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<sup>3</sup> CONNECTICUT WESTERN COASTAL AREA

# SAMUEL P. SENIOR RESERVOIR DAM CT 00108 and POPPS MOUNTAIN DIKE CT 00022

<sup>6</sup> PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM



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DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION, CORPS OF ENGINEERS WALTHAM, MASS. 02154

SEPTEMBER 1978

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DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION. CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02154

REPLY TO ATTENTION OF: NEDED

AUG 1 6 1979

Honorable Ella T. Grasso Governor of the State of Connecticut State Capitol Hartford, Connecticut 06115

Dear Governor Grasso:

I am forwarding to you a copy of the Samuel P. Senior Reservoir Dam and Popps Mountain Dike Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important

A copy of this report has been forwarded to the Department of Environmental Protection, the cooperating agency for the State of Connecticut. In addition, a copy of the report has also been furnished the owner, Bridgeport Hydraulic Company, 835 Main Street, P.O. Box 702, Bridgeport, Connecticut 06609.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Department of Environmental Protection for your cooperation in carrying out this program.

Sincerely yours,

MAX B. SCHEIDER

Incl As stated

Colonel, Corps of Engineers Division Engineer

### SAMUEL P. SENIOR DAM

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CT 00108

AND

POPPS MOUNTAIN DIKE

CT 00022

CONNECTICUT WESTERN COASTAL AREA

WESTON, CONNECTICUT

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NATIONAL DAM INSPECTION PROGRAM

PHASE I INSPECTION REPORT

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#### PHASE I REPORT

NATIONAL DAM SAFETY PROGRAM Name of Dam: SAMUEL P. SENIOR DAM Name of Dike: POPPS MOUNTAIN DIKE

State Located: Connecticut County Located: Fairfield County Stream: Saugatuck River Date of Inspection: 26 JULY 1978

#### BRIEF ASSESSMENT

Samuel P. Senior Dam is a linear concrete gravity structure, 990 feet long, with a 300-foot spillway located at the west end of the dam. The spillway is concaved looking downstream and consists of several steps on the downstream side. An earthen embankment section on the downstream side of the dam begins 61 feet below the top of dam and has slopes varying from 2:1 to 3:1. The dam is approximately 110 feet above the streambed. >Approximately 2,000 feet northeast of the dam, a concrete gravity dike 670 feet long is provided. The structural height of the dike is 36 feet.

Based on the visual inspection of the site, review of available information and past performance of the dam, the dam is judged to be in good condition. There are surface patches of spalled concrete; however, no structural cracks were observed, nor was any visible evidence of abnormal settlements, heaving, deflections or lateral movements noted. The downstream berm is generally in good condition with no sloughing or wet spots noted. Based on the visual inspection of the site, review of available information and past performance of the dike, the dike is also judged to be in good condition. There are surface patches of spalled concrete; however, no structural cracks were observed, nor was any visible evidence of abnormal settlements, heaving, deflections or lateral movements noted.

The maximum spillway capacity at top of dam is 35 percent of the peak discharge rate of the test flood. Therefore, the test flood cannot be passed by the spillway without overtopping the dam. The overflow will be 2.7 feet above the top of the dam.

It is recommended that spalling at joints along the downstream face of the dam be repaired by the owner. Arrangements should be made to exercise the 48-inch blowoff periodically to ensure continued serviceability. The owner should cut the trees and brush for a distance of 25 feet downstream of the dam and dike, ensuring that the tree roots are removed and the resulting holes are replaced with proper backfill. Because of the location of the dam, upstream of a populated area, round-the-clock surveillance should be provided during periods of high precipitation. The owner should develop a formal warning system and an operational procedure to follow in the event of an emergency.

Recommendations and remedial measures described should be implemented by the owner within 2 years after receipt of this Phase I Inspection Report.

P.E. Principal

Registered, CT 7634

This Phase I Inspection Report on Popps Mountain Dike has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the <u>Recommended Guidelines for Safety Inspection</u> of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

CHARLES G. TIERSCH, Chairman Chief, Foundation and Materials Branch Engineering Division

FRED J. RAVENS, Jr., Member Chief, Design Branch Engineering Division

and a first

SAUL COOPER, Member Chief, Water Control Branch Engineering Division

APPROVAL RECOMMENDED:

B. Fryan

JOE B. FRYAR Chief, Engineering Division

#### PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reaonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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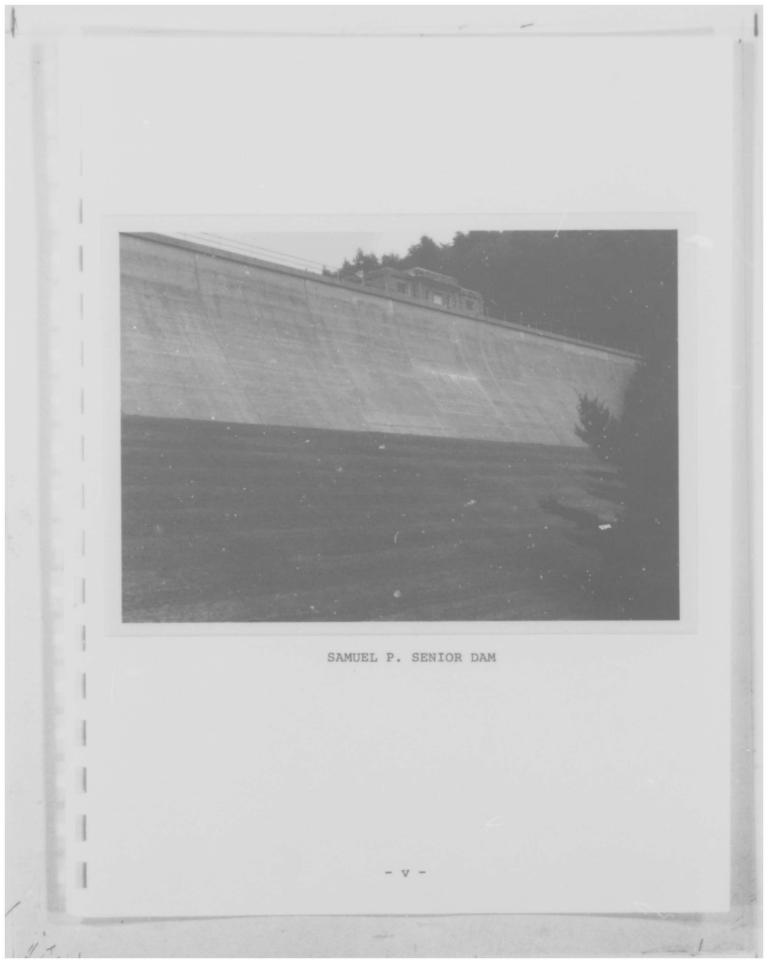
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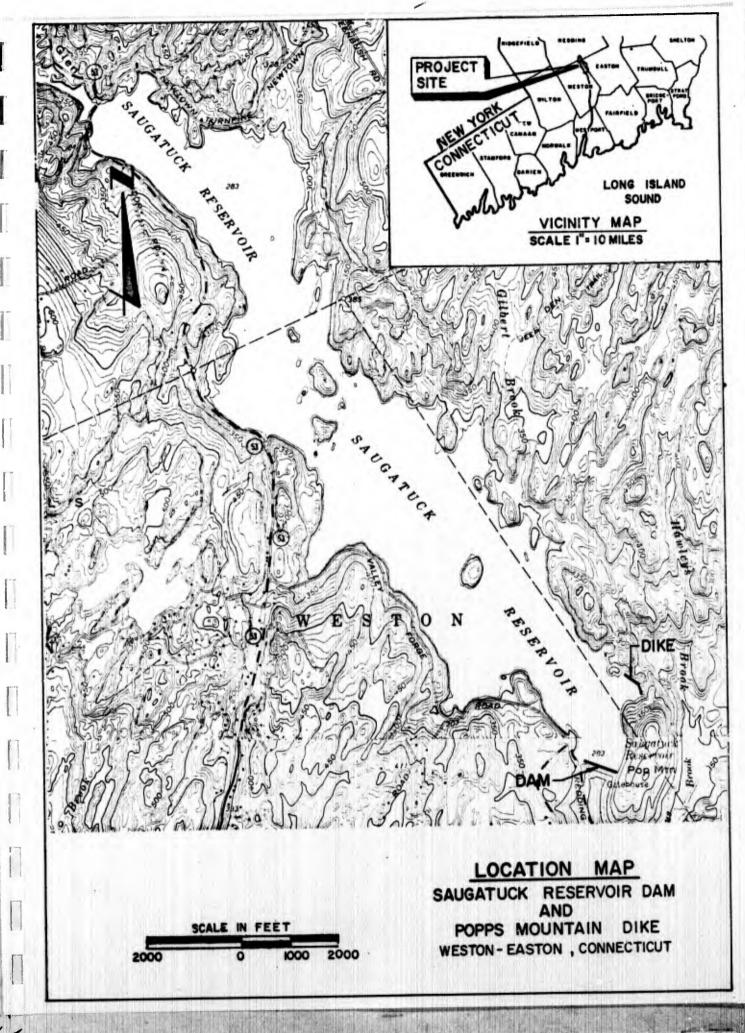
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#### PHASE I INSPECTION REPORT SAMUEL P. SENIOR DAM CT 00108

SECTION 1 - PROJECT INFORMATION

#### 1.1 GENERAL:

a. <u>Authority</u>. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection through the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Flaherty Giavara Associates, P.C. has been retained by the New England Division to inspect and report on selected dams in the State of Connecticut. Authorization and notice to proceed was issued to Flaherty Giavara Associates, P.C. under a letter of 25 April 1978 from Ralph T. Garver, Colonel, Corps of Engineers. Contract No. DACW33-78-0309 has been assigned by the Corps of Engineers for this work.

b. Purpose:

1) Perform technical inspection and evaluation of non-federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-federal interests.

2) Encourage and assist the States to initiate quickly effective dam safety programs for non-federal dams.

3) To update, verify and complete the National Inventory of Dams.

