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Volume 1



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Damage Tolerant Design Handbook

A Compilation of Fracture and Crack-Growth Data
for High-Strength Alloys

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This edition entirely revamps the 1975 edition. This edition is arranged by alloy rather than by property as in the previous addition. The data are presented in eight chapters and four volumes. Plane-strain fracture toughness (K _{IC}), critical plane stress fracture toughness, apparent fracture toughness, R-curve, fatigue crack growth rates, sustained-load crack growth rate and threshold stress intensity (K _{ISCC}) data are presented for stainless steels, titanium alloys, nickel-base alloys, alloy steels, 2000-, 6000- and 7000-series aluminum alloys. | | |

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**DAMAGE TOLERANT DESIGN HANDBOOK
MCIC-HB-01R**

ABOUT THIS HANDBOOK —

The **Damage Tolerant Design Handbook** was prepared by University of Dayton Research Institute under U.S. Air Force sponsorship and is being distributed by the Metals and Ceramics Information Center (MCIC). Its purpose is to provide a single comprehensive reference source on available fracture mechanics data for structural metal alloys of particular interest for aircraft and aerospace application.

SUPPLEMENTS —

It is intended that, as new data are generated on the fracture characteristics of structural alloys, supplements to this Handbook will be published by MCIC. Further updating and expansion of the current edition will result in supplements as significant data become available. Minor additions, errata, and inserts will be distributed as information becomes available.

KEEPING YOUR HANDBOOK UP TO DATE —

In order that we may keep all holders of the **Damage Tolerant Design Handbook** advised of supplements and new reference data, a registry of the location of all copies will be maintained. To assist us, we ask that you complete and return one of the self-addressed postcards (following this page) upon initial receipt of the Handbook. If responsibility for this copy is transferred to another party, please use one of the other postcards to advise us of the change. If there are no postcards, simply write to MCIC at the address below.

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Although a substantial and continuing effort is made to include all available appropriate fracture mechanics data in this Handbook, we recognize that important sources may have been inadvertently overlooked and, of course, that new data are regularly being generated. Should you or your organization be able to provide additional pertinent data, MCIC — and other users of this reference Handbook — will be most appreciative. To be useful, data should include the supporting facts regarding material, condition, and test specimens and procedures. If you can assist us in this respect, please call or submit such data to MCIC at the address below. Many thanks

ADDITIONAL INFORMATION —

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Volume 1

Damage Tolerant Design Handbook

**A Compilation of Fracture and Crack Growth
Data for High-Strength Alloys**

Compiled by

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Sponsored by

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December 1983

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MCIC is publishing this revised and expanded edition of the Damage Tolerant Design Handbook to increase the availability of information to the technical community. The loose leaf format was selected to facilitate updating the handbook as new information becomes available. This edition is a completely revised and expanded version of the original handbook first published by MCIC in 1972 and revised in 1973 and 1975.

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FOREWORD

This report has been prepared as AFWAL-TR-83-4144 to summarize the results of a damage-tolerant-material-property collection and reporting program conducted under USAF Contract No. F33615-80-C-5149, Damage Tolerant Design Handbook. The Materials Laboratory of Air Force Wright Aeronautical Laboratories (AFWAL/ML) was the sponsor; Mr. G. J. Petrak (AFWAL/MLSE) of the System Support Division was the Project Monitor. The University of Dayton was the contractor; the University of Dayton Research Institute (UDRI) conducted the work under the general supervision of Dr. J. P. Gallagher, program manager, and Mrs. Patricia L. Stumpff, principal investigator. Miss Elizabeth L. Johnson was responsible for the development of the software system that both stored the damage tolerant data and created the handbook graphical and tabular reports. Dr. P. W. Hovey developed the analytical french curve method used to describe the mean trend subcritical crack growth behavior. Other UDRI employees who provided extensive support for the creation of the handbook are: Dr. A. P. Berens, Mrs. Joanda D'Antuono, Mrs. JoAnn D. Jones, Miss Ellen M. Bornhorst, Miss Mary E. Stander, and Mr. Kevin Sullivan.

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A 286
D6 AC
HP 9-4-.20
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HP 9-4-.25
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HP 9-4-.45
HY-TUF
HY-150
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H11
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12-9-2 (MAR)
12Ni-5Cr-3Mo
18Ni (180) MAR
18Ni (200) MAR
18Ni (250) MAR
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18Ni (300) MAR
300M
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300M (VM)
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| 2024 | 2219 | |

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CHAPTER 1 HANDBOOK ORGANIZATION AND CONTENT

1.0 OVERVIEW

This edition of the Damage Tolerant Design Data Handbook has been entirely revamped since the last update in 1975. The major organizational change is that data are now presented and sorted by material (aluminum, titanium, etc.) and by alloy (2024, 6Al-4V, etc.) rather than by property (i.e., K_{Ic} , K_{Isc} , da/dN). The reorganization makes it possible to present all the pertinent damage tolerant data on a particular alloy within one chapter subsection. This new organization was suggested by aerospace engineers as being the format best suited for their use. Additionally, this format now conforms to other aerospace structural metals handbooks such as the Military Handbook-5 and Aerospace Structural Metals Handbook.

A survey was conducted at the beginning of this handbook program; over one-hundred aerospace design, materials, and structural engineers were canvassed for their comments relative to the proposed organization, formats, types of summaries and new data types. Many of the comments and suggestions received were incorporated into the final design of the handbook. The data types of greatest interest were found to be fracture toughness data, fatigue crack growth rate data and R-curves. Interest in specific materials were mainly for the nickel base and aluminum alloy materials.

Throughout the handbook, the data are presented in English units, i.e., ksi $\sqrt{in.}$ was the unit for the fracture toughness and applied stress intensity factor levels, and inches/hr or inches/cycle were the unit values for the growth rates. Metric units have been incorporated along with the English units on the graphical presentation of the sustained load and fatigue crack growth rate data, but limited space forced the decision not to include metric units for the tabular data.

1.1 ORGANIZATION

The handbook is divided into eight chapters and consists of four volumes. Following the first chapter on handbook usage and the the second chapter on methods of calculations are the six material chapters. The order of the chapters are as designated in Table 1.1. This order was selected to keep the data for a particular chapter together as much as possible while keeping the size reasonable and the four volumes approximately equal.

Table 1.2 depicts the basic organization of each material chapter. Within each material chapter, the data are further divided into a section of material summaries, followed by sections that contain the data for individual alloys. The first number of any section, subsection, table or figure number refers to the chapter or material as designated in Table 1.1. The second number will run consecutively from zero on. A zero in the second position indicates that the data is a material summary; each succeeding second number indicates a new alloy, with the highest second number referring to the bibliography for that material chapter.

In a given material summary section, i.e., X.0, there are five possible material summary tables listed as subsections. Tables will be listed in the order defined by Table 1.2. If not enough data are available for a particular summary, this summary will not be printed and the next summary will pick up the sequence number. Section 1.3 describes the formats for the material summaries.

In each alloy section, e.g., Sections X.1, X.2, etc., the third number in the sequence will designate whether the data are (1) an alloy summary, (2) fracture toughness data, or (3) crack growth resistance data. Within each subsection, the data tables and graphs are ordered consecutively.

TABLE 1.1
ORDER OF CHAPTERS

| <u>VOLUME NUMBER</u> | <u>CHAPTER</u> | <u>TITLE</u> |
|----------------------|----------------|--|
| 1 | 1 | Handbook Organization, Content, and Formats |
| 1 | 2 | Methods of Calculations |
| 1 | 3 | Stainless Steel Alloys |
| 1 | 4 | Titanium Alloys |
| 2 | 5 | Nickel Base Alloys |
| 2 | 6 | Alloy Steel Alloys |
| 3 | 7 | 2000 and 6000 Series Aluminum Alloys |
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- X.0.3 - Plane Stress and Transitional Fracture
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Alloy Number One
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- X.1.3 - Subcritical Crack Growth Data
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(Tables and Plots) for Alloy Number One
 - X.1.3.2 - Sustained Load Crack Growth Rate Data
 - X.1.3.3 - Stress Corrosion Cracking Threshold Data
for Alloy Number One

SECTION X.2 - Second Material Alloy

SECTION X.N - Last Material Alloy

SECTION X.N+1 - Bibliography for the Chapter

There are three possible types of fracture toughness data: plane-strain fracture toughness data, plane stress and transitional fracture toughness data, and resistance curve data; Section 1.5 provides a detailed discussion of the data formats. There are three possible types of subcritical crack growth data: fatigue crack growth rate data, sustained load crack growth rate data, and stress corrosion cracking threshold data; Section 1.6 details the formats used to present these data.

To aid the handbook user locate data, examples of actual tables and figures follow. These examples are presented to familiarize the user with the formats presented in the handbook. Each table or figure is discussed as it is presented. The discussion follows the same order as that found in the handbook.

1.2 GENERAL COMMENTS ABOUT SORTING ORDER AND ABBREVIATIONS

1.2.1 Sorting Order

Table 1.3 describes the sorting order for all mechanical property data types. The left column lists the primary (material) data fields that have been sorted; the right column then lists the specific sorting order of each material data field. In all the following discussions, when a primary data field is noted as being sorted, the order of the sorting is as listed in Table 1.3. The primary data fields are also sorted; however, because the different data fields have different significance for individual mechanical property types, the sorting order is noted as each mechanical property data format is discussed. For all property data types, the property data are generally sorted in the order of first five primary data fields listed in Table 1.3.

1.2.2 Abbreviations

To ensure that all the necessary information is presented in the data tables and figures, specific abbreviations have been employed throughout the handbook. The abbreviations can be broken down into six categories that cover the following

TABLE 1.3
SORTING ORDER OF VARIOUS FIELDS

| <u>DATA FIELD</u> | <u>SORTING ORDER</u> |
|-----------------------------|---|
| 1. Alloy | Blank Punctuation Marks (e.g., -) Alphabetic Characters (e.g., T) Numeric Characters (e.g., 6) |
| 2. Condition/Heat Treatment | Blank Punctuation Marks Alphabetic Characters Numeric Characters |
| 3. Product Forms | Sheet Plate Forging Extrusion Forged Bar Billet Casting Round Bar Welded and Stress Relieved Weldment Disk Extruded Bar Rolled Bar Bar |
| 4. Test Temperatures | Negative Test Temp. (-423°F, -300°F) From 0°F to 65°F (0°F, 32°F etc.) From 65°F to 80°F (R.T.) Above 80°F (85°F, 200°F, etc.) |
| 5. Specimen Orientation | L-S L-T T-S T-L S-T S-L L-C C-L L-R R-L R-C C-R |
| 6. Yield Strength | Lowest to Highest |
| 7. Buckling Constraints | Buckling of Crack Edges Not Restrained Buckling of Crack Edges Restrained Buckling of Crack Edges Unknown |

data fields: (1) material, (2) condition/heat treatment, (3) product form, (4) environment, (5) specimen design, and (6) specimen/crack orientation. The abbreviations and associated descriptions for these six categories can be found in Tables 1.4 through 1.8 and Figure 1.1, respectively.

1.3 MATERIAL CHAPTER SUMMARIES

Material summaries are presented at the beginning of each chapter before any alloy summaries or detailed data. These summaries are meant to aid in the selection of materials for design and for basic comparisons of property data. There are five possible material summaries (see Table 1.2), each of which compare availability or properties of damage tolerant data for the given alloys, heat treatments, and product forms of a particular material. The five summaries immediately follow the text of introductory remarks that discuss the data for that material.

1.3.1 Available Data Summary

Figure 1.2 is the first page of the available data summary for the stainless steel chapter. As noted, the first number in the data summary table is a "3" which indicates that this is the third chapter; the second number is a "0" indicating that this is a material summary; the third number is a "1" which indicates that this is the first table in the material summary section. Note that the table numbers for subsequent data summaries only change in the third digit, except for the fatigue crack growth rate summary (see below).

The available data summary defines the property data that are available in the chapter by alloy, by condition/heat treatment, and by product form. The six different types of data are listed generally across the top of the table; an "x" is marked in the appropriate column to identify the particular property data that exists for the given alloy, condition/heat treatment, etc. The alloys are listed in the order that they appear in the handbook using the sorting order outlined in Table 1.3. This sorting order was created using a system

TABLE 1.4
ABBREVIATIONS FOR MATERIAL SYSTEMS

| <u>Abbreviation</u> | <u>Materials</u> |
|---------------------|------------------------|
| ALUM | Aluminum Alloys |
| TITAN. | Titanium Alloys |
| NICKEL | Nickel-Base Alloys |
| STAIN. STEEL | Stainless Steel Alloys |
| ALLOY STEEL | Steel Alloys |

TABLE 1.5
ABBREVIATIONS FOR ALLOY CONDITIONING AND HEAT TREATMENTS

| <u>Abbreviation</u> | <u>Condition/Heat Treatment</u> |
|---------------------|---------------------------------|
| OQ | Oil Quenched |
| ABQ | Aus-Bay Quench |
| AC | Air Cool |
| WC | Water Quench |
| MA | Mill Anneal |
| BA | Beta Anneal |
| DA | Duplex Anneal |
| RA | Recrystallize Anneal |
| ST | Solution Treated |
| STA | Solution Treated And Aged |

TABLE 1.6
ABBREVIATIONS FOR PRODUCT FORMS

| <u>Abbreviations</u> | <u>Product Form</u> |
|----------------------|---------------------|
| S | Sheet |
| P | Plate |
| E | Extrusion |
| F | Forging |
| FB | Forged Bar |
| BT | Billet |
| BR | Round Bar |
| RB | Rolled Bar |
| C | Casting |
| W | Weldment |
| D | Disk |
| EB | Extruded Bar |
| B | Bar |

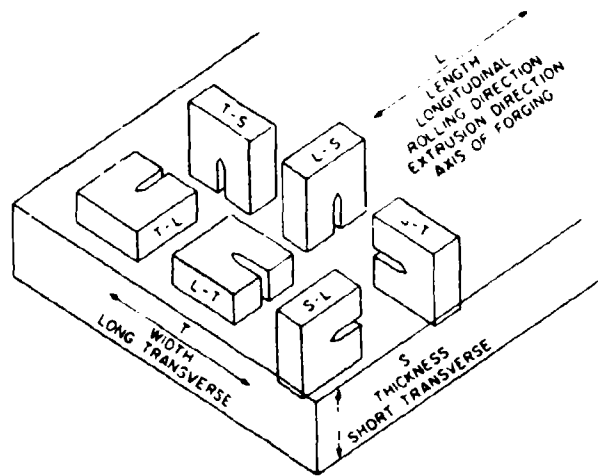
TABLE 1.7
ABBREVIATIONS FOR ENVIRONMENTAL SYSTEMS

| <u>Abbreviations</u> | <u>Environmental System</u> |
|------------------------|-----------------------------------|
| R. T. | Room Temperature (65°F-80°F) |
| L. H. A. | Low Humidity Air (< 10% RH) |
| Dry Air | Low Humidity Air (< 10% RH) |
| H. H. A. | High Humidity Air (> 80% RH) |
| Lab. Air | Laboratory Air (% RH unspecified) |
| Dist. H ₂ O | Distilled Water |
| Dist. Water | Distilled Water |
| 3.5 PCT NaCl | 3.5% Salt Water Solution |
| JP.4 | JP-4 Aircraft Fuel |
| JP.4 - Fuel | JP-4 Aircraft Fuel |
| S. T. W. | Sump Tank Water |
| S. S. W. | Simulated Sea Water |
| S. C. S. | Shop Cleaning Solvent |
| F. C. S. | Field Cleaning Solvent |
| Salt Fog | Salt Fog |
| Temp. | Temperature |

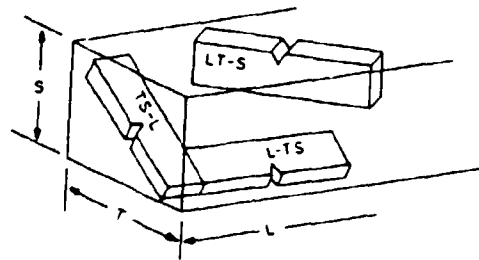
TABLE 1.8
ABBREVIATIONS FOR SPECIMEN DESIGNS

| <u>Abbreviations</u> | <u>Specimen Design*</u> |
|----------------------|------------------------------------|
| CT | Compact Tension |
| NB | 3Pt. Notched Bend |
| WOL | Wedge Open Load |
| CCP | Center Cracked Panel |
| BWOL | Bolt Loaded-Wedge Open Load |
| CANT | Cantilever Beam |
| TDCB | Tapered Double Cantilever Beam |
| CHAR | Charpy |
| PTSC | Part Through Surface Crack |
| SENT | Single Edge Notch Tension |
| K _B BAR | K _B Bar |
| 4-NB | 4 Pt. Notched Bend |
| MCT | Modified Compact Tension |
| CNT | Center Notched Tension |
| DCB | Double Cantilever Beam |
| BDCB | Bolt Loaded Double Cantilever Beam |

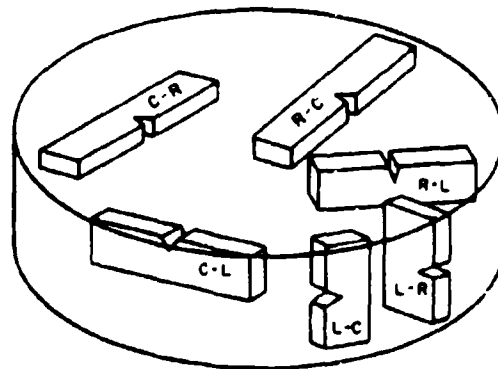
*Also note that when "SG" is used in conjunction with a specimen design, the specimen is side-grooved along the path of the crack.



(a) Crack Plane Orientation Code for Rectangular Sections



(b) Crack Plane Orientation Code for Rectangular Sections Where Specimens are Tilted with Respect to the Reference Directions



(c) Crack Plane Orientation Code for Bar and Hollow Cylinder

Figure 1.1. ASTM Abbreviations Used to Describe Specimen Orientations.

Table 3.0.1
 AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DN | DA/DT | MISCC |
|---------|--|--------------|-----|-----|----------|-------|-------|-------|
| AFC 260 | 2200F 1HR 1900F 1HR DG -100F 1HR -320F 1HR 800F 2+2 HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR DG -100F 1HR -320F 1HR 1050F 2+2HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR DG -100F 1HR -320F 1HR 900F 2+2 HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR DG -100F 1HR -320F 1HR 1000F 2+2 HR | PLATE | | | | | | X |
| | AUSTENIZED AT 2010F. QUENCHED & TEMPERED AT 810F | SHEET | | | | | X | |
| | 1800F 1HR DG, -100F 0.5HR, 500F 2+2 HR (COARSE GRAIN) | PLATE | | | | | | X |
| | 1800F 1HR DG, -100F 0.5HR, 1000F 2+2 HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR DG, -100F 0.5HR, 500F 2+2 HR (FINE GRAIN) | PLATE | | | | | | X |
| AFC 77 | 1800F 1HR DG, -100F 0.5HR, 1000F 2+2 HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 700F 2+2HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 800F 2+2HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 700F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 800F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 700F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 800F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, DG, -100F 0.5HR, 700F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |

Figure 1.2. Sample Data Summary Table, Taken From Table 3.0.1
 (Stainless Steel Alloys).

sort of the database and sorts the alloys with designations using blanks, punctuation marks and alphabetic characters first with numeric characters following. Heat treatments and conditions are also sorted in this same manner. Following the sort by alloy and by condition/heat treatment, the property data are then sorted according to product form. The particulars of the sorting by product form are also outlined in Table 1.3 with sheet data listed before plate, forging, extrusion, etc.

1.3.2 Plane Strain Fracture Toughness Material Data Summary

The first page of the stainless steel, plane-strain fracture-toughness-data summary is shown in Figure 1.3. This is the second possible material summary and the third table digit is "2". The data are again sorted and separated on the data fields of alloy, condition/heat treatment and product form. All data listed are for room temperature (65°F - 80°F) laboratory air only. Plane strain fracture toughness mean values and standard deviations are listed for the three major orientations; that is, L-T, T-L and S-L. Product thickness range and minimum specimen thicknesses are listed for general information. Dashes in a particular column indicate that no mean plane strain fracture toughness data exist for the stated conditions.

1.3.3 Plane Stress and Transitional Fracture Material Data Summary

The plane stress and transitional fracture toughness data summary is presented third in the series of summaries. Figure 1.4 illustrates that these tables are presented as a function of whether the data are collected using specimens with or without buckling constraints. Note that in Figure 1.4 (all available titanium data) and 1.4b (all available alloy steel data) that the data are sorted by alloy, condition/heat treatment, test temperature, specimen orientation and specimen width. Yield strength is not a sorting field but is given for general information. The mean K_{IC} values are listed as a function of specimen thickness which is indicated across the top of the page.

TABLE 3.0.2
PLANE STRAIN FRACTURE TOUGHNESS VALUES OF STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/II | PRODUCT FORM | NAME OF PRODUCT THICKNESSES (IN) | L-T | | | S-L | | |
|--------------|--|--------------|----------------------------------|------------------|-------|---------|------------------|-------|---------|
| | | | | SPECIMEN THICK * | MEAN | STD DEV | SPECIMEN THICK * | MEAN | STD DEV |
| AFC 77 (VAR) | 1700F 1HR. 00 2100F 1HR. MOVED TO FCE AT 1923F. WELD 1HR. 00. -100F 2*HR. 900F. 2*2HR | FORGING | 6 00 | 0 50 | 48 6 | 3 1 | 0 50 | 30 8 | 1 3 |
| | | | | 2 01 | 110 5 | 4 9 | 2 01 | 108 0 | 5 7 |
| CUSTOM 433 | 1500F 1HR. 00. 950F 4HR. AC | FORGING | 4 00 | 0 48 | 72 1 | 7 8 | | | |
| | | | | 0 48 | 46 2 | 3 3 | | | |
| PH13-6PH | ANNEALED AUSTENITE COND FORCED BAN AND TRANSFORMED AT 38F. AGED 1015F | FORGING | 3 00 | 1 01 | 114 1 | 13 7 | 1 00 | 99 6 | 22 4 |
| | | | | 1 63 | 103 0 | 19 4 | 1 63 | 89 6 | 1 8 |
| | H 950 | SHEET | 1 00-2 25 | 1 00 | 58 4 | 6 5 | 1 00 | 69 4 | 16 1 |
| | | | | 1 00 | 70 3 | 16 0 | | | |
| | H1000 | SHEET | 1 50-2 25 | 1 00 | 64 9 | 2 9 | 1 00 | 63 5 | 1 7 |
| | | | | 0 98 | 94 7 | 3 4 | | | |
| | 2 75-8 00 | EXTRUSION | 1 50 | 1 00 | 68 5 | 5 5 | 1 00 | 66 2 | 2 1 |
| | | | | 0 75 | 101 6 | 11 0 | 0 75 | 88 1 | 17 1 |

* MINIMUM SPECIMEN THICKNESS (IN)

Figure 1.3. Summary of Plane Strain Fracture Toughness (K_{IC}) Data, Taken from Table 3.0.2 (Stainless Steel Alloys).

TABLE 4.0.3

PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS OF
TITANIUM ALLOYS (WITH BUCKLING CONSTRAINTS)

| Alloy | Condition/Ht | Test Temp. (°F) | Specimen Orient | Specimen Width (in.) | Yield Strength (KSI) | Specimen Thickness (in.) = 0.020 | K_{IC} (KSI \sqrt{in}) | 0.040 | 0.050 |
|-----------------|--------------|-----------------|-----------------|----------------------|----------------------|----------------------------------|-----------------------------|----------------|---------------|
| Ti-5Al-2.5Sn | Annealed | -423 | L-T | 3.0 | 203 | 116.8/4.5 (5) | 147.6/28.9 (2) | | |
| | | | | 6.0 | 203 | 109.4/6.6 (9) | | | |
| | | | | 12.0 | 203 | 104.2/4.0 (8) | | | |
| | | | | 16.0 | 203 | 97.1/9.6 (2) | | | |
| Ti-6Al-4V | HA | R. T. | L-T | 24.0 | 136 | | | 196.4/19.9 (6) | |
| | | | T-L | 8.0 | 163 | | 159.4/7.5 (3) | | |
| Ti-6Al-4V (ELI) | Annealed | R. T. | L-T | 18.0 | 136 | 161.6/6.5 (5) | | | |
| Ti-8Al-1Mo-1V | D. A. | R. T. | L-T | 12.0 | 136 | 111.7/15.0(3) | | | 220.5/15.8(4) |
| | | | | 20.0 | 134 | | | | |

Mean/Standard Deviation (No. of Specimens)

Figure 1.4a. Format for Plane Stress and Transitional Fracture Toughness Data where Specimens were Constrained from Buckling. Example from Table 4.0.3, Titanium Alloys.

TABLE 6.0.3
 PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS OF
 STEEL ALLOYS (WITHOUT BUCKLING CONSTRAINTS)

| Alloy | Condition/Ht | Test Temp. (°F) | Specimen Orient | Specimen Width (in) | Yield Strength (Ksi) | Specimen Thickness (in) = 0.025 | K_c^a (Ksi $\sqrt{\text{in}}$) |
|----------------|--------------|-----------------|-----------------|---------------------|----------------------|---------------------------------|-----------------------------------|
| 18 Ni(300) MAR | ---- | -423 | L-T | 4.0 | 386 | 86.4/7.3 (5) | |
| | | -320 | L-T | 2.0 | 336 | 142.6/7.4 (5) | |
| | L-T | | 4.0 | 336 | 124.7/8.0 (5) | | |
| | | R. T. | L-T | 2.0 | 277 | 132.1/4.3 (5) | |
| | | | L-T | 4.0 | 277 | 128.5/3.8 (5) | |
| | | | | L-T | 18.0 | 277 | 110.3/10.9 (3) |

^a Mean/Standard Deviation (No. of Specimens)

Figure 1.4b. Format for Plane Stress and Transitional Fracture Toughness Data Where Specimens Were Not Constrained from Buckling. Example from Table 6.0.3, Alloy Steels.

Individual K_c data values are listed only if useful in determining a trend in the data. Specimen thickness variations run along the top of the page and may vary from one table to another in order to prevent overcrowding the tables while still accommodating all of the data.

1.3.4 Fatigue Crack Growth Rate Material Data Summary

An example fatigue crack growth rate (FCGR) summary is presented in Figure 1.5 where the data are taken from the Stainless Steel Chapter. Note that the data are from Table 3.0.3.1, a four number sequenced designation. The first two numbers again indicate the chapter (3) and the summary section (0). The third number in the sequence (3) indicates that this is the third ordered table in the material summary (Note that insufficient plane stress and transitional fracture toughness data were available for this material so no summary table of the K_c type was generated). The fourth number in the sequence (1) indicates that this is the first ordered table in the fatigue crack growth rate summary. Readers will find one table for each specimen orientation for which there is enough data for the table to have meaning.

All data in a particular table were collected under conditions where the stress ratio (R) is between 0.0 and 0.1, and the environment is room temperature and laboratory air; the loading frequencies vary slightly depending on the individual tests. The range of test conditions are listed at the top of each table. Beneath the general description of test conditions are the data fields of alloy, condition/heat treatment and product form for which the FCGR data comparisons can be made. The ΔK (Delta K) levels are listed across the top of the table and are identical to some of the levels associated with the tabular format of the mean trend FCGR data, i.e., at levels of 2.5, 5.0, 10.0, 20.0, 50.0, 100.0 Ksi $\sqrt{\text{in.}}$ (see Section 1.6 for a listing of all mean trend ΔK levels). The fatigue crack growth rates in units of 10^{-6} inches/cycles, are listed in the appropriate columns and rows according to the alloy, condition/heat treatment, and product form for which they apply. With this format, it is easy to determine which materials, heat

Table 3.0.3.1

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR STAINLESS STEEL ALLOYS

TEST CONDITIONS.

SPECIMEN ORIENTATION: Unknown ENVIRONMENT: LAB AIR AT R. T.
 STRESS RATIO: 0.05-0.10 FREQUENCY: 3.00-30.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | |
|-------|----------------------------|--------------|--------------|-----------|---|------|------|
| | | | | | FOR DELTA K LEVELS (K1 SORT(1IN)) = | 20.0 | 50.0 |
| 304 | ANNEALED | SHEET | 0.05 | 10.00 | .163 | 3.07 | |
| | ANNEALED | SHEET | 0.05 | 15.00 | .130 | 2.83 | |
| | ANNEALED | SHEET | 0.10 | 1.67 | | 2.84 | |
| | ANNEALED | SHEET | 0.10 | 6.00 | | 2.56 | |
| | ANNEALED & AGE | PLATE | 0.05 | 3.00 | | 1.38 | |
| 316 | ANNEALED AT 1950F, 1HR, NO | PLATE | 0.05 | 10.00 | | 2.39 | |
| 347 | 050 IN FROM CENTERLINE | WELDMENT | 0.10 | 30.00 | | 9.83 | |
| | AT CENTERLINE | WELDMENT | 0.10 | 30.00 | | 13.1 | |
| | AT HEAT AFFECTED ZONE | WELDMENT | 0.10 | 30.00 | | 17.9 | |

Figure 1.5. Summary of Fatigue Crack Growth Rate Data, Taken from Table 3.0.3 (Stainless Steel Alloys).

treatments, or product forms have the lowest growth rate at a particular ΔK level. For example, based on the data given in Figure 1.5, annealed and aged 304 stainless steel performs better than annealed 304 stainless steel.

1.3.5 Stress Corrosion Cracking Threshold Material Data Summary

Figure 1.6 illustrates, using Table 3.0.4, the format for the stress corrosion cracking threshold material data summary, the fifth possible material data summary. Because of the small number of specimens (typically one or two) that are used to generate these data, individual results are presented here rather than means and standard deviations. The data are sorted by alloy, condition/heat treatment, product form and specimen orientation. Possible environments for which K_{ISCC} data exist are listed across the top of the table; K_{ISCC} data values for each particular environment are listed in the appropriate row and column. This table summary allows for comparisons of K_{ISCC} values of various materials in a particular environment as well as a quick assessment of how various environments affect a particular material.

1.4 ALLOY SECTION SUMMARIES

Following the material summaries, the data were divided into sections by alloy. Each alloy section is further subdivided into three subsections: a summary subsection, a fracture toughness subsection, and a crack growth resistance subsection. The data content and format for these three subsections are described in this and the following two subsections, respectively.

There are two possible alloy summaries, a plane strain fracture toughness summary and fatigue crack growth rate data summary. Figure 1.7 presents the tabular format for the K_{IC} alloy summary. It is similar to the K_{IC} material summary in that the mean and standard deviation for a particular condition/heat treatment, product form and specimen orientation is given for each alloy. However, the number of specimens used to generate the data has been added. The data has also been sorted by product form first, then condition/heat treatment and specimen orientation.

TABLE 3.0.4

INDIVIDUAL STRESS CORROSION CRACKING THRESHOLD DATA FOR STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ FIT | PRODUCT FORM | SPECIMEN ORIENTATION | S _{ISCC} (ksi/in) | | |
|----------|--|-----------------|-------------------------|------------------------------|--------------------------|---|
| | | | | SIMP TANK WATER 3.5% NaCl | ENVIRONMENTS 20% NaCl | SEACOAST ATMOSPHERE INDUST. ATMOSPHERE |
| AFC 77 | 1800F 1HR O ₂ , -100F 0.5 HR, 500F 2&2 HR, (Coarse G.S.) | P | --- | 15 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 700F 2&2 HR | B | --- | 50 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 800F 2&2 HR | B | --- | 40 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 900F 2&2 HR | B | --- | 15 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 1100F 2&2 HR | B | --- | 10 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 500F 2&2 HR, & 10PCT CW, 1000F | B | --- | 30 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 500 2&2 HR, & 10PCT CW, 700F | B | --- | 90 | | |
| | 2000F 1HR O ₂ , -100F 0.5 HR, 500F 2&2 HR, & 20 PCT CW, 700F | B | --- | 48 | | |
| | 2200F 1HR, 1900F 1HR O ₂ , -100F 1HR, -300F 1HR, 900F, 2&2 HR | P | T-L | 40 | | |
| | 2200F 1HR, 1900F 1HR O ₂ , -100F 1HR, -100F 1HR 1000F 2&2 HR | P | T-L | 45 | | |
| | 2200F 1HR, 1900F 1HR O ₂ , -100F 1HR, -300F 1HR, 1050F 2&2 HR | P | T-L | 37 | | |
| | AN 355 | SCT 850 | P | T-L | 8 | 24 |
| | | B | T-L | 6 | 18 | 18 |
| SCT 1000 | | P | T-L | 37 | 52 | 99 |
| | | B | T-L | 28 | 35 | 66 |

Figure 1.6. Summary of Stress Corrosion Cracking Threshold Material Data, Taken from Table 3.0.4 (Stainless Steel Alloys).

Table 3.8.1.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF STAINLESS STEEL ALLOY PH13-8MO AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | | (NUMBER OF SPECIMENS) | |
|---|--|-----------------|-----------------------|-----|
| | L-L | I-L | I-L | S-L |
| <u>FORGED BAR</u> | | | | |
| AUSTENITE COND AND TRANSFORMED AT 38F. AGED 1015F | 103.0 ± 19.4 (2) | 89.6 ± 1.8 (2) | | |
| M1000 | 114.2 ± 0.9 (2) | 122.7 ± 3.0 (3) | | |
| <u>ROLLED BAR</u> | | | | |
| M 950 | 66.9 ± 2.9 (3) | 63.5 ± 1.7 (6) | 74.1 ± 2.1 (3) | |
| M1000 | 90.0 ± 7.1 (2) | 75.0 ± 4.2 (2) | | |
| M1050 | 103.1 ± 4.6 (3) | 94.8 ± 7.8 (6) | 92.2 ± 4.2 (2) | |

Figure 1.7. Alloy Summary Format for Plane-Strain Fracture Toughness Data, Taken from Table 3.8.1.1.1, PH 13-8Mo Stainless Steel.

This summary basically puts all the K_{IC} data for a particular condition and product form together for easy comparison. It also allows for a quick assessment of the effect that orientation has on the fracture toughness.

The FCGR alloy data summaries shown in Figure 1.8 are similar to the FCGR material data summaries described previously. Note that for a particular alloy, the data are separated by the test variables of specimen orientation and environment which are listed at the top of each page. Other test variables such as condition/heat treatment, product form, stress ratio and frequency are then listed for the data as noted. Typically, a number of FCGR data summaries are produced to describe the effects of specimen orientation and environments. Sorting on specimen orientation is as shown in Table 1.3 and sorting on environment is in the order described in Table 1.9. With these summary tables, it is possible to determine which condition/heat treatment and product form give the lowest FCGR in a given environment for a given specimen orientation. Discrepancies in data sets can also be noted as well as a quick determination of how stress ratio and frequency affect the data in a particular environment.

1.5 ALLOY FRACTURE TOUGHNESS SUBSECTION FORMATS

Within each alloy section following the alloy summaries is the fracture toughness type data. Fracture toughness data consists of plane strain data (K_{IC}), plane stress and transitional fracture toughness data (K_C), and resistance curve data (R-curves). Each of these has a different and yet somewhat similar ordering scheme which is particularly suited to that type of data.

1.5.1 Plane Strain Fracture Toughness

The format for the plane-strain fracture toughness data is shown in Figure 1.9. This particular example is taken from the stainless steel chapter for alloy AFC 77. The data are sorted by condition/heat treatment, then product form, test temperature, orientation and yield strength using the sorting order identified in Table 1.3. All K_{IC} data collected for these

Table 3.8.1.4
 FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL PH13-8MI

TEST CONDITIONS
 SPECIMEN ORIENTATION L-T

ENVIRONMENT: L.H.A.
 AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | |
|--------------|--------------|--------------|-----------|-------------------------------|---|------|------|------|----|-----|
| | | | | | 2.5 | 5 | 10 | 20 | 30 | 100 |
| H1000 | EXTRUDED BAR | 0.08 | 6.00 | | | | 2.22 | 20.8 | | |
| | EXTRUDED BAR | 0.30 | 6.00 | | | | 2.98 | | | |
| H1000 | FORGED BAR | 0.08 | 6.00 | | | | 5.82 | | | |
| H1000 | FORGED BAR | 0.30 | 6.00 | | | | 4.70 | | | |
| H1000 | FORGED BAR | 0.50 | 6.00 | | | 0.51 | 4.70 | | | |
| H1000 | BILLET | 0.00 | 6.00 | | | 0.34 | 4.02 | | | |
| H1000 | EXTRUDED BAR | 0.08 | 6.00 | | | 0.33 | 3.73 | 34.4 | | |
| H1000 | EXTRUDED BAR | 0.50 | 6.00 | | | 0.85 | 5.59 | | | |
| H1000 | ROLLED BAR | 0.08 | 1.00 | | | 0.29 | 3.57 | | | |
| H1000 | ROLLED BAR | 0.00 | 6.00 | | | 0.29 | 3.40 | | | |
| H1000 | ROLLED BAR | 0.30 | 6.00 | | | 0.62 | 4.39 | | | |
| H1000 | ROLLED BAR | 0.50 | 6.00 | | | 0.79 | 5.09 | | | |

Figure 1.8. Format for Alloy Fatigue Crack Growth Rate Data Summary, Data Taken from Table 3.8.1.4, PH 13-8 Mo Stainless Steel.

TABLE 1.9
ORDERING SCHEME FOR ENVIRONMENT

Dry Air
Low Humidity Air
Negative Temperatures/Air
0°F to Room Temperature
Room Temperature/Laboratory Air
Above Room Temperature/Air
Argon
High Humidity Air
JP-4 Fuel
Water Saturated JP-4 Fuel
Alternating JP-4 Fuel
Distilled Water
Nitrogen
Solvent Cleaning Solution
3.5% NaCl
Sump Tank Water
Simulated Sea Water
Salt Fog
Field Cleaning Solvent

Table 3.2.2.1

| CONDITION | STAINLESS STEEL AFC 77 | | | | YIELD STRENGTH (KSI) | TEST SPECIMEN THICK TEMP (IN) (F) | ORIENT | SPECIMEN DESIGN | | | CRACK LENGTH (IN) | K(IIC) MEAN (KSI*SQRT IN) | K(IIC) STAM DEV (KSI*SQRT IN) | DATE | REFER |
|--|------------------------|------------|------------|------------|----------------------|-----------------------------------|--------|-----------------|---|---|-------------------|---------------------------|-------------------------------|------------------|-------|
| | PRODUCT FORM | THICK (IN) | WIDTH (IN) | THICK (IN) | | | | M | B | A | | | | | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 1000F 2*2#R (COARSE GRAIN) | | | 1 500 | 0 500 | 173 0 | | L-T | | | | 0 05 | 25 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 700F 2*2#R (COARSE GRAIN) | | | 1 500 | 0 500 | 183 0 | | L-T | | | | 0 11 | 38 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 800F 2*2#R (COARSE GRAIN) | | | 1 500 | 0 500 | 208 0 | | L-T | | | | 0 05 | 28 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 700F 2*2#R (FINE GRAIN) | | | 1 500 | 0 500 | 203 0 | | L-T | | | | 0 15 | 49 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 800F 2*2#R (FINE GRAIN) | | | 1 500 | 0 500 | 224 0 | | L-T | | | | 0 05 | 31 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. P 0 5# R T L-T 100F 0 5#R. 1000F 2*2#R (FINE GRAIN) | | | 1 500 | 0 500 | 232 0 | | L-T | | | | 0 04 | 30 00 | | 1969 74720 (1) | |
| 1800F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 700F 2*2#R | | | 1 500 | 0 480 | 185 0 | | L-R | | | | 0 14 | 44 00 | | 1968 84302 (1) | |
| 1800F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 800F 2*2#R | | | 1 500 | 0 480 | 213 0 | | L-R | | | | 0 03 | 29 00 | | 1968 84302 (1) | |
| 1900F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 800F 2*2#R | | | 1 500 | 0 480 | 232 0 | | L-R | | | | 0 28 | 74 00 | | 1968 84302 (1) | |
| 2000F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 900F 2*2#R | | | 1 500 | 0 480 | | | L-R | | | | | 32 00 | | 1968 84302 (1) | |
| 2000F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 800F 2*2#R | | | 1 500 | 0 480 | 207 0 | | L-R | | | | 0 29 | 70 00 | | 1969 76136 (1) | |
| 2000F 1#R. 0#1. BR 3 00 R T L-R 100F 1#R. 900F 2*2#R | | | 1 500 | 0 480 | 214 0 | | L-R | | | | 0 17 | 56 00 | | 1969 76136 (1) | |

NOTE: (1) CHEMISTICAL ANALYSIS PERCENTS: 0.18C, 0.10Mn, 0.015P, 0.021S, 0.13SI, 0.21Ni, 14.0Cr, 3.02Mo, 13.4Co, 0.27V, 0.05W
THESE DATA ARE AVERAGE VALUES

Figure 1.9. Format for Plane Strain Fracture Toughness Data. Example Taken from AFC 77 Stainless Steel Alloys, Table 3.2.2.1.

same parameters are put together with the mean and standard deviation listed in a column near the right of the page. Product thickness is listed after product form, but is not a sorting parameter. Specimen dimensions including thickness, width and crack length are also listed, but are not listed in any particular order. The $2.5 (K_{IC}/\sigma_{ys})^2$ criterion value is included for information purposes only. Two additional columns list the date of the reference and the reference number so that an idea of when the data were collected can be assessed, and where additional information might be obtained should it be desired. Reference numbers from the earlier handbook have been retained and new data have been assigned a new reference number with the first two digits signifying the organization or journal from which the data was obtained. Table 1.10 lists the general format for new reference numbers. The final column at the right hand side of the page refers to the notes at the bottom and are used to indicate out-of-range compositions, average data values, and other identifying important features.

1.5.2 Plane Stress Fracture Toughness Data

The format for presenting plane stress fracture toughness (K_C) data is presented in Figure 1.10. The sorting format for the plane stress fracture toughness (K_C) data within a particular alloy section is by condition, then buckling of crack edges restrained, unrestrained, or unknown, and then by product form, test temperature, specimen orientation, specimen thickness and specimen width. Additionally, initial and final crack lengths are given as a function of the total crack length ($2a$) for center-cracked panel/specimens. Also, the onset and maximum gross stress values are listed when available. The fracture toughness parameters K_C and K_{app} are calculated as described in Chapter 2 and the individual as well as the mean and standard deviation values are listed for both K_C and K_{app} . The final two columns present the date of the reference and the reference number.

TABLE 1.10

REFERENCE NUMBERS FOR NEW DATA AND THE ORGANIZATIONS
OR JOURNALS ASSOCIATED WITH THESE DATA

1. ALxxx - Alcoa Laboratories - Alcoa Center, PA.
2. AMxxx - Airesearch Manufacturing - Los Angeles, CA.
3. BLxxx - Battelle Columbus Laboratories, Columbus, OH
4. BWxxx - Boeing Military Airplane Co., Wichita, KA
5. DAXxx - Douglas Aircraft - Long Beach, CA
6. EFMxx - Journal of Engineering Fracture Mechanics
7. FRxxx - Fairchild Republic - Farmingdale, N.Y.
8. GDxxx - General Dynamics - Fort Worth, TX
9. GExxx - General Electric - Evendale, OH
10. HDxxx - Westinghouse Hanford Development Lab., Richland, Wash.
11. LGxxx - Lockheed Georgia - Marietta, GA.
12. MAXxx - McDonnell Aircraft Co. - St. Louis, MO
13. MDxxx - McDonnell Douglas Astronautics Corp, Huntington Beach, CA.
14. MRxxx - Materials Research Laboratory - Glenwood, IL
15. NCxxx - Northrop Corporation - Hawthorne, CA
16. NLxxx - NASA Langley Research Center - Hampton, VA.
17. NRxxx - Naval Research Laboratories - Washington, DC.
18. PWxxx - Pratt & Whitney Aircraft Group - Government Products
Division - West Palm Beach Florida
19. RAXxx - Reynolds Metals Co. - Richmond, VA
20. RIxxx - Rockwell International - North American Division &
Shuttle Orbiter Div. - Los Angeles, CA.
21. UCxxx - University of Cincinnati - Cincinnati, OH
22. UDxxx - University of Dayton Research Institute, Dayton, OH
23. UMxxx - University of Missouri - Rolle, Missouri
24. WAXxx - Wright Aeronautical Laboratories- WPAFB, OH

Table 3.9.2.1

| STAINLESS STEEL PH14-8MO | | K(C) | | CRACK LENGTH GROSS STRESS | | | | | | | | | | K(C) | | | |
|------------------------------------|--------------------------------|--------------------------|--------------------|---------------------------|------------|--------|-------|-------|--------|---------|------------|-------|-------|-------------|-----------|------------|------------|
| CONDITION | --PRODUCT-- FORM THICK (IN) | TEST SPEC OR TEMP (F) | YIELD STR (KSI) | ---SPECIMEN--- | | INIT | | FINAL | | ONSET | | MAX | | K(APP) STAN | | K(C) STAN | |
| | | | | WIDTH (IN) | THICK (IN) | (IN) | (IN) | (KSI) | (KSI) | (KSI) | (KSI) | (KSI) | (KSI) | MEAN (KSI) | DEV (KSI) | MEAN (KSI) | DEV (KSI) |
| | W | B | 2A(F) | 2A(F) | S(D) | S(MAX) | | | | | | | | | | | |
| BUCKLING OF CRACK EDGES RESTRAINED | | | | | | | | | | | | | | | | | |
| SRH1050 | S | 0.03 | 63 L-T | 174.5 | 24.040 | 0.025 | 3.990 | --- | 72.60 | 231.63 | --- | --- | --- | --- | --- | --- | 1964 57573 |
| SRH1050 | S | 0.03 | R.T. L-T | 174.5 | 7.990 | 0.025 | 2.010 | --- | 118.10 | 218.44* | --- | --- | --- | --- | --- | --- | 1964 57573 |
| SRH1050 | S | 0.03 | R.T. L-T | 174.5 | 24.020 | 0.025 | 3.000 | --- | 95.90 | 210.21 | --- | --- | --- | --- | --- | --- | 1964 57573 |
| | | 0.03 | | 174.5 | 24.030 | 0.025 | 6.000 | --- | 72.40 | 231.22 | --- | --- | --- | --- | --- | --- | 1964 57573 |
| | | 0.03 | | 174.5 | 24.040 | 0.025 | 6.000 | --- | 71.90 | 229.61 | 223.7/11.7 | --- | --- | --- | --- | --- | 1964 57573 |
| SRH1050 | S | 0.05 | R.T. L-T | 196.6 | 24.010 | 0.050 | 6.000 | --- | 92.10 | 294.15 | --- | --- | --- | --- | --- | --- | 1964 57573 |
| SRH1050 | S | 0.09 | R.T. L-T | 197.4 | 24.100 | 0.093 | 6.000 | --- | 115.70 | 369.42 | --- | --- | --- | --- | --- | --- | 1964 57573 |

*NOTE- NET SECTION STRESS EXCEEDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

Figure 1.10. Format for Plane Stress Fracture Toughness Data; Example Taken from Table 3.9.2.1, PH14-8Mo Stainless Steel Alloy.

1.5.3 R-Curve Data

The format for resistance curve (R-Curve) data is shown in Figure 1.11. The information listed at the top of the page includes the material type, the alloy, the condition/heat treatment, the product form, and the thickness if known, the specimen type and orientation, the specimen dimensions, thickness and width, the K_{Ic} value, if known, and the reference number. Unless otherwise specified, the data were taken at room temperature in laboratory air environments. Only one specimen is illustrated per figure, and the figures are sorted by alloy, condition/heat treatment, test temperature and environment, orientation and specimen thickness and width.

The resistance curve data are plotted on linear scales; K_R , the applied stress intensity, as a function of Δa_{eff} , the change in effective crack length (see Chapter 2 for the details associated with the calculation). There are two possible scales for the data; (1) the vertical scale ranging from 0 to 120 Ksi $\sqrt{in.}$ and horizontal scale ranging between 0.0 to 1.1 inches, and (2) the vertical scale ranging from 0.0 to 240 Ksi $\sqrt{in.}$ and the horizontal scale ranging between 0.0 and 3.3 inches. These two scales were chosen to accommodate all the data.

1.6 ALLOY SUBCRITICAL CRACK GROWTH SUBSECTION FORMATS

The subcritical crack growth data follow the fracture toughness data within each alloy section. The subcritical crack growth data includes: fatigue crack growth rate data, sustained load crack growth rate data, and stress corrosion cracking threshold data.

1.6.1 Fatigue Crack Growth Rate Data

The fatigue crack growth rate data are presented in two complementary formats - a graphical format and a mean trend tabular format. Figure 1.12 represents the graphical format which was chosen to present fatigue crack growth rate data. Basic information common to all data on a particular page is listed at the top of the page in the header section. Below

CONDITION/HT: T351
FORM: .19" TH SHEET
SPECIMEN TYPE: CCP
ORIENTATION: L-T

SPECIMEN THK: .181"
SPECIMEN WIDTH: 11.988"
 K_{IC} (Ksi \sqrt{in}):
REFERENCE: DA001

ALUM.
ALLOY

2024

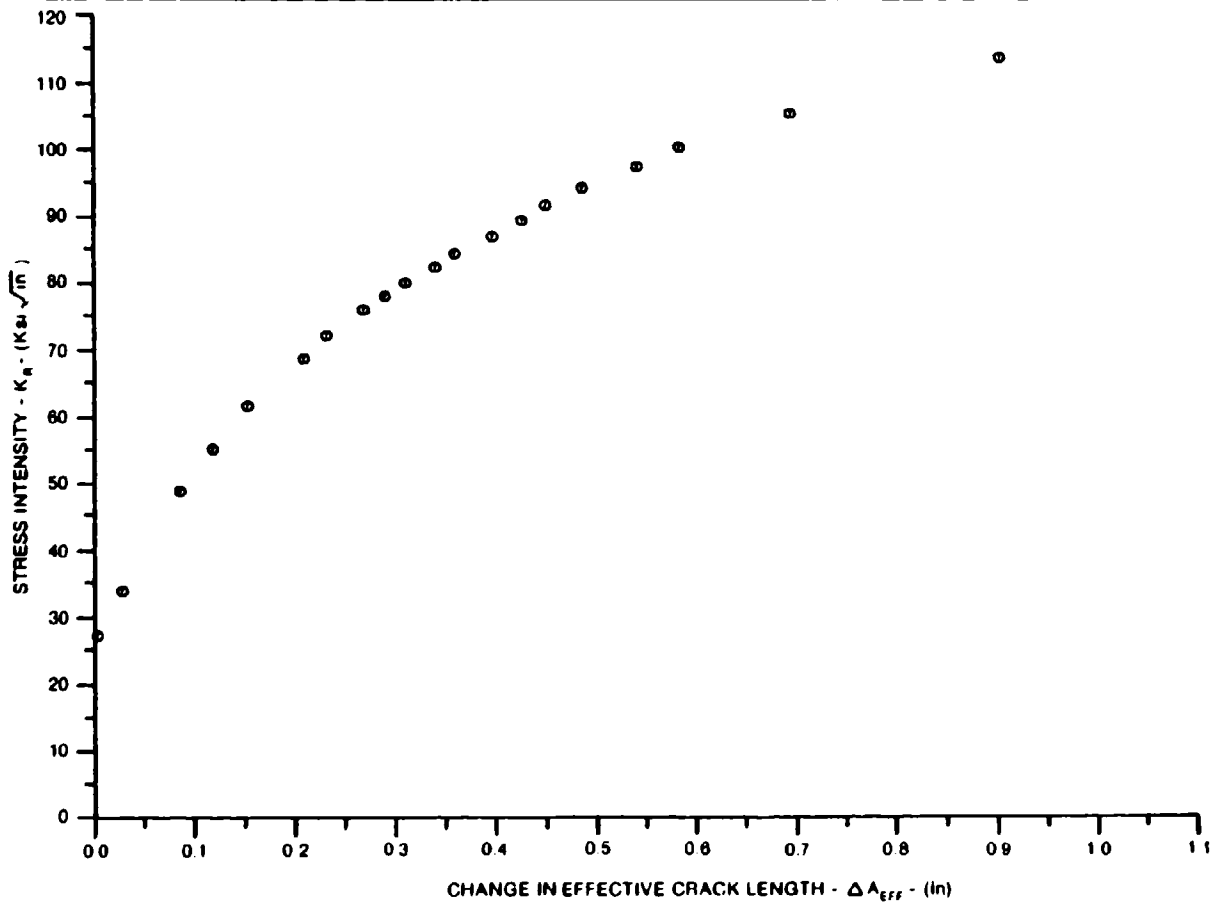


Figure 1.11. Format for Resistance Curve (R-Curve) Data.
Example Taken from Figure 7.5.2.6, 2024
Aluminum Alloy.

CONDITION/HT: H1800
 FORM: 1.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.0 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 218.0 KSI
 ULT. STRENGTH: 222.6 KSI
 SPECIMEN THK: 0.489- 0.504"
 SPECIMEN WIDTH: 3.982- 4.117"
 REFERENCES: G0009

STAIN.
 STEEL

PH13-8MO

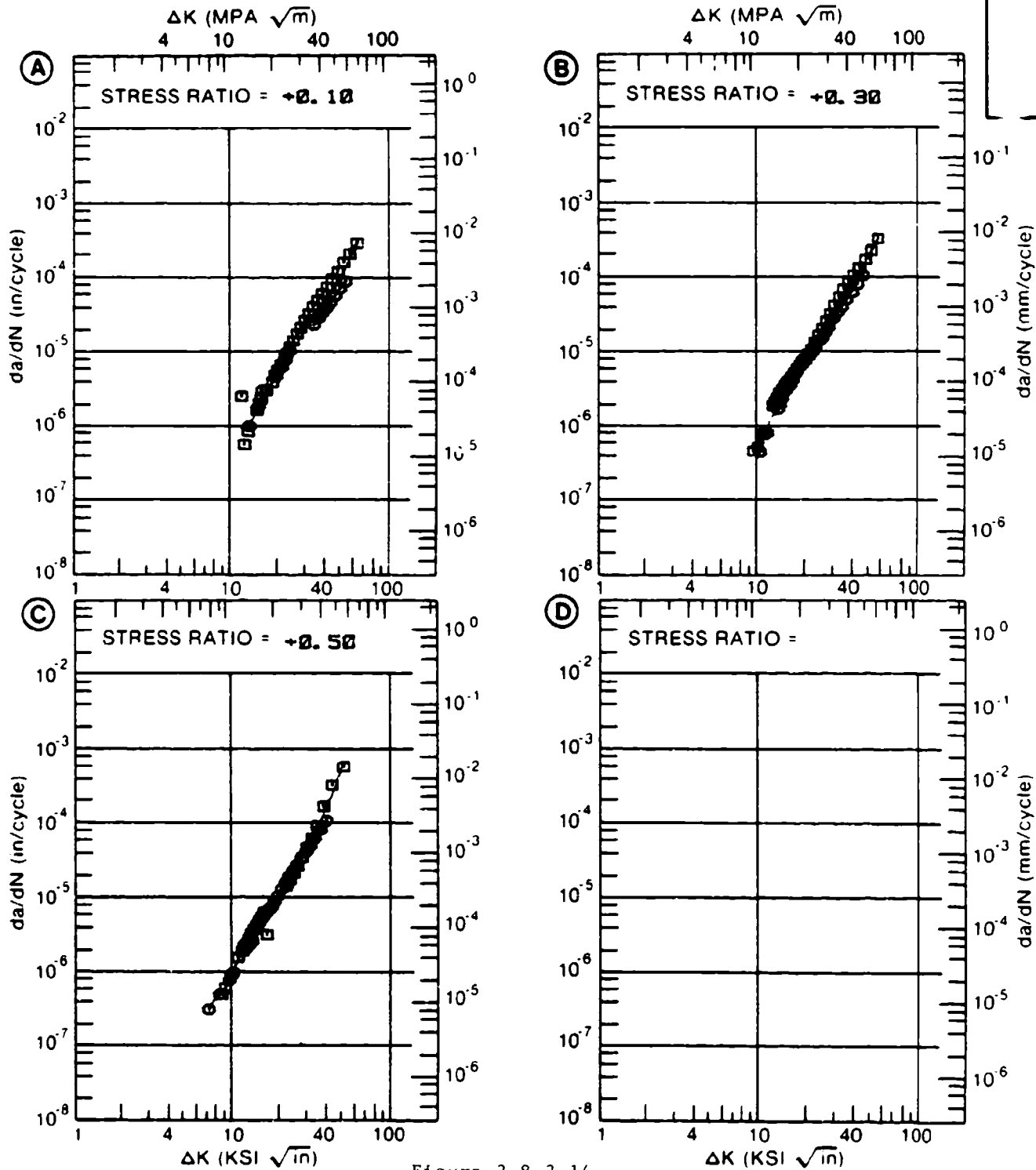


Figure 3.8.3.14

Figure 1.12. Graphical Format of the Fatigue Crack Growth Rate Data; Example Taken from Figure 3.8.3.14 Based on Stainless Steel Alloy PH13-8Mo Showing Effect of Stress Ratio.

the header section, there are four separate graphs on which the data are plotted. Each graph contains only data taken under identical conditions. Data are presented in each of the different graphs to show trends in behavior. The data on a page may describe the effects of one of three parameters: stress ratio, temperature/environment, and frequency. In order to accommodate these three variations, the header data at the top is slightly varied and the parameter being varied (e.g. stress ratio) is listed at the top of each of the active graphs as shown in Figure 1.12.

The header information at the top includes the material and alloy identifications listed in the small boxes in the upper right hand corner of each page for ease in locating the data. The condition/heat treatment is then listed at the top of the header. Below this, test and material parameters are listed in two columns; the first column listing the product form and product thickness, specimen type, specimen orientation and the two of the three parameters (i.e., stress ratio, test temperature/environment, frequency) not being varied on that particular page. The second column lists the room temperature tensile yield and ultimate strengths, the specimen dimensions of thickness and width, and the reference numbers identifying the data source.

All data are plotted as fatigue crack growth rate (da/dN) as a function of the range in the stress intensity factor (ΔK). The graphs are equal sized log-log plots ranging from 10^{-8} to 10^{-1} inches/cycle for the growth rates (i.e., seven decades), and from 1 to 200 Ksi $\sqrt{\text{in}}$ for values of ΔK . The definition of ΔK according to ASTM Standard E647 was chosen for data presentation throughout the handbook, i.e., ΔK = the maximum stress-intensity factor if the stress ratio is negative ($R \leq 0$). For other details, see Chapter 2.

English units, i.e., inches/cycle for growth rates and Ksi $\sqrt{\text{in.}}$ for ΔK , are listed to the left and the bottom of each page. Metric units, i.e., millimeters/cycle for growth rate values and megapascals $\sqrt{\text{m}}$ for ΔK , are listed at the top and right of each page.

By reviewing Figure 1.12, it can be noted that there are two different data symbols utilized in each graph. The two different symbols represent data from two different tests. Up to twenty different tests can be accommodated with the symbols defined in Table 1.11. Each graph, however, is restricted to a maximum of 300 da/dN- ΔK points; if the amount of data greatly exceeded these values, the data were separated onto two plots and the variable listed in each of the graphs is exactly the same. Mean trend curves have been established for each data set and can be seen going through the data on most of the graphs. The mean trend was developed using a cubic spline polynomial with the ability to control some aspects of the curve fit. The method is described in detail in Chapter 2. Fatigue crack growth rate data containing less than eight data points are plotted but mean trend curves were not established for these data.

Fatigue crack growth rate data are sorted slightly differently than fracture toughness data. Within a particular alloy, the data are sorted first by condition/heat treatment (using the order discussed in Table 1.3) then by product form and thickness with the order for product form defined as in Table 1.12. The product form order was altered to keep the data on forged and extruded bars near the data for forgings and extrusions, respectively. The sort on product thickness after product form is by increasing thickness. The next sort is by specimen orientation using the order defined by Table 1.3 and is followed by a sort by type of plot.

TABLE 1.11

LIST OF POSSIBLE SYMBOLS USED FOR EACH SPECIMEN
IN THE GRAPHICAL PRESENTATION OF THE FATIGUE
CRACK GROWTH RATE DATA

| <u>Test Order No.</u> | <u>Symbol</u> | <u>Test Order No.</u> | <u>Symbol</u> |
|---------------------------|---------------|---------------------------|---------------|
| 1 | ⊞ | 11 | ✕ |
| 2 | ⊙ | 12 | ✖ |
| 3 | ▲ | 13 | ✗ |
| 4 | + | 14 | ! |
| 5 | × | 15 | • |
| 6 | ◆ | 16 | ◆ |
| 7 | ↑ | 17 | ■ |
| 8 | ✕ | 18 | • |
| 9 | z | 19 | ★ |
| 10 | ∨ | 20 | - |

TABLE 1.12

ALTERNATE PRODUCT FORM SORTING ORDER
FOR CRACK PROPAGATION DATA

Sheet
Plate
Bar
Billet
Disk
Extrusion
Extruded Bars
Forgings
Forged Bars
Rolled Bars
Round Bars
Castings
Weldments

In the final series of sorts, the data are ordered so that all the pages where the data varies on stress ratio are placed before the data that varies on test temperature/environment; these data are placed before any data which varies on frequency. When there are a number of stress ratio plots, within these data sets, the data are sorted by test temperature/environment using the order listed in Table 1.9. If there are a number of stress ratio plots which also have the same test temperature/environment, then the final sort is in order of decreasing frequency. Within the group of test temperature/environment plots that follow the stress ratio plots, these are also sorted additionally by increasing stress ratio then further by decreasing frequency if necessary. Within the group of frequency plots, which follow the temperature/environment plots, the data are further subdivided by increasing stress ratio and then by the test temperature/environment sort of Table 1.9 if necessary. The above organizational scheme was established for easy comparison of data and to define the effects that defined variables had on crack growth rate. For other types of comparisons, it may be necessary to search through a subsection to find all the data of interest.

As stated earlier, in addition to the graphical presentation there also exists a tabular format of the mean trend values. This format is presented in Figure 1.13. The tabular format and the graphical format will be presented side-by-side in the handbook with the tabular format on the left and the graphical format on the right. Figure 1.13 is the tabular format of the data presented in Figure 1.12. Note that the Table and Figure numbers are identical.

On examination of Figure 1.13, one can see that the Table can be broken up into six sections. These sections are identified as: (1) the header section, (2) the maximum ΔK - da/dN values section, (3) the mean trend fatigue crack growth rate values at the specified values of ΔK section, (4) the maximum ΔK - da/dN values section, (5) the root mean square percent error (RMSPE) section, and (6) the life prediction ratio section.

Section 1, the header section, does not include all the header information that is listed on the graphical format. Here only the material, alloy, condition/heat treatment and environment (if it is a stress ratio plot) are listed. Beneath the fatigue crack growth rate data header are the axes labels ΔK (Delta K) and da/dN . The letters A, B, C, and D, under the da/dN label, correspond to the same identifying letters on the four plots on the graphical format. Below these letters are the abbreviations of E for Environment, R for Stress Ratio, and F for Frequency which identifies the variable for this particular data set. Following these abbreviations are the values of the variables for this data.

Section 2 lists the minimum ΔK values to the left and the corresponding da/dN values in the appropriate column. These points present the slowest crack growth rate on the mean trend curves shown in Figure 1.12.

Section 3 lists the mean trend values. The ΔK values are listed to the left and the da/dN values are listed for each curve to the right in the appropriate column. However, the ΔK values are now fixed values and the growth rates in the columns correspond to these ΔK values for the individual graphs. There are 28 possible ΔK values ranging from 1 to 200 ksi $\sqrt{\text{in}}$; the specific values utilized are 1.0, 1.3, 1.6, 2.0, 2.5, 3.0, 4.0, 5.0, 6.0, 7.0, 8.0, 9.0, 10.0, 13.0, 16.0, 20.0, 25.0, 30.0, 40.0, 50.0, 60.0, 70.0, 80.0, 90.0, 100.0, 130.0, 160.0, and 200.0 Ksi $\sqrt{\text{in}}$.

Note that in Figure 1.13 all 28 ΔK values are not listed, only those in which there was a mean trend data available for at least one of the graphs. This means that in this case (Figure 1.12) all ΔK values less than 7.0 and greater than 60.0 Ksi $\sqrt{\text{in}}$ are not included since none of the curves had data outside this range.

Table 3.8.3.14

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.14 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T., H. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10***-6 IN./CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | |
| MIN | A: 11.42 | .928 | | | |
| | B: 9.13 | | .466 | | |
| | C: 6.87 | | | .299 | |
| | D: | | | | |
| | 7.00 | | | .342 | |
| | 8.00 | | | .468 | |
| | 9.00 | | | .625 | |
| | 10.00 | | .543 | 1.08 | |
| | 13.00 | 1.09 | 2.16 | 3.06 | |
| | 16.00 | 2.57 | 4.48 | 5.84 | |
| | 20.00 | 6.71 | 9.37 | 11.6 | |
| | 25.00 | 15.3 | 19.2 | 24.3 | |
| | 30.00 | 26.6 | 34.6 | 47.9 | |
| | 35.00 | 38.7 | 58.0 | 91.9 | |
| | 40.00 | 52.4 | 92.8 | 174. | |
| | 50.00 | 108. | 215. | 607. | |
| | 60.00 | 259. | | | |
| MAX | A: 62.14 | 303. | | | |
| | B: 56.12 | | 339. | | |
| | C: 50.46 | | | 643. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 33.16 | 14.35 | 12.25 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | 1 | 2 | |
| SUMMARY | 1.25-2.0 | | 1 | | |
| (NP/NA) | >2.0 | | | | |

Figure 1.13. Tabular Format for Fatigue Crack Growth Rate Data; Tabular Data Corresponds to Graphical Data Shown in Figure 1.12. Example Taken from Table 3.8.3.14, PH 13-8Mo Stainless Steel Alloy.

Section 4 identifies the maximum (highest) $\Delta K - da/dN$ point on the mean trend curve in a manner similar to Section 2 which identified the lowest point on the curve.

Section 5, entitled "The Root Mean Square Percent Error" (RMSPE), is basically a description of scatter about the mean trend line; that is, a smaller value indicates a smaller scatter than a larger one. The calculation of this value is described in Chapter 2.

Section 6 presents life prediction information in terms of life prediction ratios. The life prediction ratio (LPR) is the number of cycles predicted (using the mean trend curve) divided by the actual number of cycles taken from the experimental crack length versus cycle data for a predefined interval. The actual LPR values are not listed but the results are summarized. The data summary is divided into five ranges, that is LPR's from: (1) 0.0-0.5, (2) 0.5-0.8, (3) 0.8-1.25, (4) 1.25-2.0, and (5) above 2.0. The numeric values in the columns across from the LPR range represents the number of specimens that had LPR's in that particular range. Because some data were received in reduced form only, i.e., (ΔK , da/dN) only, not all of the test specimens shown on the graphs will have LPR's, i.e., raw crack length versus cycle count data was not available for comparison. The LPR's generally were found to be in the center range, indicating an adequate mean trend fit of the data. For threshold type tests and for tests in which the loads were varied frequently through the test, LPR's tended to be outside this range.

1.6.2 Sustained Load Crack Growth Rate

The sustained load crack growth rate data are presented subsequent to the fatigue crack growth rate data and are plotted on log-log plots in a manner similar to the FCGR data (See Figure 1.14). Tabular mean trend formats are also presented where sufficient data exists (See Figure 1.15). The data are

CONDITION/HT: AUSTENITIZED AT 2010F, QUENCHED & TEMPERED AT 810F
 FORM: 0.00" TH SHEET
 SPECIMEN TYPE:
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A₀):
 K_{ISCC}:
 REFERENCES: 95544

STAIN.
 STEEL

AFC 77

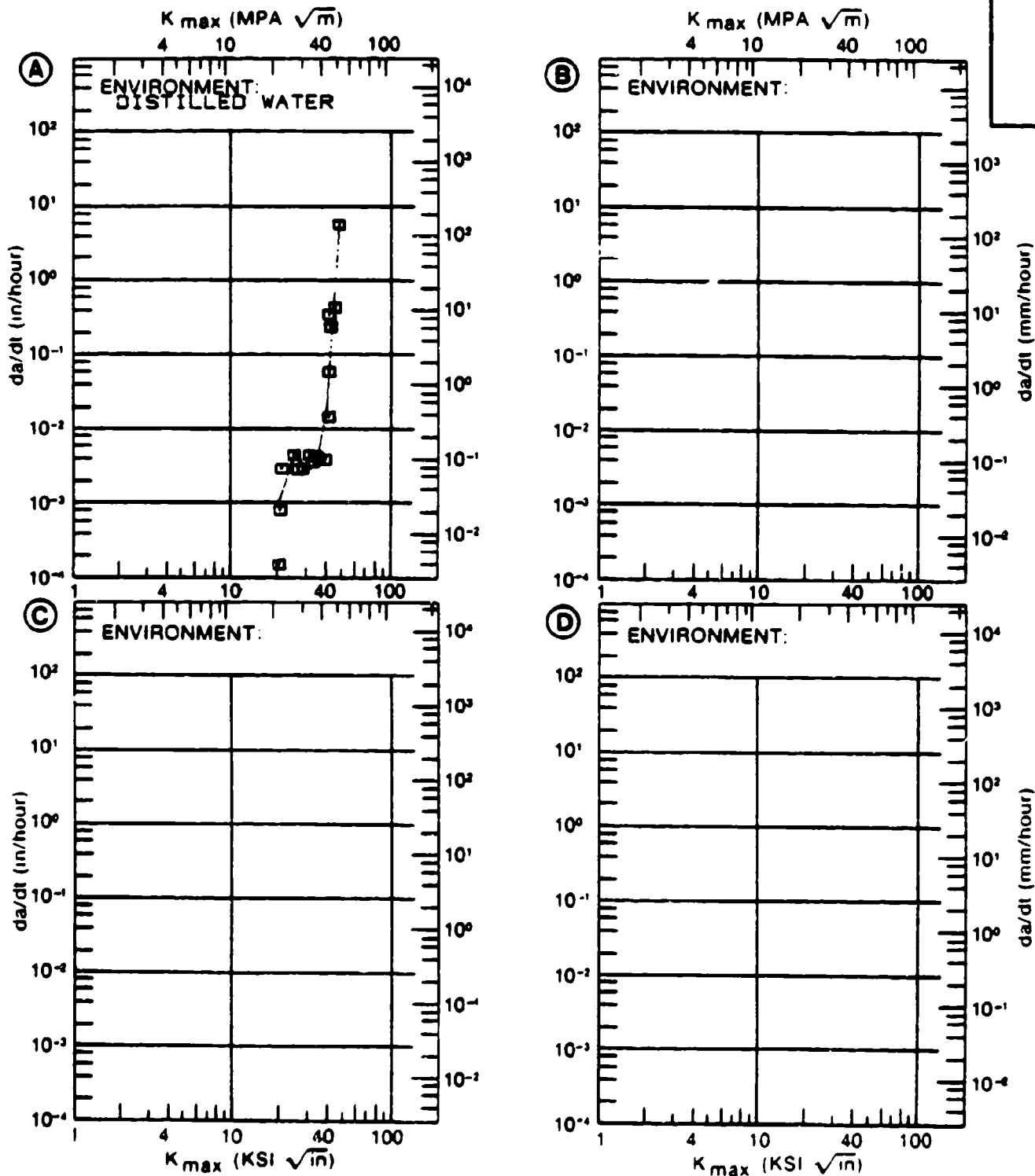


Figure 3.2.3.1

Figure 1.14. Graphical Format for Sustained Load Crack Growth Rate Data. Example Taken from Figure 3.2.3.1, AFC 77 Alloy Stainless Steel.

TABLE 3.2.3.1

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.2.3.1 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL AFC 77
CONDITION: AUSTENITIZED AT 2010F, QUENCHED & TEMPERED AT 810F

| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
|------------------------|----------|------------------------|---|---|---|
| | | A | B | C | D |
| | | E = DISTILLED WATER | | | |
| K MAX MIN | A: 20.00 | 1.01 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | 4.55 | | | |
| | 30.00 | 2.67 | | | |
| | 35.00 | 3.21 | | | |
| | 40.00 | 17.5 | | | |
| K MAX MAX | A: 47.00 | 5213. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 62.42 | | | |
| PERCENT ERROR | | | | | |

Figure 1.15. Tabular Format of Sustained Load Crack Growth Rate Data. Example Taken from Table 3.2.3.1, AFC 77 Stainless Steel Alloy.

plotted to present time based crack growth rate as a function of maximum stress-intensity factors on pages with header sections and four graphs of equal size with both English and Metric units lining the sides. Again, the header information includes the material and the alloy in the small boxes in the upper right hand corner of the pages. The condition/heat treatment is listed at the very top and the rest of the parameters are listed in two columns beneath the condition. The first column contains the parameters of form, form thickness, specimen type, specimen orientation, and test temperature/environment, while the second column contains the tensile yield strength, specimen thickness and width, initial crack length (a_0), stress corrosion cracking threshold values, K_{Isc} , and the reference numbers. As before, there are also three variations on these plots, that is, variations on form and form thickness, tensile yield strength, and test temperature/environment. There are also some data sets in which condition/heat treatment for a given alloy is varied; these variations were manually designated on the plots. In addition to the three basic plot variations noted, the sustained load crack growth rate data have two possible growth rate axes. In order to accommodate the data, the two sets of axes chosen were 10^{-6} to 10^0 inches/hr. and 10^{-4} to 10^2 inches/hour (English units). Both have maximum stress-intensity values that range from 1 to 200 Ksi $\sqrt{\text{in}}$.

Some of these data also have mean trend curves and mean trend tables associated with them. The mean trend tables are again presented directly opposite to the graphical presentation of the data, similar to that done for the fatigue crack growth rate data. Figure 1.15 is the tabular format of the data in Figure 1.14. The format of this table is similar to the fatigue crack growth rate data, so little further explanation is warranted. All of these data were received in reduced form, and therefore, no LPR's are given; due to the nature of the data, the values of the RMSPE are usually larger than for the FCGR data. Additionally, mean trend curves representative of the data were not always created; for these cases, no mean trend curve or table is presented.

1.6.3 Stress Corrosion Cracking Threshold

Following the sustained load crack growth rate data is the tabular stress corrosion cracking threshold data. An example of this data format is presented in Figure 1.16, which is similar to the fracture toughness data format. The material, alloy and data type are listed at the top of the sheet. To the left, the condition/heat treatment is listed, then product form, product thickness, test temperature, specimen orientation, yield strength, and environment. Following these parameters are the specimen thickness, width and design as well as crack length, fracture toughness, K_{ISCC} individual values, mean values, standard deviations, test times, dates and reference numbers.

The data are sorted according to (material, alloy) condition/heat treatment, product form, test temperature, specimen orientation and environment. The order of the sorts are identified in Table 1.3 except for environment which is sorted by the utility sort, i.e., by a sort similar to that for alloy and condition/heat treatment.

The fracture toughness values presented, $K(Q)$, only indicate the level of crack toughness of the material; these values were obtained from the threshold tests and are not valid plane-strain fracture toughness values. The $K(Q)$ values, however, should provide an engineer with an indication of stress-corrosion cracking sensitivity relative to fracture.

In the K_{ISCC} tabular data, there are two columns in which asterisks (*) may appear; the column on specimen design and the column on K_{ISCC} . All asterisks that appear in the specimen design column indicate that the specimen has been side-grooved along the path of the crack; note (* = SG) at the top of the column. The asterisks that appear in the K_{ISCC} column behind the individual K_{ISCC} values indicate that the crack length and/or specimen thickness were not greater than $2.5 (K_{ISCC}/\sigma_{ys})^2$, as noted at the bottom of the page.

Table 3.2.3.2

| STAINLESS STEEL AFC 77 | | K (ISCC) | | | | | | | | | | |
|--|--------------------------------------|-----------------------------|-----------------------|---------------|---------------|---------------|------------------------------|---------------------------|-------------|-------------|-----------------------|---------------|
| CONDITION | --PRODUCT-- FORM THICK OR (IN) | TEST SPEC TEMP OR (F) | YIELD STR (KSI) | ENVIRONMENT | SPECIMEN | | CRACK LENGTH K(G) (IN) | K (ISCC) (KSI*SQRT IN) | MEAN DEV | STAN DEV | TEST TIME (MIN) | DATE REFER |
| | | | | | WIDTH (IN) | THICK (IN) | | | | | | |
| | | | | | A | B | | | | | | |
| 1800F 1HR DQ, P -100F 0.5HR, 500F 2+2 HR (COARSE GRAINED STRUCTURE) | 0.56 | R.T. | 154.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 119.00 | 92.00* | | | 1969 74720 |
| 1800F 1HR DQ, P -100F 0.5HR, 1000F 2+2 HR (COARSE GRAINED STRUCTURE) | 0.56 | R.T. | 173.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 25.00 | 15.00 | | | 1969 74720 |
| 1800F 1HR DQ, P -100F 0.5HR, 500F 2+2 HR (FINE GRAINED STRUCTURE) | 0.56 | R.T. | 196.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 111.00 | 97.00* | | | 1969 74720 |
| 1800F 1HR DQ, P -100F 0.5HR, 1000F 2+2 HR (FINE GRAINED STRUCTURE) | 0.56 | R.T. | 232.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 30.00 | 20.00 | | | 1969 74720 |
| 2000F 1HR DQ, B -100F 0.5HR 1400F 2+2 HR | 3.00 | R.T. | 150.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 116.00 | 80.00* | | | 1969 76136 |
| 2000F 1HR DQ, B -100F 0.5HR 500F 2+2HR | 3.00 | R.T. | 169.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 200.00 | 105.00* | | | 1969 76136 |
| 2000F 1HR DQ, B -100F 0.5HR 700F 2+2 HR | 3.00 | R.T. | 180.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 160.00 | 50.00 | | | 1969 76136 |
| 2000F 1HR DQ, B -100F 0.5HR 800F 2+2 HR | 3.00 | R.T. | 207.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 70.00 | 40.00 | | | 1969 76136 |
| 2000F 1HR DQ, B -100F 0.5HR 900F 2+2 HR | 3.00 | R.T. | 214.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 56.00 | 35.00 | | | 1969 76136 |
| 2000F 1HR DQ, B -100F 0.5HR 1100F 2+2 HR | 3.00 | R.T. | 221.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 43.00 | 10.00 | | | 1969 76136 |

*Note - Data which do not meet minimum specimen thickness requirements of 2.5(KISCC/TYS) squared.

+Note - (*=SG) in design column implies that Asterisked specimens are side-grooved (SG).

Figure 1.16. Format for Stress Corrosion Cracking Threshold Data; Example Taken from Table 3.2.3.2, AFC 77 Stainless Steel Alloy.

Greater than (>) and less than (<) signs before the K_{ISCC} value indicates that the actual value is either greater than or less than the value stated, respectively. Data containing these signs were considered to be informative since little data exists and so were included; however, the data were not considered definitive and so were excluded from mean and standard deviation values.

CHAPTER 2
METHODS OF CALCULATIONS

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METHODS OF CALCULATIONS

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CHAPTER 2
METHODS OF CALCULATIONS

2.0 OVERVIEW

This chapter briefly describes the methods used to calculate the damage tolerant properties reported in the Handbook. The properties reported for characterizing fracture resistance include:

- K_{IC} , the plane-strain fracture toughness
- K_C , the critical plane-stress (or transitional) fracture toughness
- K_{App} , the apparent plane-stress fracture toughness
- K_R , the tearing resistance

and, the properties reported for characterizing subcritical crack growth resistance include:

- $\frac{da}{dN}$, the constant amplitude fatigue crack growth rate
- $\frac{da}{dt}$, the sustained-load crack growth rate
- K_{Isc} , the threshold for sustained load cracking

Sections 2.1 through 2.7 describe these properties and the specific methods of calculations utilized to convert laboratory (specimen) data into the properties reported.

2.0.1 Data Review and Acceptance Criteria

Newly acquired data and data available from previous revisions of the Handbook were systematically reviewed and analyzed. The principal data acceptance criteria were based on criteria established by the American Society for Testing and Materials (ASTM); these criteria are embedded within ASTM standards for test methods and practices. Table 2.1 lists those standards used to provide criteria for plane-strain fracture toughness (K_{IC}) data, for R-curve data, and for fatigue crack growth rate (da/dN) data. ASTM literature

TABLE 2.1
APPLICABLE LIST OF STANDARDS FOUND IN PART 10,
THE ASTM BOOK OF STANDARDS (1982)

| <u>ASTM STD</u> | <u>TITLE</u> |
|-----------------|--|
| E616-81 | Standard Terminology Relating to Fracture Testing |
| E399-81 | Test Method for Plane-Strain Fracture Toughness of Metallic Materials |
| E561-81 | Practice for R-Curve Determination |
| E647-81 | Test Method for Constant-Load-Amplitude Fatigue Crack Growth Rates Above 10^{-8} m/Cycle |

was also reviewed to establish criteria based on typical engineering practice for the other types of data collected and reported.

Newly acquired data was substantially easier to process than the data available from previous revisions since the data suppliers screened their data according to ASTM criteria before it was released to the data processing organization (UDRI). Also, when questions concerning newly acquired data developed, the suppliers could be called and the questions resolved.

For the case of previously available Handbook data, it was necessary to systematically review the data employing a multi-step process. First, the computer compatible input data (computer cards) supplied to UDRI by MCIC were compared to the data reported in the 1975 revision of the Handbook. When discrepancies between variables (such as stress ratio, frequency, specimen direction, etc) were found, they were marked with an asterisk on the card image data so that the differences could be investigated further. One means of settling the discrepancy was through use of the second step in the process whereby the data were compared to the original reference. Since the data on the computer cards listed the specimen identification number, the original data was normally found with relative ease and comparisons made. Every attempt was made to consult the original references and verify the accuracy of these available data. As with newly acquired data, available data were also reviewed relative to applicable ASTM criteria prior to being identified as candidate data for the 1983 revision.

The final step in the review process was the determination of whether the data were a "true" representation of the behavior they described. This step was implemented for both newly acquired data as well as for the available Handbook data in order to eliminate suspect data through subjective criteria. Unfortunately, it is not possible to detail the subjective criteria that were employed to exclude questionable data. It can be stated that the principal mode of operation here was by way of comparison between behaviors that were expected to be somewhat similar.

2.0.2 Fracture Mechanics Basis

The damage tolerant data reported in this Handbook utilize the technology of linear elastic fracture mechanics. This technology is widely applied throughout the aerospace industry to relate structural calculations for cracked structures to material behavior in the presence of cracks. In essence, fracture mechanics provides a structural parameter, the stress-intensity factor (symbol K) which characterizes the magnitude of stresses and strains in the crack tip region of essentially elastic structures. It was postulated that the stress-intensity factor represents a similitude parameter that describes crack tip behavior under various loading conditions (monotonically increasing load, fatigue loading, etc.); the hypothesis has been verified for a wide number of materials, loading conditions, and failure type mechanisms. For a more thorough review of linear elastic fracture mechanics and its applications to the aerospace industry, see AFWAL-TR-82-3073, USAF Damage Tolerant Design Handbook: Guidelines for the Analysis and Design of Damage Tolerant Aircraft Structures.

Currently, there are developments that are extending the technology of fracture mechanics to aid in the solution of crack problems for which the assumptions of linear elastic fracture mechanics are invalid. This technology is referred to as nonlinear fracture mechanics and its similitude parameter is the J-integral (J), or alternately the crack tip opening displacement (δ). To date, nonlinear fracture mechanics has been successfully utilized to characterize tearing type fractures and fractures occurring in the presence of large-scale yielding. Some evidence has been presented suggesting that J may provide a similitude parameter for non-monotonically increasing type loadings, i.e., for fatigue loadings; but, questions still exist here. It is expected that subsequent revisions of this Handbook will include nonlinear fracture mechanics type data such as J_{IC} , a plane-strain fracture toughness property, and J_R -curves, (tearing resistance curves).

2.0.3 Test Specimen Geometries

As described above, the stress-intensity factor provides a parameter that can be used to establish similitude between two cracked structures. This means that if the stress-intensity factor in structure no. 1 equals the stress-intensity factor in structure no. 2 and if other conditions (loading, material, environment, etc) are the same, then the cracks in both structures will behave the same way. This concept provides the justification for conducting material behavior studies on small laboratory test specimens (coupons) which contain cracks. If the resistance to cracking in the laboratory can be optimized by a choice of material, then improved resistance can also be obtained for structural hardware (given that the material can be fabricated into the hardware without processing degradation taking place).

The types of test specimen geometries that have been employed to generate damage tolerance (fracture mechanics) type data for this Handbook are summarized in Table 2.2. Table 2.2 also guides the reader to individual figures (Figures 2.1 through 2.14) which describe the geometries associated with individual specimen names and symbols.

To relate the crack type data collected in a cracked test specimen to other cracked structures, it is necessary to have a description of the stress-intensity factor (K) as a function of crack length (a) for the test specimen geometry. Over the last fifteen years, a great deal of attention has been given to generating accurate stress-intensity factor equations for laboratory test specimen geometries, due to their importance to standard methods of test and to reporting data. The stress-intensity factor equations are typically presented in either of the following two forms:

$$K = \sigma \sqrt{\pi a} \cdot \beta$$

where σ = remote stress (load \div area) (2.1)
 a = crack length measure
 β = function of crack length and global geometry

or

$$K = \frac{P}{BW^{\frac{1}{2}}} Y \quad (2.2)$$

where

P = load

B = thickness of specimen

W = width of specimen

Y = function of crack length (a)
and global geometry

Equation 2.1 is used when the loading is applied remotely from the crack, whereas Equation 2.2 is more typically used for point loading or localized loading conditions. One should note that K is a linear function of loading (σ in Equation 2.1 and P in Equation 2.2) and that the loading and geometric components of the equations are independent of each other. Thus, if one wishes to describe a stress-intensity factor relationship for a given geometry, they might formulate the equations in the following forms:

$$\frac{K}{\sigma} = \sqrt{\pi a} \cdot \beta \quad (2.3)$$

or

$$\frac{\frac{K}{P}}{BW^{\frac{1}{2}}} = Y \quad (2.4)$$

Equations 2.3 and 2.4 are referred to as stress-intensity factor coefficients; the right hand side of these equations only describes the effect of the crack in the given geometry.

Table 2.3 provides a listing of stress-intensity factor coefficients which were used to generate data for this Handbook. Each equation is given a stress-intensity factor equation number, e.g. SIF.7 refers to the stress-intensity factor coefficient for the WOL (Wedge Opening Load) specimen geometry illustrated in Figure 2.6. Also note that Table 2.3 has a remarks section which describes the conditions under which individual equations were used.

TABLE 2.2
CORRELATION LISTING OF TEST SPECIMEN SYMBOL,
TEST SPECIMEN GEOMETRY, AND REFERENCE FIGURE NUMBER

| SYMBOL | TEST SPECIMEN | GEOMETRY DESCRIBED IN FIGURE NUMBER |
|--------|--------------------------------|--|
| CCP | Center Crack Panel | 2.1 |
| CT | Compact (Tension) | 2.2 |
| NB | Three Point Notched Bend | 2.3 |
| 4-NB | Four Point Notched Bend | 2.4 |
| CANT | Cantilever Beam | 2.5 |
| WOL | Wedge Opening Load | 2.6 |
| BWOL | Bolt Loaded WOL | 2.7 |
| SENT | Single Edge Notch Tension | 2.8 |
| PTSC | Part-Through Surface Crack | 2.9 |
| KB-BAR | K_B BAR | 2.10 |
| DCB | Double Cantilever Beam | 2.11 |
| BDCB | Bolt Loaded DCB | 2.12 |
| TDCB | Tapered Double Cantilever Beam | 2.13 |
| CNT | Center Notch Tension | 2.14 |

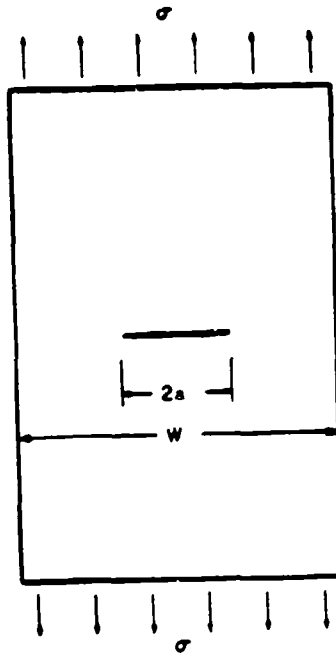


Figure 2.1. Center Cracked Panel (CCP) Specimen.

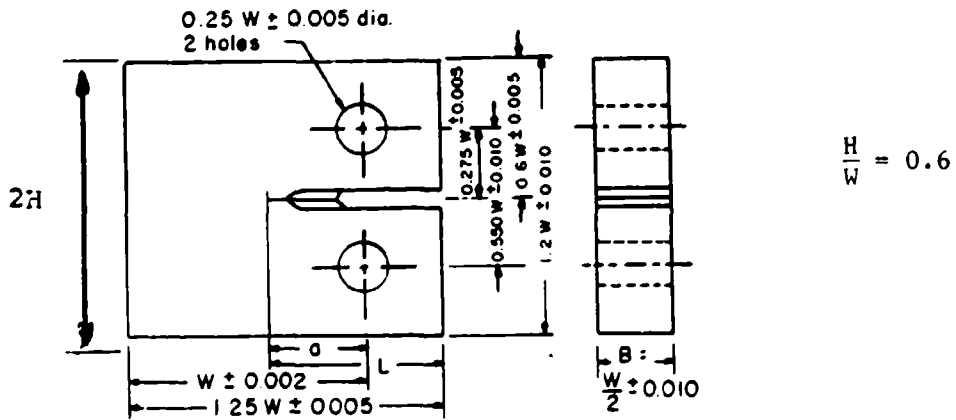


Figure 2.2. Compact Tension (CT) Specimen.

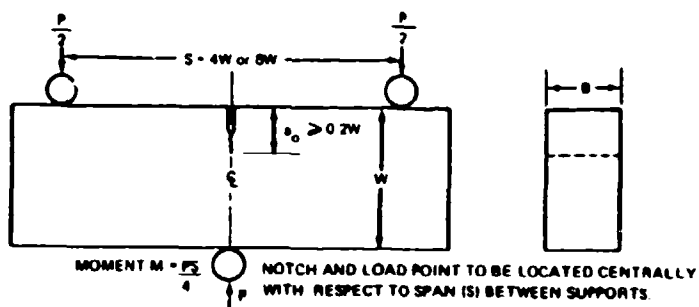


Figure 2.3. Three Point Notched Bend (NB) Specimen.

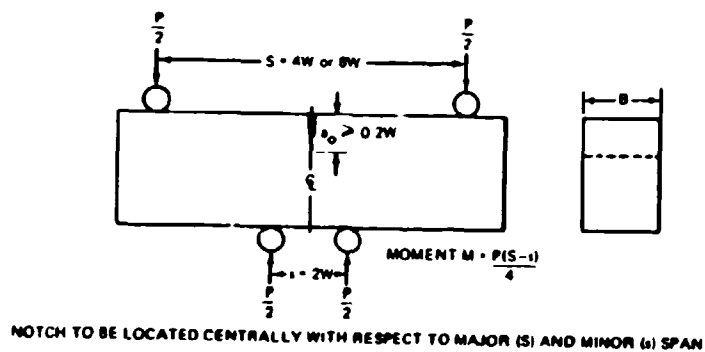


Figure 2.4. Four Point Notched Bend (4-NB) Specimen.

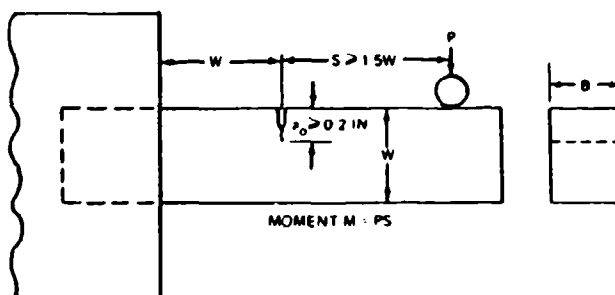
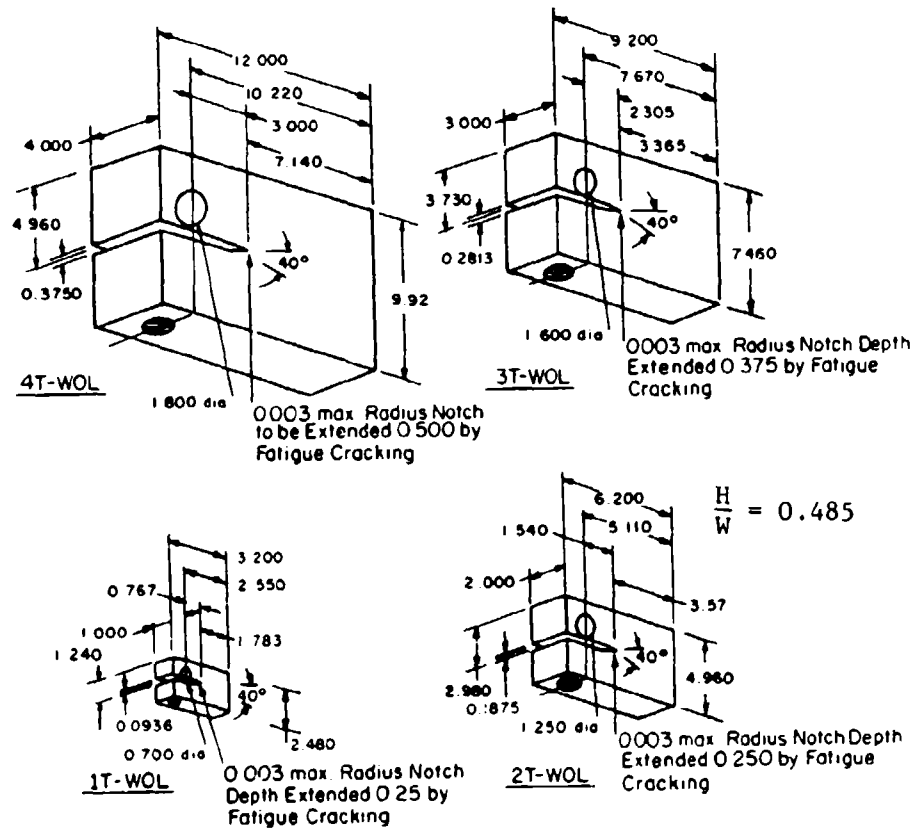


Figure 2.5. Cantilever Beam (CANT) Specimen.



Note.
All Dimensions are in Inches.

Figure 2.6. Dimensions of Several T Type Wedge Opening Load (WOL) Specimens.

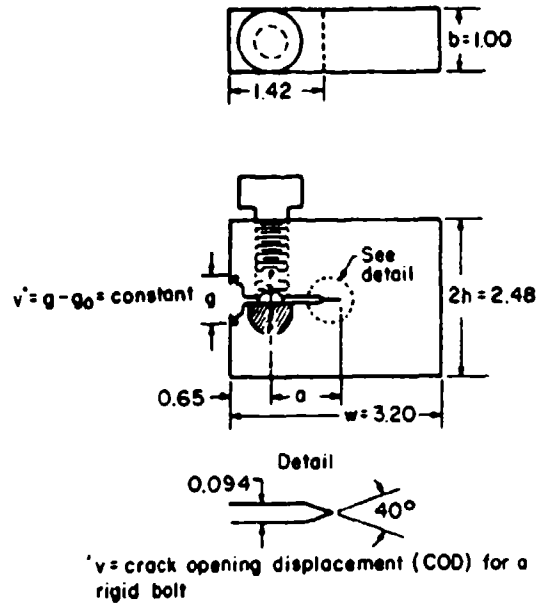


Figure 2.7 Modified 1-T WOL (BWOL) Specimen Used to Determine K_{Isc} by Bolt Loading.

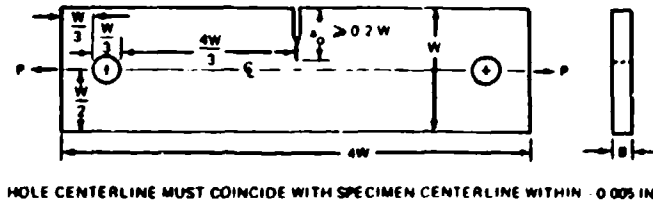


Figure 2.8. Single Edge Notch Tensile (SENT) Specimen.

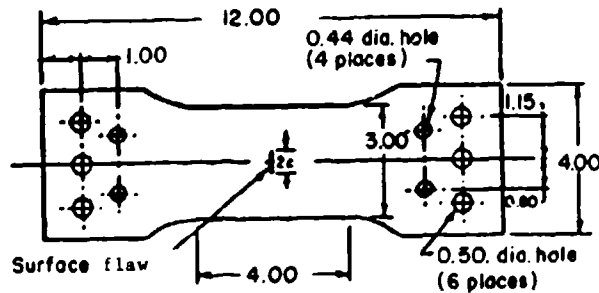
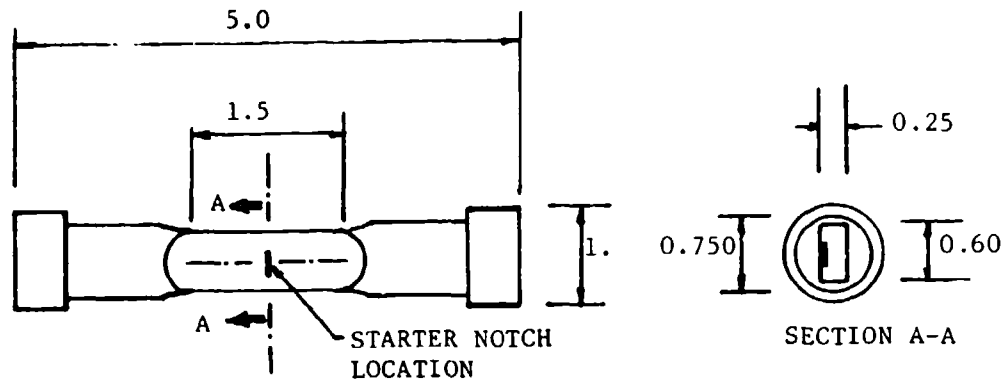


Figure 2.9. Typical Design for Part-Through-Surface-Crack (PTSC) Specimen.



ALL DIMENSIONS IN INCHES

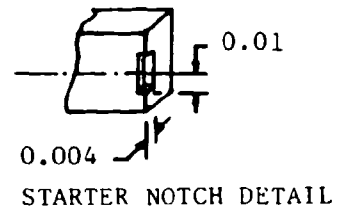


Figure 2.10. K_B Bar (KB-BAR) Specimen.

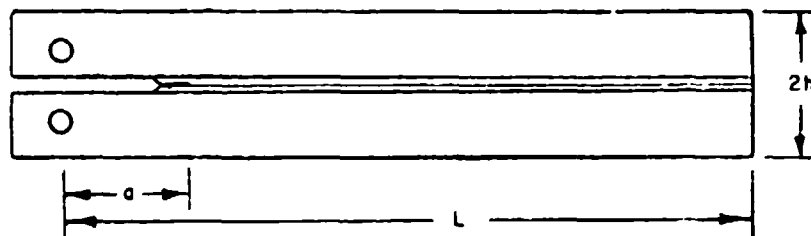


Figure 2.11. Double Cantilever Beam (DCB) Specimen with Side Grooves.

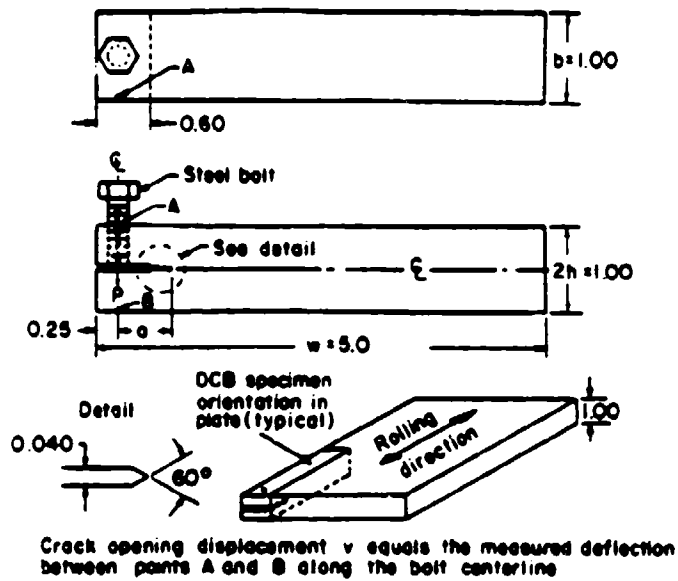


Figure 2.12. Bolt-Loaded Double Cantilever Beam (BDCB) Specimen.

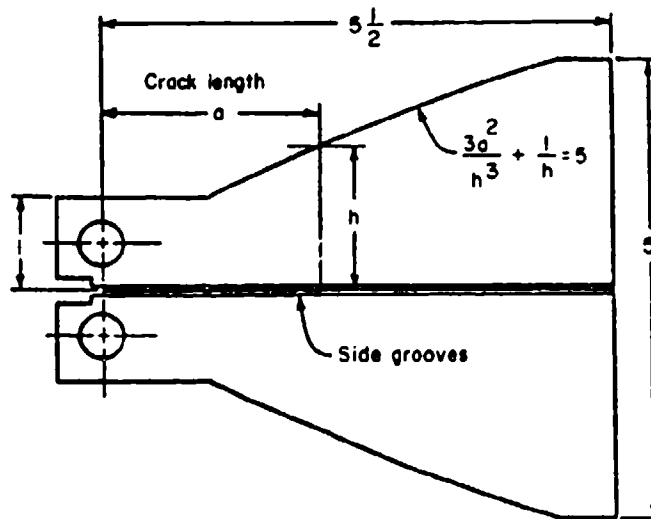


Figure 2.13. Typical Tapered Double Cantilever Beam (TDCB) Specimen with Side Grooves.

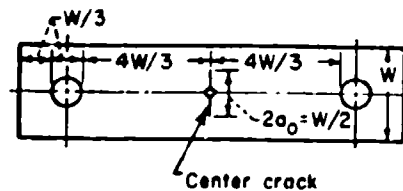


Figure 2.14. Center-Notch Tensile (CNT) Specimen.

TABLE 2.3

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

| TEST SPECIMEN GEOMETRY | STRESS-INTENSITY FACTOR COEFFICIENT | EQUATION NUMBER | REMARKS |
|---------------------------------------|--|-----------------|--|
| CCP (See Figure 2.1) | $\frac{K}{\sigma} = \sqrt{\pi a} \cdot (\text{Sec } \alpha a)^b$ $\alpha = a/W$ | SIF.1 | This equation was used whenever K was calculated for the CCP Specimen |
| CT (See Figure 2.2) | $\frac{K}{\sigma} = \frac{(2+a)}{8W^2} \cdot [0.866 + 4.64a - (2-a)^{3/2} - 13.32a^2 + 14.72a^3 - 5.6a^4]$ $\frac{a}{H} = \frac{a}{W}$ $\frac{H}{W} = 0.600$ | SIF.2 | This equation was used whenever K was calculated for data generated with the CT specimen; the equation is valid for $a/W > 0.2$ |
| CT (See Figure 2.2) | $\frac{K}{\sigma} = \frac{a^2}{8W^2} [29.6 - 185.5a + 655.7a^2 - 1017a^3 + 638.9a^4]$ $\alpha = a/W$ $\frac{H}{W} = 0.600$ | SIF.3 | This equation was used to calculate K for data incorporated into pre-1983 revisions. Reprocessed a vs N data utilized equation SIF.2 |
| NB (J PI BEND) (See Figure 2.3) | $\frac{K}{\sigma} = \frac{S a^2}{8W^2} [2.9 - 4.6a + 21.8a^2 - 37.6a^3 + 38.7a^4]$ $\alpha = a/W$ $S = \text{span length}$ | SIF.4 | No new data were processed from NB specimens. Previous data incorporated into the handbook utilized this equation. |

TABLE 2.3 (Continued)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

| TEST SPECIMEN GEOMETRY | STRESS-INTENSITY FACTOR COEFFICIENT | EQUATION NUMBER | REMARKS |
|------------------------|---|-----------------|---|
| 4-NB (4 PT BEND) | $\frac{K}{P} = \frac{3}{8W} \left[1.99 - 2.47a + 12.97a^2 - 23.17a^3 + 26.80a^4 \right]$ $u = a/W$ $M = P(S-s)/6, \text{ moment}$ $S, s = \text{major and minor span}$ | SIF.5 | No new data were processed from 4-NB specimens. Previous data incorporated into the handbook utilized this equation. s/W must be greater than 2. |
| (See Figure 2.4) | | | |
| CANT | $\frac{K}{P} = 4.12 \left[(1-a)^{3/2} - (1-a) \right]^{1/2}$ $u = a/W$ $M = P \times S, \text{ moment}$ | SIF.6 | No new data were processed from CANT specimens. Previous data incorporated into the handbook utilized this equation. |
| (See Figure 2.5) | | | |
| WOL | $\frac{K}{P} = \frac{(2+s)}{8W^{3/2}} \left[\begin{aligned} &0.8072 + 8.858s \\ &-30.23a^2 + 41.088a^3 \\ &-24.15a^4 + 4.951a^5 \end{aligned} \right]$ $u = a/W$ $M = 0.485$ | SIF.7 | All new a vs N data from WOL specimens with M = 0.485 were processed using this equation |
| (See Figure 2.6) | | | |
| BMOL | $\frac{K}{P} = \frac{3}{8W^{3/2}} \left[\begin{aligned} &30.96 - 195.8a + 730.6a^2 \\ &-1186.3a^3 + 754.6a^4 \end{aligned} \right]$ $u = a/W$ $B = \sqrt{B \cdot B_N}$ $B_N = \text{Net Thickness at Side Groove}$ | SIF.8 | Equation was used to calculate stress-intensity factors for both WOL and BMOL in prc-1983 revisions. No new BMOL raw data were received for processing. |
| (See Figure 2.7) | | | |

TABLE 2.3 (Continued)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN
GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

| | STRESS-INTENSITY FACTOR COEFFICIENT | EQUATION NUMBER | REMARKS |
|---------------------------------|---|--------------------|---|
| SENT (See Figure 2.8) | $\frac{K}{P} = \frac{1}{8W^{\frac{3}{2}}} [1.99 - 0.4124a + 18.70a^2 - 38.48a^3 + 53.85a^4]$ $u = a/W$ | SIF.9 | New da/dN data processed from SENT specimens utilized this equation. Previous data incorporated into handbook also utilized this equation. |
| PTSC (See Figure 2.9) | $\frac{K}{Q} = 1.1 \left(\frac{na}{Q} \right)^{\frac{1}{2}}$ <p>where for $(a/c) \leq 1$</p> $Q = 1.0 + 1.464 \left(\frac{a}{c} \right)^{1.65}$ <p>a = depth 2c = surface length</p> | SIF.10 | Equation was used to reduce a vs N data for PTSC specimens. Previous data incorporated into handbook also used a similar version of this equation. |
| KB bAK (See Figure 2.10) | <p>Equation used by Aircraft Engine Group of General Electric Company. Closely Approximates Newman and Raju Solution Presented in AFMAL-TR-82-3073</p> | SIF.11 | Used for da/dN testing. Data received was directly incorporated into the 1983 revision for this geometry. |
| DCB (See Figure 2.11) | $\frac{K}{P} = \frac{1}{8W^{\frac{3}{2}}} Y$ $u = a/W$ $Y = Y(a/W, H/W)$ $B = \sqrt{B_N}$ $B_N = \text{Net Thickness at Side Groove}$ | SIF.12 | Specimen used for generating da/dN, da/dt, and K _{I,DCB} data in pre-1983 revisions. The function Y was specified for given H/W. Data collected with DCB specimens were not reprocessed and no new data were received. |

TABLE 2.3 (Concluded)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

| TEST SPECIMEN GEOMETRY | STRESS-INTENSITY FACTOR COEFFICIENT | EQUATION NUMBER | REMARKS |
|--------------------------------|--|-----------------|---|
| B-DGB (See Figure 2.12) | $K = \frac{\sqrt{Eh}}{4} \frac{[3h(a+0.6h)^2 + h^3]^{1/2}}{[(a+0.6h)^2 + h^2]^{1/2}}$ | SIF.13 | Used for K1acc testing. All previously calculated using this equation were directly incorporated into the 1983 revision. |
| TDCB (See Figure 2.13) | $K = \left[\frac{E \left(\frac{dc}{da} \right)^2}{2B_N (1-\nu^2)} \right]^{1/2}$ where $\frac{dc}{da} = 1.65 - 0.925 \left(0.8 - \frac{B_N}{B} \right) \cdot 10^{-6} / 1b$ B_N = Net Thickness at Side Groove E = Elastic Modulus ν = Poisson's Ratio | SIF.14 | Equation used by McDonnell Aircraft Company to reduce data referenced in Ref. no. 84360 (Equation is based on Plane-Strain Assumptions). Data were incorporated without change. |
| TDGB (See Figure 2.13) | $K = \left[\frac{E \left(\frac{dc}{da} \right)^2}{2B} \right]^{1/2}$ where $\frac{dc}{da}$ = constant E = Elastic Modulus $B = \sqrt{B \cdot B_N}$ B_N = Net Thickness at Side Groove | SIF.15 | No new data were processed from TDGB specimens. Previous data incorporated into the handbook utilized this equation. |
| CNI (See Figure 2.14) | $K = \sqrt{Eh} \left[1 - 0.2\lambda + 4\lambda^2 \right]^{1/2}$ $\lambda = a/w$ SIF.16 is comparable to SIF.1 FOR $0 < \lambda < 0.3$ | SIF.16 | No new data were processed from CNI specimens. Previous data (K1acc) for sheet materials) incorporated into the handbook utilized this equation. |

2.1 PLANE-STRAIN FRACTURE TOUGHNESS (K_{IC})

The plane-strain fracture toughness (K_{IC}) property was initially established to characterize the fracture resistance of materials that exhibited rather abrupt fractures in the presence of cracks. Early observations showed that thickness had a pronounced effect on the critical levels of stress-intensity factor associated with fracture; a schematic illustrating this behavior is presented in Figure 2.15. As noted in the schematic, for thicknesses greater than the experimentally determined lower-bound, the critical stress-intensity factor level was found to be relatively constant.

The reasons for the independence of toughness with further increases in thickness were related to the amount and type of yielding which could occur at the crack tip under what has been referred to as plane-strain conditions. Because the thickness-independent toughness property was useful for comparing a large variety of metals for fracture resistance, ASTM (American Society for Testing and Materials) embarked on a standardization effort that eventually resulted in the ASTM Standard Test Method for plane-strain fracture toughness of metallic materials, i.e., in the ASTM Standard E399.

The ASTM Standard E399 is the current procedure for determining critical plane-strain stress intensity factors (K_{IC} values) for high-strength alloys. From the method of test, "The property K_{IC} determined by this method characterizes the resistance of a material to fracture in a neutral environment in the presence of a sharp crack under severe tensile constraint, such that the state of stress near the crack front approaches tritensile plane-strain, and the crack-tip plastic region is small compared with the crack size and specimen dimensions in the constraint direction."

Assuming that plane-strain conditions are approximated when unstable cracking occurs at the crack front during a K_{IC} test, the critical stress intensity factor calculated from the

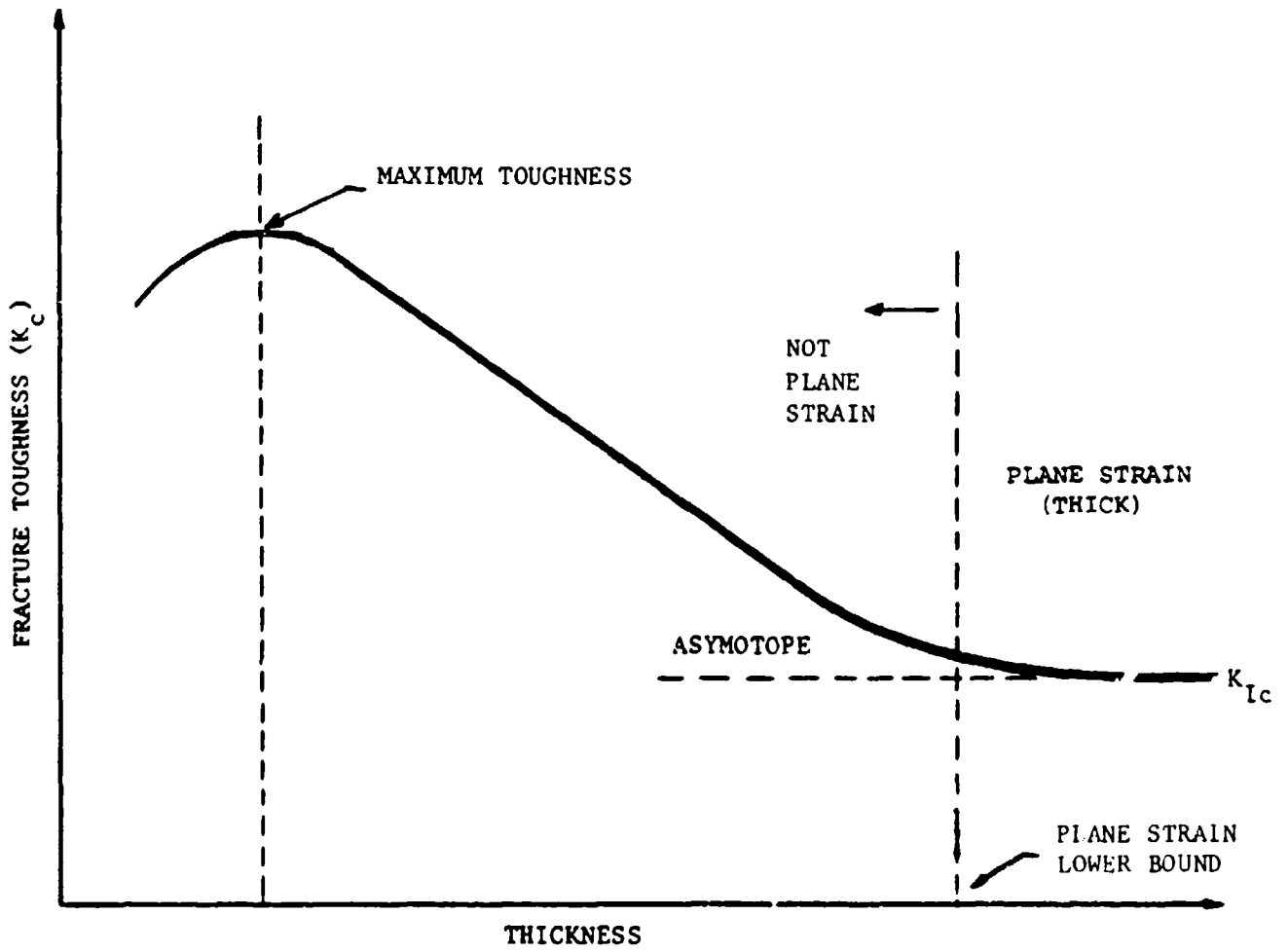


Figure 2.15. Fracture Toughness Behavior as a Function of Thickness.

test data is characteristic of the material of the specimen at the testing temperature and for the specific crack growth direction. Since the properties vary somewhat from specimen to specimen in one plate or in one heat, and from heat to heat of a given alloy type with the same heat treatment, the measured K_{IC} values for several heats will show some degree of scattering in the data. Usually, the extent of scattering is greater than that for replicate tensile tests. For this reason, a relatively large number of data points would be required to establish minimum design values for any of the fracture mechanics parameters. To minimize the scatter in data, maximum effort is required in controlling the processing, preparation, and testing of each specimen. These precautions are discussed in the Method of Test (ASTM E399).

The ASTM E399 procedure indicates that calculated K values be designated K_Q , which is a provisional value. When the validity of the results is established by the procedures designated in the Method of Test, then the K_Q value can be identified as a valid K_{IC} value. Some of the primary criteria for judging the validity of K_{IC} values are based on crack length and specimen thickness conditions. The test data must demonstrate that sufficient constraint was available to justify the plane-strain assumptions. The other requirements for validity of the K_{IC} values involve measurements of the length of the fatigue crack, contour of the crack front, out-of-plane deviation of the fatigue crack, maximum stress intensity resulting from the fatigue cracking load, and details of the load-deformation curves.

All newly acquired plane-strain fracture toughness (K_{IC}) data incorporated in the 1983 Handbook revision were generated using the ASTM Standard E399. These newly acquired data were generated using the CT specimen geometry (See Figure 2.2). All suppliers of new K_{IC} data provided only E399 validated K_{IC} data in a reduced format which facilitated direct incorporation into

the Handbook. Data incorporated in earlier revisions for the most part utilized ASTM Standard E399 or the predecessor tentative method for plane-strain fracture toughness testing; and after review, these data were also included into the 1983 revision. In some instances, nonstandard specimens were used for generating critical plane-strain stress-intensity factors in the earlier revisions. Some of these data were incorporated in the 1983 revision on the basis that a reasonable procedure was used and that corresponding data from other sources were limited for the alloys concerned. All data were checked against the criteria for specimen thickness (B) and crack length (a), i.e., $B, a \geq 2.5 (K_{IC}/\sigma_{ys})^2$ where σ_{ys} is the tensile yield strength.

2.2 CRITICAL PLANE STRESS FRACTURE TOUGHNESS

2.2.1 Plane Stress and Transitional Fracture Toughness

The critical level of the stress-intensity factor for non-plane-strain conditions is normally described with the symbol K_{IC} , see Figure 2.15, and is referred to as the plane-stress or transitional fracture toughness. Generally, plane-stress fracture-toughness testing is representative only of through-the-thickness cracks in relatively thin section materials. For a given material thickness, this configuration has the least lateral restraint on the crack front and, hence, approaches most closely the ideal plane-stress stress state conditions at the crack tip. As the material thickness increases, transitional stress state behavior is introduced by the restraint of additional material along the crack front. In contrast to that in plane-strain fracture-toughness testing, the characterization of fracture toughness in the plane-stress and transitional-stress states is complicated by the degree to which crack tip plasticity and associated stable crack extension are manifested prior to fracture. Although an explicit test method for this mode of toughness has not been formulated, there are a number of useful experimental guidelines which have been developed.

As background information, the nature of plane-stress and transitional fracture toughness is described here in terms of its deviation from that of the plane-strain stress state. Current procedures for this mode of testing and the associated analytical formulations of toughness then are presented.

The difficulties that beset the characterization of plane stress and transitional fracture are not only of a theoretical nature, but also of a practical experimental nature. Basic questions on the nature of plasticity, crack extension, and crack instability, as well as the wide variation in experimental techniques among laboratories all contribute to variability in the resulting fracture toughness evaluations. However, in spite of these difficulties, surprisingly consistent characterizations of fracture behavior can be obtained.

During the fracture test of a structural material in a plane-stress or transitional-stress state, stable extension of the initial fatigue precrack may occur as the load increases. This behavior is illustrated schematically in the crack growth curve of Figure 2.16. Depending on the material, stable crack extension may amount to 30 percent or more of the initial precrack length.

Once it is realized that fracture under these conditions is not an abrupt instability instantaneously associated with a small increment of crack extension, it must also be recognized that a single toughness parameter is not sufficient to characterize this complex behavior. In fact, the concept of crack growth resistance curves (see Section 2.4) is an outgrowth of these observations and best describes the material behavior. However, as a means of characterizing fracture behavior in plane-stress and transitional stress state, engineers have traditionally utilized abrupt fracture concepts, i.e., have used critical stress-intensity factor levels, to describe various events associated with the observed behavior.

2.2.2 Plane Stress and Transitional Fracture Toughness Testing

The procedures associated with testing thin-section center-cracked tension panels differ from those associated with plane-strain fracture toughness testing only in the additional emphasis and refinement that is directed to monitoring the slow, stable tear portion of the fracture process.

The general testing configuration is illustrated schematically in Figure 2.17. The specimen with an initial fatigue precrack, $2a_0$, is loaded slowly under load or stroke control. The onset and extension of crack growth under increasing load is usually monitored photographically, visually, or by means of compliance gage calibration until fracture occurs.

Although, as previously mentioned, more attention is currently being directed to monitoring the detail stress and crack length dimensions during the slow tear process, the preponderance

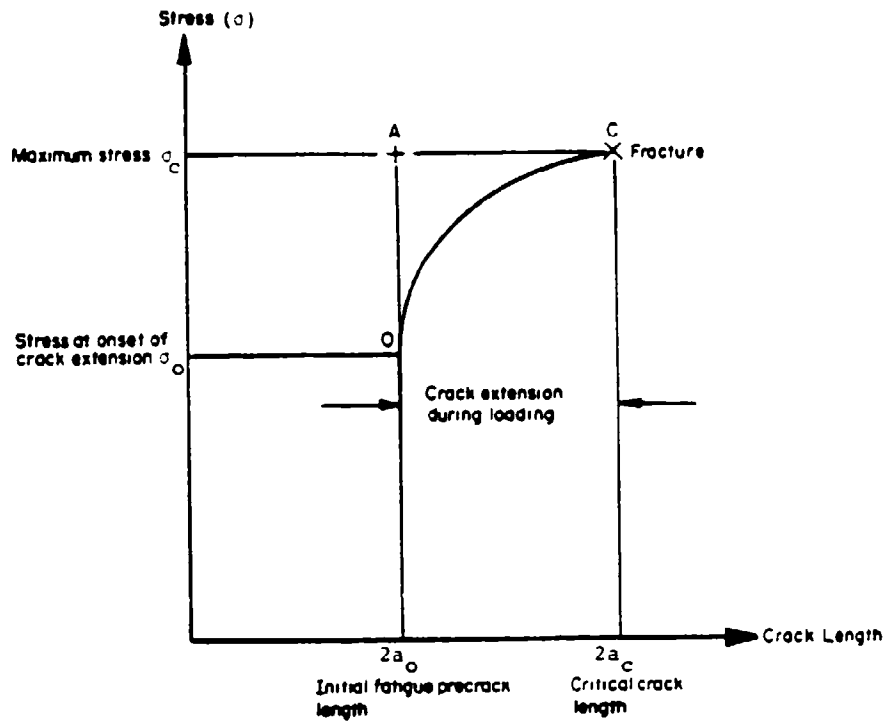


Figure 2.16. Typical Crack Growth Behavior in Plane Stress and Transitional Stress States.

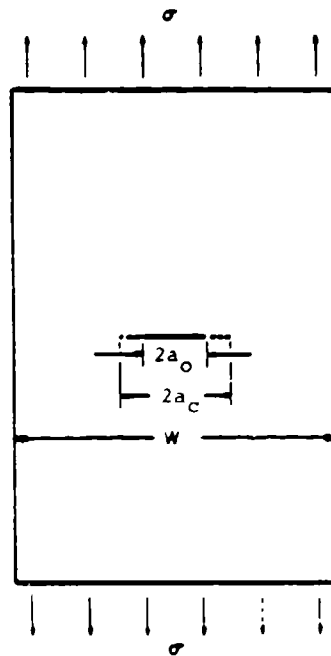


Figure 2.17. Thin-Section, Center-Cracked Tension Panel Configuration.

of available test data is limited to a record of σ_o , $2a_o$, σ_c , and $2a_c$, as indicated in Figure 2.16. It is this information which is compiled and analyzed in this Handbook.

2.2.3 Critical Stress-Intensity Factor (K_c)

There are two clearly identified points that can be noted on the crack growth resistance curve shown in Figure 2.16, i.e. points O and C which are associated with the onset of tearing and critical conditions, respectively. Using a linear elastic fracture mechanics analysis, these two structural conditions can be formulated as

$$K_{ONSET} = \sigma_o \sqrt{\pi a_o} \left(\text{Sec } \frac{\pi a_o}{W} \right)^{1/2} \quad (2.5)$$

and

$$K_c = \sigma_c \sqrt{\pi a_c} \left(\text{Sec } \frac{\pi a_c}{W} \right)^{1/2} \quad (2.6)$$

using the stress-intensity factor information given in Table 2.3, i.e. Equation SIF.1. As requested by industry engineers, available test information (σ_o , $2a_o$, σ_c , $2a_c$) were reported in the plane stress and transitional fracture toughness tables along with a calculation of the critical fracture toughness level based on Equation 2.6. While stress and crack length information was sometimes available for a calculation of the onset fracture toughness (Equation 2.5), insufficient space in the table precluded reporting this toughness.

Plane stress and transitional fracture behavior absorb much more energy than plane-strain behavior due to the lack of thickness constraint on crack tip plasticity is also insufficient, and the assumption of linear elastic fracture mechanics are violated. The in-plane geometric constraint on crack tip plasticity is required to ensure that gross plasticity is not the controlling mechanisms of fracture. Extensive study

has indicated that the condition for CCP specimen instability for ductile materials is given by a net section stress criteria and not by a fracture (crack) controlled instability criteria. While the fracture toughness values for all plane strain type tests are reported, those values calculated for stress conditions where the net section stress ($\sigma_{net} = \text{Load}/(W-2a_c)$) exceeds 80 percent of the tensile yield strength are marked with an asterisk. Asterisked values are not utilized in any mean or standard deviation calculations summarizing plane-stress fracture critical properties.

2.3 THE APPARENT FRACTURE TOUGHNESS

The apparent fracture toughness (K_{App}) is a plane stress and transitional fracture toughness property that is sometimes utilized as a lower bound on the critical fracture toughness. Its initial purpose was to preclude measurements of the tearing process observed during fracture tests of CCP specimens. As noted in Figures 2.17, and 2.16, the initial crack length ($2a_o$) extends during the loading to the critical crack length ($2a_c$). The two simplest measurements to make in such a fracture test are those of the initial crack length ($2a_o$) and critical (maximum) stress at failure (σ_c). Thus, for simplicity, a K_{App} fracture toughness calculation was made using

$$K_{App} = \sigma_c \sqrt{\pi a_o} \cdot \left(\sec \frac{\pi a_o}{W} \right)^{1/2} \quad (2.7)$$

Equation 2.7 represents the stress-intensity factor corresponding to the stress and crack length condition at point "A" in Figure 2.16. It can be noted by comparing Equations 2.6 and 2.7 that K_{App} will always be less than or equal to K_c since $a_o \leq a_c$. Also, K_{App} will always be greater than or equal to K_{ONSET} since $\sigma_o \leq \sigma_c$. A comparison of the apparent fracture toughness with the onset and critical fracture toughness is shown in Figure 2.18 for a wide center cracked panel (CCP) specimen.

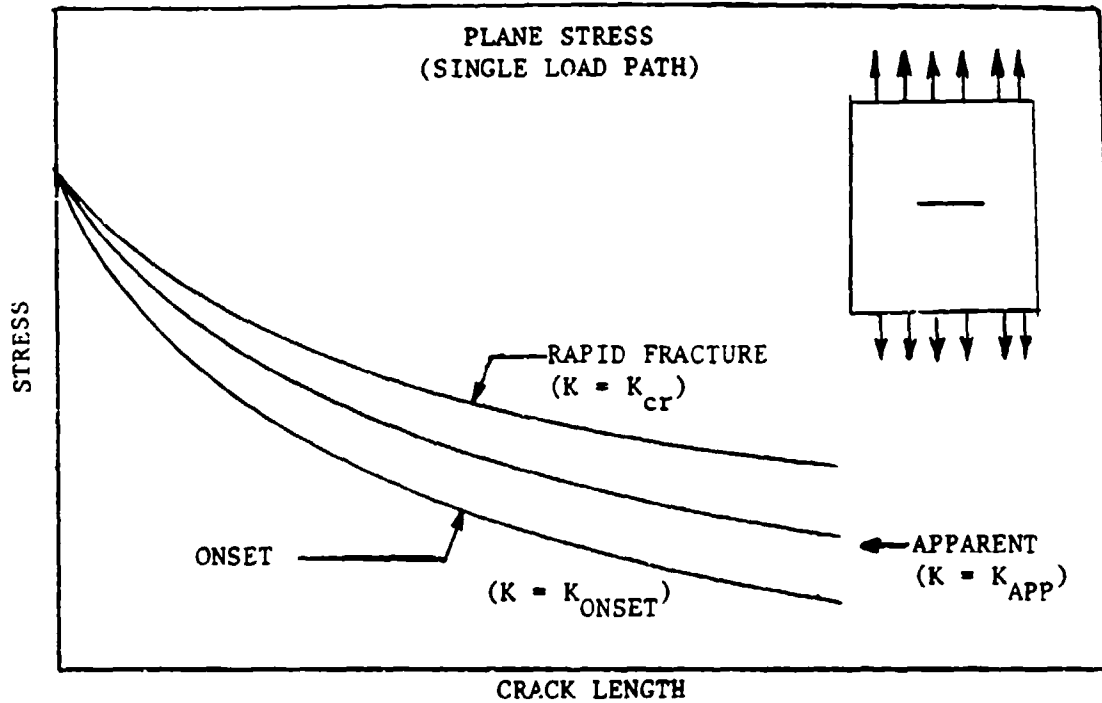


Figure 2.18. Description of the Three Fracture Toughness Criteria that are Utilized to Estimate Residual Strength Under Tearing Fracture Conditions.

When the net section stress ($\sigma_{net} = \text{Load}/(W-2a_0)$) exceeds 80 percent of the tensile yield strength, the K_{App} values are marked with an asterisk. The asterisked values are not utilized in any mean or standard deviation calculations summarizing plane-stress apparent fracture toughness properties.

2.4 R-CURVE (K_R VERSUS Δa_{eff})

The resistance curve (or R-curve) provides a complete description of the tearing fracture behavior illustrated in Figure 2.16. R-curves characterize the resistance to fracture of materials during incremental slow-stable crack extension and result from growth of the plastic zone as the crack extends. ASTM recently formalized the collection and reporting of such curves through a new standard, ASTM Standard E561, covering the standard practice for R-Curve Determination. As stated by ASTM E561: "An R-curve is a continuous record of toughness development in terms of K_R plotted against crack extension in the material as a crack is driven under continuously increased stress-intensity factor, K ."

The value of K_R (toughness) is calculated using standard stress-intensity factor equations evaluated with the instantaneous values of applied stress (σ) and crack length (a), as the crack extends. To account for the effects of plasticity, the measured crack length is enhanced with a plastic zone correction, and an effective crack length (a_{eff}) is actually used in the calculation of K_R . For example, when a CCP specimen is used to collect tearing resistance data, the K_R is calculated based on the standard stress-intensity factor equation (SIF.1) given in Table 2.3.

$$K_R = \sigma \sqrt{\pi a_{eff}} \cdot \left(\text{Sec} \frac{\pi a_{eff}}{W} \right)^{1/2} \quad (2.8)$$

where σ and a_{eff} are the current stress and effective crack length measurements in the test. The effective crack length for optical measurements is calculated from

$$a_{eff} = a + r_y \quad (2.9)$$

where a is the optically measured crack length and

$$r_y = \frac{1}{2\pi} \left(\frac{K}{\sigma_{ys}} \right)^2 \quad (2.10)$$

the plastic zone size for the current applied stress and crack length. If the crack length is automatically monitored by compliance techniques, then the effective crack length is automatically obtained using the two compliance equations presented in ASTM E561.

The K_R value calculated from Equation 2.8 can be described as a function of the increment of physical crack extension ($\Delta a = a - a_o$, a_o = initial crack length) or as suggested by ASTM 561 as a function of the increment of effective crack length ($\Delta a_{eff} = (a + r_y) - a_o$). The functions K_R versus Δa and K_R versus Δa_{eff} are referred to as R-curves (or resistance curves). Data presented in this handbook correspond to the use of the ASTM E561 definition of R-curves, i.e. K_R is presented as a function of Δa_{eff} .

One of the fundamental hypotheses behind the application of R-curves to the prediction of tearing type fractures in thin structures and in structures fabricated from ductile materials is that the R-curve (material tearing resistance) is independent of crack length for a given geometry and is independent of geometry and external loading. As long as the structure matches the monotonically increasing stress-intensity factor conditions given by the R-curve, the structure will exhibit the same tearing resistance experienced in the laboratory test specimen. The Damage Tolerant Guidelines Handbook (AFWAL-TR-82-3073) describes how the R-curve can be applied to the calculation of critical stress levels in structures.

2.5 FATIGUE CRACK GROWTH RATE

2.5.1 Fatigue Crack Growth Behavior

Under some loading conditions or environmental conditions, cracks can grow at load levels well below that required to cause fracture. As the crack continues to grow, conditions become more favorable for fracture, and eventually under the applied loading fracture does occur. This process whereby cracks are observed to grow at subcritical load levels is referred to as subcritical crack growth. Illustrated in Figure 2.19 is a fatigue crack growth curve, which shows the type of behavior typically observed during a specific subcritical crack growth process; in this case, damage is done to the material by cyclic (or fatigue) loading. This section addresses properties used to measure fatigue crack growth behavior and Sections 2.6 and 2.7 address properties used to characterize sustained load cracking in an environment.

The objective of fatigue crack growth testing is to determine the rates at which subcritical flaws propagate under cyclic loadings prior to reaching a size critical for fracture. These rates are determined from measurements of the crack extension occurring over an increment of cyclic loading. Typically, these measurements are made by monitoring crack extension optically on the specimen surface during the test. From the basic crack length and cycle count data, the fatigue-crack growth rate is determined as the quotient of the incremental crack growth divided by the incremental cycle count, i.e., $\Delta a / \Delta N$ or da/dN , the slope of the crack growth (life) curve.

The crack growth rate measures the resistance of the material to the applied loading conditions. The similitude parameter that allows data to be transferred from one cracked geometry to another is the range in stress-intensity factor (ΔK). The ΔK parameter is the difference between the maximum and minimum stress-intensity factors (K_{max} and K_{min} , respectively) for a cycle of loading. The property of fatigue crack growth rate is described throughout this Handbook as a function of ΔK .

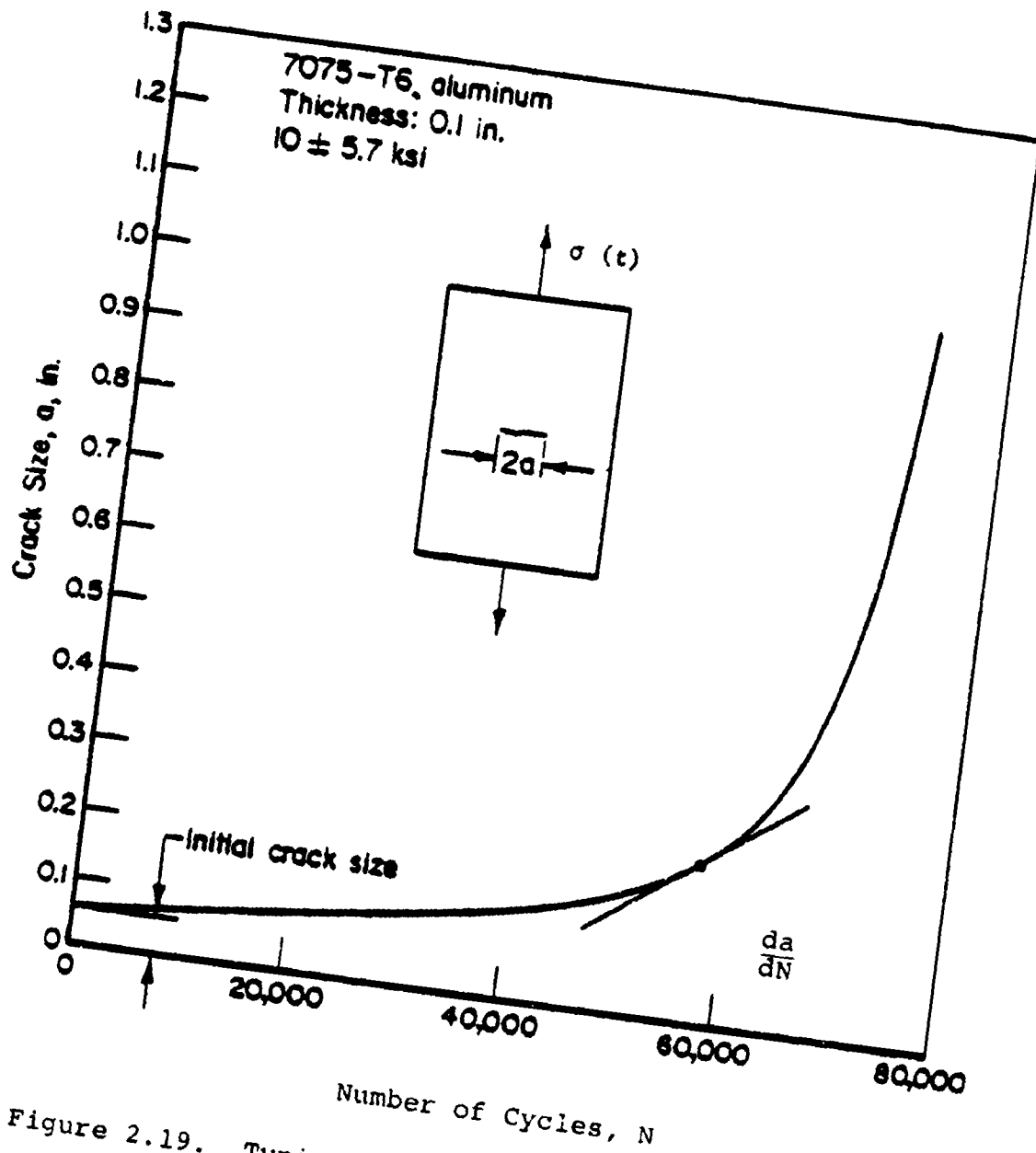


Figure 2.19. Typical Crack Growth-Life Curve.

2.5.2 Data Acceptance Criteria

In general, similar specimen configurations are used for fatigue-crack-growth testing as are used for other types of damage tolerant tests. The applied loads are reduced in magnitude and are cyclic in nature for studies of crack extension under fatigue loading conditions, and the experimental methods are extensions of the fracture testing procedures previously described. Instead of applying either a rising or sustained load to fracture the specimen, a constant amplitude cyclic load is applied to initiate and grow the crack over a significant portion of the specimen width. ASTM recently published a standard testing method, i.e., ASTM E647, which covers the collection and reporting of fatigue crack growth rate data. Most of fatigue crack growth rate data reported in the handbook were collected and reduced utilizing the guidelines and methods described by ASTM E647. For CCP and CT specimen geometries, the ASTM Standard describes 11 explicit criteria for validating the data; these criteria are summarized in Table 2.4. If data were noted to fail only one or two of the recommended criteria and provided a realistic representation of the growth rate behavior, they were incorporated into the handbook. Note is made in the handbook database of da/dN data that failed to meet the ASTM criteria listed in Table 2.4.

2.5.3 Data Reduction Procedures

Data reduction of crack growth rate from the crack length versus cycle count data was by one of two methods. The secant method was chosen when there were seven or less crack length versus cycle count measurements. A five point polynomial movable strip method was used for data with more than seven crack length versus cycle count measurements. This procedure was similar to the seven point method recommended in the ASTM standard; the five point method was chosen to provide additional data points at the extremes of growth rate range.

TABLE 2.4
CRITERIA CHECKS FOR FATIGUE CRACK GROWTH RATE DATA

| Criteria No. | ASTM E647 Paragraph | Specimen Type | Criterion |
|--------------|---------------------|---------------|---|
| 1 | 7.1.3.1 | CT | $\frac{W}{20} \leq B \leq W/4$ |
| | 7.1.3.2 | CCP | $B \leq W/8$ |
| 2 | Figure 1 | CT | $W \geq 1.00"$ |
| | | CCP | None |
| 3 | 8.6.3 | CT and CCP | If $B/W \geq 0.15$ need front and back crack lengths. |
| 4 | 7.1.1 | CT | $a_N \geq 0.2W$ |
| | 7.1.2 | CCP | None |
| 5 | 8.3 | CT and CCP | $a_1 \geq 0.1B$ or h , whichever is greater |
| 6 | 8.6.4 | CT and CCP | (Front Crack Length-Back Crack Length) < 0.025 W or 0.25 B, whichever is less. |
| 7 | 8.6.2.1 | CT | if $0.25 \leq a/W \leq 0.60$ then $\Delta a \leq 0.02 W$ if $a/W > 0.60$ then $\Delta a \leq 0.01 \bar{W}$ |
| | 8.6.2.2 | CCP | if $2a/W \leq 0.60$ then $\Delta a \leq 0.03 W$ if $2a/W > 0.60$ then $\Delta a \leq 0.02 W$ |
| 8 | 8.6.2.3 | CT and CCP | $\Delta a \geq 0.01"$ |
| 9 | 7.2.1 | CT | $W - a \geq \frac{4}{\pi} (K_{\max} / TYS)^2$ |
| | 7.2.2 | CCP | $P_{\max} / (BW)(1-2a/W) < TYS$ |
| 10 | 8.5.1 | CT and CCP | In Test , Load Variation $0 \leq \left \frac{P_{\max a+1} - P_{\max a}}{P_{\max a}} \right \leq 0.10$ |
| 11 | 8.3.1 | CT and CCP | (1) In Precracking . $\frac{P_{\max a+1} - P_{\max a}}{P_{\max a}} \leq 0.20$ |
| | | | (2) $\Delta a \geq (3/\pi) (K_{\max} / TYS)^2$ |

CT = Compact Tension
CCP = Center Cracked Panel
B = Specimen Thickness
W = Specimen Width
a = Crack Length
 a_N = Notch Size
 a_1 = Fatigue Precrack Length

h = Height of Specimen
 Δa = Change in Crack Length
 P_{\max} = Maximum Load
 K_{\max} = Maximum Stress Intensity
TYS = Tensile Yield Strength
 K'_{\max} = Maximum Stress Intensity at Smaller Crack Length being Considered

It is important to note that the calculation of stress-intensity factor range (ΔK) is the difference between the maximum and minimum stress-intensity factors (K_{\max} and K_{\min} , respectively) as defined in ASTM Standard E647. These calculations are best expressed using equations specific to a given geometry; for illustration purposes, assume that the test specimen geometry is CCP. Then, the maximum and minimum stress-intensity factors are given by

$$K_{\max} = \sigma_{\max} \sqrt{\pi a} \left(\sec \frac{\pi a}{W} \right)^{1/2} \quad (2.11)$$

and

$$K_{\min} = \sigma_{\min} \sqrt{\pi a} \left(\sec \frac{\pi a}{W} \right)^{1/2} \quad (2.12)$$

where σ_{\max} and σ_{\min} are the maximum and minimum stresses in the applied loading cycle. The range of stress-intensity factor is defined as

$$\Delta K = K_{\max} - K_{\min} \quad (2.13)$$

By ASTM convention, if K_{\min} is compressive (negative), then $K_{\min} \equiv 0$, and $\Delta K = K_{\max}$.

2.5.4 Data Reporting Procedures

The presentation of fatigue-crack-propagation rate data is far more complex than the presentation of fracture toughness data (either K_{IC} or K_C) due to the large quantities of data which must be treated. Where a fracture test generally yields a single characteristic toughness value, a fatigue-crack-growth test specimen generally yields from 10 to 100 rate data points, da/dN , which must be evaluated in terms of the stress-intensity factor ΔK range.

The Damage Tolerant Design Data Handbook presents fatigue crack growth rate (da/dn) data in both graphical and tabular formats. A graphical format is used to present da/dN versus ΔK data and the mean trend of these data are tabulated. The

least squares cubic spline approximation method has been selected from those available to provide a practical method for generating tables with fixed ΔK values. A least squares cubic spline approximation is an analytic method of fitting a "French" curve to a data set. The curve is constructed by fitting different cubic polynomials on non-overlapping, connecting subintervals over the range of the independent variable. In the Handbook, the independent variable will be ΔK . The boundary points of the intervals are referred to as knots and the cubic polynomials meet at the knots. The polynomials are also constrained so that the first and second derivatives are continuous at the knots. The result of this process is a smooth curve which passes through the center of the data.

Figure 2.20 is an example of a spline curve fit to a da/dN data set reported by Hudak et al. for 2219-T851 Aluminum alloy. The stress ratio used to establish the data shown was 0.3. The knots are marked in the figure by the large dots.

In general, da/dN data are well enough behaved so that a maximum of five knots was sufficient in generating the handbook tables. The actual number of knots used in fitting a curve to a set of data is a function of the number of da/dN data points and their pattern in $da/dN-\Delta K$ space.

The mean trend table for a set of da/dN data will be generated by selecting points from the spline curve that has been fit to the data. The ΔK values will be chosen such that they are approximately equally spaced in a logarithmic scale and cover the complete range of ΔK values expected. The da/dN values are obtained through the interpolation of the spline curve at the preselected ΔK values. The complete set of ΔK values are: 1.0, 1.3, 1.6, 2.0, 2.5, 3.0, 3.5, 4.0, 5.0, 6.0, 7.0, 8.0, and 9.9 as well as 10 times these values, and 130, 160, and 200.

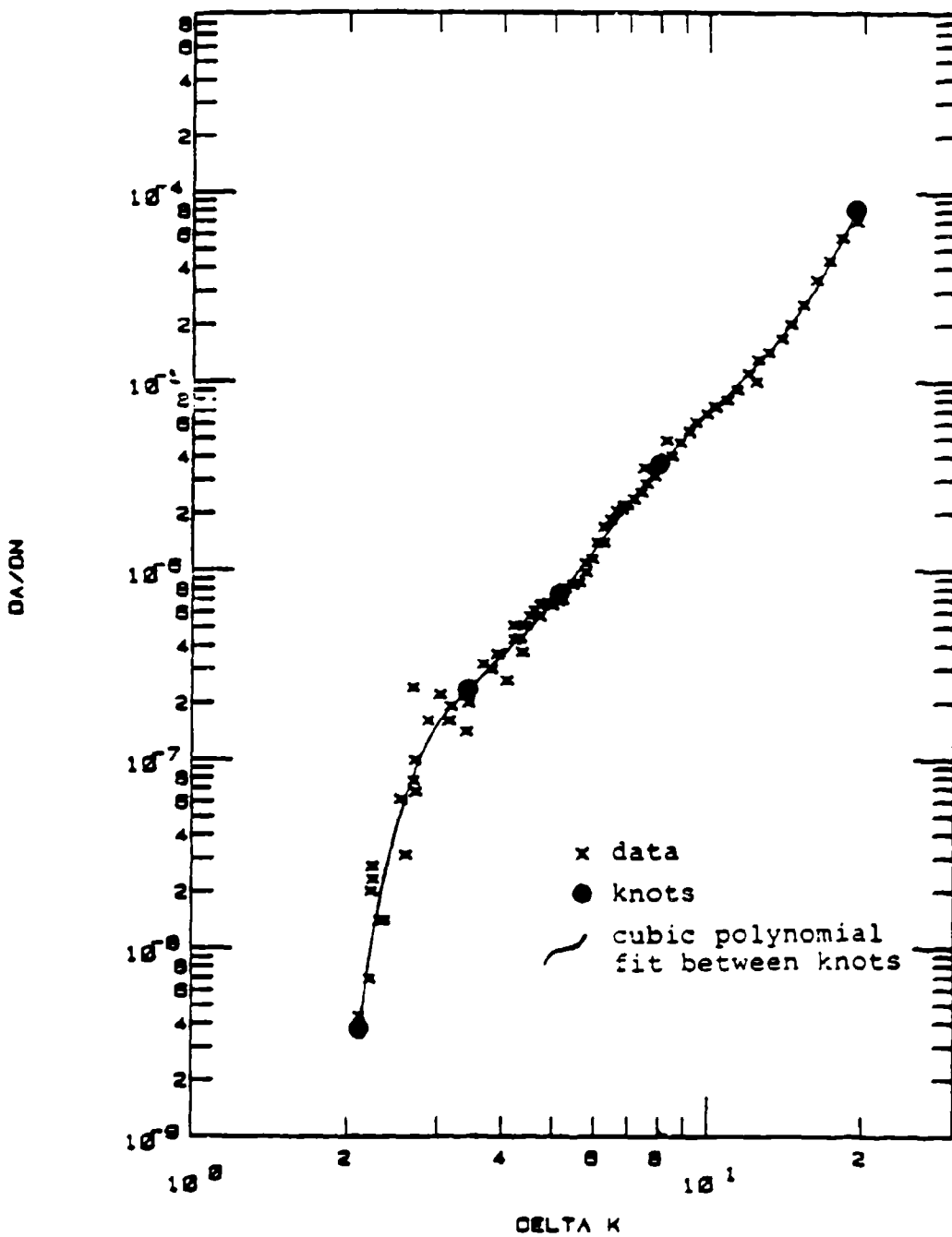


Figure 2.20. A Cubic Spline Curve Fit to FCGR Data for 2219-T851 Aluminum at a Stress Ratio of 0.3.

Because the da/dN data do not always span the complete ΔK range, the table also reports the minimum and maximum da/dN values corresponding to the recorded minimum and maximum ΔK values. The extreme pairs of (ΔK , da/dN) points correspond to the extremes of the spline curve.

Table 2.5 describes the type of table designed for the handbook. The minimum values of ΔK and da/dN as obtained from the spline curves are presented at the top of the table for each data set with a variable such as stress ratio. These tables will be directly opposite the graphical format of the da/dN data. The interpolated da/dN data are listed in the body of the table as a function of the selected ΔK values that span the data sets, and the maximum values of ΔK and da/dN as obtained from the spline curves are presented towards the bottom of the table.

The last two sections of Table 2.5 are utilized to summarize the statistics of the data fitting process. The root mean square percent error (RMSPE) is utilized to describe the statistical accuracy for the spline curve fit at each stress ratio. The RMSPE is given by:

$$\text{RMSPE} = 100 \times \sqrt{\frac{1}{n} \sum_{i=1}^n \left(\frac{y_i - \hat{y}_i}{\hat{y}_i} \right)^2} \quad (2.14)$$

where

y_i = observed da/dN_i at ΔK_i

\hat{y}_i = da/dN interpolated from table at ΔK_i .

The RMSPE is a measure of how close the data lie to the mean trend table and has a similar interpretation to the coefficient of variation, i.e., the smaller the better. The coefficient of variation is used when all the data have the same mean and is calculated by dividing the standard deviation by the mean and multiplying by 100. For da/dN data, the mean da/dN is a function of

TABLE 2.5
 EXAMPLE FATIGUE CRACK GROWTH RATE
 TABLE (2219-T851 Aluminum)

| ΔK (Ksi $\sqrt{\text{in}}$) | | | $da/dN \times 10^4$ inches/cycle | | | | |
|---|------|--------|----------------------------------|---------|---------|---------|---------|
| | | | R1=-1.0 | R2=0.1 | R3=0.3 | R4=0.5 | R5=0.8 |
| ΔK_{min} at: | R1 | 1.09 | 0.00730 | 0.00336 | 0.00369 | 0.00351 | 0.00112 |
| | R2 | 2.35 | | | | | |
| | R3 | 2.11 | | | | | |
| | R4 | 1.38 | | | | | |
| | R5 | 1.17 | | | | | |
| | 1.3 | 0.0167 | | | | | 0.00429 |
| | 1.6 | 0.0351 | | | | 0.0176 | 0.0251 |
| | 2.0 | 0.0676 | | | | 0.0569 | 0.0689 |
| | 2.5 | 0.127 | | | 0.0451 | 0.0911 | 0.128 |
| | 3.0 | 0.216 | 0.0166 | 0.152 | 0.139 | 0.228 | |
| | 3.5 | 0.336 | 0.0639 | 0.246 | 0.218 | 0.431 | |
| | 4.0 | 0.488 | 0.171 | 0.355 | 0.339 | 0.809 | |
| | 5.0 | 0.884 | 0.566 | 0.691 | 0.753 | 2.60 | |
| | 6.0 | 1.37 | 1.14 | 1.30 | 1.46 | 7.83 | |
| | 7.0 | 1.91 | 1.93 | 2.28 | 2.50 | 46.3 | |
| | 8.0 | 2.47 | 3.09 | 3.60 | 3.95 | | |
| | 9.0 | 3.08 | 4.78 | 5.14 | 6.07 | | |
| | 10.0 | 3.80 | 7.04 | 6.86 | 9.38 | | |
| | 13.0 | 7.16 | 17.0 | 14.4 | 38.4 | | |
| | 16.0 | 13.2 | 36.2 | 30.9 | | | |
| | 20.0 | 28.3 | 126.0 | | | | |
| ΔK_{max} at: | R1 | 20.7 | 32.0 | 887.0 | 81.3 | 146.0 | 47.4 |
| | R2 | 24.7 | | | | | |
| | R3 | 19.3 | | | | | |
| | R4 | 13.8 | | | | | |
| | R5 | 7.01 | | | | | |
| root mean square percent error | | | 2.2 | 80.4 | 8.6 | 6.4 | 6.1 |
| life prediction ratio summary | | | | | | | |
| 0.0 - 0.5 | | | | | | | |
| 0.5 - 0.8 | | | | 1 | | | |
| 0.8 - 1.25 | | | 1 | 3 | 1 | 2 | 2 |
| 1.25 - 2.0 | | | | | | | |
| > 2.0 | | | | | | | |

ΔK so this is taken into account when calculating the RMSPE. The RMSPE is an average percent error of the observed da/dN values from the curve established by the mean trend table.

When evaluating the mean trend da/dN description, engineers have come to rely on an evaluation of the ability of the mean trend curve to repredict the initial a versus N data and, in particular, to rely on life prediction ratio (N_p/N_A) which relates the predicted number of cycles (N_p) required to propagate a crack through a specified increment to the actual number of cycles (N_A) observed to propagate a crack through the same increment. Life prediction ratios between 0.8 and 1.25 are considered good and a life prediction ratio of 1.0 is ideal.

As a second measure of how well the mean trend curve fits the data, a summary of the life prediction ratios for the specimens used to generate the mean trend curve is included at the bottom of Table 2.5. This summary defines the number of specimens tested at each stress ratio presented whose life prediction ratios fall within the five intervals: 0.0 to 0.5, 0.5 to 0.8, 0.8 to 1.25, 1.25 to 2.0, and greater than 2.0.

The life prediction ratios summarized at the bottom of Table 2.5 are self predictions and as such will tend to be good. However, the summary is only valid for the data used to generate it and therefore should not be generalized to other situations. The life prediction ratio summary is not intended to predict how well the mean trend curve will predict crack growth for an arbitrary specimen; however, it does illustrate how well the mean trend in FCGR correlates with the lives of the cracks that were used in generating the mean trend.

In order to indicate how well the present method being used does in predicting life ratios, Table 2.6 gives a comparison on sixteen specimens of the Aluminum 2219-T851 at various stress ratios ranging from -1.0 to +0.8. The round-robin LPR resulted from an ASTM study conducted by eight organizations; the average results of the analysis are presented. From Table 2.6, it can be seen that the handbook mean trend method gives results comparable to other methods being used throughout the country.

TABLE 2.6
FULL INTERVAL COMPARISONS OF
LIFE PREDICTION RATIOS

| <u>NO.</u> | <u>SPECIMEN</u> | <u>STRESS RATIO</u> | <u>ROUND-ROBIN LPR</u> | <u>DTD HB LPR</u> |
|------------|-----------------|-------------------------|----------------------------|-----------------------|
| 1. | CT 2219-3 | .1 | 1.03 | .9910 |
| 2. | CT 4* | .1 | 0.94 | .9095 |
| 3. | CT 5 | .1 | 0.91 | .8876 |
| 4. | CT 6* | .1 | 0.91 | 1.0554 |
| 5. | CT 11* | .1 | 1.08 | 1.0475 |
| 6. | CT 20 | .1 | 0.64 | .6271 |
| 7. | CT 56* | .3 | 0.99 | 1.0221 |
| 8. | CT 58 | .3 | 0.88 | .8400 |
| 9. | CT 52 | .5 | 1.07 | 1.0769 |
| 10. | CT 54* | .5 | 1.00 | .9693 |
| 11. | CT 60* | .5 | 1.10 | .8354 |
| 12. | CT 19 | .8 | 1.71 [†] | *** |
| 13. | CT 27* | .8 | 1.02 | .8321 |
| 14. | CT 37* | .8 | 0.92 | .9607 |
| 15. | CCP 9* | -1.0 | 0.87 | .9856 |
| 16. | CCP 11 | -1.0 | 1.14 | 1.1572 |
| | | | | |
| | Mean | | 0.97 | 0.95 |
| | Std. Dev. | | 0.12 | 0.13 |

* Actual Data Were Available for Testing Life Prediction Analysis

*** Stress-Intensity Factor Out of Bounds

[†] Not Included in Calculation of Mean or Std. Dev.

2.6 SUSTAINED-LOAD CRACK GROWTH RATES

2.6.1 Sustained-Load Crack Growth Rate Behavior

Sustained-load crack growth rate behavior is another type of subcritical crack growth behavior exhibited by materials which are sensitive to environmental attack. This type of subcritical crack growth behavior normally exhibits itself as a time-dependent crack growth rate process, whereby cracks are noted to extend under steady-state (sustained) static loading conditions in the presence of environments. Crack growth mechanisms controlling the sustained-load crack growth rate process include: stress-corrosion cracking, hydrogen embrittlement, liquid metal embrittlement, grain boundary separation, and creep. In practice, the time-dependent cracking process has been found to be driven by internal (residual) tensile stresses in the fabricated structure, even in the absence of externally applied loads; typically, however, the stressing condition which drives the crack is provided by external loads.

The objective of sustained-load crack growth testing is to determine the rates at which cracks propagate in pre-cracked specimens subjected to statically applied loads and prescribed environmental conditions. As with fatigue crack growth rate tests, most of the crack length measurements are made optically on the specimen surface during the test. Non-optical methods used to establish cracking include compliance and stress wave analysis techniques. From the basic crack length and time data, the sustained-load crack growth rate is determined as the quotient of the incremental crack growth divided by the incremental time, i.e., $\Delta a/\Delta t$ or da/dt , the slope of the crack growth (time to failure) curve.

The crack growth rate measures the resistance of the material to the applied loading for the specified environment. In this case, the similitude parameter that allows data to be transferred from one cracked geometry to another is the static stress-intensity factor (K_{max}). The K_{max} parameter is the stress-intensity factor evaluated for the applied loading and current crack length. The property of sustained-load crack growth rate (da/dt) is described throughout this Handbook as a function of K_{max} .

2.6.2 Data Acceptance Criteria

For the most part, the testing methodology for da/dt properties follows that utilized to obtain da/dN properties. There are, however, no current ASTM standards that specifically cover the collection of da/dt data. Sustained-load data have been obtained with a variety of specimens including double cantilever beams (DCB), tapered double cantilever beams (TDCB), compact tension (CT) specimens, cantilever beams (CANT), single-edge-notch tensile (SENT) specimens, part-through-surface-crack (PTSC) specimens, and center-cracked panel (CCP) specimens.

One validity criterion that is sometimes applied to da/dt data is that the thickness dimension and crack length must be greater than $2.5 (K_{Ic}/\sigma_{ys})^2$.² No da/dt data were excluded from the 1983 revision, however, based on this criteria due to the scarcity of da/dt data. The reader will find K_{Ic} , σ_{ys} and thickness reported with da/dt data whenever these were available.

Readers should note that sustained load crack growth rate data in aluminum alloys in planes other than those parallel to the surface of rolled plates are questionable because of the localized corrosion that occurs on the planes even though the initial notch and crack orientation are normal to these planes.

2.6.3 Data Reduction Procedures

Data reduction of sustained-load crack growth rates was accomplished using the secant method applied to crack length (a) measurements recorded as a function of time (t). These calculations and those of static stress-intensity factor were provided to the data processing organization for reformatting.

2.6.4 Data Reporting Procedures

The data reporting procedures for sustained-load cracking data are similar to those discussed in subsection 2.5.4 for fatigue crack growth rates. The major difference between the two subcritical cracking rate reporting procedures is that da/dt vs K_{max} describes the sustained-load behavior whereas da/dN vs ΔK describes the fatigue behavior. The reader might also note that no a vs t were available to compare with the integrated crack growth mean trend data and therefore no life prediction ratios were presented.

2.7 THRESHOLD STRESS INTENSITY (K_{ISCC})

2.7.1 The Threshold

In many environments, materials exhibit a condition whereby cracks are not observed to grow if the static stress intensity factor is below a critical level, designated K_{ISCC} . This property is specific for a given material in a given environment within a specified time period. In high-strength materials, K_{ISCC} may be only a small fraction of the plane-strain fracture-toughness value (K_{IC}) of the material. In lower strength tougher materials where plane-strain conditions still prevail, K_{ISCC} may approach or equal K_{IC} , if the environment has little or no effect on the stress intensity required to propagate a crack.

K_{ISCC} data have been obtained with a variety of specimens including: Cantilever beam (CANT), 3-point loaded bend beam (ND), 4-point loaded bend beam (4-NB), Single-edge-notch tensile (SENT), Center-cracked tensile (CNT), Part-

through surface-crack (PTSC), Compact tension (CT), Bolt-loaded WOL (BWOL), Double cantilever beam (DCB), and Tapered or contoured double cantilever beam (TDCB). All specimens are notched and precracked by fatigue, and many specimens are side grooved (SG) to ensure that the crack propagates in one plane perpendicular to the applied tensile loading and also to minimize the contribution of shear lips at the edges of the crack.

The types of specimens for determining K_{Isc} fall into two broad categories: those that are loaded by weights or tensile machines (see Figure 2.21) and those that are self-loaded as by bolts. The former require bulky setups to accommodate lever arms, weights, and tensile machines while the latter are compact and portable. Thus the environment is applied to the externally loaded specimens usually in the form of a small container sealed onto the specimen, while the self-loaded specimen may be completely immersed in the environment.

Under dead-weight loading conditions, the usual practice is to run a number of specimens at various stress intensities less than K_{Ic} for a finite length of time (more than 24 hours and usually about 500 hours) to establish K_{Isc} . Another method is to step load a single specimen until the crack starts to propagate. This method requires holding after each load increment for a sufficient time to establish that crack propagation does not occur.

Under bolt self-loading conditions, sufficient load is first applied to the bolt to cause the crack to extend beyond its precracked position. The specimen is then exposed to the environment. As the crack propagates in the environment, the stress-intensity factor decreases at the tip of the advancing crack until the crack arrests at K_{Isc} . Specimen length must be sufficient to ensure that the crack arrests before completely penetrating the specimen, thus assuring that a value is obtained for K_{Isc} .

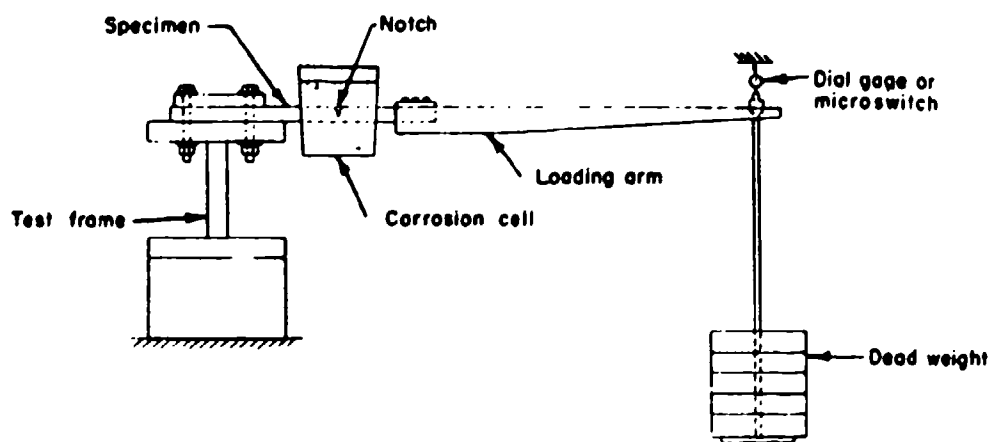


Figure 2.21. Schematic Drawing of Fatigue Cracked Cantilever Beam Test Specimen and Fixtures.

2.7.2 Conditions for Validity of Data

There are no ASTM standards that specifically cover the collection of K_{ISCC} data. The criterion typically used to validate K_{ISCC} data is that the thickness dimension (B) and crack length (a) are greater than the ASTM E399 requirement for plane-strain fracture toughness, i.e., that B and $a \geq 2.5 (K_{IC}/\sigma_{ys})^2$. Data which did not meet this criterion are identified in the K_{ISCC} tables with an asterisk. Many tests reveal a drastic reduction in the stress intensity required to propagate a crack even though the $2.5 (K_{IC}/\sigma_{ys})^2$ criterion is not met. Although these data are not recommended for material selection and design purposes, they do indicate a qualitative effect.

CHAPTER 3
STAINLESS STEEL ALLOY SECTION

| | |
|------|------------------------------------|
| 3.0 | Stainless Steel Material Summaries |
| 3.1 | AFC 260 |
| 3.2 | AFC 77 |
| 3.3 | AFC 77 (VAR) |
| 3.4 | AM 355 |
| 3.5 | AM 362 |
| 3.6 | AM 364 |
| 3.7 | Custom 455 |
| 3.8 | PH 13-8Mo |
| 3.9 | PH 14-8 Mo |
| 3.10 | PH 15-7 Mo |
| 3.11 | 15-5PH |
| 3.12 | 15-5 PH(AM) |
| 3.13 | 15-5 PH (VM) |
| 3.14 | 17-4 PH |
| 3.15 | 17-7 PH |
| 3.16 | 304 |
| 3.17 | 316 |
| 3.18 | 347 |
| 3.19 | Bibliography |

Table 3.0.1
 AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | K2C | R CURVES | DA/DM | DA/DT | R18CC |
|---------|--|--------------|-----|-----|----------|-------|-------|-------|
| AFC 260 | 2200F 1HR 1900F 1HR 0G -100F 1HR -320F 1HR 800F 2+2 HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR 0G -100F 1HR -320F 1HR 1090F 2+2HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR 0G -100F 1HR -320F 1HR 900F 2+2 HR | PLATE | | | | | | X |
| | 2200F 1HR 1900F 1HR 0G -100F 1HR -320F 1HR 1000F 2+2 HR | PLATE | | | | | | X |
| | AUSTENIZED AT 2010F, QUENCHED TEMPERED AT 810F | SHEET | | | | | X | |
| | 1800F 1HR 0G, -100F 0.5HR, 500F 2+2 HR (COARSE GRAIN) | PLATE | | | | | | X |
| | 1800F 1HR 0G, -100F 0.5HR, 1000F 2+2 HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR 0G, -100F 0.5HR, 500F 2+2 HR (FINE GRAIN) | PLATE | | | | | | X |
| AFC 77 | 1800F 1HR 0G, -100F 0.5HR, 1000F 2+2 HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, 700F 2+2HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, ROOF 2+2HR (COARSE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, 700F 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, ROOF 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, ROOF 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, ROOF 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |
| | 1800F 1HR, 0G, -100F 0.5HR, ROOF 2+2HR (FINE GRAIN) | PLATE | X | | | | | X |

Table 3.0.1 (Con't)

AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | KIC | KC | R | CURVES | DA/DN | DA/DT | KIBCC | |
|--------|--|--------------|-----|----|---|--------|-------|-------|-------|---|
| AFC 77 | 1800F 1HR. OG. -100F 1HR. 700F 2+2HR | ROUND BAR | X | | | | | | | |
| | 1800F 1HR. OG. -100F 1HR. 800F 2+2HR | ROUND BAR | X | | | | | | | |
| | 1900F 1HR. OG. -100F 1HR. 800F 2+2HR | ROUND BAR | X | | | | | | | |
| | 2000F 1HR OG. -100F 0.5HR 1400F 2+2 HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 500F 2+2HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 700F 2+2 HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 800F 2+2 HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 900F 2+2 HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 1100F 2+2 HR | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 500F 2+2HR + 10 PCT CM, 1000F | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 500F 2+2HR + 10 PCT CM, 700F | BAR | | | | | | | X | |
| | 2000F 1HR OG. -100F 0.5HR 500F 2+2HR + 20 PCT CM, 700F | BAR | | | | | | | X | |
| | 2000F 1HR. OG. -100F 1HR. 900F 2+2HR | ROUND BAR | X | | | | | | | |
| | 2000F 1HR. OG. -100F 1HR. 800F 2+2HR | ROUND BAR | X | | | | | | | |
| | 2100F 1HR. FC TO 1700F HR.D 1HR. OG. -100F 4HR. 500F 2+2 HR | FORGING | | | | | | | | X |

Table 3.0.1 (Con't)

AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | KC | R CURVES | DA/DN | DA/DT | K1S5C |
|--------------|---|--------------|-----|-----|----|----------|-------|-------|--------|
| AFC 77 (VAR) | 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. WELD 1HR.00. -100F 24HR. 900F. 2+2HR | FORGING | | X | | | | | |
| | 2100F 1HR. MOVED TO FCE AT 1900F. WELD 1HR.00. -100F 4HR. 300F 2+2HR | FORGING | | X | | | | | |
| AM 355 | MOD SCT1000 | BAR | | | | | | | X |
| | SCT 850 | PLATE BAR | | | | | | | X X |
| AM 362 | SCT1000 | PLATE BAR | | | | | | | X X |
| | H 900 | BAR | | | | | | | X |
| AM 364 | H1000 | BAR | | | | | | | X |
| | H 850 | FORGING | | | | | | | X |
| CUSTOM 453 | H 950 | FORGING | | | | | | | X |
| | H 900 | FORGING | | | | | | | X |
| | H 950 | FORGING | | | | | | | X |
| | H1000 | FORGING | | | | | | X | |
| | 1500F 1HR.00. 950F 4HR. AC | FORGING | | X | | | | | |
| | 1500F 1HR.00. 900F 4HR. AC | FORGING | | X | | | | | |

Table 3.0.1 (Con't)

AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | KIC | MC | R | CURVES | DA/DN | DA/DT | KISCC | |
|----------------------------------|---|--------------|-----|----|---|--------|-------|-------|-------|---|
| PH113-880 | ANNEALED | EXTRUDED BAR | | | | | | X | | |
| | | FORGING | X | | | | | | | |
| | | FORGED BAR | X | | | | | | | |
| | AUSTENITE COND AND TRANSFORMED AT 38F. AGED 1015F | SHEET | X | | | | | | | X |
| | | FORGING | X | | | | | | | X |
| | | ROLLED BAR | X | | | | | | | X |
| | H 950 | FORGED BAR | X | | | | | | | X |
| | | BAR | | | | | | | | X |
| | | EXTRUDED BAR | | | | | | | | X |
| | H1000 | SHEET | X | | | | | | | |
| | | PLATE | X | | | | | | | |
| | | FORGING | X | | | | | X | | |
| | | EXTRUSION | X | | | | | X | | |
| | | FORGED BAR | X | | | | | X | | |
| | | ROLLED BAR | X | | | | | X | | |
| BAR | | X | | | | | X | | | |
| BILLET | EXTRUDED BAR | | | | | | X | | | |
| | EXTRUDED BAR | | | | | | X | | | |
| H1025 | SHEET | X | | | | | | | | |
| | ROLLED BAR | X | | | | | | | | |
| H1050 | BAR | | | | | | | | X | |
| | EXTRUDED BAR | | | | | | | | X | |
| MILL 1700F. LAB 1050F 4HR | FORGING | X | | | | | | | | |
| | FORGING | X | | | | | | | | |
| | FORGING | X | | | | | | | | |
| MILL 1700F. LAB 1600F. 1000F 4HR | ROLLED BAR | X | | | | | | | | |
| | ROUND BAR | X | | | | | | | | |
| MILL 1700F. LAB 1500F. 1000F 4HR | ROLLED BAR | X | | | | | | | | |
| | ROUND BAR | X | | | | | | | | |
| R11 950 | ROLLED BAR | X | | | | | | | | |
| | ROUND BAR | X | | | | | | | | |
| R11 975 | ROLLED BAR | X | | | | | | | | |
| | ROUND BAR | X | | | | | | | | |

Table 3.0.1 (Con't)

AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KC | R | CURVES | DA/DN | DA/DT | KISCC |
|------------|----------------|-------------------------|-----|----|---|--------|-------|-------|-------|
| PH13-8PH | RH1000 | ROLLED BAR ROUND BAR | X | | | | | | X |
| | TYS=140KSI | PLATE | | | | | | | X |
| | TYS=160KSI | PLATE | | | | | | | X |
| | TYS=190KSI | PLATE | | | | | | | X |
| | TYS=200KSI | PLATE | | | | | | | X |
| | TYS=210KSI | PLATE | | | | | | | X |
| PH14-8PH | SRH1050 | SHEET | | | | X | | | |
| | RH 930 | ROLLED BAR BAR | X | | | | | | X |
| PH15-7PH | RH1050 | ROLLED BAR | X | | | | | | X |
| | TH1050 | BAR | | | | | | | X |
| 15-3PH | H 900 | ROLLED BAR BAR | X | | | | | | X |
| | H1025 | BAR | | | | | X | | |
| | H1150M | BAR | | | | | | | X |
| | TYS=150-165KSI | BILLET | | | | | | X | |
| | TYS=150-165KSI | FORGING | X | | | | | | |
| | | | | | | | | | |
| 15-5PH(2M) | H 900 | FORGING | | | | | | | X |
| | H1000 | FORGING | | | | | | | X |

Table 3.0.1 (Con't)

AVAILABLE DATA FOR STAINLESS STEEL ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DM | DA/DT | K1BCC |
|------------|----------------------------|----------------------|-----|-----|----------|-------|-------|-------|
| 15-5PH(VM) | H 700 | FORGING | | | | | | X |
| | H1090 | FORGING | | | | | | X |
| 17-4PH | H 900 | PLATE BAR | | | X | | | X |
| | H 975 | ROLLED BAR | X | | | | | |
| | H1000 | BAR | | | | | | X |
| | H1025 | ROUND BAR CASTING | X | | X | X | | |
| 17-7PH | H11 950 | BAR | | | | | | X |
| | H11050 | ROLLED BAR BAR | X | | | | | X |
| | H11050 | PLATE BAR | | | X | | | X |
| 304 | ANNEALED | SHEET PLATE | | | X | | | X |
| | ANNEALED & AGED | PLATE | | | X | | | X |
| 316 | ANNEALED | PLATE | | | X | | | X |
| | ANNEALED AT 1950F, 1HR, W0 | PLATE | | | X | | | X |
| 317 | W0 IN. FROM CENTERLINE | WELDMENT | | | X | | | X |
| | AT CENTERLINE | WELDMENT | | | X | | | X |
| | AT HEAT AFFECTED ZONE | WELDMENT | | | X | | | X |

Table 3.0.2

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | L-T | | T-L | | B-L | | | |
|--------------|--|-----------------|--------------------------------------|--------------------------|--------------|--------------------------|--------------|--------------------------|--------------|------|------|
| | | | | SPECIMEN MEAN THICK ° | STD. DEV. | SPECIMEN MEAN THICK ° | STD. DEV. | SPECIMEN MEAN THICK ° | STD. DEV. | | |
| AFC 77 (VAR) | 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | FORGING | 6.00 | 0.50 | 48.6 | 3.1 | 0.50 | 50.6 | 1.3 | --- | |
| | | | | 2.01 | 110.5 | 4.9 | 2.01 | 108.0 | 5.7 | --- | |
| CUSTOM 455 | 1500F 1HR.00. 950F 4HR. AC | FORGING | 4.00 | 0.48 | 72.1 | 7.8 | --- | --- | --- | --- | |
| | | | | 0.48 | 46.2 | 3.3 | --- | --- | --- | --- | |
| PH13-8MO | ANNEALED AUSTENITE COND FORCED BAR AND TRANSFORMED AT 36F. ARED 1015F | FORGING | 3.00 | 1.01 | 114.1 | 15.7 | 1.00 | 99.6 | 22.4 | --- | |
| | | | 2.20 | 1.63 | 103.0 | 19.4 | 1.63 | 89.6 | 1.8 | --- | |
| | | SHEET | 1.00-2.25 | 1.00 | 58.4 | 6.5 | 1.00 | 69.4 | 16.1 | --- | |
| | | | 4.00-8.00 | 1.00 | 70.3 | 16.0 | --- | --- | --- | --- | |
| | | ROLLED BAR | 2.25 | 1.00 | 66.9 | 2.9 | 1.00 | 63.5 | 1.7 | 0.75 | 74.1 |
| | | | 1.50-2.25 | 1.00 | 105.6 | 4.8 | 1.00 | 96.2 | 5.2 | --- | --- |
| H1000 | PLATE | 4.00 | 0.98 | 94.7 | 3.6 | --- | --- | --- | --- | | |
| | | 2.75-8.00 | 0.75 | 101.6 | 11.0 | 0.75 | 88.1 | 17.1 | --- | | |
| EXTRUSION | | 1.50 | 1.00 | 68.5 | 5.5 | 1.00 | 66.2 | 2.1 | --- | | |
| | | | | | | | | | | | |

* MINIMUM SPECIMEN THICKNESS (IN)

Table 3.0.2 (Con't)

FLANE STRAIN FRACTURE TOUGHNESS VALUES OF STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | L-T | | T-L | | B-L | |
|----------|------------------|-----------------|--------------------------------------|---------------------|----------------------|---------------------|----------------------|---------------------|----------------------|
| | | | | SPECIMEN THICK * | MEAN STD. DEV. | SPECIMEN THICK * | MEAN STD. DEV. | SPECIMEN THICK * | MEAN STD. DEV. |
| PH13-8MO | H1000 | FORGED BAR | 1.00 | 114.2 | 0.9 | 1.00 | 122.7 | 3.0 | --- |
| | | | 1.50 | 90.0 | 7.1 | 1.00 | 75.0 | 4.2 | --- |
| | | | 2.25 | 103.1 | 4.6 | 1.00 | 94.8 | 7.8 | 0.75 92.2 4.2 |
| PH15-7MO | RH 950 | ROLLED BAR | 1.25 | --- | --- | 1.00 | 30.6 | 0.1 | --- |
| | | ROLLED BAR | 1.25 | --- | --- | 1.00 | 40.2 | 1.5 | --- |
| 15-5PH | H 900 | ROLLED BAR | 2.25 | --- | --- | 1.00 | 72.7 | 4.5 | --- |
| | | FORGING | --- | --- | --- | 1.50 | 94.8 | 6.9 | --- |
| 17-7PH | RH1050 | ROLLED BAR | 1.25 | --- | --- | 1.00 | 47.0 | 0.7 | --- |

* MINIMUM SPECIMEN THICKNESS (IN).

Table 3.0.3.1

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR STAINLESS STEEL ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION Unknown

ENVIRONMENT: LAB AIR AT R. T.

STRESS RATIO: 0.05-0.10

FREQUENCY: 3.00-30.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) FOR DELTA K LEVELS (KSI SQRT(IN)) = | | | | | |
|-------|----------------------------|--------------|--------------|-----------|---|------|------|------|------|-------|
| | | | | | 2.5 | 3.0 | 10.0 | 20.0 | 50.0 | 100.0 |
| 304 | ANNEALED | SHEET | 0.05 | 10.00 | | .163 | 3.07 | | | |
| | ANNEALED | SHEET | 0.05 | 15.00 | | .133 | 2.83 | | | |
| | ANNEALED | SHEET | 0.10 | 1.67 | | | 2.86 | | | |
| | ANNEALED | SHEET | 0.10 | 6.00 | | | 2.56 | | | |
| 316 | ANNEALED & AGE | PLATE | 0.05 | 3.00 | | | 1.38 | | | |
| | ANNEALED AT 1950F. 1HR. WQ | PLATE | 0.05 | 10.00 | | | 2.39 | | | |
| 347 | .050 IN FROM CENTERLINE | WELDMENT | 0.10 | 30.00 | | | | | 9.83 | |
| | AT CENTERLINE | WELDMENT | 0.10 | 30.00 | | | | | 13.1 | |
| | AT HEAT AFFECTED ZONE | WELDMENT | 0.10 | 30.00 | | | | | 17.5 | |

Table 3.0.3.2

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE
STRESS INTENSITY FACTOR FOR STAINLESS STEEL ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION L-T ENVIRONMENT: LAB AIR AT R. T.
STRESS RATIO 0.00-0.10 FREQUENCY: 0.03-30.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN./CYCLE) FOR DELTA K LEVELS (KSI SQRT(IN)) = | | | | | | |
|------------|--------------|--------------|--------------|-------------|---|-----|------|------|------|-------|--|
| | | | | | 2.5 | 3.0 | 10.0 | 20.0 | 50.0 | 100.0 | |
| CUSTOM 455 | H1000 | FORGING | 0.10 | 10.00-30.00 | | | | 2.78 | | | |
| PH13-8MO | H1000 | FORGING | 0.10 | 1.00-10.00 | | | | 9.44 | 31.9 | 127. | |
| | H1000 | BAR | 0.02 | 1.00 | | | | | 31.6 | | |
| 17-4PH | H 900 | PLATE | 0.08 | 20.00 | | | 303 | 3.38 | 53.1 | | |
| 17-7PH | TH1030 | PLATE | 0.10 | 20.00 | | | 0232 | 433 | | | |
| 304 | ANNEALED | PLATE | 0.00 | .03 | | | | | | 56.0 | |
| | ANNEALED | PLATE | 0.00 | 6.67 | | | | 1.92 | 28.5 | | |

Table 3.0.3.3

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE
STRESS INTENSITY FACTOR FOR STAINLESS STEEL ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION T-L ENVIRONMENT: LAB AIR AT R.T.
STRESS RATIO 0.00-0.10 FREQUENCY: 1.00-30.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN./CYCLE) FOR DELTA K LEVELS (MSI SQRT(IN)) = |
|------------|--------------|--------------|--------------|-------------|--|
| | | | | | 2.5 5.0 10.0 20.0 50.0 100.0 |
| CUSTOM 435 | H1000 | FORGING | 0.10 | 10.00 | 25.0 |
| | H1000 | FORGING | 0.10 | 20.00 | 3.00 |
| | H1000 | FORGING | 0.10 | 20.00-30.00 | 2.58 |
| PH13-8ND | H1000 | FORGING | 0.10 | 1.00-10.00 | 5.37 32.1 143 |
| 15-5PH | H1025 | BAR | 0.05 | 10.00 | 15.3 155 |
| 17-4PH | H1025 | ROUND BAR | 0.10 | 30.00 | .0607 2.00 |
| 17-7PH | T1050 | PLATE | 0.10 | 20.00 | .0265 .388 4.44 |
| 304 | ANNEALED | PLATE | 0.00 | 6.60 | 1.86 32.5 |

TABLE 3.0.4

INDIVIDUAL STRESS CORROSION CRACKING THRESHOLD DATA FOR
STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ IT | PRODUCT FORM | SPECIMEN ORIENTATION | K _{ISCC} (ksi/in) | | | | |
|--------|---|-----------------|-------------------------|----------------------------|------------|--------------------------|------------|--|
| | | | | SUMP TANK WATER | 3.5% NaCl | ENVIRONMENTS 20% NaCl | | |
| | | | | SEACOAST | ATMOSPHERE | INDUST. | ATMOSPHERE | |
| AFC 77 | 1800F 1HR OQ, -100F 0.5 HR, 500F 2&2 HR, (Coarse G.S.) | P | --- | 15 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 700F 2&2 HR | B | --- | 50 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 800F 2&2 HR | B | --- | 40 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 900F 2&2 HR | B | --- | 15 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 1100F 2&2 HR | B | --- | 10 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 500F 2&2 HR, & 10PCT CM, 1000F | B | --- | 30 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 500 2&2 HR, & 10PCT CM, 700F | B | --- | 90 | | | | |
| | 2000F 1HR OQ, -100F 0.5 HR, 500F 2&2 HR, & 20 PCT CM, 700F | B | --- | 48 | | | | |
| | 2200F 1HR, 1900F 1HR OQ, -100F 1HR, -100F 1HR, 900F, 2&2 HR | P | T-L | 40 | | | | |
| | 2200F 1HR, 1900F 1HR OQ, -100F 1HR, -100F 1HR 1000F 2&2 HR | P | T-L | 45 | | | | |
| | 2200F 1HR, 1900F 1HR OQ, -100F 1HR, -100F 1HR, 1050F 2&2 HR | P | T-L | 37 | | | | |
| | AN 355 | SCT 850 | P | T-L | 8 | 24 | 45 | |
| | | | B | T-L | 6 | 18 | 18 | |
| | | SCT 1000 | P | T-L | 37 | 52 | 99 | |
| | | B | T-L | 28 | 35 | 66 | | |

Table 3.0.4 (Continued)

| ALLOY | CONDITION/ HT | PRODUCT FORM | SPECIMEN ORIENTATION | K _{ISCC} (Kai/in) | | | | |
|------------|------------------|-----------------|-------------------------|----------------------------|-----------|--------------------------|---------------------|--------------------|
| | | | | SUMP TANK WATER | 3.5% NaCl | ENVIRONMENTS 20% NaCl | SEACOAST ATMOSPHERE | INDUST. ATMOSPHERE |
| AM 362 | H900 | B | --- | | 12 | | | |
| | H1000 | B | --- | | 31 | | | |
| CUSTOM 455 | H900 | P | --- | | 60 | | | |
| | H950 | F | --- | | 72 | | | |
| PH13-8MO | H950 | F | T-L | | 74 | | | |
| | | FB | L-T | 48 | | 46 | 31 | 59 |
| | | B | T-L | | | | | |
| H1000 | | E | L-T | 55 | | | | |
| | | FB | L-T | 88 | | | | |
| | | FB | T-L | 100 | | | | |
| | | FB | L-T | 70 | | | | |
| | | B | T-L | | | 65 | 44 | 83 |
| H1050 | TYS=210 KSI | F | T-L | | 120 | | | |
| | | B | --- | | 14 | | | |
| PH15-7MO | H1050 | B | --- | | 18 | | | |
| | | B | --- | | | | | |
| 15-5 PH | H900 | B | --- | | 56 | 33 | 36 | 68 |
| | | P | --- | | | | | |
| 17-4 PH | H900 | B | --- | | 52 | | | |
| 17-7 PH | H1050 | B | T-L | | 16 | 65 | 12 | 24 |
| | | B | --- | | | | | |

Table 3.1.3.1

| CONDITION | --PRODUCT-- | | TEST SPEC YIELD STR ENVIRONMENT | STAINLESS STEEL | AFC 260 | K (IBCC) | SPECIMEN | | CRACK LENGTH K (S) | K (ISCC) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|-------------------------------------|-------------|---------------|------------------------------------|-----------------|---------|----------|---------------|---------------|-----------------------|----------|------|-------------|-----------------------|------------|
| | FORM | THICK (IN) | | | | | WIDTH (IN) | THICK (IN) | | | | | | |
| 2200F 1HR 1900F 1HR -320F 1HR | P | 0.36 | R.T. T-L | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 64.00 | 59.00* | | | | 1971 80685 | |
| 2200F 1HR 1900F 1HR -320F 1HR | P | 0.36 | R.T. T-L | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | | 37.00 | | | | 1971 80685 | |
| 2200F 1HR 1900F 1HR -320F 1HR | P | 0.36 | R.T. T-L | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 47.00 | 40.00 | | | | 1971 80685 | |
| 2200F 1HR 1900F 1HR -320F 1HR | P | 0.36 | R.T. T-L | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | | 45.00 | | | | 1971 80685 | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KIBCC/TYB)SQUARED

Table 3.2.2.1

| CONDITION | --PRODUCT-- | | YIELD STRENGTH (KSI) | SPECIMEN | | CRACK LENGTH (IN) | 2.9* CRACK LENGTH (K(IC)/TYS)**2 (IN) | K(IC) MEAN (KSI) STAM DEV (IN) | DATE | REFER |
|-----------------------------|-------------|---------------|----------------------|------------|------------|-------------------|---------------------------------------|--------------------------------|------|-----------|
| | FORM | THICK (IN) | | WIDTH (IN) | THICK (IN) | | | | | |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 173.0 | 1.500 | 0.500 | MB | 0.05 | 23.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 163.0 | 1.500 | 0.500 | MB | 0.11 | 38.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 208.0 | 1.500 | 0.500 | MB | 0.05 | 28.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 203.0 | 1.500 | 0.500 | MB | 0.19 | 49.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 224.0 | 1.500 | 0.500 | MB | 0.05 | 31.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 0.5HR. | P | 0.36 R.T. L-T | 232.0 | 1.500 | 0.500 | MB | 0.04 | 30.00 | 1969 | 74720 (1) |
| 1800F 1HR. 0G. -100F 1HR. | BR | 3.00 R.T. L-R | 185.0 | 1.500 | 0.480 | MB | 0.14 | 44.00 | 1968 | 64302 (1) |
| 1800F 1HR. 0G. -100F 1HR. | BR | 3.00 R.T. L-R | 213.0 | 1.500 | 0.480 | MB | 0.05 | 29.00 | 1968 | 64302 (1) |
| 1900F 1HR. 0G. -100F 1HR. | BR | 3.00 R.T. L-R | 222.0 | 1.500 | 0.480 | MB | 0.28 | 74.00 | 1968 | 64302 (1) |
| 2000F 1HR. 0G. -100F 1HR. | BR | 3.00 R.T. L-R | 207.0 | 1.500 | 0.480 | MB | 0.29 | 70.00 | 1969 | 76136 (1) |
| 2000F 1HR. 0G. -100F 1HR. | BR | 3.00 R.T. L-R | 214.0 | 1.500 | 0.480 | MB | 0.17 | 56.00 | 1969 | 76136 (1) |

NOTES:
 (1) COMPOSITION (WT PERCENT) 16C.0 18RN.0 013P.0 021S.0 13S1.0 21NI.14.0CR.5 02MO.13 4CO.0 23V.0 04N
 THESE DATA ARE AVERAGE VALUES

Table 3.2.3.1

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.2.3.1 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL AFC 77
CONDITION: AUSTENITIZED AT 2010F, QUENCHED & TEMPERED AT 810F

| K MAX (KSI*IN**1/2) | DA/DT (10**-3 IN/HOUR) | | | |
|------------------------|------------------------|---|---|---|
| | A | B | C | D |
| E= DISTILLED WATER | | | | |
| A: 20.00 | 1.01 | | | |
| B: 25.00 | 4.55 | | | |
| C: 30.00 | 2.67 | | | |
| D: 35.00 | 3.21 | | | |
| | 17.5 | | | |
| A: 47.00 | 5213. | | | |
| B: 47.00 | | | | |
| C: 47.00 | | | | |
| D: 47.00 | | | | |

ROOT MEAN SQUARE 62.42
PERCENT ERROR

CONDITION/HT: AUSTENITIZED AT 2010F, QUENCHED & TEMPERED AT 810F
 FORM: 0.08" TH SHEET
 SPECIMEN TYPE:
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 85544

STAIN.
STEEL

AFC 77

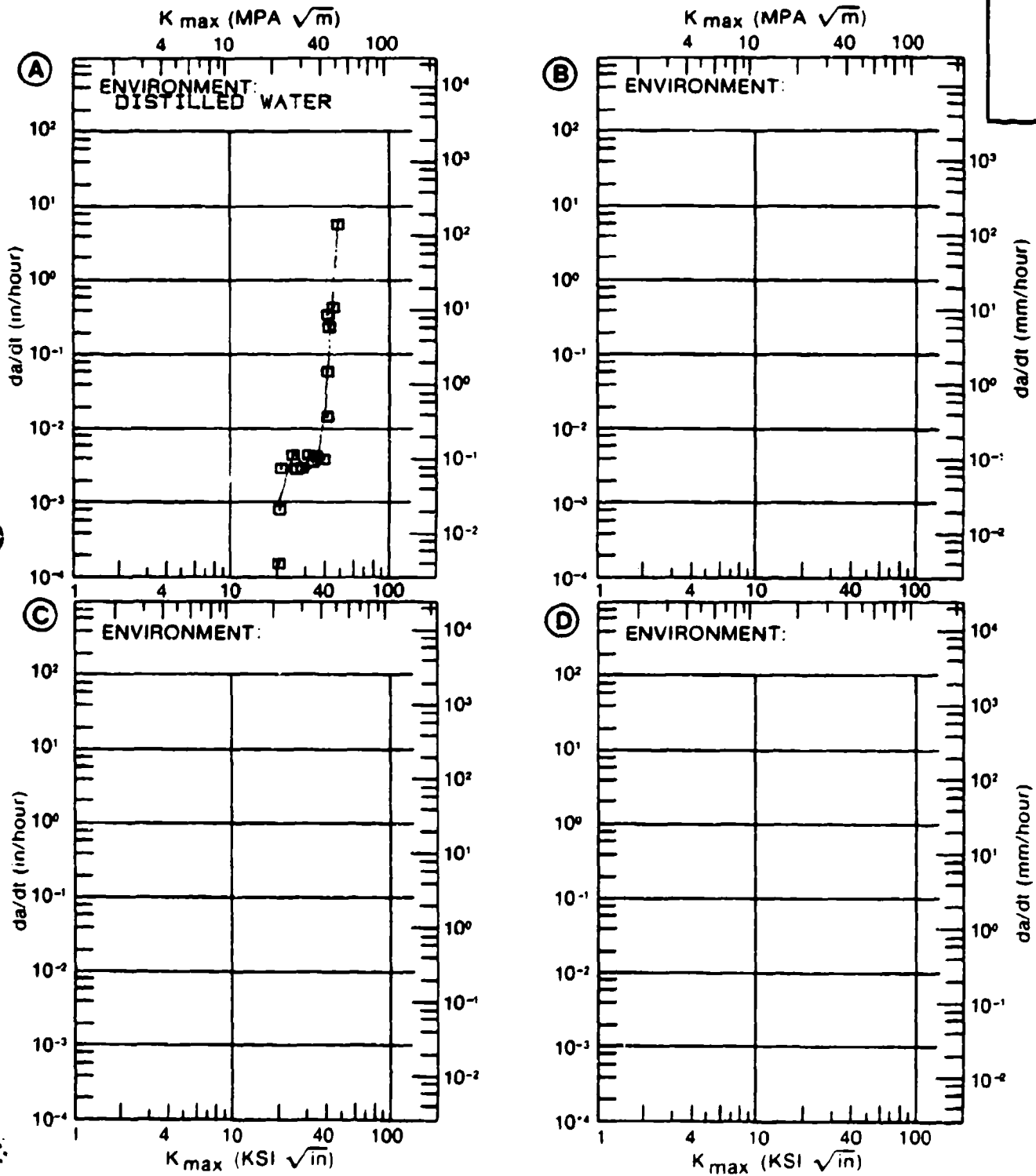


Figure 3.2.3.1

Table 3.2.3.2

| STAINLESS STEEL AFC 77 K(ISSC) | | | | | | | | | | | | | |
|--|--------------|------------|----------|----------------------|---------------|------------|------------|-------------|-------------------|---------|----------|-----------------|------------|
| CONDITION | PRODUCT FORM | THICK (IN) | TEMP (F) | SPEC YIELD STR (KSI) | ENVIRONMENT | WIDTH (IN) | SPECIMEN | | CRACK LENGTH (IN) | K(ISSC) | MEAN DEV | TEST TIME (MIN) | DATE REFER |
| | | | | | | | THICK (IN) | DESIGN (IN) | | | | | |
| 1800F 1HR OG. P -100F 0 5HR. 500F 2+2 HR (COARSE GRAINED STRUCTURE) | P | 0.56 | R T | 154.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 119.00 | 82.00* | | 1969 74720 | |
| 1800F 1HR OG. P -100F 0 5HR. 1100F 2+2 HR (COARSE GRAINED STRUCTURE) | P | 0.56 | R T | 173.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 23.00 | 15.00 | | 1969 74720 | |
| 1800F 1HR OG. P -100F 0 5HR. 500F 2+2 HR (FINE GRAINED STRUCTURE) | P | 0.56 | R T | 196.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 111.00 | 97.00* | | 1969 74720 | |
| 1800F 1HR OG. P -100F 0 5HR. 1100F 2+2 HR (FINE GRAINED STRUCTURE) | P | 0.56 | R T | 232.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 30.00 | 20.00 | | 1969 74720 | |
| 2000F 1HR OG. B -100F 0 5HR. 1400F 2+2 HR | B | 3.00 | R T | 150.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 116.00 | 80.00* | | 1969 76136 | |
| 2000F 1HR OG. B -100F 0 5HR. 500F 2+2HR | B | 3.00 | R T | 169.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 200.00 | 109.00* | | 1969 76136 | |
| 2000F 1HR OG. B -100F 0 5HR. 700F 2+2 HR | B | 3.00 | R T | 180.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 160.00 | 50.00 | | 1969 76136 | |
| 2000F 1HR OG. B -100F 0 5HR. 800F 2+2 HR | B | 3.00 | R T | 207.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 70.00 | 40.00 | | 1969 76136 | |
| 2000F 1HR OG. B -100F 0 5HR. 900F 2+2 HR | B | 3.00 | R T | 214.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 56.00 | 35.00 | | 1969 76136 | |
| 2000F 1HR OG. B -100F 0 5HR. 1100F 2+2 HR | B | 3.00 | R T | 221.0 | 3.5 PCT NAACL | 1.500 | 0.480 | CANT* | 43.00 | 10.00 | | 1969 76136 | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(K(ISSC)/TYS)SQUARED

Table 3.2.3.2 (Continued)

| CONDITION | --PRODUCT-- | | TEST SPEC | | STAINLESS STEEL | AFC | 77 | K(IISCC) | SPECIMEN | | CRACK | K(IISCC) | MEAN | STAN | TEST | DATE REFER |
|---|-------------|-------|-----------|------|-----------------|------|------|----------|----------|-------|-------|----------|--------|--------|---------|------------|
| | FORM | THICK | TEMP | DR | | | | | WIDTH | THICK | | | | | | |
| | (IN) | (F) | (RBI) | (IN) | (IN) | (IN) | (IN) | (IN) | (IN) | (IN) | (MIN) | | | | | |
| 2000F 1HR 0G, B -100F 0.5HR 500F 2+2HR + 10 PCT CM. 1000F | B | 3 00 | R.T. | --- | 252.0 | 3.5 | PCT | NACL | 1.500 | 0.480 | CANT* | --- | 60.00 | 30.00 | --- | 1969 76136 |
| 2000F 1HR 0G, B -100F 0.5HR 500F 2+2HR + 10 PCT CM. 700F | B | 3 00 | R.T. | --- | 277.0 | 3.5 | PCT | NACL | 1.500 | 0.480 | CANT* | --- | 106.00 | 90.00 | --- | 1969 76136 |
| 2000F 1HR 0G, B -100F 0.5HR 500F 2+2HR + 20 PCT CM. 700F | B | 3 00 | R.T. | --- | 297.0 | 3.5 | PCT | NACL | 1.500 | 0.480 | CANT* | --- | 107.00 | 48.00 | --- | 1969 76136 |
| 2100F 1HR. FC TO 1900F HOLD 1HR. 0G. -100F 4HR. 500F 2+2 HR | F | 10.00 | R.T. | L-T | 165.8 | 3.5 | PCT | NACL | 20.000 | 0.500 | MB | * | 0.400 | 108.00 | > 10.00 | 1973 87360 |
| 2100F 1HR. FC TO 1900F HOLD 1HR. 0G. -100F 4HR. 500F 2+2 HR | F | 10.00 | R.T. | T-L | 164.6 | 3.5 | PCT | NACL | 13.000 | 0.500 | MB | * | 0.400 | 110.00 | > 10.00 | 1973 87360 |

Table 3.3.2.1

STAINLESS STEEL AFC 77 (VAR) (IC)

| CONDITION | --PRODUCT-- | | TEST SPECIMEN | | YIELD STRENGTH (KSI) | ---SPECIMEN--- | | CRACK LENGTH (IN) | 2.9 (IN) | K(1C) MEAN (IN) | K(1C) STAN DEV (IN) | DATE | REFER |
|---|-------------|------------|---------------|--------|----------------------|----------------|------------|-------------------|----------|-----------------|---------------------|----------------|-------|
| | FORM | THICK (IN) | TEMP (F) | ORIENT | | WIDTH (IN) | THICK (IN) | | | | | | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | - 65 | L-T | 210.0 | 1.002 | 0.501 NB | 0.510 | 0.10 | 41.30 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | R.T. | L-T | 192.0 | 1.002 | 0.501 NB | 0.523 | 0.19 | 33.40 | 41.9/ 0.8 | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | - 65 | T-L | 210.0 | 1.002 | 0.501 NB | 0.523 | 0.11 | 43.30 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | R.T. | T-L | 194.0 | 1.002 | 0.501 NB | 0.520 | 0.16 | 52.40 | 47.9/ 6.4 | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | - 65 | L-T | 210.0 | 1.002 | 0.501 NB | 0.510 | 0.17 | 32.60 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | R.T. | L-T | 194.0 | 1.002 | 0.501 NB | 0.513 | 0.18 | 50.70 | 50.8/ 1.3 | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | - 65 | T-L | 210.0 | 1.002 | 0.501 NB | 0.513 | 0.16 | 52.00 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | R.T. | T-L | 194.0 | 1.002 | 0.501 NB | 0.515 | 0.17 | 49.90 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | - 65 | L-T | 210.0 | 1.002 | 0.501 NB | 0.515 | 0.17 | 51.00 | | 1973 87360 (1) | |
| 1700F 1HR.00 2100F 1HR. MOVED TO FCE AT 1933F. HELD 1HR.00. -100F 24HR. 900F. 2+2HR | F | 6.00 | R.T. | L-T | 194.0 | 1.002 | 0.501 NB | 0.515 | 0.17 | 50.40 | | 1973 87360 (1) | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | - 65 | L-T | 180.0 | 0.995 | 0.495 NB | 0.477 | 0.46 | 77.70 | | 1973 87360 | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | R.T. | L-T | 165.0 | 4.000 | 2.007 CT | 2.090 | 1.19 | 114.00 | | 1973 87360 | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | - 65 | T-L | 180.0 | 0.995 | 0.497 NB | 0.490 | 0.35 | 67.10 | | 1973 87360 | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | R.T. | T-L | 166.0 | 4.000 | 2.006 CT | 2.070 | 0.98 | 104.00 | | 1973 87360 | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | - 65 | L-T | 180.0 | 0.994 | 0.497 NB | 0.533 | 0.42 | 73.90 | 70.5/ 4.8 | 1973 87360 | |
| 2100F 1HR. MOVED TO FCE AT 1900F. HELD 1HR.00. -100F 4HR. 500F 2+2HR | F | 6.00 | R.T. | T-L | 166.0 | 4.000 | 2.007 CT | 2.110 | 1.14 | 112.00 | 108.0/ 5.7 | 1973 87360 | |

NOTES (1) COMPOSITION (WT PERCENT) 15C.0 08MN.0 012P.0 0045.0 20SI.1 17NI.13 7CR.5 02MO.13 5CO.0 30V.0 18CB.0 02ON

Table 3.4.3.1

| CONDITION | --PRODUCT-- | | TEST SPEC YIELD | | ENVIRONMENT | WIDTH | | THICK DESIGN | | CRACK | | K (ISCC) | STAN | TEST | DATE | REFER |
|-------------|-------------|-------|-----------------|-------|----------------|-------|-------|--------------|------|--------|---------|----------|------|---------|------|-------|
| | FORM | THICK | TEMP | OR | | (IN) | (IN) | (IN) | (IN) | (IN) | (IN) | | | | | |
| | | (F) | (KSI) | | | W | B | A | B | A | B | | | (MIN) | | |
| MOD SCT1000 | B | 2.25 | R.T. | 163.2 | 3.5 PCT NAACL | 1.900 | 0.480 | CANT | --- | 117.00 | 117.00* | | | > 30000 | 1971 | 84333 |
| SCT 850 | P | 1.13 | R.T. | 152.3 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | --- | 48.00 | 45.00 | | | --- | 1973 | 86688 |
| SCT 850 | P | 1.13 | R.T. | 152.3 | SEACAST ATM | 2.000 | 1.000 | CT | --- | 48.00 | 24.00 | | | --- | 1973 | 86688 |
| SCT 850 | P | 1.13 | R.T. | 152.5 | 20PCT NAACL | 2.000 | 1.000 | CT | --- | 48.00 | 8.00 | | | --- | 1973 | 86688 |
| SCT 850 | B | 2.25 | R.T. | 180.0 | 3.5 PCT NAACL | 1.900 | 0.480 | CANT | --- | 59.20 | 32.50 | | | > 30000 | 1971 | 84333 |
| SCT 850 | B | 2.00 | R.T. | 190.3 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | --- | 36.60 | 18.00 | | | --- | 1973 | 86688 |
| SCT 850 | B | 2.00 | R.T. | 190.3 | SEACAST ATM | 2.000 | 1.000 | CT | --- | 36.60 | 18.00 | | | --- | 1973 | 86688 |
| SCT 850 | B | 2.00 | R.T. | 190.3 | 20 PCT NAACL | 2.000 | 1.000 | CT | --- | 36.60 | 6.00 | | | --- | 1973 | 86688 |
| SCT1000 | P | 1.13 | R.T. | 169.7 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | --- | 104.70 | 99.00 | | | --- | 1973 | 86688 |
| SCT1000 | P | 1.13 | R.T. | 169.7 | SEACAST ATM | 2.000 | 1.000 | CT | --- | 104.70 | 52.00 | | | --- | 1973 | 86688 |
| SCT1000 | P | 1.13 | R.T. | 169.7 | 20 PCT NAACL | 2.000 | 1.000 | CT | --- | 104.70 | 37.00 | | | --- | 1973 | 86688 |
| SCT1000 | B | 2.25 | R.T. | 171.2 | 3.5 PCT NAACL | 1.900 | 0.480 | CANT | --- | 88.40 | 88.40* | | | > 30000 | 1971 | 84333 |
| SCT1000 | B | 2.00 | R.T. | 172.4 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | --- | 70.00 | 66.00 | | | --- | 1973 | 86688 |
| SCT1000 | B | 2.00 | R.T. | 172.4 | SEACAST ATM | 2.000 | 1.000 | CT | --- | 70.00 | 35.00 | | | --- | 1973 | 86688 |
| SCT1000 | B | 2.00 | R.T. | 172.4 | 20 PCT NAACL | 2.000 | 1.000 | CT | --- | 70.00 | 28.00 | | | --- | 1973 | 86688 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISCC/TYS)SQUARED

Table 3.5.3.1

| CONDITION | STAINLESS STEEL AM 362 | | K (IBCC) | | ENVIRONMENT | YIELD STR (KSI) | TEST TEMP OR STR (F) | PRODUCT-- FORM THICK (IN) | SPECIMEN-- | | CRACK LENGTH (IN) | K (IBCC) | K (IBCC) MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER | | | |
|-----------|------------------------|------------|-------------|------------|-------------|-----------------|----------------------|------------------------------|------------|-------|-------------------|----------|---------------|----------|-----------------|------------|-------|------|-------|
| | WIDTH (IN) | THICK (IN) | DESIGN (IN) | THICK (IN) | | | | | | | | | | | | | | | |
| H 900 | 1.500 | 0.480 | CANT | 30.20 | 12.50 | | | 2.25 | R.T. | 200.3 | 3.5 | PCT | MACL | 1.500 | 0.480 | CANT | 42000 | 1971 | 84333 |
| H1000 | 1.500 | 0.480 | CANT | 40.10 | 31.00 | | | 2.25 | R.T. | 178.9 | 3.5 | PCT | MACL | 1.500 | 0.480 | CANT | 36000 | 1971 | 84333 |

Table 3.6.3.1

| CONDITION | ---PRODUCT--- FORM THICK (IN) | | TEST TEMP OR (F) | SPEC OR (KSI) | YIELD (KSI) | ENVIRONMENT | STAINLESS STEEL AM 364 K (ISCC) | | K (ISCC) | | STAN DEV | TEST TIME (MIN) | DATE REFER | |
|-----------|----------------------------------|------------|------------------|---------------|-------------|---------------|------------------------------------|-------------|-------------------|--------------------|----------|-----------------|------------|------------|
| | WIDTH (IN) | THICK (IN) | | | | | DESIGN (IN) | LENGTH (IN) | CRACK LENGTH (IN) | MEAN (RSI*SORT IN) | | | | |
| H 850 | F | 3 00 | R T | T-L | 183 3 | 3 5 PCT NAACL | 1 500 | 0 480 | CANT | ----- | 131 00 | 93 00* | > 60000 | 1971 84333 |
| H 950 | F | 3 00 | R T | T-L | 186 7 | 3 5 PCT NAACL | 1 500 | 0 410 | CANT | ----- | 128 00 | 128 00* | > 60000 | 1971 84333 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KISCC/TYS)SQUARED

Table 3.7.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
STAINLESS STEEL ALLOY CUSTOM 435 AT ROOM TEMPERATURE

| CONDITION/MT | MEAN K _{IC} ± STANDARD DEVIATION | | EDGING |
|--------------------------------|---|------|--------|
| | (ABS) | (IN) | |
| | L-I | L-I | E-I |
| 1500F 1HR. 00. 950F 4HR. AC | 72.1 ± 7.0 (2) | --- | --- |
| 1500F 1HR. 00. 900F 4HR. AC | 46.2 ± 3.3 (3) | --- | --- |

Table 3.7.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL CUSTOM 433

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-------------------------------|---|---|----|----|----|-----|---|
| H1040 | FORGING | 0.10 | 10.00-30.00 | | | | | | | | 2.78 |
| H1050 | FORGING | 0.30 | 10.00-30.00 | | | | | | | | 3.72 |

Table 3.7.1.3

FATIGUE CRACK GROWTH RATE AT DELTA K LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL CUSTOM 409

TEST CONDITIONS

SPECIMEN ORIENTATION 1-1

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HIT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---------------|--------------|--------------|-------------|-------------------------------|---|
| H1000 | FORGING | 0.10 | 10.00 | 2.5 | 50 |
| H1000 | FORGING | 0.10 | 20.00 | 5 | 20 |
| H1000 | FORGING | 0.10 | 20.00-30.00 | 10 | 10 |
| | | | | 25 | 25.0 |
| | | | | 3.00 | 3.00 |
| | | | | 2.58 | 2.58 |

Table 3.7.2.1

| CONDITION | --PRODUCT-- | | TEST SPECIMEN | | YIELD STRENGTH (KSI) | | WIDTH (IN) | | SPECIMEN THICK (IN) | | DESIGN | | CRACK LENGTH (IN) | | 2.5% K(IIC)/TYS)±2 | | K(IIC) MEAN DEV | | DATE | REFER | |
|--------------------------------|-------------|------------|---------------|--------|----------------------|-------------|------------|-------|---------------------|-------|--------|-------|-------------------|-------|--------------------|------------|-----------------|-------|-------|-------|-------|
| | FORM | THICK (IN) | THICK (IN) | ORIENT | STRENGTH (KSI) | YIELD (KSI) | M | B | A | B | M | B | A | B | (KSI) STAN | (KSI) STAN | | | | | |
| 1500F 1HR. DB. 950F 4HR. AC | F | 4.00 | R.T. | L-T | 246.0 | 246.0 | 1.500 | 0.480 | 0.480 | 0.480 | 0.480 | 0.480 | 0.310 | 0.310 | 0.25 | 0.18 | 77.60 | 66.60 | 72.1/ | 7.8 | 77934 |
| 1500F 1HR. DB. 900F 4HR. AC | F | 4.00 | R.T. | L-T | 255.0 | 255.0 | 1.500 | 0.480 | 0.480 | 0.480 | 0.480 | 0.480 | 0.320 | 0.320 | 0.07 | 0.07 | 47.70 | 42.40 | 44.2/ | 3.3 | 77934 |

TABLE 3.7.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.7.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL CUSTOM 455
CONDITION: H1000
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | | |
| DELTA K MIN | A: 10.07 | 281 | | | |
| | B: 12.71 | | 1.04 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .699 | 1.10 | | |
| | 16.00 | 1.39 | 1.99 | | |
| 20.00 | 2.78 | 3.72 | | | |
| 25.00 | 4.91 | | | | |
| 30.00 | 6.90 | | | | |
| DELTA K MAX | A: 32.83 | 8.14 | | | |
| | B: 23.86 | | 5.31 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.51 | 2.74 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 3 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 2.50" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 10.0 - 30.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 195.0 KSI
 ULT. STRENGTH: 204.4 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 2.100"
 REFERENCES: R1004

STAIN.
STEEL

CUSTOM
455

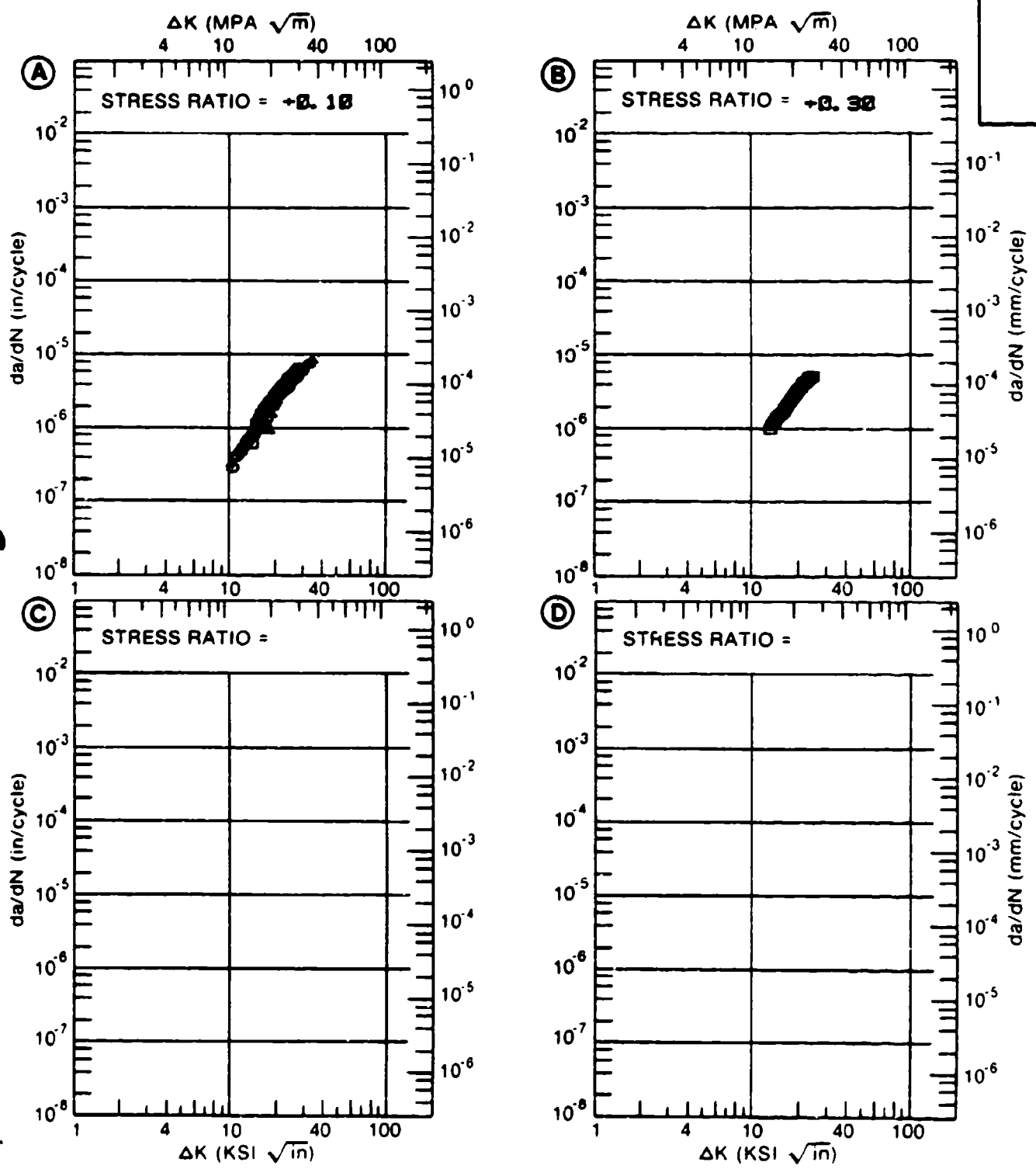


Figure 3.7.3.1

TABLE 3.7.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.7.3.2 INDICATING EFFECT
OF FREQUENCY

MATERIAL: STAINLESS STEEL CUSTOM 455
CONDITION: H1000
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|-------------|-------------|---|
| | | A | B | C | D |
| | | F(HZ)= 5.0 | F(HZ)= 10.0 | F(HZ)= 20.0 | |
| DELTA K MIN | A: 62.02 | 39.7 | | | |
| | B: 25.12 | | 4.98 | | |
| | C: 12.70 | | | .739 | |
| | D: | | | | |
| | 13.00 | | | .703 | |
| | 16.00 | | | 1.04 | |
| | 20.00 | | | 3.00 | |
| | 25.00 | | | 3.70 | |
| | 30.00 | | 7.09 | | |
| | 35.00 | | 10.0 | | |
| 40.00 | | 13.9 | | | |
| 50.00 | | 25.0 | | | |
| 60.00 | | | | | |
| 70.00 | 68.9 | | | | |
| DELTA K MAX | A: 76.71 | 82.1 | | | |
| | B: 56.40 | | 35.0 | | |
| | C: 25.96 | | | 3.16 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.70 | 9.22 | 22.29 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | 1 | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 2.50" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 105.0 KSI
 ULT. STRENGTH: 204.4 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 2.100"
 REFERENCES: R1004

STAIN.
 STEEL

CUSTOM
 455

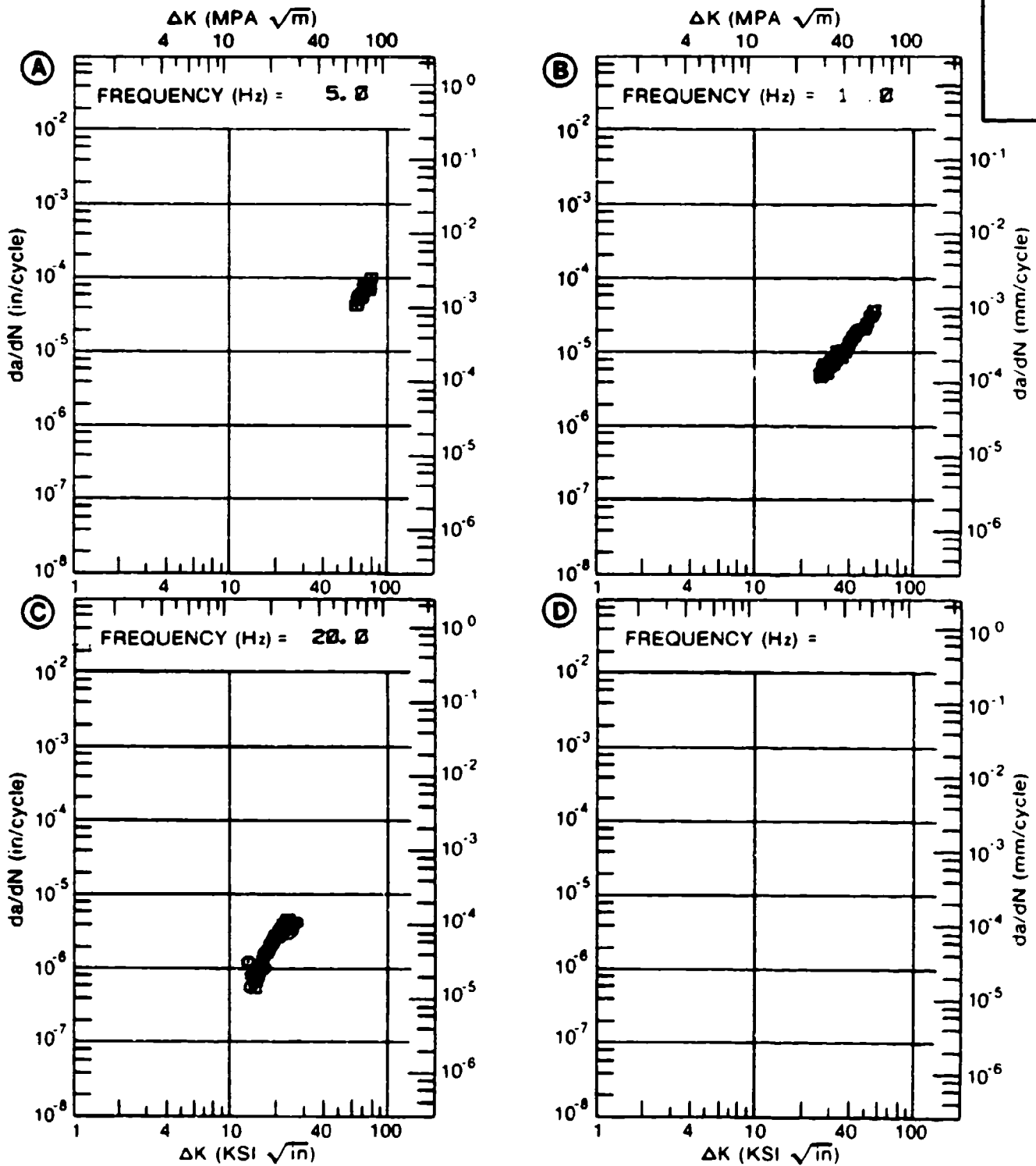


Figure 3.7.3.2

TABLE 3.7.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.7.3.3 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL CUSTOM 455
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | DA/DN (10 ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|-------------------------------------|-----------------|---|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | E=- 100F AIR | | |
| DELTA K B: MIN | A: 10.09 | .256 | | |
| | 13.00 | .828 | | |
| | 16.00 | 1.43 | | |
| | 20.00 | 2.58 | | |
| | 25.00 | 4.75 | | |
| DELTA K B: MAX | A: 27.10 | 6.32 | | |
| | | | | |

ROOT MEAN SQUARE 13.93 0.00
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 3
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H1000
 FORM: 2.50" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 20.0 - 30.0 HZ

YIELD STRENGTH: 195.0 - 205.0 KSI
 ULT. STRENGTH: 204.4 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 2.100"
 REFERENCES: RI004

STAIN.
STEEL

CUSTOM
453

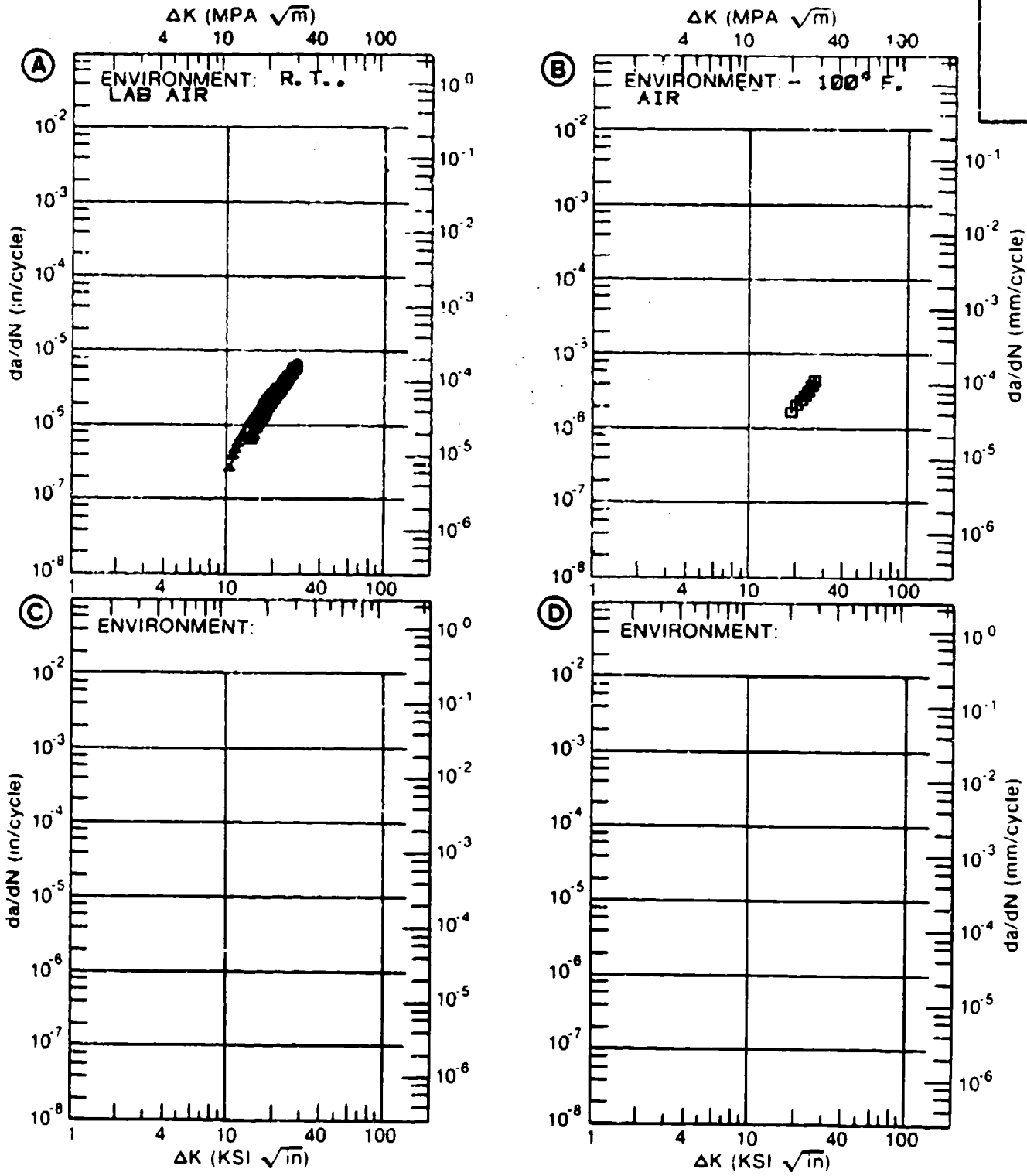


Figure 3.7.3.3

Table 3.7.3.4

| CONDITION | STAINLESS STEEL CUSTOM 435 K(ISSC) | | | | | | | | | | | | | |
|-----------|------------------------------------|------------|---------------|-------------------|-------------|--------------|------------|------------|-------------------|--------------------|----------|----------|-----------------|------------|
| | FORM | THICK (IN) | TEST TEMP (F) | SPEC OR STR (KSI) | YIELD (KSI) | ENVIRONMENT | SPECIMEN | | CRACK LENGTH (IN) | K(I) (KSI*SQRT IN) | MEAN DEV | STAN DEV | TEST TIME (MIN) | DATE REFER |
| | | | | | | | WIDTH (IN) | THICK (IN) | | | | | | |
| H 500 | F | 4 00 | R T | --- | 255.0 | 3.5 PCT NACL | 1.300 | 0.500 | CANT | --- | 62.00 | 60 00 | > 60000 | 1969 77934 |
| H 550 | F | 4 00 | R T | --- | 246.0 | 3.5 PCT NACL | 1.300 | 0.480 | CANT | --- | 72.10 | 72 10 | > 60000 | 1971 84333 |

Table 3.8.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
STAINLESS STEEL ALLOY PH13-8ND AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|------------------|---|-----------------------|
| ROD | | |
| CONDITION/HT | K _{IC} | N |
| H 950 | 58.4 ± 6.5 (2) | 69.4 ± 16.1 (4) |
| H1000 | 103.6 ± 4.8 (6) | 96.2 ± 9.2 (4) |
| PLATE | | |
| CONDITION/HT | K _{IC} | N |
| H1000 | 94.7 ± 3.6 (3) | --- |
| FORGING | | |
| CONDITION/HT | K _{IC} | N |
| ANNEALED | 114.1 ± 15.7 (5) | 99.6 ± 22.4 (6) |
| H 950 | 70.3 ± 16.0 (9) | --- |
| H1000 | 101.6 ± 11.0 (12) | 88.1 ± 17.1 (7) |
| EXTRUSION | | |
| CONDITION/HT | K _{IC} | N |
| H1000 | 68.5 ± 5.5 (8) | 66.2 ± 2.1 (6) |

Table 3.8.1.1.1 (Continued)

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
STAINLESS STEEL ALLOY PH13-8GD AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (MSI SQRT(IN)) DEVIATION | | (NUMBER OF SPECIMENS) |
|---|---|-----------------|-----------------------|
| | L-I | I-I | |
| FORGED BAR | | | |
| AUSTENITE COND AND TRANSFORMED AT 38F. ACED 1013F | 103.0 ± 19.4 (2) | 89.6 ± 1.8 (2) | ----- |
| H1000 | 114.2 ± 0.9 (2) | 122.7 ± 3.0 (3) | ----- |
| ROLLED BAR | | | |
| H 950 | 66.9 ± 2.9 (3) | 63.5 ± 1.7 (6) | 74.1 ± 2.1 (3) |
| H1000 | 90.0 ± 7.1 (2) | 75.0 ± 4.2 (2) | ----- |
| H1050 | 103.1 ± 4.6 (3) | 94.8 ± 7.8 (6) | 92.2 ± 4.2 (2) |

Table 3.8.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8W

TEST CONDITIONS

SPECIMEN ORIENTATION: L-T ENVIRONMENT: DRY AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K (LEVELS (KSI SQRT(IN))) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|------------|---------------------------------|-----|---|------|------|------|-----|
| H1000 | FORCED BAR | 0.10 | 6.00 | | | | 0.23 | 3.07 | 29.6 | |
| H1000 | FORGED BAR | 0.70 | 6.00 | | | | 0.58 | 4.17 | | |
| H1000 | FORGED BAR | 0.50 | 6.00 | | | | 0.64 | 4.79 | | |

Table 3.8.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8MO

TEST CONDITIONS

SPECIMEN ORIENTATION: L-T

ENVIRONMENT: L.H.A.
AT - 65 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
|--------------|--------------|--------------|------------|-------------------------------|---|------|------|------|----|-----|--|
| | | | | | 2.5 | 5 | 10 | 20 | 50 | 100 | |
| EXTRUDED BAR | | | | | 0.08 | 6.00 | 1.32 | 21.6 | | | |
| H1000 | EXTRUDED BAR | 0.08 | 6.00 | | | 0.23 | 2.87 | | | | |
| H1000 | ROLLED BAR | 0.08 | 6.00 | | | | 1.67 | | | | |

Table 3.8.1.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8W

TEST CONDITIONS

SPECIMEN ORIENTATION L-L

ENVIRONMENT: L.H.A. AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K (LEVELS (KSI SQRT(IN))) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|------------|---------------------------------|-----|------|------|------|------|-----|
| | EXTRUDED BAR | 0.00 | 6.00 | | | | | 2.22 | 20.8 | |
| | EXTRUDED BAR | 0.30 | 6.00 | | | | | 2.98 | | |
| H1000 | FORCED BAR | 0.08 | 6.00 | | | | | 5.82 | | |
| H1000 | FORCED BAR | 0.30 | 6.00 | | | | | 4.70 | | |
| H1000 | FORCED BAR | 0.50 | 6.00 | | | 0.91 | 4.70 | | | |
| H1000 | BILLET | 0.00 | 6.00 | | | 0.34 | 4.02 | | | |
| H1000 | EXTRUDED BAR | 0.08 | 6.00 | | | 0.33 | 3.73 | 34.4 | | |
| H1000 | EXTRUDED BAR | 0.50 | 6.00 | | | 0.85 | 5.59 | | | |
| H1000 | ROLLED BAR | 0.08 | 1.00 | | | 0.29 | 3.37 | | | |
| H1000 | ROLLED BAR | 0.00 | 6.00 | | | 0.29 | 3.40 | | | |
| H1000 | ROLLED BAR | 0.30 | 6.00 | | | 0.62 | 4.39 | | | |
| H1000 | ROLLED BAR | 0.50 | 6.00 | | | 0.79 | 5.09 | | | |

Table 3.8.1.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL PH13-8MU

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K (LEVELS (KSI SQRT(IN))) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|---------------------------------|---|
| | | | | 2.5 | 5 10 20 50 100 |
| H1000 | FORGING | 0.10 | 1.00-10.00 | | 9.44 31.9 127 |
| H1000 | BAR | 0.02 | 1.00 | | 31.6 |

Table 3.8.1.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL PH13-8PH

TEST CONDITIONS

SPECIMEN ORIENTATION: L-T

ENVIRONMENT: H.M.A.
 AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|------------|-------------------------------|-----|---|------|------|-----|-----|
| H1000 | FORGED BAR | 0.10 | 1.00 | | | | 0.29 | 7.56 | 103 | |
| H1000 | FORGED BAR | 0.30 | 1.00 | | | | 0.81 | 11.3 | 129 | |
| H1000 | FORGED BAR | 0.50 | 1.00 | | | | 0.94 | 12.5 | | |

Table 3.8.1.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL PH13-8ND

TEST CONDITIONS

SPECIMEN ORIENTATION: L-T

ENVIRONMENT: S.T.M.
 AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
|--------------|--------------|--------------|------------|-------------------------------|---|---|------|------|----|-----|------|
| | | | | | 2.5 | 5 | 10 | 20 | 50 | 100 | |
| | EXTRUDED BAR | 0.08 | 1.00 | | | | | | | | 2.85 |
| H1000 | EXTRUDED BAR | 0.08 | 1.00 | | | | 0.64 | 7.11 | | | |
| H1000 | ROLLED BAR | 0.08 | 1.00 | | | | | 4.13 | | | |
| H1000 | ROLLED BAR | 0.30 | 1.00 | | | | 0.64 | 12.2 | | | |
| H1000 | ROLLED BAR | 0.08 | 0.10 | | | | | 6.44 | | | |

Table 3.8.1.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8W

TEST CONDITIONS

SPECIMEN ORIENTATION: T-L

ENVIRONMENT: DRY AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (MSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|-----|---|------|------|------|-----|---|
| H1000 | FORGED BAR | 0.10 | 6.00 | | | | 0.26 | 3.14 | 24.3 | | |
| H1000 | FORGED BAR | 0.30 | 6.00 | | | | 0.42 | 4.17 | 37.1 | | |
| H1000 | FORGED BAR | 0.50 | 6.00 | | | | 0.51 | 4.60 | | | |

Table 3.8.1.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8PH

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: L.H.A.
AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | |
|--------------|--------------|--------------|-----------|-------------------------------|---|------|------|----|
| | | | | | 2.5 | 5 | 10 | 20 |
| H1000 | BILLET | 0.08 | 6.00 | | 0.34 | 3.47 | 31.3 | |
| H1000 | ROLLED BAR | 0.08 | 6.00 | | | 4.01 | | |

Table 3.8.1.10

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL PH13-8ND

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: H.M.A.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 30 | 100 |
|--------------|--------------|--------------|------------|---|-----|---|------|------|-----|-----|
| | | | | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
| H1000 | FORGED BAR | 0.10 | 1.00 | | | | | 6.71 | 108 | |
| H1000 | FORGED BAR | 0.30 | 1.00 | | | | 0.54 | 9.37 | 215 | |
| H1000 | FORGED BAR | 0.50 | 1.00 | | | | 1.08 | 11.6 | 607 | |

Table 3.8.1.11

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL 7H13-8M0

TEST CONDITIONS

SPECIMEN ORIENTATION T-1

ENVIRONMENT: S.T.M.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SORT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|-----|---|------|------|----|-----|---|
| H1000 | FORGED BAR | 0.08 | 1.00 | | | | | | | | 18.3 |
| H1000 | ROLLED BAR | 0.08 | 1.00 | | | | 0.28 | 6.43 | | | |

Table 3.8.2.1

| CONDITION | STAINLESS STEEL PH13-8MO | | | | | | | | | | K(IIC) | | DATE | REFER |
|--|--------------------------|------------|-------------|-----------------|------------|------------|--------|-------------------|--------------------------|---------------------------|-------------|------|-------|-------|
| | - PH13-8MO FORK | THICK (IN) | YIELD (KSI) | SPECIMEN ORIENT | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | 2.5* (K(IIC)/TVS)** (IN) | K(IIC) MEAN (KSI/ROOT IN) | STAN DEV | | | |
| | | | | | | | | | | | | A | | |
| ANNEALED | F | 3 00 | R T | L-T | 3 978 | 2 003 | CT | 2 073 | 0 66 | 103 80 | | 1976 | MC001 | |
| | | 3 00 | | | 4 000 | 2 003 | CT | 2 043 | 0 52 | 92 12 | | 1976 | MC001 | |
| | | 3 00 | | | 3 997 | 1 996 | CT | 2 058 | 1 02 | 128 41 | | 1976 | MC001 | |
| | | 3 00 | | | 2 000 | 1 007 | CT | 1 026 | 0 94 | 126 90 | | 1976 | MC001 | |
| ANNEALED | F | 3 00 | R T | T-L | 4 000 | 1 999 | CT | 2 057 | 0 83 | 119 40 | 114.1/ 15.7 | 1976 | MC001 | |
| | | 3 00 | | | 3 999 | 1 996 | CT | 2 060 | 0 43 | 83 91 | | 1976 | MC001 | |
| | | 3 00 | | | 4 000 | 2 003 | CT | 2 035 | 1 08 | 132 91 | | 1976 | MC001 | |
| | | 3 00 | | | 3 999 | 1 998 | CT | 2 061 | 0 73 | 109 27 | | 1976 | MC001 | |
| AUSTENITIC COND AND TRANSFORMED AT 36F, AGED 1015F | F8 | 2 20 | R T | L-T | 2 000 | 2 002 | CT | 2 008 | 0 36 | 79 44 | | 1976 | MC001 | |
| | | 2 20 | | | 3 938 | 2 004 | CT | 1 005 | 0 33 | 78 36 | 99.6/ 22.4 | 1976 | MC001 | |
| | | 2 20 | | | 2 000 | 1 004 | CT | 1 005 | 0 43 | 83 91 | | 1976 | MC001 | |
| | | 2 20 | | | 3 001 | 1 635 | CT | 1 577 | 0 76 | 114 70 | | 1973 | 89836 | |
| AUSTENITIC COND AND TRANSFORMED AT 36F, AGED 1015F | F8 | 2 20 | R T | T-L | 3 001 | 1 634 | CT | 1 587 | 0 43 | 90 80 | 103.0/ 19.4 | 1973 | 89836 | |
| | | 2 20 | | | 3 001 | 1 634 | CT | 1 587 | 0 43 | 98 30 | 89.6/ 1.8 | 1973 | 89836 | |
| | | 1 50 | R T | L-T | 2 000 | 1 000 | CT | 1 000 | 0 22 | 63 00 | | 1972 | 84365 | |
| | | 1 50 | | | 2 000 | 1 000 | CT | 1 000 | 0 16 | 59 80 | 58.4/ 6.5 | 1972 | 84365 | |
| H 950 | S | 1 00 | R T | T-L | 2 000 | 1 000 | CT | 1 000 | 0 38 | 81 60 | | 1972 | 84365 | |
| | | 1 50 | | | 2 000 | 1 000 | CT | 1 000 | 0 17 | 54 30 | | 1972 | 84365 | |
| | | 2 25 | | | 2 000 | 1 000 | CT | 1 000 | 0 41 | 85 00 | | 1972 | 84365 | |
| | | 1 50 | | | 2 000 | 1 000 | CT | 1 000 | 0 18 | 56 70 | 69.4/ 16.1 | 1972 | 84365 | |
| H 950 | F | 8 00 | R T | L-T | 2 000 | 1 000 | CT | 1 000 | 0 13 | 47 00 | | 1972 | 84365 | |
| | | 4 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 40 | 83 90 | | 1972 | 84365 | |
| | | 8 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 40 | 84 50 | | 1972 | 84365 | |
| | | 4 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 19 | 57 80 | | 1972 | 84365 | |
| H 950 | F | 4 00 | R T | T-L | 2 000 | 1 000 | CT | 1 000 | 0 39 | 83 60 | | 1972 | 84365 | |
| | | 4 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 47 | 91 30 | | 1972 | 84365 | |
| | | 4 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 28 | 70 50 | | 1972 | 84365 | |
| | | 8 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 19 | 58 20 | 70.3/ 16.0 | 1972 | 84365 | |
| H 950 | F | 4 00 | R T | L-T | 2 000 | 1 000 | CT | 1 000 | 0 18 | 55 90 | | 1972 | 84365 | |
| | | 4 00 | | | 2 000 | 1 000 | CT | 1 000 | 0 18 | 55 90 | | 1972 | 84365 | |

Table 3.8.2.1 (Continued)

| CONDITION | STAINLESS STEEL PH13-8MO | | | | K(IIC) | SPECIMEN | | CRACK LENGTH (IN) | 2.5* | | K(IIC) | | DATE | REFER | |
|-----------|--------------------------|------------|------------|----------------------|--------|-------------------|-------|-------------------|-------|--------|--------|--------|-------|-------|------------------|
| | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | | CRACK LENGTH (IN) | (IN) | | (IN) | MEAN | STAN | DEV | | | (K(IIC) SORT IN) |
| | THICK (IN) | TEMP (F) | ORIENT | YIELD STRENGTH (KSI) | M | B | A | 2.5* | (IN) | (IN) | (IN) | (IN) | | | |
| H 950 | RR | 2 25 | R T | L-T | 202.0 | 1.000 | CT | 1.077 | 0.25 | | 64.20 | | 1973 | 86688 | |
| | | 2 25 | | | 202.0 | 1.000 | CT | 1.069 | 0.30 | | 70.00 | | 1973 | 86688 | |
| | | 2 25 | | | 202.0 | 1.000 | CT | 1.040 | 0.27 | | 66.40 | 66.9/ | 2.9 | 1973 | 86688 |
| H 950 | NB | 2 25 | R T | T L | 197.0 | 1.000 | CT | 1.060 | 0.24 | | 60.90 | | 1973 | 86688 | |
| | | 2 25 | | | 197.0 | 1.000 | CT | 1.049 | 0.25 | | 62.80 | | 1973 | 86688 | |
| | 2 25 | | | 197.0 | 4.000 | 2.000 | CT | 2.071 | 0.26 | | 63.60 | | 1973 | 86688 | |
| | 2 25 | | | 197.0 | 4.000 | 2.000 | CT | 2.028 | 0.28 | | 66.20 | | 1973 | 86688 | |
| | 2 25 | | | 197.0 | 2.000 | 1.000 | CT | 1.030 | 0.26 | | 64.00 | | 1973 | 86688 | |
| | 2 25 | | | 197.0 | 4.000 | 2.000 | CT | 1.996 | 0.26 | | 63.40 | 63.5/ | 1.7 | 1973 | 86688 |
| H 950 | RB | 2 25 | R T | S L | 203.0 | 0.750 | CT | 0.780 | 0.33 | | 73.80 | | 1973 | 86688 | |
| | | 2 25 | | | 203.0 | 1.500 | 0.750 | CT | 0.738 | 0.35 | | 76.40 | | 1973 | 86688 |
| | | 2 25 | | | 203.0 | 1.500 | 0.750 | CT | 0.797 | 0.32 | | 72.20 | 74.1/ | 2.1 | 1973 |
| H1000 | S | 1 50 | R T | L-T | 205.0 | 1.000 | CT | 1.000 | 0.71 | | 109.00 | | 1972 | 84365 | |
| | | 1 50 | | | 205.0 | 2.000 | 1.000 | CT | 1.000 | 0.58 | | 98.30 | | 1972 | 84365 |
| | | 2 25 | | | 211.0 | | | NB | | 0.68 | | 110.00 | | 1972 | 84365 |
| | | 2 25 | | | 211.0 | | | NB | | 0.59 | | 103.00 | | 1972 | 84365 |
| | | 2 25 | | | 211.0 | 2.000 | 1.000 | CT | 1.000 | 0.60 | | 103.00 | | 1972 | 84365 |
| 1 75 | | | 219.0 | | | CT | | 0.63 | | 110.00 | 103.6/ | 4.8 | 1972 | 84365 | |
| H1000 | S | 1 50 | R T | T-L | 205.0 | 1.000 | CT | 1.000 | 0.61 | | 101.00 | | 1972 | 84365 | |
| | | 1 50 | | | 205.0 | 1.000 | CT | 1.000 | 0.59 | | 99.70 | | 1972 | 84365 | |
| | | 2 25 | | | 213.0 | 2.000 | 1.000 | CT | 1.000 | 0.49 | | 94.30 | | 1972 | 84365 |
| | | 2 25 | | | 214.0 | 2.000 | 1.000 | CT | 1.000 | 0.44 | | 89.60 | 96.2/ | 5.2 | 1972 |
| H1000 | P | 4 00 | R T | L-T | 201.0 | 0.990 | CT | 1.761 | 0.59 | | 98.10 | | ---- | 84306 | |
| | | 4 00 | | | 201.0 | 3.501 | 0.978 | CT | 1.768 | 0.55 | | 94.90 | | ---- | 84306 |
| H1000 | P | 4 00 | R T | T-L | 198.0 | 0.990 | CT | 1.782 | 0.51 | | 91.00 | 94.7/ | 3.6 | ---- | 84306 |
| | | 4 00 | | | 198.0 | 3.500 | 0.990 | CT | 1.796 | 0.54 | | 93.40 | | ---- | 84306 |
| H1000 | F | 4 00 | - | 65 L-T | 185.0 | 1.381 | CT | 1.941 | 0.21 | | 33.80 | | 1973 | 85836 | |
| | | 5 00 | | | 195.0 | 2.000 | 1.000 | CT | 1.030 | 0.14 | | 46.90 | 50.4/ | 4.9 | 1973 |
| H1000 | F | 8 00 | R T | L-T | 205.0 | 1.000 | CT | 1.000 | 0.43 | | 89.10 | | 1973 | 85034 | |
| | | 8 00 | | | 205.0 | 2.493 | 1.238 | CT | 1.232 | 0.65 | | 104.60 | | 1974 | 88136 |
| | | 8 00 | | | 205.0 | 1.000 | 2.000 | CT | 1.000 | 0.56 | | 97.30 | | 1973 | 85034 |
| | | 8 00 | | | 205.0 | 2.493 | 1.261 | CT | 1.188 | 0.58 | | 98.60 | | 1974 | 88136 |

Table 3.8.2.1 (Continued)

| CONDITION | STAINLESS STEEL PH13-8PH | | YIELD STRENGTH (KSI) | SPECIMEN | | CRACK LENGTH (IN) | K(IIC) STAN | K(IIC) MEAN DEV (KSI*SQRT IN) | DATE | REFER |
|-----------|--------------------------|------------|----------------------|----------|------------|-------------------|-------------|-------------------------------|--------|------------|
| | FORM | THICK (IN) | | ORIENT | THICK (IN) | | | | | |
| H1000 | F | 4 00 | R T | L-T | 1 000 | 2 000 | NB | 1 000 | 131.00 | 1972 84365 |
| | | 8 00 | | | 2 477 | 1 259 | CT | 1 226 | 99.50 | 1974 88136 |
| | | 4 00 | | | 1 000 | 2 000 | NB | 1 000 | 106.00 | 1972 84365 |
| | | 6 00 | | | 1 948 | 0 753 | CT | 0 986 | 100.00 | 1973 85034 |
| | | 6 00 | | | 1 997 | 0 751 | CT | 0 988 | 99.40 | 1973 85034 |
| | | 4 00 | | | 1 000 | 2 000 | CT | 1 000 | 99.80 | 1973 85036 |
| | | 4 00 | | | 1 000 | 2 000 | CT | 1 000 | 91.70 | 1973 85036 |
| | | 4 00 | | | 1 000 | 2 000 | CT | 1 000 | 104.00 | 1973 85036 |
| H1000 | F | 4 00 | - | 65 T-L | 3 000 | 1 630 | CT | --- | 56.00 | 1974 90011 |
| | | 2 25 | | | 3 000 | 1 630 | CT | --- | 53.00 | 1974 90011 |
| H1000 | F | 2 75 | R T | T-L | 2 002 | 0 752 | CT | 1 008 | 79.50 | 1973 85857 |
| | | 196.0 | | | 2 003 | 0 751 | CT | 0 990 | 73.00 | 1973 85857 |
| | | 2 75 | | | 2 004 | 0 750 | CT | 1 013 | 75.60 | 1973 85857 |
| | | 2 75 | | | 196.0 | 2 003 | CT | 1 002 | 78.20 | 1973 85857 |
| | | 6 00 | | | 199.0 | 2 001 | CT | 0 986 | 98.50 | 1973 85034 |
| | | 6 00 | | | 201.0 | 1 999 | CT | 0 982 | 90.70 | 1973 85034 |
| H1000 | E | 4 00 | R T | S-T | 1 000 | 2 000 | CT | 1 000 | 121.00 | 1973 85034 |
| | | 8 00 | | | 3 002 | 1 368 | CT | 1 499 | 86.40 | 1973 85836 |
| | | 4 00 | | | 3 000 | 1 000 | CT | --- | 52.00 | 1974 90011 |
| | | 1 50 | - | 65 L-T | 3 000 | 1 000 | CT | --- | 50.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 48.00 | 1974 90011 |
| | | 1 50 | R T | L-T | 3 000 | 1 000 | CT | --- | 61.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 66.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 70.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 61.00 | 1974 90011 |
| | | 1 50 | | | 3 999 | 1 413 | CT | 1 973 | 72.20 | 1973 85836 |
| H1000 | E | 1 50 | | | 3 999 | 1 417 | CT | 2 018 | 76.70 | 1973 85836 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 71.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 70.00 | 1974 90011 |
| | | 1 50 | - | 65 T-L | 3 000 | 1 000 | CT | --- | 48.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 48.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 50.00 | 1974 90011 |
| | | 1 50 | R T | T-L | 3 000 | 1 000 | CT | --- | 67.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 67.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 67.00 | 1974 90011 |
| | | 1 50 | | | 3 000 | 1 000 | CT | --- | 67.00 | 1974 90011 |

