding annual project costs. For the proposed development, a comparison of incremental average

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annual costs (interest, amortization, operation and maintenance) with estimated average annual benefits is made over the project life of the project. Project benefits are iscounted using a 6 7/8 percent interest rate and a 50-year economic life. All costs and benefits are based on October 1977 price levels. The base year used since the beginning of this feasibility study is 1980. A more realistic base year would now be about 1985. However, use of 1985 as the base year would not result in a change sufficient to warrant reformulation or revised scale of development studies.

### FLOOD DAMAGES

The areas subject to flooding include scattered residential, agricultural, and vacant lands in the upstream reach, nearly 300 acres of the highly developed central portion of the city, and agricultural, residential, public (mostly Southwest State College), and commercial property. Principal flood damages incurred include innundation damage to single and multiple family residential structures; the college buildings, equipment and grounds; damages to sewers, streets, and other utilities; and emergency flood fight, supporting disaster relief, and cleanup costs Intangible damages include hazards to public health and safety, community disruption, and human suffering and insecurity during major flood periods Remaining present condition flood damages with the existing project are estimated at \$352,685 at October 1977 price levels.

### BENEFITS

The principal benefits from flood damage reduction were evaluated as the reduction in flood damages due to obtaining a 133-year degree

of protection from the existing project together with needed remedial measures and the difference in flood damages to unprotected development with and without the proposed project. Residential, public, and commercial benefits were computed based on 1980 base year conditions with appropriate discounted allowances for future damage growth. In addition to the flood damage reduction benefits, significant flood proofing cost savings benefits would be obtained with the conversion of 68 acres of agricultural land with more intensive single and multiple-family residential development. Also, substantial benefits attributable to expected use of the proposed recreation facilities would be realized. Average annual project benefits attributable to protection of new unprotected development and increased locational advantages are summarized in the following table.

### Table 3 - Average Annual Benefits

### Benefit Category

Amount

| Flood damage reduction Remedial measures | \$ 204,570 |
|--|------------|
| Downstream reach                         | 58,610     |
| Future growth to 2030                    | 24,410     |
| Flood Proofing Cost Savings Benefits     | 11,110     |
| Recreation benefits                      | 43,130     |
| Total                                    | \$ 341,830 |

### FIRST COSTS

The total estimated first cost of \$2,504,000 for the project is based on October 1977 price levels for similar work in the area and is summarized in the following table.

| <u>ltem</u>                    | Cost              |
|--------------------------------|-------------------|
| Channel works                  | <b>\$</b> 738,600 |
| Levees                         | 171,800           |
| Overflow works                 | 418,200           |
| Interior drainage              | 184,000           |
| Relocations                    | 52,400            |
| Lands and damages              | 211,600           |
| Recreation facilities          | 385,600           |
| Engineering and Design         | 195,000           |
| Supervision and Administration | 146,800           |
| TOTAL FIRST COST               | \$2,504,000       |

# Table 4 - Estimated Project Costs

# ANNUAL COSTS

The annual costs of the interest, amortization, operation, and maintenance for the proposed project are \$187,590 as shown in the following table.

# Table 5 - Annual Costs

| Item                      | Cost       |
|---------------------------|------------|
| Interest and Amortization | \$ 178,590 |
| Operation and Maintenance | 9,000      |
| Total Annual Costs        | \$ 187,590 |

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### JUSTIFICATION

The proposed remedial measures to insure effective operation of the existing project to provide a 133-year degree of protection are justified in that the average annual flood damage reduction benefits exceed related average annual costs. Similarly, proposed downstream works to protect recent unprotected development are incrementally justified as shown in table 6 below. The figures given in the table represent direct tangible values only and are displayed for the National Economic Development (NED) account.

## Table 6 - Summary of Economic Analyses

| ltem                    |                                     | Amount     |
|-------------------------|-------------------------------------|------------|
| Average annual benefits | - upstream reach<br>remedial works  | \$ 221,730 |
|                         | - downstream reach -                | 76,970     |
|                         | - recreational facilities           | 43,130     |
| Average annual costs    | - remedial works                    | 124,620    |
|                         | - downstream reach                  | 28,680     |
|                         | - recreational facilities           | 34,290     |
| Incremental benefit-    |                                     |            |
| cost ratio              | - remedial works                    | 1.8        |
|                         | - downstream reach                  | 2.7        |
|                         | - recreation                        | 1.3        |
| Benefit-cost ratio      | - total flood control $\frac{1}{2}$ | 1.9        |

 $\frac{1}{Excluding}$  recreation costs and benefits.

# DIVISION OF PLAN RESPONSIBILITIES

The purpose of this section is to present pertinent information regarding cost apportionment between Federal and non-Federal interests.

### COST ALLOCATION AND APPORTIONMENT

Cost allocation among project purposes is not considered warranted for the proposed project since the proposed recreation works are limited in scope and represent a relatively small portion of the project costs and benefits. Project costs are apportioned between Federal and non-Federal interests under both existing legislation and the President's proposed cost-sharing policies as shown in Table 7.

### FEDERAL RESPONSIBILITIES

The Federal Government will design and construct the various features of the proposed works. The work charged as a Federal cost includes that for levees, channel works, the overflow diversion works, interior drainage works, aesthetic mitigation measures, and one-half the construction cost of the proposed recreation facilities. The Federal Government also assumes the cost of this study. The total Federal first cost, excluding costs of this study, is estimated at \$2,008,800 based on existing cost-sharing legislation. However, applying the President's proposed cost-sharing policies would result in a total Federal first cost of \$1,745,100.

### NON-FEDERAL RESPONSIBILITIES

Non-Federal interests must meet all elements of local cooperation which includes the assurance that they will:

- a. Provide, without cost to the United States all lands, easements, and rights-of-way including suitable areas for borrow and disposal of excavated material as determined by the Chief of Engineers for construction, operation and maintenance of the project.
- b. Hold and save the United States free from damages that may result from construction and maintenance of the project, not including damages which are due to the fault or negligence of the United States or its contractors.
- Maintain and operate the project after completion in accordance with regulations prescribed by the Chief of Engineers.
- d. Accomplish without cost to the United States all relocations and alterations of buildings (except nonstructural measures), transportation facilities, storm and sanitary sewer systems, public and private utilities, local betterments, drainage facilities, and other structures and improvements made necessary by construction of the recommended plan, as determined by the Chief of Engineers, excluding facilities necessary for the normal interception and disposal of local interior drainage at the line of protection.
- e. Prescribe and enforce regulations to prevent obstructions or encroachment on channels, floodway areas, and ponding areas which would reduce their flood-carrying capacity or hinder maintenance and operation.
- f. Provide a cash contribution for recreation equal to 50 percent of the final separable cost allocated to this function less a credit for the value of lands, easements, rights-of-way, alterations, and relocations furnished therefor.

- g. Publicize floodplain information in the areas concerned and provide this information to zoning and other regulatory agencies for their guidance and leadership in preventing unwise future development in the floodplain and in adopting such regulations as may be necessary to insure compatibility between future development and protection levels provided by the project
- h. In acquiring lands, easements, and rights-of-way for construction of the project, the local sponsor will comply with the applicable provisions of the "Uniform Relocation Assistance and Real Property Acquisition Policies Act of 1970," Public Lar 91-646, approved 2 January 1971.
- 1. At least annually inform affected interests regarding the limitations of the protection afforded by the project.

Under existing cost-sharing legislation, the total non-Federal first cost is estimated at \$495,200 (see local cooperation items a, d, and f above and table 7.) Applying the President's proposed cost-sharing policy would require non-Federal interests to contribute 20 percent of the project first costs assigned to flood damage prevention and 50 percent of the separable cost for construction of recreational facilities (see item f above) plus require the State of Minnesota to contribute 5 percent of the total first costs of construction. Thus, the President's cost-sharing policy would result in total combined non-Federal first costs estimated at \$758,900 (see table 7). Under both existing cost-sharing legislation and the President's cost-sharing policy, non-Federal interests would be required to satisfy local cooperation items b and c above, with item c estimated to result in \$9,000 annual operation and maintenance cost.

|                             |               | Non-Fe | deral     |                       |
|-----------------------------|---------------|--------|-----------|-----------------------|
| Item                        | Federal       | State  | City      | Total                 |
| Based on existing cost-shar | ing legislati | on:    |           |                       |
| Lands                       | -             | -      | \$211,600 | \$211,600             |
| Relocations                 | -             | -      | 52,400    | 52,400                |
| Channels                    | \$738,600     | -      | -         | 7 <b>38,</b> 600      |
| Levees                      | 171,800       | -      | -         | 171,800               |
| Overflow works              | 418,200       | -      | -         | 418,200               |
| Interior drainage           | 184,000       | -      | -         | 184,000               |
| Recreation facilities       | 192,800       | -      | 192,800   | 385,600               |
| Engineering, administration | 303,400       | -      | 38,400 (  | <sup>1)</sup> 341,800 |

Based on President's proposed cost-sharing policy:

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| Flood damage prevention     | \$1,332,500 | \$88,800                     | \$355,300             | \$1,776,600 |
|-----------------------------|-------------|------------------------------|-----------------------|-------------|
| Recreational facilities     | 173,500     | 19,300                       | 192,800               | 385,600     |
| Engineering, administration | 239,100     | <u>17,100</u> <sup>(2)</sup> | 85,600 <sup>(3)</sup> | 341,800     |
| Total (President's Policy)  | 1,745,100   | 125,200                      | 633,700               | 2,504,000   |

(1) Includes 50 percent of the separable Engineering, Administration (E,A)
cost (\$28,800) and 100 percent separable E,A relocations cost (\$9,600).
(2) Includes 5 percent of total E,A.
(3) Includes 20 percent of flood damage prevention E,A, cost (\$56,800) and

50 percent of recreational facility E,A cost (\$28,800).

# PLAN IMPLEMENTATION

Once a plan of improvement under the Section 216 authority has been found feasible and acceptable to local interests, the procedure necessary for its implementation involves the following steps:

- o The feasibility report on the plan and accompanying environment impact statement would be reviewed by such higher authorities as the Division Engineer, North Central, the Board of Engineers for Rivers and Harbors and the Office of the Chief of Engineers.
- The Chief of Engineers would seek formal review and comment by the Governor of Minnesota and interested Federal agencies.
- o Upon approval by the Chief of Engineers, the report is transmitted through the Secretary of the Army to the Congress for final review, authorization and appropriation of needed funding.
- Upon receipt of project funding, the District Engineer is directed to commence detailed planning studies and an estimate of cost.
- Upon completion of the detailed planning studies and subsequent review and approval by higher Corps authority, the District Engineer would be directed to prepare detailed designs and specifications and an estimate of project costs.
- o Concurrently with this detailed planning, the City of Marshall would proceed with acquisition of needed rights-of-way. The City also would enter into a local cooperation agreement with the Federal government.

- Upon completion of plans and specifications, the project would be advertised for competitive bidding by private contractors.
- After award of the contract to the lowest capable bidder, it is estimated that the project could be completed in two construction seasons.
- Upon completion of the project, local interests would commence project operation and maintenance

# VIENS OF NON-FEDERAL INTERESTS

Non-Federal interests coordinated with in the formulation of the selected plan included:

o The City of Marshall

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- o Lyon County Highway Department
- o Lyon County Historical Society
- o Minnesota Department of Natural Resources
- o Minnesota Pollution Control Agency
- o Minnesota Highway Department
- o State Historic Preservation Officer
- o Minnesota State Historical Society
- o Lyon County Board of Commissioners
- o Burlington Northern Railroad

Statements or resolutions expressing the views and recommendations of these interests are contained in Appendix II.

The proposed upstream and downstream reach flood control improvements were considered by Marshall City Council at meetings held at Marshall on 3 March and 20 October 1975 respectively. These meetings were open to and attended by the interested public. A public meeting was held at Marshall on 2 February 1977 to discuss the proposed plan of improvement and receive the public's views and comments related to the plan. A copy of the meeting transcript and related correspondence is contained in Appendix II, Pertinent Correspondence.

A meeting was held with City officials on 2 March 1978 to review revised study findings based on a review of the draft report by higher Corps authority. On 2 April 1979, a meeting was held with City officials and interested members of the public to discuss additional studies of alternative flood barrier alignments made in response to the President's Executive Orders 11988 and 11990. Upon conclusion of these discussions, the Marshall City Council adopted resolutions supporting the proposed flood plain management and recreation measures and indicating the City's willingness and intent to provide needed assurances of local cooperation when and as required.

# REVIEW BY OTHER FEDERAL AGENCIES

Federal agencies involved either in the formulation or review of the selected plan were:

- o Department of Agriculture Soil Conservation Service
- o U.S. Environmental Protection Agency
- o Department of the Interior National Park Service
  - Fish and Wildlife Service
  - Bureau of Outdoor Recreation.

The draft report with accompanying environmental impact statement was circulated for comment among the various Federal agencies. Statements received from these agencies are included in Appendix II.

## SUMMARY

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The City of Marshall and immediately adjacent flood plain reaches are subject to recurrent flooding of the Redwood River and related property damages even with the existing flood control project. The April 1979 flood clearly showed that natural conditions immediately upstream and downstream of the project were such that the design floodwaters could not be conveyed into or away from the project. This same flood also showed that substantial flood plain development in the downstream reach remains unprotected under existing conditions.

In addition to a "no further public action plan", nine possible solutions to the flood problem were analyzed. From this analysis and the demonstrated interest by the City of Marshall, it is concluded that the only feasible and acceptable plan for obtaining effective operation of the existing project and reducing flood damages to unprotected downstream reach development is the selected plan. This plan provides for channel works, levees, and overflow-diversion works to permit controlled passage of excess Redwood River flood overflows into the Cottonwood River basin. The project works would provide a 133-year degree of protection with generally three feet of allowable levee freeboard. Two feet of freeboard over the SPF flood level would be provided along the right bank levee upstream of the existing diversion structure to prevent SPF flows from overtopping the levee and entering the city.

The selected plan also provides locally desired recreational facilities, including bicycling and cross-country ski trails and limited picnicking facilities. Local interests would provide 0.9 miles of connecting trails at their expense prior to or concurrent with construction of any authorized improvements. Other recreational works, if desired by local interests and constructed at their expense,

would include nature, educational and quiet areas upstream of CSAH 7 and canoe access at the Highway 23 wayside park.

Natural resources to be committed in construction of the project would include approximately 119.8 acres of land including 71.1 acres of land for project floodway purposes. Of the 48.7 acres of land required for project construction, 4.2 acres are forested, 16.3 acres are in agricultural use, with the remainder as open space or vacant land.

Social and economic benefits of the project would include an increased and expanded level of flood protection, the enhancement of former flood plain lands, enhanced public security and well-being, the preservation of desirable community patterns, and the near elimination of the need for inefficient commitment of local resources for flood emergency activities. The proposed recreation works would partially satisfy unmet demands for recreational opportunities in the Marshall area.

The remedial measures required to obtain effective operation of the existing project are economically justified. The total project first cost is estimated at \$2,504,000. Protection of unprotected downstream reach development is incrementally justified with a benefit-cost ratio of 2.7 to 1. The upstream reach remedial measures are also justified as indicated by a 1.8 benefit-cost-ratio.

The non-Federal first cost under existing cost-sharing legislation is estimated at \$495,200. Construction of the project could be completed by the United States in two construction seasons dependent upon the availability of necessary funds, completion of plans and specifications, and receipt of non-Federal assurances of participation. Following construction, operation and maintenance of the project would be the responsibility of the City of Karshall.

#### EXECUTIVE ORDERS 11988 and 11990

Additional alternatives providing flood protection to the City of Marshall were prepared in response to E.O. 11988 and 11990 concerning flood plain development and the protection of wetlands. Analysis of the alternatives determined that they did not constitute "practicable" alternatives (as defined by the Executive Orders), nor do they preclude development in the flood plain. In addition, the selected plan generally meets the requirements in the President's 1980 budget criteria pertaining to flood plain development and wetland protection. A detailed description and evaluation of the alternatives is presented in Appendix 1, Section J.

#### SECTION 404 REQUIREMENTS

A public notice outlining the proposed flood control plans involving dredging and filling, in the Redwood River at Marshall was issued on 28 February. The notice summarized the expected significant environmental effects and offered any interested person opportunity to request a public hearing in accordance with Section 404(b) of the Federal Water Pollution Control Act Amendments of 1972. Comments on the public notice are attached to Appendix 2. \_\_\_\_\_\_\_ comments opposing the Corps of Engineers project and \_\_\_\_\_\_ requests for a public hearing were received. The proposed project would comply with the requirements of Section 404 as described in this report and the accompanying revised draft E1S.

# STATEMENT OF FINDINGS

I have reviewed and evaluated, in light of the overall public interest, the documents concerning the proposed action and the stated views of other interested agencies and the concerned public, relative to the various practical alternatives considered to insure effective operation of the existing flood control project and protect additional flood-prone development at Marshall, Minnesota.

The possible consequences of these alternatives have been studied for environmental, social well-being, and economic effects (including regional and national economic development as appropriate) and engineering feasibility.

#### BACKGROUND

Authority for the proposed plan is provided in section 216 of the 1970 River and Harbor Act.

Marshall, Minnesota, with a 1970 population of 9,886 persons, is subject to flood damages from overflows of the Redwood River. Marshall and Lyon County, of which Marshall is the county seat, requested in letters dated 3 July 1972 and 6 June 1972, respectively, that a study be made to determine what improvements can be made to increase the efficiency of the existing flood control project and provide additional protection.

The existing flood control project at Marshall was constructed by the Federal Government in 1963 at an estimated first cost of \$2,953,000 (1963 dollars). The project was designed to provide protection against a flood with an expected recurrence interval of once in about 114 years (0.88 - percent chance flood). However, as experienced during the April 1969 flood, this original level of

protection now represents only a 59-year degree of protection (1.69-percent chance flood). This reduced level of protection is mainly caused by inadequate flow capacity of the natural channel upstream and downstream of Marshall. Only a major local flood fight during the April 1969 flood prevented extensive damages to the city. However, Redwood River overflows into the Cottonwood River basin and the emergency flood fight activities resulted in moderate damages to some area farms, local highways, and other property.

Since the existing project was completed in 1963, considerable development has occurred on the flood plain immediately downstream of the project. The majority of this development, generally consisting of the Southwest State College at Marshall and student and other local housing, is not protected by the existing project. Without emergency flood barriers, this development would have been extensively damaged during the April 1969 flood.

Several meetings in support of this study were held in the city to obtain local views on city flood problems and needs. Two meetings, open to and attended by the public, were held on 3 March 1975 and 20 October 1975 to obtain the city's views on upstream and downstream reach alternatives, respectively. A late-stage meeting was held at Marshall in February 1977 to obtain local views on the selected plan. On 2 March 1978 a meeting was held with City officials to discuss revised study findings. On 2 April 1979, another meeting was held with City officials and interested members of the public to discuss additional studies of alternative flood barrier alignments made in response to Executive Orders 11988 and 11990.

#### ALTERNATIVES

Alternatives considered included no further public action, permanent evacuation of the flood plain, partial evacuation and flood proofing, upstream reservoir storage, channel modifications, levee works, and combinations of non-structural measures. The no further public action alternative represents the "without" project condition against which the impacts of all other alternatives are compared.

Except for flood plain management measures in conjunction with structural measures, none of the non-structural alternatives provide a viable, economically justified, or locally acceptable solution. Permanent flood plain evacuation would reduce most damages to unprotected development but would result in severe dislocations of established community patterns and severe adverse long-term effects to the State college. Partial evacuation and flood proofing would minimize the adverse effects to the college but still result in the locally unacceptable rearrangement of area housing patterns and other dislocations of established transportation and development.

Adequate upstream reservoir storage capacity is severely limited. One possible site exists in Camden State Park about 8 miles upstream of Marshall. A reservoir in the park would cause severe environmental losses and significantly change the use of the park. It would also be unacceptable to the State and local interests and is not economically justified. Tributary storage would, in total, result in probable major environmental losses and be technically and economically infeasible.

Several combination of levees were considered. A combination of upstream and downstream levees with channel modifications, overflow diversion, interior drainage works, aesthetic measures, and necessary relocations would insure the effective operation of the existing project and provide protection to additional areas. A comparison of estimated average annual benefits of \$157,500 with average annual costs of \$148,500 results in a benefit-cost ratio of 1.1.

Other measures for the upstream reach were considered including a perimeter levee around a 10-acre river meander area, an alternative

channel cutoff across the meander area to improve flow efficiency, a floodwater bypass channel, and raising of CSAH 7 and Highway 23 to provide temporary floodwater storage. None of these variations were recommended as they proved to be either impractical, uneconomical, or locally unacceptable or would cause unacceptable adverse environmental effects.

Of the other downstream reach structural measures considered, a combined highway-levee plan would be practical, feasible, and have only slightly more adverse environmental impacts than the other plans considered. However, the uncertainty as to the timing of local completion of required designs and availability of local funding precluded recommendation of the plan at this time. If these problems could be resolved before construction of the flood control works, the Chief of Engineers could permit construction of a joint highway-levee project. In any case, the selected plan would not foreclose the future and efficient combination of a highway with the downstream reach levee.

Various combinations of channel measures including widening, bank protection, and a channel cutoff were considered for the downstream reach. Other than 1,500 feet of channel widening to reduce slight upstream stage increases resulting from the upstream works and selected widening at bends and along a 1,000-foot reach upstream of the proposed overflow diversion structure, none of these measures had sufficient merit to warrant incorporation in the selected plan.

#### THE SELECTED PLAN

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The selected plan consists of structural flood plain management measures along the river reaches upstream and downstream of the existing flood control project at Marshall. Upstream works would generally consist of a 2,260-foot long levee along the north (left) bank and a 6,350-foot long levee with a temporary sandbag closure along the south (right) bank. The north and south bank levees would start at the upstream end of the existing project (existing diversion structure at river mile 70.2) and extend to high ground at the Burlington Northern Railroad and State Highway 23 embankments, resepctively. Other upstream improvements would include channel widening, riprap pier protection at the CSAH (County State Aid Highway) 7 bridge, an overflow diversion at the State Highway 23 wayside park with attendant 2,140-foot long overflow channel to control flood overflows into the Cottonwood River basin, interior drainage works, aesthetic measures, and necessary relocations.

Required downstream improvements would consist of a 7,670-foot long levee extending from high ground near the State Highway 23 embankment east of the city upstream to high ground in the vicinity of North 5th Street and Kossuth Avenue. For the most part, this levee would follow the alignment of a proposed highway under joint consideration by the city and Lyon County. If later desired, the highway could incorporate the levee embankment or be constructed adjacent to it. Other downstream reach levee works would include a temporary sandbag closure, a 450-foot foot long levee along the natural channel south bank just upstream of the downstream confluence of the natural channel and existing project diversion channel. An 860foot long levee about 2 feet high would bridge a low channel bank reach along the natural channel. The river channel immediately downstream of the downstream confluence would be widened to a 35-foot bottom width (an additional 5 feet) for a distance of about 1,500 feet.

Riprap bank protection would protect the widened channel bank and adjacent levee from erosion and possible damage. Related downstream interior drainage works would include a 7-acre ponding area with attendant collector ditch and outlet works. Six utility poles would be relocated along the 860-foot levee alignment.

The residual flood plain along both project reaches would be managed in accordance with existing city flood plain management regulations. Principal areas to be managed include the 71.1-acre floodway area upstream of CSAH 7, an 18-acre area along the north channel bank immediately upstream of the downstream confluence of the existing diversion channel, and the entire remaining flood plain riverward of the proposed downstream reach levee.

The proposed project would also provide for much needed recreation facilities. Initial facilities would include a 5.2-mile bike-walking trail and a 5.7-mile cross-country ski trail, trail head improvements, a rest stop at the existing softball complex, and limited picnicking facilities at Justice Park. Additional improvements that would be provided by local interests include a nature education and quiet areas in the wooded river corridor upstream of CSAH 7 and a canoe access at the State Highway 23 wayside park.

The proposed structural flood plain management measures would insure effective operation of the existing project and provide protection to presently unprotected downstream reach developments against a Redwood River flood having a 0.75-percent chance of occurring in any given year (133-year flood). The project would be constructed by the Federal Government at an estimated Federal first cost of \$2,008,800 and a non-Federal first cost of \$495,200. The project would then be turned over to the City of Marshall for operation and maintenance in accordance with the required assurances of local cooperation. Annual coperation, maintenance and equipmen<sup>c</sup> costs are estimated at \$9,000.

#### EVALUATION OF THE SELECTED PLAN

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Engineering Considerations Of the alternatives considered for the upstream reach, the combined levee-channel plan has proved to be the best method of solving the problem. The overflow structure

and attendant outlet channel in particular are considerd effective in controlling the damaging overflows into the adjacent Cottonwood River basin. The proposed plan represents the most logical solution evaluated on the basis of obtaining effective operation of the existing inefficient project, engineering feasibility, local acceptablility, and environmental effects. Total Federal and non-Federal first costs under existing cost-sharing legislation are estimated at \$2,008,800 and \$495,200 respectively. A comparison of estimated average annual benefits of \$341,830 with average annual costs of \$187,590 results in a benefit-cost ratio of 1.8.

Similarly, of the plans considered for the downstream reach, the selected plan proves to be the most effective method for improving the operation of the existing project and protecting additional development. The plan provides effective protection from the 0.75percent chance (133-year) flood and maintains the possiblity of a combined levee-highway during or at any time after construction. Thus, this portion of the overall plan also represents the most efficient plan in terms of economic benefits, technical feasibility and environmental effects.

Environmental Considerations An estimated 119.8 acres of land, including 41.0 acres of wooded land and 32.0 acres of tilled cropland, would be required for the project. The conversion of 4.2 acres of wooded land and 28.2 acres of undeveloped lands is expected to have adverse effects on small mammal communities in the area. The channel widening and bank protection measures would have at least short-term adverse effects on project areas, small mammals, amphibians, the limited area stream fishery, and other aquatic fauna. Many of these biological communities can be expected to begin repopulating the area once the construction activity ceases. The regular maintenance of the project, such as mowing of levees, will permanently suppress species that formerly occupied such areas. Although channel

excavation and bank protection works would markedly affect stream water quality during and shortly after construction, the long-term impact of these works is expected to be beneficial in terms of reduced erosion, sedimentation, and turbidity. The loss of mature shade trees and impairment of the river view at riverside residences would be a long-term adverse effect. Recreational trail use would result in a long-term change in the physical setting and increased noise levels during the summer at one riverside residence adjacent to the trail.

The proposed acquisition of 71.1 acres of flood plain lands for floodway purposes would provide a long-term beneficial impact in preserving the natural area from future encroachments. Aesthetic and wildlife habitat losses would be minimized by reseeding all disturbed areas with selected grass species and replacing lost residential trees with similar but smaller species at selected locations. The proposed works are considered to provide a balance between adverse environmental impacts and need for effective flood damage reduction at Marshall.

#### EXECUTIVE ORDERS 11988 and 11990 CONSIDERATIONS

The selected levee alignments make use of existing high ground, are economical and engineeringly efficient levee alignments. However, the selected levee alignments protect 205 acres of flood plain presently in agricultural use. In response to Executive Orders 11988 and 11990 concerning flood plain development and wetlands protection, alternate levee alignments were developed for both the upstream and downstream reaches of the project. Analysis of the alternate levee alignments determined that they did not constitute "practicable" alternatives (as defined by the Executive Orders) nor did they preclude development in the flood plain. In addition, the selected levee alignment generally fulfills the requirements from the President's 1980 budget criteria concerning flood plain development.

The selected and alternative levee alignments would have similar effects on the natural and beneficial values of the flood plain. The selected levee alignments may however, accelerate future development in the flood plain by eliminating fill requirements needed under existing conditions to meet State flood plain management criteria. The alternate levee alignments would approximately double the fill requirements necessar; for development under existing conditions, which may discourage or retard future flood plain development.

#### OTHER

Two feet of freeboard over the SPF flood levee would be provided along the right bank levee upstream of the existing diversion structure to confine flood flows exceeding the 133-year design level between the levee and the Burlington Northern Railroad embankment. Thus, the impact of floods on human safety with the proposed project would not be a major concern.

The overall study, draft report, Environmental Impact Statement, and public notices were coordinated with Federal, State, regional and local interests and groups. Appendix II of this report and Section 9.0 of the Revised Draft Environmental Impact Statement contain correspondence from the various concerned groups and interests, as well as the responses to their comments.

#### CONCLUSION

#### I find that:

a. The action proposed in the recommendations section of this report is based on a thorough analysis and evaluation of various practicable alternative courses of action for achieving the stated objectives.

b. Wherever unavoidable adverse effects are found to be involved, they cannot be avoided by reasonable alternative courses of action

which would achieve the congressionally specified project purpose.

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c. Where the proposed action results in an adverse effect, this effect is either minimized or substantially outweighed by other considerations of national policy.

d. The fill sites for the Marshall project have been evaluated and found in compliance with the Section 404(b)(1) Guidelines.

e. The selected project is in compliance with Executive Orders 11988 and 11990.

f. The selected alignment was coordinated and reviewed by the Minnesota Department of Natural Resources and found to be acceptable.

Accordingly, it is my decision that the public interest would be best served by implementation of the recommended action. Also, this plan is acceptable to the city of Marshall and the other agencies and interests associated with this study.

#### RECOMMENDATION

I recommend that the United States provide additional flood damage reduction measures and related recreational improvements at Marshall, Minnesota, generally in accordance with the plan proposed herein, with such modifications thereof as in the discretion of the Chief of Engineers may be advisable. The President in his June 1978 water policy message to Congress, proposed several changes in cost-sharing for water resources projects to allow States to participate more actively in project implementation decisions and to equalize cost-sharing between structural and nonstructural flood damage prevention projects. These changes include a cash contribution from benefiting States of 5 percent of the first costs of construction assigned to nonvendible project purposes. Application of this policy to the Marshall project would require the State of Minnesota to contribute an estimated \$125,200 in cash (5 percent of \$2,504,000 total estimated project first costs of construction assigned to nonvendible project purposes based on October 1977 price levels).

The president also proposed that the present cost-sharing requirements for flood damage prevention projects be modified to require a cash or in-kind contribution equal to 20 percent of the project first costs assigned to flood damage prevention benefits. Application of this policy to the Marshall project would require that non-Federal interests make, in addition to the State contribution, as a cash or in-kind contribution of an estimated \$412,100 (20 percent of the total project first costs of construction - separable costs assigned to recreation). Also, non-Federal interests will be required to pay, contribute in kind or repay, with interest, 50 percent of the separable cost for construction of recreational facilities, in accordance with the Federal Water Project Recreation Act of 1965. The amount involved is presently estimated at \$221,600. In addition, non-Federal interests will be required to provide assurances satisfactory to the Secretary of the Army that they will:

a. Hold and save the United States free from damages that may result from construction and maintenance of the project, not including damages which are due to the fault or negligence of the United States or its contractors.

b. Maintain and operate the project after completion in accordance with regulations prescribed by the Chief of Engineers.

The combined non-Federal share of project costs is currently estimated to be \$758,900 of total first cost and \$9,000 annual operation and maintenance cost. I recommend construction authorization for the Marshall project in accordance with the President's proposed cost-sharing policy.

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WILLIAM W. BADGER Colonel, Corps of Engineers District Engineer

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NCDFD-FF (June 1979) 1st Ind SUBJFCT: R-dwood River at Marshall, Minnesota, Feasibility Report for Flood Control

DA, North Central Division, Corps of Engineers, 536 S. Clark St., Chicago, Illinois 60605

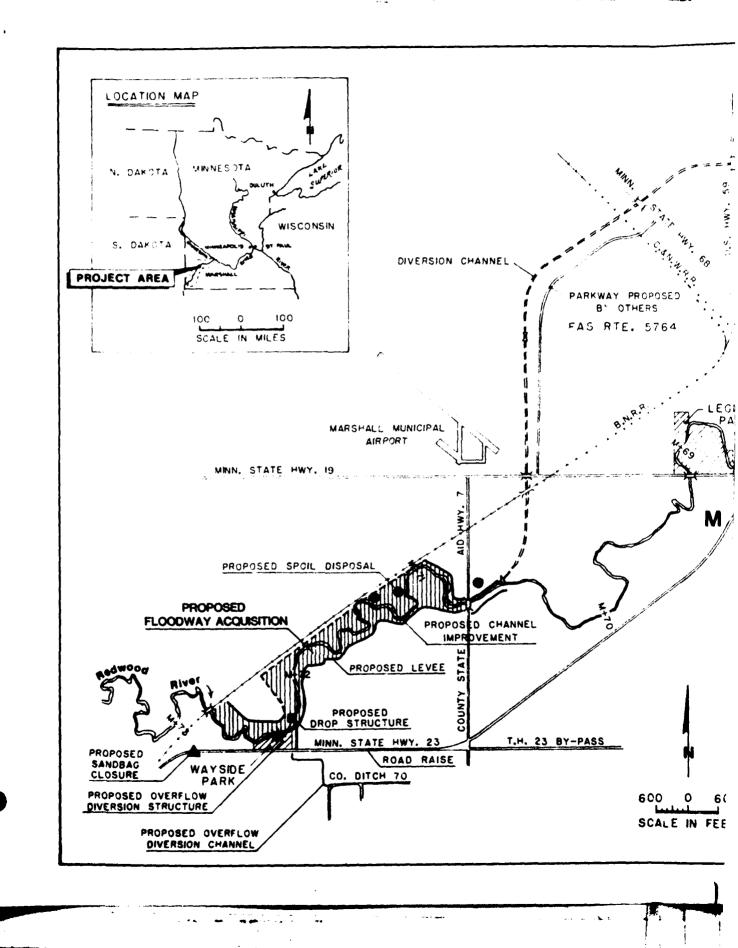
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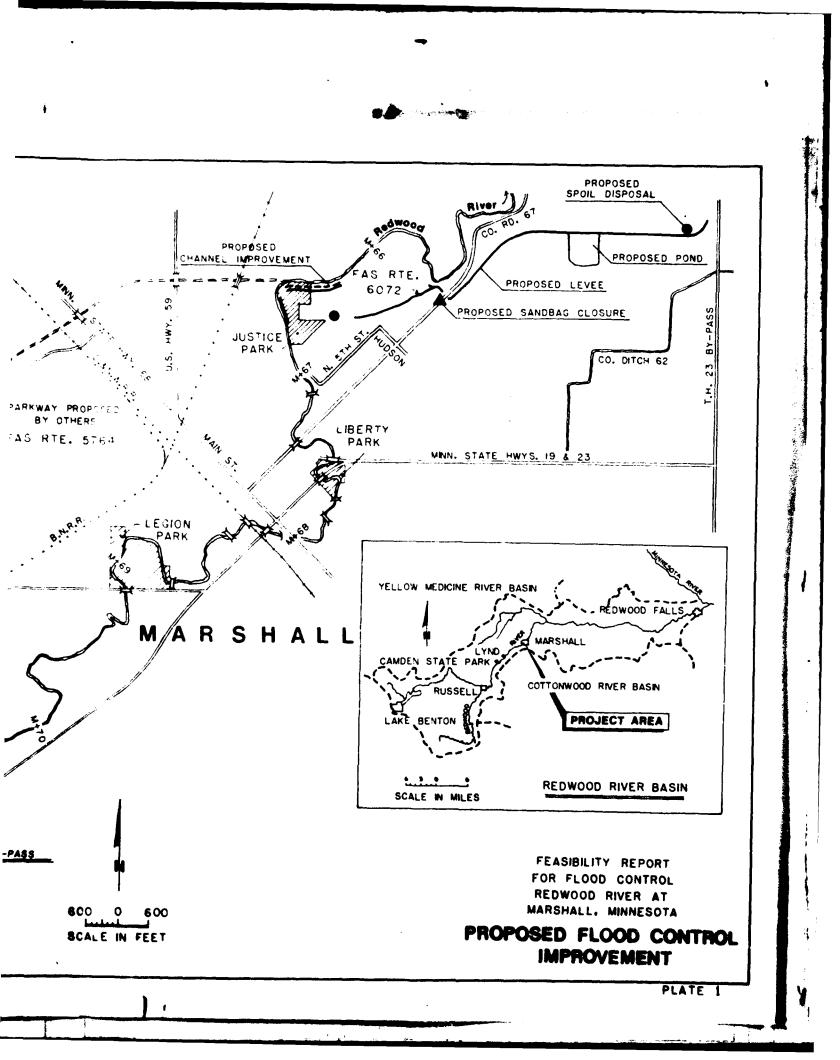
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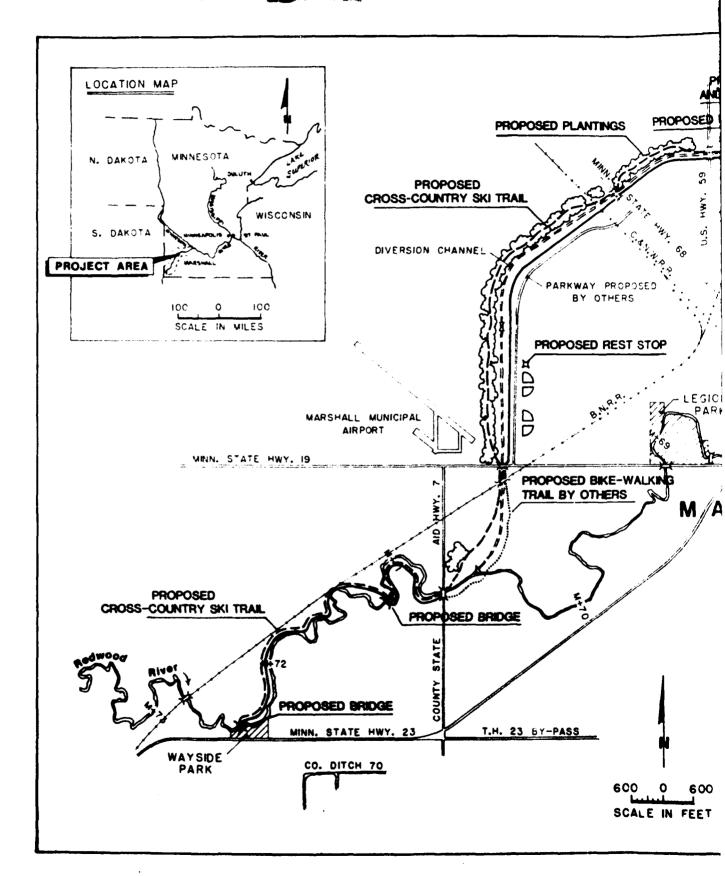
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I concur in the analysis and recommendations of the District Engineer.

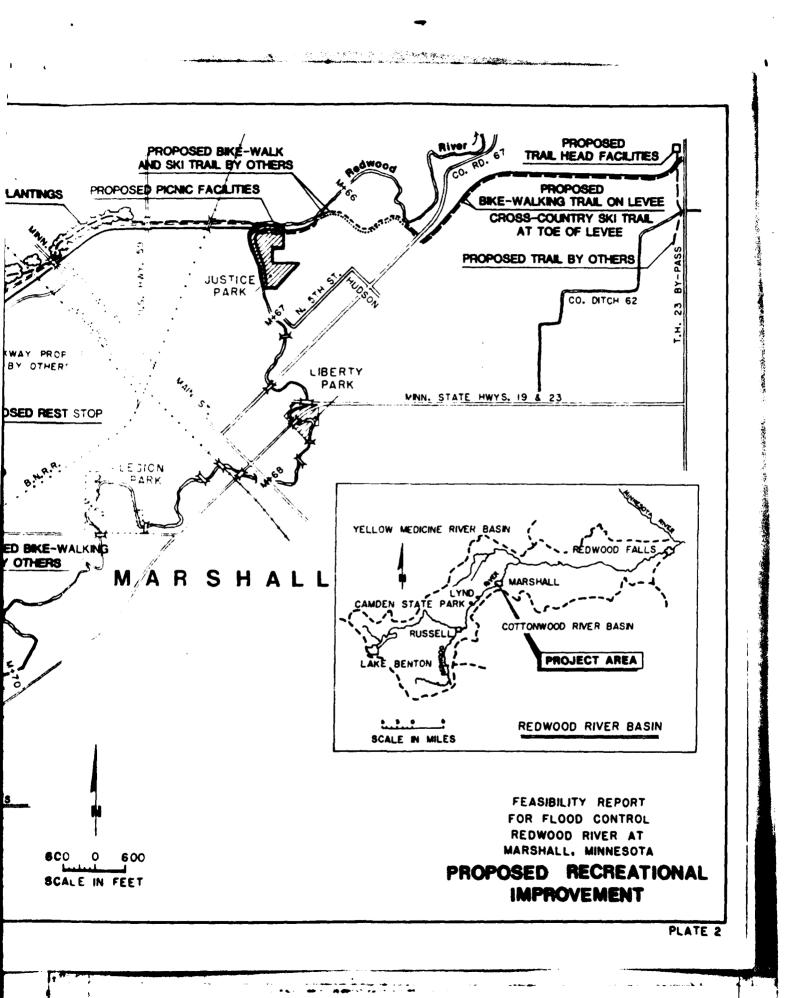
14 RICHARD L. HARRIS Major General, USA Division Engineer







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# FEASIBILITY REPORT FOR FLOOD CONTROL

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# REDWOOD RIVER AT MARSHALL, MINNESOTA

**TECHNICAL REPORT** 

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U.S. ARMY ENGINEER DISTRICT, ST. PAUL CORPS OF ENGINEERS SAINT PAUL, MINNESOTA

# SECTION A THE STUDY AND REPORT

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# SECTION A

# THE STUDY AND REPORT

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### SECTION A

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# THE STUDY AND REPORT

1. This section presents a discussion of study purpose and authority, scope of study, study participants and coordination and prior studies and reports on the same subject. It also includes a short discussion on the relationship of this technical report to the main report.

# PURPOSE AND AUTHORITY

2. Flooding of the Redwood River at Marshall has been a severe burden on the community. In 1963, permanent flood control works including channel improvements, levee works, and a channel diversion were constructed by the Federal government to reduce the recurring flood damages. The subsequent 1969 flood, however, demonstrated very clearly that the project would not convey the design flood through Marshall in the manner prescribed in the original project document and design memorandum.

3. Authority for this study is provided for in section 216 of the River and Harbor Act of 1970. This section of the Act states: "The Secretary of the Army, acting through the Chief of Engineers, is authorized to review the operation of projects the

construction of which has been completed and which were constructed by the Corps of Engineers in the interest of navigation, flood control, water supply, and related purposes, when found advisable due to significantly changed physical or economic conditions and to report thereon to Congress with recommendations on the advisability of modifying the structures of their operation, and for improving the quality of the environment in the overall public interest."

# SCOPE OF STUDY

4. This investigation concerns the adequacy of the existing Corps of Engineers project in providing flood damage reduction in the city of Marshall and adjacent urbanized area both upstream and downstream of the city. Investigations were made in sufficient detail to permit selection of the best overall plan from a series of alternatives and establish final project designs and cost estimates. Field surveys were made to obtain needed topographic information. Borings were taken at certain locations to establish foundation conditions. Field investigations were also made to identify critical erosion areas and other channel characteristics, and to determine the impact of the alternatives considered on the environment. Selection of the recommended plan was made after considering various effects, current planning policies and criteria, and views of the affected public. Coordination was maintained throughout the study with the City of Marshall and interested State and Federal agencies.

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# STUDY PARTICIPANTS AND COORDINATION

5. The principal objective during the formulation phase of this study was to devise an effective plan that is acceptable to the local public. Plan formulation, plan selection, final designs and estimates and preparation of the draft report were accomplished by Wehrman, Chapman Associates, Inc. - Minneapolis, Minnesota under contract to the St. Paul District Corps of Engineers. The St. Paul District had principal responsibility for the study including contract supervision, coordination with the public and interested local, State and Federal agencies, and preparation of the final report and environmental statement.

6. Several meetings were held with the City of Marshall to enable selection of the best plan. Formulation stage meetings with the Marshall City Council to discuss upstream and downstream improvements were held on 3 March, 1975 and 20 October 1975, respectively. Comments concerning the possible effects of a project action on area environmental, historical, and cultural values were requested from the following agencies:

- \* Minnesota Department of Natural Resources
- \* Minnesota Pollution Control Agency
- \* Minnesota Department of Highways

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- \* Fish and Wildlife Service Department of the Interior
- \* Bureau of Outdoor Recreation Department of the Interior
- \* National Park Service Department of the Interior
- \* Soil Conservation Service Department of Agriculture
- U.S. Environmental Protection Agency

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7. A late stage public meeting was held in Marshall during February 1977 to receive comments and any suggested modifications to the proposed plan of improvement. On 2 March 1978, a meeting was held with city officials to review revised study recommendations based on a review of the draft report by higher Corps authority. On 2 April 1979 a meeting was held with city officials and interested public to discuss additional studies of proposed flood barrier alignments in response to the President's Executive Orders 11988 and 11990. The city also adopted at this meeting, resolutions indicating its willingness and interest to meet local assurances of cooperation for the proposed flood plain management and recreation measures when and as required. Copies of these resolutions and transmitting correspondence are included in Appendix 2.

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# THE REPORT

8. This report consists of three parts: the main report and two appendices. The main report is a non-technical presentation concerning problems and needs alternative plans and their effects, and a recommended course of action to solve the flood problems at Marshall. The main report provides a broad view of the overall study for the benefit of both general and technical readers. It also provides emphasis on study items, such as plan implementation, report review by others, and study recommendations.

9. Appendix I is a detailed technical version of the main report. Although it follows the same general outline as the main report, it examines the problems, needs, and alternative solutions in depth for the benefit of technical review.

10. Appendix II contains all pertinent correspondence affecting coordination among Federal and State agencies and local interests and a summary of public involvement activities conducted during the study.

# PRIOR STUDIES AND REPORTS

11. House Document No. 230, 74th Congress, 1st session, includes a report submitted by the St. Paul District Engineer on 24 November, 1934, concerning water and related land resource problems in the Minnesota River Basin. However, this report did not specifically consider flooding and related problems in the Redwood River Basin.

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12. House Document 417, 86th Congress, 2nd session, includes a 25 March, 1960 report from the St. Paul District Engineer recommending flood control improvements at Marshall to include clearing and snagging of a 3.1 mile reach of the Redwood River, construction of 2,135 feet of levee, and a floodwater diversion channel at a Federal first cost of \$2,252,000 and subject to certain assurances of local cooperation.

13. A General Design Memorandum on authorized improvements on the Redwood River at Marshall was completed by the St. Paul District, U.S. Army Corps of Engineers in November 1961. This report provided the detailed designs and cost estimates for the existing Corps flood control project.

14. A flood plain information report on the Redwood River at Marshall was completed by Wehrman, Chapman Associates, Inc. Minneapolis, Minnesota under contract to the Corps of Engineers in March, 1975. This report, prepared at the request of the City of Marshall with the endorsement of the Minnesota Department of Natural Resources, contains maps, profiles, and cross-sections which indicate the extent of flooding which has been experienced and which could occur in the future at Marshall.

15. Other related reports include the Comprehensive Plan for the City of Marshall dated December 1962 with subsequent supporting updates and addendums and the State Comprehensive Outdoor Recreation Plan (SCORP).

16. A final draft Flood Insurance Study Report dated August 1976 for the City of Marshall was prepared by the St. Paul District under contract with the Federal Insurance Administration of the U.S. Department of Housing and Urban Development.

17. Flood plain management regulations adopted by the City of Marshall on 21 February 1978. These regulations designate (and regulate development in) the Floodway and Flood Fringe Districts as shown on the incorporated official zoning map.

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18. A report entitled "Archeological Survey of a Proposed Flood Control Project in Marshall, Minnesota" was prepared in 1978 by the St. Paul District, U.S. Army Corps of Engineers. This report documents the results of archeological field surveys to identify the presence and location of any archeological sites that may be affected by proposed flood control measures.

# SECTION B

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# RESOURCES AND ECONOMY OF THE AREA

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# RESOURCES AND ECONOMY

# OF THE AREA

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SECTION B

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### RESOURCES AND ECONOMY

#### OF THE AREA

1. This section of the report discusses the natural and human resources and state of development and economy at Marshall.

2. The City of Marshall (1970 population of 9,886) is located in southwestern Minnesota near the center of the Redwood River Basin as shown on plate B-1. It is located at mile  $68^{-1/2}$  on the Redwood River, which rises near the Minnesota - South Dakota boundary and flows northeasterly to a point about seven miles northeast of Marshall, where it turns and then flows generally eastward to its confluence with the Minnesota River. Marshall is a farm service center in a relatively wealthy agricultural region. Rich prairie soils in the surrounding area provide for high crop production except during drought periods.

#### ENVIRONMENTAL SETTING AND

## NATURAL RESOURCES

3. Marshall is located on the Redwood River, between approximate river miles 66.0 and 70.8 as shown on plates B-1 and B-2. The town

 $\frac{1}{A11}$  Redwood River mileages referenced to mile 0 at the confluence of the Redwood and Minnesota Rivers.

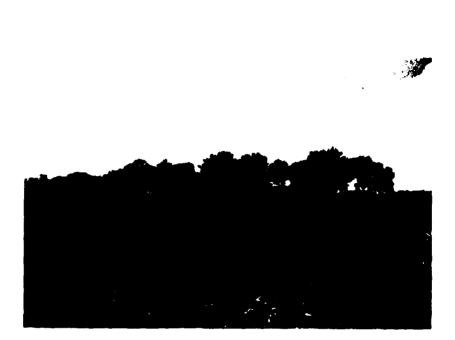
lies on the divide between the Redwood River Basin and Cottonwood River Basin, the Cottonwood River being about six miles to the south at its nearest point. The study area (plates B-1 and B-2) considered in this study is comprised of two separate Redwood River reaches. The lower reach extends from State Highway 23 (mile 58.3) to the downstream confluence of the river channel and diversion channel (mile 66.3). The upstream reach covers the remainder of the river upstream through the city to the upstream end of the existing left bank levee at river mile 73.8 located immediately upstream of the Burlington Northern Railroad bridge.

#### LAND USE

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4. Land use outside the urbanized area is predominantly agricultural with scattered rural residential and recreation uses. Typical agricultural land use along the upstream reach is shown on the following photograph. In most instances, this land use extends up to the narrow fringe of forest which borders the river channel. The Comprehensive Guide Plan<sup> $\frac{1}{}$ </sup> for Marshall indicates that by 1980. and with adequate protection against flooding, much of the agricultural (mainly crop) land in and adjacent to the city and the river corridor will be developed in about the same proportions of land use mix presently experienced. Public land use adjacent to the river corridor principally consists of a State wayside park at approximately river mile 72.5 as shown on plate B-1 and the Southwest State College at Marshall on the opposite side of town, shown on plate B-2. The only industrial use along either study reach is limited to that of the Burlington Northern Railroad at the upstream study area limit.

1/The Comprehensive Plan, City of Marshall, Minnesota December, 1962



Agricultural Land Use-Upstream Reach

#### GEOLOGY, TOPOGRAPHY AND SOILS

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5. The underlying rock formations in Lyon County date from Precambrian, Cretaceous, Pleistocene and recent times. Granite and quartziet comprise the Precambrian rocks. The Cretaceous strata overlie this and are composed of thick sections of soft shale and thin beds of sandstone. Glacial drift deposited in the Late Wisconsin glaciation of the Pleistocene period overlies the Precambrian and Cretaceous rocks, forming the surface of the area. Recent deposits of alluvium overlie the glacial drift in valleys and stream channels.

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6. In the project area, the Redwood River flows in a shallow channel across the Lowland Plain of the county. It is a slow-moving, meandering stream with a gradient of less than seven feet per mile. The river bottom is silted and relatively free of rocks and other obstructions to the water flow. Erosion can be a major problem along the riverbank as heavy rainfall and flooding wash away the topsoil along the river.

7. The Redwood River originates southwest of Marshall on an elevated till plain and flows northeastward in a well-defined, shallow valley less than 1/4 mile wide. From its origin, the river descends about 500 feet across a prominent regional slope onto an undulating till plain that slopes gently to the northeast. The river, on this lower plain, occupies a shallow channel that meanders across the plain in a meander belt 1,000 to 1,500 feet wide with no well-defined valley or flood plain for several miles northeast of the base of the regional slope. The lack of a confining valley and reduction in gradient on the lower plain contribute significantly to overland flooding in the Marshall area.

8. The city of Marshall is located about two miles northeast of the base of the regional slope. The upstream study reach is on a belt of alluvium that parallels the base of the slope. Borings in this area showed from 10 to more than 32 feet of mixed alluvial silt, clay and sand of recent origin resting on glacial sediments consisting of clayey till with some outwash sand. Some of the deeper sand identified as recent alluvium may actually be glacial outwash material. Borings for the downstream study reach showed only 2 to 12 feet of alluvial clay, silt and sand overlying glacial till. The topography along both study reaches consists of a river channel 30 to 60 feet wide and 6 to 8 feet deep meandering across nearly level

Appendix I B-4

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terrain, as shown on the plates in section E of this report. The depths to water recorded for the project borings were in most cases determined before static water-level conditions were reached and vary from 5-1/2 to 28 feet. The more reliable measurements, however, indicate that a water table under the proposed levee alignments should be expected at a depth of 5 to 7 feet. Well records in the area show that glacial sediments extend to a depth of 60 to 100 feet and are underlain by Cretaceous shale with some sandstone.

#### GROUND WATER - CITY WATER SUPPLY

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9. The municipal water supply is pumped from eleven wells which penetrate to the deeper artesian sandstones. Present storage capacity is 3.1 million gallons. The pumping capacity of these wells is 2,500 gallons per minute with an average demand of 1,500 gallons per minute. Peak demand is 2,300 gallons per minute. Fluoride is added to city water as required by state law. The water from the main artesian sandstone is quite hard with 513 ppm, containing large amounts of sodium, sulphates and chlorine.

10. Meltwater deposits associated with the Marshall moraine may have lateral subsurface extents of a mile or more beyond the limits of the surficial channels. These may have value as sources of ground water although in the lowland plain around Marshall, the glacial drift is too thin for these to be important sources of ground water. The pockets and layers of sand and gravel afford generally reliable sources of water.

11. The water table fluctuates seasonally, reflected in most wells in the area. When annual precipitation is normal, water levels rise in the spring due to heavy rainfall, snowmelt and frostmelt. This

is followed by a gradual decline from late spring until the first killing frost. The rate of decline in fall and winter gradually decreases until it is almost non-existent. Recharge to the ground water supply is effected by precipitation and discharge is accomplished through evapotranspiration and the flow of ground water into effluent streams. Minor fluctuations of the water level may be due to atmospheric pressure changes or pumping of nearby wells.

#### THE STREAM AND ITS VALLEY

12. The Redwood River rises in Pipestone County and is a major tributary of the Minnesota River. It has an elongated drainage area of approximately 743 square miles of which about 307 square miles are drained above Marshall. In both reaches the river is generally less than 40 feet wide with numerous areas of steep, eroding banks and is flanked on both sides by a fairly dense tree and understory cover as shown on the following photograph.



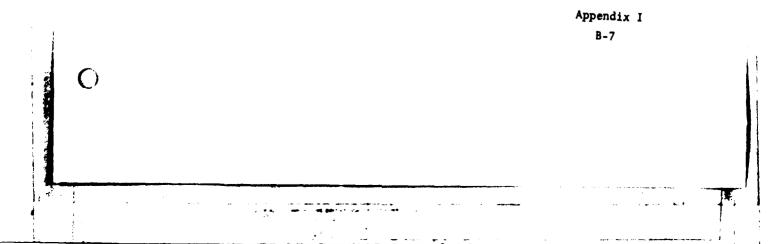
Typical Riverbank Vegetation

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|---|------|
|   |      |
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#### SURFACE WATER QUALITY

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13. The waters of the Redwood River within the project area are classified as 2B, 3C, 4A and B, 5 and 6 by the State of Minnesota. Surface water quality data for the Redwood River is presented in Table B-1. Applicable water quality standards are given in Table B-2.



c1- SI06-4 4.3 7.3 19.4 16.4 17.7 17.6 15.9 15.5 13.5 Udd Edd 103 296 941 ង 3 181 151 า 87 2.2 9. J <del>6</del>.1 9.9 7.1 6.S 8.5 10.5 E E 7.1 ÷ Mg.. g . 58 53 ÷7 © 69 63 84 64 74 CA. ECU 100 114 100 110 5 2 87 88 53 - Water Quality Data for Redwood River at Marshall + ¤ 2 mil 138 33 20 38 117 80 89 72 N-<sup>2</sup>CN לניו ৩ 5 ទ្ឋ 9 N S i-704 220 28 37 74 5 So 41 17 47 47 Tot-P L'ii ŝ SS 157 111 103 154 108 19 23 ppb1/ 1/ppm - milligrams/liter; ppb - micrograms/liter 1.0 3.6 017 017 2.7 10.3 1.3 0.7 5.7 20.8 1.5 Diss. ppm1/ 9.4 9.9 9.4 10.2 11.3 9.5 10.8 11.9 11.3 losal VinilexIV. Rogliicer 5.8 5.1 5.9 4.8 s.9 4.3 4.7 6.0 4.1 Table B-8 specitic Conductance Specitic 1050 1288 1069 1274 1745 1330 1104 1911 1454 (X11c 72.1) 74 8.7 105 (Mile 65.1) (Mile 58.3) 8.5 0.0 0 6.0 8.O 8.0 3.1 8.3 8.1 lid Sept.22,1974<u>3</u>/ Sept. 22, 1974 Sept.22,19744/ Aug. 25, 1974 **Jct. 24, 1974** Oct.24, 1974 Aug. 25, 1974 Aug. 25, 1974 Oct. 24, 1974 Station 112/ Station #2 Station 13 Sarpling ication Appendix I B-8

2/Sampling stations located upstream of Marshall, immediately downstream of Marshall, and at downstream study limit respectively.

3/ Hiver was dry upstream of Station #2 in September, but was flowing past the sample station.

4/ Kiver was dry upstream as well as downstream of Station \$3 in September. ONLY a stagment pool left.

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Table B-2 - Existing Water Quality Standard Applicable to Redwood River at Marshall

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# Limit or Range by Class

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| اف                             | ı   | I   |  |
|--------------------------------|---|---|--|
| ŝ                              | ľ   | ı   | 5.0-9.0<br>Same as   |
| 48                             | ł   | ı   |  |
| 4 <u>4</u>                     | ŀ   | 1   | -<br>-<br>6.0-8.5<br>-<br>Same as<br>er  |
| 20                             | ,   | ,   | -<br>-<br>-<br>6.0-9.0 6<br>-<br>e<br>te<br>ts.<br>for most S<br>probably<br>number over<br>100 ml.  |
| 85                             | - 6 ppm (1 Apr31 May)<br>- 5 ppm ( other times) | 5 <sup>0</sup> F above natural<br>(Max. of 86 <sup>0</sup> F) | <pre>1 ppm<br/>0.05 ppm<br/>0.01 ppm or - 1/10<br/>the 96 hour TLM valve<br/>0.02 ppm<br/>0.05 ppm<br/>0.01 ppm and none that<br/>6.5 - 9.0<br/>0.01 ppm and none that<br/>could impart odor or taste<br/>to fish flesh or other<br/>freshwater edible products.<br/>25<br/>200 most probable number 200 most<br/>per 100 ml. as a monthly probably<br/>geometric mean based number or<br/>on not less than 5 100 ml.<br/>samples a month or<br/>2000 most probable number<br/>per 1000 ml. in more than<br/>10% of all samples during<br/>2000 most probable number<br/>2000 most probable number</pre> |
| Substance or<br>Characteristic | Dissolved Oxygen                                | Temperature   | Ammonia (N)<br>Chromium (Cr)<br>Copper (Cu)<br>Cyanides (CN)<br>Oil<br>PH Valve<br>Phenols<br>Phenols<br>Turbitity Valve<br>Fecal coliform organisms   |

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Table B-2

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# Limit or Range by Class

| Substance or<br>Characteristic | 2B | 30      | <u>4A</u>                   | 84                     | 51         | 76     |
|--------------------------------|----|---------|-----------------------------|------------------------|------------|--------|
| Chlorides (CI)                 | ł  | 250 ppm | 1                           | i                      | 1          | 4      |
| Hardness                       | ı  | 500 ppm | 1                           | ſ                      | ,          | ı      |
| Bicarbonates (HCO,)            | ,  | 1       | 5 ppm                       | 1                      | 1          | 1      |
| Boron (B)                      | ı  | ,       | 0.5 ppm                     | •                      | ,          | 1      |
| Specific conductance           | •  | ı       | 700 ppm                     | r                      | f          | ı      |
| Total dissolved salts          | 1  | ŀ       | 60% of total cations as ppm | •                      | 1          | 1      |
| Sodium (Na)                    | ,  | 1       | lO ppm                      | 1                      | ſ          |        |
| Sulfate (SO.)                  | ۱  | 1       | : ,                         | None at                | ,          | ı      |
| Unspecified toxic substance    | ı  | ı       | - lev                       | levels harmful either  | ither      | ı      |
|                                |    |         | dir                         | directly or indirectly | rectly     |        |
| Hydrogen Sulfide               | ł  | ı       | 1                           | 1                      | 0.02 ppm - | 1<br>8 |
| Other                          | ı  | ı       | ,                           | ł                      | •          | ı      |

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1/The uses to be protected in this class may be under other juridictions and in other areas to which the intrastate waters of the state are tributary and may include any or all of the uses listed in the foregoing categories, plus any other possible beneficial uses. The Agency therefore reserves the right to impose any standards necessary for the protection of this class, consistent with legal limitations.

# Appendix I

**B-1**0

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14. From its source to a few miles southwest of Marshall, the Redwood River slopes at a rate of about 18 feet per mile. From this point to Redwood Falls. the slope is approximately four feet per mile. From Redwood Falls to the river's mouth at the Minnesota River, the average slope increases to about 24 feet per mile.

15. The general topography of the basin is that of rolling upland area. From the source of the river at an elevation of about 1,850 feet above sea level, the land slopes down to an elevation of 1,200 feet near Marshall. From this point, the river flows southeastward to Redwood Falls where the elevation is 1,000 feet. The relatively short distance from the City of Redwood River to the Redwood River's confluence with the Minnesota River is characterized by a drop in elevation of about 150 feet.

#### CLIMATE

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16. Marshall's climate is characteristically continental as it lies in the western portion of the Interior Lowlands. Wide seasonal variations in temperature are the norm for this area. The average July mean daily temperature is  $74^{\circ}$  F. while January, the coldest month, has a mean temperature of  $13^{\circ}$  F. The highest temperature recorded in Marshall prior to 1960 was  $107^{\circ}$  F; the lowest was  $-36^{\circ}$ F. The average annual temperature is about  $45^{\circ}$  F. The average date of the last spring freeze is May 8th while the first fall frost is generally about September 26th. The average annual growing season is approximately 150 days.

17. The average annual precipitation is 27 inches, 42 percent of this occurring during the June - August period. The average growing

season (May - September) precipitation is 14 inches. The monthly average is only 2.2 inches, although high-intensity rains of four or five inches in 24 hours are not uncommon during the spring and summer. The maximum precipitation in a 24-hour period in Marshall was the 8.07 inches recorded on June 17, 1975. The recorded maximum annual precipitation is 36.83 inches recorded in 1957. In 1976, only 12.05 inches of precipitation fell, the minimum recorded at Marshall. Annual snowfall averages 40 inches while the average annual number of days with snow cover of one inch or more is 90.

#### **VEGETATION**

18. Continued development over the years has left only a few small plots of native or virgin prairie and to a certain extent, the narrow river woodlands as the only original plant communities in the vicinity of Marshall. These communities can best be described as: natural prairie, grasslands inhabiting previously tilled crop land, domesticated agricultural or residential lands, and the woodlands near the river. The wooded river corridor along the upstream study reach is an extension of the coulee ravine woods protruding from the slopes of the Coteau des Prairie, these woods known locally as the Lynn Woods. Reed canary grass is by far the most abundant grass species along this reach and is found both on the river banks and in the river. Major tree species include American Elm, Green Ash, Cottonwood, Willows and Bur Oak. Sugar Maple and Quaking Aspen are present in limited numbers. The understory along the river is extremely dense and includes Wild Plum, Choke Cherry, High Bush Cranberry, June Berry, Sand Bar Willow, etc.

19. Most common tree species in the downstream study reach are the Box Elders. Reed canary grass is most dominant of all species along

Appendix I B-12 -

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this reach. Little evidence of shrub communities are found except near the city of Marshall. The only resemblance to native prairie vegetation can be found on two small floodway tracts enclosed by ox-bows. A typical example of vegetation along the downstream reach is shown on the following photograph.



Typical Flood Plain Vegetation - Downstream Reach

Aquatic vegetation along both reaches generally consists of a large number of species of peri-phyton (attached algae) and a few species of macro-phytes (aquatic weeds). Phyto-plankton comprised mainly of green algae and diatoms are also present.

> Appendix I B-13

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#### FISH AND WILDLIFE

20. Several wildlife management areas are located within ten miles of the study area, but none are in or adjacent to the project area. The river woodlands provide habitat, protection from predators, and a source of food and water for a variety of wildlife. The most common species of furbearing animals found in the area include the red fox, raccoon, mink, muskrat, and beaver. The woodlands along the river just downstream of Marshall are uniquely important to the local bird population as many species of wading birds are attracted to the sewage disposal ponds located north of Marshall. Species which utilize the river woodlands as roasting areas include the snowy egret (Leucophoyx Thula Thula), least tern (Sterna albatrass), piping plover (Charadrus melodus), and the buff-breasted sandpiper (Tryngites subruficallis), along with about 30 common species of birds. Game birds in the area include the ring-necked pheasant (Phasianus colchicus), redheads (ducks (Athya americana) and various species of migrant waterfowl.

21. No significant fishery exists in the Redwood River at Marshall due to 21. No significant fishery exists in the Redwood River at Marshall due to the high turbidity and intermittent periods of little or no discharge. The State area fisheries manager indicates that the stream fishery in the study area consists of common minnow (Cyprinus sp.) species, fathead (Pimephales notatus), and sucker (Catostomus sp.), minnows rough fish such as carp (Cyprinus carplo), suckers (Catostomus sp.), and bullheads (Ictalurus sp.); and possibly a few green sunfish (Lepomis cyanellus) and orange spotted sunfish (Lepomis humilis). A few northern pike (Esox lucius) may utilize the stream during spring high water to reach spawning areas.

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Appendix I B-14 -

#### THREATENED AND ENDANGERED SPECIES

22. A review of the 26 September 1975 and 16 June 1976 Federal Registers and all updates indicate that no threatened or endangered animal or plan species are found in the project area or would be affected by the project. Artic peregrive faleou are reportedly an infrequent visitor to the area. However no adverse effect on this species is considered likely.

#### ARCHEOLOGICAL - HISTORICAL

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23. In compliance with Section 106 of the National Historic Preservation Act of 1966 and Executive Order 11593, the National Register

of Historic Places has been consulted and as of 9 December 1975, no sites in the proposed project area have been designated as important historical and/or cultural sites.

24. A cultural resources literature and records search was conducted to determine the presence of known historic and/or prehistoric sites and to estimate the potential for the existence of additional sites. The search disclosed that there are no recorded prehistoric sites in the proposed project area, but that immediately upstream of the area there are recorded burial mounds. Prehistoric cultural material has been collected in the vicinity of the mounds, suggesting the presence of sites, yet unrecorded.

#### RECREATION

25. Marshall has four municipal parks - Legion Field, Liberty Park, and Freedom Park, and the generally undeveloped Justice Park. These parks provide facilities for swimming, ice skating, tennis and softball. In conjunction with this, the area schools make all of their facilities available to community residents for recreation. One private 18-hole golf course is located in Marshall. The State maintains a wayside rest area southwest of the community on State Highway 23. The Redwood River at Marshall is occasionally used for wading and swimming. The natural area along the river has walking trails outside of the city, but they are not publicly owned. Some horseback riding is also done along the river near the wayside rest area. Fishing along the river is negligible as is canoeing, due to the very shallow areas, fallen trees, etc. The City is presently making a study of a perimeter bicycle trail system around the city. This trail system would utilize existing city-owned diversion channel right-of-way and would provide connections to the college and downtown areas.

#### AESTHETICS

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26. The wooded riverine corridor provides an attractive setting for the City of Marshall, otherwise located in an area of mostly open and monotonous agricultural land. However, in certain areas, this natural setting is interrupted by rural residential development near or on the riverbank and scarred by areas of severe erosion, mud and silt deposits, and piles of junk and debris placed on the river banks.

## INSTITUTIONAL SETTING

27. In accordance with Federal criteria, the Redwood River at Marshall is classified as a navigable stream. The Minnesota Trust Doctrine provides that, on all navigable streams, the State owns absolutely the bed of a watercourse and that the riparian owner owns that shore property up to the high water mark. Chapter 105.38 of the Minnesota Statutes provides that its State policy to control and supervise, insofar as practical, the construction, reconstruction, repair, removal or abandonment of dams, reservoirs, and all control structures in any public waters of the State. This control and supervision is accomplished by the issuance of water use permits as provided in Chapters 105.37 to 105.77.

28. The Federal interest in water resource management, and more specifically, flood control at Marshall, is embodied in the specific legislation authorizing the existing project, Section 205 of the 1960 River and Harbor Act, as amended, and Section 216 of the 1970 River and Harbor Act. Section 205 provides for the construction

> Appendix I B-17

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of small flood control projects with a Federal first cost less than  $1,000,000^{1/}$  without specific legislation, and which are complete within themselves. Section 216 provides for the review of completed project with a view towards correcting project deficiencies due to significantly changed physical or economic conditions.

29. Two county ditches are located within the study area. These ditches, No. 70 and No. 62, are located as shown on plates B-1 and B-2, respectively, are maintained by Lyon County in accordance with State law. The Redwood River is classified as a judicial ditch along a reach commencing at the State Highway 23 crossing (mile 58.3) and extending downstream into Redwood County.

30. The existing flood control project at Marshall is entirely within the city limits. The City maintains and operates the project in accordance with local assurances of cooperation previously furnished by the City to the Secretary of the Army. Under present State law, communities generally do not have the expressed right to enter into cooperative agreements with Federal agencies but must seek and obtain specific enabling legislation for any such agreements. However, the City did furnish the required assurances for the existing project and very likely has the capability to provide required assurances for any additional related work. The City would also be responsible for providing any required local cash contributions. These contributions could possibly include State or County contributions towards project-related highway and other improvements of State and/or County interest

31. Under present State law, local communities are required to promulgate and enforce flood plain management regulations or be subject

Appendix I B-18

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 $<sup>\</sup>frac{1}{1}$  This amount is increased to \$2,000,000 if the area has been designated a Federally-declared disaster area within the past 5 years.

to such regulations imposed by the State in the absence of local regulations. The City of Marshall presently has a flood plain management program in effect based on a recently completed flood plain information study by the Corps of Engineers. The unincorporated flood plain reaches upstream and downstream of the city are subject to flood plain management regulations currently in effect for Lyon County.

#### HUMAN RESOURCES

32. Minnesota was organized as a territory in 1849 and Lyon County saw its first permanent settlers in 1867. The present site of Marshall was settled in 1869 by C.H. Whitney and C.H. Upton. The only advantages of the site at that time were its proximity to the river, the close location to an Indian trail between Lynd and Redwood Falls and its good farmland.

33. 1872 was a momentuous year for Marshall. In July of that year, the town was named in honor of a former governor of Minnesota. October 12th was the date on which the railroad was completed as far as Marshall. The village was platted in October and the Atlantic Hotel was opened in that month. In 1873, the State Legislature passed a bill changing the county seat from Lynd to Marshall, which was ratified by the voters in November, 1873.

34. By 1874, Marshall had a population of 300 and in 1876 it became an incorporated village. The population was 961 in 1880 and it grew to 1,203 by 1890. The 1890s witnessed the major growth of Marshall

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as the population grew to 2,088 in 1900. The city grew steadily although the Depression years were hard and by 1950, population was placed at 5,923. The growth between 1950 and 1960 was 758 persons, increasing the population to 6,681. The 1970 census places the population at 9,886, an increase of 48 percent over the 1960 population figures. This increase is attributable both to annexation by the city and the fact that the Southwest Minnesota State College was established in 1967. The college enrollment accounted for approximately 2,985 persons in 1971. The increase in Marshall's population between 1960 and 1970 would have been approximately 1,100 had the college not been established, an increase of 16 percent.

35. College enrollment has decreased since 1970 and is expected to stabilize at approximately 1,900 students in the future. Marshall will continue to grow, but at a decreasing rate over the next 25 years as indicated by the projections in table B-1, unless unforeseen circumstances arise. Projections of city populations for 1980 and 1990 are 11,856 and 13,730 respectively, while the population is expected to reach approximately 15,000 by the year 2000. Developments that might change the pattern of growth are the introduction of new industries, creating new jobs, and the possiblity of war or natural disaster.

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Appendix I B-20

|               | Pc                          | Population            |                      |  |
|---------------|-----------------------------|-----------------------|----------------------|--|
| Year          | <u>Marshall<sup>1</sup></u> | OBE Subarea 0701      | Change<br>(Marshall) |  |
| 1 <b>9</b> 00 | 2,088                       |                       |                      |  |
| 1910          | 2,152                       |                       | 3.1                  |  |
| 1 <b>9</b> 20 | 3,092                       |                       | 43.7                 |  |
| 1930          | 3,250                       |                       | 5.1                  |  |
| 1940          | 4,590                       |                       | 41.2                 |  |
| 1950          | 5,923                       | 486,028               | 29.0                 |  |
| 1960          | 6,681                       | 495,709 <sup>2/</sup> | 12.8                 |  |
| <b>19</b> 70  | <b>9,8</b> 86               | 4 <b>9</b> 5,730      | $48.0^{3/}$          |  |
| 1980 *        | 11,856                      | 4 <b>99,</b> 800      | 19.9                 |  |
| 1990 *        | 13,730                      | 524,800               | 15.8                 |  |
| 2000 *        | 15,436                      | 540,700               | 14.4                 |  |

Table B-3 -- Present and Projected Populations for Marshall $\frac{1}{2}$ 

\* Projected

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 $\frac{1}{2}$  From Comprehensive Land Use Plan for Marshall, dated December 1962  $\frac{2}{2}$  Data for 1962

 $\frac{3}{2}$ Due to establishment of Southwest Minnesota State College

# DEVELOPMENT AND ECONOMY

36. Marshall is the county seat of Lyon County, a part of the rich agricultural area of southwestern Minnesota and thus serves as an important regional government, trade and service center. Southwest State College at Marshall, a four-year liberal arts college, provides numerous educational opportunities for area residents and provides a resource base for stimulated research of area socioeconomic

needs. The agricultural base of the Marshall area has great dependence upon the marketing of animal products. This is quite evident with three of the major employers involved in food processing and employing over a total of 1,000 persons. Farming has undergone noticeable changes in recent years as cash crops have diminished, livestock and dairy farming have increased, and farms have become more specialized. More than 90 percent of the land area in Lyon County is in farms.

37. Early in its history, Marshall became the retail center for the surrounding farming area. The railroad and Marshall's importance as the county seat increased its possibilities as an employment center. Total employment is growing at present, as indicated in Table B-2.

| Category   | April<br>1 <b>9</b> 60 | July<br>1973 | July<br>1974 | Percent Change<br>1973 - 1974 |
|--|------------------------|--------------|--------------|-------------------------------|
| Trade  | 769                    | 1,354        | 1,485        | 9                             |
| Service  | 286                    | 276          | 243          | -11                           |
| Manufacturing  | 544                    | 1,193        | 1,399        | 17                            |
| Construction   | 109                    | 226          | 113          | -50                           |
| Transportation   | 134                    | 213          | 253          | 18                            |
| Government (includes city,<br>county, state and federal) | 414                    | 1,220        | 1,291        | 5                             |
| Finance, Insurance, Real<br>Estate and other Activitie   | s 142                  | 166          | 163          | - 1                           |
| TOTAL:   | 2,398                  | 4,648        | 4,947        | 6                             |

Table B-4 -- Comparative Employment Figures By Industry

Appendix I

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38. The income of the community is reflected both in the strength of its farm markets and its relationship to competition. The lack of nearby retail competition has helped Marshall become economically strong. The retail strength of Marshall is very good, especially to the west where there is very little competition. Median family income for Marshall area residents in 1970 was \$9,856 with a percapita income of \$2,840.

#### TRANSPORTATION

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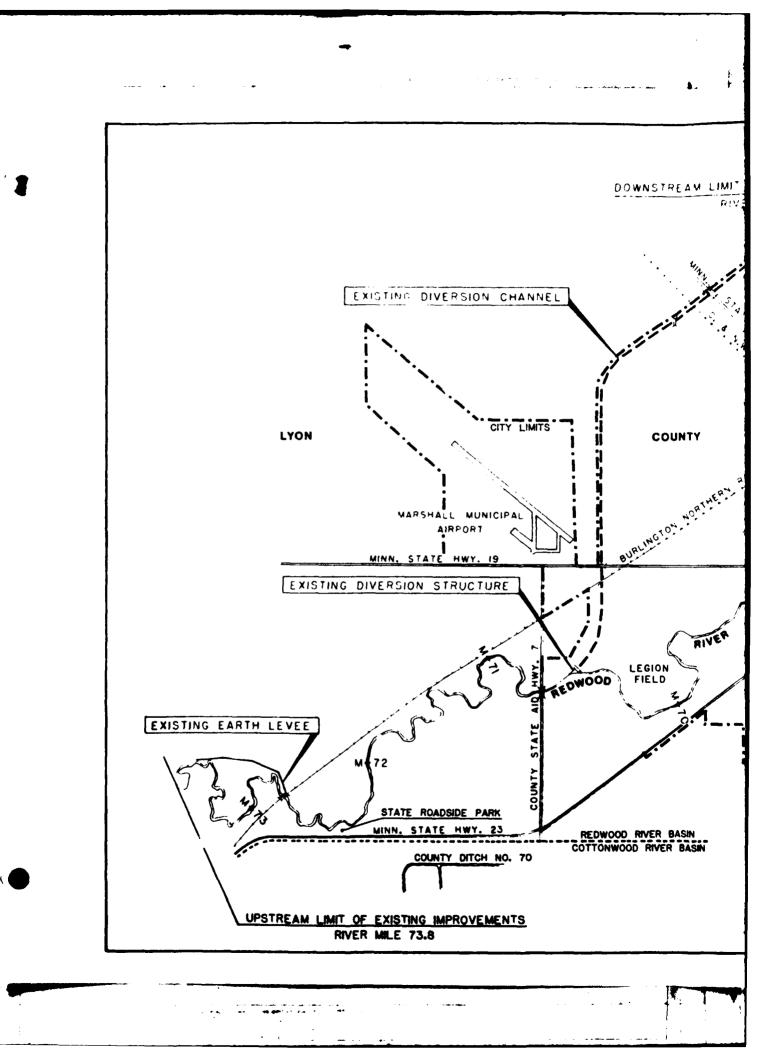
39. During the early settlement of the region, the Indian trails across the prairie provided the major means of ingress and egress from the site of Marshall. Presently there are 14 bridges across the Redwood River in Marshall and seven across the diversion channel. The major highways serving Marshall are U.S. Highway 59 and State Trunk Highways 19, 23, and 68. Interstate 29 is 63 miles west of Marshall. Rail service is provided by two companies which provide overnight service to the Twin Cities. Inter-city bus service is available. Marshall has its own airport with a charter service available. The nearest major airport is at Sioux Falls, South Dakota.

#### DESCRIPTIVE PUBLICATIONS

40. In addition to the maps of the study area, plates R-1 and B-2 of this section, available descriptive information includes aerial photography, scale 1 inch = 100 feet by the Corps of Engineers, a general highway map of Lyon County, scale 1 inch = 1 mile (5,280 feet), mapping of the City of Marshall, scale 1 inch = 500 feet, and

U.S. Geological Survey quadrangle maps, scale 1 inch = 2,000 feet and a contour interval of 10 feet. Other materials include the Comprehensive Land Use Plan for the City of Marshall, with supporting documents, an environmental inventory report made in support of this study, 1969 flood photographs in the files of the City and various local newspapers, aerial photographs taken by the Soil Conservation Service in 1967, and the flood plain information report prepared for the City by the Corps of Engineers.

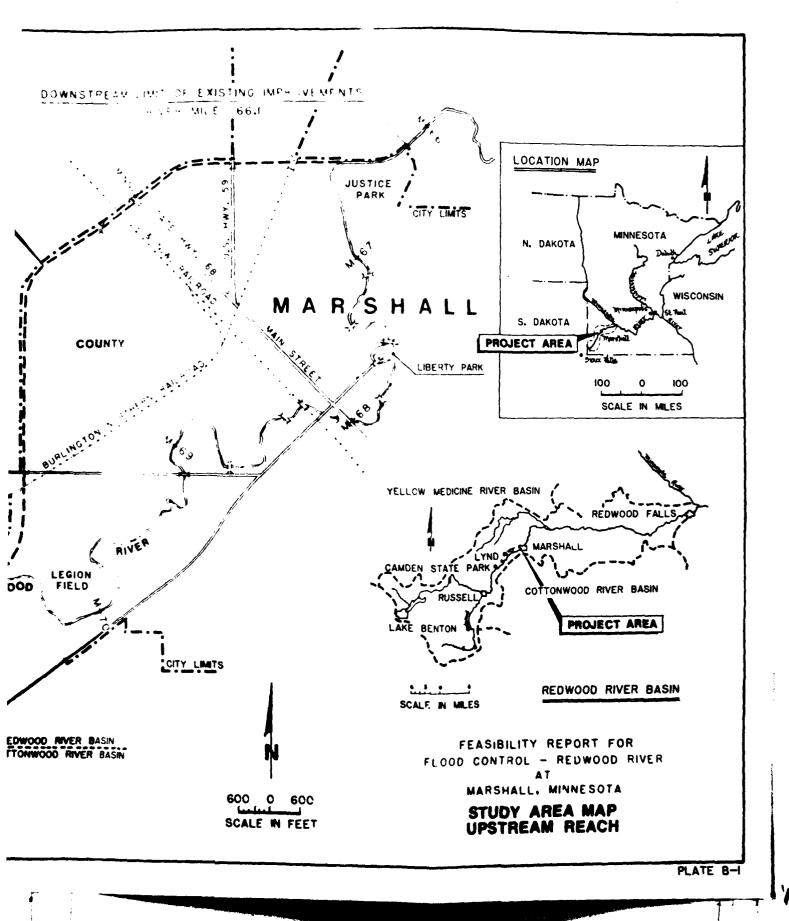
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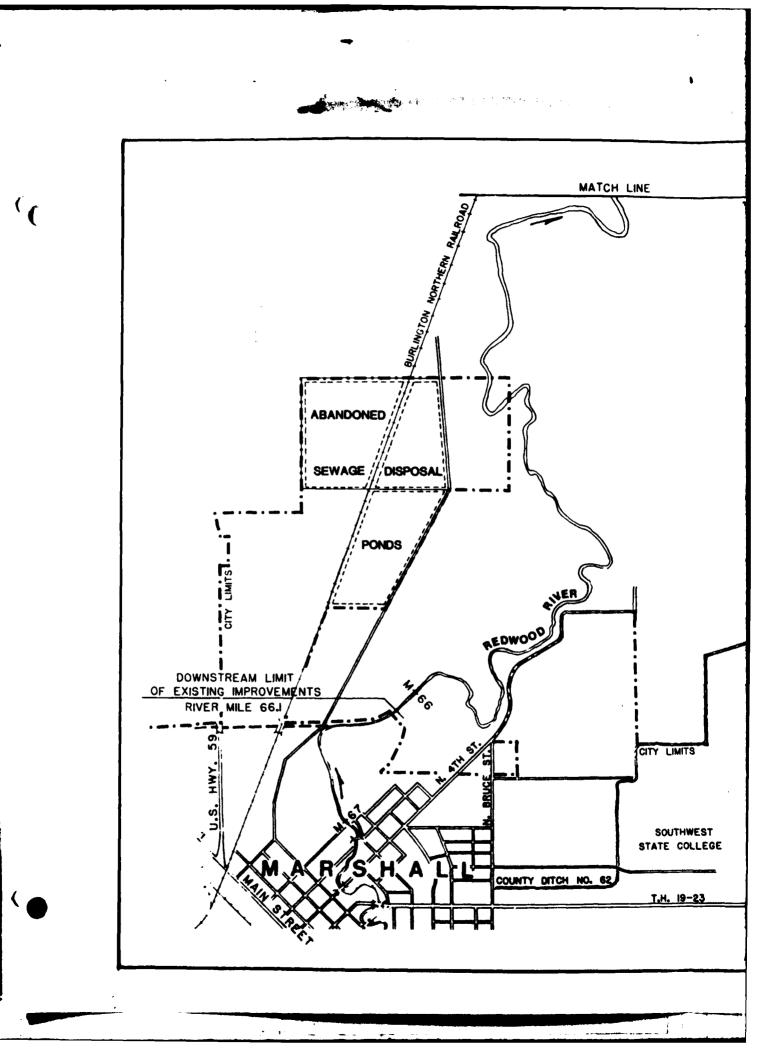


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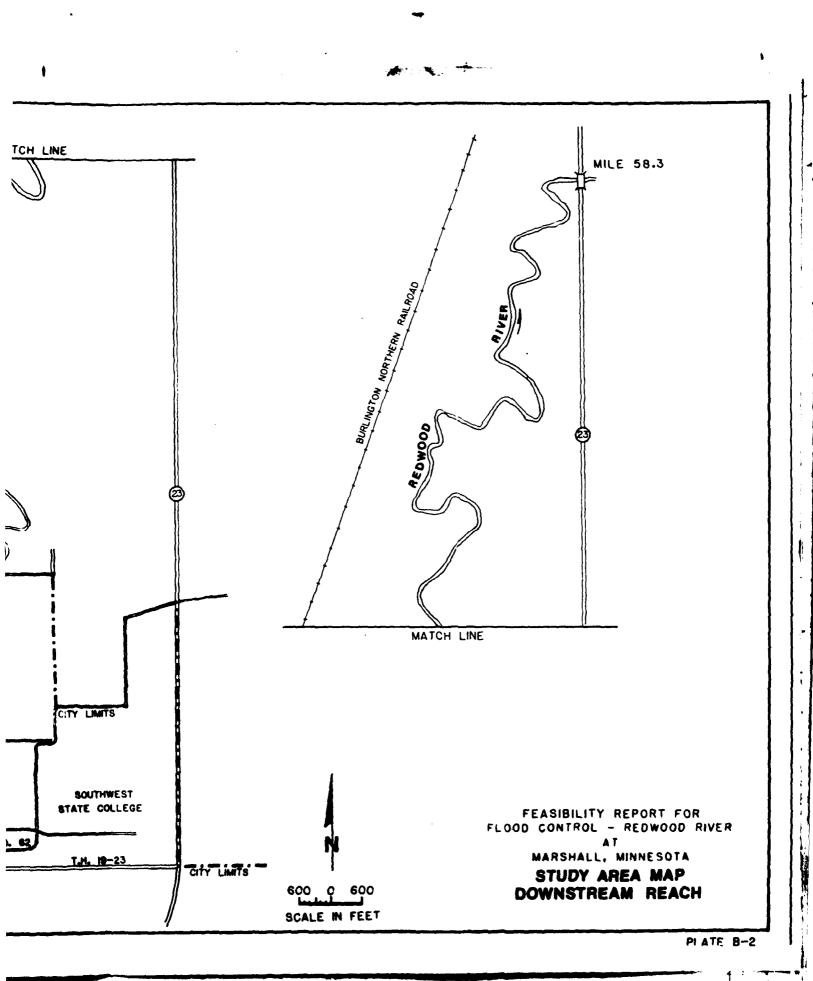








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# SECTION C

# PROBLEMS AND NEEDS

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## SEC TION C

# PROBLEMS AND NEEDS

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#### SEC TION C

# PROBLEMS AND NEEDS

1. Flooding of the Redwood River at Marshall remains the principal water resource problem in the area. This section of the technical report discusses this problem, the status of the existing Federallyconstructed flood control project, and improvements desired by the City of Marshall.

# STATUS OF EXISTING PLANS

# AND IMPROVEMENTS

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2. The City of Marshall is provided a limited amount of protection against flooding by both Federally and non-Federally constructed projects. In 1952 the City completed a 1,100-foot long cut-off on the Redwood River at about mile 67.0 (plate C-1). This cut-off reduced the channel length by about 1,000 feet and together with 1953 channel works by the Corps of Engineers provided about a one-foot reduction in flood stages in the downstream portion of the town. In 1953 the Corps of Engineers completed a channel clearing and straightening project from mile 56.3 to the downstream limit of Marshall (mile 66.8). This project provided for removal of trees and snags and construction of 900-foot long cut-off of a river loop having an original length of about a mile. The project was turned over to the City of Marshall, which has provided necessary maintenance to date.

3. The City was provided further protection by the Corps of Engineers in 1963 as a direct result of the 1957 flood experience. This project as constructed includes channel clearing and snagging on the Redwood River between river miles 70.7 and 73.08, construction of a 1,840-foot long levee on the left bank of the river at the upstream end of the project (mile 73.8), a new 2.4 mile long floodwater diversion channel between miles 66.6 to 70.5, enlargement of the river channel between the upstream diversion structure (mile 70.5) and the CSAH 7 Bridge (mile 70.7) channel enlargement and a channel cut-off between miles 66.1 and 66.6, and spoil bank dikes flanking the river channel between miles 70.5 and 70.7. Other project works include new highway and railway bridges over the diversion channel, drop structures in the diversion and natural river channels, a circulation culvert in the cut-off closure embankment, and relocation of a township road. Basic project features are shown on plate C-1. The project was designed to pass a discharge of 6,500 cfs around and through the city (1,500 cfs through natural river channel) with no significant flood damage.

4. The project was turned over the the city of Marshall for operation and maintenance in accordance with the prescribed assurances of local cooperation and an Operation Manual prepared by the St. Paul District, Corps of Engineers. This operation and maintenance has been performed satisfactorily as evidenced by periodic inspections by the District Engineer.

5. The City of Marshall currently has  $fl_{Com}$  iain management regulations in effect. The flood plain reach upstream of CSAH 7 (plate B-1) and the reach downstream of the confluence of the diversion channel and natural river channel (plate B-2) are both outside the city limits and thus subject to County flood plain management regulations for unincorporated areas.

Appendix I C-2

6. Emergency works constructed during the April 1969 flood included a levee along the left channel bank upstream of CSAH 7, levees near the college area and a levee on top of CSAH 7. Only the left bank levee upstream of CSAH 7 remains in place at this time.

# THE FLOOD PROBLEM

#### **RECENT FLOODS**

7. Marshall is subject to flooding on the Redwood River caused by rapid spring snowmelt and related runoff or summer thunderstorm activity. Recent large floods have occurred in June 1947, April 1951, April 1952, June 1957 and April 1969. The June 1957 flood was by far the most damaging, having occurred before completion of the existing project. This flood, which had a peak discharge of 6,170 cfs, covered a major part of the business and residential portions of the city and flooded wide areas of farm land on the level flood plains. Total damages including emergency flood fight costs resulting from the 1957 flood were approximately \$5,920,000 in January 1975 dollars. The next largest flood in recent years occurred in April 1969 as a result of rapid snowmelt runoff. The flood crested immediately upstream of Marshall at a peak discharge of 8,090 cfs which corresponds to an estimated frequency of occurrence of once in about 100 years, based on current flood frequency analysis. Actual flood damages incurred during this flood amounted to \$87,000 based on January 1975 price levels. Without the emergency flood fight, these damages would have increased to \$1,866,000.

### REVISED HYDROLOGIC ANALYSES

8. A coordinated restudy of hydrologic conditions in the Redwood River Basin above Marshall by the Corps of Engineers, Soil Conservation Service and the U.S. Geological Survey indicate a substantial revision in basin frequency-discharge relationships. This change is principally due to the occurrence of two major floods within a relatively short time span. As an example, the previously determined recurrence interval of 114 years for the project design flood of 6,500 cfs has been revised to a recurrence interval of about once in 59 years. Both the project document and revised frequency-discharge relationships are shown for comparison on plate H-3 of Section H.

### INADEQUATE CHANNEL CAPACITY UPSTREAM AND DOWNSTREAM OF EXISTING PROJECT

9. The existing project was designed to pass a peak flood flow of 6,500 cfs around and through the city without flooding and related damages. Of this discharge, 5,000 cfs was designed to go through the diversion and 1,500 through the natural channel. As it happened, significant overflows of the channel occurred during the 1969 flood in the vicinity of the State Wayside park (see plate C-1). At the peak of the flood, overbank flows of more than 2,500 cfs proceeded southeastward to the State Highway 23 and CSAH 7 embankments. Portions of these floodwaters crossed low points along Highway 23 near the park and then proceeded to flow southeastward into the Cottonwood River basin. An emergency levee or fill was constructed on CSAH 7 to prevent overbank flows from crossing over CSAH 7 and reentering the city at a point along the natural river downstream of the existing diversion structure. This action resulted in

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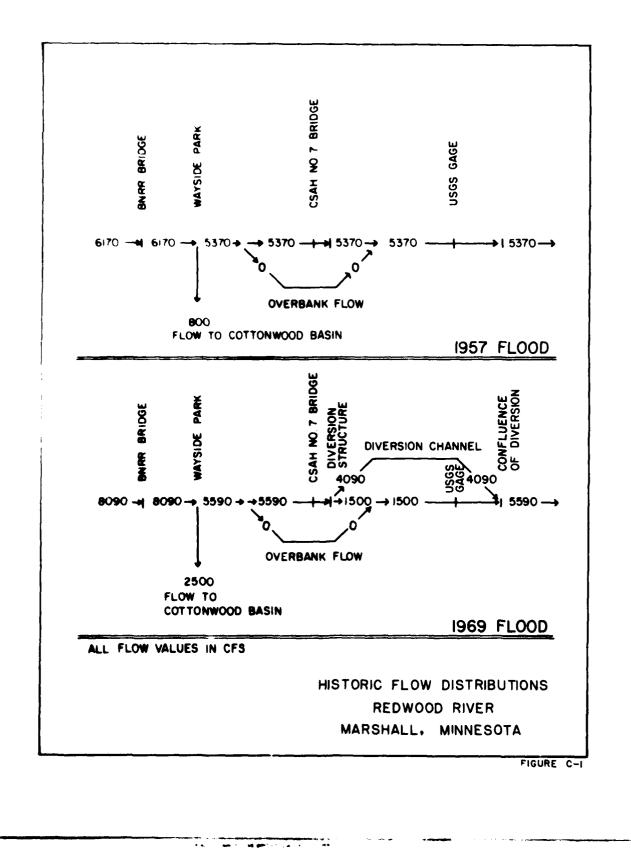
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additional flows passing over Highway 23 near its intersection with cSAH 7. Ultimately Highway 23 was breached by the city to prevent overtopping of the raised cSAH 7 and subsequent flooding of developments in Marshali. This action also increased flows into the cottenwood basin resulting in flooding and erosion damage to farms located south of Highway 23. Other farms were also affected as a result of construction of the CSAH 7 and north of Highway 23. The distribution of flood flows and attendant overflows at Marshall during the 1957 and 1969 floods is 1/4 strated on Figure C-1.

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10. Thus, from the conditions experienced during the 1969 flood, it is evident that the natural channel capacity both upstream and downstream of the existing project is inadequate. This is illustrated by the fact that, without the emergency works, damages would have been sustained at Marshall at an upstream reach flow of about 3,500 cfs over CSAH 7 (3,570 cfs corresponds to a 16 percent flood frequency).



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#### THE EXISTING FLOOD PROBLEM

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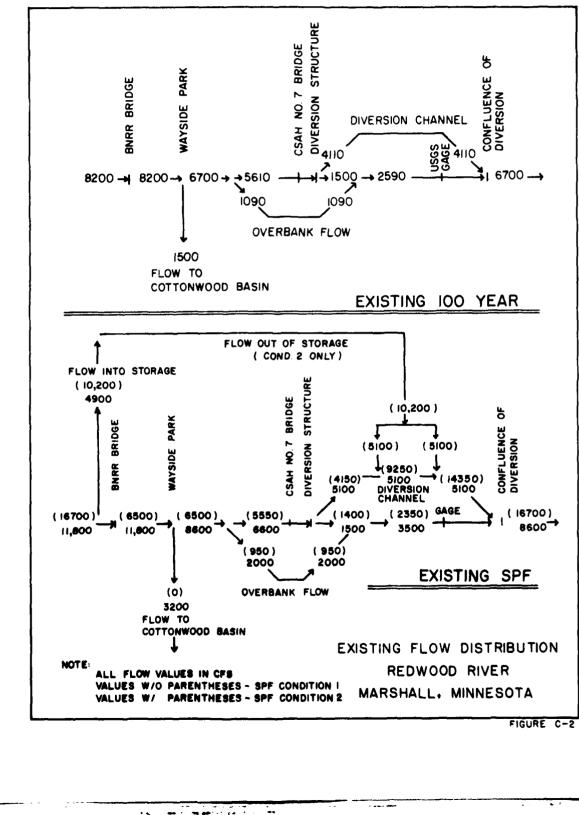
11. Although designed for a flow of 5,000 cfs, the existing floodwater diversion channel has sufficient capacity to pass the standard project flood discharge. Similarly, the upstream diversion structure (plate C-1) would provide adequate control of flows entering the natural channel at Redwood River flood flows approaching the standard project flood discharge. However, existing flood problems are concentrated in both the upstream and downstream reaches as described in the following paragraphs. A detailed discussion of the standard project flood is given in section H.

12. The principal reason for flood problems in the upstream reach (miles 66.3 - 73.8) is that overflows resulting from the inadequate capacity of the natural river channel do not reach the existing diversion channel and without emergency measures would cause overland flooding of Marshall. Channel capacity is limited by the extensive debris and vegetative growth in the channel, inadequate channel cross-section or flow area, and numerous sharp meanders. Buildup of ice in the natural channel is considered to result in increased flood stages at relatively low flows only. Of the peak 1969 flood discharge of 8,090 cfs, only 5,590 cfs reached the upstream limits of the existing project. The remaining 2,500 cfs overflowed the right bank at the state wayside park and subsequently entered the Cottonwood River basin. Overbank flow commences in the vicinity of the wayside park at a flow of about 2,500 cfs. At the original project design discharge of 6,500 cfs, most of the land area upstream of CSAH 7 would be flooded. For the revised 100-year discharge of 8,200 cfs, floodwaters commencing at a river flow of about 3,500 cfs would cross over CSAH 7 and enter the western portions of the city before re-entering the natural river channel further downstream. Beginning at the approximate 6,500 cfs discharge level, some of the

overflows would cross over State Highway 23 and flow into the Cottonwood River basin via flow over farmland before entering County Ditch No. 70, the location of which is also shown on plate C-1.

13. No flows entering the County ditch 70 would re-cross highway 23 east of CSAH 7 and re-enter Marshall at the 100-year flood level. At the SPF level, the ditch flows could cross northward through Highway via culverts located just east of the intersection with CSAH 7. These floodwaters would innundate low areas east of CSAH 7 and north of Highway 23. The temporary retention of floodwaters over the area west of CSAH 7 during the 1969 flood adversely affected one farm operation north of Highway 23. The subsequent breaching of State Highway 23 and sudden release of retained water adversely affected two farm properties south of Highway 23.

14. Similarly the downstream channel reach does not have sufficient capacity to pass even the original design flow of 6,500 cfs. This condition was evidenced during the 1969 flood when, with a peak downstream discharge of 5,590 cfs (8,090 cfs - 2,500 cfs), extensive emergency diking was needed to prevent damages to Southwest State College facilities and other developments. Thus, it is quite obvious that without emergency protective measures, significant damages would occur with the revised 100-year discharge of 6,700 cfs (8,200 - 1,500) at mile 66.1. (Approximately 1,500 cfs would leave the Redwood River basin at the Highway 23 wayside park and pass into the Cottonwood River basin). The distribution of flood flows at the existing 100-year (1% chance of occurrence) and standard project flood levels is illustrated on Figure C-2.



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15. Based on a review of the existing project's performance during the 1969 flood, it is obvious that the project cannot function as intended without additional improvements along both the upstream and downstream reaches at Marshall. As previously discussed, these improvements are needed to pass the design floodwaters both into and away from the diversion project without causing damaging overbank flows.

16. The city of Marshall has indicated that in view of the increasing interest in cross-country skiing, a growing need for a recreational trail system and other facilities in and adjacent to the city exists. A questionnaire sent to area residents by the City Parks and Recreation Department reveals that recreation trail needs rank near the top in terms of the residents' own priorities.

17. Woodlands of any type are in relatively short supply in the Marshall area. The only remaining contiguous tract is located along the river corridor upstream of County Highway 7. These woodlands provide valuable habitat, cover, and food supply to small mammals and song bird populations. In most areas, these woodlands provide an attractive background to the residences and wayside park located along the river. Reduction in the extent of these woodlands or any other adverse effects should be minimized.

18. Productive agricultural lands are located on the floodplain both upstream and downstream of the City of Marshall. As agricultural activity contributes significantly to the economic base, many are concerned about the continuing loss of valuable cropland to expanding urbanization. All of the immediately adjacent cropland has been zoned for single or multi-family residential development. Consideration should be given to minimizing adverse effects to these croplands commensurate with the economic development needs of the community.

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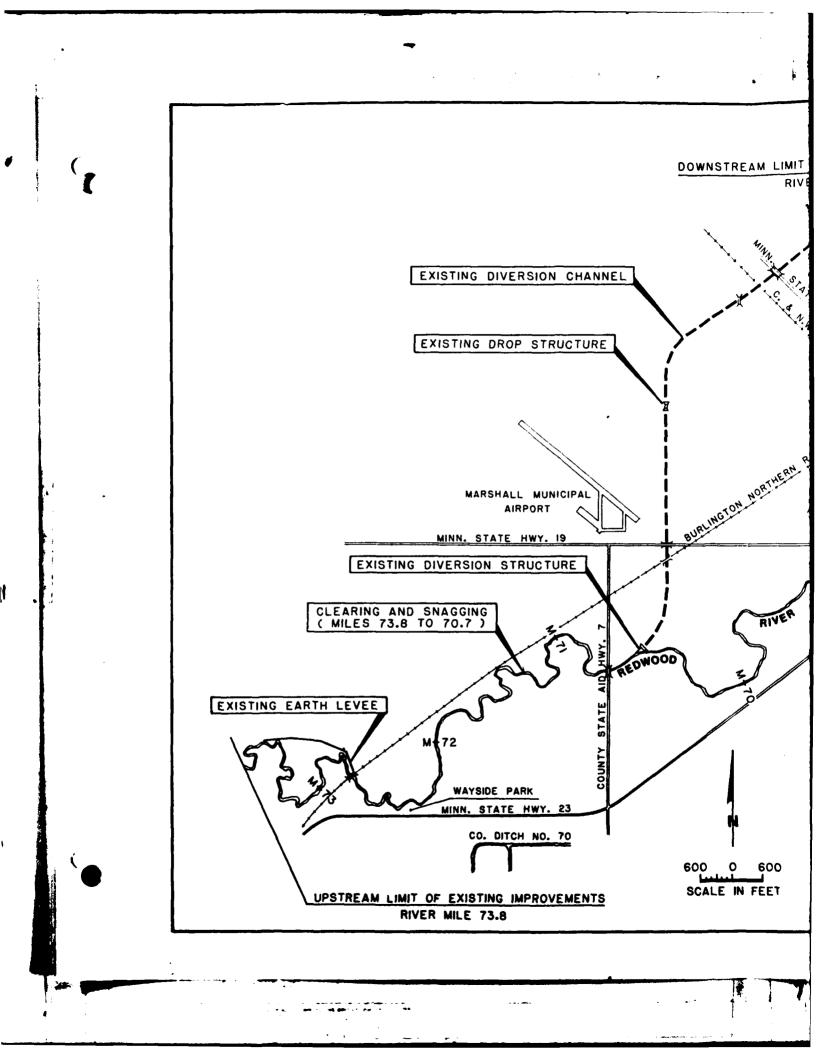
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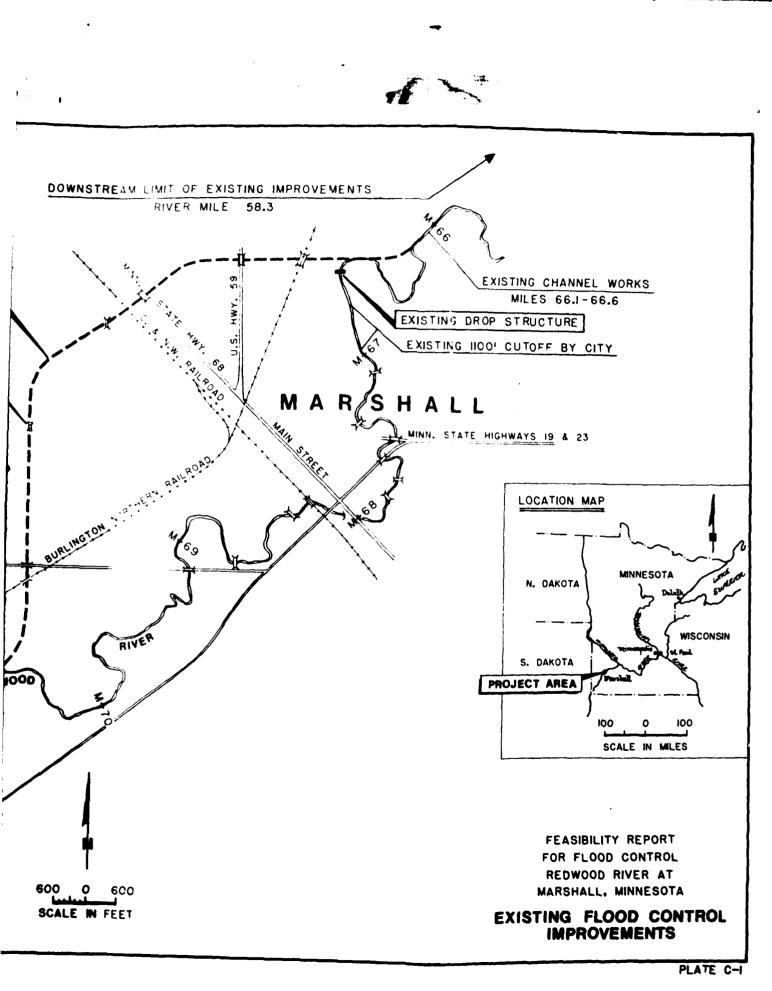
### IMPROVEMENTS DESIRED

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19. The city of Marshall incurred substantial financial losses during the April 1969 flood as a result of direct property damage, emergency floodfight activities, and court awarded damages to adversely affected farmers. In view of these losses and the potential for similar or greater recurring losses, the Lyon County Board of Commissioners requested by formal resolution adopted 6 June 1972 that the Corps of Engineers review the operation of the existing project and make modifications as necessary to insure that the project will operate at least as originally designed. By a resolution of 3 July 1972, and other written and verbal communications, the city of Marshall has also requested "...that a study be made to determine what improvements can be made to provide for additional protection and efficiency of the Redwood River Diversion Channel Project...". A copy of this resolution is contained Appendix II, Pertinent Correspondence.

20. A letter from the City requests a study of the advisability of a trail system, improvements to a softball complex on the existing diversion channel right-of-way, a riverbank improvement program at three locations to improve aesthetics and public safety, picniking facilites, and the development of quiet and nature education areas.





# SECTION D

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## FORMULATING A PLAN

### SECTION D

### FORMULATING A PLAN

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#### SECTION D

### FORMULATING A PLAN

1. The objective of the formulation portion of this study is to review the operation of the existing flood control project at Marshall with the intent of identifying solutions that will meet the study objectives identified early in the study. The following planning objectives have been identified in coordination with local and other interests:

Reduce damages from flooding along the Redwood River at
 Marshall during the period 1980 to 2030.

• Contribute to water and winter recreation needs for Marshall during the period 1980 to 2030.

• Contribute to the riverine woodland and wetland areas within the City of Marshall for ecological, diversity, and aesthetic purposes during the period 1980 to 2030.

## FORMULATION AND EVALUATION CRITERIA

2. In developing a plan to insure effective operation of the existing project and to reduce flood damages in the recently developed downstream river reach not protected by the existing project, standards and procedures which have been set forth in various flood control acts and policies and related regulations established by the Corps of Engineers have been followed. All alternatives were evaluated in accordance with the following specified criteria.

(i)

### TECHNICAL CRITERIA

- The degree of protection afforded by any proposed plan will
   be at least equivalent to the degree of protection intended for
   the original project, or the maximum practical level of protection.
   The degree of protection must also be in consonance with established
   State flood plain management regulations and the desires of
   local interests.
- o All flood barriers will provide adequate freeboard over the adopted flood level. Also appropriate freeboard will be provided between the design water surface and low member of any channel crossings. Generally, three feet of freeboard is considered appropriate, however, greater or lesser freeboard may be required in some areas depending upon risk and design uncertainties.
- o The plan must insure completeness of the existing project and insure effective operations as designed without additional future improvements.
- o The plan must be technically feasible to implement.

### ECONOMIC CRITERIA

o The selected plan must represent the most cost-effective solution and be economically feasible to implement with projected annual benefits exceeding projected annual costs. However, a

more costly plan can be recommended if appropriate gains in environmental quality and social well-being can be shown provided that the overall plan is economically feasible with benefits at least equal to the related costs.

 Annaul costs and benefits are based on a 50-year economic life, an interest rate of 6-7/8 percent and price levels and conditions existing in October 1977.

### ENVIRONMENTAL AND OTHER CRITERIA

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- The public health, safety, well-being and quality of life of affected residents are the principal considerations in the development of a project.
- The loss of area environment and aesthetic values will be minimized to the extent practicable.
- o Public acceptability of proposed improvements and the projectsponsor's ability and willingness to meet local cooperation requirements are essential considerations.
- o Specific social well-being factors considered in this study included: possible loss of life and possible hazards to the health and safety of affected area residents; preservation of aesthetic, cultural, and historic values in the area; leisure time enjoyment; injurious displacement of people and businesses; and the disruption of desirable community and regional growth.

### POSSIBLE SOLUTIONS

3. Solutions considered in this study pertain strictly to provision of additional measures required to insure effective operation of the existing project and to providing flood protection to downstream development not protected by the existing project. Area flood problems principally originate in the upstream reach where modest new development has occurred. Possible solutions considered include both non-structural measures and structural solutions such as reservoir storage, flood barriers, channels or combinations of these measures. In addition to these solutions, the consequences of doing nothing at all about recurring flood problems in Marshall is considered as a base from which to measure the impacts of positive alternative solutions.

### ALTERNATIVE PLANS ANALYZED

4. The following discussion is a detailed description of the alternative plans considered. Since the "no-public action" alternative, non-structural alternatives and reservoir storage alternatives apply to the entire Marshall study area, they are discussed first. A discussion of local structural alternatives (flood barriers and channel improvements) by respective reach, upstream and downstream, then follows. Non-structural alternatives considered include no public action, permanent evacuation, and combined partial evacuation and flood proofing. Plan costs and other impacts are shown on table D-1 found later in this section.

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### PLAN 1 - NO PUBLIC ACTION

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5. This alternative represents the "without" project or base conditions and would provide for continuation of the existing situation at Marshall without any further local, State or Federal action to provide additional measures to permit effective operation of the existing project. The base economic, social, and environmental setting of the study area is described in detail in section B of this report. The existing situation relating to flooding at Marshall is represented by warnings by the National Weather Service of impending Redwood River flood occurrences, related emergency flood fight and supporting disaster relief activities by the City and other government agencies, the required purchase of flood insurance to obtain federally-supported financing for building in flood-prone areas, and flood plain management regulations currently being developed by the City of Marshall.

6. Urban development continues to expand on the agricultural flood plain adjacent to Marshall, particularly along the downstream reach, where the development consists of municipal maintenance buildings, residential and limited commercial development, and the Southwest State College. Development in the upstream flood plain reach includes residential development along the right immediately downstream of CSAH 7, a motel, a few scattered rural residences and farmsteads, and a wayside park.

7. Under present conditions, the National Weather Service at Kansas City, Missouri with supporting elements at Minneapolis provides warning of potentially damaging flood occurrences on the Redwood River at Marshall. If the warnings indicate that flooding is imminent, emergency action will be taken by the City, and if requested by local officials, the Corps of Engineers, and other agencies. Such emergency

action may include the provision of temporary flood barriers, temporary interior drainage pumping, and flood proofing of various structures as needed.

Supporting disaster relief services provided during the April 1969 flood included temporary food and housing, evacuation of threatened areas, and other supporting services. Follow-up disaster relief efforts including removal of temporary works, replacement or repair of damaged public facilities, and post-flood cleanup are administered by the Federal Disaster Assistance Administration with the support of other Federal and State agencies. Reliance on emergency protective measures at Marshall is impractical in view of the limited time available to construct temporary flood barriers, possible inclement weather conditions, and the availability of funds.

8. Flood insurance is presently required for Federal financial assistance to any new developments constructed on the 100-year flood plain. The city became enrolled in the regular phase of the flood insurance program on 30 September 1977. Thus flood insurance is available for existing structures under subsidized rates and for new (post 30 Setember 1977) structures based on actuarial rates. Determination of flood plain property eligible for flood insurance is presently based on flooded area maps furnished to the city and county by the U.S. Department of Housing and Urban Development. Total maximum coverage obtainable at subsidized rates for existing single family residential and other residential buildings is \$35,000 and \$100,000 respectively. Non-residential structures are covered under regular rates up to \$100,000. On a regional basis, a flood insurance program would at least partially compensate individual flood losses by spreading premium costs over a wider area. However, such a program would not reduce flood damages and, at Marshall, would result in remaining average annual flood damages of over \$75,000 to unprotected downstream developments alone. It would also do little to reduce the anxiety, human misery, and community disruption currently experienced during major flood periods. Appendix I

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9. The City of Marshall presently has a flood plain management program in effect. These flood plain management regulations have been developed on the basis of a recently completed flood plain information study by the Corps of Engineers. The flood plain information study report established the 100year frequency flood outline and average depths of flooding at selected locations. A program limits the location, type and extent of new development on the 100-year flood plain and limits substantial expansions to existing flood plain developments.

10. Enforcement of flood plain regulations would do little to reduce flood damages to existing development but would be very effective in reducing future growth of flood damages due to curtailment of new flood plain growth. Although flood plain regulations alone would not substantially reduce potential flood damage in the developed flood plain, it would serve as an effective supplement to other structural or non-structural measures to arrive at a total plan of protection.

11. With the no-public action alternative, a large portion, or nearly 300 acres, of the highly developed central part of the city and developments adjacent to the city would remain vulnerable to extensive flood damages during major flood occurrences without major emergency flood fighting efforts. Planned and temporarily halted developments in fringe flood plain areas would not be accomplished until measures were provided to permit the operation of the existing project as originally designed. No further public action would perpetuate the continued burden on the city in terms of human suffering, hazards to public health and safety, and the required inefficient commitment of local financial and manpower resources. This course of action would do



little to permanently reduce flood damages and is clearly unacceptable to the city. For these reasons, this alternative was not considered further except as the base condition against which the other alternatives are compared. However, the continuation of flood warning services and the expansion of local flood plain management and flood insurance programs will be considered as integral parts of other structural or non-structural plans developed.

#### PLAN 2 - PERMANENT EVACUATION

12. Permanent evacuation would solve the residual flood problem at Marshall but would require the relocation of most developments in the city including over 1100 residences, over 200 businesses and several churches and schools. The displacement of these upstream reach developments in addition to being totally uneconomical is considered impractical and wholly unacceptable to local interests and thus, is not considered further.

13. Permanent evacuation of the recently developed 100-year downstream flood plain (see table D-1) was not considered as an alternative to the existing project, but rather as a supplement to it. Total evacuation along the downstream study reach would involve the removal of an estimated 8 new residences, a trailer court with approximately 32 mobile homes, at least 3 apartment buildings at 33 units each, 4 apartments with 8 basement level apartments in each, and seven large buildings on the college campus. Evacuated residential areas would be converted to and managed as flood-free open space, park, or recreational uses. Evacuated campus areas could be converted to relatively damage-free outdoor recreation facilities. Evacwation of the college buildings, residences, and apartments could

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be accomplished with available equipment but at great economic, social and environmental costs.

14. Movement of the large apartment complexes and college buildings would be physically impossible, leaving razing the buildings the only alternative. Immediately adjacent undeveloped and floodfree sites for the college structures do exist.

However, the removal and replacement of any of the major structures from the relatively new State College campus would place a severe economic, educational, and social impact on the community, region, and the State.

15. Although total evacuation of the presently unprotected development in the downstream reach would reduce area flood damages, the economic costs, and adverse short and long term social and environmental impacts make this plan unacceptable to all concerned interests. Thus, total evacuation of unprotected residential and public property is not considered further either in the total study reach or in the downstream reach alone.

#### PLAN 3 - PARTIAL EVACUATION AND FLOOD PROOFING

16. Instead of total evacuation of the flood plain, consideration was given to partial evacuation of selected downstream reach flood-prone structures together with flood proofing measures to remaining residential, commercial, and public structures in both reaches. Evacuated areas would be managed in accordance with local flood plain management regulations.

17. Partial evacuation measures would involve the relocation of all residential structures subject to flood depths greater than 3 feet and any structure not considered suitable for flood proofing. With this alternative, 30 residences, 5 commercial structures, and the downstream reach trailer court would be relocated out of the 100year flood plain

18. Flood proofing measures would include structural changes and other adjustments to structures, and landscaping measures. Structural changes would include sealing of doorways, windows, and other openings, sealing and bracing of basements, and in some cases, provision of flood drain standpipes and landscaping around raised structures to help offset adverse aesthetic impacts. Approximatei the eight downscream reach apartment buildings ly 65 residential uni have flood levels about + feet below ground level. Sealing of ground level window openings of these occupied units could probably be accomplished but only with the remaining threat of extensive damage and possible health and safety hazards in the event of failure of any one closure. Seepage into these units would likely be a major problem during major flood periods. Only the college buildings, commercial structures, and residential structures subject to less than 3 feet of innundation appear to lend themselves to flood proofing techniques.

19. Seven college buildings, 31 commercial structures, and 280 residences were evaluated for possible flood proofing measures. Flood proofing measures for the college buildings would include the construction of bulk heads and gate valves in underground equipment tunnels and placement of gate valves in drainage pipes running between and from the buildings. Assuming effective valve closures, this plan would prevent water damage to the buildings but could still result in extensive electrical failures due to possible electrical short circuiting of cables, switches and connections in the cable ways.