#### 1.2 DESCRIPTION OF PROJECT:

a. <u>Description of Dam and Appurtenances</u>. The Samuel P. Senior Dam, popularly known as the Saugatuck Reservoir Dam, is a linear concrete gravity structure, 990 feet long, with a 300-foot spillway located at the west end of the dam. The spillway is concaved looking downstream and consists of several steps on the downstream side whereupon the water is channeled into a 60-foot wide spillway channel until it discharges into the Saugatuck River some 400 feet downstream of the dam. An earthen embankment section on the downstream side of the dam begins at elevation 225, 61 feet below the top of dam, has a 16-foot wide top width and a 2:1 (horizontal) slope to elevation 200, then a 2-1/2:1 slope to elevation 190 and finally a 3:1 slope to elevation 182. The top of the dam is about 11 feet wide, with a railing on both the upstream and downstream sides. The dam is approximately 110 feet above the streambed. An intake structure is located in the eastern portion of the dam, equipped with 6 48-inch influent sluice gates at various elevations. From the intake structure, a 36-inch pipe supplies water to the Bridgeport Hydraulic Company's facilities while a 48-inch lined tunnel can divert water to Hemlock Reservoir. Also, from the intake structure, a 48-inch blow off and 2 8-inch drains pass through the dam to a lower gate house and then terminate at a concrete endwall to discharge into the Saugatuck River. An additional 8-inch drain is provided between the lower gate house and this endwall. A linear concrete gravity dike 670 feet long north of the dam is also provided.

b. Location. The Samuel P. Senior Dam is located on the Saugatuck River, within the Connecticut Western Coastal Area in the Town of Weston. The dam is approximately 7 miles north of the Town of Westport. The concrete dike is about 2,000 feet north of the dam on the east side of reservoir in the Town of Easton.

c. <u>Size Classification</u>. The applicable guidelines indicate that for a large size classification the height of dam must be greater than or equal to 100 feet. The Samuel P. Senior Dam is 110 feet above the streambed. Therefore, the dam is classified as large. The applicable guidelines also indicate that for an intermediate category the storage (in acrefeet) for the impoundment must be greater than or equal to 1,000 and less than 50,000. The top of dike storage is 42,000 acrefeet and therefore the dike is classified as intermediate.

d. <u>Hazard Classification</u>. The dam is classified as having a high hazard potential. More than 100 houses are located in the area that could be affected by a dam failure flood wave. The same area would be affected by a dike failure flood wave.

e. <u>Ownership</u>. Samuel P. Senior Dam and Popps Mountain Dike are owned by the Bridgeport Hydraulic Company, having its headquarters in Bridgeport, Connecticut.

f. <u>Purpose of Dam</u>. The dam was constructed to form an impounding reservoir. The reservoir forms part of the water company's supply and distribution system, providing potable water to the residents of the Greater Bridgeport area. Drawoff water can also be diverted to Hemlock Reservoir as needed.

g. <u>Design and Construction History</u>. The dam and dike were built around 1941. They were designed by Clarence M. Blair, Inc. of New Haven, Connecticut. The Bridgeport Hydraulic Company constructed the dam and dike with its own forces. h. Normal Operating Procedures. Water is withdrawn at various depths from the intake structure and then conveyed to the distribution system through a 36-inch supply pipe. When needed, water can also be withdrawn and diverted to Hemlock Reservoir through a lined tunnel. An 8" drain pipe in the intake structure is used to maintain a continuous flow in the Saugatuck River.

#### **1.3 PERTINENT DATA:**

a. Drainage Area -

 b. <u>Discharge at Dam Site</u> -<u>Maximum Known Flood</u> Warm Water Outlet Div. Tunnel Low Pool Outlet Diversion Tunnel Outlet Gated Spillway Ungated Spillway at Max. Pool

Total Spillway Cap. at Max. Pool

c. <u>Elevation (above M.S.L.)</u> -Top of Dam Max. Design Pool Full Flood Control Pool Recreation Pool Spillway Crest Ungated Upstream Portal Invert. Div. Tunnel Downstream Portal Invert. Div. Tunnel Streambed at Centerline of Dam Maximum Tailwater

d. <u>Reservoir</u> -Length of Max. Pool Length of Recreation Pool Length of Flood Control Pool

- e. <u>Storage</u> -<u>Recreation Pool</u> Flood Control Pool Design Surcharge Top of Dam
- f. <u>Reservoir Surface (acres)</u> Top of Dam Max. Pool Flood Control Pool Recreation Pool Spillway Crest

34.6 sq. miles

Unknown Not Available Not Available Not Available None 11,900 CFS @ 1 Ft. freeboard 15,600 CFS @ no freeboard

286 Not Available Not Available 280 Not Available Not Available 170+ Unknown

18,500 feet Not Applicable Not Applicable

Not Applicable Not Applicable Not Applicable 42,000 Acre-Feet

Not Available Not Available Not Applicable Not Applicable 868

Dam g. Type: Linear concrete gravity Length: 990 feet Height: 130 feet Top Width: 11 feet Side Slopes: Downstream: 1 vertical to 0.7 horizontal Upstream: 1 vertical to 0.05 horizontal Impervious Core: Not Applicable Grout Curtain: Unknown h. Dike -Type: Linear concrete gravity Length: 665 feet Height: 36 feet. Top Width: 6'-8" Side Slopes: Downstream: 1 vertical to 0.65 horizontal Upstream: 1 vertical to 0.05 horizontal Zoning: Concrete Impervious Core: Not Applicable Grout Curtain: Unknown h. Diversion and Regulating Tunnel -Type: Lined tunnel 1-1/2 miles Length: 48 inch Diameter: Access: Intake Structure Regulation: Sluice Gate i. Spillway -Type: Ogee 295 feet Length of Weir: Crest Elevation: 280 Gates: Ungated Upstream Channel: Reservoir Downstream Channel: Concrete Spillway is founded on: Bedrock j. Regulating Outlets -Gates: None Conduits: 36" diameter cast iron supply pipe 48" diameter blow off pipe, cast iron

#### SECTION 2 - ENGINEERING DATA

#### 2.1 DESIGN:

The design of the dam and dike was made by Clarence M. Blair, Inc. of New Haven, Connecticut in 1939. Pertinent sections of the following information have been utilized in this report.

a. Bridgeport Hydraulic Co. Saugatuck Development-General Plan at Dam - 1939.

b. Bridgeport Hydraulic Co. Saugatuck Development -Contour Map of Dam Site - 1937.

c. Bridgeport Hydraulic Co. Saugatuck Development -Cross Sections of Dam and Spillway - 1937.

d. Bridgeport Hydraulic Co. Saugatuck Development -Plan of Gate House and Intakes - 1939.

e. Bridgeport Hydraulic Co. Saugatuck Dam Site -Results of Borings - March 15, 1920.

f. Bridgeport Hydraulic Co. - Core Drill Boring at Saugatuck River - undated.

g. Bridgeport Hydraulic Co. - Section proposed for Saugatuck Dam - 1937.

h. Bridgeport Hydraulic Co. Saugatuck Development -Plan of Dam at Notch - Popps Mountain - 1940.

The "As-Built" drawings for this project are on file at the State Library in Hartford, Connecticut. The basis of design for the project is unknown.

#### 2.2 CONSTRUCTION:

Some construction records are available at the offices of the Bridgeport Hydraulic Company and in files maintained by the State Supervisor of Dam Maintenance in Hartford, Connecticut and a formal review of these records has been made. From the inspection report submitted by the Resident Engineer dated February 5, 1942, the following information was obtained:

"In preparing the foundation, which was gneiss rock the overburden was first stripped and then the rock was excavated until a firm solid foundation was reached. The

- 5 -

depth of necessary excavation varied considerably over the length of the dam as shown by the profile. The greater part of the foundation sloped upward from the heel to the toe but where this condition did not exist the rock was drilled and blasted to present a very rough and uneven surface.

"Between the easterly end of the dam and the gate house, after excavation had been carried to an apparently sound foundation, twenty grout holes were drilled into which grout was forced under pressure. This work was done as an additional precaution to insure a sound foundation as more rock excavation had been necessary over this area to reach what seemed to be a good bottom."

"The aggregate for the concrete contained in the dam was obtained from a gravel deposit in the reservoir bottom, where a crushing, screening and washing plant was set up. The screened and washed material was hauled from this plant to the mixing plant in trucks. The sand used all passed a #4 square mesh and the stone was screened into three sizes, varying from 1/4" to 6". "

Two classes of concrete were mixed, one called Class A which was used on all exposed faces of the dam for a width of 5 to 7 feet and the other called Class B which was used on the interior of the dam. "Cylinders 6" x 12" were made each day from concrete taken from the forms [tested by the Pittsburg Testing Laboratory], which gave average strength of 2000# per square inch in 7 days and 4200# in twenty-eight days for Class A concrete and 1800# in seven days and 3700# in twenty-eight days for Class B concrete."

"The dam was built in sections forty feet long except at the ends where the lengths were 45 feet and 48 feet. The gate house section, 69 feet in length, was constructed in two equal halves. For water stops in the joints, keys 12" x 24" spaced 10 feet apart were set at the ends of each section. Concrete was deposited in forms 4'-2" high and each lift of this height was placed in three courses. Before concrete was placed on any rock surface or on any concrete already in place all dirt, laitance and other foreign matter was removed by thoroughly washing and cleaning the surface." Extraordinary attention was paid to this cleaning because it was considered most important. The spillway was constructed in the same general way as the dam. "An earth embankment was placed against the downstream face of the dam to elevation 235. This was composed of material excavated from the dam foundation and from the spillway channel and consisted mostly of rock. Special care was taken to have coarse material against the dam itself in order to provide proper drainage."

The foundation for the Dike was prepared in the same manner as that of the dam and the concrete consisted of the same materials. Expansion joints with keys were provided at forty foot intervals and the concrete was placed in the forms in 1-1/2 yard batches after having been mixed at the same mixing plant utilized for the dam.

Construction of the dam was carried out by Bridgeport Hydraulic Company forces.

#### 2.3 OPERATION:

No formal operation records are available.

2.4 EVALUATION:

a. <u>Availability</u>. Available data was reviewed by members of the inspection team and office personnel and found to be generally accurate and complete.

b. Adequacy. The data available is adequate for the purposes of a Phase I investigation.

c. <u>Validity</u>. There is no reason to question the validity of the available data.

#### SECTION 3 - VISUAL INSPECTION.

#### 3.1 FINDINGS:

a. <u>General</u>. The structure appears to be in good condition, except for surface patches of spalled concrete. No structural cracks were observed, nor was any visible evidence of abnormal settlements, heaving, deflections or lateral movements noted. The downstream berm is generally in good condition with no sloughing or wet spots noted. The berm appeared to be relatively shallow in the vicinity of the right and left abutments.

Overall the spillway appeared to be in good condition; a crack was noted at the crest of the spillway where it meets the training wall.

b. Dam.

1) Upstream Face - At or above the water line, slight spalling was evident. Generally the concrete was in good condition.

2) Downstream Face - There was evidence of wet spots, staining, efflorescence and joint spalling at nearly every construction joint. From Station 1+90 to Station 2+30 about 30 feet above the berm there was a horizontal line of efflorescence at a horizontal pour joint. In the panel between Station 3+45 to 3+85, about 10 feet up from the top of the berm, there are four drilled holes about 2 inches in diameter, depth undetermined, spaced 3 to 4 feet apart horizontally, which were dry but showed evidence of efflorescence (the purpose of these holes is unknown). There was quite a bit of spalling below the holes and some slight spalling above them. The joint at Station 3+85 was wet and stained from about the berm to a height of 35 feet. For about 20 feet from the top of berm, the joint was badly spalled and quite deteriorated.

3) <u>Spillway</u> - The concrete in the spillway and steps was found to be in generally good condition. A crack was noted at the crest of the spillway, where it meets the training wall. Some surface spalling of the concrete steps was observed.

4) Earth Embankment - The downstream embankment is generally in good condition with no sloughing or wet spots noted. The berm is 15 feet wide at the top of the slope and slopes toward the concrete dam. There is a depression at each joint of the dam. The depressions are filled with stone. The berm appeared to be relatively shallow in the vicinity of the right and left abutments. Approximately 150 feet downstream of the toe of the downstream berm is an extensive area of dumped riprap adjacent to the blow-off outlet works. The riprap has been covered with a thin veneer of soil which has been eroded away in several locations.

Several large depressions, approximately 3' x 4', exist in the flat grassed area downstream from the earth berm approximately 125 feet in the vicinity of Station 3+0 and 3+50. The depressions vary in depth between 6" to 15". Another depression, 2' x 2' x 1' deep, was located approximately 50 feet down on the berm slope in the vicinity of Station 2+29. The origin of these depressions is not known.