Table 3.8.2.1 (Continued)

| CONDITION | FORM | | TEST SPECIMEN ORIENT (T) | YIELD STRENGTH (KSI) | SPECIMEN | | DESIGN THICK (IN) | CRACK LENGTH (IN) | K(1C) (IN) | 2.5* K(1C)/TYS (IN) | K(1C) MEAN (KSI*SQRT IN) | STAN DEV (IN) | DATE | REFER |
|--------------------------|------------|------------|--------------------------|----------------------|------------|------------|-------------------|-------------------|------------|---------------------|--------------------------|---------------|------------|-------|
| | THICK (IN) | THICK (IN) | | | WIDTH (IN) | THICK (IN) | | | | | | | | |
| H1000 | E | 1.50 | R-T | 208.0 | 3.000 | 1.000 | CT | --- | --- | 0.22 | 62.00 | --- | 1974 90011 | |
| | | 1.50 | R-T | 208.0 | 3.000 | 1.000 | CT | --- | --- | 0.27 | 68.00 | --- | 1974 90011 | |
| | | 1.50 | R-T | 208.0 | 3.000 | 1.000 | CT | --- | --- | 0.25 | 66.00 | 66.2/ | 1974 90011 | |
| H1000 | FB | 4.00 | - 65 L-T | 210.0 | 2.006 | 0.998 | CT | 1.028 | --- | 0.14 | 48.90 | --- | 1973 89836 | |
| H1000 | FB | 1.00 | R-T | 213.0 | 2.006 | 1.000 | CT | 1.052 | --- | 0.69 | 113.50 | --- | 1978 00009 | |
| | | 1.00 | R-T | 213.0 | 2.004 | 1.000 | CT | 1.051 | --- | 0.71 | 114.80 | 114.2/ | 1978 00009 | |
| H1000 | FB | 1.00 | R-T | 216.0 | 2.003 | 1.001 | CT | 1.034 | --- | 0.83 | 124.80 | --- | 1978 00009 | |
| | | 1.00 | R-T | 216.0 | 2.004 | 1.003 | CT | 1.048 | --- | 0.76 | 119.30 | --- | 1978 00009 | |
| | | 1.00 | R-T | 216.0 | 2.003 | 1.001 | CT | 1.058 | --- | 0.82 | 124.00 | 122.7/ | 1978 00009 | |
| H1000 | RB | 1.50 | R-T | 203.0 | 3.000 | 1.000 | CT | --- | --- | 0.54 | 93.00 | 90.0/ | 1974 90011 | |
| | | 1.50 | R-T | 203.0 | 3.000 | 1.000 | CT | --- | --- | 0.43 | 85.00 | --- | 1974 90011 | |
| H1000 | RB | 1.50 | R-T | 203.0 | 3.000 | 1.000 | CT | --- | --- | 0.36 | 78.00 | --- | 1974 90011 | |
| | | 1.50 | R-T | 203.0 | 3.000 | 1.000 | CT | --- | --- | 0.31 | 72.00 | 75.0/ | 1974 90011 | |
| H1025 | S | 5.00 | R-T | 200.0 | --- | --- | NB | --- | --- | 0.44 | 84.30 | --- | 1972 84363 | |
| H1050 | RB | 2.25 | R-T | 172.0 | 2.000 | 1.000 | CT | 1.019 | --- | 0.91 | 103.90 | --- | 1973 86688 | |
| | | 2.25 | R-T | 172.0 | 2.000 | 1.000 | CT | 1.018 | --- | 0.81 | 98.20 | --- | 1973 86688 | |
| | | 2.25 | R-T | 172.0 | 2.000 | 1.000 | CT | 1.034 | --- | 0.97 | 107.30 | 103.1/ | 1973 86688 | |
| H1050 | RB | 2.25 | R-T | 178.0 | 2.000 | 1.000 | CT | 1.030 | --- | 0.61 | 88.10 | --- | 1973 86688 | |
| | | 2.25 | R-T | 178.0 | 4.000 | 2.000 | CT | 2.104 | --- | 0.82 | 102.10 | --- | 1973 86688 | |
| | | 2.25 | R-T | 178.0 | 4.000 | 2.000 | CT | 2.091 | --- | 0.81 | 101.40 | --- | 1973 86688 | |
| | | 2.25 | R-T | 178.0 | 2.000 | 1.000 | CT | 1.032 | --- | 0.59 | 86.30 | --- | 1973 86688 | |
| | | 2.25 | R-T | 178.0 | 4.000 | 2.000 | CT | 2.105 | --- | 0.82 | 102.30 | --- | 1973 86688 | |
| | | 2.25 | R-T | 178.0 | 2.000 | 1.000 | CT | 1.028 | --- | 0.62 | 88.90 | 94.9/ | 1973 86688 | |
| H1050 | RB | 2.25 | R-T | 176.0 | 1.500 | 0.750 | CT | 0.762 | --- | 0.64 | 89.20 | --- | 1973 86688 | |
| | | 2.25 | R-T | 176.0 | 1.500 | 0.750 | CT | 0.781 | --- | 0.73 | 93.20 | 92.2/ | 1973 86688 | |
| MILL 1700F-LAB 1050F 4HR | F | 5.00 | - 65 L-T | 193.0 | 2.996 | 1.500 | CT | 1.546 | --- | 0.41 | 78.80 | --- | 1973 89836 | |

Table 3.8.2.1 (Continued)

| CONDITION | STAINLESS STEEL PH13-8F0 | | | | | | | | | | K(1C) | | | | |
|-----------------------------|--------------------------|---------------|-------------------------|-------------|----------------------------|---------------|---------------|--------|-------------------------|---------------------------------|-------|--------------------------------|-------------------|--------------|-------|
| | --PRODUCT-- FORM | THICK (IN) | TEST SPECIMEN ORIENT | TEMP (F) | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | CRACK 2.9σ LENGTH (IN) | | K(1C)/TYS)**2 (KSI*SQRT IN) | K(1C) MEAN DEV | STAN DATE | REFER |
| | | | | | | M | B | A | | | | | | | |
| MILL 1700F.LAB 1500F.LAB | F | 5.00 | L-T | 65 | 195.0 | 2.008 | 1.000 | CT | 1.060 | 0.30 | 67.60 | | 1973 | 85836 | |
| MILL 1700F.LAB 1500F.LAB | F | 5.00 | L-T | 65 | 195.0 | 2.006 | 0.999 | CT | 1.052 | 0.34 | 72.50 | | 1973 | 85836 | |
| RH 950 | RB | 1.50 | R.T. | L-R | 210.0 | 1.000 | 0.500 | CT | ---- | 0.18 | 57.00 | | 1974 | 90011 | |
| | | 1.50 | | | 210.0 | 1.000 | 0.500 | CT | ---- | 0.22 | 62.00 | | 1974 | 90011 | |
| | | 1.50 | | | 210.0 | 1.000 | 0.500 | CT | ---- | 0.21 | 61.00 | | 1974 | 90011 | |
| | | 1.50 | | | 210.0 | 1.000 | 0.500 | CT | ---- | 0.20 | 59.00 | 57.8/ | 2.2 | 1974 | 90011 |
| RH 975 | RB | 1.50 | R.T. | L-R | 207.0 | 1.000 | 0.500 | CT | ---- | 0.25 | 66.00 | | 1974 | 90011 | |
| | | 1.50 | | | 207.0 | 1.000 | 0.500 | CT | ---- | 0.34 | 76.00 | | 1974 | 90011 | |
| | | 1.50 | | | 207.0 | 1.000 | 0.500 | CT | ---- | 0.30 | 68.00 | 70.0/ | 5.3 | 1974 | 90011 |
| RH1000 | RB | 1.50 | R.T. | L-R | 205.0 | 1.000 | 0.500 | CT | ---- | 0.34 | 95.00 | | 1974 | 90011 | |

TABLE 3.8.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.1 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION:
ENVIRONMENT: R. T., L. H. A.

| DELTA K (KSI*IN**1/2) | DA/DN (10**6 IN./CYCLE) | | | |
|--------------------------|-------------------------|---------|---|---|
| | A | B | C | D |
| | R=+0.08 | R=+0.30 | | |
| DELTA K MIN | | | | |
| A: 13.43 | .370 | | | |
| B: 10.60 | | .114 | | |
| C: | | | | |
| D: | | | | |
| 13.00 | | .463 | | |
| 16.00 | .936 | 1.32 | | |
| 20.00 | 2.22 | 2.98 | | |
| 25.00 | 4.12 | 5.56 | | |
| 30.00 | 6.17 | 8.77 | | |
| 35.00 | 8.51 | 13.1 | | |
| 40.00 | 11.4 | 19.6 | | |
| 50.00 | 20.8 | | | |
| 60.00 | 40.2 | | | |
| DELTA K MAX | | | | |
| A: 61.76 | 45.5 | | | |
| B: 48.07 | | 38.4 | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE PERCENT ERROR 8.38 7.23

LIFE PREDICTION RATIO SUMMARY (NP/NA) 0.0-0.5 0.5-0.8 0.8-1.25 1 1.25-2.0 1 >2.0

CONDITION/HT:
 FORM: EXTRUDED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.0 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 201.0 KSI
 ULT. STRENGTH: 212.0 KSI
 SPECIMEN THK: 0.280"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 99579

STAIN.
STEEL

PH13-8MO

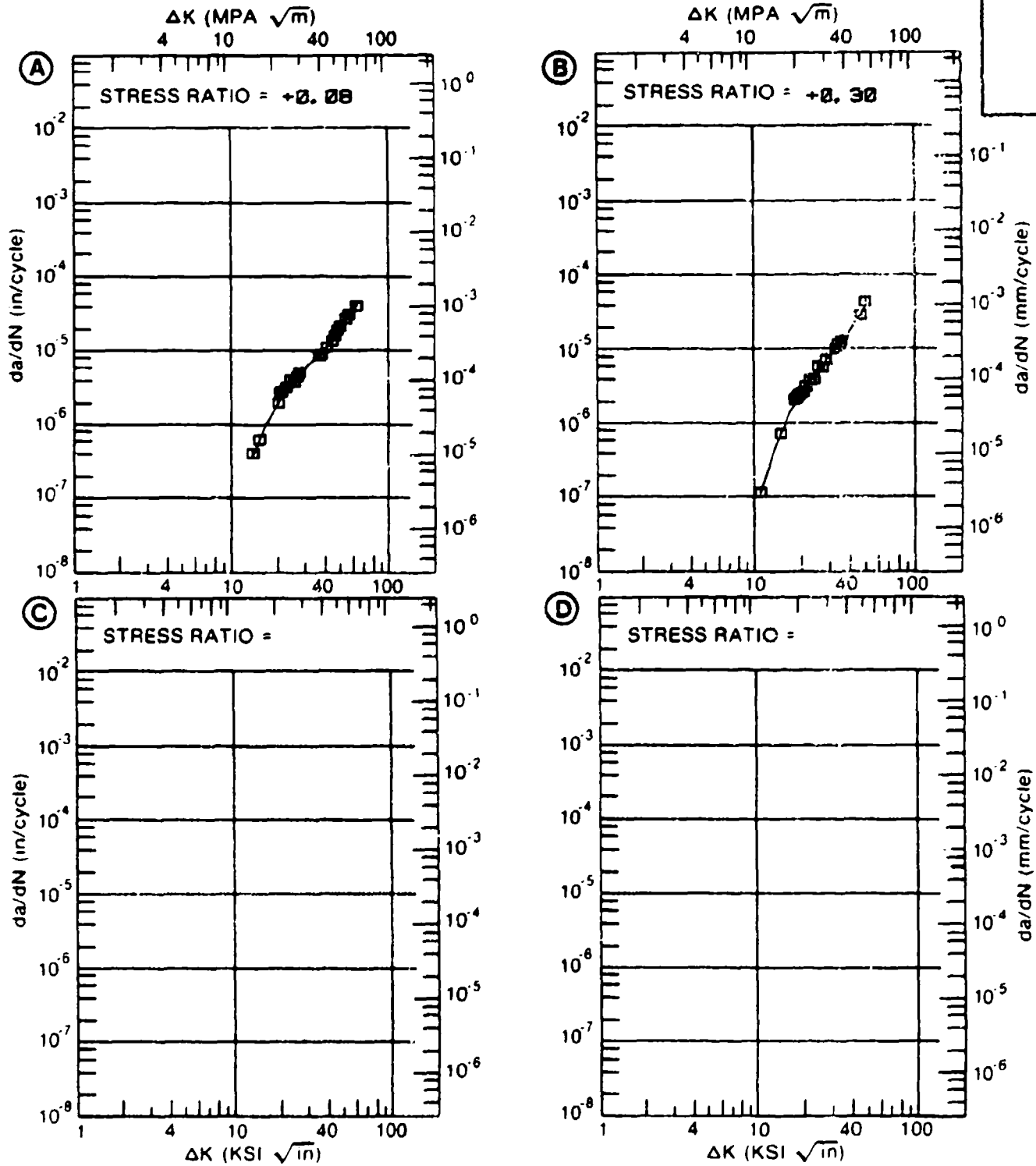


Figure 3.8.3.1

TABLE 3.8.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.2 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION:

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|---------------------------------------|--|------------------------------|------------------------------|------------------------------|---|
| | | A | B | C | D |
| | | E= R. T. L. H. A. -6. OHZ | E=- 65 F L. H. A. -6. OHZ | E= R. T. S. T. W. -1. OHZ | |
| DELTA K MIN | A: 13.43 | .370 | | | |
| | B: 13.84 | | .259 | | |
| | C: 12.50 | | | .148 | |
| | D: | | | | |
| | 13.00 | | | .211 | |
| | 16.00 | .936 | .531 | .962 | |
| | 20.00 | 2.22 | 1.32 | 2.85 | |
| | 25.00 | 4.12 | 2.79 | 6.10 | |
| | 30.00 | 6.17 | 4.78 | 10.6 | |
| | 35.00 | 8.51 | 7.39 | 17.9 | |
| | 40.00 | 11.4 | 10.8 | 31.5 | |
| | 50.00 | 20.8 | 21.6 | | |
| | 60.00 | 40.2 | 41.8 | | |
| DELTA K MAX | A: 61.76 | 45.5 | | | |
| | B: 62.88 | | 50.5 | | |
| | C: 42.46 | | | 42.5 | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 8.38 | 7.09 | 6.15 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.2! 1.25-2.0 >2.0 | 1 | 1 | 1 | |

CONDITION/HT:
 FORM: EXTRUDED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 201.0 KSI
 ULT. STRENGTH: 212.0 KSI
 SPECIMEN THK: 0.250- 0.260"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 88578

STAIN.
 STEEL
 PH13-0MC

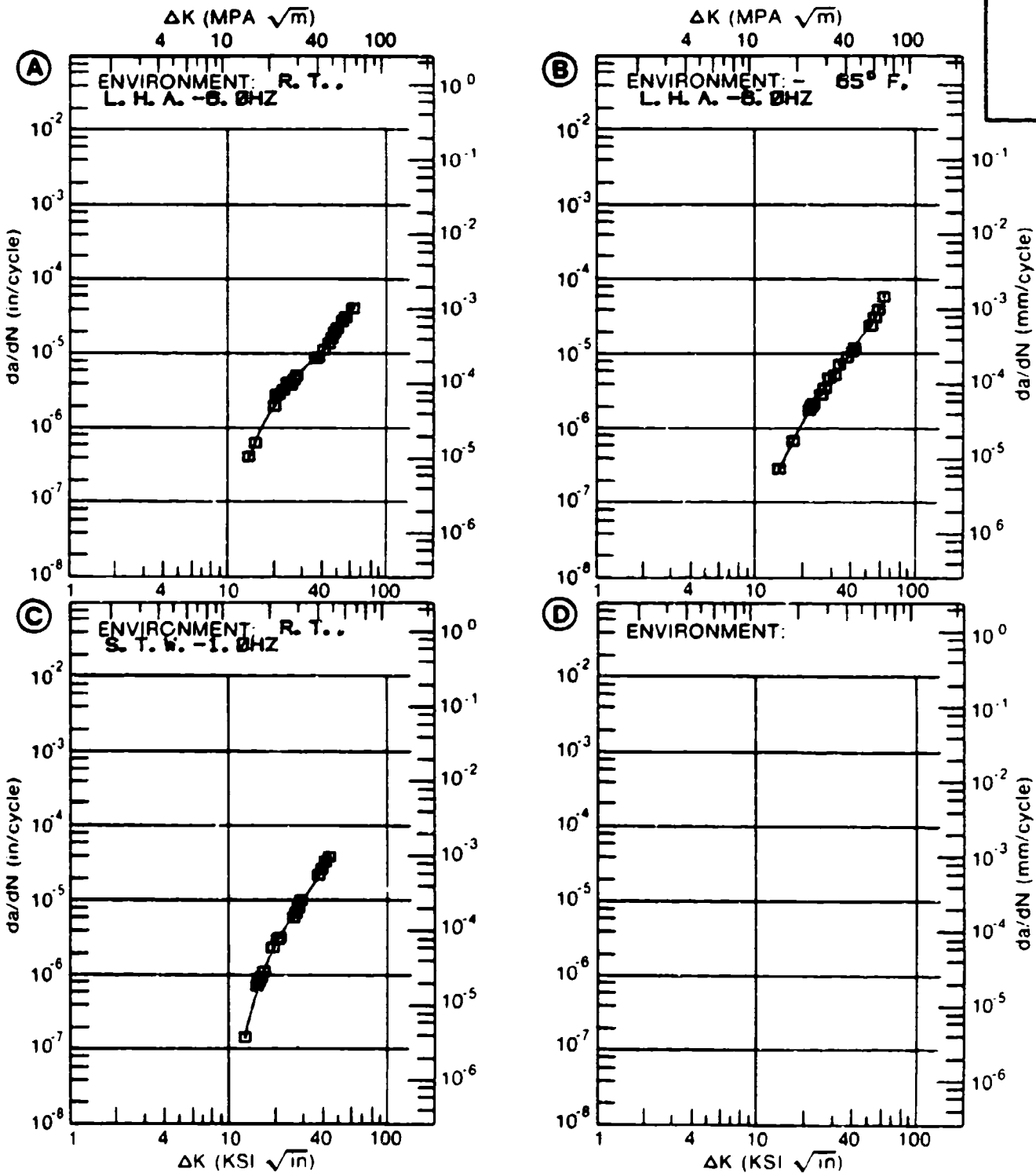


Figure 3.8.3.2

TABLE 3.8.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.3 INDICATING EFFECT
OF FREQUENCY

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | F(HZ)= 1.00 | | | |
| DELTA K MIN | A: 22.06 | 5.28 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | 6.49 | | | |
| | 30.00 | 9.06 | | | |
| | 35.00 | 12.5 | | | |
| | 40.00 | 17.1 | | | |
| | 50.00 | 31.6 | | | |
| DELTA K MAX | A: 56.54 | 46.7 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 1.97
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H1000
 FORM: 2.50" TH BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 205.0 KSI
 ULT. STRENGTH: 211.5 KSI
 SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 98136

STAIN.
 STEEL

PH13-8MO

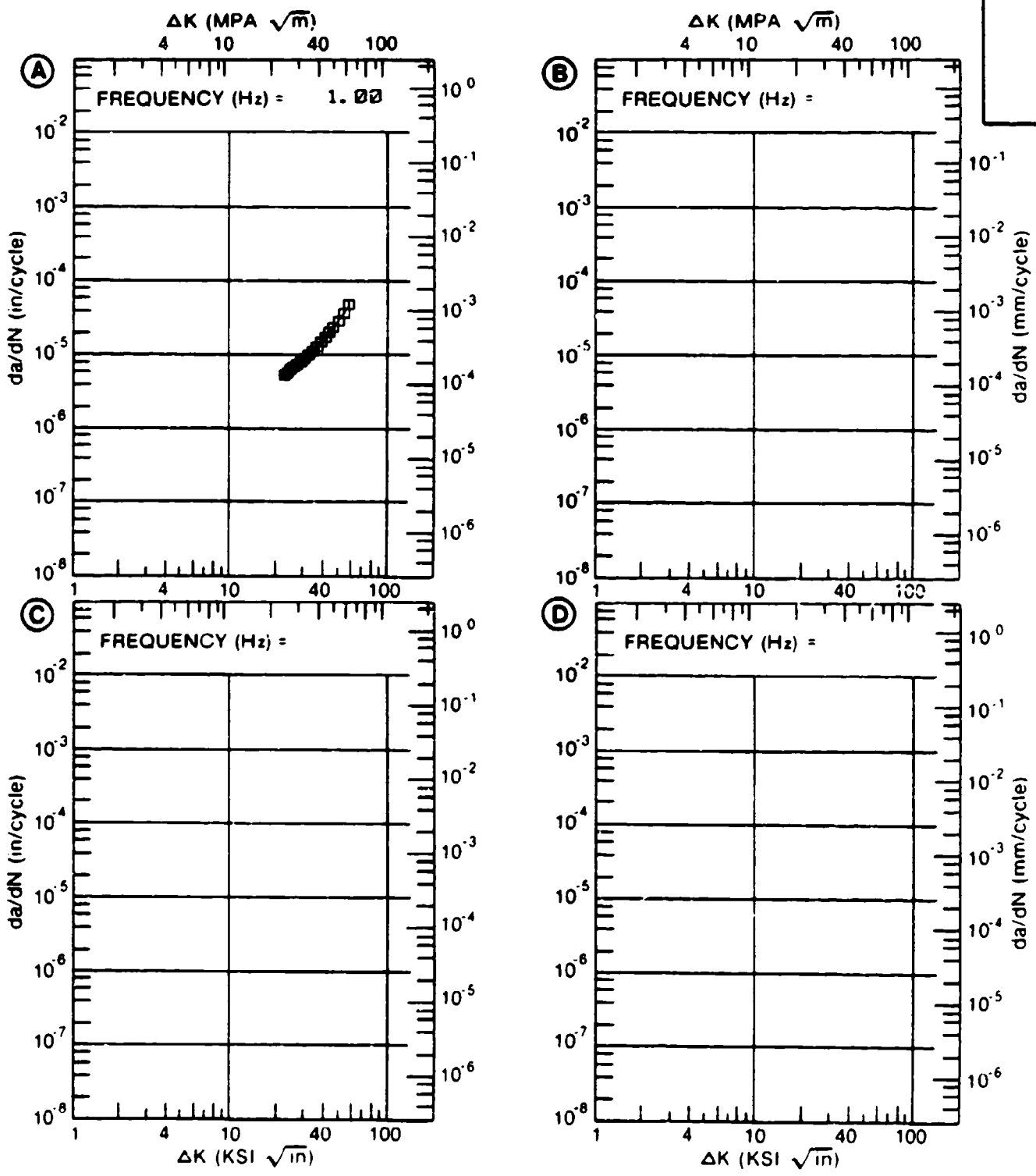


Figure 3.8.3.3

TABLE 3.8.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.4 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| DELTA K | A: 8.54 | .20 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .236 | | | |
| | 10.00 | .341 | | | |
| | 13.00 | .986 | | | |
| | 16.00 | 2.11 | | | |
| | 20.00 | 4.02 | | | |
| | 25.00 | 6.85 | | | |
| | 30.00 | 10.3 | | | |
| | 35.00 | 14.6 | | | |
| DELTA K | A: 35.80 | 15.4 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 17.07
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H1000
 FORM: 6.00" TH BILLET
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 191.0 KSI
 ULT. STRENGTH: 208.0 KSI
 SPECIMEN THK: 0.997"
 SPECIMEN WIDTH: 6.191"
 REFERENCES: 85837

STAIN.
 STEEL

PH13-8MO

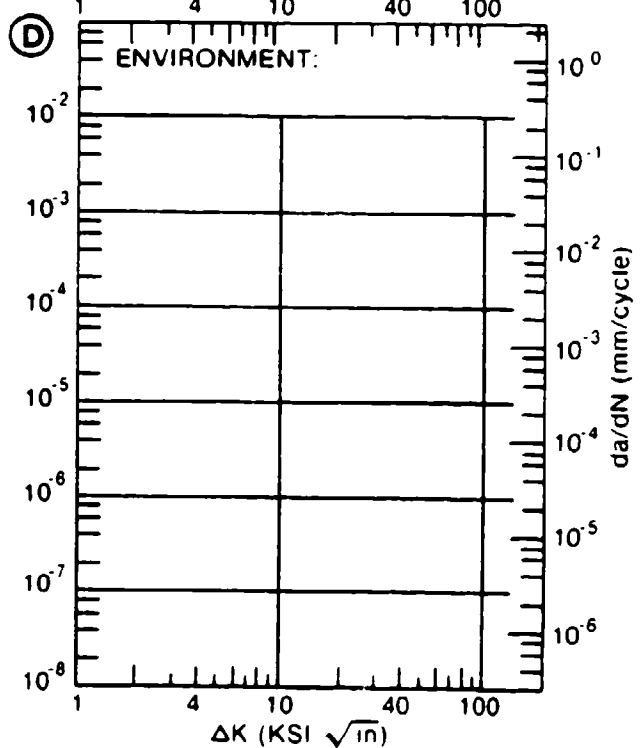
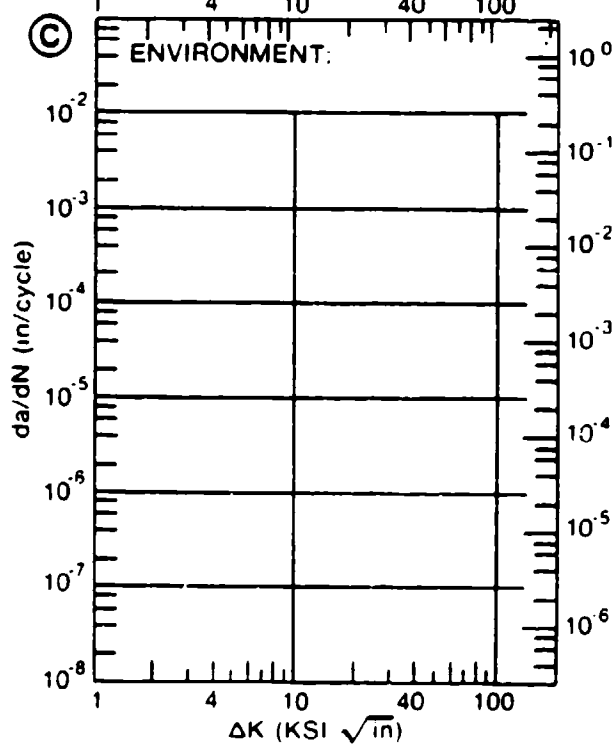
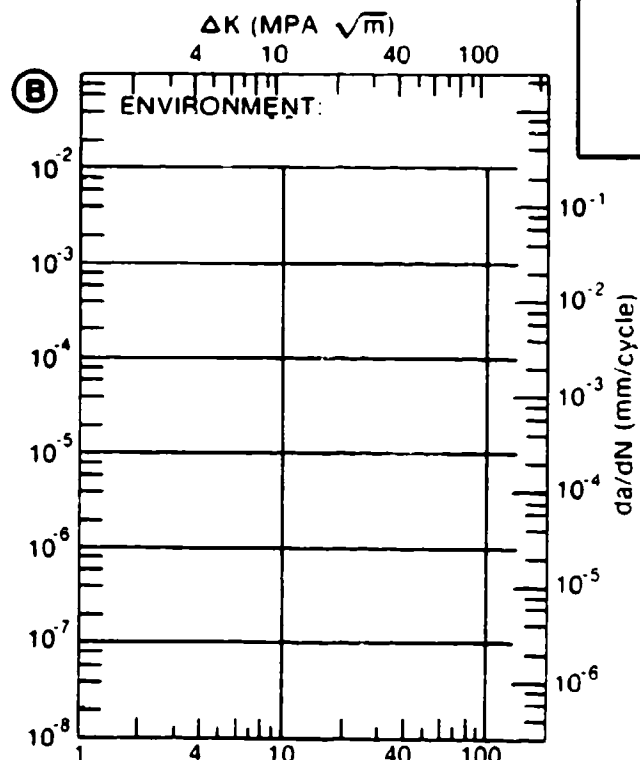
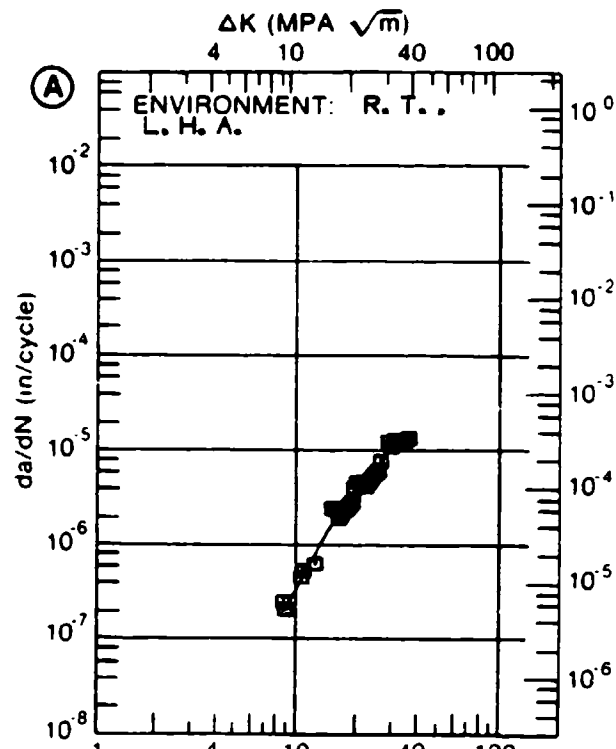


Figure 3.8.3.4

TABLE 3.8.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.5 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E = - 65F | | | |
| | | L. H. A. | | | |
| DELTA K MIN | A: 8.14 | .129 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .172 | | | |
| | 10.00 | .238 | | | |
| | 13.00 | .552 | | | |
| | 16.00 | 1.05 | | | |
| 20.00 | 2.02 | | | | |
| 25.00 | 3.92 | | | | |
| 30.00 | 7.14 | | | | |
| 35.00 | 12.7 | | | | |
| DELTA K MAX | A: 35.96 | 14.2 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 6.53
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: H1000
 FORM: 6.00" TH BILLET
 SPECIMEN TYPE: CT
 ORIENTATION: S-T
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 190.0 KSI
 ULT. STRENGTH: 207.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 4.940"
 REFERENCES: 88579

STAIN.
 STEEL

PH13-8MO

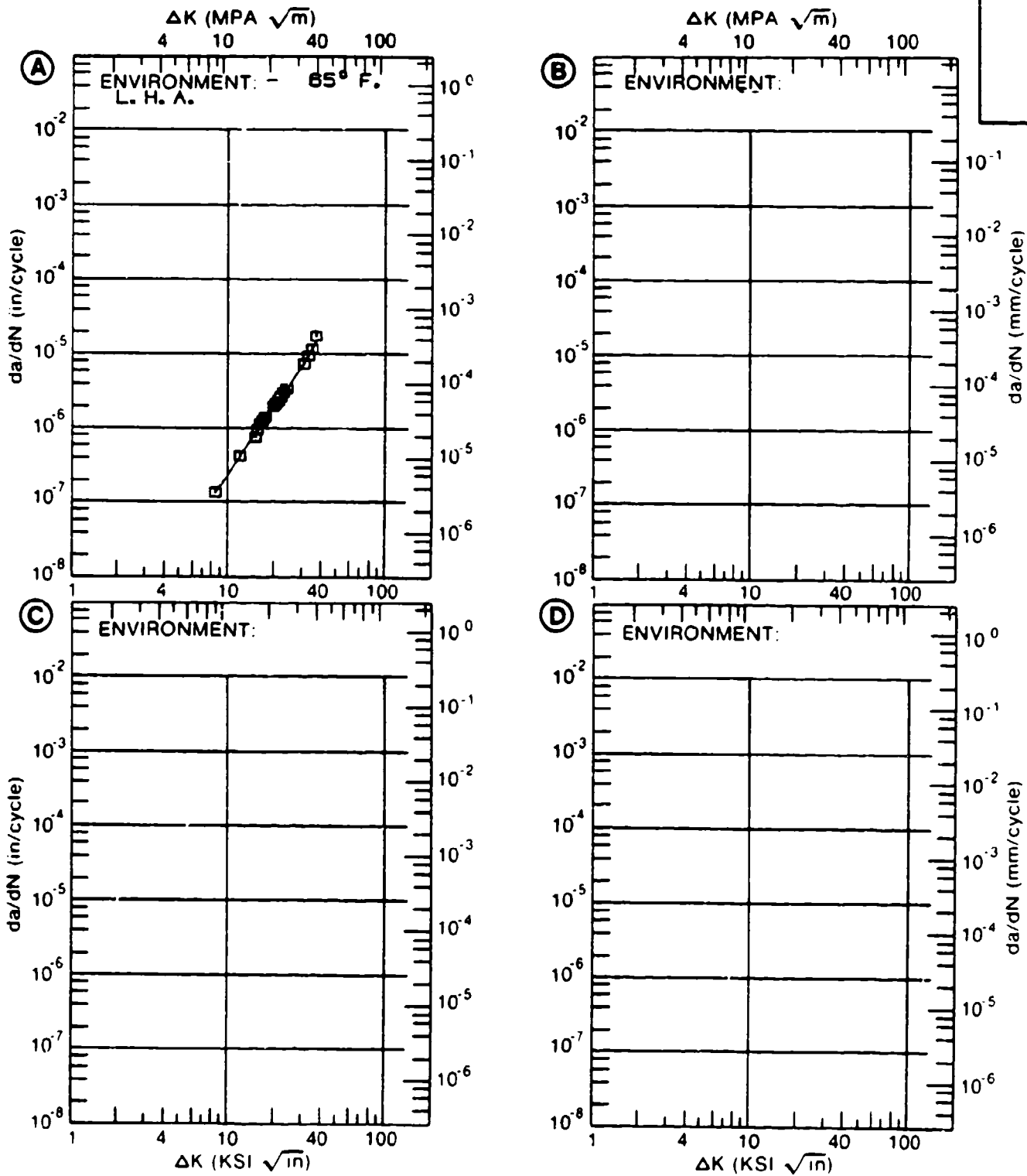


Figure 3.8.3.5

TABLE 3.8.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.6 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| DELTA K MIN | A: 8.63 | .241 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .256 | | | |
| | 10.00 | .340 | | | |
| | 13.00 | 1.01 | | | |
| | 16.00 | 2.00 | | | |
| | 20.00 | 3.47 | | | |
| | 25.00 | 5.60 | | | |
| 30.00 | 8.38 | | | | |
| 35.00 | 11.9 | | | | |
| 40.00 | 16.1 | | | | |
| 50.00 | 31.3 | | | | |
| DELTA K MAX | A: 55.15 | 54.3 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 5.25 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.3 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 22.00" TH BILLET
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 190.0 KSI
 ULT. STRENGTH: 207.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 4.940"
 REFERENCES: 88579

STAIN.
 STEEL
 PH13-8MO

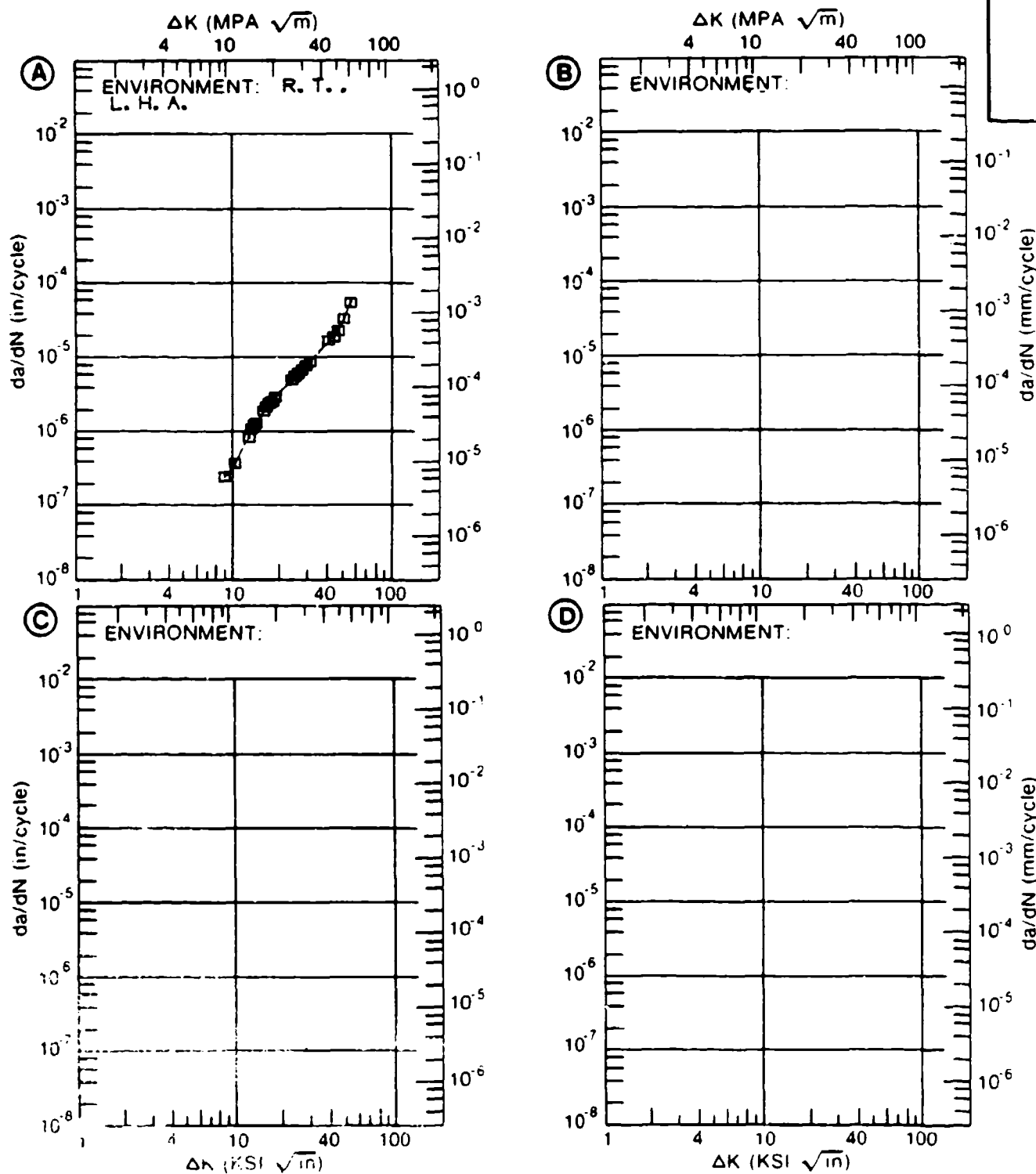


Figure 3.8.3.6

TABLE 3.8.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.7 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T., L. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.08 | R=+0.50 | | |
| DELTA K | A: 7.96 | .154 | | | |
| MIN | B: 7.25 | | .252 | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | .156 | .383 | | |
| | 9.00 | .219 | .598 | | |
| | 10.00 | .335 | .852 | | |
| | 13.00 | 1.12 | 1.82 | | |
| | 16.00 | 2.31 | 3.10 | | |
| | 20.00 | 3.83 | 5.59 | | |
| | 25.00 | 5.93 | 11.0 | | |
| | 30.00 | 9.36 | 21.3 | | |
| | 35.00 | 15.7 | | | |
| | 40.00 | 24.2 | | | |
| | 50.00 | 34.1 | | | |
| DELTA K | A: 59.52 | 48.3 | | | |
| MAX | B: 33.12 | | 32.5 | | |
| | C: | | | | |
| | D: | | | | |

APPROXIMATE FAILURE
EFFICIENT CRACK

| | | |
|--|-------|-------|
| | 15.95 | 11.43 |
|--|-------|-------|

| | | | |
|------------|--------|---|---|
| TYPE | 0.000 | | |
| PREDICTION | 0.000 | | |
| RATIO | 1-1.25 | 2 | 2 |
| SUMMARY | 5-2.0 | 1 | |
| NP/NA | 2.0 | | |

CONDITION/HT: H1000
 FORM: 1.50" TH EXTRUDED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.0 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 214.0 KSI
 ULT. STRENGTH: 221.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 6.170- 6.180"
 REFERENCES: 88579

STAIN.
STEEL

PH13-8MO

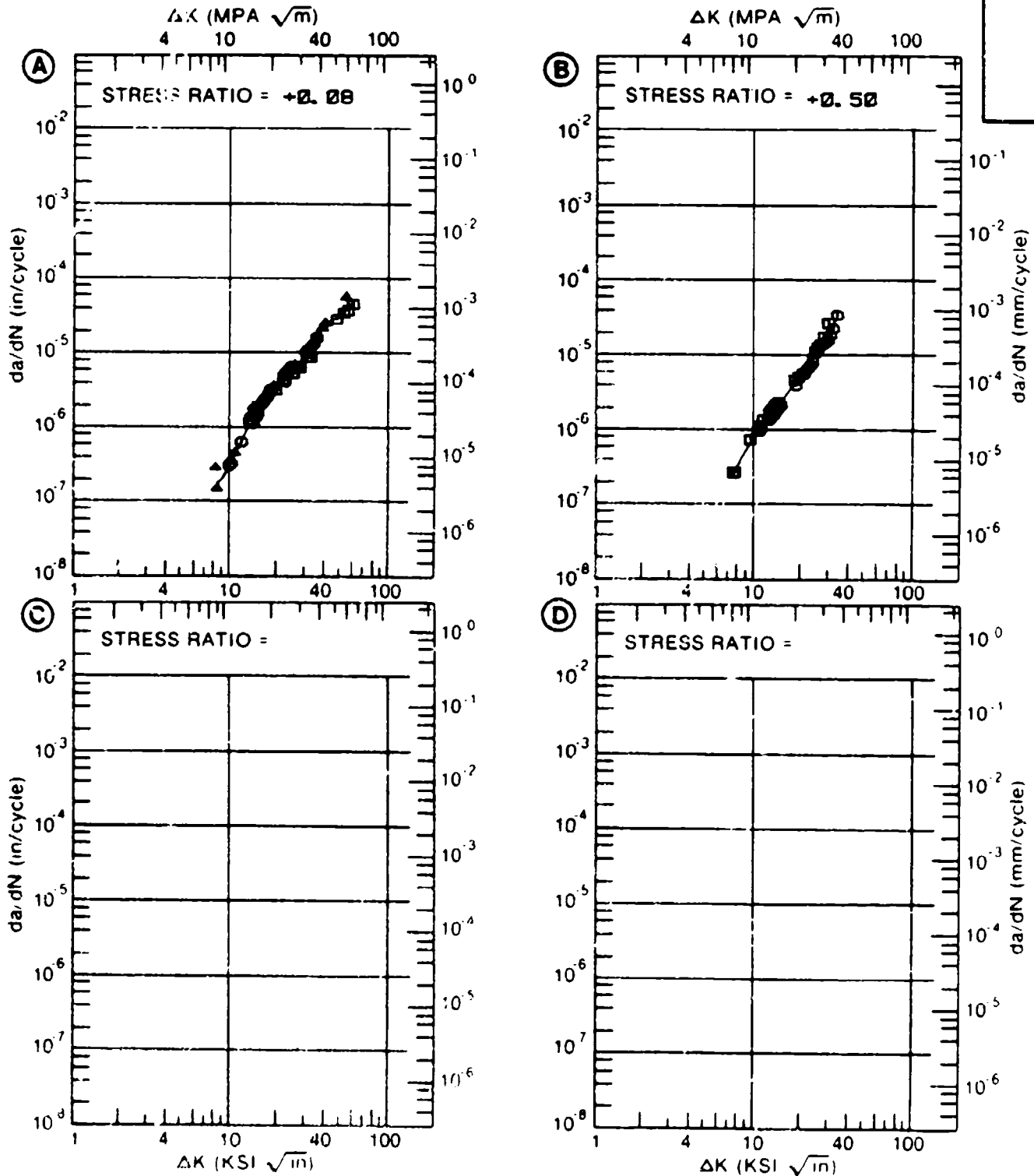


Figure 3.8.3.7

TABLE 3.8.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.8 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|---------------------------------------|----------|------------------------------|------------------------------|------------------------------|---|
| | | A | B | C | D |
| | | E= R. T. L. H. A. -6. OHZ | E=- 65 F L. H. A. -6. OHZ | E= R. T. S. T. W. -1. OHZ | |
| MIN | A: 7.96 | .156 | | | |
| | B: 7.62 | | .112 | | |
| | C: 8.27 | | | .388 | |
| | D: | | | | |
| | 8.00 | .157 | .123 | | |
| | 9.00 | .216 | .167 | .479 | |
| | 10.00 | .331 | .236 | .643 | |
| | 13.00 | 1.14 | .635 | 1.49 | |
| | 16.00 | 2.33 | 1.31 | 3.13 | |
| | 20.00 | 3.73 | 2.87 | 7.11 | |
| | 25.00 | 5.82 | 4.64 | 15.8 | |
| | 30.00 | 9.82 | | 29.0 | |
| | 35.00 | 16.2 | | | |
| | 40.00 | 23.2 | | | |
| | 50.00 | 34.4 | | | |
| MAX | A: 59.52 | 46.5 | | | |
| | B: 29.92 | | 12.3 | | |
| | C: 34.43 | | | 43.7 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.24 | 16.25 | 8.27 | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | 2 | 1 | 1 | |
| | 1.25-2.0 | 1 | | | |
| | 2.0 | | | | |

CONDITION/HT: H1000
 FORM: 1.50" TH EXTRUDED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 208.0 - 214.0 KSI
 ULT. STRENGTH: 216.0 - 221.0 KSI
 SPECIMEN THK: 0.999 - 1.000"
 SPECIMEN WIDTH: 6.170 - 6.180"
 REFERENCES: 88579, 85837

STAIN.
 STEEL

PH13-8MO

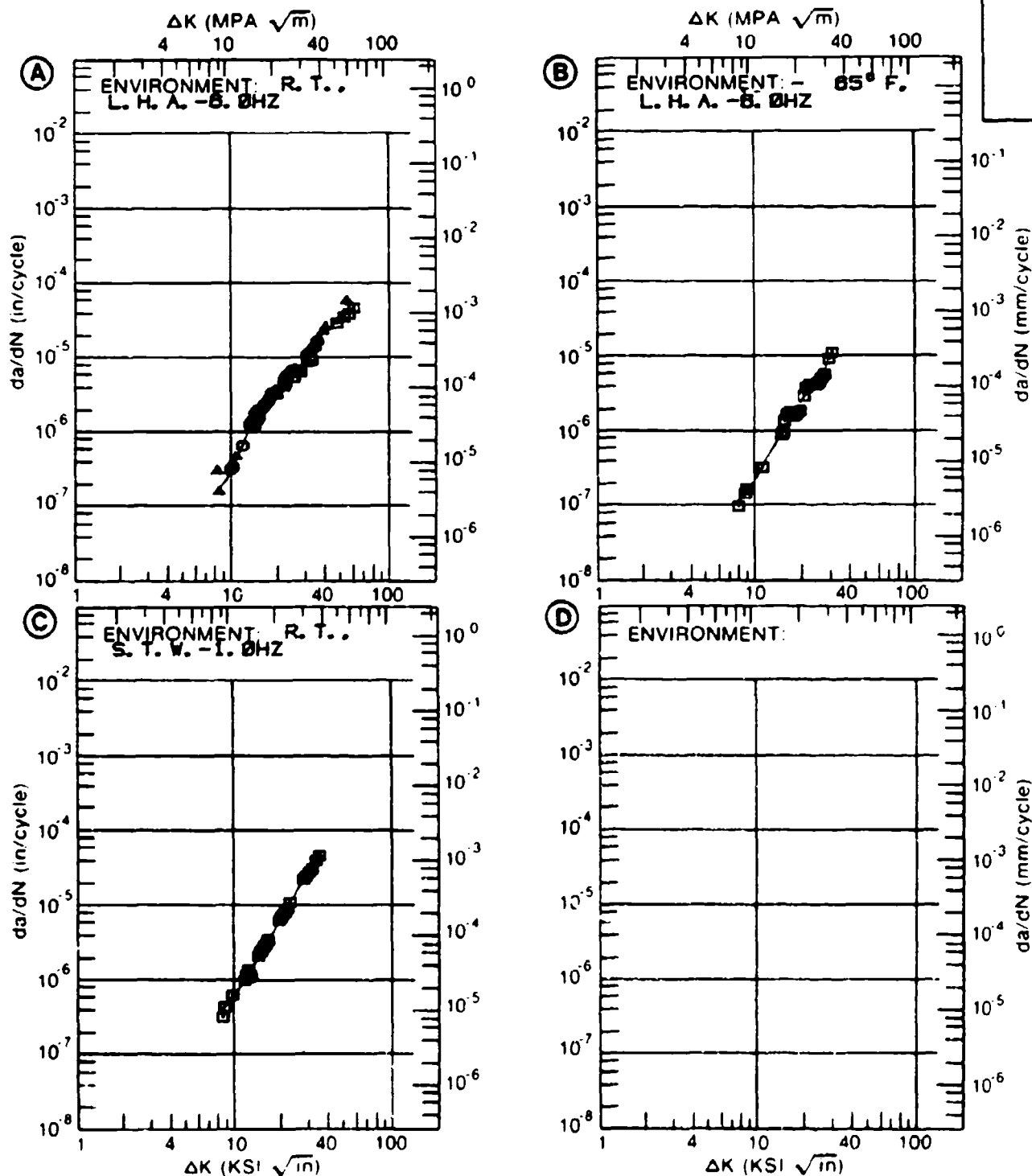


Figure 3.9.3.8

TABLE 3.8.3.9

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.9 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: STAINLESS STEEL PH13-8MO | | ----- | | | |
|------------------------------------|-----------|--------------------------------------|----------------|---|---|
| CONDITION: H1000 | | ----- | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | E= R. T. | | |
| | | LAB AIR | SIM. SEA WATER | | |
| DELTA K | A: 12.29 | 1.26 | | | |
| MIN | B: 12.13 | | 1.30 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.53 | 1.82 | | |
| | 16.00 | 2.99 | 4.36 | | |
| | 20.00 | 5.44 | 9.07 | | |
| | 25.00 | 9.04 | 16.1 | | |
| | 30.00 | 13.0 | 23.9 | | |
| | 35.00 | 17.3 | 32.3 | | |
| | 40.00 | 21.8 | 41.8 | | |
| | 50.00 | 31.9 | 65.5 | | |
| | 60.00 | 44.0 | 99.7 | | |
| | 70.00 | 58.6 | | | |
| | 80.00 | 76.7 | | | |
| | 90.00 | 99.1 | | | |
| | 100.00 | 127. | | | |
| | 130.00 | 259. | | | |
| DELTA K | A: 154.80 | 457. | | | |
| MAX | B: 69.01 | | 145. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 6.33 | 11.04 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | 2 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 3.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 1.00- 10.00 HZ

YIELD STRENGTH: 205.0 KSI
 ULT. STRENGTH: 210.6 KSI
 SPECIMEN THK: 1.003- 1.005"
 SPECIMEN WIDTH: 4.500- 7.400"
 REFERENCES: NC002

STAIN.
 STEEL

PH13-8MO

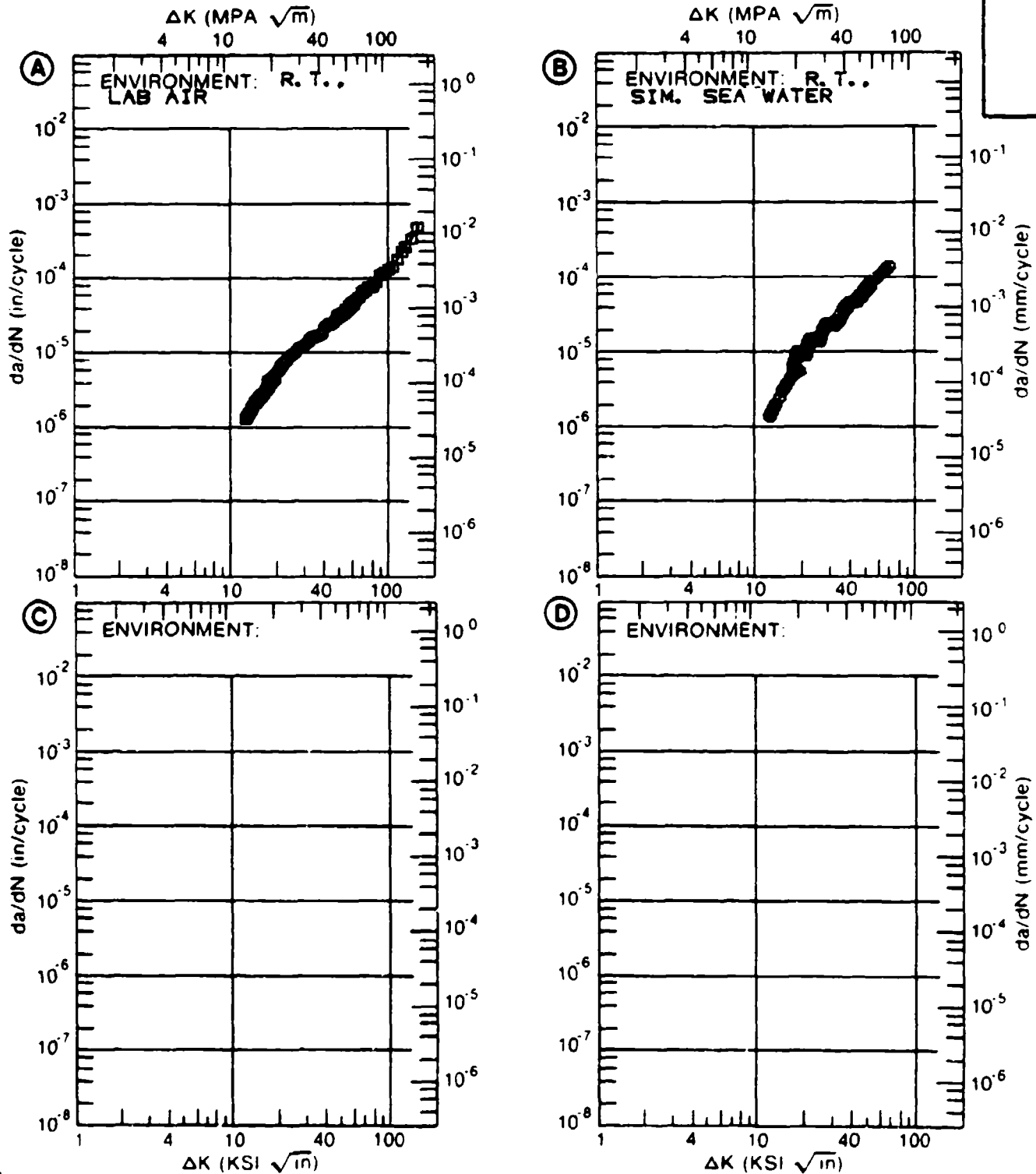


Figure 3.8.3.9

TABLE 3.8.3.10

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.10 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|-----------|--------------------------|----------------------------|---|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E= R. T. SIM. SEA WATER | | |
| DELTA K | A: 12.18 | 1.37 | | | |
| MIN | B: 12.34 | | 1.57 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.70 | 1.93 | | |
| | 16.00 | 3.16 | 4.42 | | |
| | 20.00 | 5.57 | 8.95 | | |
| | 25.00 | 9.04 | 15.5 | | |
| | 30.00 | 12.9 | 22.8 | | |
| | 35.00 | 17.0 | 31.2 | | |
| | 40.00 | 21.6 | 40.9 | | |
| | 50.00 | 32.1 | 65.4 | | |
| | 60.00 | 45.2 | 99.7 | | |
| | 70.00 | 61.7 | 148. | | |
| | 80.00 | 82.8 | 212. | | |
| | 90.00 | 110. | 296. | | |
| | 100.00 | 145. | 404. | | |
| | 130.00 | | 896. | | |
| DELTA K | A: 116.68 | 226. | | | |
| MAX | B: 137.87 | | 1074. | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 6.87 12.77
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2 2
SUMMARY 1.25-2.0
(NP/NA) 2 0

CONDITION/HT: H1000
 FORM: 3.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00- 10.00 HZ

YIELD STRENGTH: 205.4 KSI
 ULT. STRENGTH: 210.0 KSI
 SPECIMEN THK: 1.003- 1.005"
 SPECIMEN WIDTH: 4.500- 7.400"
 REFERENCES: NC002

STAIN.
STEEL

PH13-8MO

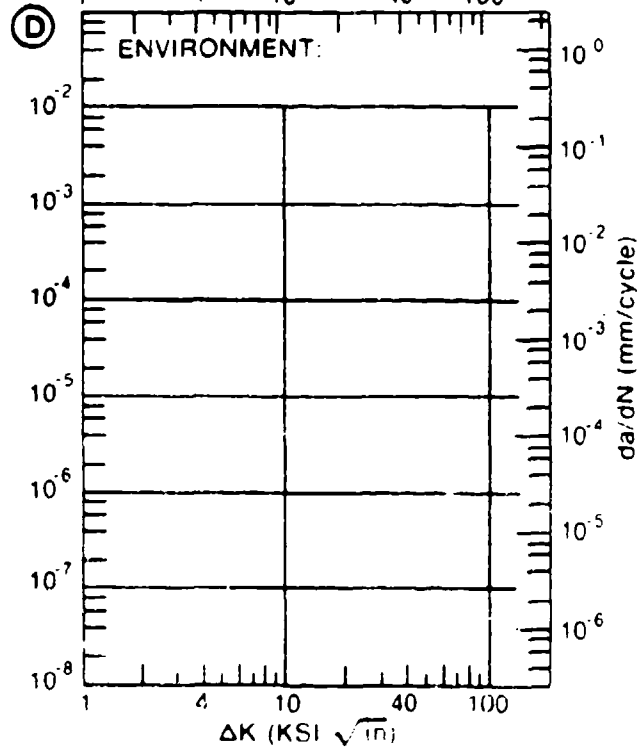
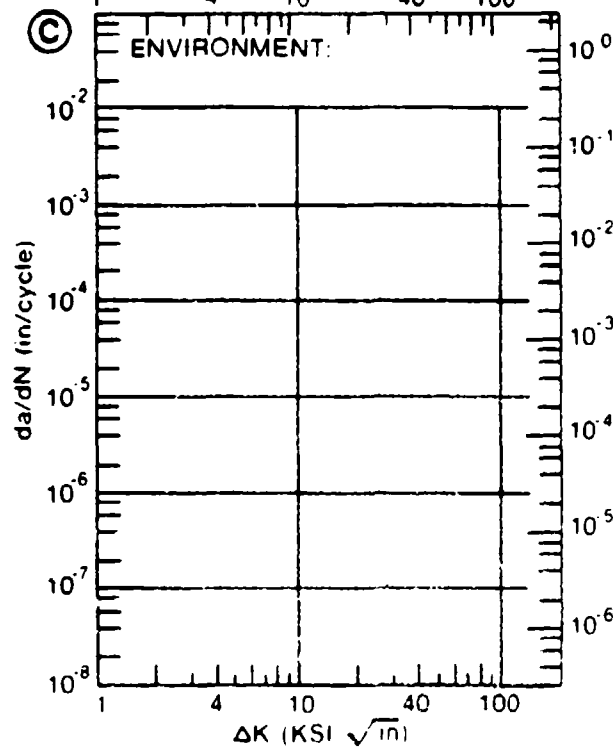
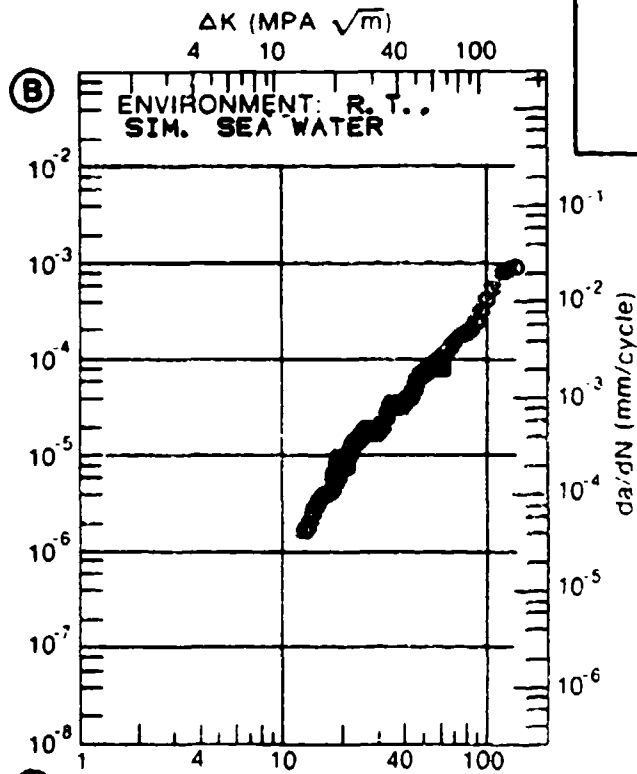
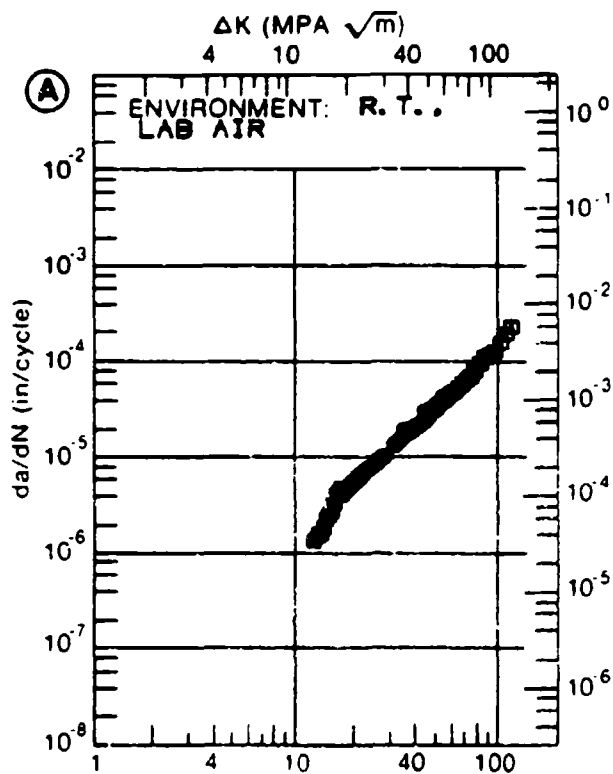


Figure 3.8.3.10

TABLE 3.8.3.11

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.11 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: F. T., DRY AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | |
| DELTA K | A: 8.91 | .137 | | | |
| MIN | B: 7.44 | | .177 | | |
| | C: 6.27 | | | .0264 | |
| | D: | | | | |
| | 7.00 | | | .120 | |
| | 8.00 | | .244 | .243 | |
| | 9.00 | .144 | .393 | .413 | |
| | 10.00 | .239 | .582 | .641 | |
| | 13.00 | .724 | 1.36 | 1.58 | |
| | 16.00 | 1.53 | 2.41 | 2.80 | |
| | 20.00 | 3.07 | 4.17 | 4.79 | |
| | 25.00 | 5.69 | 6.96 | 8.03 | |
| | 30.00 | 9.00 | 10.5 | 12.6 | |
| | 35.00 | 13.0 | 15.1 | 19.5 | |
| | 40.00 | 17.7 | 21.1 | | |
| | 50.00 | 29.6 | | | |
| | 60.00 | 45.7 | | | |
| | 70.00 | 67.2 | | | |
| | 80.00 | 95.9 | | | |
| DELTA K | A: 85.01 | 114. | | | |
| MAX | B: 40.86 | | 22.2 | | |
| | C: 37.95 | | | 25.1 | |
| | D: | | | | |

ROOT MEAN SQUARE PERCENT ERROR 5.19 5.60 6.49

LIFE PREDICTION RATIO SUMMARY (NP/NA) 0 0-0 5 0.5-0.8 0.8-1.25 1 1 1 1.25-2.0 2.0

CONDITION/HT: H1000
 FORM: 1.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 8.0 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH: 215.0 KSI
 ULT. STRENGTH: 221.0 KSI
 SPECIMEN THK: 0.500- 0.502"
 SPECIMEN WIDTH: 3.987- 3.992"
 REFERENCES: GD009

| |
|-----------------|
| STAIN. STEEL |
| PH13-8MO |
| |

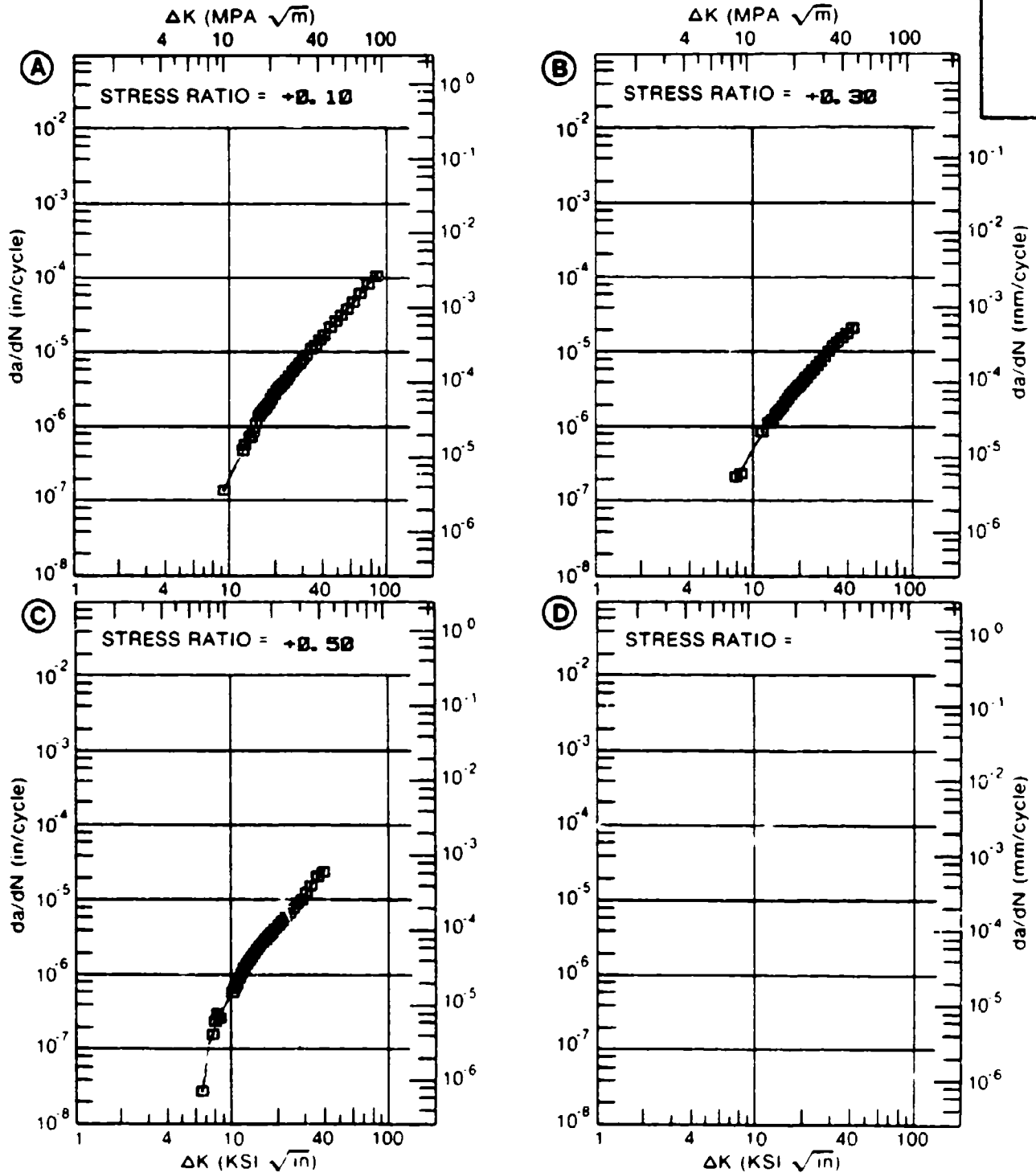


Figure 3.8.3.11

TABLE 3.8.3.12

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.12 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T., H. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | |
| DELTA K | A: 9.78 | .219 | | | |
| MIN | B: 9.28 | | .576 | | |
| | C: 6.78 | | | .393 | |
| | D: | | | | |
| | 7.00 | | | .299 | |
| | 8.00 | | | .375 | |
| | 9.00 | | | .592 | |
| | 10.00 | .294 | .218 | .942 | |
| | 13.00 | 1.52 | 2.50 | 2.89 | |
| | 16.00 | 3.61 | 5.41 | 6.11 | |
| | 20.00 | 7.56 | 11.3 | 12.5 | |
| | 25.00 | 16.0 | 21.9 | 24.6 | |
| | 30.00 | 28.7 | 36.0 | 43.1 | |
| | 35.00 | 45.4 | 53.6 | 71.2 | |
| | 40.00 | 64.9 | 74.8 | 114. | |
| | 50.00 | 105. | 129. | | |
| DELTA K | A: 59.32 | 133. | | | |
| MAX | B: 50.68 | | 134. | | |
| | C: 47.33 | | | 221. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.22 | 7.15 | 11.69 | |
| PERCENT ERROR | | | | | |

| | | | | |
|------------|----------|---|---|---|
| LIFE | 0.0-0.5 | | | |
| PREDICTION | 0.5-0.8 | | | |
| RATIO | 0.8-1.25 | 2 | 2 | 2 |
| SUMMARY | 1.25-2.0 | | | |
| (NP/NA) | >2.0 | | | |

CONDITION/HT: H1000
 FORM: 1.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.0 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 215.0 KSI
 ULT. STRENGTH: 221.0 KSI
 SPECIMEN THK: 0.501 - 0.504"
 SPECIMEN WIDTH: 3.986 - 4.006"
 REFERENCES: GD009

STAIN.
 STEEL
 PH13-8MO

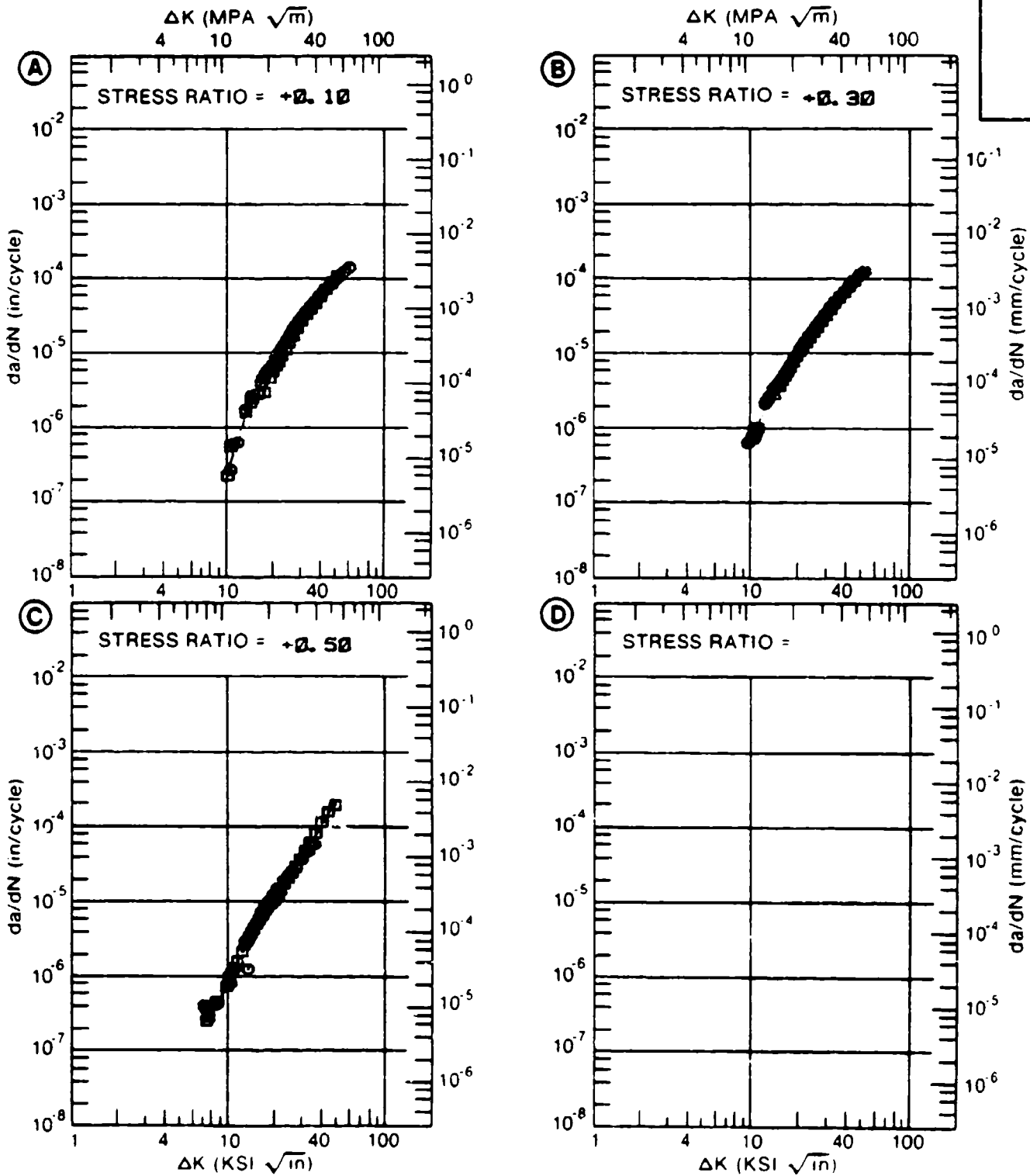


Figure 3.8.3.12

TABLE 3.8.3.13

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.13 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R.T., DRY AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**--6 IN. /CYCLE) | | | |
|--------------------------|----------|----------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | |
| DELTA K MIN | A: 9.25 | .147 | | | |
| | B: 7.78 | | .176 | | |
| | C: 6.00 | | | .121 | |
| | D: | | | | |
| | 7.00 | | | .153 | |
| | 8.00 | | .193 | .220 | |
| | 9.00 | | .289 | .335 | |
| | 10.00 | .265 | .426 | .511 | |
| | 13.00 | .737 | 1.15 | 1.40 | |
| | 16.00 | 1.59 | 2.29 | 2.62 | |
| | 20.00 | 3.14 | 4.17 | 4.60 | |
| | 25.00 | 5.52 | 6.93 | 7.62 | |
| | 30.00 | 8.27 | 10.2 | 11.5 | |
| | 35.00 | 11.4 | 14.4 | 16.8 | |
| | 40.00 | 15.0 | 19.8 | 24.1 | |
| | 50.00 | 24.3 | 37.1 | | |
| 60.00 | 37.7 | 69.9 | | | |
| 70.00 | 57.6 | 134. | | | |
| 80.00 | 87.4 | | | | |
| DELTA K MAX | A: 86.50 | 116. | | | |
| | B: 73.72 | | 171. | | |
| | C: 48.04 | | | 42.9 | |
| | D: | | | | |

ROOT MEAN SQUARE PERCENT ERROR 8.22 7.37 6.14

LIFE 0.0-0.5
PREDICTION 0.5-0.8
FATIG 0.8-1.25
SUMMARY 1.25-2.0
(NF/NA) 1.2.0

CONDITION/HT: H1000
 FORM: 1.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 6.0 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH: 216.0 KSI
 ULT. STRENGTH: 222.6 KSI
 SPECIMEN THK: 0.502- 0.503"
 SPECIMEN WIDTH: 3.991- 3.993"
 REFERENCES: GD009

STAIN.
 STEEL

PH13-8MO

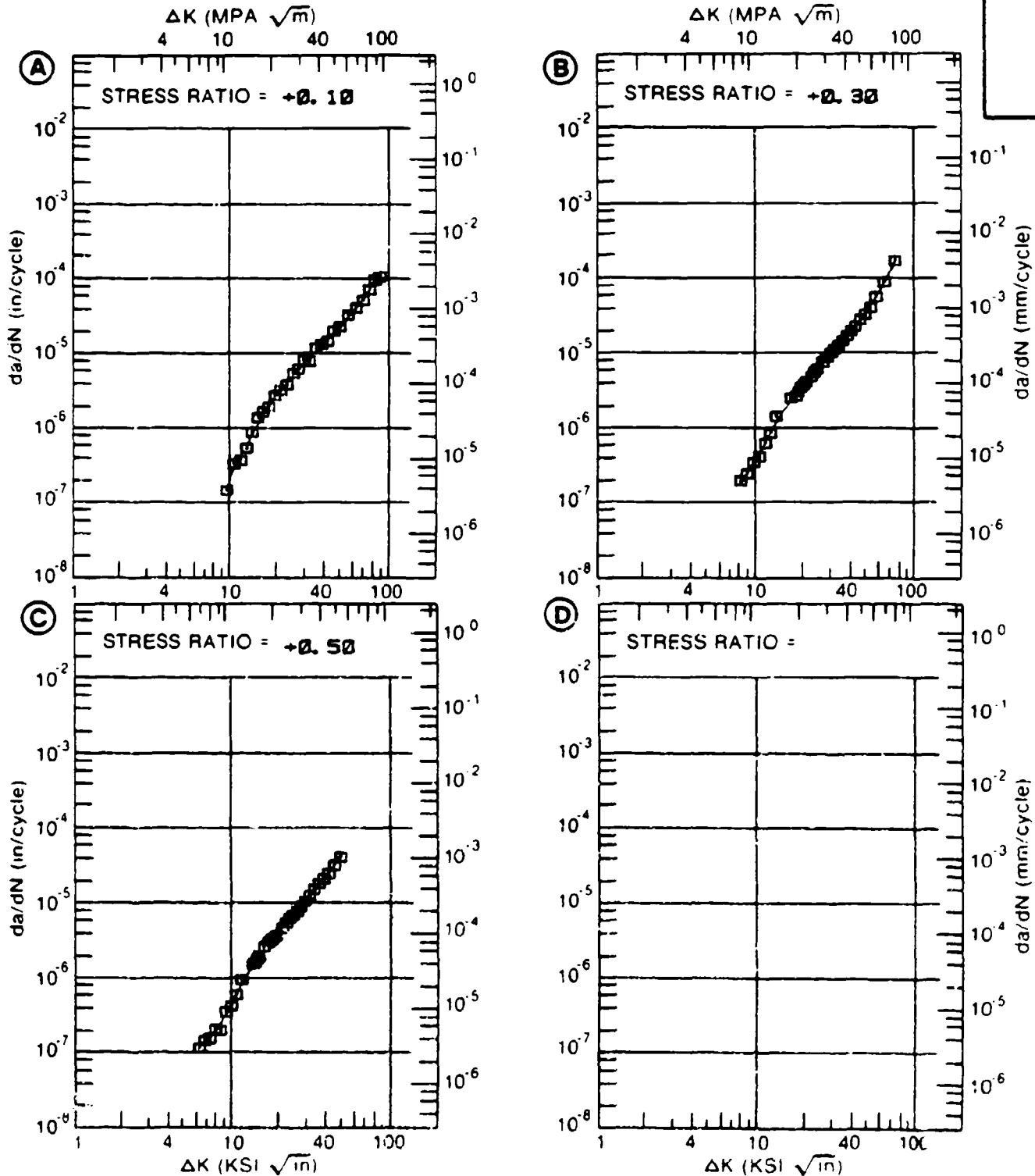


Figure 3.8.3.13

TABLE 3.8.3.14

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.14 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T., H. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | |
| DELTA K | A: 11.42 | .928 | | | |
| MIN | B: 9.13 | | .466 | | |
| | C: 6.87 | | | .299 | |
| | D: | | | | |
| | 7.00 | | | .342 | |
| | 8.00 | | | .468 | |
| | 9.00 | | | .625 | |
| | 10.00 | | .543 | 1.08 | |
| | 13.00 | 1.09 | 2.16 | 3.06 | |
| | 16.00 | 2.57 | 4.48 | 5.84 | |
| | 20.00 | 6.71 | 9.37 | 11.6 | |
| | 25.00 | 15.3 | 19.2 | 24.3 | |
| | 30.00 | 26.6 | 34.6 | 47.9 | |
| | 35.00 | 38.7 | 58.0 | 91.9 | |
| | 40.00 | 52.4 | 92.8 | 174. | |
| | 50.00 | 108. | 215. | 607. | |
| | 60.00 | 259. | | | |
| DELTA K | A: 62.14 | 303. | | | |
| MAX | B: 56.12 | | 339. | | |
| | C: 50.46 | | | 613. | |
| | D: | | | | |

ROOT MEAN SQUARE 33.16 14.35 12.25
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2 1 2
SUMMARY 1.25-2.0 1
(NP/NA) 2.0

CONDITION/HT: H1000
 FORM: 1.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.0 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 216.0 KSI
 ULT STRENGTH: 222.0 KSI
 SPECIMEN THK: 0.489 - 0.504"
 SPECIMEN WIDTH: 3.982 - 4.117"
 REFERENCES: GD009

STAIN.
 STEEL

PH13-8MO

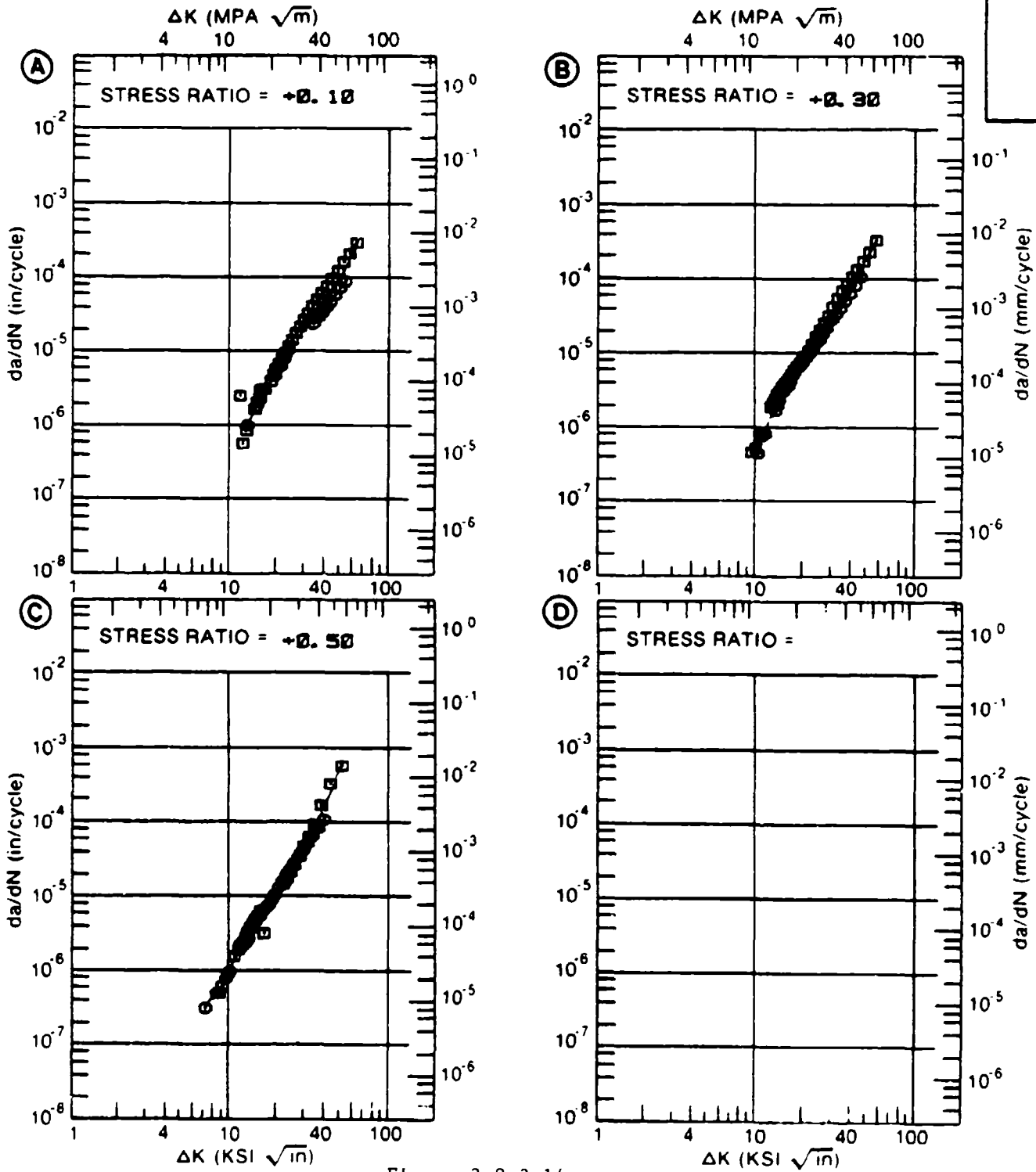


Figure 3.8.3.14

TABLE 3.8.3.15

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTORDATA ASSOCIATED WITH FIGURE 3.8.3.15 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
 CONDITION: H1000
 ENVIRONMENT: R. T., L. H. A.

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---------|---------|---|
| | A | B | C | D |
| | R=+0.08 | R=+0.30 | R=+0.50 | |
| A: 10.78 | .447 | | | |
| DELTA K B: 10.25 | | .571 | | |
| MIN C: 6.81 | | | .119 | |
| D: | | | | |
| 7.00 | | | .132 | |
| 8.00 | | | .220 | |
| 9.00 | | | .345 | |
| 10.00 | | | .515 | |
| 13.00 | 1.52 | 1.29 | 1.33 | |
| 16.00 | 3.49 | 2.52 | 2.60 | |
| 20.00 | 5.82 | 4.70 | 4.70 | |
| 25.00 | 8.52 | 8.11 | 7.10 | |
| 30.00 | 12.7 | 13.4 | | |
| A: 34.32 | 19.9 | | | |
| DELTA K B: 34.71 | | 18.7 | | |
| MAX C: 29.25 | | | 8.31 | |
| D: | | | | |
| ROOT MEAN SQUARE | 10.57 | 17.34 | 9.04 | |
| PERCENT ERROR | | | | |

| | | | | |
|------------|----------|---|---|---|
| LIFE | 0.0-0.5 | | | |
| PREDICTION | 0.5-0.8 | | | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 |
| SUMMARY | 1.25-2.0 | | | |
| (NP/NA) | >2.0 | | | |

CONDITION/HT: H1000
 FORM: 4.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.0 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 201.0 KSI
 ULT. STRENGTH: 212.0 KSI
 SPECIMEN THK: 0.990- 0.998"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 85837, 88578

STAIN.
STEEL

PH13-8MO

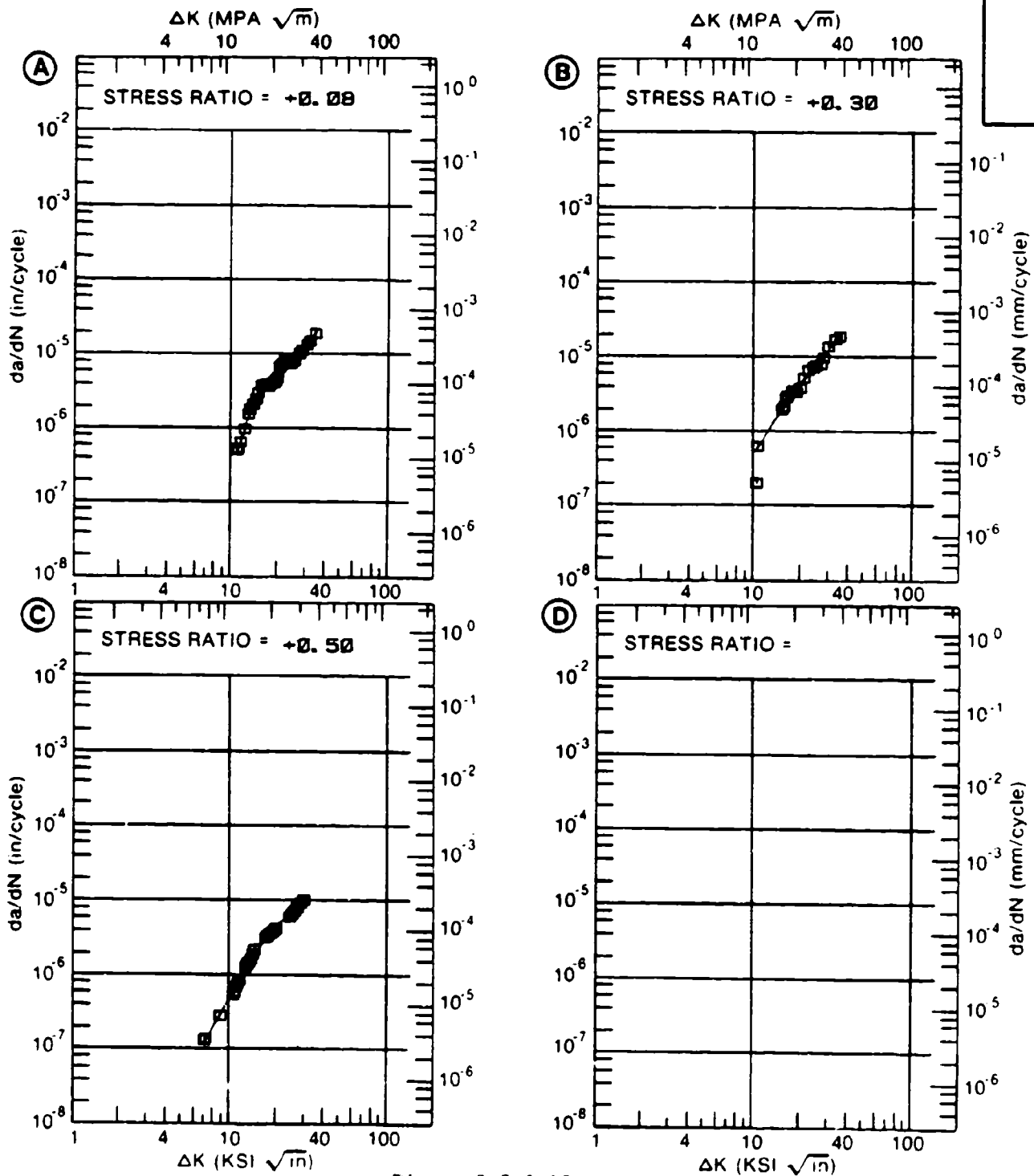


Figure 3.8.3.15

TABLE 3.8.3.16

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.16 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-BMO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. I. S. T. W. | | | |
| DELTA K MIN | A: 10.68 | 1.11 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 13.00 | 2.92 | | |
| | 16.00 | 7.61 | | | |
| | 20.00 | 18.5 | | | |
| | 25.00 | 36.1 | | | |
| | 30.00 | 50.1 | | | |
| DELTA K MAX | A: 33.64 | 54.6 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 8.98
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H1000
 FORM: 4.00" TH FORGED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.0 HZ

YIELD STRENGTH: 198.0 KSI
 ULT. STRENGTH: 206.0 KSI
 SPECIMEN THK: 0.991"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 05837

STAIN.
 STEEL
 PH13-8MO

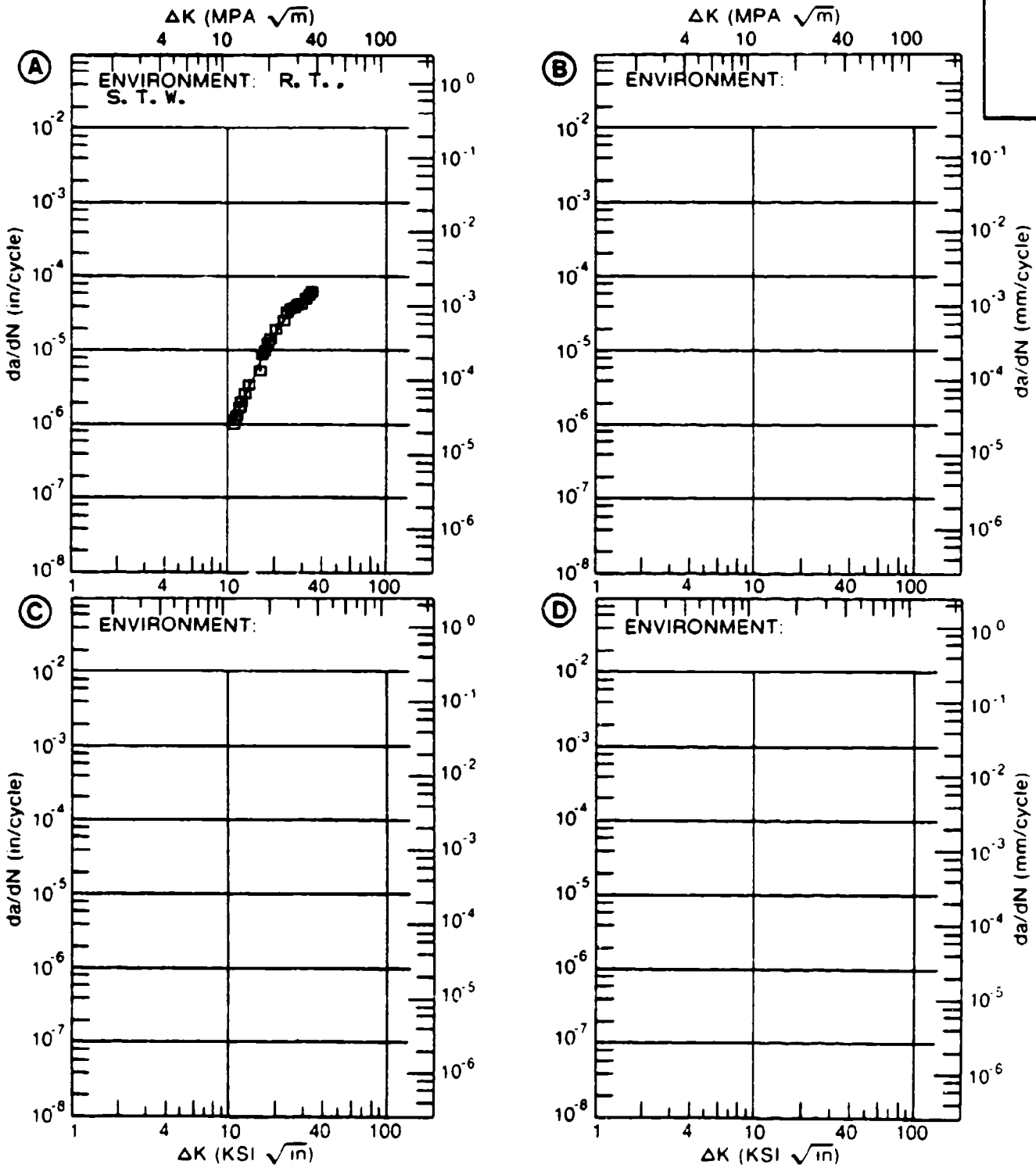


Figure 3.8.3.16

TABLE 3.8.3.17

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.17 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-BMO
CONDITION: H1000
ENVIRONMENT: R.T., L.H.A.

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------------|--------------------------------------|---------|---------|---|
| | A | B | C | D |
| | R=+0.08 | R=+0.30 | R=+0.50 | |
| DELTA K MIN | | | | |
| A: 8.33 | .155 | | | |
| B: 9.50 | | .514 | | |
| C: 9.52 | | | .593 | |
| D: | | | | |
| 9.00 | .194 | | | |
| 10.00 | .290 | .624 | .792 | |
| 13.00 | .931 | 1.49 | 2.02 | |
| 16.00 | 1.92 | 2.61 | 3.20 | |
| 20.00 | 3.40 | 4.39 | 5.09 | |
| 25.00 | 5.43 | 7.05 | 7.90 | |
| 30.00 | 7.97 | 10.3 | 11.7 | |
| 35.00 | 12.1 | 14.4 | 19.4 | |
| 40.00 | 19.4 | 19.7 | 38.0 | |
| DELTA K MAX | | | | |
| A: 42.46 | 15.5 | | | |
| B: 42.47 | | 22.8 | | |
| C: 41.04 | | | 44.6 | |
| D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | 12.32 | 5.40 | 7.95 | |

LIFE PREDICTION RATIO SUMMARY (NP/NA)

| | | | |
|----------|---|---|---|
| 0.0-0.5 | | | |
| 0.5-0.8 | | | |
| 0.8-1.25 | 2 | 1 | 1 |
| 1.25-2.0 | | | |
| >2.0 | | | |

CONDITION/HT: H1000
 FORM: 1.50" TH ROLLED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.0 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 200.0 KSI
 ULT. STRENGTH: 216.0 KSI
 SPECIMEN THK: 0.251 - 0.990"
 SPECIMEN WIDTH: 7.390 - 7.400"
 REFERENCES: 80579, 85837

STAIN.
 STEEL
 PH13-8MO

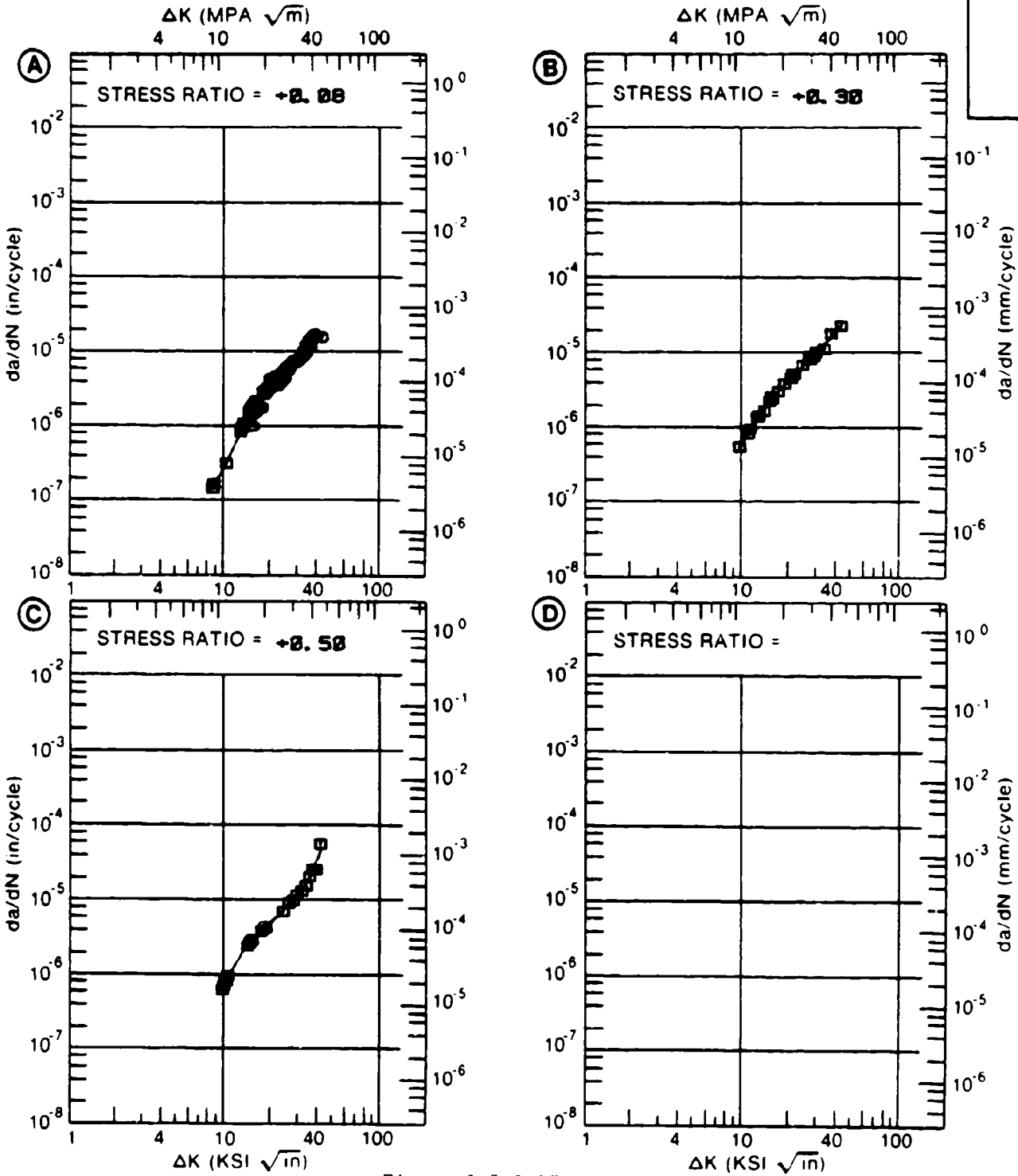


Figure 3.8.3.17

TABLE 3.8.3.18

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.18 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------------|----------|------------------------------|------------------------------|------------------------------|------|
| | | A | B | C | D |
| | | E= R. T. L. H. A. -1. OHZ | E=- 65 F L. H. A. -6. OHZ | E= R. T. S. C. S. -1. OHZ | |
| DELTA K MIN | A: 8.72 | .151 | | | |
| | B: 15.07 | | .404 | | |
| | C: 12.88 | | | .517 | |
| | D: | | | | |
| | 9.00 | .177 | | | |
| | 10.00 | .290 | | | |
| | 13.00 | .863 | | | .544 |
| | 16.00 | 1.80 | .594 | | 1.68 |
| | 20.00 | 3.57 | 1.67 | | 5.24 |
| | 25.00 | 6.47 | 3.68 | | 13.6 |
| | 30.00 | 10.0 | | | 24.5 |
| | 35.00 | 14.1 | | | 35.8 |
| | 40.00 | | | | 45.9 |
| | 50.00 | | | | 60.7 |
| DELTA K MAX | A: 36.40 | 15.3 | | | |
| | B: 29.64 | | 7.95 | | |
| | C: 56.24 | | | 66.5 | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 16.46 | 12.41 | 14.12 | |

| | | | | | | |
|---------------------------------------|----------|---------|----------|---|---|---|
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | 0.5-0.8 | 0.8-1.25 | 1 | 1 | 1 |
| | 1.25-2.0 | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 1.50" TH ROLLED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 200.0 KSI
 ULT. STRENGTH: 216.0 KSI
 SPECIMEN THK: 0.090- 0.093"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837, 88579

STAIN.
 STEEL
 PH13-8MO

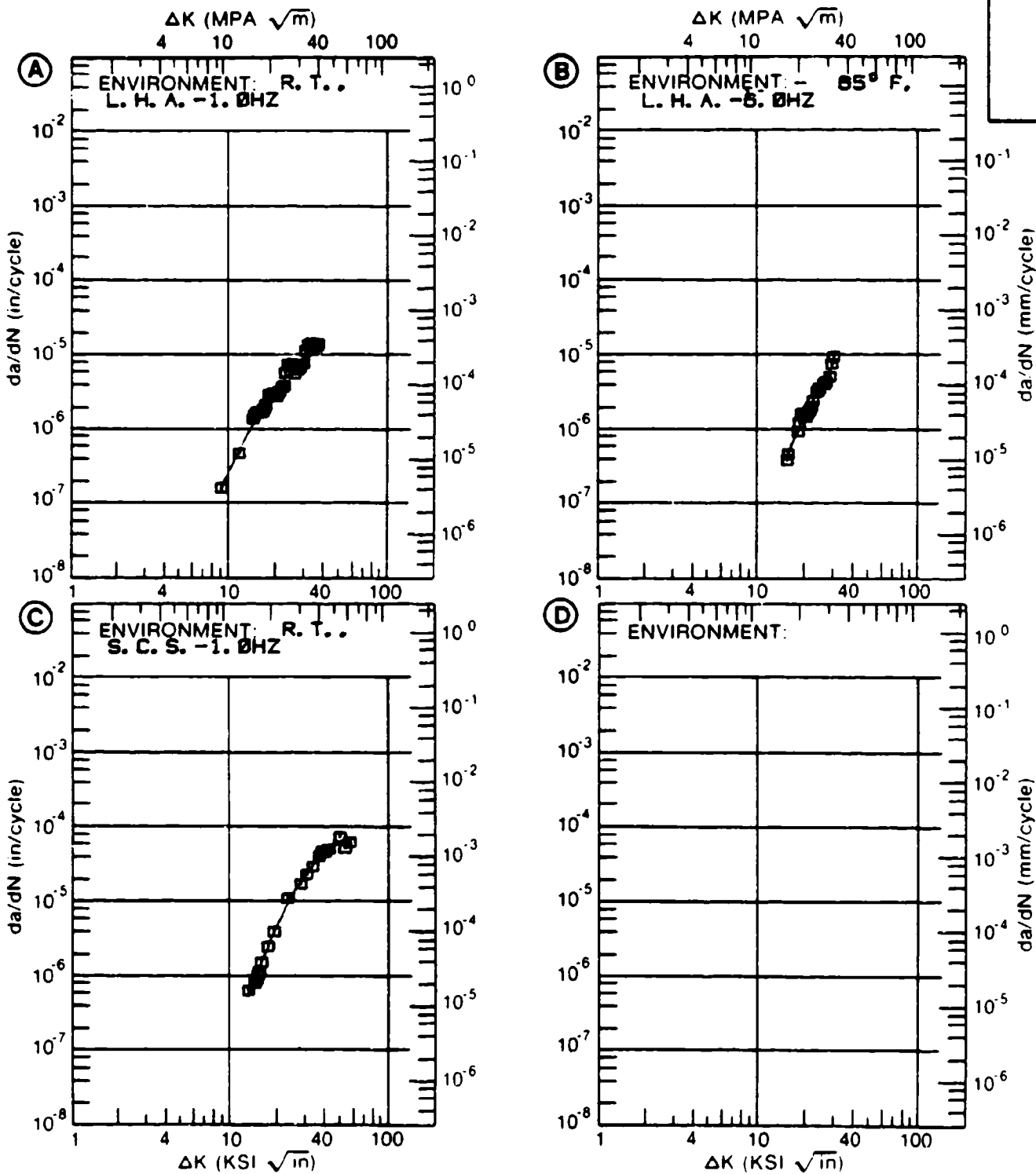


Figure 3.8.3.18

TABLE 3.8.3.19

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.19 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | | |
| DELTA K MIN | A: 11.05 | .260 | | | |
| | B: 8.60 | | .276 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | | .372 | | |
| | 10.00 | | .640 | | |
| | 13.00 | 1.07 | 2.10 | | |
| | 16.00 | 2.32 | 6.04 | | |
| | 20.00 | 4.15 | 12.2 | | |
| | 25.00 | 13.7 | 25.5 | | |
| | 30.00 | 41.7 | 70.5 | | |
| | 35.00 | 63.4 | 183. | | |
| DELTA K MAX | A: 38.49 | 65.6 | | | |
| | B: 36.46 | | 225. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 24.63 | 15.20 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | | 2 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1000
 FORM: 1.50" TH ROLLED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.0 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 208.0 KSI
 ULT. STRENGTH: 216.0 KSI
 SPECIMEN THK: 0.990- 1.002"
 SPECIMEN WIDTH: 7.390- 7.400"
 REFERENCES: 85837, 88579

STAIN.
STEEL

PH13-8MC

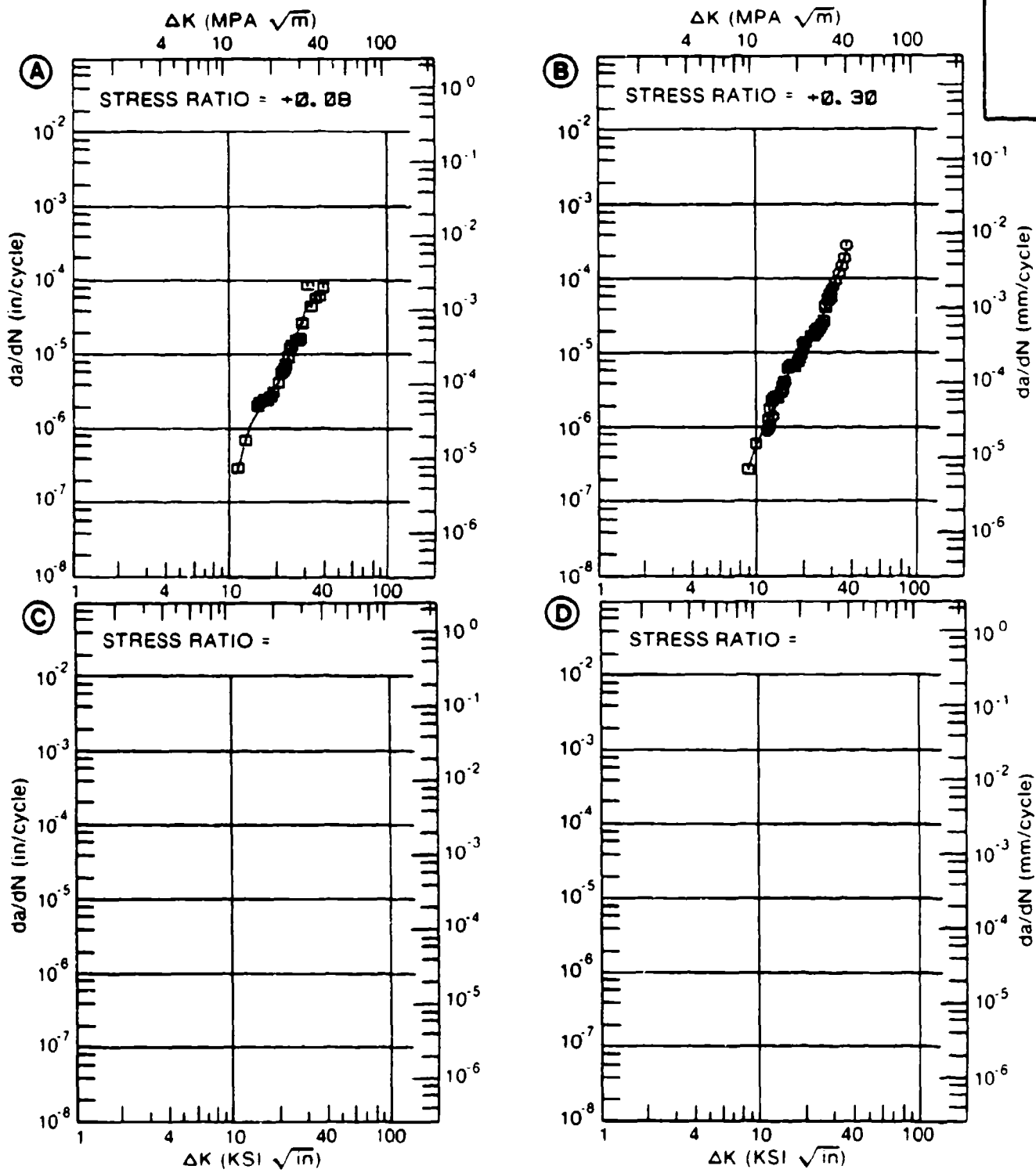


Figure 3.8.3.19

CONDITION/HT: H1000
 FORM: 1.50" TH ROLLED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 206.0 KSI
 ULT. STRENGTH: 216.0 KSI
 SPECIMEN THK: 0.990"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88579, 85837

STAIN.
 STEEL
 PH13-8MO

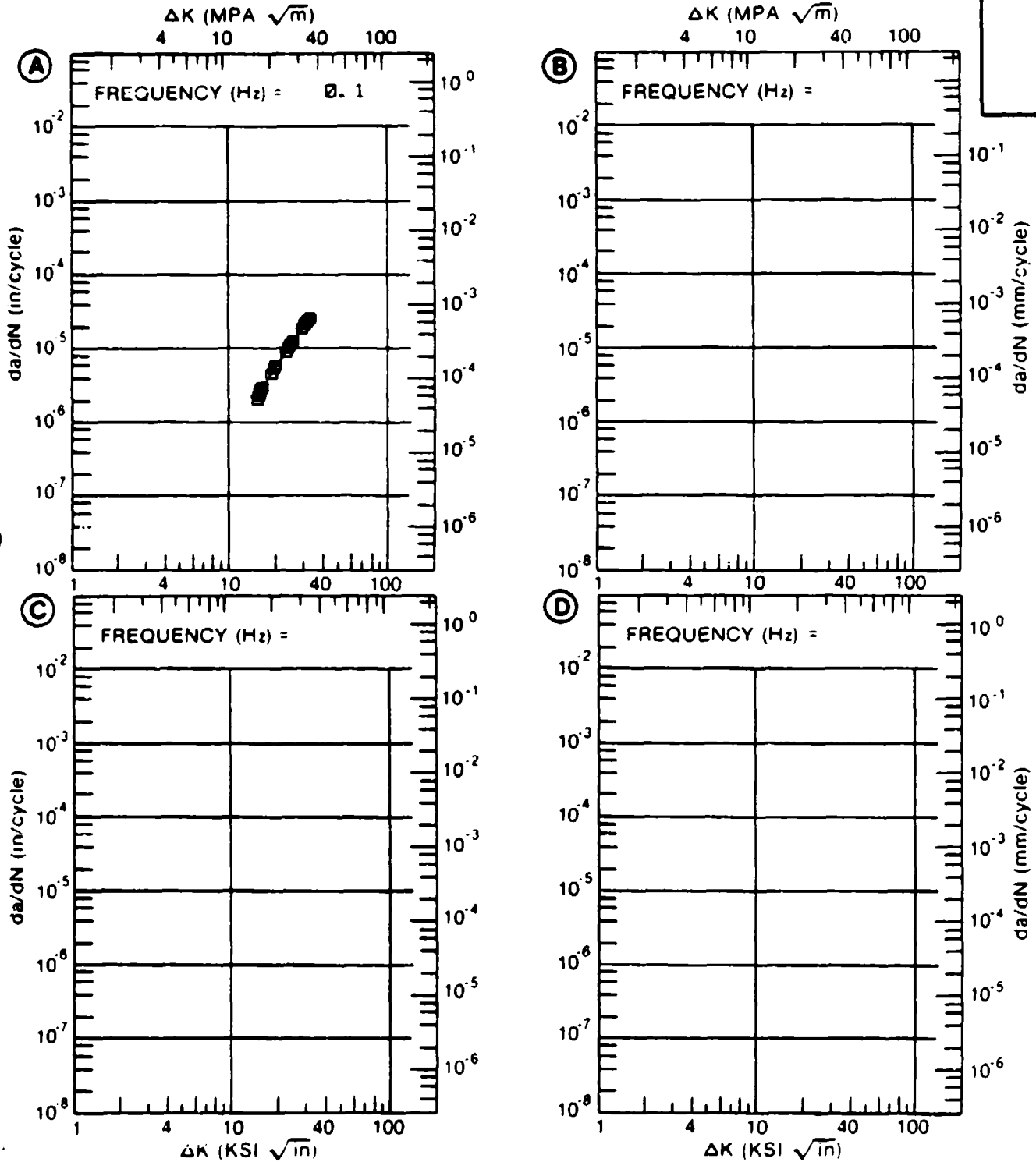


Figure 3.8.3.20

FABLE 3.8.3.21

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.8.3.21 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL PH13-8MO
CONDITION: H1000

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|---------------------------------------|--|------------------------------|------------------------------|----|
| | A | B | C | D |
| | E= R. T. L. H. A. -6. OHZ | E=- 65 F L. H. A. -6. OHZ | E= R. T. S. T. W. -1. OHZ | |
| DELTA K MIN | A: 10.66 : .158 | B: 11.98 : .360 | C: 7.82 : .101 | D: |
| | 8.00 : .106 | 9.00 : .162 | 10.00 : .286 | |
| | 13.00 : .658 | 16.00 : 1.88 | 19.00 : 1.47 | |
| | 20.00 : 4.01 | 25.00 : 6.78 | 30.00 : 9.74 | |
| | 35.00 : 13.5 | 40.00 : 18.8 | | |
| DELTA K MAX | A: 42.91 : 23.2 | B: 30.75 : 9.87 | C: 36.71 : 102. | D: |
| ROOT MEAN SQUARE PERCENT ERROR | 3.59 | 10.72 | 13.75 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | 1 | |

CONDITION/HT: H1000
 FORM: 1.50" TH ROLLED BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 210.0 - 215.0 KSI
 ULT. STRENGTH: 219.0 KSI
 SPECIMEN THK: 0.989 - 0.993"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88579, 85937

STAIN.
STEEL

PH13-8MO

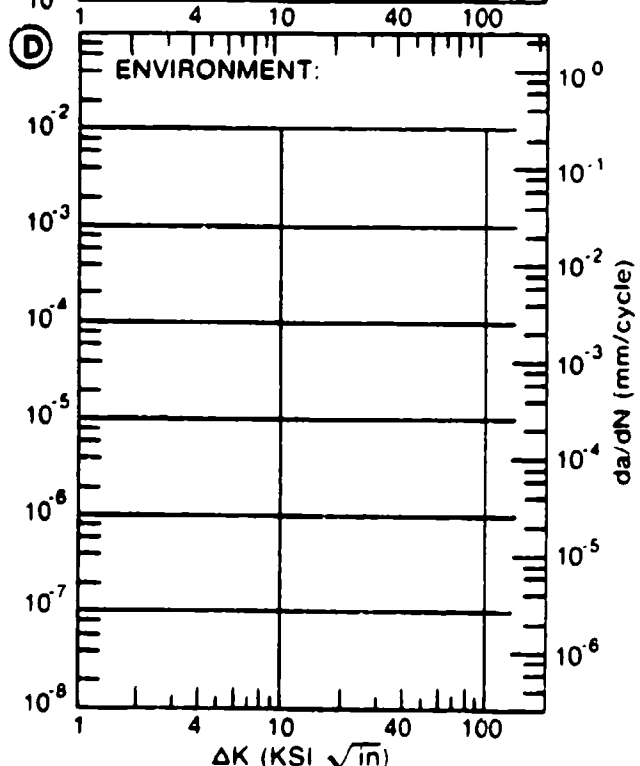
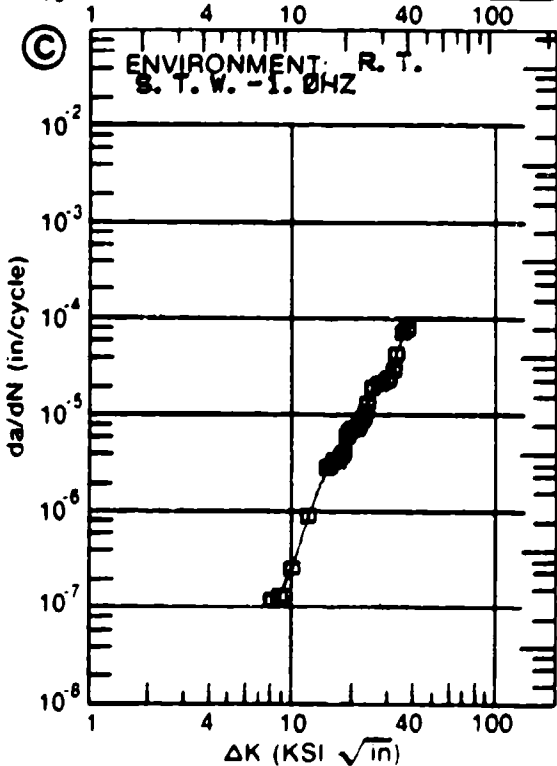
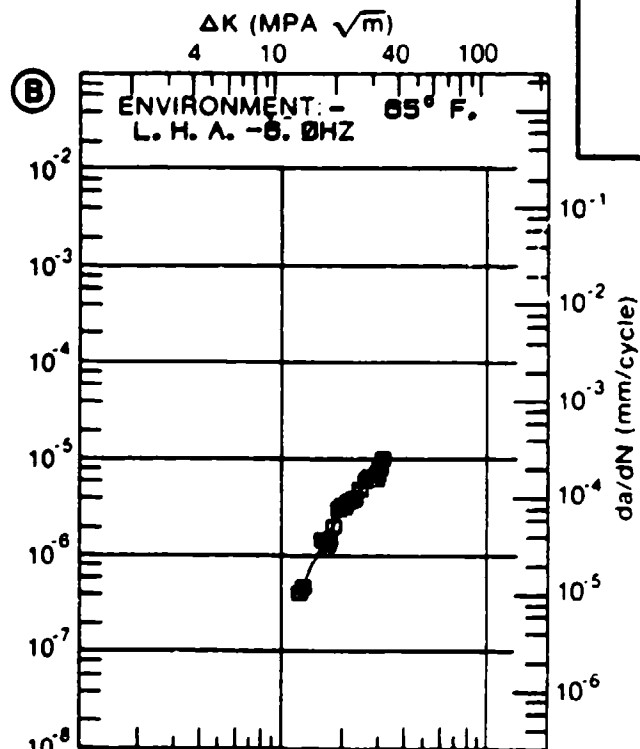
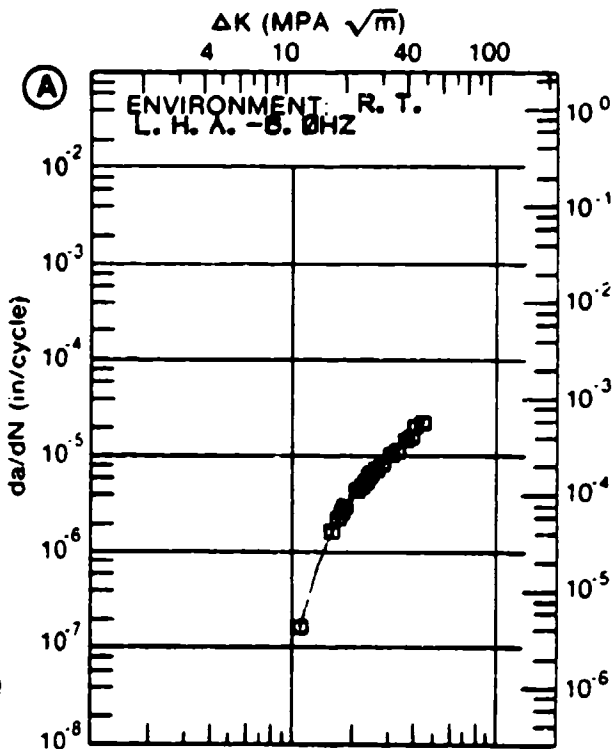


Figure 3.8.3.21

Table 3.8.3.22

| CONDITION | FORM THICK (IN) | | TEST TEMP (F) | SPEC YIELD OR STR (KSI) | ENVIRONMENT | SPECIMEN | | CRACK LENGTH (IN) | K (ISCC) | MEAN DEV | STAN | TEST TIME (MIN) | DATE REFER | | | |
|-----------|-----------------|------|---------------|-------------------------|------------------|------------|------------|-------------------|----------|----------|------|-----------------|------------|-------------|---------------|-------|
| | W | B | | | | WIDTH (IN) | THICK (IN) | | | | | | | DESIGN (IN) | (KSI-SURT IN) | |
| H 950 | 4.00 | 4.00 | R T | 207 | 5.3.5 PCT NAACL | 1.500 | 0.480 | C.N.T | 73 | 90 | 73 | 90 | > 60000 | 1971 | 84333 | |
| H 950 | 4.00 | 4.00 | R T | 204 | 0 S T M | 5.500 | 1.000 | DCB | 131 | 00 | > | 48 | 00 | 60360 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 130 | 00 | > | 50 | 00 | 60320 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 131 | 00 | > | 46 | 30 | 51720 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 131 | 00 | > | 49 | 00 | 51720 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 130 | 00 | > | 49 | 00 | 48780 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 130 | 00 | > | 48 | 00 | 51720 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 131 | 00 | > | 40 | 00 | 86280 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 130 | 00 | > | 46 | 00 | 80320 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 131 | 00 | > | 50 | 00 | 86280 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 204 | 0 | 5.500 | 1.000 | DCB | 130 | 00 | > | 48 | 00 | 48780 | 1976 | R1006 |
| | | | | | | | | | 48.0/ | 2.8 | | | | | | |
| H 950 | 2.25 | 2.25 | R T | 196 | 7 INDUSTRIAL ATM | 2.000 | 1.000 | CT | 62 | 60 | 59 | 00 | ---- | 1973 | 86688 | |
| H 950 | 2.25 | 2.25 | R T | 196 | 7 SEACAST ATM | 2.000 | 1.000 | CT | 62 | 60 | 31 | 00 | ---- | 1973 | 86688 | |
| H 950 | 2.25 | 2.25 | R T | 196 | 7 20 PCT NAACL | 2.000 | 1.000 | CT | 62 | 60 | 46 | 00 | ---- | 1973 | 86688 | |
| H1000 | 1.50 | 1.50 | R T | 214 | 0 S.T.M. | 5.500 | 1.000 | DCB | 132 | 00 | > | 53 | 00 | 116820 | 1976 | R1006 |
| | 1.50 | 1.50 | R T | 214 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | < | 53 | 00 | 116820 | 1976 | R1006 |
| | 1.50 | 1.50 | R T | 214 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | 55 | 00 | 120840 | 1976 | R1006 | |
| | 1.50 | 1.50 | R T | 214 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | > | 52 | 00 | 120840 | 1976 | R1006 |
| | 1.50 | 1.50 | R T | 214 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | < | 54 | 00 | 86280 | 1976 | R1006 |
| H1000 | 1.50 | 1.50 | R T | 213 | 0 S.T.M. | 5.500 | 1.000 | DCB | 132 | 00 | > | 54 | 00 | 116820 | 1976 | R1006 |
| | 1.50 | 1.50 | R T | 213 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | > | 53 | 00 | 116820 | 1976 | R1006 |
| | 1.50 | 1.50 | R T | 213 | 0 | 5.500 | 1.000 | DCB | 132 | 00 | < | 53 | 00 | 116820 | 1976 | R1006 |
| H1000 | 1.00 | 4.00 | R T | 215 | 0 S.T.M. | 2.544 | 0.998 | MDL | 1.207 | ----- | 88 | 10 | > | 60420 | 1978 | GD009 |
| | 4.00 | 4.00 | R T | 201 | 0 | 5.500 | 1.000 | DCB | 127 | 00 | > | 74 | 00 | 51720 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 201 | 0 | 5.500 | 1.000 | DCB | 127 | 00 | > | 80 | 00 | 80320 | 1976 | R1006 |
| H1000 | 1.00 | 1.00 | R T | 215 | 0 3.5% NAACL | 2.548 | 0.998 | MDL | 1.250 | ----- | 82 | 30 | > | 60420 | 1978 | GD009 |
| | 1.00 | 1.00 | R T | 215 | 0 | 2.549 | 0.998 | MDL | 1.110 | ----- | 94 | 80 | > | 60420 | 1978 | GD009 |
| | | | | | | | | | 88.6/ | 8.8 | | | | | | |
| H1000 | 1.00 | 1.00 | R T | 216 | 0 S.T.M. | 2.544 | 0.999 | MDL | 1.048 | ----- | 99 | 30 | > | 60420 | 1978 | GD009 |
| | 1.00 | 1.00 | R T | 216 | 0 | 2.549 | 0.999 | MDL | 1.048 | ----- | 99 | 60 | > | 60420 | 1978 | GD009 |
| | 4.00 | 4.00 | R T | 198 | 0 | 5.500 | 1.000 | DCB | 125 | 00 | > | 49 | 00 | 80320 | 1976 | R1006 |
| | 4.00 | 4.00 | R T | 198 | 0 | 5.500 | 1.000 | DCB | 125 | 00 | > | 49 | 00 | 80320 | 1976 | R1006 |

Table 3.8.3.22 (Continued)

| CONDITION | PRODUCT FORM | THICK (IN) | TEST TEMP (F) | SPEC YIELD STR (KSI) | ENVIRONMENT | SPECIMEN | | WIDTH (IN) | THICK (IN) | DESIGN (IN) | CRACK LENGTH (IN) | K(I0) | K(I0) (KSI*SQRT IN) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|-----------|--------------|------------|---------------|----------------------|-------------|----------------|-------|------------|------------|-------------|-------------------|-------|---------------------|-------|----------|-----------------|------------|
| | | | | | | M | B | | | | | | | | | | |
| H1000 | FB | 4.00 | R T | T-L | 198.0 | S.T.M. | 5.900 | 1.000 | DCB | --- | 125.00 | > | 46.00 | | | 63520 | 1976 R1006 |
| | | 4.00 | | | 179.0 | | 5.900 | 1.000 | DCB | --- | 125.00 | > | 71.00 | | | 51720 | 1976 R1006 |
| | | 4.00 | | | 198.0 | | 5.900 | 1.000 | DCB | --- | 125.00 | > | 68.00 | 99.6/ | 0.1 | 51720 | 1976 R1006 |
| H1000 | FB | 1.00 | R T | T-L | 216.0 | 3.5Z NaCl | 2.945 | 0.998 | MOL | 1.880 | --- | --- | 63.20 | | | 60420 | 1978 CD009 |
| | | 1.00 | | | 216.0 | | 2.947 | 0.999 | MOL | 1.250 | --- | --- | 85.90 | 74.4/ | 15.8 | 60420 | 1978 CD009 |
| H1000 | RR | 1.50 | R T | L-T | 208.0 | F.C.S. | 5.500 | 1.000 | DCB | --- | 132.00 | > | 75.00 | | | 75180 | 1976 R1006 |
| H1000 | RB | 1.50 | R T | L-T | 208.0 | S.C.B. | 5.500 | 1.000 | DCB | --- | 132.00 | > | 87.00 | | | 60180 | 1976 R1006 |
| | | 1.50 | | | 208.0 | | 5.500 | 1.000 | DCB | --- | 132.00 | > | 70.00 | | | 75240 | 1976 R1006 |
| H1000 | RB | 1.50 | R T | L-T | 208.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | 132.00 | > | 73.00 | | | 86280 | 1976 R1006 |
| | | 1.50 | | | 208.0 | | 5.500 | 1.000 | DCB | --- | 132.00 | > | 73.00 | | | 116820 | 1976 R1006 |
| | | 1.50 | | | 208.0 | | 5.500 | 1.000 | DCB | --- | 132.00 | > | 70.00 | | | 116820 | 1976 R1006 |
| H1000 | RB | 1.50 | R T | L-T | 208.0 | | 5.500 | 1.000 | DCB | --- | 132.00 | > | 73.00 | | | 116820 | 1976 R1006 |
| | | 1.50 | | | 215.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | 133.00 | > | 63.00 | | | 86280 | 1976 R1006 |
| | | 1.50 | | | 215.0 | | 5.500 | 1.000 | DCB | --- | 133.00 | > | 63.00 | | | 116820 | 1976 R1006 |
| H1000 | RB | 1.50 | | | 215.0 | | 5.500 | 1.000 | DCB | --- | 133.00 | > | 63.00 | | | 116820 | 1976 R1006 |
| | | 1.50 | | | 215.0 | | 5.500 | 1.000 | DCB | --- | 133.00 | > | 63.00 | | | 116820 | 1976 R1006 |
| H1050 | B | 2.25 | R T | T-L | 178.5 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | --- | 87.80 | | 83.00 | | | --- | 1973 86688 |
| H1050 | B | 2.25 | R T | T-L | 178.5 | SEACAST ATM | 2.000 | 1.000 | CT | --- | 87.80 | | 44.00 | | | --- | 1973 86688 |
| H1050 | B | 2.25 | R T | T-L | 178.5 | 20 PCT NaCl | 2.000 | 1.000 | CT | --- | 87.80 | | 65.00 | | | --- | 1973 86688 |
| RH 950 | BR | 1.50 | R T | L-S | 219.0 | S.T.M. | 5.500 | 1.000 | CT | --- | 98.00 | > | 50.00 | | | 120960 | 1976 R1006 |
| | | 1.50 | | | 217.0 | | 5.500 | 1.000 | CT | --- | 97.00 | > | 54.00 | | | 120960 | 1976 R1006 |
| | | 1.50 | | | 219.0 | | 5.500 | 1.000 | CT | --- | 98.00 | > | 51.00 | | | 120960 | 1976 R1006 |
| RH 975 | BR | 1.50 | R T | L-S | 216.0 | S.T.M. | 5.500 | 1.000 | CT | --- | 97.00 | > | 67.00 | | | 120960 | 1976 R1006 |
| | | 1.50 | | | 219.0 | | 5.500 | 1.000 | CT | --- | 98.00 | > | 58.00 | | | 120960 | 1976 R1006 |
| | | 1.50 | | | 216.0 | | 5.500 | 1.000 | CT | --- | 97.00 | > | 67.00 | | | 120960 | 1976 R1006 |

Table 3.8.3.22 (Continued)

| CONDITION | STAINLESS STEEL PH13-8MO K (ISUC) | | | | | | | | | | TEST TIME (MIN) | DATE REFER | | | | |
|------------|-----------------------------------|--------------------|--------------|-------------|-------------|---------------|------------|-------------|-------------|----------|-----------------|------------|----------|-----------|-------|-------|
| | FURN THICK (IN) | TESI SPEC TEMP (F) | OR STR (KSI) | YIELD (KSI) | ENVIRONMENT | SPECIMEN | | CRACK | | STAN DEV | | | | | | |
| | | | | | | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | | | | K (ISUC) | MEAN (IN) | | |
| RH1000 | BR | 1.50 | R.T. | L.S | 215.0 | S.T.M | 5.500 | 1.000 | CT | --- | 96.00 | 101.00 | 120960 | 1976 | R1006 | |
| | | 1.50 | | | 215.0 | | 5.500 | 1.000 | CT | --- | 96.00 | 92.00 | 120960 | 1976 | R1006 | |
| | | 1.50 | | | 218.0 | | 5.500 | 1.000 | CT | --- | 97.00 | 83.00 | 120960 | 1976 | R1006 | |
| TYS=140KSI | P | 1.00 | R.T. | T-L | 140.0 | 3.5 PCT NAACL | --- | 1.000 | CANT* | --- | 180.00 | 170.00* | --- | --- | 1972 | 83613 |
| TYS=180KSI | P | 1.00 | R.T. | T-L | 180.0 | 3.5 PCT NAACL | --- | 1.000 | CANT* | --- | 190.00 | 160.00* | --- | --- | 1972 | 83613 |
| TYS=190KSI | P | 1.00 | R.T. | T-L | 190.0 | 3.5 PCT NAACL | --- | 1.000 | CANT* | --- | 180.00 | 130.00* | --- | --- | 1972 | 83613 |
| TYS=200KSI | P | 1.00 | R.T. | T-L | 200.0 | 3.5 PCT NAACL | --- | 1.000 | CANT* | --- | 190.00 | 155.00* | --- | --- | 1972 | 83613 |
| TYS=210KSI | P | 1.00 | R.T. | T-L | 210.0 | 3.5 PCT NAACL | --- | 1.000 | CANT* | --- | 135.00 | 120.00 | --- | --- | 1972 | 83613 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISUC/TYS)SQUARED

Table 3.9.2.1

| CONDITION | PROJECT | | TEST SPEC | YIELD STR (KSI) | WIDTH (IN) | THICK (IN) | SPECIMEN | | CRACK LENGTH | | | | GROSS STRESS | | K(AFP) STAM | | K(C) STAM | | | | | |
|-----------|---------|------------|-----------|-----------------|------------|------------|----------|-------|--------------|------------|-------------|-----------|--------------|-----------|-------------|------------|-----------|----------|------|-------|------|-------|
| | FORM | THICK (IN) | | | | | W | B | INIT (IN) | FINAL (IN) | ONSET (KSI) | MAX (KSI) | K(AFP) (KSI) | MEAN (IN) | DEV (IN) | K(C) (KSI) | MEAN (IN) | DEV (IN) | DATE | REFER | | |
| | | | | | | | | | 2A(O) 2A1F) | | | | | | | | | | | | | |
| SRH1050 | S | 0.03 | 63 | L-T | 174.5 | 24.040 | 0.033 | 5.990 | | | | | 72 | 60 | 231 | 63 | | | 1964 | 97573 | | |
| SRH1050 | S | 0.03 | R T | L-T | 174.5 | 7.990 | 0.025 | 2.010 | | | | | 118 | 10 | 218 | 44* | | | 1964 | 97573 | | |
| SRH1050 | S | 0.03 | R T | L-T | 174.5 | 24.020 | 0.025 | 3.000 | | | | | 95 | 90 | 210 | 21 | | | 1964 | 97573 | | |
| | | 0.03 | | | 174.5 | 24.030 | 0.025 | 4.000 | | | | | 72 | 40 | 231 | 22 | | | 1964 | 97573 | | |
| | | 0.03 | | | 174.5 | 24.040 | 0.025 | 4.000 | | | | | 71 | 90 | 229 | 61 | 223 | 7/11.7 | ---- | ---- | 1964 | 97573 |
| SRH1050 | S | 0.05 | R T | L-T | 196.6 | 24.010 | 0.050 | 4.000 | | | | | 92 | 10 | 294 | 19 | | | 1964 | 97573 | | |
| SRH1050 | S | 0.09 | R T | L-T | 197.4 | 24.100 | 0.073 | 6.000 | | | | | 115 | 70 | 369 | 42 | | | 1964 | 97573 | | |

BUCKLING OF CRACK EDGES RESTRAINED

*NOTE- NET SECTION STRESS EXCEEDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV

Table 3.10.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
STAINLESS STEEL ALLOY PH19-7MO AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | | COLLED JAW |
|--------------|---|----------------|------------|
| | L-I | I-L | |
| RH 930 | ----- | 30.6 ± 0.1 (2) | ----- |
| RH1050 | ----- | 40.2 ± 1.9 (3) | ----- |

Table 3.10.2.1

| CONDITION | STAINLESS STEEL PH19-7MO K(1C) | | | | | | | | | | DATE | REFER |
|-----------|--------------------------------|------------|---------------|-----------------|----------------------|------------|------------|--------|-------------------|------------------|-------|-------|
| | FORM | THICK (IN) | TEST TEMP (F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | K(1C) MEAN (KSI) | | |
| RH 950 | RP | 1.25 | R T | T-1 | 204.0 | 2.000 | 1.000 | CT | A | | 30.70 | 0.1 |
| | | | | | | | | | 1.007 | 0.06 | | |
| RH1050 | RP | 1.25 | R T | T-L | 195.0 | 2.000 | 1.000 | CT | A | | 38.50 | 1.9 |
| | | | | | | | | | 1.010 | 0.11 | | |
| | 1.25 | R T | T-L | 195.0 | 2.000 | 1.000 | CT | B | | 41.30 | 1.3 | |
| | | | | | | | | 1.006 | 0.11 | | | |

Table 3.10.3.1

| CONDITION | FORM | THICK (IN) | YIELD STRENGTH (KSI) | TEST TEMP (F) | ENVIRONMENT | WIDTH (IN) | THICK (IN) | DESIGN (IN) | CRACK LENGTH (IN) | K (I SCC) | MEAN (IN) | STAN DEV | TEST TIME (MIN) | DATE REFER |
|-----------|------|------------|----------------------|---------------|--------------|------------|------------|-------------|-------------------|-----------|-----------|----------|-----------------|------------|
| | | | | | | | | | | | | | | |
| RH 950 | B | 1.75 | 196 | R.T. | 3.5 PCT NaCl | 1.500 | 0.480 | CANT | 31.50 | 14.00 | | | > 30000 | 1971 84333 |
| TH1050 | B | 1.75 | 167 | R.T. | 3.5 PCT NaCl | 1.500 | 0.480 | CANT | 33.60 | 18.50 | | | > 60000 | 1971 84333 |

Table 3.11.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
STAINLESS STEEL ALLOY 19-3PH AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|----------------------------|---|-----------------------|
| | FORGING | |
| CONDITION/HT | L-I | B-I |
| Y _S =150-165KSI | ----- | 94.8 ± 6.9 (3) |
| | ROLLED BAR | |
| CONDITION/HT | L-I | B-I |
| H 900 | ----- | 72.7 ± 4.9 (6) |

Table 3.11.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 STAINLESS STEEL 15-3PH

TEST CONDITIONS

SPECIMEN ORIENTATION: T-L

ENVIRONMENT: H. H. A.
 AT R. T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | |
|----------------|--------------|--------------|-----------|-------------------------------|---|---|------|------|------|
| | | | | | 2.5 | 5 | 10 | 20 | 50 |
| TUS-150-165KSI | BILLET | -1.00 | | | | | | 3.93 | 45.6 |
| TUS-150-165KSI | BILLET | -0.20 | | | | | | 3.05 | 33.6 |
| TUS-150-165KSI | BILLET | 0.04 | | | | | | 2.92 | 33.6 |
| TUS-150-165KSI | BILLET | 0.40 | | | | | 0.73 | 9.18 | |

Table 3.11.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL 15-5PH

TEST CONDITIONS

SPECIMEN ORIENTATION S-L

ENVIRONMENT: H.H.A.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|----------------|--------------|--------------|------------|-------------------------------|-----|---|----|----|------|------|---|
| TUS-150-165KSI | BILLET | -1.00 | | | | | | | 4.78 | 51.6 | |
| TUS-150-165KSI | BILLET | -0.20 | | | | | | | 3.46 | 39.8 | |
| TUS-150-165KSI | BILLET | 0.04 | | | | | | | 3.16 | 37.9 | |
| TUS-150-165KSI | BILLET | 0.40 | | | | | | | 6.02 | | |

Table 3.11.2.1

| CONDITION | STAINLESS STEEL 19-5PH | | | | | | | | | | K(IIC) | | DATE | REFER |
|------------------|------------------------|---------------|----------------------------|-------------------------|---------------|---------------|--------|-------------------------|--------------|---------------------|--------------------------|-------------|-------|-------|
| | --PRODUCT-- FORM | THICK (IN) | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | 2.5* (IN) | K(IIC) (KSI/√IN) | K(IIC) MEAN (KSI/√IN) | STAN DEV | | |
| H 900 | RB | 2.25 | 171.0 | T-L | 4.000 | 2.000 | CT | 2.037 | 0.43 | 70.90 | | 1973 | 86688 | |
| | | 2.25 | 171.0 | | 4.000 | 2.000 | CT | 2.064 | 0.42 | 70.50 | | 1973 | 86688 | |
| | | 2.25 | 171.0 | | 2.000 | 1.000 | CT | 1.040 | 0.38 | 66.50 | | 1973 | 86688 | |
| | | 2.25 | 171.0 | | 4.000 | 2.000 | CT | 1.049 | 0.46 | 73.10 | | 1973 | 86688 | |
| | | 2.25 | 171.0 | | 2.000 | 1.000 | CT | 2.068 | 0.54 | 79.40 | | 1973 | 86688 | |
| H 900 | RB | 4.00 | 185.0 | L-R | 2.000 | 1.000 | NE | 1.051 | 0.47 | 75.80 | 72.7/ | 4.5 | 1973 | 86688 |
| | | | | | 2.000 | 1.000 | NE | 1.000 | 0.55 | 86.90 | | | 1972 | 84212 |
| TYS=150-165KSI F | | | 155.0 | T-L | 3.000 | 1.500 | CT | | 1.07 | 102.50 | | | 1978 | 8M007 |
| | | | 155.0 | | 3.000 | 1.500 | CT | | 0.87 | 92.70 | | | 1978 | 8M007 |
| | | | 155.0 | | 3.000 | 1.500 | CT | | 0.83 | 89.20 | 94.8/ | 6.9 | 1978 | 8M007 |

TABLE 3.11.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.11.3.1 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 15-5PH
CONDITION: H1025

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|-----------------------------|---------|------------------------------|----------|
| | A | B | C | D |
| | E= R. T. LAB AIR-10. OHZ | | E= R. T. 3. 5%NACL-1. OHZ | |
| DELTA K MIN | A: 30.17 | B: 8.27 | C: 5.06 | D: 9.97 |
| | B: 17.18 | | | 15.7 |
| | C: 20.00 | | | 20.3 |
| | D: 25.00 | | | |
| | 30.00 | | | |
| | 35.00 | 15.0 | | |
| | 40.00 | 18.0 | | |
| | 50.00 | 22.0 | | |
| | 60.00 | 29.7 | | |
| | 70.00 | 41.2 | | |
| | 80.00 | 56.1 | | |
| | 90.00 | 74.1 | | |
| | 100.00 | 94.2 | | |
| DELTA K MAX | A: 124.79 | B: 146. | C: 21.5 | D: 30.88 |
| | B: 30.88 | | | |
| | C: 124.79 | | | |
| | D: 30.88 | | | |

ROOT MEAN SQUARE PERCENT ERROR B. 12 19. 17

LIFE PREDICTION RATIO SUMMARY (NP/NA) 0. 0-0. 5 0. 5-0. 8 0. 8-1. 25 1. 25-2. 0 2. 0

2 1

CONDITION/HT: H1025
 FORM: 1.50" TH BAR
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.50
 FREQUENCY:

YIELD STRENGTH: 150.7 KSI
 ULT. STRENGTH: 156.2 KSI
 SPECIMEN THK: 1.500"
 SPECIMEN WIDTH: 3.000"
 REFERENCES: 92270

STAIN.
 STEEL
 15-SPH

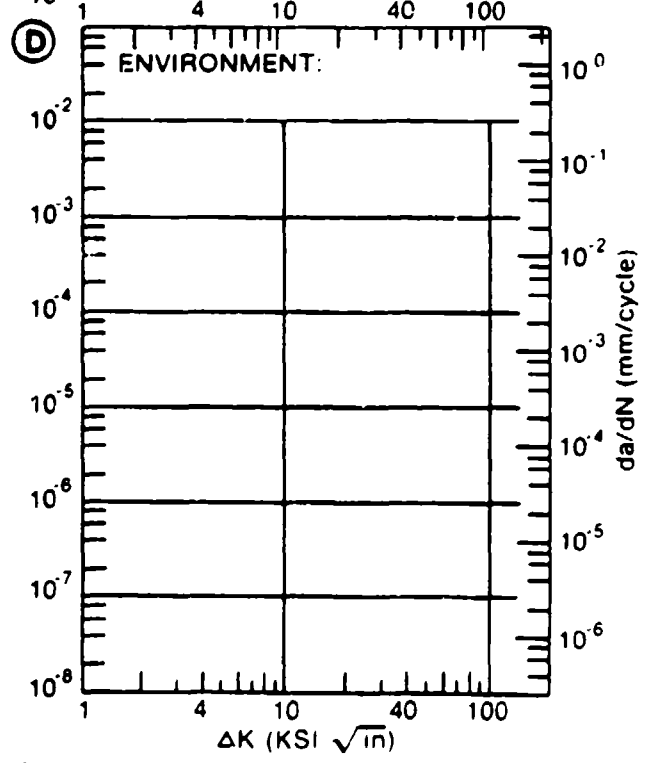
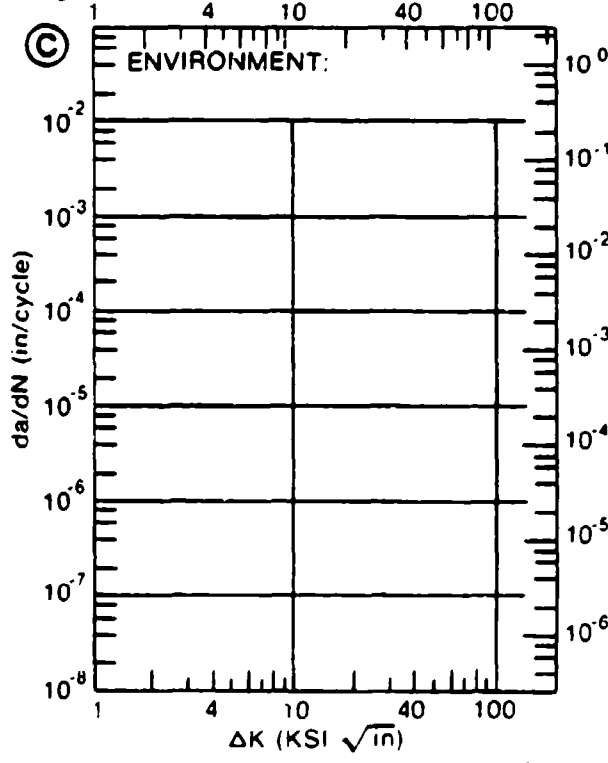
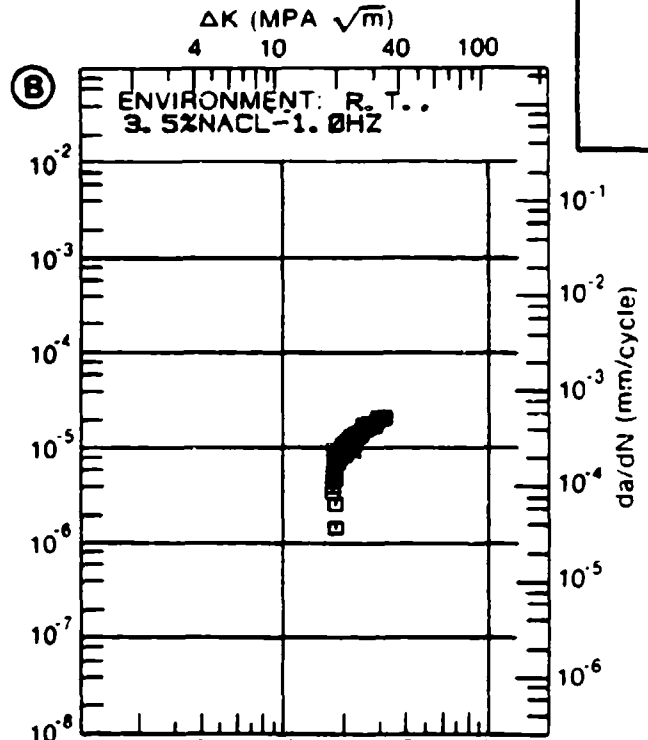
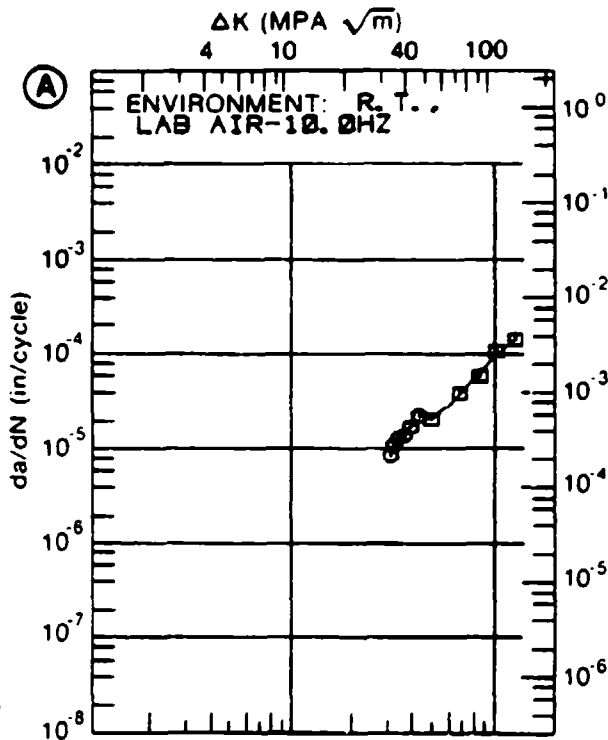


Figure 3.11.3.1

TABLE 3.11.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.11.3.2 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 15-5PH
CONDITION: H1025

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|--------------------------|--------|------|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: 28.88 | 1.50 | | |
| | B: 30.00 | 1.73 | | |
| | C: 35.00 | 3.08 | | |
| | D: 40.00 | 5.37 | | |
| | | 50.00 | 15.3 | |
| | | 60.00 | 31.1 | |
| | | 70.00 | 48.6 | |
| | | 80.00 | 70.0 | |
| | | 90.00 | 102. | |
| | | 100.00 | 155. | |
| DELTA K MAX | A: 107.17 | 219. | | |
| | B: | | | |
| | C: | | | |
| | D: | | | |

ROOT MEAN SQUARE 42.67
PERCENT ERROR

LIFE PREDICTION RATIO SUMMARY (NP/NA)

| | |
|----------|---|
| 0.0-0.5 | |
| 0.5-0.8 | |
| 0.8-1.25 | 2 |
| 1.25-2.0 | |
| >2.0 | |

CONDITION/HT: H1025
 FORM: 1.50" TH BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.05
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 151.2 KSI
 ULT. STRENGTH: 156.1 KSI
 SPECIMEN THK: 1.500"
 SPECIMEN WIDTH: 3.000"
 REFERENCES: 92270

STAIN.
STEEL

15-5PH

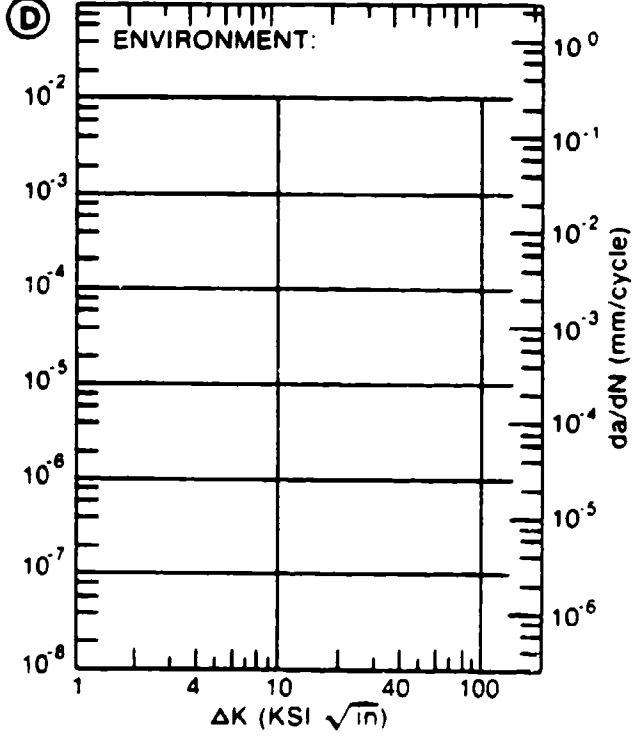
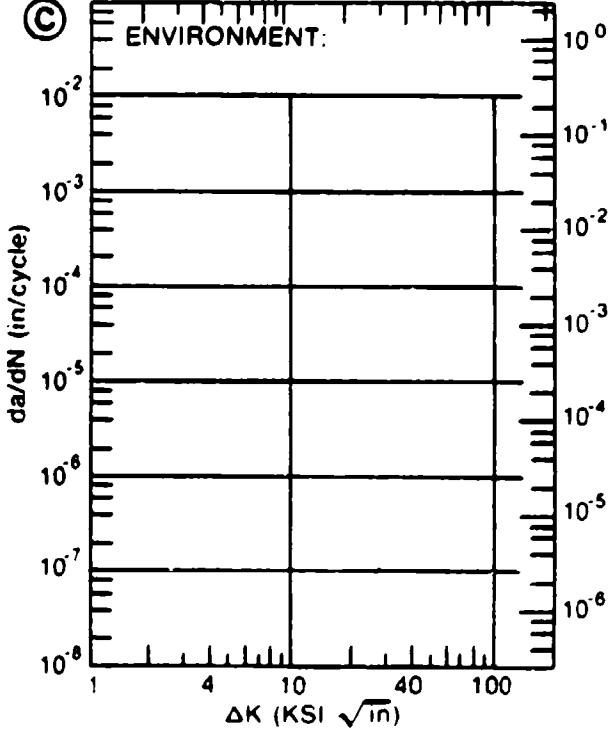
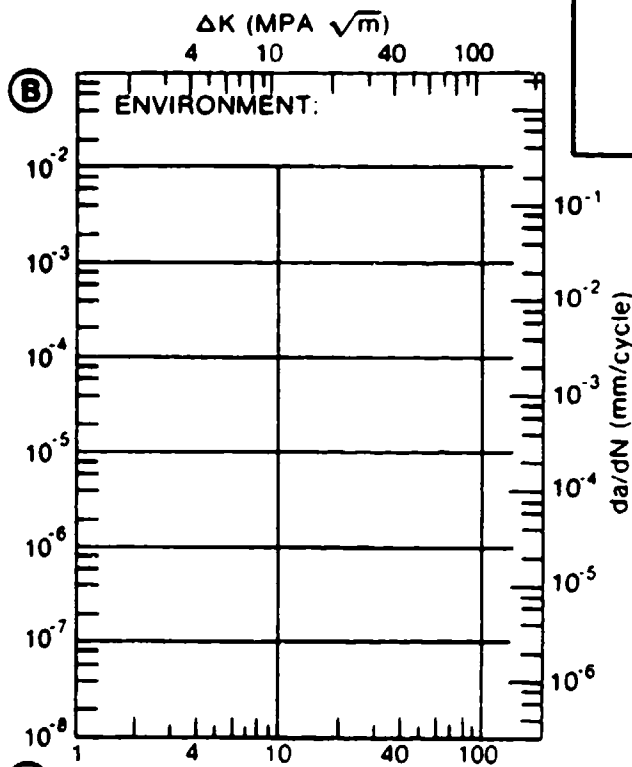
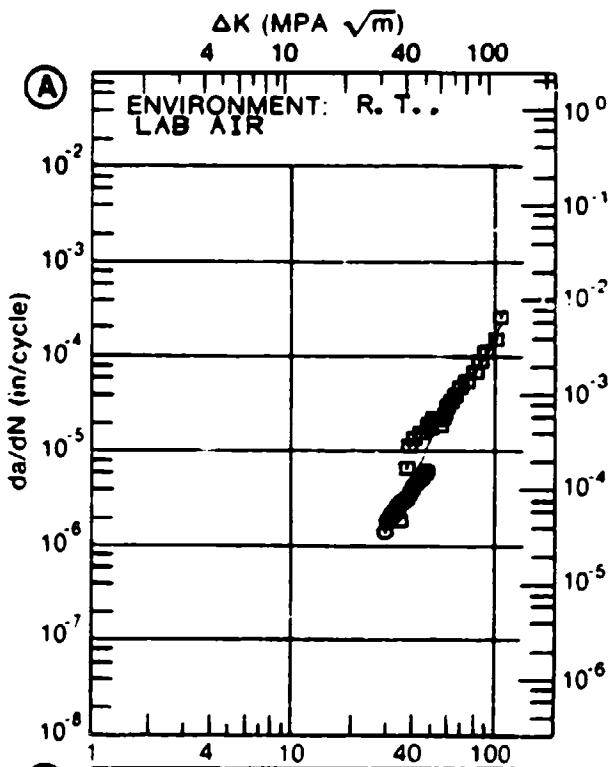


Figure 3.11.3.2

TABLE 3.11.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.11.3.3 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: STAINLESS STEEL 15-5PH | | | | | |
|----------------------------------|----------|---------------------------------------|---------|---|---|
| CONDITION: H1025 | | | | | |
| ENVIRONMENT: R. T. , 3.5% NaCl | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.05 | R=+0.50 | | |
| DELTA K | A: 33.23 | 17.9 | | | |
| MIN | B: 24.76 | | 13.2 | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | | 13.4 | | |
| | 30.00 | | 18.6 | | |
| | 35.00 | 19.9 | 26.7 | | |
| | 40.00 | 25.6 | 36.7 | | |
| | 50.00 | 39.4 | | | |
| | 60.00 | 60.4 | | | |
| DELTA K | A: 63.17 | 69.7 | | | |
| MAX | B: 43.53 | | 44.1 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 2.30 | 4.38 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1025
 FORM: 1.50" TH BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH: 151.2 KSI
 ULT. STRENGTH: 158.1 KSI
 SPECIMEN THK: 1.500"
 SPECIMEN WIDTH: 3.000"
 REFERENCES: 02270

STAIN.
 STEEL
 15-5PH

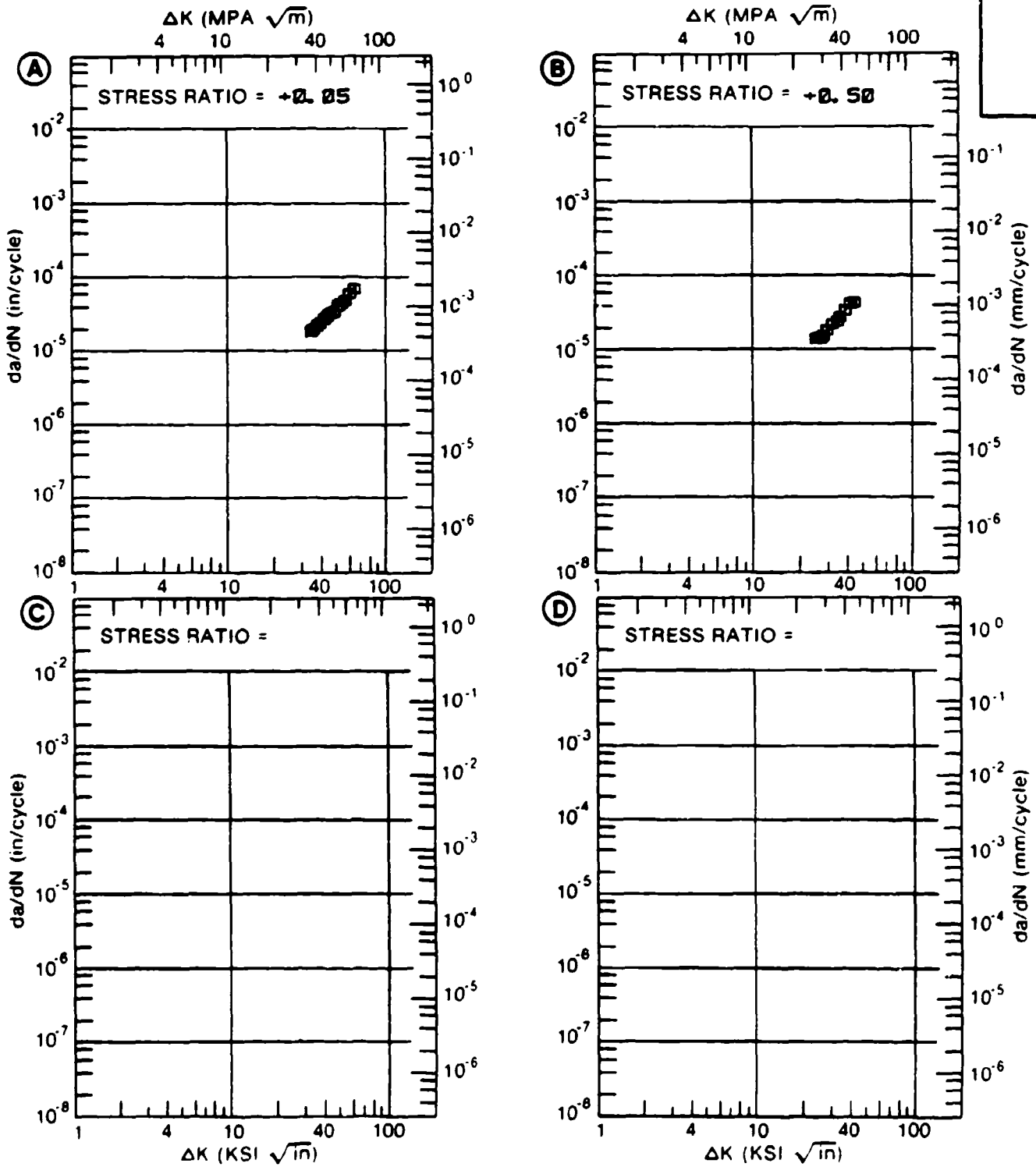


Figure 3.11.3.3

TABLE 3.11.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.11.3.4 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 15-5PH
CONDITION: TUS=150-165KSI
ENVIRONMENT: R. T., H. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---------|---------|---------|
| | | A | B | C | D |
| | | R=-1.00 | R=-0.20 | R=+0.04 | R=+0.40 |
| A: | 12.00 | .706 | | | |
| B: | 14.00 | | .915 | | |
| C: | 13.44 | | | .738 | |
| D: | 9.60 | | | | .629 |
| | 10.00 | | | | .739 |
| | 13.00 | .985 | | | 1.76 |
| | 16.00 | 2.07 | 1.52 | 1.45 | 3.05 |
| | 20.00 | 3.93 | 3.05 | 2.92 | 5.18 |
| | 25.00 | 6.82 | 5.43 | 5.22 | 8.94 |
| | 30.00 | 10.5 | 8.38 | 8.09 | 14.9 |
| | 35.00 | 15.5 | 12.2 | 11.8 | 24.9 |
| | 40.00 | 22.3 | 17.2 | 16.8 | 42.2 |
| | 50.00 | 45.6 | 33.6 | 33.6 | |
| | 60.00 | 94.6 | 66.2 | 67.8 | |
| | 70.00 | | 133. | 140. | |
| A: | 70.00 | 200. | | | |
| B: | 80.00 | | 272. | | |
| C: | 76.80 | | | 231. | |
| D: | 48.00 | | | | 101. |
| ROOT MEAN SQUARE | | 1.30 | .62 | 2.28 | 2.82 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: TUS-150-185KSI
 FORM: 0.50" TH BILLET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY:
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: BW005

STAIN.
 STEEL

15-5PH

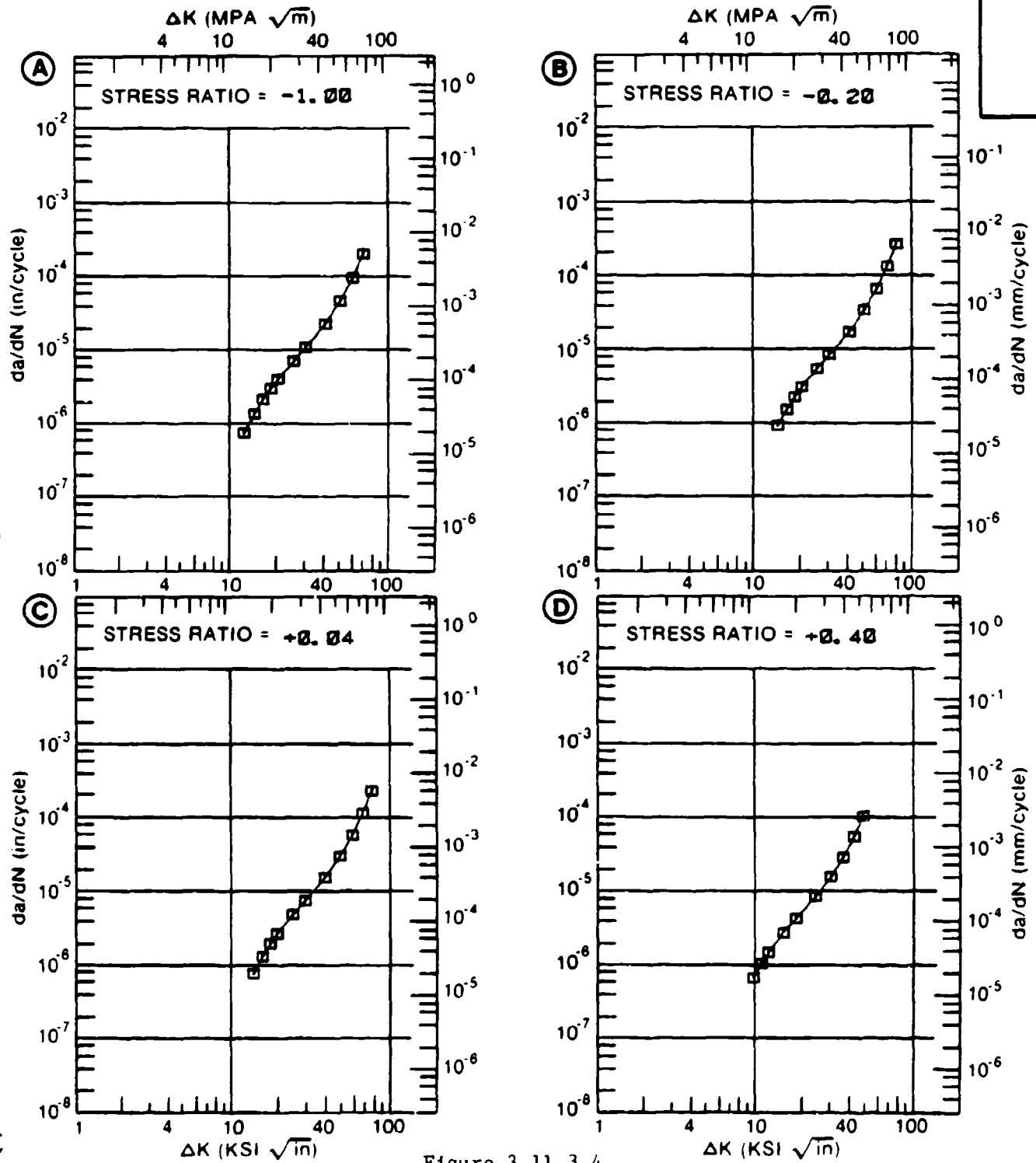


Figure 3.11.3.4

TABLE 3.11.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.11.3.5 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 15-5PH
CONDITION: TUS=150-165KSI
ENVIRONMENT: R. T., H. H. A.

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|---------------------------|--------------|--------------|--------------|
| | A R=-1.00 | B R=-0.20 | C R=+0.04 | D R=+0.40 |
| A: 14.00 | 1.67 | | | |
| B: 14.00 | | 1.31 | | |
| C: 15.36 | | | 1.56 | |
| D: 10.80 | | | | 1.24 |
| 13.00 | | | | 2.09 |
| 16.00 | 2.61 | 1.92 | 1.75 | 3.51 |
| 20.00 | 4.78 | 3.46 | 3.16 | 6.02 |
| 25.00 | 8.05 | 5.99 | 5.45 | 10.8 |
| 30.00 | 12.2 | 9.38 | 8.51 | 18.9 |
| 35.00 | 17.7 | 13.9 | 12.7 | 33.0 |
| 40.00 | 25.3 | 20.1 | 18.5 | 58.0 |
| 50.00 | 51.6 | 39.8 | 37.9 | |
| 60.00 | | | 76.5 | |
| A: 60.00 | 108. | | | |
| B: 60.00 | | 76.0 | | |
| C: 67.20 | | | 126. | |
| D: 48.00 | | | | 146. |
| ROOT MEAN SQUARE | 7.16 | 1.94 | 2.77 | 4.04 |
| PERCENT ERROR | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: TUS=150-165KSI
 FORM: 0.50" TH BILLET
 SPECIMEN TYPE: CCP
 ORIENTATION: S-L
 FREQUENCY:
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: BW004

STAIN.
STEEL

15-5PH

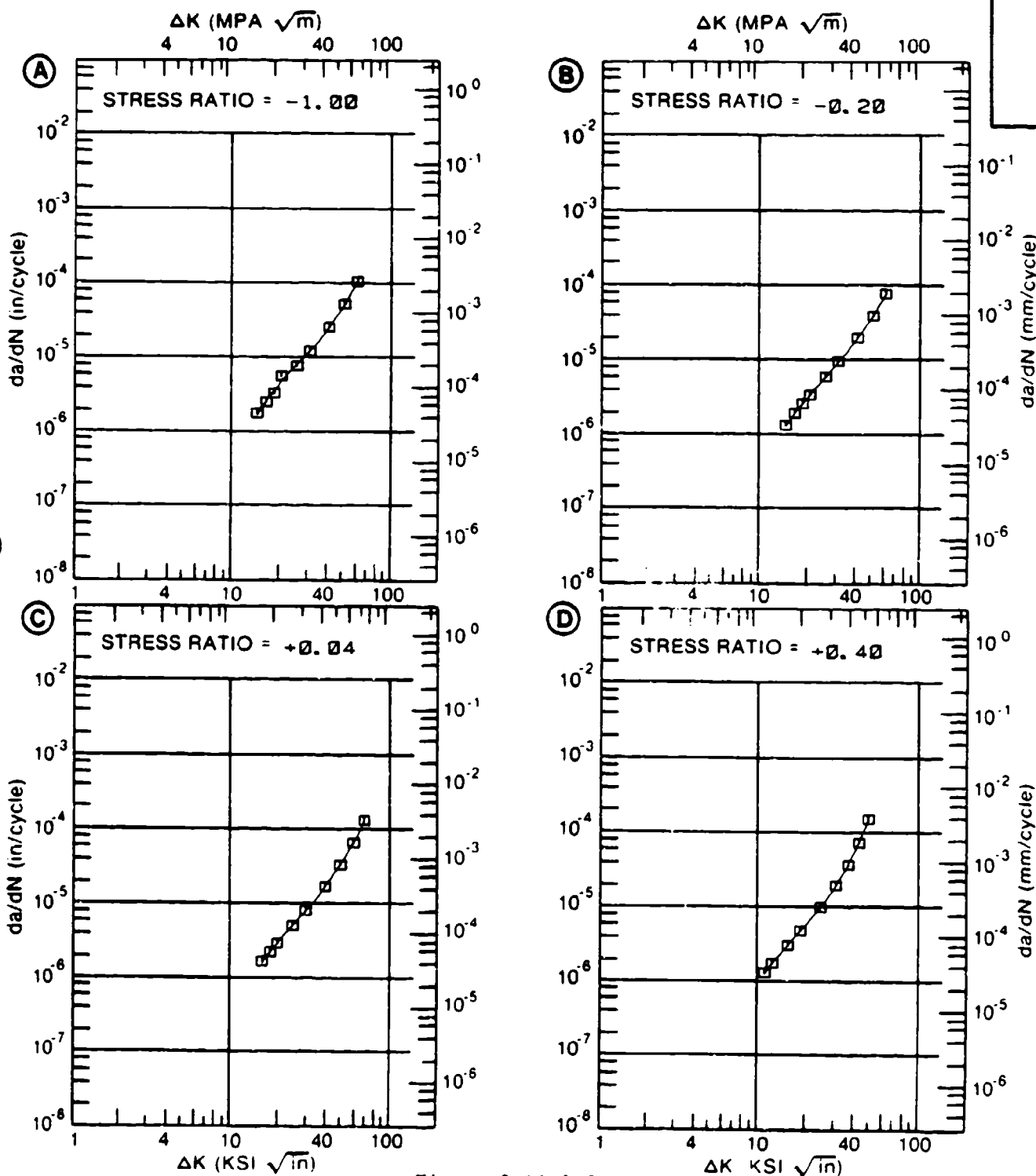


Figure 3.11.3.5

Table 3.11.3.6

| CONDITION | --PRODUCT-- | | TEST SPEC | YIELD STR | ENVIRONMENT | STAINLESS STEEL 13-3PH | | K (ISCC) | SPECIMEN | | CRACK LENGTH (IN) | K (ISCC) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|-----------|-------------|------------|-----------|-----------|---------------------|------------------------|------------|----------|------------|-------------|-------------------|----------|------|----------|-----------------|------------|
| | FORM | THICK (IN) | | | | THICK (IN) | WIDTH (IN) | | THICK (IN) | DESIGN (IN) | | | | | | |
| H 900 | B | 2.25 | R.T. | T-L | INDUSTRIAL ATH | 2.000 | 1.000 | CT | 71.80 | 68.00 | --- | --- | --- | --- | 1973 866688 | |
| H 900 | B | 2.25 | R.T. | T-L | SEACDAST ATH | 2.000 | 1.000 | CT | 71.80 | 36.00 | --- | --- | --- | --- | 1973 866688 | |
| H 900 | B | 2.25 | R.T. | T-L | 171.2 20 PCT NAACL | 2.000 | 1.000 | CT | 71.80 | 33.00 | --- | --- | --- | --- | 1973 866688 | |
| H1150M | B | 2.25 | R.T. | T-L | 93.1 INDUSTRIAL ATH | 2.000 | 1.000 | CT | 75.70 | 72.00* | --- | --- | --- | --- | 1973 866688 | |
| H1150M | B | 2.25 | R.T. | T-L | 93.1 SEACDAST ATH | 2.000 | 1.000 | CT | 75.70 | 72.00* | --- | --- | --- | --- | 1973 866688 | |
| H1150M | B | 2.25 | R.T. | T-L | 93.1 20 PCT NAACL | 2.000 | 1.000 | CT | 75.70 | 72.00* | --- | --- | --- | --- | 1973 866688 | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISCC/TYS)SQUARED

Table 3.12.3.1

| CONDITION | -- PRODUCT FORM THICK (IN) | TEST SPEC TEMP (F) | DR STR (KSI) | ENVIRONMENT | STAINLESS STEEL 15-5PH(AH) | K (ISCC) | SPECIMEN | | CRACK LENGTH (IN) | K (ISCC) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|-----------|----------------------------|--------------------|--------------|---------------------|----------------------------|----------|------------|------------|-------------------|----------|------|----------|-----------------|------------|
| | | | | | | | WIDTH (IN) | THICK (IN) | | | | | | |
| H 900 | F | 3 00 | R T | 175 0 3 5 PCT NAACL | 1 500 | 0 480 | CANT | 96 80 | 80 00* | | | > 60000 | 1971 84333 | |
| H1000 | F | 3 00 | R T | 157 9 3 5 PCT NAACL | 1 500 | 0 480 | CANT | 114 00 | 114 00* | | | > 60000 | 1971 84333 | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.3(KISCC/TYS)SQUARED

Table 3.13.3.1

| CONDITION | FORM | THICK (IN) | TEST TEMP (F) | OR STR (KSI) | SPEC YIELD ENVIRONMENT | STAINLESS STEEL 15-SPH(VH) | | K (ISCC) | | CRACK LENGTH (IN) | K (G) (KSI*SQRT IN) | Y (ISCC) | MEAN DEV | TEST TIME (MIN) | DATE REFER |
|-----------|------|------------|---------------|--------------|------------------------|----------------------------|------------|-------------|-------------|-------------------|---------------------|----------|----------|-----------------|------------|
| | | | | | | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | | | | | | |
| H 900 | F | 4.50 | R T | --- | 174.9 3.5 PCT NAACL | 1.500 | 0.480 | CANT | --- | 74.50 | 55 | 80 | | > 48000 | 1971 84333 |
| H1000 | F | 4.50 | R T | --- | 137.6 3.5 PCT NAACL | 1.500 | 0.480 | CANT | --- | 120.00 | 120 | 00* | | > 60000 | 1971 84333 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISCC/TYS)SQUARED

Table 3.14.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL 17-APH

TEST CONDITIONS

SPECIMEN ORIENTATION T :

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | |
|--------------|--------------|--------------|------------|-------------------------------|---|------|------|----|----|-----|
| | | | | | 2 | 5 | 10 | 20 | 50 | 100 |
| H1025 | ROUND BAR | 0.10 | 30.00 | | | 0.06 | 2.00 | | | |
| H1025 | ROUND BAR | 0.50 | 10.00 | | | | 5.77 | | | |
| H1025 | ROUND BAR | 0.50 | 30.00 | | | 0.03 | 0.51 | | | |

Table 3.14.2.1

| STAINLESS SIFFL 17-4PH K(IIC) | | | | | | | | | | | | | |
|-------------------------------|-----------------|---------------|------------------|--------------------|----------------------------|---------------|---------------|--------|-------------------------|----------------------|--|------|------------|
| CONDITION | PRODUCT FORM | THICK (IN) | TEST TEMP (F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | K(IIC)/IYS** (IN) | K(IIC) MEAN (K(IIC) STAN DEV IN) | DATE | REFER |
| | | | | | | W | B | | A | | | | |
| M 975 | RR | 3.25 | R.T. | L-R | 168.0 | 2.000 | 1.000 | NB | 1.000 | 0.63 | 94.60 | ---- | 84212 |
| HIC25 | BR | 3.00 | R.T. | 1-1 | 175.3 | 1.990 | 0.503 | CT | 0.937 | 0.45 | 74.50 | | 1979 DA001 |

TABLE 3.14.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.14.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 17-4PH
CONDITION: H900
ENVIRONMENT: R.T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.08 | | | |
| DELTA K MIN | A: 7.54 | .126 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | .150 | | | |
| | 9.00 | .217 | | | |
| | 10.00 | .305 | | | |
| | 13.00 | .745 | | | |
| | 16.00 | 1.54 | | | |
| | 20.00 | 3.38 | | | |
| 25.00 | 7.25 | | | | |
| 30.00 | 13.1 | | | | |
| 35.00 | 20.9 | | | | |
| 40.00 | 30.5 | | | | |
| 50.00 | 53.1 | | | | |
| DELTA K MAX | A: 56.40 | 68.4 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 22.74
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H900
 FORM: 0.56" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 20.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 170.5 KSI
 ULT. STRENGTH: 192.7 KSI
 SPECIMEN THK: 0.500"
 SPECIMEN WIDTH: 1.969"
 REFERENCES: DA001

STAIN.
 STEEL
 17-4PH

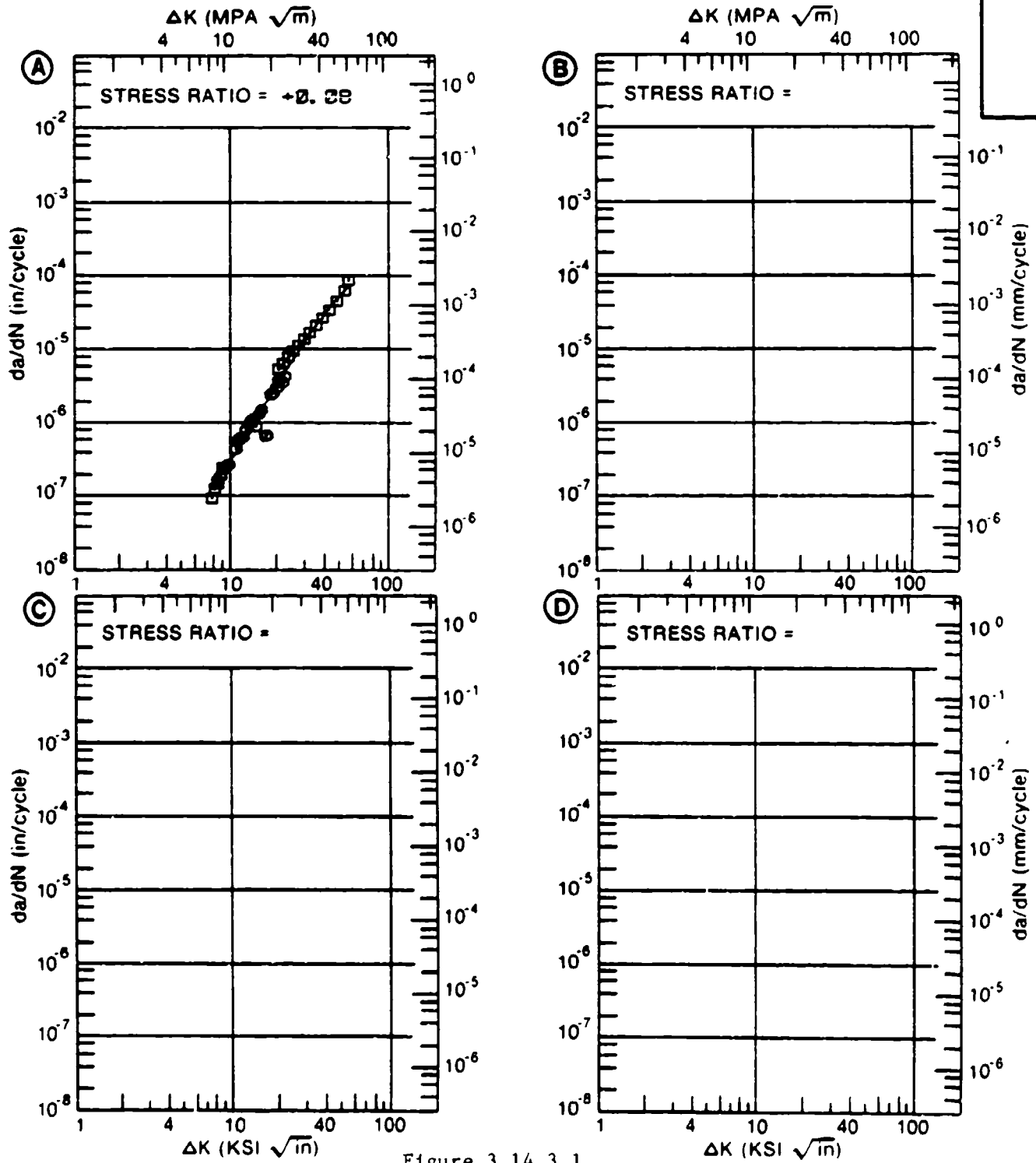


Figure 3.14.3.1

TABLE 3.14.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.14.3.2 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 17-4PH
CONDITION: H1025

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. H. H. A. | | | |
| DELTA K MIN | A: 8.33 | .214 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .245 | | | |
| | 10.00 | .330 | | | |
| | 13.00 | .945 | | | |
| | 16.00 | 2.15 | | | |
| | 20.00 | 3.51 | | | |
| DELTA K MAX | A: 20.04 | 3.51 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 17.98
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: H1025
 FORM: Ø. 13" TH CASTING
 SPECIMEN TYPE: CCP
 ORIENTATION:
 STRESS RATIO: +0.02
 FREQUENCY: 1.0 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: Ø. 103- Ø. 113"
 SPECIMEN WIDTH: 2.915- 2.955"
 REFERENCES: GD010

STAIN.
STEEL

17-4PH

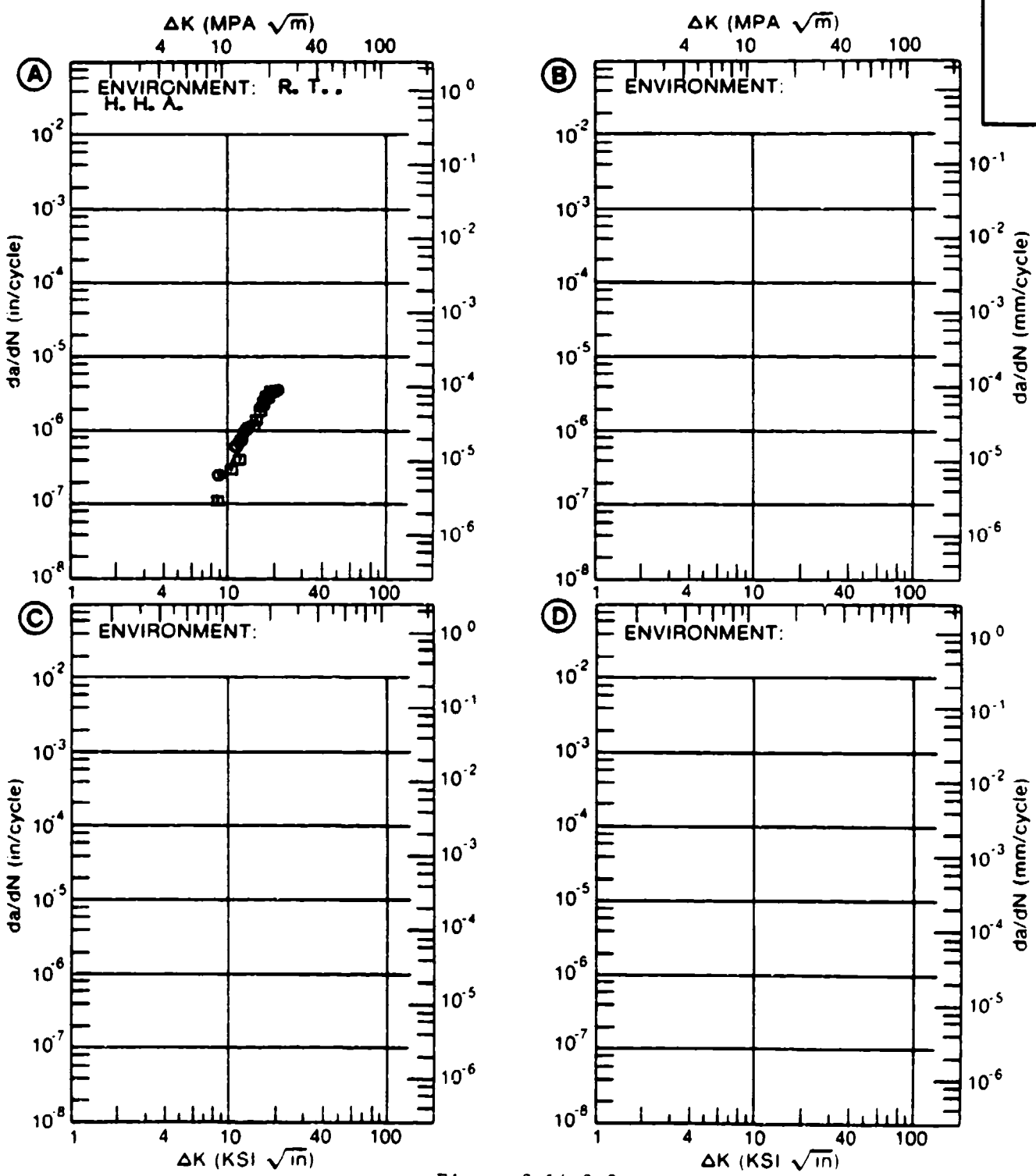


Figure 3.14.3.2

TABLE 3.14.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.14.3.3 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: STAINLESS STEEL 17-4PH | | | | | |
|----------------------------------|----------|---------------------------------------|---------|---|---|
| CONDITION: H1025 | | | | | |
| ENVIRONMENT: R.T., LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K | A: 20.54 | 1.48 | | | |
| MIN | B: 11.39 | | .708 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | | 1.33 | | |
| | 16.00 | | 2.76 | | |
| | 20.00 | | 5.77 | | |
| | 25.00 | 3.15 | 16.5 | | |
| | 30.00 | 5.61 | | | |
| | 35.00 | 9.33 | | | |
| | 40.00 | 15.9 | | | |
| DELTA K | A: 49.82 | 54.3 | | | |
| MAX | B: 28.37 | | 39.5 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 8.26 | 7.53 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.3 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1025
 FORM: 3.0" TH ROUND BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 10.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 175.3 KSI
 ULT. STRENGTH: 179.8 KSI
 SPECIMEN THK: 0.50"
 SPECIMEN WIDTH: 1.99- 2.00"
 REFERENCES: DA001

STAIN.
STEEL

17-4PH

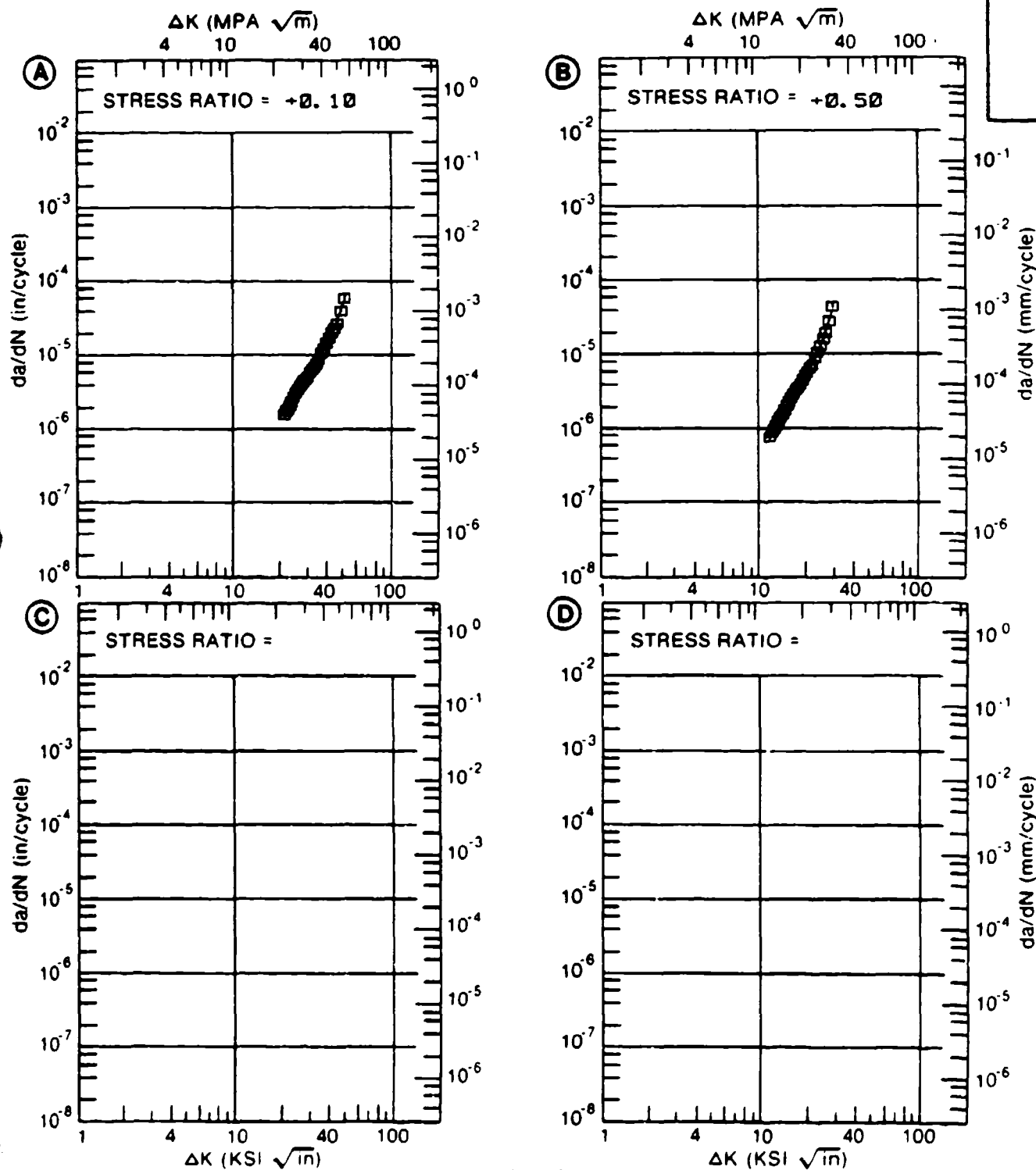


Figure 3.14.3.3

TABLE 3.14.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.14.3.4 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 17-4PH
CONDITION: H1025
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| A: | 7.48 | .0111 | | | |
| DELTA K B: | 4.00 | | .00984 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 5.00 | | .0357 | | |
| | 6.00 | | .0802 | | |
| | 7.00 | | .143 | | |
| | 8.00 | .0175 | .229 | | |
| | 9.00 | .0344 | .347 | | |
| | 10.00 | .0607 | .512 | | |
| | 13.00 | .288 | | | |
| | 16.00 | .899 | | | |
| | 20.00 | 2.00 | | | |
| | 25.00 | 3.66 | | | |
| | 30.00 | 7.22 | | | |
| | 35.00 | 13.7 | | | |
| A: | 38.39 | 19.6 | | | |
| DELTA K B: | 12.62 | | 1.41 | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 11.17 | 6.89 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: H1025
 FORM: 3.0" TH ROUND BAR
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 30.0 HZ
 ENVIRONMENT: R.T., LAB AIR

YIELD STRENGTH: 175.3 KSI
 ULT. STRENGTH: 179.8 KSI
 SPECIMEN THK: 0.25"
 SPECIMEN WIDTH: 1.99- 2.00"
 REFERENCES: DA001

STAIN.
STEEL

17-4PH

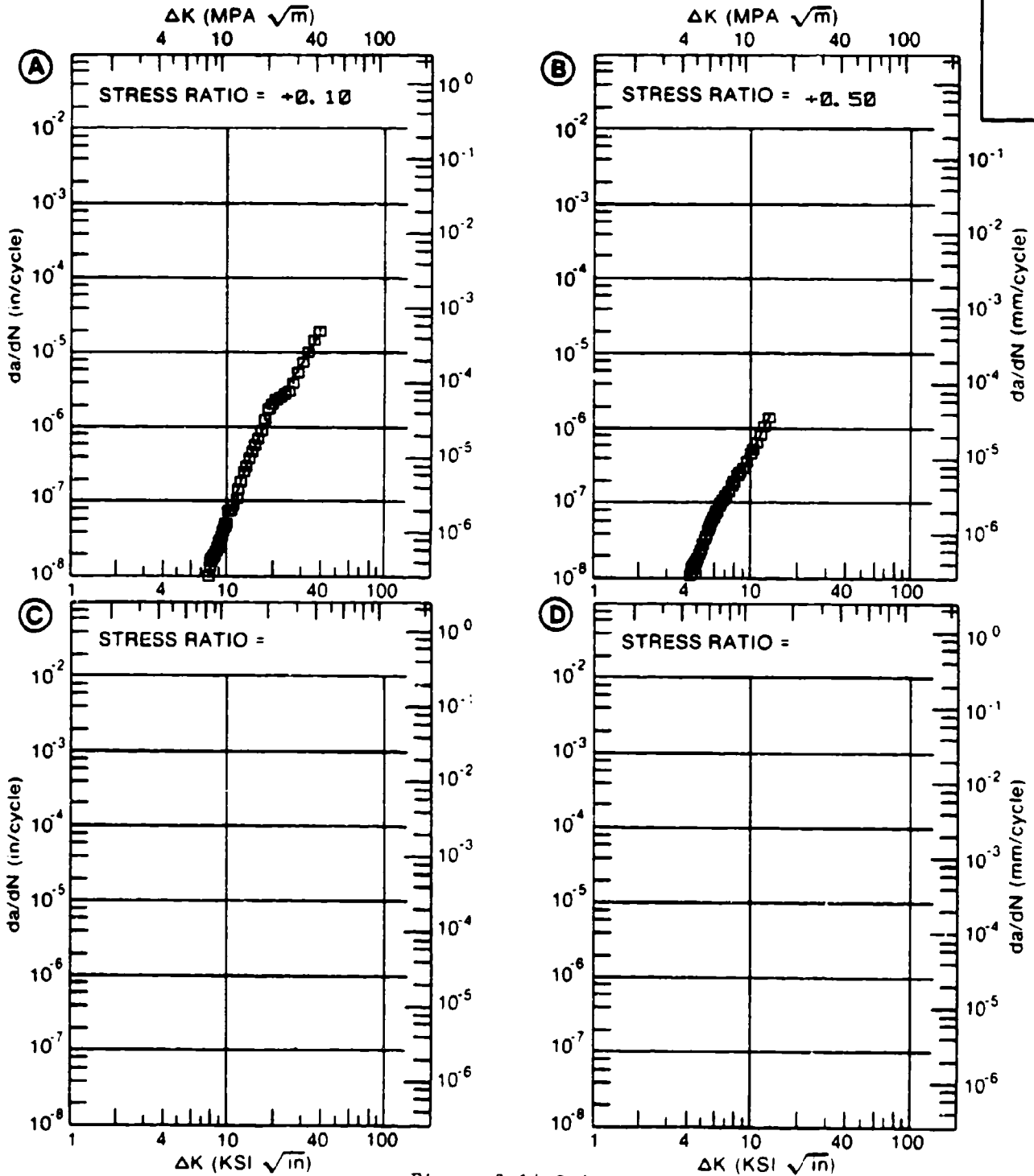


Figure 3.14.3.4

Table 3.14.3.5

| CONDITION | STAINLESS STEEL 17-4PH | | | | | | | | | | K (ISCC) | CRACK LENGTH K(O) (ISCC) | MEAN DEV | TEST TIME (MIN) | DATE REFER | | | | | | | | | |
|-----------|------------------------|------|-------|-----|-------------|-----|----------|-----|--------------|-----|----------|--------------------------|----------|-----------------|------------|------|-----|----|-----|-----|---|-------|------|-------|
| | FORM | | THICK | | ENVIRONMENT | | SPECIMEN | | THICK DESIGN | | | | | | | STAN | | | | | | | | |
| | (IN) | (T) | (IN) | (T) | (IN) | (T) | (IN) | (T) | (IN) | (T) | | | | | | | DEV | | | | | | | |
| H 500 | D | 1.75 | R.T. | --- | --- | 176 | 5 | 3 | 5 | PCT | NACL | 1.500 | 0 | 480 | CANT | --- | 51 | 50 | 51 | 50 | > | 60000 | 1971 | 84333 |
| H1000 | B | 1.75 | R.T. | --- | --- | 157 | 9 | 3 | 5 | PCT | NACL | 1.500 | 0 | 480 | CANT | --- | 119 | 00 | 119 | 00* | > | 60000 | 1971 | 84333 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KISCC/TYS) SQUARED

Table 3.15.2.1

| CONDITION | STAINLESS STEEL 17-7PH | | | | | | | | | | K(1C) | CRACK LENGTH (IN) | 2.9* K(1C)/TYS)**2 (IN) | K(1C) MEAN (KSI*SQRT IN) | K(1C) STAN DEV | DATE | REFER |
|-----------|------------------------|---------------|------------------|--------------------|----------------------------|---------------|---------------|--------|-------|------|-------|-------------------------|-------------------------------|-----------------------------|-------------------|------|-------|
| | ---PRODUCT--- FORM | THICK (IN) | TEST TEMP (F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | M | B | | | | | | | |
| RH1050 | RB | 1.25 | R.T. | T-L | 190.0 | 2.000 | 1.000 | CT | 1.066 | 0.15 | 46.30 | 1973 | 86688 | | | | |
| | | 1.25 | | | 190.0 | 2.000 | 1.000 | CT | 1.025 | 0.15 | 47.70 | 1973 | 86688 | | | | |
| | | 1.25 | | | 190.0 | 2.000 | 1.000 | CT | 1.026 | 0.15 | 47.10 | 1973 | 86688 | | | | |

TABLE 3.15.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.15.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 17-7PH
CONDITION: TH1050
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----|---------------------------|--------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: | 2.85 | .00325 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 3.00 | .00435 | | |
| | | 3.50 | .00947 | | |
| | | 4.00 | .0156 | | |
| | | 5.00 | .0252 | | |
| | | 6.00 | .0425 | | |
| | | 7.00 | .0857 | | |
| DELTA K MAX | | 8.00 | .162 | | |
| | | 9.00 | .276 | | |
| | | 10.00 | .433 | | |
| | | 13.00 | 1.19 | | |
| | | 16.00 | 2.38 | | |
| | A: | 18.70 | 3.75 | | |

ROOT MEAN SQUARE 11.25
PERCENT ERROR

LIFE 0.0-0.3
PREDICTION 0.5-0.8 1
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: TH1050
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 20.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 194.0 KSI
 ULT STRENGTH: 208.1 KSI
 SPECIMEN THK: 0.500"
 SPECIMEN WIDTH: 1.000"
 REFERENCES: DA001

STAIN.
STEEL

17-7PH

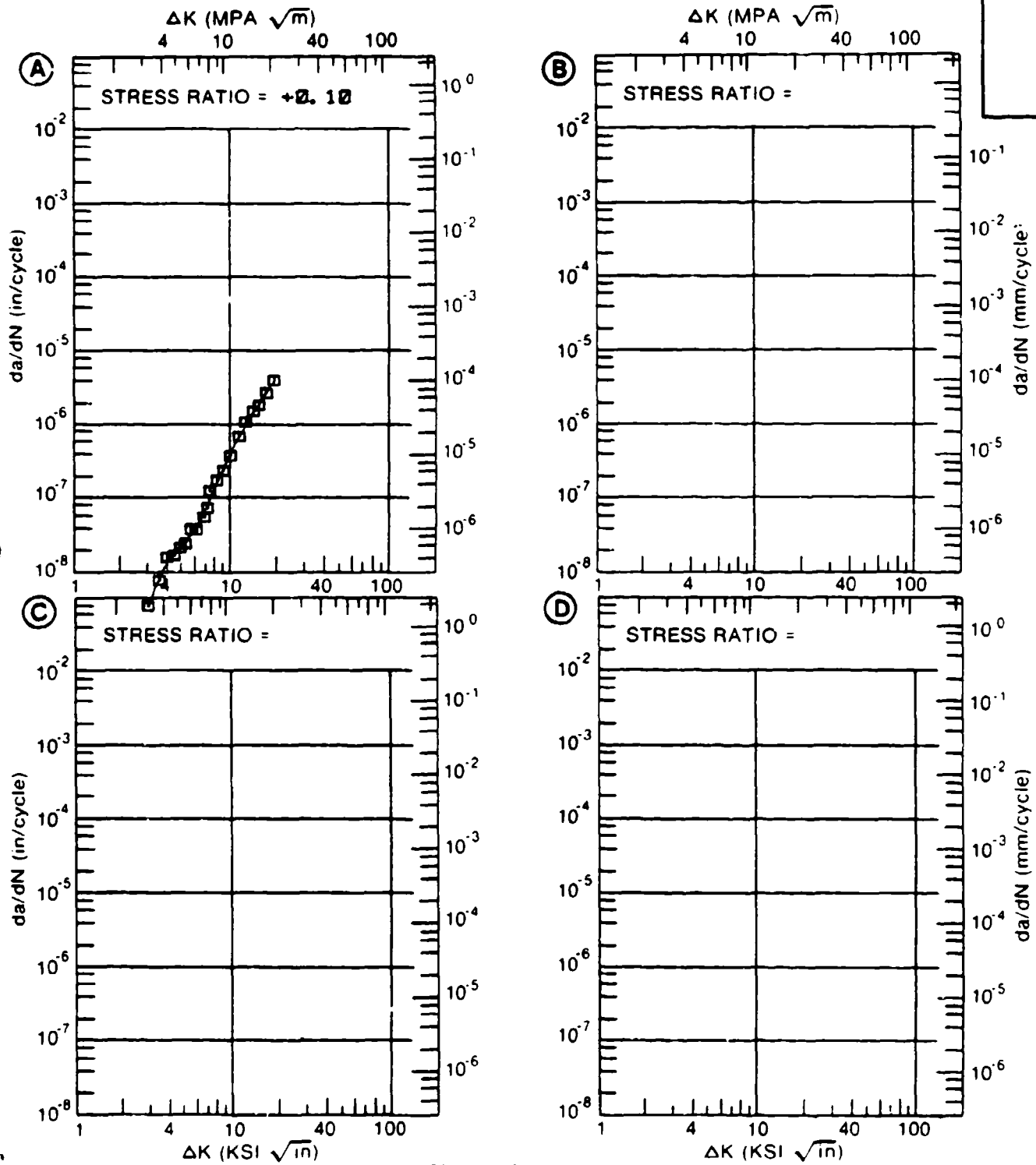


Figure 3.15.3.1

TABLE 3.15.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.15.3.2 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 17-7PH
CONDITION: TH1050
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 3.82 | .00558 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 4.00 | .00944 | | | |
| | 5.00 | .0264 | | | |
| | 6.00 | .0447 | | | |
| | 7.00 | .0841 | | | |
| | 8.00 | .153 | | | |
| | 9.00 | .253 | | | |
| | 10.00 | .388 | | | |
| | 13.00 | 1.03 | | | |
| | 16.00 | 2.12 | | | |
| | 20.00 | 4.44 | | | |
| | 25.00 | 9.34 | | | |
| | 30.00 | 17.5 | | | |
| | 35.00 | 30.7 | | | |
| | 40.00 | 51.4 | | | |
| DELTA K | A: 49.65 | 205. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 11.14
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8 1
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) 2.0

CONDITION/HT: TH1050
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 20.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 180.3 KSI
 ULT. STRENGTH: 203.3 KSI
 SPECIMEN THK: 0.500"
 SPECIMEN WIDTH: 1.989"
 REFERENCES: DA001

STAIN.
STEEL

17-7PH

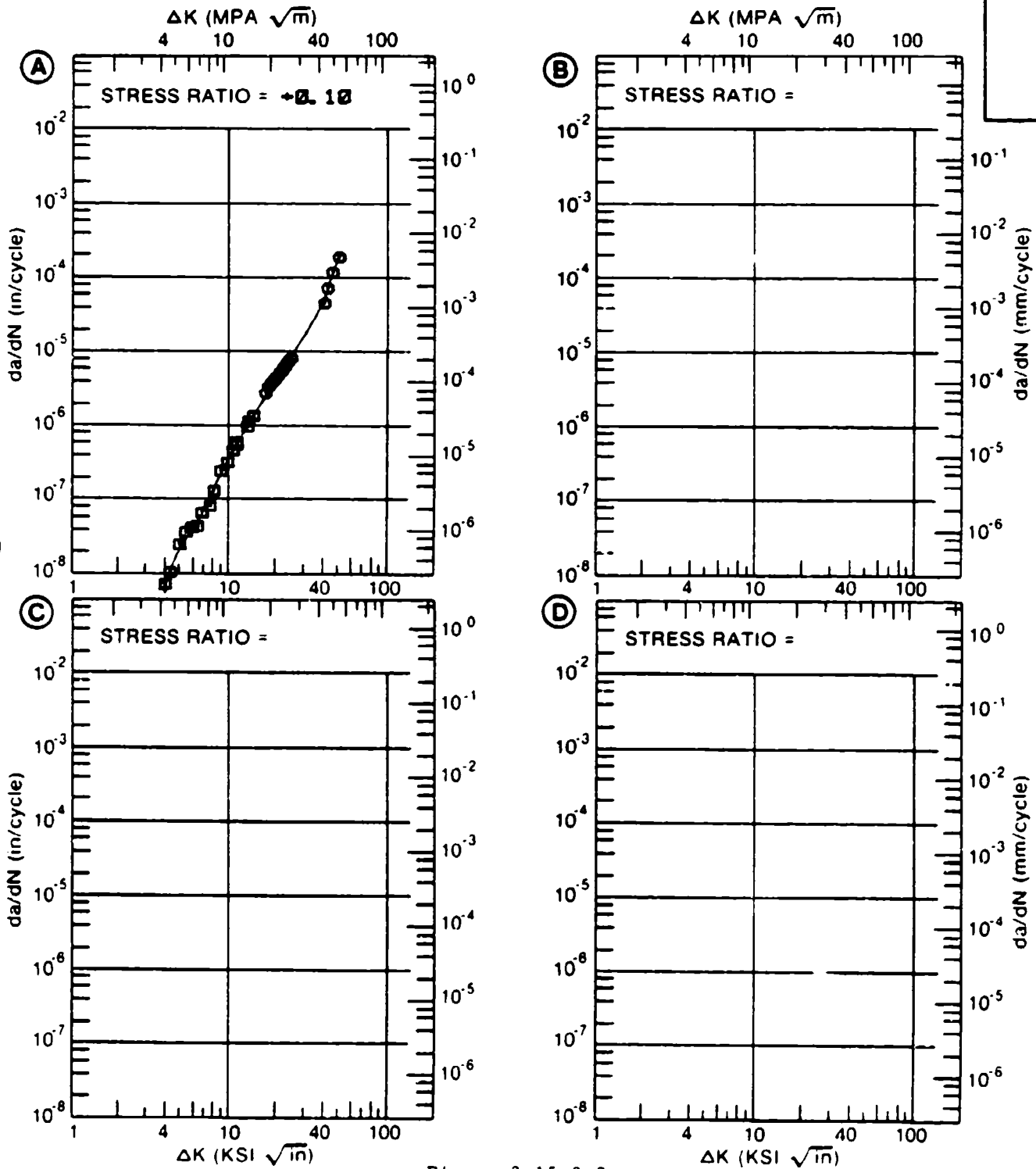


Figure 3.15.3.2

Table 3.16.1.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
STAINLESS STEEL 304

TEST CONDITIONS

SPECIMEN ORIENTATION Unknown

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|----------------|--------------|--------------|------------|-------------------------------|---|
| | | | | | 2.5 5 10 20 50 100 |
| ANNEALED | SHEET | 0.09 | 10.00 | | 0.16 3.07 |
| ANNEALED | SHEET | 0.09 | 19.00 | | 0.13 2.83 |
| ANNEALED | SHEET | 0.10 | 1.67 | | 2.86 |
| ANNEALED | SHEET | 0.10 | 6.00 | | 2.56 |
| ANNEALED & AGE | PLATE | 0.09 | 3.00 | | 1.38 |

Table 3.16.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

STAINLESS STEEL 304

TEST CONDITIONS

SPECIMEN ORIENTATION: L-T

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K (LEVELS (KSI SQRT(IN))) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|---------------------------------|-----|---|----|----|------|------|---|
| ANNEALED | PLATE | 0.00 | 0.03 | | | | | | | | 36.0 |
| ANNEALED | PLATE | 0.00 | 6.67 | | | | | | 1.92 | 28.5 | |

TABLE 3.16.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.1 INDICATING EFFECT

OF FREQUENCY

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|-------------|------|---|
| | | A | B | C | D |
| | | F(HZ)= 10.0 | F(HZ)= 15.0 | | |
| DELTA K MIN | A: 9.98 | .160 | | | |
| | B: 9.16 | | .112 | | |
| | C: | | | | |
| | D: | | | | |
| | | 10.00 | .163 | .133 | |
| | 13.00 | .438 | .360 | | |
| | 16.00 | 1.37 | 1.01 | | |
| | 20.00 | 3.07 | 2.83 | | |
| DELTA K MAX | A: 23.49 | 6.30 | | | |
| | B: 21.04 | | 3.45 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 15.06 | 26.43 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.23 | 3 | 3 | | |
| SUMMARY | 1.25-2.0 | | 1 | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION:
 STRESS RATIO: +0.05
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.010"
 SPECIMEN WIDTH: 0.995- 1.000"
 REFERENCES: HD000

STAIN.
STEEL

304

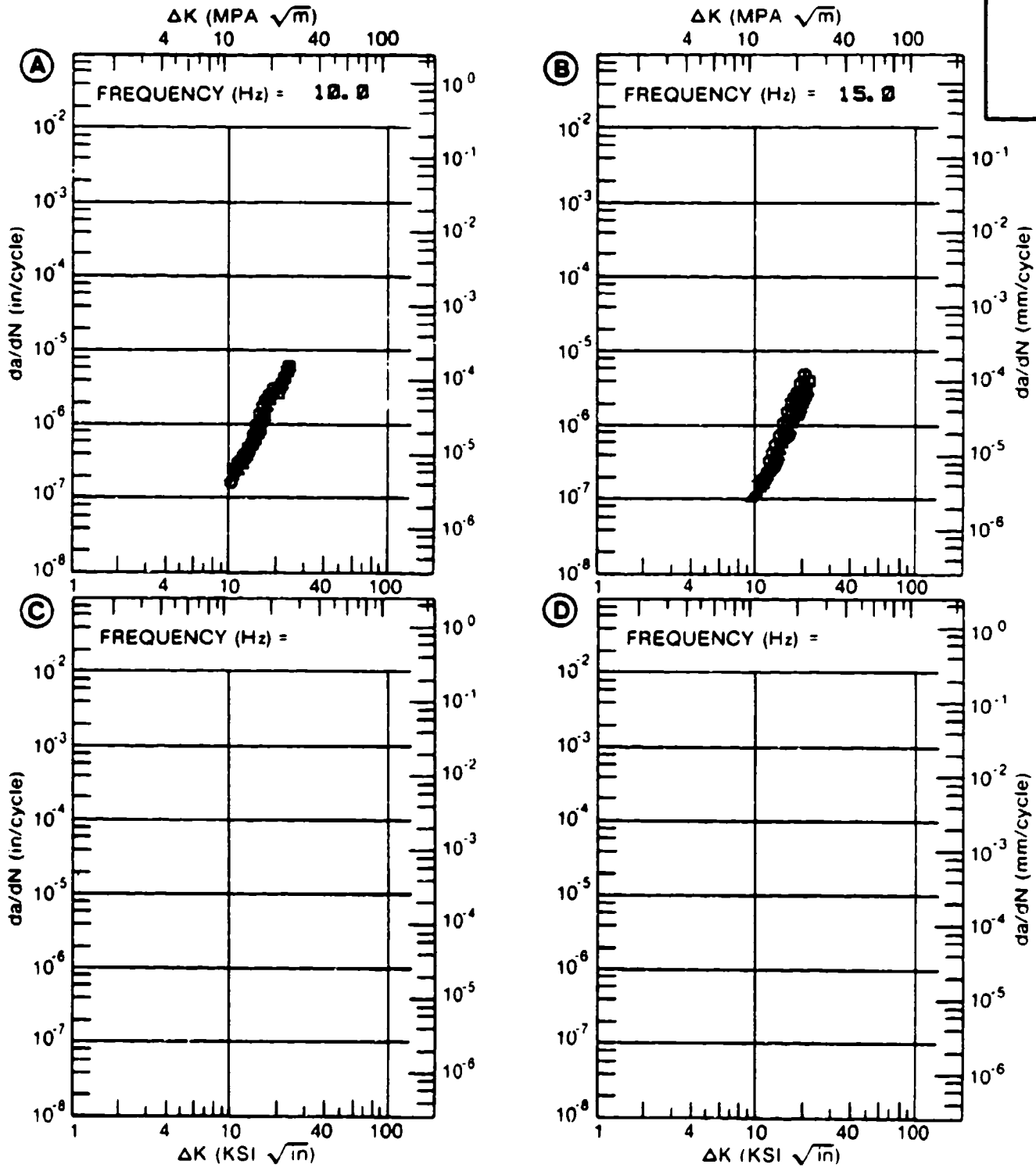


Figure 3.16.3.1

TABLE 3.16.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.2 INDICATING EFFECT

OF FREQUENCY

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|---------------------------------------|------|-------------|------|
| | A | B | C | D |
| | F(HZ)= 1.67 | | F(HZ)= 6.00 | |
| DELTA K MIN | A: 14.71 | .772 | B: 10.85 | .128 |
| | C: 13.00 | | D: 16.00 | .312 |
| | | 1.19 | | .657 |
| | | 2.86 | | 2.56 |
| | | 4.61 | | |
| | | 10.6 | | |
| DELTA K MAX | A: 32.52 | 20.3 | B: 21.51 | 4.77 |
| | C: | | D: | |
| ROOT MEAN SQUARE PERCENT ERROR | 23.51 | 8.28 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | 2 | 0.5-0.8 | 2 |
| | 0.8-1.25 | 2 | 1.25-2.0 | 1 |
| | >2.0 | | | |

CONDITION/HT: ANNEALED
 FORM: SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION:
 STRESS RATIO: +0.10
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.010"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: HD000

STAIN.
 STEEL

304

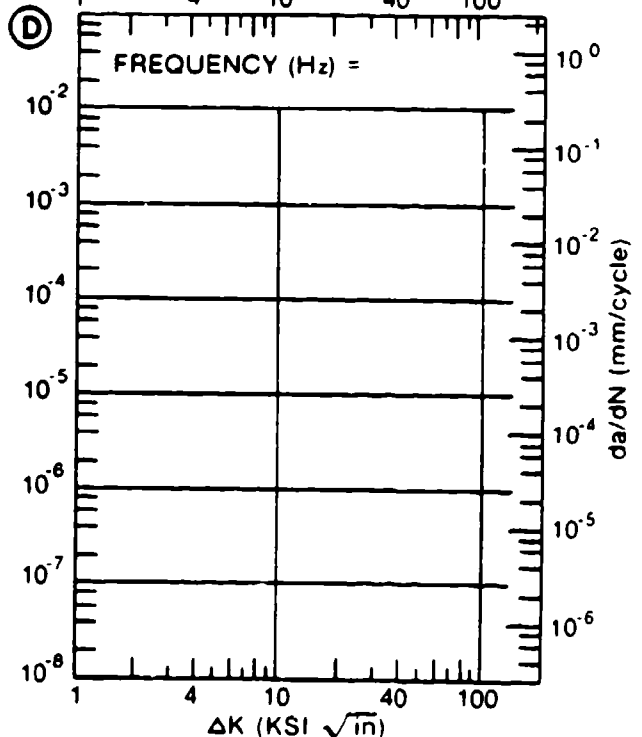
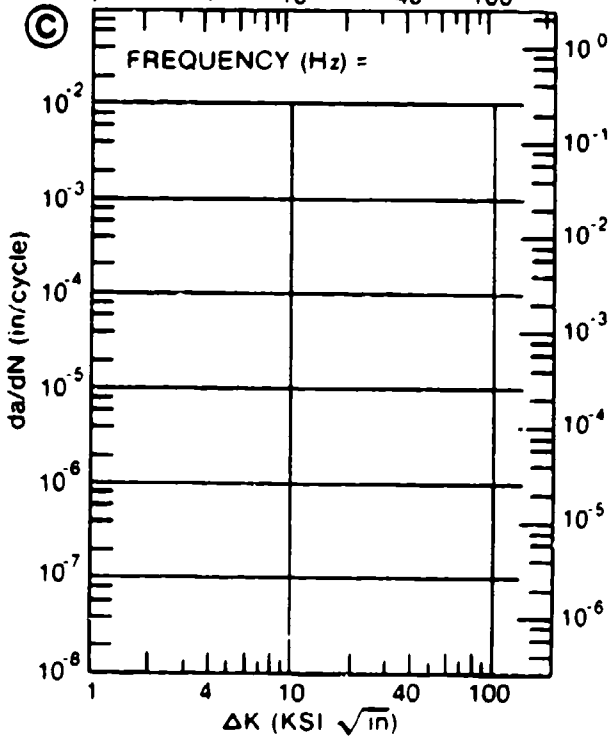
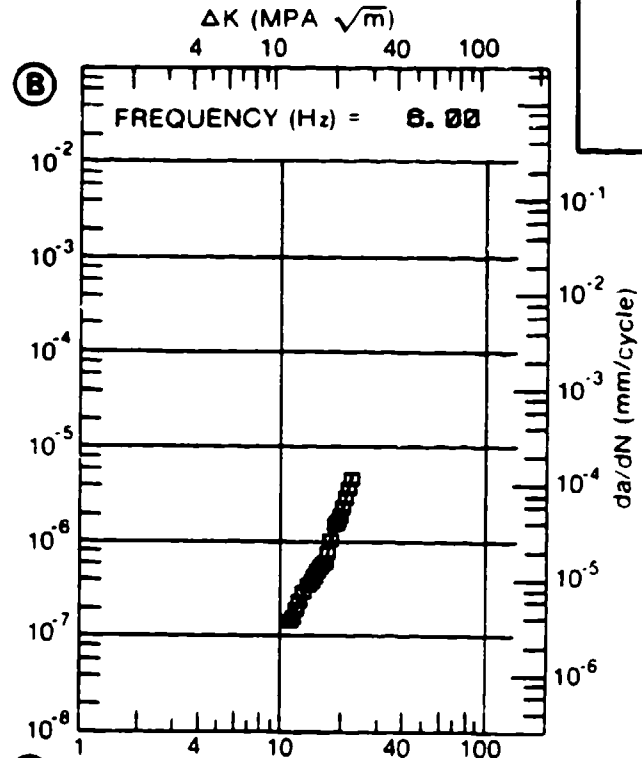
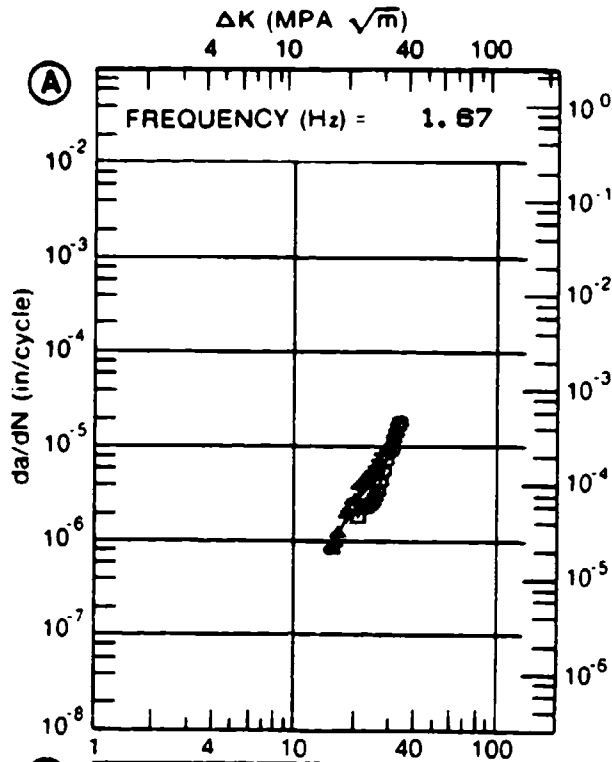


Figure 3.16.3.2

TABLE 3.16.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.3 INDICATING EFFECT
OF FREQUENCY

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|------|-------------|---|
| | | A | B | C | D |
| | | F(HZ)= 0.03 | | F(HZ)= 6.67 | |
| DELTA K | A: 32.53 | 11.1 | | | |
| MIN | B: 16.50 | | 854 | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | | 1.92 | | |
| | 25.00 | | 3.05 | | |
| | 30.00 | | 4.50 | | |
| | 35.00 | 14.7 | 8.12 | | |
| | 40.00 | 24.7 | 15.3 | | |
| | 50.00 | 56.0 | 28.5 | | |
| | 60.00 | 101. | 45.7 | | |
| | 70.00 | 154. | | | |
| | 80.00 | 205. | | | |
| DELTA K | A: 82.69 | 217. | | | |
| MAX | B: 69.22 | | 78.3 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 5.23 | 5.67 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: SENT
 ORIENTATION: L-T
 STRESS RATIO: +0.00
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 39.6 KSI
 ULT. STRENGTH: 77.1 KSI
 SPECIMEN THK: 0.491"
 SPECIMEN WIDTH: 4.910- 4.950"
 REFERENCES: HD007

| |
|-----------------|
| STAIN. STEEL |
| 304 |
| |

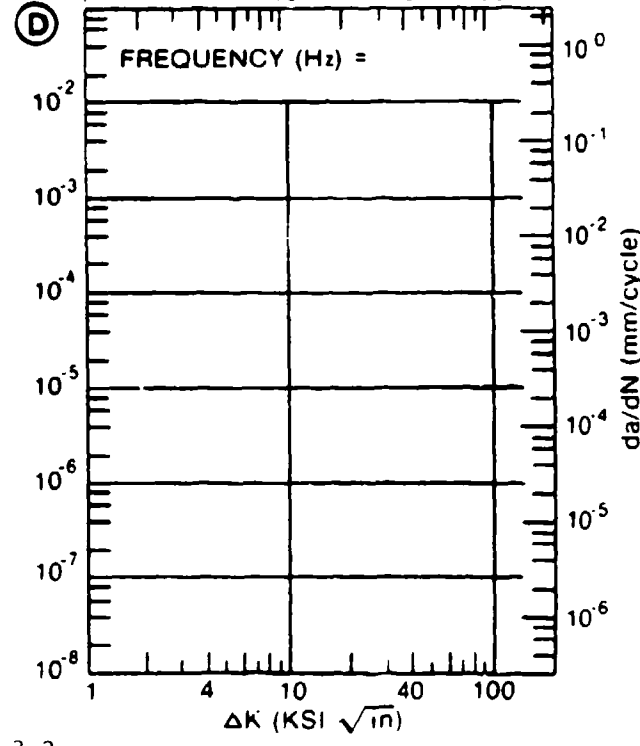
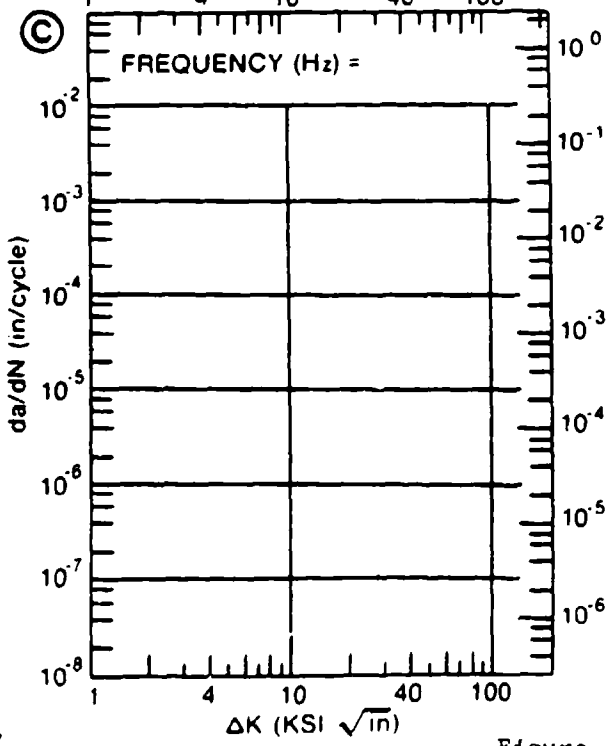
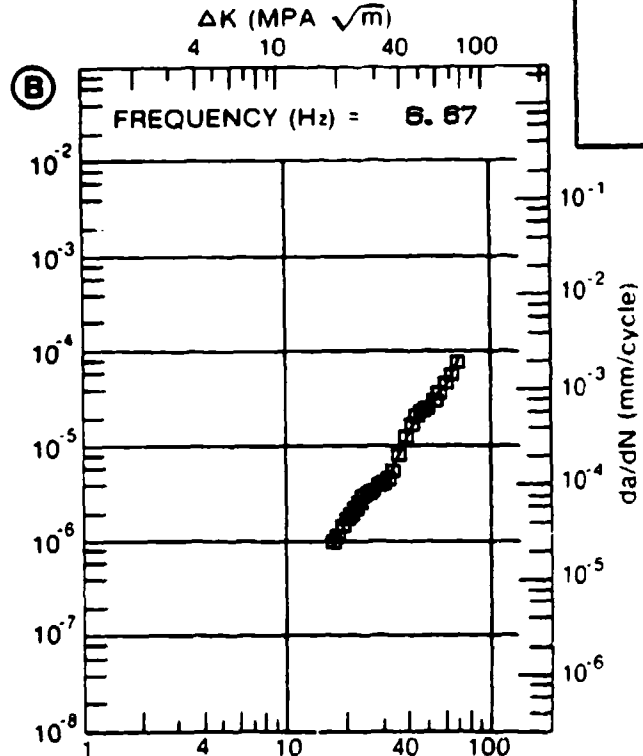
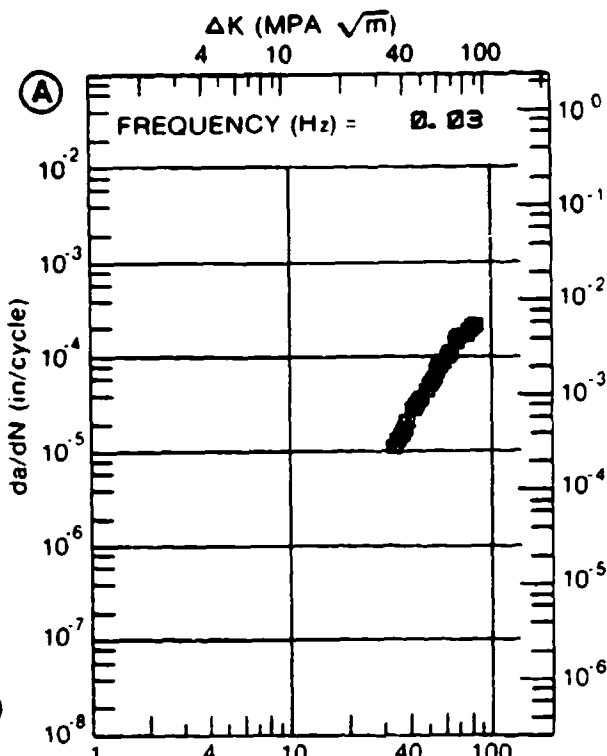


Figure 3.16.3.3

TABLE 3.16.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.4 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED
ENVIRONMENT: R.T., LAB AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|--------------------------|---|---|---|
| | A | B | C | D |
| | R=+0.05 | | | |
| DELTA K A: | | | | |
| MIN B: | | | | |
| C: | | | | |
| D: | | | | |
| 200.00 | | | | |
| DELTA K A: | | | | |
| MAX B: | | | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 0.00
PERCENT ERROR

| | |
|------------|----------|
| LIFE | 0.0-0.5 |
| PREDICTION | 0.5-0.8 |
| RATIO | 0.8-1.25 |
| SUMMARY | 1.25-2.0 |
| (NP/NA) | >2.0 |

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: VOL
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 39.6 KSI
 ULT. STRENGTH: 77.1 KSI
 SPECIMEN THK: 0.494"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: HD007

STAIN.
 STEEL

304

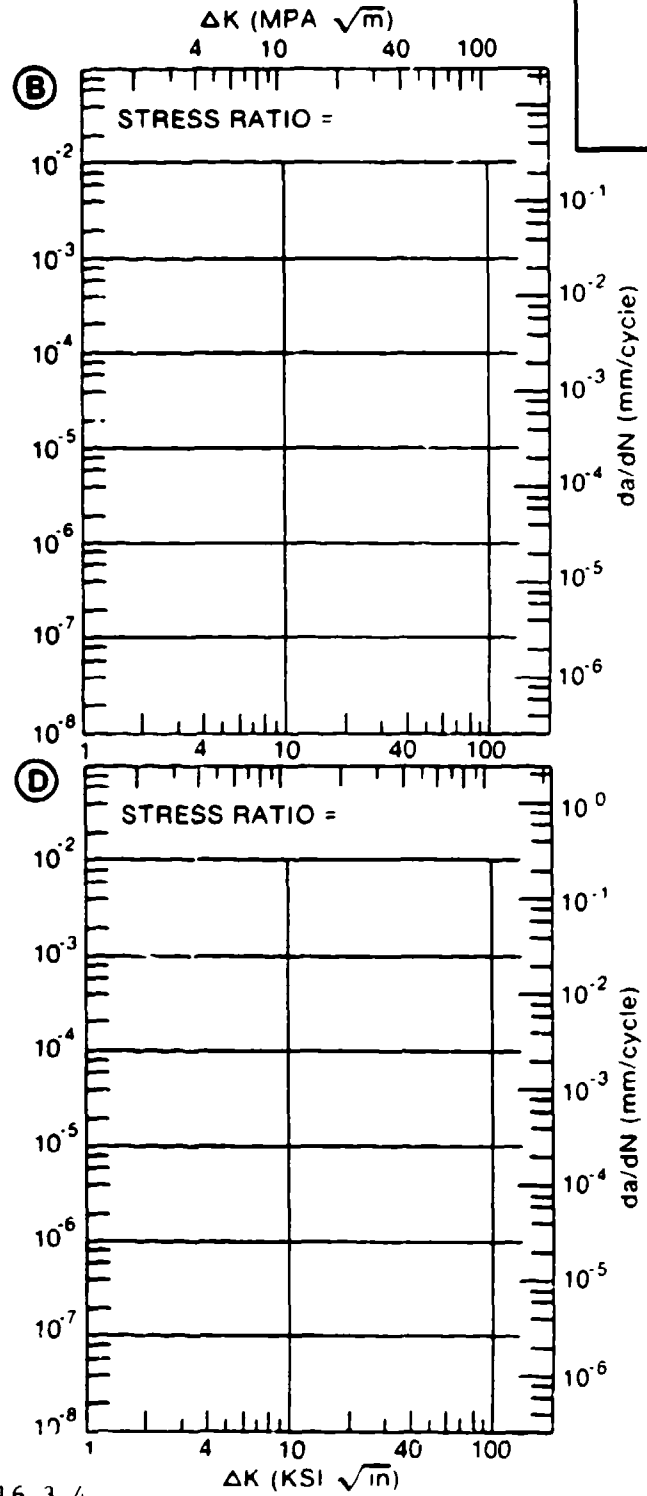
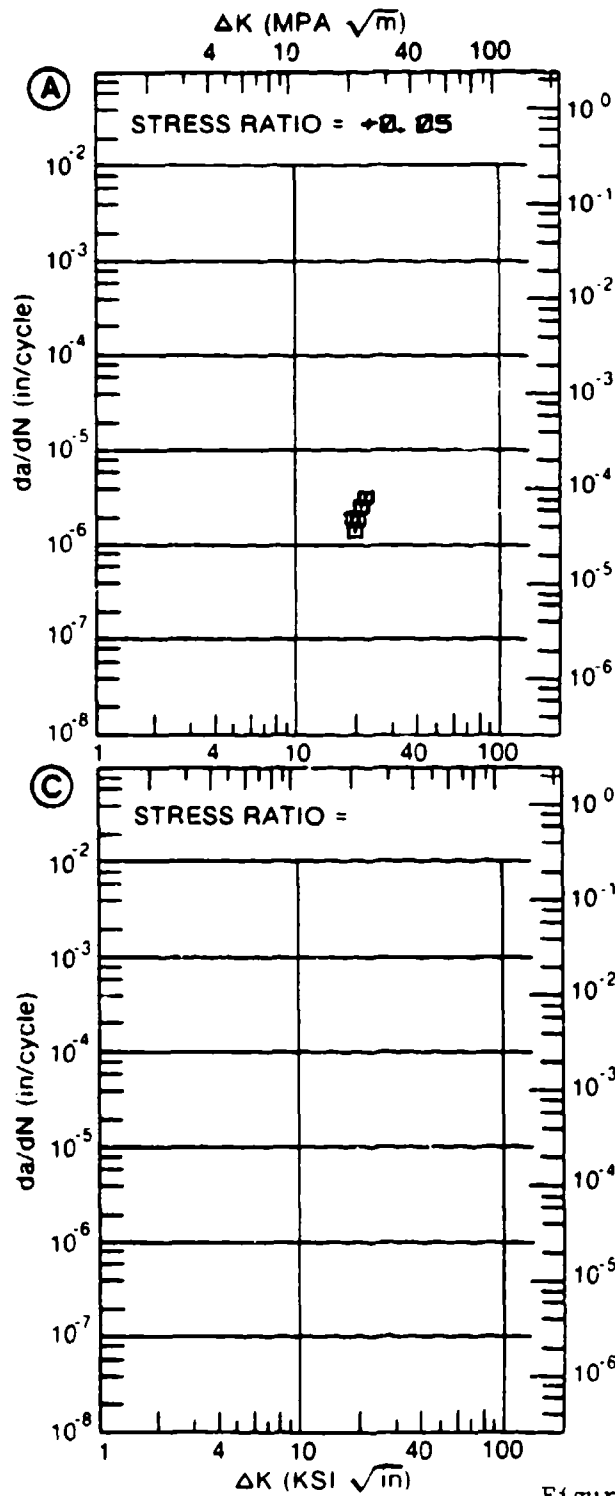


Figure 3.16.3.4

TABLE 3.16.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.5 INDICATING EFFECT
OF FREQUENCY

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED
ENVIRONMENT: R.T., LAB AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|--|---------|-------------|---|
| | A | B | C | D |
| | F(HZ)= 3.00 | | F(HZ)= 6.67 | |
| DELTA K MIN | A: | B: 1.09 | | |
| | C: | | | |
| | D: | | | |
| | 20.00 | 1.86 | | |
| | 25.00 | 3.44 | | |
| | 30.00 | 5.93 | | |
| | 35.00 | 9.64 | | |
| | 40.00 | 15.0 | | |
| | 50.00 | 32.5 | | |
| | 60.00 | 63.2 | | |
| DELTA K MAX | A: | B: 101. | | |
| | C: | | | |
| | D: | | | |
| ROOT MEAN SQUARE | 0.00 | 5.89 | | |
| PERCENT ERROR | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | | |

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: SENT
 ORIENTATION: T-L
 STRESS RATIO: +0.00
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 39.8 KSI
 ULT. STRENGTH: 77.1 KSI
 SPECIMEN THK: 0.493- 0.498"
 SPECIMEN WIDTH: 4.910- 4.915"
 REFERENCES: HD007

| |
|-----------------|
| STAIN. STEEL |
| 304 |

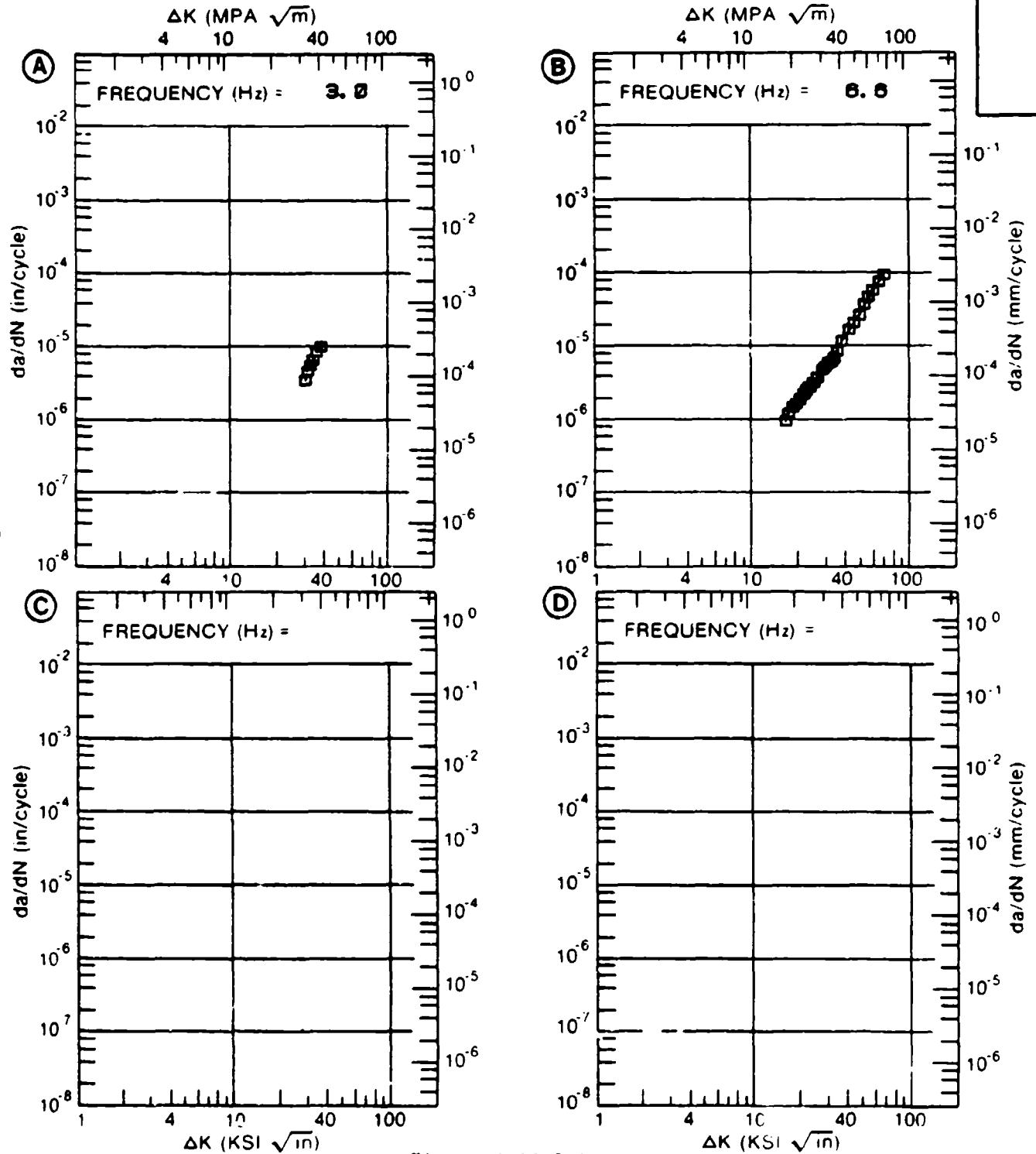


Figure 3.16.3.5

TABLE 3.16.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.6 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E=+ 800 F | | | |
| | | AIR | | | |
| DELTA K MIN | A: 12.99 | 1.46 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.46 | | | |
| | 16.00 | 2.90 | | | |
| | 20.00 | 5.70 | | | |
| | 25.00 | 10.3 | | | |
| | 30.00 | 21.0 | | | |
| DELTA K MAX | A: 34.83 | 47.9 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 15.35
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 4
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION:
 STRESS RATIO: +0.05
 FREQUENCY: 0.8 HZ

YIELD STRENGTH: 39.6 KSI
 ULT. STRENGTH: 77.5 KSI
 SPECIMEN THK: 0.300- 0.500"
 SPECIMEN WIDTH: 1.157- 2.998"
 REFERENCES: HD011, HD012

STAIN.
 STEEL
 304

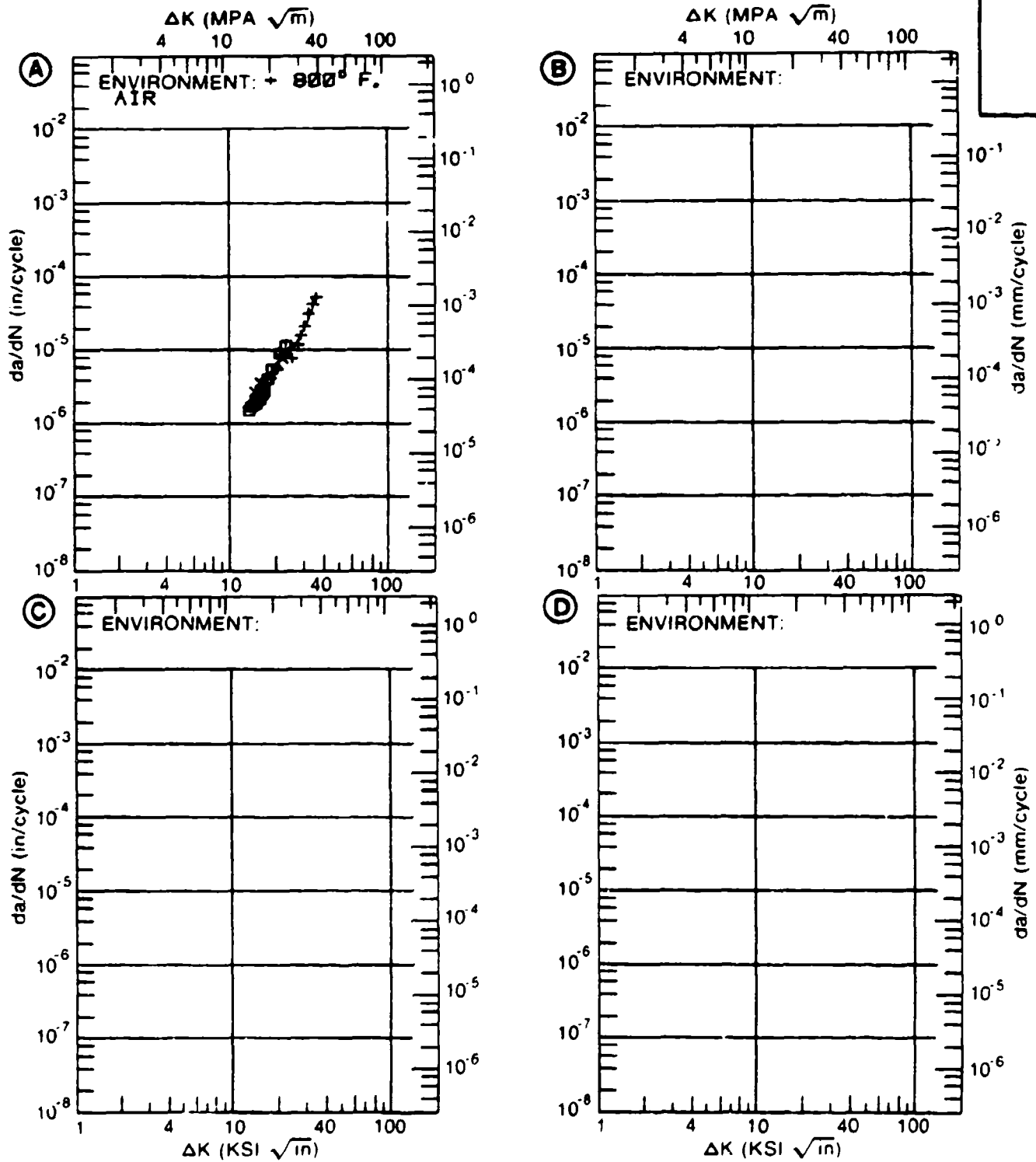


Figure 3.16.3.6

TABLE 3.16.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.7 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | E=+ 550 F | | | |
| | | : AIR | | | |
| DELTA K | A: 17.34 | 1.23 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 1.65 | | | |
| | 25.00 | 4.94 | | | |
| | 30.00 | 12.0 | | | |
| | 35.00 | 19.4 | | | |
| | 40.00 | 36.7 | | | |
| | 50.00 | 94.3 | | | |
| DELTA K | A: 51.20 | 86.4 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 15.97
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: ANNEALED
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.05
 FREQUENCY: 2.5 HZ

