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REPORT ON A VISIT TO THE USA DURING JANUARY 1982  
RELATING TO THE EFFECT OF (U) AERONAUTICAL RESEARCH  
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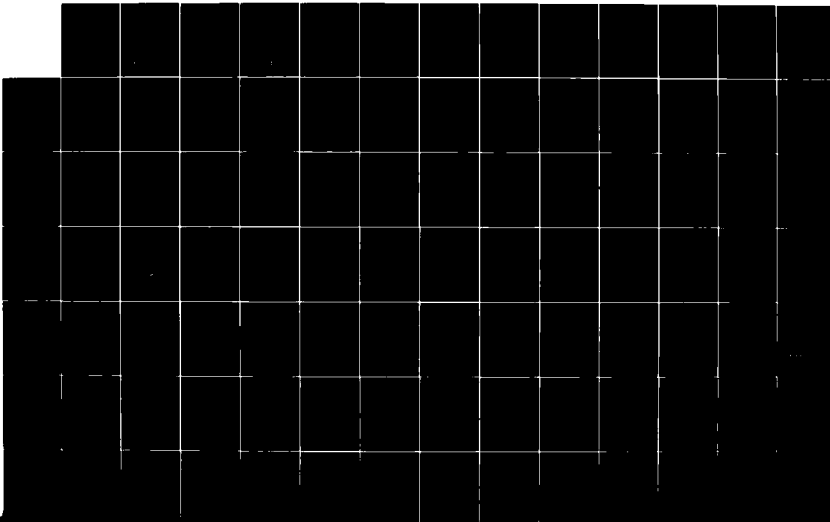
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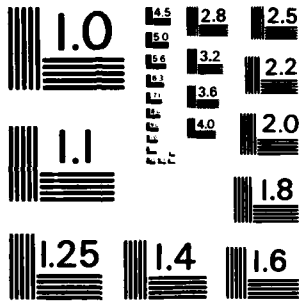
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Structures Technical Memorandum 344 (Supplement)

REPORT ON A VISIT TO THE U.S.A. DURING JANUARY 1982  
RELATING TO THE EFFECT OF TURBULENCE AND OTHER  
METEOROLOGICAL HAZARDS ON AIRCRAFT FLIGHT

Douglas J. SHERMAN

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REPORT ON A VISIT TO THE U.S.A. DURING JANUARY 1982  
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METEOROLOGICAL HAZARDS ON AIRCRAFT FLIGHT

by

Douglas J. SHERMAN

SUMMARY

In January, 1982 the author visited the United States to attend and present a paper at the 12th Conference on Severe Local storms in San Antonio Texas. This report highlights certain aspects of that conference and details other discussions held both before and after the conference with the NOAA Environmental Research Laboratories, the FAA, the NASA Langley Research Centre, and the National Severe Storms Laboratory. This supplement contains appendices 4 to 16 of the report.



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POSTAL ADDRESS: Chief Superintendent, Aeronautical Research Laboratories,  
P.O. Box 4331, Melbourne, Victoria, 3001, Australia.

SLIDE 1. AWS SHIELD.

SLIDE 2. MILITARY APPLICATIONS OF METSAT DATA.

GOOD MORNING/AFTERNOON LADIES AND GENTLEMEN. I'M AL KAEHN, COMMANDER OF THE AIR WEATHER SERVICE (AWS), AND THIS MORNING/AFTERNOON I WOULD LIKE TO GIVE YOU SOME OF MY THOUGHTS ON THE MILITARY APPLICATIONS OF METSAT DATA AND, IN PARTICULAR, THE EVOLUTION OF AWS'S USE OF THE DEPARTMENT OF DEFENSE METSAT, THE POLAR-ORBITING DEFENSE METEOROLOGICAL SATELLITE PROGRAM OR DMSP, ORIGINALLY KNOWN AS DATA ACQUISITION AND PROCESSING PROGRAM, OR DAPP.

I WILL FOCUS ON OUR METSAT USE AT AIR FORCE GLOBAL WEATHER CENTRAL (AFGWC), OUR CENTRALIZED FACILITY, AND BY OUR FIELD UNITS DEPLOYED AROUND THE WORLD. IN ADDITION, I'LL POINT OUT SOME EXAMPLES OF THE DOD MISSION PAYOFFS DMSP HAS PROVIDED IN THE PAST, AND SOME OF OUR IDEAS FOR FUTURE DMSP ENHANCEMENTS.

SLIDE 3. AWS MISSION.

THE PRIMARY MISSION OF AWS IS TO SUPPORT AIR FORCE AND ARMY COMBAT OPERATIONS. IMPORTANT KEYS TO SUCCESSFUL COMBAT OPERATIONS INCLUDE TARGET DETECTION, IDENTIFICATION, TRACKING, AND DESTRUCTION. IN MODERN WARFARE, THE PRESENCE OR ABSENCE OF CLOUDS DIRECTLY IMPACTS THE ABILITY TO SUCCESSFULLY AND ECONOMICALLY PERFORM THESE MISSIONS, AND WITH THE RECENT DEVELOPMENT OF EXTREMELY EXPENSIVE CLOUD-SENSITIVE WEAPONS SYSTEMS (SUCH AS TV, IP, AND LASER-GUIDED BOMBS AND MISSILES), THE ACCURACY OF CLOUD INFORMATION ASSUMES AN EVEN GREATER ROLE.

Administrative routing slip with handwritten signatures and stamps.



SLIDE 4. DATA SOURCES.

AWS USES ALL AVAILABLE DATA TO SATISFY MISSION REQUIREMENTS. PEACETIME CLOUD-DATA SOURCES INCLUDE THE DEFENSE METEOROLOGICAL SATELLITE PROGRAM, NOAA POLAR AND GEOSTATIONARY SATELLITES, WORLDWIDE SURFACE AND UPPER AIR DATA, AND FOREIGN GEOSTATIONARY NETSATS. HOWEVER, DURING WARTIME ONLY DATA SOURCES TOTALLY UNDER DOD CONTROL CAN BE RELIED ON. OF THE DATA SOURCES I JUST MENTIONED, ONLY ONE, DMSP, SATISFIES THIS CONDITION.

SLIDE 5. DMSP MISSION.

IN THIS REGARD, THE MISSION OF THE DMSP IS TO PROVIDE, AT ALL LEVELS OF CONFLICT, GLOBAL ENVIRONMENTAL DATA TO SUPPORT WORLDWIDE DOD OPERATIONS. THIS MISSION DEMANDS AT LEAST TWO OPERATIONAL SPACECRAFT ON ORBIT AT ALL TIMES, WITH THE SENSOR COMPLEMENT AND ORBIT TIMES SELECTED TO PROVIDE THE MAXIMUM ENVIRONMENTAL SUPPORT TO MILITARY DECISIONMAKERS.

SLIDE 6. DMSP HISTORY.

THE DMSP HISTORY HAS BEEN ONE OF CONSTANT EVOLUTION. THE SYSTEM WAS ORIGINALLY CONCEIVED AND DESIGNED IN THE 1960's TO SATISFY IMPORTANT, SPECIFIC MILITARY REQUIREMENTS. THE EARLY VEHICLES CARRIED VIDECON CAMERAS PROVIDING ONLY IR AND VISUAL CLOUD IMAGERY. SINCE ITS INCEPTION, A CORNERSTONE DMSP REQUIREMENT WAS TO PUT DATA IN THE HANDS OF THE MILITARY DECISIONMAKERS AS SOON AS POSSIBLE. THEREFORE, DMSP WAS CONFIGURED TO PROVIDE DATA IN TWO WAYS: THE RECORDED AND DIRECT READOUT DATA MODES.

SLIDE 7. DMSP HISTORY.

IN THE RECORDED DATA MODE, DATA ARE RECORDED ABOARD THE SPACECRAFT AND DOWNLINKED TO READOUT SITES AT LORING AFB, MAINE, AND FAIRCHILD AFB, WASHINGTON. IN THE EARLIER DAYS, THE DATA WERE PASSED TO AFGWC AT OFFUTT AFB, NEBRASKA, BY LANDLINES. TODAY THEY ARE PASSED BY A COMMUNICATIONS SATELLITE. IN RECENT YEARS THE SYSTEM HAS INCLUDED A COMSAT DOWNLINK TO FLEET NUMERICAL OCEANOGRAPHY CENTER IN MONTEREY, CALIFORNIA, AND AN ADDITIONAL READOUT SITE AT KAENA POINT, HAWAII.

THOUGH THE ROUTING OF THE RECORDED DATA HAS NOT CHANGED TOO MUCH DURING THE LIFE OF THE DMSP SYSTEM, THE TYPES OF RECORDED DATA HAVE INCREASED SIGNIFICANTLY. THE FIRST MISSION SENSOR OTHER THAN THE CLOUD IMAGER WAS A GAMMA RADIATION DETECTOR FLOWN IN 1971. THE DMSP MISSION EXPANDED TO INCLUDE AN ADDITIONAL TROPOSPHERIC AND ITS FIRST IONOSPHERIC MISSION IN NOV 1972 WITH THE LAUNCH OF A VEHICLE WITH A TROPOSPHERIC TEMPERATURE SOUNDER AND A PRECIPITATING ELECTRON SPECTROMETER. THE FIRST OPERATIONAL LINESCAN SYSTEM, OR OLS, A VASTLY IMPROVED SYSTEM FOR CLOUD SENSING, WAS FLOWN IN SEPTEMBER OF 1976.

THE INITIAL TRANSPORTABLE TERMINALS, USING THE DIRECT READOUT DATA, SUPPORTED AIR FORCE AND ARMY COMMANDERS AROUND THE WORLD. THE NAVY CAME ON BOARD WITH THEIR REQUIREMENT FOR DIRECT READOUT DATA IN 1971, INSTALLING THEIR FIRST SHIPBOARD CAPABILITY ON THE USS CONSTELLATION.



(OPTIONAL ANECDOTE. AS FOLLOWS: DMSP ANTENNAS WERE LOCATED MIDSHIP BELOW AND ON EITHER SIDE OF THE FLIGHT CHECK. IN TWO SEPARATE INCIDENTS (72 AND EARLY 73), AIRCRAFT (AN A-7 AND AN F-4) BROKE THE ARRESTING CABLE ON LANDING. THE CABLE WRAPPED AROUND THE DMSP ANTENNA (DESTROYING IT IN EACH CASE) AND THE BARRIER HELD. THEREFORE, DMSP (WEATHER) COULD BE CONSIDERED TO HAVE SAVED TWO AIRCRAFT).

TODAY, DIRECT READOUT DATA CONTINUE TO PROVIDE DIRECT CLOUD IMAGERY SUPPORT TO ARMY AND AIR FORCE FIELD COMMANDERS AND NAVY OPERATIONS AFLOAT.

SLIDE 8. UNIQUE DMSP CAPABILITIES.

DMSP CONTINUES TODAY TO GROW AND CHANGE TO MEET DOD REQUIREMENTS. UNIQUE CAPABILITIES ARE DOD COMMAND AND CONTROL UNCONSTRAINED BY EXTERNAL AGREEMENTS, THE CAPABILITY OF ENCRYPTED COMMUNICATIONS INTO COMBAT ZONES, ORBITS AND SENSORS SPECIFICALLY SELECTED TO OPTIMIZE DOD REQUIREMENTS SATISFACTION, FLEXIBILITY TO ALTER COVERAGE TO RESPOND TO RAPIDLY CHANGING DOD SUPPORT NEEDS, AND A SYSTEM DESIGNED TO MINIMIZE DELAY IN READOUT OF CRITICAL RECORDED DATA.

IN ADDITION, TODAY'S DMSP POSSESSES OTHER CHARACTERISTICS EXTREMELY VALUABLE TO AHS: ITS CONSTANT CROSS SCAN HIGH RESOLUTION IMAGING IS VALUABLE FOR SNOW/CLOUD DISCRIMINATION AND "BLACK STRATUS" ANALYSIS. ITS LOW LIGHT NIGHTTIME CAPABILITY IS VALUABLE IN DETERMINING THE MAGNITUDE AND EXTENT OF THE AURORAL OVAL, AND FINALLY, IT HAS A FULL COMPLEMENT OF IONOSPHERIC SENSORS CRITICAL TO MANY DOD SYSTEMS OPERATING IN OR THROUGH THE NEAR EARTH ENVIRONMENT.

SLIDE 9. AIR FORCE DMSP USAGE.

IN THE NEXT FEW MINUTES I WILL AMPLIFY ON THE USE OF RECORDED AND DIRECT READOUT DMSP DATA BY THE AIR FORCE. BRIEFLY, RECORDED DMSP DATA RECEIVED AT AFGWC RESULTS IN DOCUMENTED SAVINGS OF HUNDREDS OF MILLIONS OF DOLLARS PER YEAR. RECORDED DATA ARE USED TO SUPPORT WORLDWIDE OPERATIONS SUCH AS THE RAPID DEPLOYMENT JOINT TASK FORCE, HURRICANE/TYPHOON POSITIONING, AERIAL REFUELING AND STRATEGIC AIR COMMAND AIRCRAFT RECONNAISSANCE MISSIONS. DIRECT READOUT DATA ARE USED BY METEOROLOGISTS IN FORWARD AREAS TO SUPPORT BATTLEFIELD COMMANDERS CONDUCTING COMBAT OPERATIONS. CRITICAL TO THE EFFECTIVENESS OF BOTH CAPABILITIES, ESPECIALLY RECORDED DATA, IS SPACECRAFT COMMAND AND CONTROL.

SLIDE 10. COMMAND AND CONTROL.

TO MEET RIGID OPERATIONAL SUPPORT TIMELINES, COMMAND AND CONTROL MUST BE RESPONSIVE. THEREFORE, THE SPACECRAFT GROUND COMMAND AND CONTROL SYSTEM IS COLLOCATED WITH THE AFGWC. IF WE NEED DMSP DATA THAT ARE NOT NORMALLY COLLECTED, TO SATISFY A SHORT-NOTICE REQUIREMENT, NEW SOFTWARE COMMANDS CAN BE GENERATED AND IMPLEMENTED WITHIN 6 HOURS THROUGH THE CONTROL READOUT SITES.

SLIDE 11. DMSP DATA FLOW. (RECORDED DATA.)

MILITARY REQUIREMENTS FOR FORECASTS OF ICING, TURBULENCE, SEVERE WEATHER, FIELDS OF SMALL CELL CUMULUS AND SNOW/CLOUD DISCRIMINATION DEMAND IMMEDIATE MANUAL APPLICATION OF HIGH-QUALITY 0.3 AND 1.5 NM RESOLUTION VISUAL AND IR IMAGERY DATA. THESE DATA ARE DISPLAYED ON "HARD COPY" TRANSPARENCIES FOR USE BY FORECASTERS AT AFGMC. (AFTER THE DATA ARE NO LONGER OPERATIONALLY USEFUL, THE TRANSPARENCIES ARE ARCHIVED AT THE UNIVERSITY OF WISCONSIN FOR PUBLIC USE.) AT THE SAME TIME, THE DATA FLOW INTO A COMPLETELY AUTOMATED PROCESSING SYSTEM.

SLIDE 12. AUTOMATED PROCESSING SYSTEM.

THE TELEMETRY DATA ARE SPLIT OFF FOR COMMAND AND CONTROL PURPOSES. ATMOSPHERIC AND SPACE ENVIRONMENTAL DATA ARE STRIPPED OUT AND PROCESSED BY SENSOR-UNIQUE SOFTWARE. TEMPERATURE SOUNDER DATA ARE CURRENTLY USED GLOBALLY IN THE STRATOSPHERE. THEY ARE ALSO USED IN THE TROPOSPHERE--BOTH IN THE SOUTHERN HEMISPHERE, AND DATA-SPARSE OCEAN AREAS IN THE NORTHERN HEMISPHERE.

UNIQUE SPACE ENVIRONMENTAL DATA ARE PROVIDED BY THE PRECIPITATING ELECTRON SPECTROMETER, THE PLASMA MONITOR, AND THE VISUAL CLOUD SENSOR. THE VISUAL DATA AND THE ELECTRON SPECTROMETER LOCATE THE AURORAL OVAL--IMPORTANT TO FORECASTS FOR HIGH FREQUENCY RADIO COMMUNICATIONS IN POLAR REGIONS AND THE HIGH LATITUDE EARLY WARNING AND TRACKING RADAR NETWORK IN NORTH AMERICA AND EUROPE. THE PLASMA MONITOR PROVIDES IN-SITU ELECTRON DENSITIES--ESSENTIAL TO SPACE SYSTEM EPHEMERIS CALCULATIONS AND ANOMALY INVESTIGATIONS AS WELL AS TRANSIONOSPHERIC PROPAGATION FOR THE SPACE DETECTION AND TRACKING SYSTEM.

