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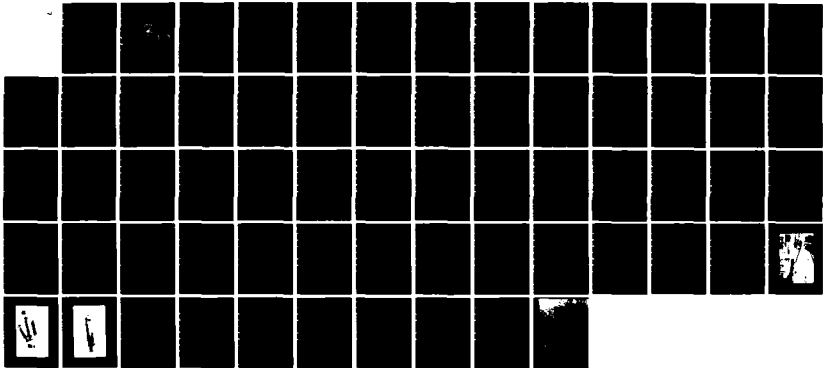
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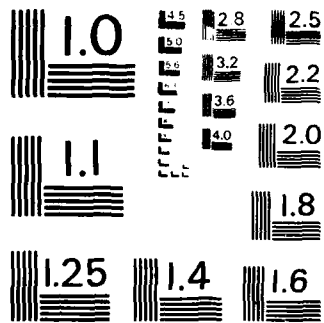
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# NAVAL POSTGRADUATE SCHOOL

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## THESIS

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CERENKOV RADIATION GENERATED BY PERIODIC  
ELECTRON BUNCHES IN A FINITE AIR PATH

by

Lawrence A. Newton

December 1983

Thesis Advisor: F. R. Buskirk

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Cerenkov Radiation Generated  
by Periodic Electron Bunches  
in a Finite Air Path

by

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MASTER OF SCIENCE IN PHYSICS

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**ABSTRACT**

Microwave Cerenkov radiation is measured for the case of bunched electron beams which exceed the velocity of light in a finite air path. The theoretical equation for prediction of the form of the power for Cerenkov radiation is tested experimentally for this case. Initial verification of the theory is observed.

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## TABLE OF CONTENTS

I.	INTRODUCTION . . . . .	7
II.	EXPERIMENT . . . . .	14
	A. BASIC EXPERIMENTAL DESIGN . . . . .	14
	B. EXPERIMENTAL APPARATUS . . . . .	15
	1. LINAC . . . . .	16
	2. Air Path . . . . .	16
	3. Mirror . . . . .	17
	4. End Station Detection Apparatus . . . . .	17
	5. Cable . . . . .	21
	6. Observer Station . . . . .	21
III.	RESULTS . . . . .	25
	A. METHOD OF DATA REDUCTION . . . . .	25
	B. DATA . . . . .	25
	C. CONCLUSIONS . . . . .	32
	APPENDIX A: FORTRAN PROGRAM FOR CALCULATING CERENKOV RADIATION CURVES . . . . .	35
	APPENDIX B: FORTRAN PROGRAM - CERENKOV CURVES WITH DATA POINTS . . . . .	40
	APPENDIX C: FORTRAN PROGRAM - SUM OF CERENKOV CURVES WITH DATA POINTS . . . . .	46
	APPENDIX D: EXPERIMENTAL APPARATUS . . . . .	52
	APPENDIX E: TABULAR DATA FOR FIGURES . . . . .	56
	LIST OF REFERENCES . . . . .	61
	INITIAL DISTRIBUTION LIST . . . . .	62

**LIST OF TABLES**

I.	Variable Definitions . . . . .	10
II.	LINAC Parameters . . . . .	16
III.	Tabular Data for Figure 3.1 . . . . .	56
IV.	Tabular Data for Figure 3.2 . . . . .	57
V.	Tabular Data for Figure 3.3 . . . . .	58
VI.	Tabular Data for Figure 3.4 . . . . .	59
VII.	Tabular Data for Figure 3.5 . . . . .	60



## LIST OF FIGURES

1.1	Cerenkov Radiation . . . . .	8
1.2	Third Harmonic for $L = 0.7, 0.9, 1.5$ meters . . .	12
1.3	Harmonics 3,5,7 for $L = 1.0$ meters . . . . .	13
2.1	Experimental Design . . . . .	15
2.2	Antenna Beam Profile for the Electric Field . .	19
2.3	Antenna Beam Profile for the Magnetic Field . .	20
2.4	Filter Band-pass for the Third Harmonic . . . .	22
2.5	Filter Bandpass for the Fourth Harmonic . . . .	23
3.1	Harmonic=3 : $L=1.0$ m: Filter = 3rd . . . . .	27
3.2	Harmonic=4 : $L = 1.0$ m : Filter=4th . . . . .	28
3.3	Harmonics= 3-7 : $L = 1.0$ m : Filter = Waveguide . . . . .	29
3.4	Harmonics= 3 + 4 : $L=1.0$ m : Filter = Waveguide . . . . .	32
3.5	Harmonics= 3 + 6 : $L=1.0$ m : Filter = 3rd . . .	33
D.1	LINAC End-Station . . . . .	53
D.2	Detection Apparatus Components . . . . .	54
D.3	Assembled Detection Apparatus . . . . .	55

## I. INTRODUCTION

Since the speed of light is modified by the index of refraction in a dielectric, it is possible for relativistic electrons to have a velocity which actually exceeds that of light in the medium. In this circumstance a phenomenon known as Cerenkov radiation arises. This radiation appears in a cone, around the direction of motion of the electrons, defined by the Cerenkov angle.

$$\theta_c = \cos^{-1} (c/nv), \quad (\text{eqn 1.1})$$

where  $c$  is the speed of light in a vacuum,  $n$  is the index of refraction, and  $v$  is the velocity of the electrons. This radiation is analogous to acoustic shock waves in air.

F. R. Buskirk and J. R. Neighbours [Ref. 1] calculated the power of Cerenkov radiation for the case where the electrons are bunched and the dielectric medium is of finite length. The experiments described in this thesis were designed to check those theoretical calculations.

Figure 1.1 depicts the pertinent physical relationships for this situation. See Table I for definitions of the variables. The first step in the theoretical derivation was to calculate the vector potential  $\underline{A}$  and the scalar potential,  $\phi$ , at a field point  $\underline{r}$  resulting from an element of charge at a location within the electron bunch. A key factor in the analysis is that the current and charge densities which appear in the expressions for the potentials are periodic and may be expressed as Fourier series. Therefore, the potentials themselves may also be expressed as Fourier series, with Fourier coefficients representing the frequency components.

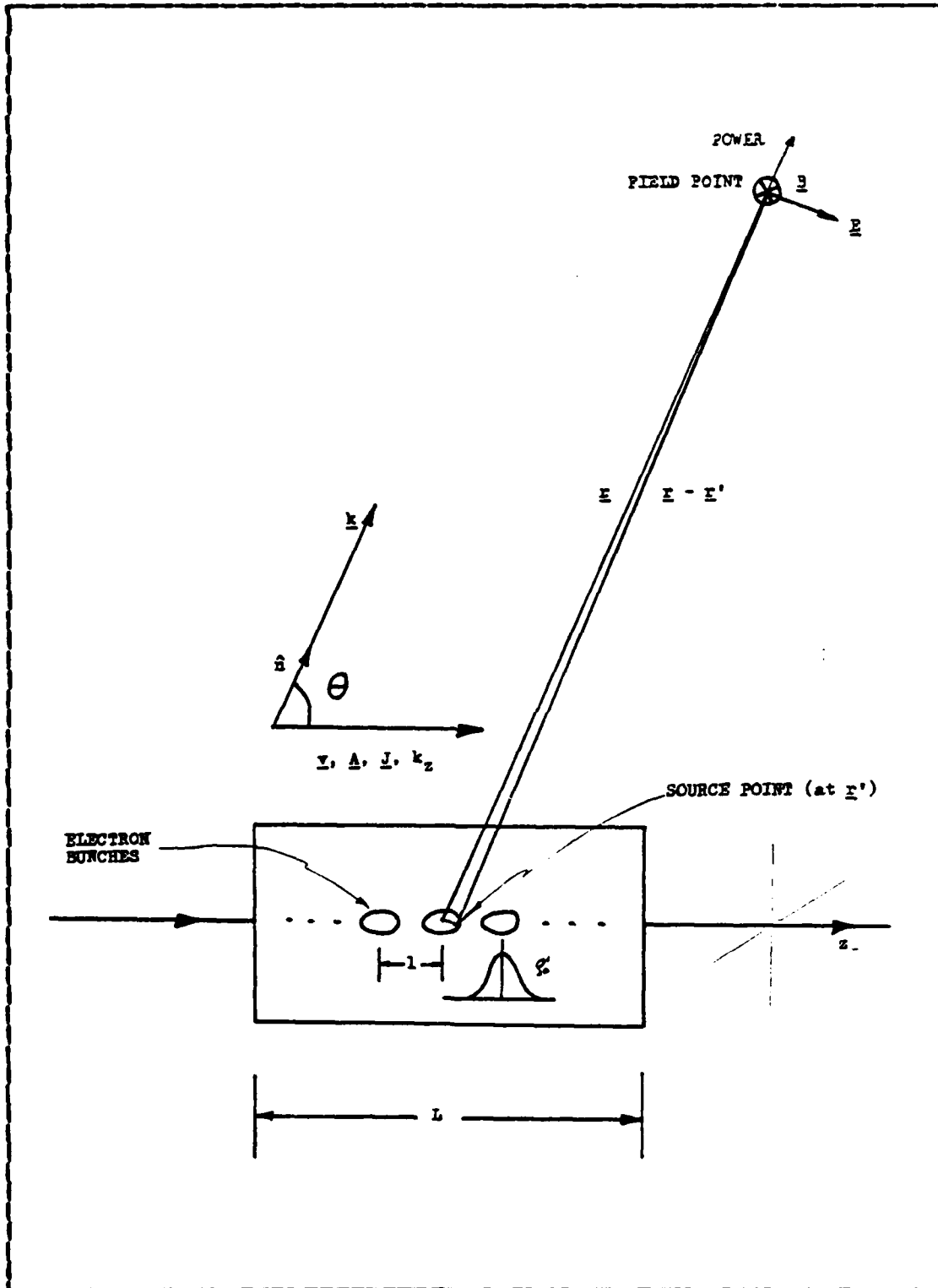


Figure 1.1 Cerenkov Radiation.

It is convenient to carry out the rest of the analysis in terms of the Fourier coefficients. The electric and magnetic field components are obtained from the potentials, and these, in turn, are used to find the frequency components of the average radiated power. An important assumption inherent in the procedure, which may directly affect experimental validity, is that the field point is assumed to be far from the source region. For details of the entire analysis, see [Ref. 2].

A principal result of [Ref. 2] is slightly recast in [Ref. 3] as the following expression for the power per unit solid angle at a given frequency,

$$W(\nu, n) = \frac{\mu}{2c} L^2 \nu^2 \nu_0^2 \sin^2 \theta |\rho'_0(\underline{k})|^2 I^2(u) , \quad (\text{eqn 1.2})$$

with the parameters defined as follows:

$$u = \frac{kL}{2} (\cos \theta_c - \cos \theta) , \quad (\text{eqn 1.3})$$

$$I(u) = \frac{\sin u}{u} , \quad (\text{eqn 1.4})$$

and

$$\rho'_0(\underline{k}) = \iiint_{-\infty}^{\infty} d^3r e^{-i\underline{k} \cdot \underline{r}} \rho'_0(\underline{k}) . \quad (\text{eqn 1.5})$$

Refer to figure 1.1 and table I for clarification of these parameters.

The frequencies appearing in equation 1.2 are harmonics of the electron bunch frequency, which is a constant ( $\nu_0$ ). Thus, writing ( $\nu$ ) as ( $j\nu_0$ ), and using a one-dimensional

**TABLE I**  
**Variable Definitions**

$\underline{J}$	= $\rho \underline{v}$	= current density
$l$	= $\underline{v}/\nu_0$	= bunch spacing
$\nu_0$		= bunch frequency
$\underline{v}$		= bunch velocity
$\underline{k}$		= power propagation direction
$\underline{n}$		= unit vector in the $\underline{k}$ direction
$L$		= length of finite emission region
$\underline{A}$		= vector potential
$\underline{r}$		= position vector of field point
$\underline{r}'$		= position vector of source point
$\rho'$		= Gaussian distribution of longitudinal bunch (charge) distribution
$b$		= parameter for the charge distribution
$\underline{E}$		= electric field vector
$\underline{H}$		= magnetic field vector

Gaussian distribution to describe the longitudinal bunch dimension, a relatively simple Cerenkov radiation power function is given by equation 1.6 (equations 9 and 10 of [Ref. 3] ). This is the expression which was used to compare theoretical to experimental results.

$$P_j(\theta) = \frac{2\mu\nu_0^4 q^2}{c} \frac{1}{4} L^2 \sin^2\theta \left( \frac{\sin u}{u} \right)^2 \text{Exp} \left( \frac{-k_z^2 b^2}{2} \right), (\text{eqn 1.6})$$

Note that the radiation function varies with the square of the harmonic number, the length  $L$  of the emission region, and the angle at which the radiation is being observed. Note also the interference factor, similar to what might be experienced with optical radiation, and the way in which the bunch dimension,  $b$ , appears in the expression. The length of the emission region and the angle appear not only directly, but also through the factor  $u$  (see equation 1.3).

The results of this simple equation are quite interesting. Due to the finite size of the emission region, radiation no longer appears only at the Cerenkov angle, but throughout a range of angles determined by the  $(\sin u)/u$  factor. Figure 1.2 shows how the radiation is spread for three different sizes of emission region. For a given harmonic, smaller emission regions cause greater spread, or diffraction of the radiation. The power is distributed to varying degrees among the different harmonics also, as depicted by figure 1.3. Higher harmonics have larger peak powers, and are peaked at a smaller angle than are lower harmonics.

For this experiment, the microwave portion of the spectrum was investigated, and the dielectric medium for the electron path was chosen to be air. The electrons were accelerated to relativistic velocities by the Naval Postgraduate School LINAC, which produces electrons with energies of approximately 100 Mev. For the theoretical calculations, a Fortran program (see appendix A) was used to calculate the power as a function of angle from equation 1.6. Variants of this program (appendices B and C) were used to superimpose data points over the theoretical curves.

The experimental apparatus and procedures are described in detail in the next chapter.