YIELD STRENGTH: 39.0 KSI
 ULT. STRENGTH: 84.0 KSI
 SPECIMEN THK: 0.252- 0.999"
 SPECIMEN WIDTH 1.899- 8.001"
 REFERENCES: HD010

| |
|-----------------|
| STAIN. STEEL |
| 304 |
| |

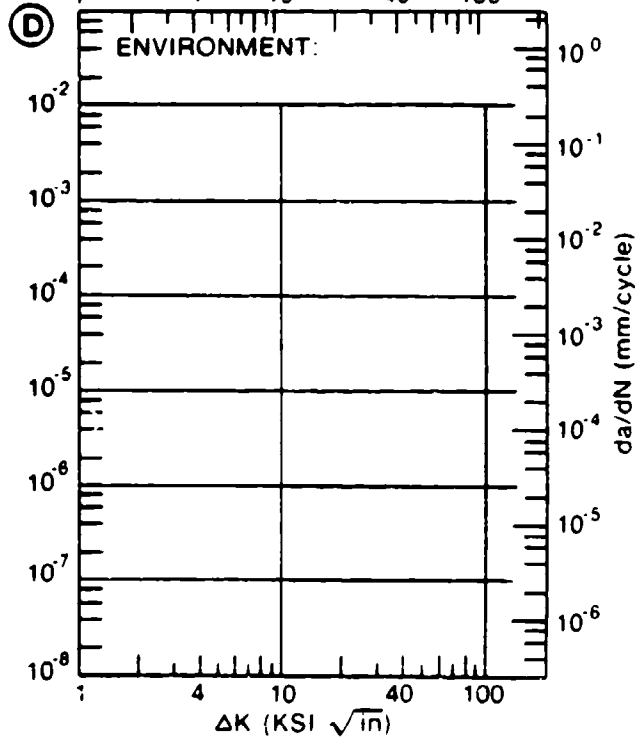
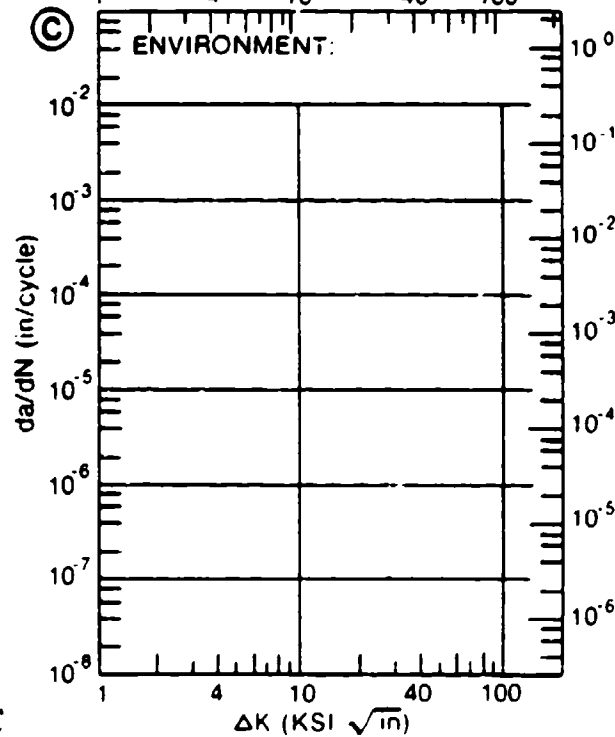
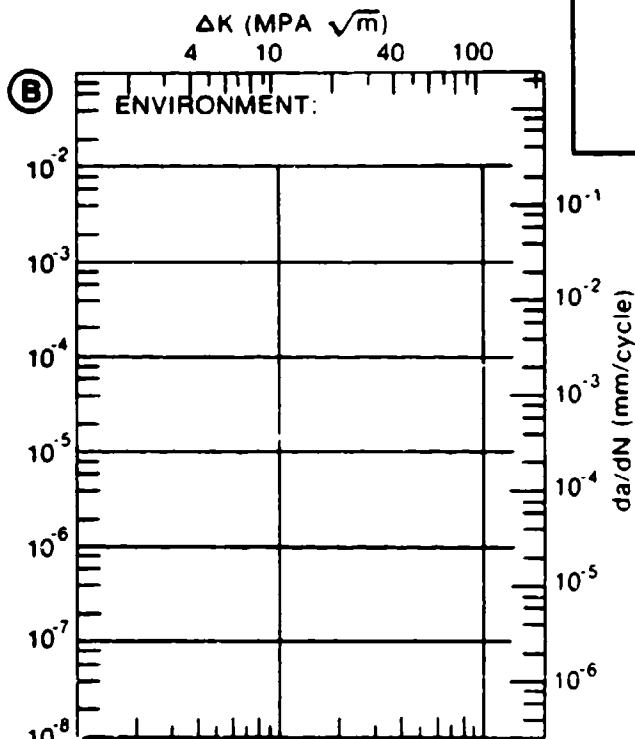
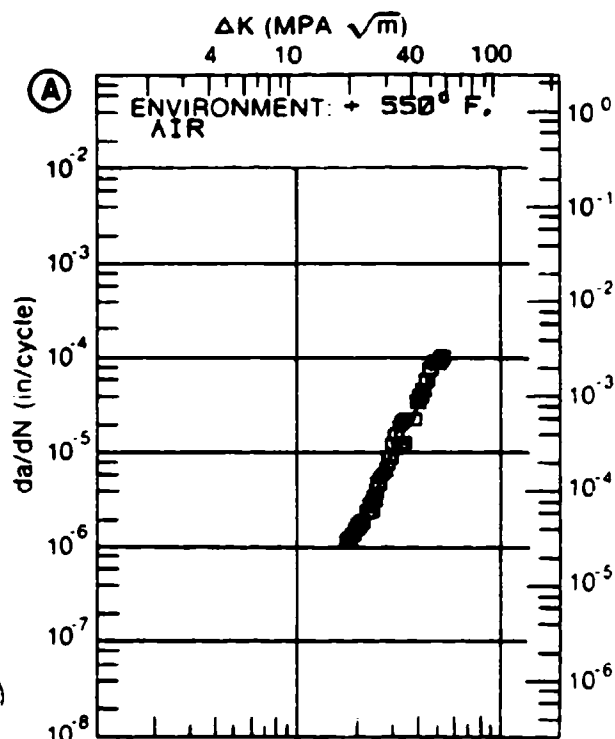


Figure 3.16.3.7

TABLE 3.16.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.16.3.8 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 304
CONDITION: ANNEALED & AGED

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---|---|---|
| | | A | B | C | D |
| | | E = R. T. LAB AIR | | | |
| DELTA K | A: 19.08 | 1.17 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 1.38 | | | |
| | 25.00 | 3.99 | | | |
| | 30.00 | 11.4 | | | |
| | 35.00 | 27.8 | | | |
| DELTA K | A: 35.83 | 31.6 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 8.08 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED & AGE
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION:
 STRESS RATIO: +0.05
 FREQUENCY: 3.0 HZ

YIELD STRENGTH: 39.6 KSI
 ULT. STRENGTH: 77.1 KSI
 SPECIMEN THK: 0.468"
 SPECIMEN WIDTH: 2.001"
 REFERENCES: H0008

STAIN.
STEEL

304

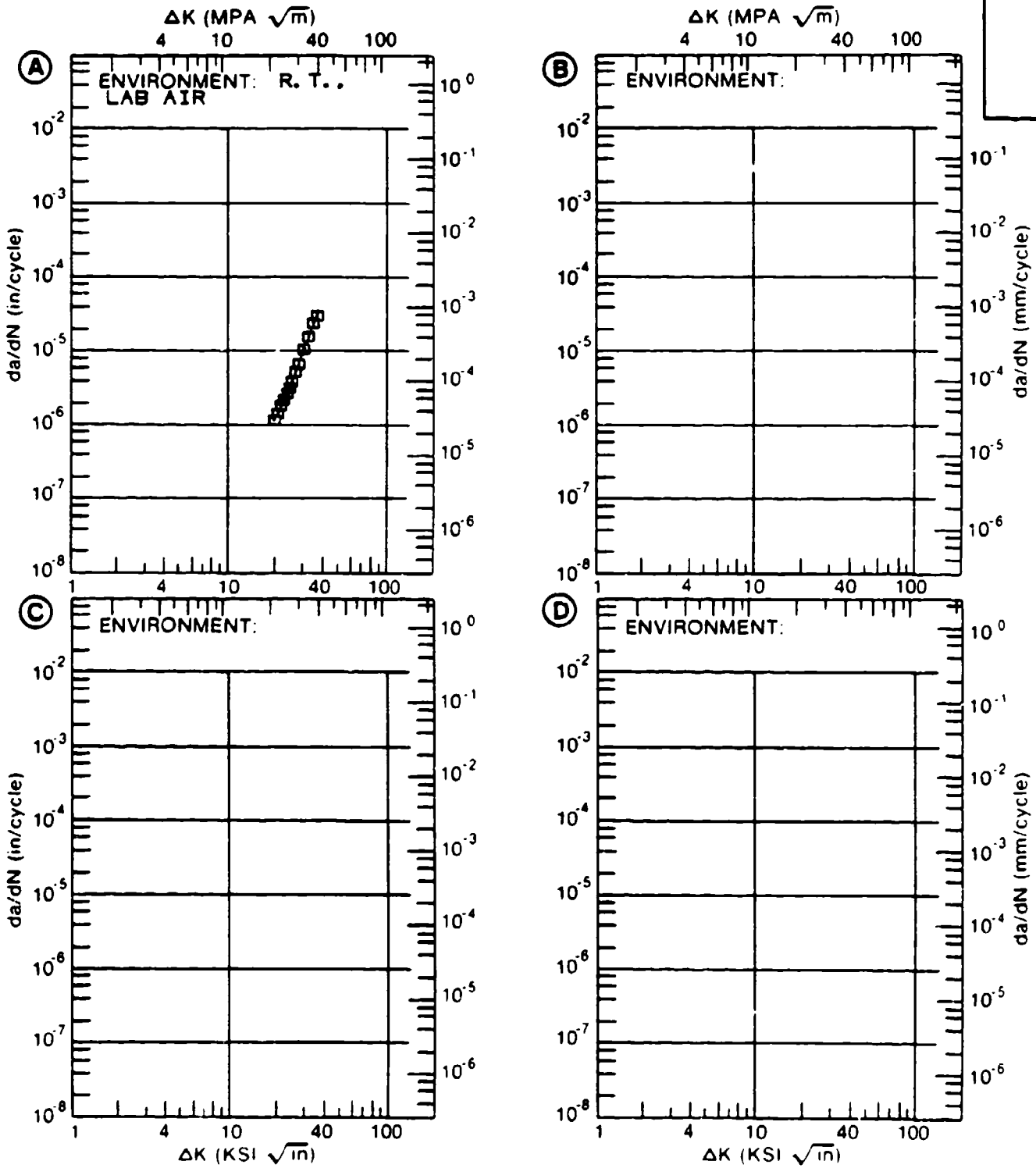


Figure 3.16.3.8

TABLE 3.17.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.17.3.1 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 316
CONDITION: ANNEALED

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|---------------------------|---|---|---|
| | A | B | C | D |
| | E=+ 98 F | | | |
| | AIR | | | |
| A: 17.85 | .435 | | | |
| DELTA K B: | | | | |
| MIN C: | | | | |
| D: | | | | |
| 20.00 | .868 | | | |
| 25.00 | 2.81 | | | |
| 30.00 | 6.38 | | | |
| 35.00 | 12.0 | | | |
| 40.00 | 20.1 | | | |
| 50.00 | 47.3 | | | |
| 60.00 | 98.5 | | | |
| A: 60.48 | 102. | | | |
| DELTA K B: | | | | |
| MAX C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 6.93
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) 2.0

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: SENT
 ORIENTATION:
 STRESS RATIO: +0.04
 FREQUENCY: 0.8 HZ

YIELD STRENGTH: 44.1 KSI
 ULT. STRENGTH: 82.1 KSI
 SPECIMEN THK: 0.504"
 SPECIMEN WIDTH: 4.501"
 REFERENCES: HD013

STAIN.
 STEEL

318

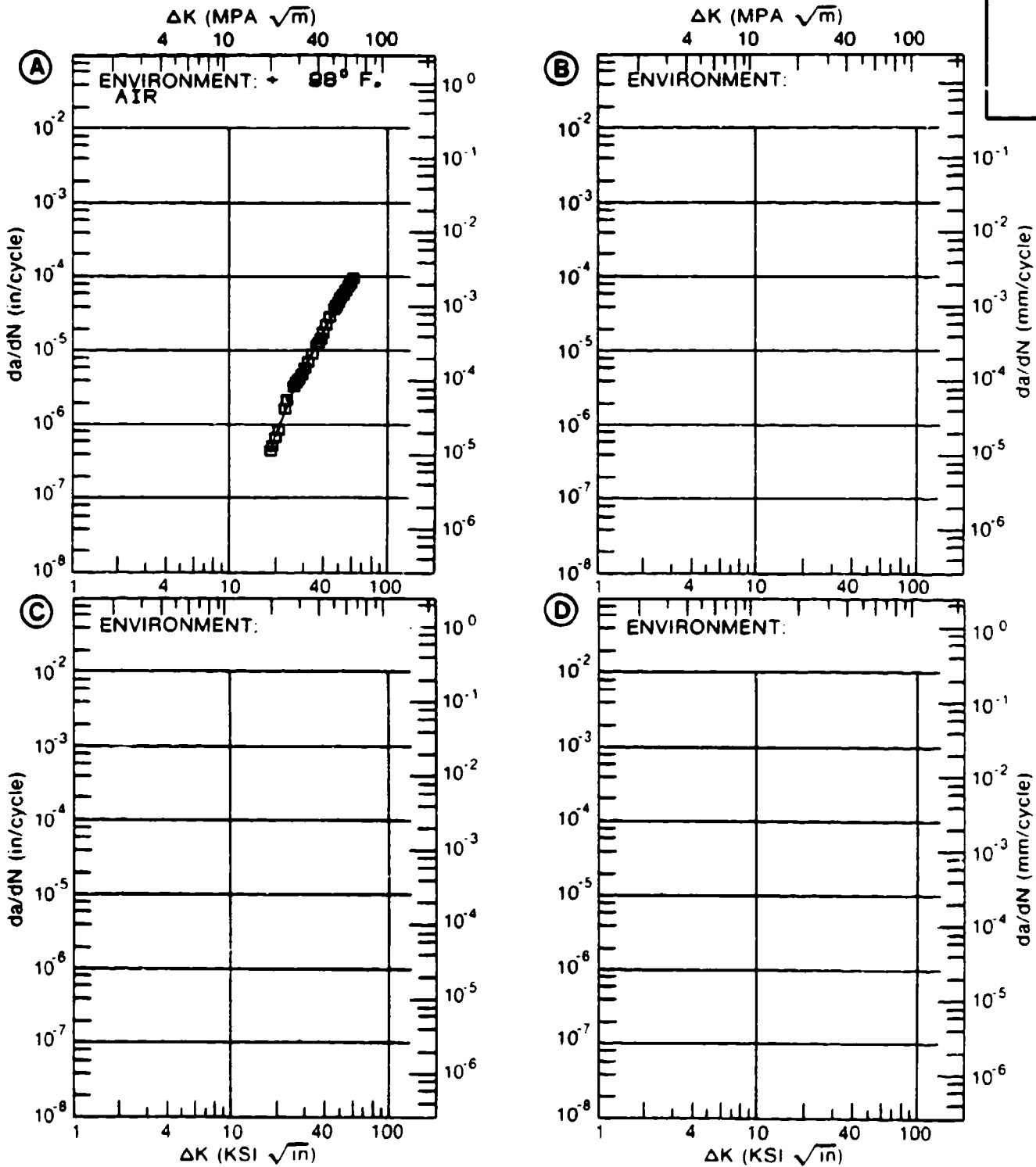


Figure 3.17.3.1

TABLE 3.17.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.17.3.2 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: STAINLESS STEEL 316
CONDITION: ANNEALED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|--|-----------|--|
| | | A | | B | |
| | | E=+ 600 F | | E=+ 800 F | |
| | | AIR | | AIR | |
| DELTA K MIN | A: 13.24 | 1.10 | | 2.43 | |
| | B: 16.21 | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 2.02 | | | |
| | 20.00 | 4.63 | | 5.14 | |
| | 25.00 | 12.5 | | 15.7 | |
| | 30.00 | | | 35.2 | |
| DELTA K MAX | A: 28.41 | 18.5 | | 38.1 | |
| | B: 30.70 | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 14.78 | | 7.64 | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION | 0.0-0.5 | | | | |
| RATIO SUMMARY | 0.5-0.8 | | | | |
| (NP/NA) | 0.8-1.25 | 2 | | 1 | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION:
 STRESS RATIO: +0.05
 FREQUENCY: 0.6 HZ

YIELD STRENGTH: 44.1 KSI
 ULT. STRENGTH: 82.1 KSI
 SPECIMEN THK: 0.486- 0.504"
 SPECIMEN WIDTH: 1.998- 2.047"
 REFERENCES: HD013, HD012

STAIN.
 STEEL

316

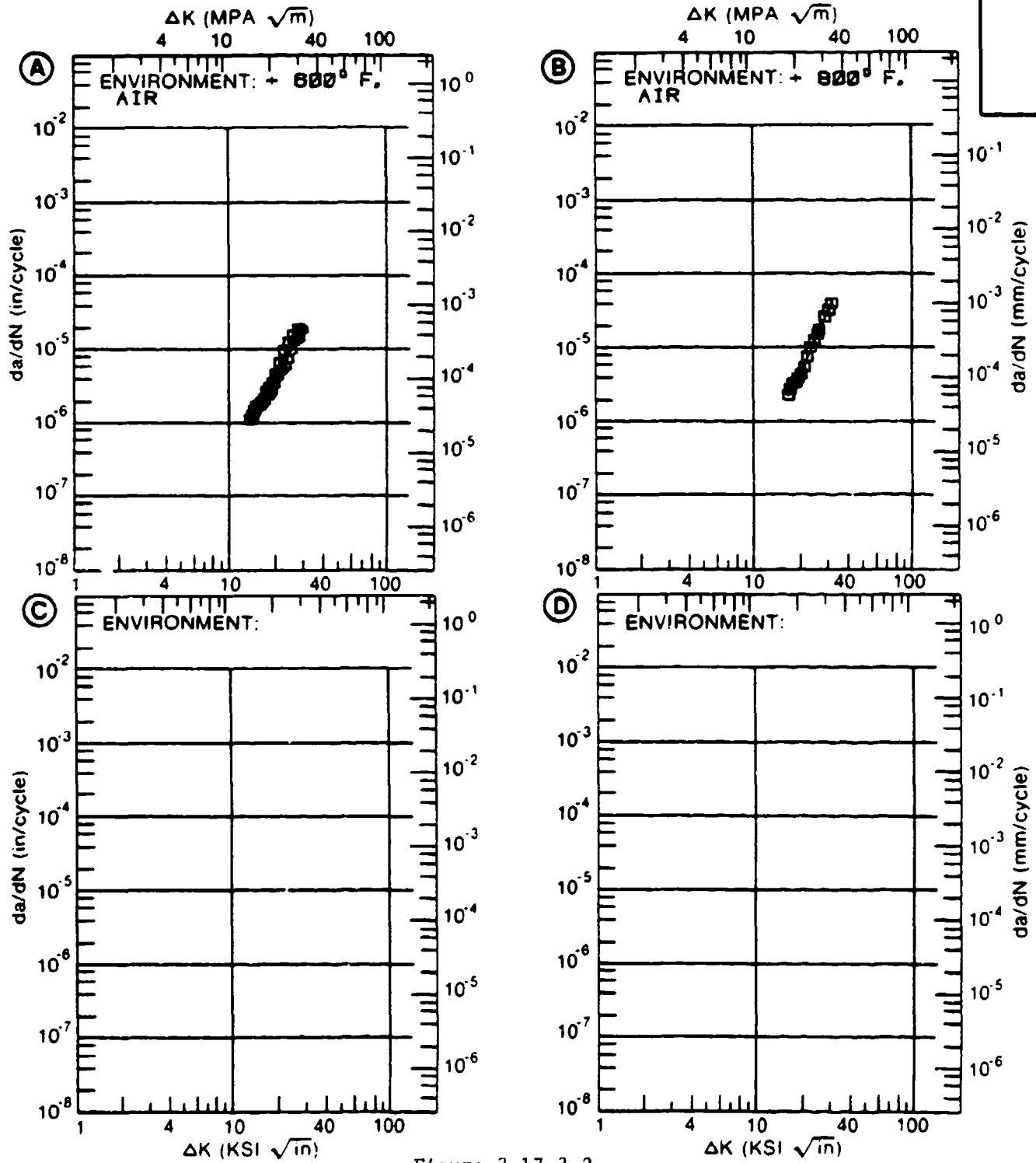


Figure 3.17.3.2

TABLE 3.17.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.17.3.3 INDICATING EFFECT
OF FREQUENCY

MATERIAL: STAINLESS STEEL 316
CONDITION: ANNEALED AT 1950F, 1HR, WG
ENVIRONMENT: R. T., LAB AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|---------------------------------------|--|-------|--------------|------|
| | A | B | C | D |
| | F(HZ)= 5.00 | | F(HZ)= 10.00 | |
| DELTA K MIN | A: 21.20 | 2.84 | B: 19.09 | 2.51 |
| | C: | | D: | |
| | 20.00 | | 2.39 | |
| | 25.00 | 5.45 | 6.24 | |
| | 30.00 | 11.6 | 13.1 | |
| | 35.00 | 22.8 | 30.9 | |
| | 40.00 | 42.4 | 53.1 | |
| DELTA K MAX | A: 40.78 | 46.5 | B: 40.55 | 53.6 |
| | C: | | D: | |
| ROOT MEAN SQUARE PERCENT ERROR | 4.22 | 20.54 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | 1 | 1 |

CONDITION/HT: ANNEALED AT 1950F, 1HR, WQ
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION:
 STRESS RATIO: +0.05
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 43.0- 44.1 KSI
 ULT. STRENGTH: 81.5- 82.1 KSI
 SPECIMEN THK: 0.495- 0.525"
 SPECIMEN WIDTH: 2.000- 2.001"
 REFERENCES: HD014, HD013

STAIN.
STEEL

316

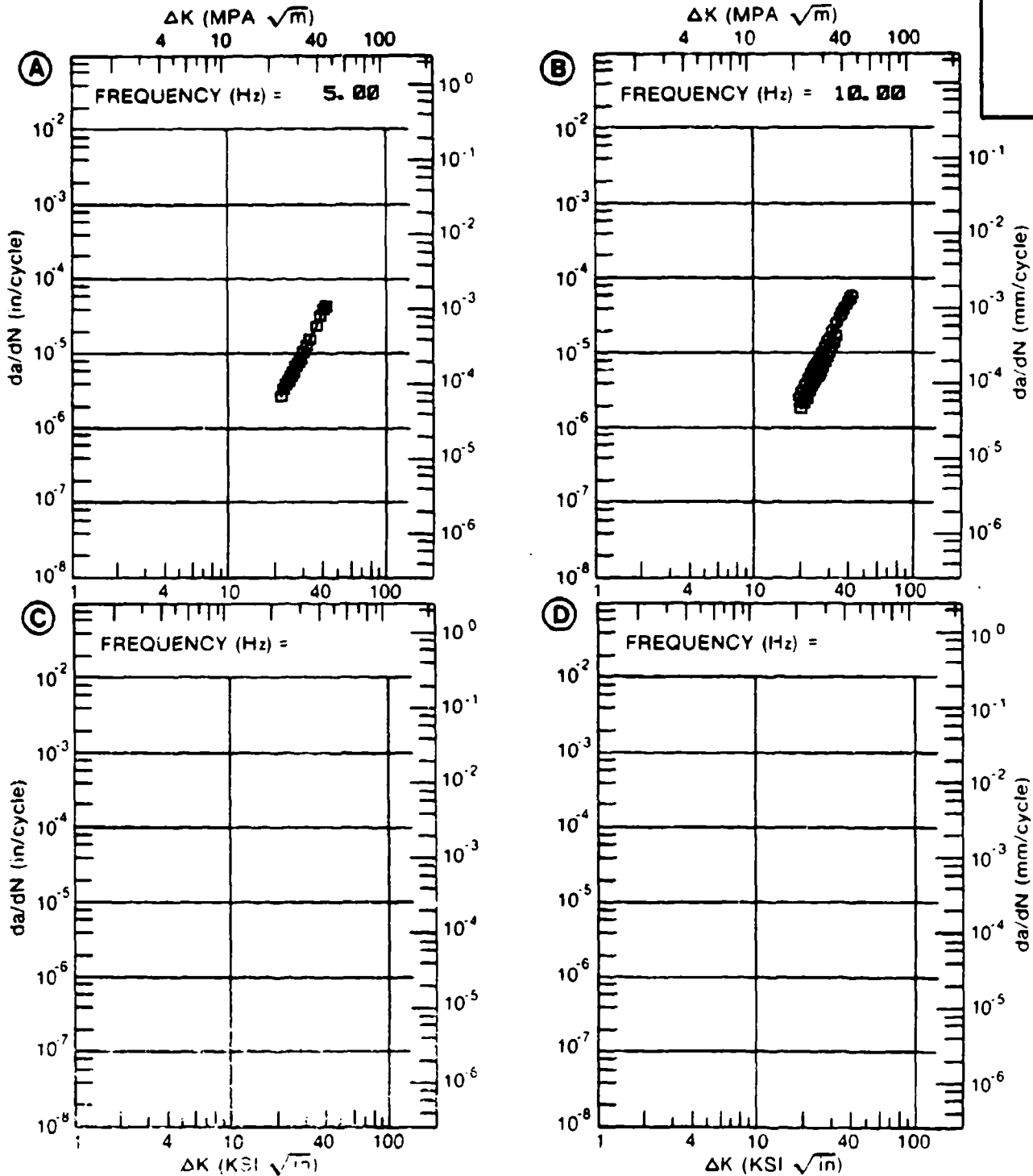


Figure 3.17.3.3

Figure 3.18.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
STAINLESS STEEL 304

INSPECTION

ENVIRONMENT

LAB AIR
AT R.T.

| CRACK LOCATION | WELDMENT | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | |
|-------------------------|----------|--------------|-----------|-------------------------------|---|----|----|----|------|
| | | | | 2.5 | 5 | 10 | 20 | 50 | 100 |
| 0.50 IN FROM CENTERLINE | WELDMENT | 0.10 | 30.00 | | | | | | 9.83 |
| AT CENTERLINE | WELDMENT | 0.10 | 30.00 | | | | | | 12.1 |
| AT HEAT AFFECTED ZONE | WELDMENT | 0.10 | 30.00 | | | | | | 17.9 |

TABLE 3.18.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.18.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 347
CONDITION: AT CENTERLINE
ENVIRONMENT: R.T. LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: 36.67 | 1.71 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| 40.00 | | 3.05 | | | |
| 50.00 | | 13.1 | | | |
| 60.00 | | 44.1 | | | |
| DELTA K MAX | A: 69.67 | 92.0 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 12.11
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: AT CENTERLINE
 FORM: WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION:
 FREQUENCY: 30.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: AM001

STAIN.
 STEEL

347

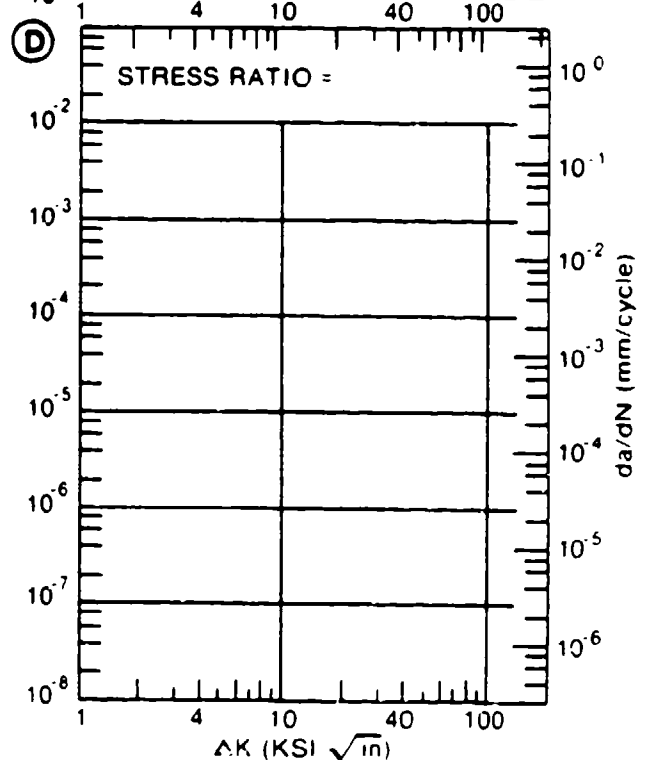
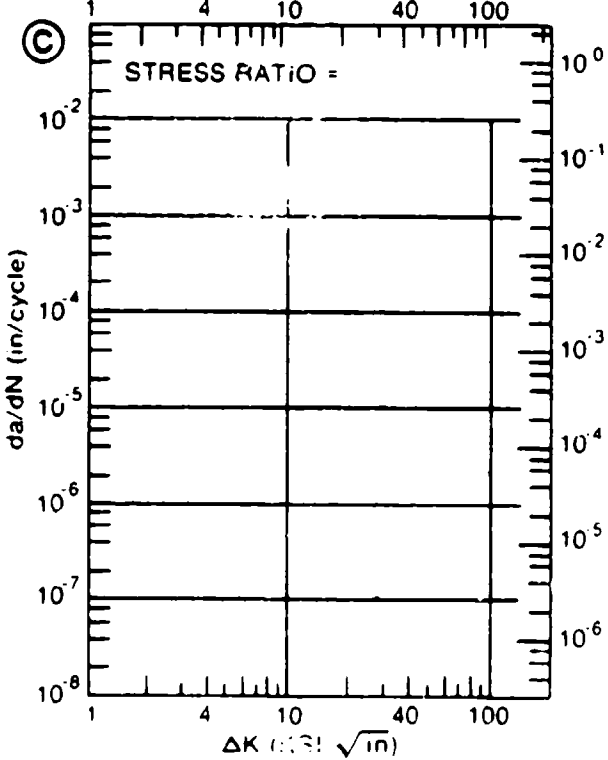
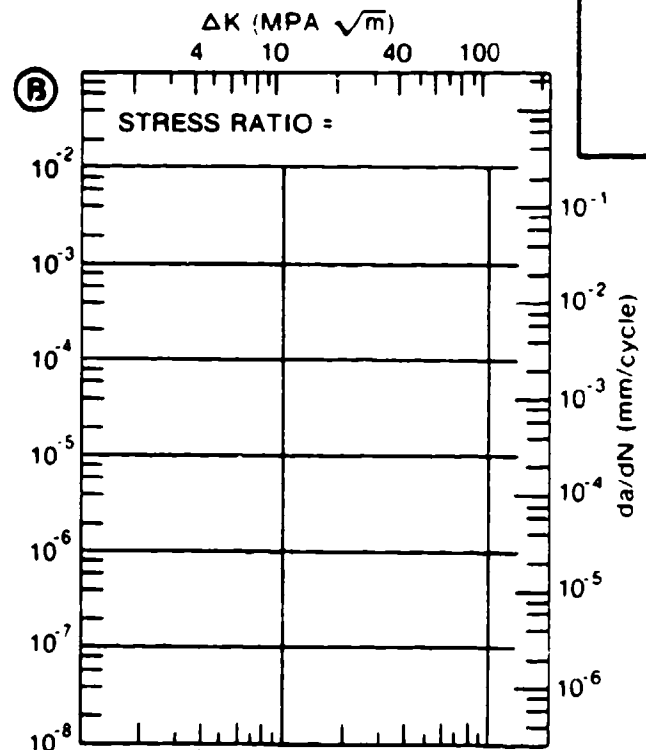
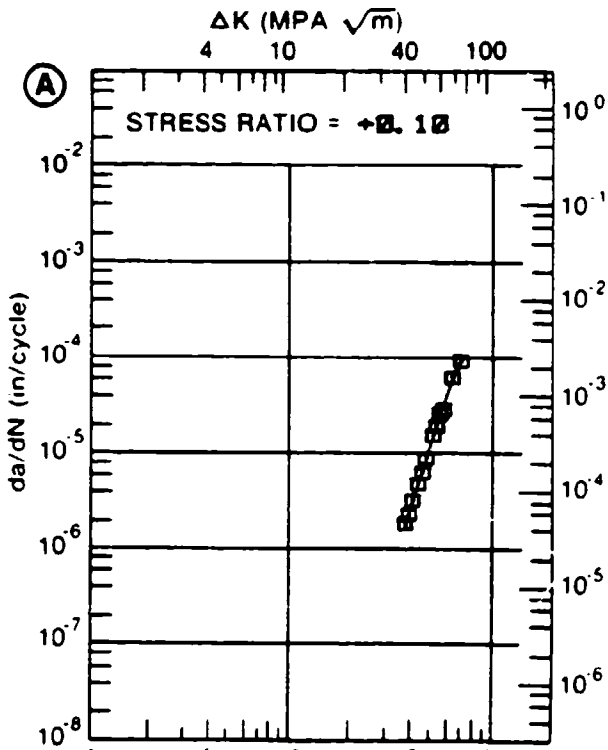


Figure 3.18.3.1

TABLE 3.18.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.18.3.2 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 347
CONDITION: AT HEAT AFFECTED ZONE
ENVIRONMENT: R.T. LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: 30.61 | 2.27 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 35.00 | 4.06 | | | |
| | 40.00 | 6.87 | | | |
| | 50.00 | 17.5 | | | |
| | 60.00 | 46.5 | | | |
| DELTA K MAX | A: 68.77 | 121. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 9.70
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: AT HEAT AFFECTED ZONE
 FORM: WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION:
 FREQUENCY: 30.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: AM001

STAIN.
 STEEL

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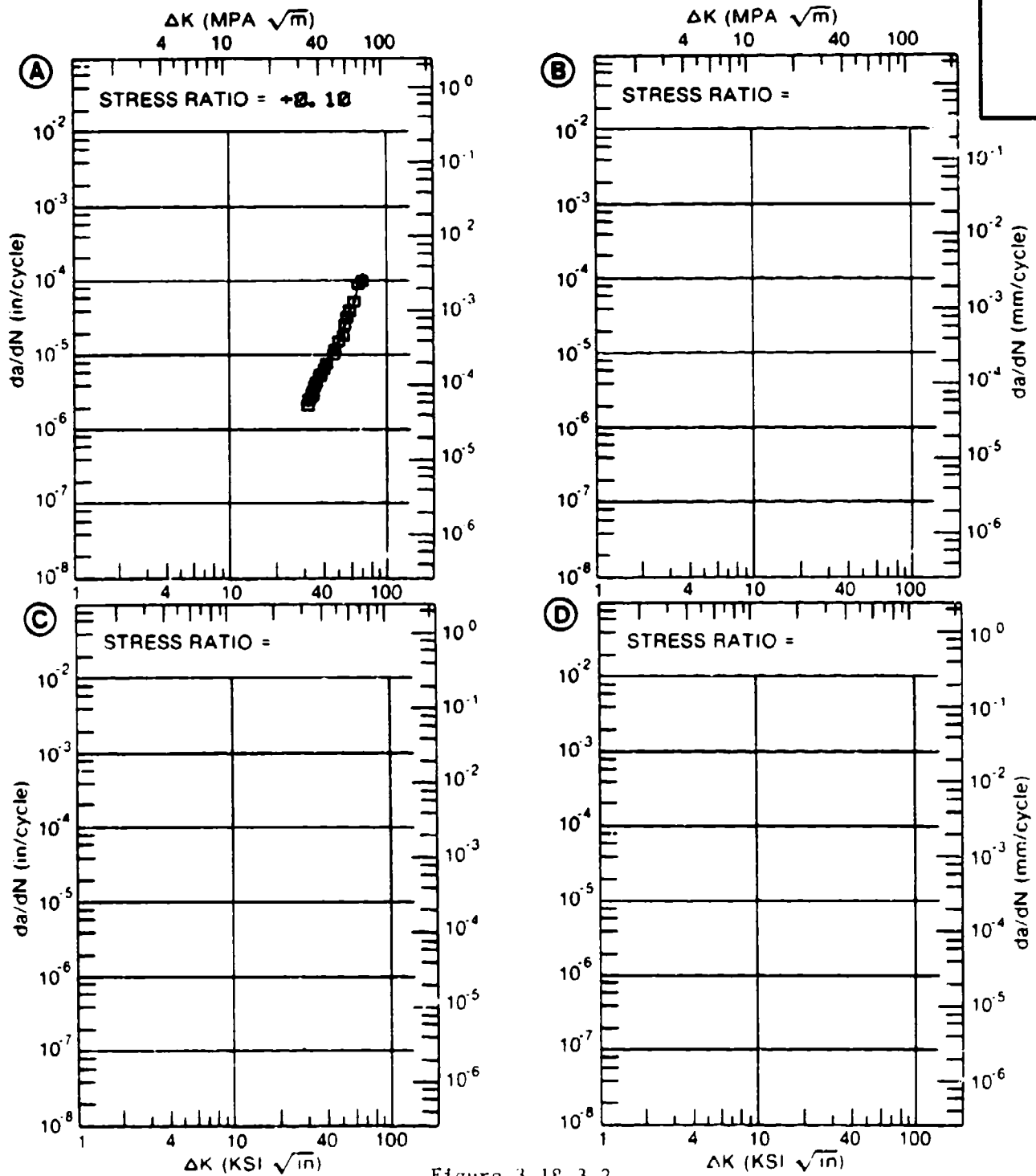


Figure 3.18.3.2

TABLE 3.18.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 3.18.3.3 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: STAINLESS STEEL 347
CONDITION: .050 IN. FROM CENTERLINE
ENVIRONMENT: R. T. LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|-------|---------------------------------------|------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: | 36.21 | 2.53 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 40.00 | 4.98 | | |
| | | 50.00 | 9.83 | | |
| | 60.00 | 18.0 | | | |
| | 70.00 | 47.3 | | | |
| | 80.00 | 89.2 | | | |
| DELTA K MAX | A: | 81.77 | 93.9 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 10.14
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: .050 IN. FROM CENTERLINE
 FORM: WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION:
 FREQUENCY: 30.0 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: AM001

STAIN.
 STEEL

347

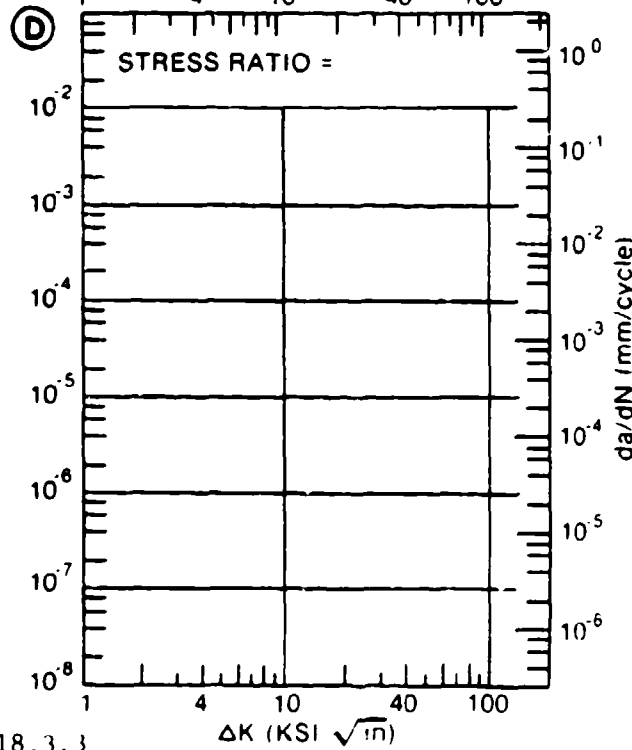
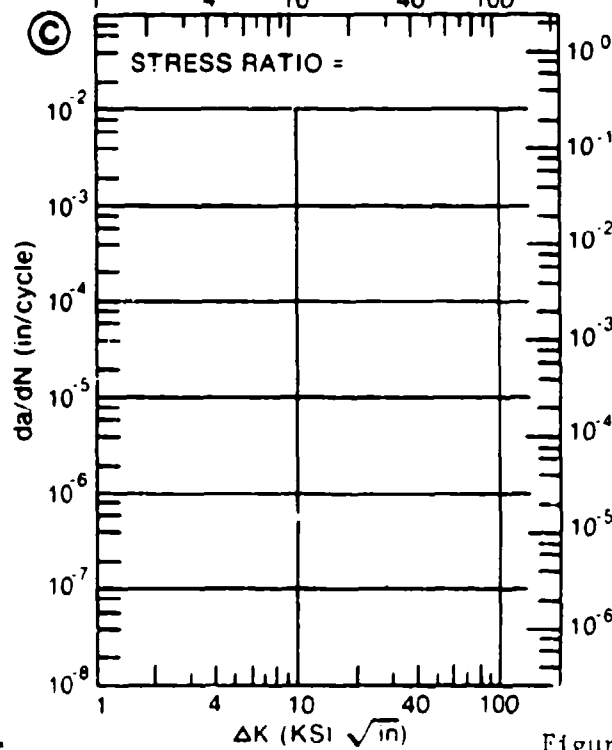
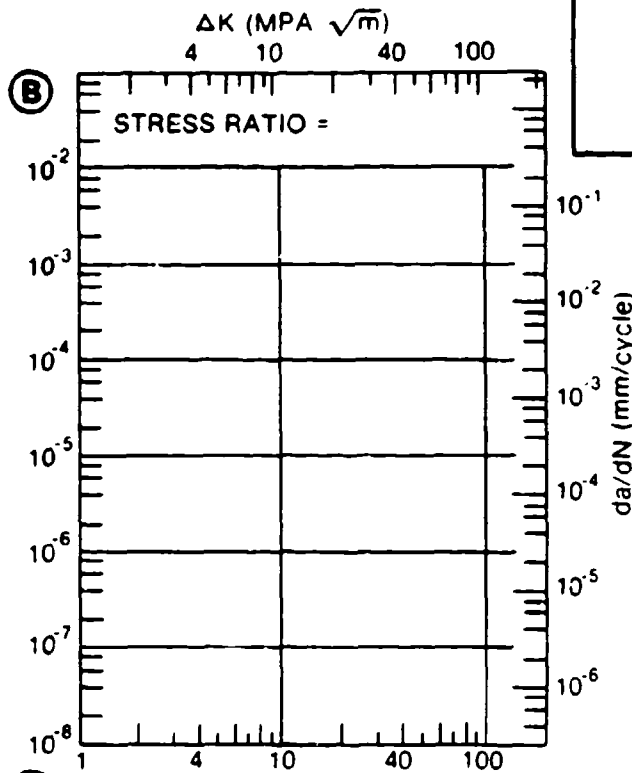
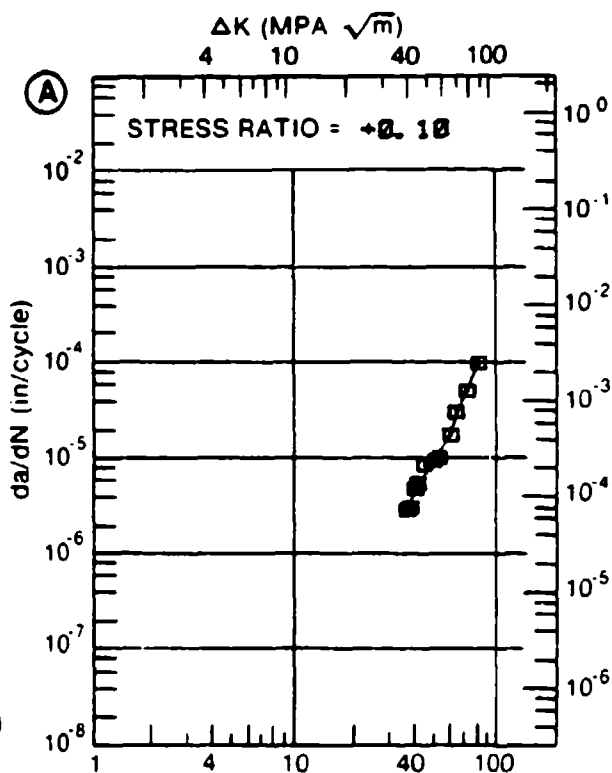


Figure 3.18.3.3

TABLE 3.19
REFERENCES FOR STAINLESS STEEL DATA

| | |
|-------|--|
| 57573 | PH14-8Mo K _c Anon., "Fracture Toughness and Tear Tests," Air Force Materials Laboratory, Research and Technology Division, Report No. ML-TDR-64-238, October 1964. |
| 70887 | PH 13-8Mo K _{ISCC} Peterson, M.H., Brown, B. P., Newbegin, R. L., and Groover, R. E., Stress Corrosion Cracking of High Strength Steels and Titanium Alloys in Chloride Solutions at Ambient Temperature," Corrosion, 23, (5), pp. 142-148, May 1967. |
| 74720 | AFC 77 K _{IC} K _{ISCC} Webster, D., "The Use of Deformation Voids to Refine the Austenitic Grain Size and Improve the Mechanical Properties of AFC 77," Research Report D6-23870, The Boeing Co., Renton, WA., ARPA Contract N00014-66-C-0365, February 1969. |
| 76136 | AFC 77 K _{IC} K _{ISCC} da/dt Webster, D., "The Stress Corrosion Resistance and Fatigue Crack Growth Rate of a High Strength Martensitic Stainless Steel, AFC 77," Research Report D6-23973, The Boeing Co., Renton, WA., ARPA Contract N00014-66-C-0365, June 1969. |
| 77934 | Custom 455 K _{IC} K _{ISCC} Uchida, J. M., "Evaluation of Carpenter Custom 455," Research Report D6-23928, The Boeing Co., Renton, WA., November 18, 1969. |
| 80685 | AFC 260 K _{IC} K _{ISCC} Webster, D., "Optimization of Strength and Toughness in Two High Strength Stainless Steels," Metallurgical Transactions, 2, (7), pp. 1857-1862, July 1971. |
| 83613 | PH 13-8M K _{ISCC} Sandoz, G., "The Resistance of Some High Strength Steels to Slow Crack Growth in Salt Water," NRL Memorandum Report 2454, Naval Research Laboratory, Washington, D.C., February 1972. |
| 84212 | 15-5 PH K _{IC} 17-4 PH K _{IC} Takas, E. G., "Fracture Toughness Tests, Data on Armco 17-4PH and 15-5 PH Alloys," letter to J.E. Campbell, Battelle Columbus, October 18, 1972. |
| 84302 | AFC 77 K _{IC} Webster, D., "Increasing the Toughness of Martensitic Stainless Steel AFC 77 By Control of Retained Austenite Content, Ausforming and Strain Aging," Transactions of the ASM, 61, (4) pp. 816-838, December 1968. |
| 84306 | PH 13-8 Mo K _{IC} Harrigan, M. J., "B-1 Fracture Mechanics Data for Air Force Handbook Usage," Report TFD-72-501, North American Rockwell, Los Angeles Division, Los Angeles, CA., April 21, 1972. |
| 84333 | AM 355 K _{ISCC} AM 362 K _{ISCC} AM 364 K _{ISCC} CUSTOM 455 K _{ISCC} PH 13-8 Mo K _{ISCC} PH 15-7 Mo K _{ISCC} 15-5 PH K _{ISCC} 17-4 PH K _{ISCC} 17-7 PH K _{ISCC} Carter, C. S., Farwick, D. G., Ross, A. M., Uchida, J. M., "Stress Corrosion Properties of High Strength Precipitation Hardening Stainless Steels," Corrosion 27, (5), pp. 190-197, May 1971. |

TABLE 3.19 (Continued)

| | |
|-------|---|
| 84365 | PH 13-8Mo K_{Ic} Takacs, E. G., "Plane Strain Fracture Toughness - PH 13-8 Mo," Tabulated Data from Armco Steel Corporation, Advanced Materials Division, Baltimore, Md., July 11, 1972. |
| 85034 | PH 13-8 Mo K_{Ic} Mitchell, John, "Laboratory Reports on Fracture Toughness Tests," per memo from Ed Cawthorne of February 5, 1973; data sheets from Shultz Steel Co., South Gate, CA. |
| 85544 | AFC 77 da/dN Speidel, M.O., "Dynamic and Static Embrittlement of a High Strength Steel in Water," preprint from L' Hydrogen Dans Les Metaux, 1, Editions Science et Industries, Paris, France (no date). |
| 85836 | PH 13-8Mo K_{Ic} "B-1 Fracture Toughness Data (K_{Ic}) - Rockwell International," Rockwell International Corp., Los Angeles, CA., April 24, 1973. |
| 85837 | PH 13-8 Mo da/dN "Fracture Toughness Data Collection, Rockwell International Corporation, from B-1 Program," Rockwell International Corporation, Los Angeles, CA., April 1973. |
| 85857 | PH 13-8 Mo K_{Ic} Shultz Steel Company - Fracture Toughness Data - May 10, 1973, per memo from Ed. Cawthorne of May 10, 1973. |
| 86688 | AM 355 K_{Isc} PH 13-8Mo K_{Isc} PH 15-7 Mo K_{Ic} 15-5 PH K_{Ic} 17-7 PH K_{Ic} K_{Isc} Sprowls, D. O., et al., "Evaluation of Stress Corrosion Cracking Susceptibility Using Fracture Mechanics Techniques," Final Report Part I, Aluminum Co. of America, Alcoa Technical Center, Alcoa, Pa., Contract NASA-21487, May 31, 1973. |
| 87360 | AFC 77 K_{Ic} K_{Isc} Caton, R. G., and Carter, C. S., "Evaluation of AFC 77 Martensitic Stainless Steel for Airframe Structural Applications," Report AFML- TR-73-182, Boeing Commercial Airplane Co., Seattle, WA., Contract F33615-71-C-1550, September 1973. |
| 88136 | PH 13-8 Mo K_{Ic} Dill, H. D., "Evaluation of Steel Alloys 300M, HP-9Ni-4Co-20, HP-9Ni-4Co - 30, and PH 13-8Mo," Report MDC-A2639, McDonnell Aircraft Co., McDonnell Douglas Corp., St. Louis, Mo., December 21, 1973, with data supplements received May 2, 1974. |
| 88579 | PH 13-8Mo da/dN "B-1 Program da/dN Data for Aluminum Alloys," Rockwell International Corporation, Memorandum to H.D. Moran from E.W. Cawthorne Battelle's Columbus Laboratories, April 3, 1974. |

TABLE 3.19 (Continued)

| | |
|-------|---|
| 90011 | PH 13-8Mo K_{Ic} "Rockwell International, B-1 Program Fracture Toughness Data of August 5, 1974," with memorandum from E.W. Cawthorne to H.D. Moran of Battelle's Columbus Laboratories, August 5, 1974. |
| 92270 | 15-5 PH da/dN Rice, R. L., "Fracture Toughness and Fatigue Crack Propagation in 15-5 PH Stainless Steel Bar," memorandum to J. E. Campbell, Battelle Columbus Laboratories, Columbus, Ohio, January 31, 1975. |
| AM001 | 347 da/dN "Fatigue Crack Propagation in a 347 Stainless Steel Weld," Prepared for Airesearch Manufacturing Co., by Del West Associates, Inc., July 29, 1975. |
| BW004 | 15-5 PH da/dN Watson, K. R., "Pylon Durability and Damage Tolerance Analysis," The Boeing Co., Wichita, KA., Contract No. F33657-78-C-0108-PZ0036, Document No. D361-400 41-2, September 1980. |
| BW005 | 15-5 PH da/dN Watson, K. R., "Weapons Bay Durability and Damage Tolerance Analysis," The Boeing Co., Wichita, KA., Contract No. F33657-78-C-0108-PZ0036, Document No. D361-40041-1, September 1980. |
| BW007 | 15-5 PH K_{Ic} Hananel A., Watson, K., Knoff, K., and Sherrich, G., "Fracture Mechanics Testing of B-52/CMI Materials," Final Test Report, The Boeing Co., Wichita, KA., Contract No. F33657-78-C00108-PZ0036, Document No. D361-11197-1, December 1978. |
| DA001 | 17-4 PH K_{Ic} da/dN 17-7 PH da/dN Fatigue Crack Growth Rate Data Sheets on Aluminum Alloys 2024, 7010, 7050, 7075, and 7475; Stainless Steel Alloys 17-4 PH and 17-7 PH, and Alloy Steels 4340, A286, H-11, HY-180 and 12-9-2, Sent from Mr. Paul Abelkis, Douglas Aircraft Co., McDonnell Douglas Corp., Long Beach, CA., March 1982. |
| GD009 | PH 13-8 Mo K_{Ic} K_{Isc} da/dN Margolis, W. S., "F-16 Material Allowables Evaluation of PH 13-8Mo Steel Alloy, H1000 Temper," General Dynamics, Fort Worth Division, Report No. 16PR1084, October 1978. |
| GD010 | 17-4PH da/dN Margolis, W. S., "Constant Amplitude Fatigue Crack Growth Rate of 17-4 PH Steel Alloy Casting, H1025, Repair Welded and Stress Relieved at 90F," General Dynamics, Fort Worth Division, Report No. 16PR1195, May 1979. |
| HD007 | 304 da/dN James, L. A., Schwenk, E. B., "Fatigue-Crack Propagation Behavior of Type 304 Stainless Steel at Elevated Temperatures," Metallurgical Transactions, Vol. 2, pp. 491-496, (1971). |
| HD008 | 304 da/dN James, L. A., "Effect of Thermal Aging Upon the Fatigue-Crack Propagation of Austenitic Stainless Steels," Metallurgical Transactions, Vol. 5, pp. 831-838, (1974). |

TABLE 3.19 Continued)

| | | |
|-------|--------------------------|--|
| HD009 | 304 da/dN | James, L. A., Staalsund, J. L., Bauer, R. E., "Optimization of Fatigue Crack Growth Testing for First Wall Materials Development Evaluations," Journal of Nuclear Materials, Vol. 85-86, Part B, pp. 851-854, (1979). |
| HD010 | 304 da/dN | James, L. A., "Specimen Size Considerations in Fatigue-Crack Growth Rate Testing in Fatigue Crack Growth Measurement and Data Analysis, STD-738, pp. 45-47, ASTM, (1981). |
| HD011 | 304 da/dN | James, L. A., "Frequency Effects in the Elevated Temperature Crack Behavior of Austenitic Stainless Steels-A Design Approach," Journal of Pressure Vessel Technology, Vol. 101, pp. 171-176, (1979). |
| HD012 | 304 da/dN 316 da/dN | James, L. A., "Some Observations Regarding Specimen Size Criteria for Fatigue-Crack Growth Rate Testing," Report HEDL-TME 77-87, Westinghouse Hanford Co., Richland, WA., August 1977. |
| HD013 | 316 da/dN | James, L. A., "The Effect of Elevated Temperature Upon the Fatigue-Crack Propagation Behavior of Two Austenitic Stainless Steels," Mechanical Properties of Materials, Vol. III, pp. 341-352, Society of Materials Science, Japan, 1972. |
| HD014 | 316 da/dN | James, L. A., "A Survey of the Effect of Heat-to-Heat Variations Upon the Fatigue-Crack Propagation Behavior of Types 304 and 316 Stainless Steels," Report HEDL-TME 75-37, Westinghouse Hanford Co., Richland, WA., May 1975. |
| MA001 | PH 13-8Mo K_{Ic} da/dN | Fracture Toughness and Fatigue Crack Growth Rate Data for Stainless Steel PH 13-8 Mo. Data supplied by D. L. Rich of McDonnell Aircraft Co., St. Louis, Mo.; Attachment No. 1, Received March 12, 1982. |
| NC001 | PH 13-8 Mo K_{Ic} | Plane Strain Fracture Toughness Data Sets on Aluminum, Steel and Titanium Alloys. Data sent from P.G. Porter of Northrop Corporation, March 1, 1982. |
| NC002 | PH 13-8Mo da/dN | Fatigue Crack Growth Rate Data on Aluminum Steel and Titanium Alloys. Data sent from P.G. Porter of Northrop Corp., March 1, 1982. |
| RI004 | CUSTOM 455 da/dN | Mines, R. G., "Fracture Mechanics Evaluation of Custom 455 Stainless Steel," Rockwell International, Shuttle Orbiter Division, Laboratory Test Report No. 2761-41-33, May 1980 |
| RI006 | PH 13-8Mo K_{Isc} | Ferguson, R. R., Berryman, R. C., "Fracture Mechanics Evaluation of B-1 Materials," Rockwell International, B-1 Division, Los Angeles, CA., Contract No. F33657-70-C-0800, Report No. AFML-TR-76-137, October 1976. |

CHAPTER 4
TITANIUM ALLOY SECTIONS

- 4.0 Titanium Material Summaries
- 4.1 Beta
- 4.2 Beta C
- 4.3 Beta III
- 4.4 Corona 5
- 4.5 Ti-6Al-2Sn-2Zr-2Mo-2Cr-2.5Si
(also see Section 4.8)
- 4.6 Ti-4Al-3Mo-1V
- 4.7 Ti-5Al-2.5Sn
- 4.8 Ti-6-2-2-2-2 (also see Section 4.5)
- 4.9 Ti-6-2-4-2
- 4.10 Ti-6-2-4-6 (also see Section 4.15)
- 4.11 Ti-6Al-4V
- 4.12 Ti-6Al-4V (ELI)
- 4.13 Ti-6Al-6V-2Sn
- 4.14 Ti-6Al-6V-2.5Sn
- 4.15 Ti-6Al-2Sn-4Zr-6Mo (also see
Section 4.10)
- 4.16 Ti-8Al-1Mo-1V
- 4.17 Ti-8Mo-8V-2Fe-3Al
- 4.18 Ti-5Al-2.5Sn (ELI)
- 4.19 Ti-6Al-6V-2Sn (ELI)
- 4.20 Bibliography

TABLE 4.0.1

AVAILABLE DATA FOR ILLINOIS ALBIS

| COMPILATION/MT | PRODUCT FORM | KIC | KC | R CURVES | DA/DM | DA/DT | KISCC |
|----------------|--|-----|----|----------|-------|-------|-------|
| BETA | BETA STAB | | | | | | X |
| | 1745F WA | | | | | | X |
| | 1745F W0. +1095F 61HR | | | | | | X |
| | 1745F W0. +1095F 1000HR | | | | | | X |
| | 1745F W0. +1095F 16HR | | | | | | X |
| | 1745F W0. +1095F 250HR | | | | | | X |
| | 1745F W0. +1095F 500HR | | | | | | X |
| BETA C | STA | | X | | | | |
| BETA III | AGED 1000F. 100HR | | | | | X | |
| | AGED 1250F. 50HR | | | | | X | |
| | AGED 900F. 100HR | | | | | X | |
| | BETA STAB +AGED 900F 1HR | | | | | | X |
| | STA | | | | X | | |
| | STA 900F 100HR | | | | | X | |
| | STA 900F 40HR | | | | | X | |
| | STA 900F 0HR | | | | | X | |
| | STA-1325F W0. 1045F 8HR (ELECTRON BEAM WELD ZONE) | | X | | | | |
| | STA-1325F W0. 1045F 8HR (HEAT AFFECTED ZONE) | | X | | | | |
| | STA-1325F W0. 1045F 8 HR | | X | | | | |
| | STA C. B WELDMENT (WELD ZONE) | | | | X | | |
| | STA. E. B WELDMENT (HEAT AFFECTED ZONE) | | | | | X | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR LITHIUM ALLOYS

| ALLOY | CONDITION/T | PRODUCT FORM | KTC | KC | R CURVES | DA/CN | DA/DT | KISCC |
|-------------------|--------------------------------------|--------------|-----|----|----------|-------|-------|-------|
| BETA III | 1025F 27HR. NO 925F 8HR | PLATE | X | | | | | |
| | 1750F 0.5 HR. NO. 925F 8HR. AC | EXTRUSION | X | | | | | |
| BETA II | BETA STABILIZED | SHEET | | | | | | X |
| BETA C | SIA | SHEET | | | | | X | |
| CONDITION 5 | ALPHA BETA FORGED & LOW ANNEAL 8 HR. | FORGING | X | | | | | |
| TI 5A1 2 55N(F11) | ANNEALED | FORGING | X | | | | | |
| | ANNEALED (ES) | FORGING | X | | | | | |
| | ANNEALED (IS) | FORGING | X | | | | | |
| TI 5A1 6 55N(F11) | 1605F 1 HR. NO. 1070F 4 HR. AC | PLATE | X | | | | | |
| | 1450F 1 HR. NO. 1125F 4 HR. AC | PLATE | X | | | | | |
| TI 4A1 3HR 10 | MILL ANNEALED | PLATE | | | | | | X |
| TI 5A1 2 55N | -- | SHEET | | | | | X | |
| | ANNEALED | SHEET | | | X | | | |
| TI 5A1 55N/2HR/0 | BETA PROCESSED | FORGING | X | | | | | |
| | RU. B FIN 10MA BETA UPSET. | FORGING | X | | | | | |
| | BETA FINISH D. 10% PRIMARY ALPHA | | | | | | | |
| | MILL ANNEALED 1500F 1 HR. AC | | | | | | | |
| | RU. B FIN 105TA BETA UPSET. | FORGING | X | | | | | |
| | BETA FINISHED 10% PRIMARY ALPHA. | | | | | | | |
| | SOLUTION TREATED & AGED | | | | | | | |
| | 1625F 1 HR. AC 1100F 8 HR. AC | | | | | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION: HT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DN | DA/DT | KISCC |
|---------------------------|--|--------------|-----|-----|----------|-------|-------|-------|
| Ti-6Al-2Sn-1Zr-0.1P-0.1Mg | BU, B FIN-100% BETA UPSET BETA FINISHED, 10% PRIMARY ALPHA SOLUTION TREATED/COVERAGED 1625F 1 HR. AC. 1700F 1 HR. AC | FORGING | X | | | | | |
| | BU, B FIN-50% BETA UPSET. BETA FINISHED, 50% PRIMARY ALPHA. MILL ANNEALED 1300F 1 HR. AC | FORGING | X | | | | | |
| | TU, B FIN-50% BETA UPSET. BETA FINISHED 50% PRIMARY ALPHA. SOLUTION TREATED & AGED. 1625F 1 HR. AC. 1100F 8 HR. AC | FORGING | X | | | | | |
| | BU, HAFIN100% BETA UPSET. HI ALPHA BETA FINISHED, 10% REDUCTION. SOLUTION TREATED & AGED. 1625F 1HR. AC. 1100F 8HR. AC | FORGING | X | | | | | |
| | BU, HAFIN100% BETA UPSET. HI ALPHA BETA FINISHED, 30% REDUCTION. SOLUTION TREATED & AGED. 1625F 1 HR. AC. 1100F 8HR. AC | FORGING | X | | | | | |
| | BU, LABFIN100% BETA UPSET. LO ALPHA BETA FINISHED, 10% REDUCTION. SOLUTION TREATED & AGED 1650F 1 HR. AC. 1100F 8HR. AC | FORGING | X | | | | | |
| | STA 1625F 2 HR. AC. 1100F 8 HR. AC | FORGING | X | | | | | |
| | 50% PRIMARY ALPHA | FORGING | X | | | | X | |
| | AB FORGED-MA ALPHA-BETA FORGED. MILL ANNEALED | FORGING | X | | | | | |
| | AB FORGED-RA ALPHA-BETA FORGED. RECRYSTALLIZED ANNEAL 1200F 4 HR. FC. TO 1000F 1 AC | FORGING | X | | | | | |

11-661-4V

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | KIC | KC | R | CURVES | DA/DN | DA/DT | KISCC |
|---|------------------------------------|--------------|-----|----|---|--------|-------|-------|-------|
| Ti-6Al-4V | ALPHA-BETA FORGED | FORGING | | | | | | | X |
| | ANNEALED | FORGING | X | | | | | | |
| | | EXTRUSION | X | | | | | | |
| | | BILLET | X | | | | | | X |
| | | SHEET | X | | X | | | | |
| | | PLATE | | | | | | | X |
| | ANNEALED AT 1375F. 3HRS. AC | BILLET | X | | | | | | |
| | ANNEALED 1000F 2 HR. AC | FORGING | X | | | | | | |
| | ANNEALED 1300F 4 HR. AC | PLATE | X | | | | | | |
| | ANNEALED 1375F 3HR. AC | FORGING | X | | | | | | |
| | ANNEALED 2700F 2 HR | FORGED BAR | X | | | | | | |
| | AS RECEIVED | PLATE | | | | | | | X |
| | AS RECEIVED PROBABLY MA | FORGED BAR | X | | | | | | |
| | AS RECEIVED (ALPHA-BETA FORGED) | FORGED BAR | X | | | | | | |
| | AS WELDED (B WELDMENT (WELD ZONE)) | WELDMENT | | | | | | | X |
| AS WELDED (B WELDMENT (HEAT AFFECTED ZONE)) | WELDMENT | | | | | | | X | |
| B FORGED (BETA FORGED REHEATED TO 1950F DRAIN TO SIZE. ANNEALED 1300F | FORGED BAR | X | | | | | | | |
| B FORGED (MA BETA FORGED. MILL ANNEALED. 1300F 2 HR. AC | FORGING | X | | | | | | | |
| BA | SHEET | | | | | | | X | |
| | PLATE | | | | | | | X | |
| | FORGING | | | | | | | X | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DN | DA/DT | KISCC | |
|-----------|--|----------------|-----|-----|----------|-------|-------|-------|---|
| Ti-6Al-4V | RR-AB FINISHED BETA BLOCKED. ALPHA BETA FINISHED. 10% REDUCTION. SOLUTION TREATED & OVERAGED 1750F 1HR. MO. 1300F 2 HR. AC | FORGING | | X | | | | | |
| | DR-AB FINISHED BETA-BLOCKED. ALPHA BETA FINISHED. 30% REDUCTION. SOLUTION TREATED & OVERAGED 1750F 3HR. MO. 1300F 2 HR. AC | FORGING | | X | | | | | |
| | RR-AB FIN-MA BETA BLOCKED. ALPHA-BETA FINISHED. MILL ANNEALED | FORGING | | X | | | | | |
| | DR-AB FIN-RA BETA BLOCKED. ALPHA BETA FINISHED. RECRYSTALLIZED. ANNEAL 1700F 4 HR. FC TO 1000F. AC | FORGING | | X | | | | | |
| | RR-AB FIN-30MA BETA BLOCKED. ALPHA BETA FINISHED. 30% REDUCTION. MILL. ANNEALED. 1300F 2 HR. AC | FORGING | | X | | | | | |
| | RR-0 FINISHED BETA FINISHED. 10%REDUCTION. SOLUTION TREATED & OVERAGED. 1750F 1 HR. MO. 1300F 2HR. AC | FORGING | | | | | | | |
| | RR-0 FIN-10MA BETA BLOCKED. BETA FINISHED. 10%REDUCTION. MILL. ANNEALFD. 1300F 2 HR. AC | FORGING | | X | | | | | |
| | BETA ANNEALED | PLATE | | X | | | | | |
| | BETA FORCED | FORGING | | | | | | X | |
| | BETA PROCESSED-MILL ANNEALED | SHEET PLATE | | X | | | | X | X |

TABLE 4.0.1 (cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DN | DA/DT | MISCC |
|--|--|--------------|-----|-----|----------|-------|-------|-------|
| Ti-6Al-4V | DB | PLATE | | | | X | | |
| | DB + 1H | PLATE | | | | X | | |
| | DR + 2DBTC | PLATE | | | | X | | |
| | DB + 4DBTC | PLATE | | | | X | | |
| | DB1 + PC | PLATE | | | | X | | |
| | DBTC | PLATE | | | | X | | |
| | DDTC (HA) | PLATE | | | | X | | |
| | DIFFUSION BOND | PLATE | X | | | | | |
| | DIFFUSION BOND | BILLET | X | | | | | |
| | DIFFUSION BOND ANNEALED | BILLET | X | | | | | |
| | EB WELD, STRESS RELIEVED (HEAT AFFECTED ZONE) | WELDMENT | | | | | X | |
| | CR WELD, STRESS RELIEVED (WELD ZONE) | WELDMENT | | | | | X | |
| | FINISH ROLLED 1340F | PLATE | | | | | | X |
| | GTA WELD POSTWELD 1200F 1HR (HEAT AFFECTED ZONE) | PLATE | | | | | | X |
| | GTA WELD POSTWELD 1400F 1HR (HEAT AFFECTED ZONE) | PLATE | | | | | | X |
| GTA WELD POSTWELD 1100F 2HR (WELD ZONE) | PLATE | | | | | | X | |
| GTA - WELD POSTWELD 1100F 2HR (HEAT AFFECTED ZONE) | PLATE | | | | | | X | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | KIC | R | CURVES | DA/DN | DA/DT | KISCC |
|--|---|--------------|-----|-----|---|--------|-------|-------|-------|
| Ti-6Al-4V | MA | PLATE | | X | | | X | | |
| | | SHEET | | X | | | X | | |
| | MA COARSE GRAIN 1300F 2 HR. AC | EXTRUSION | | | | | X | | |
| | | FORGING | | X | | | | | |
| | MA FINE GRAIN 1300F 2 HR. AC | FORGING | | X | | | | | |
| | | FORGING | | X | | | | | |
| | MA 10-20%ALPHA 10 TO 20% PRIMARY ALPHA MILL ANNEALED 1300F 2 HR. AC | FORGING | | X | | | | | |
| | | DISK | | | | | | X | |
| | MA 1300F 2HRS AC | --- | | | | | | X | |
| | | --- | | | | | | | X |
| MA 40 50%ALPHA 40 TO 50% PRIMARY ALPHA. MILL ANNEALED 1300F 2 HR. AC | FORGING | | X | | | | | | |
| | MILL ANNEALED | | | | | | | | X X |
| MILL ANNEALED 1300F 2HR. AC | PLATE | | X | | | | | | |
| | SHEET | | | | | | | | X X |
| MINUTEMAN CASTING | EXTRUSION | | X | | | | | | |
| | FORGING | | X | | | | | | |
| RA | BILLET | | X | | | | | | |
| | PLATE | | | | | | | | X |
| RA(FAST COOLED) | PLATE | | | | | | | | X X |
| | FORGING | | | | | | | | X X |
| RECRYSTALLIZE ANNEAL | PLATE | | | | | | | | X |
| | FORGING | | X | | | | | | X |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/TIT | PRODUCT FORM | K1C | KIC | R CURVES | DA/DN | DA/DT | KISCC |
|---|---|---------------|-----|-----|----------|-------|-------|-------|
| Ti 6AL-4V | SDR TREATED 1050F 4HR. WELDED 1050F 4HR | FORGING | | | | | | X |
| | SDR TREATED 1050F 4+4 HR | FORGING | | | | | | X |
| | STA | PLATE FORGING | X | | | | | |
| | | PLATE FORGING | X | | | X | | |
| | STA | PLATE FORGING | X | | | | | |
| | SDR 1750F 1 HR. AC. 1300F 2 HR. AC | FORGING | X | | | | | |
| | STRESS RELIEVED E B WELDMENT (WELD ZONE) | WELDMENT | | | | X | | |
| | STRESS RELIEVED E B WELDMENT (WAT AFFECTED ZONE) | WELDMENT | | | | X | | |
| | WELDED & STRESS RELIEVED 1100F 2HRS (HAZ) | WELDMENT | | | | X | | |
| | 1000F 2HR | FORGING | | | | | X | |
| | 1300F 1HR. AC | FORGING | | X | | | | |
| | 1300F 2HR AC | EXTRUSION | | | | | | X |
| 1450F. 1HR. AC | PLATE | X | | | | | | |
| 1550F 4HRS T.C. 1700F 4HRS ARGON COOLED | FORGING | | | | X | | | |
| 1700F 4HR F.C. TO 1400F AC. DIFFUSION BOND THERMAL CYCLE | PLATE | | | | | | X | |
| 1700F 5 HR. AC. 1400F 6 HR. AC | FORGING | | X | | | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/THT | PRODUCT FORM | KIC | KC | R CURVES | FA/DN | DA/DT | MISCC |
|---|---|--------------|-----|----|----------|-------|-------|-------|
| Ti-6Al-4V | 1725F 1HR WQ 1250F 4HR AC (STDA) | EXTRUSION | | | | | | X |
| | 1725F 1HR WQ 1000F 1HR AC (STA) | EXTRUSION | | | | | | X |
| | 1750F WQ 1000F 8HR 1000F (ALPHA+ETA) | FORGING | | | | | | X |
| | 1750F 1 HR.WQ.1000F 4 HR | FORGING | X | | | | | |
| | 1750F 1HR FC TO 1100F.AC | PLATE | X | | | | | |
| | 1750F 1HR.FC TO RT | PLATE | X | | | | | |
| | 1750F 1000F 2HR AC | FORGING | | | | | | X |
| | 1750F 2 HR.FC TO 900F AT 100F/HR.AC | FORGING | X | | | | | |
| | 1750F 2HR.WQ.1000F 2HR.AC. 1000F 2HR.AC.STA | PLATE | X | | | | | |
| | 1770F 1 2HR WQ 1050F-1100F 8HR. 950F 8HR | FORGING | | | | | | X |
| | 1750F 3HRS ARGON COOLED. 100 OF 4HRS ARGON COOLED | FORGING | | | | X | | |
| | 1775F 1HR WQ. 1675F 1HR WQ. 1000F 4HRS AC. 900F 5HRS AC | DISK | | | | X | | |
| | 1775F 1HR WQ. 1575F 1HR WQ. 1000F 1200F 2-8HRS AC | DISK | | | | X | | |
| | 1750F 1 5HR WQ 1150F 8HR + 1020F 8HR AC | SHIPT | | | | | | X |
| | 1500F 0 5HR 675F 2HRS AC | PLATE | | | | | | |
| 1950F 4HRS WQ. 1000F 4HRS ARG ON COOLED | FORGING | | | | X | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/T | PRODUCT FORM | K1C | KIC | KC | R CURVES | DA/DN | DA/DT | KISCC |
|-----------------|--|--------------|-----|-----|----|----------|-------|-------|-------|
| Ti-6Al-4V (ELI) | ANNEALED | SHEET | | | X | | | | |
| | BA | PLATE | | | | | X | | |
| Ti-6Al-4V (ELI) | ANNEALED | FORGING | X | | | | | X | |
| | BA | PLATE | | | | | | X | |
| | RECRYSTALLIZED ANNEAL 1800F 1HR HELIUM COOL | PLATE | | X | | | | | X |
| Ti-6Al-6V-2Zr | ANNEALED 10-20-10-20% PRIMARY ALPHA ANNEALED 1350F 2 HR. AC | FORGING | | X | | | | | |
| | ANNEALED 40-50-40-50% PRIMARY ALPHA ANNEALED 1350F 2 HR. AC | FORGING | | X | | | | | |
| | ANNEAL-COARSE GRAIN-1350F 2 HR. AC | FORGING | | X | | | | | |
| | ANNEAL-FINE GRAIN 1350F 2 HR. AC | FORGING | | X | | | | | |
| | BA | PLATE | | | | | | X | |
| Ti-6Al-6V-2Zr | BA | FORGING | | X | | | | | |
| | DR. AB FIN-10% BETA BLOCKED. ALPHA-BETA FINISH-D. 10% REDUCTION. SOLUTION TREATED & OVERAGED 1650 1 HR. WQ 1300F 2 HR. AC | FORGING | | X | | | | | |
| Ti-6Al-6V-2Zr | DR. AB FIN-10% BETA BLOCKED. ALPHA-BETA FINISH-D. 10% REDUCTION. MILL ANNEALED 1350F 2 HR. AC | FORGING | | X | | | | | |
| | DR. AB FIN-30% BETA BLOCKED. ALPHA-BETA FINISH-D. 30% REDUCTION. SOLUTION TREATED & OVERAGED. 1650F 1HR. WQ 1350F 2 HR. AC | FORGING | | X | | | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | MTC | KC | R CURVES | DA/DN | DA/DT | MISCC |
|---------------|--|-------------------------------|--------|----|----------|-------|-------|-------------|
| Ti-6Al-4V-2Sn | BB, AB FIN-30MA BETA BLOCKED. ALPHA BETA FINISHED. 10% REDUCTION. MILL ANNEALED 1350F 2 HR. AC | FORGING | X | | | | | |
| | BB, B FIN-10 BETA BLOCKED. BETA FINISHED. 10% REDUCTION. SOLUTION TREATED & OVERAGED. 1550F 1 HR. HQ. 1300F 2HR. AC | FORGING | X | | | | | |
| | BB, P FIN-10MA BETA BLOCKED. BETA FINISHED. 10% REDUCTION. MILL ANNEALED 1350F 2 HR. AC | FORGING | X | | | | | |
| | BETA ANNEAL | PLATE | X | | | | | |
| | BETA ANNEAL 1810F 1 HR. ARGON COIL | PLATE | X | | | | | |
| | BETA ANNEAL & STUA-1800F 0.5HR. AC. 1575F 0.5HR. HQ. 1050F 8 HR. AC | PLATE | X | | | | | |
| | BF, AB FOR-ANN BETA FLECTED. ALPHA BETA FORGED. ANNEALED. 1350F 2 HR. AC | FORGING | X | | | | | |
| | BF, B FOR-ANN BETA FLECTED. BETA FORGED. ANNEALED 1350F 2 HR. AC | FORGING | X | | | | | |
| | PF, AB FOR-ANN BETA FLECTED. LOW ALPHA BETA FORGED (1500F) ANNEALED. 1350F 2 HR. AC | FORGING | X | | | | | |
| | DUPLEX ANNEAL | PLATE | X | | | | | |
| | MA | ----- EXTRUSION FORGING | | | | | | X X X |
| | MILL ANNEALED | PLATE FORGING | X X | | | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR LIQUID ALLOYS

| ALLOY | CONDITION/THT | PRODUCT FORM | KIC | KC | R | DA/DN | DA/DT | KISCC |
|-------------------------------|---|-------------------|-----|----|---|-------|-------|-------|
| Ti-6Al-4V-2Sn | MILL ANNEALED | FORGED BAR | X | | | | | |
| | | HILLET | X | | | | | |
| | MILL ANNEALED 1000F 2 HR. AC | PILLET | X | | | | | X |
| | RA | | | | | | | |
| | RECRYSTALLIZE ANNEAL | PLATE | X | | | | | |
| | STA-1450F 0.5HR. WQ. 1050F 6 HR. AC | FORGING | X | | | | | |
| | STA-1650F 0.5HR. WQ. 1050F 24 HR. AC | FORGING | X | | | | | |
| | STA-1675F 0.25 HR. WQ. 1100F 4 HR | PLATE | X | | | | | |
| | STDA | PLATE | | | | | | X |
| | STDA-1500F 1 SHP. WQ. 1250F 6 HR. AC | EXTRUSION | X | | | | | |
| | STDA-1450F 1 HR. WQ. 1300F 2 HR. AC | FORGING | X | | | | | |
| | STDA 1700F 1 HR. WQ. 1400F 1 HR. AC | PLATE | X | | | | | |
| | 1700F 2HR | HILLET FORGING | X | | | | | X |
| | 1650 1 HR WQ. | FORGING | X | | | | | |
| | 1675F 2 HR. AC 1600F 1 HR. FC | PLATE | X | | | | | |
| 1675F 2 HR. AC 1600F 1 HR. FC | FORGING | X | | | | | | |
| 1675F 2 HR. AC 1800F 1 HR. FC | FORGED BAR | X | | | | | | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | K1C | K1C | R | CURVES | DA/DN | DA/DT | K1SCC |
|----------------|---|--------------|-----|-----|---|--------|-------|-------|-------|
| Ti-6Al-4V L15N | 1000F 2HR AC | PLATE | | | | | | | X |
| | 1100F 2HR AC | FORGING | | | | | | | X |
| | 1500F 1HR WQ | FORGING | | | | | | | X |
| | 1500F 1HR WQ | PLATE | | | | | | | X |
| Ti-6Al-2Zr-1Sn | ST | PLATE | | | | X | | | |
| | SFA | PLATE | | | | X | | | |
| | 1750F 1HR AC, 1100F 2HRS AC | FORGING | | | | X | | | |
| Ti-6Al-2Zr-1Sn | 1750F 1HR AC, 1100F 2HRS AC | EXTRUSION | | | | X | | | |
| | 1500F 2HRS AC, 1500F 2HRS OG, 1100F 2HRS AC | FORGING | | | | X | | | |
| Ti-6Al-1Mo-1V | 1000F 2HR AC | SHEET PLATE | | | | | X | X | X |
| | 1100F 2HR AC | SHEET PLATE | | | | | X | X | X |
| | 1500F 1HR WQ | SHEET | | | | X | | | |
| | 1500F 1HR WQ | SHEET PLATE | | | | X | X | X | |
| | MILL ANNEALED | PLATE | | | | | | | X |
| | MILL ANNEALED 1350F 8HR FC | SHEET | | | | | | | X |
| | VAC ANNEALED | PLATE | | | | | | | X |
| | 1500F 1HR WQ | PLATE | | | | | | X | |
| | 1500F 1HR AC, 1100F 2HR AC, 1000F 2HR AC | PLATE | | | | | | | X |
| | 1700F 1HR AC, 1200F 2HR WQ | PLATE | | | | | | | X |
| | 1725F FC, 1200F 3HR WQ | PLATE | | | | | | X | |

TABLE 4.0.1 (Cont)

AVAILABLE DATA FOR TITANIUM ALLOYS

| ALLOY | CONDITION/HT | PRODUCT FORM | KIC | MC | R | CURVES | DA/DN | DAY/DT | MISCC |
|--------------------|--|--------------|-----|----|---|--------|-------|--------|-------|
| Ti-6Al-4V | 1775F 0.5HR FC TO 1200F. 1200F 0.5HR AC. 1200F 3HR AIRGUN QUENCH | PLATE | | | | | | | X |
| | 1825F 1HR AC | PLATE | | | | | | | X |
| | 1825F 1HR AC. 1350F 2HRS AC | | | | | | X | | |
| | 1810F 1HR WQ. 1100F 8HRS AC | FORGING | X | | | | X | | |
| | 2000F. 0.5HR. AC | PLATE | | | | | | | X |
| Ti-6Al-2Zr-2Fe-3Al | STA REAGED AT 1100F 6HR | PLATE | X | | | | | | |
| | 1475F 1.5 HR. WQ. 1000F 8 HR. AC | EXTRUSION | Y | | | | | | |
| Ti-6* | STA-1740F 1 HR. AC. 1000F 8HR. AC | PLATE | X | | | | | | |
| | 1740F 1 HR. AC | PLATE | X | | | | | | |
| | ALPHA BETA FORGED | FORGING | | | | | | | X |

TABLE 4.0.2

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | L-T | | T-L | | S-L | | | |
|-----------|---|-----------------|--------------------------------------|--------------------------|--------------|--------------------------|--------------|--------------------------|--------------|------|------|
| | | | | SPECIMEN MEAN THICK * | STD. DEV. | SPECIMEN MEAN THICK * | STD. DEV. | SPECIMEN MEAN THICK * | STD. DEV. | | |
| BETA C | BTA | PLATE | 2.50 | 1.00 | 44.1 | 1.4 | 1.00 | 43.9 | 0.6 | --- | --- |
| BETA III | 1325F 925F 8HR | PLATE | 0.80 | 0.75 | 49.8 | 1.2 | --- | --- | --- | --- | --- |
| TI-6 | STA-1740F 1 HR. AC. 1000F 8HR. AC | PLATE | 0.62 | 0.62 | 59.3 | 1.9 | --- | --- | --- | --- | --- |
| | 1740F 1 HR. AC | PLATE | 0.62 | 0.63 | 61.6 | 1.6 | --- | --- | --- | --- | --- |
| TI-6AL-4V | AS FORGED-MA ALPHA-BETA FORGED. HILL ANNEALED | FORGING | 2.25 | --- | --- | --- | 1.00 | 39.4 | 2.7 | --- | --- |
| | ANNEALED | FORGING | 3.00 | 1.50 | 84.4 | 1.8 | 1.49 | 83.4 | 9.9 | --- | --- |
| | | EXTRUSION | 4.00 | --- | --- | --- | 1.63 | 93.3 | 2.3 | --- | --- |
| | | BILLET | 6.00 | 1.25 | 79.6 | 9.6 | --- | --- | --- | --- | --- |
| | ANNEALED 1000F 2 HR. AC | BILLET | 2.50 | 1.25 | 50.9 | 0.6 | --- | --- | --- | --- | --- |
| | ANNEALED 1300F 4 HR. AC | FORGING | 2.50 | 0.75 | 58.1 | 1.2 | 0.75 | 62.2 | 3.0 | 0.75 | 68.1 |
| | ANNEALED 1375F 3HR. AC | PLATE | 2.75 | 1.25 | 60.4 | 5.5 | --- | --- | --- | --- | --- |
| | AS RECEIVED | FORGED BAR | 1.00-3.90 | 0.96 | 57.1 | 10.4 | 0.90 | 54.9 | 10.8 | --- | --- |
| | B FORGED BETA FORGED REHEATED TO 1950F DRAWN TO SIZE. ANNEALED 1500F | FORGED BAR | 2.25 | --- | --- | --- | 1.00 | 42.6 | 4.3 | --- | --- |

* MINIMUM SPECIMEN THICKNESS (IN.)

TABLE 4.0.2 (Cont)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | K1C (KSI SQRT(IN)) | | L-T | | T-L | | S-L | | |
|--|--|-----------------|--------------------------------------|-----------------------|----------------------|---------------------|----------------------|---------------------|----------------------|---------------------|----------------------|-----|
| | | | | SPECIMEN THICK * | MEAN STD. DEV. | SPECIMEN THICK * | MEAN STD. DEV. | SPECIMEN THICK * | MEAN STD. DEV. | SPECIMEN THICK * | MEAN STD. DEV. | |
| TI-6AL-4V | B FORGED-NA BETA FORGED, MILL ANNEALED 1300F 2 HR, AC | FORGING | 2.00 | 1.00 | 70.6 | 4.9 | 1.00 | 71.0 | 0.4 | 1.00 | 73.9 | 2.9 |
| | | | 3.00 | 1.50 | 94.9 | 4.8 | --- | --- | --- | --- | --- | --- |
| | | | 1.00-3.50 | 0.98 | 68.2 | 9.7 | 0.68 | 64.2 | 11.8 | --- | --- | --- |
| | BETA PROCESSED MILL ANNEALED | PLATE | 1.00-1.50 | 1.24 | 55.6 | 1.3 | --- | --- | --- | --- | --- | --- |
| | | | 1.25-2.00 | --- | --- | --- | 1.25 | 100.6 | 6.8 | --- | --- | --- |
| | | | 1.90-4.00 | 1.47 | 83.5 | 3.1 | 1.50 | 87.5 | 4.1 | --- | --- | --- |
| | DIFFUSION BOND ANNEALED | BILLET | 2.00 | 1.00 | 47.7 | 2.9 | 1.00 | 49.5 | 3.9 | 1.00 | 43.6 | 5.8 |
| | | | 2.30 | 1.25 | 84.0 | 3.4 | --- | --- | --- | --- | --- | --- |
| | | | 1.00-2.50 | 1.13 | 82.8 | 7.8 | 1.00 | 80.8 | 10.8 | --- | --- | --- |
| | MILL ANNEAL MILL ANNEALED | EXTRUSION | 1.20-6.70 | 1.25 | 83.6 | 5.5 | 1.25 | 83.9 | 6.9 | 1.25 | 88.9 | 3.2 |
| | | | 0.62 | --- | --- | --- | 0.63 | 42.6 | 2.0 | --- | --- | --- |
| | | | 1.40 | 1.25 | 73.9 | 4.2 | 1.28 | 81.2 | 5.8 | --- | --- | --- |
| | RECRYSTALLIZE ANNEAL | FORGING | 3.00 | --- | --- | --- | 2.00 | 79.3 | 4.9 | --- | --- | --- |
| | | | 1.50 | --- | --- | --- | 1.50 | 91.5 | 2.1 | --- | --- | --- |
| | | | 1.50 | 1.50 | 71.8 | 3.2 | 1.50 | 91.6 | 1.3 | --- | --- | --- |
| STA 1700F 6 HR, AC, 1400F 6 HR, AC | PLATE | 0.62 | 0.63 | 41.4 | 2.3 | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| 1750F 1 HR, HQ, 1000F 4 HR | FORGING | 3.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| 1750F 1HR FC TO 1100F, AC | PLATE | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| 1750F 1HR, FC TO RT | PLATE | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| 1750F 2HR, HQ, 1000F 2HR, AC, 1300F 2HR, AC, STA | PLATE | 0.62 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |
| | | 1.50 | --- | --- | --- | --- | --- | --- | --- | --- | --- | |

* MINIMUM SPECIMEN THICKNESS (IN.)

TABLE 4.0.2 (Cont)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | K1C (KSI SQRT(IN)) | | | | | | | |
|----------------|--|-----------------|--------------------------------------|--------------------------|----------------------------|----------------------------|--------------------------|----------------------------|--------------------------|----------------------------|-----|
| | | | | L-T | T-L | B-L | | | | | |
| | | | | SPECIMEN MEAN THICK * | SPECIMEN MEAN STD. DEV. | SPECIMEN MEAN STD. DEV. | SPECIMEN MEAN THICK * | SPECIMEN MEAN STD. DEV. | SPECIMEN MEAN THICK * | SPECIMEN MEAN STD. DEV. | |
| TI-6AL-4V(ELI) | ANNEALED | FORGING | 3.00 | 2.00 | 83.5 | 1.3 | 2.01 | 84.3 | 0.4 | --- | --- |
| | RECRYSTALLIZE ANNEAL | PLATE | 3.00 | 2.00 | 76.1 | 4.0 | 2.00 | 76.8 | 0.7 | --- | --- |
| TI-6AL-6V-2SN | BETA ANNEAL 1810F 1 HR. AIRCOOL | PLATE | 0.50 | --- | --- | --- | 0.45 | 94.3 | 2.0 | --- | --- |
| | BETA ANNEAL & STDA-1800F 0.5HR.AC.1975F 0.5HR.WB.1050F 8 HR.AC | PLATE | 0.62 | 0.63 | 50.1 | 1.8 | --- | --- | --- | --- | --- |
| | DUPLEX ANNEAL | PLATE | 0.50 | --- | --- | --- | 0.50 | 65.1 | 2.0 | --- | --- |
| | MILL ANNEALED | PLATE | 0.50-1.00 | --- | --- | --- | 0.49 | 59.0 | 5.2 | --- | --- |
| | FORGING | FORGING | 3.80 | 1.00 | 98.6 | 2.7 | --- | --- | --- | --- | --- |
| | BILLET | BILLET | 2.20 | 1.24 | 52.3 | 6.4 | --- | --- | --- | --- | --- |
| | MILL ANNEALED 1000F 2 HR.AC | BILLET | 2.20 | 1.29 | 97.1 | 2.2 | --- | --- | --- | --- | --- |
| | STA-1600F 0.5HR.WB.1000F 6 HR.AC | FORGING | 3.80 | 1.01 | 30.8 | 0.7 | --- | --- | --- | --- | --- |
| | STA-1679F 0.25 HR.WB. 1100F 4 HR | PLATE | 1.25 | --- | --- | --- | 0.50 | 34.1 | 3.8 | --- | --- |
| | STDA-1700F 1 HR.WB.1400F 1 HR.AC | PLATE | 0.38 | 0.38 | 42.9 | 1.2 | 0.38 | 46.1 | 3.1 | --- | --- |
| | BILLET | BILLET | 12.00 | 1.02 | 62.8 | 6.9 | 1.02 | 97.0 | 3.7 | --- | --- |
| | STA-1600F 1100F 5 HR | PLATE | 1.00 | 1.00 | 54.0 | 1.0 | 0.99 | 93.9 | 1.0 | --- | --- |

* MINIMUM SPECIMEN THICKNESS (IN).

TABLE 4.0.2 (Cont)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/ HT | PRODUCT FORM | RANGE OF PRODUCT THICKNESSES (IN) | K _{IC} (KSI SQRT(IN)) | | | | | |
|-----------------|------------------|-----------------|--------------------------------------|-----------------------------------|--------------|--------------------------|--------------|--------------------------|--------------|
| | | | | L-T | T-L | S-L | | | |
| | | | | SPECIMEN MEAN THICK * | STD. DEV. | SPECIMEN MEAN THICK * | STD. DEV. | SPECIMEN MEAN THICK * | STD. DEV. |
| Ti6Al4V2Sn(ELI) | 1600F 1 HR. W.B. | PLATE | 1.00 | 0.29 | 29.8 | 0.5 | | | |
| | 1050F 4 HR. AC | | | | | | | | |
| | 1650F 1 HR. W.B. | PLATE | 1.00 | 0.29 | 34.0 | 3.5 | | | |

* MINIMUM SPECIMEN THICKNESS (IN.).

TABLE 4.0.3

PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS OF
TITANIUM ALLOYS (WITH BUCKLING CONSTRAINTS)

| Alloy | Condition/Mt | Test Temp. (°F) | Specimen Orient | Specimen Width (in.) | Yield Strength (ksi) | K_{IC}^0 (ksi/in) | | |
|-----------------|--------------|-----------------|-----------------|----------------------|----------------------|----------------------------------|----------------|-------|
| | | | | | | Specimen Thickness (in.) = 0.020 | 0.040 | 0.050 |
| Ti-6Al-2.5Sn | Annealed | -423 | L-T | 3.0 | 203 | 116.8/4.5 (5) | | |
| | | | | 6.0 | 203 | 109.4/6.6 (9) | | |
| | | | | 12.0 | 203 | 104.2/4.0 (8) | | |
| | | | | 16.0 | 203 | 97.3/9.6 (2) | | |
| | | | T-L | 12.0 | 210 | 107.7/16.0 (2) | 147.6/28.9 (2) | |
| Ti-6Al-4V | NA | R. T. | L-T | 24.0 | 136 | | 196.4/19.9 (6) | |
| | | -110 | T-L | 8.0 | 163 | | 159.4/7.5 (3) | |
| Ti-6Al-4V (ELI) | Annealed | R. T. | L-T | 18.0 | 136 | 161.6/6.3 (5) | | |
| Ti-6Al-1Mo-1V | D. A. | R. T. | L-T | 12.0 | 136 | 111.7/15.0(3) | | |
| | | | | 20.0 | 134 | | 220.5/15.8(4) | |

Mean/Standard Deviation (No. of Specimens)

TABLE 4.0.4.1

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR TITANIUM ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION: L-T ENVIRONMENT: LAB AIR AT R.T.
 STRESS RATIO: 0.00-0.10 FREQUENCY: 0.10-90.00KHZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) FOR DELTA K LEVELS (MSI SQRT(IN)) - | | |
|-------------------------------|-----------------------------|--------------|--------------|-------------|---|------|------|
| | | | | | 2.5 | 5.0 | 10.0 |
| TI-3AL-2.5BN | ANNEALED | SHEET | 0.10 | 30.00 | 11.6 | 124. | |
| | ANNEALED | SHEET | 0.10 | 50.00 | 11.7 | | |
| TI-6-2-4-6 | ----- | EXTRUSION | 0.10 | 20.00 | .619 | 9.70 | |
| | ANNEALED | BILLET | 0.02 | 10.00-20.00 | .270 | 9.49 | |
| TI-6AL-4V | ANNEALED AT 1375F. 3HRB. AC | PLATE | 0.02 | 10.00-20.00 | .263 | 9.70 | |
| | BA | FORGING | 0.02 | 10-20.00 | | 2.99 | 102. |
| BETA PROCESSED -HILL ANNEALED | | PLATE | 0.10 | 1.00 | | .917 | |
| | MA | PLATE | 0.02 | 10-30.00 | .0193 | 12.4 | |
| MA | MA | PLATE | 0.02 | 10-30.00 | | 8.92 | |
| | MA | PLATE | 0.04 | 20.00 | | 96.9 | |
| MA | MA | PLATE | 0.03 | 20.00 | | 6.97 | |
| | MA | FORGING | 0.02 | 1.00-30.00 | | 8.18 | 292. |
| MA | EXTRUSION | 0.10 | 1.00-20.00 | | 9.30 | 202. | |
| TI-6AL-4V(ELI) | ANNEALED | FORGING | 0.10 | 1.00-10.00 | | 12.9 | 204. |
| | BA | PLATE | 0.10 | 10.00 | | 10.6 | |

TABLE 4.0.4.1 (Cont)

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR TITANIUM ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION: L-T ENVIRONMENT: LAB AIR AT R. T.
 STRESS RATIO: 0.00-0.10 FREQUENCY: 0.10-50.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN./CYCLE) FOR DELTA K LEVELS (KSI SQRT(IN)) = | | |
|----------------|--------------|--------------|--------------|------------|--|------|------|
| | | | | | 2.5 | 5.0 | 10.0 |
| TI-6AL-6V-2SN | MA | EXTRUSION | 0.02 | 10-20.00 | 0440 | 620 | 7.73 |
| | --- | SHEET | 0.02 | 10-12.00 | | 2.28 | 13.9 |
| TI-6AL-11MO-1V | DA | SHEET | 0.00 | 1.00-30.00 | | | 144. |
| | DA | SHEET | 0.10 | 43.00 | | | 67.2 |
| | MA | SHEET | 0.10 | 43.00 | | | 246. |

TABLE 4.0.4.2

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR TITANIUM ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION: T-L ENVIRONMENT: LAB AIR AT N. Y.
 STRESS RATIO: 0.02-0.10 FREQUENCY: 0.10-53.30KHZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) FOR DELTA K LEVELS (KSI SQRT(IN)) - | | | | | |
|----------------|---|--------------|--------------|-------------|---|------|------|------|-------|-------|
| | | | | | 2.5 | 5.0 | 10.0 | 20.0 | 50.0 | 100.0 |
| TI-6AL-2.5ZN | ANNEALED | SHEET | 0.10 | 30.00-53.30 | | | 11.8 | | | |
| | ANNEALED | SHEET | 0.10 | 30.00 | | | 11.9 | 141. | | |
| TI-6AL-4V | AS WELDED E. B. WELDMENT (WELD ZONE) | WELDMENT | 0.10 | 10.00 | | | 5.94 | | | |
| | | WELDMENT | 0.10 | 10.00 | | | 6.52 | | | |
| | BA | FORGING | 0.02 | 10-20.00 | | | 2.27 | 103. | 3242. | |
| | | EXTRUSION | 0.10 | 3.00-20.00 | | | 13.7 | 281. | | |
| | RA | PLATE | 0.10 | 10.00 | | | 21.3 | | | |
| | STRESS RELIEVED E. B. WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 10-10.00 | | | 14.2 | 344. | | |
| WELDMENT | | 0.10 | 10-10.00 | | | 10.1 | | | | |
| TI-6AL-4V(ELI) | ANNEALED | FORGING | 0.10 | 1.00-20.00 | | | 11.9 | 171. | | |
| | RA | PLATE | 0.10 | 1.00-10.00 | | | 7.75 | 240. | | |

TABLE 4.0.4.3

COMPARISON OF FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS OF THE STRESS INTENSITY FACTOR FOR TITANIUM ALLOYS

TEST CONDITIONS:

SPECIMEN ORIENTATION: C-R

ENVIRONMENT: LAB AIR AT R. T.

STRESS RATIO: 0.03-0.10

FREQUENCY: 0.16-30.00HZ

| ALLOY | CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQUENCY | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | |
|---------------|---|--------------|--------------|-----------|---|------|------|
| | | | | | 2.5 | 5.0 | 10.0 |
| TI-6-2-4-2 | 1790F 1HR AC. | FORGING | 0.10 | .16 | | | 10.3 |
| | 1100F 8HRS AC | | | | | | |
| TI-6-2-4-6 | 1690F 2HRS AC. | FORGING | 0.10 | 30.00 | .109 | .985 | |
| | 1550F 2HRS OS. 1100F 8HRS AC | | | | | | |
| TI-6AL-4V | 1775F 1HR WQ. | DISK | 0.05 | .33-10.00 | | | 152. |
| | 1675F 1HR WQ. 1000F 4HRS AC. 900F 3HR | | | | | | |
| TI-6AL-1MD-IV | 1775F 1HR WQ. | DISK | 0.03 | .33-0.50 | | .843 | 1.0 |
| | 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | | | | | | |
| TI-6AL-1MD-IV | 1830F 1HR WQ. 1100F 8HRS AC | FORGING | 0.10 | 30.00 | .107 | 1.50 | |

TABLE 4.0.5

STRESS CORROSION CRACKING THRESHOLD DATA FOR TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/HT | PRODUCT FORM | SPECIMEN ORIENTATION | INDUSTRIAL ATMOSPHERE | ENVIRONMENTS | | | | K _{ISCC} (KSI $\sqrt{\text{in.}}$) | | |
|---------------|---|--------------|----------------------|-----------------------|---------------------|-----------------|-----------|-----------|---|------------------------|------|
| | | | | | SEACOAST ATMOSPHERE | SUMP TANK WATER | JP-4 FUEL | 3.5% NaCl | SHOP CLEANING SOLVENT | FIELD CLEANING SOLVENT | |
| Ti-6Al-4V | Alpha-Beta Forged | F | T-L | 27.0 | 18.0 | | | 27.0 | | | |
| | Beta Forged | F | T-L | 42.0 | 42.0 | | | 34.0 | | | |
| | Finish Rolled | P | T-S | | | | | 76.2(7) | | | |
| | GTA Weld Postweld 2HR (Heat Affected Zone) | P | L-T | | | 58.0 | | | | | |
| | Mill Annealed | P | L-S | | | | | 32.0 | | | |
| | RA | P | L-T | | | 59.3(7) | | | 69.0(2) | 70.0 | |
| | | F | T-L | | | 59.8(6) | | | | | |
| | | F | T-L | | | 53.0(2) | | | | | |
| | | F | S-L | | | 56.0(4) | | | | | |
| | | P | L-T | | | 66.0(2) | | | 69.0 | | 70.0 |
| | | | | | 55.2(5) | | | | | | |
| | 1700F 4HR FC TO 1400F AC Diffusion Bond Thermal Cycle | E | L-S | | | | | 60.0 | | | |
| | 1725F 1HR WQ, 1250F 4HR AC (STOA) | E | L-S | | | | | | 48.5(2) | | |
| | 1725F 1HR WQ, 1000F 1HR AC (STA) | F | L-T | | | 31.0 | 43.3 | | | | |
| | 1750F, 1010F 2HR AC | F | L-T | | | | | | | | |
| Ti-6Al-6V-2Sn | 1000F 2HR AC | F | L-T | | | | | | 30.5 | | |
| | 1300F 2HR AC | F | L-T | | | | | | 32.4 | | |
| | 1550F 1HR WQ | P | T-S | | | | | | 21.0 | | |
| | 900F 4HR AC | | | | | | | | | | |

TABLE 4.0.5 (Cont)

STRESS CORROSION CRACKING THRESHOLD DATA FOR TITANIUM ALLOYS AT ROOM TEMPERATURE

| ALLOY | CONDITION/HT | PRODUCT FORM | SPECIMEN ORIENTATION | ENVIRONMENTS | | | | K _{Isc} (Ksi $\sqrt{in.}$) | | FIELD CLEANING SOLVENT |
|---------------|--|--------------|----------------------|-----------------------|---------------------|-----------------|-----------|---|-----------------------|------------------------|
| | | | | INDUSTRIAL ATMOSPHERE | SEACOAST ATMOSPHERE | SUMP TANK WATER | JP-4 FUEL | 3.5% NaCl | SHOP CLEANING SOLVENT | |
| Ti-8Al-1Mo-IV | Mill Annealed | P | L-S T-S | | | | | 20.0 39.4(5) | | |
| | Mill Annealed | | | | | | | | | |
| | 1435F 8HR FC | P | T-S | | | | | 21.0 | | |
| | Vacuum Annealed | P | T-L | | | | | 24.3(3) | | |
| | 1520 1HR WQ | P | T-L | | | | | 21.4 | | |
| | 1675F 1HR AC, 1075F 8HR AC, 1000F 2HR AC | P | T-L | | | | | 26.4 | | |
| | 1700F 1HR AC 1200F 2HR WQ | P | T-S | | | | | 28.0 | | |
| | 1825F 1HR AC | P | T-S | | | | | 23.0 | | |
| | 2000F 0.5 HR AC | P | T-L | | | | | 47.3 | | |

TABLE 4.1.3.1

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.1.3.1 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | BETA TI | | | |
|----------------------------|----|-------------------------|----|----|--|
| CONDITION: BETA STABILIZED | | | | | |
| K MAX (KSI*IN**1/2) | A: | DA/DT (10**--3 IN/HOUR) | | | |
| | | B: | C: | D: | |
| | | E= 3.5% NAACL | | | |
| K MAX | B: | | | | |
| MIN | C: | | | | |
| | D: | | | | |
| | | 200.00 | | | |
| K MAX | A: | | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: BETA STABILIZED
 FORM: 0.1" TH SHEET
 SPECIMEN TYPE:
 ORIENTATION:
 YIELD STRENGTH: 136.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.180"
 SPECIMEN WIDTH: 8.000"
 CRACK LENGTH (A₀):
 K_{ISCC}: 68.00 KSI (SQRT IN)
 REFERENCES: 77458

TITAN.
 ALLOY

BETA TI

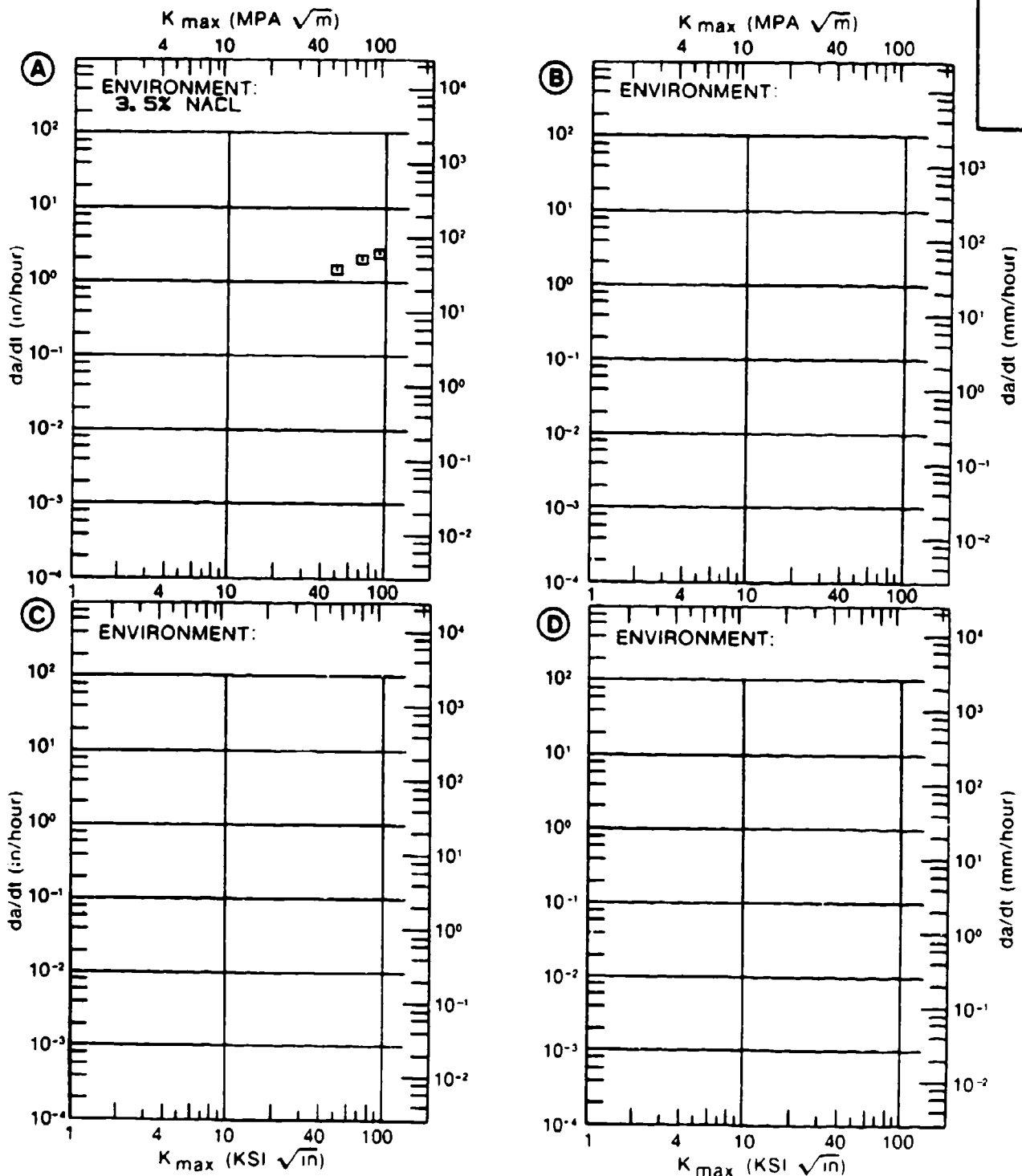


Figure 4.1.3.1

TABLE 4.1.3.2

| CONDITION | TITANIUM | | YIELD STR (KSI) | TEST TEMP OR (F) | ENVIRONMENT | BETA | | K(ISSC) | | STAN DEV | TEST TIME (MIN) | DATE REFER | | | | |
|-------------------------|----------|------------|-----------------|------------------|------------------|------------|------------|----------------------------------|-------|----------|-----------------|------------|-----|------|-------|-------|
| | FORM | THICK (IN) | | | | THICK (IN) | THICK (IN) | CRACK LENGTH K(I) (INSI) SORT IN | MEAN | | | | | | | |
| BETA STAR | S | 0.16 | R.T. | L-S | 136.0 | 3.9 | PCT NaCl | 8.000 | 0.140 | CNT | 72.00 | < 68.00* | 20 | 1969 | 77456 | |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, +1000MV | --- | --- | SENT | --- | SENT | 100.00 | 44.00 | --- | --- | 1970 | 82651 |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, -1000MV | --- | --- | SENT | --- | SENT | 100.00 | 55.00* | --- | --- | 1970 | 82651 |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, 0 MV | --- | --- | SENT | --- | SENT | 100.00 | 32.00 | --- | --- | 1970 | 82651 |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, +500MV | --- | --- | SENT | --- | SENT | 100.00 | 34.00 | --- | --- | 1970 | 82651 |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, -500MV | --- | --- | SENT | --- | SENT | 100.00 | 22.00 | --- | --- | 1970 | 82651 |
| 1745F W3 | S | --- | R.T. | --- | .6M KCL, -750MV | --- | --- | SENT | --- | SENT | 100.00 | 28.00 | --- | --- | 1970 | 82651 |
| 1745F W3, +1095F 61HR | S | --- | R.T. | --- | .6M KCL, -500MV | --- | --- | SENT | --- | SENT | 32.00 | 22.00 | --- | --- | 1970 | 82651 |
| 1745F W3, +1095F 1000HR | S | --- | R.T. | --- | .6M KCL, -500MV | --- | --- | SENT | --- | SENT | 8.00 | 8.00 | --- | --- | 1970 | 82651 |
| 1745F W3, +1095F 16HR | S | --- | R.T. | --- | .6M KCL, -900MV | --- | --- | SENT | --- | SENT | 60.00 | 26.00 | --- | --- | 1970 | 82651 |
| 1745F W3, +1095F 250HR | S | --- | R.T. | --- | .6M KCL, -500MV | --- | --- | SENT | --- | SENT | 22.00 | 16.00 | --- | --- | 1970 | 82651 |
| 1745F W3, +1095F 300HR | S | --- | R.T. | --- | .6M KCL, -500MV | --- | --- | SENT | --- | SENT | 8.00 | 8.00 | --- | --- | 1970 | 82651 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.3(K(ISSC/TYS)SQUARED

TABLE 4.2.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY BETA C AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|--------------|---|-----------------------|
| CONDITION/HT | L-I | I-I |
| STA | 44.1 ± 1.4 (3) | 43.9 ± 0.6 (2) |
| | | E-I |

TABLE 4.2.2.1

| CONDITION | TITANIUM | | | | | | | | | | K (IC) | K (IC) STAN MEAN DEV (KSI*SQRT IN) | DATE | REFER |
|-----------|-------------|------------|---------------|--------|----------------------|------------|------------|--------|-------------|---------------------|--------|--|-----------|-------|
| | --PRODUCT-- | | TEST SPECIMEN | | SPECIMEN | | CRACK | | 2.5* | | | | | |
| | FORM | THICK (IN) | THICK (IN) | ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | LENGTH (IN) | K (IC)/TYS)**2 (IN) | | | | |
| STA | P | 2.50 | 65 | I-T | --- | 1.993 | 1.001 | CT | 1.107 | 0.07 | 31.40 | 1974 | 88575 (1) | |
| | | 2.50 | | | --- | 2.002 | 1.000 | CT | 1.076 | 0.06 | 30.50 | 1974 | 88575 (1) | |
| | | 2.50 | | | --- | 1.988 | 0.978 | CT | 1.044 | 0.07 | 31.30 | 1974 | 88575 (1) | |
| | | | | | | | | | | | 31.1/ | 0.3 | | |
| STA | P | 2.50 | R.T. | I-T | 180.0 | 1.993 | 0.999 | CT | 1.042 | 0.15 | 43.80 | 1974 | 88575 | |
| | | 2.50 | | | 180.0 | 1.974 | 1.004 | CT | 1.074 | 0.14 | 42.80 | 1974 | 88575 | |
| | | 2.50 | | | 180.0 | 1.976 | 1.001 | CT | 1.090 | 0.16 | 45.60 | 1974 | 88575 | |
| STA | P | 2.50 | R.T. | T-L | 180.0 | 1.996 | 1.002 | CT | 1.047 | 0.14 | 43.40 | 1974 | 88575 | |
| | | 2.50 | | | 180.0 | 1.995 | 1.001 | CT | 1.041 | 0.15 | 44.30 | 1974 | 88575 | |

NOTES
(1) TYS APPROX 190

TABLE 4.2.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.2.3.1 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM BETA-C
CONDITION: STA
ENVIRONMENT: R. T. , DRY AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---------|---|---|
| | A | B | C | D |
| | R=+0.10 | R=+0.50 | | |
| A: 5.37 | .164 | | | |
| DELTA K B: | | | | |
| MIN C: | | | | |
| D: | | | | |
| 6.00 | .301 | | | |
| 7.00 | .624 | | | |
| 8.00 | 1.07 | | | |
| 9.00 | 1.62 | | | |
| 10.00 | 2.26 | | | |
| 13.00 | 4.56 | | | |
| 16.00 | 7.40 | | | |
| 20.00 | 12.3 | | | |
| 25.00 | 21.6 | | | |
| 30.00 | 37.1 | | | |
| 35.00 | 63.5 | | | |
| 40.00 | 110. | | | |
| A: 41.22 | 125. | | | |
| DELTA K B: | | | | |
| MAX C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 22.03 0.00
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: STA
 FORM: 0.13" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 8.00 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH: 187.7 KSI
 ULT. STRENGTH: 193.5 KSI
 SPECIMEN THK: 0.125- 0.126"
 SPECIMEN WIDTH: 8.002- 8.028"
 REFERENCES: 98575

TITAN.
ALLOY

BETA-C

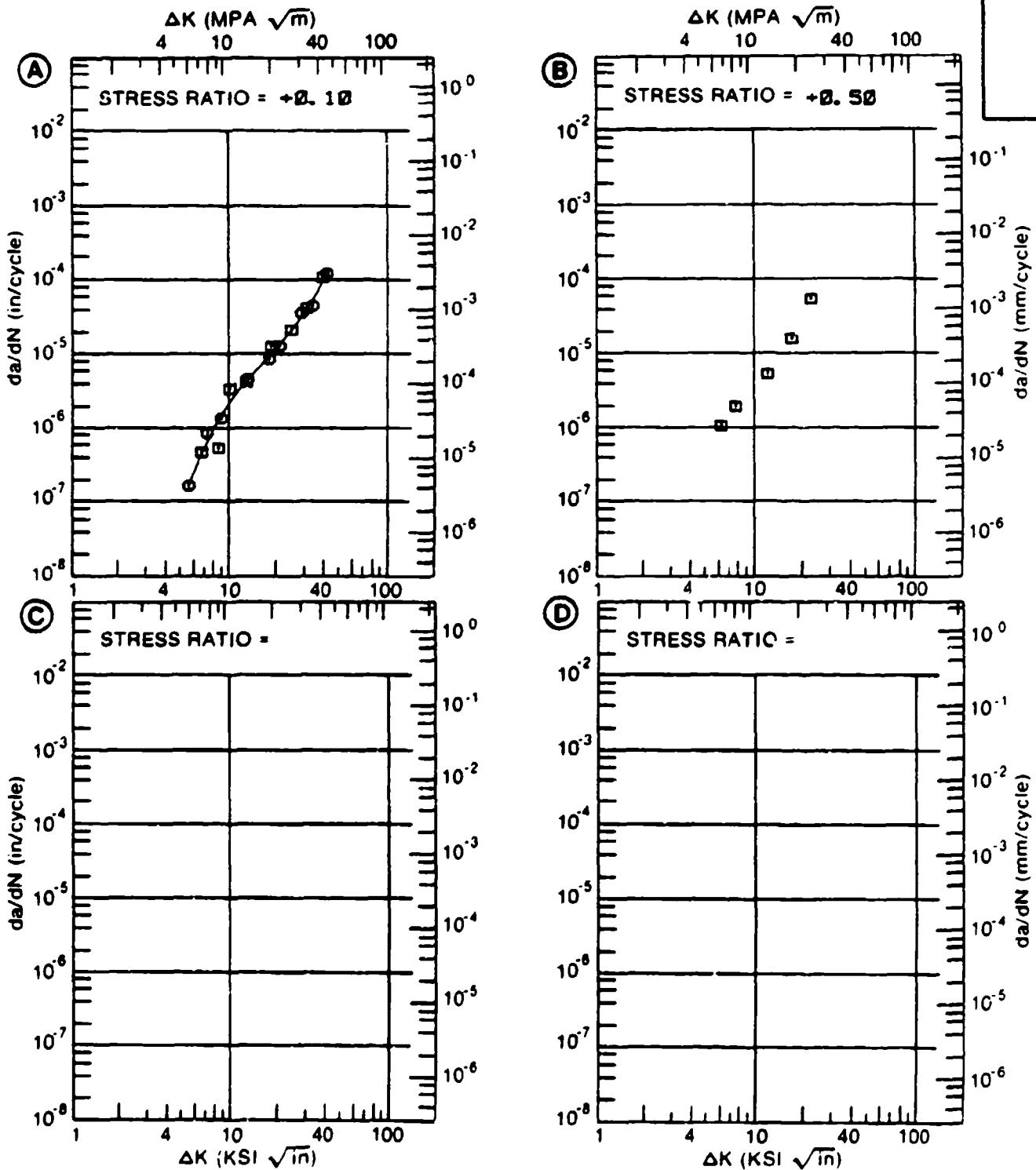


Figure 4.2.3.1

TABLE 4.2.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.2.3.2 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM BETA-C
CONDITION: STA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K | A: 6.58 | .805 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 7.00 | 1.03 | | | |
| | 8.00 | 1.67 | | | |
| | 9.00 | 2.45 | | | |
| | 10.00 | 3.35 | | | |
| | 13.00 | 6.72 | | | |
| | 16.00 | 11.3 | | | |
| | 20.00 | 20.2 | | | |
| | 25.00 | 39.4 | | | |
| | 30.00 | 75.1 | | | |
| | 35.00 | 143. | | | |
| | 40.00 | 271. | | | |
| DELTA K | A: 42.90 | 394. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 29.18 0.00
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 4
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: STA
 FORM: 0.12- 0.13" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 0.10- 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 107.7 KSI
 ULT. STRENGTH: 183.5 KSI
 SPECIMEN THK: 0.116- 0.127"
 SPECIMEN WIDTH: 6.002- 6.023"
 REFERENCES: 09575

TITAN.
ALLOY

BETA-C

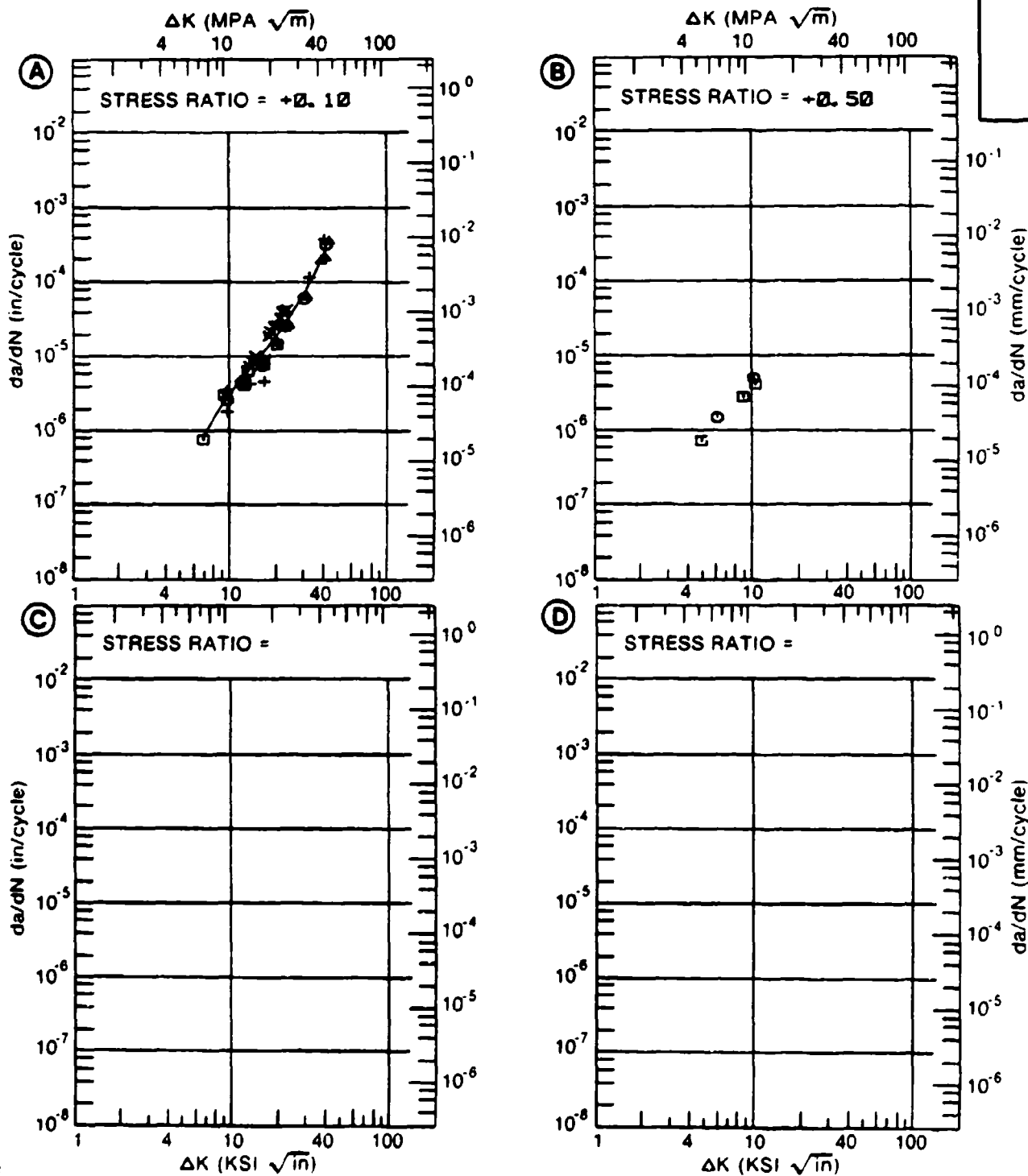


Figure 4.2.3.2

TABLE 4.2.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.2.3.3 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM BETA-C
CONDITION: STA
ENVIRONMENT: R. T. , S. T. W.

DELTA K
(KSI*IN**1/2)

DA/DN (10**-6 IN. /CYCLE)

A B C D

R=+0.10

DELTA K A:
MIN B:
 C:
 D:

200.00

DELTA K A:
MAX B:
 C:
 D:

ROOT MEAN SQUARE
PERCENT ERROR

0.00

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: STA
 FORM: 0.13" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 167.7 KSI
 ULT. STRENGTH: 183.5 KSI
 SPECIMEN THK: 0.127"
 SPECIMEN WIDTH: 6.009"
 REFERENCES: 89575

TITAN.
ALLOY

BETA-C

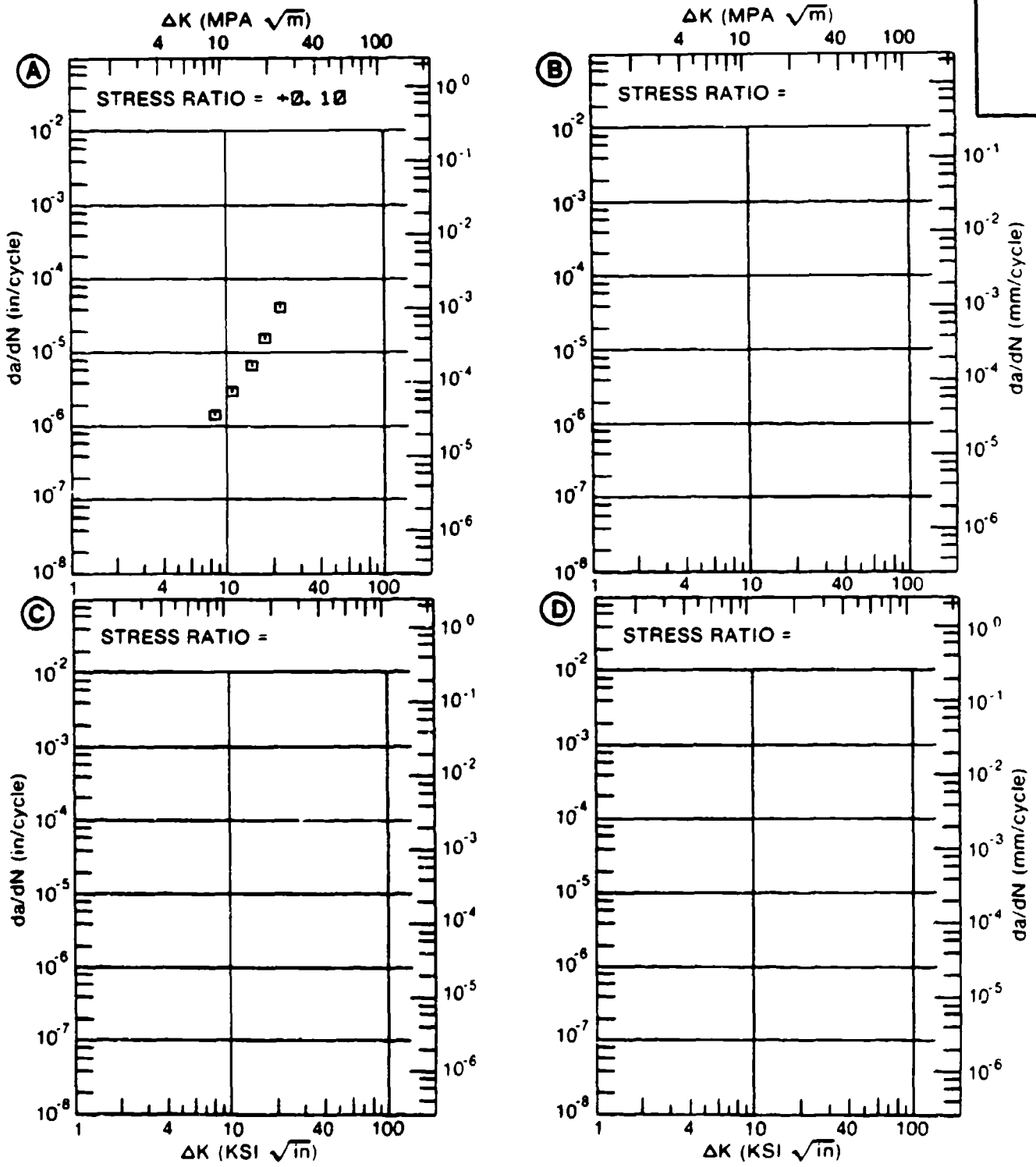


Figure 4.2.3.3

TABLE 4.3.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY BETA III AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|----------------------------|---|-----------------------|
| CONDITION/HT | L-I | L-I |
| 1325F 25HR. NR 925F 8HR | 49.8 ± 1.2 (3) | ----- |
| | | L-I |

TABLE 4.3.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM BETA III

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT AIR AT 175 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--|--------------|--------------|------------|-------------------------------|---|
| | | | | 2 5 5 10 20 50 100 | |
| STA | PLATE | 0.10 | 0.10-10.00 | | 110 |
| STA. F B WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 0.10-10.00 | | 97.2 |

TABLE 4.3.2.1

| CONDITION | TITANIUM | | BETA III | | K(IIC) | | K(IIC) STAN K(IIC) MEAN DEV (KSI*SQRT IN) | DATE | REFER | | | | |
|-------------------------------|----------------|-------------------------|---------------------------------|-----------|-----------|-----------|---|------|-------|------|-------|------|-------------|
| | YIELD (KSI) | CRACK LENGTH (IN) | 2.5" CRACK LENGTH (IN) | W (IN) | B (IN) | A (IN) | | | | | | | |
| STA-1325F WG.1045F BWR | P | 1.00 | R.T. | T-L | 150.0 | 2.000 | 0.991 | CT | 0.917 | 0.17 | 42.20 | 1973 | 193144 |
| STA-1325F WG.1045F BWR | P | 1.00 | R.T. | T-L | 150.0 | 2.000 | 0.996 | CT | 0.930 | 0.35 | 76.30 | 1973 | 88144 |
| STA-1325F WG.1045F B WR | P | 1.00 | R.T. | T-L | 150.0 | 2.000 | 1.005 | CT | 0.977 | 0.67 | 83.70 | 1973 | 88144 |
| 1325F 204R. W0 204F BWR | P | 0.80 | R.T. | L-T | 186.0 | 1.504 | 0.750 | CT | 0.763 | 0.17 | 48.40 | 1974 | 91793 |
| | | 0.60 | | | 186.0 | 1.503 | 0.750 | CT | 0.795 | 0.18 | 50.50 | 1974 | 91793 |
| | | 0.80 | | | 186.0 | 1.502 | 0.750 | CT | 0.775 | 0.18 | 50.40 | 1974 | 91793 |
| 1325F WG.950F BWR. AC | E | 3.00 | R.T. | C-R | 178.0 | 1.459 | 0.750 | CT | 0.773 | 0.24 | 55.20 | 1973 | 87230 (1) |
| | | 3.00 | | | 178.0 | 1.479 | 0.750 | CT | 0.789 | 0.26 | 56.80 | 1973 | 87230 (1) |
| | | 3.00 | | | 178.0 | 1.499 | 0.751 | CT | 0.790 | 0.23 | 53.20 | 1973 | 87230 (1) |

NOTES
(1) ALPHA PRECIPITATE IN BETA MATRIX
STRAIGHTNESS OF CRACK FRONT MAY NOT MEET ASTM E399-72 REQUIREMENTS

TABLE 4.3.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.3.3.1 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: TITANIUM | | BETA III | | | |
|--------------------------|----------|--------------------------|----------|---|---|
| CONDITION: STA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E=- 65F | E=+ 175F | | |
| | | AIR | AIR | | |
| DELTA K | A: 26.74 | 28.9 | | | |
| MIN | B: 20.02 | | 10.1 | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | | 19.1 | | |
| | 30.00 | 34.0 | 31.8 | | |
| | 35.00 | 41.6 | 47.8 | | |
| | 40.00 | 52.2 | 66.7 | | |
| | 50.00 | 100. | 110. | | |
| | 60.00 | 260. | | | |
| DELTA K | A: 68.42 | 291. | | | |
| MAX | B: 58.85 | | 149. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 23.87 | 5.19 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: STA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 88144

TITAN.
ALLOY

BETA III

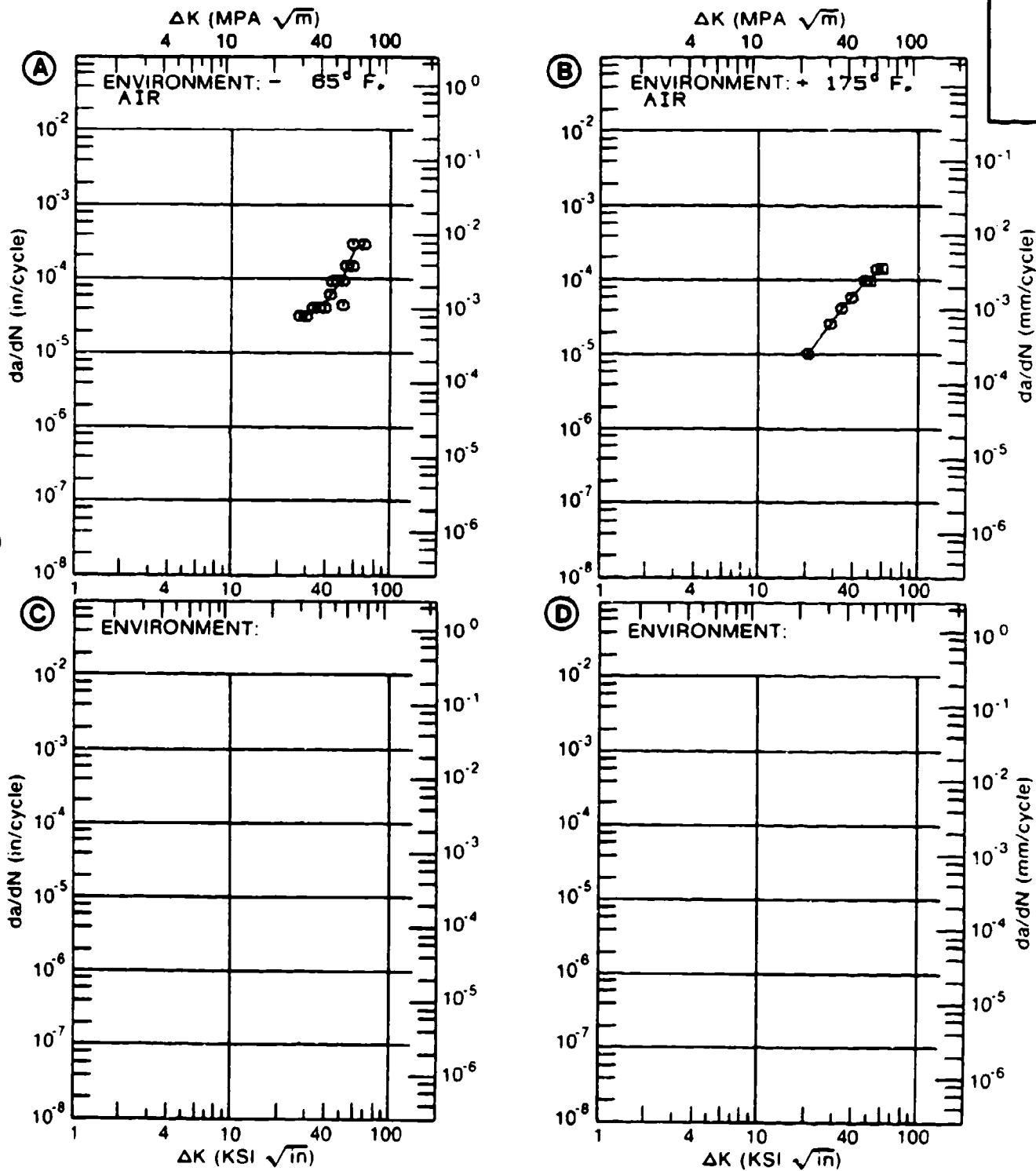


Figure 4.3.3.1

TABLE 4.3.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.3.3.2 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | BETA III | | | |
|--|--|--------------------------------------|---|---|---|
| CONDITION: STA. E. B. WELDMENT (WELD ZONE) | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | LAB AIR | | | |
| DELTA K MIN | A: B: C: D: | | | | |
| | 200.00 | | | | |
| DELTA K MAX | A: B: C: D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 0.00 | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: STA. E. B. WELDMENT (WELD ZONE)

FORM: 1.00" TH WELDMENT

SPECIMEN TYPE: CT

ORIENTATION: T-L

STRESS RATIO: +0.10

FREQUENCY: 10.00 HZ

YIELD STRENGTH:

ULT. STRENGTH:

SPECIMEN THK: 1.000"

SPECIMEN WIDTH: 2.550"

REFERENCES: 88144

TITAN.
ALLOY

BETA III

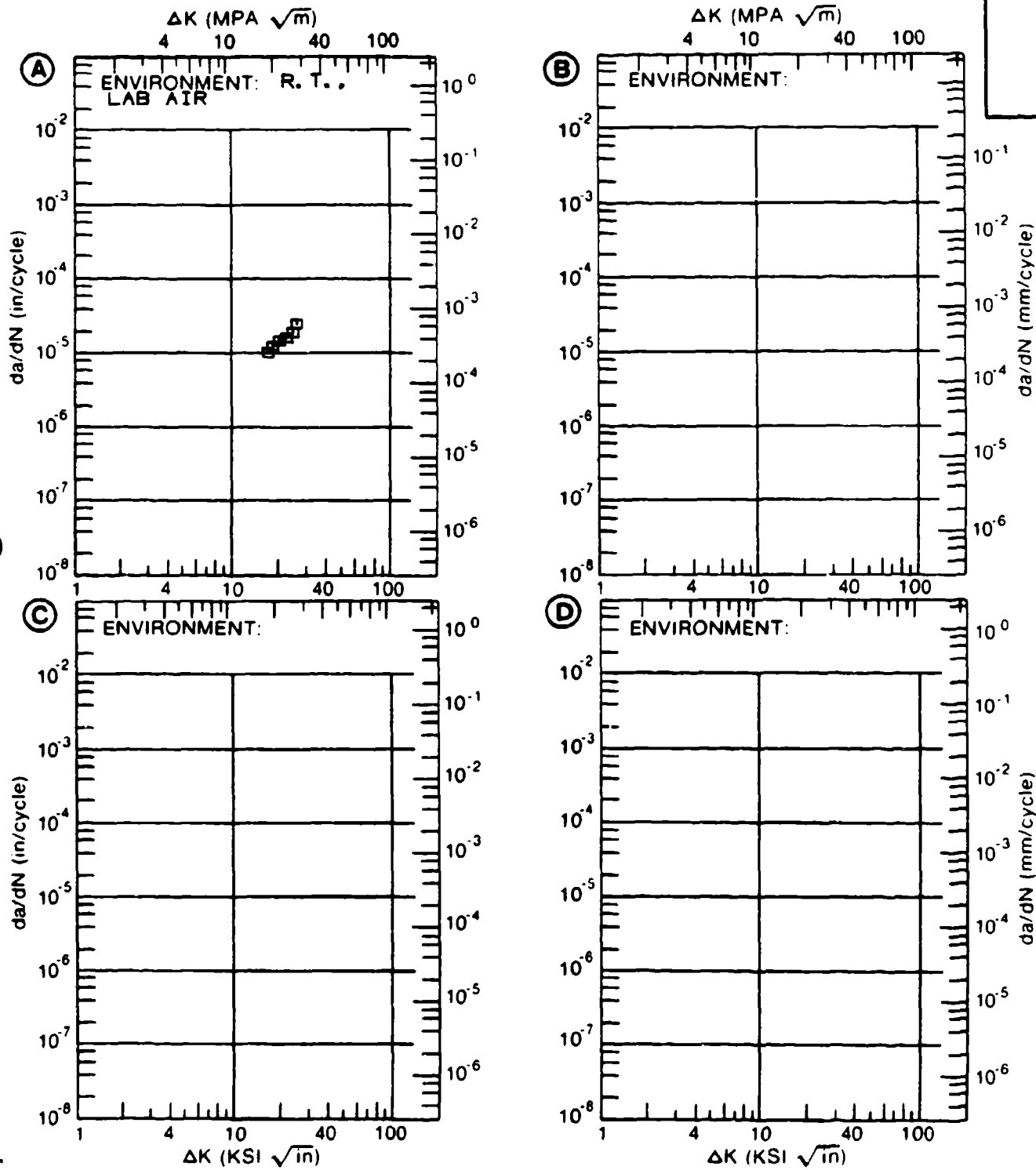


Figure 4.3.3.2

TABLE 4.3.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.3.3.3 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | BETA III | | | |
|---|----------|--------------------------------------|---|---|---|
| CONDITION: STA, E. B. WELDMENT (HEAT AFFECTED ZONE) | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E=+ 175F | | | |
| | | : AIR | | | |
| DELTA K | A: 24.74 | : 12.8 | | | |
| MIN | B: | : | | | |
| | C: | : | | | |
| | D: | : | | | |
| | 25.00 | : 13.2 | | | |
| | 30.00 | : 23.2 | | | |
| | 35.00 | : 35.2 | | | |
| | 40.00 | : 50.1 | | | |
| | 50.00 | : 97.2 | | | |
| DELTA K | A: 58.23 | : 171. | | | |
| MAX | B: | : | | | |
| | C: | : | | | |
| | D: | : | | | |
| ROOT MEAN SQUARE | | 9.56 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: STA. E.B. WELDMENT (HEAT AFFECTED ZONE)

FORM: 1.00" TH WELDMENT

SPECIMEN TYPE: CT

ORIENTATION: T-L

STRESS RATIO: +0.10

FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:

ULT. STRENGTH:

SPECIMEN THK: 1.000"

SPECIMEN WIDTH: 2.550"

REFERENCES: 08144

TITAN.
ALLOY

BETA III

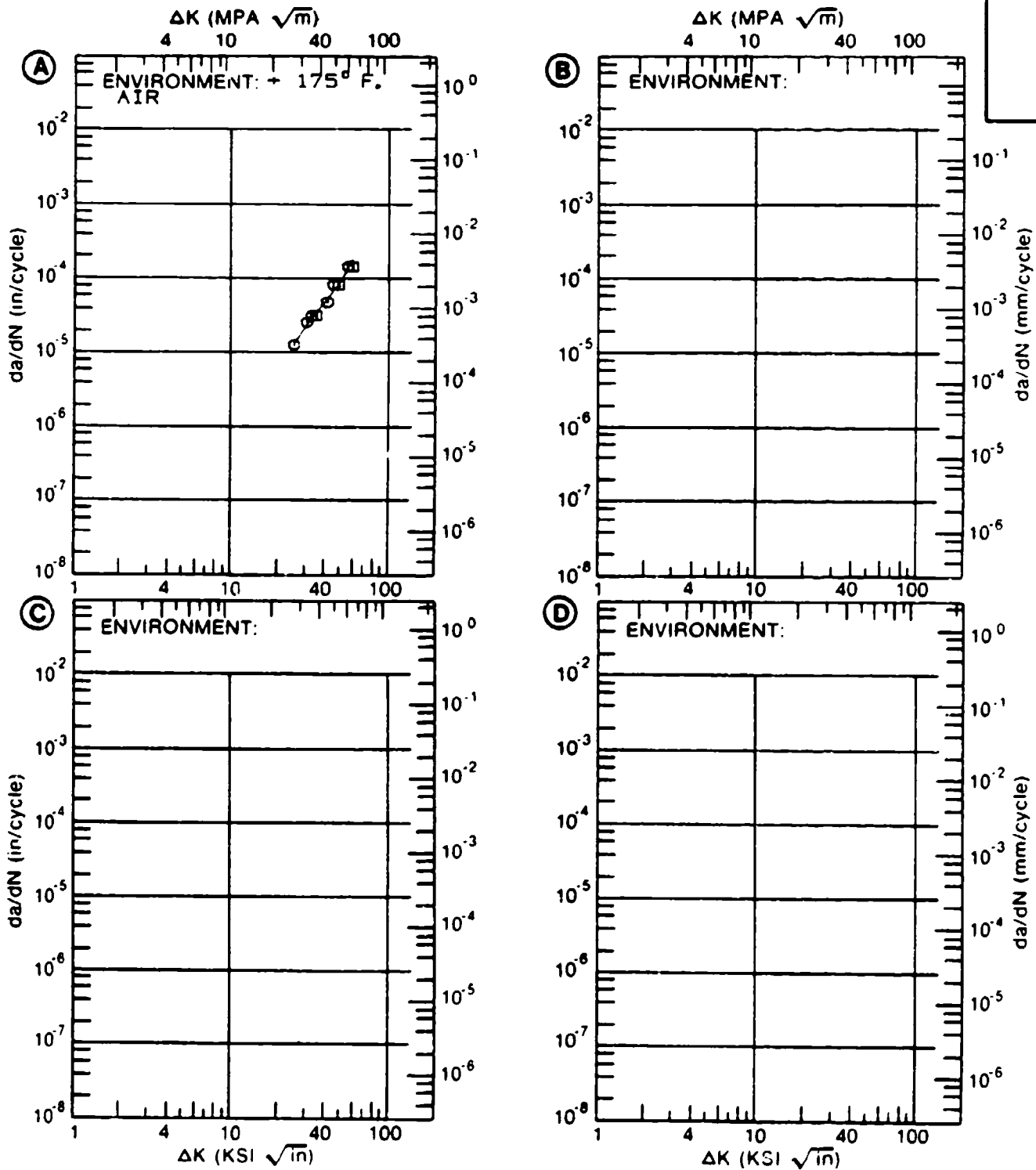


Figure 4.3.3.3

TABLE 4.3.3.4

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.3.3.4 INDICATING EFFECT

OF CONDITION

| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
|------------------------|----------|------------------------------------|----------------------------|---------------------------|---|
| | | A | B | C | D |
| | | C= AGED 900F 100HRS | C= AGED 1000F 100HRS | C= AGED 1250F 50HRS | |
| K MAX MIN | A: 15.50 | 40051. | | | |
| | B: 23.00 | | 11709. | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 40305. | | | |
| | 20.00 | 41048. | | | |
| | 25.00 | 40606. | 13521. | | |
| | 30.00 | 40032. | 15835. | | |
| 35.00 | 39804. | 16116. | | | |
| 40.00 | 40045. | 15677. | | | |
| 50.00 | 41973. | 15093. | | | |
| 60.00 | | 16211. | | | |
| 70.00 | | 19830. | | | |
| K MAX MAX | A: 59.50 | 45536. | | | |
| | B: 80.00 | | 27367. | | |
| | C: | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 8.50 | 6.09 | 0.00 | |
| PERCENT ERROR | | | | | |

CONDITION/HT:
 ENVIRONMENT: R. T., 0. 6M KCL
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 82851

TITAN.
 ALLOY
 BETA III

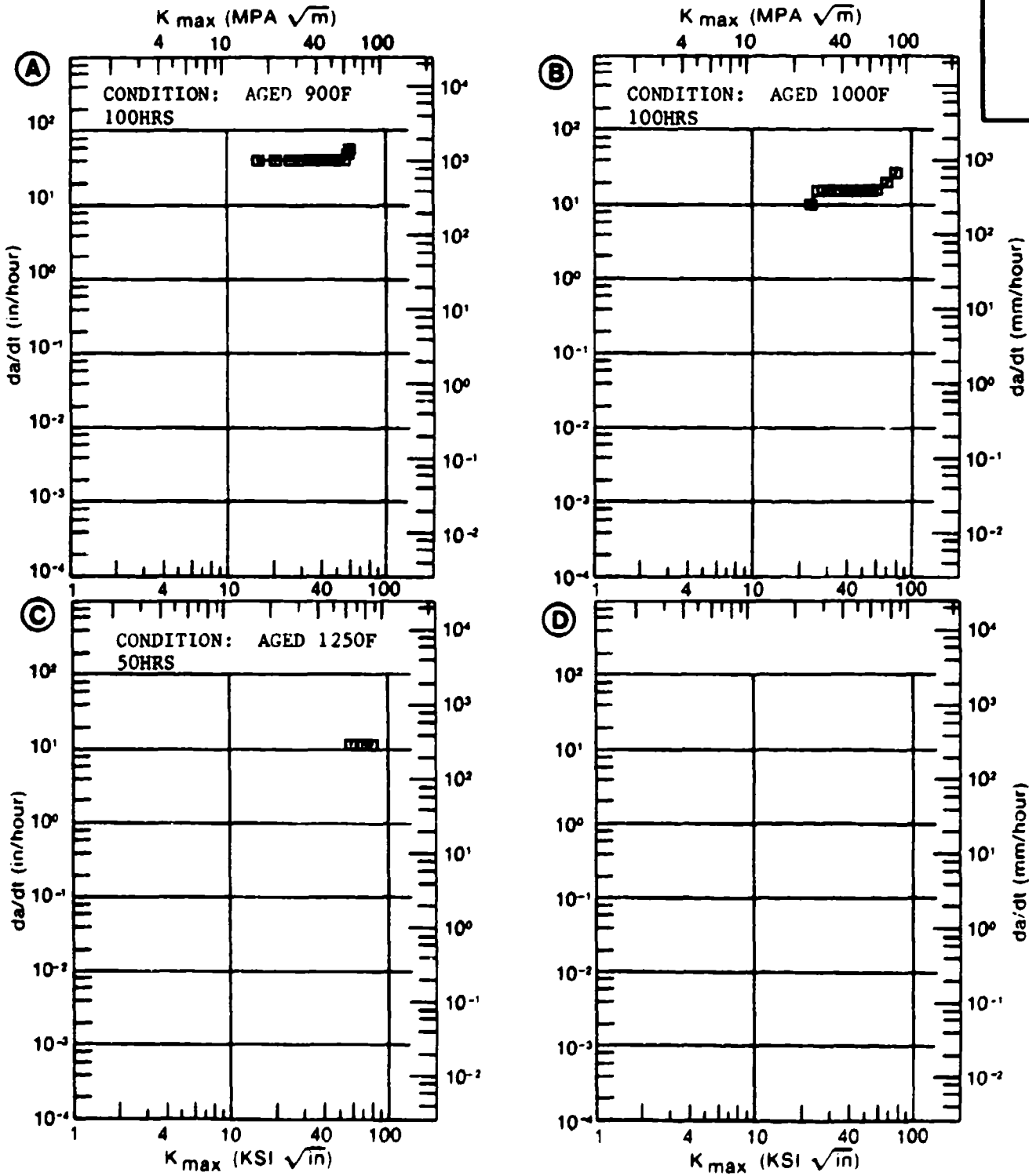


Figure 4.3.3.4

TABLE 4.3.3.5

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.3.3.5 INDICATING EFFECT
OF CONDITION

| MATERIAL: TITANIUM | | BETA III | | | |
|------------------------|----------|--------------------------|---------------------|----------------------|-------|
| ENVIRONMENT: 0.6M KCL | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | C= STA 900F 100HRS | C= STA 900F 8HRS | C= STA 900F 40HRS | |
| K MAX MIN | A: 15.00 | 35940. | | | |
| | B: | | | | |
| | C: 25.50 | | | 2144. | |
| | D: | | | | |
| | 16.00 | 36148. | | | |
| | 20.00 | 36335. | | | |
| | 25.00 | 36035. | | | |
| | 30.00 | 35746. | | | 3216. |
| 35.00 | 35668. | | | 4046. | |
| 40.00 | 35843. | | | 4457. | |
| 50.00 | 36930. | | | 4444. | |
| K MAX MAX | A: 56.00 | 38016. | | | |
| | B: | | | | |
| | C: 55.00 | | | 4234. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 7.67 | 0.00 | 6.13 | |
| PERCENT ERROR | | | | | |

CONDITION/HT:
 ENVIRONMENT: 0.8M KCL
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 82851

TITAN.
 ALLOY
 BETA II

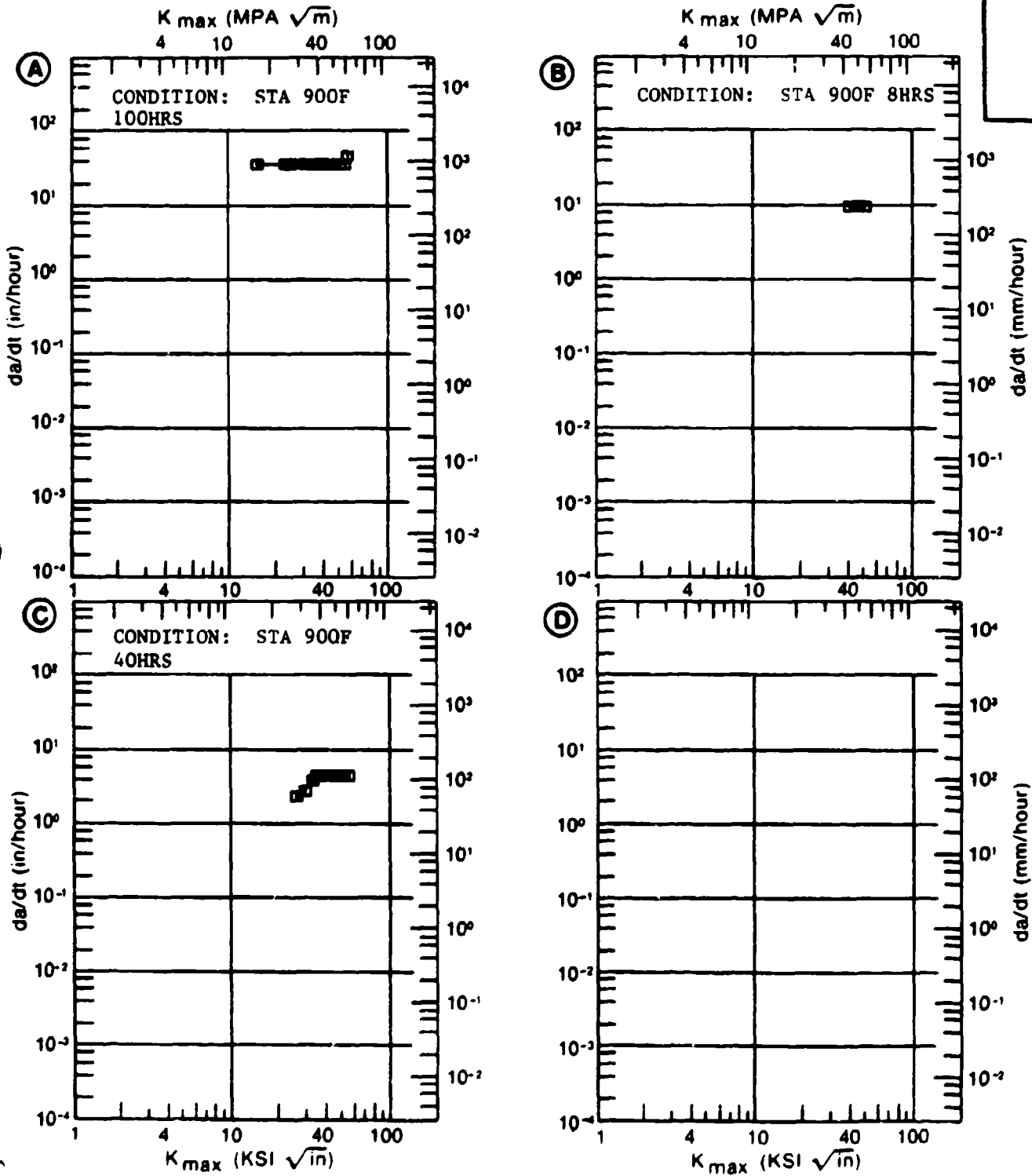


Figure 4.3.3.5

TABLE 4.3.3.6

| CONDITION | --PRODUCT-- FORM | THICK (IN) | TEST TEMP (F) | SPEC YIELD OR STR (KSI) | ENVIRONMENT | TITANIUM | | BETA III | | K(ISSC) | | MEAN | STAN DEV | TEST TIME (MIN) | DATE | PEFER |
|-----------------------------|---------------------|---------------|------------------|-------------------------------|---------------------|---------------|-------------------|----------------|----------------|------------------|-------|--------|-------------|-----------------------|------|-------|
| | | | | | | WIDTH (IN) | THICKNESS (IN) | DESIGN (IN) | LENGTH (IN) | CRACK K(ISSC) | | | | | | |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, -1500MV | --- | SENT | --- | SENT | --- | 65.00 | 55.00* | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, -1000MV | --- | BENT | --- | BENT | --- | 65.00 | 28.00 | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, +1000MV | --- | SENT | --- | SENT | --- | 65.00 | 25.00 | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, 0MV | --- | BENT | --- | BENT | --- | 65.00 | 21.00 | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, +900MV | --- | SENT | --- | SENT | --- | 65.00 | 24.00 | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, -500MV | --- | SENT | --- | SENT | --- | 65.00 | 14.00 | --- | --- | 1970 | 82651 |
| BETA STAB +AGED 900F 1HR | S | --- | R. T. | --- | .6M KCL, -750MV | --- | SENT | --- | SENT | --- | 65.00 | 16.00 | --- | --- | 1970 | 82651 |

*NOTE - DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KISSC/TYS) SQUARED

TABLE 4.4.2.1

| (CONDITION) | TITANIUM | | TEST SPECIMEN ORIENT | YIELD STRENGTH (KSI) | CORDON 9 | | K(KIC) | CRACK LENGTH (IN) | 2.5 ^o CRACK LENGTH (K(KIC)/TYS) ^{0.25} (IN) | K(KIC) MEAN DEV (KSI ^{0.25} BORT IN) | K(KIC) STAN | DATE | REFER |
|---------------------------------------|-----------------|------------|----------------------|----------------------|------------|------------|--------|-------------------|---|---|-------------|------|-------|
| | FORN THICK (IN) | THICK (IN) | | | WIDTH (IN) | THICK (IN) | | | | | | | |
| ALPHA-BETA FORGED & LOW ANNEAL. & AGE | F | 2.00 | R.T | 136.3 | M | 2.000 | 0.57 | 64.84 | | | | | RIOUS |

TABLE 4.5.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY TI-6 AT ROOM TEMPERATURE

| CONDITION/MT | MEAN K _{IC} ± STANDARD DEVIATION | | PLATE |
|---|---|-------|-------|
| | (KSI) | (MPa) | |
| STA-1740F 1 HR. AC. 1000F 8HR. AC | 55.3 ± 1.5 (3) | --- | PL |
| 1740F 1 HR. AC | 61.6 ± 1.6 (3) | --- | --- |

TABLE 4.5.2.1

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT | THICK (IN) | TEMP (F) | SPECIMEN | | DESIGN | CRACK LENGTH (IN) | K(1C) (KSI/RT IN) | K(1C) MEAN DEV (KSI/RT IN) | K(1C) BTM | DATE | REFER |
|-----------------|----------|-------|----------------------|----------------------|------------|----------|------------|------------|--------|-------------------|-------------------|----------------------------|-----------|-----------|-------|
| | TI-9 | K(1C) | | | | | WIDTH (IN) | THICK (IN) | | | | | | | |
| | | | | | M | B | | | | | | | | | |
| STA-1740F | P | | 157.0 | R.T. | 0.62 | L-T | 2.000 | 0.624 | CT | 1.000 | 57.00 | | 1974 | 88186 (1) | |
| 1 HR. AC. 100HF | | | 157.0 | | 0.62 | | 2.000 | 0.625 | CT | 1.000 | 54.70 | | 1974 | 88186 (1) | |
| RWP. AC | | | 157.0 | | 0.62 | | 2.000 | 0.625 | CT | 1.000 | 54.30 | 35.3/ | 1974 | 88186 (1) | |
| | | | | | | | | | | | | 1.5 | | | |
| 1740F 1 HR. AC | P | | 148.0 | R.T. | 0.62 | L-T | 2.000 | 0.626 | CT | 1.000 | 62.00 | | 1974 | 88186 (1) | |
| | | | 148.0 | | 0.62 | | 2.000 | 0.625 | CT | 1.000 | 62.90 | | 1974 | 88186 (1) | |
| | | | 148.0 | | 0.62 | | 2.000 | 0.625 | CT | 1.000 | 59.60 | 61.6/ | 1974 | 88186 (1) | |
| | | | | | | | | | | | | 1.6 | | | |

UNITS
(1) * - GAL - 27R - 2HO - 2CR - 0.2591

TABLE 4.6.3.1

| TITANIUM | | TI-4AL-3MO-1V | | K(I18CC) | | | | | | | | | |
|-----------------|-----------------------------------|-----------------------------|-----------------------|---------------|--------------------|----------------------------------|---------------------------|----------------------|-----------------------|-----|------|-----------------------|---------------|
| CONDITION | --PRODUCT-- FORM THICK (IN) | TEST SPEC TEMP OR (F) | YIELD STR (KSI) | ENVIRONMENT | WIDTH (IN) W | THICK DESIGN (IN) (P-SG) B | CRACK LENGTH (IN) A | K(I18CC) K(I18CC) | MEAN (K1818QRT IN) | DEV | BTAN | TEST TIME (MIN) | DATE REFER |
| HILL ANNEALFD P | 0.50 | R.T. | L-S | 3.5 PCT NACl. | | | | 117.00 | 105.00* | | | | 1969 75386 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.3(K18CC/TY8)SQUARED

TABLE 4.7.1.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-SAL-2 35N

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: DRY ARGON
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-------------------------------|-----|------|------|------|------|-----|---|
| ANNEALED | SHEET | 0.10 | 30 00 | | | | | 5.96 | 94.7 | | |
| ANNEALED | SHEET | 0.10 | 50 00 | | | | | 4.77 | | | |
| ANNEALED | SHEET | 0.67 | 55 00-98 30 | | | 0.03 | 0.27 | | | | |

TABLE 4.7.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-5AL-2.5SN

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | 5 | 10 | 20 | 30 | 100 |
|--------------|--------------|--------------|-------------|--------------------------------|------|------|------|-----|-----|
| ANNEALED | SHEET | 0.10 | 30.00 | | | | 11.6 | 124 | |
| ANNEALED | SHEET | 0.10 | 50.00 | | | | 11.7 | | |
| ANNEALED | SHEET | 0.67 | 55.00-58.00 | | 0.15 | 2.13 | | | |

TABLE 4.7.1.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-5AL-2.5SN

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT 3.5% NaCl AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-----------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| ANNEALED | SHEET | 0.10 | 30.00 | | 30.2 157 |
| ANNEALED | SHEET | 0.10 | 50.00 | | 23.5 |
| ANNEALED | SHEET | 0.67 | 55.00-58.30 | | 0.29 7.97 |

TABLE 4.7.1.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM T1-SAL-2 35N

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT DRY ARGON AT R. T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-------------------------------|---|
| ANNEALED | SHEET | 0.10 | 30.00 | 2.5 5 10 20 50 100 | 9.38 114 |
| ANNEALED | SHEET | 0.10 | 50 00-53 30 | | 3.35 |
| ANNEALED | SHEET | 0.67 | 54 20-58 30 | | 0.49 |

TABLE 4.7.1.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM T1-5AL-2.5Sn

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: LAB AIR AT R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| ANNEALED | SHEET | 0.10 | 30.00 | | 11.9 141 |
| ANNEALED | SHEET | 0.10 | 50.00-53.30 | | 11.8 |
| ANNEALED | SHEET | 0.67 | 54.20-98.30 | | 0.15 3.08 |

TABLE 4.7.1.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-5AL-2.5Sn

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: DIST H₂O
AT R. T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-------------|-------------------------------|-----|------|------|------|-----|-----|
| ANNEALED | SHEET | 0.10 | 30.00 | | | | | 12.5 | 130 | |
| ANNEALED | SHEET | 0.10 | 50.00-53.30 | | | | | 12.0 | | |
| ANNEALED | SHEET | 0.67 | 34.20-36.30 | | | 0.36 | 3.72 | | | |

TABLE 4.7.1.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-5AL-2.5SN

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT 3.5% NaCl AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATE (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|-------------------------------|-----|---|------|------|----|-----|--|
| ANNEALED | SHEET | 0.10 | 30.00 | | | | | | | | 176 |
| ANNEALED | SHEET | 0.10 | 50.00-53.30 | | | | | | | | 24.5 |
| ANNEALED | SHEET | 0.67 | 54.20-58.30 | | | | 0.98 | 1.46 | | | |

TABLE 4.7.2.1

| TITANIUM | | 11-3AL-2.5BN | | K(C) | | | | | | |
|-----------|---|--------------------------|---------------------------|---------------|---------------------|-------------------------------------|--|--|------------|--------------------------|
| CONDITION | --PRODUCT-- FORM THICK TEMP OR STR (IN) (F) | TEST SPEC YIELD (KSI) | CRACK LENGTH CROSS STRESS | | | | K(I) STAN MEAN DEV (KBI*SQRT IN) | K(C) STAN MEAN DEV (KBI*SQRT IN) | REFER | |
| | | | WIDTH (IN) | THICK (IN) | INIT 2A(D) 2A(F) | FINAL ONSET (KSI) B(D) S(MAX) | | | | MAX (KSI) B(D) S(MAX) |
| ANNEALED | S | 0 02 - 423 L-T | 203.5 | 0.018 | 0.500 | 110.10 | 99.28 | 111.85 | 1967 68968 | |
| | | | 203.5 | 0.019 | 1.040 | 1.300 | 69.00 | 75.34 | 1967 68968 | |
| | | | 203.5 | 0.019 | 0.150 | 0.270 | 169.40 | 80.41* | 108.26* | 1967 68968 |
| | | | 203.5 | 0.019 | 1.000 | --- | 69.50 | 93.33 | --- | 1967 68968 |
| | | | 203.5 | 0.019 | 1.240 | --- | 72.20 | 98.51 | --- | 1967 68968 |
| | | | 203.5 | 0.019 | 0.320 | 0.500 | 129.90 | 92.75 | 117.13 | 1967 68968 |
| | | | 203.5 | 0.019 | 0.340 | 0.670 | 127.90 | 94.22 | 135.40* | 1967 68968 |
| | | | 203.5 | 0.019 | 0.120 | 0.300 | 181.00 | 78.64* | 123.02* | 1967 68968 |
| | | | 203.5 | 0.019 | 0.340 | 0.810 | 103.60 | 97.37 | 122.41 | 1967 68968 |
| | | | 203.5 | 0.019 | 0.510 | 0.750 | 107.60 | 98.06 | 119.62 | 1967 68968 |
| ANNEALED | S | 0 02 - 423 L-T | 203.5 | 0.020 | 0.270 | 138.90 | 90.91 | 121.19* | 1967 68968 | |
| | | | 203.5 | 0.020 | 1.030 | 1.280 | 68.60 | 94.20 | 109.88 | 1967 68968 |
| | | | 203.5 | 0.030 | 0.150 | 0.350 | 172.70 | 83.96* | 92.6/ 2.3 | 1967 68968 |
| ANNEALED | S | 0 02 - 423 L-T | 203.5 | 0.017 | 2.010 | 49.00 | 93.63 | 100.40 | 1967 68968 | |
| | | | 203.5 | 0.018 | 0.490 | 50.10 | 93.42 | 107.82 | 1967 68968 | |
| | | | 203.5 | 0.018 | 0.490 | 103.90 | 93.29 | 120.03 | 1967 68968 | |
| | | | 203.5 | 0.018 | 0.490 | 110.50 | 97.34 | 111.58 | 1967 68968 | |
| | | | 203.5 | 0.018 | 0.130 | 0.250 | 181.60 | 82.09* | 113.92* | 1967 68968 |
| | | | 203.5 | 0.019 | 0.250 | 0.530 | 153.30 | 96.17 | 140.55* | 1967 68968 |
| | | | 203.5 | 0.019 | 0.240 | 0.640 | 156.40 | 96.12 | 157.72* | 1967 68968 |
| | | | 203.5 | 0.018 | 1.000 | 1.350 | 73.70 | 93.98 | 109.87 | 1967 68968 |
| | | | 203.5 | 0.018 | 2.000 | 2.420 | 48.80 | 92.73 | 105.98 | 1967 68968 |
| | | | 203.5 | 0.019 | 0.500 | 0.720 | 109.10 | 97.10 | 117.07 | 1967 68968 |
| ANNEALED | S | 0 02 - 423 L-T | 203.5 | 0.019 | 1.020 | 71.40 | 92.02 | 100.98 | 1967 68968 | |
| | | | 203.5 | 0.019 | 0.250 | 157.20 | 98.63* | 154.87* | 1967 68968 | |
| | | | 203.5 | 0.019 | 1.000 | 74.10 | 94.47 | 110.94 | 1967 68968 | |
| | | | 203.5 | 0.018 | 0.130 | 0.220 | 191.90 | 86.74* | 112.90* | 1967 68968 |
| | | | 203.5 | 0.018 | 0.490 | 0.620 | 104.30 | 91.60 | 103.10 | 1967 68968 |
| | | | 203.5 | 0.019 | 4.000 | 4.450 | 35.40 | 95.35 | 102.42 | 1967 68968 |
| | | | 203.5 | 0.019 | 0.490 | 0.660 | 108.60 | 95.30 | 110.78 | 1967 68968 |
| | | | 203.5 | 0.019 | 0.130 | 0.380 | 178.40 | 80.62* | 137.92* | 1967 68968 |
| | | | 203.5 | 0.018 | 0.180 | 0.190 | 76.00 | 94.68 | 104.54 | 1967 68968 |
| | | | 203.5 | 0.018 | 0.130 | 0.220 | 191.90 | 86.74* | 112.90* | 1967 68968 |

*NOTE- NET SECTION STRESS EXCEEDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV

TABLE 4.7.2.1 (con't)

| TITANIUM | | TISAL-2.5SN | | K(C) | | CRACK LENGTH | | GROSS STRESS | | K(APP) STAM | | K(C) STAM | | | | | |
|-----------|----------|-------------------------|-----------------|------------|------------|--------------|------------|--------------|-----------|--------------|------------|-----------|------------|------------|-----------|------|-------|
| CONDITION | PROPERTY | TEST SPEC OR THICK (IN) | YIELD STR (KSI) | SPECIMEN | | INIT (IN) | FINAL (IN) | ONSET (KSI) | MAX (KSI) | K(APP) (KSI) | MEAN (KSI) | DEV (KSI) | K(C) (KSI) | MEAN (KSI) | DEV (KSI) | DATE | REFER |
| | | | | WIDTH (IN) | THICK (IN) | | | | | | | | | | | | |
| ANNEALED | S | 0.02 - 423 L-T | 203.5 | 12.000 | 0.019 | 2.000 | 2.460 | --- | 51.20 | 92.34 | --- | --- | 103.34 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.018 | 0.240 | 0.620 | --- | 154.40 | 94.82 | --- | --- | 126.30* | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.018 | 0.500 | 0.690 | --- | 103.60 | 91.91 | --- | --- | 108.08 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.019 | 1.000 | 1.170 | --- | 71.30 | 89.79 | --- | --- | 97.23 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.019 | 2.000 | 2.410 | --- | 52.10 | 93.96 | --- | 93.3/ 2.0 | 103.97 | 104.2/ 4.0 | --- | 1967 | 68968 |
| ANNEALED | S | 0.02 - 423 L-T | 203.5 | 12.000 | 0.020 | 4.000 | 4.040 | --- | 39.20 | 105.59 | --- | --- | 106.28 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.020 | 0.120 | 0.260 | --- | 183.90 | 79.83* | --- | --- | 117.56* | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.020 | 0.120 | 0.310 | --- | 181.10 | 78.63* | --- | --- | 126.43* | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.021 | 2.000 | 2.330 | --- | 51.60 | 93.06 | --- | --- | 101.08 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.020 | 4.020 | 4.350 | --- | 35.20 | 95.12 | --- | --- | 100.26 | --- | --- | 1967 | 68968 |
| ANNEALED | S | 0.02 | 203.5 | 12.000 | 0.021 | 0.240 | 0.400 | --- | 151.30 | 92.92 | --- | --- | 120.01 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.020 | 0.240 | 0.470 | --- | 153.20 | 94.09 | --- | --- | 131.76 | --- | --- | 1967 | 68968 |
| | | 0.02 | 203.5 | 12.000 | 0.021 | 0.990 | 1.370 | --- | 70.90 | 88.79 | --- | 94.9/ 5.7 | 104.85 | 110.7/12.5 | --- | 1967 | 68968 |
| | | 0.02 - 423 L-T | 193.3 | 15.930 | 0.016 | 4.980 | 5.480 | --- | 32.80 | 97.69 | --- | --- | 103.92 | --- | --- | 1967 | 68968 |
| | | 0.02 | 193.3 | 15.930 | 0.019 | 4.980 | 5.380 | --- | 29.20 | 86.97 | --- | 92.3/ 7.6 | 90.29 | 97.1/ 9.6 | --- | 1967 | 68968 |
| ANNEALED | S | 0.06 - 423 L-T | 228.0 | 1.000 | 0.063 | 0.410 | --- | --- | 63.90 | 57.34 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.06 | 228.0 | 1.000 | 0.064 | 0.480 | --- | --- | 54.60 | 55.53 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.06 | 228.0 | 1.000 | 0.062 | 0.080 | --- | --- | 131.10 | 46.66 | --- | --- | --- | --- | --- | 1971 | 80104 |
| ANNEALED | S | 0.06 | 228.0 | 1.000 | 0.064 | 0.170 | --- | --- | 115.50 | 60.77 | --- | 55.1/ 6.0 | --- | --- | --- | 1971 | 80104 |
| | | 0.06 - 423 L-T | 228.0 | 2.000 | 0.063 | 0.180 | --- | --- | 115.10 | 61.51 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.06 | 228.0 | 2.000 | 0.063 | 0.140 | --- | --- | 123.00 | 57.86 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.06 | 228.0 | 2.000 | 0.063 | 0.790 | --- | --- | 46.80 | 57.80 | --- | --- | --- | --- | --- | 1971 | 80104 |
| ANNEALED | S | 0.06 | 228.0 | 2.000 | 0.064 | 0.420 | --- | --- | 78.30 | 65.39 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.06 | 228.0 | 2.000 | 0.062 | 0.080 | --- | --- | 147.10 | 52.20 | --- | 59.0/ 4.9 | --- | --- | --- | 1971 | 80104 |
| ANNEALED | S | 0.06 - 423 L-T | 228.0 | 3.000 | 0.064 | 0.990 | --- | --- | 48.50 | 64.89 | --- | --- | --- | --- | --- | 1971 | 80104 |
| ANNEALED | S | 0.10 - 423 L-T | 211.0 | 1.000 | 0.113 | 0.240 | --- | --- | 116.90 | 74.44 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.10 | 211.0 | 1.000 | 0.113 | 0.360 | --- | --- | 90.30 | 73.90 | --- | --- | --- | --- | --- | 1971 | 80104 |
| | | 0.10 | 211.0 | 1.000 | 0.111 | 0.120 | --- | --- | 161.30 | 70.66* | 74.2/ 0.4 | --- | --- | --- | --- | 1971 | 80104 |

BUCKLING OF CRACK EDGES RESTRAINED

*NOTE - NET SECTION STRESS EXCEEDS BOX OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.7.2.1 (con't)

| CONDITION | TITANIUM | | TI-SAL-2.5BN | | K(C) | | CRACK LENGTH GROSS STRESS | | | | K(IAPP) STAN | | K(C) STAN | | |
|-----------|----------|------------|---------------|---------|-----------------|------------|---------------------------|-----------|------------|-------------|--------------|----------------------------|------------------------|-------------------------|------------------------|
| | FORM | THICK (IN) | TEST TEMP (F) | SPEC OR | YIELD STR (KSI) | SPECIMEN | | INIT (IN) | FINAL (IN) | ONSET (KGI) | MAX (KBI) | K(IAPP) MEAN (KSI*SQRT IN) | STAN DEV (KSI*SQRT IN) | K(C) MEAN (KSI*SQRT IN) | STAN DEV (KSI*SQRT IN) |
| | | | | | | WIDTH (IN) | THICK (IN) | | | | | | | | |
| ANNEALED | 0 | 0.10 | - 423 | L-T | 211.0 | 2.000 | 0.112 | 0.130 | --- | 138.30 | 71.72* | --- | --- | --- | 1971 80104 |
| | | 0.10 | | | 211.0 | 2.000 | 0.114 | 0.270 | --- | 119.00 | 78.38 | --- | --- | --- | 1971 80104 |
| | | 0.10 | | | 211.0 | 2.000 | 0.113 | 0.380 | --- | 97.30 | 76.89 | 77.6/ 1.1 | --- | --- | 1971 80104 |
| ANNEALED | S | 0.10 | - 423 | L-T | 211.0 | 3.000 | 0.116 | 1.090 | --- | 55.20 | 76.77 | --- | --- | --- | 1971 80104 |
| | | 0.10 | | | 211.0 | 3.000 | 0.116 | 0.990 | --- | 56.30 | 78.01 | 77.4/ 0.9 | --- | --- | 1971 80104 |
| ANNEALED | S | 0.06 | - 420 | L-T | 228.0 | 3.000 | 0.064 | 1.000 | --- | 44.90 | 60.47 | --- | --- | --- | 1971 80104 |
| ANNEALED | S | 0.02 | - 320 | L-T | 171.2 | 15.940 | 0.018 | 3.000 | 3.400 | 44.60 | 133.16 | --- | 139.93 | --- | 1967 68968 |
| ANNEALED | S | 0.02 | - 320 | L-T | 171.2 | 16.230 | 0.020 | 4.980 | 3.610 | 44.80 | 133.11 | --- | 143.73 | --- | 1967 68968 |
| ANNEALED | S | 0.02 | R.T. | L-T | 109.3 | 19.950 | 0.018 | 3.060 | 4.780 | 54.50 | 163.94 | --- | 200.71* | --- | 1967 68968 |
| ANNEALED | S | 0.02 | R.T. | L-T | 109.3 | 16.390 | 0.018 | 3.070 | 6.660 | 58.70 | 176.16 | --- | 211.86* | --- | 1967 68968 |
| ANNEALED | S | 0.20 | R.T. | L-T | 110.7 | 13.880 | 0.202 | 4.950 | --- | 68.70 | 196.87* | --- | --- | --- | 1966 66218 |
| ANNEALED | S | 0.02 | - 423 | T-L | 211.8 | 12.000 | 0.015 | 1.130 | 1.590 | 64.70 | 86.67 | --- | 96.40 | --- | 1966 66103 |
| | | 0.02 | | | 211.8 | 12.000 | 0.015 | 0.930 | 0.710 | 112.40 | 80.96 | 83.8/ 4.0 | 118.96 | 107.7/16.0 | 1966 66103 |
| ANNEALED | S | 0.03 | - 423 | T-L | 207.3 | 12.000 | 0.036 | 0.280 | 1.070 | 129.00 | 85.38 | --- | 168.07 | --- | 1966 66103 |
| | | 0.03 | | | 207.3 | 12.000 | 0.036 | 1.200 | 1.840 | 73.70 | 101.81 | 93.7/11.5 | 127.14 | 147.6/28.9 | 1966 66103 |

BUCKLING OF CRACK EDGES RESTRAINED

*NOTE- NET SECTION STRESS EXCEEDS BOX OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.7.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.1 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.5SN | | | |
|---------------------------------------|--|---------------------------------------|-----------------------|-------------------------|-------------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. : DRY ARGON | E= R. T. : LAB AIR | E= R. T. : DIST. H2O | E= R. T. : 3.5% NaCl |
| DELTA K MIN | A: 16.59 : | 2.12 | | | |
| | B: 17.50 : | | 8.19 | | |
| | C: 16.62 : | | | 7.49 | |
| | D: 17.57 : | | | | 16.3 |
| | 20.00 : | 4.77 | 11.7 | 11.8 | 23.5 |
| | 25.00 : | 10.0 | 20.7 | 20.4 | 37.5 |
| DELTA K MAX | 30.00 : | 17.3 | 32.5 | 31.1 | 50.5 |
| | 35.00 : | 28.6 | 47.3 | 42.4 | 64.2 |
| | 40.00 : | | | 52.7 | |
| | A: 38.01 : | 38.7 | | | |
| | B: 37.81 : | | 57.0 | | |
| | C: 42.00 : | | | 56.3 | |
| D: 38.00 : | | | | 73.6 | |
| ROOT MEAN SQUARE PERCENT ERROR | | 4.48 | 2.10 | 7.50 | 4.46 |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 2 | 2 | 2 |

CONDITION/HT: ANNEALED
 FORM: 0.008" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 50.00 HZ

YIELD STRENGTH: 122.3 KSI
 ULT. STRENGTH: 139.9 KSI
 SPECIMEN THK: 0.003- 0.004"
 SPECIMEN WIDTH: 2.754- 2.758"
 REFERENCES: 88911

TITAN.
ALLOY

TI-5AL-
2.5SN

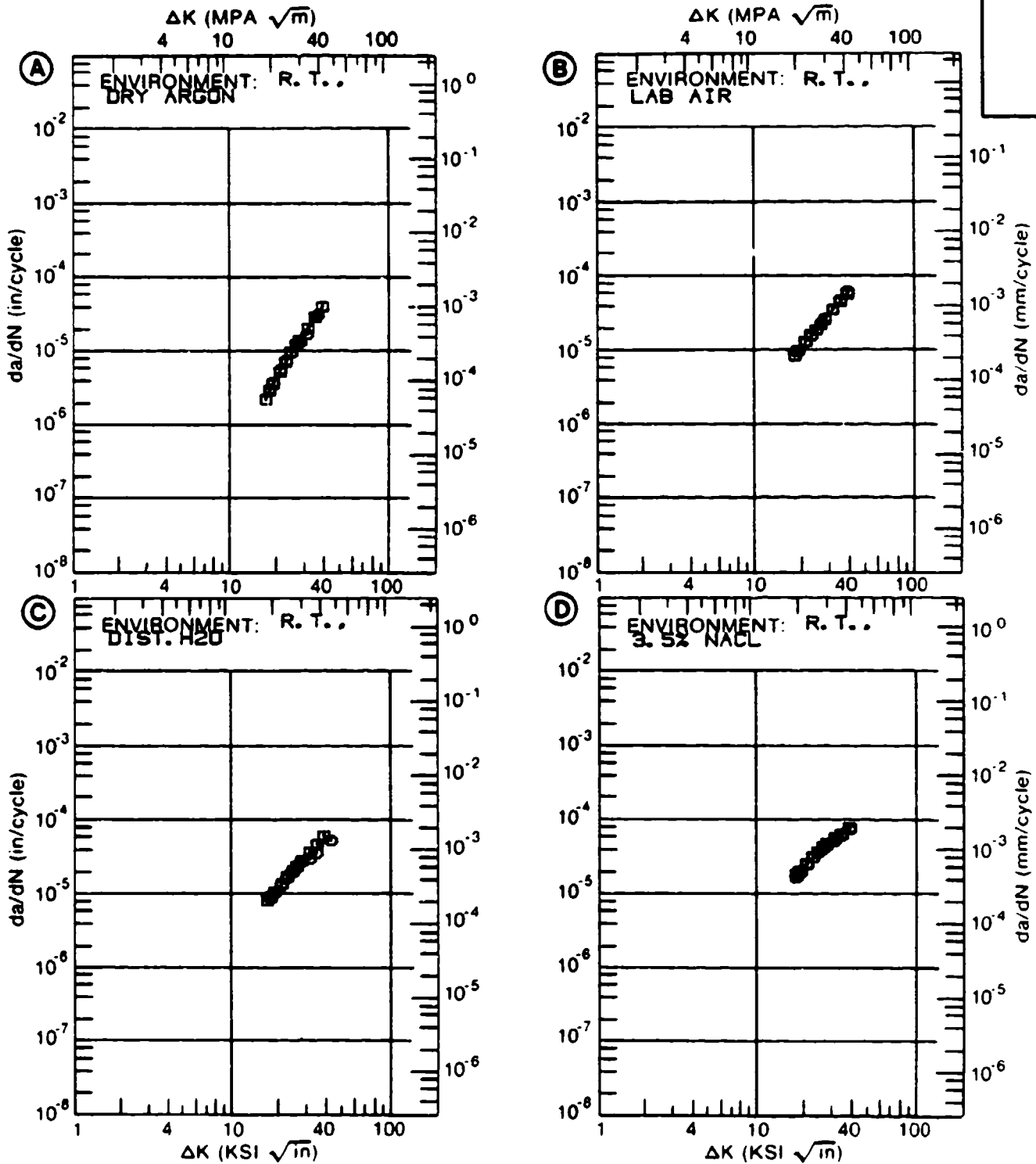


Figure 4.7.3.1

TABLE 4.7.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.2 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.5SN | | | |
|---------------------------------------|--|--------------------------------------|---------------------|-----------------------|-----------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. LAB AIR | E= R. T. DIST. H2O | E= R. T. 3.5% NaCl |
| DELTA K MIN | A: 18.13 | 4.02 | | | |
| | B: 18.23 | | 8.87 | | |
| | C: 21.49 | | | 16.0 | |
| | D: 20.00 | | | | 30.2 |
| | 20.00 | 5.56 | 11.6 | | |
| | 25.00 | 11.6 | 21.3 | 23.4 | 51.1 |
| | 30.00 | 20.8 | 34.4 | 35.8 | 69.4 |
| | 35.00 | 33.6 | 51.0 | 51.0 | 86.5 |
| | 40.00 | 50.3 | 71.3 | 69.9 | 105. |
| | 50.00 | 94.7 | 124. | 124. | 157. |
| DELTA K MAX | A: 53.17 | 112. | | | |
| | B: 53.30 | | 145. | | |
| | C: 53.14 | | | 148. | |
| | D: 53.17 | | | | 181. |
| ROOT MEAN SQUARE | | 4.36 | 3.18 | 4.21 | 4.45 |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 2 | 2 | 2 |

CONDITION/HT: ANNEALED
 FORM: 0.08" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 30.00 HZ

YIELD STRENGTH: 122.3 KSI
 ULT. STRENGTH: 133.9 KSI
 SPECIMEN THK: 0.083- 0.084"
 SPECIMEN WIDTH: 2.754- 2.764"
 REFERENCES: 88911

TITAN.
ALLOY

TI-5AL-
2.5SN

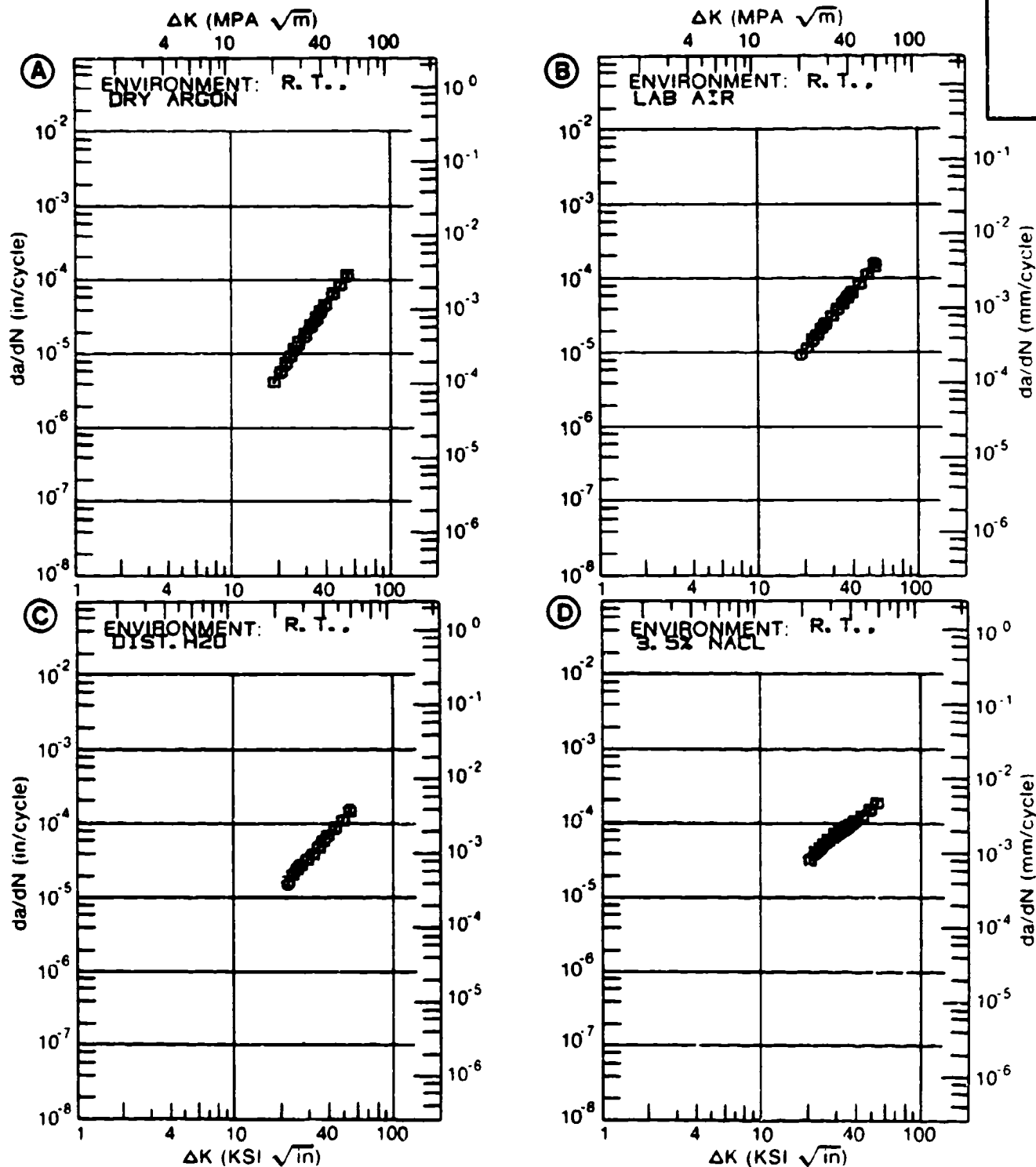


Figure 4.7.3.2

TABLE 4.7.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.3 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.5SN | | | |
|--------------------------|----------|--------------------------------------|---------------------|-----------------------|------------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. LAB AIR | E= R. T. DIST. H2O | E= R. T. 3.5% NAACL |
| DELTA K | A: 4.31 | .0150 | | | |
| MIN | B: 3.99 | | .0597 | | |
| | C: 3.44 | | | .0749 | |
| | D: 3.77 | | | | .125 |
| | 3.50 | | | .0781 | |
| | 4.00 | | .0604 | .114 | .149 |
| | 5.00 | .0301 | .152 | .253 | .295 |
| | 6.00 | .0444 | .310 | .526 | .719 |
| | 7.00 | .0558 | .558 | .984 | 2.34 |
| | 8.00 | .0782 | .922 | 1.65 | 5.30 |
| | 9.00 | .136 | 1.43 | 2.51 | 7.20 |
| | 10.00 | .278 | 2.13 | 3.49 | 7.97 |
| DELTA K | A: 11.87 | .999 | | | |
| MAX | B: 12.86 | | 5.60 | | |
| | C: 12.87 | | | 5.99 | |
| | D: 12.93 | | | | 12.4 |
| ROOT MEAN SQUARE | | 18.92 | 14.40 | 8.05 | 13.28 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | 3 | 4 | 4 | 4 |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: 0.08" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.07
 FREQUENCY: 55.00- 50.30 HZ

YIELD STRENGTH: 122.3 KSI
 ULT. STRENGTH: 133.9 KSI
 SPECIMEN THK: 0.003- 0.005"
 SPECIMEN WIDTH: 2.752- 2.756"
 REFERENCES: 00011

TITAN.
 ALLOY
 TI-5AL-
 2.5SN

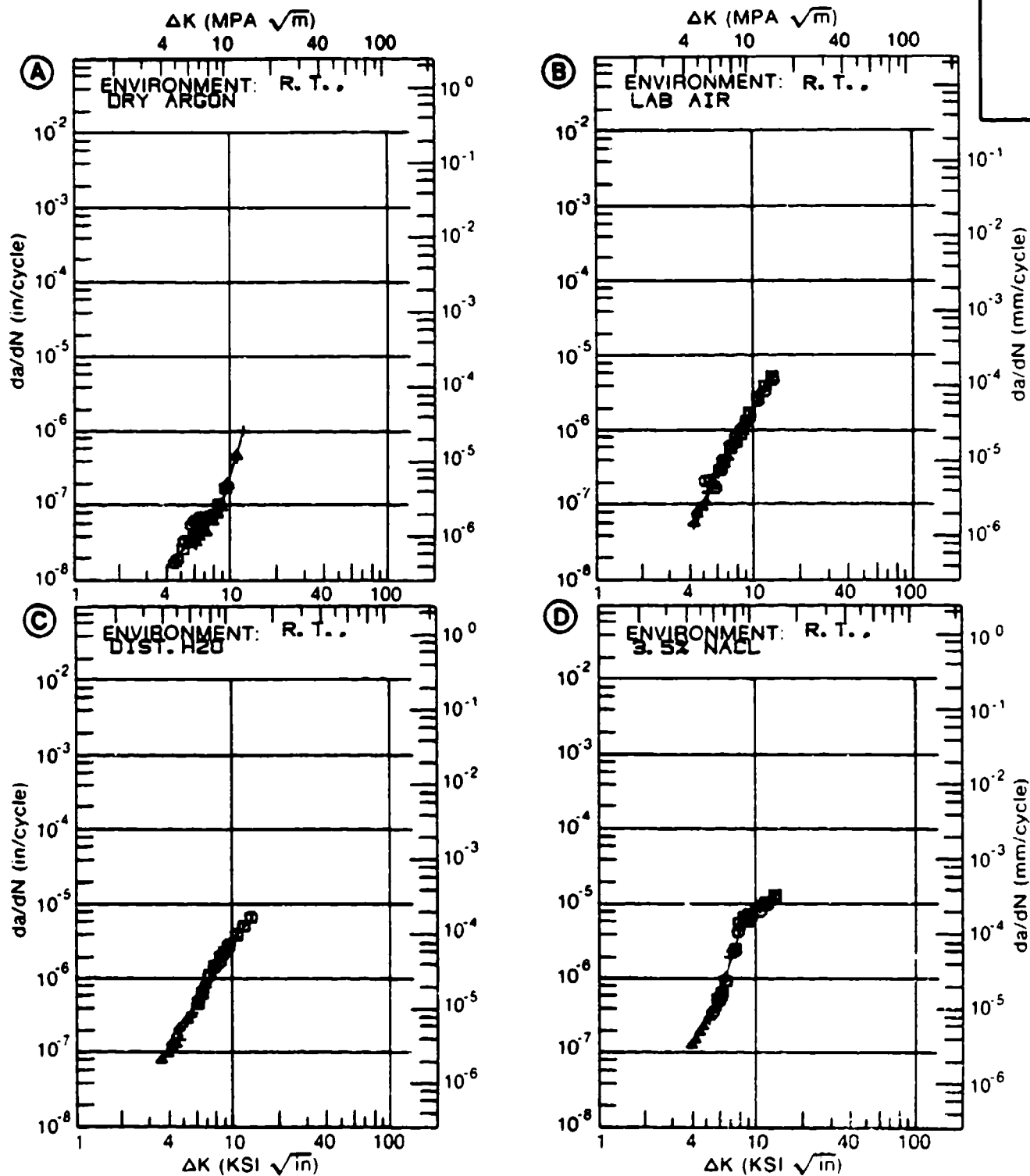


Figure 4.7.3.3

TABLE 4.7.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.4 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.58N | | | |
|---------------------------------------|--|--------------------------------------|---------------------|-----------------------|-----------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. LAB AIR | E= R. T. DIST. H2O | E= R. T. 3.5% NaCl |
| DELTA K MIN | A: 17.46 | 3.21 | | | |
| | B: 16.63 | | 7.03 | | |
| | C: 16.57 | | | 7.01 | |
| | D: 16.28 | | | | 13.7 |
| | 20.00 | 5.35 | 11.8 | 12.0 | 24.5 |
| | 25.00 | 11.7 | 20.2 | 21.3 | 39.2 |
| | 30.00 | 21.2 | 31.1 | 33.4 | 53.7 |
| | 35.00 | 34.7 | 46.5 | 49.2 | 69.3 |
| DELTA K MAX | A: 37.87 | 44.6 | | | |
| | B: 38.10 | | 59.5 | | |
| | C: 37.79 | | | 59.9 | |
| | D: 37.84 | | | | 79.1 |
| ROOT MEAN SQUARE PERCENT ERROR | | 3.75 | 4.85 | 5.63 | 5.62 |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 2 | 2 | 2 |

CONDITION/HT: ANNEALED
 FORM: 0.08" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 50.00- 53.30 HZ

YIELD STRENGTH: 125.4 KSI
 ULT. STRENGTH: 193.9- 195.2 KSI
 SPECIMEN THK: 0.083- 0.085"
 SPECIMEN WIDTH: 2.755- 2.758"
 REFERENCES: 00011

TITAN.
 ALLOY
 TI-5AL-
 2.55N

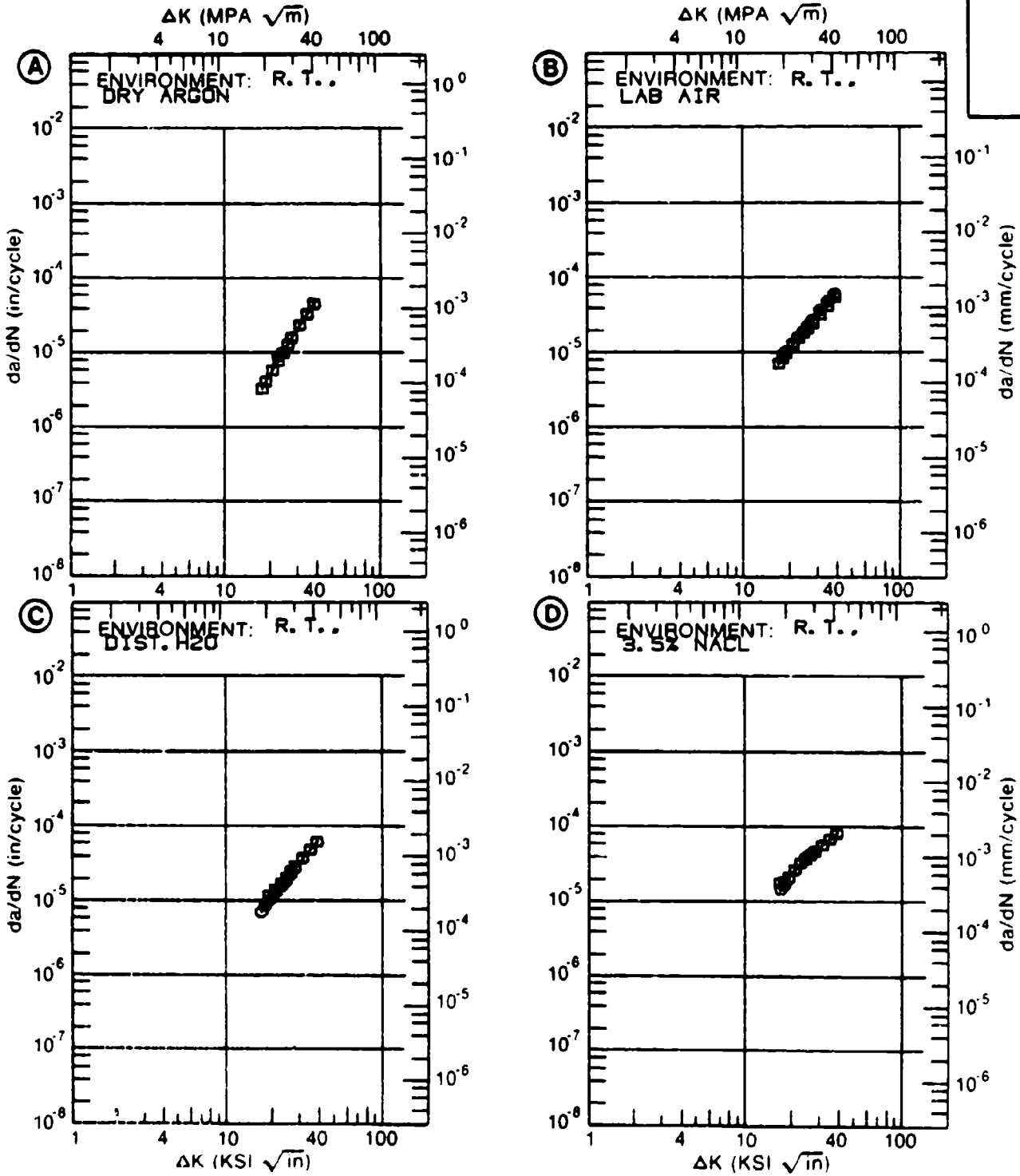


Figure 4.7.3.4

TABLE 4.7.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.5 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.5SN | | | |
|---------------------------------------|--|---------------------------------------|---------------------|-----------------------|-----------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. LAB AIR | E= R. T. DIST. H2O | E= R. T. 3.5% NaCl |
| DELTA K A: | 18.62 | 3.96 | | | |
| DELTA K B: | 19.82 | | 11.5 | | |
| MIN C: | 18.18 | | | 9.45 | |
| D: | 21.52 | | | | 35.6 |
| | 20.00 | 5.38 | 11.9 | 12.5 | |
| | 25.00 | 12.4 | 23.1 | 23.6 | 49.4 |
| | 30.00 | 22.2 | 37.4 | 38.6 | 68.1 |
| | 35.00 | 35.5 | 55.1 | 57.2 | 87.1 |
| | 40.00 | 53.5 | 77.2 | 79.0 | 109. |
| | 50.00 | 114. | 141. | 130. | 176. |
| DELTA K A: | 53.29 | 145. | | | |
| MAX B: | 53.22 | | 169. | | |
| C: | 53.08 | | | 148. | |
| D: | 53.13 | | | | 207 |
| ROOT MEAN SQUARE | | 9.40 | 4.52 | 5.31 | 16.48 |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 2 | 2 | 2 |

CONDITION/HT: ANNEALED
 FORM: 0.00" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 30.00 HZ

YIELD STRENGTH: 125.4 KSI
 ULT. STRENGTH: 193.9- 135.2 KSI
 SPECIMEN THK: 0.003- 0.005"
 SPECIMEN WIDTH: 2.753- 2.757"
 REFERENCES: 00011

TITAN.
ALLOY

TI-SAL-
2.55N

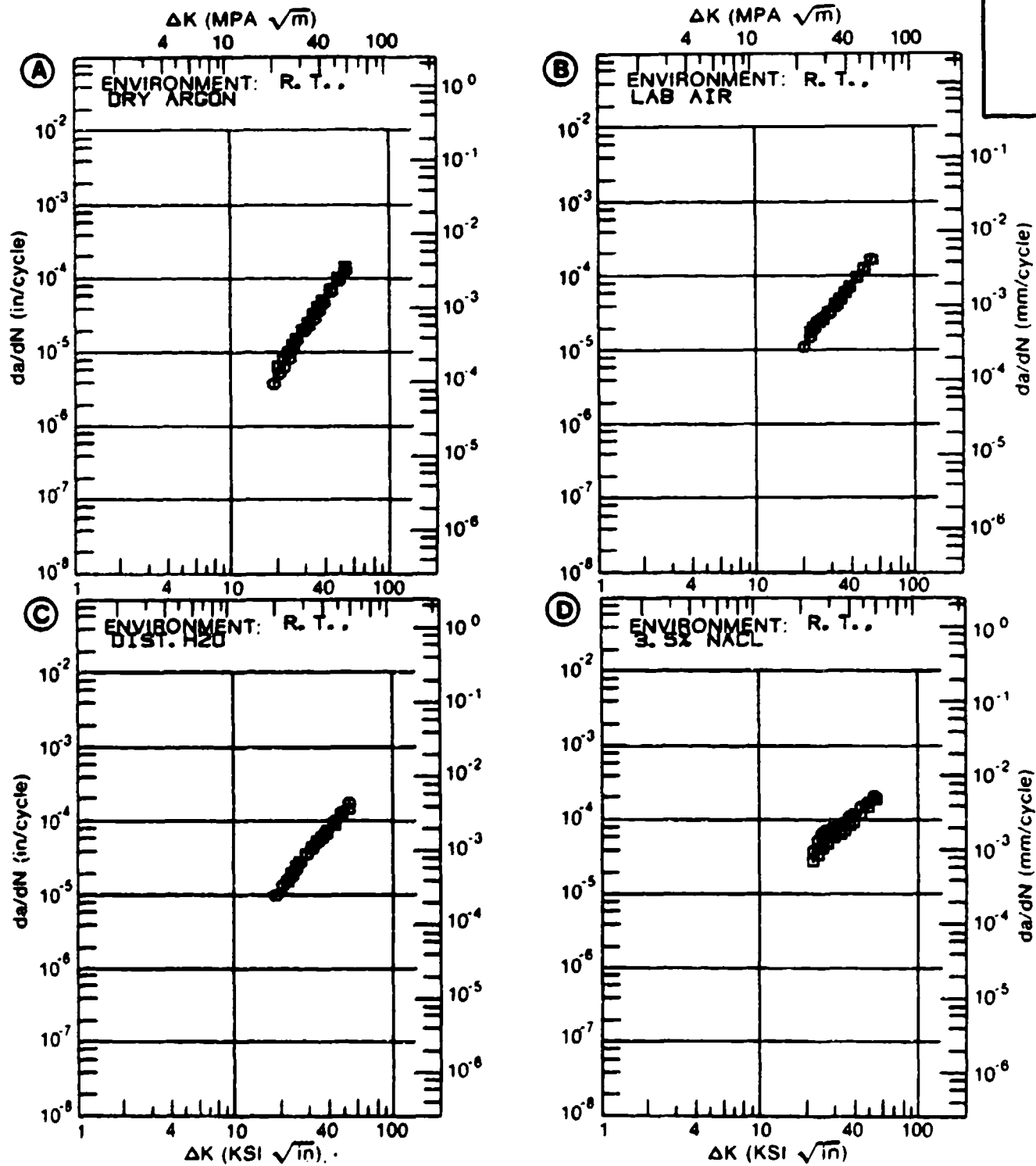


Figure 4.7.3.5

TABLE 4.7.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.7.3.6 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-5AL-2.5SN | | | |
|--------------------------|----------|--------------------------------------|---------------------|-----------------------|-----------------------|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. LAB AIR | E= R. T. DIST. H2O | E= R. T. 3.5% NaCl |
| DELTA K A: | 5.83 | .0930 | | | |
| DELTA K B: | 3.69 | | .0501 | | |
| MIN C: | 4.28 | | | .237 | |
| D: | 4.23 | | | | .209 |
| | 4.00 | | .0662 | | |
| | 5.00 | | .158 | .363 | .981 |
| | 6.00 | .0905 | .347 | .658 | 3.37 |
| | 7.00 | .105 | .685 | 1.13 | 6.92 |
| | 8.00 | .164 | 1.23 | 1.81 | 10.5 |
| | 9.00 | .285 | 2.02 | 2.68 | 13.1 |
| | 10.00 | .497 | 3.08 | 3.72 | 14.6 |
| | 13.00 | 1.86 | 7.57 | | |
| DELTA K A: | 13.02 | 1.87 | | | |
| DELTA K B: | 13.07 | | 7.68 | | |
| MAX C: | 12.74 | | | 6.71 | |
| D: | 10.00 | | | | 14.6 |
| ROOT MEAN SQUARE | | 16.96 | 11.13 | 7.18 | 37.84 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | 3 |
| RATIO | 0.8-1.25 | 3 | 4 | 4 | 1 |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: 0.08" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 STRESS RATIO: +0.87
 FREQUENCY: 54.20- 58.30 HZ

YIELD STRENGTH: 125.4 KSI
 ULT. STRENGTH: 133.9- 135.2 KSI
 SPECIMEN THK: 0.083- 0.085"
 SPECIMEN WIDTH: 2.753- 2.757"
 REFERENCES: 88911

TITAN.
 ALLOY
 TI-5AL-
 2.5SN

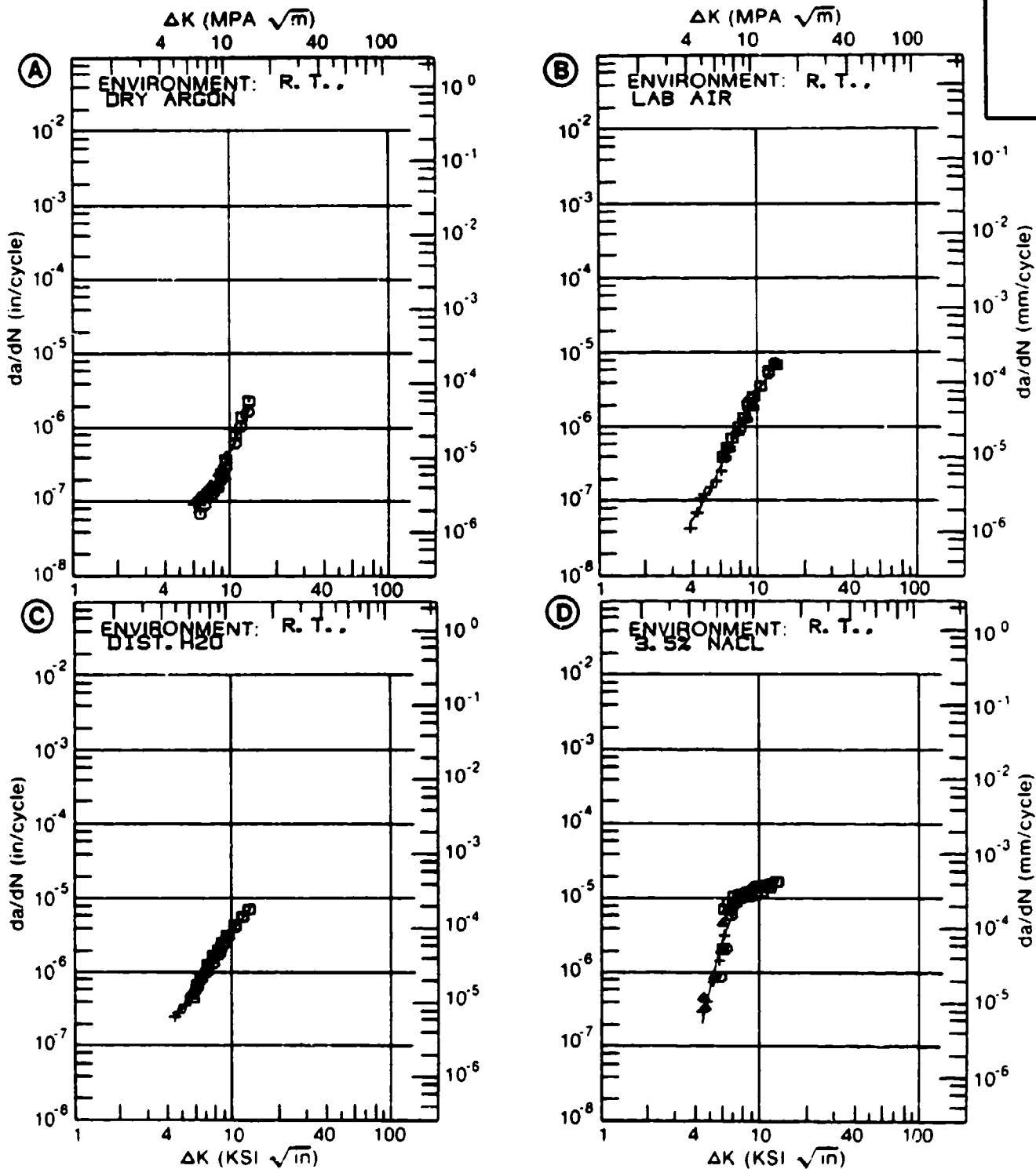


Figure 4.7.3.6

TABLE 4.8.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM Ti6-2-2-2

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: H.H.A
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-------------------------------|---|---|------|------|------|-----|
| ST | PLATE | 0.10 | 1.00 | | | | 2.38 | 13.3 | 271 | |
| SF | PLATE | 0.10 | 20.00 | | | | 1.50 | 10.7 | 98.4 | |
| STA | PLATE | 0.10 | 1.00 | | | | 1.87 | 17.3 | 423 | |
| STA | PLATE | 0.10 | 20.00 | | | | 0.16 | 2.37 | 13.5 | |

TABLE 4.8.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM Ti6-2-2-2

TEST CONDITIONS

SPECIMEN ORIENTATION -T

ENVIRONMENT: 3.5% NaCl
A R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-------------------------------|-----|------|------|------|------|-----|
| ST | PLATE | 0.10 | 1.00 | | | | 2.10 | 47.6 | 361 | |
| ST | PLATE | 0.10 | 20.00 | | | 0.31 | 4.70 | 30.7 | | |
| STA | PLATE | 0.10 | 1.00 | | | | | | 77.4 | |
| STA | PLATE | 0.10 | 20.00 | | | 0.47 | 5.90 | 15.2 | | |

TABLE 4.8.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.8.3.1 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI62222 | | | |
|---------------------------------------|--|-----------------------------|------------------------------|--------------------------------|---------------------------------|
| CONDITION: ST | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H. H. A. 1HZ | E= R. T. H. H. A. 20HZ | E= R. T. 3. 5% NAACL 1HZ | E= R. T. 3. 5% NAACL 20HZ |
| DELTA K MIN | A: 8.23 | 1.20 | | | |
| | B: 5.05 | | .076 | | |
| | C: 6.77 | | | .584 | |
| | D: 3.89 | | | | .048 |
| | 4.00 | | | | .0691 |
| | 5.00 | | | | .319 |
| | 6.00 | | .186 | | .742 |
| | 7.00 | | .378 | .630 | 1.39 |
| | 8.00 | | .659 | .915 | 2.27 |
| | 9.00 | 1.67 | 1.03 | 1.38 | 3.37 |
| | 10.00 | 2.38 | 1.50 | 2.10 | 4.70 |
| | 13.00 | 4.98 | 3.45 | 6.80 | 10.0 |
| | 16.00 | 8.12 | 6.12 | 18.0 | 17.6 |
| | 20.00 | 13.3 | 10.7 | 47.6 | 30.7 |
| | 25.00 | 22.3 | 18.2 | 110. | 50.9 |
| | 30.00 | 36.4 | 27.7 | 194. | 73.5 |
| | 35.00 | 59.0 | 39.8 | 291. | 96.6 |
| | 40.00 | 96.4 | 55.1 | 390. | 119. |
| | 50.00 | 271. | 98.4 | 561. | |
| | 60.00 | 834. | | 673. | |
| | 70.00 | 2775. | | | |
| DELTA K MAX | A: 71.40 | 3301. | | | |
| | B: 56.48 | | 139. | | |
| | C: 63.48 | | | 697. | |
| | D: 49.43 | | | | 155. |
| ROOT MEAN SQUARE PERCENT ERROR | | 8.80 | 8.83 | 22.49 | 11.12 |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | 1 |

CONDITION/HT: ST
 FORM: 0.83" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 157.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.151- 0.152"
 SPECIMEN WIDTH: 3.000"
 REFERENCES: 86844

TITAN. ALLOY

TI-6-2-2-2-2

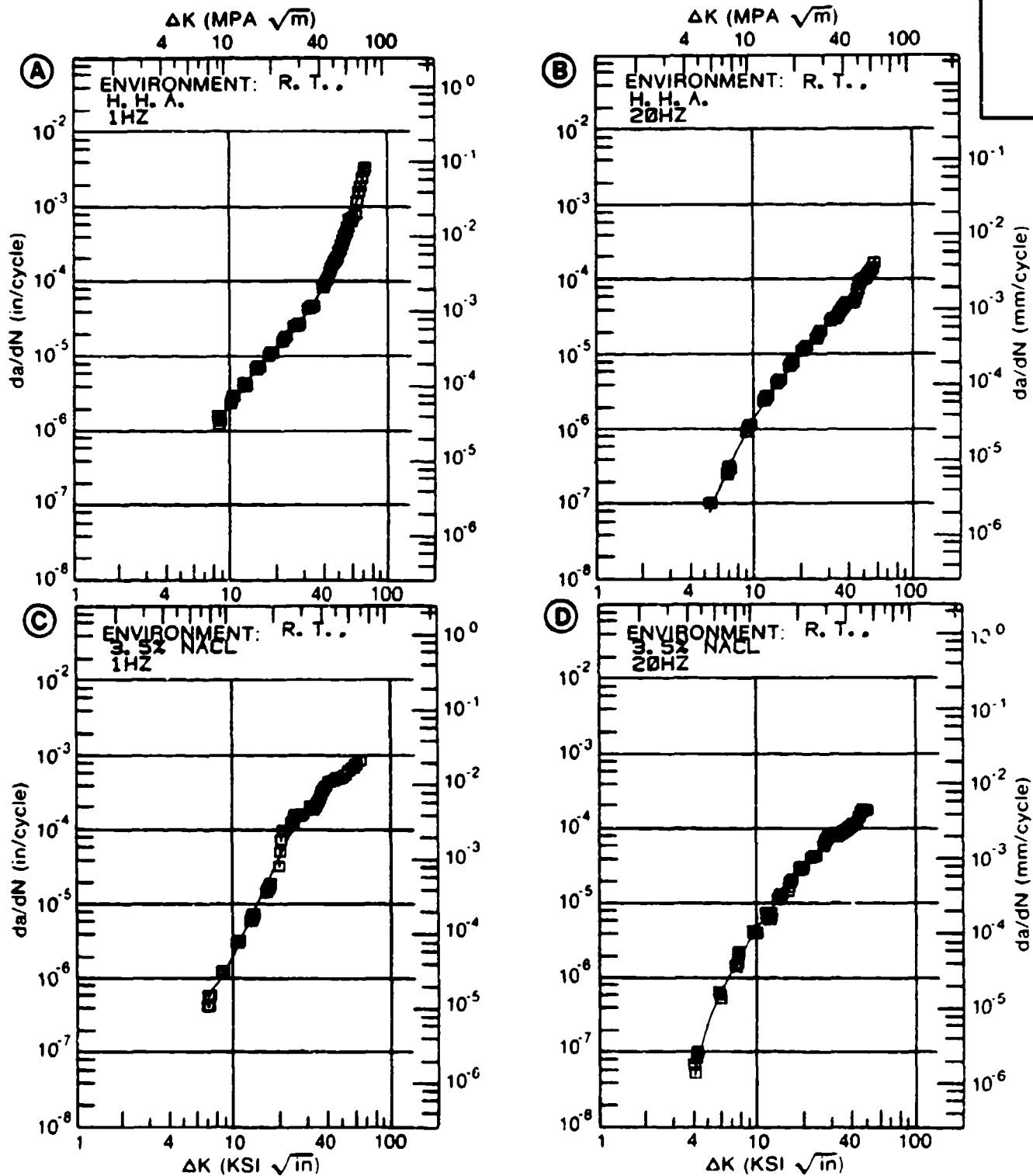


Figure 4.8.3.1

TABLE 4.8.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.8.3.2 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI62222 | | | |
|--------------------------|------------|---------------------------------------|------------------------------|-------------------------------|--------------------------------|
| CONDITION: STA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H. H. A. 1HZ | E= R. T. H. H. A. 20HZ | E= R. T. 3. 5% NACL 1HZ | E= R. T. 3. 5% NACL 20HZ |
| DELTA K | A: 7.18 : | .54 | | | |
| MIN | B: 4.13 : | | .06 | | |
| | C: 16.00 : | | | 35.9 | |
| | D: 3.64 : | | | | .06 |
| | 4.00 : | | | | .125 |
| | 5.00 : | | .164 | | .471 |
| | 6.00 : | | .369 | | 1.13 |
| | 7.00 : | | .686 | | 3.09 |
| | 8.00 : | .811 | 1.12 | | 3.27 |
| | 9.00 : | 1.26 | 1.69 | | 4.57 |
| | 10.00 : | 1.87 | 2.37 | | 5.90 |
| | 13.00 : | 4.73 | 5.02 | | 9.60 |
| | 16.00 : | 9.07 | 8.36 | 35.9 | 12.5 |
| | 20.00 : | 17.3 | 13.5 | 77.4 | 15.2 |
| | 25.00 : | 32.7 | 20.3 | | |
| | 30.00 : | 56.9 | 27.1 | | |
| | 35.00 : | 95.6 | 33.8 | | |
| | 40.00 : | 158. | 40.2 | | |
| | 50.00 : | 423. | | | |
| | 60.00 : | 1195. | | | |
| DELTA K | A: 64.83 : | 2030. | | | |
| MAX | B: 41.87 : | | 42.5 | | |
| | C: 20.37 : | | | 78.9 | |
| | D: 20.05 : | | | | 15.2 |
| ROOT MEAN SQUARE | | 7.39 | 8.43 | 14.68 | 20.21 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 | |
| SUMMARY | 1.25-2.0 | | | | 1 |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: STA
 FORM: 0.89" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 157.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.143- 0.147"
 SPECIMEN WIDTH: 3.070"
 REFERENCES: 88844

TITAN.
ALLOY

TI-6-2-
2-2-2

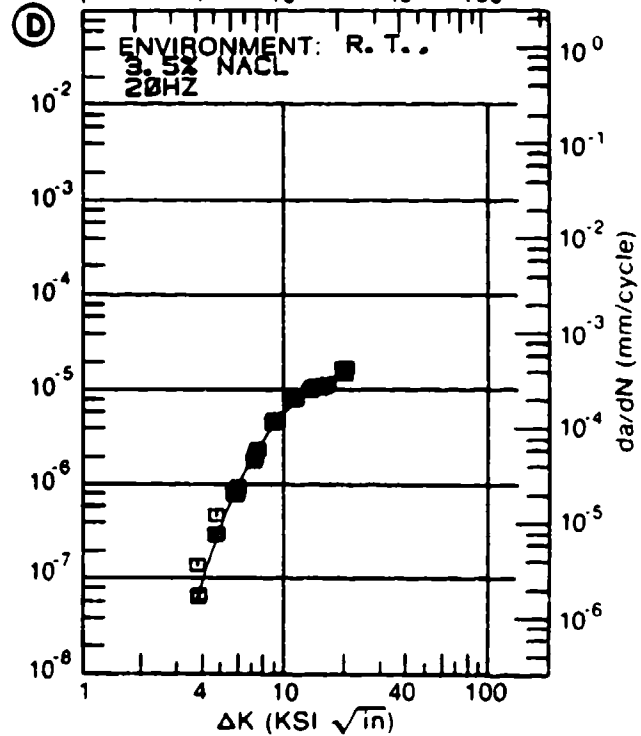
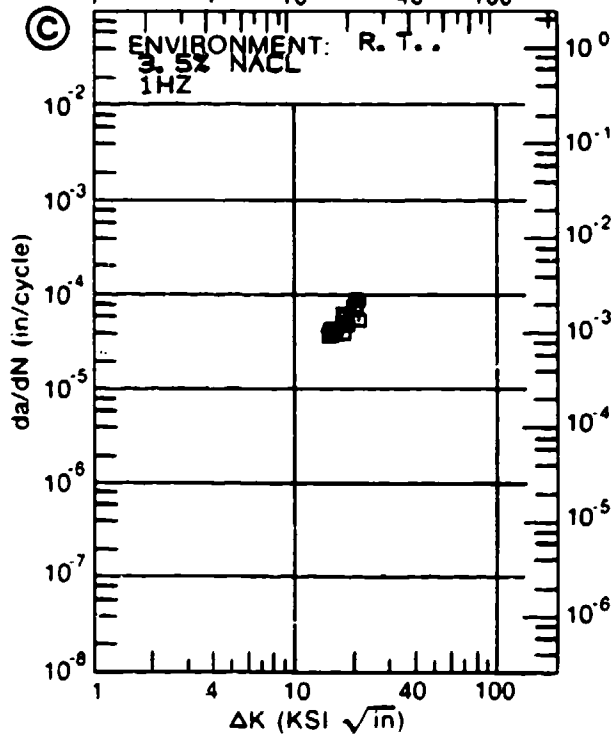
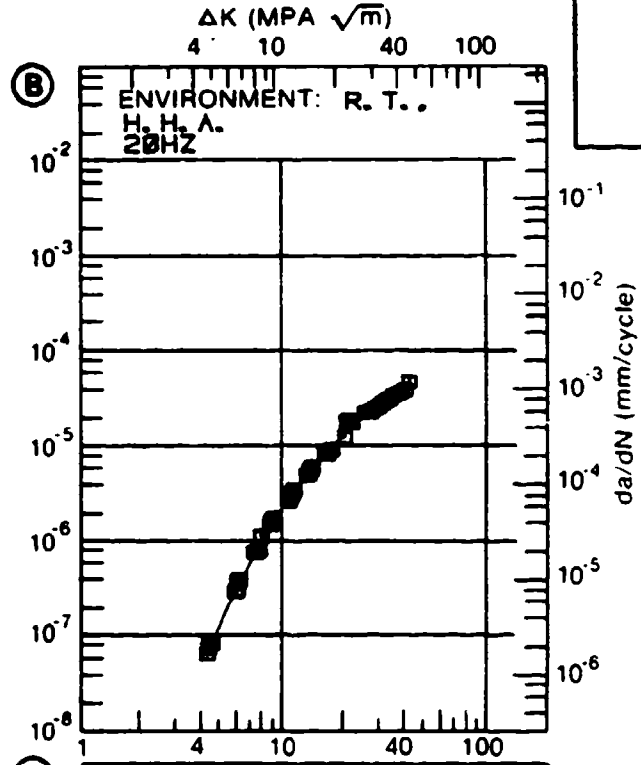
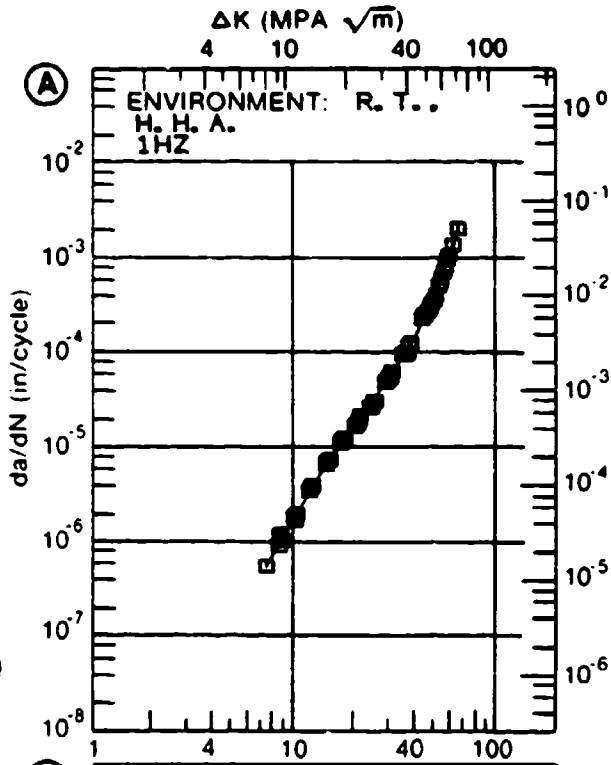


Figure 4.8.3.2

TABLE 4.9.1.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6-2-4-2

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------------------------|--------------|--------------|-----------|-------------------------------|---|
| | | | | 2 5 5 10 20 50 100 | |
| 1790F 1HR AC. 1100F 8HRS AC | FORGING | 0.10 | 0.16 | | 10.3 |
| 1790F 1HR AC. 1100F 8HRS AC | FORGING | 0.50 | 0.16 | | 2.27 |

TABLE 4.9.1.2

CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6-2-4-2

IE 51

SPECIMEN:
ORIENTATION:

ENVIRONMENT: AIR
AT 800 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------------------------|--------------|--------------|-----------|---|-----|------|------|----|----|-----|
| | | | | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
| 1790F 1HR AC. 1100F 6HRS AC | FORGING | 0.10 | 30.00 | | | 0.27 | 1.22 | | | |
| 1790F 1HR AC. 1100F 6HRS AC | FORGING | 0.50 | ----- | | | 5.69 | 20.9 | | | |
| 1790F 1HR AC. 1100F 6HRS AC | FORGING | 0.70 | 0.16 | | | 5.35 | | | | |

TABLE 4.9.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6-2-4-2

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT AIR AT 1000 F

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | ENVIRONMENT | | | FATIGUE CRACK GROWTH RATES (MICRO IN./CYCLE) | | | | |
|--------------------------------|--------------|--------------|-----------|-------------------------------|---|---|--|------|----|----|-----|
| | | | | DELTA K LEVELS (KSI SQRT(IN)) | 2 | 5 | | 10 | 20 | 50 | 100 |
| 1790F 1HR AC. 1100F 8HRS AC | FORGING | 0.10 | 30.00 | | | | 2.24 | | | | |
| 1790F 1HR AC. 1100F 8HRS AC | FORGING | 0.50 | 0.16 | | | | 9.16 | 30.2 | | | |

TABLE 4.9.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.9.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6-2-4-2
CONDITION: 1790F 1HR AC, 1100F 8HRS AC
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K | A: 11.61 | 1.81 | | | |
| MIN | B: 7.05 | | .52 | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | | .919 | | |
| | 9.00 | | 1.50 | | |
| | 10.00 | | 2.27 | | |
| | 13.00 | 2.52 | 5.70 | | |
| | 16.00 | 4.82 | 10.5 | | |
| | 20.00 | 10.3 | | | |
| DELTA K | A: 24.68 | 22.0 | | | |
| MAX | B: 19.52 | | 17.1 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 7.82 | 9.78 | | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1700F 1HR AC, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 FREQUENCY: 0.10 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 139.4 KSI
 ULT. STRENGTH: 151.6 KSI
 SPECIMEN THK: 0.079"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-2

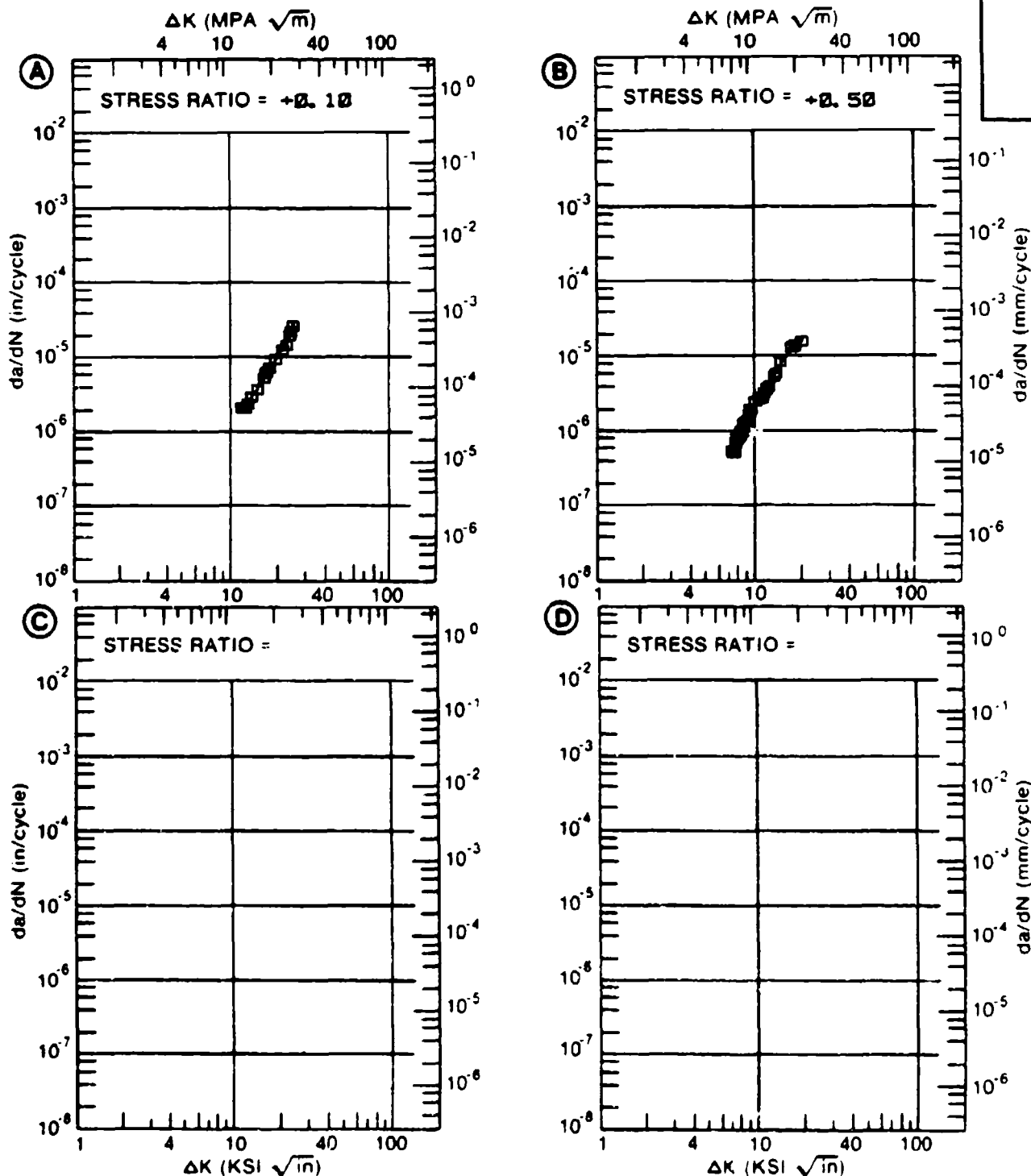


Figure 4.9.3.1

TABLE 4.9.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.9.3.2 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6-2-4-2
CONDITION: 1790F 1HR AC, 1100F 8HRS AC
ENVIRONMENT: + 800F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.70 | | | |
| DELTA K MIN | A: 5.15 | 1.36 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | 2.04 | | | |
| | 7.00 | 2.71 | | | |
| | 8.00 | 3.36 | | | |
| | 9.00 | 4.16 | | | |
| | 10.00 | 5.35 | | | |
| | 13.00 | 15.5 | | | |
| DELTA K MAX | A: 13.08 | 16.0 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 15.01
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1790F 1HR AC, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 FREQUENCY: 0.18 HZ
 ENVIRONMENT: + 800° F, AIR

YIELD STRENGTH: 135.5- 140.9 KSI
 ULT. STRENGTH: 148.5- 152.3 KSI
 SPECIMEN THK: 0.080- 0.081"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-2

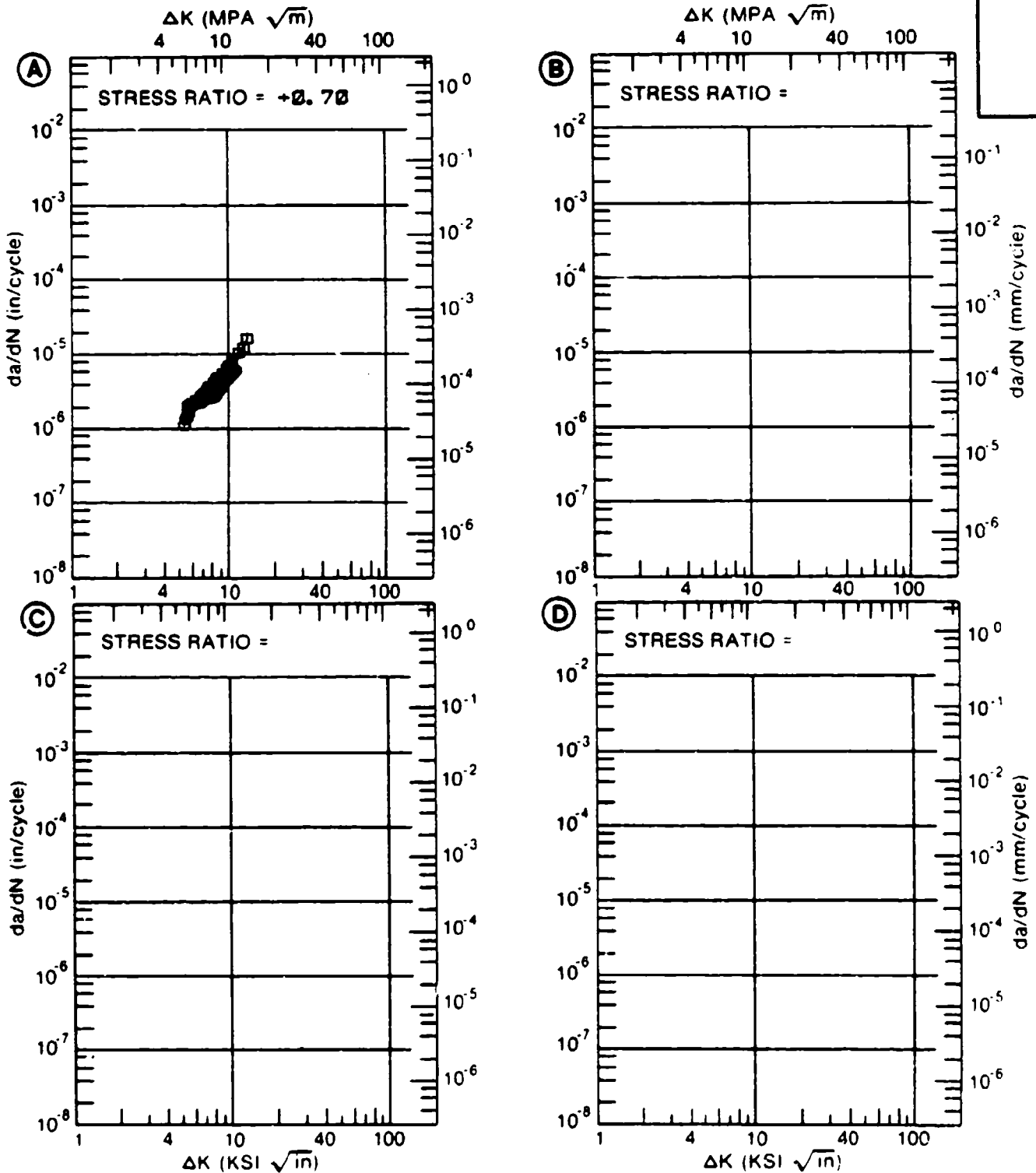


Figure 4.9.3.2

TABLE 4.9.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.9.3.3 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6-2-4-2
CONDITION: 1790F 1HR AC, 1100F 8HRS AC
ENVIRONMENT: +1000F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.50 | | | |
| DELTA K MIN | A: 5.60 | 3.89 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | 4.28 | | | |
| | 7.00 | 5.34 | | | |
| | 8.00 | 6.50 | | | |
| | 9.00 | 7.77 | | | |
| | 10.00 | 9.16 | | | |
| | 13.00 | 14.0 | | | |
| | 16.00 | 20.1 | | | |
| | 20.00 | 30.2 | | | |
| DELTA K MAX | A: 20.12 | 30.5 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE PERCENT ERROR 4.85

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1700F 1HR AC, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 FREQUENCY: 0.18 HZ
 ENVIRONMENT: +1000° F, AIR

YIELD STRENGTH: 139.4 KSI
 ULT STRENGTH: 151.8 KSI
 SPECIMEN THK: 0.074"
 SPECIMEN WIDTH: 1.750"
 REFERENCES PW002

TITAN.
 ALLOY

TI-6-2-
 4-2

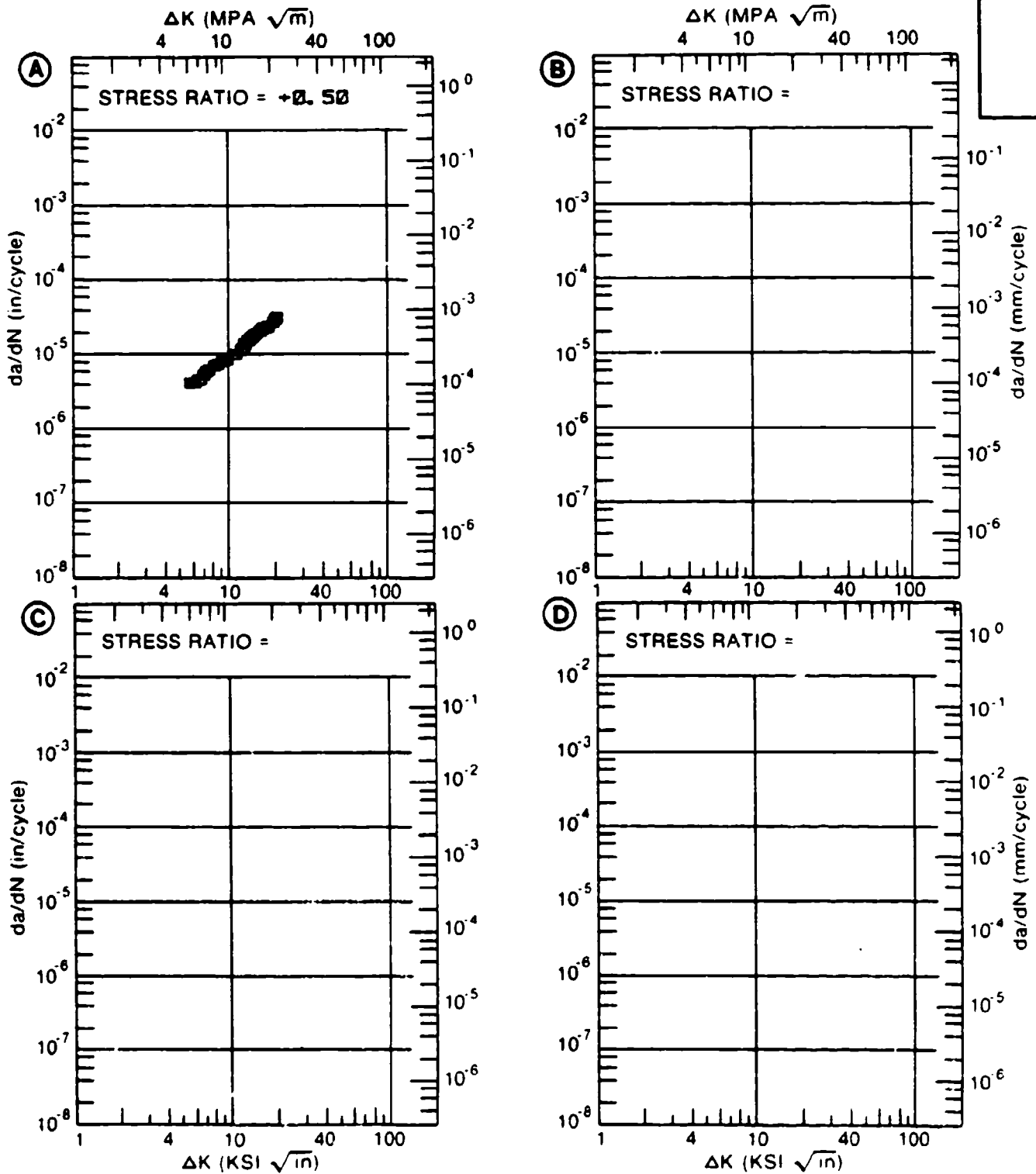


Figure 4.9.3.3

TABLE 4.9.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.9.3.4 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6-2-4-2 | | | |
|--|----------|--------------------------|----------|---|---|
| CONDITION: 1750F 1HR AC, 1100F 8HRS AC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E=+ 800F | E=+1000F | | |
| | | AIR | AIR | | |
| DELTA K A: | 4.95 | .26 | | | |
| DELTA K B: | 5.44 | | .70 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 5.00 | .270 | | | |
| | 6.00 | .378 | .846 | | |
| | 7.00 | .511 | 1.12 | | |
| | 8.00 | .682 | 1.43 | | |
| | 9.00 | .910 | 1.80 | | |
| | 10.00 | 1.22 | 2.24 | | |
| | 13.00 | 2.99 | 4.34 | | |
| | 16.00 | 6.35 | 8.64 | | |
| DELTA K A: | 18.28 | 9.39 | | | |
| DELTA K B: | 18.45 | | 15.5 | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 5.98 | 4.40 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: 1700F 1HR AC, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.10
 FREQUENCY: 30.00 HZ

YIELD STRENGTH: 139.4- 140.9 KSI
 ULT. STRENGTH: 151.6- 152.3 KSI
 SPECIMEN THK: 0.073- 0.083"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-2

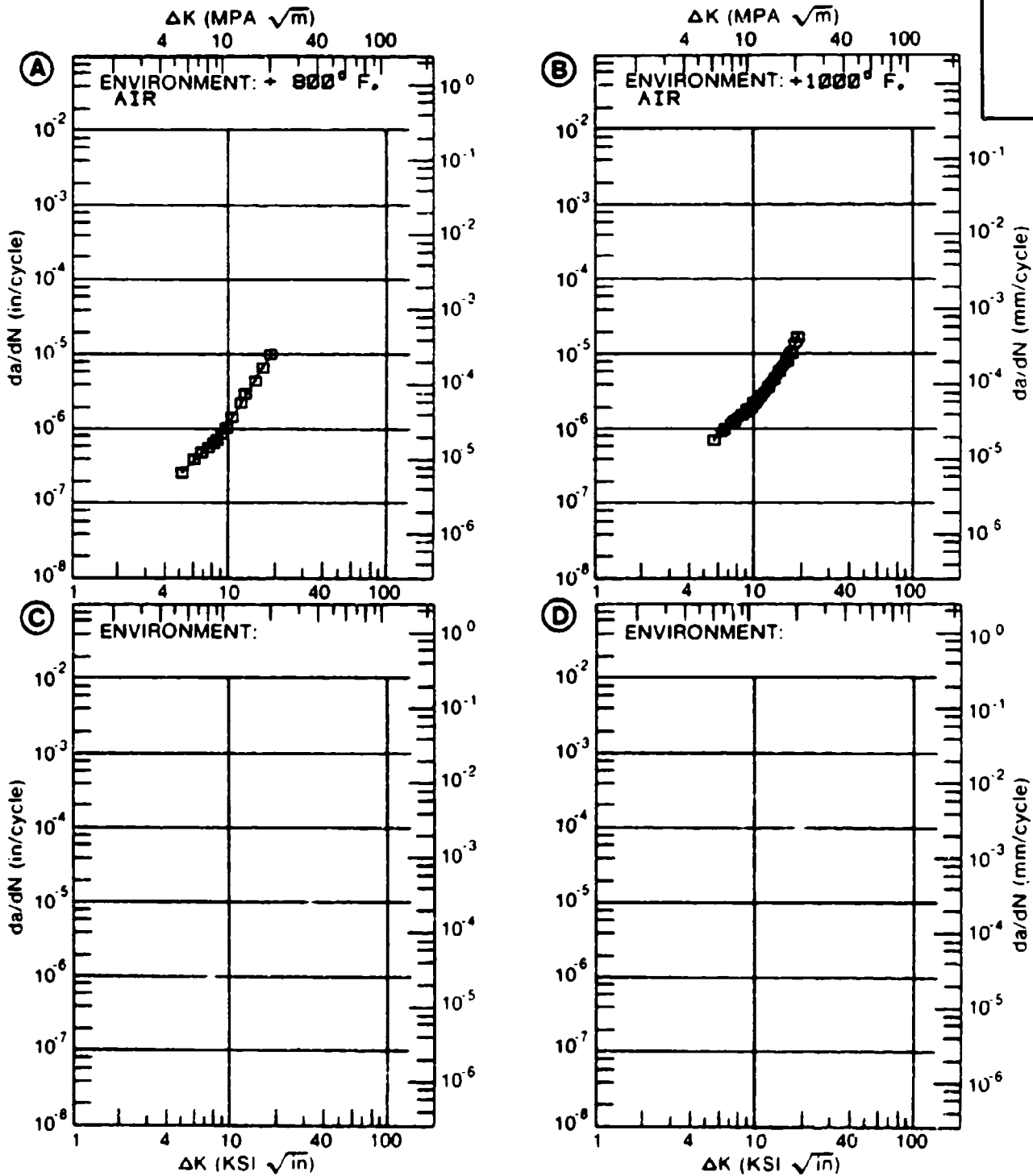


Figure 4.9.3.4

TABLE 4.9.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.9.3.5 INDICATING EFFECT
OF FREQUENCY

MATERIAL: TITANIUM TI-6-2-4-2
CONDITION: 1790F 1HR AC, 1100F 8HRS AC
ENVIRONMENT: + 800F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|-------|---|------|---|---|
| | | A | B | C | D |
| | | F(HZ)=2 MIN. HOLD TRAPEZOIDAL WAVEFORM | | | |
| DELTA K MIN | A: | 8.97 | 5.44 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 9.00 | 5.44 | | |
| | | 10.00 | 5.69 | | |
| | 13.00 | 7.89 | | | |
| | 16.00 | 12.0 | | | |
| | 20.00 | 20.9 | | | |
| DELTA K MAX | A: | 22.81 | 29.5 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 7.30
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1700F 1HR AC, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.50
 ENVIRONMENT: + 800° F, AIR

YIELD STRENGTH: 140.9 KSI
 ULT. STRENGTH: 152.3 KSI
 SPECIMEN THK: 0.082"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-2