No animal burrows were encountered on the slopes of the downstream embankment.

#### c. Appurtenant Structures.

1) <u>Spillway Channel</u> - The spillway channel is in good condition. Low concrete walls on the right and left side of the channel are also in good condition. Layered mica gneiss bedrock is exposed in the bottom of the spillway channel from the spillway weir to the large pool at the end of the left concrete training wall. A small amount of seepage was noted in the channel floor. A rock fall has occurred in the upper part of the channel from its east bank, however, it does not restrict flow. The blow-off discharge structure is in excellent condition.

2) Upper Gate House - This structure, located on upstream face of dam, was clean and neat. Gates are reportedly operated once a year, and were inspected by divers in 1977 with minor repair work required at stem guides. There are cracks in the brickwork in the northwest, west, and southwest walls. The cracks are wide enough to allow daylight through in some places. The building has 100 amp, 240 volt electrical service for lights and a deicer which is located adjacent to the spillway.

3) Lower Gate House - This structure, on the downstream side of the dam, is in good condition, but is subject to condensation and high humidity due to the cold water flowing in the pipes through the structure. It has 30 amp, 120 volt electrical service for lights, flow meters, and a furnace.

4) <u>Concrete Gravity Dike (Popps Mountain)</u> - Generally the dike is in good condition. Along the full length of the upstream face about 2 feet above the water line, scouring of the concrete has occurred. At the top of the dike, at Station 1+80, there is a crack the full width of the dam and the lip or coping has deteriorated.

At Station 4+20 there is a crack adjacent to the joint for the full width, and at the upstream edge, the lip has spalled off.

At Station 4+63 at the top, a one foot wide strip several inches deep for the full width has deteriorated and spalled off, and the lip at the upstream face has also spalled off.

At Station 5+40, there is a crack adjacent to the joint the full width of the dike and on the downstream face, the lip has spalled off.

On the downstream face of the dike, at Station 1+80, from the top to about 4 feet down from the top there is a piece of concrete about one foot in width and several inches deep breaking away from the face.

Considerable tree growth and bushes exist in the filled area along the toe of the dike.

No evidence of seepage or wet areas were found along the toe of the dam from the right to left abutments. At approximately Station 1+25, a wet area exists approximately 100 feet east of the dam in a naturally occurring gully. There is a small amount of iron-stained seepage flowing north from this area. It is not evident whether the flow is from underneath the dam or naturally occurring drainage from the adjacent steep watershed area.

d. <u>Reservoir Area</u>. The reservoir perimeter has well vegetated banks at moderate to steep slopes. There was no evidence of slides or sloughing. No noticeable debris or obstructions were seen in the vicinity of the intake tower. The depth of sediment, and rate of accumulation in the reservoir, is unknown.

e. <u>Downstream Channel</u>. The open channel extending downstream from the junction of the 48" blow-off and spillway channels is in excellent condition. It has a bed of coarse gravel and cobbles, and there is no evidence of aggradation or recent degradation. The banks are partly lined with riprap, and are stable. Seepage was observed entering this channel between the spillway and blow-off channels. This clear water is apparently seeping from a bank of fill material overlying the original stream channel.

# 3.2 EVALUATION:

a. Dam. Visual observation revealed that the dam and attendant structures are structurally sound and that no immediate actions to remedy any serious problems should be taken. There was no visual indication of dam weakness.

b. <u>Dike</u>. Visual observations indicated that the dike was in good condition. Although spalling has occurred at several joints, this does not affect the stability of the dike.

- 11 -

#### SECTION 4 - OPERATIONAL PROCEDURES

#### 4.1 PROCEDURES:

The dam 8" blow-off drain line is operated to maintain minimum flow of the Saugatuck River. The reservoir is used as a storage reservoir and is connected into the upper end of Hemlocks Reservoir through a tunnel about 1-1/2 miles long. Take off points from the reservoir are changed periodically.

#### 4.2 MAINTENANCE OF DAM:

The dam, dike and associated structures are well maintained with a regular program of grass mowing and general maintenance in effect. Yearly routine inspections are carried out by Bridgeport Hydraulic Company staff. A consultant was hired to perform a cursory inspection of Bridgeport Hydraulic Company dams during November 1976.

#### 4.3 MAINTENANCE OF OPERATING FACILITIES:

The operating valves were inspected recently; although the results of the inspection are not available, generally the valves/valve stems need some repair.

#### 4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT:

There was no warning system of any kind in effect at the time of the inspection.

#### 4.5 EVALUATION:

The Samuel P. Senior Dam and dike, which are almost 40 years old, are well operated and maintained. Although not designed for rapid drawdown, it should be noted that, if the need should arise, drawdown could be effected by the following procedures:

a. Allowing for maximum discharge through the 48" blow-off and 8" drain line.

b. Allowing for maximum discharge through the 6' - 4" inside horseshoe shaped concrete tunnel to Hemlocks Reservoir.

The blow-off was not operated during the site inspection, therefore comments on the serviceability cannot be made. The valve should be tested on a periodic basis to insure that it could be operated if required.

#### SECTION 5 - HYDRAULICS/HYDROLOGY

#### 5.1 EVALUATION OF FEATURES:

a. <u>Design Data</u>. There is no available information on the hydraulic design criteria for this dam and appurtenances. Under established criteria (OCE Guidelines) the recommended spillway design flood for size (large) and hazard potential (high) classification is the probable maximum flood (PMF). The PMF is the flood that may be expected from the most severe combination of critical meteorologic and hydrologic conditions that are reasonably possible in the region.

An estimate of the magnitude of the PMF at the site is based on an analysis of several sets of regional flood frequency data as presented in Appendix II.

As a conservative approach to the investigation, the more critical design PMF hydrograph was used throughout. The peak inflow rate of the PMF of 48,800 CFS was used as the test flood.

A stage-discharge relationship was calculated for the spillway and indicates the following flows, based upon a coefficient of 3.6 and an effective length of 295 feet.

Stage	Head, Ft.	Discharge Rate, CFS	
280	0	0	
281	1	1,060	
282	2	3,000	
283	3	5,520	
284	4	8,500	
285	5	11,870	
286	6	15.610	

#### Stage - Discharge Relationship

The maximum spillway capacity, with no freeboard, is equal to about 35 per cent of the peak discharge rate of the test flood. In order to determine the effect of the reservoir storage capacity, a hydrograph of the test flood was routed through the reservoir.

The hydrograph was formed by assuming the test flood had a duration of 24 hours, with the peak of 48,800 CFS occurring at 8 hours from the beginning of runoff. The rising and falling limbs of the hydrograph were assumed to be changing at a constant rate, forming a triangle. The routing operation indicated that the peak rate of discharge would be reduced to 46,000 CFS, resulting in a stage elevation of 288.7 feet. b. Experience Data. During the flood of October 15 - 17, 1955, the dam was not overtopped. United States Geologic Survey information indicates that the flow of October 16, 1955 had a peak rate of 7,100 CFS, which is the maximum flood of record for the Saugatuck River.

c. <u>Visual Observations</u>. The on-site inspection of the dam provided the data for the hydraulic evaluation of the spillway.

d. Overtopping Potential. The elevation-discharge relations indicate that the test flood would not be passed by the spillway without overtopping the dam. The spillway capacity is about 35 per cent of the test flood, and the stage would be 2.7 feet above the top of the dam and dike.

# SECTION 6 - STRUCTURAL STABILITY

# 6.1 EVALUATIONS OF STRUCTURAL STABILITY:

a. Visual Observations. No evidence was observed that would indicate structural instability of the dam and dike.

b. <u>Design and Construction Data</u>. The design and construction data available are not sufficient to formally evaluate the stability of the dam and dike.

c. Operating Records. There are no available records which indicate evidence of stability problems since the dam and dike were constructed in the early 1940's. As the Samuel P. Senior dam has been designed and constructed as a water supply dam and has been subjected to a full head of water a majority of the time since construction, its stability could be considered to be adequate based on past performance.

d. <u>Post-Construction Changes</u>. The bridge that provided access to the dam site, across the spillway section, has been removed.

e. <u>Seismic Stability</u>. This dam is in Seismic Zone 1 and, in accordance with recommended Phase I guidelines, does not warrant seismic analysis.

#### SECTION 7 - ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

#### 7.1 DAM ASSESSMENT:

a. <u>Condition</u>. Based on the visual inspection, records available and past operational performance, the dam is judged to be in good condition.

The project will not pass the test flood without overtopping the dam, and therefore the spillway capacity is inadequate. The spillway capacity is judged seriously inadequate, as the project will not pass one-half the test flood without overtopping the dam.

b. <u>Adequacy of Information</u>. The information available is such that the assessment of the safety of the dam must be based primarily on the visual inspection and past operational performance of the structure.

c. <u>Urgency</u>. The recommendations and remedial measures should be implemented by the owner within 2 years after receipt of this report.

d. <u>Need for Additional Investigation</u>. Additional investigations to further assess the adequacy of the dam do not appear necessary. However, it appears that detailed investigations should be initiated by the owner to determine requirements for obtaining additional spillway capacity.

#### 7.2 RECOMMENDATIONS:

It is recommended that the following measures be undertaken by the owner:

1) Spalling at joints along the downstream face should be repaired.

#### 7.3 REMEDIAL MEASURES:

Although the dam is generally maintained in good condition, it is considered important that the following items be accomplished:

- 16 -

a. Alternatives. Not applicable.

b. Operation and Maintenance and Procedures.

1) Arrangements should be made to exercize the 48" blow-off periodically to ensure continued serviceability.

2) The owner should cut the trees and brush for a distance of 25 feet downstream of the dam and dike, ensuring that the tree roots are removed and the resulting holes are replaced with proper backfill.

3) Because of the location of the dam, upstream of a populated area, round the clock surveillance should be provided during periods of high precipitation.

4) The owner should develop a formal warning system. An operational procedure to follow in the event of an emergency should also be adopted.

5) The owner should provide continued periodic inspections at a two year frequency.

# APPENDIX A

VISUAL INSPECTION - CHECK LIST

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INSPECTOR Anthony D. Rummo	04
	DISCIPLINE Structural
INSPECTOR Robert C. Smith	DISCIPLINE Project Manager
AREA EVALUATED	CONDITION
CONCRETE DAM STRUCTURE	
General Condition Concrete Surfaces	The condition of concrete is good.
Movement or Settlement of Crest	No noticeable movement of dam crest or side slopes.
Vertical Alignment	Good horizontal and vertical alignment.
Horizontal Alignment	;
Condition at Abutment and Other Structures	
Structural Cracking	None
Spalling	Slight surface spalling D/S face.
Visible Reinforcing	
Rusting or Staining of Concrete	Slight staining of several joints
Condition of Monolith/ Construction Joints	Good
<b>Drains</b> - Foundation, Joint, Faces	None observed.
Any Seepage or Efflorescence	Some efflorescence observed.
Foundation Damage, Undermining	None observed.
Water Passages	Spillway in good condition, minor spalling.
Abutments	sparring.