VISUAL AND IR IMAGERY ARE MAPPED INTO A SATELLITE GLOBAL DATA BASE, A DIGITAL-DATA BASE WITH A 3NM RESOLUTION. THIS DATA BASE IS CONSTANTLY UPDATED BY CONTINUOUS ON-LINE PROCESSING OF THE IMAGERY AND IS AVAILABLE IN VISUAL AND IP DISPLAY FOR BOTH HEMISPHERES.

SLIDE 13. SGDB APPLICATIONS.

UNDER THE SHARED METSAT DATA CONCEPT, THE SATELLITE GLOBAL DATA BASE IS PLANNED TO BE PROVIDED TO NOAA/NESS AND FNOC. WE APPLY THE AUTOMATED DATA BASE IN THREE WAYS:

- (1) HIGH QUALITY DISPLAYS ARE SENT BY DIGITAL FACSIMILE TO AIR FORCE COMMAND AND CONTROL CENTERS. THE DATA ARE ALSO RELAYED TO A MYRIAD OF OTHER GOVERNMENT AGENCIES.
- (2) SECOND, DISPLAYS ARE USED AS LARGE OVERLAYS FOR FORECAST APPLICATIONS WITHIN AFGWC.
- (3) THE THIRD APPLICATION IS UNIQUE TO AMS. AFGWC IS A PIONEER IN USING COMPUTERS TO BLEND SATELLITE DATA WITH OTHER DATA AND BUILD AUTOMATED CLOUD ANALYSES WHICH, IN TURN, ARE USED TO INITIALIZE AUTOMATED CLOUD FORECASTS.

SLIDE 14. CLOUD ANALYSIS MODEL. THE AUTOMATED CLOUD ANALYSIS MODEL INTEGRATES THE VISUAL AND IR IMAGERY, AND REMOTE SENSED TEMPERATURE SOUNDINGS, ALONG WITH CONVENTIONAL OBSERVATIONS, TO CREATE A 25 NM RESOLUTION THREE DIMENSIONAL CLOUD ANALYSIS. DATA COVERING HIGH PRIORITY AREAS ARE ANALYZED IMMEDIATELY UPON RECEIPT, WHILE THE NORMAL GLOBAL ANALYSIS IS ACCOMPLISHED EVERY THREE HOURS. THE PROCESS IS TOTALLY AUTOMATED WITH THE EXCEPTION THAT ANALYSIS

IN HIGH PRIORITY AREAS CAN BE MANUALLY MODIFIED IF NEEDED. WE HAVE NOW BEGUN WORK TO DEVELOP A REAL-TIME CLOUD ANALYSIS MODEL THAT WILL ANALYZE ALL SATELLITE DATA IMMEDIATELY UPON RECEIPT. THUS THE REALTIME ANALYSIS WILL ALWAYS INCLUDE THE MOST CURRENT SATELLITE DATA.

SLIDE 15. CLOUD FORECAST MODEL.

THE CLOUD ANALYSIS INITIALIZES THE FINAL STEP IN THE PROCESS--THE AUTOMATED CLOUD FORECAST MODEL. IT IS PROCESSED EVERY THREE HOURS AND FORECASTS CLOUD COVER AND PRECIPITATION OUT TO 48 HOURS IN THE NORTHERN HEMISPHERE AND 24 HOURS IN THE SOUTHERN HEMISPHERE.

SLIDE 16. SUMMARY OF RECORDED DATA MODE CAPABILITIES.

AS YOU CAN SEE, RECORDED DATA ARE USED TODAY AT AFGWC IN A COMPLEX SYSTEM RELYING ON A CONSIDERABLE AMOUNT OF COMPUTER HARDWARE AND SOFTWARE. YET, THE SYSTEM IS EXTREMELY RELIABLE. OVER 95% OF THE DMSP DATA ARE ROUTINELY PROCESSED THROUGH THE SYSTEM AND ARE USED IN THE FORECAST MODELS. NOT ONLY DO UNITS IN THE FIELD RECEIVE ANALYSIS AND FORECAST PRODUCTS FROM AFGWC TO SUPPORT TACTICAL REQUIREMENTS, BUT ALSO THEY HAVE ACCESS TO DMSP DIRECT READOUT DATA.

SLIDE 17. DMSP DIRECT READOUT

THE DMSP DIRECT READOUT DATA CAPABILITY SATISFIES DOD REQUIREMENTS FOR WORLDWIDE, RESPONSIVE, SECURE, HIGH RESOLUTION METSAT INFORMATION. THE SYSTEM IS COMPLETE AND SELF-SUFFICIENT, AND THE TRANSPORTABLE TERMINALS HAVE THEIR OWN POWER SUPPLY AND DATA PROCESSING CAPABILITY. IN THIS MODE, DMSP PROVIDES TIMELY VISUAL AND INFRARED IMAGERY DIRECTLY TO TRANSPORTABLE TERMINALS COLLOCATED WITH BATTLEFIELD COMMANDERS.

SLIDE 18. TACTICAL USES.

THROUGH THESE FEW EXAMPLES: SUPPORT OF CRITICAL DECISIONS IN VIETNAM; SUPPORT TO U.S. FORCES IN DATA DENIED AREAS--SUCH AS ISRAEL; SUPPORT TO EUROPE WHERE WEATHER DATA WILL BE USED AS A WEAPONS MULTIPLIER; SUPPORT OF U.S. READINESS FORCES SUCH AS REDCOM AND TAC; AND SUPPORT OF U.S. RESOURCE PROTECTION EFFORTS IN THE PACIFIC.....I PLAN TO SHOW HOW WE'VE USED THE DMSP IN THE PAST AND HOW WE'RE CURRENTLY USING IT.

SLIDE 19. TARGET ACQUISITION.

GENERAL MOMYER, AF COMMANDER IN VIETNAM, RELATING HIS EXPERIENCE WITH THE DMSP SYSTEM SAID, "AS FAR AS I AM CONCERNED, THIS (DMSP) WEATHER PICTURE IS PROBABLY THE GREATEST INNOVATION OF THE WAR." WHILE DISCUSSING THE SCHEDULING, TARGETING AND LAUNCHING OF STRIKE MISSIONS AGAINST NORTH VIETNAM, IN HIS BOOK HE WENT ON TO SAY THAT, "WITHOUT THEM (MEANING THE DMSP PHOTOS)...MANY MISSIONS WOULD NOT HAVE BEEN LAUNCHED."

SLIDE 20. COMBAT SUPPORT -- VIETNAM.

THE RESPONSIVENESS OF THE DMSP TO MILITARY REQUIREMENTS WAS FIRST DEMONSTRATED DURING THE EARLY STAGES OF VIETNAM WHEN A SATELLITE WAS LAUNCHED TO SUPPORT OUR BOMBING MISSIONS. AF COMMANDERS IN VIETNAM MAKING GO/NO GO DECISIONS AFFECTING STRIKE MISSIONS USED DMSP BECAUSE IT IS A COMPLETE SYSTEM WITH A TACTICAL READOUT CAPABILITY. THE TACTICAL, OR DIRECT READOUT TERMINAL LOCATED IN SAIGON PROVIDED PROCESSED, ANALYZED PICTURES OF THE WEATHER IN THE VARIOUS TARGET AREAS IN A MATTER OF MINUTES AFTER BEING OBSERVED. THIS INFORMATION WAS USED TO UPDATE AND ADJUST STRIKE TARGETS AND THE LIFE SUSTAINING REFUELING AREAS BASED ON THE CURRENT WEATHER OBSERVED BY THE DMSP.

IN LATE 1970, VERY SPECIFIC WEATHER WAS REQUIRED TO SUPPORT THE MISSION TO EXTRACT U.S. PRISONERS OF WAR FROM A NORTH VIETNAMESE PRISON CAMP. THIS MISSION, THE SON TAY PRISON RAID, WAS SCHEDULED TO COINCIDE WITH THE BREAK IN WEATHER BETWEEN TWO TROPICAL STORMS. CONVENTIONAL WEATHER DATA WERE DENIED AND AN AERIAL WEATHER RECONNAISSANCE FLIGHT MIGHT TIP OFF THE OPERATION. THE NEED FOR SECRECY AND LIMITING THE NUMBER OF PEOPLE WHO KNEW OF OUR INTEREST IN THE WEATHER NEAR SON TAY WAS SATISFIED BY THE OPERATIONAL SECRECY AVAILABLE WITH THE DMSP. THE DMSP DATA, PROVIDED TO THE 7TH AF PLANNERS FROM THE DMSP TACTICAL TERMINAL AT SAIGON WERE CRUCIAL IN IDENTIFYING THE BEST WEATHER WINDOW POSSIBLE TO ACHIEVE THE PRECISION TIMING NECESSARY FOR THIS MISSION, YET MAINTAINING THE SECRECY NECESSARY IN SUCH A SENSITIVE MILITARY OPERATION.

SLIDE 21. CRISIS DATA DENIAL.

GLOBAL WAR IS NOT NECESSARY TO AFFECT THE FREE EXCHANGE OF METEOROLOGICAL DATA AMONG NATIONS. INCREASED LOCAL TENSIONS BETWEEN TWO OR MORE NATIONS CAN CUT THE FLOW OF NECESSARY WEATHER DATA. DURING THE YOM KIPPUR WAR ALL NATIONS IN THE AREA OF CONFLICT STOPPED TRANSMISSION OF STANDARD METEOROLOGICAL DATA OVER CIVIL COMMUNICATIONS CIRCUITS - DESPITE INTERNATIONAL AGREEMENTS TO THE CONTRARY - BECAUSE WEATHER DATA COULD POSSIBLY AID OPPOSITION COMMANDERS IN MAKING MILITARY DECISIONS. EARLY IN THE U.S. RESUPPLY EFFORT OF ISRAEL, LOD AIRPORT AT TEL AVIV WAS CLOSED DUE TO HEAVY FOG AND STRATUS AND OUR RESUPPLY FLOW WAS DISRUPTED. WEATHER DATA FROM THE DMSP ENABLED US TO DETERMINE THE WEATHER PATTERN WAS FRONTAL IN NATURE AND TO ACCURATELY

PREDICT CLEARING, ENSURING EARLIEST POSSIBLE COMPLETION OF THE VITAL AIRLIFT DURING THE INITIAL PHASES OF THE WAR. DURING A EUROPEAN WAR, OUR ENEMIES WILL ALMOST CERTAINLY STOP TRANSMITTING WEATHER DATA. IN ADDITION, OUR ALLIES MAY STOP TRANSMITTING WEATHER DATA BECAUSE OF ITS USEFULNESS TO WARSAW PACT COUNTRIES, AND THE ENCRYPTED DMSP DATA AVAILABLE AT TACTICAL TERMINALS IN EUROPE MAY BE THE ONLY WEATHER DATA OUR EUROPEAN FORCES HAVE TO USE. DURING AUG 79, WE USED DMSP TO SUPPORT OPERATIONS IN NICARAGUA FROM THE TACTICAL TERMINAL AT HOWARD AFB, WHEN CONVENTIONAL DATA WERE NOT AVAILABLE IN NICARAGUA DURING THE OVERTHROW OF THE SOMOZA REGIME.

SLIDE 22. COMBAT DEPLOYMENT.

THE U.S. READINESS COMMAND'S MISSION REQUIRES SHORT NOTICE DEPLOYMENT OF A JOINT TASK FORCE TO VIRTUALLY ANY AREA OF THE WORLD. HIGH RESOLUTION SATELLITE DATA, RESPONSIVE TO THE DEPLOYED MILITARY COMMANDER, ARE OFTEN THE SOLE SOURCE OF WEATHER DATA IN A CONTINGENCY AREA WHERE DATA ARE EITHER SPARSE OR DENIED. IN SUPPORT OF U.S. COMMITMENTS TO NATO, THE U.S. REGULARLY DEPLOYS TACTICAL FIGHTER SQUADRONS FROM U.S. BASES TO DESIGNATED ALLIED AIRFIELDS IN EUROPE. DECISIONS TO LAUNCH, DELAY, OR CHANGE REFUELING AREAS; NOT ONLY FOR THE FIGHTER AIRCRAFT, BUT ALSO FOR THE TANKER AIRCRAFT NEEDED FOR REFUELING, ARE OFTEN MADE SOLELY BASED ON THE HIGH RESOLUTION DATA AVAILABLE FROM THE DMSP.

SLIDE 23. DOD RESOURCE PROTECTION.

A DMSP TACTICAL TERMINAL, AS WELL AS RECORDED DATA FROM AFGWC, PROVIDE COVERAGE NECESSARY FOR THE AIR FORCE WEATHER SATELLITE



SUPPORT TO THE JOINT TYPHOON WARNING CENTER (JTWC) LOCATED AT GUAM IN THE PACIFIC. JTWC PROVIDES TYPHOON WARNINGS AND ACCURATE FIXES OF STORM POSITIONS AND ALSO PROVIDES DOD WITH RESOURCE-PROTECTION WARNINGS NECESSARY IN THIS PREDOMINANTLY DATA-SPARSE AREA. IN 1978 AND 1979, MORE THAN HALF OF THE JTWC'S WARNING IN THE WESTERN PACIFIC WERE BASED ON SATELLITE POSITIONS OF TROPICAL CYCLONES. IN THE INDIAN OCEAN, WHERE AIRCRAFT AND LAND-BASED RADAR WERE NOT AVAILABLE, OVER 95 PERCENT OF THE JTWC'S WARNINGS WERE BASED ON SATELLITE FIXES. THIS INFORMATION, REQUIRED BY MILITARY COMMANDERS THROUGHOUT THE PACIFIC, IS ALSO MADE AVAILABLE TO CIVIL AND INTERNATIONAL AGENCIES.

SLIDE 24. FUTURE DMSP--AWS SUPPORT.

THE EXAMPLES I'VE JUST DISCUSSED HIGHLIGHT THE EXTENSIVE USE OF DMSP BY AIR WEATHER SERVICE. LIMITED MILITARY RESOURCES AND CONTINUED TENSIONS WORLDWIDE CALL FOR INCREASED RESPONSIVENESS OF THE DMSP SYSTEM. IN ADDITION, COMMANDERS USING MORE COMPLEX, SOPHISTICATED WEAPONS SYSTEMS WHICH ARE HIGHLY SENSITIVE TO ENVIRONMENTAL FACTORS DICTATE THE FURTHER EXPLOITATION AND EXPANSION OF THE DMSP. TO MEET THESE GROWING OPERATIONAL SUPPORT REQUIREMENTS DURING THE 1980'S, WE HAVE PROGRAMMED ADDITIONAL CAPABILITIES FOR THE DMSP.

SLIDE 25. DMSP IMPROVEMENTS.

THE SPACE ENVIRONMENT MISSION WILL BE STRENGTHENED WITH THE ADDITION OF BOTH A TOPSIDE IONOSONDE AND A REFINED PLASMA DENSITY MONITOR FOR DETAILED PROFILES OF ELECTRON DENSITY. THE MICROWAVE IMAGERY WILL ALLOW US TO RECOVER AERIAL EXTENT AND RATES OF

PRECIPITATION OVER THE GLOBE. WE ENVISION THESE DATA WILL GIVE US AN IMPROVED CLOUD ANALYSIS CAPABILITY AND OVER DATA-DENIED AREAS WILL, WHEN COMBINED WITH KNOWLEDGE OF THE TERRAIN, PROVIDE IMPROVED TRAFFICABILITY FORECASTS FOR ARMY COMMANDERS. THIS WILL ALLOW COMMANDERS TO MORE EFFECTIVELY EMPLOY THEIR HEAVY TANKS, TRUCKS, AND ARTILLERY PIECES IN THEIR OVERALL STRATEGY. FINALLY, INCREASED SYSTEM SURVIVABILITY AND RELIABILITY WILL INCREASE THE DMSP UTILITY AT THE AIR FORCE GLOBAL WEATHER CENTRAL. WE PLAN TO IMPROVE THE AUTOMATED IMAGERY-PROCESSING SYSTEM BY INSTALLING INTERACTIVE AND SOFTCOPY DISPLAY CONSOLES TO INCREASE DATA BASE ACCESSIBILITY AND REDUCE CRITICAL PROCESSING TIMELINESS. ALSO, THE CLOUD ANALYSIS MODEL IS BEING IMPROVED SO INCOMING DATA WILL UPDATE THE ANALYSIS CONTINUOUSLY. THEREFORE, CLOUD FORECASTS CAN BE RUN AT ANY TIME USING THE LATEST DATA AVAILABLE.