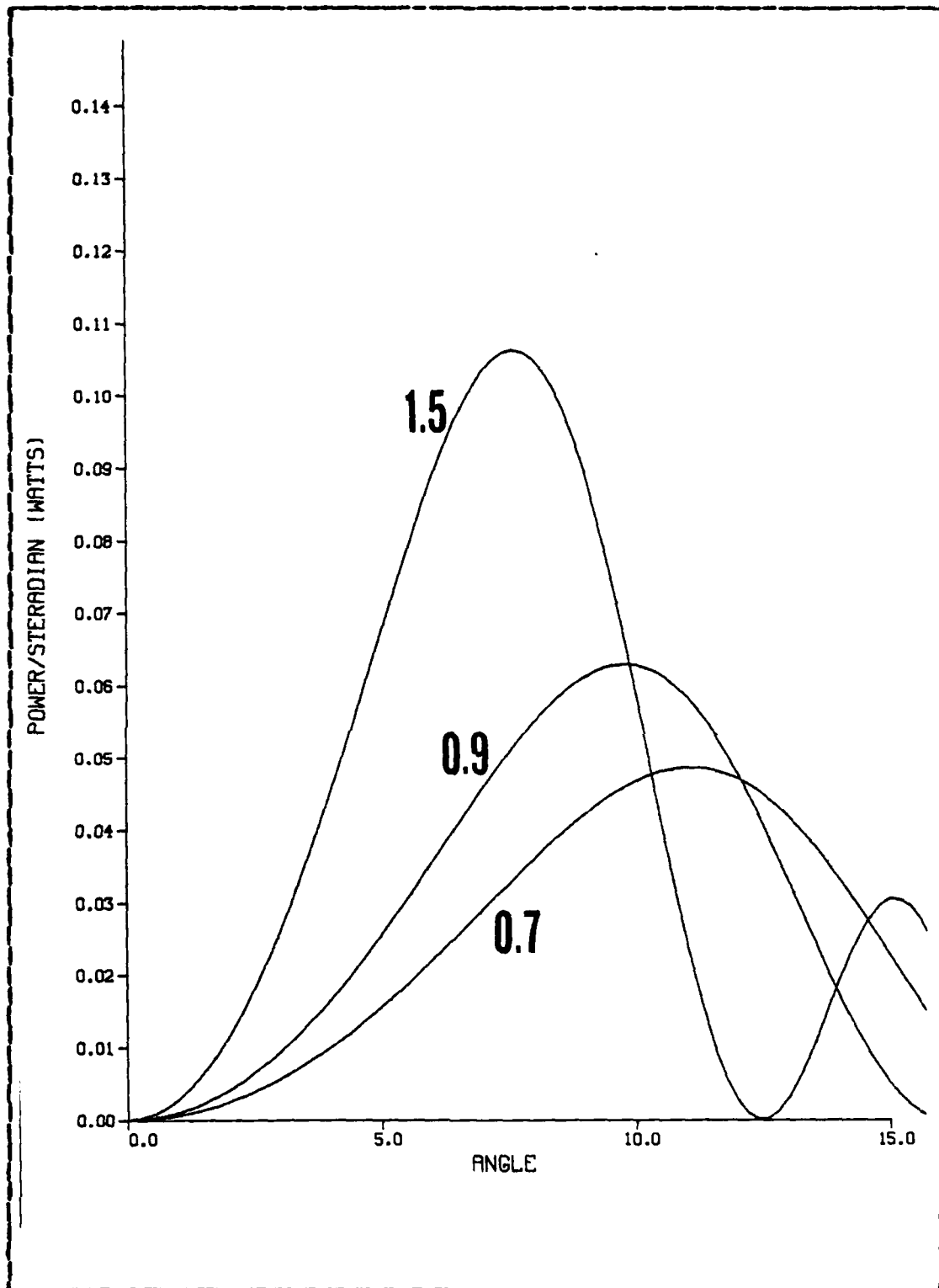


Figure 1.2 Third Harmonic for  $L = 0.7, 0.9, 1.5$  meters.

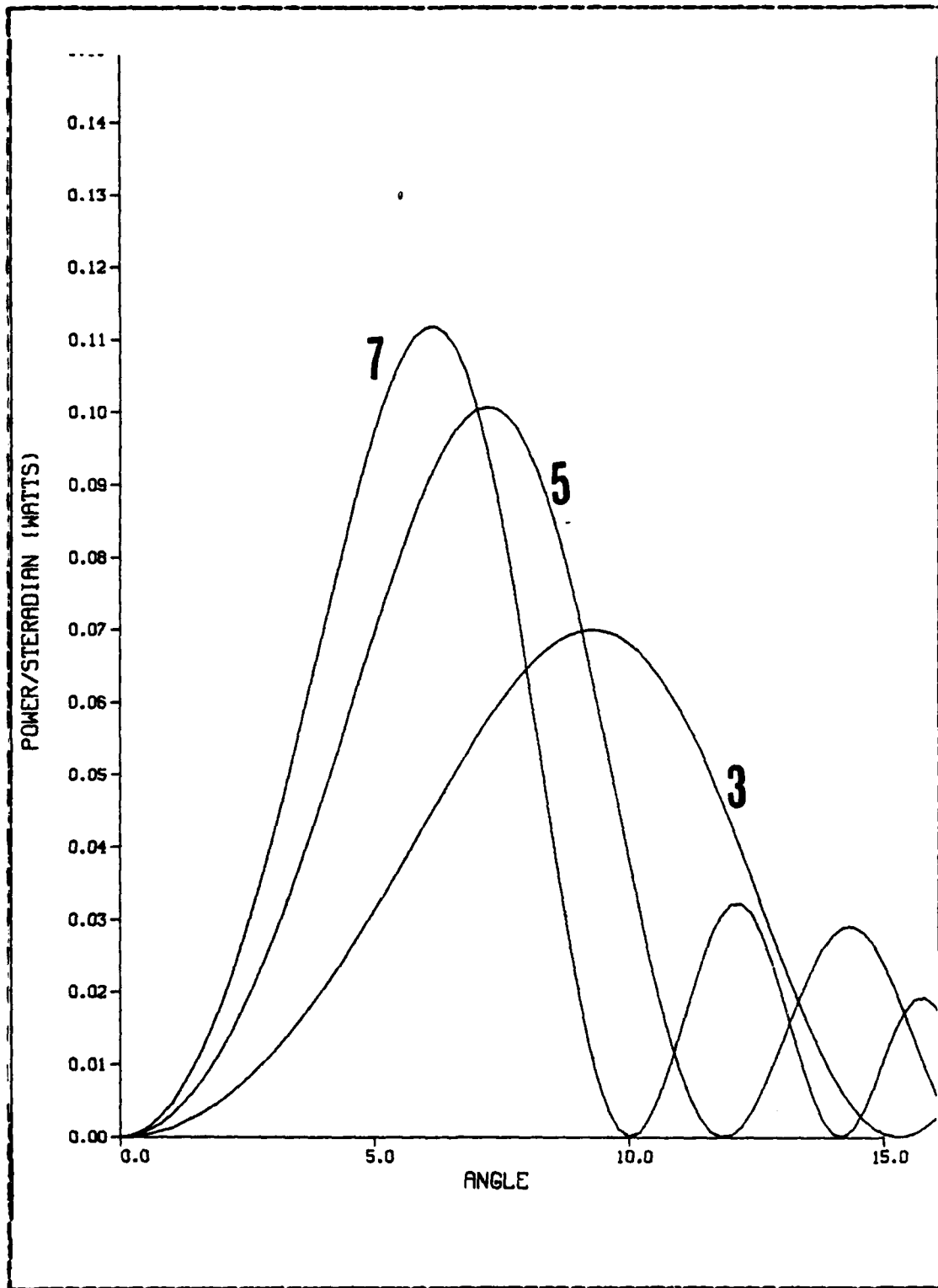


Figure 1.3 Harmonics 3,5,7 for L = 1.0 meters.



## II. EXPERIMENT

### A. BASIC EXPERIMENTAL DESIGN

The purpose of this experiment was to measure the power from Cerenkov radiation as a function of angle, in order to compare it with theoretical curves such as those depicted in figures 1.2 and 1.3. The basic design for this experiment is shown in figure 2.1. Photographs of the experimental apparatus are presented in Appendix D. The electron bunches exit the Linac aperture and emit Cerenkov radiation until they reach the aluminum mirror. This mirror allows the electrons to pass and proceed into the beam dump, while the microwave radiation of interest is reflected into the detector area. The mirror therefore performs the function, required by theory, that the radiation be emitted over a finite distance. The detector is mounted on a pivot arm, which is placed such that the detector is always pointed at the virtual center of the emission region. The pivot arm also fixes the distance from the center of the emission region to the detector, so that the distance over which the radiation travels is eliminated as a variable.

With this experimental setup, the basic experimental procedure was to sweep the detector over the angular range of interest using a small motor in the detector mount. The signal picked up by the detector was transmitted to the observer station, where it was fed into an amplifier and then into both an oscilloscope and a pulse height analyzer. The oscilloscope allowed a gross measure of power, while the frequency distribution measured by the pulse height analyzer gave a more precise value. The end result of this procedure was tabular data in the form of signal versus angle.

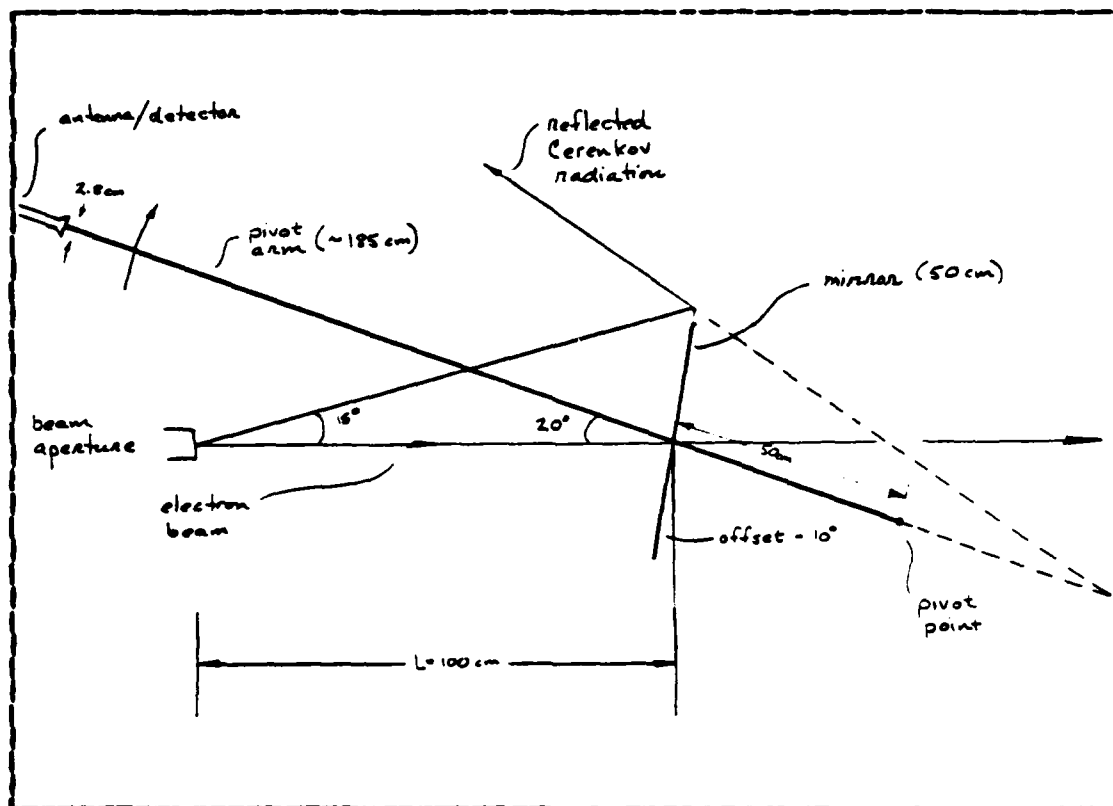


Figure 2.1 Experimental Design.

This brief overview of the experimental design is amplified in the next section with a more detailed look at various elements of the experimental apparatus.

## B. EXPERIMENTAL APPARATUS

In this section, the components of the experimental apparatus will be examined, in order to provide a precise understanding of the experiment. The various components of the signal train will be reviewed in order, from the originating device (the LINAC) to the final detection and analysis components.

## 1. LINAC

The salient features of the LINAC are listed in table II. These parameters are the same as those calculated by A. Saglaa in prior thesis work with the LINAC at the

TABLE II  
LINAC Parameters

Bunch Frequency:	2.856 GHz
Bunch Velocity:	2.997886E08 m/s
Bunch Size Parameter:	0.24 cm
Electron Energy:	100 MeV
Bunch Spacing:	10.5 cm

Naval Postgraduate School [Ref. 4]. These parameters also meet those chosen in [Ref. 3] which gives the theoretical curves for Cerenkov radiation. The LINAC provided fairly consistent signals for the experiments which are reported here. However, the signal eventually developed instabilities which precluded further experiments. That is, it became impossible to distinguish between signal variation due to the LINAC and that due to variation in the angle of detection. It may be that some of the experimental deviation from theory can be adequately explained by the variability of the LINAC itself.

## 2. Air Path

The air path was chosen to be 1.0 meter in length, which was convenient for the dimensions of the LINAC end station. The characteristic index of refraction for air was taken to be 1.000268, which is the same as that given for

air in [Ref. 3]. This gives a speed of light in air of 2.997127E08 meters per second, which is less than the velocity of 100 Mev electrons (see Table II).

### 3. Mirror

A polished aluminum mirror 50 centimeters in length was used to fix the path length. The mirror performed the dual function of allowing the electron bunches to pass and proceed into the beam dump, while causing the microwave Cerenkov radiation to be reflected into the detection area. The electron bunches continued to emit Cerenkov radiation after passing through the mirror. It was assumed that this radiation did not reach the detection area, due to the inherent weakness of the signal, and due to the distance and multiple reflections it would have to travel through in order to reach the detection area.

The mirror was tilted 10 degrees, causing the reflection axis to be offset 20 degrees from the beam axis. Therefore, the actual length of the emission region varied between approximately 95 and 105 centimeters. Measurements were made over a range of from 0 to 15 degrees. The mirror was long enough to reflect most, but not all, of the radiation at 15 degrees. See figure 2.1 for details of the geometry of the experiment.

### 4. End Station Detection Apparatus

The detection apparatus was mounted at the end of a pivot arm of fixed length. The pivot point was located at the center of the virtual image projected by the mirror, in order for the detector to always be pointed at the virtual center of the emission region. Theory assumed that the emission region would be a short distance, small compared to the detector distance  $r'$  (field point). Focusing the detector on the center of the emission region was done to

approximate theory as closely as possible. The pivot arm also kept the detector at a fixed distance from the (virtual) center of the emission region. Therefore, the distance of travel of the measured radiation was approximately the same for all angles, so that variation in distance would have minimal effect on the signal variation.

a. Antenna

A small antenna, with a lateral dimension of 2.8 centimeters, served as the forward end of the detection apparatus. This antenna served two functions. First, it was small enough that, with the given length of the pivot arm, the antenna subtended an arc length of approximately 1 degree. Therefore, an experimental measurement resolution of 1 degree was obtained. Further, this antenna had a very wide beam width. The antenna profiles for the electric and magnetic fields are given in figures 2.2 and 2.3. Using the half-power points as cutoffs, the beam width is found to be greater than 60 degrees for both the E and H fields, and thus for the power as well. At a distance equal to the average of that between the antenna and the mirror, approximately 130 centimeters, the beamwidth covers an arc length of 68 centimeters, which is larger than the length of the mirror.