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20. Evacuation of the residences, commercial structures, and trailer homes is estimated to cost about \$4,200,000 including appropriate allowances for relocation expenses. Flood proofing of the remaining residences, apartments, commercial buildings, and college buildings would cost another \$8,752,000 as shown on table D-1. Total Federal first costs at an assumed 80 percent cost share would be \$10,361,600 as shown on table D-1. Minnesota State flood proofing regulations indicate that flood proofing of habitable basement space is usually not permitted. This plan would result in the near elimination of potential flood damages, but only at excessive economic and social well-being costs. Environmental losses would probably not be major as the required new development sites would very likely be on presently tilled cropland outside of Marshall.

21. The removal and relocation of the much needed residential housing from areas near the college and presently zoned and developed for this activity to productive agricultural areas would have a decided adverse effect on established community patterns, educational opportunities and general cohesiveness of the area. Present occupants, most of whom are in some way associated with the school, depend on this nearby housing. Local interests object to this considered gross rearrangement of area residential housing and the related effects, and indicate a preference for a more positive method of flood protection for the college campus. Since this alternative lacks local support in all aspects, it is not considered further.

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### PLAN 4 - UPSTREAM RESERVOIR STORAGE

22. Reservoir storage was investigated as a possible means of flood damage reduction at Marshall during the earlier feasibility scope studies made in support of the existing project. During those studies, only one site could be identified as having sufficient storage capacity to reduce flooding at Marshall, but the site would require floodwater storage in Camden State Park located about eight miles upstream of Marshall. Increased channel flow capatity via the existing diversion channel in combination with levees in the upstream reach would increase the effectiveness of upstream reservoir storage but not enough to eliminate the threat of longer floods nor make it feasible justifying the reservoir economically. In addition, a reservoir in the park would clearly have substantial and unacceptable adverse environmental effects on natural ecosystems as provided in the park and presently in relatively short supply in this agricultural region (see table D-1).

23. A system of small reservoirs on headwater tributary streams presently under consideration by the U.S. Soil Conservation Service to solve localized agricultural flooding would have too little storage volume to have any appreciable effect at Marshall. Although a system of three small reservoirs would influence control over 58% of the total drainage area, their combined storage capacity would only control 0.4 inches of run-off. This represents 9% of the average annual run-off, 6% of the 100-year run-off, and 3% of the SPF run-off. Thus, for these reasons, upstream reservoir storage via a single large reservoir or a system of small tributary reservoirs is not considered further in this analysis as a viable solution to Marshall's flood problems.

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### FLOOD BARRIERS AND CHANNEL WORKS - UPSTREAM REACH

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24. Both flood barriers and channel works were considered separately as additional measures required to permit efficient operation of the existing project. Early in the supporting hydraulic studies, it became evident that, because of inadequate channel flow area and channel obstructions, neither levees nor channel works alone would achieve the desired flood damage reduction. Thus, all upstream alternatives include a combination of levee and channel works and are essentially variations in the location and extent of such works. Since Redwood River overflows into the adjoining Cottonwood River basin occurred under natural conditions prior to the construction of the existing project and presently occur with the project, all considered levee-channel alternatives in the upstream reach provide for the continuation of such overflows in some manner.

#### PLAN 5U - COMBINED LEVEE - CHANNEL WORKS

25. This plan would provide protection against the 100-year frequency flood with the construction of levees, channel widening measures, and clearing and snagging along 2 miles of channel between the existing diversion structure (mile 70.2) and the Burlington Northern Railroad (BNRR) bridge at Mile 72.6 (plate D-1). Approximately 2,260 feet of levee ranging in height from 3 to 6 feet would be required along the left or north bank commencing at

the CSAH 7 bridge and extending to the BN railroad embankment. Along the remainder of the left bank reach, the railroad embankment would serve as a barrier to prevent floods from escaping to the north and flooding city developments further downstream. Flap gates would be installed on four culverts passing through the railroad embankment. About 6,300 lineal feet of levee from 3 to 12 feet high would be required on the right or south bank as shown on Plate D-1. The existing right and left bank levees between the existing diversion structure and the CSAH 7 bridge would be raised an average of one and six feet, respectively. Clearing and snagging would be accomplished at scattered locations along the entire reach to remove fallen trees, debris, and other obstructions to flow in the channel.

26. This alternative would also provide for an overflow weir with attendant outlet channel that would be located in the vicinity of the wayside park (mile 72.1). The proposed 540-foot long weir would divert up to approximately 50 percent of overflows in excess of the present project design discharge of 6,500 cfs, or a maximum of about 850 cfs at the 100-year Redwood River flood flow of 8,200 cfs. Overflows would be conveyed by a natural ditch on the east side of the park and would pass through proposed multiple culverts are required to prevent overtopping of State Highway 23 and possible overland flooding of Marshall.

27. This plan would also provide for riprap bank protection measures, minor interior drainage measures, relocation of one house and utility relocations. Plan effects and estimated total first costs of about \$1.7 million are shown on table D-1. The plan would accomplish the desired flood damage reduction generally in accordance with the desires of local interests. Thus, it is carried forward for detailed impact analysis and possible combination with downstream reach improvements to develop a total plan for the Marshall area.

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28. A minor modification to this plan (5U-Mod. 1) was suggested by local interests. This modification would permit flood-free use of a 10-acre parcel of land within a large river meander (miles 70.45 to 70.88) with realignment of the levee as shown on plate D-1. Local interests would be responsible for additional costs of \$160,000 over the most cost effective alignment (plan 5U). This plan modification is also carried forward for detailed impact and tradeoff analysis. Estimated total first costs with this modification would be about \$1,860,000.

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29. Another possible modification to this plan (5U-Mod. 2) would provide the same principal features as plan 5U but would include a 600-foot long channel cut-off across the river meander between river miles 70.75 and 70.86, as shown on plate D-1. This cut-off channel would reduce the required channel works and riprap bank protection around the river bend for a net savings of about \$50,000 excluding financial losses to the property owner. Utilization of the unprotected 10-acre area slated for industrial development in the future would be adversely affected as access would be hindered by back water in the cut-off channel every one to two years. Local interests do not favor this modification. Therefore, it is dropped from further consideration.

30. An additional modification of this plan (5U-Mod. 3) would include both the 600-foot long cut-off and a 700-foot long channel cut-off between river miles 71.2 and 71.7 as shown on plate D-1. This cut-off would further reduce the length of the natural channel by 2,800 feet and would pass flood flows in excess of 3,600 cfs (the capacity of the natural channel at the upstream end of the cutoff). This alternative would result in a slight reduction in levee height from those levees considered in plan 5U but at an additional total first cost of about \$250,000. Since the additional benefits gained are clearly not commensurate with added first costs, this modification was not considered further.

31. A fourth modification of this plan (SU-Mod. 4 or E011988 Plan) would eliminate the proposed right bank leyee works between the gabion control structure and CSAH #7. In addition, State Trunk Highway 23 and CSAH 7 would be raised to a 100-year design elevation of 1183.0 feet including 3 feet of freeboard (1185.0 SPF). Flood flows in this upstream reach would then be contained between the river, CSAH 7, Highway 23, and right bank levees in the vicinity of the overflow and gabion control structures forming a flood water storage reservoir as shown on plate D-1. Analysis, however, of this triangular area shows little storage capacity and that flood flows would flow back into the river channel (200 feet upstream of CSAH 7) as quickly as they leave the channel (downstream of the gabion control structure). This modification was investigated for both the 100-year and SPF design levels. Additional discussion of this alternative is given in Section J of this appendix.

32. At the 100-year design level, this modification would reduce channel modification costs by about \$491,000 (66 percent) and total Federal first costs by \$451,000 or 23 percent. However, approximately 127 acres of productive farm land and vacant land would have to be either acquired in fee or flood easements paid. As acquisition of these lands would appear the most probably course of action based on discussions with local interests, non-Federal first costs would increase by about \$460,000. Additional raising of the roadways together with a new CSAH 7 bridge to achieve a Standard Project Flood level of protection would further increase total Federal and Non-Federal First Costs by \$745,000 and \$153,000 respectively. Since this modification would be more costly at either the 100-year or SPF flood levels than the considered levee plan at no additional benefit it was not considered further. Substituting levess (Plate D-1) in lieu of the considered road raises would significantly reduce the increase in plan first costs as discussed in Section J.

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33. Two alternatives were considered to the proposed overflow structure along the right channel bank at the wayside park. The first alternative would involve lowering of State Highway 23 in the vicinity of the wayside park to permit unimpeded Redwood River overflows into the Cottonwood River basin. With the lowered highway, maintenance of required river stages at the park to assure passage of river overflows would require limited channel improvements downstream of the park. Conversely, the limited channel widening measures would result in expected severe erosion problems and possible damage to required river bank levees without extensive and costly riprap. In view of this effect, the frequency and duration of flooding of the highway, and potentially increased damages from higher overflows (1,250 cfs vs. 850 cfs with plan 5U) to farm property south of the highway, this modification was not considered further.

34. The second overflow alternative would involve using the existing westbound Highway 23 embankment as the overflow weir, together with raising of a driveway east of the park to confine overflows to the park area. This plan, together with downstream channel widening measures would actually result in lesser overflows into the Cottonwood basin than under plan 5U and corresponding increased downstream discharges through Marshall. Any future changed channel conditions downstream of the park or related backwater stage fluctuations at the park would make control of overflows over the highway extremely difficult. In view of these problems, the potential damages to the highway itself, and traffic disruptions during major floods, this alternate overflow concept was also dropped from further consideration.

#### PLAN 6U - FLOODWATER DIVERSION CHANNEL

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35. In response to suggestions by city officials, consideration was also given to a floodwater diversion channel between river miles 70.4 and 72.5 as shown on plate D-1. This channel would be about 4,200 feet long, 18 feet deep, have a top width of about 200 feet and

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would pass a flow of 4,850 cfs, which in combination with the 2,500 cfs capacity of the natural channel would be capable of safely passing the 100-year flood flow of 7,350 cfs. A combination sheetpile diversion and drop structure would be located at the upstream Another drop structure, about 4 feet high, would end. be required in the diversion channel to reduce erosive velocities. Other required improvements would include realigning and widening of the natural channel between river miles 70.2 and 70.4, riprap bank protection at critical erosion areas, clearing and snagging of approximately 1.8 miles of river channel, 1,300 feet of levee about 5 feet high on the left bank and 4,800 feet about 2 feet high on the right bank. These levees would be along the diversion channel cut-off and would not negate the need for levees along the natural channel. Levee heights along the natural channel with this plan would be reduced an average of 3 feet from those given in plan 50. This plan would also require relocation of one house, a house trailer, five utility poles, and would require a total of 35.3 acres of land, 7 acres of which would be forested. Estimated total plan first cests of \$3,418,500 and significant plan impacts are displayed on table D-1. This plan would accomplish the same result as other levee-channel alternatives in the upstream reach but at substantially higher economic and environmental costs. However, it is considered further for detailed impact and trade-off analysis at the request of local interests.

36. A considered modification to plan 6U (6U-Mod.1) would include an increased diversion channel capacity of 5,850 cfs with a slight increase in channel depth and width. This design would reduce the right bank levee along the natural channel by about 800 feet with an additional reduction in levee height of about 0.5 feet. As this modification would result in only minor added flood damage reduction benefits at moderately higher economic and environmental costs, it was not considered further.

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### FLOOD BARRIERS AND CHANNEL WORKS - DOWNSTREAM REACH

37. All downstream reach structural alternatives were formulated on the basis of their capability to permit operation of the existing project to at least a 100-year degree of protection and to provide at least a similar level protection to unprotected flood plain development. Alternatives considered included channel works, levees, combined levee-channel works, and combined levee-highway works as discussed in the following paragraphs. An itemized breakdown of plan first costs and other impacts is also shown on table D-1.

#### PLAN 7D - CHANNEL WORKS

38. Considered channel improvements as shown on plate D-2 to reduce downstream reach flood stages would include widening of the river channel bottom to a minimum of 35 feet by excavation of the right bank only between river miles 64.6 and 65.5 and 65.9 to 66.3. This plan would also include excavation of a channel cutoff to eliminate a sharp river bend between river miles 65.2 and 65.9 This 1,300-foot long cut-off would have a 35-foot bottom width, 1 on 3 side slopes, and an approximately 100-foot top width. Clearing and snagging would be accomplished over the river reach between the State Highway 23 bridge (mile 58.3) and river mile 66.3 to remove all fallen trees, stumps, and debris from the river channel. Riprap slope protection would be placed on the outside of sharp channel bends between river miles 65.0 to 65.1 and 65.4 to 65.6 to prevent erosion of channel banks and possible damage to County Road 67 and a residence. Total plan first costs would be \$303,000 as shown on Table D-1.

39. Hydraulic and economic studies indicate that these channel works alone would provide at most an 18 percent reduction in flood

damages to downstream reach development. These improvements would result in a moderate loss of tree, brush and other bank cover, and would result in temporary increases in stream turbidity. In view of the very minor flood damage reduction benefits (0.6 benefit-cost ratio) and possible adverse environmental effects, channel improvements will not be considered further except in combination with downstream levee works.

### PLAN 8D - HIGHWAY ALIGNMENT LEVEE

40. This alternative would include a 7,670-foot long levee extending from high ground at 5th Street and Hudson Avenue (see plate D-2) eastward to high ground near the State Highway 23 embankment and contiguous with a proposed Federal-aid highway (FAS6072) alignment presently under joint consideration by the City and County. A levee along this alignment would principally protect development not protected by the existing project as intended in the original design would include a 450-foot long levee along the right channel bank immediately upstream of the downstream confluence with the diversion channel (mile 66.3). A 200-foot long levee would be required on the right channel bank to bridge a low channel bank area at river mile 66.1. The levees would have a 10-foot top width and average heights from 2 to 10 feet.

41. Other works required with this plan would include a 7-acre interior drainage ponding area with attendant outlet works to County Ditch No. 62, a collector ditch along the landward toe of the levee, a temporary 100-foot long sand bag closure, and limited clearing and grubbing. A total of 18.1 acres of land would be required including 8.5 acres for the levee works and 2.1 acres for the collector

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ditch. Estimated total first costs (table D-1) for this flood damage reduction plan would be about \$348,000. In addition to upgrading the existing project, Plan 8D would provide 100-year flood protection to presently unprotected residential and college property along the downstream reach. Protection of unprotected downstream reach property would be economically feasible with a resultant incremental benefitcost ratio of about 2.5. Since this plan provides the desired downstream reach flood protection, is incrementally economically feasible as it relates to the new development, and is generally acceptable to local interests, it is carried forward for detailed impact and trade-off analysis.

#### PLAN 9D - COMBINED HIGHWAY - LEVEE

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42. This alternative would involve a combined highway-levee embankment along the same alignment shown for plan 8D, as shown on plate D-2. This plan would include the 450-foot long river bank levee (mile 66.3) as in plan 8D but would not require the 200-foot long channel-bank levee. Interior drainage needs would be similar to those for plan 8D. Real estate requirements would increase by about 20 acres to 38 acres.

43. Plan 9D provides for incorporation of the required levee crosssection into the proposed highway embankment. Raising of the twolane embankment to provide the required three feet of freeboard would increase local road fill costs by about \$45,000. A modified plan placing the proposed roadway on the inside or protected side of the considered levee would eliminate the added \$45,000 fill cost but would require off-setting increased local rights-of-way costs

of about \$50,000. With either variation, the Federal costs would be limited to the equivalent levee cross-section required for flood control together with needed interior drainage works. Thus, project first costs for flood control would remain the same as for plan 8D. As this alternative is favored by the City, it is carried forward for further impact analysis.

PLAN 10D - COMBINED LEVEE - CHANNEL WORKS

44. Consideration was given to a combined levee-channel plan to further reduce flood stages in the downstream reach. This alternative would include the channel works described in alternative 7D together with the highway alignment levee, plan 8D. This plan would reduce downstream water levels slightly for an average levee height of about 3.5 feet. Interior drainage requirements would be essentially the same as for plan 8D. Construction of the channel widening measures would require replacement of the 200-foot levee with an 850-foot long levee (mile 66.1) of slightly higher average height. Total plan first costs are estimated at \$580,800 as shown on table D-1. Incremental average annual first costs of \$22,000 for the channel works portion when compared with incremental average annual benefits of \$11,400 indicates that addition of the channel work is not economically feasible. Further, this alternative would have a greater adverse environmental effect in terms of channel bank clearing, bank reshaping, and increased turbidity levels. Accordingly, plan 10D is not considered further.

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#### TABLE D. L ... COMPARENTE OF ALTERNATIVE

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|---|--|--|---|--|--|
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| Public for Litter   | he offices   | Whise long-town advorus<br>offset due to releastion<br>of public buildings and<br>other facilities from<br>dumtion area.   | Notes there term adverse<br>offects des co-relocation<br>and Medification of existin<br>public buildings in floode<br>dres  | Major img-tema afverse<br>effect due to immudation o<br>tga major pertion of Camion<br>5 State Farb.                         | Hajor reduction :=<br>f industed losses to<br>buildings, outdoor<br>and grownia Appe<br>reduction is flow<br>to public facilit |
| Public services   | Normal public services<br>disrupted for several<br>ders during flunding<br>in city   | Adverse short-term offect<br>due to relocation of<br>Decilities  | Maderate short-term<br>shorts effects<br>dat to relection<br>and reconstruction<br>officient  | Mayut jung-term likesen<br>of yark services of Cambon<br>State Park,   | Major long-torm is<br>offect from mainte<br>of public services<br>both flows energy<br>flowsfrom period.                       |
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| Bealance des federical Activity   | Hajer there-tark advers<br>Effect due to damaged<br><i>structures, factilitage</i><br>ded inventory and shar<br>down during periods of<br>Majer Lowings of<br>Majer Lowings due<br>200 militeres could be<br>Affected with a 100-year<br>or grouter fland ecourt | Poprands activities  | ModerNie Mud-Lerb adverse<br>offici due to remared<br>attivity during partial<br>evenuelae and flood<br>presting a Livities.  | Beduced business losses<br>due to bajor reduction in<br>frauericy and senterity of<br>flooding.                              | Hajer Bing-torn he<br>offict to reduced<br>Larson. Existing<br>Dollars' Lases of<br>reduced gener sit                          |
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|  | UPSTREAM RE   | ACH ONLY   |   | CONNETREAN RE   | ACH ONLY   |   |
|--|---|--|---|---|--|---|
|  | FLAN SP   | PLAN 6U  | Plan 70   | Plan 80   | PLAN 90  | Plan 100  |
|  | Combined Lever-<br>Channel Works  | Floodwater<br>Diversion Channel  | Channel<br>Improvements   | Highstay Alignment<br>Levee   | Combined Highway<br>Levee  | Combined Levee-<br>Channel Norks  |
| forest and acr<br>er. Change and<br>etat.on in Los<br>serveir in acu | s of mixed forest<br>understory cover.<br>s of terrestial and<br>atic vegetation a-<br>g riprapped channel  | Permanent loss of 7<br>acres of forest cover.<br>Temporary loss of<br>ground cover along<br>lavees until reseeding<br>is established.            | Temporary loss(4 to 5)<br>years) of ground cover,<br>shrubs slong 2 miles of<br>river bank. Permanent<br>loss of mature trees<br>along river in the vi-<br>cinity of channel mod-<br>ifications.  | 0.5 acres of upland<br>grasses, forus, shrubs   | Temporary loss of about<br>4.4 acres of native<br>grasses, shrubs and a<br>few scattered trees.              | Temporary vegetative<br>ground cover losses<br>along levee areas.<br>Permanent loss along<br>riprapped channel<br>bank areas.   |
|  | Minor long-term adv<br>habitat. Short-term<br>due to increased st:<br>struction. Permanent  | erse effect on eiparian<br>(2-scason) adverso effect<br>ream turbidity during con-<br>t loss of wooded wild life<br>loss of 15.8 acres of tilled | Temporary and long term<br>term disruption of small<br>memori habitat along re<br>worked river banks and<br>nel cutoff. Short term<br>effect on immited area<br>due to increased turbid<br>porary adverse effect t<br>birdlife utilizing wood<br>river as a resting place | cropland, formanient for<br>chan-<br>koverse<br>lithery<br>ity, Test-<br>transient<br>s along         | n of smail mammal hab-<br>s of 19 acres of tilled  | Short-term adverse<br>effect to stream fish-<br>ery and other aquatic<br>life due to increased<br>turbidity and sedi-<br>mentations. Long-term lo<br>of small magmal habitat<br>the yicinity of channel<br>modifications. |
| nd other<br>sting<br>h crea-<br>h lake.                              | <ul> <li>Permatent visual ch.<br/>impacted access to<br/>where levees pass t<br/>lots</li> </ul>  | anges and slightly<br>river at ? locations<br>hrough resident:sl   | Long-term changes in areas where channelizat takes place.   |   | hange to natural setting<br>acre ponding area.   | with completion   |
|  |   | føct   | Na Effect   | No effect   | Na effect  | No effect   |
| 5 yr) in<br>e, dust,<br>products<br>ir clear-<br>construction.       | - Short term (2 krs.)<br>and construction prod<br>protect constructio   |  | Slight increase in<br>two-season constr   |   | ducts during and for a si  | iort time after   |
| ater qual-<br>et life.<br>ect at Mar-<br>educed sedi                 | Major increase in st<br>ing and shortly afte<br>tere improvement due<br>stabilization.  | r construction. Long   | Major increase in strea<br>turbidity levels during<br>construction period.  | a No effect   | No effect  | Significant increase in<br>stream turbidity and<br>sedimentation during<br>and shortly after chan-<br>nel construction work.  |
| loads.   | during onstruction  | period   |   | orary increase during co  | nstruction period  | •••••   |
|  | of  | ces expended   | Energy resources used<br>for construction.  | Snergy resources a<br>projec: constructi  | ad reinforced concrete u<br>on.  | 1ed for   |
| as of<br>Actities<br>Voir Ares.                                      | One house would be<br>located a short dis<br>Four other would be<br>somewhat affected b<br>the close proximity<br>considered flood bu<br>Other flood prome s<br>would be significan<br>susceptible to recu<br>flood damage. | tance.<br>y<br>of<br>rriers.<br>tructures<br>tip less  | No significant effect<br>other than raising and<br>widening one bridge.   | Major beneficial<br>effect to college<br>complex with<br>increased level<br>of flood protect-<br>ion. | A considered feeder hig<br>could be efficiently<br>integrated with the cor<br>sidered levee embank-<br>ment. |   |
| is of<br>-flowing<br>-inmunda-                                       | Permanent loss of about 4.2 acres of woodland,  | Permanent loss of about 7 acres of forested area.  | Permanent loss of<br>about 0.10 acres of<br>channel bank woodlands.   | No significant effect to<br>natural resources.  | > Same as Plan ≇D  | Same as Plan BD   |

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# ALTERNATIVES CONSIDERED FURTHER

## UPSTREAM REACH

45. To provide increased flood protection at Marshall, the principal resource management problem in the study area, the formulation analysis considered both non-structural and structural alternatives. Present programs, such as flood plain regulation and flood insurance, under the no further public action alternative, although effective flood plain management tools, would not provide a comprehensive solution to the study area flood problems. Non-structural alternatives involving permanent evacuation or partial evacuation and flood proofing could provide a 100-year level of flood damage reduction but were found to be uneconomic and socially unacceptable. Of the structural alternatives, reservoir storage was found to be technically and economically infeasible due to lack of needed storage capacity and unacceptable due to the adverse social and environmental impacts. Thus, localized improvements including levees and channel works together with flood plain regulation and flood insurance are left as the only feasible and practical means of providing needed additional flood damage reduction.

46. The selection of upstream reach alternatives for further analysis was based on the need for providing locally acceptable and viable measures for insuring effective operation of the existing diversion project. The alternatives carried forward were then subjected to an in-depth impact and trade-off analysis to provide a technically and economically viable plan commensurate with the equal needs of preservation and/or enhancement of area environment, social, and cultural values. To make this analysis, all selected alternatives were evaluated on the basis of criteria outlined earlier in this section.

> Appendix I D-23

47. Of the upstream reach structural alternatives considerd, only the combined levee-channel plan (plan 5U) and the flood water diversion channel plan (plan 6U) would meet study area flood plain management needs and are considered further. Plan 5U provides the least costly plan in terms of both first costs and subsequent operation and maintenance costs to the city. This plan would enable potentially damaging flood flows to reach and pass through the existing project without problems and the expense of local resources similar to those incurred during the 1969 flood. The considered works would have temporary adverse effects in terms of impaired water quality, increased noise and air pollution levels, and channel bank habitat changes. Marked increases in stream turbidity and sedimentation would occur during construction but diminish to below current levels after a short period due to protection of presently eroding river banks. Increased noise, dust, combustion product levels, and smoke from the controlled burning of debris and trees would cease almost immediately after construction. Revegetation of disturbed channel bank areas would reduce small mammal habitat losses. Relatively permanent effects would include the loss of about 4.2 acres of woodlands and related small mammal and bird habitat, and aesthetic changes where the proposed level is in close proximity to seven residences.

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Appendix I D-24

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48. Plan 5U would provide substantial beneficial effects in terms of added flood protection for the City of Marshall, which in turn would maintain desirable community growth patterns and assure Marshall's status as a vigorous regional trade, service and educational center.

49. Modification of plan 5U to include protection to the 10-acre river meander area (plan 5U-mod. 1) would be technically feasible but economically unjustified since the entire area could be filled an average of about one foot to the 100-year flood level. Estimated fill costs are about \$28,700 as compared to the perimeter levee costs of approximately \$172,000. Levee construction around the river loop would also result in considerable fringe woodland loss as compared to no loss with the basic plan 5U levee across the open farm land. Although a slight inconvenience to area access, the proposed levee would be ramped and surfaced for unimpeded access to the unprotected meander area. This proposed modification would also result in the loss over Plan 5U of an additional two acres of fringe woodland and understory cover already in relatively short supply.

50. The flood water diversion channel (plan 6U) would also provide Marshall an adequate level of flood protection, but at twice the costs of plan 5U. A lower and shorter right bank levee with this plan would have lesser adverse aesthetic effects to affected residences. However, increased woodland and understory cover losses of about 1.8 acres would result with further adverse effects on floodway wildlife. However, plan 6U clearly lacks economic feasibility as indicated by the 0.8 benefit-cost ratio (table D-1).

> Appendix I D-25

## DOWNSTREAM REACH

51. Of the downstream reach structural alternatives considered, both the highway alignment levee (plan 8D) and the combined highway-levee plan (plan 9D) are discussed further. In addition, limited channel measures immediately below the downstream confluence of the river and diversion channel are considered with both plans. Plan 8D with limited channel widening, would, in combination with upstream reach plan 5U, provide the most cost-effective additional measures to achieve a 100-year degree of protection for the city and adjacent downstream developments. Plan 8D would result in minimal environmental losses as the proposed levee would traverse presently tilled cropland with essentially no native grass or tree losses. The required channel widening works would occur entirely on reworked channel bank areas presently covered with scattered weed growth. This plan would result in the immediate loss of about 15 acres of cropland and likely facilitate the eventual conversion of another 80 acres to urban development.

Appendix I D-25a

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52. The combined levee-highway plan (plan 9D) would accomplish the same degree and extent of protection as plan 8D and at nearly the same Federal first cost for flood damage reduction. This plan would result in the immediate conversion of about 50 acres of cropland to flood control purposes. Except for slightly increased vegetative ground cover losses in the vicinity of an old river oxbow, plan environmental effects would be similar to those with plan 8D. Although plan 9D was initially suggested by the City, it is now considered unlikely that local plans for the proposed highway would be ready in time to permit combined construction assuming normal Federal approval and funding of any recommended flood control works.

# CONTRIBUTIONS OF ALTERNATIVES

# TO NATIONAL OBJECTIVES

## GENERAL

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53. The selected water resource plan for added measures to assure operation of the existing project as designed and protecting downstream reach developments at Marshall must not only satisfy specific objectives for the study area but provide positive contributions to the national economic development and environmental quality objectives. To achieve a balanced plan reflecting the area's dual concern for improved flood plain management while maintaining and enhancing the natural environment, separate plans -- one optimizing economic efficiency, the other emphasizing the environmental quality objective -- were developed. Through a series of trade-offs among public preferences and beneficial and adverse plan impacts, the plan

> Appendix I D-26

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which contributed most to the local and national planning objectives was developed and further refined. Table D-2 gives a comparison of beneficial and adverse plan impacts for the selected plan, NED Plan and EQ Plan in accordance with the system of accounts established by the Water Resources Council.

## NATIONAL ECONOMIC DEVELOPMENT (NED) PLAN

54. The NED Plan must, from the national point of view, represent the best return on the investment of economic resources, including capital, labor, and irreplaceable natural resources needed for construction. For upstream reach measures to assure effective operation of the existing project, plan 5U incorporating levees, an overflow weir with attendant outlet works, channel widening and bank stabilization measures represents the most economically feasible plan that would provide the desired degree of flood damage reduction. Similarly, and as shown on table D-2, the proposed downstream reach levee along the considered highway alignment (plan 8D) together with minor channel widening measures (part of plan 7D) provides the most economical method of improving the operation of the existing project and providing a minimum 100-year degree of protection to presently unprotected downstream reach flood plain development.

## ENVIRONMENTAL QUALITY (EQ) PLAN

55. The EQ plan is the alternative which enhances the quality of the environment through the preservation or enhancement of important natural and cultural resources and ecological systems, and which

Appendix I D-27

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minimizes adverse effects on environmental quality. The alternatives chosen for further analysis were formulated principally on the basis of the flood damage reduction objective. An evaluation of these alternatives in the context of enhanced environmental quality was made to develop the environmental quality plan. Since all alternatives were formulated based on satisfying the specific flood damage reduction objective and the EQ plan must also satisfy this objective, the EQ alternative was with relatively minor alteration, among the alternatives considered for further analysis.

56. The selected framework environmental quality alternative was that which is initially least environmentally disruptive to the existing project area. After selection of the framework EQ alternative, measures to better fulfill specific study objectives were added incrementally to develop the most acceptable and environmentally beneficial plan. From such an analysis of alternatives considered further for principally flood damage reduction, it was determined that the EQ plan would include:

Upstream Reach -- Plan 5U incorporating added measures such as reshaping and relocation of certain portions of the flood barrier at nearby residential structures; addition of a recreational trail and other facilities on or near the levee crown to enhance local recreation opportunities; modification of the overflow weir to better blend into the existing roadside park setting; and tree and shrub plantings to minimize the visual impact on the levee works. Clearing and snagging measures would be deleted with only a slight adverse effect on channel hydraulic capacity but with significant gains in environmental quality. This alternative would have long term beneficial environmental effect in terms of assured flood protection for Marshall, reduced river bank erosion and improved water quality. Short-term adverse effects would include loss of natural habitat and

> Appendix I D-28

associated temporary losses in benthic organisms and small mammal populations. Reseeded channel bank, levee, and spoil areas would return to a near-native state within a few years after construction.

Downstream Reach -- Plan 8 D. together with limited channel widening, aesthetic tree and shrub plantings, and a recreational trail system on or near the levee, and flood plain management measures for residual unprotected flood plain areas, was selected as the EQ plan as well as the NED plan since it would have the least adverse effect ... the natural and cultural setting while still satisfying the flood damage reduction objective. This alternative would require no wooded areas and very limited grassed areas as the proposed levee alignment would be along presently tilled cropland. Small mammals frequenting the area would only be temporarily displaced by the construction activities.

# PLAN SELECTION

57. Selecting the best plan of improvement for the City of Marshall involved the comparison of alternatives which satisfy established water resource planning objectives and formulation and evaluation criteria. Of the upstream reach alternatives considered further, plan 5U, with continued flood warning services and flood plain management of the residual 10-acre river meander area and addition of environmental enhancement measures, is considered in balance the best possible plan. As local highway plans are not expected to be completed in time to permit a combined project, plan 8D together with minor channel widening and management of residual flood plain areas is the best downstream reach plan.

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58. Together, these plans provide an effective and locally acceptable combined plan of improvement for resolving the residual flood problem at Marshall. Thus, the combined plan is selected for detailed design and cost estimates. At several meetings held at Marshall, the city, county, and Minnesota Department of Highways have provided substantial input to the plan formulation process and all generally concur with the selected plan. Table D-4 displays the system of accounts for the selected plan.

# SCALE OF DEVELOPMENT

#### GENERAL

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59. To permit selection of the optimum economic level of flood damage reduction for the City of Marshall, costs and benefits were evaluated for five degrees of flood protection that would be provided by varying the design flood discharge for the flood control project. Results of the plan optimization studies are discussed separately in the following paragraphs.

60. To determine the optimum level of protection, annual costs and benefits were determined for the 50-year (6100 cfs), 100-year (8200cfs), 150-year (9500), 200-year (10,500 cfs), and 250-year (11,500 cfs) flood levels. Although the SPF flood flow upstream of the BN Railroad bridge at mile 72.6 is 16,700 cfs, only 11,800 cfs can enter the project area through the Burlington Northern Railroad bridge at mile 72.6. Thus, this flow, equivalent to a 270-year flood frequency flow, is considered to represent Standard Project Flood conditions in the upstream reach as the remaining 4900 cfs which would flow north eastward through the airport grounds and re-enter the existing diversion channel does not significantly contribute to the damage potential within the heavily developed areas of Marshall (Reaches B, C & D). The SPF level flow of 16,700 cfs was used to reflect annual costs and benefits for related downstream reach flood damage reduction measures.

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61. From an analysis of annual costs and benefits for these five levels of protection an optimum relationship between average annual costs and benefits for the entire project exists when flood protection is provided against a flood having a recurrence interval of once in about 133 years. Plan optimization data are given in table D-2 and shown graphically on Plate D-3.

## Table D-2 Plan Optimization Data (6 7/8% Interest Rate)

| Level of   | Annual    | Annual    | Net       | Benfit-           |
|------------|-----------|-----------|-----------|-------------------|
| Protection | Cost      | Benefits  | Benefits  | <u>Cost Ratio</u> |
| 50-year    | \$113,330 | \$146,800 | \$ 33,470 | 1.30              |
| 100-year   | 142,240   | 260,800   | 118,560   | 1.83              |
| 150-year   | 218,070   | 309,100   | 91,030    | 1.42              |
| 200-year   | 430,640   | 334,610   | -96,030   | 0.78              |
| 250-year   | 483,320   | 350,220   | -133,100  | 0.72              |

62. As a higher level of protection would be justified by a benefitcost ratio greater than unity but at reduced net benefits as indicated in table D-2, a sensitivity analysis of interest rates varying over time versus benefit-cost ratios was made to determine the limits of economic feasibility. Interest rates selected to provide a broad range of rates were the 6 7/8, 7 5/8, 8 3/8, and 12 percent rates. These rates were assumed to increase one-fourth of one percent per year until fixed by assumed authorization of the project. The analysis indicated that the earliest the rates would be fixed would be in year 1985 at a rate of 8 3/8 percent. A tabulation of benefit-cost ratios versus interest rates for the 50-year through 200-year levels of protection is given in table D-3. Similar data for the 250-year flood level was not derived as a benefit-cost ratio less than unity is indicated at the current 6 7/8 percent interest rate.

Appendix I D-31

|               |                | Level            | of Protectio    | on              | <u> </u> |
|---------------|----------------|------------------|-----------------|-----------------|----------|
| Interest Rate | <u>50-year</u> | <u> 100-year</u> | <u>133-year</u> | <u>150-year</u> | 200-year |
| 6 7/8         | 1.3            | 1.8              | 1.8             | 1.4             | 0.78     |
| 7 5/8         | 1.2            | 1.7              | 1.6             | 1.3             | 0.71     |
| 8`3/8         | 1.1            | 1.5              | 1.5             | 1.2             | 0.65     |
| 12            | 0.8            | 1.1              | 1.04            | 0.83            | 0.46     |

## Table D-3 Sensitivity Analysis-Comparison of Benefit-Cost Ratios with Varying Interest Rates

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63. From Table D-3 it is evident that the maximum feasible level of protection would be about the 150-year flood level at the 8 3/8% interest rate. Increasing the level of protection from the 133-year level to the 150-year flood level (12.8% increase) would result in a 29.6 percent reduction in net benefits or \$38,300. The analysis also indicated that up to about the 133-year flood level, total first costs generally increase proportionately with respect to increased flood barrier heights. However, once this level is exceeded, added costly measures would sharply increase total project first costs as generally indicated by the flattened upper portion of the optimization curve shown on Plate D-3. Principal added measures to assure an effective 150-year level of protection would include raising of the CSAH 7 bridge with related grade transitions, raising of the BN railroad subgrade adding an impervious clay blanket along the innerward side of the railroad embankment upstream of County Highway 7, added channel works, and additional flood barrier works upstream of the downstream confluence river and existing diversion channel.

64. Provision of this added increment of protection would result in increased Federal and Non-Federal first costs by about \$680,000 and \$360,000 respectively for a total increase in project first costs of about \$1,040,000.

A CALL AND THE SHOP

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Appendix I D-32

65. Provision of a standard project flood level of protection would require further extension of the service drive road raise upstream of the Highway 23 wayside park. The resultant 6 to 7 foot raise would result in severe and unacceptable driveway grades at several residences. Provision of a SPF level of protection would also result in severe dislocations of established residential areas with the required relocations of 5 houses upstream of CSAH 7 and numerous residences and businesses in the developed downtown area (1.2 mile backwater flood barrier reach). As indicated in Table D-2, a 250-year level of protection, which is close (11,500 cfs v.s. 11,800 cfs) to the SPF flow downstream of the BN railroad bridge at mile 72.6 is clearly infeasible as indicated by the 0.72 benefit-cost ratio.

66. Assuming a levee failure at the SPF flow, approximately 3500 cfs would enter the densely urbanized portion of the city. Of this amount, 2000 cfs would represent overland flow over County Highway 7 and which would re-enter the river channel downstream of the existing diversion structure. The total flow of 3500 cfs would result in a flooded area along the river with an average width of about 1200 feet and average water depths of 2 to 4 feet. Overbank velocities would be less than 0.8 feet per second. Several hundred commercial and residential structures would be adversely affected by either basement or first floor flooding.

67. However, as nearly all of the proposed levees along both study reaches would be relatively low (4 to 5 feet average height) the potential for loss of life is not considered great. To assure that no flows would overtop flood barriers upstream of the existing diversion structure, two feet of freeboard above the SPF flood level would be provided along the right bank levee between the existing diversion structure and the proposed overflow works at the wayside park.

Appendix I D-33

68. After review of the draft feasibility report, the City of Marshall stated (See April 1978 letter from City of Marshall in Appendix 2) that provision of a SPF level of protection would be unrealistic and unacceptable to the City. They further advised that the design 133-year plan of protection would be acceptable subject to a few minor modifications. Subsequent to this correspondence, additional study effort was made to establish the maximum practical but still feasible level of protection. As discussed in earlier paragraphs, this level is about the 150-year flood level. This reanalysis was presented to the City for their review. By letter of 21 February, 1979 (See Appendix 2) the City advised that the "... proposed 133-year level of protection would still be a most acceptable level of protection" and that "... the additional work and cost involved do not warrant the relatively small degree of additional protection...". Thus, based on the foregoing optimation and sensitivity analyses, consideration of the impact of a SPF levee failure, and views of the City, a 133-year degree of protection was selected as the appropriate level for project designs and estimates.

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69. At several coordination meetings subsequent to the basic formulation studies of upstream reach flood damage reduction alternatives, the City has indicated a perceived need for acquiring the flood plain lands upstream of CSAH 7 and lying between the right bank flood barriers and the Burlington Northern Railroad right-of-way. About 71.1 acres of flood plain land would be affected at the 133-year design flood level. The City believes that local developmental conditions would force either outright purchase of these lands or equally costly flood easements. Acquisition of these lands by local interests is part of the proposed project is considered advisable as any significant developments (encroachments) in the floodway may adversely affect design flood levels and operation of the proposed project. Inclusion of the additonal estimated cost of \$101,000 for these lands in the completed plan formulation estimates would

> Appendix I D-34

not significantly influence the conclusions reached. Thus, acquisition by local interests of the additional 71.1 acres of flood plain lands for project floodway purposes is incorporated as a feature of the selected plan.

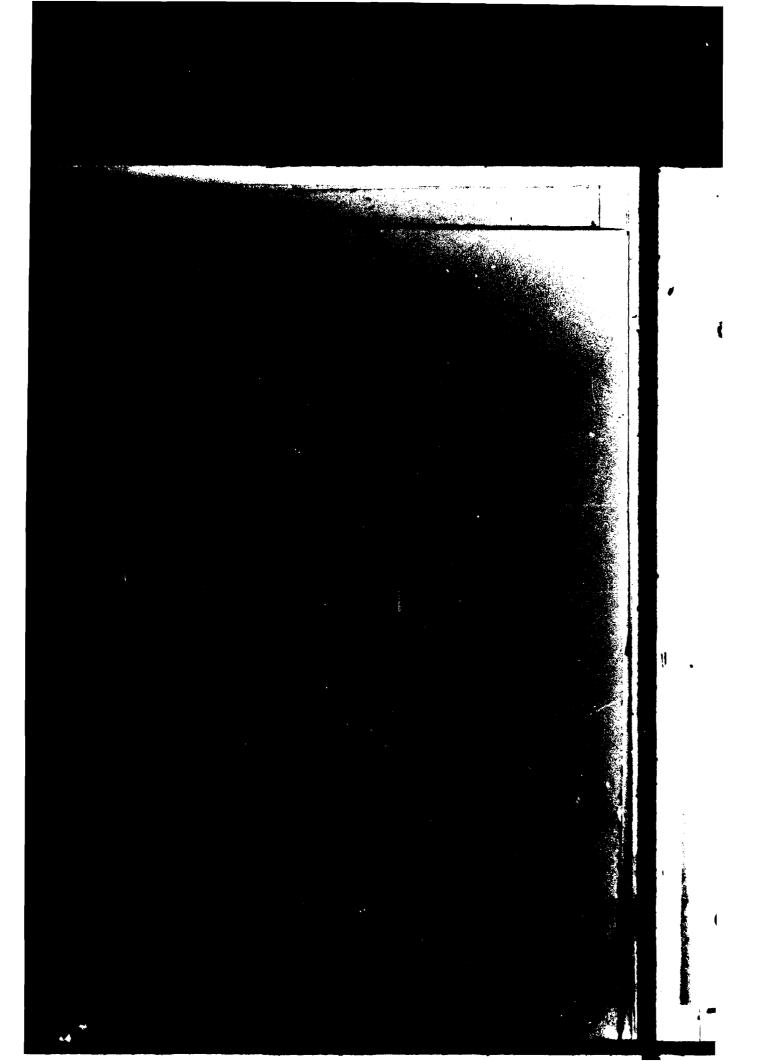
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|   |             |         |             |                     |                |                          |                             |                  |                  | :                 |                   |                   |       |    |   |
|   |             |         |             |                     |                |                          |                             |                  |                  | _                 | • /**             |                   |       |    |   |
| , |             |         |             |                     |                | ŀ                        | _                           |                  |                  |                   | •                 |                   |       |    |   |
|   |             |         |             |                     |                |                          |                             |                  |                  |                   |                   |                   |       |    |   |
|   |             |         |             |                     |                |                          |                             |                  |                  |                   |                   |                   |       |    |   |
|   |             |         |             |                     |                |                          |                             |                  |                  |                   |                   |                   |       | 1. |   |
|   |             |         |             |                     |                |                          |                             |                  |                  |                   | _                 |                   |       |    |   |



SYSTEM OF ACCOUNTS

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# Table D-4 - relected Plan

|   |  |        | Q                          | Regional<br>Development |                   | [   | Inc<br>Inc       | A Summary<br>Income Classes | es                         |
|---|--|--------|----------------------------|-------------------------|-------------------|---|------------------|-----------------------------|----------------------------|
| <ol> <li>National Economic Development</li> <li>Beneficial (x \$1000)<br/>Increased output</li> <li>Flood Control (Av. Ann.) III 260.8 A,b 0 0 260.8 A,b 29.2 0.5<br/>Floodproof Cost Savings<br/>Benefits III 9.8 A,b 0 0 43.1 A,b</li> <li>Floodproof Cost Savings III 43.1 A,b 0 0 43.1 A,b</li> <li>Recreation III 43.1 A,b 0 0 0 313.7 34.6 0.5</li> <li>Adverse (x \$1000)</li> <li>Adverse (x \$1000)</li> <li>Adverse (x \$1000)</li> <li>Adverse for project construction I 26.7 A,b 0 139.9 166.6 A,b</li> <li>Adverse for Normal Science for (Nr. Ann.)</li> <li>External diseconomies<sup>1</sup></li> <li>I 10 A,c 0 0 1.0 A,c</li> <li>Adverse Ann.)</li> <li>Sternal diseconomies<sup>1</sup></li> <li>Recreation II 26.7 A,b 0 0 1.0 A,c</li> <li>Barting (Mathematical diseconomies)</li> <li>I 1.0 A,c 0 0 1.0 A,c</li> <li>Fixinonmental Quality</li> <li>Wild § Scenic Rivers</li> <li>Archeological</li> <li>Historical</li> </ol>   | Effects  | Timing | Marshall                   | Southwest<br>Minnesota  | Rest of<br>Nation |   | kesi-<br>lential | Comm.<br>Indust.            | Public                     |
| Beneficial (x \$1000)           Increased output           Flood Control (xv. Ann.)           Increased output           Flood Control (xv. Ann.)           Flood Control (xv. Ann.)           Floodproof Cost Savings           III         9.8 A,b         0         0         8.4,b         0.5           Floodproof Cost Savings         III         43.1 A,b         0         0         43.1 A,b         -           Recreation         III         43.1 A,b         0         0         43.1 A,b         -         -           Recreation         III         43.1 A,b         0         0         43.1 A,b         -         -           Recreation         III         43.1 A,b         0         0         43.1 A,b         -         -           Adverse         (x \$1000)         1         143.1 A,b         0         0.5         -           Adverse         (x \$1000)         1         1313.7         0         0.5         -           Adverse         (x \$1000)         1         1         1.0 A,c         -         -         -           Adverse         (x \$1000)         1         1         1.0 A,c         0         0 <t< th=""><th>1. National Economic Development</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>   | 1. National Economic Development                             |        |                            |                         |                   |   |                  |                             |                            |
| Increased output         Increased output           Flood Control (Av. Ann.)         111         260.8 A,b         0         0         260.8 A,b         29.2         0.5           Floodproof Cost Savings         111         9.8 A,b         0         0         9.8 A,b         100.0         0           Recreation         111         43.1 A,b         0         0         43.1 A,b         -         -           Recreation         111         43.1 A,b         0         0         313.7         54.6         0.5           TOTAL BENEFICIAL         313.7         0         0         313.7         54.6         0.5           Adverse (x \$1000)         Value of resources for         313.7         0         0         10.6.6 A,b         -         -           Adverse (x \$1000)         1         1.0 A,c         0         0         313.7         54.6         0.5           Adverse (x \$1000)         1         1.0 A,c         0         0         313.7         54.6         0.5           Adverse         1         1.0 A,c         0         0         1.0 A,c         -         -           Value of resources for         1         1.0 A,c         0         0         <   | Beneficial (x \$1000)  |        |                            |                         |                   |   |                  |                             |                            |
| Flood Control (av. Ann.)         III $260.8$ A,b $29.2$ $0.5$ Floodproof Cost Savings<br>Benefits         III $260.8$ A,b $29.2$ $0.5$ Floodproof Cost Savings<br>Benefits         III $26.1$ A,b $0$ $0$ $31.3$ A,b $100.0$ $0$ Recreation         III $43.1$ A,b $0$ $0$ $43.1$ A,b $ -$ Retreation         III $43.1$ A,b $0$ $0$ $43.1$ A,b $ -$ TOTAL BENEFICIAL $313.7$ $0$ $0$ $313.7$ $0$ $0.5$ $34.6$ $0.5$ Adverse $x$ 31000) $1$ $26.7$ A,b $0$ $0$ $313.7$ $34.6$ $0.5$ Adverse $0$ $0$ $1$ $1.00.0$ $0$ $34.6$ $0.5$ $0$ Å M (Av. Ann.) $1$ $1.0$ $0$ $0.4$ $0.6$ $0.5$ $0.5$ $0$ Å M (Av. Ann.) $1$ $1.0$ $0$ $0$ $0$ $0$   | Increased output   |        |                            |                         |                   |   |                  |                             |                            |
| Floodproof Cost Savings<br>Benefits         III         9.8 A,b         0         0         9.8 A,b         100.0         0           Recreation         III         43.1 A,b         0         0         43.1 A,b         -         -           Recreation         III         43.1 A,b         0         0         43.1 A,b         -         -           Fxternal Economics  |  | 111    | 260.8 A,b                  |                         | 0                 | 260.8 A,b   | 29.2             | 0.5                         | 70.3                       |
| Recreation         III         43.1 A,b         0         0         43.1 A,b         -<   |  | 111    | <b>9.</b> 8 A,b            |                         | 0                 | 9.8 A,b   |                  | 0                           | 0                          |
| External Economics       External Economics       Morecase       Stress       Stress </td <td>Recreation</td> <td>111</td> <td>43.1 A,b</td> <td></td> <td>0</td> <td>43.1 A,b</td> <td></td> <td>,</td> <td>ł</td> | Recreation   | 111    | 43.1 A,b                   |                         | 0                 | 43.1 A,b  |                  | ,                           | ł                          |
| TOTAL BENEFICIAL       313.7       0       0       313.7       34.6       0.5         Adverse       (x \$1000)       313.7       34.6       0.5       34.6       0.5         Adverse       (x \$1000)       Value of resources for project construction (Av. An.)       1       26.7 A,b       0       139.9       166.6 A,b           Yeal       1       1.0 A,c       0       0       1.0 A,c            Kitemal diseconomics <sup>1</sup> /       1       26.7 A,b       0       139.9       166.6 A,b           Kitemal diseconomics <sup>1</sup> /       1       1.0 A,c       0       0       8.4   | External Economics   | 1      |                            | None                    |                   |   |                  |                             |                            |
| Adverse(x \$1000)Value of resources for<br>project construction<br>(Av. Ann.)I26.7 A,b0139.9 166.6 A,bValue of resources for<br>project construction<br>(Av. Ann.)I26.7 A,b0139.9 166.6 A,bExternal diseconomies <sup>1</sup> /<br>(Av. Ann.)I1.0 A,c001.0 A,cO § M (Av. Ann.)I8.4 A,b008.4TOTAL ADVERSE36.10139.9 176.034.60.5Environmental QualityNild § Scenic RiversNoneNoneLakesBuried archeological sites possible Effects unknownHistoricalNo known effects  | TOTAL BENEFICIAL   |        | 313.7                      | 0                       | 0                 | 313.7   | 34.6             | 0.5                         | 64.9                       |
| Value of resources for<br>project construction<br>(Av. Ann.)I26.7 A,b0139.9166.6 A,b(Av. Ann.)I1.0 A,c001.0 A,cExternal diseconomies <sup>1</sup> /I1.0 A,c001.0 A,c0 § M (Av. Ann.)I8.4 A,b008.4TOTAL ADVERSE36.10139.9176.034.60.5Furionmental QualityMild § Scenic Rivers  | Adverse (x \$1000)   |        |                            |                         |                   |   |                  |                             |                            |
| External diseconomies <sup>1</sup> /<br>0 & M (Av. Ann.)       I       1.0 A,c       0       0       1.0 A,c       0         0 & M (Av. Ann.)       I       8.4 A,b       0       0       8.4       0       0         707AL ADVERSE       36.1       0       139.9       176.0       34.6       0.5         Fivironmental Quality       36.1       0       139.9       176.0       34.6       0.5         Fild & Scenic Rivers       36.1       0       139.9       176.0       34.6       0.5         Lakes  | Value of resources for<br>project construction<br>(Av. Ann.) | П      | 26.7 A,b                   |                         | 139.9             | 166.6 A,b   |                  | 1                           |                            |
| 0 & M (Av. Ann.)       I       8.4 A,b       0       0       8.4           TOTAL ADVERSE       36.1       0       139.9       176.0       34.6       0.5         Environmental Quality       36.1       0       139.9       176.0       34.6       0.5         Mild & Scenic Rivers      None      None            Lakes      Buried archeological sites possible Effects unknown            Historical      Nown effects   | External diseconomies <sup>1/</sup>                          | I      | 1.0 A,c                    |                         | 0                 | 1.0 A,C   | <br> <br> <br>   |                             | 1                          |
| TOTAL ADVERSE36.10139.9176.034.60.5Environmental QualityMild & Scenic Rivers  | 0 & M (Av. Ann.)   | Ч      | 8.4 A,b                    |                         | 0                 | 8.4   |                  | 8                           | 1                          |
| Environmental Quality<br>Wild & Scenic Rivers   | TOTAL ADVERSE  |        | 36.1                       | 0                       | 139.9             | 176.0   | 34.6             | 0.5                         | 64.9                       |
| Rivers  |  |        |                            |                         |                   |   |                  |                             |                            |
| Buried archeological sites possible Effects unknown   | Wild & Scenic Rivers   |        | *<br>*<br>*<br>*<br>*<br>* | None                    |                   | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 |                  | +<br> <br> <br>             | 1                          |
| Buried archeological sites possible Effects unknown   | Lakes  |        |                            | None                    |                   |   | 1<br>1<br>1<br>1 |                             | 1<br>1<br>1                |
|   | Archeological  |        | -Buried arc                | heological s            | ites pos          | sible E   | ffects ur        | iknown                      | f<br>1<br>1<br>1<br>1<br>1 |
|   | Historical   |        |                            | No known €              | ffects            |   |                  | * + -                       |                            |

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Appendix I D-36

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Table D-4 - Selected Plan (continued)

|                                       |        |   | Regional<br>Development |                   |                                      |                  | A Summary<br>Income Classes | asses            |
|---------------------------------------|--------|---|-------------------------|-------------------|--------------------------------------|------------------|-----------------------------|------------------|
| <br>Effects                           | Timing | Marshall  | Southwest<br>Minnesota  | Rest of<br>Nation | Totals                               | Resi-<br>dential | Comm.<br>Indust.            | Public           |
| Ecological Systems                    | -      | Project would convert about 9.1 acres<br>of cropland to intermittently wet<br>ditches and ponding area. Some shift<br>of terrestial floral and faunal species<br>to semi-aquatic species expected.<br>Approximately 4.2 acres of forest and<br>understory cover would be converted to<br>grassed areas. Acquisition of approx-<br>imately 70 acres of flood plain lands<br>upstream of CAM 7 would preserve these<br>lands in their current natural state.<br>Reseeding of disturbed areas would limit<br>most losses to one or two growing<br>seasons. A,b |                         |                   | Same as for<br>Marshall              |                  |                             |                  |
| <b>Irreversible Effects</b>           | 1, 111 | Commitment of material and energy<br>resources for project construction.<br>Loss of 4.2 acres of mature forest cover.<br>Conversion of 119.8 acres to flood<br>control uses. A,c,F,   |                         |                   | Same as for<br>Marshall              |                  |                             |                  |
| 3. Regional Development               |        |   |                         |                   |                                      |                  |                             |                  |
| Income - Summary<br>National Accounts | 111    | 175.0 F = Ave. ann. cost +<br>0 § M - 1,000   | 0                       | 139.9 +           | 35.1                                 | 34.6             | 0.5                         | 04.9             |
| *Employment Stability                 | 11     | Likely increase, not quantified.A,B   |                         |                   | 8<br>8<br>9<br>9<br>8<br>8<br>8<br>8 |                  | 4<br>1<br>1<br>1            |                  |
| Population Distribution               | 111    | Increased residential population in protected area  | lation in p             | protected         | 8rea                                 | 3<br>4<br>4      | 1<br>1<br>1<br>1            |                  |
| *Desirable Regional Growth            | 111    | Enhanced community growth pattern.<br>A,b,F   | 1                       | 8<br>1<br>3<br>8  |                                      |                  | 1                           | 4<br>6<br>9<br>9 |
| · Local Tax Revenues                  | 111    | Increase, not quantified. A,b   |                         | 0                 | 0                                    | 1<br>1<br>1<br>1 |                             |                  |
| *Property Values                      | 111    | Likely increase in some areas to<br>reduced flood risk. A,b,P   |                         | 0                 | 0                                    |                  |                             | 1<br>1<br>1<br>1 |

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Table D-4 - Selected Plan (continued)

| - <u>-</u>       |                             | T<br>ining | Marshall  | Regional<br>Development<br>Southwest<br>Minnesota                          | Rest of<br>Nation | Totals                  | The Natio<br>A Summary<br>Income Cla<br>Resi-<br>Comm. | E SSes |  |
|------------------|-----------------------------|------------|---|--|-------------------|-------------------------|--|--------|--|
|                  | nd Quality                  | 1, 111     | 4.2 acres of<br>version of<br>land to flood<br>seervation of<br>flood<br>natural state due<br>natural state due   | Loss of 4.2 acres<br>of wood lands out<br>of a limited<br>regional supply. |                   | Same as for<br>Marshall | ;  |        |  |
|                  | •Air Quality and Noise I    |            | Temporary increase in smoke, dust<br>and fuel combustion products in<br>air and increased noise levels<br>during 2-season construction period.<br>A,b   |  |                   | Same as for<br>Marshall |  |        |  |
|                  | Streatbank erosions         | 1, 111     | Terrporary increase during and shortly<br>after construction. Long-term<br>decrease due to bank stabilization.<br>A,c   | A1   |                   | Same as for<br>Marshall |  |        |  |
|                  | •Mater Quality              | 1, 111     | Temporary marked increase in stream<br>turbidity during and for a short<br>time after construction. Long-term<br>improvement due to channel bank<br>stabilization. A,b                                      |  |                   | Same as for<br>Marshall |  |        |  |
|                  | Biological Resources        | 1          | Initial loss of benthic fauma due<br>to channel works. Temporary de-<br>struction of other small mammal<br>habitat. Some re-population of species<br>expected within a few years after<br>construction. A,b | cies   |                   | Same as for<br>Marshall |  |        |  |
| Appendi:<br>D-38 | Rare and endangered species |            |   | ect  |                   |                         |  |        |  |

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Table D.4 -- Selected Plan (continued)

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|   |  | Regional<br>Development                  |   |                                      | F                | The Nation:<br>A Sumary<br>Income Classes | 13865  |
|---|--|--|---|--------------------------------------|------------------|---|--------|
| Rfocts Tining   | Marshall   | Southwest<br>Minnesota                   | Rest of<br>Nation Tr  | Totals                               | Resi-<br>dential | Com.<br>Indust.                           | Public |
| 4. Social Mell-being<br>Reduced Flood Risk I  | Reduced demages to all cate-<br>gories of development. A,c,F.  |  | Reduced   | Reduced threat to<br>all categories. | -                |   | ;      |
| Loss of Agricultural<br>Lands   | Approximately 14.3 acres of No appl<br>cropised lest with construction effect.<br>of lowes and interior drainage   | Mo appreciable<br>effect.                | A,c,F<br>Insignificant Same as for<br>effect. Marshall  | as for<br>hall                       |                  | ł   | ;      |
| Recreation  | works.<br>Added opportunities for leisure No appreciable<br>time enjoyment. A,c,F  | No appreciable<br>effect.                | No effect. Same as<br>Marshail  | Same as for<br>Marshall              | ;                |   | 1      |
| NUTATION: Actual and Potential Effects  | i Uncertainty Non-Exclusivity  | Y Tining                                 |   |                                      |                  |   |        |
| <ul> <li>A - No Gevernment action meeded other<br/>than implementing agencies.</li> <li>B - Government action meeded and likely<br/>to produce beneficial effect; ad-<br/>verse effect can and likely will<br/>be prevented by Government action.</li> <li>C - Gevernment action meeded but not<br/>estaured to produce beneficial<br/>effect; Government Sction can pre-<br/>vent adverse effect but such<br/>action not assured.</li> </ul> | <ul> <li>a - 50% or F - Overlapping more antry with with with web; fully</li> <li>b - 10-50% NED; fully</li> <li>c - less than monetarized in NED account.</li> <li>c - verlapping tertially</li> <li>monetarized in NED;</li> <li>account.</li> </ul> | I -<br>mt. II -<br>III -<br>IIY -<br>V - | Construction or<br>within a few years<br>of construction.<br>Over project life,<br>main impact by<br>year 10.<br>Over project life<br>main impact by<br>20-15 years.<br>Over project life,<br>anin impact by<br>sain impact by<br>S0 years. |                                      |                  |   |        |

Mammal loss of production on 15.8 acres of cropland lost to leves and interior drainage works.

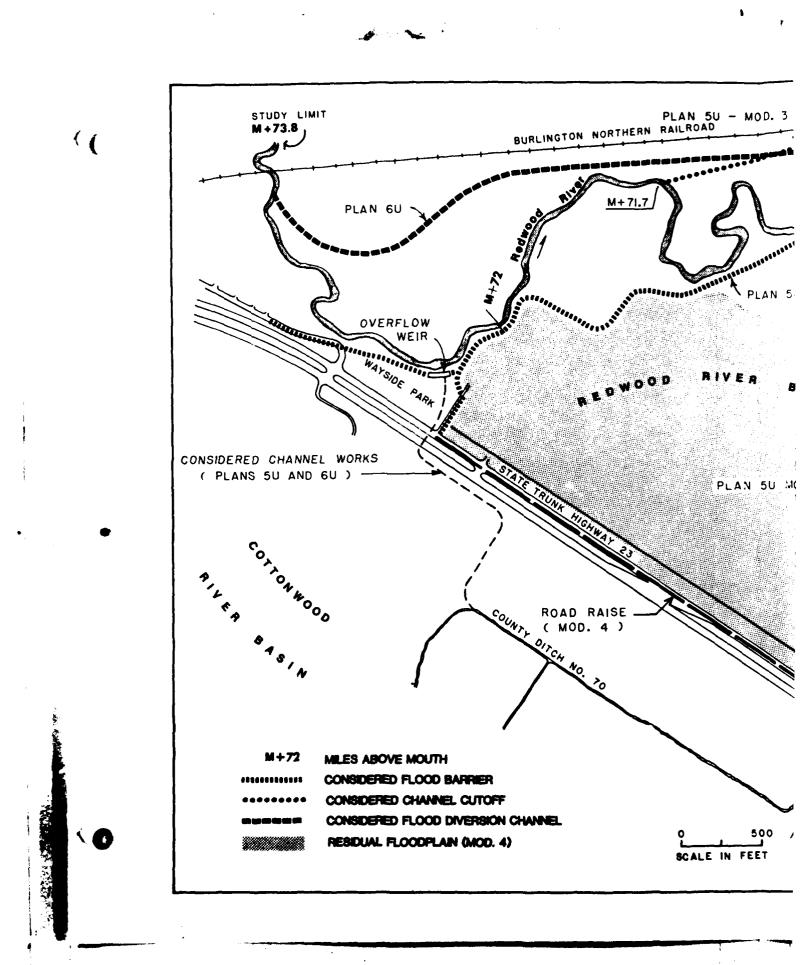
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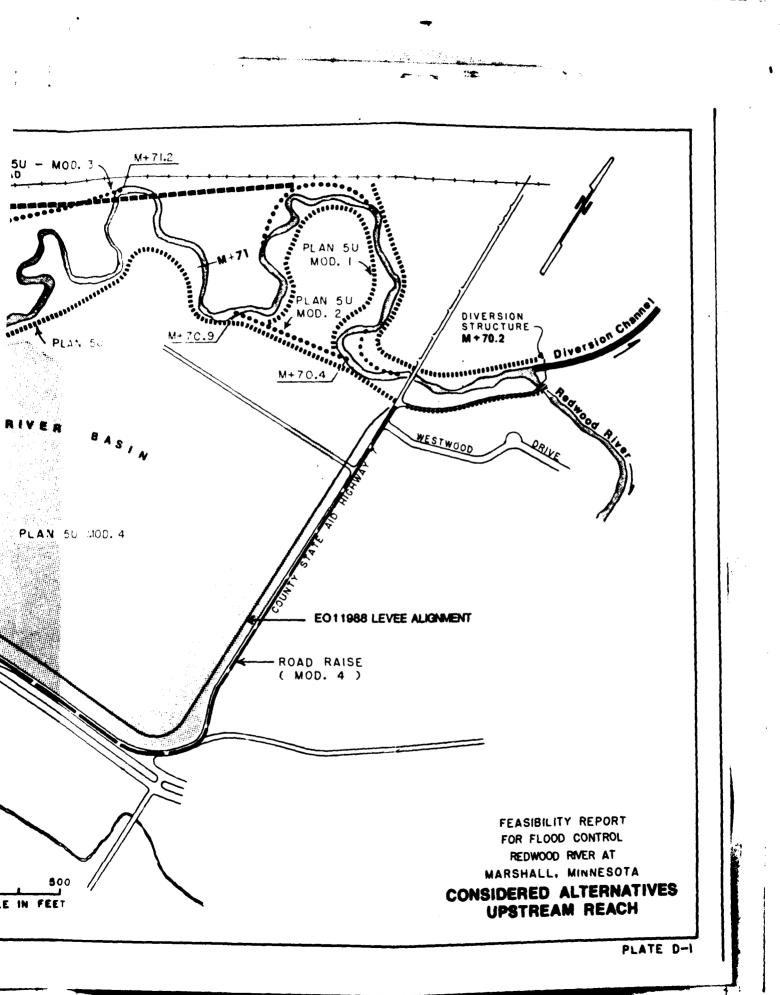
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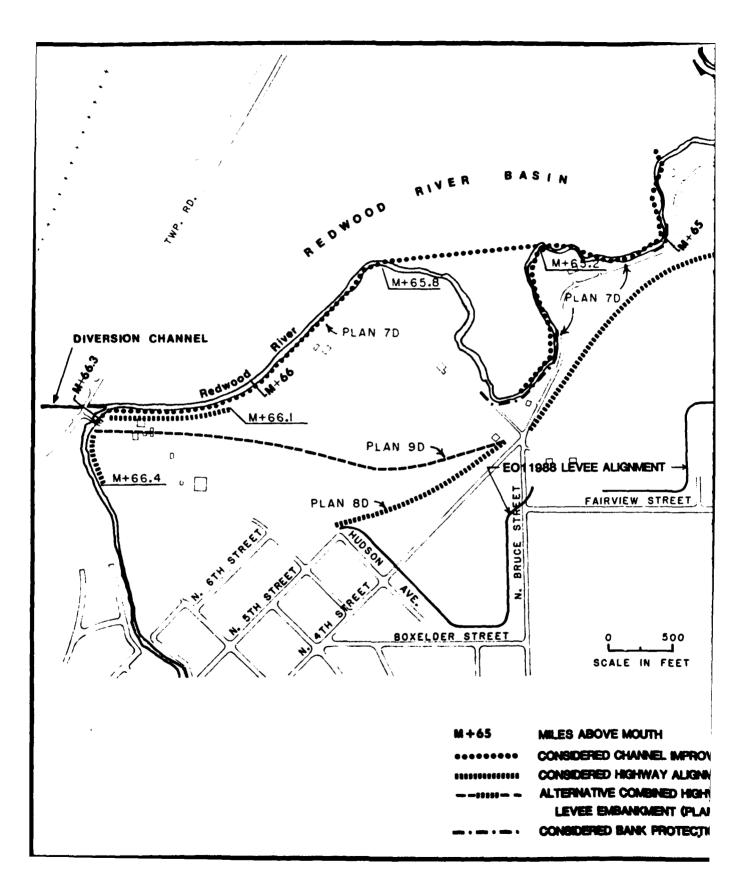
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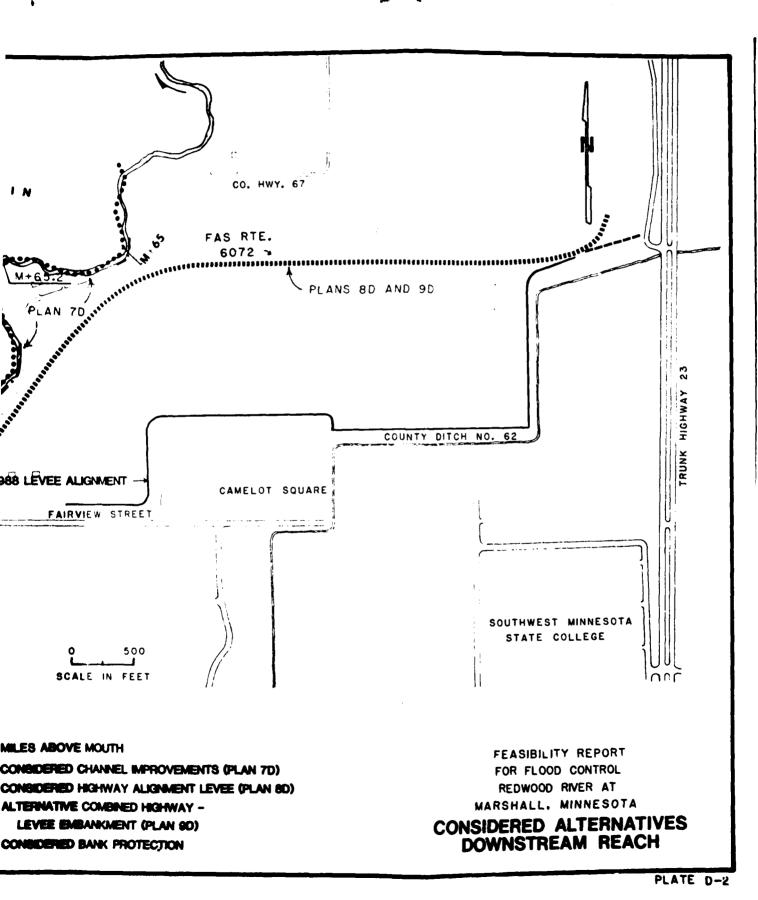
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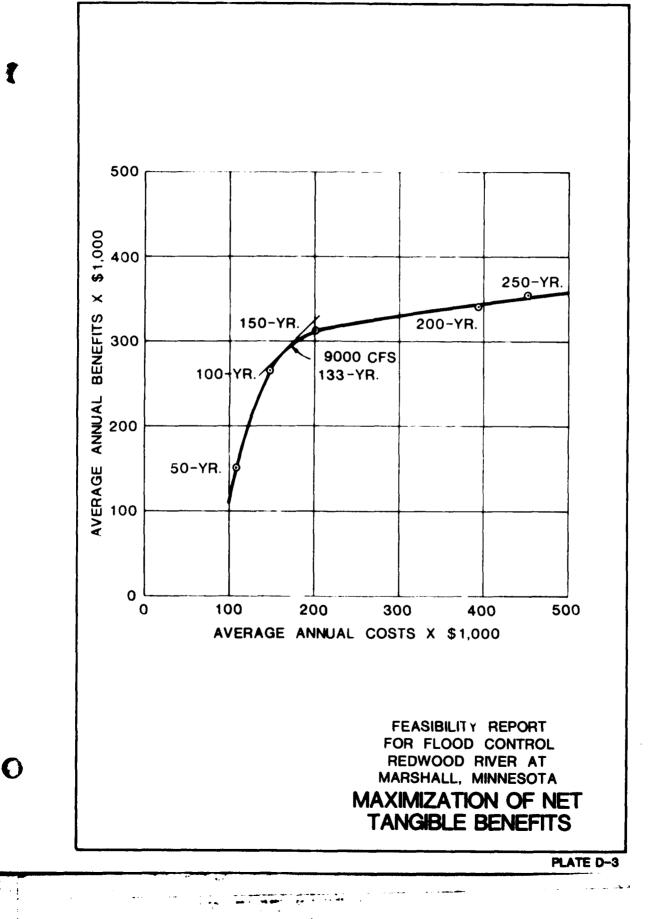
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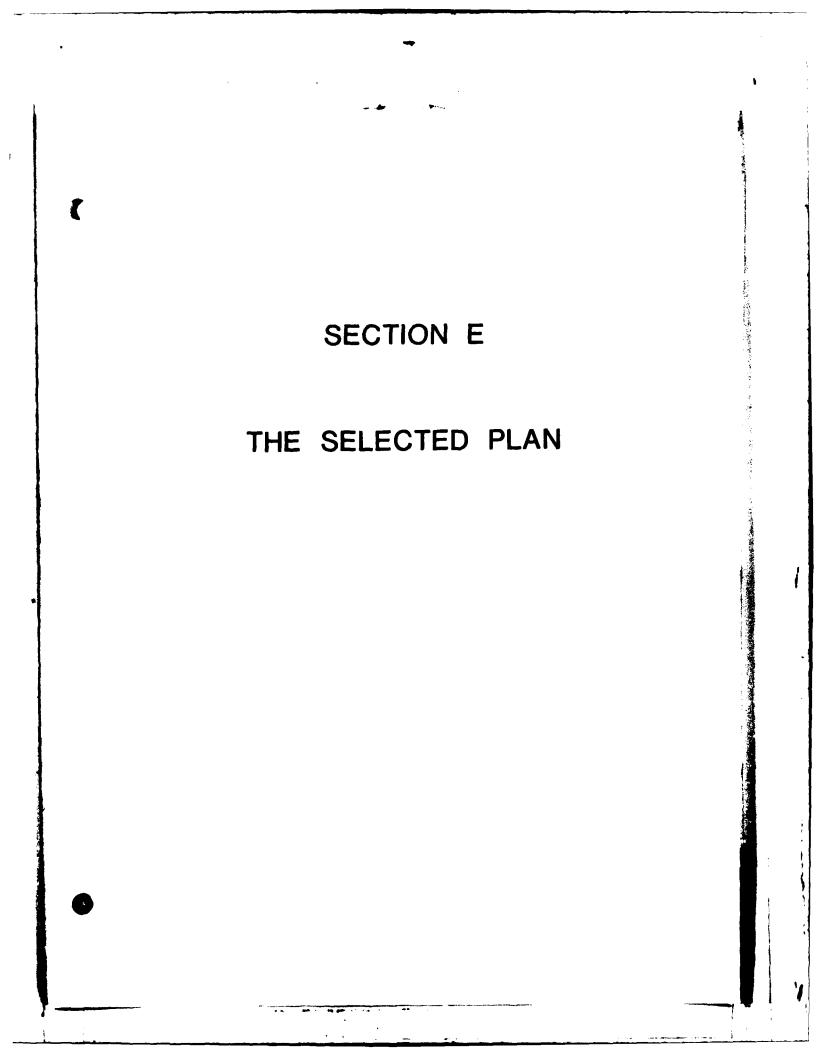
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# SECTION E

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# THE SELECTED PLAN

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## SECTION E

# THE SELECTED PLAN

1. This section of the report describes the plan of improvement as selected in the previous section on formulation. In addition to the basic description, all meaningful effects, both beneficial and adverse, are identified and discussed. Pertinent information concerning design, construction, and operation and maintenance of the plan is also represented to provide the reader with a broader understanding of the technical aspects involved for implementation. Plates E-1 through E-12 show the important features of the selected plan.

# PLAN DESCRIPTION - UPSTREAM REACH

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2. The plan of improvement, selected for assuring effective operation of the existing project and protection of new development along the reach below the confluence of the Redwood River and the diversion channel, is comprised of two parts - that for the upstream reach (river mile 66.3 to 73.8) and that for the downstream reach (river mile 58.3 to 66.3), respectively. Flood barriers for the selected plan are designed (with one exception as discussed in Paragraph 5) to accommodate the 133-year flood with 3 feet of freeboard along both reaches.

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## GENERAL

5. The proposed plan of improvement for the upstream reach consists of levees; channel widening and reshaping; an overflow diversion structure with attendant overflow channel and other works; channel and levee slope protection; minor interior drainage faminities; and utility and building relocations. The plan would also include a recreational trail system, and limited prenicking facilities. Nesthetic and environmental mitigation measures are also provided to offset vegetation and aesthetic losses and help blend the proposed project into the natural setting. Flood plain management measures are proposed for residual flood plain areas. In addition, river and flood forelasting by the National Weather Service, an integral part of the design and operation of levees and other flood control systems and essential for multi-purpose water resource management will continue to be needed.

### LEVEES

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4. The proposed upstream works provide for a 2,260-foot long levee along the left or north bank commencing at the existing diversion structure (mile 70.2) and extending to the Burlington Northern Railroad embankment at the upstream end as shown on plate L-1. The existing left bank levee between stations 0 + 00 and 8 + 60 would require a raise of about seven feet. Levee heights between stations 8 + 60 and 22 + 60 would range from 4 to 7 feet with an average height of 5 feet. The entire levee would have a 10-foot top width except at the widened or warped section between

Appendix I

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station 9 + 00 and 14 + 00. Landward and riverward side slopes would both be 1 on 3 except along the warped levee section. Typical cross-sections for the left bank levee are shown on plate E-6. Also included would be a 1,660-foot long levee between the proposed gabion drop structure and high ground north of the wayside park. Average height would be 4 feet. Pertinent features of this levee are shown on plates E-2 and E-3.

5. The proposed upstream work would also include a 6,350-foot long levee extending along the right bank from the existing diversion structure upstream to high ground at the State Highway 23 embankment in the vicinity of the State wayside park, as shown on plates E-1, E-2 and E-3. Except for a required 3-foot raise of the existing levee between stations 0 + 00 and 9 + 00, and a 3 foot raise of a private driveway between stations 60 + 00 and 63 + 50, levee heights providing three feet of freeboard over the 133-year design flood level would range from 4 to 13 feet with the maximum height over an old channel crossing between stations 48 + 00 and 52 + 00. However, the right bank levee between station 0 + 00and 60 + 00 would be raised to provide two feet of freeboard over the SPF flood level. Both the landward and riverward levee side slopes would be 1 on 3 except along a short reach of residential property immediately upstream of CSAH 7 (station 9 + 40 to 13 + 00), at the access ramp to the area within the large river meander (station 17 + 00) and at two residences between stations 53 + 20 and 58 + 00). The short levee reaches near the three residences would have 1 on 3 riverward slope and an irregular and flattened landward slope to provide for plantings to mitigate tree and other aesthetic losses. The access ramp at station 17 + 00 (section F-F, plate E-7), would have 1 on 6 side slopes and a 10-foot wide compacted gravel surface course to provide easier vehicular movement.

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6. Two temporary sandbag closures would tie the right bank levee into high ground. A 100-foot long closure would tie the road raise at station 63 + 50 into the Highway 23 embankment to divert standard project flood flows into the Cottonwood River basin. A 45-foot

Appendix I E-3 long closure at the upstream end of the road raise west of the wayside park would provide sufficient freeboard to contain the 133year flood.

7. The top width of the right bank levee would be 10 feet except along the existing service drive between stations 0 + 00 and 9 + 00and the driveway between stations 60 + 00 and 63 + 50. Along the service drive, the levee would have 20-foot top width with a 10-foot wide gravel surface course. The raised driveway would have a 12foot top width with an 8-foot wide gravel surface course. Typical cross-sections showing the standard levee sections, irregular sections, and raised road sections are shown on plates E-1, E-6 and E-7.

8. The riverward toe of both the left and right bank levees would be located at least 10 feet from the top of the channel bank except along reaches where the channel bank is to be riprapped and at five areas where existing structures are located close to the river channel. Along these latter areas, the riverward levee slope would represent an upward extension of the riprapped channel side slope. Typical cross-sections illustrating this condition are shown on plate E-6.

## CHANNEL IMPROVEMENTS

9. Proposed channel improvements would include realignment of the river channel between river stations 9 + 40 and 14 + 40 to alleviate a sharp channel bend. The bottom width of the realigned channel would vary from 80 feet at the County State Aid Highway 7 (CSAH 7) bridge to 50 feet at a point approximately 500 feet upstream of the bridge. Other channel works would include widening by excavation

Appendix I

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of one bank only between stations 48 + 00 to 55 + 00 and 106 + 00 to 119 + 60, and channel realignment between stations 97 + 00 to 106 + 00. The channel widening between stations 97 + 00 to 119 + 60 would lower the water surface to that of the existing conditions. Minimum channel bottom widths along these widened reaches would be 50, 45, and 55 feet respectively. Also included would be reshaping and riprapping of 6 channel bends as shown on plates E-1, E-2 and E-3. Typical channel cross-sections are shown on plates E-6 and E-7.

10. The proposed 540-foot long overflow diversion structure would commence at right bank levee station 58 + 90 and extend westward along the Redwood River as shown on plate E-3. This structure would consist of a gabion embankment with a 10-foot top width and 1 vertical on 2.5 horizontal side slopes. The 540-foot long overflow portion of this embankment would have a crest of constant slope with elevations of 1192.64 at the downstream end and 1192.94 at the upstream end. The existing ditch located at the east side of the park would be slopes in the direction of the overflow culverts to pass flood overflows through the State Highway 23 embankment. The overflow structure would commence operation at a river flow of 6,500 cfs and would accommodate up to 50 percent of the excess river flow over 6,500 cfs or a peak flow of 1,260 cfs at the design 133year Redwood River discharge.

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11. The proposed gabion drop structure would be located at river station 97 + 45 (river mile 72.04). The structure would consist of a gabion embankment with a 9-foot grouted crest and 1 vertical on 4 horizontal and 1 vertical on 6 horizontal upstream and downstream side slopes. There would be four 36" R C P culverts to pass low flows. The drop structure would be overtopped at a discharge of 300 cfs, or about every other year on the average.

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12. The proposed 2,140-foot long overflow channel would have a 20-foot bottom width and a channel bottom slope of 0.2 percent between stations 0 + 00 and 12 + 00 and 0.25 percent between stations 12 + 00 and 21 + 40. Channel side slopes would be 1 on 6 and 1 on 4 respectively for the left and right banks for the channel reach along the State Highway 23 right-of-way. Channel slopes downstream of the Highway 23 right-of-way would be 1 on 6 on both sides to permit movement of farm equipment. The overflow channel would join County Ditch No. 70 which ultimately drains into Cottonwood River. Three 115-inch by 72-inch concrete arch culverts would pass the peak design discharge of 1,260 cfs through the State Trunk Highway 23 (T.H. 23) embankment. Typical overflow structure, overflow channel and culvert details are shown on plates E-3 and E-4.

#### BRIDGE PROTECTION

13. Riprap bank and pier protection would be provided at the CSAH 7 bridge. Riprap would be placed over the entire channel section and extend 30 feet upstream and 50 feet downstream of the bridge. Typical cross-sections at this location are shown on plate E-6.

## INTERIOR DRAINAGE

14. Required upstream interior drainage works would include modification of the State Highway 23 drainage system at the wayside park, installation of flap gates on two double 30-inch railroad culverts,

Appendix I E-6 an 18-inch flap-gated culvert at station 10 + 00 of the left bank levee, installation of a flap-gate on an existing driveway culvert at station 63 + 50, and installation of a 12-inch C M P culvert through a driveway at right bank levee station 11 + 20. Modification of the State Highway 23 drainage system would include installation of a 10-foot wide parabolic channel leading to the overflow structure, and a flap-gated 36-inch reinforced concrete culvert through the structure.

The land area drained by the culverts is, in all instances, very small (less than 2.5 acres) or the land slopes away from the levees. Thus, installation of the flap gates would not create any adverse effects. Minor landscaping measures would also be accomplished at right bank levee station 27 + 00 to fill a low area adjacent to the proposed levee. Typical details for the upstream reach interior drainage facilities are shown on plates E-4 and E-8.

#### SPOIL DISPOSAL

15. The proposed upstream channel works would require the excavation of approximately 61,125 cubic yards of material. Of this amount, 44,590 cubic yards would be used as embankment fill. Two small disposal areas would be located on the left channel bank at station 30 + 00 and 48 + 00 to accommodate waste material not easily accessible to the levee works. The 0.2-acre and 0.5-acre areas would contain a total of 4,520 cubic yards of spoil material to a maximum depth of about 4 feet. Spoil bank levees would be bulldozed at each location to prevent return of the excavated material to the channel. The remaining 12,015 cubic yards of material obtained from the channel works would be trucked from the area to the existing

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spoil area on the left bank of the existing diversion channel. Surface material stripped from the levee alignment and accessible channcl bank areas would be stockpiled and re-used as topsoil.

16. Of the 26,775 cubic yards of material to be excavated from the overflow channel, approximately 6,180 cubic yards would be used as random backfill or fill for the overflow structure. An additional 16,735 cubic yards of waste material would also be stockpiled for subsequent city re-use at the existing diversion channel spoil bank area.

#### RELOCATIONS

17. The proposed upstream levee overflow works, and channel improvements would require the acquisition of an estimated 22.8 acres of land, temporary construction easements along two private driveways and one other property, relocation of one house, 500 lineal feet of overhead line, temporary relocation of 700 feet of buried utility cable, and relocation of about 550 feet of farm fencing. Placement of the culverts through the four-lane T.H. 23 would require construction of a temporary by-pass across the median to permit two-way traffic during project construction. The extent and locations of required relocations are shown on plates E-1 and E-3.

#### AESTHETIC TREATMENT MEASURES

18. Aesthetic treatment measures would be provided at various locations along the left and right bank levees to lessen the adverse

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effects of levee construction near residential structures. Excluding riprapped areas, all disturbed areas would be reseeded with native vegetation or other ground cover such as wheat grass or sweet clover. Other measures would include tree and shrub planting and warped or enlarged levee sections with irregular landward slopes to blend the levees into the natural topography. The plantings on or near the enlarged landward slope would partially offset the loss of existing tree and shrub growth and soften the visual effects of the flood barriers at affected residences.

19. In addition to the proposed structural measures, flood plain management measures (principally zoning) would be utilized in managing residual flood plain areas riverward of the levees to preclude flood prone development in these areas. An additional 71.1 acres of flood plain lands located between the proposed right bank levee and the Burlington Northern (BN) Railroad embankment and extending from CSAH 7 upstream to the BN railroad bridge (mile 72.6) would be purchased to insure preservation of the area as a floodway.

# DOWNSTREAM REACH

#### GENERAL

20. Proposed flood control improvements along the downstream river reach would include levees, channel improvements, channel slope protection, interior drainage facilities, flood plain management measures, and beautification measures.

#### LEVEES

21. The proposed downstream works would provide for a 7,670-foot long levee commencing at high ground near the State Highway 23 embankment and extending to high ground at 5th Street and Hudson Avenue as shown on plates E-9, E-10, and E-11. The levee would have a 10-foot top width and 1 on 3 riverward and landward side slopes. Levee heights would range from 3 to 10 feet with an average height of 5 feet. A 450-foot long levee would also be required along the right bank of the river just upstream of its confluence with the diversion channel as shown on plate E-11. With the same typical cross-section as the longer levee, average levee height would be 2.0 feet. A low 2.0-foot high levee would be required to bridge a low channel bank reach between river stations 0 + 00 and 9 + 00. A 2-foot high by 100-foot long temporary sandbag closure across County Highway 67 would be required to maintain a continuous 3foot freeboard allowance over the design 133-year flood. Typical cross-sections for these levees are shown on plate E-12.

#### CHANNEL IMPROVEMENTS

22. Proposed downstream channel improvements would include widening of the river channel bottom to approximately 35 feet by excavation of only the right bank between river stations 0 + 00 and 13 + 50. Riprap slope protection would be provided along the entire widened bank. Riprapped side slopes would be 1 on 3. Typical channel cross-sections are also shown on plate E-12.

#### INTERIOR DRAINAGE

23. Required downstream interior drainage facilities would include a 7-acre ponding area at station 27 + 00, a collector ditch along the levee toe, and a 24-inch diameter drainage conduit with appurtenant works leading to County Ditch No. 62. Two 24-inch diameter R C P culverts would pass collector ditch flows through the County Highway 67 embankment. The ponding area would be excavated to elevation 1134.0 for an average depth of about 4 feet. Removal of ponded peak design runoff is estimated to take about 2 days. A plan view and typical section for required downstream interior drainage works are shown on plates E-9 and E-12. The contributing interior drainage area is shown on plates E-9 and E-10.

#### SPOIL DISPOSAL

24. The proposed downstream channel works would require the excavation of 6,390 cubic yards of material. Of this material, approximately 1,700 cubic yards would be used as channel bank levee fill, the remaining material to be placed on available City-owned property

on the right channel bank near river station 10 + 00. Of the 47,700 cubic yards of material excavated from the ponding area and collector ditches, 34,100 cubic yards would be used as levee fill. The remaining material would be used to fill a low area along the collector ditch, a partially filled oxbow on municipal property, and two low areas adjacent to the ponding area as shown on plates E-9 and E-11. Topsoil stripped from the ponding area and ditches would be stockpiled for replacement on disturbed areas.

#### RELOCATIONS.

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25. Relocations would be limited to the relocation of 900 lineal feet of overhead utility line along the channel bank levee alignment.

26. Alternative alignments to the proposed flood barrier alignments ...ere evaluated to minimize impacts on study area wetlands. These alternative are discussed in Section J of this Appendix.

#### RECREATIONAL FACILITIES

27. Proposed recreational facilities would include a 5.7 mile long multi-use recreational trail system with rest and observation areas extending from State Highway 23 at the downstream end of the proposed project upstream to the Highway 23 wayside park and limited picnic facilities in conjunction with the levee works at Justice Park and the existing softball complex north of State Highway 19.  $\lambda$  0.6-mile section of the trail system between State Highway 19 and CSAH 7 is expected to be completed by the City prior to any construction of proposed project features.

A 0.3-mile section of trail upstream of County Highway 67 (Plate G-2) would be completed by the City concurrent with the construction of any authorized recreational trail facilities. Future development to be provided by the City might include the development of a quiet and nature educational area in the wooded flood plain area upstream of CSAH 7, an improved canoe access at or near the State Highway 23 wayside park, and additional facilities at Justice Park. Plan views and pertinent area sections for the proposed recreational facilities are shown on Plates G-1, G-2, and G-3.

> Appendix I E-12a

#### AESTHETIC TREATMENT MEASURES

28. Downstream reach aesthetic treatment measures would consist of reseeding all disturbed areas with suitable ground cover species. Actual grass mixes would be determined during preparation of final project plans and specifications.

### PLAN ACCOMPLISHMENTS

29. The major accomplishments resulting from the selected plan of improvement would be the improved operation of the existing flood control project and protection of downstream reach development not protected by the existing project. The proposed improvements would eliminate damaging overbank flows up to the 133-year design discharge. Flood flows in excess of the existing design discharge of 6,500 cfs would be equally passed downstream through the existing project and through the upstream overflow diversion works into the Cottonwood River basin. The overflow works would reduce the frequency and magnitude of floodwaters into the Cottonwood River basin resulting from cross flow from the Redwood River about 43 percent at the 133-year design flood level and 26 percent at the standard project flood discharge.

30. The elimination of most present and future flood damages at Marshall would not only enhance the economic development and stability of the City, but would also enhance the social well-being

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of the affected people. Specifically, the plan would provide for efficient operation of the existing project to provide protection against a flood with a 0.75 percent chance of occurring in any given year and provide flood protection and related security to most of the unprotected downstream development, including the facilities of the Southwest State College at Marshall. The plan would also significantly satisfy the demand for new, expanded or improved outdoor recreational facilities. Thus, the proposed plan accomplishes the study purpose and desired improvements as expressed by the City of Marshall and Lyon County.

# EFFECT ON THE ENVIRONMENT

31. The selected plan would likely facilitate on-going changes in land use in the flood plain. Approximately 120 acres of tilled agricultural land and over 100 acres of undeveloped and partially developed vacant land in the upstream reach would probably be developed as single family or multiple family dwelling units. Similarly, and in accordance with established zoning classifications, a large portion of the vacant land along the downstream reach may be developed into an expanded trailer park and residential dwelling units. Protected flood plain property owned by the College would likely be developed by the College as the need for additional building and outdoor facilities arose.

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32. The selected plan of improvement would have both temporary and permanent effects on the natural environment. Temporary adverse effects would include: increased turbidity and sedimentation during and for a short time after construction with association effects on the very limited area fishery, benthos populations; the minor

long-term loss of native ground cover on disturbed levee and channel bank areas with associated losses and shifts in small mammal habitat; increased noise levels during construction and slightly reduced air quality during construction due to increased levels of dust and fuel combustion products. Stream water quality would be temporarily worsened due to increased turbidity and sediment levels, particularly as a result of the channel works.

53. Provisions would be made in final designs and specifications for appropriate spoil disposal, debris burning, runoff and other pollution control measures and construction inspection procedures to minimize adverse effects. Construction would be scheduled to provide the least impact on nesting waterfowl and other bird life. Mitigation of temporary vegetative losses would be accomplished by reseeding of disturbed areas with grass species native to the area.

34. Relatively permanent environmental effects would include the loss of a total of about 4.2 acres of trees and brush cover along principally the upstream reach, including about 80 mature trees along the upstream reach, the commitment of an additional 119.8 acres of land in the Marshall area for flood control purposes, and the commitment of materials, primarily earth fill, rock riprap, and fuel for project construction. Of the mature trees removed near widely separated upstream residences, few could be replaced in size or location over the 50-year project life. These trees serve as shade trees, landscaping enhancements and provide valuable shelter and resting areas for area bird life. This tree loss would be partially offset with replanting of similar but much smaller trees and shrubs on warped levee sections or as near as possible to the levee while still providing access for project maintenance.

35. Other tree and understory cover loss represents a relatively minor extension of a large expanse of woodlands located a short distance upstream. Species of trees lost, primarily elm, green ash, cottonwood, willow, and bur oak, are commonly found in the adjacent flood plain areas and in the protected woodland of Camden State Park located about 8 miles upstream of the project area. Water quality would probably be improved in the long-term due to the proposed bank stabilization measures. The purchase of 71.1 acres of flood plain lands upstream of CSAH 7 for floodway purposes would maintain the natural characteristics of the area.

36. Research at local libraries, the Marshall and Lyon County historical centers, and the Southwest State College at Marshall indicate that no known architecturally, historically or archeologically significant resources are present in the project area. Unknown buried resources may be present in the project area, and if uncovered during project construction, would be preserved, relocated or otherwise disposed of in an acceptable manner. Recent contacts with the State Historical Preservation Officer indicate that no sites on or eligible for the National Register of Historical Places are evident in the project area.

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# OTHER EFFECTS

37. The selected plan, without appropriate mitigation measures, would have permanent adverse aesthetic effects due to tree and shrub losses at localized areas, particularly just upstream of CSAH 7. In a few instances, the levees would either block or detract from the present view of the river. These effects would be

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at least partially offset by the proposed landscaping, tree and shrub planting and reseeding measures.

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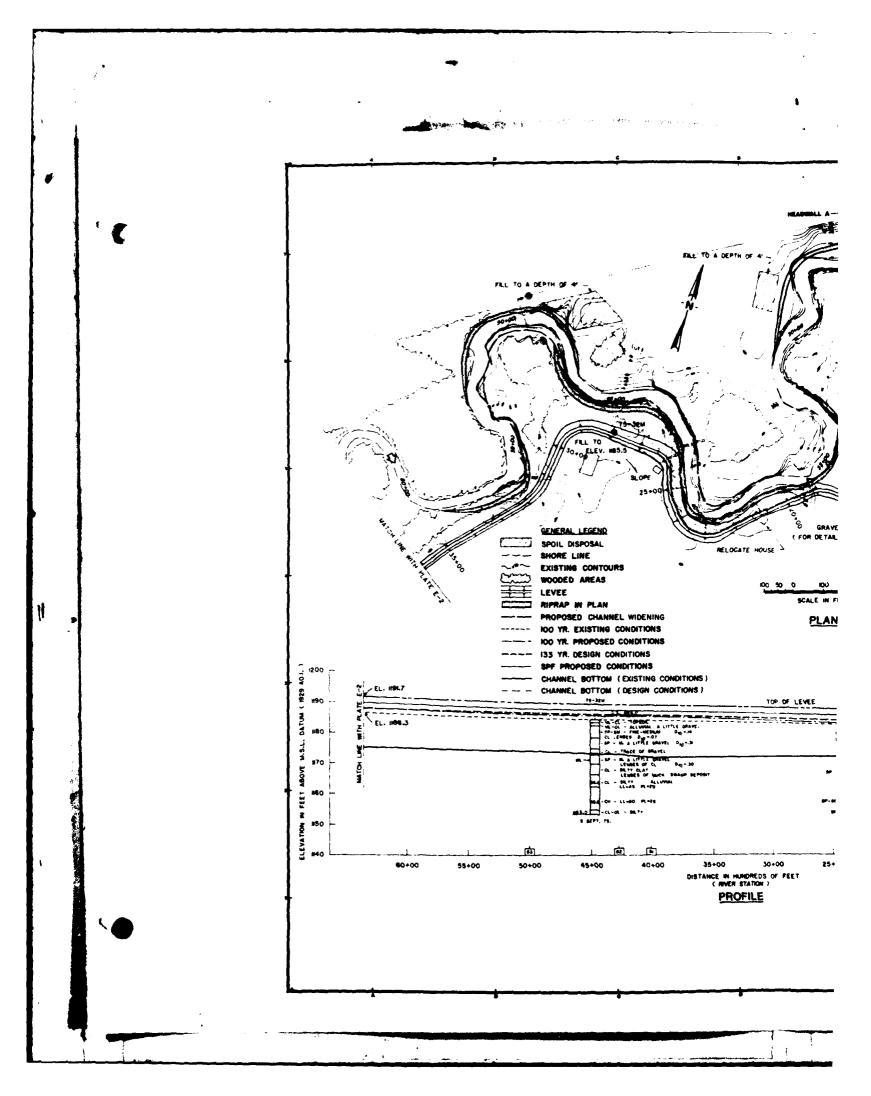
33. Vehicular traffic on T.H. 23 would be inconvenienced for a period of about one month due to placement of the overflow channel culverts. Traffic on CSAH 67 and No. Bruce Street would be inconvenienced for a few days during placement of the collector ditch culverts. Similarly, agricultural activities along both the project reaches would be affected for two seasons due to the levee construction.

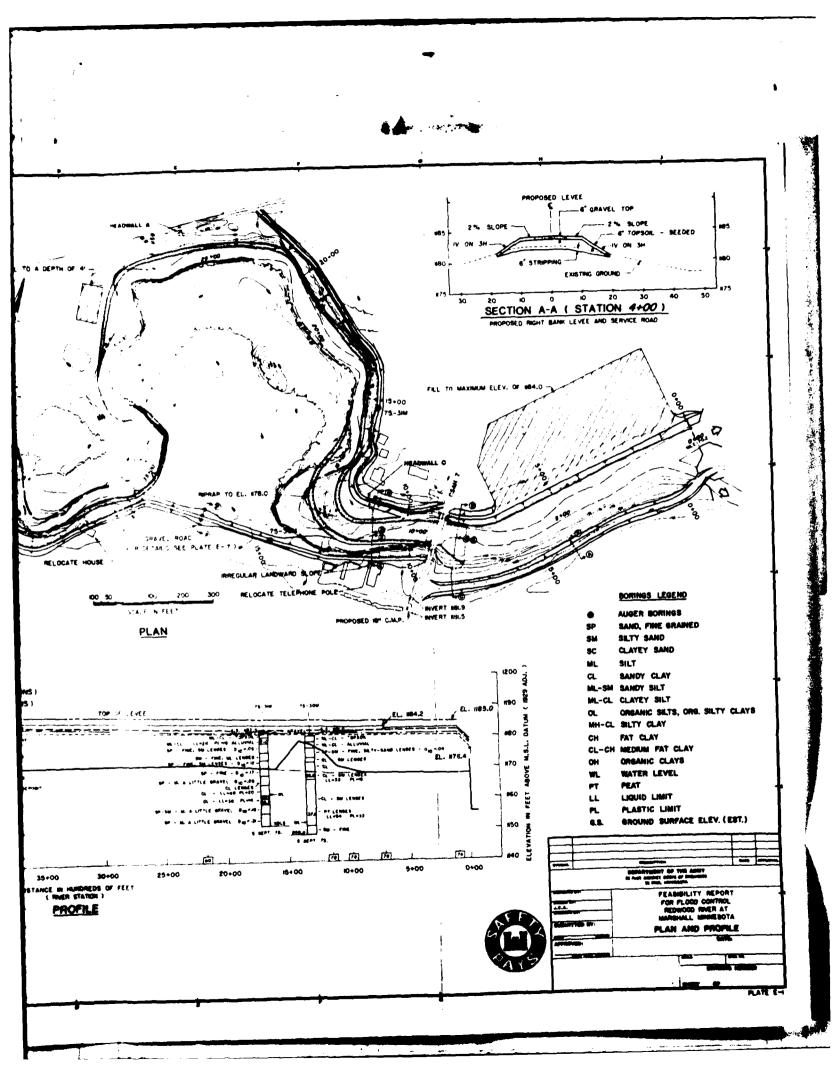
39. The selected plan would reduce future flood damages at Marshall, thus stabilizing, preserving, and enhancing the economic stability of the area, community development patterns, and the general security and social well-being of the affected people. The plan, if implemented, would nearly negate the need, as in 1969, for the periodic and inefficient commitment of local financial, manpower, and material resources for emergency flood fight activities.

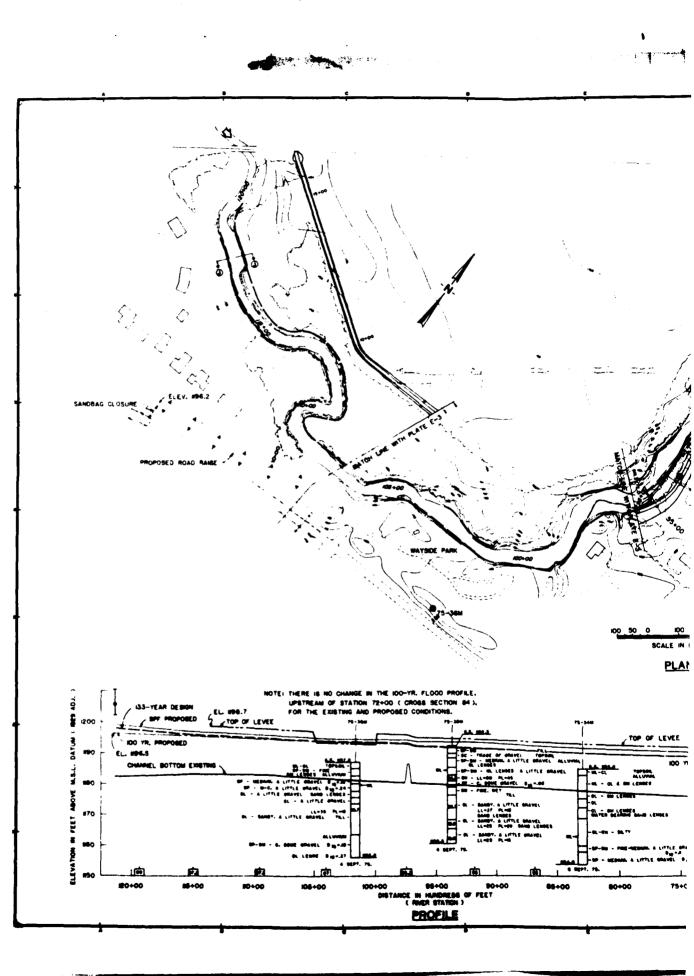
40. The completed overflow diversion structure and channel would provide an attractive extension of the wayside park. Structure slopes would be gradual enough to permit free pedestrian access.