ROJECT Samuel P. Senior Dam	DATEJuly 26, 1978	
NSPECTOR Richard F. Murdock	DISCIPLINE Geotechnical	
INSPECTOR Robert C. Smith	DISCIPLINE Project Manager	
AREA EVALUATED	CONDITION	
DAM EMBANKMENT		
Crest Elevation	286	
Current Pool Elevation	279	
Maximum Impoundment to Date		
Surface Cracks		
Pavement Condition		
Movement or Settlement of Crest		
Lateral Movement	None	
Vertical Alignment	Good	
Horizontal Alignment	Good	
Condition at Abutment and at Concrete Structures	Good .	
Indications of Movement of Structural Items on Slopes	None	
Trespassing on Slopes		
Sloughing or Erosion of Slopes or Abutments	Some minor surface erosion on west slope of dam.	
Rock Slope Protection - Riprap Failures	None	
Unusual Movement or Cracking at or near Toes	None	
Unusual Embankment or Down- stream Seepage	None	

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ROJECT	Samuel P. Senior Dam	DATE July	26, 1978
NSPECTOR	Richard F. Murdock	DISCIPLINE_	Geotechnical
INSPECTOR	Robert C. Smith	DISCIPLINE_	Project Manager

AREA EVALUATED	CONDITION	
DAM EMBANKMENT - (continued)		
Piping or Boils	None	
Foundation Drainage Features	None	
Toe Drains	None	
Instrumentation System	None	

ROJECT	Popps Mountain Dike	DATE July	26, 1978
NSPECTOR	Richard F. Murdock	DISCIPLINE_	Geotechnical
	Robert C. Smith	DISCIPLINE_	Project Manager

AREA EVALUATED	CONDITION
DIKE EMBANKMENT	
Crest Elevation	286
Current Pool Elevation	279
Maximum Impoundment to Date	
Surface Cracks	
Pavement Condition	• •
Movement or Settlement of Crest	
Lateral Movement	
Vertical Alignment	
Horizontal Alignment	
Condition at Abutment and at Concrete Structures	
Indications of Movement of Structural Items on Slopes	None
Trespassing on Slopes	
Sloughing or Erosion of Slopes or Abutments	None
Rock Slope Protection - Riprap Failures	None
Unusual Movement or Cracking at or near Toes	None
Unusual Embankment or Down- stream Seepage	Seepage observed at Station 1+0, approximately 100 ft. downstream of dam.

ROJECT	Popps	Mount	air	Dike	
NSPECTOR	Ric	chard	F.	Murdock	

UNSPECTOR Robert C. Smith

DATE	nlv	26.	1978	
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DISCIPLINE Geotechnical

DISCIPLINE Project Manager

AREA EVALUATED	CONDITION
DIKE EMBANKMENT - (continued)	
Piping or Boils	None
Foundation Drainage Features	None
Toe Drains	None
Instrumentation System	None

ROJECT Popps Mountain Dike	DATE July 26, 1978
NSPECTOR Anthony D. Rummo	DISCIPLINE Structural
NSPECTOR Robert C. Smith	DISCIPLINE Project Manager
AREA EVALUATED	CONDITION
CONCRETE DAM STRUCTURE	
General Condition Concrete Surfaces	The concrete in dike is in good condition.
Movement or Settlement of Crest	None observed.
Vertical Alignment	Good alignment.
Horizontal Alignment	
Condition at Abutment and Other Structures	Excellent
Structural Cracking	None .
Spalling .	Some surface spalling observed at top of dike.
Visible Reinforcing	
Rusting or Staining of Concrete	None
Condition of Monolith/ Construction Joints	Good
Drains - Foundation, Joint, Faces	
Any Seepage or Efflorescence	Very slight
Foundation Damage, Undermining	None
Water Passages	None

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PROJECT Samuel P. Senior Dam	DATE July 26, 1978		
INSPECTOR James MacBroom	DISCIPLINE Hydraulics/Hydrology		
INSPECTOR	DISCIPLINE		
AREA EVALUATED	CONDITION		
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE			
a. Approach Channel			
Slope Conditions			
Bottom Conditions			
Rock Slides or Falls	· · · · · · · · · · · · · · · · · · ·		
Log Boom			
Debris	•••		
Condition of Concrete Lining			
Drains or Weep Holes			
b. Intake Structure			
Condition of Concrete	Good condition, slight spalling at water line.		
Stop Logs and Slots	Good condition.		

OJECT Samuel P. Senior Dam	DATE July 26, 1978
ISPECTOR James MacBroom	DISCIPLINE Hydraulics/Hydrology
SPECTOR	DISCIPLINE
AREA EVALUATED	CONDITION
TLET WORKS - CONTROL TOWER	
Concrete and Structural	
General Condition	
Condition of Joints	
Spalling	
Visible Reinforcing	
Rusting or Staining of Concrete	
Any Seepage or Efflorescence	
Joint Alignment	
Unusual Seepage or Leaks in Gate Chamber	
Cracks	
Rusting or Corrosion of Steel	
. Mechanical and Electrical	
Air Vents	
Float Wells	
Crane Hoist	
Elevator	۶. ۲
Hydraulic System	

## PERIODIC INSPECTION CHECK LIST

PROJECT Samuel P. Senior Dam

DATE July 26, 1978

INSPECTOR James MacBroom

INSPECTOR

AREA EVALUATED

OUTLET WORKS - CONTROL TOWER (continued)

Service Gates

Emergency Gates

Lightning Protection System

Emergency Power System

Wiring and Lighting System In Gate Chamber DISCIPLINE Hydraulics/Hydrology

DISCIPLINE

CONDITION

Good condition

Unknown

Good condition

PERIODIC INSPECTIO	N CHECK LIST
PROJECT Samuel P. Senior Dam,	DATE July 26, 1978
INSPECTOR Richard F. Murdock	DISCIPLINE Geotechnical
INSPECTOR James MacBroom	DISCIPLINE Hydraulics/Hydrology
AREA EVALUATED	CONDITION
OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS	
a. Approach Channel	Underwater (Reservoir)
General Condition	
Loose Rock Overhanging Channel	
Trees Overhanging Channel	
Floor of Approach Channel	
b. Weir and Training Walls	
General Condition of Concrete	Good condition
Rust or Staining	None
Spalling	
Any Visible Reinforcing	None
Any Seepage or Efflorescence	None
Drain Holes	Some drainage of drain boles.
c. Discharge Channel	
General Condition	
Loose Rock Overhanging Channel	
Trees Overhanging Channel	A few large healthy trees present.
Floor of Channel	Good - bedrock surfaces.
Other Obstructions	None

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## PERIODIC INSPECTION CHECK LIST

PROJECT Samuel P. Senior Dam

DATE\_\_\_\_July 26, 1978

INSPECTOR James MacBroom

DISCIPLINE Hydraulics/Hydrology

INSPECTOR

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DISCIPLINE

No trees or loose rock over- hanging channel.
The channel is in excellent condition.
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# APPENDIX B

ENGINEERING DATA

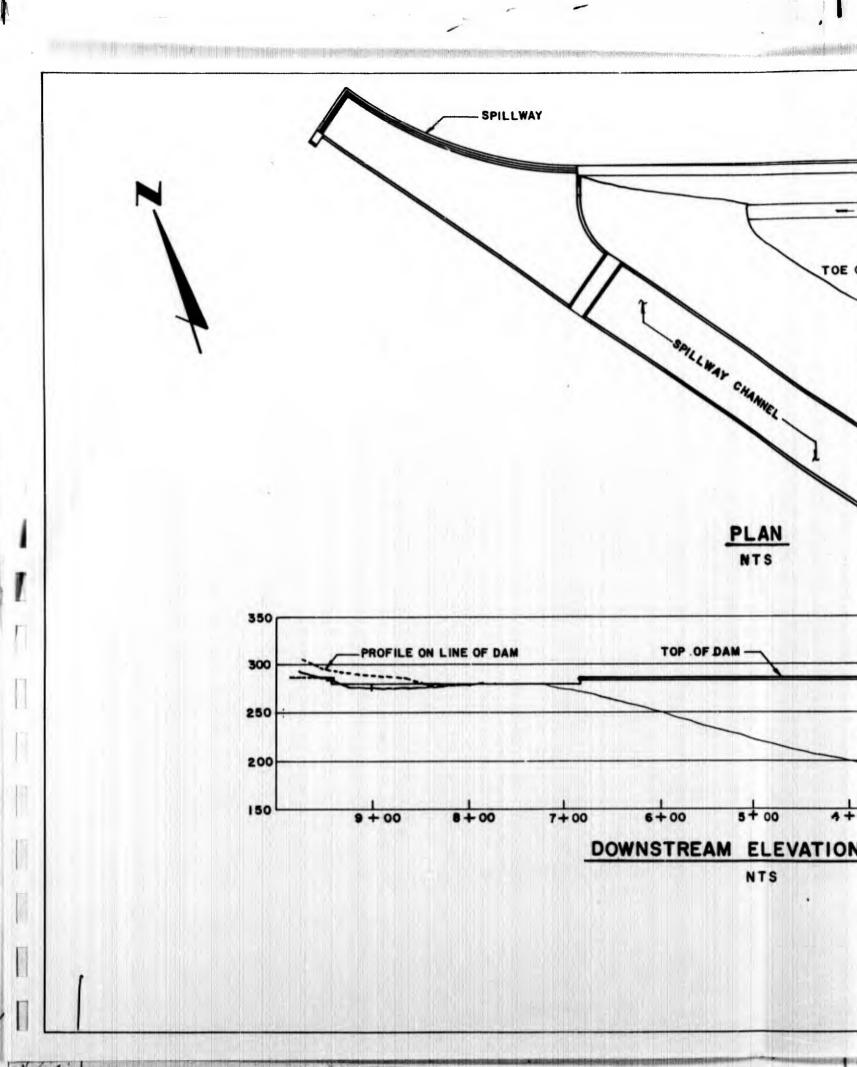
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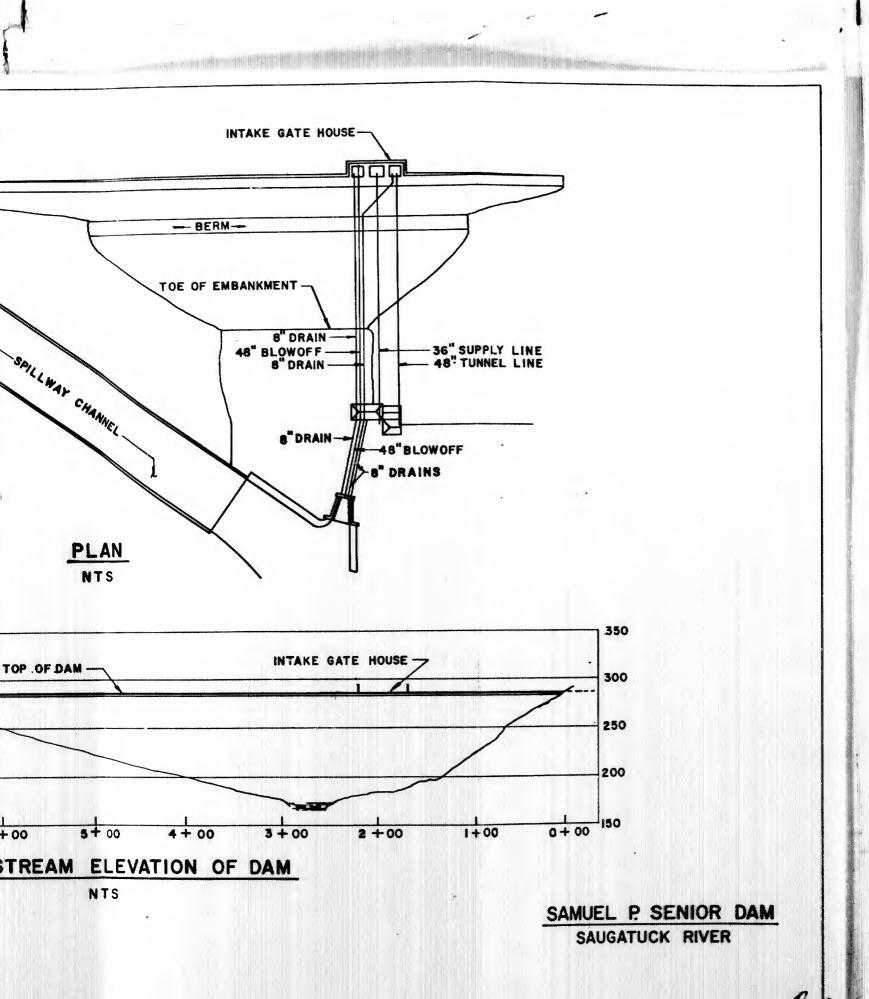
	CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I	NAME OF DAM Samuel P. Senior I.D. NO. CT 00108
- M344	REMARKS	
AS-BUILT DRAWINGS	Conn. State Library - Hartford	
REGIONAL VICINITY MAP	Available From U.S.G.S.	
CONSTRUCTION HISTORY	Records State D.E.P. and Bridgeport Hydraulic Co.	Hydraulic Co.
TYPICAL SECTIONS OF DAM	Available From Plans.	
OUTLETS - Plan	From Plans	
Details	From Plans	
- Constraints	Unknown	
- Discharge Ratings	Unavailable	
RAINFALL/RESERVOIR RECORDS	From Bridgeport Hydraulic Co.	
DESIGN REPORTS	None	
GEOLOGY REPORTS	None	
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	None None Available From Plan None	
MATERIALS INVESTIGATIONS BORINGS RECORDS LABORATORY FIELD	None From Plan None None	