Therefore, radiation arriving at the antenna and originating from any part of the emission region would be collected by the antenna. This again approximates the theoretical condition that the emission region be a point source, since the antenna "sees" the entire emission region at every angle of interest.

In summary, the antenna's narrow dimensions have provided spatial resolution, while its wide beamwidth has approximated a theoretical requirement.

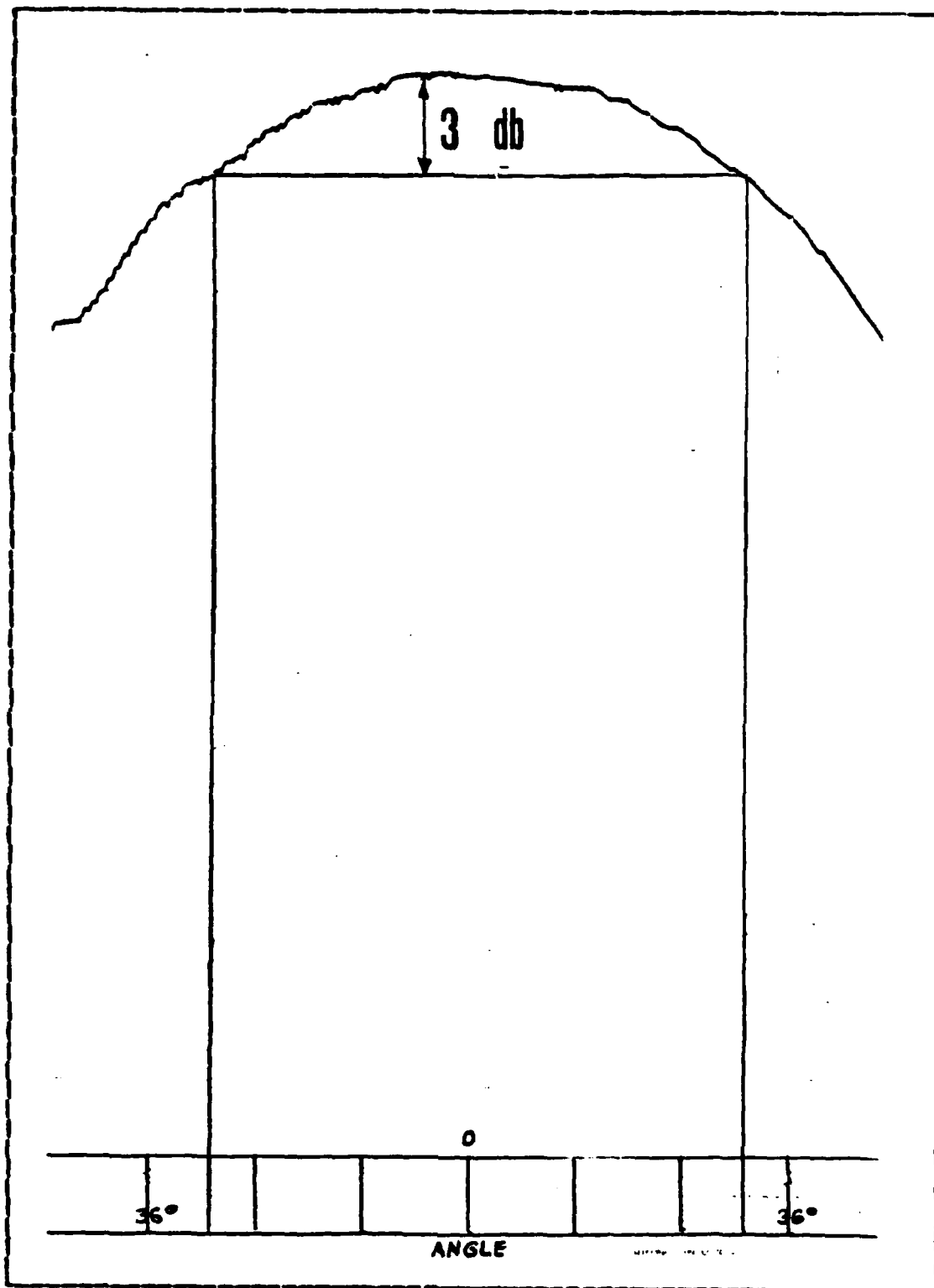


Figure 2.2 Antenna Beam Profile for the Electric Field.

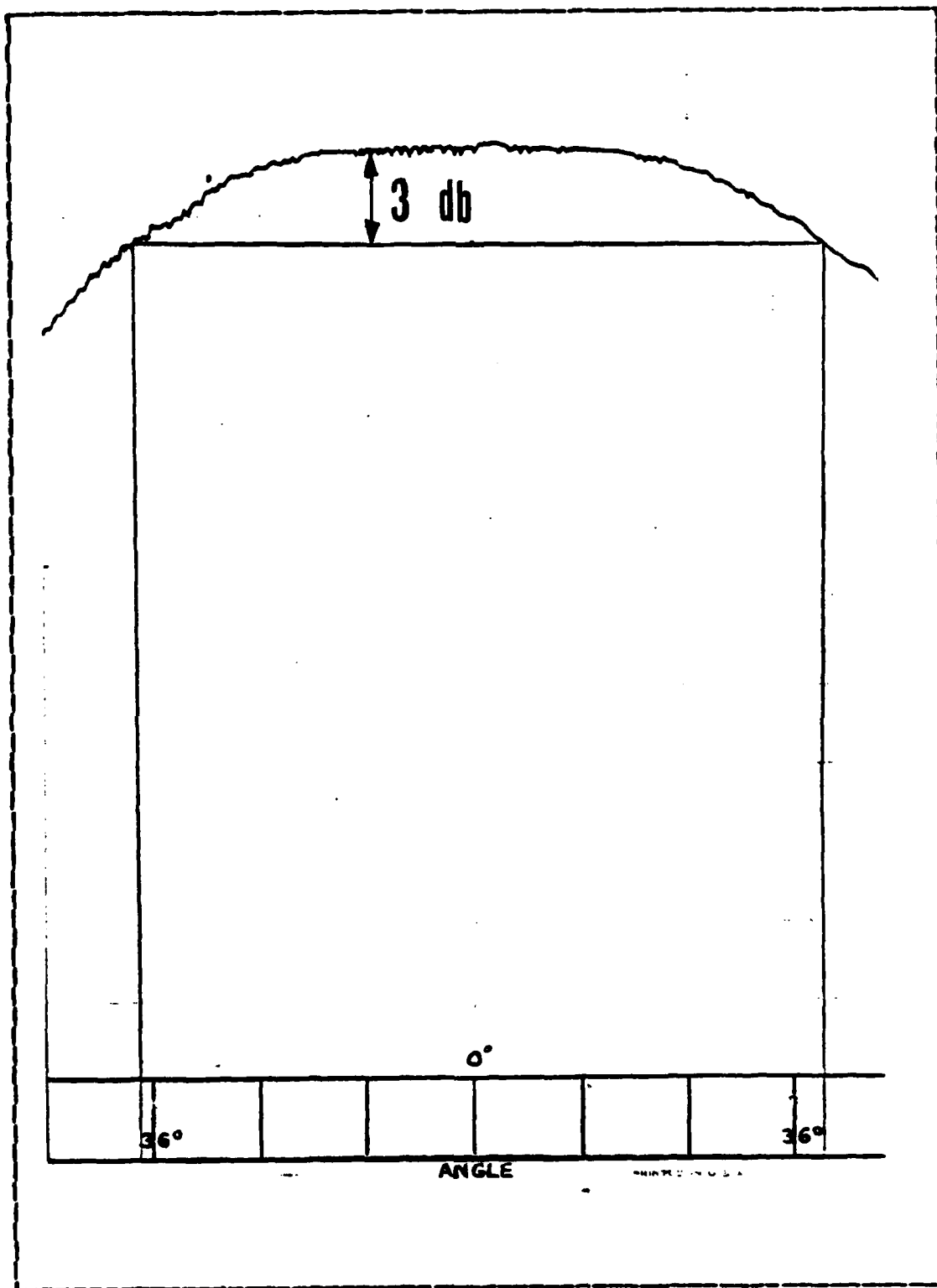


Figure 2.3 Antenna Beam Profile for the Magnetic Field.

## b. Filters

In previous experiments reported in [Ref. 4] a section of X-band waveguide was included between the antenna and the crystal detector. This waveguide serves as a partial filter of the microwave radiation, since it does not pass the fundamental frequency (2.86 GHz) nor the second harmonic (5.71 GHz). Use of the X-band waveguide as a filter was included as one of the variants in this experiment. Additionally, filters were available which were able to select the third and the fourth harmonics of the bunch frequency. These filters were designed and built by K. Alexander and S. Hamel [Ref. 5]. The band-pass characteristics for these filters are shown in figures 2.4 and 2.5.

## c. Detector

The final component in the detection apparatus was the detector itself, an HP X-band X424A crystal detector. The detector was used without the square-law load. Therefore, the response varied linearly with the input (Cerenkov) signal.

## 5. Cable

In the work done by A. Saglam [Ref. 4] the experimental area (end station of the LINAC) was described as very noisy due to the electromagnetic energy radiated by the LINAC klystrons. This problem was effectively solved in this experiment by using doubly-shielded cable to transmit the detected signal to the observer station.

## 6. Observer Station

The analyzing equipment consisted of an ORTEC 450 Research Amplifier, a TEKTRONIX 7904A Oscilloscope, and a TRACER NORTHERN TN-7200 Pulse Height Analyzer (PHA). The



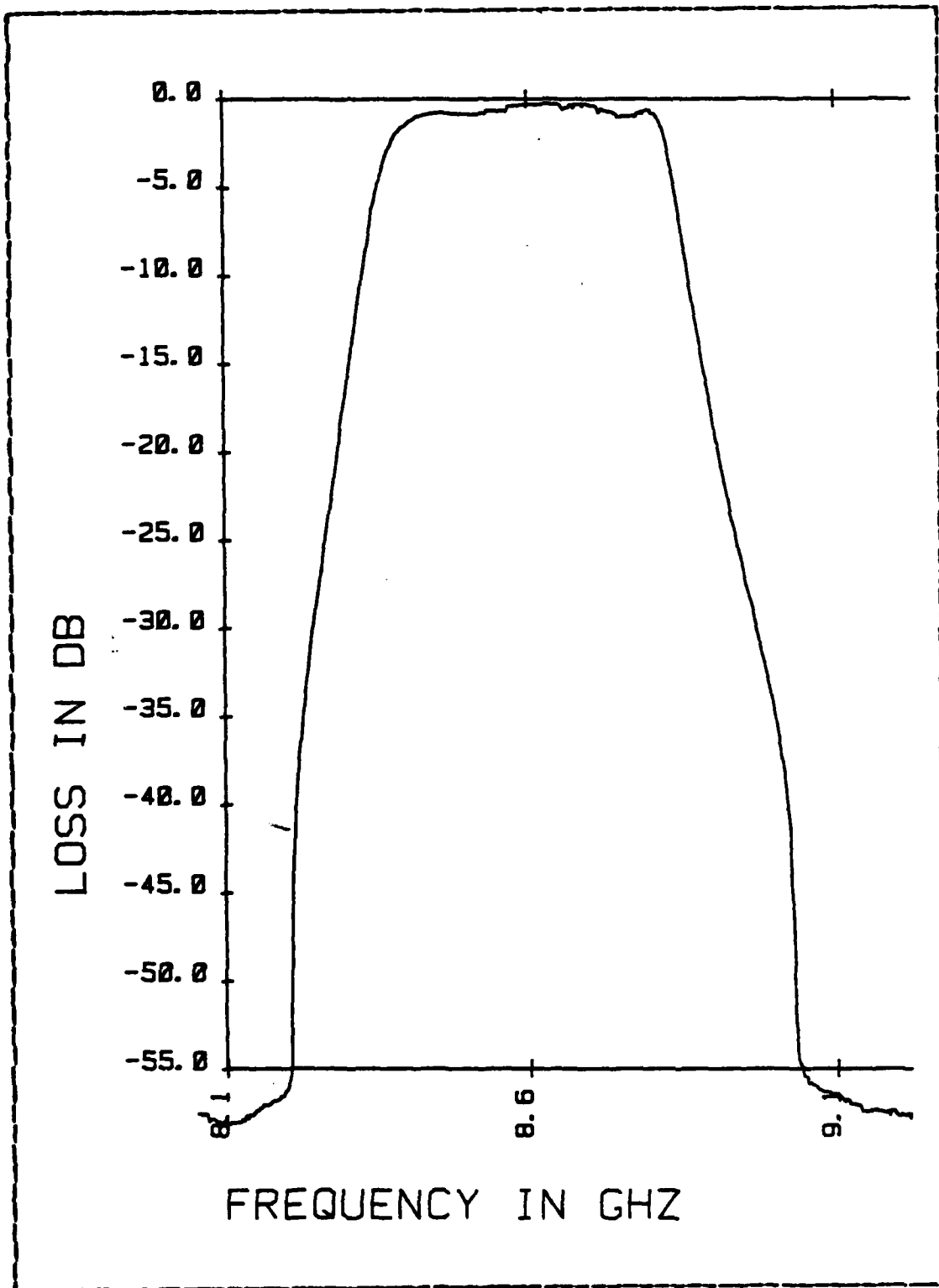


Figure 2.4 Filter Band-pass for the Third Harmonic.