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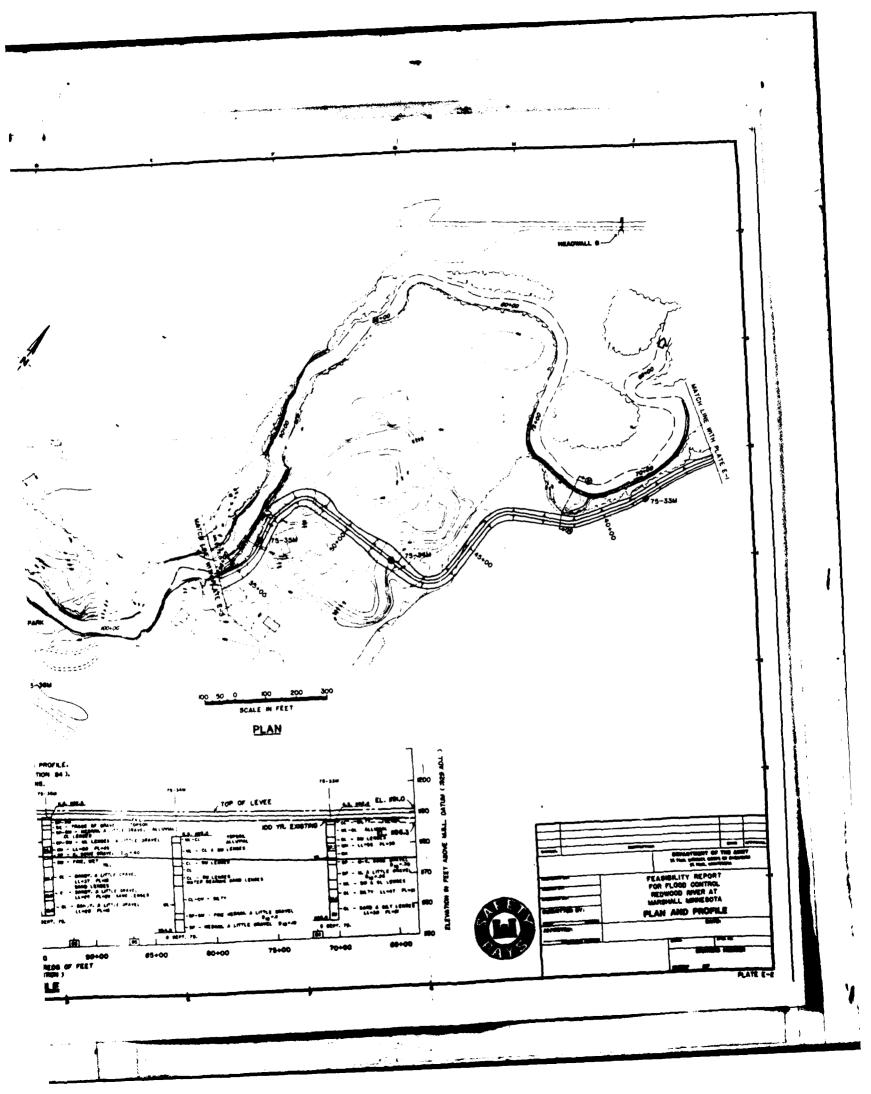
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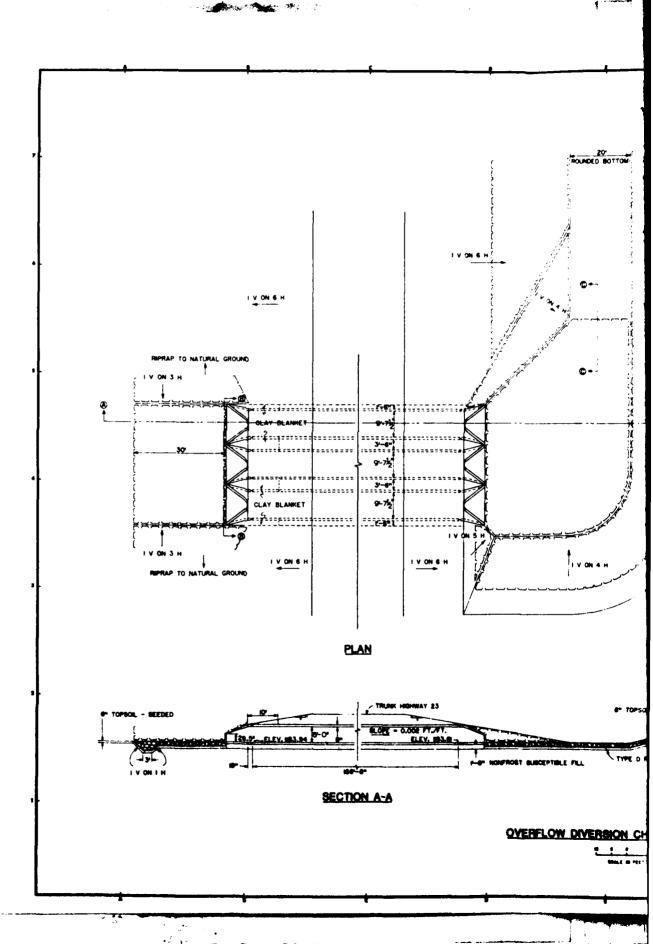






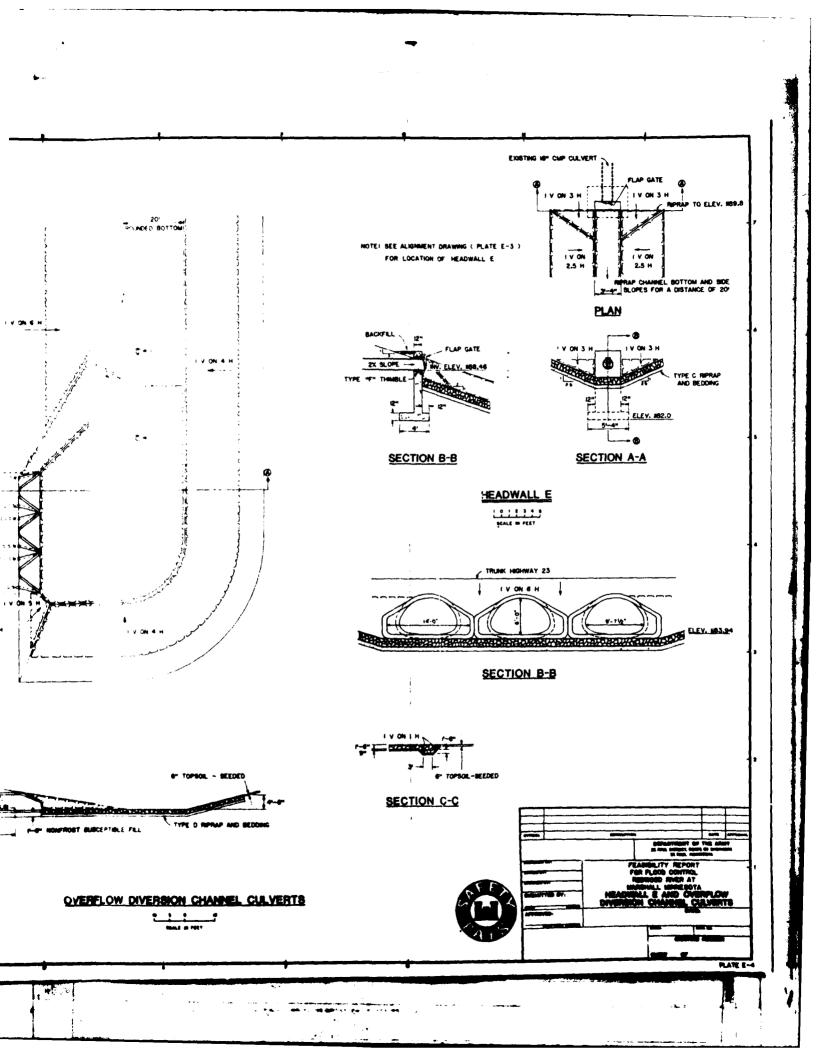
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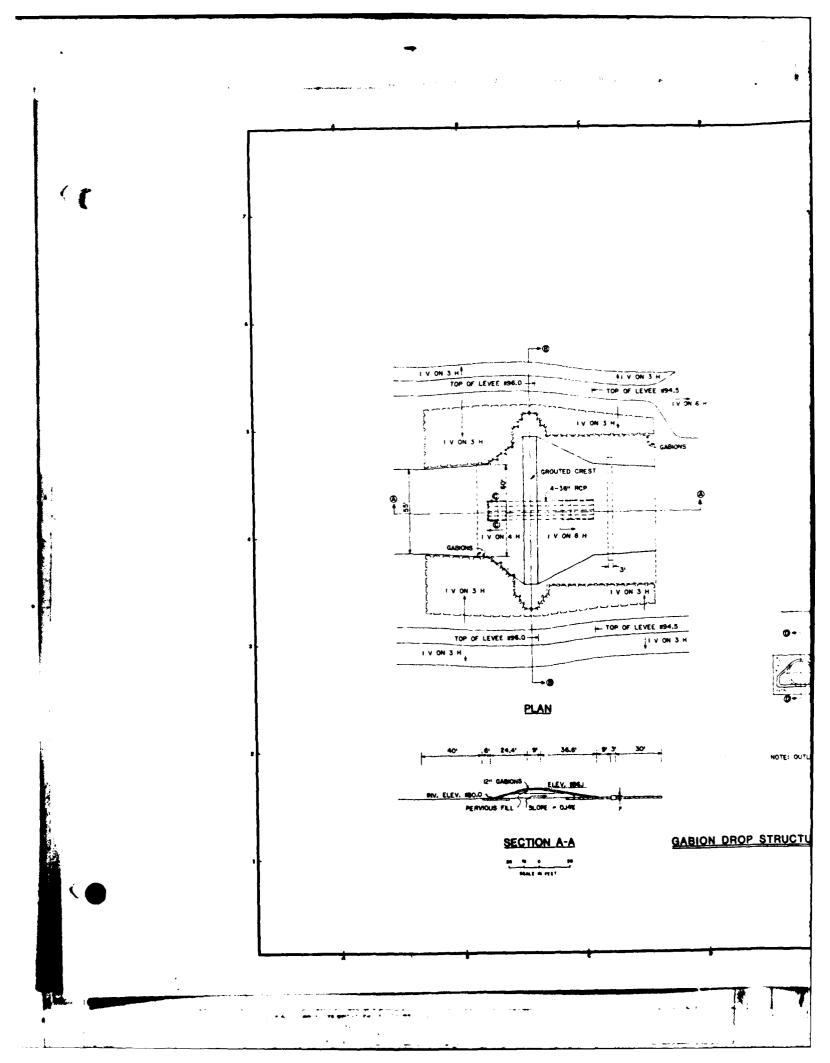


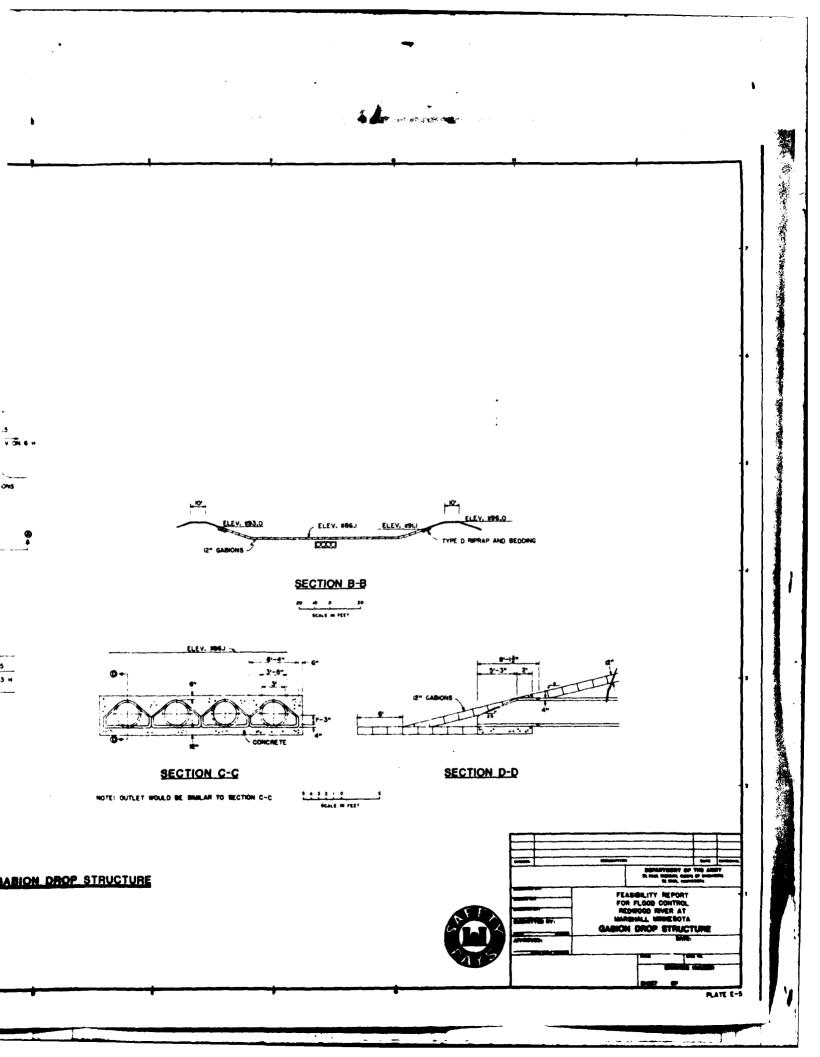


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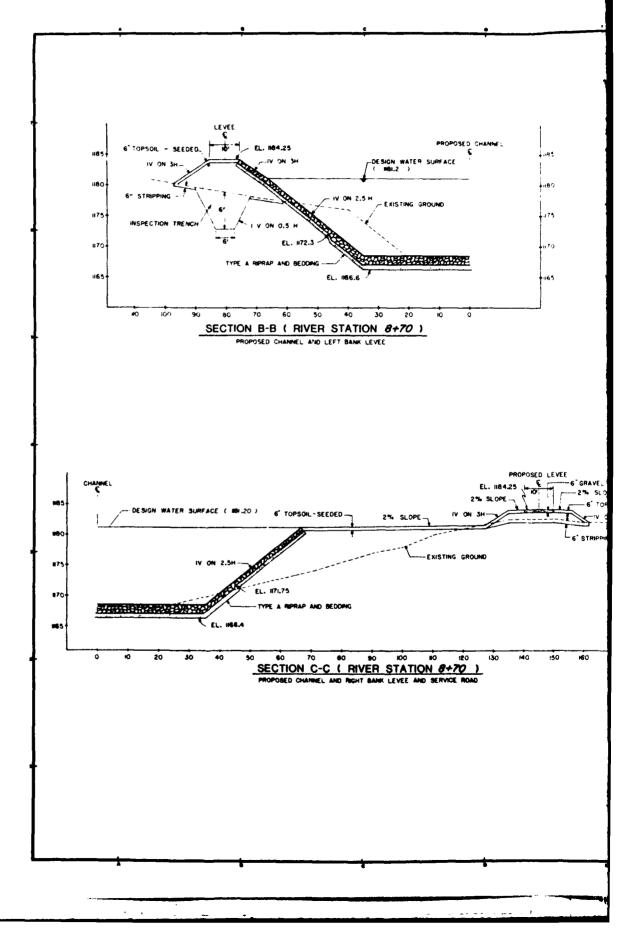


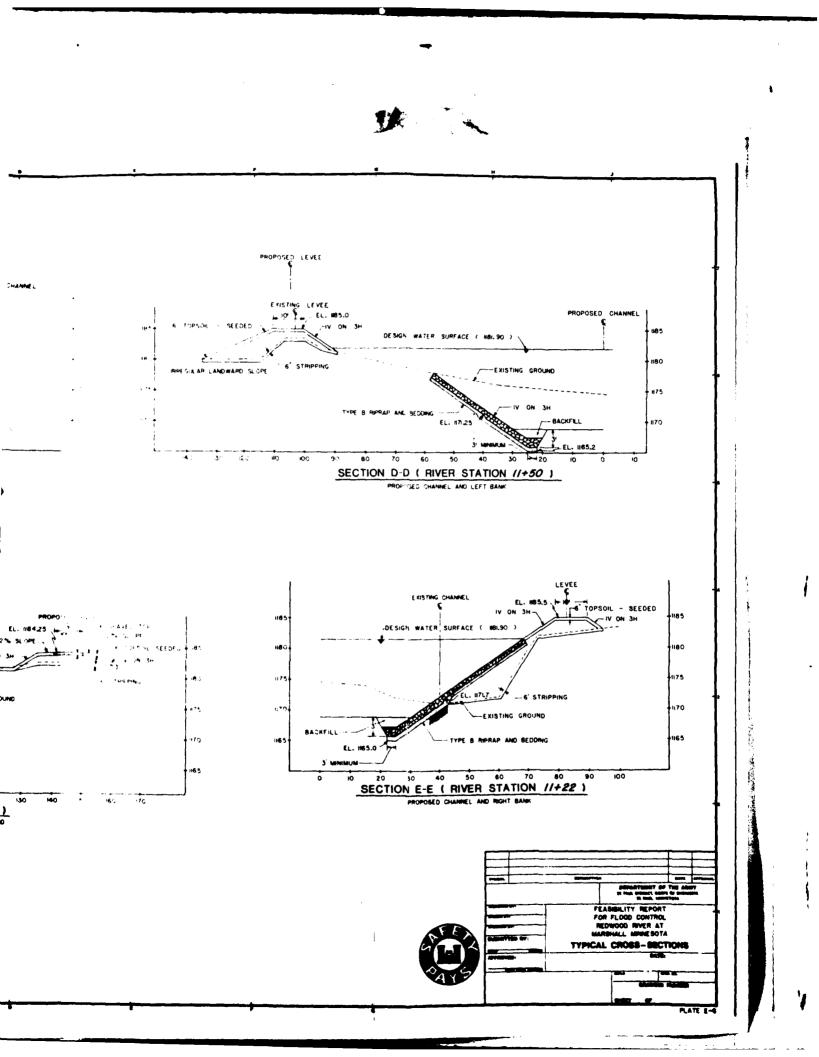


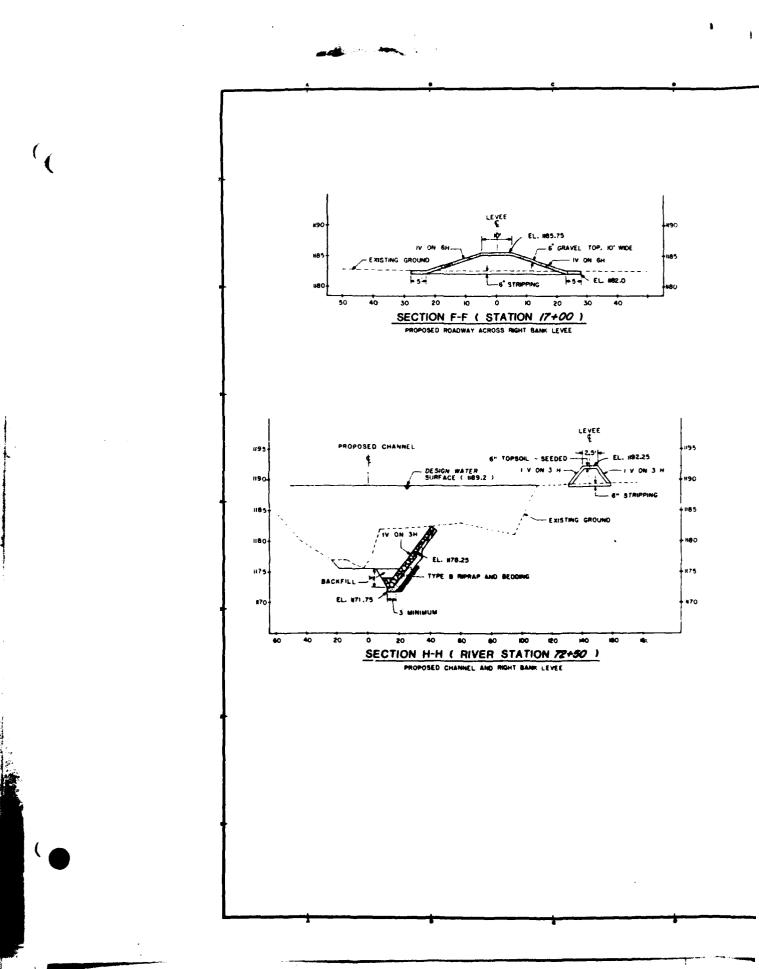


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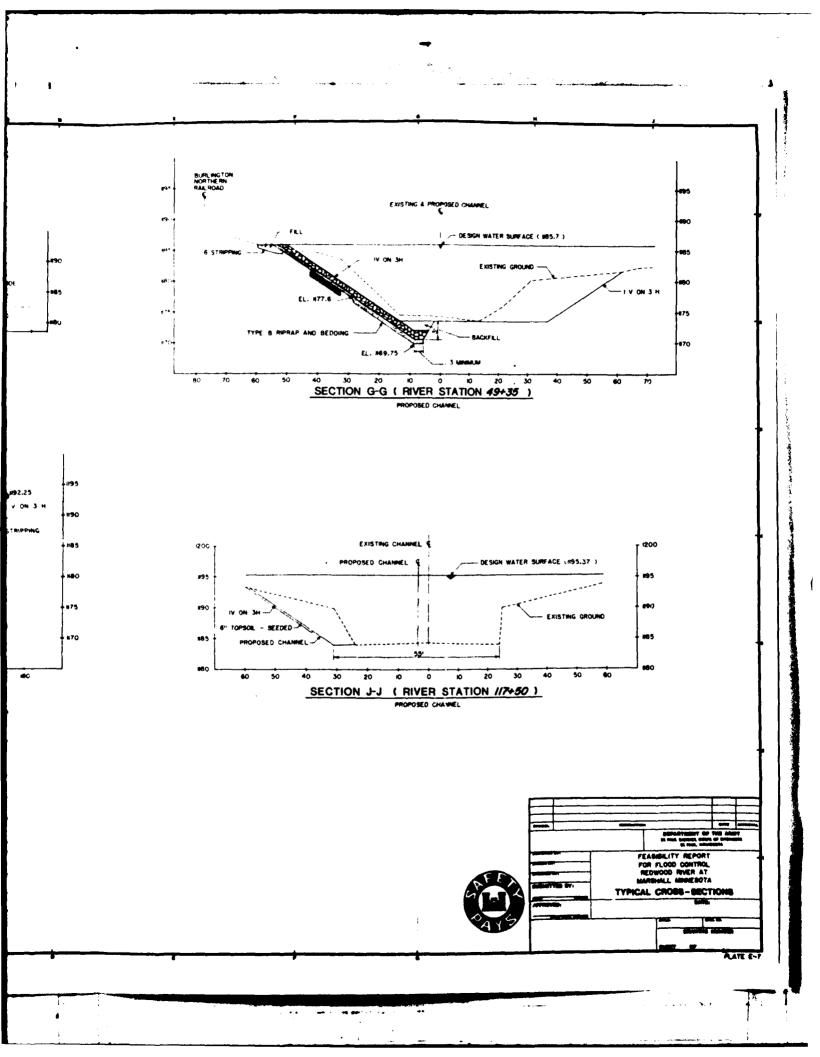
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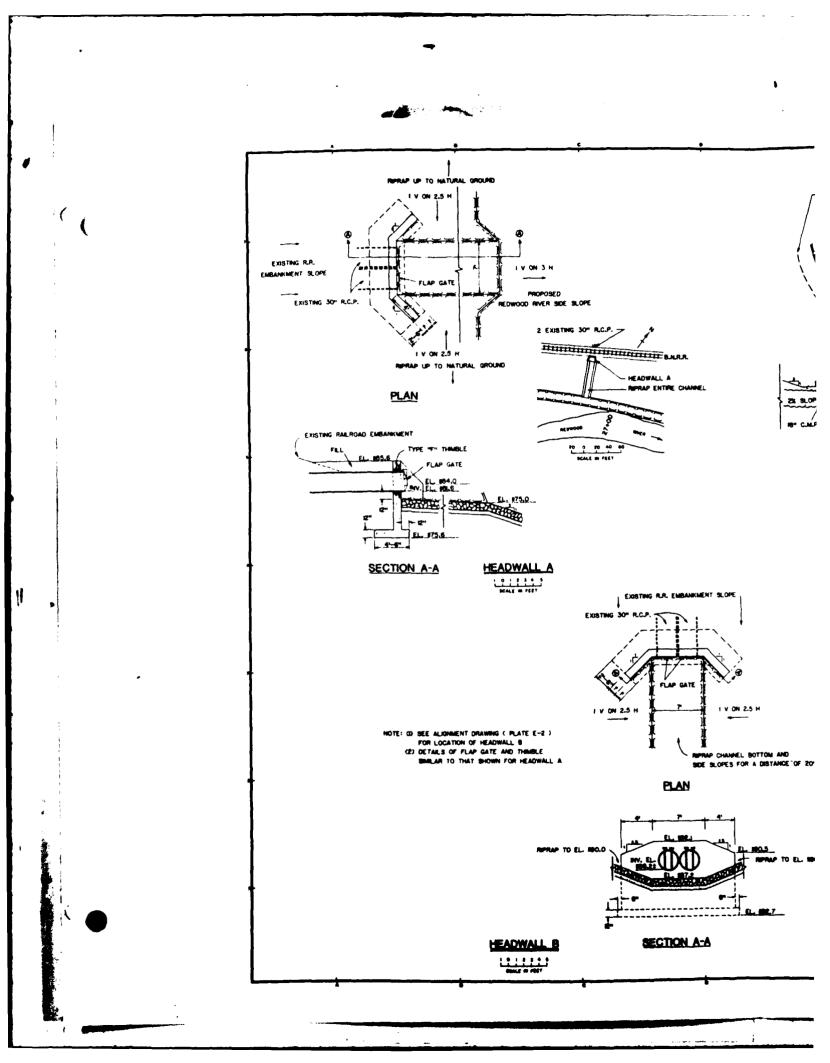


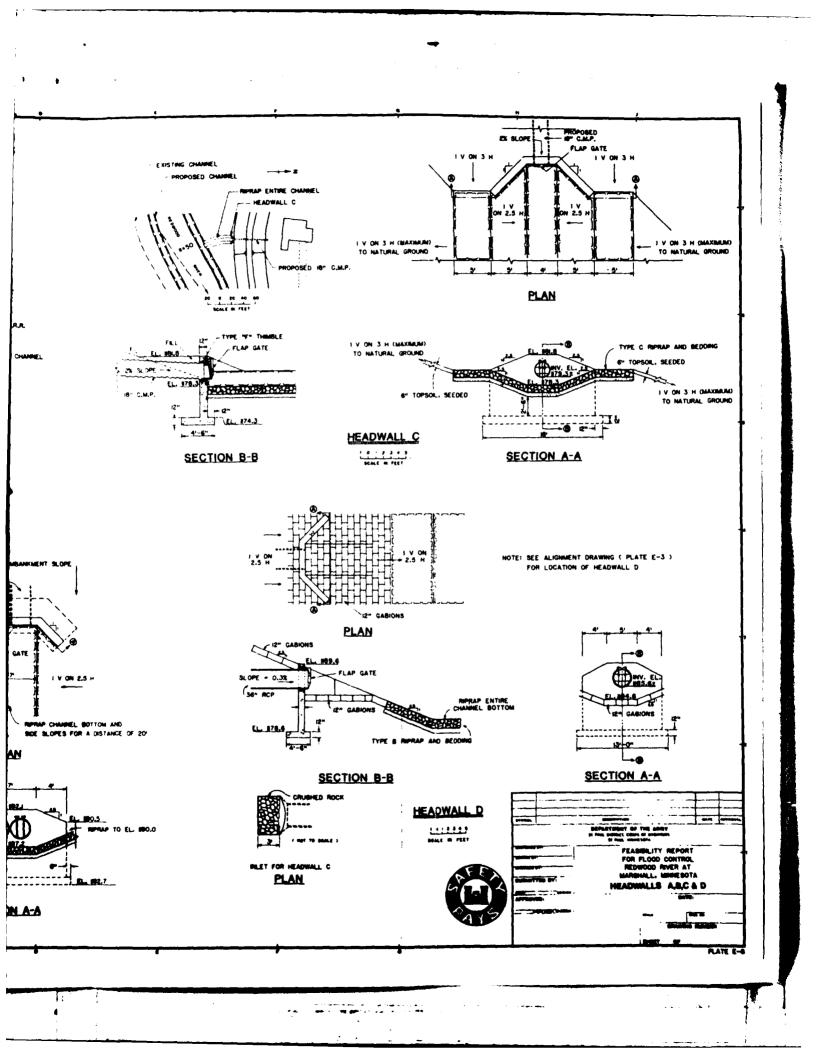


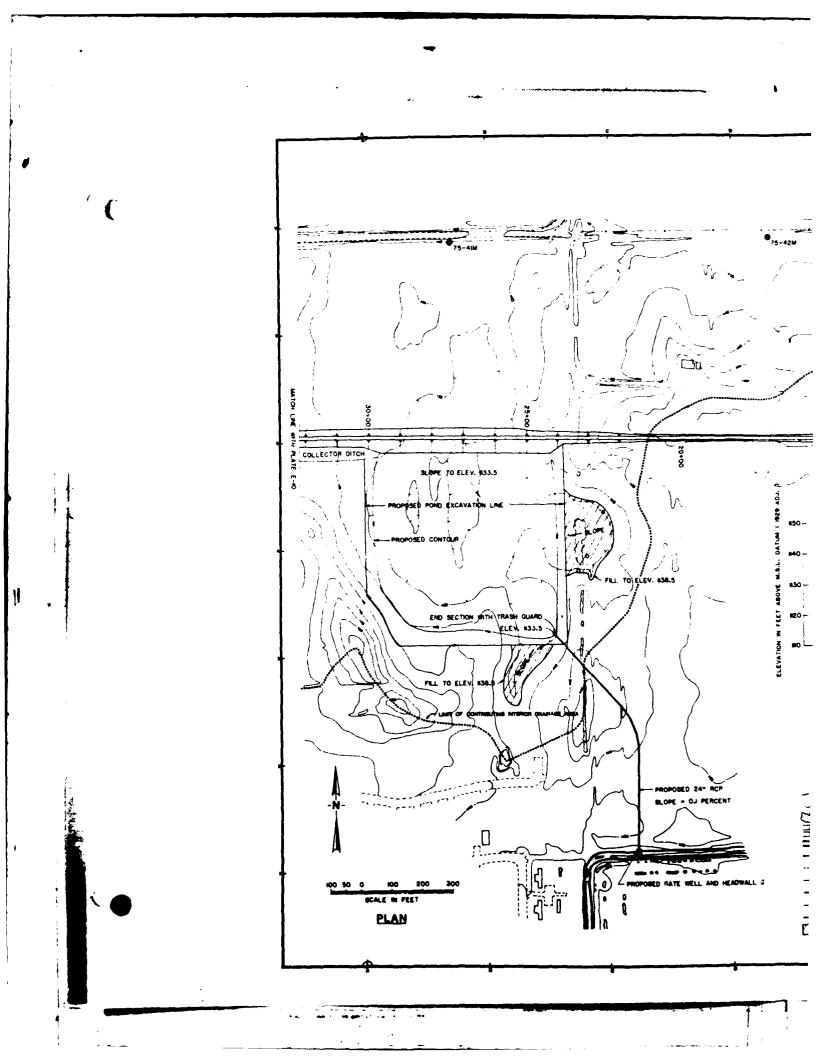


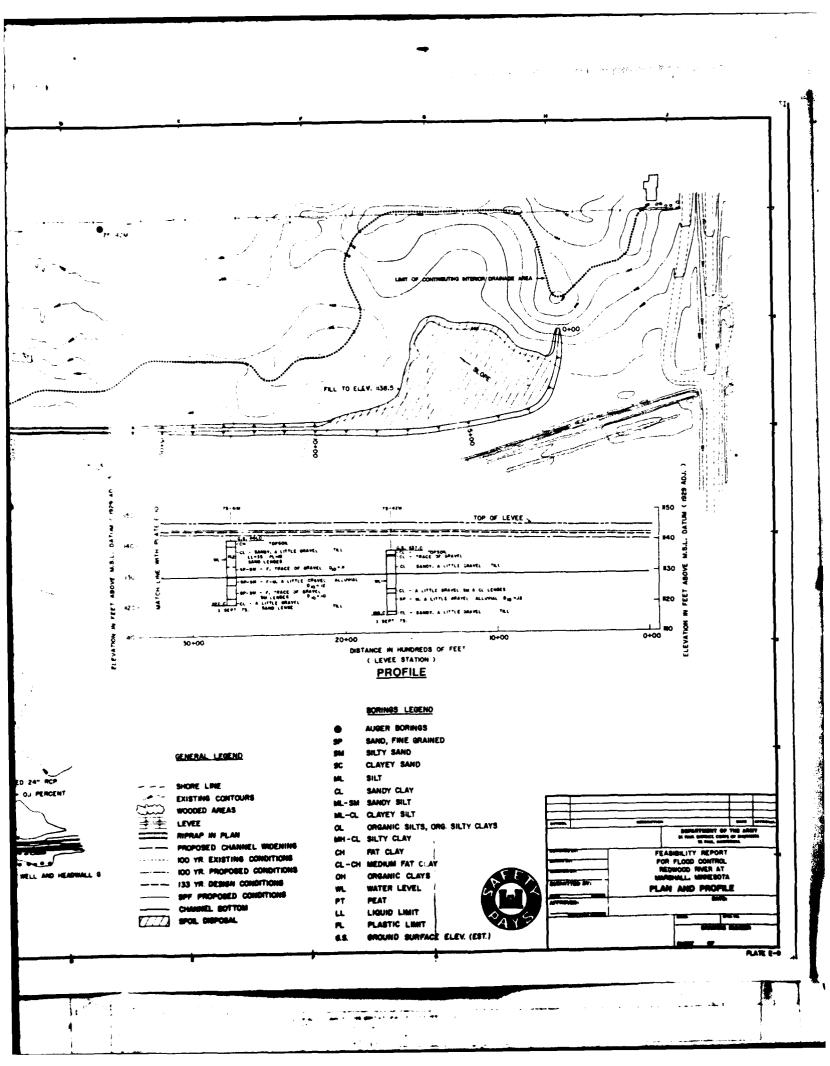
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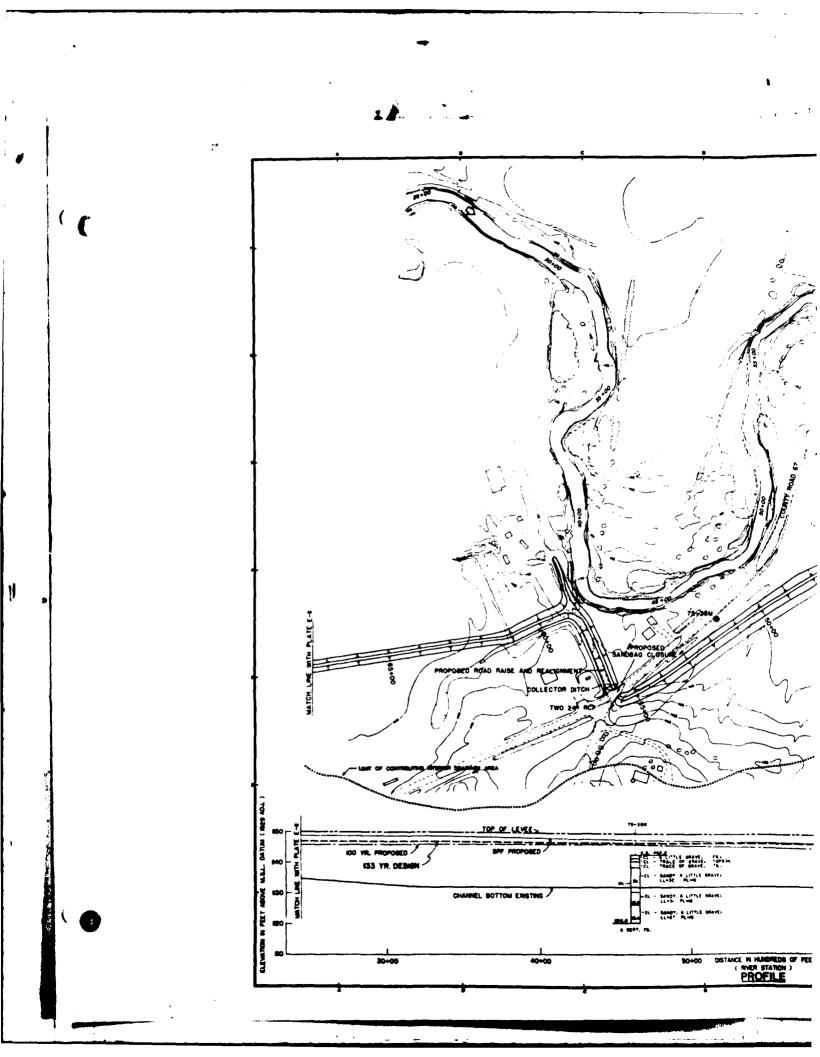


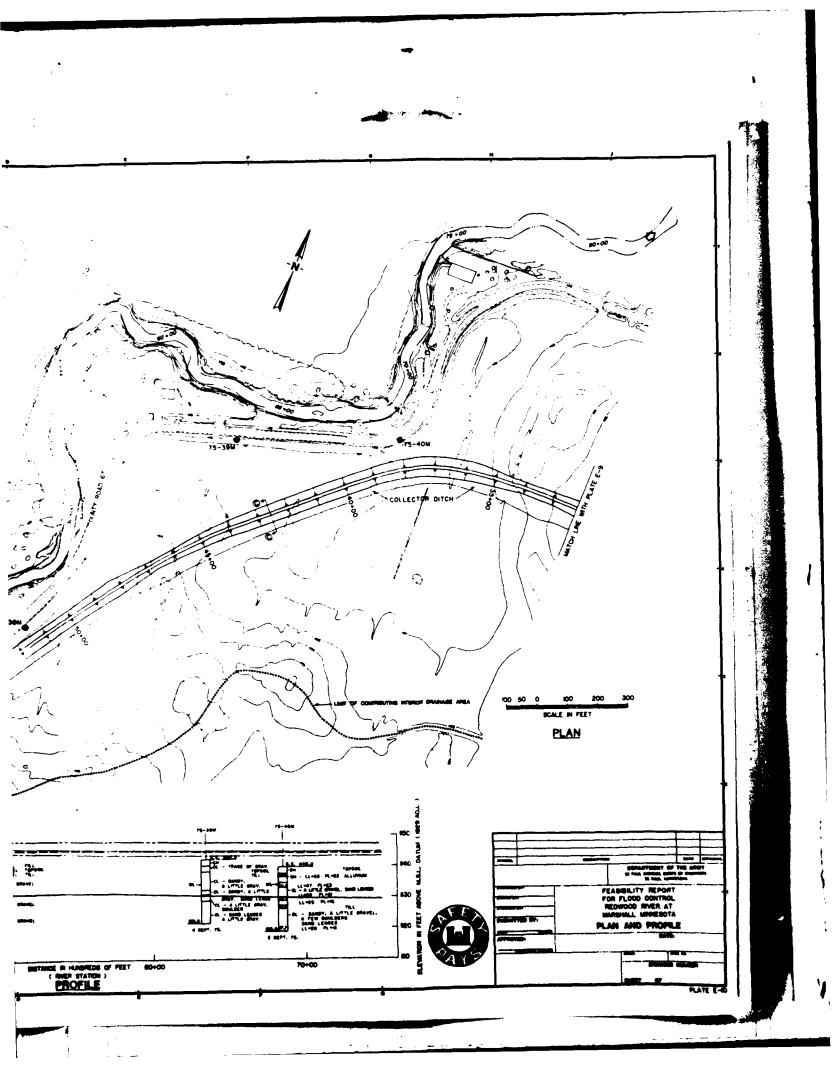


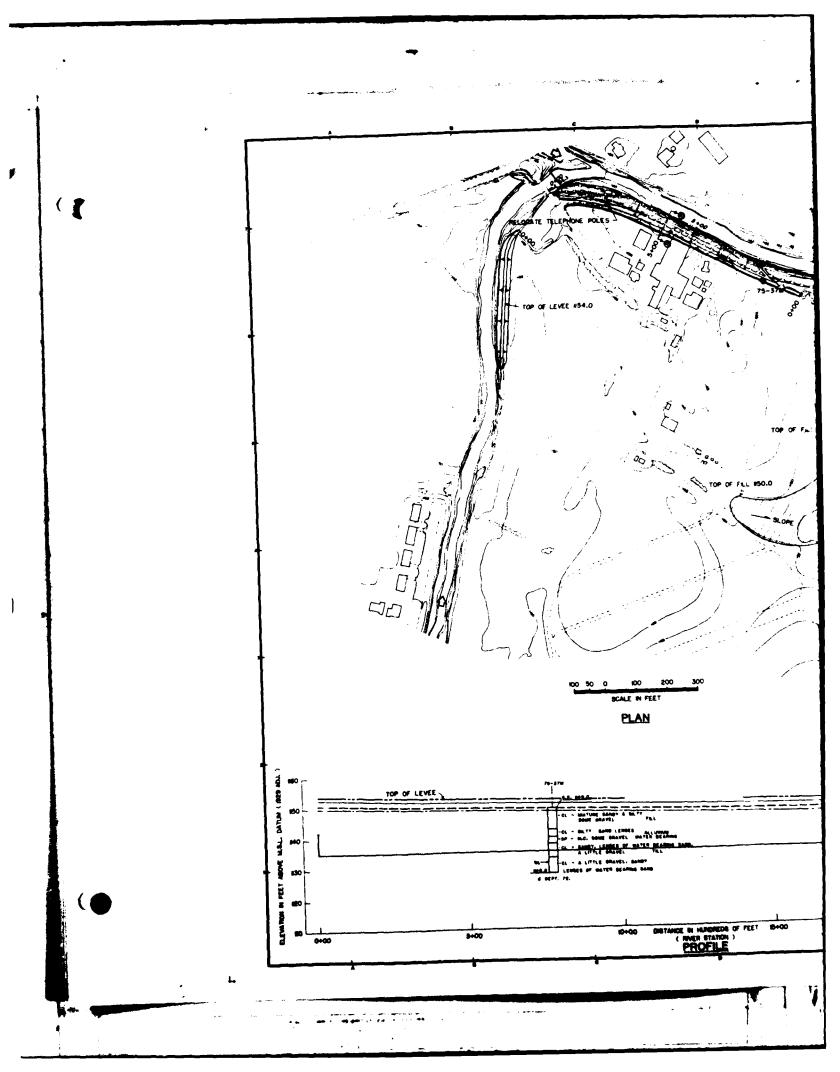


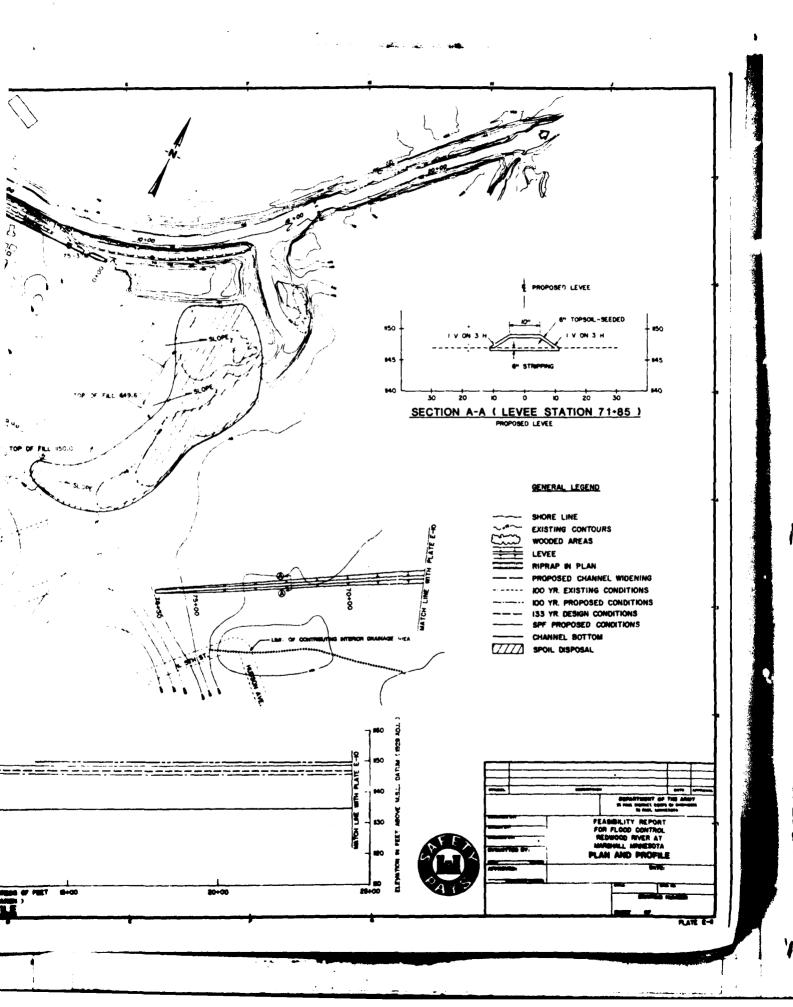


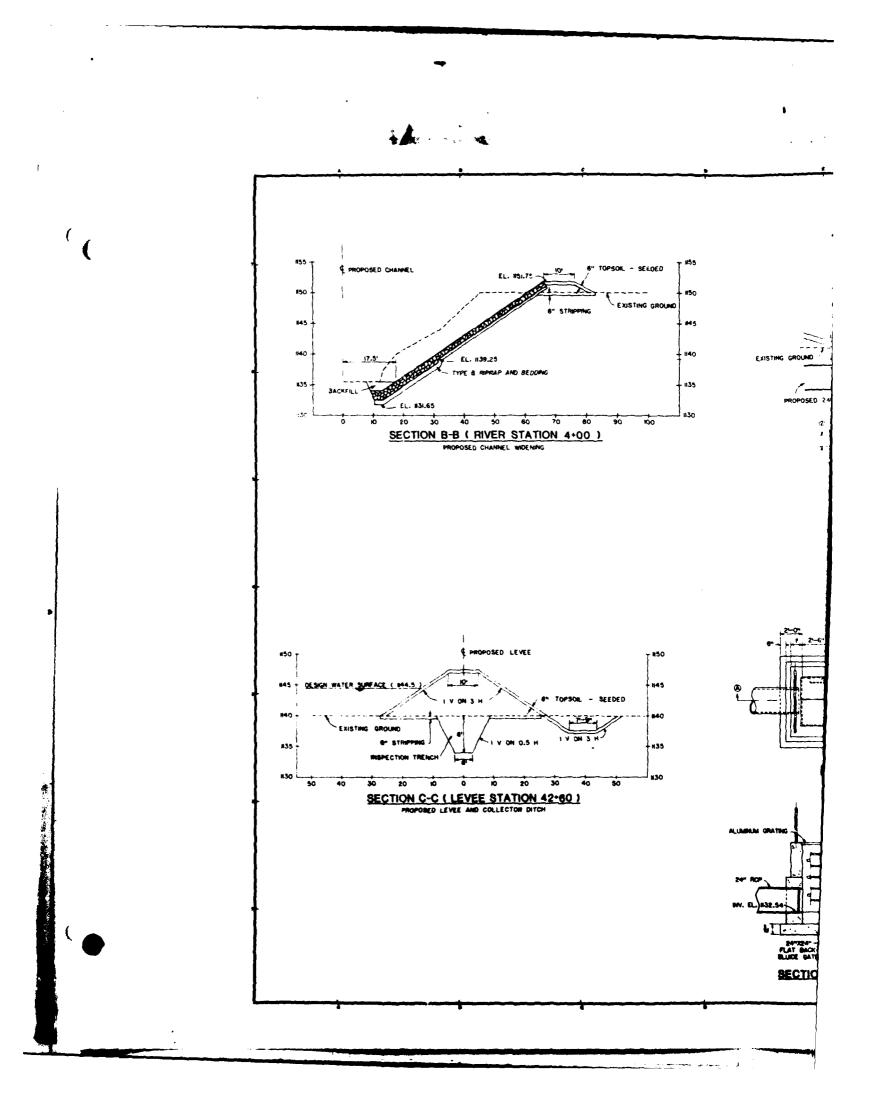


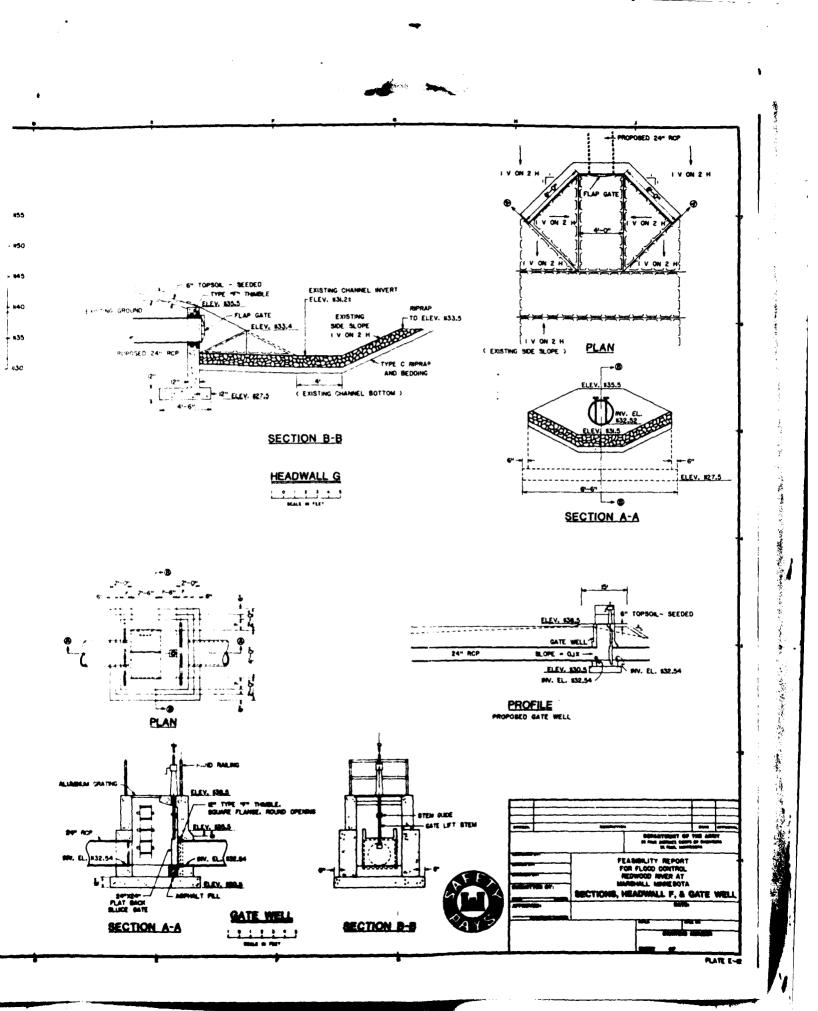












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# SECTION F

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# ECONOMICS OF SELECTED PLAN

SECTION F

# ECONOMICS OF SELECTED PLAN

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#### SECTION F

### ECONOMICS OF SELECTED PLAN

1. The purpose of this section is to present the procedures used in determining the benefits and costs of the selected plan. Included are pertinent discussions on flood damage evaluation, determination of project benefits in accordance with ER 1105-2-351, estimated project costs, project justification and optimization.

### METHODOLOGY

2. The evaluation of project benefits and costs were accomplished separately for the upstream and downstream reaches. These reaches were identified early in the study to aid in the evaluation of remedial measures required to insure effective operation of the existing project and measures needed to protect downstream reach development not protected by the existing project. The upstream reach extends from the downstream confluence of the natural river and existing project diversion channel (mile 66.1) upstream to the Burlington Northern Railroad bridge at mile 73.8 as shown on plate F-3. The downstream study reach extends downstream from mile 66.1 to the U.S. Highway 23 bridge at mile 58.3. Justification of needed upstream improvements was based on the need for additional measures to assure effective operation of the existing project as originally designed. Selection of the plan for the upstream reach is based on a comparison of net benefits attributable to the most physically feasible and implementable alternatives, environmental impacts, and desires of local interests.

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3. The determination of plan benefits, justification, and optimization of required downstream works was based on the need for upgrading the existing project, mitigating any adverse effects from the proposed upstream improvements, and providing protection to downstream reach flood plain growth not protected by the existing project.

4. Agricultural flood damages along the 270-acre agricultural area downstream of the city between river miles 65 and 58.3 were not evaluated since this area is outside the limits of the existing project and would not be substantially benefitted by works needed to upgrade the existing project. Further, protection of this relatively long and narrow reach would be incrementally unjustified by itself.

5. Information developed in support of plan formulation studies was updated and expanded upon to develop a detailed economic analysis for the selected plan. Project costs and benefits were estimated for a 50-year project life and a 6-7/8 percent interest rate. Price levels are based on October, 1977 prices for similar work done in the area. The base year used in this economic analysis since the beginning of this feasibility study was 1980. A more realistic base year would now be about 1985. However, projection of interim damage growth and reduction of future damage growth to base year 1985 would not affect the analysis contained herein enough to warrant a change in plan formulation or scale of development analyses.

#### CHARACTER OF FLOODED AREA

6. Without additional measures, substantial flooding would occur in the highly developed or central portion of the city. Approximately 293 acres of mixed open-space recreational, single and multiple-family dwelling, commercial, and light industrial property remains subject to flood damage due to floodwaters entering the area principally from the upstream reach. Of the total upstream area subject to flooding, about 120 acres are in agricultural use, slightly over 40 acres are committed to existing or planned residential use, and the remaining acreage occupied by the river corridor or utilized for transportation and other uses as shown on Plate F10, Existing and Proposed Land Use. Without the existing project deficiency, all of this land should have been protected during the April 1969 flood.

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7. The downstream reach area subject to flooding generally includes the flood plain area between River Mile 66.1 and State Highway 23 in an east-west direction and between State Highway 19 and the Highway 23 bridge (river mile 58.3) in a south-north direction. (See plate B-2 for area map.) Approximately 215 acres (or 24 percent) of this approximately 880-acre area is occupied by the Southwest State College campus. About 356 acres (or 60 percent) are in agricultural use. Single and multiple-family dwelling units occupy another 85 acres. Commercial land use is generally confined to a 40-acre narrow strip of land along State Highwa 19 between North Bruce St. and State Highway 23. The remaining flood plain land is either vacant, used for County Ditch No. 62, or is in transportation use. The existing 100-year and SPF flooded area outlines for both the upstream and downstream reaches were determined in the Flood Plain Information Study for Marshall and are shown on plate F-1.

#### TYPES OF FLOOD DAMAGE

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8. Tangible flood damages determined through field surveys and research of flood records consist of the following categories: residential; commercial; damages to buildings, equipment and grounds at Southwest State College; damages to streets, sewers, and other utilities; and emergency flood fight and cleanup costs. Minor agricultural damages would occur within or immediately adjacent to the developed area with a 100-year flood under present conditions. However, most of the agricultural land use and related damage potential along the upstream reach (immediately upstream of CSAH 7) is expected to be converted to residential development shortly after completion of the proposed project (see Plate F-10 for map of proposed land use). A total of 80 acres of agricultural land along the downstream reach would be protected from flooding with the project.

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Intangible damages, such as hazards to public health and safety, community disruption and human suffering and insecurity are not evaluated herein in monetary units but are discussed later in this report as appropriate.

### EVALUATION OF FLOOD DAMAGES

9. This evaluation of flood damages includes an analysis of upstream reach flood damages that would occur under existing project and developmental conditions and the associated benefits attributed to a maximum practical level of protection to reduce these damages. It also includes an analysis of downstream reach flood damages to determine the feasibility of measures to protect existing development not protected by the existing flood control project.

# REDUCTION IN FLOOD DAMAGES DUE TO UPGRADING OF EXISTING PROJECT

10. To facilitate the evaluation of upstream reach flood damages, the total upstream reach extending from river mile 66.1 to 73.8 is seperated into four seperate sub-reaches as shown on Plate F-3 and described in Table F-1. These sub-reaches correspond to those used in the original economic studies for the existing project and permit an accurate comparison of existing conditions (with existing project) and proposed project conditions.

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#### Table F-1 Description of Sub-Reaches

| Sub-Reach | <u>River Mile</u>   | Type of Development $\frac{1}{2}$    |
|-----------|---------------------|--------------------------------------|
| A         | 70.7 - 73.8         | Agricultural, Public,<br>Residentíal |
| В         | <b>69.1</b> - 70.7  | Public, Residential,<br>Commercial   |
| С         | 67.9 - 69.1         | Commercial, Residential,<br>Public   |
| D         | 66.1 - 67 <b>.9</b> | Residential, Commercial,<br>Public   |

Listed in order of dominant type of development and related flood damage potential. See plate F-10 for map of existing land use.

11. Under present conditions the City of Marshall is subject to flood damages when flood flows upstream of CSAH 7 reach about 3,500 cfs (16-year frequency). At this river flow, floodwater overflows would cross over CSAH 7 south of the CSAH 7 bridge and pass through sub-reaches B and C before re-entering the natural river channel in Marshall about 2,500 feet downstream of the existing diversion structure. At the 100-year and SPF (11,800 cfs) flood flows, the overflows into ''arshall would be 1,090 and 2,000 cfs respectively. At the SPF flow the existing diversion channel has sufficient capacity to pass the remaining 8,300 cfs flood flow without adverse effects.

12. In addition to these potential damages within the highly developed area of Marshall from the overflows over CSAH 7, the flood plain area upstream of CSAH 7 (reach A) is also subject to flood damage. Overland flow commences at a river flow of about 2,500 cfs and inunndates park property, agricultural lands west of CSAH 7 and north of State Highway 23, and limited commercial development along Highway 23.

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Another factor contributing to increased flood damages in Marshall are the increased flood stages along the natural channel (Reach D) as a result of backwater from high river stages immediately downstream of the downstream confluence of the existing diversion channel and river at river mile 66.3. At the 100-year flood flow, the backwater effect would extend up the natural channel to north 6th St. At the SPF flood flow, the backwater effect would extend further upstream to the vicinity of East College Drive (see plate D-2 for street locations).

13. The extent of flood damage reduction with the proposed works is measured as the difference in remaining flood damages with and without the proposed project. To evaluate these damages in accordance with ER 1105-351, the project document damages were updated to present conditions reflecting interim flood plain growth and October 1977 price levels. These damage estimates were further modified to reflect the conversion of some agricultural lands (primarily in Reach B) to commercial and residential development since completion of the existing project. In addition, the proportionate increase in the value of residential contents over the approximately 15 year interim (1961-1976) was evaluated. A summary of total updated potential flood damages for the upstream study reach at Marshall is given in Table F-2.

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### TABLE F-2

# SUMMARY OF TOTAL UPSTREAM REACH FLOOD DAMAGES ${}^{V}$

### REACHA

|                | Apr. 51 (2740 cfs) | June 57 (5370 cfs) | 7900 cfs              |
|----------------|--------------------|--------------------|-----------------------|
| Res.<br>Public | \$ 930<br>930      | \$ 2,740<br>13,160 | \$ 5,580<br>19,850    |
| Ag. and Comm.  | 14,180             | 142,500            | 160, 420              |
|                | \$ 16,040          | \$ 158,400         | \$ 185,850            |
|                |                    | REACHB             |                       |
| Res.           | \$ 9,170           | \$ 24,710          | \$ 50,220             |
| Public         | 8,980              | 103,750            | 162,240               |
| Ag, and Comm,  | 5,470              | 9,340              | 10,260                |
|                | \$ 23,620          | \$137,800          | \$ 222,720            |
|                |                    | REACHC             |                       |
| Res.           | \$543,070          | \$ 2,038,030       | \$ 2,193,260          |
| Public         | 365,980            | 1,416,770          | 1,832,910             |
| Ag. and Comm.  | <b>568,82</b> 0    | 3,646,780          | 5,512,130             |
|                | \$ 1,477,870       | \$ 7,101,580       | \$ 9,538,300          |
|                |                    | REACH D            |                       |
| Res.           | \$ 199,780         | \$ 572,560         | \$ 629,820            |
| Pub.           | 119,970            | 343,370            | \$ 629,820<br>440,420 |
| Ag. and Comm.  |                    | 213,580            | 458,490               |
|                |                    |                    |                       |
|                | \$ 507,100         | \$ 1,129,510       | \$ 1,528,730          |
|                |                    |                    |                       |

Updated for price level changes from October 1959 to October 1977

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14. To analyze the remaining flood damage potential along the upstream study reach at Marshall, elevation-damage and frequency-damage relationships were developed for each sub-reach and are displayed on Plates F-4 through F-7. From these relationships, total remaining average annual upstream reach flood damages with the existing project are estimated at \$286,285. Present condition (October 1977) average annual residential, public and agricultural and commercial flood damages are estimated at \$78,890, \$63,435, and \$143,960 respectively as shown in Table F-3.

| Damage Reach | Residential           | Public          | Agricultural <sup>2/</sup><br>and Commercial | Total            |
|--------------|-----------------------|-----------------|--|------------------|
| A            | \$ 230                | \$ 810          | \$ 8520                                      | \$ 9560          |
| В            | 970                   | 3640            | 280  | 4890             |
| С            | 59 <b>900</b>         | 45125           | 123800                                       | 228825           |
| D            | 17790                 | 13860           | 11360  | 43010            |
|              | <mark>\$</mark> 78890 | <b>\$</b> 63435 | <b>\$</b> 143960                             | <b>\$</b> 286285 |

Table F-3 - Estimated Average Annual Damages  $\frac{1}{}$  - Upstream Reach

 $\frac{1}{0}$  October 1977 prices and conditions

 $\frac{2}{Agricultural}$  damages in Reach A only

15. Flood damages attributable to future developmental growth would be limited to conforming flood plain use, development above the 100-year flood level or flood-proofed improvements. The estimated number of future structures expected to be located within the 100-year flood plain is tabulated by decade in table F-4. No increase in number of structures is projected for residential or commercial structures. Agricultural land use in reach A is expected to decline and eventually be converted to multi-family residential development as shown on plate F-10.

|              |                  | Num  | ber of | Struc | tures |      |      | _ |
|--------------|------------------|------|--------|-------|-------|------|------|---|
|              | Existing         |      |        | Fut   | ure   |      |      |   |
| Project Type | 1977             | 1980 | 1990   | 2000  | 2010  | 2020 | 2030 |   |
| Residential  | 1084             | 1084 | 1084   | 1084  | 1084  | 1084 | 1084 |   |
| Public       | 172              |      | 19     | 21    | 22    | 23   | 25   |   |
| Commercial   | 200 <sup>2</sup> | 200  | 200    | 200   | 200   | 200  | 200  |   |

### Table F-4 - Estimated Future Development $\frac{1}{2}$

1/Upstream reach and developed downtown area flood plain extending downstream to mile 66.1.

 $\frac{2}{Estimated}$  from extension of June 1957 flood data.

16. Future residential damages -- In accordance with ER 1105-2-351 only the growth in damages to contents is evaluated. Although the value of contents may by regulations equal 75 percent of the structure value the future maximum value of contents in this area is estimated at 60 percent of the structure value based on field surveys of existing structural conditions of area housing. With an existing total residential property valuation of \$32,791,000 and an existing contents value of 25 percent of the structural value or \$8,197,800, the limiting damage growth factor is 2.4. An inspection of Series E per capita income projections for OBE Area 099, within which Marshall is located, indicates a growth factor of 4.179 for the 50-year period between 1980 and 2030. A 50-year (1980-2030) Series E per capita growth factor of 4.179 indicates a compound growth rate of 2-7/8 percent. With a limiting factor of 2.4, future growth of contents will cease in year 31. With a base year average annual total residential damage of \$81,730 and estimating that contents incur 40 percent of flood losses, the 1980 base year average annual damage to contents is \$32,690. Adjusted unit flood damages reflecting the effects of the affluence factor are shown by decade in Table F-5. Future growth of average annual damages at a 2.4 limiting growth factor is \$78,460. With 31 years of growth,

and no growth over the next 19 years, the average annual equivalent value of this future growth is  $78,460 - 32,690 \times 0.3676$  or 16,825 as shown on table F-6. Total average annual residential damages would thus be 98,555.

| Property                              | Ave. Ann. Damage:<br>Under Existing <u>1</u> /<br>Conditions | Projecting Ed        |                      |      |                             | nages<br>e Fact<br>2020 | includ-<br>or<br>2030 |
|---------------------------------------|--|----------------------|----------------------|------|-----------------------------|-------------------------|-----------------------|
| Туре                                  | 1977   | 1980                 | 1990                 | 2000 | 2010                        | 2020                    | 2030                  |
| Residential:<br>Structure<br>Contents | \$ 44<br>29<br>\$ 73   | \$ 44<br>32<br>\$ 76 | \$ 44<br>42<br>\$ 86 | 56   | <b>\$</b> 44<br>74<br>\$118 | \$ 44<br>74<br>\$118    | \$ 44<br>74<br>\$118  |

Table F-5 - Adjusted Unit Flood Damages - Upstream Reach

 $\frac{1}{Remaining}$  upstream reach flood damages with existing project.

17. Remaining flood damages to public property along the upstream study reach and located within the 100-year floodplain are expected to grow in accordance with increasing area population. At a 0.74 percent straight line growth rate over the 50-year project life (from State Demographer), future growth of the 1980 base year damage of \$64,830 is estimated at \$24,050. Discounted over the 50-year project life, the average annual equivalent value of this future damage growth would be \$6,580 as shown on Table F-6.

18. No future growth of upstream reach commercial property damages is forecast beyond year 1980, as nearly all available lands are presently developed or are unsuitable. The minor amount of agricultural activity in the area is expected to cease in a few years. Total average annual

remaining flood damages within the present project area (upstream reach) reflecting both existing conditions, future growth, and effects of the affluence factor are shown in Table F-6.

19. The reduction of flood damages along the upstream reach (upstream of mile 66.1) with the provision of upstream works alone would result in a slight increase in downstream reach damages. An increase of 1260 cfs into the downstream reach with the 133-year design flood flow would raise the corresponding downstream water surface about one-half foot at the confluence of the natural channel and diversion channel and along the agricultural area east of the County 67 river crossing. However, the proposed channel widening measures immediately downstream of the confluence would reduce this rise in the vicinity of the confluence to existing condition water levels. As no additional measures are proposed along the agricultural reach downstream of mile 65.0, this one-half foot rise would result in increased average annual damages of about \$1,310, as illustrated on Plate F-9.

#### EVALUATION OF DOWNSTREAM REACH DAMAGES

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20. Downstream reach (downstream of mile 66.1) flood damages were determined for three theoretical peak flood levels to adequately reflect the relationship of damages to river flood stages. Flood damage data were obtained for each category of development for the 100-year, 100-year minus one foot, and 100-year plus one foot levels as shown in table F-7. The hypothetical flood levels correspond to river flood stages of 1143.0, 1142.0, and  $1144.0^{1/}$ , as shown on the rating curve given in Plate F-8. Corresponding recurrence intervals for these three peak flood stages are once in about 100 years, 20 years, and 227 years respectively.

21. Emergency flood fight, cleanup, and disaster relief costs are also reflected in the damage figures given in table F-7. All

 $\frac{1}{R}$  River stages referenced to rating curve location at river mile 65.16.

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Table F-6 -- Existing and Future Flood Upstream Reach Damages Including Effects of Affluence Factor

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| Physical                                     | Ave.Ann. <u>1</u> /<br>Damage<br>Under |   |                   |                     |                    |               | 2                             | Ave. Ann.<br>Equiva-<br>lent In-<br>crease |  |
|--|--|---|-------------------|---------------------|--------------------|---------------|-------------------------------|--|--|
| Flood Losses<br>Reported By<br>Property Type | Existing<br>Conditions<br>1977         | Projected Total Future Flood Damages Including Effectsof Affluence Factor1980 5/19902000201020202030                                      | ure Flood<br>2000 | Damages In<br>2010  | cluding Ef<br>2020 | fects<br>2030 | in-<br>crease<br>over<br>1980 | Uver<br>50-Year<br>Project<br>Life         | Total<br>Ave. Ann.<br>Dam <b>ag</b> es |
| Residential                                  | \$ 78,890                              | <b>\$</b> 81,730 <sup>2</sup> / <b>\$</b> 93,220 <b>\$</b> 108,400 <b>\$</b> 127,500 <b>\$</b> 127,500 <b>\$</b> 127,500 <b>\$</b> 45,770 | \$ 108,400        | \$127,500           | \$127,500          | \$127,500     | \$45,770                      | <b>\$</b> 16,825                           | \$ 98,555                              |
| Public                                       | 63,435                                 | 64,830 <sup>3/</sup> 69,630   | 74,440            | 79,230              | 84,020             | 88,880        | 24,050                        | 6,580                                      | 71,410                                 |
| Agricultural<br>and Commercial               | 143,960                                | 152,740 <u>4</u> / 152,740  | 152,740           | 152,740             | 152,740            | 152,740       | 0                             | 0  | 152,740                                |
|  | \$28 <b>6,</b> 285                     | \$299,300 \$315,590   |                   | \$335,580 \$359,470 | \$364,260          | \$369,120     | \$69,820                      | \$23,405                                   | \$322,705                              |

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1/Total average annual damages for sub-reaches A,B, C and D = \$9560, 4890, 228,825 and 43,010 respectively. See Table F-3 for break-down by developmental category.

2/2-7/8% Compound growth

 $\frac{3}{0.741}$  Straight line growth (Factor = 1.022)

 $\frac{4}{2^{\circ}}$  2<sup>°</sup> Straight line growth (Factor = 1.061)

5/See paragraph 5 for discussion of base year

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damages shown in table F-7 are present condition damages to property not measurably protected by the existing diversion channel or earlier local and Federal downstream channel improvements.

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22. Residential flood damages along the downstream reach under present conditions commence at a river stage elevation of 1137.5 at mile 65.16 with a corresponding discharge of 725 cfs as indicated by the rating curve shown on plate F-8. First floor flooding up to about one foot deep would occur to some single family dwellings with the occurrence of the 100-year flood and no emergency flood fight. Home values in this area are approximately \$45,000 based on October 1977 price levels. A few permanent residences would be subject to basement flooding via seepage and sewer backup. Thirty-four single and double unit trailer homes would be similarly affected. The basement levels of two large apartment complexes would incur severe damage at the 100-year flood level.

23. Field inspections and interviews with home and property owners provided data for determining physical damages and values of residences. Evaluation of residential damages as derived from depthflooded-damage tables considered the value of the home and depth of flooding above basement or first floor levels. Results of damage surveys indicate that total residential damages at the 100year flood level would be \$355,000 based on October 1977 price levels.

24. Business damage would consist of loss of or damage to goods and property by water, loss of income by employers and employees due to shutdown, and cost of repairs and cleanup necessary for a

return to normal business operation. Of the businesses inspected and interviewed, the most affected by flooding include a nursery and a few other small businesses located on the north side of State Highway 19. Total damages that would be caused by the occurrence of the 100-year flood without emergency protective measures is estimated at \$990 based on October 1977 price levels.

25. Flood damage to downstream reach public property at Marshall consists of damages to public streets, sewers, and other utilities, and damages to buildings, grounds, & equipment at the S.W. State College at Marshall. Public street, sewer, and utility damage is minimal at the 100-year flood level. Extensive damage to lowlevel electrical and mechanical equipment would occur and extensive cleanup efforts required at the college in the event of a recurrence of the 100-year level without the construction of effective emergency flood barriers. Flooding of electrical and mechanical equipment would render them inoperative with a likely closing of the campus. A four to five day temporary closure of the college would result in increased annual operating expenses of approximately \$50,000. Total public damages resulting from a flood similar to the 100-year flood level and without effective emergency flood barriers would be \$198,000 as shown in table F-7.

#### Table F-7 -- Flood Damage Data - Downstream Reach

| Flood      | Frequency<br>Percent | Peak Flood<br>Stage<br>Feet | Dis-<br>charge<br>cfs | Resi-<br>dential<br>Damage | Business<br>Damage | Public<br>Damage |
|------------|----------------------|-----------------------------|-----------------------|----------------------------|--------------------|------------------|
| 100-yr1'   | 4.90                 | 1142.0                      | 4000                  | \$ 63,800                  | \$ 0               | \$185,000        |
| 100-yr.    | 1.00                 | 1143.0                      | 6700                  | 355,000                    | 900                | 198,000          |
| 100-yr.+1' | 0.44                 | 1144.0                      | <b>91</b> 00          | 807,900                    | 35,400             | 226,000          |

 $\frac{1}{R}$  Rating curve location at mile 65.16 (existing conditions)

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#### Derivation Of Average Annual Damage

26. Field studies were made to establish high water marks for the April 1969 flood, flood damage areas and zero damage elevations. Initial damage along the downstream reach occurs at a river stage of about 1137.5 (above mean sea level, 1929 adj.) at mile 65.16. Significant flood damage commences at a river stage of about 1143 with a corresponding discharge of 5500 cfs. This elevation corresponds to a discharge of about 725 cfs and an expected frequency of occurrence of one in about 2.1 years. Damage surveys made in November 1974 and May 1975 for the downstream reach determined the depth of flooding and pertinent damage elevations at residences and other structures. Residential damages were determined from flooded-depth-damage relationships. Commercial damages were determined through local inspection and interviews with affected property owners and/or managers. Estimates of public damages were obtained through research of records and/or interviews with City and Southwest State College officials.

27. Using this basic information and previously determined stagedischarge and frequency-discharge relationships, discharge-damage and frequency-damage relationships for both present and 1980 base year conditions for each damage category were developed. Dischargedamage and frequency-damage curves are shown on plate F-9. As determined in this manner for existing conditions, average annual residential, commercial (business), and public damages are estimated at \$13,450, \$375, and \$52,575 respectively.

#### Future Flood Damage

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28. Future flood plain development is expected to occur in accordance with flood plain regulations that have recently been adopted by the City.

Thus, damages to new development would be limited to conforming flood plain use, development above the 100-year flood level or flood-proofed improvements. The estimated future numbers of downstream reach flood plain structures is tabulated by decade in table F-8.

|                 |             |      | Num         | ber  |      |      |      |
|-----------------|-------------|------|-------------|------|------|------|------|
|                 | Existing    |      |             |      | ure  |      |      |
| Property Type   | <u>1977</u> | 1980 | <u>1990</u> | 2000 | 2010 | 2020 | 2030 |
|                 |             |      |             |      |      |      |      |
| Residential:    |             |      |             |      |      |      |      |
| Single-Family   | 44          | 44   | 44          | 44   | 44   | 44   | 44   |
| Multiple-Family | 66          | 66   | 66          | 66   | 66   | 66   | 66   |
| Commercial      | 3           | 3    | 3           | 3    | 3    | 3    | 3    |
| Public          | 7           | 7    | 8           | 9    | 9    | 10   | 10   |

Table F-8 -- Estimated Future Development - Downstream Reach

29. Residential -- Present condition average annual flood damages were increased as appropriate to reflect new damage growth over the 50-year project life. In projecting future residential flood damages, and in accordance with ER 1105-2-351, only the growth in damages to contents is evaluated. Further, the future value of the contents is not expected to exceed 60% of the structural value. The existing value of damage-prone residential structures in the downstream reach is approximately \$1,560,000. With a current contents value of 25 percent of the structural value, the limiting growth factor is 2.4. An inspection of Series E per capita income projections for OBE area 099, within which Marshall is located, indicates a growth factor of 4.179 for the 50-year period between 1980 and 2030. This growth factor indicates a compound growth rate of approximately 2-7/8 percent. A limiting factor of 2.4 thus indicates that future

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growth of contents will cease in year 31. With a base year average annual total residential damage of \$14,660, and assuming that contents incur 40 percent of flood losses, the 1980 base year average annual damage to contents is \$5,860. Adjusted unit flood damages reflecting the effects of the affluence factor are shown by decade in table F-9. Future growth of average annual damage to contents at a 2.4 limiting growth factor is \$14,060. With a 31-year growth period and no growth thereafter over the 50-year project life, the average annual equivalent value of the net future growth is  $\$8,200 \times 0.3676$  or \$3,015, as shown on table F-10. Thus, total average annual residential damages are estimated at \$17,675.

### Table F-9 -- Adjusted Unit Flood Damages - Downstream Reach

| Physical<br>Flood<br>Losses by<br>Property | Ave.Ann.Dam-<br>ages under<br>Existing<br>Conditions | -     |               | it Flood |       |       | uding |
|--|--|-------|---------------|----------|-------|-------|-------|
| Туре                                       | <u>1977</u>  | 1980  | 1990          | 2000     | 2010  | 2020  | 2030  |
| Residential:                               |  |       |               |          |       |       |       |
| Structure                                  | \$ 73  | \$ 80 | \$ 80         | \$ 80    | \$ 80 | \$ 80 | \$ 80 |
| Contents                                   | 49   | 53    | 70            | 93       | 128   | 128   | 128   |
|  | \$122  | \$133 | <b>\$</b> 150 | \$173    | \$208 | \$208 | \$208 |

30. Flood damages to public facilities are expected to grow generally in accordance with the growth in such facilities needed to meet the needs of an increasing area population. Although the population of the southwest region of the state is expected to decline, both the OBERS series E and State demographer's projections indicate a rising population for Lyon County. The city of Marshall is a growing regional educational trade and farm service center for the region and is expected to continue growing over the next 50

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years. The projections by the State Demographer are considered to best represent this local growth situation with a 50-year growth increase of 37.1 percent, or an annual straight line growth rate of 0.7 percent simple growth rate over the 50-year project life is estimated at \$19,920. Discounted, this future growth would be \$5,450 on an average annual basis as shown on Table F-10.

31. No future growth of damages to commercial establishments is anticipated beyond base year 1980. Expansion of a flood-prone nursery will be accomplished outside the flood plain. No further expansion of other small establishments was indicated in interviews with building owners and operators.

32. Total average annual downstream reach flood damages of \$77,235 flecting both existing conditions and future growth and including effects of the affluence factor are shown in table F-10.

Table F-10-- Existing and Future Downstream Reach Flood Damages Including Effects of Affluence Factor

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| E.<br>E  | 2            | 19  | 19  | 12   |
|--|--------------|---|---|--|
| Projected Total Future Flood Damages Including Effects<br>of Affluence Factors | 2000 2010    | <b>,</b> 070 <b>\$</b> 22,860   | 430 430<br>61,650 65,635  | 1,150 \$ 88,925  |
| cluding Effects  | 2020 2030    | <b>\$ 14,660 \$ 16,530 \$ 19,070 \$ 22,860 \$ 22,860 \$ 22,860 \$ 22,860 \$ 8,200 \$ 3,015<sup>1</sup> \$17,675</b> | 430 430<br>69,620 73,600  | <b>\$ 68,770 \$ 74,625 \$ 81,150 \$ 88,925 \$ 92,910 \$ 96,890 \$ 28,120</b> |
| ů.   | 1980         | \$ 8,200 \$   | 0<br>19,920   | \$ 28,120  |
|  | Life Uamages | 3,015 <sup>1/</sup> \$17.675  | $\begin{array}{ccc} 0 & 430 \\ 5,450^{-2/} & 59,130 \\ \end{array}$ | 8,465 77,235   |

 $\frac{1}{\Lambda ve}$ . ann. equivalent factor, compound growth for 31 years = 0.3676

 $\frac{2}{\Lambda}$  Ave. ann. equivalent factor, straight line growth for 50 years = 0.2736

def 3/See paragraph 5 of text for discussion of base year used.
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# BENEFITS

33. Project benefits include the benefits attributable to reduction of flood damages in the upstream and downstream study reaches. They also include location benefits attributable to the incidental protection of present agricultural property which would likely be converted to more intensive development with protection from flooding. Recreation benefits that would be realized from proposed facilities attendant to the proposed flood damage reduction measures are determined in Section G of Appendix I and included in the summary of benefits given later in this section. Similar to the prior discussion of flood damages, the discussion of related flood damage reduction benefits is presented seperately for the upstream and downstream study reaches.

Appendix I F-19a

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#### FLOOD DAMAGE REDUCTION BENEFITS

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34. Flood damage reduction benefits considered in this analysis consist of both benefits attributable to additional measures required to assure effective operation of the existing project and protection of presently unprotected downstream property. These benefits were derived in accordance with the following rationale. Flood control benefits represent the difference in flood damages with and without the selected plan (133-year degree of protection). First, benefits from improving the operation of the existing project were determined from revised frequency-damage relationships as the reduction in remaining flood damages with and without the proposed remedial measures. Then, increased downstream reach flood damages caused by the approximate one-half foot raise in water levels along the unprotected agricultural reach downstream of mile 65.0 were subtracted to obtain net benefits. Benefits attributable to protection of presently unprotected downstream reach property were also evaluated based on an analysis of discharge-damage and frequencydamage relationships shown on plates F-4 through F-7 and F-9. Average annual flood damage reduction benefits under present conditions were computed as the difference in areas (converted to equivalent dollar damages) under the "with" and "without" project frequency-damage curves as shown on plates F-4 through F-7 and F-9. Present (1977) condition average annual benefits attributable to obtaining effective operation of the existing project (upstream study reach) and protection of unprotected downstream development are estimated at \$195,710 and \$56,600 respectively.

35. To determine benefits resulting from the reduction in future flood damages, present condition residential and public benefits are considered to increase in the same proportion as future flood damages. The development of total average annual flood damage reduction benefits of \$221,730 attributable to assuring effective operation of the existing project and benefits of \$65,860 attributable to protection of downstream developments not protected by the existing project is shown in tables F-11 and F-12 respectively.

Table F-11 -- Derivation of Flood Damage Reductions Benefits Due To Improving the Operation of the Existing Project

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| Appen                               |                      |   |   |  |  |               |                         |                    |
|-------------------------------------|----------------------|---|---|--|--|---------------|-------------------------|--------------------|
| dix I                               | Present<br>Condition | Remaining<br>Ave. Ann.<br>Damages<br>with 133-vr. | Remaining<br>Ave. Ann.<br>Damages<br>with SPF | Present<br>Condition                               | 1980<br>Base Year                          |               | Ave. Ann.<br>Equivalent | TOTAL<br>Average   |
| Benefit<br>Category                 | Remaining<br>Damages | Remedial<br>Measures                              |   | Ave. Ann <sub>1</sub> /<br>Benefits <sup>1</sup> / | Ave. Ann <u>2</u> /<br>Benefits <u>2</u> / | 2030-<br>1980 | ot Future<br>Growth     | Annual<br>Benefits |
| Residential                         |                      |   |   |  |  |               |                         |                    |
| Structural<br>Contents              | \$78,890             | \$22,095  | \$11,005                                      | \$34,080<br>22,715                                 | \$34,080<br>24,760                         | -<br>34,660   |                         | \$34,080<br>37,500 |
| Public                              | 63,435               | 20,815  | 9,880   | 42,620   | 43,560                                     | 16,160        | 4,420                   | 47,980             |
| <b>Commercial 6</b><br>Agricultural | 143,960              | 47,665  | 24,310  | 96,295   | 102,170                                    | 0             | 0                       | 102,170            |
|                                     | \$286,285            | \$90,575  | \$45,195                                      | \$195,710  | \$204,570                                  | \$50,820      | \$17,160                | \$221,730          |
|                                     |                      |   | 1   |  |  |               |                         |                    |

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<u>1/Total average annual present-condition benefits for sub-reaches</u> A, B, C and D are \$7,070, \$3,150, \$154,880 and \$28,140 respectively.

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 $\frac{2}{5}$  See paragraph 5, page F-2 for discussion of base year

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Table F-12-- Derivation of Downstream Reach Flood Damage Reduction Benefits

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| Benefit<br>Category                   | Present<br>Condition<br>Ave.Ann.<br>Damages | Remaining<br>Ave.Ann.<br>Damages<br>With<br>Project | Benefits<br>Under<br>Existing<br>Conditions | 1980<br>Base <u>1</u> /<br>Year <u>-</u><br>Condi-<br>tions | Future<br>Growth<br>1980-<br>2030 | Av Ann.<br>Eq of<br>Future<br>Growth | TOTAL<br>Average<br>Annual<br>Benefits |
|---------------------------------------|---|---|---|---|-----------------------------------|--------------------------------------|--|
| Residential<br>Structural<br>Contents | \$ 13,450                                   | \$ 1,730  | \$7,030<br>4,690                            | \$ 7,660<br>5,110   | \$ 7,660 \$ 0<br>5,110 7,150      | \$ 0 \$ 7<br>2,630 5 7               | \$ 7,660<br>7,740                      |
| Public                                | 52,575                                      | 8,015   | 44,560                                      | 45,500  | 16,880                            | 4,620                                | 50,120                                 |
| Commercial                            | 375   | 55  | 320   | 340   | 0                                 | 0                                    | 340                                    |
|                                       | \$ 66,400                                   | \$ 9,800  | \$56,600                                    | \$58,610  | \$24,030                          | \$ 7,250                             | \$65,860                               |

 $\underline{I}/See$  paragraph 5, page F-2 for discussion of base year

Appendix I F-22

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# DOWNSTREAM REACH

36. Approximately 85 acres of downstream reach flood plain land presently in crop use would be protected by the project levee. This area is presently zoned for single family and multiple-family development as shown on Plate F-10. Local interests indicate that this area would be developed even without a project due to its close proximity to existing thoroughfares and utilities and the downtown service area. The "without-project" condition represents development of these areas. This development is expected to commence immediately after completion of the project. Of the 85 acres available for development, 65 acres could reasonably be developed. Of this acreage, 56 acres would be developed with residential dwellings, the remaining 12 acres to be used for streets, utilities and open space areas. No change in land use and intensity of development is anticipated with the project. The current value of this land reflects agricultural use with appreciation due to eminent urbanization. The difference in value between agricultural land under urbanization pressure and agricultural use sustained into the future is about \$2,000 per acre. A market value increase is anticipated with the project equal to the capitalized costs savings of not incurring flood proofing development costs. However, these project benefits are evaluated as an innundation reduction cost savings benefit.

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#### REDUCED FLOOD PROOFING COST SAVINGS BENEFIT

37. In accordance with ER 1105-351, reduced flood proofing costs were calculated as an innundation reduction benefit for the downstream reach under proposed project conditions. In the absence of providing levee protection to the net 56 developable acres, an average of 3.2 feet of earthen fill would be required to bring the area up to the 133-year design water surface elevation. Of the required 244,000 cubic yards of fill, approximately 40 percent would be hauled in from other areas and could consist of demolition debris, excavated material from area building projects or new borrow. Estimated total first costs of \$155,800 capitalized at a 6-7/8 percent rate of return give a net savings or benefit of \$11,110.

A very limited number of present land owners would receive benefits from flood proofing cost savings with protection of their property against flooding. Protection of the 56 developable acres is incidental to the selection of the most cost effecitve levee alignment. Local interests indicate that adjustment of the levee alignment to exclude this property would require their probable payment of flood easements equal or greater in value to any flood proof cost savings.

#### OTHER BENEFITS

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38. The proposed project would provide in addition to the eavluated monetary benefits, intangible benefits including reduced apprehension and anxiety of area residents, reduced hazards to health and safety, and reduced disruptions to established community growth patterns. Construction of the recreational trail system and picnic facilities would provide substantial benefits in terms of increased leisure time opportunities and direct monetary benefits in terms of

local expenditures for enjoyment of recreational biking, crosscountry skiing, walking, picnicking, and other activities. These benefits are presently estimated at \$43,130. 1 }

39. Estimated downstream reach flood damage reduction benefits of 76,970 including flood proof cost savings are summarized in Table F-14.

### Appendix I F-25

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### Table F-13 - Summary of Benefits

| Flood damage reduction                           |            |
|--|------------|
| Improvement of existing project (upstream reach) |            |
| 1980 Base year conditions                        | \$ 204,570 |
| Future growth                                    | 17,160     |
| Downstream reach                                 |            |
| 1980 Base year conditions                        | 58,610     |
| Future growth                                    | 7,250      |
| Reduced Flood Proofing Cost Savings Benefit      | 11,110     |
| Recreation benefits (entire study area)          | 43,130     |
|  | \$341,830  |

# DETAILED COST ESTIMATE

40. A detailed estimate of project costs based on October 1977 price levels and reflecting similar work done by the St. Paul District in the area is given in Table F-4. Estimated land co ts are based on recent market transactions in the area.

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| (hamels)         Main Channel         Clear and grub       ac.       3.6       \$1,000.00       \$3,600         Excavation       c.y.       67,515       1.50       101,300         Spoil wasted on river       bank       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       1,905       0.80       1,500         Spoil trucked to disposal       c.y.       1,905       0.80       1,500         spoil hauled for levee       and random channel fill       c.y.       54,700       .35       19,100         Channel fill       Random       c.y.       10,100       0.75       7,600         Pervious       c.y.       8,850       2.00       17,700         Riprap       c.y.       17,755       20.50       364,000         Bedding       c.y.       10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       I23,100       1.10       \$17,500         Otal channels       \$738,600       \$738,600       \$738,600         Eevees <th>l t em</th> <th>Unit</th> <th>Quantity</th> <th>Unit<br/>Cost</th> <th>lotal<br/>Cost</th> | l t em              | Unit | Quantity | Unit<br>Cost | lotal<br>Cost |
|---|---------------------|------|----------|--------------|---------------|
| Main Channel         Clear and grub       ac.       3.6       \$1,000.00       \$ 3,600         Excavation       c.y.       67,515       1.50       101,300         Spoil wasted on river       bank       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       1,905       0.80       1,500         Spoil hauled for levee       and random channel fill       c.y.       54,700       .35       19,100         Channel fill       c.y.       10,100       0.75       7,600         Pervious       c.y.       10,100       0.75       7,600         Bedding       c.y.       17,755       20.50       364,000         Bedding       c.y.       10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       Iz3,100       Iz3,100         otal thannels       \$738,600       \$738,600         evees       Stripping       c.y.       15,930       1.10       \$17,500         Levee fill       c.y.       77,660       0.80       62,100  | lederal first Costs |      |          |              |               |
| Clear and grub       ac.       3.6       \$1,000.00       \$ 3,600         Excavation       c.y.       67,515       1.50       101,300         Spoil wasted on river       bank       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       10,910       0.40       4,400         Spoil trucked to disposal area       c.y.       1,905       0.80       1,500         spoil hauled for levee and random channel fill       c.y.       54,700       .35       19,100         Channel fill       c.y.       54,700       .35       19,100         Channel fill       c.y.       8,850       2.00       17,700         Riprap       c.y.       10,100       0.75       7,600         Bedding       c.y.       10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100       1.10       \$ 17,500         otal channels       \$738,600       \$       \$ 5738,600         eevees       Stripping       c.y.       15,930       \$ 1.10       \$ 17,500         bevee fill       c.y.       15,930       \$ 1.10       \$ 17,500   | (hannels            |      |          |              |               |
| Excavation       c.y.       67,515       1.50       101,300         Spoil wasted on river       c.y.       10,910       0.40       4,400         Spoil wasted on river       c.y.       10,910       0.40       4,400         Spoil trucked to disposal       c.y.       1,905       0.80       1,500         spoil hauled for levee       and random channel fill       c.y.       54,700       .35       19,100         Channel fill       c.y.       10,100       0.75       7,600       Pervious       c.y.       17,700         Random       c.y.       10,100       0.75       7,600       100       17,700         Riprap       c.y.       17,755       20.50       364,000       1,000       1,000         Bedding       c.y.       10,585       9.00       95,300       1,23,100         Contingencies (20%)       123,100       123,100       123,100         otal channels       \$738,600       \$738,600         eevees       Stripping       c.y.       15,930       1.10       \$17,500         Levee fill       c.y.       77,660       0.80       62,100         Iopsoil       c.y.       14,935       1.75       26,100   | Main Channel        |      |          |              |               |
| Spoil wasted on river<br>bank       c.y. 10,910       0.40       4,400         Spoil trucked to disposal<br>area       c.y. 1,905       0.80       1,500         Spoil hauled for levee<br>and random channel fill       c.y. 1,905       0.80       1,500         Spoil hauled for levee<br>and random channel fill       c.y. 54,700       .35       19,100         Channel fill       c.y. 10,100       0.75       7,600         Pervious       c.y. 10,100       0.75       7,600         Riprap       c.y. 17,755       20.50       364,000         Bedding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100       1.10       \$17,500         otal channels       \$738,600       \$738,600         aevees       \$tripping       c.y. 15,930       \$1.10       \$17,500         Levee fill       c.y. 77,660       0.80       62,100         Iopsoil       c.y. 13,6       650.00       8,800   | (lear and grub      | ac.  | 3.6      | \$1,000.00   | \$ 3,600      |
| bank       c.y. 10,910       0.40       4,400         Spoil trucked to disposal<br>area       c.y. 1,905       0.80       1,500         spoil hauled for levee<br>and random channel fill       c.y. 54,700       .35       19,100         Channel fill       c.y. 54,700       .35       19,100         Channel fill       c.y. 54,700       .35       19,100         Channel fill       c.y. 8,850       2.00       17,700         Riprap       c.y. 10,585       9.00       95,300         Seeding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100       1.10       \$17,500         otal channels       \$738,600       \$738,600         evees       Stripping       c.y. 15,930       \$1.10       \$17,500         Levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Excavation          | c.y. | 67,515   | 1.50         | 101,300       |
| area       c.y. 1,905       0.80       1,500         spoil hauled for levee       and random channel fill       c.y. 54,700       .35       19,100         Channel fill       c.y. 10,100       0.75       7,600         Pervious       c.y. 8,850       2.00       17,700         Riprap       c.y. 17,755       20.50       364,000         Bedding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100       123,100         otal channels       \$738,600       \$738,600         eevees       \$5tripping       c.y. 15,930       \$ 1.10       \$ 17,500         levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  | •                   | с.у. | 10,910   | 0.40         | 4,400         |
| and random channel fill       c.y. 54,700       .35       19,100         Channel fill       Random       c.y. 10,100       0.75       7,600         Pervious       c.y. 8,850       2.00       17,700         Riprap       c.y. 10,585       9.00       95,300         Bedding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100       123,100         otal channels       \$738,600       \$738,600         evees       Stripping       c.y. 15,930       \$ 1.10       \$ 17,500         levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  |                     | c.y. | 1,905    | 0.80         | 1,500         |
| Random       c.y. 10,100       0.75       7,600         Pervious       c.y. 8,850       2.00       17,700         Riprap       c.y. 17,755       20.50       364,000         Bedding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100         otal thannels       \$738,600         evees       \$1.10       \$17,500         Stripping       c.y. 15,930       \$1.10       \$17,500         Levee fill       c.y. 77,660       0.80       62,100         Jopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  |                     | c.y. | 54,700   | .35          | 19,100        |
| Pervious       c.y.       10,100       0.175       17,000         Riprap       c.y.       17,755       20.50       364,000         Bedding       c.y.       10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100         otal channels       \$738,600         eevees       \$738,600         Stripping       c.y.       15,930       \$1.10       \$17,500         Levee fill       c.y.       77,660       0.80       62,100         Jopsoil       c.y.       14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Channel fill        |      |          |              |               |
| Riprap       c.y.       17,755       20.50       364,000         Bedding       c.y.       10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100         otal Channels       \$738,600         evees       \$5tripping       c.y.       15,930       \$1.10       \$17,500         Levee fill       c.y.       77,660       0.80       62,100         lopsoil       c.y.       14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  | Kandom              | с.у. | 10,100   | 0.75         | 7,600         |
| Bedding       c.y. 10,585       9.00       95,300         Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100         otal channels       \$738,600         evees       \$738,600         btripping       c.y. 15,930       \$1.10       \$17,500         Levee fill       c.y. 77,660       0.80       62,100         Jopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Pervious            | с.у. | 8,850    | 2.00         | 17,700        |
| Seeding       ac.       1.4       700.00       1,000         Contingencies (20%)       123,100         otal thannels       \$738,600         evees       \$778,600         Stripping       c.y.       15,930       \$       1.10       \$       17,500         Levee fill       c.y.       77,660       0.80       62,100         lopsoil       c.y.       14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Riprap              | с.у. | 17,755   | 20.50        | 364,000       |
| Contingencies (20%)       123,100         otal channels       \$738,600         evees       \$738,600         Stripping       c.y. 15,930       \$ 1.10       \$ 17,500         Levee fill       c.y. 77,660       0.80       62,100         Iopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  | Bedding             | с.у. | 10,585   | 9.00         | 95,300        |
| otal Channels       \$738,600         evecs       \$tripping       c.y. 15,930       \$ 1.10       \$ 17,500         Levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Seeding             | ac.  | 1.4      | 700.00       | 1,000         |
| acvees       stripping       c.y. 15,930       \$ 1.10       \$ 17,500         Levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800   | Contingencies (20%) |      |          |              | 123,100       |
| Stripping       c.y. 15,930       \$ 1.10       \$ 17,500         Levee fill       c.y. 77,660       0.80       62,100         lopsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  | lotal Channels      |      |          |              | \$738,600     |
| Levee fill       c.y. 77,660       0.80       62,100         topsoil       c.y. 14,935       1.75       26,100         Seeding       ac.       13.6       650.00       8,800  | Levees              |      |          |              |               |
| Iopsoil         c.y.         14,935         1.75         26,100           Seeding         ac.         13.6         650.00         8,800   | Stripping           | c.y. | 15,930   | \$ 1.10      | \$ 17,500     |
| Seeding ac. 13.6 650.00 8,800   | Levee fill          | с.у. | 77,660   | 0.80         | 62,100        |
|   | lopsoil             | c.y. | 14,935   | 1.75         | 26,100        |
| Clear and grub ac. 1.6 1,000.00 1,600   | Seeding             | ac.  | 13.6     | 650.00       | 8,800         |
|   | Clear and grub      | ac.  | 1.6      | 1,000.00     | 1,600         |

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Table F-14 - Detailed Estimate of First Costs

Appendix I

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| ltem  | Unit   | Quantity  | Unit<br>Cost   | Total<br>Cost   |
|---|--|---|--|---|
| ederal First Costs (continued   | i)   |   |  |   |
| Levees (continued)  |  |   |  |   |
| Remove existing pavement  | ts.y.  | 1,550   | \$ 1.75  | \$ 2,700  |
| Remove and replace base course  | c.y.   | 350   | 2.50   | 900   |
| Bit, wear course  | ton  | 180   | 15.00  | 2,700   |
| Bit. Binder course  | ton  | 180   | 10.00  | 1,800   |
| Bit. material   | ton  | 15  | 100.00   | 1,500   |
| Plantings   | jod  | sum   |  | 17,500  |
| Contingencies (20%)   |  |   |  | 28,600  |
| Total Levees  |  |   |  | \$ 171,800  |
| Floodway Control and  |  |   |  |   |
| Diversion Structures  |  |   |  |   |
| Diversion Structures<br>(Overflow structure)  |  | 2 010   | <b>*</b> 1 10  |   |
| Diversion Structures<br>(Overflow structure)<br>Stripping   | c.y.   | 2,810   | \$ 1.10  | -   |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill  | c.y.   | 4,035   | 0.90   | 3,600   |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation  | с.у.<br>с.у.                                 | 4,035<br>19,465   | 0.90   | 3,600<br>11,700   |
| Diversion Structures<br>(Overflow Structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away   | с.у.<br>с.у.<br>с.у.                         | 4,035<br>19,465<br>17,320                                   | 0.90<br>0.60<br>.75                                  | 3,600<br>11,700<br>13,000   |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap   | с.у.<br>с.у.<br>с.у.<br>с.у.                 | 4,035<br>19,465<br>17,320<br>2,370                          | 0.90<br>0.60<br>.75<br>20.50                         | 3,600<br>11,700<br>13,000<br>48,600                               |
| Oiversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap<br>Bedding  | c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y.         | 4,035<br>19,465<br>17,320<br>2,370<br>1,185                 | 0.90<br>0.60<br>.75<br>20.50<br><b>9.</b> 00         | 3,600<br>11,700<br>13,000<br>48,600<br>10,700                     |
| Oiversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap<br>Bedding<br>Channel fill                                      | с.у.<br>с.у.<br>с.у.<br>с.у.                 | 4,035<br>19,465<br>17,320<br>2,370                          | 0.90<br>0.60<br>.75<br>20.50                         | \$ 3,100<br>3,600<br>11,700<br>13,000<br>48,600<br>10,700<br>\$00 |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap<br>Bedding  | c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y.         | 4,035<br>19,465<br>17,320<br>2,370<br>1,185                 | 0.90<br>0.60<br>.75<br>20.50<br><b>9.</b> 00         | 3,600<br>11,700<br>13,000<br>48,600<br>10,700<br>\$00             |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap<br>Bedding<br>Channel fill<br>Topsoil from channel              | c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y. | 4,035<br>19,465<br>17,320<br>2,370<br>1,185<br>250          | 0.90<br>0.60<br>.75<br>20.50<br>9.00<br>2.00<br>1.25 | 3,600<br>11,700<br>13,000<br>48,600<br>10,700                     |
| Diversion Structures<br>(Overflow structure)<br>Stripping<br>Embankment fill<br>Channel excavation<br>Spoil hauled away<br>Riprap<br>Bedding<br>Channel fill<br>Topsoil from channel<br>stripping | c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y.<br>c.y. | 4,035<br>19,465<br>17,320<br>2,370<br>1,185<br>250<br>1,775 | 0.90<br>0.60<br>.75<br>20.50<br>9.00<br>2.00<br>1.25 | 3,600<br>11,700<br>13,000<br>48,600<br>10,700<br>500<br>2,200     |

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## Table F-14 - Detailed Estimate of First Costs (continued)

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| <u>ุฬท</u>  | Unit   | Quantity | Unit<br>Cost |    | Total<br>Cost  |
|---|--------|----------|--------------|----|----------------|
| leral First Costs (continued)                             | )      |          |              |    |                |
| Floodway Control and<br><u>Diversion Structures</u> (cont | inued) |          |              |    |                |
| (Overflow Structure) (cont                                | inued) |          |              |    |                |
| 115x72" R C P arch cul.                                   | 1.f.   | 501      | \$ 215.00    | \$ | 107,700        |
| 115x72" R C P aprons                                      | ea.    | 6        | 1,000.00     |    | 6,000          |
| Asphaltic concrete  | ton    | 85       | 23.00        |    | 2,000          |
| Class 5 gravel  | c.y.   | 85       | 5.50         |    | 500            |
| Class 3 gravel  | c.y.   | 210      | 4.50         |    | 900            |
| Frost free fill   | c.y.   | 490      | 8.50         |    | 4,200          |
| Temporary Hwy. 23 bypass                                  | job    | sum      |              |    | 12,000         |
| Contingencies (20%)                                       |        |          |              |    | 61,000         |
| Sub-total Overflow Structu                                | re     |          |              | 5  | 366,100        |
| (Channel Drop Structure)                                  |        |          |              |    |                |
| Gabion slope protection (1' deep)                         | c.y.   | 530      | \$ 65.00     | \$ | 34,400         |
| Gabion end sill (3 <sup>t</sup> deep                      | )c.y.  | 22       | 44.00        |    | 1,000          |
| Mass concrete   | c.y.   | 30       | 65.00        |    | 1, <b>9</b> 00 |
| Grout   | c.y.   | 6.4      | 40.00        |    | 300            |
| 24" R C P - CL 111  | 1.f.   | 152      | 30.00        |    | 4,600          |
| End section for 24" pipe                                  | ea.    | 8        | 150.00       |    | 1,200          |
| Contingencies (20%)                                       |        |          |              |    | 8,700          |
| Sub-total Drop Structure                                  |        |          |              | \$ | 52,100         |
| Total Floodway Control Div                                | crsion | Structur | c            | \$ | 418,200        |

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# Table F-14 - Detailed Estimate of First Costs (continued)

Appendix I F-29

| ltcm                                 | Unit | Quantity | Unit<br>Cost | Total<br><u>Cost</u> |
|--------------------------------------|------|----------|--------------|----------------------|
| Hederal First Costs (continued       | )    |          |              |                      |
| Interior Drainage                    |      |          |              |                      |
| Headwall A                           |      |          |              |                      |
| Concrete headwall                    | jub  | sum      | :            | \$ 1,100             |
| Riprap                               | c.y. | 20       | \$ 20.00     | 400                  |
| Bedding                              | c.y. | 9        | 10.00        | 100                  |
| 30" Flap gate with<br>Type F thimble | ea.  | 2        | 2,000.00     | 4,000                |
| lleadwall B                          |      |          |              |                      |
| Concrete headwall with<br>riprap     | job  | sum      |              | 1,800                |
| 30" Flap gate with<br>Type F thimble | ea.  | 2        | 2,000.00     | 4,000                |
| Headwall C                           |      |          |              |                      |
| Concrete headwall                    | job  | sum      |              | 1,300                |
| 18" C M P with end section           | 1.f. | 55       | 28.00        | 1,500                |
| Riprap                               | c.y. | 46       | 20.50        | 1,000                |
| Bedding                              | c.y. | 23       | 9.00         | 200                  |
| 18" Flap gate with<br>Type F thimble | ca.  | 1        | 1,400.00     | 1,400                |
| Headwall D                           |      |          |              |                      |
| Concrete headwall                    | jod  | sum      |              | 1,200                |
| 16" Flap gate with<br>Type F thimble | ca.  | 1        | 1,200.00     | 1,200                |

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## Table F-14 - Detailed Estimate of First Costs (continued)

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| ltem   | Unit      | Quantity | Unit<br>Cost | Total<br>Cost |
|--|-----------|----------|--------------|---------------|
| <u>Hederal First Costs</u> (continued<br><u>Interior Drainage</u> (continu |           |          |              |               |
| Headwall F   |           |          |              |               |
| Excavation (headwall and 210-foot channel)                                 | c.y.      | 170      | \$ 5.50      | <b>\$</b> 900 |
| Concrete headwall  | job       | sum      |              | 500           |
| 36" Flap gate with<br>Type F thimble                                       | ea.       | 1        | 2,400.00     | 2,400         |
| Driveway Culvert   |           |          |              |               |
| (Rt. bank sta. 9+50)   |           |          |              |               |
| 18" C M P  | 1.f.      | 30       | 1 . 50       | 600           |
| Ponding Area and<br>Collector Ditch  |           |          |              |               |
| Ponding area ex-<br>cavation   | c.y.      | 41,940   | .75          | 31,400        |
| Collector ditch excava<br>tion   | -<br>с.у. | 6,180    | 3.00         | 18,500        |
| Spoil trucked to dis-<br>posal area  | c.y.      | 5,300    | 0.75         | 4,000         |
| •<br>Stripping   | c.y.      | 7,400    | 1.10         | 8,100         |
| Topsoil from stripping   | •         | 7,450    | 1.40         | 10,400        |
| Seeding  | ac.       | 10.0     | 650.00       | 6,500         |
| 24" R C P ditch culverts   | 1.f.      | 130      | 24.00        | 3,100         |
| End sections for 24"<br>R C 원  | ea.       | 4        | 150.00       | 600           |

# Table F-14 - Detailed Estimate of First Costs (continued)

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Appendix I

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| ltem  | <u>Unit</u>        | Quantity | Unit<br>Cost | Total<br>Cost |
|---|--------------------|----------|--------------|---------------|
| <u>Federal First Costs (</u> continued)<br><u>Interior Drainage</u> (continue |                    |          |              |               |
| Gate Well   |                    |          |              |               |
| Reinforced concrete   | c.y.               | 9        | \$ 175.00    | \$ 1,600      |
| Manhole f <b>rame, cover</b><br>and steps                                     | job                | sum      |              | 600           |
| 24" sluice gate   | ea.                | 1        | 2,700.00     | 2,700         |
| Headwall G  |                    |          |              |               |
| Concrete headwall   | јоъ                | sum      |              | 1,600         |
| 24" R C P CL 111  | 1.f.               | 808      | 24.00        | 19,400        |
| End section with grate<br>for 24" pipe  | ea.                | 1        | 400.00       | 400           |
| 24" Flap gate with<br>Type F thimble  | ea.                | 1        | 1,800.00     | 1,800         |
| Contingencies (20%)   |                    |          |              | 30,700        |
| Total Interior Drainage   |                    |          | :            | \$ 184,000    |
| Recreational Facilities $\frac{1}{2}$   |                    |          |              |               |
| Recreational Bike Trail   | (From              | Section  | G est.)      | \$ 279,600    |
| Cross Country Ski Trail   |                    | "        |              | 2,900         |
| Beautification Plantings  |                    | *1       |              | 36,000        |
| Picnic Facilities   |                    | **       |              | 2,800         |
| Contingencies   |                    | 11       |              | 64,300        |
| Total Recreational Facil  | ities <sup>2</sup> | ./       |              | \$ 385,600    |

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### Table F-14 - Detailed Estimate of F rst Costs (continued)

Appendix I F-32

| l t em                                      | Unit    | Quantit  | Unit<br>y Cost |     | Total<br>Cost |
|---|---------|----------|----------------|-----|---------------|
| Lederal First Costs (continued              | l)      |          |                |     |               |
| Engineering and Design $\frac{3}{2}$        |         | 3/       |                | \$  | 189,800       |
| Supervision and Administ                    | ration  | <u>.</u> |                |     |               |
| Inspection                                  |         |          |                |     | 94,900        |
| Overhead                                    |         |          |                |     | 47,500        |
| Total Engineering, Design,                  | , Supv. | and Adm  | in.            | \$  | 332,200       |
| Total Cost (Federal First<br>plusNon-Federa |         | ribution | s)             | \$2 | ,230,400      |
| Less Non-Federal Contribut                  | tion    |          |                |     | 221,600       |
| Total Federal First Costs                   |         |          |                | \$2 | 2,008,800     |
| Non-Federal First Costs                     |         |          |                |     |               |
| Lands and damages                           |         |          |                |     |               |
| llood Control - fee<br>purchase             | ac.     | 119.8    | \$1,400,00     | \$  | 167,700       |
| Acquisition and ease-<br>ments              | job     | sum      | •-             |     | 8,600         |
| Contingencies (20%)                         |         |          |                |     | 35,300        |
| Total Lands and Damage                      | 5       |          |                | \$  | 211,600       |
| Relocations                                 |         |          |                |     |               |
| Remove and replace                          |         |          |                |     |               |
| (6' x 50') foot bridge                      | job     | sum      |                | \$  | 16,000        |
| Relocate dwelling                           | job     | SLUIN    |                |     | 8,000         |
| Appendix I                                  |         |          |                |     |               |
| F-33  |         |          |                |     |               |

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# lable F-14 - Detailed Estimate of First Costs (continued)

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| ltem                                     | Unit  | Quantity   | Unit<br>Cost | Total<br>Cost |
|--|-------|------------|--------------|---------------|
| Non-Federal First Costs (contin          | nued) |            |              |               |
| Relocations (continued)                  |       |            |              |               |
| Overhead power lines                     | 1.f.  | 1,400.0 \$ | 11.00        | \$ 15,400     |
| Underground utility                      |       |            |              |               |
| cable                                    | 1.f.  | 550        | 6.60         | 3,600         |
| Farm fence                               | 1.f.  | 700.0      | 0.90         | 630           |
| Contingencies (20%)                      |       |            |              | 8,800         |
| Total Relocations                        |       |            |              | \$ 52,400     |
| Engineering and Design                   |       |            |              | \$ 5,200      |
| Supervision and Administra               | tion  |            |              |               |
| Insepction                               |       |            |              | \$ 2,800      |
| Overhead                                 |       |            |              | 1,600         |
| Non-Federal Contributions                |       |            |              |               |
| Recreation facilities (50% of est. cost) |       |            |              | \$ 192,800    |
| Indirect Costs                           |       |            |              | 28,800        |
| Total Non-F <b>edera</b> l Contribu      | tions |            |              | \$221,600     |
|  |       |            |              | \$221,000     |
| Non-Federal First Costs                  |       |            |              | \$495,200     |
| Total Project First Costs <sup>5</sup>   |       |            |              | \$2,504,000   |
|  |       |            | Appen        | dix I         |

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#### Table F-14 - Detailed Estimate of First Costs (continued)

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#### Table F-14 - Detailed Estimate of First Costs (continued)

1/ See Section G for detailed estimate.
2/ Includes 50 percent Non-Federal contribution.
3/ Includes Non-Federal contribution for indirect costs on recreational facilities.
4/ Includes items 2 and 3 above.
5/ Exclusive of pre-authorization study costs.

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#### ANNUAL COSTS

41. Annual costs are computed on the basis of a 50-year economic life and an interest rate of 6-7/8 percent. Included in the total estimated annual charges shown below are the costs of non-Federal operation and maintenance of the proposed project. Since the project would be completed in two construction seasons or less, no charges are included for interest during construction.

#### FEDERAL

| Estimated first cost                            | <b>\$</b> 2 | 2,008,800 |
|---|-------------|-----------|
| Interest during construction                    |             | 0         |
| Total Federal investment                        | \$ 2        | 2,008,800 |
| Federal Annual Charges                          |             |           |
| Interest and amortization                       | \$          | 143,270   |
| Total Federal Annual Charges                    | \$          | 143,270   |
| NON-FEDERAL                                     |             |           |
| Estimated first cost                            | \$          | 495,200   |
| Interest during construction                    |             | 0         |
| Total Non-Federal investment                    | \$          | 495,200   |
| Non-Federal Annual Charges                      |             |           |
| Interest and amortization (\$495,200 @ 0.07132) | \$          | 35,320    |
| Operation and maintenance                       |             | 9,000     |
| Total Non-Federal Annual Charges                | 5           | 44,320    |
| TOTAL ANNUAL CHARGES                            | \$          | 187,590   |
|   | Арре        | ondix I   |

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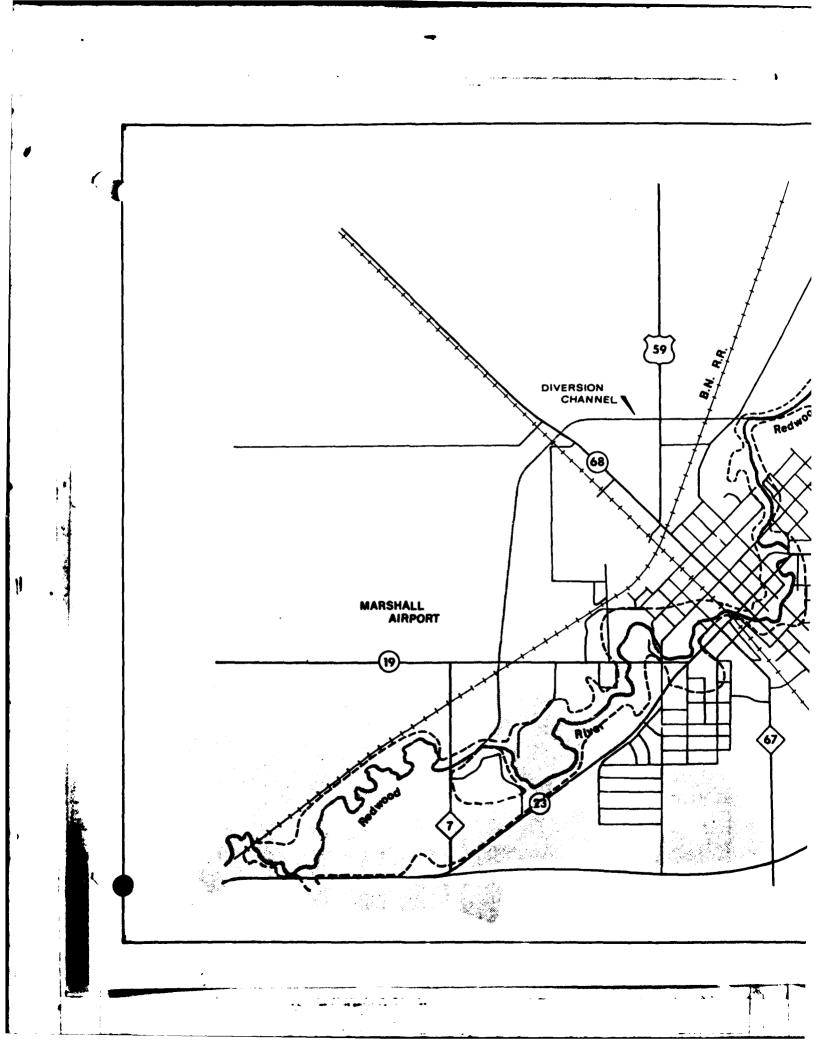
#### PROJECT JUSTIFICATION

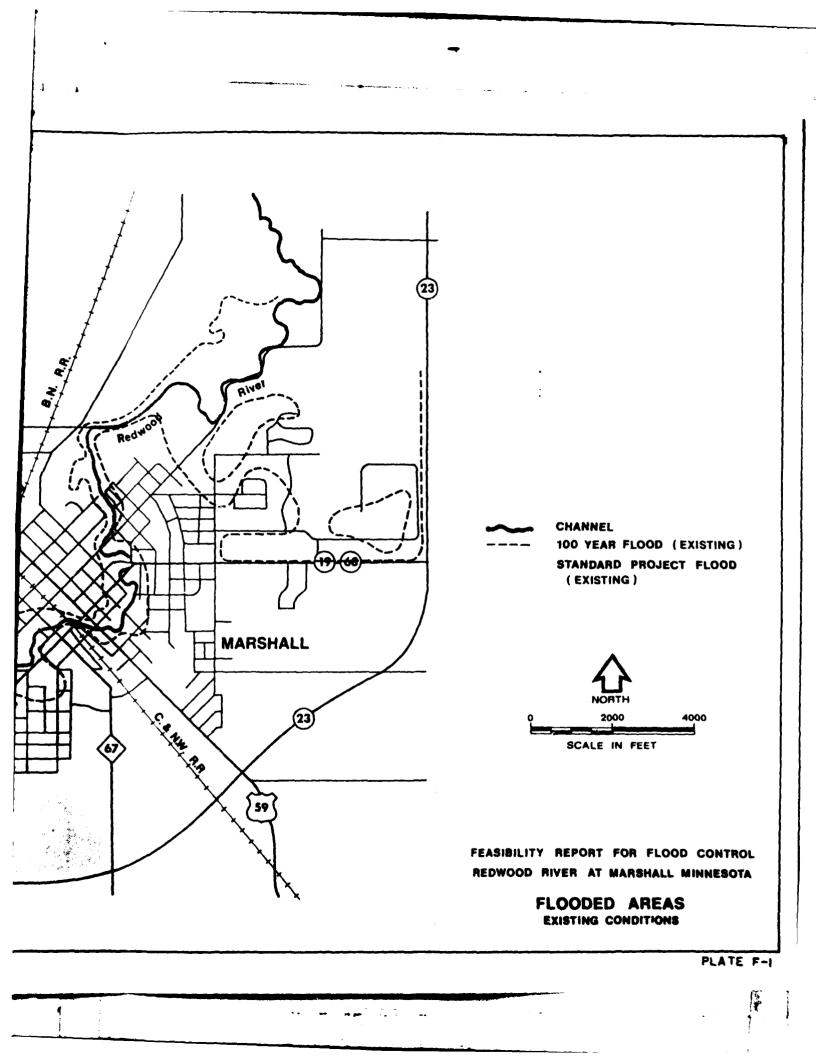
42. In accordance with established procedures, both the remedial measures and protection of downstream reach development are economically justified. A comparison of incremental annual costs versus annual benefits for the remedial measures indicates an incremental benefit-cost ratio of 1.8. A similar comparison for the downstream reach improvements indicates a favorable 2.7 benefit-cost ratio. Average annual charges of \$22,300 versus related average annual benefits of \$54,160 indicates that the proposed recreational facilities are justified. A comparison of all project costs together with related benefits indicates that the entire project as a whole is also justified as shown in Table F-15. A comparison of average annual benefits and costs indicates an internal rate of return of about 12 percent and that annual project benefits would exceed annual project costs immediately upon completion of the project.

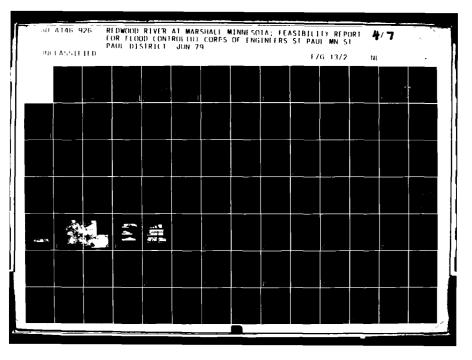
| Feature                        | Total<br>First<br>Costs | Average<br>Annual<br>Costs | Average<br>Annual<br>Benefits | Benefit<br>Cost<br>Ratio |
|--------------------------------|-------------------------|----------------------------|-------------------------------|--------------------------|
| Upstream Reach                 | \$1,674,800             | \$124,620                  | <b>\$</b> 221,730             | 1.8                      |
| Downstream Reach<br>protection | 386,000                 | 28,680                     | 76,970 <sup>1/</sup>          | 2.7                      |
| Recreational facilities        | 443,200                 | 34,290                     | 43,130                        | 1.3                      |
| Total Project                  | \$2,504,000             | \$187,590                  | \$341,830                     | 1.8                      |

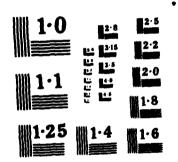
#### Table F-15 - Comparison of Average Annual Costs and Benefits

1/Includes \$11,110, flood proof cost savings benefit







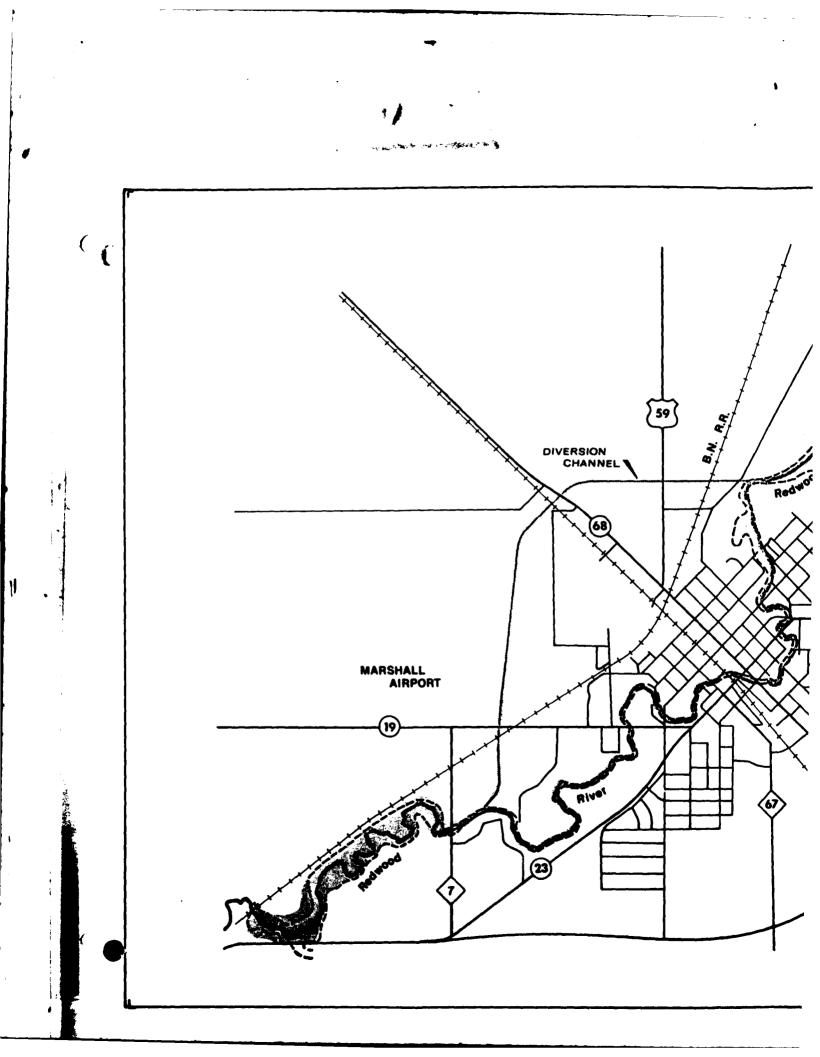


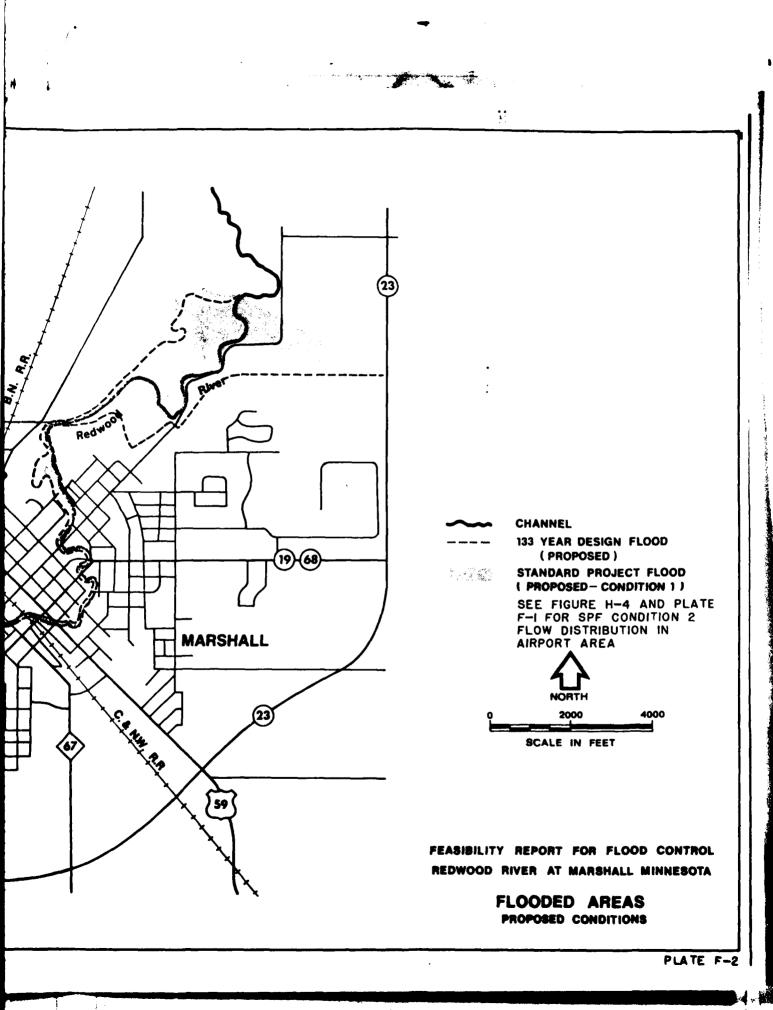
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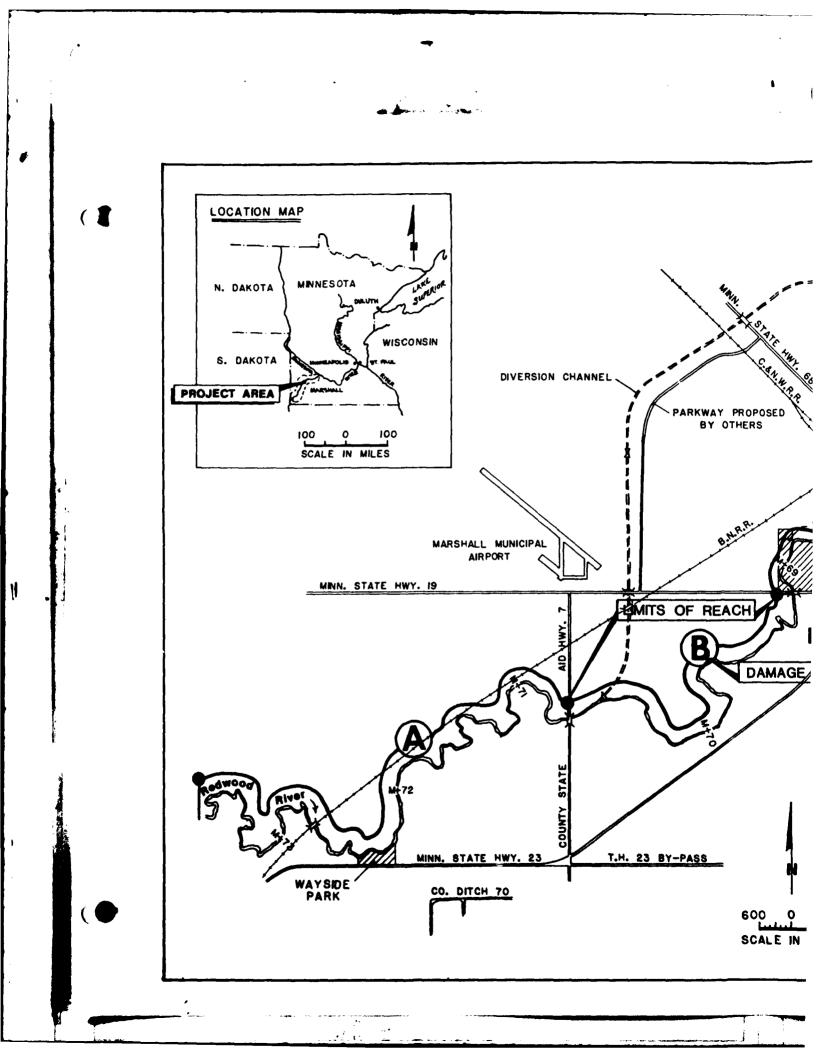
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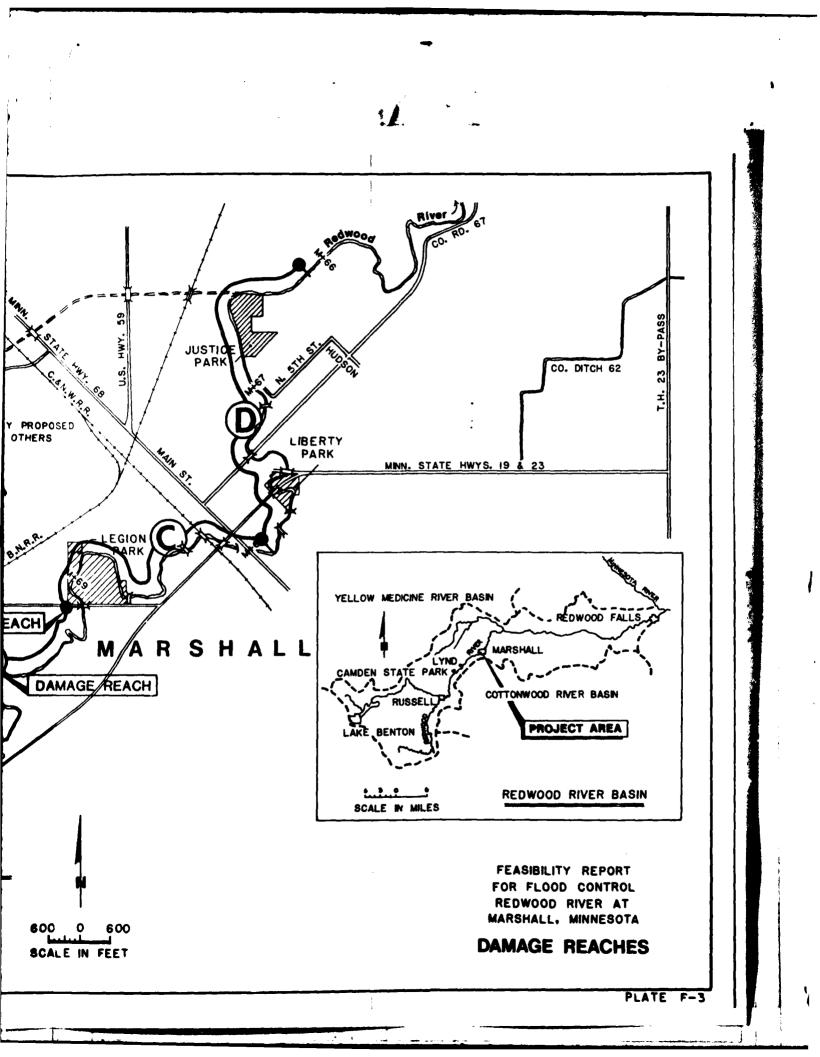
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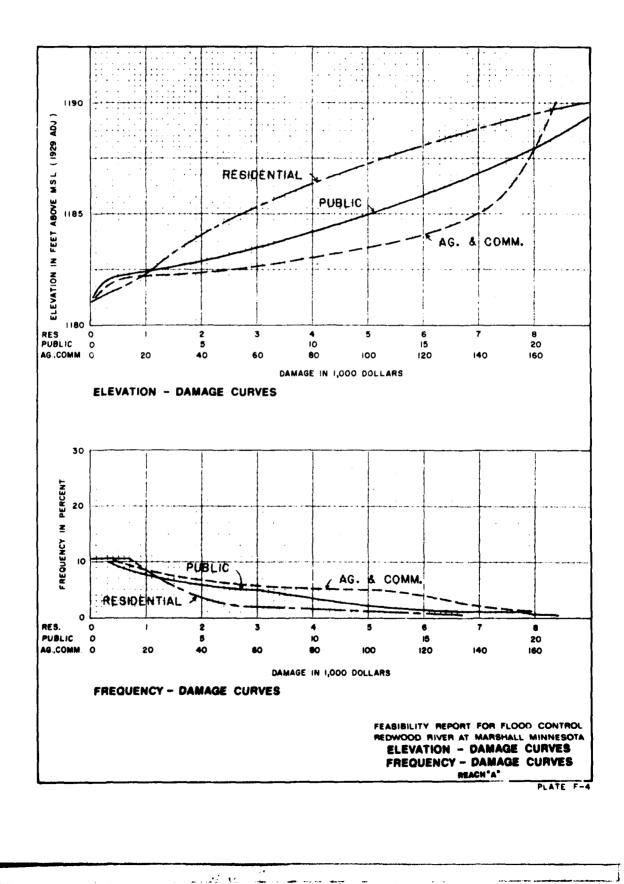




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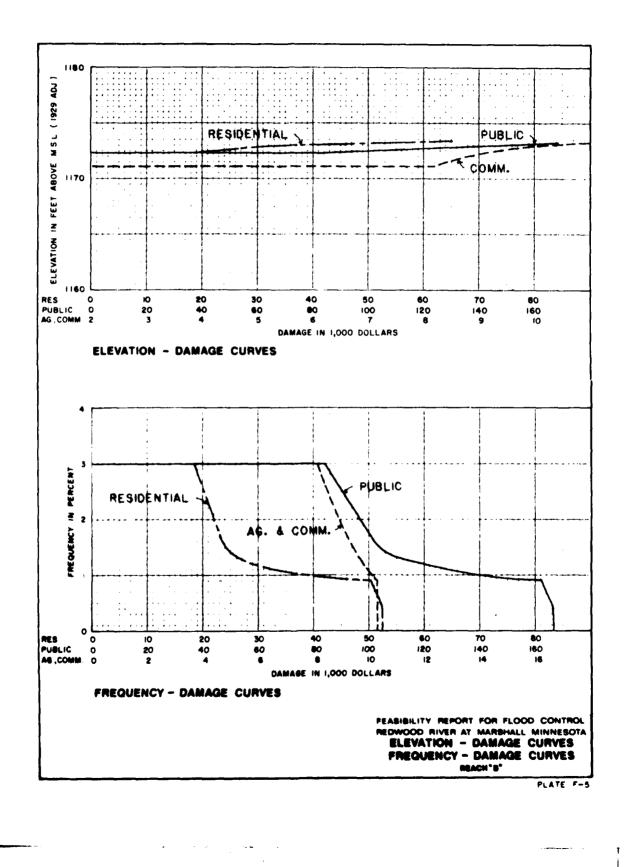




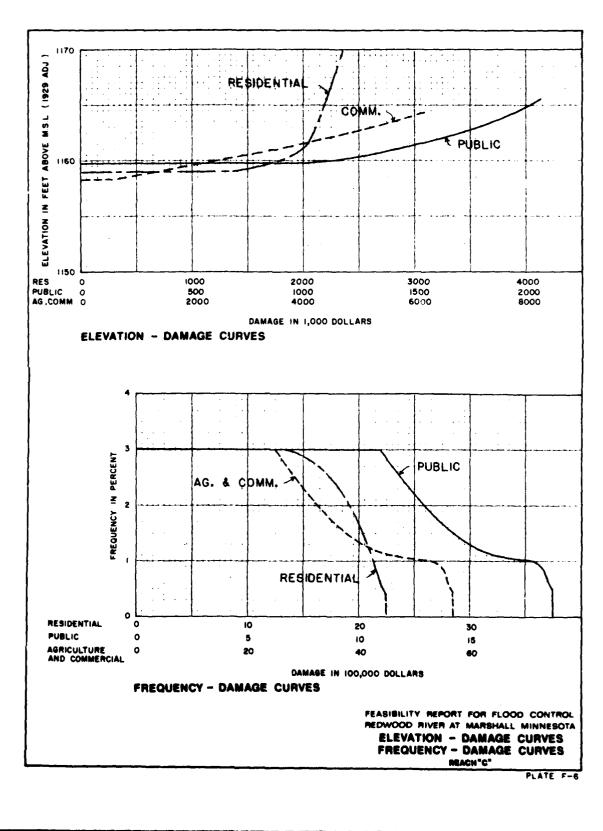




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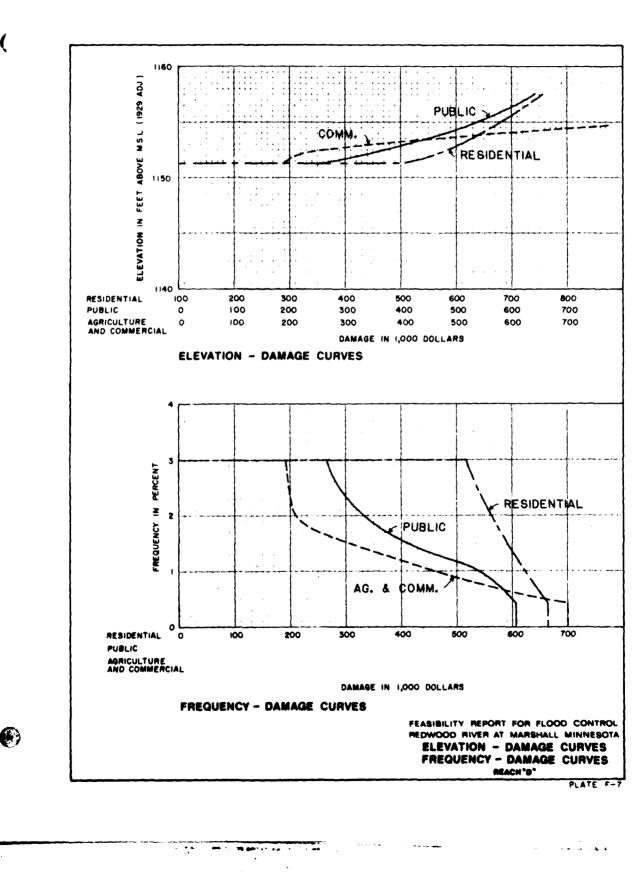


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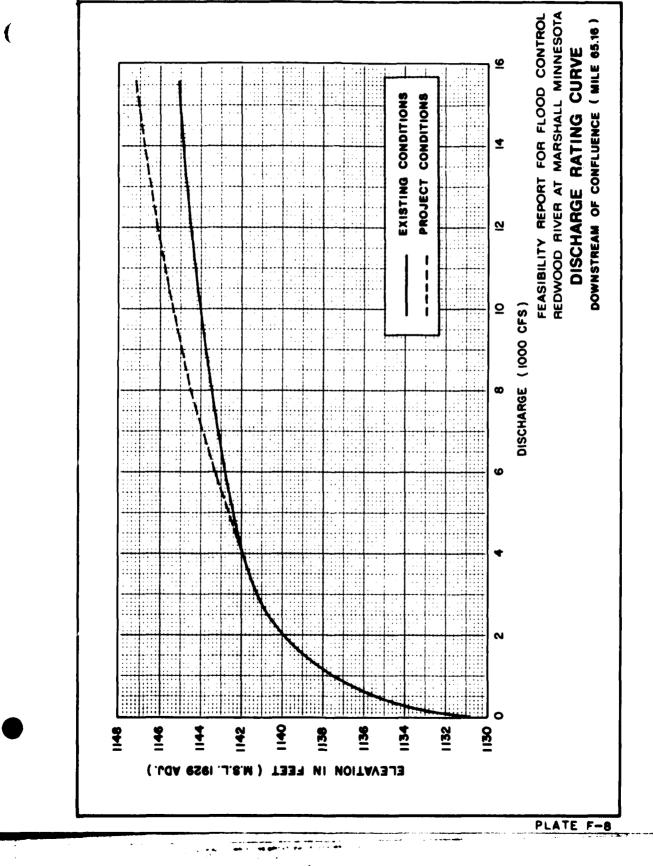
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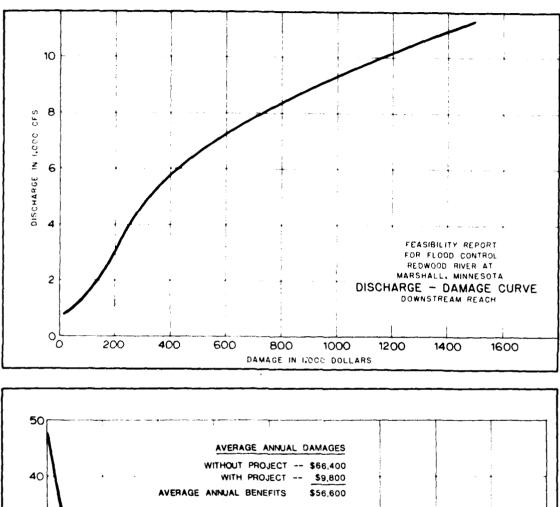


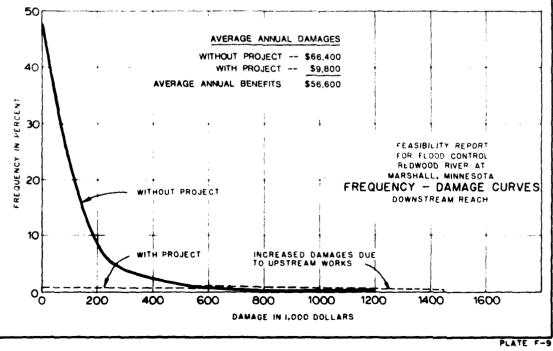
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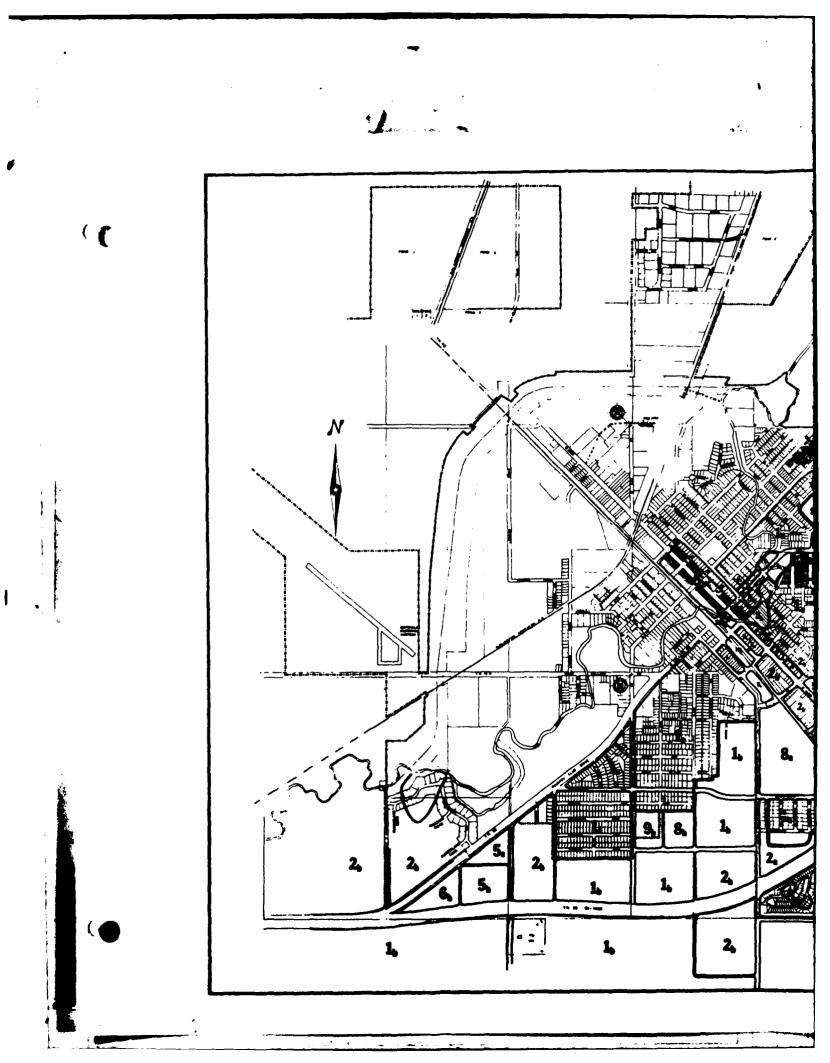


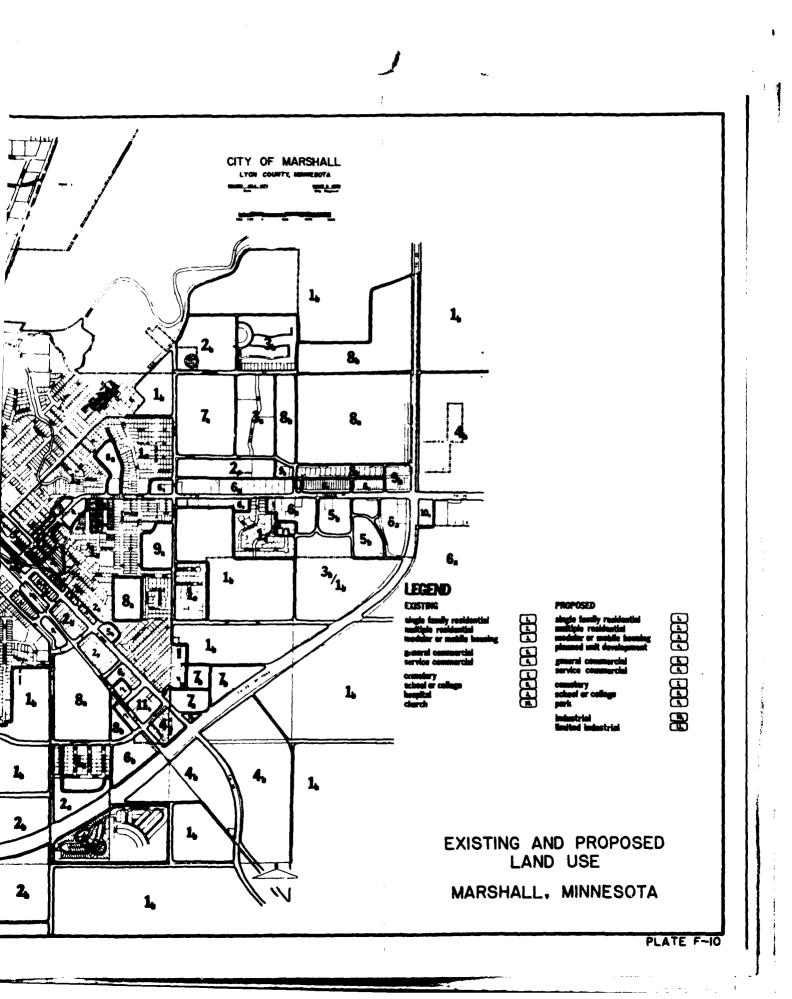
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# SECTION G

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## **RECREATION RESOURCES**

## SECTION G

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## RECREATION RESOURCES

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G-3 Typical Recreational Facility Illustration

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#### SECTION G

### RECREATION RESOURCES

## AUTHORITY

1. Section 4 of the 1944 Flood Control Act, as subsequently amended by Section 207 of the 1962 Flood Control Act, grants the Corps of Engineers general permissive authority to construct recreational developments at all water resource developments under control of the Secretary of the Army. The Federal Water Project Recreation Act of 1965 (P.L. 89-72) established development of the recreational potential at Federal water resource projects as a full project purpose. Corps policy (ER1120-2-404) establishes guidelines for cost sharing agreements on local flood control projects in keeping with the principles of P.L. 89-72).