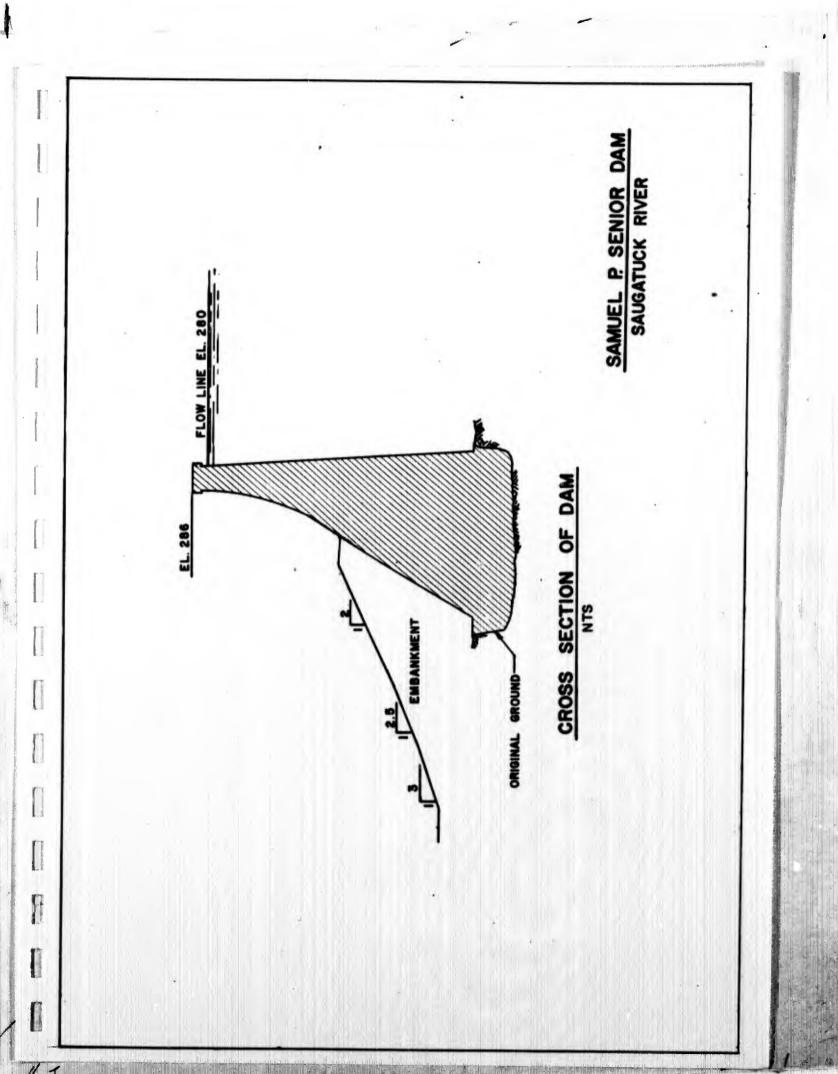
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8	CHECK LIST NAME OF DAM Samuel P. Senior ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION I.D. NO. CT 00108 PHASE I
ITEM	REMARKS
POST-CONSTRUCTION SURVEYS OF DAM	None
BORROW SOURCES	Construction Records
MONITORING SYSTEMS	None
MODIFICATIONS	Unknown
HIGH POOL RECORDS	Approximate From Bridgeport Hydraulic Co. Records
POST-CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
MAINTENANCE OPERATION RECORDS	Inspection Reports From Bridgeport Hydraulic Co.
SPILLWAY PLAN	
SECTIONS	Plans
DETAILS	Plans
OPERATING EQUIPMENT PLANS & DETAILS	Plans

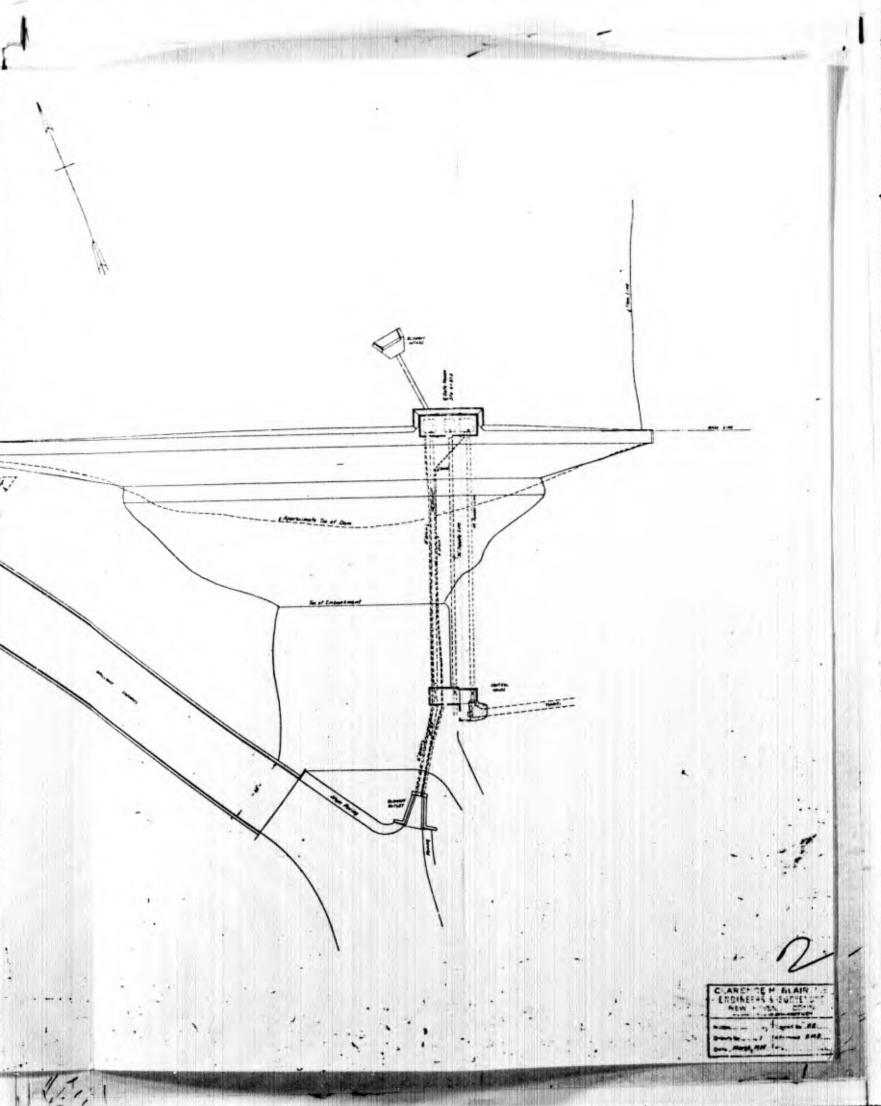
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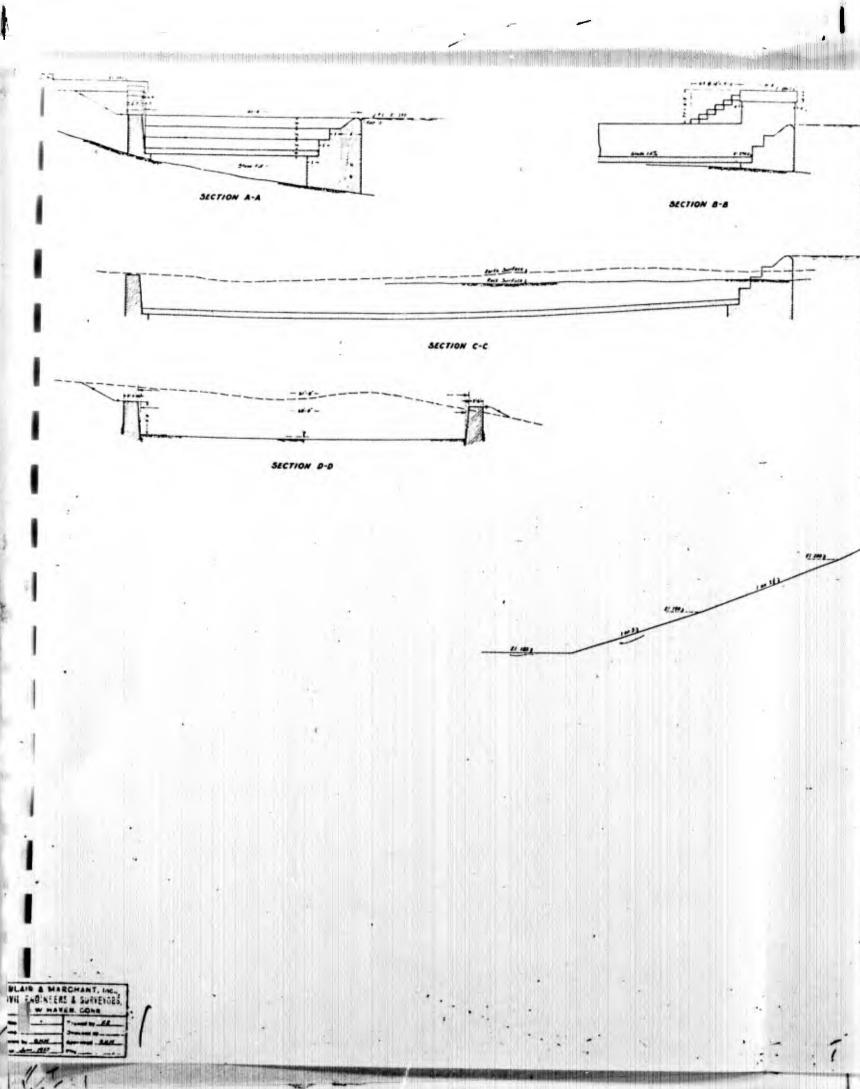