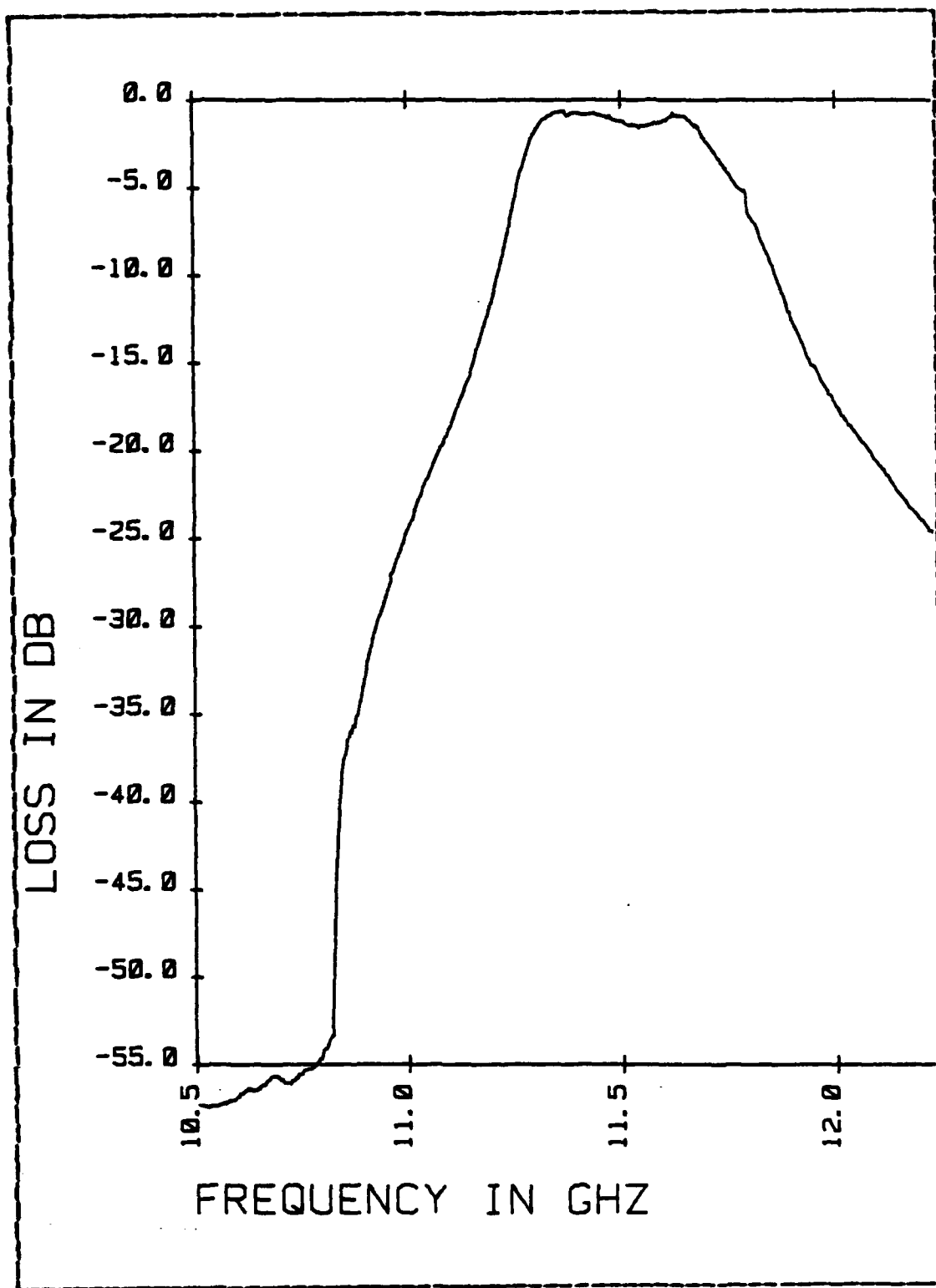


Figure 2.5 Filter Bandpass for the Fourth Harmonic.

critical piece of equipment for experimental purposes was the PHA. This instrument divided the detection range into a predetermined number of channels (e.g. 1024) and then recorded graphically the frequency with which each signal channel was detected. This allowed the observer to deal with a certain degree of variability in the signal, by choosing the observed value to be the peak of the frequency distribution. The frequency distributions observed ranged from very sharp spikes at the lower signal levels to typically broader peaks at higher signal levels. The PHA display also provided an measure of LINAC stability. If the frequency distribution of the detected signal was extremely broad or if multiple peaks were formed while detection angle remained constant, machine instabilities were indicated.

This concludes the discussion of the experimental apparatus. Comparison of experimental results to theoretical curves is presented in the next chapter.

### III. RESULTS

#### A. METHOD OF DATA REDUCTION

As explained in Chapter 2, the raw data from the experiment was in the form of signal (power) versus angle. Since the signal was processed through a series of elements (filter, detector, amplifier, PHA), a measurement of the absolute power was not available. Therefore, it was necessary to normalize these measurements in order to make comparisons with the theoretical curves. The method of normalization chosen was the matching of peaks. For a given experiment, the experimental points were examined to determine which one had the peak value. This value was then adjusted such that it exactly matched (in magnitude) the peak value of the appropriate theoretical curve. All other experimental points for that experiment were then adjusted by the same factor, so that the experimental points maintained the same relative magnitudes.

#### B. DATA

The results presented here are characteristic for the experiments which were performed. Each figure shows the theoretical curve for the harmonics assumed to be present for a given filter, with the experimental points overlaid and normalized to the peak value of the theoretical curve. Tabular data for figures 3.1 through 3.5 are presented in Appendix E. Figure 3.1 and 3.2 compare the theoretical curves for harmonics three and four to the radiation measured with the appropriate filters inserted before the detector. Figure 3.3 compares the theoretical curve for the sum of harmonics three through seven with the radiation

measured with an X-band waveguide inserted before the detector.

These results appear to be good enough to indicate an initial verification of the theory. Results were best for the fourth harmonic (figure 3.2), with very close agreement between theory and experimental points. The experimental results for the third harmonic (figure 3.1) are shifted somewhat to the left of theory, while the results for the sum of harmonics (figure 3.3) are shifted to the right.

One predicted effect which is clearly evident despite the shifting is the relative spread of the Cerenkov angle for different harmonics. The third harmonic is predicted to spread the radiation over a broader range of angles than does the fourth harmonic, and this is verified by the experimental results.

There are several possible explanations for the deviations from theory which are shown here. For example, certain assumptions necessary for theoretical simplicity may not hold in the experimental situation. It may be that the charge distribution of the electron bunches is not Gaussian, or that a lateral parameter should be included in the Gaussian to account for divergence of the beam over the air path. Another factor possibly affecting the results was the mirror tilt, which caused the air path length to be longer than one meter on one side of the beam, and shorter on the other.

Another factor which must affect the results to some degree is simply the experimental geometry. For a number of reasons, theory calls for the field point distances to be much greater than the source point distances. That is, the path length should be small in relation to the distance to the point at which the fields are measured. However, the dimensions of the LINAC end station prohibit this, so that at angles larger than just a few degrees, there is ambiguity

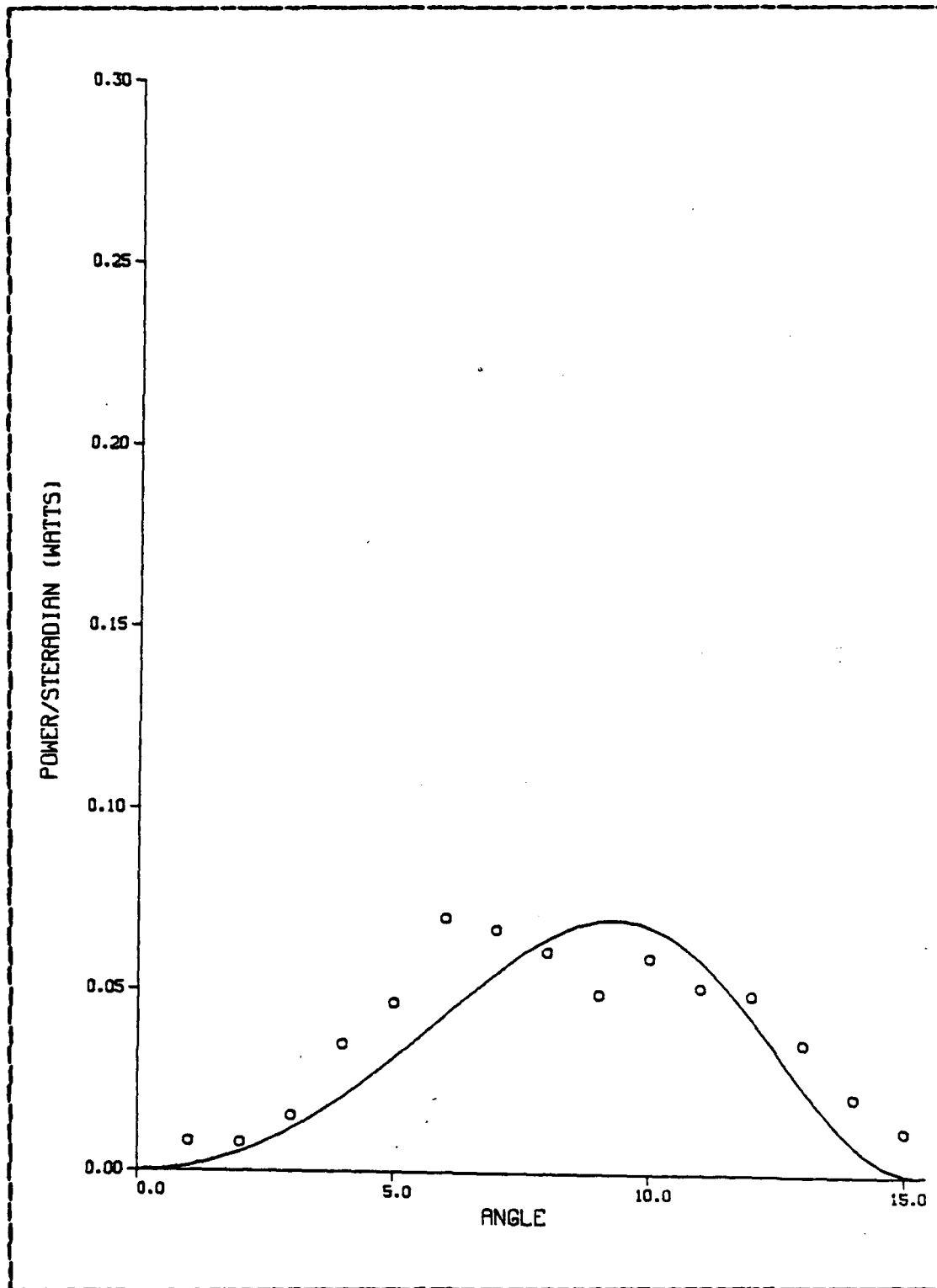


Figure 3.1 Harmonic=3 : L=1.0 m: Filter = 3rd.

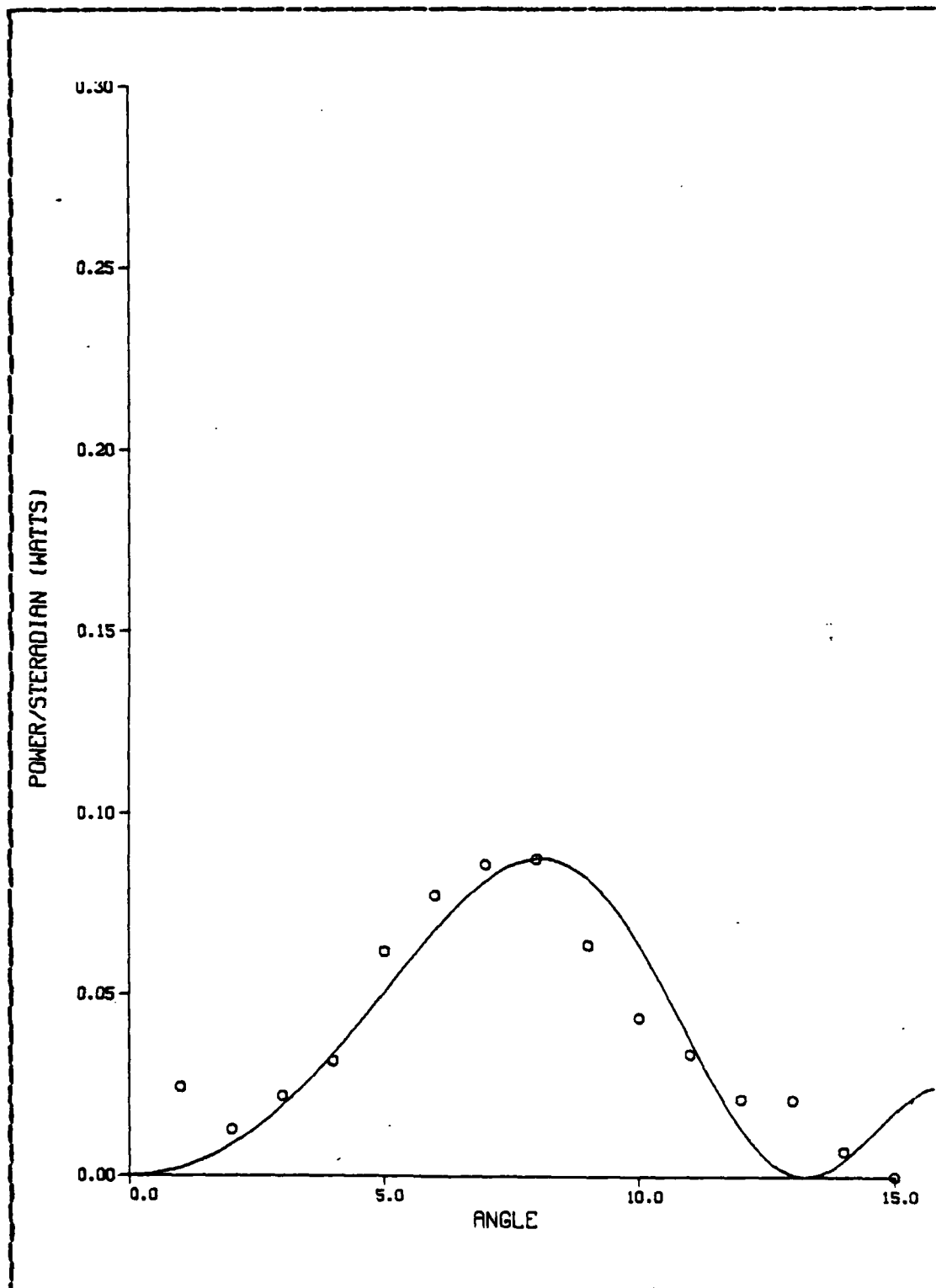


Figure 3.2 Harmonic=4 : L = 1.0 m : Filter=4th.