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## PURPOSE

2. This report section appraises area recreation resources and facilities, provides estimates of the magnitude of existing and projected growth of public use, and identifies additional needed resources. It also displays the optimum scale of initial and future recreational developments, related costs and benefits, and location and extent of lands to be acquired for public use.

#### SCOPE

3. The investigation of recreational resource needs at Marshall considered geographically, the same upstream and downstream reaches of the flood control study and the existing diversion channel rightof-way. Specific elements of the study were established early in project efforts. Specific study elements investigated included the need for:

- A combined bike-walking and a cross-country ski trail along the proposed levee alignments or river corridor commencing at the State Highway 23 roadside park and extending downstream via the existing diversion channel and proposed levee works to the Highway 23 service drive north of the college.
- Limited picnicking facilities at Justice Park in conjunction with the proposed levee works.

o The need for quiet area development and nature education areas.

4. Lands quired for any considered recreational developments would, in accordance with current Federal policy, be limited to those lands acquired for the existing and proposed flood control project or immediately adjacent lands purchased entirely at local expense to provide access to considered developments.

5. At the onset of this study, local interests indicated a need (See Section C-Improvements Desired) for improvements to the softball complex located on existing diversion channel right-of-way just north of State Highway 19. However, these improvements are expected to be made in the near future in conjunction with contemplated modifications to the ball fields to accommodate the proposed diversion channel parkway and are thus not considered in this study.

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6. Required base resource information developed for the flood control study is also sufficient for this study and is documented in Section B of the appendix. Local interests have expressed a desire and willingness to participate in construction of the needed recreational facilities as indicated in a resolution (See Appendix II) passed by the Marshall City Council on 2 March 1979.

7. Background information used in this analysis included results of city-conducted user surveys; numerous discussions with the city recreation planner, other city officials, a local member of the Governor's Trails Advisory Committee, and local sporting goods stores. It also included analysis of the 1974 State Comprehensive Outdoor Recreation Plan with accompanying "Projections Methodology Report", and results of a 1974 user survey for nearby Camden State Park.

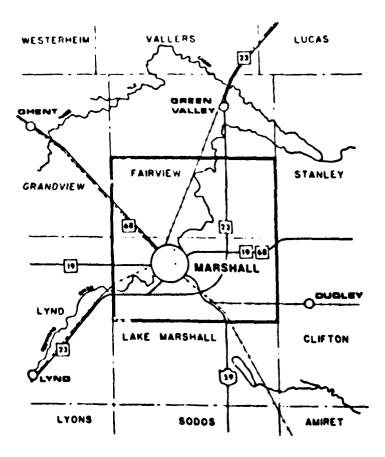
## RECREATION MARKET AREA

#### RECREATION ZONE OF INFLUENCE

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8. The area that can be expected to contribute 80 percent of the recreational day use includes the City of Marshall and the adjacent onehalf of each of the surrounding two townships. Only one-half of the population of each township (the half adjacent to Marshall) would be expected to frequently use facilities at Marshall. Residents in the outer one-half of the Townships would more likely use the closer facilities at Garvin and Camden Parks. This contributing area would exclude competing day use at Camden State Park, 8 miles southwest of the city, and the Garvin County Park, located 12 miles south of Marshall. This investigation indicates that some of the present recreational

use at these two areas by Marshall area residents would undoubtedly revert to similar facilities at Marshall, if provided. This is particularly true of present school use of nature, educational and scientific facilities at these areas. Some usage of the considered facilities at Marshall could be expected from regional sports teams and informal groups outside the established market area during tournaments, but this usage is expected to be relatively minor. : )



#### PRESENT AND PROJECTED MARKET AREA POPULATION

Current (1970) population within the zone of influence is shown on Table G-1.

| lable | 6-1 | Popul. | it ion 1/ | in | Lone | of | Influence |
|-------|-----|--------|-----------|----|------|----|-----------|
|       |     |        |           |    |      | _  |           |

| Area                   | Population        |
|------------------------|-------------------|
| City of Marshall       | 9,886             |
| Fairview Township      | $300\frac{2}{2}$  |
| Lake Marshall Township | 379 <sup>2/</sup> |
| Total                  | 10,565            |

 $\frac{1}{1970}$  U.S. Census statistics

 $\frac{2}{2}$  One-half of Township population.

9. Although the southwest region of Minnesota is expected to experience a continuing population decline, Marshall is expected to grow but at a declining rate. Future growth at Marshall is most probably due to the City's strong position as the regional retail trade and farm service center. The presence of the Southwest State College, expanded air service facilities, and new shopping centers are all expected to maintain Marshall's positive growth posture in relation to the rest of the region. The two contributing Townships are expected to incur continuing population losses, due either to migration to Marshall or annexation by Marshall. In either case, the contributing day use population would remain about the same. Projected population within the zone of influence is shown on table G-2.

#### Table G-2 - Projected Population within Zone of Influence

| Area                   | 1980   | 2000   | 2030   |
|------------------------|--------|--------|--------|
| Marshall               | 11,856 | 15,436 | 20,375 |
| Fairview Township      | 325    | 300    | 275    |
| Lake Marshall Township | 350    | 325    | 300    |
| Total                  | 12,531 | 16,061 | 20,950 |

 $\frac{1}{M_{\text{innesota Department of Health, et al.}}$ 

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#### RECREATION DEMAND

10. The enjoyment of leisure time always has been and continues to be an important activity at Marshall. To help meet the needs of this continuing activity, the City and Lyon County have developed a system of attractive existing parks and other recreational facilities. However, these facilities fall far short of meeting current demands for some area activities, such as bicycling, picnicking and cross-country skiing. Camden State Park, 8 miles southwest of Marshall is the only regional state park convenient to Marshall.

11. Existing recreational facilities in the Marshall area are shown on plates G-1 and G-2. Supporting data on the capacity of existing facilities in the market area is presented in table G-7 entitled "Existing Facilities Serving Market Area:. An increasing shortage of needed recreational facilities is particularly true at Marshall which is increasing in population while other areas in the region are losing people. Activities and related facility needs considered for analysis were selected based on known project resource capacities and identified market area needs as determined and documented by the contractor. A detailed discussion of the demand for area recreational activities is presented in the following paragraphs.

12. Bicycling is an increasing area activity as indicated by limited registration data and sales information. Current traffic, both functional and recreational, must use moderate to heavily travelled streets with a potential for auto-bicycling accidents. The City is presently planning a circumferential recreational bike trail system which would, in part, traverse the existing diversion channel right-

of-way and proposed levee works. This sytem would divert much of the recreational traffic off auto lanes. A portion of the city bike trail system along the diversion channel between CSAH 7 and State Highway 19 is expected to be completed prior to construction of any authorized project-related recreational improvements.

13. Picnicking, popular most everywhere, is increasing at all parks in the city. Present group picnicking facilities at Legion Park (plate G-1) are used on a reservation basis to permit optimum use. Only very limited facilities are available for northeast Marshall residents at Justic Park (plate G-2). The City desires further expansion of picnic facilities, quiet areas, play lots, etc. at this park. A summary of existing recreation facilities is shown on Table G-3.

14. The recognition of natural resources and aesthetic values is translated into an increasing nature walk activity. Presently limited by inadequate public access to the river corridor, this activity would be participated in by both the casual observer and organized school education groups. Local interest indicates that area high school students involved in nature education and ecology classes must travel to other regional parks for field research activities with time consuming travel involved. This activity, as indicated, would most likely utilize local facilities, if provided.

15. Similarly, the demand for pleasure walking or pedestrian sightseeing is enjoying an increase. Again, however, the availability

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Table 0-3 - Existing Recreation Facilities at Marshall

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| Park or Picture Pictur | Picnic<br>Facilities | Les      | Playground<br>Equipment | Soft bull | Baseball | Tennis | Outside<br>Bisketball | Multi-Use<br>Hard Sur- | Sanitary  |
|--|----------------------|----------|-------------------------|-----------|----------|--------|-----------------------|------------------------|-----------|
| 1  | bles                 | Shelters | (area)                  | Fields    | Fieids   | Courts | Gurts                 | face Areas Facilities  | Facilitie |
| Legion Park  | 71                   | 1        | 1                       | C ł       | 1        | 9      | 1                     | ·                      | -         |
| Liberty Park   | 80                   | 7        | 64                      | ı         | ۱        | ١      | ·                     | ı                      | 1         |
| Justice Park   | •                    | ·        | -1                      | ,         | ł        | ·      | ·                     | ı                      | ı         |
| Freedom Park   | 4                    | ı        | 1                       | 1         | ı        | ı      | <b>C1</b>             | ı                      | 1         |
| Jiversion Channel<br>Jallfield complex   | י<br>א ד             | ı        | ,                       | 4         | ,        | ŗ      | ı                     | ،                      | ·         |
| Highway 23 Road-<br>side Park  | 9                    | ,        | •                       |           | ·        | ۲      | ı                     | ı                      | 1         |
| <del>d</del> ign School <u>1</u> /   | •                    | ۱        | ı                       | ı         | 1        | ı      | •                     | ı                      | ı         |
| west Side Elemen-<br>tary School <sup>1</sup>  | ,                    | ۲        | 1                       | ·         |          | 1      | ı                     | 1                      | •         |
| East Side Elemen-<br>tary School <u>l</u>  | 1                    | ı        | 1                       | ~         | ·        | ŀ      | ı                     | 1                      | •         |
| Firochial School   | 1                    | ı        | 1                       | ı         | •        | ı      | ı                     | 1                      | ı         |
| Southwest State<br>University <sup>1/</sup>  | •                    | ·        | ı                       | 'n        | 1        | ę      | ı                     |                        | ,         |

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of public access to the river setting is restricted. A continuous trail along the river corridor at Marshall would offer vastly increased visual-hiking opportunities.

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16. Although no documented data is available, bird watching along the river is significant at Marshall. The annual visitation of transient waterfowl provides the most important present focus for this activity. Two state-noted ornithologists provide guidance and field leadership in this area activity. Local interests again indicate that public access to wooded songbird habitat and other areas restricts this activity. A companion activity, wildlife photography, though not a major activity, is enjoyed by the bird watchers, plant and animal researchers and others. Again, the demand for improved access to conducive habitat is indicated.

17. Local sales figures indicate that the sales of cross-country skis have increased 75 fold at Marshall in the last five years. With no designated or improved trails, local enthusiasts must make use of open hospital, cemetery, and school grounds. With increasing demands for informal and weekend tour group use, the City desires an improved ski trail in conjunction with a biking trail if possible.

18. Other recognized recreational activities and related resource problems includes a minimal springtime canoeing activity. Canoeing needs generally relate to the lack of convenient accesses.

19. In support of local trends, the Minnesota State Comprehensive Outdoor Recreation Plan (SCORP) indicates a continued demand for regional (region 8) recreational facilities as shown on table G-4. Facility needs for picnicking are projected to increase about 8 percent between years 1975 and 1990. A statewide 1990 increase of 32 percent is projected for pleasure walking.

#### Table G-4 - Projected Region 8 Facility Needs (SCORP-1974)

| Activity   | Unit             | 1975                             | <b>198</b> 0 | 1990        |
|------------|------------------|----------------------------------|--------------|-------------|
|            |                  |                                  |              |             |
| Bicycling  | Miles            | <u>1</u> /                       | 1/           | 1/          |
| Picnicking | No. of<br>tables | $\frac{2}{1188}(-216)\frac{3}{}$ | 1280 (~308)  | 1287 (-315) |
| Canoeing   | Stream<br>Miles  | 38 (+58)                         | 44 (+52)     | 51 (+45)    |

1/ No SCORP facility requirements for bicycling.

2/ Projected facility requirements.

3/ Projected surplus or deficiency of facilities as compared to 1972 SCORP base conditions (+ denotes surplus)

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## DETERMINATION OF OUTDOOR RECREATIONAL ATTENDANCE PER CAPITA PARTICIPATION RATES

20. The following paragraphs present a discussion of the methodology used to determine per capita participation rates for expected activities and the assumptions made to adjust the regional rates to reflect local conditions in the study area. Also discussed is the expected annual participation for the various activities as measured in visitor days for the years 1980, 2000 and 2030.

21. Per capita participation rates developed for the recreational activities expected at the project reflect the limited marked area, short travel distances involved, and mix of opportunities provided. In the absence of documented local user data, the rates displayed in table G-5 were determined from discussions with the City recreation director and other interests knowledgeable on local day use characteristics, an analysis of rates provided in the SCORP, and a review of the Bureau of Outdoor Recreation's 1969 participation rates published for the West North Central Region. Major departures from the SCORP rates were reductions in rates for bicycling,

walking for pleasure, and canoeing. Rates for cross-country skiing were derived from an analysis of the local activity without the benefit of comparative values from other sources.

## ASSUMPTIONS AFFECTING DEVELOPMENT OF LOCAL PARTICIPATION RATES

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22. The present and projected participation in area bicycling can be expected to follow the state trend of an increasing rate of adult use with a declining rate of increase for sub-adult use. Local bicycle retail outlets confirm this observation via the recent and continuing increase in new and used bikes to area adults. Although widely popular for both functional and recreational use, the extent of local participation is expected to be inhibited for some time to come due to the limited availability of separate and safe bikeways.

23. Local participation in walking for pleasure in the project area is not expected to equal the state average. While a significant activity, it is not expected to reach the status of a similar recreation experience enjoyed -- say in walking through a continuous developed parkway or greenbelt area. A 1980 value for this local activity would appear to be about one-half of the statewide figure of 10.0.

24. Increasing local participation in cross-country skiing is evident by the 75-fold increase in ski sales over the last 5 years. Local enthusiasts estimate the extent of this activity to be at least equal to the recreational bicycling activity. Lower than SCORP rates for the local canoeing activity are indicated due to the relatively short six-week duration and fairly unique nature of this spring high water activity which appeals to a limited sector of the population.

25. All of the activities are expected to experience some increase in rates of participation as shown in Table G-5. With minor exceptions, these projected increases are generally expected to follow statewide trends to year 2000. Projected rates for year 2030 generonly represent a declining rate of increase after year 2000, or in a few instances, a straight-line projection of the 1990-2000 rate of increase.

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|                      |      | ted Rat<br>rket Ar |      | SCORP R<br>for Reg |            |
|----------------------|------|--------------------|------|--------------------|------------|
| Activity             | 1980 | 2000               | 2030 | 1980               | 1990       |
| Bicycling            | 20.0 | 24.4               | 27.1 | 48.0               | 54.3       |
| Picnicking           | 5.7  | 6.9                | 8.7  | 5.7                | 6.3        |
| Nature walks         | 1.0  | 1.08               | 1.21 | <u>2</u> /         | <u>2</u> / |
| Walking for pleasure | 5.0  | 5.8                | 6.2  | 10.0               | 11.0       |
| Bird watching        | 1.10 | 1.28               | 1.32 | <u>2/</u>          | <u>2</u> / |
| Wildlife photography | 0.19 | 0.25               | 0.34 | <u>2/</u>          | <u>2/</u>  |
| Cross-country skiing | 1.8  | 2.2                | 2.6  | <u>2</u> /         | <u>2</u> / |
| Canoeing             | 0.20 | 0.22               | 0.29 | 0.86               | 1.04       |

### Table G-5 - Participation Rates

 $\frac{1}{No}$  SCORP rates available for year 2000 and 2030.

 $\frac{2}{No}$  SCORP rates (1974 report) for these activities.

## INITIAL AND PROJECTED ATTENDANCE

26. Total potential annual participation in each of the given activities is obtained by multiplication of the established participation rates by the market area population. Annual attendance expressed in annual activity occasions and visitor days for years 1980, 2000, and 2030 is given in table G-6.

Table G-6 - Total Projected Annual Activity Occasions Within Market Area

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|                               |               | 1980          |       | 2000        |        | 2030       |
|-------------------------------|---------------|---------------|-------|-------------|--------|------------|
|                               | Pop<br>Farti- | Pop - 12, 531 | Pop   | Pop. 16,061 | Pop.   | Pop 20,450 |
|                               | cipa-         | Annual        | cipa- | Annul       | CIDA-  | Annual     |
|                               | t Lon         | Activity      | tion  | Activity    | t ton  | ACTIVITY   |
| Activity                      | Rate          | Occasions     | Rate  | Occasiens   | Rate   | Occasions  |
| Bicycling                     | 20.0          | 250,620       | 24.4  | 391,588     | 27.1   | 567,745    |
| Picnicking                    | 5.7           | 71,427        | 6.9   | 110,821     | ۲<br>8 | 182,265    |
| Nature walks                  | 1.0           | 12,531        | 1.08  | 17,346      | 121    | 25,350     |
| Walking for pleasure          | <b>5</b> .0   | 62,653        | 5.8   | 93,154      | 6 2    | 129,590    |
| Bird watching                 | 1.10          | 13, 784       | 1 28  | 20,558      | 1.32   | 27,654     |
| Wildl:fe photography          | 0.19          | 2,381         | 0.25  | 1,015       | 0.34   | 7,123      |
| Cross-country skiing          | 1.8           | 22,556        | 2.2   | 34,334      | 2.6    | 54,470     |
| Canoeing                      | 0.2           | 2,506         | a.22  | 3,533       | 0.29   | 6,0~5      |
| Totals                        |               | 438,460       |       | 676,649     |        | 1,000,572  |
| Total visitor-days <u>1</u> / |               | 175,384       |       | 270,660     |        | 400,229    |

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Visitor-days = Activity occasions + 2.5 Term "Visitor-Day" is synonymous with "Recreation-Day" in Supplement No. 1 to Senate Document 99. '\_ /

## LAND AND FACILITY REQUIREMENTS

#### GENERAL

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27. The determination of land and facility needs to meet present and projected usage is obtained as the difference between needs determined via a design-day load-facility load criteria analysis and suitable existing facilities.

## FACILITY LOAD CRITERIA

28. Facility load criteria for the considered recreational resource needs is based on the maximum use rate which will still permit a relaxing and pleasing experience. Specific criteria are based on accepted industry and governmental planning standards as available. Others, such as for cross-country skiing were based upon an examination of the potential resource capability such as trail length, governing grades, ingress and egress, and shelter. No criteria is established for bird watching and wildlife photography since spatial demands for these activities can be reflected in walking trail criteria. Only limited needs for additional canoeing stream miles are indicated for the project area. However, the lack of an improved canoe access at or near the un-supervised roadside park results in continued safety hazard for persons landing or launching canoes at the steep river banks. These potential threats to public safety are even more acute during the most favorable spring high water canoeing period. Facility load criteria for selected activities is given in table G-7.

#### DESIGN DAY LOAD

29. To convert total visitation to required facilities, the following formula was used to compute the design day load as peak weekend day use for each activity.

L =  $\frac{(a - 1)}{(2.5w)}$  d where L = design day load a = seasonal attendance expressed as a percent of total annual attendance w = number of weeks in normal recreation season d = weekend day use as a percent of weekly use 2.5 = factor used to convert annual activity occasions to annual recreation days.

To illustrate the use of this relationship, the following computation is shown for expected 1980 design picnicking day use in visitor days.

 $a = 0.80^{\frac{1}{2}} \times 1.42^{\frac{1}{2}} = 57,142$   $d = 0.3^{\frac{1}{2}}$  w = 13 $l = \frac{57,142}{2.5 \times 13} \times .3 = 527$ 

 $\frac{1}{2}$  Percentage equals seasonal use divided by total annual use.

 $\frac{2}{2}$  Fercentage equals design Sunday use divided by total week use.

Similar computations for projected years 2000 and 2030 give design day use values of 818 and 1346 respectively. Design day use values for all activities are also given in table G-7.

#### **REQUIRED FACILITIES**

30. Applying the facility load criteria to the computed market area design day use values provides the total number or extent of required facilities. Required facilities for bicycling, picnicking, nature walks, walking for pleasure, cross-country skiing, and canoeing are given in table G-7.

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Table G-7 - Determination of Required Lands and Facilities

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|                      |                |       | 1            | Facility Load Criteria<br>Turn- | teria<br>Turn- | Total F<br>quired | Total Facilities Re-<br>ouired to Serve Mar- | s Re-<br>Mar- |
|----------------------|----------------|-------|--------------|---------------------------------|----------------|-------------------|--|---------------|
|                      | Design Day Use | Day L | Jse -        | 6                               | over           | ket Are           | ket Area Population                          | tion          |
| Activity             | 1980           | 2020  | 2020 2030    | Unit Load Ra                    | Rate           | 1980              | 2000   | 2030          |
| Bicycling            | 948            | 1447  | 20 <b>96</b> | 10 bikes/mile                   | æ              | 11.9              | 18.1   | 26.2          |
| Picnicking           | 527            | 818   | 1346         | 4 persons/table                 | 7              | 66                | 102  | 168           |
| Cross-country skiing | 271            | 412   | 654          | 20 persons/mi./hr.              | 9              | 2.3               | 3.4  | 5.5           |
| Nature walks         | 46             | 64    | 94           | 4 persons/mi./hr                | Ŷ              | 1.9               | 2.7  | 3.9           |
| Walking for pleasure | 202            | 301   | 420          | 16 persons/mi./hr.              | 4              | 3.1               | 4.7  | 6.6           |
| Bi rdwatching        | 34             | 51    | 68           | ;                               | ;              | :                 | :  | ;             |
| "lulife photography  | 14             | 24    | 43           | ( ,                             | ;              | :                 | 1  | *             |
| Canoeing             | 25             | 35    | 61           | 17.2 persons/<br>stream mile    | 20             | 0.7               | 1.0  | 1.8           |
|                      |                |       |              |                                 |                |                   |  |               |

1/ Calculated design-day for cross-country skiing is based on a 10-week season from 25 December to 7 March. The canoeing season extends over a 6-week period between 15 April and 1 June. All other activities are based on a 13-week summer season.

## PROPOSED RECREATIONAL IMPROVEMENTS

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## DESCRIPTION

31. The proposed recreation improvements as shown on Plates G-1 and G-2 would generally consist of a 5.2 mile long by 8-foot wide paved biking-walking trail including trail head facilities, a rest stop and benches; a 5.7 mile long cross-country ski trail; and limited picnic facilities at the softball complex and on project lands at Justice Park. Local improvements to provide a continuous trail system would include a 0.6 mile section of bike-walking trail between CSAH 7 and State Highway 19 (See Plate G-1) and a 0.3 mile section of both bike-walking trail and cross-country ski trail extending westward from County Highway 67 as shown on Plate G-2. The 0.6 mile bike-walking trail is currently in the planning stages and is expected to be completed prior to any authorized federally cost-shared improvements. The 0.3 mile section of trail upstream of County Highway 67 would be constructed by local interests on non-project lands adjacent to the proposed parkway at the time of construction of any authorized recreational improvements.

32. The proposed bike-walking trail would extend from the eastern terminus of the downstream reach levee (Plate G-2) upstream along the existing diversion channel to the CSAH 7 bridge (Plate G-1) and provide a much needed facility, largely free of conflicts with motorized vehicles. The trail would offer a variety of visual and other sensory experiences. These experiences would occur in an open prairie environment -- unprotected from the elements, a linear "closed in" environment, and possibly in the future with an upstream extension, a natural wooded - streamside environment. Although much of the proposed trail would be nearly flat, a number of slopes to seven

Appendix I G-18

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and one-half percent would challenge the bike rider as well as the pleasure walker. A rest area is proposed as part of the improvements at the playfield facilities north of U.S. Highway 19. The proposed trail would be hard surfaced with a bituminous mat. Typical sections showing how the trail would relate to the levees, the diversion channel, etc. are given on plate G-3.

33. Trail head facilities would be located at each end of the trail system. A trail head with drinking water, toilet facilities, bike racks, and parking area would be located at the eastern or downstream trail terminus at the service drive adjacent to State Highway 23 (See plate G-2). Pedestrian or bike access to these facilities would be provided by an 8-foot wide gravel trail from the college area and which would be constructed at local expense. Existing park facilities would satisfy similar trail-end needs at the upstream terminus of trail system at the Highway 23 wayside park as shown on Plate G-1. Also included as part of the trail facilities would be a rest stop with a shelter, toilet, and drinking facilities, and benches as illustrated in Sketch I on Plate G-3.

34. The trail system along the existing diversion channel right-ofway would pass over or under four highway and three railroad bridges as dictated by available clearance. Timber retaining walls would be used to retain diversion channel side slopes along trail crossings under bridges. A typical trail crossing incised into the diversion channel side slope is illustrated on Section B-B of Plate G-3. Where bridge clearances are inadequate, marking signs would be provided at the two-street level trail crossings required.

35. Upstream of CSAH, the proposed trail system would traverse project lands to be acquired for floodway purposes. Two 8-foot wide timber bridges would be provided in this reach as shown on Plate G-1. An illustration of a proposed typical bridge is given in Sketch 3 of Plate G-3.

**36.** The cross-country ski trail generally would follow the alignment of the bike-walking trail except that it may freely transgress the invert of the diversion channel whereas the bike-walking trail could not. The ski trail, therefore, would generally occur on the north and west side of the diversion channel and traverse proposed wooded areas. These new wooded areas would provide protection from wind as well as improve and preserve snow cover. The relationship between the ski trail and the bike-walking trail is illustrated on plate G-3.

37. Limited picnic facilities are proposed as part of the improvements on project lands at Justice Park and at the outdoor games area located north of U.S. Highway 19. It is anticipated that the proposed limited picnic facilities at the softball complex rest stop would serve both trail users, softball players and spectators. A sketch showing possible arrangements of these latter facilities is shown on plate G-3.

38. Planting improvements are also included as part of the proposed development for the west and north side of the diversion channel and the rest area at the outdoor games area north of U.S. Highway 19. A very high priority should be assigned these improvements for reason described earlier and perhaps more importantly, to upgrade the general character of the recreational area.

39. A future rest area and picnic facilities desired by the community at Justice Park, which would complement the proposed trail systems, might include additional picnicking equipment; nature trails and quiet area development, added child play area, tree and shrub planting, toilet and drinking water facilities, and hard surface parking area. Local planning efforts for these facilities which would be provided by the City at its own expense are currently underway.

40. A substantial area for nature walks, bird watching and wildlife photography is located between the Minnesota Highway Department's Highway 23 wayside park and CSAH 7. Use of this area would be compatible with the proposed use of the area as a designated floodway. Nature trails that would link to the biking trail would be located in the future by local interests within the area after careful field study.

41. Implementation of the proposed recreational improvements would provide facilities which are generally unavailable within the Marshall service area at the present time. They could be provided at a moderate cost by utilization of the existing and proposed flood control facilities for location of these improvements.

#### AREA MANAGEMENT CONCERNS

42. A potential management problem could be the unauthorized use of motorized vehicles on the trail. The project sponsor would be expected to prohibit access to motorized vehicles. Vertical timber or other suitable barriers would be provided at trail access points to bar the use of these vehicles. Although some occasional conflicts may occur, the simultaneous trail use by bicyclists, wheelchair patients, and pedestrians along some segments is considered manageable. Occasional rest and widened areas on the trail would help maintain a suitable balance of activities on the trail. Skiing on the bicycle trail is not provided for nor encouraged due to the hard paved surface and expected lack of continuous snow cover on the levee crown.

43. Also of some local concern is the close proximity of the proposed

trails to nearby residences immediately upstream of CSAH 7. Chain-link fencing and screen plantings would be provided to screen the trail from view and prohibit indiscriminate entry on non-project lands.

## CAPABILITY OF PROJECT TO SATISFY EXCESS DEMAND

44. Construction of the proposed facilities would satisfy part or in some cases all of the projected demand within the market area. Results of an analysis of project-related capability is given in table G-8.

## DETERMINATION OF RECREATION BENEFITS

#### GENERAL

45. The derivation of project recreation benefits is dependent on actual project-related use, the extent of facilities which can be accommodated with the proposed flood damage reduction measures and application of a dollar unit recreation day value to the average annual recreation day value. Total recreation day use is discounted over a 50-year project life at a 6 7/8 percent interest rate. $\frac{1}{2}$ 

#### PROJECT-RELATED USE

A potential management problem could be the unauthorized use of motorized vehicles on the trail. The project sponsor would be expected to prohibit access to motorized vehicles. Although some occasional conflicts may occur, the simultaneous trail use by bicyclists, wheelchair patients, and pedestrians along some segments is considered manageable. Occasional rest and widened areas on the trail would help maintain a suitable balance of activities on the trail. Skiing on the bicycle trail is not provided for nor encouraged due to the hard paved surface and expected lack of continuous snow cover on the levee crown.

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|   | Ferina. | to i Dec | ion Dav       | Fernated Design Day Maximum  | Demand Met              |             |                      |          |                                  |         |          |
|---|---------|----------|---------------|------------------------------|-------------------------|-------------|----------------------|----------|----------------------------------|---------|----------|
|   | 1.1     |          | (m.)          | Project<br><b>Decion Dav</b> | By Exist-<br>ing Facil- | Tat . 1     | Tat 1 'Inmet flaman' | f. ne Ha | Unmet Facility Require-<br>ments | ulity R | equite-  |
| ACTIVITY  | 1950    | 0007     | 2030          | Use Car                      | Ities                   | <b>NS61</b> | 2000                 | 2030     | 1980                             | 2000    | 2030     |
| Bicycling                                       | \$15    | _ tt I   | 2096          | 440                          | 240                     | 268         | ے'<br>ت              | 1416     | -E + 4                           | 9.6     | 1.1      |
| Picnicking                                      | 527     | 818      | 1346          | <b>8</b> U                   | 012                     | 207         | 198                  | 1026     | 26                               | 62      | 128      |
| Nature walks                                    | ;<br>†  | 64       | 76            | 40 (est.)                    | 0 <u>2</u> /            | ¢           | 77                   | 54       | 0 2 mr.                          | 1 0     | ri<br>ri |
| Malking for<br>Fleasure                         | 202     | 301      | 024           | 108 (eit.)                   | 0 <u>3</u> /            | 3           | 193                  | 312      | 1.5 ml                           | 3 O     | ი<br>+   |
| <b>Bird watching</b>                            | 54      | 51       | 68            | ;                            | •                       | Note        | Not estimated        |          | ;                                | +       | ;        |
| hildlife photo-<br>graphy                       | . =     | 24       | 43            | :                            | ;                       | Not e       | Not estimated        |          | ;                                | ł       | ;        |
| Cross-country<br>skiing                         | 271     | 214      | 654           | 552                          | σ                       | o           | 0                    | Ø        | 0 mi.                            | σ       | 0        |
| Canoeing  | 25      | 35       | 61            | 61+                          | D                       | Ð           | D                    | 0        | 0                                | σ       | σ        |
| 1/ Number of persons on a decign caseon Sunday. | sons on | a deci   | 90 <b>9</b> 3 | on Sundau                    |                         | 1           |                      |          |                                  |         |          |

wer of persons on a design season Sunday.

 $\frac{2}{3}$  / Presently utilized undeveloped walking areas not evaluated.  $\frac{3}{3}$  / No estimate made of extent of city streets and open areas presently used.

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|                      | Projec | ated Max<br>ct Capao<br>Percent<br>Use | city | Projec | ated Act<br>of Use a<br>nt of To<br>i | as a |
|----------------------|--------|--|------|--------|---------------------------------------|------|
| Activity             | 1980   | 2000                                   | 2030 | 1980   | 2000                                  | 2030 |
| Bicycling            | 46     | 30                                     | 21   | 20     | 20                                    | 20   |
| Picnicking           | 15     | 10                                     | 6    | 10     | 10                                    | 6    |
| Nature walks         | 87     | 63                                     | 43   | 20     | 20                                    | 20   |
| Walking for pleasure | 53     | 36                                     | 26   | 10     | 10                                    | 10   |
| Bird watching        | -      | -                                      |      | 20     | 20                                    | 20   |
| Wildlife photography | -      | -                                      | -    | 15     | 15                                    | 15   |
| Cross-country skiing | 83     | 186                                    | 117  | 25     | 25                                    | 25   |
| Canoeing             | -      | -                                      | -    | 0      | 3                                     | 3    |

## Table G-9 - Estimated Actual Project-Related Recreational Use

47. What table G-9 indicates, say for bicycling, is that while the proposed trail could accommodate 46 percent of the total 1980 market area demand (72 percent of the 1980 demand including existing facilities), it is unlikely that this level of actual utilization would be reached. As indicated, for reasons of constraints discussed previously a more realistic estimate of project utilization would be about 20 percent. Particularly, as in the case of pleasure walking, the actual estimates attempt to account for the unestimated available quantities of less desirable present facilities which are available.

Appendix I G-24

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48. As evident in the table, some project-related use for nature walks, walking for pleasure, bird watching, and wildlife photography can be expected generally as the result of improved public access to the riverine corridor. Adjusted project-related recreational use in total activity occasions based on proposed facility capacity and estimated use is given in Table G-10.

(

| Activity                     | Per-<br>cent<br>Effi-<br>cient | <u>1980</u><br>Adjusted<br>Activity<br>Occasions <sup>2/</sup> | Per-<br>cent<br>Effi-<br>cient | 2000<br>Adjusted<br>Activity<br>Occasions | Per-<br>cent<br>Effi-<br>cient | 2030<br>Adjusted<br>Activity<br>Occasions <sup>2/</sup> |
|------------------------------|--------------------------------|--|--------------------------------|---|--------------------------------|---|
| Bicycling                    | 20                             | 50,124   | 20                             | 78,278                                    | 20                             | 113,549   |
| Picnicking                   | 10                             | 7,140  | 10                             | 11,082                                    | 6                              | 18,226  |
| Nature walks                 | ; 20                           | 2,506  | 20                             | 3,469                                     | 20                             | 5,070   |
| Walking for pleasure         | 10                             | 6,265  | 10                             | 9,315                                     | 10                             | 12,989  |
| Bird watchin                 | ng20                           | 2,757  | 20                             | 4,117                                     | 20                             | 5,531   |
| Wildlife<br>photography      | 15                             | 357  | 15                             | 602                                       | 15                             | 1,068   |
| Cross-counti<br>skiing       | ry<br>25                       | 5 <b>,639</b>  | 25                             | 8,833                                     | 25                             | 13,617  |
| Canoeing                     | 0                              | 0  | $3^{3/2}$                      | 106                                       | 3                              | 182   |
|                              |                                |  |                                |   |                                |   |
| Total Adjust<br>Activity Occ |                                |  |                                |   |                                |   |
| sions                        |                                | 74,788   |                                | 115,902                                   |                                | 175,232   |
| Recreation o                 | $lays^{4/}$                    | 29,915   |                                | 46,360                                    |                                | 70,093  |

## Table G-10 - Adjusted Project-Related Recreational Use

 $\underline{1}/\text{Estimated}$  percent of peak day use that proposed facilities would satisfy as given in Table G-9.

 $\frac{2}{A}$  Adjusted activity occasions = Activity Occasions (table G-6 x Percent Effective (project-related).

 $\frac{3}{0}$  Only minor use attributed to improved river access in future years.

<u>4</u>/Recreation days = Activity Occasions ÷ 2.5 (average number of activity occasions per recreation-day).

49. The growth of recreation day use at the proposed project recreation facilities is shown graphically on figure G-1. Also shown

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is expected attendance three years after construction of the recreation features. The following methodology was used to compute average annual recreation day use. Specific area designations correspond to those shown on figure G-1.

#### Area A

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| Rate of increase per year (32,511 + 3)           | = | 10,837  |
|--|---|---------|
| Value of increasing annuity for 3 years @ 6-7/8% | = | 5.144   |
| Interest and amortization over 50 years          | 3 | 0.07132 |

Ave. ann. recreation days = (10,837) (5,172) (0.07132) = 3,997

#### Area B

| = 32,511  |
|-----------|
| = 13.9064 |
| = .8192   |
| = .07132  |
|           |

Ave. Ann. Recreation days = (32,511) (13.9064) (0.8192) x (0.07132) = 26,415

#### Area C

(See Area A procedure). Rate of Increase =  $\frac{46360 - 32,511}{17 \text{ years}}$  = 815 Ave. ann. recreation days = (815) (73,2453) (0.8192) x (0.07132) = 3,485

### Area D

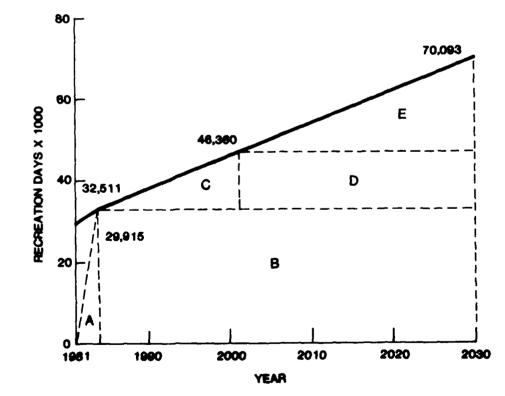
(See Area B procedure)

• 4.

Ave. Ann. recreation days = (13,849) (12.5665) (0.2645) x (0.07132) = 3,285

> Appendix I G-27

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EXPECTED VISITATION

FIGURE G-1

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<u>Area E</u> (See Area A procedure)

| Ave.  | ann.   | recı | eation | days = $(79)$ | 1) (135,982) (0.2645) |   |        |
|-------|--------|------|--------|---------------|-----------------------|---|--------|
|       |        |      |        |               | x (0.07132)           | z | 2,030  |
|       |        |      |        |               |                       | _ |        |
| Total | L Avei | rage | Annual | Recreation    | Days                  | Ŧ | 39,212 |

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## ESTIMATE OF RECREATION BENEFITS

50. The 0.5. water Resources Council has established that unit dollar values for recreational experiences similar to those expected at Marshall range from \$0.75 to \$2.25 per recreation day. Recognizing that a suitable value is based on factors such as user willingness to pay, degree of opportunities provided, and the extent of development, a reasonable user day value for activities at Marshall is considered to be about \$1.10. Multiplying average innual recreation days of 39, 12 by this unit benefit value gives average annual recreation benefits of \$43,130.

## COORDINATION

(4) Active participants or agencies and interests providing imjust to the recreation study included the following:

Montresita Department of Natural Resources - Bureau of Environmental Planning and Protection Division of Parks and Recreation

Minnesota Department of Health

City of Marshall - City Engineer's Office Department of Parks and Recreation

Member, Governor's Trails Advisory Committee

Local sporting goods retail outlets.

52. Review and comment on this study element was also provided by the Federal, state, and local agencies listed in section A of this technical report. Late-stage meetings to discuss the proposed recreation facilities were held with City officials on 2 March 1978 and 2 April 1979. Based on these discussions, major changes, including addition of trail head facilities at the downstream end of the trail and the deletion of 0.6 miles of proposed hike trail between CSAH and State Highway 19 were made to the proposed recreation facility plan.

## IDENTIFICATION OF SPECIAL PROBLEMS

53. There is little potential for encroachment on proposed project areas because of the proposed levee project which should prevent further development of the presently undeveloped river corridor. Proposed facilities located within the existing diversion channel right-of-way would also be spared interim or future encroachment as this city-owned right-of-way is reserved for flood control and commensurate purposes only.

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54. The City of Marshall is presently planning a parkway (FAU 5764) along a portion of the diversion channel right-of-way. Maximum vehicle speeds on this route would be posted at 40 mph. Designs for this highway in the vicinity of the softball complex would necessarily include provisions for bicycle access from the trail system to the proposed rest stop. This parkway crossing could be accomplished with either an overhead or underground trail crossing. Because of the uncertain timing of the considered parkway at this time, development of designs for this crossing would be accomplished in post-authorization studies.

55. Gentle grades at trail access points and other features such as widened rest and passing areas and highly visible signs at two street level crossings would provide for wheelchair use and the elderly in conformance with existing city and college programs and facilities for these users. A few short trail segments along the diversion channel would traverse the channel slope at gentle grades under two highway bridges and three railroad bridges to avoid busy street and rail crossings.

56. No conflicts with other agency programs are expected as the proposed facilities would complement and be in concert with the City's flood control and recreational program.

## MANAGEMENT AND COST SHARING

#### CORPS RESPONSIBILITY

57. Section 4 of the Flood Control Act of 1944 (16 U.S.C. 460d), as amended by Section 207 of the Flood Control Act of 1962, grants general permissive authority to construct recreational developments at all water resource developments.  $\frac{1}{}$  The Federal Water Project Recreation Act of 1965 (PL 89-72) modifies section 4 authority by imposing requirements of non-Federal cooperation and cost sharing for recreation and fish and wildlife enhancement at projects authorized after 1 January 1965. This law requires matching local participation in terms of money and/or lands that will equal the Federal share. In this instance, if the local interests are not financially capable of participating, no Federal recreational development will be provided. Corps policy (ER1120-2-404) establishes guidelines for cost sharing agreements on local flood control projects in keeping with the principles of PL89-72.

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#### NON-FEDERAL RESPONSIBILITIES

58. The City of Marshall must provide all lands required for development and control of the proposed public use areas. Present policy indicates that lands are not eligible for credit towards the non-Federal sponsor's share of recreation development costs.

Of the proposed facilities, the Federal government would pro-59. vide one-half the cost of all features except for lands required for trail development. The City would operate, maintain, and replace without expense to the Federal Government the recreational areas and all installed facilities. If long-term repayment is elected, however, all costs, including interest, must be repaid within 50 years of the date of first use of the initial recreation facilities. If all or part of long-term repayment of the City's share of initial separable costs is to be financed through user fees, the schedule of such fees and the portion thereof dedicated to repayment are subject to renegotiation at intervals not exceeding 5 years. User fees can be collected and may be used to support operation and maintenance costs. Monies received from non-Federal interests shall be deposited in the Treasury as miscellaneous receipts. By a resolution of the City Council adopted 2 April 1979, the City of Marshall furnished assurances of its willingness and ability to meet conditions proposed for non-Federal assumption of responsibilities for development, operation, maintenance, and replacement of the proposed recreational facilities.

## ENVIRONMENTAL QUALITY

60. Public acceptance of the proposed recreational facilities would depend on its environmental and/or aesthetic quality. Various grass mixes, shrub and tree plantings would be provided to enhance wildlife habitat, improve aesthetics, and optimize the recreational experience. Overburden sections with plantings along the levee portion of the trail would provide rest and observation areas, and help blend the entire works into the natural setting.

## COSTS

#### FIRST COSTS

61. Estimated Federal and non-Federal first costs for the proposed facilities based on existing cost-sharing legislation are given in table G-11 and are based on October 1977 price levels. These costs are presently estimated at \$192,800 and \$192,800 respectively. Applying the President's proposed cost-sharing policies would result in Federal and non-Federal first costs of \$173,500 and \$212,100 respectively.

|      | Lubic  | 0.44            | isticateli                         | HIST COST I                | or Recreation                        | Facilities                       |                                      |
|------|--|-----------------|------------------------------------|----------------------------|--------------------------------------|----------------------------------|--------------------------------------|
| Iter |  | tuit            | quantity                           | Unit Cost                  | Federal<br>Cost                      | Non-Federal<br>Cost              | Total<br>Cost                        |
| 1.   | TRATE DEVELOPMENT  |                 |                                    |                            |                                      |                                  |                                      |
|      | Bicycle Trail and Ir   | ail He          | ы                                  |                            |                                      |                                  |                                      |
|      |  |                 |                                    |                            |                                      |                                  | A 17 030                             |
|      | convectional   | vd <sup>3</sup> | 19,416                             | 0.90                       | < 8,960<br>16,060                    | < 8,960<br>16,060                | \$ 17,920<br>32,120                  |
|      | Base Four-   | 99. V.          |                                    | 1.25<br>2.40               | 30,840                               | 30,840                           | 61,680                               |
|      | Wear course  | · · · ·         | 25,700<br>8.0                      | 675.00                     | 2,700                                | 2,700                            | 5,400                                |
|      | "eeding  | avre<br>Gere    | 1.3                                | 1,000.00                   | 900                                  | 900                              | 900                                  |
|      | <pre>(learing a soullying) Timber Retaining</pre>  |                 | ••                                 | .,                         |                                      |                                  |                                      |
|      | Walls  | 1.:.            | 2,450                              | 14.00                      | 14,350                               | 14,350                           | 28,700                               |
|      | Benches  | C.1.            | 10                                 | 110.00                     | 550                                  | 550                              | 1,100                                |
|      | Bike Backs   |                 | •                                  | 500.00                     | 500                                  | 500                              | 1,000                                |
|      | loilet building and  |                 |                                    |                            |                                      |                                  |                                      |
|      | brinking fount in  | ed.             | .'                                 | 34,500.00                  | 34,500                               | 34,500                           | 69,000                               |
|      | SIGDS  | ea.             | 30                                 | 30.00                      | 450                                  | 450                              | 900                                  |
|      | Bridges  | 00.             | .'                                 | se <b>.</b> 000.00         | \$6,000                              | 30,000                           | 60,000                               |
|      |  |                 |                                    |                            |                                      | <del>.</del>                     |                                      |
|      |  | - 41 - 14       | or il Bicache                      | - Itail                    | \$139,810                            | \$139,810                        | \$279,620                            |
| в.   | <pre>cross-toutty ki fr<br/>clearing soruthing<br/>Marking ofens<br/>frail Plantings<br/>free and shrab<br/>glatting</pre> | an din<br>ana L | l.s<br>≥_<br>l.jrm<br>(tal ≤ki Ir. | 1,000,00<br>30,00<br>24,00 | 6, 40<br>780)<br>1840(R)<br>5-194430 | 650<br>780<br>18,000<br>3-19,410 | 1,300<br>1,560<br>36,000<br>5 38,860 |
| 11.  | F11 N10 F130   | es Si           | 19 A.A - 19 M.A                    | LOPMENT                    | \$159,240                            | \$159,240                        | 5318,480                             |
|      | Ficnic <sub>1/</sub><br>Tables c.  | ۱.              | ]                                  | \$280.0                    | 90 8 <b>1,4</b> 00                   | : 1,400                          | \$ 2,800                             |
|      |  | Sub-L           | stal "icnick                       | ing                        | 1,400                                | 1,400                            | 2,800                                |
|      |  | TOTAL           | CONSTRUCT U                        | S (084                     | \$160,640                            | \$160,640                        | \$321,280                            |
|      |  | Contin          | ngencies (20                       | (°)                        | 32,160                               | 52,160                           | 64,320                               |
|      |  | Engine          | ering and D                        | esign (10%)                | 19,200                               | 19,200                           | 38,400                               |
|      |  | Super           | vision and A                       | dmivistrati                |                                      | 9,600                            | 19,200                               |
|      | TOTAL FIR:   | 51 COST         | - PROPOSED                         | DEVELOPMENT                | \$221,600                            | \$221,600                        | \$443,200                            |

#### Table (11) Estimated First Cost for Recreation Facilities

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1/Federal cost sharing in picnic tables on flood control project lands only.

## Appendix 1

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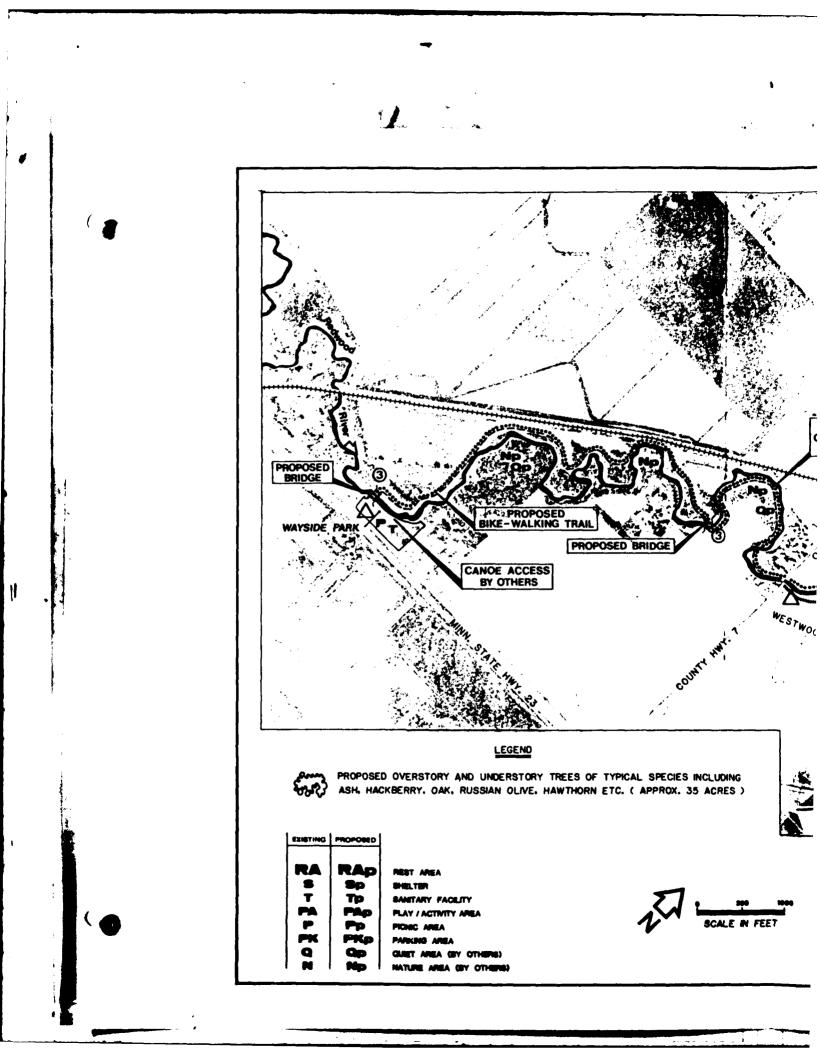
62. Estimated Federal and non-Federal annual costs, including non-Federal operation and maintenance costs, and based on existing costsharing legislation are shown in table G-12 below. The operation and maintenance costs reflect annualized costs of periodic trail maintenance, annual grooming, periodic repair of other facilities and normal trash removal and clean-up activities.

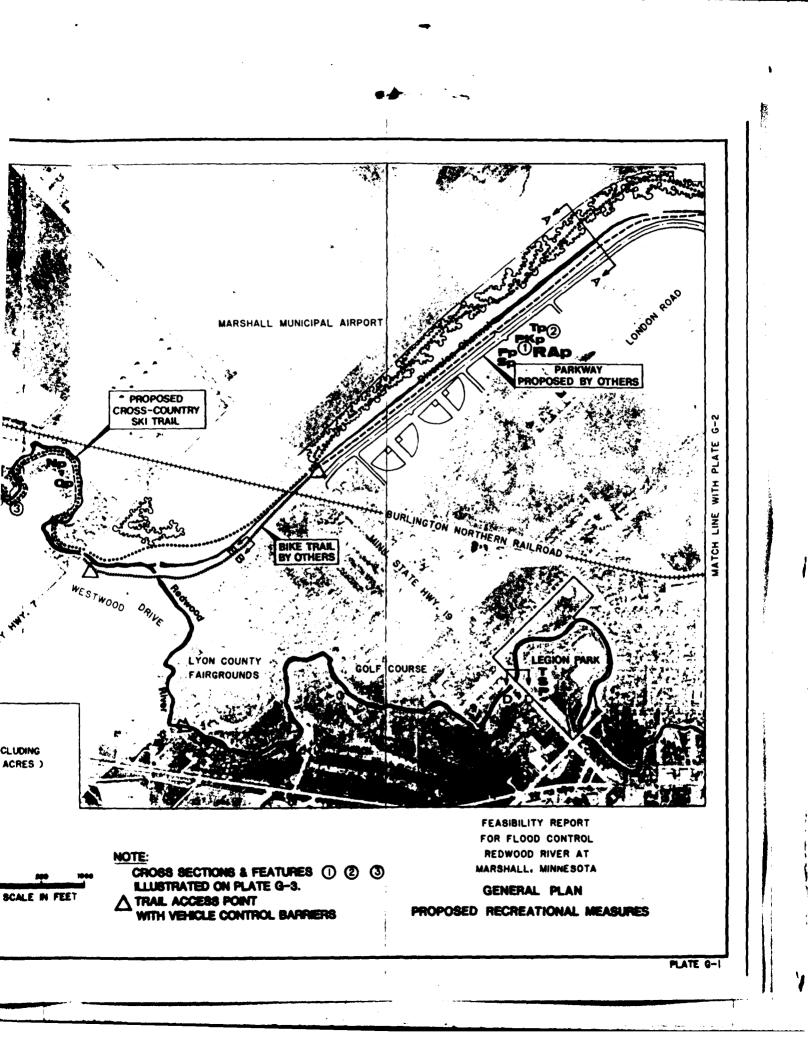
Table G-12 - Estimated Annual Costs

| <u>Federal</u><br>Total First Cost   | \$221,600         |
|--|-------------------|
| Interest and Amortization (\$221,600 x 0.07132)                              | 15,800            |
| Total Federal Annual Costs   | \$ 15,800         |
| <u>Non-Federal</u><br>Total First Cost                                       | <b>\$</b> 221,600 |
| Interest and Amortization (\$221,600 x 0.07132)<br>Operation and Maintenance | 15,800<br>2,690   |
| Total Non-Federal Annual Costs   | <b>\$</b> 18,490  |
| TOTAL ANNUAL COSTS   | \$ 34,290         |
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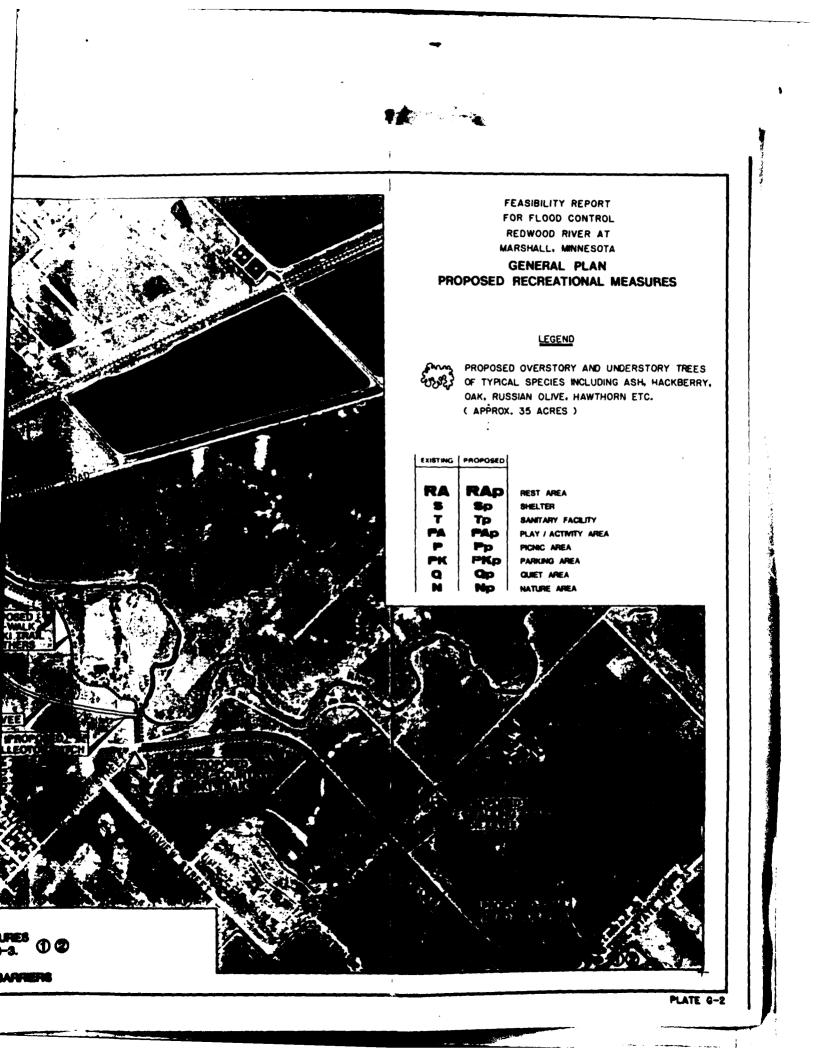
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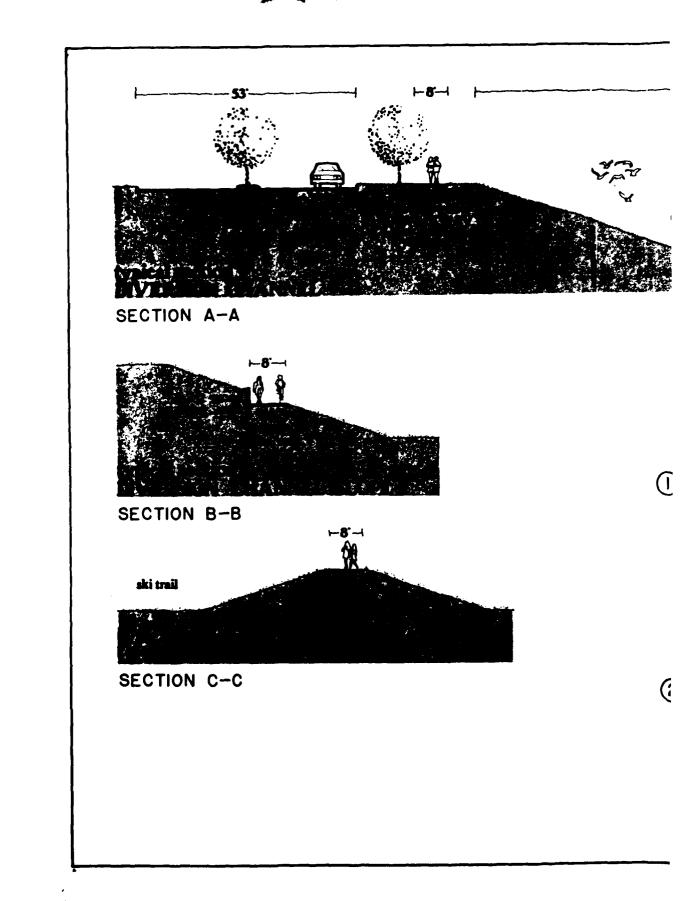
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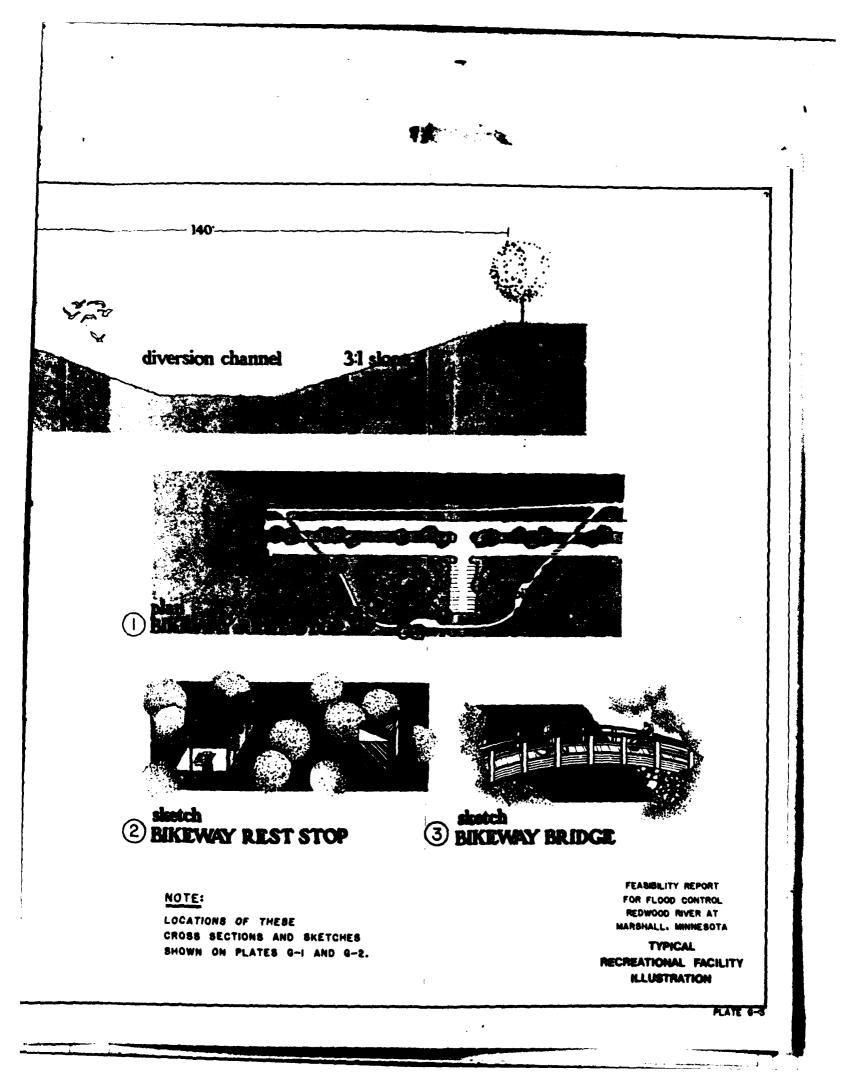




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# SECTION H

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## DETAILED DESIGNS

## DESIGN CONSIDERATIONS

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# SECTION H

# DESIGN CONSIDERATIONS

# GENERAL

1. This section presents a detailed discussion of the data used in designing the selected plan. Included are discussions of hydrologic and hydraulic studies, geologic and soils studies, and structural designs made in support of the overall study.

# HYDROLOGIC AND HYDRAULIC DESIGN

## MAJOR FLOODS OF RECORD

2. Table H-1 lists the pertinent data for all the floods that exceeded 1,500 cfs since the establishment of the Fourth Street U.S.G.S. age at Marshall in 1940. Included in the table are the dates of occurrence, instantaneous peak discharge, and maximum observed flood stage. To compare the peak stages to the existing conditions, all stages have been adjusted to the U.S.G.S. rating curve No. 22, effective November, 1971, and shown on table H-1. Channel cutoffs, clearing and snagging and scour below Marshall have greatly reduced river stages at the U.S.G.S gaging station at Marshall.

3. Flood of April 1969 - The flood of April 1969, the greatest known flood at Marshall, was caused by the melting of a heavy snow cover (water equivalent approximately 8 inches) and approximately one inch of rain. The maximum discharge at the Burlington Northern Railroad (river mile 72.6) has been estimated at 8,090 cfs. This discharge has a frequency of occurrence of once in approximately 100 years. With an emergency levee raise on CSAH 7 preventing flow over this road into Marshall, approximately 2,500 cfs of this flow is estimated to have crossed over Trunk Highway (T.H.) 23 into the Cottonwood River basin. Of the remaining 5,590 cfs (8,090 - 2,500), 4,090 cfs passed through the existing diversion channel and 1,500 cfs in the Redwood River through the city of Marshall.

4. River stages during the 1969 flood were considerably affected by backwater from ice jams downstream of Marshall, as evident from the observed stages at the U.S.G.S. gaging station at North 4th Street (plate H-1). The hydrograph adopted by the U.S. Army Corps of Engineers for the April 1969 flood reflects the flow into the Cottonwood River basin, the overbank storage upstream of CSAH 7, and is shown on plate H-2.

5. Flood of June 1957 - The flood of June 1957 was caused by heavy rainfall and related fast runoff. The largest 24-hour rainfall depth of 8.67 inches, resulting from this storm, was recorded at the National Weather Service Station at Minnesota, 12 miles northwest of Marshall and outside of the Redwood basin on June 17, 1957. The corresponding 24-hour rainfall depth at Marshall was 8.03 inches. Special surveys conducted by the National Weather Service, shortly after this storm, showed that amounts exceeding 10 inches fell in an area west of Marshall.

6. The maximum stream flow at the U.S.G.S. gaging station was determined to be 5,370 cfs. This includes the flow through the business

district which bypassed the gage. However, this does not include the natural diversion of approximately 800 cfs into the Cottonwood River basin at the wayside park. The discharge, upstream of the natural diversion of the roadside park is estimated at 6,170 cfs. This has the frequency of occurrence of once in 51 years. After having reached the peak, the flow dropped down to a discharge of 2,900 cfs approximately 20 hours later. After approximately 12 more hours, or 36 hours after the first flood stage peak, a second peak at 4,200 cfs occurred. It is possible that the second peak could have been caused by a second storm occurring shortly after the first one<sup>1/</sup> and/or by the discharge from Coon Creek which drains into the Redwood River at Russell, southwest of Marshall.

> Table H-1 - Flood Data, Redwood River at Marshall, Minnesota under Existing Conditions <u>2/</u>

| Date                 | Maximum<br><u>Discharge</u><br>(cfs) | Maximum<br>Recorded<br>Gage<br><u>Height</u><br>(ft) | Estimated Maximum<br>Stage on Rating <u>3/</u><br>Curve No. 22<br>(ft) |
|----------------------|--------------------------------------|--|--|
| April <b>9,</b> 1969 | 5590                                 | 7.62 <u>4/</u>                                       | 10.17  |
| June 17, 1957        | 5370 <sup>1/</sup>                   | 10.14  | 10.12  |
| April 6, 1951        | 2740                                 | 11.05  | 9.22   |
| April 9, 1965        | 2220                                 | 5.76   | 8.34   |
| April 8, 1952        | 1800                                 | 10.22  | 7.32   |
| June 10, 1947        | 1800                                 | 9.64   | 7.32   |
| May 5, 1944          | 1530                                 | 8.97   | 6.56   |

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 $\frac{1}{\ln 1957}$ , there were no recording gages in the Redwood River basin to measure the distribution of the rainfall.

 $\frac{2}{1965}$  and 1969 Floods affected by existing project that was completed in 1963.

<sup>3</sup>/All gage heights are based on the assumption that entire discharge would pass through town and do not take into account flow that crossed over to the Cottonwood Basin.

<sup>4</sup>/The gage height is for a discharge of 1,500 cfs flowing through the Redwood River Channel.

Appendix I

H-3

## FLOOD FREQUENCY RELATION SHIPS

7. The discharge-frequency relationships developed for this study are for existing conditions and for the total discharge above the natural diversion into the Cottonwood River Basin. These frequency curves are related to a location 1.2 miles upstream of the Burlington Northern railroad bridge.

8. The adopted discharge-frequency curve for the Redwood River at Marshall, Minnesota, is based on 34 years of US Geological Survey records (1940-1973) at Marshall. This data is summarized on Table H-2. This period includes two floods that overflowed into the Cottonwood Basin. These floods (17 June 1957 and 9 April 1969) were estimated by the Corps of Engineers as having peak overflows of 800 cfs and 2,500 cfs, respectively. Thus the peak was raised to 6170 cfs from 5370 and the 1969 peak was raised to 8090 from 5590 cfs, from the published values respectively. Both were adjusted to a longer record period due to the large storm rainfall in 1957 and the high snow water-equivalent in 1969. The adopted discharge frequency curve is based on statistical computations using annual peaks and expected probability adjustment  $(P_N)$ . The statistical computed line was used below 5 percent; above 5 percent the line is drawn through the 100-year value of 8200 cfs and guided graphically by the two highest flood peaks, which were considered to be the highest values in a 66-year period. The plotting positions for the lowest 32 values were plotted in a 34-year period. The statistical computations were made with two low flows adjusted, 1959 peak from 24 to 100 cfs and 1956 peak from 47 to 130 cfs. The 100-year intermediate regional or regulatory flood (8200 cfs) was agreed to by the U.S. Geological Survey, the Soil Conservation Service, and the Corps of Engineers. This discharge-frequency curve was used for the Marshall flood plain information report, December 1974 and for the Marshall

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flood insurance study, August 1976 and is now adopted for the Section 216 Feasibility Study for Flood Control, Redwood River at Marshall, Minnesota. This frequency curve is shown on Plate H-3. This adopted discharge frequency curve which was computed using the latest guidelines and procedures outlined in the WRC Bulletin No. 17 and is also shown on Plate H-4.

9. The peak discharge data for the partial-duration series are summarized on Table H-2, and the partial-duration series curve is shown as a dashed line on the adopted curve on Plate H-4.

Plotting Points For Discharge-Frequency, Floods Of Record, Redwood River At Marshall, Minnesota (Annual Peaks and Partial - Duration Series: Table H-2

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| ANNUAL PEAKS         PARTIAL-DURATIO           PEAK         DISCIANTE         PARI           PEAK         DISCIANTE         PARI           PEAK         DISCIANTE         PARI           ISCIANTE         PROBABILITY         DATE         YEAR           1969         6090 <sup>⊥</sup> 1.0         9 April         1969           1957         6170 <sup>⊥</sup> 2.5         17 June         1957           1955         2740         7.8         April         1969           1955         10.7         9 April         1952           1960         13.6         8 April         1952           1944         16.6         10.7         9 April         1955           1947         1800         16.6         10.1         960           1944         16.40         19.5         20 May         1944           1946         19.5         20 May         1945           1947         1800         31.1         20 Cotober         1945           1948         1250         21.4         1         April         1945           1949         1090         31.1         20 Cotober         1946           1941  |          |      |                     | (621120                  |            |         |                     |
|--|----------|------|---------------------|--------------------------|------------|---------|---------------------|
| PEAK         DATE         YEAK           ISCHARGE         PROBALLITY         DATE         YEAR           ISCHARGE         PROBALLITY         DATE         YEAR           ISCHARGE         PROBALLITY         DATE         YEAR           ISCHARGE         BADOL         1.0         9 April         1957           I 1951         2740         7.8         6 April         1957           I 1952         2730         10.7         9 April         1957           I 1952         1800         13.6         8 April         1952           I 1952         1800         15.6         10 June         1947           I 1952         1800         16.6         10 June         1947           I 1952         1800         16.6         10 June         1942           I 1960         19.6         31.1         1960         1942           I 1960         1960         31.1         1960         1942      <   |          | A    | UNUAL PEAKS         |                          | PARTIA     | L-DURAT | ION SERIES          |
| DISCIMAGEPROBABILITYDATEYEAR19698000 <sup>1</sup> /11.09April19691957 $6170^{1}$ 2.51.09April19511957 $6170^{1}$ 2.510.79April19521958 $2740$ 7.86April19521951 $2740$ 7.86April19521952180013.69April19521953180016.610.79April19521954180016.610.700April19521954180016.610.720March19471962127022.41April196219421963127022.41April196219461963127023.41April196219461963108031.120March194619401943891.6.936.47April19461954199033.8.42.720March1943195365843.643.72087.41940195365851.415106371943195365851.4151071943195365851.41510619431954195354.457.3511947195657.3 <th></th> <th></th> <th>PEAK</th> <th></th> <th></th> <th></th> <th>PEAK</th>  |          |      | PEAK                |                          |            |         | PEAK                |
| 1969 $8090\frac{J}{10}$ 1.09 April19691957 $6170\frac{J}{10}$ 2.517 June19571951 $2740$ 7.86 April19511952180013.69 April19651952180013.69 April19521952180016.610.79 April19521952180016.6109 April19551947180016.6109 April19521947180016.6101019441960141022.41April19501960141022.411April19601960141022.4114pril19601960141022.4114pril19601960141022.4114pril19601960137025.331.11196019441962127025.331.1119601963104054.07April19461973891.66.939.8330me19431973830.42.720March19431973830.42.720March19431973197319731244.419431973830.42.72631.419431973197319741244.4194319731973 <th>DATE</th> <th>YEAR</th> <th>DISCHARGE<br/>(CFS)</th> <th>PROBABILITY<br/>(PERCENT)</th> <th>DATE</th> <th>YEAR</th> <th>DI SCHARGE<br/>(CFS)</th>   | DATE     | YEAR | DISCHARGE<br>(CFS)  | PROBABILITY<br>(PERCENT) | DATE       | YEAR    | DI SCHARGE<br>(CFS) |
| 1957       6170 <sup>JJ</sup> 2.5       17 June       1951         1951       2740       7.8       6 April       1951         1965       2220       10.7       9 April       1965         1965       2220       10.7       9 April       1965         1965       2220       10.7       9 April       1965         1947       1800       16.6       8 April       1965         1944       16.40       19.5       8 April       1965         1944       16.6       19.5       8 April       1965         1944       16.40       19.5       20 May       1947         1960       1410       22.4       1 April       1960         1962       1270       25.3       31 March       1962         1963       1270       28.2       20 March       1963         1949       1040       54.0       7 April       1949         1943       891       .6.9       3 June       1943         1943       1949       3 June       1943       1949         1953       668       48.6       3 June       1943         1953       658       51.4       12 M   | 9 April  | 1969 | 8090 <u>1</u> /     | 1.0                      | 9 April    | 1969    | 8090 <u>1</u> /     |
| 195127407.86April19511965222010.79April19651965180013.68April19521947180016.610.1me19471947180016.610.1me19471944164019.520 <may< td="">19441960141022.41April1960141022.414pril1962127025.331<march< td="">19621963127025.331<march< td="">19461964131021.414pril1965127028.220<march< td="">1948196331.12031<march< td="">19461949104054.03131<march< td="">19461943891.6.93030<march< td="">19461943891.6.930<march< td="">1946194619403131<march< td="">1946195489039.8303131195383042.722<march< td="">1943195365848.6313131195365851.4151945195365851.4151945195354.451.4151945195057.354.4151945195057.354.4151945195057.354.4151945195057.3<td< td=""><td>17 June</td><td>1957</td><td>6170<sup>1</sup>/</td><td>2.5</td><td>17 June</td><td>1957</td><td>6170<u>1</u>/</td></td<></march<></march<></march<></march<></march<></march<></march<></march<></march<></may<>   | 17 June  | 1957 | 6170 <sup>1</sup> / | 2.5                      | 17 June    | 1957    | 6170 <u>1</u> /     |
| 1965         2220         10.7         9         April         1965           1952         1800         13.6         8         April         1952           1947         1800         15.6         8         April         1952           1944         1640         19.5         10         June         1947           1944         1640         19.5         20         May         1944           1960         1410         22.4         1         April         1962           1962         1270         25.3         31         March         1962           1963         1250         28.2         21         March         1963           1964         1090         31.1         20         October         1968           1943         891         -0.69         31.1         20         646           1943         891         -0.69         31.0         1946         1946           1943         891         -0.69         31.0         1949         1946           1943         891         -0.69         31.0         1946         1946           1943         891         45.6         32  | 6 April  | 1951 | 2740                | 7.8                      | 6 April    | 1951    | 2740                |
| 1952         1800         13.6         8         April         1952           1947         1800         16.6         10         June         1947           1947         1800         16.6         10         June         1947           1944         1640         19.5         20         May         1944           1946         1410         22.4         1         April         1960           1962         1270         25.3         31         1         1960           1963         1270         25.3         31         1         1960           1964         1270         25.3         31         1         1960           1963         31.1         20         0ctober         1963           1940         1040         54.0         7         April         1949           1943         890         39.8         54.0         30         1949           1945         830         -6.9         30         31         1949           1954         19         30         31         1949         1943           1953         677         45.6         12         1943           <  | 9 April  | 1965 | 2220                | 10.7                     | 9 April    | 1965    | 2220                |
| 1947       1800       16.6       10 June       1947         1944       1640       19.5       20 May       1947         1946       1410       22.4       1       April       1960         1966       1410       22.4       1       April       1960         1962       1270       25.3       31 March       1962         1948       1250       28.2       21 March       1962         1949       1080       31.1       20 October       1948         1940       1040       54.0       7 April       1949         1943       891       Ju6       30 March       1949         1943       891       Ju6       30 March       1946         1954       890       39.8       30 March       1946         1954       194       7 April       1949       1943         1954       194       30 March       1943       1943         1955       830       42.7       22 March       1943         1953       654       12 March       1943       1943         1955       1956       48.6       26 March       1973         1955       54.4  | 8 April  | 1952 | 1800                | 13.6                     | 8 April    | 1952    | 1800                |
| 1944         1640         19.5         20 May         1944           1960         1410         22.4         1 April         1960           1962         1270         25.3         31 March         1962           1963         1270         25.3         31 March         1962           1948         1250         28.2         31 March         1962           1948         1250         28.2         31.1         1940           1948         1250         28.2         20 March         1948           1949         1080         31.1         20 October         1948           1940         1040         54.0         7 April         1949           1943         891         J66         30.8         1949           1944         1040         54.0         7 April         1949           1945         890         39.8         3 June         1943           1973         830         42.7         22 March         1943           1973         830         3 June         1943           1973         830         42.4         12 March         1943           1973         668         48.6         26 Ma   | l0 June  | 1947 | 1800                | 16.6                     | 10 June    | 1947    | 1800                |
| 1960141022.41April19601962127025.331March19621948125028.228.222March19481949108031.120October19481949108031.120October19481949108054.07April19491943891.6.954.07April19491943891.6.950.830303030195489039.842.722March1940197383042.722March1940197383042.722March1943197366848.612March1943197365851.412March194319505354.42419431943195057.354.42419431943195057857.331July1963  | 20 May   | 1944 | 1640                | 19.5                     | 20 May     | 1944    | 1640                |
| 1962         1270         25.3         31         March         1962           1948         1250         28.2         2         March         1962           1948         1250         28.2         2         March         1962           1948         1250         28.2         2         2         March         1962           1949         1080         31.1         2         0ctober         1948           1940         1040         54.0         7         April         1949           1943         891         .6.9         30.8         1949         1949           1954         890         39.8         30.7         42.7         2         March         1940           1953         677         45.6         12         3         June         1943           1953         628         51.4         12         March         1973           1954         1955         12         March         1943         1943           1953         658         48.6         12         1943         1943           1954         1955         12         March         1943         1943           1   | 1 April  | 1960 | 1410                | 22.4                     | 1 April    | 1960    | 1410                |
| 1948         1250         28.2         22         March         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1948         1949         1949         1949         1949         1949         1949         1949         1949         1949         1949         1940         1940         1940         1940         1940         1940         1943 | 51 March | 1962 | 1270                | 25.3                     | 31 March   | 1962    | 1270                |
| 1949         1080         31.1         20         October         1968           1940         1040         54.0         7         April         1949           1943         891         .6.9         7         April         1949           1943         891         .6.9         30.8         7         1940           1954         890         39.8         30         42.7         1940         1943           1973         830         42.7         22         March         1943           1963         677         45.6         12         March         1973           1972         668         48.6         12         March         1973           1973         628         51.4         12         March         1973           1973         628         51.4         15         1945         1943           1946         623         54.4         24         1943         1962           1950         57.3         51.01Y         1963         31.01Y         1963  | 22 March | 1948 | 1250                | 28.2                     | 22 March   | 1948    | 1250                |
| 1940104054.07April19491943891J6.9J6.9J0.6J491943890J6.9J0.6J0.61943195483042.7J0.61943197383042.722March1954196367745.612March1973197266848.626March1943195362851.415June1943195057.357.351.0J1.01963  | 7 April  | 1949 | 1080                | 31.1                     | 20 October |         | $1100^{2/}$         |
| 1943       891       J6.9       30 March       1940       1         1954       890       39.8       3 June       1943         1954       890       39.8       3 June       1943         1973       830       42.7       22 March       1954         1963       677       45.6       12 March       1954         1972       668       48.6       12 March       1973         1973       658       48.6       26 March       1943         1953       628       51.4       15 June       1943         1956       53.4       54.4       24 May       1962         1950       57.3       51 July       1963       31 July       1963  | 0 March  | 1940 | 1040                | 54.O                     | 7 April    | 1949    | 1080                |
| 195489039.83 June1943197383042.722 March1954196367745.612 March1973197266848.626 March1943195362851.415 June1943194662354.424 May1962195057.357.331 July1963   | 3 June   | 1943 | 891                 | J6.9                     | 30 March   | 1940    | 1040                |
| 1973       830       42.7       22 March       1954         1963       677       45.6       12 March       1973         1972       668       48.6       26 March       1973         1972       668       48.6       26 March       1943         1953       628       51.4       15 June       1943         1946       623       54.4       24 May       1962         1950       57.3       31 July       1963  | 22 March | 1954 | 890                 | 39.8                     | 3 June     | 1943    | 891                 |
| 1963         677         45.6         12         March         1973           1972         668         48.6         26         March         1943           1953         628         51.4         15         June         1943           1946         623         54.4         24         May         1962           1950         57.3         57.3         31         July         1963   | 12 March | 1973 | 830                 | 42.7                     | 22 March   | 1954    | 890                 |
| 1972         668         48.6         26 March         1943           1953         628         51.4         15 June         1943           1946         623         54.4         24 May         1962           1950         578         57.3         31 July         1963  | il July  | 1963 | 677                 | 45.6                     | 12 March   | 1973    | 830                 |
| 1953         628         51.4         15 June         1943           1946         623         54.4         24 May         1962           1950         578         57.3         31 July         1963  | 4 May    | 1972 | 668                 | 48.6                     | 26 March   | 1943    | $700^{2/}$          |
| 1946         623         54.4         24 May         1962           1950         578         57.3         31 July         1963   | 21 March | 1953 | 628                 | 51.4                     | 15 June    | 1943    | 700 <sup>2/</sup>   |
| <b>1950</b> 578 57.3 31 July 1963  | 16 March | 1946 | 623                 | 54.4                     | 24 May     | 1962    | 700-                |
|  | 3 April  | 1950 | 578                 | 57.3                     | 31 July    | 1963    | 677                 |

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Table H-2 (Continued)

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|          | -    | ANNUAL PEAKS      |             | PARTIA   | L-DURATI | PARTIAL-DURATION SERIES |
|----------|------|-------------------|-------------|----------|----------|-------------------------|
|          |      | PEAK<br>DISCHARGE | PROBABILITY |          |          | PEAK<br>DISCHARGE       |
| DATE     | YEAR | (CFS)             | (PERCENT)   | DATE     | YEAR     | (CFS)                   |
| 7 July   | 1971 | 523               | 60.2        | 4 May    | 1972     | 668                     |
| S April  | 1970 | 485               | 63.1        | 21 March | 1953     | 628                     |
| 13 March | 1966 | 445               | 66.0        | 16 March | 1946     | 623                     |
| 1 July   | 1942 | 437               | 68.9        | 7 July   | 1962     | 620 <u>2/</u>           |
| 9 April  | 1958 | 388               | 71.8        | 27 March | 1944     | 600 <u>2/</u>           |
| 27 March | 1941 | 382               | 74.7        | 19 April | 1962     | 600 <u>2/</u>           |
| 16 June  | 1967 | 373               | 77.6        | 3 April  | 1950     | 578                     |
| 15 March | 1945 | 320               | 80.5        | 7 July   | 1971     | 523                     |
| 19 May   | 1961 | 190               | 83.4        | 24 April | 1947     | 500 <u>2/</u>           |
| 21 Sept. | 1968 | 162               | 86.4        | 23 June  | 1952     | 500 <u>2/</u>           |
| 14 March | 1955 | 162               | 89.3        | 1 June   | 1972     | 500 <sup>2/</sup>       |
| 2 July   | 1964 | 138               | 92.2        | 5 April  | 1970     | 485                     |
| 26 June  | 1956 | 130 <u>3/</u>     | 95.1        | 13 March | 1966     | 445                     |
| 23 March | 1959 | 1004/             | 98.0        | 1 July   | 1942     | 437                     |
|          |      |                   |             |          |          |                         |

 $\frac{1}{r}$  peak discharge includes overflow into Cottonwood River Basin

 $\frac{2}{1000}$ Instantaneous peaks estimated from mean daily peaks.

 $\frac{3}{2}$  Peak flow for 1956 adjusted from 47 cfs to 130 cfs.

4/Peak flow for 1959 adjusted from 24 cfs to 100 cfs.

DEVELOPMENT OF FREQUENCY CURVE USING WRC BULLETIN NO. 17

10. The discharge-frequency curve for the Redwood River at Marshall, Minnesota, was computed in accordance with WRC Bulletin No. 17 subsequent to completion of the Draft Feasibility Report. The frequency curve is based on annual series with the distribution based on a log Pearson type III distribution. The expected probability adjustment  $P_n$  is used in accordance with draft ER 1110-2-1450 dated 30 August 1976. The Weibull plotting position formula was used for plotting the discharge-frequency data. This discharge-frequency curve is for existing conditions for the Redwood River at Marshall and for the total discharge above the natural diversion into the Cottonwood River basin. The curve applies to the upstream limit of existing improvements at river mile 73.8 as shown on Plate C-1.

11. During the period of record at Marshall, from 1940 through 1976, peak flows from the Redwood River naturally diverted into the Cottonwood River basin on two occasions. Studies made by this office indicated that the overflow for the 17 June 1957 flood peak was 800 cfs and that the total discharge upstream from this overflow area was 5,370 + 800 = 6,170 cfs. The Corps of Engineers estimate of the overflow for the 9 April 1969 flood was 2,500 cfs or a total discharge of 5,590 + 2,500 = 8,090 cfs upstream of the natural diversion. It has been determined that the April 1969 flood at Marshall was the largest flood, at least since 1882, and one high outlier was used when computing the discharge frequency curve in accordance with Bulletin No. 17. Two peak flows, 1956 (47 cfs) and 1959 (29 cfs), were adjusted to 60 cfs and 80 cfs, respectively.

12. A generalized skew value of 0.0 was used in accordance with the St. Paul District skew map (17 February 1977). Using Bulletin No. 17 and the previously described conditions, the adopted skew was zero and the computed skew was zero.

13. Table H-3 shows the annual maximum peak discharge-year data inputs and statistical output from the computer program. The frequency curve is shown on Plate H-4 along with the adopted 216 feasibility study curve dated 25 June 1974 for comparison. The 5 percent and 95 percent confidence limit lines are also plotted and indicate that both of the curves are well within these limits. The curve using Bulletin No. 17 is slightly lower than the adopted curve. The adopted curve passed through the 1-percent chance flood discharge of 8,200 cfs which is also the regulatory flood for Minnesota State flood plain management purposes.

14. 100-Year Flood - In 1963, when the diversion channel was constructed, the design discharge of 6,500 cfs had an expected frequency of occurrence of once in 114 years. However, after the 1969 flood, and the occurrence of the major floods over a short time period (1957 and 1969), the discharge frequency curve has been revised. The new curve, derived by the U.S. Army Corps of Engineers, in cooperation with U.S.G.S. and S.C.S. is based on statistical computations and 34 years of records (1940-1973) at Marshall. This curve shows that a discharge of 8,200 cfs has a frequency of occurrence of once in 100 years as shown on plate H-3.

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15. As a supplement to the discharge-frequency curve at the upstream study limit, discharge-frequency curves were developed by approximate methods for three additional locations within the study reaches. These additional curves are shown on Plates H-5 through H-7 and their locations are shown on Plate H-10. Rating curves which were developed utilizing the HEC-2 computer model for the same locations are also shown on these plates.

A H-10

| ppendix | I |  |
|---------|---|--|
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#### STANDARD PROJECT FLOOD (SPF) HYDROGRAPH

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16. The standard project flood (SPF) hydrograph, computed by U.S. Army Corps of Engineers, was derived using the unit hydrograph adopted for the 1969 flood. The SPF which was computed for a total runoff of 7.50 inches, results in a peak discharge of 16,700 cfs as shown on Plate H-9. The SPF index rainfall was 10.0 from Plate 2 of EM 1110-2-1411. The loss rate used was 0.9 inches per 6-hours. A higher than normal base flow (500 cfs) was used to account for the 40 square miles eliminated above Lake Benton. Table H-4 shows the standard project storm and rainfall and rainfall excess.

17. The unit hydrograph adopted for this study is based on an estimated observed hydrograph of the April 1969 flood upstream of the natural overflow into the Cottonwood River basin. This hydrograph was based on all available published data plus estimates of the magnitude and time of overflow. The rise portion of this observed hydrograph was shortened because of slow snowmelt for the first few days. The recession of this observed hydrograph was estimated (shortened) excluding 40.5 square miles of drainage area above the mouth of Benton Lake. Benton Lake has a surface area of approximately 2,900 acres.

18. For the computation of the unit hydrograph, the drainage area above Lake Benton (approximately 40 square miles) was eliminated. The unit hydrograph derived in the recently completed flood plain information study in accordance with accepted criteria was computed for a net area of 210 square miles and was from a runoff of 4.53 inches. The peak discharge from this unit hydrograph was computed to be 1,750 cfs and was peaked 25 percent to 2,200 cfs. This adopted 6-hour unit hydrograph is for discharge above the natural breakout into the Cottonwood River basin and is shown on Plate H-8.

19. The unit hydrograph for the April 1969 flood was not optimized since the recorded flow at the gage is only a small part of the total flow. The greater part of the total flow passes through the diversion channel. Cross-flow into the Cottonwood River basin upstream of Marshall further complicates any attempt at optimization.

| Hour  | Rainfall<br>(inches) | Loss<br>(inches) | Rainfall<br>Excess<br>(inches) |
|-------|----------------------|------------------|--------------------------------|
| 6     | 0.01                 | 0.01             | 0                              |
| 12    | 0.04                 | 0.04             | 0                              |
| 18    | 0.26                 | 0.26             | 0                              |
| 24    | 0.02                 | 0.02             | 0                              |
| 30    | 0.05                 | 0.05             | 0                              |
| 36    | 0.17                 | 0.17             | 0                              |
| 42    | 1.23                 | 0.90             | 0.33                           |
| 48    | 0.10                 | 0.10             | 0                              |
| 54    | 0.32                 | 0.32             | 0                              |
| 60    | 1.09                 | 0.90             | 0.19                           |
| 66    | 7.88                 | 0.90             | 6.98                           |
| 72    | 0.66                 | 0.66             | 0                              |
| 78    | 0.02                 | 0.02             | 0                              |
| 84    | 0.06                 | 0.06             | 0                              |
| 90    | 0.44                 | 0.44             | 0                              |
| 96    | 0.03                 | 0.03             | 0                              |
| Total | 12.38                | 4.88             | 7.50                           |

# Table H-4 - Standard Project Rainfall and Rainfall Excess

Note: Rainfall depth in inches ending at hour.

Appendix I H-12

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## **STREAM FLOW**

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18. Stream flows at Marshall, ordinarily range from periods of no flow during winter to well under 100 cfs during summer. Spring floods have mostly occurred between late March and early April, occasional summer floods are not uncommon. Ice jams during spring floods have caused considerable back water effect, resulting in higher stages as evident during the 1969 flood which resulted in stage two feet higher at mile 66.1. Heavy summer rains, with considerable runoff, frequently result in a double peak approximately a day apart at Marshall.

19. The U.S. Geological Survey (USGS) has maintained a stream gage on the Redwood River at Marshall since March 1940, on the downstream side of North 4th Street Bridge (river mile 67.2). The largest flood of record occurred on April 9, 1969. The discharge for this flood has been estimated at 8,090 cfs<sup>1</sup>. The second largest flood occurred on June 17, 1957, with a peak discharge estimated at 6,170 cfs<sup>2</sup>. The average discharge for the 32-year period through 1972 was 48.1 cfs. Average annual runoff total about 2.61 inches over the 250.7<sup>3</sup>/ square miles (sq.mi.) of drainage area above Marshall.

#### Historical Flood Flow Distributions

20. The floods of 1957 and 1969 proved that high Redwood River stages will overtop the minimum roadway elevation of Highway 23 at the wayside park, and therefore, during times of high river stages, some

Discharges at the Burlington Northern Railroad Bridge, upstream from natural diversion into Cottonwood River basin.

<sup>&</sup>lt;sup>2</sup>/Discharges at the Burlington Northern Railroad Bridge, upstream from natural diversion into Cottonwood River basin.

<sup>&</sup>lt;sup>3</sup>/After a recent study by Soil Conservation Service (SCS), the drainage area has been revised from 307 square miles.

flow will be discharged into the Cottonwood River basin. During the 1957 flood, it was estimated by Corps employees observing the phenomenon, that approximately 800 cfs passed into the Cottonwood Basin (see figure H-1). During the 1969 flood, it was estimated that about 2,500 cfs flowed into the Cottonwood Basin. However, it was also estimated that about 1,100 cfs of this was forced by the emergency dike on CSAH 7, and the breaching of Highway 23, and therefore, only 1,400 cfs of the total overflow to the Cottonwood basin was considered to be natural as illustrated on the flow distribution diagrams for the 1969 flood in Figure H-1. It was also estimated that overflows commenced at a Redwood River discharge of 4000 cfs. Since the 1969 flood, the Minnesota State Department of Transportation has upgraded Highway 23 to a four lane structure. The roadway was raised about 0.5 feet as a part of the improvement. The maximum flow that will now pass through the wayside park with no overflow to the Cottonwood is 6,500 cfs. Also indicated on Figure H-1 are flow values at other locations along the Redwood River at Marshall.

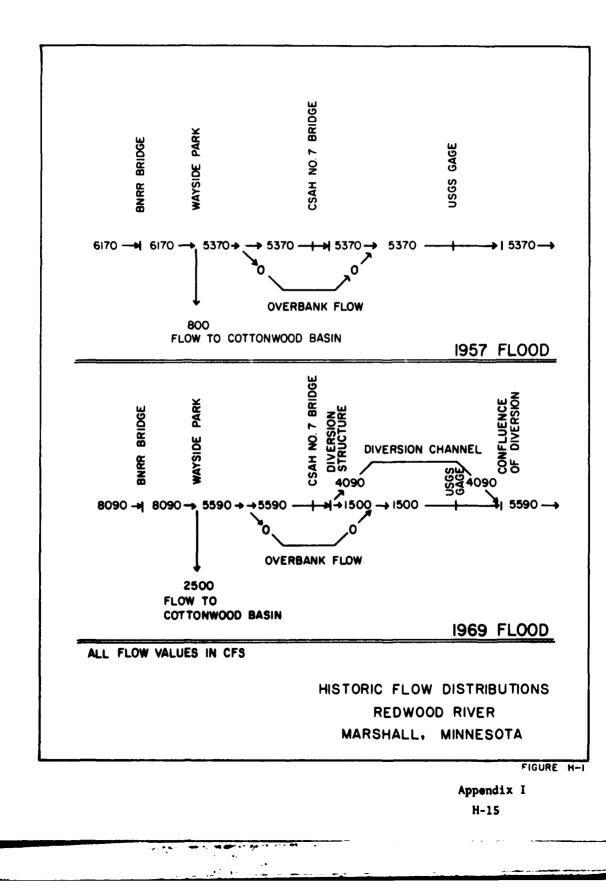
Future Flood Flow Distributions - 100 Year Flood

21. It has been determined in a recently completed (1974) flood plain information study at Marshall, that under existing conditions and a 100-year discharge of 8,200 cfs, an estimated 1,500 cfs would cross over T.H. 23, in the vicinity of the wayside park, and flow into the Cottonwood River basin. It was also determined that 1,090 cfs would cross over the right overbank of C.S.A.H. 7, bypassing the diversion structure and re-entering the Redwood River approximately 2,500 feet downstream of the diversion structure. Of the remaining 5,610 cfs (8,200 - (1,500 + 1,090)), reaching the diversion structure, 4,110 cfs would pass through the diversion channel and 1,500 cfs would enter the natural Redwood River channel as shown in Table H-5 and Figure H-3. Thus, the total discharge in the Redwood River,

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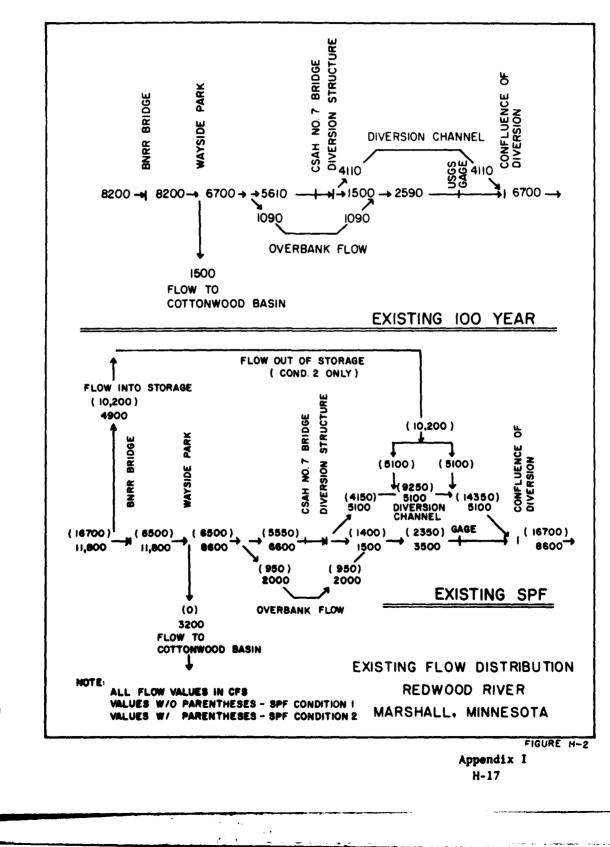
through the city of Marshall would be 2,590 cfs (1,500 + 1,090). The total discharge at the downstream confluence of the diversion channel and the Redwood River would be 6,700 cfs (4,110 + 2,590). See Figure H-2 for a schematic view of this existing 100-year condition flood flow distribution. The 100-year and 133-year design flood flow distributions with the proposed project are shown on Figure H-3.

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Standard Project Flood

22. The SPF was also analyzed in the previously mentioned flood plain information study and, in this analysis of the SPF, two conditions were considered. The first condition would occur about onehalf day before the SPF peak arrives and would result in maximum damages to the upstream reach at Marshall; the second condition, occurring at the time of the peak, would result in maximum damages to the downstream reach at Marshall. Existing flow distributions for both of these conditions are shown on Figure H-2.

23. A part of the existing flood control project is a levee, with a minimum top elevation of 1199, located on the left bank of the Redwood River upstream of the Burlington Northern Railroad bridge. Discharges in excess of 11,800 cfs, about the 250-year flood, would overtop this levee. For the SPF with a peak flow of 16,700 cfs, certain assumptions with respect to the mode of failure of this levee have been made. The hydrograph of the SPF, Plate H-9, indicates that a flow of 11,800 cfs would occur approximately one-half day before the peak. It is assumed that by the time the peak occurs the levee is completely washed away. Under this assumption, the maximum discharge that would flow under the Burlington Northern Railroad bridge is 11,800 cfs occurring one-half day before the peak (condition 1). At the peak only 6,500 cfs would flow under the bridge (condition 2).



# Table H-5 - Flood Flow Distribution At Marshall

# Existing Conditions

# Discharge Changes Throughout Study Reach

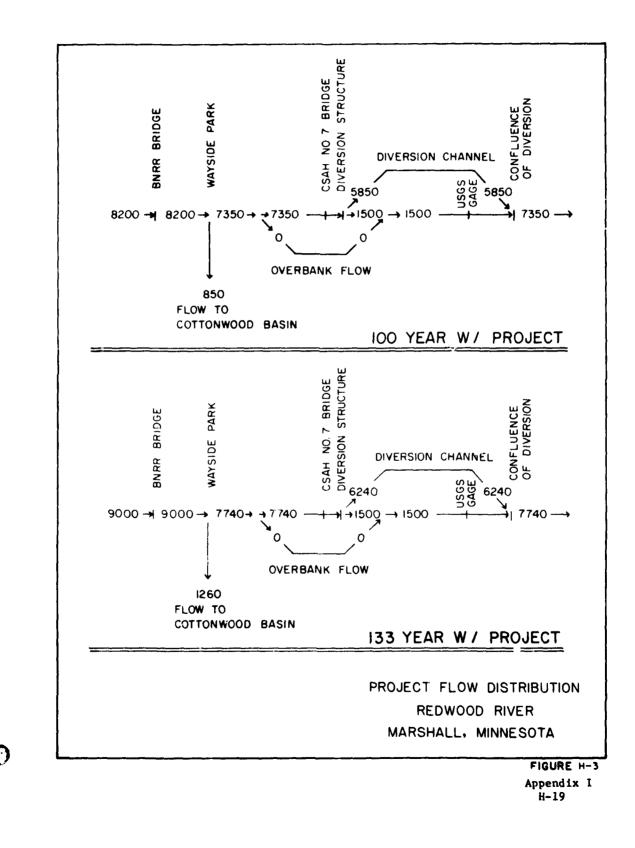
|              |                    | 100 YR                    |         | SPF               |
|--------------|--------------------|---------------------------|---------|-------------------|
|              |                    | (CES)                     | Cond. 1 | Cond.             |
|              |                    | (CFS)                     | (CFS)   | (CFS)             |
|              |                    |                           |         |                   |
| surlington : | Northern RR Bridge |                           |         |                   |
|              | Upstream           | 8200                      | 16700   | 16700             |
|              | Downstream         | 8200                      | 11800   | 6500              |
|              |                    |                           |         |                   |
| Wayside Parl | k                  |                           |         |                   |
|              | Downst ream        | 6700                      | 8600    | 6500              |
|              |                    |                           |         |                   |
| CSAH #7      |                    |                           |         |                   |
|              | Downstream         | 5610                      | 6600    | 5550              |
| Diversion S  | tructure           |                           |         |                   |
|              | Upstream           | 5610                      | 6600    | 5550              |
|              | Downstream         |                           |         |                   |
|              | Redwood River      | 1500 <u>1/</u>            | 1500    | 1400 <sup>2</sup> |
|              | Div. Channel       | <u>4110<sup>1</sup></u> / | 5100    | 41502             |
|              |                    |                           |         |                   |
| U.S.G.S. Ga  | -                  |                           |         |                   |
|              | Redwood River      | 2590                      | 3500    | 2350              |
| Confluence   |                    |                           |         |                   |
|              | Downstream         | 6700                      | 8600    | 16700             |

<sup>1</sup>/These discharges differ slightly from the original project report rating curve values of 1400 and 4210 cfs respectively as obtained from Plate H-11. However, the tabulated values have been used in the Marshall FPM and Flood Insurance Study reports.

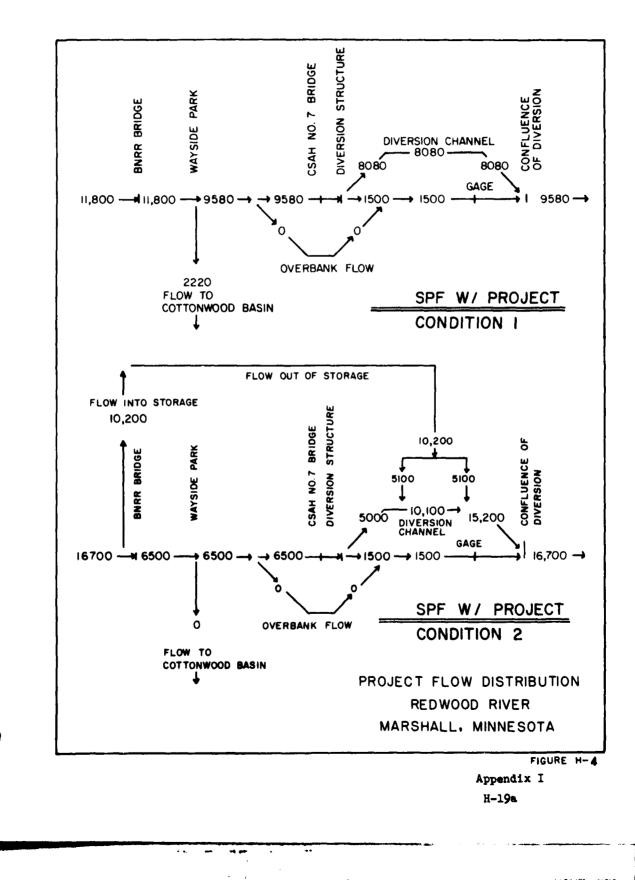
 $\frac{2}{These}$  figures from original project report rating curve.

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24. When the levee is overtopped by discharges greater than 11,800 cfs, the excess water flows north of the Burlington Northern Railroad tracks in a northeasterly direction and eventually enters the diversion channel upstream of Minnesota State Highway 68. It is assumed that, until the SPF reaches the peak, all the flows going north of the Burlington Northern Railroad tracks would go into storage on lands north of the tracks and west of the diversion channel. This would result in a volume of 6,300 acre-feet flooding approximately 2,800 acres at an average depth of 2.3 feet. At the peak of the SPF, 10,200 cfs would pass through the storage area. Two low spots on the diversion channel - at the drop structure and Chicago-Northwestern Railroad (CNR) bridge - are the most likely places where the flow would enter the diversion channel. It is assumed that one-half of the discharge, flowing north of the Burlington Northern Raoilroad tracks, would enter the diversion channel at the existing drop structure and the other half at the Chicago Northwestern Railroad bridge.

25. Under Condition 1, of the 11,800 cfs that would flow under the Burlington Northern Railroad bridge, an estimated 3,200 cfs would cross over T.H. 23 into the Cottonwood River basin, 2,000 cfs would cross over the right overbank and the CSAH 7 embankment, bypassing the diversion structure, and reentering the Redwood River approximately 2,500 feet downstream of the diversion structure. Of the 6,600 cfs (11,900 - (3,200 + 2,000) reaching the diversion structure, 5,100 cfs would enter the diversion channel. The total discharge at the downstream confluence of the diversion channel and the Redwood River would be 8,600 cfs (5,100 + 3,500). This discharge reflects the temporary loss of flow due to temporary storage northeast of the Burlington Northern Railroad tracks.