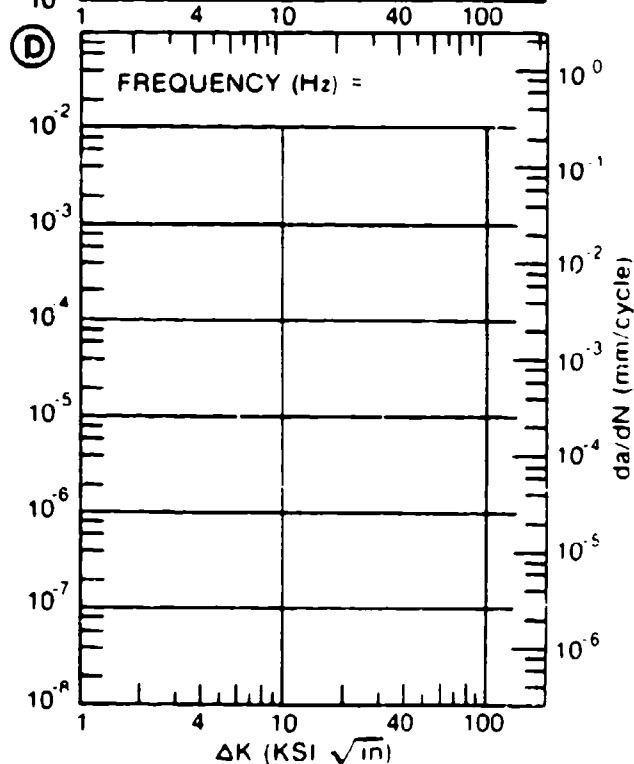
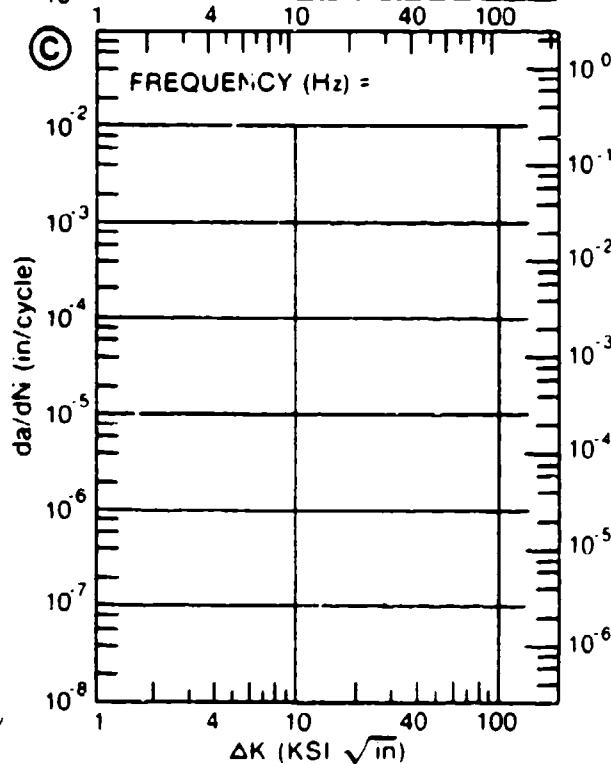
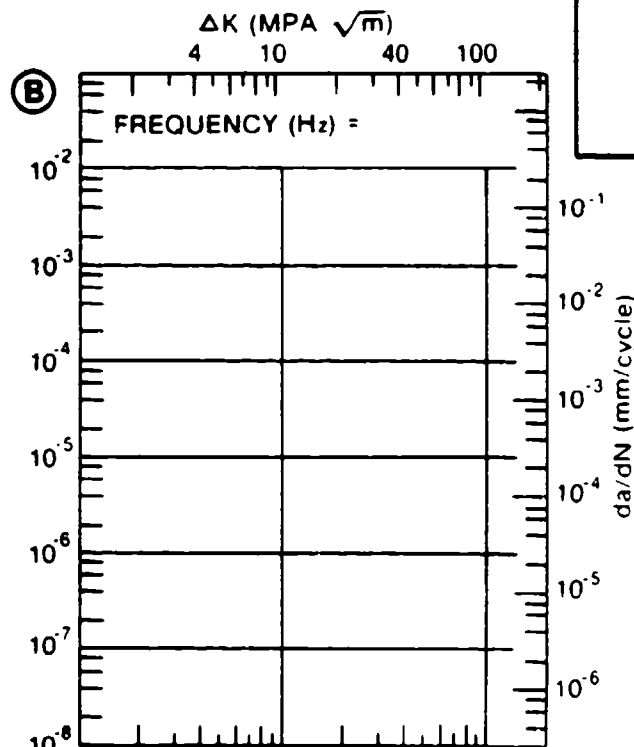
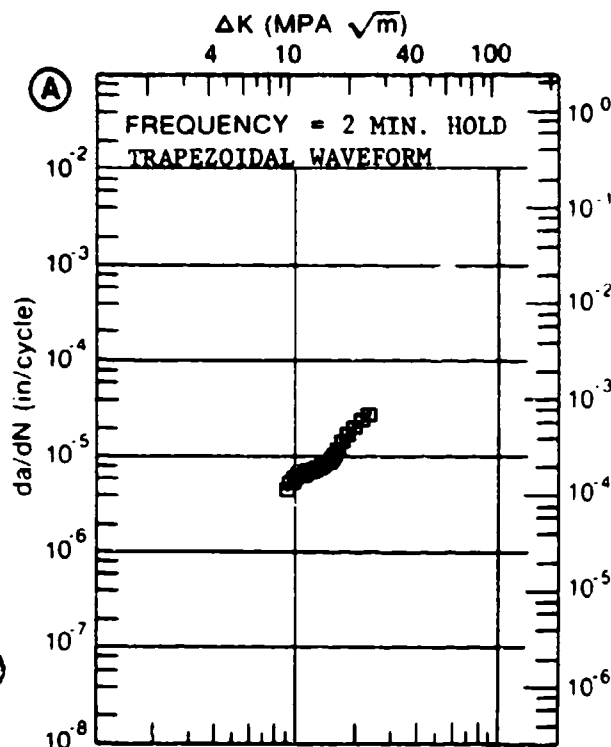


Figure 4.9.3.5

TABLE 4.10.1.1.1

FATIGUE CRACK GROWTH RATE AT DIFFERENT LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM T1-6-2-4-6

TEST CONDITIONS

SPECIMEN ORIENTATION 1-1

ENVIRONMENT AIR AT 800 F

| (IN)DIRECTION (1) | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|-------------------|--------------|--------------|------------|---|-----|------|------|------|----|-----|
| | | | | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
| | EXTRUSION | 0.10 | 20.00 | | | | 1.69 | 10.1 | | |
| | EXTRUSION | 0.30 | 20.00 | | | | 2.09 | 12.3 | | |
| | EXTRUSION | 0.50 | 20.00 | | | | 3.11 | | | |
| | EXTRUSION | 0.70 | 20.00 | | | 0.81 | 3.42 | | | |

TABLE 4.10.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI 6-2-4-6

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT AIR AT 600 F

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
|---|--------------|--------------|---|-------------------------------|---|---|----|----|----|-----|------|
| | | | | | 2.5 | 5 | 10 | 20 | 50 | 100 | |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 8HRS AC | FORGING | 0.10 | 0.16 | | | | | | | | 9.04 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 8HRS AC | FORGING | 0.10 | 30.00 | | | | | | | | 1.41 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 8HRS AC | FORGING | 0.50 | 0.16 | | | | | | | | 3.80 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 8HRS AC | FORGING | 0.50 | 2 MIN HOLD TIME TRAPEZOIDAL WAVEFORM | | | | | | | | 12.0 |

TABLE 4.10.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM Ti-6-2-4-6

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT: AIR AT 800 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---|--------------|--------------|-----------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 6HRS AC | FORGING | 0.06 | 30.00 | | 2.03 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 6HRS AC | FORGING | 0.10 | 0.16 | | 11.5 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 6HRS AC | FORGING | 0.10 | 30.00 | | 1.87 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 6HRS AC | FORGING | 0.50 | 0.16 | | 4.67 |
| 1690F 2HRS AC. 1550F 2HRS OQ. 1100F 6HRS AC | FORGING | 0.70 | 0.16 | | 2.48 6.71 |

TABLE 4.10.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.1 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6-2-4-6 | | | |
|------------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 7.20 | .185 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | .291 | | | |
| | 9.00 | .496 | | | |
| | 10.00 | .819 | | | |
| | 13.00 | 2.65 | | | |
| | 16.00 | 5.25 | | | |
| | 20.00 | 9.70 | | | |
| | 25.00 | 22.0 | | | |
| | 30.00 | 48.0 | | | |
| DELTA K | A: 33.04 | 61.9 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 21.73 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM: EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 20.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 147.2 KSI
 ULT. STRENGTH: 159.1 KSI
 SPECIMEN THK: 0.300"
 SPECIMEN WIDTH: 1.400"
 REFERENCES: UD001

TITAN.
 ALLOY
 TI-6-2-
 4-6

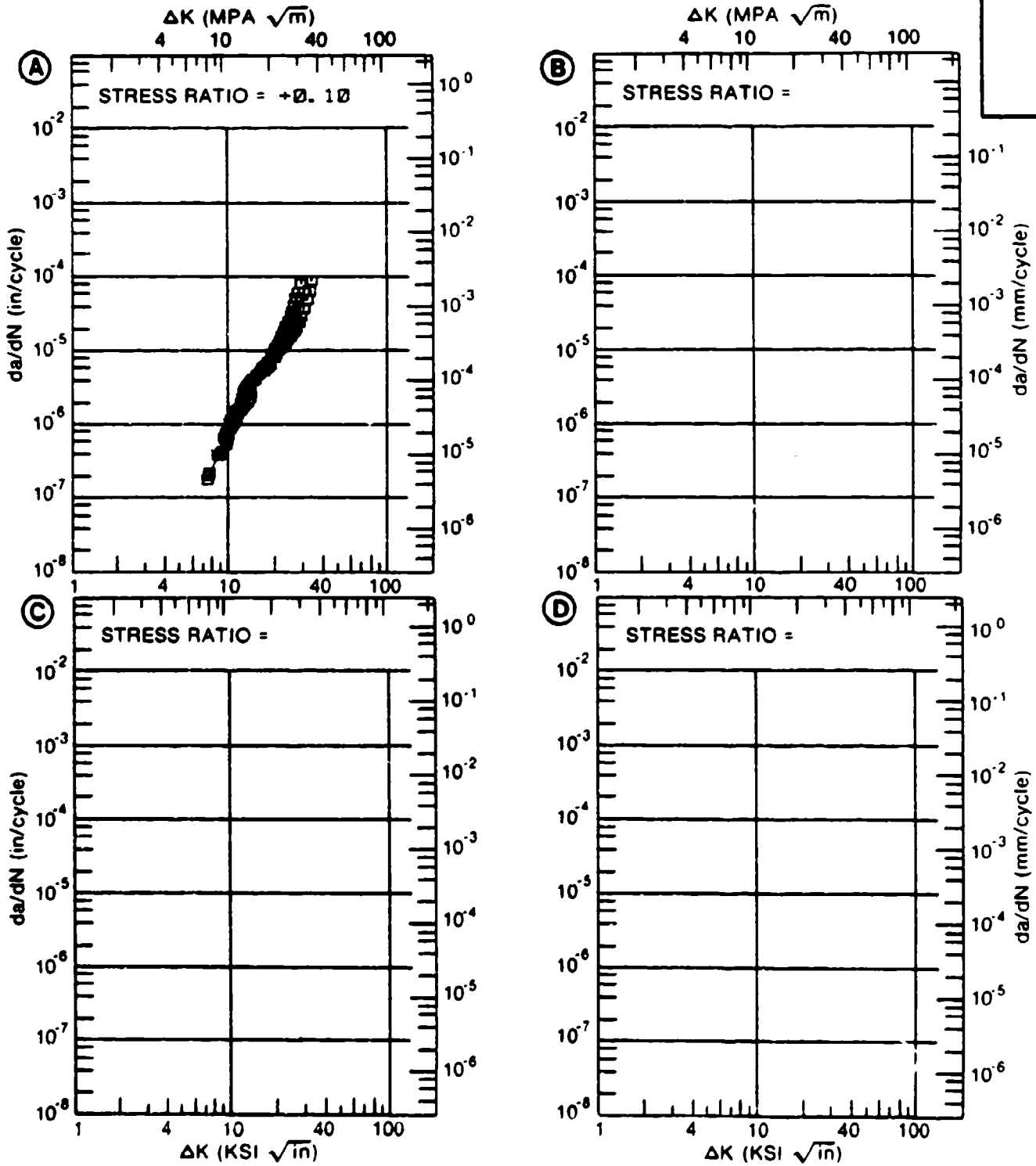


Figure 4.10.3.1

TABLE 4.10.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.2 INDICATING EFFECT

OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6-2-4-6 | | | |
|--------------------------|----------|--------------------------------------|---------|---------|---------|
| CONDITION: | | | | | |
| ENVIRONMENT: + 800F. AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.50 | R=+0.70 |
| DELTA K | A: 8.87 | 1.05 | | | |
| MIN | B: 5.52 | | .654 | | |
| | C: 5.54 | | | .861 | |
| | D: 4.89 | | | | .815 |
| | 5.00 | | | | .819 |
| | 6.00 | | .747 | .977 | .976 |
| | 7.00 | | .984 | 1.31 | 1.31 |
| | 8.00 | | 1.28 | 1.77 | 1.83 |
| | 9.00 | 1.14 | 1.65 | 2.37 | 2.53 |
| | 10.00 | 1.69 | 2.09 | 3.11 | 3.42 |
| | 13.00 | 3.27 | 3.96 | 6.30 | 6.81 |
| | 16.00 | 5.65 | 6.77 | 10.8 | |
| | 20.00 | 10.1 | 12.3 | | |
| | 25.00 | 17.1 | 22.5 | | |
| | 30.00 | 24.7 | 36.9 | | |
| | 35.00 | | 55.4 | | |
| DELTA K | A: 33.38 | 29.7 | | | |
| MAX | B: 35.34 | | 56.8 | | |
| | C: 19.33 | | | 16.9 | |
| | D: 13.67 | | | | 7.59 |
| ROOT MEAN SQUARE | | 10.51 | 7.69 | 4.42 | 9.94 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM: EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 20.00 HZ
 ENVIRONMENT: + 800° F. AIR

YIELD STRENGTH: 147.2 KSI
 ULT. STRENGTH: 159.1 KSI
 SPECIMEN THK: 0.300"
 SPECIMEN WIDTH: 1.400"
 REFERENCESUD001

TITAN.
ALLOY

TI-6-2-
4-6

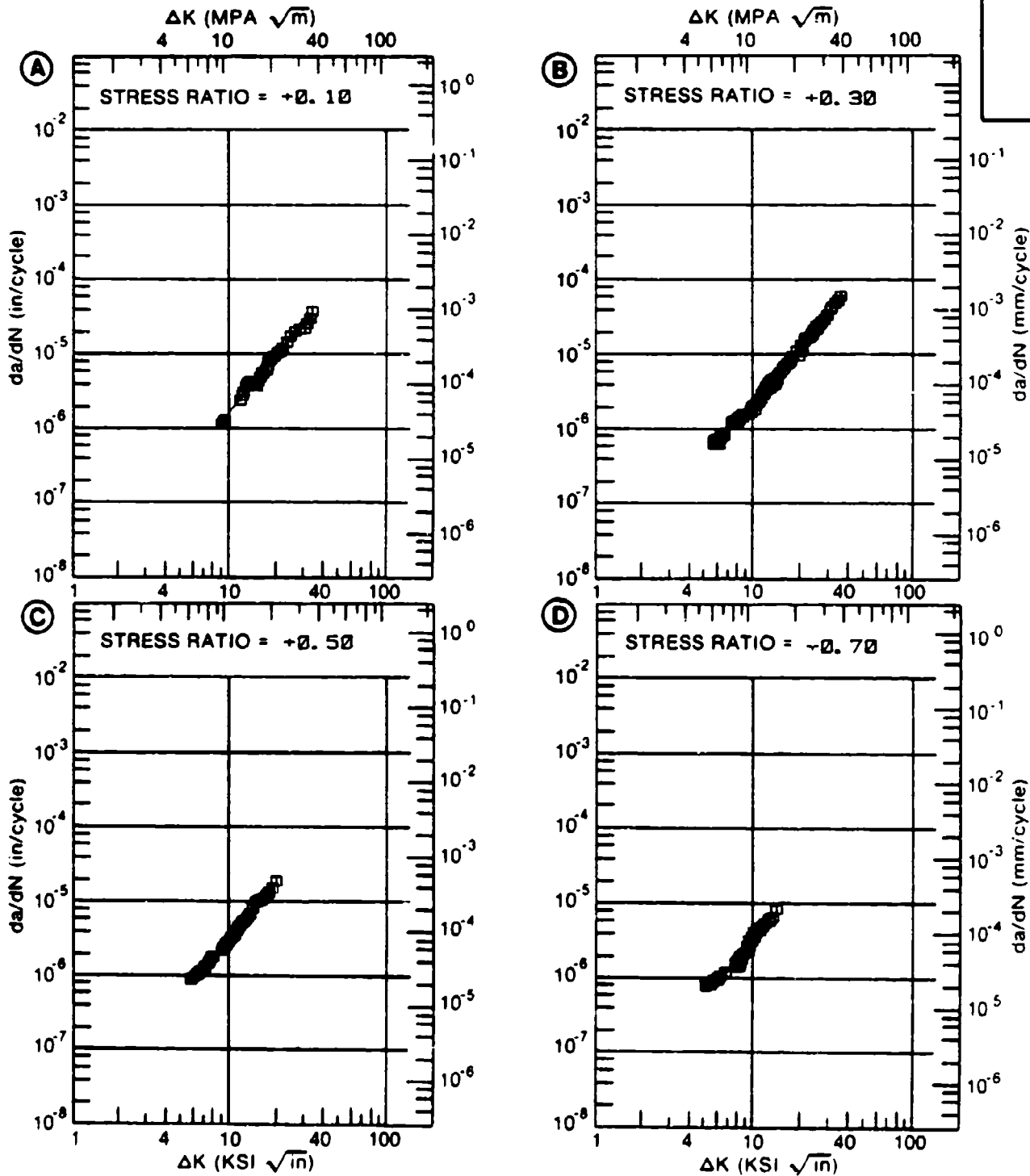


Figure 4.10.3.2

TABLE 4.10.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.3 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6-2-4-6
CONDITION: 1690F 2HRS AC, 1550F 2HRS OG, 1100F 8HRS
AC

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|--------------------------------------|------|---|---|
| | A | B | C | D |
| | E=+ 800F AIR | | | |
| DELTA K MIN | A: 5.05 | .43 | | |
| | B: 6.00 | .587 | | |
| | C: 7.00 | .816 | | |
| | D: 8.00 | 1.12 | | |
| | 9.00 | 1.52 | | |
| | 10.00 | 2.03 | | |
| | 13.00 | 4.36 | | |
| DELTA K MAX | A: 14.76 | 6.43 | | |
| | B: | | | |
| | C: | | | |
| | D: | | | |

ROOT MEAN SQUARE 5.79
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1800F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 1.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.08
 FREQUENCY: 30.00 HZ

YIELD STRENGTH: 185.5 KSI
 ULT. STRENGTH: 180.8 KSI
 SPECIMEN THK: 0.077"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
ALLOY

TI-6-2-
4-8

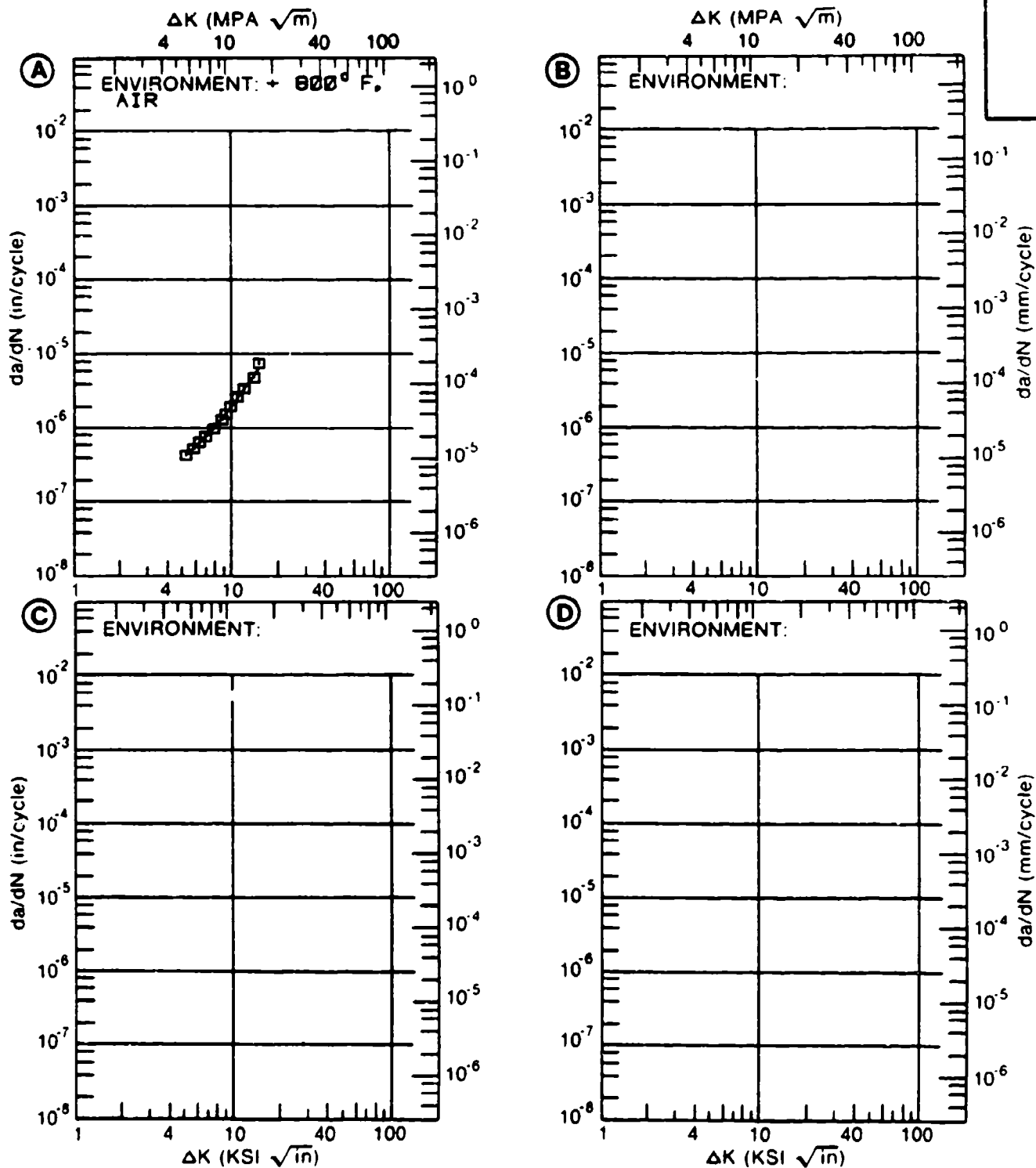


Figure 4.10.3.3

TABLE 4.10.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.4 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6-2-4-6
CONDITION: 1690F 2HRS AC, 1550F 2HRS DG, 1100F 8HRS AC

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E=+ 600F | | | |
| | | AIR | | | |
| DELTA K | A: 13.85 | 4.87 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 7.10 | | | |
| | 20.00 | 12.0 | | | |
| | 25.00 | 19.6 | | | |
| | 30.00 | 29.6 | | | |
| | 35.00 | 43.1 | | | |
| | 40.00 | 61.6 | | | |
| DELTA K | A: 47.39 | 103. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 8.21
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1690F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 1.80" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.50
 FREQUENCY: 2 MIN. HOLDTIME
 TRAPEZOIDAL WAVEFORM

YIELD STRENGTH: 165.5 KSI
 ULT. STRENGTH: 180.8 KSI
 SPECIMEN THK: 0.074"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY
 TI-6-2-
 4-6

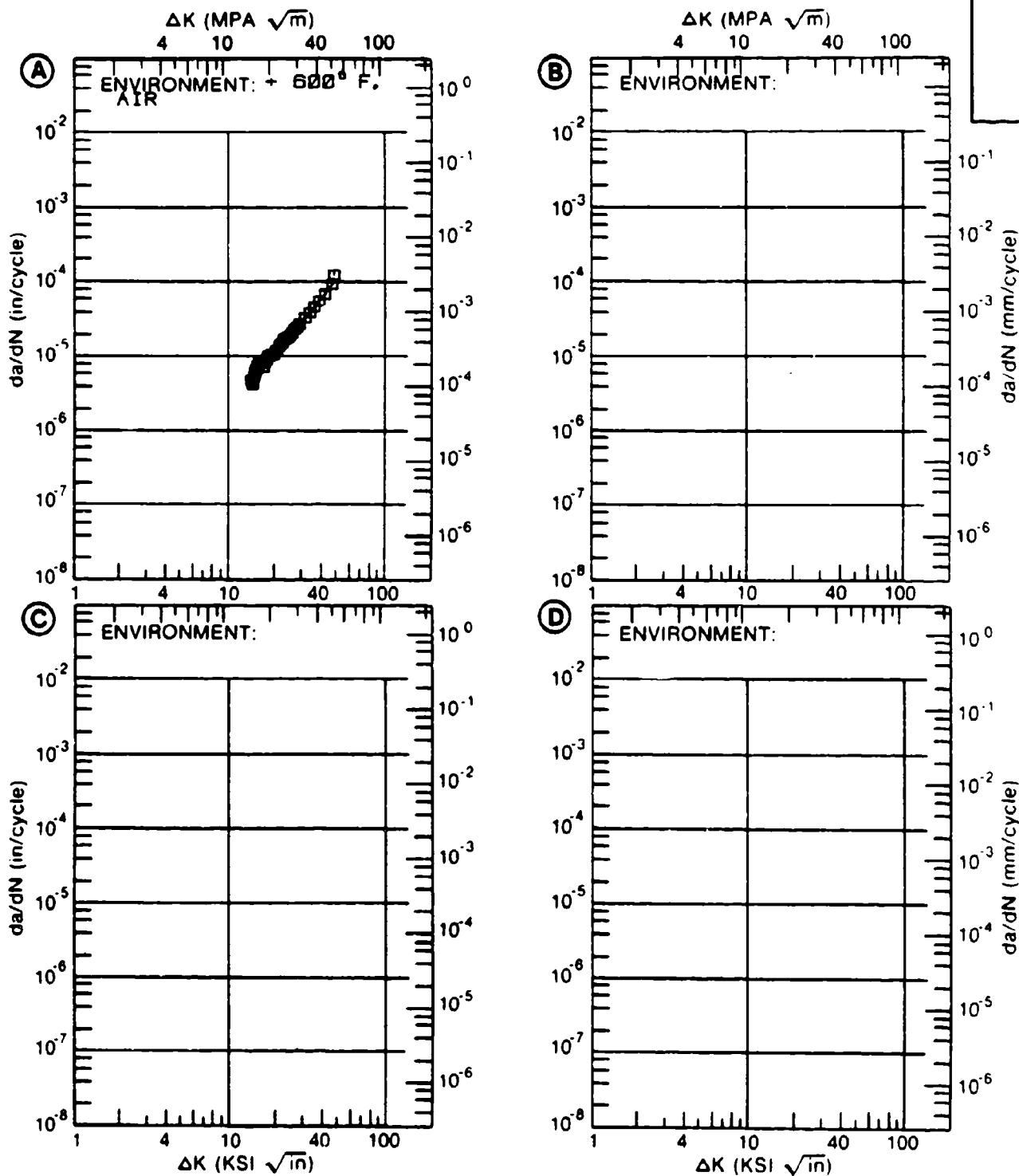


Figure 4.10.3.4

TABLE 4.10.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.5 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6-2-4-6
CONDITION: 1690F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS
AC

| DELTA K (KBI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---|---|---|
| | | A | B | C | D |
| | | E → 800F | | | |
| | | AIR | | | |
| DELTA K | A: 4.73 | 2.46 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | 2.48 | | | |
| | 6.00 | 2.81 | | | |
| | 7.00 | 3.43 | | | |
| | 8.00 | 4.31 | | | |
| | 9.00 | 5.40 | | | |
| | 10.00 | 6.71 | | | |
| | 13.00 | 11.6 | | | |
| DELTA K | A: 14.43 | 14.3 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 5.34
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1800F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 1.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.70
 FREQUENCY: 0.16 HZ

YIELD STRENGTH: 185.5 KSI
 ULT. STRENGTH: 180.8 KSI
 SPECIMEN THK: 0.083"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-6

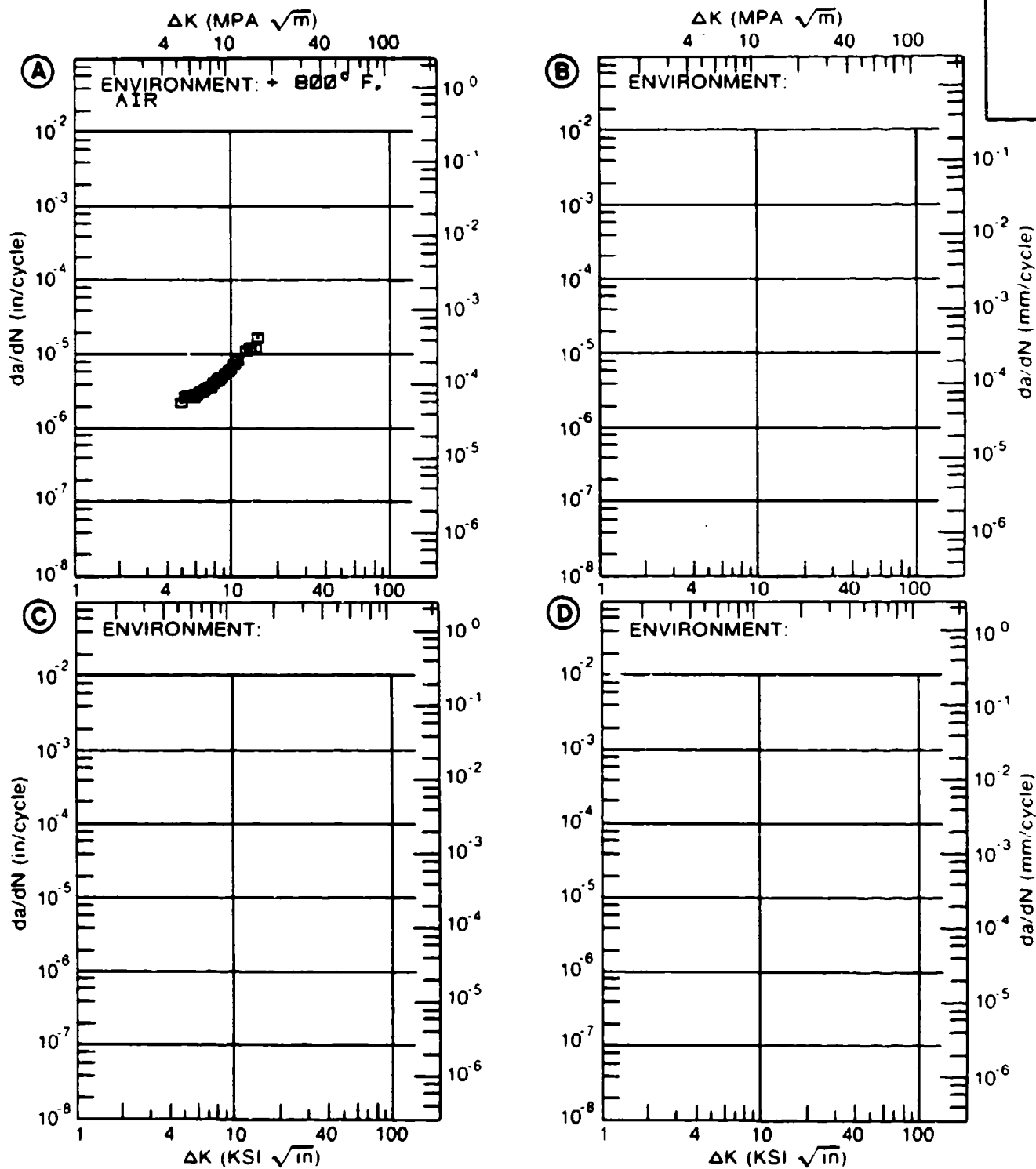


Figure 4.10.3.5

TABLE 4.10.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.6 INDICATING EFFECT
OF ENVIRONMENT

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|--|---------------------------------------|-----------------|-----------------|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E=+ 600F AIR | E=+ 800F AIR | |
| DELTA K MIN | A: 4.87 | .09 | | | |
| | B: 8.23 | | .71 | | |
| | C: 8.51 | | | 1.09 | |
| | D: | | | | |
| | 5.00 | .105 | | | |
| | 6.00 | .185 | | | |
| | 7.00 | .314 | | | |
| | 8.00 | .496 | | | |
| | 9.00 | .718 | .991 | 1.36 | |
| | 10.00 | .985 | 1.41 | 1.87 | |
| | 13.00 | 2.44 | 3.20 | 3.49 | |
| | 16.00 | | 6.41 | 7.28 | |
| DELTA K MAX | A: 14.06 | 5.88 | | | |
| | B: 17.43 | | 8.91 | | |
| | C: 17.28 | | | 11.0 | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 5.96 | 3.55 | 6.28 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: 1600F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 2.80" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.10
 FREQUENCY: 30.00 HZ

YIELD STRENGTH: 186.0 KSI
 ULT. STRENGTH: 182.3 KSI
 SPECIMEN THK: 0.078- 0.082"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
 ALLOY

TI-6-2-
 4-6

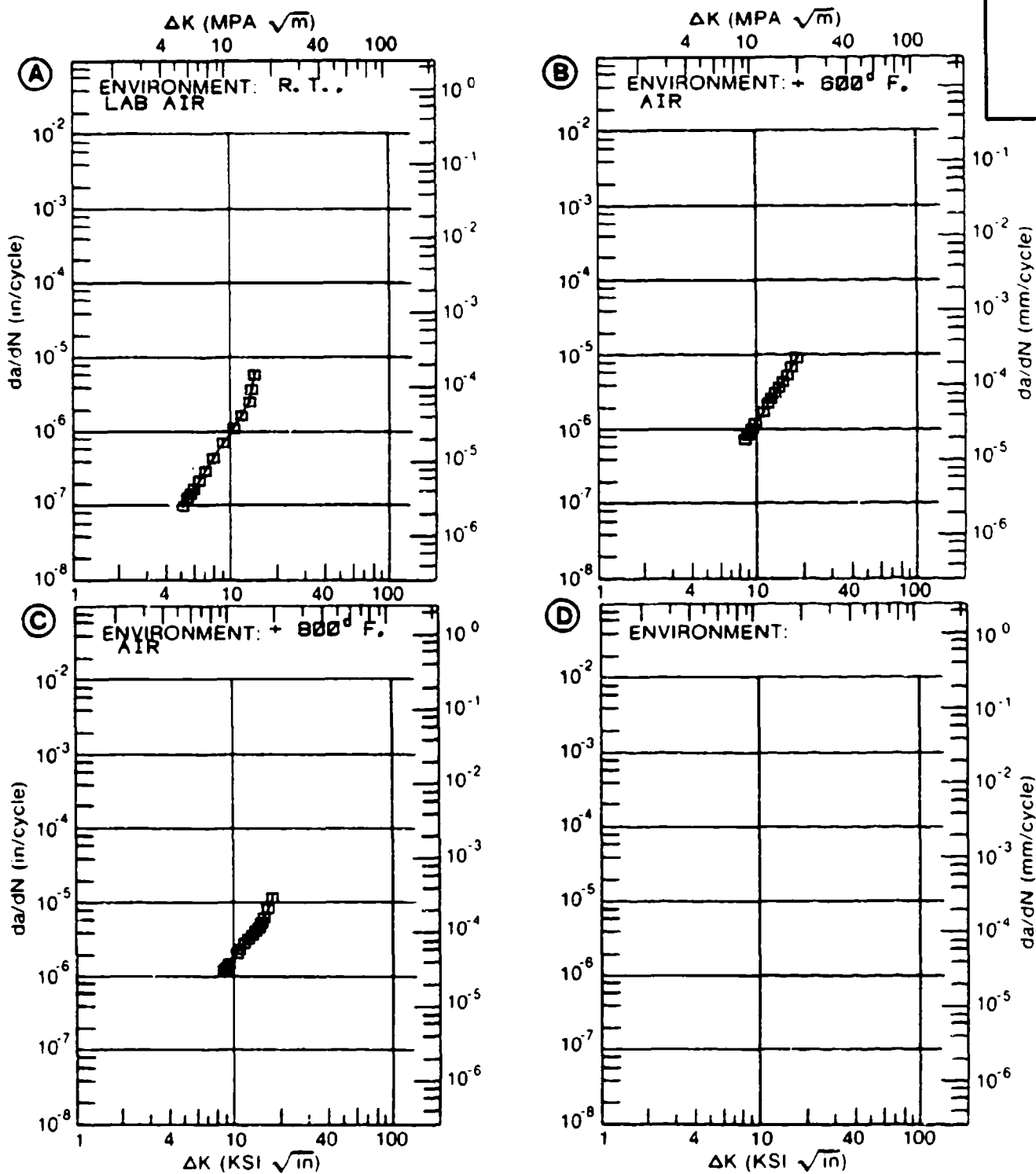


Figure 4.10.3.6

TABLE 4.10.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.7 INDICATING EFFECT
OF ENVIRONMENT

| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
|---------------------------------------|----------|---------------------------|--|-----------|--|
| | | A | | B | |
| | | E==+ 600F | | E==+ 800F | |
| | | AIR | | AIR | |
| DELTA K MIN | A: 10.60 | 1.71 | | 4.20 | |
| | B: 13.03 | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 2.58 | | 6.96 | |
| | 16.00 | 4.56 | | 11.5 | |
| | 20.00 | 9.04 | | 18.9 | |
| | 25.00 | 17.6 | | 29.3 | |
| | 30.00 | 28.0 | | 44.4 | |
| | 35.00 | | | | |
| DELTA K MAX | A: 32.52 | 33.1 | | 61.4 | |
| | B: 39.00 | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.22 | | 7.08 | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | | | | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: 1000F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.10
 FREQUENCY: 0.16 HZ

YIELD STRENGTH: 186.0 KSI
 ULT. STRENGTH: 192.3 KSI
 SPECIMEN THK: 0.079- 0.081"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
ALLOY

TI-6-2-
4-6

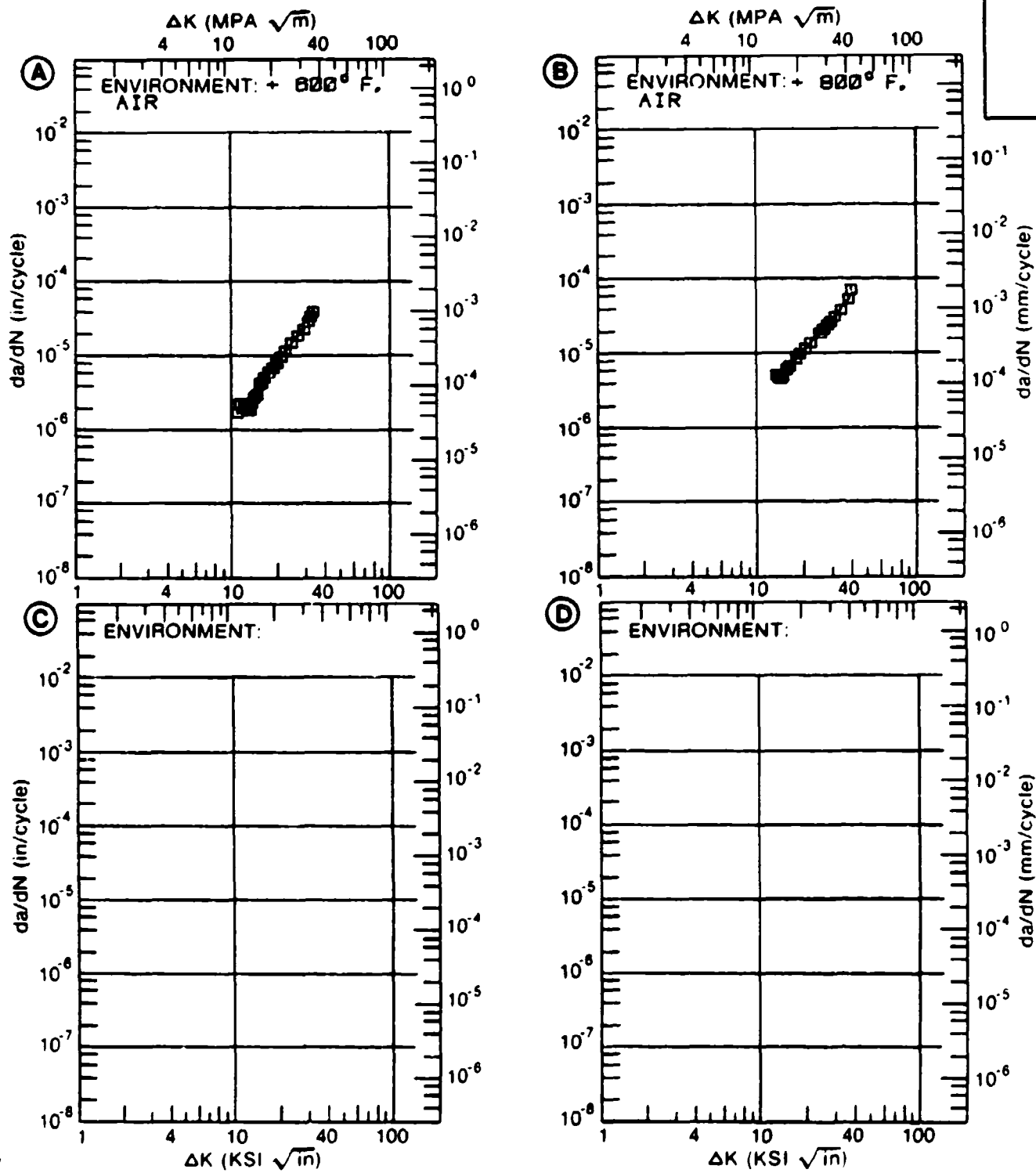


Figure 4.10.3.7

TABLE 4.10.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.8 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6-2-4-6
CONDITION: 1690F 2HRS AC, 1550F 2HRS OG, 1100F 8HRS
AC

| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
|---------------------------------------|--|--------------------------|-----------------|---|---|
| | | A | B | C | D |
| | | E=+ 600F AIR | E=+ 800F AIR | | |
| DELTA K MIN | A: 7.88 | 1.35 | | | |
| | B: 8.16 | | 3.26 | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | 1.51 | | | |
| | 9.00 | 2.80 | 3.82 | | |
| | 10.00 | 3.80 | 4.67 | | |
| | 13.00 | | 8.96 | | |
| | 16.00 | | 18.1 | | |
| DELTA K MAX | A: 12.83 | 7.75 | | | |
| | B: 16.58 | | 20.9 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 6.25 | 4.12 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: 1800F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 2.80" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.50
 FREQUENCY: 0.18 HZ

YIELD STRENGTH: 186.0 KSI
 ULT. STRENGTH: 182.3 KSI
 SPECIMEN THK: 0.080- 0.081"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
ALLOY

TI-8-2-
4-6

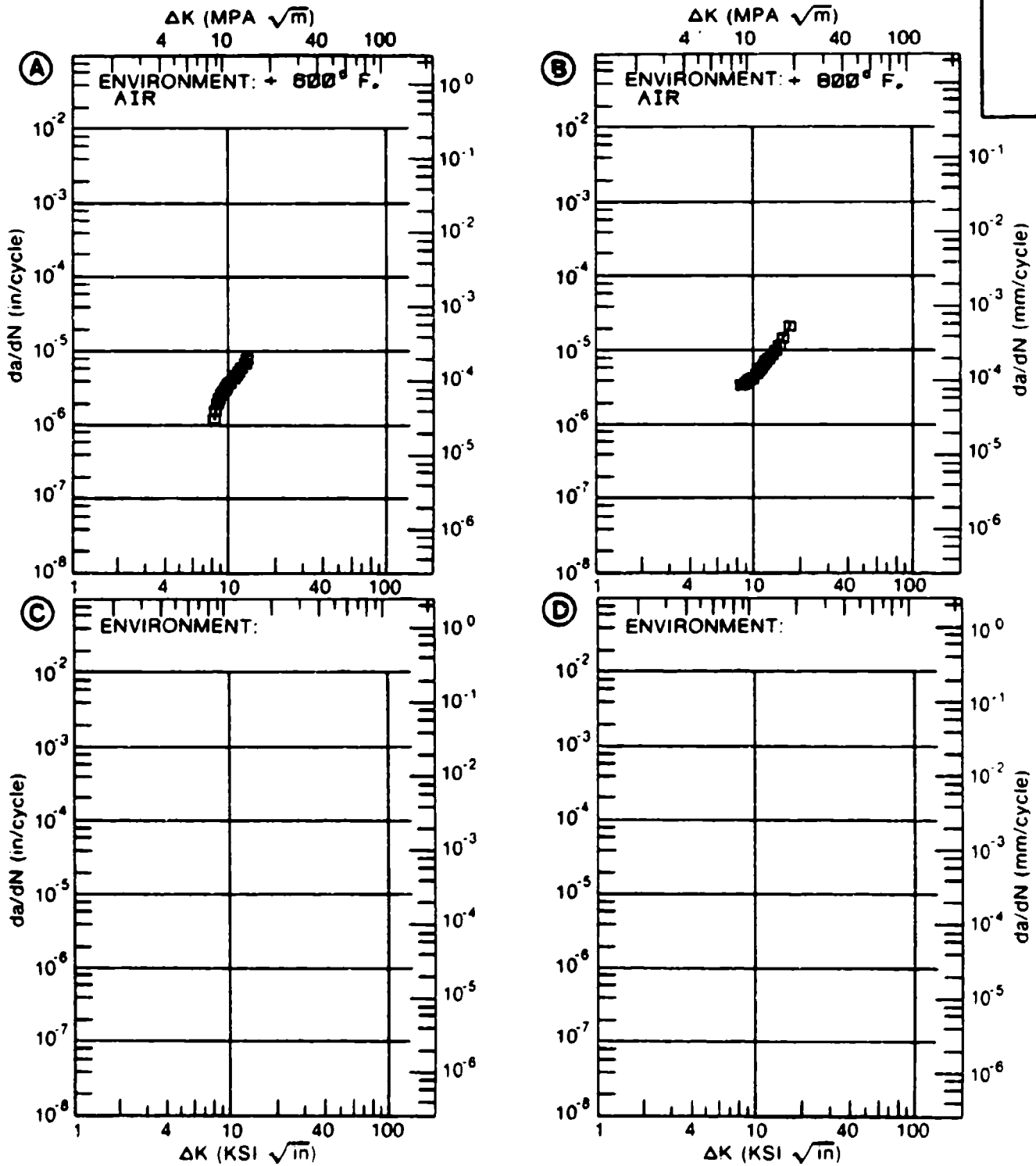


Figure 4.10.3.8

TABLE 4.10.3.9

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.10.3.9 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6-2-4-6 | | | |
|--|--|---------------------------------------|---------------------------------|--------------------------|---|
| CONDITION: 1690F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR .16HZ | E= R. T. LAB AIR 999.99HZ | E=+ 600F AIR .16HZ | |
| DELTA K MIN | A: 3.89 | .31 | | | |
| | B: 1.86 | | .00 | | |
| | C: 4.41 | | | .79 | |
| | D: | | | | |
| | 2.00 | | .0130 | | |
| | 2.50 | | .0636 | | |
| | 3.00 | | .121 | | |
| | 3.50 | | .176 | | |
| | 4.00 | .317 | .237 | | |
| | 5.00 | .524 | .460 | 1.12 | |
| | 6.00 | 1.53 | | 1.65 | |
| | 7.00 | 4.73 | | 2.18 | |
| | 8.00 | 12.2 | | 2.80 | |
| | 9.00 | | | 3.61 | |
| | 10.00 | | | 4.74 | |
| | 13.00 | | | 12.5 | |
| DELTA K MAX | A: 8.59 | 18.9 | | | |
| | B: 5.84 | | 1.48 | | |
| | C: 14.50 | | | 22.0 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.54 | 20.47 | 7.74 | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: 1800F 2HRS AC, 1550F 2HRS OQ, 1100F 8HRS AC
 FORM: 2.80" TH FORGING
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.70
 FREQUENCY:

YIELD STRENGTH: 186.0 KSI
 ULT. STRENGTH: 182.3 KSI
 SPECIMEN THK: 0.079- 0.081"
 SPECIMEN WIDTH: 1.750"
 REFERENCES: PW002

TITAN.
ALLOY

TI-8-2-
4-8

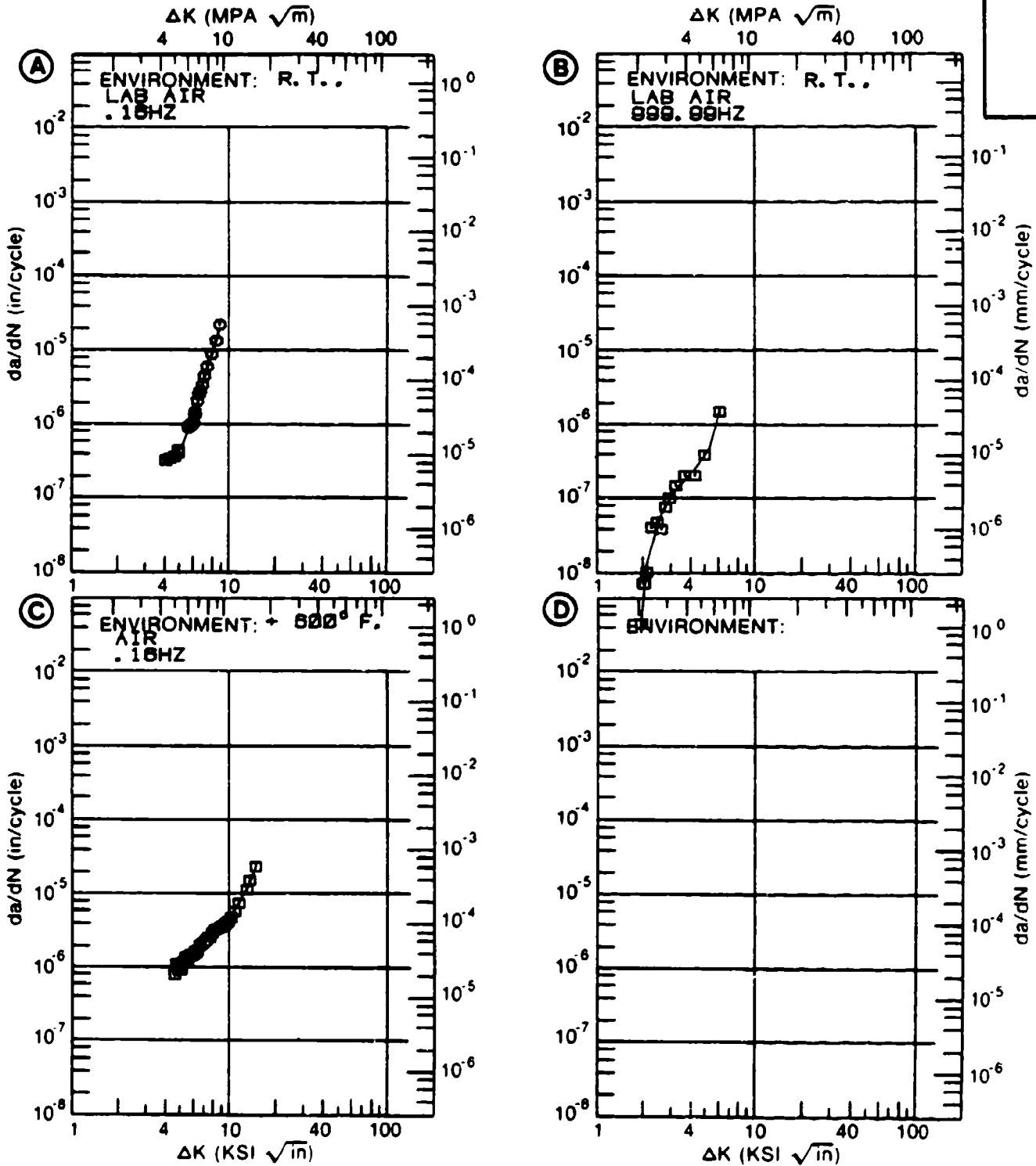


Figure 4.10.3.9

TABLE 4.11.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY TI-6AL-4V AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI BURTIN) DEVIATION | | (NUMBER OF SPECIMENS) | |
|--|---|------------------|-----------------------|----------------|
| | K _{IC} | S _D | K _{IC} | S _D |
| ANNEALED 1375F 3HR. AC | 60.4 ± 5.9 (2) | --- | --- | --- |
| BETA PROCESSED MILL ANNEALED | 94.9 ± 4.8 (3) | --- | --- | --- |
| MILL ANNEAL | 55.6 ± 1.3 (2) | --- | --- | --- |
| MILL ANNEALED | --- | 100.6 ± 6.8 (6) | --- | --- |
| RECRYSTALLIZE ANNEAL | 82.8 ± 7.8 (22) | 80.8 ± 10.8 (22) | --- | --- |
| STA | --- | 42.6 ± 2.0 (3) | --- | --- |
| 1750F 1HR FC TO 1100F. AC | --- | 91.5 ± 2.1 (2) | --- | --- |
| 1750F 1HR. FC TO RT | 71.8 ± 3.2 (2) | 91.6 ± 1.3 (2) | --- | --- |
| 1750F 2HR. HB. 1000F 2HR. AC. 1300F 2HR. AC. STA | 41.4 ± 2.3 (2) | --- | --- | --- |
| FORGING | | | | |
| AB FORGED-MA ALPHA-BETA FORGED. MILL ANNEALED | --- | 35.4 ± 2.7 (4) | --- | --- |
| ANNEALED | 84.4 ± 1.8 (2) | 83.4 ± 9.9 (2) | --- | --- |
| ANNEALED 1300F 4 HR. AC | 58.1 ± 1.2 (3) | 62.2 ± 3.0 (3) | 68.1 ± 1.0 (2) | --- |

TABLE 4.11.1.1 (con't)

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY TI-6AL-4V AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|--|---|--------------------------------|
| | FORGING | |
| | L-I | B-I |
| B FORGED-FA BETA FORGED, MILL ANNEALED 1300F 2 HR. AC | 70.6 ± 4.9 (3) | 71.0 ± 0.4 (3) 73.9 ± 2.5 (2) |
| MILL ANNEALED 1300F 2 HR. AC | 47.7 ± 2.9 (3) | 49.9 ± 3.9 (3) 43.6 ± 3.8 (3) |
| RECRYSTALLIZE ANNEAL | 83.6 ± 5.9 (41) | 83.9 ± 6.9 (50) 86.9 ± 3.2 (9) |
| 1700F 6 HR. AC, 1400F 6 HR. AC | 79.9 ± 4.2 (6) | 81.2 ± 5.0 (6) ----- |
| 1750F 1 HR. WD, 1000F 4 HR | ----- | 79.3 ± 4.9 (3) ----- |
| | EXTRUSION | |
| | L-I | B-I |
| ANNEALED | ----- | 73.3 ± 2.3 (2) ----- |
| MILL ANNEALED | 83.9 ± 3.1 (9) | 87.5 ± 4.1 (6) ----- |
| | FORGED BAR | |
| | L-I | B-I |
| AS RECEIVED | 97.1 ± 10.4 (14) | 94.9 ± 10.8 (21) ----- |
| B FORGED BETA FORGED REHEATED TO 1950F DRAIN TO SIZE, ANNEALED 1300F | ----- | 42.6 ± 4.3 (4) ----- |

TABLE 4.11.1.1 (con't)

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY T1-6AL-4V AT ROOM TEMPERATURE

| CONDITION/MT | MEAN K _{IC} ± STANDARD DEVIATION | | BILLET | K _{IC} | K _{IC} |
|---------------------------------|---|-----------|-------------|-----------------|-----------------|
| | (KSI) | (BMT(IN)) | | | |
| ANNEALED | 79.6 ± 9.6 | (2) | | | |
| ANNEALED 1000F 2 HR. AC | 50.9 ± 0.6 | (2) | | | |
| DIFFUSION BOND ANNEALED | 68.2 ± 9.7 | (9) | 64.2 ± 11.8 | (13) | |
| MILL ANNEALED 1300F 2 HR. AC | 84.0 ± 3.4 | (3) | | | |

TABLE 4.11.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: DRY AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|-------------------------------|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.10 | 6.00 | | 0.22 9.19 |
| BA | PLATE | 0.10 | 6.00 | | 0.06 5.42 85.6 |
| BA | PLATE | 0.30 | 6.00 | | 0.30 9.75 |
| BA | PLATE | 0.50 | 6.00 | | 1.19 10.9 |
| <hr/> | | | | | |
| BETA PROCESSED -MILL ANNEALED | SHEET | 0.10 | 10.00 | | 48.8 |
| BETA PROCESSED -MILL ANNEALED | PLATE | 0.10 | 10.00 | | 4.51 |
| BETA PROCESSED -MILL ANNEALED | PLATE | 0.10 | 10.00 | | 48.7 |
| BETA PROCESSED -MILL ANNEALED | PLATE | 0.10 | 10.00 | | 4.66 |

TABLE 4.11.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: L.H.A.
AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | |
|--------------|--------------|--------------|------------|-----------------------------------|--|---|------|-------------|------|-----|
| | | | | | 2.5 | 5 | 10 | 20 | 50 | 100 |
| DBTC | PLATE | 0.08 | 1.00 | | | | 16.4 | 753 | | |
| DBTC | PLATE | 0.30 | 1.00 | SPEC THK=1.00" | | | 0.35 | 13.1 | 265 | |
| DBTC | PLATE | 0.30 | 1.00 | SPEC THK=0.50" | | | 0.62 | 19.4 | 2180 | |
| MA | SHEET | 0.08 | 6.00 | | | | 1.79 | 13.7 | | |
| MA | SHEET | 0.30 | 6.00 | | | | 2.24 | | | |
| MA | SHEET | 0.50 | 6.00 | | | | 2.30 | 21.1 | | |
| MA | PLATE | 0.30 | 1.00 | DATA OUT OF TREND | | | | <u>72.6</u> | | |
| MA | PLATE | 0.30 | 1.00- 6.00 | | | | 0.42 | 24.7 | 402 | |
| MA | PLATE | 0.30 | 1.00- 6.00 | | | | 0.46 | 11.2 | 255 | |
| MA | EXTRUSION | 0.08 | 1.00 | | | | | 13.9 | | |
| MA | EXTRUSION | 0.08 | 6.00 | | | | 0.37 | 11.7 | | |
| MA | EXTRUSION | 0.30 | 6.00 | | | | | 16.8 | | |
| MA | EXTRUSION | 0.50 | 6.00 | | | | | 17.3 | | |
| RA | PLATE | 0.08 | 6.00 | | | | | 10.4 | | |
| RA | PLATE | 0.08 | 6.00 | | | | | 7.80 | | |
| RA | PLATE | 0.08 | 6.00 | DATA OUT OF TREND | | | | <u>3.34</u> | 145 | |
| RA | PLATE | 0.08 | 6.00 | | | | 0.72 | 11.3 | | |

TABLE 4.11.1.3 (Con't)

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: L.H.A.
AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-------------------------------|-----|---|------|------|-----|-----|
| RA | PLATE | 0.08 | 6.00 | | | | 0.49 | 9.42 | 171 | |
| RA | PLATE | 0.30 | 6.00 | | | | 1.39 | 15.9 | | |
| RA | PLATE | 0.50 | 6.00 | | | | 1.94 | 16.8 | | |
| RA | PLATE | 0.70 | 6.00 | | | | 3.12 | | | |
| RA | FORGING | 0.08 | 1.00 | | | | 0.38 | 5.78 | 166 | |
| RA | FORGING | 0.08 | 6.00 | | | | | 6.76 | | |
| RA | FORGING | 0.30 | 6.00 | | | | 1.22 | 16.2 | 324 | |

TABLE 4.11.1.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT LAB AIR AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|-------------------------------|--------------|--------------|-------------|-------------------------------|---|
| ANNEALED | BILLET | 0.02 | 10 00-20.00 | 2.5 5 10 20 50 100 | 0.27 9.49 |
| ANNEALED AT 1375F. 3HRS. AC | PLATE | 0.02 | 10 00-20.00 | | 0.28 9.70 |
| SA | FORGING | 0.02 | 0.10-20.00 | | 2.55 102 |
| RETA PROCESSED -MILL ANNEALED | PLATE | 0.10 | 1.00 | | 0.91 |
| DETA PROCESSED MILL ANNEALED | PLATE | 0.50 | 1.00 | | 1.47 |
| MA | PLATE | -1.00 | 10.00 | | 1.14 12.8 328 |
| MA | PLATE | 0.02 | 0.10-30.00 | DATA OUT OF TREND | 0.01 0.44 (12.4) |
| MA | PLATE | 0.02 | 0.10-30.00 | | 0.15 5.92 |
| MA | PLATE | 0.04 | 20.00 | | 96.5 |
| MA | PLATE | 0.05 | 20.00 | | 6.97 |
| MA | PLATE | 0.30 | 20.00 | | 0.99 |
| MA | PLATE | 0.50 | 10.00 | | 8.52 92.4 |
| MA | FORGING | 0.02 | 1.00-30.00 | | 8.18 292 |

TABLE 4.11.1.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: H.H.A.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.10 | 0.10 | | 4.10 115 |
| BA | PLATE | 0.30 | 0.10 | | 9.31 |
| BA | PLATE | 0.50 | 0.10 | | 12.0 1009 |

TABLE 4.11.1.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM T1-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT: J.P. 4
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 30 | 50 | 100 |
|---|--------------|--------------|------------|--------------------------------|-----|---|------|------|------|--------|-----|
| FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | | | | | | |
| BA | FORGING | 0.02 | 0.10-20.00 | | | | | 2.08 | 88.2 | 4343.0 | |
| MA | EXTRUSION | 0.08 | 6.00 | | | | 1.47 | 12.9 | | | |
| MA | EXTRUSION | 0.08 | 1.00 | | | | | 12.0 | | | |
| RA | PLATE | 0.08 | 1.00 | | | | 0.66 | 12.8 | | | |
| RA | FORGING | 0.08 | 1.00 | | | | | 5.54 | | | |

TABLE 4.11.1.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS:

SPECIMEN ORIENTATION L-T

ENVIRONMENT: S.T.M.
AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-------------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.10 | 1.00 | | 11.1 163 |
| ----- | | | | | |
| DBTC | PLATE | 0.08 | 1.00 | | 0.62 13.9 |
| ----- | | | | | |
| MA | SHEET | 0.08 | 1.00 | | 3.22 |
| MA | PLATE | 0.03 | 1.00 | SPEC THK=0.50" | 87.5 |
| MA | PLATE | 0.03 | 1.00 | SPEC THK=1.00" | 589 31.3 |
| MA | EXTRUSION | 0.08 | 1.00 | | 14.3 266. |
| MA | EXTRUSION | 0.10 | 1.00--10.00 | | 11.2 254. |
| ----- | | | | | |
| RA | PLATE | 0.08 | 0.10 | | 11.0 |
| RA | PLATE | 0.08 | 1.00 | | 0.59 8.98 344 |
| RA | PLATE | 0.08 | 1.00 | | 9.34 |
| RA | PLATE | 0.08 | 1.00 | | 0.77 13.4 |
| RA | PLATE | 0.30 | 1.00 | | 2.27 24.5 |
| RA | PLATE | 0.50 | 1.00 | | 4.23 |
| RA | FORGING | 0.08 | 1.00 | | 1.65 36.8 |

TABLE 4.11.1.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 TITANIUM TI-6AL-4V

TEST CONDITIONS
 SPECIMEN ORIENTATION T-S ENVIRONMENT: 3.5% NaCl AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.10 | 10.00 | | 0.62 17.6 |
| RA | PLATE | 0.10 | 10.00 | | 49.7 |

TABLE 4.11.1.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT DRY AIR AT RT

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|---|
| RA | PLATE | 0.10 | 0.10 | 2.5 | 50 |
| RA | PLATE | 0.10 | 1.00 | 2.5 | 20 |
| RA | PLATE | 0.50 | 0.10 | 2.5 | 10 |
| RA | PLATE | 0.50 | 1.00 | 2.5 | 5 |
| | | | | | 100 |
| | | | | | 224 |
| | | | | | 9.08 |
| | | | | | 164 |
| | | | | | 1.08 |
| | | | | | 20.4 |
| | | | | | 1.52 |
| | | | | | 17.2 |

TABLE 4.11.1.10

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: L.H.A.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-----------------------------------|-----|---|------|------|------|-----|
| DB | PLATE | 0.08 | 6.00 | | | | 0.39 | 12.1 | | |
| DB | PLATE | 0.30 | 6.00 | | | | | 33.1 | | |
| ----- | | | | | | | | | | |
| DBTC | PLATE | 0.08 | 1.00 | | | | | 7.70 | 169 | |
| DBTC | PLATE | 0.30 | 1.00 | | | | 0.56 | 12.5 | 278 | |
| ----- | | | | | | | | | | |
| MA | SHEET | 0.08 | 6.00 | | | | | | 9.22 | |
| MA | PLATE | 0.30 | 1.00-6.00 | | | | 0.46 | 11.2 | 255 | |
| MA | EXTRUSION | 0.08 | 6.00 | | | | | 12.7 | | |
| ----- | | | | | | | | | | |
| RA | PLATE | 0.08 | 6.00 | | | | 0.53 | 11.4 | 208 | |
| RA | PLATE | 0.08 | 6.00 | | | | | 9.89 | | |
| RA | FORGING | 0.08 | 6.00 | | | | | 7.65 | 135 | |
| RA | FORGING | 0.30 | 6.00 | | | | 2.68 | 19.8 | | |

TABLE 4.11.1.11

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION: T-L

ENVIRONMENT: LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--|--------------|--------------|------------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| AS WELDED E B WELDMENT (WELD ZONE) | WELDMENT | 0.10 | 10.00 | | 5.94 |
| AS WELDED E. B. WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 10.00 | | 6.52 |
| BA | FORGING | 0.02 | 0 10-20.00 | | 2.27 103 3242 |
| MA | EXTRUSION | 0.10 | 5 00-20.00 | | 13.7 261. |
| RA | PLATE | 0.10 | 10.00 | | 21.3 |
| STRESS RELIEVED E. B. WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 0 10-10.00 | | 14.2 344 |
| STRESS RELIEVED E. B. WELDMENT (WELD ZONE) | WELDMENT | 0.10 | 0 10-10.00 | | 10.1 |

TABLE 4.11.1.12

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: AIR AT 175 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| NA | PLATE | 0.10 | 0 10-10.00 | | 11.7 135 |
| STRESS RELIEVED E B WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 0 10-10.00 | | 8.82 150 |

TABLE 4.11.1.13

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: H.H.A.
AT R.T.

| CONDITION/HT | PRODUCT FURN | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-----------|-------------------------------|-----|------|------|------|----|-----|---|
| RA | PLATE | 0.10 | 10.00 | | | | | 14.4 | | | |
| RA | PLATE | 0.10 | 10.00 | | | | 3.97 | 23.8 | | | |
| RA | PLATE | 0.90 | 10.00 | | | 0.32 | 3.63 | 64.9 | | | |
| RA | PLATE | 0.50 | 10.00 | | | | 6.45 | 26.8 | | | |
| | | | | | | | | | | | DATA OUT OF TREND |

TABLE 4.11.1.14

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: JP-4 FUEL AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--|--------------|--------------|------------|--------------------------------|---|
| BA | FORGING | 0.02 | 0.10-20.00 | 2.5 5 10 20 50 100 | 2.40 103 |
| RA | PLATE | 0.08 | 1.00 | | 0.72 14.2 |
| STRESS RELIEVED F.B. WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 0.10-10.00 | | 9.65 1560 |

TABLE 4.11.1.15

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: WATER SATURATED JP-4 FUEL AT R. T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-----------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| RA | PLATE | 0.10 | 0.10 | | 204 |
| RA | PLATE | 0.10 | 1.00 | | 179 |
| RA | PLATE | 0.50 | 0.10 | | 17.0 |
| RA | PLATE | 0.50 | 1.00 | | 1.93 18.4 |

TABLE 4.11.1.16

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM 11-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT DIST. WATER AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | |
|-----------------|--------------|--------------|------------|--------------------------------|---|------|------|------|------|
| | | | | 2.5 | 5 | 10 | 20 | 50 | 100 |
| BA | PLATE | 0.10 | 0.10 | | | | | | 126 |
| RA | PLATE | 0.00 | 15.00 | | | 0.43 | | | |
| RA | PLATE | 0.10 | 0.10 | | | | 19.0 | 254 | |
| RA | PLATE | 0.10 | 1.00 | | | | | 197 | |
| RA | PLATE | 0.50 | 0.10 | | | | 21.8 | | |
| RA | PLATE | 0.50 | 1.00 | | | | 2.64 | 36.8 | |
| STRESS RELIEVED | | | | | | | | | |
| E B WELDMENT | | | | | | | | | |
| (WELD ZONE) | | | | | | | | | |
| | | | | | | | | | 2052 |

TABLE 4.11.1.17

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: DIST. WATER AT 175 F

| CONDITION/RT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---|--------------|--------------|------------|--------------------------------|---|
| | PLATE | 0.50 | 1.00 | 2.5 5 10 20 50 100 | |
| RA | | | | | 29.6 |
| STRESS RELIEVED E B WELDMENT (HEAT AFFECTED ZONE) | WELDMENT | 0.10 | 0 10-10 00 | | 952 |

TABLE 4.11.1.18

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT 3 SZNACL AT R.T.

| (CONDITION/MT) | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS | | FATIGUE CRACK GROWTH RATES | | | | | |
|---|--------------|--------------|------------|----------------|------|----------------------------|---|------|------|-------|------|
| | | | | (KSI SQRT(IN)) | (IN) | 2 | 5 | 10 | 20 | 50 | 100 |
| BA | PLATE | 0.10 | 1.00 | | | | | 38.5 | 281 | | |
| BA | PLATE | 0.10 | 10.00 | | | 0.98 | | 13.8 | 109 | | |
| RA | PLATE | 0.00 | 15.00 | | | | | | | 0.64 | |
| RA | PLATE | 0.10 | 0.10 | | | | | | | | 1852 |
| RA | PLATE | 0.10 | 0.10 | | | | | 3.50 | 44.7 | | |
| RA | PLATE | 0.10 | 1.00 | | | | | 28.6 | 526 | | |
| RA | PLATE | 0.10 | 10.00 | | | | | 4.86 | 63.0 | | |
| RA | PLATE | 0.10 | 10.00 | | | | | | 58.9 | | |
| RA | PLATE | 0.50 | 0.10 | | | | | | 2.95 | | |
| RA | PLATE | 0.50 | 1.00 | | | | | 2.65 | 117 | | |
| RA | PLATE | 0.50 | 10.00 | | | | | 33.7 | 168 | | |
| STRESS RELIEVED E B WELDMENT (WELD ZONE) | | | | | | | | | | 19134 | |
| STRESS RELIEVED E B WELDMENT (HEAT AFFECTED ZONE) | | | | | | | | | | 13.9 | |

TABLE 4.11.1.19

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT S.T.M.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | DATA OUT OF TRENDS | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | |
|--------------|--------------|--------------|------------|-------------------------------|--------------------|---|------|------|-----|
| | | | | 2 | 5 | 10 | 20 | 50 | 100 |
| BA | PLATE | 0.10 | 0.10 | | | 0.58 | 6.43 | 400 | |
| BA | PLATE | 0.10 | 1.00 | | | | 35.3 | 192 | |
| BA | PLATE | 0.10 | 10.00 | | | | 18.6 | 94.3 | |
| DB | PLATE | 0.08 | 1.00 | | | | 8.20 | 214 | |
| DB + 2DBTC | PLATE | 0.08 | 1.00 | | | | 7.93 | 244 | |
| DB + 4DBTC | PLATE | 0.08 | 1.00 | | | | 9.03 | 209 | |
| DBT + PC | PLATE | 0.08 | 1.00 | | | | 11.2 | | |
| DBTC | PLATE | 0.08 | 1.00 | | | | 1.83 | 18.4 | |
| MA | EXTRUSION | 0.08 | 6.00 | | | | 0.62 | 11.1 | |
| MA | EXTRUSION | 0.10 | 1.00-10.00 | | | | 25.9 | 324 | |
| RA | PLATE | 0.00 | 15.00 | | | | 0.64 | | |
| RA | PLATE | 0.08 | 1.00 | | | | 2.08 | 48.7 | |
| RA | PLATE | 0.08 | 1.00 | | | | 0.96 | 12.7 | 285 |

TABLE 4.11.1.19 (Con't)

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM 11-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT S T M
A T R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-------------------------------|---|---|------|------|------|-----|
| RA | PLATE | 0.08 | 1.00 | | | | | 9.12 | | |
| RA | PLATE | 0.08 | 1.00 | | | | | 8.98 | | |
| RA | PLATE | 0.10 | 0.10 | | | | | | 905 | |
| RA | PLATE | 0.10 | 0.10 | | | | | | 3950 | |
| RA | PLATE | 0.10 | 1.00 | | | | | | | 310 |
| RA | PLATE | 0.50 | 1.00 | | | | 2.02 | 52.5 | | |
| RA | FORGING | 0.08 | 1.00 | | | | | 16.1 | 225. | |
| RA | FORGING | 0.08 | 1.00 | | | | 0.69 | 14.0 | 192. | |
| RA | FORGING | 0.08 | 1.00 | | | | 0.74 | 14.9 | | |
| RA | FORGING | 0.50 | 1.00 | | | | 3.39 | 61.3 | | |

TABLE 4.11.1.20

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION 5-T

ENVIRONMENT: S.T.M.
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| DB | PLATE | 0.08 | 1.00 | | 0.78 21.3 |
| DB + TR | PLATE | 0.08 | 1.00 | | 9.78 |

TABLE 4.11.1.21

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION: I-R

ENVIRONMENT: AIR AT 300 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
|------------------|--------------|--------------|------------|-------------------------------|---|---|------|------|----|-----|
| | | | | | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | |
| PA 1300F 2MRS AC | DISK | 0.60 | 0.33 | | | | | 6.72 | | |
| PA 1300F 2MRS AC | DISK | 0.25 | 0.33 | | | | | 13.5 | | |
| PA 1300F 2MRS AC | DISK | 0.54 | 0.33 | | | | 1.19 | | | |

TABLE 4.11.1.22

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM TI-6AL-4V

| TEST CONDITIONS | | ENVIRONMENT | | FATIGUE CRACK GROWTH RATES | | | | | | |
|---|--------------|--------------|-----------|-------------------------------|-----|---|------|------|-----|-----|
| SPECIMEN ORIENTATION | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 |
| 1550F 4HRS FC, 1000F 4HRS, ARGON COOLED | FORGING | 0.10 | 10.00 | | | | 0.19 | 3.81 | | |
| 1550F 4HRS FC, 1000F 4HRS, ARGON COOLED | FORGING | 0.10 | 10.00 | | | | | 4.08 | | |
| 1750F 4HRS ARGON COOLED, 1000F 4HRS, ARGON COOLED | FORGING | 0.10 | 9.99 | | | | | 4.13 | | |
| 1750F 4HRS ARGON COOLED, 1000F 4HRS, ARGON COOLED | FORGING | 0.10 | 10.00 | | | | | 4.05 | | |
| 1950F 4HRS WQ, 1000F 4HRS ARGON COOLED | FORGING | 0.10 | 10.00 | | | | | 2.38 | 257 | |

TABLE 4.11.1.23

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT: ARGON AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--|--------------|--------------|-----------|-------------------------------|---|
| 1750F 4HRS ARGON COOLED, 1000F 4HRS ARGON COOLED | FORGING | 0.10 | 10.00 | 2.5 5 10 20 50 100 | 4.61 |
| 1950F 4HRS WQ, 1000F 4HRS ARGON COOLED | FORGING | 0.10 | 10.00 | | 3.37 |

TABLE 4.11.1.24

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT: LAB AIR AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--|--------------|--------------|------------|--------------------------------|---|
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F 4HRS AC. 900F 3HR | DISK | 0.05 | 0.33-10.00 | 2.5 5 10 20 50 100 | 152 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-6HRS AC | DISK | 0.03 | 0.33- .90 | | 0.86 11.0 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-6HRS AC | DISK | 0.25 | 0.33- 50 | | 18.9 |

TABLE 4.11.1.25

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT: AIR AT 300 F

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---|--------------|--------------|------------|--------------------------------|---|
| | | | | | 2.5 5 10 20 50 100 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.03 | 0.33 | | 0.74 10.1 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.25 | 0.33 | | 11.9 |

TABLE 4.11.1.26

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V

TEST CONDITIONS

SPECIMEN ORIENTATION C-R

ENVIRONMENT AIR AT 600 F

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|---|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.03 | 0.33 | | 1.03 9.87 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.03 | 0.33 | | 1.77 12.6 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.25 | 0.33 | | 2.04 13.3 |
| 1775F 1HR WQ. 1675F 1HR WQ. 1000F-1200F 2-8HRS AC | DISK | 0.54 | 0.33 | | 2.12 |

TABLE 4.11.2.1

| CONDITION | --PRODUCT-- | | TEST TEMP (F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | TITANIUM | | WIDTH (IN) | TRICK DESIGN | CRACK LENGTH (IN) | 2.9σ K(1C)/TYS)*2 (IN) | K(1C) MEAN (KSI*SQRT IN) | STAN DEV | DATE | REFER |
|--|-------------|------------|---------------|-----------------|----------------------|-----------|-------|------------|--------------|-------------------|------------------------|--------------------------|----------|------|-------|
| | FIRM | THICK (IN) | | | | TI-6AL-4V | K(1C) | | | | | | | | |
| AB FORGED-FA ALPHA-BETA FORGED, HILL ANNEALED | F | --- | R.T. | --- | 133.0 | 2.500 | 1.250 | CT | 1.250 | 0.57 | 63.60 | 1973 90584 | (1) | | |
| | | --- | | --- | 133.0 | 2.500 | 1.250 | CT | 1.250 | 0.50 | 59.40 | 1973 90584 | (1) | | |
| | | --- | | --- | 134.0 | 2.500 | 1.250 | CT | 1.250 | 0.62 | 66.50 | 1973 90584 | (1) | | |
| | | --- | | --- | 134.0 | 2.500 | 1.250 | CT | 1.250 | 0.41 | 54.10 | 1973 90584 | (1) | | |
| | | --- | | --- | 134.0 | 2.500 | 1.250 | CT | 1.250 | 0.43 | 55.90 | 1973 90584 | (1) | | |
| 4 HR. FC TO 1000F, AC | | 2.75 | | | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.44 | 56.30 | 1973 90584 | (1) | | |
| | | 2.75 | | | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.41 | 55.20 | 1974 88962 | (2) | | |
| | | | | | | | | | | | 58.5/ | 1974 88962 | (2) | | |
| | | | | | | | | | | | 4.4 | | | | |
| AB FORGED-FA ALPHA-BETA FORGED, HILL ANNEALED | F | 2.25 | R.T. | T-L | 145.0 | 2.000 | 1.000 | CT | 1.065 | 0.18 | 38.60 | 1973 86688 | (1) | | |
| | | 2.25 | | | 145.0 | 2.000 | 1.500 | CT | 1.556 | 0.12 | 32.20 | 1973 86688 | (1) | | |
| | | 2.25 | | | 145.0 | 2.000 | 1.000 | CT | 1.071 | 0.15 | 36.00 | 1973 86688 | (1) | | |
| | | 2.25 | | | 145.0 | 2.000 | 1.000 | CT | 1.074 | 0.14 | 34.90 | 1973 86688 | (1) | | |
| AB FORGED-FA ALPHA-BETA FORGED, RECRYSTALLIZED ANNEAL, 1700F 4 HR. FC TO 1000F, AC | F | --- | R.T. | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.74 | 67.90 | 1973 90584 | (1) | | |
| | | --- | | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.79 | 72.10 | 1973 90584 | (1) | | |
| | | --- | | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.72 | 68.60 | 1973 90584 | (1) | | |
| | | --- | | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.70 | 68.00 | 1973 90584 | (1) | | |
| | | --- | | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.74 | 69.60 | 1973 90534 | (1) | | |
| | --- | | --- | 128.0 | 2.500 | 1.250 | CT | 1.250 | 0.70 | 67.70 | 1973 90584 | (1) | | | |
| | --- | | --- | 132.0 | 2.500 | 1.250 | CT | 1.250 | 0.60 | 64.50 | 1973 90584 | (1) | | | |
| | --- | | --- | 132.0 | 2.500 | 1.250 | CT | 1.250 | 0.54 | 61.70 | 1973 90584 | (1) | | | |
| | | | | | | | | | | | 67.8/ | 1973 90584 | (1) | | |
| | | | | | | | | | | | 3.3 | | | | |
| ANNEALED | F | 3.00 | R.T. | L-T | 114.0 | 3.001 | 1.501 | CT | 1.366 | 1.41 | 83.70 | 1973 85034 | (1) | | |
| | | 3.00 | | | 119.0 | 2.978 | 1.500 | CT | 1.556 | 1.22 | 83.10 | 1973 85034 | (1) | | |
| ANNEALED | F | 3.00 | R.T. | T-L | 118.0 | 3.003 | 1.500 | CT | 1.549 | 1.46 | 90.40 | 1973 85034 | (1) | | |
| | | 3.00 | | | 120.0 | 3.001 | 1.494 | CT | 1.618 | 1.01 | 76.40 | 1973 85034 | (1) | | |
| ANNEALED | E | 4.00 | R.T. | L-T | 122.0 | 4.006 | 1.624 | CT | 2.027 | 1.42 | 92.00 | 1973 85836 | (3) | | |
| ANNEALED | E | 4.00 | R.T. | T-L | 122.0 | 4.003 | 1.639 | CT | 2.027 | 1.51 | 94.90 | 1973 85836 | (3) | | |
| | | 4.00 | | | 122.0 | 4.003 | 1.633 | CT | 1.995 | 1.41 | 91.70 | 1973 85836 | (3) | | |
| ANNEALED | BT | 6.00 | R.T. | L-T | 123.0 | 2.501 | 1.250 | CT | 1.249 | 0.87 | 72.00 | 1975 MA003 | (1) | | |

NOTES:
 (1) F-14 OUTBOARD COVER
 (2) CURP DISK
 (3) COMPOSITION (Wt PERCENT) 6.35AL, 4.31V, 0.022C, 0.16FE, 0.009N, 0.006H, 0.16O

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT | TEST TEMP (F) | FORM THICK (IN) | SPECIMEN | | CRACK LENGTH (IN) | 2.5* K(1C)/TYS**2 (IN) | K(1C) MEAN DEV (K(1C) SORT IN) | K(1C) STAN DEV | DATE | REFER | |
|-------------------------|-----------|-------|----------------------|----------------------|---------------|-----------------|----------|-------|-------------------|------------------------|--------------------------------|----------------|-------|-----------|-------|
| | TI-6AL-4V | K(1C) | | | | | M | B | | | | | | | A |
| ANNEALED 1375F 2 HR, AC | P | 2.75 | 129.0 | R-T | R-T | 2.497 | 1.250 | CT | 1.224 | 0.48 | 56.57 | | 1975 | MA003 | |
| | | 2.75 | 129.0 | L-T | | 2.477 | 1.250 | CT | 1.200 | 0.62 | 64.30 | 60.4/ | 5.5 | 1975 | MA003 |
| ANNEALED 2000F 2 HR | F | 1.00 | 140.0 | R-T | | 2.000 | 1.000 | CT | 1.000 | 0.50 | 62.80 | | 1974 | 88962 (1) | |
| | | 1.00 | 140.0 | | | 2.000 | 1.000 | CT | 1.000 | 0.43 | 58.20 | | 1974 | 88962 (1) | |
| | | 1.00 | 140.0 | | | 2.000 | 1.000 | CT | 1.000 | 0.39 | 55.20 | | 1974 | 88962 (1) | |
| | | 1.00 | 140.0 | | | 2.000 | 1.000 | CT | 1.000 | 0.44 | 50.80 | | 1974 | 88962 (1) | |
| | | 1.00 | 140.0 | | | 2.000 | 1.000 | CT | 1.000 | 0.35 | 52.40 | | 1974 | 88962 (1) | |
| | | | | | | | | | | | | 57.5/ | 3.9 | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| AS RECEIVED | FR | | 124.0 | R-T | L-T | 2.000 | 1.002 | CT | 1.020 | 0.61 | 61.10 | | 1974 | 90012 | |
| | | 3.50 | 126.0 | | | 2.006 | 1.000 | CT | 1.074 | 0.59 | 61.30 | | 1974 | 90012 | |
| | | 1.00 | 126.0 | | | 1.998 | 1.001 | CT | 1.019 | 0.62 | 62.50 | | 1974 | 90012 | |
| | | 3.50 | 129.0 | | | 1.997 | 0.625 | CT | 0.994 | 0.59 | 61.30 | | 1974 | 90012 | |
| | | | 130.0 | | | 1.976 | 1.002 | CT | 1.006 | 0.48 | 56.60 | | 1974 | 90012 | |
| | | | 130.0 | | | 1.998 | 1.000 | CT | 1.029 | 0.79 | 72.90 | | 1974 | 90012 | |
| | | | 130.0 | | | 2.000 | 1.000 | CT | 1.053 | 0.53 | 60.10 | | 1974 | 90012 | |
| | | 3.50 | 131.0 | | | 1.970 | 0.998 | CT | 1.036 | 0.72 | 70.60 | | 1974 | 90012 | |
| | | 1.50 | 134.0 | | | 2.000 | 0.563 | CT | 1.005 | 0.32 | 47.70 | | 1974 | 90012 | |
| | | | 134.0 | | | 1.998 | 1.003 | CT | 1.013 | 0.61 | 66.10 | | 1974 | 90012 | |
| | | 2.50 | 136.0 | | | 1.998 | 1.003 | CT | 1.053 | 0.20 | 38.40 | | 1974 | 90012 | |
| | | 2.60 | 137.0 | | | 2.000 | 0.999 | CT | 1.032 | 0.37 | 52.90 | | 1974 | 90012 | |
| | | 2.70 | 137.0 | | | 2.001 | 1.000 | CT | 1.021 | 0.24 | 42.60 | | 1974 | 90012 | |
| | | | 143.0 | | | 2.001 | 0.999 | CT | 1.022 | 0.26 | 45.70 | 57.1/ | 10.4 | 1974 | 90012 |
| AS RECEIVED | FB | 3.50 | 127.0 | R-T | T-L | 1.978 | 0.998 | CT | 1.064 | 0.68 | 66.40 | | 1974 | 90012 | |
| | | | 128.0 | | | 1.970 | 0.732 | CT | 1.023 | 0.42 | 52.50 | | 1974 | 90012 | |
| | | 1.00 | 129.0 | | | 1.997 | 0.779 | CT | 1.018 | 0.66 | 66.50 | | 1974 | 90012 | |
| | | 1.50 | 130.0 | | | 1.990 | 0.502 | CT | 1.000 | 0.41 | 52.60 | | 1974 | 90012 | |
| | | | 130.0 | | | 1.779 | 0.645 | CT | 0.998 | 0.43 | 54.00 | | 1974 | 90012 | |
| | | 2.00 | 131.0 | | | 1.990 | 1.003 | CT | 1.023 | 0.53 | 60.10 | | 1974 | 90012 | |
| | | 1.50 | 132.0 | | | 1.999 | 1.002 | CT | 1.055 | 0.16 | 33.80 | | 1974 | 90012 | |
| | | | 133.0 | | | 2.000 | 1.002 | CT | 1.027 | 0.69 | 69.90 | | 1974 | 90012 | |
| | | | 133.0 | | | 1.998 | 1.001 | CT | 1.024 | 0.50 | 59.40 | | 1974 | 90012 | |
| | | 3.50 | 133.0 | | | 1.970 | 1.005 | CT | 1.045 | 0.56 | 62.70 | | 1974 | 90012 | |
| | 3.50 | 134.0 | | | 2.000 | 1.000 | CT | 1.028 | 0.58 | 64.50 | | 1974 | 90012 | | |

NOTES
(1) INTERMEDIATE GRAIN SIZE

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT (F) | THICK (IN) | TEMP (F) | SPECIMEN | | DESIGN (IN) | CRACK LENGTH (IN) | K(1C) (K(1C)/TYB)?? (KRIEGRDT IN) | K(1C) MEAN DEY (IN) | DATE | REFER |
|--|----------|------------|----------------------|--------------------------|------------|----------|------------|-----------|-------------|-------------------|-----------------------------------|---------------------|------------|------------|
| | FORM | WIDTH (IN) | | | | | THICK (IN) | 2.5% (IN) | | | | | | |
| AS RECEIVED | FB | 1.50 | 135.0 | R.T. | T-L | | 1.996 | 0.560 | CT | 0.994 | 0.45 | 57.40 | 1974 | 90012 |
| | | | 135.0 | | | | 2.003 | 1.001 | CT | 1.023 | 0.46 | 57.80 | 1974 | 90012 |
| | | | 139.0 | | | | 2.001 | 1.002 | CT | 1.016 | 0.44 | 58.20 | 1974 | 90012 |
| | | | 139.0 | | | | 2.000 | 0.634 | CT | 1.010 | 0.37 | 53.50 | 1974 | 90012 |
| | | | 139.0 | | | | 1.998 | 1.003 | CT | 1.033 | 0.35 | 52.10 | 1974 | 90012 |
| | | | 140.0 | | | | 2.002 | 0.999 | CT | 1.014 | 0.14 | 32.80 | 1974 | 90012 |
| | | | 141.0 | | | | 2.002 | 1.001 | CT | 1.033 | 0.18 | 37.40 | 1974 | 90012 |
| | | | 142.0 | | | | 1.999 | 0.999 | CT | 1.048 | 0.36 | 53.70 | 1974 | 90012 |
| | | | 142.0 | | | | 1.993 | 1.001 | CT | 1.034 | 0.35 | 66.89 | 1974 | 90012 |
| | | | 145.0 | | | | 2.000 | 0.999 | CT | 1.028 | 0.17 | 40.10 | 54.9/ 10.8 | 1974 90012 |
| AS RECEIVED-AB (ALPHA-BETA FORGED) | FB | 3.50 | 127.0 | R.T. | L-L | | 2.000 | 1.000 | CT | 1.033 | 0.92 | 77.10 | 1974 | 90012 |
| AS RECEIVED-AB (ALPHA-BETA FORGED) | FR | 3.50 | 131.0 | R.T. | T-L | | 2.000 | 1.000 | CT | 1.023 | 0.95 | 80.90 | 1974 | 90012 |
| R FORGED BETA FORGED REHEATED TO 1750F DRAWN TO SIZE, ANNEALED 1300F | FR | 2.25 | 135.0 | R.T. | T-L | | 2.000 | 1.000 | CT | 1.046 | 0.30 | 46.80 | 1973 | 86688 |
| | | | 135.0 | | | | 3.000 | 1.500 | CT | 1.471 | 0.20 | 37.80 | 1973 | 86688 |
| | | | 135.0 | | | | 2.000 | 1.000 | CT | 1.038 | 0.28 | 45.60 | 1973 | 86688 |
| | | | 135.0 | | | | 2.000 | 1.000 | CT | 1.058 | 0.22 | 40.20 | 42.6/ 4.3 | 1973 86688 |
| R FORGED-MA BETA FORGED, MILL ANNEALED, 1300F 2 HR, AC | F | 2.75 | 131.0 | R.T. | | | 2.000 | 1.000 | CT | 1.000 | 0.88 | 77.70 | 1974 | 88962 (1) |
| | | | 131.0 | | | | 2.000 | 1.000 | CT | 1.000 | 0.77 | 72.90 | 1974 | 88962 (1) |
| R FORGED-MA BETA FORGED, MILL ANNEALED 1300F 2 HR, AC | F | 2.00 | 137.0 | R.T. | L-T | | 2.000 | 1.000 | CT | ---- | 0.59 | 66.40 | 1971 | 80338 |
| | | | 137.0 | | | | 2.000 | 1.000 | CT | ---- | 0.77 | 76.00 | 1971 | 80338 |
| | | | 137.0 | | | | 2.000 | 1.000 | CT | ---- | 0.64 | 67.30 | 1971 | 80338 |
| R FORGED-MA BETA FORGED, MILL ANNEALED 1300F 2 HR, AC | F | 2.00 | 131.0 | R.T. | T-L | | 2.000 | 1.000 | CT | ---- | 0.73 | 70.60 | 1971 | 80338 |

NOTES:
(1) COMP. DISK

TABLE 4.11.2.1 (con't)

| CONDITION | --PRODUCT-- FORM | | TEST TEMP (°F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | TITANIUM TI-6AL-4V | | CRACK LENGTH (IN) | 2.5* K(IC)/TYS) ^{0.5} (IN) | K(IC) MEAN (KSI*SQRT IN) | K(IC) STAN DEV | DATE | REFER |
|---|---------------------|---------------|-------------------|--------------------|----------------------------|-----------------------|----------------|-------------------------|---|-----------------------------|-------------------|-----------------|-------|
| | THICK (IN) | MIDTH (IN) | | | | THICK (IN) | DESIGN (IN) | | | | | | |
| B FORCED-MA BETA FORGED, MILL ANNEALED 1300F 2 HR, AC | F | 2.00 | R. T. | I-L | 131.0 | 2.000 | 1.000 | CT | 0.74 | 71.10 | | 1971 80338 | |
| | | 2.00 | | | 2.000 | 1.000 | CT | 0.74 | 71.40 | 71.0/ 0.4 | 1971 80338 | | |
| B FORCED-MA BETA FORGED, MILL ANNEALED 1300F 2 HR, AC | F | 2.00 | R. T. | S-L | 132.0 | 2.000 | 1.000 | CT | 0.74 | 72.10 | | 1971 80338 | |
| | | 2.00 | | | 2.000 | 1.000 | CT | 0.82 | 73.70 | 73.9/ 2.5 | 1971 80338 | | |
| DB, AB FIN-MA BETA BLOCKED, ALPHA-BETA FINISHED, MILL ANNEALED | F | --- | R. T. | --- | 132.0 | 2.500 | 1.250 | CT | 0.78 | 73.50 | | 1973 90384 (1) | |
| | | --- | | | 2.500 | 1.250 | CT | 0.89 | 78.70 | | 1973 90384 (1) | | |
| | | --- | | | 2.500 | 1.250 | CT | 0.59 | 65.10 | | 1973 90384 (1) | | |
| | | --- | | | 2.500 | 1.250 | CT | 0.72 | 72.10 | 72.4/ 5.6 | 1973 90384 (1) | | |
| DB, AB FIN-RA BETA BLOCKED, ALPHA-BETA FINISHED, RECRYSTALLIZED ANNEAL 1700F 4 HR, FC TO 1000F, AC | F | --- | R. T. | --- | 135.0 | 2.500 | 1.250 | CT | 0.87 | 80.70 | | 1973 90384 (1) | |
| | | --- | | | 2.500 | 1.250 | CT | 0.76 | 74.40 | | 1973 90384 (1) | | |
| | | --- | | | 2.500 | 1.250 | CT | 0.74 | 74.80 | | 1973 90384 (1) | | |
| | | --- | | | 2.500 | 1.250 | CT | 0.66 | 70.50 | 73.1/ 4.3 | 1973 90384 (1) | | |
| BB, AB FIN-30% BETA BLOCKED, ALPHA-BETA FINISHED, 30% REDUCTION, MILL ANNEALED, 1300F 2 HR, AC | F | 2.50 | R. T. | --- | 127.0 | 2.000 | 1.000 | CT | 1.00 | 80.50 | | 1974 88962 | |
| | | 2.50 | | | 2.000 | 1.000 | CT | 0.89 | 75.90 | 78.2/ 3.3 | 1974 88962 | | |
| DB, AB FIN-10% BETA BLOCKED, ALPHA-BETA FINISHED, 10% REDUCTION, SOLUTION TREATED & OVERAGED, 1750F 1 HR, WQ, 1300F 2 HR, AC | F | 2.50 | R. T. | --- | 136.0 | 2.000 | 1.000 | CT | 0.84 | 72.00 | | 1974 88962 | |
| | | 2.50 | | | 2.000 | 1.000 | CT | 0.99 | 83.50 | | 1974 88962 | | |
| ALPHA-BETA FINISHED, 10% REDUCTION, SOLUTION TREATED & OVERAGED, 1750F 1 HR, WQ, 1300F 2 HR, AC | F | 2.50 | R. T. | --- | 136.0 | 2.000 | 1.000 | CT | 0.88 | 80.50 | | 1974 88962 | |
| | | 2.50 | | | 2.000 | 1.000 | CT | 0.88 | 80.50 | 81.7/ 3.4 | 1974 88962 | | |

NOTES:
/ 1) F-14 OUTBOARD COVER

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | SPECIMEN THICKNESS (IN) | DESIGN THICKNESS (IN) | CRACK LENGTH (IN) | 2.5* K(1C)/TYS**2 (KSI*SQRT IN) | K(1C) MEAN DEV (KSI*SQRT IN) | DATE | REF |
|---|----------------|---------------|----------------------|-------------------------|-----------------------|-------------------|---------------------------------|------------------------------|--------|------------|
| | PRODUCT-- FURN | TEST TEMP (F) | | | | | | | | |
| 08.8B FIN-10HA BETA-BLOCKED, ALPHA-BETA FINISHED. 30% REDUCTION, SOLUTION TREATED & OVERAGED, 1750F 1 HR., 1300F 2 HR., AC | 2 50 | R.T. | 137.0 | 2.000 | 1.000 | CT | 1.000 | 0.81 | 78.00 | 1974 88962 |
| | 2 50 | | 137.0 | 2.000 | 1.000 | CT | 1.000 | 0.60 | 67.40 | 1974 88962 |
| | 2 50 | | 137.0 | 2.000 | 1.000 | CT | 1.000 | 0.72 | 73.80 | 1974 88962 |
| 08.8B FIN-10HA BETA-BLOCKED, ALPHA-BETA FINISHED. 10% REDUCTION, MILL ANNEALED, 1300F 2 HR., AC | 2 50 | R.T. | 128.0 | 2.000 | 1.000 | CT | 1.000 | 0.85 | 74.50 | 1974 88962 |
| | 2 50 | | 128.0 | 2.000 | 1.000 | CT | 1.000 | 0.84 | 74.40 | 1974 88962 |
| | 2 50 | | 128.0 | 2.000 | 1.000 | CT | 1.000 | 0.77 | 71.10 | 1974 88962 |
| 08.8B FIN-10HA BETA-BLOCKED, ALPHA-BETA FINISHED. 10% REDUCTION, SOLUTION TREATED & OVERAGED, 1750F 1 HR., 1300F 2 HR., AC | 2 50 | R.T. | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.96 | 85.60 | 1974 88962 |
| | 2 50 | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.98 | 86.40 | 1974 88962 |
| | 2 50 | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.98 | 86.40 | 1974 88962 |
| BETA ANNEALED PLATE EB WELDED THEN BETA ANNEALED IN PLANE OF FRACTURE | 2 50 | R.T. | 116.0 | 1.994 | 0.999 | CT | 1.133 | 0.90 | 67.80 | 1974 88575 |
| | 2 50 | | 116.0 | 1.992 | 0.951 | CT | 1.140 | 0.87 | 68.50 | 1974 88575 |
| | 2 50 | 65 | L-T | 125.0 | 3.997 | 2.001 | CT | 2.072 | 1.90 | 109.10 |
| BETA ANNEALED | 2 50 | | 125.0 | 4.003 | 1.998 | CT | 2.105 | 1.79 | 105.90 | 1974 88575 |
| | 2 50 | | 125.0 | 4.003 | 1.991 | CT | 2.116 | 2.06 | 113.50 | 1974 88575 |
| | 2 50 | | 125.0 | 4.003 | 2.000 | CT | 2.192 | 1.95 | 110.50 | 1974 88575 |
| BETA ANNEALED | 2 50 | | 125.0 | 4.009 | 2.005 | CT | 2.084 | 1.86 | 108.00 | 1974 88575 |
| | 1 00 | R.T. | 126.0 | 2.500 | 1.000 | WDL | ---- | 0.98 | 79.20 | 1977 JEM01 |
| | 3 00 | R.T. | 130.4 | 3.000 | 1.500 | CT | ---- | 1.44 | 99.00 | 1975 UD008 |
| BETA PROCESSED MILL ANNEALED | 3 00 | | 130.4 | 3.000 | 1.500 | CT | ---- | 1.35 | 96.00 | 1975 UD008 |
| | 3 00 | | 130.4 | 3.000 | 1.500 | CT | ---- | 1.18 | 87.60 | 1975 UD008 |

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD (KSI) | STRENGTH | WIDTH (IN) | THICKNESS (IN) | DESIGN | CRACK LENGTH (IN) | K(1C) (IN) | K(1C) (KSI*SQRT IN) | K(1C) STAN MEAN DEV | DATE | REFER |
|------------------------------|----------|-------------------|----------------|----------|---------------|-------------------|--------|-------------------------|---------------|------------------------|------------------------|------|-----------|
| | FORM | THICKNESS (IN) | | | | | | | | | | | |
| DIFFUSION BONDED | P | 0.62 | R.T. | --- | 4.003 | 2.002 | CT | 1.966 | 1.47 | 92.10 | | 1973 | 85836 (1) |
| DIFFUSION BONDED | P | 0.62 | R.T. | L-T | 3.004 | 1.500 | CT | 1.974 | 1.11 | 79.90 | | 1973 | 85836 (1) |
| DIFFUSION BONDED | P | 0.62 | R.T. | T-L | 3.005 | 1.501 | CT | 1.975 | 1.20 | 83.10 | | 1973 | 85836 (1) |
| DIFFUSION BONDED | P | 1.50 | R.T. | S-T | 4.000 | 1.500 | CT | --- | 1.34 | 88.00 | | 1974 | 89004 (1) |
| | | 1.50 | | | 4.000 | 1.500 | CT | --- | 1.31 | 87.00 | | 1974 | 89004 (1) |
| | | 1.50 | | | 4.000 | 1.500 | CT | --- | 1.16 | 82.00 | 89.7/ 3.2 | 1974 | 89004 (1) |
| DIFFUSION BONDED | P | 2.50 | R.T. | S-L | 4.000 | 1.500 | CT | --- | 1.14 | 81.00 | | 1974 | 89004 (1) |
| DIFFUSION BONDED | BT | 0.62 | R.T. | L-T | 3.000 | 1.500 | CT | --- | 1.11 | 80.00 | | 1974 | 89004 (1) |
| DIFFUSION BONDED ANNEALED | BT | 3.50 | R.T. | L-T | 2.000 | 1.000 | CT | 1.072 | 0.93 | 77.50 | | 1974 | 90012 (2) |
| | | 1.00 | | | 2.001 | 1.002 | CT | 1.092 | 0.98 | 80.70 | | 1974 | 90012 (2) |
| | | --- | | | 2.002 | 1.004 | CT | 1.032 | 0.75 | 70.80 | | 1974 | 90012 (2) |
| | | 1.50 | | | 2.000 | 1.003 | CT | 1.019 | 0.45 | 56.10 | | 1974 | 90012 (2) |
| | | --- | | | 1.995 | 1.000 | CT | 1.083 | 0.83 | 76.30 | | 1974 | 90012 (2) |
| | | 3.50 | | | 1.999 | 1.003 | CT | 1.029 | 0.68 | 69.00 | | 1974 | 90012 (2) |
| | | 2.60 | | | 1.996 | 0.975 | CT | 1.017 | 0.48 | 58.10 | | 1974 | 90012 (2) |
| | | 3.70 | | | 1.999 | 1.000 | CT | 1.030 | 0.69 | 70.40 | | 1974 | 90012 (2) |
| | | 2.70 | | | 2.000 | 1.001 | CT | 1.024 | 0.40 | 54.70 | 68.2/ 9.7 | 1974 | 90012 (2) |
| DIFFUSION BONDED | BT | 0.62 | R.T. | T-L | 3.000 | 1.500 | CT | --- | 1.20 | 83.00 | | 1974 | 87004 (1) |
| DIFFUSION BONDED ANNEALED | BT | --- | R.T. | T-L | 2.000 | 1.003 | CT | 1.032 | 0.80 | 70.80 | | 1974 | 90012 (2) |
| | | --- | | | 1.997 | 0.876 | CT | 0.992 | 0.65 | 64.00 | | 1974 | 90012 (2) |
| | | --- | | | 2.001 | 0.999 | CT | 1.043 | 0.90 | 76.90 | | 1974 | 90012 (2) |
| | | 3.50 | | | 1.973 | 1.000 | CT | 1.048 | 0.84 | 76.00 | | 1974 | 90012 (2) |
| | | 3.50 | | | 1.998 | 0.999 | CT | 1.013 | 0.67 | 60.20 | | 1974 | 90012 (2) |
| | | 2.00 | | | 1.978 | 1.000 | CT | 1.028 | 0.75 | 72.70 | | 1974 | 90012 (2) |
| | | 3.50 | | | 2.000 | 0.999 | CT | 1.019 | 0.72 | 71.40 | | 1974 | 90012 (2) |

NOTES:
 (1) DIFFUSION BONDED - 1700F 4HR, FC TO 1400F AT 100F/HR THEN TO 900F IN 0.75HR
 (2) DIFFUSION BONDED ANNEALED - 1750F 1.5 TO 4HR, FC TO 900F AT 100F/HR

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | | | | | | | | | K (IC) | K (IC) STAN MEAN DEV (KSI*SQRT IN) | DATE | REFER |
|--|-------------|------------|---------------|----------------------|------------|------------|--------|-------------|-------------|--------------------------|-----------|--|-----------|-------|
| | --PRODUCT-- | | TEST SPECIMEN | | SPECIMEN | | CRACK | | 2.5° | | | | | |
| | FORM | THICK (IN) | ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | LENGTH (IN) | K (IC) (IN) | CRACK (K(1C)/TYS)*2 (IN) | | | | |
| DIFFUSION DIBID ANNEALED | BT | 1.50 | R.T. | Y-L | 134.0 | 2.000 | 1.000 | CT | 1.043 | 0.39 | 53.10 | 1974 | 90012 (1) | |
| | | | | | 135.0 | 2.000 | 1.001 | CT | 1.033 | 0.66 | 69.20 | 1974 | 90012 (1) | |
| | | 2.50 | | | 137.0 | 1.998 | 0.877 | CT | 1.021 | 0.33 | 47.50 | 1974 | 90012 (1) | |
| | | 2.70 | | | 138.0 | 1.997 | 0.979 | CT | 1.031 | 0.27 | 43.10 | 1974 | 90012 (1) | |
| | 1.00 | | | 142.0 | 2.001 | 1.004 | CT | 1.018 | 0.25 | 44.60 | 1974 | 90012 (1) | | |
| | | | | | | | | | | | | | | |
| DIFFUSION UNBOND | BT | 8.00 | R.T. | S-T | ---- | 3.999 | 1.495 | CT | 1.926 | 1.32 | 87.40 | 1972 | 84306 (2) | |
| | | 8.00 | | | ---- | 3.999 | 1.497 | CT | 1.881 | 1.18 | 82.40 | 1972 | 84306 (2) | |
| | | 8.00 | | | ---- | 3.998 | 1.495 | CT | 1.920 | 1.33 | 87.80 | 1972 | 84306 (2) | |
| | | 8.00 | | | ---- | 3.998 | 1.495 | CT | 1.963 | 1.43 | 90.90 | 1972 | 84306 (2) | |
| | 8.00 | | | ---- | 3.998 | 1.492 | CT | 1.969 | 1.45 | 91.60 | 1972 | 84306 (2) | | |
| | | | | | | | | | | 64.2/ 11.8 | | | | |
| HA. COARSE GRAIN 1300F 2 HR. AC | F | 14.00 | R.T. | -- | 139.0 | 2.000 | 1.000 | CT | 1.000 | 0.35 | 52.20 | 1974 | 88962 | |
| | | 14.00 | | | 139.0 | 2.000 | 1.000 | CT | 1.000 | 0.36 | 53.20 | 1974 | 88962 | |
| | | 14.00 | | | 139.0 | 2.000 | 1.000 | CT | 1.000 | 0.40 | 53.30 | 1974 | 88962 | |
| | | 14.00 | | | 139.0 | 2.000 | 1.000 | CT | 1.000 | 0.42 | 56.70 | 1974 | 88962 | |
| | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.35 | 52.10 | 53.9/ 2.0 | 1974 | 88962 | |
| HA FINE GRAIN 1300F 2 HR. AC | F | 6.00 | R.T. | --- | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.44 | 59.60 | 1974 | 88962 | |
| | | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.62 | 64.10 | 1974 | 88962 | |
| | | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.60 | 67.60 | 1974 | 88962 | |
| | | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.54 | 64.00 | 1974 | 88962 | |
| | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.85 | 80.60 | 1974 | 88962 | | |
| | 6.00 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.76 | 76.10 | 67.3/ 7.7 | 1974 | 88962 | |
| HA 10-20ALPHA 10 TO 20X PRIMARY ALPHA. MILL ANNEALED 1300F 2 HR. AC | F | 2.50 | R.T. | --- | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.57 | 67.10 | 1974 | 88962 | |
| | | 2.50 | | | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.67 | 73.10 | 1974 | 88962 | |
| | | 2.50 | | | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.58 | 68.00 | 1974 | 88962 | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | 69.4/ 3.2 | | | |

NOTES:
 (1) DIFFUSION BOND ANNEALED = 1700F 1.5 TO 4HR. FC TO 900F AT 100F/HR
 (2) DIFFUSION BOND = 1700F 4HR. FC TO 1400F AT 100F/HR THEN TO 900F IN 0.75HR

TABLE 4.11.2.1 (con't)

| CONDITION: | TITANIUM | | | | | | | | | | K(IIC) STAN K(IIC) MEAN DEV (ASISTORT IN) | DATE | REFER |
|--|-----------|------------|-------------|----------------|------------|------------|-------------|-------------|----------------------|---------------------------------|---|------|------------|
| | II-6AL-4V | | K(IIC) | | CRACK | | 2.3% | | K(IIC) STAN | | | | |
| | FORM | THICK (IN) | YIELD (KSI) | STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | (K(IIC)/TYS)**2 (IN) | (K(IIC) MEAN DEV (ASISTORT IN)) | | | |
| MA 40-50ZALPHA 40 TO 50% PRIMARY ALPHA, MILL ANNEALED 1370F 2 HR.AC | F | 2.50 | R.T. | --- | 135.0 | 2.000 | 1.000 | CT | 1.000 | 0.70 | 71.50 | 1974 | 88962 |
| | | 2.50 | | | 135.0 | 2.000 | 1.000 | CT | 1.000 | 0.58 | 63.20 | 1974 | 88962 |
| | | 2.50 | | | 135.0 | 2.000 | 1.000 | CT | 1.000 | 0.68 | 70.60 | 1974 | 88962 |
| | | | | | | | | | | | 69.17 | | 3.4 |
| MILL ANNEAL. | P | 1.50 | R.T. | L-T | 133.0 | 2.496 | 1.244 | CT | 1.330 | 0.45 | 56.59 | 1981 | MA002 |
| | | 1.50 | | | 133.0 | 2.502 | 1.255 | CT | 1.297 | 0.42 | 54.70 | 1981 | MA002 |
| MILL ANNEAL. | P | 1.00 | R.T. | T-L | 146.1 | 2.550 | 1.000 | MDL | ---- | 0.17 | 38.20 | 1977 | JEM01 |
| MILL ANNEALED | P | 2.00 | R.T. | L-T | 127.0 | 4.000 | 2.003 | CT | 2.137 | 1.94 | 112.00 | 1972 | 85064 |
| MILL ANNEALED | P | 2.00 | 65 | T-L | 157.0 | 4.000 | 2.002 | CT | 1.980 | 0.94 | 83.70 | 1973 | 88144 |
| | | 2.00 | | | 157.0 | 4.000 | 2.004 | CT | 1.970 | 1.03 | 89.70 | 1973 | 88144 |
| | | 2.00 | | | 157.0 | 4.000 | 2.003 | CT | 1.990 | 0.99 | 88.20 | 1973 | 88144 |
| MILL ANNEALED | P | 1.25 | R.T. | T-L | 119.4 | 3.475 | 1.245 | CT | 1.741 | 1.16 | 93.30 | 1972 | 84306 |
| | | 1.25 | | | 119.4 | 3.479 | 1.245 | CT | 1.824 | 1.20 | 97.00 | 1972 | 84306 |
| | | 1.25 | | | 119.4 | 3.500 | 1.247 | CT | 1.817 | 1.15 | 94.80 | 1972 | 84306 |
| | | 2.00 | | | 126.0 | 4.000 | 2.002 | CT | 2.038 | 1.53 | 98.70 | 1972 | 85064 |
| | | 2.00 | | | 126.0 | 4.000 | 2.001 | CT | 2.097 | 1.94 | 112.00 | 1972 | 85064 |
| | | 2.00 | | | 126.0 | 4.000 | 2.002 | CT | 2.048 | 1.75 | 103.90 | 1972 | 85064 |
| MILL ANNEALED | E | 4.00 | R.T. | L-T | 123.5 | 3.997 | 1.465 | CT | 1.937 | 1.21 | 87.60 | 1972 | 84306 (1) |
| | | 1.80 | | | 124.0 | 3.934 | 1.578 | CT | 2.031 | 1.17 | 85.09 | 1976 | MC001 |
| | | 1.80 | | | 124.0 | 3.930 | 1.578 | CT | 2.036 | 1.12 | 83.06 | 1976 | MC001 |
| | | 1.80 | | | 124.5 | 3.995 | 1.577 | CT | 2.049 | 1.09 | 82.37 | 1976 | MC001 |
| | | 1.80 | | | 124.5 | 3.995 | 1.578 | CT | 2.115 | 1.01 | 79.17 | 1976 | MC001 |
| MILL ANNEALED | E | 4.00 | R.T. | T-L | --- | 4.000 | 1.496 | CT | 1.947 | 1.30 | 92.50 | 1972 | 84306 (2) |
| | | 1.80 | | | --- | 4.000 | 1.496 | CT | 2.084 | 1.29 | 92.10 | 1972 | 84306 (2) |
| | | 1.80 | | | 125.5 | 3.995 | 1.575 | CT | 2.102 | 1.06 | 81.82 | 1976 | MC001 |
| | | 1.80 | | | 125.5 | 3.995 | 1.577 | CT | 2.113 | 1.21 | 87.42 | 1976 | MC001 |
| | | 1.80 | | | 127.0 | 3.995 | 1.578 | CT | 2.096 | 1.13 | 85.71 | 1976 | MC001 |
| | | 1.80 | | | 127.0 | 3.738 | 1.577 | CT | 2.079 | 1.13 | 83.64 | 1976 | MC001 |

NOTES
 (1) COMPOSITION (WGT PERCENT) 6.51AL, 4.06V, 0.02AC, 0.19FE, 0.012N, 0.0064H, 0.150
 (2) COMPOSITION (WGT PERCENT) 6.33AL, 4.31V, 0.022C, 0.14FE, 0.007N, 0.0064H, 0.160

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT (F) | THICK (IN) | FORM | SPECIMEN | | CRACK LENGTH (IN) | 2.5* CRACK LENGTH (K(IIC)/TYS)**2 (IN) | K(IIC) MEAN (KBI/ROOT IN) | K(IIC) STAN DEV (IN) | DATE | REFL | |
|--------------------------------|-----------|--------|----------------------|--------------------------|------------|-------|------------|-------------------|-------------------|--|---------------------------|----------------------|------|-------------|-------|
| | TI-6AL-4V | K(IIC) | | | | | WIDTH (IN) | THICK DESIGN (IN) | | | | | | | |
| MILL ANNEALED 1200F 2HR.AC | F | 4.50 | R.T. | L-T | 130.0 | 2.478 | 1.248 | CT | 1.355 | 0.54 | 60.59 | | 1981 | MA002 | |
| MILL ANNEALED 1300F 2 HR.AC | F | 2.00 | R.T. | L-T | 132.0 | 2.000 | 1.000 | CT | --- | 0.31 | 46.70 | | 1971 | 80538 | |
| | | 2.00 | | | 132.0 | 2.000 | 1.000 | CT | --- | 0.30 | 45.40 | | 1971 | 80538 | |
| | | 2.00 | | | 132.0 | 2.000 | 1.000 | CT | --- | 0.37 | 51.00 | 47.7/ | 2.9 | 1971 | 80538 |
| MILL ANNEALED 1300F 2 HR.AC | F | 2.00 | R.T. | T-L | 133.0 | 2.000 | 1.000 | CT | --- | 0.30 | 46.50 | | 1971 | 80538 | |
| | | 2.00 | | | 133.0 | 2.000 | 1.000 | CT | --- | 0.32 | 48.00 | | 1971 | 80538 | |
| | | 2.00 | | | 133.0 | 2.000 | 1.000 | CT | --- | 0.41 | 53.90 | 49.5/ | 3.9 | 1971 | 80538 |
| MILL ANNEALED 1300F 2 HR.AC | F | 2.00 | R.T. | S-L | 140.0 | 2.000 | 1.000 | CT | --- | 0.18 | 37.90 | | 1971 | 80538 | |
| | | 2.00 | | | 140.0 | 2.000 | 1.000 | CT | --- | 0.31 | 49.50 | | 1971 | 80538 | |
| | | 2.00 | | | 140.0 | 2.000 | 1.000 | CT | --- | 0.24 | 43.50 | 43.6/ | 5.8 | 1971 | 80538 |
| MILL ANNEALED 1300F 2 HR.AC | BT | 2.50 | R.T. | L-T | 120.0 | 2.500 | 1.250 | CT | 1.277 | 1.13 | 60.50 | | 1971 | 84360 | |
| | | 2.50 | | | 127.0 | 2.500 | 1.250 | CT | 1.271 | 1.16 | 86.80 | | 1971 | 84360 | |
| | | 2.50 | | | 127.0 | 2.498 | 1.251 | CT | 1.225 | 1.11 | 85.00 | 84.0/ | 3.4 | 1971 | 84360 |
| RECRYSTALLIZE ANNEAL | P | 1.50 | - | 65 | L-T | --- | 3.999 | 1.502 | CT | 2.044 | 60.40 | | 1972 | 84306 (1) | |
| RECRYSTALLIZE ANNEAL | F | 1.50 | R.T. | L-T | 118.0 | 4.003 | 1.502 | CT | 2.021 | 0.97 | 74.90 | | 1972 | 84306 (1) | |
| | | 1.50 | | | 118.0 | 4.005 | 1.502 | CT | 2.004 | 1.08 | 79.00 | | 1972 | 84306 (1) | |
| | | 2.00 | | | 119.0 | 6.003 | 1.873 | CT | 3.138 | 1.43 | 96.40 | | 1972 | 84306 (1) | |
| | | 2.00 | | | 119.0 | 6.002 | 1.780 | CT | 3.075 | 1.64 | 97.50 | | 1972 | 84306 (1) | |
| | | 1.50 | | | 120.0 | 4.000 | 1.501 | CT | 2.103 | 1.16 | 81.80 | | 1973 | 85836 (1) | |
| | | 2.50 | | | 120.0 | 4.000 | 2.000 | CT | --- | 0.95 | 74.00 | | 1974 | 89004 (1) | |
| | | 2.50 | | | 120.0 | 4.000 | 2.000 | CT | --- | 1.11 | 80.00 | | 1974 | 89004 (1) | |
| | | 1.25 | | | 120.0 | --- | 1.250 | CT | --- | 1.08 | 79.00 | | 1974 | 89004 (1) | |
| | | 2.50 | | | 120.0 | 2.979 | 1.126 | CT | 1.926 | 0.83 | 67.00 | | 1973 | 85836 (1) | |
| | | 1.25 | | | 120.0 | --- | 1.250 | CT | --- | 1.03 | 77.00 | | 1974 | 89004 (1) | |
| | | 2.50 | | | 120.0 | --- | 1.250 | CT | --- | 1.38 | 87.00 | | 1974 | 89004 (1) | |
| | | 1.25 | | | 120.0 | --- | 1.250 | CT | --- | 0.98 | 75.00 | | 1974 | 89004 (1) | |
| | | 2.50 | | | 120.0 | --- | 1.250 | CT | --- | 1.31 | 87.00 | | 1974 | 89004 (1) | |
| | | 1.25 | | | 120.0 | --- | 1.250 | CT | --- | 0.92 | 73.00 | | 1974 | 89004 (1) | |
| | | 2.50 | | | 120.0 | 4.000 | 2.000 | CT | --- | 1.17 | 82.00 | | 1974 | 89004 (1) | |

NOTES
1. 1) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 1.75HR

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | SPECIMEN ORIENT | TEST TEMP (F) | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | K(IIC) (IN) | 2.9° K(IIC)/TYS**2 (IN) | K(IIC) MEAN (K(IIC) REPORT IN) | STAN DEV | DATE | REFER | |
|----------------------|-----------|------|----------------------|-----------------|---------------|------------|------------|--------|-------------------|-------------|-------------------------|--------------------------------|-----------|------|-----------|--------|
| | TI-6AL-4V | | | | | | | | | | | | | | | K(IIC) |
| | M | B | | | | | | | | | | | | | | |
| RECRYSTALLIZE ANNEAL | P | 1.25 | 120.0 | L-Y | R.T. | 1.250 | CT | --- | 1.14 | 81.00 | --- | 81.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 120.0 | | | 6.000 | 1.370 | CT | 1.11 | 80.00 | --- | 80.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 121.0 | | | 6.000 | 1.476 | CT | 1.44 | 91.00 | 3.080 | 91.00 | --- | 1972 | 84306 (1) | |
| | | 1.50 | 121.0 | | | 3.500 | 1.500 | CT | 1.29 | 87.00 | --- | 87.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 121.0 | | | 3.500 | 1.500 | CT | 1.44 | 92.00 | --- | 92.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 121.0 | | | 6.000 | 1.500 | CT | 1.30 | 86.60 | 3.103 | 86.60 | --- | 1972 | 84306 (1) | |
| | | 1.50 | 121.0 | | | 6.001 | 1.497 | CT | 1.41 | 90.20 | 3.065 | 90.20 | --- | 1972 | 84306 (1) | |
| | | | | | | | | | | | | | 82.8/ 7.8 | | | |
| RECRYSTALLIZE ANNEAL | P | 1.50 | --- | T-L | 65 | 3.997 | 1.476 | CT | 1.03 | 77.00 | 2.110 | 77.00 | --- | 1972 | 84306 (1) | |
| RECRYSTALLIZE ANNEAL | P | 2.50 | 120.0 | T-L | R.T. | 3.000 | 1.108 | CT | 0.83 | 69.30 | 1.520 | 69.30 | --- | 1973 | 85836 (1) | |
| | | 2.50 | 120.0 | | | 1.250 | 1.250 | CT | 0.92 | 73.00 | --- | 73.00 | --- | 1974 | 89004 (1) | |
| | | 1.25 | 120.0 | | | 4.000 | 2.000 | CT | 1.25 | 85.00 | --- | 85.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | 4.000 | 2.000 | CT | 1.00 | 76.00 | --- | 76.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | 4.000 | 2.000 | CT | 0.83 | 69.00 | --- | 69.00 | --- | 1974 | 89004 (1) | |
| | | 2.00 | 120.0 | | | --- | --- | CT | 1.50 | 93.00 | --- | 93.00 | --- | 1974 | 89004 (1) | |
| | | 2.00 | 120.0 | | | 6.001 | 2.009 | CT | 1.97 | 106.40 | 3.048 | 106.40 | --- | 1973 | 85836 (1) | |
| | | 1.25 | 120.0 | | | --- | --- | CT | 0.95 | 74.00 | --- | 74.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 120.0 | | | 6.000 | 1.370 | CT | 1.28 | 86.00 | --- | 86.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 120.0 | | | 4.001 | 1.478 | CT | 1.45 | 91.50 | 2.131 | 91.50 | --- | 1973 | 85836 (1) | |
| | | 1.25 | 120.0 | | | --- | --- | CT | 1.14 | 81.00 | --- | 81.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | 4.000 | 2.000 | CT | 0.98 | 75.00 | --- | 75.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 120.0 | | | 3.000 | 1.500 | CT | 1.25 | 85.00 | --- | 85.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | --- | --- | CT | 1.44 | 91.00 | --- | 91.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | 3.000 | 1.127 | CT | 0.90 | 71.90 | 1.344 | 71.90 | --- | 1973 | 85836 (1) | |
| | | 2.00 | 120.0 | | | 5.999 | 1.997 | CT | 1.79 | 101.50 | 3.056 | 101.50 | --- | 1973 | 85836 (1) | |
| | | 2.50 | 120.0 | | | 2.997 | 1.374 | CT | 0.84 | 69.40 | 1.534 | 69.40 | --- | 1973 | 85836 (1) | |
| | | 2.50 | 120.0 | | | --- | --- | CT | 1.14 | 81.00 | --- | 81.00 | --- | 1974 | 89004 (1) | |
| | | 1.25 | 120.0 | | | --- | --- | CT | 0.85 | 70.00 | --- | 70.00 | --- | 1974 | 89004 (1) | |
| | | 2.50 | 120.0 | | | 4.000 | 2.000 | CT | 1.00 | 76.00 | --- | 76.00 | --- | 1974 | 89004 (1) | |
| | | 1.50 | 121.0 | | | 3.500 | 1.500 | CT | 1.18 | 83.00 | --- | 83.00 | --- | 1974 | 89004 (1) | |
| | | 1.00 | 135.0 | | | 2.550 | 1.000 | MDL | 0.65 | 69.20 | --- | 69.20 | --- | 1977 | JEM01 (2) | |
| RECRYSTALLIZE ANNEAL | F | --- | --- | L-T | R.T. | 3.000 | 1.500 | CT | 1.03 | 77.00 | --- | 77.00 | --- | 1974 | 89004 (2) | |
| | | --- | --- | | | 4.000 | 2.030 | CT | 1.20 | 83.00 | --- | 83.00 | --- | 1974 | 89004 (2) | |
| | | --- | --- | | | 3.000 | 1.500 | CT | 0.92 | 73.00 | --- | 73.00 | --- | 1974 | 89004 (2) | |
| | | 2.25 | 114.0 | | | 4.000 | 1.790 | CT | 1.06 | 78.00 | --- | 78.00 | --- | 1974 | 89004 (2) | |
| | | --- | --- | | | 2.977 | 1.499 | CT | 1.43 | 86.10 | 1.528 | 86.10 | --- | 1973 | 85034 (1) | |

NOTES
 (1) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 75HR
 (2) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 75HR
 TYS: APPNDX 120

TABLE 4.11.2.1 (con't)

| CONDITION | --PRIDUCT-- | | TITANIUM | | SPECIMEN | | YIELD STRENGTH (KSI) | M | N | B | A | CRACK LENGTH (IN) | K(1C) | 2.5σ (IN) | K(1C)/TYS)*2 | K(1C) MEAN DEV (KBI-GMOT IN) | K(1C) STAN DEV | DATE | REFER |
|---------------|-------------|------------|------------|--------|------------|------------|----------------------|-------|-------|----|-------|-------------------|-------|-----------|--------------|------------------------------|----------------|------|-------|
| | FORM | THICK (IN) | THICK (IN) | DESIGN | WIDTH (IN) | THICK (IN) | | | | | | | | | | | | | |
| RECRYSTALLIZE | F | 2.25 | R.T. | 1-1 | 1.500 | CT | 115.0 | 2.999 | 1.500 | CT | 1.524 | 1.49 | 89.00 | 1973 | 85034 | (1) | | | |
| ANNEAL | | 2.25 | | | 1.499 | CT | 116.0 | 2.978 | 1.503 | CT | 1.939 | 1.30 | 83.60 | 1973 | 85034 | (1) | | | |
| | | 3.40 | | | 1.503 | CT | 117.0 | 2.979 | 1.500 | CT | 1.934 | 1.47 | 89.70 | 1973 | 85034 | (1) | | | |
| | | 2.25 | | | 1.500 | CT | 117.0 | 3.002 | 1.500 | CT | 1.539 | 1.05 | 76.00 | 1973 | 85034 | (1) | | | |
| | | 5.62 | | | 1.499 | CT | 118.0 | 3.004 | 1.499 | CT | 1.540 | 1.46 | 90.30 | 1973 | 85034 | (1) | | | |
| | | 3.25 | | | 1.499 | CT | 118.0 | 2.999 | 1.499 | CT | 1.526 | 1.19 | 81.30 | 1973 | 85034 | (1) | | | |
| | | 5.62 | | | 1.497 | CT | 119.0 | 3.008 | 1.497 | CT | 1.536 | 1.46 | 90.90 | 1973 | 85034 | (1) | | | |
| | | 2.20 | | | 1.498 | CT | 119.0 | 3.007 | 1.498 | CT | 1.563 | 1.49 | 91.90 | 1973 | 85857 | (1) | | | |
| | | 2.20 | | | 1.500 | CT | 119.0 | 3.003 | 1.500 | CT | 1.932 | 1.36 | 87.60 | 1973 | 85857 | (1) | | | |
| | | 3.40 | | | 1.501 | CT | 119.0 | 3.002 | 1.501 | CT | 1.933 | 1.39 | 80.90 | 1973 | 85034 | (1) | | | |
| | | 2.20 | | | 1.502 | CT | 120.0 | 3.006 | 1.502 | CT | 1.981 | 1.41 | 90.10 | 1973 | 85857 | (1) | | | |
| | | 6.70 | | | 1.502 | CT | 121.0 | 3.000 | 1.502 | CT | 1.941 | 0.96 | 75.10 | 1973 | 85034 | (1) | | | |
| | | 1.20 | | | 1.376 | CT | 121.0 | 3.004 | 1.376 | CT | 1.615 | 1.23 | 84.40 | 1973 | 85857 | (1) | | | |
| | | 1.20 | | | 1.374 | CT | 121.0 | 3.005 | 1.374 | CT | 1.989 | 1.27 | 86.10 | 1973 | 85857 | (1) | | | |
| | | 1.20 | | | 1.345 | CT | 121.0 | 3.010 | 1.345 | CT | 1.936 | 1.15 | 82.10 | 1973 | 85857 | (1) | | | |
| | | 6.70 | | | 1.500 | CT | 121.0 | 3.001 | 1.500 | CT | 1.948 | 1.04 | 78.70 | 1973 | 85034 | (1) | | | |
| | | 2.20 | | | 1.502 | CT | 121.0 | 3.003 | 1.502 | CT | 1.989 | 1.17 | 82.60 | 1973 | 85857 | (1) | | | |
| | | 2.20 | | | 1.504 | CT | 121.0 | 3.002 | 1.504 | CT | 1.955 | 1.24 | 85.10 | 1973 | 85857 | (1) | | | |
| | | 2.20 | | | 1.499 | CT | 122.0 | 3.003 | 1.499 | CT | 1.633 | 1.18 | 83.90 | 1973 | 85857 | (1) | | | |
| | | 1.20 | | | 1.318 | CT | 122.0 | 3.009 | 1.318 | CT | 1.983 | 1.12 | 81.70 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.417 | CT | 123.0 | 2.998 | 1.417 | CT | 1.993 | 0.95 | 75.90 | 1973 | 85034 | (1) | | | |
| | | 1.20 | | | 1.377 | CT | 123.0 | 3.006 | 1.377 | CT | 1.605 | 1.17 | 84.30 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.377 | CT | 123.0 | 3.002 | 1.377 | CT | 1.978 | 0.80 | 73.20 | 1973 | 85034 | (1) | | | |
| | | 2.20 | | | 1.501 | CT | 124.0 | 3.003 | 1.501 | CT | 1.607 | 1.16 | 84.40 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.409 | CT | 124.0 | 3.004 | 1.409 | CT | 1.977 | 0.94 | 76.00 | 1973 | 85034 | (1) | | | |
| | | 3.20 | | | 1.504 | CT | 124.0 | 3.001 | 1.504 | CT | 1.983 | 1.49 | 93.70 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.504 | CT | 124.0 | 2.999 | 1.504 | CT | 1.985 | 0.98 | 77.60 | 1973 | 85034 | (1) | | | |
| | | 2.20 | | | 1.504 | CT | 124.0 | 3.005 | 1.504 | CT | 1.949 | 1.08 | 81.50 | 1973 | 85034 | (1) | | | |
| | | 1.20 | | | 1.375 | CT | 125.0 | 3.001 | 1.375 | CT | 1.612 | 1.14 | 81.60 | 1973 | 85857 | (1) | | | |
| | | 2.20 | | | 1.495 | CT | 126.0 | 3.003 | 1.495 | CT | 1.991 | 1.11 | 83.60 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.248 | CT | 127.0 | 3.001 | 1.248 | CT | 1.542 | 1.17 | 86.70 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.250 | CT | 127.0 | 3.003 | 1.250 | CT | 1.527 | 1.24 | 89.50 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.250 | CT | 127.0 | 3.001 | 1.250 | CT | 1.983 | 1.20 | 88.00 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.248 | CT | 129.0 | 2.979 | 1.248 | CT | 1.988 | 1.07 | 84.40 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.249 | CT | 129.0 | 2.997 | 1.249 | CT | 1.440 | 1.08 | 84.60 | 1973 | 85857 | (1) | | | |
| | | 1.50 | | | 1.372 | CT | 130.0 | 3.002 | 1.372 | CT | 1.560 | 0.92 | 78.80 | 1973 | 85034 | (1) | | | |
| RECRYSTALLIZE | F | --- | R.T. | 1-1 | 1.750 | CT | --- | 3.500 | 1.750 | CT | --- | 1.31 | 87.00 | 1974 | 89004 | (2) | | | |
| ANNEAL | | | | | | | | | | | | | | | | | | | |

83.6/ 9.5

NOTES:
 (1) RECRYSTALLIZE ANNEAL=1700F 4 HR, FC TO 1400F AT 100F/HR, COOL TO 900F IN 75HR
 (2) RECRYSTALLIZE ANNEAL=1700F 4 HR, FC TO 1400F AT 100F/HR, COOL TO 900F IN 75HR
 TYS: APPRIK 120

TABLE 4.11.2.1 (con't)

| CONDITION | --4" RODUCT-- | | YIELD STRENGTH (KSI) | SPECIMEN | | CRACK LENGTH (IN) | 2.5* K(1C)/TVS**2 (IN) | K(1C) MEAN DEV (KSI*SQRT IN) | K(1C) STAN DEV | DATE | REFER |
|---------------|---------------|------------|----------------------|------------|-------------------|-------------------|------------------------|------------------------------|----------------|------|-----------|
| | FORM | THICK (IN) | | THICK (IN) | DESIGN THICK (IN) | | | | | | |
| RECRYSTALLIZE | F | --- | --- | 3.000 | 1.500 | CT | 1.03 | 77.00 | | 1974 | 89004 (1) |
| ANNEAL | | --- | --- | 3.000 | 1.500 | CT | 0.85 | 70.00 | | 1974 | 89004 (1) |
| | | --- | --- | 3.500 | 1.750 | CT | 1.40 | 90.00 | | 1974 | 89004 (1) |
| | | 3.40 | 116.0 | 3.000 | 1.502 | CT | 1.544 | 85.70 | | 1973 | 85034 (1) |
| | | 5.62 | 117.0 | 3.001 | 1.500 | CT | 1.34 | 82.50 | | 1973 | 85034 (1) |
| | | 6.70 | 118.0 | 2.997 | 1.500 | CT | 1.578 | 85.80 | | 1973 | 85034 (1) |
| | | 5.62 | 119.0 | 3.001 | 1.500 | CT | 1.18 | 81.80 | | 1973 | 85034 (1) |
| | | 3.40 | 119.0 | 3.002 | 1.500 | CT | 1.345 | 84.90 | | 1973 | 85034 (1) |
| | | 5.62 | 120.0 | 2.977 | 1.499 | CT | 1.518 | 77.00 | | 1973 | 85034 (1) |
| | | 3.50 | 120.0 | 3.007 | 1.502 | CT | 1.374 | 88.40 | | 1973 | 85857 (1) |
| | | 5.62 | 120.0 | 3.005 | 1.498 | CT | 1.25 | 84.70 | | 1973 | 85034 (1) |
| | | 1.90 | 121.0 | 3.004 | 1.500 | CT | 1.573 | 80.20 | | 1973 | 85857 (1) |
| | | 6.70 | 121.0 | 3.002 | 1.500 | CT | 1.546 | 68.80 | | 1973 | 85034 (1) |
| | | 1.90 | 122.0 | 3.000 | 1.245 | CT | 1.475 | 84.80 | | 1973 | 85857 (1) |
| | | 1.90 | 122.0 | 3.000 | 1.248 | CT | 1.547 | 75.50 | | 1973 | 85857 (1) |
| | | 3.40 | 123.0 | 2.998 | 1.497 | CT | 1.493 | 70.40 | | 1973 | 85034 (1) |
| | | 4.75 | 123.0 | 3.004 | 1.502 | CT | 1.558 | 82.00 | | 1973 | 85034 (1) |
| | | 6.70 | 123.0 | 3.000 | 1.501 | CT | 1.544 | 89.60 | | 1973 | 85034 (1) |
| | | 3.50 | 123.0 | 2.978 | 1.500 | CT | 1.32 | 89.20 | | 1973 | 85034 (1) |
| | | 2.20 | 124.0 | 3.002 | 1.502 | CT | 1.24 | 87.30 | | 1973 | 85857 (1) |
| | | 6.70 | 124.0 | 2.996 | 1.502 | CT | 1.12 | 83.00 | | 1973 | 85034 (1) |
| | | 4.75 | 125.0 | 3.001 | 1.502 | CT | 1.24 | 87.90 | | 1973 | 85034 (1) |
| | | 2.20 | 125.0 | 3.006 | 1.498 | CT | 1.03 | 90.30 | | 1973 | 85857 (1) |
| | | 3.20 | 126.0 | 3.000 | 1.508 | CT | 1.589 | 90.70 | | 1973 | 85857 (1) |
| | | 2.25 | 126.0 | 2.993 | 1.502 | CT | 1.51 | 91.50 | | 1973 | 85034 (1) |
| | | 3.20 | 126.0 | 2.998 | 1.500 | CT | 1.02 | 90.50 | | 1973 | 85034 (1) |
| | | 2.20 | 126.0 | 3.000 | 1.501 | CT | 1.47 | 96.50 | | 1973 | 85857 (1) |
| | | 2.25 | 127.0 | 3.008 | 1.502 | CT | 1.38 | 94.40 | | 1973 | 85857 (1) |
| | | 2.20 | 127.0 | 3.001 | 1.500 | CT | 1.34 | 93.10 | | 1973 | 85034 (1) |
| | | 2.20 | 127.0 | 3.002 | 1.500 | CT | 1.03 | 81.40 | | 1973 | 85857 (1) |
| | | 1.90 | 128.0 | 3.002 | 1.508 | CT | 0.97 | 79.70 | | 1973 | 85034 (1) |
| | | 2.20 | 128.0 | 3.006 | 1.500 | CT | 0.88 | 75.90 | | 1973 | 85857 (1) |
| | | 1.50 | 129.0 | 3.001 | 1.377 | CT | 0.85 | 73.40 | | 1973 | 85034 (1) |
| | | 1.50 | 129.0 | 3.003 | 1.424 | CT | 0.83 | 74.20 | | 1973 | 85034 (1) |
| | | 1.50 | 129.0 | 2.979 | 1.353 | CT | 1.11 | 82.90 | | 1973 | 85034 (1) |
| | | 1.50 | 129.0 | 3.000 | 1.367 | CT | 1.02 | 82.20 | | 1973 | 85034 (1) |
| | | 1.20 | 130.0 | 3.004 | 1.347 | CT | 1.26 | 92.50 | | 1973 | 85857 (1) |
| | | 1.50 | 130.0 | 3.001 | 1.368 | CT | 1.16 | 88.60 | | 1973 | 85034 (1) |
| | | 1.20 | 130.0 | 3.010 | 1.319 | CT | 1.22 | 90.80 | | 1973 | 85857 (1) |

NOTES: (1) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 75HR TVS APPROX 120

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | SPECIMEN THICK (IN) | DESIGN | CRACK LENGTH (IN) | 2.5* (K(1C)/TYS)±0.3 (IN) | K(1C) MEAN (KSI±0.01 IN) | K(1C) STAN DEV (KSI±0.01 IN) | DATE | REF |
|--|-----------|---------------|----------------------|---------------------|--------|-------------------|---------------------------|--------------------------|------------------------------|------|-----------|
| | FORM (IN) | TEST TEMP (F) | | | | | | | | | |
| RECRYSTALLIZE AIRCAL | F | 1.50 | 130.0 | 3.004 | 1.399 | CT | 1.987 | 81.70 | | 1973 | 85034 (1) |
| | | 1.20 | 130.0 | 3.008 | 1.344 | CT | 1.653 | 92.60 | | 1973 | 85857 (1) |
| | | 2.25 | 130.0 | 3.000 | 1.500 | CT | 1.522 | 94.50 | | 1973 | 85034 (1) |
| | | 1.20 | 131.0 | 3.005 | 1.375 | CT | 1.599 | 76.30 | | 1973 | 85857 (1) |
| | | 2.20 | 131.0 | 3.006 | 1.497 | CT | 1.592 | 80.60 | | 1973 | 85857 (1) |
| | | 1.50 | 132.0 | 3.000 | 1.409 | CT | 1.563 | 79.00 | | 1973 | 85034 (1) |
| | | 1.20 | 133.0 | 3.006 | 1.374 | CT | 1.577 | 77.90 | | 1973 | 85857 (1) |
| | | 2.25 | 134.0 | 2.998 | 1.499 | CT | 1.537 | 86.30 | | 1973 | 85034 (1) |
| | | 1.20 | 134.0 | 3.009 | 1.380 | CT | 1.625 | 91.00 | | 1973 | 85857 (1) |
| | | 1.20 | 136.0 | 3.007 | 1.377 | CT | 1.585 | 89.40 | 83.9/ | 1973 | 85857 (1) |
| RECRYSTALLIZE AIRCAL | F | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| | | 4.60 | 118.0 | 3.000 | 1.500 | CT | --- | 83.00 | | 1974 | 89004 (2) |
| | | 6.70 | 121.0 | 3.001 | 1.502 | CT | 1.559 | 89.30 | | 1973 | 85634 (1) |
| | | 6.70 | 122.0 | 3.000 | 1.502 | CT | 1.552 | 92.30 | | 1973 | 85034 (1) |
| | | 4.75 | 122.0 | 3.000 | 1.500 | CT | 1.540 | 91.10 | | 1973 | 85034 (1) |
| | | 6.70 | 122.0 | 2.997 | 1.501 | CT | 1.573 | 90.20 | | 1973 | 85034 (1) |
| | | 4.60 | 122.0 | 3.001 | 1.501 | CT | 1.532 | 90.60 | | 1973 | 85034 (1) |
| | | 4.75 | 124.0 | 3.005 | 1.502 | CT | 1.540 | 86.70 | | 1973 | 85634 (1) |
| | | 6.70 | 125.0 | 3.001 | 1.501 | CT | 1.544 | 91.70 | | 1973 | 85034 (1) |
| | | | | | | | | | 88.9/ | 1972 | 85034 (1) |
| STA | P | 0.62 | 160.0 | 3.503 | 0.633 | CT | 1.831 | 40.30 | | 1973 | 85856 |
| | | 0.62 | 160.0 | 3.503 | 0.634 | CT | 1.801 | 43.50 | | 1973 | 85856 |
| | | 0.62 | 160.0 | 3.501 | 0.632 | CT | 1.790 | 44.00 | 42.6/ | 1973 | 85856 |
| STA | F | 2.00 | 126.9 | --- | 2.000 | --- | --- | 92.32 | | --- | R1003 |
| STA | F | 2.00 | 132.0 | --- | 2.000 | --- | --- | 83.32 | | --- | R1003 |
| STA 1750F 1 HR. WQ. 1300F 2 HR. AC | F | 2.50 | 142.0 | 2.000 | 1.000 | CT | 1.000 | 59.80 | | 1974 | 88962 |
| | | 2.50 | 142.0 | 2.000 | 1.000 | CT | 1.000 | 56.90 | | 1974 | 88962 |
| | | 2.50 | 142.0 | 2.000 | 1.000 | CT | 1.000 | 61.40 | 59.4/ | 1974 | 88962 |

NOTES:
 (1) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 75HR
 (2) RECRYSTALLIZE ANNEAL=1700F 4 HR. FC TO 1400F AT 100F/HR. COOL TO 900F IN 75HR
 TYS APPROX. 120

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | YIELD (NSI) | THICKNESS (IN) | TEST TEMP (F) | SPECIMEN ORIENT | SPECIMEN | | CRACK LENGTH (IN) | K(IIC) (KSI√IN) | K(IIC) MEAN (KSI√IN) | STAN DEV | DATE | REFER | |
|-------------------|----------|-------------------|----------------|-------------------|------------------|-----------------|---------------|-------------------|----------------------|--------------------|-------------------------|-------------|------|-------|--------|
| | FORM | THICKNESS (IN) | | | | | WIDTH (IN) | THICKNESS (IN) | | | | | | | DESIGN |
| 1450F 1HR AC P | 1.00 | | 146.0 | | R.T. | T-L | 1.000 | CT | --- | 0.23 | 44.00 | | 1981 | MR001 | |
| 1700F 6 HR AC F | 1.40 | | 118.0 | 3.006 | R.T. | L-T | 1.317 | CT | 1.605 | 0.97 | 74.10 | | 1973 | 85857 | |
| 1450F 6 HR AC | 1.40 | | 119.0 | 3.002 | | | 1.365 | CT | 1.615 | 1.16 | 81.30 | | 1973 | 85857 | |
| | 1.40 | | 119.0 | 3.002 | | | 1.231 | CT | 1.587 | 0.91 | 71.60 | | 1973 | 85857 | |
| | 1.40 | | 119.0 | 3.004 | | | 1.350 | CT | 1.588 | 1.16 | 81.10 | | 1973 | 85857 | |
| | 1.40 | | 119.0 | 3.003 | | | 1.301 | CT | 1.583 | 0.94 | 73.00 | | 1973 | 85857 | |
| | 1.40 | | 120.0 | 3.002 | | | 1.290 | CT | 1.604 | 1.07 | 74.40 | 79.9/ | 4.2 | 1973 | 85857 |
| 1700F 6 HR AC F | 1.40 | | 126.0 | 3.001 | R.T. | T-L | 1.357 | CT | 1.564 | 1.17 | 86.30 | | 1973 | 85857 | |
| 1400F 6 HR AC | 1.40 | | 126.0 | 3.002 | | | 1.311 | CT | 1.599 | 0.91 | 76.00 | | 1973 | 85857 | |
| | 1.40 | | 127.0 | 3.004 | | | 1.353 | CT | 1.617 | 1.18 | 87.50 | | 1973 | 85857 | |
| | 1.40 | | 129.0 | 3.006 | | | 1.325 | CT | 1.500 | 0.88 | 74.80 | | 1973 | 85857 | |
| | 1.40 | | 129.0 | 3.005 | | | 1.279 | CT | 1.568 | 1.09 | 85.20 | | 1973 | 85857 | |
| | 1.40 | | 129.0 | 3.006 | | | 1.336 | CT | 1.632 | 0.92 | 77.10 | 81.2/ | 5.8 | 1973 | 85857 |
| 1750F 1 HR. WQ. F | 3.00 | | 159.0 | 5.100 | 75 | T-L | 2.000 | WOL | 1.998 | 0.43 | 66.30 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 159.0 | 5.100 | | | 2.000 | WOL | 2.091 | 0.48 | 70.00 | 68.2/ | 2.6 | 1966 | 76411 |
| 1750F 1 HR. WQ. F | 3.00 | | 153.0 | 5.100 | 40 | T-L | 2.000 | WOL | 2.088 | 0.63 | 76.80 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 153.0 | 5.100 | | | 2.000 | WOL | 2.059 | 0.47 | 66.20 | 71.9/ | 7.5 | 1966 | 76411 |
| 1750F 1 HR. WQ. F | 3.00 | | 147.0 | 5.100 | 0 | T-L | 2.000 | WOL | 1.998 | 0.51 | 66.40 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 147.0 | 5.100 | | | 2.000 | WOL | 2.081 | 0.61 | 72.90 | 69.7/ | 4.6 | 1966 | 76411 |
| 1750F 1 HR. WQ. F | 3.00 | | 148.0 | 5.100 | 32 | T-L | 2.000 | WOL | 2.041 | 0.47 | 64.40 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 148.0 | 5.100 | | | 2.000 | WOL | 2.011 | 0.49 | 65.30 | 63.0/ | 0.8 | 1966 | 76411 |
| 1750F 1 HR. WQ. F | 3.00 | | 140.0 | 5.100 | R.T. | T-L | 2.000 | WOL | 1.986 | 0.91 | 84.90 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 140.0 | 5.100 | | | 2.000 | WOL | 2.019 | 0.75 | 76.60 | | 1966 | 76411 | |
| | 3.00 | | 140.0 | 5.100 | | | 2.000 | WOL | 2.010 | 0.74 | 76.30 | 79.3/ | 4.9 | 1966 | 76411 |
| 1750F 1 HR. WQ. F | 3.00 | | 133.0 | 5.100 | 100 | T-L | 2.000 | WOL | 1.969 | 0.75 | 72.90 | | 1966 | 76411 | |
| 1000F 4 HR | 3.00 | | 133.0 | 5.100 | | | 2.000 | WOL | 2.049 | 0.68 | 67.30 | 71.1/ | 2.5 | 1966 | 76411 |

TABLE 4.11.2.1 (con't)

| CONDITION | TITANIUM | | TI-6AL-4V | K(1C) | --PHOSPHOR-- | | TEST SPECIMEN | | YIELD STRENGTH (KSI) | WIDTH (IN) | SPECIMEN | | CRACK LENGTH (IN) | 2.5% K(1C)/TYS**2 (KSI*SQRT IN) | K(1C) MEAN DEV | K(1C) STAN DEV | DATE | REFER |
|--|----------|------------|-----------|-------|--------------|--------|---------------|--------|----------------------|------------|----------|------------|-------------------|---------------------------------|----------------|----------------|------|-------|
| | FORM | THICK (IN) | | | THICK (IN) | DESIGN | THICK (IN) | DESIGN | | | W | R | | | | | | |
| 1750F 1 HR. WQ. 1000F 4 HR | F | 3 00 | 150 | Y-L | 127.0 | 5 100 | 2 000 | WOL | 1 970 | 0 85 | 74 00 | 1966 76411 | | | | | | |
| | | 3 00 | | | 127.0 | 5 100 | 2 000 | WOL | 2 033 | 1 00 | 82 00 | 1966 76411 | | | | | | |
| 1750F 1HR.FC TO 1100F.AC | P | 1 50 | R.T. | L-T | 120.0 | 4 005 | 1 501 | CT | 1 991 | 1 20 | 83 00 | 1973 85836 | | | | | | |
| 1750F 1HR.FC TO 1100F.AC | P | 1 50 | R.T. | T-L | 120.0 | 4 004 | 1 501 | CT | 1 938 | 1 41 | 70 00 | 1973 85836 | | | | | | |
| | | 1 50 | | | 120.0 | 4 000 | 1 500 | CT | ---- | 1 50 | 93 00 | 1974 89004 | | | | | | |
| 1750F 1HR.FC TO RT | P | 1 50 | R.T. | L-T | 120.0 | 4 004 | 1 502 | CT | 1 717 | 0 84 | 69 50 | 1973 85836 | | | | | | |
| | | 1 50 | | | 120.0 | 4 004 | 1 501 | CT | 1 718 | 0 95 | 74 00 | 1973 85836 | | | | | | |
| 1750F 1HR.FC TO RT | P | 1 50 | R.T. | T-L | 120.0 | 4 008 | 1 502 | CT | 1 956 | 1 43 | 90 60 | 1973 85836 | | | | | | |
| | | 1 50 | | | 120.0 | 4 003 | 1 502 | CT | 1 986 | 1 49 | 92 90 | 1973 85836 | | | | | | |
| 1750F 2 HR.FC TO 900F AT 100F/1HR.AC | F | 3 00 | R.T. | L-T | 115.0 | 3 005 | 1 500 | CT | 1 716 | 1 20 | 79 80 | 1973 88440 | | | | | | |
| 1750F 2 HR.FC TO 900F AT 100F/1HR.AC | F | 3 00 | R.T. | T-L | 130.0 | 3 005 | 1 500 | CT | 1 581 | 1 21 | 90 90 | 1973 88440 | | | | | | |
| 1750F 2HR.WQ. 1000F 2HR.AC. 1350F 2HR.AC.STA | P | 0 62 | R.T. | L-T | 150.0 | 3 501 | 0 634 | CT | 1 865 | 0 17 | 39 80 | 1973 85836 | | | | | | |
| | | 0 62 | | | 150.0 | 3 501 | 0 633 | CT | 1 880 | 0 20 | 43 00 | 1973 85836 | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| 1500F. 0 5HR. AC 1350F. 21MS. AC | P | 1 00 | R.T. | T-L | 126.0 | ---- | 1 000 | CT | ---- | 1 44 | 95 60 | 1981 NR001 | | | | | | |

TABLE 4.11.2.2

| TITANIUM | | TI-6AL-4V | | K(C) | | CRACK LENGTH | | CROSS STRESS | | K(I) STAN | | K(I) STAN | | | | | | | | |
|------------------------------------|-------------------|---------------|-----------------------------|-----------------------|---------------|--------------|--------------|---------------|----------------|-------------|--------------|-----------|------|------|------|--------------|-------------|------|-------|------------|
| CONDITION | PRODUCT-- FORM | THICK (IN) | TEST SPEC TEMP OR (F) | YIELD STR (KSI) | WIDTH (IN) | THICK B | INIT (IN) | FINAL (IN) | ORSET (KSI) | MAX S(I) | K(I) | K(I) | STAN | K(I) | STAN | MEAN (IN) | DEV (IN) | DATE | REFER | |
| | | | | | | | | | | | | | | | | | | | | W |
| BUCKLING OF CRACK EDGES RESTRAINED | | | | | | | | | | | | | | | | | | | | |
| ANNEALED | S | 0.04 | -109 | L-T | 163.0 | 8.000 | 0.040 | 3.060 | --- | 47.40 | 114.42 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 1.040 | --- | 94.10 | 121.54 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 0.890 | --- | 101.00 | 117.52 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 1.340 | --- | 77.20 | 122.89 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 2.000 | --- | 73.60 | 135.72 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 4.840 | --- | 33.60 | 121.50 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 163.0 | 8.000 | 0.040 | 4.440 | --- | 35.30 | 116.22 | 121.4 | 7.0 | --- | --- | --- | --- | --- | --- | 1963 54304 |
| BUCKLING OF CRACK EDGES RESTRAINED | | | | | | | | | | | | | | | | | | | | |
| ANNEALED | S | 0.04 | R.T. | L-T | 137.3 | 8.000 | 0.040 | 4.050 | --- | 47.50 | 143.18 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 3.030 | --- | 36.20 | 137.12 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 2.030 | --- | 78.60 | 145.78 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 0.930 | --- | 108.30 | 133.46* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 1.950 | --- | 95.50 | 152.36* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 3.030 | --- | 61.20 | 146.71 | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 137.3 | 8.000 | 0.040 | 0.480 | --- | 126.00 | 109.63*143.2 | 4.3 | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| BUCKLING OF CRACK EDGES RESTRAINED | | | | | | | | | | | | | | | | | | | | |
| ANNEALED | S | 0.04 | 590 | L-T | 96.7 | 8.000 | 0.040 | 0.250 | --- | 111.20 | 69.73* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 96.7 | 8.000 | 0.040 | 1.260 | --- | 91.00 | 130.02* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 96.7 | 8.000 | 0.040 | 0.570 | --- | 101.20 | 96.06* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 96.7 | 8.000 | 0.040 | 0.950 | --- | 94.90 | 116.95* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |
| | | 0.04 | | | 96.7 | 8.000 | 0.040 | 2.020 | --- | 80.50 | 149.31* | --- | --- | --- | --- | --- | --- | --- | --- | 1963 54304 |

BUCKLING OF CRACK EDGES UNKNOWN

| | | | | | | | | | | | | | | | | | | | | |
|----|---|------|------|-----|-------|--------|-------|--------|--------|-------|-------|--------------|------------|---------|-----|-----|-----|-----|-----|------------|
| MA | P | 0.25 | R.T. | L-T | 130.0 | 9.630 | 0.266 | 3.780 | 6.860 | 18.70 | 37.80 | 148.60 | --- | --- | --- | --- | --- | --- | --- | 1971 83984 |
| | | 0.25 | | | 130.0 | 9.630 | 0.280 | 3.800 | 5.220 | 23.60 | 51.70 | 140.00 | --- | --- | --- | --- | --- | --- | --- | 1971 83984 |
| | | 0.25 | | | 130.0 | 9.630 | 0.293 | 1.920 | --- | 36.50 | 85.10 | 151.32*144.3 | 6.1 | --- | --- | --- | --- | --- | --- | 1971 83984 |
| MA | P | 0.25 | R.T. | L-T | 130.0 | 16.110 | 0.285 | 12.930 | 13.950 | 11.30 | 15.40 | 125.65 | --- | --- | --- | --- | --- | --- | --- | 1971 83984 |
| MA | P | 0.25 | R.T. | L-T | 130.0 | 16.120 | 0.240 | 8.020 | 10.580 | 31.30 | 45.10 | 189.99 | --- | --- | --- | --- | --- | --- | --- | 1971 83984 |
| | | 0.25 | | | 130.0 | 16.120 | 0.275 | 3.990 | 6.100 | 31.10 | 67.50 | 175.67 | 182.8/10.1 | 229.36* | --- | --- | --- | --- | --- | 1971 83984 |

*NOTE - NET SECTION STRESS EXCEEDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.11.2.2 (con't)

| TITANIUM | | TI-6AL-4V | | K(C) | | CRACK LENGTH GROSS STRESS | | | | | | K(APP) STAN | | K(C) STAN | | | |
|-----------|---|-----------------------|---------------------------|---------------|--------------|---------------------------|----------------|--------------|---------|------------|-----------------------|-------------|--------------|-----------------------|-------------|-------|------------|
| CONDITION | --PRODUCT-- FORM THICK TEMP OR (IN) (F) | YIELD STR (KSI) | SPECIMEN WIDTH (IN) | THICK (IN) | INIT (IN) | FINAL (IN) | ONSET (KSI) | MAX (KSI) | R(D) | S(MAX) | MEAN (KSI*80RT IN) | DEV (IN) | STAN K(C) | MEAN (KSI*80RT IN) | DEV (IN) | REFER | |
| | | | | | | | | | | | | | | | | | M |
| MA | S 0.20 R.T. L-T | 129.3 | 24.070 | 0.212 | 3.010 | --- | --- | 93.10 | 204.41* | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| | C 20 | 129.3 | 24.080 | 0.220 | 10.000 | --- | --- | 59.30 | 249.86 | 238.9/11.2 | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.05 82 L-T | 136.9 | 24.070 | 0.051 | 5.990 | 7.100 | 43.30 | 47.50 | 151.53 | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.05 - 110 T-L | 163.3 | 8.000 | 0.050 | 1.980 | 3.130 | 39.00 | 84.70 | 153.28 | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| | 0.05 | 163.3 | 8.010 | 0.050 | 1.970 | 2.540 | 72.50 | 77.30 | 141.29 | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| | 0.05 | 164.3 | 8.010 | 0.032 | 1.920 | 2.370 | 66.60 | 75.50 | 132.97 | 144.2/10.0 | 194.07 | 159.4/ 7.5 | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.03 R.T. T-L | 127.0 | 8.040 | 0.025 | 1.980 | 2.600 | 61.20 | 75.60 | 138.54 | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.05 R.T. T-L | 136.0 | 8.010 | 0.052 | 2.000 | 2.220 | 90.00 | 95.30 | 175.72* | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.13 R.T. T-L | 139.7 | 8.050 | 0.127 | 1.980 | 2.740 | 48.00 | 103.70 | 170.02* | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.03 650 F-L | 80.2 | 8.030 | 0.025 | 2.060 | 2.460 | 79.70 | 77.70 | 145.73* | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |
| MA | S 0.05 650 T-L | 81.7 | 8.020 | 0.031 | 2.000 | 2.090 | 63.40 | 75.40 | 139.01* | --- | --- | --- | --- | --- | --- | --- | 1964 57573 |

BUCKLING OF CRACK EDGES RESTRAINED

| TITANIUM | | TI-6AL-4V | | K(C) | | CRACK LENGTH GROSS STRESS | | | | | | K(APP) STAN | | K(C) STAN | | | |
|--------------|---|-----------------------|---------------------------|---------------|--------------|---------------------------|----------------|--------------|------|--------|-----------------------|-------------|--------------|-----------------------|-------------|-------|------------|
| CONDITION | --PRODUCT-- FORM THICK TEMP OR (IN) (F) | YIELD STR (KSI) | SPECIMEN WIDTH (IN) | THICK (IN) | INIT (IN) | FINAL (IN) | ONSET (KSI) | MAX (KSI) | R(D) | S(MAX) | MEAN (KSI*80RT IN) | DEV (IN) | STAN K(C) | MEAN (KSI*80RT IN) | DEV (IN) | REFER | |
| | | | | | | | | | | | | | | | | | M |
| 1300F 1HR.AC | F | --- | R.T. L-T | 147.1 | 5.970 | 0.382 | 2.020 | 3.200 | --- | 53.50 | 102.64 | --- | --- | --- | --- | --- | 1964 58782 |
| | --- | --- | --- | 147.1 | 5.970 | 0.382 | 2.020 | 3.180 | --- | 51.90 | 99.57 | 101.1/ 2.2 | 141.72 | 144.4/ 3.7 | --- | --- | 1964 58782 |
| 1300F 1HR.AC | F | --- | R.T. L-T | 147.1 | 8.970 | 0.732 | 3.000 | 5.000 | --- | 54.40 | 126.94 | --- | --- | --- | --- | --- | 1964 58782 |
| 1300F 1HR.AC | F | --- | R.T. L-T | 147.1 | 8.970 | 0.998 | 3.000 | 5.200 | --- | 28.30 | 64.05 | --- | --- | --- | --- | --- | 1964 58782 |

-NOTE- NET SECTION STRESS EXCEEDS 80% OF YIELD STRENGTH VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.11.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.1 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|------|---|---|
| CONDITION: | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: | 6.09 | .129 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 7.00 | .238 | | |
| | 8.00 | .340 | | | |
| | 9.00 | .572 | | | |
| | 10.00 | 1.36 | | | |
| DELTA K MAX | A: | 12.31 | 2.80 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.09 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM:
 SPECIMEN TYPE:
 ORIENTATION:
 STRESS RATIO: +0.10
 FREQUENCY: 30.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.081"
 SPECIMEN WIDTH: 2.500"
 REFERENCES: PW003

TITAN.
ALLOY

TI-6AL-
4V

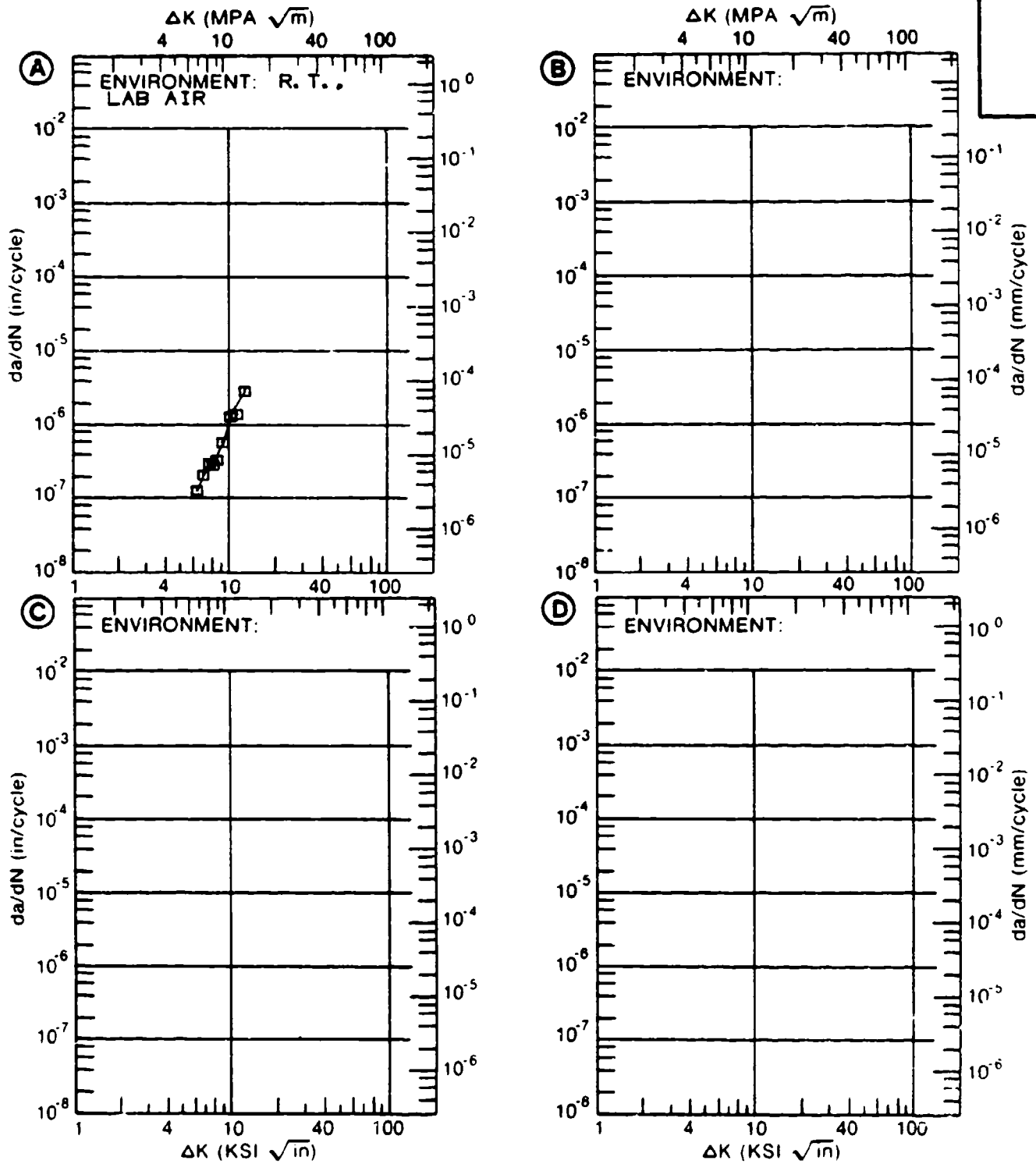


Figure 4.11.3.1

TABLE 4.11.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.2 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION:
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|----------|----------|----------|
| | | A | B | C | D |
| | | R=+0. 10 | R=+0. 30 | R=+0. 50 | R=+0. 70 |
| DELTA K | A: 11.07 | 1.31 | | | |
| MIN | B: 7.27 | | .201 | | |
| | C: 5.18 | | | .0883 | |
| | D: 3.07 | | | | .0336 |
| | 3.50 | | | | .0473 |
| | 4.00 | | | | .0707 |
| | 5.00 | | | | .152 |
| | 6.00 | | | .165 | .300 |
| | 7.00 | | | .334 | .544 |
| | 8.00 | | .400 | .656 | 1.04 |
| | 9.00 | | .904 | 1.14 | |
| | 10.00 | | 1.65 | 1.81 | |
| | 13.00 | 2.86 | 4.56 | 5.34 | |
| | 16.00 | 5.86 | 8.52 | 12.1 | |
| | 20.00 | 10.4 | 17.0 | | |
| | 25.00 | 17.8 | | | |
| | 30.00 | 31.2 | | | |
| | 35.00 | 58.9 | | | |
| | 40.00 | 121. | | | |
| DELTA K | A: 41.03 | 142. | | | |
| MAX | B: 21.70 | | 20.4 | | |
| | C: 18.26 | | | 18.5 | |
| | D: 8.80 | | | | 1.80 |
| ROOT MEAN SQUARE | | 12.53 | 16.74 | 28.71 | 12.56 |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT:
 FORM:
 SPECIMEN TYPE: CT
 ORIENTATION: C-R
 FREQUENCY: 20.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.280 - 0.299"
 SPECIMEN WIDTH: 2.500"
 REFERENCES PW003

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TI-6AL-
4V

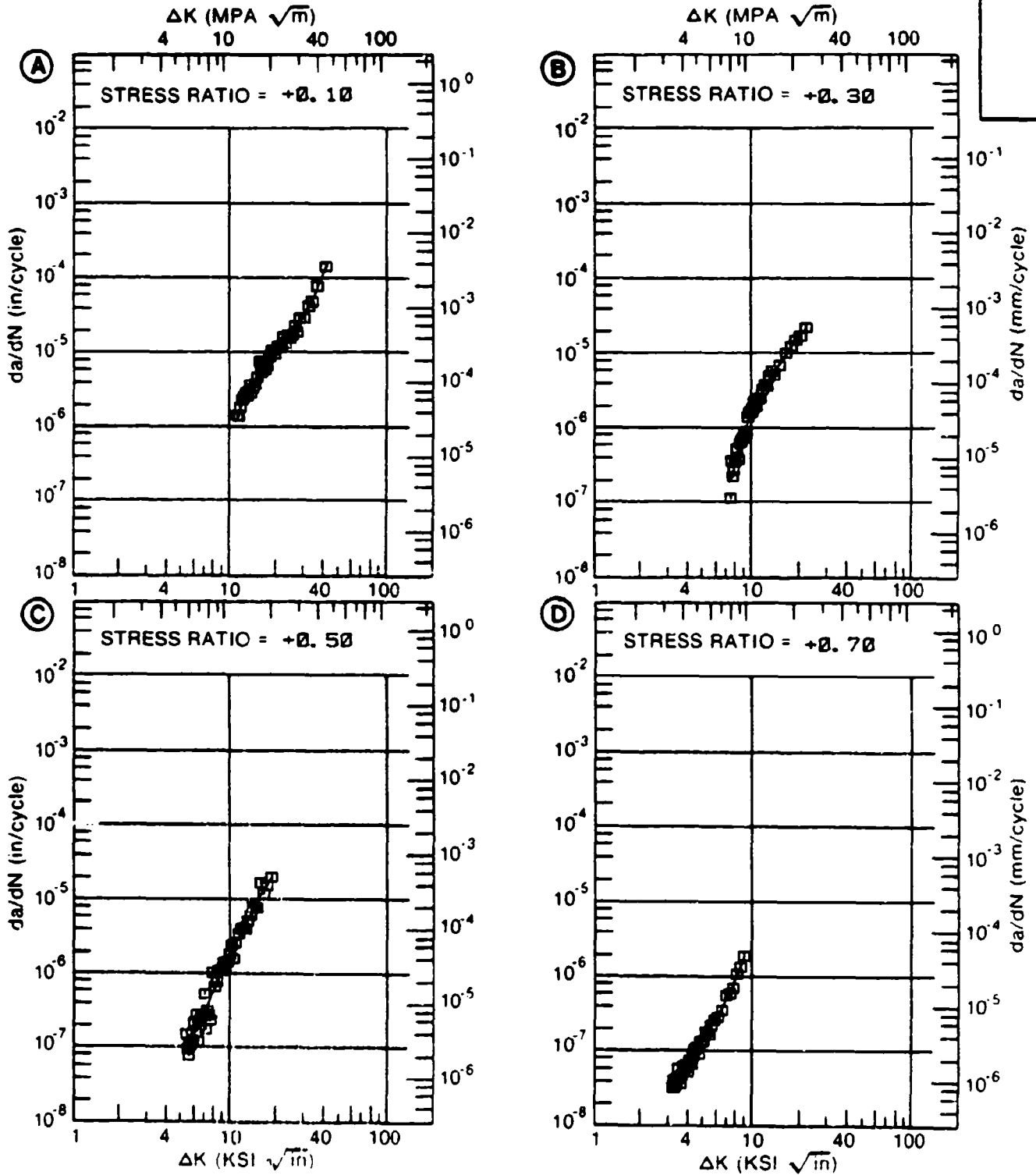


Figure 4.11.3.2

TABLE 4.11.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.3 INDICATING EFFECT

OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION:

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|-------|----------|---|
| | | A | B | C | D |
| | | E= R. T. | | E=+ 300F | |
| | | LAB AIR | | AIR | |
| DELTA K MIN | A: | 8.55 | .799 | | |
| | B: | 8.26 | | .885 | |
| | C: | | | | |
| | D: | | | | |
| | | 9.00 | .849 | .976 | |
| | 10.00 | 1.13 | 1.26 | | |
| | 13.00 | 4.02 | 3.60 | | |
| | 16.00 | 12.1 | 9.07 | | |
| DELTA K MAX | A: | 17.54 | 20.1 | | |
| | B: | 18.42 | | 15.0 | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.07 | 23.47 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM:
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: -1.00
 FREQUENCY: 0.16 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.297 - 0.301"
 SPECIMEN WIDTH: 2.500"
 REFERENCES: PW003

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 4V

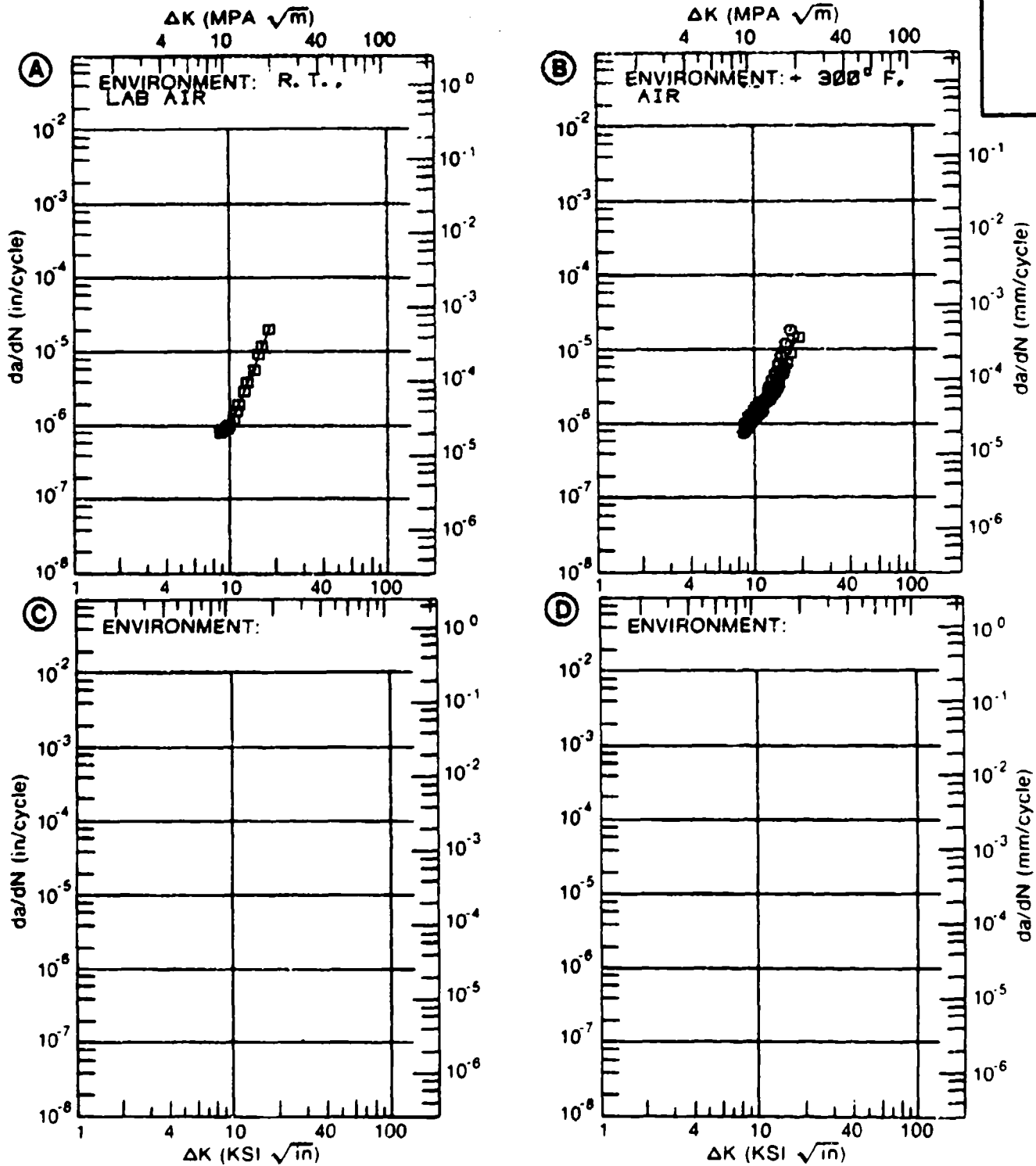


Figure 4.11.3.3

TABLE 4.11.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.4 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|-----------------|---|---|
| CONDITION: | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E=+ 300F AIR | | |
| DELTA K | A: 8.19 | .424 | | | |
| MIN | B: 8.12 | | .208 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .695 | .495 | | |
| | 10.00 | 1.14 | .971 | | |
| | 13.00 | 3.68 | 2.95 | | |
| | 16.00 | 11.3 | 6.42 | | |
| DELTA K | A: 16.57 | 14.2 | | | |
| MAX | B: 18.48 | | 13.6 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 17.73 | 27.56 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM:
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: -0.50
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 0.301 - 0.302"
 SPECIMEN WIDTH: 2.500"
 REFERENCES: PW003

TITAN.
ALLOY

TI-6AL-
4V

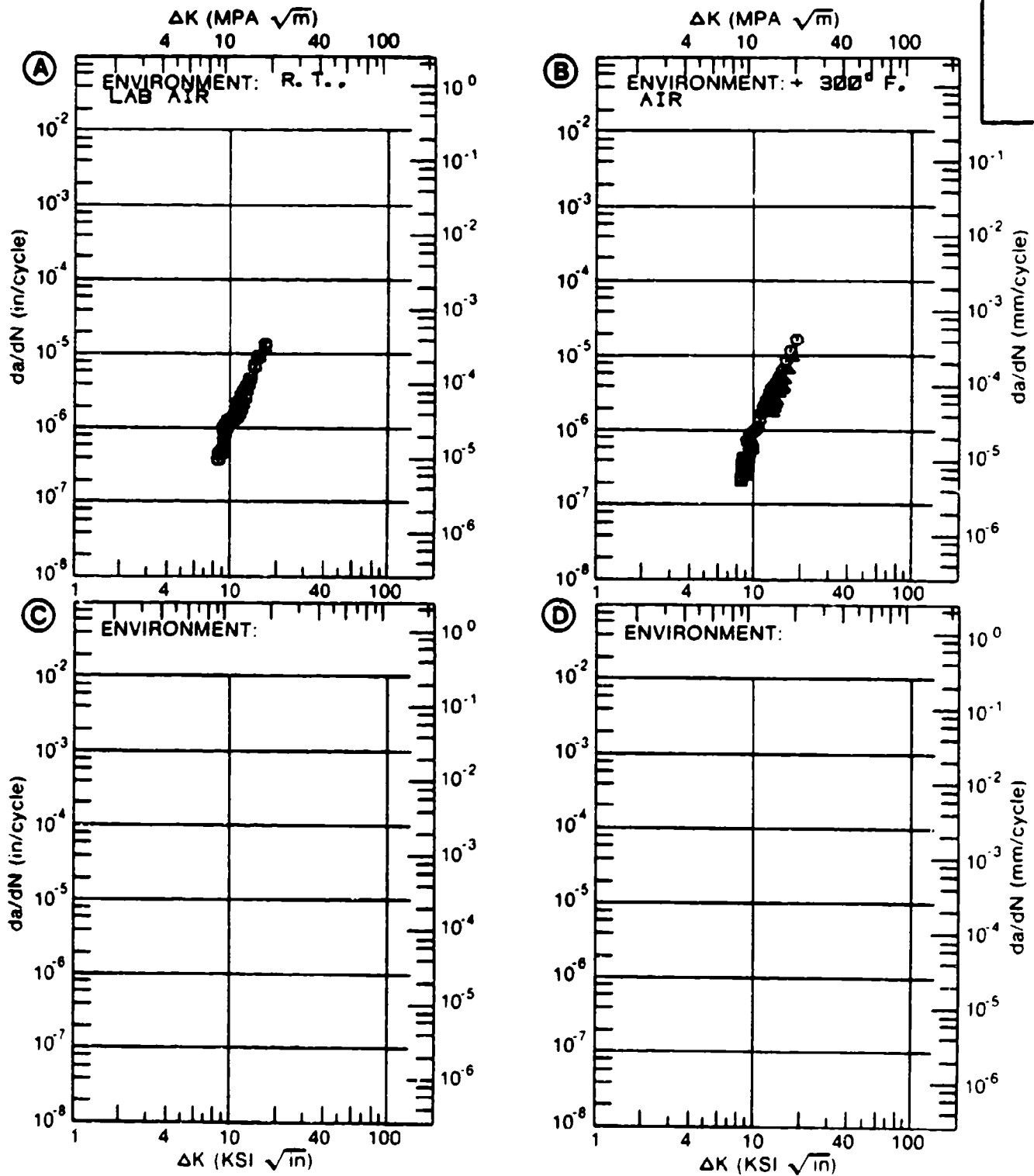


Figure 4.11.3.4

TABLE 4.11.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.5 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: ANNEALED
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K | A: 9.04 | .135 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .270 | | | |
| | 13.00 | 1.30 | | | |
| | 16.00 | 3.67 | | | |
| | 20.00 | 9.49 | | | |
| | 25.00 | 21.3 | | | |
| | 30.00 | 38.2 | | | |
| | 35.00 | 60.1 | | | |
| | 40.00 | 87.2 | | | |
| DELTA K | A: 44.93 | 120. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 24.21
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8 1
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: ANNEALED
 FORM: 8.00" TH BILLET
 SPECIMEN TYPE: WOL
 ORIENTATION: L-T
 FREQUENCY: 10.00- 20.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 123.0 KSI
 ULT. STRENGTH: 135.0 KSI
 SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: MA003

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TI-6AL-
4V

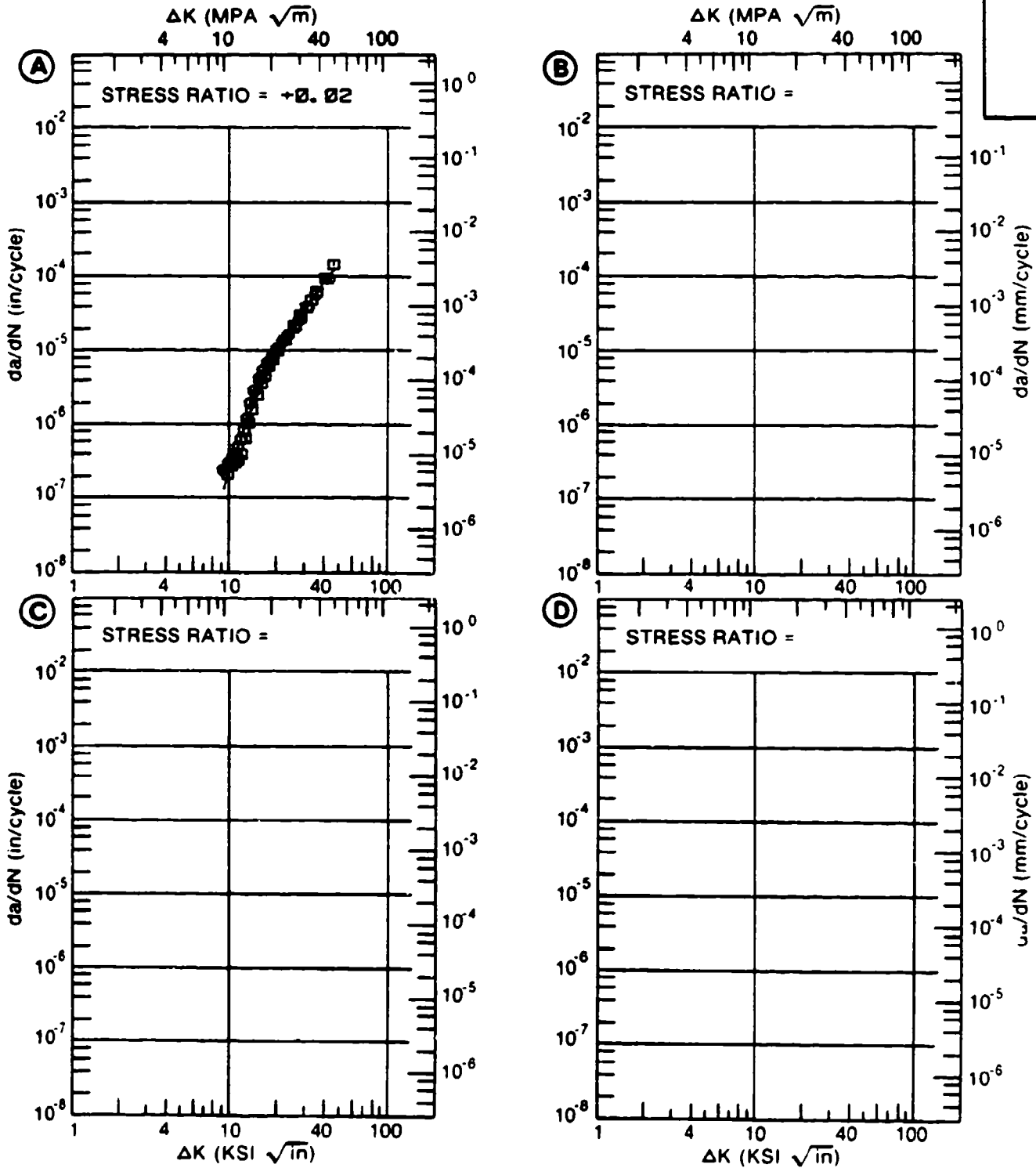


Figure 4.11.3.5

TABLE 4.11.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.6 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: ANNEALED AT 1375F, 3HRS, AC
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K | A: 8.52 | .0853 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .131 | | | |
| | 10.00 | .283 | | | |
| | 13.00 | 1.41 | | | |
| | 16.00 | 3.88 | | | |
| | 20.00 | 9.70 | | | |
| | 25.00 | 21.7 | | | |
| | 30.00 | 40.8 | | | |
| | 35.00 | 70.2 | | | |
| | 40.00 | 116. | | | |
| DELTA K | A: 42.37 | 145. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 25.31 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 2 | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED AT 1375F, 3HRS, AC

FORM: 2.75" TH PLATE

SPECIMEN TYPE: WOL

ORIENTATION: L-T

FREQUENCY: 10.00- 20.00 HZ

ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 129.0 KSI

ULT. STRENGTH: 139.0 KSI

SPECIMEN THK: 1.250"

SPECIMEN WIDTH: 5.000"

REFERENCES MA003

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4V

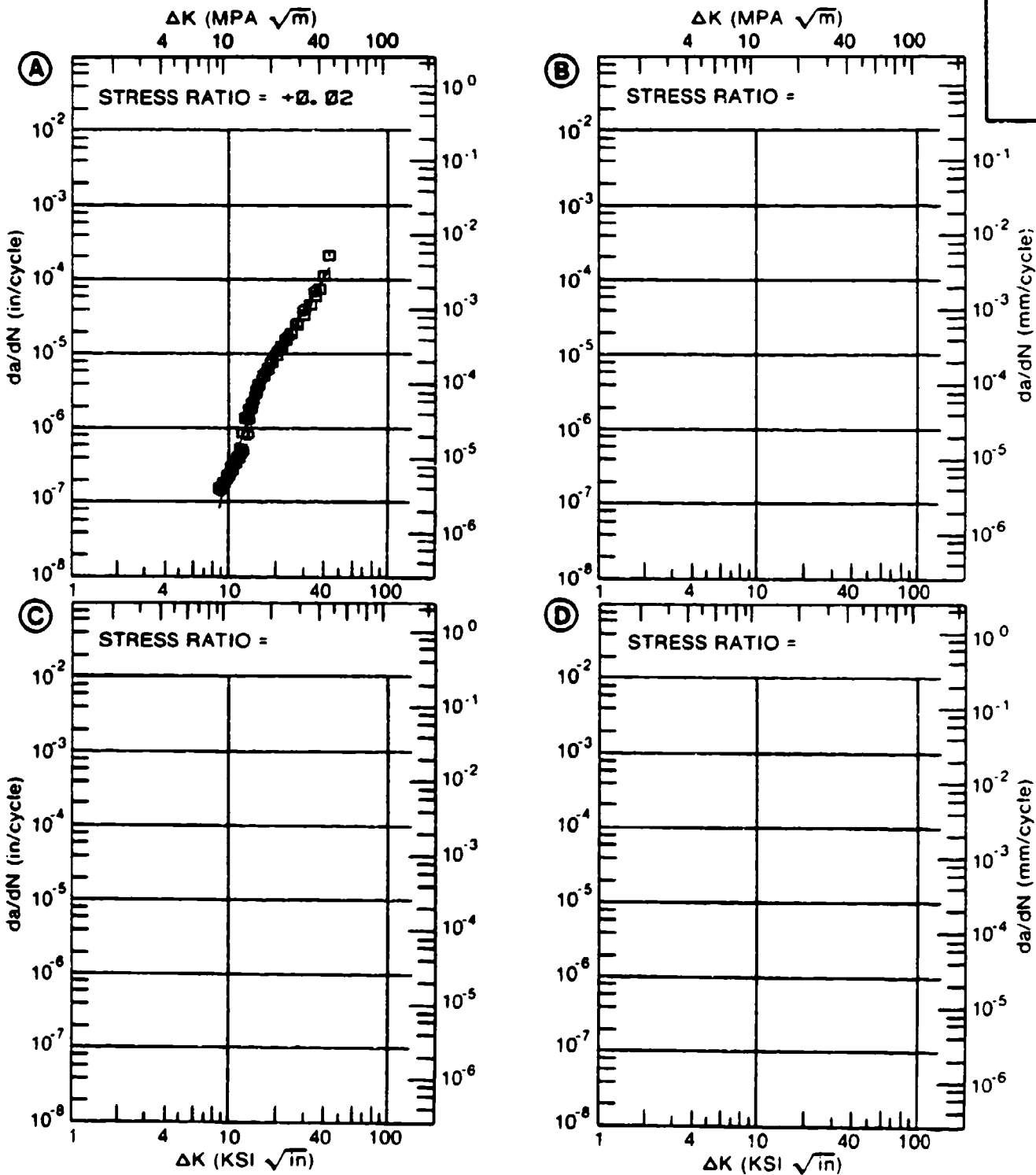


Figure 4.11.3.6

TABLE 4.11.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.7 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|----------|---------------------------|---|---|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: 5.13 | 1.45 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | 1.91 | | | |
| | 7.00 | 2.47 | | | |
| | 8.00 | 3.10 | | | |
| | 9.00 | 3.82 | | | |
| | 10.00 | 4.66 | | | |
| | 13.00 | 8.43 | | | |
| | 16.00 | 15.4 | | | |
| DELTA K MAX | A: 18.19 | 24.2 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.35 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CT
 ORIENTATION:
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.050"
 SPECIMEN WIDTH: 3.940"
 REFERENCES: NL001

| |
|-----------------|
| TITAN. ALLOY |
| TI-6AL- 4V |
| |

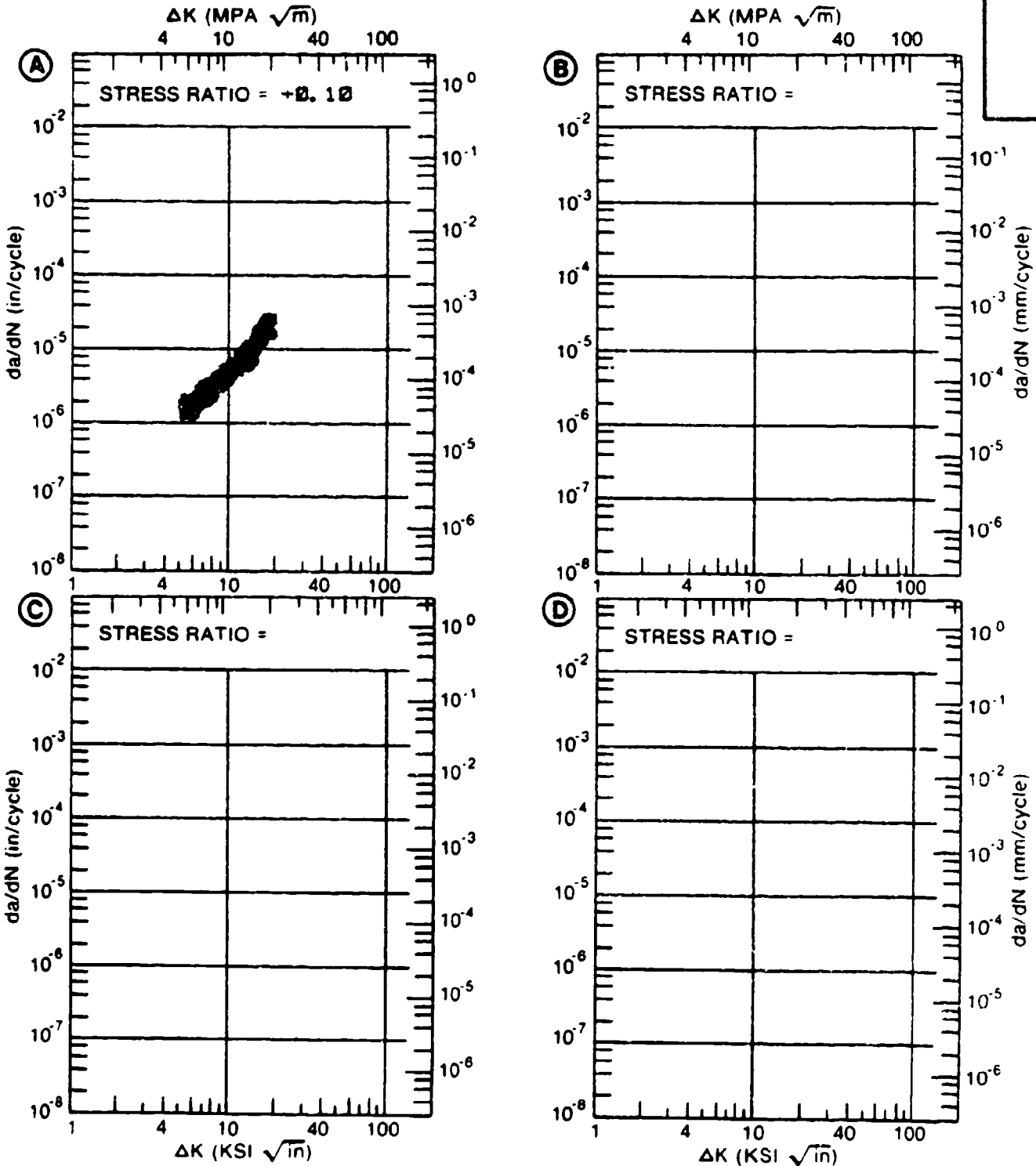


Figure 4.11.3.7

TABLE 4.11.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.8 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|----------|---------------------------------------|---------|---------|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | R=+0.70 | |
| DELTA K A: | 9.98 | 1.84 | | | |
| DELTA K B: | 17.87 | | 10.4 | | |
| MIN C: | 9.03 | | | 2.34 | |
| D: | | | | | |
| | 10.00 | 1.86 | | 3.90 | |
| | 13.00 | 4.87 | | 9.31 | |
| | 16.00 | 8.71 | | 14.6 | |
| | 20.00 | 14.5 | 15.1 | 24.4 | |
| | 25.00 | 22.7 | 26.9 | 53.8 | |
| | 30.00 | 32.7 | 40.7 | 150. | |
| | 35.00 | 45.7 | 59.7 | | |
| | 40.00 | 63.2 | 89.2 | | |
| | 50.00 | 121. | 224. | | |
| | 60.00 | 238. | | | |
| | 70.00 | 476. | | | |
| DELTA K A: | 71.28 | 521. | | | |
| DELTA K B: | 59.74 | | 643. | | |
| MAX C: | 33.00 | | | 311. | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 8.97 | 11.51 | 15.91 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 2 | 1 | 1 | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION:
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.050"
 SPECIMEN WIDTH: 3.150"
 REFERENCES: NL001

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 TI-6AL-
 4V

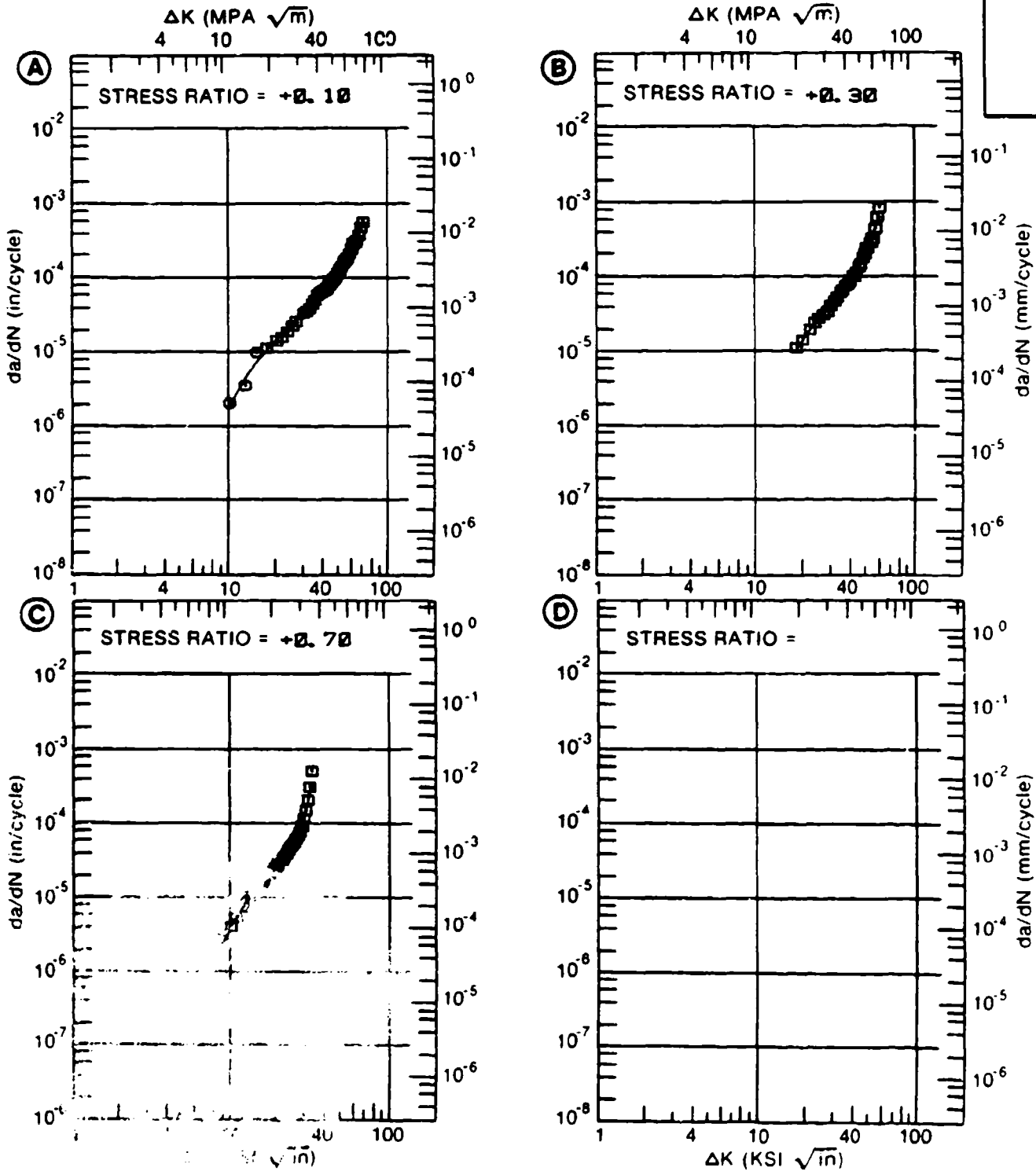


Figure 4.11.3.8

TABLE 4.11.3.9

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.9 INDICATING EFFECT
OF FREQUENCY

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BA
ENVIRONMENT: R. T. , 3.5% NaCl

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | F(HZ)= 10.00 | | | |
| DELTA K | A: 9.65 | .46 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .625 | | | |
| | 13.00 | 3.62 | | | |
| | 16.00 | 9.15 | | | |
| | 20.00 | 17.6 | | | |
| | 25.00 | 26.5 | | | |
| | 30.00 | 33.4 | | | |
| DELTA K | A: 34.71 | 39.3 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 4.39
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 0.63" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 STRESS RATIO: +0.10
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH: 124.5 KSI
 ULT. STRENGTH: 136.4 KSI
 SPECIMEN THK: 0.672"
 SPECIMEN WIDTH: 1.500"
 REFERENCES: 90981

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TI-6AL-
4V

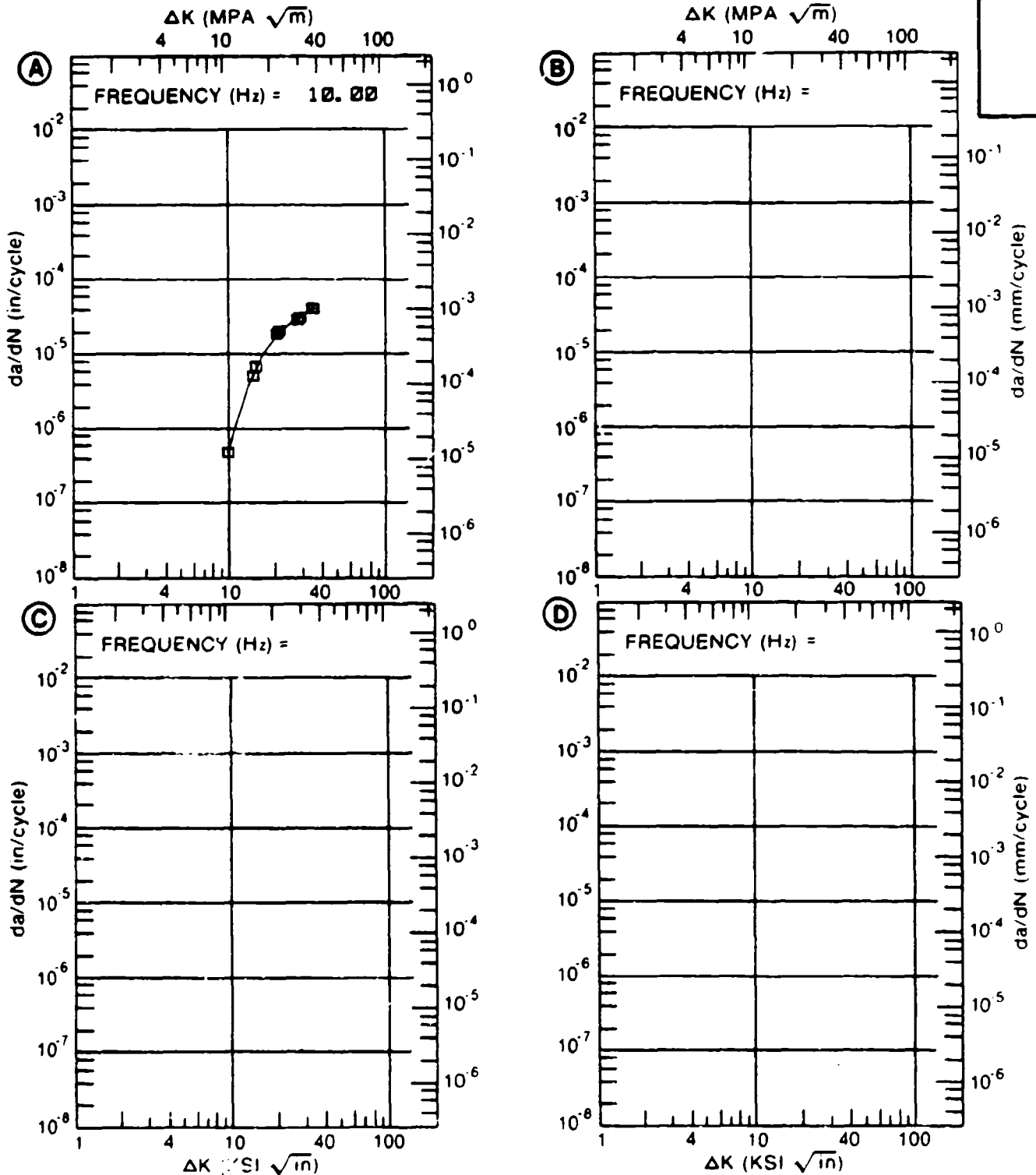


Figure 4.11.3.9

TABLE 4.11.3.10

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.10 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: BA

TI-6AL-4V

DELTA K
(KSI*IN**1/2)

DA/DN (10**⁻⁶ IN. /CYCLE)

A

B

C

D

E= R. T.
DRY AIR

E= R. T.
3. 5%NaCl

DELTA K A:
MIN B: 8. 24
C:
D:

. 237

9. 00

. 574

10. 00

. 985

13. 00

2. 65

16. 00

0. 65

20. 00

13. 8

25. 00

22. 6

30. 00

31. 4

35. 00

41. 7

40. 00

59. 9

50. 00

109.

60. 00

245.

DELTA K A:
MAX B: 68. 19
C:
D:

517.

ROOT MEAN SQUARE
PERCENT ERROR

0. 00

18. 95

LIFE 0. 0-0. 5
PREDICTION 0. 5-0. 8
RATIO 0. 8-1. 25
SUMMARY 1. 25-2. 0
(NP/NA) >2. 0

1

CONDITION/HT: BA
 FORM: 0.83" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 124.5 KSI
 ULT. STRENGTH: 136.4 KSI
 SPECIMEN THK: 0.660"
 SPECIMEN WIDTH: 2.550- 2.554"
 REFERENCES: 90981

| |
|-----------------|
| TITAN. ALLOY |
| TI-BAL- 4V |
| |

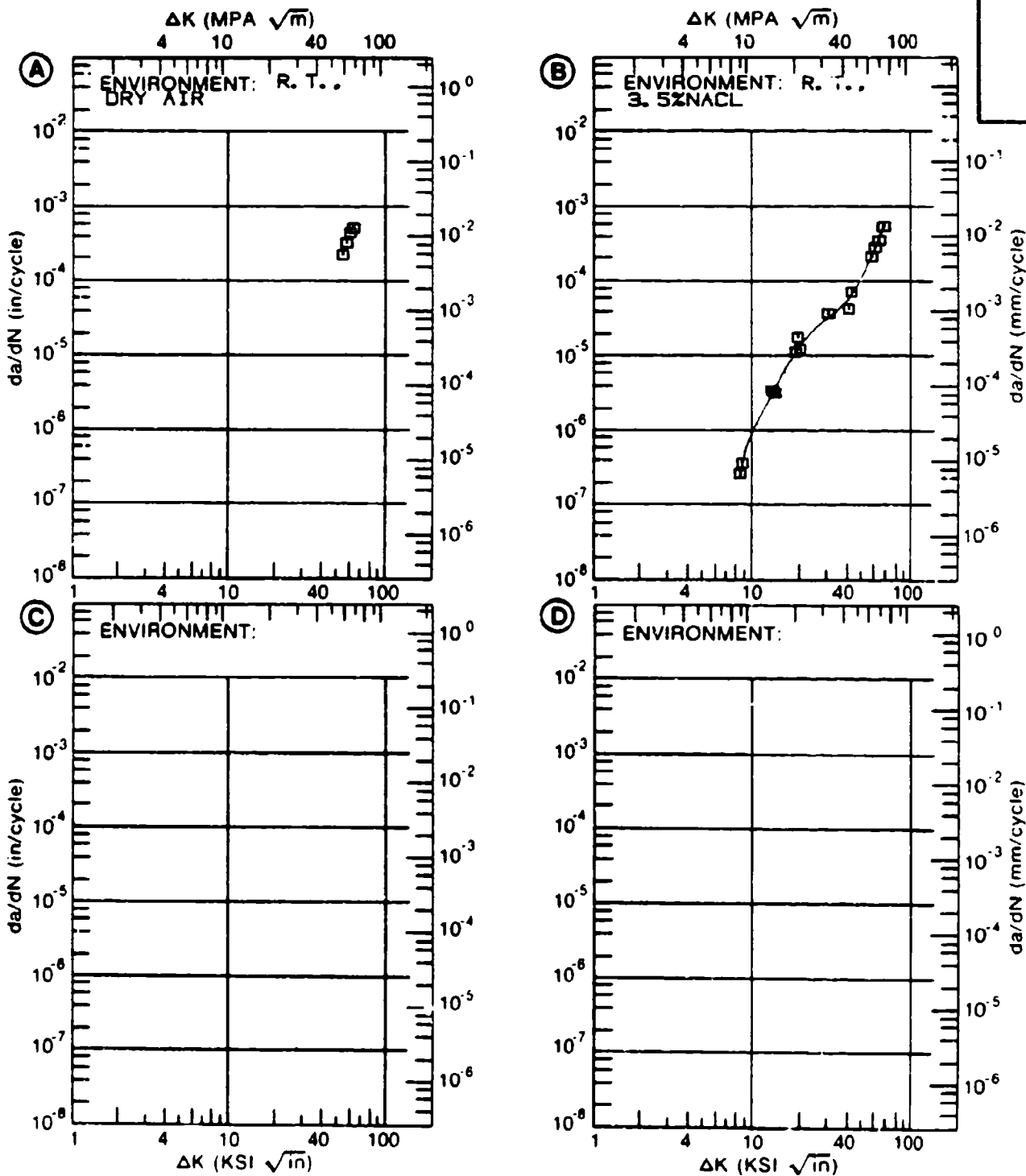


Figure 4.11.3.10

TABLE 4.11.3.11

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.11 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BA

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---|---|---|
| | A | B | C | D |
| | E= R. T. | | | |
| | S. T. W. | | | |
| DELTA K A: 15.85 | 11.7 | | | |
| MIN B: | | | | |
| C: | | | | |
| D: | | | | |
| 16.00 | 11.9 | | | |
| 20.00 | 18.6 | | | |
| 25.00 | 28.3 | | | |
| 30.00 | 39.2 | | | |
| 35.00 | 51.3 | | | |
| 40.00 | 64.5 | | | |
| 50.00 | 94.3 | | | |
| 60.00 | 129. | | | |
| 70.00 | 168. | | | |
| 80.00 | 213. | | | |
| DELTA K A: 87.57 | 252. | | | |
| MAX B: | | | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 10.42
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 0.63" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 124.5 KSI
 ULT. STRENGTH: 136.4 KSI
 SPECIMEN THK: 0.660"
 SPECIMEN WIDTH: 2.554"
 REFERENCES: 90981

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 ALLOY
 TI-6AL-
 4V

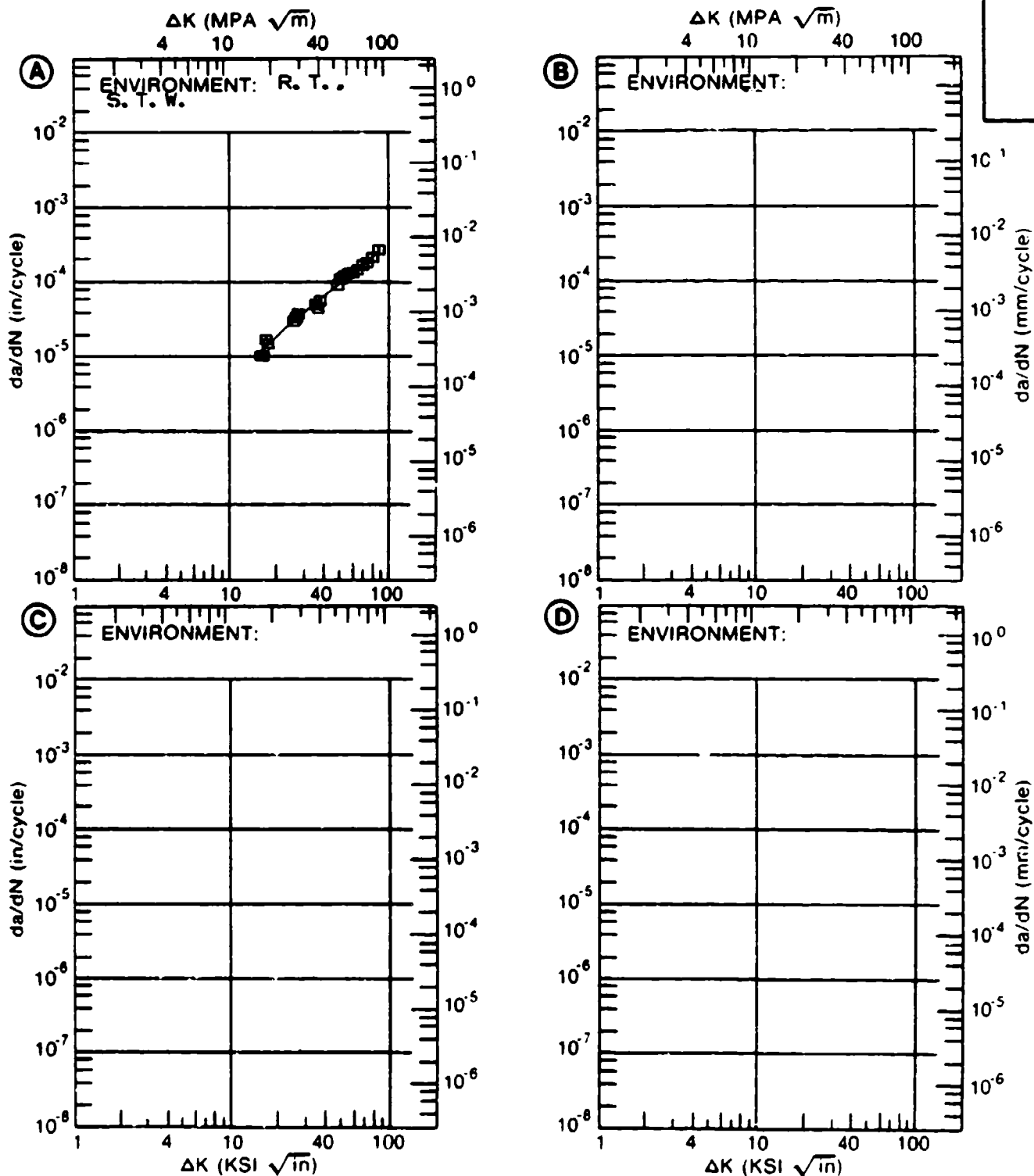


Figure 4.11.3.11

TABLE 4.11.3.12

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.12 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|---------------------------|-------|----------|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | E= R. T. | |
| | | 3.5%NaCl | | S. T. W. | |
| DELTA K MIN | A: 10.21 | .250 | | | |
| | B: 18.51 | | 30.5 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 5.35 | | | |
| | 16.00 | 16.0 | | | |
| | 20.00 | 38.5 | 35.3 | | |
| | 25.00 | 66.4 | 73.3 | | |
| | 30.00 | 83.1 | 95.4 | | |
| | 35.00 | 100. | 103. | | |
| | 40.00 | 136. | 112. | | |
| | 50.00 | 281. | 192. | | |
| | 60.00 | | 489. | | |
| DELTA K MAX | A: 57.34 | 342. | | | |
| | B: 69.64 | | 1087. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 17.39 | 15.35 | | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | 1 | | |

CONDITION/HT: BA
 FORM: 0.63" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 124.5 KSI
 ULT. STRENGTH: 136.4 KSI
 SPECIMEN THK: 0.660"
 SPECIMEN WIDTH: 2.550- 2.554"
 REFERENCES: 90981

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4V

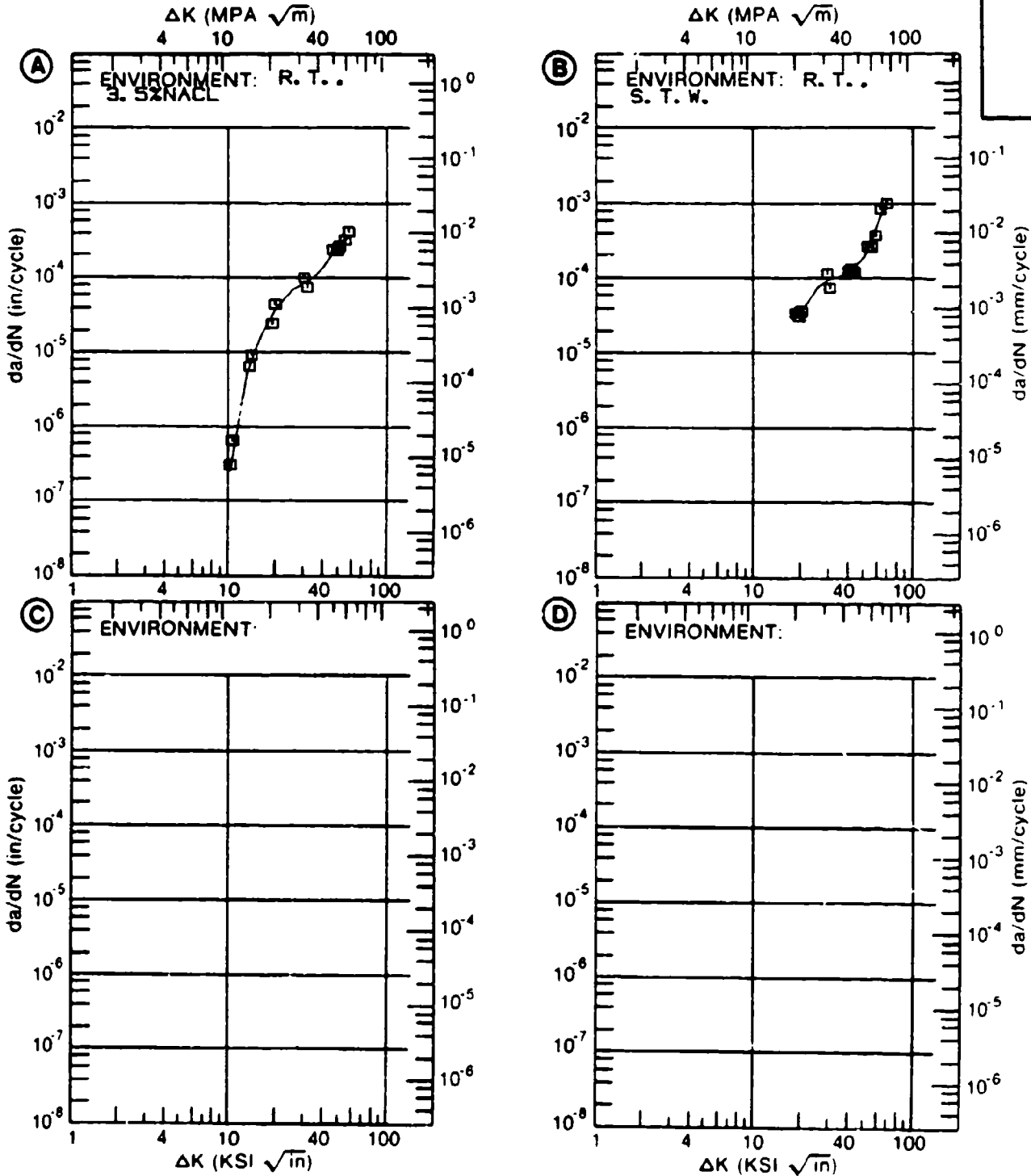


Figure 4.11.3.12

TABLE 4.11.3.13

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.13 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: BA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. S. T. W. | | | |
| DELTA K | A: 9.81 | .55 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .581 | | | |
| | 13.00 | 1.31 | | | |
| | 16.00 | 2.73 | | | |
| | 20.00 | 6.43 | | | |
| | 25.00 | 16.2 | | | |
| | 30.00 | 36.1 | | | |
| | 35.00 | 72.9 | | | |
| | 40.00 | 136. | | | |
| | 50.00 | 400. | | | |
| | 60.00 | 987. | | | |
| DELTA K | A: 69.91 | 2127. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 43.57
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 0.83" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH: 124.5 KSI
 ULT. STRENGTH: 136.4 KSI
 SPECIMEN THK: 0.860"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 90981

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4V

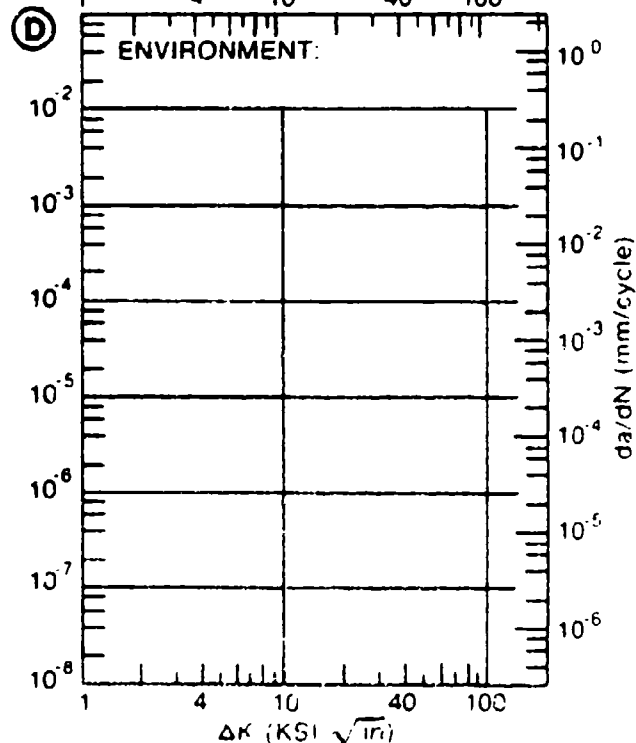
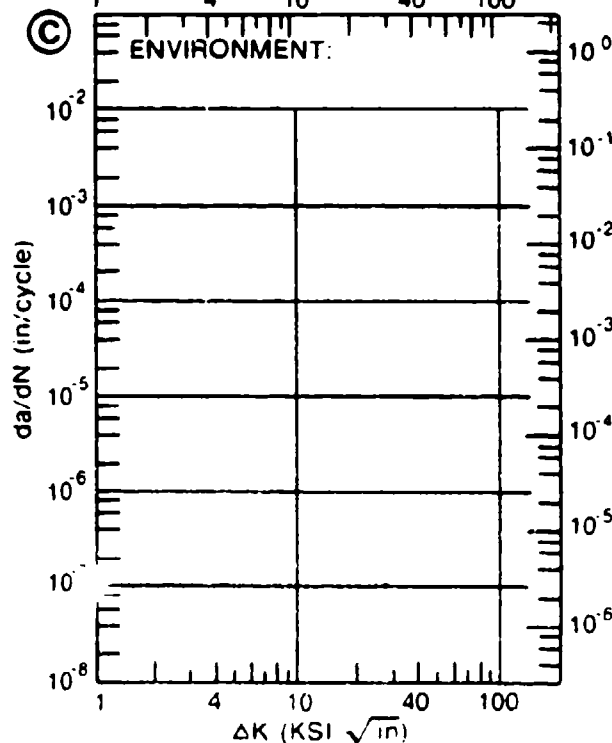
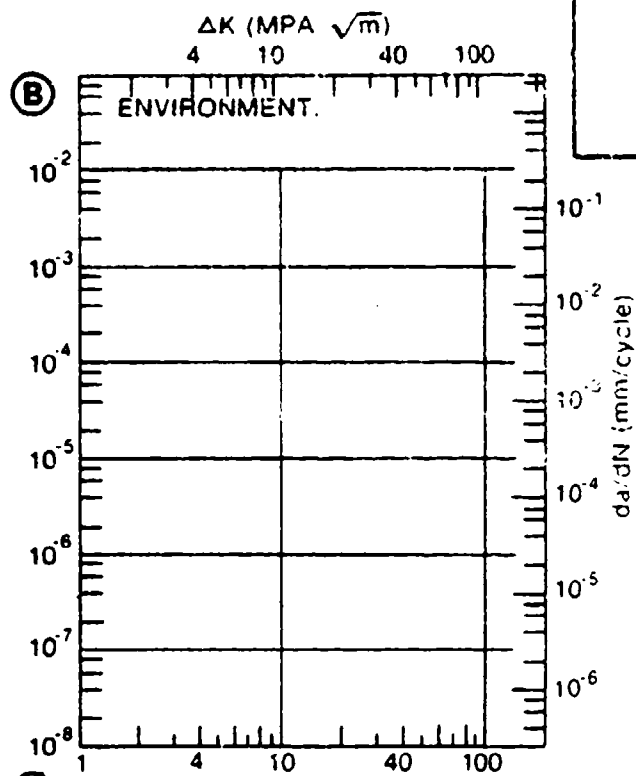
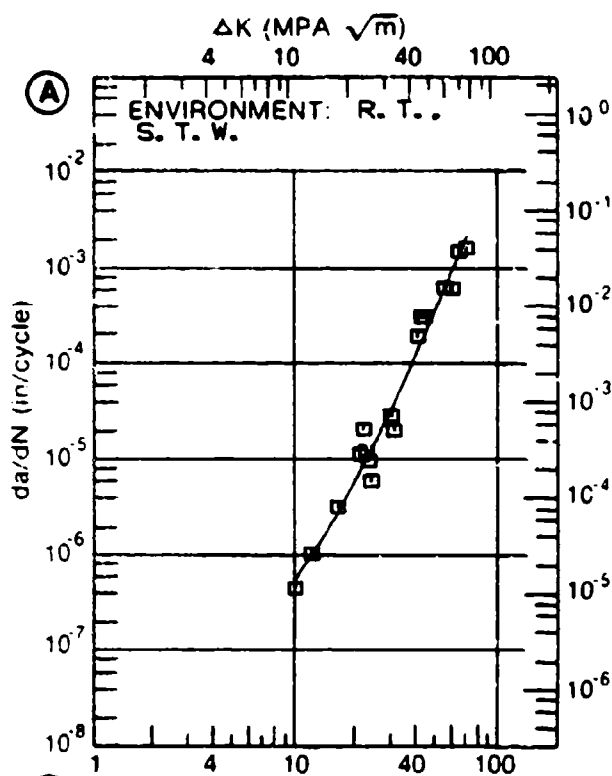


Figure 4.11.3.13

TABLE 4.11.3.14

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.14 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|------------|---------------------------------------|---------|---|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , DRY AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.30 | | |
| DELTA K | A: 7.64 : | .108 | | | |
| MIN | B: 9.89 : | | .284 | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 : | .113 | | | |
| | 9.00 : | .150 | | | |
| | 10.00 : | .227 | .302 | | |
| | 13.00 : | .937 | 1.79 | | |
| | 16.00 : | 3.17 | 4.90 | | |
| | 20.00 : | 9.10 | 9.75 | | |
| | 25.00 : | 19.6 | 18.5 | | |
| | 30.00 : | 33.0 | 32.2 | | |
| | 35.00 : | 51.5 | 52.4 | | |
| | 40.00 : | 78.0 | | | |
| DELTA K | A: 45.52 : | 122. | | | |
| MAX | B: 39.92 : | | 80.2 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.21 | 10.73 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | 1 | | |
| SUMMARY | 1.25-2.0 | 1 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 0.78" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.00 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH: 116.3 KSI
 ULT. STRENGTH: 125.7 KSI
 SPECIMEN THK: 0.747- 0.748"
 SPECIMEN WIDTH: 4.995- 5.008"
 REFERENCES 98575

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4V

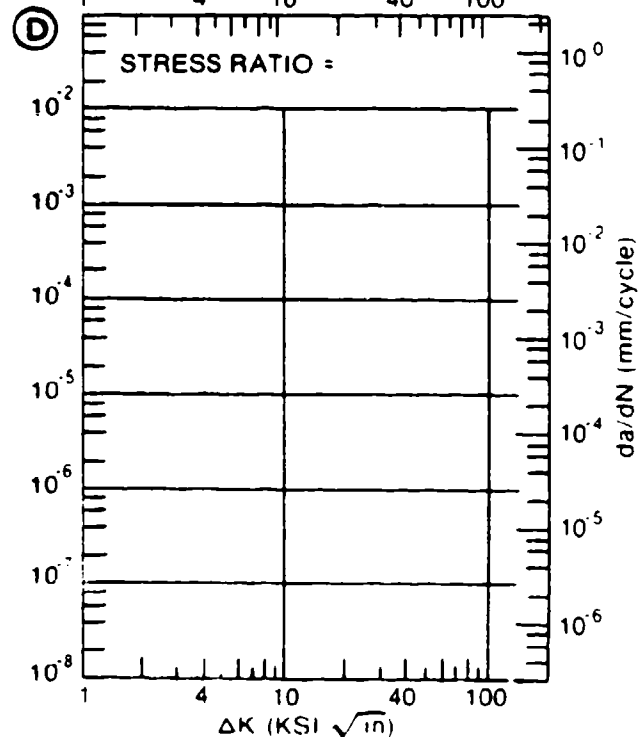
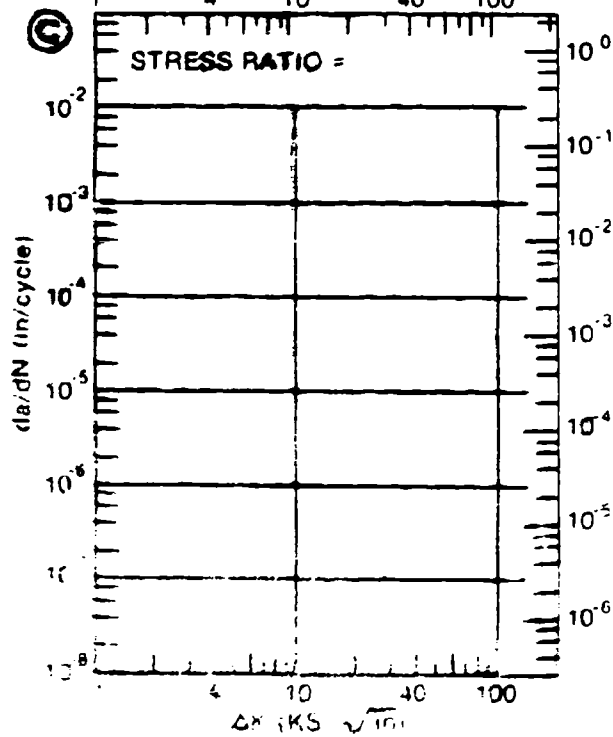
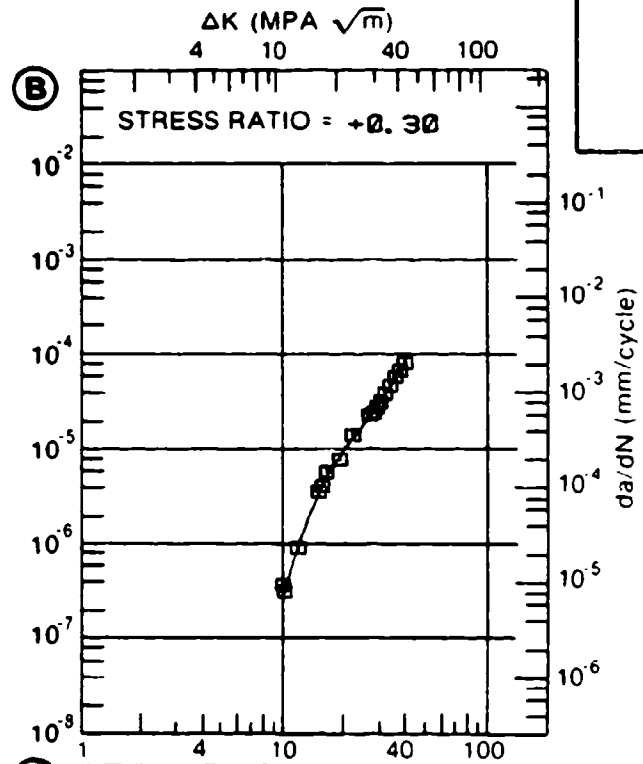
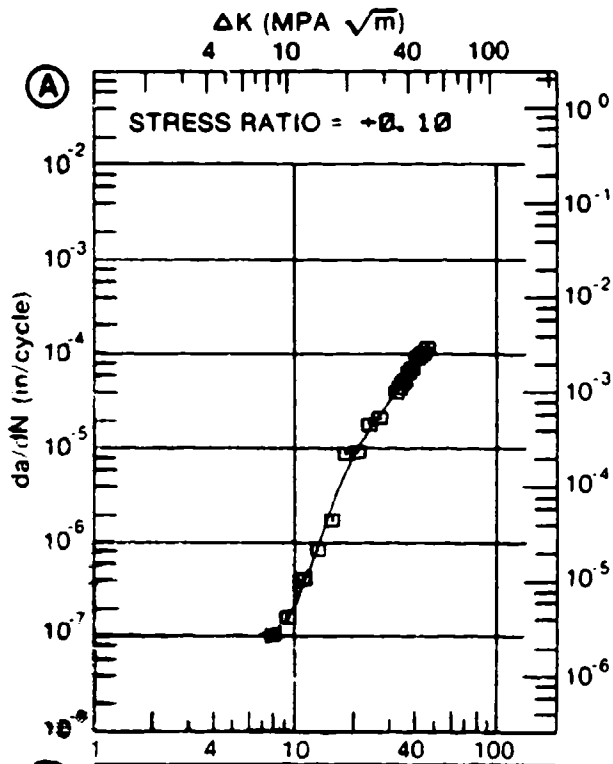


Figure 4.11.3.14

TABLE 4.11.3.15

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.15 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|----------|---------------------------|---------|---|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , S. T. W. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K A: | 11.43 | .30 | | | |
| DELTA K B: | 24.08 | | 53.3 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 13.00 | .730 | | | |
| | 16.00 | 3.08 | | | |
| | 20.00 | 11.1 | | | |
| | 25.00 | 27.6 | 61.5 | | |
| | 30.00 | 48.0 | 86.0 | | |
| | 35.00 | 70.5 | 119. | | |
| | 40.00 | 95.9 | | | |
| | 50.00 | 163. | | | |
| DELTA K A: | 59.09 | 264. | | | |
| DELTA K B: | 36.06 | | 134. | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 16.76 | 3.81 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | 1 | | |
| SUMMARY | 1.25-2.0 | 2 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 0.75- 0.76" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 116.3 KSI
 ULT. STRENGTH: 125.7 KSI
 SPECIMEN THK: 0.746- 0.751"
 SPECIMEN WIDTH: 4.986- 5.019"
 REFERENCES: 89575

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 4V

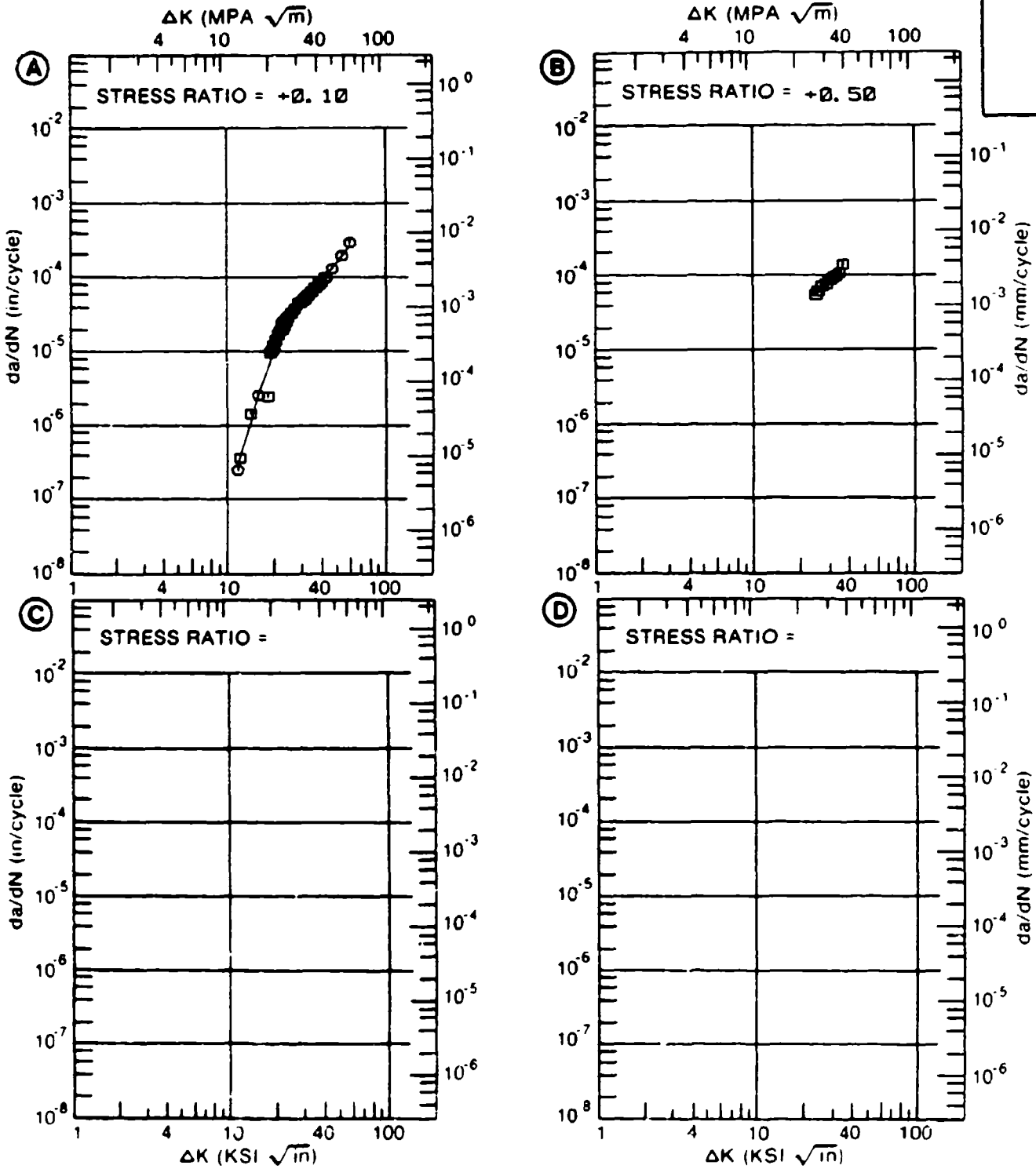


Figure 4.11.3.15

TABLE 4.11.3.16

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.16 INDICATING EFFECT
OF FREQUENCY

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|--------------------------|---|---|---|
| | A | B | C | D |
| | F(HZ)= 0.10 | | | |
| DELTA K A: | | | | |
| MIN B: | | | | |
| C: | | | | |
| D: | | | | |
| 200.00 | | | | |
| DELTA K A: | | | | |
| MAX B: | | | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 0.00
PERCENT ERROR

| | |
|------------|----------|
| LIFE | 0.0-0.5 |
| PREDICTION | 0.5-0.8 |
| RATIO | 0.8-1.25 |
| SUMMARY | 1.25-2.0 |
| (NP/NA) | >2.0 |

CONDITION/HT: BA
 FORM: 0.75" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.50
 ENVIRONMENT: R. T. . S. T. W.

YIELD STRENGTH: 116.3 KSI
 ULT. STRENGTH: 125.7 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 5.008"
 REFERENCES: 88575

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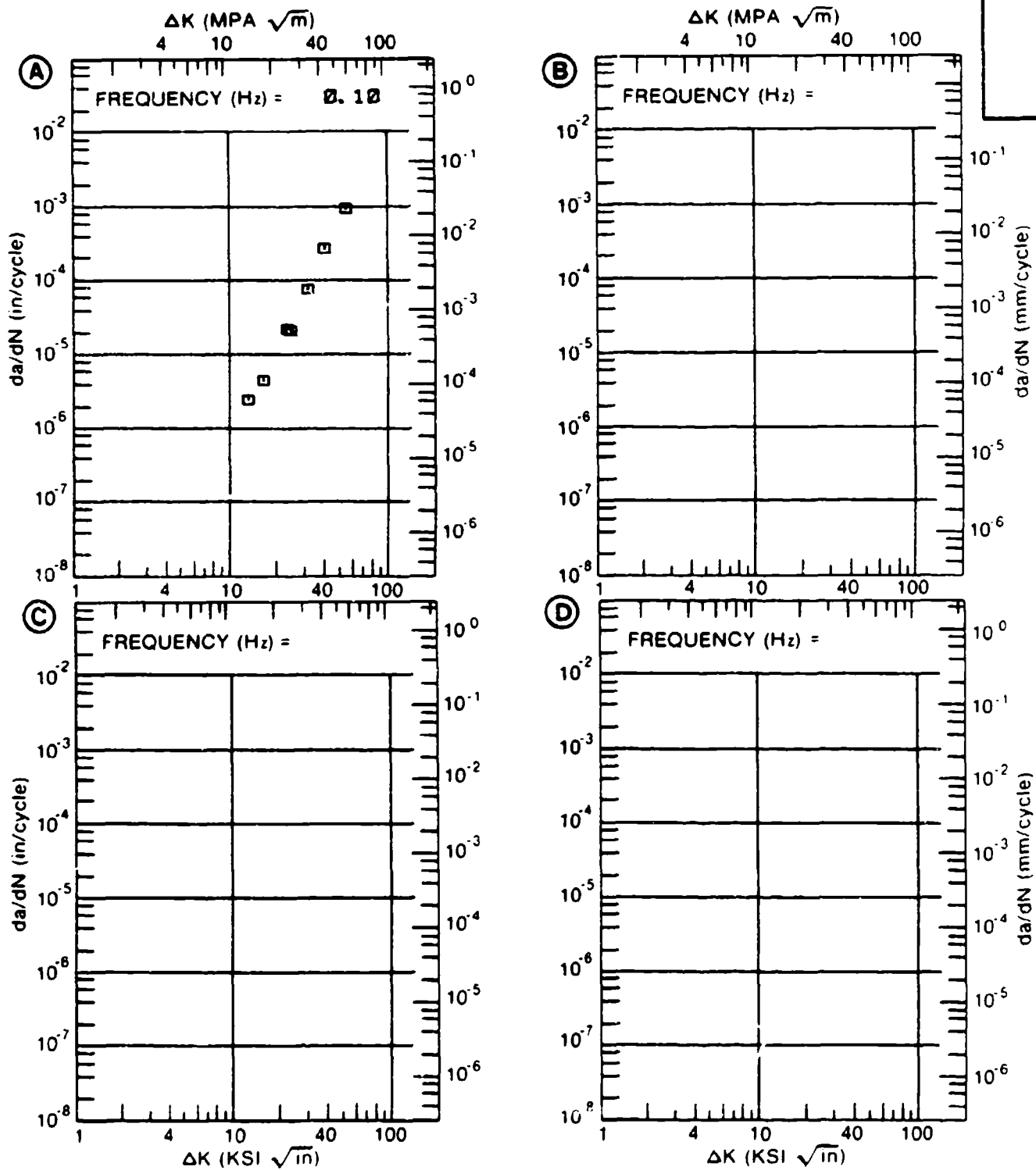


Figure 4.11.3.16

TABLE 4.11.3.17

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.17 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|----------------------------------|------------|---------------------------|----------|---|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , DIST. WATER | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0. 10 | R=+0. 50 | | |
| DELTA K A: | 26. 53 | 15. 5 | | | |
| MIN B: | | | | | |
| C: | | | | | |
| D: | | | | | |
| | 30. 00 | 26. 2 | | | |
| | 35. 00 | 45. 2 | | | |
| | 40. 00 | 67. 8 | | | |
| | 50. 00 | 126. | | | |
| | 60. 00 | 218. | | | |
| DELTA K A: | 63. 96 | 271. | | | |
| MAX B: | | | | | |
| C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 3. 71 | 0. 00 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | | | | |
| SUMMARY | 1. 25-2. 0 | | | | |
| (NP/NA) | >2. 0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 FREQUENCY: 0.10 HZ
 ENVIRONMENT: R. T., DIST. WATER

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

TITAN.
ALLOY

TI-6AL-
4V

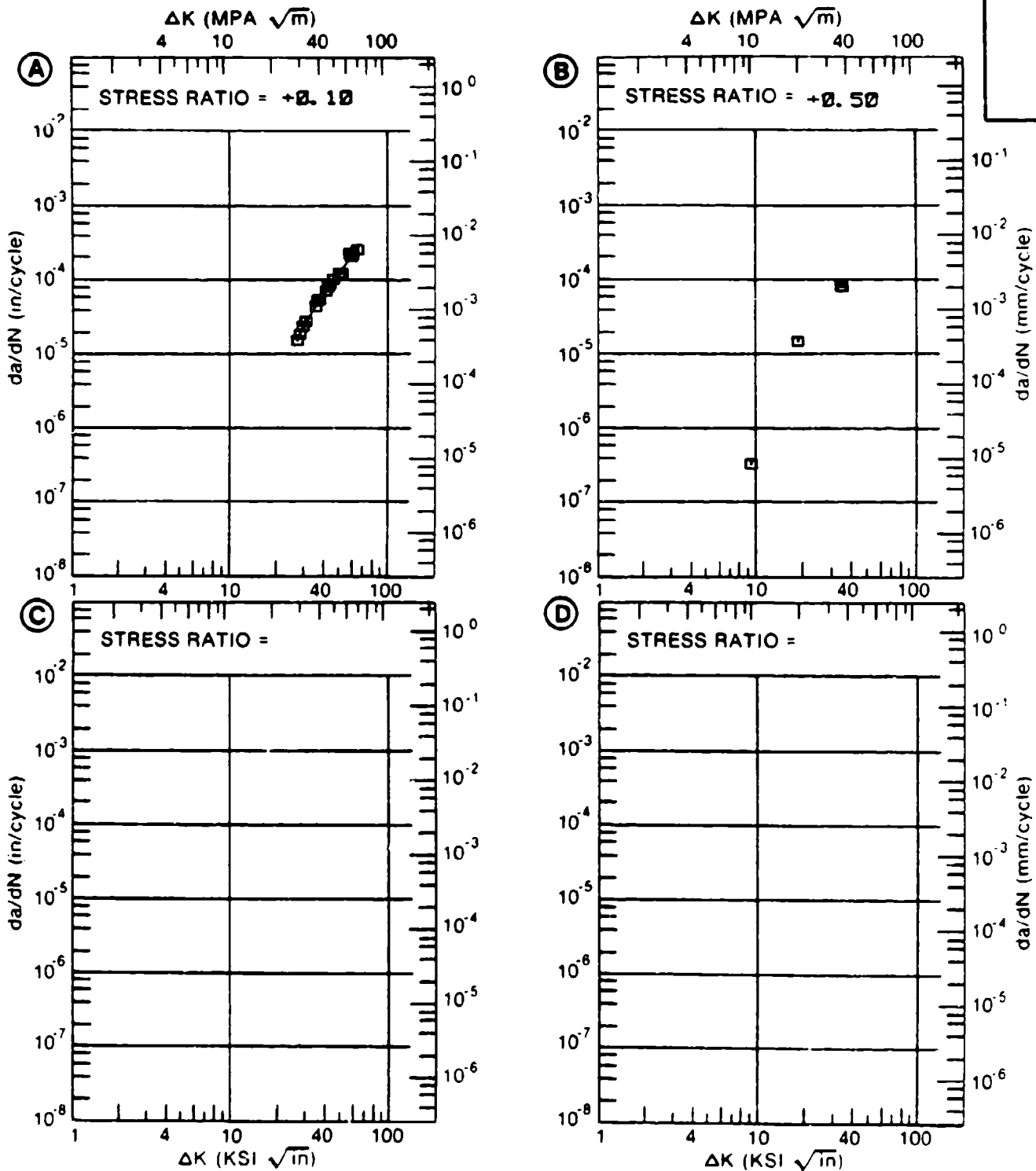


Figure 4.11.3.17

TABLE 4.11.3.18

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.18 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|------------|---------------------------------------|----------|----------|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , H. H. A. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0. 10 | R=+0. 30 | R=+0. 50 | |
| DELTA K A: | 12. 84 | . 965 | | | |
| MIN B: | 10. 82 | | . 451 | | |
| C: | 10. 92 | | | 1. 47 | |
| D: | | | | | |
| | 13. 00 | . 929 | 1. 15 | 1. 62 | |
| | 16. 00 | 1. 19 | 3. 13 | 3. 85 | |
| | 20. 00 | 4. 10 | 9. 31 | 12. 0 | |
| | 25. 00 | 12. 4 | 23. 5 | 27. 6 | |
| | 30. 00 | 25. 3 | 38. 6 | 44. 0 | |
| | 35. 00 | 41. 9 | 52. 8 | 78. 0 | |
| | 40. 00 | 62. 0 | 84. 8 | 182. | |
| | 50. 00 | 115. | | 1010. | |
| | 60. 00 | 208. | | | |
| DELTA K A: | 66. 20 | 454. | | | |
| MAX B: | 48. 80 | | 210. | | |
| C: | 50. 10 | | | 1013. | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 15. 43 | 11. 45 | 16. 49 | |
| PERCENT ERROR | | | | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | 1 | | 1 | |
| SUMMARY | 1. 25-2. 0 | | 1 | | |
| (NP/NA) | >2. 0 | | | | |

CONDITION/HT: BA
 FORM: 2.25" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 0.10 HZ
 ENVIRONMENT: R. T. . H. H. A.