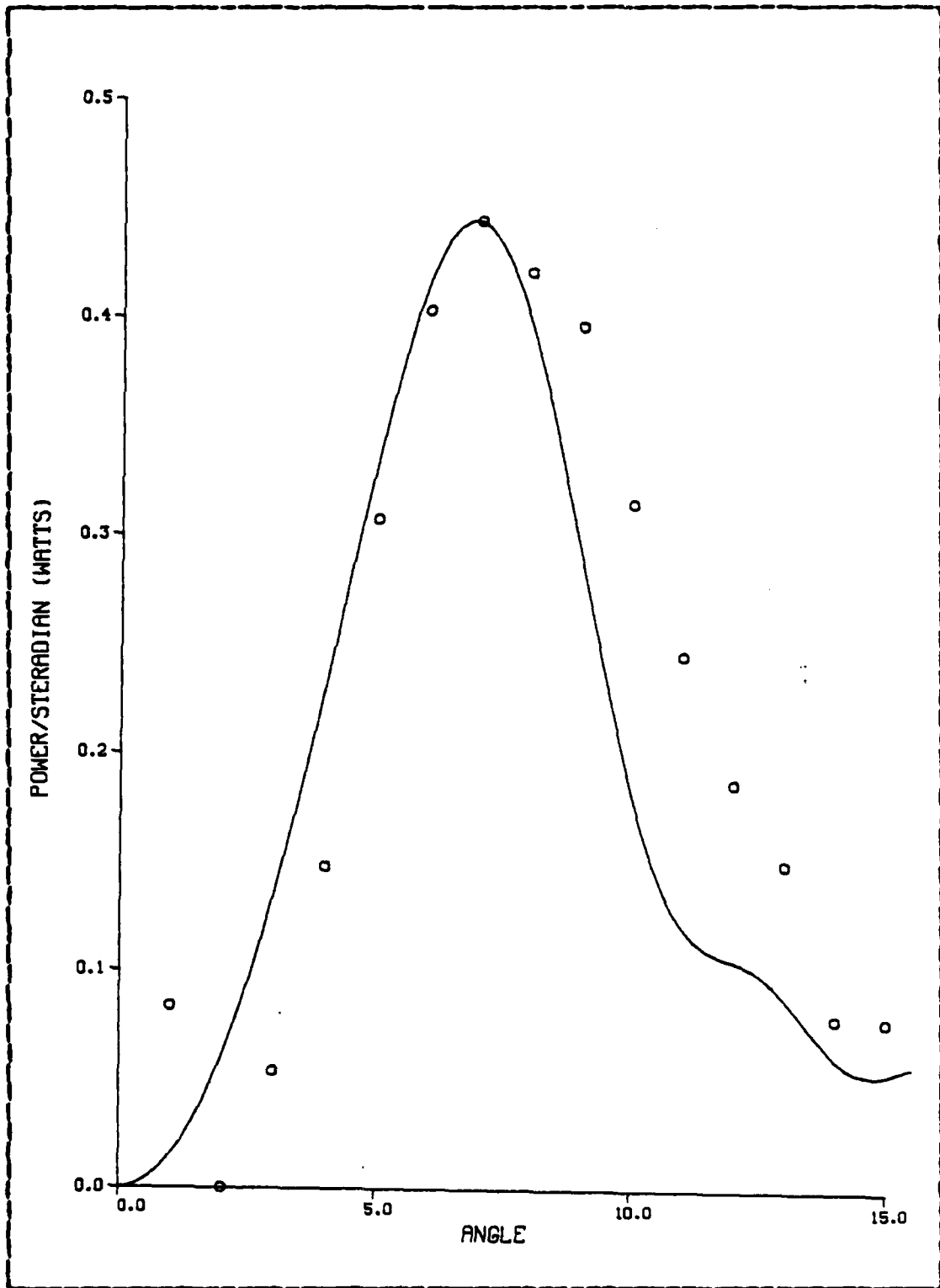


Figure 3.3 Harmonics= 3-7 : L = 1.0 m : Filter = Waveguide.



regarding exactly which angle is being measured. For small observation angles, the air path does look like a point, but as the angles become larger there are increasing differences between the angle as measured from the beginning of the air path and the angle as measured from the end of the air path. At large angles (greater than five degrees) the angle as measured from the center of the air path is substantially smaller than that measured from the end of the path. Since the radiation originating from the end of the path is stronger (it has traveled a smaller distance to the detector), and since this radiation originates at an angle larger than that which is being measured, the radiation at the measured angle is actually overstated. This may be the cause of the shift to higher angles observed in figure 3.3.

Finally, the frequency range over which the filters are valid must be considered. The X-band filters and waveguide used in this experiment are designed for use with radiation in the frequency range 8.2 to 12.4 GHz. Radiation within this band will only propagate in the dominant TE mode in X-band waveguide. Note that this encompasses only the third (8.57 GHz) and the fourth (11.42 GHz) harmonics of the LINAC bunch frequency. When radiation outside this frequency band is fed into the waveguide (as with the fifth and higher harmonics of the bunch frequency which are expected in Cerenkov radiation), modes other than the dominant may be excited in the waveguide. As indicated by [Ref. 6], the effects of coupling multiple modes into and out of a waveguide are complex, and the normal single probe configuration for detecting signal energy in the dominant mode cannot be reliably used in this situation. Since frequencies outside the X-band operating range were expected to be present in this experiment, modes higher than the dominant may have been excited, thereby causing inaccuracies in the measurement of power by the signal detector.

A comparison was made to test for the possibility that frequencies outside the X-band operating range were not being accurately measured by the single probe detector. Figure 3.3 compares the theoretical sum of harmonics 3-7 with the data measurements from the X-band waveguide, using no filter in the waveguide. Adding higher harmonics to the sum, although theoretically correct, would cause a larger discrepancy between theory and experiment, since higher harmonics are shifted towards smaller angles. Assuming the worst case, that harmonics five and above excite modes in the waveguide which are somehow not correctly coupled and detected, implies the possibility that only harmonics three and four are being measured when X-band waveguide is used as a filter. Figure 3.4, showing the data gathered with the waveguide filter normalized against the sum of harmonics three and four, appears to fit the data better, in that the width of the theoretical curve is more closely approximated by the experimental points than in figure 3.3. This lends some credence to the supposition that the detector does not respond well to harmonics higher than the fourth.

A second comparison was made to investigate the possibility that the filters which were used to isolate the third and fourth harmonics were also passing higher resonant frequencies. Such higher frequencies would be close to multiples of the frequency which the filter was designed to pass. For example, figure 3.1 compares the data gathered with the filter for the third harmonic to the theoretical curve for the third harmonic. Figure 3.5 compares the same data to the theoretical sum of the third and sixth harmonics. Note that a somewhat better fit of the data at the smaller angles is obtained in figure 3.5, indicating that the filter may be passing higher resonant frequencies, which in this case are measured by the detector, despite the effects of higher modes which may have been excited.

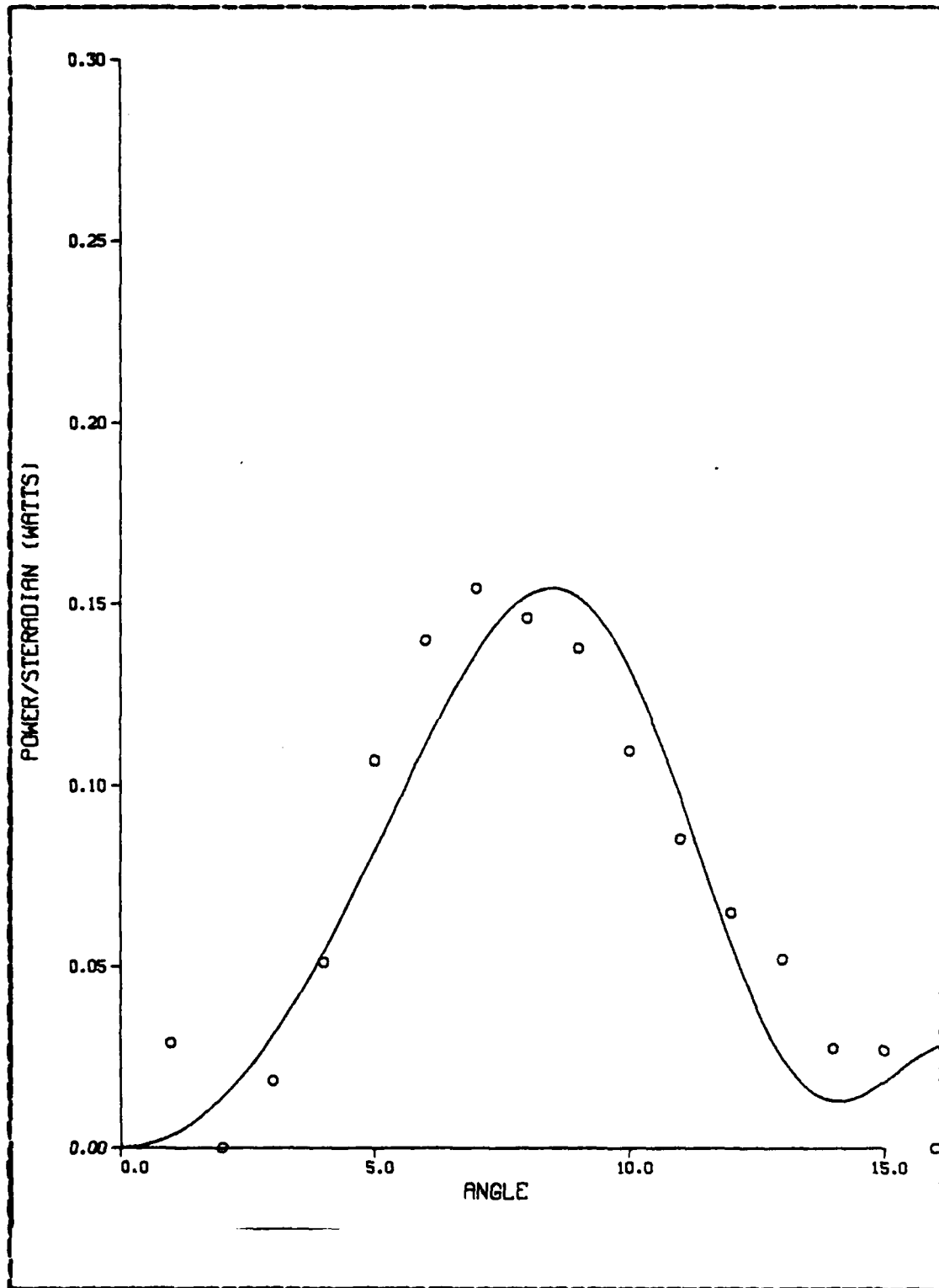


Figure 3.4 Harmonics= 3 + 4 : L=1.0 m : Filter = Waveguide.

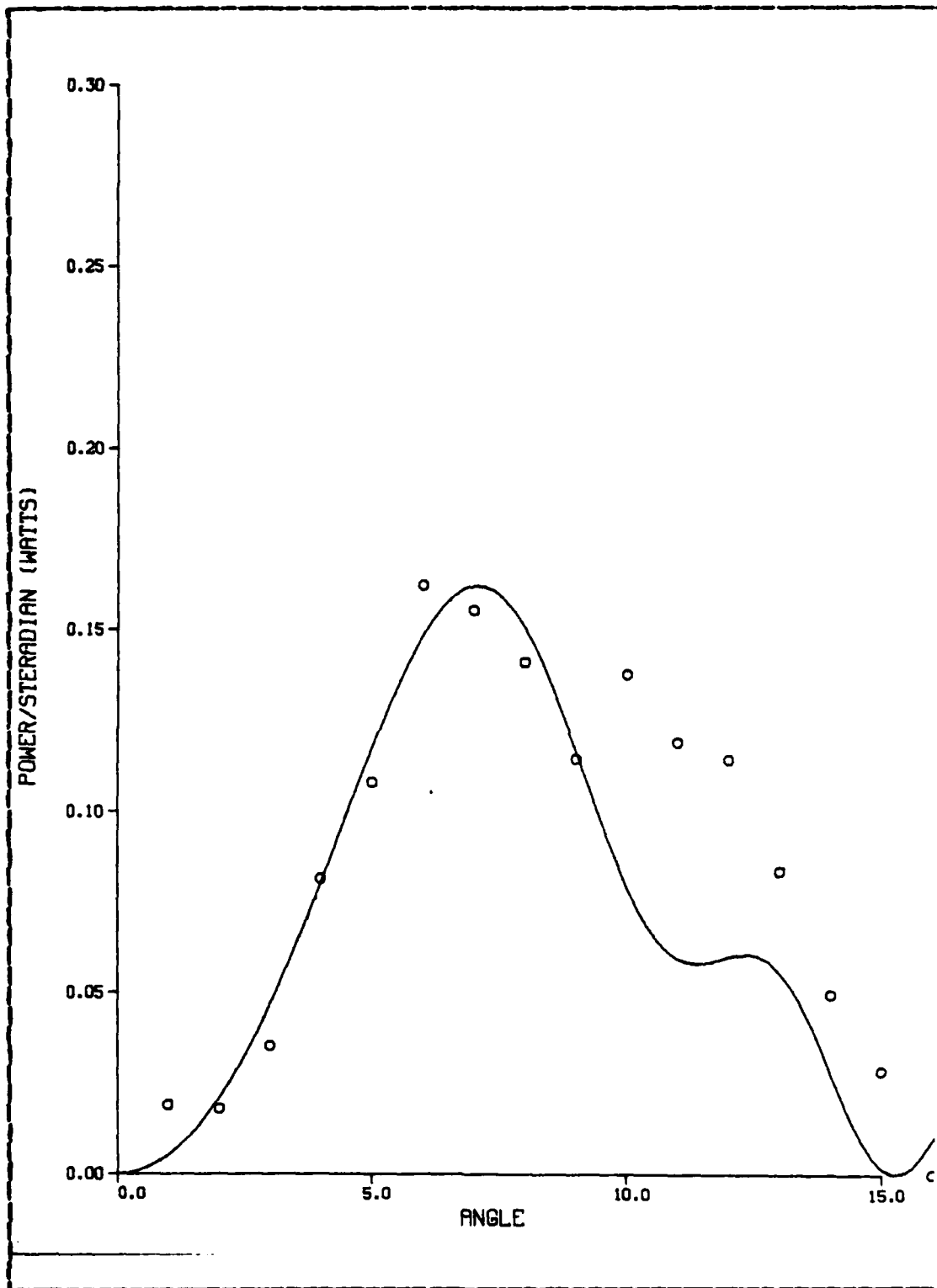


Figure 3.5 Harmonics= 3 + 6 : L=1.0 m : Filter = 3rd.

### C. CONCLUSIONS

The results presented here demonstrate initial confirmation of the theory. Although it is difficult to improve the geometry of the experiment, definite improvements can be made in the measurement of the microwave radiation. Instead of using waveguide filters and a crystal detector (the use of which leads to measurement ambiguities for harmonics greater than the fourth), a tunable YIG filter coupled to a spectrum analyzer of appropriate sensitivity should be used. This will enable the observer to isolate harmonics for measurement without ambiguity, as well as allowing the measurement of absolute (vice relative) power.