SLIDE 26. MARK IV TACTICAL DEPLOYMENT.

AF IS CURRENTLY DEPLOYING AN IMPROVED DIRECT READOUT TERMINAL FOR TACTICAL USE. THE MARK IV IS A TOTALLY SELF-SUFFICIENT TACTICAL TERMINAL, TRANSPORTABLE ON C-130 TYPE AIRCRAFT SHOWN ON THE SLIDE AS OPPOSED TO THE LARGER C-5 SIZED AIRCRAFT NEEDED TO AIRLIFT OUR CURRENT TACTICAL TERMINALS.

SLIDE 27. TACTICAL VAN IMPROVEMENTS.

IN THE FUTURE, MULTIPLE SENSOR DATA, SUCH AS MICROWAVE IMAGERY AND ATMOSPHERIC SOUNDER DATA, ARE PLANNED TO BE INCLUDED IN THE DIRECT READOUT MODE. THESE DATA WILL INCREASE THE CAPABILITY OF THE BATTLEFIELD METEOROLOGIST TO PROVIDE THE TACTICAL COMMANDER CRITICAL SUPPORT WHEN CONVENTIONAL WEATHER DATA ARE DENIED. IN

ADDITION, WE PLAN TO INCLUDE A DATA PROCESSING CAPABILITY IN THE FUTURE TACTICAL VAN. THIS SYSTEM WILL BE ABLE TO PROVIDE INSTANTANEOUS UPDATES ON THE WEATHER TO THE TACTICAL COMMANDERS' AUTOMATED SYSTEMS. COMMANDERS WILL THEN BE ABLE TO MAKE IMMEDIATE CHANGES TO TARGETS OR TACTICS MAXIMIZING THE POTENTIAL OF THEIR AUTOMATED COMMAND AND CONTROL SYSTEMS.

SLIDE 28. SUMMARY.

THE DMSP, A SYSTEM RESPONSIVE TO MILITARY REQUIREMENTS, HAS GROWN CONSIDERABLY DURING THE PAST DECADE. THE CLOSE INTERACTION AMONG THE WEATHERMAN AT THE TACTICAL READOUT TERMINAL DIRECTLY SUPPORTING THE TACTICAL COMMANDER, THE AIR FORCE GLOBAL WEATHER CENTRAL BUILDING AND APPLYING ITS WORLDWIDE DATA BASE, AND DEDICATED COMMAND AND CONTROL OF THE ON-ORBIT DMSP SATELLITES HAS PROVIDED A FINELY TUNED MILITARY SYSTEM CAPABLE OF RESPONDING TO NATIONAL SECURITY REQUIREMENTS. IN SHORT, MILITARY METSAT APPLICATIONS HAVE PROVEN TO BE A VITAL SOURCE OF DATA FOR AWS'S SUPPORT TO NATIONAL DEFENSE AND WILL CONTINUE TO EVOLVE TO MEET THE CHANGING NEEDS OF MILITARY DECISIONMAKERS.

4-15

AWS SHIELD

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## **MILITARY APPLICATIONS OF METSAT DATA**

**- DOD METSAT - DMSP**

**- AFGWC**

**- FIELD UNITS**

**- DOD PAYOFFS**

**- FUTURE ENHANCEMENTS**

## **AWS MISSION**

**PRIMARY MISSION: SUPPORT AIR FORCE AND ARMY COMBAT OPERATIONS**

**- SUCCESSFUL COMBAT OPERATIONS DEPEND ON TARGET:**

**-- DETECTION**

**-- IDENTIFICATION**

**-- TRACKING**

**-- DESTRUCTION**

**- NEW WEAPONS SYSTEMS EXTREMELY WEATHER SENSITIVE**

## **DATA SOURCES**

**USE ALL AVAILABLE DATA TO SATISFY MISSION REQUIREMENTS**

**- PEACETIME - MANY SOURCES**

**- WARTIME - DMSP**

## **DMSP MISSION**

**PROVIDE - AT ALL LEVELS OF CONFLICT - GLOBAL ENVIRONMENTAL DATA  
TO SUPPORT WORLDWIDE DOD OPERATIONS.**

- REQUIRES AT LEAST 2 OPERATIONAL SATELLITES**
- SENSOR COMPLEMENT/ORBIT TAILORED TO DOD NEEDS**



## **DMSP HISTORY**

### **EVOLVING SYSTEM**

- RESPONSIVE TO MILITARY REQUIREMENTS**
- EARLY VEHICLES CLOUD IMAGERY ONLY**

**DATA TO DESIGNER IN MINIMUM TIME**

## DMSP HISTORY

### CONFIGURATION - RECORDED AND DIRECT READOUT RECORDED DATA EVOLUTION

- DATA FLOW
- SENSOR COMPLEMENT RESPONSIVE TO DOD NEEDS
  - TROPOSPHERIC MISSION
  - IONOSPHERIC MISSION
  - IMPROVED CLOUD SENSOR

### DIRECT READOUT EVOLUTION

- INITIALLY AIR FORCE/ARMY USE
- NAVY ON BOARD IN 1971

**UNIQUE DMSP CAPABILITIES**

**DOD COMMAND & CONTROL**

**ENCRYPTION**

**ORBIT OPTIMIZATION**

**FLEXIBILITY**

**MINIMIZE READOUT TIMES**

**CONSTANT CROSS SCAN RESOLUTION**

**LOW LIGHT NIGHT TIME CAPABILITY**

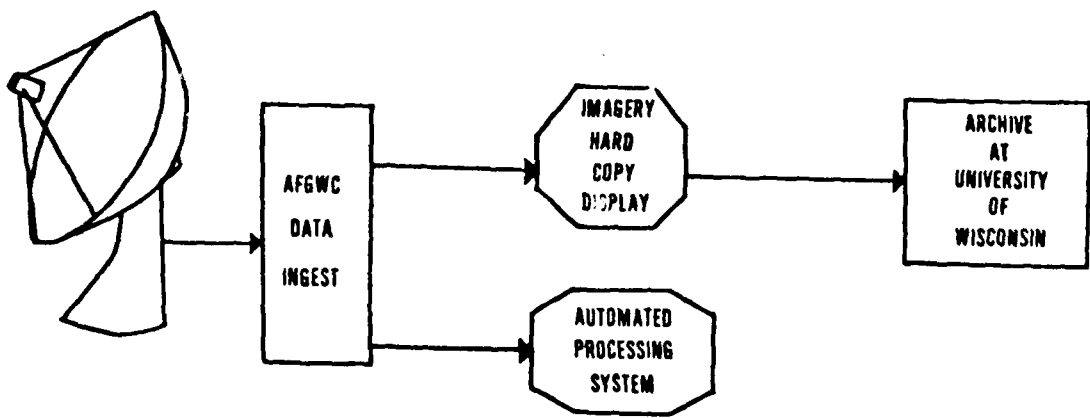
**IONOSPHERIC SENSORS**

**AIR FORCE DMSP USAGE****DATA TYPE****RECORDED****DIRECT****LOCATION****AFGWC****BATTLEFIELD****MISSION****WORLDWIDE FORECAST SUPPORT****COMBAT OPERATIONS**

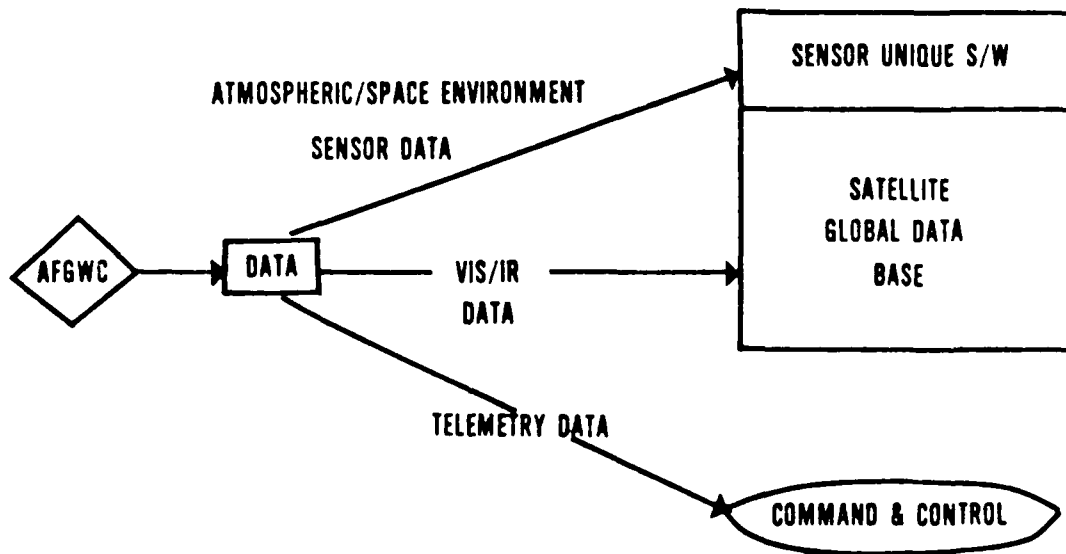
**COMMAND & CONTROL**

**RESPONSIVE - GROUND SYSTEM COLLOCATED WITH AFGWC  
CHANGE ON BOARD COMMAND WITHIN 6 HOURS**

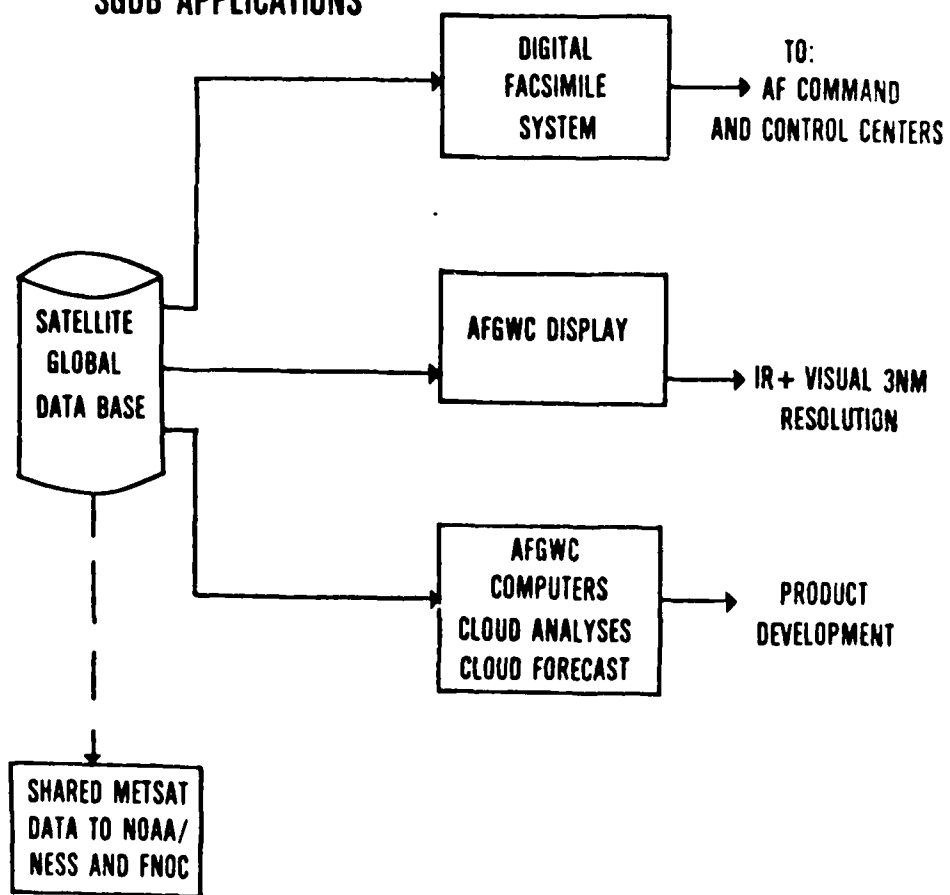
### DMSP DATA FLOW (RECORDED DATA)



# AUTOMATED PROCESSING SYSTEM



### SGDB APPLICATIONS





## **CLOUD ANALYSIS MODEL**

### **AUTOMATED CLOUD ANALYSIS INTEGRATES**

- **SATELLITE**
  - **VISUAL**
  - **IR**
  - **TEMPERATURE SOUNDINGS**
- **CONVENTIONAL**
  - **SURFACE**
  - **UPPER AIR**
  - **PILOT REPORTS**

### **ANALYSIS CHARACTERISTICS**

- **25 NM**
- **UPDATED EVERY 3 HOURS**
- **TOTALLY AUTOMATED**

## **CLOUD FORECAST MODEL**

- PROCESSED EVERY THREE HOURS**
- FORECASTS TO 48 HOURS**
  - CLOUD COVER**
  - PRECIPITATION**

## **SUMMARY OF RECORDED DATA MODE CAPABILITIES**

### **-- AFGWC PROCESSING AND APPLICATION**

**- COMPLEX HARDWARE/SOFTWARE MIX**

**- 95% DATA USAGE RELIABILITY**

## DMSP DIRECT READOUT

- DOD REQUIREMENT SATISFACTION
  - WORLDWIDE
  - RESPONSIVE
  - SECURE
  - HIGH RESOLUTION
  
- COMPLETE SYSTEM
  - SATELLITE TO CUSTOMER
    - VISUAL AND IR SENSORS
    - TACTICAL TERMINALS

## TACTICAL USES

- COMBAT TARGET ACQUISITION
  - VIETNAM
- CRISIS DATA DENIAL
  - YOM KIPPUR WAR
- NATO COMMITMENTS
  - EUROPE
- COMBAT DEPLOYMENT
  - READINESS COMMAND
  - AIRCRAFT DEPLOYMENTS
- DOD RESOURCE PROTECTION
  - JOINT TYPHOON WARNING CENTER

## TARGET ACQUISTION

**"THIS (DMSP) WEATHER PICTURE IS PROBABLY  
THE GREATEST INNOVATION OF THE WAR."**

**GEN WILLIAM MOMYER (1967)**

**"WITHOUT THEM (DMSP PHOTOS) .... MANY MISSIONS  
WOULD NOT HAVE BEEN LAUNCHED."**

**GEN WILLIAM MOMYER (1978)**

## **COMBAT SUPPORT - VIETNAM**

### **- STRIKE MISSIONS**

**- GO/NO GO LAUNCH**

**- IN-THEATER TACTICAL TERMINALS**

### **- SON TAY RAID**

**- TIMING**

**- DATA DENIAL**

**- SECRECY**

## **CRISIS DATA DENIAL**

- YOM KIPPUR WAR**
- NATIONS STOP WEATHER EXCHANGE**
- DMSP**
  - ONLY DATA SOURCE**
  - AIDED CRITICAL RESUPPLY**
- PROSPECTS IN EUROPE**
- NICARAGUAN CONTINGENCY**



## COMBAT DEPLOYMENT

- REDCOM
  - WORLDWIDE MISSION
  - LIMITED WEATHER DATA
    - DATA SPARSE REGIONS
    - DATA DENIAL
- TAC DEPLOYMENTS
  - NATO COMMITMENTS
  - LAUNCH/REFUELING DECISIONS