YIELD STRENGTH: 117.0 KSI
 ULT. STRENGTH: 129.4 KSI
 SPECIMEN THK: 0.749- 0.753"
 SPECIMEN WIDTH: 5.009- 5.013"
 REFERENCES: G007

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ALLOY

TI-6AL-
4V

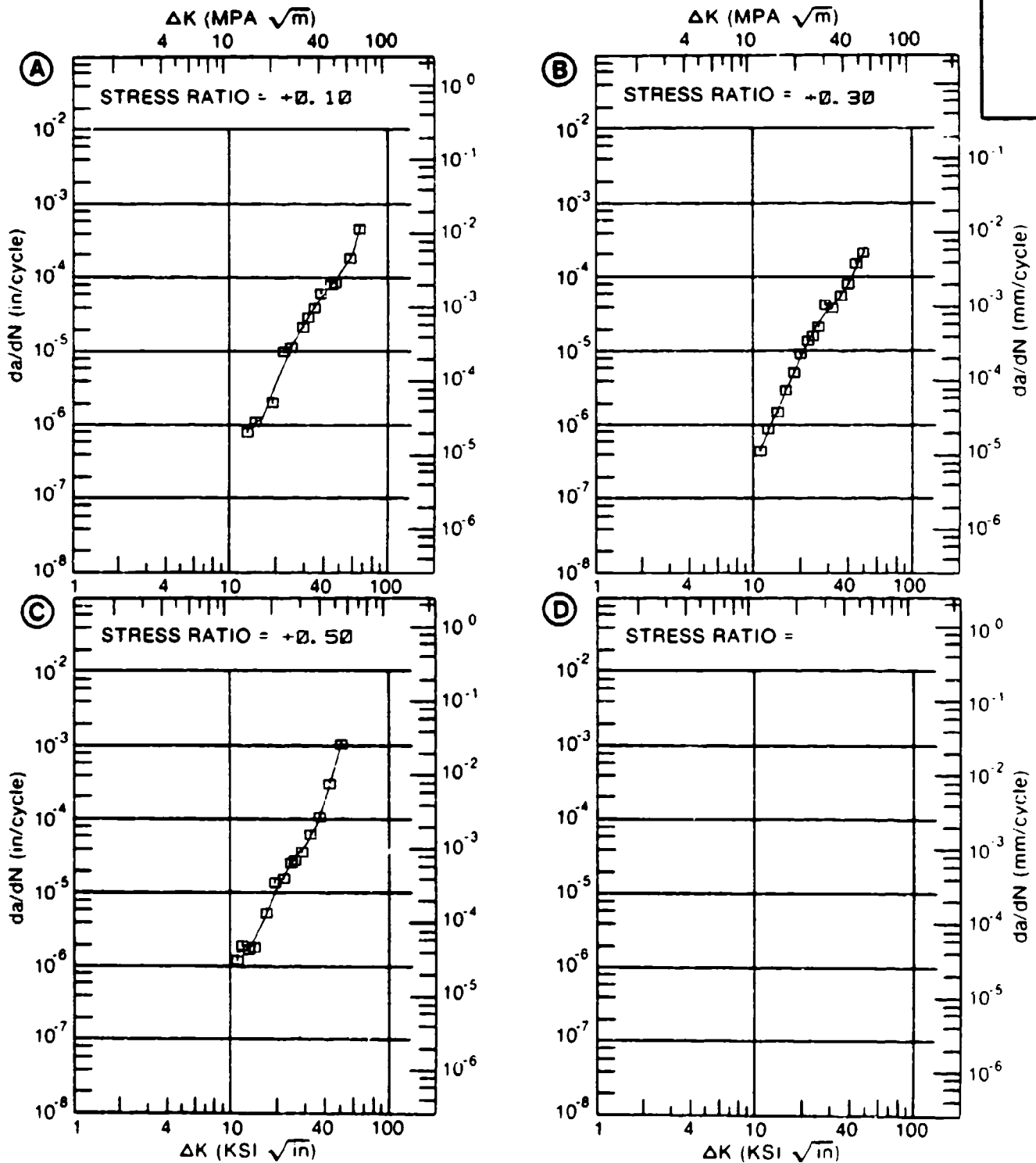


Figure 4.11.3.18

TABLE 4.11.3.19

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.19 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BA
ENVIRONMENT: R. T. , DRY AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|-------|--------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| A: | 9.56 | .04 | | | |
| DELTA K B: | 7.43 | | .40 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 8.00 | | .538 | | |
| | 9.00 | | .826 | | |
| | 10.00 | .0692 | 1.19 | | |
| | 13.00 | .482 | 2.85 | | |
| | 16.00 | 1.62 | 5.49 | | |
| | 20.00 | 5.42 | 10.9 | | |
| | 25.00 | 15.7 | 21.5 | | |
| | 30.00 | 32.2 | 38.1 | | |
| | 35.00 | 51.7 | 62.5 | | |
| | 40.00 | 69.3 | | | |
| | 50.00 | 85.6 | | | |
| A: | 50.68 | 85.7 | | | |
| DELTA K B: | 36.97 | | 74.9 | | |
| MAX C: | | | | | |
| D: | | | | | |

ROOT MEAN SQUARE 22.63 47.03
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0 1 1
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 2.79" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.00 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH: 116.3 KSI
 ULT. STRENGTH: 125.7 KSI
 SPECIMEN THK: 0.760- 0.762"
 SPECIMEN WIDTH: 4.993- 4.996"
 REFERENCES: 88575

TITAN.
 ALLOY

TI-6AL-
 4V

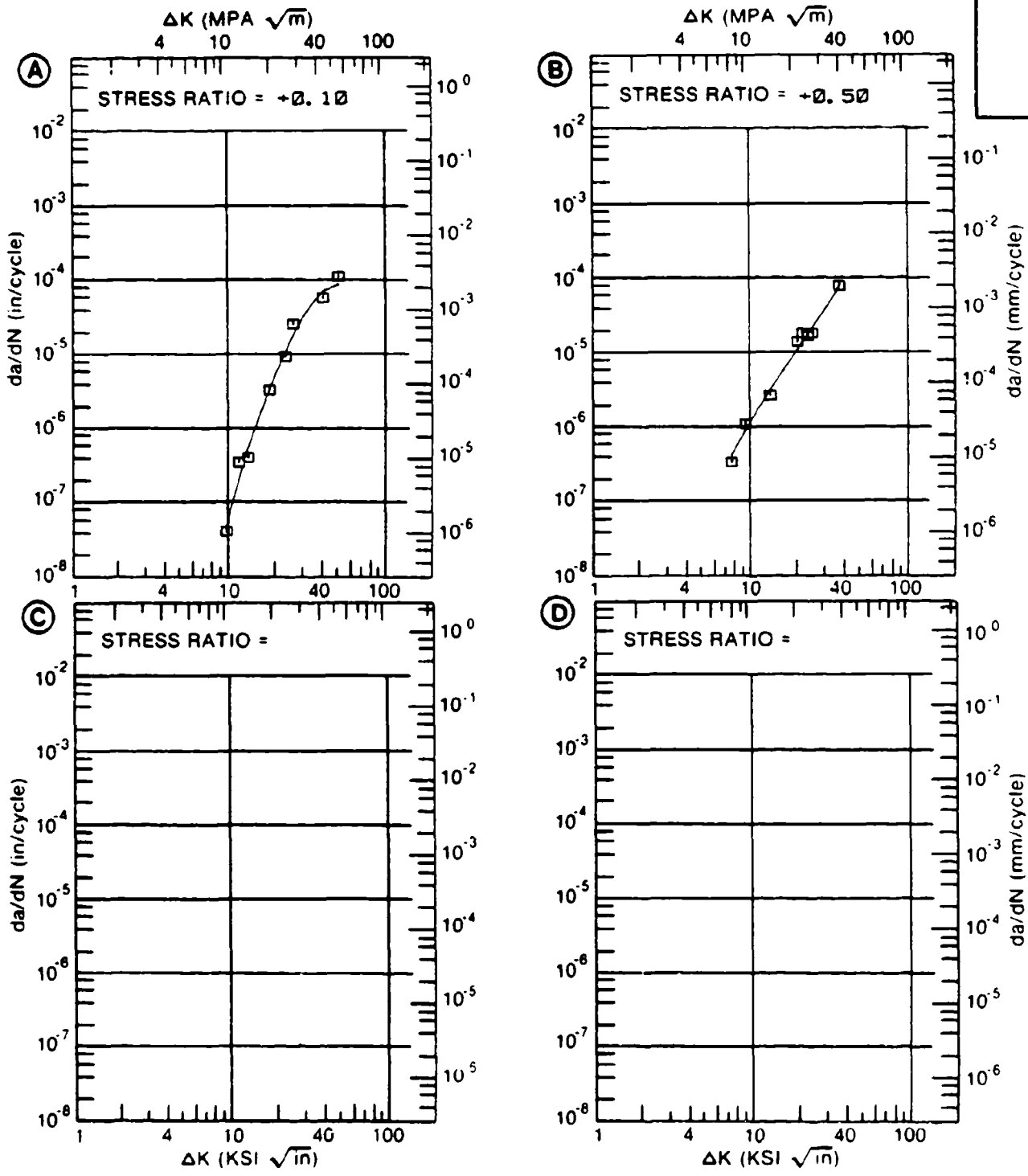


Figure 4.11.3.19

TABLE 4.11.3.20

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.20 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|-------------------------|---|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K | A: | | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 200.00 | | | | |
| DELTA K | A: | | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 2.79" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: S-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 116.3 KSI
 ULT. STRENGTH: 125.7 KSI
 SPECIMEN THK: 1.002"
 SPECIMEN WIDTH: 1.996"
 REFERENCES: 88575

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TI-6AL-4V

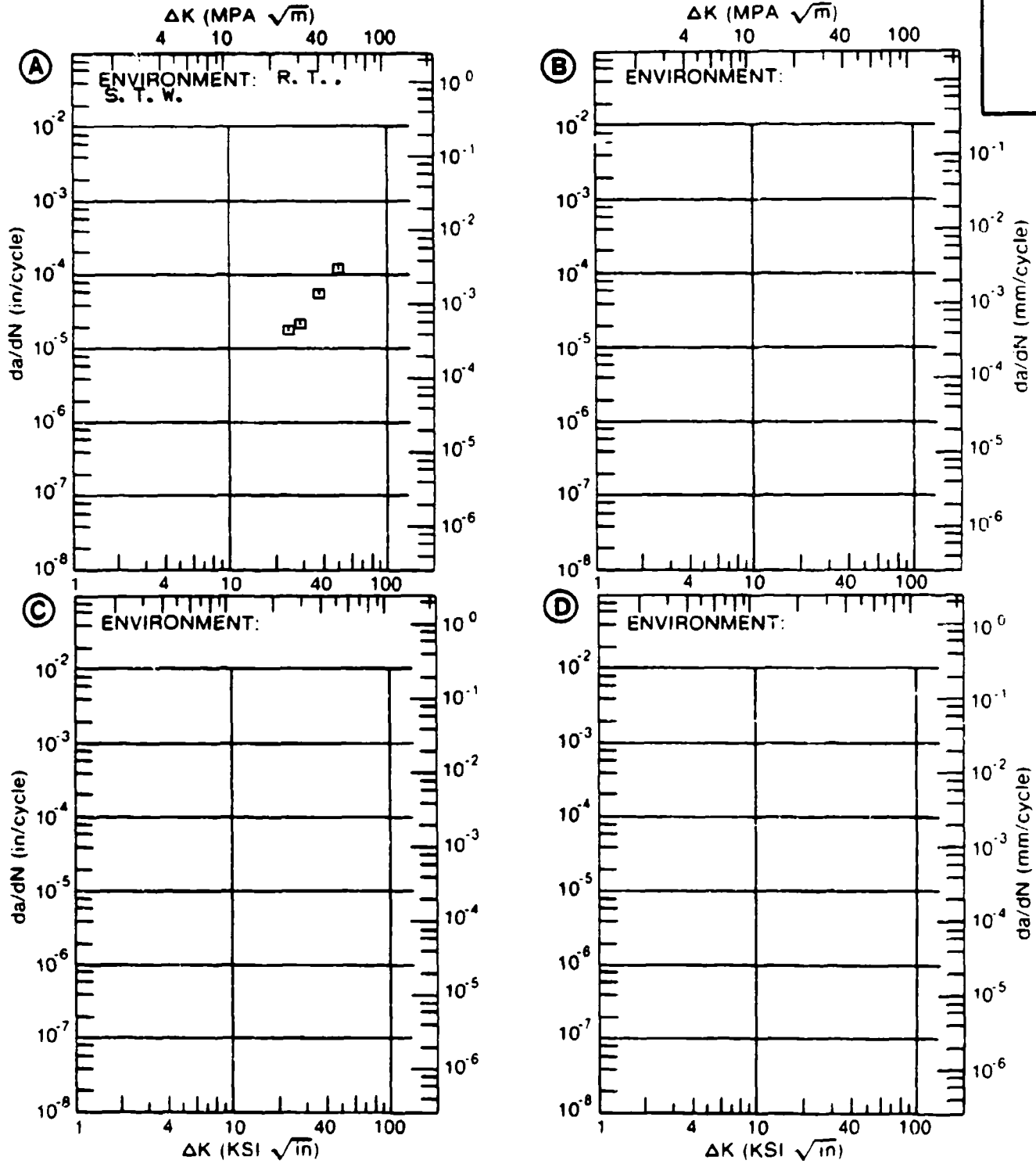


Figure 4.11.3.20

TABLE 4.11.3.21

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.21 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: BA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|--------------------------------------|-----------------------|---------------------------|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | E= R. T. JP-4 FUEL | E= R. T. SIM SEA WATER | |
| DELTA K A: 10.25 | .0872 | | | |
| MIN B: 12.23 | | .115 | | |
| C: 10.06 | | | .219 | |
| D: | | | | |
| 13.00 | .284 | .165 | .779 | |
| 14.00 | .820 | .566 | 1.94 | |
| 20.00 | 2.55 | 2.08 | 4.82 | |
| 25.00 | 7.52 | 6.89 | 11.6 | |
| 30.00 | 17.1 | 16.1 | 23.8 | |
| 35.00 | 31.9 | 28.9 | 43.1 | |
| 40.00 | 51.8 | 44.6 | 70.5 | |
| 50.00 | 102. | 88.2 | 149. | |
| 60.00 | 183. | 168. | 254. | |
| 70.00 | 356. | 339. | 438. | |
| 80.00 | 794. | 736. | 933. | |
| 90.00 | 2039. | 1726. | 2619. | |
| 100.00 | | 4343. | | |
| DELTA K A: 99.83 | 5876. | | | |
| MAX B: 101.83 | | 5178. | | |
| C: 99.93 | | | 9645. | |
| D: | | | | |
| ROOT MEAN SQUARE | 26.01 | 24.42 | 25.45 | |
| PERCENT ERROR | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 1.30" TH FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 FREQUENCY: 0.10- 20.00 HZ

YIELD STRENGTH: 111.0- 111.5 KSI
 ULT. STRENGTH: 122.5- 127.5 KSI
 SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: MA005

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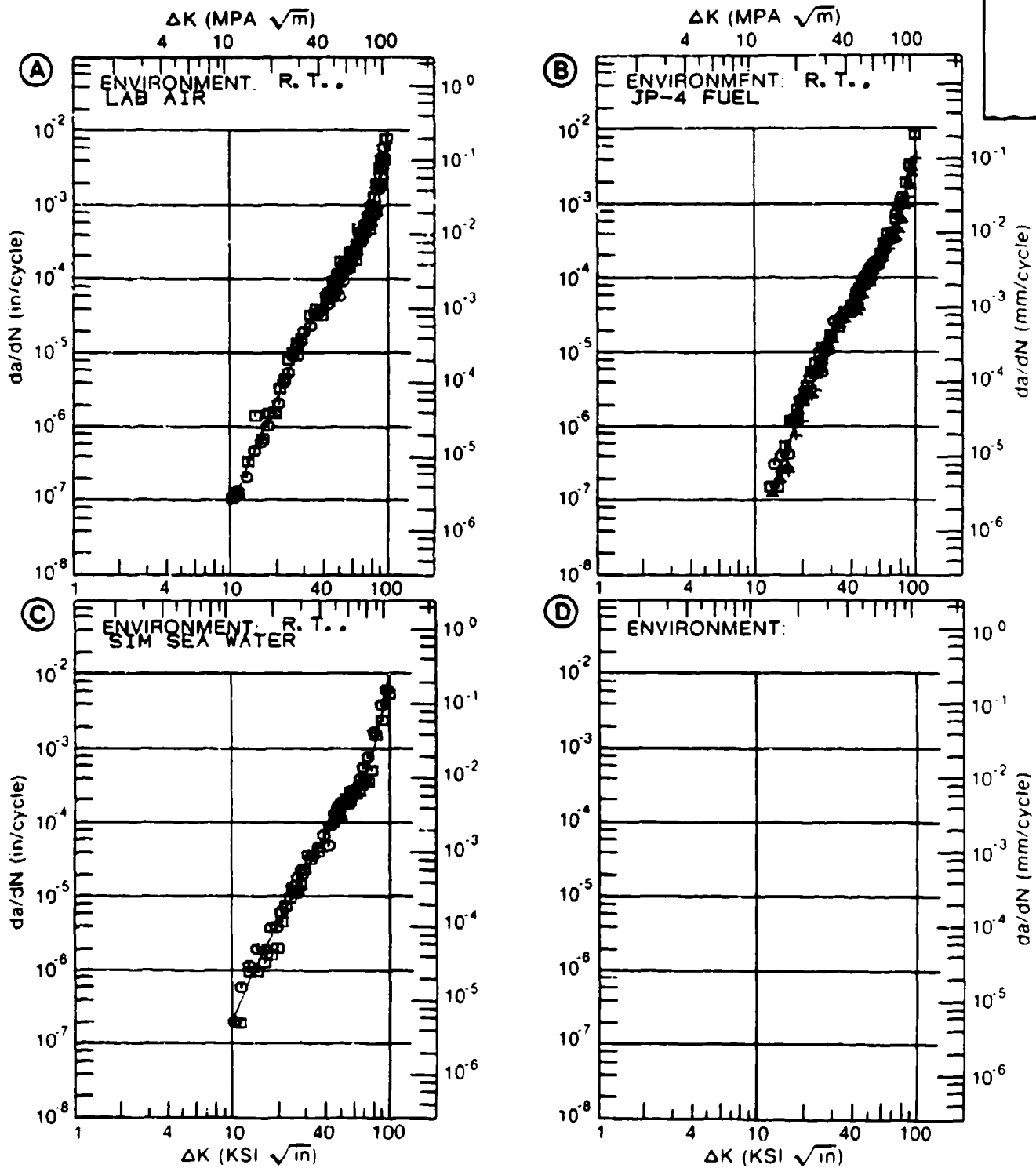


Figure 4.11.3.21

TABLE 4.11.3.22

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.22 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------|-----------------------|---------------------------|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E= R. T. JP-4 FUEL | E= R. T. SIM SEA WATER | |
| A: | 10.97 | .0750 | | | |
| DELTA K B: | 11.53 | | .0872 | | |
| MIN C: | 10.11 | | | .177 | |
| D: | | | | | |
| | 13.00 | .226 | .204 | .651 | |
| | 16.00 | .743 | .741 | 1.66 | |
| | 20.00 | 2.27 | 2.40 | 4.09 | |
| | 25.00 | 6.15 | 6.63 | 9.39 | |
| | 30.00 | 13.1 | 14.0 | 18.0 | |
| | 35.00 | 24.3 | 25.6 | 31.2 | |
| | 40.00 | 41.5 | 42.9 | 50.5 | |
| | 50.00 | 103. | 103. | 118. | |
| | 60.00 | 227. | 224. | 250. | |
| | 70.00 | 467. | 457. | 499. | |
| | 80.00 | 918. | 903. | 959. | |
| | 90.00 | 1746. | 1743. | 1789. | |
| | 100.00 | 3242. | | 3259. | |
| DELTA K A: | 104.34 | 4214. | | | |
| B: | 99.96 | | 3302. | | |
| MAX C: | 102.34 | | | 3739. | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 27.58 | 29.08 | 34.70 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.30" TH FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: T-L
 STRESS RATIO: +0.02
 FREQUENCY: 0.10- 20.00 HZ

YIELD STRENGTH: 110.0- 110.5 KSI
 ULT. STRENGTH: 124.5- 125.0 KSI
 SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: MA005

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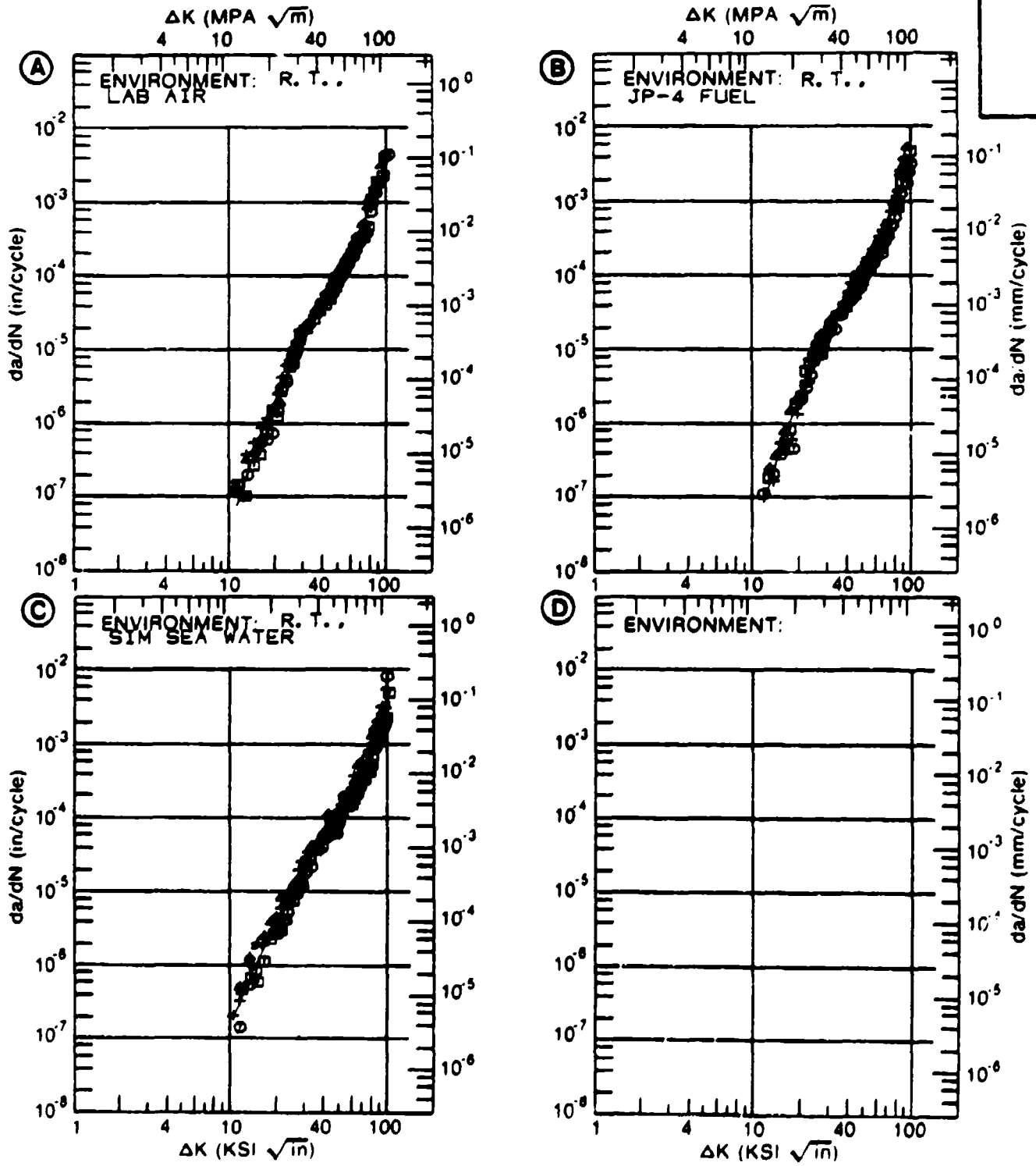


Figure 4.11.3.22

TABLE 4.11.3.23

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.23 INDICATING EFFECT

JF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BETA PROCESSED-MILL ANNEALED

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---|---|---|
| | A | B | C | D |
| | E= R. T. DRY AIR | | | |
| A: 23.05 | 5.27 | | | |
| DELTA K B: | | | | |
| MIN C: | | | | |
| D: | | | | |
| 25.00 | 6.45 | | | |
| 30.00 | 10.3 | | | |
| 35.00 | 15.7 | | | |
| 40.00 | 23.4 | | | |
| 50.00 | 48.8 | | | |
| A: 59.48 | 94.0 | | | |
| DELTA K B: | | | | |
| MAX C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 7.55
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BETA PROCESSED-MILL ANNEALED
 FORM: 0.13" TH SHEET
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 01332

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4V

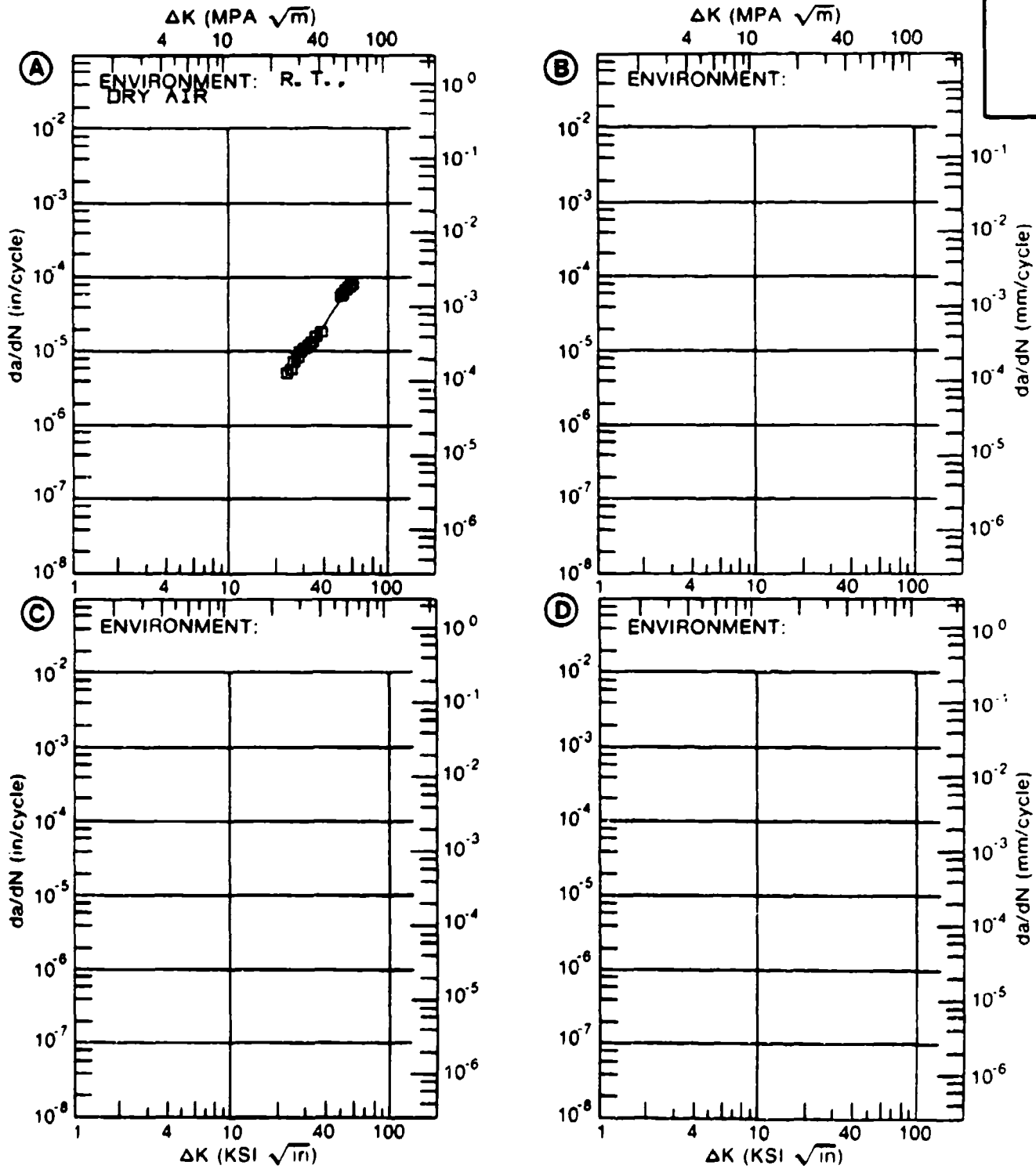


Figure 4.11.3.23

TABLE 4.11.3.24

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.24 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BETA PROCESSED-MILL ANNEALED

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|--------------------------|------|---|---|
| | A | B | C | D |
| | E= R. T. DRY AIR | | | |
| DELTA K MIN | A: 23.71 | 5.76 | | |
| | 25.00 | 6.20 | | |
| | 30.00 | 9.23 | | |
| | 35.00 | 14.6 | | |
| | 40.00 | 22.9 | | |
| | 50.00 | 48.7 | | |
| | 60.00 | 82.7 | | |
| DELTA K MAX | A: 60.18 | 83.4 | | |

ROOT MEAN SQUARE PERCENT ERROR 15.14

LIFE PREDICTION RATIO SUMMARY (NP/NA) 0.0-0.5
0.5-0.8
0.8-1.25
1.25-2.0
>2.0

CONDITION/HT: BETA PROCESSED-MILL ANNEALED
 FORM: 0.30" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 91332

TITAN.
ALLOY

TI-6AL-
4V

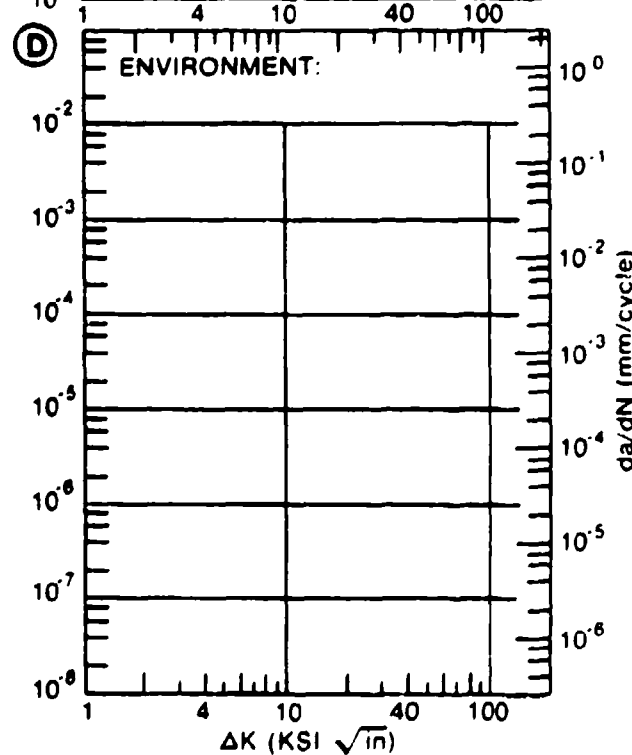
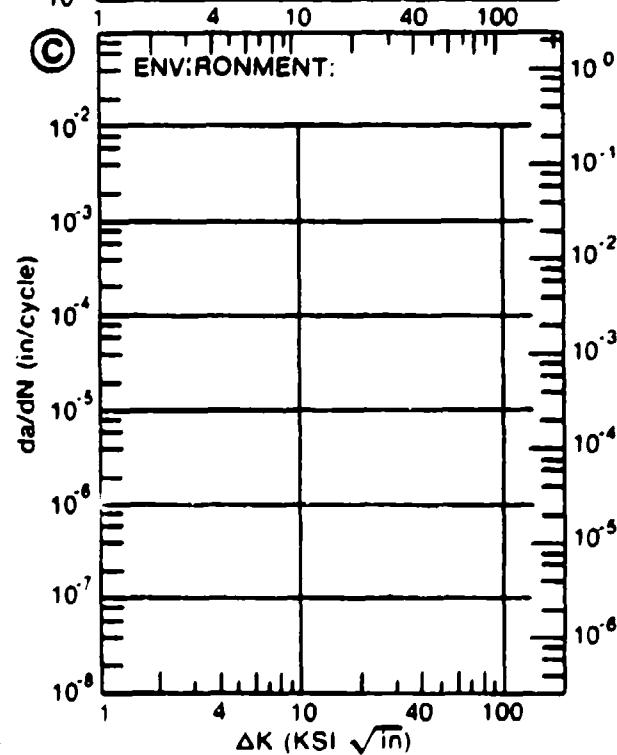
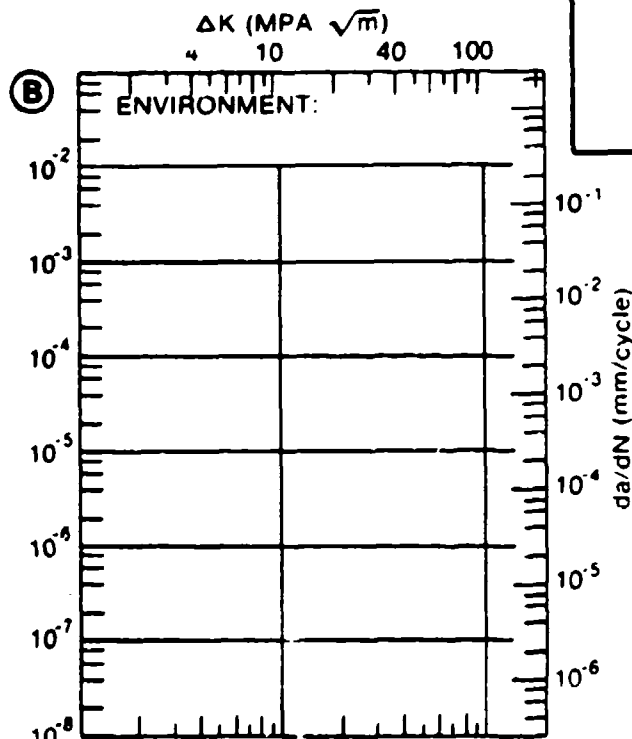
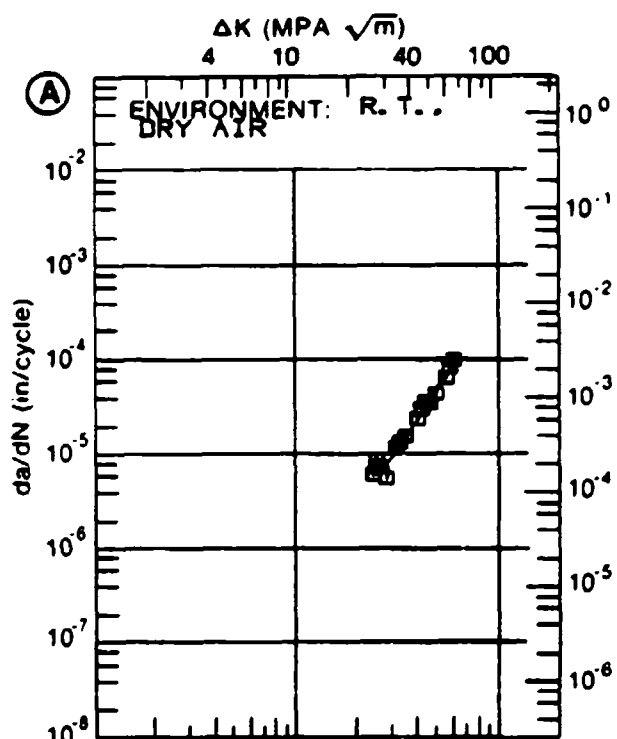


Figure 4.11.3.24

TABLE 4.11.3.25

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.25 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: BETA PROCESSED-MILL ANNEALED
ENVIRONMENT: R. T. , DRY AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K MIN | A: | 17.02 | 2.69 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 20.00 | 4.51 | | |
| | 25.00 | 9.81 | | | |
| | 30.00 | 16.8 | | | |
| | 35.00 | 28.4 | | | |
| DELTA K MAX | A: | 35.59 | 31.4 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | | | | |
| ROOT MEAN SQUARE | | 7.19 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BETA PROCESSED-MILL ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES 91332

TITAN.
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TI-6AL-
4V

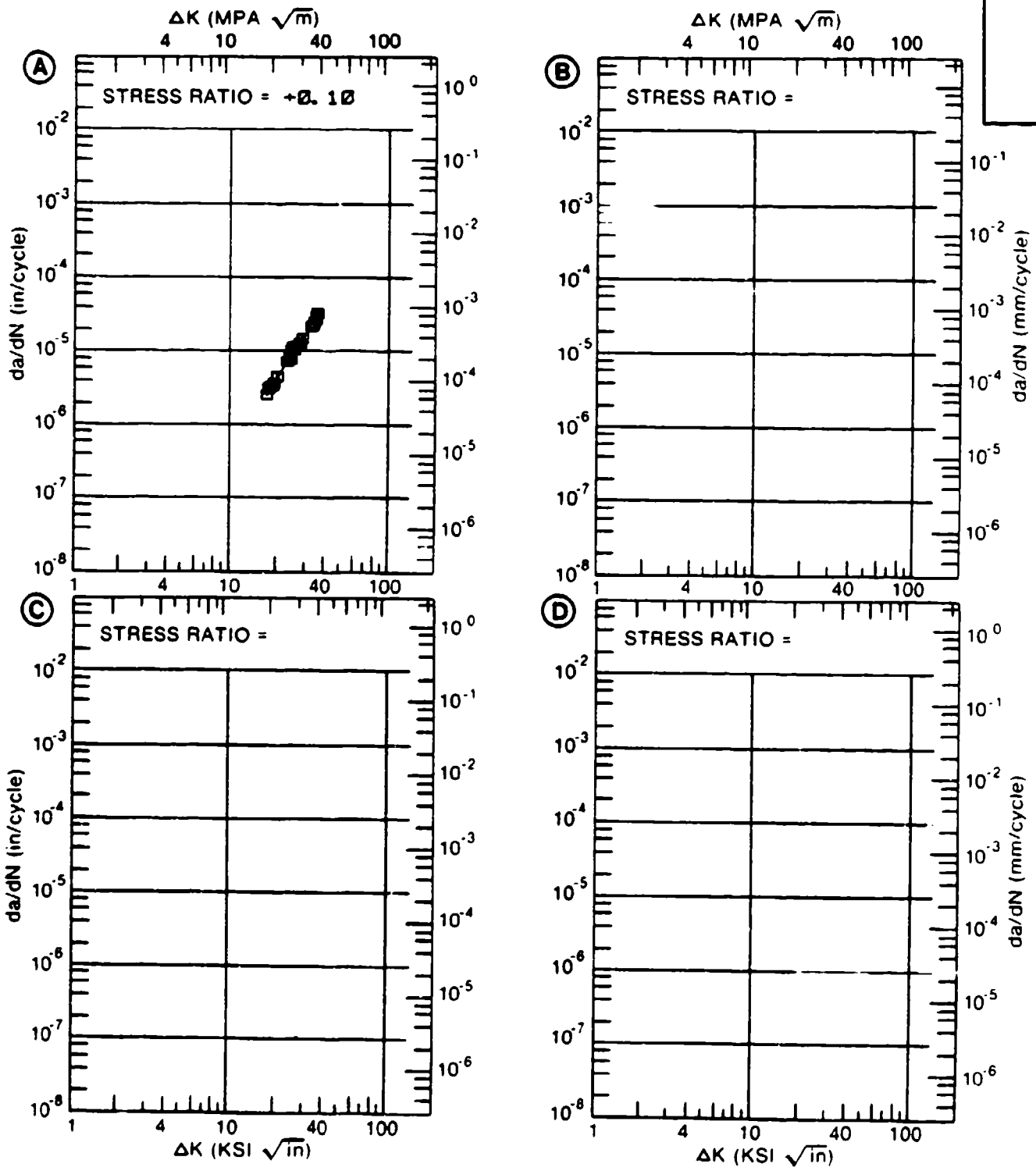


Figure 4.11.3.25

TABLE 4.11.3.26

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.26 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---|----------|--------------------------|---|---|---|
| CONDITION: BETA PROCESSED-MILL ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. : DRY AIR | | | |
| DELTA K | A: 16.77 | 2.51 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 4.66 | | | |
| | 25.00 | 9.56 | | | |
| | 30.00 | 16.9 | | | |
| | 35.00 | 27.8 | | | |
| DELTA K | A: 36.12 | 30.9 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 6.21 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BETA PROCESSED-MILL ANNEALED
 FORM: 0.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 01332

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TI-6AL-
4V

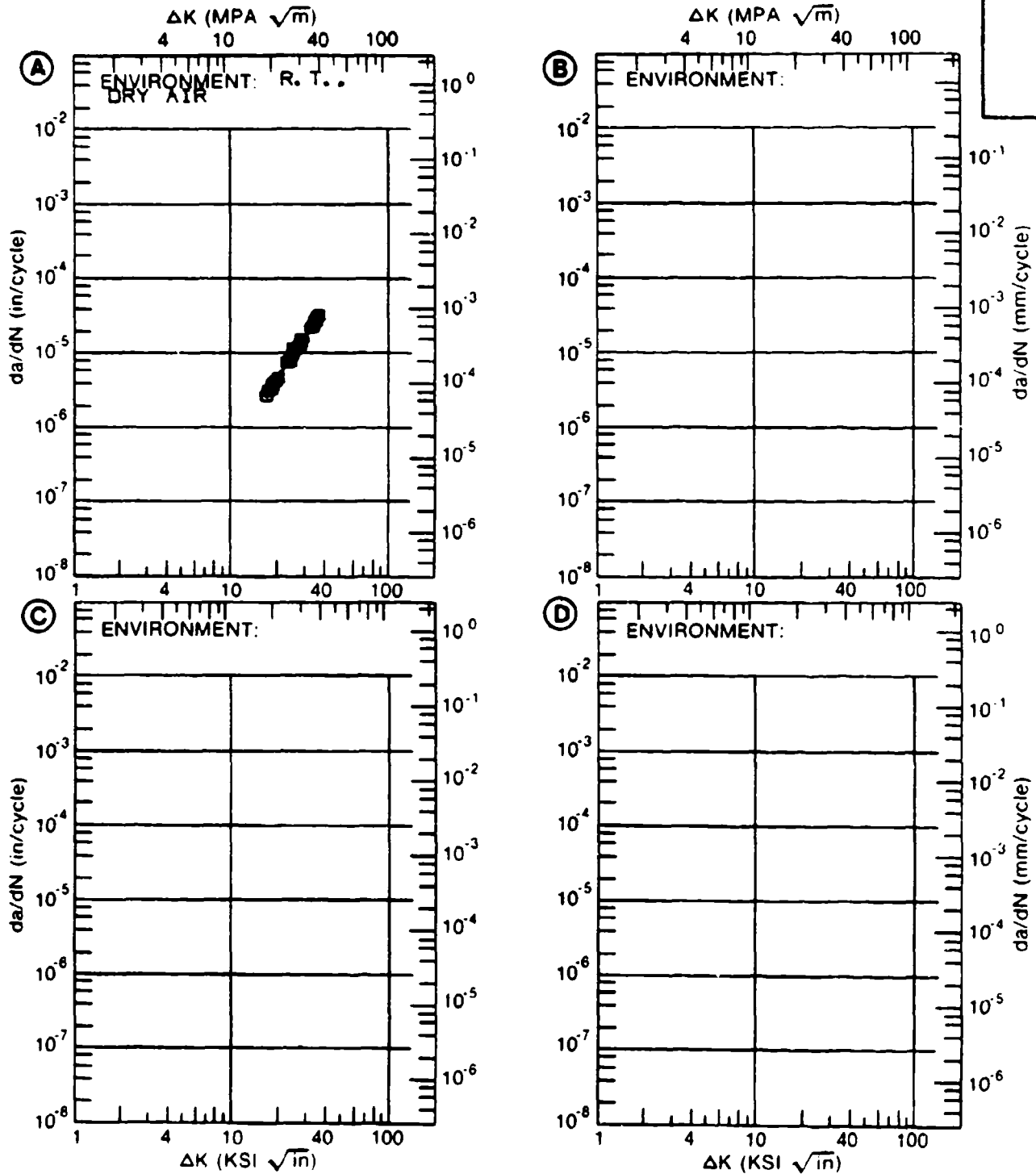


Figure 4.11.3.26

TABLE 4.11.3.27

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.27 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---|----------|--------------------------------------|---------|---|---|
| CONDITION: BETA PROCESSED-MILL ANNEALED | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K A: | 14.50 | .518 | | | |
| DELTA K B: | 6.57 | | .0730 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 7.00 | | .133 | | |
| | 8.00 | | .387 | | |
| | 9.00 | | .827 | | |
| | 10.00 | | 1.47 | | |
| | 13.00 | | 4.98 | | |
| | 16.00 | .593 | 13.6 | | |
| | 20.00 | .917 | | | |
| | 25.00 | 2.12 | | | |
| | 30.00 | 6.80 | | | |
| | 35.00 | 25.7 | | | |
| DELTA K A: | 38.26 | 43.2 | | | |
| DELTA K B: | 16.76 | | 17.6 | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 13.98 | 18.86 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BETA PROCESSED-MILL ANNEALED

FORM: 3.00" TH PLATE

SPECIMEN TYPE: WOL

ORIENTATION: L-T

FREQUENCY: 1.00 HZ

ENVIRONMENT: R. T. LAB AIR

YIELD STRENGTH: 130.4 KSI

ULT. STRENGTH: 138.1 KSI

SPECIMEN THK: 1.000"

SPECIMEN WIDTH: 2.550"

REFERENCES: JD008

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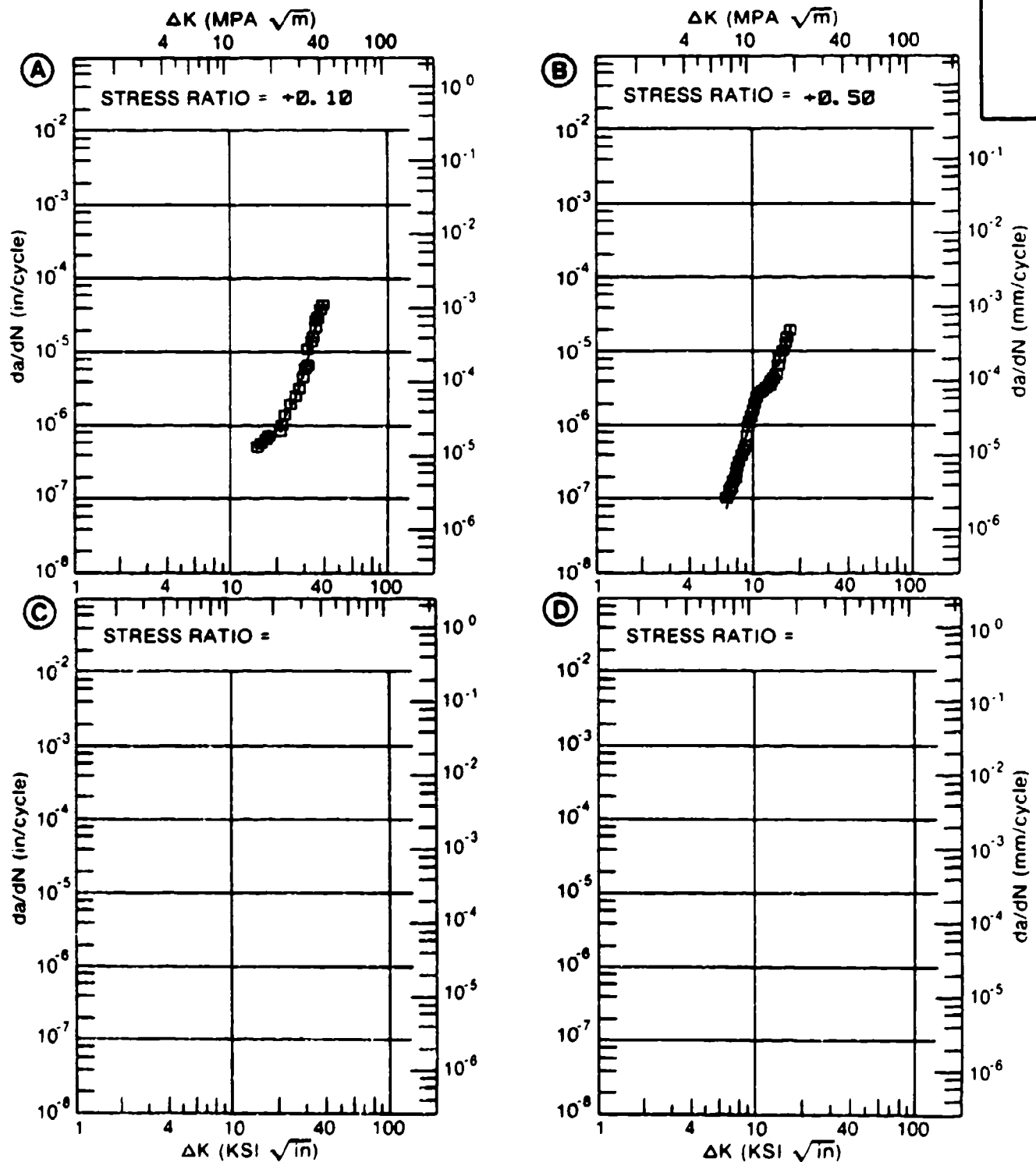


Figure 4.11.3.27

TABLE 4.11.3.28

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.28 INDICATING EFFECT
OF FREQUENCY

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: DB
ENVIRONMENT: R. T. , L. H. A.

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|-------|---|---|
| | A | B | C | D |
| | F(HZ)= 6.00 | | | |
| DELTA K MIN | A: 13.23 | 14.0 | | |
| | 16.00 | 21.7 | | |
| | 20.00 | 33.1 | | |
| | 25.00 | 61.3 | | |
| | 30.00 | 144. | | |
| | 35.00 | 415. | | |
| DELTA K MAX | A: 37.82 | 1316. | | |
| | | | | |

ROOT MEAN SQUARE 12.23
PERCENT ERROR

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | |
| (NP/NA) | >2.0 | |

CONDITION/HT: DB
 FORM: 0.63" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.30
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 153.0 KSI
 ULT. STRENGTH: 165.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 88579

TITAN.
ALLOY

TI-6AL-
4V

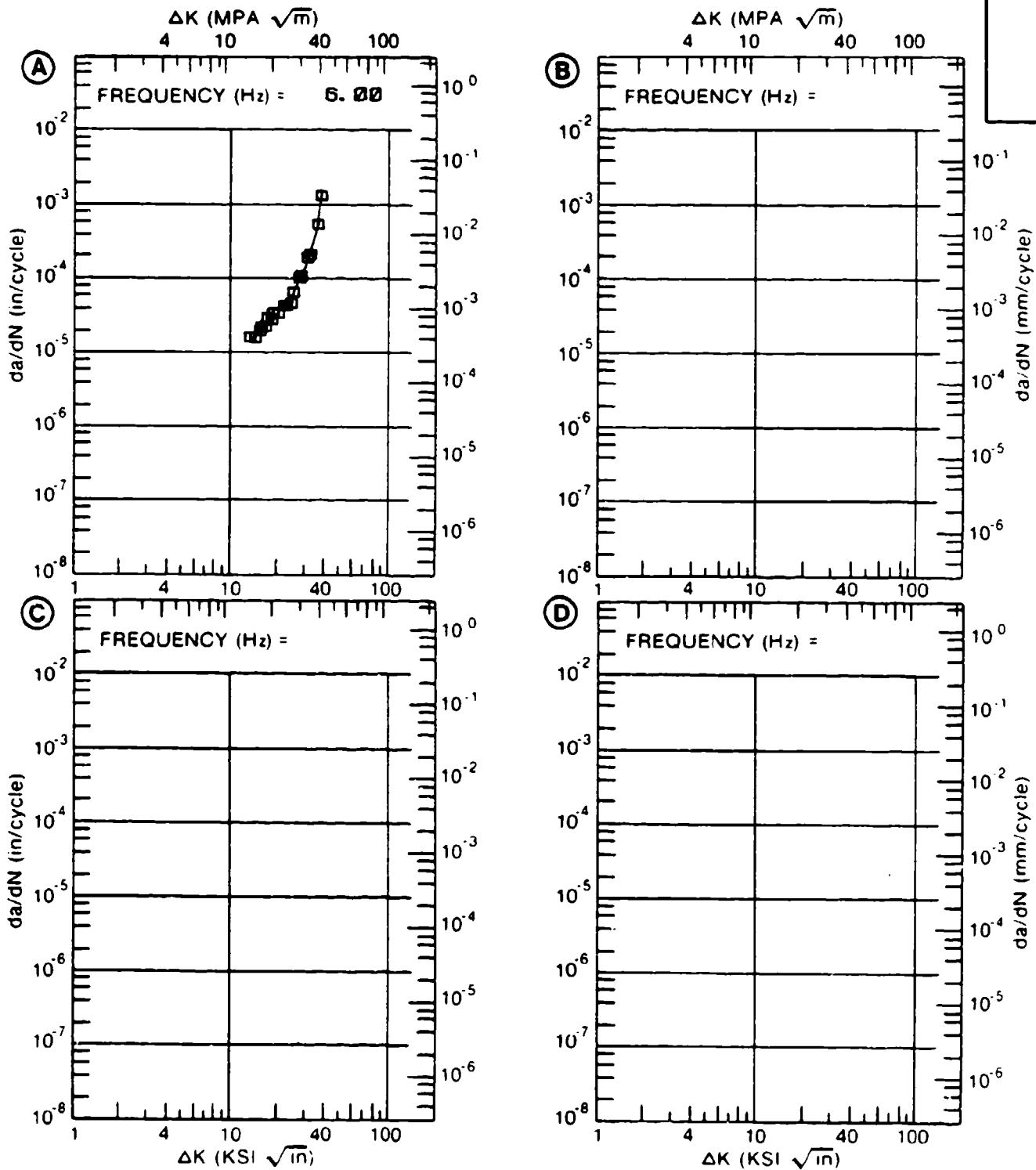


Figure 4.11.3.28

TABLE 4.11.3.29

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.29 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: DB

TI-6AL-4V

| DELTA K (KSI*(N**1/2)) | | DA/DN (10**--6 IN./CYCLE) | | | |
|---------------------------|-------|---------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| A: | 7.88 | .139 | | | |
| DELTA K B: | | | | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 8.00 | .147 | | | |
| | 9.00 | .242 | | | |
| | 10.00 | .397 | | | |
| | 13.00 | 1.52 | | | |
| | 16.00 | 4.41 | | | |
| | 20.00 | 12.1 | | | |
| | 25.00 | 25.6 | | | |
| | 30.00 | 35.2 | | | |
| A: | 32.73 | 36.6 | | | |
| DELTA K B: | | | | | |
| MAX C: | | | | | |
| D: | | | | | |

ROOT MEAN SQUARE 17.52
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: DB
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 8.00 HZ

YIELD STRENGTH: 115.0 KSI
 ULT. STRENGTH: 126.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 4.040"
 REFERENCES: 98579

TITAN.
ALLOY

TI-6AL-
4V

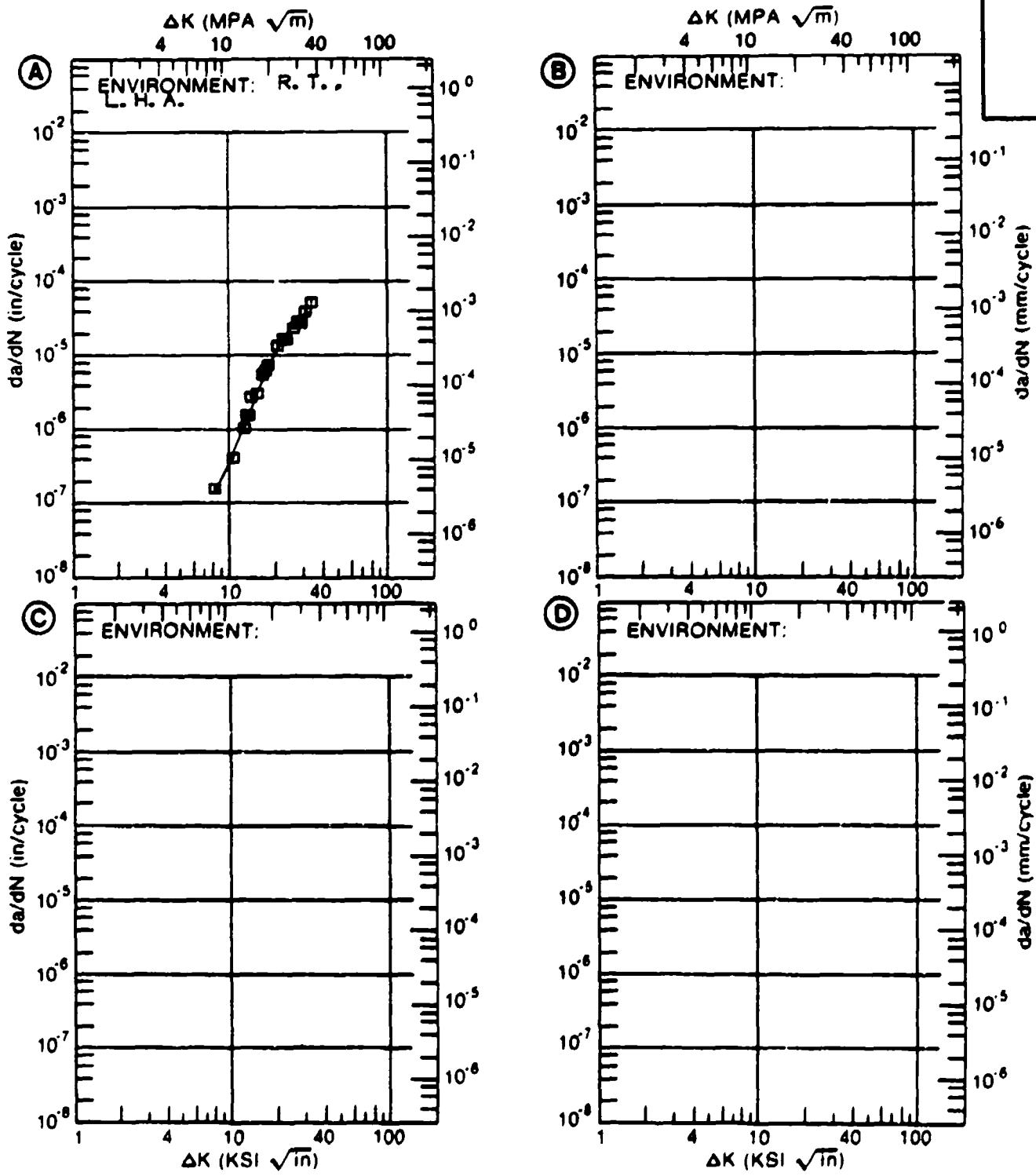


Figure 4.11.3.29

TABLE 4.11.3.30

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.30 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: DB

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K MIN | A: 12.21 | .149 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .469 | | | |
| | 16.00 | 1.98 | | | |
| | 20.00 | 8.20 | | | |
| | 25.00 | 22.2 | | | |
| | 30.00 | 41.4 | | | |
| | 35.00 | 65.8 | | | |
| | 40.00 | 98.3 | | | |
| | 50.00 | 214. | | | |
| DELTA K MAX | A: 54.03 | 296. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 19.51
PERCENT ERROR

LIFE PREDICTION RATIO SUMMARY (NP/NA)

| | |
|----------|---|
| 0.0-0.5 | |
| 0.5-0.8 | |
| 0.8-1.25 | 1 |
| 1.25-2.0 | |
| >2.0 | |

CONDITION/HT: DB
 FORM: 8.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 118.0 KSI
 ULT. STRENGTH: 128.0 KSI
 SPECIMEN THK: 0.992"
 SPECIMEN WIDTH: 8.000"
 REFERENCES: 85837

TITAN.
 ALLOY
 TI-6AL-
 4V

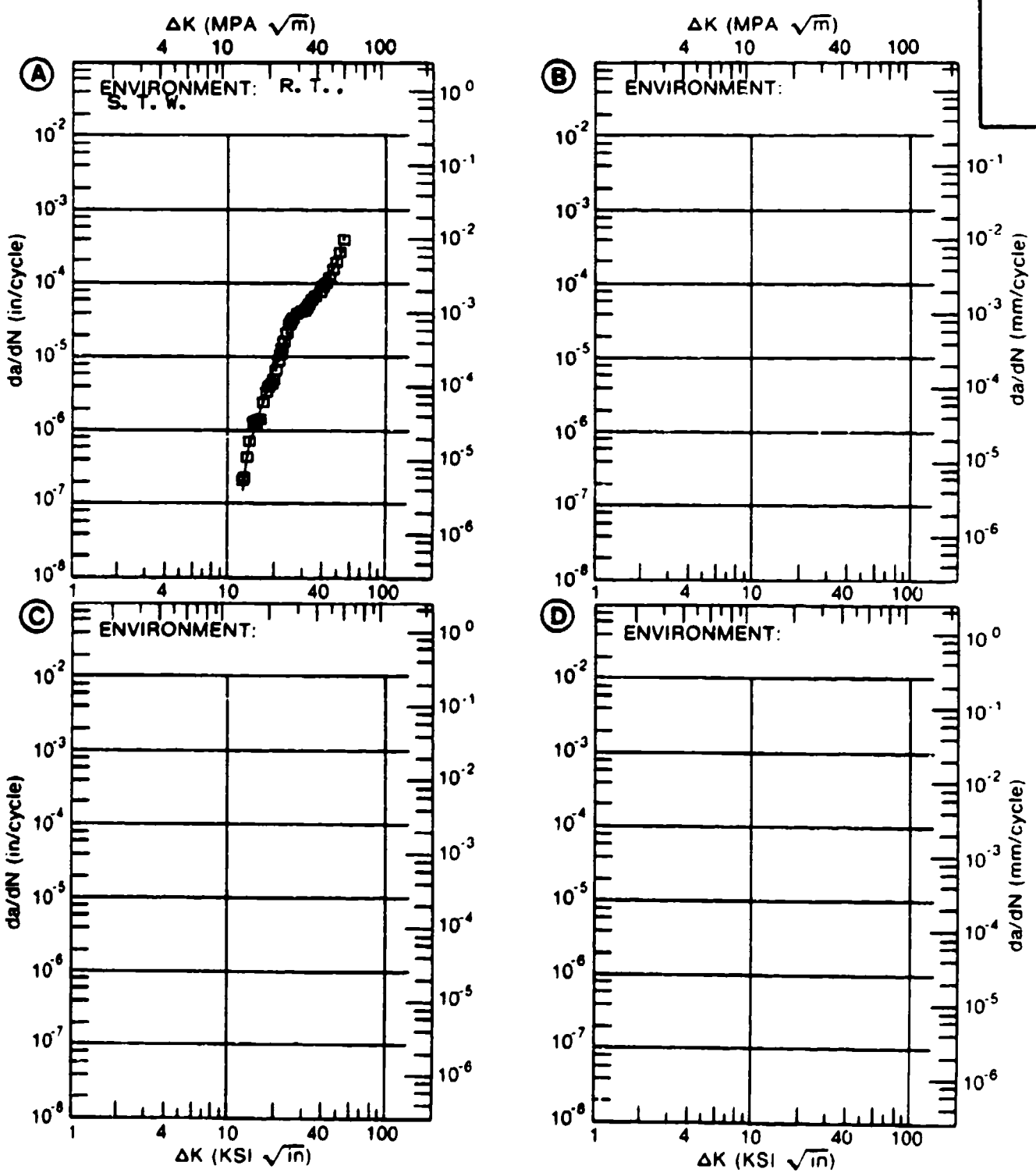


Figure 4.11.3.30

TABLE 4.11.3.31

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.31 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: DB | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K | A: 9.39 | .371 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .782 | | | |
| | 13.00 | 4.03 | | | |
| | 16.00 | 11.4 | | | |
| | 20.00 | 21.3 | | | |
| | 25.00 | 31.5 | | | |
| | 30.00 | 46.2 | | | |
| | 35.00 | 77.1 | | | |
| | 40.00 | 151. | | | |
| DELTA K | A: 47.88 | 497. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.26 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DB
 FORM: 8.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: S-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 114.0 KSI
 ULT. STRENGTH: 129.0 KSI
 SPECIMEN THK: 0.993"
 SPECIMEN WIDTH: 4.940"
 REFERENCES: 85837

TITAN.
ALLOY

TI-6AL-
4V

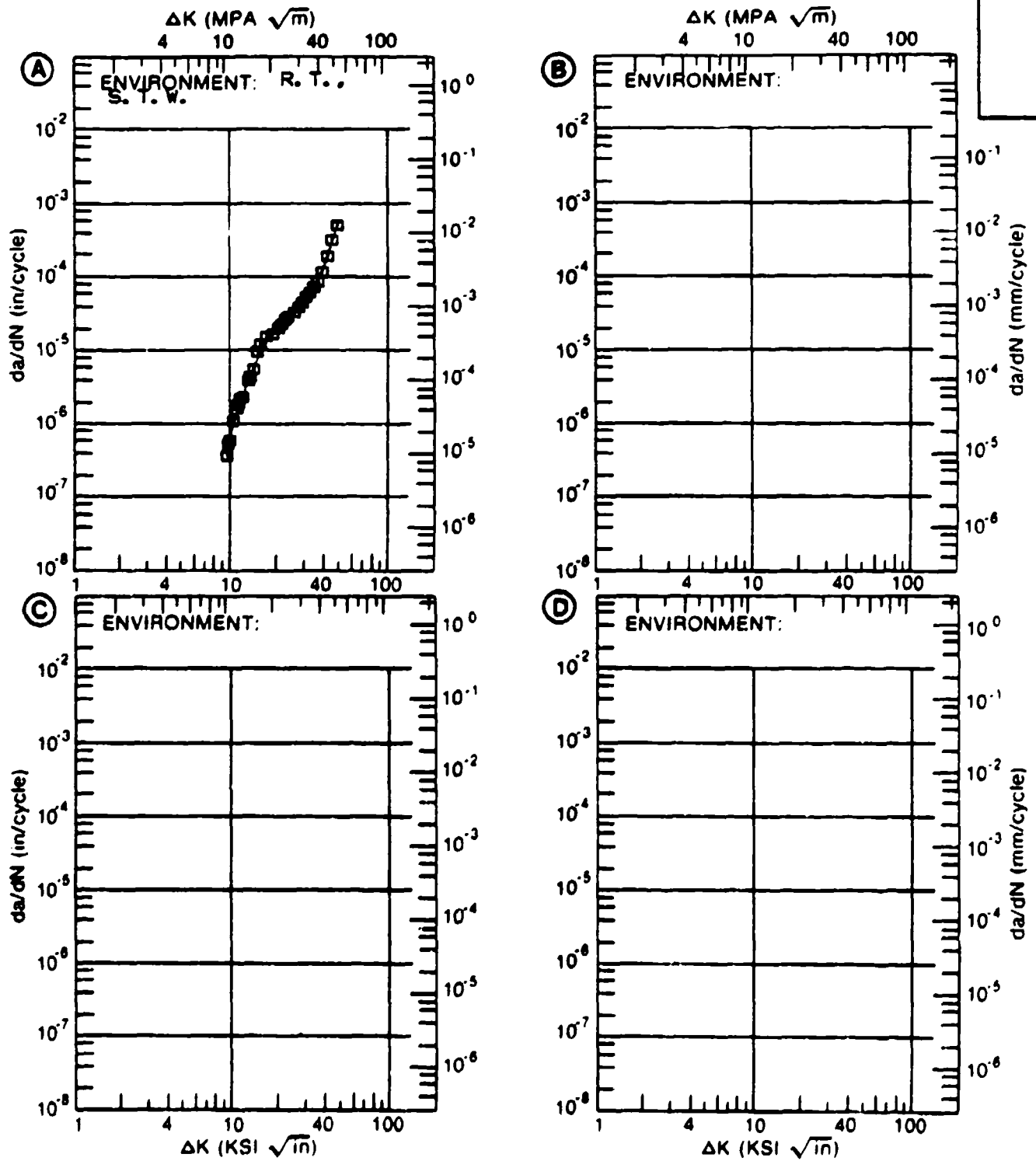


Figure 4.11.3.31

TABLE 4.11.3.32

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.32 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|------------|--------------------------|---|---|---|
| CONDITION: DB + TR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K | A: 10.12 | .176 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .448 | | | |
| | 16.00 | 2.01 | | | |
| | 20.00 | 9.78 | | | |
| | 25.00 | 29.1 | | | |
| | 30.00 | 50.6 | | | |
| | 35.00 | 83.1 | | | |
| | 40.00 | 155. | | | |
| DELTA K | A: 44.78 | 337. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 15.89 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 1 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DB + TR
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: S-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 111.0 KSI
 ULT. STRENGTH: 128.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 88579

TITAN.
ALLOY

TI-6AL-4V

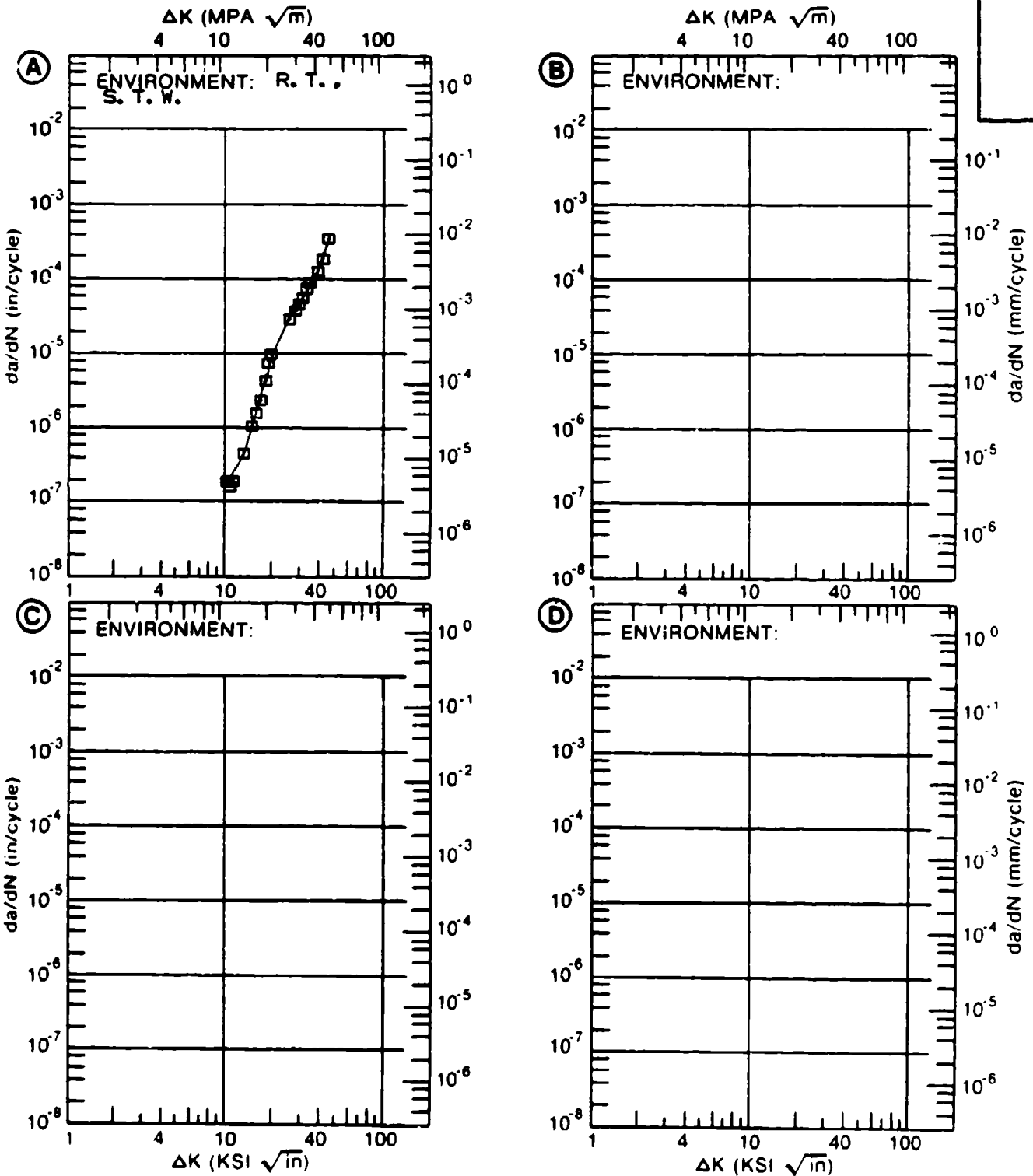


Figure 4.11.3.32

TABLE 4.11.3.33

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.33 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------|---|---|---|
| CONDITION: DB + 2DBTC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K | A: 13.92 | 1.11 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 2.14 | | | |
| | 20.00 | 7.93 | | | |
| | 25.00 | 23.1 | | | |
| | 30.00 | 45.2 | | | |
| | 35.00 | 74.0 | | | |
| | 40.00 | 112. | | | |
| | 50.00 | 244. | | | |
| | 60.00 | 545. | | | |
| DELTA K | A: 62.46 | 671. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 6.56 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DB + 2DBTC
 FORM: 8.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 114.0 KSI
 ULT. STRENGTH: 128.0 KSI
 SPECIMEN THK: 0.998"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 85837

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4V

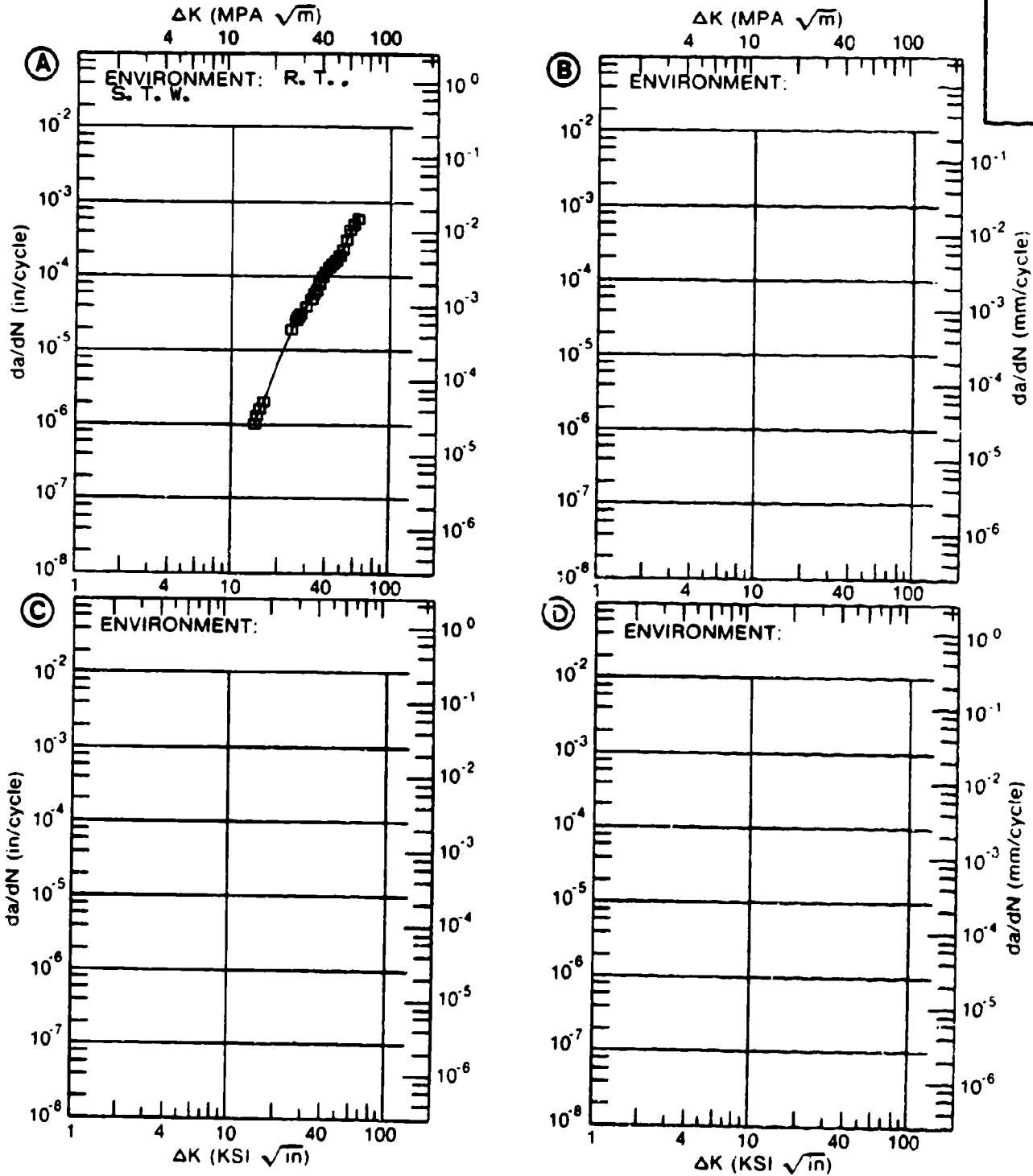


Figure 4.11.3.33

TABLE 4.11.3.34

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.34 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------|---|---|---|
| CONDITION: DB + 2DBTC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| DELTA K | A: 14.18 | 2.57 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 5.81 | | | |
| | 20.00 | 8.36 | | | |
| | 25.00 | 30.9 | | | |
| DELTA K | A: 26.83 | 31.9 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.76 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DB + 2DBTC
 FORM: 8.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: S-T
 STRESS RATIO: +0.08
 FREQUENCY: 8.00 HZ

YIELD STRENGTH: 114.0 KSI
 ULT. STRENGTH: 128.0 KSI
 SPECIMEN THK: 0.983"
 SPECIMEN WIDTH: 4.950"
 REFERENCES: 85837

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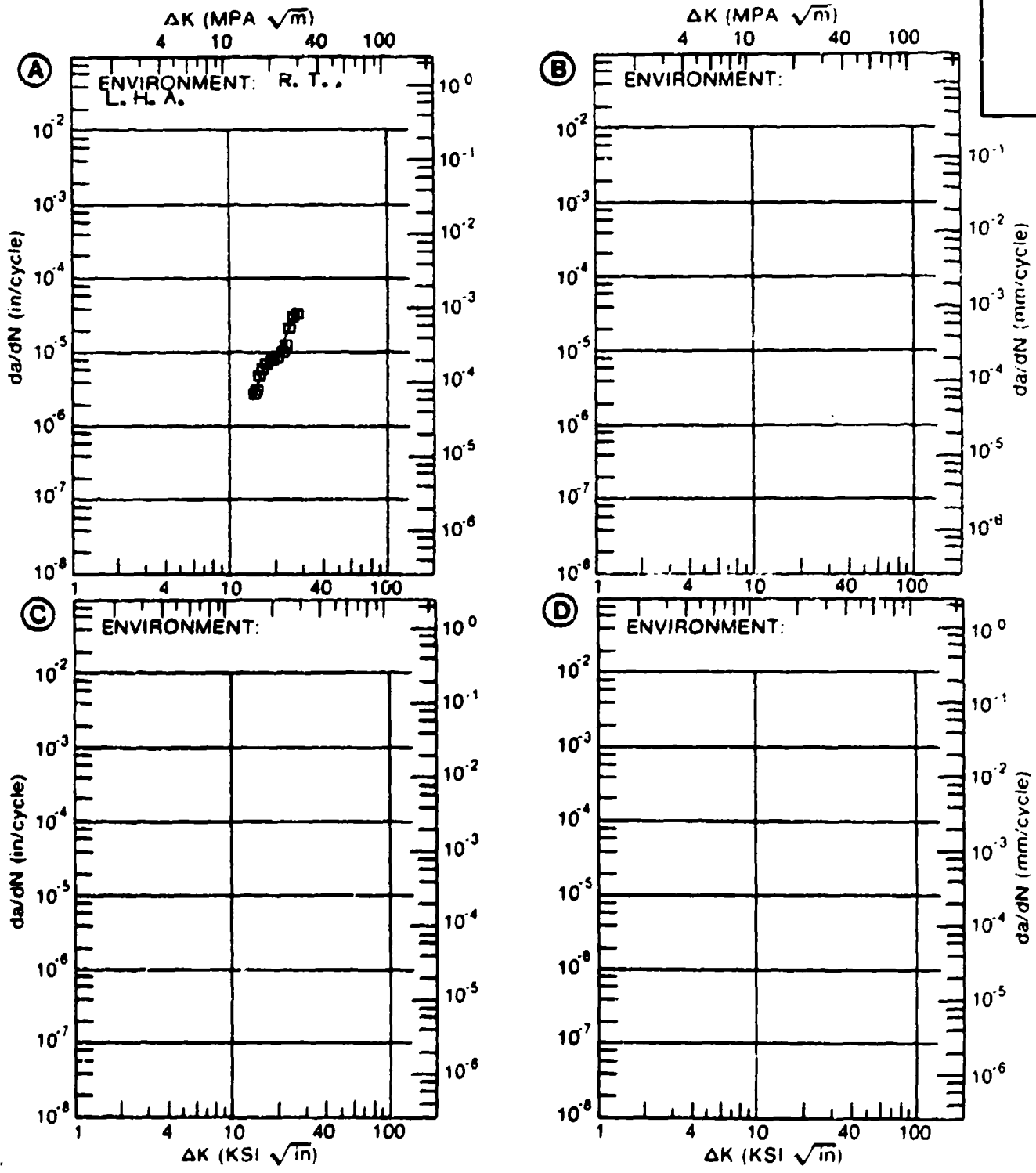


Figure 4.11.3.34

TABLE 4.11.3.35

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.35 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: DB + 4DBTC

| DELTA K (KSI*IN**1/2) | DA/DN (10**5 IN./CYCLE) | | | |
|--------------------------|-------------------------|------|---|---|
| | A | B | C | D |
| | E= R. T. S. T. W. | | | |
| DELTA K MIN | A: 11.85 | .262 | | |
| | 13.00 | .473 | | |
| | 16.00 | 2.26 | | |
| | 20.00 | 9.02 | | |
| | 25.00 | 26.2 | | |
| | 30.00 | 48.5 | | |
| | 35.00 | 77.4 | | |
| | 40.00 | 112. | | |
| | 50.00 | 209. | | |
| DELTA K MAX | A: 54.46 | 270. | | |

ROOT MEAN SQUARE PERCENT ERROR 13.83

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: DB + 4DBTC
 FORM: 8.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 115.0 KSI
 ULT. STRENGTH: 126.0 KSI
 SPECIMEN THK: 0.990"
 SPECIMEN WIDTH: 8.000"
 REFERENCES: 85837

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 4V

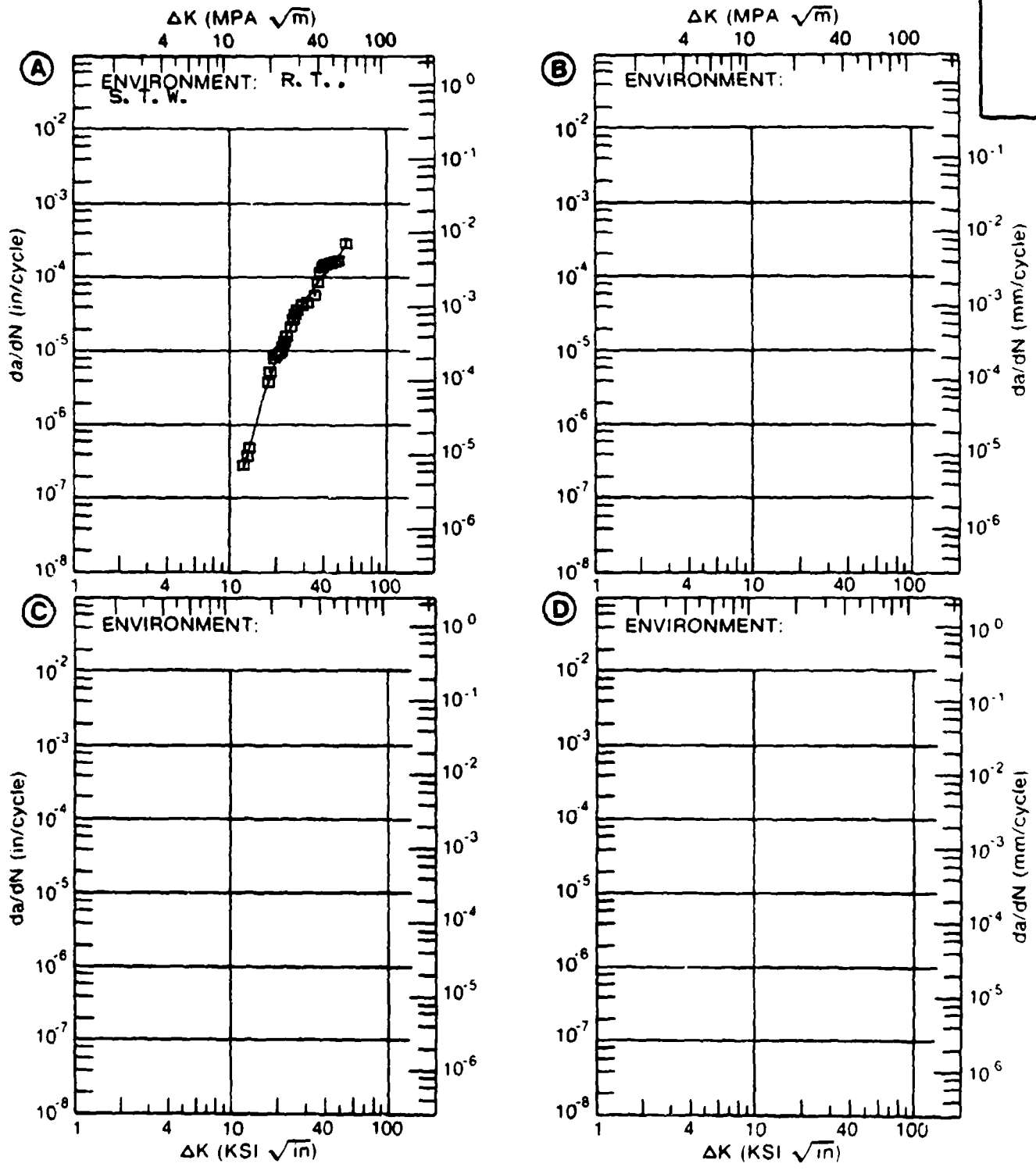


Figure 4.11.3.35

TABLE 4.11.3.36

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.36 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: DBT + PC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. S. T. W. | | | |
| DELTA K | A: 10.37 | .256 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .631 | | | |
| | 16.00 | 1.82 | | | |
| | 20.00 | 11.2 | | | |
| | 25.00 | 30.5 | | | |
| DELTA K | A: 27.18 | 41.3 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 24.25 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DBT + PC
 FORM: 2.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 122.0 KSI
 ULT. STRENGTH: 135.0 KSI
 SPECIMEN THK: 0.350"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 98570

TITAN.
ALLOY

TI-6AL-
4V

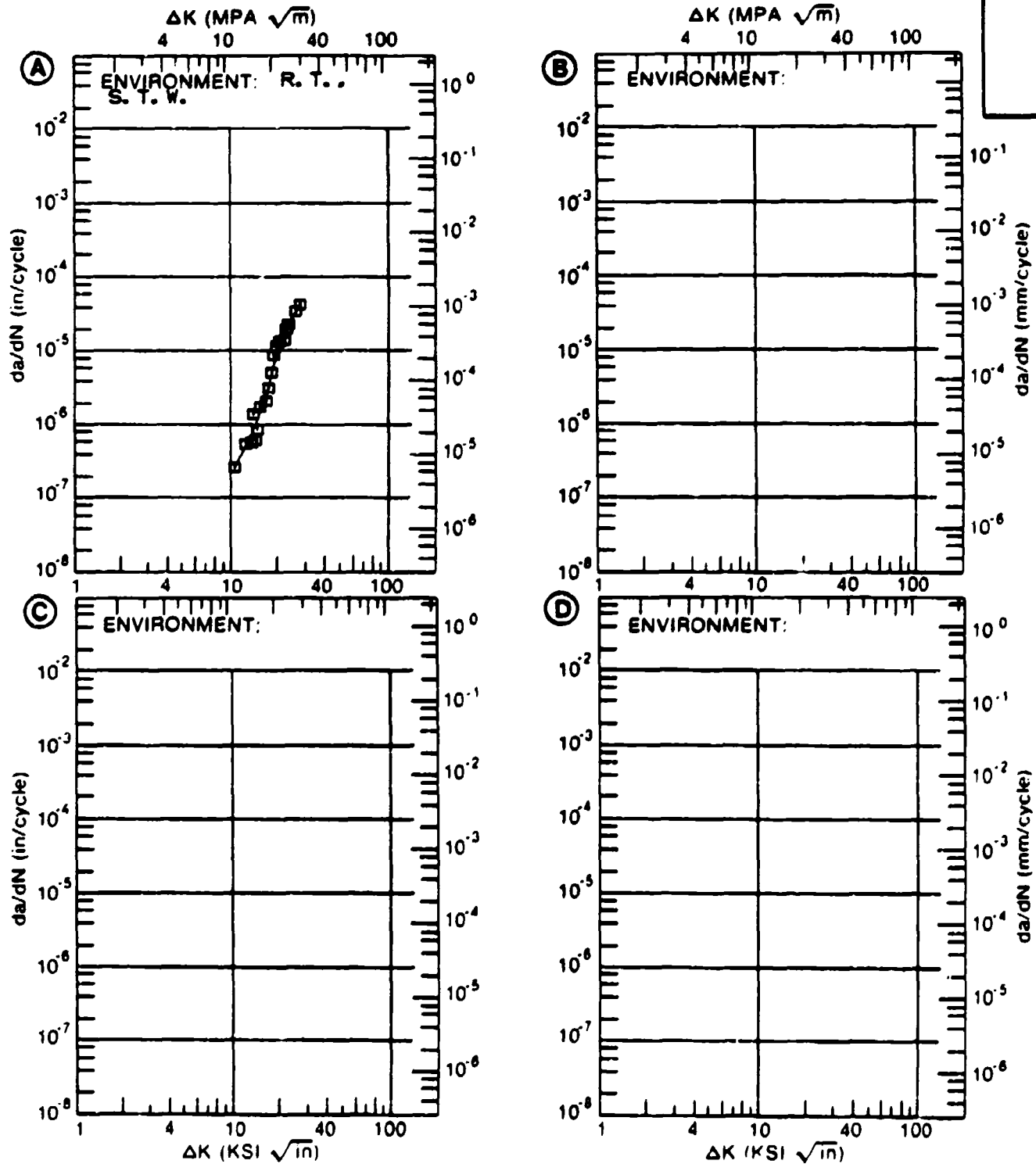


Figure 4.11.3.36

TABLE 4.11.3.37

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.37 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|----------|---------------------------|---------|---|---|
| CONDITION: DBTC | | | | | |
| ENVIRONMENT: R. T. , L. H. A. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**--6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | | |
| DELTA K | A: 13.74 | 3.40 | | | |
| MIN | B: 9.83 | | .53 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | | .626 | | |
| | 13.00 | | 3.62 | | |
| | 16.00 | 8.58 | 8.93 | | |
| | 20.00 | 16.4 | 19.4 | | |
| | 25.00 | 29.4 | 44.3 | | |
| | 30.00 | 51.4 | 108. | | |
| | 35.00 | 95.1 | 285. | | |
| | 40.00 | 191. | 683. | | |
| | 50.00 | 753. | 2181. | | |
| DELTA K | A: 58.30 | 1802. | | | |
| MAX | B: 56.14 | | 4408. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.57 | 11.54 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DBTC
 FORM: 0.62- 0.63" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 138.0- 140.0 KSI
 ULT. STRENGTH: 148.0- 150.0 KSI
 SPECIMEN THK: 0.496- 0.500"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 88579, 85837

TITAN.
ALLOY

TI-6AL-
4V

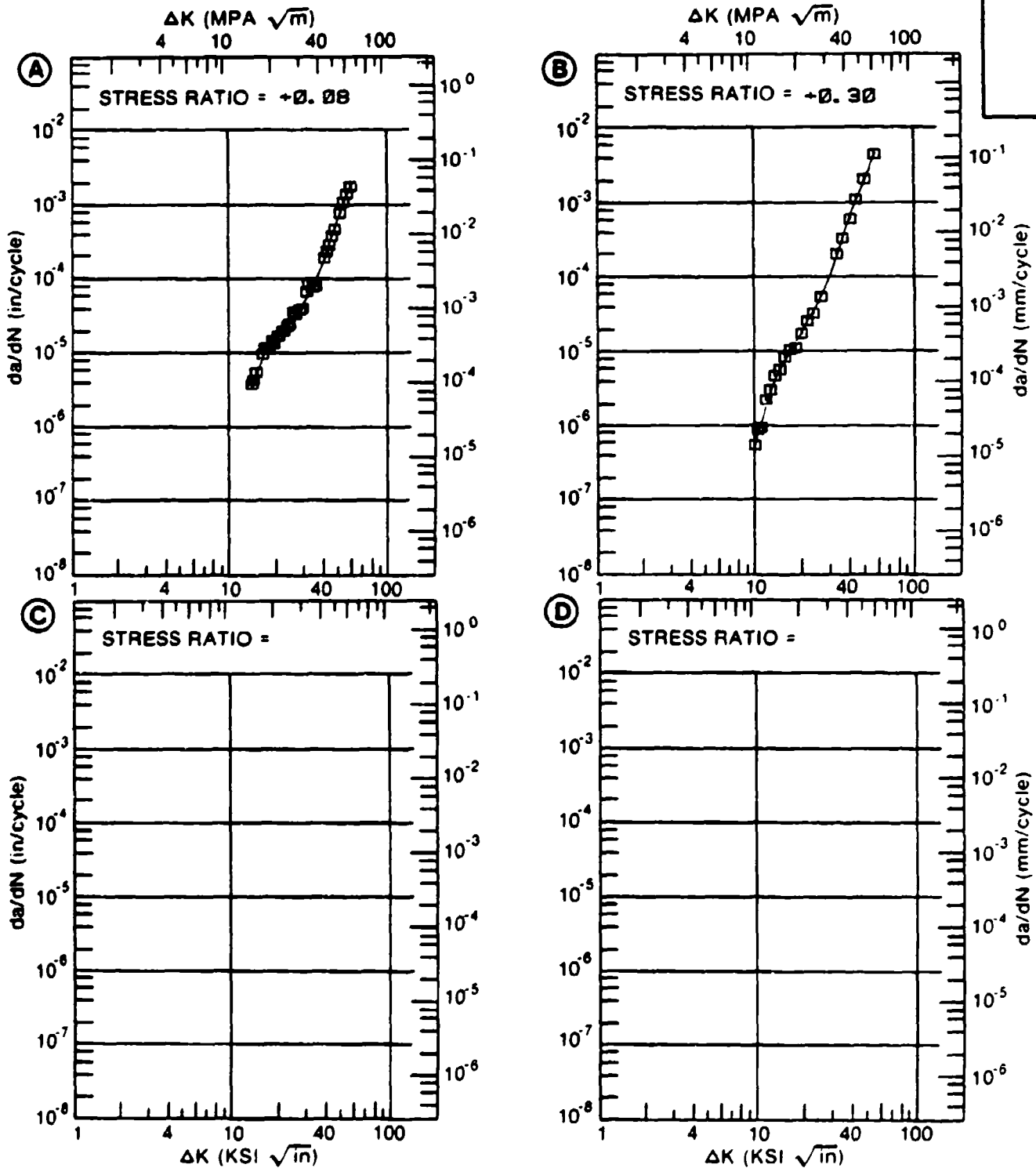


Figure 4.11.3.37

TABLE 4.11.3.38

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.38 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|----------|--------------------------------------|----------------------|---|---|
| CONDITION: DBTC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. S. T. W. | | |
| DELTA K MIN | A: 10.00 | .359 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.30 | | | |
| | 16.00 | 4.77 | | | |
| | 20.00 | 13.1 | | | |
| | 25.00 | 26.2 | | | |
| | 30.00 | 43.1 | | | |
| | 35.00 | 69.0 | | | |
| | 40.00 | 110. | | | |
| | 50.00 | 285. | | | |
| DELTA K MAX | A: 59.95 | 750. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 29.28 | 0.00 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | 1 | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | | | | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: DBTC
 FORM: 1.25" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.30
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 125.0 KSI
 ULT. STRENGTH: 137.0 KSI
 SPECIMEN THK: 0.000 - 1.000"
 SPECIMEN WIDTH: 8.000"
 REFERENCES: 88578, 85837

TITAN.
 ALLOY
 TI-6AL-
 4V

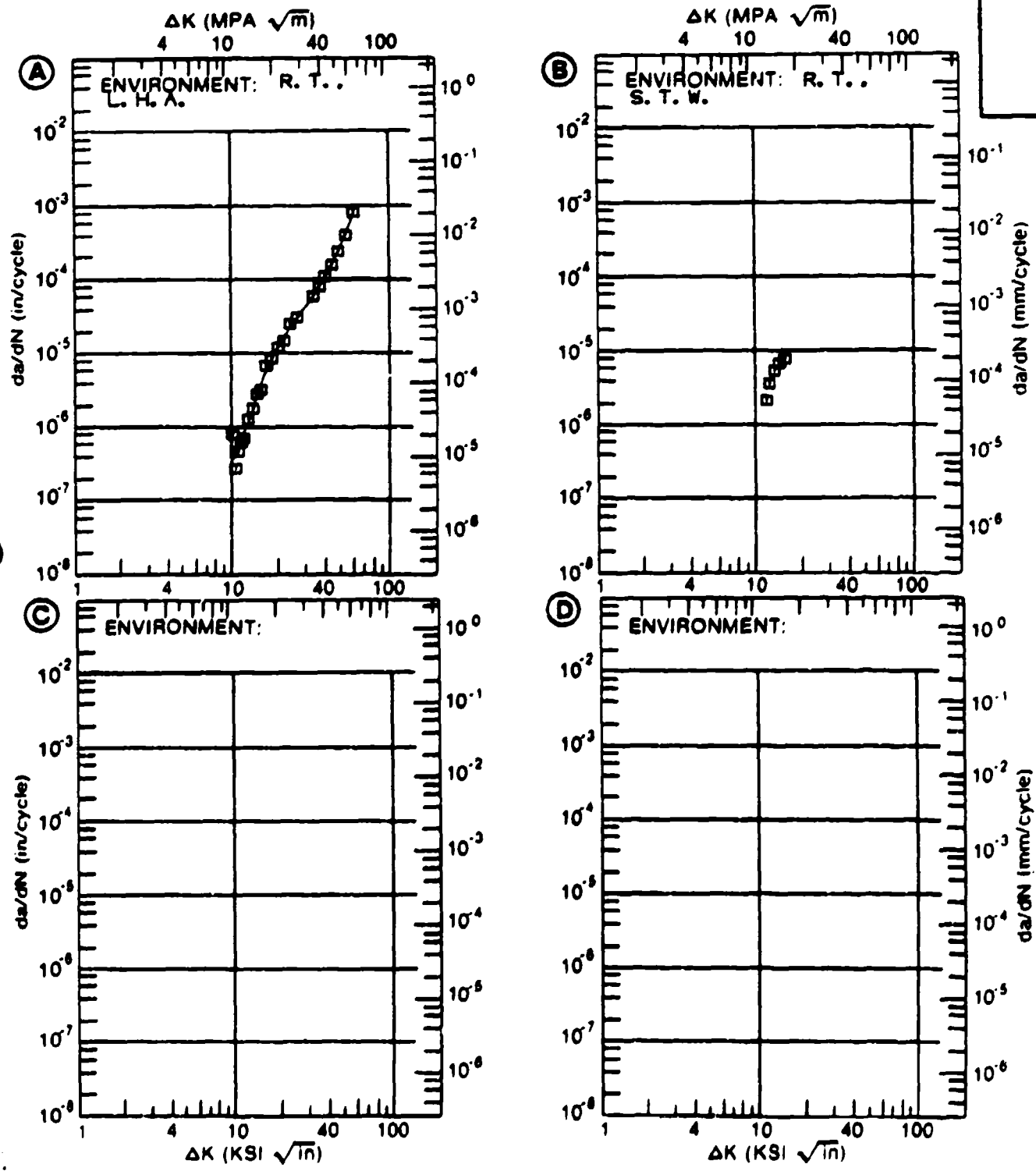


Figure 4.11.3.38

TABLE 4.11.3.39

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.39 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: DBTC

| DELTA K (KBI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|------|---|---|
| | A | B | C | D |
| | E= R. T. L. H. A. | | | |
| DELTA K MIN | A: 9.82 | .564 | | |
| | 10.00 | .567 | | |
| | 13.00 | 1.45 | | |
| | 16.00 | 4.82 | | |
| | 20.00 | 12.5 | | |
| | 25.00 | 24.0 | | |
| | 30.00 | 41.1 | | |
| | 35.00 | 69.5 | | |
| | 40.00 | 114. | | |
| | 50.00 | 278. | | |
| DELTA K MAX | A: 56.48 | 685. | | |
| | | | | |

ROOT MEAN SQUARE 14.29
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: DBTC
 FORM: 1.25" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.30
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 128.0 KSI
 ULT. STRENGTH: 138.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 8.000"
 REFERENCES: 98570

TITAN.
ALLOY

TI-6AL-
4V

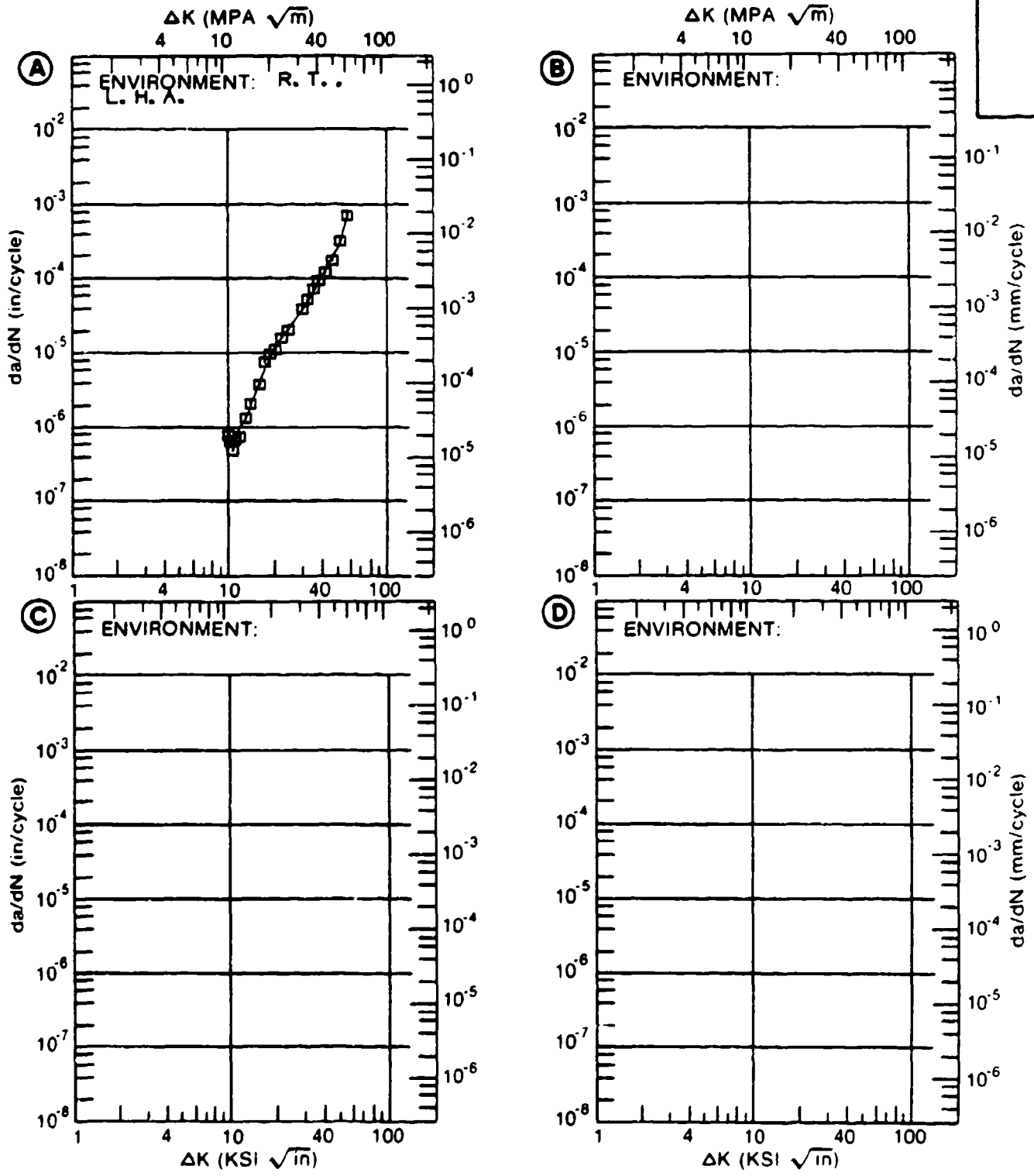


Figure 4.11.3.39

TABLE 4.11.3.40

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.40 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|------|---|---|
| CONDITION: DBTC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | S. T. W. | | | |
| DELTA K MIN | A: | 6.24 | .115 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 7.00 | .122 | | |
| | | 8.00 | .192 | | |
| | | 9.00 | .349 | | |
| | | 10.00 | .629 | | |
| | | 13.00 | 2.52 | | |
| | | 16.00 | 6.33 | | |
| DELTA K MAX | | 20.00 | 13.9 | | |
| | | 25.00 | 27.4 | | |
| | | 30.00 | 48.6 | | |
| | | 35.00 | 84.4 | | |
| | A: | 36.57 | 100. | | |
| | B: | | | | |
| | C: | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 33.64 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | 1 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DBTC
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 117.0 - 124.0 KSI
 ULT. STRENGTH: 129.0 - 138.0 KSI
 SPECIMEN THK: 0.990 - 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88578, 85837

TITAN.
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TI-6AL-
4V

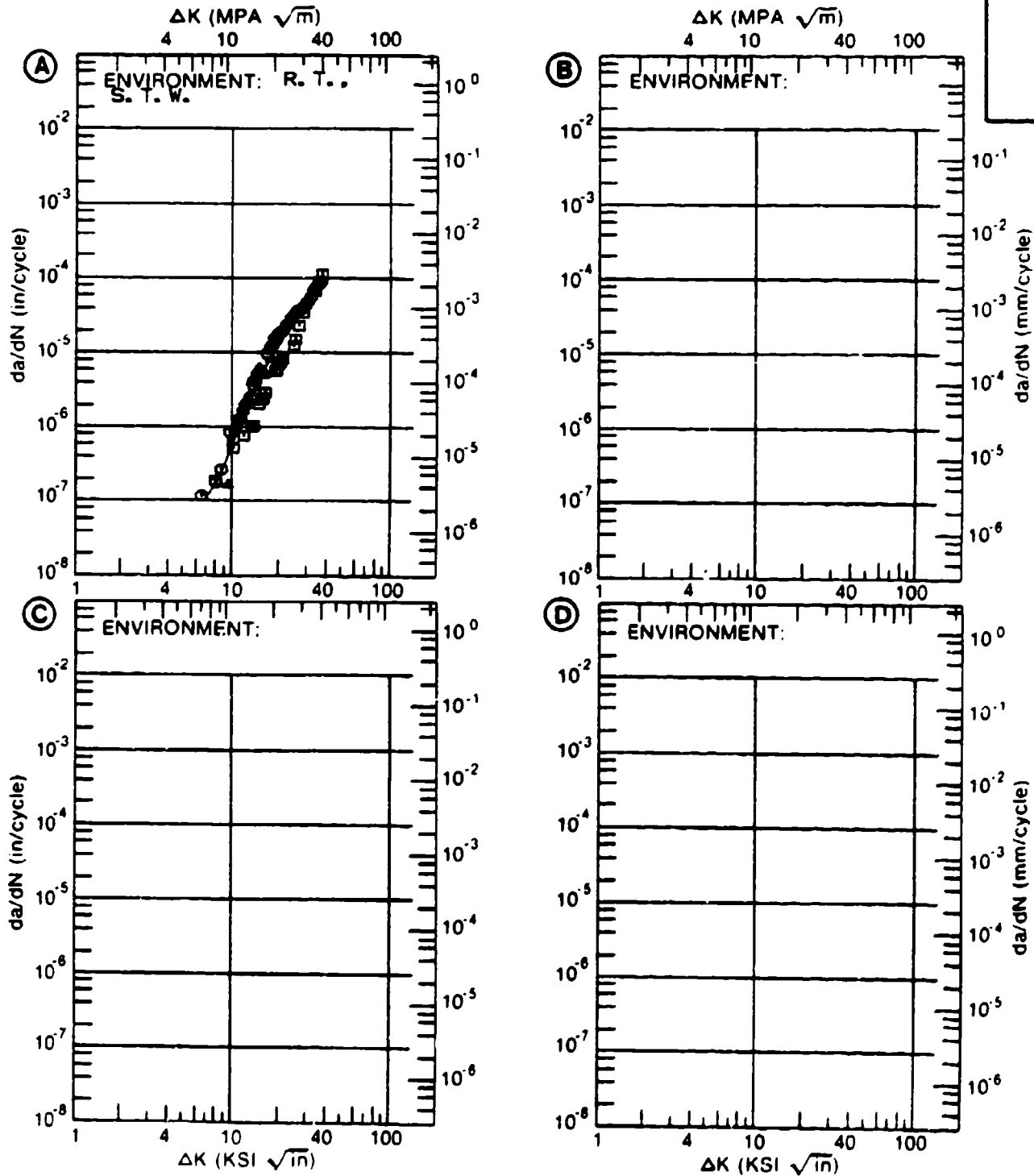


Figure 4.11.3.40

TABLE 4.11.3.41

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.41 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------|----------------------|---|---|
| CONDITION: DBTC | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. B. T. W. | | |
| DELTA K | A: 12.36 | .999 | | | |
| MIN | B: 9.01 | | 1.16 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | | 1.83 | | |
| | 13.00 | 1.31 | 4.86 | | |
| | 16.00 | 3.42 | 9.41 | | |
| | 20.00 | 7.70 | 18.4 | | |
| | 25.00 | 15.2 | 37.3 | | |
| | 30.00 | 26.0 | | | |
| | 35.00 | 41.9 | | | |
| | 40.00 | 66.5 | | | |
| | 50.00 | 169. | | | |
| DELTA K | A: 57.13 | 336. | | | |
| MAX | B: 29.65 | | 68.3 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 8.80 | 14.34 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 2 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DBTC
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 118.0- 125.0 KSI
 ULT. STRENGTH: 134.0- 135.0 KSI
 SPECIMEN THK: 0.960- 0.994"
 SPECIMEN WIDTH: 7.390- 7.460"
 REFERENCES: 88578, 85837

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4V

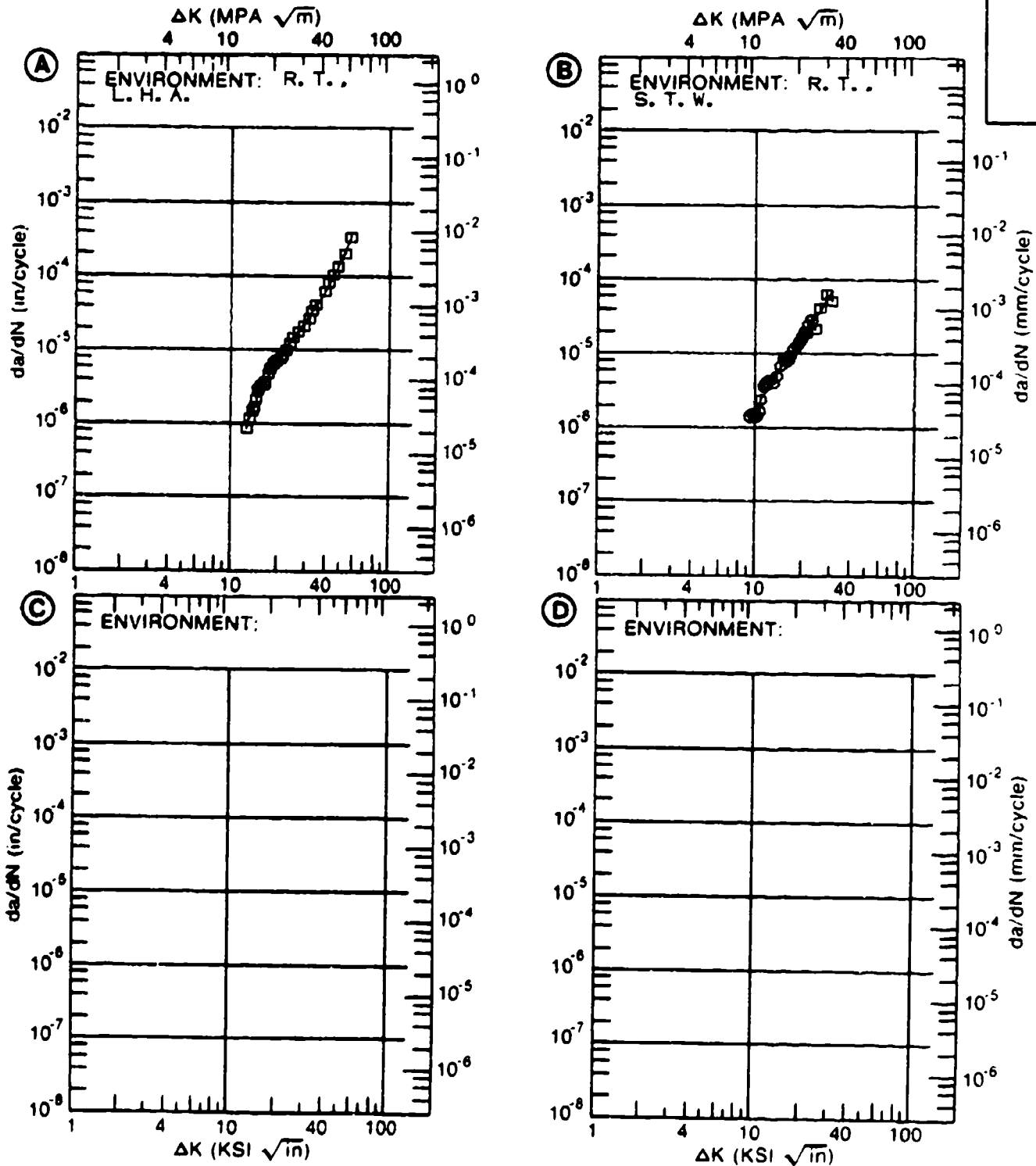


Figure 4.11.3.41

TABLE 4.11.3.42

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.42 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: DBTC

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. STW/JP4 | | | |
| DELTA K MIN | A: 9.95 | .448 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .450 | | | |
| | 13.00 | .892 | | | |
| | 16.00 | 2.13 | | | |
| | 20.00 | 5.48 | | | |
| | 25.00 | 14.0 | | | |
| | 30.00 | 27.0 | | | |
| DELTA K MAX | A: 32.61 | 33.8 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.81 | | | |
| PERCENT ERROR | | | | | |

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | |
| (NP/NA) | >2.0 | |

CONDITION/HT: DBTC
 FORM: 2.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 119.0 KSI
 ULT. STRENGTH: 132.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 4.940"
 REFERENCES: 89579

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 4V

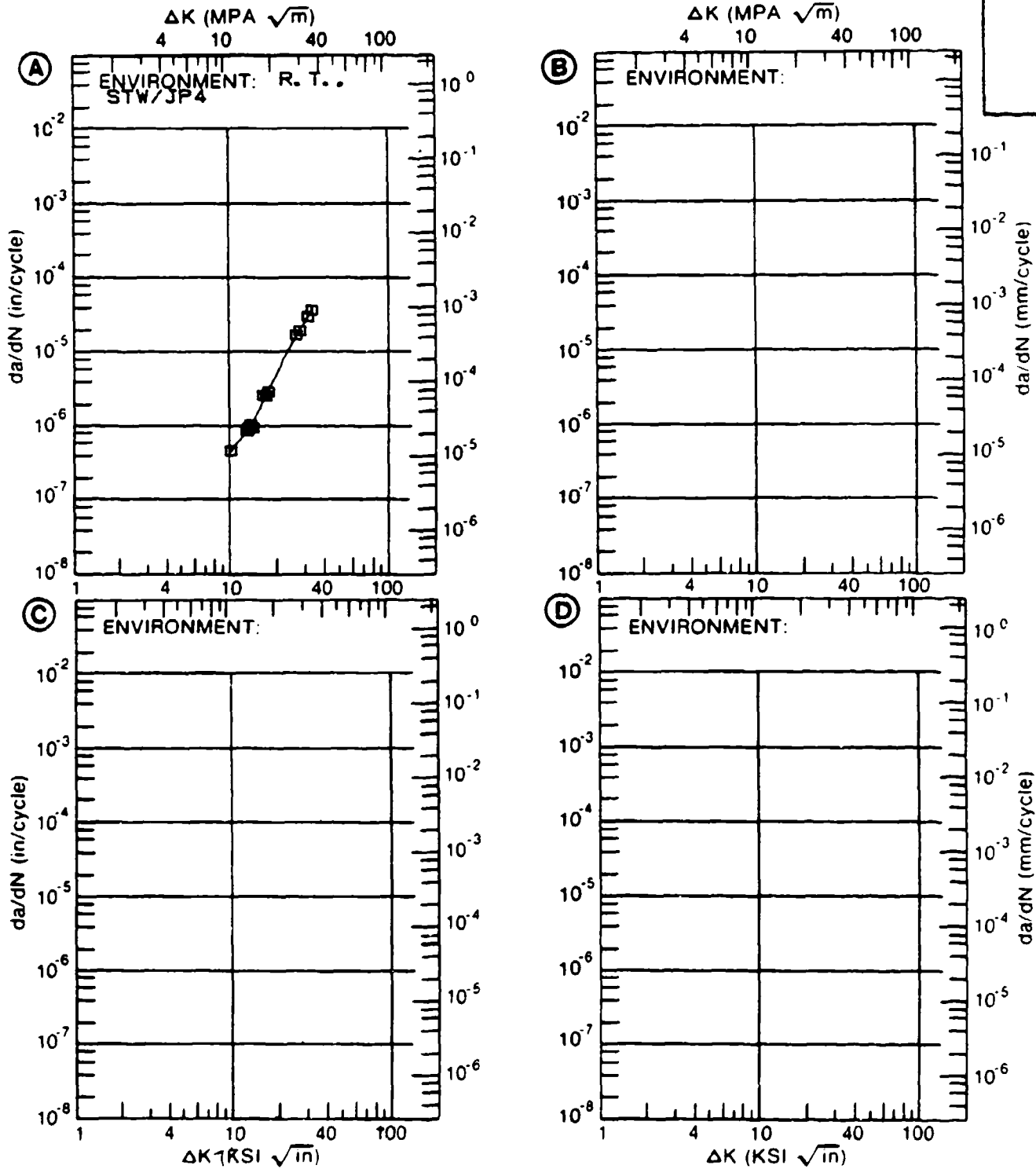


Figure 4.11.3.42

TABLE 4.11.3.43

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.43 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: DBTC(RA)
ENVIRONMENT: R. T. , L. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.30 | | | |
| DELTA K MIN | A: 30.88 | 57.1 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 35.00 | 116. | | | |
| | 40.00 | 182. | | | |
| DELTA K MAX | A: 40.98 | 198. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 13.89
PERCENT ERROR

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | |
| (NP/NA) | >2.0 | |

CONDITION/HT: DBTC (RA)
 FORM: 0.63" TH FLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 134.0 KSI
 ULT. STRENGTH: 145.0 KSI
 SPECIMEN THK: 0.500"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 86579

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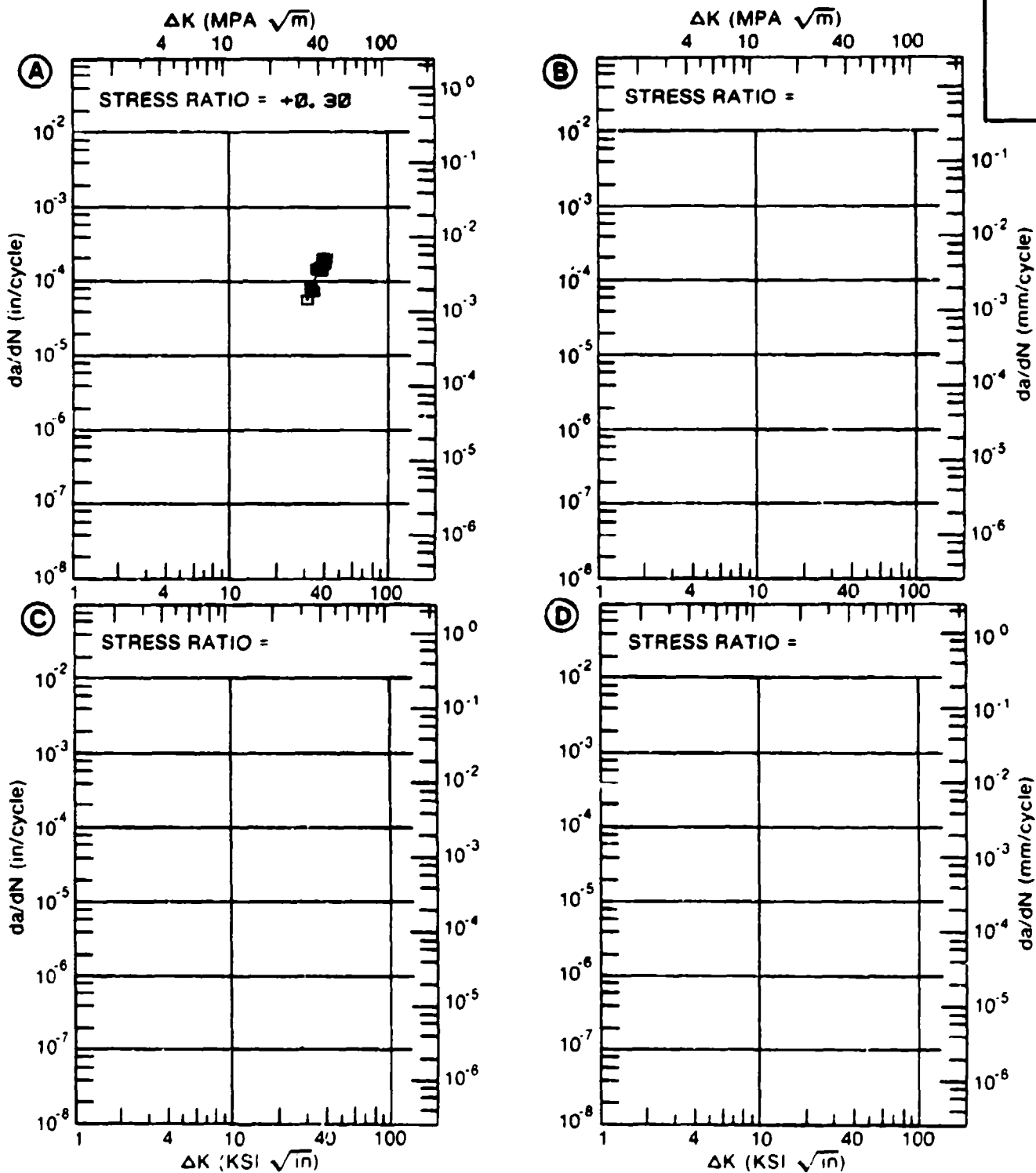


Figure 4.11.3.43

TABLE 4.11.3.44

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.44 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|----------|---------------------------|---------|---------|---|
| CONDITION: MA | | | | | |
| ENVIRONMENT: R. T. , L. H. A. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | R=+0.50 | |
| A: | 7.65 | .624 | | | |
| B: | 6.62 | | .529 | | |
| C: | 8.06 | | | .930 | |
| D: | | | | | |
| | 7.00 | | .504 | | |
| | 8.00 | .755 | .790 | | |
| | 9.00 | 1.21 | 1.44 | 1.53 | |
| | 10.00 | 1.79 | 2.24 | 2.30 | |
| | 13.00 | 4.27 | 4.98 | 5.34 | |
| | 16.00 | 7.75 | 7.91 | 9.87 | |
| | 20.00 | 13.7 | | 21.1 | |
| | 25.00 | 23.2 | | | |
| | 30.00 | 34.8 | | | |
| A: | 30.60 | 36.4 | | | |
| B: | 17.28 | | 9.32 | | |
| C: | 20.31 | | | 22.4 | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 12.56 | 13.85 | 4.35 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | 1 | 1 | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 0.10" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 6.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 137.0 KSI
 ULT. STRENGTH: 147.0 KSI
 SPECIMEN THK. 0.093- 0.101"
 SPECIMEN WIDTH: 23.980- 24.220"
 REFERENCES 86575

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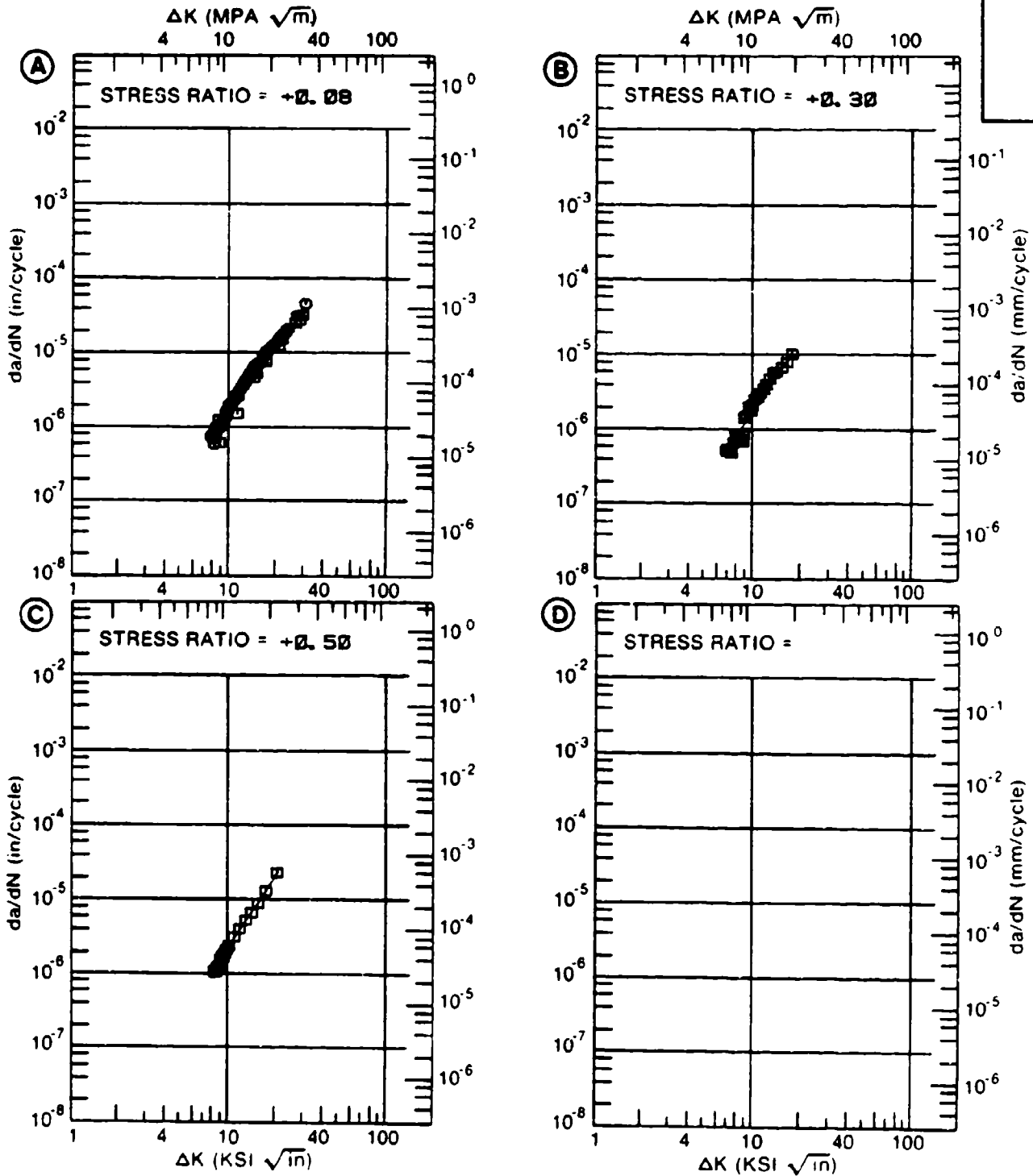


Figure 4.11.3.44

TABLE 4.11.3.45

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.45 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|------------------------------|-----------------------------|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. 1HZ | E= R. T. JP-4 FUEL 6HZ | E= R. T. S. T. W. 1HZ | |
| DELTA K | A: 9.64 | 1.36 | | | |
| MIN | B: 8.05 | | 1.10 | | |
| | C: 5.67 | | | .45 | |
| | D: | | | | |
| | 6.00 | | | .505 | |
| | 7.00 | | | .743 | |
| | 8.00 | | | 1.16 | |
| | 9.00 | | 1.23 | 1.91 | |
| | 10.00 | 1.57 | 1.47 | 3.22 | |
| | 13.00 | 4.02 | 2.88 | 15.0 | |
| | 16.00 | 7.47 | 5.82 | 30.2 | |
| | 20.00 | 12.9 | 12.9 | | |
| | 25.00 | | 24.2 | | |
| | 30.00 | | 30.2 | | |
| DELTA K | A: 24.57 | 19.3 | | | |
| MAX | B: 30.58 | | 30.3 | | |
| | C: 19.01 | | | 37.1 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 7.29 | 21.18 | 6.77 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 0.10" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 137.0 KSI
 ULT. STRENGTH: 147.0 KSI
 SPECIMEN THK: 0.002- 0.006"
 SPECIMEN WIDTH: 24.000"
 REFERENCES: 00575

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TI-6AL-
4V

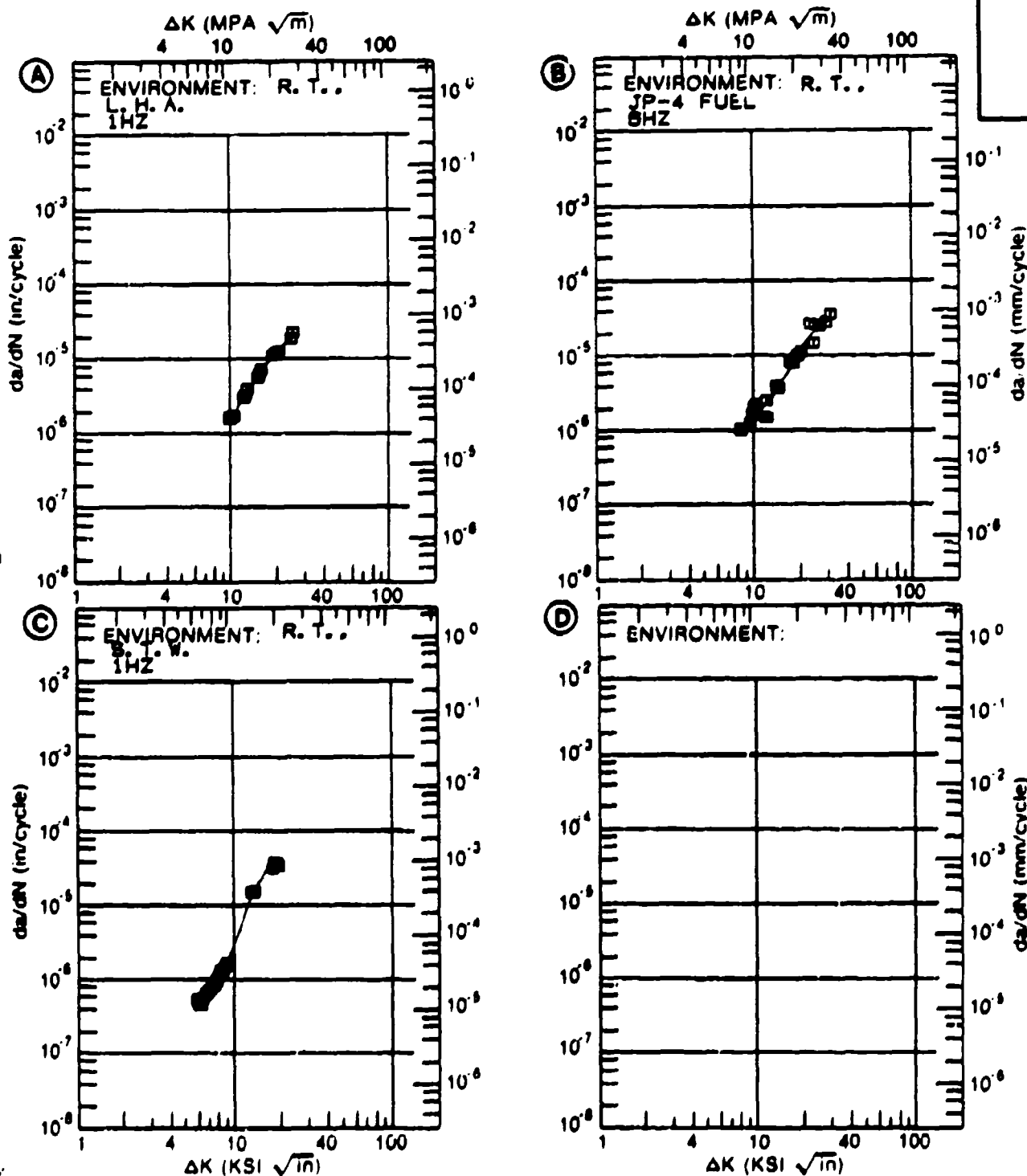


Figure 4.11.3.45

TABLE 4.11.3.46

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.46 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|--|---------------------------------------|----------------------|---|---|
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. S. T. W. | | |
| DELTA K MIN | A: 11.52 | 2.24 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 3.06 | | | |
| | 16.00 | 5.19 | | | |
| | 20.00 | 9.22 | | | |
| | 25.00 | 16.7 | | | |
| | 30.00 | 28.0 | | | |
| | 35.00 | 44.3 | | | |
| | 40.00 | 67.5 | | | |
| DELTA K MAX | A: 44.86 | 99.0 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 5.77 | 0.00 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | 1 | | |

CONDITION/HT: MA
 FORM: 0.10" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 8.00 HZ

YIELD STRENGTH: 143.0 KSI
 ULT. STRENGTH: 151.0 KSI
 SPECIMEN THK: 0.006- 0.007"
 SPECIMEN WIDTH: 24.000"
 REFERENCES: 88575

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4V

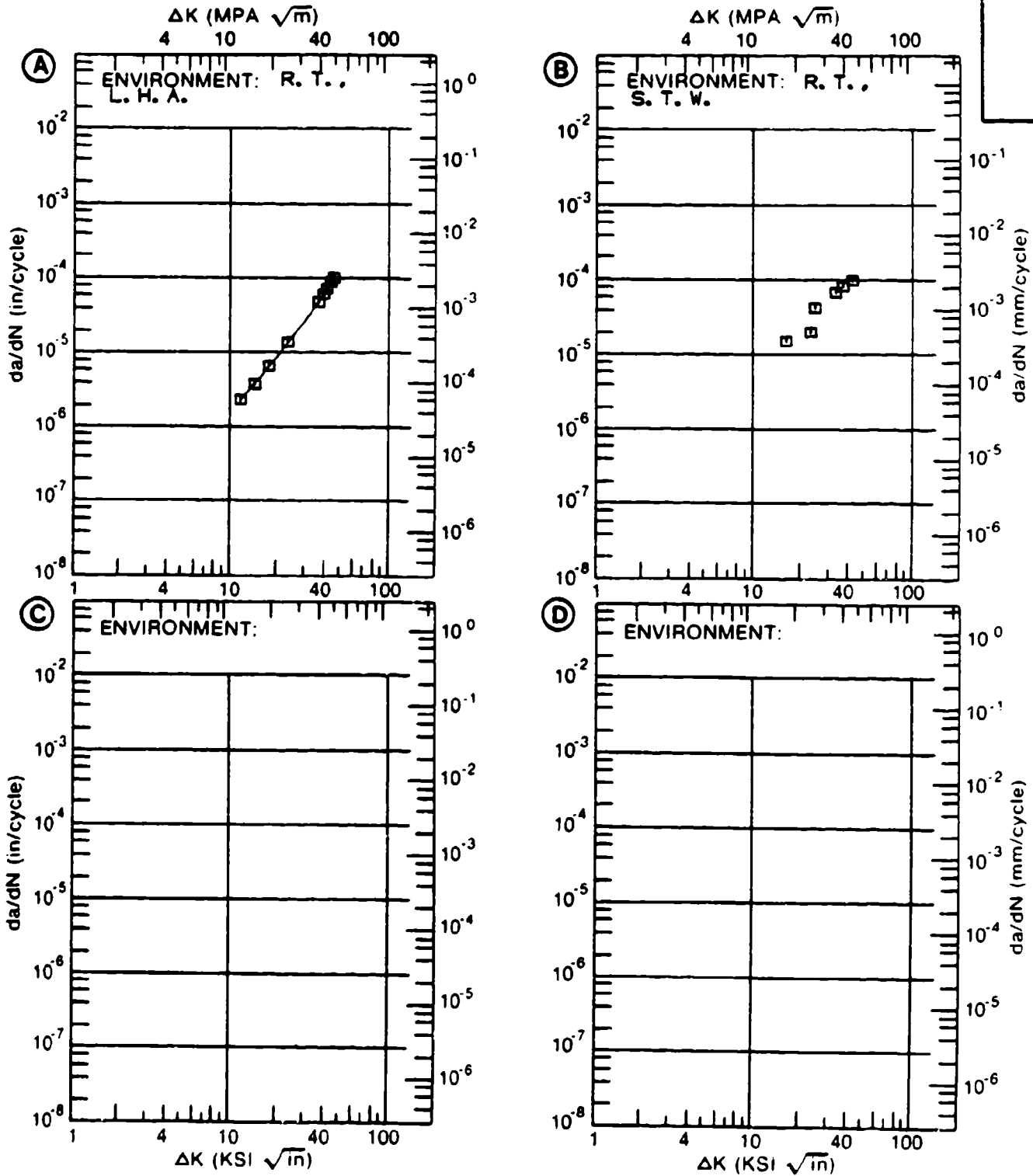


Figure 4.11.3.46

TABLE 4.11.3.47

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.47 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K | A: 4.82 | .0166 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | .0193 | | | |
| | 6.00 | .0414 | | | |
| | 7.00 | .0822 | | | |
| | 8.00 | .152 | | | |
| | 9.00 | .266 | | | |
| | 10.00 | .442 | | | |
| | 13.00 | 1.59 | | | |
| | 16.00 | 4.34 | | | |
| | 20.00 | 12.4 | | | |
| | 25.00 | 33.5 | | | |
| | 30.00 | 71.4 | | | |
| | 35.00 | 129. | | | |
| DELTA K | A: 38.83 | 185. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 27.55
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: MA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 0.10- 30.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 137.0 KSI
 ULT. STRENGTH: 145.0 KSI
 SPECIMEN THK: 0.241- 0.242"
 SPECIMEN WIDTH: 3.052- 3.053"
 REFERENCES: MA002

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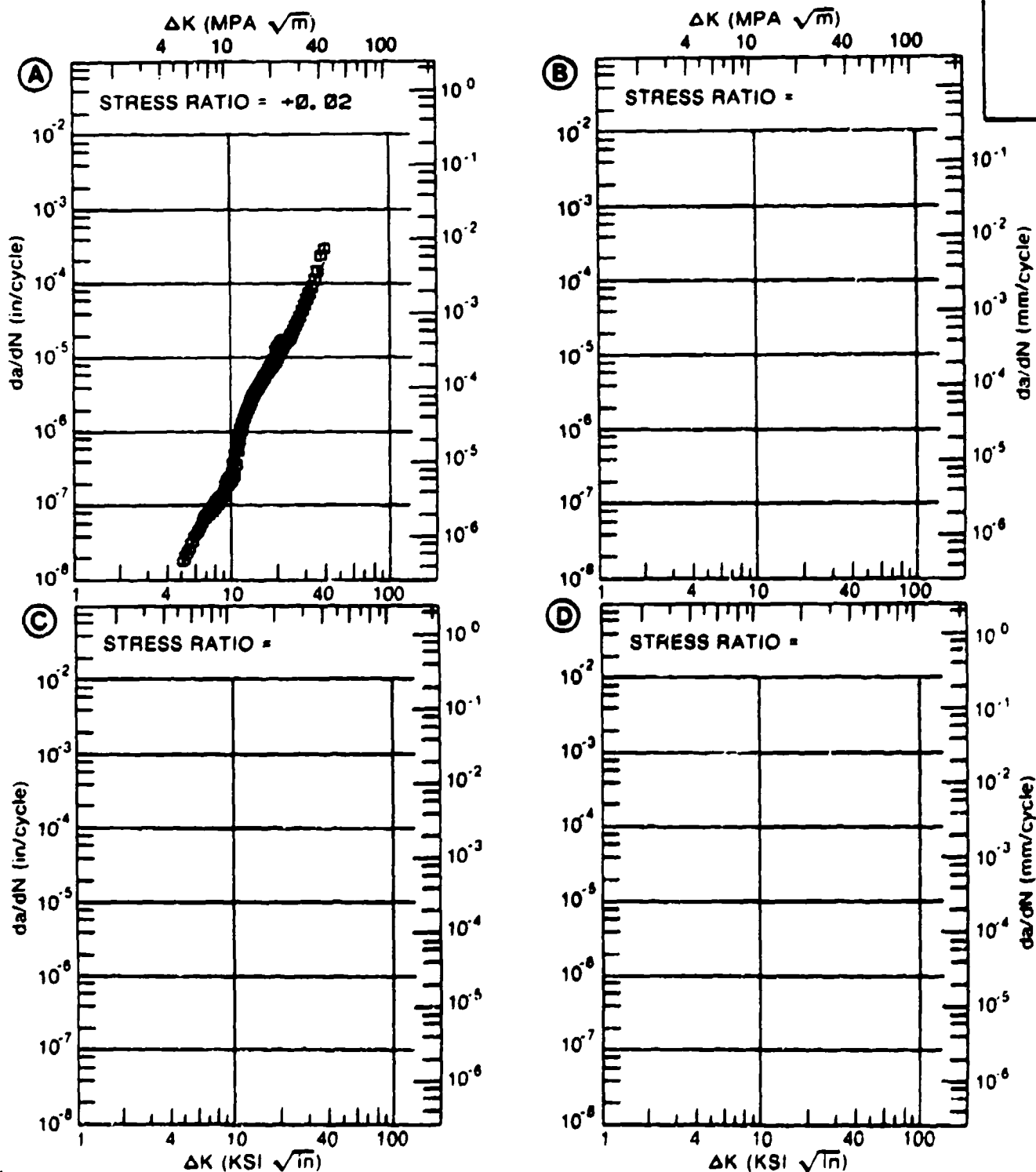


Figure 4.11.3.47

TABLE 4.11.3.48

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.48 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--|--|--|---|
| CONDITION: MA | | | | | |
| DELTA K (KBI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. SP. THK. = . 67" | E= R. T. L. H. A. SP. THK. = . 50" | E= R. T. S. T. W. SP. THK. = . 49" | |
| DELTA K | A: 26.05 | 144. | | | |
| MIN | B: 11.30 | | 4.69 | | |
| | C: 10.36 | | | 21.1 | |
| | D: | | | | |
| | 13.00 | | 8.27 | 33.8 | |
| | 16.00 | | 20.4 | 47.9 | |
| | 20.00 | | 72.6 | 87.5 | |
| | 25.00 | | 452. | | |
| | 30.00 | 313. | 2284. | | |
| | 35.00 | 679. | | | |
| DELTA K | A: 39.74 | 1469. | | | |
| MAX | B: 33.26 | | 3567. | | |
| | C: 23.71 | | | 198. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 7.55 | 17.55 | 22.03 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 0.83" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: $\rightarrow 0.30$
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 138.0 KSI
 ULT. STRENGTH: 148.0 KSI
 SPECIMEN THK:
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 88579

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 4V

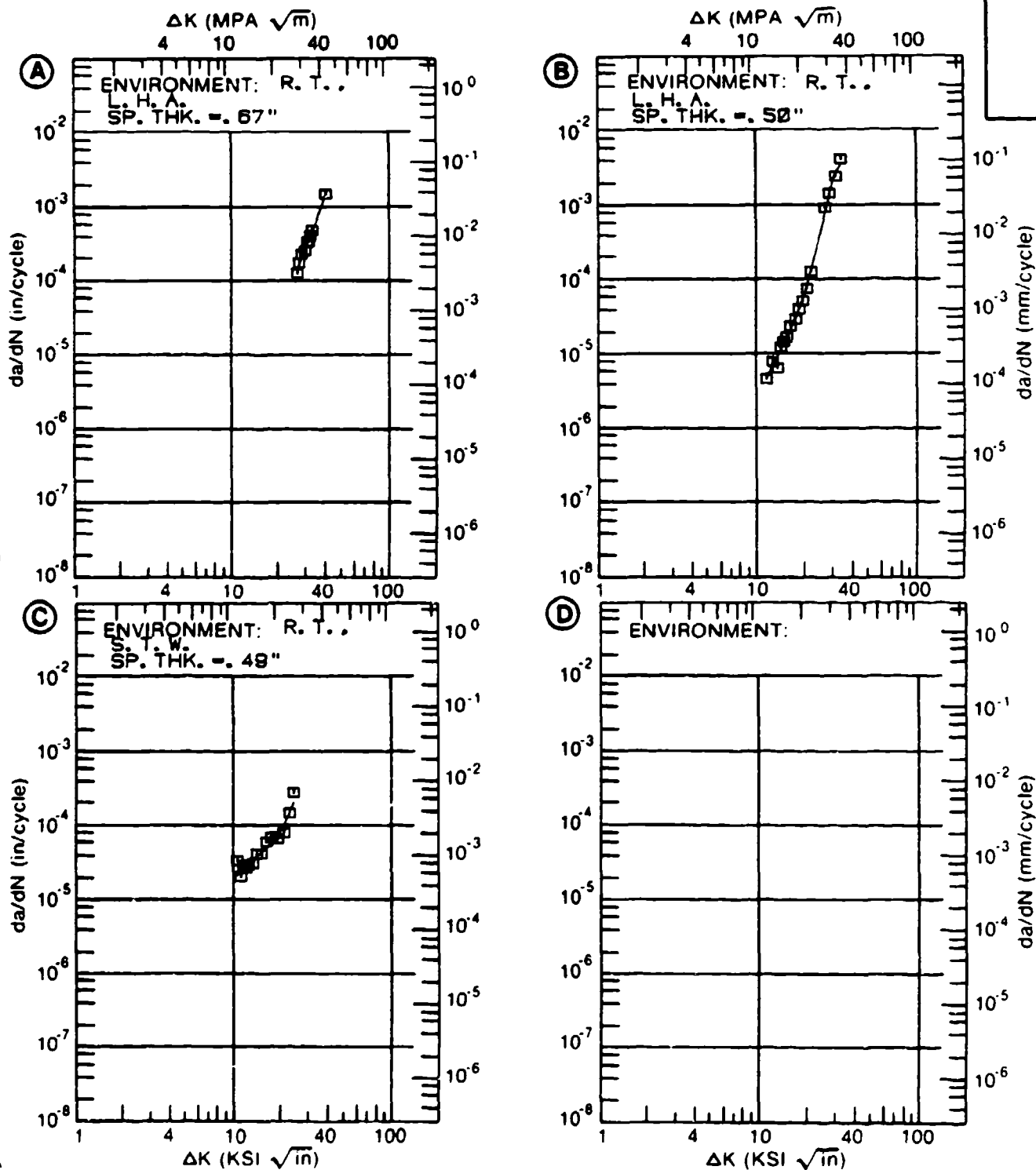


Figure 4.11.3.48

TABLE 4.11.3.49

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.49 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|----------|---------------------------------------|---------|---|---|
| CONDITION: MA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.05 | R=+0.30 | | |
| DELTA K | A: 11.31 | .313 | | | |
| MIN | B: 8.78 | | .342 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | | .429 | | |
| | 10.00 | | .995 | | |
| | 13.00 | .568 | 3.46 | | |
| | 16.00 | 2.98 | | | |
| | 20.00 | 6.97 | | | |
| | 25.00 | 9.80 | | | |
| | 30.00 | 13.8 | | | |
| | 35.00 | 25.4 | | | |
| DELTA K | A: 38.24 | 45.0 | | | |
| MAX | B: 14.23 | | 4.08 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 24.23 | 22.40 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | 1 | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 0.75" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 20.00 HZ
 ENVIRONMENT: R. T. LAB AIR

YIELD STRENGTH: 135.3 KSI
 ULT. STRENGTH: 137.6 KSI
 SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 2.500"
 REFERENCES: 00460

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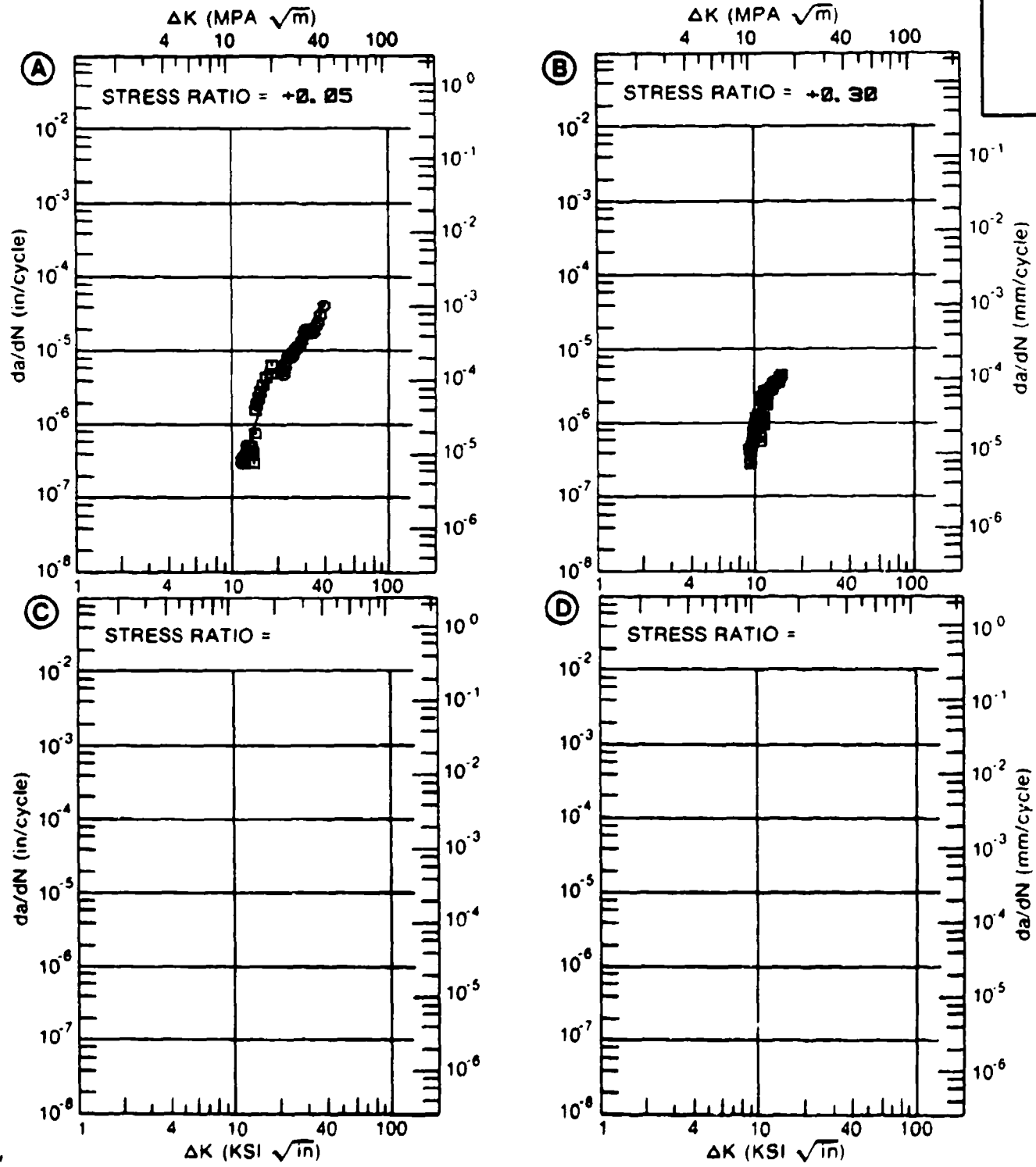


Figure 4.11.3.49

TABLE 4.11.3.50

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.50 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------|---|---|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | LAB AIR | | | |
| DELTA K | A: 31.29 | 17.0 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 35.00 | 25.5 | | | |
| | 40.00 | 39.6 | | | |
| | 50.00 | 96.5 | | | |
| DELTA K | A: 59.30 | 220. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 8.28 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 0.75" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.04
 FREQUENCY: 20.00 HZ

YIELD STRENGTH: 135.3 KSI
 ULT. STRENGTH: 137.6 KSI
 SPECIMEN THK: 0.290"
 SPECIMEN WIDTH: 6.011"
 REFERENCES: 88468

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TI-6AL-
4V

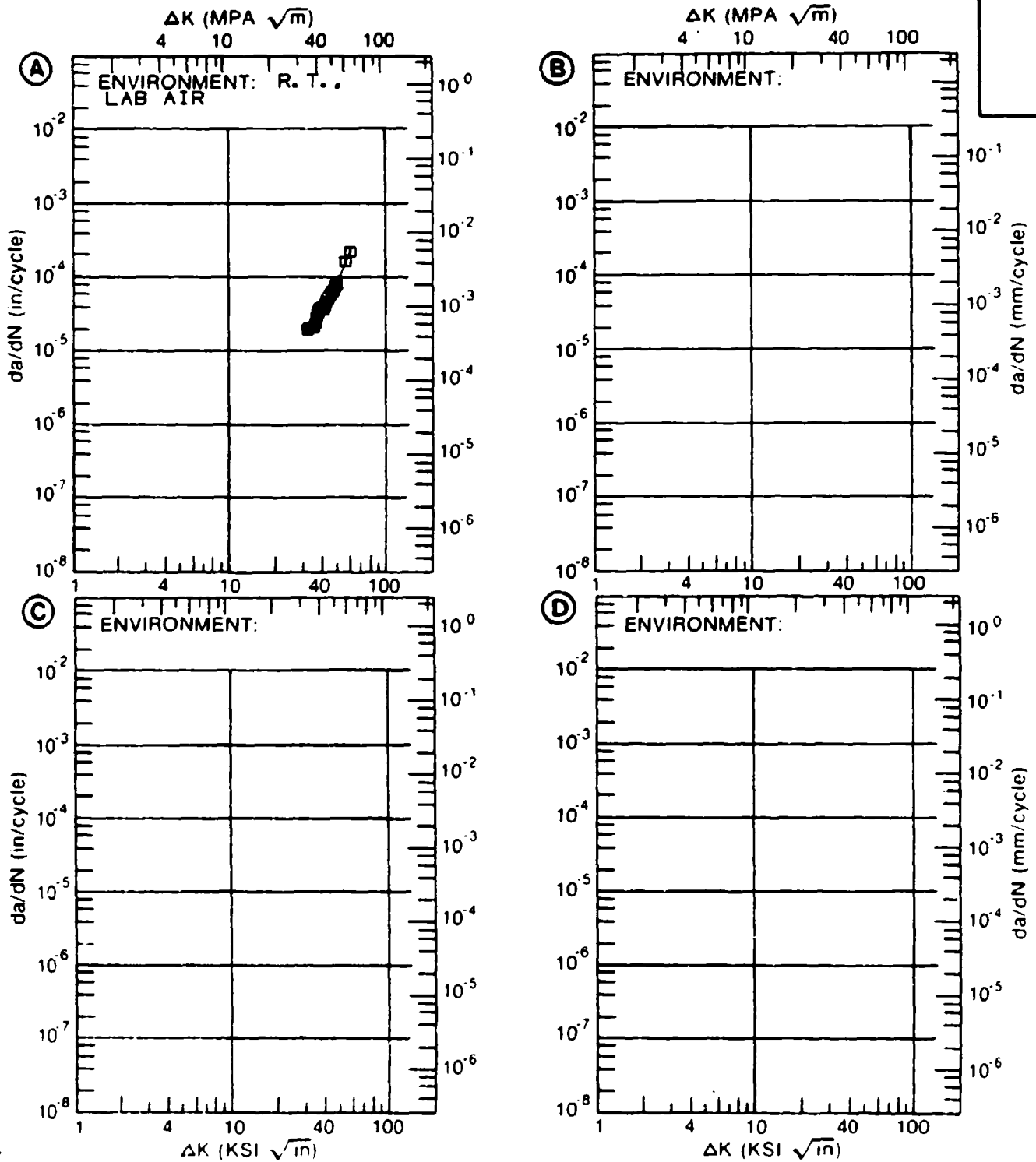


Figure 4.11.3.50

TABLE 4.11.3.51

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.51 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
|--------------------------|-------|--------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=-1.00 | R=+0.50 | | |
| DELTA K A: | 8.85 | .632 | | | |
| DELTA K B: | 5.43 | | .380 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 6.00 | | .734 | | |
| | 7.00 | | 1.77 | | |
| | 8.00 | | 3.40 | | |
| | 9.00 | .688 | 5.65 | | |
| | 10.00 | 1.14 | 8.52 | | |
| | 13.00 | 3.27 | 21.2 | | |
| | 16.00 | 6.55 | 41.9 | | |
| | 20.00 | 12.8 | 92.4 | | |
| | 25.00 | 24.8 | 206. | | |
| | 30.00 | 44.0 | 316. | | |
| | 35.00 | 75.3 | 381. | | |
| | 40.00 | 127. | 524. | | |
| | 50.00 | 328. | | | |
| | 60.00 | 724. | | | |
| | 70.00 | 1345. | | | |
| | 80.00 | 2115. | | | |
| | 90.00 | 2858. | | | |
| DELTA K A: | 92.48 | 3016. | | | |
| DELTA K B: | 49.27 | | 1688. | | |
| MAX C: | | | | | |
| D: | | | | | |

ROOT MEAN SQUARE 10.15 18.86
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: MA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 132.5 KSI
 ULT. STRENGTH: 138.0 KSI
 SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 4.000"
 REFERENCES: MA006

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TI-6AL-4V

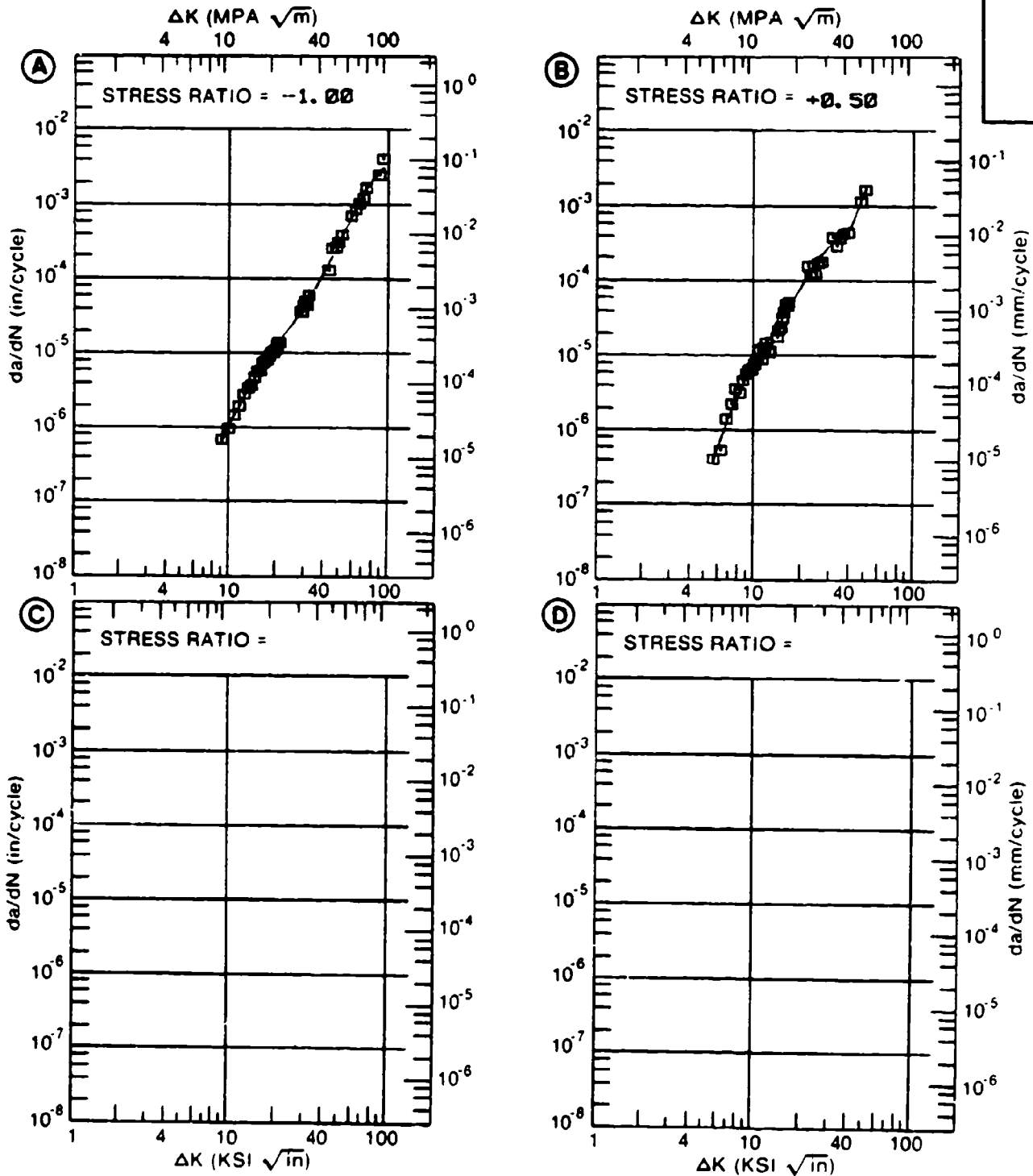


Figure 4.11.3.51

TABLE 4.11.3.52

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.52 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|----------|---|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E=- 65F | E=+ 175F | | |
| | | AIR | AIR | | |
| DELTA K | A: 25.62 | 26.3 | | | |
| MIN | B: 17.93 | | 8.57 | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | | 11.7 | | |
| | 25.00 | | 20.6 | | |
| | 30.00 | 55.6 | 31.8 | | |
| | 35.00 | 158. | 46.5 | | |
| | 40.00 | 1500. | 66.6 | | |
| | 50.00 | | 135. | | |
| | 60.00 | | 280. | | |
| DELTA K | A: 41.96 | 5475. | | | |
| MAX | B: 65.73 | | 429. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 39.40 | 11.28 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 00144

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TI-6AL-
4V

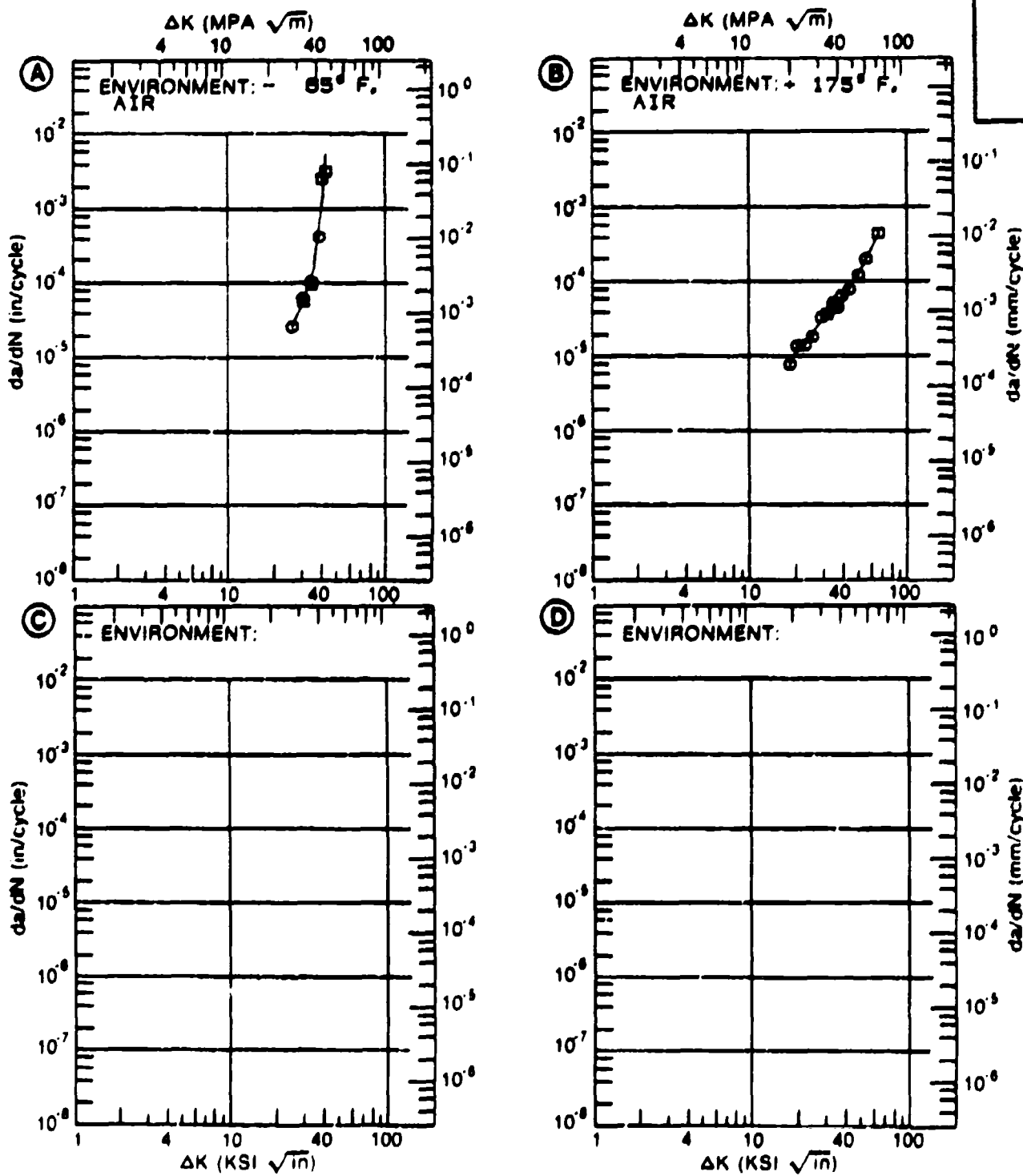


Figure 4.11.3.52

TABLE 4.11.3.53

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.53 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|-----------------------------|---|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. 1-6HZ | E= R. T. S. T. W. 1HZ | | |
| DELTA K | A: 6.95 | .123 | | | |
| MIN | B: 8.19 | | .441 | | |
| | C: | | | | |
| | D: | | | | |
| | 7.00 | .127 | | | |
| | 8.00 | .203 | | | |
| | 9.00 | .286 | .436 | | |
| | 10.00 | .415 | .589 | | |
| | 13.00 | 2.22 | 2.89 | | |
| | 16.00 | 9.87 | 11.3 | | |
| | 20.00 | 24.7 | 31.5 | | |
| | 25.00 | 38.2 | 58.6 | | |
| | 30.00 | 49.7 | 77.8 | | |
| | 35.00 | 68.7 | | | |
| | 40.00 | 109. | | | |
| | 50.00 | 402. | | | |
| DELTA K | A: 55.67 | 771. | | | |
| MAX | B: 32.78 | | 84.7 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 14.83 | 22.37 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | 1 | | |
| RATIO | 0.8-1.25 | 2 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 1.25" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.30
 FREQUENCY:

YIELD STRENGTH: 120.0 KSI
 ULT. STRENGTH: 134.0 KSI
 SPECIMEN THK: 0.990- 0.997"
 SPECIMEN WIDTH: 6.000- 6.010"
 REFERENCES: 05837

| |
|-----------------|
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| TI-6AL- 4V |
| |

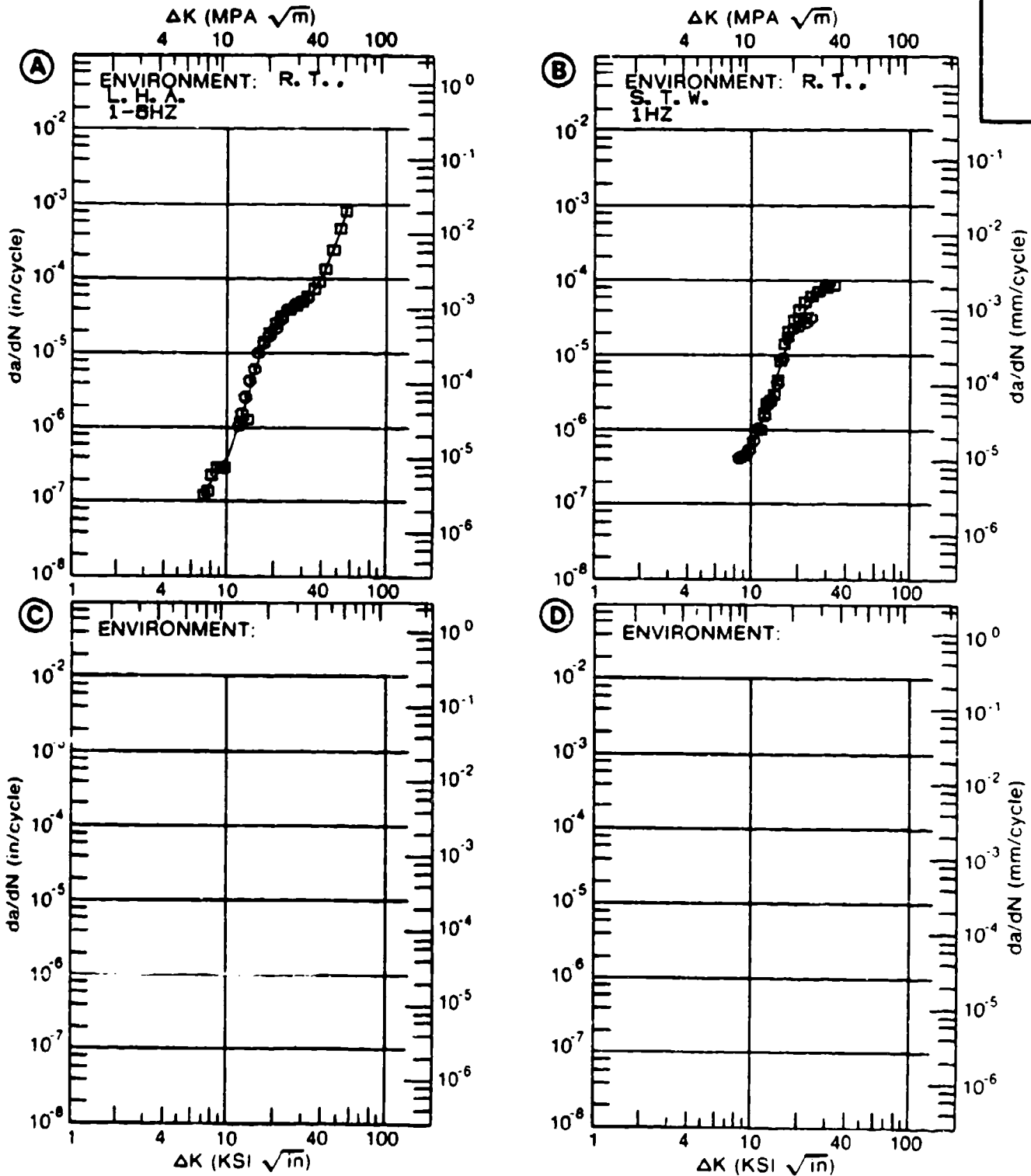


Figure 4.11.3.53

TABLE 4.11.3.54

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.54 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA
ENVIRONMENT: R. T. , L. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|-------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.30 | | | |
| A: | 6.36 | .14 | | | |
| DELTA K B: | | | | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 7.00 | .147 | | | |
| | 8.00 | .195 | | | |
| | 9.00 | .293 | | | |
| | 10.00 | .460 | | | |
| | 13.00 | 1.63 | | | |
| | 16.00 | 4.30 | | | |
| | 20.00 | 11.2 | | | |
| | 25.00 | 26.4 | | | |
| | 30.00 | 48.3 | | | |
| | 35.00 | 75.9 | | | |
| | 40.00 | 113. | | | |
| | 50.00 | 255. | | | |
| A: | 58.57 | 557. | | | |
| DELTA K B: | | | | | |
| MAX C: | | | | | |
| D: | | | | | |

ROOT MEAN SQUARE 12.47
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: MA
 FORM: 1.5" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00- 6.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 120.1 KSI
 ULT. STRENGTH: 134.1 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 8.000"
 REFERENCES: 94301

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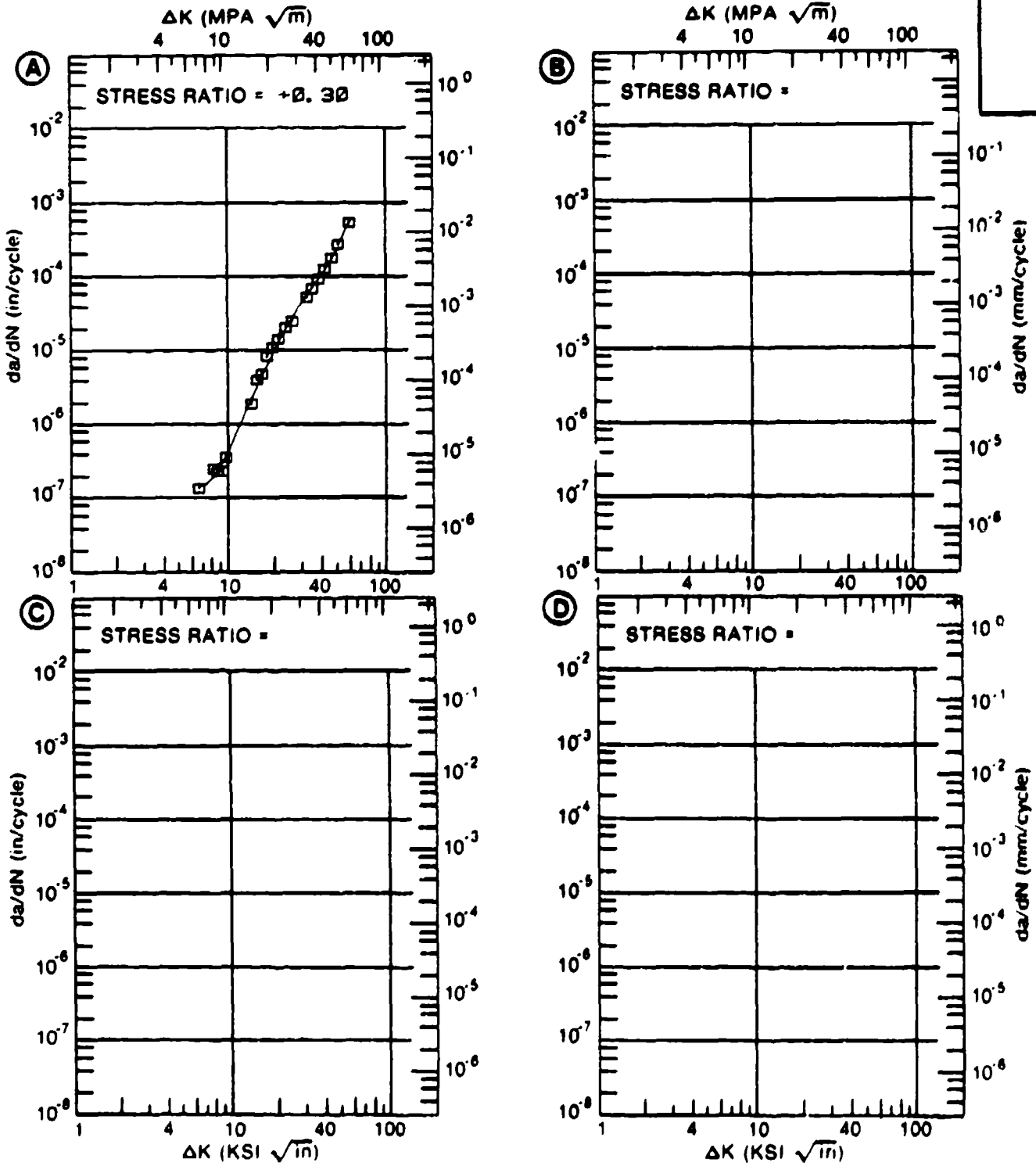


Figure 4.11.3.54

TABLE 4.11.3.55

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.55 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: MA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K MIN | A: 5.91 | .0335 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | .0340 | | | |
| | 7.00 | .0448 | | | |
| | 8.00 | .0653 | | | |
| | 9.00 | .0996 | | | |
| | 10.00 | .154 | | | |
| | 13.00 | .554 | | | |
| DELTA K MAX | A: 44.29 | 171. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 1.71 | | | |
| | 20.00 | 5.92 | | | |
| | 25.00 | 19.4 | | | |
| | 30.00 | 46.1 | | | |
| | 35.00 | 86.0 | | | |
| | 40.00 | 133. | | | |
| ROOT MEAN SQUARE | | 35.86 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 0.10- 30.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 133.0 KSI
 ULT. STRENGTH: 142.0 KSI
 SPECIMEN THK: 0.188- 0.191"
 SPECIMEN WIDTH: 3.957- 3.964"
 REFERENCES: MA002

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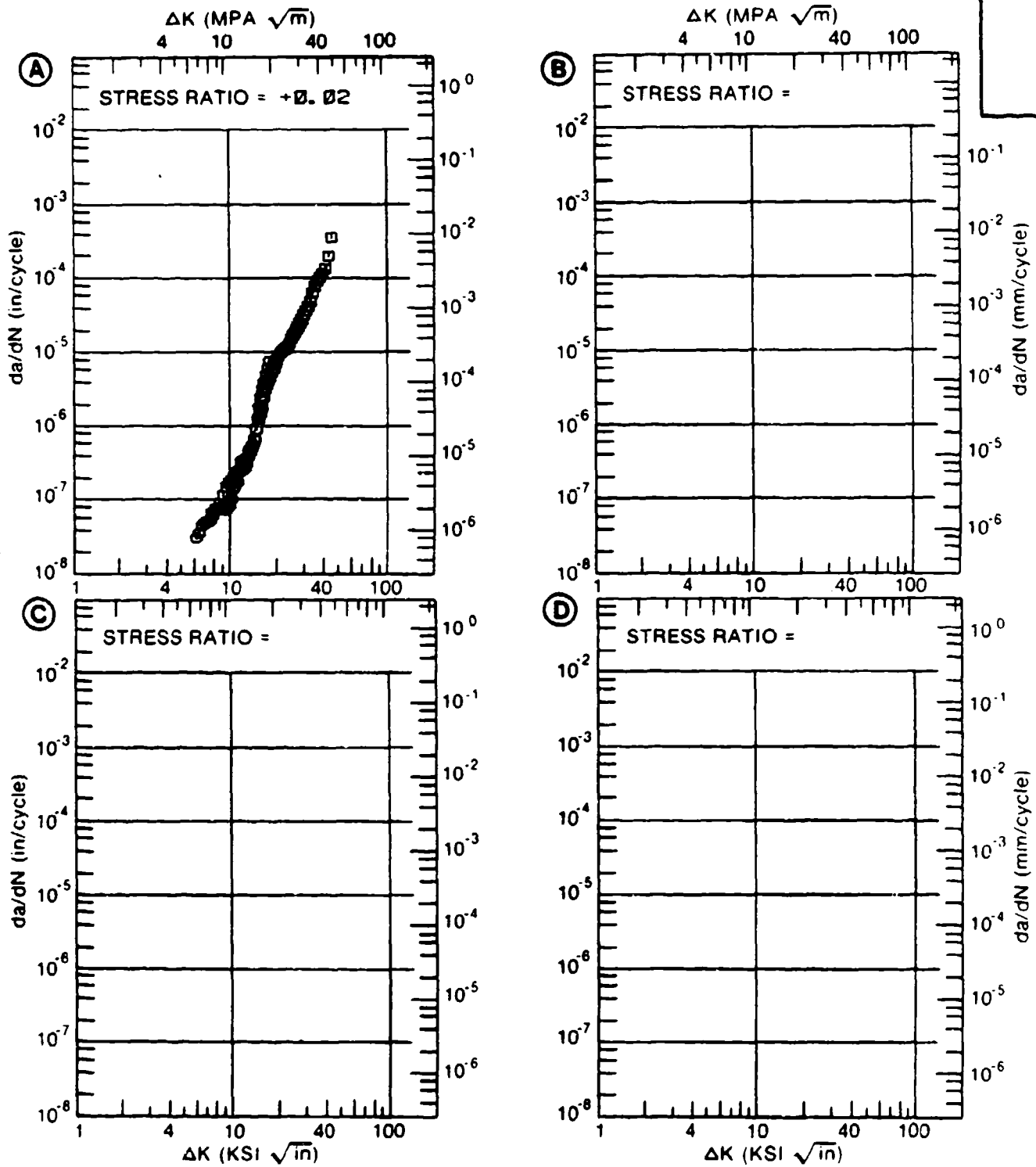


Figure 4.11.3.55

TABLE 4.11.3.56

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.56 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA
ENVIRONMENT: R. T. , L. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|-------|--------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | R=+0.50 | |
| A: | 7.76 | .147 | | | |
| DELTA K B: | 11.48 | | 1.20 | | |
| MIN C: | 10.32 | | | 1.70 | |
| D: | | | | | |
| | 8.00 | .161 | | | |
| | 9.00 | .241 | | | |
| | 10.00 | .373 | | | |
| | 13.00 | 1.36 | 3.31 | 5.53 | |
| | 16.00 | 4.04 | 9.32 | 9.75 | |
| | 20.00 | 11.7 | 16.8 | 17.3 | |
| | 25.00 | 25.9 | 38.1 | 47.0 | |
| | 30.00 | 36.2 | 66.0 | 94.0 | |
| A: | 34.01 | 36.7 | | | |
| DELTA K B: | 30.00 | | 66.0 | | |
| MAX C: | 30.83 | | | 94.6 | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 21.28 | 14.01 | 8.00 | |
| PERCENT ERROR | | | | | |

| | | | | |
|------------|----------|---|---|---|
| LIFE | 0.0-0.5 | | | |
| PREDICTION | 0.5-0.8 | | | |
| RATIO | 0.8-1.25 | 2 | 1 | 1 |
| SUMMARY | 1.25-2.0 | | | |
| (NP/NA) | >2.0 | | | |

CONDITION/HT: MA
 FORM: EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 8.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 122.0- 123.5 KSI
 ULT. STRENGTH: 135.5- 139.0 KSI
 SPECIMEN THK: 0.003- 0.007"
 SPECIMEN WIDTH: 3.770- 4.040"
 REFERENCES 95837

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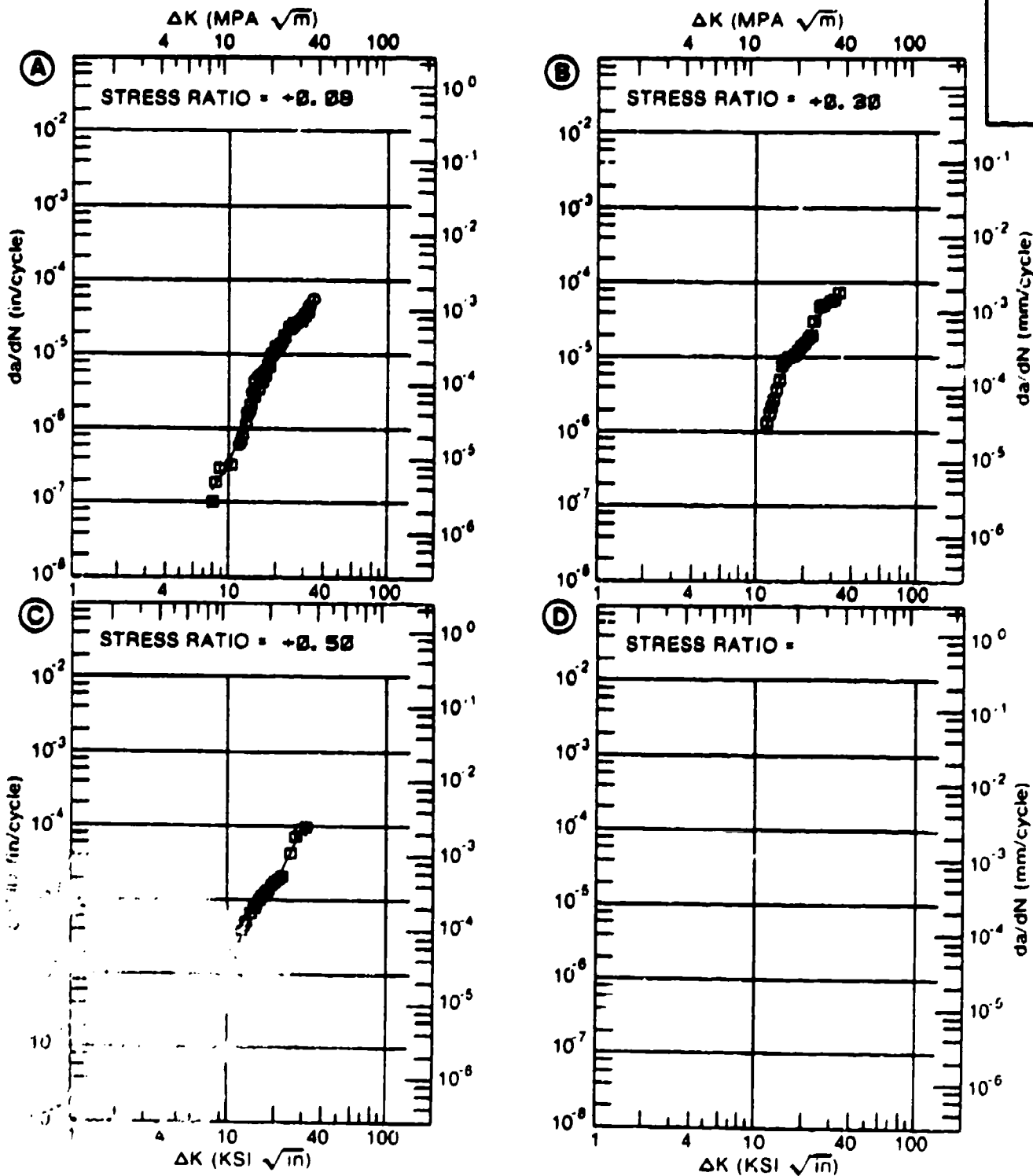


Figure 4.11.3.56

TABLE 4.11.3.57

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.57 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|--------------------------------------|---------------------|----------------------|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. J. P. 4 | E= R. T. S. T. W. | |
| DELTA K MIN | A: 13.17 | 1.51 | | | |
| | B: 18.10 | | 8.27 | | |
| | C: 11.48 | | | 1.35 | |
| | D: | | | | |
| | 13.00 | | | 1.82 | |
| | 16.00 | 5.07 | | 5.04 | |
| | 20.00 | 13.9 | 12.0 | 14.3 | |
| | 25.00 | 28.7 | 25.1 | 32.4 | |
| | 30.00 | 46.5 | 43.5 | 53.9 | |
| | 35.00 | 68.2 | 68.4 | 80.4 | |
| | 40.00 | 97.1 | 103. | 117. | |
| | 50.00 | | | 266. | |
| DELTA K MAX | A: 42.59 | 116. | | | |
| | B: 46.81 | | 171. | | |
| | C: 51.63 | | | 308. | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 13.77 | 3.38 | 8.04 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | 1 | 1 | |

CONDITION/HT: MA
 FORM: EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 123.5- 127.0 KSI
 ULT. STRENGTH: 135.5- 139.0 KSI
 SPECIMEN THK: 0.994- 1.000"
 SPECIMEN WIDTH: 3.770"
 REFERENCES: 85837, 88579

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TI-6AL-
4V

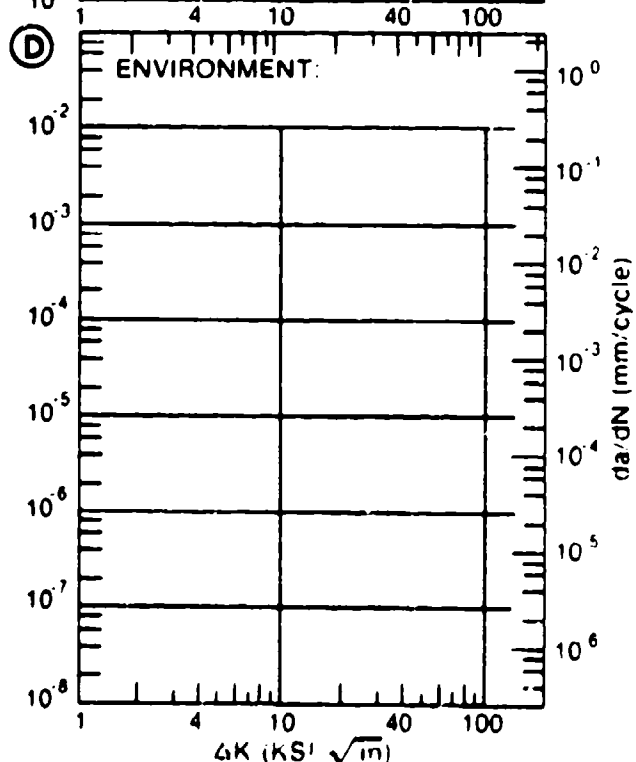
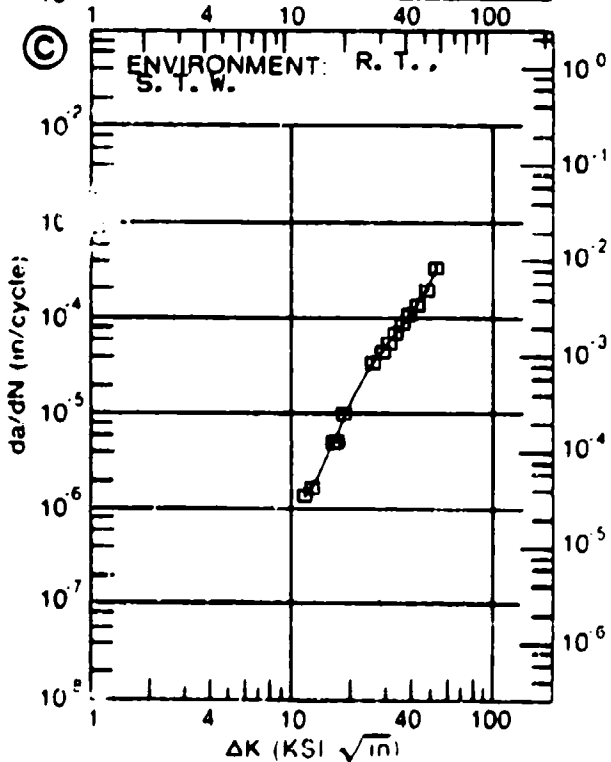
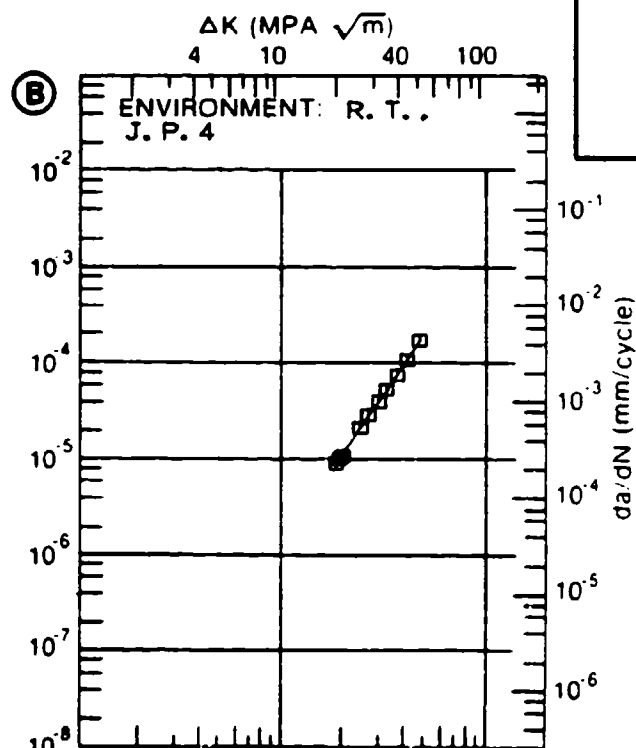
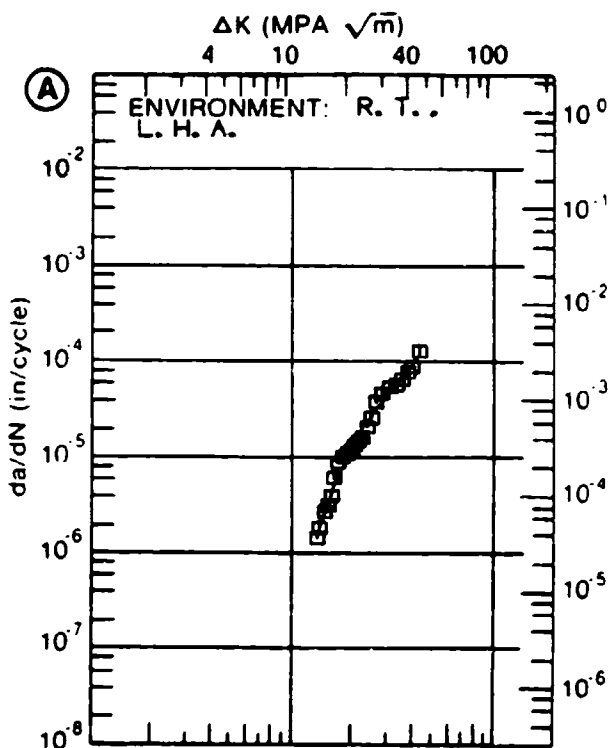


Figure 4.11.3.57

TABLE 4.11.3.58

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.58 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|-----------------------------|---|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. 6HZ | E= R. T. S. T. W. 6HZ | | |
| DELTA K | A: 13.81 | 1.76 | | | |
| MIN | B: 9.22 | | .428 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | | .620 | | |
| | 13.00 | | 1.97 | | |
| | 16.00 | 5.21 | 4.67 | | |
| | 20.00 | 12.7 | 11.1 | | |
| | 25.00 | 15.9 | 24.8 | | |
| | 30.00 | 36.0 | 45.1 | | |
| | 35.00 | | 71.6 | | |
| DELTA K | A: 32.77 | 90.6 | | | |
| MAX | B: 39.27 | | 98.5 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.43 | 6.59 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 125.0 KSI
 ULT. STRENGTH: 142.0 KSI
 SPECIMEN THK: 0.994"
 SPECIMEN WIDTH: 3.770"
 REFERENCES: 85837

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TI-6AL-
4V

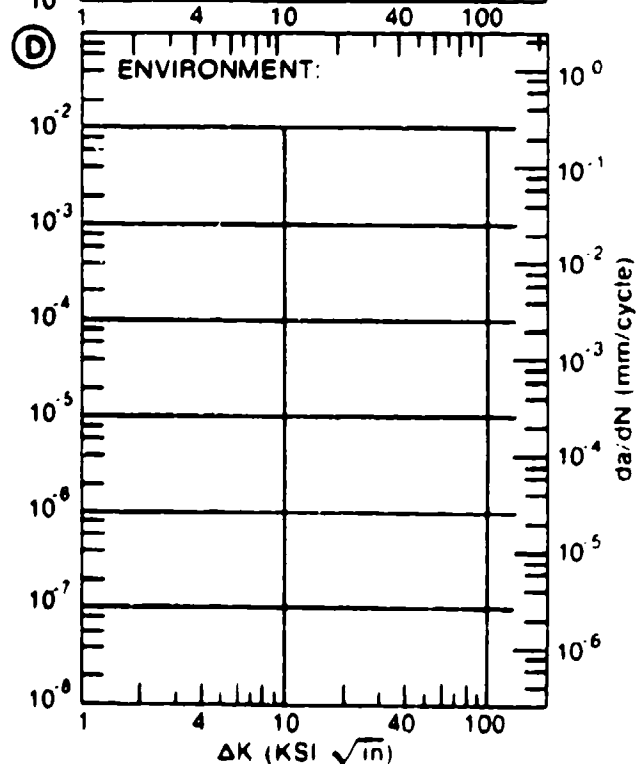
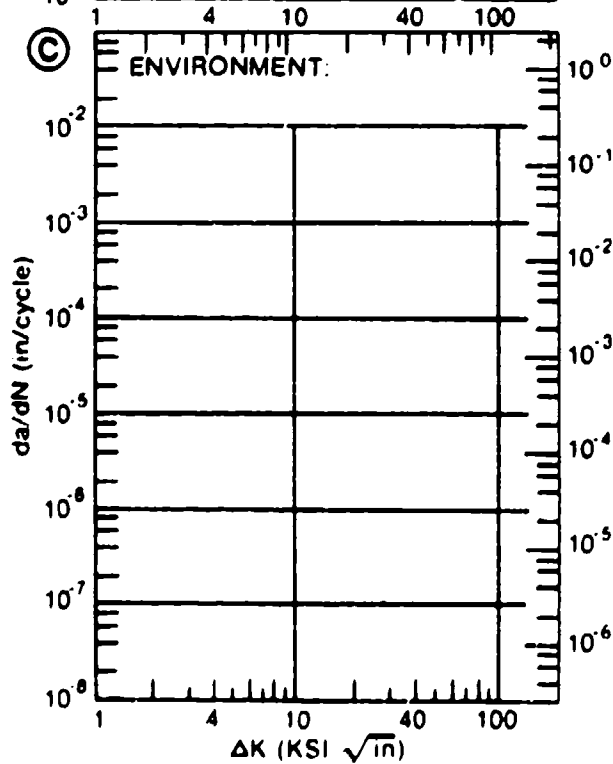
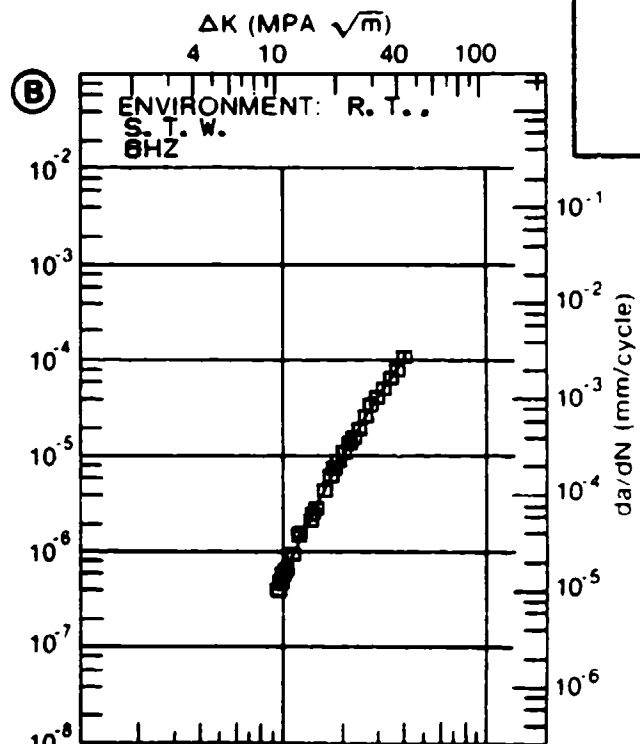
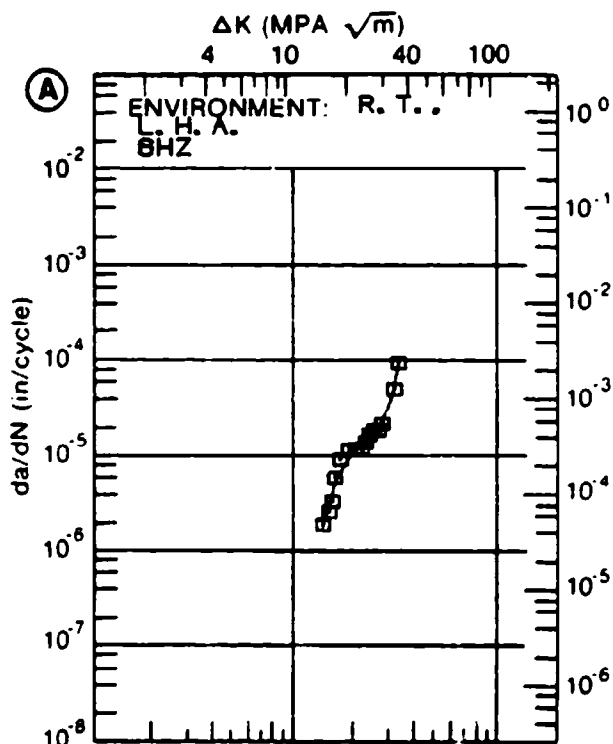


Figure 4.11.3.58

TABLE 4.11.3.59

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.59 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|--------------------------------|--------------------------------------|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR 1-20HZ | E= R. T. S. T. W. 1-10HZ | E= R. T. SIM. SEA WATER 1-10HZ | |
| DELTA K A: | 12.95 | .690 | | | |
| DELTA K B: | 10.86 | | 1.21 | | |
| MIN C: | 10.22 | | | .987 | |
| D: | | | | | |
| | 13.00 | .712 | 2.42 | 2.42 | |
| | 16.00 | 3.12 | 5.16 | 4.84 | |
| | 20.00 | 9.50 | 11.2 | 9.69 | |
| | 25.00 | 21.0 | 23.9 | 19.3 | |
| | 30.00 | 35.6 | 43.9 | 34.5 | |
| | 35.00 | 55.1 | 73.8 | 58.5 | |
| | 40.00 | 83.7 | 116. | 95.9 | |
| | 50.00 | 202. | 254. | 242. | |
| | 60.00 | 548. | 496. | 580. | |
| | 70.00 | 1660. | | | |
| DELTA K A: | 74.97 | 2988. | | | |
| DELTA K B: | 60.69 | | 518. | | |
| MAX C: | 66.66 | | | 1019. | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 18.14 | 27.52 | 31.04 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | 2 | 2 | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 1.00" TH EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 124.4 KSI
 ULT. STRENGTH: 135.3 KSI
 SPECIMEN THK: 1.000- 1.003"
 SPECIMEN WIDTH: 4.500"
 REFERENCES: NC002

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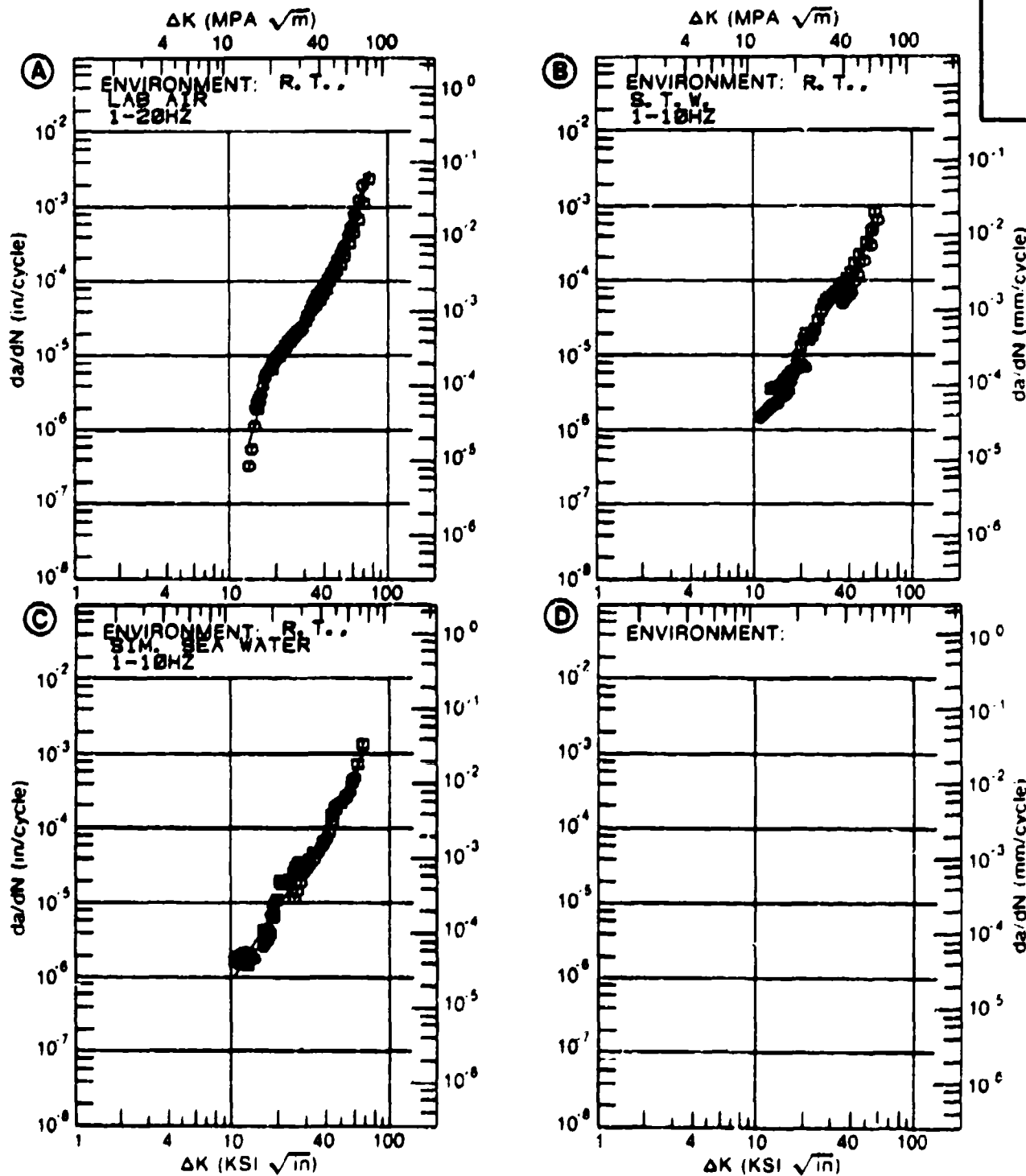


Figure 4.11.3.50

TABLE 4.11.3.60

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.60 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|-------------------------------|--------------------------------|--------------------------------------|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR 5-20HZ | E= R. T. S. T. W. 1-10HZ | E= R. T. SIM. SEA WATER 1-10HZ | |
| DELTA K | A: 11.73 | 1.23 | | | |
| MIN | B: 10.98 | | 2.31 | | |
| | C: 10.52 | | | 2.98 | |
| | D: | | | | |
| | 13.00 | 2.34 | 4.93 | 3.88 | |
| | 16.00 | 6.39 | 11.3 | 9.08 | |
| | 20.00 | 13.7 | 25.9 | 18.0 | |
| | 25.00 | 24.8 | 47.7 | 31.2 | |
| | 30.00 | 39.5 | 67.3 | 47.3 | |
| | 35.00 | 61.7 | 90.6 | 69.1 | |
| | 40.00 | 98.6 | 128. | 100. | |
| | 50.00 | 281. | 324. | 220. | |
| | 60.00 | | | 538. | |
| DELTA K | A: 59.40 | 863. | | | |
| MAX | B: 56.74 | | 737. | | |
| | C: 63.55 | | | 874. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.97 | 17.66 | 28.94 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | 1 | |
| RATIO | 0.8-1.25 | 2 | 2 | | |
| SUMMARY | 1.25-2.0 | | | 1 | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 1.00" TH EXTRUSION
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 126.6 KSI
 ULT. STRENGTH: 138.6 KSI
 SPECIMEN THK: 1.000-1.003"
 SPECIMEN WIDTH: 4.500"
 REFERENCES: NC002

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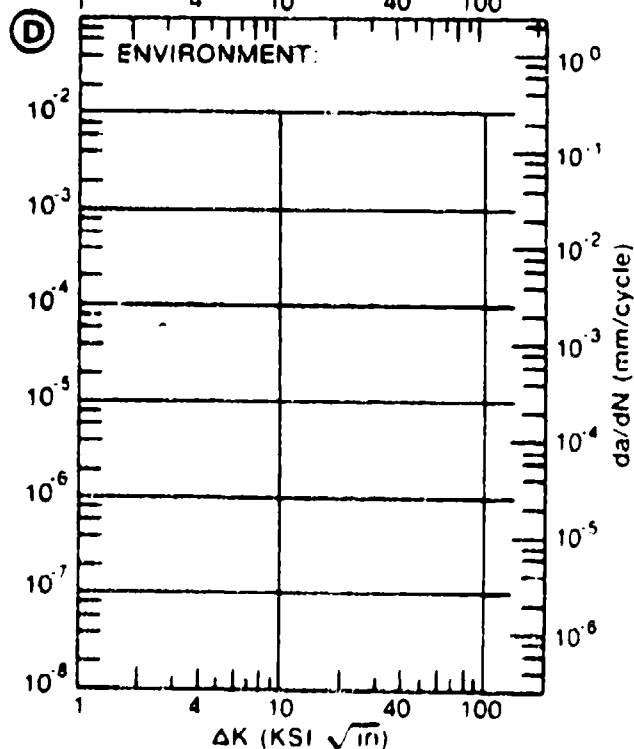
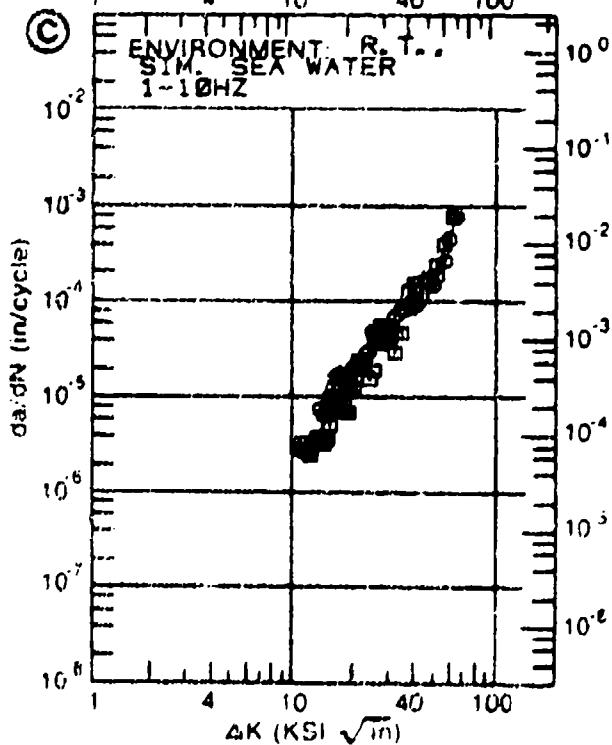
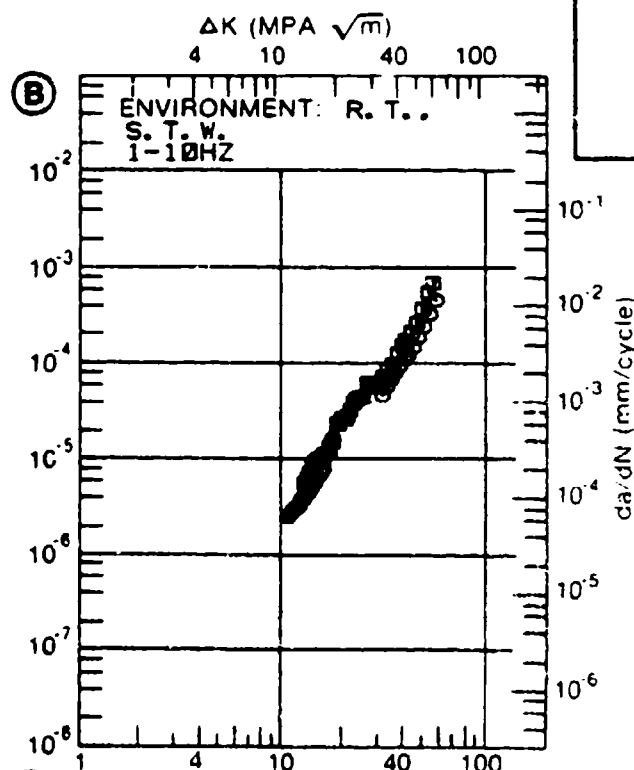
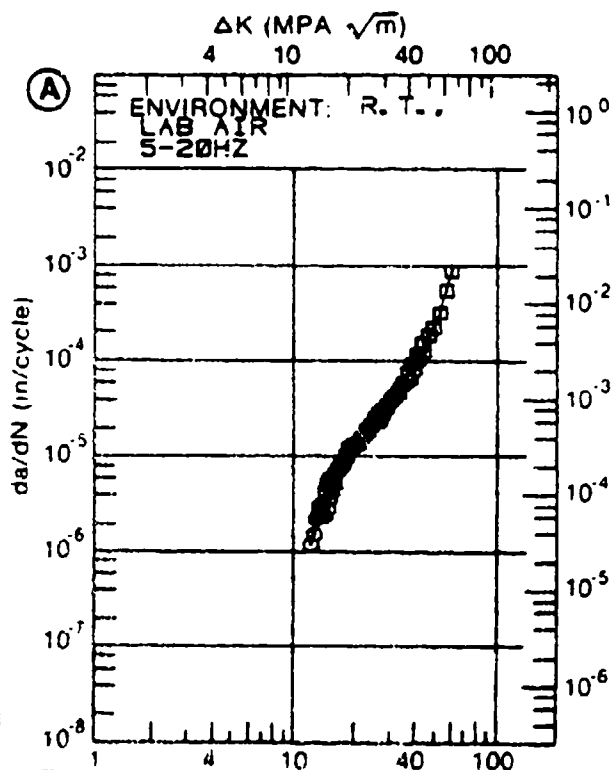


Figure 4.11.3.69

TABLE 4.11.3.61

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.61 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------------|----------|--------------------------------------|--------------------------------|---------------------------------------|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON 10HZ | E= R. T. DRY AIR 08-10HZ | E= R. T. SIMULATED FUEL 09-10HZ | |
| DELTA K B: | 15.25 | | 5.87 | | |
| MIN C: | 13.51 | | | 2.61 | |
| D: | | | | | |
| | 16.00 | | 7.15 | 5.95 | |
| | 20.00 | | 15.6 | 14.2 | |
| | 25.00 | | 30.9 | 31.1 | |
| | 30.00 | | 55.5 | 63.1 | |
| | 35.00 | | 99.4 | 130. | |
| | 40.00 | | 183. | 280. | |
| | 50.00 | | 696. | 1513. | |
| DELTA K B: | 51.67 | | 882. | | |
| MAX C: | 51.36 | | | 1932. | |
| D: | | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 0.00 | 59.69 | 39.37 | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: DCB
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 FREQUENCY:

YIELD STRENGTH: 127.0- 145.0 KSI
 ULT. STRENGTH: 190.0- 198.0 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 5.500"
 REFERENCES: 04300

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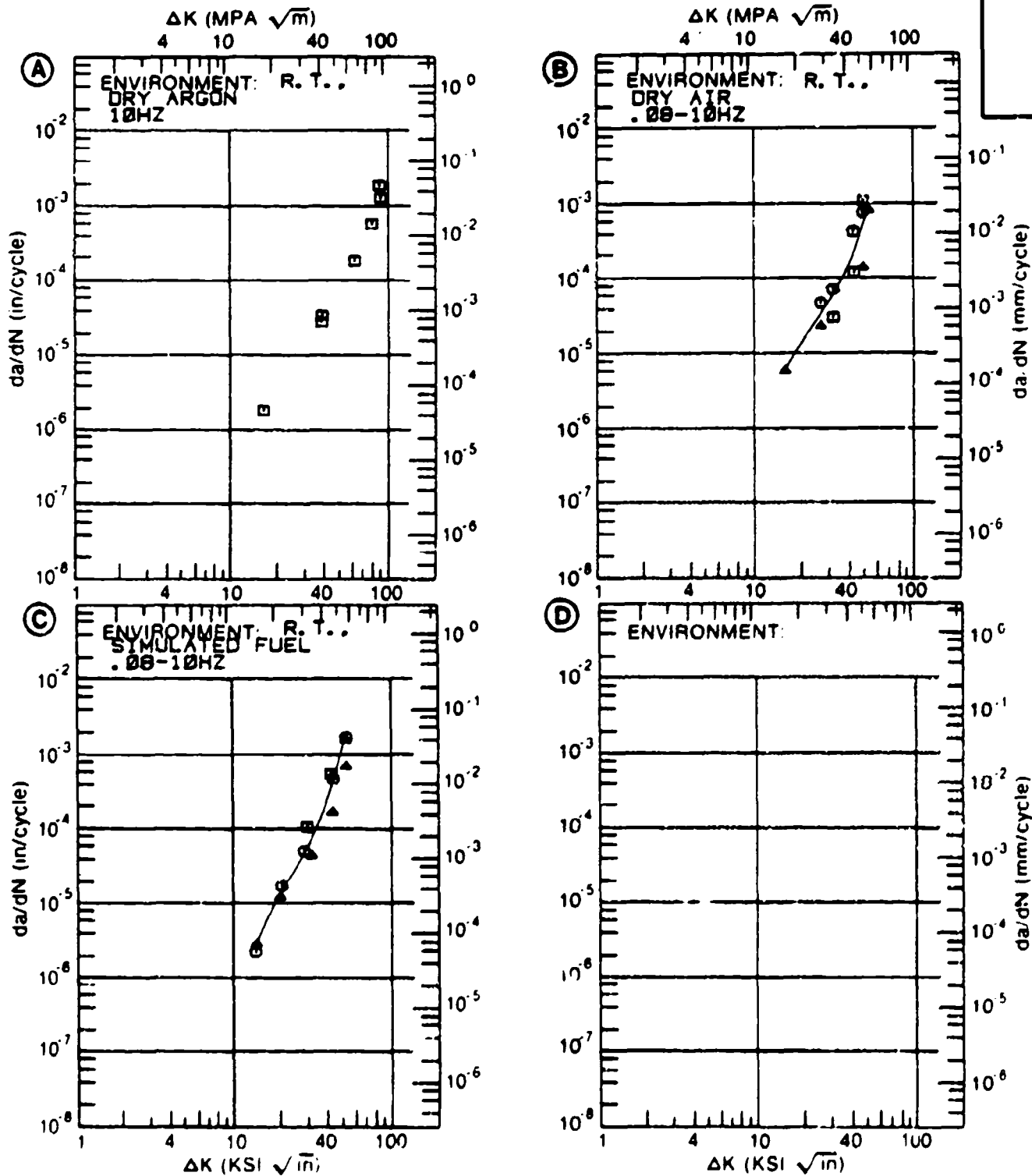


Figure 4.11.3.61

TABLE 4.11.3.62

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.62 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----|---------------------------------|----------------------------------|---|---|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DIST. WATER 10HZ | E= R. T. 3.5% NAACL 1-10HZ | | |
| DELTA K | A: | | | | |
| MIN | B: | 21.94 | 13.3 | | |
| | C: | | | | |
| | D: | | | | |
| | | 25.00 | 29.1 | | |
| | | 30.00 | 61.4 | | |
| | | 35.00 | 93.1 | | |
| | | 40.00 | 123. | | |
| | | 50.00 | 197. | | |
| | | 60.00 | 342. | | |
| | | 70.00 | 694. | | |
| | | 80.00 | 1657. | | |
| DELTA K | A: | | | | |
| MAX | B: | 82.01 | 2010. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | 41.05 | | |
| PERCENT ERROR | | | | | |
| LIFE | | 0.0-0.5 | | | |
| PREDICTION | | 0.5-0.8 | | | |
| RATIO | | 0.8-1.25 | | | |
| SUMMARY | | 1.25-2.0 | | | |
| (NP/NA) | | >2.0 | | | |

CONDITION/HT: MA
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: DCB
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 FREQUENCY:

YIELD STRENGTH: 145.0 KSI
 ULT. STRENGTH: 156.0 KSI
 SPECIMEN THK: 0.750- 0.875"
 SPECIMEN WIDTH: 5.500"
 REFERENCES: 04360

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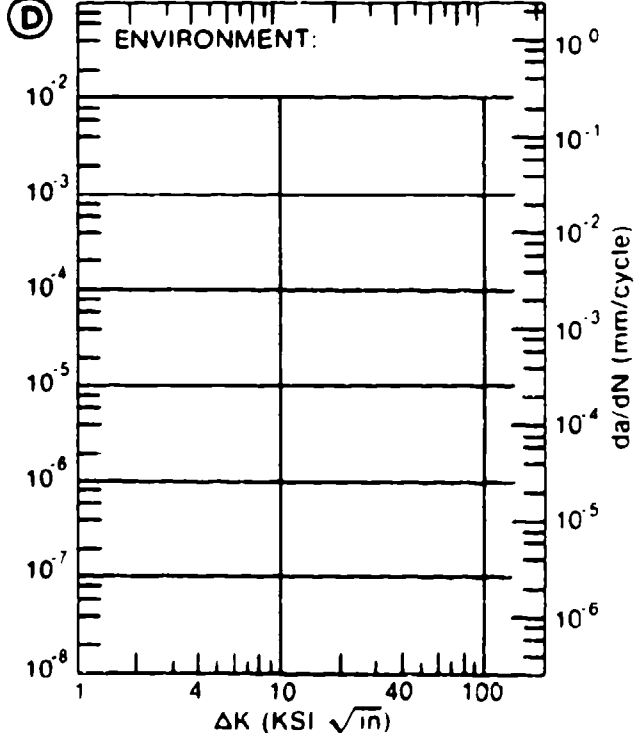
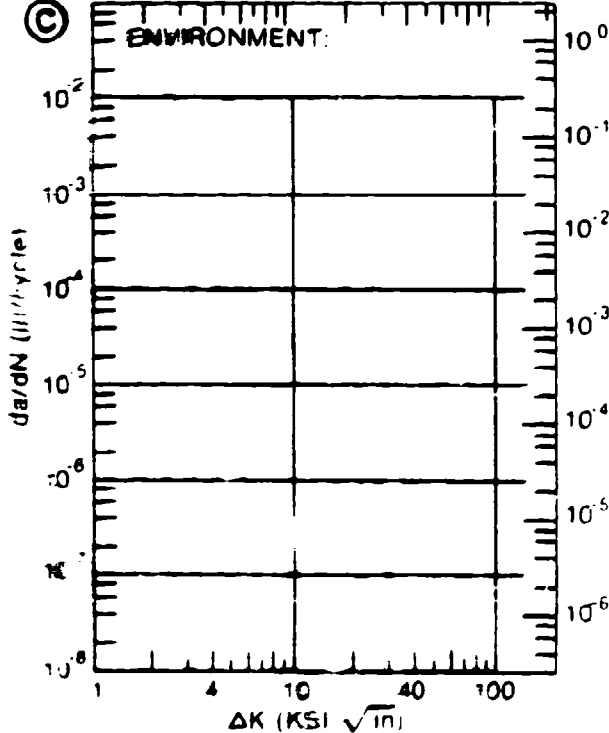
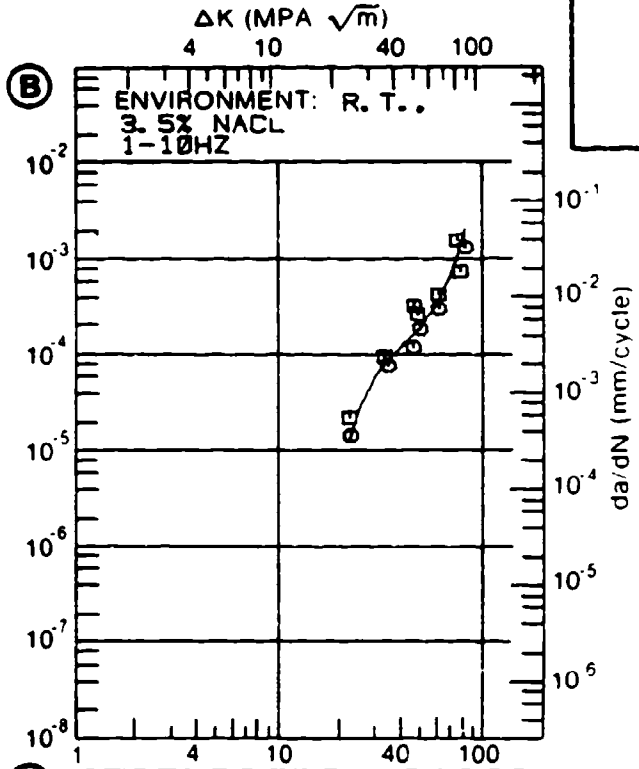
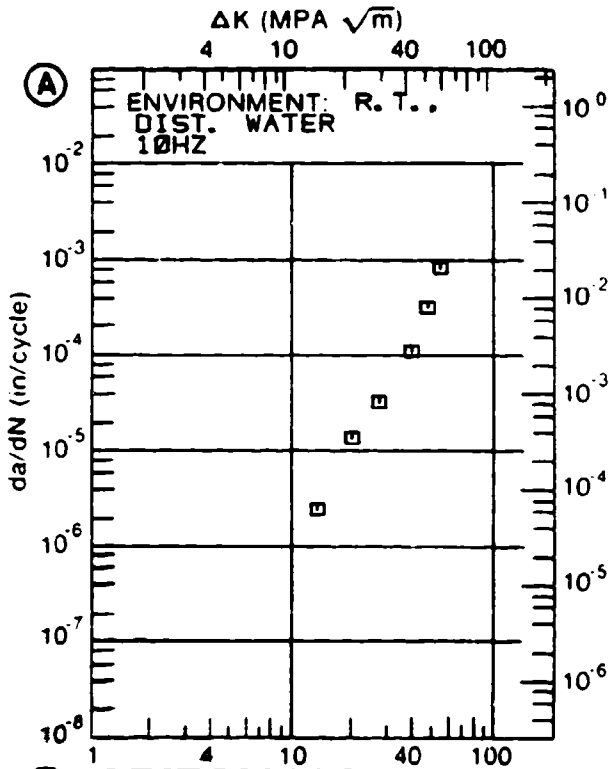


Figure 4.11.3.62

TABLE 4.11.3.63

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.63 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------------|----------|---------------------------|---|---|---|
| CONDITION: MA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K MIN | A: 18.15 | 6.34 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 8.18 | | | |
| | 25.00 | 15.7 | | | |
| | 30.00 | 29.2 | | | |
| | 35.00 | 53.0 | | | |
| | 40.00 | 95.0 | | | |
| | 50.00 | 292. | | | |
| | 60.00 | 857. | | | |
| DELTA K MAX | A: 60.61 | 914. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.19 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 4.50" TH FORGING
 SPECIMEN TYPE: WDL
 ORIENTATION: L-T
 FREQUENCY: 1.00- 30.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH: 139.0 KSI
 SPECIMEN THK: 0.553- 0.555"
 SPECIMEN WIDTH: 4.999- 5.000"
 REFERENCES: MA002

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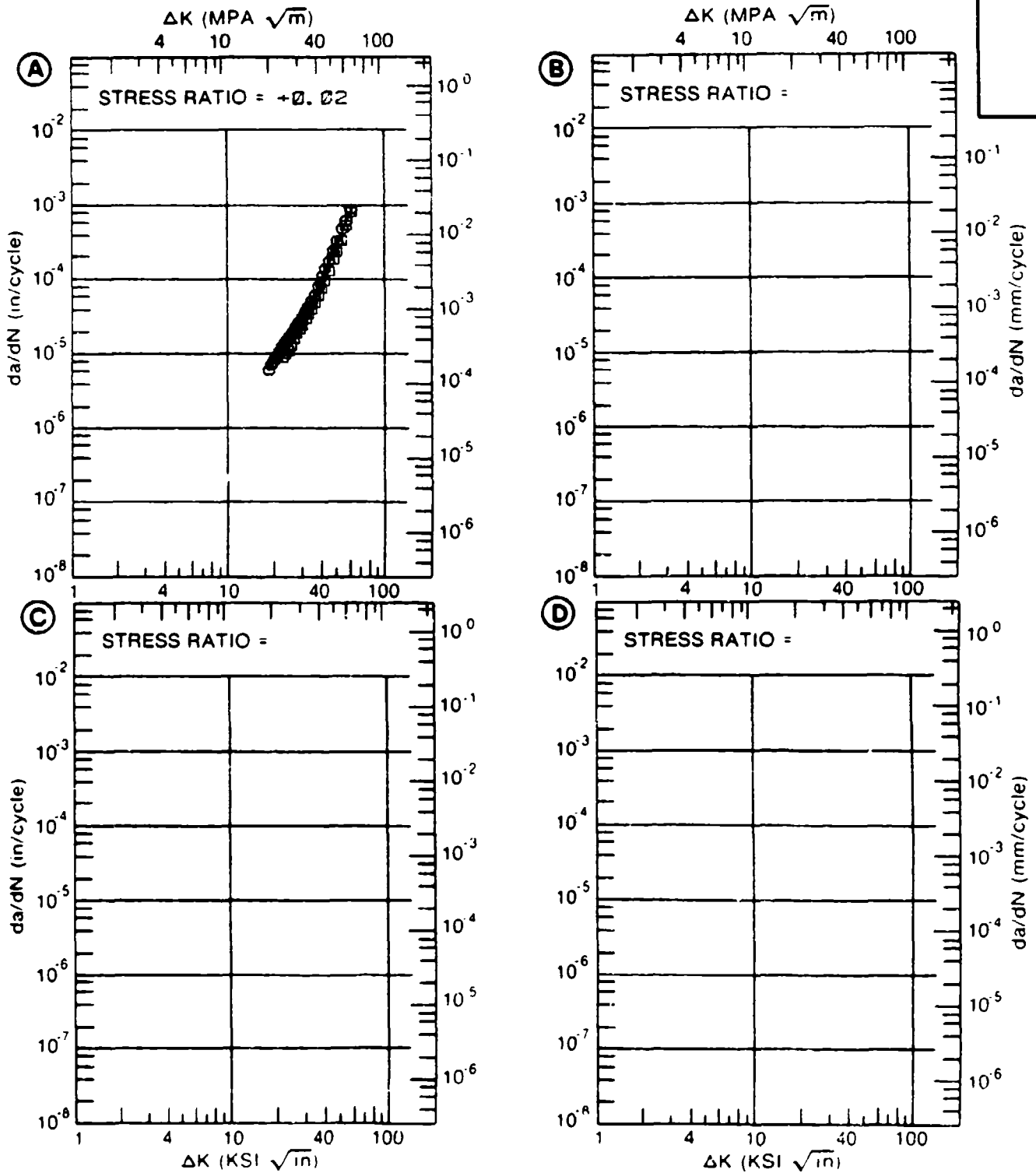


Figure 4.11.3.63

TABLE 4.11.3.64

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.64 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|---------|---------|---|
| CONDITION: MA | | 1300F 2HRS AC | | | |
| ENVIRONMENT: + 300F, AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.00 | R=+0.25 | R=+0.54 | |
| DELTA K | A: 10.32 | .610 | | | |
| MIN | B: 10.79 | | 1.01 | | |
| | C: 7.74 | | | .589 | |
| | D: | | | | |
| | 8.00 | | | .621 | |
| | 9.00 | | | .925 | |
| | 10.00 | | | 1.19 | |
| | 12.00 | 1.29 | 2.58 | 3.77 | |
| | 16.00 | 2.79 | 6.11 | 9.69 | |
| | 20.00 | 6.72 | 13.5 | | |
| | 25.00 | 16.1 | 28.1 | | |
| | 30.00 | 31.4 | | | |
| | 35.00 | 52.2 | | | |
| | 40.00 | 76.6 | | | |
| DELTA K | A: 44.22 | 97.8 | | | |
| MAX | B: 27.30 | | 37.7 | | |
| | C: 19.93 | | | 20.8 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 20.23 | 28.07 | 43.68 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.8 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA 1300F 2HRS AC
 FORM: 1.75" TH DISK
 SPECIMEN TYPE: KB BAR
 ORIENTATION: L-R
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: + 300° F, AIR

YIELD STRENGTH: 120.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.244- 0.250"
 SPECIMEN WIDTH: 1.000- 1.005"
 REFERENCES: GE007

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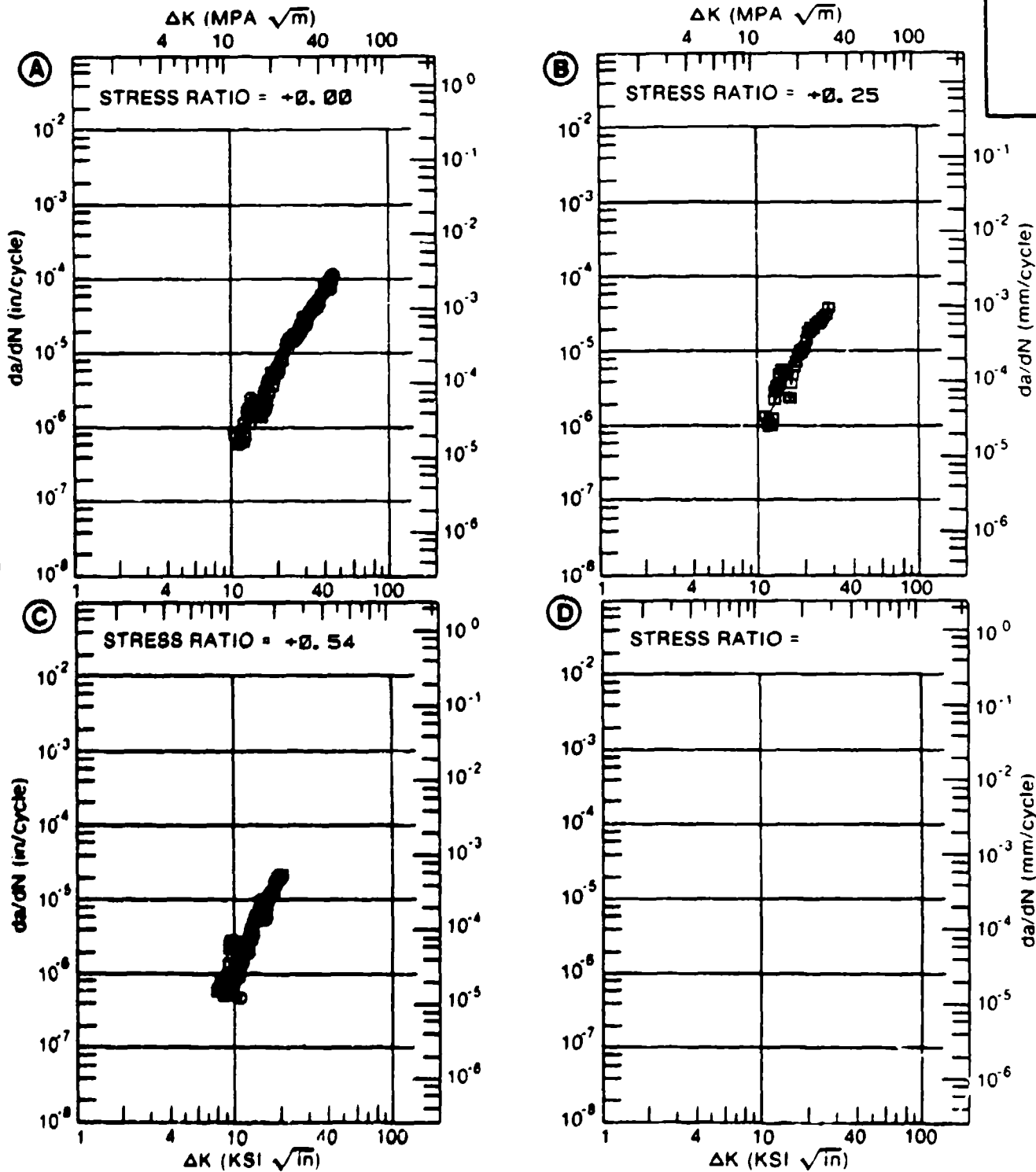


Figure 4.11.3.64

TABLE 4.11.3.65

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.65 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: MA 1300F 2HRS AC
ENVIRONMENT: + 600F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.00 | R=+0.25 | R=+0.54 | |
| MIN | A: 10.19 | 1.49 | | | |
| | B: 8.78 | | 1.23 | | |
| | C: 8.13 | | | .684 | |
| | D: | | | | |
| | 9.00 | | 1.21 | .964 | |
| | 10.00 | | 1.24 | 1.46 | |
| | 13.00 | 2.32 | 2.08 | 4.75 | |
| | 16.00 | 3.90 | 4.36 | 12.4 | |
| | 20.00 | 7.83 | 11.2 | 30.9 | |
| | 25.00 | 18.0 | 28.1 | | |
| | 30.00 | 39.4 | | | |
| | 35.00 | 81.4 | | | |
| | 40.00 | 160. | | | |
| MAX | A: 41.78 | 202. | | | |
| | B: 28.82 | | 46.2 | | |
| | C: 20.36 | | | 32.9 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 21.78 | 23.65 | 26.02 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA 1300F 2HRS AC
 FORM: 1.75" TH FORWARD SPOOL
 SPECIMEN TYPE: KB BAR
 ORIENTATION: L-R
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: + 800° F. AIR

YIELD STRENGTH: 120.0 KSI
 ULT STRENGTH:
 SPECIMEN THK: 0.249- 0.253"
 SPECIMEN WIDTH: 0.995- 1.003"
 REFERENCES: GE007

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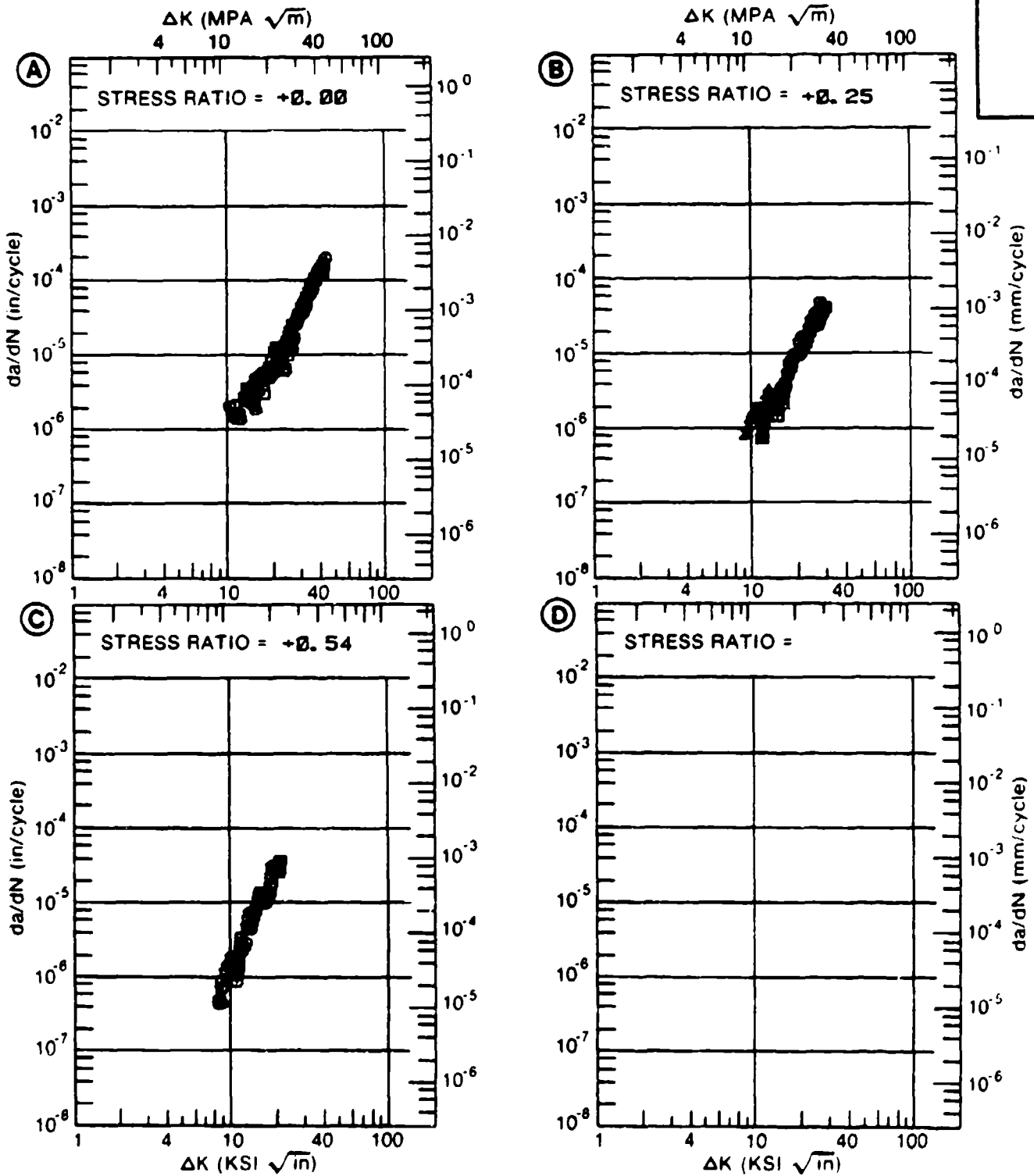


Figure 4.11.3.65

TABLE 4.11.3.66

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.66 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , H. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K | A: 8.50 | 2.47 | | | |
| MIN | B: 4.86 | | .285 | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | | .326 | | |
| | 6.00 | | .698 | | |
| | 7.00 | | 1.21 | | |
| | 8.00 | | 1.85 | | |
| | 9.00 | 2.81 | 2.65 | | |
| | 10.00 | 3.57 | 3.63 | | |
| | 13.00 | 6.80 | 8.44 | | |
| | 16.00 | 12.0 | 19.2 | | |
| | 20.00 | 23.8 | 64.9 | | |
| | 25.00 | 51.4 | | | |
| | 30.00 | 105. | | | |
| | 35.00 | 203. | | | |
| | 40.00 | 378. | | | |
| DELTA K | A: 42.13 | 487. | | | |
| MAX | B: 22.81 | | 169. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 8.97 | 13.03 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.13" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 149.1- 149.2 KSI
 ULT. STRENGTH: 156.2 KSI
 SPECIMEN THK: 0.124- 0.125"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

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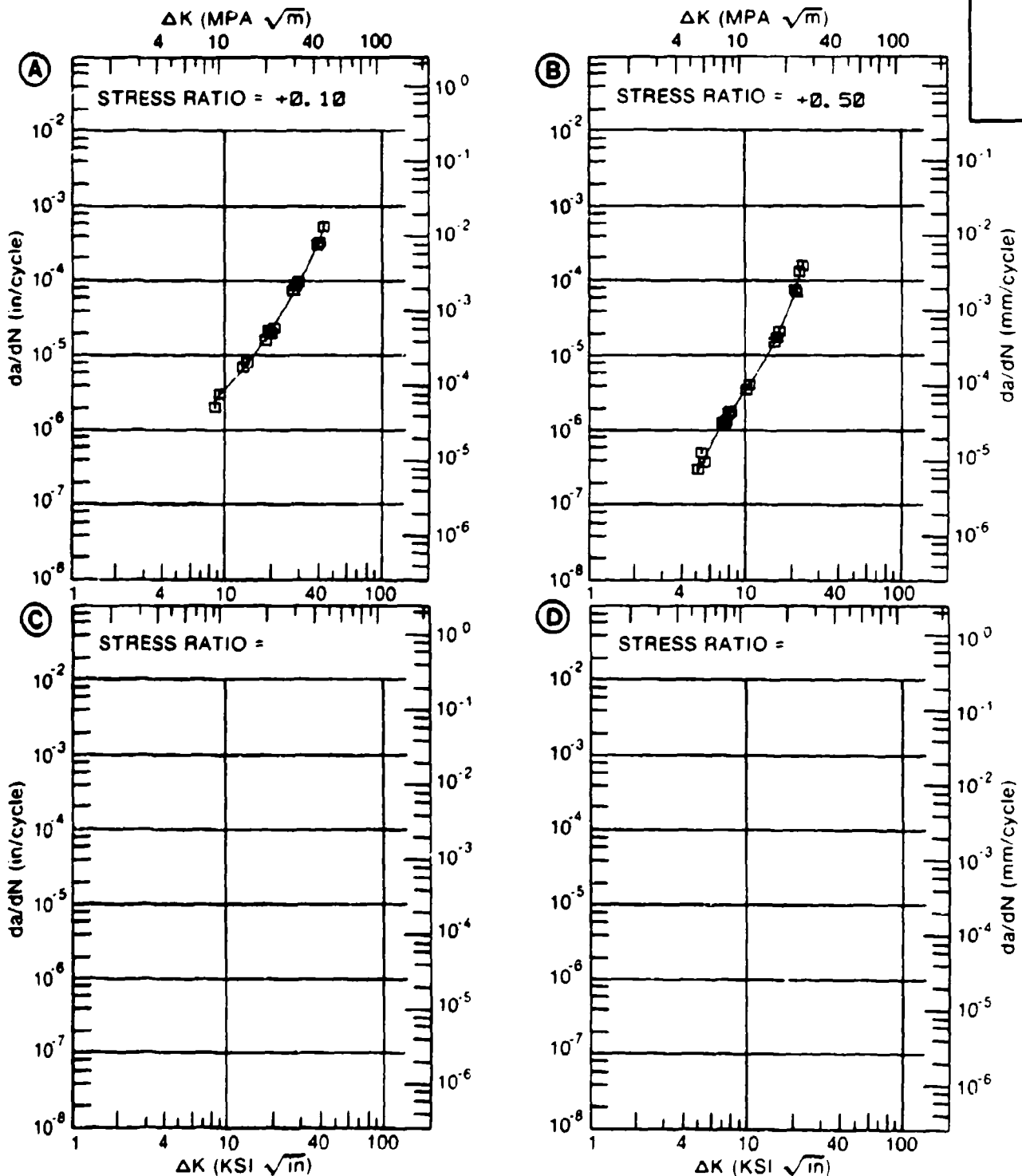


Figure 4.11.3.66

TABLE 4.11.3.67

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.67 INDICATING EFFECT
OF FREQUENCY

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|----------|--------------------------------------|------|--------------|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , 3.5% NaCl | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | F(HZ)= 0.10 | | F(HZ)= 10.00 | |
| DELTA K MIN | A: 8.36 | 2.00 | | | |
| | B: 8.72 | | 2.33 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | 2.47 | 2.79 | | |
| | 10.00 | 3.50 | 4.86 | | |
| | 13.00 | 9.45 | 15.6 | | |
| | 16.00 | 21.1 | 32.6 | | |
| | 20.00 | 44.7 | 63.0 | | |
| | 25.00 | 74.0 | 111. | | |
| | 30.00 | | 168. | | |
| | 35.00 | | 237. | | |
| | 40.00 | | 321. | | |
| DELTA K MAX | A: 26.41 | 79.4 | | | |
| | B: 42.50 | | 370. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.04 | 9.11 | | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | 1 | 1 | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | | | | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.13" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: +0.10
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH: 149.2 KSI
 ULT. STRENGTH: 156.2 KSI
 SPECIMEN THK: 0.125"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

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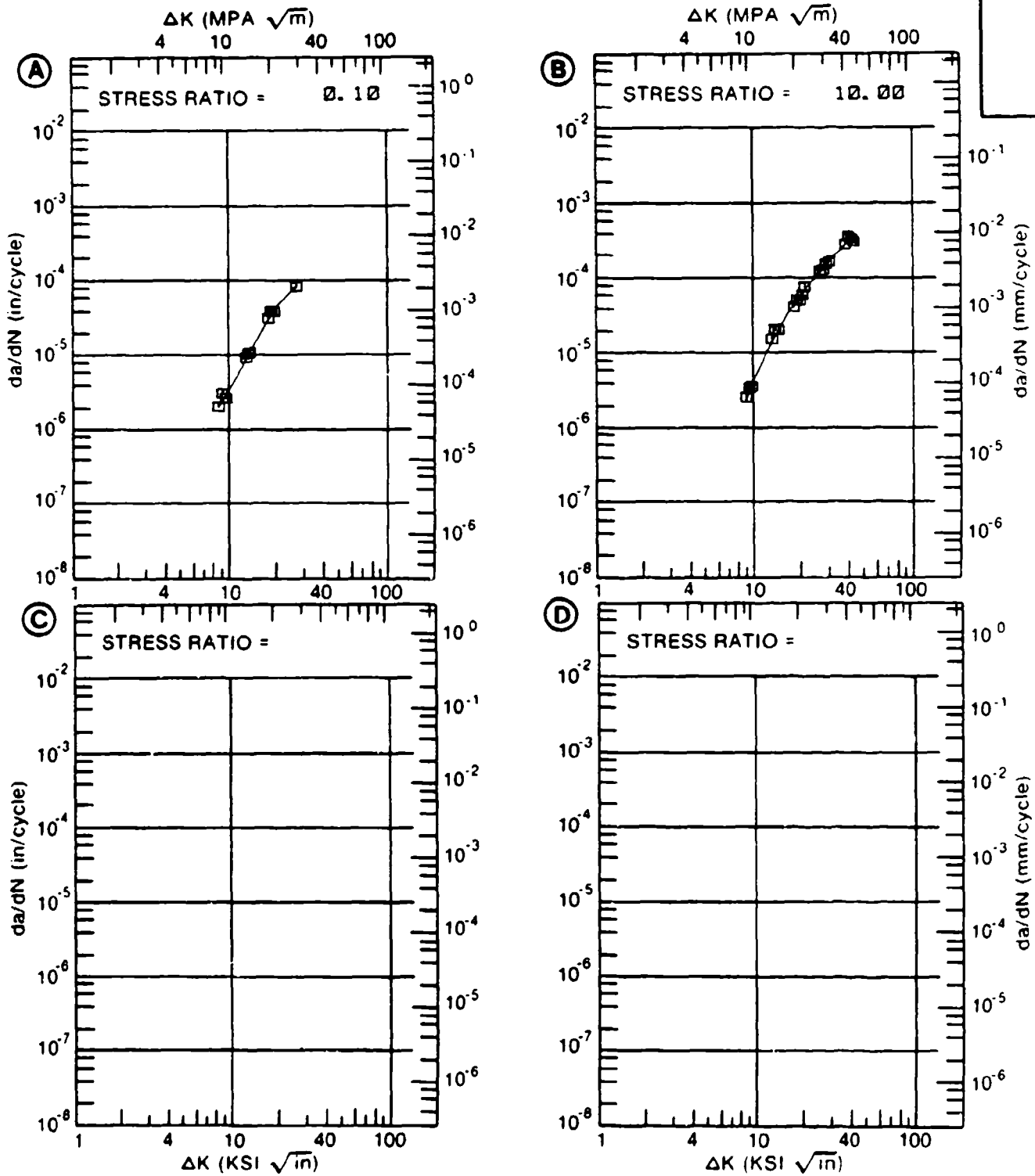