## APPENDIX A

### FORTRAN PROGRAM FOR CALCULATING CERENKOV RADIATION CURVES

This is an interactive program which calculates and plots Cerenkov radiation curves for the case of a finite path length. Up to five different harmonics of the electron bunch frequency and five different lengths of emission path may be selected for presentation. The program also allows for adjustment of all basic parameters and constants of the Cerenkov power equation. A different curve will be plotted for each distinct combination of path length and harmonic.

```

C THIS PROGRAM CALCULATES AND PLOTS CERENKOV RADIATION CURVES. UP TO
C FIVE HARMONICS AND FIVE LENGTHS OF EMISSION REGION MAY BE CHOSEN.
C A DIFFERENT CURVE WILL BE PLOTTED FOR EACH DISTINCT COMBINATION OF
C LENGTH AND HARMONIC.
C
C REAL N, MU, KAY, MQ, NUO, IF, B, C, GAMMA, BETA, V, COSTC,
C * U, F, CO, N, MU, NUO, Q, E, MO, B
C DIMENSION W(1000), THETA(1000), HARM(5), CELL(5)
C
C INITIALIZE CONSTANTS
C DATA IC, CO, I, IA, N, I, IMU, MO, I, INUO, NUO, I, IY, Y, I, INO, N, I
C NPCINT = 101
C THETA1 = 20.0
C PI = 3.14159265359
C DGTIRC = 0.0174532525189
C RDTICG = 57.29577551308
C
C *** INITIALIZE PROGRAM CONSTANTS
C CO = 2.99792458E08
C N = 1.000268E00
C MU = 1.256E-06
C NUC = 2.85E09
C Q = 1.94E-12
C E = 1.6E-11
C MO = 5.10953E-31
C B = .0024E00
C
C *** ARE PROGRAM CONSTANTS OK?
C WRITE(6,90C) CO, N, MU, NUO, Q, E, MO, B
C READ(5,501) IANS
C IF (IANS.EQ.INC) GC TO 40
C *** NO PROGRAM CONSTANTS NEED TO BE CHANGED
C WRITE(6,902) IANS
C READ(5,503) IANS
C
C IF (IANS.NE.IC) GO TO 11
C WRITE(6,504) IANS
C READ(5,505) CO
C GC TO 10
C
C IF (IANS.NE.IN) GO TO 12
C WRITE(6,904) IANS
C READ(5,506) N
C GC TO 10
C
C IF (IANS.NE.IMU) GO TO 13
C WRITE(6,904) IANS

```

```

CEROC10
CEROC20
CEROC30
CEROC40
CEROC50
CEROC60
CEROC70
CEROC80
CEROC90
CEROC100
CEROC110
CEROC120
CEROC130
CEROC140
CEROC150
CEROC160
CEROC170
CEROC180
CEROC190
CEROC200
CEROC210
CEROC220
CEROC230
CEROC240
CEROC250
CEROC260
CEROC270
CEROC280
CEROC290
CEROC300
CEROC310
CEROC320
CEROC330
CEROC340
CEROC350
CEROC360
CEROC370
CEROC380
CEROC390
CEROC400
CEROC410
CEROC420
CEROC430
CEROC440
CEROC450
CEROC460
CEROC470
CEROC480

```

C490  
 CEROC500  
 CEROC510  
 CEROC520  
 CEROC530  
 CEROC540  
 CEROC550  
 CEROC560  
 CEROC570  
 CEROC580  
 CEROC590  
 CEROC600  
 CEROC610  
 CEROC620  
 CEROC630  
 CEROC640  
 CEROC650  
 CEROC660  
 CEROC670  
 CEROC680  
 CEROC690  
 CEROC700  
 CEROC710  
 CEROC720  
 CEROC730  
 CEROC740  
 CEROC750  
 CEROC760  
 CEROC770  
 CEROC780  
 CEROC790  
 CEROC800  
 CEROC810  
 CEROC820  
 CEROC830  
 CEROC840  
 CEROC850  
 CEROC860  
 CEROC870  
 CEROC880  
 CEROC890  
 CEROC900  
 CEROC910  
 CEROC920  
 CEROC930  
 CEROC940  
 CEROC950  
 CEROC960

```

C 13      READ (5,*) MU
          GO TC 10
          IF(IANS.NE. INU0) GO TO 14
          WRITE (6,904) IANS
          READ (5,*) NU0
          GO TO 10

C 14      IF(IANS.NE. IQ) GO TO 15
          WRITE (6,904) IANS
          READ (5,*) C
          GO TC 10

C 15      IF(IANS.NE. IE) GO TO 16
          WRITE (6,904) IANS
          READ (5,*) E
          GO TO 10

C 16      IF(IANS.NE. IMO) GO TO 17
          WRITE (6,904) IANS
          READ (5,*) MO
          GO TC 10

C 17      IF(IANS.NE. IB) GO TO 18
          WRITE (6,904) IANS
          READ (5,*) B
          GO TC 10

C 18      ** ERRCR
          WRITE (6,910)
          GO TO 10

C 40      WRITE (6,505)
          READ (5,*) HARM(1), HARM(2), HARM(3), HARM(4), HARM(5)
          WRITE (6,506)
          READ (5,*) CELL(1), CELL(2), CELL(3), CELL(4), CELL(5)

          CALL TEK618
          CALL PTEKAL(72,6)
          CALL VRSTEC(0,0,0)
          CALL CCMPRS

          CALL NCERDR
          CALL PAGE(8.5,11.0)

          C THE LOCATION OF THE ORIGIN:
          CALL PHYSOR(1.0,1.0)
  
```



```

C THE AREA IN INCHES BY INCHES:
C CALL AREA2D(7.0,10.0)
C
C WHAT EVER LABELS DESIRED ON X AND Y AXIS:
C CALL XNAME ('ANGLE $',100)
C CALL YNAME ('PCWHR/STERADIAN (WATTS) $',100)
C CALL YA>ANG(0)
C
C WHAT EVER HEADING DESIRED FOR GRAPH:
C CALL HEADING('THIS IS A HEADING$',100)
C CALL HEADING('HEADING ON NEXT LINE$',100)
C
C RANGE AND INCREMENTS OF X AND RANGE AND INCREMENTS OF Y
C CALL GRAF (0.0, 5.0,15.0, 0.0, .01,0.15)
C
C NEED SPLINE FOR SMOOTH FIT (OTHERWISE GET LINEAR FIT)
C CALL SPLINE
C DO 70 J=1,5
C IF (HARM(J).EQ.0) GC TO 70
C
C 50 DO 70 K=1,5
C IF (CELL(K).EQ.0) GO TO 70
C
C *** BEGIN CALCULATIONS
C CO = N
C GAMMA = E / (MO*CO*CO)
C BETA = (1.0 - 1.0 / (GAMMA*GAMMA)) ** 0.5
C V = BETA * CO
C CCSTC = C / V
C CI = MU*C*NUC*NUO*Q / (8.0*FI*FI)
C KAY = 2.0*PI*HARM(J)*NUO / C
C
C WRITE(50,*) KAY,COSTC,HARM(J), CELL(K)
C
C *** CALCULATE FUNCTIONAL VALUES
C RADCF = THETA*F * DGTORD
C XECINT = FLOAT(NPOINT-1)
C CC 80 I = 1, NPOINT
C RATIO = FLGCAT(I-1) / XPOINT
C ANGLE = RATIO * RADF
C THETA(I) = RATIO * THETAF
C F = 1 / (EXP(0.25 * B*KAY*CO*(ANGLE) * B*KAY*CO*(ANGLE)) * (CCSTC-CCS(ANGLE))) / 2
C IF = (KAY * CELL(K) * (COSTC-CCS(ANGLE))) / U
C W(I) = SIN(CI * (F*KAY*CELL(K)*SIN(ANGLE))*IF) ** 2

```

CERO G570  
CERO C580  
CERO C590  
CERO I1000  
CERO I1010  
CERO I1020  
CERO I1030  
CERO I1040  
CERO I1050  
CERO I1060  
CERO I1070  
CERO I1080  
CERO I1090  
CERO I1100  
CERO I1110  
CERO I1120  
CERO I1130  
CERO I1140  
CERO I1150  
CERO I1160  
CERO I1170  
CERO I1180  
CERO I1190  
CERO I1200  
CERO I1210  
CERO I1220  
CERO I1230  
CERO I1240  
CERO I1250  
CERO I1260  
CERO I1270  
CERO I1280  
CERO I1290  
CERO I1300  
CERO I1310  
CERO I1320  
CERO I1330  
CERO I1340  
CERO I1350  
CERO I1360  
CERO I1370  
CERO I1380  
CERO I1390  
CERO I1400  
CERO I1410  
CERO I1420  
CERO I1430  
CERO I1440

```

C 80      WRITE(50,*) W(I),THETA(I),F,IF
C          CONTINUE
C          CALL CURVE FOR EACH CURVE DESIRED (Q IN LAST PARAMETER
C INDICATES DO NOT DISPLAY DATA POINTS, 1 MEANS DISPLAY
C EVERY DATA POINT)
C          CALL CLFVE (THETA,W,NPOINT,0)
C          CALL CLFVE (X,Y,N,0)
C          CALL CLFVE (X,YY,N*0)
C 75      CONTINUE
C 70      CONTINUE
C          CALL ENDPL(0)
C          ** USER WANT ANOTHER RUN?
C          WRITE(6,508) IANS
C          REAL(5,901) IANS
C          IF (IANS.EQ. IV) GO TO 10
C          CONTINUE
C          STGP
C 90
C 900     FORMAT(/,' PROGRAM CONSTANTS CURRENTLY HAVE VALUES AS FOLLOWS: ',/
C          * 5X,'CC = SPEED OF LIGHT IN VACUUM = 2.99792458E14.7, //
C          * 5X,'N = AIR REFRACTIVE INDEX = 1.0000000000E14.7, //
C          * 5X,'ML = PERMEABILITY CF AIR = 1.25663706E14.7, //
C          * 5X,'NLO = BUNCH FREQUENCY = 1.0000000000E14.7, //
C          * 5X,'C = ELECTRON CHARGE = 1.60217663E14.7, //
C          * 5X,'MC = ELECTRON REST MASS = 9.10938291E14.7, //
C          * 5X,'B = BUNCH SIZE PARAMETER = 1.0000000000E14.7, //
C          * 5X,'YCU = BUNCH TO CHANGE ANY OF THESE VALUES? ( Y OR N )' )
C          DO 1 YCU
C          FORMAT(A1)
C          FORMAT(/7) ENTER CCNSTANT TO BE CHANGED: //
C          FORMAT(A4) ENTER NEW VALUE FOR 'A4: //
C          FORMAT(//) ENTER VALUES FOR HARMONIC OF BUNCH FREQUENCY: //
C          FORMAT(//) ENTER VALUES FOR CELL LENGTH OF EMISSION REGION: //
C          FORMAT(//) ENTER ANOTHER RUN? ( ENTER Y OR N ) //
C          FORMAT(//) WANT ANOTHER RUN? ( ENTER Y OR N ) //
C          FORMAT(//) THE VARIABLE SELECTED IS NOT IN THE LIST - TRY AGAIN //
C          END
CER01450
CER01460
CER01470
CER01480
CER01490
CER01500
CER01510
CER01520
CER01530
CER01540
CER01550
CER01560
CER01570
CER01580
CER01590
CER01600
CER01610
CER01620
CER01630
CER01640
CER01650
CER01660
CER01670
CER01680
CER01690
CER01700
CER01710
CER01720
CER01730
CER01740
CER01750
CER01760
CER01770
CER01780
CER01790
CER01800
CER01810
CER01820
CER01830
CER01840
CER01850
CER01860
CER01870
CER01880
CER01890
CER01900

```

## APPENDIX B

### **FORTRAN PROGRAM - CERENKOV CURVES WITH DATA POINTS**

This is an interactive program which calculates and plots several Cerenkov radiation curves as well as a single set of experimentally observed data points. Up to five different harmonics of the bunch frequency and five different lengths of the emission path may be chosen for presentation. A different curve will be plotted for each distinct combination of path length and harmonic. The program also allows adjustment of all basic parameters and constants of the Cerenkov power equation. The program then prompts for 20 data measurements of power (one per degree) which will be superimposed over the curves.

```

C THIS PROGRAM CALCULATES AND PLOTS CERENKOV RADIATION CURVES FOR
C UP TO FIVE DIFFERENT HARMONICS AND FIVE DIFFERENT LENGTHS OF
C EMISSION REGION. A DIFFERENT CURVE WILL BE CALCULATED FOR EACH
C DISTINCT COMBINATION OF LENGTH AND HARMONIC. THE PROGRAM THEN ASKS
C FOR 20 DATA POINTS (ONE PER DEGREE) TO BE SUPERIMPOSED OVER THE
C CURVES.
C
C REAL N, MU, KAY, MO, NUO, IF, B, C, GAMMA, BETA, V, COSTC,
C * DIMENSION W(1000), THETA(1000), HARM(5), CELL (5), THETA(20),
C *
C INITIALIZE CONSTANTS
C DATA IC/CO, I/IN, IN, I/IMU, MU, I/INUC, NUO, I/IB, Y, I, INO, N,
C *
C NPCINT = 101
C THETA(1) = 3.14159265359
C PI = 3.14159265359
C DGTICRD = 0
C RDTCOG = 57.29577551308
C
C *** INITIALIZE PROGRAM CONSTANTS
C CO = 2.997925E08
C NU = 1.0000268E00
C MU = 1.256E-06
C NUO = 2.85E09
C Q = 1.94E-12
C E = 1.6E-11
C MO = 5.10953E-31
C B = .0024E00
C
C *** ARE PROGRAM CONSTANTS OK?
C WRITE(6,900) CO, N, MU, NUO, Q, E, MO, B
C REAL(5,901) IANS
C IF (IANS.EQ.INC) GC TO 40
C *** NO PROGRAM CONSTANTS NEED TO BE CHANGED
C WRITE(6,902) IANS
C REAL(5,903) IANS
C
C IF (IANS.NE.IC) GO TO 11
C WRITE(6,904) IANS
C READ(5,*) CO
C GC TC 10
C
C 11 IF (IANS.NE.IN) GO TO 12
C WRITE(6,904) IANS
C READ(5,*) N
C GC TC 10
C
C CEROC010
C CEROC020
C CEROC030
C CEROC040
C CEROC050
C CEROC060
C CEROC070
C CEROC080
C CEROC090
C CEROC100
C CEROC110
C CEROC120
C CEROC130
C CEROC140
C CEROC150
C CEROC160
C CEROC170
C CEROC180
C CEROC190
C CEROC200
C CEROC210
C CEROC220
C CEROC230
C CEROC240
C CEROC250
C CEROC260
C CEROC270
C CEROC280
C CEROC290
C CEROC300
C CEROC310
C CEROC320
C CEROC330
C CEROC340
C CEROC350
C CEROC360
C CEROC370
C CEROC380
C CEROC390
C CEROC400
C CEROC410
C CEROC420
C CEROC430
C CEROC440
C CEROC450
C CEROC460
C CEROC470
C CEROC480

```

CEROC490  
 CEROC500  
 CEROC510  
 CEROC520  
 CEROC530  
 CEROC540  
 CEROC550  
 CEROC560  
 CEROC570  
 CEROC580  
 CEROC590  
 CEROC600  
 CEROC610  
 CEROC620  
 CEROC630  
 CEROC640  
 CEROC650  
 CEROC660  
 CEROC670  
 CEROC680  
 CEROC690  
 CEROC700  
 CEROC710  
 CEROC720  
 CEROC730  
 CEROC740  
 CEROC750  
 CEROC760  
 CEROC770  
 CEROC780  
 CEROC790  
 CEROC800  
 CEROC810  
 CEROC820  
 CEROC830  
 CEROC840  
 CEROC850  
 CEROC860  
 CEROC870  
 CEROC880  
 CEROC890  
 CEROC900  
 CEROC910  
 CEROC920  
 CEROC930  
 CEROC940  
 CEROC950  
 CEROC960

```

C 12 IF(IANS.NE.IMU) GO TO 13
      WRITE(6,904) IANS
      READ(5,*) MU
      GC TC 10

C 13 IF(IANS.NE.INUO) GO TO 14
      WRITE(6,904) IANS
      READ(5,*) NUO
      GC TC 10

C 14 IF(IANS.NE.IQ) GO TO 15
      WRITE(6,904) IANS
      READ(5,*) Q
      GC TC 10

C 15 IF(IANS.NE.IE) GO TO 16
      WRITE(6,904) IANS
      READ(5,*) E
      GC TC 10

C 16 IF(IANS.NE.IMO) GO TO 17
      WRITE(6,904) IANS
      READ(5,*) MO
      GC TC 10

C 17 IF(IANS.NE.IB) GO TO 18
      WRITE(6,904) IANS
      READ(5,*) B
      GC TC 10

C 18 *** ERROR
      WRITE(6,910)
      GC TO 10

C 40 WRITE(6,905)
      READ(5,*) HARM(1), HARM(2), HARM(3), HARM(4), HARM(5)
      WRITE(6,906)
      READ(5,*) CELL(1), CELL(2), CELL(3), CELL(4), CELL(5)

C      WRITE(6,907)
      DO 41 I = 1,20
      READ(5,*) POWER(I)
      CONTINUE

C 41 DO 42 I = 1,20
      IFETAP(I) = I
      CONTINUE

C 42 CONTINUE
  