## **DOD RESOURCE PROTECTION**

### **- JOINT TYPHOON WARNING CENTER (JTWC)**

**- STORM WARNING**

**- RESOURCE PROTECTION**

**- SATELLITE STORM POSITIONING**

**WESTPAC - 50%**

**INDIAN OCEAN - 95%**

**- MILITARY REQUIREMENT/CIVIL AVAILABILITY**

**FUTURE DMSP - AWS SUPPORT**

**LIMITED DOD RESOURCES - CONTINUED WORLD TENSION - NEW WEAPONS DRIVE**

**- INCREASED DMSP RESPONSIVENESS**

**- FURTHER EXPLOITATION/EXPANSION OF DMSP**

## **DMSP IMPROVEMENTS**

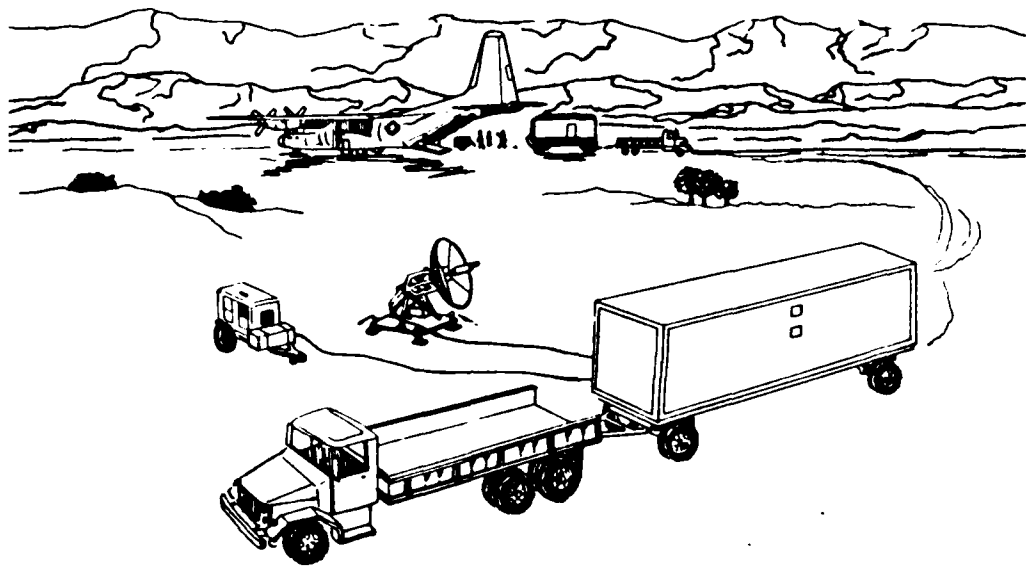
**SPACE ENVIRONMENT MISSION**

**MICROWAVE IMAGER**

**AUTOMATED IMAGERY PROCESSING IMPROVEMENT**

**IMPROVED CLOUD ANALYSIS/FORECAST**

# MARK IV TACTICAL DEPLOYMENT



**TACTICAL VAN IMPROVEMENTS**

**MULTIPLE SENSOR DATA**

**- MICROWAVE IMAGER**

**- ATMOSPHERIC SOUNDERS**

**DATA PROCESSING CAPABILITY**

## SUMMARY

- DMSP
- FINE TUNED TOTAL SYSTEM
- RESPONSIVE TO MILITARY REQUIREMENTS

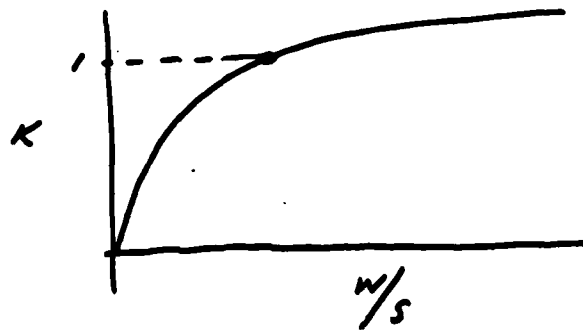


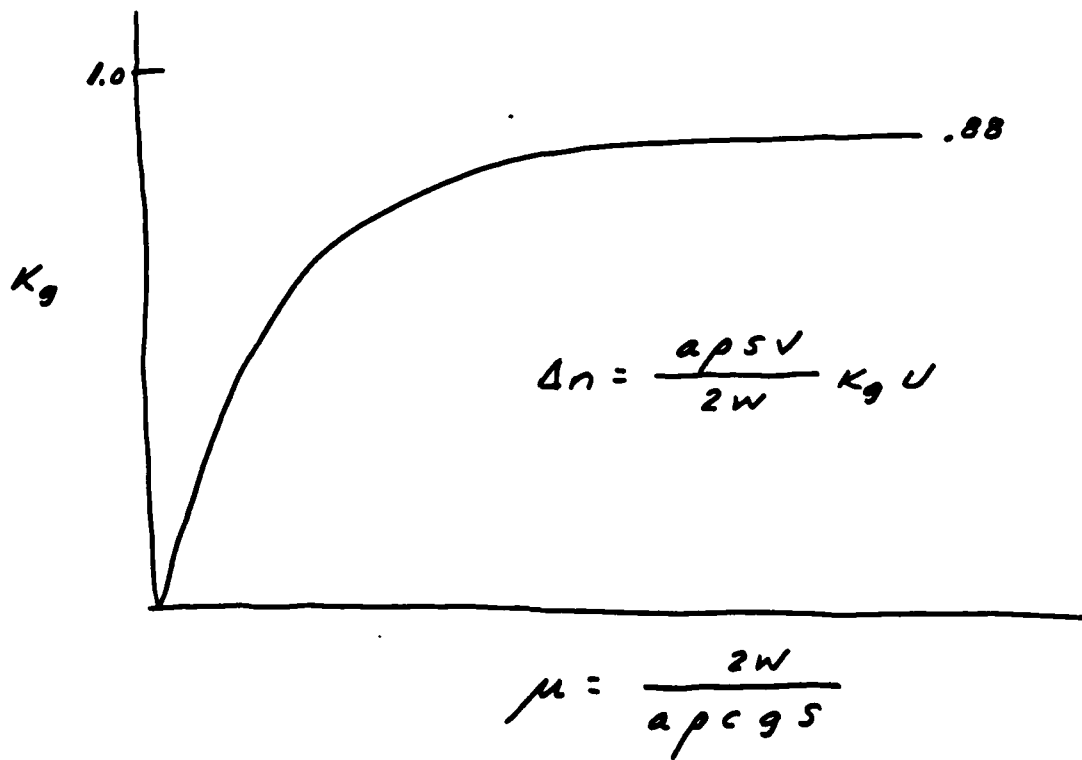


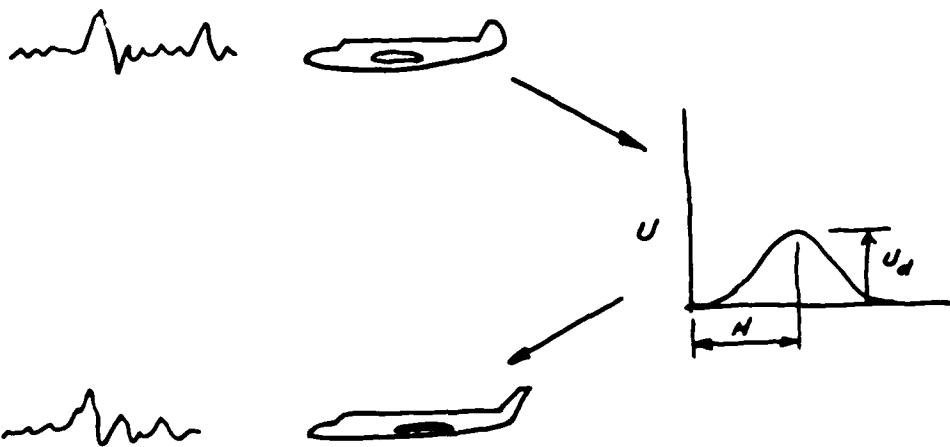
$$L = \Delta n W = \frac{\rho}{2} S V^2 \frac{U}{V}$$

$$\Delta n = \frac{\rho S V}{2 W} U$$

$$\Delta n = \frac{\rho S V}{2 W} K U$$







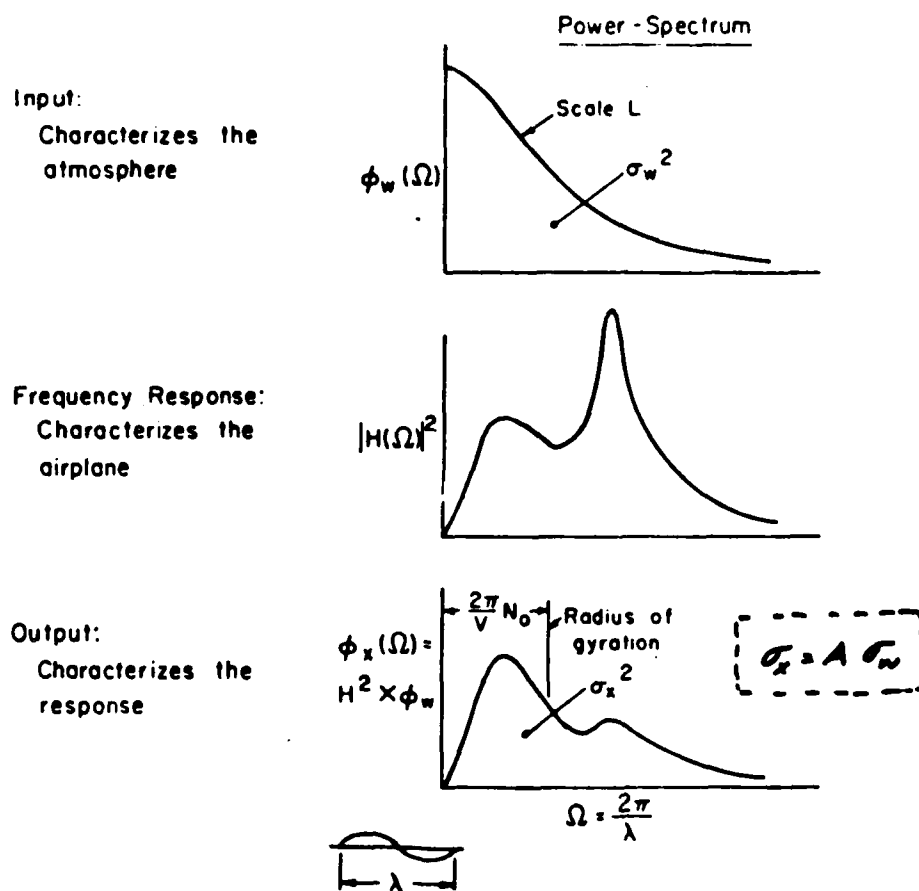


Fig. 1.- Input-Output Relation for Gust Response

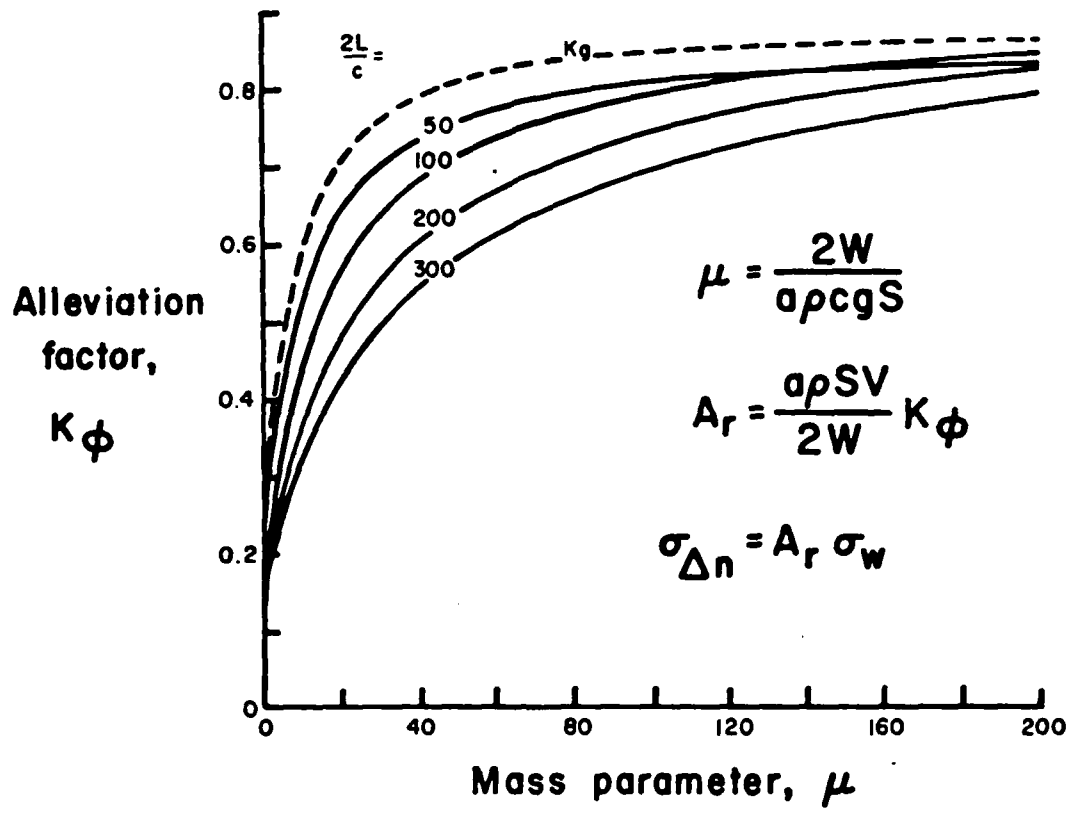
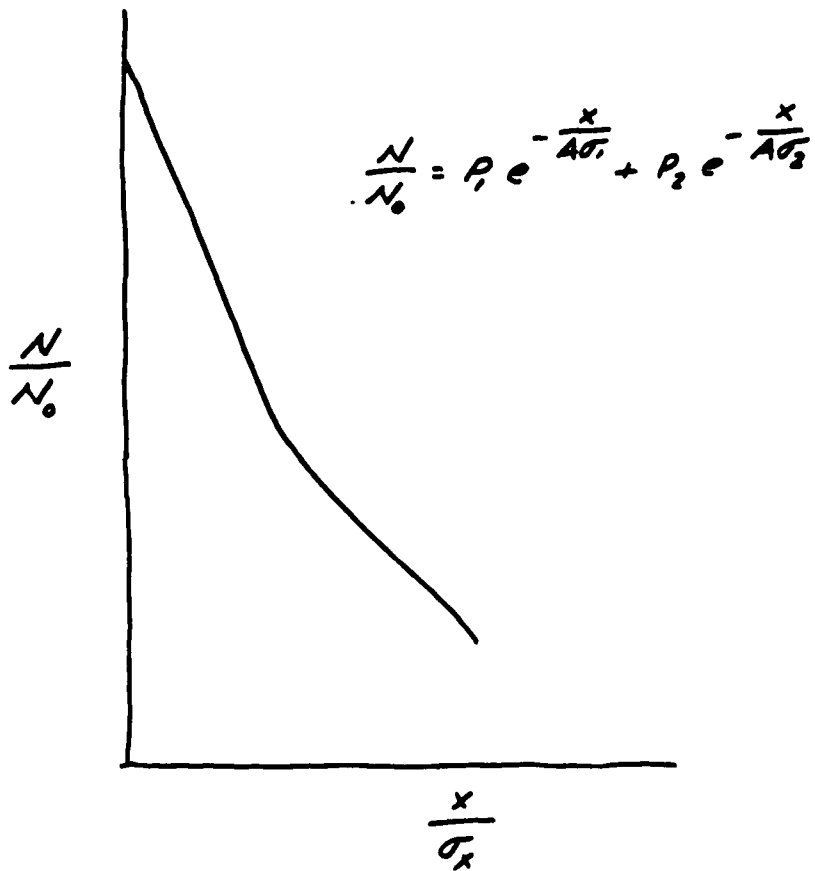


Fig. 3.- Spectral Results for Rigid Airplane



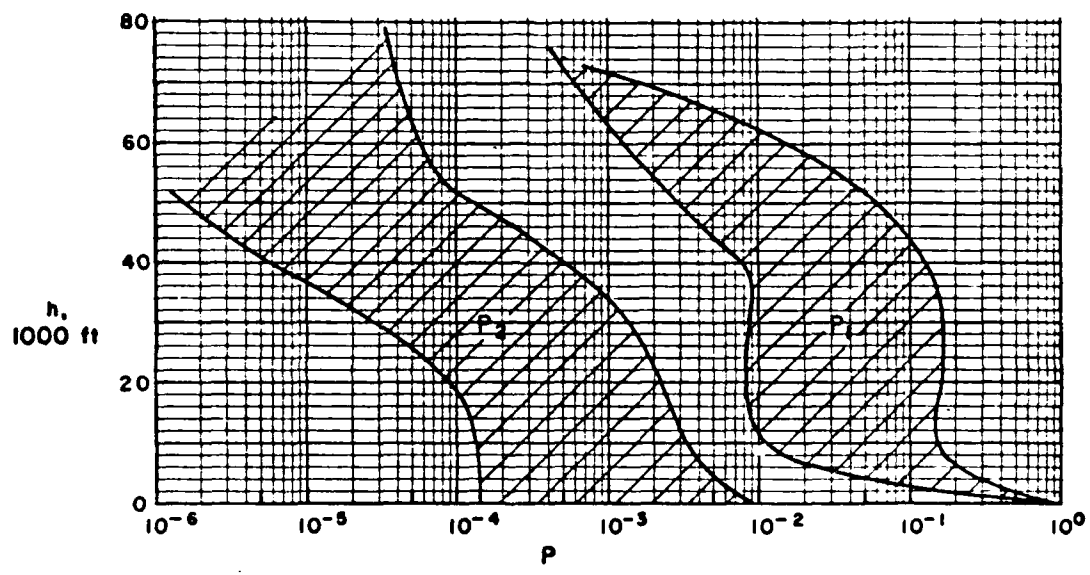


Figure 1. Range of P<sub>1</sub> and P<sub>2</sub> values indicated by various studies