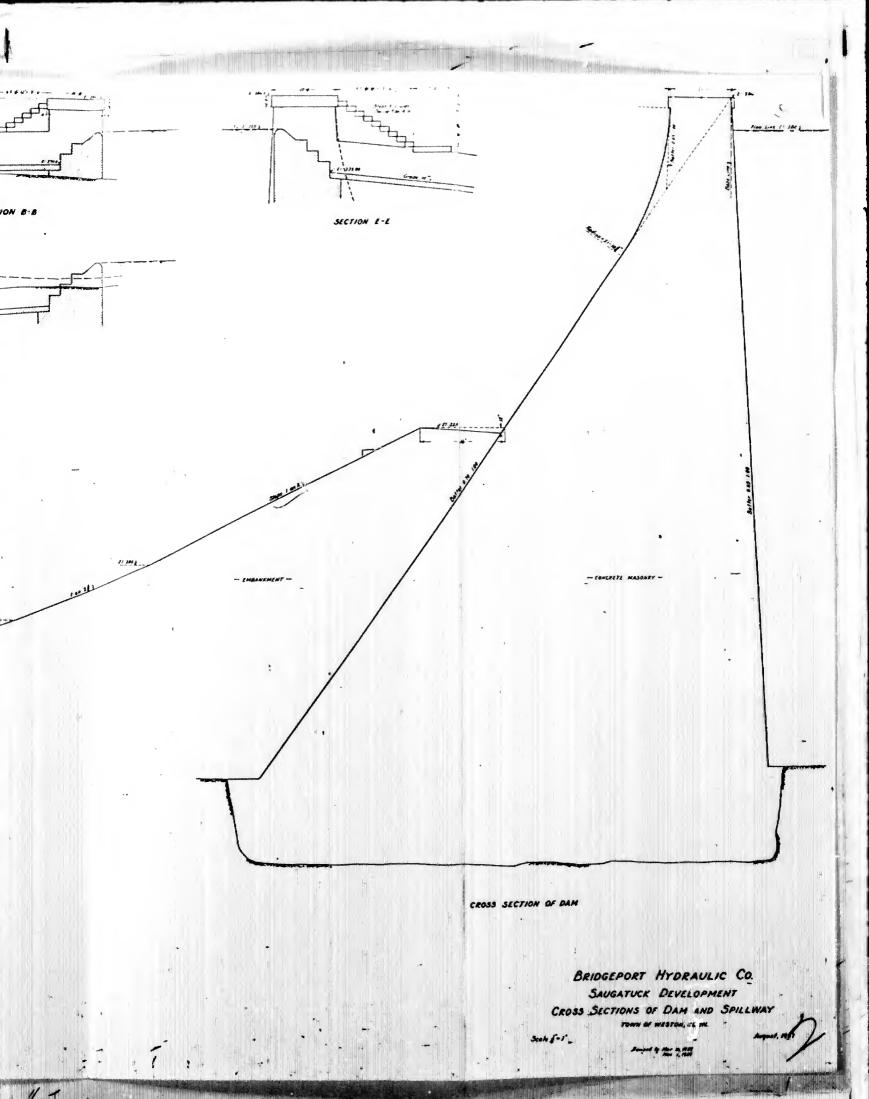
17 BRIDGEPORT HYDRAULIC CO. SAUGATUCK, DEVELOPMENT GENERAL PLAN AT DAM TOWN OF WESTON, COM -----