```

CER0C570  
 CER0C580  
 CER0C590  
 CER01C00  
 CER01C10  
 CER01C20  
 CER01C30  
 CER01C40  
 CER01C50  
 CER01C60  
 CER01C70  
 CER01C80  
 CER01C90  
 CER01100  
 CER01110  
 CER01120  
 CER01130  
 CER01140  
 CER01150  
 CER01160  
 CER01170  
 CER01180  
 CER01190  
 CER01200  
 CER01210  
 CER01220  
 CER01230  
 CER01240  
 CER01250  
 CER01260  
 CER01270  
 CER01280  
 CER01290  
 CER01300  
 CER01310  
 CER01320  
 CER01330  
 CER01340  
 CER01350  
 CER01360  
 CER01370  
 CER01380  
 CER01390  
 CER01400  
 CER01410  
 CER01420  
 CER01430  
 CER01440

```

CALL TEK618
CALL PR1PLT(72,6)
CALL VRSTEC(0,0.0)
CALL CCAPRS

CALL NCEBRD
CALL PAGE(8.5,11.0)

THE LOCATION OF THE ORIGIN:
CALL PHYSOR(1.0,1.0)

THE AREA IN INCHES BY INCHES:
CALL AREA2D(7.0,10.0)

WHATEVER LABELS DESIRED ON X AND Y AXIS:
CALL XNAME('ANGLE $',100)
CALL YXANG(0)
CALL YNAME('POWER/STERADIAN (WATTS) $',100)

WHATEVER HEADING DESIRED FOR GRAPH:
CALL HEADIN('THIS IS A HEADING$',100,1.2,2)
CALL HEADIN('HEADING ON NEXT LINES$',100,1.2,2)

RANGE AND INCREMENTS OF X AND RANGE AND INCREMENTS OF Y
CALL GRAF(0.0,5.0,15.0,0.0,0.0,0.01,0.15)

NEED SPLINE FOR SMOOTH FIT (OTHERWISE GET LINEAR FIT)
CALL SPLINE
DO 70 J = 1,5
IF (HARM(J).EQ.0) GC TO 70

45 DO 75 K = 1,5
IF (CELL(K).EQ.0) GO TO 70

50 DO 75 K = 1,5
IF (CELL(K).EQ.0) GO TO 70

C *** BEGIN CALCULATIONS
C = CO / N
GAMMA = E / (MO*CO*CO)
BETA = (1.0 - 1.0 / (GAMMA*GAMMA)) ** 0.5
V = BETA * CO
CCSTC = C / V
C1 = MU*C*NUC*NUO*Q / (8.0*PI*PI)
KAY = 2.0*PI*HARM(J)*NUO / C

C WRITE(50,*) KAY,COSTC,HARM(J), CELL(K)

```

```

C C      *** CALCULATE FUNCTIONAL VALUES
      RACF = THETA*F * DGTORD
      XFOINT = FLOAT(NTPCINT-1)
      DC 80 I=1,NPCINT
      ANGLE = FLCAI(I-1) / XPCINT
      THETA(I) = RATIO * RADE
      F = 1/(EXP(0.25 * B*KAY*COS(ANGLE) * B*KAY*COS(ANGLE) )/2
      U = (KAY * CELL(K) * (COSTC-COS(ANGLE)))
      W(I) = SIN(U) / U
      W(I) = (F*KAY*CELL(K))*SIN(ANGLE)*IF)**2
      WRITE(50,*) W(I),THETA(I),F,IF
      CONTINUE
C 80
C      CALL CURVE FOR EACH CURVE DESIRED (0 IN LAST PARAMETER
C      INDICATES CG NOT DISPLAY DATA POINTS, 1 MEANS DISPLAY
C      EVERY DATA POINT)
      CALL CURVE (THETA, W,NPOINT,0)
      CALL CLFVE (X,Y,N,0)
      CALL CLFVE (X,Y,N,0)
C 75
C      CONTINUE
C 70
C      CALL CURVE (THETA,POWER,20,-1)
C      CALL ENCLP(C)
C
C      ** USER WANT ANOTHER RUN?
      WRITE(6,508)
      REAC(5,901) IANS
      IF(IANS.EQ.1) GC TC 10
      CALL DCNEPL
      CONTINUE
      STCP
C 90
C 900
      FORMAT(/,' PROGRAM CONSTANTS CURRENTLY HAVE VALUES AS FOLLOWS: ',/
      ' 5X, CC = SPEED OF LIGHT IN VACUUM =',E14.7,/,
      ' 5X, AN = AIR REFRACTIVE INDEX =',E14.7,/,
      ' 5X, MLO = PERMEABILITY OF AIR =',E14.7,/,
      ' 5X, MLC = BUNCH FREQUENCY =',E14.7,/,
      ' 5X, MLC = ELECTRON CHARGE =',E14.7,/,
      ' 5X, MLC = ELECTRON ENERGY =',E14.7,/,
      ' 5X, MLC = ELECTRON REST MASS =',E14.7,/)

```

```

CER01450
CER01460
CER01470
CER01480
CER01490
CER01500
CER01510
CER01520
CER01530
CER01540
CER01550
CER01560
CER01570
CER01580
CER01590
CER01600
CER01610
CER01620
CER01630
CER01640
CER01650
CER01660
CER01670
CER01680
CER01690
CER01700
CER01710
CER01720
CER01730
CER01740
CER01750
CER01760
CER01770
CER01780
CER01790
CER01800
CER01810
CER01820
CER01830
CER01840
CER01850
CER01860
CER01870
CER01880
CER01890
CER01900
CER01910
CER01920

```

CER01530  
 CER01540  
 CER01550  
 CER01560  
 CER01570  
 CER01580  
 CER01590  
 CER02000  
 CER02010  
 CER02020  
 CER02030  
 CER02040

```

* I DO YOU WANT TO CHANGE ANY OF THESE VALUES? ( Y OR N )
* BUNCH SIZE PARAMETER = E14.7 //
FORMAT(A1) : ENTER CCNSTANT TO BE CHANGED:)
FORMAT(A4) : ENTER NEW VALUE FOR 'A4' : )
FORMAT(A4) : ENTER VALUES FOR HARM (HARMONIC OF BUNCH FREQUENCY): )
FORMAT(A4) : ENTER VALUES FOR CELL LENGTH (EMISSION REGION): )
FORMAT(A4) : ENTER EXPERIMENTAL VALUES FOR POWER: )
FORMAT(A4) : WANT ANOTHER RUN? ( ENTER Y OR N ) : )
FORMAT(A4) : THE VARIABLE SELECTED IS NCT IN THE LIST - TRY AGAIN: )
ENC

```

901  
 902  
 903  
 904  
 905  
 906  
 907  
 908  
 910



## APPENDIX C

### FORTRAN PROGRAM - SUM OF CERENKOV CURVES WITH DATA POINTS

This is an interactive program which calculates and plots a single Cerenkov radiation curve and superimposes a single set of data points over the curve. The single Cerenkov curve will represent a sum of curves. The sum will be composed of each distinct combination of harmonic and path length chosen. Up to five different lengths of emission path and five different harmonics of the bunch frequency may be chosen. The program also allows adjustment of all basic parameters and constants of the Cerenkov power equation. The program will prompt for 20 data measurements of power (one for each degree of angle).

```

C C C C C C
THIS PROGRAM CALCULATES AND PLOTS A SUM OF CERENKOV RADIATION
CURVES. UP TO FIVE HARMONICS AND FIVE LENGTHS OF EMISSION REGION
MAY BE CHOSEN; THE PROGRAM WILL INCLUDE A DIFFERENT CURVE IN THE SUM
FOR EACH LIST INCT COMBINATION OF LENGTH AND HARMONIC. THE PROGRAM
THEN ASKS FOR 20 DATA POINTS (ONE PER DEGREE) TO BE SUPERIMPOSED
OVER THE CURVE.
REAL N, MU, KAY, MO, NUO, IF, B, C, GAMMA, BETA, V, COSTC,
* CI, U, F, CO, N, MU, NUO, Q, E, MO, E
* DIMENSION W(1000), THETA(1000), HARM(5), CELL(5), THE TAP(20),
* SUM(1000)
C C
INITIALIZE CONSTANTS
DATA IC/CO, IE/IE, IN/IN, IMU/MO, INUQ/NUO, IB/IE, IY/Y, INO/N, /
* NP/INT = 101.0
* THE TAP = 20.55265359
* PI TCRD = 3.14159265359
* DGT CRD = 0.0174532525199
* RDT CDG = 57.29577551308
C C
*** INITIALIZE PROGRAM CONSTANTS
CO = 2.997925E08
N = 1.000268E00
MU = 1.254E-06
NUC = 2.85E09
Q = 1.94E-12
E = 1.6E-11
MO = 5.10553E-31
B = .0024E00
C C 10
*** ARE PROGRAM CONSTANTS OK?
WRITE(6,900) CO, N, MU, NUO, Q, E, MO, B
READ(5,901) IANS
IF (IANS.EQ. INCT) GC TO 40
C C
*** NO PROGRAM CONSTANTS NEED TO BE CHANGED
WRITE(6,902)
REAL(5,503) IANS
C C
IF (IANS.NE. ICO) GO TO 11
WRITE(6,504) IANS
READ(5,*) CO
GC TC 10
C C 11
IF (IANS.NE. IN) GO TO 12
WRITE(6,904) IANS
READ(5,*) N
GC TC 10
SUM00010
SUM00020
SUM00030
SUM00040
SUM00050
SUM00060
SUM00070
SUM00080
SUM00090
SUM00100
SUM00110
SUM00120
SUM00130
SUM00140
SUM00150
SUM00160
SUM00170
SUM00180
SUM00190
SUM00200
SUM00210
SUM00220
SUM00230
SUM00240
SUM00250
SUM00260
SUM00270
SUM00280
SUM00290
SUM00300
SUM00310
SUM00320
SUM00330
SUM00340
SUM00350
SUM00360
SUM00370
SUM00380
SUM00390
SUM00400
SUM00410
SUM00420
SUM00430
SUM00440
SUM00450
SUM00460
SUM00470
SUM00480

```

SUM0C490  
 SUM0C500  
 SUM0C510  
 SUM0C520  
 SUM0C530  
 SUM0C540  
 SUM0C550  
 SUM0C560  
 SUM0C570  
 SUM0C580  
 SUM0C590  
 SUM0C600  
 SUM0C610  
 SUM0C620  
 SUM0C630  
 SUM0C640  
 SUM0C650  
 SUM0C660  
 SUM0C670  
 SUM0C680  
 SUM0C690  
 SUM0C700  
 SUM0C710  
 SUM0C720  
 SUM0C730  
 SUM0C740  
 SUM0C750  
 SUM0C760  
 SUM0C770  
 SUM0C780  
 SUM0C790  
 SUM0C800  
 SUM0C810  
 SUM0C820  
 SUM0C830  
 SUM0C840  
 SUM0C850  
 SUM0C860  
 SUM0C870  
 SUM0C880  
 SUM0C890  
 SUM0C900  
 SUM0C910  
 SUM0C920  
 SUM0C930  
 SUM0C940  
 SUM0C950  
 SUM0C960

```

C 12 IF(IANS,NE,IMU) GO TO 13
      WRITE(6,904) IANS
      READ(5,*) MU
      GC TC 10

C 13 IF(IANS,NE,INUC) GO TO 14
      WRITE(6,904) IANS
      READ(5,*) NUO
      GO TC 10

C 14 IF(IANS,NE,IQ) GO TC 15
      WRITE(6,904) IANS
      READ(5,*) C
      GO TC 10

C 15 IF(IANS,NE,IE) GO TO 16
      WRITE(6,904) IANS
      REAC(5,*) E
      GO TO 10

C 16 IF(IANS,NE,IMO) GO TO 17
      WRITE(6,904) IANS
      READ(5,*) MO
      GC TC 10

C 17 IF(IANS,NE,IB) GO TO 18
      WRITE(6,904) IANS
      READ(5,*) B
      GC TC 10

C 18 *** ERROR
      WRITE(6,910)
      GO TO 10

C 40 WRITE(6,905)
      READ(5,*) HARM(1), HARM(2), HARM(3), HARM(4), HARM(5)
      WRITE(6,906)
      READ(5,*) CELL(1), CELL(2), CELL(3), CELL(4), CELL(5)

C
      WRITE(6,907)
      DO 41 I = 1,20
      CONTINUE
      READ(5,*) POWER(I)

C 41 CONTINUE

C 42 DO 42 I = 1,20
      IFETAP(I) = 1
      CONTINUE
  
```

SUM0C570  
 SUM00580  
 SUM00990  
 SUM01000  
 SUM01010  
 SUM01020  
 SUM01030  
 SUM01040  
 SUM01050  
 SUM01060  
 SUM01070  
 SUM01080  
 SUM01090  
 SUM01100  
 SUM01110  
 SUM01120  
 SUM01130  
 SUM01140  
 SUM01150  
 SUM01160  
 SUM01170  
 SUM01180  
 SUM01190  
 SUM01200  
 SUM01210  
 SUM01220  
 SUM01230  
 SUM01240  
 SUM01250  
 SUM01260  
 SUM01270  
 SUM01280  
 SUM01290  
 SUM01300  
 SUM01310  
 SUM01320  
 SUM01330  
 SUM01340  
 SUM01350  
 SUM01360  
 SUM01370  
 SUM01380  
 SUM01390  
 SUM01400  
 SUM01410  
 SUM01420  
 SUM01430  
 SUM01440

```

C CC CALL TEK618
C CC CALL PRIPLOT (72,61)
C CC CALL VRSTEC(0,0,0)
C CC CALL CCMPRS
C CC CALL NCBDRR
C CC CALL PAGE(8.5,11.0)

C CC THE LOCATION OF THE ORIGIN:
C CC CALL PHYSOR(1.0,1.0)

C CC THE AREA IN INCHES BY INCHES:
C CC CALL AREA2D(7.0,10.0)

C CC WHATEVER LABELS DESIRED ON X AND Y AXIS:
C CC CALL XNAME ('ANGLE $,100)
C CC CALL YNAME ('POWER/STERADIAN ( WATTS) $',100)
C CC CALL YAXANG (0)

C CC WHATEVER HEADING DESIRED FOR GRAPH:
C CC CALL HEADIN('THIS IS A HEADING$,100,1.2,2)
C CC CALL HEADIN('HEADING ON NEXT LINE$',100,1.2,2)

C CC RANGE AND INCREMENTS CF X AND RANGE AND INCREMENTS OF Y
C CC CALL GRAF (0.0, 5.0,15.0, 0.0,0.05,0.30)

C CC NEED SPLINE FOR SMOOTH FIT (OTHERWISE GET LINEAR FIT)
C CC CALL SPLINE

C 69 DO 69 I = 1,NPOINT
C 69 SUM(I) = 0
C 69 CONTINUE

C 45 DO 70 J = 1,5
C 45 IF (FARM(J),EQ.0) GO TO 70

C 50 DO 75 K = 1,5
C 50 IF (CELL(K),EQ.0) GO TO 70

C CC *** BEGIN CALCULATIONS
C CC C = CO / N
C CC GAMMA = E / (MO*CO*CO)
C CC BETA = (1.0 - 1.0 / (GAMMA*GAMMA)) ** 0.5
C CC V = BETA * CO
C CC CCSTC = C / V