26. Under Condition 2, the discharge through the Burlington Northern Railroad bridge would be approximately 6,500 cfs with no flow entering the Cottonwood basin. The flow traveling northeast of the Burlinton Northern

tracks would be 10,200 cfs. By the time the flow reaches this magnitude, however, the available storage north of the BNRR tracks will have been used up so 10,200 cfs will be discharged almost immediately into the diversion channel via the two low areas. Based on this assumption, the discharge downstream of the confluence will be 16,700 cfs. Of the 6,500 cfs which continues down the Redwood River channel below the Highway 23 Roadside Park, 950 cfs would flow over CSAH 7, eventually reentering the river 2,500 feet downstream of the diversion structure, leaving 5,550 cfs to be split at the diversion structure. Of this 5,550 cfs, 1,400 cfs would flow through the diversion structure culverts into the main channel and 4,150 cfs would flow into the diversion channel. At the U.S.G.S. gage the flow would be 2,350 cfs (1,400 + 950).

27. The Condition 1 and Condition 2 SPF flow distributions with the proposed project are shown on Figure H-4. Overflow to the Cotton-wood River basin would be reduced to 2,220 cfs for Condition 1, and flow over CSAH 7 would be reduced to zero for both conditions.

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#### WATER SURFACE PROFILES

## General

28. Water surface profiles for both existing and proposed project conditions were derived by backwater computations using a computer model based on the Hydrologic Engineering Center's computer program HEC-2. The existing condition profiles were obtained using the model which was developed for the report titled "Flood Plain Information, Redwood River at Marshall, Minnesota". The various hydraulic parameters for this report were established using a manual optimization technique which involved establishing or revising hydraulic parameters, then comparing the computed profile with the recorded 1969 flood profile until the desired reproduction of the recorded profile was obtained. See Table H-6 for a summary of the finalized modeling data from the Flood Plain Information report. For the proposed conditions, channel roughness coefficients and cross section geometery were appropriately adjusted for reaches where channel excavation and/or riprap are proposed. Typical channel cross-sections for the existing diversion structure and Redwood River channel through Marshall are shown on Plate H-18.

#### UPSTREAM REACH

29. Backwater computations for the upstream study reach were started at critical depth at the diversion structure spillway. (See plate H-19 for sketch). The discharge over the spillway was determined from the diversion structure rating curve shown on plate H-11. The rating curve was obtained from an earlier study, "Flood Control General Design Memorandum on Redwood River at Marshall, Minnesota". At the design discharge, the proposed levee would result in approximately a 0.75 foot stage increase. However, upstream of the wayside park, there would only be a slight increase in stage. Water surface profiles for existing and proposed conditions along the upstream reach are shown on plates H-10 and plates E-1, E-2, and E-3.

| Cross        |   | Elevat           |                     |              | annings "     | n''                                   |
|--------------|---|------------------|---------------------|--------------|---------------|---------------------------------------|
| Sect.<br>No. | Description                               | Observed<br>1969 | HEC - 2<br>Computed | left<br>Bank | Right<br>Bank | Channel                               |
|              |   |                  |                     |              |               | · · · · · · · · · · · · · · · · · · · |
| 10           | Highway 67                                | 1125.8           | 1125.8              | 0.1          | 0.1           | .035                                  |
| 20           | ffl Limit                                 |                  | 1139.81             | 0.1          | 0.1           | .035                                  |
| 27           | Southwest State College                   |                  | 1141.52             | 0.1          | 0.1           | . 035                                 |
| 28           | Dike                                      |                  | 1142.09             | .08          | . 0 <b>8</b>  | . 035                                 |
| 29           | Residential Dike                          | 1145             | 1144.46             | . 08         | . 08          | .035                                  |
| 31           | Mile ob 1                                 | 1149.5 🚧         | 1147.51             | , 08         | . 08          | 035                                   |
| 513          | Township Road Bridge                      |                  | 1149.77             | .05          | .05           | .03                                   |
| 59-          | Broy Structure T.W.                       | *****            | 1153.40             | .05          | .05           | . 03                                  |
| 299          | Diversion Channel<br>Dron Structure       |                  | 1159.7              | .05          | .05           | .035                                  |
| 643.5        | Diversion Structure                       |                  | 1168.67             | .05          | .05           | .034                                  |
| 34           | Kossuth Ave. Bridge                       | 1149.4           | 1149.4              | 0.1          | 0.1           | .0365                                 |
| 40           | N. 4th St. (U.S.G.S.<br>gaging station)   | 1152.5           | 1152.49             | 0.1          | 0.1           | .0365                                 |
| 43           | N. 3rd Street                             |                  | 1154.31             | 0.1          | 0.1           | .044                                  |
| 45           | N. 2nd St. (E. College Dr                 | ive)             | 1154.96             | 0.1          | 0.1           | .044                                  |
| 49           | Main Street                               |                  | 1157.82             | 0.1          | 0.1           | .044                                  |
| 51           | W. College Drive (S. 2nd )                | St.)             | 1158.22             | 0.1          | 0.1           | .044                                  |
| 53           | C & N. W. R. R.                           |                  | 1158.73             | 0.1          | 0.1           | .046                                  |
|              | Saratoga Street                           |                  | 1159.69             | 0.1          | 0.1           | .046                                  |
| 58           | S 4th Street                              |                  | 1162.33             | 0.1          | 0.1           | .042                                  |
| 6.           | West College Dr. (TH 19)                  |                  | 1165.06             | 0.1          | 0.1           | .042                                  |
| 72           | Diversion Channel Culvert                 | 5                | 1174 25             | 0.1          | 0.1           | .047                                  |
| 76           | CSAH 7                                    | 1177.8           | 1177.72             | 0.1          | 0.1           | .0495                                 |
| 87           | B.N.R.R. Bridge (Upstream<br>study limit) | 1195.9*          | 1195.87             | 0.1          | 0.1           | .040                                  |

#### COMPUTER MODEL DATA FOR MARSHALL, MN

\* Estimated High Water Mark

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\*\* It was assumed that this elevation was unnaturally high due to ice in downstream channel, therefore, the rating curve elevation of 1147.57 was matched.

Shock loss coefficients = .3 and .1 at All Locations (Expansion and Contraction Respectively)

Special Bridge Routine Used At All Bridges

30. D2 and tailwater rating curves for the existing diversion structure and existing diversion channel drop structure are shown on Plate H-17. Tailwater elevations computed using the HEC-2 computer program (n assumed = 0.030) are also shown for each structure. The computed tailwater elevations correspond closely to the most probable extension of the original design curve. Illustrations of these structures are shown on Plate H-19.

#### DOWNSTREAM REACH

31. Backwater computations for the downstream reach were made using slope-area methods starting with normal depth at a point upstream of the T.H. 23 bridge (mile 58.3). At design discharge, the proposed levee would result in approximately a 0.5 foot stage increase over existing conditions. The proposed channel widening between station 0 + 00 and 13 + 50 would eliminate river stage increases upstream of the confluence of the Redwood River and diversion channel caused by the 1260 cfs flow increase from the upstream reach under proposed diversion conditions. Water surface profiles for existing and proposed conditions along the downstream reach are shown on Plate H-10.

#### STREAM VELOCITIES

32. Average design flow velocities for improve conditions at selected locations are shown in Table H-7.

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| River Station $\frac{1}{2}$ | Channel<br>(fps) | Maximum Overbank<br>(fps) |
|-----------------------------|------------------|---------------------------|
| Upstream Reach              |                  |                           |
| 8 + 75                      | 4.7              | * <u>2/</u>               |
| 9 + 25 (CSAH 7 bridge       | 9) 4.9           | * <u>2/</u>               |
| 9 + 90                      | 5.7              | 0.9                       |
| 21 + 75                     | 7.2              | 1.1                       |
| 40 + 00                     | 4.6              | 1.0                       |
| 42 + 87                     | 7.2              | 1.4                       |
| 71 + 75                     | 6.9              | 1.4                       |
| <b>91 +</b> 75              | 5.1              | 1.1                       |
| 100 + 75                    | 7.5              | 1.6                       |
| 121 + 40 (BNR bridge)       | 5.0              | * <u>2/</u>               |
| Downstream Reach            |                  |                           |
| 3 + 80                      | 6.1              | 0.7                       |
| 15 + 20                     | 8.0              | 1.4                       |
| 24 + 06                     | 5.6              | 1.1                       |
| 32 + 30                     | 3.0              | 0.7                       |
| 57 + 20                     | 5.2              | 1.0                       |
| 75 + 00                     | 4.8              | 1.2                       |

Table H-7 - Computed Average Velocities Under Proposed Conditions at Selected Locations

 $\frac{1}{Stationing}$  proceeds upstream from the existing diversion structure and downstream from the drop structure at the confluence of the diversion channel and the Redwood River.

 $\frac{2}{N_{o}}$  overbank flooding.

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EFFECT ON BRIDGES

33. Two bridges are located along the upstream reach. These are the C.S.A.H. 7 bridge and the Burlington-Northern Railroad bridge. Riprap slope protection would be required only at the C.S.A.H. 7 bridge. At design conditions, the proposed improvements would have no significant effect on the existing 100-year water surface elevation and/or the velocity at the Burlington-Northern Railroad bridge. However, at the 133-year design conditions, the proposed improvement would result in a 2.1-foot increase in stage and 0.1 decrease in velocity at the C.S.A.H. 7 bridge. Two bridges are also located along the downstream study reach. However, these bridges are located downstream of the proposed improvements with the nearest bridge approximately 3-1/2 miles downstream of the proposed improvements. Pertinent bridge data and design water surface elevation are given in table E-8.

## Table H-8 - Bridge Data

| Item                 | C.S.A.H. 7<br>Bridge | Burlington-<br>Northern<br>Railroad<br>Bridge |
|----------------------|----------------------|---|
|                      |                      |   |
| Deck elevation       | 1184.2               | 1205.0  |
| Low steel elevation  | 1182.9               | 1201.5  |
| Design water surface | 1182.58              | 1195.4  |
| Length               | 152 feet             | 85 feet                                       |
| Waterway opening 1/  | 1607 square feet     | 2335 square feet                              |

 $\frac{1}{N}$  Net flow area up to low steel

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# BACKWATER EFFECTS WITHIN MARSHALL

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34. During times of major flooding, backwater effects caused by the combined Redwood River and diversion channel flows are evident within the downstream areas of the City of Marshall. This phenomenon was verified by the HEC-2 model by utilizing a constant 1500 cfs discharge through the City and downstream reaches to determine a natural profile. The model was then used to compute the 100-year and SPF existing condition profiles. These profiles were then compared to the natural profile to determine the extent of backwater effect within Marshall. According to this analysis, the 100-year backwater effect will extend to approximately North 6th Street and the SPF (Condition 2) effect will extend to East Main Street. (See plate H-10 for street crossing locations). However, the proposed channel widening measures downstream of the confluence would eliminate the 100-year backwater effects.

# ANALYSIS OF PROPOSED OVERFLOWS TO COTTONWOOD BASIN

35. Water surface profiles of the 133-year and Standard Project flood overflows to the Cottonwood Basin were derived using the HEC-2 Computer Program. These profiles followed the alignment of County Ditch #70, starting at critical depth approximately 1,000 feet downstream of County Road 67 and extending upstream west of CSAH #7 to the approximate end of the proposed overflow channel. The computations indicated an SPF profile which was 3-9 feet below the Highway 23 profile at all locations except in the vicinity of the intersections of the ditch and CSAH #7. At this location, the elevation of the SPF overflow profile would be about 1/2 foot below the elevation of Highway 23. SPF floodwaters could pass through five culverts through the Hwy.23 embankment but would not reach the developed area of Marshall based on existing topographic information. None of the culverts would be affected at the design flood level.

#### SEDIMENT TRANSPORT

36. A comparison of the pre-existing project with the existing project rating curves for the USGS gage site (mile o7.2) reveals the occurrence of sediment deposition between gage heights of 0 to 7 feet. The maximum increase in stage due to sediment deposition occurs at a stage of about 5 feet (1,000 cfs). Between the gage heights of 7 and 10 feet sediment loss is evident, and at a gage height of 9 feet the maximum decrease in stage (0.12 feet) due to this loss occurs. The above phenomena indicates that at low stages, the sediment load within the Redwood river is less than at high stages. This is due primarily to low velocities, characteristic of low stages, which allow the sediment to settle out and the opposite which is true for the high velocities characteristic of high stages.

#### HYDRAULIC DESIGN OF OVERFLOW-DIVERSION STRUCTURE

37. The hydraulic design of the proposed overflow diversion structure is based on controlled overflows commencing at a Redwood River discharge of approximately 6,500 cfs. Approximately one-half of the discharge in excess of 6,500 cfs would be diverted into the Cottonwood basin with the remaining 50 percent passing downstream through Marshall. The 540-foot long overflow diversion structure would commence at right bank levee station 58 + 90 and extend westward along the Redwood River as shown on plate E-3. The structure would consist of a gabion embankment with a 6-inch high by 6-inch wide concrete projection on the crest to provide positive control. The crest elevation would be 1192.64 at the downstream end and 1192.94 at the upstream end. Plate E-3, section A-A, shows a typical section through the overflow diversion structure.

38. At the design discharge of 9,000 cfs, approximately 1260 cfs would be diverted into the Cottonwood River basin. Plate H-12 depicts the rating curve for the overflow diversion structure. The rating curve on plate H-13 shows the discharge relationship between Redwood River flows and flows diverted into the Cottonwood River basin.

#### HYDRAULIC DESIGN OF GABION DROP STRUCTURE

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39. The proposed gabion drop structure would be located at station 97 + 45 (river mile 72.04), approximately 220 feet downstream of the proposed overflow weir. The design for this structure was based on ETL 110-2-194. The structure would be 6.1 feet high, have IV on 4H and IV on 6H slopes on the respective upstream and downstream faces. The weir crest (elev. = 1186.1) would be grouted, have a length of 91.6 feet, and a width of 9 feet. Four 36" RCP culverts through the structure would pass low flows (maximum = 300 cfs).

40. Approximately once every 1.3 years, discharged mentioned exceed the capacity of the culverts and this additional flow would pass over the weir crest. Plate H-13 shows the rating curve for the proposed gabion drop structure. According to Plate 4 of the ETL, free flow would still exist during the design and SPF discharges and therefore the structure would provide a positive control of river stages in the vicinity of the overflow diversion. Channel widening upstream of the drop structure would lower the water surface upstream of the park to that of existing conditions.

## HYDRAULIC DESIGN OF OVERFLOW CULVERTS

41. Three 115-inch by 72-inch arch culverts, 155 feet long, would be required to pass the design discharge of 1,260 cfs through T.H. 23 embankment. These culverts would have a slope of 0.25 percent and an inlet invert elevation of 1183.9. At design discharge of 1,260 cfs, the water surface in the park would be 1.5 feet below the minimum highway elevation  $\sqrt{2}$  1193.3. A maximum flow of 1,500 cfs would pass through the culverts before T.H. 23 is overtopped. This flow would correspond to a discharge of 9,800 cfs (167-year flood) in the Redwood River upstream of the overflow diversion structure. At standard project flood conditions, 2,220 cfs would be diverted into the Cottonwood River basin. Hydraulic design details for the culverts are shown on plate E-4.

## HYDRAULIC DESIGN OF RIPRAP

42. A hydraulic study was made to determine required riprap sizes based on an analytical determination of shear force created by channel flow and the ability of the riprap revetment to withstand these forces. This method is defined in EM 1110-2-1601, "Hydraulic Design of Flood Control Channels", July 1, 1970, and ETL 1110-2-120, "Additional Guidance for Riprap Channel Protection", May 16, 1971. In addition, Report No. 47 of Massachusetts Institute of Technology Hydrodynamics Laboratory on "Stream Dynamics and Boundary Stream

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Distributions for Curve Trapezoidal Channels", by A. T. Ippen, et al, January, 1962, was referred to.

43. Studies indicate that the riprap size required would range from 12 inches to 24 inches ( $D_{50}$  minimum from 5 to 17 lb.). The entire channel would be lined with riprap in the vicinity of C.S.A.H. 7 bridge (30 feet upstream and 50 feet downstream). Channel side slopes in the vicinity of the proposed gabion drop Structure (both 40 feet upstream and downstream) would be riprapped. In other areas, riprap would be placed on the outside bank of the channel bends. Table H-9 gives the required riprap types. Plates E-1 through E-3 and E-11 show the locations of required riprapped bank areas.

44. Bedding material (uniformly graded coarse material) would be placed in thicknesses ranging from 6 inches to 9 inches. This material would be placed at one-half the riprap thickness to a maximum of 12 inches for above water placement and 18 inches for underwater placement.

#### Table H-9 - Proposed Riprap Type

| Location                 | Riprap Type |
|--------------------------|-------------|
| Upstream reach stations: |             |
| 8 + 35 to 9 + 65         | Туре А      |
| All other locations      | Туре В      |
| All headwalls            | Туре С      |

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|          | ан <b>46-9;</b><br>Пан <b>46-9;</b> | P | EDWOOD<br>DR FLOC<br>AUL DIS |   | AT MAR<br>ROL(U)<br>JUN 79 | CORES | UNNESO<br>OF ENG | 1A; FE/<br>INFERS | ST PAU | TY REPO<br>L MIN 51<br>G 13/2 | )RT <b>S</b><br>I | 77 |  |
|----------|-------------------------------------|---|------------------------------|---|----------------------------|-------|------------------|-------------------|--------|-------------------------------|-------------------|----|--|
|          |                                     |   |                              |   |                            |       |                  |                   |        | 0 1372                        |                   |    |  |
| _        |                                     |   |                              |   | <u> :</u>                  |       |                  |                   |        |                               |                   |    |  |
|          |                                     |   |                              |   |                            |       |                  | -                 |        |                               | :                 |    |  |
|          |                                     |   |                              | 1 |                            |       |                  |                   |        |                               |                   |    |  |
|          |                                     |   |                              |   |                            |       |                  |                   |        |                               |                   |    |  |
|          |                                     |   |                              |   |                            |       |                  |                   |        |                               |                   |    |  |
|          |                                     |   |                              | - | -                          | ·     |                  | -                 |        |                               | ·                 | -  |  |
| <u>.</u> |                                     |   |                              |   |                            |       |                  |                   |        |                               |                   |    |  |
|          |                                     |   |                              |   |                            |       |                  |                   |        |                               |                   |    |  |



### Table H-9 - Proposed Riprap Type (continued)

| Location                   | Riprap Type |
|----------------------------|-------------|
| Overflow channel stations: |             |
| 3 + 60 to $6 + 90$         | Type D      |
| 5 + 20 to 7 00             | Type D      |
| All other locations        | Туре С      |

Downstream reach stations:

0 + 00 to 13 + 50 Type B

## INTERIOR DRAINAGE

UPSTPEAU REACH

45. Required upstream interior drainage works would include modification of the State Highway 23 drainage system at the roadside park, installation of flap-gates on two double 30-inch railroad culverts (headwalls A and B), an 18-inch flap-gated culvert (headwall C) at station 11 + 20 of the left bank levee, installation of a flap-gate on an existing driveway culvert (headwall E) at stations 63 + 50, and installation of a 12-inch C M P culvert through a driveway at right bank levee station 10 + 00. Modification of the State Highway 23 drainage system would include installation of a flap-gate on the existing 36-inch highway culvert (headwall F), excavation of a 10-foot wide parabolic channel leading to the overflow structure, and a flap-gated 36-inch reinforced concrete culvert (headwall E) through the structure. Minor landscaping measures would also be accomplished at right bank levee.

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46. The ditch on the north side of the railroad tracks slopes in the northeasterly direction towards the city of Marshall. Headwalls A and B will prevent water from entering the ditch and flowing towards the city. The culvert at headwall C will provide drainage for approximately 2.5 acres of land located adjacent to the levee. Installation of flap-gated headwalls D and F will prevent Redwood River water from getting into the Cottonwood River basin except via the overflow diversion channel. The land south of State Highway 23 slopes in the south-asterly direction towards County Ditch 70. Thus, flap-gating the State Highway 23 culvert will not create any problems. The existing culvert at station 63 + 50 provides drainage for less than one acre of land. The installation of a flap-gate on this culvert will likewise not create any adverse effects. Typical details for the upstream reach interior drainage facilities are shown on plates E-4 and E-8 at the end of Section E.

## DOWNSTREAM REACH

#### General

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47. The proposed levee alignment would obstruct the runoff from approximately 57 acres of land under existing conditions. This runoff would flow unrestricted into the Redwood River. The proposed plan incorporating a 7-acre pond at approximate levee station 27 + 00 would provide approximately 36 acre-feet of storage at elevation 1138.0. A collector ditch would be provided alongside the levee for collection and transfer of runoff to the ponding area. The pond would be drained into County Ditch 62 via a 24-inch R C P. The inlet to the 24-inch R C P would consist of a flared section with a trestle guard. Outflows into the County

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ditch would be controlled by a manually-operated gate well and flap-gate. Since this portion of County Ditch No. 62 is several miles upstream from its junction with the Redwood River, water levels in the ditch upstream of the State Highway 23 crossing are unaffected by river stage changes in the Redwood River. Plates E-9 and E-12 show the details of the pond and the outlet structures.

48. The proposed pond and gravity outlet were studied in detail to determine the maximum pond level and added flow into County Ditch No. 62. For this analysis, two major past floods -- the floods of 1957 and 1969, and the 50-year, 100-year, and standard project storms were considered. Results of these studies are presented in the following paragraphs.

49. Unit hydrograph -- A unit hydrograph, using Snyder's method, was developed for the 57-acre area. The following parameters were used in the development of the unit hydrograph.

A = 0.089 square miles. L = 0.756 miles. t = 0.897 hours. C = 0.469 C = 1.4

where A = drainage area

L = length of channel to outlet

t = lag time for unit rainfall duration to peak of unit p hydrograph.

 $C_p$  and  $C_t$  = drainage basin characteristics coefficients. Table H-10depicts 30-minute unit hydrograph ordinates.

Table H-10 - Unit Hydrograph

Time 5.5 6.0 5.0 3.0 3.5 .0 4.5 (hours) 0.5 1 0 1.5 2 0 2 5 Runoff 30 ٥ 12 29 (cfs)

50. Precipitation and Precipitation Excess -- Rainfall and rainfall excess values for the 1957 flood were obtained from an earlier flood control study of the Redwood River at Marshall, Minnesota. Table H-11 shows the precipitation, precipitation excess and the computed runoff hydrograph. The initial snow pack moisture content for the 1969 flood was obtained from data gathered during field surveys by the Corps of Engineers. Snow melt computations were based on mean daily temperature. Rainfall that occurred between 8 and 15 April was added to the snow melt. Precipitation and temperature records were obtained from climatologic data recorded by the National Weather Service. Table H-12 depicts the precipitation excess and values for the computed runoff hydrograph.

| Table | H-11- | Precipitation, Precipitation Exc | cess  |
|-------|-------|----------------------------------|-------|
|       |       | and Runoff Hydrograph for 1957 S | Storm |

| Tim <b>e</b><br>(hours) <u>1</u> / | 3    | 6    | 9    | 12   | 15   | 18   | 21   | 24   | 27   |
|------------------------------------|------|------|------|------|------|------|------|------|------|
| Rainfall<br>(ins.)                 | 0.48 | 0.82 | 0.62 | 1.12 | 1.50 | 2.47 | 0.38 | 0.10 | 0.05 |
| Loss<br>(ins.)                     | 0.48 | 0.82 | 0.19 | 0.22 | 0.15 | 0.15 | 0.15 | 0.10 | 0.05 |
| Rainfall<br>Excess<br>(ins.)       | 0.00 | 0.00 | 0.43 | 0.90 | 1.35 | 2.32 | 0.33 | 0.00 | 0.00 |

 $\frac{1}{1}$  Time in hours from start of rainfall on June 16

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Table H-11- Precipitation, Precipitation Excess and Runoff Hydrograph for 1957 Storm (continued)

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| 8.5       0         9.0       5         9.5       13         10.0       12         10.5       8         11 0       5         11.5       3         12.0       13         12.5       28         13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         21.5       14         21.0       13         22.5       8 | Time in Hours 1/ | Runoff in cfs. |
|--|------------------|----------------|
| 9.0       5         9.5       13         10.0       12         10.5       8         11 0       5         11.5       3         12.0       13         12.5       28         13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         21.5       14         21.0       13         22.5       8                     | 8.5              | 0              |
| 9.5       13         10.0       12         10.5       8         11 0       5         11.5       3         12.0       13         12.5       28         13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         21.5       15         22.0       12  |                  | 5              |
| 10.0 $12$ $10.5$ $8$ $11.0$ $5$ $11.5$ $3$ $12.0$ $13$ $12.5$ $28$ $13.0$ $27$ $13.5$ $17$ $14.0$ $10$ $14.5$ $5$ $15.0$ $20$ $15.5$ $42$ $16.0$ $40$ $16.5$ $25$ $17.0$ $16$ $17.5$ $8$ $18.0$ $33$ $18.5$ $72$ $19.0$ $69$ $19.5$ $43$ $20.0$ $27$ $20.5$ $14$ $21.0$ $13$ $21.5$ $15$ $22.5$ $8$  |                  | 13             |
| 11.0511.5312.01312.52813.02713.51714.01014.5515.02015.54216.04016.52517.01617.5818.03318.57219.06919.54320.02720.51421.01321.51522.01222.58  |                  | 12             |
| 11 05 $11.5$ 3 $12.0$ 13 $12.5$ 28 $13.0$ 27 $13.5$ 17 $14.0$ 10 $14.5$ 5 $15.0$ 20 $15.5$ 42 $16.0$ 40 $16.5$ 25 $17.0$ 16 $17.5$ 8 $18.0$ 33 $18.5$ 72 $19.0$ 69 $19.5$ 43 $20.0$ 27 $20.5$ 14 $21.0$ 13 $21.5$ 15 $22.5$ 8  |                  | 8              |
| 12.0       13         12.5       28         13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         21.5       14         21.0       13         22.5       8   |                  | 5              |
| 12.5       28         13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         22.5       8   |                  | 3              |
| 13.0       27         13.5       17         14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.5       8   | 12.0             | 13             |
| 13.51714.01014.5515.02015.54216.04016.52517.01617.5818.03318.57219.06919.54320.02720.51421.01321.51522.01222.58  | 12.5             | 28             |
| 14.0       10         14.5       5         15.0       20         15.5       42         16.0       40         16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         22.5       8   | 13.0             | 27             |
| 14.5514.52015.54216.04016.52517.01617.5818.03318.57219.06919.54320.02720.51421.01321.51522.58  | 13.5             | 17             |
| 145 $20$ $155$ $42$ $16.0$ $40$ $165$ $25$ $170$ $16$ $175$ $8$ $18.0$ $33$ $18.5$ $72$ $19.0$ $69$ $19.5$ $43$ $20.0$ $27$ $20.5$ $14$ $21.0$ $13$ $21.5$ $15$ $22.5$ $8$   | 14.0             |                |
| 15.0 $42$ $16.0$ $40$ $16.5$ $25$ $17.0$ $16$ $17.5$ $8$ $18.0$ $33$ $18.5$ $72$ $19.0$ $69$ $19.5$ $43$ $20.0$ $27$ $20.5$ $14$ $21.0$ $13$ $21.5$ $15$ $22.5$ $8$  | 14.5             |                |
| 16.0 $40$ $16.5$ $25$ $17.0$ $16$ $17.5$ $8$ $18.0$ $33$ $18.5$ $72$ $19.0$ $69$ $19.5$ $43$ $20.0$ $27$ $20.5$ $14$ $21.0$ $13$ $21.5$ $15$ $22.5$ $8$  | 15.0             |                |
| 16.5       25         17.0       16         17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.5       8  | 15.5             | 42             |
| 17.016 $17.5$ 8 $18.0$ 33 $18.5$ 72 $19.0$ 69 $19.5$ 43 $20.0$ 27 $20.5$ 14 $21.0$ 13 $21.5$ 15 $22.0$ 12 $22.5$ 8   | 16.0             | 40             |
| 17.5       8         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8  | 16.5             |                |
| 17.3       33         18.0       33         18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 17.0             |                |
| 18.5       72         19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 17.5             |                |
| 19.0       69         19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 18.0             |                |
| 19.5       43         20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 18.5             |                |
| 20.0       27         20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 19.0             |                |
| 20.5       14         21.0       13         21.5       15         22.0       12         22.5       8   | 19.5             |                |
| 21.0       13         21.5       15         22.0       12         22.5       8   | 20.0             |                |
| 21.5       15         22.0       12         22.5       8   | 20.5             |                |
| 22.0<br>22.5<br>12<br>8  | 21.0             |                |
| 22.5 <b>8</b>  | 21.5             |                |
| 22.5 8   |                  |                |
|  | 22.5             |                |
| 23.0 6   |                  | 6              |

 $\underline{U}_{\text{Time in hours from start of rainfall on June 16.}}$ 

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Table H-12 Precipitation Excess and Runoff from 1969 Snow Melt

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| Date: April 2      | ril 2 | r    | -7  | 2   | ٥                           | Prec<br>7 | Precipitation Excess         11         12         13         14         15  | n Exce:<br>9    | 55<br>10       | 11  | 12  | 13              | 14  | 15                 |
|--------------------|-------|------|-----|-----|-----------------------------|-----------|--|-----------------|----------------|-----|-----|-----------------|-----|--------------------|
| Excess<br>(ins.) ( | 0.75  | 0.57 | 0.9 | 0.0 | û.63                        | 1.2       | <b>0.57 0.9 0.0 0.63 1.2 1.71</b> <sup><u>1</u>/ <b>0.38</b><u>1/</u> <b>0.11</b><u>1/</u> <b>0.0 0.0 0.03</b><sup><u>2/</u></sup> <b>0.0 0</b>.12<sup><u>2/</u></sup></sup> | 0.38 <u>1</u> / | 0.11 <u>1/</u> | 0.0 | 0.0 | 0.03 <u>2</u> / | 0.0 | 0.12 <sup>2/</sup> |
|                    |       |      |     |     | Rumoff - April 8 <u>3</u> / | April     | 83/  |                 |                |     |     |                 |     |                    |

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| Time in Hours<br>0.0<br>0.5<br>1.0<br>1.5<br>2.5<br>3.0<br>3.5<br>4.0<br>4.5 |  | Time in Hours Runoff (cfs) | 0.0 | 0.5 5 | 1.0 13 | 1.5 12 | 2.0 8 | 2.5 5 | 3.0 3 | <b>3.5</b> 2 | 4.0 1 | 4.5 .S |
|--|--|----------------------------|-----|-------|--------|--------|-------|-------|-------|--------------|-------|--------|
|--|--|----------------------------|-----|-------|--------|--------|-------|-------|-------|--------------|-------|--------|

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|                               | 50-Yr.5                 | storm Ra                          | i <b>nfall</b>       | 100-Yr.S                | Storm Ra                          | ainfall |                         | d Projec<br>ainfall               | t                    |
|-------------------------------|-------------------------|-----------------------------------|----------------------|-------------------------|-----------------------------------|---------|-------------------------|-----------------------------------|----------------------|
| Time<br>in<br><u>Hours</u> -/ | Rain-<br>fall<br>(ins.) | Rain-<br>fall<br>Excess<br>(ins.) | Run-<br>off<br>(cfs) | Rain-<br>fall<br>(ins.) | Rain-<br>fall<br>Excess<br>(ins.) | Run -   | Rain-<br>fall<br>(ins.) | Rain-<br>fall<br>Excess<br>(ins.) | Run-<br>ofi<br>(cfs) |
| 89.0                          |                         |                                   | 0                    |                         |                                   | 0       |                         |                                   | 0                    |
| 89.5                          | 0.335                   | 0.234                             | 3                    | 0.536                   | 0.375                             | 5       | 0.353                   | 0.328                             | 4                    |
| 90.0                          | 0.165                   | 0.116                             | 8                    | 0.264                   | 0.185                             | 13      | 0.187                   | 0.162                             | 12                   |
| 90.5                          | 0.058                   | 0.033                             | 11                   | 0.125                   | 0.100                             | 18      | 0.126                   | 0.101                             | 16                   |
| 91.0                          | 0.042                   | 0.017                             | 9                    | 0.075                   | 0.050                             | 16      | 0.075                   | 0.050                             | 14                   |
| 91.5                          | 0.125                   | 0.100                             | 7                    | 0.125                   | 0.100                             | 13      | 0.126                   | 0.101                             | 12                   |
| 92.0                          | 0.075                   | 0.050                             | 7                    | 0.075                   | 0.050                             | 11      | <b>0</b> .075           | 0.050                             | 11                   |
| 92.5                          | 0.125                   | 0.100                             | 8                    | 0.125                   | 0.100                             | 10      | 0.260                   | 0.235                             | 11                   |
| 93.0                          | 0.075                   | 0.050                             | 8                    | 0.075                   | 0.050                             | 9       | 0.140                   | 0.115                             | 14                   |
| 93.5                          | 0.190                   | 0.165                             | 9                    | 0.259                   | 0.234                             | 11      | 0.260                   | 0.235                             | 16                   |
| 94.0                          | 0.108                   | 0.083                             | 11                   | 0.141                   | 0.116                             | 14      | 0.140                   | 0.115                             | 18                   |
| 94.5                          | 0.393                   | 0.368                             | 15                   | 0.393                   | 0.368                             | 18      | 0.528                   | 0.503                             | 22                   |
| 95.0                          | 0.207                   | 0.182                             | 20                   | 0.207                   | 0.182                             | 23      | 0.273                   | 0.24 <b>8</b>                     | 29                   |
| <b>95</b> .5                  | 1.934                   | 1.909                             | 43                   | 2.135                   | 2.110                             | 47      | 2.739                   | 2.714                             | 61                   |
| 96.0                          | 0.966                   | 0.941                             | 83                   | 1.065                   | 1.040                             | 91      | 1.361                   | 1.336                             | 117                  |
| <b>96</b> .5                  |                         |                                   | 92                   |                         |                                   | 102     |                         |                                   | 131                  |
| 97.0                          |                         |                                   | 67                   |                         |                                   | 73      |                         |                                   | <b>9</b> 5           |
| 97.5                          |                         |                                   | 41                   |                         |                                   | 45      |                         |                                   | 58                   |
| <b>98</b> .0                  |                         |                                   | 24                   |                         |                                   | 26      |                         |                                   | 33                   |
| <b>98</b> .5                  |                         |                                   | 14                   |                         |                                   | 16      |                         |                                   | 20                   |
| 100.0                         |                         |                                   | 8                    |                         |                                   | 9       |                         |                                   | 12                   |
| 100.5                         |                         |                                   | 4                    |                         |                                   | 5       |                         |                                   | 6                    |
| 101.0                         |                         |                                   | 3                    |                         |                                   | 3       |                         |                                   | 4                    |
| 101.5                         |                         |                                   | 3                    |                         |                                   | 3       |                         |                                   | 4                    |
| 102.0                         |                         |                                   | 1                    |                         |                                   | 1       |                         |                                   | 1                    |
| 102.5                         |                         |                                   | 0                    |                         |                                   | 0       |                         |                                   | 0                    |

# Table H-13 Precipitation, Precipitation Excess and Runoff Ilydrograph for Hypothetical Storm

Hypothetical flood time - accumulative hours to end of period.

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51. Future Storms - Rainfall and rainfall excess values for the 50-year, 100-year and the standard project storm were computed according to the method described in EM 1110-2-1410. These storms resulted in a peak discharge of 92 cfs, 102 cfs and 113 cfs respectively. Table H-13 depicts the precipitation, precipitation excess and runoff for these storms.

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52. Other Past Storm - Other past storms considered but not analyzed in detail are the June 1947 and June 1952. The June 1947 storm had a total precipitation of 2.86 inches. The June 1952 storm resulted in a total precipitation of 2.13 inches. None of these storms have the intensity of the 1957 storm or the runoff magnitude of the 1969 snow melt. Consequently, they we we dropped from further consideration.

53. Collector Ditch - The collector ditch was designed to accommodate the runoff from the 50-year storm. In determining the capacity of the collector ditch, the peak discharge of 92 cfs has been prorated along the length of the levee. The collector ditch would have a slope of 0.00167 feet/foot and 0.00256 feet/foot between levee stations 62 + 00 to 50 + 10 and 50 + 10 to 29 + 20respectively. The bottom width would be 7 feet and 9 feet between levee stations 62 + 00 to 38 + 00 and 38 + 00 to 29 + 20 respectively The ditch side slopes would be 1 vertical on 3 horizontal. Two 24-inch R C P culverts would pass ditch flows under County Highway 67. The protected land area on the east side of the ponding area either slopes towards County Ditch 62 or towards the pond. Thus a collector ditch is not needed in this area.

54. The maximum recorded runoff occurred during the 1969 snow melt. The 1969 snow melt (tableH-12) between April 2 and 15 resulted in 6 4 inches of runoff. This would require approximately 30.4 acre-feet

of storage. As shown on plate H-15, the design storage capacity of the proposed pond including the collector ditch is approximately 36 acre-feet. The 50-year, 100-year, and standard project storms would result in 4.35, 5.06, and 6.29 inches of runoff respectively. These storms would require 20.65, 24.03, and 29.89 acre-feet of storage respectively. Thus, the Standard Project Storm runoff or the largest recorded historical runoff could be stored in the proposed ponding area.

55. Outflow from Ponding Area - The outflow from the ponding area into County Ditch 62 would be via an 800-foot long by 24-inch diameter R C P pipe and would be controlled by a gate well. Proposed gate operating procedure requires that the gate well would not be opened until the water level in County Ditch 62 recedes to the crown of the outlet pipe. With the maximum water surface in the pond and the water surface in the County Ditch at the crown of the outlet pipe, the peak outflow would be approximately 13 cfs. It would take approximately 2-1/2 days for the pond to drain out completely.

## FOUNDATIONS AND MATERIALS

#### SUBSURFACE EXPLORATION AND TESTING

56. Soil borings were taken in the upstream sector of the project and six in the downstream sector to determine the levee foundation profile. Two borings were taken at the location of the overflow channel. All borings were 20 feet deep and taken by a truck-mounted rig. Three-inch diameter tube samples were obtained at most holes. The borings are shown on plates E-1 thru E-3 and E-9 thru E-11.

57. Laboratory testing of subsurface samples included 29 moisture content and Atterberg limit determinations, 33 graduations, and 11 Q-triaxial tests on undisturbed samples. The results of these tests are shown on tables H-15 and H-16 and Plates H-20 thru H-51.

#### SUBSURFACE PROFILE

58. The surface profile at Marshall is quite variable. The levee sites were divided into 9 typical reaches based on the subsurface profile and surface geometry. The limits of these reaches are shown on plate H-17. Borings for reaches 8 and 9 found cohesive soil throughout the full depth of the boring. Borings in reaches 1, 3, 4, 5 and 7 show a pervious zone greater than 5 feet thick and a semi-pervious zone overlying it. The semi-pervious zone is greater than 5 feet thick except in reaches 1 and 3. The boring in reach 1 shows mostly cohesive soil and a 3-foot seam of slightly pervious material while reach 6 appears to have 13 feet of pervious material overlying cohesive material. Cohesive soils in the project area are generally low plasticity clays with moisture contents ranging from 15 percent to 40 percent and liquid limits from 25 to 60. Pervious soils in the area range from medium sands to silty sand.  $D_{10}$  sizes range as high as .37 mm.

#### SEEPAGE AND UPLIFT

#### GENERAL

59. Methods for development of the various constants and analyses for seepage and uplift pressures were taken from Technical Memorandum No. 3-424, Volume 1, "Investigation of Underseepage and Its Control - Lower Mississippi River Levees by Waterways Experiment Station, Vicksburg, Mississippi," October, 1956. As described under the heading "Subsurface Profile", the foundation conditions for the levee generally consist of an impervious to a semi-impervious blanket overlying a relatively pervious sand zone.

60. Average horizontal permeabilities  $(k_f)$  of the pervious strata were determined by using the method shown on plate H-16. Values of  $K_b$  used in the analysis were determined from the  $D_{10}$  grain sizes of field pumping tests as summarized on figure 17, page 51, TM3-424. In this analysis, the various layers of soil making up the top stratum were transformed to a single blanket with a permeability equal to that of the most impervious stratum as illustrated by the sample calculation on plate H-16. Plate H-16 also summarizes the major parameters used in seepage and uplift analysis, along with the results. Values of  $k_V$  were based on data suggested in table 38, page 265, TM 3-424 according to soil classification and total thickness of blanket to the bottom of each stratum.

#### UPLIFT PRESSURES

61. Uplift pressures were analyzed using hydrostatic pressures caused by a water surface at the top of the flood barrier. The

blanket in reaches 1 and 3 was considered to be so thin that it probably would not be continous or effective in causing uplift pressures. There is no uplift problem in reaches 8 and 9 since the subsurface is mostly clay. The factor of safety for reach 7 is 2.1. This is dependent on the blanket being continuous throughout the surrounding area, giving an S distance of 400 feet. This assumption seems to be justified since all borings in the downstream area show as great or greater depth of clay. This assumption, however, will be verified by more borings prior to construction. The factor of safety in all other reaches was calculated to be greater than 1.5 and these reaches were consequently considered to be safe. A unit weight of 110 pcf for the semi-pervious zone was used for all uplift calculations.

#### NOTATIONS

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62. Notations used in the relief well design shown on plate C-26 are as follows: as follows: c A constant for natural top stratum where  $c = \begin{bmatrix} k_b \\ k_f & z_b \end{bmatrix}$ 

- $D_{10}$  Effective grain size, 10 percent of grains smaller than stated size
  - d Thickness of each stratum comprising pervious substratum
  - D Total thickness of the pervious substratum
  - F Factor of safety against uplift
  - g Acceleration due to gravity
  - H Total net head on levee, or height of top of flood barrier above average low-ground surface, or tail water, landward of levee
- h. Allowable (net) head beneath landside top stratum

He Total net head on levee, height of design water surface,

above average low-ground surface, or tail water, landward of leven

k<sub>b</sub>. Vertical permeability of top stratum

 $k_{f}$  Permeability of pervious foundation

 $k_{\rm h}$  Horizontal permeability of individual strata

 $k_{\rm p}$  Vertical permeability of individual strata

L Length of reach

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 $L_{\underline{2}}$  . Horizontal width of levee from landward toe to riverward toe

 $q_e$ . Fotal unit seepage within a reach

Q. Total seepage within a reach

S Distance from landside toe of levee to effective source of seepage entry

X<sub>3</sub> Distance from landside toe of levee to effective seepage exit

z Total thickness of top stratum

 $z_{\rm b}$  Transformed thickness of top stratum (for seepage)

 $z_{t}$  Thickness of landside top stratum (for uplift)

m Moist unit weight of soil

w Unit weight of water

#### SEEPAGE

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63. In all reaches seepage quantities were computed using maximum hydrostatic pressures at the design water surface as follows:

a. In reach 6, where no blanket was defected, seepage was calculated by:

$$Q_s = Lq_s = \frac{7.48 L K_f H_{ws} D}{L_2 + .86 D}$$
 (gpm)

b. In all other reaches seepage is:  $Q_{s} = Lq_{s} = \frac{7.48 L K_{f} DH_{ws}}{S + X_{s}}$ 

Total seepage quantities are shown on plate H-16.

STABILITY

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64. The levee foundation is a variable mixture of cohesive and non-cohesive soils. Since no strikingly weak stratum were detected by the borings, the stability section was chosen at a location where the geometry was most critical. This occurred in reach 6 near boring 75-35M. The soil constants used and problem geometry are shown on plate H-16. The undrained strength of the foundation clay was based on Q-triaxial tests, estimated to be at the lower one-third point of the range. The drained parameter of the sand was estimated from blow counts. The undrained strength of the embankment and OH layer were conservatively estimated based on testing for other projects. Safety factors were calculated with the aid of a digital computer conforming with the methods stated in EM 1110-2-1902 for the end of construction case for circular and noncircular arcs. The critical factor of safety was 1.25. This was considered satisfactory since it is the factor of safety for a natural sand slope calculated by the infinite slope formula. Any failure associated with this formula would be only a surface slough. The factor of safety for all arcs through the levee were well in excess of 1.3.

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#### CHANNEL SIDE SLOPES

65. With two exceptions, channel side slopes of 1V and 3H are proposed for channel improvements along the existing river channel. The riverward slope of the gabion and riprapped surfaced overflow weir would be 1V on 2.5H. Riprapped channel side slopes immediately downstream of the C.S.A.H. 7 bridge would also be 1V on 2.5H. Channel side slopes along the overflow channel would be 1V on 6H on the highway shoulder slope and 1V on 4H on the back slope to meet highway safety design criteria. Other reaches of the channel would have 1V on 6H side slopes to permit movement of farm machinery. The channel reach along the highway right-of-way would also have a parabolic channel bottom in conformance with highway safety standards.

#### LEVEE EMBANKMENT

bb. Levee side slopes would be 1V or 3H in all cases except at the overflow-diversion structure where both the riverward and landward side slopes would be 1V on 2.5H and along three short levee reaches in close proximity to residences. At these locations, the landward slope would be an irregular flattened slope to better blend the levee into the natural setting. Where not otherwise protected, all levee slopes and crowns would be topsoiled to a sixinch depth and seeded with selected grasses.

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#### INSPECTION TRENCH

67. To insure that there are no buried pipes, drain tiles, sand lenses, or other items beneath the levee foundation which would cause unforeseen seepage, it will be necessary to inspect the foundation to a depth of 6 feet below the ground surface whenever the height of the levee is greater than 5 feet for a significant length of levee. Reaches 1 and 3 will be inspected regardless of levee height. Such an inspection will be accomplished by several means. In areas where the channel excavation is directly adjacent to the levee alignment, the open face on the channel cut will serve the purposes of an inspection trench. In other areas where feasible, the excavation for the installation of the interior drainage system will be deepened to a depth of 6 feet for inspection and then backfilled to the grade required for the interior drainage systems. In areas where neither the channel excavation nor the excavation for interior drainage will serve for foundation inspection, a trench with a 6-foot bottom width will be excavated beneath the levee and backfilled with impervious fill.

#### SLOPE PROTECTION

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68. Where proposed levees are from 20 to 50 feet from the channel bank, the levee-ward channel side slope would be riprapped up to the top of the channel banks along reaches where, at design discharge, velocities in excess of 4 feet per second occur. Where the riverward levee side slopes are extensions of the channel side slopes, these slopes would be riprapped up to the top of the levee. The left channel bank within 100 feet of the Burlington Northern Railroad embankment (stations 27 + 50 and 52 + 00) would also be

> Appendix I H-47

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riprapped The entire channel cross-section would be riprapped a distance of 30 feet upstream and 50 feet downstream of the C.S.A.H. 7 bridge. Riprap would be provided to the design water surface elevation over the channel transition at the gabion drop structure. Riprap would also be provided on the widened right channel bank reach below the downstream confluence of the existing diversion channel.

69. Required riprap sizes would range from 12 to 18 inches. Table H-14 shows the riprap gradation and thickness needed at the various locations.

| Туре | Percent L<br>Lighter | Limits of Stone Weight<br>Pounds | Layer Thickness       |
|------|----------------------|----------------------------------|-----------------------|
| A    | 100                  | 26 - 10                          | 12 inches above water |
|      | 50                   | 11 - 5                           | surface and 18 inches |
|      | 15                   | 5 - 2                            | below water surface.  |
| в    | 100                  | 86 - 35                          | 12 inches above water |
|      | 50                   | 26 - 17                          | surface and 18 inches |
|      | 15                   | 13 - 5                           | below water surface.  |
| C    | Sar                  | me as B                          | 12 inches.            |
| D    | 100                  | 56 - 35                          | 18 inches.            |
|      | 50                   | 36 - 17                          |                       |
|      | 15                   | <b>18</b> - 5                    |                       |

Table H-14 Riprap Type, Gradation, and Layer Thickness

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70. The above riprap design was determined from guidance contained in EM 1110-2-1601 and ETL 1110-2-120. Design conditions were based on the 133-year flood. Riprap design shear is based on channel and levee side slopes of 1 on 3 at all places except in the vicinity of the C.S.A.H. 7 bridge, where the channel and levee side slopes would be 1 on 2.5 and 1 on 3 respectively.

#### SOURCES OF CONSTRUCTION MATERIAL

#### BORROW

71. Required levee fill for the upstream reach levees would be obtained in sufficient quantity from the required channel works. In most instances, this material, after removal of unsuitable material, would be placed directly on or near the levee alignment without the need for extensive truck haul. Levee fill for the downstream reach levees would be obtained from the channel widening works, collector ditch excavation, and proposed ponding area. Maximum haul distance in any one direction would be 0.9 mile from the proposed ponding area.

#### RIPRAP AND BEDDING

72. Material of adequate quality for riprap and bedding can be obtained from quartzite or granite quarries located near New Ulm, Morton, Sanborn, and Ortonville, Minnesota. The haul distances from these sources range from 44 to 80 miles, and the material can be transported by truck or railroad. Riprap previously used at Marshall was fieldstone obtained from the

immediate Marshall area. The availability of fieldstone for the proposed project has not, however, been determined.

#### CONCRETE AGGREGATE

73. Concrete aggregate of suitable quality can be furnished in the required quantities from local suppliers.

## STRUCTURAL DESIGN

74. Structural measures included in the proposed improvements include the culvert headwalls, the control weir on the overflow diversion structure, and the gatewell at the outlet of the ponding area drainage conduit. All culvert headwalls would be cast in place and involve minor amounts of reinforcing steel T1 540-foot long overflow weir control device would involve 90 cubic yards of concrete and is designed to withstand overturning or dislodgement at peak discharges as shown on section A-A, plates E-3.

75. The reinforced concrete gatewell would include a 24-inch diameter R C P with a 24-inch by 24-inch flat back sluice gate and a manually operated gate lift system. Other features would include a standardized manhole frame with cover, and safety hand railing. Structural details of the proposed gatewell are shown on plate E-12.

## CONSTRUCTION

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76. Construction of the proposed project could be completed in two construction seasons. Placement of the arch culverts through the Highway 23 embankment would require the restriction and diversion of highway traffic for a two to four-week period. Placement of the collector ditch culverts through County Highway 67 would require traffic control for a few days.

### OPERATION AND MAINTENANCE

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77. Operation and maintenance of the project would include: upkeep of levee and channel slopes, ponding area, and collector ditch; regular mowing of selected levee and overflow channel areas excluding specified ground cover for wildlife habitat; periodic inspection and maintenance of riprap, culvert flap, gates, and drop structure culverts, sediment removal from the roadside park and overflow channel as required; manual operation of the sluice gate at the ponding area outlet as needed; and maintenance of the service roads on the levees. Also included would be the periodic placement of the two temporary sandbag closures as required and maintenance of the recreational facilities. These operation and maintenance measures would be in addition to the present responsibility of maintaining and operating the existing project. The average annual cost of the proposed operation and maintenance is estimated at \$9,000.

## Table H-15 - Laboratory Test Data

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DATE: October 13, 1975

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| Boring<br>No.   | Sample<br>No. | Depth<br>(in Ft)                        | Soil Type                  | Moisture<br>Content<br>(%) | Liquid<br>Limit<br>(%) | Plastic<br>Limit<br>_(%) | Plasticity<br>Index |
|-----------------|---------------|---|----------------------------|----------------------------|------------------------|--------------------------|---------------------|
| 75-2 <b>9</b> M | 4             | 5'-6'                                   | Sandy Clay (CL)            | 17.2                       | 36.1                   | 17.7                     | 18.4                |
| 75-29M          | 5             | 75'-85'                                 | Sandy Clay (CL)            | 17.9                       | 31.0                   | 15.6                     | 15.4                |
| 75-30M          | 8             | 12 <sup>1</sup> 2'-13 <sup>1</sup> 2'   | Silty Clay (CL)            | 26.9                       | 35.2                   | 18.5                     | 16.7                |
| 7 <b>5-30M</b>  | 13            | 25 <sup>1</sup> 3' - 26 <sup>1</sup> 3' | Silty Clay (MH-CL)         | 37.1                       | 53.6                   | 32.5                     | 21.1                |
| 75-31M          | 3             | 2 <sup>1</sup> 5' - 3 <sup>1</sup> 5'   | Clayey Silt (ML-CL)        | 6.2                        | 23.7                   | 19.0                     | 4.7                 |
| 75-31M          | 9             | 20'-21'                                 | Lean Clay (CL)             | 28.1                       | 48.7                   | 20.3                     | 28.4                |
| 75-31M          | 10T           | 21'-23'                                 | Silty Clay (CL)            | 23.3                       | 29.7                   | 13.8                     | 15.9                |
| 75- <b>3</b> 2M | 9             | 20'-21'                                 | Silty Clay (CL)            | 34.4                       | 44.6                   | 20.0                     | 24.6                |
| 75 <b>- 32M</b> | 11T           | 26'-28'                                 | Fat Clay (CH)              | 40.9                       | 59.5                   | 25.9                     | 33.6                |
| 75-33M          | 5             | 7 <sup>1</sup> 2'-8 <sup>1</sup> 2'     | Silty Clay (MH-CL)         | 27.7                       | 55.1                   | 29.7                     | 25.4                |
| 75-33M          | 12            | 25'-26'                                 | Silty Clay (CL)            | 34.8                       | 46.5                   | 20.5                     | 26.0                |
| 75-33M          | 13            | 30'-31'                                 | Silty Clay (CL)            | 21.1                       | 38.1                   | 21.2                     | 16.9                |
| 7 <b>5-35M</b>  | 5             | 10'-11'                                 | Organic Silty<br>Clay (OH) | 64.3                       | 79.7                   | 45.1                     | 34 . 6              |
| 75-35M          | 9T            | 18'-19 <sup>1</sup> 1'                  | Sandy Clay (CL)            | 23.5                       | 38.7                   | 15.7                     | 23 0                |
| 75-35M          | 10            | 20'-21'                                 | Sandy Clay (CL)            | 23.7                       | 36.6                   | 17.6                     | 19.0                |
| 75- <b>35M</b>  | 11            | 25'-26'                                 | Clayey Sand (SC)           | 18.5                       | 25.1                   | 19.9                     | 5.2                 |
| 75-35M          | 12            | 30'-31'                                 | Sandy Clay (CL)            | 18.6                       | 28.5                   | 15.3                     | 13.2                |
| 75-36M          | 7             | 15'-16'                                 | Sandy Clay (CL)            | 19.7                       | 34.6                   | 17.7                     | 16.9                |
| 75-38M          | 5             | 713'-812'                               | Sandy Clay (CL)            | 21.1                       | 30.4                   | 17.9                     | 12.5                |
| 75-38M          | 10            | 15'-16'                                 | Sandy Clay (CL)            | 17.6                       | 30.5                   | 16.4                     | 14.1                |
| 75-38M          | 11            | 15-16                                   | Sandy Clay (CL)            | 15.4                       | 26.9                   | 14.8                     | 12.1                |
| 75- <b>39M</b>  | 8T            | 16'-18'                                 | Sandy Clay (CL)            | 16.8                       | 27.9                   | 15.5                     | 12.4                |
| 75-40M          | 2             | 212' - 312'                             | Medium Fat Clay (CH)       | 22.6                       | 55.3                   | 22.7                     | 32.6                |
| /5-40M          | 3             | 51-61                                   | Medium Fat Clay<br>(CL-CH) | 30.2                       | 46.5                   | 22.5                     | 24.0                |
| 5-40M           | ST            | 6' - 7 <b>i</b> s'                      | Sandy Clay (CL)            | 20.6                       | 28.7                   | 17.0                     | 11.7                |
| /5-40M          | 7             | 10'-11'                                 | Sandy Clay (CL)            | 30.7                       | <b>39</b> .0           | 20.5                     | 18.5                |
| 5-40M           | 8             | 125'-135                                | Sandy Clay (CL)            | 16.8                       | 24.6                   | 15.9                     | 8.7                 |
| 5-40M           | 10            | 20'-21'                                 | Sandy Clay (CL)            | 17.7                       | 27.6                   | 15.7                     | 11 9                |
| /5-41M          | 3             | 5'-6'                                   | Sandy Clay (CL)            | 19.2                       | 34.9                   | 17.6                     | 17.3                |

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PROJECT: REDWOOD RIVER - MARSHALL, MY

Table H-16. Sieve Analysis Tests

DATE: October 13, 1975

JOB NO. #21791

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| Boring No.                             | 75-29M             | 75-30N                           | 75-30M                | 75-31M                           | 75-31M | 75-31M  | 75-31M                        | 75-31M   | 75-211  |     |
|--|--------------------|----------------------------------|-----------------------|----------------------------------|--------|---|-------------------------------|--|---------|-----|
| Semple No.                             | ŝ                  | M                                | 14                    | 4                                | ŝ      | ور  | t<br>t                        | 5<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | nuc-c/  |     |
| _                                      | 24, - 34,          | 51-61                            | 30'-31'               | 5'-6'                            | 7484.  | .1101   | 12-, '-134,'                  | 15'-16'  | 25'-26' |     |
| Soil Type<br>Meight ôf<br>Total Semple | Silty Sand<br>(SM) | Sand, fine<br>grained<br>(SP-SM) | Sandy Silt<br>(ML-SN) | Sand, fine<br>grained<br>(SP-SN) |        | Silty Sand Sand, fine<br>(SM) grained<br>(SP) | Sand, fine<br>grained<br>(SP) | and,<br>edium<br>rained  | SP),    | (SP |
| (Grams)<br>Besed on Total              | 106                | 131                              | 102                   | 137                              | 104    | 133   | 216                           | 173  | 201     |     |
| Sample, § finer<br>than 1"             | 100                | 100                              | 100                   | 100                              | 100    | 100   | 100                           | 100  | 100     |     |
| 3/8"                                   | 100                | 100                              | 100                   | 100                              | 100    | 100   | 100                           | 97.7   | 100     |     |
| 2                                      | 100                | 100                              | 100                   | 100                              | 100    | 100   | 100                           | 92.6   | 92.2    |     |
| 01#                                    | 100                | 100                              | 100                   | 100                              | 100    | 100   | 100                           | 79.3   | 69.C    |     |
| 440                                    | <b>59</b> . 3      | 98.6                             | 99.5                  | - 68                             | 97.5   | 87.2  | 64.9                          | 22.3   | 44.5    |     |
| 0014                                   | 62.8               | 37.7                             | 88.9                  | 33.2                             | 54.0   | 13.6  | 6.8                           | 5.0  | 9.3     |     |
| \$ 200                                 | 34.1               | 14.4*                            | 59.5*                 | 13.6*                            | 38.0   | 6.3*  | 2.6                           | 3.2  | 5       |     |

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Percentage of fines influenced by lenses

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PROJECT: REDNOOD RIVER - MARSHALL, AN

JOB NO. #21791

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Table H-16 . Sieve Analysis Tests (continued)

| 12<br>30'-31'<br>fine<br>fine<br>(SP)<br>(SP)<br>100<br>100<br>100<br>100<br>5.7<br>68.6<br>90.5<br>3.7<br>68.6<br>5.7<br>5.7   | BOTING No.                    | 75-31M                             | 75-32N | 75-32''         | 75-324                             | 75-33M  | 75-33M                             | 75-34M   | 75- 24M                          | 76 JEN                                  |
|---|-------------------------------|------------------------------------|--------|-----------------|------------------------------------|---|------------------------------------|--|----------------------------------|---|
| 30'-31'         24'-44'         5'-6'         74'-64'         124'-134'         15'-16'         25'-26'         30'-31'           Stard,<br>medium         Sand,<br>medium         Sand,<br>medium         Sand,<br>medium         Sand,<br>medium         Sand,<br>fine to         Sand,<br>fine         Sand,<br>sand,<br>(SP)         Sand,<br>sand,<br>grained         Sand,<br>medium         Sand,<br>medium         Sand,<br>sand,<br>grained         Sand,<br>sand,<br>grained         Sand,<br>sand,<br>grained         Sand,<br>sand,<br>grained         Sand,<br>grained         Sand,<br>graine         Sand,<br>grained         Sand,<br>graine </td <td>ple No.</td> <td>13</td> <td>ħ</td> <td>4</td> <td>ın</td> <td>0</td> <td>10</td> <td>11</td> <td>12</td> <td><b>H</b>20-0/</td>   | ple No.                       | 13                                 | ħ      | 4               | ın                                 | 0   | 10                                 | 11   | 12                               | <b>H</b> 20-0/                          |
| Sand,<br>Band,<br>Feriture         Sand,<br>Sand,<br>Feriture         Sand,<br>Sand,<br>Feriture         Sand,<br>Sand,<br>Feriture         Sand,<br>Sand,<br>Feriture         Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>Sand,<br>San | th (ft)                       | 30'-31'                            |        | 5 <b>1</b> - 6° | 74 <b>5 - 8</b> 45 -               | 124-134   | 15'-16'                            | 25'-26'  | <b>30'-</b> 31'                  | 41£'                                    |
| 263     175     183     270     243     245     188     273       100     100     100     100     100     100     100     100       97.8     89.5     87.5     84.5     72.7     100     100     100       97.8     89.5     87.5     84.5     72.7     100     100     100       97.8     89.5     87.5     84.5     72.7     100     100       97.8     89.5     87.5     84.5     72.7     100     100       96.3     79.0     79.2     84.5     72.7     100     100       86.3     79.0     79.2     84.5     72.7     100     100       86.3     79.0     79.5     89.5     92.6     90.5       61.6     67.1     70.7     53.6     54.6     98.9     90.5       16.5     34.2     40.8     15.7     15.0     28.7     59.0     68.6       4.5     11.1     18.6     4.1     4.5     2.3     12.8     3.7       3.7     6.8     10.4     3.1     1.2     8.6     2.2  | l Type<br>pht of<br>al Sample | Sand,<br>Mecium<br>grained<br>(SP) |        |                 | Sand,<br>medium<br>grained<br>(SP) | Sand,<br>medium<br>to coarse<br>grained<br>(SP) | Sand,<br>medium<br>grained<br>(SP) | Sand,<br>fine to<br>medium<br>grained<br>(SP-SN) | Sand,<br>fine<br>grained<br>(SP) | Fill, Silty<br>Sand and<br>sand mixture |
| 100       100       100       100       100       100       100       100       100       100         97.8       89.5       87.5       84.5       72.7       100       100       100       100         97.8       89.5       87.5       84.5       72.7       100       100       100       100         96.3       79.0       79.2       69.6       52.1       98.6       98.9       99.8         61.6       67.1       70.7       53.5       34.6       89.5       95.9       90.5         16.5       34.2       40.9       15.7       15.0       28.7       59.0       68.6         4 5       11.1       18.6       4.1       4.5       2.3       12.8       3.7         3.7       6.8       10.4       3.1       3.1       1.2       8.6       2.2   |                               | 263                                | 175    | 183             | 270                                | 243   |                                    | 981  | ***                              | 1                                       |
| 100         100 <td>l sample,<br/>ner than</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>   | l sample,<br>ner than         |                                    |        |                 |                                    |   |                                    |  |                                  |   |
| "       97.8       89.5       87.5       84.5       72.7       100       10.2       23.5       34.6       89.5       99.6       99.8       90.5         16.5       34.2       40.9       15.7       53.6       34.6       89.5       59.0       68.6       68.6       6       6       5.7       59.0       68.6       5.7       55.0       58.7       59.0       58.7       55.0       58.6       5.7       57.7   | .,                            |                                    | 100    | 100             | 100                                | 88.7  | 100                                |  | uur                              |   |
| 86.3       79.0       79.2       69.5       52.1       98.6       98.9       99.8         61.6       67.1       70.7       53.5       34.6       89.5       98.6       99.8         16.5       34.2       40.8       15.7       53.5       15.0       28.7       59.0       66.6         45       34.2       40.8       15.7       15.0       28.7       59.0       66.6         45       11.1       18.6       4.1       4.5       2.3       12.8       3.7         3.7       6.8       10.4       3.1       3.1       1.2       8.6       2.2   | 3/8"                          | 97.8                               | 89.5   | 87.5            | 84.5                               | 72.7  | 001                                |  |                                  | 100                                     |
| 61.6 67.1 70.7 53.5 34.6 89.5 98.9 99.8<br>16.5 34.2 40.9 15.5 15.0 28.7 59.0 68.6<br>4.1 4.5 2.3 12.8 3.7<br>3.2 6.8 10.4 3.7 3.1 1.2 8.6 2.2  | 54                            | 86.3                               | 79.0   | 8°.64           | 9 <b>b</b> y                       |   |                                    | 100  | 001                              | 100                                     |
| 16.5     34.2     40.9     15.7     15.0     38.7     99.5       4     1     18.6     4.1     4.5     2.3     12.8     3.7       3.2     6.8     10.4     3.1     3.1     1.2     8.6     2.2   | 010                           | 61.6                               | 67.1   | 70.7            | 2 <b>2</b> 2                       | 1.10  | 48. h                              | 98.9   | 8.66                             | 99.5                                    |
| 4 5     11.1     18.6     4.1     4.5     2.3     12.8     3.7       3.2     6.8     10.4     3.7     3.1     1.2     8.6     2.2   | 40                            | 16.5                               | 34.2   | 40.9            | 15.9                               | 0.#C  | 25.50<br>28.7                      | 95,9   | 5.09                             | 99.4                                    |
| 3.2 6.8 10.4 3.7 3.1 1.2 8.6 2.2  | 00                            |                                    | 11.1   | 18.6            | 4.1                                | 4.5   | 2.3                                | 12.8   | <b>68</b> .6<br>3.7              | 96.3<br>67 7                            |
|   | 8                             | 14<br>12                           | 6.8    | 10. ¢           | 3.)                                | 3.1   | 1.2                                | 8.6  | 2.2                              | 41.3                                    |

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PROJECT: REDWOOD RIVER - MARSHALL, MN

JOB NO. #21791

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Table H-16. Sieve Analysis Tests (continued)

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| boring iv.                                | 75-33:.             | 75-3SM  | 75-3SM                              | 75-3 <b>SM</b>                                  | 75 <b>-35</b> M       | 75-3 <b>6</b> M                     | 75-36M                             | 75-36M   | 75-36M                                |
|---|---------------------|---|-------------------------------------|---|-----------------------|-------------------------------------|------------------------------------|--|---------------------------------------|
| Sample No.                                | 2                   | ۶   | -                                   | Q   | 7                     | 2                                   | £                                  | 4  | σι                                    |
| Bupth (ft)                                | 24, - 34,           | <b>5</b> ' - 6'                                 | 74 <b>- 8</b> 4                     | 124-134   | 15'-16'               | 241-341                             | 5'-6'                              |  | 25'-26'                               |
| Soil Type<br>Maisht of                    | Clayey<br>sand (SC) | Sand,<br>medium to<br>fine grain-<br>ed (SP-SN) | Sand,<br>fine<br>grained<br>(SP-SM) | Sand,<br>Medium to<br>coarse<br>grained<br>(SP) | Silty<br>sand<br>(SM) | Sand,<br>fine<br>grained<br>(SP-SM) | Sand,<br>medium<br>grained<br>(SP) | Sand,<br>medium to<br>coarse<br>grained<br>fsp | Sand,<br>coarse<br>grained<br>(SP-SM) |
| Total Sample<br>(Grans)                   | 111                 | 84  | 7                                   | 264   | 126                   | 101                                 | 220                                | 243  | 269                                   |
| Bised on<br>Total Sample,<br>A finer than |                     |   |                                     |   |                       |                                     |                                    |  |                                       |
| 1.  | 100                 | 100   | 100                                 | <b>10</b> ن                                     | 100                   | 100                                 | 100                                | 100  | 100                                   |
| 3/8"                                      | 100                 | 100   | 100                                 | 95.3  | 100                   | 100                                 | 67.7                               | 80.7   | 75.5                                  |
| 2   | <b>50</b> .6        | 96. 5   | 5. 7                                | 79.0  |                       | 8.66                                | 54.4                               | 61.7   | 59.8                                  |
| 010                                       | <b>99</b> .2        | <b>86</b> .5                                    | 98.2                                | 54 . 1  |                       | 96.7                                | 42.0                               | 43.9   | 40.2                                  |
| 940                                       | 97.5                |   | 94.9                                | 7.0   | 98.6                  | 85.5                                | 33.4                               | 20.6   | 21.6                                  |
| 901.                                      | <b>5</b> 7.0        | 29.5  | 34.9                                | 4   | 61.1                  | 40.2                                | 6.6                                | 4.5  | 8.1                                   |
| 5021                                      | 39.1                | 16.9*   | 22.8.                               | 3.2   | 39.0                  | 22.7*                               | 3.7                                | 2.8  | 6.7                                   |
|   |                     |   |                                     |   |                       |                                     |                                    |  |                                       |

· Percentage of fines influenced by lenses

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PROJECT: REDNOOD RIVER - MANSHALL, NN

JOB NO. #21791

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Table H-16 Sieve Analysis Tests (continued)

| PULTING NO.                            | 75-36M                                       | 75-3 <b>9N</b>        | 75-41M                        | 75-41M                           | 75-41M                     | 75-4 2M                    |
|--|--|-----------------------|-------------------------------|----------------------------------|----------------------------|----------------------------|
| Sample No.                             | 10   | S                     | S                             | Ŷ                                | 7                          | 10                         |
| Depth (ft)                             | 30'- 31'                                     | 1111                  | 10'-11'                       | 124'-134'                        | 15'-16'                    | 15'-16'                    |
| Soil Type<br>Weight of<br>Total Sample | Sand, coarse<br>to medium grained<br>(SP-SW) | Sandy Clay<br>(CL-SC) | Sand, fine<br>grained (SP-SM) | Sand, fine<br>grained<br>(SP-SM) | Sand, fine<br>grained (SP) | Sand, fine<br>grained (SP) |
| (Grans)                                | 184  | 102                   | 116                           | 175                              | 180                        | 126                        |
| Based on Total<br>Sample, % finer      |  |                       |                               |                                  |                            | 2                          |
| than 1"                                | 100  | 100                   | 100                           | 100                              | 100                        | 100                        |
| 3/8"                                   | 90.5   | 100                   | 100                           | 98.5                             | 99.4                       | 87.4                       |
| :                                      | 71.3   | 99.3                  | 99.4                          | 91.9                             | 98.3                       | 85.9                       |
| #10                                    | 46.5   | 95.7                  | 0.86                          | 82.9                             | 96.3                       | 80.2                       |
| <b>14</b> 0                            | 11.2   | 91.4                  | 87.9                          | 76.8                             | 87.1                       | 72.2                       |
| .100                                   | 7.1  | 64.8                  | 17.9                          | 13.5                             | 17.6                       | 14.3                       |
| \$200                                  | 5.5  | 52.9                  | 7.S                           | <b>6</b> .5                      | 8.6*                       | 5.3                        |

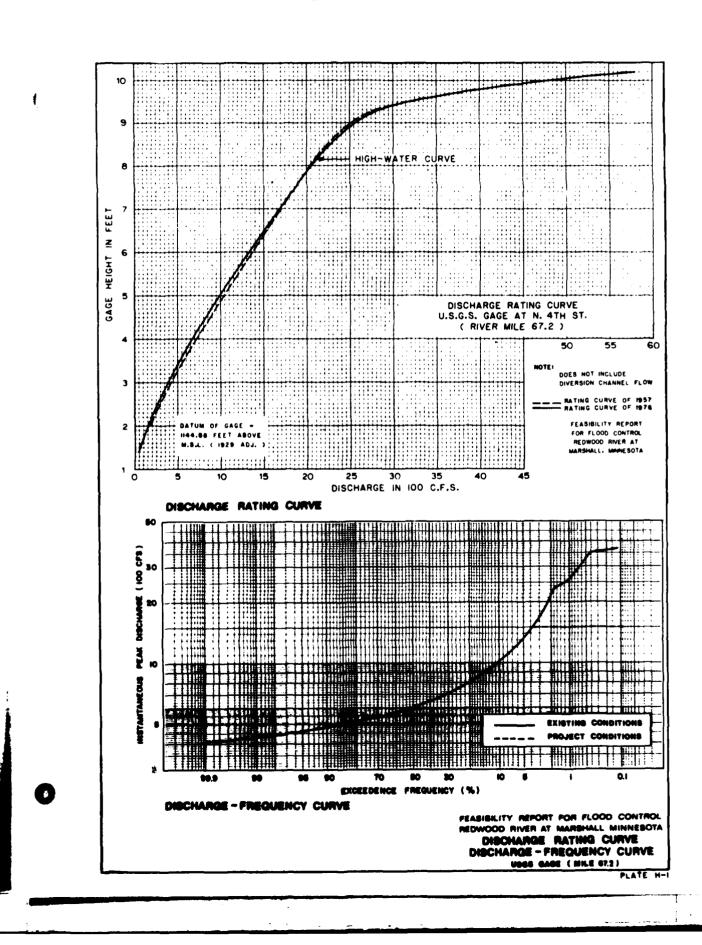
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· Percentage of fines influenced by lenses

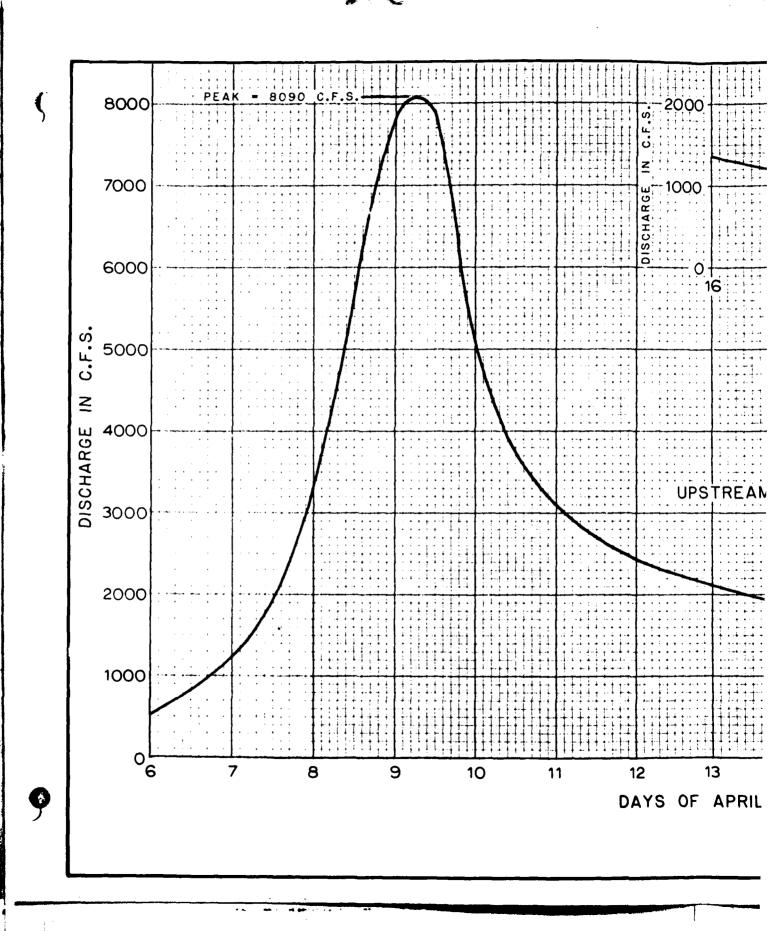
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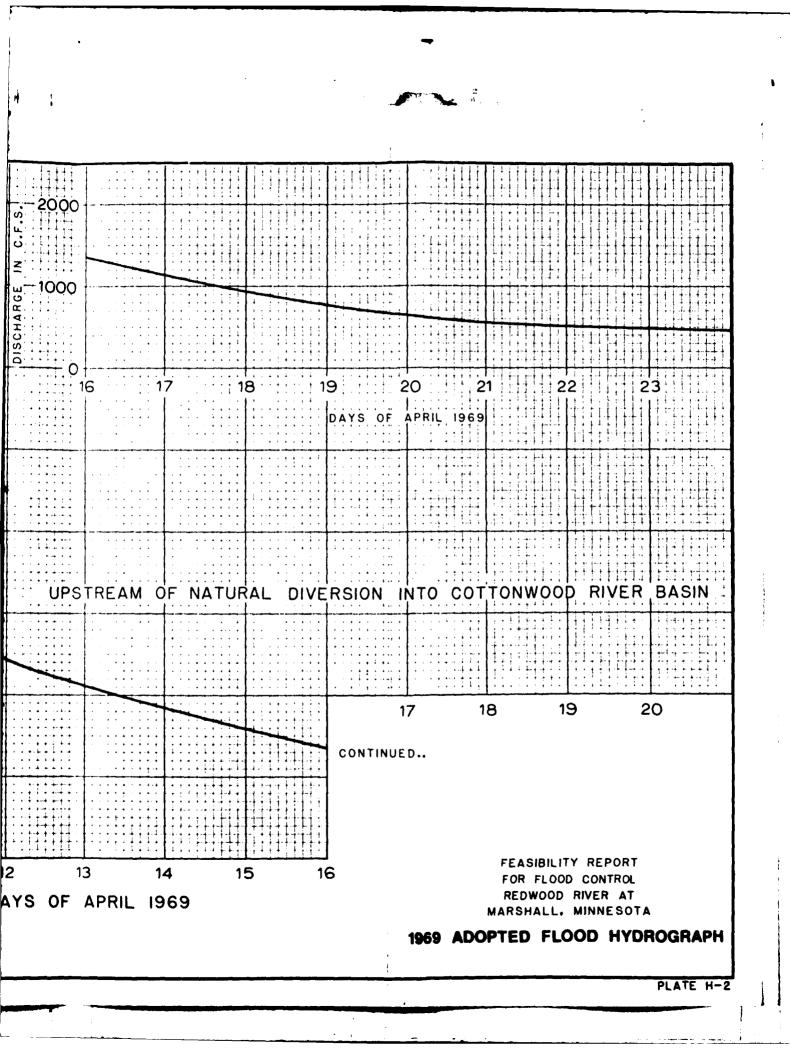
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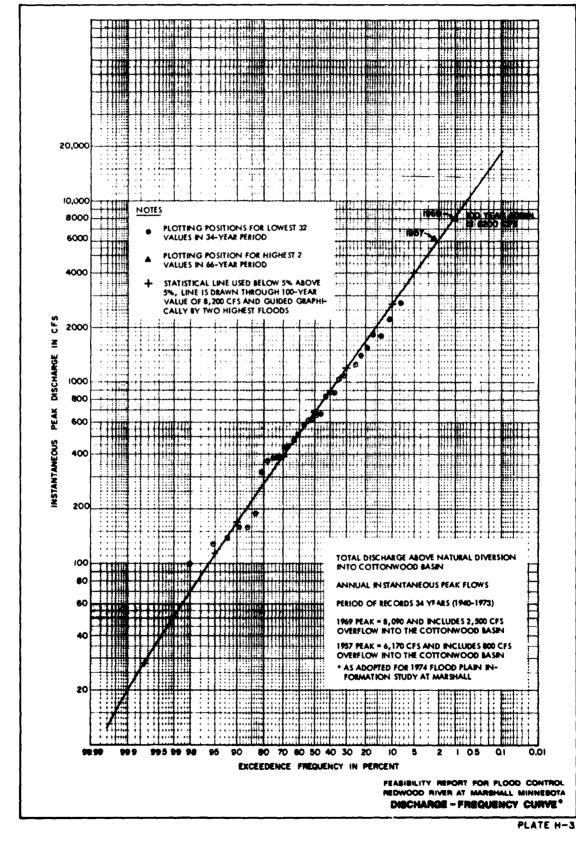


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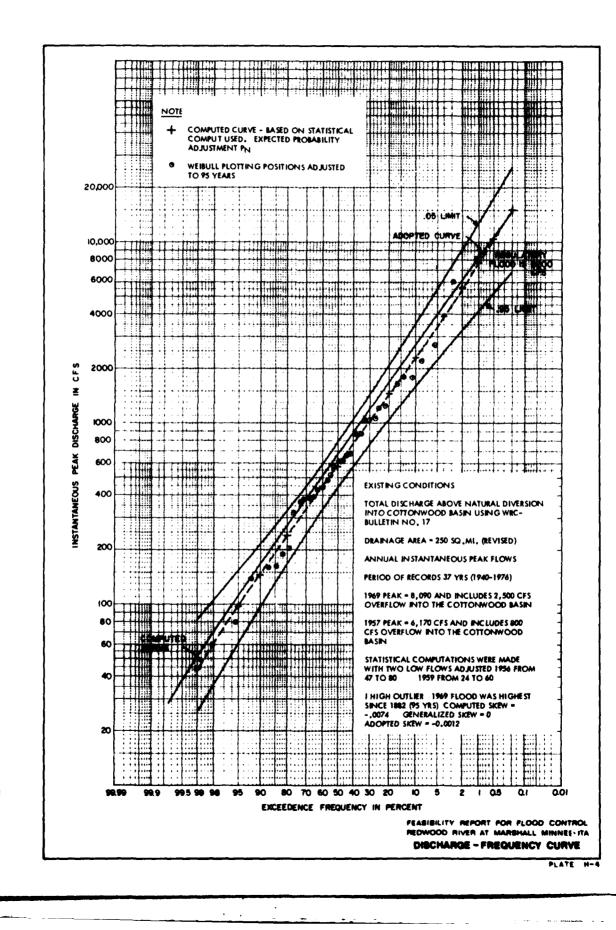




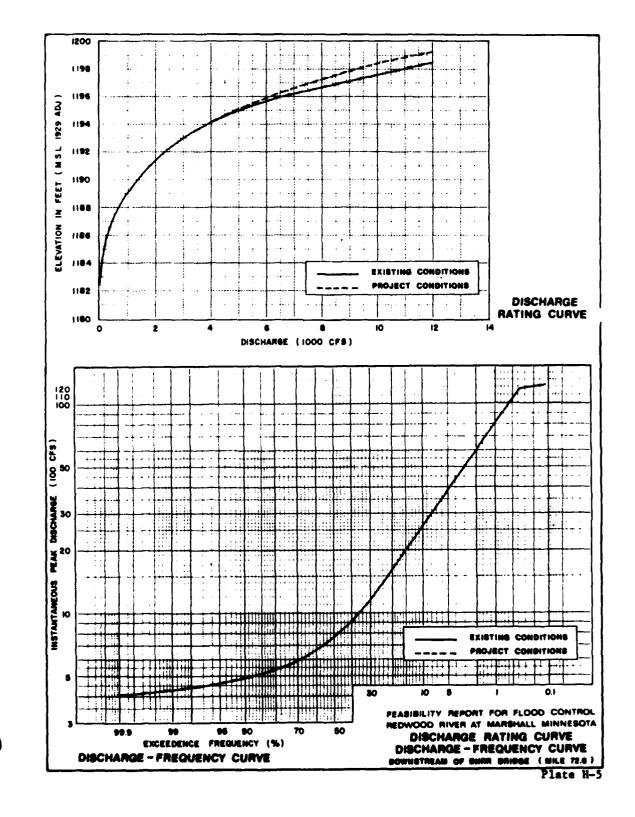
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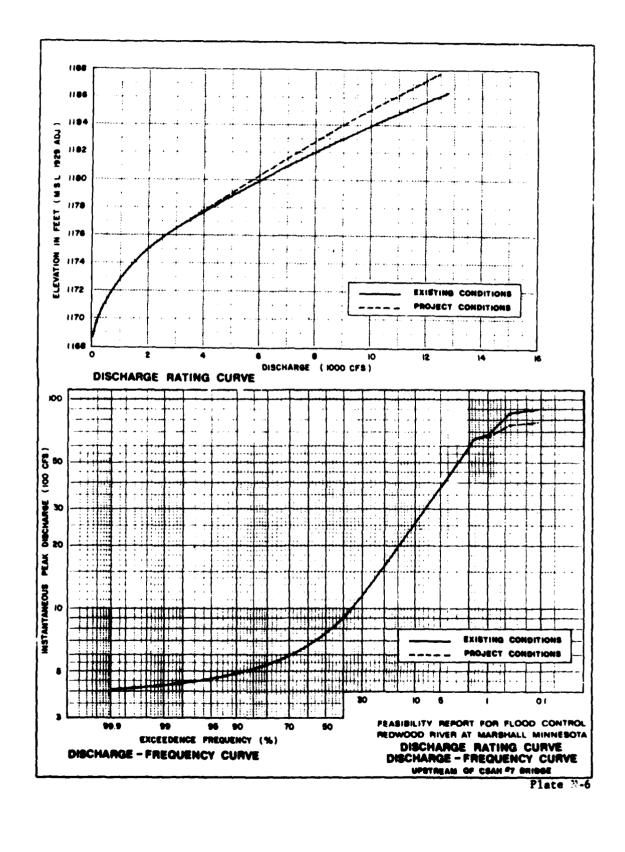


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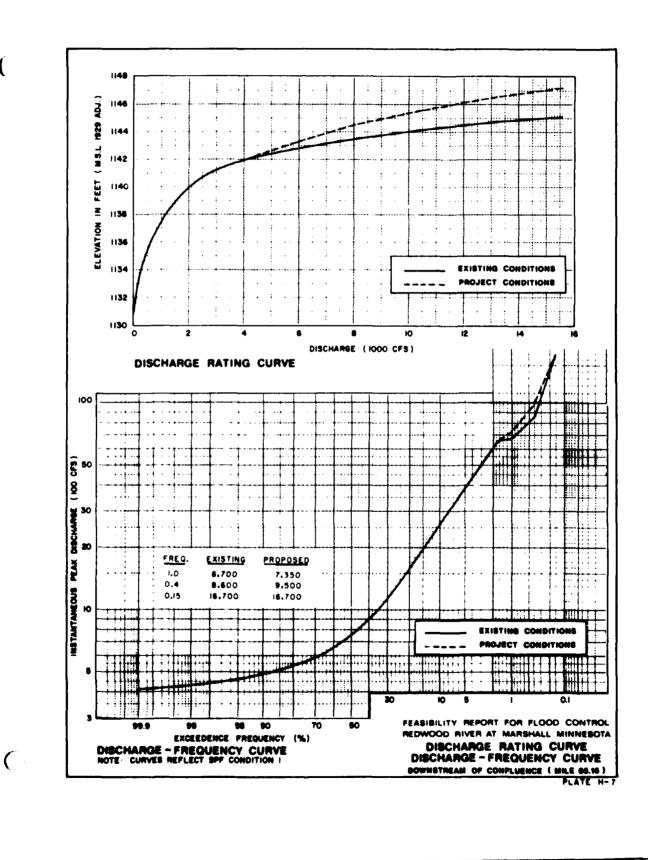


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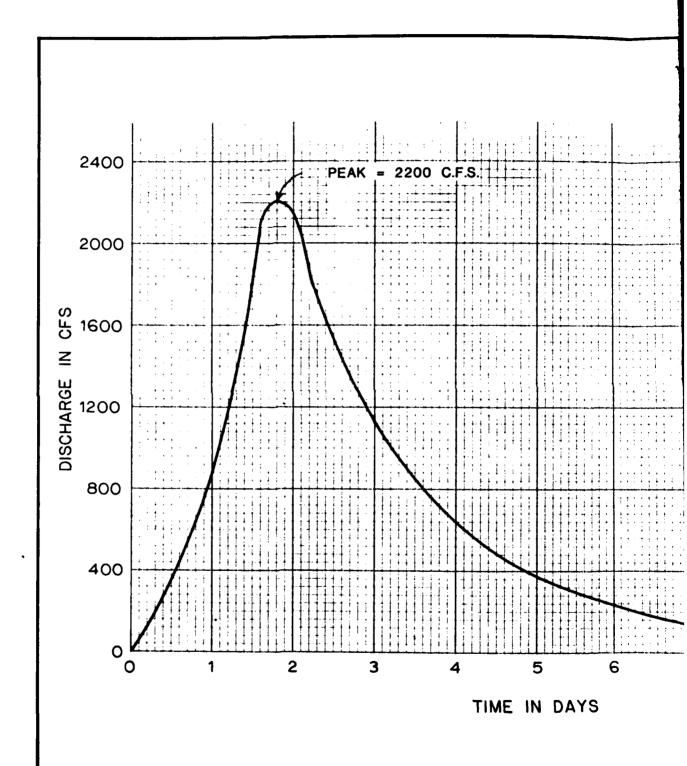
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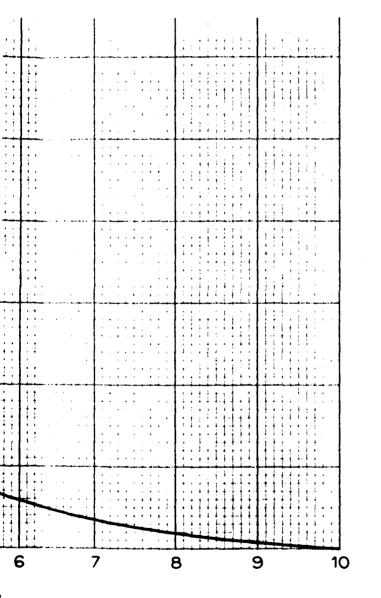
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PLATE H-P

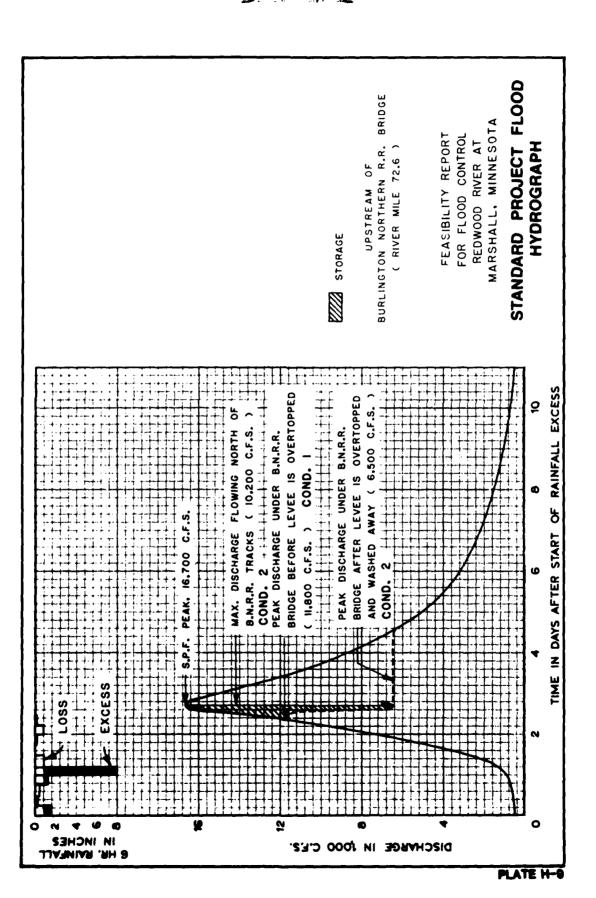
## 6-HOUR UNIT HYDROGRAPH

FEASIBILITY REPORT FOR FLOOD CONTROL REDWOOD RIVER AT MARSHALL, MINNESOTA



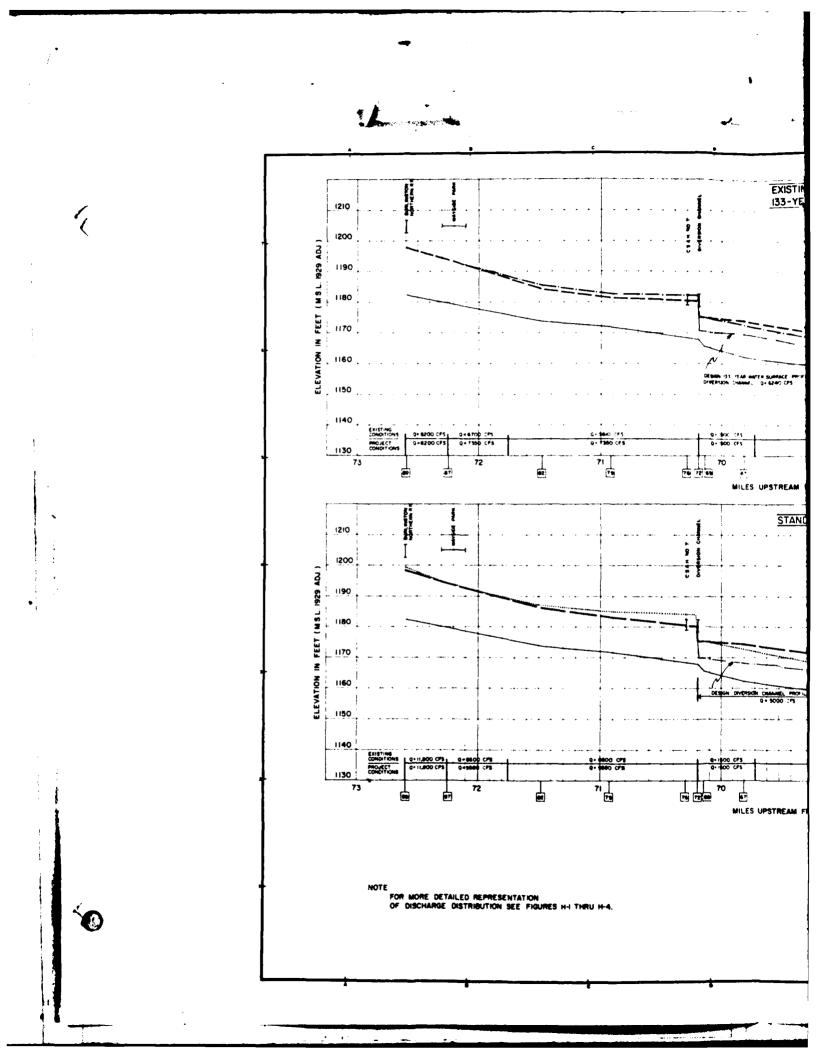
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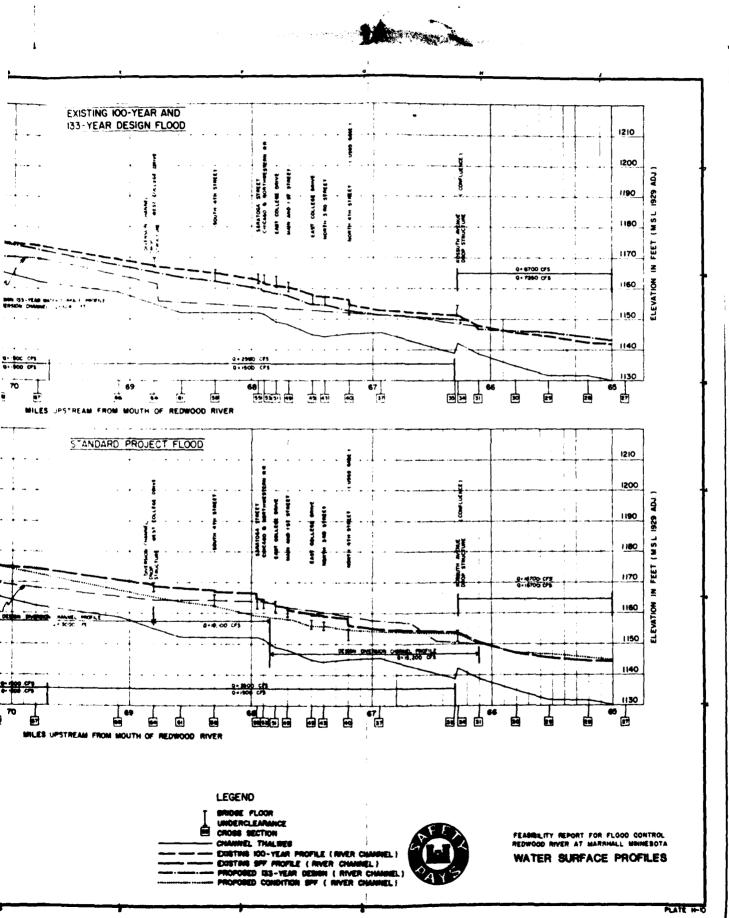
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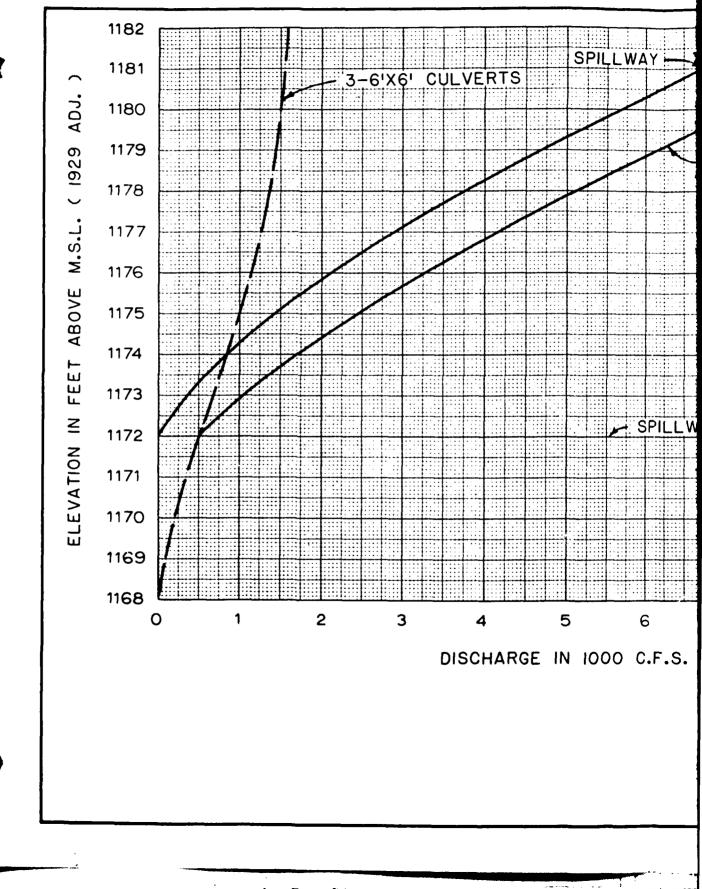
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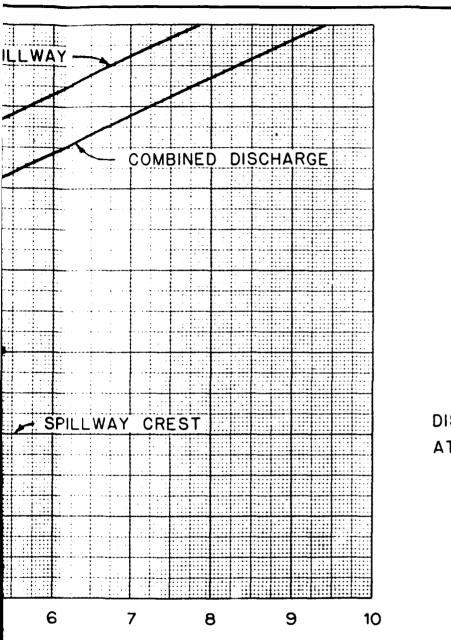




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DISCHARGE RATING CURVE AT DIVERSION STRUCTURE ( RIVER MILE 70.2 )

> FEASIBILITY REPORT FOR FLOOD CONTROL REDWOOD RIVER AT MARSHALL, MINNESOTA

## DISCHARGE RATING CURVE



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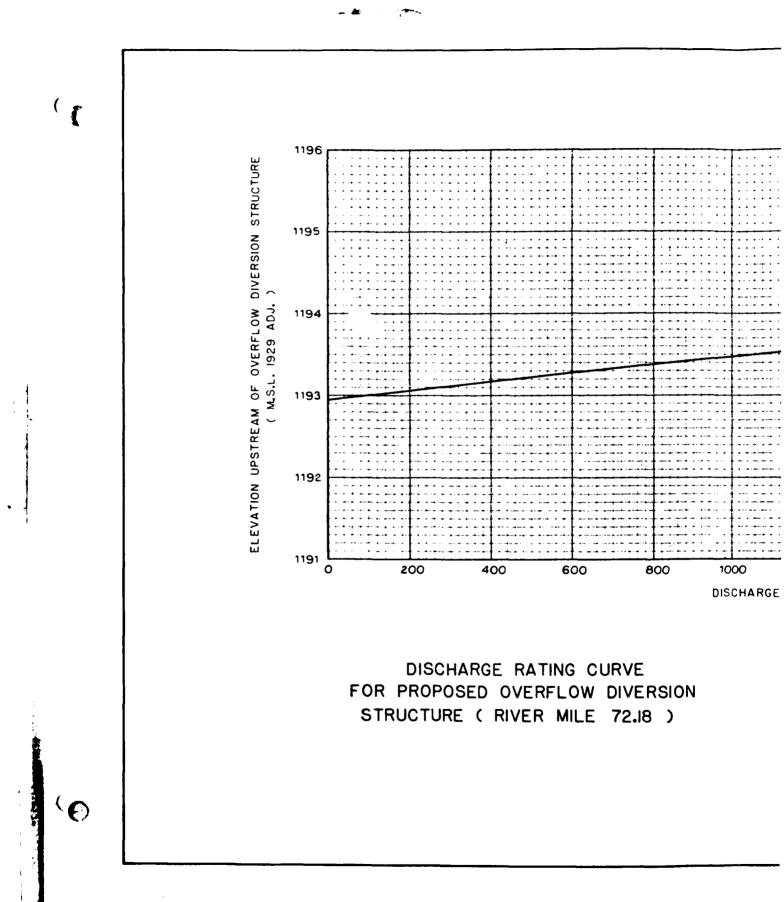


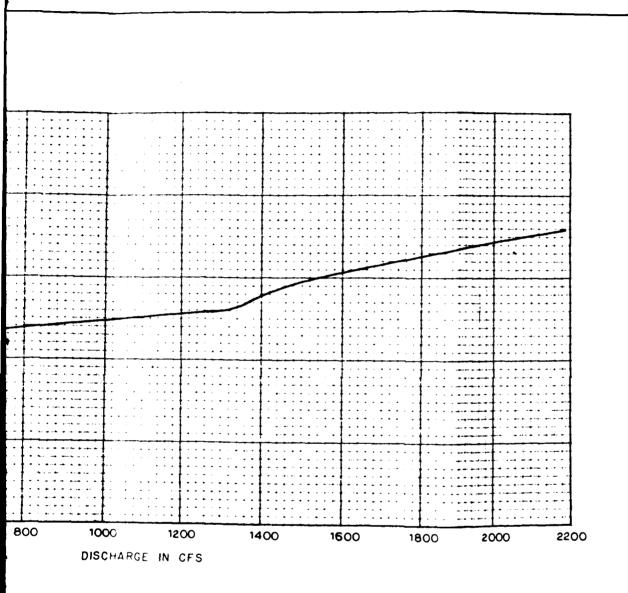
PLATE H-12

## MARSHALL, MINNESOTA DISCHARGE RATING CURVE

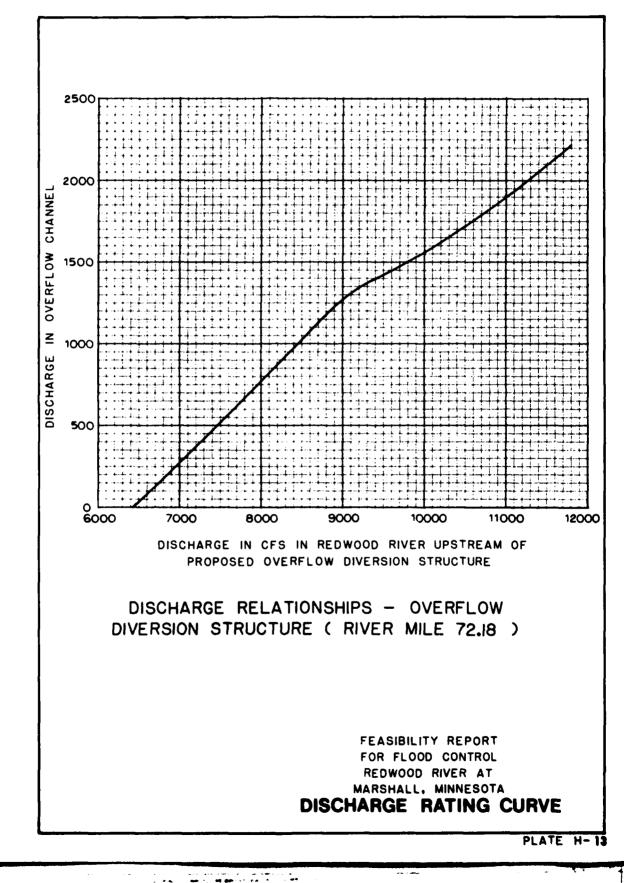
FEASIBILITY REPORT FOR FLOOD CONTROL REDWOOD RIVER AT

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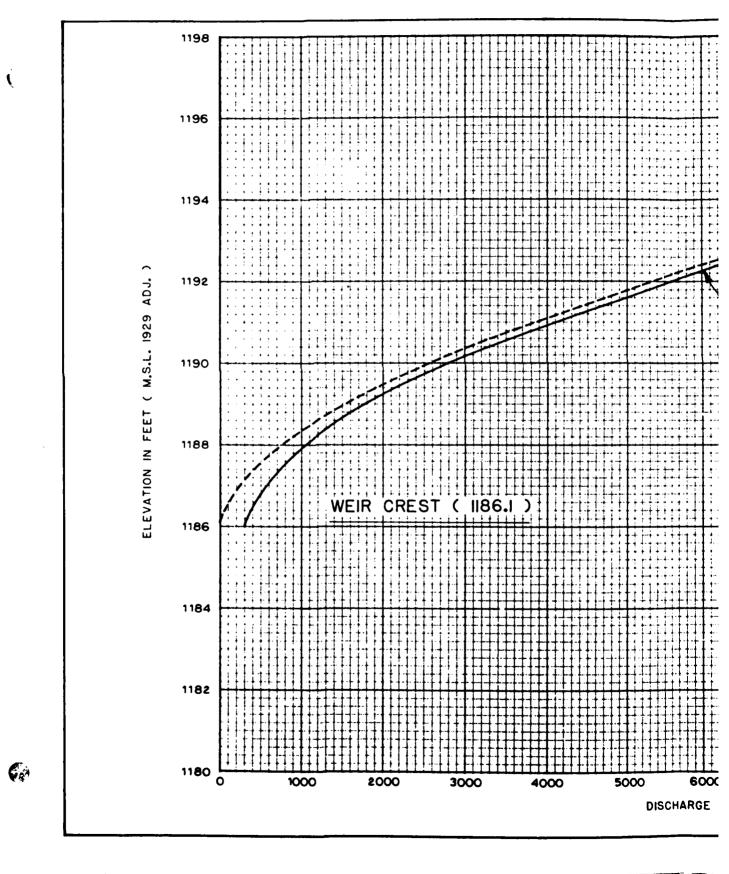




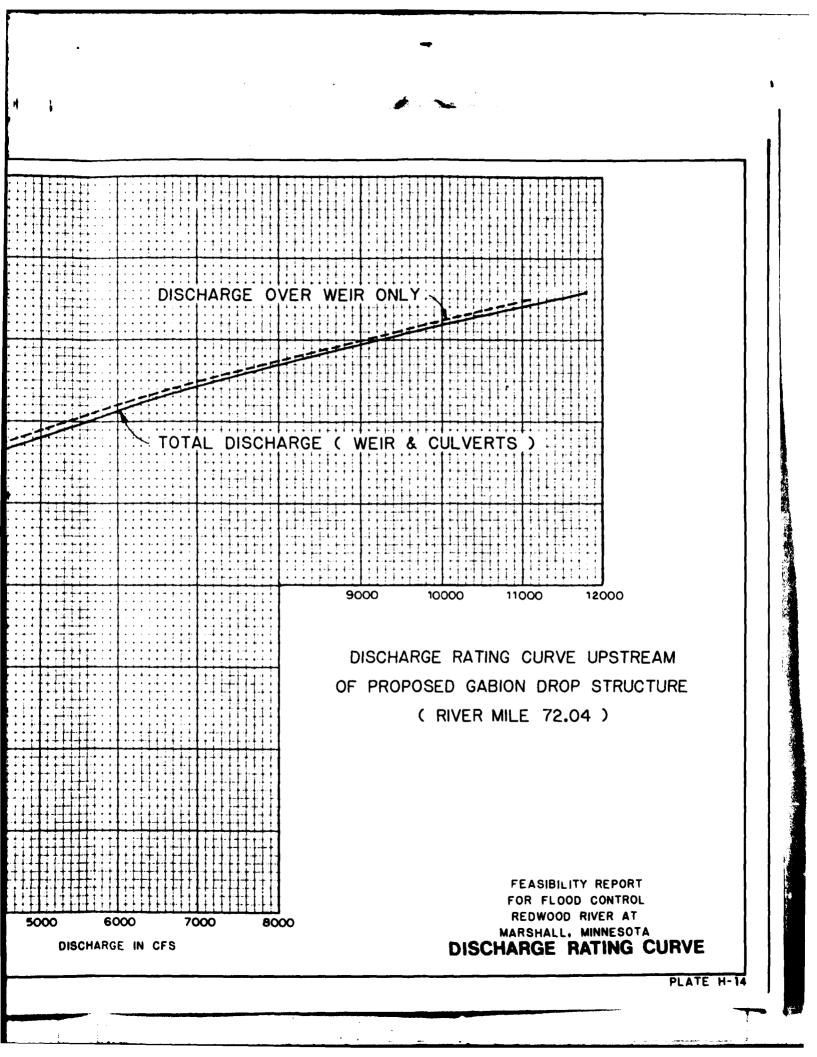
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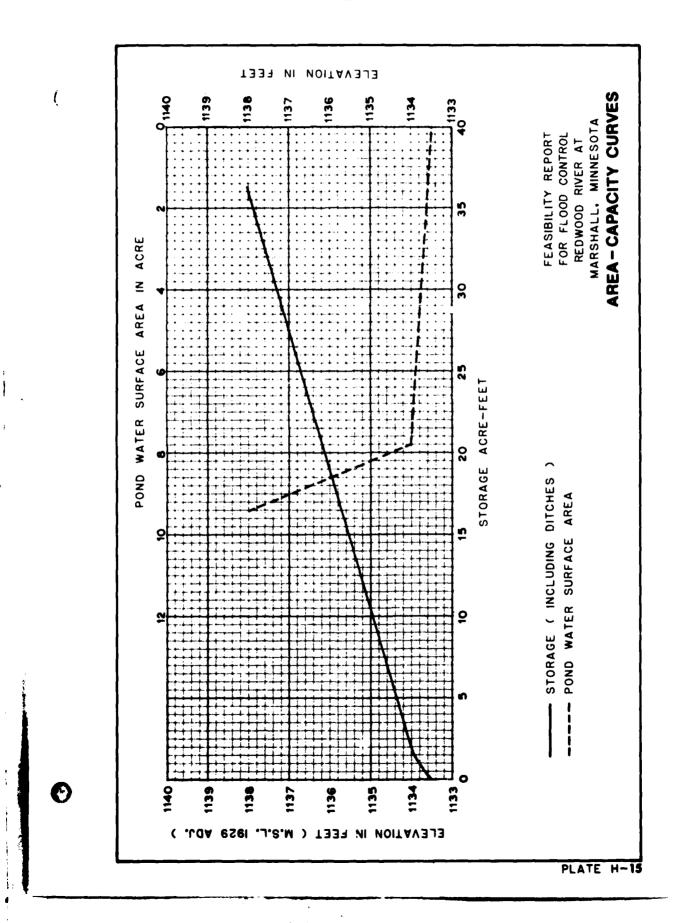
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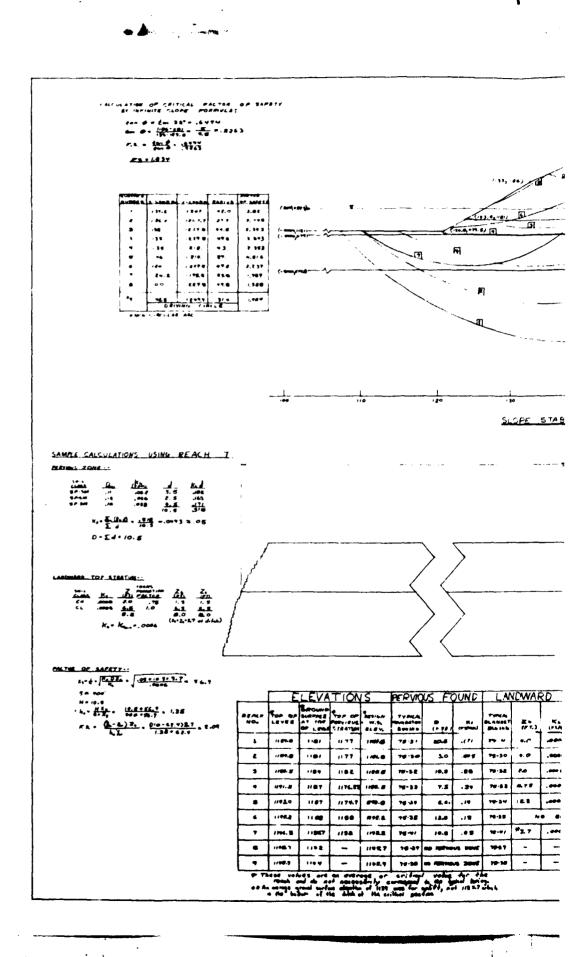


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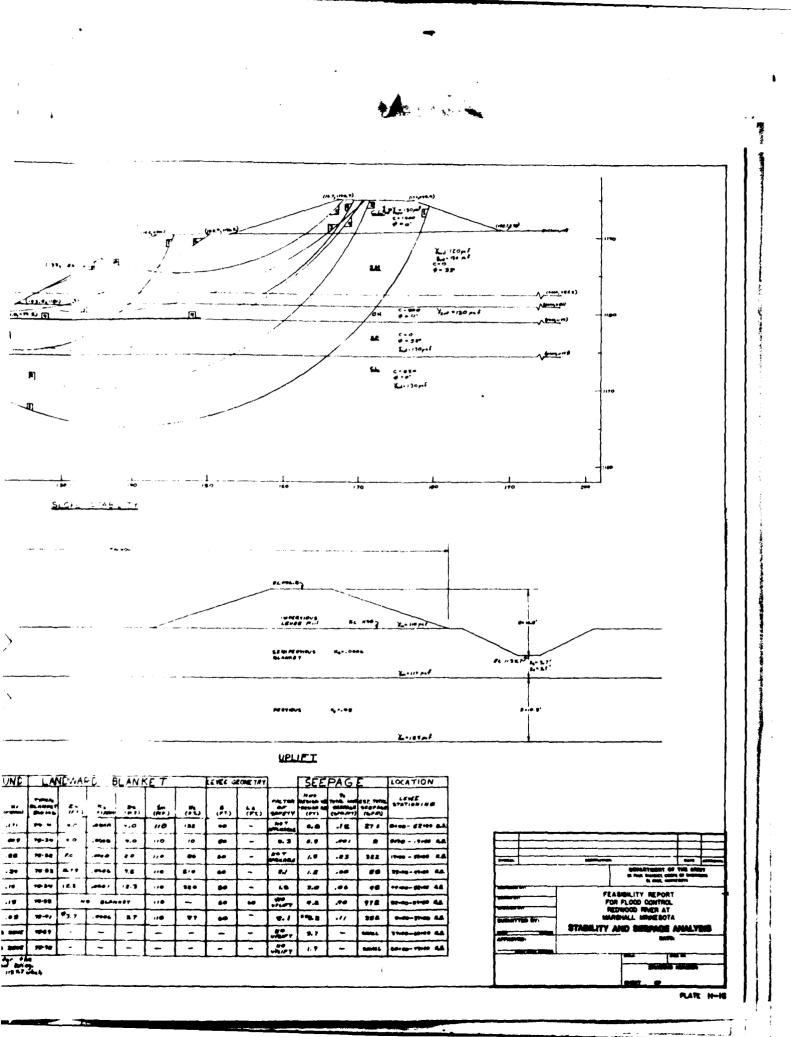
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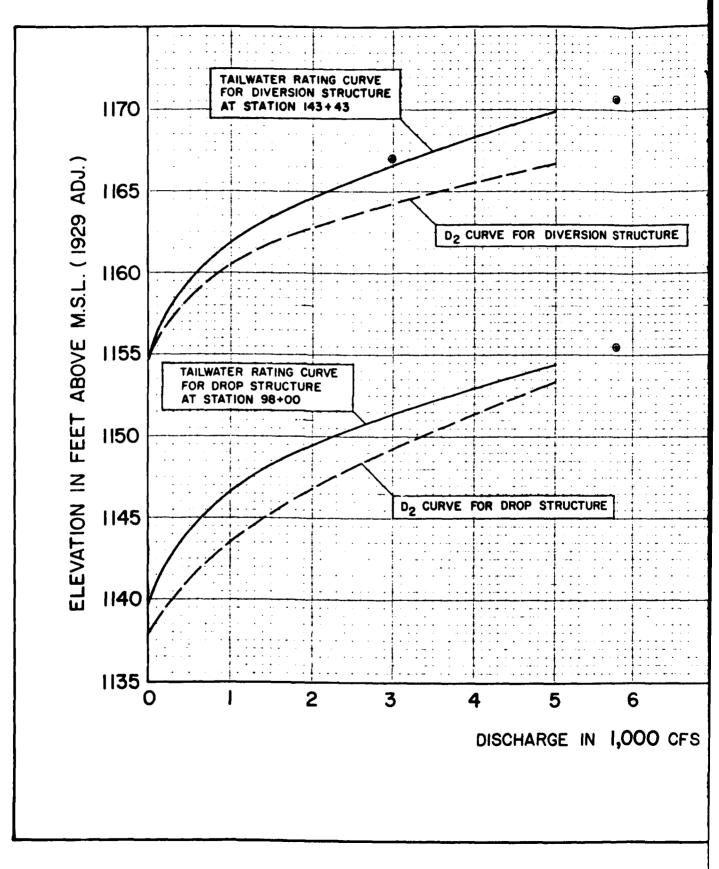
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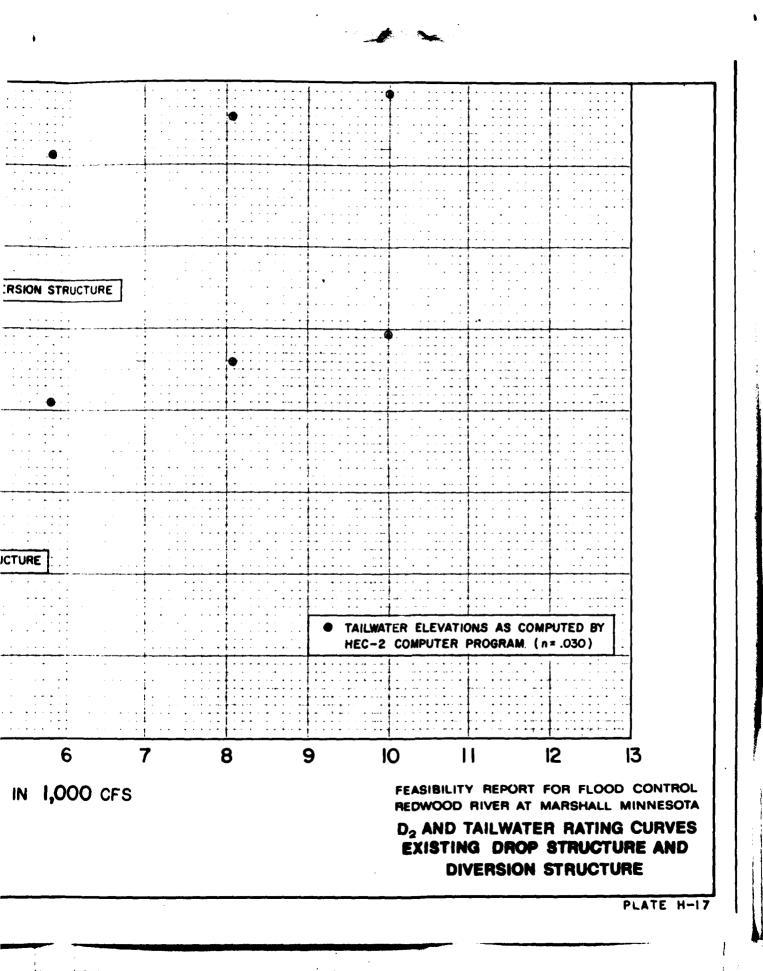