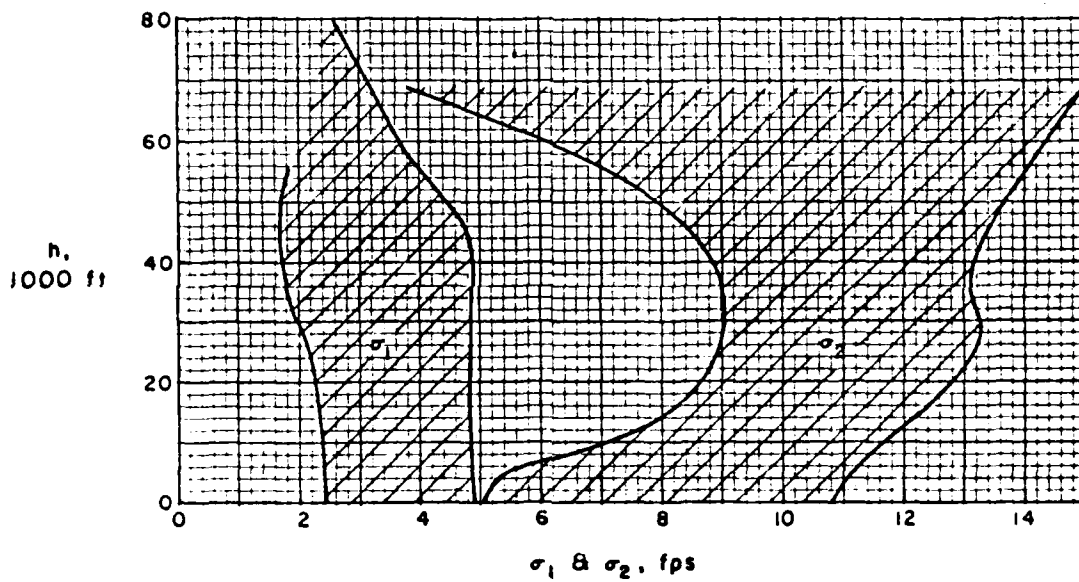


Figure 2. Range in  $\sigma_1$  and  $\sigma_2$  values indicated by various studies



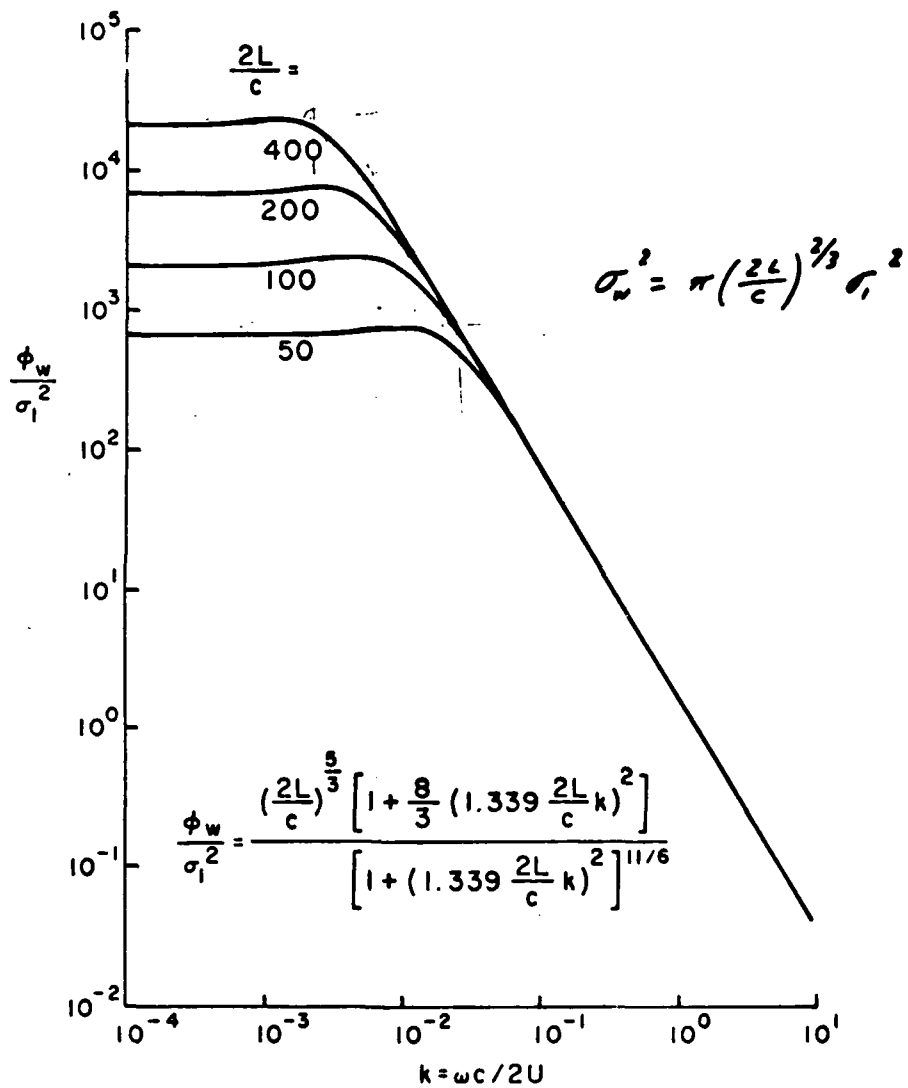


Figure 4.- Gust Input Spectrum Independent of  $\frac{2L}{c}$  at High Frequencies

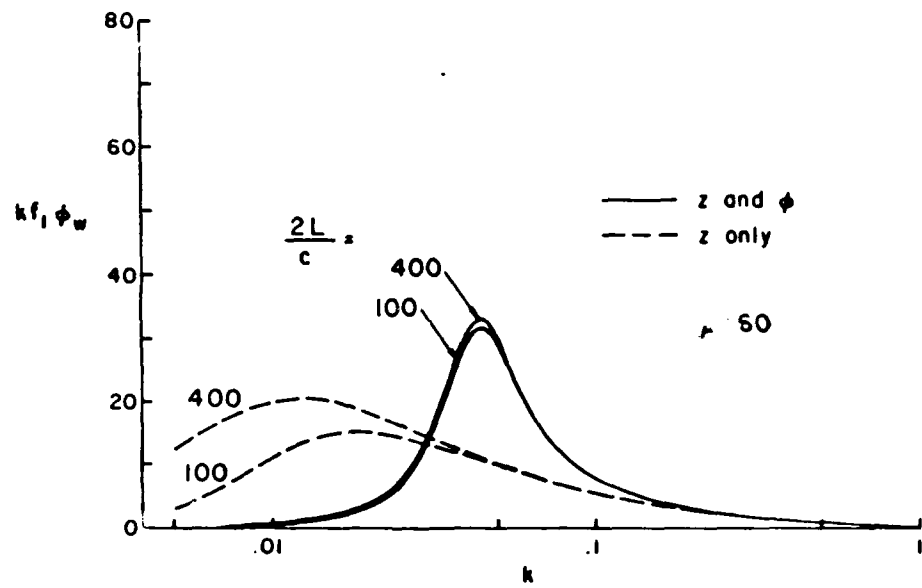
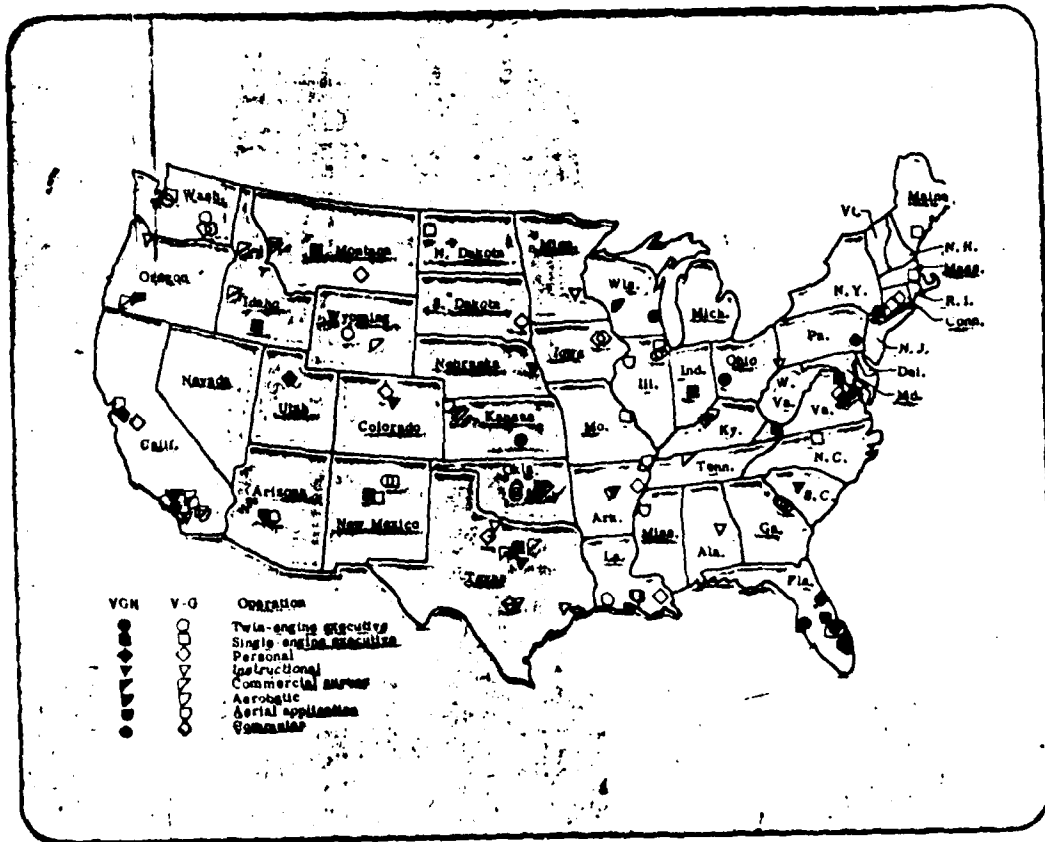


Figure 7.- Distribution of Response Power for One and Two Degrees of Freedom

VG/VGH GENERAL AVIATION PROGRAM STATUS

| OPERATIONS              | COLLECTED |        |           |         | REPORTED  |        |           |        |
|-------------------------|-----------|--------|-----------|---------|-----------|--------|-----------|--------|
|                         | VGH DATA  |        | VG DATA   |         | VGH DATA  |        | VG DATA   |        |
|                         | AIRPLANES | HOURS  | AIRPLANES | HOURS   | AIRPLANES | HOURS  | AIRPLANES | HOURS  |
| TWIN-ENGINE EXECUTIVE   | 11        | 4,975  | 20        | 20,795  | 9         | 3,909  | 18        | 13,622 |
| SINGLE-ENGINE EXECUTIVE | 9         | 2,020  | 16        | 12,125  | 8         | 1,182  | 15        | 7,808  |
| PERSONAL                | 10        | 1,558  | 23        | 11,504  | 6         | 712    | 16        | 5,283  |
| INSTRUCTIONAL           | 8         | 4,031  | 22        | 18,413  | 6         | 2,759  | 17        | 9,499  |
| COMMERCIAL SURVEY       | 8         | 3,154  | 15        | 38,979  | 4         | 2,997  | 14        | 23,585 |
| AEROBATIC               | 1         | 12     | 5         | 721     | 1         | 12     | 5         | 406    |
| AERIAL APPLICATION      | 4         | 1,040  | 9         | 4,638   | 2         | 487    | 7         | 1,837  |
| COMMUTER                | 2         | 4,263  | 7         | 16,078  | 2         | 940    | 5         | 4,358  |
| TOTAL                   | 53        | 21,053 | 117       | 123,253 | 38        | 12,998 | 97        | 66,198 |



### ALTITUDE OPERATING PRACTICES

PRESSURE  
ALTITUDE

45  $\times 10^3$

40

25

20

15

10

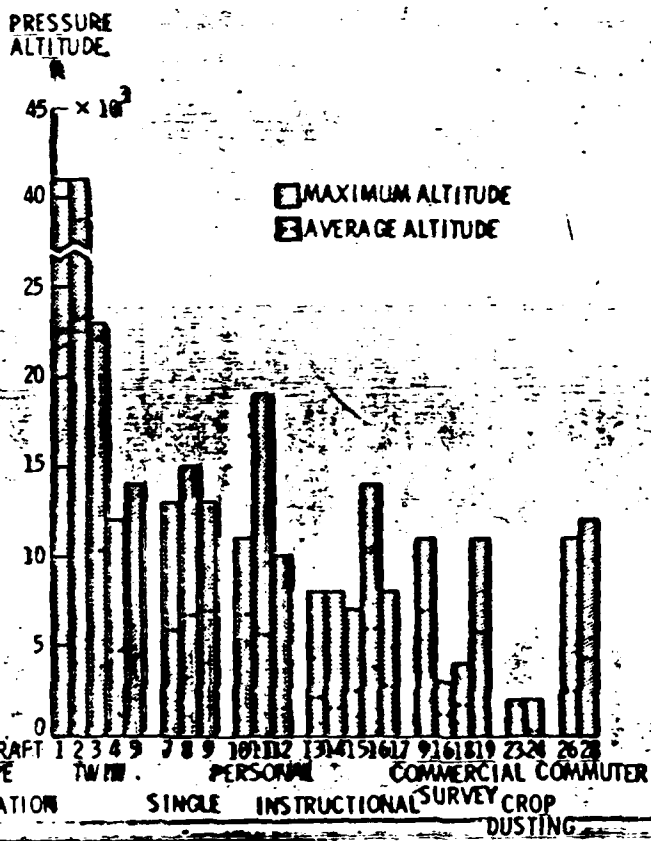
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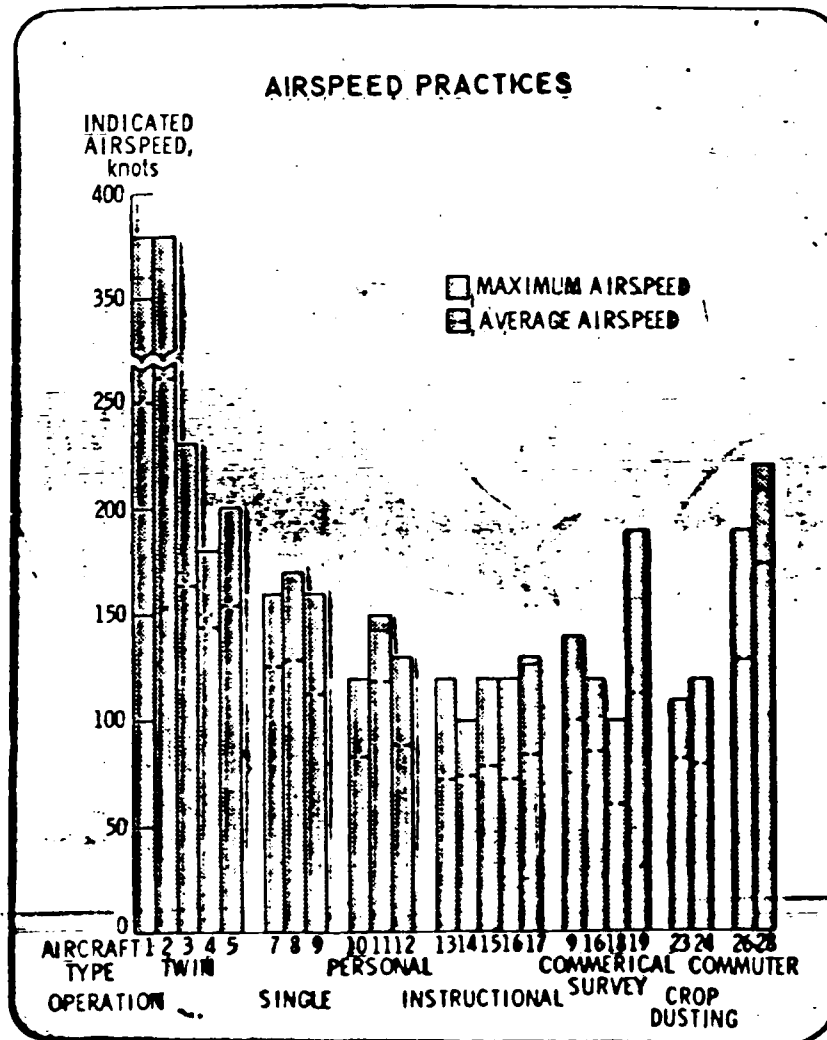
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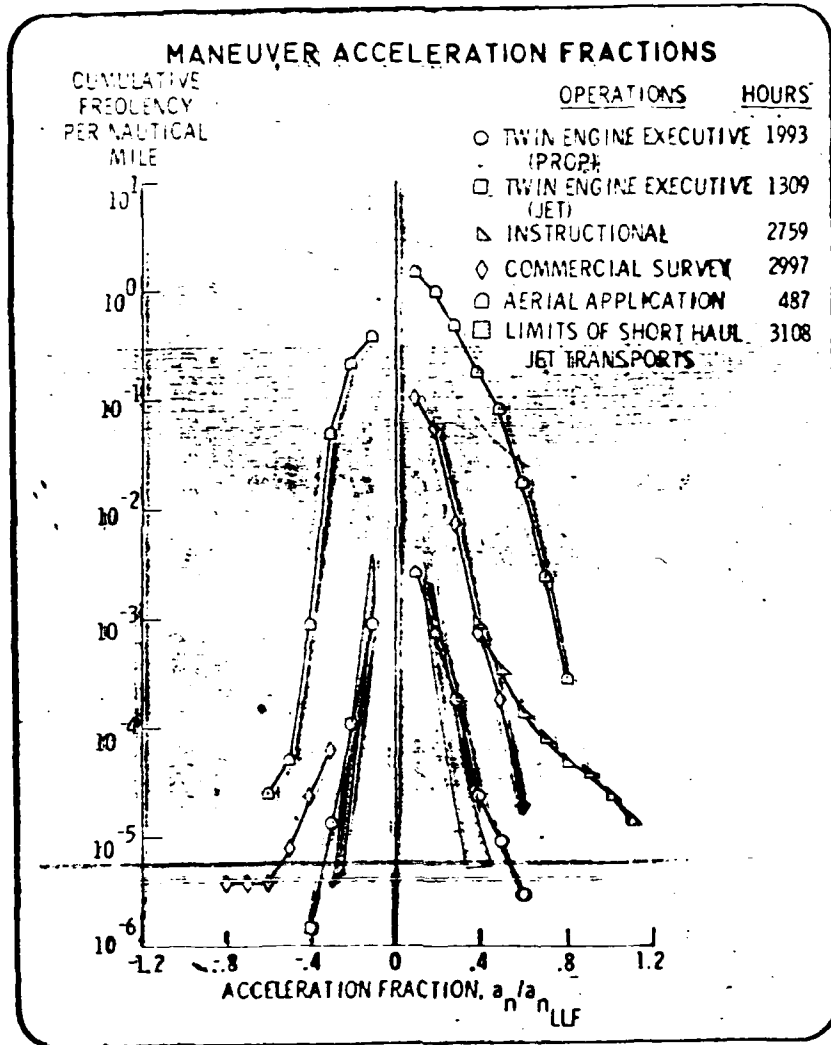
□ MAXIMUM ALTITUDE  
▨ AVERAGE ALTITUDE