```

SUM01450  
 SUM01460  
 SUM01470  
 SUM01480  
 SUM01490  
 SUM01500  
 SUM01510  
 SUM01520  
 SUM01530  
 SUM01540  
 SUM01550  
 SUM01560  
 SUM01570  
 SUM01580  
 SUM01590  
 SUM01600  
 SUM01610  
 SUM01620  
 SUM01630  
 SUM01640  
 SUM01650  
 SUM01660  
 SUM01670  
 SUM01680  
 SUM01690  
 SUM01700  
 SUM01710  
 SUM01720  
 SUM01730  
 SUM01740  
 SUM01750  
 SUM01760  
 SUM01770  
 SUM01780  
 SUM01790  
 SUM01800  
 SUM01810  
 SUM01820  
 SUM01830  
 SUM01840  
 SUM01850  
 SUM01860  
 SUM01870  
 SUM01880  
 SUM01890  
 SUM01900  
 SUM01910  
 SUM01920

```

C      C1 = MU*C*NUO*NUO*Q*C / (8.0*PI*PI)
C      KAY = 2.0*PI*HARM(J)*NUO / C
C      WRITE(50,*) KAY,COSTC,HARM(J), CELL(K)

*** CALCULATE FUNCTIONAL VALUES
RADF = THETA*F*DGTRD
XFCINT = FLOAT(NPOINT-1)
CC 80 I=1,NPCINT
  RATIO = FLCAT(I-1) / XPOINT
  ANGLE = RATIO*PI / RADF
  THETA(I) = RATIO*THETA
  F = 1/(EXP(0.25*B*KAY*PI*PI*CELL(K)*COS(COS(C-ANGLE))) / 2
  IF = SIN(U) / L
  W(I) = C1 * (F*KAY*CELL(K)*SIN(ANGLE)*IF)**2
  SUM(I) = W(I) + SUM(I)
  WRITE(50,*) SUM(I),THETA(I)

C      WRITE(50,*) W(I),THETA(I),F,IF
C      CONTINUE
C      CALL CURVE FOR EACH CURVE DESIRED (O IN LAST PARAMETER
C      INDICATES CC NOT DISPLAY DATA POINTS, I MEANS DISPLAY
C      EVERY DATA POINT)
C      CALL CURVE (THETA,W,NPOINT,0)
C      CALL CURVE (X,Y,N,0)
C      CALL CURVE (X,YY,N,0)
C 75   CONTINUE
C 70   CONTINUE
C      CALL CURVE (THETA,SUM,NPOINT,0)
C      CALL CURVE (THETA,POWER,20,-1)
C      CALL ENCL(0)
C      ** USER WANT ANOTHER RUN?
C      WRITE(6,508)
C      READ(5,901) IANS
C      IF (IANS.EQ.1) GO TO 10
C      CONTINUE
C      STCP
C 90
C 900 FORMAT(/, ' PROGRAM CONSTANTS CURRENTLY HAVE VALUES AS FOLLOWS: ', /

```



**APPENDIX D**  
**EXPERIMENTAL APPARATUS**

This appendix contains photographs of the experimental apparatus used in this experiment. Figure D.1 shows the end station of the LINAC. At the right is the LINAC beam aperture, with the reflecting aluminum mirror at the left. The detector assembly, mounted at the end of the pivot arm, is shown in the foreground of the photograph. Also shown, located along the beam path between the aperture and the mirror, is a small portable laser used to align the mirror.

Figure D.2 shows the waveguide filter with the fin-line insert for one of the harmonics, along with the detector and horn. Figure D.3 shows the detector apparatus assembled.



Figure D.1 LINAC End-Station.



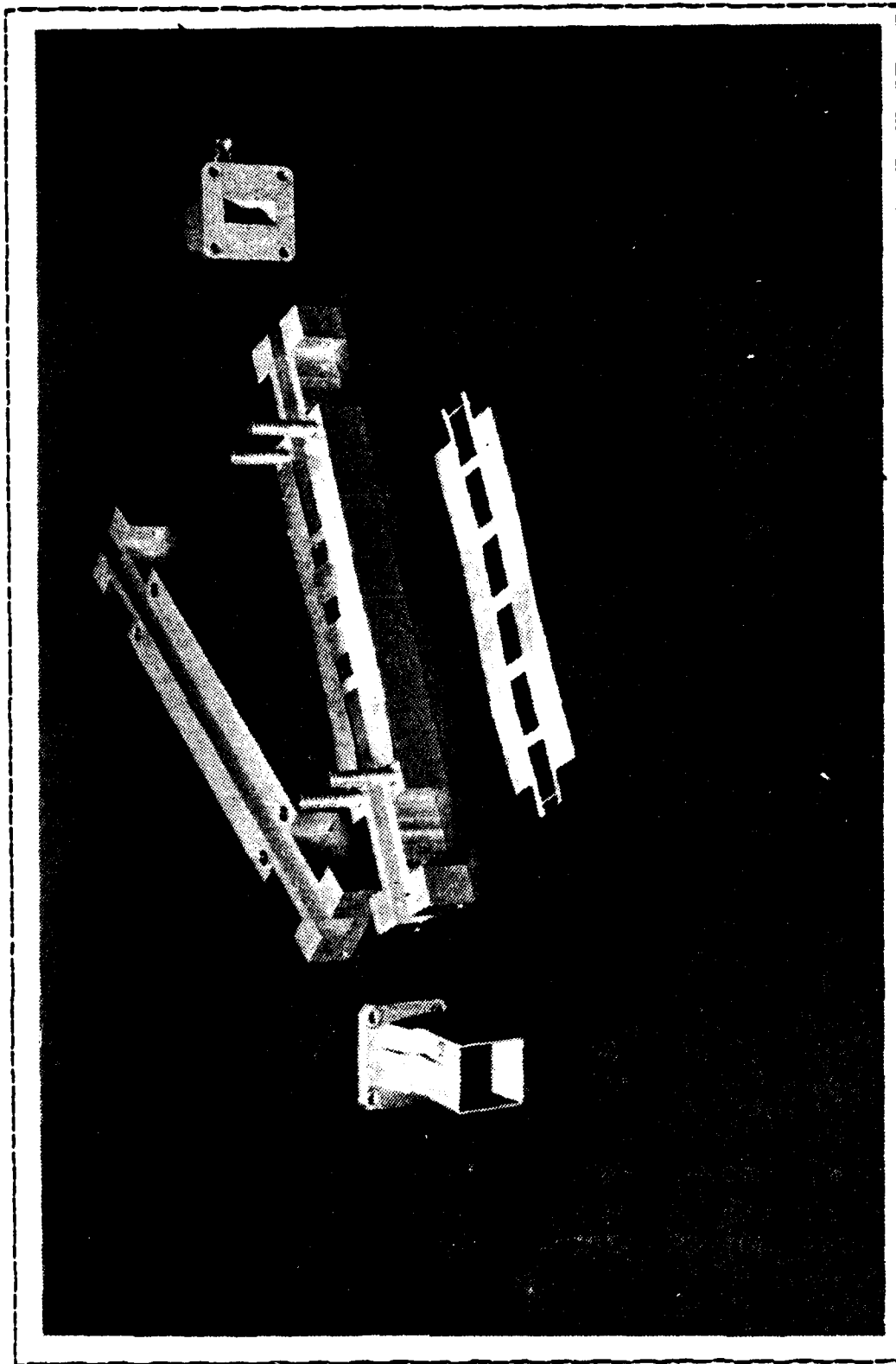


Figure D.2 Detection Apparatus Components.

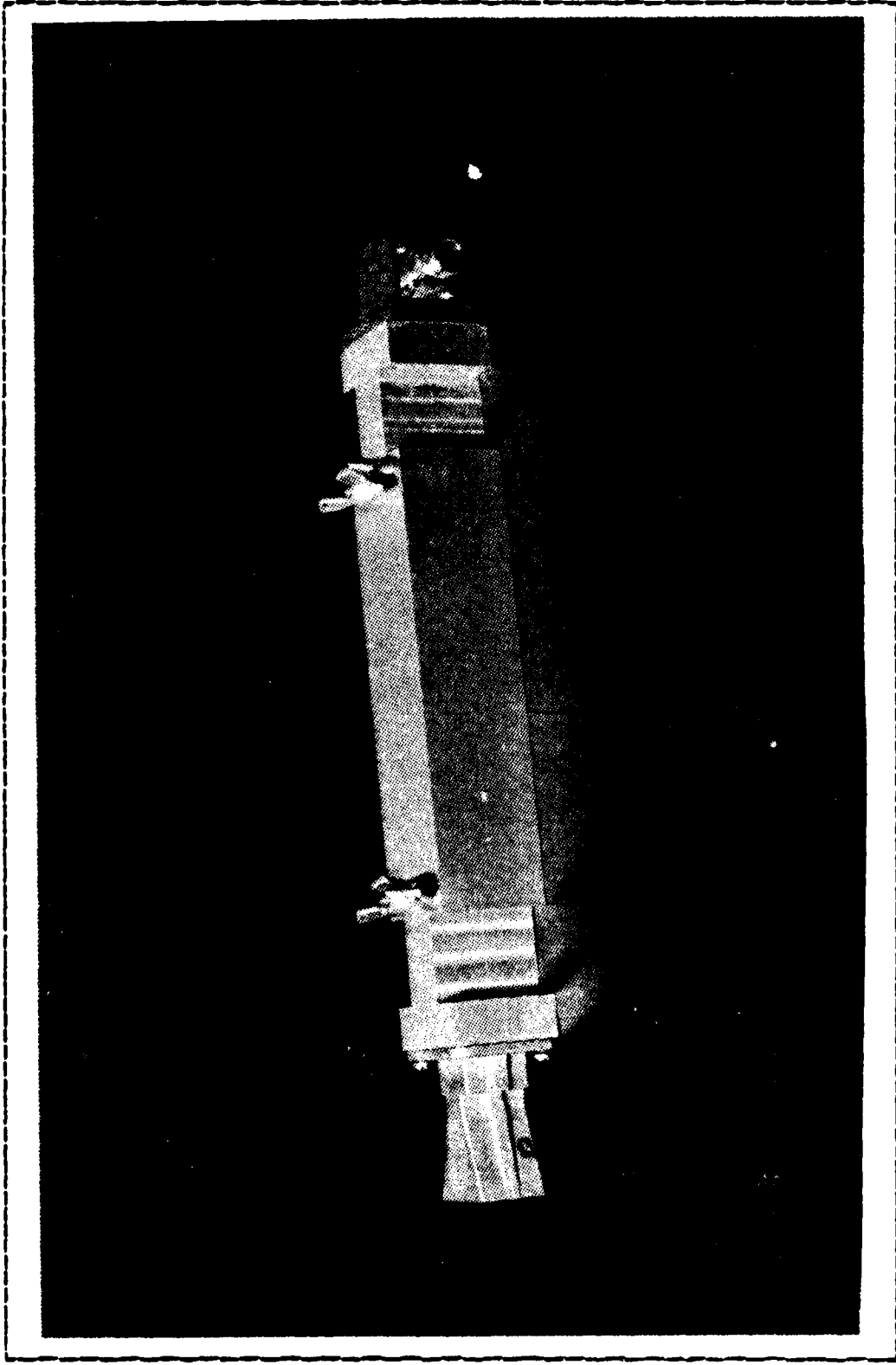


Figure D.3 Assembled Detection Apparatus.

APPENDIX B  
TABULAR DATA FOR FIGURES

TABLE III  
Tabular Data for Figure 3.1

Degree	Channel	Normalized Value
1	101	.0082
2	96	.0078
3	188	.0153
4	434	.0352
5	575	.0467
6	864	.0701
7	828	.0672
8	752	.0610
9	610	.0495
10	734	.0596
11	635	.0515
12	609	.0494
13	446	.0362
14	265	.0215
15	152	.0123

-Channel values were read from the Pulse Height Analyzer

-Normalizing factor was  $8.1134E-05$

-Beam current =  $4.0E-08$  Amps

TABLE IV  
Tabular Data for Figure 3.2

Degree	Channel	Normalized Value
1	219	.0244
2	114	.0127
3	198	.0221
4	284	.0317
5	556	.0620
6	694	.0774
7	772	.0861
8	786	.0877
9	572	.0638
10	393	.0438
11	304	.0339
12	193	.0215
13	190	.0212
14	64	.0071
15	0	.0000

-Channel values were read from Pulse Height Analyzer

-Normalizing factor was  $1.1158E-04$

-Beam current =  $4.0E-08$  Amps

TABLE V  
Tabular Data for Figure 3.3

Degree	Channel	Normalized Value
1	117	.0837
2	0	.0000
3	75	.0537
4	207	.1481
5	431	.3083
6	565	.4042
7	623	.4457
8	590	.4221
9	556	.3978
10	442	.3162
11	344	.2461
12	262	.1874
13	210	.1502
14	111	.0794
15	109	.0780

-Channel values were read from Pulse Height Analyzer

-Normalizing Factor was  $3.9502E-04$

-Beam current =  $4.0E-08$  Amps

**TABLE VI**  
**Tabular Data for Figure 3.4**

Degree	Channel	Normalized Value
1	117	.0290
2	0	.0000
3	75	.0186
4	207	.0513
5	431	.1069
6	565	.1401
7	623	.1545
8	590	.1463
9	556	.1379
10	442	.1096
11	344	.0853
12	262	.0650
13	210	.0521
14	111	.0275
15	109	.0270

-Channel Values were read from the Pulse Height Analyzer

-Normalizing factor was 2.48E-04

-Beam current = 4.0E-08 Amps

**TABLE VII**  
**Tabular Data for Figure 3.5**

Degree	Channel	Normalized Value
1	101	.0190
2	96	.0180
3	188	.0353
4	434	.0815
5	575	.1080
6	864	.1623
7	828	.1555
8	752	.1413
9	610	.1146
10	734	.1379
11	635	.1193
12	609	.1144
13	446	.0838
14	265	.0498
15	152	.0286

- Channel values were read from the Pulse Height Analyzer
- Normalizing factor was  $1.878E-04$
- Beam current =  $4.0E-08$  Amps

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