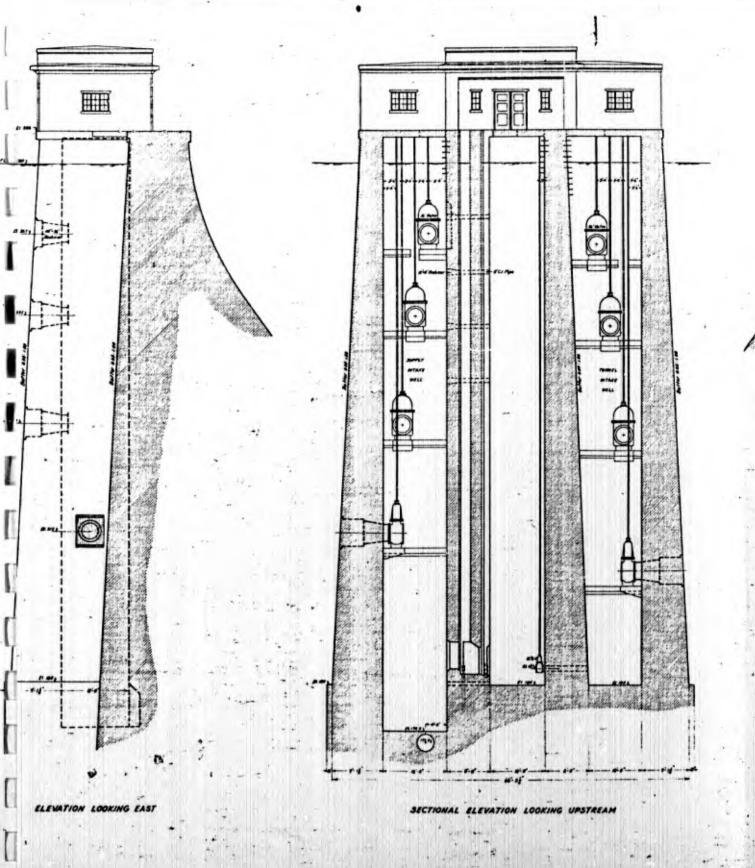


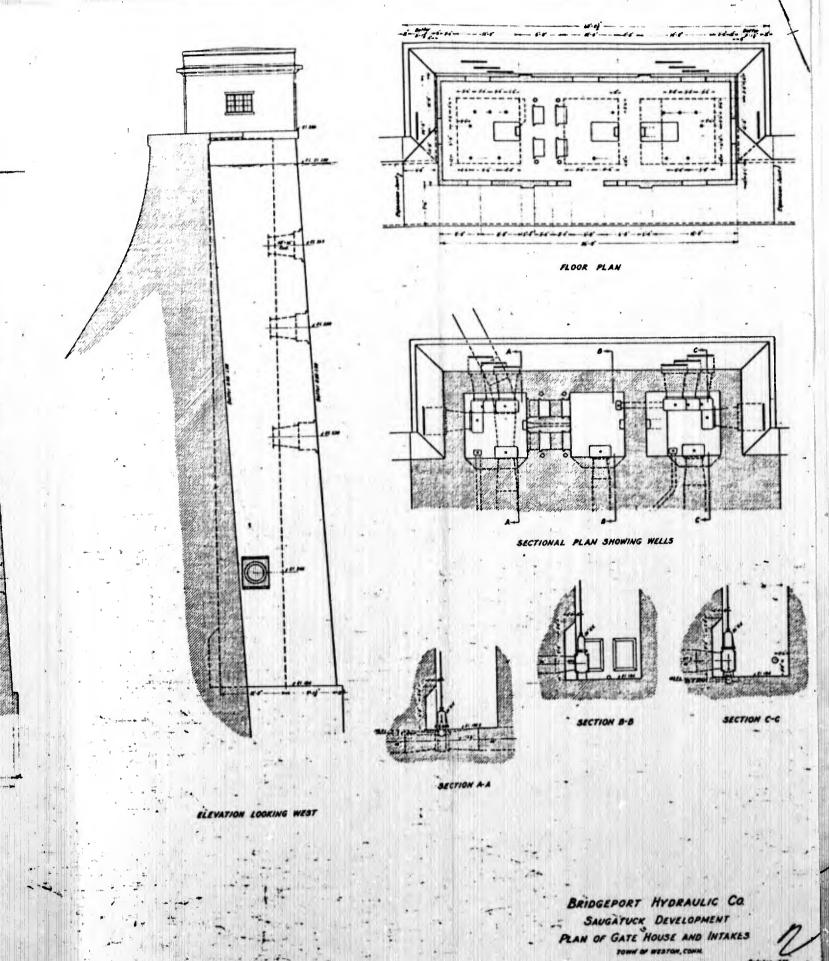








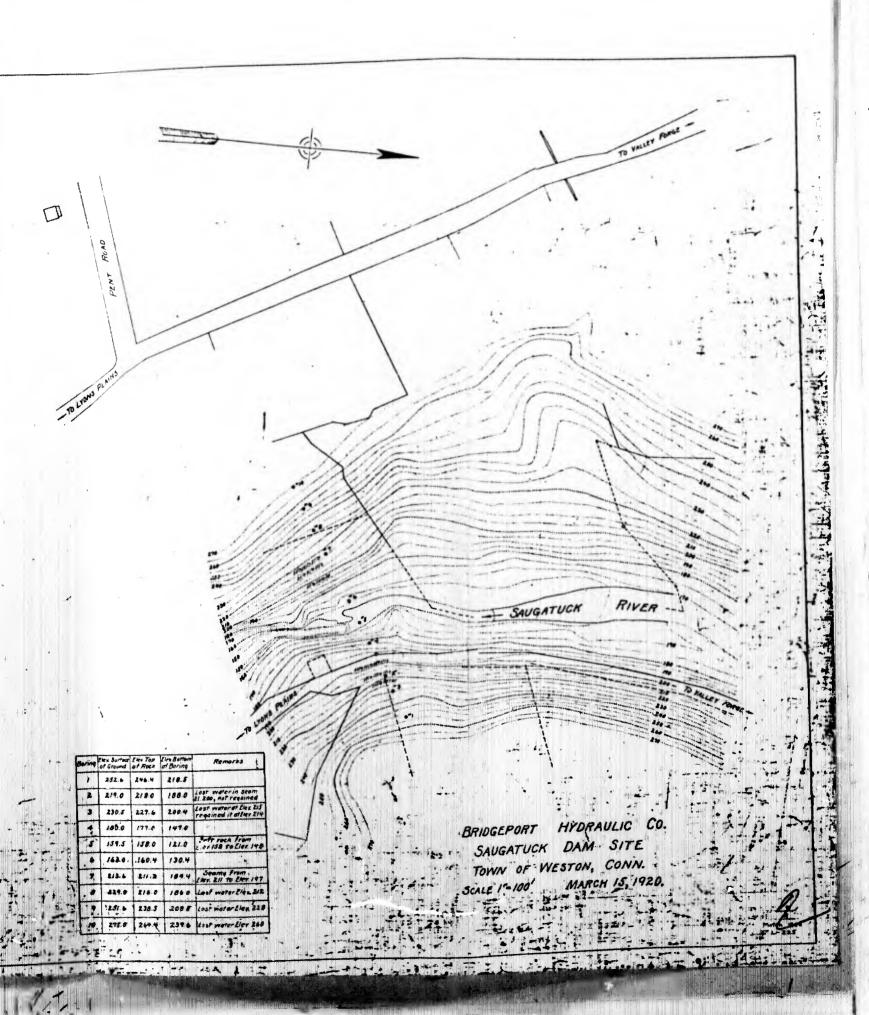


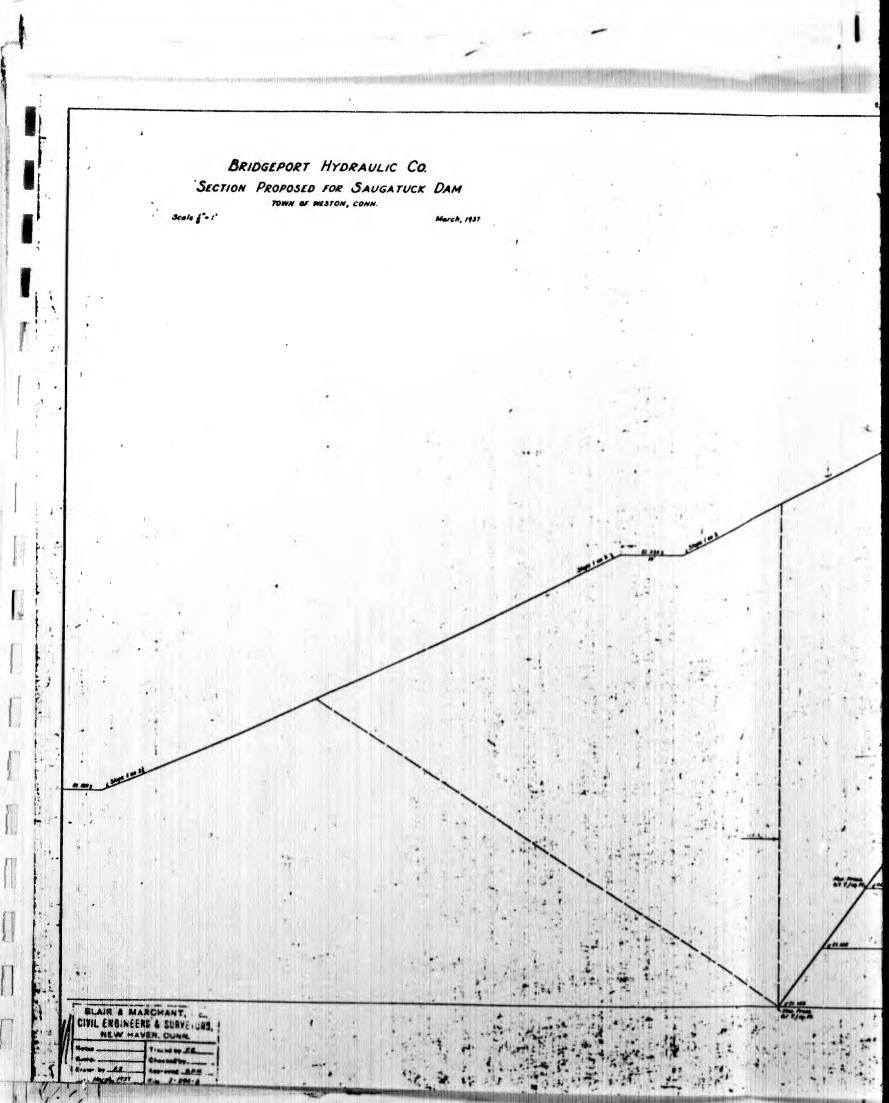


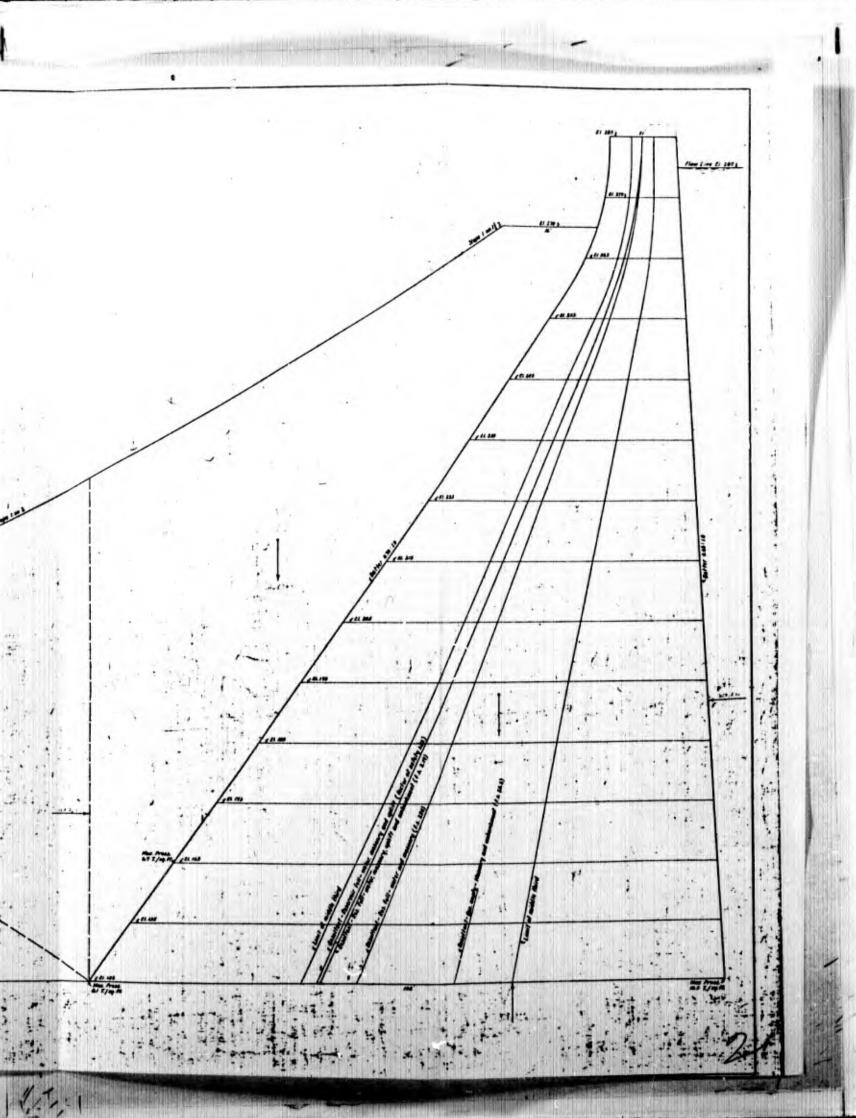
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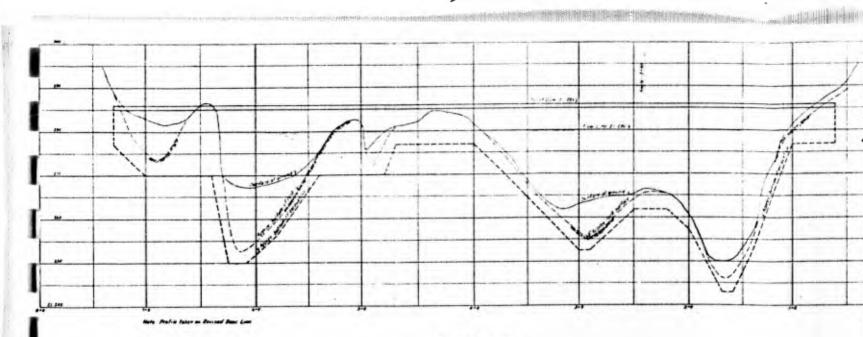