|               |             |   |   |   |           |   |   |   |               |    |    |    |               |    |    |    |        |    |    |    |            |    |    |    |          |  |  |  |              |  |  |  |
|---------------|-------------|---|---|---|-----------|---|---|---|---------------|----|----|----|---------------|----|----|----|--------|----|----|----|------------|----|----|----|----------|--|--|--|--------------|--|--|--|
| AIRCRAFT TYPE | 1           | 2 | 3 | 4 | 5         | 7 | 8 | 9 | 10            | 11 | 12 | 13 | 14            | 15 | 16 | 17 | 19     | 16 | 18 | 19 | 23         | 24 | 26 | 27 |          |  |  |  |              |  |  |  |
| OPERATION     | TWIN ENGINE |   |   |   | PERSONNEL |   |   |   | SINGLE ENGINE |    |    |    | INSTRUCTIONAL |    |    |    | SURVEY |    |    |    | COMMERCIAL |    |    |    | COMMUTER |  |  |  | CROP DUSTING |  |  |  |

### ALTITUDE OPERATING PRACTICES



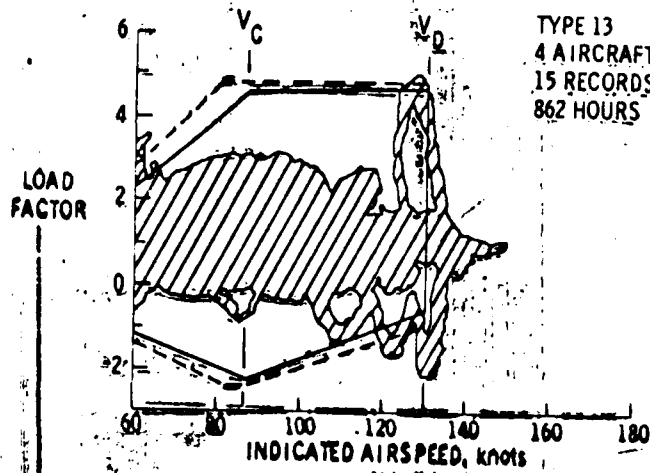


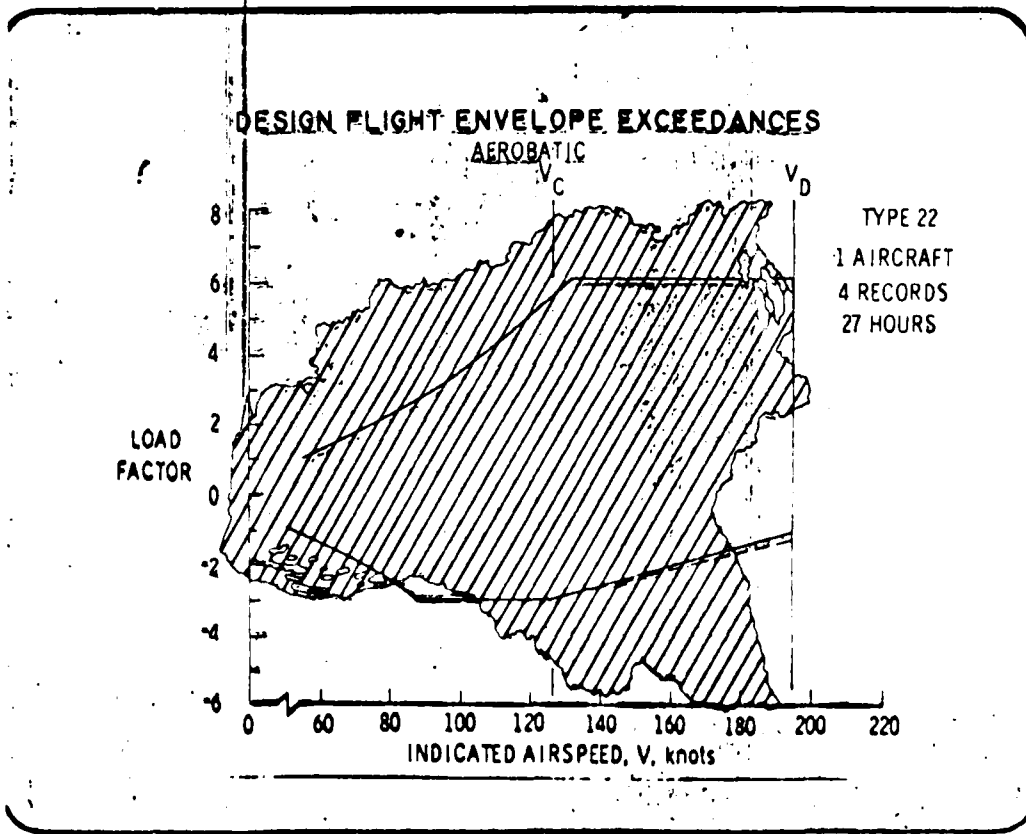




### DESIGN FLIGHT ENVELOPE EXCEEDANCES

INSTRUCTIONAL





### GUST ACCELERATION FRACTIONS I

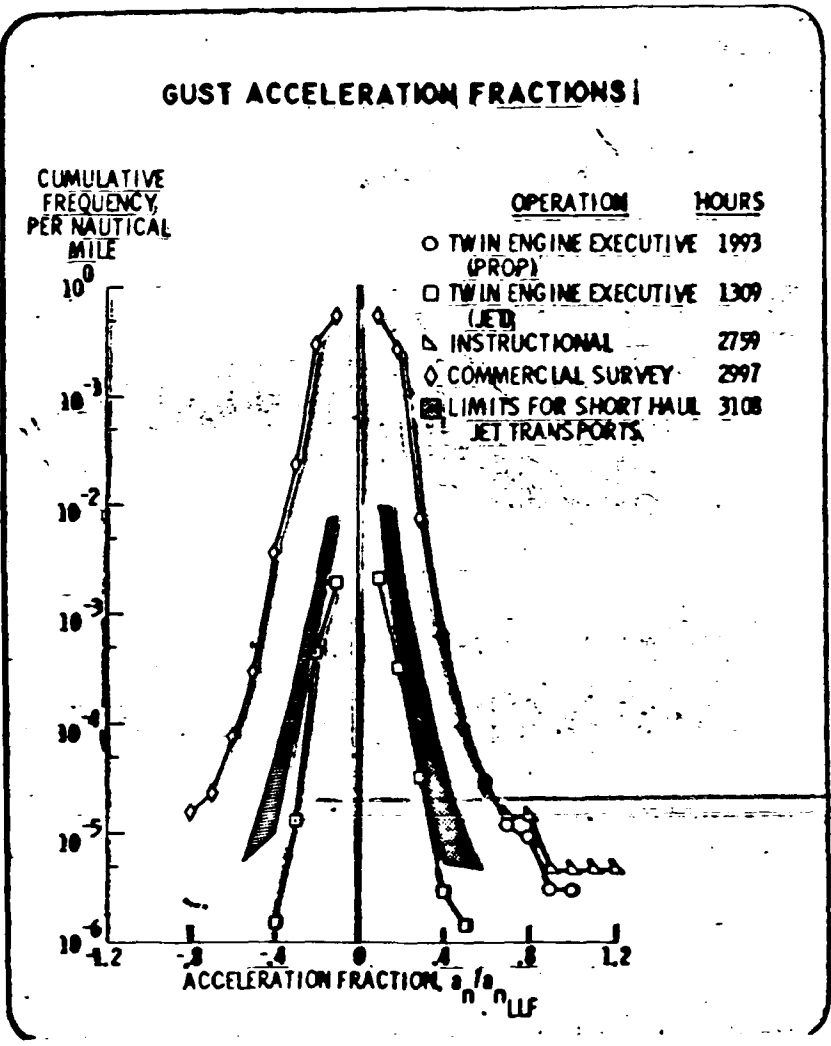
CUMULATIVE  
FREQUENCY  
PER NAUTICAL  
MILE

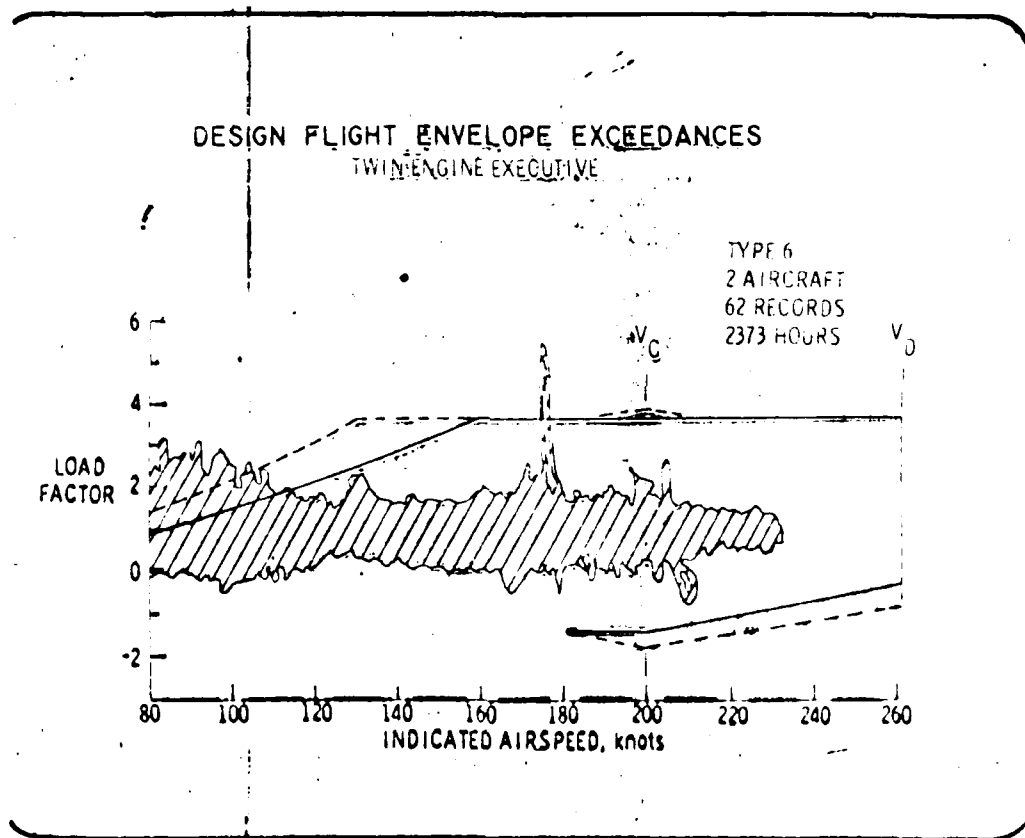
10<sup>0</sup>  
10<sup>-1</sup>  
10<sup>-2</sup>  
10<sup>-3</sup>  
10<sup>-4</sup>  
10<sup>-5</sup>  
10<sup>-6</sup>

ACCELERATION FRACTION  $a/n_{LLF}$

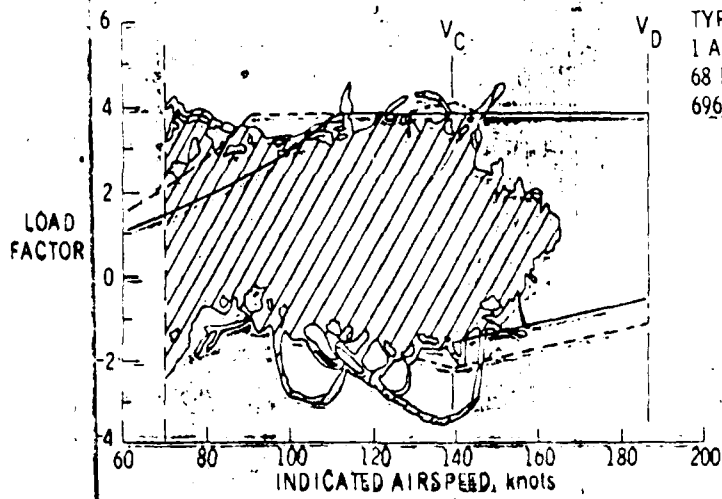
OPERATION HOURS

- TWIN ENGINE EXECUTIVE (PROP) 1993
- TWIN ENGINE EXECUTIVE (JET) 1309
- △ INSTRUCTIONAL 2759
- ◇ COMMERCIAL SURVEY 2997
- ▨ LIMITS FOR SHORT HAUL JET TRANSPORTS 3108