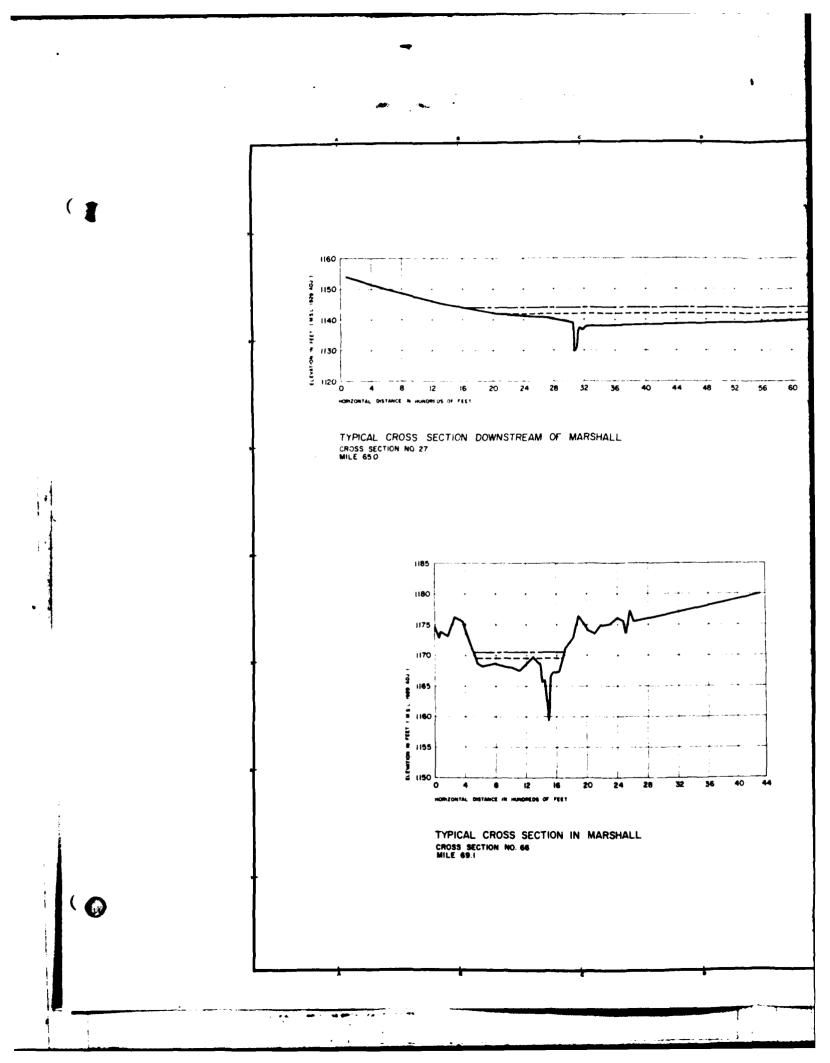
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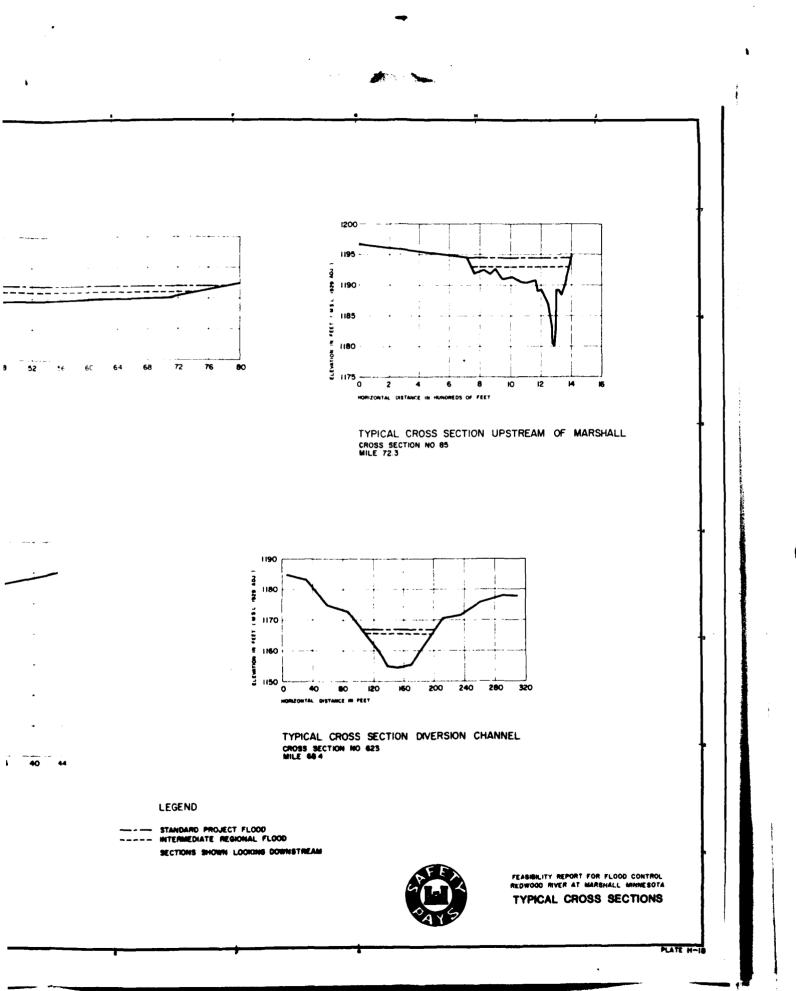


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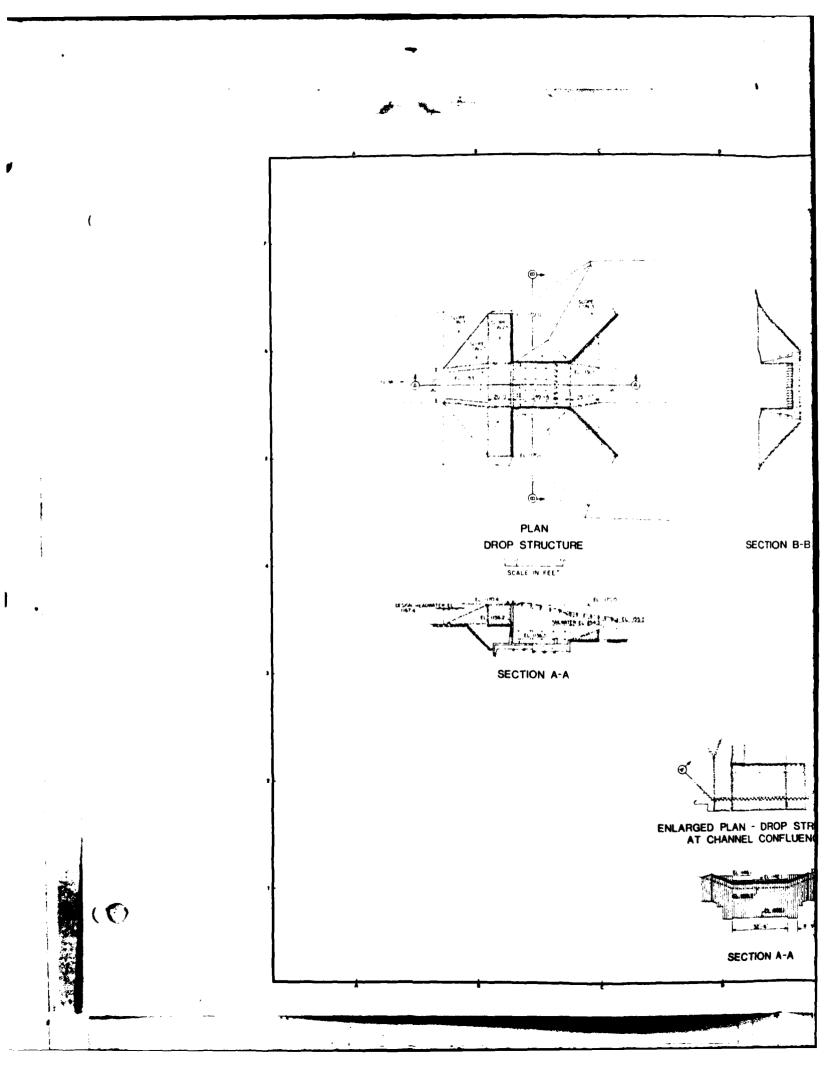


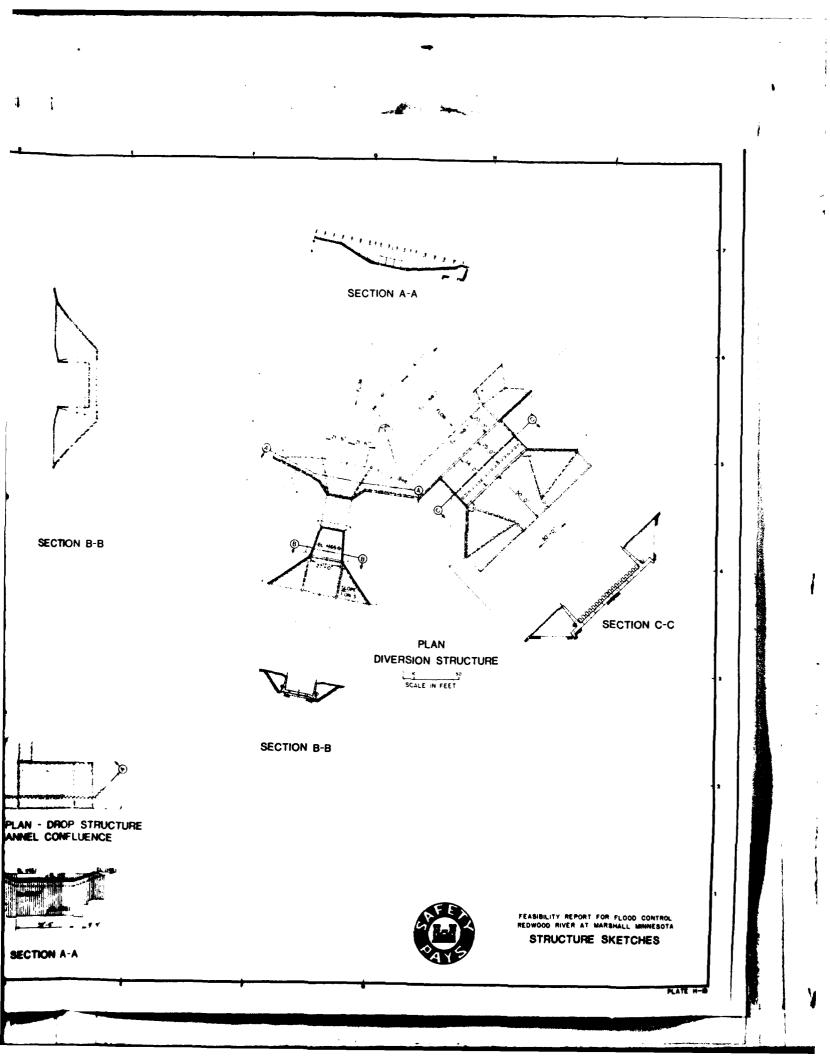




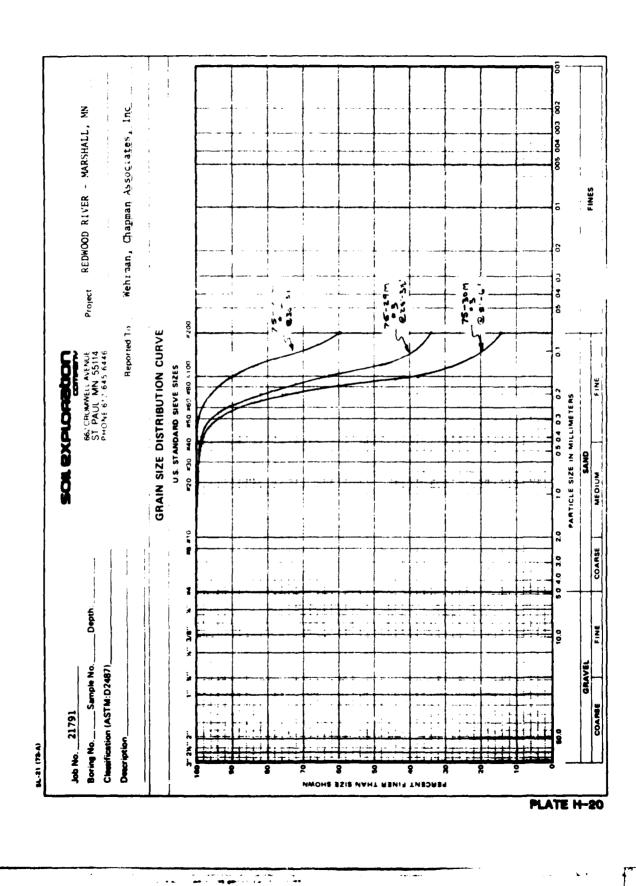
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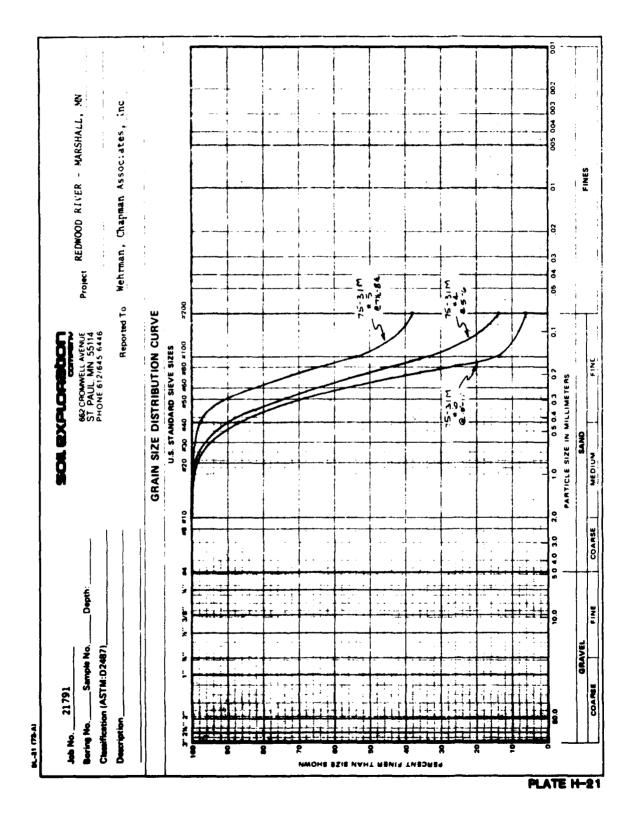
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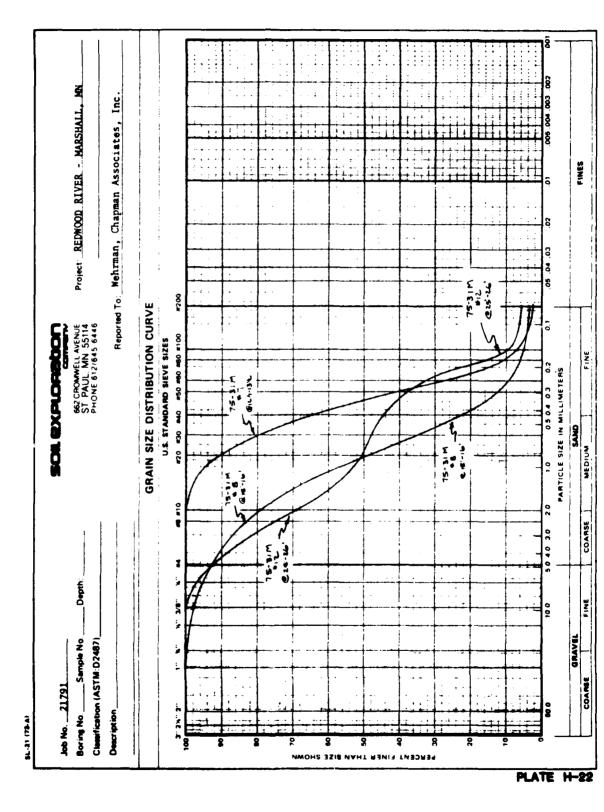
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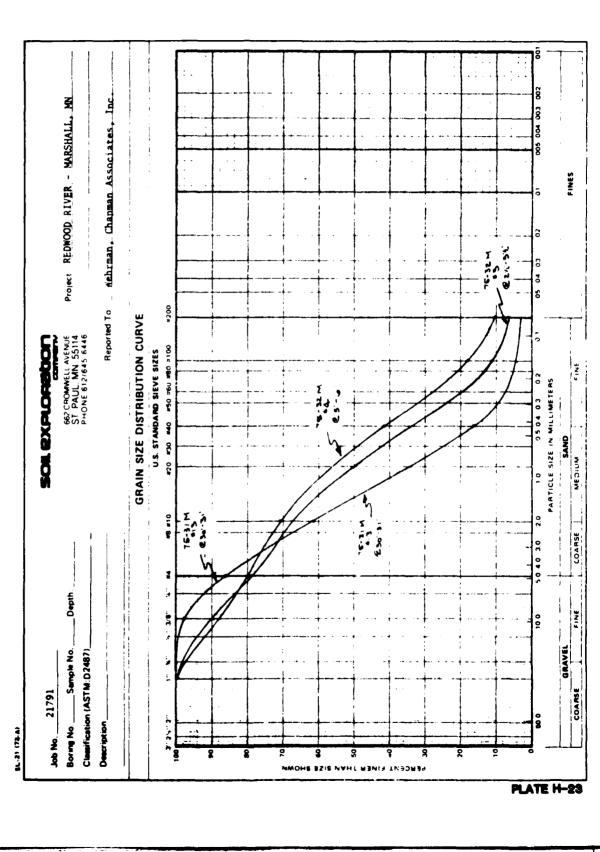


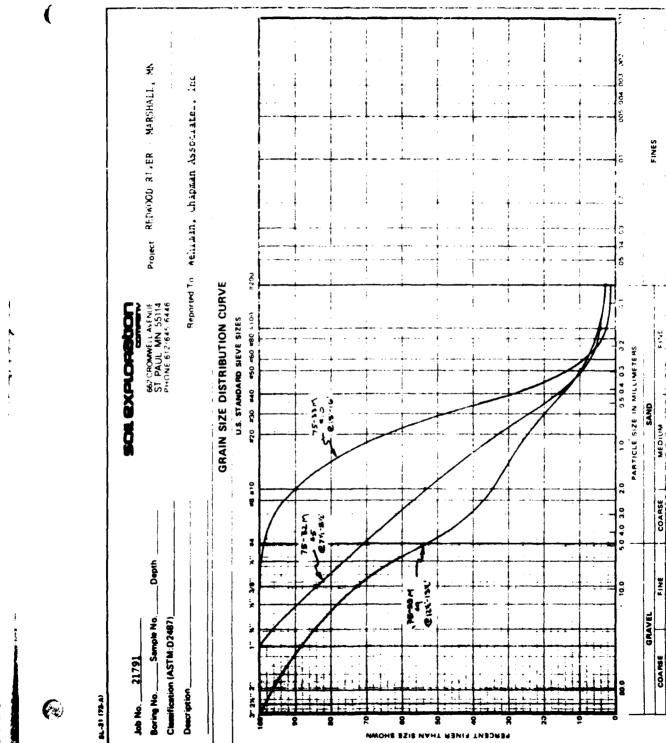
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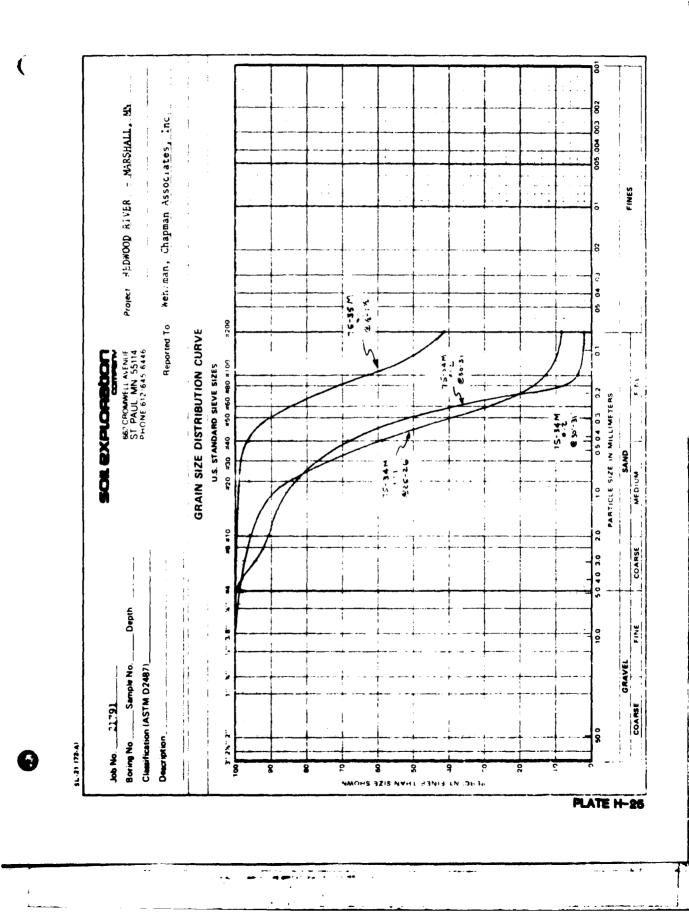
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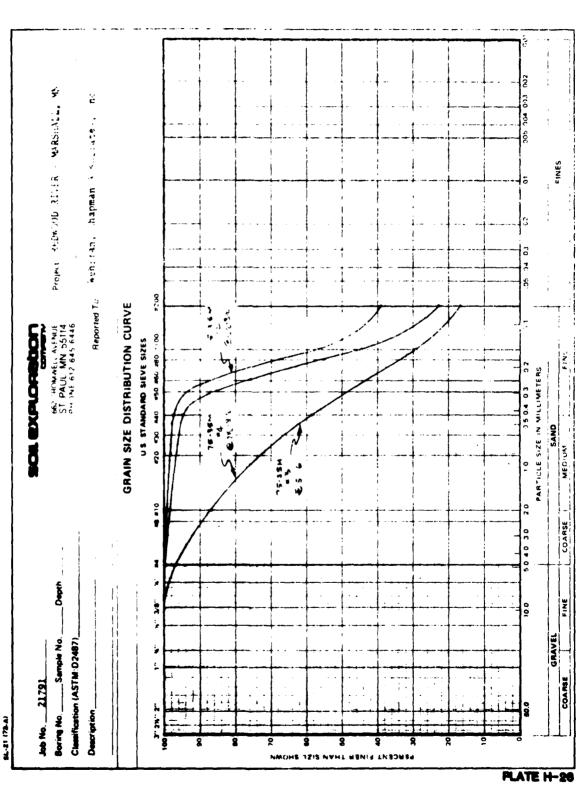
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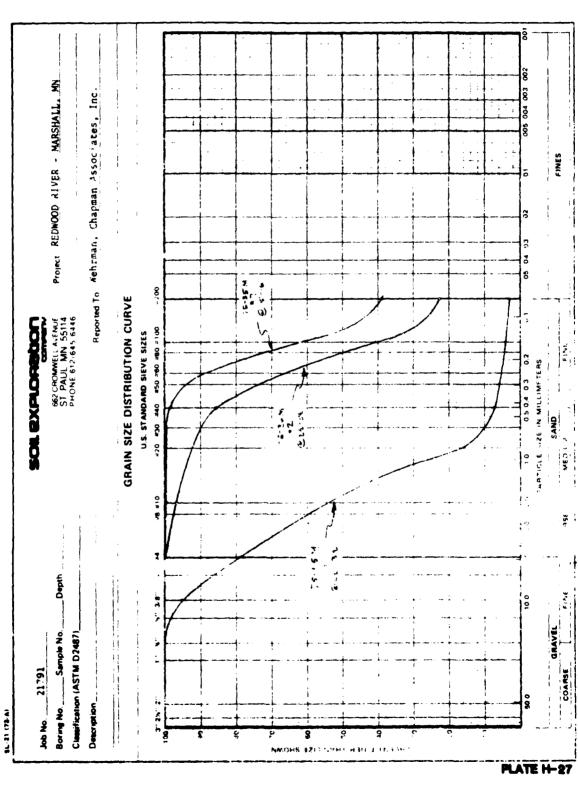
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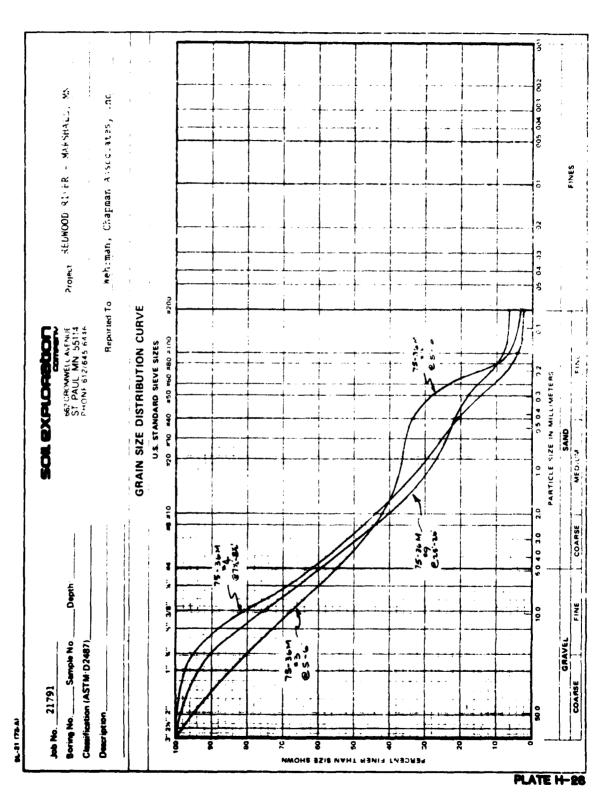
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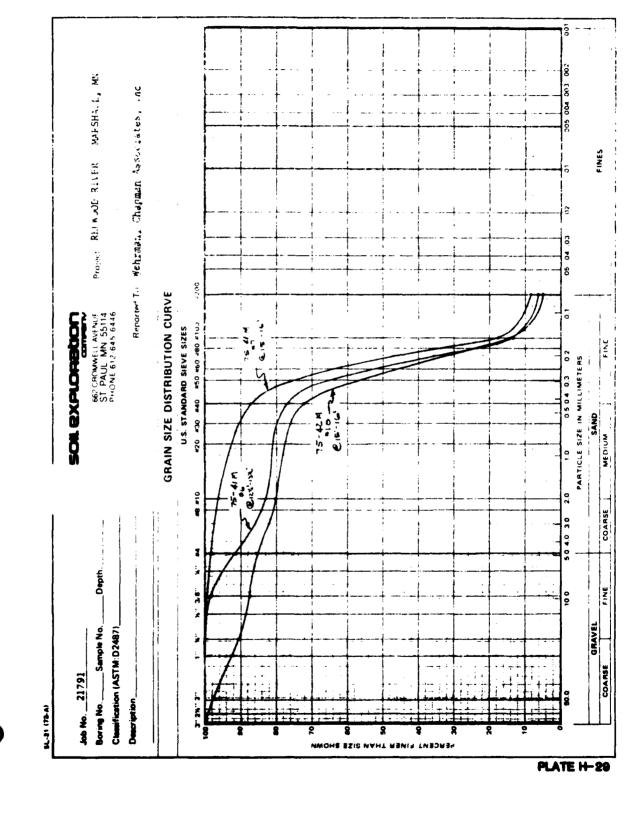


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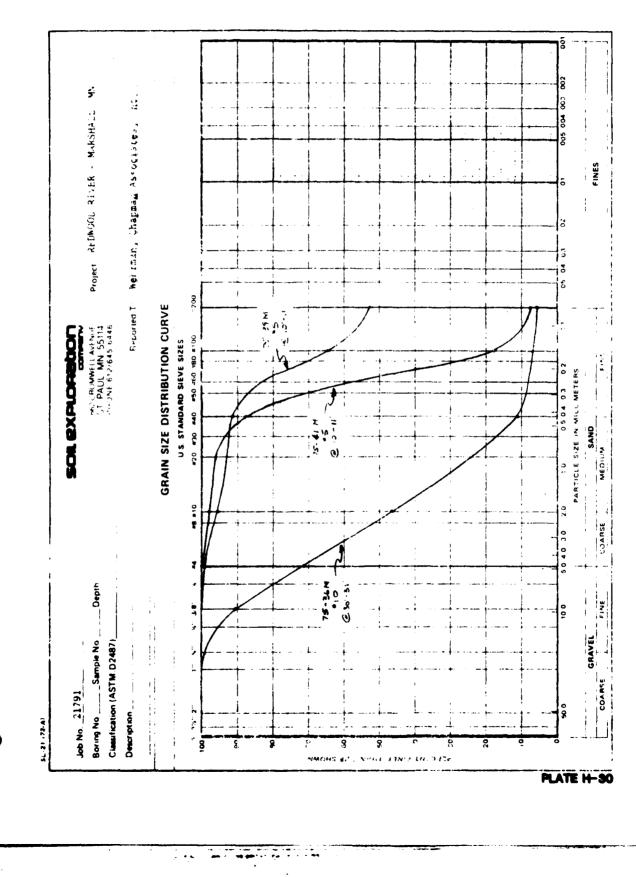
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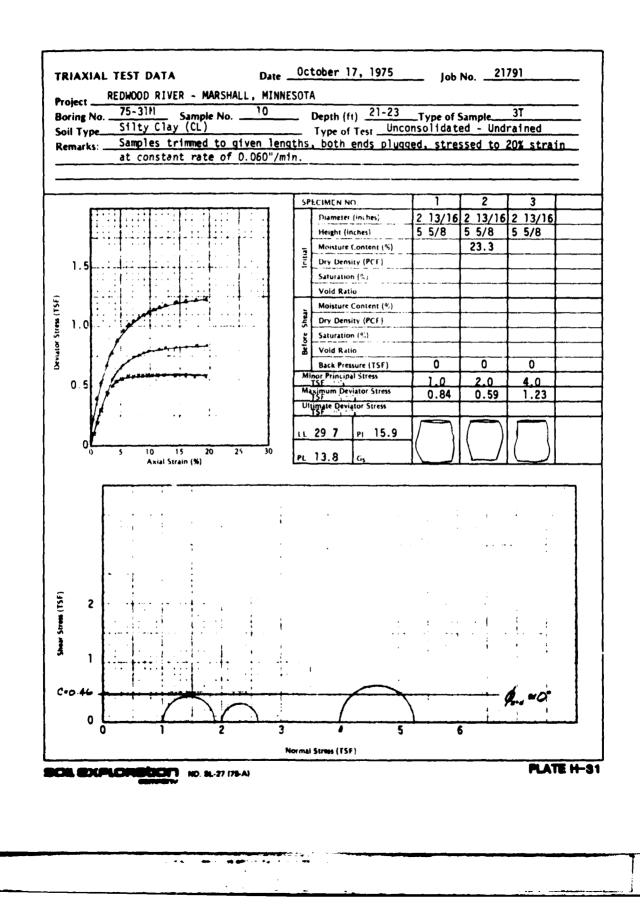


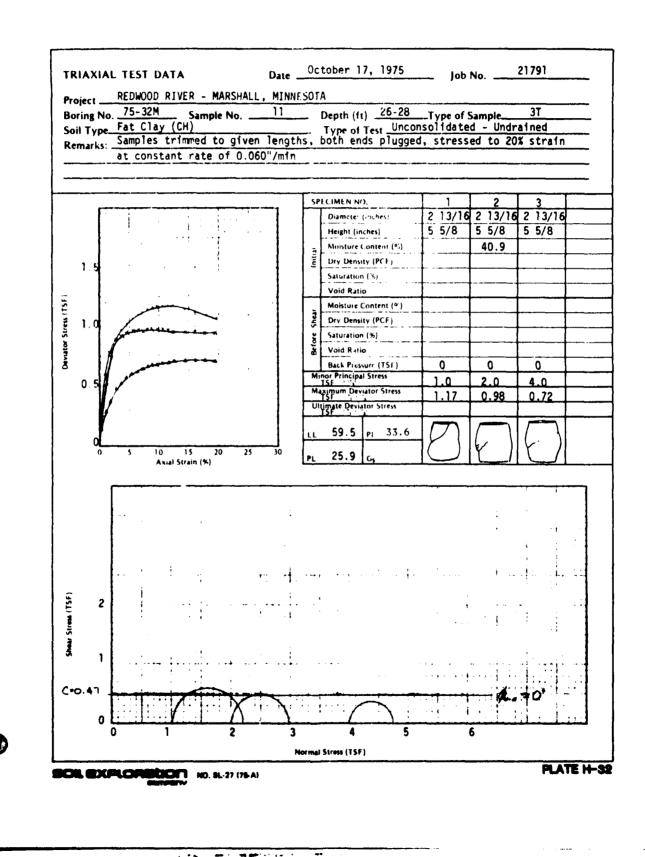
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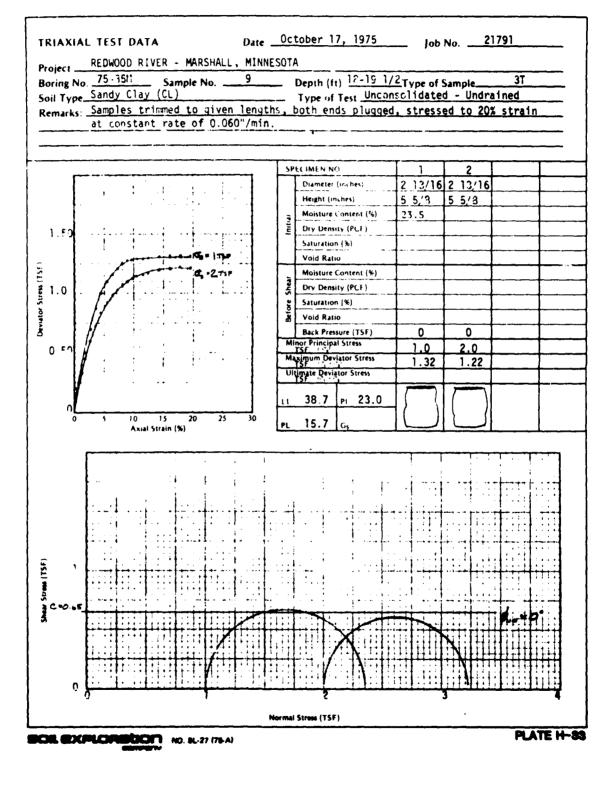
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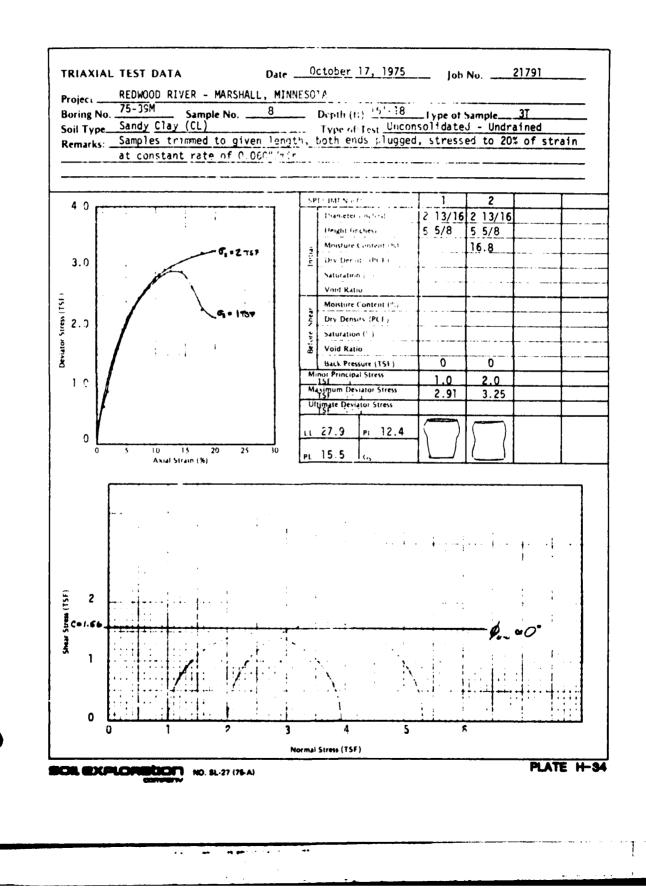
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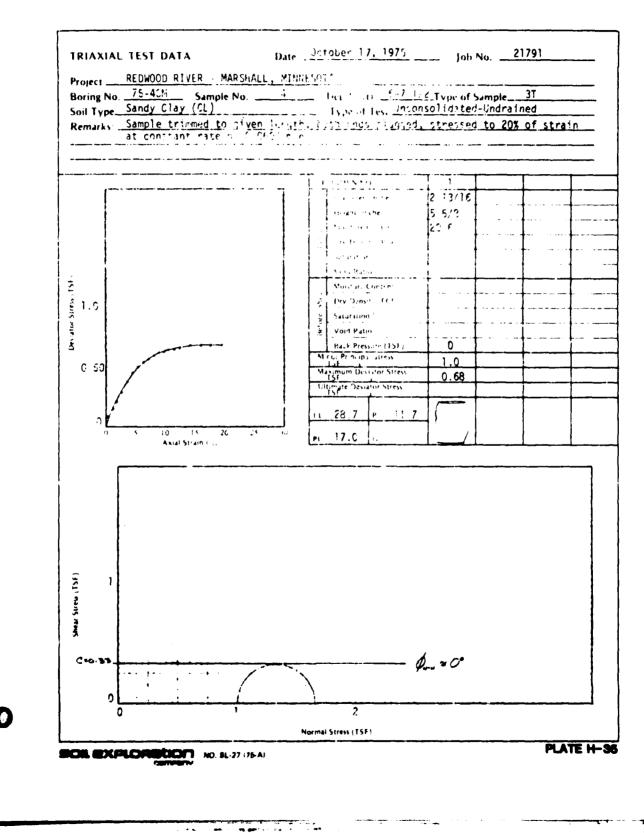


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| PROJEC              | TRED             |   |                    | N OF MATER                      | MINNESOT       | <u>A</u>        |               |          | <del></del> |     |          |     |        |                 |      |
|---------------------|------------------|---|--------------------|---------------------------------|----------------|-----------------|---------------|----------|-------------|-----|----------|-----|--------|-----------------|------|
| DEPTH<br>IN<br>FEET |                  |   |                    |                                 | ·~L            | 080 J           | JOGIC<br>IGIN | N        | WL          |     | TYPE     | W   | D      |                 | 0    |
|                     | SILTY            | CLAY, da  | irk brow           | nish gra                        | , rath-        |                 |               | 13       |             | 1   | SS       |     |        | PL              |      |
| 1                   |                  | SILT, b   |                    | gray r                          |                | FI:             | SOIL<br>NE    | 1 1.5    |             | 2   | SS       |     |        |                 |      |
| 2 <sup>1</sup> 2    |                  |   |                    | i sandy                         |                | ALLU<br>COA     |               | 8        | ł           | 3   | SS       |     |        |                 | м.   |
| 44                  | moist,           | loose,  | a fex :            | and, bro<br>anses of            | sandy          | ALLU            |               |          | Ì           |     |          |     |        |                 |      |
| •7                  | mottle           | CLAY, a   | m to ra            | gravel,<br>ther sti<br>ove S'r' | brown<br>ff, a | TI              | LL            | 6        |             | 4   | SS       | 17  |        | <u>36</u><br>18 |      |
|                     |                  |   |                    | (C1)                            |                |                 |               | 6        |             | 5   | SS       | 18  |        | $\frac{31}{16}$ |      |
|                     |                  |   |                    |                                 |                | -<br>-<br>-     |               | 7        |             | 6   | ss       |     |        |                 |      |
|                     |                  |   |                    |                                 |                | <br> <br> <br>1 |               | 15       |             | 7   | ss       |     |        |                 |      |
|                     |                  |   |                    |                                 |                | i               |               | 11       |             | 8   | ss       |     |        |                 |      |
| 195                 | SANDY<br>rather  | SANDY CLAY, a little gravel, gray, rather stiff |                    |                                 |                |                 |               | 12       |             |     | SS<br>3T |     |        |                 |      |
| I                   |                  |   |                    |                                 |                |                 |               |          |             | 11  | 3T       |     |        |                 |      |
|                     |                  |   |                    |                                 |                |                 |               | 9        |             |     |          |     |        |                 |      |
| 29                  |                  |   |                    |                                 |                |                 |               |          |             |     |          |     |        |                 |      |
| 30.1                | FAT CL<br>boulde |   |                    | r stiff.<br>(CH)                | 8              | See             | Note          | 25       |             | 12  | ss       |     |        |                 |      |
|                     | Note:<br>** (ML  | FINE ALL  | uction<br>.UVIUM o | r SHALE                         |                |                 |               | 0.1      |             |     |          |     |        |                 |      |
|                     |                  |   |                    |                                 | 178            |                 |               | START_   | 9-4         | 1-7 | 5        | 00  | MPLETE | 9-4             | - 75 |
| DATE                | TIME             | SAMPLED<br>DEPTH                                | CASING<br>DEPTH    | CAVE-IN<br>DEF*H                | BAILED DE      |                 | LEVEL         | METHOD   | 31          | C H | 5A 0'    | - 2 | 91, 1  | 1               | 2:0  |
| 9-4<br>9-4          | 12:05            | <u> </u>  | 295'<br>Nonc       | 30'<br>16'                      | 10<br>10       |                 | ione<br>Ione  | <u> </u> |             |     |          |     |        |                 | •    |
| 9-6                 | 7:40             | 30.1  | None               | 12'                             | 10             |                 | 91            | <b>_</b> |             | ·   |          |     |        |                 | ·    |

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|            |                                    |                         |                        | 50                           | il exp              | UDA          | COMPL        |          |      |        |           |        |        |                        |     |
|------------|------------------------------------|-------------------------|------------------------|------------------------------|---------------------|--------------|--------------|----------|------|--------|-----------|--------|--------|------------------------|-----|
| JOB NO     |                                    | 791<br>EDWOOD I         | RIVER -                |                              | CAL SCALE           |              | <u>، ۱</u>   | LOG      | OF T | EST E  | ORINC     | i NO _ | 75-    | 30M                    |     |
| DEPTH      |                                    |                         |                        | N OF MATER                   |                     |              |              | 1        | T    | SAI    | MPLE      | LA     | BORA   | OBY T                  | sts |
| IN<br>FEET |                                    |                         | N                      |                              |                     | GEO          | OGIC<br>GIN  | N        | WL   | NO     | TYPE      | w      | 0      |                        | Qu  |
|            |                                    | SILT, o<br>stiff        | iark bro               | wnish gr<br>(ML-             | ay,<br>CL)          | TOP          | 501 L        | 9        |      | 1      | ss        |        |        |                        |     |
| 2          | CLAYEY                             | SILT, d                 | lark bro               | wn, medi<br>(ML-             | ເ <b>ນກ</b><br>-CL) | FI.<br>ALLU  |              | 8        |      | 2      | ss        |        |        |                        |     |
| 4          |                                    |                         |                        | ight bro<br>lenses o<br>(SP- | f silty             | COAI<br>ALLU |              | 9        |      | 3      | ss        |        |        |                        | м.А |
| 7          |                                    |                         |                        | brown, m<br>sand {(          |                     | FI           | VF           | 8        |      | 4      | SS        |        |        |                        |     |
| 84 ;       |                                    |                         | ock, med               |                              |                     | ALLU         |              |          |      | 5<br>6 | 3T<br>3T* |        |        |                        |     |
| 115:       |                                    |                         |                        |                              | ,                   |              |              | 7        |      | 7      | ss        |        |        |                        |     |
| ****       | SILTY                              | •                       |                        | tied, me<br>sand and<br>(CL) | d silt              |              |              | 6        |      | 8      | SS        | 27     |        | $\frac{35}{19}$        |     |
| 14         | mottle                             |                         | unito so               | brownisł<br>ft, a fe<br>(CL) | ew .                |              |              | 5        |      | 9      | SS        |        |        |                        |     |
|            |                                    |                         |                        |                              |                     |              |              | 4        |      | 10     | ss        |        |        |                        |     |
|            |                                    |                         |                        |                              |                     |              |              |          |      | 11     | 3T        |        |        |                        |     |
| 24         | SILTY CLAY, brownish gray, soft, a |                         |                        |                              |                     |              |              |          |      | 12     | 3T        |        |        |                        |     |
|            | few le<br>lenses                   | nses of<br>of peas      | silty s<br>t below     | and, a 1<br>26' iMH-         | few<br>-CL)         |              |              | 4        |      | 13     | SS        | 37     |        | <u>54</u><br><u>33</u> |     |
| 29         | lenses                             |                         |                        |                              | rbearing            | COAL         |              |          |      |        |           |        |        |                        |     |
|            | sand                               |                         |                        | (ML-                         | SM)                 |              |              | 6        |      | 14     | SS        |        |        |                        | M./ |
| 32         |                                    | End                     | of Borin               | 2                            |                     |              |              | <u> </u> | Ļ    | ليليلي |           |        | l      | Ļ                      | L   |
|            | WATER LEVEL MEASUREMENTS           |                         |                        |                              |                     |              |              | START .  | 9-   | 5-7    | 5         | œ      | MPLETE | 9-5                    | -75 |
| 041E       | TIME<br>8:45                       | SAMPLED<br>DEPTH<br>321 | CARING<br>DEPTH<br>294 | CAVE-IN<br>DEPTH             | BAILED DEI          | PTHS         | UEVEL        | METHOD   | 34   | HS     | A 0'      | - 29   | 94'    | •8                     | :45 |
| 9-5        | 9:05<br>9:45                       | <u> </u>                | None                   | 185'                         | 10<br>10            |              | None<br>None |          |      |        |           |        |        |                        |     |
| <u> </u>   | +                                  |                         | +                      | h                            | 10                  |              |              | -        | HIEF |        | redo      |        |        |                        |     |

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|---------------------|---------------------------|---|---|--------------------------|--|---------------|----------------|----------|-----------|----------|----------|------------|--------|---------------------------------------|-------|
| JOU NO              |                           | 1<br>EDWOOD   | RIVER -   | MARSHALL                 | L. MINNE   | 1'' =<br>SOTA | 4'             | <b></b>  | OF T      | EST E    | KC≦NG    | NO _       | 75-    | 31M                                   |       |
| _                   |                           |   | ESCRIPTION  |                          |  |               |                |          | 1         | SAI      | APLE     | LA         | BORAT  | ORY TE                                | STS   |
| DEPTH<br>IN<br>FEET |                           |   | ·   |                          |  | 660,<br>194   | IGIN<br>IGIN   | N        | WL        |          | TYPE     |            | D      | LL<br>PL                              | Qu    |
| 3                   |                           | SILT, da  | of LEAN_<br>ark gray  |                          | •n, ¦  | TOP:          | 5CT1.          | 12       |           | 1<br>2   | 55<br>55 |            |        |                                       |       |
|                     | CLAYEY                    | SILT, d   | ark brow  | n, medin<br>(ML-)        |  | F : :<br>ALLU |                | 7        | <br> <br> | 3        | ss       | 6          |        | 24<br>19                              |       |
| <b>4</b> f          | SAND, f<br>moist,<br>sand |   | ined, ii<br>a few le  |                          | silty  | CON<br>ALL    | RSE<br>IV TUM  | -<br>-   |           | 4        | ss       |            |        |                                       | M.A.  |
| -                   | brown a                   | ind brow  | ne grain<br>n, moist<br>f silt  | , er)                    | 10050,   |               |                | i<br>J   | 1         | 5        | ss       |            |        |                                       | м.а.  |
| 9 <sup>1</sup> 9    | SAND, 1<br>loose,         | ine gra<br>a few 1  | ined, br<br>enses of  | own, mo<br>silty<br>(SP) | sand   |               |                | Ŕ        |           | 6        | SS       |            |        |                                       | M.A.  |
| 12                  | SAND, 1<br>moist,         |   | ined, li  | ght bro<br>(SP)          |  |               |                | 7        |           | )<br>  7 | ss       |            |        |                                       | м.а.  |
|                     | light l<br>lenses         | orown, m  | rained,<br>Hoist, de<br>Clay  | ense, a                  | few  |               |                | 16       |           | 8        | SS       |            |        |                                       | М.А.  |
| 175                 |                           | LAY, dar  | k gray 1  | to gray,<br>(CL)         |  | FIN<br>ALLU   | _              | 9        |           | 9        | SS       | 28         |        | 49                                    |       |
| 21                  | mottle                    | d, mediu  | ight gray<br>ma, a ler  |                          | silty  | <br> <br>     |                | 1        |           |          | 3T       | 23         |        | $\frac{\overline{20}}{\overline{14}}$ |       |
| 2312                | SAND,                     | GAND, medium grained a little<br>gravel, gray, waterbearing, medium |   |                          |  |               | RSE<br>UVIUM   | 12       |           |          | 3T       |            |        |                                       | M.A.  |
|                     |                           |   | .TY CLAY,<br>prownish   | ,                        |  |               |                |          |           |          |          |            |        |                                       |       |
| 31                  |                           | End of  | fBoring   |                          |  |               |                | 9        |           | 13       | ss       |            |        |                                       | M.A.  |
|                     | WATER LEVEL MEASUREMENTS  |   |   |                          |  |               |                | START    |           |          |          |            | OMPLET |                                       |       |
| DATE                | THAT                      | SAMPLED<br>DEPTH  | CABING<br>DEPTH   | CAVE-IN<br>DEPTH         | BAILED D   | EPTHS         | WATER<br>LEVEL | WETHO    | •         | 34 1     | isa (    | <u>, -</u> | 294'   | •                                     | 10:45 |
| 9-5                 |                           | 26'   | 23'   |                          | 10   |               | 2041           | ┫        |           |          |          |            |        |                                       |       |
| <u>9-5</u><br>9-5   |                           | <u>31'</u><br>31'   | 2951<br>None  | 14'                      | 10   |               | 23'<br>None    | 1        |           |          |          |            |        |                                       |       |
|                     |                           |   | The second se |                          | And in case of the local division of the loc |               |                | CREW     |           |          | laged    |            |        |                                       |       |

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PLATE H-S

| JOB NO<br>PROJEC |  | 21791<br>DWOOD R | IVER - M            | ARSHALL               | MINNESC          | TA -        | •           | LOG      |   |            |          |    | _      |                   |            |
|------------------|--|------------------|---------------------|-----------------------|------------------|-------------|-------------|----------|---|------------|----------|----|--------|-------------------|------------|
| IN<br>FEET       |  | ELEVATIO         |                     | SCRIPTION OF MATERIAL |                  | GEOLOGIC    |             | N        |   | h          | TYPE     | w  | D      | <u>LL</u>         | Qu         |
|                  | 1  |                  | dark bro            | wnish gi              | ray, soft        |             |             | +        |   |            |          |    |        | Pi                | -          |
| 1                |  |                  | dark bro            | (AL)                  | - <u>CL)</u>     |             | SOIL        | 5        |   | 12         | SS<br>SS |    |        |                   |            |
| 2                |  |                  | to 1:ne             | <u></u>               | <u>- (, ), )</u> | See N       | ote:        | +        | 1 | -          |          |    |        |                   | ļ          |
|                  |  |                  | , brown,            |                       | -                |             | ARSE        | 6        |   | 3          | SS       |    |        |                   | м.         |
| [                |  |                  | se, some            |                       | or               | ALLU        | -           | 1        |   |            |          |    |        |                   |            |
| i                | SILLY  | sanu an          | d silty             |                       | -SM)             |             |             | 1.4      |   |            | ss       |    |        |                   |            |
| 6                |  |                  |                     | <u></u>               |                  | -           |             | 14       |   | 4          | 55       |    |        |                   | M./        |
| İ                | -  |                  | grained,            |                       |                  |             |             |          | 1 |            |          |    | ,<br>i |                   | [          |
| l                | gravel                                       | , light          | brown,              | moist, (<br>(SP)      |                  |             |             | 1 17     |   | s          |          |    |        |                   | M.         |
|                  |  |                  |                     |                       | ,<br>,           |             |             | 1 -      |   | 1          |          |    |        |                   |            |
| 9 <sup>1</sup> 3 | IFAN C                                       | TAV a            | trace of            | araval                | derk             | міх         | FD          | +        |   | 1          |          |    |        |                   |            |
| :                | gray,  |                  | clace of            | (CL)                  |                  |             | VIUM        | 3        |   | 6          | ss       |    |        |                   | ĺ          |
| 114              | SILTY  | CAND -           |                     | as model              | a little         |             |             | 1        |   |            |          |    |        |                   |            |
|                  |  |                  | , moist             |                       |                  | COA<br>ALLU | RSE         | 8        |   | <b>1</b> 7 | ss       |    |        | )                 | ļ          |
|                  |  |                  | •                   | •                     | nd moist         | ALLO        | VIUM        | 0        |   |            | 33       |    |        |                   |            |
| 145              |  | erbeari          |                     | (SM)                  |                  | C 114       |             | +        | } | ]          |          |    |        | }                 |            |
|                  |  |                  | CLAY, d<br>ses of b |                       |                  | SWA<br>DEP  | MP<br>OSITS | 15       |   | 8          | SS       |    |        |                   |            |
|                  | muck   |                  |                     | (OL                   |                  |             |             |          |   |            |          |    |        |                   |            |
|                  |  |                  |                     |                       |                  |             |             |          | ĺ |            |          |    |        |                   | ļ          |
| 18               | SILTY  | CLAY. g          | ray, sof            | t                     |                  |             |             | 1        |   | l          |          |    |        | 1                 | 1          |
|                  |  | •••••            | ,,                  | (CL                   | )                | FI          |             |          |   |            |          |    |        |                   |            |
| -                |  |                  |                     |                       |                  | ALLU        | VIUM        | 2        |   | 9          | SS       | 34 |        | 45                |            |
|                  |  |                  |                     |                       |                  |             |             | •        |   | 1          |          | 54 |        | 20                |            |
| 22 -             | FAT CI                                       | AV are           | y and br            |                       | tad              |             |             |          | ł | l          |          |    |        | 1                 |            |
|                  | medium                                       |                  | y and DI            | (CH)                  |                  |             |             |          |   |            |          |    |        |                   |            |
|                  |  |                  |                     |                       |                  |             |             | Ì        |   |            |          |    | ļ      |                   |            |
|                  |  |                  |                     |                       |                  |             |             | 6        |   | 10         | ss       |    |        | ĺ                 |            |
|                  | NOTE   | FINE AL          | LUVIUM              |                       | I                |             |             |          | { | i          |          |    |        |                   |            |
|                  |  |                  |                     |                       |                  |             |             |          | ļ | 11         | 3T       | 41 |        | $\frac{60}{26}$   | ļ          |
|                  |  |                  |                     |                       |                  |             |             |          |   | ļ          |          |    |        |                   |            |
| 295              |  |                  | ·                   |                       |                  |             |             |          |   | 12         | 3T       |    |        |                   |            |
|                  |  |                  | ark brow            |                       |                  |             |             | 5        | } | 13         | ss       |    |        | ł                 | }          |
| 31               |  | d, medi          |                     |                       | -UL)             |             |             | 1        | ļ |            |          |    |        |                   |            |
|                  |  | End of           |                     | -,                    |                  |             | · · ·       |          |   |            |          |    |        | L                 |            |
|                  | <u>,                                    </u> |                  | TER LEVEL B         |                       | <u></u>          |             |             | START_   |   | 5-7        |          |    | MPLET  | : <u>9</u> .<br>1 | <u>5-7</u> |
| DATE<br>9-5      | 7 mile<br>2:10                               | SAMPLED<br>DEPTH | CASING<br>DEPTH     | CAVE IN<br>DEPTH      | BANED DE         | PTHS        | UEVEL       | METHOD   | 3 | K H        | SA O     |    | 28'    | 10                | 2:5        |
| 9-5              | 4:10   | 31               | 28'                 |                       | 10               |             | 25'         | <u> </u> |   |            |          |    |        | <del>.</del>      |            |
| 9-5              | 4:35   | - 31 '           | None                | 91                    | 10               |             | None        | ]        |   |            |          |    |        |                   |            |

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SOIL EXPLORATION LOG OF TEST BORING NO \_\_\_\_\_\_\_ 75-33M 1" = 4' 21791 VENTICAL SCALE REDWOOD RIVER- MARSHALL, MINNESOTA JOB NO PROJECT DESCRIPTION OF MATERIAL SAMPLE LABORATORY TESTS DEPTH GEOLOGIC NO TYPE 쁥 FEET SURFACE ELEVATION w D Qu N wι SILTY CLAY, dark brownish gray (CL) 1 SS TOPSOIL 6 1 SS 2 CLAYEY SILT, dark gray, medium (ML-CL) FINE 3 SS ALLUVIUM 6 5 SILTY CLAY, brown and gray mottled, 4 SS soft to medium, a few lenses of sand and silty sand above ?"  $\frac{55}{30}$ (CL to MH-S SS 28 CL) ; 3T 6 95 3T · MEDIUN FAT CLAY, brownish gray, 8 SS 8 medium (CH) 12 SAND, medium to coarse grained, 9 M.A. 19 SS with gravel, brown, waterbearing, COARSE dense\_\_\_\_(SP)\_\_\_\_ 14 SAND, medium grained, a little ALLUVIUM gravel, brown, waterbearing, very MÎA. 10 SS 4 (ŠP) loose 19 51LT, light brownish gray, wet, very FINE ALLUVIUM loose, a rew lenses of silty sand 11 55 3 and silty clay (ML) 22 SILTY CLAY, dark brownish gray, soft (CL) 12 88 135 4 - 1 21 SILTY CLAY, gray, soft, lenses of silt, silty sand, and waterbearing sand (CL) \* Thinwall tube sample obtained from adjacent secondary boring 38 1 15155 121  $\overline{21}$ 32 End of Boring ----9-5-75 9-5 WATER LEVEL MEASUREMENTS 51 AR1 COMPLETE \_ SAMPLED DEPTH CASING DEPTH WATER LEVEL CAVE IN DEPTH 34 HSA BAILED DEPTHS 2941 DATE THE METHOD 0' 12' 12' 9-5 5:20 137. 1251 5:55 32' 294' 221 9-5 ית 32' 9-5 6:15 None None ۱0 Hagedorn 5 2 170-A PLATE H-40

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|            |                  |                                   |                     | SC                         | M. EXF            |                   | Cominii         |        |      |        |          |             |       |        |      |
|------------|------------------|-----------------------------------|---------------------|----------------------------|-------------------|-------------------|-----------------|--------|------|--------|----------|-------------|-------|--------|------|
| JOB NC     |                  | 21791<br>EDWOOD R                 | IVER M              |                            | MINNESC           | 1 <u>''</u><br>TA | = 4'            | LOG    | OF T | EST E  | BORING   | NO <u>7</u> | 5-34  | IM     |      |
| DEPTH      |                  |                                   | DESCRIPTIO          | N OF MATER                 | NAL               |                   |                 | 1      | T    | SAI    | MPLE     | LA          | BORAT | ORY TE | STS  |
| IN<br>FEET | SURFA            | CE ELEVATIO                       | N                   |                            |                   | GE                | OLOGIC<br>RIGIN | N      | WL   | NO     | TYPE     | w           | D     | LL     | Qu   |
| <b>\</b>   | CLAYEY           | í SILT, d                         | iark bro            |                            | rav, soft<br>-{L} |                   | PSOIL           | i ,    | •    | +<br>1 | 'SS      |             |       | PL     |      |
| 2          |                  | brown, r<br>s of silt             |                     | 005 <b>e, s</b> (          | ome<br>1          | FI                | NE<br>LUVIUM    | 7      |      | 2      | SS       |             |       |        |      |
|            |                  |                                   |                     |                            |                   |                   |                 | 6      |      | 3      | ss       |             |       |        |      |
| 7          | medium<br>and su | CLAY, bi<br>n, some l<br>and      | cown and<br>enses o | gray mo<br>f silty<br>(CL) | sand              |                   |                 | 6      |      | 4      | ss       |             |       |        |      |
| 9 <b>%</b> | SILTY            | CLAY, bi<br>d, rathe              | ownish<br>er stiff  | gray and<br>(CL)           | l brown           |                   |                 | 10     |      | 5      | SS       |             |       |        |      |
| 125        | SILTY<br>soft,   | CLAY, bi<br>a few le<br>bearing s | enses of            | gray mo<br>silty s<br>(CL) | and and           |                   |                 | 4      |      | 6      | SS       |             |       |        |      |
| 16         | <br>STITY        | CLAY, gi                          | ev med              |                            |                   |                   |                 | 4      |      | 7      | SS       |             |       |        |      |
| 1          | 51611            | curi, gi                          | ,                   |                            | -CH)              |                   |                 | ł      |      | -      | 3T       |             |       |        |      |
| 8          | rise             | : Water )<br>to dept<br>rvation v | of abo              | ut 13' 1                   | ed to<br>based on |                   |                 | 5      |      |        | 3T<br>SS |             |       |        |      |
| 25         | SAND,            | fine to                           | medium              | grained,                   | , <b>a</b>        |                   |                 | 6      |      | 11     | SS       |             |       |        | M*/  |
| 27         | SAND,            | medium g<br>l, brown,             | rained,             | <u>s littl</u>             | e<br>medium       |                   | ARSE<br>JVIUM   |        |      |        |          |             |       |        |      |
| 31         |                  | <u></u>                           | End of              | Boring                     |                   |                   |                 | 15     |      | 12     | SS       |             |       |        | Mt/  |
| 1          |                  |                                   |                     |                            | NTS               |                   |                 | START_ | 9-6  | - 75   |          |             |       | 9-6    | - 75 |
| DATE       | THE              | SAMPLED<br>DEPTH                  | CASING<br>DEPTH     | CAVE-IN<br>DEPTH           | BAILED DE         | PTHS              | WATER<br>LEVEL  | METHOD |      | -      | -        | -           | _     | .9     |      |
| 9-6<br>9-6 | 9:10<br>9:30     | 31'                               | 2941<br>None        | 124                        | to<br>to<br>to    |                   | 22*<br>None     |        |      |        |          |             |       |        |      |
|            |                  |                                   |                     |                            | to                |                   |                 | CREW C | NEF  | . Н    | agedo    | 110         |       | ATE    |      |

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|                   |                            |                    |   | 50                            | IL EXP                   | LOA         | eto                   | n        |      |         |          |                  |        |                 |             |
|-------------------|----------------------------|--------------------|---|-------------------------------|--------------------------|-------------|-----------------------|----------|------|---------|----------|------------------|--------|-----------------|-------------|
| IOB NO<br>MOJEC   |                            | 791<br>200012 RT   | VEN - M                                   |                               | MINNESO                  | <u>1"</u> = | 4'                    |          | OF T | EST B   | ORING    | 3 NO 2           | /5-35  | M               |             |
|                   |                            |                    | DESCRIPTION                               |                               |                          |             |                       | 1        |      | SAL     | APLE     |                  | BORA   |                 | 515         |
| EPTH<br>IN<br>EET |                            |                    | N   |                               |                          | GEOI<br>PO  | .ogic<br>Igi <b>n</b> | N        | WL   | h       | TYPE     | w                | D      |                 | 0u          |
|                   |                            |                    | of SAND                                   |                               | TY SAND,                 | FII         | LL                    | 13       |      | 1       | SS       |                  |        |                 | M.A         |
| 2 <sup>1</sup> 2  |                            |                    | trace of stiff                            |                               | 1, dark                  | TOPs        | SOIL                  | 1 1 7    |      | 2       | ss       |                  |        |                 | <b>M</b> .A |
| 4 4.              | SAND, i<br>little<br>a few | gravel,            | o fine ;<br>brown,                        | grained,<br>moist,<br>sand an | a<br>loose,<br>id clayey | co          | ARSE                  | 8        |      | 3       | SS       |                  |        |                 | M.A         |
| -                 | moist                      | to 8' t'           | ined, g<br>er wate<br>leruss o            | rbearing                      | rown,                    |             |                       | 5        | Y    | 4       | ss       |                  |        |                 | м.А         |
| 95 -              | and or                     | ganic si           | CLAY, D                                   | <u>(\$P-</u>                  | SM)<br>ft                |             | AMP<br>DSITS          | 3        |      | 5       | SS       | 64               |        | 80<br>45        |             |
| 115.              | with g                     | ravel, t           | n coar-<br>black, w                       |                               | ing,                     |             | ARSE                  | 3        |      | 6       | SS       | 4<br>4<br>4<br>4 |        |                 | M.A         |
| 135 -             | SILTY                      | SAND, fi           | ne grai:<br>wet, ve                       | ned, bro                      | wn and                   | ALLI        | JV I UMI              | 4        |      | 7       | SS       |                  |        |                 | M.          |
| 18' .             |                            |                    |   |                               |                          |             |                       |          |      | 8       | ۲T       | 23               |        | $\frac{39}{16}$ |             |
|                   | and a<br>medium            | little :<br>to rat | little<br>light gr<br>mer stif<br>ng sand | ay mottl<br>f, a few          | ed,<br>lenses            | TI          | LL                    | 9        |      | 9<br>10 | 3T<br>SS | 24               |        | 37<br>18        |             |
| 24                | CLAYEY                     | SAND.              | a little                                  | gravel                        | PTAY                     |             |                       |          |      |         |          |                  |        |                 |             |
|                   | and br                     | own mot            | tied, st<br>erb <b>ea</b> rin             | aff, a f                      | few                      |             |                       | 23       |      | 11      | ss       | 19               |        | 25<br>20        |             |
| 27                |                            | CLAY, a<br>stiff   | little                                    | gravel.<br>(CL)               |                          |             |                       |          |      |         |          |                  |        |                 |             |
|                   | • No m                     | easurem            | ent reco                                  | rded                          |                          |             |                       | 10       |      | 12      | ss       | 19               |        | 29<br>15        |             |
| 32                | ·E                         | nd of B            | bring                                     |                               |                          |             |                       | <u> </u> |      |         |          |                  |        |                 |             |
|                   |                            |                    |   | ALASUREME                     | TS                       |             |                       | START _  | 9-4  | -75     |          | 0                | OMPLET | 9-4             | -75         |
| DATE              | TIME                       | SAMPLED<br>DEPTH   |   | CAVE IN                       | BAILED DE                | PTHS        | WATER                 | METHOD   | 3    | ₩ H     | SA O     | ! -              |        | 7               | 5:00        |
| 9-4               | 3:45                       | 9'                 | 71  | 84                            | to                       |             | 81                    | 1        |      |         |          |                  |        |                 |             |
| 9-4               | \$:00                      | 32'                | 294                                       |                               | 10                       |             | ٠                     |          |      |         |          |                  |        |                 |             |
| 9-4               | 5:20                       | 32'                | None                                      |                               | 10                       |             | •                     | ┟───     |      |         |          |                  |        |                 |             |
|                   | 1 1                        |                    | L   |                               | 10                       | 1           |                       | CREW CI  | HEF  | . Н     | aged     | OTD              |        |                 |             |

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|            | ~ •               | -01                             |              | SC               |             |         | COMPO             |          |       |          |            |    |       |          | _                |
|------------|-------------------|---------------------------------|--------------|------------------|-------------|---------|-------------------|----------|-------|----------|------------|----|-------|----------|------------------|
|            |                   | 791<br>WOOD RIV                 | FR - MA      |                  | ICAL SCALE  |         | 4'                | LOG      | OF TI | EST E    | BORING     |    | 25-36 | M        | ··               |
| EPTH       |                   |                                 | DESCRIPTIO   |                  |             |         |                   |          |       | SAI      | MPLE       | L/ | BORA  | ORY T    | STS              |
| IN<br>FEET |                   | CE ELEVATIO                     | N            |                  |             | GE      | OLOGIC<br>IRIGIN  | N        | WL    | NO       | TYPE       | w  | D     |          | Qu               |
|            | CLAYEY<br>medium  | SILT, d                         | lark bro     | wnish gr<br>(ML- | • •         | TO      | SOIL              | 6        |       | 1        | SS         |    |       |          |                  |
| 2<br>45    |                   | fine gra<br>lenses              |              |                  |             |         | DARSE<br>LUV I UM | 6        |       | 2        | 55         |    |       |          | M.A              |
| -          |                   | medium g<br>brown, m            |              |                  |             |         |                   | 9        |       | 3        | SS         |    |       |          | M.A              |
| 7          | little            | medium t<br>gravel,<br>aterbear | brom,        | moist t          | o 75'       |         |                   | 10       |       | 4        | SS         |    |       |          | MĂ               |
|            | mottle<br>_bearin | g sand                          | a few        | lenses c         | of water-   | Т       | I LL.             | 4        |       | 5        | ss         |    |       |          |                  |
| 135        |                   |                                 |              |                  | stiff       |         |                   | 9        |       | 6        | ss         |    |       |          |                  |
|            |                   | CLAY, a<br>to rath              |              |                  |             |         |                   | 7        |       | 7        | <b>S</b> S | 20 |       | 35<br>18 |                  |
|            |                   |                                 |              |                  |             |         |                   | 31       |       | 8        | 55         |    |       |          |                  |
| 2312       | gray,             | coarse g<br>Waterbea<br>y sandy | ring. de     | chise, a         | lense<br>11 |         | DARSE<br>2V (UM   | 29       |       | 9        | <b>S</b> 5 |    |       |          | M.A              |
| 51         | • No #            | End of                          | Boring       |                  |             |         |                   | 16       |       | 10       | SS         |    |       |          | M <sup>®</sup> A |
|            |                   |                                 |              |                  | NTS         | <b></b> |                   | START_   | 9.    | 4-       | 75         | ~  | MPLET | 9-       | 4-75             |
| DATE       | TIME              | SAMPLED DEPTH                   | CASING DEPTH | CAVE IN<br>DEPTH | BAILED DE   | PTHE    | WATER             | METHOD   | y     | H        | SA 01      |    | 941   | 102:     | 30               |
| 9-4        | 1:50              | 21                              | 71           | 81               | 10          |         | 7141              | 1        |       | <u> </u> |            |    |       |          |                  |
| 9-4        | 2:30              | 31'                             | 2951         |                  | 10          |         | •                 | <b>I</b> |       |          |            |    |       |          |                  |
| 9-4        | 2:50              | 31'                             | None         |                  | 10<br>10    |         | · · ·             | CREW CH  |       | Ha       | redo       | n  |       |          |                  |
|            |                   | L                               |              |                  | <b>1</b>    |         | 1                 | TOWER CH | 198 P |          |            |    |       |          |                  |

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|                   |   | 791  |  |  | CAL SCALE   | 1" = 4'            |                  | ()F T | ESTE     | ORING        | NO . | 23-3                  | 2 <u>.</u> M |          |
|-------------------|---|--|--|--|---|--------------------|------------------|-------|----------|--------------|------|-----------------------|--------------|----------|
| PROJE             | 01 <u>RED</u>   | WOOD R1  | <u>VER - MA</u>  | RSHALL, I  | MINNESOT  | <u>A</u>           |                  |       |          |              |      |                       |              | _        |
| IN<br>FEET        |   | CE ELEVATIO  |  | IN OF MATERI   | AL  | GEOLOGIC<br>ORIGIN | N                | w     | <b>⊢</b> | MPLE<br>TYPE |      | D                     |              | STS<br>2 |
| <b> </b><br> <br> | SILTI   |  | d gravel   | AY, a 11<br>, brown,   |   | FILL               | 5                | •     | 1        | SS           |      |                       |              |          |
|                   |   |  |  |  |   |                    | 15               |       | 2        | 55           |      | ,<br>,<br>,<br>,<br>, |              |          |
| <br> <br>         |   |  |  |  |   |                    | 4                |       | 3        | ss           |      |                       |              |          |
|                   | tled,<br>sand a   |  | ome lens   | n and gri<br>es of si<br>(CL)  |   | FINE<br>ALLUVIUM   |                  |       | 4        | 55           |      |                       |              |          |
| ) <u>1</u> 2      | SAND,<br>gravel   | . brown  | . waterb   | e grained<br>earing, 1<br>[5P]   | aed ເພ  | COARSE<br>ALLUVIUM | 0.1              |       | 5        | SS           |      |                       |              |          |
|                   | SANDY<br>mottle   | CLAY, a<br>d, rath   | little<br>er sciff   | gravel, l<br>, a řew .<br>(CL)   | brown   | TILL               | 9                |       | 6        | SS           |      |                       |              |          |
|                   |   |  |  |  |   |                    | 1                | 1     |          |              |      |                       | ĺ            |          |
| 6                 | · · · · · · · · · · · · · · · · · · ·                         |  |  |  |   |                    | 13               |       | 17       | SS           |      | 1                     |              | 1        |
| 6                 | rather  | stiff,   |  | gravel,<br>inses of t<br>(CL)  |   |                    | 13               |       | Ĺ        | SS<br>3T     |      |                       |              |          |
|                   | rather<br>bearin  | stiff,   | some le<br>below 18  | nses of i  |   |                    | 13               |       | Ĺ        |              |      |                       |              |          |
|                   | rather<br>bearin<br>* Note<br>rise                            | End of<br>Water<br>to dep  | some le<br>below 18<br>Boring<br>level :<br>th of ab   | nses of i  | ed to<br>based                                    |                    | 13               |       | Ĺ        |              |      |                       |              |          |
|                   | <pre>* Note     rise     on o     ** Hig</pre>                | End of the server.   | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>ion whil<br>count du                                     | s expect.  | ed to<br>based<br>ng.                             | -                  | 13               |       | Ĺ        |              |      |                       |              |          |
|                   | * Note<br>r1se<br>on o<br>** Hig                              | End of the server.   | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>ion whil<br>count du                                     | nses of i<br>(CL)<br>s expected<br>out פיבי<br>e המשקוו<br>e to ence                     | ed to<br>based<br>ng.                             |                    | 13               |       | Ĺ        |              |      |                       |              |          |
|                   | * Note<br>r1se<br>on o<br>** Hig                              | End of the sand the s | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>jon whil<br>count du<br>or small                         | nses of (<br>(CL)<br>(CL)<br>s expected<br>out 9½ 1<br>e samplin<br>e to ence<br>boulder | ed to<br>based<br>ng.<br>punter                   |                    |                  |       | 8        | 3T           |      |                       |              |          |
|                   | * Note<br>r1se<br>on o<br>** Hig                              | End of<br>End of<br>End of<br>Servat.<br>bolow of<br>gravel of<br>ww   | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>jon whil<br>count du<br>or small                         | nses of (<br>(CL)<br>s expected<br>out 9½ l<br>e samplin<br>e to ence<br>boulder         | ed to<br>based<br>ng.<br>punter                   |                    | 13<br>1<br>51481 | 9     | Ĺ        | 3T           | α    |                       | 9-0          |          |
| 16<br>21<br>Date  | * Note<br>r1se<br>on o<br>** Hig                              | End of the sand the s | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>jon whil<br>count du<br>or small                         | nses of (<br>(CL)<br>(CL)<br>s expected<br>out 9½ 1<br>e samplin<br>e to ence<br>boulder | ed to<br>based<br>ng.<br>punter                   | PTHS WATER         |                  |       | -6-      | 3T           |      |                       | 9-0          |          |
| 21<br>Date<br>9-6 | <pre>rather bearin * Note rise on o ** Hig of The 11:00</pre> | End of<br>End of<br>Water<br>to dep<br>bservat<br>h blow<br>gravel<br>Sample<br>Deprin<br>21   | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>Jon whil<br>count du<br>or small<br>Count du<br>or small | nses of (<br>(CL)<br>s expects<br>out 3's' l<br>e samplin<br>e to enco<br>boulder        | ed to<br>based<br>ng.<br>bunter                   | THS LEVEL          | 1<br>START_      |       | -6-      | 3T           |      |                       | •            |          |
| 21<br>Date        | rather<br>bearin<br>* Note<br>rise<br>on o<br>** Hig<br>of    | End of<br>End of<br>Water<br>to dep<br>bserval<br>h blow o<br>gravel o   | some le<br>below 18<br>Boring<br>level i<br>th of ab<br>Jon whil<br>count du<br>or small                         | nses of (<br>(CL)<br>s expected<br>out 9½ l<br>e samplin<br>e to ence<br>boulder         | ed to<br>based<br>ng.<br>Dunter<br>TS<br>BARED DE | PTHS LEVEL         | 1<br>START_      |       | -6-      | 3T           |      |                       | •            |          |

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|                   | ור      | 1.101               |                 |                     |            | 1077800<br>207     |   | ~       |          |                 |        |         | 75-3 | 8M              |          |
|-------------------|---------|---------------------|-----------------|---------------------|------------|--------------------|---|---------|----------|-----------------|--------|---------|------|-----------------|----------|
| JOB NO<br>PROJEC  |         |                     | ER - MA         | KSHALL,             | ICAL SCALE |                    |   | LOG     | OFT      | EST             | BORING | 5 NO _  |      |                 |          |
| DEPTH             |         |                     |                 | N OF MATER          |            | 050000             |   | T T     | Î.       | SA              | MPLE   | L       | BORA | ORY TE          | STS      |
| IN<br>FEET        |         | E ELEVATIO          | N               |                     |            | GEOLOGIC<br>ORIGIN |   | N       | wi       | NO              | TYPE   | w       | D    | LL              | 0        |
|                   |         |                     |                 | CLAT AT             |            | Fi11               |   | +       | <b>+</b> | <del>{-</del> - | ss     |         |      | ٣L              | <u> </u> |
| 1                 | JAND, I | AY. a *             | gravel          | , see No            | dark       |                    |   | 6       | 1        | 1               | ISS .  |         | ł    |                 |          |
| 2                 |         |                     |                 | gravel<br>(CL)      |            | TOPSOIL            | L   | ÷       | 1        | 14              | 33     |         |      |                 |          |
|                   |         | LAY, a t.<br>medium | race of         | gravel,<br>(CL)     | grayish    |                    |   | i<br>17 |          | 3               | 55     |         | •    |                 |          |
| 4                 | orown,  | meartin             |                 | (06)                |            |                    |   | l í     | 1        |                 | 55     |         |      |                 | ļ        |
|                   |         |                     |                 | gravel,             |            |                    |   |         |          | 1               |        |         |      |                 | ĺ        |
|                   | mottle  | d, mediu            | un to ra        | the: sti            |            | ***                |   | 9       | i –      | 4               | SS     |         |      |                 |          |
| 1                 |         |                     |                 | (CL)                | ļ          | TILL               |   |         | 1        | ł               |        |         |      |                 |          |
|                   |         |                     |                 |                     |            |                    |   | 1       |          |                 |        |         |      |                 |          |
|                   |         |                     |                 |                     |            |                    |   | 11      |          | 5               | ss     | 21      |      | <u>30</u>       |          |
|                   |         |                     |                 |                     |            |                    |   |         | T        | 6               | 3T     |         |      | 18              |          |
|                   |         |                     |                 |                     |            |                    |   | 1       |          | 7               | 3T*    |         |      |                 |          |
|                   |         |                     |                 |                     |            |                    |   | 12      | ļ        | 8               | ss     |         | [    |                 |          |
|                   |         |                     |                 |                     |            |                    |   | 1       |          | 1               |        | ļ       | .    |                 |          |
| 12                |         | ~                   |                 | · · · ·             | · · ·      |                    |   |         | İ        |                 |        |         |      |                 | [        |
|                   |         |                     |                 | gravel,<br>ther sti |            |                    |   | 1 12    | 1        | 9               | ss     |         |      |                 |          |
|                   | and of  | own mott            |                 | Cher Str<br>(CL)    |            |                    |   |         |          | [               |        |         |      |                 | İ.       |
|                   |         |                     |                 | -,                  |            |                    |   | 1       | 1        | }               |        |         | 1    |                 |          |
| • /               |         |                     |                 |                     |            |                    |   | 10      |          | 1.0             | ee     | 10      |      | 31              |          |
| 16                | SANDY   |                     | }. <b>**</b> !# | gravel,             | GTAV       |                    |   | 12      | 1        | 10              | 55     | 18      | Ì    | 16              |          |
| i                 | rather  |                     |                 | graver,<br>(LL)     |            | )                  |   | 1       |          |                 | j      |         |      |                 |          |
|                   |         |                     |                 |                     |            |                    |   |         |          | 1               | ļ      |         |      |                 |          |
|                   |         |                     |                 |                     |            | ĺ                  |   | 1       |          | 1               | j l    |         | }    |                 |          |
|                   |         |                     |                 |                     |            |                    |   | i       | į        | ļ               |        |         |      |                 |          |
|                   |         |                     |                 |                     |            | ľ                  |   | 12      | ł        | 11              | 85     | 15      |      | $\frac{27}{15}$ |          |
|                   |         |                     |                 |                     |            |                    |   | 1       | 1        | ĺ               | 1      |         |      | 12              |          |
| 22                |         | <br>1 m.e           |                 |                     |            |                    | •   | ł       |          | 1               |        |         |      |                 | 1        |
|                   |         | End of              | <u>อกา เปล่</u> |                     |            | j                  |   | ;       | 1        | ļ               | }      |         |      |                 | 1        |
|                   |         |                     |                 |                     |            |                    |   | 1       | i        | ļ               |        |         |      |                 |          |
|                   |         |                     |                 | e obtain            |            |                    |   | i       | 1        | ļ               |        |         |      |                 |          |
| 1                 | from    | adjacor             | nt secon        | dar) bo             | ring       |                    |   | İ       |          | ł               |        |         | l    |                 | ł        |
|                   | Note #  | 1. brow             | unish er        | az                  |            |                    |   |         | 1        |                 |        | ł       | 1    |                 |          |
|                   |         |                     | •               |                     |            |                    |   | i       | İ        | !               |        |         |      |                 | ł        |
| 1                 |         |                     |                 |                     | i          |                    |   | 1       | 1        |                 |        |         | 1    |                 |          |
| 1                 |         |                     |                 |                     |            |                    |   | 1       |          | 1               |        |         |      |                 |          |
| I.                |         |                     |                 |                     | I          |                    |   | 1       | 1        |                 |        |         |      |                 |          |
| ı                 |         |                     |                 |                     |            |                    |   | }       | ļ        |                 |        |         |      |                 | ł        |
|                   |         |                     |                 |                     |            |                    |   | l       |          |                 | ļ      |         | l    |                 | l        |
| ]                 |         |                     |                 |                     |            |                    |   | START   | 9-       | 4-7             | L<br>S |         |      | 9-4             | - 75     |
|                   |         | SAMPLED<br>DEPTH    |                 | Y                   | T          | WAT                | EF  | <b></b> | -        |                 | SA 0   |         |      | 7               | 0:1      |
| DATE              | TIME    |                     | CASING<br>DEPTH | CAVE IN<br>DEPTH    | BAILED DE  | LEV                |   | WETHOD  |          | 1 1             | JAU    |         | 123  |                 | 0.1      |
| <u>9-4</u><br>9-4 | 10:10   | <u>22'</u><br>22'   | 1951<br>None    | 22'                 | 10<br>10   | No1                |   | ┨────   |          |                 |        | <u></u> |      | <u>.</u>        |          |
| 9-5               | 12:05   | 22'                 | None            | 11'                 | 10         |                    | <u>, , , , , , , , , , , , , , , , , , , </u> | 1       |          |                 |        |         |      |                 |          |
|                   | 1       |                     |                 |                     |            |                    |   |         |          |                 | xedo;  |         |      |                 |          |

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|---------------------|----------------------------|------------------------------|-------------------------------|------------------------------|----------------|------------------------|------------------|--------|----------|----------------|----------|----------------|--------------|------------------|
| JOB NO              | ne                         | 1791<br>הגרמת הישר           | VER . N                       | VERT                         | MI NNESO       | $\frac{1'' - 4'}{T_A}$ |                  | 3 of 1 | 651      | BORIN          | NO .     | , <u>,</u> , , | -9M          |                  |
| PROJEC              | T NL                       |                              | DESCRIPTIO                    |                              |                | 14                     |                  |        |          |                | r        |                |              |                  |
| DEPTH<br>IN<br>FEET | <b>-</b>                   |                              |                               | NOFMATER                     | IAL            | GEOLOGIC<br>ORIGIN     |                  |        | <u> </u> | MPLE           |          | T              | LURY TI      | T                |
| FEET                | •                          | ELEVATIO                     |                               |                              |                |                        | N                | WL     | NO       | TYPE           | <b>*</b> | D              | PL           | Qu               |
|                     | MEDIUM                     | FAT CLA                      | N, blac                       | k, mediu<br>(CH)             |                | TOPSOIL                | 8                |        | 1        | SS             |          |                | 1            | Ì                |
| 2                   |                            |                              | trace of<br>rather            |                              |                |                        | 10               |        | 2        | ss             |          |                |              |                  |
| 4 -                 | SANDY<br>and 11<br>medium  | ght gra)                     | little<br>ish bro             | gravel,                      | brown<br>ed,   | 11LL                   |                  | -      | 3        | 55             |          |                |              |                  |
|                     |                            |                              |                               |                              |                |                        | 7                |        | 4        | 55             |          |                |              |                  |
| 10                  | mottle                     |                              | little<br>er stiff            |                              |                |                        | 9                |        | 5        | 55             |          |                |              | м"А.             |
| 115                 | LEAN C<br>at 12'<br>rather | LAY, 3 1<br>, brown<br>stiff | irtle g<br>and gr             | iavel, a<br>aj motil<br>(CL) | boulder<br>ed, |                        | 14               |        | 6        | 55             |          |                |              | ;<br>;<br>;      |
| 137                 | rather                     | stiff,                       | little<br>some le<br>below 15 | nses of                      | water-         |                        | 13               |        | 7        | 55             |          |                |              |                  |
|                     |                            |                              |                               |                              |                | :                      |                  |        | 8        | ;<br>}.54<br>} | 17       |                | 28<br>16     | 1                |
|                     |                            |                              |                               |                              |                |                        |                  |        | 9        | 3T             |          |                |              |                  |
| 21 -                |                            |                              |                               |                              |                |                        | <u>1</u> 4       | í      | 10       | 55             |          |                |              |                  |
|                     |                            | LAU UI                       | f Boring                      |                              |                |                        | :<br>:<br>:<br>; |        | 1        | 1              |          |                |              |                  |
|                     | * wate:                    | rbearing                     | sand a                        | t about<br>(CL-              |                |                        |                  |        |          |                |          |                |              | -<br>-<br>-<br>- |
|                     |                            |                              |                               |                              |                |                        |                  |        |          |                |          |                |              |                  |
|                     |                            | WA                           | TER LEVEL N                   | EASURENEN                    | 175            |                        | START            | 9-4    | - 5      |                | 0        |                | 9-4          | - 75             |
| DATE                | TIME                       | SAMPLED<br>DEPTH             | CASING<br>DEPTH               | CAVE IN<br>DEPTH             | BARED DE       |                        | METHO            | _      |          | se a           |          | 181.           | 1 <u>, 3</u> | : 50             |
| 9-4                 | 8:50                       | 21'                          | 195'                          |                              | 10             | 174                    |                  |        |          |                |          |                |              |                  |
| G. A                | 9:00                       |                              | None                          | 1551                         | ło             | None                   |                  |        |          |                |          |                |              |                  |
| <u>9-4</u><br>9-5   | 12:05                      | 21 '                         | None                          | 11'                          | 10             | 8'                     | <b>—</b> ——      |        |          |                |          |                |              |                  |

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|            | 217   | 91   |                     | VERTIC  |           | 1" =          | 4'                | <b></b> 10G | OF T |             | 00000           | NC   | 75-4     | OM              |     |
|------------|---|--|---------------------|---|-----------|---------------|-------------------|-------------|------|-------------|-----------------|------|----------|-----------------|-----|
| NOB NC     |   | WOOD RIV                                       | ER - MA             | RSHALL. N                                       | INNESOT   |               |                   | LOG         | OFI  | ESTE        | IORING          | NO _ | <u> </u> |                 |     |
| EPTH       |   |  | DESCRIPTIO          | N OF MATERIA                                    | NL I      | 650           | LOGIC             |             | T    | SAI         | MPLE            | ٤A   | BORAT    | ORY TE          | STS |
| FEET       |   | ELEVATIO                                       | N                   | ·····   |           | OR            | IGIN              | N           | WL   | NO          | TYPE            | w    | D        |                 | O.  |
|            | MEDIUM  | FAT CL   | Y, blac             | k, rathen<br>(CH)                               | r stiff   | TOP           | SOIL              | 9           |      | 1           | ss              |      |          |                 |     |
| 2          | gray m  |  | rather              | nish gra)<br>stiff to<br>(CH 1<br>CH)           |           | FII<br>ALLU   |                   | 12          |      | 2           | SS              | 23   |          | <u>55</u><br>33 |     |
| 6          |   |  |                     | ·   |           |               |                   | 4           | Y    | 3           | SS              | 30   |          | $\frac{47}{23}$ |     |
|            | and a<br>a few<br>below   | little p<br>lenses d<br>8 <sup>1</sup> 2', a p | ray mot<br>of witer | gravel, t<br>tled, med<br>bearing s<br>e shells | lium,     | MIXEI<br>ALLU |                   | 5           |      | 4<br>5<br>6 | 3T<br>3T*<br>SS | 21   |          | <u>29</u><br>17 |     |
|            | above   | ? <b>`</b> .'                                  |                     | (CL)  |           |               |                   | 6           |      | 7           | SS              | 31   |          | <u>39</u><br>21 |     |
| 24         | boulde  | rs, gra)                                       | , rathe             | gravel, a<br>r stiff t                          | to 0      | TI            | LL                | 10          |      | 8           | SS              | 17   |          | 25<br>16        |     |
|            | stiff,<br>sand  | some le  | inses of            | waterbea<br>(CL)                                | aring     |               |                   | 10          |      | 9           | SS              |      |          |                 |     |
| 21         | 4   | End of   | Boring              | ···· · · ·                                      |           |               |                   | 19          |      | 10          | કડ              | 18   |          | 28<br>16        |     |
|            |   |  |                     | es obtair<br>dary bori                          |           |               |                   |             |      |             |                 |      |          |                 |     |
|            | <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> |  |                     | MEASUME MEMT                                    | rs        |               |                   | START_      |      | -           |                 |      |          | 9-3             |     |
|            | TIME  | SAMPLED<br>DEPTH                               | CASING<br>DEPTH     | CAVE IN<br>DEPTH                                | BAILED DE | PTHS          | WATER LEVEL       | METHOD      | 3    | h H         | <u>5A Q'</u>    | - 1  | 941      | <u>ه ه</u>      | ;20 |
| <u>9-3</u> | 5:20  | 21'  | 194'                | L   | 10        |               | 16'               | ┫           |      |             |                 |      |          |                 |     |
| 9-3        | 5:35  | 21'  | None<br>None        | <u>11'</u><br>9'5'                              | 10        | +             | <u>94'</u><br>54' | -1          |      |             |                 |      |          |                 |     |
| 9-5        | 112:15  |  |                     |   | to        |               |                   |             |      |             |                 |      |          |                 |     |

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|          |              |   | soil e                                |      |                    |         |      |       |             |      |        |                 |                    |
|----------|--------------|---|---------------------------------------|------|--------------------|---------|------|-------|-------------|------|--------|-----------------|--------------------|
| JOB NO   | 21791        |   | VERTICAL SC                           | CALE | <u>- 4'</u>        |         | OF T | EST ( | BORING      | NO _ | 75-4   | IM_             |                    |
| PROJEC   |              | RIVER - MAR.                              | HALL MINNE                            |      |                    |         |      |       |             |      |        |                 |                    |
| DEPTH    |              |   | OF MATERIAL                           | - T  | GEOLOGIC           |         |      | SA    | MPLE        | LA   | BORAT  | ORY T           | STS                |
| FEET     |              | ATION                                     |                                       |      | GEOLOGIC<br>ORIGIN | N       | WL   | NO    | TYPE        | w    | D      |                 | Qu                 |
|          | MEDIUM FAT   | CLAY, black                               | c, medium<br>Cfto                     |      | TOPSOIL            | 5       |      | 1     | ss          |      |        |                 |                    |
| 2        | and light g  | grayish beri                              | ravel, brow<br>on mottled,            |      | TILL               | 9       |      | 2     | ss          |      |        |                 |                    |
|          |              |   | Cucaring sa (CL)                      |      |                    | 7       | T    | 3     | ss          | 19   |        | $\frac{35}{18}$ |                    |
| 85       |              |   |                                       |      |                    | 17      |      | 4     | SS          |      |        |                 |                    |
|          |              | grained, a<br>own, waterbe                | trace of<br>earing, medi<br>:SP-SM)   | un   | COARSE<br>ALLUVIUM | 13      |      | 5     | ss          |      |        |                 | м <b>.</b> /       |
| 12       |              |   | g:ained, a<br>h brown, wat<br>(SP-SM) | er-  |                    | 17      |      | 6     | ss          |      |        |                 | м. <i>.</i> /      |
| *413     | gravel, gra  | grained, a<br>ay, waterbea<br>of silty sa | iring, dense                          | , a  |                    | 21      |      | 7     | ss          |      |        |                 | м.                 |
| 19<br>21 | rather still | ff, a lense                               | gravel, gray<br>of sand at            |      | TILL               | 9       |      | 8     | 55          |      |        |                 |                    |
|          | Er           | nd of Boring                              | ŝ                                     |      |                    |         |      |       |             |      |        |                 |                    |
|          |              |   |                                       |      |                    |         | 1    | 1     | 1           |      |        | ļ               | ļ                  |
|          |              |   |                                       |      |                    |         |      |       |             |      |        |                 |                    |
|          |              |   |                                       |      |                    |         | 9.   | 3-    | 75          |      |        | 9.5             | <b>1</b> -75       |
|          |              | WATER LEVEL N                             | (A.4.)N                               |      |                    | START . | _    | .3-   |             |      | MPLETE | 1               |                    |
| DATE     | THATE SAMP   | LED CASING<br>TH DEPTH                    | (A.4.)N                               |      |                    | START.  | _    |       | 75<br>5A 0' |      |        | 1               | <u>3-75</u><br>:00 |
| 9-3      | 4:00 21      | LED CASING<br>TH DEPTH                    | PAVE IN<br>DEFTH BAI                  | to   | HS LEVEL           | 1       | _    |       |             |      |        | 1               | 3-75               |
|          |              | TH CASING<br>TH DEPTH<br>1941<br>None     | FASE IN                               |      | HS LEVEL           | 1       | _    |       |             |      |        | 1               |                    |

**(**)

| JOB NO<br>PROJECT<br>DEPTH<br>IN<br>FEET<br>15<br>2 |               |  |                         |                         | CAL SCALE  | !'' =    | 4'                    |          |     |      |        |      | 75-1  | 1 2M     |             |
|---|---------------|--|-------------------------|-------------------------|------------|----------|-----------------------|----------|-----|------|--------|------|-------|----------|-------------|
| ПЕРТН<br>(N<br>FEET                                 |               |  |                         | липьь. М                | INNESOTA   |          | <u> </u>              | LOG      | OFT | ESTE | IORING | NO   | / 3-4 |          |             |
| 14  | <u> </u>      |  | DESCRIPTION             |                         |            |          |                       | T        |     | SAI  | MPLE   | LA   | BORA  | TORY T   | ESTS        |
| 15 -  | <u> </u>      | ELEVATIO   | N                       |                         |            | 912<br>0 | ดแอ <b>ตต</b><br>ศาสท | N        | WL  |      | TYPE   |      | D     | LL<br>PL | Qu          |
| - 1   | TFAN CI       | AY. dar  | k grayis                | h brown                 | med-       |          |                       | <u>+</u> |     |      |        | ┢──┤ |       | PL       | <u>}</u>    |
| - 1   | ium           |  | •                       | (CL)                    | 1          | TO       | PSOIL                 | 7        |     | 1    | ss     |      |       |          |             |
| - ,   | LEAN C        | AY, a t  | race of                 | graveT,                 | See        |          |                       | •        | 1   | 2    | ss     |      |       | {        | 1           |
|   |               |  | little,                 |                         |            | T        | I L L                 | 7        |     |      | ss     |      |       | ļ        |             |
|   | mottle        | d, medin   | m to rat                | her sti                 | ff         |          |                       | 1        |     |      | 33     |      |       |          |             |
|   |               |  |                         | (CL)                    | 1          |          |                       | 1        |     |      |        |      |       |          |             |
|   |               |  |                         | 10.1                    | ļ          |          |                       | 7        |     | 4    | ss     |      |       | {        |             |
|   |               |  |                         |                         | 1          |          |                       |          |     | 5    | 3T     |      |       | 1        |             |
|   |               |  |                         |                         | Ì          |          |                       | ł        |     | -    | 3T*    |      |       | }        |             |
|   |               |  |                         |                         |            |          |                       | 9        |     | 7    | ss     |      |       | 1        |             |
|   |               |  |                         |                         | 1          |          |                       | 1        |     |      |        |      |       | ł        |             |
|   |               |  |                         |                         | 1          |          |                       | 10       | Y   | 8    | ss     |      |       | 1        | }           |
|   |               |  |                         |                         | i          |          |                       | i        |     | J    |        |      |       | }        |             |
| 1 3   |               |  |                         |                         | †          |          |                       | 1        |     |      |        |      |       |          |             |
| 125   | SANDY         | TAY  | little ;<br>enses of    | ravel,                  | gray,      |          |                       | 17       |     | 9    | ss     |      |       | 1        |             |
| 14  | below         | 13' I  | GU262 01                |                         | Janu       |          |                       | <b>•</b> |     | -    |        |      |       | 1        | 1           |
| -   |               |  | ined, a                 |                         |            |          |                       | ł        |     | 1    |        | }    |       | Ì        |             |
|   |               |  | waterb<br>of sandy      |                         |            |          | DARSE<br>LUVIUM       | 19       |     | 10   | S5     |      |       |          | M.          |
|   | 151.1         | ienses (   | a sanay                 | SF i                    |            |          |                       | i –      | 1   |      |        |      |       | {        | 1           |
| 20 21   | • Bro<br>rat: | <u>stiff</u><br>End of<br>wn and b<br>her stif<br>wall tub | Bor.ng<br>brownish<br>f | giay, m<br>(CL)<br>(CL) | witled,    | <u> </u> | <u>111</u>            | 13       |     | 11   | SS     |      |       |          |             |
|   | 11010         | 80,80 <b>7</b> 1   | in seran                |                         | - ···P     |          |                       | 1        |     | 1    |        |      |       |          | }           |
| !   |               |  |                         |                         | į          |          |                       | 1        |     |      |        |      |       |          | 1           |
|   |               |  |                         |                         | 1          |          |                       |          |     |      |        |      |       |          |             |
|   |               |  |                         |                         |            |          |                       | 1        |     |      |        |      |       |          |             |
| <u>i</u>  |               |  |                         |                         |            |          |                       | L        | L   |      |        |      |       |          | L           |
| ······································              |               |  | TER LEVEL N             | EABURENEN               | TS         |          | <b>.</b>              | START_   | 9-  | 3-7  | 5      | 00   | MPLET | 9-3      | 5-75        |
| DATE  | THAE          | SAMPLED<br>DEPTH   | CASING<br>DEPTH         | CAVE IN<br>DEPTH        | BAILED DEP | THS      | WATER<br>LEVEL        | METHOD   | 34  | HS   | A 0'   | - 19 | 14'   |          | <u>2:35</u> |
| 9-3   | 2:35          | 21'  | 194'                    |                         | 10         |          | 16'                   |          |     |      |        |      |       |          |             |
| _ <b>9-3_</b><br>9-5                                | 2:45          | 21'  | None<br>None            | <u>14'</u><br>11'       | 10         |          | 13'                   | 1        |     |      |        |      |       |          | _           |
| _د-و  | 146162        | <b>6</b> A   |                         | **                      | 10         |          |                       | CREW CH  | HEF | He   | redo   |      |       |          |             |

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|   |  | GENERAL NOTES  |  |   |
|---|--|--|--|---|
| DRIL  | LING & SAMPLING SYMBOLS  |  | LABORATORY TE  | ST SYMBOLS  |
| SYNBOL  | DEFINITION   | SYMBOL   | DEFINITION   |   |
| C S   | Continuous Sampling  | w  |  | percent of dry weight                               |
| PD  | 2-3 8" Pipe Drill  | D  | Dry density pound  |   |
| C 0   | Cleanout Tube  | I,L. PL  |  | timits determined in<br>STM D 423 and D 424         |
| 3% HSA<br>4 FA                                | 3'a'' ID Hollow Stem Auger<br>4'' Diameter Flight Auger  | Qu   |  | ssive strength-pounds per                           |
| 6 FA  | 6" Diameter Flight Auger   |  | square foot in acc   | ordance with ASTMD 2166-6                           |
| 2'1 C   | 2':" Casing  |  | Additional insertions  | in Ou column  |
| 40  | 4" Casing<br>Dritting Mud  | _  |  |   |
| DM<br>J.W.                                    | Jet Water  | Pq<br>Is   | Torvane reading-to   | ng-tons/square foot                                 |
| нА  | Hand Auger   | 6  | Specific gravity -   |   |
| NXC   | Size NX Casing   | SL   | Shrinkage limit - A  |   |
| BXC   | Size BX Casing<br>Size AX Casing   | pH   | Hydrogen (on cont<br>Organic content-c   |   |
| SS  | 2" O.D. Split Spoon Sample   | 0<br>M A *   | Grain size analys  |   |
| 27  | 2" Thin Wall Tube Sample   | C•   | One dimensional of   |   |
| 31  | 3" Thin Wail Tube Sample   | üc•  | Triaxial compress  | ion   |
|   |  | *See attach  | ed data sheet and or gra   | ph  |
|   |  | WATER LEVEL  |  |   |
|   |  | SYMBOL - 🔽   |  |   |
|   | Water levels shown on the born   | ng logs are the levels m   | easured in the borings a   | t the time  |
|   | and under the conditions indi  | cated. In sand, the ind  | icated levels can be c   | onsidered   |
|   | reliable ground water levels,<br>water level within the normal r   | In clay soil, it is not p  | possible to determine t  | ne ground<br>Ire lenses                             |
|   | or layers of more pervicus wat   | erbearing soil are prese   | nt and then a long perio   | id of time  |
|   | may be necessary to reach equ  | ilibrium. Therefore the p  | nosition of the water lev  | el Symbol   |
|   | for cohesive or mixed texture table. The available water level   | soils may not indicate t   | he true level of the gro   | und wäter   |
|   |  |  |  |   |
|   | · · · · · · · · · · ·  | SCRIPTIVE TERMINOL   |  |   |
|   | DENSITY  | SCRIPTIVE TERMINOL   | OGY<br>CONSIS  | TENCY   |
|   | · · · · · · · · · · · · ·  | SCRIPTIVE TERMINOL   | CONSIS   | "N" VALUE<br>0-4                                    |
|   | DENSITY<br>RM ''N'' VALUE<br>Joose 0.4   | SCRIPTIVE TERMINOL   | CONSIS<br>TERM<br>Soft<br>Medium   | "N" VALUE<br>0-4<br>5-8                             |
| Loos  | DENSITY           NM         ''N''         VALUE           / loose         0.4           ie         5:8           um Dense         9.15  | SCRIPTIVE TERMINOL   | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff   | "N" VALUE<br>0-4<br>5-8<br>9-15                     |
| Ven<br>Lone<br>Med<br>Dens                    | DENSITY<br>Imm ''N'' VALUE<br>/ loose 0 4<br>ie 5:8<br>ium Dense 9 15<br>ie 16 30  | SCRIPTIVE TERMINOL   | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff  | ""N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30           |
| Ven<br>Lone<br>Med<br>Dens                    | DENSITY           NM         ''N'' VALUE           / loose         0.4           e         5.8           um Dense         9.15   | SCRIPTIVE TERMINOL   | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff   | "N" VALUE<br>0-4<br>5-8<br>9-15                     |
| Very<br>Lone<br>Med<br>Dens<br>Very           | DENSITY           RM         ''N'' VALUE           r Joose         0.4           e         5.8           num Dense         9.15           se         16.30           Dense         Over 30   |  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Ma ''N'' VALUE<br>r Joose 0 4<br>le 5-8<br>Jum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo   | t of a 140 pound hammer  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>MM ''N'' VALUE<br>/ loose 0.4<br>le 5.8<br>rum Dense 9.15<br>le 16.30<br>Dense Over 30<br>d''N'' Penetration Blows per foo  | t of a 140 pound hammer  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Man ''N'' VALUE<br>r Joose 0 4<br>le 5-8<br>Jum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo  | t of a 140 pound hammer  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0-5%   | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>MM ''N'' VALUE<br>r loose 0 4<br>le 5.8<br>Jum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM   | t of a 140 pound hammer  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0-5%<br>5-15%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>IM ''N'' VALUE<br>r laose 0 4<br>le 5.8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace  | t of a 140 pound hammer  | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0.5%<br>5-15%<br>15-30%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>MM ''N'' VALUE<br>/ loose 0 4<br>e 5.8<br>ium Dense 9 15<br>ie 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little   | t of a 140 pound hammer<br>RELATIVE PROPORTIO                    | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0-5%<br>5-15%<br>15:30%<br>30:50%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>MM ''N'' VALUE<br>/ loose 0 4<br>le 5.8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some  | t of a 140 pound hammer<br>RELATIVE PROPORTION                   | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0.5%<br>5-15%<br>15-30%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>MM ''N'' VALUE<br>/ loose 0 4<br>le 5.8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some  | t of a 140 pound hammer<br>RELATIVE PROPORTION                   | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0-5%<br>5-15%<br>15:30%<br>30:50%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>IM ''N'' VALUE<br>r loose 0 4<br>le 5.8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel  | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-15%<br>15:30%<br>30:50%   | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Im ''N'' VALUE<br>r loose 0 4<br>ie 5.8<br>ium Dense 9 15<br>ie 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse  | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0-5%<br>5-15%<br>15-30%<br>30-50%   | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Imm ''N'' VALUE<br>/ Joose 0 4<br>e 5-8<br>jum Dense 9 15<br>ise 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse<br>Fine   | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-15%<br>15:30%<br>30:50%   | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>M ''N'' VALUE<br>r loose 0 4<br>le 5-8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse<br>Fine<br>Sand   | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>0.5%<br>5-15%<br>15-30%<br>30-50%  | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>IM ''N'' VALUE<br>r Joose 0 4<br>ie 5.8<br>ium Dense 9 15<br>ie 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse<br>Fine<br>Sand<br>Coarse | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>C-5%<br>5-15%<br>15-30%<br>30-50%   | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>M ''N'' VALUE<br>r loose 0 4<br>le 5-8<br>lum Dense 9 15<br>le 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse<br>Fine<br>Sand   | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-15%<br>5-15%<br>15:30%<br>30:50%<br>Over 3''<br>Na'' 3''<br>R4-%''                              | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Imm ''N'' VALUE<br>/ Joose 0 4<br>e 5-8<br>ium Dense 9 15<br>e 16 30<br>Dense Over 30<br>d ''N'' Penetration Blows per foo<br>TERM<br>Trace<br>A Little<br>Some<br>With<br>Boulders<br>Gravel<br>Coarse<br>Fine<br>Send<br>Coarse<br>Medium                             | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-15%<br>15:30%<br>30:50%<br>Over 3''<br>N4-10<br>#10-#40<br>#40-#200<br>Determined by plasticity | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Imm ''N'' VALUE<br>/ loose 0 4<br>e 5.8<br>ium Dense 9 15<br>ie 16 30<br>Dense Over 30<br>TERM<br>Trace<br>A Little<br>Soulders<br>Gravel<br>Coarse<br>Fine<br>Sand<br>Coarse<br>Medium<br>Fine<br>Silt and Clay  | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling J0 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-115%<br>15-30%<br>30-50%<br>Over 3''<br>%''-3''<br>#4-#10<br>#40-#200                           | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |
| Ven<br>Loos<br>Med<br>Dens<br>Very<br>Stander | DENSITY<br>Imm ''N'' VALUE<br>/ loose 0 4<br>e 5.8<br>ium Dense 9 15<br>ie 16 30<br>Dense Over 30<br>TERM<br>Trace<br>A Little<br>Soulders<br>Gravel<br>Coarse<br>Fine<br>Sand<br>Coarse<br>Medium<br>Fine<br>Silt and Clay  | t of a 140 pound hammer<br>RELATIVE PROPORTION<br>PARTICLE SIZES | CONSIS<br>TERM<br>Soft<br>Medium<br>Rather Stiff<br>Stiff<br>Very Stiff<br>falling 30 inches on a 2<br>NS<br>RANGE<br>(1-5%<br>5-15%<br>15:30%<br>30:50%<br>Over 3''<br>N4-10<br>#10-#40<br>#40-#200<br>Determined by plasticity | "N" VALUE<br>0-4<br>5-8<br>9-15<br>16-30<br>Over 30 |

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|  |   |                    | (  | ASTM Designation: D 2  | S FOR ENGINEERING PURPOSES<br>1487 – 69 AND D 2488 – 69<br>assification System)   |
|--|---|--------------------|--|--|---|
| Ma   | or division   | ons                | Group  | Typicat names  | Classification criteria   |
|  | e ct  | gravels            | GW   | Well-graded gravels and<br>gravel-sand mixtures little<br>or no fines                                      | $C_{U} = \frac{D60}{D10} \text{ greater than 4}$ $C_{Z} = \frac{(D30)^{2}}{D10 \times D60} \text{ between 1 and 3}$ $C_{Z} = \frac{(D30)^{2}}{D10 \times D60} \text{ between 1 and 3}$ Not meeting both criteria for GW |
|  | Gravels<br>more of coarse fraction<br>lined on No. 4 sieve  | Clean              | GP   | Poorly graded gravels and<br>gravel-sand mixtures, little<br>or no fines                                   |   |
| 00 steve   |   | Gravets with fines | GM   | Silty gravels, gravel-sand-<br>silt-mixtures   | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   |
| thed soils<br>ad on No. 2                              | Š   | 50g                | GС   | Clavey gravels, gravel<br>sand-clay mixtures   | 5      Atterberg limits above     Cations requiring use of dual symbols       6          7  |
| Coarse grained soils<br>50% retained on No. 200 sieve* | Sands<br>s of coarse fraction<br>No. 4 sieve<br>Clean sands | 5₩                 | Well graded sands and gra<br>velly sands little or no<br>fines | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |   |
| More then  |   | SP                 | Popriv graded sands and gravelly sands. Little or no fines     | C X 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  |   |
|  |   |                    | SM   | Silty sands, sand-silt mix<br>tures  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |
|  | More  | Sands w            | sc   | Clayey sands, sand-clay<br>mixtures  | Atterberg limits above<br>"A" line with P.,<br>greater than 7   |
|  | 5   | or tess            | ML   | Inorganic silts, very fine<br>sands, rock flour, silty or<br>clayey fine sands                             | Plasticity Chart<br>60<br>For classification of fine-grained<br>soils and fine fraction of coarse   |
| ţ  | Suits and clays   | 1 mit 50% o        | CL   | Inorganic clays of low to<br>medium plasticity, gravelly<br>clays, sandy clays, silty<br>clays, lean clays | 50 grained soils.<br>Atterberg Limits plotting in<br>hatched area are borderline<br>classifications requiring use of  |
| gramed soils<br>basses No. 200 sieve*                  | ū   | Liquid             | OL   | Organic silts and organic<br>silty clays of low plasticity   | x         40         dual symbols.           Equation of A-line         PI = 0.73 (LL = 20)           0         30  |
|  | 1   | 102 wett           | MH   | Inorganic silts, micaceous<br>or diatomaceous fine sands<br>or silts, elartic silts                        | £ 20  |
| Fine<br>50% or more                                    | Silts and clays<br>Liquid limit greater tha                 | СН                 | Inorganic clays of high<br>plasticity, fat clays               | 10<br>7<br>4<br>CL-ML<br>W ML and OL   |   |
|  | <u> </u>  |                    | он   | Organic clays of medium to<br>high plasticity  | 0 10 20 30 40 50 60 70 80 90 100  |
|  | Highiy<br>Brighiy<br>Brighio                                |                    | Pt   | Peet. muck and other highly<br>organic soils   | *Based on the material passing the 3 in. (76 mm) sieve.   |

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# DIVISION OF PLAN RESPONSIBILITIES

SECTION I

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SECTION I

### DIVISION OF PLAN

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### RESPONSIBILITIES -

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#### SECTION I

## DIVISION OF PLAN RESPONSIBILITIES

### INTRODUCTION

1. This section presents the details of project responsibilities and related cost apportionment between Federal and non-Federal agencies. The proposed improvements are principally for a single purpose, i.e. flood control, with minimal related recreation and aesthetic measures. Since the proposed recreational facilities and resulting benefits do not have a decisive influence on project feasibility, the recreation purpose and costs were considered incremental. Therefore, cost allocation between project purposes are not considered warranted. The apportionment of project costs, including appropriate engineering, design, supervision, and administrative costs under both existing legislation and the President's proposed cost-sharing policies, is shown in table I-1.

### COST APPORTIONMENT

#### FEDERAL

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2. The Federal government would design and construct the various features of the flood protection and recreation works. The work

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charged as a Federal cost includes that for all upstream and downstream reach levee and channel works, interior drainage works, and a maximum of three percent of the total construction cost for aesthetic mitigation-beautification measures. Federal cost sharing would also include approximately one-half the first costs of the

recreational trail system and project related picnicking facilities at Justice Park. The Federal Government also assumes the cost of this study. The total Federal first cost for both upstream and downstream reach improvements excluding costs of this study is estimated at \$2,008,800 based on existing cost-sharing legislation. However, applying the President's proposed cost-sharing policies would result in a total Federal first cost of \$1,745,100 as shown on table 1-1.

#### NON-FEDERAL

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3. The City of Marshall would be required to operate and maintain all project works and bear all costs of required lands, easements and rights-of-way required for construction and subsequent operation and maintenance of the project; all relocations and alterations to structures, roads, and utilities (except parts of utilities passing ov r, through, or under the protective works); and one-half the first costs of recreational facilities eligible for Federal cost sharing.

Appendix I I-2 -

|                              |                | Non-F                        | ederal                |             |
|------------------------------|----------------|------------------------------|-----------------------|-------------|
| Item                         | Federal        | State                        | City                  | Total       |
| Based on existing cost-shari | ng legislation | :                            |                       |             |
| Lands                        | -              | -                            | \$211,600             | \$211,600   |
| Relocations                  | -              | -                            | 52,400                | 52,400      |
| Channe 1s                    | \$738,600      | -                            | -                     | 738,600     |
| Levees                       | 171,800        | -                            | -                     | 171,800     |
| Overflow works               | 418,200        | -                            |                       | 418,200     |
| Interior drainage            | 184,000        | -                            | -                     | 184,000     |
| Recreation facilities        | 192,800        | -                            | 192,800               | 385,600     |
| Engineering, administration  | 303,400        | <u> </u>                     | 38,400 <sup>(1)</sup> | 341,800     |
| Total (existing legislation) | 2,008,800      | -                            | 495,200               | 2,504,000   |
| Based on President's propose | d cost-sharing | policy:                      |                       |             |
| Flood damage prevention      | \$1,332,500    | <b>\$8</b> 8,800             | \$355,300             | \$1,776,600 |
| Recreational facilities      | 173,500        | 19,300                       | 192,800               | 385,600     |
| Engineering, administration  | 2 39,100       | <u>17,100</u> <sup>(2)</sup> | <u>    85,600</u> (3) | 341,800     |
| Total (President's policy)   | 1,745,100      | 125,200                      | 633,700               | 2,504,000   |

(1) Includes 50 percent of the separable Engineering, Administration (E,A) cost (\$28,800) and 100 percent separable E,A relocations cost (\$9,600).

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(2) Includes 5 percent of total E,A.
(3) Includes 20 percent of flood damage prevention E,A cost (\$56,800) and 50 percent of recreational facility E,A cost (\$28,800).

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4. All maintenance and operation costs for the proposed project are assigned to non-Federal interests. The estimated annual charges, based on a 6-7/8 percent interest rate and a 50-year project life, are given in table 1-2 below.

#### Table 1-2 - Estimate of Annual Charges

| Federal   |                 |        |           |
|---|-----------------|--------|-----------|
| Interest and amortization (\$2,008,800 x 0,07132) |                 |        | \$143,270 |
| Non-Federal                                       |                 |        |           |
| Interest and amortization (\$495,200 x .07132)    | \$              | 35,320 |           |
| Operation and Maintenance                         | (Flood Control) | 6,300  |           |
|   | (Recreation)    | 2,700  |           |
| Total Non-Federal Charges                         |                 |        | 44,320    |
| TOTAL ANNUAL CHAP                                 | RGES            |        | \$187,590 |

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5. Prior to the start of construction and in accordance with Section 221 of the 1970 Flood Control Act of 1970, the City would be required to enter into a local cooperation agreement satisfactory to the Secretary of the Army, which would provide that the City will:

- Provide, without cost to the United States, all lands, easea. ments, and rights-of-way, including suitable areas for borrow and disposal of excavated material as determined by the Chief of Engineers, for construction, operation and maintenance of the project.
- b. Hold and save the United States free from damages that may result from construction and maintenance of the project, not including damages which are due to the fault or negligence of the United States or its contractors.
- C. Maintain and operate the project after completion in accordance with regulations prescribed by the Chief of Engineers.

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- d. Accomplish without cost to the United States all relocations and alterations of buildings (except nonstructural measures), transportation facilities, storm and sanitary sewer systems, public and private utilities, local betterments, drainage facilities, and other structures and improvements made necessary by construction of the recommended plan, as determined by the Chief of Engineers, excluding facilities necessary for the normal interception and disposal of local interior drainage at the line of protection.
- e. Prescribe and enforce regulations to prevent obstructions or encroachment on channels, floodway areas, and ponding areas which would reduce their flood-carrying capacity or hinder maintenance and operation.