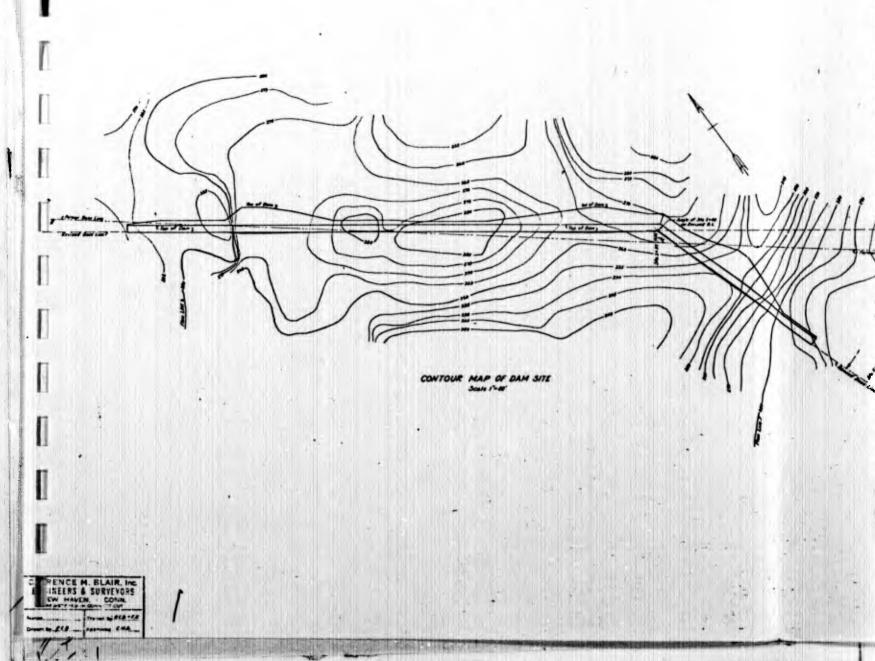


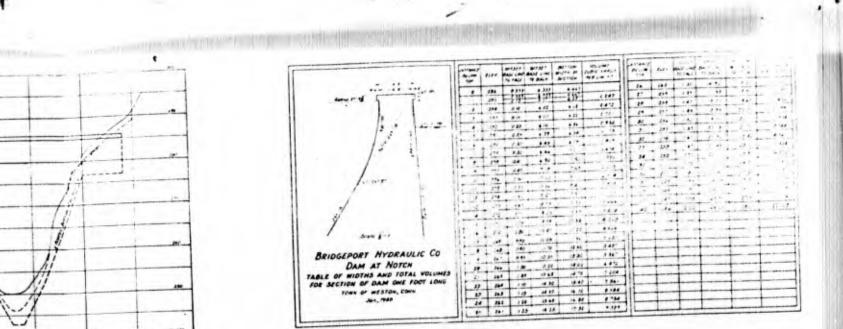


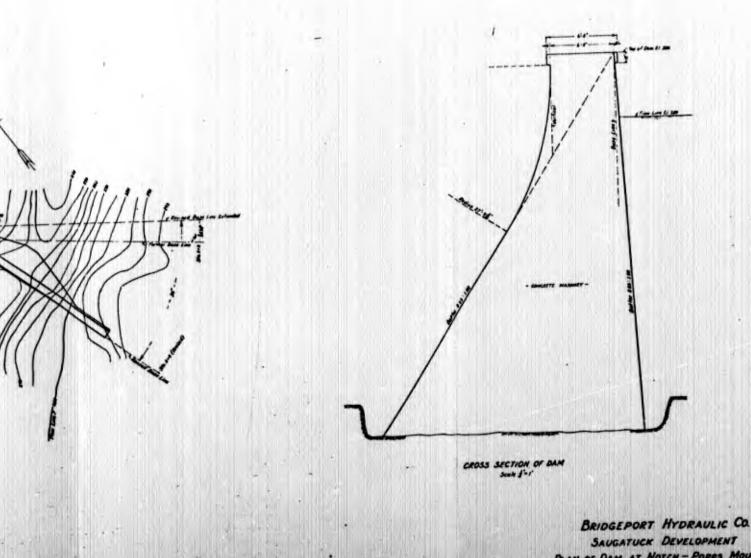




PROFILE OF DAM







SAUGATUCK DEVELOPMENT PLAN OF DAM AT NOTCH - POPPS MOUNTAIN -----

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### APPENDIX C

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PHOTOGRAPHS

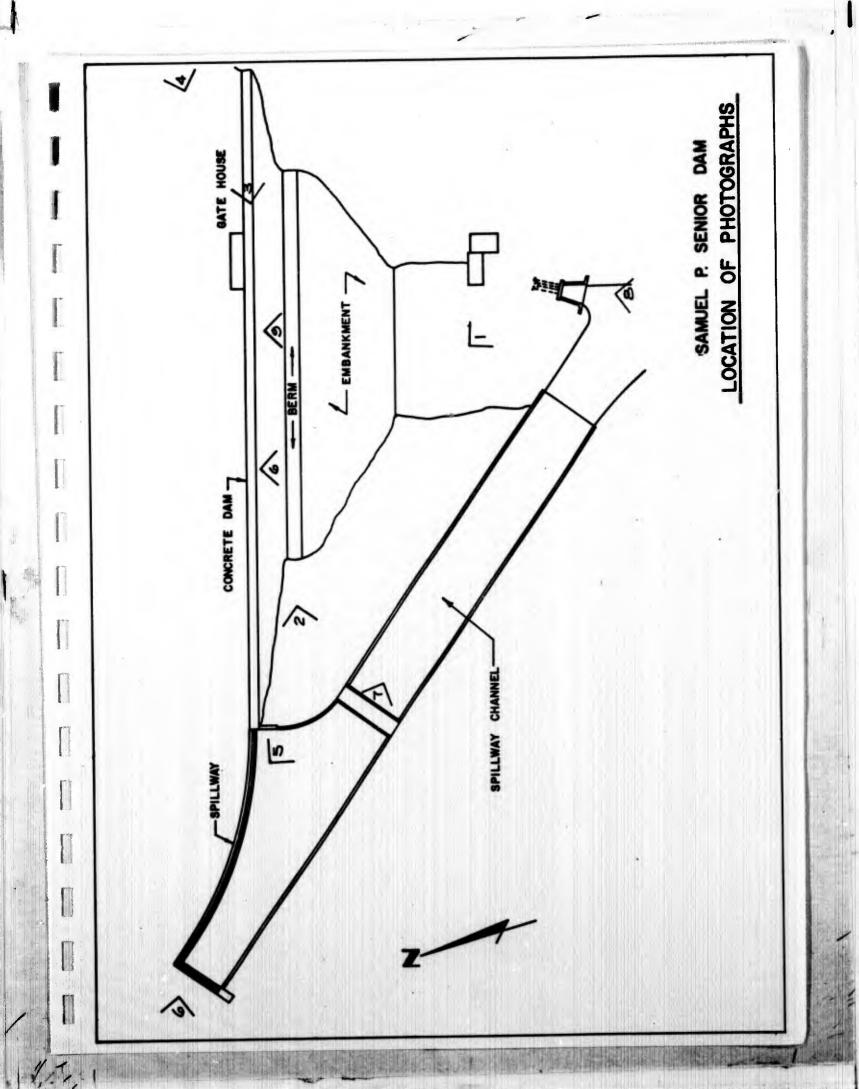




PHOTO #1: View of the western, downstream face of the dam.



PHOTO #2: View along the face of the dam, looking east.

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PHOTO #3: Looking west along the crest of the dam.



PHOTO #4: Upstream face of the dam and upper gate house.

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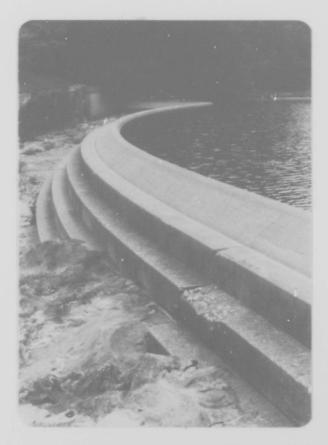


PHOTO #5: View of the spillway, looking west.



PHOTO #6: View of the spillway and dam, looking east from west abutment.

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PHOTO #7: The spillway discharge channel, looking down at the natural river in the background.



PHOTO #8: Blow-off discharge point, showing the wingwalls and riprap.

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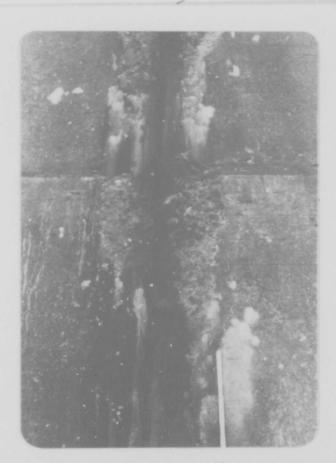


PHOTO #9: Typical spalling at a construction joint.



PHOTO #10: Holes cored in concrete dam-purpose unknown.

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PHOTO #11: View looking south along the concrete dike.



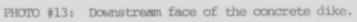
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PHOTO #12: View looking north along the concrete dike.





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#### APPENDIX D

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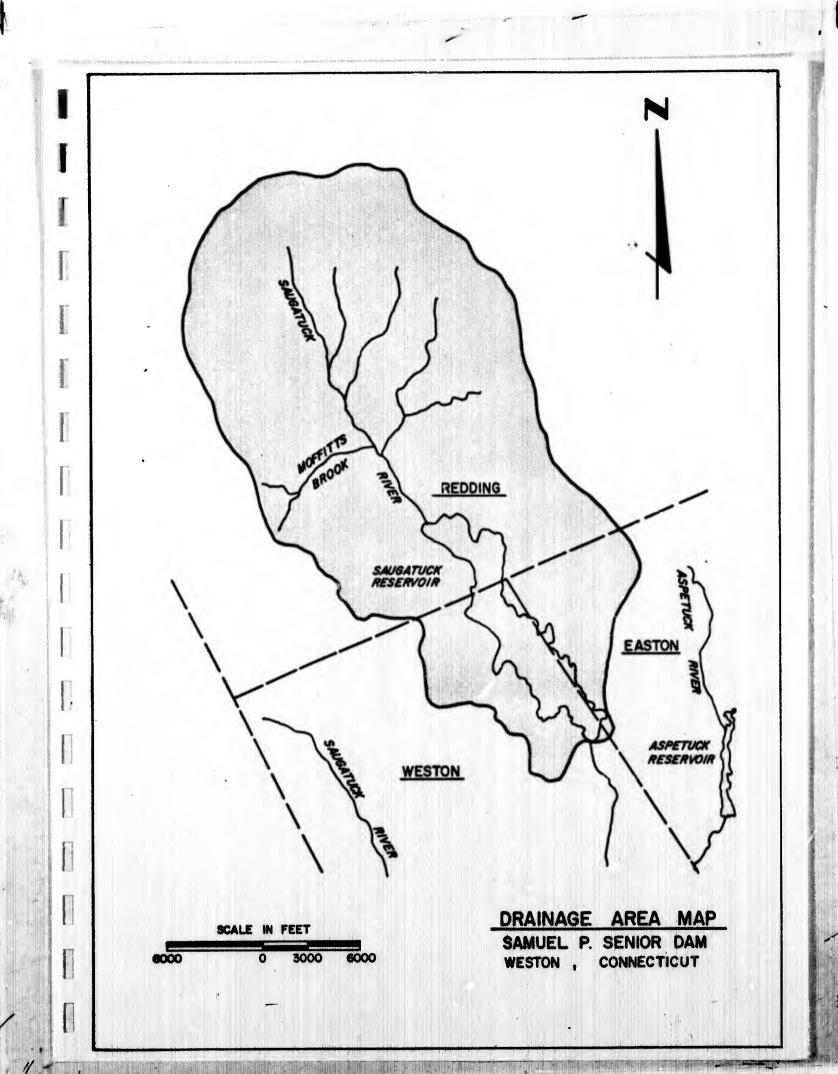
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HYDROLOGIC COMPUTATIONS



CT\_78-36-10 FLAHERTY-GIAVARA ASSOCIATES SHEET NO .\_ OF\_ ENVIRONMENTAL DESIGN CONSULTANTS BY JGM DATE 8/7/70 ONE COLUMBUS PLAZA, NEW HAVEN, CONN. 06510/203/789-1260 CHK'D. BY CONTE 2/2/2-UNATUCK DAM P.M.F. PEAK FLOW ESTIMATE DRAINAGE AREA IS 34,6 SQ. MILES METHOD #/ REFER TO PRELIMINARY GUIDANCE FOR ESTIMATING PMF DISCHARGES " by NEW ENGLAND DIVISION, CORPS OF ENGINEERS UNIT FLOW = 1410 CFS /Mi 2 (Rolling Curve) PMF = (34.6 SQ mi) × (1410 CFS/mi2) = 48,786CFS METHOD #2 REFER TO "CONN WATER RESOURCE BULLETIN NO. 17, PART 4" BY U.S.G.S. MEAN ANNUAL FLOOD = 1200 CFS Q100 = 5×MAF = 5×1200 CFS = 6000 CFS PMF = 5 × Q100 (APPROXIMATE) PMF = 5x 6000 CFS = 30,000 CFS METHOD #3 REFER TO FAIRFIELD , CT F.I.A. FLOOD INSURANCE STUDY, \* FREQUENCY, DISCHARGE, DRAINAGE AREA CURVES" Q100 = 7000 CFS PMF = 5 × Qico (APPROXIMATE)

PMF = 5x7000 CFS= 35,000 CFS

\* USE 48,800 CFS FOR SPILLWAY TEST FLOOD



FORMATION OF INFLOW HYDROGRAPH

1) P.M.F. = 48,800 CFS

T 10-36-10

JGATUCK DAM

2) FORM A TRIANGULAR HYDROGRAPH WITH A 24 HOUR DURATION, PEAK @ 8 HOURS

TIME	NIT FLOW	FLOW RATE
0246802604	0.00 0.25 0.50 0.75 1.00 0.875 0.75 0.75 0.50 0.25 0.25	0012,200 24,400 36,600 42,7000 42,7000 36,600 12,200 12,200

78-36-10 Ugatuck Dam

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FLAHERTY-GIAVARA ASSOCIATES SHE ENVIRONMENTAL DESIGN CONSULTANTS BY... ONE COLUMBUS PLAZA. NEW HAVEN, CONN. 06510/203/769-1260 CHK

SHEET NO. 3 OF 3 BY JGM DATE 8/7/78 CHK'D.BY

SPILLWAY CAPACITY

 $Q = C L H^{3/2}$ 

C ≈	3.6		
L =	295 FT	(EFFECTIVE	
H =	G FT	(EL. 286-	EL. 280)

 $Q_{MAX} = 3.6(295)(6)^{1.5} = 15,608 \text{ cFS}$ 

 $\frac{SPILLWAY CAPACITY}{TEST FLOOD} = \frac{15,608}{48,800} = 32\%$ 

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#### APPENDIX E

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INFORMATION - NATIONAL INVENTORY OF DAMS

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