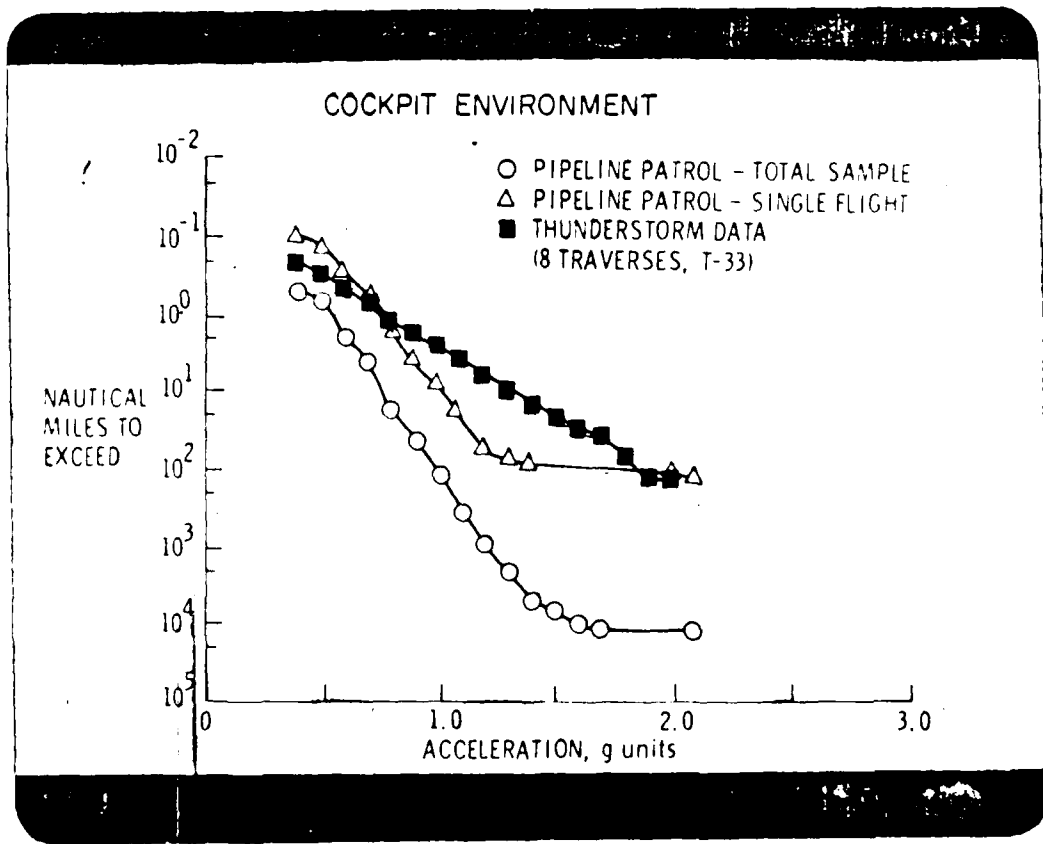




DESIGN FLIGHT ENVELOPE EXCEEDANCES  
COMMERCIAL SURVEY

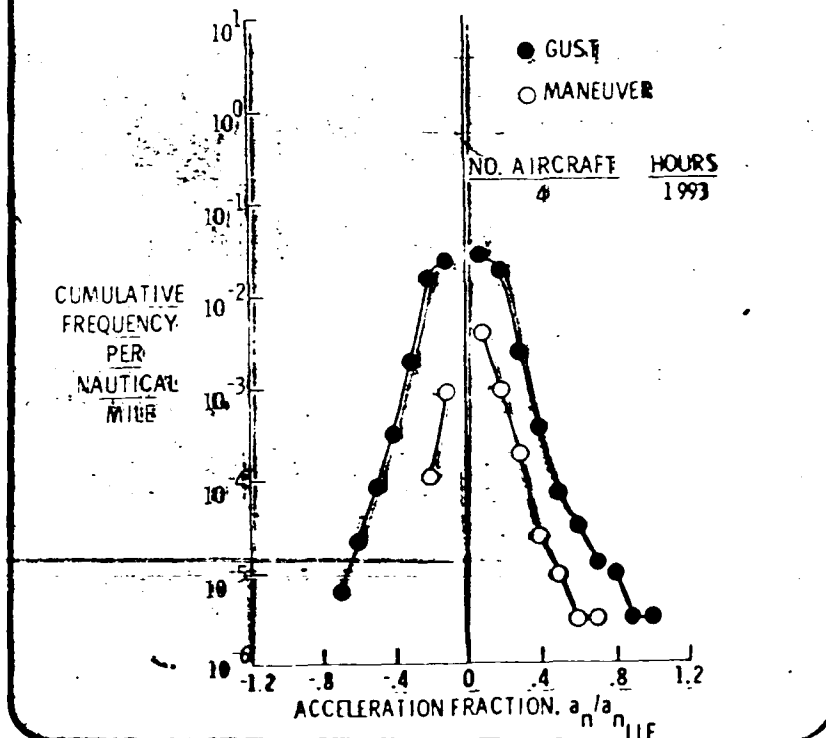


TYPE 9D  
1 AIRCRAFT  
68 RECORDS  
6966 HOURS



### COMPARISON OF GUST AND MANEUVER ACCELERATION FRACTIONS

TWIN ENGINE EXECUTIVE (PROP)

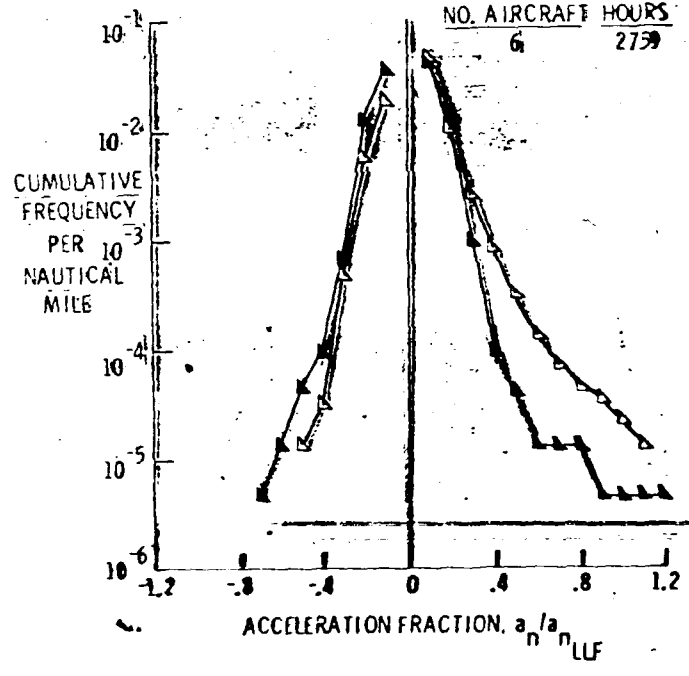


### COMPARISON OF GUST AND MANEUVER ACCELERATION FRACTIONS

INSTRUCTIONAL

- ▲ GUSTS
- △ MANEUVERS

NO. AIRCRAFT HOURS  
6      2759



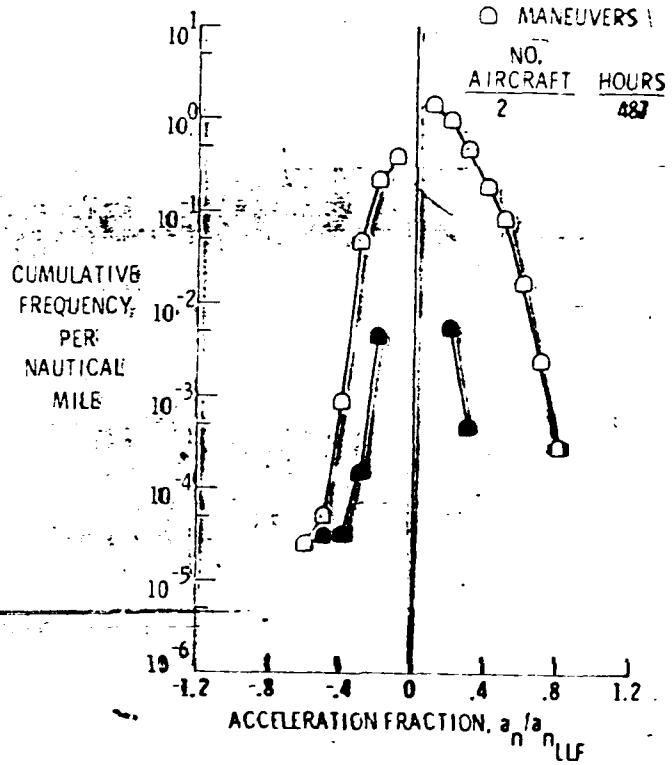


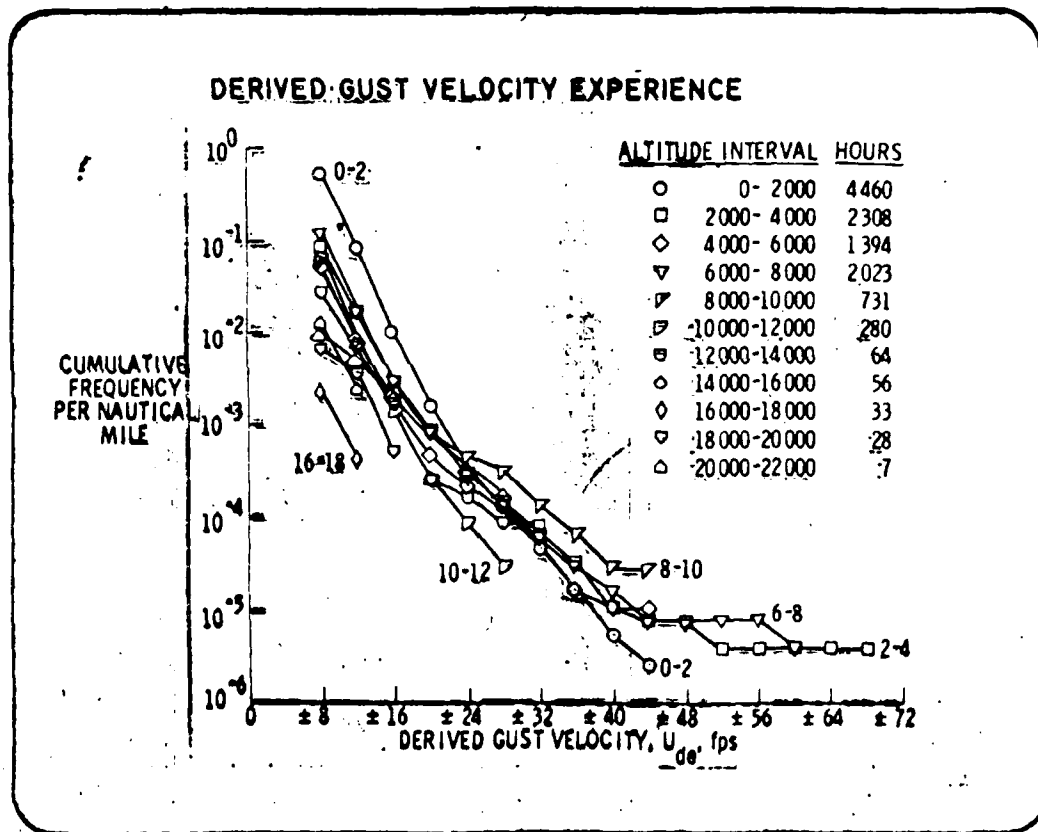
### COMPARISON OF GUST AND MANEUVER ACCELERATION FRACTIONS

AERIAL APPLICATION ● GUSTS

○ MANEUVERS

| NO. AIRCRAFT | HOURS |
|--------------|-------|
| 2            | 487   |





PREDICTIONS OF LANDINGS REQUIRED TO REACH  
OR EXCEED THE MINIMUM DESIGN LOAD FACTOR, 2.67

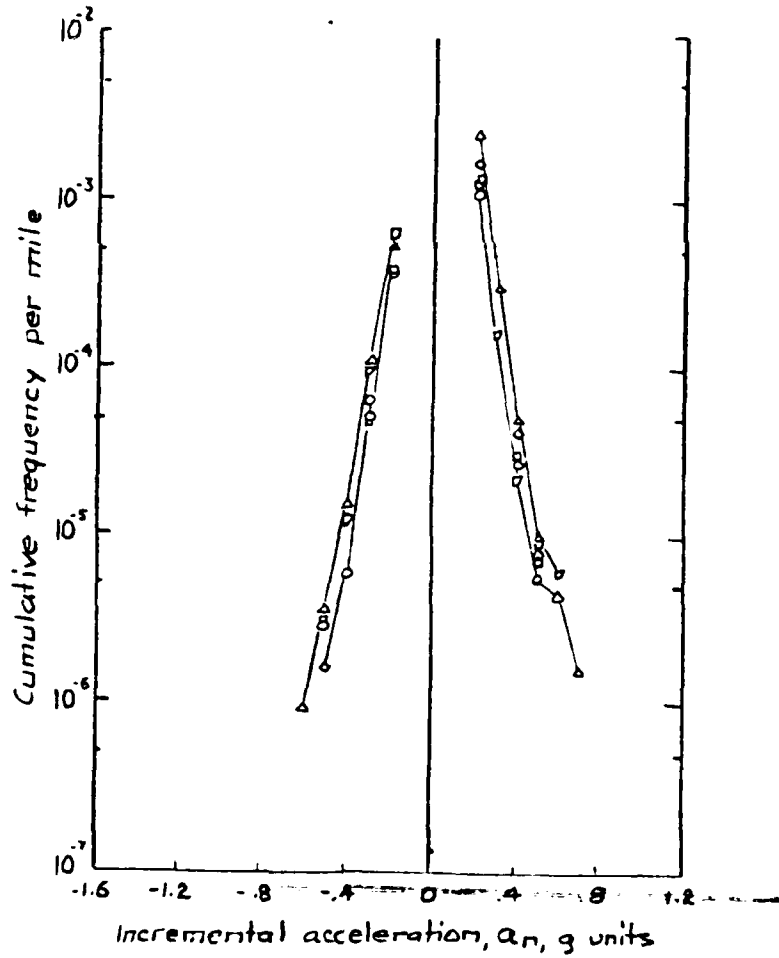
| <u>OPERATIONAL CATEGORY</u> | <u>NUMBER OF LANDINGS</u> |
|-----------------------------|---------------------------|
| AERIAL APPLICATION          | 860                       |
| INSTRUCTIONAL               | 3393                      |
| SINGLE ENGINE EXECUTIVE     | 19295                     |
| PERSONAL                    | 19554                     |
| COMMERCIAL SURVEY           | 81321                     |
| TWIN ENGINE EXECUTIVE       | 269297                    |
| COMMUTER                    | 1507121                   |

CONCLUSIONS

1. COMPETITIVE AEROBATIC AND INSTRUCTIONAL AIRPLANES REACH OR EXCEED THE DESIGN DIVING SPEED MORE FREQUENTLY THAN AIRPLANES IN OTHER TYPES OF OPERATIONS.
2. AVERAGE FLIGHT ALTITUDES FOR PISTON-POWERED AIRPLANES ARE BELOW 7,000 FT AND MAXIMUM ALTITUDES DO NOT EXCEED 15,000 FT.
3. THE MOST SEVERE OVERALL IN-FLIGHT LOADS ARE RECORDED BY AIRPLANES FLOWN IN COMPETITIVE AEROBATICS, AND IN PIPELINE PATROL OPERATIONS OVER MOUNTAINOUS REGIONS.
4. THE FREQUENCY OF OCCURRENCE OF GIVEN GUST ACCELERATIONS VARIES BY AS MUCH AS THREE ORDERS OF MAGNITUDE BETWEEN AIRPLANES FLOWN IN DIFFERENT OPERATIONS.
5. THE MOST SEVERE DERIVED GUST VELOCITIES FROM THE STANDPOINT OF MAGNITUDE AND FREQUENCY OF OCCURRENCE WERE EXPERIENCED BELOW 10,000 FT.
6. THE MOST SEVERE MANEUVER LOADS WERE EXPERIENCED BY AIRPLANES FLOWN IN AERIAL APPLICATIONS, COMPETITIVE AEROBATICS, AND INSTRUCTIONAL OPERATIONS.
7. GENERAL AVIATION AIRPLANES ARE FLOWN CLOSER TO THE DESIGN FLIGHT ENVELOPE THAN COMMERCIAL TRANSPORT AIRPLANES.