- f. Provide a cash contribution for recreation equal to 50 percent of the final separable cost allocated to this function less a credit for the value of lands, easements, rights-of-way, alterations, and relocations furnished therefore.
- 8. Publicize flood plain information in the areas concerned and provide this information to zoning and other regulatory agencies for their guidance and leadership in preventing unwise future development in the flood plain and in adopting such regulations as may be necessary to insure compatibility between future development and protection levels provided by the project.
- h. In acquiring lands, easements, and rights-of-way for construction of the project, the local sponsor will comply with the applicable provisions of the "Uniform Relocation Assistance and Real Property Acquisition Policies Act of 1970", Public Law 91-646, approved 2 January 1971.

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SECTION J

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## EXECUTIVE ORDERS 11988 AND 11990

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#### SECTION J EXECUTIVE ORDERS 11968 AND 11990

#### INTRODUCTION

1. This section describes in detail the evaluation of an alternative levee alignment formulated to address compliance with Executive Order 11988, pertaining to direct or indirect inducement of flood plain development, and Executive Order 11990, pertaining to the protection of wetlands.

#### EXECUTIVE ORDER 11988

#### OBJECTIVE

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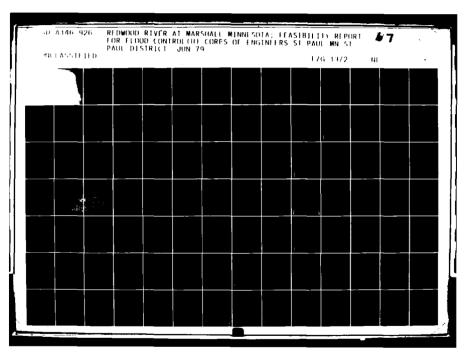
2. The objective of Executive Order 11988 is to avoid to the extent possible the long- and short-term adverse impacts associated with occupancy and modification of floodplains and to avoid direct and indirect support of floodplain development wherever there is a practicable alternative. The order requires Federal agencies to provide leadership and take action to:

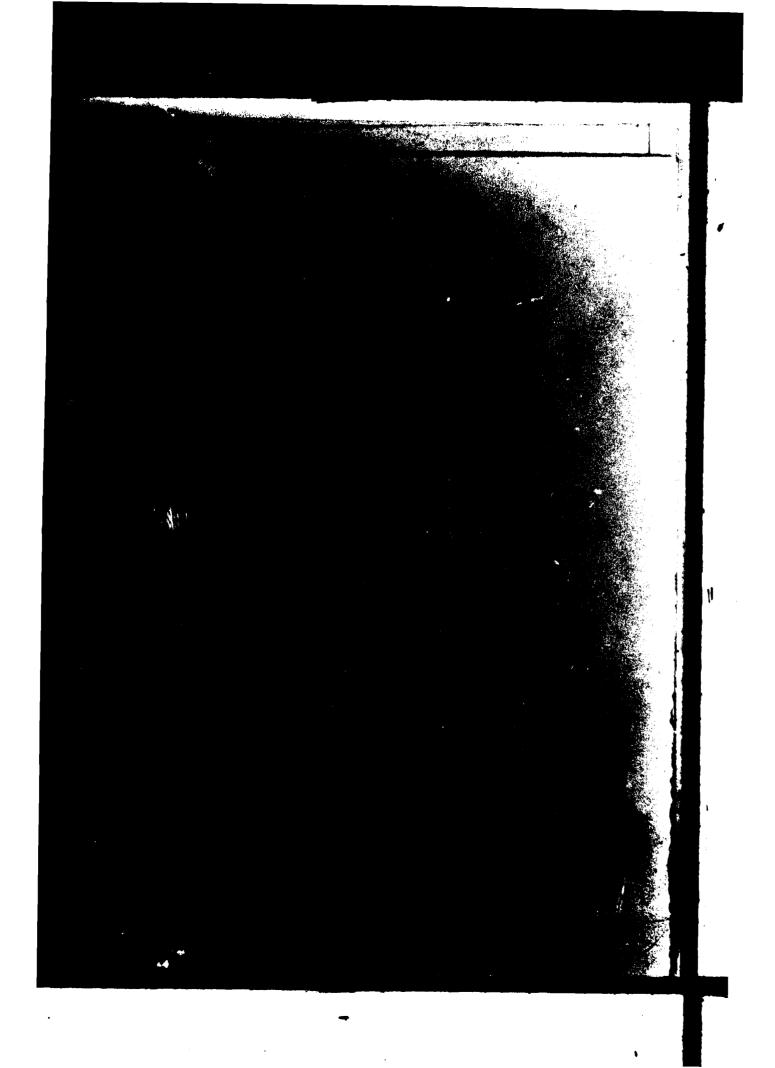
a. Avoid the base floodplain unless it is the only practicable alternative.

b. Reduce the hazard and risk of flood loss.

c. Minimize the impact of floods on human safety, health and welfar.

d. Restore and preserve the natural and beneficial floodplain values. Direct support of floodplain development is an action in the floodplain that encourages, allows, serves, or otherwise facilitates additional floodplain development. An example of direct support would be provision of flood protection measures to undeveloped or underutilized floodplain lands for the purpose of permitting future development and growth.





#### DESCRIPTION OF THE AREAS AFFECTED

3. The existing diversion channel at Marshall is unable to adequately protect the city due to insufficient channel capacity both upstream and downstream of the diversion structure. Upstream, should a flood greater than or equal to the 1969 flood occur, overflows would bypass the diversion channel and rejoin the Redwood River in Marshall, causing damages to developing residential areas and the central city. Downstream of the diversion channel, considerable development has occurred that is not protected by the existing project. The majority of this development consists of Southwest State University and student and other local housing.

4. The selected project modifications upstream and downstream of the diversion channel consist of channel widening, straightening, and bank reshaping measures; levees; an overflow diversion structure with appurtenant control and outlet works; interior drainage works; aesthetic measures; recreation facilities; required relocations; and revegetation of all disturbed areas. The selected plan would provide 133-year protection for the city of Marshall.

#### UPSTREAM REACH

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5. <u>Problem area</u>. - The area of concern for the upstream reach is located upstream of the existing diversion structure and bypass channel between State Highway 23 and the Redwood River. This area is divided by County Highway 7 which crosses the Redwood River about 1,000 feet above the existing flood diversion structure. The existing project was designed to allow a near natural division of high flows south across Highway 23 to the Cottonwood River basin with the balance flowing down the Redwood River to the diversion structure. The flood of 1969 did not overflow as expected. About 2,500 cfs overflowed into the Cottonwood River basin in the vicinity of the Highway 23 wayside park. Additional overbank flow entered the area from overbank areas downstream of the park and flowed southeast toward the junction of County Highway 7 and State Highway 23.

This latter overflow threatened to overtop County Highway 7, reenter a residential area, and flow through the Marshall business district at a point downstream of the existing diversion structure. To prevent this overflow, County Highway 7 was temporarily raised. Subsequently, Highway 23 near the junction of County Highway 7 was breached to let some of the ponded overflow pass into the Cottonwood River basin. This raising and resulting flood-flow backup and subsequent breaching is believed to have caused about 1,100 cfs of the total 25,000-cfs overflow into the Cottonwood River basin. Legal claims due to floodwater retention riverward of Highway 23 and the sudden release of water from the subsequent breaching of Highway 23 resulted in a payment of \$124,000 to affected property owners between Highways 7 and 23 and the Redwood River and about \$80,000 to affected property owners south of Highway 23 in the Cottonwood River basin.

6. Under existing conditions the city would be in an untenable position should another flood equal to or greater than the 1969 flood occur. Without some structural measures, overflows would cross Highway 7, pass through the developing residential area downstream of the highway. enter the Redwood River below the diversion structure, and cause damages in the central city. In addition, since the distance via the overflow route is shorter than the Redwood River meander channel, high velocities could develop as a specific overflow channel concentrated the overflow. Highway 7 would probably wash out, with gully erosion developing from the Redwood River upstream through the developed area. Ultimately, the overflow area could possibly capture the entire river flow and become the main river channel. If the city were to take emergency action to prevent future flooding in the central city by raising Highway 7, it would again be liable for substantial damage claims, with a precedent having been established.

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7. Selected plan. - The selected plan described in section E, appendix 1 (see attached plate J-1 for alignment) provides for an earth levee along the right bank extending from the existing diversion structure upstream to the Highway 23 roadside park. The location of this right bank levee was selected to minimize impacts on forested areas and adjacent cropland areas and provide a technically sound and cost effective alignment. As designed, the levee would provide the 150-acre area with protection against a 133-year flood with 4.6 feet of freeboard (2.0 feet freeboard above SPF). All former overland flows would be confined to the area riverward of the proposed levee. With flows exceeding the design flood flow, the 4.6 feet of freeboard above the proposed levee would prevent overtopping or failure of the levee (and subsequent damages to developing residential areas) by confining the flood flow between the BNRR embankment and the proposed levee.

8. The floodplain area east of County Highway 7 is a developing residential area with several new homes in place and others under construction. Utilities are in place for the area. The 150-acre area west of County Highway 7 is presently about 85-percent (125 acres) cropland and 15-percent residential and commercial land. This area is presently zoned by Lyon County as an agricultural area. The city of Marshall's land use plan developed in 1974 (see plate F-10) indicates that this area is proposed for multifamily residential development. Required utilities can easily be extended from nearby facilities serving the area east of County Highway 7.

#### DOWNSTREAM REACH

9. <u>Problem area</u>. - The downstream channel reach has insufficient channel capacity to pars even the original design flow of 6,500 cfs with the diversion channel. This condition was evident during the 1969 flood when, with a peak downstream discharge of 5,600 cfs,

Appendix I

J-4

extensive emergency diking was needed to prevent damages to Southwest State University and other developments. Under existing conditions, damages would begin to occur in the downstream reach whenever flood flows exceed 725 cfs unless emergency protective measures are provided.

10. <u>Selected plan</u>. - The selected plan described in section E, appendix I (see attached plate J-2 for alignment) provides for an earth levee along the right bank commencing at high ground near the Highway 23 embankment and extending 7,670 feet to high ground at Fifth Street and Hudson Avenué. For the most part, this alignment would follow the alignment of a proposed highway under joint consideration by the city and Lyon County. If later desired, the highway could incorporate the levee embankment or be constructed adjacent to it. As designed, the levee would provide protection to downstream areas against a 133-year flood with 3 feet of freeboard.

11. Approximately 80 acres of downstream reach floodplain land presently in crop use would be protected by the selected levee alignment. The city's 1974 land use plan indicates the proposed land use for this area is single- and multiple-family residential, and school or college.

#### DESCRIPTION OF ALTERNATIVES

12. The selected alignment's compliance with Executive Order 11988 was evlautaed because the upstream levee alignment protects 125 acres of undeveloped floodplain and the downstream levee alignment protects an additional 80 acres of undeveloped floodplain. An alternative levee alignment was formulated to exclude these areas from protection.

#### UPSTREAM REACH

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13. To evaluate the applicability of Executive Order 11988 to protection of the floodplain area, an alternative flood barrier alignment (see plate J-1) excluding the 125 acres of undeveloped

floodplain from protection was analyzed. This alternative could involve either raising County Highway 7 and State Highway 23 or constructing levees paralleling the highways. Since levees would accomplish the same purpose with only minor additional land requirements but at reduced costs, the highway raises were not considered further. These alternate levees would include a levee having an average height of 7.5 feet extending from the County Highway 7 bridge south along the west side of the highway to the State Highway 23 right-of-way, then a levee with an average height of 4.7 feet from that point west along Highway 23 to the driveway at the east side of the roadside park.

14. This alternative would eliminate the need for about 5,500 feet of the selected alignment right bank levee extending upstream from County Highway 7. The selected plan's right bank channel modifications (Plates E-1, E-2, E-3) along most of this removed levee section would also be eliminated. Flood flows would freely enter the affected area at a location downstream of the wayside park. At the standard project flood level, a farmstead and three other residences would be inundated. The maximum design water level in the ponded area would be at elevation 1182, an approximate 1-foot (4 ft. at standard project flood level) increase over existing conditions. With this alternative, Federal first costs would be reduced by about \$490,400. However, because of increased water level and inducement of flood damages the city would be required to either acquire by fee or easement about 125 acres at an estimated cost of \$3,600 per acre.

15. The \$3,600 per acre land value reflects prime agricultural land with excellent near-term development potential. In addition, local interests would have to purchase four homes and a farmstead, pay relocation assistance expenses, and remove affected structures from the area. Thus, non-Federal first costs would increase by \$910,300 over the selected plan. The net change in total plan first costs with the alternate levee alignment would be \$910,300 less \$490,000 or a \$419,900 increase.

Appendix I J-6

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16. With the alternative levee alignment, land required for construction would increase by 144 acres over land required for the selected alignment. The majority of this increase would be agricultural lands; however, a reduction of 2.6 acres of forested land would be realized. In addition, the alternative levee alignment would require relocation of 4 residences and 10 structures, displacing 10 to 15 residents. A comparison of the economic, environmental, and social impacts of the selected and alternative levee alignment and net effects is displayed in table J-1.

| Table J-1                          | - Upstream reach | impacts            |                   |
|------------------------------------|------------------|--------------------|-------------------|
|                                    |                  | Project with       | Net change        |
|                                    |                  | Executive          | with              |
|                                    | Selected         | Order 11988        | Executive         |
|                                    | project          | modification       | Order 11988       |
| Economics                          |                  |                    |                   |
| Federal first costs                | \$2,008,800      | \$1,518,400        | -490,400          |
| Non-Federal first costs            | 495,200          | 1,405,400          | +910,300          |
| Total first costs                  | 2,504,000        | 2,923, <b>9</b> 00 | 419 <b>,9</b> 00  |
| Benefit-cost ratio                 | 1.82             | 1.57               |                   |
| Cost to developers $\frac{1}{}$    | 0                | 500,000            | +500,000          |
| Environmental                      |                  |                    |                   |
| Channel modifications (fee         | t) 8,750         | 4,750              | -4,000            |
| Lands required for project (acres) |                  |                    |                   |
| - Agricultural                     | 28.1             | 168.6              | +140.5 2/         |
| - Forest                           | 41.0             | 38.4               | -2.6              |
| - Other (open)                     | 30.4             | 36.6               | +6.2              |
|                                    | <b>99.</b> 5     | 243.6              | +144.1            |
| Effect on local and regional       | growth patterns  | (see separate wr:  | lte-up)           |
| Social                             |                  |                    |                   |
| Residences relocated               | 1                | 4                  | +3                |
| Structures relocated               | -                | 10                 | +10               |
| Utilities relocated (ft)           | 1,200            | 1,750              | +550              |
| Number of persons displace         | d 1-3            | 10-15              | +9-12             |
|                                    |                  |                    | Appendix I<br>J-7 |

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#### Table J-1 - Upstream reach impacts (Cont)

#### Other

- Driveways to two residences would be impassable during high flood flows with water (100-year level) very near one of the homes.
- Increased local costs of about \$910,300.
- Affected access to area via road ramps and/or closure structures.

1/ Developable area is about 125 acres and 105 acres for selected project and Executive Order 11988 modified project, respectively.

 $\frac{2}{1}$  This area could continue to exist as productive agricultural land. In accordance with E.O. 11988, agriculture is an acceptable use of floodplain lands.

#### DOWNSTREAM REACH

17. An alternative flood barrier alignment was developed for the downstream reach in response to Executive Order 11988 (see plate J-2) excluding the 80 acres of agricultural land from flood protection. This alternative involves an earth levee commencing at high ground near the State Highway 23 embankment, following the alignment of County Ditch 62, to the Camelot Square Trailer Court. The levee then follows the exterior boundary of the trailer court to high ground at Fairview Street. A second levee commencing at high ground near Fifth Street and Hudson Avenue follows north of Hudson Avenue, east to Bruce Street, and then follows Bruce Street north to high ground at Fairview Street.

18. With this alternative, Federal first costs would be increased \$202,000. Non-Federal first costs used for purchase of required lands would decrease \$2,600. The net change in total first costs would be an increase of \$199,400. A reduction of 3.8 acres of lands required for the project would be realised, with only minor relocation of residential fencing required. A comparison of the economic, environmental, and social impacts of the selected and alternative levee alignments and net effects is displayed in table J-2.

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| <u>Table J</u> .   | -2 - Downstr<br>Selected | eam reach impacts<br>Project with<br>Executive Order | Net change with<br>Executive Order |  |
|--|--------------------------|--|------------------------------------|--|
| Item   | project                  | 11988 modifications                                  | 11988 modifications                |  |
| Economic   |                          |  |                                    |  |
| Federal first costs  | \$2,008,800              | \$2,210,800  | +\$202,000                         |  |
| Non-Federal first costs  | 495,200                  | 492,600  | -2,600                             |  |
| Total first costs  | 2,504,000                | 2,703,400  | 199,400                            |  |
| Benefit-cost ratio   | 1.82                     | 1.69   |                                    |  |
| Environmental  |                          |  |                                    |  |
| Lands required for<br>project (acres)                                  |                          |  |                                    |  |
| Agricultural   | 15.0                     | 12.0   | -3.0                               |  |
| Forest   | -                        | 0.5  | +0.5                               |  |
| Other (open)   | 5.3                      | 4.0  | -1.3                               |  |
|  | 20.3                     | 16.5   | -3.8                               |  |
| Effect on local and regional growth patterns - (see separate write-up) |                          |  |                                    |  |
| <u>Social</u>  |                          |  |                                    |  |
| Residences relocated   | -                        | -  |                                    |  |
| Structures relocated   | -                        | Residential fenci                                    | ng                                 |  |
| Utilities relocated<br>(feet)  | 900                      | 900  |                                    |  |
| Number of persons dis-<br>placed                                       | -                        | -  |                                    |  |

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#### DEVELOPMENT OF AFFECTED AREAS

19. Marshall can be described as a vibrant community. The projected growth rate to the year 2000 is from 15 to 20 percent. Development at Marshall will most likely occur southeast, west, and northwest of the city, all south of the Redwood River, in or adjacent to the floodplain. The proposed levee alignment would protect 205 acres of undeveloped land, located near existing utilities, northwest and southeast of the city.

#### UPSTREAM DEVELOPMENT

20. <u>Development under existing conditions</u>. - Under the existing flood and institutional setting, only a very small portion (5 acres) of the affected area could be developed without changes to the topography. This small area is located immediately upstream of County Highway 7, south of the river, and in the immediate vicinity of the only farmstead in the area. To develop the remaining portion, the floodplain lands would require fill to the 100-year flood elevation plus 1 foot. Maximum fill height would be about 6 feet and the average fill height would be about 2.2 feet. Any such landfill would have to provide for maintenance of a suitable floodway meeting State floodplain management requirements. Any future developments would be subject to flooding from floods exceeding the flood protection elevation.

21. Various options would be available to local interests to achieve a designed floodway. One would be the creation of a floodway along the southeast overland flood flow path to the County Highway 7 overflow area and through the area east of County Highway 7 to the river below the existing diversion structure. Floodway requirements could also be met by routing the floodway along the edge of the affected area to tie into the County Highway 7 overflow area. Third, a floodway could be designated along the river channel only with no provision for future overflow over County Highway 7. Preliminary studies indicate that approximately 10 to 15 acres of the cropland area would be required for floodway purposes.

22. Under existing conditions, with no provision for a floodway through the area, approximately 460,000 cubic yards of fill would be required to achieve the 100-year plus 1-foot elevation in the area above Highway 7. Estimated local fill costs would be about \$250,000. This area can be developed with or without the selected project. The city's proposed land use of this area is multifamily residential (see plate F-10). Sewer and water facilities of an adjacent development are of sufficient size to accommodate development in this area, and the area is easily accessible to downtown shopping and other essential public facilities.

23. With the selected alignment, the 125 acres could be developed in accordance with State floodplain management criteria without any fill requirements. Thus, the selected levee alignment would result in a direct savings of about \$250,000 by not having to fill the area.

24. <u>Development with alternative levee alignment.</u> - With the alternative levee alignment, at least four options are evident for future use of the affected lands: (1) the city, having purchased the land in fee (city considers alternative purchase of flood easements to cost as much) could choose to let the land revert to a natural vegetative state; (2) the city could choose to develop the purchased lands as flood damagefree open-space recreation area, not a critical need now or in the foreseeable future; (3) the city could lease the acquired lands to an eperator for continued agricultural productivity; or (4) the acquired lands could be resold for development provided that landfill elevations and floodway requirements are in accordance with State floodplain management regulations.

25. Thus, under the alternative levee alignment, local interests could also develop the floodplain area bounded by the roadside levees provided fill elevation requirements were met. As this alternative would result in an increase in design water surface levels of about 2 feet over existing conditions (due to restriction of the flood flow area), fill requirements would be about double those required under existing conditions for a fill cost of around \$500,000.

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#### DOWNSTREAM DEVELOPMENT

26. <u>Development under existing conditions</u>. - Under existing conditions, the 80 acres of agricultural floodplain lands could be developed in compliance with State floodplain management law, if the area were filled to an elevation 1 foot above the 100-year flood level. A 3to 5-foot maximum fill would be needed to fulfill these requirements. The city's proposed land use of this area is single- and multi-family residential, and school or college (see plate F-10).

27. <u>Development with selected levee alignment</u>. - The selected levealignment allows for development of the 80 acres of floodplain witho requiring the fill that would have been necessary under existing conditions. This is an induced benefit of the levee, in that flood protection afforded by the levee may encourage development in the floodplain to occur sooner than the conditions without flood protection.

28. <u>Development with alternative levee alignment.</u> - As the 80 acres of agricultural land are excluded from flood protection by the levee, development could occur only by filling the area 1 foot above the 100-year flood level, in accordance with State floodplain management criteria. Therefore, there is no direct or indirect encouragement for development by the Executive Order 11988 proposal. However, if the Highway 23 bypass was constructed along the proposed highway alignment, the alternative levee would be rendered obsolete, with a resultant loss of \$199,000 to the national economic development account, in addition to the cost of additional fill required by the bypass to replace the levee that would have been used under the selected plan.

#### SUMMARY OF FLOODPLAIN DEVELOPMENT POSSIBILITIES

29. The primary purpose in developing the alternative levee alignment was to preclude development of undeveloped agricultural floodplain protected by the proposed levee alignment. However, development in the floodplain may still occur, in accordance with State floodplain management criteria, by filling the floodplain lands to 1 foot above the 100year flood elevation. With the upstream reach alternative levee alignment, fill costs would be approximately double those with existing conditions (due to the increase in flood stages), while the downstream fill costs would stay approximately the same. Therefore, floodplain development with both the upstream and downstream alternative levee alignments is more expensive, but not precluded.

#### PRACTICABILITY CONSIDERATIONS

30. Included in the objective of the Executive Order is a statement: "Avoid the base floodplain unless it is the only <u>practicable</u> alternative." The practicability of the alternative levee alignment versus the proposed levee alignment was evaluated on the basis of 16 factors listed in the guidelines for implementing the Executive Organ.

#### DEFINITION OF PRACTICABILITY

31. Practicable is defined in the guidelines for implementing the Executive Order as "capable of being done within the existing constraints. The test of what is practicable depends upon the situation and includes consideration of the pertinent factors, such as environment, cost, or technology." Table J-3 is the comparison table developed for determining the practicability of the alternative levee alignment.

| the prople   | - Arceptable to the city of<br>Noroholl,  | <ul> <li>Bot acceptable to the city of<br/>Marchail.</li> <li>Bosigned to deter unviae<br/>flood plain development.</li> </ul>   |
|--|---|--|
| Bonds and welfare of   | -Requires relocation of 1 res<br>1-3 people.  |  |
|  | ing else to encomplate<br>development in this area, an<br>the 100-year flood level wow<br>State floodplain management   | ild not be required under  |
|  | engineeringly officient<br>levee alignment.<br>- Lover cost to develop,<br>realising that adjacent<br>sever and vater mains<br>in place are of suffic-  | -Requires relocation of<br>4 residences, 10 structures,<br>and displaces 10-15 people.   |
| Locational advantage   | - Makesuse of existing high<br>ground, is economically<br>cheaper, and is a mure<br>contention official   | - Increases the amount of fill re<br>quired for development under<br>existing conditions.  |
| Food production  | Future development of flood-<br>plain agriculturel lands<br>may be accelerated.   | Future development of floodplain<br>agricultural lands would be<br>discouraged or retarded.  |
| Water quality  |   | s between alignments   |
| Water supply   |   | s between alignments   |
| Becreational   | Ko major difference   | s between alignments   |
| le fuges   | •   | e  |
| Fruierai and State<br>designation of<br>scenic or wild rivers          | X X   |  |
| Endengered and<br>threatened species                                   | Xog   | e  |
|  | adverse effects on songbide<br>and small mammals which de-<br>pend on the trees for habite<br>May accelerate future devele<br>sent of agricultural lands i<br>the floodplain which provide<br>wildlife habitet. | it.<br>  |
| Yish and wildlife<br>habitat values                                    | removal of approximately 30<br>large mature shade trees,<br>with resulting long-term  | Would discourage or retard future<br>development of agricultural lan<br>in the floodplain which provide<br>wildlife habitat.   |
| Wistoric values  | Ro major difference   | s between alignments   |
| The functional need for<br>locating the develop-<br>ment in floodplain | Proposed upstream development<br>is not immediately floodplain<br>dependent. However, any down-<br>stream development involving<br>Southwest State University is<br>floodplain dependent.                       | is not immediately floodplain<br>dependent because of the added<br>cost for fill, alternative sites  |
| Impect of floods on<br>burnen safety                                   | design levels, the additional<br>to be contained between the l<br>Railroad tracks. Therefore,   | n flood level, 2.0 feet over<br>overflows would occur to the<br>stion. At floods higher than   |
| Natural and beneficial<br>values served by the<br>floodplain           | May accelerate future develop-<br>ment of agricultural lands in<br>the floodplain.  | Would discourage or retard future<br>development of agricultural lan<br>in the floodplain.   |
| Arothetics   | May accelerate future develop-<br>ment of agricultural lands in<br>the floodplain.  | Yould diacourage or retard future<br>development of appricultural lan<br>in the floodplain.  |
|  |   | of \$619,300<br>- Incr. ase in non-Frderal first<br>costs of \$910,300. It is<br>considered unlikily that the<br>city has the financial capa-<br>bility to provide this amount<br>- Forgone cost to the city in<br>that sever and water mains<br>have been sired to facilitate<br>development in the area ga-<br>cluded from protection. |
| Econosica  | ment of agricultural lands in<br>the floodplate which provide<br>wildlife hubitat.  | <ul> <li>dow lopmont of sericultural law</li> <li>in the floodplain which provide</li> <li>wildlife habitat.</li> <li>Increase in total first costs</li> </ul>   |
| Conservation   |   | Would discourase or recard futur   |

#### Table 3-3 - Comparison table for determining most practicable alternative

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## EVALUATION OF ALTERNATIVE LEVEE ALIGNMENT

32. The determination of whether a practicable alternative exists is based on the advantages and disadvantages of floodplain and nonfloodplain sites. Factors to be considered in making this determination and the evaluation of these factors are shown in table J-3.

33. As shown in table J-3, one of the major factors considered in this situation was economics. The alternative levee alignment would result in a \$910,300 increase in non-Federal costs, an amount city officials say is "far beyond the reasonable acceptance of the city."<sup>1</sup>/ In addition, the alternative levee alignment would approximately double the amount of fill needed to meet State floodplain management regulations for development of the area, which amounts to an increase in cost of \$250,000. Adjacent sewer and water facilities can accommodate development in this area. Additional location benefits are realized by the selected levee alignment in that it makes use of existing high ground, is economically cheaper, and is a more engineeringly efficient levee alignment.

34. Of the remaining factors listed for practicability considerations, additional benefits to fish and wildlife habitat values were realized by the alternative levee alignment. Approximately half of the proposed channel modifications would not be necessary with the alternate levee alignment. In addition, the alternative levee alignment would discourage or retard future development of agricultural lands which provide wildlife habitat. The selected riverbanks levee alignment requires the removal of approximately 30 large mature shade trees with resulting long-term adverse effects on songbirds and small mammal populations.

35. The alternative levee alignment was determined not to be a practicable alternative as the negative economic and location benefits far outweigh

1/ Taken from a letter to the Corps of Engineers from Mr. Robert C. Hirmer, President of the Marshall City Council, dated 10 August 1978.

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the benefits realized to fish and wildlife habitat values. In addition, the alternative levee alignment is unacceptable to the city of Marshall.

## PRESIDENT'S BUDGETARY CRITERIA

36. The President's fiscal year 1980 budgetary criteria require that a "Project does not, directly or indirectly, support future floodplain development in areas other than those near already urbanized areas or where floodplain values have been largely lost and avoids, to the extent possible, the long- and short-term adverse impacts associated with the destruction or modification of wetlands." The selected levee alignment generally meets requirements in that Marshall is an urbanized area, the floodplain land is presently in agricultural use, and the alignment avoids, to the extent possible, adverse impacts associated with any destruction or modification of wetlands.

## EXECUTIVE ORDER 11990

### OBJECTIVE

37. The objective of Executive Order 11990 is to avoid to the extent possible the long- and short-term impacts associated with destruction or modification of wetlands wherever there is a practicable alternative.

## DESCRIPTION OF AREAS AFFECTED

38. The area of concern pertaining to Executive Order 11990 is located upstream of the diversion structure and was described previously in the Executive Order 11988 upstream problem area description (paragraph 5, section J). The selected project is also discussed in the Executive Order 11988 analysis (paragraph 7, section J). Conflict with the objective of Executive Order 11990 resulted from the loss of 2.3 acres of riparian woodland (Type 1 wetland) required by the selected plan for channel modifications.

## DESCRIPTION OF ALTERNATIVES

39. The alternative levee alignment described previously in the Executive Order 11988 analysis (paragraph 13, section J) was evaluated with regard to Executive Order 11990 and protection of wetlands. By removing the right bank levee and replacing it with the highway levee alignments, right bank channel modifications would not be required. However, this alternative would still result in the loss of 1.4 acres of riparian woodland (Type 1 wetland) required by the left bank channel improvements. The left bank channel improvements are necessary to protect the Burlington Northern Railroad embankment and the left bank levees near County State Aid Highway 7 and downstream of the drop structure.

## PRACTICABILITY CONSIDERATIONS

#### GENERAL

40. Included in the President's Executive Order 11990 is a statement that new construction should not be allowed in the wetlands unless "there is no practicable alternative to such construction and . . . the proposed action includes all practicable measures to minimize harm to wetlands which may result from such use." The alternative levee alignment was evaluated to determine if it was a practicable alternative capable of minimizing the loss of 2.3 acres of Type 1 wetland.

EVALUATION OF ALTERNATIVE LEVEE ALIGNMENT

41. The alternative levee alignment would save 0.9 acre of riparian woodland from destruction due to right bank channel modifications, resulting in an increase in non-Federal first costs of \$910,300.

However, this alignment would still require the taking of 1.4 acres of Type 1 wetland. This large increase in costs is unacceptable to the city of Marshall. Other factors relating to the practicability of the alternative were discussed previously in the Executive Order 11988 analysis (paragraph 32, section J). For these reasons, the alternative levee alignment is considered not to constitute a practicable alternative.

## CONCLUSION

42. The District Engineer has determined that the selected alignment is in complete compliance with Executive Orders 11988 and 11990 and is the only practicable alternative for providing flood protection to the city of Marshall. The selected alignment is also generally in agreement with the requirements in the President's 1980 fiscal year budget criteria pertaining to floodplain development. The selected alignment has been coordinated with and reviewed by the Minnesota Department of Natural Resources. The alternative levee alignment was found to be not implementable as it does not constitute a practicable alternative, does not preclude development in the floodplain, and is not acceptable to the city of Marshall.

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30. Current projection C represents the most likely future based on recent changes and information. Estimates for 1975 through 1979 use the census estimate for 1977 as a basis for adjusting estimates between 1975 and 1979. The estimates by Southwest State University for student population were assumed throughout the projection period. Increase in dwelling units of all types thus becomes the only other source of resident population increase. According to Barton-Aschman Associates, Inc. there were 3,474 dwelling units in 1977. Based on building and permit activities during 1977 and estimates through 1979, there will be a phemonenal 18 percent increase in dwelling units to a total of 4,077 during the 3-year span. Records of building permit activity for the past 5-years are presented in Table J-5.

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|               |               |                        | •                 |
|---------------|---------------|------------------------|-------------------|
| Year          | Single Family | Multiple Family        | Total             |
| 1975          | 62            | 54                     | 116               |
| 1976          | 61            | 102                    | 163               |
| 1 <b>9</b> 77 | 80            | 138                    | 218               |
| 1978          | 100           | 85                     | 185               |
| 1979          | 75            | 125                    | 200               |
| TOTAL         | 378 (45 per   | cent) 504 (55 percent) | 882 (100 percent) |

## Table J-5 - Building permits for new housing (dwelling units) for Marshall, Mn., 1975-79

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31. The estimated corresponding increases in population represented by occupancy of these dwelling units is shown in table J-5. An average of three persons per dwelling unit was used to convert dwelling units to population. Estimated absorption of residential land for these dwelling units is also represented based on land use of three single-family dwelling units per acre and 12 multiple-family dwelling units per acre.

Table J-6 - Estimated Increase in Yearly Resident Population at Marshall and Corresponding Demand for Residential Land, 1975-79

| Year  | Population changes | New residential land absorbed (acres) |
|-------|--------------------|---------------------------------------|
| 1975  | + 348              | + 26                                  |
| 1976  | + 489              | + 29                                  |
| 1977  | + 654              | + 45                                  |
| 1978  | + 555              | + 41                                  |
| 1979  | + 600              | + 36                                  |
| TOTAL | .646               | 177                                   |

32. In addition to these residential lands absorbed, other categories of public and commercial also increased. These have not been estimated over the same period.

33. Population and economic growth at Marshall was spurred by the location and expansion of Southwest State University during the period 1965-1970. However, population fell during the 1970 to 1975 period as student enrollment dropped drastically. Similar declines at universities were recorded elsewhere in the State and throughout the country. Since 1975 student population at Southwest State University has slowly risen. Marshall is a very vibrant community at the present time. Growth and development at Marshall since 1975 has therefore

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been stimulated principally by commercial/business activity. Employment has increased significantly at two agribusiness production companies. These companies have entered an expansion period which has seen development and production of new food products. Aggressive marketing and distribution of these food products throughout the region has been very successful to date. Steady increases in employment at these companies and others is projected to increase for some years to come based on local announcements. In addition to food products, a large nationally known manufacturer of glass products for energy saving storm windows established a plant since 1975 with a large work force. Recent announcements indicate that plant expansion in the next 3 to 5 years will probably double employment. Together with employment multipliers, which increase the service related employment industry, and attendant location of dependents of new employees at Marshali, significant vigorous population growth and economic development can be easily predicted between now and 1985. To a much greater extent than the student population growth from 1965-70, employment growth significantly increases related economic and population changes. However, since the economic activity horizon at Marshall cannot be visualized beyond 1985, a lesser normal increase was assumed from 1985 to 1990. The population change from 1990 to 2000 was extended at the average compound rate of growth for the entire decade of the 1980 to 1990 period. The projected population change from 1979 to 1990 represents an implicit demand for and a projected use of 340 acres of current developable land. These land use needs, estimated by category, are presented in Table J-7.

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## Table J-7 - Projected land use needs at Marshall, Mn. (1979-1990)

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| Category               | Development<br>lands (acres) |  |
|------------------------|------------------------------|--|
| Residential - single   | 180                          |  |
| Residential - multiple | 50                           |  |
| Commercial             | 50                           |  |
| Public and Other       | 60                           |  |
| TOTAL                  | 340                          |  |

34. Lands required for residential use are based on densities per acre previously discussed. Commercial and public categories are in consonance with ratios and needs identified by Barton-Aschman Associates, Inc.<sup>(1)</sup>

35. The land supply analysis indicates that, at this time sufficient land (725 acres) is available for site selection through the market process. Generally, as a minimum, twice the number of acres actually used during the demand period should be zoned for the proposed uses.

36. The most probable location of the projected development before 1990 includes land in both the upstream and downstream existing undeveloped floodplain areas as well as the available undeveloped nonfloodplain. Identified development pressure is in the process of determining this future land use pattern. Factors affecting and limiting supply have also been evaluated. Partial residential development is projected to be a pre-project condition in the upstream 125-acre alternate levee alignment area. At a minimum, one residential addition of from 15 to 30 acres is projected before 1990. A maximum development of 30 to 60 acres could occur before 1990. Ultimate development, however, is not projected to occur until after 1990.

(1) Source:

37. Pre-project development conditions in the downstream area will depend on the needs of Southwest State University and ownership of floodplain lands. Residential development will occur unless institutional arrangements (legal options) have precluded such development. Since the University is floodplain dependent for ready expansion, these acres should be protected and reserved for future expansion at Southwest State University.

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38. The above pre-project development conditions are readily predictable based on the above analysis. Specific factors which will stimulate the predicted development pattern are summarized below:

- a. Intense near-term demand for 340 acres of available developable land before 1990.
- b. Near-term reduction of 150 to 200 acres in supply of existing undeveloped nonfloodplain land due to the Green Acres Protection Act. A portion of these lands should become available prior to project construction but not quickly enough to satisfy the immediate demands.
- c. The 315 acres of developable floodplain are all in the 50- to 100-year floodplain except for about 30 acres upstream.
- d. Floodplain and nonfloodplain existing undeveloped lands are nearly cost-equal for development purposes above the 50-year flood elevation.
- e. Forecast development is presently ongoing in and out of the floodplain adjacent to the floodplain areas associated with the alternate levee alignment and Executive Order 11988; affected upstream area lands are already developer-owned with a similar residential floodplain development project on the market.
- f. Undeveloped nonfloodplain lands are available outside the city boundaries which would be developed at higher costs with additional limitations in the existing service delivery system. This type of development is not compatible with the present city development approach as it would necessitate leap-frog development.

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## SUCIAL CONSIDERATIONS

39. Social considerations involved in local floodplain development decisions for the affected areas included an analysis of related development costs, perceptions of the flood threat, related attractiveness, and access to essential services. Thus, the purpose of this discussion is to assess the potential social implications involved in floodplain development decisions at Marshall.

40. The preceeding paragraphs discuss in detail the existing conditions in the community related to supply and demand for vacant developable lands as well as prospective growth and development in the city. At the present, time, the largest proportion of immediately developable lands within the city boundaries are located in the Marshall floodplain. Consequently, on a short-term basis, it is expected that new development will locate in these floodplain areas, as opposed to areas of higher development cost outside the city limits. Additional development costs would include increased investments in the form of either alterations to the city sewer and water system, or separate well and selfenclosed sewage disposal systems. The Minnesota State Floodplain Management requirement for fill 1 foot above the 100-year floodplain is not considered to be of a sufficient cost (in areas requiring relatively low fill requirements) to offset the added development expense necessary to construct outside the city boundaries at this time.

41. On an intermediate and long-term basis, it is expected that both floodplain and nonfloodplain lands, within the city limits, will be available for development and sufficient to meet projected needs. Choices between these lands for development purposes (assuming equivalent availability) will be made on the basis of cost, perceptions of threat, relative attractiveness, and access to services and amenities.

The relative development costs of readily available floodplain and nonfloodplain areas within the city appear to be equivalent at this time, therefore cost will probably not be a distinguishing criteria in decisions on where to develop.

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42. Perceptions of flood threat are not currently impeding development in floodplain area. The Minnesota State Floodplain Management requirements are perceived as providing sufficient protection against severe flood damages, and the provision for flood insurance offered by the Federal Flood Insurance Program provides compensatory payments for any residual damages which may occur from flood events exceeding this level of protection. Threats to human safety associated with potential flooding exceeding this level of protection are not guaranteed against by the fill requirements, yet these residual threats have not served as operational factors in deciding to avoid floodplain areas for residential development. Perceptions of threat may affect development location decisions in areas where personal injuries or deaths have occurred from flood events in recent years. However, no personal injuries or deaths have occurred in the Marshall floodplain during recent floods and therefore the flood threat is not expected to be a major factor in development locational decisions.

43. Aesthetic factors often serve as criteria in determining locations for development, especially for residential uses. As such, development is often attracted to natural floodplains in rural areas, due to the diversity of natural vegetation provided by riverine environments. In the undeveloped portions of the Marshall floodplain the majority of the area is currently under agricultural production and only those lands in close proximity to the river channel exhibit a diverse, riverine vegetation pattern. Therefore, this type of aesthetic consideration is not expected to be an important development inducement for most of the floodplain lands. Another type of aesthetic consideration involved in residential development attraction is compatibility

of different land uses visually proximate to the developable area. Zoning plans by the city for both undeveloped floodplain and nonfloodplain lands provide for highly compatible uses (e.g. areas zoned for residential development are physically separated from lands zoned for commercial and industrial use). In the case of the nonfloodplain developable acreage, park facilities are either currently available or lands are projected for park development in the near future.

44. Access to services and amenities in the form of transportation, retail shopping, and social services also plays a role in locating residential development. The existing road system in Marshall provides easy access to the downtown service area from both the floodplain and nonfloodplain vacant lands being considered for development. As Marshall does not provide a mass transit system which could be used for transportation from outlying residential areas, private vehicles serve as the primary mode of transportation for area residents to necessary services Neither of the undeveloped floodplain or nonfloodplain areas under study could be considered within easy and safe pedestrian access to all existing community services.

45. In summary, there appears to be little differentiation in the relative attractiveness of floodplain and nonfloodplain lands in determining potential development locations, according to the social factors discussed above. Development patterns, should, therefore, be determined solely on the basis of relative cost and availability during periods of peak demand. Since cost are roughly equivalent for both floodplain and nonfloedplain areas, availability is expected to be the key determinant in locating new development. On this basis, a significant proportion of the available undeveloped floodplain acreage is projected to be developed prior to the initiation of any Corps' protection works.

### UPSTREAM DEVELOPMENT

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46. Development under existing conditions -- Under the existing flood and institutional setting, only a very small portion (5 acres) of the affected area could be developed without changes to the topography. This small area is located immediately upstream of County Highway 7, south of the river, and in the immediate vicinity of the only farmstead in the area. To develop the remaining portion, the floodplain lands would require fill to the 100-year flood elevation plus 1 foot. Such changes are currently occurring inside the alternative levee area on floodplain lands and are readily predictable outside the alternative levee area in the upstream floodplain. Maximum fill height would be about 6 to 8 feet and the average fill height would be about 2.2 feet. Any such landfill would have to provide for maintenance of a suitable floodway meeting State floodplain management requirements. Any future development would be subject to flooding from floods exceeding the flood protection elevation. Residential development of 15 to 60 acres of this floodplain is predicted to be a pre-project condition.

47. Various options would be available to local interests to achieve a designated floodway. One would be the creation of a floodway along the southeast overland flood flow path to the County Highway 7 overflow area and through the area east of County Highway 7 to the river below the existing diversion structure. Floodway requirements could also be met by routing the floodway along the edge of the affected area to tie into the County Highway 7 overflow area. Third, a floodway could be designated along the river channel only with no provision for future overflow over County Highway 7. Preliminary studies indicate that approximately 10 to 15 acres of the cropland area would be required for floodway purposes.

48. Under existing conditions, with no provision for a floodway through the area, approximately 460,000 cubic yards of fill would be required to achieve the 100-year plus 1-foot elevation in the area above Highway 7. Estimated local fill costs would be about \$250,000. This area can be developed with or without the selected project. The city's proposed land use of this area is multi-family residential (see plate F-10). Sewer and water facilities of an adjacent development are of sufficient size to accommodate development in this area, and the area is easily accessible to downtown shopping and other essential public facilities.

49. Development of portions of the 125 acre upstream floodplain area would result in certain social effects. Structural flood damages should be avoided for those structures built to State floodplain management standards and any residual damages for flood events exceeding these standards would be compensated for those residences possessing flood insurance. The reduction in risk for property damages, however, does not necessarily imply that no adverse social effects would occur. Until full development of the upstream floodplain area occurred, the periodic presence of ponded water in low-lying unfilled areas would present a safety hazard, especially for small children, if the area was not properly cordoned off. This would be particularly true for that area which currently serves as an overflow area near County Highway #7. In addition to the flood hazard in the 150-acre upstream floodplain area, the developing lands immediately downstream of County Road #7 would have to continue to comply with State floodplain management fill requirements due to continuance of floodwater overflows of County Road #7 during flood events. Other adverse social effects would occur to residents of the floodplain. area from disruptions in transportation patterns and the delivery of goods and services.

Appendix I J-28

50. Development with Selected Levee Alignment -- With the selected alignment, the 125 acres could be developed in accordance with State floodplain management criteria without any fill requirements. Thus, the selected levee alignment would result in a direct savings of about \$250,000 by not having to fill the area. This is an induced benefit of the levee in that flood protection afforded by the levee may encourage development in the floodplain to occur sooner than the conditions without flood protection. This is particularly true for the lowlying overflow areas on both sides of County Highway #7. However, in the long-term, these areas would be developed under either condition.

51. As previously described in the discussion under "Selected Plan", measures have been incorporated into the levee design to minimize the impacts on human safety, health, and welfare. Based on considering the exposure, severity, and preventative measures, the risk to human safety, potential for loss of life, and magnitude of economic loss are less with the selected plan than without. Interior drainage facilities have been included in the levee design and appropriate storm sewer systems would be required in the upstream floodplain area as urban development occurs.

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52. Development with Alternative Levee Alignment -- In the absence of action by the city, 15 to 60 acres of residential development is predicted to occur prior to project construction outside the alternative levee. Alignment with the alternative levee alignment presents at least four evident options for future use of the undeveloped affected lands: (1) the city, having purchased the land in fee (city considers alternative purchase of flood easements to cost as much) could choose to let the land revert to a natural vegetative state; (2) the city could choose to develop the purchase of lands as flood damage-free open-space recreation area, not a critical need now or in the foreseeable future; (3) the city could lease the acquired lands to an operator for continued agricultural productivity; or (4) the acquired lands could be resold for development provided that landfill elevations and floodway requirements are in accordance with State floodplain management regulations.

53. Thus, under the alternative levee alignment, local interests could also develop the floodplain area bounded by the roadside levees provided fill elevation requirements were met. As this alternative would result in an increase in design water surface levels of about 2 feet over existing conditions (due to restriction of the flood flow area), fill requirements would be about double those required under existing conditions for a fill cost of around \$500,000. Likewise, the added 2 feet would make the pre-project development again subject to 100-year flood elevations despite raised 1st floors. 54. The alternative levee alignment would result in a number of adverse social impacts in the upstream floodplain area. Development which has and would occur prior to project construction would have to be relocated from the area, as the current fill levels would be inadequate to meet floodproofing requirements with the raised flood elevations. Residential development of the area would be hampered by the levee which would rise well above the first floor elevations of most homes. If the area were not used for residential development purposes, an adequate amount of land would not be available to satisfy short-term demands. Thus, a short-term "tight" land market would occur resulting in escalation of land values in the area. This alternative would have accelerated growth effects similar to those of the selected plan in the low lying floodplair. area east of County Road #7. , )

## DOWNSTREAM DEVELOPMENT

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55. Development under existing conditions -- Under existing conditions, the 80 acres of agricultural floodplain lands could be developed in compliance with State floodplain management law, if the area were filled to an elevation 1 foot above the 100-year flood level. A 3to 5-foot maximum (1.7 foot average) fill would be needed to fulfill these requirements. This would involve approximately 220,000 cubic yards of fill at estimated local costs of \$120,000. The city's proposed land use of this area is single- and multi-family residential, and a school or college (see plate F-10). Pre and post-project residential

development is predicted to occur in this area in order to satisfy future urban residential growth and development and Southwest State University expansion. The projected expansion of Southwest State University is limited in terms of potential location by the need for keeping facilities (especially student housing) in close proximity to the existing University complex. Development of these facilities on the east side of the 1.H. 23 bypass would require certain safety precautions. This might include traffic semaphores or pedestrian overpasses which would either be not in keeping with highway department standards or beyond the present financial capacities of the University. On the west side of T.H. 23, the only nonfloodplain lands available for development and in close proximity to the campus area are presently zoned by the city for general and service commercial development. As growth is also projected for these uses, it is questionable whether the city would transfer these lands for University development. Although city residential growth is floodplain dependent, it can be accommodated in other areas of the city. However, development of the downstream floodplain area is essential to the expansion needs of Southwest State University. Additional undeveloped lands zoned for residential use are available on the east side of T.H. 23, and are currently undergoing minor development. Extension of city services to these lands, however, would result in costs in excess of those required to develop the available floodplain lands, and city annexation of this area might prove difficult due to the present outside development activites.

56. Development with selected levee alignment -- The selected levee alignment allows for development of the 80 acres of floodplain without requiring the fill that would have been necessary under existing conditions. Thus, the selected levee alignment would result in a direct savings of about \$120,000 by not having to fill the area. This is an induced benefit of the levee, in that flood protection afforded by the levee may encourage development in the floodplain to occur sooner than the conditions without flood protection. However, on the long-term, the area would be developed under either condition.

**(**)

57. Development with alternative levee alignment - As the 80 acres of agricultural land are excluded from flood protection by the levee. development could occur only by filling the area 1 foot above the 100-year flood level, in accordance with State floodplain management criteria. The fill requirements and cost of fill would be the same as that required under existing conditions. Therefore, there is no direct or indirect encouragement for development by the Executive Order 11988 proposal. However, the pre- and post-project residential urban development and Southwest State University expansion which is floodplain dependent would be outside the levee projected area and separated by the embankment from existing pertinent university facilities. Further, if the Highway 23 bypass was constructed along the proposed highway alignment, the alternative levee would be rendered obsolete, with a resultant loss of \$199,000 to the national economic development account, in addition to the cost of additional fill required by the bypass to replace the levee that would have been used under the selected plan.

## SUMMARY OF FLOODPLAIN DEVELOPMENT POSSIBILITIES

58. The primary purpose in developing the alternative levee alignment was to preclude any induced development of undeveloped agricultural floodplain protected by the proposed levee alignment. Floodplain development with both the upstream and downstream alternative levee alignments is more expensive, but not precluded. Development in the floodplain may still occur in accordance with State floodplain management criteria by filling the floodplain lands to 1 foot above the 100year flood elevation. With the upstream reach alternative levee alignment, fill costs would be approximately double those with existing conditions (due to the increase in flood stages), while the downstream fill costs would stay approximately the same.

## PRACTICABILITY CONSIDERATIONS

59. Included in the objective of the Executive Order is a statement: "Avoid the base floodplain unless it is the only practicable alternative." The practicability of the alternative levee alignment versus the proposed levee alignment was evaluated on the basis of 16 factors listed in the guidelines for implementing the Executive Order.

## DEFINITION OF PRACTICABILITY

60. Practicable is defined in the guidelines for implementing the Executive Order as "capable of being done within the existing constraints. The test of what is practicable depends upon the situation and includes consideration of the pertinent factors, such as environment, cost, or technology." Table J-8 is the comparision table developed for determining the practicability of the alternative levee alignment.

## EVALUATION OF ALTERNATIVE LEVEE ALIGNMENT

61. The determination of whether a practicable alternative exists is based on the advantages and disadvantages of floodplain and nonfloodplain sites. Factors to be considered in making this determination and the evaluation of these factors are shown in table J-8.

62. As shown in table J-8, one of the major factors considered in this situation was economics. The alternative levee alignment would result in a \$891,100 increase in non-Federal costs, an amount city officials say is "far beyond the reasonable acceptance of the city".<sup>(1)</sup>

In addition, the alternative levee alignment would approximately double the amount of fill needed to meet State floodplain management regulations for development of the area, which amounts to an increase in cost of \$250,000. Adjacent sewer and water facilities can accommodate development in this area. Addition location benefits are realized by the

(1) Taken from a letter to the Corps of Engineers from Mr. Robert C. Hirmer, President of the Marshall City Council, dated 10 August 1978. Appendix I

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11.

## Table J-8 - Comparison table for determining most practicable alternate

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| tal Eves  | Selector (even al Times)  | Alternative revealignment  |  |
|---|---|--|--|
| Colvervat LON   | May acculate future development of<br>agricultural lanas in the floodplain which<br>provide wildlife habitat  | Hould discourage or fetard to: not<br>pievent future development of agricultural<br>lands in the floodplain which provide<br>wildlife habitat.   |  |
| Economics   |   | <ul> <li>Increase in total first costs of \$650,700<sup>1</sup></li> <li>Increase in non-Federal first costs of \$691,100<sup>1</sup></li> <li>It is considered unlikely that the city has the financial capability to provide this amount.</li> </ul>   |  |
| Aesthet:cs  | May accelerate future development of agricultural lands in the floodplain.  | Would discourage or retard but not<br>prevent future development of agricultural<br>lands in the floodplain. Would create a<br>barrier between existing and predicted<br>pre- and post-project development.  |  |
| Natural and beneficial<br>values served by the<br>gloodplain            | May accelerate future development of agricultural lands in the floodplain   | Abuid discourage or retard future<br>development of agricultural lands in the<br>thoodplain  |  |
| impact of floods on<br>human safety                                     | with the selected mirghment, there is<br>sufficient freeboard (4 there user 133<br>year design flood level, 20 teet user SPH<br>lever to assure that no overrises would occur<br>to the undersloped floodplain in question. At<br>ricods higher than design levels, the additional<br>treeboard would cause water to be contained<br>between the levee and the Burlington Northern<br>Religiond tracks. Therefore, there is no signa-<br>ficent difference between wingments.                               | With the alternative altgnment, there is<br>sufficient freeboard (4.6 feet over 133-<br>year design flood level, 2.0 feet over SPF<br>level' to assure that no overflows would<br>occur to the waisting developed city flood-<br>plain area. However, the alignment would<br>cause water to be contined between the alter-<br>nutive levee and Burlington Northern Rail-<br>road track which would impound water and<br>traise stages, frequency, and duration of<br>flooding to the undeveloped upstream flood-<br>plain in question. |  |
| The functional need for<br>locating the develop-<br>ment in floodplain. | Based on market analysis, pro- and post-project<br>upstream development and downstream develop-<br>ment involving Southwest store (niveristy are<br>floodplain dejendent and protected by project<br>alignment.   | Bused on market analysis, pre- and post-pro-<br>ject upstream development and downstream<br>development involving backhwest State<br>University are floodplain dependent and not<br>protected by project alignment.  |  |
| Nistoric Values   |   |  |  |
| Fish and wildlife<br>habitat values                                     | Riverbank dignment requises removal of approx-<br>imately 30 large mature shade trees, with<br>resulting long-term diverse effects on sung-<br>birds and small manasis which depend on the<br>trees for habitat. May accelerate future develo<br>went of agricultural lands it, the floodplain<br>which provide wildlife halitat.   | prevent future development of agricultural<br>lands in the floodplain which provide<br>wildlife habitat.   |  |
| Endangered and<br>threatened species                                    |   |  |  |
| Føderal and State<br>designation of<br>scenic or wild rivers            | Nuner   |  |  |
| Re fuges  | None  |  |  |
| Recreations1  |   | es between alignments  |  |
| Water supply  |   |  |  |
| Water quality   | No wajor differences b  |  |  |
| Food production   | Future development of floodplain agricultural<br>lands may be accelerated.  | Future development of floodplain agricultur<br>lands would be discouraged or retarded but<br>not prevented.  |  |
| Locational advantage  | <ul> <li>Makes use of existing high ground, is<br/>economically cheaper, and is a more<br/>engineeringly efficient levee alignment.</li> <li>Lover cost to develop, realigning that adjacen<br/>sever and water mains in place are of suffic-<br/>ient size to accommodate development in this<br/>area, and fill to 1 foot above the 100-year f<br/>level would not be required under State flood<br/>management criteria.</li> <li>Requires relocation of 1 residence and displa<br/>2 people.</li> </ul> | lood<br>plain  |  |
| Needs and welfare of<br>the people                                      | Acceptable to the city of Marshall and satisfic<br>present and projected future needs.  | <ul> <li>Not acceptable to the city of Mershel;<br/>set:sfies existing, but not future needs</li> <li>Designed to deter unwise floodplain<br/>development.</li> </ul>  |  |
| IS to at acres of lan   | ed displacements of pre-project construction resid  |  |  |

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selected levee alignment in that it makes use of existing high ground, is economically cheaper, and is a more engineeringly efficient levee alignment.

63. Of the remaining factors listed for practicability considerations, additional benefits to fish and wildlife habitat values were realized by the alternative levee alignment. Approximately half of the proposed channel modifications would not be necessary with the alternative levee alignment. In addition, the alternative levee alignment would discourage or retard future development of agricultural lands which provide wildlife habitat. The selected riverbanks levee alignment requires the removal of approximately 30 large mature shade trees with resulting long-term adverse effects on songbirds and small mammal populations.

64. The alternative levee alignment was determined not to be a practicable alternative as the negative economic, functional need for locating development in the floodplain, and location advantages far outweigh the benefits realized to fish and wildlife habitat values. In addition, the alternative levee alignment is unacceptable to the city of Marshall.

#### PRESIDENT'S BUDGETARY CRITERIA

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65. The President's fiscal year 1980 budgetary criteria require that a "Project does not, directly or indirectly, support future floodplain development in areas other than those near already urbanized areas or where floodplain values have been largely lost and avoids, to the extent possible, the long-and short-term adverse impacts associated with the destruction or modification of wetlands." The selected levee alignment generally meets requirements in that Marshall is an urbanized area, the floodplain land is presently in agricultural use, and the alignment avoids, to the extent possible, adverse impacts associated with any destruction or modification of wetlands.

## EXECUTIVE ORDER 11990

## OBJECTIVE

66. The objective of Executive Order 11990 is to avoid to the extent possible the long- and short-term impacts associated with destruction or modification of wetlands wherever there is a practicable alternative. + )

## DESCRIPTION OF AREAS AFFECTED

67. The area of concern pertaining to Executive Order 11990 is located upstream of the diversion structure and was described previously in the Executive Order 11988 upstream problem area description (paragraph 5, section J). The selected project is also discussed in the Executive Order 11988 analysis (paragraph 7, section J). Conflict with the objective of Executive Order 11990 resulted from the loss of 2.3 acres of riparian woodland (Type 1 wetland) required by the selected plan for channel modifications.

## DESCRIPTION OF ALTERNATIVES

68. The alternative levee alignment described previously in the Executive Order 11988 analysis (paragraph 13, section J) was evaluated with regard to Executive Order 11990 and protection of wetlands. By removing the right bank levee and replacing it with the highway levee alignments, right bank channel modifications would not be required. However, this alternative would still result in the loss of 1.4 acres of riparian woodland (Type 1 wetland) required by the left bank channel improvements. The left bank channel improvements are necessary to protect the Burlington Northern Railroad embankment and the left bank levees near County State Aid Highway 7 and downstream of the drop structure.

## PRACTICABILITY CONSIDERATIONS

## GENERAL

69. Included in the President's Executive Order 11990 is a statement that new construction should not be allowed in the wetlands unless "there is no practicable alternative to such construction and ... the proposed action includes all practicable measures to minimize harm to wetlands which may result from such use." The alternative levee alignment was evaluated to determine if it was a practicable alternative capable of minimizing the loss of 2.3 acres of Type 1 wetland.

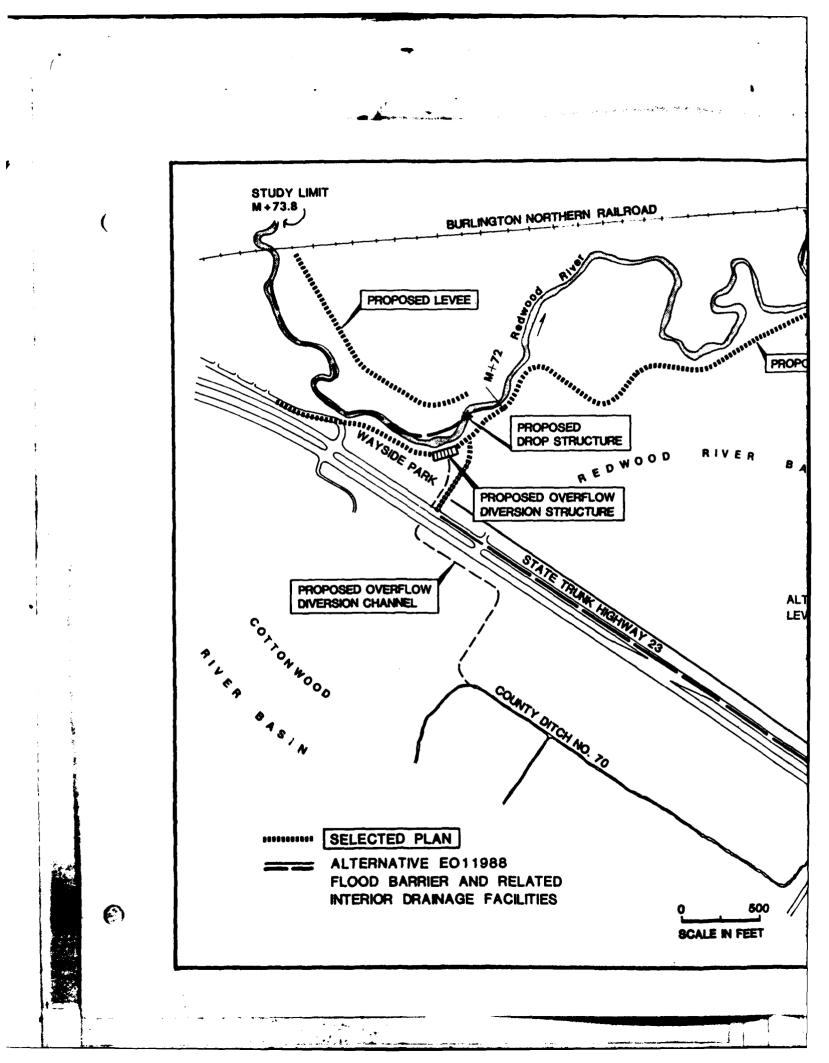
## EVALUATION OF ALTERNATIVE LEVEE ALIGNMENT

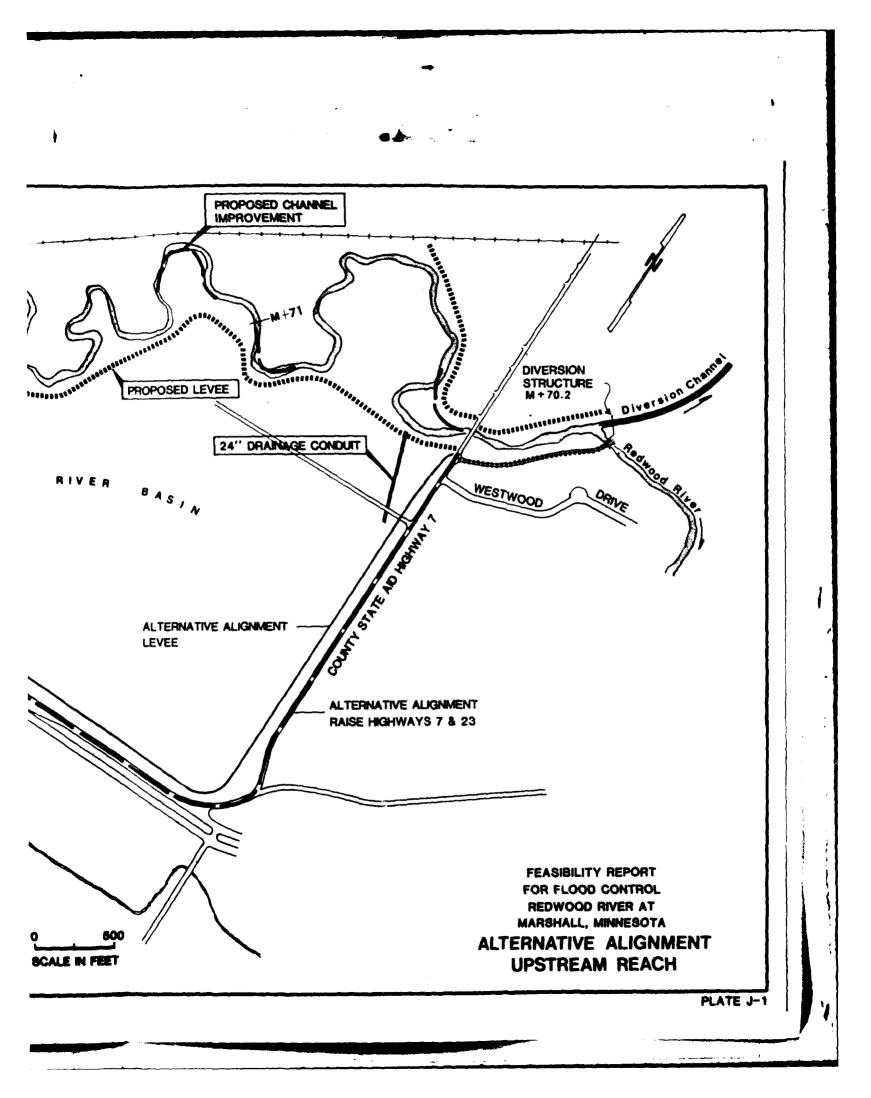
70. The alternative levee alignment would save 0.9 acre of riparian woodland from destruction due to right bank channel modifications, resulting in an increase in non-Federal first costs of \$891,000. However, this alignment would still require the taking of 1.4 acres of Type 1 wetland. This large increase in costs is unacceptable to the city of Marshall. Other factors relating to the practicability of the alternative were discussed previously in the Executive Order 11988 analysis (paragraph 54, Section J). For these reasons, the alternative levee alignment is considered not to constitute a practicable alternative.

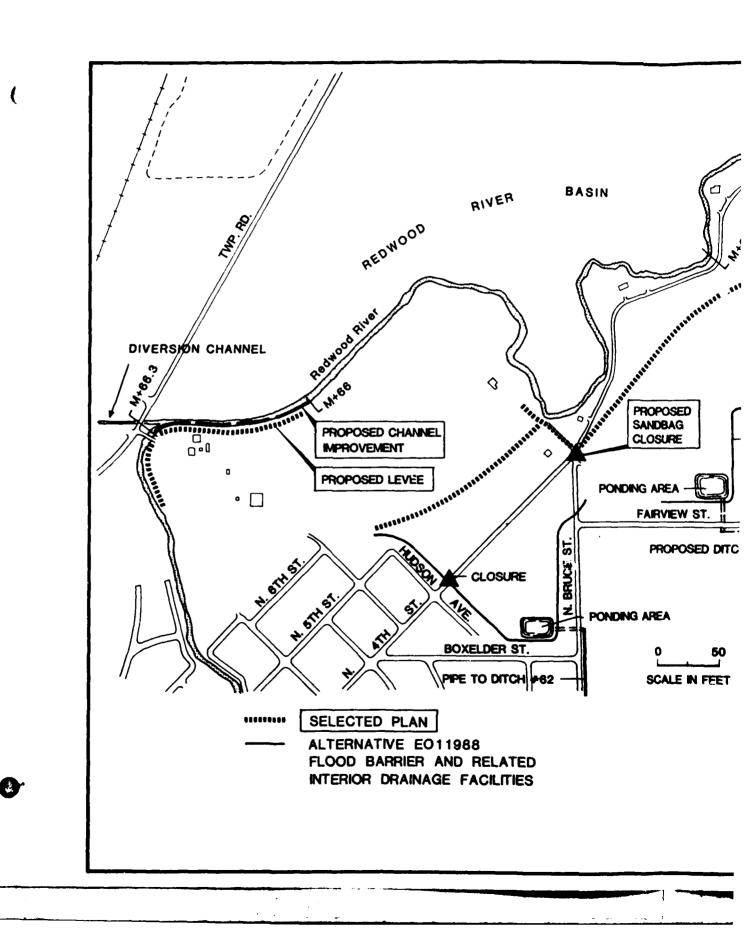
## CONCLUSION

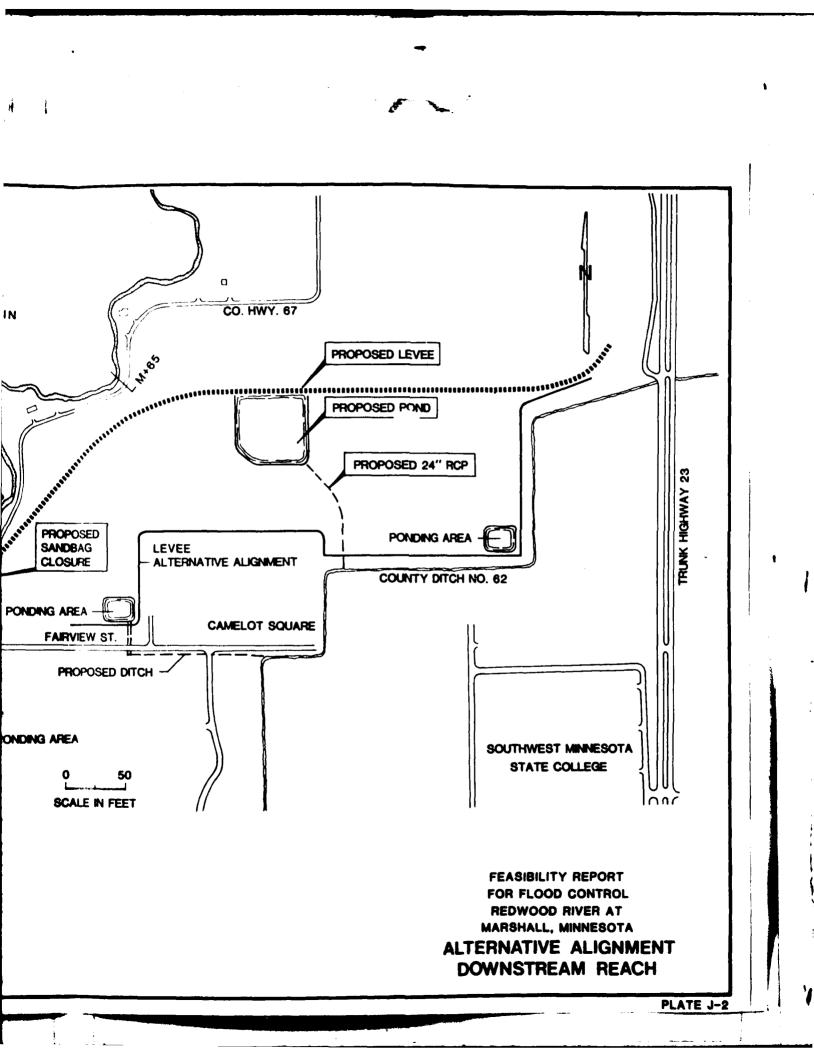
71. The District Engineer has determined that the selected alignment is in complete compliance with Executive Orders 11988 and 11990 and is the only practicable alternative for providing flood protection to the city of Marshall. The selected alignment is also generally in agreement with the requirements in the President's 1980 fiscal year budget

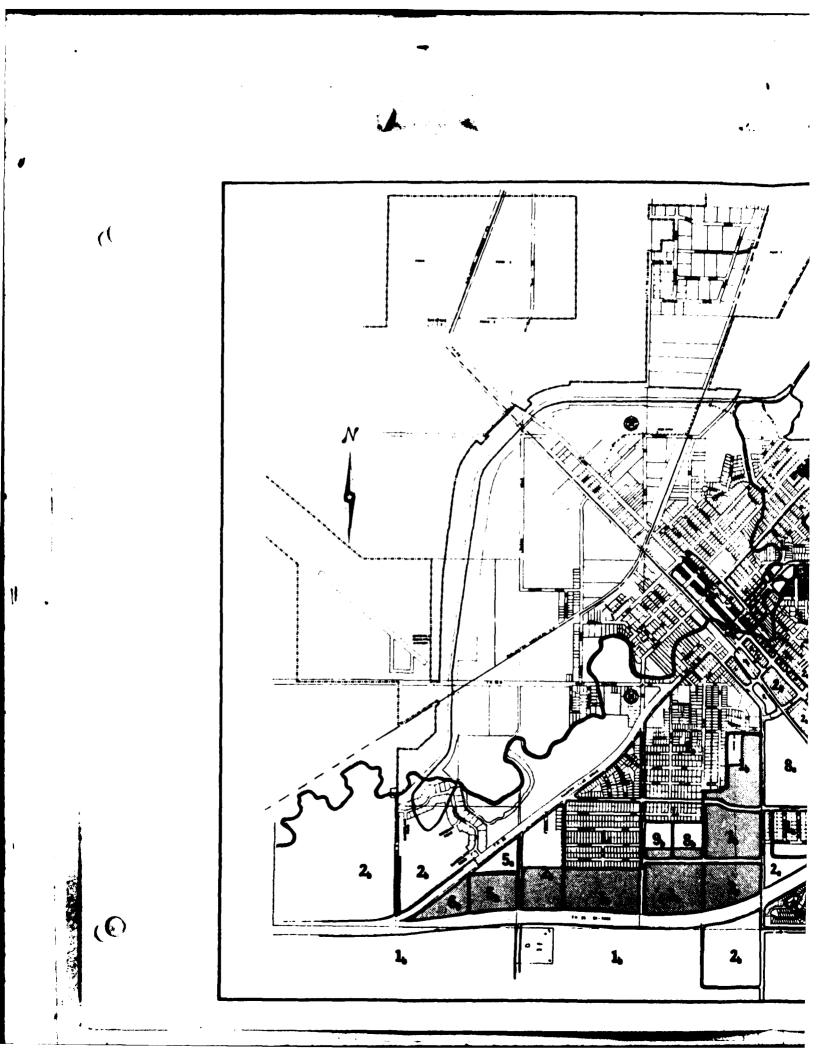
criteria pertaining to floodplain development. The selected alignment has been coordinated with and reviewed by the Minnesota Department of Natural Resources. The alternative levee alignment was found to be not implementable as it does not constitute a practicable alternative, does not preclude development in the floodplain, and is not acceptable to the cite of Marshall.

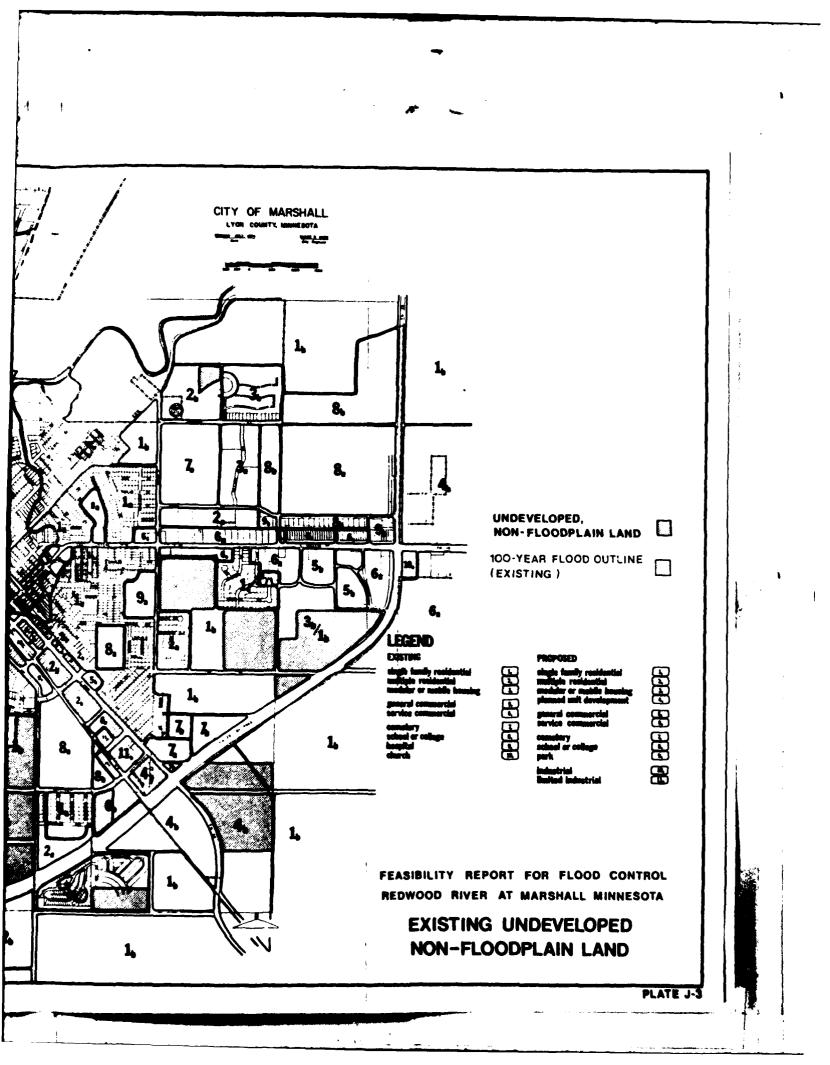












# FEASIBILITY REPORT FOR FLOOD CONTROL

# REDWOOD RIVER AT MARSHALL, MINNESOTA

## PERTINENT CORRESPONDENCE

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U.S. ARMY ENGINEER DISTRICT, ST. PAUL CORPS OF ENGINEERS SAINT FAUL, MINNESOTA

## Appendix 2

Coordination With Other Interests and Public Involvement

## Coordination

The Marshall feasibility study for flood control was initiated in 1974. Several working meetings were held with representatives of the City of Marshall, Lyon County, Minnesota Department of Transportation regional office at Willmar, Minnesota, and the Minnesota Department of Natural Resources field office at Marshall. Various other State and Federal agencies having an interest in the study area were either contacted in person or by correspondence. Other organizations and individuals contacted during the study included the Burlington Northern Railroad regarding their improvements in the area, the State College at Marshall, and numerous individuals interested in area flood damage reduction and recreation needs.

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Formulation stage meetings to apprise local officials and the public on alternative measures considered for the upstream and downstream study reaches were held on 3 March 1975 and 20 October 1975 respectively. Views and comments received at these meetings were used in developing the proposed plan of improvement. A draft Marshall, Minnesota feasibility report was distributed to all interested Federal, State, and local agencies for review and comment in November 1976. A late stage public meeting was held in Marshall during February 1977 to receive comments and any suggested modifications to the proposed plan of improvement. Other than minor alignment changes suggested by the City, no major adverse comments were received regarding a plan providing a 100-year level of flood protection.

> Appendix II II-1

Subsequent review by higher Corps authority of the draft report resulted in a recommendation for reformulation of upstream reach alternatives to include consideration of two additional alternatives and re-analyses of the proposed level of protection. The additional studies resulted in no basic change to the proposed plan of improvement but provided for an increase in the level of protection to the 133-year flood level with attendant raises in flood barrier heights and re-sizing of the proposed State Highway 23 culverts.

On 2 March 1978, a meeting was held with City officials to review the revised study recommendations. The City generally concurs with the recommendations as indicated in their March 1978 letter included in the attachments to this report section. Since no major changes to the original study findings were made, recirculation of the draft report and draft EIS and another late-stage public meeting were not considered necessary.

On 30 March 1978, a meeting was held at the Minnesota Department of Natural Resources to discuss the proposed project. St. Paul District, Corps of Enginers, U.S. Soil Conservation Service, Southern Minnesota River Basin Commission, and Minnesota Department of Natural Resources were represented. Discussions at this meeting covered the proposed project with emphasis on the interbasin crossflow analysis, the protection of undeveloped lands, and mitigation of the 4.2 acres of woodland that would be lost. Subsequent new evaluation of these concerns resulted in no significant changes to the report other than clarification of existing condition and proposed project condition overflows into the Cottonwood River basin.

Subsequent to this coordination, extensive analysis was made of the proposed levee alignments in response to Executive Orders 11988 and 11990. A substantial reanalysis of the proposed recreational improvements was also made resulting in the extension of the proposed trail system upstream of the Highway 23 wayside park and deletion of two connecting segments from the proposed federally cost-shared plan.

Appendix II II-2 The results of these studies and studies responding to Section 404 concerns were discussed with City officials and interested public at a 2 April 1979 meeting in Marshall. Resolutions of intent to meet required items of local cooperation for both the proposed flood control and recreational improvements were adopted by the City at this meeting. Related correspondence and the resolutions from the City are included in the attachments to this report section.

A summary of comments received regarding the draft report submitted in November 1976 together with a related discussion is given on the following pages. Correspondence received subsequent to this initial review and interim correspondence received since the February 1977 late-stage public meeting is included in the attachments.

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Comments and Responses

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# ATTACHMENTS

U.S. Environmental Protection Agency Letter From

Department of the Interior - Office of the Secretary u.s.

U.S. Department of the Interior - National Park Service

U.S. Department of Transportation - U.S. Coast Guard

U.S. Department of Transportation - Federal Highway Administration

U.S. Department of Commerce - National Oceanic and Atmospheric Administration National

Weather Service Forecast Office - Minneapolis National Weather Service - River Forecast Center - Kansas City

U.S. Department of Agriculture - Soil Conservation Service

Minnesota State Planning Agency

Minnesota Pollution Control Agency

Minnesota Department of Agriculture

Minnesota Department of Natural Resources

Minnesota State Archeologist

City of Marshall

Mr. Robert Runchey

Transcript of February 1977 Public Meeting

LIST OF ATTACHMENTS

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Appendix II II-4

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| 1<br>Řespense   | stutement and Noted<br>1004 Friver at<br>5 on either  | isibility re- Noted  | irely shown on Changes have been<br>sidthy. Proposed made to the report.<br>past of the exist-<br>nerly and easterly<br>it point FAS 6072<br>of the river and<br>s northerly bypass  | its would make ref- Changes have been<br>in the confines of made to the report.<br>rreatment as dis-<br>xment.   | Park Service Noted<br>Aistoric, Natural<br>De adversely  | filer was consul- Noted<br>2. We suggest<br>procedures for   | tes existing An archeological survey<br>scamend an would be made of the<br>is affected by proposed project area<br>o Archaeologist, during the post-authori-<br>University of zation planning studies<br>in order to and would be closely cu-<br>uring project ordinated with the State<br>Archeologist.  |
|---|---|--|--|--|--|--|---|
| Agency Commerts on Marshall, Minnesoti<br>Feasibility Report For Flood Control<br>Comment | We have reviewed the drait covary maentum reputt studement and<br>feasibility report for Flood Control on the Redwood River at<br>Marshall, Minnesota, We have no curneit to offer on wither<br>document. | Thank you for the opportunity to review your feasibility re-<br>port and environmental angaet statement. | The approved Federal and roud system is not entirely whown on<br>the exhibits and the discussion of them is very skethy. Proposed<br>FAU 5704 starts west of Murshull at TH 19 just bast of the exist-<br>ing river diversion channel and follows it northerly and easterly<br>to where it ends at the edisting river. From that point FAS 6072<br>extends in a generally custerly direction south of the river and<br>ends at TH 23. This total system constitutes the northerly bypass<br>of Marshall. | It would be desirable if the text and the exhibits would make ref-<br>erence to approved Federal-aid road system within the confines of<br>the project limits. This would entail the same treatment as dis-<br>cussed under comments on the environmental statement. | No established or studies units of the National Park Service<br>or situs eligible for registration as National Mistoric, Natural<br>or Environmental Educational Landmarks appear to be adversely<br>affected by this study. | We note that the State Historic Presentation Officer and consul-<br>ted concerning this proje t (page 57). Therefore, we suggest<br>that his recommendations of followed including procedures for<br>archaeological resource mitigation. | Due to the high probability of archaeological sites existing<br>within the impact area (Appendix 1, 8-11), we recommend an<br>archaeological survey be undertaken for all are is affected by<br>the proposed action. Consultation with the State Archaeologist,<br>Dr. Elden Johnson, Department of Anthropology, University of<br>Minnesota, Minneapolis, NN 55455, is suggested in order to<br>coordinate archaeological survey and recovery during project<br>development. |
| Appendix<br>II-5  | H U.S. Jept. of Transportation  | U.S. Coast Guard   | Federal Highway Administration   |  | U.S. Dept. of the Interior<br>National Park Service  |  |   |

Agency Comments on Marshall Minnesota (Continuel) Feasibility Report For Flood Control

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| Agency                               | Comment  | Response   |
|--------------------------------------|--|--|
| U.S. Dept.of Interior<br>(continued) | Our review of this document and the Fish and Wildlife Service's in-<br>vestigation of the project has disclosed that fish and wildlife re-<br>sources of the area would be affected in minor or temporary ways as<br>described in the DEIS. We believe that adequate measures have been<br>proposed in the report to minimize these adverse effects. However, we<br>believe that the feasibility report, as an authorizing document, does<br>not contain an adequate description of the fish and wildlife resources<br>nor the effects of the project on them. Therefore, we recommend that<br>the description of the fish and wildlife resources and the affects of<br>the project on them, as found in the DEIS, be included in the appro-<br>priate sections of the Draft Feasibility Report. | We believe that as an<br>accompanying document,<br>the draft EIS is the<br>appropriate document for<br>a detailed discussion of<br>impacts on resources dis-<br>cussed in Section B and<br>F of the draft Report.                            |
| U.S. Dept.of Agri-<br>culture        | The effects of the proposed project on agriculture land and agricul-<br>tural production appear to be adequately addressed by the draft.   | Noted  |
| Soil Conservation<br>Service         | Page 20, Section 4.005, last sentence - figure should be 0,500 not<br>8,200.   | The appropriate change<br>has been made to the<br>report.  |
|                                      | We feel that the proposed plan will provide the needed protection for<br>Marshall and is the most feusible solution presently avai.able for<br>the reduction of flood damages in the city of Marshall, M.nnesota.  | Noted  |
| ۹۹<br>ر                              | We suggest that the section on Upstream Reservoir Storage - Plan 4, be rewritten to allow for reappraisal under the authorized joint, Army Corps of Engineers and Soil Conservation Service "639 Study".   | The description of al-<br>ternative plan 4 - Up-<br>stream Storage, in both<br>the main and technical<br>reports has been revised<br>to reflect consideration<br>of upstream storage poss-<br>ibilities in the current<br>joint "639" study. |
| endix II<br>I-6                      | Preliminary flood routings made as a part of the Southern Minnesota<br>Type IV Study, indicated that a reservoir structural program would<br>reduce peak flows at Marshall. Considerable agricultural flood dam-<br>ages occur along the Redwood River both upstream and down:tream of<br>!Marshali. This problem will be addressed by the "639 Study".  | See above paragraph  |

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Agency Comments on Marshall, Winnesota (Fortinuel, Feasibility Report For Flood Control

| Response | See above paragraph.   | Change made to draft<br>report.   | Change Made to <b>draft</b><br>report.  | Noted   | Not od  | Change made to draft<br>report.   | Change made to draft<br>report.  |
|----------|--|---|---|---|---|---|--|
| Comment  | We do feel that the flood control project for Marshall will complement<br>any overall monaures proposed for the Redwood River as a just of the<br>joint "639 Study". | Page 18, 2nd paragraph of Druit Rupurt, last contence add dullar sign to 609,200. | Page 21, of Draft Report, Upstream Reservoir Storage - Plin 4 -<br>Several Comments | This write up should allow for poss bla "639 Study" project solutions. For example, "any reduction in peak flows resulting from upstream storage would compliment this proposal by reducing both the over flow into the Cottonwood River Basin and flows through the project area". | The Southern Minnesotu Type IV Study indicated that utili ation of<br>storage on Lake Benton, Dead Coon Lake and other potentia. upstream lo-<br>cations would reduce the 100-year discnarge to approximatily 5,500 efs<br>at Mayside park where the proposed diversion is located. | Page 21, Plan 4 states in part - "Clearly shows that a single large<br>reservoir would lack sufficient storage capacity". Appendix 1-011<br>stares that "One site was identified as having sufficient storage". | Fage 21, Plan 4, 2nd paragraph. Suggest changlig in part to read -<br>A system of small reservoirs on headwater tributary streams presently<br>under consideration to solve agrict ural flooding would be located<br>too far upstream and have too little storage volume to provide the<br>desired flood protection for the city of Marshall. The last sentence<br>in the above paragraph could remain as is. Appendix I page D12 should<br>be changed to reflect the above working. |
|          | - F Soil Conservation<br>* Service (Continued)<br>H  | U.S. Dept.of Agricul-<br>ture   | Soi. Conservation<br>Service (Continued)  |   |   |   |  |

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dix I has been revised to reflect the most current Page 8-7 of report Appenhas been expanded to include suggested addition Page E-2, 1st paragraph flect suggested changes. has been revised to re-Page 18 of the report climatological data. Response al text. Noted warnings are not at fixed time intervals, but are due to hydrometeorolo-gical conditions as they are anticipated to occur. Accordingly, we suggest in line 3 - "flood warnings issued by the National Weather Service Forecast Office in Minneapolis of impending Redwood River flood may be of value to the body of the report. On page F7 Appendix 1, of the Feasibility Report under the section labelled "Climate" I offer one revision. The total liquid precipitation for 1976 totailed 12.05 inches at the NWS's Murshall station and this quite easily surpasses the pre-Page 18, Line 2-3 of Draft Report - "periodic" should be removed. Flood Page E-2, Firs: Para: We suggest  $\delta$  \_ast sentence as follows: "In addition, riveT and flood forecasting, an intergral part of the design and operation  $\psi f$  levees and other flood control systems and basic to good multi-puryose water management, will continue to be needed." With climatological data received for the 1976 calendar year a change I would only mention the needs which the National Meather Service has with regard to its flood forecasting responsibility to the Marshall area. We see the need to locate a r ver gage such that complete discharge information can be obtained from a single reading. Telephone conversations between our two offices indicate that this work is pro-Agency Comments on Marshall, Minnesota (Continued) Fessibility Report For Flood Control ceeding which we find most reassuring. viously held record of 17.36 inches. occurrences...atc." Comment National Weather Service Forecast Office U.S. Department of Agency Commerce Appendix II II-8

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Agency (omments on Marshall, Minnesota (Continued) Feisibility Report For Flood Control

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| ent      | We have completed our review of the Draft Environmental Impact State-<br>ment (EIS) for 1100d Control Redwood River at Marshall, Minnesota.<br>Your letter of fecember 1, 1976, requested our views and comments on<br>the proposed action. As note from our review of the FIS Mant con-<br>struction is being permitted to take place within flood prone areas.<br>We believe flood protection measures ris appropriate for previoually<br>developed areas, but that a comprehen we flowd control program should<br>include restriction of turner development in flood prone areas.  |
|----------|---|
| Comment  | We had and Your Your Your the part of the |
| Agency   | U.S. Environmental<br>Protection Agency<br>II x Protection Agency   |
| App<br>I | endix II<br>I-9   |
| <b>•</b> | - /   |

Flood protection, should be provided only for these areas which are developed at the time of the filing of the DRaft LLS with the Council on Environmental Quality. Furthermore, the Final EIS should also contain additional information on the construction impacts and the impacts which will result from the completion of the flood diversion channel.

Our detailed corments fellow.

Response

that included undeveloped Alternative levce alignprotection and docreased the area of the college. He acknowledge that the test the developed area Not constitute "practi-cable" alternitives The piinary purpose of of Marshall both withthe project is to proand downstream reaches due to increased flood in the City and downstream of the city in available for development in both upstream they proclude developthe selected alignment protection. Analysis of these alternatives ments were developed showed that they did plain. In addition, E.O. 11958) nor did generally meets the requirements in the project would make flood plain lands criter\_a pertaining fill requirements. President's fiscal ment of the flood field plain from year 1980 budget (as dofined by

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Agency Comments on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

<u>Agency</u>

Contant

U.S. Environmental Protection Agency (continued)

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 to flood plain development. (See also Aprendix 1, Section J). The City of Marshall has recently adopted a flood plain zoning ordinance which is based on a Corp of Engineers flood plain information study. The unincorporated flood plain reaches upstream and downstream of the city are subject to flood plain management regulations currently in effect for Lyon County.

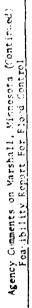
As part of the flood protection, a flood diversion channel will be constructed. This flood diversion channel will divert one-huit of the excess of the present design discharge. Those excess overflows will be discharged into the Cottorwood River Busin. Additional information and discussion must be provided on the present water quality of the receiving stream. The effect upon the water quality from the addition of flood flows also needs to be assessed. Based upon information the EIS, we have assumed the diversion channel to be dry during normal periods of the year. Flood flows can have a high velocity and great be assessed.

anticipated with designed No water quality data is Redwood River basin. However, since the frequency increased adverse effect: on water quality are ex-pected. The potential fo: erosion during high flow riprap provided at crit-ical channel bank, bend, cess overflows from the overflows would both be available for the re-ceiving stream at the point of inflow of exin the overflow diverless than occurs under present conditions, no sion channel has been and magnitude of such and bottom areas.

> Appendix II II-10

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| ant      | Since flood flow, will be us charges<br>an assessment of flooding actioning<br>The two watershess are essentially a<br>meteorological conditions would be<br>if flood flows were occurring in th<br>effect flowd flows were efforts of f |
|----------|--|
| Comment  | Since<br>an as<br>The t<br>meteo<br>experies   |
| Agency   | U.S. Environmental<br>Protection Agency<br>(continued)   |
| App<br>1 | endix II<br>II-11  |

Since flood flow will be uncharged and the fattenward River Fastn. The an assessment of flooding material in this bain should be provided. The The two watershes are essentially next to each other and the sume meteorological conditions would be erp ated over each basin. Envelope, the if flood flows wre occurring in the flavood River Pastr, one reald expect flood flows in the Octobing of the flavoid basin. Envelope which would change the effects of flooding in the flored danages and are the proximity to commuties, areas subject to flood danages and coop and land datages and channel depth and width. The Final FIS should thoroughly discuss how the diversion of flood flows from the Riv Redword River lation will affect the Octtonwood based.

### 5 - 10C - 40

bain multicate both which recurs than that which recurs under present conditions. Thus, flooding potential on the Uottonwood River will be sitchtly reduced. A detailed analysis of the anu without a project muy bu iu nd in under conditions with River overflows into the Cottonwood River magnitude of Redwood Appendix 1 of the Feasibility Report. diversion of flow The frequency and Section H of

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Agency Comments on Marshall, Mannesota (Continued) Feasibility Report For Flood Control

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U.S. Environmental **Protection Agency** (Continued)

charges to meet water quality standards. Information on the dis-channel works would likely im-charge points and changes in the stream's assimilative capacity prove stream water quality due to which may occur as a result of construction should be provided. reduced channel bank erosion and which may occur as a result of construction should be provided. reduced channel bank erosion This information will indicate whether or not the discharger will turbidity. Elimination of still be capable of meeting water quality standards. The proposed channel work may affect the ability of stream dis-

not encourage development in flood hazard areas. To minisize flood damages and project cost, protection should be provided The EIS stated the flood control priject is necessary to jrotect new development in hazard area. It is our opinion that we recommend building restrictions on previously undeveloaed flood plain areas to assure adequate flood protection to the EIS with the Council on Environmental Quality. As a minimum, protection only to areas which are presently developed, and flood protection and flood control projects should provid; where development has occurred prior to the filing of the communty.

The EIS has indicated the reoccurence interval for this pro-ject has been reduced from 114 years to 59 years. The Finil EIS should discuss whether or not this reoccurence interval will be further reduced.

Response

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shallow slack water pools in areas of channel improvement would like-Implementation of the proposed

ly improve the assimilative capa-

discharges would not be affected

city of the stream. Individual

flood plain in accordance with criteria by placement of fill response to EPA comment No. 1 Development may occur in the state flood plain management to 1-foot above the 100-year and Appendix I, Section J of flood elevating. See also the Feasibility Report. by the proposed works.

flood now represents a 59-year fre under existing conditions has been quency based on revised frequencythe present project. The frequency formally agreed upon by interagency agreement between the Corps of Engineers, SCS, and USGS. Nor further revision of this relationship major floods in recent years whereas only one (the 1957 flood) discharge relationship at Marshall discharge relationship primarily attributed to the occurrence of had occurred prior to study of The recurrence interval of 114 years for the original design is anticipated. Agency Constents on Marthal, Minnesota (Continuel) Heasibility Report For Flood Control

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| Appendi<br>II-13 | <u>Agency</u><br>U.S. Environmental<br>Protection Agency | Feasibility R port For Fleod Control<br>Comment<br>In the EIS, water quality studies have indicated any pooling<br>of the Redwood River could promote algal growth during periods  | Response<br>Algue blooms and insect propoga-<br>tion are not expected to be a pro-  |
|------------------|--|--|---|
| x II             | (continued)  | of suitable light and temperature conditions. Part of the<br>flowd control pien calls for a ponding area to be constructed.<br>The potential for algal blooms and insect propagation at this<br>ponding area should be assessed.   | bion in the proposed ponding area<br>since the ponding area would not<br>have any isolated shallow areas<br>and would contain water for only<br>a few days.   |
|                  |  | There are two beaver dams within the wutershed. One beaver dam<br>will be removed during construction. The EIS should indicate<br>whether r not the beaver dam is causing increased flood con-<br>ditions at Redwood. This loss of the beaver dam should be<br>avoided, if possible.   | Mithough detailed hydraulic an-<br>al/sis of the effect of the beaver<br>dum is impractical, it is con-<br>sidered that the dam together<br>with others channel obstructions<br>raises the stream level during<br>flood periods. Required reshaping<br>and riprapping of the river<br>channel in the vicinity of the<br>dam to prevent channel back ero-<br>sion requires removal of the dam. |
|                  |  | Additional information in regard to the disposal of levue ex-<br>cavation material should be provided.   | Other than removal of topsoil<br>along the levee alignment and ex-<br>cavation of an inspection trench<br>along selected reaches, no other<br>evcavation would be reviited.<br>Topsoil removed would be stored<br>in the project area for re-use<br>on the levee. Unsuitable material<br>excavated from the inspection<br>trench would be disposed of on<br>the designated disposal areas.    |
|                  | Minn. Dept. of<br>Agriculture                            | The plan proposes the conversion of 15.8 acres of agricultural<br>land for the flood control project plus 178 acres for project-<br>induced residential and commercial-industrial development. The<br>report states, "This cropland loss is insignificant in itself,<br>but a part of cumulative losses of agricultural land through-<br>out the United States." | The report has been revised to<br>properly indicate the signifi-<br>cance of agricultural lands re-<br>quired for construction of the<br>proposed project and in the  |

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Agency Comments on Marshall Minnesota (Continued Feasibility Report For Flood Control

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|  | Feasibility Report For Flood Control   |   |
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| Agency                                       | Lor J ent  | Response  |
| Ninn. Dept. of<br>Agriculture<br>(Continued) | This Department is very concerned about the loss of agri-<br>cultural land in Minnesota. We feel that any loss of the<br>magnitude proposed for this project is significant, and we do<br>not appreciate such proposals. However, we realize the<br>necessity for fluod control projects which, hopefully, will<br>minimize adverse conditions to the surrounding environmental,<br>gricultural production and human life. We generally support<br>such proposals. | future lost to induced residential<br>development. The projected con-<br>version of agricultural lands to<br>future residential development is<br>indicated in Comprehensive Plan<br>for the City of Marshall.  |
|  | It uppears at this time that any agriculturally related topics<br>have been sufficiently addressed by the Draft Environmentul<br>Impact Statement and Feasibility Revort.  | Noted   |
| Minn. Pollution<br>Control Agency            | It is our understanding that the pr posed project is the "hird<br>attempt for flood control measures on the Redwood River a:<br>Marshall. Previous attempts by the City and Corps of Engineers<br>have been unsuccessful in relieving the flood problems. S:v-<br>eral questions remain unanswered concerning the increase un<br>flood potential. The MPCA requests that attention be given to<br>the following concerns:  | Existing flood damage reduction<br>mrasures have been completed by<br>the City and the U.S. Army Corps<br>of Engineers. These projects have<br>reduced flood damages as evidenced<br>during the April 1969 flood. It<br>wis also evident that the existing<br>federally-constructed project did<br>function as designed but that<br>channel upstream of Marshall pre-<br>vented adequate conveyance of<br>floodwaters to the project.   |
| Appendix II<br>II-14                         | <ul> <li>a. What have been the impacts of such activities as drain-<br/>age of wetlands, agricultural and municipal development<br/>and previous flood control measures on the floed stage?</li> </ul>   | Undoubtedly the increased drainage<br>of wetlands and agricultural lands<br>and increased rates of runoff from<br>developed basin lands have cortri-<br>buted to an increased flood poten-<br>tial at Narshall. The reversal of<br>these activities to original con-<br>ditions would be unrealistic. As<br>indicated above, the local and<br>federally constructed measures<br>have reduced flood stages but<br>still leave the City without an<br>adequate level of protection. |

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Agency Corrects on Nurshall Minnesota (Continued Feasibility Report For Flood Control

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| <u>Comments</u> | b. Why have flood estimates been increased so substantially<br>from previous estimates? Is this due to the short period<br>of record and, if so, should the floods in recent years be<br>considered aberrant? |
|-----------------|---|
| Acency          | Minn. Pollution<br>Control Agency<br>(Continued)  |
| Appe<br>I       | ndix II<br>I-15   |

 If drained wetlands were restored and farming practices modified, would upstream reservoirs be an alternative to channelization?

Due to complex natural flow upstream and downstream of the project, attention should be given to the impact on flood stages downstream in the Reusod and Cottonwood Rivers. Previous failures to control floous would indicate that basin floods are not properly understood. The draft feasibility flood are not properly understood. The draft feasibility flood impacts before an assessment of the benefits and the costs can be properly made.

## Response

Fludd discharge-values have been revised based upon an updated frequency - discharge analysis reflecting recent large floods and mutually agreed upon by the Corps of Engineers, SCS, and USuS.

The restoration of wetlands as terporary peak flood storage areas would aid in reducing peak flood stages but would be inudequate to provide enough storage for the major flood peaks

River is understood. Approximately conditions, cross over into the Cuttonwood River basin is diverted through Marshall and downstream overflow which would under present stream of Marshall on the Rodwood along the Redwood River. This inslight stage rise along the agriincrease in stage are estimated ut \$1300 annually or 2 percent of flows is presently being investi-gated in the joint SCS-Corps 639 50 percent of the 100-year flood crease in flow would result in a and the U.S. Highway 23 crossing Average annual damages from this Marshall and have been reflected matter of interbasin flood over-The impact of flood flows downcultural reach between Marshall total annual ficed damages at in the economic analyses. The at Redwood River mile 58.3. study.

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Agency Communts on Marshall Minnesota (Continued) E-assibility Report For Flood Control

Located on high ground, the wasteenvironmentally adverse dissuption adequate natural channel capacity upstream of the diversion channel. Studies conducted by the Corps of Engineers in 1960 and a recont ing facilities would be of little since the real problem is the incapacity. Expansion of the existwith recent SCS studies indicate water stabilization ponds do not would be adequately protected by the proposed flood control review of these studies together benefit without the proposed uponly potential site of adequate irom increasing the capacity of flood damage reduction reasures is inadequate without the total stream and downstream measures. existing waste treatment works Little benefit would be gained that upstream storage capacity the existing diversion channel require flood protection. The of the Camden State Park, the sufficient to eliminate local measures. Response Will further protection be needed for the wastewater stabiliza-tion ponds and other waste water treatment systems? believe the proposed project adequately addresses alternitives We believe that these studies do not adequately address the upstream and downstream impacts and increased water pollution control measures. Finally, we believe that further evaluation of the predicted flood levels is necessary to determine the Can the diversion channel which was constructed in 1963 be expanded to carry flood waters? Would this alternative re-sult in less aquatic biological, terrestrial, wildlife, such as upstream reservoirs and expansion of the 1963 flcod from secondary effects. At this time, the MPCA does not need for and/or the ultimate scope of the project. aesthetic and water quality impact:? Comments Minr. Pollution Control Agency (Continued) Agency

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Appendix II II-16 1

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# Agency (Comments on Marshall, Minnesota (Continued) Feisibility Report For Flood Control

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| Appe<br>I1       | Agency                         | <u>Comments</u>   | Response  |
|------------------|--------------------------------|---|---|
| endix II<br>1-17 | Minn. State Planning<br>Agency | In order to maintain "natural" hydrologic conditions, 50% of<br>the overflows in the vicinity of the Highway 23 roadsude park<br>will be diverted into the Cottonwood River Basin (page 22,<br>paragraph 1). Are conditions still "natural or pre-develop-<br>ment"? If they are not, can an equivalent percentage of over-<br>flow be diverted to the adjacent basin without damage to land<br>or property in this area? | It is believed<br>distribution c<br>between the Re<br>Bluer most clo<br>that thich would<br>prodevologram<br>ditions withou<br>ditions withou<br>di<br>ditions withou<br>ditions withou<br>ditions withou<br>ditions withou<br>di |
|                  |                                | Areas downstream of the study limits were not evaluated<br>since they would not benefit from the project (F-2, para-<br>graph 4). Might these areas be adversely affected? If so,<br>how and to what extent? If there are potential adverse<br>effects downstream, shouldn't this be included in the B/C<br>analysis as an additional cost?   | The effects of<br>damage reduction<br>flood plain re-<br>of Warshall hu<br>At the design<br>proposed measu<br>in approximate<br>stage increass<br>between Marsha<br>Highway 23 riv<br>dimished incre<br>levels beyond<br>increase in st<br>in ustimuted a<br>of less than 2<br>estimated aver   |
|                  |                                | Newly protected floodplains will attract development. Will<br>this expansion plus the proposed flood control facilities<br>necessitate future flood control measures? Will future<br>zoning restrict development in the adjacent unprotected<br>floodplain?   | The proposed f<br>es at Warshall<br>result in the<br>future measure<br>explicitly rec   |

of that the near equal of flood overflows tedagod and Cottonacod it and existing con-but emergency flood os. This distribution dered to result in seconomic flent dar-se effects to dewild eccur under both rsely represents both basins.

average annuml losses 2 percent of lotal orage annual darages. f the prepased flood cases in flord water ion measures on the asures would result itely One-half foot iss along the river thall and the U.S. its been evaluated. I flood level the that point. This tage would result ver crossing with reach downstream

ures since the analysis flood control measur-11 are not expected f: > need for additional plain regulations to control Je-velopment in unprotected areas be in effect and enforced prior to possible construction of the proexplicitly recognizes that flood posed measures. ł

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| Agency                                     | Comment.s  | Response   |
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| Ninn. State Planning<br>Agency (Continued) | The Feasibility Report states the acreage that will become<br>available for levelopment due to the projected flood pro-<br>tection. Varying figures for the land types opening up for<br>residential development are listed. (E-13, F-20) Please con-<br>solidate and clarify this information as to the acreage of<br>land types becoming available for development. Also, is the<br>64 acres suggested for future nature area acquisition in-<br>cluded in any of the acreages of lor l soon available for de-<br>velopment? | In summary, 85 acres of agricul-<br>tural land in the flood plain<br>downstrear of Marshall would<br>be provided flood protection.<br>Another 120 acres of vacant and<br>agricultural land in the flood<br>plain immediately upstrear of<br>Marshall would be afforded pro-<br>tection. Approximately 42 acres<br>of land would be required for<br>construction of the proposed<br>measures.                     |
|  | Please check Table 1, Comparison of Alternatives Considered<br>Feasibility Report. It appears (x \$1000) was inadvertantly<br>omitted following the Economic Planning Objective Parameters<br>of Flood Damage Reduction and AVerage Annual Benefits.   | The appropriate changes have<br>been mude to Tables 1 and 0-1<br>of the report.  |
| Appendix 11<br>11-18                       | We question the inclusion of location benefits (F-20) in the economic analysis. Since a benefit is attributed to the increased value of newly protected fluodplain land, shouldn't the possible costs to downstream areas also be included   | The inclusion of flood<br>proofing cost savings<br>benefits is considered<br>appropriate in this<br>case since the presently<br>undeveloped area to<br>be protected is iden-<br>tified as future residential<br>development in the approved<br>Marshall Comprehensive<br>Plan and since this area<br>represents the best<br>eccnomic choice over<br>flood-free lands lo-<br>cated further away from<br>Marshall. |

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Agency Communts on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

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| Agency                                     | Comments  | <u>Respurse</u>   |
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| Minn. State Planning<br>Agency (Continued) | What specifically is planned for each of the two years of con-<br>struction? How will the timing of the various stages of pro-<br>ject construction be implemented to minimize pollution<br>(erosion, dust, etc.)?  | The specific sequence of proposed<br>construction activities would be<br>established in detailed planning<br>studies if authorized. However, it<br>is expected that construction ac-<br>tivities would be scheduled to<br>minimize adverse effects on area<br>wildlife. Neasures to reduce<br>pollution such as dust, turbidity,<br>and burning of debris would be<br>accomplished in accordance with<br>Corps regulations. |
|  | Basically, the report is quite complete. Our major concerns<br>are the possibility of adverse effects in the Cottonwood<br>River Basin and in downstream areas beyond the study limits,<br>the possible need for expanding flood control measures in the<br>future, and the timing of construction.   | . ot ed   |
|  | We would like to stress that out agency supports more nol-<br>structural flood control alternatives, i.e., zoning to r2-<br>strict residential development in floodplains that structural<br>alternatives which encourage floodplain development.   |   |
| Minn. Dept. of<br>Natural Resources        | Page 11, paragraph 2, sentence 3. This statement is inaccurate<br>in that the adjaccnt flood plain reachesin unincorporated<br>reachesare subject to Lyon County Flood Plain regulation<br>rather than state regulation.  | Change made to report   |
|  | Page 18, paragraph 2, sentence 3. This statement downplays the The report text has been revised<br>long-term results of flood plain zoning regulations. While it is to more appropriately reflect the<br>true that flood plain zoning will not significantly reduce flood effect of flood plain zoning.<br>damage in the short-term, the long-term result will be to reduce<br>non-conforming flood plain uses which will reduce flood damages.<br>We would request that you be more generous to the concept of<br>flood plain management in your next draft. | The report text has been revised<br>to more appropriately reflect the<br>effect of flood plain zoning.  |

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Agency Communts on Narshal., Minnesota (Continued) Feasibility Report For Flood Control

## Agency

The Distance

Minn. Dept of Natural Resources (Continued)

## Corments

Page 36, Level of Protection Section. According to this discussion, standard project protection will not be provided by all the levees propused in this project. The exact impact of these levees being overtopped has been given only curiory review. Questions which should be addressed in the final document include: if levees are overtopped, what are the depths of flooding; what are the probably dollar damages; and what provisions are being made to provide for internal drainage? How is the project design being reconciled with the fact that Minnesota Flood Plain Regulations NR 89( $^{-}$ )(2) (aa) require that levees built for unter protection shall have a minimum height of at least three fact above the standard Froject Flood, whichever provides the greater protection from flooding? Fage F-7, Table F-1 and Section F-15. This section and table imply that public buildings would continue to be constructed in a non-conforming manner even though flood plain regulations would be in affect. Public buildings would have to conform to any applicable local ordinances. The average annual equivalent value of this future growth (\$5800) would, therefore, nct apply. Page F-20, Location Benefits. We would strongly recommend that location benefits, as used in the bracfit/cost analysis outlined on page F-20, be re-evaluat d. There is no shortage of buildable land around the City of Marshall so there should be no real net gain in land value. The increase of \$1900 per acre is a one-time windfall gain for certain landowners and would conset the expense of other lands that are suitable for development without construction of the flood control project.

## Response

Although protoction against the Sib flood level would be clearly infeasible, measures are provided to prevent the possibility of a levee failure and overflows into Marshall. The right bank levee upstream of the existing diversion structure would provide two feet of freeboard over the SPF flood level. The downstream reach flood barriers would contain the SPF flood flow within the design flood flow within the design The analysis of damage growth to future growth of public duvelopment reflects only the residual damages with flood plain regulations in effect - i.e. the projection of similar underground flood-related damages to structures and usingles to roads and utilities.

The report economic analysis of floodproof cust savings benefits reflects a real economic savings due to protection of the undeveloped lands slated for future development as compared to the cost of developing flood-free lands located further away from established transportation and utility

> Appendix II II-20

Agency Comments on Marshal , Minnesota (Continued) Feasibility Report For Flood Control

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| Agency   | Comment  | K. nonse  |
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| Minn. Dept. of<br>Natural Resources<br>(Continued) |  | reutes. Further, the inclusion<br>of the protected acrease<br>represents the most economically<br>feasible and socially acceptable<br>levee alignment to protect<br>the developed downstream<br>reach area.   |
|  | We would like to reiterate our concern about the problem of<br>Cross-over flooding. While the proposed project is designed<br>to reduce flood damages in Marshall the problem of cross-<br>over flooding is of regional concern and should be analyzed<br>as such.                                     | The problem of cross-flow flood-<br>ing is being investigated on a<br>regional basis in a joint U.S.<br>Army Corps of Engineers - U.S.<br>Soil Conservation "639" study.  |
|  | We are also concerned about the general aesthetic impact that<br>flood control levees have. We would hope that efforts would be<br>expanded, particularly in future projects, but to whatever ex-<br>tent is possible for the Marshall project, to mitigate ae<br>thetic concerns into project design. | Aesthetic impacts of proposed<br>flood barriers have been recogni-<br>zed throughout the study. Proposed<br>mitigation measures to reduce such<br>impacts would include tree and<br>shrub plantings to replace those<br>removed and warped levee cross-<br>sections in selected areas to<br>mitigate the physical impact of<br>levees located close to residences |
|  | In conclusion, the State of Minnesota supports the general con-<br>cept of the proposed project, that is flood damage reduction<br>on the Redwood River in Marshall, Minnesota. You can be<br>assured of our continued interest a d support for the goa. of<br>flood damage reduction.                 | Not <del>e</del> d  |
| Minn. State Arche-<br>ologist                      | I have read the draft environmental impact statement on the<br>plars for Redwood River flood control activities near Mar-<br>shall, Minnesota. I agree with the statements and the rec-<br>ommendations concerning cultural resources that appear in<br>sections 2.026 and 2.027 of that document.     | Not <del>o</del> d  |

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Marshall, Minnesota (Continued) ŝ

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| Agency           | Comment  | Response           |
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| City of Marshall | After review, the proposed project, as presented, appears to<br>be totally consistant with and compliminaty to all existing<br>and currently proposed local land use blans, policies, regu-<br>lations, and objectives. The same hulds true for the various<br>plans and policies for flood control, traffic thoroughfare,<br>parks, and coning. | Not ed             |
|                  | While the City of Marshall does not now have a Comprchensive<br>Master Plan for the City, it is possible that one will be de-<br>veloped within the next couple of years. However, it would<br>not appear at this time that a Comprehensive Master Flan<br>would result in any potential conflict with the proposed flood<br>control project.    | Not <del>e</del> d |

Appendix II 11-22

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|  | Feasionlity Report Lor Flood Control         | Fonsionlity Report For Flood Control  |
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| Individual/Organ_zation                          | ation Connent                                | Rest in the   |
| Mr. Robert C. Runchey<br>Rop. For Westside Acres | See Mr. Runchev's letter<br>in "Attachments" | Account to Wou Runchey, Next Side Acres found along the upstream<br>reach south of the Redmond River would be along the uffected by the<br>priposed plan in terms of valuable property taken and probably<br>future flood damage. |
|  |  | Lands required for the proposed project cast of (34) Tare prosently<br>owned by the city as existing project right-of-say. As significant   |

h additional long needs are unity and long durages in the keet S' e Acres area would be constantially reduced with the eurihition of present condition overflows over USAH Tinto the area. The sel-ected levee alignment upstream of USAH T represents the most uc-onomizilly feasible alignment and was selected to minimize affects on a gener lands. Plan 50, involving a by-puss channel between CSAH T and the BN bridge was found to be economically infeasible and significantly more environmentally disruptive in terms of forest and ground cover losses than the proposed plan.

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Agency Comments City Engineer - It is my opinion that the project as designed for a 133 Noted City of Marshall year degree of protection would very adequately provide the protection to the City of Marshall and adjacent area. Protection to the Standard Project Flood level would appear to be beyond the requirements and realisticly feasibile flood protection level. This subalternative plan which included the raising of County Highway No. 7 and State Highway No. 23 as flood barriers, additional levee height, railroad embankaent protection, additional structures work, etc. in my opinion would be an extremely costly and questionable needed level of protection. For front and plans as selected for the 133 year flood recurfort and plans as selected for the 133 year flood recurtenee frequency protection level. However, there are several minor areas of the plan that we would request further consideration be given to at the wonskire

Agency Comments on Marshall, Minnesota Feasibility Report for Flood Control (Continued)

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; ; ; However, there are several minor areas of the plan that we would request further consideration be given to at the time of the detailed plans preparation. These items would not materially affect the feasibility report as written but are items that we feel should have some attention at some later date when the plan; proceed to the detail planning stage. One of the primary concerns is the lands lying between County State Aid Highway No. 7 and the wayside park area in the upstream protection area. In my opinion, all lands between the proposed levee and the Burlington Northern Railroad will be for all practical purpose undevelopable due to the restrictions that would be placed on this area. Therefore, it may be more advantageous and more practical to purchase these lands in fee title in the interest of the project rather than only obtain essents on a portion of these lands. To support this statement, the report also states that access to this property will be predicted. It project budget would have to b increased considerably. It should also be noted that these lands could then be used for recreational purposes in the form of quiet areas, bike trails and so on as was discussed in the report. The report refers to these quiet areas as being a part of the plan.

> Appendix II II-24

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The report analysis have absequently been revised to retlect the fee purchase by local interests of 71.1 upstream of COMPT and upstream of COMPT for project floodemy purposes.

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| <br>It may also be advantageous to make a more complete<br>analysis of the location of the leve in the area of<br>Mile T to derivation of the leve in the area of  | å  |
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|  |  |
| In the area of Mile 66 further review should also be<br>given to the location of the lavee with the possi-<br>bility of following the chainel more closely than<br>as proposed.  | Şee  |
| Another area that I would request a further review<br>of would be the ponding area located on the down-<br>stream improvement between Highway 33 and County Road<br>No. 7. This ponding area is a sizeable area that<br>would be undevelopable and could present some con-<br>timual maintenance problems particularly as it re-<br>lates to the relatively infrequent prodes of time<br>that the pond will actually be utilized. During<br>the detail plan preparation I would request that we<br>further review this and look at other alternatives<br>as well as design alternatives. | det to branch the branch of th |
| We appreciate your atte: .ur to this project and [<br>can advise you that the City of Marshall is very<br>concerned over flood problems and responsive to flood<br>improvements. As a result of the 1969 flood it was<br>realized that there are some deficiencies. However,<br>if should also be noted that we realize now that we<br>are quite vulnerable to flooding conditions and there-<br>fore hope that this project can be expedited as quick-<br>ly as possible to provide the protection as outlined in<br>the feasibility report.  | Note   |

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his matter could also be investighted in statled planning studies. The applies libro of resently adopted libro for lo annangement regulations to protection f these flowd plain lands would be care-ully evaluated.

## e previous response.

This matter could also be reviewed in any subsequent detailed studies. However, the propred matter ponding area is con-sidered to represent the least uostly alternative for downstream reach infertur darainage. Nith grassed side stopes and bottom and regular moning, maintenance is not expected to be a problem. (c)lec-ted runoff from the more frequent and lesser intensity rainstorms would be quickly discharged from the ponding area leaving the area open for possible out-door game or similar uses.