Figure 4.11.3.67

TABLE 4.11.3.68

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.68 INDICATING EFFECT
OF FREQUENCY

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------------|----------|---------------------------|---|---|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , HUMID AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | F(HZ)= 10.00 | | | |
| DELTA K | A: 8.50 | .637 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .792 | | | |
| | 10.00 | 1.18 | | | |
| | 13.00 | 3.12 | | | |
| | 16.00 | 6.30 | | | |
| | 20.00 | 12.1 | | | |
| | 25.00 | 19.9 | | | |
| | 30.00 | 26.1 | | | |
| | 35.00 | 29.2 | | | |
| DELTA K | A: 37.14 | 29.6 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.83 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: L-S
 STRESS RATIO: +0.10
 ENVIRONMENT: R. T., HUMID AIR

YIELD STRENGTH: 119.1 KSI
 ULT. STRENGTH: 139.1 KSI
 SPECIMEN THK: 0.376"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90001

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TI-6AL-
4V

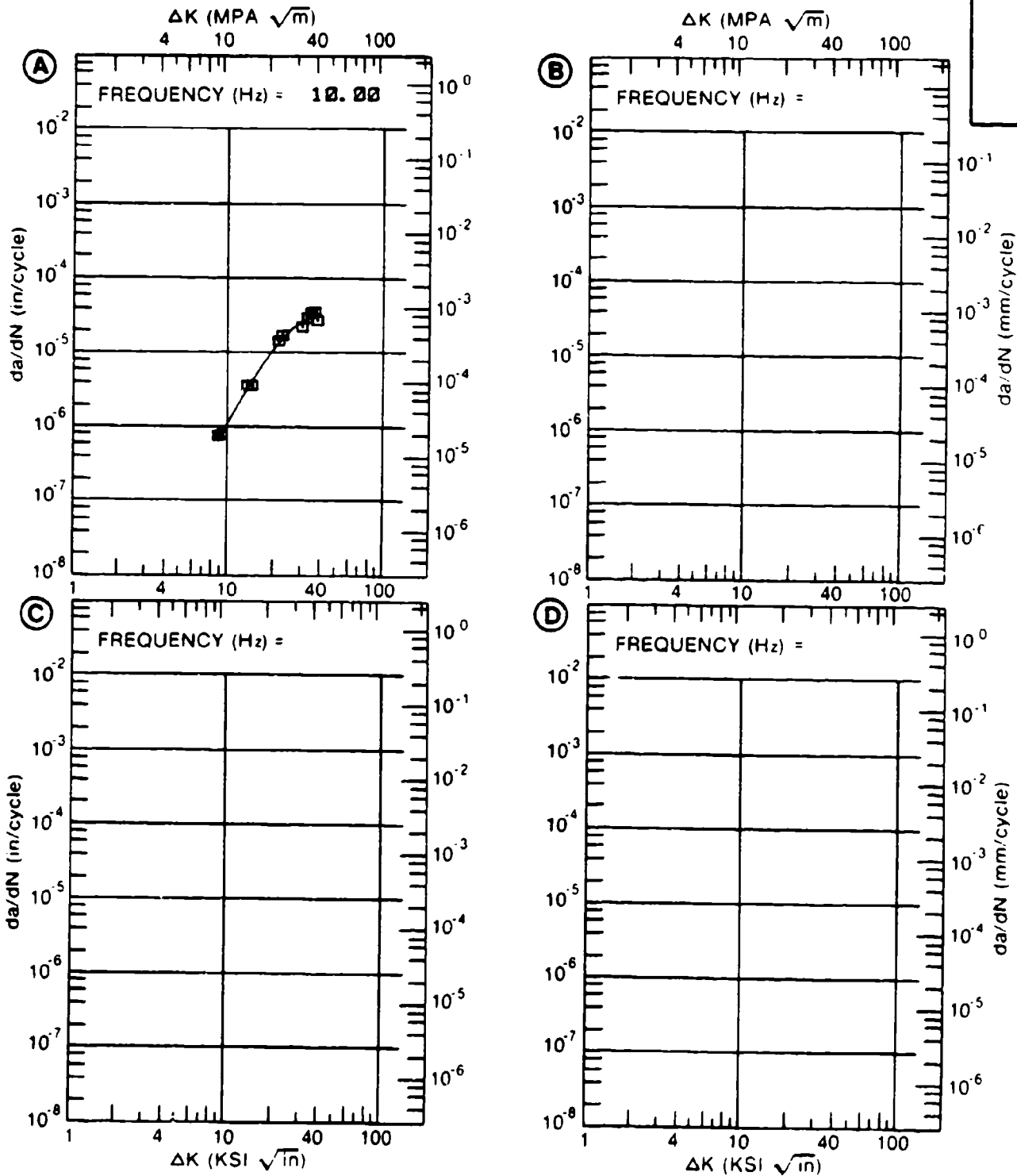


Figure 4.11.3.68

TABLE 4.11.3.69

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.69 INDICATING EFFECT
OF FREQUENCY

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , 3.5% NaCl

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | F(HZ)= 10.00 | | | |
| DELTA K MIN | A: 15.77 | 37.3 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 37.9 | | | |
| | 20.00 | 49.7 | | | |
| | 25.00 | 67.2 | | | |
| | 30.00 | 84.6 | | | |
| | 35.00 | 99.2 | | | |
| DELTA K MAX | A: 35.80 | 101. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 22.70 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 STRESS RATIO: +0.10
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH: 141.7 KSI
 ULT STRENGTH: 151.9 KSI
 SPECIMEN THK: 0.377"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

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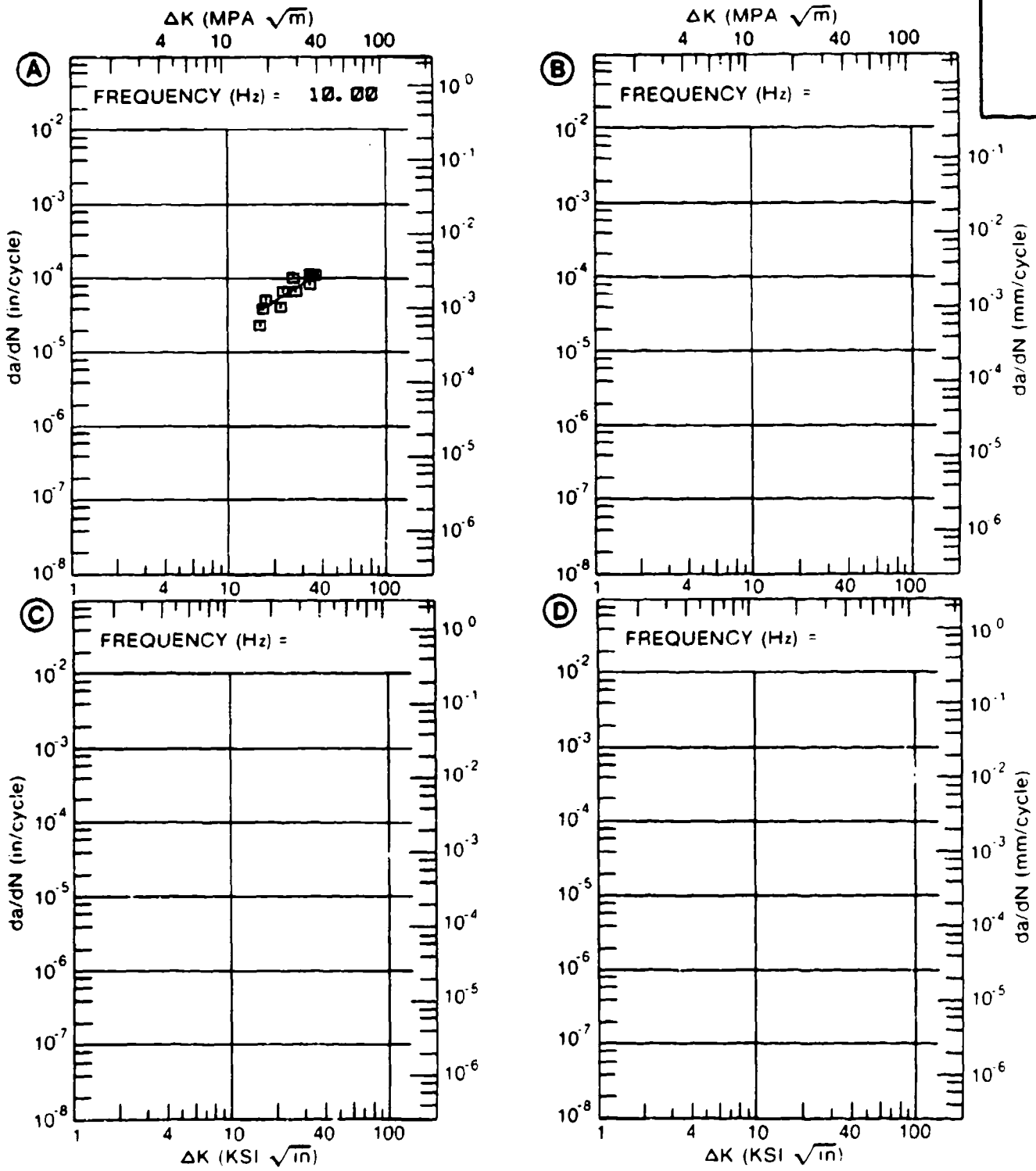


Figure 4.11.3.69

TABLE 4.11.3.70

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.70 INDICATING EFFECT
OF STRESS RATIO

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K A: | 10.10 | 4.77 | | | |
| DELTA K B: | 5.41 | | .99 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 6.00 | | 1.54 | | |
| | 7.00 | | 2.63 | | |
| | 8.00 | | 3.84 | | |
| | 9.00 | | 5.12 | | |
| | 10.00 | | 6.45 | | |
| | 13.00 | 6.51 | 10.9 | | |
| | 16.00 | 9.27 | 16.7 | | |
| | 20.00 | 14.4 | 26.8 | | |
| | 25.00 | 23.2 | | | |
| DELTA K A: | 28.25 | 27.0 | | | |
| DELTA K B: | 23.27 | | 33.7 | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 5.20 | 12.89 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 141.7 KSI
 ULT. STRENGTH: 151.8 KSI
 SPECIMEN THK: 0.370- 0.371"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

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 4V

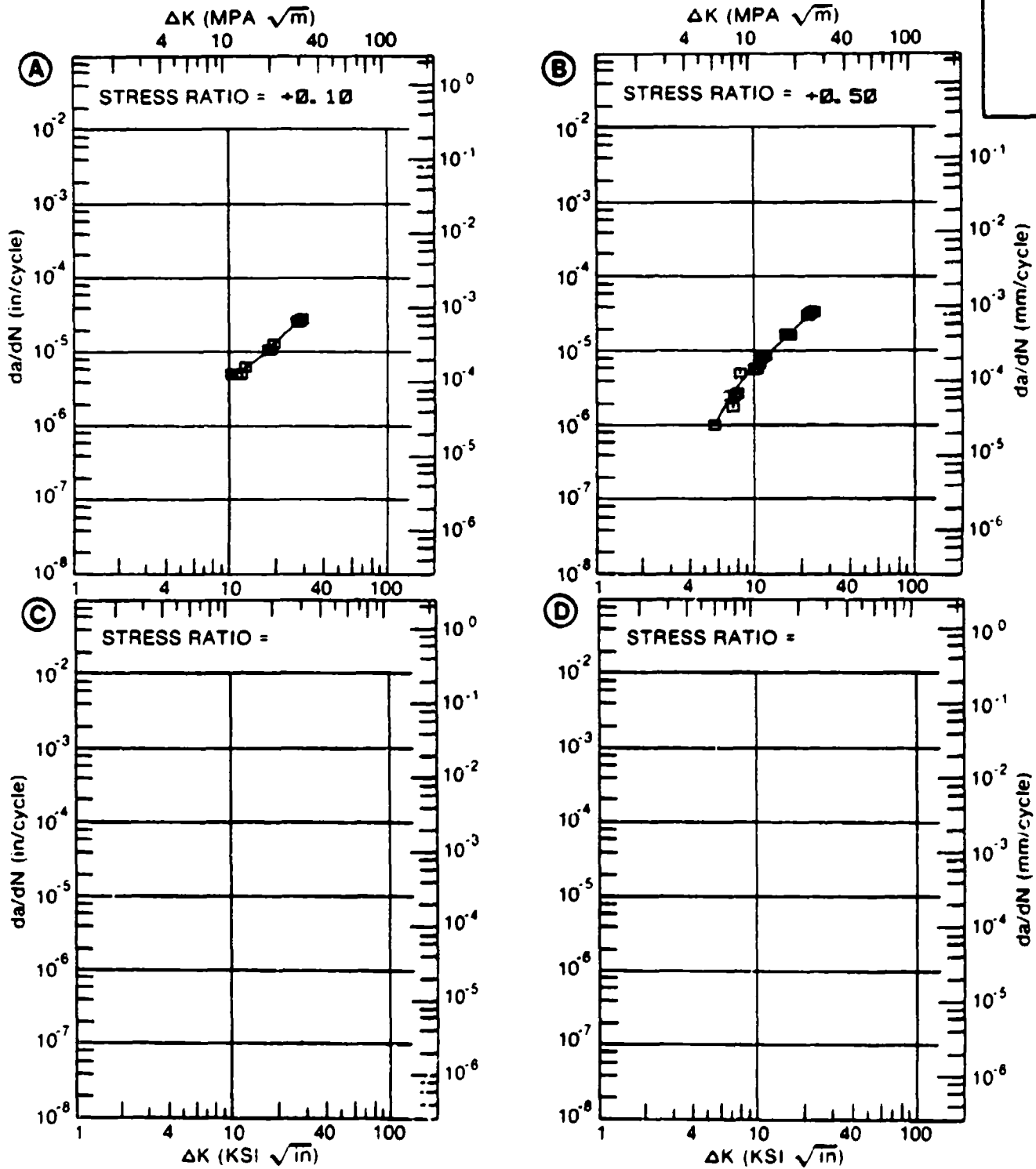


Figure 4.11.3.70

TABLE 4.11.3.71

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.71 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|------------------------------------|---------|---|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , 3.5% NaCl | | | | | |
| DELTA K (KSI*IN ^{1/2}) | | DA/DN (10 ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K MIN | A: 17.57 | 35.8 | 15.2 | | |
| | B: 6.24 | | | | |
| | C: | | | | |
| | D: | | | | |
| | 7.00 | | 15.8 | | |
| | 8.00 | | 22.0 | | |
| | 9.00 | | 28.4 | | |
| | 10.00 | | 33.7 | | |
| | 13.00 | | 51.4 | | |
| | 16.00 | | 86.8 | | |
| | 20.00 | 58.9 | 148. | | |
| | 25.00 | 86.0 | | | |
| | 30.00 | 132. | | | |
| | 35.00 | 181. | | | |
| | 40.00 | 206. | | | |
| DELTA K MAX | A: 42.87 | 209. | 697. | | |
| | B: 23.07 | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 11.25 | 18.49 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | 1 | | |

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH: 141.7 KSI
 ULT. STRENGTH: 151.8 KSI
 SPECIMEN THK: 0.372"
 SPECIMEN WIDTH: 5.000"
 REFERENCES 90001

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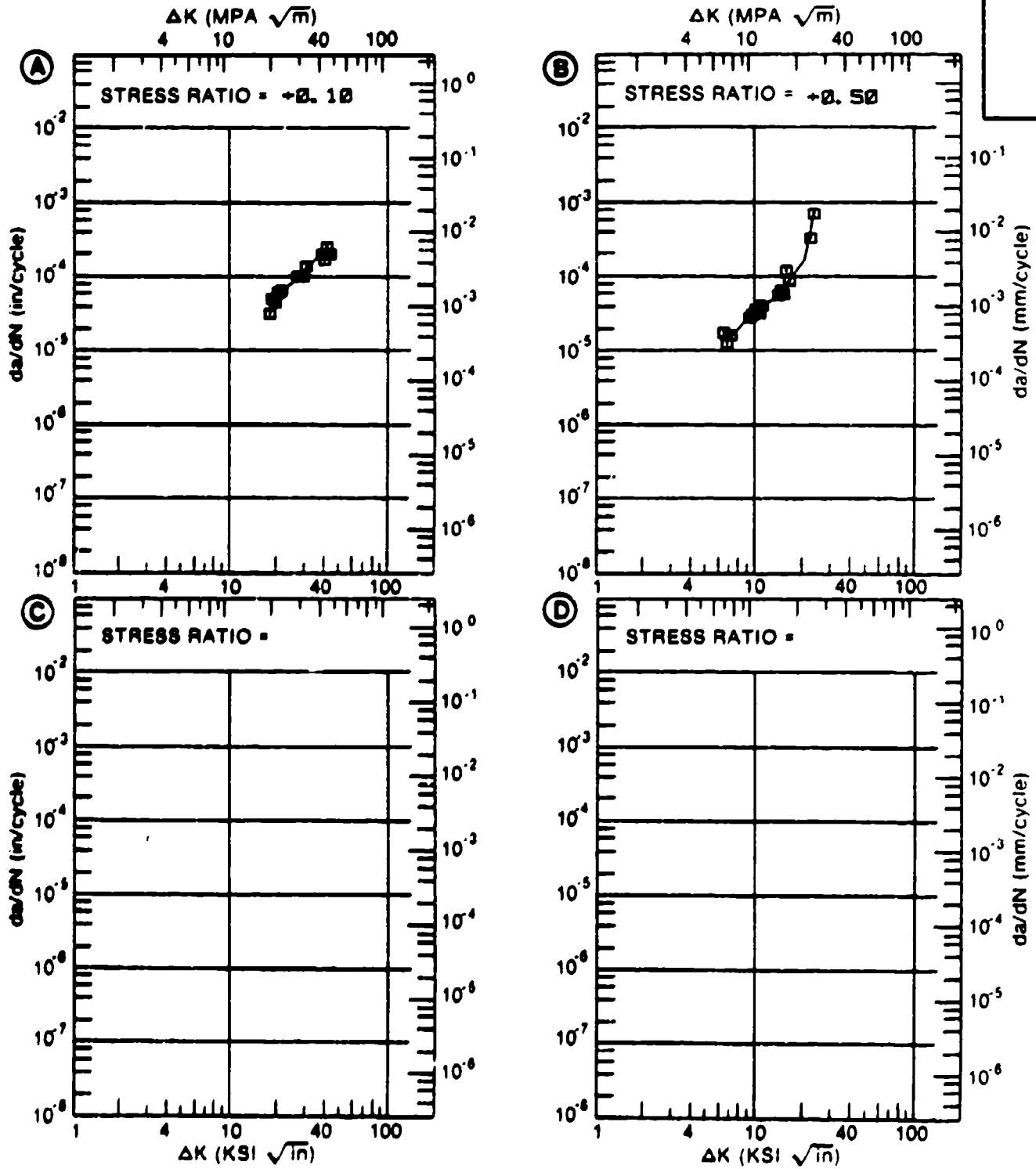


Figure 4.11.3.71

TABLE 4.11.3.72

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.72 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.08 | | | |
| DELTA K | A: 5.67 | .224 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | .262 | | | |
| | 7.00 | .437 | | | |
| | 8.00 | .747 | | | |
| | 9.00 | 1.26 | | | |
| | 10.00 | 2.08 | | | |
| | 13.00 | 7.51 | | | |
| | 16.00 | 19.9 | | | |
| | 20.00 | 48.7 | | | |
| DELTA K | A: 23.65 | 81.2 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 22.66 | | | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.9
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0 1
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 129.0 KSI
 ULT. STRENGTH: 140.0 KSI
 SPECIMEN THK: 0.410"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 99579

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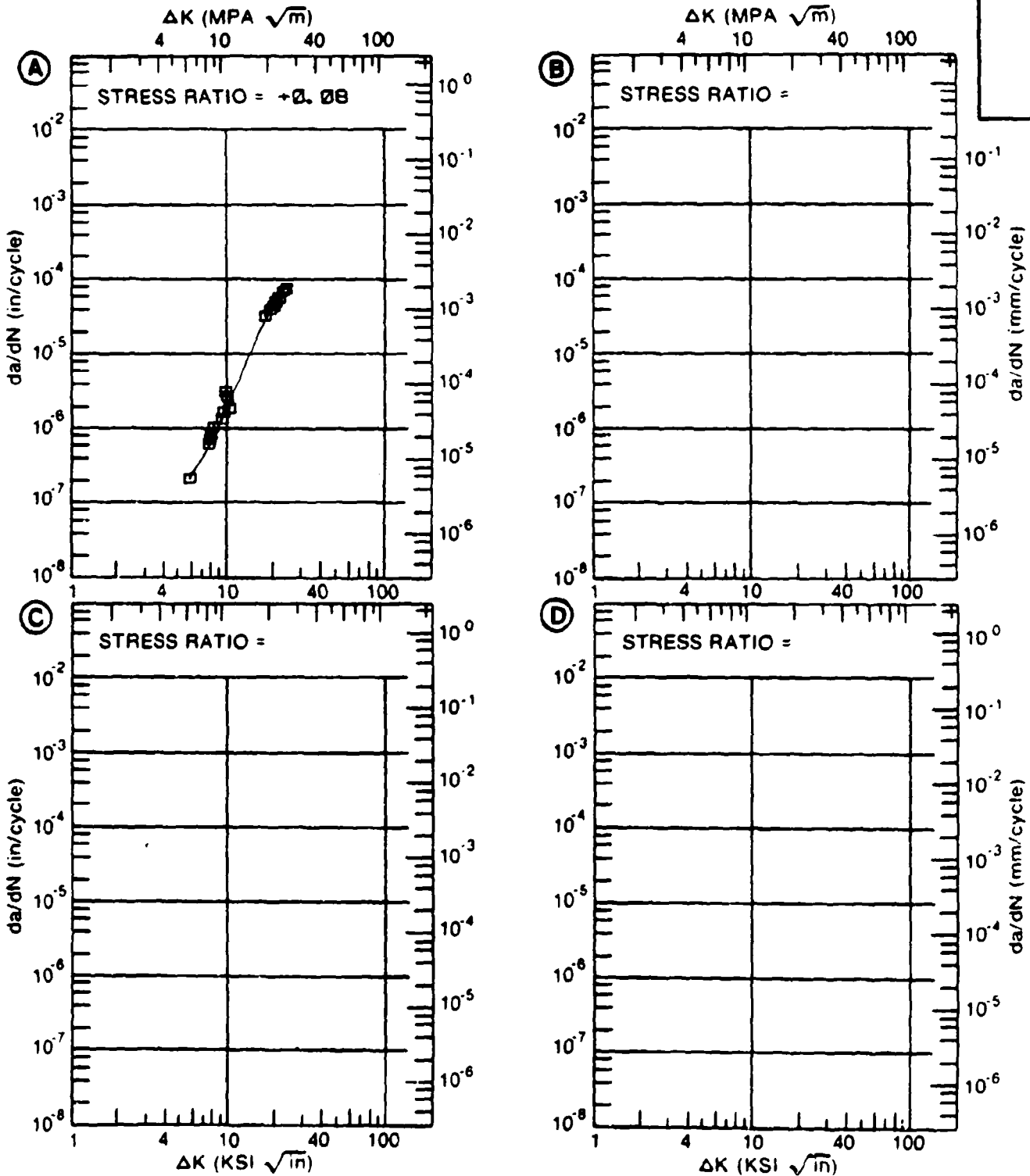


Figure 4.11.3.72

TABLE 4.11.3.73

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.73 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|-----------------|---------------------------------------|---|---|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , S. T. W. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 29.01 | 1405. | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 30.00 | 1418. | | | |
| | 35.00 | 1800. | | | |
| | 40.00 | 2531. | | | |
| | 50.00 | 3951. | | | |
| DELTA K | A: 52.51 | 4043. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.89 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 2 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 0.10 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 141.7 KSI
 ULT. STRENGTH: 151.8 KSI
 SPECIMEN THK: 0.374- 0.375"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 90981

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4V

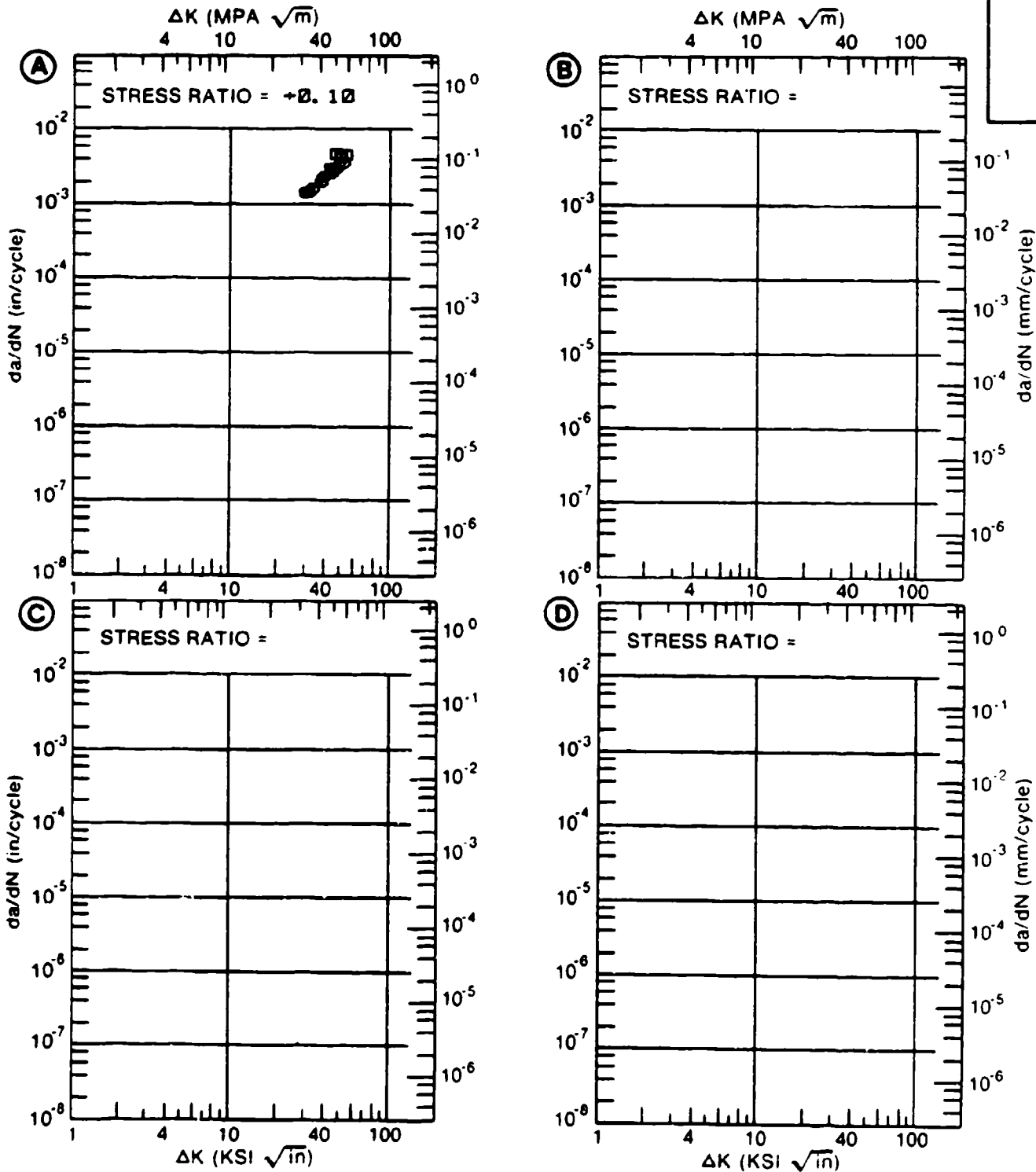


Figure 4.11.3.73

TABLE 4.11.3.74

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.74 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K | A: 13.05 | 4.93 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 11.0 | | | |
| | 20.00 | 21.3 | | | |
| | 25.00 | 41.9 | | | |
| | 30.00 | 87.4 | | | |
| | 35.00 | 205. | | | |
| DELTA K | A: 36.63 | 279. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.02 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 0.39" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 149.2 KSI
 ULT. STRENGTH: 156.2 KSI
 SPECIMEN THK: 0.372"
 SPECIMEN WIDTH: 2.549"
 REFERENCES: 90991

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 4V

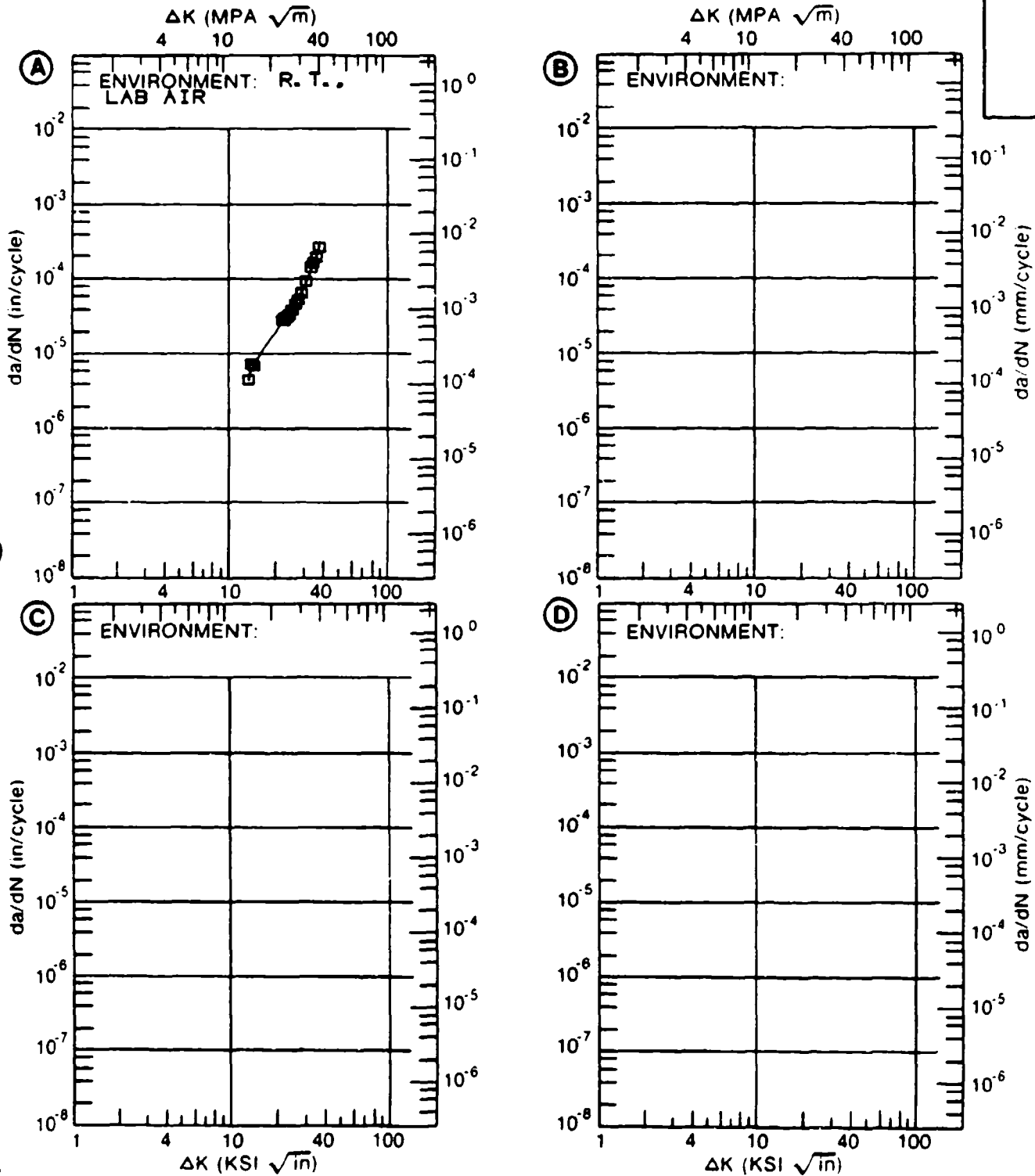


Figure 4.11.3.74

TABLE 4.11.3.75

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.75 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|------------------------|----------------------|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DIST. WATER | E= R. T. 3. 5% NACL | E= R. T. S. T. W. | |
| DELTA K | A: 9.44 | .241 | | | |
| MIN | B: 8.60 | | .341 | | |
| | C: 9.40 | | | .364 | |
| | D: | | | | |
| | 9.00 | | .405 | | |
| | 10.00 | .434 | .646 | .646 | |
| | 13.00 | | 2.66 | | |
| DELTA K | A: 11.75 | 1.32 | | | |
| MAX | B: 13.55 | | 3.37 | | |
| | C: 12.61 | | | 2.09 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 15.71 | 16.16 | 11.43 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.00
 FREQUENCY: 15.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES 88140

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 ALLOY
 TI-6AL-
 4V

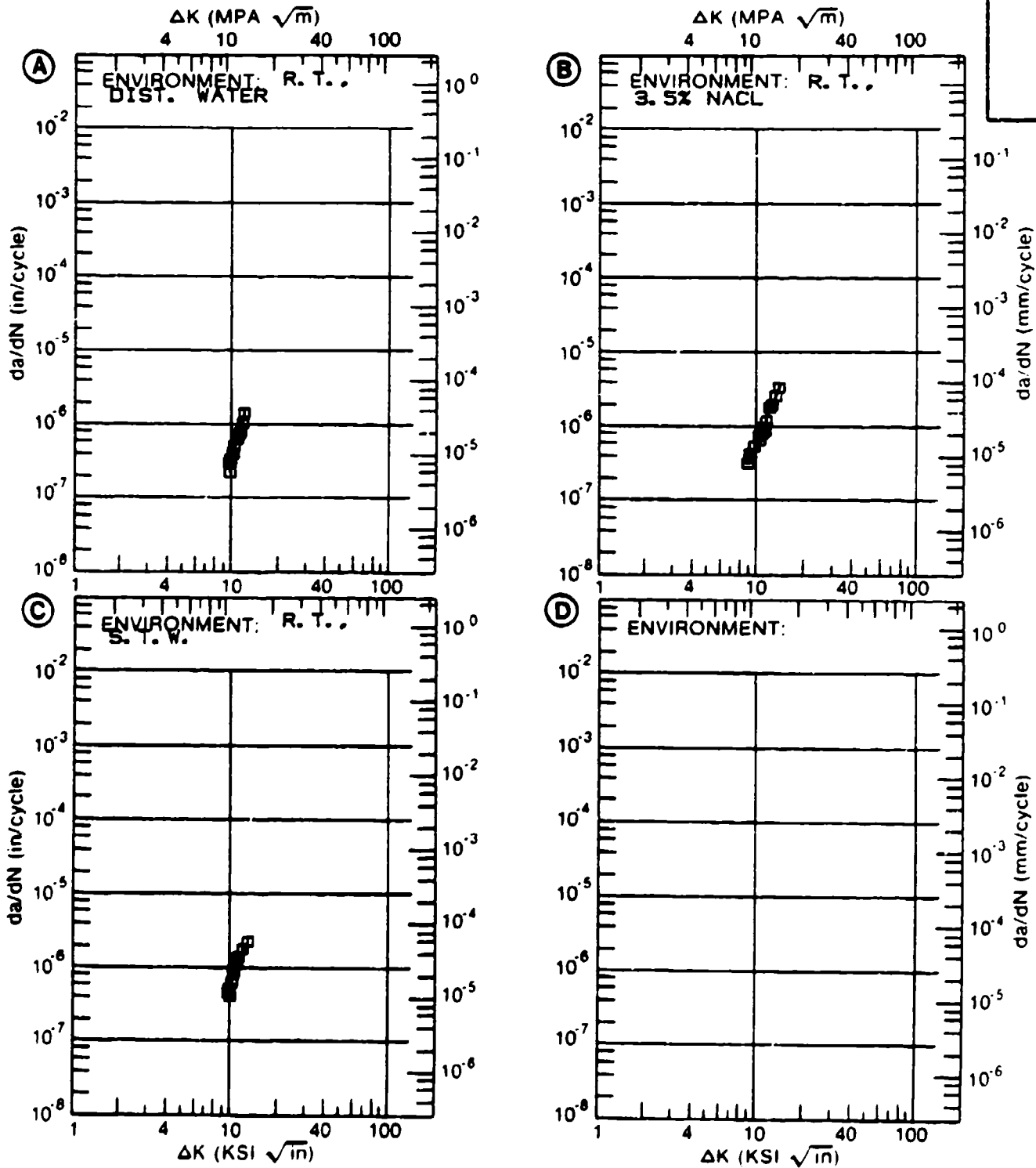


Figure 4.11.3.75

TABLE 4.11.3.76

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.76 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: RA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|--|-------------------------|---|
| | | A | B | C | D |
| | | E= R. T. DRY AIR | E= R. T. H2O STAURATED JP-4 FUEL | E= R. T. DIST. WATER | |
| DELTA K | A: 12.23 | 1.04 | | | |
| MIN | B: 28.27 | | 32.7 | | |
| | C: 26.64 | | | 30.5 | |
| | D: | | | | |
| | 13.00 | 1.45 | | | |
| | 16.00 | 3.88 | | | |
| | 20.00 | 9.08 | | | |
| | 25.00 | 18.5 | | | |
| | 30.00 | 31.5 | 36.7 | 44.5 | |
| | 35.00 | 49.5 | 51.9 | 67.7 | |
| | 40.00 | 74.9 | 75.9 | 96.3 | |
| | 50.00 | 164. | 179. | 197. | |
| | 60.00 | | 465. | 455. | |
| | 70.00 | | 1304. | 1228. | |
| | 80.00 | | | 3814. | |
| DELTA K | A: 58.67 | 322. | | | |
| MAX | B: 71.17 | | 1476. | | |
| | C: 81.31 | | | 4465. | |
| | D: | | | | |

ROOT MEAN SQUARE 25.19 10.30 22.32
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES 88140

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ALLOY

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4V

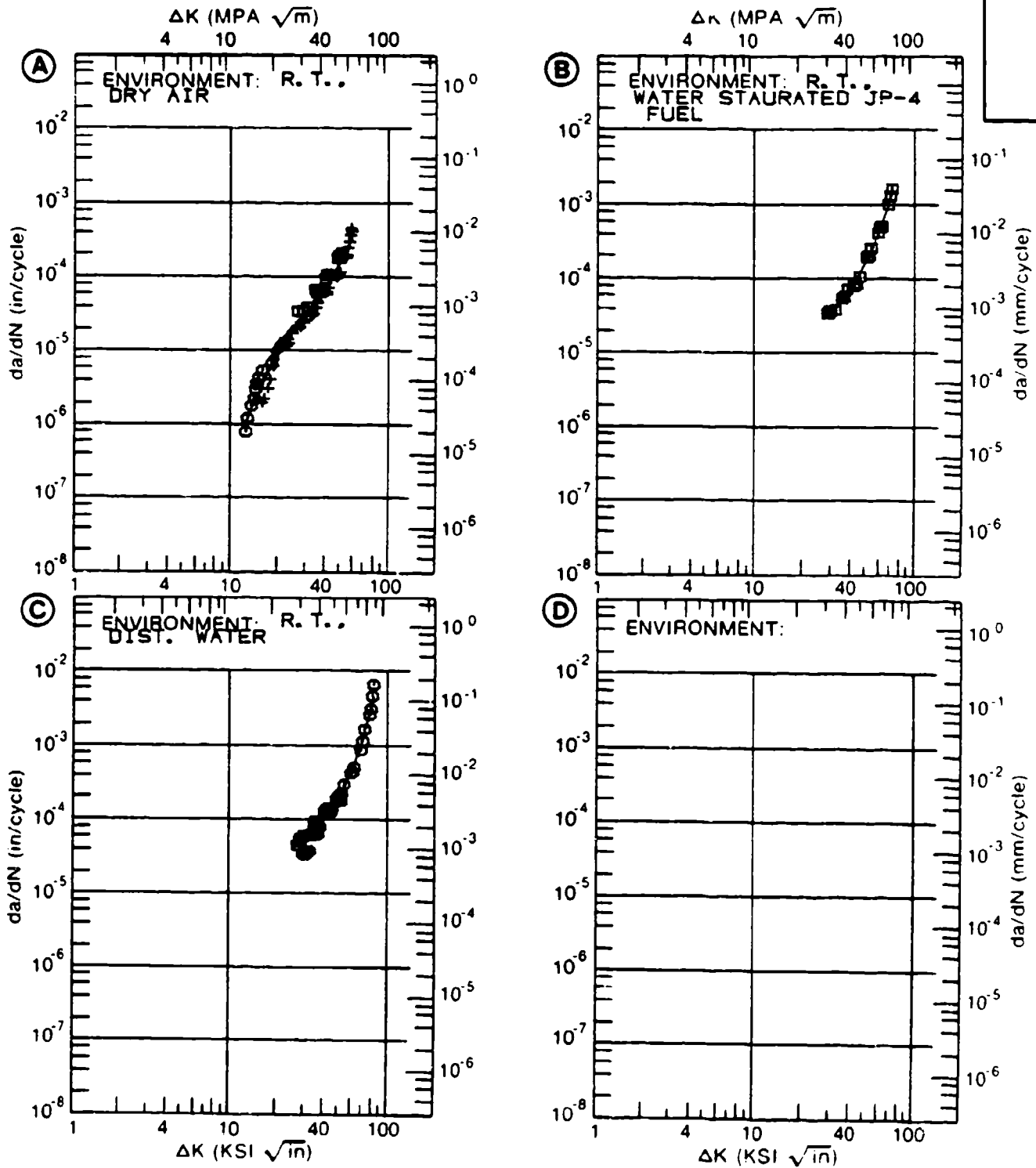


Figure 4.11.3.76

TABLE 4.11.3.77

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.77 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|----------------------------|----------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**--6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3. 5% NACL | E= R. T. S. T. W. | | |
| DELTA K | A: 14.96 | 14.1 | | | |
| MIN | B: 28.42 | | 84.9 | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 16.3 | | | |
| | 20.00 | 28.6 | | | |
| | 25.00 | 54.7 | | | |
| | 30.00 | 97.2 | 100. | | |
| | 35.00 | 161. | 144. | | |
| | 40.00 | 251. | 187. | | |
| | 50.00 | 526. | 310. | | |
| | 60.00 | 943. | 604. | | |
| | 70.00 | 1504. | 1456. | | |
| | 80.00 | | 4302. | | |
| DELTA K | A: 72.43 | 1660. | | | |
| MAX | B: 81.35 | | 5050. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 14.68 | 8.17 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0 0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

TITAN.
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4V

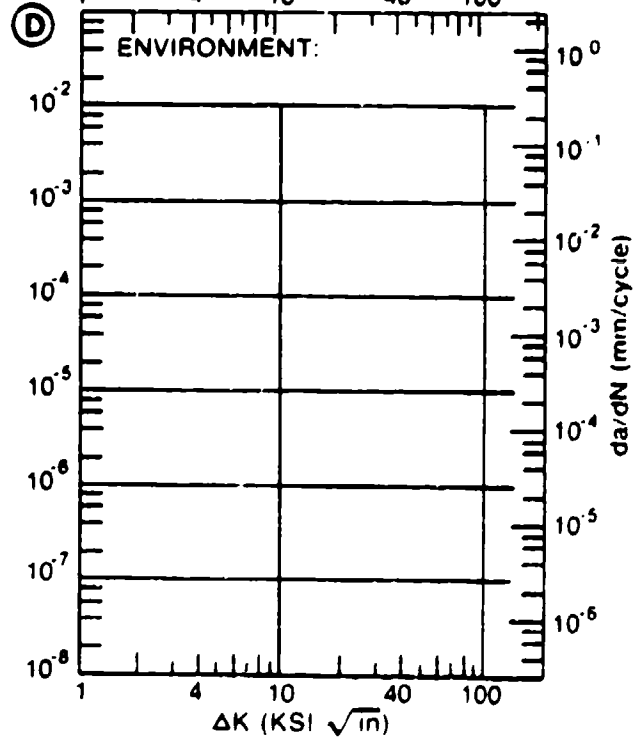
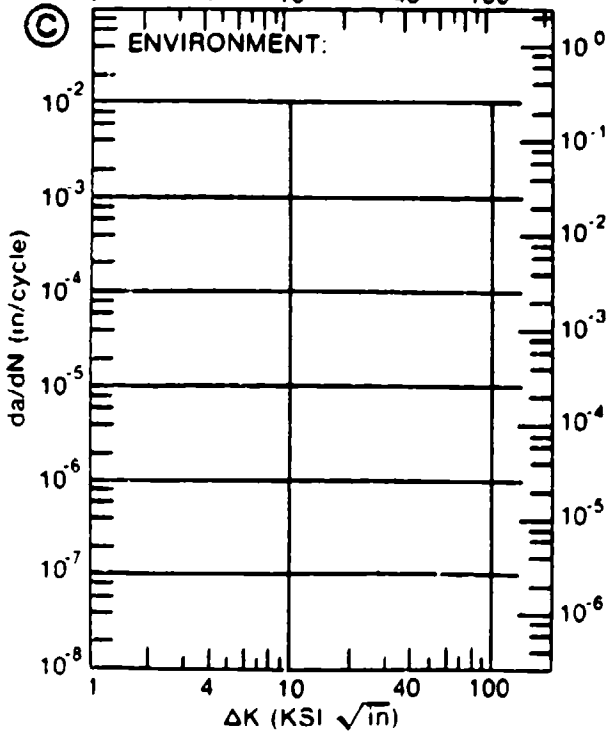
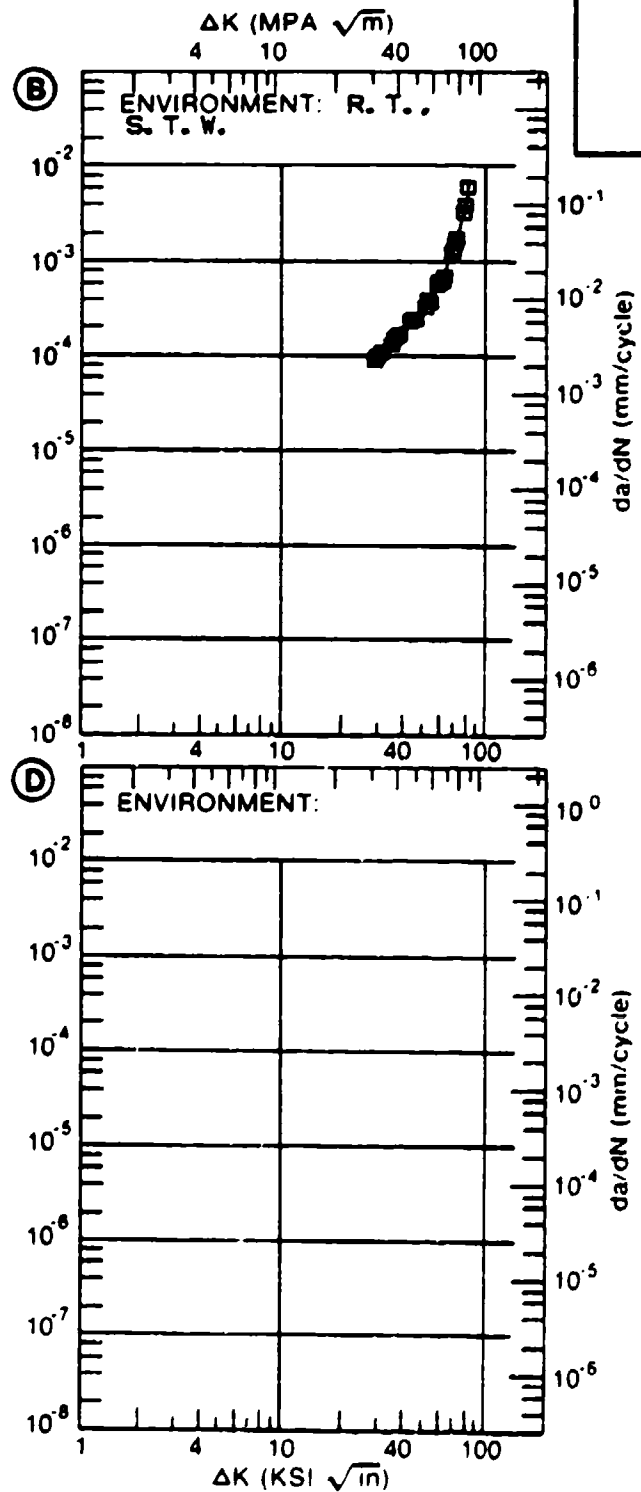
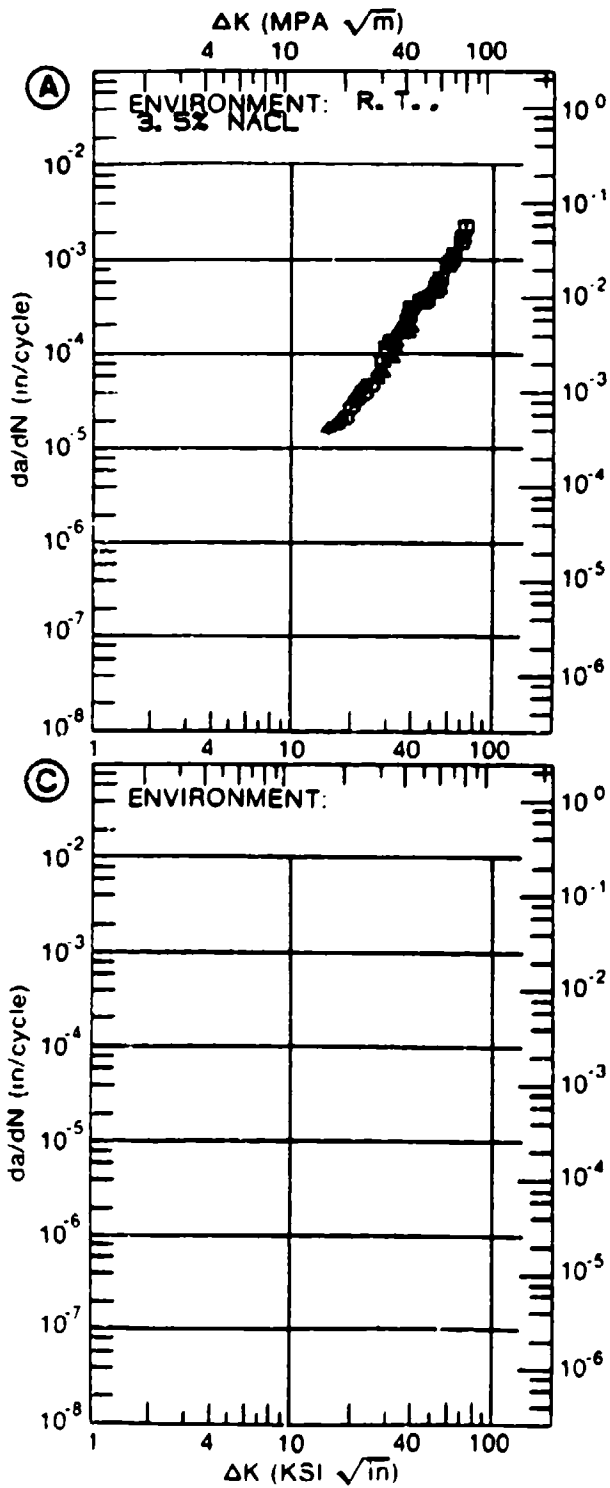


Figure 4.11.3.77

TABLE 4.11.3.78

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.78 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|--|-------------------------|---|
| CONDITION: RA | | | | | |
| DELTA K (KBI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY AIR | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. DIST. WATER | |
| DELTA K | A: 27.66 | 26.8 | | | |
| MIN | B: 28.99 | | 42.8 | | |
| | C: 14.90 | | | 3.43 | |
| | D: | | | | |
| | 16.00 | | | 6.83 | |
| | 20.00 | | | 19.0 | |
| | 25.00 | | | 34.4 | |
| | 30.00 | 37.9 | 47.2 | 63.3 | |
| | 35.00 | 66.1 | 70.6 | 105. | |
| | 40.00 | 101. | 99.2 | 152. | |
| | 50.00 | 224. | 204. | 254. | |
| | 60.00 | 582. | 507. | 468. | |
| | 70.00 | | 1547. | 1243. | |
| DELTA K | A: 62.76 | 787. | | | |
| MAX | B: 79.39 | | 5230. | | |
| | C: 78.93 | | | 8143. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 7.58 | 13.78 | 16.77 | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
 PREDICTION 0.5-0.8
 RATIO 0.8-1.25
 SUMMARY 1.25-2.0
 (NP/NA) >2.0

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

TITAN.
ALLOY

TI-6AL-4V

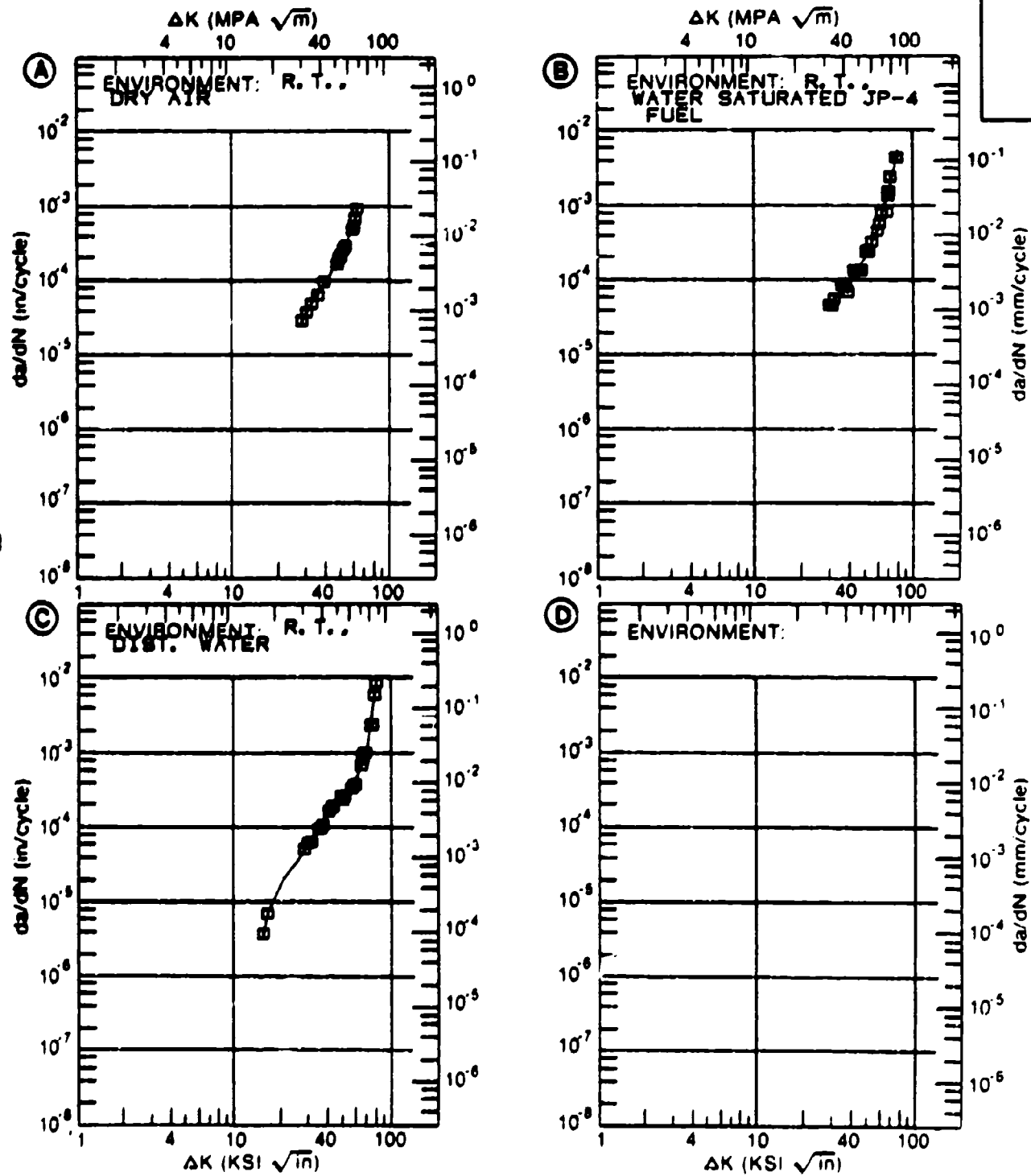


Figure 4.11.3.78

TABLE 4.11.3.79

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.79 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------------|------------------|---------------------------|----------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3. 5% NACL | E= R. T. S. T. W. | | |
| DELTA K MIN | A: 26. 28 | 363. | | | |
| | B: 30. 23 | | 143. | | |
| | C: | | | | |
| | D: | | | | |
| | 30. 00 | 642. | | | |
| | 35. 00 | 984. | 286. | | |
| | 40. 00 | 1262. | 449. | | |
| 50. 00 | 1852. | 905. | | | |
| 60. 00 | 3042. | 2145. | | | |
| 70. 00 | 6176. | | | | |
| DELTA K MAX | A: 75. 42 | 9991. | | | |
| | B: 60. 36 | | 2225. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 18. 75 | 15. 79 | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | | | | |
| SUMMARY (NP/NA) | 1. 25-2. 0 >2. 0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
 ALLOY
 TI-8AL-
 4V

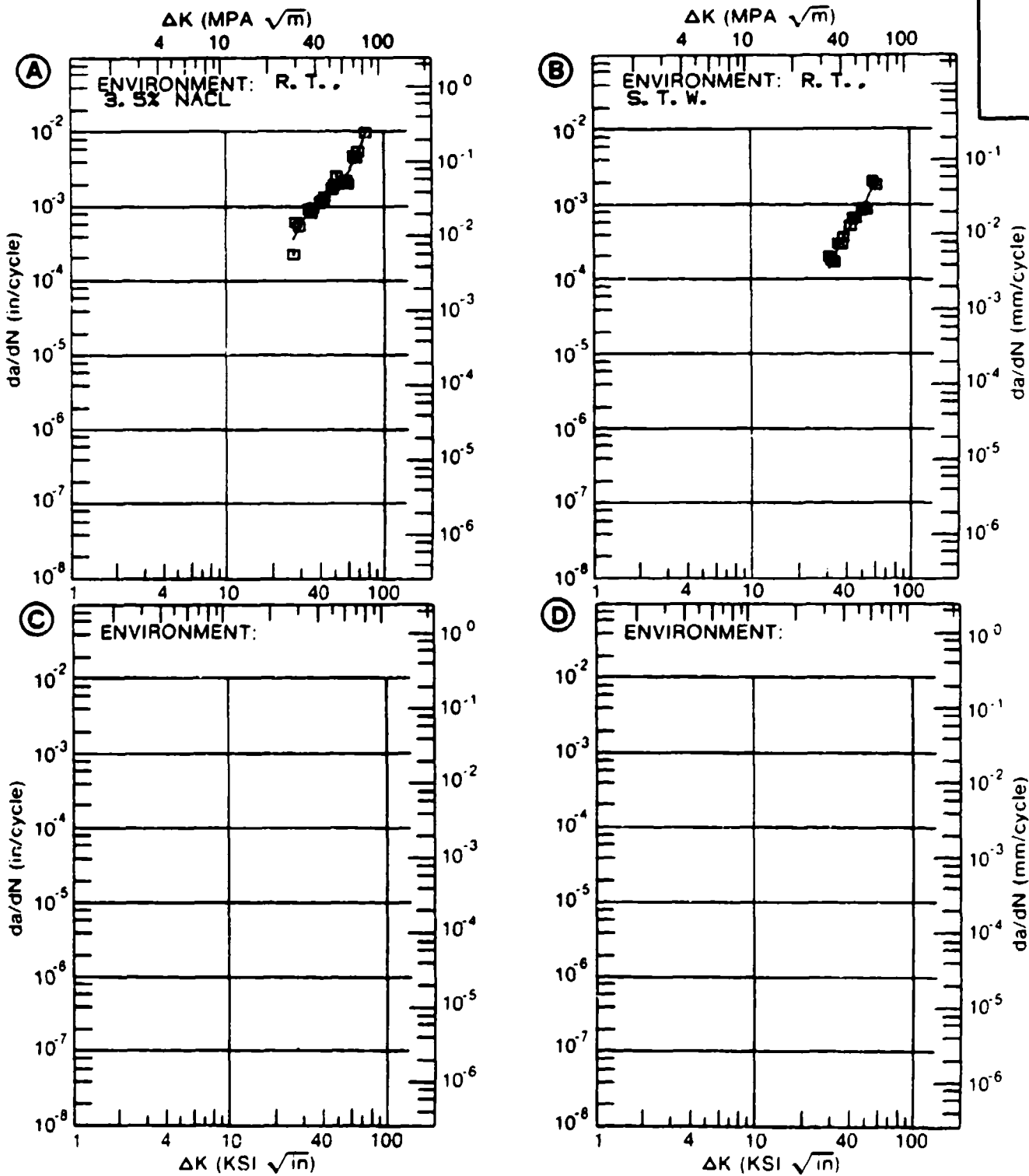


Figure 4.11.3.79

TABLE 4.11.3.80

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.80 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------|--|--|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY AIR | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. ALT JP-4 FUEL & DIST. WATER | |
| DELTA K | A: 7.95 | .364 | | | |
| MIN | B: 8.65 | | .789 | | |
| | C: 7.94 | | | 1.07 | |
| | D: | | | | |
| | 8.00 | .381 | | 1.07 | |
| | 9.00 | .840 | .950 | 1.16 | |
| | 10.00 | 1.52 | 1.53 | 1.55 | |
| | 13.00 | 4.71 | 4.57 | 6.24 | |
| | 16.00 | 9.13 | 9.49 | 19.1 | |
| | 20.00 | 17.2 | 18.4 | 35.4 | |
| | 25.00 | 34.7 | 35.1 | 51.4 | |
| | 30.00 | 71.5 | 64.4 | 80.0 | |
| | 35.00 | 157. | 120. | 157. | |
| | 40.00 | | 278. | | |
| DELTA K | A: 37.05 | 220. | | | |
| MAX | B: 45.45 | | 2354. | | |
| | C: 39.99 | | | 396. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.89 | 17.75 | 23.26 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-
4V

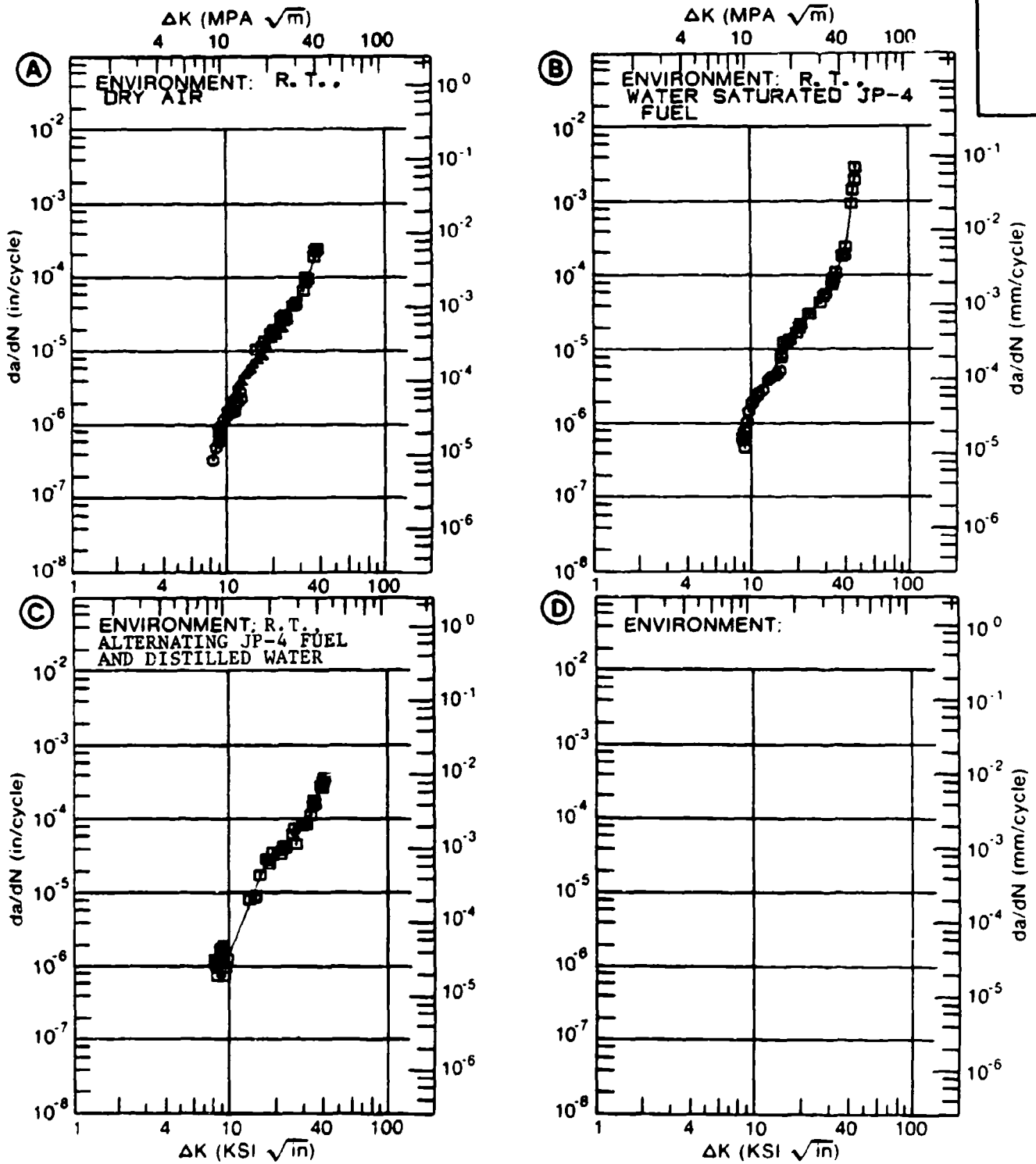


Figure 4.11.3.80

TABLE 4.11.3.81

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.81 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|------------|---------------------------------------|-----------------------|-------------------------|------------------------|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E=+ 175F DRY AIR | E=+ 175F JP-4 FUEL | E=+ 175F DIST. WATER | E=+ 175F 3. 5% NACL |
| DELTA K | A: 15. 65 | 6. 24 | | | |
| MIN | B: 16. 60 | | 10. 4 | | |
| | C: 15. 44 | | | 13. 0 | |
| | D: 16. 62 | | | | 39. 9 |
| | 16. 00 | 6. 72 | | 15. 2 | |
| | 20. 00 | 13. 3 | 16. 9 | 29. 6 | 266. |
| | 25. 00 | 24. 8 | 27. 0 | 43. 6 | 477. |
| | 30. 00 | 41. 7 | 40. 7 | 60. 8 | 537. |
| | 35. 00 | 67. 2 | 64. 2 | 93. 6 | 698. |
| | 40. 00 | 107. | 109. | 166. | 1277. |
| DELTA K | A: 42. 30 | 133. | | | |
| MAX | B: 45. 72 | | 219. | | |
| | C: 44. 48 | | | 314. | |
| | D: 46. 18 | | | | 4629. |
| ROOT MEAN SQUARE | | 9. 95 | 6. 80 | 6. 53 | 36. 25 |
| PERCENT ERROR | | | | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | | | | |
| SUMMARY | 1. 25-2. 0 | | | | |
| (NP/NA) | >2. 0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 99140

TITAN.
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TI-6AL-4V

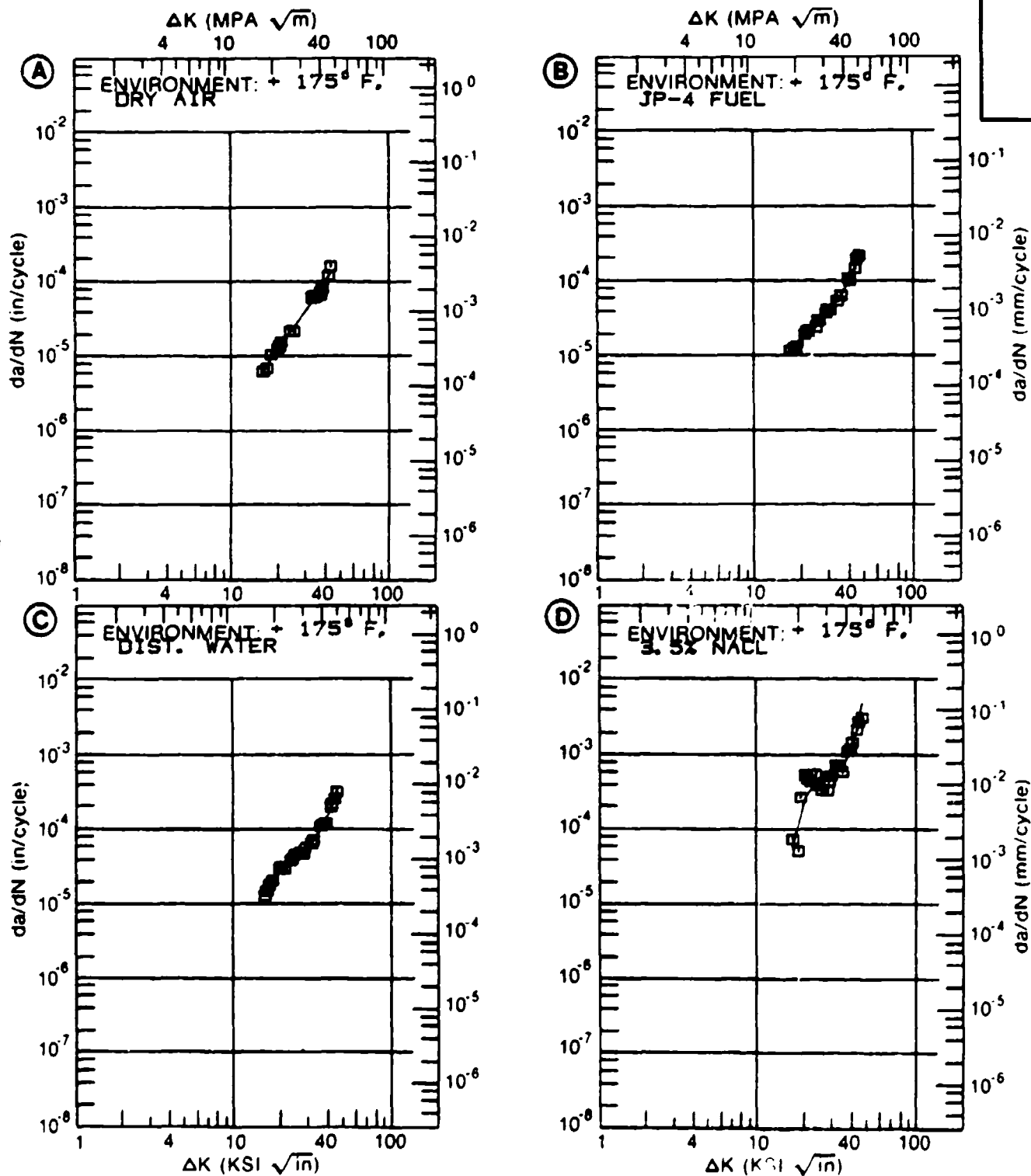


Figure 4.11.3.81

TABLE 4.11.3.82

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.82 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|---------------------------|--|-----------------------|----------------------|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DIST. WATER | E= R. T. DIST. H2O CRACK SPRAYED WITH LPS-3 | E= R. T. 3.5% NaCl | E= R. T. S. T. W. |
| DELTA K MIN | A: 8.08 | 507 | 11.9 | 1.02 | 1.21 |
| | B: 15.22 | | | | |
| | C: 8.86 | | | | |
| | D: 9.27 | | | | |
| | 9.00 | 1.26 | | 1.15 | |
| | 10.00 | 2.64 | | 2.65 | 2.02 |
| | 13.00 | 10.3 | | 20.3 | 9.56 |
| | 16.00 | 20.9 | 11.1 | 63.4 | 24.9 |
| | 20.00 | 36.8 | 22.8 | 117. | 52.5 |
| | 25.00 | 61.9 | 42.7 | 165. | 93.6 |
| | 30.00 | 102. | 65.0 | 236. | 149. |
| | 35.00 | 177. | 121. | 401. | 235. |
| | 40.00 | 394. | 369. | 838. | 384. |
| DELTA K MAX | A: 44.55 | 1764. | 8433. | 1937. | 403. |
| | B: 44.64 | | | | |
| | C: 44.53 | | | | |
| | D: 40.49 | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 15.72 | 32.49 | 30.11 | 12.99 |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-4V

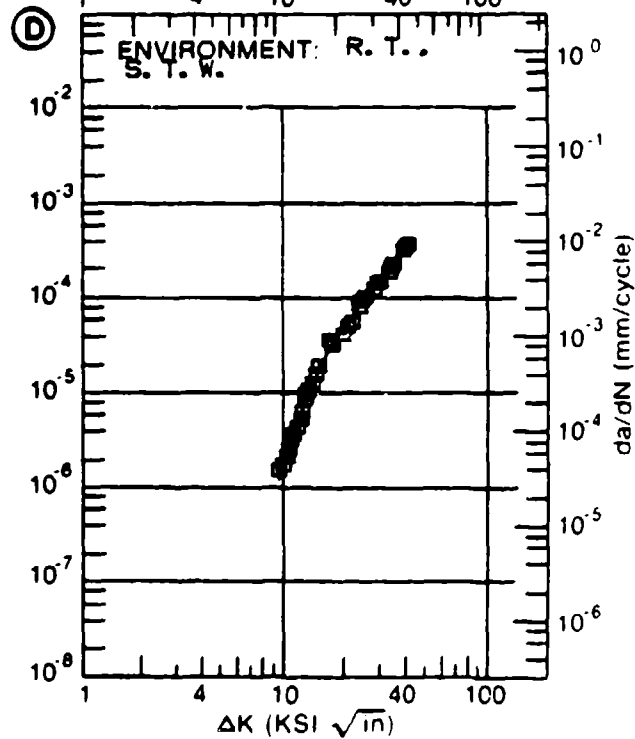
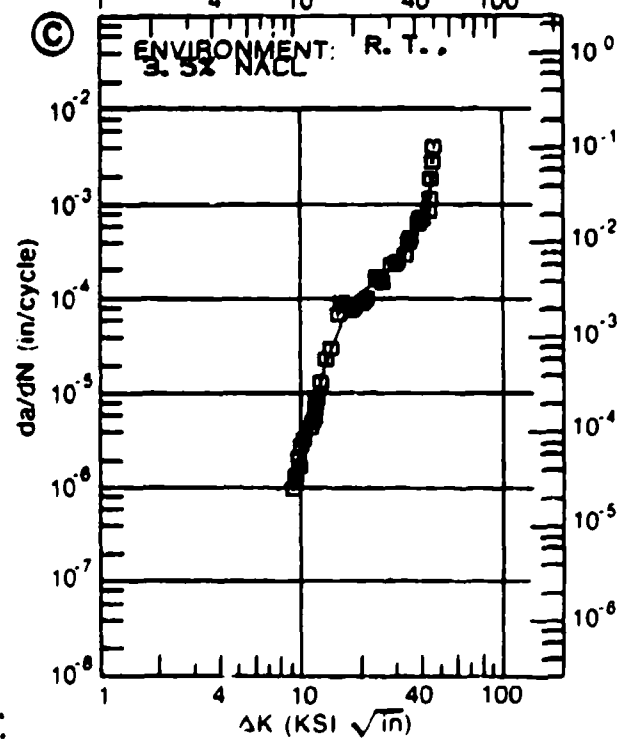
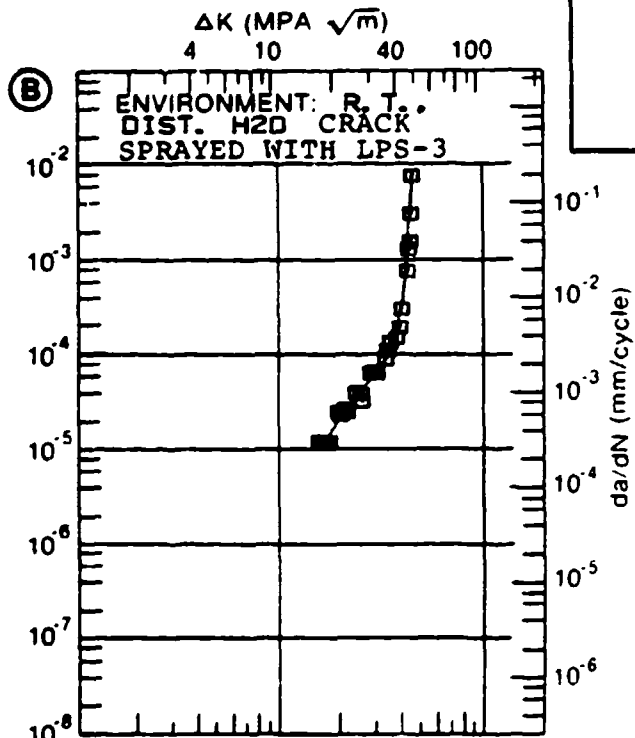
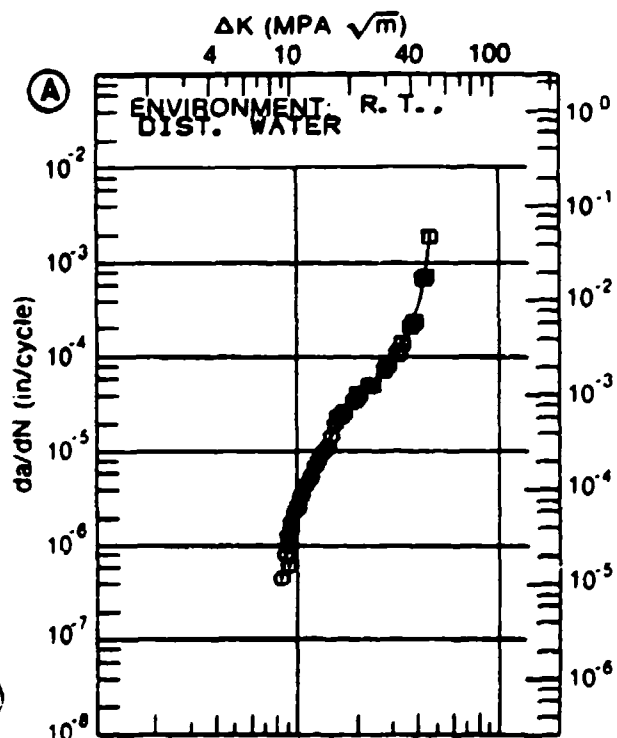


Figure 4.11.3.82

TABLE 4.11.3.83

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.83 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E=- 65F NITROGEN & AIR | | | |
| DELTA K | A: 17.05 | 5.84 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 12.2 | | | |
| | 25.00 | 21.7 | | | |
| | 30.00 | 37.0 | | | |
| | 35.00 | 83.7 | | | |
| DELTA K | A: 39.00 | 209. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.05 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-
4V

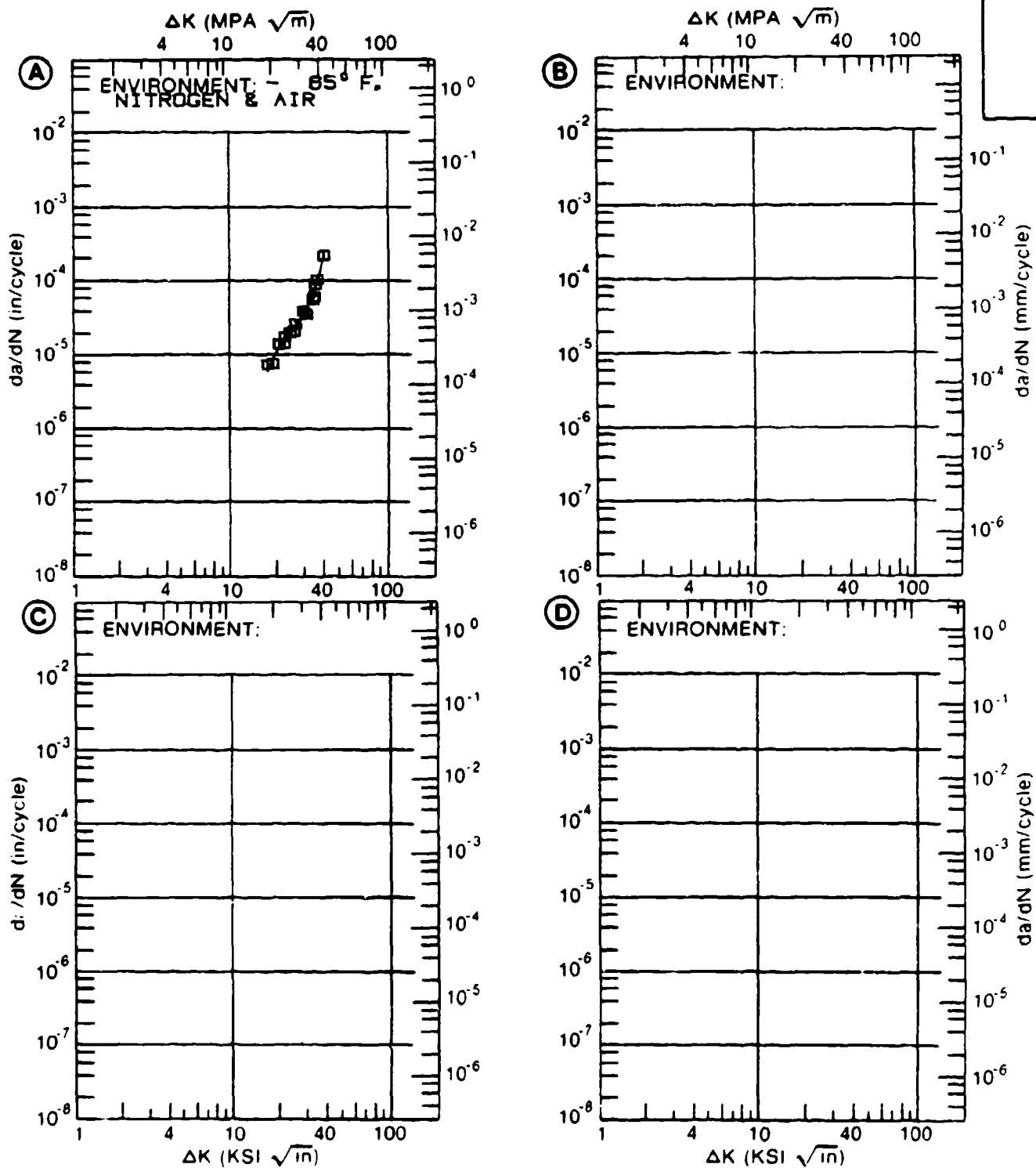


Figure 4.11.3.83

TABLE 4.11.3.84

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.84 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: RA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---|------------------------------|---|
| | A E= R. T. DRY AIR | B E= R. T. H2O SATURATED JP-4 FUEL | C E= R. T. DIST. WATER | D |
| A: 8.99 | .930 | | | |
| DELTA K B: 15.67 | | 12.1 | | |
| MIN C: 14.81 | | | 9.45 | |
| D: | | | | |
| 9.00 | .930 | | | |
| 10.00 | 1.08 | | | |
| 13.00 | 2.57 | | | |
| 16.00 | 6.86 | 12.3 | 12.2 | |
| 20.00 | 20.4 | 17.0 | 21.8 | |
| 25.00 | 48.6 | 36.3 | 43.6 | |
| 30.00 | 70.2 | 70.5 | 117. | |
| 35.00 | | 128. | 391. | |
| 40.00 | | 302. | 1251. | |
| A: 31.84 | 72.2 | | | |
| DELTA K B: 46.00 | | 2006. | | |
| MAX C: 40.19 | | | 1196. | |
| D: | | | | |
| ROOT MEAN SQUARE | 92.37 | 14.73 | 12.84 | |
| PERCENT ERROR | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 99140

TITAN.
 ALLOY
 TI-6AL-
 4V

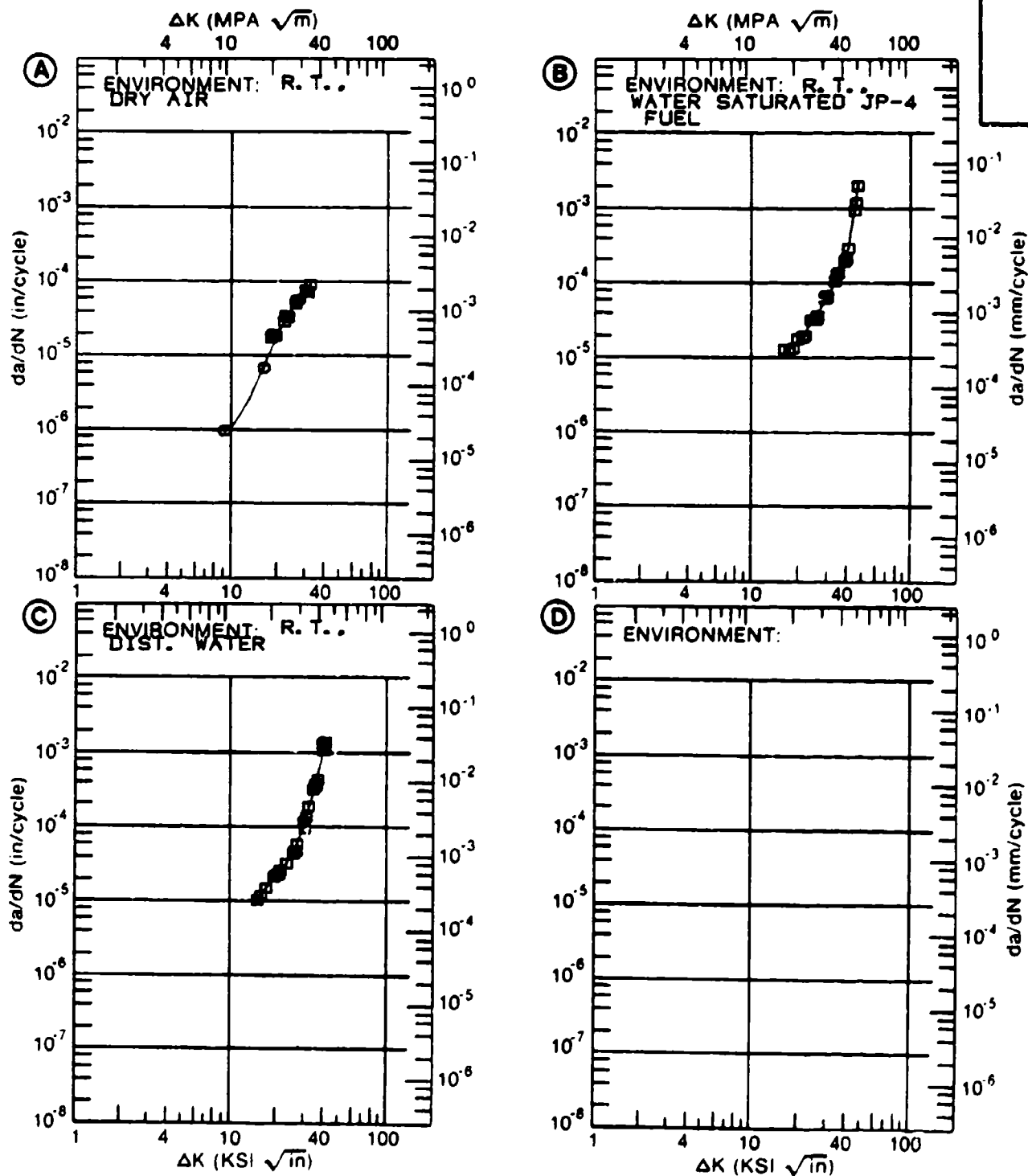


Figure 4.11.3.84

TABLE 4.11.3.85

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.85 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|----------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3.5% NaCl | E= R. T. S. T. W. | | |
| DELTA K | A: 7.97 | .992 | | | |
| MIN | B: 22.18 | | 77.7 | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | 1.02 | | | |
| | 9.00 | 1.82 | | | |
| | 10.00 | 2.55 | | | |
| | 13.00 | 5.07 | | | |
| | 16.00 | 14.8 | | | |
| | 20.00 | | | | |
| | 25.00 | | 160. | | |
| | 30.00 | | 209. | | |
| DELTA K | A: 19.93 | 31.4 | | | |
| MAX | B: 34.79 | | 262. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 21.59 | 10.99 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

TITAN.
ALLOY

TI-6AL-4V

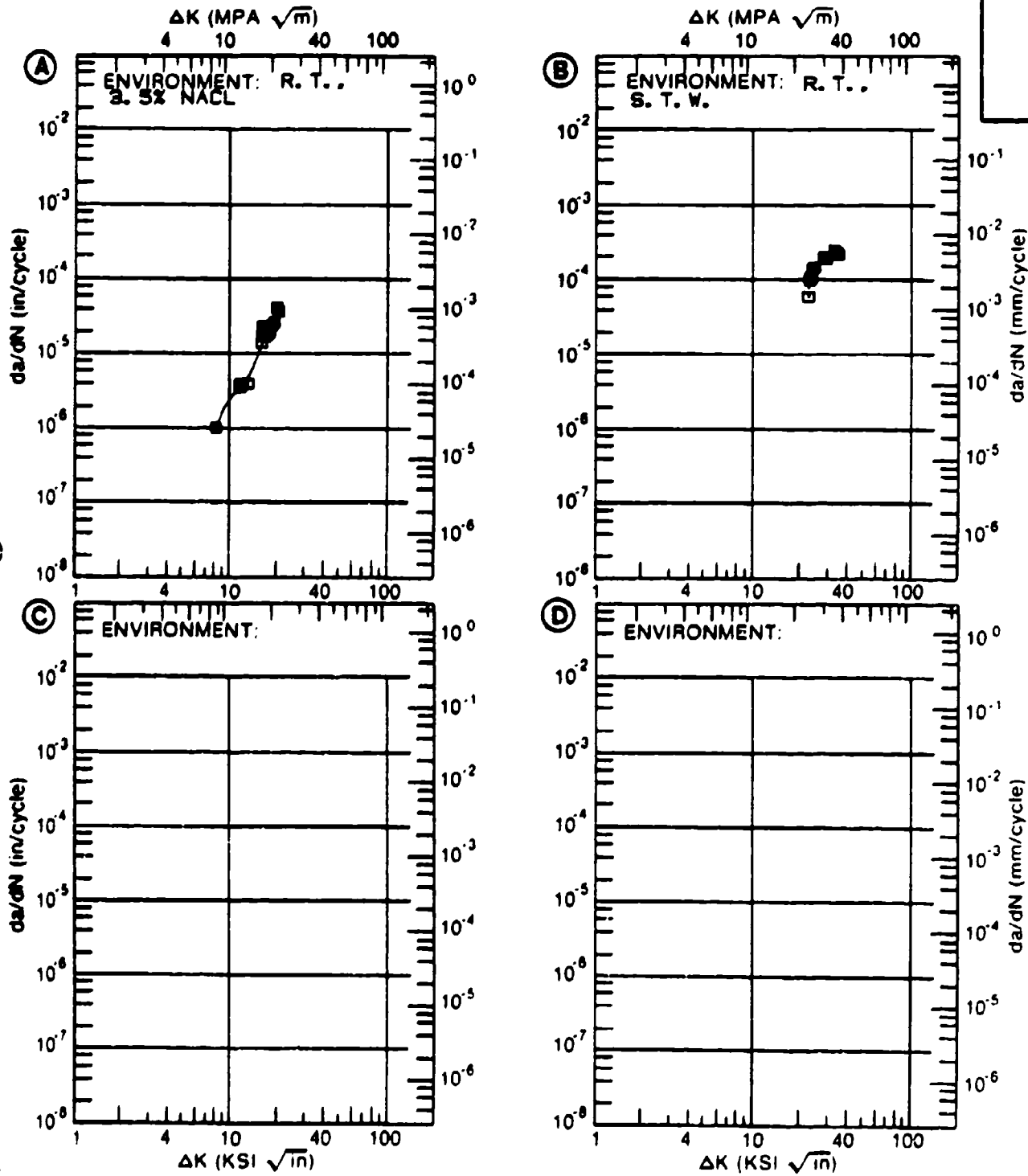


Figure 4.11.3.85

TABLE 4.11.3.86

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.86 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|------------|--------------------------------------|---------|---------|---------|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , L. H. A. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | R=+0.50 | R=+0.70 |
| | A: 5.98 : | .0135 | | | |
| DELTA K | B: 6.12 : | | .109 | | |
| MIN | C: 6.39 : | | | .226 | |
| | D: 5.11 : | | | | .146 |
| | 6.00 : | .0139 | | | .375 |
| | 7.00 : | .0485 | .229 | .371 | .798 |
| | 8.00 : | .127 | .464 | .726 | 1.40 |
| | 9.00 : | .270 | .839 | 1.25 | 2.17 |
| | 10.00 : | .499 | 1.39 | 1.94 | 3.12 |
| | 13.00 : | 1.84 | 4.24 | 5.08 | 7.33 |
| | 16.00 : | 4.30 | 8.75 | 9.54 | 14.9 |
| | 20.00 : | 9.42 | 15.9 | 16.8 | |
| | 25.00 : | 19.0 | 23.2 | | |
| | 30.00 : | 32.7 | | | |
| | 35.00 : | 52.2 | | | |
| | 40.00 : | 79.4 | | | |
| | 50.00 : | 171. | | | |
| DELTA K | A: 52.96 : | 213. | | | |
| MAX | B: 25.92 : | | 24.1 | | |
| | C: 20.65 : | | | 18.1 | |
| | D: 19.21 : | | | | 30.8 |
| ROOT MEAN SQUARE | | 33.97 | 20.34 | 21.38 | 6.79 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | 1 | 1 | |
| RATIO | 0.8-1.25 | 2 | 1 | 1 | 1 |
| SUMMARY | 1.25-2.0 | 3 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 6.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 113.0- 121.0 KSI
 ULT. STRENGTH: 127.0- 135.0 KSI
 SPECIMEN THK: 0.990- 1.000"
 SPECIMEN WIDTH: 7.400- 7.410"
 REFERENCES: 8579, 8587

TITAN.
 ALLOY
 TI-6AL-
 4V

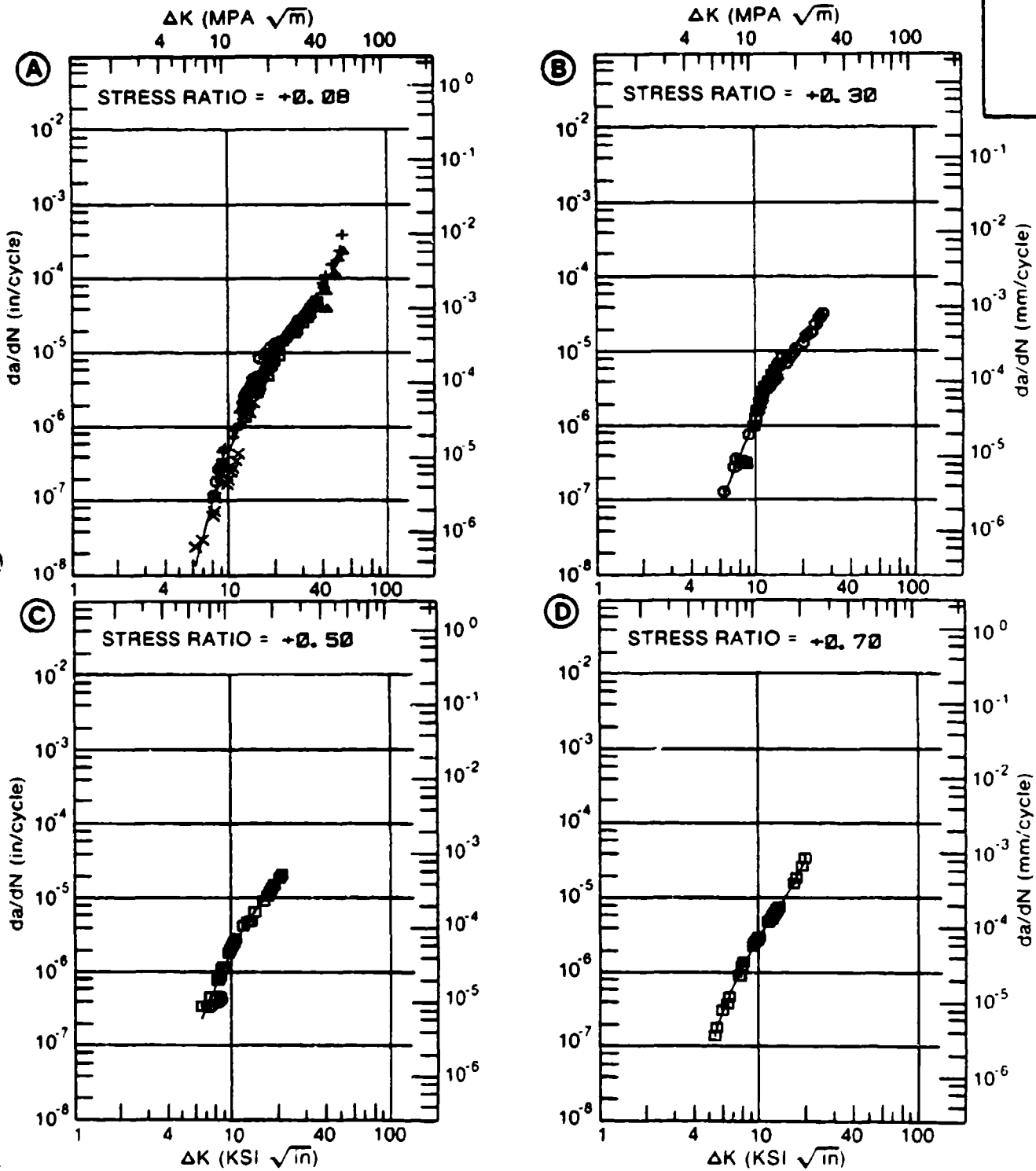


Figure 4.11.3.86

TABLE 4.11.3.87

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.87 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------|---------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | R=+0.50 | |
| | A: | .340 | | | |
| DELTA K | B: | | .385 | | |
| MIN | C: | | | .293 | |
| | D: | | | | |
| | 6.00 : | | | .300 | |
| | 7.00 : | | | .649 | |
| | 8.00 : | | .784 | 1.32 | |
| | 9.00 : | .423 | 1.37 | 2.46 | |
| | 10.00 : | .590 | 2.27 | 4.23 | |
| | 13.00 : | 1.52 | 7.32 | 13.5 | |
| | 16.00 : | 3.49 | 19.3 | 24.6 | |
| | 20.00 : | 8.98 | 24.5 | | |
| | 25.00 : | 23.4 | | | |
| | 30.00 : | 50.6 | | | |
| | 35.00 : | 94.6 | | | |
| | 40.00 : | 158. | | | |
| | 50.00 : | 344. | | | |
| | 60.00 : | 591. | | | |
| DELTA K | A: | 772. | | | |
| MAX | B: | | 26.4 | | |
| | C: | | | 28.0 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 58.58 | 11.40 | 10.86 | |
| PERCENT ERROR | | | | | |

| | | | | |
|------------|----------|---|---|---|
| LIFE | 0.0-0.5 | | | |
| PREDICTION | 0.5-0.8 | 2 | | |
| RATIO | 0.8-1.25 | | 1 | 1 |
| SUMMARY | 1.25-2.0 | 2 | | |
| (NP/NA) | >2.0 | | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 118.0 - 124.0 KSI
 ULT. STRENGTH: 129.0 - 138.0 KSI
 SPECIMEN THK: 0.988 - 0.998"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837, 88579

TITAN.
 ALLOY

TI-6AL-
 4V

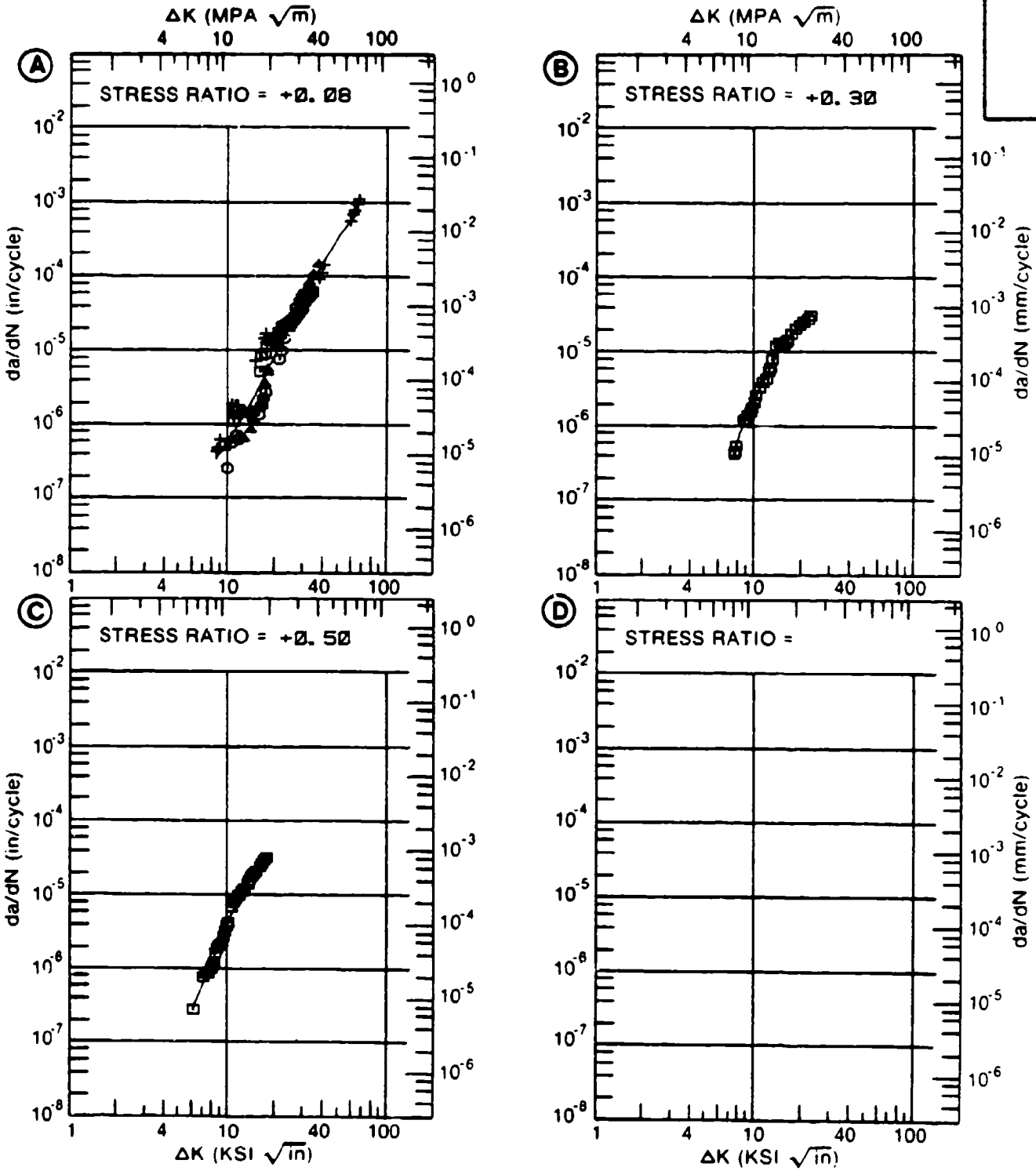


Figure 4.11.3.87

TABLE 4.11.3.88

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.88 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|-------|----------|---|
| | | A | B | C | D |
| | | E= 65F | | E= R. T. | |
| | | L. H. A. | | L. H. A. | |
| DELTA K MIN | A: 12.57 | 2.09 | | | |
| | B: 5.98 | | .0135 | | |
| | C: | | | | |
| | D: | | | | |
| | 6.00 | | .0139 | | |
| | 7.00 | | .0485 | | |
| | 8.00 | | .127 | | |
| | 9.00 | | .270 | | |
| | 10.00 | | .499 | | |
| | 13.00 | 2.46 | 1.84 | | |
| | 16.00 | 5.61 | 4.30 | | |
| | 20.00 | 11.1 | 9.42 | | |
| | 25.00 | 20.6 | 19.0 | | |
| | 30.00 | 36.8 | 32.7 | | |
| | 35.00 | | 52.2 | | |
| | 40.00 | | 79.4 | | |
| | 50.00 | | 171. | | |
| DELTA K MAX | A: 31.93 | 46.2 | | | |
| | B: 52.96 | | 213. | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 4.90 33.97
PERCENT ERROR

| | | | |
|-----------------|----------|---|---|
| LIFE PREDICTION | 0.0-0.5 | | |
| RATIO | 0.5-0.8 | | |
| SUMMARY (NP/NA) | 0.8-1.25 | 1 | 2 |
| | 1.25-2.0 | | 3 |
| | >2.0 | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 113.0- 121.0 KSI
 ULT. STRENGTH: 127.0- 135.0 KSI
 SPECIMEN THK: 0.990- 1.000"
 SPECIMEN WIDTH: 7.400- 7.410"
 REFERENCES: 85837, 88579

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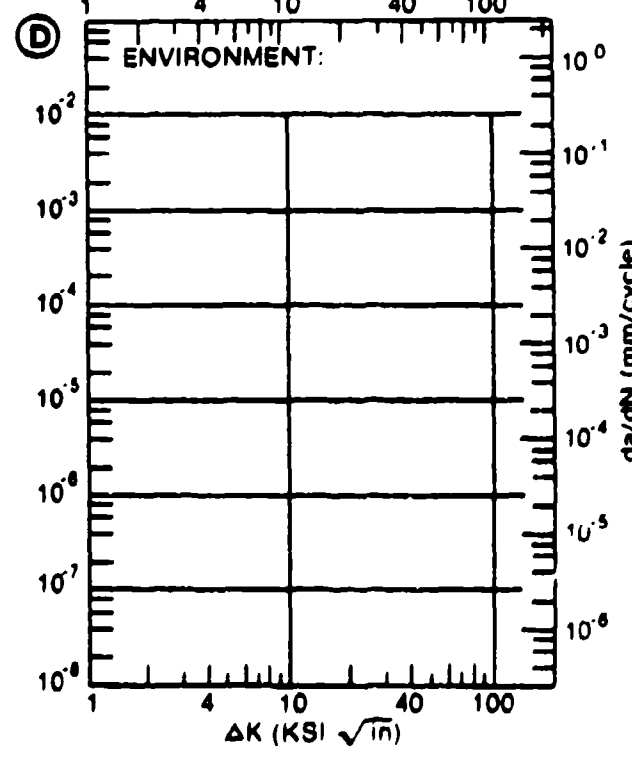
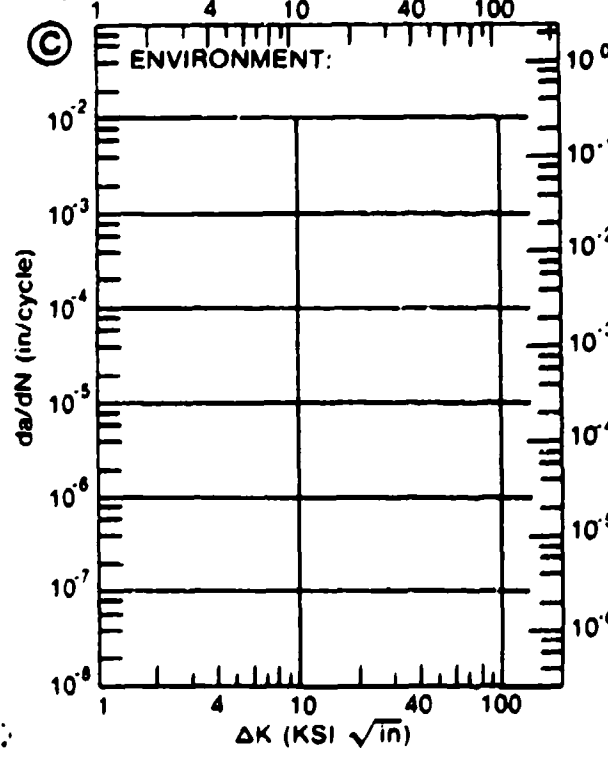
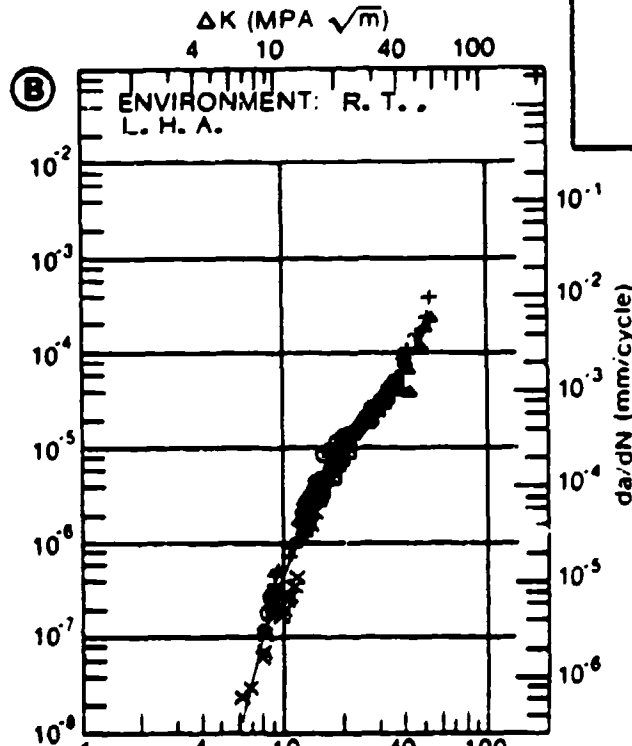
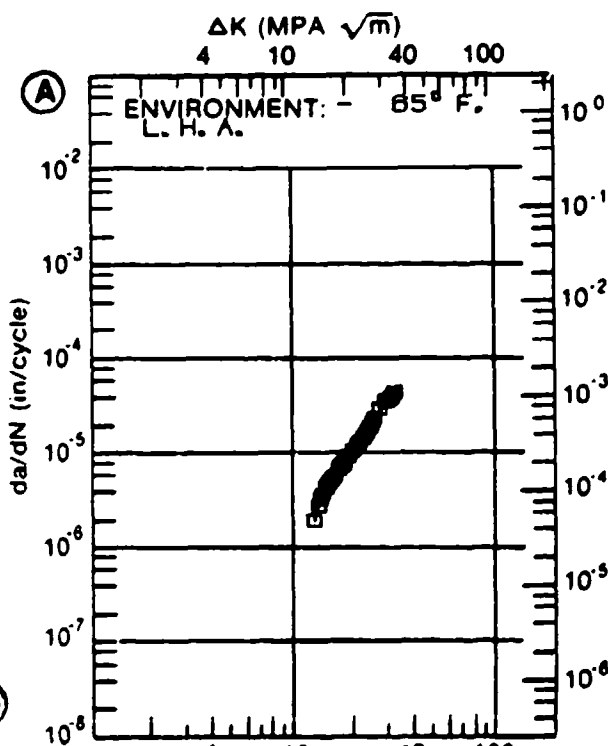


Figure 4.11.3.88

TABLE 4.11.3.89

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.89 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|--------------------------------------|----------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | E=+ 265F | | |
| | | L. H. A. | L. H. A. | | |
| DELTA K MIN | A: 8.22 | .230 | | | |
| | B: 14.47 | | 3.05 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .401 | | | |
| | 10.00 | .728 | | | |
| | 13.00 | 2.59 | | | |
| | 16.00 | 5.76 | 5.05 | | |
| | 20.00 | 11.3 | 11.6 | | |
| | 25.00 | 18.6 | 21.8 | | |
| 30.00 | | 36.8 | | | |
| DELTA K MAX | A: 28.48 | 23.2 | | | |
| | B: 32.07 | | 45.8 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 13.20 | 8.62 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 1 | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 118.0- 121.0 KSI
 ULT. STRENGTH: 129.0- 134.0 KSI
 SPECIMEN THK: 0.254- 0.990"
 SPECIMEN WIDTH: 5.000- 7.400"
 REFERENCES: 85837, 88579

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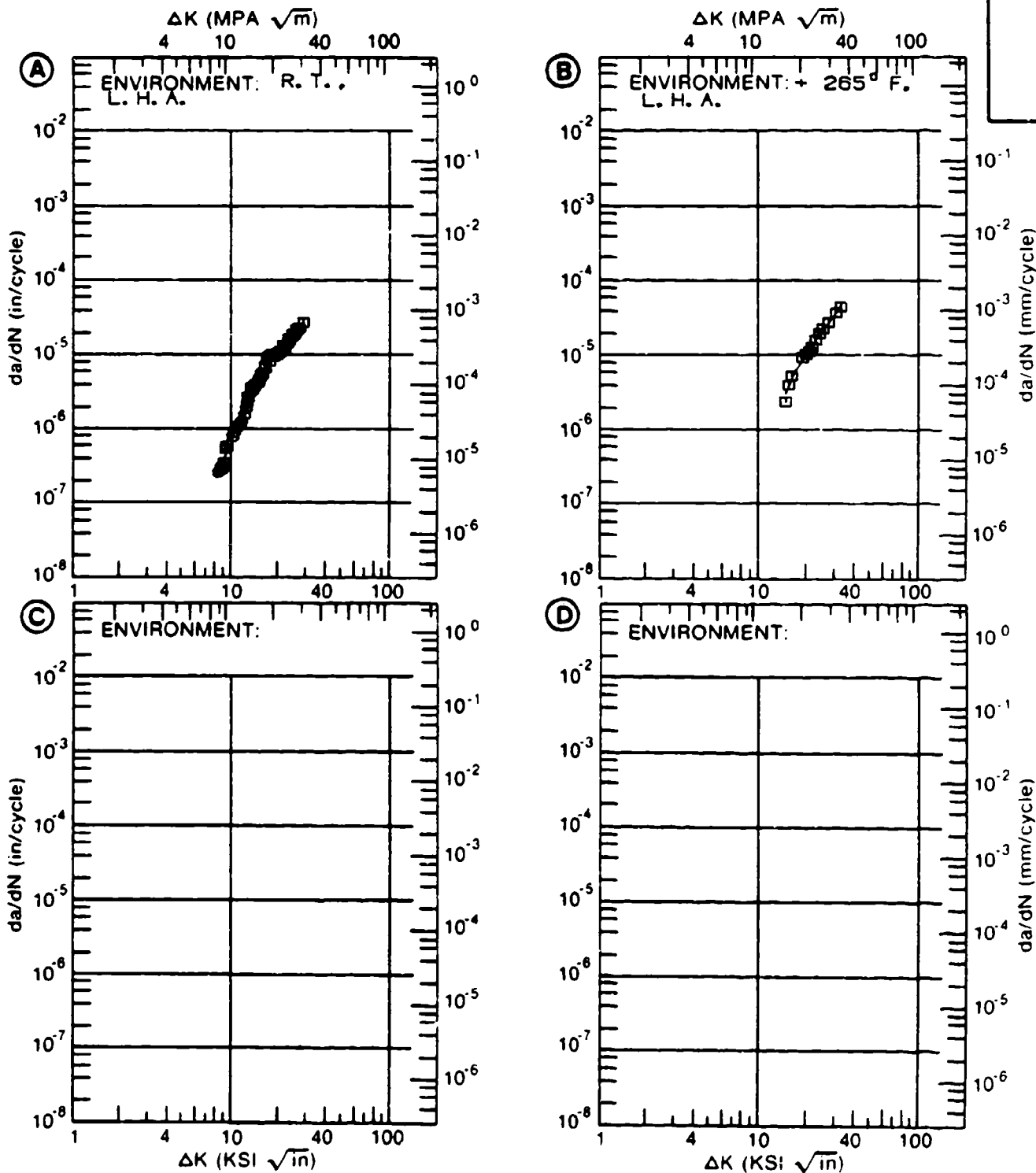


Figure 4.11.3.89

TABLE 4.11.3.90

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.90 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: RA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|---------------------------------------|--|--------------------------|---------------------|----------------------|---|
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. J. P. 4 | E=+ 150F S. T. W. | |
| DELTA K MIN | A: 24.00 | 14.4 | | | |
| | B: 7.83 | | .107 | | |
| | C: 12.49 | | | 2.27 | |
| | D: | | | | |
| | 8.00 | | .126 | | |
| | 9.00 | | .308 | | |
| | 10.00 | | .663 | | |
| | 13.00 | | 3.00 | 2.73 | |
| | 16.00 | | 6.83 | 5.97 | |
| | 20.00 | | 12.8 | 11.8 | |
| | 25.00 | 16.6 | 20.2 | 24.4 | |
| | 30.00 | 30.7 | | 53.4 | |
| | 35.00 | 50.0 | | | |
| | 40.00 | 74.7 | | | |
| DELTA K MAX | A: 41.69 | 84.3 | | | |
| | B: 26.71 | | 22.7 | | |
| | C: 33.71 | | | 102. | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 4.34 | 20.62 | 16.88 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 | 1 | 1 | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 117.0- 121.0 KSI
 ULT. STRENGTH: 129.0- 135.0 KSI
 SPECIMEN THK: 0.992- 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837, 88579

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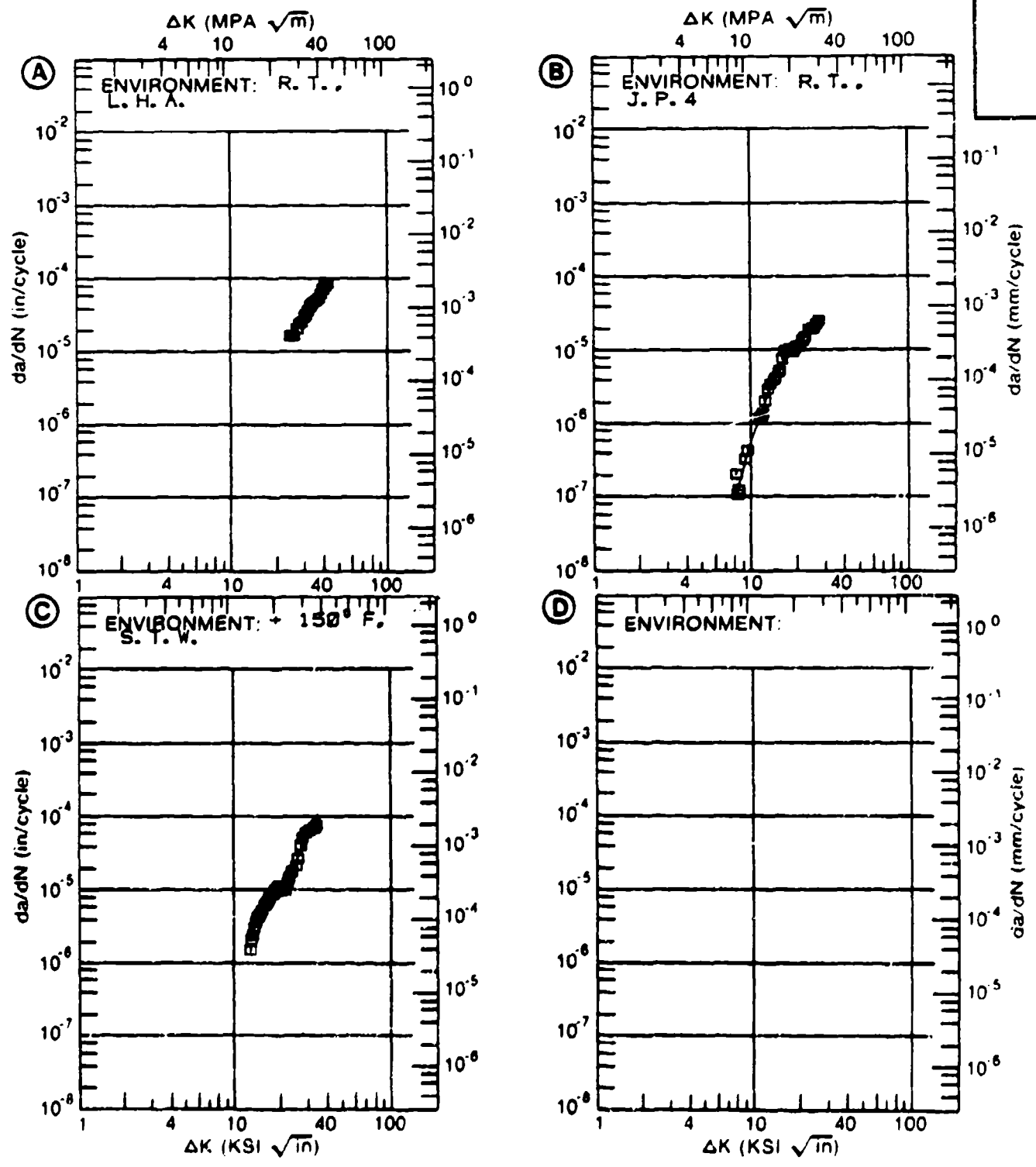


Figure 4.11.3.90

TABLE 4.11.3.91

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
 ΔK STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.91 INDICATING EFFECT
 OF FREQUENCY

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-------------------------------|----------|---------------------------|-------|-------------|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. , S. T. W. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | F(HZ)= 0.10 | | F(HZ)= 1.00 | |
| DELTA K | A: 11.17 | 1.07 | | | |
| MIN | B: 8.35 | | .340 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | | .423 | | |
| | 10.00 | | .590 | | |
| | 13.00 | 2.24 | 1.52 | | |
| | 16.00 | 4.15 | 3.49 | | |
| | 20.00 | 11.0 | 8.98 | | |
| | 25.00 | 21.4 | 23.4 | | |
| | 30.00 | 49.0 | 50.6 | | |
| | 35.00 | | 94.6 | | |
| | 40.00 | | 158. | | |
| | 50.00 | | 344. | | |
| | 60.00 | | 591. | | |
| DELTA K | A: 32.56 | 89.8 | | | |
| MAX | B: 66.77 | | 772. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.74 | 58.58 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | 2 | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | 2 | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 118.0 - 124.0 KSI
 ULT. STRENGTH: 129.0 - 138.0 KSI
 SPECIMEN THK: 0.988 - 1.010"
 SPECIMEN WIDTH: 7.380 - 7.400"
 REFERENCES: 88579, 85837

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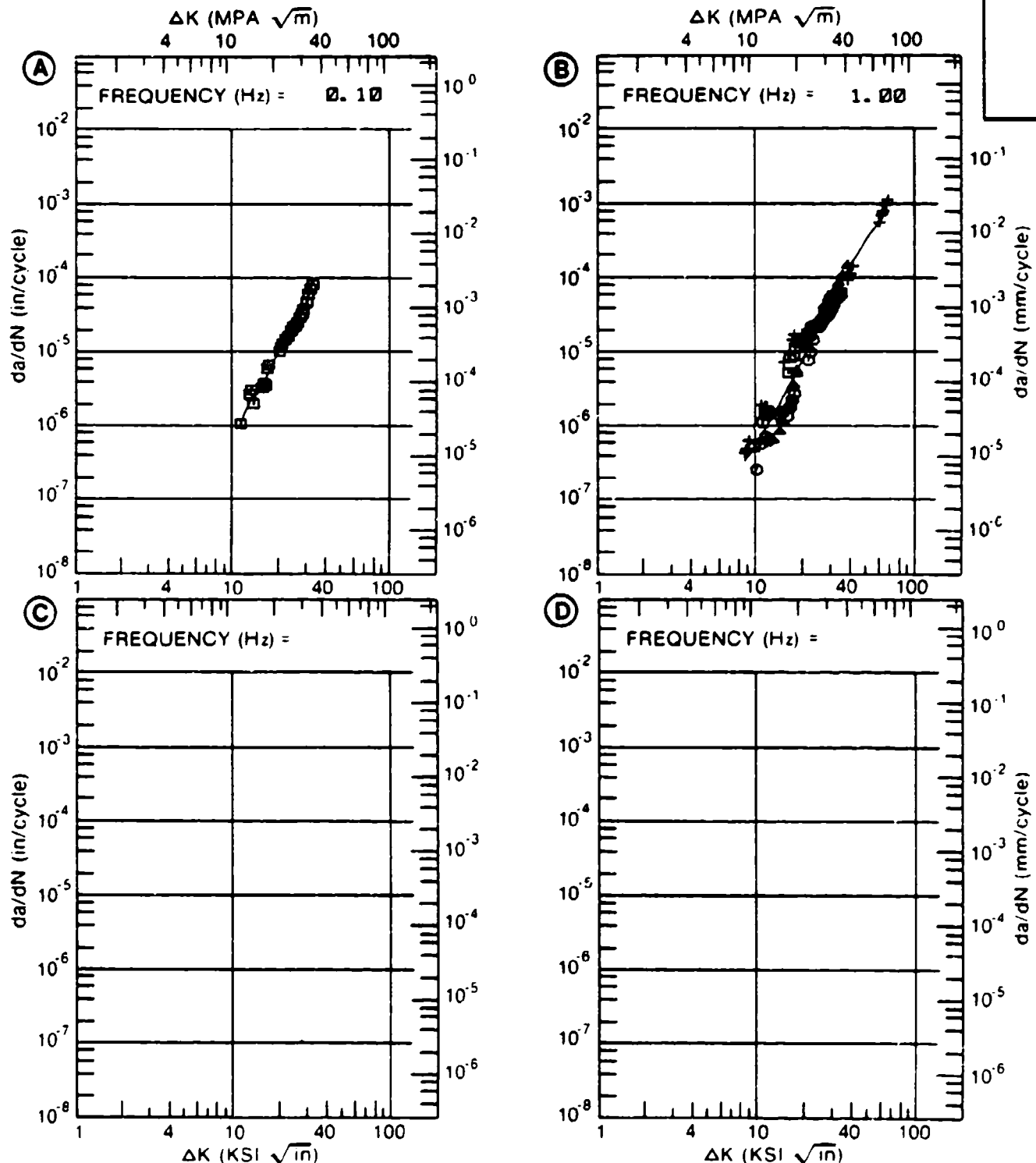


Figure 4.11.3.91

TABLE 4.11.3.92

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.92 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|-----------------------------------|---|--|--------------------------------------|---|
| | A | B | C | D |
| | E= R. T. L. H. A. 6HZ | E= R. T. J. P. 4 1HZ | E= R. T. S. T. W. 1HZ | |
| DELTA K MIN | A: 8.94 : B: 7.99 : C: 6.08 : D: : | .231 | .226 | .0803 |
| | 7.00 : 8.00 : 9.00 : 10.00 : 13.00 : 16.00 : 20.00 : 25.00 : 30.00 : 35.00 : 40.00 : 50.00 : 60.00 : 70.00 : | .244 .537 2.45 5.74 11.4 20.2 32.0 49.9 78.5 208. 609. | .226 .375 3.58 7.91 14.2 | .175 .346 .604 .964 2.78 5.93 12.7 26.3 47.6 79.4 126. 285. 592. 1160. |
| DELTA K MAX | A: 63.39 : B: 24.76 : C: 71.06 : D: : | 893. | 25.7 | 1242. |
| ROOT MEAN SQUARE PERCENT ERROR | | 27.79 | 12.87 | 33.61 |

| | | | | |
|--------------------|------------------|---|---|---|
| LIFE | 0.0-0.5 | | | |
| PREDICTION | 0.5-0.8 | 1 | | 1 |
| RATIO | 0.8-1.25 | 1 | 1 | |
| SUMMARY (NP/NA) | 1.25-2.0 >2.0 | 1 | | 1 |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 122.0- 125.0 KSI
 ULT. STRENGTH: 134.0- 135.0 KSI
 SPECIMEN THK: 0.501- 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837, 88579

TITAN.
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TI-6AL-
4V

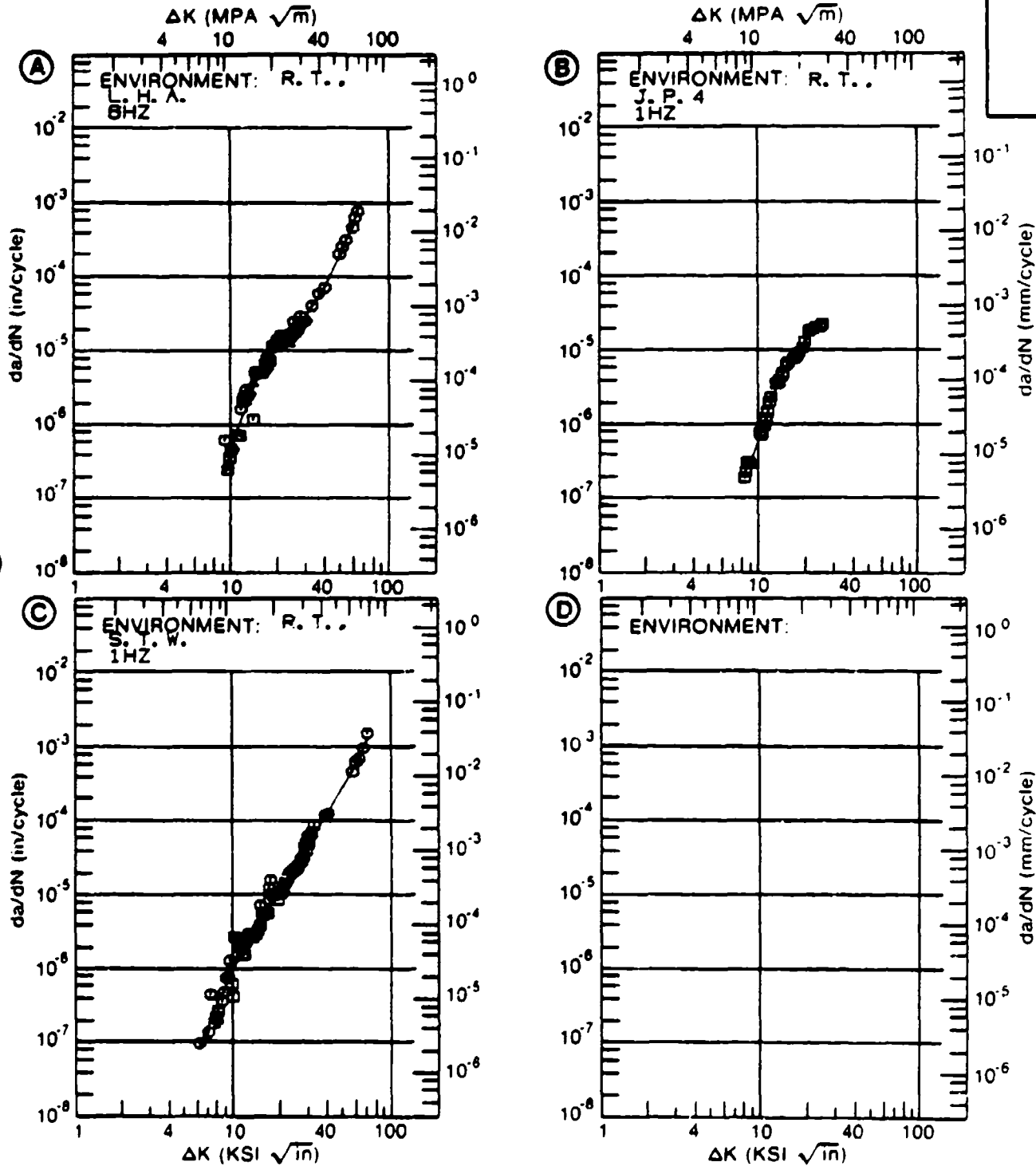


Figure 4.11.3.92

TABLE 4.11.3.93

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.93 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | F. C. S. | | | |
| DELTA K | A: 13.81 | 3.33 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 4.56 | | | |
| | 20.00 | 8.72 | | | |
| | 25.00 | 16.8 | | | |
| | 30.00 | 24.7 | | | |
| DELTA K | A: 30.21 | 24.9 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 4.69 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 117.0 KSI
 ULT. STRENGTH: 133.0 KSI
 SPECIMEN THK: 1.390"
 SPECIMEN WIDTH: 4.000"
 REFERENCES: 88579

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4V

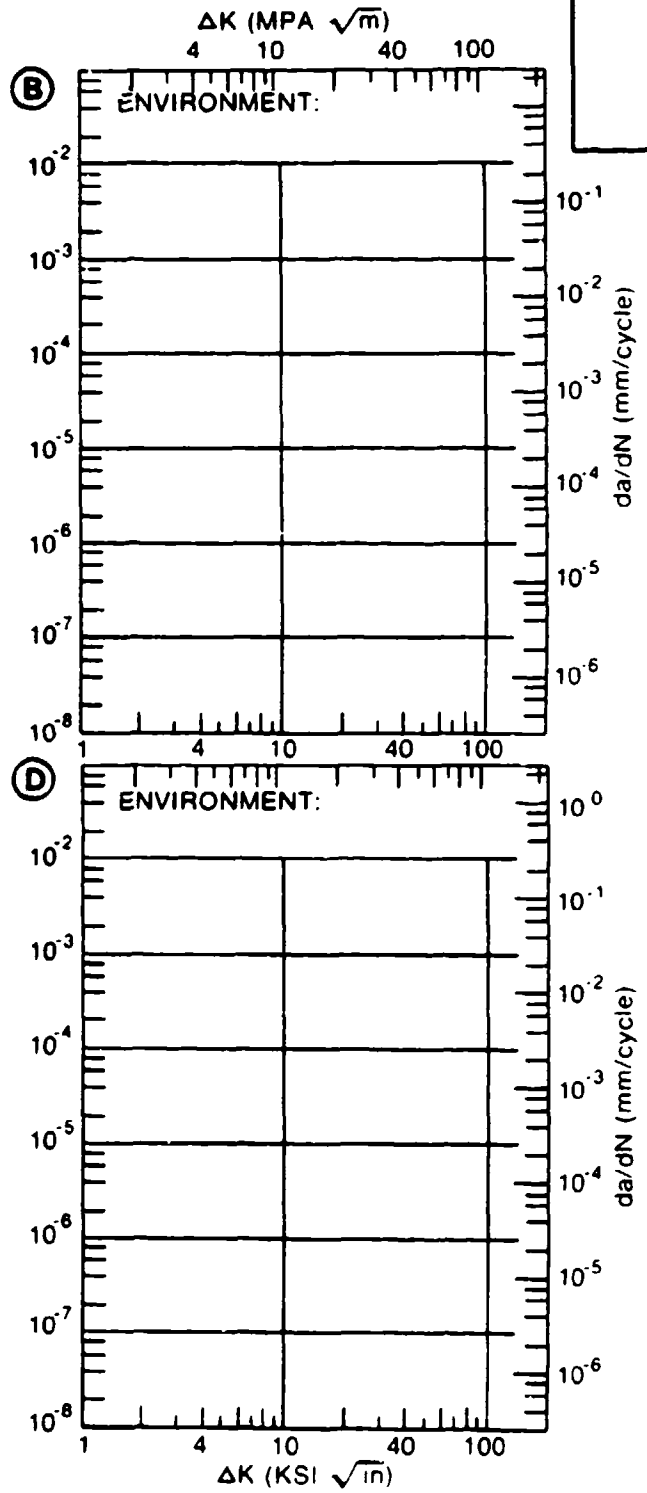
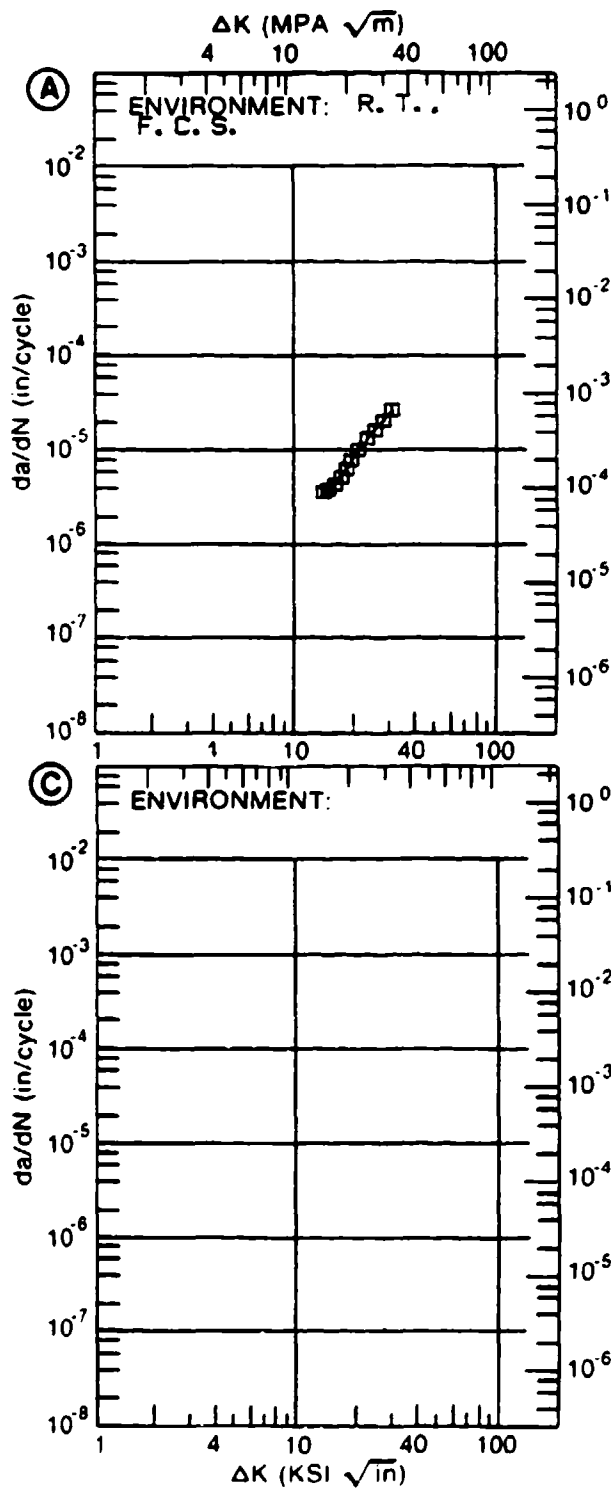


Figure 4.11.3.93

TABLE 4.11.3.94

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.94 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| DELTA K | A: 11.70 | 1.48 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 2.98 | | | |
| DELTA K | A: 15.81 | 5.79 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 10.94 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 1.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 121.0 KSI
 ULT. STRENGTH: 135.0 KSI
 SPECIMEN THK: 1.013"
 SPECIMEN WIDTH: 7.380"
 REFERENCES: 85837

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4V

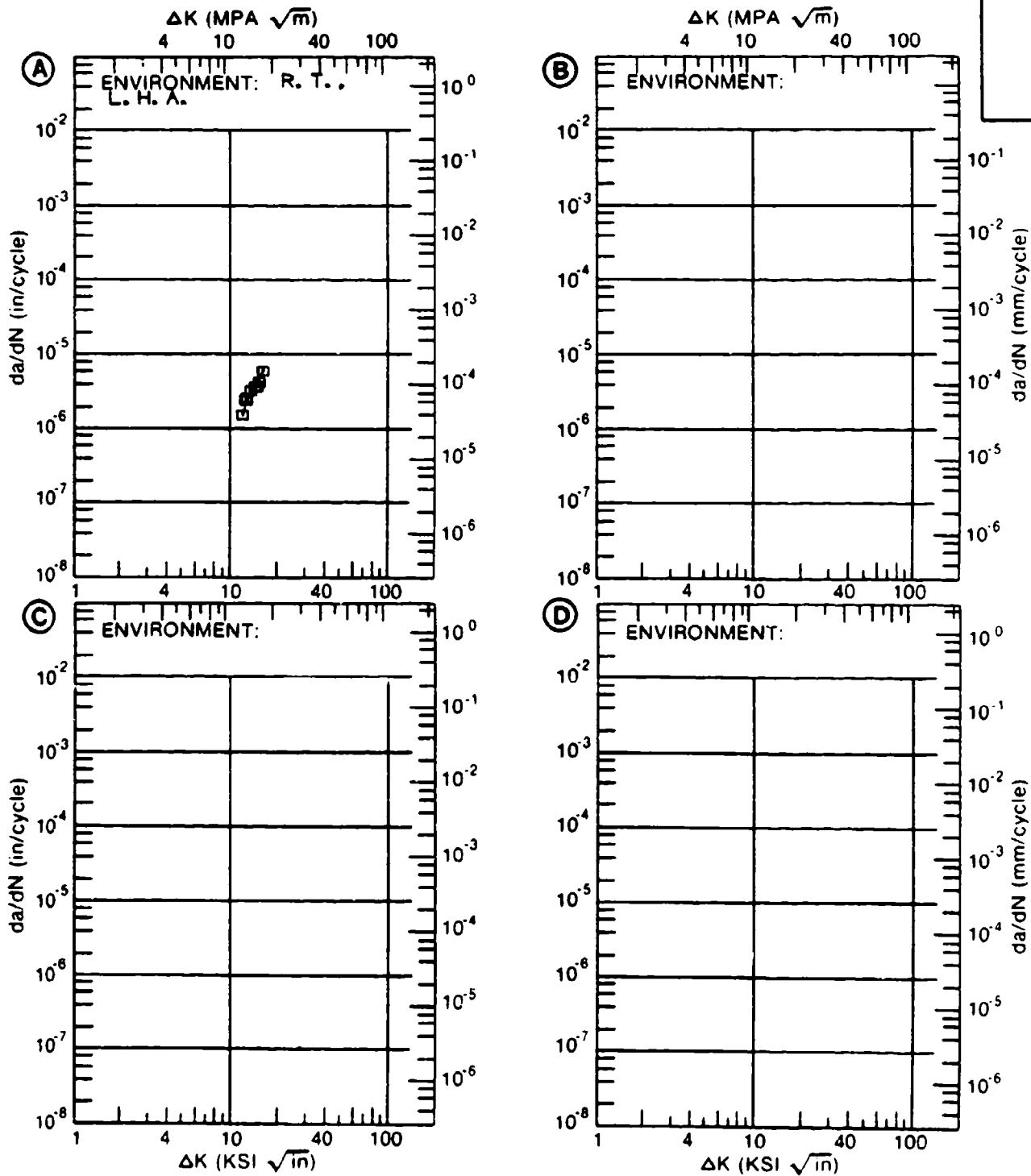


Figure 4.11.3.94

TABLE 4.11.3.95

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.95 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|-------------------------|----------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | E=+ 150F | | |
| | | L. H. A. | S. T. W. | | |
| | | 6HZ | 1HZ | | |
| DELTA K | A: 15.66 | 1.74 | | | |
| MIN | B: 12.77 | | .99 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | | 1.06 | | |
| | 16.00 | 2.12 | 2.71 | | |
| | 20.00 | 7.80 | 9.37 | | |
| | 25.00 | 17.5 | 31.9 | | |
| | 30.00 | | 67.8 | | |
| DELTA K | A: 29.18 | 45.5 | | | |
| MAX | B: 34.28 | | 93.1 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.60 | 11.76 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 2.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 119.0- 122.0 KSI
 ULT. STRENGTH: 131.0- 133.0 KSI
 SPECIMEN THK: 0.998- 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837, 88579

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4V

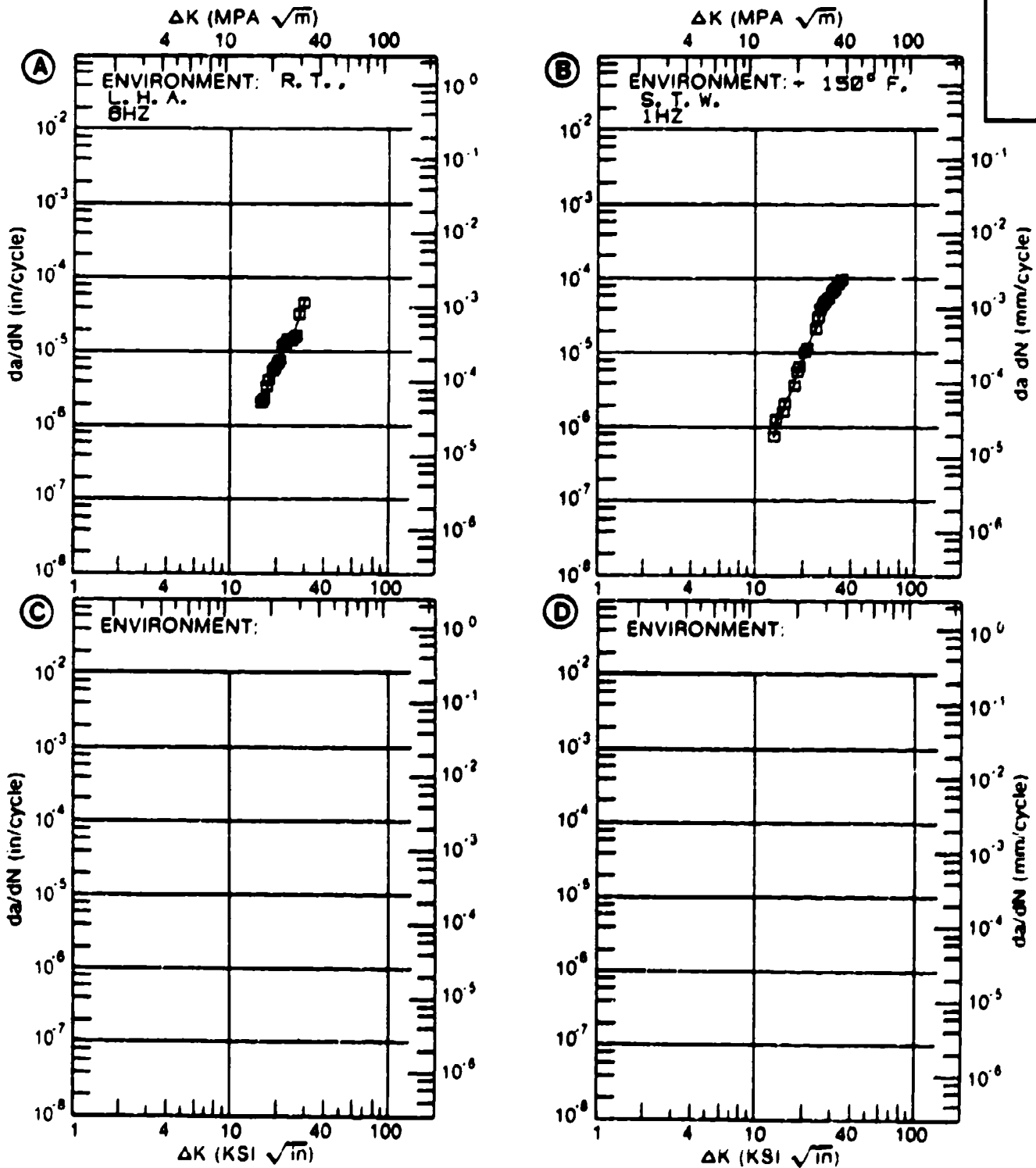


Figure 4.11.3.95

TABLE 4.11.3.96

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.96 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: RA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----|--------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. T. S. T. W. | | | |
| DELTA K MIN | A: | 13.83 | .788 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 16.00 | 2.13 | | |
| | | 20.00 | 8.98 | | |
| | | 25.00 | 27.5 | | |
| DELTA K MAX | A: | 26.33 | 33.2 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 10.04
PERCENT ERROR

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | |
| (NP/NA) | >2.0 | |

CONDITION/HT: RA
 FORM: 2.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 126.0 KSI
 ULT. STRENGTH: 135.0 KSI
 SPECIMEN THK: 0.997"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 85837

TITAN.
ALLOY

TI-6AL-
4V

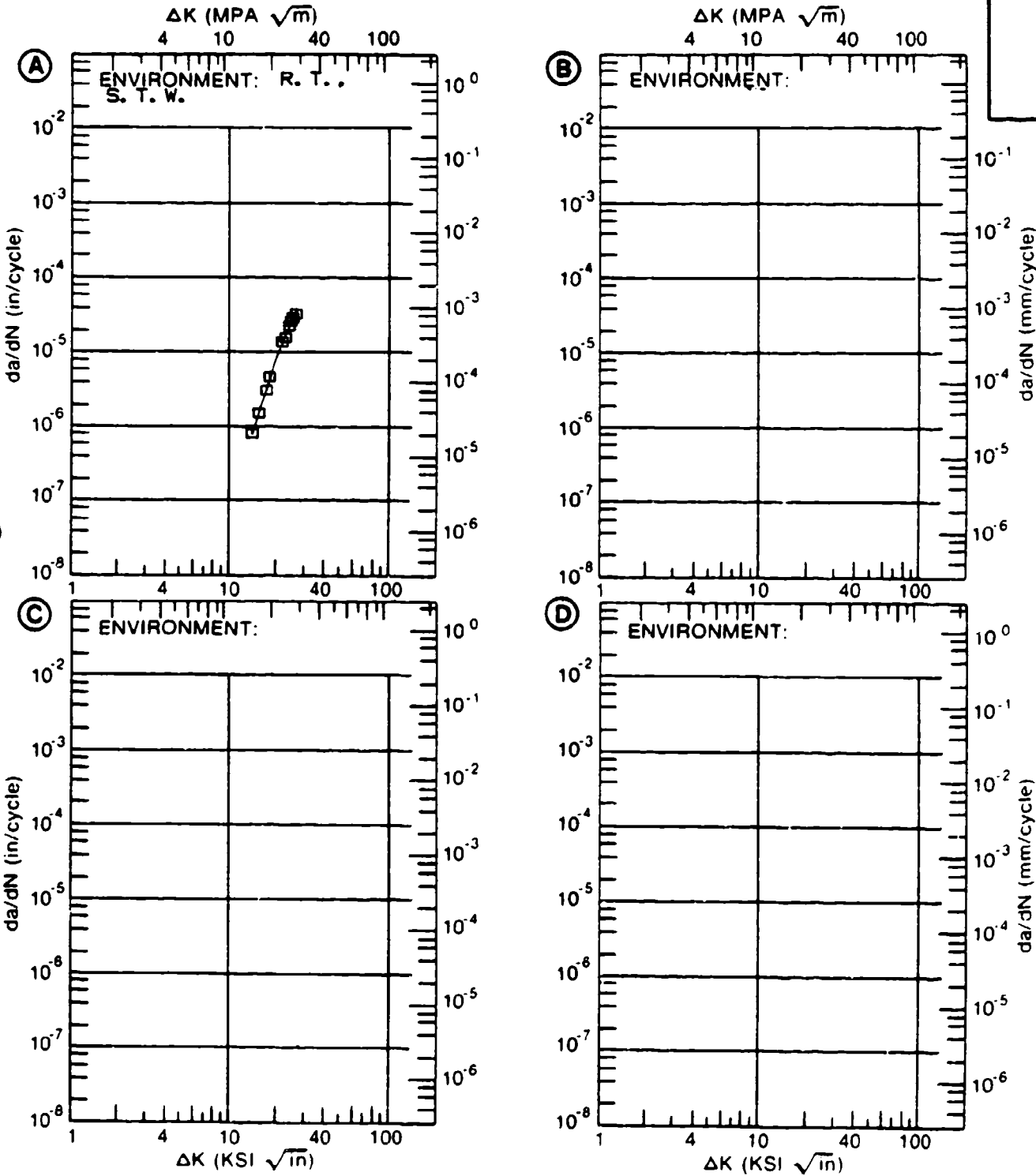


Figure 4.11.3.96

TABLE 4.11.3.97

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.97 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.08 | | | |
| DELTA K | A: 7.80 | .142 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | .215 | | | |
| | 9.00 | .594 | | | |
| | 10.00 | .778 | | | |
| | 13.00 | 1.31 | | | |
| | 16.00 | 3.25 | | | |
| | 20.00 | 13.4 | | | |
| | 25.00 | 37.5 | | | |
| DELTA K | A: 28.44 | 54.6 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 22.56
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 2.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T. . S. T. W.

YIELD STRENGTH: 120.0 KSI
 ULT. STRENGTH: 131.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 88578

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4V

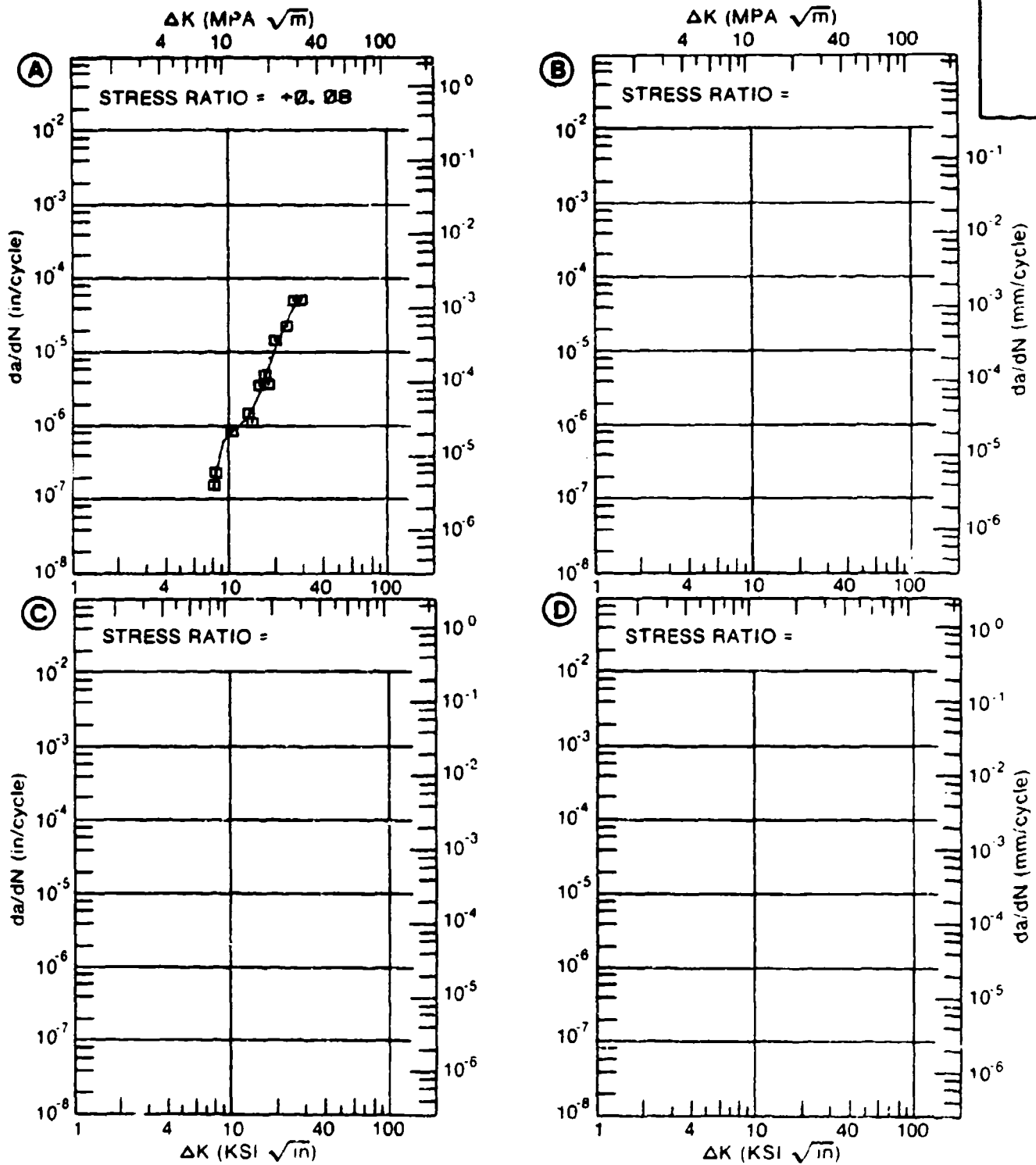


Figure 4.11.3.97

TABLE 4.11.3.98

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.98 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|--------------------------------------|-----------------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. 6HZ | E= R. T. S. T. W. 1HZ | | |
| DELTA K | A: 11.40 | .581 | | | |
| MIN | B: 11.39 | | .991 | | |
| | C: | | | | |
| | D: | | | | |
| | 12.00 | .811 | 1.70 | | |
| | 12.00 | 4.76 | 3.96 | | |
| | 20.00 | 10.4 | 9.34 | | |
| | 25.00 | 19.9 | 28.1 | | |
| | 30.00 | 34.8 | | | |
| DELTA K | A: 32.46 | 42.9 | | | |
| MAX | B: 27.68 | | 34.6 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.29 | 15.40 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 2 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 2.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY:

YIELD STRENGTH: 122.0 KSI
 ULT. STRENGTH: 136.0 KSI
 SPECIMEN THK: 0.990- 1.000"
 SPECIMEN WIDTH: 7.390- 7.400"
 REFERENCES: 88579

| |
|-----------------|
| TITAN. ALLOY |
| TI-6AL- 4V |
| |

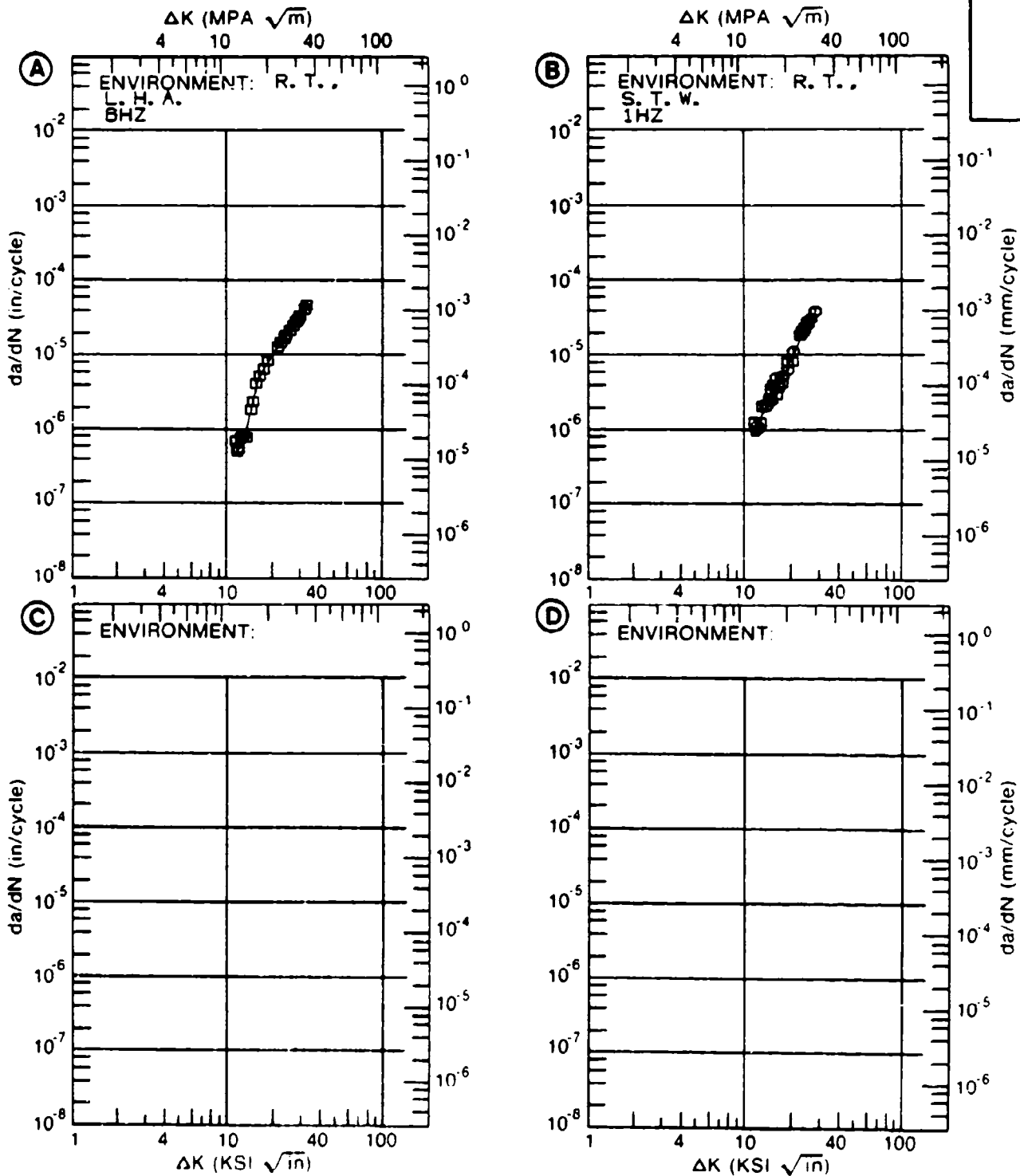


Figure 4.11.3.98

TABLE 4.11.3.99

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.99 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|-----------------------------|-----------------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. 6HZ | E= R. T. S. T. W. 1HZ | | |
| DELTA K | A: 10.70 | .357 | | | |
| MIN | B: 10.73 | | .743 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.12 | 1.37 | | |
| | 16.00 | 3.51 | 3.28 | | |
| | 20.00 | 9.89 | 9.12 | | |
| | 25.00 | 20.7 | 23.1 | | |
| | 30.00 | | 40.6 | | |
| DELTA K | A: 29.26 | 27.4 | | | |
| MAX | B: 31.56 | | 45.4 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 9.23 | 15.54 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | 1 | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 2.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: ± 0.08
 FREQUENCY:

YIELD STRENGTH: 122.0 KSI
 ULT. STRENGTH: 135.0 KSI
 SPECIMEN THK: 0.990- 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 98579

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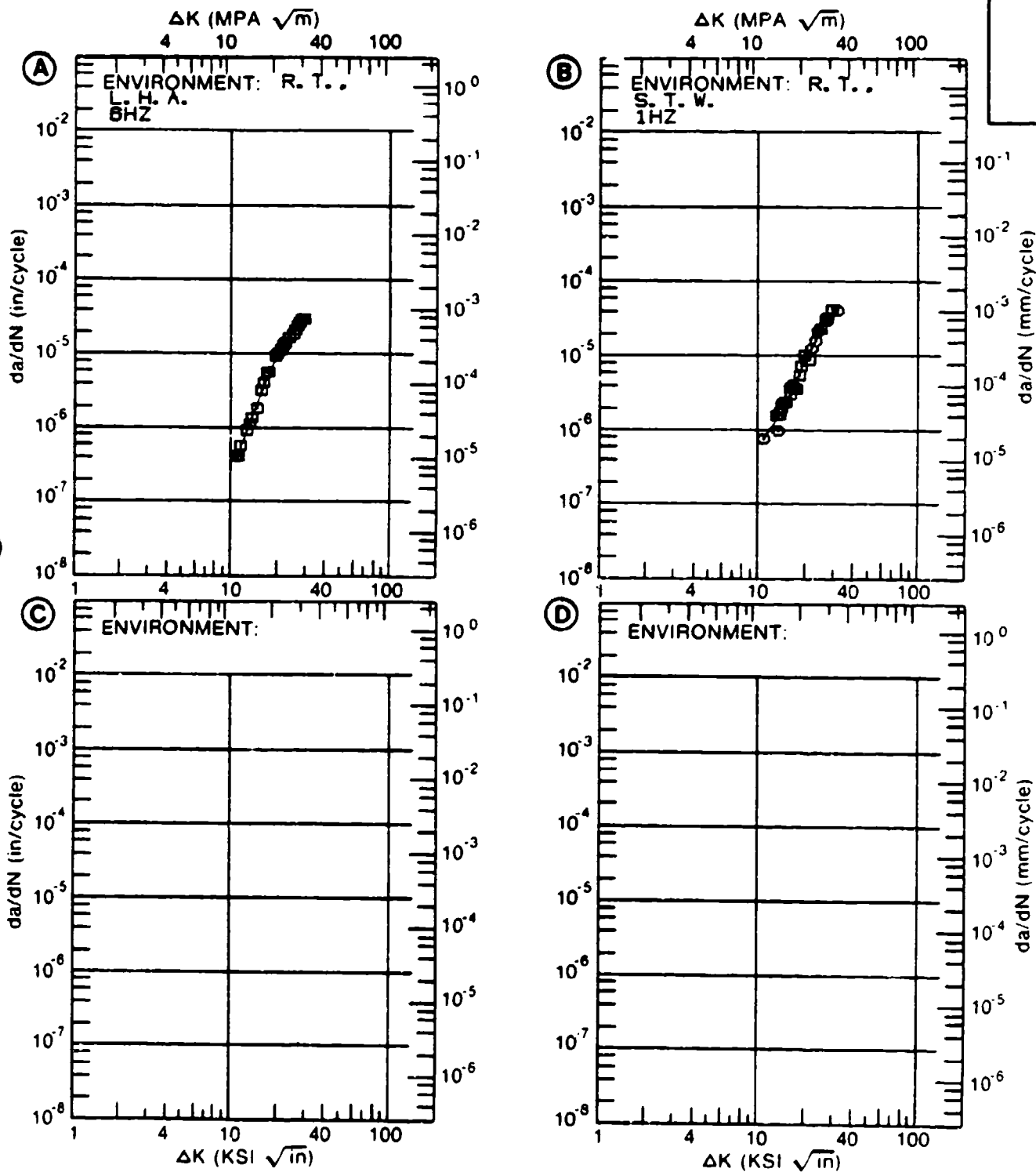


Figure 4.11.3.99

TABLE 4.11.3.100

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.100 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---|---|---|
| | A | B | C | D |
| | E= R. T. L. H. A. | | | |
| DELTA K A: 18.54 | 2.02 | | | |
| MIN B: | | | | |
| C: | | | | |
| D: | | | | |
| 20.00 | 3.34 | | | |
| 25.00 | 10.6 | | | |
| 30.00 | 21.5 | | | |
| 35.00 | 36.3 | | | |
| 40.00 | 57.6 | | | |
| 50.00 | 145. | | | |
| 60.00 | 405. | | | |
| DELTA K A: 62.29 | 521. | | | |
| MAX B: | | | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 8.69
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 3.50" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 6.00 HZ

YIELD STRENGTH: 118.0 KSI
 ULT. STRENGTH: 129.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 6.000"
 REFERENCES 88578

TITAN.
ALLOY

TI-6AL-
4V

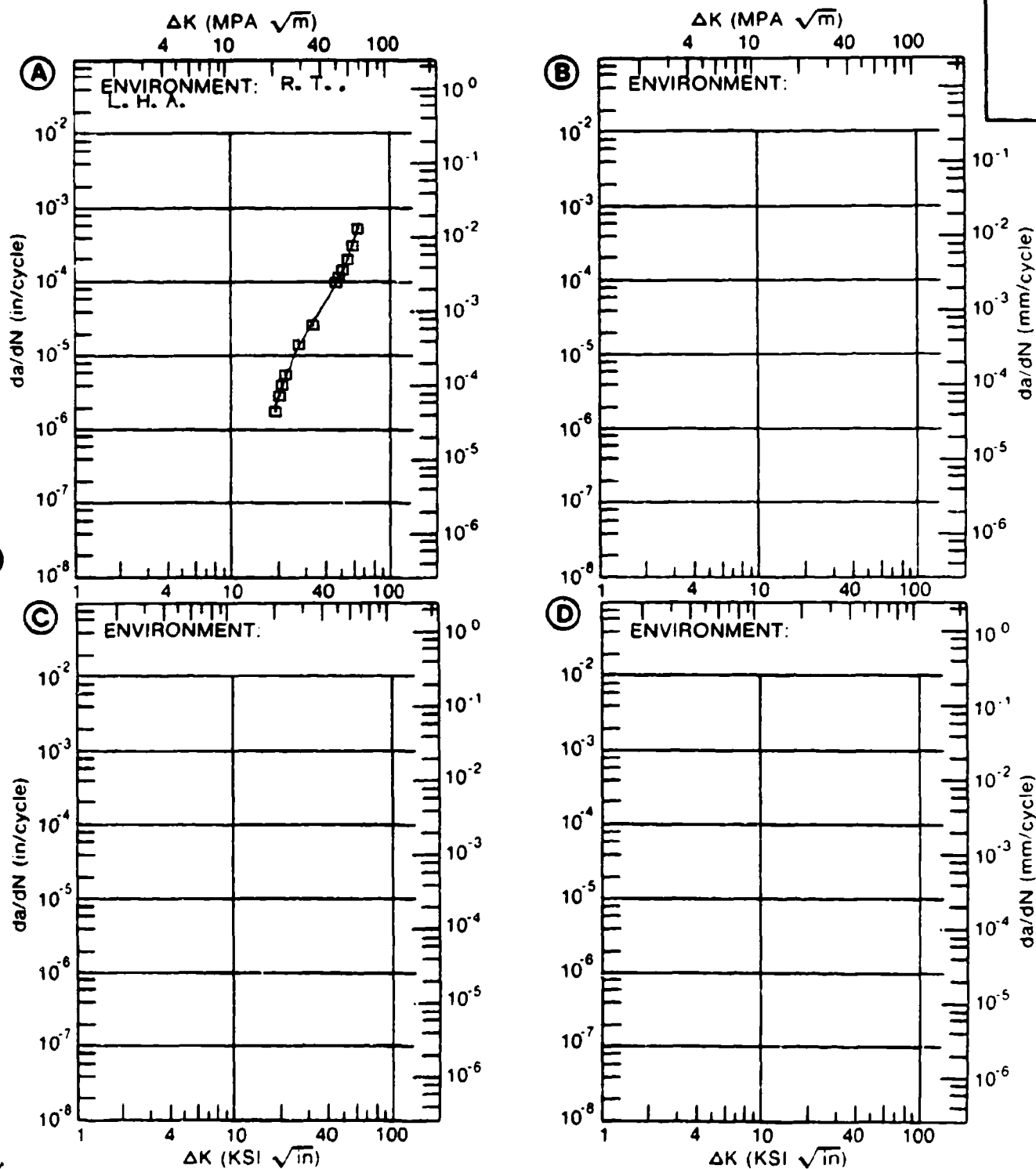


Figure 4.11.3.100

TABLE 4.11.3.101

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.101 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.08 | | | |
| DELTA K MIN | A: 6.72 | .356 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 7.00 | .384 | | | |
| | 8.00 | .573 | | | |
| | 9.00 | .957 | | | |
| | 10.00 | 1.65 | | | |
| | 13.00 | 7.24 | | | |
| | 16.00 | 20.0 | | | |
| | 20.00 | 36.8 | | | |
| DELTA K MAX | A: 21.08 | 38.2 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 9.22
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 123.0 KSI
 ULT. STRENGTH: 136.0 KSI
 SPECIMEN THK: 0.000"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 00578

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 4V

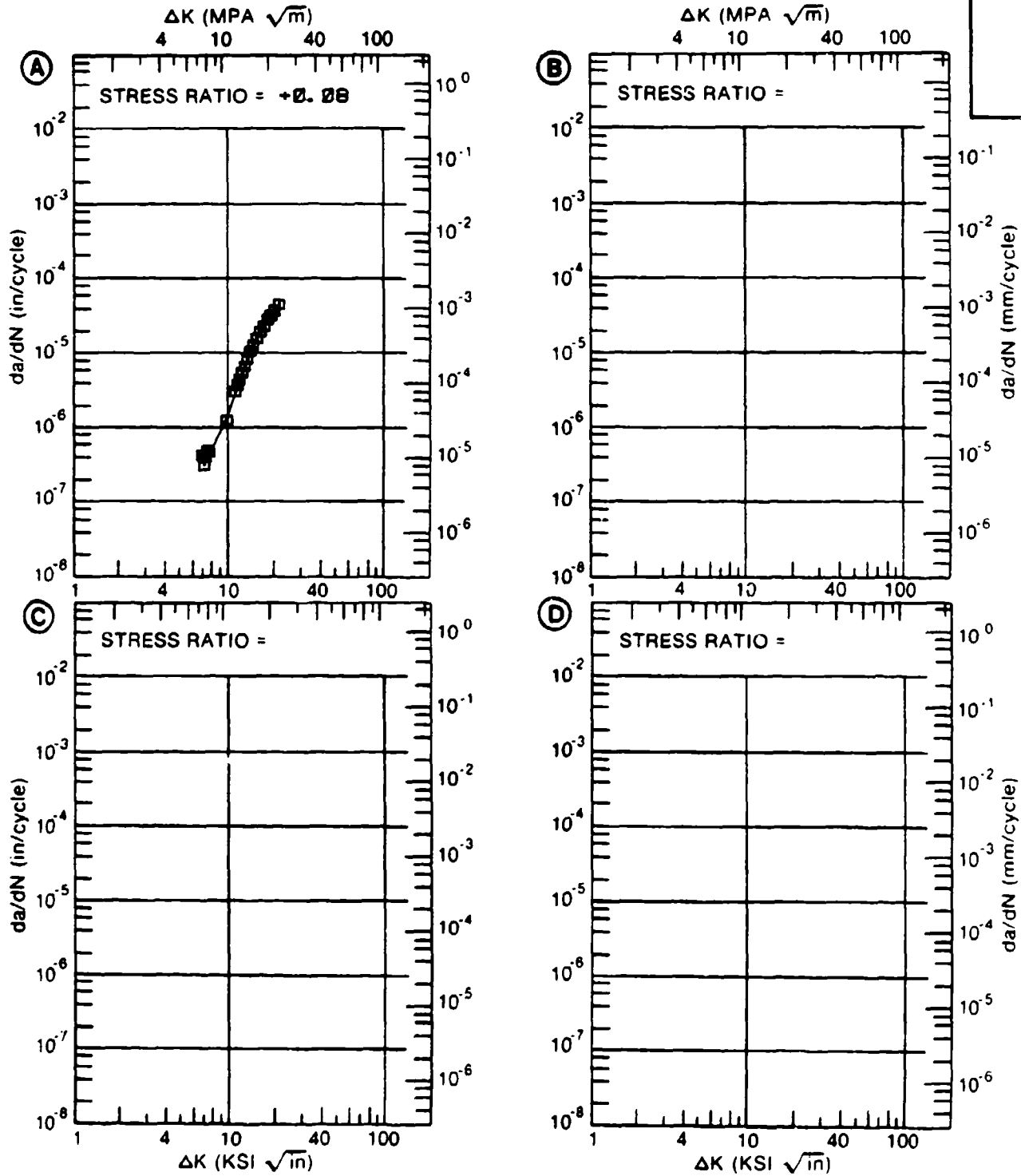


Figure 4.11.3.101

TABLE 4.11.3.102

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.102 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.08 | | | |
| DELTA K MIN | A: 10.96 | 1.07 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 2.50 | | | |
| | 16.00 | 6.47 | | | |
| | 20.00 | 16.1 | | | |
| | 25.00 | 36.1 | | | |
| 30.00 | 64.4 | | | | |
| 35.00 | 99.4 | | | | |
| 40.00 | 139. | | | | |
| 50.00 | 225. | | | | |
| DELTA K MAX | A: 54.52 | 264. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 22.85
PERCENT ERROR

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | 1 |
| (NP/NA) | >2.0 | |

CONDITION/HT: RA
 FORM: FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 110.0 - 124.0 KSI
 ULT. STRENGTH: 132.0 - 136.0 KSI
 SPECIMEN THK: 0.010 - 1.010"
 SPECIMEN WIDTH: 0.000"
 REFERENCES 00579

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 4V

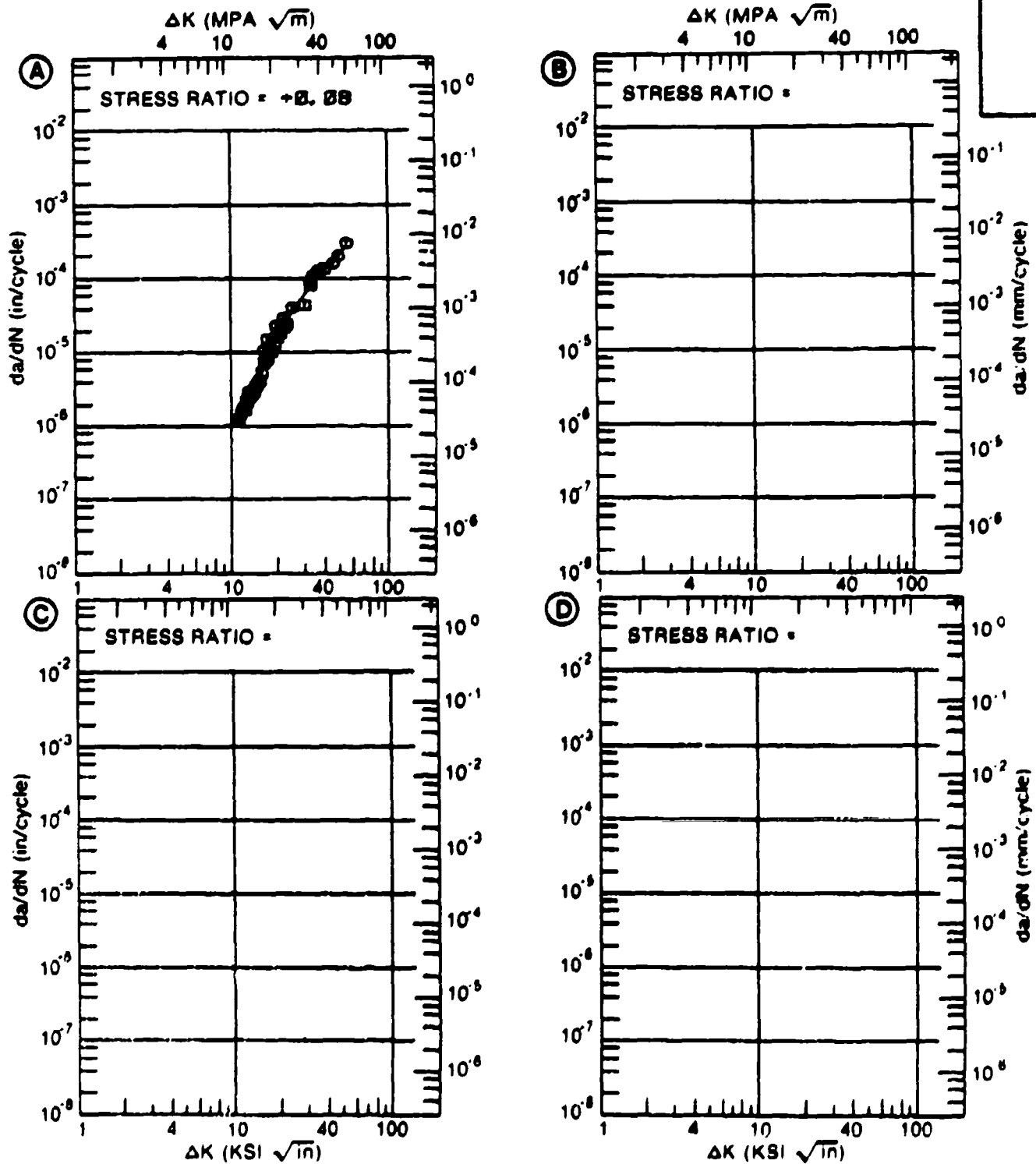


Figure 4.11.3.102

TABLE 4.11.3.103

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.10 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , L. H. A.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**~6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.08 | R=+0.30 | | |
| DELTA K | A: 10.40 | .132 | | | |
| MIN | B: 9.44 | | .866 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | | 1.22 | | |
| | 13.00 | .618 | 4.26 | | |
| | 16.00 | 1.93 | 8.77 | | |
| | 20.00 | 6.76 | 16.2 | | |
| | 25.00 | 13.9 | 28.2 | | |
| | 30.00 | 23.3 | 45.4 | | |
| | 35.00 | | 72.4 | | |
| | 40.00 | | 117. | | |
| | 50.00 | | 324. | | |
| DELTA K | A: 34.94 | 36.0 | | | |
| MAX | B: 57.20 | | 710. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.27 | 8.17 | | |
| PERCENT ERROR | | | | | |

| | | | |
|------------|----------|---|---|
| LIFE | 0.0-0.5 | | |
| PREDICTION | 0.5-0.8 | | |
| RATIO | 0.8-1.25 | | 1 |
| SUMMARY | 1.25-2.0 | 1 | |
| (NP/NA) | >2.0 | | |

CONDITION/HT: RA
 FORM: 4.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 FREQUENCY: 8.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 121.0 KSI
 ULT. STRENGTH: 132.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 98579

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 ALLOY

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 4V

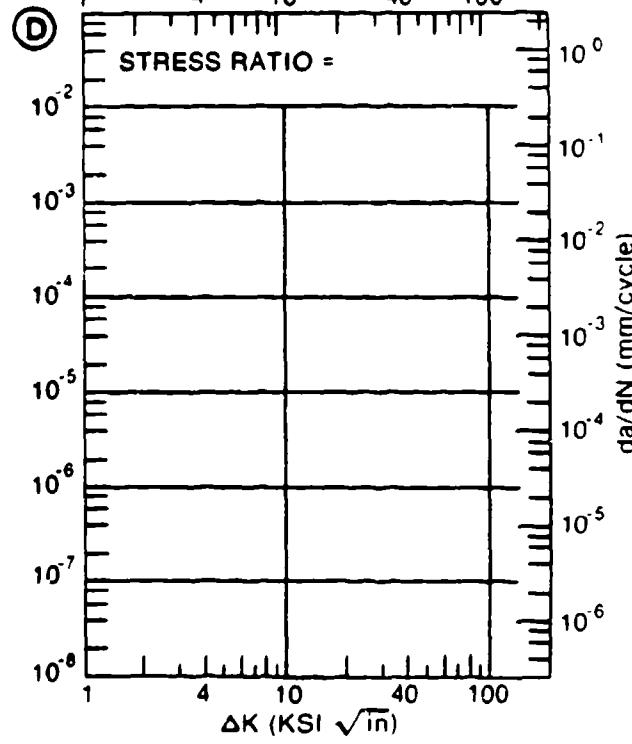
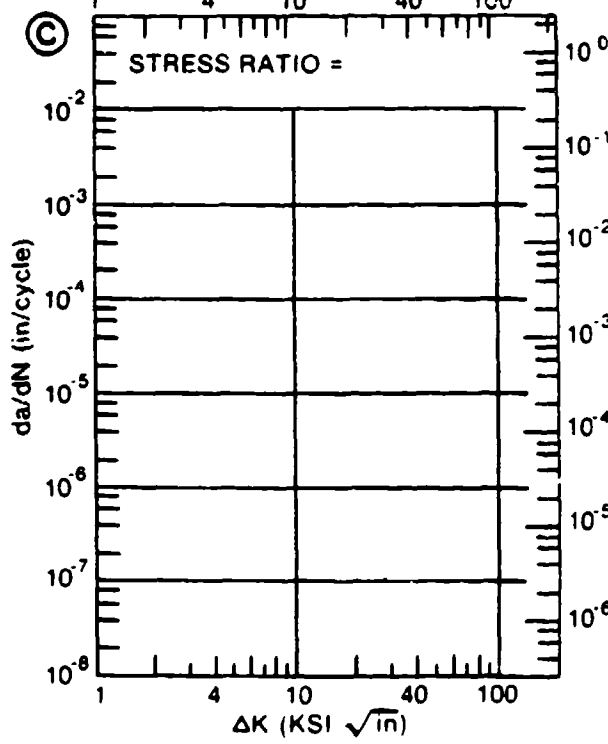
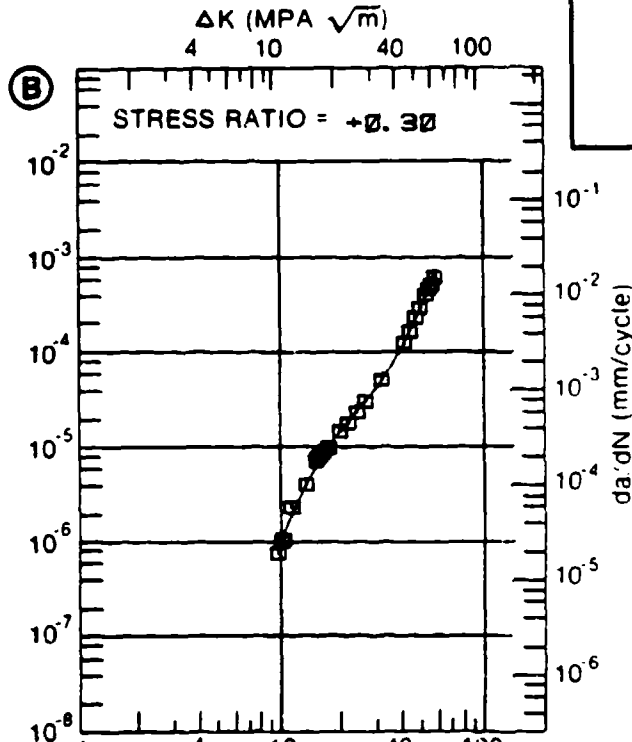
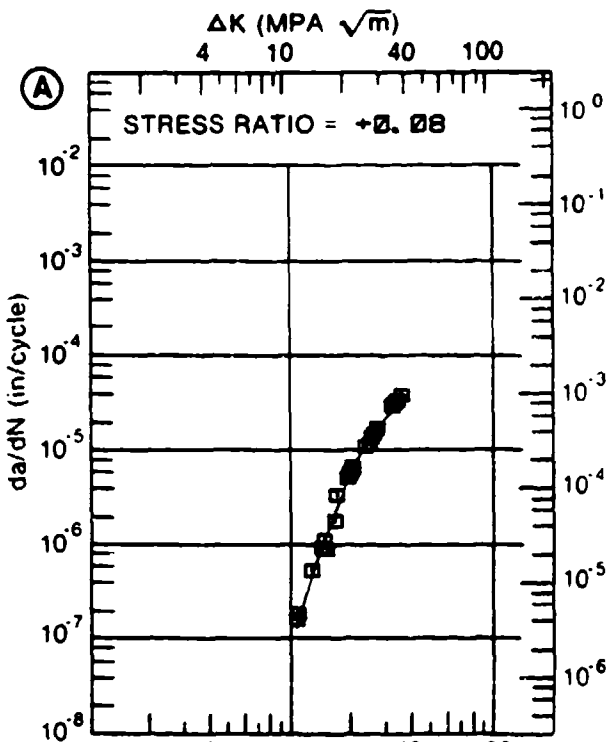


Figure 4.11.3.103

TABLE 4.11.3.104

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.104 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---------------------------------------|--|--------------------------|---------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. L. H. A. | E= R. T. J. P. 4 | | |
| DELTA K MIN | A: 9.37 | .349 | | | |
| | B: 12.53 | | .933 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .388 | | | |
| | 13.00 | .844 | .812 | | |
| | 16.00 | 2.04 | 1.38 | | |
| | 20.00 | 5.78 | 5.54 | | |
| | 25.00 | 15.9 | 14.2 | | |
| | 30.00 | 34.1 | 26.6 | | |
| | 35.00 | 60.1 | | | |
| | 40.00 | 91.3 | | | |
| | 50.00 | 166. | | | |
| DELTA K MAX | A: 58.69 | 341. | | | |
| | B: 32.23 | | 34.8 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 25.76 | 17.89 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 2 | 1 | | |

CONDITION/HT: RA
 FORM: 4.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 121.0 KSI
 ULT. STRENGTH: 132.0 KSI
 SPECIMEN THK: 0.950- 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88579

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 4V

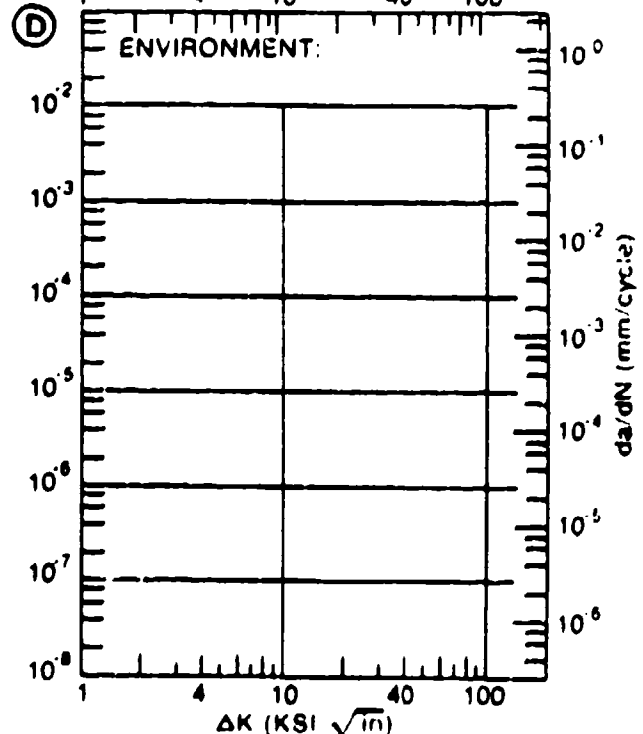
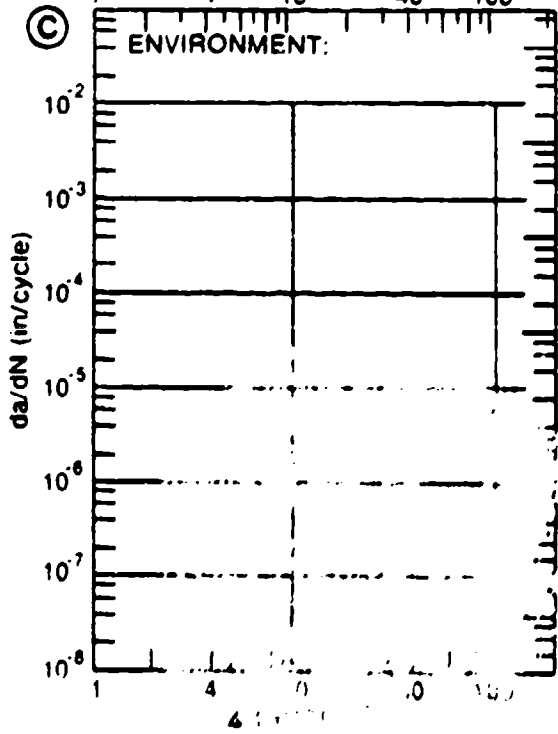
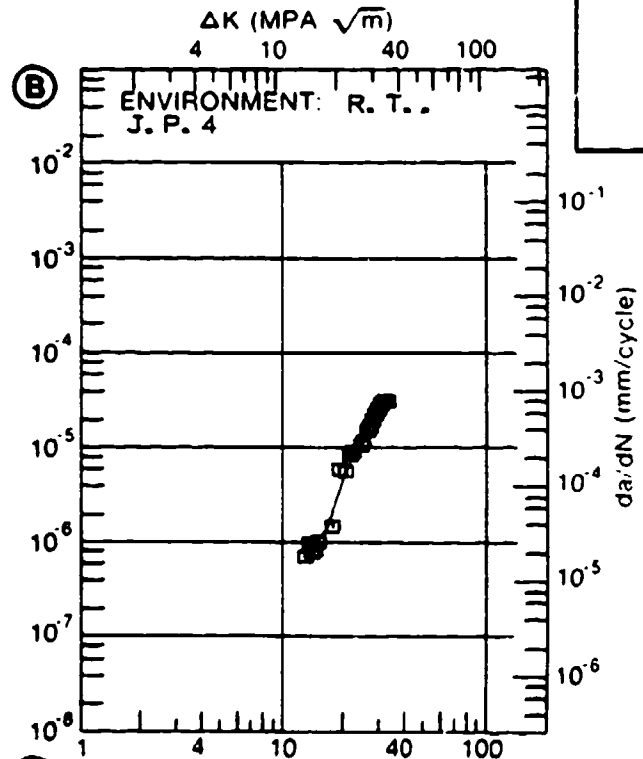
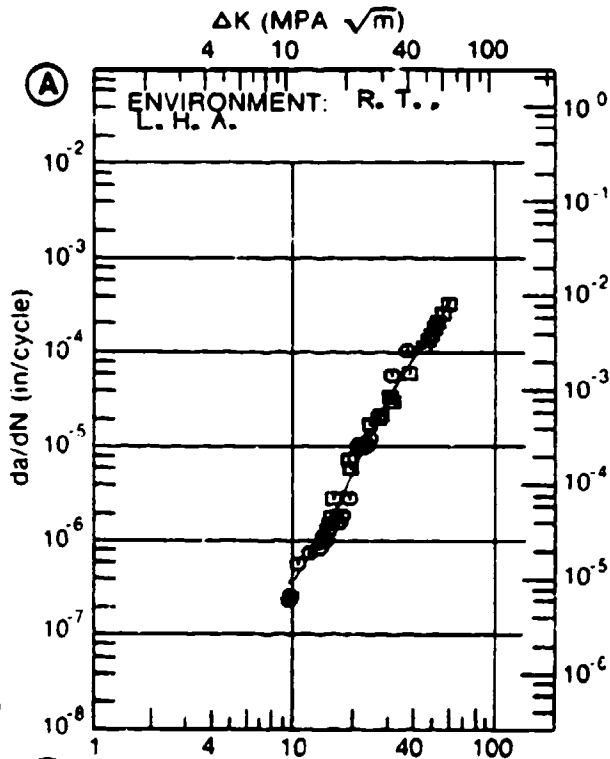


Figure 4.11.3.104

TABLE 4.11.3.105

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.105 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-----------------------------|----------|--------------------------------------|---------|---|---|
| CONDITION: RA | | | | | |
| ENVIRONMENT: R. T. J. H. A. | | | | | |
| DELTA K (KBI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.08 | R=+0.50 | | |
| DELTA K A: | 12.73 | .837 | | | |
| DELTA K B: | 9.49 | | 2.14 | | |
| MIN C: | | | | | |
| D: | | | | | |
| | 10.00 | | 2.68 | | |
| | 13.00 | .920 | 6.78 | | |
| | 16.00 | 2.53 | 11.9 | | |
| | 20.00 | 7.65 | 19.8 | | |
| | 25.00 | 19.1 | 32.7 | | |
| | 30.00 | 32.8 | 51.6 | | |
| | 35.00 | 48.1 | 71.3 | | |
| | 40.00 | 67.2 | | | |
| | 50.00 | 135. | | | |
| | 60.00 | 327. | | | |
| DELTA K A: | 68.69 | 885. | | | |
| DELTA K B: | 37.30 | | 101. | | |
| MAX C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 13.63 | 7.38 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | 2.0 | | | | |

CONDITION/HT: RA
 FORM: 4.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 8.00 HZ
 ENVIRONMENT: R. T., L. H. A.

YIELD STRENGTH: 119.0 - 128.0 KSI
 ULT. STRENGTH: 127.0 - 136.0 KSI
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88579

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4V

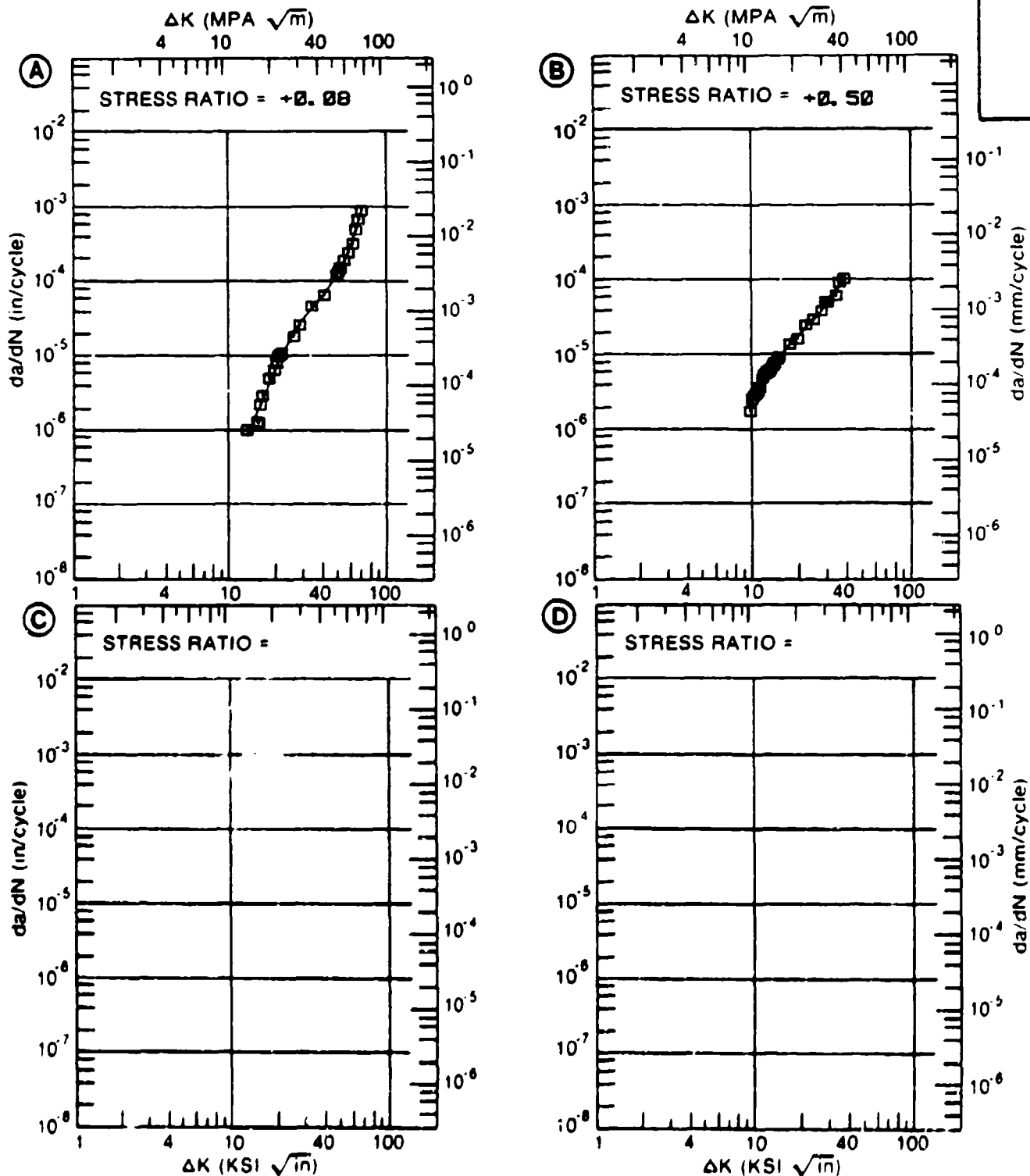


Figure 4.11.3.195

TABLE 4.11.3.106

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.106 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: RA
ENVIRONMENT: R. T. , S. T. W.

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.50 | | | |
| DELTA K | A: 7.69 | 1.88 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 8.00 | 1.81 | | | |
| | 9.00 | 2.18 | | | |
| | 10.00 | 3.39 | | | |
| | 13.00 | 14.7 | | | |
| | 16.00 | 33.8 | | | |
| | 20.00 | 61.3 | | | |
| | 25.00 | 103. | | | |
| | 30.00 | 171. | | | |
| | 35.00 | 277. | | | |
| | 40.00 | 426. | | | |
| DELTA K | A: 40.43 | 440. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 15.31
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: RA
 FORM: 4.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., S. T. W.

YIELD STRENGTH: 128.0 KSI
 ULT. STRENGTH: 138.0 KSI
 SPECIMEN THK: 0.880"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 98579

TITAN.
 ALLOY

TI-6AL-
 4V

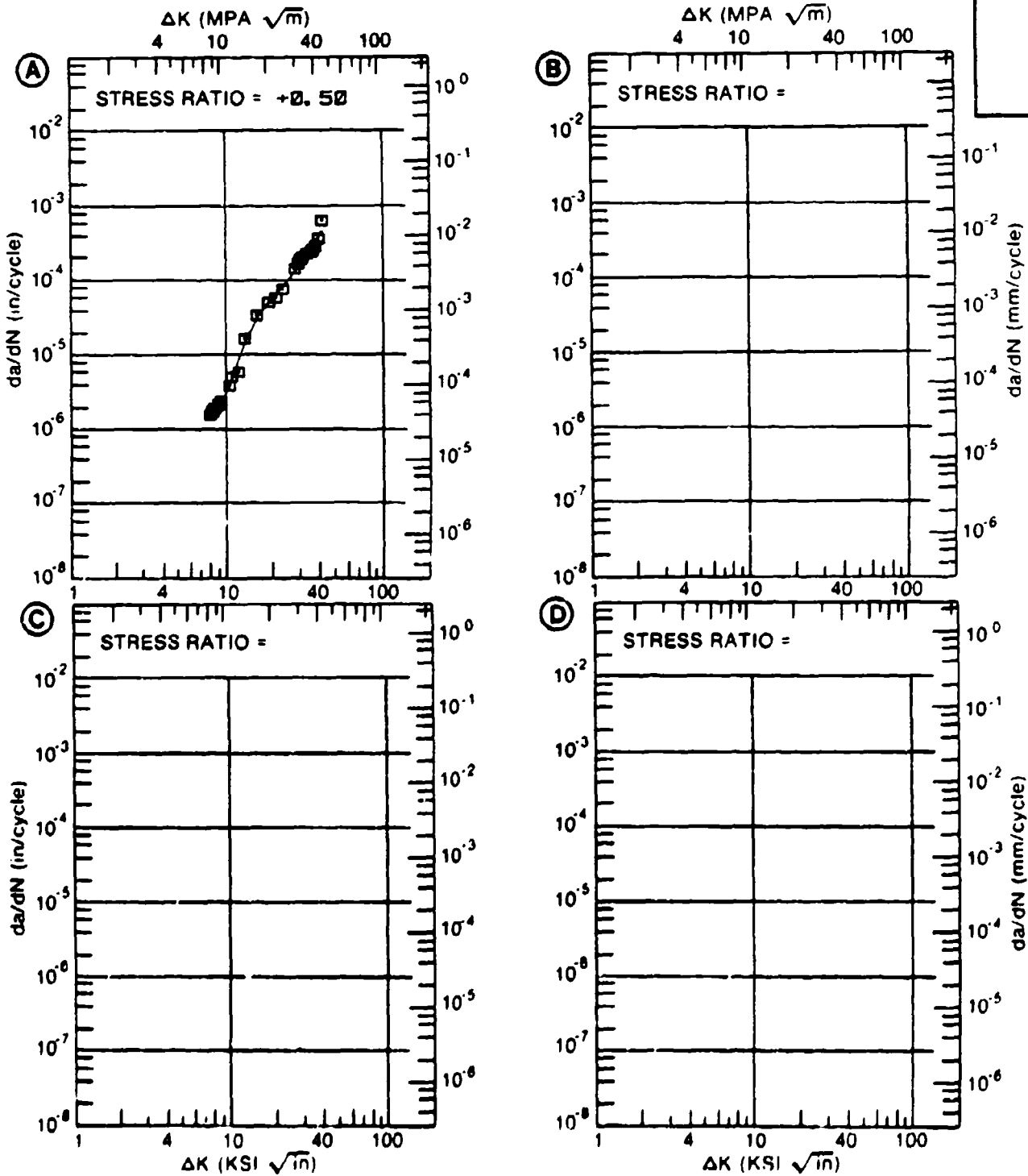


Figure 4.11.3.106

TABLE 4.11.3.107

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.10 INDICATING EFFECT

OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: RA

TI-6AL-4V

| DELTA K (KSI*IN**1/2) | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|---|------|--|------|
| | A | B | C | D |
| | E= R. T. S. T. W. SP. THK. =. 77" | | E= R. T. S. T. W. SP. THK. =1. 04" | |
| DELTA K MIN | A: 9.95 | .707 | B: 8.02 | .186 |
| | 9.00 | | | .398 |
| | 10.00 | .694 | | .742 |
| | 13.00 | 1.60 | | 2.75 |
| | 16.00 | 5.77 | | 6.48 |
| | 20.00 | 14.0 | | 14.9 |
| | 25.00 | 29.9 | | 33.5 |
| | 30.00 | 51.9 | | |
| | 35.00 | 79.6 | | |
| | 40.00 | 112. | | |
| | 50.00 | 192. | | |
| DELTA K MAX | A: 58.05 | 270. | B: 28.61 | 56.2 |

ROOT MEAN SQUARE PERCENT ERROR 10.30 25.37

LIFE PREDICTION RATIO SUMMARY (NP/NA)

| | |
|----------|---|
| 0.0-0.9 | |
| 0.5-0.9 | |
| 0.9-1.25 | 1 |
| 1.25-2.0 | 1 |
| >2.0 | |

CONDITION/HT: RA
 FORM: 4.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 119.0 - 128.0 KSI
 ULT. STRENGTH: 127.0 - 136.0 KSI
 SPECIMEN THK:
 SPECIMEN WIDTH: 7.400"
 REFERENCES: 88579

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TI-6AL-
4V

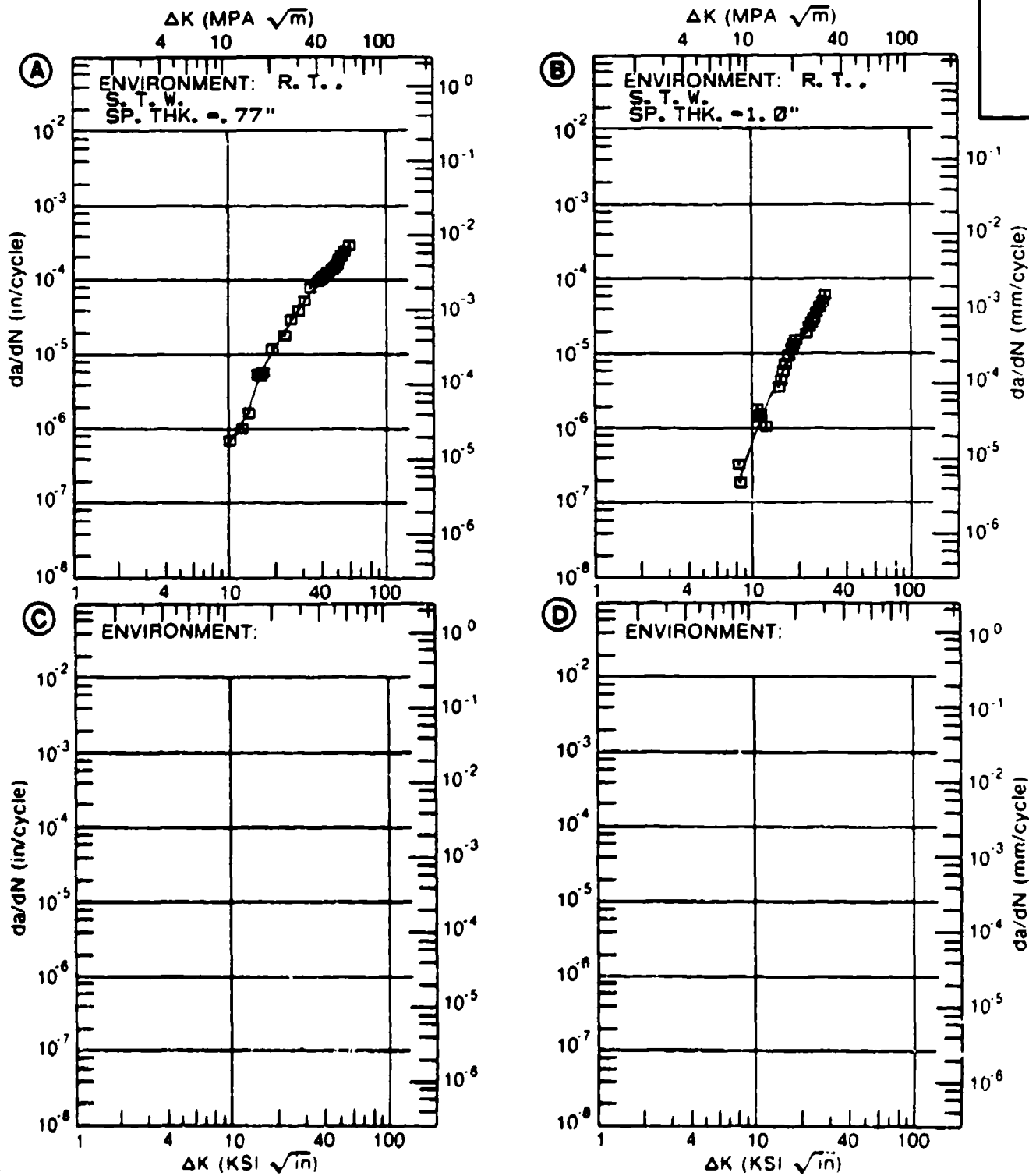


Figure 4.11.3.107

TABLE 4.11.3.108

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.108 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: STOA

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----|---------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | L. H. A. | | | |
| DELTA K MIN | A: | 11.82 | 9.43 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 13.00 | 9.10 | | |
| | | 16.00 | 20.2 | | |
| DELTA K MAX | A: | 18.56 | 37.1 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 10.90
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: ST0A
 FORM: 0.82" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.30
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 140.0 KSI
 ULT. STRENGTH: 150.0 KSI
 SPECIMEN THK: 0.491"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: 85837

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 4V

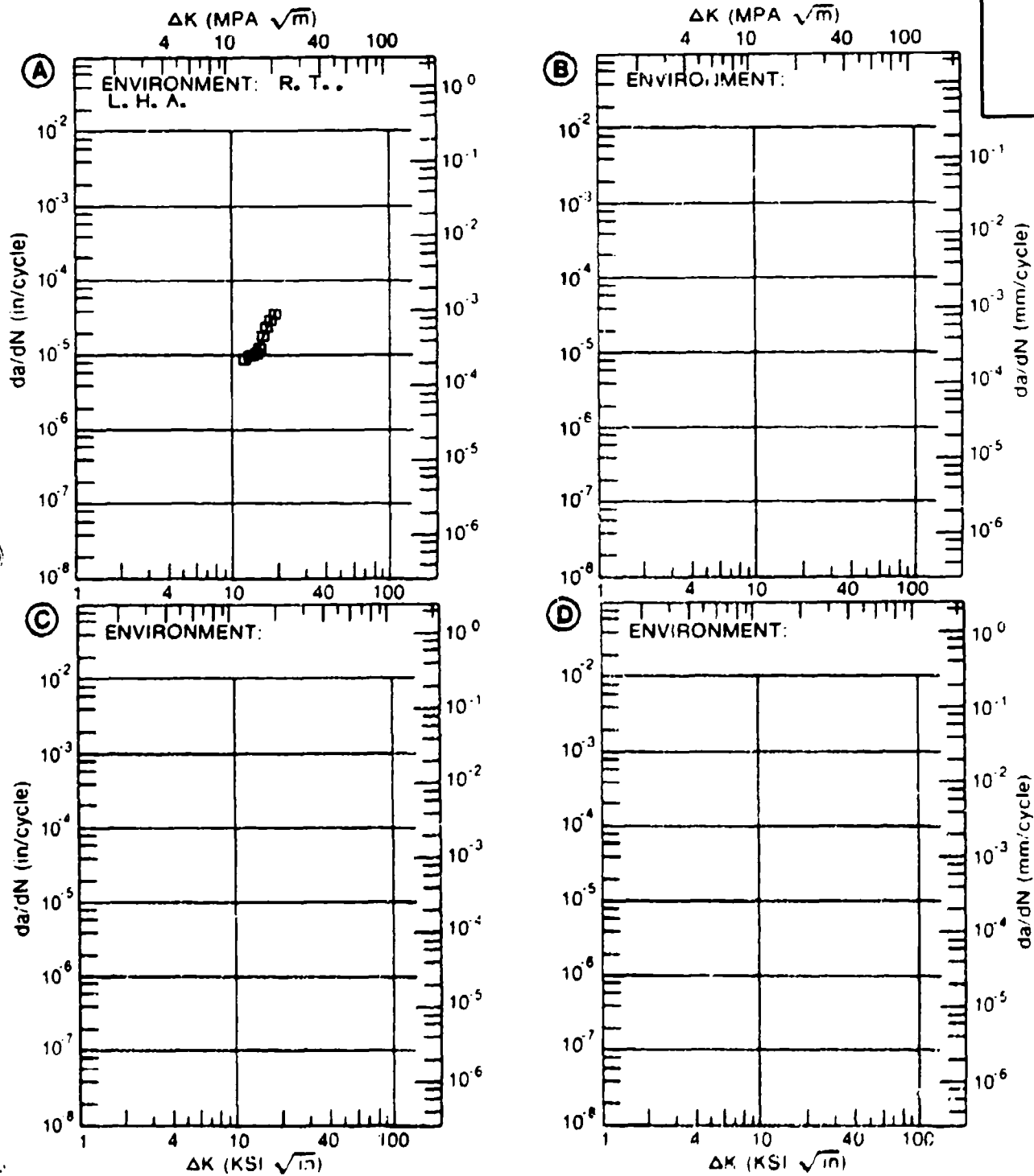


Figure 4.11.3.108

TABLE 4.11.3.109

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.8.109 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: STRESS RELIEVED E. B. WELDMENT (WELD ZONE)

| DELTA K (KSI*IN**1/2) | DA/DN (10**--6 IN. /CYCLE) | | | |
|--------------------------------|----------------------------|-------------------------|---|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | E= R. T. DIST. WATER | | |
| DELTA K MIN | A: 15.48 : 2.20 | B: 5.22 | | |
| | B: 25.76 | | | |
| | C: 16.00 : 4.77 | | | |
| | D: 20.00 : 10.1 | | | |
| | 25.00 : 24.6 | | | |
| | 30.00 : 63.5 | 19.2 | | |
| | 35.00 : 175. | 78.6 | | |
| | 40.00 : 1080. | 273. | | |
| | 50.00 : | 2053. | | |
| | 60.00 : | 9009. | | |
| DELTA K MAX | A: 40.52 : 1462. | B: 21786. | | |
| | B: 68.14 | | | |
| | C: | | | |
| | D: | | | |
| ROOT MEAN SQUARE PERCENT ERROR | 39.26 | 111.76 | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: STRESS RELIEVED E. B. WELDMENT (WELD ZONE)
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: 89144

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4V

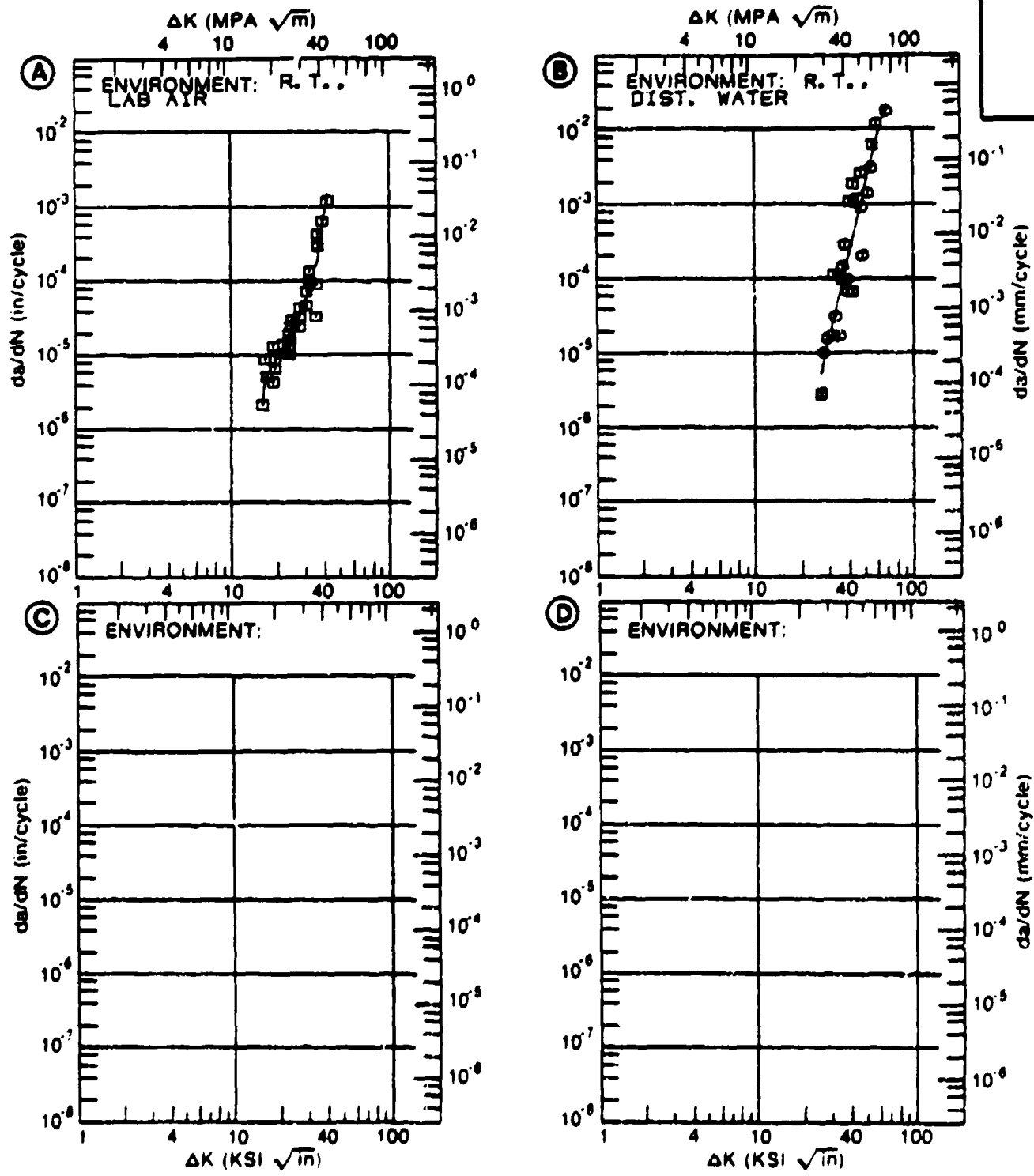


Figure 4.11.3.109

TABLE 4.11.3.110

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.110 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---|----------|--------------------------------------|-----------|---|---|
| CONDITION: STRESS RELIEVED E. B. WELDMENT (WELD ZONE) | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R.T. | E=+ 175F | | |
| | | 3.5% NaCl | 3.5% NaCl | | |
| DELTA K MIN | A: 21.95 | 17.8 | | | |
| | B: 28.50 | | 31.1 | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | 120. | | | |
| | 30.00 | 854. | 53.6 | | |
| | 35.00 | 2746. | 179. | | |
| | 40.00 | 8987. | 895. | | |
| | 50.00 | 18134. | | | |
| DELTA K MAX | A: 51.09 | 20210. | | | |
| | B: 46.69 | | 8328. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 74.94 | 39.82 | | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | | | | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: STRESS RELIEVED E. B. WELDMENT (WELD ZONE)
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 88144

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TI-6AL-4V

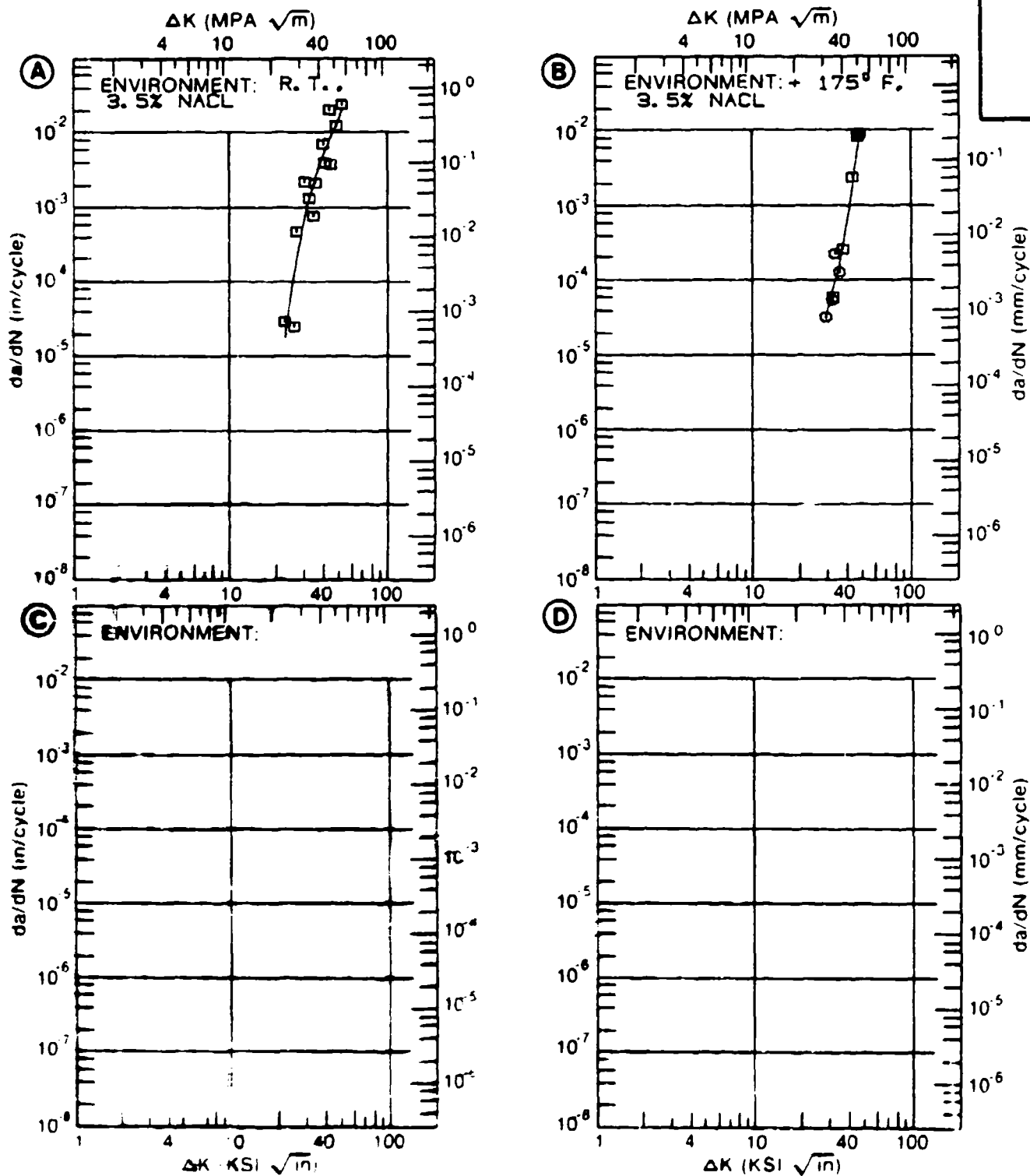


Figure 4.11.3.11

TABLE 4.11.3.111

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.111 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: STRESS RELIEVED E. B. WELDMENT (HEAT
AFFECTED ZONE)

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|--|-------------------------------|-------------------------------|---|
| | A | B | C | D |
| | E= R. T. 3.5% NACL .1-10HZ | E=+ 175F 3.5% NACL 10HZ | E=+ 175F 3.5% NACL .1HZ | |
| DELTA K MIN | A: 19.78 | 14.6 | | |
| | 20.00 | 13.9 | | |
| | 25.00 | 17.7 | | |
| | 30.00 | 84.5 | | |
| | 35.00 | 626. | | |
| | 40.00 | 4908. | | |
| DELTA K MAX | A: 49.52 | 172725. | | |
| | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | 113.68 | 0.00 | 0.00 | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | |

CONDITION/HT: STRESS RELIEVED E. B. WELDMENT (HEAT AFFECTED ZONE)
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY:
 YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: 88144

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4V

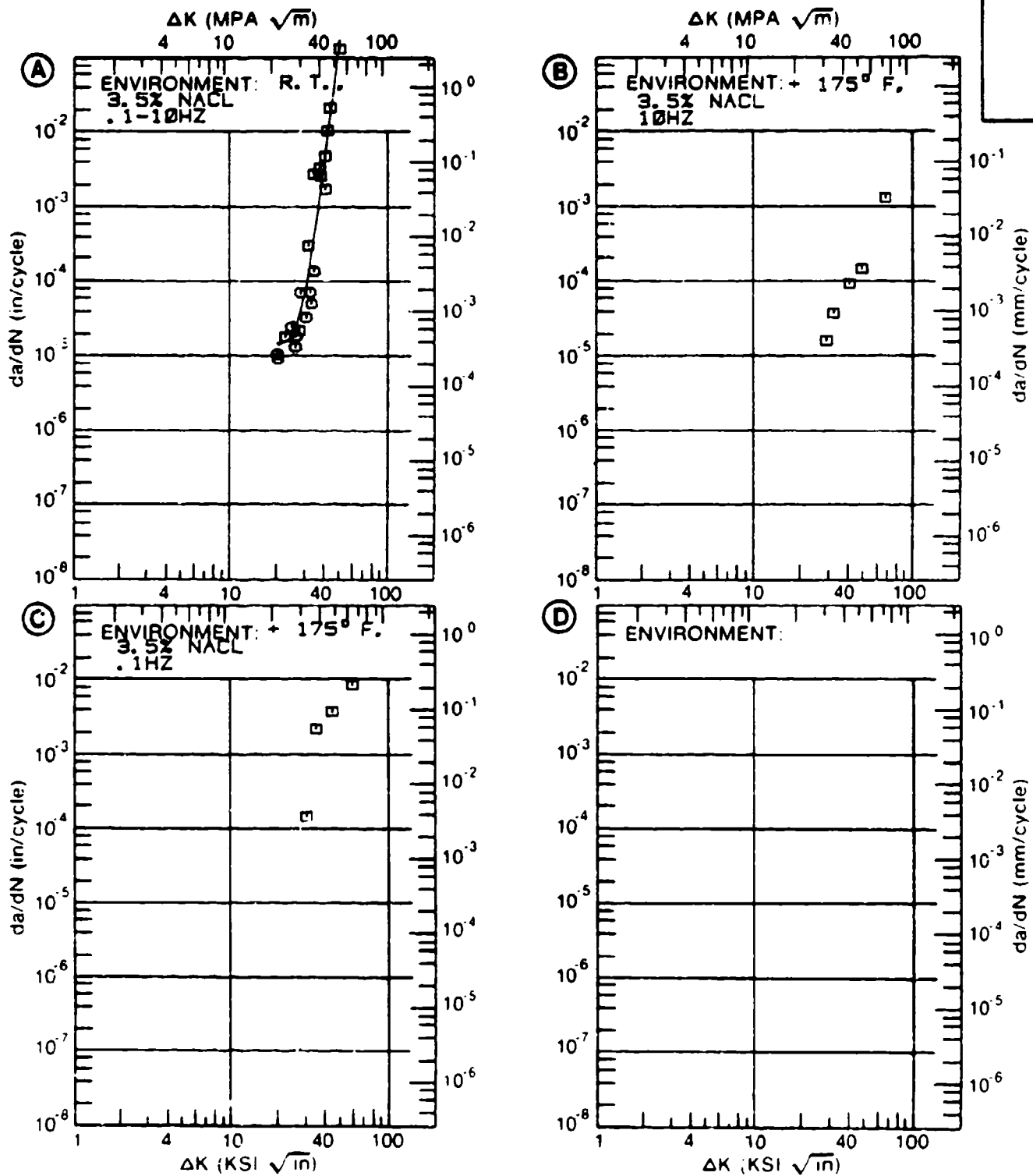


Figure 4.11.3.111

TABLE 4.11.3.112

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.112 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: STRESS RELIEVED E. B. WELDMENT (HEAT
AFFECTED ZONE)

| DELTA K (KSI*IN**1/2) | DA/DN (10**6 IN./CYCLE) | | | |
|--------------------------|-------------------------|-------|------|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: 15.64 | 3.64 | | |
| | B: 16.00 | 4.27 | | |
| | C: 20.00 | 14.2 | | |
| | D: 25.00 | 29.9 | | |
| | | 30.00 | 47.5 | |
| | | 35.00 | 71.9 | |
| | | 40.00 | 113. | |
| | | 50.00 | 344. | |
| DELTA K MAX | A: 52.34 | 1326. | | |
| | B: | | | |
| | C: | | | |
| | D: | | | |

ROOT MEAN SQUARE 34.88
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: STRESS RELIEVED E. B. WELDMENT (HEAT AFFECTED ZONE)
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: 08144

| |
|-----------------|
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| TI-6AL- 4V |
| |

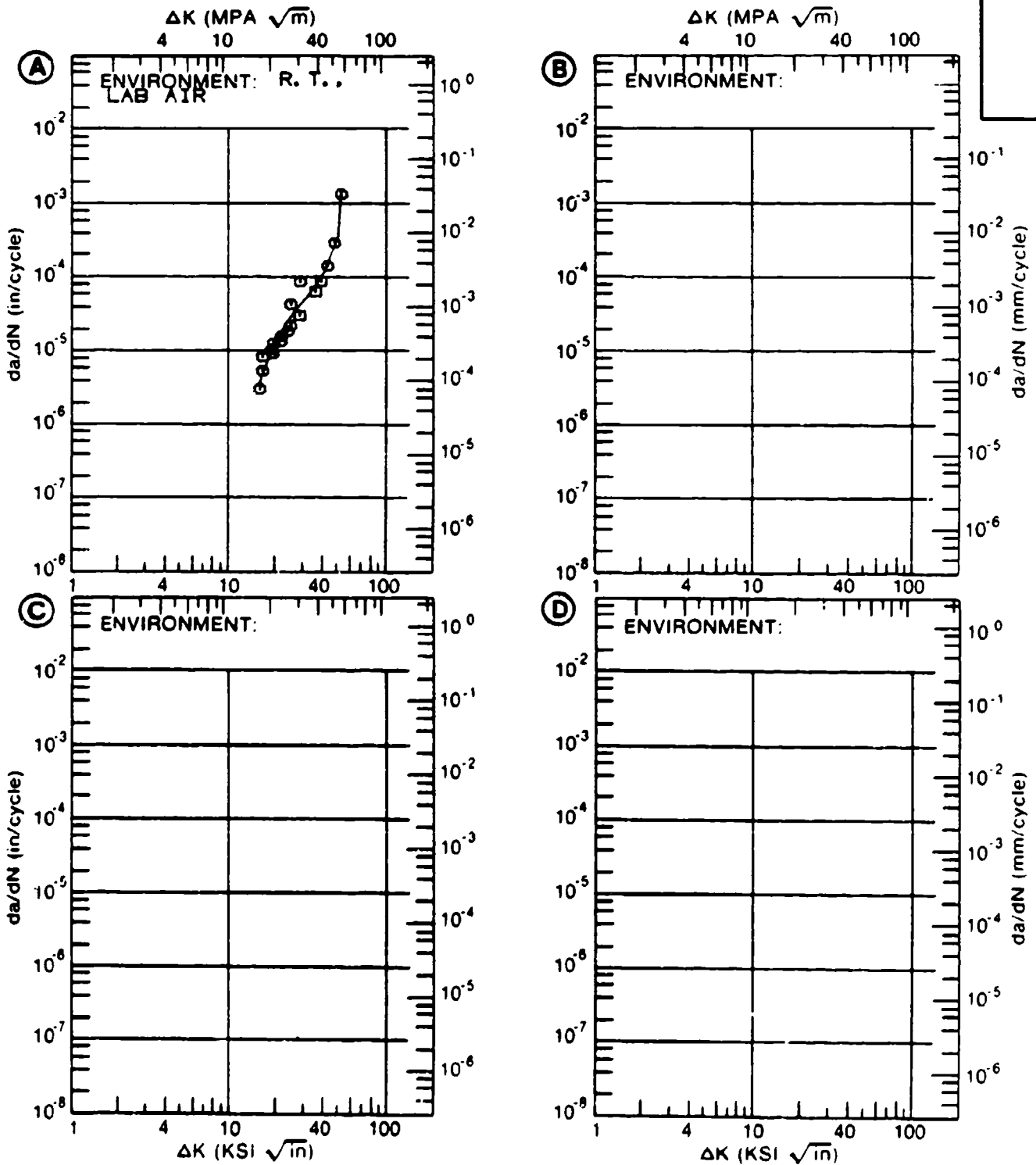


Figure 4.11.3.112

TABLE 4.11.3.113

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.113 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: STRESS RELIEVED E. B. WELDMENT (HEAT
AFFECTED ZONE)

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | | |
|--------------------------|-------|---------------------------------------|-----------------|-----------------------|-------------------------|------|
| | | A | B | C | D | |
| | | E=- 65F AIR | E=+ 175F AIR | E= R. T. JP-4 FUEL | E=+ 175F DIST. WATER | |
| DELTA K MIN | A: | 29.03 | 59.9 | | | |
| | B: | 16.93 | | 4.81 | | |
| | C: | 18.23 | | 5.47 | | |
| | D: | 29.99 | | | 46.8 | |
| | | 20.00 | | 8.82 | 9.65 | |
| | | 25.00 | | 15.2 | 16.8 | |
| | | 30.00 | 56.6 | 22.0 | 22.4 | 46.9 |
| | | 35.00 | 143. | 32.1 | 43.5 | 85.6 |
| | | 40.00 | 461. | 49.8 | 145. | 192. |
| | | 50.00 | | 150. | 1561. | 952. |
| | 60.00 | | 1058. | | 3157. | |
| DELTA K MAX | A: | 43.08 | 585. | | | |
| | B: | 61.62 | | 2449. | | |
| | C: | 56.28 | | 2318. | | |
| | D: | 67.44 | | | 5530. | |
| ROOT MEAN SQUARE | | 54.47 | 24.73 | 75.15 | 53.19 | |
| PERCENT ERROR | | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: STRESS RELIEVED E. B. WELDMENT (HEAT AFFECTED ZONE)
 FORM: 1.00" TH WELDMENT YIELD STRENGTH:
 SPECIMEN TYPE: CT ULT. STRENGTH:
 ORIENTATION: T-L SPECIMEN THK: 1.000"
 STRESS RATIO: +0.10 SPECIMEN WIDTH: 2.550"
 FREQUENCY: 0.10- 10.00 HZ REFERENCES: 00144

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 4V

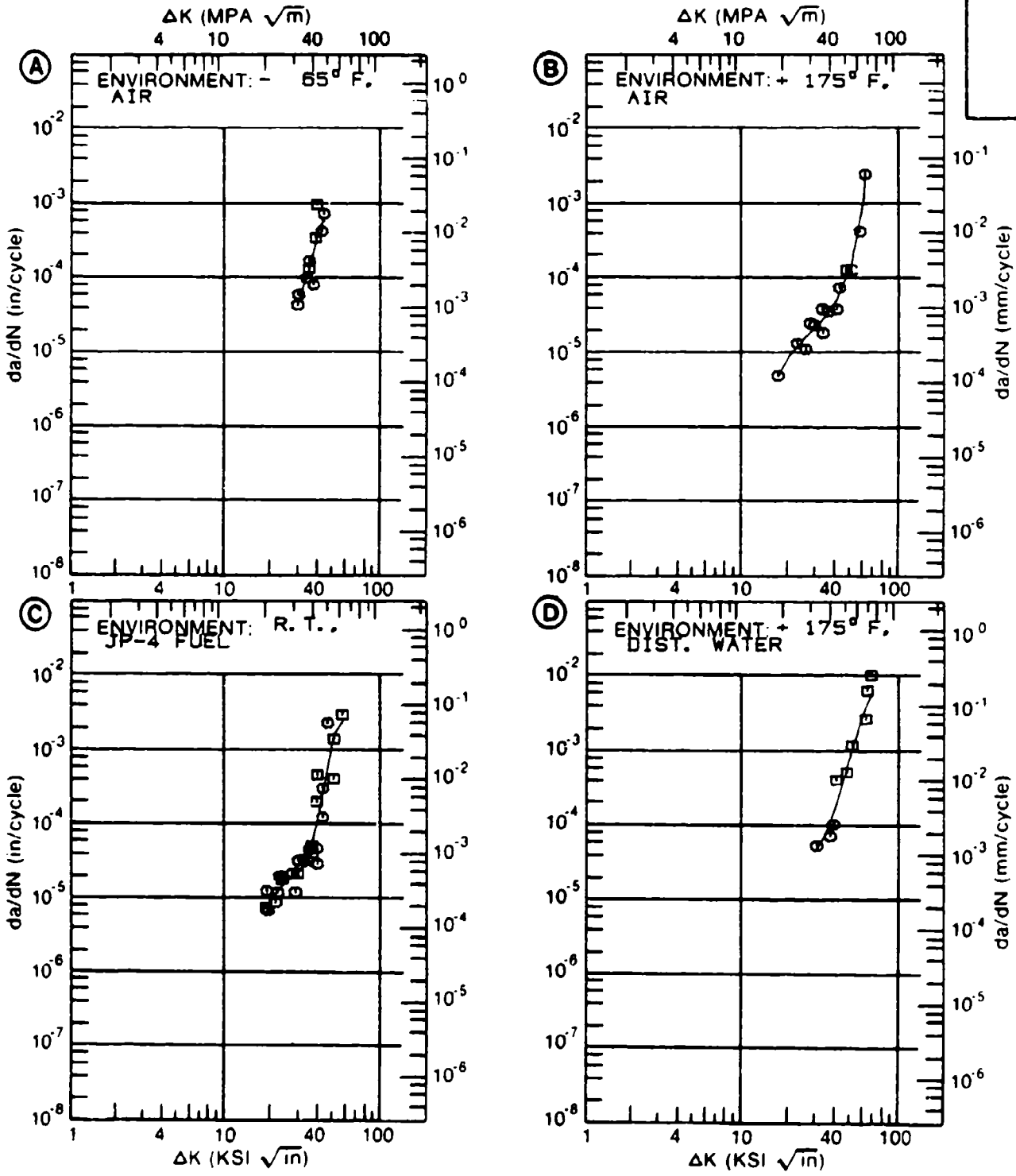


Figure 4.11.3.113

TABLE 4.11.3.114

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.114 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|--------------------------|----------|----------------------------|------|---|---|
| CONDITION: AS WELDED | | E. B. WELDMENT (WELD ZONE) | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: | 16.39 | .700 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 5.94 | | | |
| | 25.00 | 18.0 | | | |
| DELTA K MAX | A: | 25.00 | 18.0 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 37.12 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: AS WELDED
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

E. B. WELDMENT (WELD ZONE)
 YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: 00144

| |
|-----------------|
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| TI-6AL- 4V |
| |

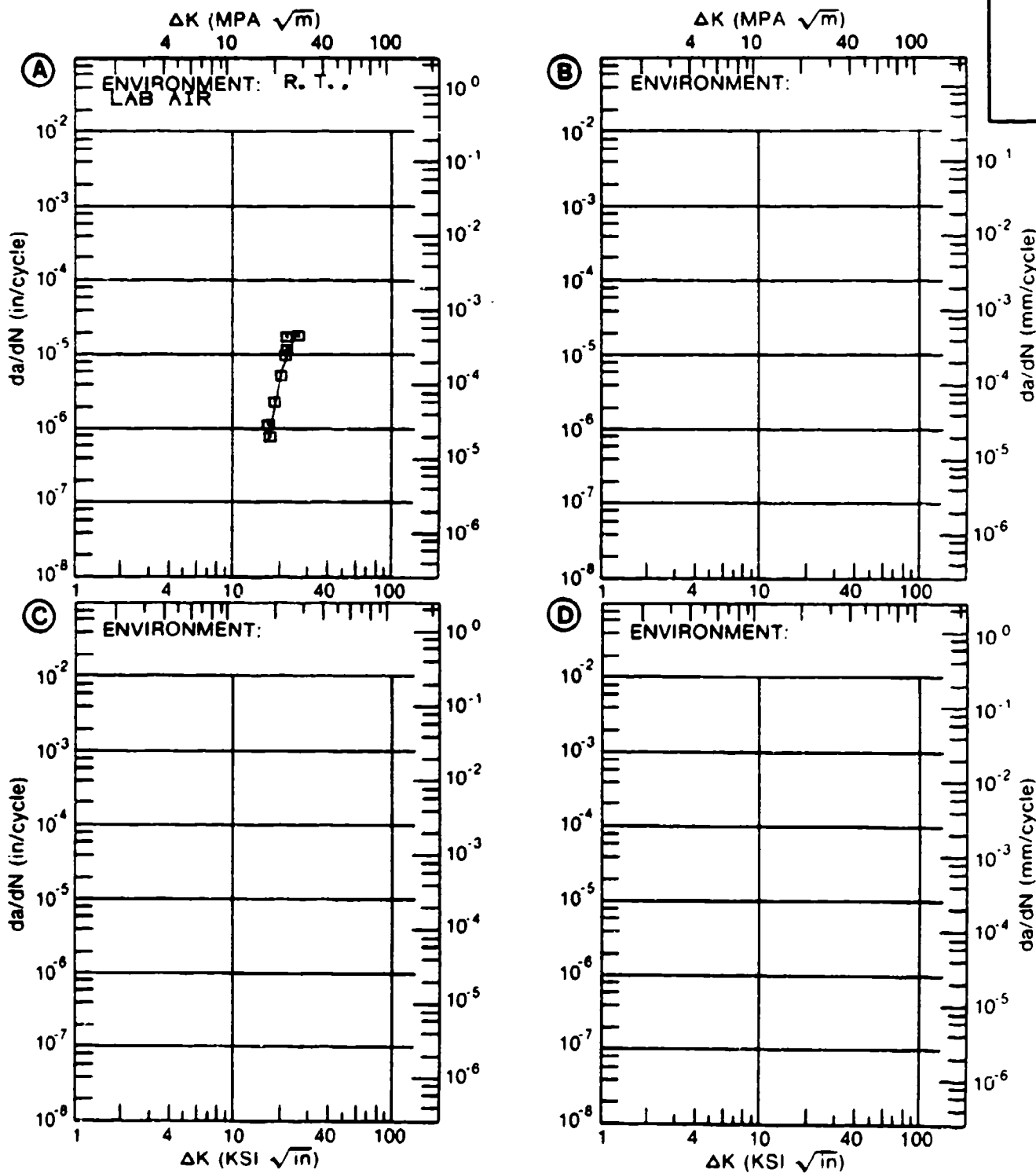


Figure 4.11.3.114

TABLE 4.11.3.115

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.11 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: AS WELDED E. B. WELDMENT (HEAT AFFECTED
ZONE)

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|-------|--------------------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: | 15.35 | 1.98 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 16.00 | 2.50 | | |
| | | 20.00 | 6.52 | | |
| | 25.00 | 13.2 | | | |
| | 30.00 | 24.7 | | | |
| | 35.00 | 50.2 | | | |
| DELTA K MAX | A: | 35.34 | 52.9 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 7.47
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: AS WELDED E. B. WELDMENT (HEAT AFFECTED ZONE)
 FORM: 1.00" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.000"
 REFERENCES: 00144

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TI-6AL-4V

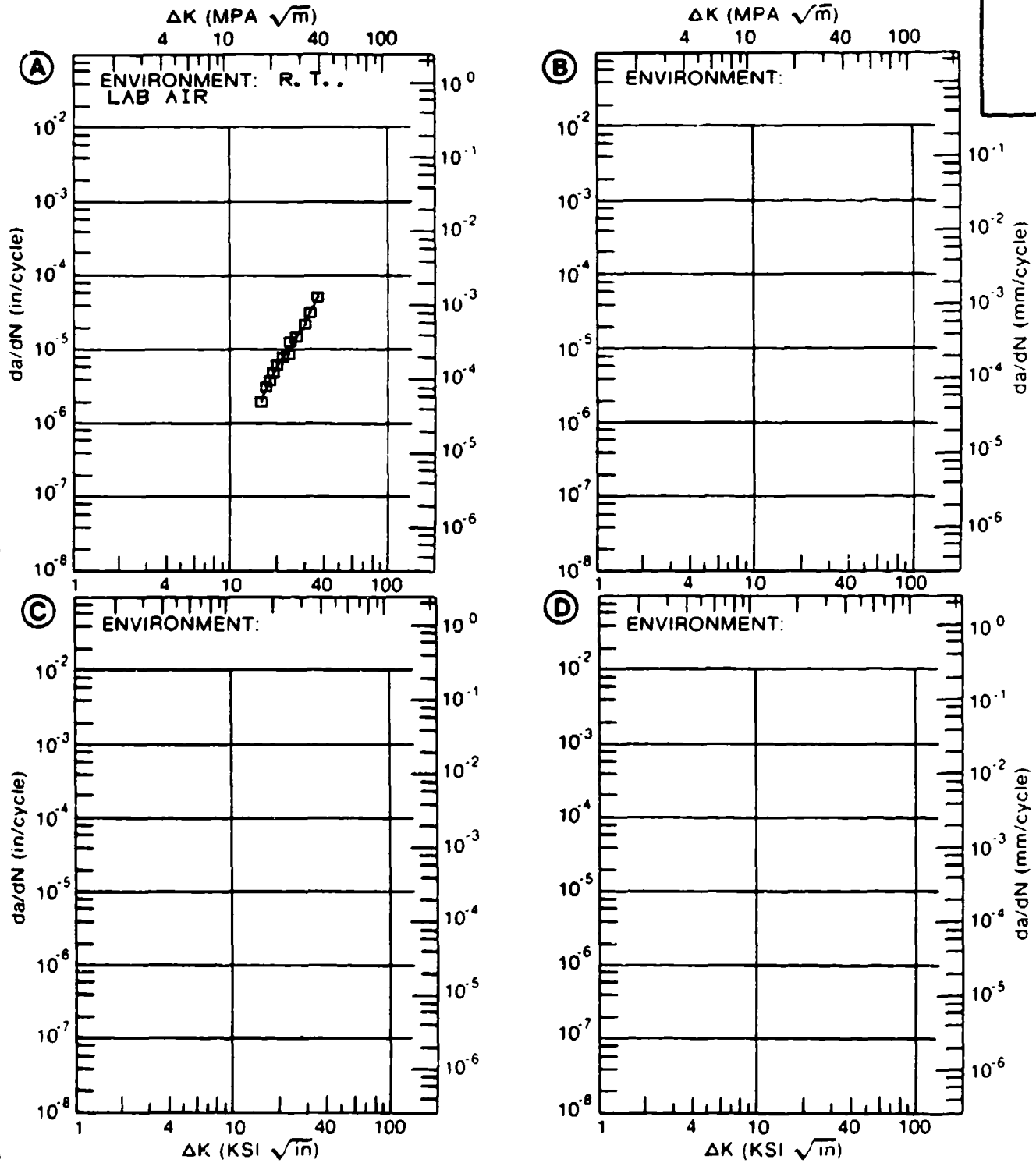


Figure 4.11.3.115

TABLE 4.11.3.116

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.116 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: WELDED & STRESS RELIEVED 1100F 2HRS (HAZ)

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|--------------------------------------|----------------------|---|---|
| | A | B | C | D |
| | E= R. T. L. H. A. | E= R. T. S. T. W. | | |
| DELTA K MIN | | | | |
| 200.00 | | | | |
| DELTA K MAX | | | | |

ROOT MEAN SQUARE 0.00 0.00
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: WELDED & STRESS RELIEVED 1100F 2HRS (HAZ)
 FORM: WELDMENT
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.08
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 131.0 KSI
 ULT. STRENGTH: 139.0 KSI
 SPECIMEN THK: 0.088- 0.100"
 SPECIMEN WIDTH: 24.000"
 REFERENCES: 88575

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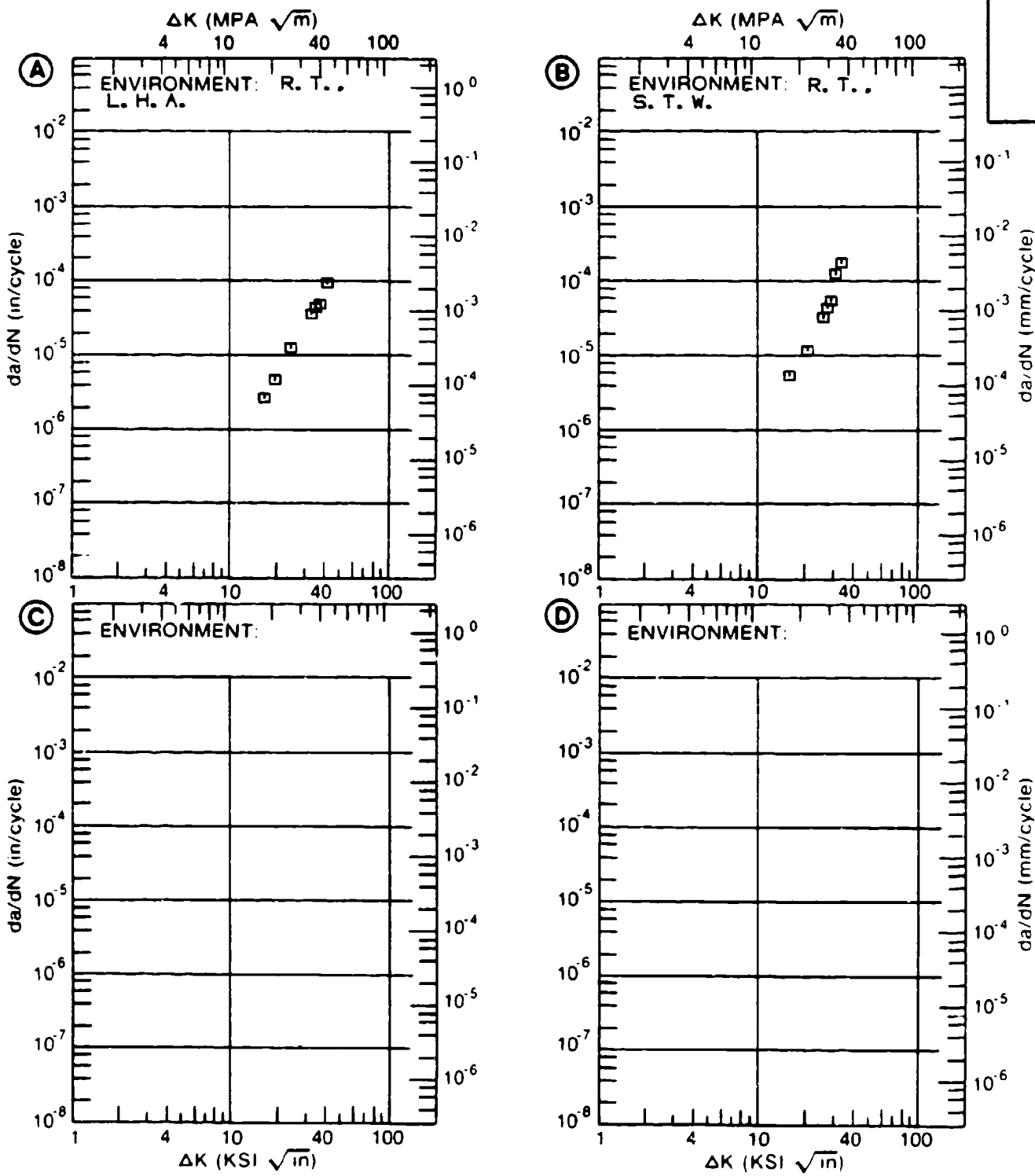


Figure 4.11.3.116

TABLE 4.11.3.117

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.117 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1550F 4HRS FC, 1000F 4HRS, ARGON COOLED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|-------------------|---|---|
| | | A | B | C | D |
| | | E= R. T. ARGON | E= R. T. ARGON | | |
| DELTA K MIN | A: 9.68 | .15 | | | |
| | B: 10.56 | | .26 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | .195 | | | |
| | 13.00 | .886 | .854 | | |
| | 16.00 | 1.94 | 1.96 | | |
| | 20.00 | 3.81 | 4.08 | | |
| | 25.00 | 7.97 | 9.01 | | |
| | 30.00 | 18.1 | 21.0 | | |
| 35.00 | 46.8 | 54.5 | | | |
| 40.00 | 137. | 158. | | | |
| DELTA K MAX | A: 44.83 | 434. | | | |
| | B: 41.26 | | 209. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 29.57 | 28.88 | | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1550F 4HRS FC, 1000F 4HRS, ARGON COOLED
 FORM: FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: R-C
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 140.9 KSI
 ULT STRENGTH: 150.1 KSI
 SPECIMEN THK: 0.800"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: UM001

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ALLOY

TI-6AL-
4V

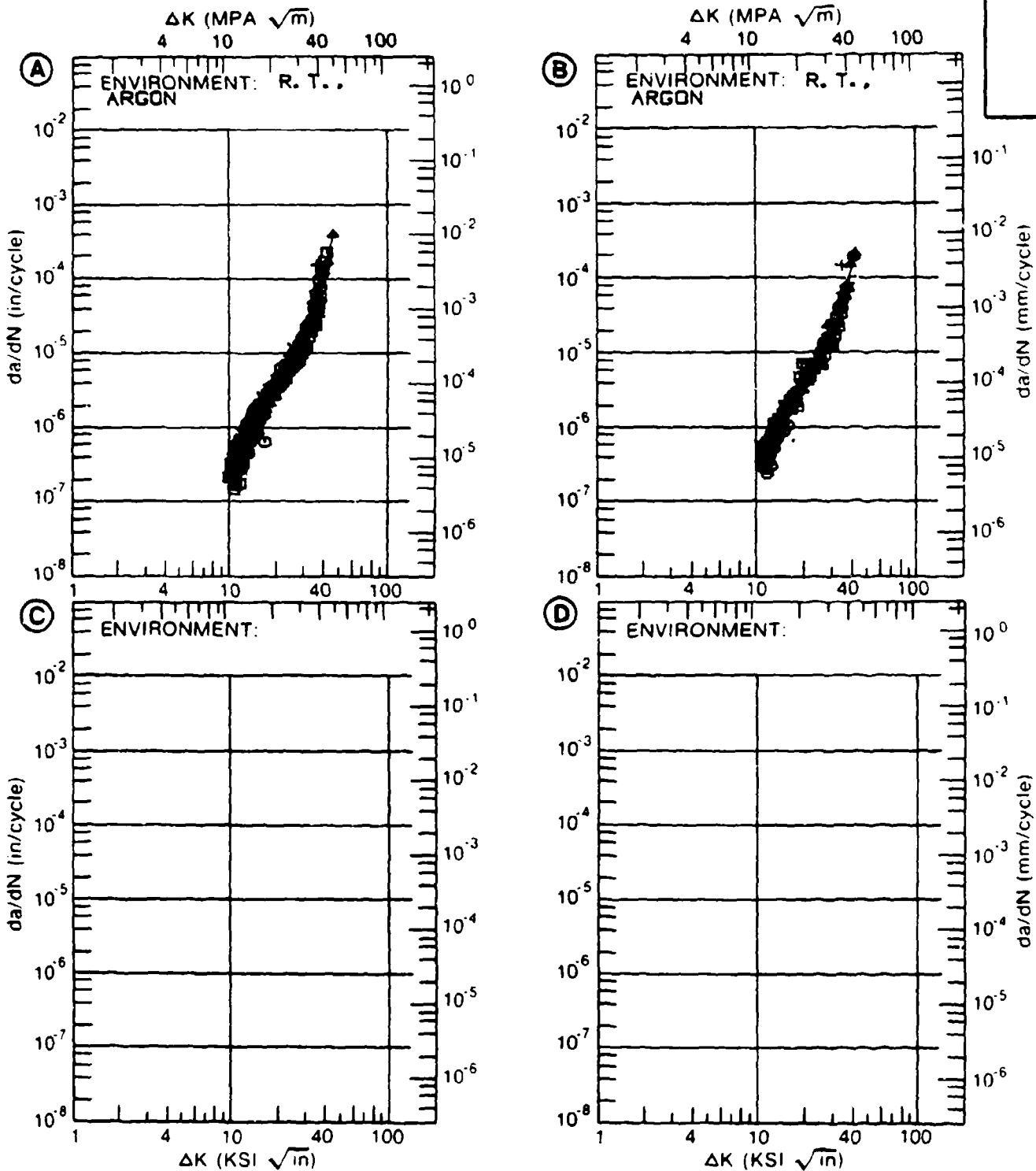


Figure 4.11.3.117

TABLE 4.11.3.118

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.118 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1750F 4HRS ARGON COOLED, 1000F 4HRS,
ARGON COOLED

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------------|---------------------------------------|-------|-------------------|------|
| | A | B | C | D |
| | E= R. T. ARGON | | E= R. T. ARGON | |
| DELTA K MIN | A: 10.46 | .20 | B: 10.57 | .15 |
| | C: 13.00 | .850 | D: 16.00 | .539 |
| | | 2.04 | | 1.54 |
| | | 4.05 | | 4.13 |
| | | 8.51 | | 10.5 |
| | | 20.4 | | 23.1 |
| | | 59.1 | | 48.0 |
| | | 207. | | 97.7 |
| DELTA K MAX | A: 42.45 | 407. | B: 43.64 | 163. |
| | C: | | D: | |
| ROOT MEAN SQUARE PERCENT ERROR | 31.31 | 41.13 | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1750F 4HRS ARGON COOLED, 1000F 4HRS, ARGON COOLED
 FORM: FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: R-C
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 135.7 KSI
 ULT. STRENGTH: 144.9 KSI
 SPECIMEN THK: 0.000"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: UM001

TITAN.
ALLOY

TI-6AL-
4V

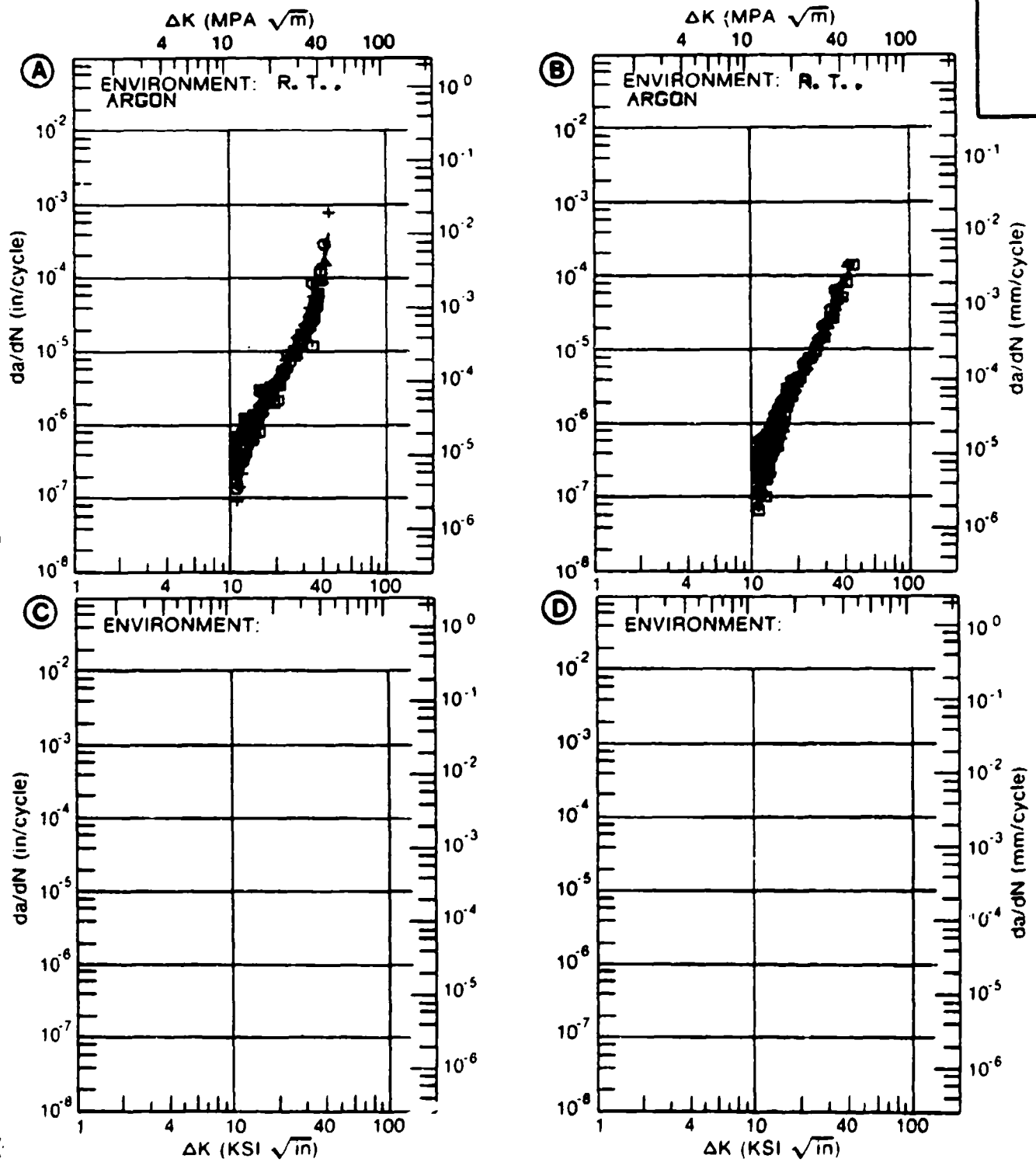


Figure 4.11.3.118

TABLE 4.11.3.119

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.119 INDICATING EFFECT

OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1750F 4HRS ARGON COOLED, 1000F 4HRS
ARGON COOLED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|-------|--------------------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. T. ARGON | | | |
| DELTA K MIN | A: | 10.71 | .231 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 13.00 | .681 | | |
| | | 16.00 | 1.81 | | |
| | | 20.00 | 4.61 | | |
| | 25.00 | 11.7 | | | |
| | 30.00 | 27.1 | | | |
| | 35.00 | 60.7 | | | |
| | 40.00 | 229. | | | |
| DELTA K MAX | A: | 40.42 | 360. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 23.92 | | | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1750F 4HRS ARGON COOLED, 1000F 4HRS ARGON COOLED
 FORM: FORGING YIELD STRENGTH: 135.7 KSI
 SPECIMEN TYPE: WOL ULT. STRENGTH: 144.9 KSI
 ORIENTATION: C-R SPECIMEN THK: 0.800"
 STRESS RATIO: +0.10 SPECIMEN WIDTH: 2.550"
 FREQUENCY: 10.00 HZ REFERENCES: UM001

TITAN.
ALLOY

TI-6AL-
4V

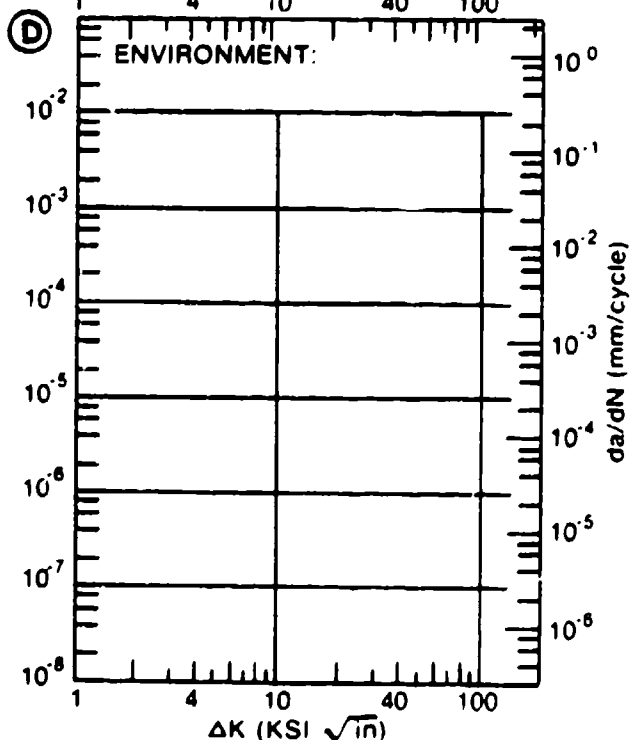
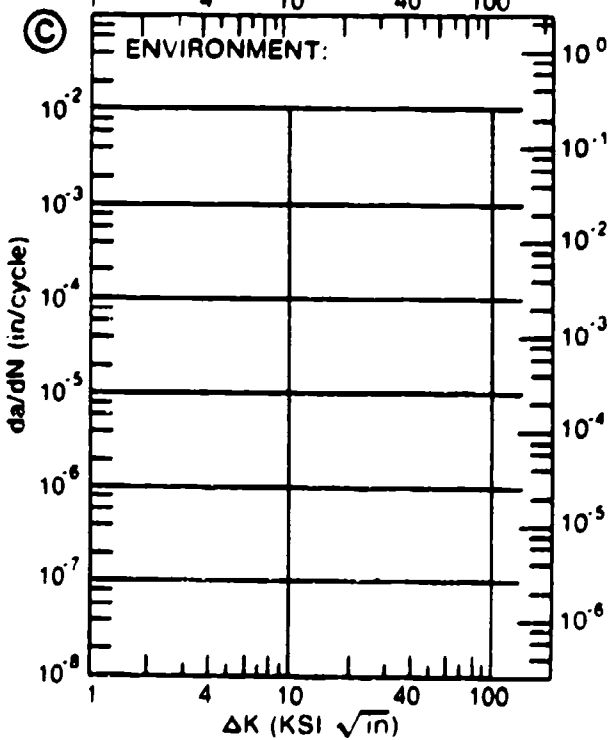
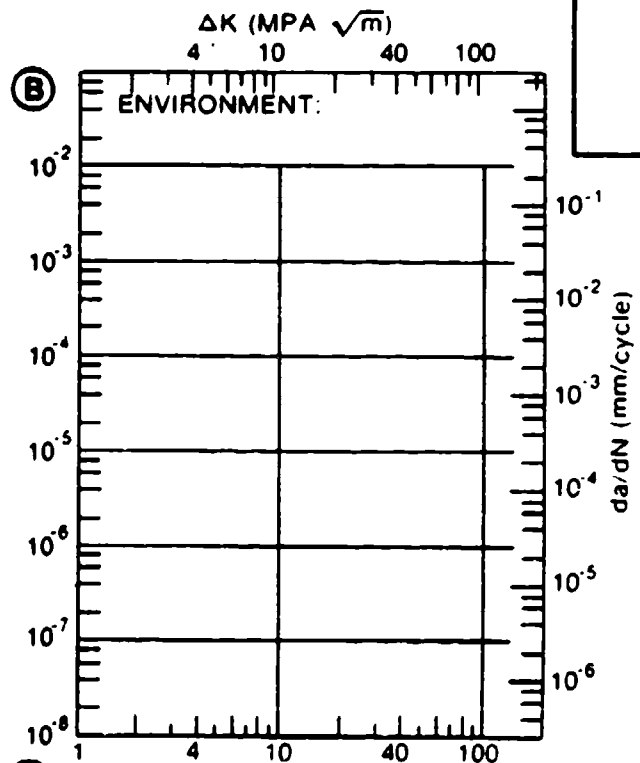
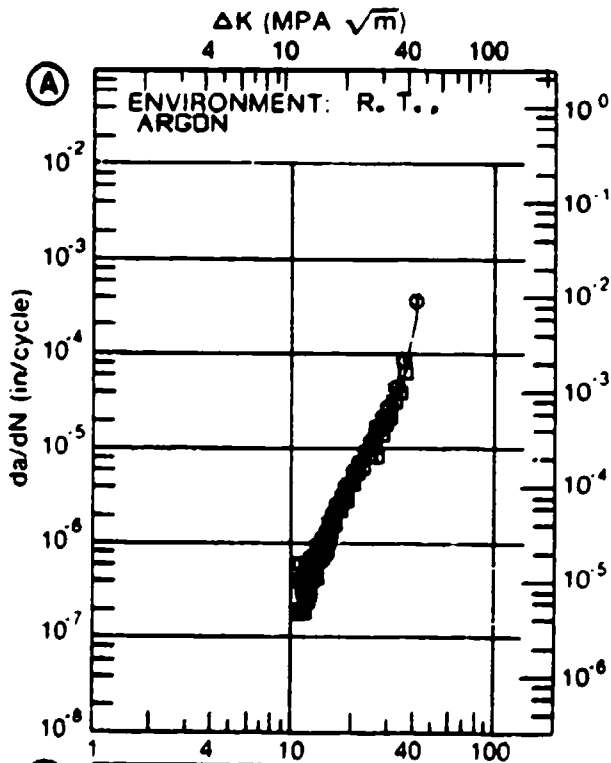


Figure 4.11.3.119

TABLE 4.11.3.120

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.120 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1775F 1HR WG, 1675F 1HR WG, 1000F 4HRS
AC, 900F 5HR AC

| DELTA K (KSI*IN**1/2) | DA/DN (10**6 IN./CYCLE) | | | |
|--------------------------------|-------------------------|-------|-----------------|---|
| | A | B | C | D |
| | E= R. T. LAB AIR | | E=+ 200F AIR | |
| DELTA K MIN | A: 30.47 | 37.2 | B: 48.5 | |
| | B: 30.79 | | | |
| | C: | | | |
| | D: | | | |
| | 35.00 | 58.5 | 96.8 | |
| | 40.00 | 83.9 | 167. | |
| | 50.00 | 152. | 356. | |
| | 60.00 | 290. | 745. | |
| | 70.00 | 625. | 1817. | |
| | 80.00 | 1545. | | |
| DELTA K MAX | A: 80.58 | 1635. | B: 2874. | |
| | B: 74.44 | | | |
| | C: | | | |
| | D: | | | |
| ROOT MEAN SQUARE PERCENT ERROR | 7.07 | | 7.10 | |

LIFE PREDICTION RATIO SUMMARY (NP/NA)

| | |
|----------|---|
| 0.0-0.5 | |
| 0.5-0.8 | 1 |
| 0.8-1.25 | 1 |
| 1.25-2.0 | |
| >2.0 | |

CONDITION/HT: 1775F 1HR WQ, 1875F 1HR WQ, 1000F 4HRS AC, 900F 5HR AC
 FORM: 0.50" TH DISK
 SPECIMEN TYPE: CCP
 ORIENTATION: C-R
 STRESS RATIO: +0.05
 FREQUENCY: 0.33- 10.00 HZ

YIELD STRENGTH: 120.0 KSI
 ULT. STRENGTH: 130.0 KSI
 SPECIMEN THK: 0.120"
 SPECIMEN WIDTH: 1.980"
 REFERENCES: GE003

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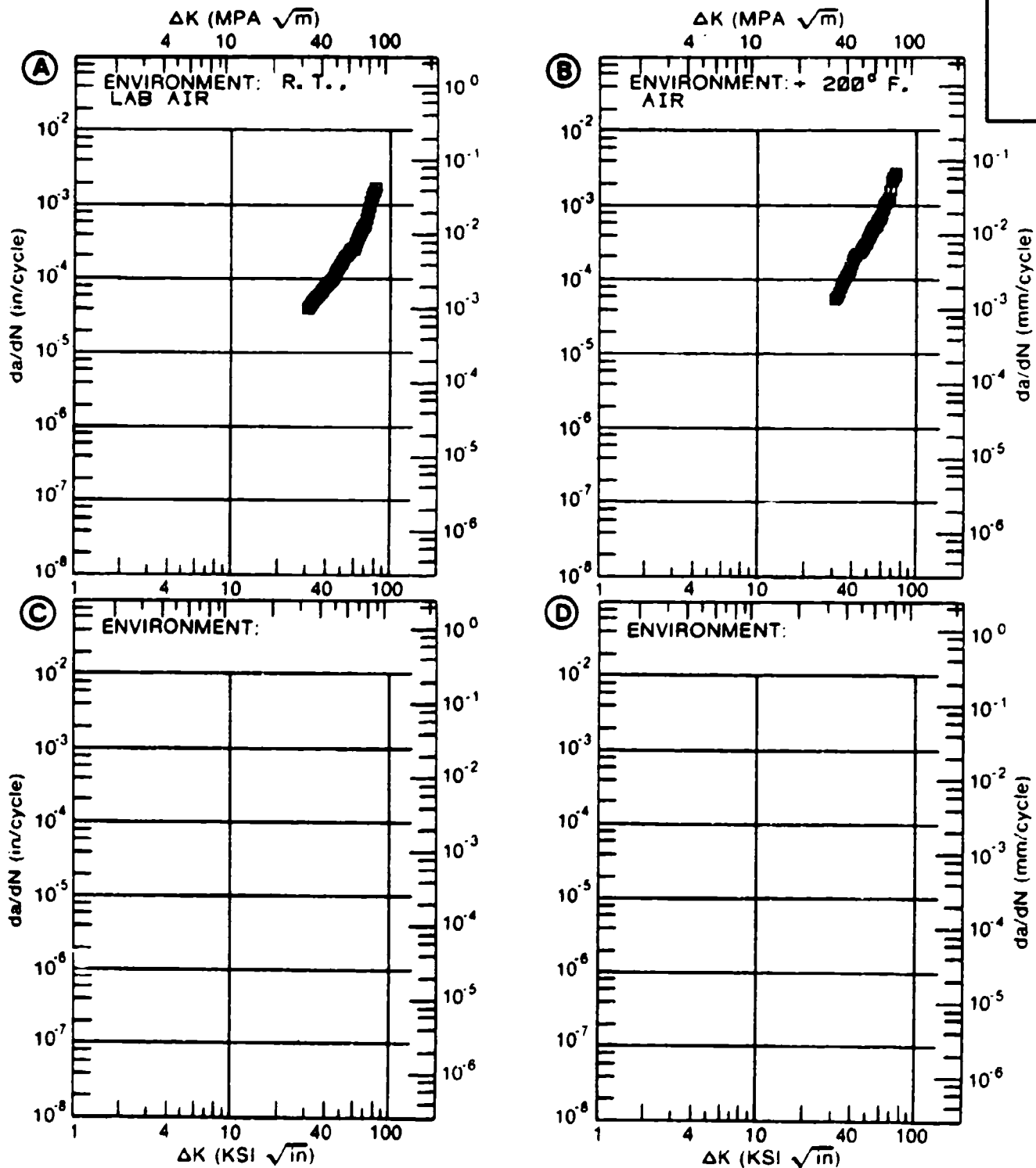


Figure 4.11.3.120

TABLE 4.11.3.121

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.121 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1775F 1HR WG, 1675F 1HR WG, 1000F-1200F
2-8HRS AC
ENVIRONMENT: R. T. , LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.03 | R=+0.25 | R=+0.54 | |
| DELTA K MIN | A: 9.85 | .788 | | | |
| | B: 10.87 | | 2.71 | | |
| | C: 10.48 | | | 3.11 | |
| | D: | | | | |
| | 10.00 | .865 | | | |
| | 13.00 | 3.13 | 4.91 | 6.16 | |
| | 16.00 | 6.22 | 9.51 | 11.5 | |
| | 20.00 | 11.0 | 18.9 | | |
| 25.00 | 18.9 | 37.5 | | | |
| 30.00 | 32.1 | 66.2 | | | |
| 35.00 | 57.0 | | | | |
| 40.00 | 107. | | | | |
| DELTA K MAX | A: 44.18 | 191. | | | |
| | B: 30.68 | | 71.1 | | |
| | C: 19.06 | | | 15.7 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 15.97 | 10.81 | 14.72 | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F 2-8HRS AC
 FORM: 0.94" TH DISK
 SPECIMEN TYPE: KB BAR
 ORIENTATION: C-R
 FREQUENCY: 0.33- 0.50 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 150.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.251- 0.252"
 SPECIMEN WIDTH: 0.989- 1.000"
 REFERENCES: GE007

TITAN.
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TI-6AL-
4V

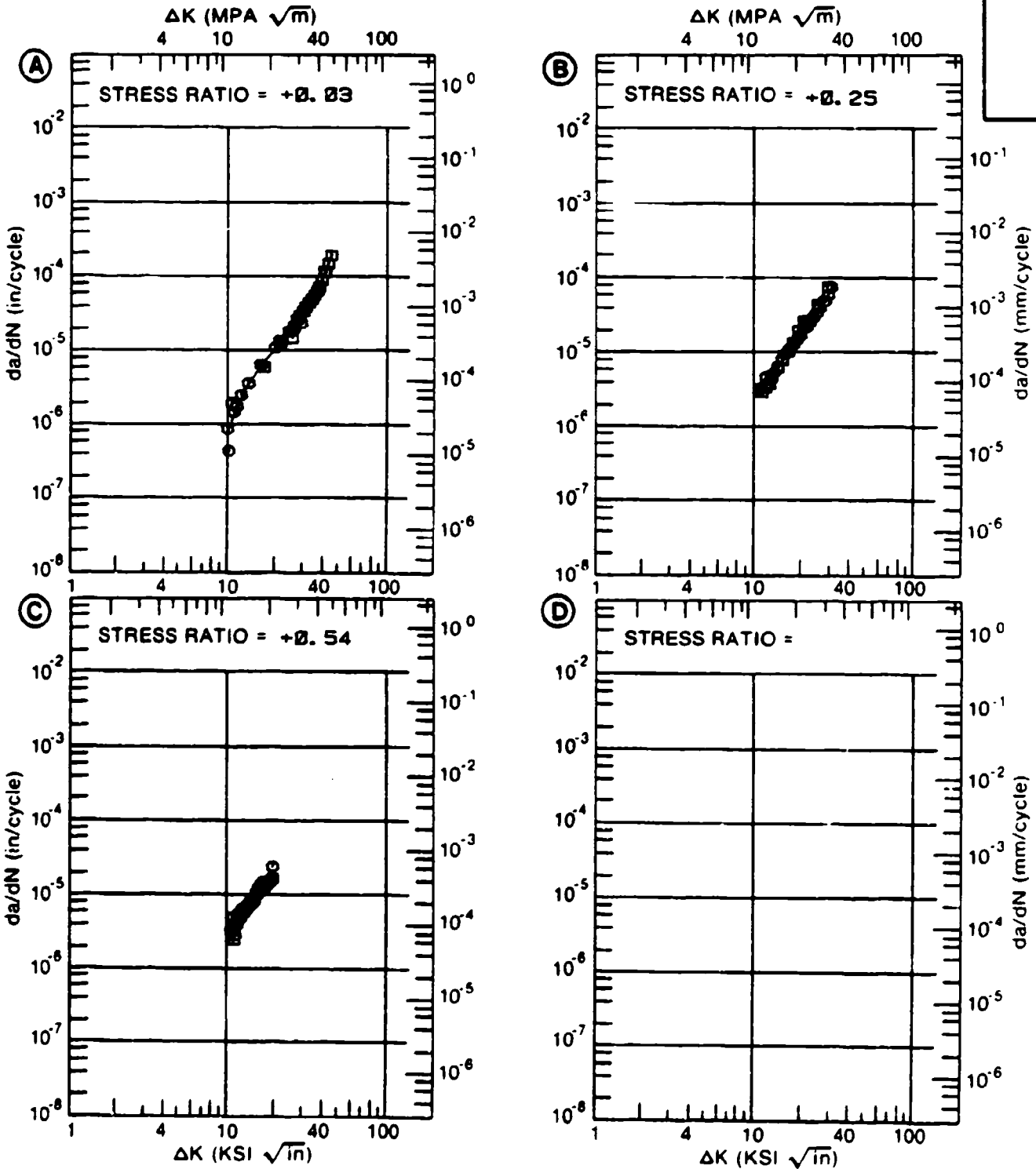


Figure 4.11.3.121

TABLE 4.11.3.122

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.122 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F
2-8HRS AC
ENVIRONMENT: + 300F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------------|----------|---------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.03 | R=+0.25 | R=+0.54 | |
| MIN | A: 9.83 | .687 | | | |
| | B: 10.90 | | 1.46 | | |
| | C: 11.42 | | | 3.45 | |
| | D: | | | | |
| | 10.00 | .746 | | | |
| | 13.00 | 2.32 | 3.46 | 5.10 | |
| | 16.00 | 4.94 | 6.88 | 8.22 | |
| | 20.00 | 10.1 | 11.9 | | |
| | 25.00 | 19.7 | 20.9 | | |
| | 30.00 | 33.4 | 39.8 | | |
| | 35.00 | 52.7 | | | |
| | 40.00 | 79.8 | | | |
| MAX | A: 41.12 | 87.2 | | | |
| | B: 32.83 | | 60.4 | | |
| | C: 18.98 | | | 11.5 | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 15.61 | 21.04 | 6.65 | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F 2-8HRS AC
 FORM: 0.94" TH DISK
 SPECIMEN TYPE: KB BAR
 ORIENTATION: C-R
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: + 300° F. AIR
 YIELD STRENGTH: 150.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.252"
 SPECIMEN WIDTH: 0.991- 0.999"
 REFERENCES GE007

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ALLOY

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4V

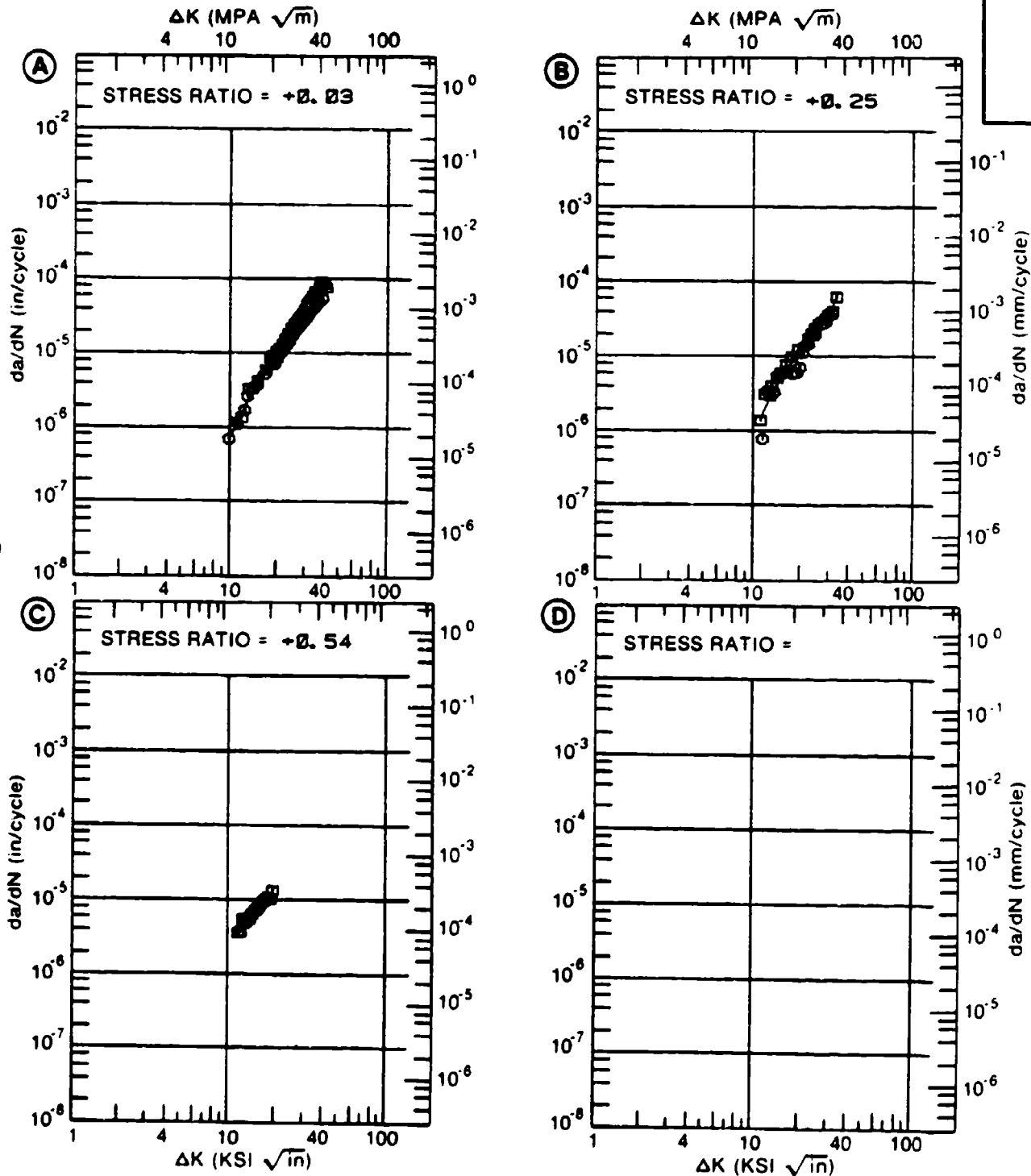


Figure 4.11.3.122

TABLE 4.11.3.123

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.123 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1775F 1HR WG, 1675F 1HR WG, 1000F-1200F
2-8HRS AC
ENVIRONMENT: + 600F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.03 | R=+0.25 | R=+0.54 | |
| DELTA K | A: 8.19 | .501 | | | |
| MIN | B: 9.28 | | 1.84 | | |
| | C: 8.94 | | | 1.96 | |
| | D: | | | | |
| | 9.00 | .715 | | 1.96 | |
| | 10.00 | 1.05 | 2.04 | 2.12 | |
| | 13.00 | 2.57 | 3.70 | 4.38 | |
| | 16.00 | 4.99 | 6.85 | 8.94 | |
| | 20.00 | 9.87 | 13.3 | | |
| | 25.00 | 19.2 | 22.6 | | |
| | 30.00 | 32.9 | 28.3 | | |
| | 35.00 | 52.0 | | | |
| | 40.00 | 77.8 | | | |
| DELTA K | A: 42.82 | 95.8 | | | |
| MAX | B: 30.82 | | 28.7 | | |
| | C: 19.48 | | | 13.6 | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.62 | 14.03 | 14.72 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F 2-8HRS AC
 FORM: 0.94" TH DISK
 SPECIMEN TYPE: KB BAR
 ORIENTATION: C-R
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: + 600° F, AIR

YIELD STRENGTH: 150.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.251- 0.253"
 SPECIMEN WIDTH: 0.995- 1.002"
 REFERENCES: GE007

TITAN.
ALLOY

TI-6AL-
4V

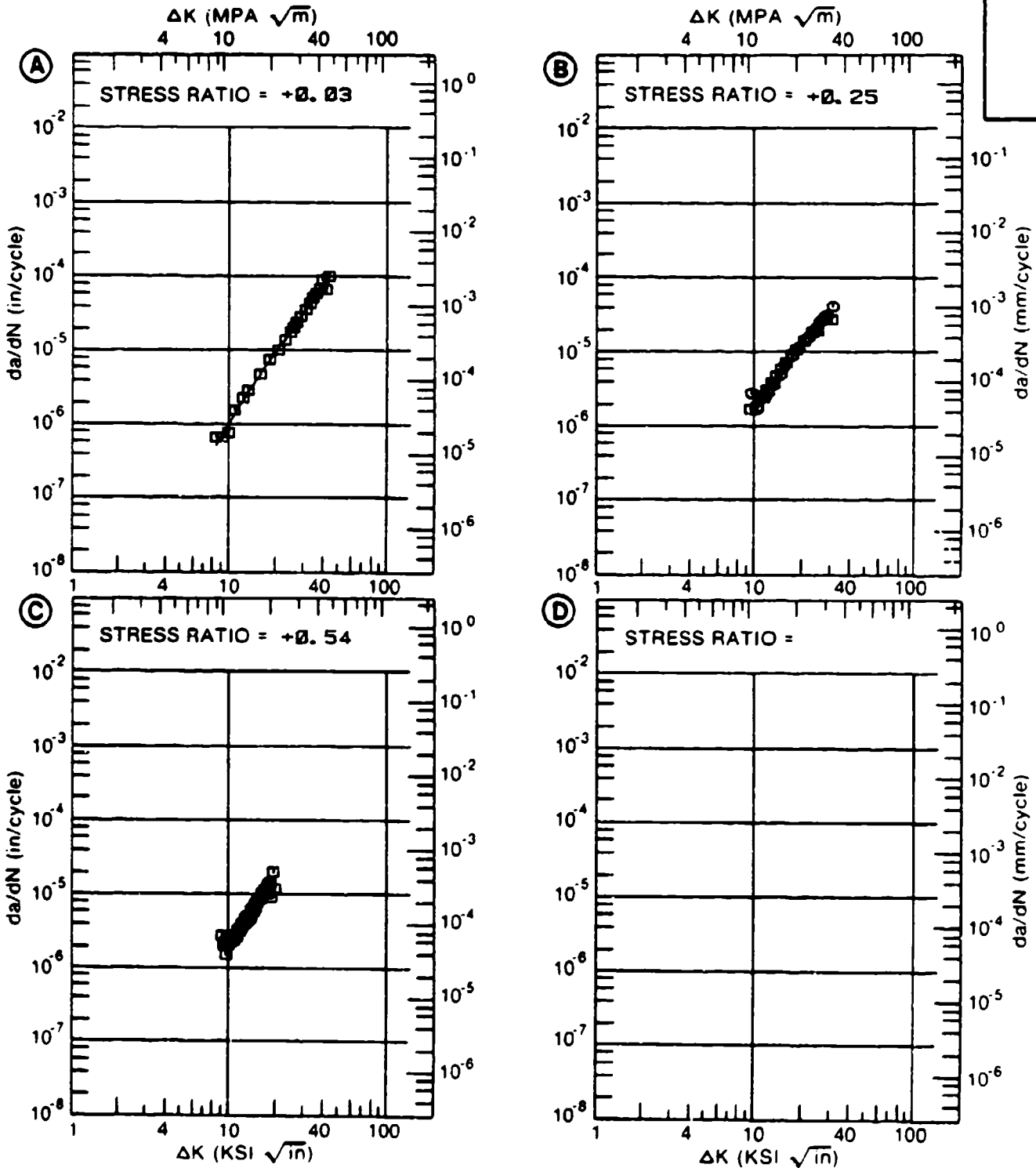


Figure 4.11.3.123

TABLE 4.11.3.124

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.124 INDICATING EFFECT

OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F
2-8HRS AC
ENVIRONMENT: + 600F, AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| | | A | B | C | D |
| | | R=+0.03 | | | |
| DELTA K | A: 8.01 | .906 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | 1.29 | | | |
| | 10.00 | 1.77 | | | |
| | 13.00 | 3.85 | | | |
| | 16.00 | 6.94 | | | |
| | 20.00 | 12.6 | | | |
| | 25.00 | 21.6 | | | |
| | 30.00 | 32.2 | | | |
| | 35.00 | 43.5 | | | |
| | 40.00 | 54.6 | | | |
| DELTA K | A: 42.55 | 60.1 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 7.35
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1775F 1HR WQ, 1675F 1HR WQ, 1000F-1200F 2-8HRS AC
 FORM: 1.15" TH DISK
 SPECIMEN TYPE: KB BAR
 ORIENTATION: C-R
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: + 800° F, AIR

YIELD STRENGTH: 145.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.251"
 SPECIMEN WIDTH: 1.000"
 REFERENCES: GE007

TITAN.
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TI-6AL-
4V

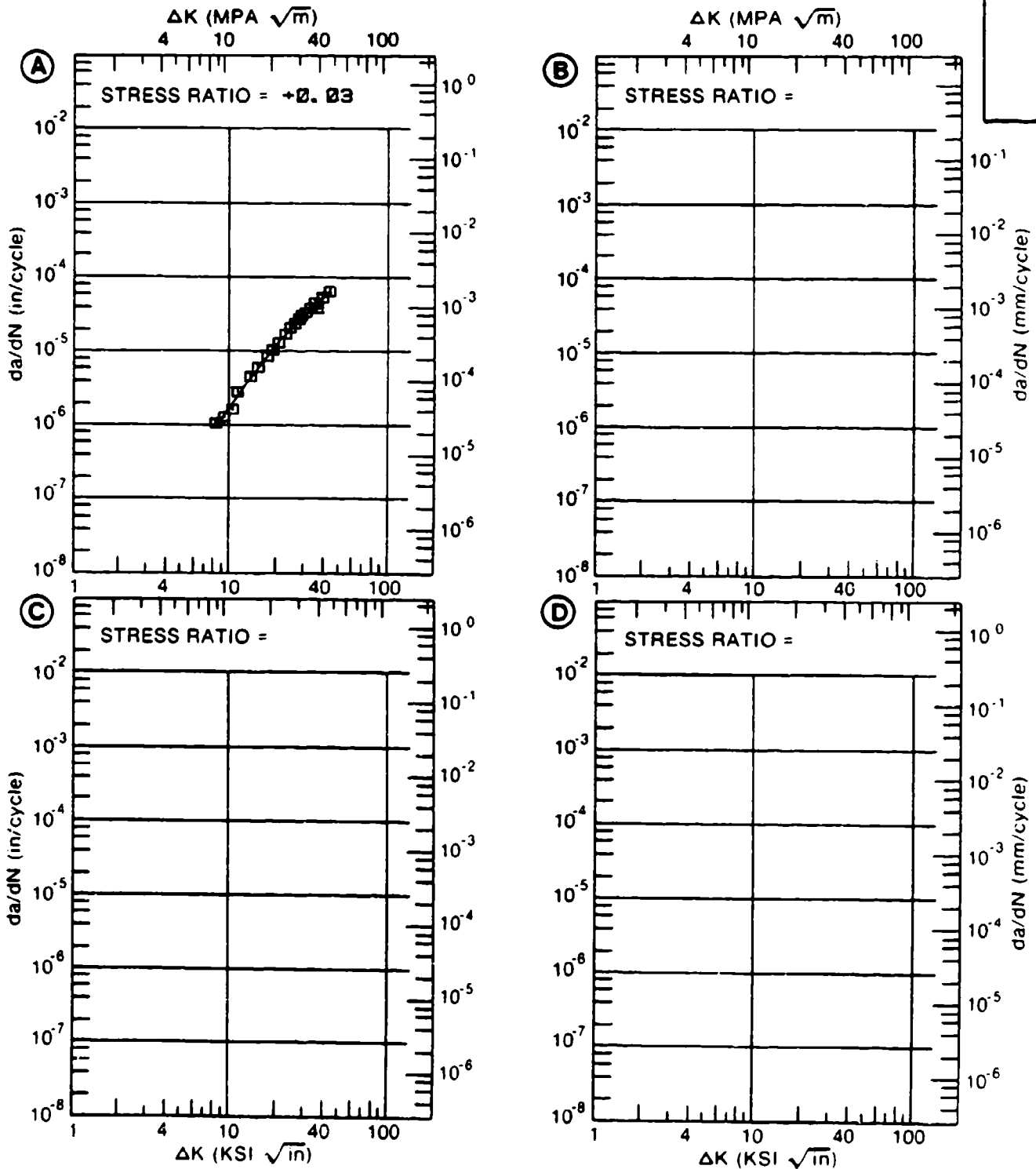


Figure 4.11.3.124

TABLE 4.11.3.125

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.125 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1950F 4HRS WG, 1000F 4HRS ARGON COOLED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. ARGON | | | |
| DELTA K | A: 10.04 | .179 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .508 | | | |
| | 16.00 | 1.08 | | | |
| | 20.00 | 2.38 | | | |
| | 25.00 | 5.58 | | | |
| | 30.00 | 12.3 | | | |
| | 35.00 | 26.6 | | | |
| | 40.00 | 56.9 | | | |
| | 50.00 | 257. | | | |
| DELTA K | A: 50.06 | 260. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 57.10
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1950F 4HRS WQ, 1000F 4HRS ARGON COOLED
 FORM: FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: R-C
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 136.4 KSI
 ULT. STRENGTH: 147.9 KSI
 SPECIMEN THK: 0.800"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: UM001

TITAN.
ALLOY

TI-6AL-4V

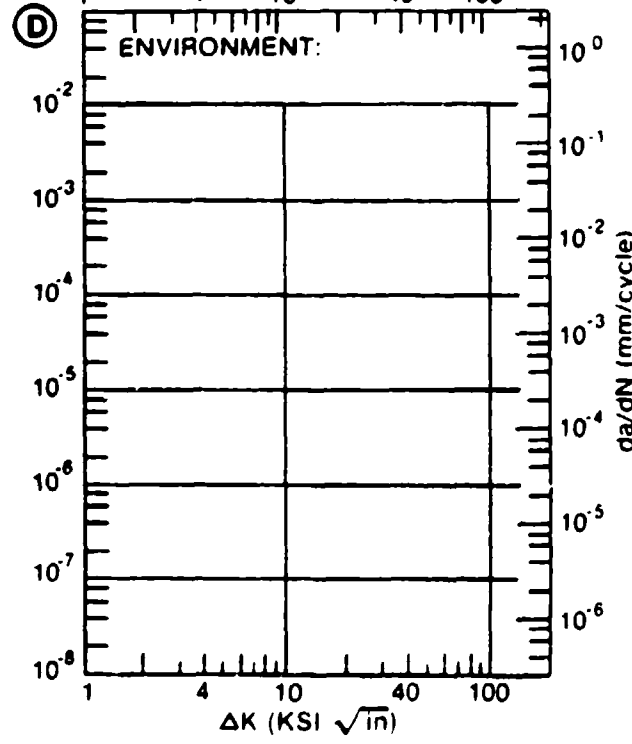
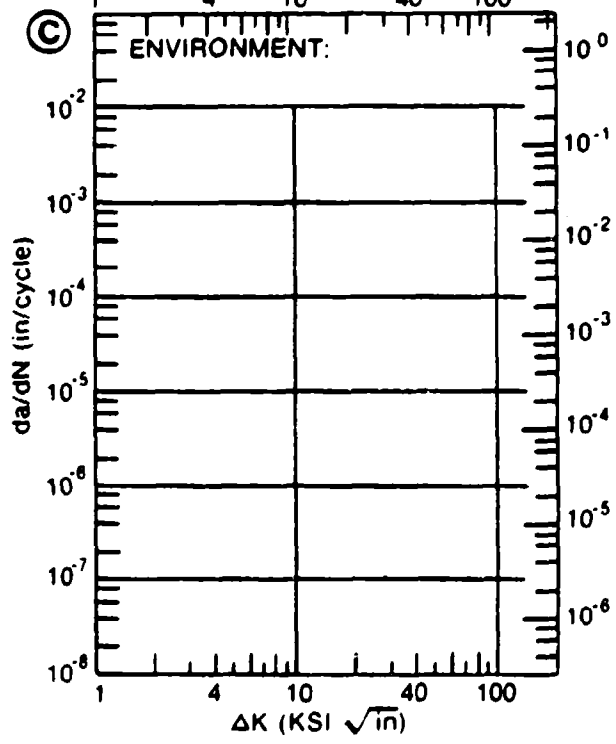
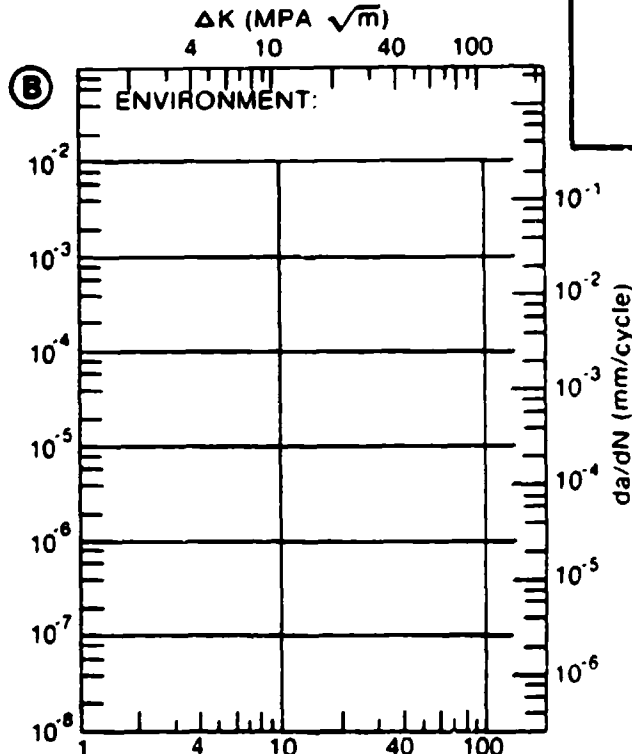
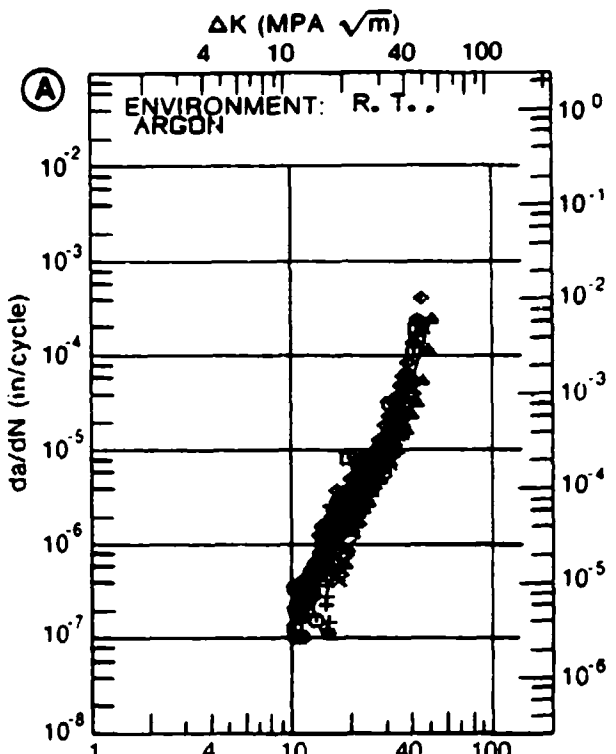


Figure 4.11.3.125

TABLE 4.11.3.126

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.126 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: 1950F 4HRS WQ, 1000F 4HRS ARGON COOLED

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|-------|---------------------------------------|------|---|---|
| | | A | B | C | D |
| | | E= R. T. ARGON | | | |
| DELTA K MIN | A: | 11.18 | .159 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 13.00 | .442 | | |
| | | 16.00 | 1.31 | | |
| | 20.00 | 3.37 | | | |
| | 25.00 | 8.42 | | | |
| | 30.00 | 20.3 | | | |
| | 35.00 | 51.3 | | | |
| DELTA K MAX | A: | 35.49 | 56.4 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 39.65
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1950F 4HRS WQ, 1000F 4HRS ARGON COOLED
 FORM: FORGING
 SPECIMEN TYPE: WOL
 ORIENTATION: C-R
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 136.4 KSI
 ULT. STRENGTH: 147.8 KSI
 SPECIMEN THK: 0.800"
 SPECIMEN WIDTH: 2.550"
 REFERENCES: UM001

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4V

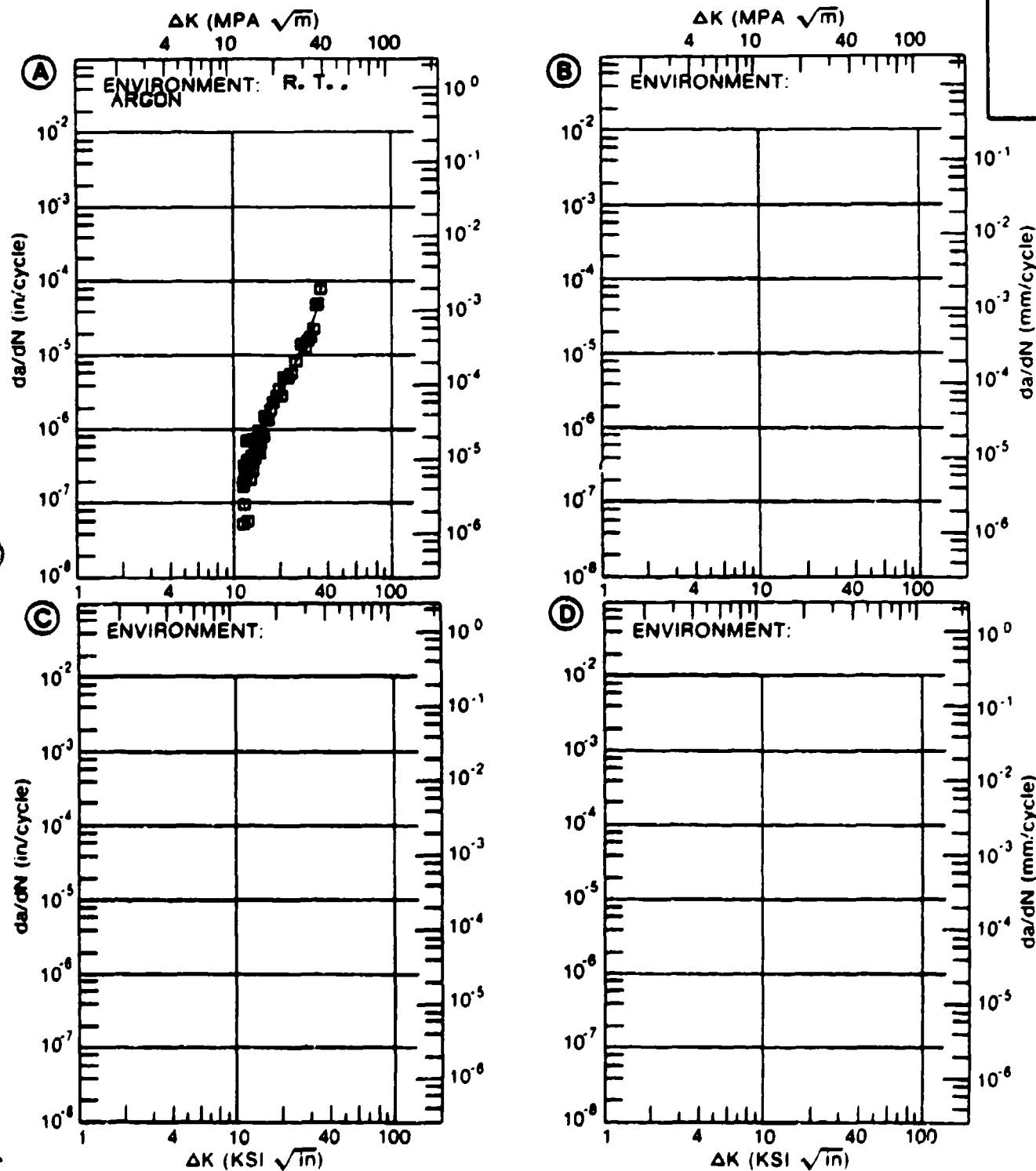


Figure 4.11.3.126

TABLE 4.11.3.127

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.127 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V
CONDITION: EB WELD, STRESS RELIEVED (HEAT AFFECTED ZONE)

| K MAX (KSI*IN**1/2) | DA/DT (10**-6 IN/HOUR) | | | |
|-----------------------------------|------------------------|------|-----------|----|
| | A | B | C | D |
| | E= | | E= | |
| | 3.5% NACL; 75F | | AIR; 175F | |
| K MAX MIN | A: | B: | C: | D: |
| 200.00 | | | | |
| K MAX MAX | A: | B: | C: | D: |
| | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | 0.00 | 0.00 | | |

CONDITION/HT: EB WELD, STRESS RELIEVED (HEAT AFFECTED ZONE)
 FORM: 1.0" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 YIELD STRENGTH: 132.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 CRACK LENGTH (A₀):
 K_{ISCC}: 33.00 KSI (SQRT IN)
 REFERENCES: 88144

TITAN.
ALLOY

TI-6AL-4V

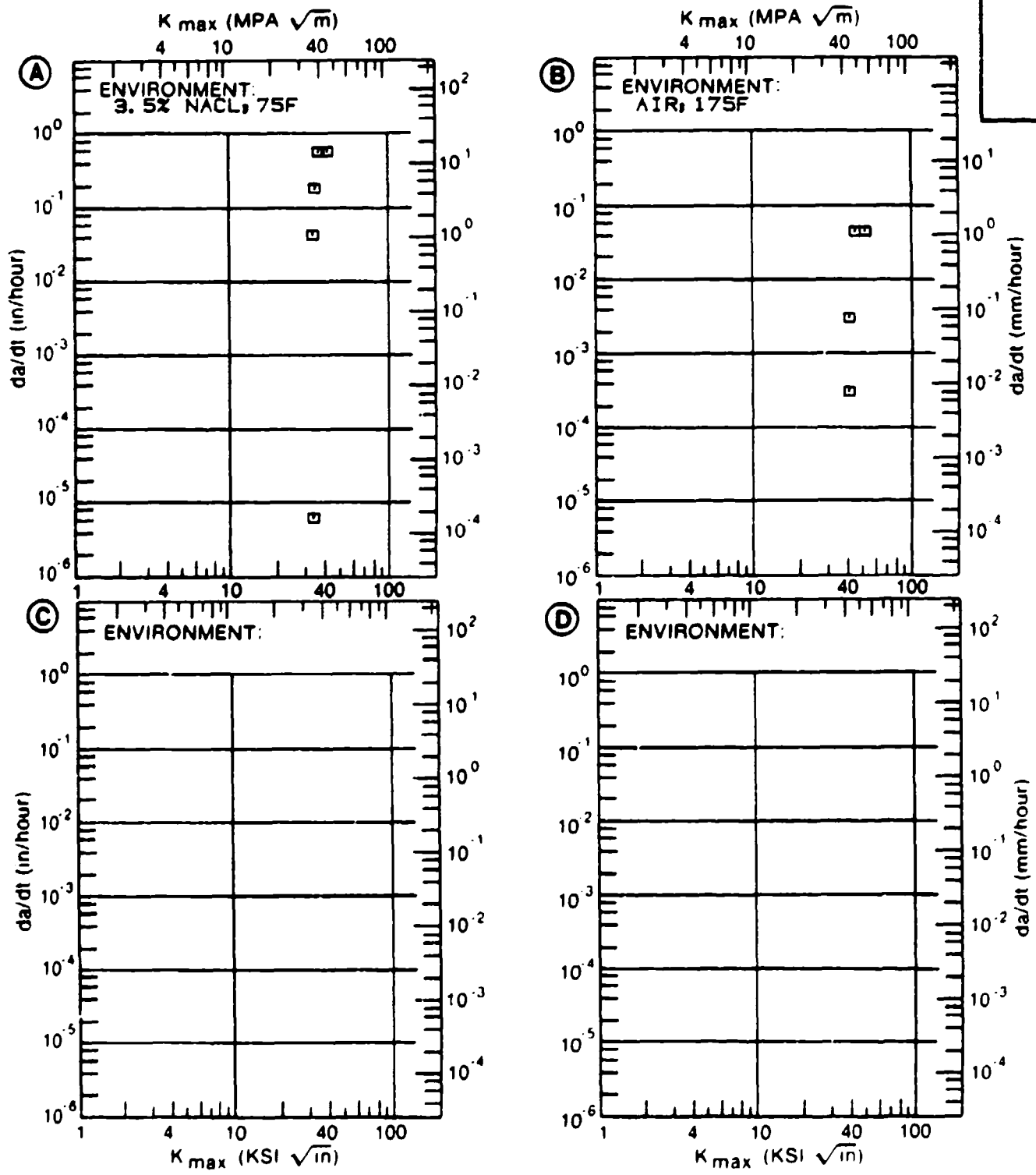


Figure 4.11.3.127

TABLE 4.11.3.128

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.128 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|---|----------|-------------------------|------|-----------|---|
| CONDITION: EB WELD, STRESS RELIEVED (WELD ZONE) | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**--6 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= | E= | | |
| | | 3.5% NACL; 75F | | AIR; 175F | |
| K MAX | A: 36.00 | 171. | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 40.00 | 724548. | | | |
| K MAX | A: 44.00 | 964781. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 48.35 | 0.00 | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: EB WELD, STRESS RELIEVED (WELD ZONE)
 FORM: 1.0" TH WELDMENT
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 YIELD STRENGTH: 132.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 CRACK LENGTH (A₀):
 K_{ISCC}: 36.00 KSI (SQRT IN)
 REFERENCES: 08144

TITAN.
 ALLOY
 TI-6AL-
 4V

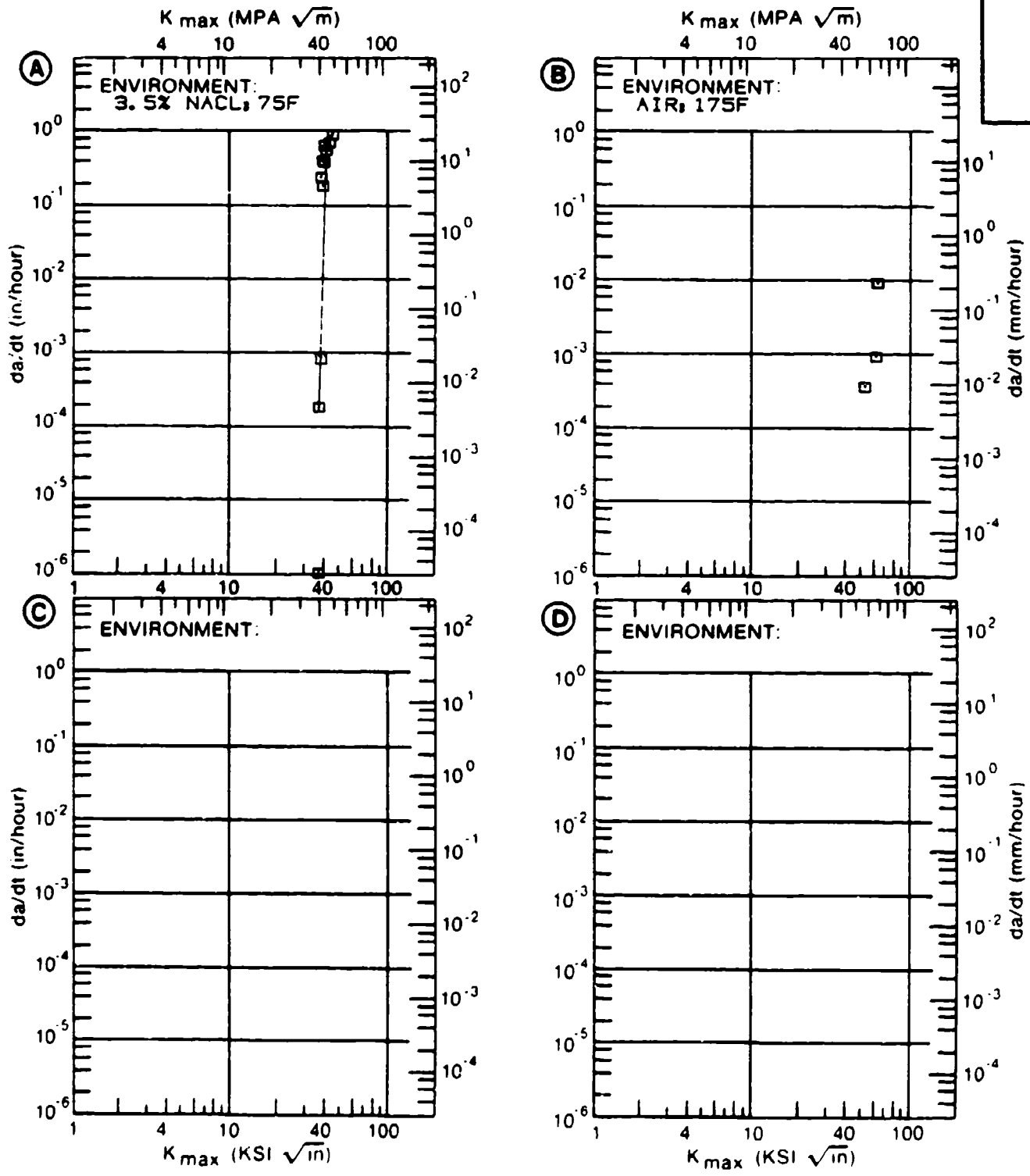


Figure 4.11.3.128

TABLE 4.11.3.129

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.129 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------|----------|------------------------------------|-------|-------------------|---|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. | | E= R. T. | |
| | | 0.6M KCL -500 MV | | 0.6M KCL -1000 MV | |
| K MAX MIN | A: 22.00 | 240. | | | |
| | B: 23.00 | | 232. | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | 542. | 266. | | |
| | 30.00 | 854. | 299. | | |
| | 35.00 | 933. | 341. | | |
| | 40.00 | 1059. | 474. | | |
| K MAX MAX | A: 45.20 | 1499. | | | |
| | B: 45.20 | | 867. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 13.23 | 13.95 | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.2" TH SHEET
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.200"
 SPECIMEN WIDTH:
 CRACK LENGTH (A₀):
 K_{ISCC}:
 REFERENCES: 81221

TITAN.
 ALLOY

TI-6AL-
 4V

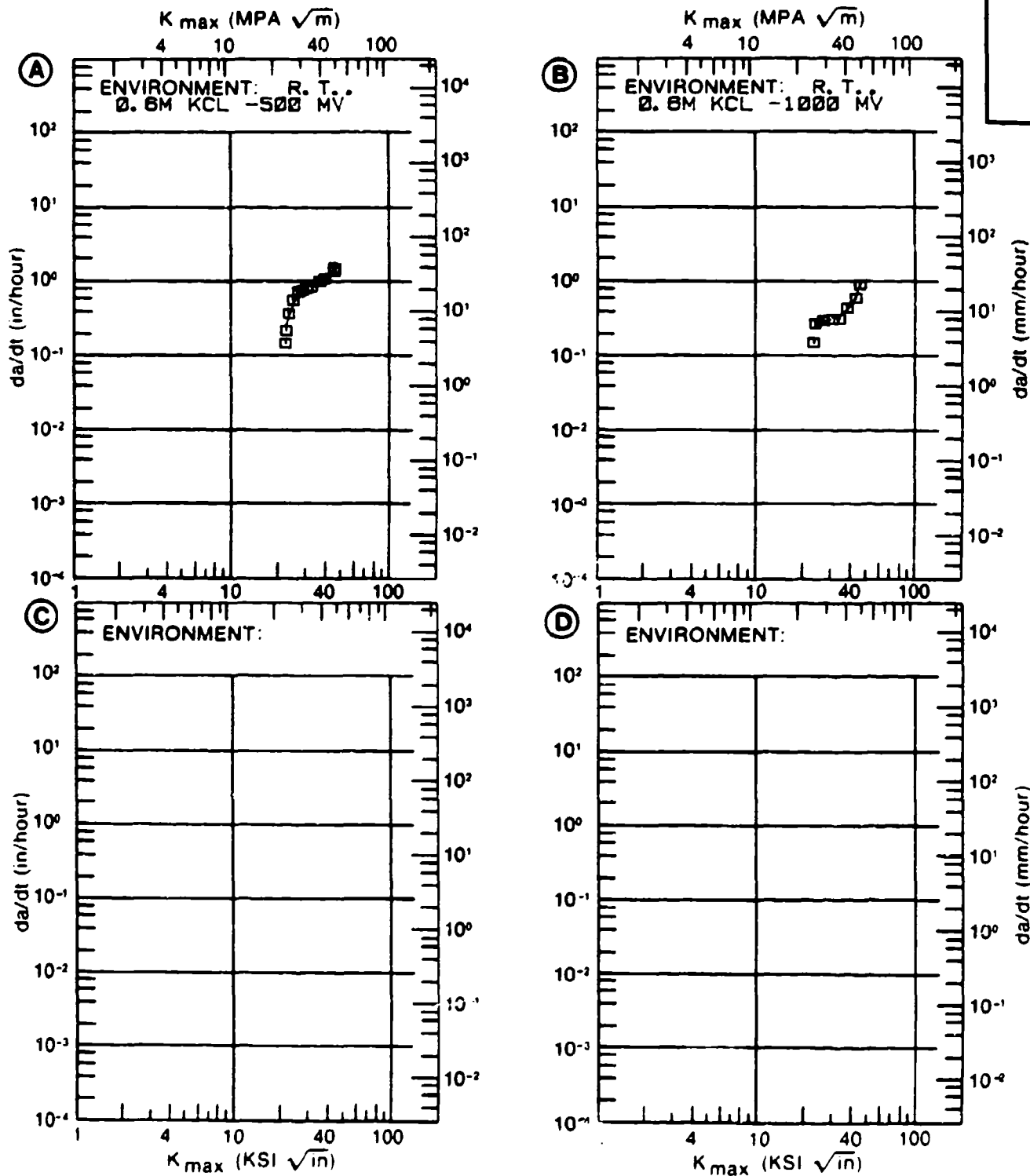


Figure 4.11.3.129

TABLE 4.11.3.130

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.130 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------|----------|----------------------------|---------------------------|------------------------|---------------------------|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 5M KI +1000 MV | E= R. T. 5M KI +500 MV | E= R. T. 5M KI 0 MV | E= R. T. 5M KI -500 MV |
| K MAX | A: | | | | |
| MIN | B: 17.50 | | 970. | | |
| | C: 18.50 | | | 1202. | |
| | D: 19.20 | | | | 1271. |
| | 20.00 | | 17493. | 6645. | 3216. |
| | 25.00 | | 26009. | 15774. | 9982. |
| | 30.00 | | 38482. | 27636. | 15327. |
| | 35.00 | | | 42504. | 21875. |
| | 40.00 | | | 56727. | 30115. |
| K MAX | A: | | | | |
| MAX | B: 34.00 | | 52976. | | |
| | C: 44.80 | | | 65998. | |
| | D: 44.70 | | | | 40011. |
| ROOT MEAN SQUARE | | 0.00 | 29.55 | 12.77 | 12.68 |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.2" TH SHEET
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.200"
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 81221

TITAN.
 ALLOY

TI-6AL-4V

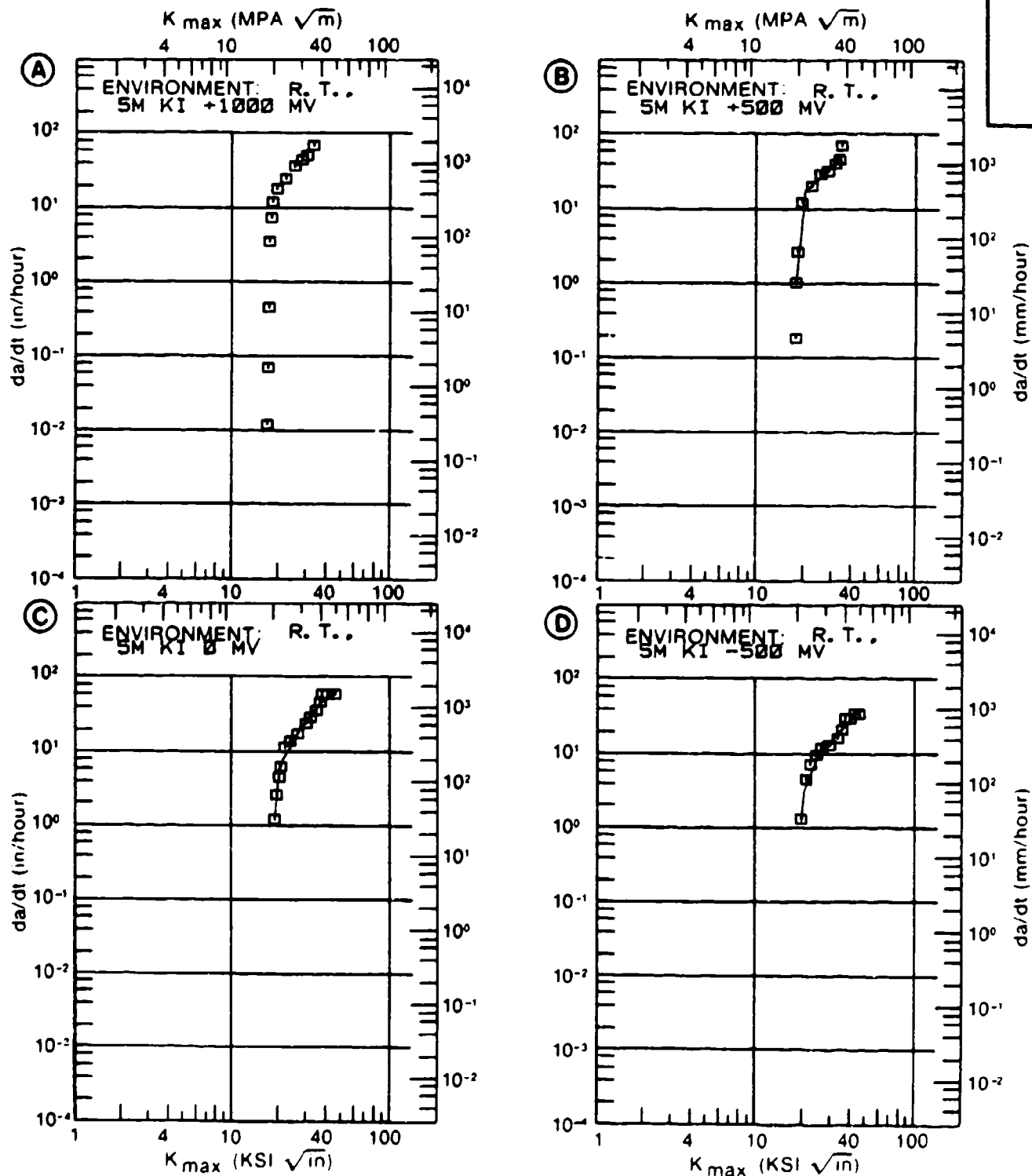


Figure 4.11.3.130

TABLE 4.11.3.131

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.131 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------|----|----------------------------|--------|----------------------------|---|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 5M KI -1000 MV | | E= R. T. 5M KI -1500 MV | |
| K MAX MIN | A: | 30.00 | 1328. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 35.00 | 2562. | | |
| | | 40.00 | 9680. | | |
| K MAX MAX | A: | 44.00 | 10010. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.47 | | 0.00 | |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.2" TH SHEET
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.200"
 SPECIMEN WIDTH:
 CRACK LENGTH (A_c):
 K_{ISCC} :
 REFERENCES: 81221

TITAN.
 ALLOY

TI-6AL-
 4V

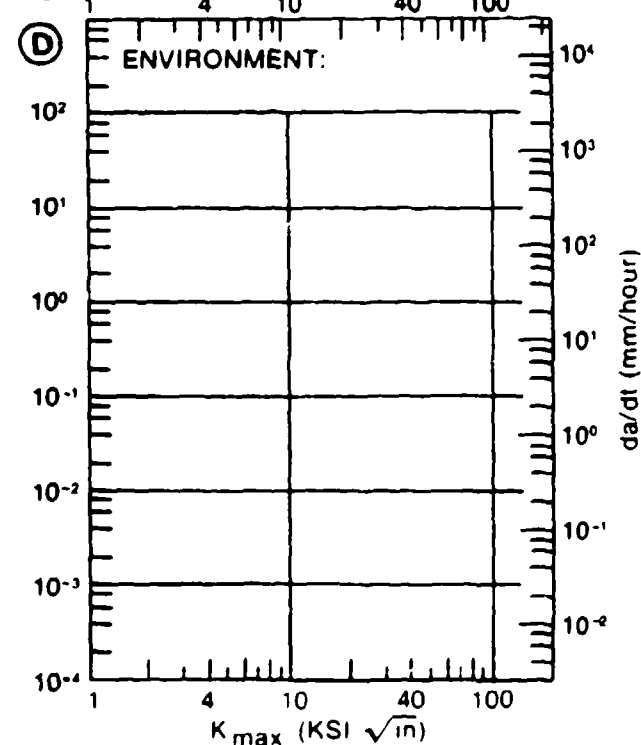
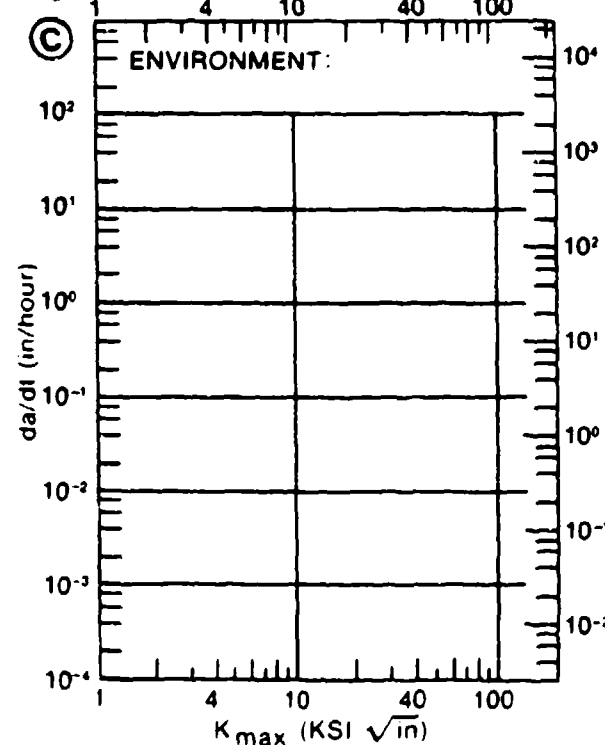
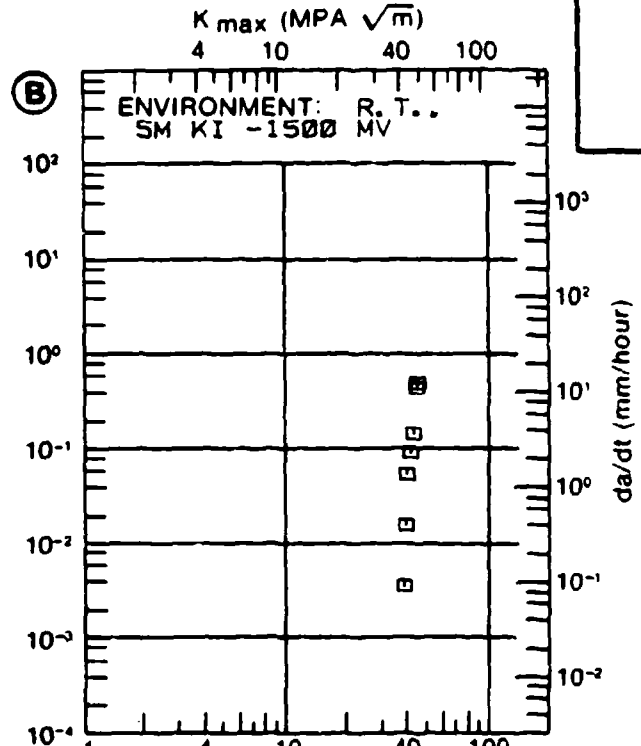
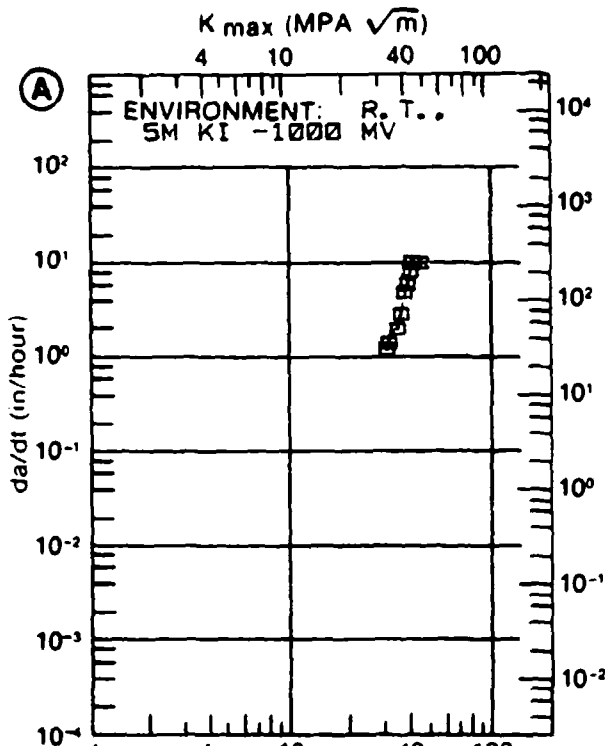


Figure 4.11.3.131

TABLE 4.11.3.132

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.132 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------|----------|------------------------------------|-------------------|-------------------|-------------------------|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 6M KF | E= R. T. 3M KF | E= R. T. 1M KF | E= R. T. DIST. WATER |
| K MAX MIN | A: 30.00 | 461. | | | |
| | B: | | | | |
| | C: 35.00 | | | 30.0 | |
| | D: 31.40 | | | | 196. |
| | 35.00 | 1075. | | | 381. |
| | 40.00 | 2121. | | 207. | 485. |
| K MAX MAX | A: 44.50 | 3590. | | | |
| | B: | | | | |
| | C: 44.20 | | | 529. | |
| | D: 45.00 | | | | 522. |
| ROOT MEAN SQUARE | | 11.57 | 0.00 | 11.33 | 2.17 |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.2" TH SHEET
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.200"
 SPECIMEN WIDTH:
 CRACK LENGTH (A₀):
 K_{ISCC}: 35.00 KSI (SQRT IN)
 REFERENCES: B1221

TITAN.
 ALLOY

TI-6AL-
 4V

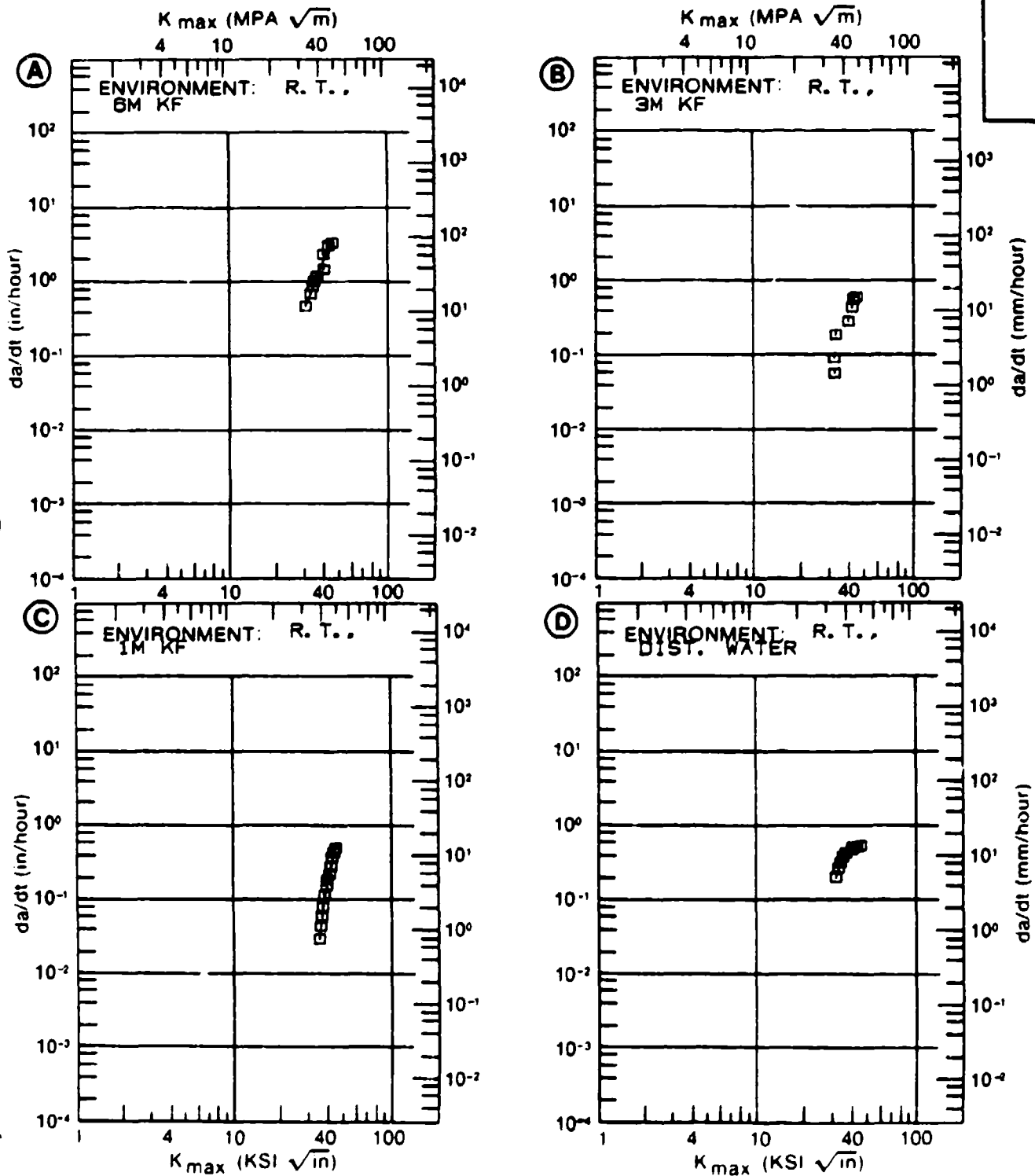


Figure 4.11.3.132

TABLE 4.11.3.133

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.133 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM CONDITION: MA | | TI-6AL-4V | | | |
|-------------------------------------|-------|------------------------------------|----------------------------------|---------------------------------|---------------------------|
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 0.6M KCL +2000 MV | E= R. T. 0.6M KCL +1000 MV | E= R. T. 0.6M KCL +500 MV | E= R. T. 0.6M KCL 0 MV |
| K MAX | A: | | 363. | | |
| MIN | B: | | | 882. | |
| | C: | | | | 576. |
| | D: | | | | |
| | 25.00 | | 1708. | 1236. | 869. |
| | 30.00 | | 2448. | 1823. | 1303. |
| | 35.00 | | 3586. | 2242. | 1789. |
| | 40.00 | | 5102. | 3027. | 2398. |
| K MAX | A: | | | | |
| MAX | B: | | 6844. | | |
| | C: | | | 5110. | |
| | D: | | | | 3230. |
| ROOT MEAN SQUARE | | 0.00 | 8.77 | 7.97 | 9.38 |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.2" TH SHEET
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.200"
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 01221

TITAN.
 ALLOY

TI-6AL-
 4V

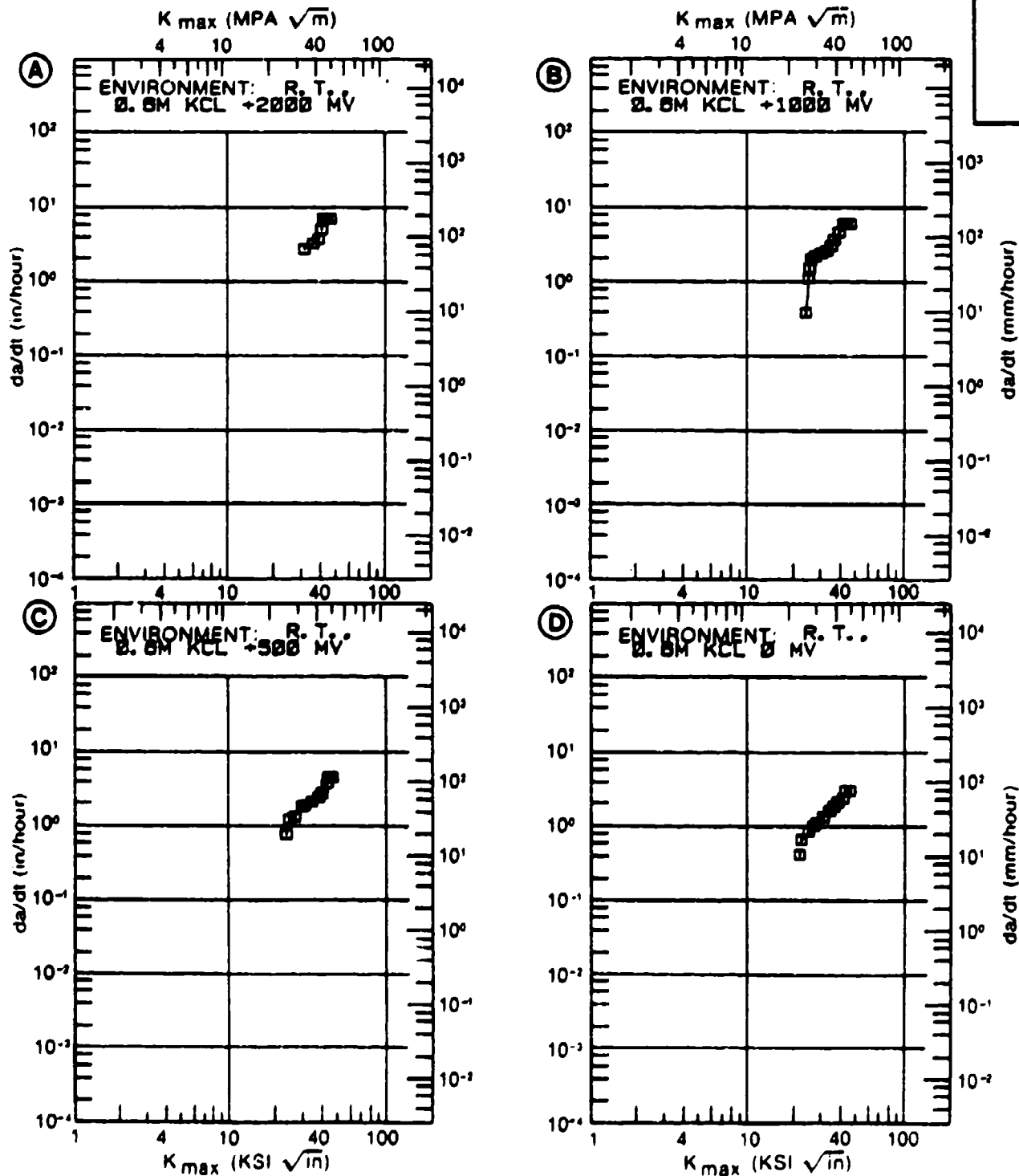


Figure 4.11.3.133

TABLE 4.11.3.134

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.134 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|-----------------------------------|----------|------------------------------------|------------------------|---|---|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E = R. T. 3.5% NaCl | E = R. T. JP-4 FUEL | | |
| K MAX MIN | A: 30.00 | .693 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 35.00 | 1879. | | | |
| | 40.00 | 2253. | | | |
| K MAX MAX | A: 45.00 | 4520. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 27.43 | 0.00 | | |

CONDITION/HT: MA
 FORM: 1.0" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 YIELD STRENGTH: 132.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 1.000"
 SPECIMEN WIDTH: 2.550"
 CRACK LENGTH (A_0):
 K_{Isc} : 30.0; 49.0 KSI
 REFERENCES: 00144

TITAN.
ALLOY

TI-6AL-
4V

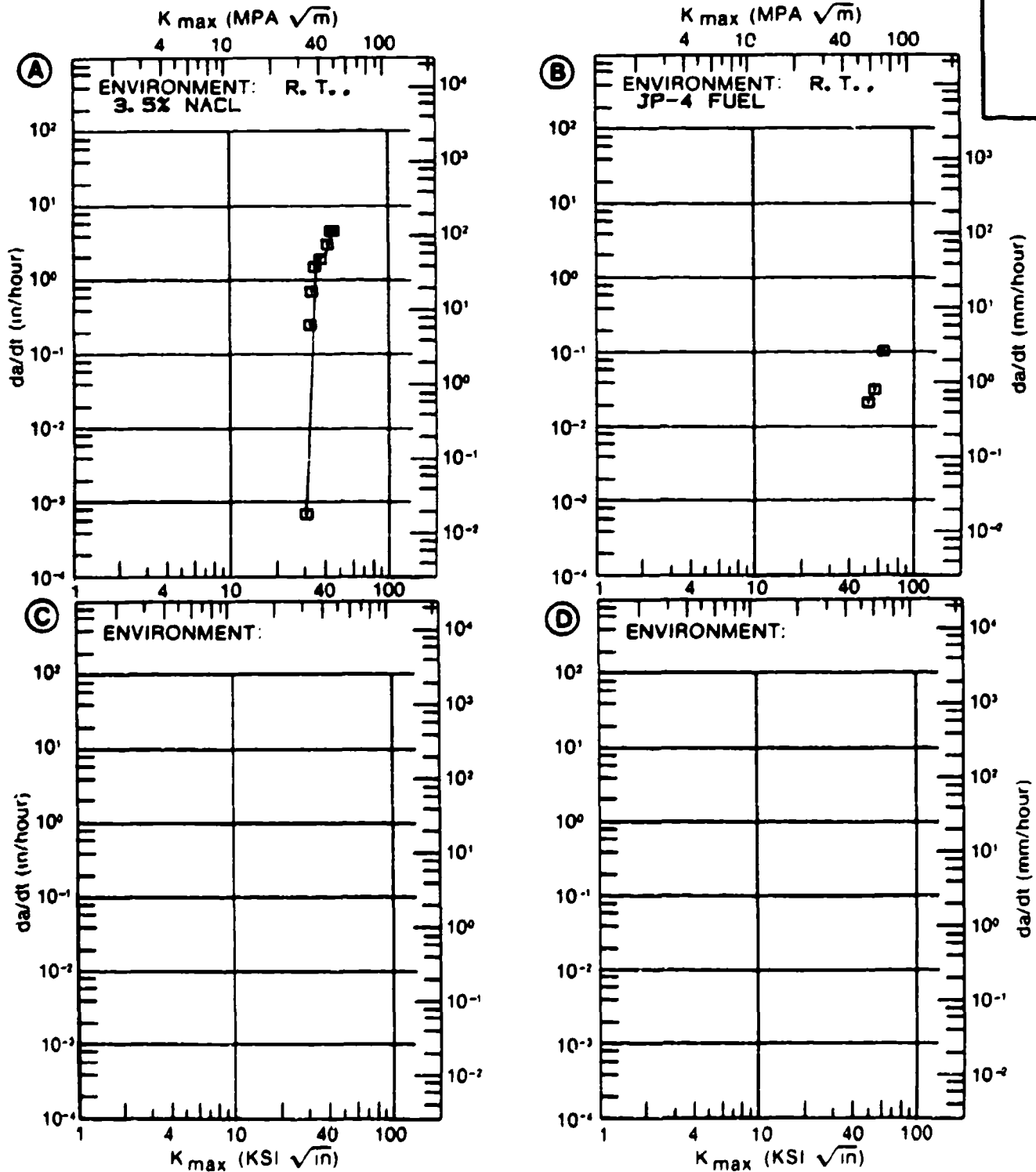


Figure 4.11.3.134

TABLE 4.11.3.135

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.11.3.135 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V | | | |
|------------------------|----|------------------------|-----------------------|---|---|
| CONDITION: 1000F 2HR | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 3. 5% NACL | E= R. T. JP-4 FUEL | | |
| K MAX MIN | A: | 35.60 | 222. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 40.00 | 3703. | | |
| K MAX MAX | A: | 47.00 | 28832. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 46.58 | 0.00 | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1000F 2HR
 FORM: 2.0" TH FORGING
 SPECIMEN TYPE: TDCB
 ORIENTATION: L-T
 YIELD STRENGTH: 145.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.500"
 CRACK LENGTH (A_0):
 K_{Isc} : 31.0; 43.0 KSI (SORT IN)
 REFERENCES: 84380

TITAN.
 ALLOY

TI-6AL-
 4V

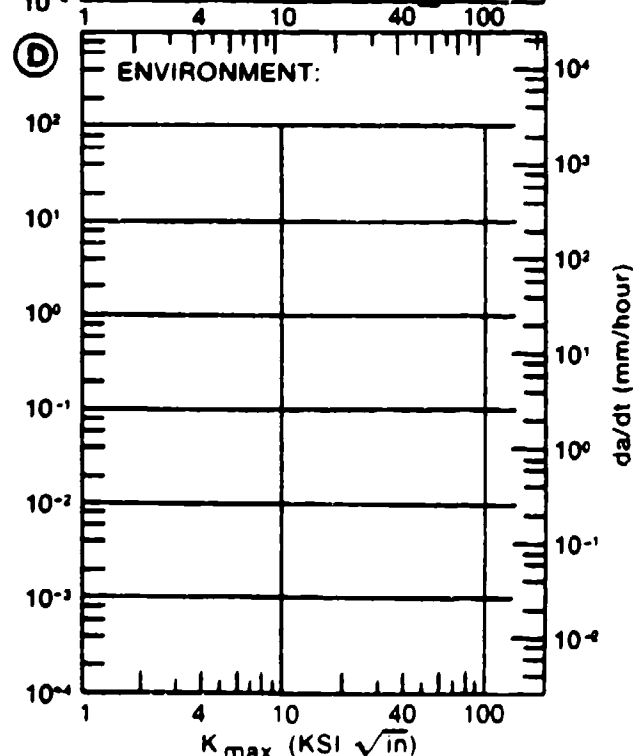
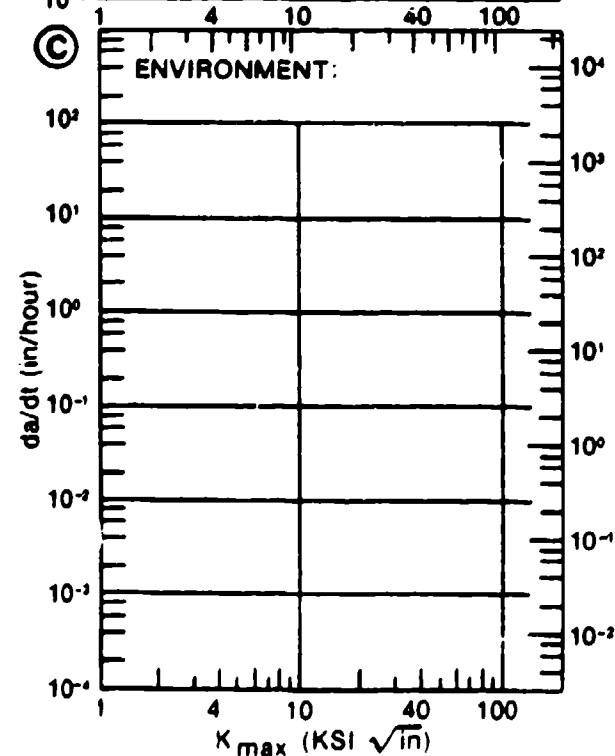
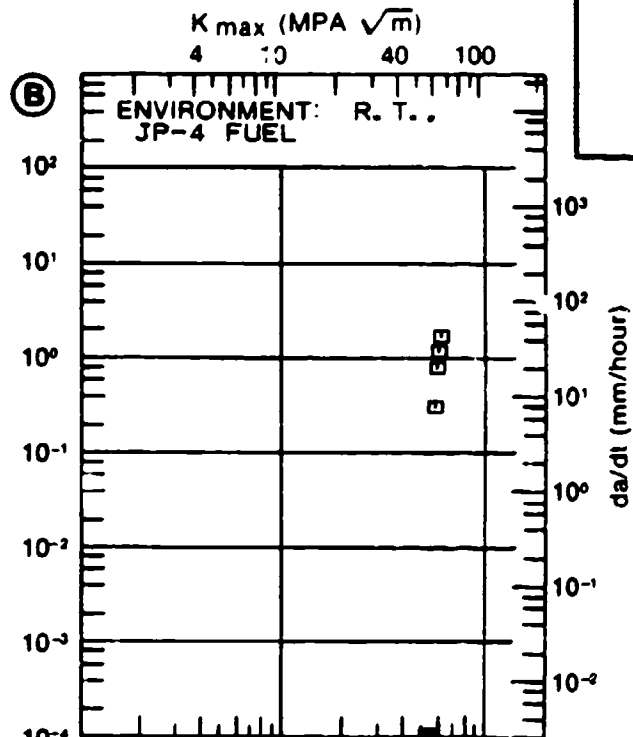
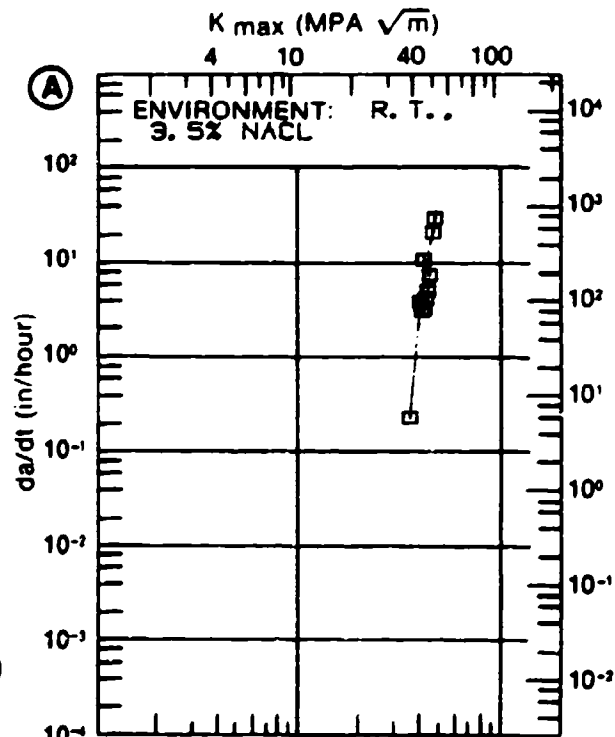


Figure 4.11.3.135

TABLE 4.11.3.136

| CONDITION | PROPR T... FORM THICK (IN) | TEST SPEC TEMP OR (F) | YIELD STR (KSI) | ENVIRONMENT | SPECIMEN | | WIDTH (IN) | DESIGN (IN) | CRACK LENGTH (IN) | K(I) | K(I) (KSI*SQRT IN) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|----------------------------|----------------------------------|-----------------------------|-----------------------|----------------|-------------|-----------|----------------|----------------|-------------------------|-------|-----------------------|---------|-------------|-----------------------|--------------------|
| | | | | | TI-TITANIUM | TI-6AL-4V | | | | | | | | | |
| | | R T | 116.0 | 3.5 PCT NAACL | | | | | | | | | | | 1967 70887 |
| | | R T | 103.0 | METHANOL | 1.100 | 0.750 | CANT | | 115.00 | | 95.00* | | | | 1968 R4328 |
| | | R T | 103.0 | N-HEXANE | 1.100 | 0.750 | CANT | | 98.00 | | 80.00* | | | | 1968 R4328 |
| | | R T | 103.0 | 3.5 PCT NAACL | 1.100 | 0.750 | CANT | | 98.00 | | 80.00* | | | | 1968 R4328 |
| | 1.25 | R T | 106.0 | JP-4 FUEL | 3.073 | 1.249 | BMOL | 1.365 | | | 66.50 | | | | >133920 1977 MA005 |
| | 1.25 | | 106.0 | | 3.073 | 1.231 | BMOL | 1.335 | | | 66.60 | | | | >133920 1977 MA005 |
| | 1.25 | | 108.0 | | 3.078 | 1.231 | BMOL | 1.384 | | | 69.00 | | | | >133920 1977 MA005 |
| | 1.25 | | 108.0 | | 3.078 | 1.252 | BMOL | 1.363 | | | 68.00 | | | | >133920 1977 MA005 |
| | 1.25 | R T | 106.0 | SIM. SEA WATER | 3.077 | 1.249 | BMOL | 1.619 | | | 69.60 | | | | >133920 1977 MA005 |
| | 1.25 | | 106.0 | | 3.077 | 1.230 | BMOL | 1.369 | | | 69.30 | | | | >133920 1977 MA005 |
| | 1.25 | | 108.0 | | 3.077 | 1.231 | BMOL | 1.364 | | | 67.70 | | | | >133920 1977 MA005 |
| | 1.25 | | 108.0 | | 3.073 | 1.233 | BMOL | 1.335 | | | 68.50 | | | | >133920 1977 MA005 |
| ALPHA-BETA FORCED | F | 2.25 | R T | T-L | 144 | 9 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | 36.50 | 27.00 | | | 1973 R668R |
| ALPHA-BETA FORCED | F | 2.25 | R T | T-L | 144 | 9 | SEACOAST ATM | 2.000 | 1.000 | CT | 36.50 | 18.00 | | | 1973 R668R |
| ALPHA-BETA FORCED | F | 2.25 | R T | T-L | 144 | 9 | 3.5 PCT NAACL | 2.300 | 1.000 | CT | 36.50 | 27.00 | | | 1973 R668R |
| AS RECEIVED PROBABLY PA | P | | R T | T-8 | 125 | 0 | 3.5 PCT NAACL | | | CANT* | 120.00 | 103.00* | | | 1968 74395 |
| BETA FORCED | F | 2.25 | R T | T-L | 134 | 9 | INDUSTRIAL ATM | 2.000 | 1.000 | CT | 44.20 | 42.00 | | | 1973 R668R |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KI)SCC/(YS)SQUARED

TABLE 4.11.3.136 (Con't)

| CONDITION | --PRODUCT-- | | TEST SPEC YIELD | | TITANIUM | | TI-6AL-4V | | K(ISSC) | | STAN DEV | TEST TIME (MIN) | DATE REPEF | |
|---|-------------|---------------|-----------------|-----------------|---------------|----------------|----------------|----------------|---------|-------|-------------|-----------------------|------------|------------|
| | FORM | THICK (IN) | TEMP (F) | OR STR (KSI) | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | K(I) | K(II) | | | | |
| BETA FORGED | F | 2.25 | R.T. | T-L | 134.9 | SEACOAST | ATM | 2.000 | 1.000 | CT | 44.20 | 42.00 | 1973 B6685 | |
| BETA FORGED | F | 2.25 | R.T. | T-L | 134.9 | 3.5 PCT | NACL | 2.000 | 1.000 | CT | 44.20 | 34.00 | 1973 B6680 | |
| FINISH RINLED 1420F | P | 3.00 | R.T. | T-S | 114.0 | 0.5 PCT | NACL | 2.000 | 0.750 | NB | 1.166 | 116.00 | 90.10* | 1972 B4036 |
| | | | | | | | | 2.000 | 0.750 | NB | 1.215 | 116.00 | 95.00* | 1972 B4036 |
| | | | | | | | | 2.000 | 0.750 | NB | 0.303 | 116.00 | 94.00* | 1972 B4036 |
| | | | | | | | | 2.000 | 0.750 | NB | 1.153 | 116.00 | 94.60* | 1972 B4036 |
| | | | | | | | | 3.000 | 1.500 | NB | 1.105 | 79.60 | 79.60 | 1972 B4036 |
| | | | | | | | | 3.000 | 1.500 | NB | 1.051 | 74.30 | 74.30 | 1972 B4036 |
| | | | | | | | | 3.000 | 1.500 | NB | 1.163 | 87.20 | 87.20 | 1972 B4036 |
| | | | | | | | | 3.000 | 1.500 | NB | 1.043 | 78.60 | 78.60 | 1972 B4036 |
| | | | | | | | | 3.000 | 2.000 | NB | 0.920 | 61.90 | 61.90 | 1972 B4036 |
| | | | | | | | | 3.000 | 2.000 | NB | 1.005 | 78.00 | 78.00 | 1972 B4036 |
| | | | | | | | | | | | | | 76.2/ 7.8 | |
| GTA - WELD POSTWELD 1100F 2HR (HEAT AFFECTED ZONE) | P | 1.25 | R.T. | L-T | | FIELD CLEANING | SOLVENT | 5.500 | 0.500 | DCB | | > 48.00 | 1974 B9004 | |
| GTA - WELD POSTWELD 1100F 2HR (HEAT AFFECTED ZONE) | P | 1.25 | R.T. | L-T | | S.T.M. | | 5.500 | 0.500 | DCB | | > 69.00* | 1974 B9004 | |
| | | | | | | | | 5.500 | 0.750 | DCB | | 76.00* | 1974 B9004 | |
| | | | | | | | | 5.500 | 1.000 | DCB | | 58.00 | 1974 B9004 | |
| GTA - WELD POSTWELD 1100F 2HR (HEAT AFFECTED ZONE) | P | 1.25 | R.T. | L-T | | SHOP CLEANING | SOLVENT | 5.500 | 0.500 | DCB | | > 64.00* | 1974 B9004 | |
| GTA WELD POSTWELD 1200F 1HR (HEAT AFFECTED ZONE) | P | 1.25 | R.T. | L-T | | S.T.M. | | 5.500 | 0.125 | DCB | | > 67.00* | 1974 B9004 | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISSC/TYS)SQUARED

TABLE 4.1.1.3.136 (Con't)

| CONDITION | - PRODUCT - FORM THICK (IN) | TEST SPEC TEMP (F) | OR STR (KSI) | YIELD | TITANIUM | TI-6AL-4V | K(ISSC) | SPECIMEN | | CRACK LENGTH K(B) | K(ISSC) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|--|-----------------------------------|--------------------------|-----------------|-------|----------------|-----------|---------|---------------|---------------|----------------------|---------|-------|-------------|-----------------------|------------|
| | | | | | | | | WIDTH (IN) | THICK (IN) | | | | | | |
| GTA WELD POSTWELD 1400F 1HR (HEAT AFFECTED ZONE) | P 1.25 | R.T. | L-T | ---- | S.T.W. | 3.500 | 0.125 | DCB | ----- | > | 62.00* | ----- | ----- | 1974 | 89004 |
| GTA WELD POSTWELD 1200F 1HR (HEAT AFFECTED ZONE) | P 1.25 | R.T. | L-T | ---- | S.T.W. | 3.500 | 0.250 | DCB | ----- | > | 66.00* | ----- | ----- | 1974 | 89004 |
| GTA WELD POSTWELD 1400F 1HR (HEAT AFFECTED ZONE) | P 1.25 | R.T. | L-T | ---- | S.T.W. | 3.500 | 0.250 | DCB | ----- | > | 70.00* | ----- | ----- | 1974 | 89004 |
| GTA WELD POSTWELD 1100F 2HR (WELD ZONE) | P 1.25 | R.T. | L-T | ---- | S.T.W. | 3.500 | 0.500 | DCB | ----- | ----- | 93.00* | ----- | ----- | 1974 | 89004 |
| MILL ANNEALED S | 0.13 | R.T. | --- | ---- | A-50 | 1.300 | 0.125 | WOL | ----- | ----- | 68.00* | ----- | ----- | 1974 | 88700 |
| MILL ANNEALED S | 0.13 | R.T. | --- | ---- | MCB | 1.300 | 0.125 | WOL | ----- | ----- | 38.60* | ----- | ----- | 1974 | 88700 |
| MILL ANNEALED S | 0.13 | R.T. | --- | ---- | MCB/1PCT COR | 1.300 | 0.125 | WOL | ----- | ----- | 40.80* | ----- | ----- | 1974 | 88700 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | DIST WATER | ----- | 0.200 | DCB | ----- | ----- | 33.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 1 M KF | ----- | 0.200 | DCB | ----- | ----- | 35.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 3 M KF | ----- | 0.200 | DCB | ----- | ----- | 37.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 6 M KF | ----- | 0.200 | DCB | ----- | ----- | 31.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 6M KF, 0 MV | ----- | 0.200 | DCB | ----- | ----- | 19.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 6M KF, +1000RV | ----- | 0.200 | DCB | ----- | ----- | 16.00* | ----- | ----- | 1971 | 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | ---- | 6M KF, +500RV | ----- | 0.200 | DCB | ----- | ----- | 17.00* | ----- | ----- | 1971 | 81221 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KI/SCC/TYB)SQUARED

TABLE 4.11.3.136 (Con't)

| CONDITION | ---PRODUCT--- FORM THICK (IN) | TEST TEMP OR STR (F) | SPECIMEN THICK (IN) | YIELD STR (KSI) | ENVIRONMENT | TITANIUM | | WIDTH (IN) | THICK DESIGN (IN) | CRACK LENGTH (IN) | K (IBCC) | K (ISCC) | K (ISCC) (KSI*SQRT IN) | MEAN DEV | STAN DEV | TEST TIME (MIN) | DATE REFER |
|---------------------|-------------------------------------|-------------------------|------------------------|--------------------|---------------|--------------|----------|---------------|----------------------|----------------------|----------|----------|---------------------------|-------------|-------------|-----------------------|-------------------|
| | | | | | | TI-6AL-4V | K (IBCC) | | | | | | | | | | |
| | | | | | | W | A | | | | | | | | | | |
| MILL ANNEALED S | 0.20 | R.T. | T-L | --- | 6M KF.-1000RV | --- | 0.200 | DCB | --- | --- | --- | --- | 31.00* | --- | --- | --- | 1971 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | --- | 6M KF.-1500RV | --- | 0.200 | DCB | --- | --- | --- | --- | 38.00* | --- | --- | --- | 1971 81221 |
| MILL ANNEALED S | 0.20 | R.T. | T-L | --- | 6M KF.-300RV | --- | 0.200 | DCB | --- | --- | --- | --- | 20.00* | --- | --- | --- | 1971 81221 |
| MILL ANNEALED P | 0.50 | R.T. | L-S | --- | 3.5 PCT NaCl | --- | --- | NB | --- | --- | --- | --- | 61.00 | --- | --- | --- | 1969 75386 |
| MILL ANNEALED P | 1.00 | R.T. | T-S | 120.0 | 3.5 PCT NaCl | 1.000 | 0.750 | CANT* | --- | --- | --- | --- | 88.00 | --- | --- | --- | 1967 70931 |
| MILUTEMAN CASING | P | --- | R.T. | T-S | 165.0 | 3.5 PCT NaCl | 0.750 | 0.100 | CANT | --- | --- | --- | 64.00 | --- | --- | --- | 1967 70931 |
| RA | P | 1.50 | R.T. | L-T | 117.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | --- | --- | 74.00 | --- | --- | --- | 60300 1976 R1006 |
| | | 1.50 | | | 117.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 74.00 | > | --- | --- | 60300 1976 R1006 |
| | | 1.50 | | | 117.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 74.00 | --- | --- | --- | 60300 1976 R1006 |
| | | 1.50 | | | 121.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 76.00 | --- | --- | --- | 54360 1976 R1006 |
| | | 1.50 | | | 121.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 76.00 | > | --- | --- | 54360 1976 R1006 |
| | | 1.50 | | | 121.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 76.00 | > | --- | --- | 54360 1976 R1006 |
| | | 2.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 70140 1976 R1006 |
| | | 2.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 70140 1976 R1006 |
| | | 2.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 54360 1976 R1006 |
| | | 2.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 54360 1976 R1006 |
| | | | | | | | | | | | | | | 59.3/ | 2.9 | | |
| RA | P | 1.50 | R.T. | T-L | 122.0 | F.C.S. | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 119100 1976 R1006 |
| RA | P | 1.50 | R.T. | T-L | 122.0 | B.C.S. | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 59100 1976 R1006 |
| | | 1.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 112200 1976 R1006 |
| RA | P | 1.50 | R.T. | T-L | 122.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 60300 1976 R1006 |
| | | 1.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 54360 1976 R1006 |
| | | 1.50 | | | 122.0 | | 5.500 | 1.000 | DCB | --- | --- | --- | 77.00 | --- | --- | --- | 60300 1976 R1006 |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KISCC/TYS) SQUARED

TABLE 4.11.3.136 (Con't)

| CONDITION | --PRODUCT-- FORM THICK (IN) | TEST SPEC OR STR (KSI) | YIELD | ENVIRONMENT | TITANIUM | | M (IN) | W (IN) | SPECIMEN | | DESIGN LENGTH (IN) | CRACK (K(ISC)) | K(ISC) | MEAN | STAN DEV | TEST TIME (MIN) | DATE REFER |
|--|--------------------------------|------------------------|-------|-------------|-----------|---------------------------|--------|--------|------------|-------------|--------------------|----------------|--------|------|----------|-----------------|------------|
| | | | | | TI-6AL-4V | M (K(ISC)) | | | THICK (IN) | DESIGN (IN) | | | | | | | |
| PA | P | 1.50 | R.T. | F-L | 122.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | 77.00 | 62.00 | 60300 | 1976 | R1006 | | |
| | | 2.00 | | | 126.0 | | 5.500 | 1.000 | DCB | --- | 80.00 | 61.00 | 61980 | 1976 | R1006 | | |
| | | 2.00 | | | 126.0 | | 5.500 | 1.000 | DCB | --- | 80.00 | 59.00 | 61980 | 1976 | R1006 | | |
| PA | F | 4.00 | R.T. | T-L | 119.0 | S.T.M. | 5.500 | 1.000 | DCB | --- | 79.00 | 59.00 | 60360 | 1976 | R1006 | | |
| | | 4.00 | | | 119.0 | | 5.500 | 1.000 | DCB | --- | 79.00 | 51.00 | 60360 | 1976 | R1006 | | |
| RA | F | --- | R.T. | S-L | --- | S.T.M. | 5.500 | 1.000 | DCB | --- | 78.00 | > 57.00 | 64920 | 1976 | R1006 | | |
| | | --- | | | --- | | 5.500 | 1.000 | DCB | --- | 79.00 | 56.00 | 60180 | 1976 | R1006 | | |
| | | --- | | | --- | | 5.500 | 1.000 | DCB | --- | 79.00 | 56.00 | 60660 | 1976 | R1006 | | |
| | | --- | | | --- | | 5.500 | 1.000 | DCB | --- | 78.00 | > 71.00 | 60660 | 1976 | R1006 | | |
| | | 4.00 | | | 129.0 | | 5.500 | 1.000 | DCB | --- | 79.00 | 59.00 | 64920 | 1976 | R1006 | | |
| | | 4.00 | | | 129.0 | | 5.500 | 1.000 | DCB | --- | 79.00 | 57.00 | 61680 | 1976 | R1006 | | |
| SOL TREATED 1050F 4HR. INCLUDED 1050F 4HR | F | --- | 85 | --- | 133.0 | N204 315PSIG | 1.500 | 0.062 | PTSC | 0.026 | 47.00 | 32.00* | --- | 1969 | 78535 | | |
| | | --- | | | 139.0 | | 1.500 | 0.062 | PTSC | 0.026 | 47.00 | 31.00* | --- | 1969 | 78535 | | |
| SOL TREATED 1050F 4+4 HR | F | --- | 85 | --- | 160.0 | N204 315PSIG | 1.000 | 0.092 | PTSC | 0.018 | 49.00 | 28.00* | --- | 1969 | 78535 | | |
| | | --- | | | 161.0 | | 1.000 | 0.092 | PTSC | 0.018 | 49.00 | 30.00* | --- | 1969 | 78535 | | |
| 1300F 2HR AC | E | 0.50 | R.T. | L-S | 121.2 | 3.5 PCT NAACL | 1.500 | 0.480 | NB | --- | 94.70 | 65.00* | --- | 1972 | 84282 | | |
| 1300F 2HR AC | E | 0.50 | R.T. | L-T | 128.9 | 3.5 PCT NAACL | 1.500 | 0.480 | NB | --- | 83.30 | 73.00* | --- | 1972 | 84282 | | |
| 1700F 4HR FC TO 1400F AC. DIFFUSION BOND THERMAL CYCLE | F | 1.50 | R.T. | L-T | --- | S.T.M. | 5.500 | 1.000 | DCB | --- | --- | 66.00 | --- | 1974 | 89004 | | |
| 1700F 4HR FC TO 1400F AC. DIFFUSION BOND THERMAL CYCLE | F | 1.50 | R.T. | T-L | --- | FIELD CLEANING IN SILVENT | 5.500 | 1.000 | DCB | --- | 94.00 | 70.00 | --- | 1974 | 89004 | | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.3(K(ISC)/TYS)SQUARED

TABLE 4.11.3.136 (Con't)

| CONDITION | | -- PRODUCT -- FORM THICK (IN) | | TEST SPEC TEMP OR (F) | | YIELD STR (KSI) | | ENVIRONMENT | | TITANIUM TI-6AL-4V K11SCC) | | SPECIMEN WIDTH (IN) W | | THICK DESIGN (IN) B | | CRACK LENGTH K(G) (IN) A | | K11SCC) MEAN (IN) | | STAN DEV | | TEST TIME (MIN) | | DATE REFER | | |
|--|--|----------------------------------|------|-----------------------|-----|---------------------------|--|-------------------------|--|-------------------------------|-------|--------------------------|-------|---------------------|------|--------------------------|--------|-------------------|-----|----------|-----|-----------------|-----|------------|-----|-----------------|
| 1700F 4HR FC TO 1400F AC, DIFFUSION BOND THERMAL CYCLE | | P | 1.50 | R.T. | T-L | S.T.W. | | S.M.P. CLEANING SOLVENT | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 92.00 | 60.00 | 35.2/ | 7.0 | --- | --- | --- | --- | --- | --- | 1974 07004 |
| | | | 1.00 | | | | | | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 92.00 | 44.00 | | | --- | --- | --- | --- | --- | --- | 1974 07004 |
| | | | 2.00 | | | | | | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 94.00 | 61.00 | | | --- | --- | --- | --- | --- | --- | 1974 07004 |
| | | | 2.00 | | | | | | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 92.00 | 53.00 | | | --- | --- | --- | --- | --- | --- | 1974 07004 |
| | | | 2.00 | | | | | | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 92.00 | 58.00 | | | --- | --- | --- | --- | --- | --- | 1974 09004 |
| 1700F 4HR FC TO 1400F AC, DIFFUSION BOND THERMAL CYCLE | | P | 1.50 | R.T. | T-L | S.M.P. CLEANING SOLVENT | | S.M.P. CLEANING SOLVENT | | 5.500 | 1.000 | DCB | 5.500 | 1.000 | DCB | 94.00 | 69.00 | --- | --- | --- | --- | --- | --- | --- | --- | 1974 09004 |
| 1725F 1HR WQ 1250F 4HR AC (STA) | | E | 0.50 | R.T. | L-S | 139.4 3.5 PCT NAACL 140.3 | | | | 1.500 | 0.480 | NB | 1.500 | 0.480 | NB | 77.80 | 60.00 | --- | --- | --- | --- | --- | --- | --- | --- | 1972 04202 |
| | | | 0.50 | | | | | | | 1.500 | 0.480 | NB | 1.500 | 0.480 | NB | 74.90 | 70.00* | --- | --- | --- | --- | --- | --- | --- | --- | 1972 04202 |
| 1750F 1HR WQ 1000F 1HR AC (STA) | | E | 0.50 | R.T. | L-S | 145.7 3.5 PCT NAACL 146.9 | | | | 1.500 | 0.480 | NB | 1.500 | 0.480 | NB | 67.20 | 51.00 | --- | --- | --- | --- | --- | --- | --- | --- | 1972 04202 |
| | | | 0.50 | | | | | | | 1.500 | 0.480 | NB | 1.500 | 0.480 | NB | 65.80 | 46.00 | --- | --- | --- | --- | --- | --- | --- | --- | 1972 04202 |
| 1750F WQ 1000F 8HR 1000F (ALPHA+BETA) | | F | 0.50 | R.T. | --- | 160.0 DIST WATER +50 | | | | 1.000 | 0.030 | PTSC | 1.000 | 0.030 | PTSC | 43.90 | 40.00* | --- | --- | --- | --- | --- | --- | --- | --- | 1080 1968 77290 |
| 1750F WQ 1000F 8HR 1000F (ALPHA+BETA) | | F | 0.50 | R.T. | --- | 160.0 METHANOL | | | | 1.000 | 0.030 | PTSC | 1.000 | 0.030 | PTSC | 43.90 | 26.00* | --- | --- | --- | --- | --- | --- | --- | --- | 180 1968 77290 |
| | | | 0.50 | | | 160.0 | | | | 1.000 | 0.060 | PTSC | 1.000 | 0.060 | PTSC | 45.90 | 26.00* | --- | --- | --- | --- | --- | --- | --- | --- | 180 1968 77290 |
| 1750F WQ 1000F 8HR 1000F (ALPHA+BETA) | | F | 0.50 | R.T. | --- | 160.0 PPM NA2CR2O7 | | | | 1.000 | 0.060 | PTSC | 1.000 | 0.060 | PTSC | 43.90 | 43.00* | --- | --- | --- | --- | --- | --- | --- | --- | 1080 1968 77290 |
| 1750F 1 5HR WQ 1000F 8HR 950F 8HR | | F | --- | R.T. | --- | 160.9 AERDZINE 90 | | | | 0.800 | 0.095 | PTSC | 0.800 | 0.095 | PTSC | 52.20 | 37.00* | --- | --- | --- | --- | --- | --- | --- | --- | 1969 75528 |
| | | | --- | | | 161.4 | | | | 0.800 | 0.095 | PTSC | 0.800 | 0.095 | PTSC | 51.90 | 38.00* | --- | --- | --- | --- | --- | --- | --- | --- | 1969 75528 |

*NOTE: DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (K11SCC/TYS) SQUARED

TABLE 4.11.3.136 (Con't)

| CONDITION | TITANIUM | | TEST SPEC OR STR (KSI) | YIELD | ENVIRONMENT | TI-6AL-4V | | K (ISCC) | CRACK LENGTH (IN) | K (ISCC) | MEAN | DEV | TEST TIME (MIN) | DATE REFER | | |
|--|----------|-------|------------------------|-------|--|------------|------------|----------|-------------------|----------|------|-----|-----------------|------------|--------|----------|
| | SPECIMEN | | | | | WIDTH (IN) | THICK (IN) | | | | | | | | DESIGN | K (ISCC) |
| | A | B | | | | | | | | | | | | | | |
| 1750F 1 SHR WQ F 1050F-1100F BRL, 950F BHR | 0.800 | 0.095 | PTSC | 161.4 | FREON TF | 0.800 | 0.095 | PTSC | 51.50 | 42.00* | | | 1969 75528 | | | |
| | 0.800 | 0.095 | PTSC | 160.9 | | | | | 52.20 | 39.00* | | | 1969 75528 | | | |
| 1750F 1 SHR WQ F 1050F-1100F BRL, 950F BHR | 0.800 | 0.095 | PTSC | 160.9 | MS04 | 0.800 | 0.095 | PTSC | 52.20 | 40.00* | | | 1969 75528 | | | |
| | 0.800 | 0.095 | PTSC | 161.4 | | | | | 51.50 | 41.00* | | | 1969 75528 | | | |
| 1750F 1000F 2HR AC | 2.30 | R.T. | L-T | 144.9 | JP-4 FUEL | 5.000 | 1.250 | TDCB | 50.90 | 43.30 | | | 1971 84360 | | | |
| 1750F 1000F 2HR AC | 2.30 | R.T. | L-T | 144.9 | 3.5 PCT NAACL | 5.000 | 1.250 | TDCB | 50.90 | 31.00 | | | 1971 84360 | | | |
| 1790F 1 SHR WQ S 1160F BHR + 1023F BHR AC | 1.300 | R.T. | | | MARTIN MARIETTA REFINED GRADE HYDRAZINE | 1.300 | 0.125 | WOL | | 46.20* | | | 1974 88700 | | | |
| 1790F 1 SHR WQ S 1160F BHR + 1023F BHR AC | 1.300 | R.T. | | | PROPELLANT GRADE HYDRAZINE | 1.300 | 0.125 | WOL | | 64.30* | | | 1974 88700 | | | |

*NOTE-DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KISCC/TYS)SQUARED

TABLE 4.12.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY Ti-6Al-4V(ELI) AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|-------------------------|---|-----------------------|
| CONDITION/HT | I-I | 8-H |
| RECRYSTALLIZE ANNEAL | 76.1 ± 4.0 (3) | 76.8 ± 0.7 (3) |
| CONDITION/HT | I-I | 8-H |
| ANNEALED | 83.5 ± 1.3 (3) | 84.3 ± 0.4 (3) |

TABLE 4.12.1.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI 6AL-4V(ELI)

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT LAB AIR AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN./CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|--|
| ANNEALED | FORSIMS | 0 10 | 1.00-10.00 | 2.5 5 10 20 50 100 | 12.9 206 |
| RA | PLATE | 0 10 | | | 10.8 |

TABLE 4.12.1.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 TITANIUM T1-6AL-4V (ELI)

TEST CONDITIONS

SPECIMEN ORIENTATION: T-L

ENVIRONMENT: DRY AIR AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | | |
|--------------|--------------|--------------|-----------|-------------------------------|---|---|----|------|------|-----|-----|
| | | | | | 2 | 5 | 10 | 20 | 50 | 100 | |
| BA | PLATE | 0.00 | 15.00 | | | | | 4.02 | | | |
| BA | PLATE | 0.10 | 1.00 | | | | | | | | 128 |
| BA | PLATE | 0.50 | 0.10-1.00 | | | | | | 12.8 | | |
| BA | PLATE | 0.80 | 1.00 | | | | | 1.12 | | | |

TABLE 4.12.1.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V(E11)

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT LAB AIR AT R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|---|
| ANNEALED | FORGING | 0 10 | 1 00-50 00 | 2 5 5 10 20 50 100 | 11.9 171 |
| RA | PLATE | 0 10 | 1 00-10 00 | | 7.75 240 |

TABLE 4.12.1.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
 TITANIUM TI-6AL-4V (ELI)

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: 100 SATURATED JP-4 FUEL
 AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.00 | 15.00 | | 5.14 |
| BA | PLATE | 0.10 | 0.10 | | 123 |
| BA | PLATE | 0.10 | 1.00 | | 106 |
| BA | PLATE | 0.50 | 1.00 | | 13.8 |
| BA | PLATE | 0.50 | 0.10 | | 13.9 |

TABLE 4.12.1.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V (ELI)

TEST CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT: DIST WATER AT R. T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|--------------------------------|---|
| | | | | 2.5 5 10 20 50 100 | |
| BA | PLATE | 0.00 | 15.00 | | 9.20 |
| BA | PLATE | 0.10 | 1.00 | | 141 |
| BA | PLATE | 0.50 | 1.00 | | 0.27 13.7 |

TABLE 4.12.1.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-4V (ELI)

TEST CONDITIONS

SPECIMEN

ORIENTATION T-L

ENVIRONMENT: 3.5% NaCl
AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-----------|-------------------------------|-----|---|----|----|----|-----|---|
| BA | PLATE | 0.00 | 15.00 | | | | | | | | 14.5 |
| BA | PLATE | 0.10 | 0.10 | | | | | | | | 393 |
| BA | PLATE | 0.10 | 1.00 | | | | | | | | 214 |
| BA | PLATE | 0.50 | 1.00 | | | | | | | | 31.3 |
| BA | PLATE | 0.50 | 0.10 | | | | | | | | 15.0 |

TABLE 4.12.1.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM Ti-6Al-4V (ELI)

| TEST CONDITIONS | | ENVIRONMENT | | S T W | | FATIGUE CRACK GROWTH RATES: | | | | |
|----------------------|--------------|--------------|------------|--------------------------------|---|-----------------------------|------|------|----|-----|
| SPECIMEN ORIENTATION | T-L | | | AT R. T. | | | | | | |
| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | 2 | 5 | 10 | 20 | 50 | 100 |
| BA | PLATE | 0.10 | 1.00 | | | | | | | 214 |
| BA | PLATE | 0.50 | 0.10 | | | | | 12.7 | | |
| BA | PLATE | 0.50 | 1.00 | | | | 1.13 | 28.2 | | |

TABLE 4.12.2.1

| CONDITION | TITANIUM | | | | | | | | | | K(IIC) STAN DEV | DATE | REFER |
|-------------------------|---------------------|---------------------|--------------------|----------------------------|---------------|---------------|-------------------------|-------------------------------|------------------------------|----------------------------|--------------------|------|-------|
| | --PRODUCT-- FORM | TEST TEMP (F) | SPECIMEN ORIENT | YIELD STRENGTH (KSI) | SPECIMEN----- | | CRACK LENGTH (IN) | 2.9* K(IIC)/TYS**2 (IN) | K(IIC) MEAN (KSI*SQRT IN) | K(IIC) STAN DEV (IN) | | | |
| | | | | | WIDTH (IN) | THICK (IN) | | | | | | | |
| ANNEALED | F | 3 00 | R T | L-T | 117 0 | 4 000 | 2 005 | CT | 2 170 | 1 24 | 82 42 | 1976 | MC001 |
| | | 3 00 | | | 117 0 | 3 926 | 2 001 | CT | 2 136 | 1 31 | 84 91 | 1976 | MC001 |
| | | 3 00 | | | 117 0 | 3 996 | 2 005 | CT | 2 143 | 1 26 | 83 21 | 1976 | MC001 |
| ANNEALED | F | 3 00 | R T | 1-L | 117 0 | 3 997 | 2 023 | CT | 2 157 | 1 31 | 84 71 | 1976 | MC001 |
| | | 3 00 | | | 117 0 | 3 991 | 2 005 | CT | 2 126 | 1 29 | 84 23 | 1976 | MC001 |
| | | 3 00 | | | 117 0 | 3 995 | 2 020 | CT | 2 146 | 1 28 | 83 69 | 1976 | MC001 |
| RECRYSTALLIZE ANNEAL | P | 3 00 | R T | L-T | 119 0 | 4 000 | 2 000 | CT | 2 072 | 0 94 | 73 32 | 1976 | MC001 |
| | | 3 00 | | | 119 0 | 4 000 | 2 000 | CT | 2 088 | 1 14 | 80 66 | 1976 | MC001 |
| | | 3 00 | | | 119 0 | 4 000 | 1 999 | CT | 2 117 | 0 97 | 74 26 | 1976 | MC001 |
| RECRYSTALLIZE ANNEAL | P | 3 00 | R T | T-1 | 122 0 | 4 000 | 2 000 | CT | 2 059 | 0 97 | 76 19 | 1976 | MC001 |
| | | 3 00 | | | 122 0 | 4 000 | 2 000 | CT | 2 034 | 1 01 | 77 61 | 1976 | MC001 |
| | | 3 00 | | | 122 0 | 4 000 | 2 000 | CT | 2 102 | 0 98 | 76 61 | 1976 | MC001 |

TABLE 4.12.2.2

| TITANIUM | | TI-6AL-4V (ELI) K1C | | | | | | | | | | | | | | | |
|------------|---------------------|---------------------|-----------------|--------------|-------|----------------|---------------|---------------------------|---------------|----------------|--------------|----------------------------------|-------------|---------------------------------|-------------|------|-------|
| CONDITION | --PRODUCT-- FORM | THICK (IN) | TEST SPEC OR | YIELD STR | (KSI) | ---SPECIMEN--- | | CRACK LENGTH CROSS STRESS | | | | K(IAPP) MEAN (KSI*SQRT IN) | STAN DEV | K(I C) MEAN (KSI*SQRT IN) | STAN DEV | DATE | REFER |
| | | | | | | WIDTH (IN) | THICK (IN) | INIT (IN) | FINAL (IN) | UNSET (KSI) | MAX (KSI) | | | | | | |
| UNREPEATED | S | 0.03 | R.T. | L-T | 136.0 | 0.025 | 0.490 | 0.780 | --- | 104.00 | 94.77* | 127.27* | 1964 | 60378 | | | |
| | 0.03 | 0.03 | 0.025 | 0.480 | 0.800 | --- | 104.00 | 93.63* | 129.62* | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 0.470 | 0.750 | --- | 107.00 | 95.20* | 127.37* | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 0.480 | 0.750 | --- | 104.00 | 93.63* | 123.79* | 1964 | 60378 | | | | | | |
| UNREPEATED | S | 0.03 | R.T. | L-T | 136.0 | 0.025 | 0.480 | 0.700 | --- | 105.00 | 94.53* | 119.24* | 1964 | 60378 | | | |
| | 0.03 | 0.03 | 0.025 | 1.270 | 1.600 | --- | 71.80 | 108.22 | 126.53* | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 1.280 | 1.700 | --- | 68.50 | 103.76 | 126.31* | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 1.260 | 1.650 | --- | 70.60 | 105.88 | 127.29* | 1964 | 60378 | | | | | | |
| UNREPEATED | S | 0.03 | R.T. | L-T | 136.0 | 0.025 | 1.270 | 1.550 | --- | 73.60 | 110.82 | 125.44* | 1964 | 60378 | | | |
| | 0.03 | 0.03 | 0.025 | 1.270 | 1.650 | --- | 74.90 | 112.74*107.2/ | 3.0 | 134.72* | -----/ | 1964 | 60378 | | | | |
| | 0.03 | 0.03 | 0.025 | 3.490 | 6.190 | --- | 49.50 | 154.33 | 164.70 | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 3.490 | 7.610 | --- | 42.10 | 131.26 | 164.08 | 1964 | 60378 | | | | | | |
| UNREPEATED | S | 0.03 | R.T. | L-T | 136.0 | 0.024 | 3.480 | 7.350 | --- | 44.10 | 137.33 | 167.42 | 1964 | 60378 | | | |
| | 0.03 | 0.03 | 0.025 | 3.900 | 6.980 | --- | 41.60 | 129.83 | 152.10 | 1964 | 60378 | | | | | | |
| | 0.03 | 0.03 | 0.025 | 3.490 | 7.350 | --- | 41.60 | 129.68 | 136.9/10.3 | 151.6/ | 6.5 | 1964 | 60378 | | | | |
| | 0.03 | 0.03 | 0.025 | 3.490 | 7.350 | --- | 41.60 | 129.68 | 136.9/10.3 | 151.6/ | 6.5 | 1964 | 60378 | | | | |

*NOTE - MFT SECTION STRESS EXCEEDS BOX OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.12.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.1 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: ANNEALED

TI-6AL-4V (ELI)

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K MIN | A: 12.87 | 2.61 | | | |
| | B: 13.00 | 2.73 | | | |
| | C: 16.00 | 6.36 | | | |
| | D: 20.00 | 12.9 | | | |
| | 25.00 | 23.5 | | | |
| | 30.00 | 37.6 | | | |
| | 35.00 | 57.6 | | | |
| | 40.00 | 87.5 | | | |
| | 50.00 | 206. | | | |
| | 60.00 | 506. | | | |
| DELTA K MAX | A: 67.30 | 1005. | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 6.38 | | | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 2
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: ANNEALED
 FORM: 3.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY: 1.00- 10.00 HZ

YIELD STRENGTH: 116.8 KSI
 ULT. STRENGTH: 126.7 KSI
 SPECIMEN THK: 0.991- 1.014"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: NC002

TITAN. ALLOY

TI-6AL-4V (ELI)

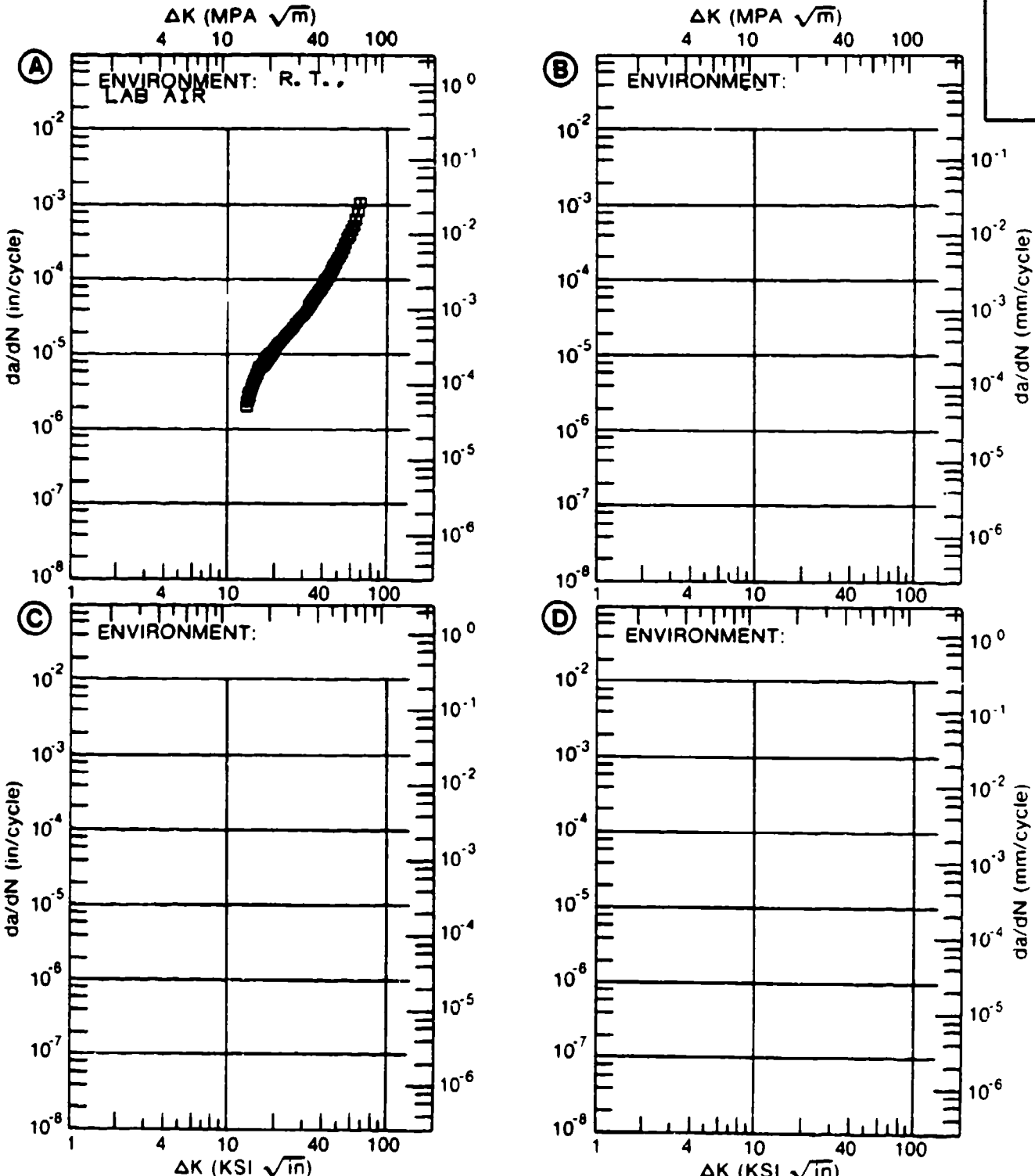


Figure 4.12.3.1

TABLE 4.12.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.2 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: ANNEALED | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K | A: 12.55 | .717 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .974 | | | |
| | 16.00 | 4.18 | | | |
| | 20.00 | 11.9 | | | |
| | 25.00 | 23.6 | | | |
| | 30.00 | 36.4 | | | |
| | 35.00 | 52.3 | | | |
| | 40.00 | 75.1 | | | |
| | 50.00 | 171. | | | |
| | 60.00 | 461. | | | |
| DELTA K | A: 63.28 | 662. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 26.42 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | 1 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ANNEALED
 FORM: 3.00" TH FORGING
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00- 20.00 HZ

YIELD STRENGTH: 116.9 KSI
 ULT. STRENGTH: 127.0 KSI
 SPECIMEN THK: 0.999- 1.002"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: NC002

TITAN.
ALLOY

TI-6AL-
4V (ELI)

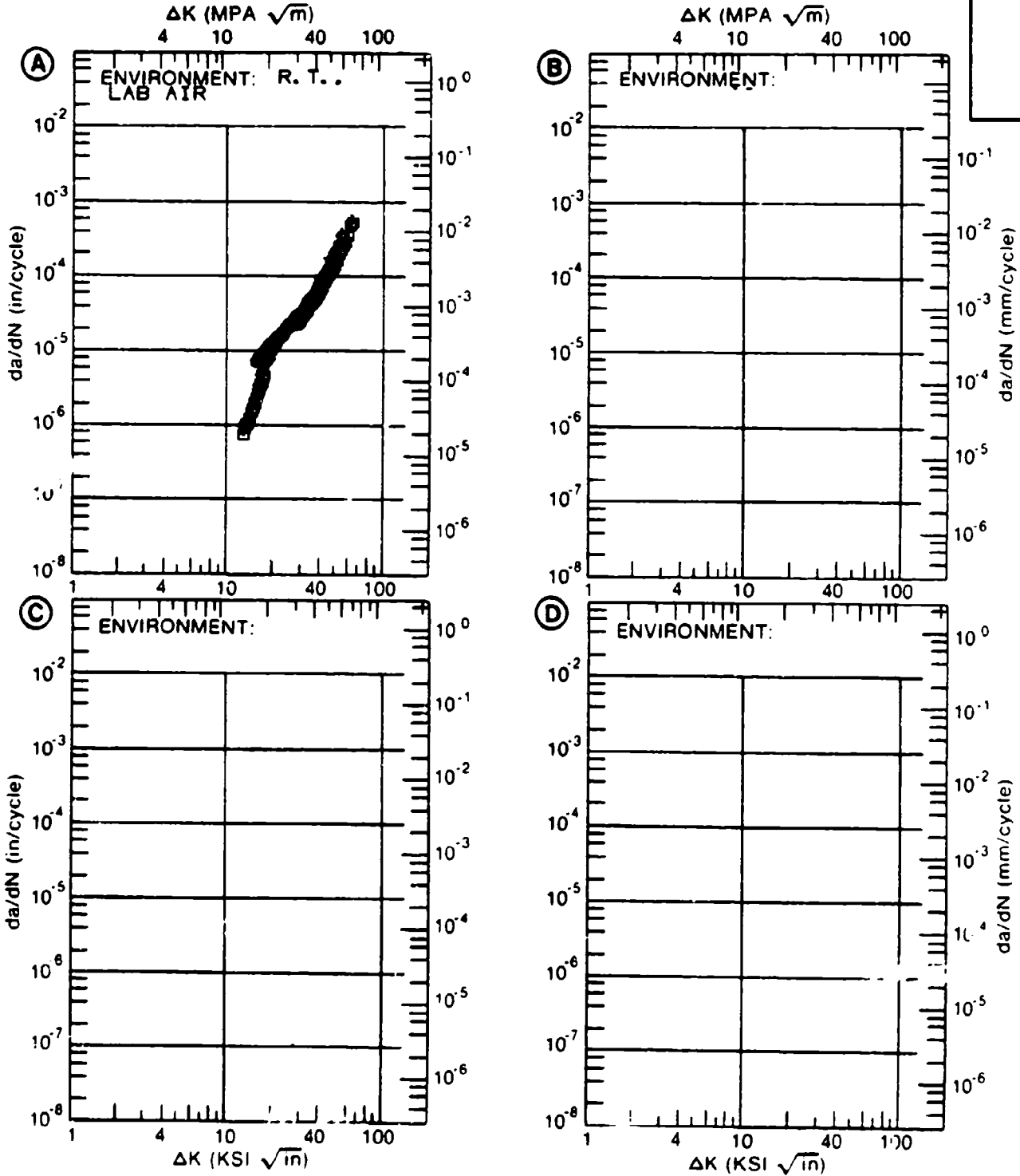


Figure 4.12.3.2

TABLE 4.12.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.3 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|------------------------------|------------|---------------------------------------|----------|---|---|
| CONDITION: BA | | | | | |
| ENVIRONMENT: R. T. , DRY AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0. 10 | R=+0. 80 | | |
| DELTA K | A: 40. 32 | 58. 0 | | | |
| MIN | B: 7. 50 | | . 190 | | |
| | C: | | | | |
| | D: | | | | |
| | 8. 00 | | . 286 | | |
| | 9. 00 | | . 597 | | |
| | 10. 00 | | 1. 12 | | |
| | 13. 00 | | 4. 50 | | |
| | 16. 00 | | | | |
| | 20. 00 | | | | |
| | 25. 00 | | | | |
| | 30. 00 | | | | |
| | 35. 00 | | | | |
| | 40. 00 | | | | |
| | 50. 00 | 128. | | | |
| | 60. 00 | 229. | | | |
| | 70. 00 | 401. | | | |
| DELTA K | A: 71. 02 | 426. | | | |
| MAX | B: 13. 61 | | 5. 54 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 4. 60 | 10. 38 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | | | | |
| SUMMARY | 1. 25-2. 0 | | | | |
| (NP/NA) | >2. 0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., DRY AIR

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 98140

| |
|---------------------|
| TITAN. ALLOY |
| TI-6AL- 4V (ELI) |
| |

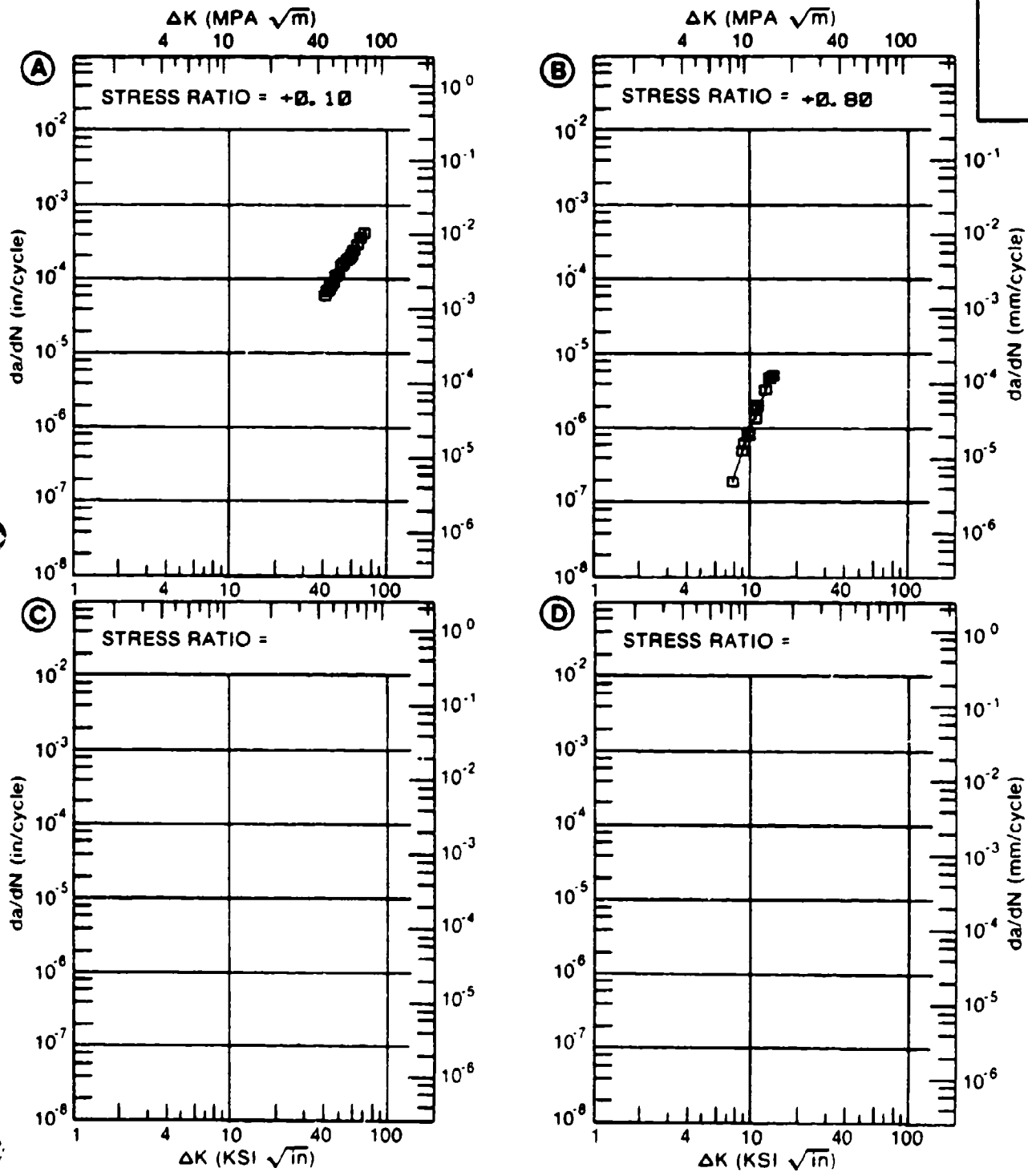


Figure 4.12.3.3

TABLE 4.12.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.4 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-4V (ELI)
CONDITION: BA
ENVIRONMENT: R. T. , 3. 5% NACL

| DELTA K (KBI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|----|----|----|
| | A | B | C | D |
| | R=+0. 80 | | | |
| DELTA K MIN | A: | B: | C: | D: |
| 200. 00 | | | | |
| DELTA K MAX | A: | B: | C: | D: |

ROOT MEAN SQUARE 0. 00
PERCENT ERROR

LIFE 0. 0-0. 5
PREDICTION 0. 5-0. 8
RATIO 0. 8-1. 25
SUMMARY 1. 25-2. 0
(NP/NA) >2. 0

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 FREQUENCY: 1.00 HZ
 ENVIRONMENT: R. T., 3.5% NaCl

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-4V (ELI)

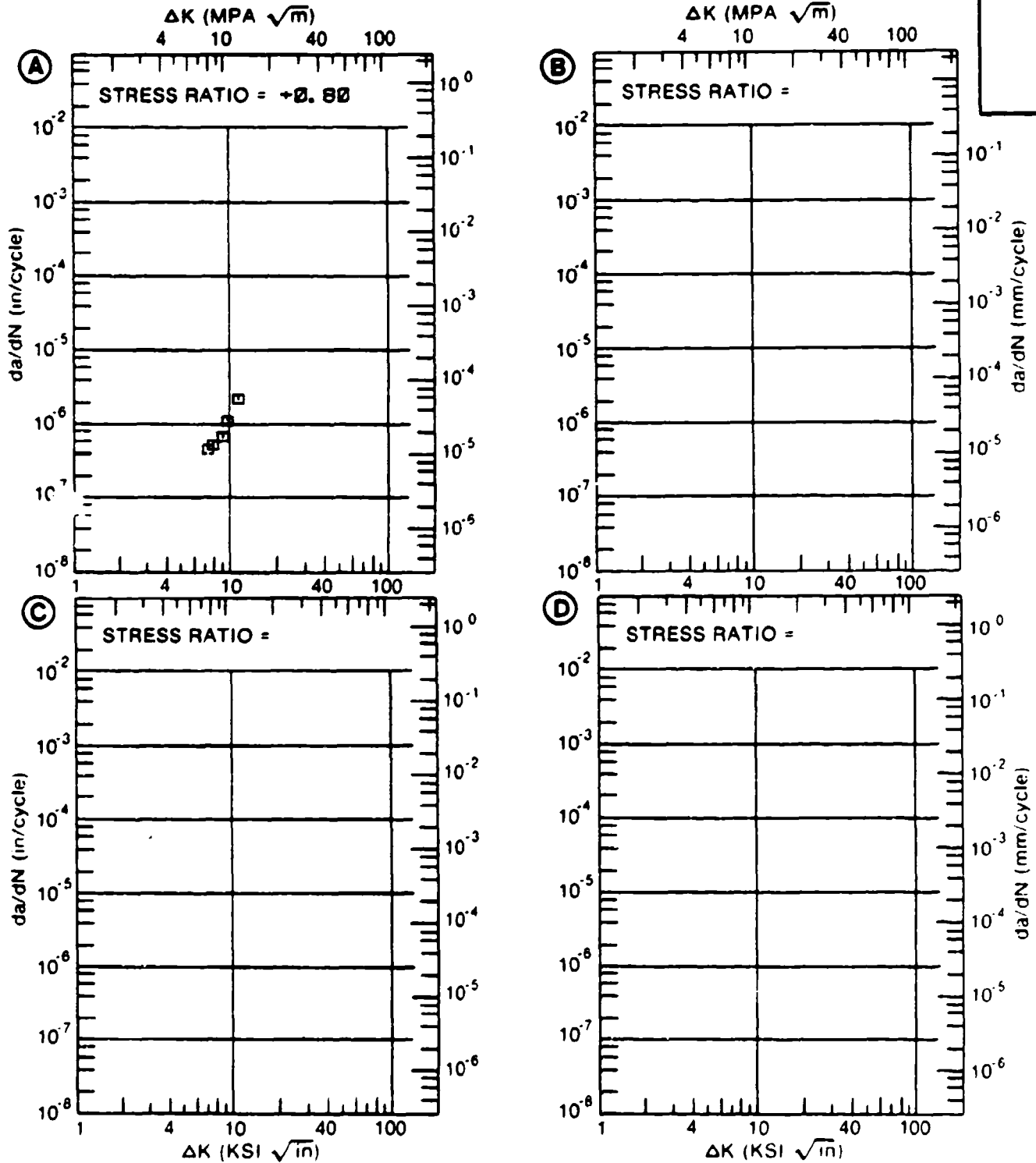


Figure 4.12.3.4

TABLE 4.12.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.5 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-4V (ELI)
CONDITION: BA

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|-------|---|---|
| | A | B | C | D |
| E= R. T. DRY AIR | | | | |
| DELTA K MIN | A: 11.53 | .0879 | | |
| | B: | | | |
| | C: | | | |
| | D: | | | |
| | 13.00 | .227 | | |
| | 16.00 | 1.01 | | |
| | 20.00 | 4.02 | | |
| | 25.00 | 11.9 | | |
| | 30.00 | 22.4 | | |
| | 35.00 | 31.3 | | |
| DELTA K MAX | A: 37.95 | 34.5 | | |
| | B: | | | |
| | C: | | | |
| | D: | | | |

ROOT MEAN SQUARE 24.63
PERCENT ERROR

| | |
|------------|----------|
| LIFE | 0.0-0.5 |
| PREDICTION | 0.5-0.8 |
| RATIO | 0.8-1.25 |
| SUMMARY | 1.25-2.0 |
| (NP/NA) | >2.0 |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.00
 FREQUENCY: 15.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-
4V (ELI)

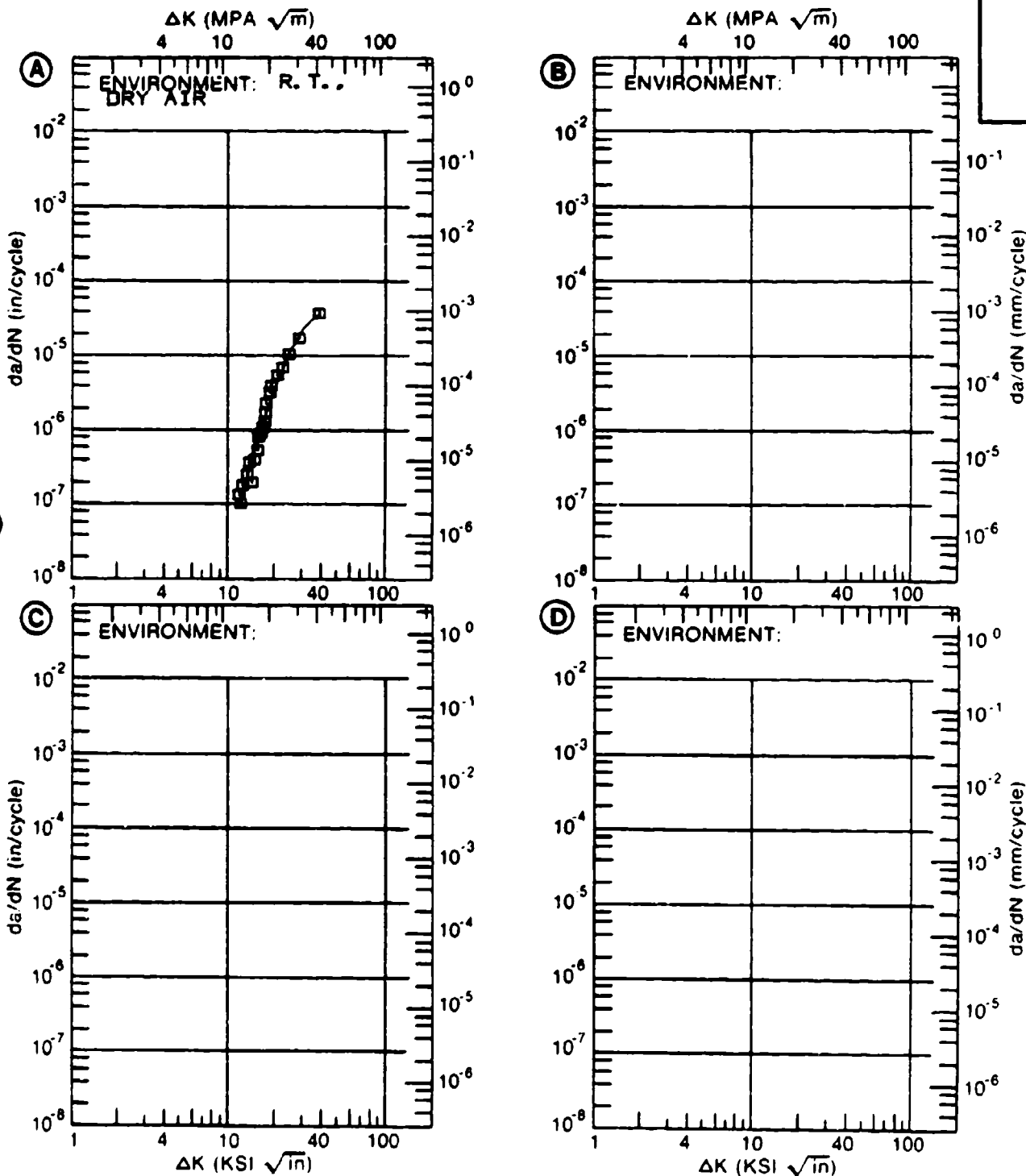


Figure 4.12.3.5

TABLE 4.12.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.6 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--|-------------------------|-----------------------|----------------------|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. DIST. WATER | E= R. T. 3.5% NACL | E= R. T. S. T. W. |
| DELTA K MIN | A: 14.45 | .387 | | | |
| | B: 15.47 | | .968 | | |
| | C: 10.07 | | | .117 | |
| | D: 13.53 | | | | .400 |
| | 13.00 | | | 1.36 | |
| | 16.00 | 1.06 | 1.27 | 2.99 | 1.64 |
| | 20.00 | 5.14 | 5.20 | 14.5 | |
| | 25.00 | 13.4 | 13.0 | | |
| | 30.00 | 22.4 | 22.8 | | |
| | 35.00 | 32.4 | 35.7 | | |
| 40.00 | 45.9 | 55.4 | | | |
| DELTA K MAX | A: 43.49 | 59.6 | | | |
| | B: 40.10 | | 55.9 | | |
| | C: 24.47 | | | 24.0 | |
| | D: 16.98 | | | | 3.23 |
| ROOT MEAN SQUARE | | 11.94 | 19.22 | 22.82 | 17.58 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.00
 FREQUENCY: 15.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
 ALLOY
 TI-6AL-
 4V (ELI)

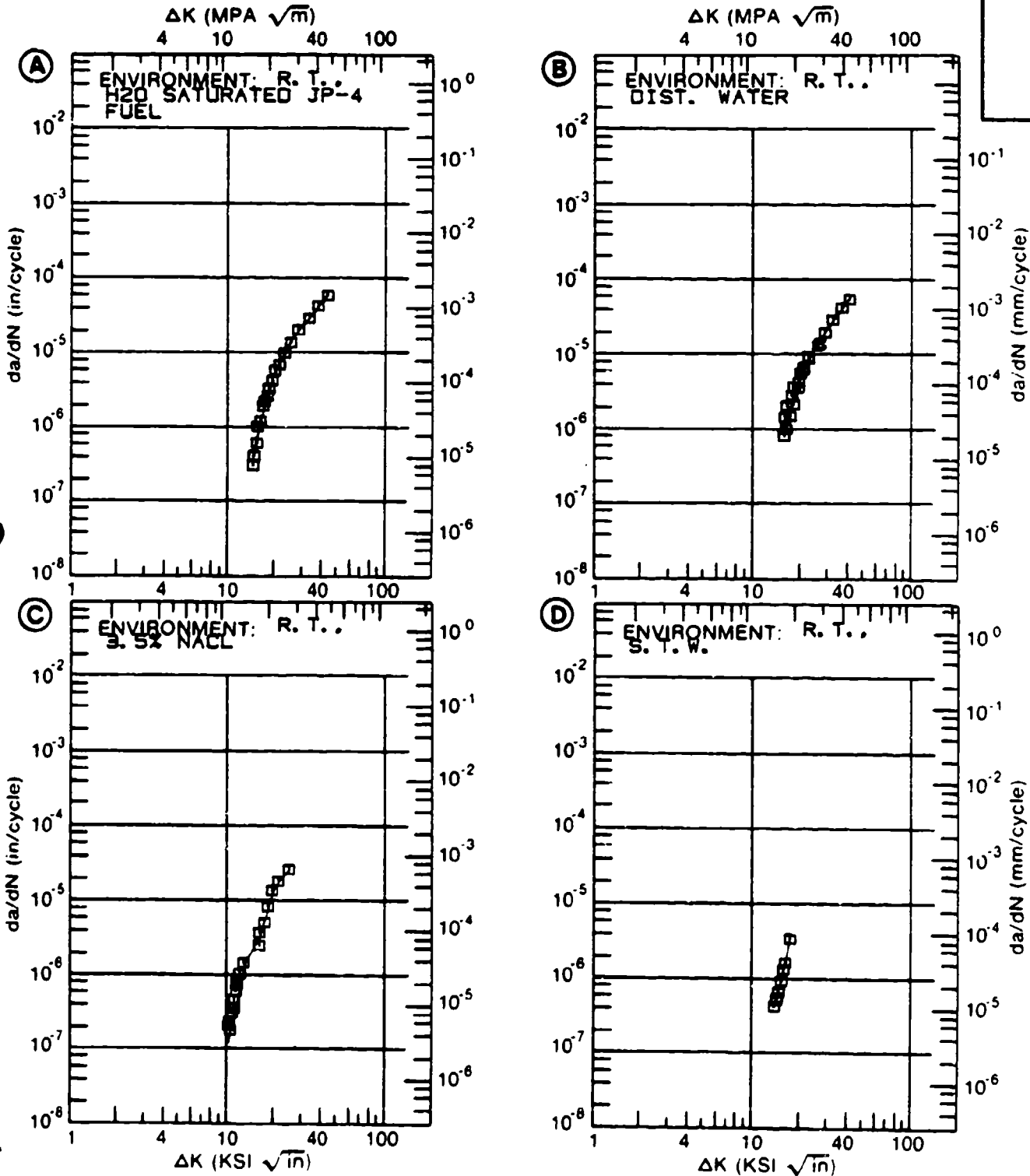


Figure 4.12.3.6

TABLE 4.12.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.7 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--|---|-------------------------|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. ALT JP4-FUEL & DIST. WATER | E= R. T. DIST. WATER | |
| DELTA K | A: 27.33 | 19.4 | | | |
| MIN | B: 26.24 | | 19.2 | | |
| | C: 42.57 | | | 63.1 | |
| | D: | | | | |
| | 30.00 | 26.4 | 31.1 | | |
| | 35.00 | 40.8 | 48.9 | | |
| | 40.00 | 57.7 | 69.0 | | |
| | 50.00 | 106. | 122. | 141. | |
| | 60.00 | 200. | 212. | 210. | |
| | 70.00 | 402. | 388. | 383. | |
| DELTA K | A: 72.48 | 483. | | | |
| MAX | B: 73.62 | | 489. | | |
| | C: 74.51 | | | 607. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 10.21 | 12.84 | 5.17 | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 98140

TITAN.
ALLOY

TI-6AL-4V (ELI)

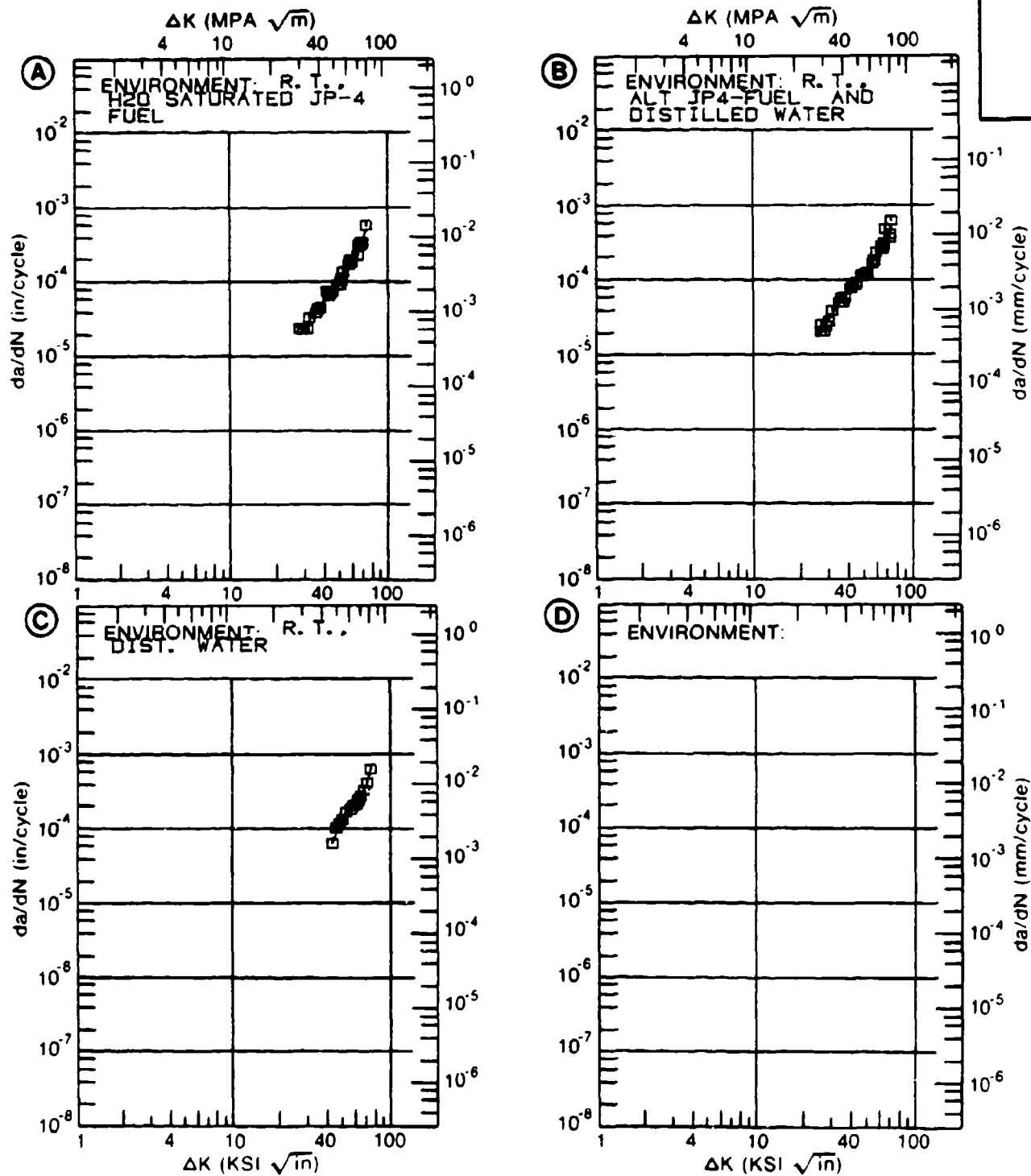


Figure 4.12.3.7

TABLE 4.12.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.8 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|---------------------------------------|---|---------------------------|----------------------|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3. 5% NACL | E= R. T. S. T. W. | | |
| DELTA K MIN | A: 26. 53 | 51. 6 | | | |
| | B: 27. 01 | | 37. 8 | | |
| | C: | | | | |
| | D: | | | | |
| | 30. 00 | 74. 9 | 53. 2 | | |
| | 35. 00 | 107. | 70. 8 | | |
| | 40. 00 | 138. | 89. 9 | | |
| | 50. 00 | 214. | 214. | | |
| | 60. 00 | 355. | 616. | | |
| | 70. 00 | 657. | | | |
| DELTA K MAX | A: 73. 43 | 833. | | | |
| | B: 64. 60 | | 757. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 7. 81 | 10. 86 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0. 0-0. 5 0. 5-0. 8 0. 8-1. 25 1. 25-2. 0 >2. 0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-4V (ELI)

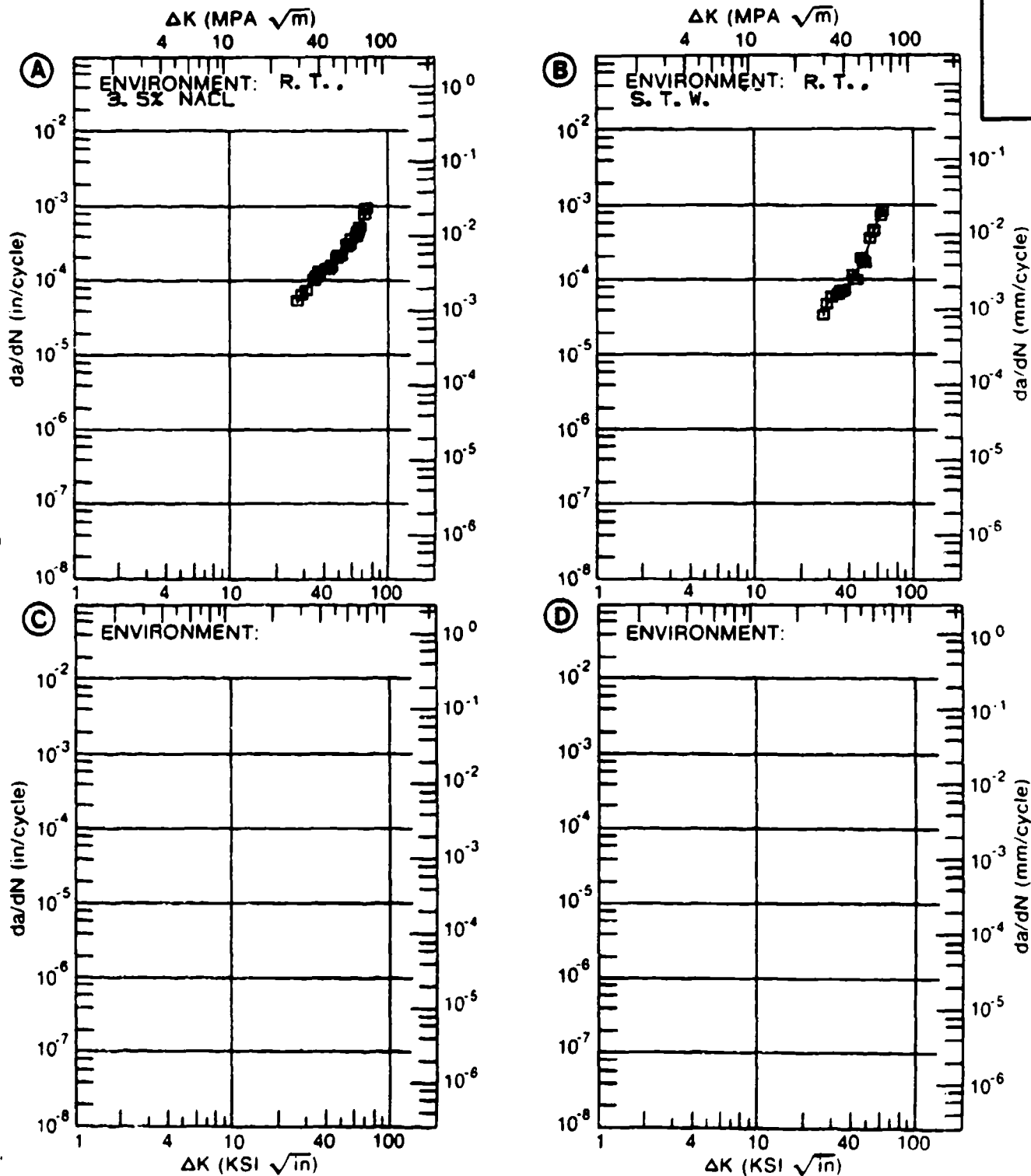


Figure 4.12.3.8

TABLE 4.12.3.9

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.9 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--|------------------------|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. 3.5% NAACL | | |
| DELTA K MIN | A: 26.50 | 15.3 | | | |
| | B: 26.84 | | 11.0 | | |
| | C: | | | | |
| | D: | | | | |
| | 30.00 | 28.0 | 36.5 | | |
| | 35.00 | 47.5 | 110. | | |
| | 40.00 | 67.9 | 194. | | |
| | 50.00 | 123. | 353. | | |
| | 60.00 | 230. | 624. | | |
| | 70.00 | 501. | 1449. | | |
| DELTA K MAX | A: 76.78 | 1014. | | | |
| | B: 75.41 | | 2636. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 10.69 | 18.13 | | |
| PERCENT ERROR | | | | | |
| 1.0 | 0.0-0.5 | | | | |
| 0.5 | 0.5-0.8 | | | | |
| 0.25 | 0.8-1.25 | | | | |
| 0.1 | 1.25-2.0 | | | | |
| 0.05 | 2.0-3.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-
4V (ELI)

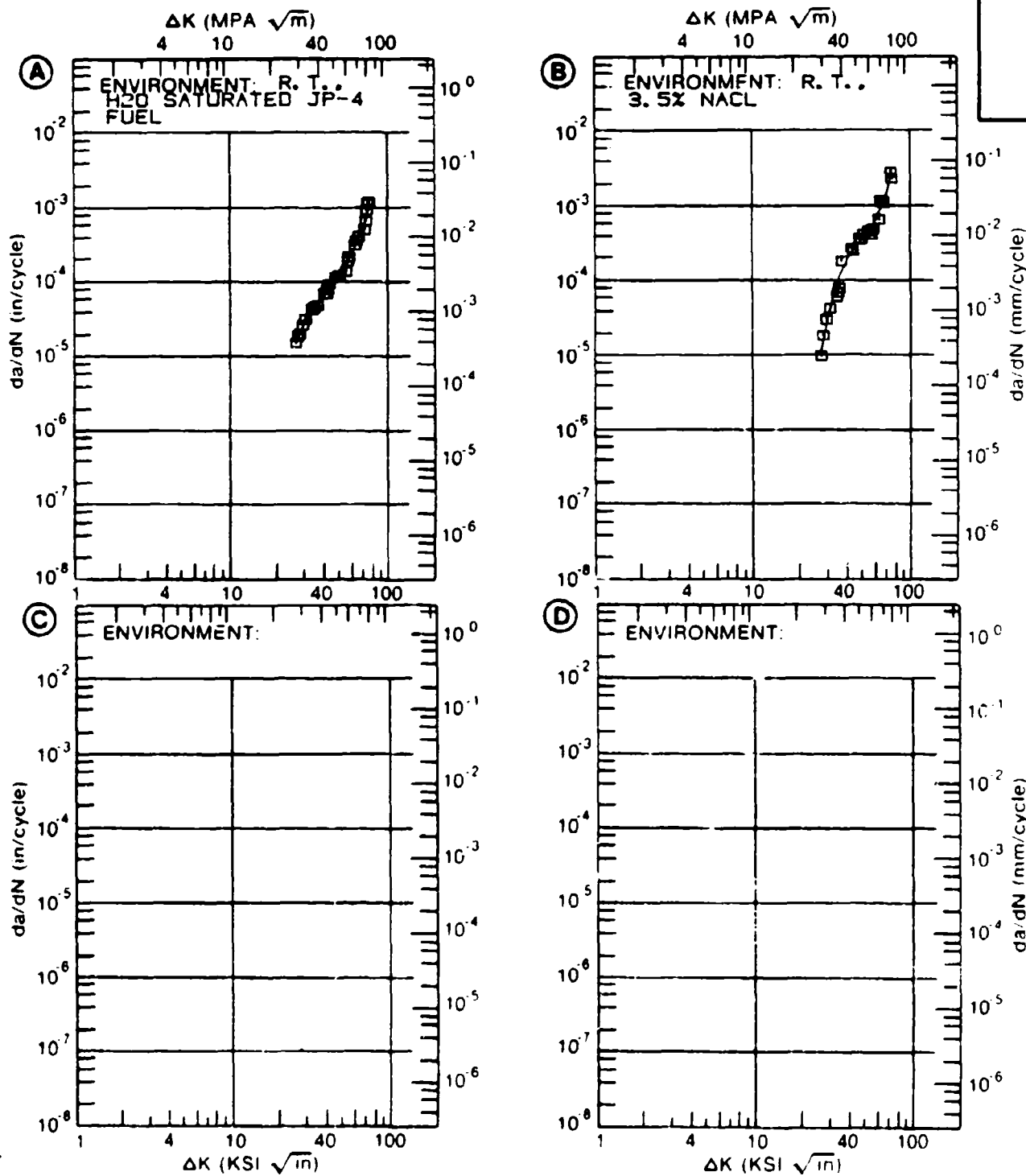


Figure 4.12.3.9

TABLE 4.12.3.10

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.10 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E-- 65F NITROGEN & AIR | | | |
| DELTA K MIN | A: 15.30 | 2.20 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 16.00 | 2.69 | | | |
| | 20.00 | 9.07 | | | |
| | 25.00 | 15.4 | | | |
| | 30.00 | 22.0 | | | |
| | 35.00 | 33.1 | | | |
| | 40.00 | 53.4 | | | |
| DELTA K MAX | A: 42.13 | 66.9 | | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 11.19 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES 8B140

TITAN.
ALLOY

TI-6AL-4V (ELI)

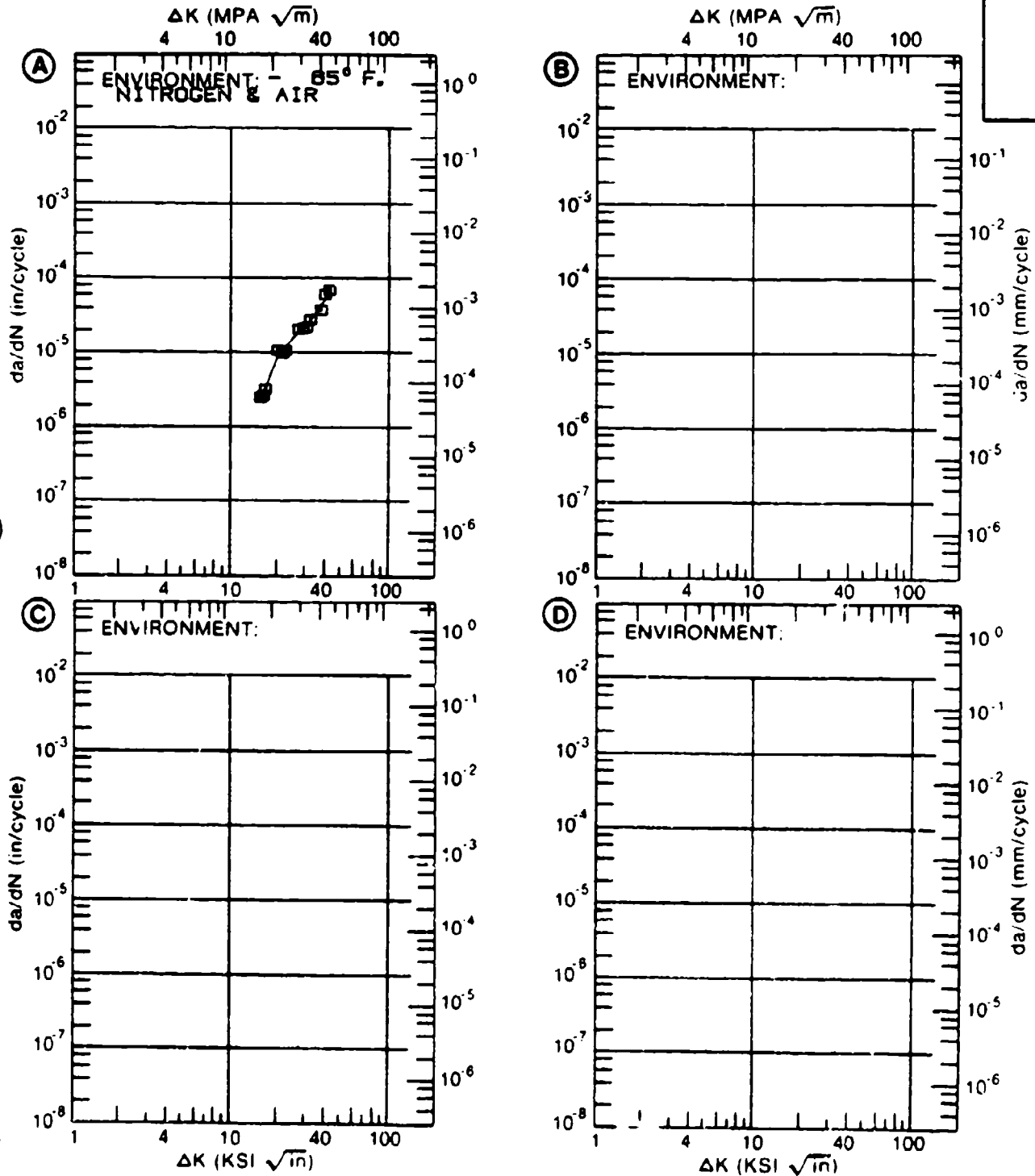


Figure 4.12.3.10

TABLE 4.12.3.11

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.11 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|---------------------------------------|--|--------------------------------------|-----------------------|-------------------------|-----------------------|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E=+ 175F DRY AIR | E=+ 175F JP-4 FUEL | E=+ 175F DIST. WATER | E=+ 175F 3.5% NaCl |
| DELTA K MIN | A: 15.15 | 4.42 | | | |
| | B: 14.71 | | 3.87 | | |
| | C: 21.49 | | | 19.1 | |
| | D: 15.01 | | | | 3.51 |
| | 16.00 | 5.69 | 5.02 | | 6.93 |
| | 20.00 | 12.1 | 13.3 | | 17.8 |
| | 25.00 | 20.7 | 24.0 | 29.8 | 48.6 |
| | 30.00 | 33.5 | 36.9 | 50.4 | 100. |
| | 35.00 | 56.1 | 59.6 | 73.3 | 159. |
| | 40.00 | 78.0 | 99.0 | 91.9 | |
| DELTA K MAX | A: 40.96 | 80.3 | | | |
| | B: 42.28 | | 101. | | |
| | C: 41.36 | | | 95.5 | |
| | D: 35.56 | | | | 165. |
| ROOT MEAN SQUARE PERCENT ERROR | | 9.05 | 14.61 | 7.92 | 12.39 |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 88140

TITAN.
ALLOY

TI-6AL-4V (ELI)

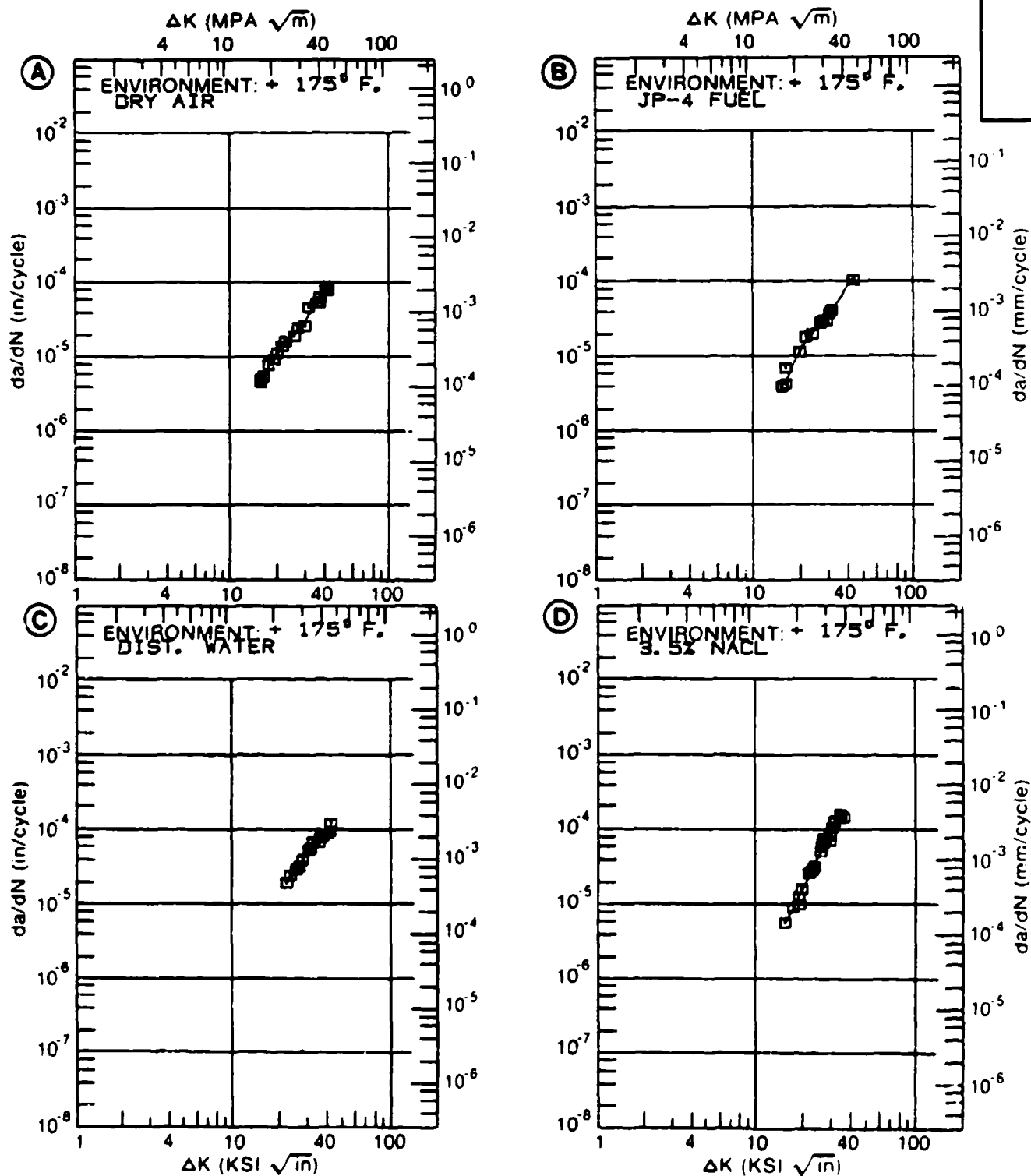


Figure 4.12.3.11

TABLE 4.12.3.12

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.12 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--|---|-------------------------|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. ALT JP4-FUEL & DIST. WATER | E= R. T. DIST. WATER | |
| DELTA K MIN | A: 10.91 | .61 | | | |
| | B: 10.34 | | .50 | | |
| | C: 9.85 | | | .23 | |
| | D: | | | | |
| | 10.00 | | | .273 | |
| | 13.00 | 2.24 | 2.19 | 2.03 | |
| | 16.00 | 6.47 | 5.87 | 6.01 | |
| | 20.00 | 13.8 | 12.9 | 13.7 | |
| | 25.00 | 24.6 | 23.5 | 25.5 | |
| | 30.00 | 39.7 | 35.5 | 40.7 | |
| | 35.00 | 66.0 | 50.1 | 63.0 | |
| | 40.00 | 117. | | 98.7 | |
| DELTA K MAX | A: 41.26 | 137. | | | |
| | B: 36.59 | | 55.4 | | |
| | C: 44.21 | | | 148. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 22.06 | 20.98 | 16.08 | |
| PERCENT ERROR | | | | | |

LIFE 0.0-0.5
 PREDICTION 0.5-0.8
 RATIO 0.8-1.25
 SUMMARY 1.25-2.0
 (NP/NA) >2.0

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 99140

TITAN.
ALLOY

TI-6AL-
4V (ELI)

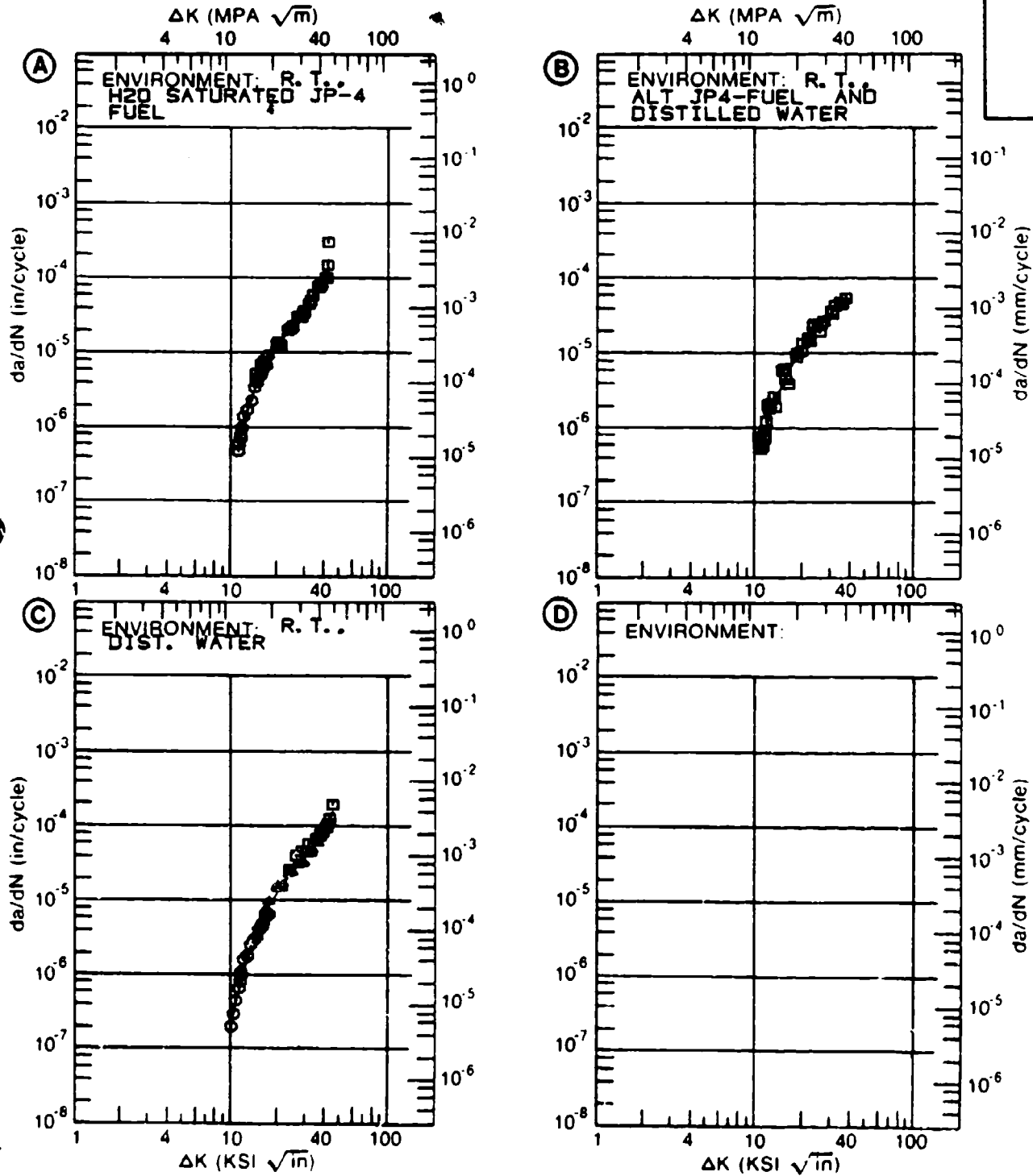


Figure 4.12.3.12

TABLE 4.12.3.13

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.13 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|---------------------------------------|----------|--------------------------------------|----------------------|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3.5% NaCl | E= R. T. S. T. W. | | |
| DELTA K MIN | A: 10.16 | .980 | | | |
| | B: 9.76 | | .991 | | |
| | C: | | | | |
| | D: | | | | |
| | 10.00 | | 1.13 | | |
| | 13.00 | 2.61 | 3.77 | | |
| | 16.00 | 7.36 | 9.26 | | |
| | 20.00 | 31.3 | 28.2 | | |
| | 25.00 | 69.0 | 62.3 | | |
| | 30.00 | 115. | 86.9 | | |
| | 35.00 | 184. | 120. | | |
| | 40.00 | 308. | 196. | | |
| DELTA K MAX | A: 40.69 | 333. | | | |
| | B: 42.18 | | 258. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 18.54 | 15.96 | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | | | | |
| | 1.25-2.0 | | | | |
| | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

| |
|---------------------|
| TITAN. ALLOY |
| TI-6AL- 4V (ELI) |
| |

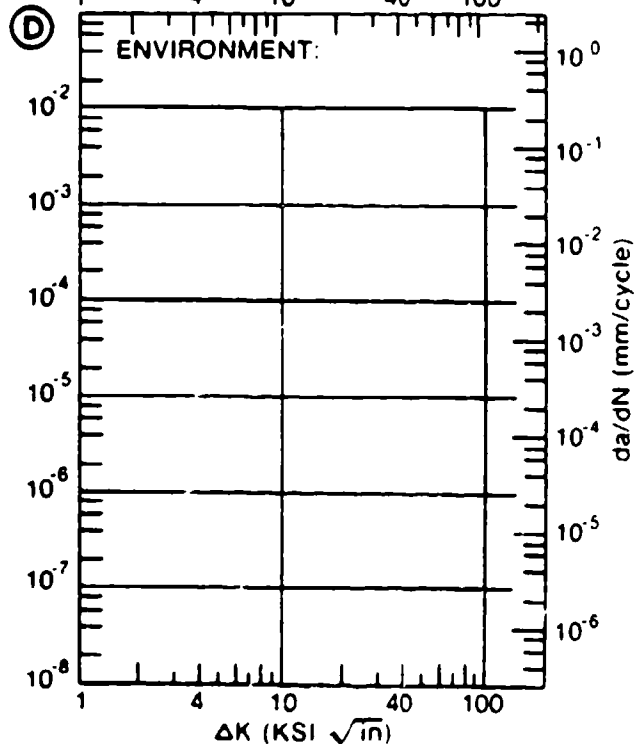
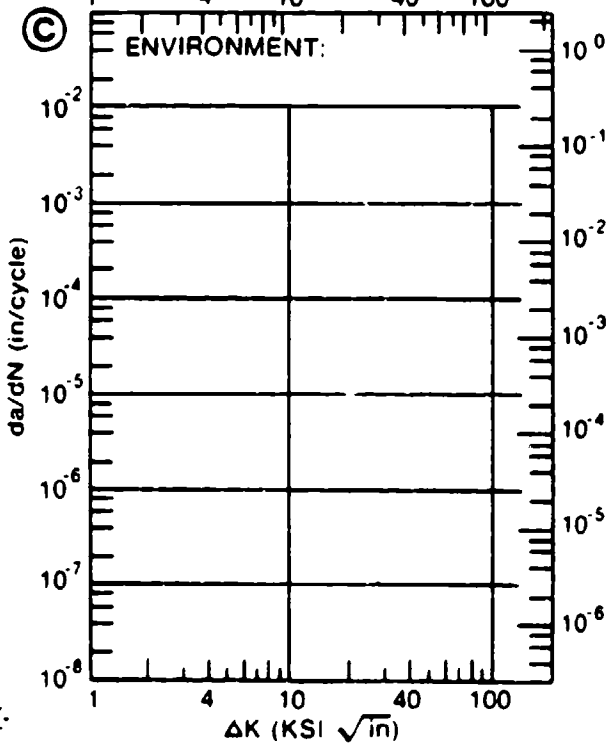
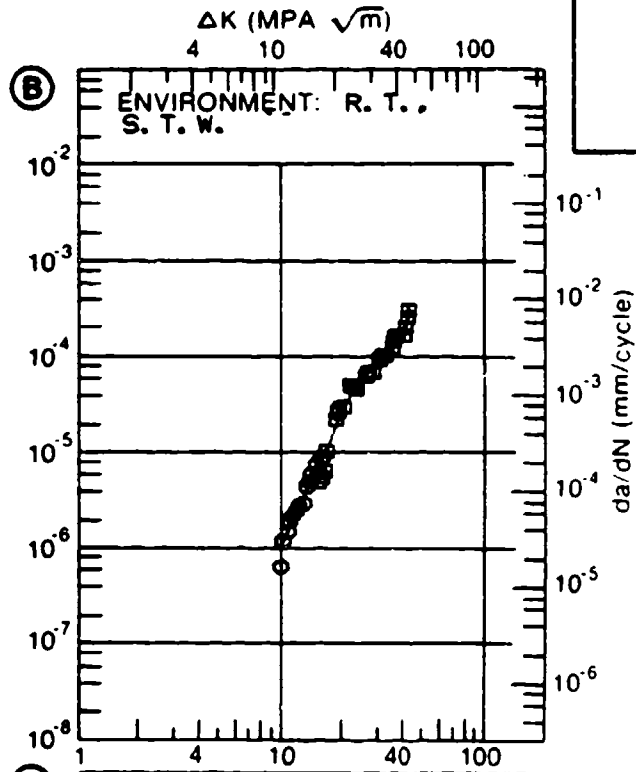
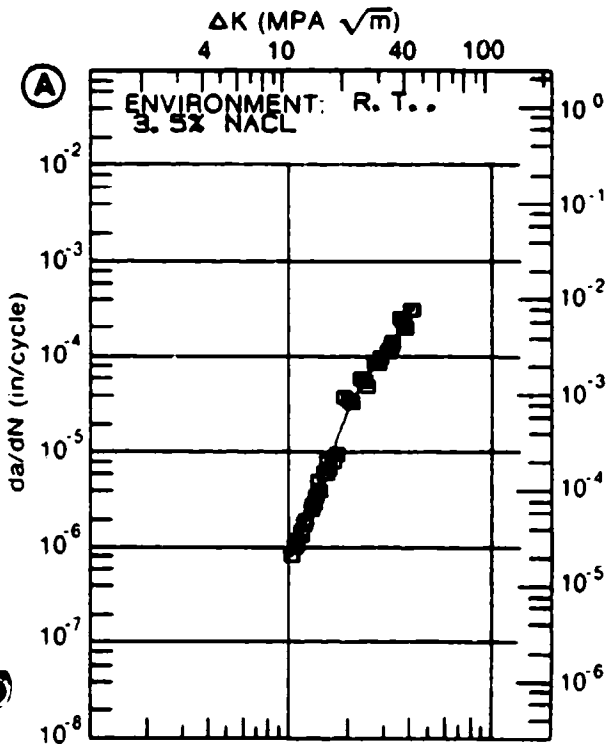


Figure 4.12.3.13

TABLE 4.12.3.14

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.14 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| CONDITION: BA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. : DRY AIR | | | |
| DELTA K | A: 10.10 | .424 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 2.46 | | | |
| | 16.00 | 6.34 | | | |
| | 20.00 | 12.8 | | | |
| | 25.00 | 22.4 | | | |
| | 30.00 | 36.2 | | | |
| | 35.00 | 60.4 | | | |
| | 40.00 | 107. | | | |
| DELTA K | A: 40.48 | 113. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 20.59 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 0.10- 1.00 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES 00140

TITAN.
 ALLOY
 TI-6AL-
 4V (ELI)

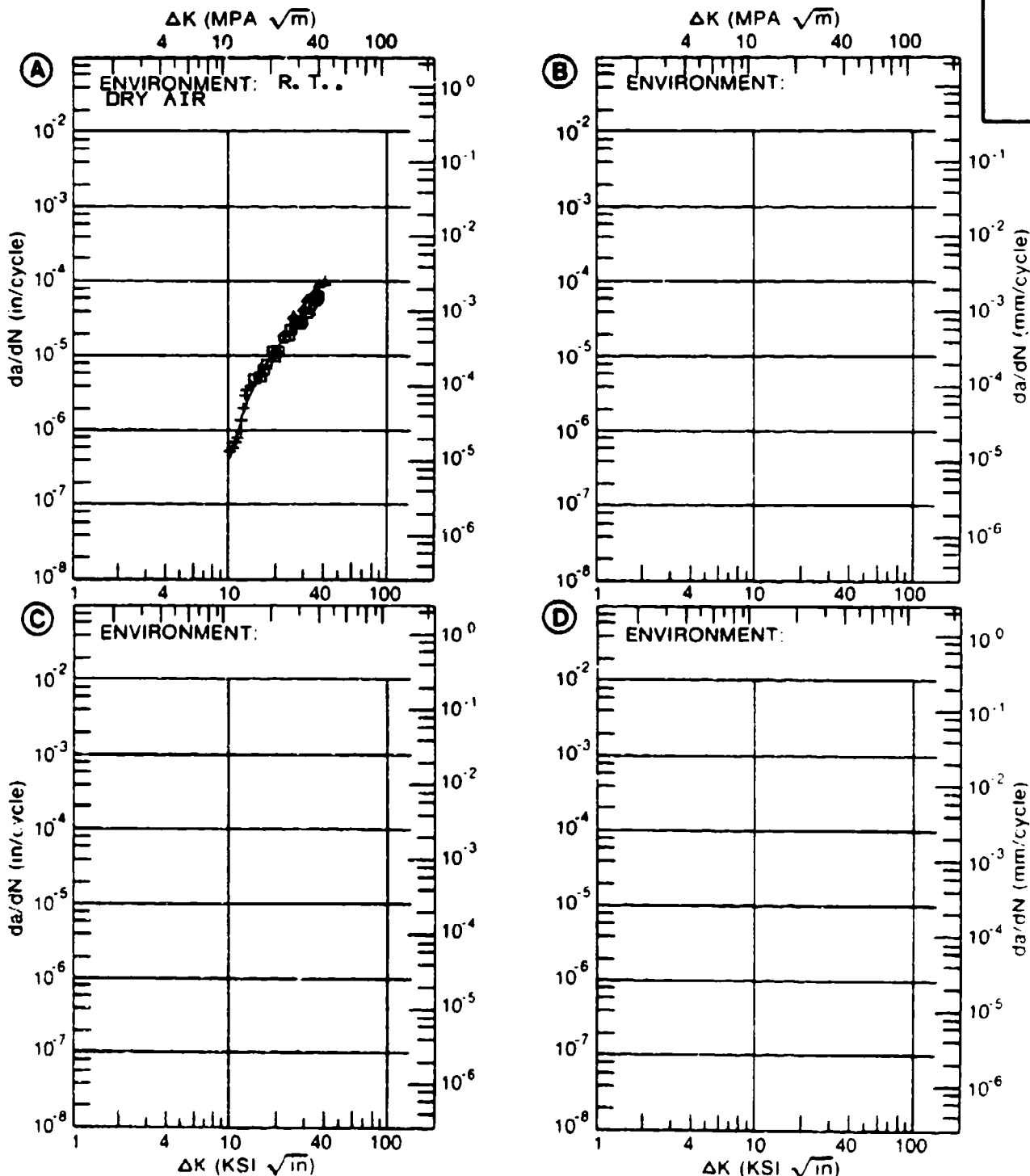


Figure 4.12.3.14

TABLE 4.12.3.15

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.15 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: BA

TI-6AL-4V (ELI)

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
|-----------------------------------|--|--------------------------------------|--------------------------------------|--|
| | A | B | C | D |
| | E= R. T. H2O SATURATED JP-4 FUEL | E= R. T. 3. 5% NACL | E= R. T. S. T. W. | |
| DELTA K MIN | A: 14.08 : B: 15.54 : C: 15.38 : D: | 3.65 | 5.62 | 4.56 |
| | 16.00 : 20.00 : 25.00 : 30.00 : 35.00 : 40.00 : | 6.63 13.9 25.0 42.8 78.6 | 6.80 15.0 37.8 178. 264. | 5.42 12.7 27.2 54.1 110. 233. |
| DELTA K MAX | A: 37.10 : B: 35.28 : C: 42.70 : D: | 105. | 264. | 357. |
| ROOT MEAN SQUARE PERCENT ERROR | | 7.84 | 21.27 | 9.49 |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/MA) >2.0

CONDITION/HT: BA
 FORM: 1.00" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 STRESS RATIO: +0.50
 FREQUENCY: 0.10 HZ

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 00140

TITAN.
 ALLOY
 TI-6AL-
 4V (ELI)

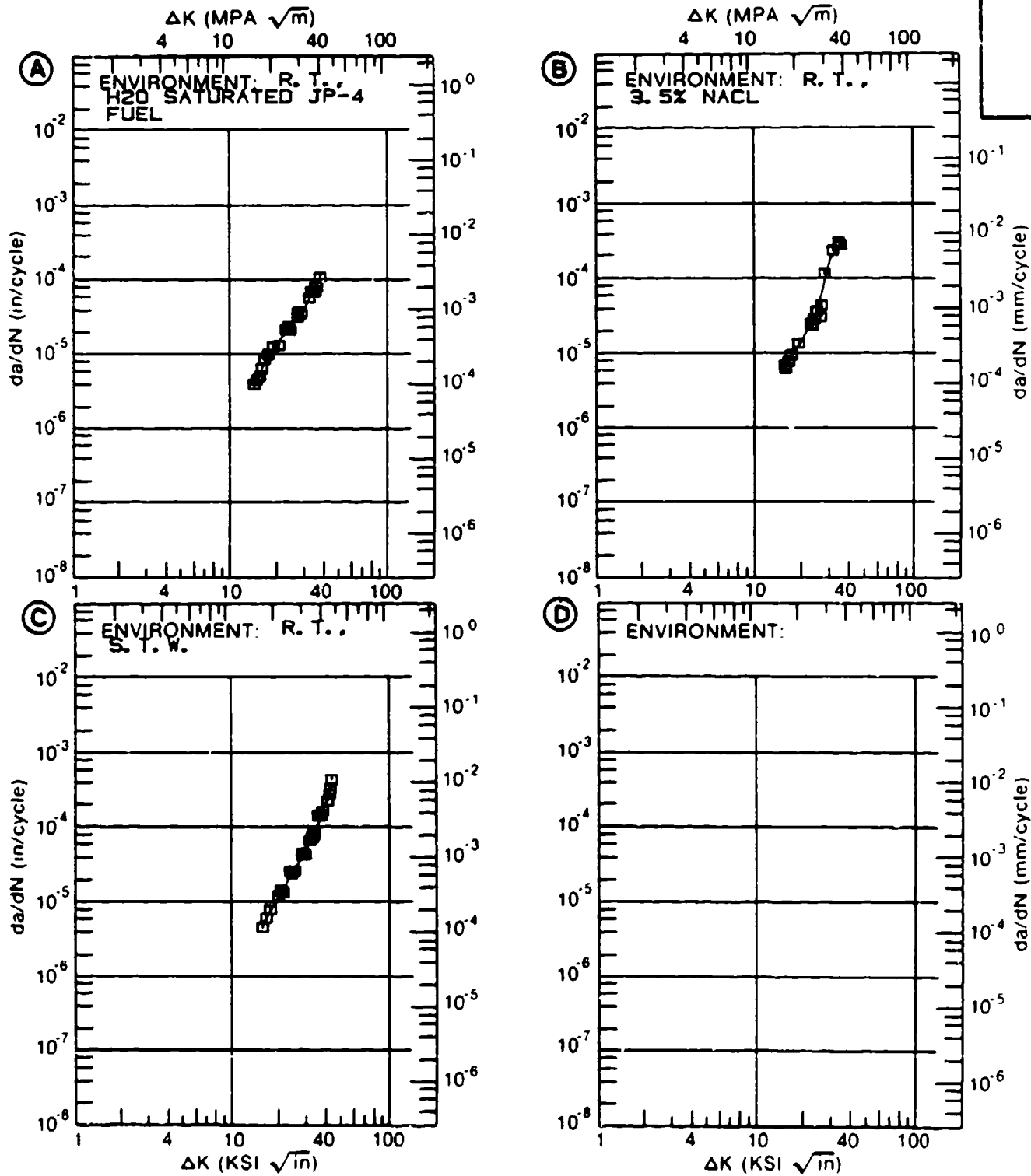


Figure 4.12.3.15

TABLE 4.12.3.16

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.16 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|--------------------------|----------|--------------------------------------|--------------------------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR 10HZ | E= R. T. SIM. SEA WATER 1-10HZ | | |
| DELTA K | A: 12.94 | .519 | | | |
| MIN | B: 10.88 | | 3.44 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | .565 | 3.90 | | |
| | 16.00 | 4.94 | 7.39 | | |
| | 20.00 | 10.8 | 15.0 | | |
| | 25.00 | 19.4 | 32.1 | | |
| | 30.00 | 30.8 | 64.3 | | |
| | 35.00 | 50.6 | 121. | | |
| | 40.00 | 91.5 | 204. | | |
| | 50.00 | | 393. | | |
| DELTA K | A: 47.16 | 202. | | | |
| MAX | B: 50.76 | | 404. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 33.80 | 20.45 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | | 2 | | |
| SUMMARY | 1.25-2.0 | 1 | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM: 3.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 119.4 KSI
 ULT. STRENGTH: 127.8 KSI
 SPECIMEN THK: 1.003- 1.040"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: NC002

TITAN. ALLOY

TI-6AL-4V (ELI)

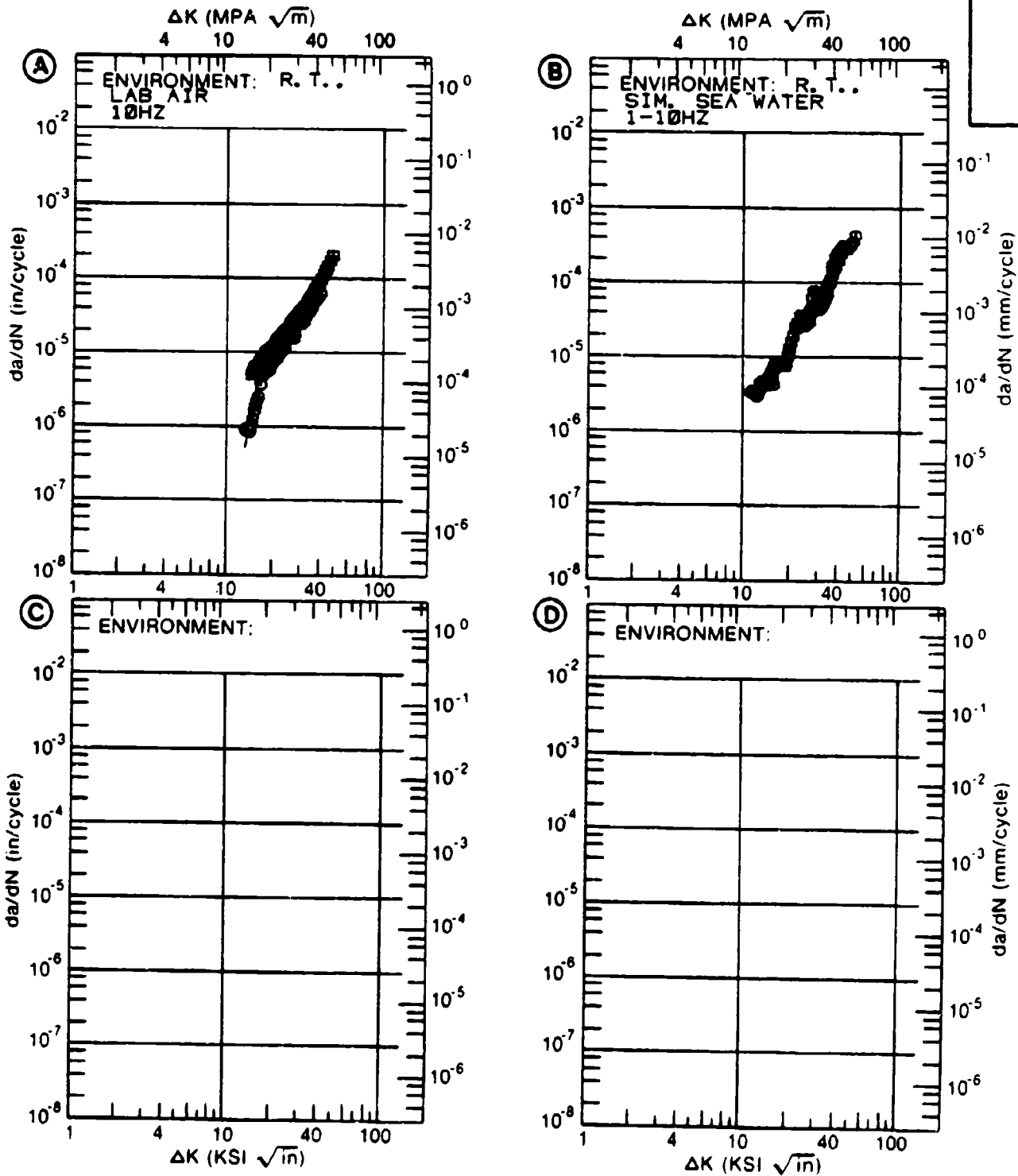


Figure 4.12.3.16

TABLE 4.12.3.17

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.12.3.17 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-4V (ELI) | | | |
|---------------------------------------|--|--------------------------------------|----------------------------|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E= R. T. SIM. SEA WATER | | |
| DELTA K MIN | A: 12.57 | 1.50 | | | |
| | B: 13.17 | | 2.76 | | |
| | C: | | | | |
| | D: | | | | |
| | 13.00 | 1.71 | | | |
| | 16.00 | 3.68 | 3.88 | | |
| | 20.00 | 7.75 | 7.96 | | |
| | 25.00 | 16.0 | 20.1 | | |
| | 30.00 | 29.4 | 45.1 | | |
| | 35.00 | 51.4 | 87.4 | | |
| | 40.00 | 87.2 | 146. | | |
| | 50.00 | 240. | | | |
| | 60.00 | 638. | | | |
| DELTA K MAX | A: 67.29 | 1287. | | | |
| | B: 45.43 | | 221. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.76 | 30.38 | | |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 0.5-0.8 0.8-1.25 1.25-2.0 >2.0 | 1 2 | 1 1 | | |

CONDITION/HT: RA
 FORM: 3.00" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 1.00- 10.00 HZ

YIELD STRENGTH: 122.0 KSI
 ULT. STRENGTH: 130.2 KSI
 SPECIMEN THK: 0.923- 1.010"
 SPECIMEN WIDTH: 7.400"
 REFERENCES: NC002

TITAN.
 ALLOY
 TI-6AL-
 4V (ELI)

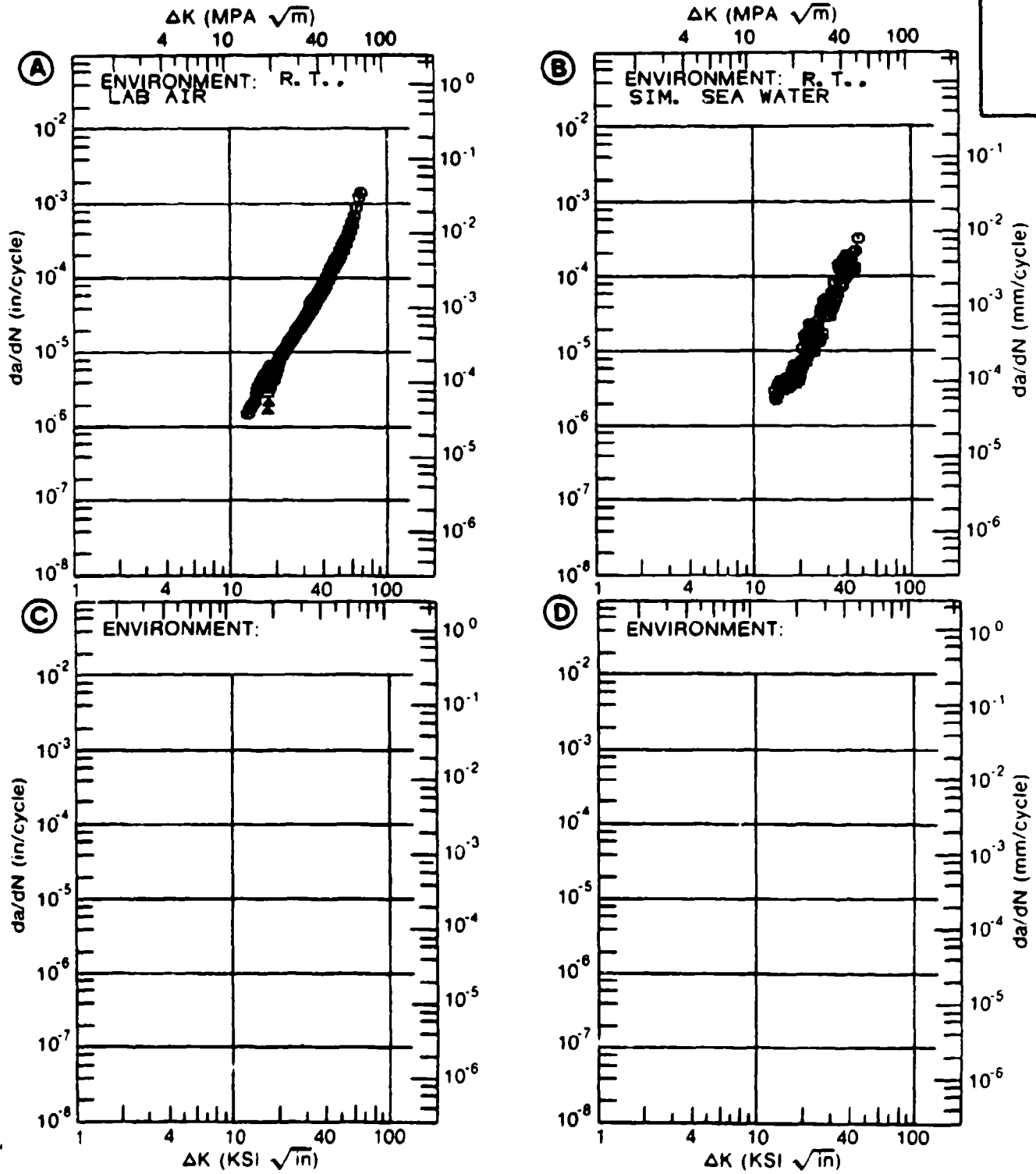


Figure 4.12.3.17

TABLE 4.12.3.18

| CONDITION | --PRODUCT-- | | TEST TEMP OR (F) | SPEC YIELD STR (KSI) | ENVIRONMENT | TITANIUM | | TI-6AL-4V(ELI) K(IISCC) | | STAN DEV | TEST TIME (MIN) | DATE PEFER |
|-----------------------|-------------|------------|------------------|----------------------|---------------|------------|------------|-------------------------|-------------|----------|-----------------|------------|
| | FORM | THICK (IN) | | | | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | | | |
| 100%F 1HR HELIUM COOL | F | 1.00 | R.T | 115.2 | 3.5 PCT NAACL | 1.000 | 0.500 | CANT* | 112.00 | 84.00* | | 1967 70931 |

*NOTE--DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5 (KIBCC/TYB)SQUARED

TABLE 4.13.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY Ti-6Al-6V-2Sn AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | | (NUMBER OF SPECIMENS) | |
|--|---|----------------|-----------------------|-----|
| | L-I | H-I | L-I | H-I |
| BETA ANNEAL 1810F 1 HR. ARGON COOL | --- | 54.3 ± 2.0 (3) | --- | --- |
| BETA ANNEAL & STDA-1600F 0.5HR.AC. 1975F 0.5HR.WG. 1050F 8 HR.AC | 50.1 ± 1.8 (2) | --- | --- | --- |
| DUPLEX ANNEAL | --- | 65.1 ± 2.0 (3) | --- | --- |
| MILL ANNEALED | --- | 39.0 ± 3.2 (4) | --- | --- |
| BTA-1675F 0.25 HR.WG. *100F 4 HR | --- | 34.1 ± 3.8 (3) | --- | --- |
| STDA-1700F 1 HR.WG. 1400F 1 HR.AC | 42.9 ± 1.2 (3) | 46.1 ± 3.1 (4) | --- | --- |
| FORGING | | | | |
| MILL ANNEALED | L-I | H-I | L-I | H-I |
| BTA-1600F 0.5HR.WG. 1000F 6 HR.AC | 38.6 ± 2.7 (3) | --- | --- | --- |
| | 30.8 ± 0.7 (3) | --- | --- | --- |

TABLE 4.13.1.1 (Con't)

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY TI-6AL-6V-2SN AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | | (NUMBER OF SPECIMENS) | |
|---|---|----------------|-----------------------|-----|
| | L-I | I-L | L-I | I-L |
| MILL ANNEALED | 32.3 ± 6.4 (4) | --- | --- | 8-L |
| MILL ANNEALED 1000F 2 HR. AC | 57.1 ± 2.2 (2) | --- | --- | --- |
| STDA-1700F 1 HR. WQ. 1400F 1 HR. AC | 62.8 ± 6.9 (4) | 57.0 ± 3.7 (4) | --- | --- |

TABLE 4.13.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

TEST CONDITIONS

SPECIMEN ORIENTATION L-S

ENVIRONMENT H H A
A T R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2 | 5 | 10 | 20 | 50 | 100 |
|--------------|--------------|--------------|-----------|-------------------------------|---|---|------|------|----|-----|
| STDA | PLATE | 0.10 | 0.10 | | | | 1.73 | 10.2 | | |
| STDA | PLATE | 0.10 | 10.00 | | | | 2.58 | 9.03 | | |

TABLE 4.13.1.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT H M A
A T R T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-----------|-------------------------------|-----|------|------|------|-----|-----|---|
| STOA | PLATE | 0.10 | 1.00 | | | | 1.64 | 15.1 | 396 | | |
| STOA | PLATE | 0.10 | 20.00 | | | 0.11 | 1.76 | 13.4 | | | |

TABLE 4.13.1.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT 3.5% NaCl AT R.T.

| CONDITION/MT | PRODUCT FORM | STRESS RATIO | FREQ. (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|-----|------|------|------|------|-----|---|
| STDA | PLATE | 0.10 | 1.00 | | | | 2.35 | 38.4 | 2560 | | |
| STDA | PLATE | 0.10 | 20.00 | | | 0.23 | 3.13 | 19.3 | | | |

TABLE 4.13.1.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

TEST CONDITIONS

SPECIMEN ORIENTATION T-S

ENVIRONMENT

M.H.A.
A.R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | 2.5 | 5 | 10 | 20 | 50 | 100 | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|-----------|-------------------------------|-----|---|------|------|----|-----|---|
| STDA | PLATE | 0.10 | 0.10 | | | | 1.15 | 41.6 | | | |
| STDA | PLATE | 0.50 | 0.10 | | | | 2.67 | 63.9 | | | |

TABLE 4.13.1.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

TEST CONDITIONS

SPECIMEN ORIENTATION T-S

ENVIRONMENT 3.5% NaCl AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) |
|--------------|--------------|--------------|------------|-------------------------------|---|
| | | | | 2.5 | 5 |
| | | | | 10 | 20 |
| | | | | 50 | 100 |
| BA | PLATE | 0.10 | 0.10-10.00 | | 1.31 |
| ST0A | PLATE | 0.10 | 1.00 | | 1.49 92.1 |

TABLE 4.13.1.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR

TITANIUM TI-6AL-6V-2SN

IFSI CONDITIONS

SPECIMEN ORIENTATION T-L

ENVIRONMENT HUMID AIR AT R.T

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS: (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICRO IN/CYCLE) | | | | | |
|--------------|--------------|--------------|-----------|--------------------------------|---|------|------|------|------|-----|
| | | | | | 2.5 | 5 | 10 | 20 | 50 | 100 |
| STOA | PLATE | 0.10 | 10.00 | | | | 2.16 | 12.4 | | |
| STOA | PLATE | 0.10 | 10.00 | | | | 0.73 | 5.98 | 42.3 | |
| STOA | PLATE | 0.50 | 10.00 | | | 0.33 | 2.38 | 49.5 | | |

TABLE 4.13.2.1

| TITANIUM | | TI-6AL-6V-2SN | | K(IIC) | | | | | | | | | | | | | |
|--|------|---------------|----------|----------------------|----------------------|------------|------------|-------------------|--|-------------------------------|-----------------|-------|-------|-------------|------|-------|-------|
| CONDITION | FORM | THICK (IN) | TEMP (F) | TEST SPECIMEN ORIENT | YIELD STRENGTH (KSI) | SPECIMEN | | CRACK LENGTH (IN) | 2.5 ^a CRACK (K(IIC)/YB) **2 | K(IIC) MEAN DEV (KSI*SQRT IN) | M(IIC) STAN DEV | DATE | REFER | | | | |
| | | | | | | WIDTH (IN) | THICK (IN) | | | | | | | DESIGN (IN) | | | |
| ANNEAL-COARSE GRAIN-1350F 2 HR.AC | F | 1 00 | R.T. | --- | 143 0 | 2 000 | 1 000 | CT | 1 000 | 75 60 | 0 70 | 1974 | 88962 | | | | |
| | | | | | | | | | | 143 0 | 1 000 | CT | 1 000 | 0 52 | 1974 | 88962 | |
| | | | | | | | | | | 143 0 | 2 000 | 1 000 | CT | 1 000 | 0 48 | 1974 | 88962 |
| | | | | | | | | | | 143 0 | 2 000 | 1 000 | CT | 1 000 | 0 52 | 1974 | 88962 |
| ANNEAL-FINE GRAIN-1350F 2 HR.AC | F | 6 00 | R.T. | --- | 148 0 | 2 000 | 1 000 | CT | 1 000 | 54 40 | 0 34 | 1974 | 88962 | | | | |
| | | | | | | | | | | 148 0 | 2 000 | 1 000 | CT | 1 000 | 0 36 | 1974 | 88962 |
| | | | | | | | | | | 148 0 | 2 000 | 1 000 | CT | 1 000 | 0 32 | 1974 | 88962 |
| | | | | | | | | | | 148 0 | 2 000 | 1 000 | CT | 1 000 | 0 34 | 1974 | 88962 |
| ANNEALCD 40-50 40-50% PRIMARY ALPHA ANNEALED 1350F 2 HR.AC | F | 2 50 | R.T. | --- | 149 0 | 2 000 | 1 000 | CT | 1 000 | 50 40 | 0 30 | 1974 | 88962 | | | | |
| | | | | | | | | | | 149 0 | 2 000 | 1 000 | CT | 1 000 | 0 31 | 1974 | 88962 |
| | | | | | | | | | | 149 0 | 2 000 | 1 000 | CT | 1 000 | 0 26 | 1974 | 88962 |
| | | | | | | | | | | 149 0 | 2 000 | 1 000 | CT | 1 000 | 0 28 | 1974 | 88962 |
| 88. AB FIN-10 BETA BLOCKED. ALPHA-BETA FINISHED. 10% REDUCTION. SOLUTION TREATED & OVERAGED. 1650F 1 HR. W3. 1300F 2 HR.AC | F | 2 50 | R.T. | --- | 148 0 | 2 000 | 1 000 | CT | 1 000 | 48 10 | 0 54 | 1974 | 88962 | | | | |
| | | | | | | | | | | 148 0 | 2 000 | 1 000 | CT | 1 000 | 0 67 | 1974 | 88962 |
| | | | | | | | | | | 147 0 | 2 000 | 1 000 | CT | 1 000 | 0 67 | 1974 | 88962 |
| | | | | | | | | | | 147 0 | 2 000 | 1 000 | CT | 1 000 | 0 60 | 1974 | 88962 |
| 88. AB FIN-10MA BETA BLOCKED. ALPHA-BETA FINISHED 10% REDUCTION. MILL ANNEALED 1300F 2 HR.AC | F | 2 50 | R.T. | --- | 147 0 | 2 000 | 1 000 | CT | 1 000 | 84 70 | 0 83 | 1974 | 88962 | | | | |
| | | | | | | | | | | 147 0 | 2 000 | 1 000 | CT | 1 000 | 0 60 | 1974 | 88962 |
| | | | | | | | | | | 147 0 | 2 000 | 1 000 | CT | 1 000 | 0 60 | 1974 | 88962 |
| | | | | | | | | | | 147 0 | 2 000 | 1 000 | CT | 1 000 | 0 60 | 1974 | 88962 |

TABLE 4.13.2.1 (Con't)

| CONDITION | TITANIUM | | TI-6AL-6V-2SN | | K(1C) | | YIELD STRENGTH (KSI) | WIDTH (IN) | THICKNESS (IN) | DESIGN | CRACK LENGTH (IN) | 2.9% K(1C)/TVB**2 (IN) | K(1C) MEAN (MSE) (IN) | K(1C) STAN DEV | DATE | REFER |
|--|----------|----------------|---------------|-----------|---------------|-------|----------------------|------------|----------------|--------|-------------------|------------------------|-----------------------|----------------|------|-------|
| | FORM | THICKNESS (IN) | ORIENT | REDUCTION | MILL ANNEALED | 1350F | | | | | | | | | | |
| RB, AB FIN-10MA BETA BLOCKED, ALPHA-BETA FINISHED | F | 2.50 | R.T. | 147.0 | 2.000 | 1.000 | CT | 1.000 | 0.64 | 74.60 | 77.0/ | 6.8 | | | 1974 | 88962 |
| RB, AB FIN-30 BETA BLOCKED, ALPHA-BETA FINISHED, 30% REDUCTION, SOLUTION TREATED & OVERAGED, 1650F 1 HR, NO. 1350F 2 HR.AC | F | 2.50 | R.T. | 148.0 | 2.000 | 1.000 | CT | 1.000 | 0.47 | 64.30 | | | | | 1974 | 88962 |
| RB, AB FIN-30MA BETA BLOCKED, ALPHA-BETA FINISHED, 30% REDUCTION, MILL ANNEALED 1350F 2 HR.AC | F | 2.50 | R.T. | 143.0 | 2.000 | 1.000 | CT | 1.000 | 0.49 | 64.40 | | | | | 1974 | 88962 |
| RB, AB FIN-10 BETA BLOCKED, ALPHA-BETA FINISHED, 10% REDUCTION, SOLUTION TREATED & OVERAGED, 1650F 1 HR, NO. 1350F 2 HR.AC | F | 2.50 | R.T. | 140.0 | 2.000 | 1.000 | CT | 1.000 | 0.69 | 73.60 | | | | | 1974 | 88962 |
| RB, B FIN-10MA BETA BLOCKED, ALPHA-BETA FINISHED, 10% REDUCTION, MILL ANNEALED 1350F 2 HR.AC | F | 2.50 | R.T. | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.66 | 69.70 | | | | | 1974 | 88962 |
| RB, B FIN-10MA BETA BLOCKED, ALPHA-BETA FINISHED, 10% REDUCTION, MILL ANNEALED 1350F 2 HR.AC | F | 2.50 | R.T. | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.66 | 70.20 | | | | | 1974 | 88962 |
| BETA ANNEAL | P | 1.00 | R.T. | 138.4 | 2.500 | 1.000 | WDL | | 0.73 | 74.60 | | | | | 1977 | JEM01 |
| BETA ANNEAL 1810F 1 HR, ARGON COOL | P | 0.50 | R.T. | 139.8 | 1.000 | 0.447 | CT | 0.348 | 0.36 | 53.20 | | | | | 1971 | 83222 |
| | | 0.50 | | 139.8 | 1.000 | 0.447 | CT | 0.313 | 0.41 | 56.60 | | | | | 1971 | 83222 |
| | | 0.50 | | 139.8 | 1.000 | 0.446 | CT | 0.358 | 0.36 | 53.00 | | | | | 1971 | 83222 |

TABLE 4.13.2.1 (Con't)

| CONDITION | --PRODUCT-- | | TEST SPECIMEN | | YIELD | | WIDTH | | THICKNESS | | DESIGN LENGTH | | CRACK | | K(IIC) STAN | | DATE | REFER |
|---|-------------|------------|---------------|--------|----------------|-------|-------|-----|-----------|------|---------------|------|-------|------|-------------|-----------------|------|-------|
| | FORM | THICK (IN) | THICK (IN) | ORIENT | STRENGTH (KSI) | (IN) | (IN) | M | B | A | (IN) | (IN) | (IN) | (IN) | (KSI) | (IN) | | |
| BETA ANNEAL & STAID-1800F | P | 0.62 | R T | L-T | 156.0 | 2.000 | 0.626 | CT | 1.000 | 0.27 | 51.30 | | | | | 1974 88186 | | |
| 0 5HR. AC. 1575F 0 5HR. WQ. 1050F 8 HR. AC | | 0.62 | | | 156.0 | 2.000 | 0.626 | CT | 1.000 | 0.24 | 48.80 | | | | 50.1/ 1.8 | 1974 88186 | | |
| RF. B FOR-ANN | F | 2.50 | R T | --- | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.73 | 74.50 | | | | | 1974 88962 | | |
| BETA FLECTED. | | 2.50 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.82 | 79.30 | | | | | 1974 88962 | | |
| ALPHA-BETA FORGED. ANNEALED. 1350F 2 HR. AC | | 2.50 | | | 138.0 | 2.000 | 1.000 | CT | 1.000 | 0.68 | 72.10 | | | | 73.3/ 3.7 | 1974 88962 | | |
| RF. B FOR-ANN | F | 2.50 | R T | --- | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.74 | 73.90 | | | | | 1974 88962 | | |
| BETA FLECTED. | | 2.50 | | | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.74 | 73.80 | | | | | 1974 88962 | | |
| BETA FORGED. ANNEALED 1350F 2 HR. AC | | 2.50 | | | 136.0 | 2.000 | 1.000 | CT | 1.000 | 0.75 | 74.70 | | | | 74.1/ 0.5 | 1974 88962 | | |
| DF. LAB FOR-ANN | F | 2.50 | R T | --- | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.42 | 58.10 | | | | | 1974 88962 | | |
| BETA FLECTED. | | 2.50 | | | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.38 | 55.20 | | | | | 1974 88962 | | |
| LOW ALPHA-BETA FORGED(11500F). ANNEALED. 1350F 2 HR. AC | | 2.50 | | | 141.0 | 2.000 | 1.000 | CT | 1.000 | 0.39 | 55.70 | | | | 36.3/ 1.6 | 1974 88962 | | |
| DUPLEX ANNEAL | P | 0.50 | R T | T-L | 150.5 | 2.000 | 0.500 | CT | 0.988 | 0.44 | 64.50 | | | | | 1971 83222 (1) | | |
| | | 0.50 | | | 150.5 | 2.000 | 0.500 | CT | 1.078 | 0.44 | 63.50 | | | | | 1971 83222 (1) | | |
| | | 0.50 | | | 150.5 | 2.000 | 0.495 | CT | 1.056 | 0.50 | 67.40 | | | | 65.1/ 2.0 | 1971 83222 (1) | | |
| MILL ANNEALED | P | 2.00 | R T | --- | 157.0 | 2.500 | 1.250 | CT | 1.250 | 0.18 | 42.30 | | | | | 1973 90384 (2) | | |
| | | 2.00 | | | 157.0 | 2.500 | 1.250 | CT | 1.250 | 0.18 | 42.30 | | | | 42.3/ 0.0 | 1973 90384 (2) | | |
| MILL ANNEALED | P | 1.00 | R T | T-L | 151.3 | 2.500 | 1.000 | WQL | --- | 0.20 | 42.80 | | | | | 1977 JEN01 | | |
| | | 0.50 | | | 163.3 | 1.000 | 0.495 | CT | 0.522 | 0.09 | 32.00 | | | | | 1971 83222 | | |
| | | 0.50 | | | 163.3 | 1.000 | 0.494 | CT | 0.537 | 0.09 | 32.10 | | | | | 1971 83222 | | |

NOTES

- (1) 1700F 1 HR. ARGON COOL. 1400F 1 HR. ARGON COOL
- (2) COMPOSITION(WT PERCENT) 5 GAL. 5 4V. 2 OSN. 0 026C. 0 37FE. 0 014N. 0 084H. 0 180. 0 50CU

TABLE 4.13.2.1 (Con't)

| CONDITION | TITANIUM | | YIELD STRENGTH (KSI) | TEST SPECIMEN ORIENT | THICKNESS (IN) | TEMP (F) | WIDTH (IN) | THICKNESS (IN) | DESIGN | CRACK LENGTH (IN) | 2.5* K(1C)/TVS**2 (IN) | K(1C) MEAN DEV (ABS) (IN) | K(1C) STAN DEV | DATE | REFER |
|-----------------|----------|----------|----------------------|----------------------|----------------|----------|------------|----------------|--------|-------------------|------------------------|---------------------------|----------------|------|-------|
| | FORM | W | | | | | | | | | | | | | |
| MILL ANNEALED | P | 0.50 | 163.3 | T-L | 1.000 | R.T. | 0.495 | CT | 0.517 | 0.10 | 33.20 | 35.07 | 5.2 | 1971 | 83222 |
| MILL ANNEALED | F | --- | 144.0 | -- | 2.500 | R.T. | 1.250 | CT | 1.250 | 0.37 | 35.70 | 35.70 | 0.1 | 1973 | 90584 |
| MILL ANNEALED | F | 3.80 | 165.0 | L-T | 2.502 | 65 | 1.007 | CT | 1.312 | 0.19 | 47.70 | 47.70 | 5.7 | 1973 | 90589 |
| | | 3.80 | 169.0 | | 2.498 | | 1.008 | CT | 1.299 | 0.19 | 37.60 | 37.60 | | 1973 | 90589 |
| | | 3.00 | 169.0 | | 2.503 | | 1.003 | CT | 1.297 | 0.12 | 44.20 | 44.20 | | 1973 | 90589 |
| MILL ANNEALED | F | 3.80 | 149.0 | L-T | 2.499 | R.T. | 0.999 | CT | 1.299 | 0.43 | 61.70 | 61.70 | 2.7 | 1973 | 90589 |
| | | 3.80 | 149.0 | | 2.501 | | 1.006 | CT | 1.300 | 0.36 | 56.90 | 56.90 | | 1973 | 90589 |
| | | 3.00 | 149.0 | | 2.495 | | 0.995 | CT | 1.301 | 0.37 | 57.30 | 57.30 | | 1973 | 90589 |
| MILL ANNEALED | FB | 1.50 | 153.0 | -- | 2.500 | R.T. | 1.250 | CT | 1.250 | 0.20 | 43.10 | 43.10 | | 1973 | 90584 |
| MILL ANNEALED | BT | 2.20 | 144.0 | L-T | 2.500 | R.T. | 1.251 | CT | 1.332 | 0.37 | 55.60 | 55.60 | 6.4 | 1971 | 84360 |
| | | 2.20 | 144.0 | | 2.507 | | 1.243 | CT | 1.262 | 0.42 | 58.90 | 58.90 | | 1971 | 84360 |
| | | 2.20 | 146.0 | | 2.500 | | 1.243 | CT | 1.216 | 0.30 | 50.40 | 50.40 | | 1971 | 84360 |
| | | 2.20 | 146.0 | | 2.495 | | 1.253 | CT | 1.297 | 0.23 | 44.30 | 44.30 | | 1971 | 84360 |
| MILL ANNEALED | RT | 2.20 | 155.0 | L-T | 2.495 | R.T. | 1.235 | CT | 1.295 | 0.32 | 55.50 | 55.50 | 2.2 | 1971 | 84360 |
| 1000F 2 HR. AC | | 2.20 | 155.0 | | 2.500 | | 1.234 | CT | 1.234 | 0.36 | 58.60 | 58.60 | | 1971 | 84360 |
| RECRYSTALLIZE | P | 1.00 | 150.0 | T-L | 2.550 | R.T. | 1.000 | MOL | ---- | 0.45 | 63.70 | 63.70 | | 1977 | JEM01 |
| ANNEAL | | | | | | | | | | | | | | | |
| STA-1600F | F | 3.80 | 209.0 | L-T | 2.474 | 65 | 1.010 | CT | 1.326 | 0.05 | 20.70 | 20.70 | 0.6 | 1973 | 90589 |
| 0 HR. MO. 1000F | | 3.80 | 209.0 | | 2.499 | | 1.005 | CT | 1.267 | 0.05 | 28.80 | 28.80 | | 1973 | 90589 |
| 6 HR. AC | | 3.00 | 209.0 | | 2.476 | | 1.007 | CT | 1.283 | 0.04 | 27.80 | 27.80 | | 1973 | 90589 |
| STA-1600F | F | 3.80 | 184.0 | L-T | 2.478 | R.T. | 1.005 | CT | 1.290 | 0.07 | 31.40 | 31.40 | 0.7 | 1973 | 90589 |
| 0 HR. MO. 1000F | | 3.80 | 184.0 | | 2.502 | | 1.006 | CT | 1.296 | 0.07 | 30.20 | 30.20 | | 1973 | 90589 |
| 6 HR. AC | | 3.80 | 184.0 | | 2.501 | | 1.007 | CT | 1.278 | 0.07 | 30.60 | 30.60 | 0.7 | 1973 | 90589 |
| STA-1600F | F | 3.80 | 165.0 | L-T | 2.501 | 300 | 1.001 | CT | 1.292 | 0.28 | 55.50 | 55.50 | | 1973 | 90589 |
| 0 HR. MO. 1000F | | 6 HR. AC | | | | | | | | | | | | | |

TABLE 4.13.2.1 (Con't)

| CONDITION | TITANIUM | | | | | | | | | | K(IIC) STAN | DATE | REFER |
|--|-----------|------------|---------------|------------|-------------|------------|------------|-------------|-----------------|----------------------|-------------|----------------|-------|
| | --PRIMA-- | | TEST SPECIMEN | | SPECIMEN | | CRACK | | K(IIC) MEAN DEV | | | | |
| | FORM | THICK (IN) | THICK (IN) | ORIENT (I) | YIELD (KSI) | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | (K(IIC)/TYS)**2 (IN) | | | |
| STA-1650F 0.5HR. WQ. 1000F 6 HR. AC | F | 3.00 | 300 | L-T | 165.0 | 2.497 | 1.015 | CT | 1.278 | 0.27 | 54.20 | 1973 90589 | |
| | | 3.00 | | | 165.0 | 2.479 | 1.009 | CT | 1.272 | 0.22 | 47.40 | 1973 90589 | |
| STA-1650F 0.5HR. WQ. 1000F 24 HR. AC | F | | R.T. | L-C | 188.0 | 0.998 | 0.500 | CT | 0.508 | 0.04 | 24.60 | 1972 86494 (1) | |
| | | | | | 188.0 | 0.994 | 0.500 | CT | 0.507 | 0.04 | 24.50 | 1972 86494 (1) | |
| | | | | | 188.0 | 0.997 | 0.498 | CT | 0.532 | 0.03 | 23.50 | 1972 86494 (1) | |
| | | | | | 188.0 | 1.000 | 0.499 | CT | 0.536 | 0.03 | 23.60 | 1972 86494 (1) | |
| STA-1650F 0.5HR. WQ. 1050F 24 HR. AC | F | | R.T. | C-L | 188.0 | 1.005 | 0.500 | CT | 0.517 | 0.06 | 29.10 | 1972 86494 (1) | |
| | | | | | 188.0 | 1.001 | 0.500 | CT | 0.523 | 0.05 | 29.60 | 1972 86494 (1) | |
| | | | | | 188.0 | 1.001 | 0.500 | CT | 0.505 | 0.05 | 29.30 | 1972 86494 (1) | |
| STA-1675F 0.25 HR. WQ. 1100F 4 HR | P | 1.25 | R.T. | T-L | 173.3 | 2.000 | 0.499 | CT | 1.080 | 0.11 | 37.00 | 1971 83222 | |
| | | 1.25 | | | 173.3 | 2.000 | 0.499 | CT | 1.138 | 0.07 | 29.80 | 1971 83222 | |
| | | 1.25 | | | 173.3 | 2.000 | 0.499 | CT | 1.046 | 0.10 | 33.50 | 1971 83222 | |
| STA-1600F 1 HR. WQ. 1200F 6 HR. AC | E | 3.00 | R.T. | C-R | 143.0 | 1.476 | 0.750 | CT | 0.779 | 0.36 | 54.20 | 1973 87230 (2) | |
| | | 3.00 | | | 143.0 | 1.408 | 0.750 | CT | 0.808 | 0.33 | 52.00 | 1973 87230 (2) | |
| | | 3.00 | | | 143.0 | 1.499 | 0.749 | CT | 0.783 | 0.34 | 54.50 | 1973 87230 (2) | |
| STA-1650F 1 HR. WQ. 1300F 2 HR. AC | F | 2.50 | R.T. | | 154.0 | 2.000 | 1.000 | CT | 1.000 | 0.18 | 41.60 | 1974 88962 | |
| | | 2.50 | | | 154.0 | 2.000 | 1.000 | CT | 1.000 | 0.17 | 40.40 | 1974 88962 | |
| STA-1700F 1 HR. WQ. 1400F 1 HR. AC | P | 0.38 | R.T. | L-T | 156.0 | 1.000 | 0.375 | CT | | 0.20 | 44.30 | 1974 90981 | |
| | | 0.38 | | | 156.0 | 1.000 | 0.375 | CT | | 0.18 | 41.90 | 1974 90981 | |
| | | 0.38 | | | 156.0 | 1.000 | 0.375 | CT | | 0.18 | 42.50 | 1974 90981 | |