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(Continued) Feasibility Report For Flood Control Agency Comments on Marshall, Minnesota

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CSAM 7 and State Highway 23 receipt of these comments. 3 concerns subsequent to substituting levees in A modified alternative lieu of the considered evaluated in response Executive Order 11988 See response to Lyon County Department of road raises has been Highways letter. Response to a maximum 3 feet above the eastboind roadway causes a problem at the highway junction with C.S.A.H. 7. Your Plate D-1 does not indicate the left-turn lanes, nor the T.H. 7 junction as they exist today. In it is projected to carry. Any improvement along this road would have to be consistent with the proper design standards. Thus, an 8 foot fill section is not cnly a volume of fill in the road area, but also in the recovery area and slope to meet the existing grade. In response to your letter of August 29, 1978, which is addressed to Mr. F.C. Narshall, we have reviewed the effect of raising the T.H. 23 roadway to act as a dike (along with County Road No. 7) upstream from the City of Marshall. This relates to your modification 4 of Plan location is not acceptable; and, at this location, the eastbound roadway would also have to be raised at least 2 feet. Five accidents one fatal) have been investigated at this junction in the past year. Consideration of raising only the we thound Trunk Highway 23 roadway fill.) The levee could be constructed to serve as flood protection, In response to your letter of August 29, 1978, regarding plan 5U MOD. 4 with the <u>Redwood River</u> in <u>Marshall</u>, NN, the following is (See the attached sheet for a typical section involving the 8 foot Another minor concern would be the esthetics of having an elevated properties, but this is not a direct concern of the County Highway Department. One area of minor concern is CSAH 7 south of T.H. 23. CSAH 7 is currently not up to standards for the volume of traffic I am sure the City of Marshall any case, a 3 foot elevation difference between roadways at this and concerned residents would object in regards to this problem. With the grade of T.H. 23 raised, CSAH 7 will have to match. There may be problems regarding access to and from adjacent 5U on Plate D-1 " considered alternatives upstream reach". an answer to the questions you posed. and serve the highway needs as well. road abutting a residential area. Coment of Transportation (29 Minnesota Department of Highways (7 Sept. 78 ltr.) Dept. Sept. 78 ltr.) Lyon County Aschev

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Appendix II 11-26

Agency Comments on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

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furnished to the Society are located within the Nups showing the area All fill sources for levee construction surveyed have been for review. Response showing the location of the surface finds, rest pits, areas subjected to surface reconnaissance in addition to the proposed project locations. In order for us to fully concur with your finding that no archaeological sites will be damaged by the proposed flood control project, it is The entire junction of C.S.A.H. 7 and T.H. 23 would have to he modified necessary for us to be able to accurately locate what kinds of investigations were done, and where. I have found it difficult to make this evaluation from the report. Therefore, I would appreciate it if you C.S.A.P. 7 would possibly require a sandbag plug at times of highwater. I might add that it is also important to review fill sources for levee tion plans for T.H. 23 show that a 24 inch diameter concrete culvert is constructed through C.S.A.H. 7 to the north of T.H. 23 which drains construction. If these lie outside the areas surveyed, we would like the opportunity to make that review. in elevation to provide suitable access. Additionally, our construc-Ne would recommend that consideration to given to constructing a dike adjacent to T.H. 25 right-of-way to the desired elevation. This dike could be swung northerly and tied in with the raised C.S.A.H. 7, some could provide this office with a copy of the appropriate portions of the Marshall, Minn., 7.5 series, USGS topographic quadrangle map Survey of a Proposed Flood Control Project in Marshall, Minnesota". constructing T.H. 23. On field entrance access, some 1300' vest of distance north of its junction with a cicy street, about 500' north of T.H. 23. Such dike construction need not disrupt trunk highway Please give maximum consideration to reducing the effects of this traffic and might possible be considered less expensive than re-Thank you very much for sending us the report "An Archaeological the north roadway ditch and the proposed Redwood River Basin. project to our wayside rest area. Comment Minnesota Department of fransportation (29 Minnesota Historical Society (25 Aug. 78 Itr.) Sept. 78 ltr.) (continued) Agency Appendix II 11-27

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area surveyed.

reflects these concerns Report and in Section B The revised report dissurveyed in relation to cussion on the optimum A map showing the area Archeological Survey report on file at the office of the St. Paul scale of development of Appendix 1 of the Draft Feasibility Archeological Survey the project area is included with the Corps of Engineers. District, U.S Army Thuse concerns are documented in the of the City. Response Report. Noted. Consultation with the State Historic Preservation Officer, State Archeo-logist, and the latest listing of properties on the National Register The attached soil maps identify prime farmlands within the areas out-lined on plates G-1 and G-2. There is no unique farmland at this site. Mr. Robert Northrup of your office recently contact Mr. Duame Aden, our City Engineer, pertaining to the degree of protection for proposed Flood Improvement Fruject for the City of Marsnail, Minnesota. still be a most acceptable level of protection. This is in accordance This is in reply to your request for assistance in identifying prime or unique farmlands that may be affected by the proposed fluod control did evaluate the 150 year Flood frequency protection level and it is our opinion that the additional work and cost involved do not warrant We have reviewed the report on "An Archeological Survey of a Proposed Flood Control Project in Marshall, Minnesota" by Philip H. Salking and offer the following comments. 20, 1979 and it is the determination of the City staff and City Council that the originally proposed 133 year Flood frequency would with the draft feasibility report as prepared by your office. We We discussed this matter at the City (ouncil Meeting on Febiuary (Continued) of Historic Places should be document a in the report. the relatively small degree of additional protection. project on the Redwood River at Marshall, Minnesota. Feasibility Report For Flood Control Agency Comments on Marshall, Minnesota 10/00/000 Heritage and Conservation Service (27 March U.S. Dept. of Interior tion Service (11 Aug. U.S. Soil Conserva-City of Marshall (21 Feb. 79 ltr.) 1978 ltr.) 1978 ltr.) Agency Appendix II II-28

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Agency Communts on Marshall, M nnesota (Continued) Feasibility Report For Flood Control

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|                  | Agency                                  | Coment  | Response   |
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| endix II<br>I-29 | City of Marshall<br>(18 Apr. 1979 ltr.) | Transmitted herewith please find the City of Marshall's Revolution<br>No. 288 pertaining to the City's approval of a Flood Control Project<br>and its intent and willingness to cooperate with the United States<br>i the construction of the project. This resolution was approved on<br>accordance with the feasibility report prepared by the Corps of<br>Engineers and the appropriate local responsibilities and cost<br>sharing analysis outlined in this report.   | The referenced resolu-<br>tions are included as<br>attachments to this<br>report appendix. |
|                  |   | Also enclosed is Resolution No. 289 which is a resolution ceclaring<br>the intention of the City of Marshall and the Corps of Engineers<br>concerning local participation and recreation features as & part of a<br>project for flood control.  |  |
|                  |   | We are aware of the fact that the cost sharing provisions ire being<br>charged to a 20% local share of the total project as per ricent<br>presidential policy. However, since this project has been under<br>development and preparation for approximately 8 of 9 year, we would<br>suggest that the funding for the project be in accordance with the<br>rules and policy as have been in effect during the development of<br>this project and as outlined in the feasibility report. If it does<br>become absolutely necessary to change the method of funding for the<br>project, we would acknowledge this fact and I would assume the City<br>of Marshall would be the feact that the project is of utmost importance<br>to the residents of the Marshall community. | Noted.   |
|                  |   | It is also our understanding that more formal assurances will be<br>required on the part of the city following the congressional authori-<br>zation and prior to any construction activities through the Corps of<br>Engineers contracts.   | Noted.   |
|                  |   | We would request that we continue to expedite this project as quickly<br>as possible so that we can eliminate the existing potential flood<br>damage and inconveniences to the residents of the Marshall community.<br>Thank you for your assistance.   | Noted.   |

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## Agency Comments on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

## Agency Comment

Chicago and North- The propos western Transportation walking-bi Company (26 March the divers 1979 Itr.) not defini

The proposed recreition facilities with respect to this project proposes walking-biking trails and cross-country ski trails in two locations along the diversion channel around Marshall, Minneseta. While the plans are not definitive in the location of these trails, it would appear that it would be necessary some time in the future that these trails will cross the track of the Cancago & North Western Fransportation Company. At that time it will be necessary for a license to be executed between responsible public body and the Transportation Company for these responsible public body and the Transportation Company for these responsible public body and the Transportation Company for these responses the provided the transportation Company for these responses the track of the bubble bubbble bubble bubble bubble bubbble bubble bubbb

crossings.

#### Response

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The final locations of proposed trail crossings would be reevaluated in detailed Post-arthorization rtudics. Coordination with ail offected interests during these study efforts to develop trail crossings underneath bridges where feasible.

> Appendix II II-30

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(Continued) Feasibility Report For Flood Control Agency Comments on Marshall, Minnesota

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| AgencyConmentResponseU.S. bepartment of the<br>Interior, Fish and<br>wildlife ServiceThis responds to your letter of August 1, 1978 requesting formul documenta-<br>Noted.Noted.U.S. bepartment of the<br>Interior, Fish and<br>Wildlife ServiceThis responds to your letter of August 1, 1978 requesting formul documenta-<br>Noted.Noted.U.S. bepartment of the<br>Nildlife ServiceThis responds to your letter of August 1, 1978 requesting formul documenta-<br>tion of compliance with the 1958 Fish and<br>(33 Aug. 1978 Itr.)Noted.Service<br>agencies to coordinate with the Department of Interior to provide that<br>wildlife conservation shall receive equal consideration with other features<br>of resource development programs. In project planning compliance with<br>the Act occurred through consultation with U.S. Fish and Wildlife Service<br>and by receipt of the Department of Interior's January 31, 1977 comments<br>on the Draft Environmental Impact Sticement for the Redwood River at Marshall. | Response | documenta- Noted.<br>ct<br>River<br>that<br>r features<br>with<br>Service<br>omments<br>at Marshall.  |
|--|----------|---|
| Agency Co<br>U.S. Department of the Th<br>Interior, Fish and ti<br>Wildlife Service (4<br>(23 Aug. 1978 Itr.) ag<br>wi<br>vi   | ment     | is responds to your letter of August 1, 1978 requesting formul-<br>on of compliance with the 1958 Fish and Wildlife Coordination A<br>8 Stat. 401, as amended; 16 U.S.C. 661 et seq.) for the Redwood<br>ood Control Project at Marshall, Minnesota. This Act requires<br>encies to coordinate with the Department of Interior to provide<br>1dlife conservation shall receive equal consideration with othe<br>resource development programs. In project planning compliance<br>development programs. In project planning compliance<br>dby receipt of the Department of Interior's January 31, 1977 c<br>the Draft Environmental Impact Sticement for the Redwood River |
|  |          | U.S. Department of the Ti<br>Interior, Fish and to<br>Wildlife Service (5<br>(23 Aug. 1978 Itr.) FI<br>wi<br>wi<br>of of the<br>service of the<br>wi  |

II-30a

To solve the existing flooding problem in Marshall, Minnesota a 2,260 foot long levee along the left (north) bank and a 6,280 foot-long levee along the right (south) bank are proposed for construction in the upstream portion of the project. Also included would be upstream channel molifications consisting of 500 feet of channel realignment, reshaping and riprapping. The project alternative would involve encroachment into 4.2 ares of floodplain of which 2.3 are classified as riparian woodland of Type I wetland (U.S. Fish and Mildlife Circular 39). In the view of the Fish and Wildlife Service, this action would conflict with Executive Order 11990-Protection of Metlands and Executive Order 11588.

determination has been made President's 1980 budgetory criteria concerning these with the executive orders project is in compliance mination is contained in Section J of Appendix 1 with practicability criteria contained in Executive Orders 11988 and 11990 and the and that no practicable reviewed in accordance . ~ concerning this deterand alternatives con-The proposed project Detailed discussion ulternatives exist. sidered have been executive orders. that the proposed of this report.

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## Agency Comments on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

## Agency

Comment

Executive Order 11936 - Floydrian Manayement is based in fart of the National Environmental Policy Act of 1905, and adds new prominence to the environmental aspects of floodplain management. This Order requires that decision-making by Federal agencies clearly recognizes that flood-plains have unique and significant public values. Consideration must be given, therefore, to natural and beneficial floodplain values and to the public benefit to be derived from their restoration or pre-U.S. Department of the Willife Service (23 Aug. 1974 ltr.) Interior, Fish and (Cuntinued)

servation.

To comply with Frecutive Order 11990 and 11585 by avoiding the direct or indirect support of construction in wethends and floodplains further investigation into the alternative of raising the grades of State Trunk Highway 23 and County State Aid Highway 7 on the South and East border of Section 7 T. 111 N., R. 41 K., Lyons County. This would provide the necessary project objective of moderating floods by revolding a broad area to spread and slow floodwaters, thereby reducing relocities and flood peaks anu it would allow the floodplain to continue to provide the following benefits: water quality maintenance, ground water recharge, fish and wildlife habitat, aesthetics, outdoor ducation and recreation, agriculture, aquaculture, and forstry.

## Response

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This alternative together with a similar alternative incorporating levees in lieu of the road raises have been studied in detail and found to be not practical. A detailed discussion of these alternatives is contained in Section J, Appendix 1 of the Feasibility Report.

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(Continued) Feasibility Report For Flood Control Agency Comments on Marshall, Minnesota

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Coment Agency

Wildlife Service U.S. Fish and

would Statement and Feasibility Report being prepared for this project. incompatible development in floodplains and wetlands. The Public tive levee alignment involving raising the grades of State Trunk Highway 23 and CSAH 7 on the South and East borders of Section 7, TIIIN., R4IW was presented in that correspondence as a method Notice indicates that use of the wetland complies with Executive Me have reviewed the proposed construction and find problems with 1978 discussed compliance with the Executive Orders. An alterna-(U.S. Fish and Wildlife Circular 39). Our letter of Auguest 23, is consistent with the directives of both Executive Orders that to conserve wetland and floodplain acreage. This alternative clearly documented in the Revised Draft Environmental Impact Floodplain Management. As proposed the construction project Order 11990-Protection of Wetlands. This finding should be involve encroachment into 4.2 acres of floodplain, of which agencies consider alternatives to avoid adverse effects and the project as it relates to compliance with Executive Order 2.3 are classified as riparian woodland or Type 1 wetland 11990-Protection of Wetlands and Executive Order 11988-(30 March 1979 ltr)

not promote construction in the floodplain. The 125 acre floodplain In the view of In addition to conserving the wetland acreage the alternative levee quality maintenance, ground water recharge, wildlife habitat and agricultural production. Compliance with Executive Order 11988 from development. By use of this alternative, the project would would continue to provide an area for floodwater storage, water the Fish and Wildlife Service the alternative levee alignment alignment would protect approximately 125 acres of floodplain along T.H. 23 and CSAH 7 remains a practicable alternative. should also be documented in the Revised Draft EIS.

indicates that recurrent floods on the Redwood River together with resulted in flood damages and the need for local flood protection. Yet, within the construction plans chosen to solve the flooding problems, an overflow diversion structure is planned to direct In identifying the problems that brought about a flood damage damaging overflows into the adjoining Cottonwood River basin reduction project at Marshall, Minnesota; the Public Notice

### Response

is not a practicable alternative has been made in accordance with that the road raise alternative criteria for implementing these Detailed studies have indicated the President's 1980 budgetary alignment. This determination Statement and in Section J of to the selected flood barrier This finding is the provisions of Executive Draft Environmental Impact Orders 11988 and 11990 and documented in the Revised the Feasibility Report. directives.

this finding, other plan effects, and the impracticability water storage capability of this alternative to be insignificant. Detailed discussion concerning Detailed flood routing studies is contained in Section J of of the alternative alignment have shown the added floodthe Feasibility Report.

remaining flood problems at Marshall. cross-over flow situation provides sion works is based on the premise The design of the proposed diverthat maintenance of the existing the most equitable solution to The proposed project would be Winnesota River Subbasin plan complementary to any Upper

II- 30 C Agency Conments on Marshall, Minnesota (Continued) Feasibility Report For Flood Control

for this project area and identified as he primary problem of the approximately one-half the Redwood River flood flows in excess of solution seems to pertuate the crossever flooding problem noted Upper Minnesota River Subbasin Study Are. (Public Law 87-639) 6,500 cfs into the Cottonwood River basin. This as a chosen Comont (30 March 1979 Ltr) Wildlife Service U.S. Fish and

(continued)

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promotion of crossover flooding by the Redwood River Flood Control Project does not scem justified in view of the increased problem problem individually have had limited success because it is inter-Area further state: that attempts to solve the crossover flooding related among 5 subbasins. Therefore, major efforts in the 639 The Draft Plan of Study for the Upper Minnesota River Subbasin Study are directed toward correcting the problem on the larger scale of S subbasins in the Upper Minnesota River Basin. The of which the Redwood and Cottonwood River basins are a part. created for the 63. Study Area.

accordance with provisions of the Fish and Wildlife Coordination These comments have been prepared under the authority of and in in our August 23, 1978 letter would allot the project to be in consistent with the National Environmental Policy Act of 1969. Act (48 Stat. 401, as amended; 16 U.S.C. 661 et seq.) and are In our opinion use of the construction a termative indicated compliance with Executive Order 11988 and 11990.

### Response

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diversion works have been coordinat-ed with the joint Corps-SCS "639" and design of the proposed overflow subbasin plans. The formulation developed and would not restrain the formulation of alternative subbasin study.

impracticability of the road raise alternative is discussed in detail in Section F of the Feasibility The determination of the Report.

II-30d

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#### ATTACHMENTS

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#### ATTACHED CORRESPONDENCE

| Department of Transportation      | - U.S. Coast Guard                     |
|-----------------------------------|--|
|                                   | - Federal Highway Administration       |
| U.S. Department of the Interior   | ~ National Park Service                |
|                                   | - Office of the Secretary              |
| U.S. Department of Agriculture    | - Soil Conservation Service            |
| U.S. Department of Commerce       | - National Weather Service             |
|                                   | Forecast Office - Minneapolis          |
|                                   | - Office of the Secretary              |
|                                   | - River Forecast Center - Kansas City, |
|                                   | Missouri                               |
|                                   | - Assistant Secretary For Policy       |
| U.S. Environmental Protection     |  |
| Agency                            | - Region V                             |
| U.S. Department of Interior Herit | 8g e                                   |
| and Conservation Service          |  |
|                                   |  |

U.S. Soil Conservation Service

#### State

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Federal

Minnesota Department of Agriculture Minnesota State Planning Agency Minnesota Pollution Control Agency Minnesota Department of Natural Resources Minnesota Department of Transportation Minnesota Historical Society

#### County

Lyon County Department of Highways

#### Local

City of Marshall - December 9, 1976 April 11, 1978 February 21, 1979 April 18, 1979

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#### Appendix II II-31

Local (continued)

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Mr. Robert C. Runchey

Chicago and Northwestern Transportation Company

Transcript of 23 February 1977 Public Meeting

Appendix II II-32 こうないないというがあるので、



#### DEPARTMENT OF TRANSPORTATION UNITED STATES COAST GUARD

MAILING ADDRESS

CUMMANDER (dp]/eis) SECOND COANT GUAND DISTRICT FLOENAL BLDG ISO MARKET ST ST LOUIS MO (5103

16475 Ser 009 14 December 1976

Department of the Army St. Paul District, Corps of Engineers ATTN: NCSED-PB 1135 U.S. Post Office and Custom House St. Paul, MN 55101

#### Gentlemen:

We have reviewed the draft environmental impact statement and feasibility report for Flood Control on the Redwood River at Marshall, Minnesota. We have no comment to offer on either document.

Thank you for the opportunity to review your feasibility report and environmental impact statement.

Sincerely,

C. E. JOHNSON, JR. Environmental Protection Administrator By direction of the District Commander

Copy to: COMDT (G-WEP-2/73) DOT SECREP Region V DOT (tes), Office of Environmental Affairs CEQ (5)

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U.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION REGION 5 18209 DIXIE HIGHWAY HOMEWOOD. ILLINOIS 60430 January 5, 1977

IN REPLY REFER TO

05-00.5

District Engineer St. Paul District, Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Sir:

The draft environmental statement and draft feasibility report for flood control at Marshall, Minnesota on the Redwood River have been reviewed. Our review comments are as follows:

The approved Federal-aid road system is not entirely shown on the exhibits and the discussion of them is very sketchy. Proposed FAU 5764 starts west of Marshall at TH 19 just east of the existing river diversion channel and follows it northerly and easterly to where it ends at the existing river. From that point FAS 6072 extends in a generally easterly direction south of the river and ends at TH 23. This total system constitutes the northerly bypass of Marshall.

#### Environmental Statement - RE: ED-ER

- 1. The "proposed parkway by others" on Plate 2 should be shown as FAU 5764 since it is an approved route.
- 2. The general location of FAU 5764 should be shown on Plates 2 and 3.
- 3. The general location of FAS 6072 should be shown on Plate 3 because it is an approved route.
- 4. Highway Alignment Levees and Combined Highway Alignment Levees, as discussed on pages 38 and 39, and shown as alternates on Plate 5, should be identified as approved system routes.

## Feasibility Report - RE: ED-PB

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It would be desirable if the text and the exhibits would make reference to approved Federal-aid road system within the confines of the project limits. This would entail the same treatment as discussed under comments on the environmental statement.

Sincerely yours,

Donald E. Trull Regional Administrator

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By:

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W. G. Emrich, Director Office of Environment and Design

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# United States Department of the Interior

NATIONAL PARK SERVICE MIDWEST REGION 1709 JACKSON STREET OMAHA, HEBRASKA 68102

REPLY REFTR TO:

L7423 MWR DCL

Colonel Forrest T. Gay, III District Engineer, St. Paul District Corps of Engineers 1135 U. S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

**Reference** your letter NCSED-PB, December 1, 1976, pertaining to your **feasibility** study for flood control on the Redwood River at Marshall, **Minnesota**.

No established or studied units of the National Park Service or sites eligible for registration as National Historic, Natural or Environmental Educational Landmarks appear to be adversely affected by this study.

We note that the State Historic Preservation Officer was consulted concerning this project (page 57). Therefore, we suggest that his recommendations be followed including procedures for archaeological resource mitigation.

Due to the high probability of archaeological sites existing within the impact area (Appendix I, B-11), we recommend an archaeological survey be undertaken for all areas affected by the proposed action. Consultation with the State Archaeologist, Dr. Elden Johnson, Department of Anthropology, University of Minnesota, Minneapolis, Minnesota 55455, is suggested in order to coordinate archaeological survey and recovery during project development.

Copies of all correspondence should be included within the impact statement to aid in the review process.

Sincerely yours,

mond A. Scal

Merrill D. Beal Regional Director





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# United States Department of the Interior

#### OFFICE OF THE SECRETARY NORTH CENTRAL REGION 230 S. DEARDORN STREET, 2nd FLOOR CHICAGO, ILLINOIS 60604 January 31, 1977

ER 76/1150

Colonel Forrest T. Gay III District Engineer U.S. Army Engineer District St. Paul 1135 U.S. Post Office & Custom House St. Paul, Hinnesota 55101

Dear Colonel Gay:

This responds to your letter of December 1, 1976, requesting commonts on the Draft Feasibility Report (your reference ED-PB) and Draft Environmental Impact Statement (your reference ED-ER) for the Redwood River at Harshall, Minnesota. You further requested that we furnish our comments separately on the two reports.

We have reviewed the documents and have the following comments:

#### DRAFT ENVIRONMENTAL IMPACT STATEMENT (DEIS)

We believe that the statement is an adequate and accurate assessment of the impacts of the flood control project on the resources within our area of jurisdiction and expertise.

### DRAFT FEASIBILITY REPORT

Our review of this document and the Fish and Wildlife Service's investigation of the project has disclosed that fish and wildlife resources of the area would be affected in minor or temporary ways as described in the DEIS. We believe that adequate measures have been proposed in the report to minimize these adverse effects. However, we believe that the feasibility report, as an authorizing document, does not contain an adequate description of the fish and wildlife resources nor the effects of the project on them. Therefore, we recommend that the description of the fish and wildlife resources and the effects of the project on them, as found in the DEIS, be included in the appropriate sections of the Draft Feasibility Report.

The National Park Service has advised that its comments on this report have been presented previously to you.

Sincercly yours, Madoana

Madonna F. NcGrath Acting Special Assistant to the Sucretary





United States Department of the Interior

HERITAGE CONTERMATION AND RECEERTION SERVICE INTERAGENCY ARCHEOLOGICAL SERVICES - DENVER OFFICE OF ARCHEOLOGY AND HISTORIC PRESERVATION 1978 SOUTH GARRISON - ROOM 107 DENVER, COLORADO 80227

IN REPLY REFER TO

H2415-(HCRS)PI

### AUG 1 1 1078

Mr. Robert F. Post Chief, Environmental Resources Branch **Engineering Division** Army Corps of Engineers 1135 U.S. Post Office & Customhouse St. Paul, Minnesota 55101

Dear Mr. Post:

We have reviewed the report on "An Archeological Survey of a Proposed Flood Control Project in Marshall, Minnesota" by Philip H. Salkin and offer the following comments.

Consultation with the State Historic Preservation Officer, State Archeologist, and the latest listing of properties on the National Register of Historic Places should be documented in the report.

A mup outlining the actual project area along with the area surveyed should be included in the report. This map should also depict the areas of test excavations.

The author's recommendations on page 10 should be followed. Any sites discovered during construction should be reported immediately to the State Historic Preservation Officer and the State Archeologist.

Other than these few comments, we found the report to be fairly thorough and the author should be commended for doing a good job.

If we can be of any further assistance, please feel free to contact us.

Sincerely yours,

Jack R Rudy Chief, Interagency Archeological Services - Denver

cc:

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Russell Fridley, SHPO MN Dr. Elden Johnson, State Archeologist



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# United States Department of the Interior

IN BEPLY PEPLE TO:

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HSH AND WEDERT SERVICE St. Paul Field Office, Ecological Services 538 Federal Building and U.S. Court House 316 North Robert Street

**St. Paul, Minnosota 55101** 

P 7 AUG 1978

Colonel Forrest T. Gay District Engineer U.S. Army Corps of Engineers St. Paul District 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Attn: NCSEC-ER

Dear Colonel Gay:

This responds to your letter of August 1, 1978 requesting formal documentation of compliance with the 1958 Fish and Wildlife Coordination Act (48 Stat. 401, as amended; 16 U.S.C. 661 et seq.) for the Redwood River Flood Control Project at Marshall, Minnesota. This Act requires agencies to coordinate with the Department of Interior to provide that wildlife conservation shall receive equal consideration with other features of resource development programs. In project planning compliance with the Act occurred through consultation with U.S. Fish and Wildlife Service and by receipt of the Department of Interior's January 31, 1977 comments on the Draft Environmental Impact Statement for the Redwood River at Marshall.

Additional comments are now proved regarding the planned construction and recent Executive Orders that recognize the Nation's floodplains as the scene of:

- 1. unacceptable and increasing flood losses and
- 2. degradation of natural and beneficial values.

To solve the existing flooding problem in Marshall, Minnesota a 2,260 foot long levee along the left (north) bank and a 6,280 foot-long levee along the right (south) bank are proposed for construction in the upstream portion of the project. Also included would be upstream channel modifications consisting of 500 feet of channel realignment, reshaping and riprapping. The project alternative would involve encroachment into 4.2 acres of floodplain of which 2.3 are classified as riparian woodland or Type I wetland (U.S. Fish and Wildlife Circular 39). In the view of the Fish and Wildlife Service, this action would conflict with Executive Order 11990-Protection of Wetlands and Executive Order 11988 Floodplain Management as a practicable alternative appears to exist. Most of the Nation's wetlands are located in floodplains, thus agency procedures for floodplain management will frequently apply to wetlands. Executive Order 11990 Protection of Wetlands, states that "each agency to the extent permitted by law, shall avoid undertaking or providing assistance for new construction located in wetlands unless the head of the agency finds (1) that there is no practicable alternative to such construction, and (2) that the proposed action includes all practicable measures to minimize harm to wetlands which may result from such use.

Executive Order 11988 - Floodplain Management is based in part on the National Environmental Policy Act of 1969, and adds new prominence to the environmental aspects of floodplain management. This Order requires that decision-making by Federal agencies clearly recognizes that floodplains have unique and significant public values. Consideration must be given, therefore, to natural and beneficial floodplain values and to the public benefit to be derived from their restoration or preservation.

To comply with Executive Order 11990 and 11988 by avoiding the direct or indirect support of construction in wetlands and floodplains further investigation into the alternative of raising the grades of State Trunk Highway 23 and County State Aid Highway 7 on the South and East border of Section 7 T. 111 N., R. 41 W., Lyons County. This would provide the necessary project objective of moderating floods by providing a broad area to spread and slow floodwaters, thereby reducing velocities and flood peaks and it would allow the floodplain to continue to provide the following benefits: water quality maintenance, ground water recharge, fish and wildlife habitat, aesthetics, outdoor education and recreation, agriculture, aquaculture, and forestry.

We strongly suggest further consideration of this alternative that will allow the project to comply with Executive Orders 11990 and 11988.

Sincerely,

Kaney B. Walters

Field Office Supervisor

cc: MN DNR, St. Paul, MN

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# United States Department of the Interior

LINEAND WED FELSTRVICE TWIN CITIES AREA OFFICE 530 Federal Building and US Court House 316 North Robert Street St. Paul, Minnesota 55101

# MAR 30 100

Colonel Forrest T. Gay, III District Engineer U.S. Army Corps of Engineers St. Paul District 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

This responds to the Public Notice dated February 28, 1979, regarding the Corps of Engineer's compliance with Section 404 of the Clean Water Act of 1977 for flood control plans involving dredging and filling in the Redwood River at Marshall, Minnesota. The flood damage reduction plan would provide protection for the city of Marshall and adjacent agricultural areas. The plan of work on the Redwood River consists of channel widening, straightening, and bank reshaping measures; levees; an overflow diversion structure with appurtenant control and outlet works; interior drainage works; aesthetic measures; recreation facilities; and required relocations.

We have reviewed the proposed construction and find problems with the project as it relates to compliance with Executive Order 11990-Protection of Wetlands and Executive Order 11988-Floodplain Management. As proposed the construction project would involve encroachment into 4.2 acres of floodplain, of which 2.3 are classified as riparian woodland or Type 1 wetland (U.S. Fish and Wildlife Circular 39). Our letter of August 23, 1978 discussed compliance with the Executive Orders. An alternative levee alignment involving raising the grades of State Trunk Highway 23 and CSAH 7 on the South and East borders of Section 7, T111N., R41W was presented in that correspondence as a method to conserve wetland and floodplain acreage. This alternative is consistent with the directives of both Executive Orders that agencies consider alternatives to avoid adverse effects and incompatible development in floodplains and wetlands. The Public Notice indicates that use of the wetland complies with Executive Order 11990-Protection of Wetlands. This finding should be clearly documented in the Revised Draft Environmental Impact Statement and Feasibility Report being prepared for this project.

In addition to conserving the wetland acreage the alternative levee alignment would protect approximately 125 acres of floodplain from development. By use of this alternative, the project would not promote construction in the floodplain. The 125 acre floodplain would continue to provide an area for floodwater storage, water quality maintenance, ground water recharge, wildlife habitat and agricultural production. Compliance with Executive Order 11988 should also be documented in the Revised Draft EIS. In the view of the Fish and Wildlife Service the alternative levee alignment along T.H. 23 and CSAH 7 remains a practicable alternative. In identifying the problems that brought about a flood damage reduction project at Marshall, Minnesota; the Public Notice indicates that recurrent floods on the Redwood River together with damaging overflows into the adjoining Cottonwood River basin resulted in flood damages and the need for local flood protection. Yet, within the construction plans chosen to solve the flooding problems, an overflow diversion structure is planned to direct approximately one-half the Redwood River flood flows in excess of 6,500 cfs into the Cottonwood River basin. This as a chosen solution seems to perpetuate the crossover flooding problem noted for this project area and identified as the primary problem of the Upper Minnesota River Subbasin Study Area (Public Law 87-639) of which the Redwood and Cottonwood River basins are a part. The Draft Plan of Study for the Upper Minnesota River Subbasin Area further states that attempts to solve the crossover flooding problem individually have had limited success because it is interrelated among 5 subbasins. Therefore, major efforts in the 639 Study are directed toward correcting the problem on the larger scale of 5 subbasins in the Upper Minnesota River Basin. The promotion of crossover flooding by the Redwood River Flood Control Project does not seen justified in view of the increased problem created for the 639 Study Area.

These comments have been prepared under the authority of and in accordance with provisions of the Fish and Wildlife Coordination Act (48 Stat. 401, as amended; 16 U.S.C. 661 et seq.) and are consistent with the National Environmental Policy Act of 1969. In our opinion use of the construction alternative indicated in our August 23, 1978 latter would allow the project to be in compliance with Executive Order 11988 and 11990.

Sincerely yours,

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#### UNITED STATES DEPARTMENT OF AGRICULTURE

SOIL CONT AVAILON STRVICE

316 North Robert Street, St. Paul, Minnesota 55101

January 31, 1977

Colonel Forrest T. Gay, III St. Paul District, Corps of Engineers To, artment of the Army 1222 U.S. Post Office & Custom House St. Paul, Hinnesota 55101

Dear Sir:

Subject: Draft Environmental Impact Statement, Flood Control Redwood River at Marshall, Minnesota

Thank you for furnishing the subject draft to this office for review and comment.

The effects of the proposed project on agriculture land and agricultural production appear to be adequately addressed by the draft.

Page 20, Section 4.005, last sentence - figure should be 6,500 not 8,200.

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Sincerely,

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Larry 12 Major / State Conservationist

## UNITED STATES DEPARTMENT OF AGRICULTURE

SOIL CONCERVATION SERVICE

up holds Robert Street, St. Laul, Minnesota 55101

January 31, 1977

Colored Forrest T. Gay, III St. Faul District, Compared Engineers Department of the Army 1222 U.S. Post Office & Custom House St. Faul, Linnescon 55101

Dear Sir:

Subject: Comments - Redwood River at Marshall, Minnesota Draft Feasibility Report for Flood Control

We feel that the proposed plan will provide the needed protection for Marshall and is the most feasible solution presently available for the reduction of flood damages in the city of Marshall, Minnesota.

We suggest that the section on Upstream Reservoir Storage - Plan 4, be rewritten to allow for reappraisal under the authorized joint, Army Corps of Engineers and Soil Conservation Service "639 Study".

Preliminary flood routings made as a part of the Southern Minnesota Type JV Study, indicated that a reservoir structural program would reduce peak flows at Marshall. Considerable agricultural flood damages occur along the Redwood River both upstream and downstream of Marshall. This problem will be addressed by the "639 Study".

We to feel that the flood control project for Marshall will complement any overall measures proposed for the Redwood River as a part of the joint "639 Study".

Specific editorial comments on the subject draft are listed on the attached sheet.

Sincerely,

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Hárry N. Dajor State Conservationist

Att: chment

cc: Gerald A. Simpson, Area Concervationist, SCS, Marshall, MN Furion Stream, Director, Hidwest TSC, Lincoln, Matradea Jon V. Padreet, Asa't State Concervationist, SCS, St. Faul, MN Specific Comments on Subject Draft

Page 18, 2nd paragraph, last sontence add dollar sign to 609,200.

Page 21, Upstream Reservoir Storage - Plan 4 - Several Comments

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This write up should allow for possible "639 Study" project solutions. For example, "any reduction in peak flows resulting from upstream storage would compliment this proposal by reducing both the over flow into the Cottonwood River Basin and flows through the project area".

The Southern Minnesota Type IV Study indicated that utilization of storage on Lake Benton, Deed Coon Lake and other potential upstream locations would reduce the 100-year discharge to approximately 6,500 cfs at Wayside park where the proposed diversion is located.

Page 21, Plan 4 states in part -"Clearly shows that a single large reservoir would lack sufficient storage capacity". Appendix I-D11 states that "One site was identified as having sufficient storage".

Page 21, Plan 4, 2nd paragraph. Suggest changing in part to read -A system of small reservoirs on headwater tritutary streams presently under consideration to solve agricultural flooding would be located to far upstream and have to little storage volume to provide the desired flood protection for the city of Marshall. The last sentence in the above paragraph could remain as is. Appendix I page D12 should be changed to reflect the above wording. 1217-08 / days + 6 820 - March 19

## UNITED STATES DEPARTMENT OF AGRICULTURE

#### SOIL CONSERVATION SERVICE

316 North Robert Street, St. Paul, Minnesota 55101

March 27, 1978

File: NCSED-ER

Mr. Robert F. Post Chief, Environmental Resources Branch, Engineering Division Dept. of the Army St. Paul District, Corps of Engineers 1125 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Mr. Post:

This is in reply to your request for assistance in identifying prime or unique furnhands that may be affected by the proposed flood control project of the Redwood River at Marshall, Minnesota.

The collacted soil maps identify prime farmlands within the areas outlined on plates G-1 and G-2. There is no unique farmland at this site.

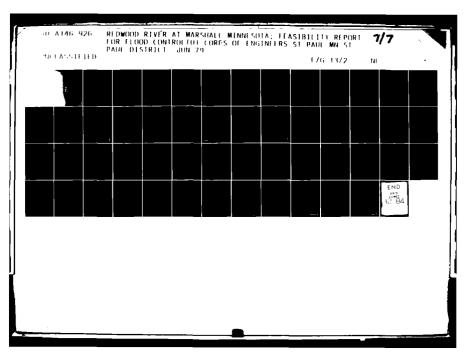
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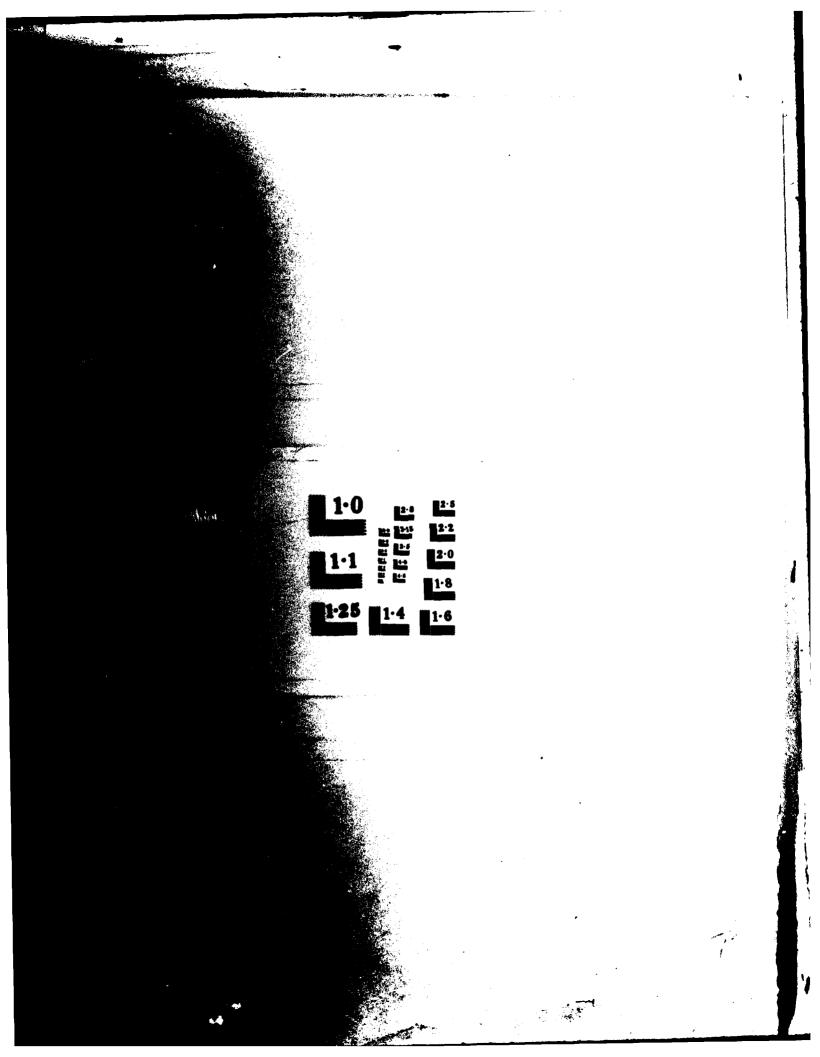
🐪 Major Harry

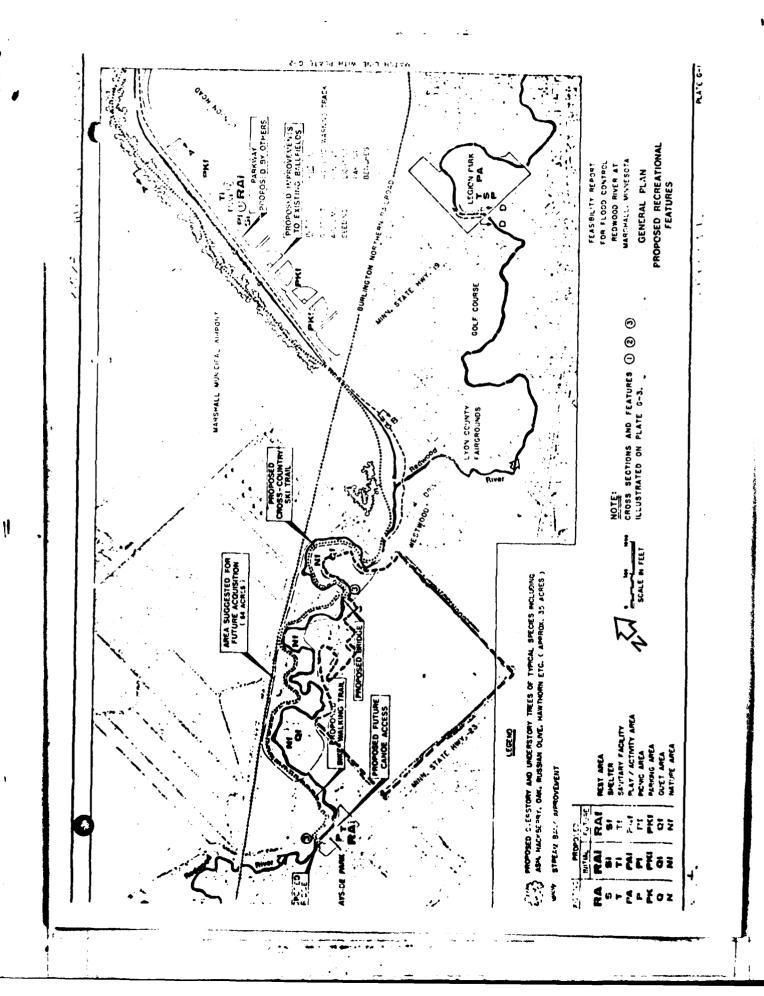
St.te Conservationist

Enclosures

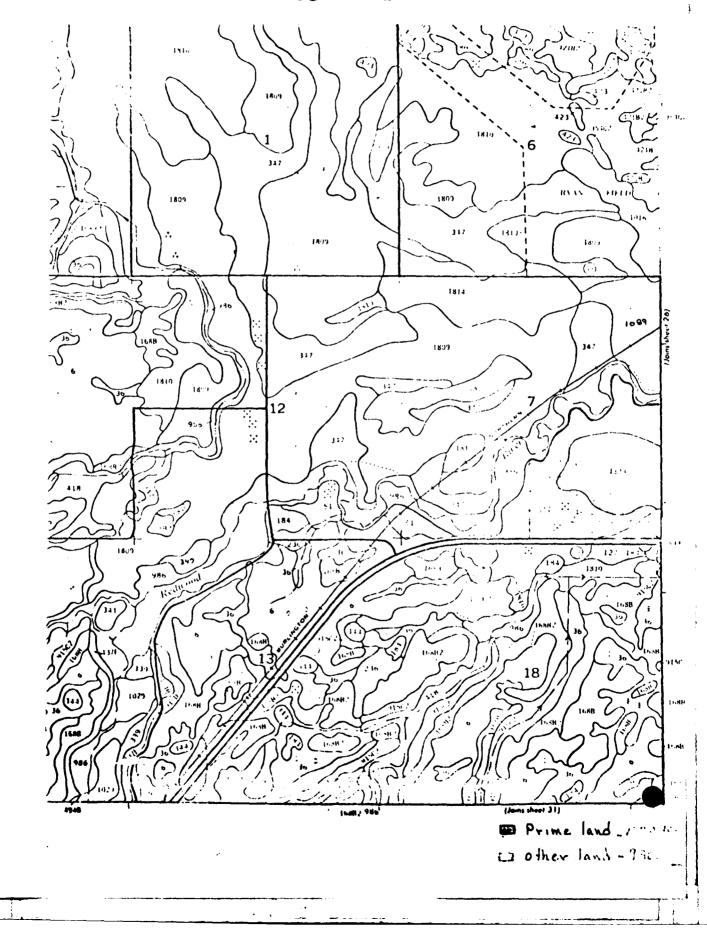






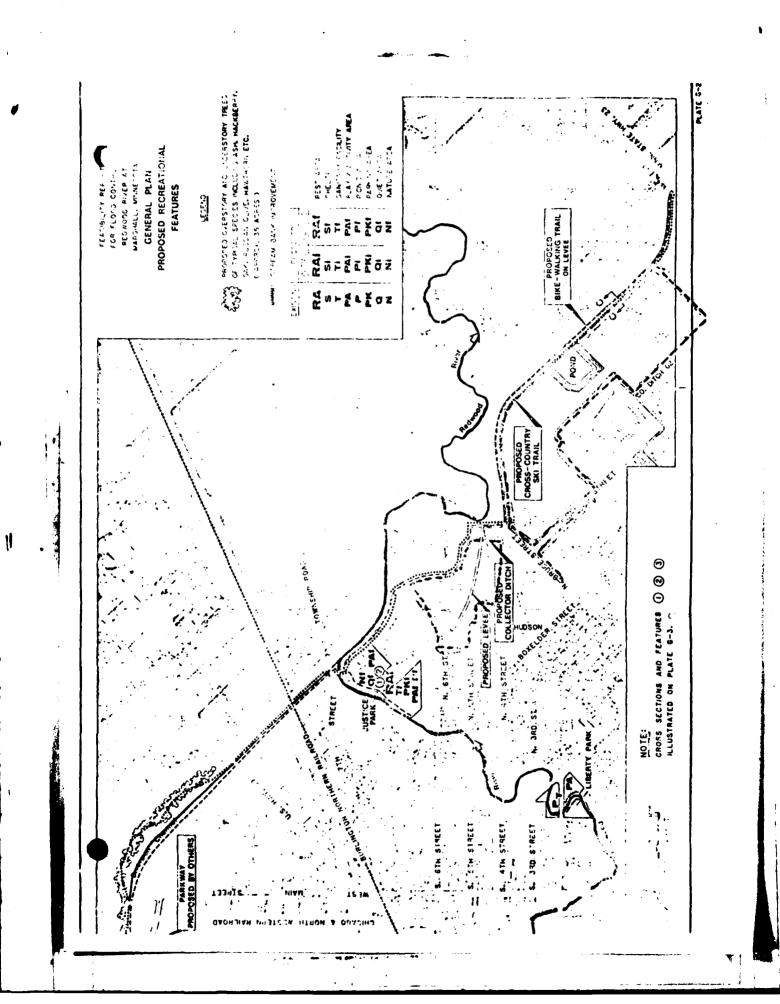


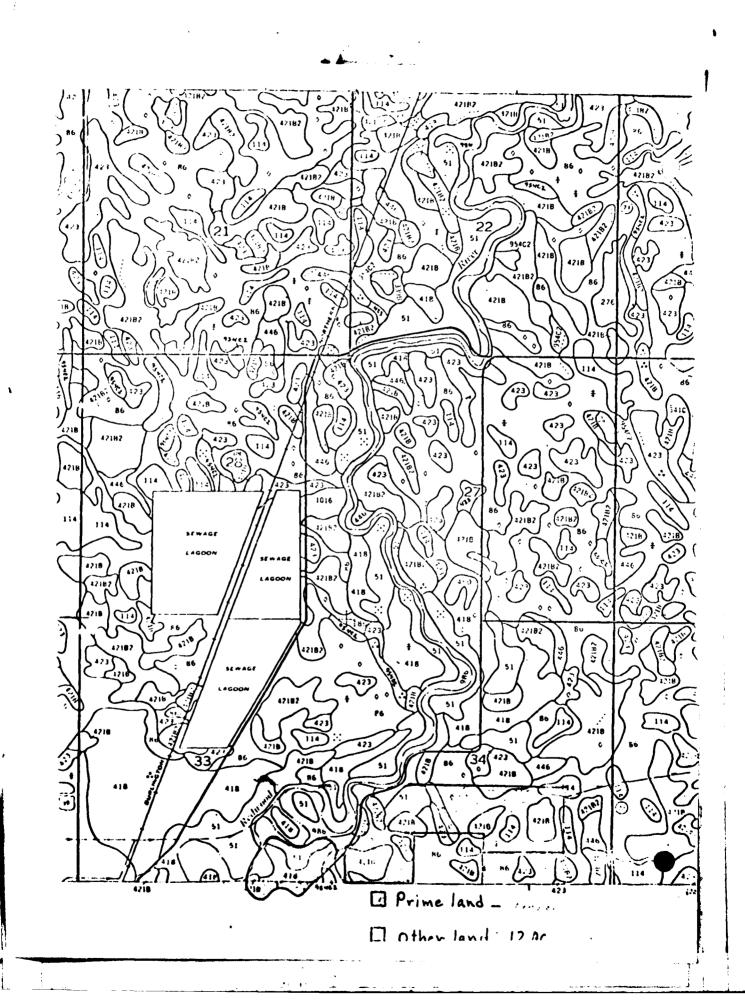
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U.S. DEPARTMENT OF COMMERCE National Oceanic and Atmospheric Administration NATIONAL WEATHER SERVICE FORECAST OFFICE Federal Aviation Building 6301 34th Avenue South Minneapolis, NN 55450

March 1, 1977

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531.1

Mr. Roger Fast Chief, Engineering Division St. Paul District Corps of Engineers 1135 U.S. Post Office and Custom House St. Paul, NN 55101

Dear Mr. Fast:

I wish to offer the following revised comments concerning the Feasibility Study and Environmental Impact Statement for Flood Control at Marshall, MN.

I would only mention the needs which the National Weather Service has with regard to its flood forecasting responsibility to the Marshall area. We see the need to locate a river gage such that complete discharge information can be obtained from a single reading. Telephone conversations between our two offices indicate that this work is proceeding which we find most reassuring.

With climatological data recently received for the 1976 calendar year a change may be of value to the body of the report. On page B7 Appendix I, of the Feasibility Report under the section labelled "Climate" I offer one revision. The total liquid precipitation for 1976 totalled 12.05 inches at the NWS's Marshall station and this quite easily surpasses the previously held record of 17.36 inches.

Sincerely,

John V. Graff

Motcorologist in Charge



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U.S. DEPARTMENT OF COMMERCE National Oceanic and Atmospheric Administration NATIONAL WEATHER SERVICE FORECAST OFFICE Federal Aviation Building 6301 34th Avenue South Minneapolis, NN 55450

531.1

**January 25, 1977** 

Col. Forrest T. Gay III District Engineer St. Paul District Corps of Engineers 1135 U.S. Post Office and Custom House St. Paul, Mn 55101

Dear Col. Gay:

Three publications from the St. Paul District Corps of Engineers have been studied recently which detail the current flood control studies for the Redwood River at Marshall, Minnesota. These publications are:

Flood Plain Information, December 1974 Draft Feasibility Report for Flood Control, November 1976 Draft E.I.S. - Flood Control, November 1976

The comments which follow are this office's efforts to supply additional facts on past floods as well as to suggest and request that Corps of Engineers-National Weather Service cooperation be maintained to assure adequate flood warning, control and avoidance at Marshall.

In neither of the afore-mentioned November 1976 reports was there any mention of the vital role which the National Weather Service has in its hydrologic responsibility of flood forecasting nor that it was responsible for accurately forecasting the floods of June 1957 and April 1969 to mention only the biggest ones.

The National Weather Service realizes the legal responsibilities and bounds of its charter, and, therefore, not only lends support to, but solicits help from cooperating agencies with related interests and concerns. As you well know, this cooperation extends to State as well as Federal agencies. In this vein, and as an important operative within the National Weather Service, this office has always given credit where deserved and we only expect an equal and fair return on this.

The late Joe Strub, my predecessor as Meteorologist in Charge, made each person in this office well aware of the delicacy with which flooding situations had to be handled. Let me sight one example in particular that occurred during the late April 1975 floods in the Mississippi River Headwaters area. Heavy rains falling over an already ripe, melting snowpack made it necessary for the Reservoir Regulation Section to increase its already sizeable discharges. In no briefing to the press or local citizens during the flood did he mention that the Corps was responsible for flow augmentation. Through carefully worded statements he attempted to save the St. Paul



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#### January 25, 1977

Page 2

District from any possible anger from Aitkin area residents.

I have been here at Minneapolis since 1969 and have been a part of many such situations. As Meteorologist in Charge, I am continuing to stress cooperation in all phases of our work. This past summer's drought with its multiple aspects was closely monitored, but each agency contributed its own complement to the crisis. The DNR conference on the Twin Cities water supply problem held on September 10 is a good example.

In a situation such as the one at Marshall where such a wide spectrum of Federal, State and Local agencies as well as private interests are involved, you are undoubtedly aware that full coordination of all duties is an absolute must. Past successes of both of our agencies speak well of the adequate ground work which was laid.

At this point in the Marshall project, I see an urgent need to coordinate our activities. This work, if started now, will allow ample time prior to the beginning of the 1977 Spring snowmelt season for us to persue other important related matters.

The problem of obtaining an accurate hydrologic picture of the Redwood River stage and discharge involves collection of same - time gage readings from both the U.S.G.S. gage in town as well as from the project structure. Our limited staff size has permitted us only recently to personally investigate the situation. Mr. Craig Sanders from this office, after an inspection of the area, made it apparent that this situation must be rectified by the establishment of a single gage. This is in agreement with the suggestions of the Regional Hydrologist at our Central Region Office in Kansas City, MO.

In a letter to John Seemann of the Reservoir Regulation Section dated October 12, 1976, I requested that work be started to resolve the problem. However, I assume that the water crises in other portions of the District took priority, thus preventing his study and immediate help, and I can fully understand this. Nonetheless, the need is still valid.

My suggestion toward consolidation of the two gages is that a wire weight or an otherwise suitable gage be set on the Highway 7 bridge 0.2 miles upstream from the diversion structure. This will suffice as an interim arragnement even though the high discharge problem of overland flow to the Cottonwood River still exists. Since rating curves and channel cross sections are presently available for both the structure and the U.S.G.S. gage, the task of synthesizing the gages does not appear to be impossible. My request of you is that we receive some affirmation that this work is being pursued so we can in turn brief and instruct our river and rainfall observor there. January 25, 1977

Page 3

In future publications from the Corps, I feel it should be explicitly mentioned that because of gage relocation, hydrologic services will be maintained despite what may appear as disorganization during the construction phase of the project. Most communities such as Marshall have law enforcement people who are instructed in reading various types of gages for us at very inopportune times. These tasks could prove most important to all of us during the construction phase should such a rainfall event affect the area. For our general information, I would like to see a tentative work schedule so we can be kept abreast of progress.

Finally, since the ultimate responsibility of operating the structure rests with the City of Marshall would you please furnish us with a copy of the current regulation manual plus any revisions which come about as a result of the planned work. It will afford us much better coordination with the city.

I am looking forward to hearing from you and would be most anxious to discuss the Marshall situation with you, your staff or other elements of the Corps. Thank you.

Sincerely,

- 1. 8 - Jun 4

John V. Graff Meteorologist in Charge



UNITED STATES DEPARTMENT OF COMMERCE Office of the Secretary Federal Diction V CNA Building, Roam 1302 55 East Jackson Builleyard Chicago, Illinois 60004

February 14, 1977

Colonel Forrest T. Gay, III Corps of Engineers District Engineer Department of the Army 1135 U. S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

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This letter transmits review comments on the draft feasibility Report for Flood Control -Redwood River, Marshall, Minnesota. The Economic Development Administration is completing their review, which we will forward under separate cover.

If you have any questions, please let us know.

Sincerely,

Jamey, J. Stirling

Representative of the Secretary

cc: Donald Baker



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U.S. DEPARTMENT OF COMMERCE National Occuric and Atmospheric Administration' NATIONAL WEATHER SERVICE River Forecast Center Rm. 1715A, 601 E. 12th Street Kansas City, MO 64106

February 1, 1977

T0:

James P. Stirling, Representative of the Secretary U.S. Department of Commerce Federal Region V CNA Building, Room 1302 55 East Jackson Blvd. Chicago, Illinois 60604

- FROM: Herman F. Mondschein Hydrologist in Charge
- SUBJECT: Draft Feasibility Report for Flood Control Redwood River at Marshall, MN (Nov 76)

Following are our comments relative to the above report:

Page 18, Line 2-3: "periodic" should be removed. Flood warnings are not at fixed time intervals, but are due to hydrometeorological conditions as they are anticipated to occur. Accordingly, we suggest in line 3 -"flood warnings issued by the National Weather Service Forecast Office in Minneapolis of impending Redwood River flood occurrences...etc."

The above comments also impact on the next paragraph. Insert a second sentence to read as follows:

"However, it is recognized that flood warnings, if timely and accurate, tend to mitigate flood losses and are essential for public safety."

Start the third sentence with:

"Nevertheless," and drop the work "periodic".

Page E-2, First Para:

We suggest a last sentence as follows: "In addition, river and flood forecasting, an integral part of the design and operation of levees and other flood control systems and basic to good multi-purpose water management, will continue to be needed."



The same or similar statements should be repeated in other general paragraphs of this nature where appropriate.

cc: Dr. Gayle W. Jackson, UMRBC Commissioner, DOC Elroy C. Balke, Regional Hydrologist, NWSCRH Donald R. Baker, DOC Water Resources Coordinator, Office of the Assistant Secretary for Policy, Washington, DC Allen Flanders, Assistant to the Associate Director, Hydrology, NWS

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UNITED STATES DEPARTMENT OF COMMERCE The Assistant Secretary for Policy Washington, D.C. 20230

December 21, 1976

Colonel Forrest T. Gay, III, USA St. Paul District, Corps of Engineers Department of the Army 1135 U.S. Post Office and Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

1

We recently received copies of your feasibility study for flood control and its associated draft environmental impact statement on the Redwood River at Marshall, Minnesota.

The organizational structure for the area of water resources within the Department of Commerce is such that direct mailing of <u>feasibility</u> reports to Washington, D.C. for <u>field</u> review can slow the review process. Therefore, may I suggest that in the future six (6) copies of reports or studies for field review be forwarded to the Secretarial Representative in the pertinent Federal region. In this instance, we have sent all copies of the feasibility study to:

> Mr. James P. Stirling Secretarial Representative, Region V Department of Commerce CNA Bldg., Room 1402 55 East Jackson Blvd. Chicago, Illinois 60604

Mr. Stirling's office will circulate the study to appropriate field offices and that office will prepare the consolidated reply to you.

In addition, please continue to send <u>all</u> copies of the Draft Environmental Impact Statements for review and comment to:

Dr. Sidney Galler Deputy Assistant Secretary for Environmental Affairs Department of Commerce Washington, D.C. 20230



I am confident that for a field review, direct mailing of the Corps of Engineers feasibility study to the Secretarial regional representative will result in a timely and efficient review process.

-2-

Thank you for your consideration in this matter.

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Sincerely,

Non Balser

Donald R. Baker Water Resources Coordinator





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Colonel Forrest T. Gay, III District Engineer U.S. Corps of Engineers, St. Paul 1135 U.S. Fost Office & Custom House St. Paul, Linnesota 55101

> RE: 76-115-194 D-COE-F36047-NN

JAN 27 1077

Dear Colonel Gay:

We have completed our review of the Draft Environmental Impact Statement (EIS) for Flood Control Redwood River at Marshall, Minnesota. Your letter of December 1, 1976, requested our views and comments on the proposed action. We note from our review of the EIS that construction is being permitted to take place within flood prone areas. We believe flood protection measures are appropriate for previously developed areas, but that a comprehensive flood control program should include restriction of further development in flood prone areas. Flood protection should be provided only for those areas which are developed at the time of the filing of the Draft EIS with the Council on Environmental Quality. Furthermore, the Final EIS should also contain additional information on the construction impacts and the impacts which will result from the completion of the flood diversion channel. Our detailed comments follow.

As part of the flood protection, a flood diversion channel will be constructed. This flood diversion channel will divert one-half of the excess of the present design discharge. These excess overflows will be discharged into the Cottonwood River Basin. Additional information and discussion must be provided on the present water quality of the receiving stream. The effect upon the water quality from the addition of flood flows also needs to be assessed. Based upon information in the EIS, we have assumed the diversion channel to be dry during normal periods of the year. Flood flows can have a high velocity and great amount of energy. The potential for erosion and channel damage should be assessed.

Since flood flows will be discharged into the Cottonwood River Basin, an assessment of flooding potential in this basin should be provided. The two watersheds are essentially next to each other and the same meteorological conditons would be expected over each basin. Therefore, if flood flows were occurring in the Redwood River Basin, one would expect flood flows in the Cottonwood River Basin. The circumstances which would change the effects of flooding in the Cottonwood Basin are the proximity to communities, areas subject to flood damages and crop and land damages and channel depth and width. The Final EIS should thoroughly discuss how the diversion of flood flows from the Redwood River Basin will affect the Cottonwood Basin. The proposed channel work may affect the ability of stream discharges to meet water quality standards. Information on the discharge points and changes in the stream's assimilative capacity which way occur as a result of construction should be provided. This information will indicate whether or not the discharger will still be capable of meeting water quality standards.

The FIS stated the flood control project is necessary to protect new development in hazard areas. It is our opinion that flood protection and flood control projects should provide protection only to areas which are presently developed, and not encourage development in flood hazard areas. To minimize flood damages and project cost, protection should be provided where development has occurred prior to the filing of the EIS with the Council on Environmental Quality. As a minimum, we recommend building restrictions on previously undeveloped flood plain areas to assure adequate flood protection to the community.

The EIS has indicated the reoccurence interval for this project has been reduced from 114 years to 59 years. The Final EIS should discuss whether or not this reoccurence interval will be further reduced.

In the EIS, water quality studies have indicated any pooling of the Redwood River could promote algal growth during periods of suitable light and temperature conditions. Part of the flood control plan calls for a ponding area to be constructed. The potential for algal blooms and insect propagation at this ponding area should be assessed.

There are two beaver dams within the watershed. One beaver dam will be removed during construction. The EIS should indicate whether or not the beaver dam is causing increased flood conditions at Redwood. This loss of the beaver dam should be avoided, if possible.

Additional information in regard to the disposal of levee excavation material should be provided.

We have rated the project as ER (environmental reservations) and classified the EIS as Category 2 (additional information necessary). The date and classification of our comments will be published in the <u>Federal Pegister</u> in accordance with our responsibility to inform the public of our views on other agencies' projects. We appreciate the opportunity to review this Draft EIS. Meen the Final LIS is filed with the Gameil on Environmental Quality, please forward 3 copies to us. If you have any questions in regard to our comments, please contact Mr. William D. Frank at 312-353-2307.

Sincerely yours,

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and the second

Gary A. Williams Chief, Environmental Review Section

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## STATE OF MINNESOTA

DEPARTMENT OF AGRICULTURE STATE OFFICE BUILDING SAINT PAUL, MINN. 55155 TELEPHONE: (612) 296-\_\_\_2856\_\_\_

LAND OF QUALITY FOODS

January 20, 1977

Colonel Forrest T. Gay, District Engineer Department of the Army St. Paul District, Corps of Engineers 1135 U. S. Post Office and Custom Office St. Paul, Minnesota 55101

RE: NCSED-PB

Dear Colonel Gay:

We have reviewed the Draft Environmental Impact Statement and Feasibility Report for Flood Control on the Redwood River at Marshall, Minnesota.

The plan proposes the conversion of 15.8 acres of agricultural land for the flood control project plus 178 acres for project-induced residential development. The report states, "This cropland loss is insignificant in itself, but a part of cumulative losses of agricultural land throughout the United States." This Department is very concerned about the loss of agricultural land in Minnesota. We feel that any loss of the magnitude proposed for this project is significant, and we do not appreciate such proposals. However, we realize the necessity for flood control projects which, hopefully, will minimize adverse conditions to the surrounding environmental, agricultural production and human life. We generally support such proposals.

it appears at this time that any agriculturally related topics have been sufficiently addressed by the Draft Environmental impact Statement and Feasibility Report.

Thank you for the opportunity to comment on the proposed plans for Flood Control on the Redwood River.

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Sincerely,

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MINNESOTA DERARTMENT OF AGRICULTURE

Rollin M. Dennistoun, Ph.D. Assistant Commissioner

RMD:hk



## STATE OF MINNESOTA

STATE PLANNING AGENCY 100 CAPITOL SQUARE BUILDING 550 CEDAR STREET ST. PAUL, 55101

February 9, 1977

Colonel Forrest T. Gay, II1 District Engineer Department of the Army St. Paul District, Corps of Engineers 1135 U.S. Post Office and Custom House St. Paul, Minnesota 55101

RE: Draft Feasibility Report for Flood Control Redwood River at Marshall Minnesota

Dear Colonel:

The Environmental Division of the State Planning Agency (SPA) has reviewed the Draft Feasibility Report for Flood Control. In general the document cites the potential impacts of the proposed measures. However, we do have the following comments and questions on the extent and manner to which some issues were addressed.

I. Land

- A) Will the proposed flood control measures have any adverse effects in the Cottonwood River Basin or in the floodplain downstream of the project's study limits?
  - 1. In order to maintain "natural" hydrologic conditions, 50% of the overflows in the gicinity of the Highway 23 roadside park will be diverted into the Cottonwood River Basin (page 22, paragraph 1). Are conditions still "natural or pre-development"? If they are not, can an equivalent percentage of overflow be diverted to the adjacent basin without damage to land or property in this area?
  - 2. Areas downstream of the study limits were not evaluated since they would not benefit from the project (F-2, paragraph 4). Might these areas be adversely affected? Is so, how and to what extent? If there are potential adverse effects downstream, shouldn't this be included in the B/C analysis as an additional cost?

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- B) Newly protected floodplains will attract development. Will this expansion plus the proposed flood control facilities necessitate future flood control measures? Will future zoning restrict development in the adjacent unprotected floodplain?
- C) The Feasibility Report states the acreage that will become available for development due to the projected flood protection. Varying figures for the land types opening up for residential development are listed. (E-13, F-20) Please consolidate and clarify this information as to the acreage of land types becoming available for development. Also, is the 64 acres suggested for future nature area acquisition included in any of the acreages of land soon available for development?

#### II. Economic

- A) Please check Table 1, Comparison of Alternatives Considered Feasibility Report. It appears (x \$1000) was inadvertantly omitted following the Economic Planning Objective Parameters of Flood Damage Reduction and Average Annual Benefits.
- B) We question the inclusion of location benefits (F-20) in the economic analysis. Since a benefit is attributed to the increased value of newly protected floodplain land, shouldn't the possible costs to downstream areas also be included as pointed out in I.A(2) of these comments?

#### III. Construction

What specifically is planned for each of the two years of construction? How will the timing of the various stages of project construction be implemented to minimize pollution (erosion, dust, etc.)?

**Basically**, the report is quite complete. Our major concerns are the possibility of adverse effects in the Cottonwood River Basin and in downstream areas beyond the study limits, the possible need for expanding flood control measures in the future, and the timing of construction.

We would like to stress that our agency supports more non-structural flood control alternatives, i.e., zoning to restrict residential development in floodplains that structural alternatives which encourage floodplain development.

If you have any questions on our comments and questions, please feel free to contact Carol Booth or Charles Kenow of my staff at 296-8254.

Sincerely.

Joseph Sizer, Director Environmental Planning Division

JS/dh



# Minnesota Pollution Control Agency

MAY 3 1 1977

Colonel Forrest T. Gay, III District Engineer U.S. Army Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

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The Minnesota Pollution Control Agency (MPCA) has completed the review of the feasibility report and Draft Environmental Impact Statement (EIS) for flood control on the Redwood River at Marshall, Minnesota. The following comments are offered for your consideration.

- In the table of State Water Quality Standards, on page E15
   13, the applicable classifications of the Redwood River should include 3C,4A & B, 5 & 6.
- 2. It is our understanding that the proposed project is the third attempt for flood control measures on the Redwood River at Marshall. Previous attempts by the City and Corps of Engineers have been unsuccessful in relieving the flood problems. Several questions remain unanswered concerning the increase in flood potential. The MPCA requests that attention be given to the following concerns:
  - a. What have been the impacts of such activities as drainage of wetlands, agricultural and municipal development, and previous flood control measures on the flood stage?
  - b. Why have flood estimates been increased so substantially from previous estimates? Is this due to the short period of record and, if so, should the floods in recent years be considered aberrant?
  - c. If drained wetlands were restored and farming practices modified, would upstream reservoirs be an alternative to channelization?

1935 West County Road 82, Roseville, Minnesola 55113

Page 2 Colonel Forrest T. Gay, III

MAY 31 1977

- 3. Due to the complex natural flow upstream and downstream of the project, attention should be given to the impact on flood stages downstream in the Redwood and Cottonwood Rivers. Previous failures to control floods would indicate that basin floods are not properly understood. The draft feasibility report should include a complete discussion on downstream flood impacts before an assessment of the benefits and the costs can be properly made.
- 4. Will further protection be needed for the wastewater stabilization ponds and other wastewater treatment systems?
- 5. Can the diversion channel which was constructed in 1963 be expanded to carry flood waters ? Would this alternative result in less aquatic biological, terrestrial, wildlife, aesthetic and water quality impacts?

We believe that these studies do not adequately address the upstream and downstream impacts and increased water pollution from secondary effects. At this time, the MPCA does not believe the proposed project adequately addresses alternatives such as upstream reservoirs and expansion of the 1963 flood control measures. Finally, we believe that further evaluation of the predicted flood levels is necessary to determine the need for and/or the ultimate scope of the project.

The MPCA appreciates the opportunity to comment on the draft feasibility report and Draft EIS for flood control on the Redwood Piver.

If you have any questions, please contact Louis Flynn, Permits Section at 296-7225.

Yours truly,

isth.x Sandra S./Gardelring Executive( Director

SSG:pah

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STATE OF WINDESOTA DEPARTMENT OF NATURAL RESOURCES CENTENNIAL OFFICE BUILDING + ST. PAUL, MINNESOTA + 55155

### March 8, 1977

ONR INFORMATION (612) 296-6157

Colonel Forrest T. Gay III District Engineer U.S. Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Dear Colonel Gay:

Staff from the Department of Natural Resources has reviewed the project documents for flood control on the Redwood River at Marshall, Minnesota and the following comments are offered:

DRAFT ENVIRONMENTAL IMPACT STATEMENT:

Section 2.024 identifies the first inhabitants as being the Dakota (Sioux) Indians whereas Section 2.026 discusses pre-historic cultural materials being found in the area. Perhaps Section 2.024 should be revised to identify the Sioux as the first inhabitants in historic times.

DRAFT FEASIBILITY REPORT FOR FLOOD CONTROL:

Page 11, paragraph 2, sentence 3. This statement is inaccurate in that the adjacent flood plain reaches...in unincorporated reaches ...are subject to Lyon County Flood Plain regulation rather than state regulation.

Page 18, paragraph 2, sentence 3. This statement downplays the longterm results of flood plain zoning regulations. While it is true that flood plain zoning will not significantly reduce flood damage in the short-term, the long-term result will be to reduce non-conforming flood plain uses which will reduce flood damages. We would request that you be more generous to the concept of flood plain management in your next draft.

Page 36, Level of Protection Section. According to this discussion, standard project protection will not be provided by all the levees proposed in this project. The exact impact of these levees being overtopped has been given only cursory review. Questions which should be addressed in the final document include: if levees are overtopped, what are the depths of flooding; what are the probable dollar damages; and what provisions are being made to provide for internal drainage? How is the project design being reconciled with the fact that Minnesota Flood Plain Regulations NR 89(c)(2) (aa) require that levees built for urban protection shall have a minimum height of at least three feet above the elevation of the regional flood or at the elevation of the Standard Project Flood, whichever provides the greater protection from

# Col. Forrest T. Gay III-USCE

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Page F-7, Table F-1 and Section F-15. This section and table imply that public buildings would continue to be constructed in a nonconforming manner even though flood plain regulations would be in affect. Public buildings would have to conform to any applicable local ordinances. The average annual equivalent value of this future growth (\$5800) would, therefore, not apply.

-2-

Page F-20, Location Benefits. We would strongly recommend that location benefits, as used in the benefit/cost analysis outlined on page F-20, be re-evaluated. There is no shortage of buildable land around the City of Marshall so there should be no real net gain in land value. The increase of \$1900 per acre is a one-time windfall gain for certain landowners and would come at the expense of other lands that are suitable for development without construction of the flood control project.

### SOME GENERAL COMMENTS

We would like to reiterate our concern about the problem of crossover flooding. While the proposed project is designed to reduce flood damages in Marshall, the problem of cross-over flooding is of regional concern and should be analyzed as such.

We are also concerned about the general aesthetic impact that flood control levees have. We would hope that efforts would be expended, particularly in future projects, but to whatever extent is possible for the Marshall project, to mitigate aesthetic concerns into project design.

## MITIGATION MEASURES

We offer the following as acceptable alternatives for mitigation of the 4.1 acres of forested habitat that will be lost:

- 1. Acquisition of additional land adjacent to the Redwood Wildlife Management Area in Section 28 of Lynn Township, T.111N., P.42W., This could either be more river bottom, woods or else cropland for a food plot or nesting cover.
- 2. Acquisition of additional land adjacent to the Russell Wildlife Management Area in Lyons Township.
- 3. Restoration and future protection against the filling of the Type IV wetland located in the Eastern ½ of the Southwestern ½ of Section 32, T.112N., R.41W., in Fairview Township.

In conclusion, the State of Minnesota supports the general concept of the proposed project, that is flood damage reduction on the Redwood River in Marshall, Minnesota. You can be assured of our continued interest and support for the goal of flood damage reduction.

Sincerely, Gerald D. Scinwill, Director

Gerald D. Scinwill, Director Division of Waters



# MINNESOTA DEPARTMENT OF TRANSPORTATION

TENTH & PACIFIC, BOX 758 WILLMAR, MINNESOTA 56201

PHONE: (612) 235-4554

September 29, 1978

Department of the Army St. Paul District, Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Minnesota 55101

Attn: Forrest T. Gay, III

RE: Flood Control - Marshall, Minnesota

Dear Mr. Gay:

In response to your letter of August 29, 1978, which is addressed to Mr. F. C. Marshall, we have reviewed the effect of raising the T.H. 23 rendway to act as a dike (along with County Road No. 7) upstream from the City of Marshall. This relates to your modification 4 of Plan 5U on Plate D-1 "considered alternatives upstream reach".

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Consideration of raising only the westbound Trunk Highway 23 roadway to a maximum 3 feet above the eastbound roadway causes a problem at the highway junction with C.S.A.H. 7. Your Plate D-1 does not indicate the loft-turn lanes, nor the T.H. 7 junction as they exist today. In any case, a 3 foot elevation difference between roadways at this location is not acceptable; and, at this location, the eastbound roadway would also have to be raised at least 2 feet. Five accidents (one fatal) have been investigated at this junction in the past year.

The entire junction of C.S.A.H. 7 and T.H. 23 would have to be modified in elevation to provide suitable access. Additionally, our construction plans for T.H. 23 show that a 24 inch diameter concrete culvert is constructed through C.S.A.H. 7 to the north of T.H. 23 which drains the north roadway ditch and the proposed Redwood River Basin.

### AN EQUAL OPPORTUNITY EMPLOYER

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We would recommend that consideration to given to constructing a dike adjacent to T.H. 23 right-of-way to the desired classified. This dike could be swing northerly and tied in with the ranged C.S.A.H. 7, some distance north of its junction with a city street, is but 500' north of T.H. 23. Such dike construction need not disrupt trunk highway traffic and might persibly be considered less expressive than reconstructing T.H. 23. One field entrance access, some 1300' west of C.S.A.H. 7 would possibly require a sand bag plug at times of high water.

Please give maximum consideration to reducing the effects of this project to our wayside rest area.

Thank you for the opportunity to commont upon the purposed alternative SU, modification 4.

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Sincerely,

K. A. Madole, P.E. District Director

Copies: F. C. Marshall W. C. Merritt -

# 25 August 1978

Mr. Robert F. Felt Chief, Expirons stal Resources Branch Englishering Oldstion Toportiset of the Army St. Foal Discret, Corps of Englishers 1435 F.S. Post Office & Conten Bouge St. Parl, Minnesta 55101

Dear Mr. Post:

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RE: Archaeo'scheal Subsy-Flood Councel Preject Marshill, Minnesets

# MIS Referral File . "ler G193

CARAL SOCIETY

COMPANY SHITT

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The Algory very such for scaling us the report the Algoridation is a frequencial because of a frequencial field control Project in Localed 1. More staff, the second for us to tally contart with user finding that no crelecological size will be defined by the proposed flood control project, it is note that us to be able to accurately locate that kinds of investigations taken is and where. I have found it deficient to be this evaluation further the report. Therefore, I would appreciate it if you could provide this office with a copy of the appreciate it if you could provide this office with a copy of the appreciate and more showing the location of the surface finds, test pits, areas subjected to surface account to the proposed project locations.

f sight add that it is also is portant to review fill sources for leves constructs of all these lie outside the areas surveyed, we would like the opportuality to make that review.

Thank you for your continuing support for preserving Minnesota's cultural resources.

Sinceraly Rüssell W. Fridley

State Historic Preservation Officer

Founded 1849 • The oldest institution () the state

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LYOR COUNTY DE HIGHWAYS

September 7, 1978

Marshall, Minnesota scasa

ROBERT J. MCPARTEIN

ENGINEER

Forest T. Gav, 100 Colonel, Corps of Engineers District Engine :: 1135 U.S. Post Holze & Custom House St. Paul, SN - 55101 Attention: NCSE D - PB

Dear Mr. Gay:

In response to your lotter of August (2) 1978, regarding plan 50 MOD.4 with the Related River in Multi 11, IN, the following is an answer to the questions you used.

CSAH 7 is currently not up to standar for the volume of traffic it is projected to carry. Any index dent along this road world have to be concludent with the for design standards. Thus, an 8 foot fill section is not only a volume of fill in the road area, but also in the star of a area and slope to next the existing grade. (See the althous scheet for a typical section involving the 3 foot fill.) The level could be constructed to serve as flood protection, and serve the highway mends as well.

Traffic safety would be slightly weater 1 with a raise in the road profile, but not something that the be prohibitive. Anytime the road deviation from the grade of the ditch, the possibility of a serious accident is greater. However, when a wide cheuder and flat inslope is provided, the "unsafe condition" is greatly reduced.

There may be problems regarding notes to and from adjacent properties, but this is not a direct concern of the County Highway Department. One area of minor concern is CSAH 7 south of T.H. 23. With the grade of T.H. 23 raised, CSAH 7 will have to match.

Another minor concern would be the estimates of having an elevated road abutting a residential area. I am sure the City of Marshall and concerned residents would object in regards to this problem.

The major objection that the Lyon County Highway Department would have against this project is the cost factor. With the amount of fill required, it would but a drain on our funding sources, which is a priced at spiraling upward, and the that inflation and rices are spiraling upward, and the funds are not keeping up, I cannot justify spending County money for a project such as this, when so many other roads are in need of repair.

An Equal Opportunity Employer

Post st T. Gay, DIT

# September 7, 1978

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Even if the Correctore to essist in the financing, it would users to be an unnecentary sheart of fill to place - hence, tax and the state. Another diternative that could be considered Introduct presented in term sketch is the possibility of present curves to the test of CSAH 7 10% and north of T.H. 23 its. As a site matter total be less contly in that roadway weather is large to be reclarged, and the fill would be smaller in volum. However, this plan would reduce the volume of the Deceiver by a slight a punt.

In surgery, the position of the Lyon County Highway Departint i:

- 1) The could be built to act as a flood reservoir and perve the transportation needs.
- 2) Traffic Safety problems would be worsened, but only to a sm. 11 degree.
- 3) Access would be a minor problem, but more so to the City, not the County.
- 4) There may be an aesthetic problem with the local people.
- 5) There is a major problem with financing on the County level.
- 6) A more logical and cheaper solution has not been offered for consideration.

If you wish any further comments, please feel free to contact me.

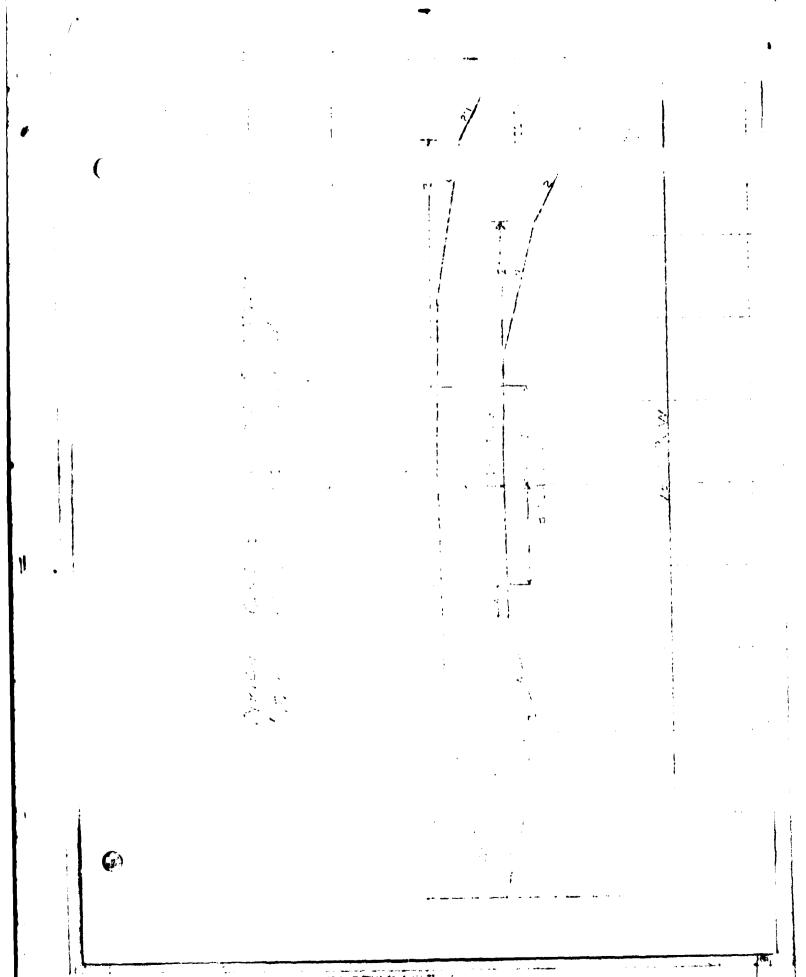
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Yours truly, Clarid fin Robert J. McPartlin

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Office of CITY ADMINISTR/ Phone (507) 532: P. O. Box 47;

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December 9, 1976

Mr. Forrest T. Gay, III, Colonel District Engineer Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Mn. 55101

RE: NCSED-ER

Dear Mr. Gay:

I am writing in response to your letter of December 1, 1976 regarding an environmental impact statement being prepared for a flood control project on the Redwood River at Marshall, Minnesota.

After review, the proposed project, as presented, appears to be totally consistant with and complimentary to all existing and currently proposed local land use plans, policies, regulations, and objectives. The same holds true for the various plans and policies for flood control, traffic thoroughfare, parks, and zoning.

While the City of Marshall does not now have a Comprehensive Master Plan for the City, it is possible that one will be developed within the next couple of years. However, it would not appear at this time that a Comprehensive Master Plan would result in any potential conflict with the proposed flood control project.

I trust this provides the necessary information requested. If the City of Marshall can provide any additional assistance in the development of this project, we will of course do so.

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Sincerely yours,

James R. Heller City Administrator

JRH:LM

1. 19. 14 Person I . altera CITY HALL BUILDIN. 344 WEST # 101 CIN Phone 507-532-26at Land Store 1: 161\_ 56253

# OFFICE OF CITY ENGINEER

April 11, 1978

Mr. J. R. Calton Chief, Planning Branch Engineering Division Department of the Army St. Paul District Corps of Engineers 1135 U.S. Post Office & Custon House St. Paul, NN 55101

Re: NCSED-PS

Dear Mr. Calton:

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Mr. Stonley Kummer of your office recently furnished no with a revised draft feasibility report for clood control on the clood River here in the City of Marshall. If ave reviewed this  $c \in P$  lifty report and would offer my comments to you for your consideration.

It is my opinion that the project as designed for a 133 year degree of protection would very adequately provide the procession to the City of Marshall and adjacent area. Protection to the Same and Project Flood level would appear to be beyond the requirements as creatisticity feasible fleed protection level. This subsitive live plan which included the raising of County Highway No. 7 and State Fighway No. 23 as flood barriers, additional leves height, railroad embandment protection, additional structures work, etc. in my opinion would be an extremely costly and quescionable moded level of protection.

Consequently, we basically agree with the feasibility report and plans as selected for the 133 year flood recurrence frequency protection level.

However, there are several minor areas of the plan that we would request further consideration be given to at the time of the detailed plans preparation. These items would not materially affect the feasibility report as written but are items that we feel should have some attention at some later data the plans procedure the detail planning stage. One of the planet constant is the last 1 may between County State Aid Highway No. 7 and the wayside park area in the upstream protection area. Mr. J. R. Calton Abill **11, 1978** Page Two

In the openion, all lands between the proposed leave and the Burlington-Nations if if road will be two all practical purpose undevelopable due to the restriction should be blacked on this area. Therefore, it may been resonants, our and the practical to purchase these lands in feetitle is the interval of the project rather than only obtain easements on a pertion of these land. This support this statement, the report also state that as we to this property will be permanently affected. If this becomes a tast, then the lands cost of the project budget would have to be increased considerably. It should also be noted that these lands could then be used for recreational purposes in the form of quiet areas, blue trails and so on as was discussed in the report. The report refers to the prior as being a part of the advantage of the plan.

It is all site countageous to make a more complete analysis of the location of the lower in the area of Mile 71 to determine whether or not the loce should follow the channel in a more close and parallel manner. At the location to be is presently a considerable area of land above flows plain local. This land renders itself to being very desirable developable property and a lower would cut off this land and would potentfally restrict development in the area.

In the area of Mill 66 further review should also be given to the location of the levee with the possibility of foll bing the channel more closely thum as proposed.

Another area that I would request a further review of would be the ponding area located on the dometream improvement beth on Highway 23 had County Fond Net 7. This popling area is a sizeable area that would be underelopable and could present some continual maintenance problems particularly as it relates to the relatively infrequent periods of time that the pond will actually be utilized. During the detail plan preparation I would request that we further review this and look at other alternatives as well as design alternatives.

We appreciate your attention to this project and I can advise you that the City of Mirchaell is very concerned over flood problems and responsive to flood to remember. As a result of the 1969 flood it was realized that there are some deficiencies. However, it should also be noted that we realize now that we are quite vulnerable to flooding conditions and therefore hope that this project can be expedited as quickly as possible to provide the protection as outlined in the feasibility report.

Thank you for your opportunity to review this feasibility report and comment on it.

Sincerely,

Duane D. Aden City Engineer

DDA: LM

Tipes M. R. - Recover a little good the

CITY HALF BUILD: 6.9 CITY OF 344 WEST MAR Phone 507-532-26 BREAR A. R. CLORELDA, RE C. 11:00200010 56250

OFFICE OF CITY ENGINEER February 21, 1979

Mr. Forrest T. Gay, III Colouch, Corps of Engineers District Engineer Department of the Army St. Paul District Corps of Engineers 1135 U.S. Post Office & Custom House St. Paul, Mi 55101

Ref: NCSED-PB

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Dear Colonel Gay:

Mr. Robert Northrup of your office recently contacted Mr. Duane Aden, our City Engineer, pertaining to the degree of protection for proposed Flood Improvement Project for the City of Marshall, Minnesota.

We discussed this matter at the City Council Meeting on February 20, 1979 and it is the determination of the City staff and City Council that the originally proposed 133 year Flood frequency would still be a most acceptable level of protection. This is in accordance with the draft feasibility report as prepared by your office. We did evaluate the 150 year Flood frequency protection level and it is our opinion that the additional work and cost involved do not warrant the relatively small degree of additional protection.

We would request that you proceed accordingly and expedite our project us quickly as possible. If you should any further comments or questions pertaining to this decision, you may contact Mr. Duane D. Aden, the City Engineer.

Sincerely,

Ribert Charles and Robert J. Schlagel Mayor of Marshall, MN.

RJS:jb

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CITY HALL BUILDING 344 WEST MAIN Plione 507 532-2612

Aperinasoli 56258

OFFICE OF CITY ENGINESA April 18, 1979

Mr. Formest T. Gay, III Colonal, Corps of Engineers District Engineer Department of the Army St. Paul District Corps of Engineers 1135 U.S. Post Office and Custom House St. Paul, MV 55101



Ref: NCSED-PB

Dear Colonel Gay:

Transmitted berewith please find the City of Marshall's Resolution No. 228 pertaining to the City's approval of a Flood Control Project and its intent and willingness to conjerate with the United States in the construction of the project. This resolution has approved on accordance with the Camibility report prepared by the Corps of Engineers and the appropriate local responsibilities and cost sharing analysis outlined in this report.

Also enclosed is Resolution No. 289 which is a resolution declaring the intention of the City of Marshall and the Corps of Engineers concerning local participation and recreation features as a part of a project for flood control.

We are aware of the fact that the cost sharing provisions are being changed to a 20 local share of the total project as per mecent presidencial policy. However, since this project has been under development and preparation for approximately F or 9 years, we would suggest that the funding for the project be in accordance with the rules and policy as have been in effect during the development of this project and as outlined in the feasibility report. If it does become absolutely necessary to change the method of funding for the project, we would acknowledge this fact and I would assume the City of Marshall would be receptive to whatever decision is appropriate. Particularly due to the fact that the project is of utmost importance to the residents of the Marshall community. Mr. Forrest T. Gay, 111 Colorel, Corps of Engineers District Engineer Department of the Arry St. Paul District Corps of Engineers 1135 U.S. Post Office and Custom Home St. Paul, MN 55101

Ref: NCSED-PB

Page two

It is also our understanding that more formal assurances will be required on the part of the city following the congressional authorization and prior to any construction activities through the Corps of Engineers contracts.

We would request that we continue to expedite this project as quickly as possible so that we can eliminate the existing potential flood damage and inconveniences to the residents of the Marshall community. Thank you for your assistance.

Sincerely, Value to Raddonal \_\_\_\_\_ Robert J. Schlagel / Mayon

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| рт. – с.<br>2. – Дл.<br>– с. н. М. М. | UNIVERSITY OF MINNESOTA<br>Twin cities | Department of Anthropology<br>215 Ford Half<br>Minneapolis, Minnesota 55455 |
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January 14, 1977

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Col. Forrest T. Gay III District Engineer St. Paul District, Corps of Engineers U.S. Post Office Building St. Paul, Minnesota 55101

Att'n: ED-PB

Dear Col. Gay:

I have examined the frasibility report on flood control on the Redwood River at Marshall, Minnesota, and agree with the statements and recommondations relating to cultural resources that appear on pages 6-8 and 43-44.

Sincerely, 21/10 TIL

Elden Johnson State Archaeologist

EJ:dl cc: R. Fridley CHICAGO AND TRANSPORTATION COMPANY March 26, 1979

ASSISTANT DIVISION MANAGER ENGINEERING

File 1-51-9

Nr. F. T. Gay, III Colorel, Corps of Engineers, Dist. Engr. St. Paul District-Corps of Engineers 1135 U. S. Post Office & Custom House St. Paul, Minnesota 55101

# Attention: Planning Branch

Dear Mr. Gay:

Please refer to your public notice regarding flood control plans involving dredging and filling in the Redwood River at Marshall, Minnesota, dated February 28, 1979.

The proposed recreation facilities with respect to this project proposes walking-biking trails and cross-country ski trails in two locations along the diversion channel around Marshall. Minnesota. While the plans are not definitive in the location of these trails, it would appear that it would be necessary some time in the future that these trails will cross the track of the Chicage & North Western Transportation Company. At that time it will be necessary for a license to be executed between responsible public body and the Transportation Company for these crossings.

It would appear from this notice that there are no other facilities that will affect the Transportation Company. I would appreciate advice as to how this will be handled in the future.

Sincerely,

Tesar

Asst. Div. Mgr.-Engr.

MAE:jm

PO BOX 201 / 600 + 14-41 STICLET, N.W. / MASON CITY, IOWA S0401 / (515) 424-1659

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LAW OFFICER MOLTER, RUNCHEY, LOUWAGIE & WELLMAN WEBTERN STATE BANK BUILDING EAST COLLEGE DRIVE MARSHALL, MINNESOTA 56258

ON B. MOLTER OBERT C. RUNCHEY CSEPH H. LOUWAG'E TEVEN C. WELLMAN

March 30, 1977

PHONE

807-832-3281

Corps of Engineers St. Paul District Office 1135 U.S. Post Office and Custom House St. Paul, Minnesota 55101

> RE: MEETING--COUNCIL CHAMBERS--2-17-77 MUNICIPAL BUILDING 344 WEST MAIN STREET MARSHALL, MINNESOTA 56258

Gentlemen:

Major Walter H. Heme addressed a group of Lyon County residents relative to the proposed flood control project on the Redwood River at Marshall, Minnesota, on February 17, 1977. A number of land owners were present and the undersigned represented the owners of land located to the south of said project.

The owners of valuable property on the upstream area would be directly affected by any flood control project. We pointed out that under the proposed 5U plan, the undersigned owners of the Westside Acres and their property to the south of Plan 5U would sustain substantial damages for valuable property taken for the levy involved, together with probable damage from flooding in the future.

A detailing of the previous floods experienced in this area were made known at this hearing. However, it was disclosed by the Corps of Engineers that there was no data relating to the amount of run-off water resulting from the extensive drainage and tiling of the agricultural lands in this area to the present time. There have been numerous floods in the recent years from the swift run-offs resulting in floods from any above average rains. Consequently, our area is now subjected to flooding conditions frequently, whereas heretofore floods were experienced during very infrequent periods. We strongly urge that the most realistic solution to the problem is to have the diversion channel extended between the Redwood River and the Burlington Railroad as identified in Plan 6U. This plan would clearly result in the most feasable control necessary for the discharge of flood waters. Additionally, the costs of damages due to the property of the undersigned would be greatly reduced, which would not be the case under the proposed plan 5U.

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The long range costs of this project, together with the lower land acquisition costs under plan 6U clearly make this the preferable plan for a proper flood control project.

We urge you to adopt plan 6U as the most feasable long range flood control project for the needs of our area.

Yours truly,

Zalutt. Qunchey

Robert C. Runchey, Representative for Westside Acres

RCR/mmm

cc Representative Richard Nolan 1019 Longworth Office Building Washington, D.C. 20515 STATEMENT BY DISTRICT ENGINEER U.S. ARMY CORPS OF ENGINEERS, ST. PAUL DISTRICT

MARSHALL, MINNESOTA, PUBLIC MEETING

INTRODUCTION

THANK YOU, MAYOR SCHLAGEL.

SLIDE 1 -ST. PAUL DISTRICT LOGO

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GOOD EVENING LADIES AND GENTLEMEN. I AM MAJOR WALTER HEME, DEPUTY DISTRICT ENGINEER FOR THE U.S. ARMY CORPS OF ENGINEERS, ST. PAUL DISTRICT, HEADQUARTERED IN ST. PAUL. THIS EVENING I WILL DISCUSS OUR INVOLVEMENT IN THE STUDY FOR FLOOD CONTROL IMPROVEMENT ON THE REDWOOD RIVER. FIRST, I WOULD LIKE TO INTRODUCE SOME OF THE PEOPLE WITH ME HERE TONIGHT WHO HAVE BEEN RESPONSIBLE FOR THE FLOOD CONTROL STUDY. THEY ARE MR. ROBERT STENFORS, MR. JIM HOLLERAH, AND MR. TED ONDLER OF OUR STAFF, AND MR. PAUL KERAHEN OF WEHRMAN, CHAPMAN, ASSOCIATES, INC., WHOM WE HAVE CONTRACTED TO CONDUCT THE FLOOD CONTROL STUDY. THESE GENTLEMEN ARE AVAILABLE THIS EVENING TO ANSWER ANY SPECIFIC QUESTIONS YOU MAY HAVE CONCERNING THE STUDY.

BEFORE WE BEGIN, IF YOU HAVE NOT DONE SO ALREADY, I ASK THAT YOU FILL OUT THE ATTENDANCE CARD WHICH WAS GIVEN TO YOU AS YOU ENTERED. THESE ATTENDANCE CARDS ARE USED TO RECORD YOUR NAMES AND ADDRESSES SO THAT WE CAN INFORM YOU OF ANY FUTURE PUBLIC MEETINGS

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RELATEL TO THIS PROJECT AND ALSO TO IDENTITY THOSE WHO WISH TO MAKE A STATEMENT HERE TONIGHT. TO ASSURE THAT ALL STATEMENTS MADE TONIGHT WILL BE AVAILABLE FOR FURTHER CONSIDERATION, WE HAVE ARRANGED FOR MR. CHARLES LEHMAN, TO RECORD THE PROCEEDINGS OF THIS MEETING. PLEASE IDENTIFY YOURSELF BY NAME WHENEVER YOU MAKE A STATEMENT OR HAVE A QUESTION SO THAT MR. LEHMAN CAN PROPERLY RECORD YOUR PART IN THE MEETING.

SLIDE 2 - PURPOSE OF MEETING REPORT COVERS-FR AND EIS

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OUR PURPOSE FOR BEING HERE THIS E.\_ JING IS TWOFOLD: FIRST, TO INFORM YOU OF THE PROGRESS AND FINDINGS TO DATE ON THE FLOOD CONTROL STUDY AND SECOND, AND MORE IMPORTANYLY, TO OBTAIN YOUR VIEWS ON THE STUDY.

AS INDICATED IN OUR ANNOUNCEMENT OF THIS MEETING, WE RECENTLY COM-PLETED A DRAFT FEASIBILITY REPORT AND ENVIRONMENTAL IMPACT STATEMENT PRESENTING THE PRELIMINARY RESULTS OF OUR STUDY FINDINGS. COPIES OF THESE REPORTS HAVE BEEN MADE AVAILABLE TO ALL KNOWN INTERESTS INCLUDING FEDERAL, STATE AND LOCAL AGENCIES, ORGANIZATIONS AND INDIVIDUALS FOR REVIEW AND COMMENT.

AFTER RECEIVING ALL VIEWS AND COMMENTS, INCLUDING THOSE PRESENTED HERE TONIGHT, WE PLAN TO REVISE THE DRAFT REPORT AS NECESSARY, TO ENSURE THAT THE PLAN ULTIMATELY RECOMMENDED TO CONGRESS TRULY REFLECTS YOUR NEEDS AND DESIRES. THUS, THE RESULTS OF OUR MEETING TONIGHT REPRESENT AN IMPORTANT STEP TOWARD MEETING THAT OBJECTIVE.

#### BACKGROUND

SLIDE 3 -BASIN MAP THE CITY OF MARSHALL IS LOCATED ON THE REDWOOD RIVER, A TRI-BUTARY OF THE MINNESOTA RIVER AS SHOWN ON THIS SLIDE. THE REDWOOD RIVER HAS A HISTORY OF FLOODING CAUSED EITHER BY EXCESSIVE RAINFALL OR SNOWMELT. THE SECOND LARGEST FLOOD OF RECORD ON THE REDWOOD RIVER OCCURRED IN JUNE 1957 WHEN MORE THAN 8 INCHES OF RAIN FELL OVER THE BASIN AND CAUSED THE RIVER TO OVERFLOW ITS BANKS INUNDATING MOST OF THE DEVELOPED AREA OF MARSHALL. THIS NEXT SERIES OF SLIDES SHOWS THE EFFECT OF THE 1957 FLOOD IN MARSHALL.

BLANK SLIDE

1957 FLOOD SLIDES

> AT THE REQUEST OF THE CITY OF MARSHALL POLLOWING THE 1957 FLOOD WE MADE A STUDY OF THE CITY'S FLOOD PROBLEM. THIS STUDY LED TO THE CONSTRUCTION OF THE EXISTING FLOOD CONTROL PROJECT IN 1963.

EXISTING FLOOD CONTROL PROJECT

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AS SHOWN ON THIS SLIDE THE EXISTING FLOOD CONTROL PROJECT AT MARSHALL INCLUDES A LEVEE ABOVE THE BURLINGTON NORTHERN BRIDGE AND NO CLEARING AND SNAGGING IN THE UPSTREAM REACH, A 2.4 MILE DIVERSION CHANNEL TO DIVERT EXCESS FLOOD FLOWS AROUND THE CITY AND CHANNEL IMPROVEMENTS IN THE DOWNSTREAM REACH. THE DIVERSION CHANNEL WAS DESIGNED TO PASS A MAXIMUM DISCHARGE OF 5,000 CFS WHILE PERMITTING NORMAL FLOWS UP TO 1,500 CFS TO PASS THROUGH THE NATURAL CHANNEL THROUGH THE CITY.

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IN APRIL 1969, THE LARGEST FLOOD OF RECORD OCCURRED ON THE RED-WOOD RIVER WITH A DISCHARGE OF  $\theta_{1}$ ,000 CUBIC FEET PER SECOND. FROM THIS FLOOD WE FOUND THAT THE DIVERSION CHANNEL WOULD HAVE HAD SUFFICIENT CAPACITY TO PASS THE PEAK FLOW BUT THE PROBLEM WAS THAT THE FLOW DID NOT ADEQUATELY REACH THE DIVERSION STRUCTUPE.

DURING THE 1969 FLOOD EMERGENCY MEASURES WERE UNDERTAKEN BY THE CORPS OF ENGINEERS UNDER PUBLIC LAW 99 AS REQUESTED BY THE CITY OF MARSHALL. COUNTY POAD 7 WAS RAISED TO PREVENT RIVER OVERFLOW FROM IN-UNDATING THE CENTRAL AREA OF MARSHALL AND HIGHWAY 23 WAS BREACHED TO PERMIT PART OF THE OVERFLOW TO FLOW SOUTHWARD INTO THE COTTONNOOD RIVER BASIN THEREBY FURTHER PREVENTING FLOCOTING IN MARSHALL. THIS NEXT SERIES OF SLIDES DEPICTS THE EMERGENCY ACTIONS THAT WERE UNDERTAKEN IN THE UP-STREAM REACH IN 1969.

19/19 FLOOD SLIDES UPSTREAM

> DURING THE 1969 FLOOD ANUTHER PROBLEM DEVELOPED IN THE DOWNSTREAM REACH. IN THIS REACH IT WAS NECESSARY TO CONSTRUCT AN EMERGENCY LEVEE TO PREVENT FLOODING OF THE MORE RECENTLY DEVELOPED AREA IN THE VICINITY OF SOUTHWEST STATE COLLEGE, AS SHOWN ON THESE SLIDES.

1969 FLOOD S. 1DES DOWN-STREAM

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WITHOUT FURTHER FLOOD CONTROL IMPROVEMENTS OR EMERGENCY MEASURES THE CITY OF MARSHALL REMAINS SUBJECT TO FLOODING BY FLOODS EQUAL TO OR GREATER THAN ONE HAVING ABOUT A 5 PERCENT CHANCE OF OCCURRINF DURING ANY ONE YEAR (20-YEAR FLOOD). THIS NEXT SLIDE SHOWS THE OUTLINE IN LIGHT BLUE OF A FLOOD HAVING A 1 PERCENT CHANCE OF OCCURRING DURING ANY 1 YEAR (100-YEAR SLIDE OF 100-YEAR FLOODPLAIN

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FLOOD). THE 100-YEAR FLOOD IS APPROXIMATELY EQUAL IN MAGNITUDE TO THE RECORD 1969 FLOOD. THE RETRACTED DARK BLUE OUTLINE SHOWN ON THE SLIDE IS THE 100-YEAR FLOOD OUTLINE FOR PROPOSED CONDITIONS WHICH I WILL DIS-CUSS LATER. THE EXISTING CONDITIONS FLOOD OUTLINE IS TAKEN FROM OUR FLOODPLAIN INFORMATION REPORT WHICH WE COMPLETED FOR THE CITY IN DECEMBER 1974.

#### BLANK SLIDE

DUE TO THE LIMITATIONS OF THE EXISTING FLOOD CONTROL PROJECT AS EXPERIENCED DURING THE 1969 FLOOD, IT IS EVIDENT THAT THE PRESENT PRO-JECT CANNOT PROVIDE SUFFICIENT FLOOD PROTECTION TO MARSHALL AND THE DEVELOPED FLOODPLAIN AREA ADJACENT TO THE CITY. ACCORDINGLY, IN 1972, RESOLUTIONS WERE RECEIVED FROM LYON COUNTY AND THE CITY OF MARSHALL REQUESTING THAT A STUDY BE CONDUCTED TO DETERMINE WHAT IMPROVEMENTS COULD BE MADE TO PROVIDE ADDITIONAL FLOOD PROTECTION AND INCREASED EFFICIENCY OF THE EXISTING FLOOD CONTROL PROJECT. LATER, AS THE STUDY PROGRESSED, MARSHALL CITY OFFICIALS INDICATED A DESIRE FOR IMPROVED RECREATIONAL OPPORTUNITIES FOR THE CITY, INCLUDING CROSS-COUNTRY SKIING TRAILS, EXPANDED PICNICKING FACILITIES AND NATURE AREAS.

#### ALTERNATIVE FLOOD CONTROL MEASURES CONSIDERED

ALTERNATIVES

SEVERAL ALTERNATIVE FLOOD CONTROL MEASURES HAVE BEEN CONSIDERED DURING OUR COURSE OF STUDY. TONIGHT I WILL BRIEFLY REVIEW THESE ALTERNATIVES FOR YOU. DETAILED DESCRIPTIONS CAN BE FOUND IN THE DRAFT FEASIBILITY REPORT WHICH HAS BEEN MADE AVAILABLE TO YOU.

IN THE RELIEST, WE DESCRIPTED A THE PROPERTY AND THE ADDRAWS TO REDUCE THES OFTIGE SUMMERS MEANS RELIANCE IN FAILTHY, PROPARES TO REDUCE FLOOD DAWARS, CORRENTLY, FURTHEAN, FLOOD CAUTER MEASURES INCLUDE THE PROVENT TOORRELESSONSTRUCTED FROM THEAD RELIEVE AN ELOND WARDING AND ENERGING FLOOD FIGHT AND DISADLES RELIEVE AN ELOND WARDING AND ENERGING FLOOD FIGHT AND DISADLES RELIEF ACTIVITIES BY GOVERNMENTAL ADERTICU, AND THE MARSHALL CITY COUNCIES. SUMERINES THE MORE NO ACTION ALTER-NATIVE WARD NOT MENT THE FRIMMY ORDER DISC OF THE STUDY, I.E. THE PRO-VISION OF RELIAST FLOOD DAWAGE AFORTION, ME DID NOT CONSIDER THE AUTOMEDIA TO FORTHOR. 1

THE SECTION ALTERNATIVE AL CONSIDERED IS EVALUATION OF THE FLOOD-PLAIN. THRUCH EVACUATION WILLD ACHIEVE PERMARAT PROTECTION, THIS ALTERNATIVE WOULD BE VERY CONTLY TO ACHIEVE ON SUCH A LARGE SCALE DUE TO THE MANY RESIDENTIAL AND BUSINESS DEVELOPMENTS AS WELL AS SCHOOLS AND CHIPCHES IN THE AREA. IN ADDITION TO THE COSTS EXCEEDING THE BENEFILTS WILLY WORLD ACCRUE, THE EVACUATION ALTERNATIVE WOULD BE TOTALLY (MACCEPTABLE TO ALL CONCEANED INFERISTS.

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PLAN 3 AS DESCRIBED IN THE PEPDRT IS A MODIFICATION OF THE JUST-MENTIONED PLAN, CALLING FOR PARTIAL EVACUATION AND SOME FLOOD PROOFING. INSTEAD OF TOTAL EVACUATION, SOME AREAS COULD BE FLOOD PROOFED, ESPECIALLY WHERE FLOOD DEPTHS ARE NOT YOO GREAT. HOWEVER, EVEN THOUGH THE COSTS WOULD BE LESS THEN COMPLETE EVACUATION, WE FIND THAT THE COST REDUCTION . WOULD NOT BE SUFFICIENT TO FCONUMICALLY JUSTIFY THE EVACUATION-FLOOD PROOFING ALTERNATIVE. IN ADDITION, SOCIAL UNACCEPTABILITY WOULD ALSO BE A DETERRENT TO THIS ALTERNATIVE.

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UPSTREAM RESERVOIR STOKAGE WAS ALSO CONSIDERED AS A POSSIBLE SOLUTION. TWO APPROACHES WERE REVIEWED IN CONNECTION WITH THE PROPOSAL. ONE WOULD INVOLVE A SINGLE, LARGE RESERVOIR LOCATED IN CANDEN STATE PARK. FROM A TECHNICAL VIEWPOINT, THE PARK WOULD AFFORD THE ONLY PRACTICAL SITE. HOWEVER, UPON REVIEW, OUR STUDIES SHOWED THAT SUCH A RESERVOIR WOULD HAVE INSUFFICIENT STORAGE CAPACITY. IT WOULD ALSO RESULT IN SEVERE ENVIRONMENTAL LOSSES, SIGNIFICANTLY CHANGE THE USE OF THE PARK AND BE ECONOMICALLY UNJUSTIFIED.

THE OTHER RESERVOIR ALTERNATIVE CONSIDERED WAS A SYSTEM OF SHALL TRIBUTARY RESERVOIRS. SMALL RESERVOIRS BY THEMSELVES WERE CONSIDERED INFEASIBLE SINCE THE RESERVOIRS WOULD BE SITUATED TOO FAR UPSTREAM AND WOULD ALSO HAVE INADEQUATE STORAGE CAPABILITY TO SIGNIFICANTLY REDUCE DAMAGES FROM MAJOR FLOODS. HOWEVER, IN OUR STUDY OF FIVE MINNESOTA RIVER SUBBASING WHICH WE ARE CONDUCTING JOINTLY WITH THE SOIL CONSERVATION SERVICE, UNDER PUBLIC LAW 87-639, WE ARE CONSIDERING A NUMBER OF SMALL RESERVOIRS ON SEVERAL TRIBUTARIES INCLUDING THE REDWOOD RIVER. DEPENDING ON THEIR FEASIBILITY, THESE SMALL RESERVOIRS WOULD SERVE AS AN IMPORTANT SUPPLEMENT TO THE PROPOSED PLAN OF IMPROVEMENT.

CONSIDERED ALTERNATIVES SLIDE

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SEVERAL WARIATIONS OF LEVEES AND CHANNEL IMPROVEMENT WERE ALSO INVESTIGATED AS POSSIBLE SOLUTIONS FOR FLOOD CONTROL IN THE UPSTREAM REACH OF MARSHALL AS SHOWN ON THIS SLIDE.

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THIS THE HER COMPLETED TO AN USE PREDECTION TO PREVENT. CLEAR PART AND THREE A CHARAGE HER AND PROTECTION TO PREVENT BANK 1905101. SUCH CHANNEL WHEN WELL PROVIDE ONLY MINOR FLOOD DAMAGE RECTIFIED TO THE NEW REVELOPMENTS.

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LEVEE CONSTRUCTION WAS ANOTHER CONSIDERATION. ONE PROPOSAL IN THE DOWNSTREAM REACH WOULD INVULVE LEVEE CONSTRUCTION, A DRAINAGE PONDING AREA WITH DITCH AND OUTLET WORKS, AND A TEMPORARY SANDBAG CLOSURE. THESE MEASURES WOULD PROVIDE MORE EFFICIENT OPERATION OF THE EXISTING PROJECT AND PROVIDE PROTECTION FOR NEW DEVELOPMENTS.

AT THE REQUEST OF THE CITY, A COMBINED HIGHWAY-LEVEE ALTERNATIVE WAS INVESTIGATED. THIS WOULD BE QUITE SIMILAR TO THE PRECEDING PLAN EXCEPT THAT THE PROPOSED HIGHWAY WOULD SERVE AS A LEVEE.

CONSIDERATION WAS ALSO GIVEN TO A COMBINED LEVEE-CHANNEL WORKS TO REDUCE FLOOD STAGES AND REQUIRED EMBANKMENT HEIGHTS. THIS ALTER-NATIVE, HOWEVER, WOULD BE ENVIRONMENTALLY HARMFUL IN TERMS OF VEGETA-TIVE AND HABITAT LOSSES DUE TO CHANNEL BANK CLEARING AND RESHAPING.

## SELECTED PLAN

PROPOSED FLOOD CONTROL PLAN THIS NEXT SLIDE SHOWS THE SELECTED FLOOD CONTROL PLAN. THIS PLAN CONSISTS OF IMPROVEMENTS ALONG THE RIVER REACHES BOTH UPSTREAM AND DOWNSTREAM OF THE EXISTING FLOOD CONTROL PROJECT.

UPSTREAM WORKS WOULD CONSIST OF A 2,260-FOOT-LONG LEVEE ALONG THE LEFT BANK AND A 6,350-FOOT-LONG LEVEE WITH TWO TEMPORARY SANDWAG CLOSURES ALONG THE RIGHT BANK. THE LEFT AND RIGHT BANK LEVEES WOULD COMMENCE AT THE UPSTREAM END OF THE EXISTING PROJECT AND EXTEND TO

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THE REPORT FOR THE ONG LEVEE nw, 1.  $(\mathbf{F}_{1},\ldots,\mathbf{F}_{n}) \in \mathbb{R}^{n}$ 1.677 EMBANACHENT OP-Externel -ST AN T AN THE FREE AND HERSON AV 1996 CONTRACTOR OF A ANDBAG CLOSURE, ALVES CONSIST OF THE DOWN-STREAM TREAT TO A CHARGE STREAM TO A CHARGE STREAM TO A CHARMEL. A THE REAL AND A THE SHE THE HATCHAL GWREN MENTED IN THE RIVER and an in the second THE WAR AND AND CHANNEL BANK AND ADD ADD TO THE REAL OF IN ADDITION, A PONESTA ANT / ALC 1 CONTRACTOR OF CONTRACT S INCLEED BY THIS HEAD TO HERE E RETAIL STRUCTURE THE PROPOSED LEVEE.

SLIDE OF 100-YEAR FLOODFLAIN

THE RELEVANCE HELTING OF A DESCRIPTION PRODUCT REACH WORLD RE-QUIRE WARDERS - REACTION DESCRIPTION AND ADDRESS AND REGULATIONS PRESERVED FROM THE MOVE TO CONTRACT OF WITHOUT RATING RESOURCES. THE RESIGNAL CONTRACT ON FORM TO CONTRACT THE RELATION DARK BLUE.

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PROPOSED RE-

THE PROPOSED PLAN WOULD ALSO PROVIDE FOR MUCH NEEDED RECREATIONAL FACILITIES. INITIAL FACILITIES WOULD INCLUDE BICYCLE AND CROSS-COUNTRY SKI TRAILS, IMPROVEMENT TO AN OUTDOOR GAMES AREA ON THE PROJECT RIGHT-OF-WAY, AND LIMITED PICNICKING ACCOMMODATIONS. FUTURE PHASE IMPROVE-MENTS WOULD INCLUDE A NATURAL EDUCATION AND QUIET AREA, ADDITIONAL IM-PROVEMENTS TO THE OUTDOOR GAMES AREA, AND A CANOE ACCESS AT THE HIGHWAY 23 ROADSIDE PARK.

THE SELECTED PLAN IS ECONOMICALLY FEASIBLE AT AN ESTIMATED TOTAL COST OF \$2,145,000 AND A BENEFIT-COST RATIO OF 2.0. THE PROJECT WOULD BE CONSTRUCTED BY THE FEDERAL GOVERNMENT AT AN ESTIMATED FEBERAL COST OF \$1,120,000. THE NON-FEDERAL SHARE WOULD BE ABOUT \$424,000.

## LOCAL COOPERATION

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THE OVERALL FLOOD CONTROL PROJECT FOR MARSHALL WOULD BE CONSTRUCTED UNDER CONTRACT BY THE FEDERAL GOVERNMENT. THE FEDERAL GOVERNMENT WOULD BE RESPONSIBLE FOR DESIGN AND CONSTRUCTION OF THE VARIOUS FEATURES OF THE PROPOSED WORKS. THE COST OF THIS STUDY IS ALSO ASSUMED BY THE FEDERAL GOVERNMENT.

FOLLOWING CONSTRUCTION, NON-FEDERAL INTERESTS WOULD BE RESPONSIBLE FOR MAINTAINING ALL PROJECT WORKS. IN ADDITION, THE LOCAL SPONSOR WOULD BE RESPONSIBLE FOR MEETING ALL ELEMENTS OF LOCAL COOPERATION AS OUTLINED IN THE DRAFT FEASIBILITY REPORT. PRIOR TO INITIATION OF ANY CONSTRUC-TION WORK, THE SPONSOR WOULD ALSO BE REQUIRED TO ENTER INTO A LEGAL AND

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THIS CONCLUDES MY FORMAL PRESENTATION. I WILL NOW OPEN THE MEETING UP FOR YOUR VIEWS AND COMMENTS ON THE SELECTED PLAN AND CON-SIDERED ALTERNATIVES. FIRST, I WILL CALL ON THOSE WHO INDICATED ON THEIR CARDS THAT THEY WISH TO MAKE A STATEMENT. AFTER THAT, I WILL CALL ON OTHERS WHO MAY WISH TO EXPRESS THEIR VIEWS. AS YOU RISE TO SPEAK, PLEASE GIVE YOUR FULL NAME AND THE INTEREST YOU REPRESENT, IF ANY, SO THAT WE MAY HAVE THIS INFORMATION FOR THE PUBLIC RECORD.

## CLOSING

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IF THERE ARE NO FURTHER COMMENTS, I WILL TURN THE MEETING BACK OVER TO MAYOR SCHLAGEL. I TRUST THAT EVERYONE HERE TONIGHT HAS HAD AN OPPORTUNITY TO PRESENT THEIR VIEWS. HOWEVER, THE RECORD OF THIS MEETING WILL BE KEPT OPEN FOR A PERIOD OF 30 DAYS FOR ANY ADDITIONAL WRITTEN STATEMENTS. WE THANK YOU FOR COMING OUT HERE TONIGHT AND MEETING WITH US.