NOTES
 (1) ISOTHERMAL FORGING FOR AIRCRAFT NOSE WHEEL
 (2) ALPHA PRECIPITATE IN BETA MATRIX
 STRAIGHTNESS OF CRACK FRONT MAY NOT MEET ASIN E399-72 REQUIREMENTS

TABLE 4.13.2.1 (Con't)

| CONDITION | TITANIUM | | | | | | | | | | K(IC) | | | | | |
|---|----------------|--------------------------------------|---------------|----------|---|---|---|----------------------------|---|--------------------------------------|---|--|------------|------|-------|-----|
| | ---PROBABLE--- | | TEST SPECIMEN | | YIELD | | SPECIMEN--- | | CRACK | | 2.9° | | K(IC) STAN | DATE | REFER | |
| | FORM | THICK (IN) | THICK (IN) | TEMP (F) | ORIENT | SIRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | LENGTH (IN) | K(IC)/TVB)*2 | K(IC) MEAN (KSI) (REPERT IN) | | | | DEV |
| | | | | | | | M | B | A | | | | | | | |
| ST0A-1700F 1 HR. HQ. 140HF 1 HR. AC | P | 0.38 0.38 0.38 | R. T. | T-I | 160.0 160.0 160.0 | 1.000 1.000 1.000 | 0.375 0.375 0.375 | CT CT CT | --- | 0.19 0.23 0.18 | 44.00 48.30 49.10 | 1974 90981 1974 90981 1974 90981 | 3.1 | | | |
| ST0A-1700F 1 HR. HQ. 140HF 1 HR. AC | BT | 12.00 12.00 12.00 | R. T. | L-I | 147.0 147.0 148.0 148.0 | 2.000 2.000 2.000 2.000 | 1.020 1.020 1.020 1.020 | NB NB NB NB | --- | 0.33 0.37 0.46 0.46 | 53.60 70.40 63.70 63.40 | 1974 90981 1974 90981 1974 90981 1974 90981 | 6.9 | | | |
| ST0A-1700F 1 HR. HQ. 140HF 1 HR. AC | BT | 12.00 12.00 12.00 | R. T. | T-I | 144.0 144.0 143.0 143.0 | 2.000 2.000 2.000 2.000 | 1.020 1.020 1.020 1.020 | NB NB NB NB | --- | 0.42 0.40 0.32 0.42 | 58.80 58.00 51.30 59.60 | 1974 90981 1974 90981 1974 90981 1974 90981 | 3.7 | | | |
| 1650F 1 HR. HQ. 1050F 1 HR. AC | F | 4.50 4.50 | --- | L-C | 270.0 270.0 | 0.501 0.978 | 0.250 0.501 | NB NB | 0.122 0.193 | 0.02 0.02 | 22.60 24.50 | 1965 84316 1965 84316 | 1.3 | | | |
| 1650F 1 HR. HQ. 1050F 1 HR. AC | F | 4.50 4.50 4.50 4.50 4.50 | R. T. | L-C | 184.0 184.0 184.0 184.0 184.0 | 0.978 0.978 0.501 0.251 0.502 | 0.501 0.501 0.251 0.502 0.250 | NB NB NB NB NB | 0.191 0.301 0.177 0.274 0.139 | 0.06 0.07 0.07 0.08 0.09 | 27.80 31.40 30.40 32.40 34.30 | 1965 84316 1965 84316 1965 84316 1965 84316 1965 84316 | 2.2 | | | |
| 1675F 2 HR. AC 1600F 1 HR. FC | P | 2.00 2.00 | R. T. | --- | 150.0 150.0 | 2.500 2.500 | 1.250 1.250 | CT CT | 1.250 1.250 | 0.34 0.30 | 55.00 52.50 | 1973 90384 (1) 1973 90384 (1) | 1.8 | | | |
| 1675F 2 HR. AC 1600F 1 HR. FC | F | --- | R. T. | --- | 138.0 138.0 | 2.500 2.500 | 1.250 1.250 | CT CT | 1.250 1.250 | 0.36 0.46 | 52.70 58.90 | 1973 90384 1973 90384 | 4.4 | | | |
| 1675F 2 HR. AC 1600F 1 HR. FC | FB | 1.50 1.50 | R. T. | --- | 150.0 150.0 | 2.500 2.500 | 1.250 1.250 | CT CT | 1.250 1.250 | 0.43 0.38 | 62.20 58.20 | 1973 90384 1973 90384 | 2.8 | | | |

NOTES
(1) COMPOSITION (WT PERCENT) 5.6AL, 3.4V, 2.0SN, 0.02AC, 0.57FE, 0.014N, 0.004H, 0.18D, 0.50CU

TABLE 4.13.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.1 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-6V-2SN
CONDITION: BA
ENVIRONMENT: R. T. , HUMID AIR

| DELTA K (KSI*IN**1/2) | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|---------------------------------------|---|---|---|
| | A | B | C | D |
| | R=+0.10 | | | |
| DELTA K A: | | | | |
| MIN B: | | | | |
| C: | | | | |
| D: | | | | |
| 200.00 : | | | | |
| DELTA K A: | | | | |
| MAX B: | | | | |
| C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 0.00
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., HUMID AIR

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.375"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90001

TITAN.
ALLOY

TI-6AL-
6V-2SN

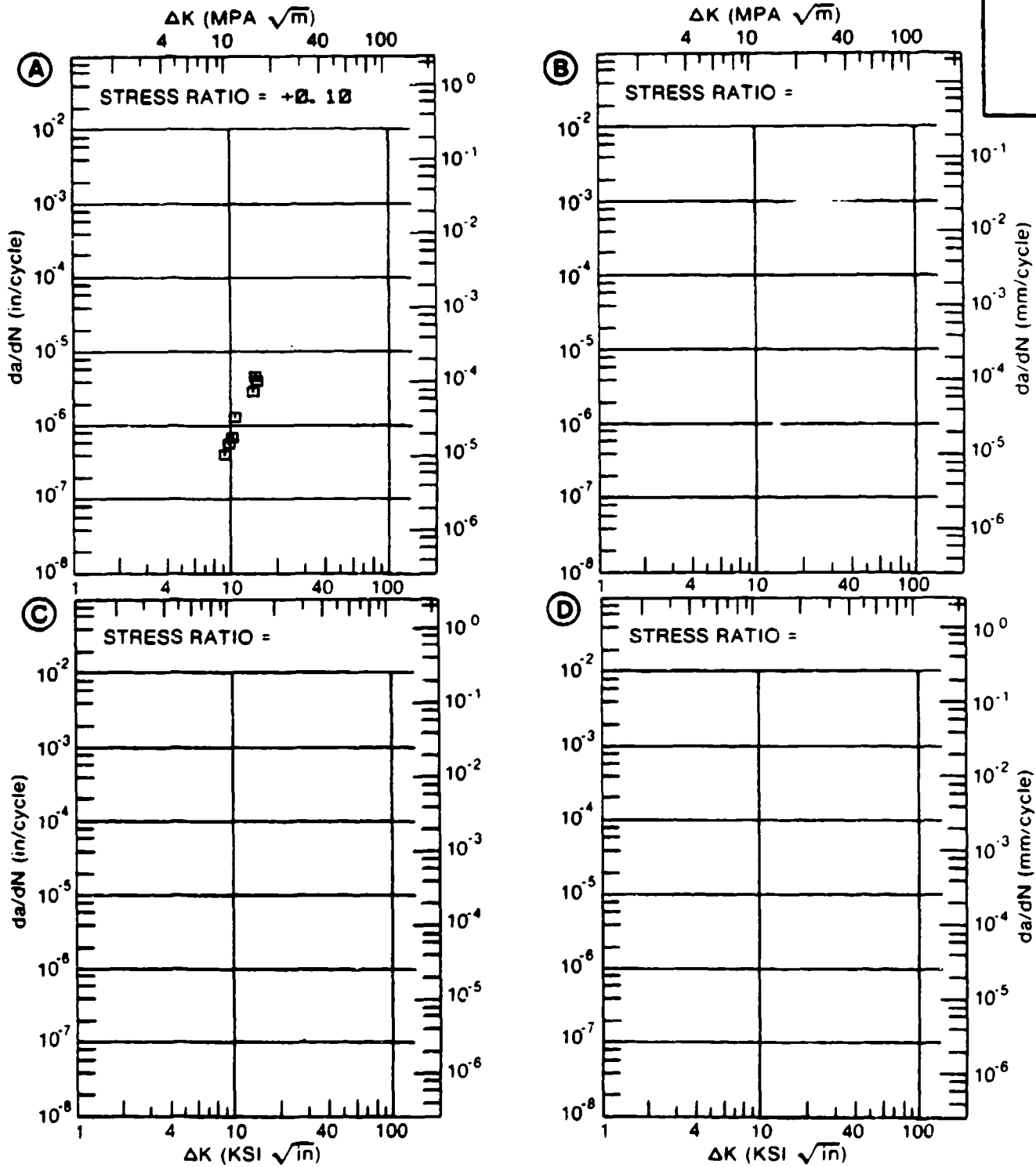


Figure 4.13.3.1

TABLE 4.13.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.2 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: BA

TI-6AL-6V-2SN

DELTA K
(KSI*IN**1/2)

DA/DN (10**⁻⁶ IN. /CYCLE)

A

B

C

D

E= R. T.
3.5% NAACL

DELTA K MIN
A: 8.91 : 1.38
B:
C:
D:

9.00 : 1.36
10.00 : 1.51
13.00 : 5.40
16.00 : 12.5

DELTA K MAX
A: 17.76 : 12.0
B:
C:
D:

ROOT MEAN SQUARE 27.07
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: BA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 STRESS RATIO: +0.10
 FREQUENCY: 0.10- 10.00 HZ

YIELD STRENGTH: 180.0 KSI
 ULT. STRENGTH: 188.0 KSI
 SPECIMEN THK: 0.375"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90001

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TI-6AL-
4V-2SN

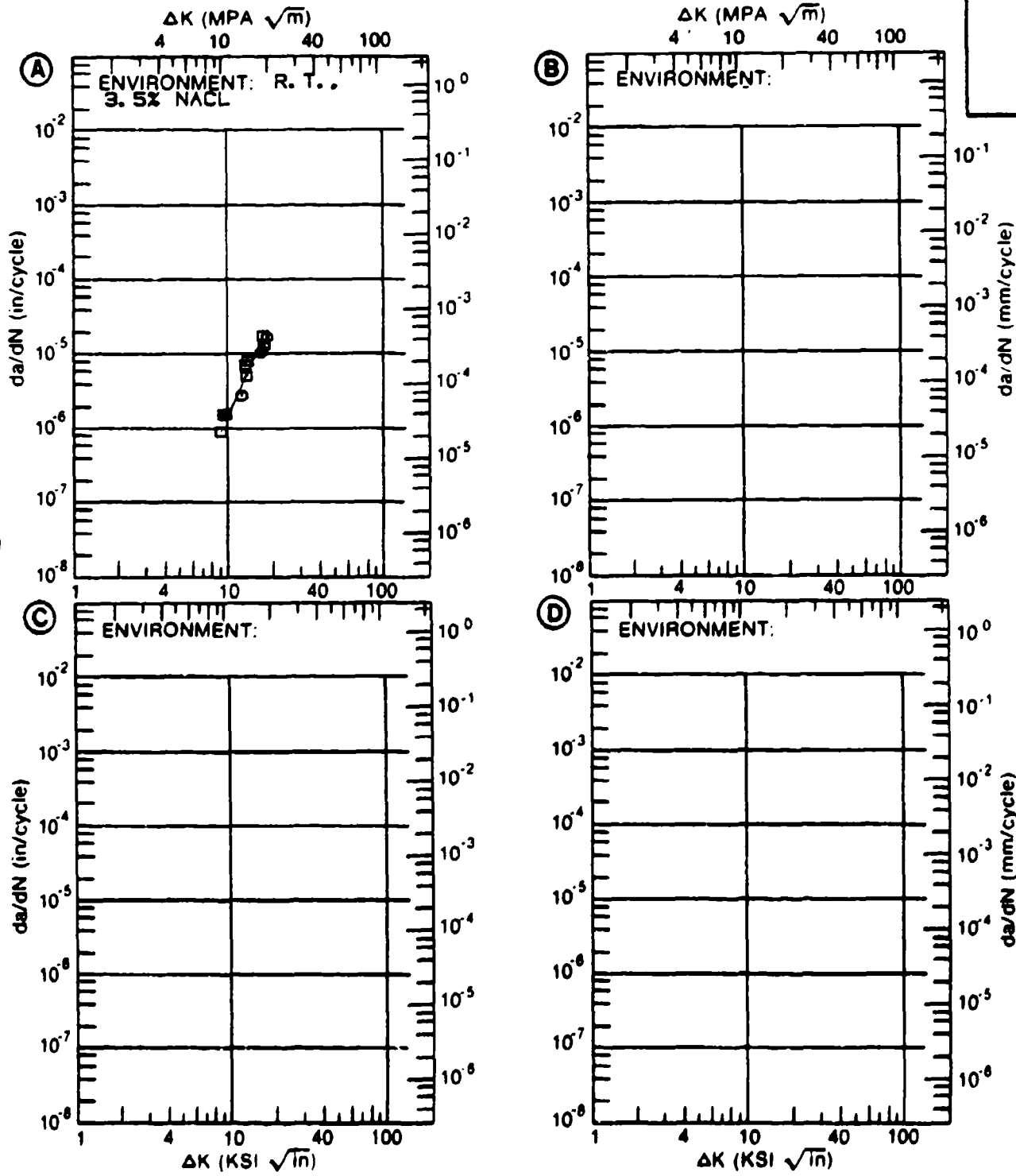


Figure 4.13.3.2

TABLE 4.13.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.3 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM
CONDITION: MA

TI-6AL-6V-2SN

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
|-----------------------------------|----------|--|--|------|---|
| | | A | B | C | D |
| | | E= R. T. INTERSTITIAL OXYGEN=0.08% | E= R. T. INTERSTITIAL OXYGEN=0.16% | | |
| DELTA K MIN | A: | 16.07 | 3.37 | | |
| | B: | 18.53 | | 8.57 | |
| | C: | | | | |
| | D: | | | | |
| | | 20.00 | 9.21 | 11.7 | |
| | | 25.00 | 17.8 | 30.7 | |
| | 30.00 | 26.7 | 66.7 | | |
| | 35.00 | 37.7 | | | |
| | 40.00 | 53.5 | | | |
| DELTA K MAX | A: | 49.10 | 112. | | |
| | B: | 31.63 | | 171. | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 5.19 | 12.71 | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM:
 SPECIMEN TYPE:
 ORIENTATION:
 STRESS RATIO:
 FREQUENCY:

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 91945

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TI-6AL-
 2V-2SN

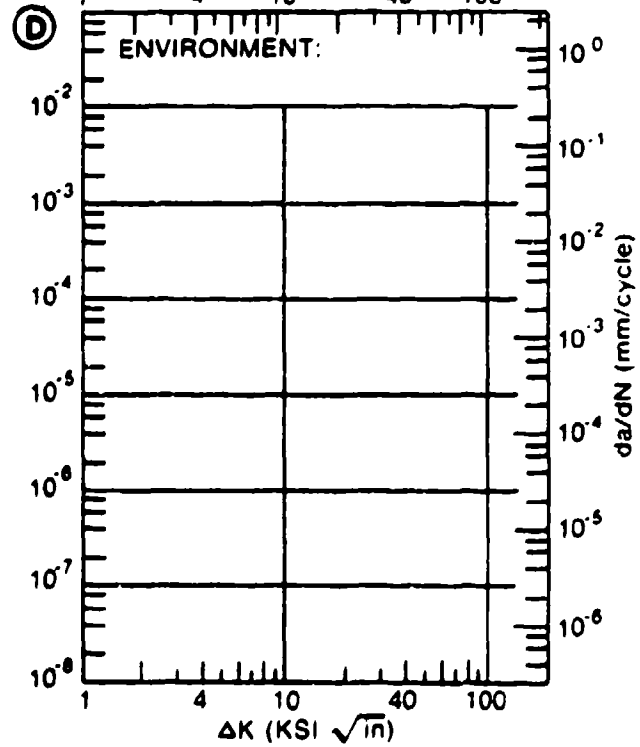
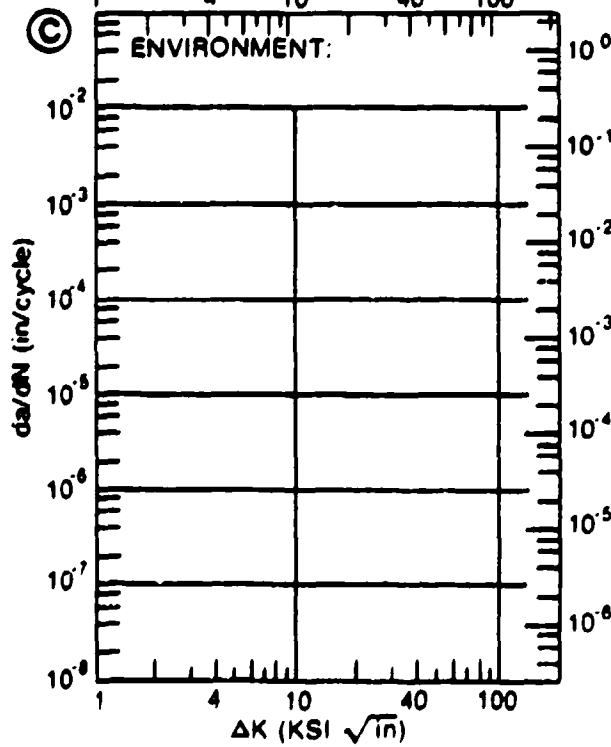
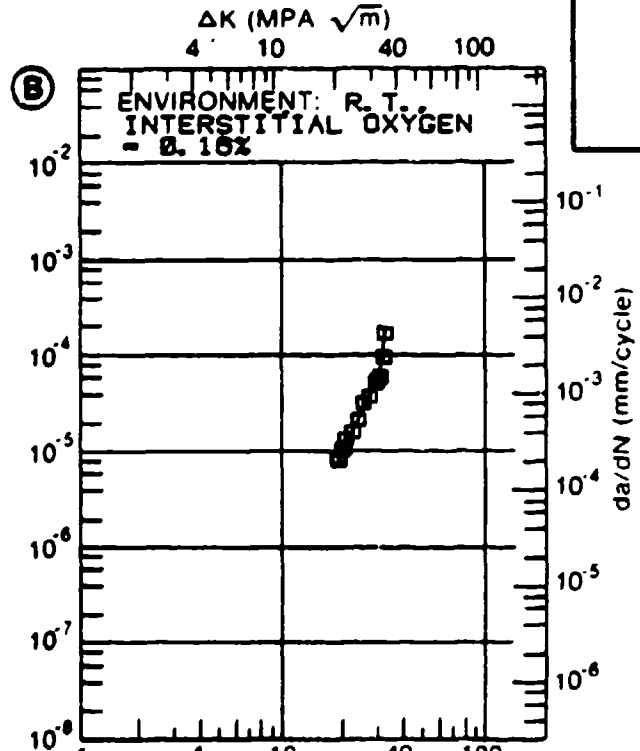
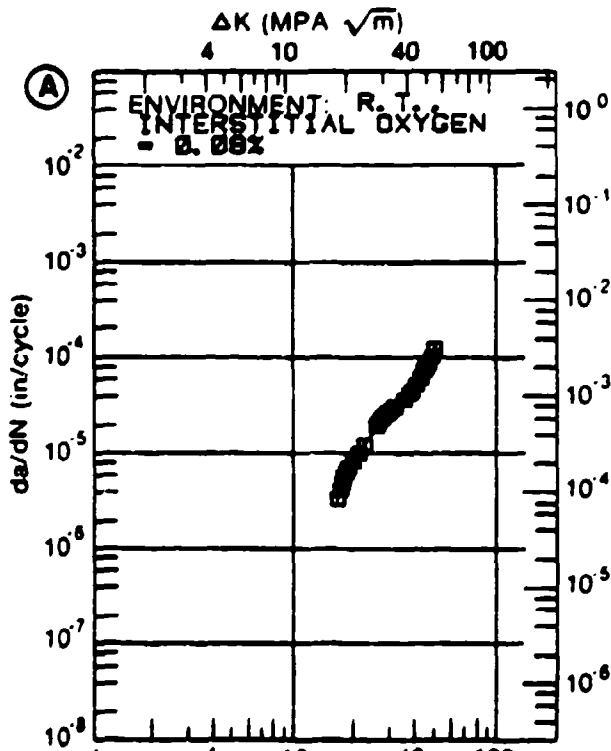


Figure 4.13.3.3

TABLE 4.13.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.4 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-6V-2SN
CONDITION: MA

| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
|--------------------------|----------|--------------------------|---|---|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | | | |
| DELTA K | A: 4.16 | .0207 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | .0440 | | | |
| | 6.00 | .0905 | | | |
| | 7.00 | .164 | | | |
| | 8.00 | .271 | | | |
| | 9.00 | .420 | | | |
| | 10.00 | .620 | | | |
| | 13.00 | 1.61 | | | |
| | 16.00 | 3.43 | | | |
| | 20.00 | 7.73 | | | |
| | 25.00 | 17.7 | | | |
| | 30.00 | 35.2 | | | |
| | 35.00 | 64.0 | | | |
| | 40.00 | 109. | | | |
| DELTA K | A: 41.81 | 130. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 19.73
PERCENT ERROR

| | | |
|------------|----------|---|
| LIFE | 0.0-0.5 | |
| PREDICTION | 0.5-0.8 | 1 |
| RATIO | 0.8-1.25 | 1 |
| SUMMARY | 1.25-2.0 | |
| (NP/NA) | >2.0 | |

CONDITION/HT: MA
 FORM: EXTRUSION
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 FREQUENCY: 0.10- 20.00 HZ

YIELD STRENGTH: 143.0 KSI
 ULT. STRENGTH: 157.0 KSI
 SPECIMEN THK: 0.001- 0.002"
 SPECIMEN WIDTH: 3.509- 3.519"
 REFERENCES: MA002

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4V-2SN

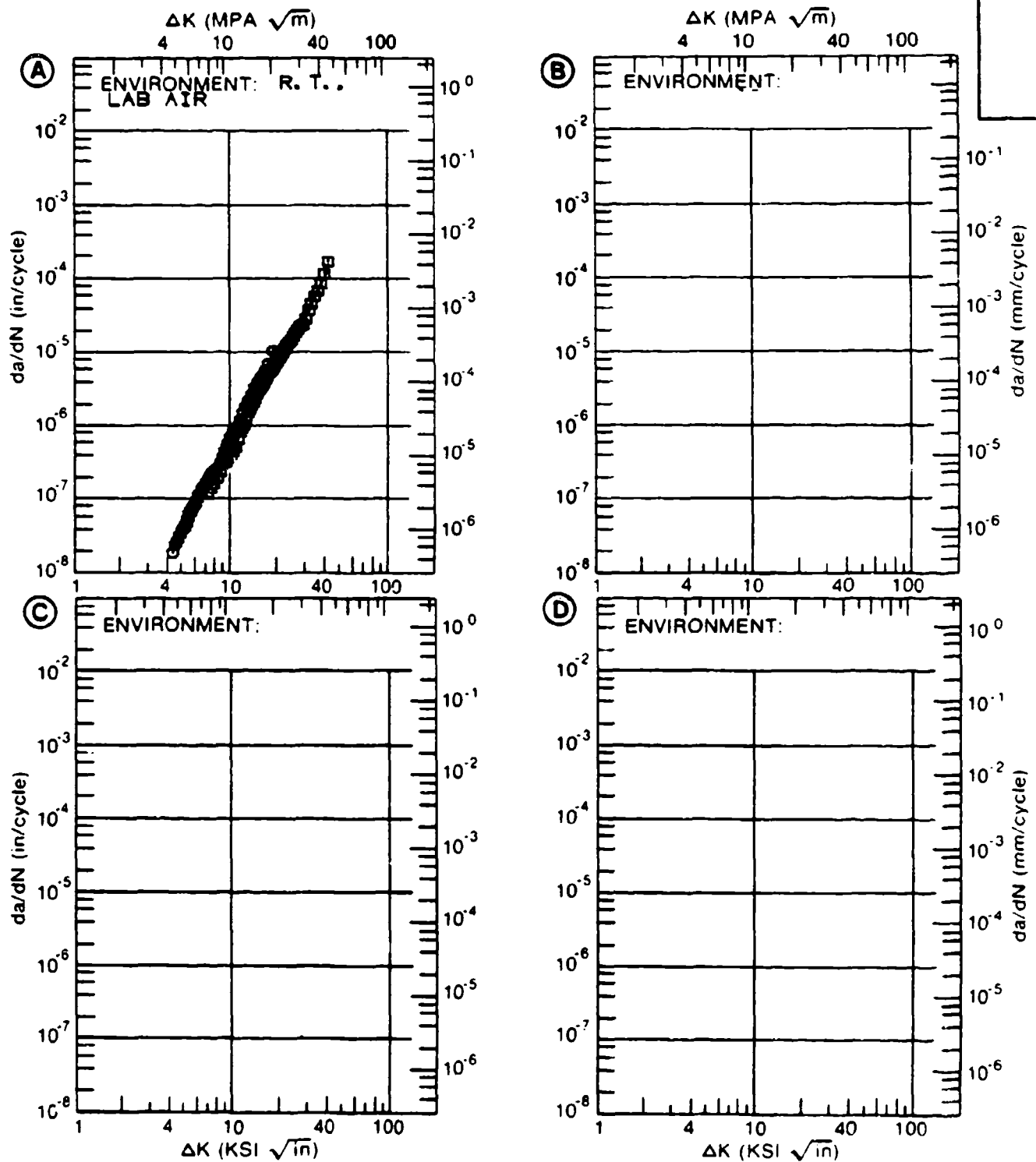


Figure 4.13.3.4

TABLE 4.13.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.5 INDICATING EFFECT

OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|--------------------------|----------|--------------------------|---------------------|-----------------------|-------------------------|
| CONDITION: MA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. DRY ARGON | E= R. T. DRY AIR | E= R. T. JP-4 FUEL | E= R. T. DIST. WATER |
| DELTA K | A: 13.02 | 4.85 | | | |
| MIN | B: 10.24 | | 1.28 | | |
| | C: 10.06 | | | 2.41 | |
| | D: 10.25 | | | | .93 |
| | 13.00 | | 3.53 | 5.70 | 2.36 |
| | 16.00 | 6.20 | 7.54 | 10.9 | 4.79 |
| | 20.00 | 10.3 | 11.1 | 22.4 | 9.77 |
| | 25.00 | 21.0 | 19.1 | 51.6 | 17.9 |
| | 30.00 | 40.9 | 48.9 | 118. | 36.9 |
| | 35.00 | 72.9 | 107. | 271. | 65.4 |
| | 40.00 | 120. | 164. | 632. | 113. |
| | 50.00 | 633. | 391. | | 322. |
| DELTA K | A: 55.28 | 911. | | | |
| MAX | B: 58.24 | | 1749. | | |
| | C: 42.78 | | | 1015. | |
| | D: 58.29 | | | | 747. |
| ROOT MEAN SQUARE | | 23.61 | 29.90 | 21.93 | 25.52 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 2.00" TH FORGING
 SPECIMEN TYPE: DCB
 ORIENTATION: L-T
 STRESS RATIO: +0.02
 FREQUENCY: 0.00- 10.00 HZ

YIELD STRENGTH: 144.0- 155.0 KSI
 ULT. STRENGTH: 151.0- 164.0 KSI
 SPECIMEN THK: 0.750"
 SPECIMEN WIDTH: 5.500"
 REFERENCES: 04300

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TI-6AL-
6V-2SN

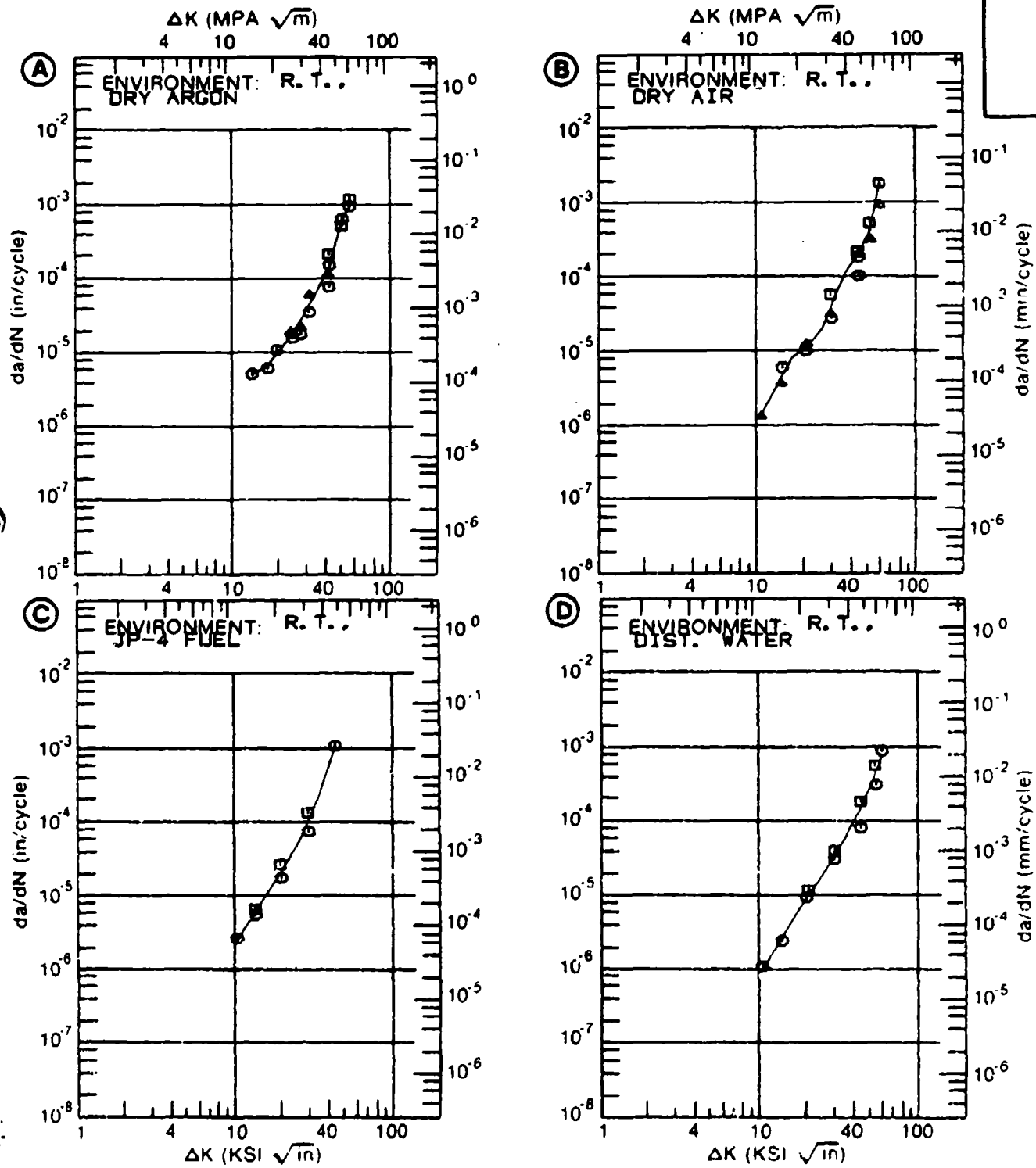


Figure 4.13.3.5

TABLE 4.13.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.6 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|--------------------------|----------|--|--|---|---|
| CONDITION: RA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. INTERSTITIAL OXYGEN=0.08% | E= R. T. INTERSTITIAL OXYGEN=0.16% | | |
| DELTA K MIN | A: 18.44 | 4.64 | | | |
| | B: 21.24 | | 10.6 | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 6.36 | | | |
| | 25.00 | 13.6 | 23.7 | | |
| | 30.00 | 23.0 | 47.1 | | |
| | 35.00 | 34.8 | 72.4 | | |
| | 40.00 | 49.3 | 96.3 | | |
| | 50.00 | 86.0 | | | |
| DELTA K MAX | 60.00 | 125. | | | |
| | 70.00 | 154. | | | |
| | 80.00 | 176. | | | |
| | 90.00 | 195. | | | |
| | A: 91.66 | 199. | | | |
| B: 48.09 | | 129. | | | |
| C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 10.65 | 7.01 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: RA
 FORM:
 SPECIMEN TYPE:
 ORIENTATION:
 STRESS RATIO:
 FREQUENCY:

YIELD STRENGTH:
 ULT. STRENGTH:
 SPECIMEN THK:
 SPECIMEN WIDTH:
 REFERENCES: 91845

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TI-6AL-
 2V-2SN

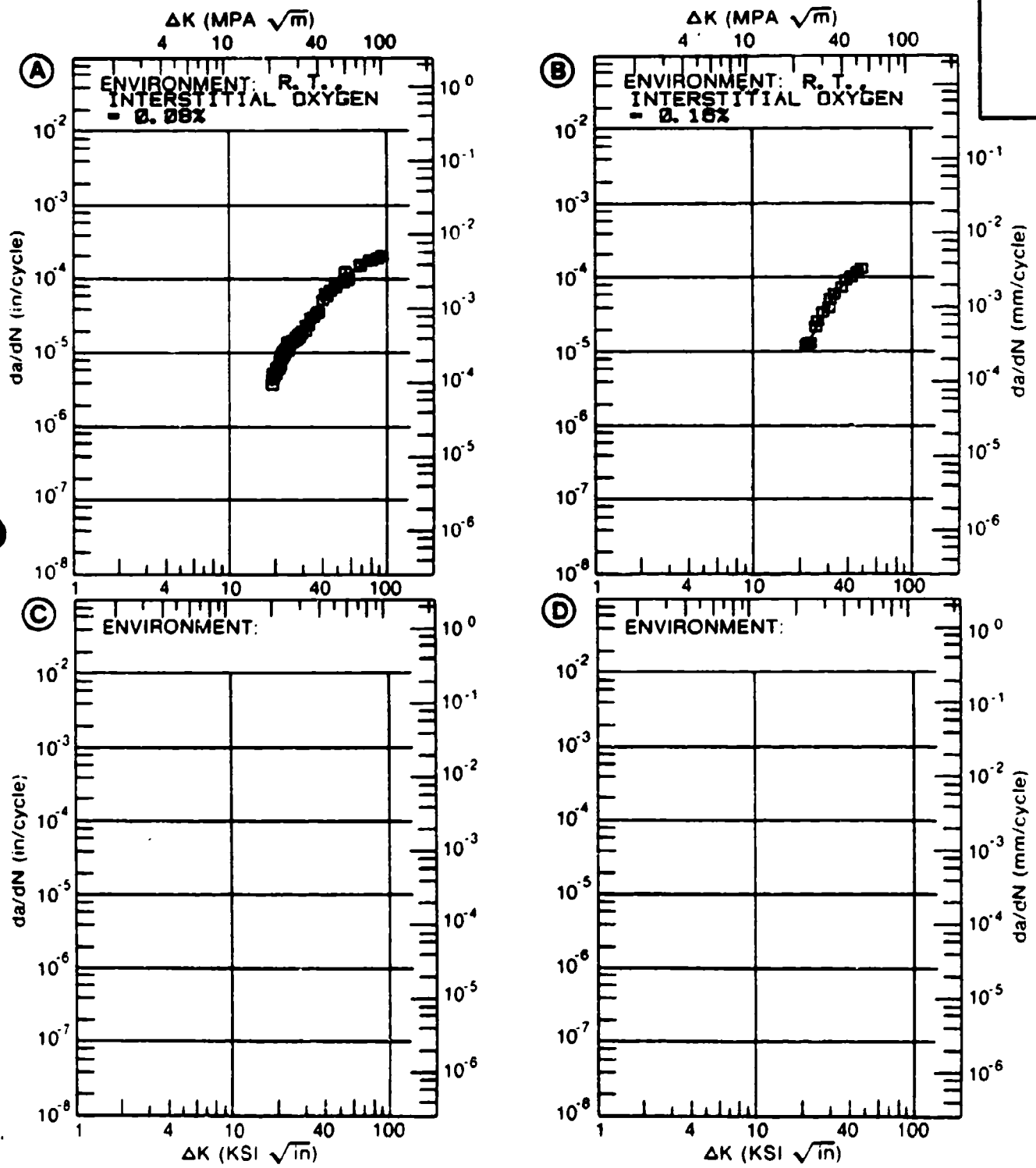


Figure 4.13.3.6

TABLE 4.13.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.7 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-6V-29N | | | |
|--------------------------------|----------|---------------------------|---|---|---|
| CONDITION: STOA | | | | | |
| ENVIRONMENT: R. T. , HUMID AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 8.20 | .39 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .525 | | | |
| | 10.00 | .734 | | | |
| | 13.00 | 1.67 | | | |
| | 16.00 | 3.15 | | | |
| | 20.00 | 5.98 | | | |
| | 25.00 | 10.8 | | | |
| | 30.00 | 16.7 | | | |
| | 35.00 | 23.2 | | | |
| | 40.00 | 29.9 | | | |
| | 50.00 | 42.3 | | | |
| DELTA K | A: 54.31 | 46.9 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 33.44 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: STDA
 FORM: 0.13" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., HUMID AIR

YIELD STRENGTH: 137.4 KSI
 ULT. STRENGTH: 143.0 KSI
 SPECIMEN THK: 0.125"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 00001

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TI-6AL-
4V-2SN

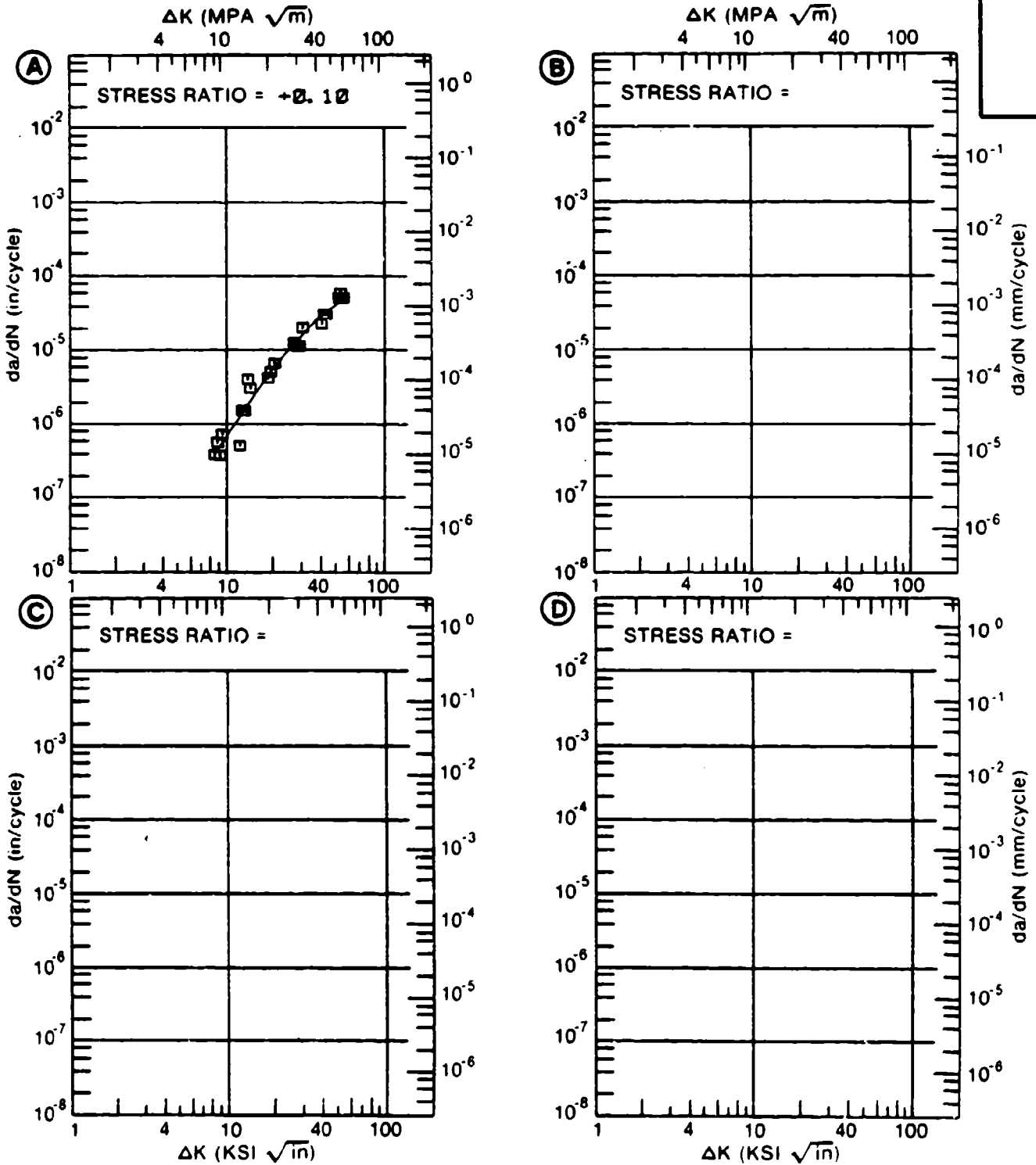


Figure 4.13.3.7

TABLE 4.13.3.8

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.8 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|--------------------------|------------|---------------------------------------|------------------------|---|---|
| CONDITION: STOA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H. H. A. | E= R. T. 3. 5% NACL | | |
| DELTA K | A: 9.04 | . 526 | | | |
| MIN | B: 8.98 | | 2. 50 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | | 2. 48 | | |
| | 10.00 | 2. 58 | 3. 14 | | |
| | 13.00 | 4. 48 | 15. 0 | | |
| | 16.00 | 5. 34 | 20. 8 | | |
| | 20.00 | 9. 03 | 29. 2 | | |
| | 25.00 | 20. 5 | 53. 7 | | |
| | 30.00 | 47. 9 | 61. 1 | | |
| | 35.00 | 104. | | | |
| DELTA K | A: 39.96 | 140. | | | |
| MAX | B: 30.00 | | 61. 1 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12. 68 | 8. 44 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0. 0-0. 5 | | | | |
| PREDICTION | 0. 5-0. 8 | | | | |
| RATIO | 0. 8-1. 25 | | | | |
| SUMMARY | 1. 25-2. 0 | | | | |
| (NP/NA) | >2. 0 | | | | |

CONDITION/HT: ST0A
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: L-S
 STRESS RATIO: +0.10
 FREQUENCY: 10.00 HZ

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH: 187.2 KSI
 SPECIMEN THK: 0.373- 0.374"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

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TI-6AL-
4V-2SN

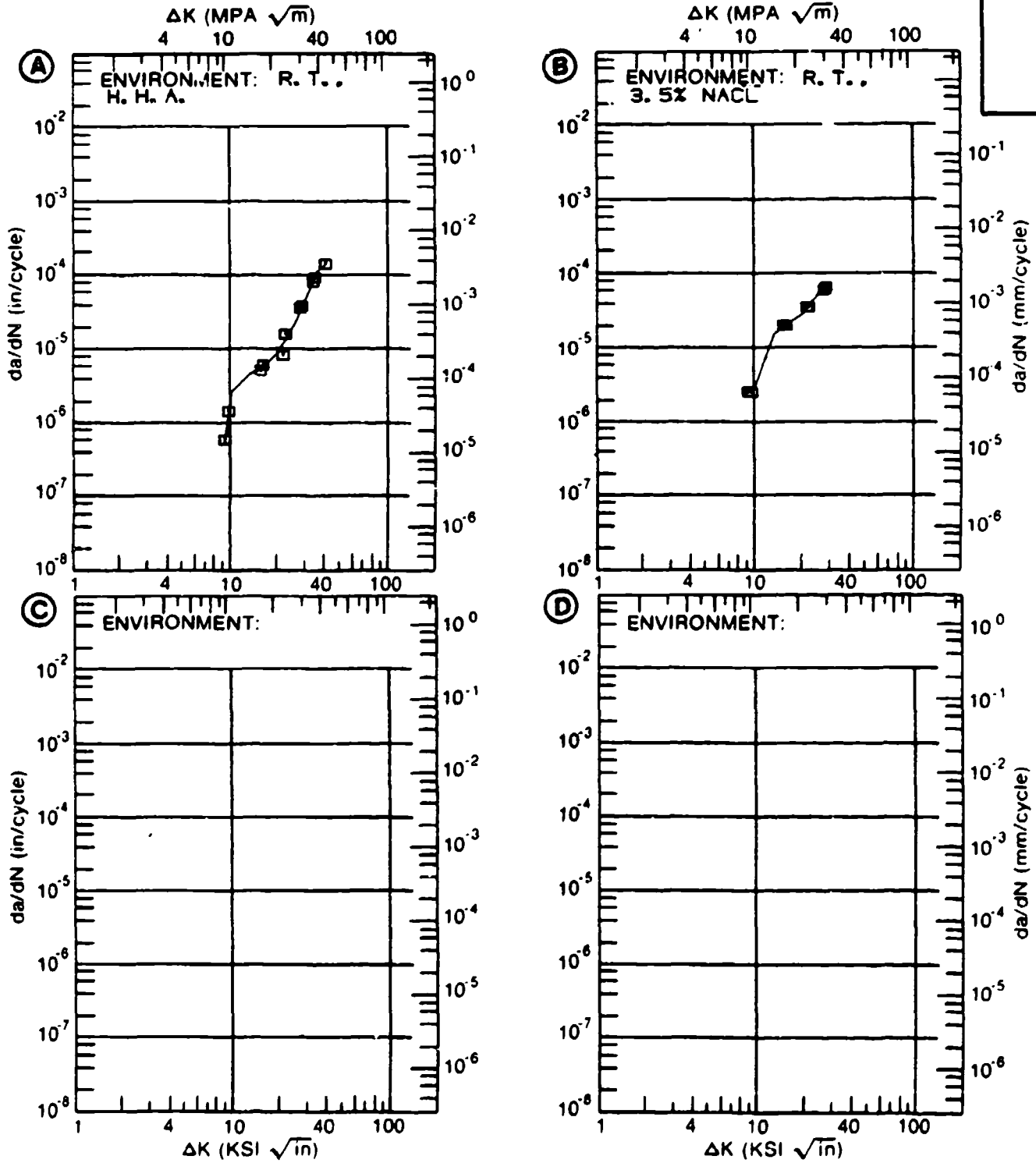


Figure 4.13.3.8

TABLE 4.13.3.9

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.9 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-28N | | | |
|--------------------------|----------|--------------------------------------|---|---|---|
| CONDITION: ST0A | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. | | | |
| | | H. H. A. | | | |
| DELTA K | A: 8.70 | .824 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | 1.01 | | | |
| | 10.00 | 1.73 | | | |
| | 13.00 | 4.16 | | | |
| | 16.00 | 6.42 | | | |
| | 20.00 | 10.2 | | | |
| | 25.00 | 20.7 | | | |
| | 30.00 | 53.0 | | | |
| DELTA K | A: 34.23 | 139. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 16.00 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ST0A
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: L-S
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH: 187.2 KSI
 SPECIMEN THK: 0.372"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 00001

TITAN.
ALLOY

TI-6AL-
4V-2SN

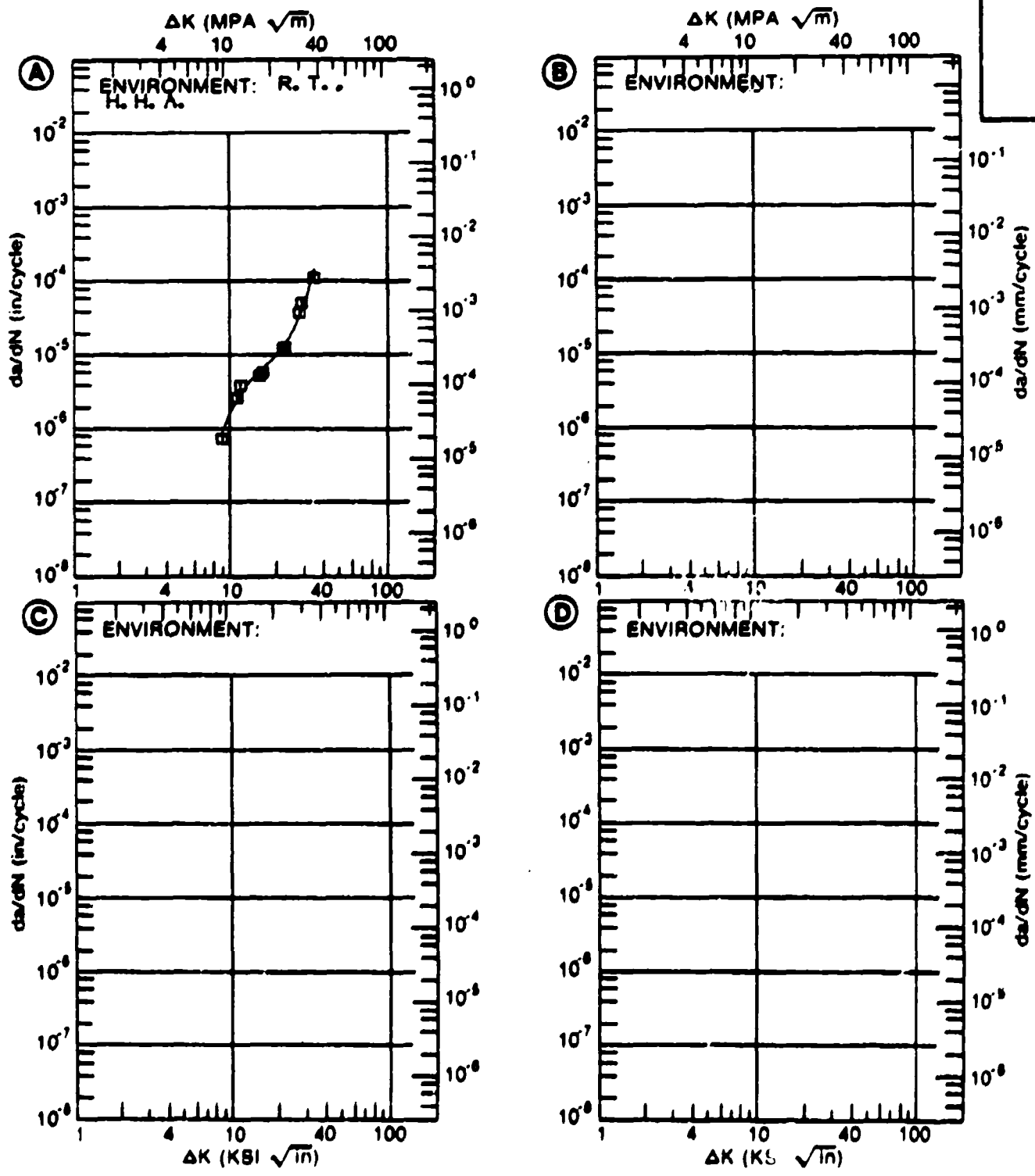


Figure 4.13.3.9

TABLE 4.13.3.10

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.10 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|-------------------------------|----------|---------------------------|---------|---|---|
| CONDITION: STCA | | | | | |
| ENVIRONMENT: R. T. , H. H. A. | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K MIN | A: 8.60 | .537 | | | |
| | B: 8.90 | | 1.35 | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | .670 | 1.45 | | |
| | 10.00 | 1.15 | 2.67 | | |
| | 13.00 | 4.83 | 11.7 | | |
| 16.00 | 14.7 | 31.4 | | | |
| 20.00 | 41.6 | 63.5 | | | |
| 25.00 | 88.0 | | | | |
| 30.00 | 119. | | | | |
| DELTA K MAX | A: 33.13 | 122. | | | |
| | B: 22.70 | | 75.8 | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 45.83 | 36.19 | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ST0A
 FORM: 0.30" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 FREQUENCY: 0.10 HZ
 ENVIRONMENT: R. T., H. H. A.

YIELD STRENGTH: 130.0 KSI
 ULT. STRENGTH: 187.2 KSI
 SPECIMEN THK: 0.373- 0.374"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 00001

TITAN.
ALLOY

TI-6AL-
4V-2SN

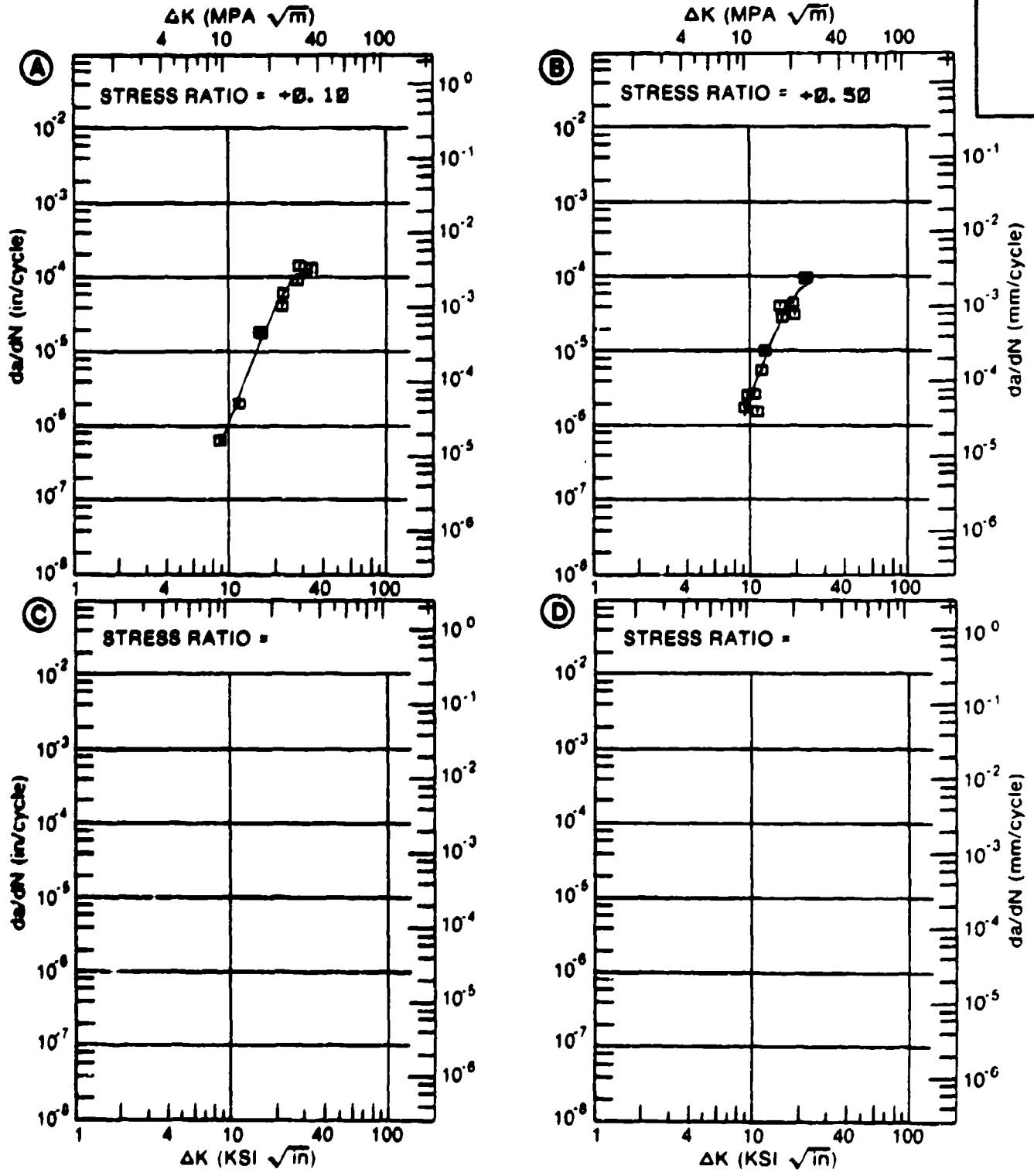


Figure 4.13.3.10

TABLE 4.13.3.11

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.11 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-6AL-6V-2SN
CONDITION: STOA

| DELTA K (KSI*IN**1/2) | DA/DN (10**6 IN. /CYCLE) | | | |
|--------------------------|--------------------------|---|---|---|
| | A | B | C | D |
| | E= R. T. 3. 5% NACL | | | |
| A: 9.26 | 1.28 | | | |
| DELTA K B: | | | | |
| MIN C: | | | | |
| D: | | | | |
| 10.00 | 1.49 | | | |
| 13.00 | 6.18 | | | |
| 16.00 | 27.2 | | | |
| 20.00 | 92.1 | | | |
| 25.00 | 185. | | | |
| 30.00 | 282. | | | |
| 35.00 | 423. | | | |
| 40.00 | 685. | | | |
| A: 45.85 | 2081. | | | |
| DELTA K B: | | | | |
| MAX C: | | | | |
| D: | | | | |

ROOT MEAN SQUARE 32.03
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: ST0A
 FORM: 0.98" TH PLATE
 SPECIMEN TYPE: PTSF
 ORIENTATION: T-S
 STRESS RATIO: +0.10
 FREQUENCY: 1.00 HZ

YIELD STRENGTH: 156.5 KSI
 ULT. STRENGTH: 187.8 KSI
 SPECIMEN THK: 0.375"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90981

TITAN. ALLOY

TI-6AL-6V-2SN

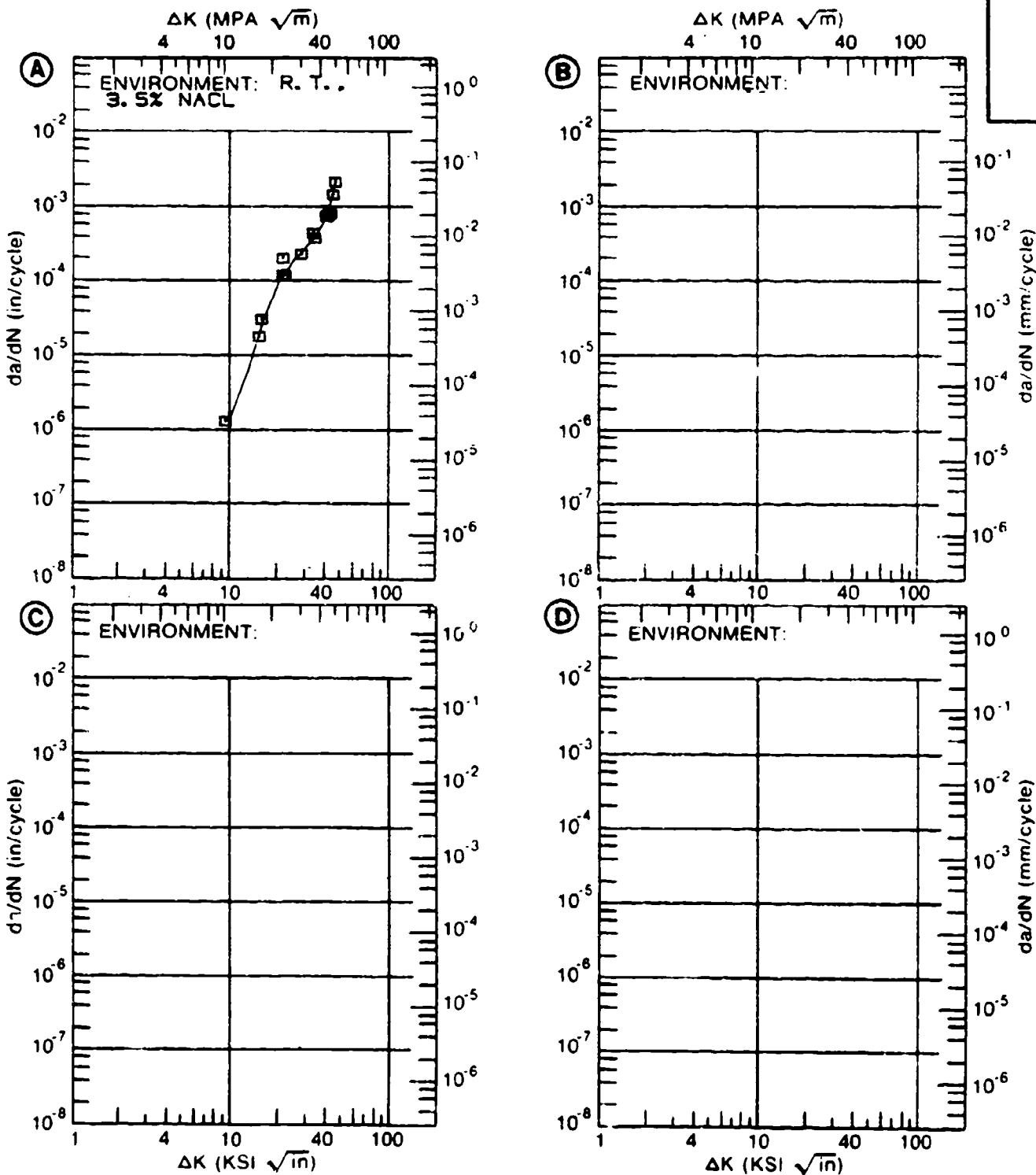


Figure 4.13.3.11

TABLE 4.13.3.12

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.12 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-6AL-6V-2SN
CONDITION: STQA
ENVIRONMENT: R. T. , HUMID AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10**+6 IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------|---------|---|---|
| | | A | B | C | D |
| | | R=+0.10 | R=+0.50 | | |
| DELTA K | A: 7.71 | .61 | | | |
| MIN | B: 4.54 | | .23 | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | | .334 | | |
| | 6.00 | | .592 | | |
| | 7.00 | | .907 | | |
| | 8.00 | .764 | 1.29 | | |
| | 9.00 | 1.40 | 1.77 | | |
| | 10.00 | 2.16 | 2.38 | | |
| | 13.00 | 4.71 | 5.66 | | |
| | 16.00 | 7.45 | 13.9 | | |
| | 20.00 | 12.4 | 49.5 | | |
| | 25.00 | 24.7 | | | |
| | 30.00 | 56.3 | | | |
| | 35.00 | 146. | | | |
| | 40.00 | 421. | | | |
| DELTA K | A: 41.04 | 531. | | | |
| MAX | B: 22.27 | | 105. | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 16.17 19.45
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25 1 1
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: STDA
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 FREQUENCY: 10.00 HZ
 ENVIRONMENT: R. T., HUMID AIR

YIELD STRENGTH: 180.3 KSI
 ULT. STRENGTH: 187.8 KSI
 SPECIMEN THK: 0.375"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 90881

TITAN.
ALLOY

TI-6AL-
6V-2SN

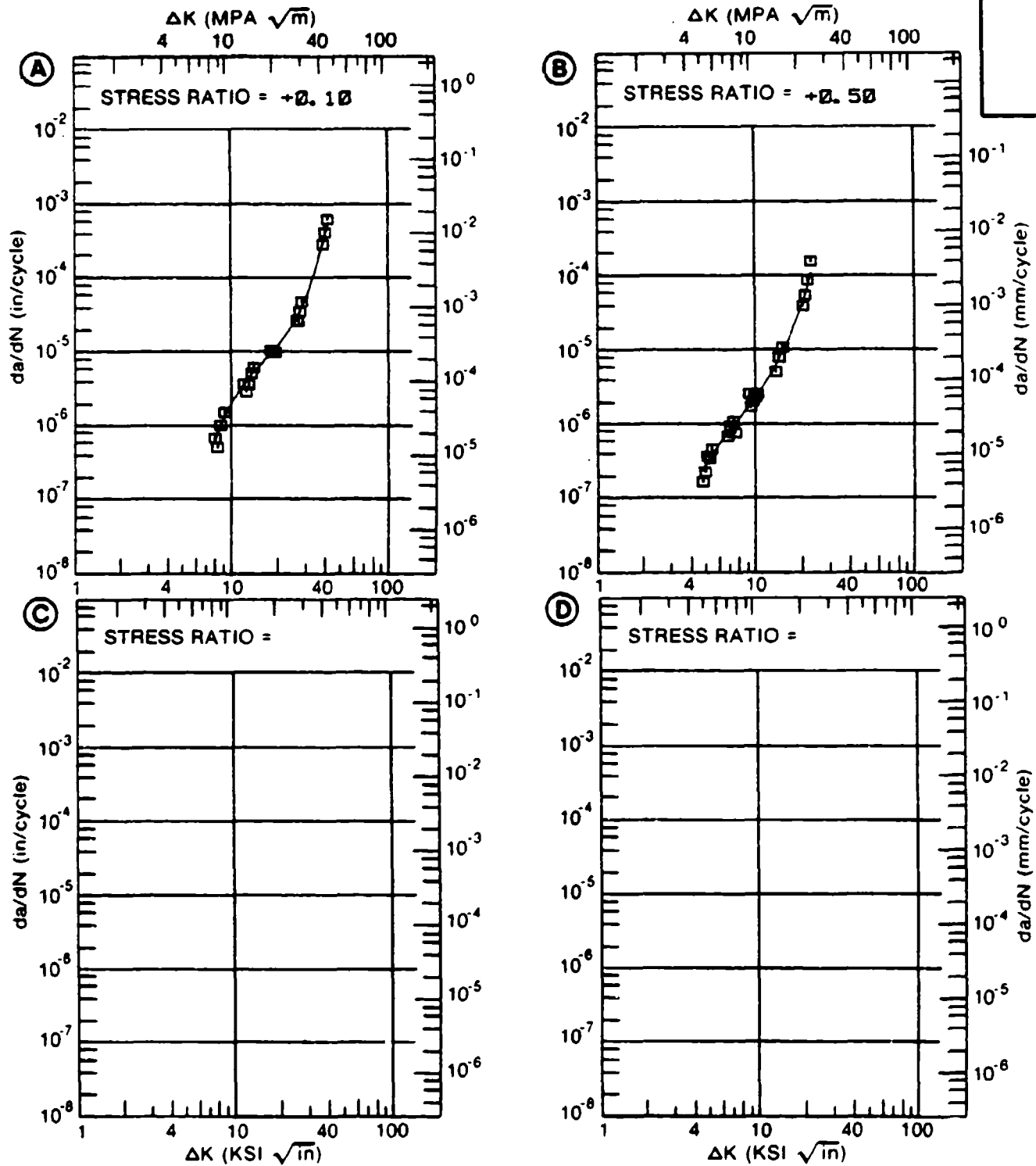


Figure 4.13.3.12

TABLE 4.13.3.13

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.13 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|--------------------------|------------|---------------------------|---|---|---|
| CONDITION: STOA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. 3. 5% NACL | | | |
| DELTA K | A: 8.30 | 1.38 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 9.00 | 1.71 | | | |
| | 10.00 | 2.35 | | | |
| | 13.00 | 6.07 | | | |
| | 16.00 | 13.5 | | | |
| | 20.00 | 30.1 | | | |
| DELTA K | A: 23.43 | 48.2 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 15.51 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 1 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ST0A
 FORM: 0.38" TH PLATE
 SPECIMEN TYPE: CCP
 ORIENTATION: T-L
 STRESS RATIO: +0.10
 FREQUENCY: 0.10 HZ

YIELD STRENGTH: 180.3 KSI
 ULT. STRENGTH: 187.8 KSI
 SPECIMEN THK: 0.375"
 SPECIMEN WIDTH: 5.000"
 REFERENCES: 00001

TITAN.
ALLOY

TI-6AL-
6V-2SN

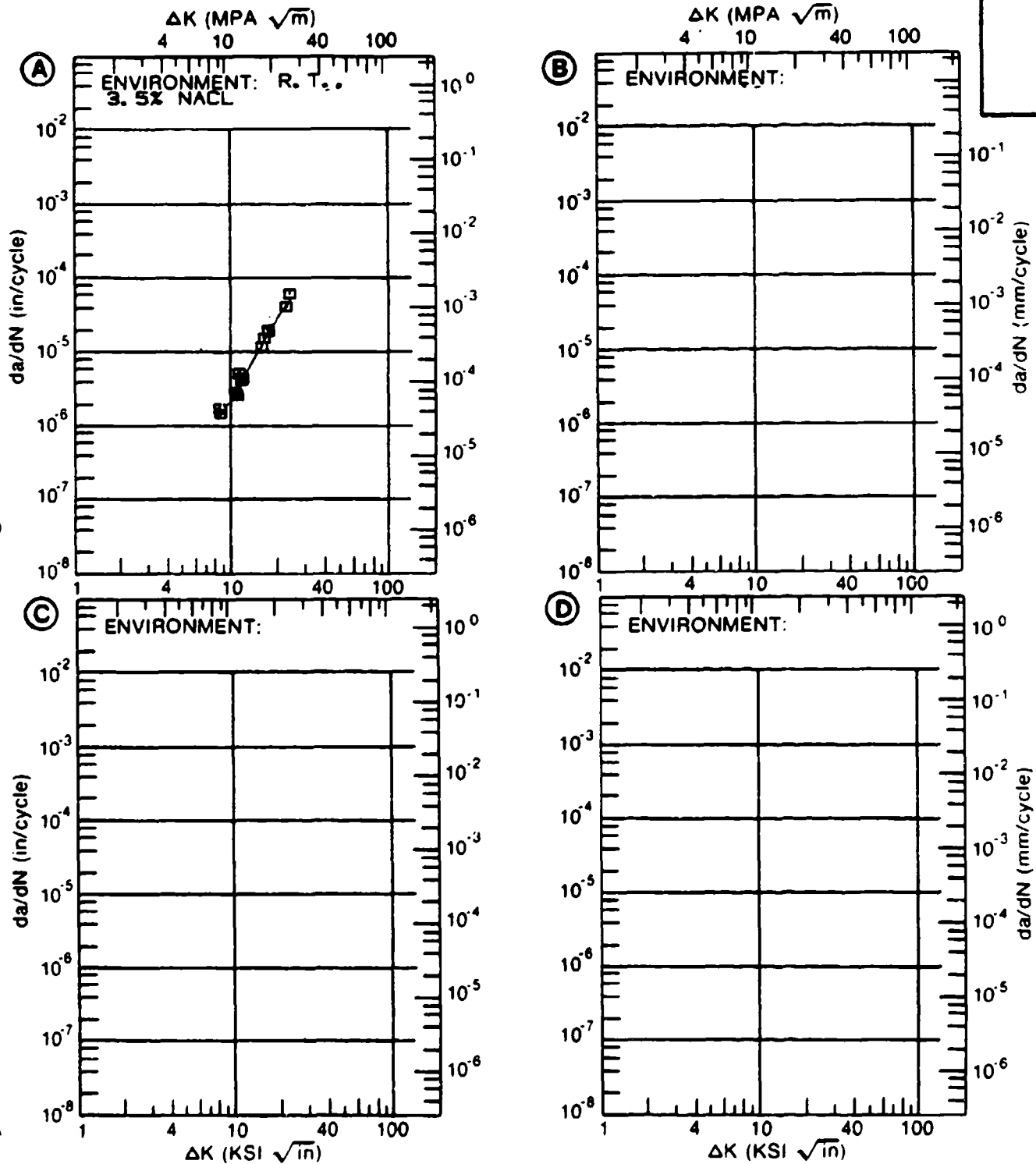


Figure 4.13.3.13

TABLE 4.13.3.14

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.14 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|--------------------------|----------|--------------------------------------|-------------------------------|------------------------------|--------------------------------|
| CONDITION: STOA | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN./CYCLE) | | | |
| | | A | B | C | D |
| | | E= R. T. H. H. A. 1HZ | E= R. T. 3. 5% NACL 1HZ | E= R. T. H. H. A. 20HZ | E= R. T. 3. 5% NACL 20HZ |
| DELTA K | A: 7.86 | .602 | | | |
| MIN | B: 6.57 | | .540 | | |
| | C: 4.47 | | | .0681 | |
| | D: 4.61 | | | | .174 |
| | 5.00 | | | .118 | .231 |
| | 6.00 | | | .240 | .469 |
| | 7.00 | | .634 | .419 | .869 |
| | 8.00 | .652 | 1.01 | .715 | 1.45 |
| | 9.00 | 1.08 | 1.60 | 1.17 | 2.21 |
| | 10.00 | 1.64 | 2.35 | 1.76 | 3.13 |
| | 13.00 | 4.12 | 5.51 | 4.20 | 6.72 |
| | 16.00 | 7.84 | 12.8 | 7.53 | 11.4 |
| | 20.00 | 15.1 | 38.4 | 13.4 | 19.3 |
| | 25.00 | 29.4 | 85.1 | 24.3 | 32.8 |
| | 30.00 | 52.4 | 150. | 41.2 | 51.9 |
| | 35.00 | 89.5 | 264. | 68.5 | 79.2 |
| | 40.00 | 149. | 505. | 113. | |
| | 50.00 | 396. | 2561. | | |
| | 60.00 | 1011. | | | |
| DELTA K | A: 63.06 | 1341. | | | |
| MAX | B: 54.97 | | 6717. | | |
| | C: 45.10 | | | 187. | |
| | D: 39.72 | | | | 116. |
| ROOT MEAN SQUARE | | 14.47 | 19.12 | 9.46 | 12.48 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 1 | 1 | 1 | 1 |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: ST0A
 FORM: 0.63" TH PLATE
 SPECIMEN TYPE: CT
 ORIENTATION: L-T
 STRESS RATIO: +0.10
 FREQUENCY:

YIELD STRENGTH: 160.0 KSI
 ULT. STRENGTH: 170.0 KSI
 SPECIMEN THK: 0.148- 0.151"
 SPECIMEN WIDTH: 3.000"
 REFERENCES: 88844

TITAN.
ALLOY

TI-6AL-
6V-2SN

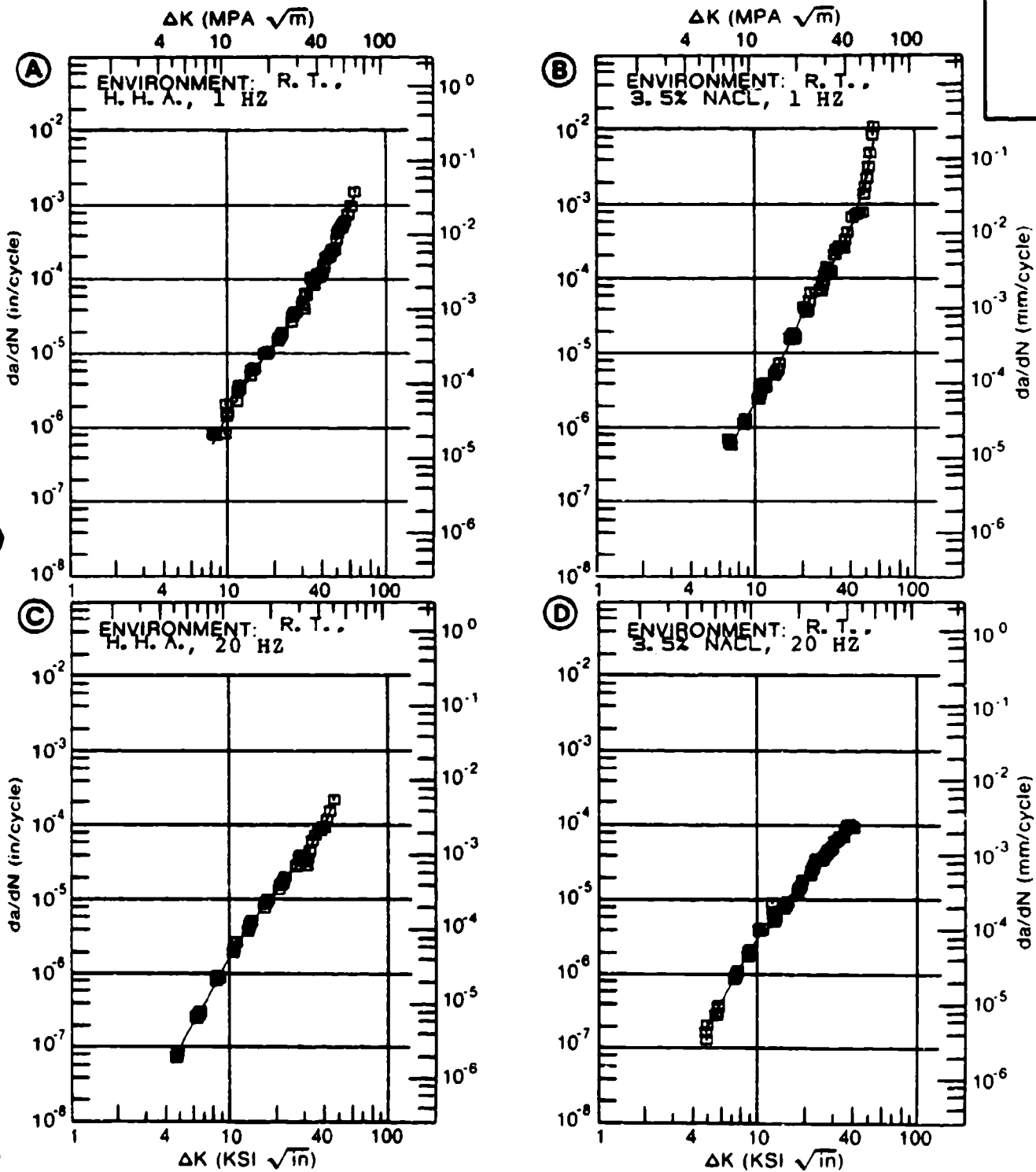


Figure 4.13.3.14

TABLE 4.13.3.15

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.13.3.15 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-6AL-6V-2SN | | | |
|------------------------|---|------------------------|-----------------------|---|---|
| CONDITION: 1300F 2HR | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 3.5% NACL | E= R. T. JP-4 FUEL | | |
| A: | : | | | | |
| K MAX B: | : | | | | |
| MIN C: | : | | | | |
| D: | : | | | | |
| 200.00 | : | | | | |
| A: | : | | | | |
| K MAX B: | : | | | | |
| MAX C: | : | | | | |
| D: | : | | | | |
| ROOT MEAN SQUARE | | 0.00 | 0.00 | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1300F 2HR
 FORM: 2.0" TH FORGING
 SPECIMEN TYPE: TDCB
 ORIENTATION: L-T
 YIELD STRENGTH: 140.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 1.250"
 SPECIMEN WIDTH: 5.500"
 CRACK LENGTH (A₀):
 K_{ISCC}: 32.00 KSI (SQRT IN)
 REFERENCES: 84380

TITAN.
 ALLOY

TI-6AL-
 8V-2SN

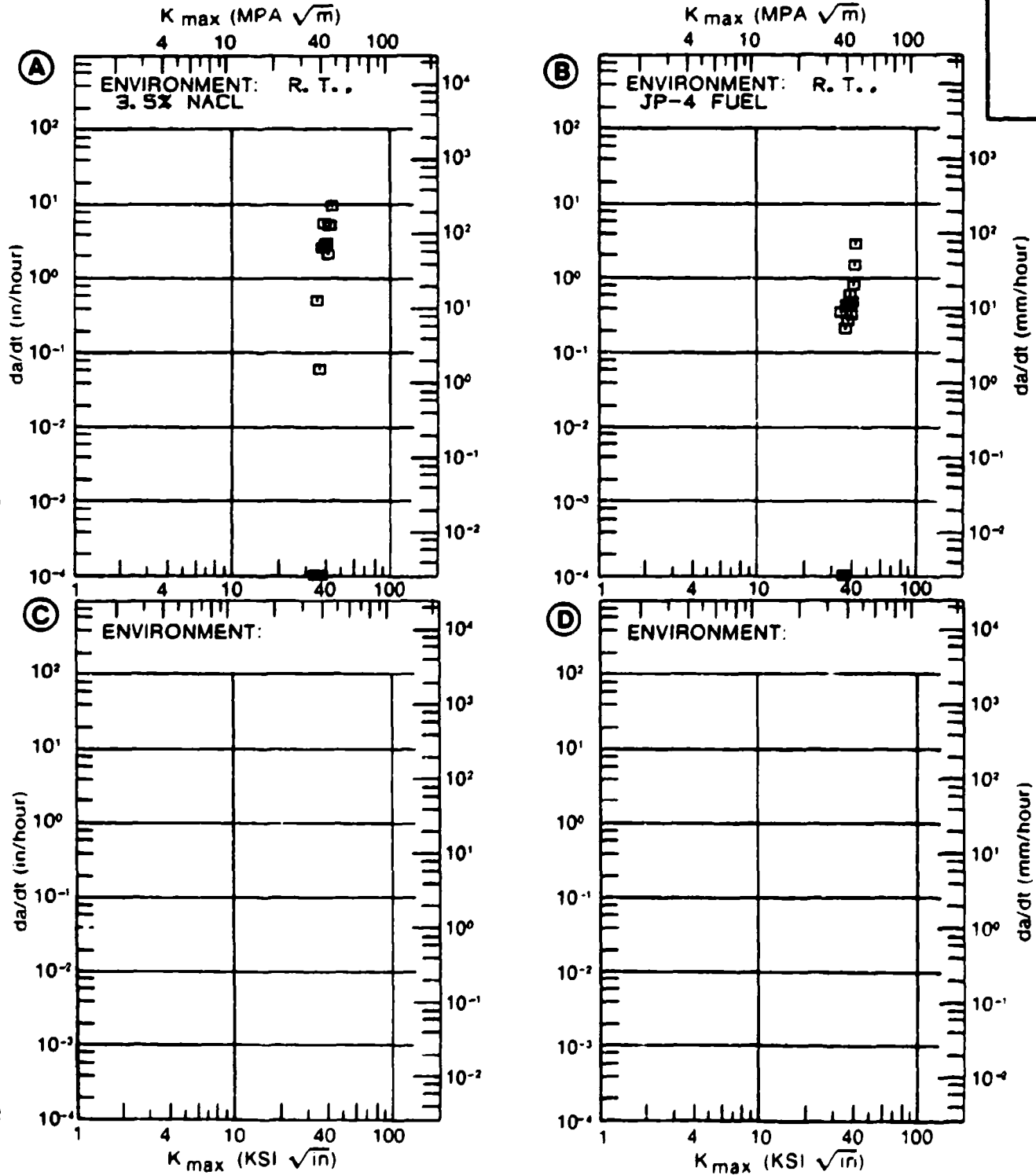


Figure 4.13.3.15
 4.13-45

TABLE 4.14.3.1

| CONDITION | | PRODUCT | | TEST SPEC | | YIELD | | TITANIUM | | TI-6AL-6V-2.5SN K (ISCC) | | SPECIMEN | | CRACK | | STAN | | TEST | | | | |
|------------------|------------|----------|--------|--------------------|------------|--------------|-------------|-------------|--------|--------------------------|-----------|----------|-----|------------|-------|-------|-----|------------|------|-------|------|-------|
| FORM | THICK (IN) | TEMP (F) | OR STR | ENVIRONMENT | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | K (IN) | K (IN) | MEAN (IN) | STAN | DEV | TIME (MIN) | DATE | REFER | DEV | TIME (MIN) | DATE | REFER | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| P | | R.T. | | 18A.0 3.5 PCT NaCl | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| 1050F 20R AC | F | 2 20 | R.T. | L-1 | 159.1 | JP-4 | FUEL | | 9.000 | 1.250 | TBCB | | | | 57.10 | 30.50 | | | | | 1971 | 84360 |
| 1500F 20R AC | F | 2 20 | R.T. | L-1 | 146.2 | 3.5 PCT NaCl | | | 9.000 | 1.250 | TBCB | | | | 47.30 | 32.40 | | | | | 1971 | 84360 |
| 1550F 14R 40R AC | P | 1.00 | R.T. | T-5 | 179.6 | 3.5 PCT NaCl | | | 1.000 | 0.750 | CANT* | | | | 55.00 | 21.00 | | | | | 1967 | 70931 |

TABLE 4.15.2.1

| CONDITION | --PRODUCT-- | | TEST SPECIMEN | YIELD | ---SPECIMEN--- | | CRACK | 2.50 | R(1C) STAM | DATE | REFER |
|--|-------------|------|---------------|-------|----------------|----------|-------|------|----------------|------|------------------|
| | FURN | TEMP | | | ORIENT | STRENGTH | | | | | |
| | (100) | (°) | (KSI) | (MPa) | (IN) | (IN) | (IN) | (IN) | (SUBSCRIPT IN) | | |
| TITANIUM 71-6422872400 R(1C) | | | | | | | | | | | |
| BETA FROSTED F | 2 00 | R T | --- | 154.6 | --- | 2 000 | --- | 0.52 | 71.44 | --- | 81003 |
| BETA FRO-100% F | 2 75 | R T | --- | 148.0 | 2 000 | 1 000 | CT | 0.09 | 28.50 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 148.0 | 2 000 | 1 000 | CT | 0.08 | 24.70 | --- | 1974 80742 (1) |
| BETA FRO-25% F | 2 75 | R T | --- | 148.0 | 2 000 | 1 000 | CT | 0.09 | 28.50 | --- | 1974 80742 (1) |
| 10% PRIMARY ALPHA, HELL, ANNEALED 1300F 1 HR, AC | | | | | | | | | | | |
| BETA FRO-100% F | 2 75 | R T | --- | 142.0 | 2 000 | 1 000 | CT | 0.10 | 31.40 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 142.0 | 2 000 | 1 000 | CT | 0.09 | 30.40 | --- | 1974 80742 (1) |
| BETA FRO-25% F | 2 75 | R T | --- | 142.0 | 2 000 | 1 000 | CT | 0.10 | 31.30 | --- | 1974 80742 (1) |
| 10% PRIMARY ALPHA, SOLUTION TREATED & AGED 1425F 1 HR, AC, 1100F 0 HR, AC | | | | | | | | | | | |
| BETA FRO-100% F | 2 75 | R T | --- | 148.0 | 2 000 | 1 000 | CT | 0.08 | 27.10 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 148.0 | 2 000 | 1 000 | CT | 0.10 | 29.70 | --- | 1974 80742 (1) |
| BETA FRO-25% FRO-100% ALPHA, SOLUTION TREATED & AGED 1425F 1 HR, AC, 1300F 1 HR, AC | | | | | | | | | | | |
| BETA FRO-100% F | 2 75 | R T | --- | 154.0 | 2 000 | 1 000 | CT | 0.05 | 22.70 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 154.0 | 2 000 | 1 000 | CT | 0.04 | 24.90 | --- | 1974 80742 (1) |
| BETA FRO-25% FRO-50% PRIMARY ALPHA, HELL, ANNEALED 1300F 1 HR, AC | | | | | | | | | | | |
| BETA FRO-100% F | 2 75 | R T | --- | 147.0 | 2 000 | 1 000 | CT | 0.05 | 24.00 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 147.0 | 2 000 | 1 000 | CT | 0.05 | 24.00 | --- | 1974 80742 (1) |
| BETA FRO-25% FRO-50% PRIMARY ALPHA, SOLUTION TREATED & AGED 1425F 1 HR, AC, 1100F 0 HR, AC | | | | | | | | | | | |
| BETA FRO-100% F | 2 75 | R T | --- | 159.0 | 2 000 | 1 000 | CT | 0.14 | 40.50 | --- | 1974 80742 (1) |
| BETA FRO-50% F | 2 75 | R T | --- | 159.0 | 2 000 | 1 000 | CT | 0.10 | 42.50 | --- | 1974 80742 (1) |
| BETA FRO-25% FRO-50% PRIMARY ALPHA, SOLUTION TREATED & AGED 1425F 1 HR, AC, 1100F 0 HR, AC | | | | | | | | | | | |

NOTES
1. 1) COMP DATA

TABLE 4.15.2.1 (con't)

| TITANIUM T1-ALUMINUM R10C | | | | | | | | | | | | | | |
|---------------------------|------------------|--------------------|----------------------|-----------|----------------|-----------------------|---|------|-------|-------------------|-----------------------------------|-----------------------------------|------------|-----------|
| CONDITION | TEMPERATURE (°F) | TEST SPECIMEN TYPE | YIELD STRENGTH (KSI) | UTS (KSI) | ELONGATION (%) | REDUCTION OF AREA (%) | SOLUTION TREATED & AGED 1625°F 1 HR. AC. 1100°F 8 HR. AC. | CT | 1.000 | CRACK LENGTH (IN) | R10C/UTS) x 10 ² (MPA) | R10C/UTS) x 10 ² (KSI) | STAIN DEVI | REFER |
| | | | | | | | | | | | | | | |
| ALPHA-BETA F | 2.75 | R.T. | 157.0 | 2.000 | 1.000 | CT | 1.000 | 0.17 | 41.30 | 41.30 | 41.47 | 0.9 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 161.0 | 2.000 | 1.000 | CT | 1.000 | 0.13 | 36.90 | 36.90 | 37.47 | 1.3 | 1974 | R0962 (1) |
| BETA (PSE) F | 2.75 | R.T. | 161.0 | 2.000 | 1.000 | CT | 1.000 | 0.15 | 38.90 | 38.90 | 39.47 | 1.1 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 161.0 | 2.000 | 1.000 | CT | 1.000 | 0.13 | 36.90 | 36.90 | 37.47 | 1.3 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 153.0 | 2.000 | 1.000 | CT | 1.000 | 0.22 | 43.00 | 43.00 | 44.77 | 1.1 | 1974 | R0962 (1) |
| BETA (PSE) F | 2.75 | R.T. | 153.0 | 2.000 | 1.000 | CT | 1.000 | 0.20 | 43.00 | 43.00 | 44.77 | 1.1 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 153.0 | 2.000 | 1.000 | CT | 1.000 | 0.21 | 44.00 | 44.00 | 44.77 | 1.1 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 163.0 | 2.000 | 1.000 | CT | 1.000 | 0.10 | 32.40 | 32.40 | 33.27 | 1.3 | 1974 | R0962 (1) |
| BETA (PSE) F | 2.75 | R.T. | 163.0 | 2.000 | 1.000 | CT | 1.000 | 0.10 | 32.40 | 32.40 | 33.27 | 1.3 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 163.0 | 2.000 | 1.000 | CT | 1.000 | 0.09 | 31.00 | 31.00 | 31.87 | 1.3 | 1974 | R0962 (1) |
| BETA (PSE) F | 2.75 | R.T. | 164.0 | 2.000 | 1.000 | CT | 1.000 | 0.08 | 29.20 | 29.20 | 30.07 | 1.3 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.75 | R.T. | 164.0 | 2.000 | 1.000 | CT | 1.000 | 0.08 | 30.20 | 30.20 | 31.07 | 1.3 | 1974 | R0962 (1) |
| ALPHA-BETA F | 2.00 | R.T. | 150.0 | 2.000 | 2.000 | --- | --- | 0.21 | 43.94 | 43.94 | --- | --- | --- | R1003 |

NOTES
 (1) CRP DISK
 (2) CRP DISK COMPE CRAIN SIZE
 (3) CRP DISK FINE CRAIN SIZE

TABLE 4.16.1.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF THE STRESS-INTENSITY FACTOR
TITANIUM TI-8AL-1ND-1V

TEST CONDITIONS

SPECIMEN ORIENTATION L-T

ENVIRONMENT LAB AIR AT R.T.

| CONDITION/HT | PRODUCT FORM | STRESS RATIO | FREQ (HZ) | DELTA K LEVELS (KSI SQRT(IN)) | FATIGUE CRACK GROWTH RATES (MICR IN/CYCLE) | |
|--------------|--------------|--------------|------------|-------------------------------|--|------|
| | | | | 2.5 5 10 20 50 100 | | |
| | SHEET | 0.02 | 0 10-12 00 | | 2.28 13.5 144 | 1243 |
| DA | SHEET | 0.00 | 1 00-30 00 | | | 67.2 |
| DA | SHEET | 0.10 | 43.00 | | 7.56 246 | |
| DA | SHEET | 0.25 | 1 00-30 00 | | | 162 |
| DA | SHEET | 0.43 | 1 00-30.00 | | | 13.3 |
| DA | SHEET | 0.67 | 1 00-30 00 | | 2.22 | |
| MA | SHEET | 0.10 | 43.00 | | | 7.47 |

TABLE 4.16.2.1

| CONDITION | TITANIUM | | TI-6AL-1MD-IV | | K(IIC) | | CRACK LENGTH (IN) | CRACK LENGTH (IN) | K(IIC)/TYSI**2 (KSI*SQRT IN) | K(IIC) MEAN DEV (IN) | K(IIC) STAH | DATE | REFER |
|--------------------------------|----------|------------|---------------|------------|--------|--------|-------------------|-------------------|------------------------------|----------------------|-------------|------|-------|
| | FORM | THICK (IN) | THICK (IN) | THICK (IN) | DESIGN | DESIGN | | | | | | | |
| PROOF THR 40, 1100F RHNS AC | F | --- | R T | C-R | 142.0 | 2.500 | 0.500 | --- | 0.18 | 38.32 | --- | 1977 | PH002 |
| | | | | | | | | | | | | | |

TABLE 4.16.2.2

| TITANIUM | | TI-BAL-1MO-IV K(IC) | | | | | | | | | | K(IC) STAN | | | | |
|-----------|------|---------------------|----------|------------------|------------|------------|---------------------------|------------|-------------|-----------|-----------------------------|--------------------------|----------------------------|--------------------------|------------|------------|
| CONDITION | FORM | THICK (IN) | TEMP (F) | SPEC YIELD (KSI) | SPECIMEN | | CRACK LENGTH CROSS STRESS | | | | K(APP) MEAN (KSI) (SORT IN) | STAN DEV (KSI) (SORT IN) | K(IC) MEAN (KSI) (SORT IN) | STAN DEV (KSI) (SORT IN) | DATE | REFER |
| | | | | | WIDTH (IN) | THICK (IN) | INIT (IN) | FINAL (IN) | ONSET (KSI) | MAX (KSI) | | | | | | |
| DA | S | 0.02 | R.T. | L-T | 135.5 | 9.000 | 0.020 | 2.110 | 2.630 | 62.20 | 73.30 | 138.16 | 157.35 | | | 1966 67821 |
| DA | S | 0.02 | R.T. | L-T | 135.5 | 12.000 | 0.020 | 0.560 | 0.700 | 79.00 | 110.20 | 105.54* | 115.80* | | | 1966 67821 |
| | | 0.02 | | | 135.5 | 12.000 | 0.020 | 2.120 | 2.800 | 42.50 | 55.90 | 104.02 | 121.33 | | | 1966 67821 |
| | | 0.02 | | | 135.5 | 12.000 | 0.020 | 2.020 | 2.360 | 41.60 | 47.90 | 86.85 | 94.49 | | | 1966 67821 |
| | | 0.02 | | | 135.5 | 12.000 | 0.020 | 0.950 | 1.240 | 75.00 | 85.00 | 104.24 | 98.4/10.0 | 111.7/15.0 | | 1966 67821 |
| DA | S | 0.04 | R.T. | L-T | 132.6 | 9.000 | 0.045 | 2.100 | 2.970 | 45.90 | 66.10 | 124.25 | 153.19 | | | 1966 67821 |
| DA | S | 0.05 | R.T. | L-T | 133.6 | 8.000 | 0.050 | 1.500 | 3.050 | 62.00 | 87.50 | 137.30* | 210.73* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 8.000 | 0.050 | 3.500 | 4.790 | 27.00 | 79.90 | 213.08* | 285.48* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 8.000 | 0.050 | 1.020 | 2.100 | 75.20 | 105.00 | 134.26* | 199.24* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 8.000 | 0.050 | 1.970 | 3.390 | 52.90 | 79.20 | 145.62 | 206.08* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 8.000 | 0.050 | 5.010 | 5.700 | 19.00 | 33.70 | 127.02 | 136.3/13.2 | 152.64* | | 1968 71709 |
| DA | S | 0.05 | R.T. | L-T | 133.6 | 20.000 | 0.050 | 2.060 | 9.000 | 62.40 | 85.90 | 155.54 | 250.46* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 2.020 | 4.000 | 29.10 | 77.40 | 138.75 | 198.94 | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 8.020 | 14.500 | 26.50 | 42.70 | 168.60 | 314.95* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 9.940 | 15.000 | 22.80 | 36.40 | 170.65 | 285.62* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 6.040 | 10.000 | 26.80 | 47.60 | 155.45 | 224.35 | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 9.980 | 15.600 | 19.30 | 30.50 | 143.50 | 259.41* | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 4.800 | 11.080 | 36.40 | 45.60 | 160.64 | 236.94 | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 4.260 | 7.500 | 36.90 | 58.90 | 156.77 | 221.71 | | | 1968 71709 |
| | | 0.05 | | | 133.6 | 20.000 | 0.050 | 3.760 | 7.520 | 48.60 | 67.80 | 173.43 | 198.1/11.8 | 263.23* | 220.5/15.8 | 1968 71709 |
| DA | S | 0.05 | R.T. | T-L | 135.3 | 8.000 | 0.050 | 4.910 | 9.700 | 26.90 | 37.80 | 139.02 | 171.22* | | | 1968 71709 |
| | | 0.05 | | | 135.3 | 8.000 | 0.050 | 1.000 | 2.250 | 65.00 | 103.00 | 132.88* | 207.62* | | | 1968 71709 |
| | | 0.05 | | | 135.3 | 8.000 | 0.050 | 2.940 | 4.250 | 39.40 | 62.00 | 145.55 | 195.48* | | | 1968 71709 |
| | | 0.05 | | | 135.3 | 8.000 | 0.050 | 2.020 | 3.450 | 42.90 | 80.10 | 148.56 | 220.88* | | | 1968 71709 |
| | | 0.05 | | | 135.3 | 8.000 | 0.050 | 1.320 | 3.100 | 51.70 | 91.80 | 145.09* | 144.4/ 4.9 | 223.65* | | 1968 71709 |

*NOTE- NET SECTION STRESS EXCEEDS BOX OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STD. DEV.

TABLE 4.16.3.1

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.1 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-8AL-1MO-1V | | | |
|------------------------------|-----------|---------------------------|---|---|---|
| CONDITION: | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KBI*IN**1/2) | | DA/DN (10**-6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.02 | | | |
| DELTA K | A: 6.38 | .621 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 7.00 | .824 | | | |
| | 8.00 | 1.22 | | | |
| | 9.00 | 1.70 | | | |
| | 10.00 | 2.28 | | | |
| | 13.00 | 4.56 | | | |
| | 16.00 | 7.75 | | | |
| | 20.00 | 13.5 | | | |
| | 25.00 | 23.6 | | | |
| | 30.00 | 37.3 | | | |
| | 35.00 | 55.4 | | | |
| | 40.00 | 78.7 | | | |
| | 50.00 | 144. | | | |
| | 60.00 | 243. | | | |
| | 70.00 | 387. | | | |
| | 80.00 | 589. | | | |
| | 90.00 | 867. | | | |
| | 100.00 | 1243. | | | |
| DELTA K | A: 118.36 | 2281. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 34.16 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT:
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 0.10- 12.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 119.5 KSI
 ULT. STRENGTH: 134.0 KSI
 SPECIMEN THK: 0.050"
 SPECIMEN WIDTH: 6.000"
 REFERENCES: MA011

TITAN.
ALLOY

TI-6AL-
4V

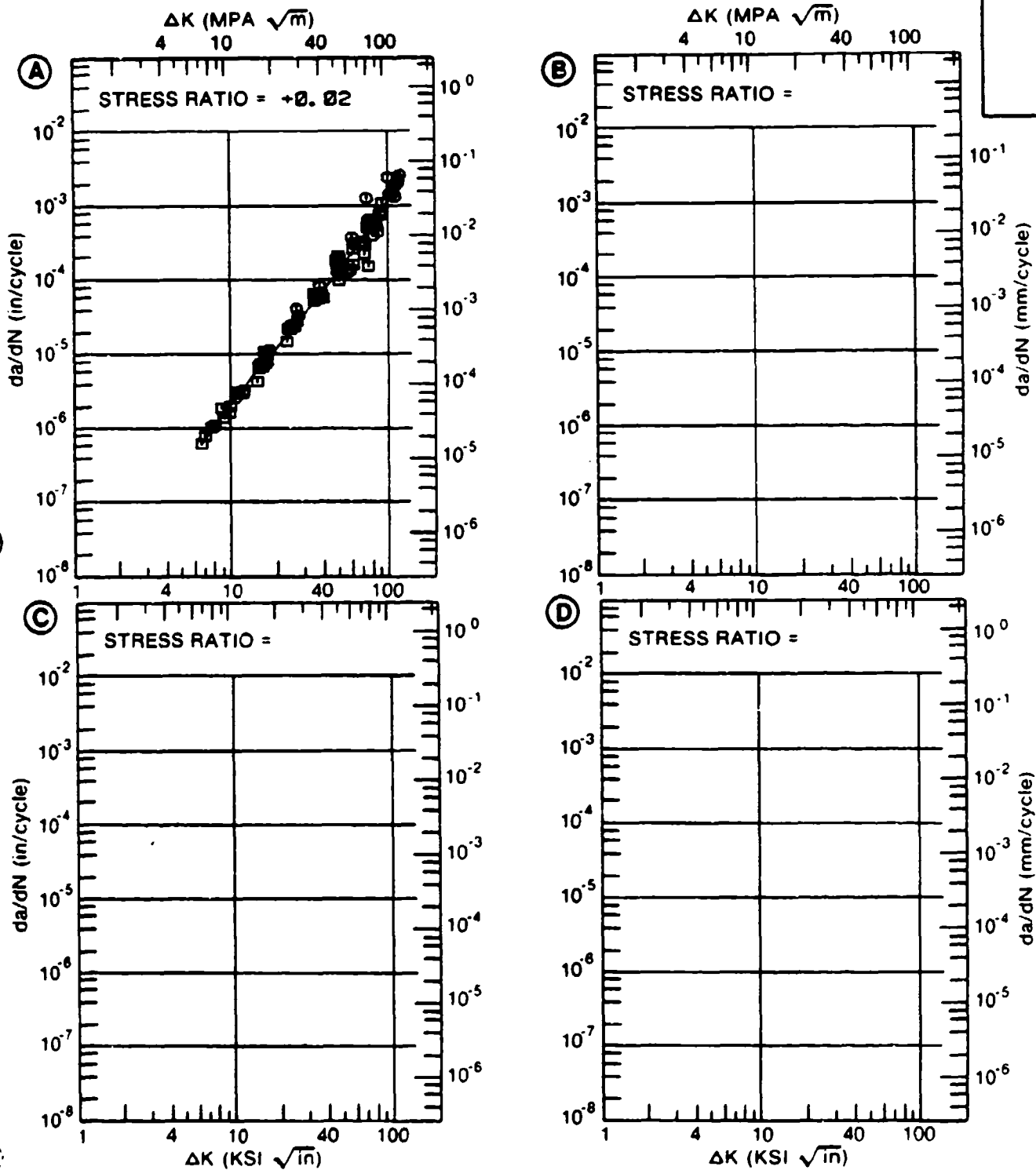


Figure 4.16.3.1

TABLE 4.16.3.2

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.2 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-BAL-1MO-1V | | | |
|------------------------------|----------|---------------------------------------|---|---|---|
| CONDITION: DA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 17.97 | 5.41 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 7.58 | | | |
| | 25.00 | 10.5 | | | |
| | 30.00 | 14.1 | | | |
| | 35.00 | 24.9 | | | |
| | 40.00 | 60.4 | | | |
| | 50.00 | 246. | | | |
| | 60.00 | 787. | | | |
| DELTA K | A: 62.14 | 1256. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 12.44 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | 2 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DA
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 43.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 140.0 KSI
 ULT. STRENGTH: 149.2 KSI
 SPECIMEN THK: 0.064"
 SPECIMEN WIDTH: 3.000"
 REFERENCES 86099

TITAN.
ALLOY

TI-8AL-
1MO-1V

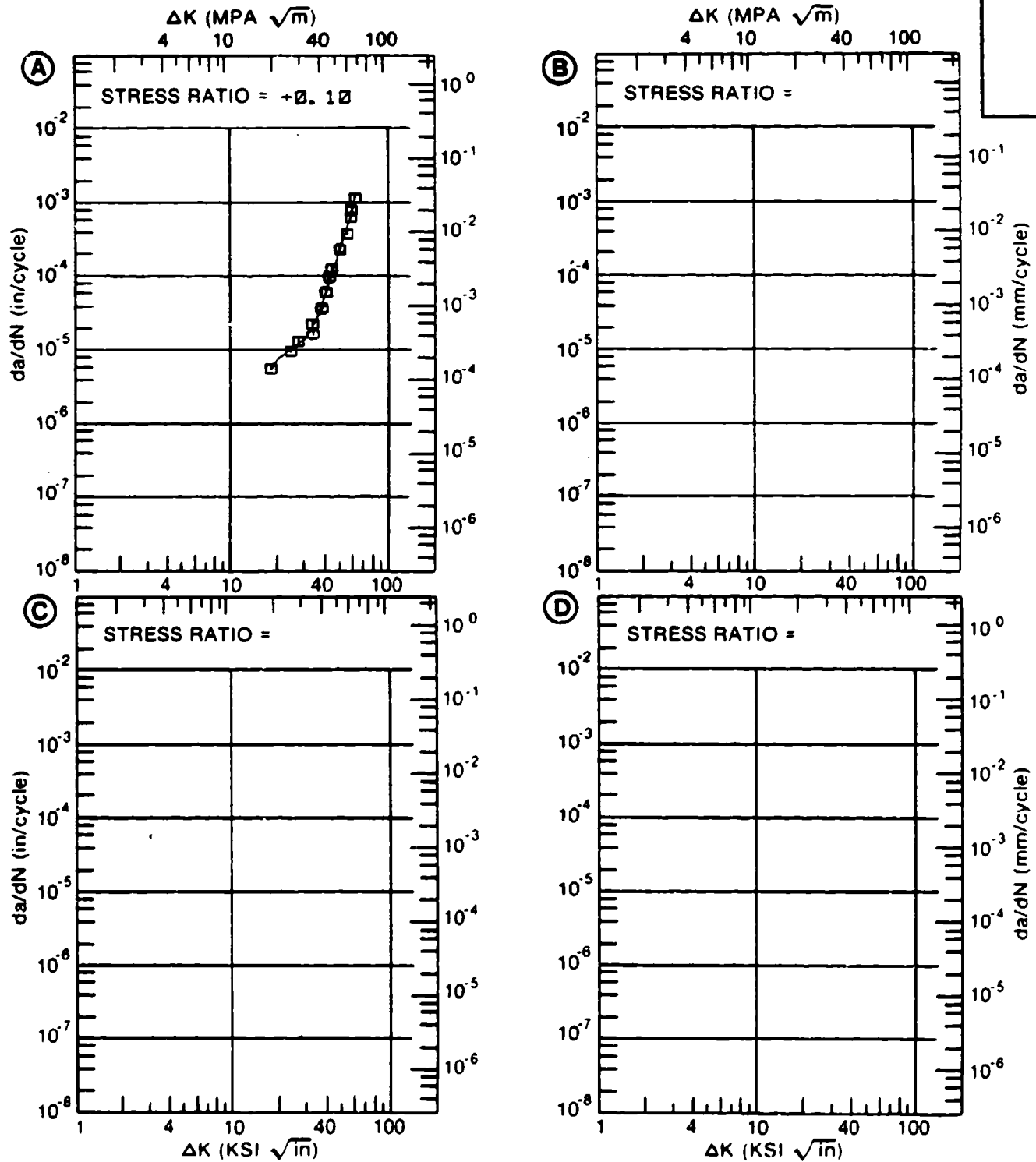


Figure 4.16.3.2

TABLE 4.16.3.3

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.3 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-BAL-1MD-1V | | | |
|------------------------------|----------|--------------------------|---------|---------|---------|
| CONDITION: DA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.00 | R=+0.25 | R=+0.43 | R=+0.67 |
| DELTA K | A: | | | | |
| MIN | B: 29.33 | | 33.3 | | |
| | C: | | | | |
| | D: | | | | |
| | 30.00 | | 35.3 | | |
| | 35.00 | | 51.0 | | |
| | 40.00 | | 71.5 | | |
| | 50.00 | | 162. | | |
| DELTA K | A: | | | | |
| MAX | B: 59.13 | | 439. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | 6.87 | 0.00 | 0.00 |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | | | | |
| RATIO | 0.8-1.25 | | 1 | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: DA
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 1.00-30.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 136.3 KSI
 ULT. STRENGTH: 150.7 KSI
 SPECIMEN THK: 0.050"
 SPECIMEN WIDTH: 20.000"
 REFERENCES 86099

TITAN.
 ALLOY
 TI-6AL-
 4V

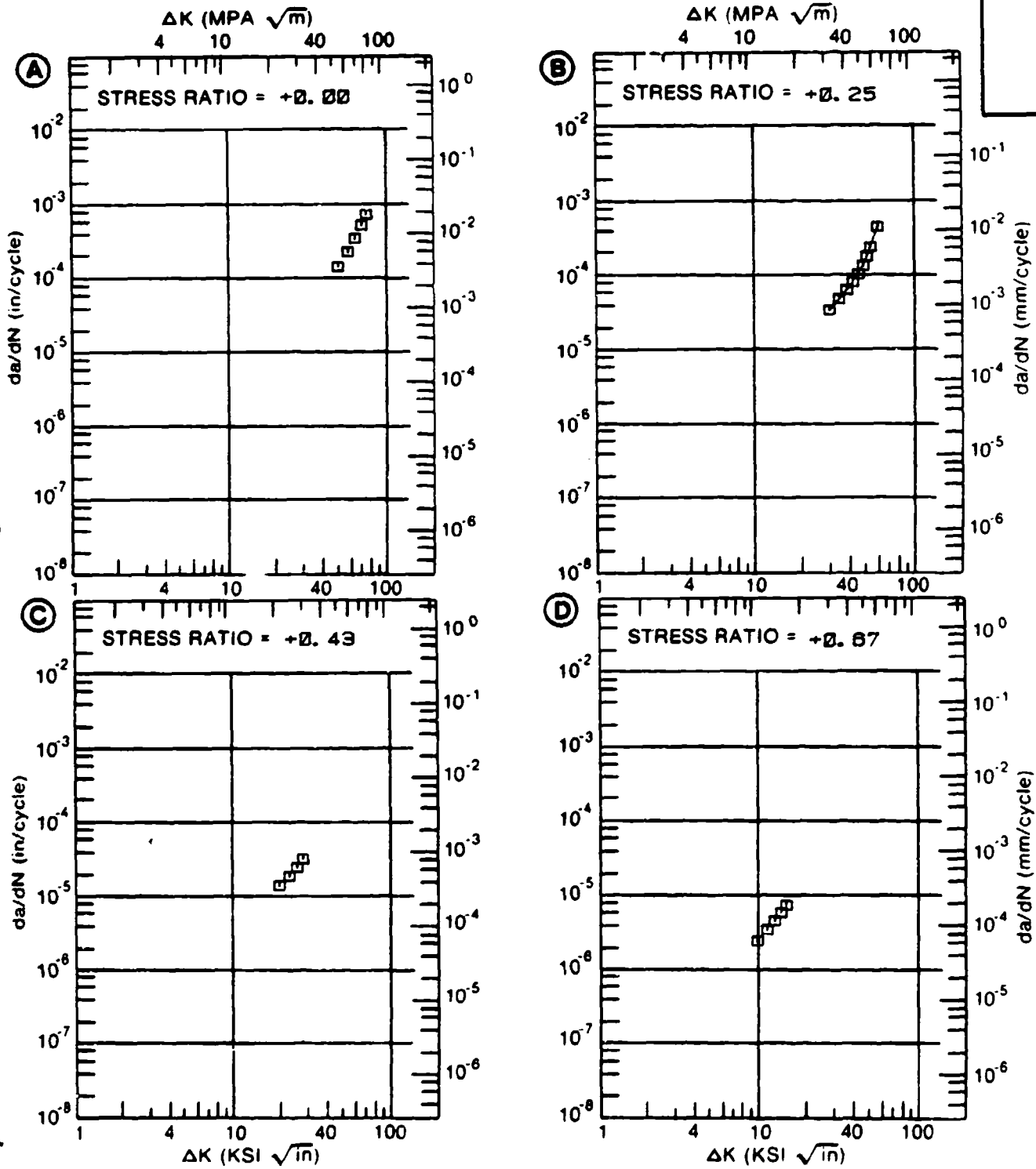


Figure 4.16.3.3

TABLE 4.16.3.4

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.4 INDICATING EFFECT

OF STRESS RATIO

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|---------------------------------------|-----------------|---------------------------------------|---------|---------|---------|
| | | A | B | C | D |
| | | R=+0.00 | R=+0.25 | R=+0.43 | R=+0.67 |
| MATERIAL: | TITANIUM | | | | |
| CONDITION: | DA | | | | |
| ENVIRONMENT: | R. T. , LAB AIR | | | | |
| | A: 37.15 | 28.2 | | | |
| DELTA K MIN | B: 22.28 | | 13.3 | | |
| | C: 14.82 | | | 6.14 | |
| | D: 7.48 | | | | .598 |
| | 8.00 | | | | .860 |
| | 9.00 | | | | 1.48 |
| | 10.00 | | | | 2.22 |
| | 13.00 | | | | 5.13 |
| | 16.00 | | | 7.88 | 10.2 |
| | 20.00 | | | 13.3 | |
| | 25.00 | | 15.6 | 21.1 | |
| | 30.00 | | 24.6 | | |
| | 35.00 | | 39.8 | | |
| | 40.00 | 32.8 | 60.8 | | |
| | 50.00 | 67.2 | | | |
| DELTA K MAX | A: 56.83 | 95.6 | | | |
| | B: 41.40 | | 67.5 | | |
| | C: 28.99 | | | 32.5 | |
| | D: 18.26 | | | | 17.6 |
| ROOT MEAN SQUARE | | 16.65 | 12.77 | 9.57 | 19.18 |
| PERCENT ERROR | | | | | |
| LIFE PREDICTION RATIO SUMMARY (NP/NA) | 0.0-0.5 | | | | |
| | 0.5-0.8 | | | | |
| | 0.8-1.25 | 3 | 4 | 4 | 3 |
| | 1.25-2.0 | 1 | | | 1 |
| | >2.0 | | | | |

CONDITION/HT: DA
 FORM: 0.05" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 1.00- 30.00 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 133.7- 136.3 KSI
 ULT. STRENGTH: 150.7- 152.1 KSI
 SPECIMEN THK: 0.050"
 SPECIMEN WIDTH: 2.000- 7.992"
 REFERENCES 88099

TITAN.
ALLOY

TI-6AL-
1MO-1V

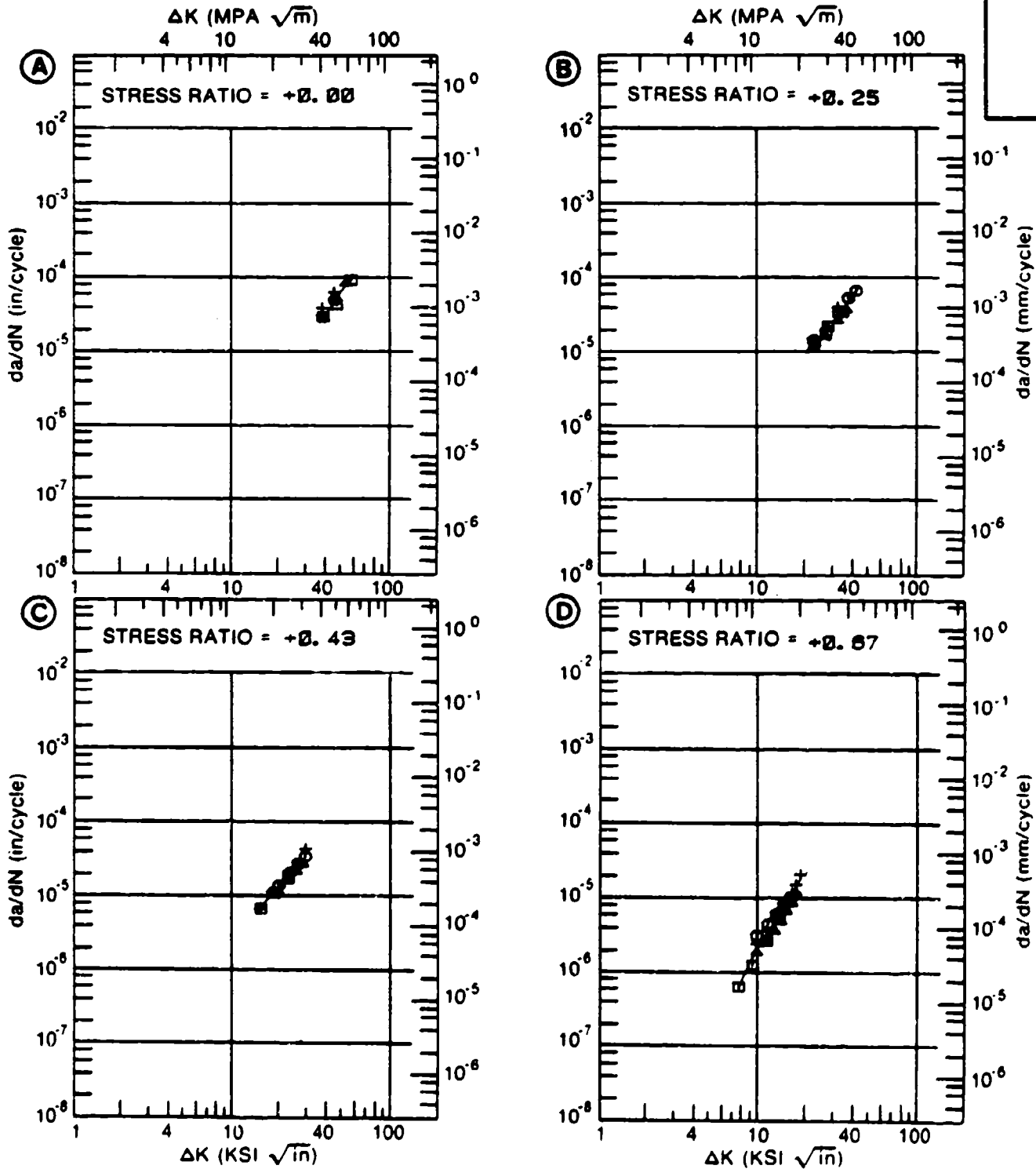


Figure 4.16.3.4

TABLE 4.16.3.5

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.5 INDICATING EFFECT
OF STRESS RATIO

| MATERIAL: TITANIUM | | TI-BAL-1MO-1V | | | |
|------------------------------|----------|--------------------------|---|---|---|
| CONDITION: MA | | | | | |
| ENVIRONMENT: R. T. , LAB AIR | | | | | |
| DELTA K (KSI*IN**1/2) | | DA/DN (10**6 IN. /CYCLE) | | | |
| | | A | B | C | D |
| | | R=+0.10 | | | |
| DELTA K | A: 19.10 | 6.63 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | 7.47 | | | |
| | 25.00 | 10.2 | | | |
| | 30.00 | 24.4 | | | |
| | 35.00 | 54.3 | | | |
| DELTA K | A: 39.05 | 87.0 | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 28.77 | | | |
| PERCENT ERROR | | | | | |
| LIFE | 0.0-0.5 | | | | |
| PREDICTION | 0.5-0.8 | 1 | | | |
| RATIO | 0.8-1.25 | 1 | | | |
| SUMMARY | 1.25-2.0 | | | | |
| (NP/NA) | >2.0 | | | | |

CONDITION/HT: MA
 FORM: 8.82" TH SHEET
 SPECIMEN TYPE: CCP
 ORIENTATION: L-T
 FREQUENCY: 42.88 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 154.9 KSI
 ULT. STRENGTH: 189.2 KSI
 SPECIMEN THK: 8.818"
 SPECIMEN WIDTH: 2.888"
 REFERENCES: 80899

TITAN.
 ALLOY
 TI-6AL-
 4V

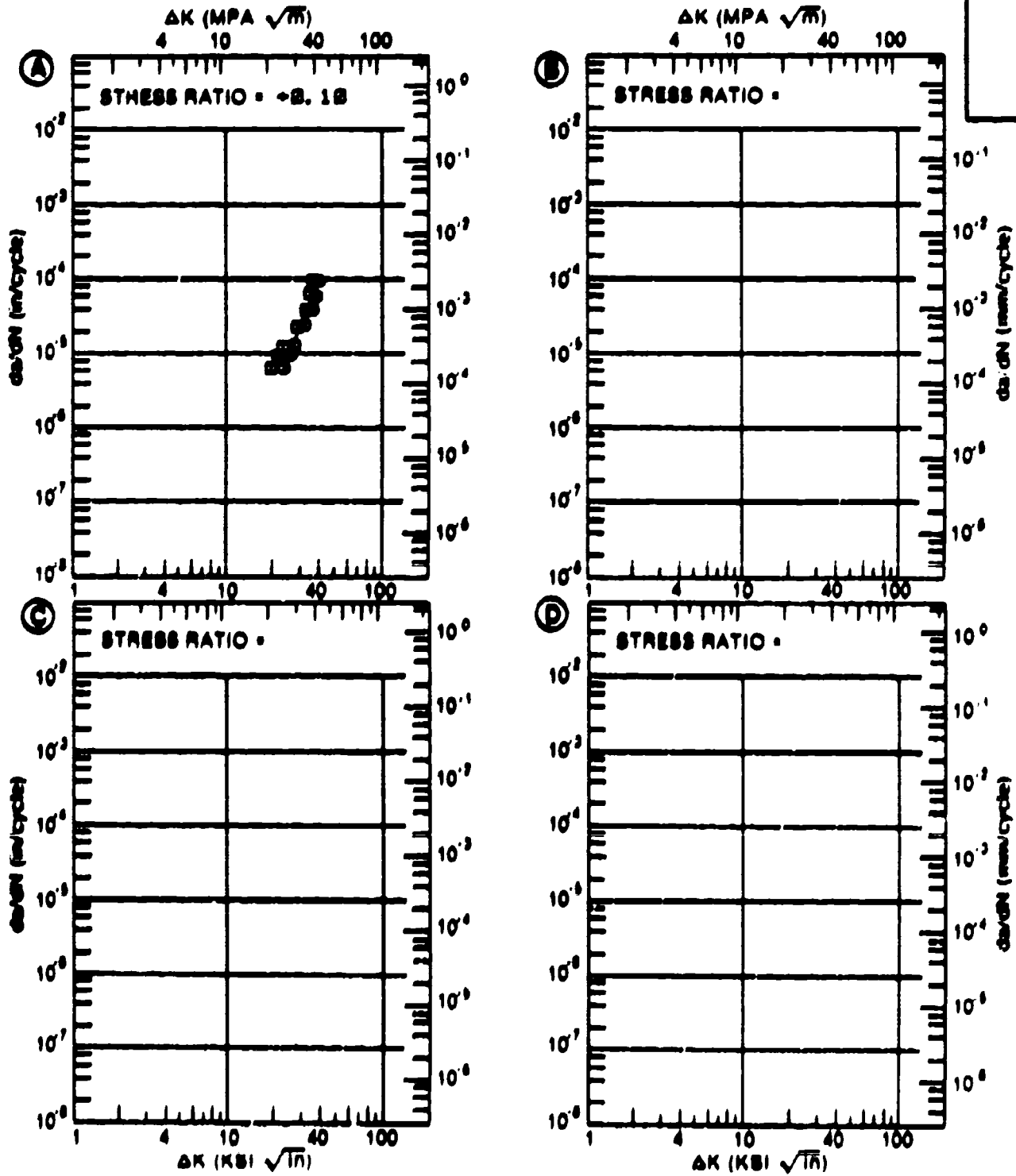


Figure 4.16.1.1

TABLE 4.16.3.6

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.6 INDICATING EFFECT
OF STRESS RATIO

MATERIAL: TITANIUM TI-8AL-1MO-1V
CONDITION: 1825F 1HR AC, 1350F 2HRS AC
ENVIRONMENT: R.T., LAB AIR

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------------|----------|---------------------------------------|---------|---------|---|
| | | A | B | C | D |
| | | R=+0.00 | R=+0.04 | R=+0.54 | |
| DELTA K MIN | A: 13.50 | 2.16 | | | |
| | B: 6.37 | | .0417 | | |
| | C: 10.39 | | | 2.48 | |
| | D: | | | | |
| | 7.00 | | .0911 | | |
| | 8.00 | | .214 | | |
| | 9.00 | | .379 | | |
| | 10.00 | | .581 | | |
| | 13.00 | | 1.60 | 6.62 | |
| | 16.00 | 2.86 | 4.92 | 19.0 | |
| | 20.00 | 10.6 | | | |
| | 25.00 | 23.3 | | | |
| | 30.00 | 75.2 | | | |
| DELTA K MAX | A: 31.31 | 107. | | | |
| | B: 19.64 | | 28.6 | | |
| | C: 16.74 | | | 21.9 | |
| | D: | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 17.10 | 20.60 | 11.15 | |

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1925F 1HR AC, 1350F 2HRS AC
 FORM: 2.50" TH FAN BLADES
 SPECIMEN TYPE: KB BAR
 ORIENTATION: L-T
 FREQUENCY: 0.33 HZ
 ENVIRONMENT: R. T., LAB AIR

YIELD STRENGTH: 120.0 KSI
 ULT. STRENGTH:
 SPECIMEN THK: 0.251- 0.253"
 SPECIMEN WIDTH: 0.750"
 REFERENCES: GE006

TITAN.
ALLOY

TI-8AL-
1MO-1V

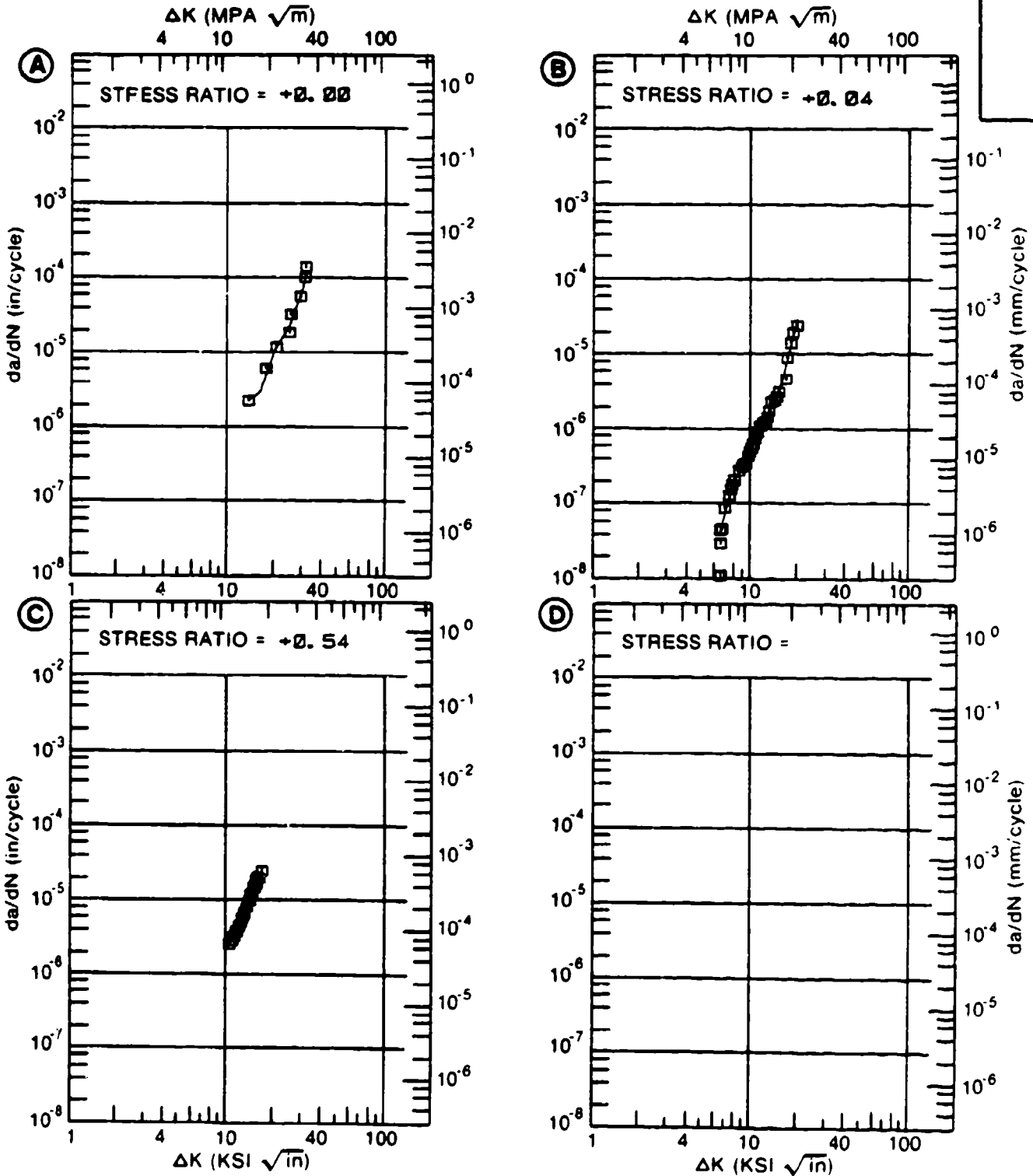


Figure 4.16.3.6

TABLE 4.16.3.7

FATIGUE CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.7 INDICATING EFFECT
OF ENVIRONMENT

MATERIAL: TITANIUM TI-8AL-1MO-1V
CONDITION: 1830F 1HR WG, 1100F 8HRS AC

| DELTA K (KSI*IN**1/2) | | DA/DN (10** ⁻⁶ IN. /CYCLE) | | | |
|--------------------------|----------|---------------------------------------|-----------------|---|---|
| | | A | B | C | D |
| | | E= R. T. LAB AIR | E=+ 800F AIR | | |
| DELTA K MIN | A: 4.09 | .0338 | | | |
| | B: 5.78 | | .455 | | |
| | C: | | | | |
| | D: | | | | |
| | 5.00 | .107 | | | |
| | 6.00 | .200 | .450 | | |
| | 7.00 | .355 | .484 | | |
| | 8.00 | .598 | .591 | | |
| | 9.00 | .967 | .769 | | |
| | 10.00 | 1.50 | 1.03 | | |
| 13.00 | 4.70 | 2.51 | | | |
| 16.00 | | 5.52 | | | |
| DELTA K MAX | A: 15.89 | 11.5 | | | |
| | B: 19.11 | | 10.7 | | |
| | C: | | | | |
| | D: | | | | |

ROOT MEAN SQUARE 10.00 8.96
PERCENT ERROR

LIFE 0.0-0.5
PREDICTION 0.5-0.8
RATIO 0.8-1.25
SUMMARY 1.25-2.0
(NP/NA) >2.0

CONDITION/HT: 1830F 1HR WQ, 1100F 8HRS AC

FORM: 1.00" TH FORGING

SPECIMEN TYPE: CCP

ORIENTATION: C-R

STRESS RATIO: +0.10

FREQUENCY: 30.00 HZ

YIELD STRENGTH: 135.5- 145.8 KSI

ULT. STRENGTH: 148.5- 159.3 KSI

SPECIMEN THK: 0.078- 0.080"

SPECIMEN WIDTH: 1.750"

REFERENCES: PW002

TITAN.
ALLOY

TI-8AL-
1MO-1V

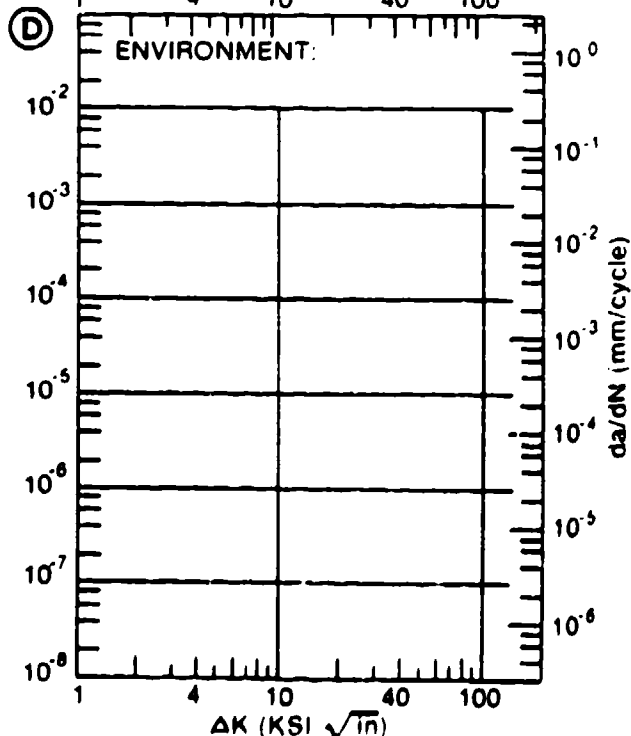
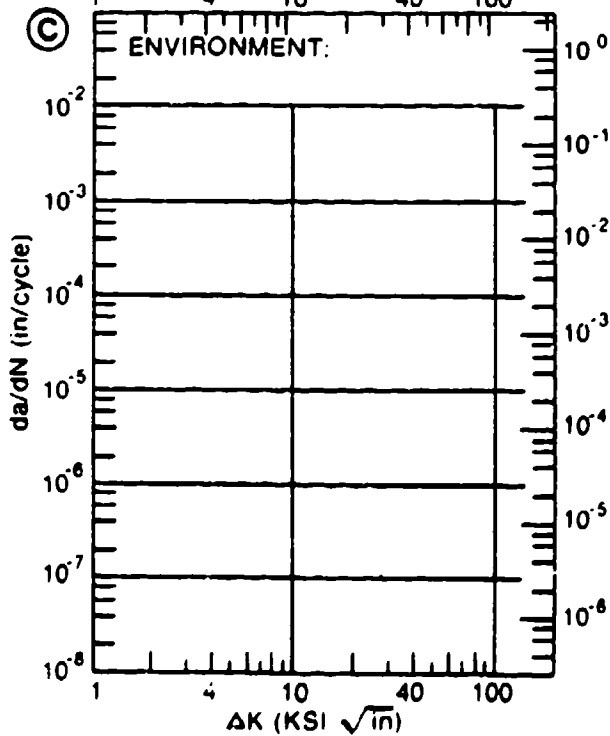
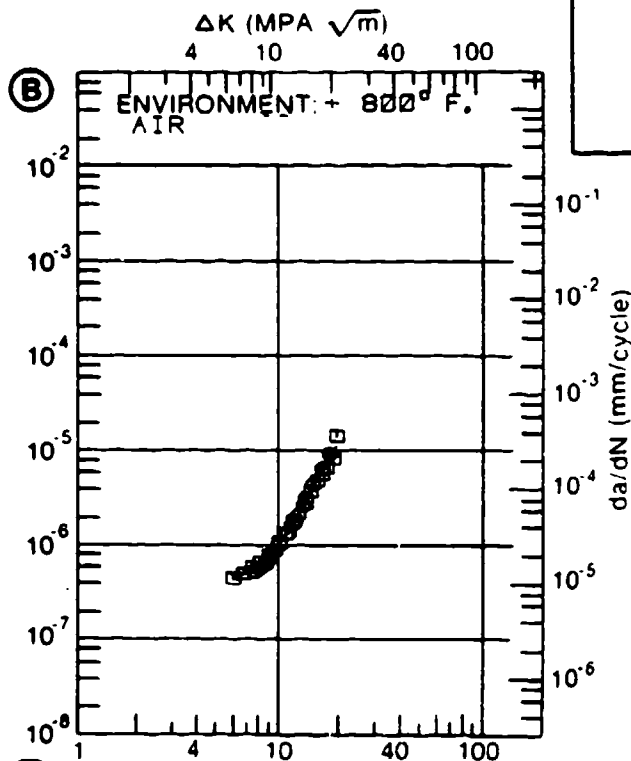
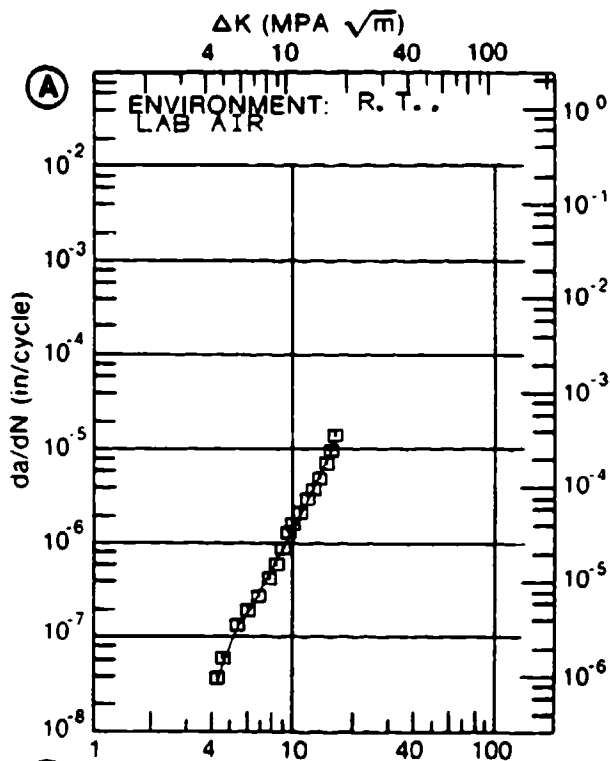


Figure 4.16.3.7

TABLE 4.16.3.8

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.8 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-8AL-1MD-1V | | | |
|------------------------|----------|------------------------|----------------------|---|---|
| CONDITION: | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= DRY CCL4 | E= WATER SAT CCL4 | | |
| K MAX MIN | A: 28.00 | 581. | | | |
| | B: 29.50 | | 855. | | |
| | C: | | | | |
| | D: | | | | |
| | 30.00 | 751. | 896. | | |
| | 35.00 | 1259. | 1149. | | |
| | 40.00 | 1854. | 1358. | | |
| | 50.00 | 3149. | 2767. | | |
| | 60.00 | 4395. | 5272. | | |
| | 70.00 | 5470. | | | |
| K MAX MAX | A: 74.50 | 5887. | | | |
| | B: 67.50 | | 6317. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 19.95 | 19.48 | | |
| PERCENT ERROR | | | | | |

CONDITION/HT:
 FORM:
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 82651

TITAN.
 ALLOY

TI-8AL-
 1MO-1V

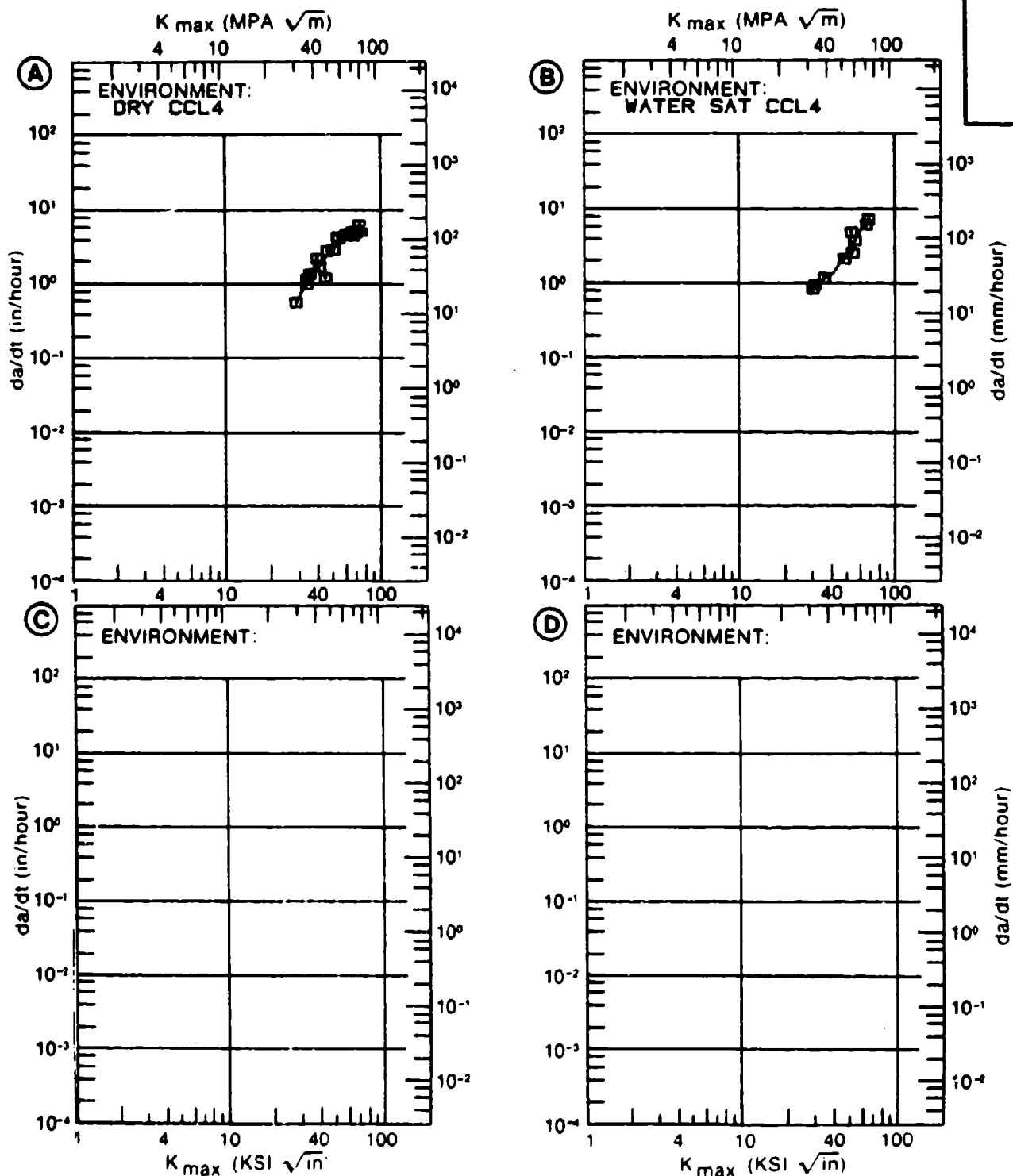


Figure 4.16.3.8

TABLE 4.16.3.9

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.9 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-BAL-1M0-1V | | | |
|------------------------|----|------------------------|---------------------------|-----------------|---|
| CONDITION: | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= DRY CH2CL2 | E= WATER SAT CH2CL2 | E= DRY CH2I2 | |
| K MAX | A: | | | | |
| MIN | B: | | | | |
| | C: | 28.50 | | 1394. | |
| | D: | | | | |
| | | 30.00 | | 1601. | |
| | | 35.00 | | 2163. | |
| | | 40.00 | | 2507. | |
| | | 50.00 | | 2739. | |
| | | 60.00 | | 2740. | |
| K MAX | A: | | | | |
| MAX | B: | | | | |
| | C: | 70.00 | | 2753. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | 0.00 | 1.14 | |
| PERCENT ERROR | | | | | |

CONDITION/HT:
 FORM:
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK:
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 92851

TITAN.
 ALLOY

TI-9AL-
 1MO-1V

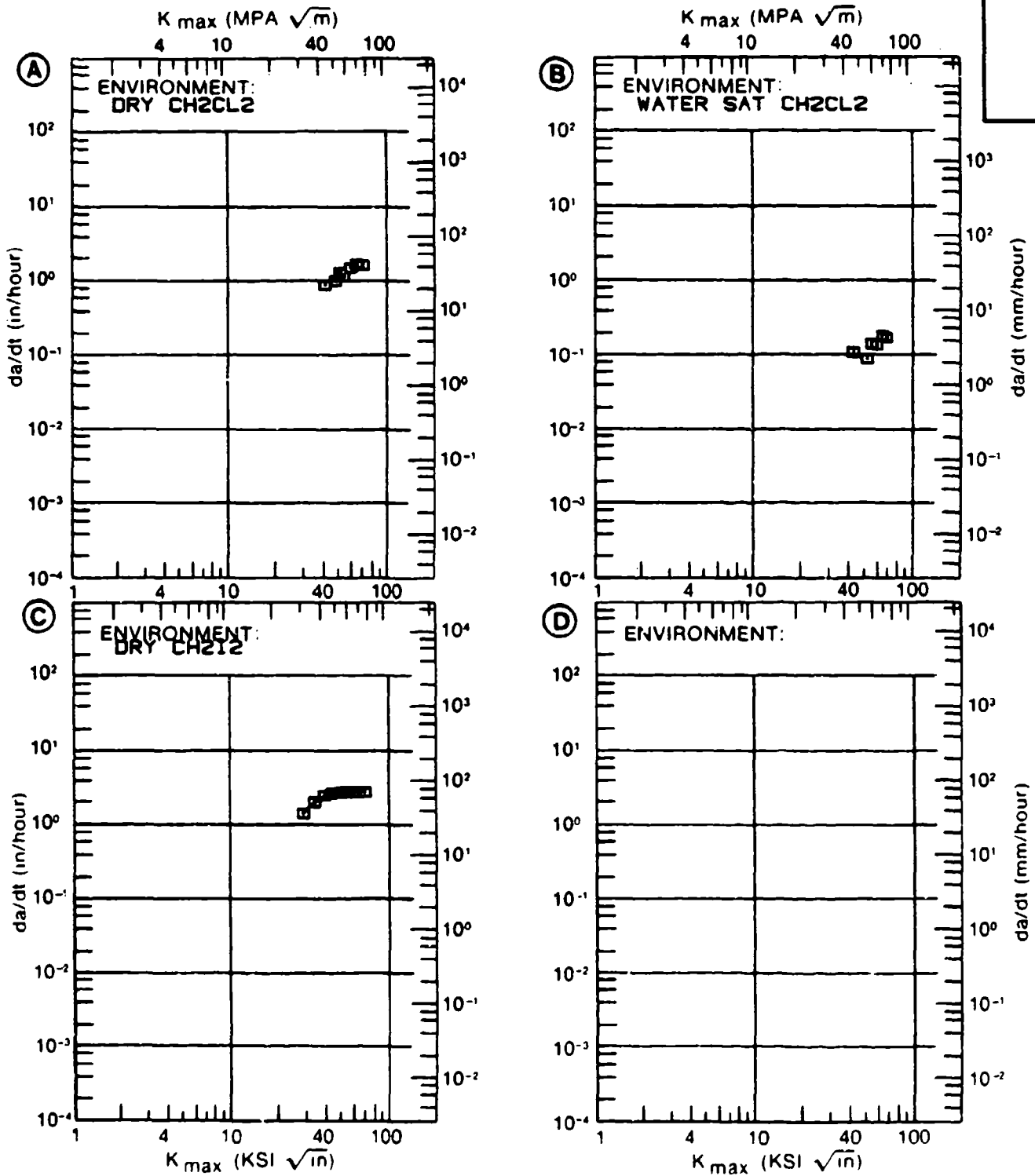


Figure 4.15.3.9

TABLE 4.16.3.10

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.10 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-8AL-1MO-1V | | | |
|------------------------|------------------------------------|---------------|---|---|--|
| CONDITION: | | | | | |
| K MAX (KSI*IN**1/2) | DA/DT (10** ⁻³ IN/HOUR) | | | | |
| | A | B | C | D | |
| | E= 3.5% NAACL | | | | |
| A: | | | | | |
| B: | | | | | |
| MIN | | | | | |
| C: | | | | | |
| D: | | | | | |
| 200.00 | | | | | |
| A: | | | | | |
| B: | | | | | |
| MAX | | | | | |
| C: | | | | | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 0.00 | | | |
| PERCENT ERROR | | | | | |

CONDITION/HT:
 FORM: 0.1" TH SHEET
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH: 150.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.125"
 SPECIMEN WIDTH: 3.000"
 CRACK LENGTH (A₀):
 K_{ISCC}: 22.00 KSI (SQRT IN)
 REFERENCES: 77458

TITAN.
 ALLOY
 TI-8AL-
 1MO-1V

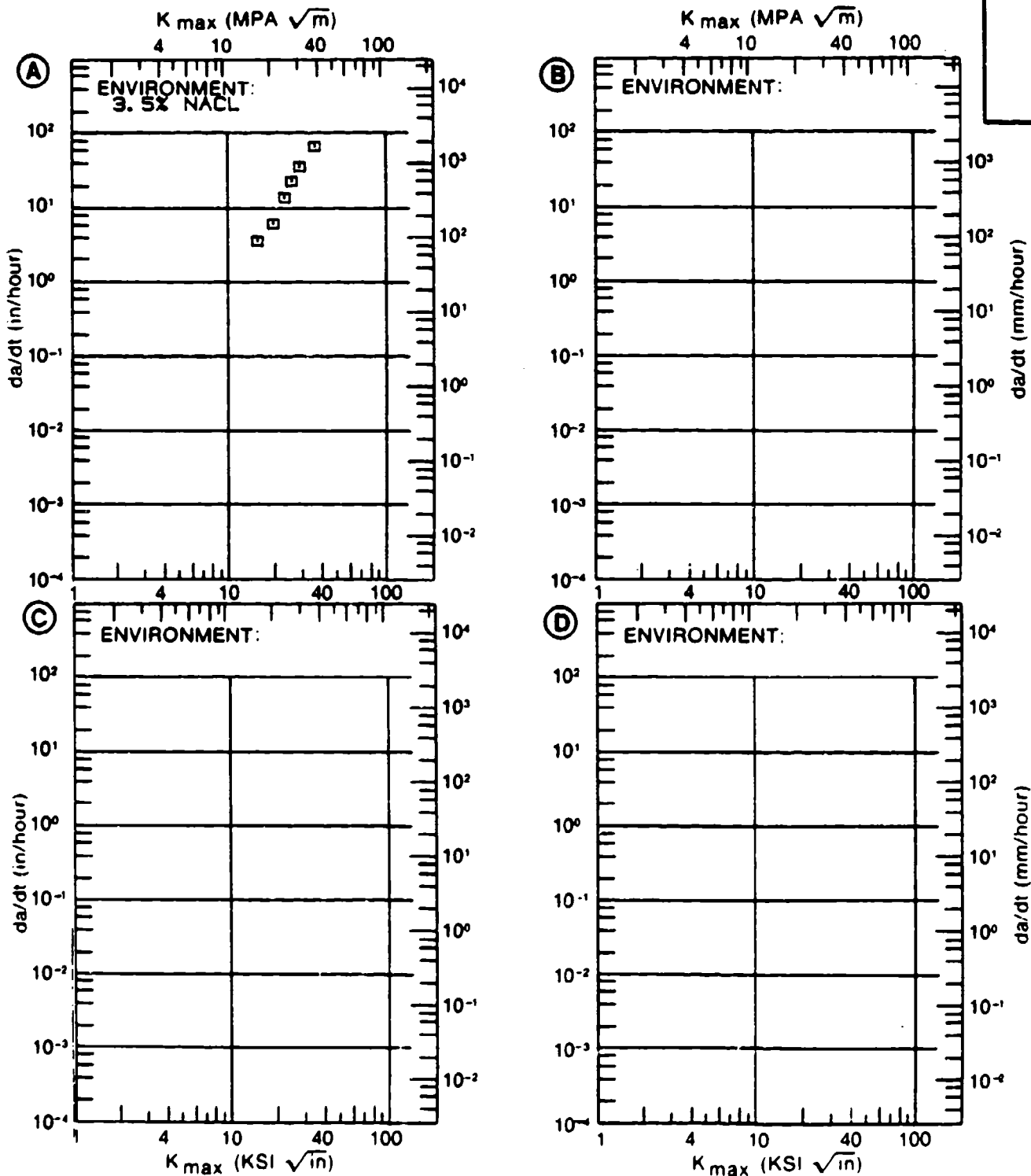


Figure 4.16.3.10

TABLE 4.16.3.11

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.11 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-BAL-1MO-1V | | | |
|------------------------|----------|------------------------------------|---|---|---|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= 3.5% NaCl | | | |
| K MAX | A: 20.80 | 59.2 | | | |
| MIN | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | 25.00 | 11168. | | | |
| K MAX | A: 29.50 | 29280. | | | |
| MAX | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 59.14 | | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: 0.1" TH SHEET
 SPECIMEN TYPE:
 ORIENTATION:
 YIELD STRENGTH: 145.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.100"
 SPECIMEN WIDTH: 8.000"
 CRACK LENGTH (A₀):
 K_{ISCC}: 21.00 KSI (SQRT IN)
 REFERENCES: 04290

TITAN.
ALLOY

TI-BAL-
1MO-1V

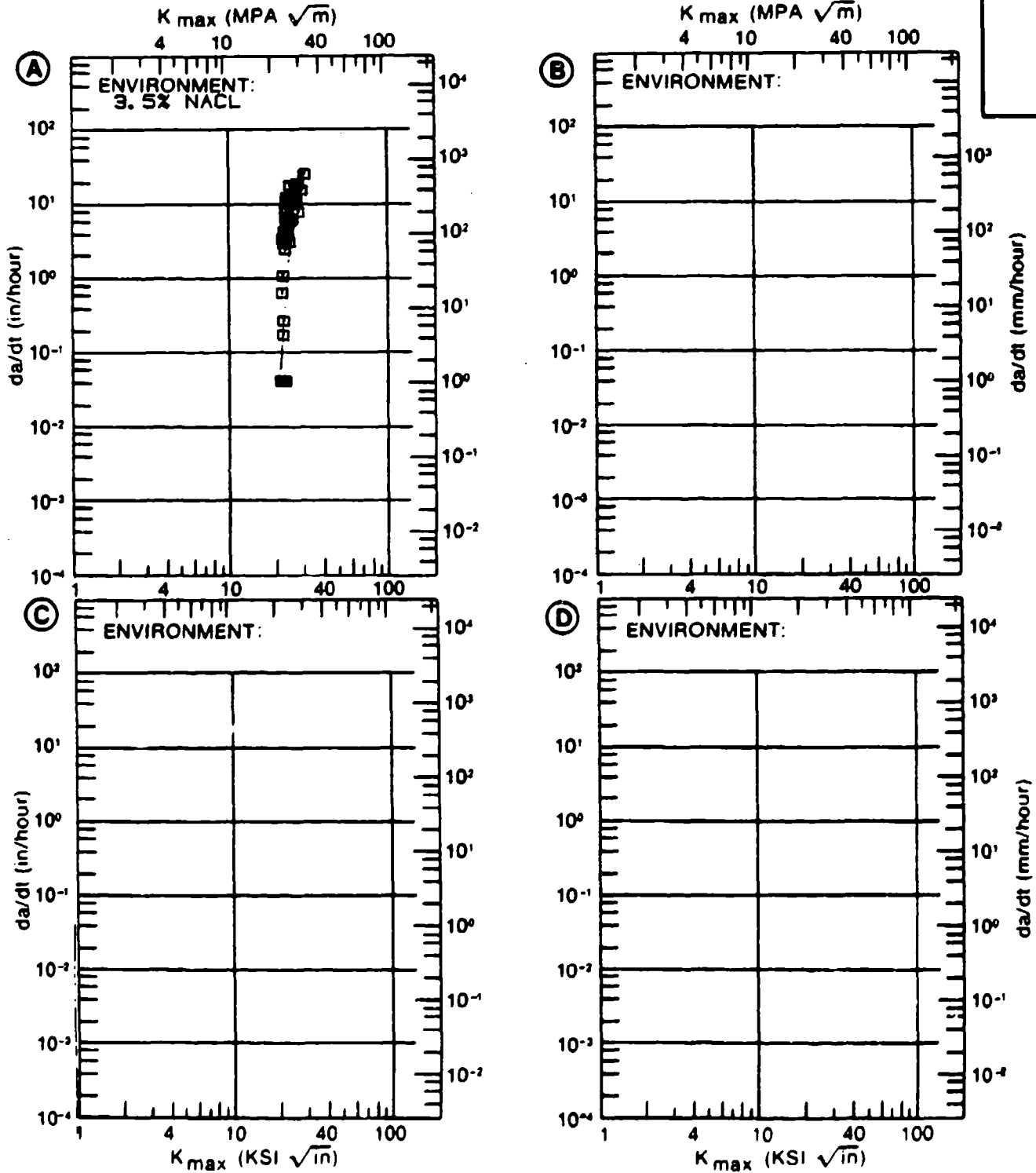


Figure 4.16.3.11

TABLE 4.16.3.12

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.12 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-BAL-1MO-1V | | | |
|------------------------|-------|------------------------------------|-------|---|---|
| CONDITION: MA | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E ⁻⁴ DIST. WATER | | | |
| K MAX MIN | A: | 20.00 | 10.0 | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| | | 25.00 | 110. | | |
| | 30.00 | 601. | | | |
| | 35.00 | 1289. | | | |
| | 40.00 | 1533. | | | |
| K MAX MAX | A: | 49.00 | 1610. | | |
| | B: | | | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 25.16 | | | |
| PERCENT ERROR | | | | | |

CONDITION/HT: MA
 FORM: B, 2" TH PLATE
 SPECIMEN TYPE: SENT
 ORIENTATION:
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.288"
 SPECIMEN WIDTH: 2.888"
 CRACK LENGTH (A_0):
 K_{ISCC}:
 REFERENCES: 01741

TITAN.
ALLOY

T1-8AL-
 1MO-1V

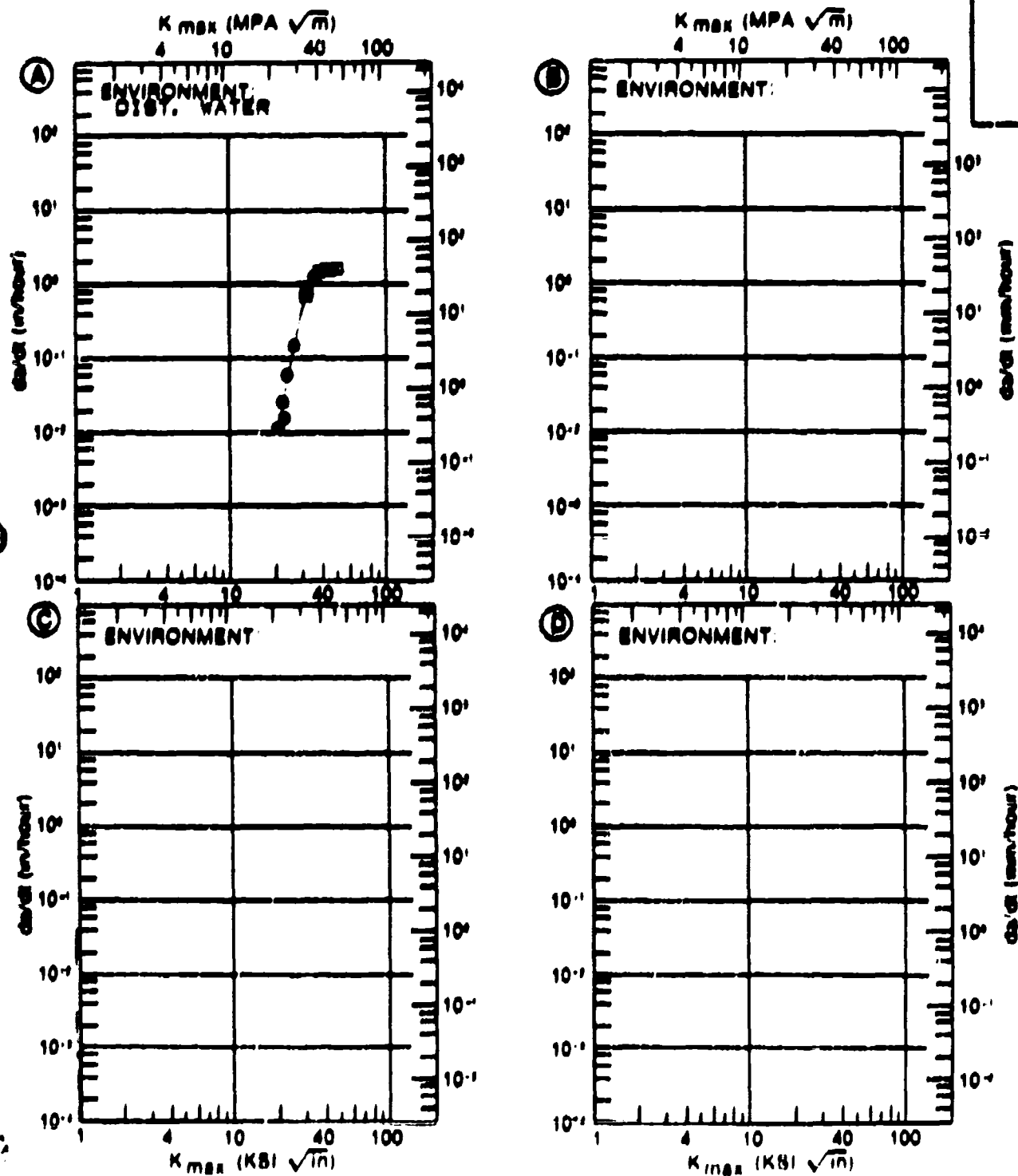


FIGURE 4.16.1.12

TABLE 4.16.3.13

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.13 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-BAL-1MO-1V | | | |
|-----------------------------------|----------|-------------------------|-------------------------|----------------------|---|
| CONDITION: 1520F 1HR WQ | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 9MHCL TICL3 | E= R. T. DIST. WATER | E= R. T. METHANOL | |
| K MAX MIN | A: 16.00 | 430. | | | |
| | B: 26.00 | | 93.3 | | |
| | C: 12.00 | | | 1.98 | |
| | D: | | | | |
| | 13.00 | | | 5.76 | |
| | 16.00 | | | 42.1 | |
| | 20.00 | 1875. | | 129. | |
| | 25.00 | 3467. | | 192. | |
| | 30.00 | 4989. | 182. | 197. | |
| | 35.00 | 6257. | 330. | 188. | |
| 40.00 | 7222. | 488. | 189. | | |
| 50.00 | 8360. | 672. | 256. | | |
| K MAX MAX | A: 60.00 | 8778. | | | |
| | B: 60.00 | | 604. | | |
| | C: 60.00 | | | 527. | |
| D: | | | | | |
| ROOT MEAN SQUARE PERCENT ERROR | | 18.81 | 10.02 | 26.51 | |

CONDITION/HT: 1520F 1HR WQ
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION:
 YIELD STRENGTH: 124.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC}:
 REFERENCES: 93899

TITAN.
 ALLOY

TI-8AL-
 1MO-1V

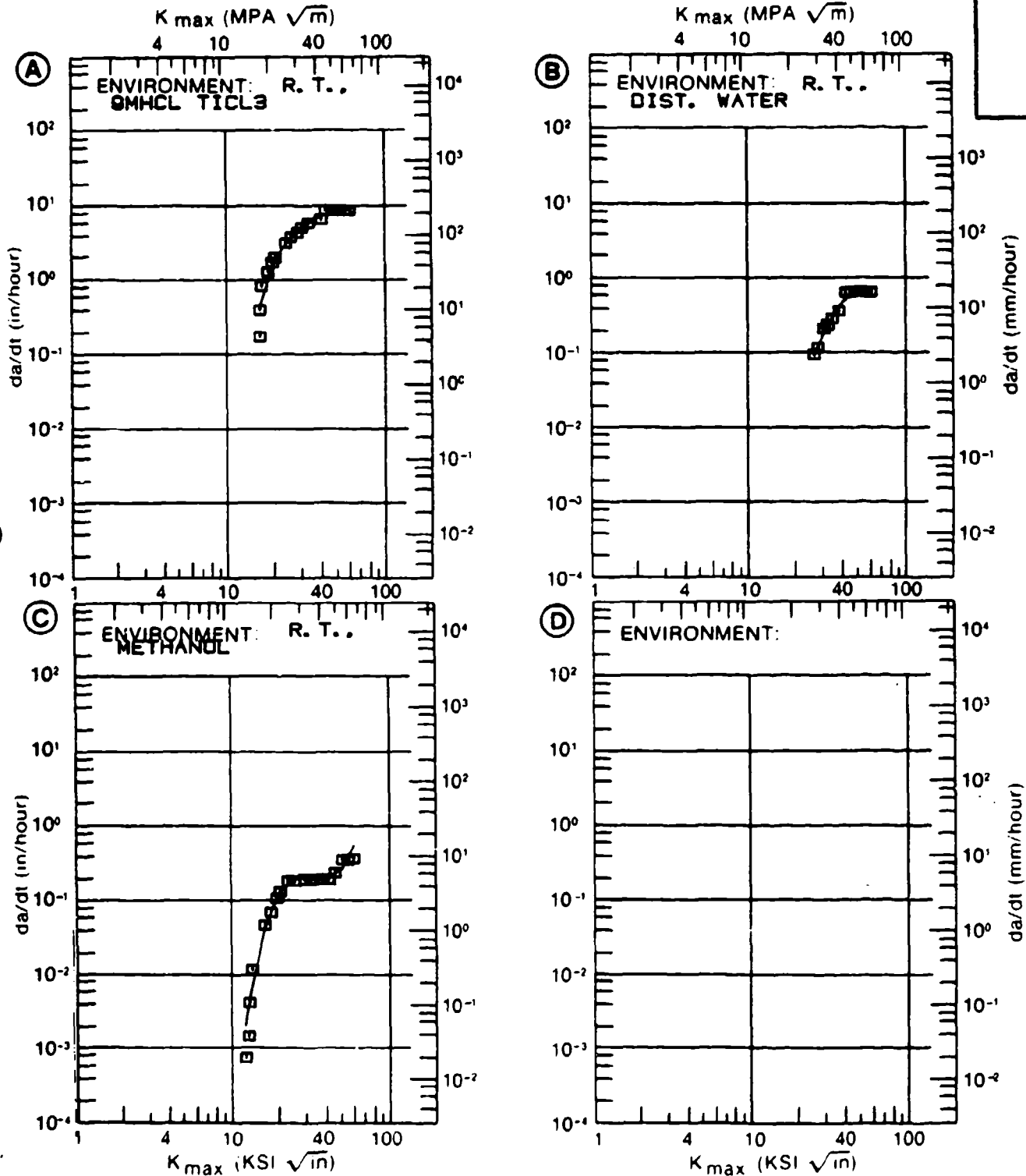


Figure 4.16.3.13

TABLE 4.16.3.14

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.14 INDICATING EFFECT
OF ENVIRONMENT

| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
|------------------------|----------|------------------------|-----------------------|------------------|---|
| | | A | B | C | D |
| | | E= R. T. TI CL4 | E= R. T. GLYCERINE | E= R. T. HNO3 | |
| K MAX MIN | A: 16.80 | 15.2 | | | |
| | B: 26.00 | | 1.64 | | |
| | C: 33.80 | | | 1.35 | |
| | D: | | | | |
| | 20.00 | 23.4 | | | |
| | 25.00 | 32.1 | | | |
| | 30.00 | 37.0 | 1.92 | | |
| | 35.00 | 40.3 | 3.14 | 1.46 | |
| | 40.00 | 44.0 | 5.32 | 2.44 | |
| | 50.00 | 56.3 | 10.2 | 6.40 | |
| | D: | | | | |
| K MAX MAX | A: 60.00 | 81.2 | | | |
| | B: 60.00 | | 9.11 | | |
| | C: 60.00 | | | 7.20 | |
| D: | | | | | |
| ROOT MEAN SQUARE | | 19.57 | 18.00 | 16.69 | |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1520F 1HR, WD
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION:
 YIELD STRENGTH: 124.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH:
 CRACK LENGTH (A_0):
 K_{ISCC} :
 REFERENCES: 93000

TITAN.
ALLOY

TI-6AL-4V

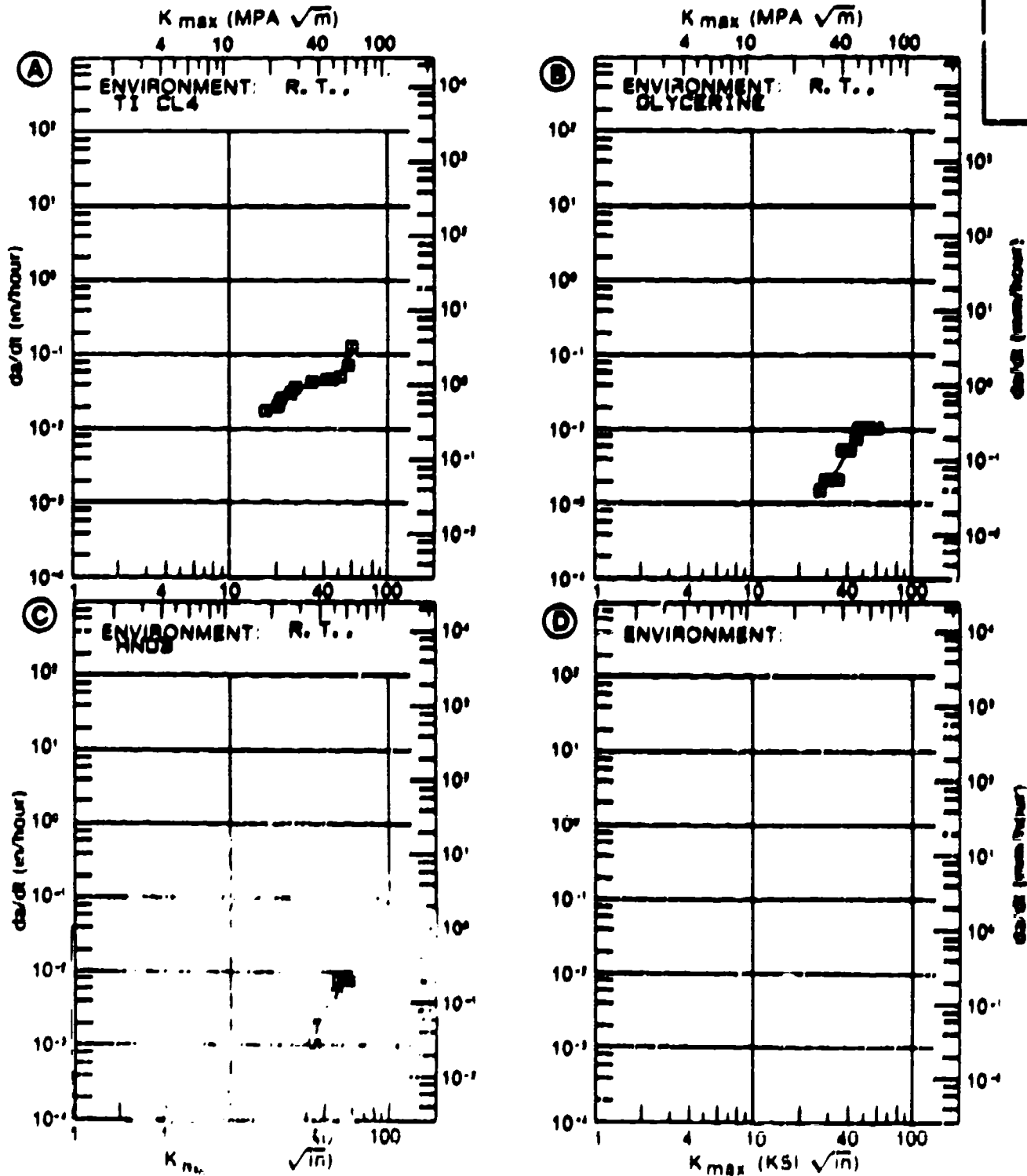


Figure 4.16.3.14

TABLE 4.16.3.15

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.15 INDICATING EFFECT

OF ENVIRONMENT

MATERIAL: TITANIUM TI-8AL-1MO-1V
CONDITION: 1520F 1HR WQ

| K MAX (KSI*IN**1/2) | DA/DT (10** ⁻³ IN/HOUR) | | | |
|------------------------|------------------------------------|-----------------------------------|--------------------------------|---|
| | A | B | C | D |
| | E= R. T. 5H2O/1HCL, -1000 MV | E= R. T. 5H2O/1HCL, -400 MV | E= R. T. 5H2O/1HCL, -200 MV | |
| A: 17.00 | 12.6 | | | |
| B: 15.70 | | 29.0 | | |
| C: 19.50 | | | 5910. | |
| D: | | | | |
| 16.00 | | 35.1 | | |
| 20.00 | 1621. | 1310. | | |
| 25.00 | 2968. | 2062. | | |
| 30.00 | 4042. | 2828. | | |
| 35.00 | 4890. | 3618. | | |
| 40.00 | 5667. | 4463. | | |
| 50.00 | 7553. | 6750. | 5861. | |
| 60.00 | 10704. | 9081. | 15121. | |
| A: 70.00 | 16458. | | | |
| B: 68.00 | | 11808. | | |
| C: 70.00 | | | 15986. | |
| D: | | | | |
| ROOT MEAN SQUARE | 19.71 | 20.45 | 0.15 | |
| PERCENT ERROR | | | | |

CONDITION/HT: 1520F 1HR WQ
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH: 124.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 1.000"
 CRACK LENGTH (A₀): 0.985"
 K_{ISCC}:
 REFERENCES: 83689

TITAN.
ALLOY

TI-6AL-
4V

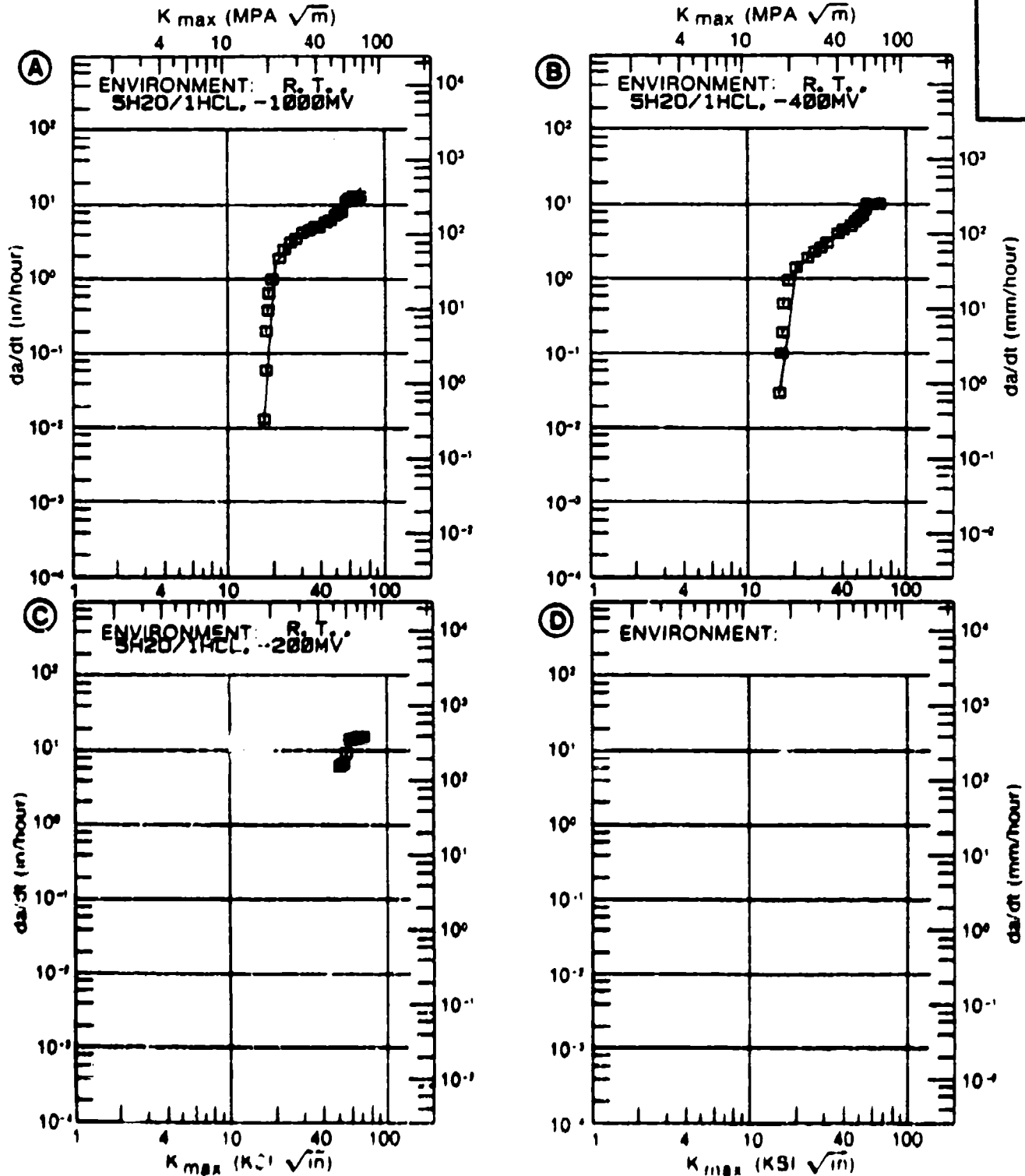


Figure 4.16.3.15

TABLE 4.16.3.16

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.16 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-8AL-1MO-1V | | | |
|-------------------------|----|------------------------------------|------------------------------------|--|---|
| CONDITION: 1520F 1HR WQ | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
| | | A | B | C | D |
| | | E= R. T. 5H2O/1HCL, +500 MV | E= R. T. 5H2O/1HCL, +1000 MV | E= R. T. 5H2O/1HCL, -1.9 TO -1.5 | |
| K MAX | A: | | | | |
| MIN | B: | | | | |
| | C: | 46.50 | | 4942. | |
| | D: | | | | |
| | | 50.00 | | 5303. | |
| | | 60.00 | | 5814. | |
| K MAX | A: | | | | |
| MAX | B: | | | | |
| | C: | 70.00 | | 5752. | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 0.00 | 0.00 | 1.65 | |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1520F 1HR WQ
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: DCB
 ORIENTATION: T-L
 YIELD STRENGTH: 124.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 1.000"
 CRACK LENGTH (A₀): 0.995"
 K_{ISCC}:
 REFERENCES: 83689

TITAN.
 ALLOY
 TI-8AL-
 1MO-1V

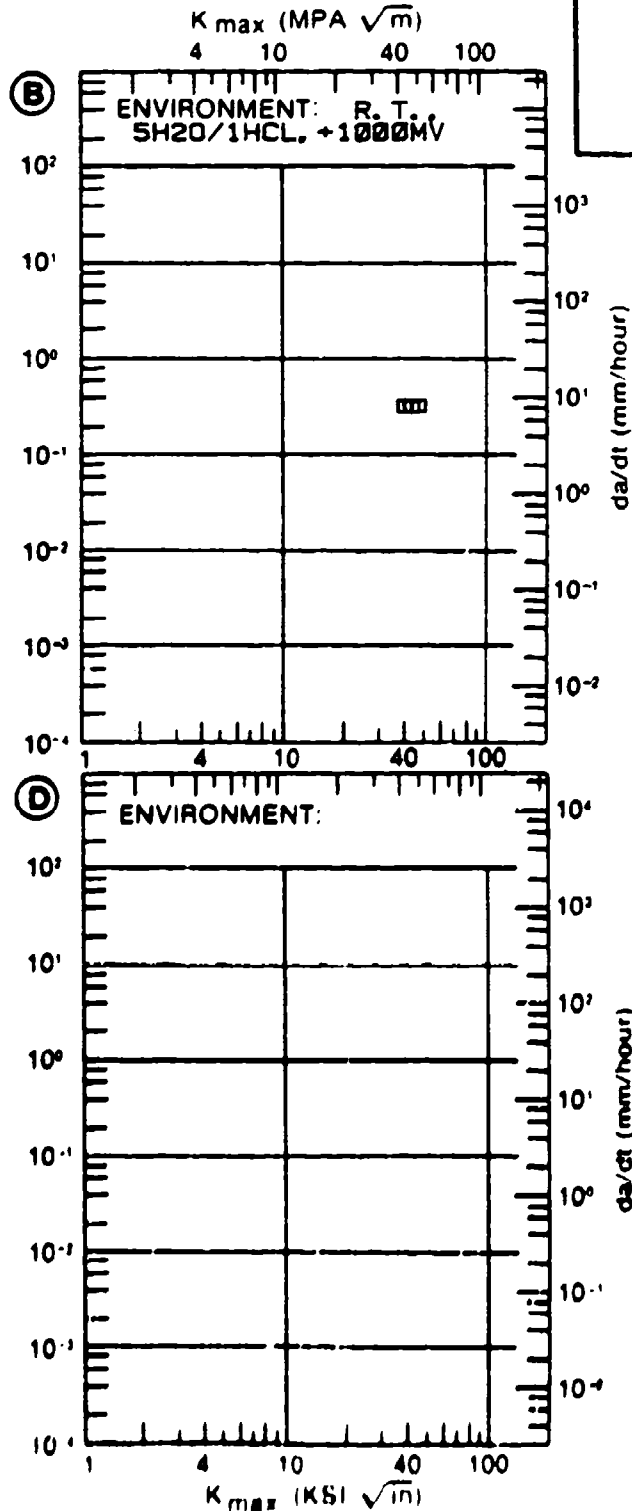
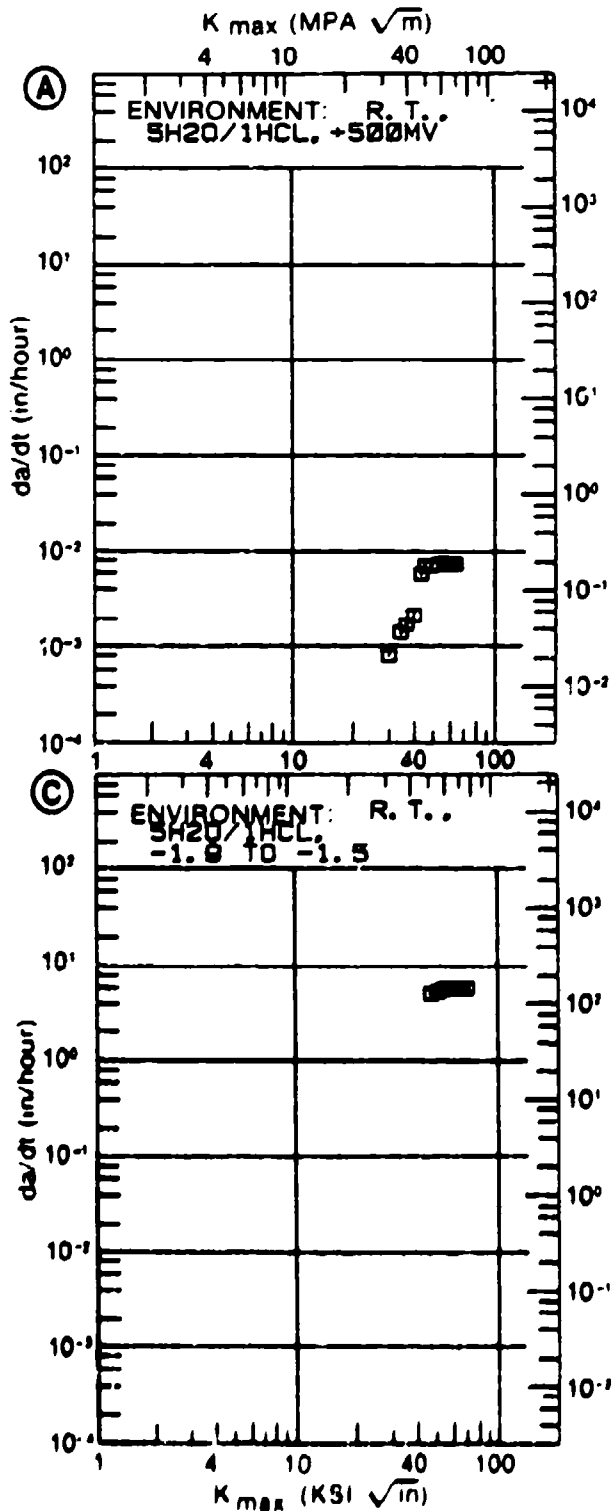


Figure 4.16.3.16

TABLE 4.16.3.17

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.17 INDICATING EFFECT
OF ENVIRONMENT

| K MAX (KSI*IN**1/2) | | DA/DT (10** ⁻³ IN/HOUR) | | | |
|------------------------|----------|------------------------------------|-------------------------|--------------------------|---------------------------|
| | | A | B | C | D |
| | | E= 2100PPM CL 32F | E= 2100PPM CL 72F | E= 2100PPM CL 140F | E= 12100PPM CL 200F |
| K MAX MIN | A: 21.00 | 3113. | | | |
| | B: 17.00 | | 5014. | | |
| | C: | | | | |
| | D: | | | | |
| | 20.00 | | 7759. | | |
| | 25.00 | 4963. | 11801. | | |
| | 30.00 | 6674. | 14738. | | |
| 35.00 | 7737. | 16734. | | | |
| 40.00 | 8432. | 18121. | | | |
| 50.00 | 9637. | 20090. | | | |
| 60.00 | 11481. | | | | |
| K MAX MAX | A: 61.00 | 11729. | | | |
| | B: 57.00 | | 21366. | | |
| | C: | | | | |
| | D: | | | | |
| ROOT MEAN SQUARE | | 6.18 | 3.03 | 0.00 | 0.00 |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1725F FC. 1200F 3HR WQ
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: CANT
 ORIENTATION: T-L
 YIELD STRENGTH:
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 2.000"
 CRACK LENGTH (A₀): 0.250"
 K_{ISCC}:
 REFERENCES: 85855

TITAN.
ALLOY

TI-BAL-
1MO-1V

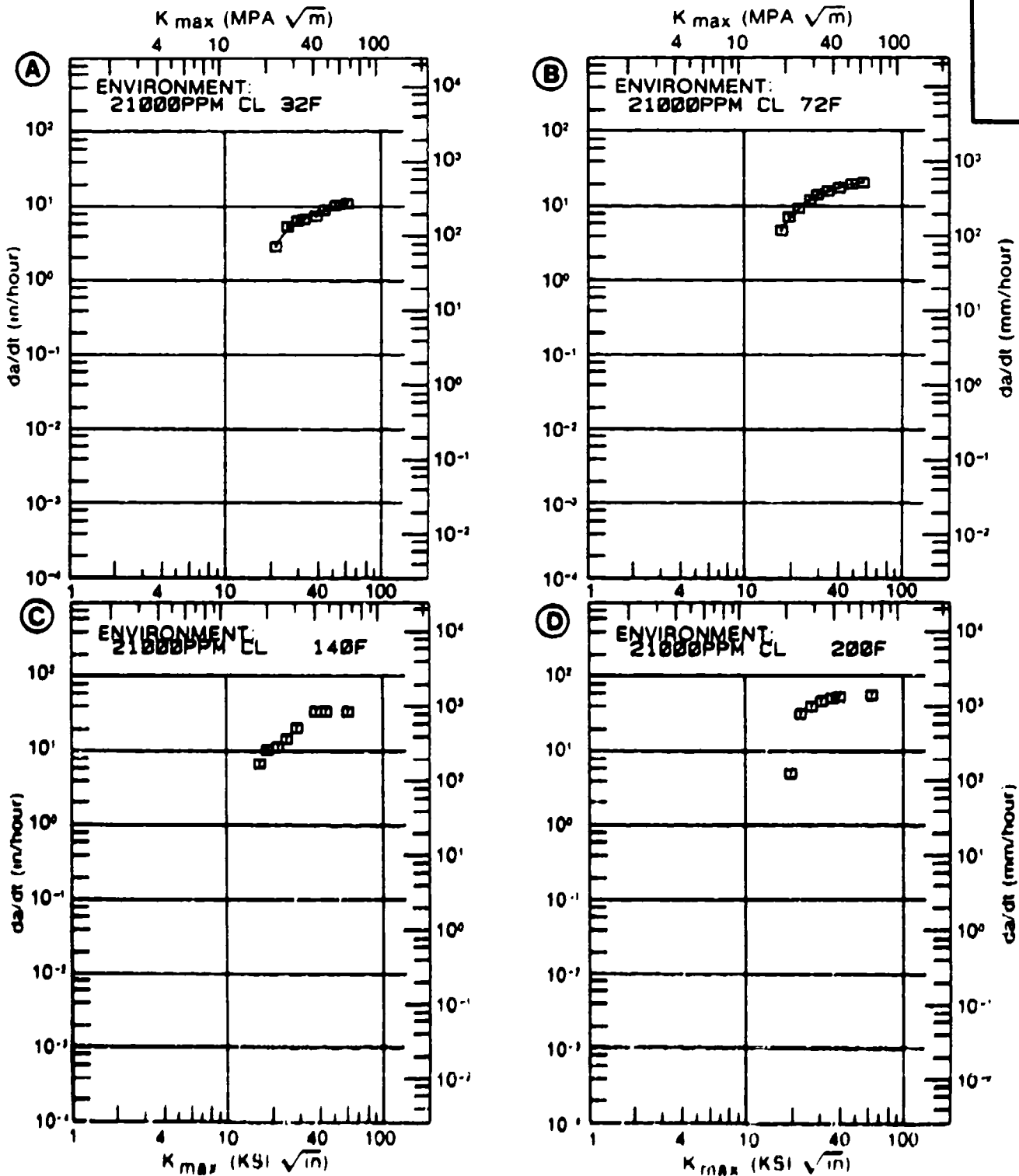


Figure 4.16.3.17

TABLE 4.16.3.18

SUSTAINED CRACK GROWTH RATES AT DEFINED LEVELS
OF STRESS INTENSITY FACTOR

DATA ASSOCIATED WITH FIGURE 4.16.3.18 INDICATING EFFECT
OF ENVIRONMENT

| MATERIAL: TITANIUM | | TI-BAL.-1MO-1V | | | |
|-----------------------------------|-------|--------------------------------|--------------------------------|---------------------------------|----------------------------------|
| CONDITION: 1725F FC, 1200F 3HR WQ | | | | | |
| K MAX (KSI*IN**1/2) | | DA/DT (10**-3 IN/HOUR) | | | |
| | | A | B | C | D |
| | | E=+ 32F WATER, 0.1PPM CL | E=+ 32F WATER, 100PPM CL | E=+ 32F WATER, 6000PPM CL | E=+ 32F WATER, 21000PPM CL |
| K MAX MIN | A: | | | | |
| | B: | | | | |
| | C: | 22.00 | | 4288. | |
| | D: | 16.00 | | | 4246. |
| | | 20.00 | | | 6984. |
| | | 25.00 | | 7535. | 12536. |
| | | 30.00 | | 11710. | 15437. |
| | | 35.00 | | 13591. | 16541. |
| | 40.00 | | 14216. | 17074. | |
| | 50.00 | | 15481. | 19061. | |
| K MAX MAX | A: | | | | |
| | B: | | | | |
| | C: | 58.00 | | 18718. | |
| | D: | 58.00 | | | 23086. |
| ROOT MEAN SQUARE | | 0.00 | 0.00 | 7.67 | 13.28 |
| PERCENT ERROR | | | | | |

CONDITION/HT: 1725F FC, 1200F 3HR WQ
 FORM: 0.2" TH PLATE
 SPECIMEN TYPE: CANT
 ORIENTATION: T-L
 YIELD STRENGTH: 150.0 KSI
 ULT. STRENGTH:

SPECIMEN THK: 0.250"
 SPECIMEN WIDTH: 2.000"
 CRACK LENGTH (A_0): 0.250"
 K_{ISCC} :
 REFERENCES: 05055

TITAN.
ALLOY

TI-8AL-
1MO-1V

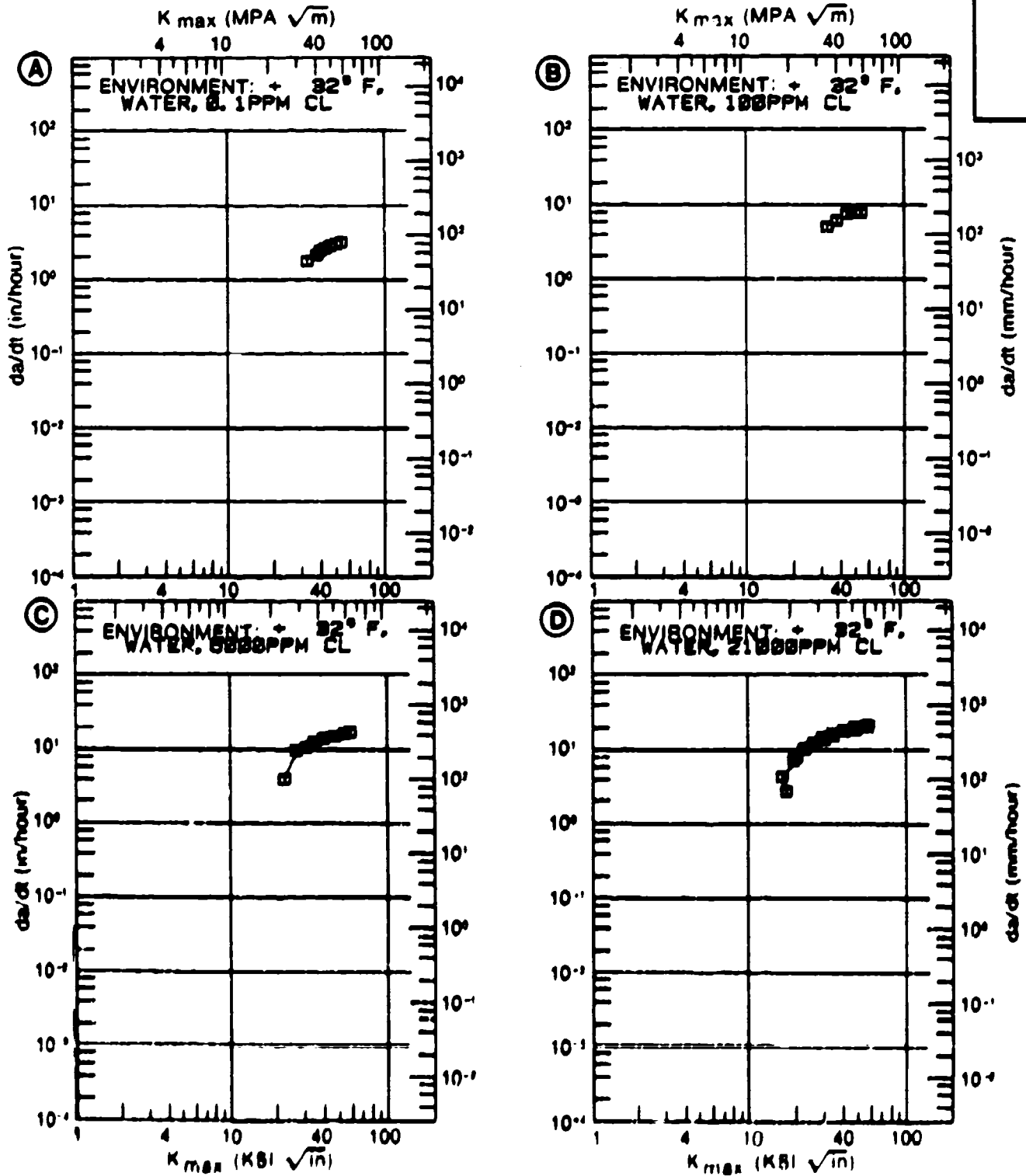


Figure 4.16.3.14

TABLE 4.16.3.19

| TITANIUM | | | | | | | | | | | | |
|-------------|--------------|----------------|----------------------|---------------------------------------|------------|----------------|-------------------|---------|----------|-----------------|------------|-------------|
| COMPOSITION | PRODUCT FROM | TEST TEMP (°F) | YIELD STRENGTH (KSI) | SPECIFICATION | WIDTH (IN) | THICKNESS (IN) | CRACK LENGTH (IN) | K(ISSC) | MEAN DEF | TEST TIME (MIN) | DATE REFER | |
| | | | | | | | | | | | | ENVIRONMENT |
| S | 0 13 | RT | 1-3 | 130 (0.3 PCT NaCl) | 1.000 | 0.125 | CANT | 54.00 | 18.00 | --- | 1967 70931 | |
| P | --- | RT | --- | --- | --- | --- | CANT | 100.00 | 38.00 | --- | 1967 70987 | |
| P | 0 50 | RT | 1-5 | --- | --- | --- | --- | 43.00 | 20.00 | --- | 1969 73386 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 0.150 | CANT | 73.00 | 46.00* | --- | 1967 84327 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 0.250 | CANT | 73.00 | 38.00 | --- | 1967 84327 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 0.250 | CANT | 73.00 | 41.00* | --- | 1967 84327 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 0.500 | CANT | 83.00 | 41.00 | --- | 1967 84327 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 1.000 | CANT | 83.00 | 38.00 | --- | 1967 84327 | |
| P | 1 00 | RT | 1-5 | 123 (0.3 PCT NaCl) | 1.000 | 1.000 | CANT | 83.00 | 37.00 | --- | 1967 84327 | |
| | | | | | | | | | | 37.47 | 1.5 | |
| S | 0 13 | RT | 1-3 | 130 (0.3 PCT NaCl) | 3.000 | 0.125 | SEMT | 53.50 | 22.00* | 60 | 1969 71936 | |
| P | 0 16 | --- | --- | --- | 0.000 | 0.160 | CNT | 0.000 | 21.00 | --- | 1967 70733 | |
| P | --- | RT | 1-4 | 130 (0.3 PCT NaCl) | 1.000 | 0.270 | CANT | 43.00 | 34.00 | --- | 1968 84326 | |
| P | --- | --- | --- | --- | 1.000 | 0.270 | CANT | 44.00 | 34.00 | --- | 1968 84326 | |
| P | --- | RT | 1-4 | 130 (0.3 PCT NaCl) | 1.000 | 0.270 | CANT | 44.00 | 23.00 | --- | 1968 84326 | |
| P | --- | --- | --- | --- | 1.000 | 0.270 | CANT | 102.00 | 22.00 | --- | 1968 84326 | |
| P | --- | --- | --- | --- | 1.000 | 0.270 | CANT | 43.00 | 23.00 | --- | 1968 84326 | |
| P | --- | RT | 1-4 | 130 (0.3 PCT NaCl) | 1.000 | 0.270 | CANT | 102.00 | 27.00 | --- | 1968 84326 | |
| P | --- | --- | --- | --- | 1.000 | 0.270 | CANT | 44.00 | 23.00 | --- | 1968 84326 | |
| P | --- | --- | --- | --- | 1.000 | 0.270 | CANT | 43.00 | 23.00 | --- | 1968 84326 | |
| | | | | | | | | | | 34.37 | 2.3 | |
| P | 0 25 | 31 | 1-4 | 124 (0.5 TO 1 SILVER TO SILVER WATER) | 1.000 | 0.250 | BCB | 0.900 | 93.00 | 20.00 | 1963 80487 | |
| P | 0 25 | 15 | 1-4 | 124 (0.5 TO 1 WATER LNCL) | 1.000 | 0.250 | BCB | 0.900 | 93.00 | 22.70 | 1963 80487 | |

NOTE: DATA WHICH DO NOT MEET MINIMUM SPECIFICATION REQUIREMENTS OF 2.341SSC/TVS/SHAMES

TABLE 4.16.3.19 (Con't)

| COMPTON | PROPERTY | | NEW SPEC VIELD | | TIMBER | SPECIES | | CHECK | | START | DATE | REFER | | | | |
|---------|----------|------|----------------|----|--------|--------------------------------------|----|-------|-------|-------|-------|-------|----|------|-------|-------|
| | TYPE | NO | NO | WT | | NO | WT | NO | WT | | | | | | | |
| 1000 | 100 | 0.75 | 12 | 14 | 120 | COLA | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 1962 | BOAUF | |
| 1000 | 100 | 0.75 | 27 | 14 | 120 | WATER LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 1962 | BOAUF | |
| 1000 | 100 | 0.75 | 26 | 14 | 120 | WATER LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 46 | 17 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 26 | 14 | 120 | WATER LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 23 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | AIR | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 26 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | COLA | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 26 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | COLLEMAN | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 21 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | WATER LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 19 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | GLYCERIN | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 26 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | GLYCERINE LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 19 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | INDIANWELL - PNEUMATIC BRASSK | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 27 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | NETWORK | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 13 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | NETWORK LKCL | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 13 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | PRIMER BRASSK | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 23 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | 2 TO 1 BRASSK TO BRASSK ACTIVATOR | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 20 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | GLYCERINE LKCL - ACTIVATOR | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 20 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | WATER | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 26 | 1962 | BOAUF |
| 1000 | 100 | 0.75 | 07 | 14 | 120 | WATER | 1 | 0.00 | 0.250 | 0.03 | 0.980 | 93 | 00 | 21 | 1962 | BOAUF |

NET DATA CHECKED BY NET TEST PERSONNEL SPECIES IDENTIFICATION BY 2.3.1962/TVS/HEMARD

TABLE 4.16.3.19 (Con't)

| COMPOSITION | TEST SPEC YIELD | | WATER | ENVIRONMENT | SPECIMEN | | CRACK | | MEAN | STAN | TEST | DATE | PAPER | | | | | | |
|---------------|-----------------|-------|-------|-------------|----------|-------|-------|-------------|-------|-------|-------|------|-------|-------|-------------|-------|-------------|-------|-------------|
| | FURN | TRUCK | | | TEMP | OR | STR | ENVIRONMENT | | | | | | WATER | ENVIRONMENT | WATER | ENVIRONMENT | WATER | ENVIRONMENT |
| | (PS) | (T) | | (MSI) | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| 1507 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 16.20 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1508 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 19.20 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1509 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 14.70 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1510 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 13.20 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1511 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 17.00 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1512 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 20.80 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1513 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 27.70 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1514 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 20.80 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1515 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.20 | 19.90 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1516 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 20.00 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1517 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 24.80 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1518 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 23.20 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1519 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 24.20 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |
| 1520 100 MB P | 0.25 | R T | 1-1 | 124 | 0 | WATER | WATER | WATER | WATER | 1.000 | 0.250 | BCB | 0.985 | 73.00 | 18.00 | ---- | 1962 | 82687 | |
| | | | | | | | | | | | | | | | | | | | |

TABLE 4.16.3.19 (Con't)

| TEST NO | SPEC | YIELD (%) | TEMP (F) | CRACK LENGTH (IN) | SPECIMEN | WATER (g) | TI-BAL-100-1V | | K (ISCC) | K (ISCC) | MEAN DEV | TEST TIME (MIN) | DATE REFER |
|---------|------|-----------|----------|-------------------|----------|-----------|---------------|--------|----------|----------|----------|-----------------|------------|
| | | | | | | | W (IN) | W (IN) | | | | | |
| 1520F | 14P | W | 0.25 | 174 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 19.30 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 174 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 19.00 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 124 | T-L | 1.000 | 0.180 | DCB | 0.985 | 93.00 | 23.20 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 184 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 19.30 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 131 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 25.00 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 136 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 13.00 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 140 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 21.80 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 151 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 30.00 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 151 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 26.00 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 194 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 30.20 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 203 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 21.30 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 203 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 22.20 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 203 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 23.90 | 1962 | 83689 |
| 1520F | 14P | W | 0.25 | 203 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 29.00 | 1962 | 83687 |
| 1520F | 14P | W | 0.25 | 203 | T-L | 1.000 | 0.250 | DCB | 0.985 | 93.00 | 26.00 | 1962 | 83689 |

TABLE 4.16.3.19 (Con't)

| CONDITION | TITANIUM | | | | | | | | | | TEST TIME (MIN) | DATE REFER | | | |
|------------------|--------------|----------|------------------------|-------|-------------|-------------------------|-------------|-------------|---------|---------|-----------------|------------|----------|------|-------|
| | PRODUCT FORM | | TEST SPEC OR STR (KSI) | YIELD | ENVIRONMENT | | SPECIMEN | | CRACK | | | | STAN DEV | | |
| | THICK (IN) | TEMP (F) | | | WIDTH (IN) | THICK (IN) | DESIGN (IN) | LENGTH (IN) | K (KSI) | K (KSI) | | | | | |
| 1520F 1HP W9 | P | 0.25 | 205 | T-L | 124.0 | WATER | 1.000 | 0.250 | DCB | 0.985 | 95.00 | 42.00* | ----- | 1962 | 83689 |
| 1520F 1HP W9 | P | 0.25 | 205 | T-L | 124.0 | WATER LICL | 1.000 | 0.250 | DCB | 0.985 | 95.00 | 20.80 | ----- | 1962 | 83689 |
| 1520F 1HP W9 | P | 0.25 | 212 | T-L | 124.0 | SILICONE OIL | 1.000 | 0.250 | DCB | 0.985 | 95.00 | 65.00* | ----- | 1962 | 83689 |
| 1520F 1HP W9 | P | 0.25 | 205 | T-L | 124.0 | WATER LICL | 1.000 | 0.250 | DCB | 0.985 | 95.00 | 22.70 | ----- | 1962 | 83689 |
| 1520F 1HP W9 | P | 0.25 | 412 | T-L | 124.0 | GLYCERINE LICL | 1.000 | 0.250 | DCB | 0.985 | 95.00 | 26.00 | ----- | 1962 | 83689 |
| 1450F 1HP AC P | 1.00 | R T | T-L | 138 | 9.5 | 5% NaCl | ----- | 0.866 | CANT | ----- | 26.40 | ----- | ----- | 1981 | 1R001 |
| 1700F 3HP W9 | P | 1.00 | R T | T-S | 107.9 | 3.5 PCT NaCl | 1.000 | 0.500 | CANT* | ----- | 112.00 | 28.00 | ----- | 1967 | 70931 |
| 1750F 0.5HP FC P | 0.25 | 32 | T-L | 150 | 0 | WATER 21000PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 65.40 | 17.70 | ----- | 1973 | 85855 |
| 1750F 0.5HP FC P | 0.25 | R T | T-L | 150 | 0 | WATER 0.1PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 59.50 | 24.20 | ----- | 1973 | 85855 |
| 1750F 0.5HP FC P | 0.25 | R T | T-L | 150 | 0 | WATER 100PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 58.70 | 20.80 | ----- | 1973 | 85855 |
| 1750F 0.5HP FC P | 0.25 | R T | T-L | 150 | 0 | WATER 21000PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 67.40 | 14.00 | ----- | 1973 | 85855 |

*NOTE: DATA WHICH DO NOT MEET MINIMUM SPECIMEN THICKNESS REQUIREMENTS OF 2.5(KSICC/TYS)SQUARED

TABLE 4.16.3.19 (Con't)

| CONDITION | | - PRODUCT - | | TEST SPEC YIELD | | TITANIUM | | TI-BAL-1MD-1V | | K(ISSC) | | STAN | | TEST | | | |
|-----------|---|-------------|-----|-----------------|-----|----------|----------------------------|---------------|-------|---------|--------|---------------|-------|------|-------|-------|-------|
| | | THICK | OR | TEMP | DR | STR | ENVIRONMENT | WIDTH | THICK | DESIGN | LENGTH | K(I) | MEAN | DEV | TIME | DATE | |
| | | (IN) | | (F) | | (KSI) | | (IN) | (IN) | (#-50) | (IN) | (RSI*SORT IN) | | | (MIN) | REFER | |
| | | | | | | | | W | B | A | | | | | | | |
| 1775 | 0.5HR FC P TO 1200F, 1200F 0.5HR AC, 1200F 3HR AIR/QUI QUENCH | 0.25 | T-L | RT | 150 | 0 | WATER 6000PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 60.30 | 18.40 | | ---- | 1973 | 85833 |
| 1750 | 0.5HR FC P TO 1200F, 1200F 0.5HR AC, 1200F 3HR AIR/QUI QUENCH | 0.25 | T-L | 140 | 150 | 0 | WATER 21000PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 62.10 | 14.70 | | ---- | 1973 | 85833 |
| 1750 | 0.5HR FC P TO 1200F, 1200F 0.5HR AC, 1200F 3HR AIR/QUI QUENCH | 0.25 | T-L | 200 | 150 | 0 | WATER 21000PPH CHLORIDE | 2.000 | 0.250 | CANT | 0.200 | 66.30 | 19.40 | | ---- | 1973 | 85833 |
| 1800F | 1HR AC P TO 1200F, 1200F 0.5HR AC, 1200F 3HR AIR/QUI QUENCH | 0.60 | T-S | RT | 120 | 4 | 3.5 PCT NAACL | 1.000 | 0.500 | CANT* | ---- | 88.00 | 23.00 | | ---- | 1967 | 70921 |
| 2000F | 0.5HR AC P TO 1200F, 1200F 0.5HR AC, 1200F 3HR AIR/QUI QUENCH | 1.00 | T-L | RT | 115 | 1 | 3.5% NAACL | ---- | 0.866 | CANT | ---- | ---- | 47.30 | | ---- | 1981 | NR001 |

TABLE 4.17.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY Ti-60/30/2Fe/2Al AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | (NUMBER OF SPECIMENS) |
|-----------------------------|---|-----------------------|
| | | PLATE |
| CONDITION/HT | L-I | L-I |
| STA. REAGED AT 1100F 6HR | 54.0 ± 1.0 (3) | 53.9 ± 1.0 (3) |
| | | --- |

TABLE 4.17.2.1

| CONDITION | TITANIUM TI-8MOB2FF3AL K11C | | | | | | | | | | | | | |
|---------------------------------|-----------------------------|------------|---------------|-----------------|-------------|------------|-------|------------|-------|-------------------|--|----------|------|----------------|
| | --PRODUCT-- FORM | THICK (IN) | TEST TEMP (F) | SPECIMEN ORIENT | YIELD (KSI) | WIDTH (IN) | | THICK (IN) | | CRACK LENGTH (IN) | 2.9% CRACK (K1C1)/TYS)±2 (K1C1) MEAN (KBI±BORT IN) | STAN DEV | DATE | REFER |
| | | | | | | W | B | A | B | | | | | |
| STA. REAGED AT 1100F 6HR | P | 1.00 | R.T. | L-T | 170.0 | 1.989 | 0.998 | CT | 1.001 | 0.26 | 53.00 | | ---- | 86429 |
| | | 1.00 | | | 170.0 | 1.990 | 1.002 | CT | 0.994 | 0.24 | 53.10 | | ---- | 86429 |
| | | 1.00 | | | 170.0 | 1.995 | 1.005 | CT | 0.995 | 0.29 | 53.90 | 54.0/ | 1.0 | ---- |
| STA. REAGED AT 1100F 6HR | P | 1.00 | R.T. | T-L | 177.0 | 1.991 | 0.991 | CT | 0.987 | 0.23 | 53.40 | | ---- | 86429 |
| | | 1.00 | | | 177.0 | 1.995 | 0.998 | CT | 1.008 | 0.24 | 55.00 | | ---- | 86429 |
| | | 1.00 | | | 177.0 | 1.993 | 0.996 | CT | 1.014 | 0.23 | 53.20 | 53.9/ | 1.0 | ---- |
| 1475F 1.5 HR. 10.1000F 8 HR. AC | E | 3.00 | R.T. | | 155.0 | 1.498 | 0.750 | CT | 0.747 | 0.12 | 34.10 | | | 1973 87230 (1) |
| | | 3.00 | | | 155.0 | 1.500 | 0.750 | CT | 0.776 | 0.14 | 36.30 | | | 1973 87230 (1) |
| | | 3.00 | | | 155.0 | 1.498 | 0.750 | CT | 0.766 | 0.12 | 34.30 | 34.9/ | 1.2 | |

NOTES:
 (1) COMPOSITION (WT PERCENT) 2.26AL, 7.99V, 8.17MO, 0.022C, 0.018N, 0.007OH, 0.160, 0.006CU
 ALPHA PRECIPITATE IN BETA MATRIX
 STRAIGHTNESS OF CRACK FRONT MAY NOT MEET ASTM E399-72 REQUIREMENTS

TABLE 4.18.2.1

| TITANIUM 115AL2.5SN(ELI) K(IC) | | | | | | | | | | | | | | | |
|--------------------------------|------|------------|----------|-----|--------|----------------------|------------|------------|--------|-------------------|--------------------------------------|--------------------------|---------------------|-------|-----|
| CONDITION | FORM | THICK (IN) | TEMP (F) | SFC | ORIENT | YIELD STRENGTH (KSI) | WIDTH (IN) | THICK (IN) | DESIGN | CRACK LENGTH (IN) | 2.5σ (K(IC)/TYS) ^{0.2} (IN) | K(IC) MEAN (KSI±0.01 IN) | K(IC) STAN DEV (IN) | DATE | REF |
| | | | | | | | | | | | | | | | |
| ANNEALED | F | 17.00 | 423 | --- | --- | 186.0 | 2.000 | 1.006 | CT | 1.010 | 0.32 | 66.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 66.60 | 1970 | 88439 | |
| | | | | | | | | | | | | 61.10 | 1970 | 88439 | |
| | | | | | | | | | | | | 74.50 | 1970 | 88439 | |
| | | | | | | | | | | | | 67.00 | 1970 | 88439 | |
| ANNEALED | F | 17.00 | 423 | N-L | --- | 187.0 | 2.000 | 1.000 | CT | 0.930 | 0.34 | 69.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 74.50 | 1970 | 88439 | |
| | | | | | | | | | | | | 67.90 | 1970 | 88439 | |
| | | | | | | | | | | | | 69.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 71.30 | 1970 | 88439 | |
| ANNEALED | F | 17.00 | 423 | N-C | --- | 189.0 | 2.000 | 1.000 | CT | 1.040 | 0.17 | 49.80 | 1970 | 88439 | |
| | | | | | | | | | | | | 52.40 | 1970 | 88439 | |
| | | | | | | | | | | | | 57.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 57.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 57.30 | 1970 | 88439 | |
| ANNEALED (ES) | F | 17.00 | 423 | --- | --- | 186.0 | 2.000 | 1.004 | CT | 1.020 | 0.36 | 71.20 | 1970 | 88439 | |
| | | | | | | | | | | | | 69.80 | 1970 | 88439 | |
| | | | | | | | | | | | | 70.00 | 1970 | 88439 | |
| | | | | | | | | | | | | 70.00 | 1970 | 88439 | |
| | | | | | | | | | | | | 70.00 | 1970 | 88439 | |
| ANNEALED (ES) | F | 17.00 | 423 | --- | --- | 186.0 | 2.000 | 1.000 | CT | 1.010 | 0.35 | 70.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 77.60 | 1970 | 88439 | |
| | | | | | | | | | | | | 83.30 | 1970 | 88439 | |
| | | | | | | | | | | | | 71.70 | 1970 | 88439 | |
| | | | | | | | | | | | | 75.20 | 1970 | 88439 | |

NOTES
 1) COAXIAL STRUCTURE
 2) INTERMEDIATE STRUCTURE BETWEEN PLATELET ALPHA AND FINE EQUIAxed GRAINS

TABLE 4.19.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS DATA OF
TITANIUM ALLOY TIGALANZBN(ELI) AT ROOM TEMPERATURE

| CONDITION/HT | MEAN K _{IC} ± STANDARD (KSI SQRT(IN)) DEVIATION | | (NUMBER OF SPECIMENS) | |
|-----------------------------------|---|-----|-----------------------|-----|
| | L-I | I-I | L-I | I-I |
| 1600F 1 HR. WQ. 1050F 4 HR. AC | 29.6 ± 0.6 (2) | --- | --- | --- |
| 1650F 1 HR. WQ. 1125F 4 HR. AC | 34.0 ± 3.5 (2) | --- | --- | --- |

TABLE 4.19.2.1

| CONDITION | TITANIUM | | | | | | | | | | | | K (IC) STAN DEV | DATE | REFER |
|------------------------------------|------------------------|-----------------------|---------------------------|----------------------------|---------------|---------------------------|--------|-------------------------|-------------------------------|-----------------------------|-------|------|--------------------|------|-------|
| | Ti6Al6V2Sn(ELI) K (IC) | | | | | | | | | | | | | | |
| | PRIMA L | TEST THICK (IN) | SPECIMEN ORIENT (F) | YIELD STRENGTH (KSI) | WIDTH (IN) | SPECIMEN THICK (IN) | DESIGN | CRACK LENGTH (IN) | 2.5° K (IC)/TYS)*2 (IN) | K (IC) MEAN (KSI*ORT IN) | | | | | |
| 1600F 1 HR. WQ. 10:00F 4 HR. AC | P | 1.00 | R T | L-S | 179.0 | 0.477 | 0.231 | NB | 0.215 | 0.10 | 35.10 | 1965 | 04316 | | |
| | | 1.00 | | | 179.0 | 0.479 | 0.230 | NB | 0.184 | 0.07 | 30.10 | 1965 | 04316 | | |
| | | 1.00 | | | 179.0 | 0.477 | 0.230 | NB | 0.222 | 0.08 | 32.10 | 1965 | 04316 | | |
| 1600F 1 HR. WQ. 10:00F 4 HR. AC | P | 1.00 | R. T. | L-T | 179.0 | 0.479 | 0.230 | NB | 0.177 | 0.07 | 30.20 | 1965 | 04316 | | |
| | | 1.00 | | | 179.0 | 0.479 | 0.247 | NB | 0.223 | 0.07 | 29.20 | 1965 | 04316 | | |
| | | 1.00 | | | 179.0 | 0.499 | 0.233 | NB | 0.200 | 0.07 | 30.00 | 1965 | 04316 | | |
| 1500F 1 HR. WQ. 11:25F 4 HR. AC | P | 1.00 | - 320 | L-S | 258.0 | 0.479 | 0.230 | NB | 0.221 | 0.02 | 24.70 | 1965 | 04316 | | |
| | | 1.00 | | | 258.0 | 0.499 | 0.230 | NB | 0.206 | 0.02 | 22.60 | 1965 | 04316 | | |
| 1500F 1 HR. WQ. 11:25F 4 HR. AC | P | 1.00 | R. T. | L-S | 170.0 | 0.499 | 0.230 | NB | 0.203 | 0.13 | 38.60 | 1965 | 04316 | | |
| | | 1.00 | | | 170.0 | 0.479 | 0.230 | NB | 0.191 | 0.12 | 37.50 | 1965 | 04316 | | |
| 1650F 1 HR. WQ. 11:25F 4 HR. AC | P | 1.00 | R. T. | L-T | 170.0 | 0.499 | 0.248 | NB | 0.191 | 0.09 | 31.50 | 1965 | 04316 | | |
| | | 1.00 | | | 170.0 | 0.499 | 0.231 | NB | 0.219 | 0.11 | 36.50 | 1965 | 04316 | | |

TABLE 4.20

REFERENCES FOR THE TITANIUM ALLOY DATA

- 54304 TI-6AL-4V K_C
 Figge, I. E., "Residual Static Strength of Several Titanium and Stainless Steel Alloys and One Superalloy at - 109 F, 70 F, and 550 F", NASA TN D-2045, Langley Research Center (December 1963).
- 57573 TI-6AL-4V K_C
 Anon., "Fracture Toughness and Tear Tests". Air Force Materials Laboratory, Research and Technology Division, Report No. ML-TDR-64-238 (October 1964).
- 58782 TI-5AL-4V K_C
 Anon., "Thick Section Fracture Toughness", ML-TDR-64-236, Boeing-North American (October 1964).
- 60578 TI-6AL-4V(ELI) K_C
 Christian, J. L., Yang, C. T., and Witzell, W. E., "Physical and Mechanical Properties of Pressure Vessel Materials for Application in a Cryogenic Environment", ASD-TDR-62-258, Part III, General Dynamics/Aeronautics (December 1964).
- 66103 TI-5AL-2.5Sn K_C
 Ferguson, C. W., "Hypervelocity Impact Effects on Liquid Hydrogen Tanks", NASA CR-54852, Douglas Aircraft Co., Inc. (March 1966).
- 66218 TI-5AL-2.5Sn K_C
 Tiffany, C. F., Lorenz, P. M., and Hall, L. R., "Investigation of Plane-Strain Flaw Growth in Thick-Walled Tanks", NASA CR-54837, The Boeing Company (February 1966).
- 67821 TI-8AL-1MO-1V K_C
 Walker, E. K., "A Study of the Influence of Geometry on the Strength of Fatigue Cracked Panels", AFFDL-TR-66-92, Northrop Norair (June 1966).
- 68968 TI-5AL-2.5Sn K_C
 Sullivan, T. L., "Uniaxial and Biaxial Fracture Toughness of Extra-Low-Interstitial 5AL-2.5Sn Titanium Alloy Sheet at 20 K", NASA TN D-4016, Lewis Research Center (June 1967).
- 70733 TI-8AL-1MO-1V K_{Isc}
 Smith, H. R., et al., "A Study of Stress Corrosion Cracking by Wedge-Force Loading", Report D6-19768, The Boeing Company, Renton, Wash., Contract N00014-66-C-0365 (June 1967).
- 70887 TI-6AL-4V K_{Isc}
 TI-6AL-6V-2.5Sn K_{Isc}
 TI-8AL-1MO-1V K_{Isc}
 Peterson, M. H., Brown, B. F., Newbegin, R. L., and Croover, R. E., "Stress Corrosion Cracking of High Strength Steels and Titanium Alloys in Chloride Solutions at Ambient Temperature". Corrosion, 23 (5), 142-148 (May 1967).
- 70931 TI-6AL-4V K_{Isc}
 TI-6AL-4V(ELI) K_{Isc}
 TI-6AL-6V-2.5Sn K_{Isc}
 TI-8AL-1MO-1V K_{Isc}
 Judy, Jr., R. W., and Goode, R. J., "Stress-Corrosion Cracking Characteristics of Titanium in Salt Water", Interim Report 6564, Naval Research Laboratory, Washington, D.C., Contracts NONR-610(09), NONR-760(31) and N00014-66-C0365 (July 21, 1967).

TABLE 4.20 (continued)

| | | |
|-------|---|--|
| 71709 | TI-8AL-1MO-1V K_{Ic} | Figge, I. E., "Residual-Static-Strength and Slow-Crack-Growth Behavior of Duplex-Annealed TI-8AL-1MO-1V Sheet", NASA TN D-4358, Langley Research Center (March 1968). |
| 74355 | TI-6AL-4V K_{Isc} | Stanley, J. K., "Solutions to Some Stress Corrosion Cracking Problems in Aerospace Applications", Technical Report TR-0200 (4112.22)-1, Aerospace Corporation, El Segundo, Calif., Contract F04701-68-C-0200 (November 1968). |
| 75386 | TI-4AL-3MO-1V K_{Isc} TI-6AL-4V K_{Isc} TI-8AL-1MO-1V K_{Isc} | Curtis, R. E., et al., "Relationship Between Composition, Microstructure, and Stress Corrosion Cracking (In Salt Solution) In Titanium Alloys", ASM Transactions Quarterly, <u>62</u> (2), 457-469 (June 1969). |
| 75528 | TI-6AL-4V K_{Isc} | Bixler, W. D., "Fracture Characteristics of 6Al-4V Titanium Alloy Forgings Containing Alpha Stringer Microstructure", NASA Final Report CR-99512, The Boeing Company, Seattle, Wash., Contract NAS-9-8809 (January 1969). |
| 76411 | TI-6AL-4V K_{Ic} | Wessel, E. T., et al., "Engineering Methods for the Design and Selection of Materials Against Fracture", Final Technical Report, Westinghouse Research Laboratories, Pittsburgh, Pa., Contract DA-30-069-AMC-602 (T) (June 24, 1966). |
| 77290 | TI-6AL-4V K_{Isc} | Reuter, W. G., et al., "Monitoring of Crack Growth on Ti-6Al-4V Alloy by the Stress Wave Analysis Technique", NASA Report CR-101888, Aerojet General Corporation, Sacramento, Calif. (December 1968). |
| 77456 | BETA da/dt , K_{Isc} TI-8AL-1MO-1V da/dt , K_{Isc} | Katz, Y., "Micro-Mechanical Approach to Stress Corrosion Cracking in Titanium Alloys", Thesis Report No. UCRL-19046, University of California, Lawrence Radiation Laboratory, Berkeley, Calif., AEC Contract W-7405-eng-48 (September 1969). |
| 78535 | TI-6AL-4V K_{Isc} | Masters, J. N., et al., "Fracture and Nitrogen Tetroxide/Sustained Load Flaw Growth in 6Al-4V Titanium", Final Report D2-121397-1, NASA CR-109366, The Boeing Company, Seattle, Wash., Contract NAS7-100 (October 1969). |
| 80104 | TI-5AL-2.5Sn K_{Ic} | Orange, T. W., Sullivan, T. L., and Calfo, F. D., "Fracture of Thin Sections Containing Through and Part-Through Cracks", NASA TN D-6305, Lewis Research Center (April 1971). |
| 80538 | TI-6AL-4V K_{Ic} | Petrak, G. J., "Mechanical Property Evaluation of Beta Forged Ti-6Al-4V", Report APHL-TR-70-291, University of Dayton Research Institute, Dayton, Ohio, Contract F33613-69-C-1471 (January 1971). |

TABLE 4.20 (continued)

| | | |
|-------|---|---|
| 81221 | Ti-6Al-4V da/dt. K_{Isc} | Beck, T. R., et al., "Stress Corrosion Cracking of Titanium Alloys: Studies of Cracks in Thin Specimens; SCC of Ti-6Al-4V in Chloride, Iodide and Fluoride Solutions; Stress Corrosion Cracking in Molten Salts; Electrochemistry of Freshly Generated Titanium Surfaces", Report 20, The Boeing Company, Seattle, Wash., Contract NAS 7-489 (June 1971). |
| 81741 | Ti-8Al-1Mo-1V da/dt | Bucci, R. J., and Paris, P. C., "Observations on Sustained Load Environmental Crack Growth of a Titanium 8Al-1Mo-1V Alloy", Corrosion, <u>27</u> (12) 525-530 (December 1971). |
| 82651 | BETA K_{Isc} BETA III da/dt Ti-8Al-1Mo-1V da/dt | Beck, T. R., and Blackburn, M. J., "Stress Corrosion Cracking of Titanium Alloys: SCC Velocity; Concentration of $TiCl_3$ ", Report 18, The Boeing Company, Seattle, Wash., Contract NAS 7-489 (December 1970). |
| 83222 | Ti-6Al-6V-2Sn K_{Ic} | Amateau, M. F., et al., "F-15 Program Final Report Ti-6Al-6V-2Sn and Ti-6Al-4V Fatigue Crack Propagation", Report No. ATR-72(9990)-3, The Aerospace Corporation, El Segundo, Calif. (September 29, 1971). |
| 83689 | Ti-8Al-1Mo-1V da/dt. K_{Isc} | Beck, T. R., et al., "Fundamental Investigation of Stress Corrosion Cracking", Report D180-15006-1, The Boeing Company, Aerospace Group, Seattle, Washington, Contract NASW-2245 (April 1962). |
| 83984 | Ti-6Al-4V K_c | Peddersen, C. E., and Hylar, W. S., "Fracture and Fatigue-Crack-Propagation Characteristics of $\frac{1}{4}$ -Inch Mill-Annealed Ti-6Al-4V Titanium Alloy Plate", Report G-9706, Battelle, Columbus Laboratories, Columbus, Ohio, Contract N00156-70-C-1336 (November 1, 1971). |
| 84036 | Ti-6Al-4V K_{Isc} | Beacham, C. D., and Meyn, D. A., "The Effect of Thickness Upon Sustained Load Crack Propagation in Ti-6Al-4V Alloy Tested in 3% NaCl Solution", NRL Report 7449, Naval Research Laboratory, Washington, D.C. (August 8, 1972). |
| 84282 | Ti-6Al-4V K_{Isc} | Spurr, W. F., "SST Technology Follow-On Program, Phase I, Titanium Alloy 6Al-4V Extrusion", Report No. FAA-SS-72-06, Boeing Report D6-60206, The Boeing Company, Commercial Airplane Group, Seattle, Wash., Contract No. DOT-FA-SS-71-12 (July 1972). |
| 84290 | Ti-8Al-1Mo-1V da/dt | Smith, H. E., Piper, D. E., and Downey, F. K., "A Study of Stress-Corrosion Cracking by Wedge Force Loading", Engineering Fracture Mechanics, <u>1</u> , p 123-128 (1968), Pergamon Press. |

TABLE 4.20 (continued)

| | |
|-------|---|
| 84306 | TI-6AL-4V K_{Ic} Harrigan, M. J., "B-1 Fracture Mechanics Data for Air Force Handbook Usage", Report TFD-72-501, North American Rockwell, Los Angeles Division, Los Angeles, California (April 21, 1972). |
| 84316 | TI-6AL-2Sn K_{Ic} TI-6AL-2Sn(ELI) K_{Ic} DeSisto, T. S., and Hickey, Jr., C. F., "Low-Temperature Mechanical Properties and Fracture Toughness of Ti-6Al-6V-2Sn", ASTM Proceedings, <u>65</u> , 641-653 (1965). |
| 84326 | TI-8AL-LMO-1V K_{Isc} Report of NRL Progress, Naval Research Laboratory, Washington, D.C. (May 1968). |
| 84327 | TI-8AL-LMO-1V K_{Isc} Report of NRL Progress, Naval Research Laboratory, Washington, D.C. (May 1967). |
| 84328 | TI-6AL-4V K_{Isc} Report of NRL Progress, Naval Research Laboratory, Washington, D.C. (November 1968). |
| 84360 | TI-6AL-4V K_{Ic} , da/dN , da/dt , K_{Isc} TI-6AL-6V-2Sn K_{Ic} , da/dN TI-6AL-6V-2.5Sn K_{Isc} McDonnell Aircraft Company, McDonnell Douglas Corp., St. Louis, Mo., Phase B Test Program, Report MDC A0913 (May 18, 1971). |
| 85034 | TI-6AL-4V K_{Ic} Mitchell, John, "Laboratory Reports on Fracture Toughness Tests", per memo from Ed Cawthorne of February 5, 1973; data sheets from Shultz Steel Company, South Gate, California. |
| 85064 | TI-6AL-4V K_{Ic} Bjeletich, J. G., "Development of Engineering Data on Thick-Section Electron-Beam-Welded Titanium", Report N-LJ-71-18, Lockheed Aircraft Corporation, Lockheed Palo Alto Research Laboratory, Palo Alto Calif., Contract F33615-71-C-1338 (October 12, 1972). |
| 85634 | TI-6AL-4V K_{Ic} "Fracture Toughness and Tensile Properties Data for Ti-6Al-4V Forgings", Shultz Steel Company, South Gate, Calif., Attached to memo from Ed Cawthorne dated March 5, 1973. |
| 85836 | TI-6AL-4V K_{Ic} "B-1 Fracture Toughness Data (K (sub $1c$)) - Rockwell International Corporation, Los Angeles, Calif. (April 24, 1973). |
| 85837 | TI-6AL-4V da/dN "Fracture Toughness Data Collection, Rockwell International Corporation, from B-1 Program", Rockwell International Corporation, Los Angeles, Calif. (April 1973). |

TABLE 4.20 (continued)

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|-------|--|--|
| 85855 | TI-8AL-1MO-1V da/dt, K_{Isc} | Boyd, J. D., "Stress-Corrosion Cracking of Ti-8Al-1Mo-1V in Aqueous Environments: 1. The Kinetics of Subcritical Crack Propagation", Metallurgical Transactions, <u>4</u> (4) 1029-1035 (April 1973). |
| 85857 | TI-6AL-4V K_{Ic} | "Shultz Steel Company - Fracture Toughness Data - May 10, 1973", per memo from Ed Cawthorne of May 10, 1973. |
| 86099 | TI-8AL-1MO-1V da/dN | Wanhill, R. J. H., "A Review and Analysis of Fatigue Crack Propagation in Titanium Alloys at Room Temperature", Report No. NRL-TR-71033U, National Aerospace Laboratory, The Netherlands (February 1971). |
| 86429 | TI-8-8-2-3 K_{Ic} | "Fracture Toughness Data", Progress Report on Materials Test Program, General Dynamics Corporation, Fort Worth Division, Fort Worth, Texas, Contract F33615-72-C-2149 (Received July 6, 1973). |
| 86494 | TI-6AL-6V-2Sn K_{Ic} | Harnsworth, C. L., "Evaluation Report - Fracture Toughness Evaluation of Isothermally Forged Ti-6Al-6V-2Sn STA", Report MXE 72-64, Air Force Materials Laboratory, WPAFB, Ohio (November 15, 1972). |
| 86575 | TI-6AL-4V K_{Ic} , K_{Isc} | "Rockwell International, B-1 Program, da/dN Data, Center-Cracked Tension Specimens", Lockheed California Company, Burbank, CA, Report LR25152 (Received July 1973) (Memo from Ed Cawthorne dated July 10, 1973). |
| 86688 | TI-6AL-4V K_{Ic} , K_{Isc} | Scrowls, D. O., et al., "Evaluation of Stress-Corrosion Cracking Susceptibility Using Fracture Mechanics Techniques", Final Report, Part I, Aluminum Company of America, Alcoa Technical Center, Alcoa Center, PA, Contract NAS8-21487 (May 31, 1973). |
| 86844 | TI-6AL-6V-2Sn da/dN | "Crack Growth Rate Data Generated Under USAF Contract F33615-72-C-2165", Lockheed Aircraft Corporation, Lockheed-Georgia Company, Marietta, GA, Contract F33615-72-C-2165, Data sheets received from AFFDL August 13, 1973. |
| 87230 | BETA III K_{Ic} TI-6AL-6V-2Sn K_{Ic} TI-8-8-2-3 K_{Ic} | DeSisto, T. S., "Fracture Toughness Measurements of Three Titanium Alloy Extrusions", Report AMARC-TR-73-31, Army Materials and Mechanics Research Center, Watertown, MA (July 1973). |
| 88140 | TI-6AL-4V da/dN TI-6AL-4V(ELI) da/dN | Hall, L. R., Finger, R. W., and Spurr, W. F., "Corrosion Fatigue Crack Growth in Aircraft Structural Materials", Report AFML-TR-73-204, Boeing Aerospace Company, Seattle, WA, Contract AF33615-71-C-1687 (September 1973). |

TABLE 4.20 (continued)

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|-------|--|
| 88144 | BETA III K_{Ic} , da/dN TI-6AL-4V K_{Ic} , da/dt |
| | Bjeletic, J. G., "Development of Engineering Data on Thick-Section Electron Beam Welded Titanium", Report AFML-TR-73-197, Lockheed Missiles and Space Company, Inc., Palo Alto, CA, Contract F33615-71-C-1338 (August 1973). |
| 88186 | TI-6-2-2-2-2 K_{Ic} TI-6AL-6V-2Sn K_{Ic} |
| | "Selected Pages from Materials Section of Final Report on Cargo/Tanker Phase IA (AFFDL-TR-73-51) and Lockheed Report SMN 378", Summary Report, Lockheed-Georgia Company, Marietta, GA, Contract F33615-72-C-2165 (February 8, 1974). |
| 88439 | TI-5AL-2.5Sn(ELI) K_{Ic} |
| | Reuter, W. G., "Fracture Toughness of Ti-5Al-2.5Sn ELI Forgings at -423 F", Summary Report, Aerojet-General Corporation, Sacramento, CA (September 9, 1970). |
| 88440 | TI-6AL-4V K_{Ic} |
| | "Titanium-6Al-4V Fracture Toughness and Tensile Test Data of December 19, 1973", Memo from E. W. Cawthorne with fracture toughness data from Shultz Steel Company (December 19, 1973). |
| 88468 | TI-6AL-4V da/dN |
| | Bell, P. D., "Data Sheets for Constant Amplitude Crack Growth Data Generated by Grumman Aerospace Corporation for 2219-T851 Aluminum and Mill Annealed 6Al-4V Titanium Alloy Plate", in letter to J. E. Campbell from Grumman Aerospace Corporation, Bethpage, NY, Contract F33615-72-C-1744 (March 15, 1974). |
| 88575 | BETAC K_{Ic} , da/dN TI-6AL-4V K_{Ic} , da/dN |
| | "Advanced Metallic Air Vehicle Structure Program", Material Property Data Test Report Phase II, Report F2M-6148A, General Dynamics, Convair Aerospace Division, Fort Worth, TX, Contract AF33615-73-C-3001 (January 1974). |
| 88579 | TI-6AL-4V da/dN |
| | "B-1 Program da/dN Data for Aluminum Alloys", Rockwell International Corporation, memorandum to H. D. Moran from E. W. Cawthorne, Battelle's Columbus Laboratories (April 3, 1974). |
| 88700 | TI-6AL-4V K_{Isc} |
| | Gilbreath, W. P., and Adamson, M. J., "The Stress Corrosion Susceptibility of Several Alloys in Hydrazine Fuels", NASA Technical Note, Report NASA TN D-7604, Ames Research Center, Moffett Field, CA (February 1974). |
| 88911 | TI-5AL-2.5Sn da/dN |
| | Wanhill, R. J. H., et al., "Fatigue Crack Propagation Data for Titanium Sheet Alloys - Interim Report No. 3:Ti-5Al-2.5Sn", Report NLR TR 72093 U, National Aerospace Laboratory, The Netherlands (July 1972). |

TABLE 4.20 (continued)

| | |
|-------|---|
| 88962 | <p> TI-6AL-4V K_{Ic} TI-6AL-6V-2Sn K_{Ic} TI-6-2-4-6 K_{Ic} </p> <p> Sparks, R. B., and Long, J. R., "Improvement Manufacturing Methods for Producing High Integrity More Reliable Titanium Forgings", Report AFML-TR-73-301, Wyman-Gordon Company, Worcester, MA, Contract AF33615-71-C-1560 (February 1974). </p> |
| 89004 | <p> TI-6AL-4V K_{Ic}, K_{Isc} </p> <p> "Rockwell International, B-1 Program Titanium K_{Ic}, K_{Ic}, and K_{Isc} Data for HB-01 Revision", with data attached to memorandum from E. W. Cawthorne to H. D. Moran (May 1, 1974). </p> |
| 89504 | <p> TI-6AL-4V K_{Ic} </p> <p> Cervay, R. E., "Mechanical Properties of Ti-6Al-4V Annealed Forgings", Report AFML-TR-74-49, University of Dayton Research Institute, Dayton, OH, Contract F33615-72-C-1282 (March 1974). </p> |
| 90012 | <p> TI-6AL-4V K_{Ic} </p> <p> "Ti-6Al-4V Fracture Toughness Data - Shultz Steel Company, South Gate, CA, of August 8, 1974", with memorandum from E. W. Cawthorne to H. D. Moran of Battelle's Columbus Laboratories (August 8, 1974). </p> |
| 90584 | <p> TI-6AL-4V K_{Ic} TI-6AL-6V-2Sn K_{Ic} </p> <p> DeMay, S., "Improved Fracture Toughness of Titanium", Final Report, Grumman Aerospace Corporation, Bethpage, NY, Contract N62269-73-C-0127 (June 1973) (AD 778 652). </p> |
| 90589 | <p> TI-6AL-6V-2Sn K_{Ic} </p> <p> Fiftal, C. F., and Beck, E. J., "Development of Fracture Mechanics Data for 6Al-6V-2Sn Titanium Alloy", Report MCR-74-43, Martin Marietta Corp., Denver Division, Denver, CO, Contract NAS 9-13599 (January 1974). </p> |
| 90981 | <p> TI-6AL-4V da/dN TI-6AL-6V-2Sn K_{Ic}, da/dN </p> <p> Krupp, W. E., Wimmer, F. T., Pettit, D. E., and Hoepfner, D. W., Data Sheets for Final Report on "Investigation of the Effects of Stress and Chemical Environments on the Prediction of Fracture in Aircraft Structural Materials", Rye Canyon Research Laboratory, Lockheed-California Company, Burbank, CA, Contract F33615-71-C-1688, data sheets received October 21, 1974. </p> |
| 91332 | <p> TI-6AL-4V da/dN </p> <p> Wells, R. E., "New Alloys for Advanced Metallic Fighter-Wing Structures" Northrop Corporation, Aircraft Division, Hawthorne, Ca, AIAA/ASME/SAE 15th Structures, Structural Dynamics and Materials Conference, Las Vegas, NV (April 17-19, 1974). </p> |

TABLE 4.20 (continued)

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|-------|---|---|
| 91793 | BETA III K_{Ic} | Van Stone, R. H., Low J. R. Jr., and Shannon, J. L., Jr., "The Effect of Microstructure on the Fracture Toughness of Titanium Alloys", NASA Technical Report No. 2-Ti, Carnegie-Mellon University, Pittsburgh, Pa., and NASA, Lewis Research Center, Cleveland, Ohio, Research Grant NGR 39-087-047 (December 1974). |
| 91945 | Ti-6Al-6V-2Sn da/dN | Kondas, K. R., et al., "Cyclic-Crack-Growth and Fracture Resistance of Ti-6Al-6V-2Sn as Influenced by Recrystallization Anneal and Interstitial Oxygen Content", NRL Report 7844, Naval Research Laboratory, Washington, D.C. (January 8, 1975). |
| GD006 | | Margolis, W. S., "F-16 Material Test Allowables for Aluminum Alloy 7475, 3.0" Plate - T7351 Temper and 0.5" Plate (92" Width) - T7651 Temper and - T7351 Temper", General Dynamics, Fort Worth Division, Report No. 16PR926, April 1978. |
| GD007 | Ti-6Al-4V da/dN | Margolis, W. S., "F-16 Material Allowables Evaluating Beta Annealed 6Al-4V Titanium Alloy", General Dynamics, Fort Worth Division, Report No. 16PR944, September 1978. |
| GE006 | Ti-6Al-1Mo-1V da/dN | "Fatigue Crack Growth Rate Data on Titanium Ti-8-1-1 Alloy Using K_{Ic} Bar Specimens from the TF34 DTA Effort", Data Sent from M. S. Gilbert, General Electric Co., Evendale, Ohio, October 1982. |
| GE007 | Ti-6Al-4V da/dN | "Fatigue Crack Growth Rate Data on Titanium Ti-6-4 Alloy Using K_{Ic} Bar Specimens from the TF34 DTA Effort", Data sent from M. S. Gilbert, General Electric Co., Evendale, Ohio, October 1982. |
| JEM01 | Ti-6Al-4V K_{Ic} Ti-6Al-6V-2Sn K_{Ic} | Yoder, G. R., Cooley, L. A., and Crooker, T. W., "Enhancement of Fatigue Crack Growth and Fracture Resistance in Ti-6Al-4V and Ti-6Al-6V-2Sn Through Micro-Structural Modification", Journal of Engineering Materials and Technology, Vol. 99, pp. 315-318, October 1977. |
| MA002 | Ti-6Al-4V K_{Ic} , da/dN Ti-6Al-6V-2Sn da/dN | Fracture Toughness of Ti-6Al-4V Plate and Forging, Aluminum 2124-T851 Plate and 7175-T73652 Forging and Fatigue Crack Growth Rate for Ti-6Al-4V Plate and Forging, Ti-6Al-6V-2Sn Extrusion, Aluminum 2124-T851 Plate and Aluminum 7175-T73652 Forging, Data Submitted by D. L. Rich of McDonnell Aircraft Co., St. Louis, MO, Attachment #2, Received March 12, 1982. |
| MA003 | Ti-6Al-4V K_{Ic} , da/dN | Seay, S., and Krieg, J. F., "Wing Carry Through Lug Joint Crack Growth Tests", McDonnell Aircraft Co., St. Louis, MO, Report MDC AJ449, Attachment #3, Submitted by D. L. Rich, March 12, 1982. |

TABLE 4.20 (continued)

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|-------|---|--|
| MA005 | TI-6AL-4V da/dN, K_{Isc} | Garland, K., and Krieg, J. F., "Final Report - Basic Fracture Data for F-18 Material", McDonnell Aircraft Co., St. Louis, MO, Report No 3 NA-66-7KW, Attachment #5, 1977. |
| MA006 | TI-6AL-4V da/dN | Garland, K., and Krieg, J. F., "Evaluation of the Effect of Material Cyclic Softening and Hardening on Crack Initiation Life and Crack Growth, with and without Overloads, as a Function of Stress Ratio", McDonnell Aircraft Co., St. Louis, MO, April 1978. |
| MA011 | TI-8AL-1MO-1V da/dN | "Final Report, F/RP-4C/D Damage Tolerance and Life Assessment Study - Vol. II", McDonnell Aircraft Co., St. Louis, MO, Contract No. AFSC F33657-73-A-0062, Report No. MDC A2883, February 1975. |
| NCO01 | TI-6AL-4V K_{Ic} TI-6AL-4V(ELI) K_{Ic} | "Plane Strain Fracture Toughness Data Sets on Aluminum, Steel and Titanium Alloys", Data Sent from P. G. Porter of Northrop Corp., Hawthorne, CA, March 1, 1982. |
| NCO02 | TI-6AL-4V da/dN TI-6AL-4V(ELI) da/dN | "Fatigue Crack Growth Rate Data on Aluminum, Steel, and Titanium Alloy", Data sent from P. G. Porter, Northrop Corp., Hawthorne, CA, March 1, 1982. |
| NLO01 | TI-6AL-4V da/dN | Data Sheets on Ti-6Al-4V - Fatigue Crack Growth Rate Tests - submitted by W. S. Johnson, NASA Langley Research Center, Hampton, VA, March 1982. |
| NRO01 | TI-6AL-4V K_{Ic} TI-8AL-1MO-1V K_{Isc} | Yoder, G. R., Cooley, L. A., and Crooker, T. W., "Effects of Microstructure and Frequency on Corrosion-Fatigue Crack Growth in Ti-8Al-1Mo-1V and Ti-6Al-4V", Naval Research Laboratory, Washington, D.C., Report 4678, December 1981. |
| PW002 | TI-6-2-4-2 da/dN TI-8AL-1MO-1V K_{Ic} | Beyer, J. R., Sims, D. L., and Wallace, R. M., "Titanium Damage Tolerant Design Data for Propulsion Systems", United Technologies Corp., Pratt and Whitney Aircraft Group, West Palm Beach, FL, Report AFML-TR-77-101, Contract No. F33615-75-C-5130, June 1977. |
| PW003 | TI-6AL-4V da/dN | Fatigue Crack Growth Rate Data on Titanium and Nickel Base Alloy from B. S. Schwartz, Pratt and Whitney Aircraft Group, Government Products Division, West Palm Beach, FL. July 1982. |

TABLE 4.20 (continued)

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| RI005 | <p>CORONA5 K_{Ic} TI-6-2-4-6 K_{Ic} TI-6AL-4V K_{Ic}</p> <p>Cheynutt, J. C., et al., "Fatigue Crack Propagation and Fracture of Titanium Alloys", Rockwell International Science Center, Thousand Oaks, CA, and Department of Metallurgy and Material Science, Carnegie-Mellon University, Pittsburgh, PA.</p> |
| RI006 | <p>TI-6AL-4V K_{Isc}</p> <p>Ferguson, R. R., and Berryman, R. C., "Fracture Mechanics Evaluation of B-1 Materials", Rockwell International, B-1 Division, Los Angeles, CA, Contract No. F33657-70-C-0800, Report No. AFML-TR-76-137, October 1976.</p> |
| UD001 | <p>TI-6-2-4-6 da/dN</p> <p>Carvey, R. R., "Ti-6-2-4-6 Elevated Temperature Modeling of Fatigue Crack Growth Rate Data", University of Dayton Research Institute, Dayton, Ohio, Contract No. F33615-80-C-5011 Technical Memorandum UDR-TM-81-48, December 1981.</p> |
| UD008 | <p>TI-6AL-4V K_{Ic}, da/dN</p> <p>Carvey, R. R., "Beta Processed Titanium 6Al-4V Fracture Properties", University of Dayton Research Institute, Dayton, Ohio, Contract No. F33615-74-C-5024, Technical Memorandum UDRI-TM-75-08, July 1975.</p> |
| UM001 | <p>TI-6AL-4V da/dN</p> <p>Wilson, D. A., "A Statistically Based Investigation of Microstructural Effect on the Fatigue Properties of Titanium and Titanium Alloys", Dissertation to University of Missouri, in Partial Fulfillment of PhD Requirement, December 1978.</p> |