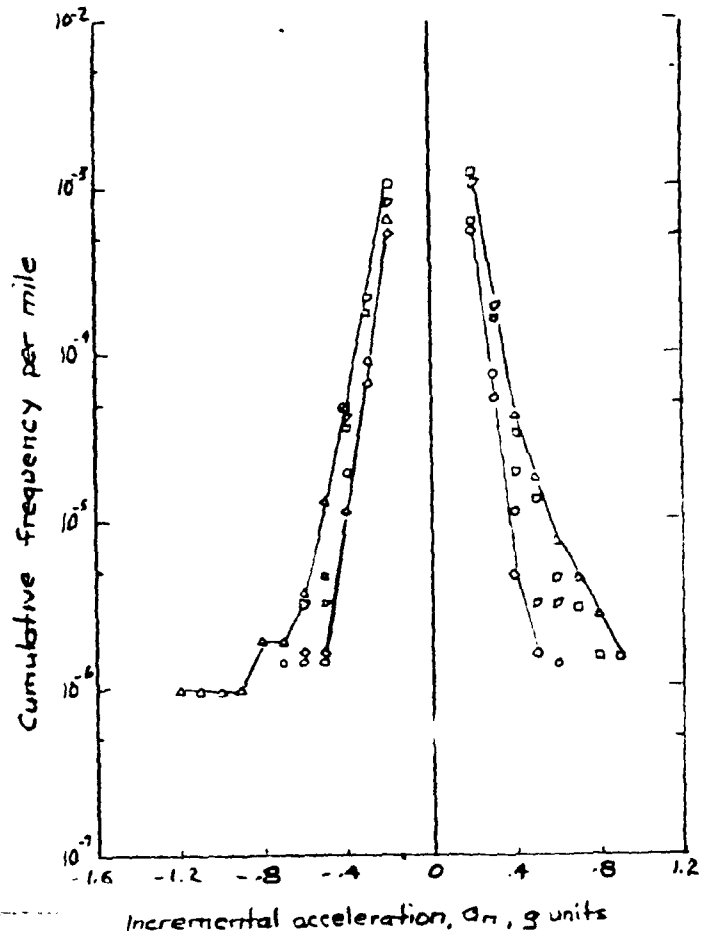
OPERATIONAL MANEUVER ACCELERATIONS EXPERIENCED  
BY WIDE-BODY JET TRANSPORTS

| Operator | No. A/C | Miles | FH. Hours |      |
|----------|---------|-------|-----------|------|
| ○        | F       | 2     | 702 326   | 1506 |
| □        | M       | 1     | 687 395   | 1455 |
| △        | N       | 1     | 1 103 142 | 2381 |
| ◇        | P       | 1     | 643 880   | 1391 |
| ▽        | R       | 1     | 323 338   | 716  |



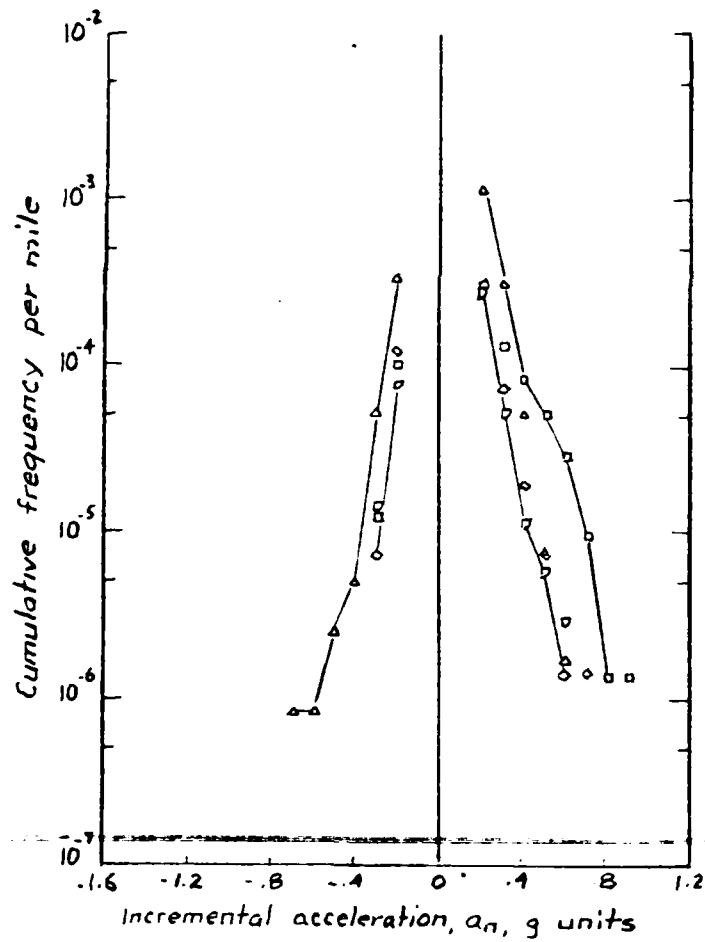
GUST ACCELERATIONS EXPERIENCED BY WIDE-BODY JET TRANSPORTS

| Operator | No AC | Miles | Flt hours |      |
|----------|-------|-------|-----------|------|
| O        | F     | 2     | 702 326   | 1506 |
| □        | M     | 1     | 687 395   | 1455 |
| △        | N     | 1     | 1 031 42  | 2381 |
| ◇        | P     | 1     | 643 880   | 1391 |
| ○        | Q     | 1     | 323 358   | 716  |



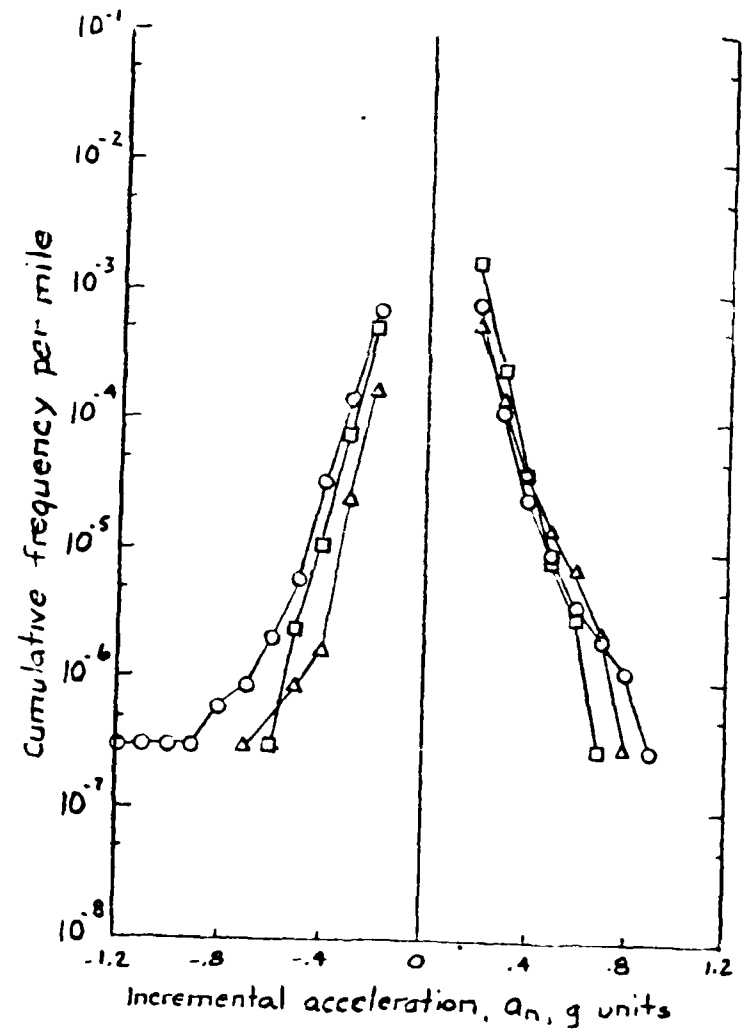
CHECK-FLIGHT MANEUVER ACCELERATIONS EXPERIENCED  
BY WIDE-BODY JET TRANSPORTS

|   | Operator | No. A/c | Miles   | Flt. Hours |
|---|----------|---------|---------|------------|
| □ | M        | 1       | 691691  | 1474       |
| △ | N        | 1       | 1115607 | 2450       |
| ◇ | P        | 1       | 646707  | 1405       |
| ▽ | Q        | 1       | 325970  | 727        |



### COMPARISON OF ACCELERATION SOURCES FOR WIDE-BODY JET TRANSPORTS

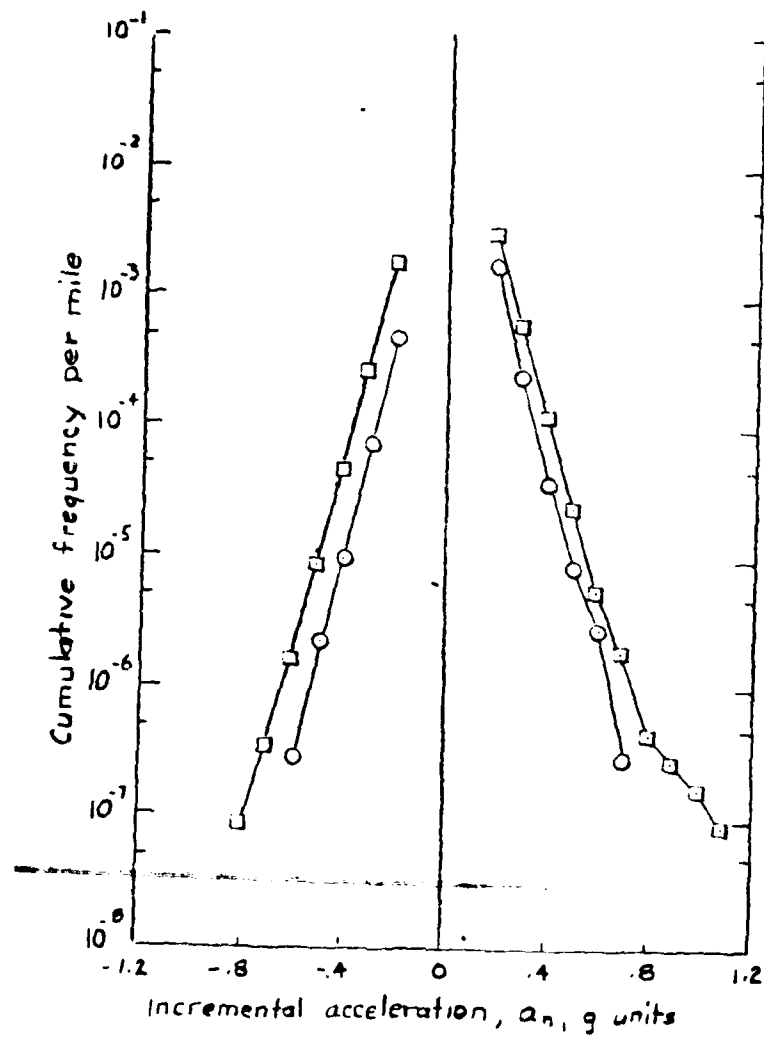
| Acceleration source     | Miles     | Hours |
|-------------------------|-----------|-------|
| ○ Gust                  | 3 460 081 | 7 450 |
| □ Operational maneuver  | 3 460 081 | 7 450 |
| △ Check-flight maneuver | 3 482 301 | 7 562 |





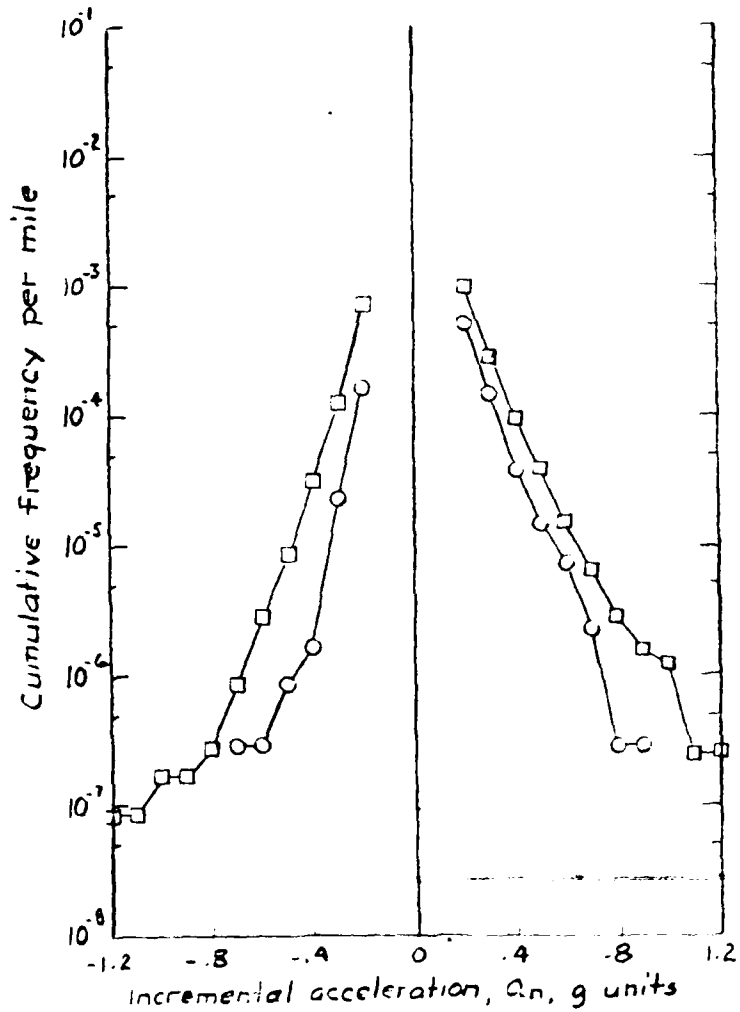
COMPARISON OF MANEUVER ACCELERATIONS FOR  
WIDE AND NARROW BODY JET TRANSPORTS

| Aircraft type | No A/C | Miles     | Flt hours |
|---------------|--------|-----------|-----------|
| ○ Wide body   | 6      | 3 460 081 | 7 450     |
| □ Narrow body | 12     | 26 854    |           |



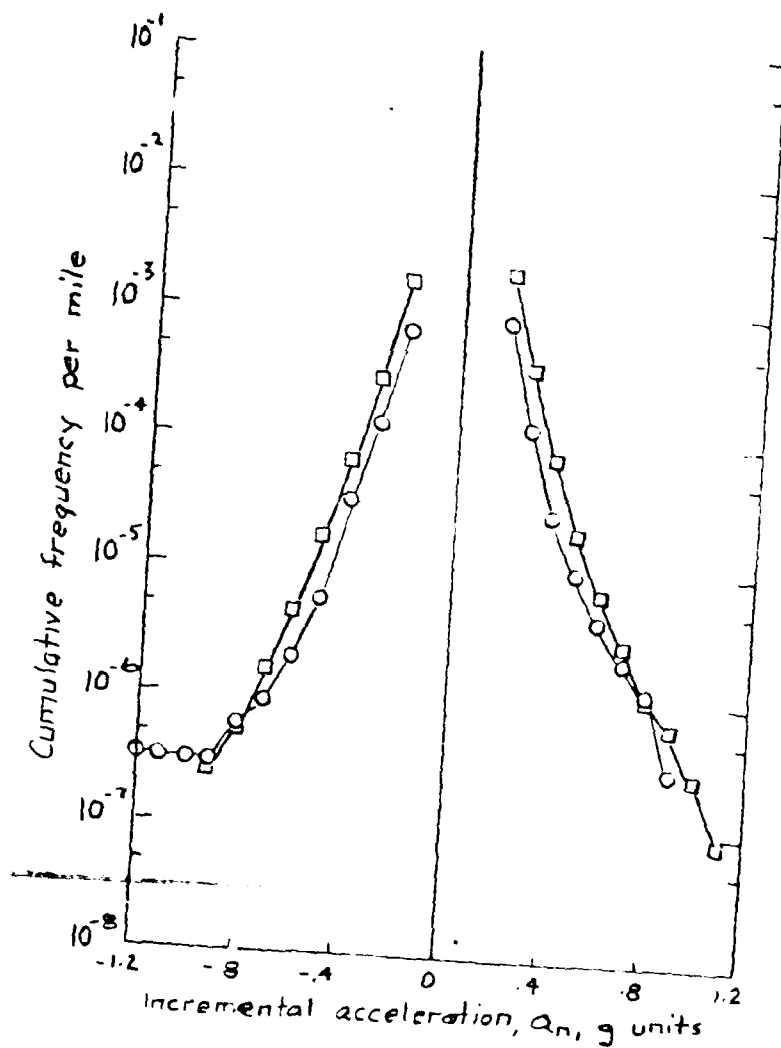
COMPARISON OF CHECK-FLIGHT MANEUVER ACCELERATIONS FOR WIDE AND NARROW-BODY JET TRANSPORTS

| Aircraft type | No A/C | Miles      | Flt hours |
|---------------|--------|------------|-----------|
| Wide body     | 6      | 3 482 301  | 7 562     |
| Narrow body   | 12     | 12 092 676 | 27 410    |



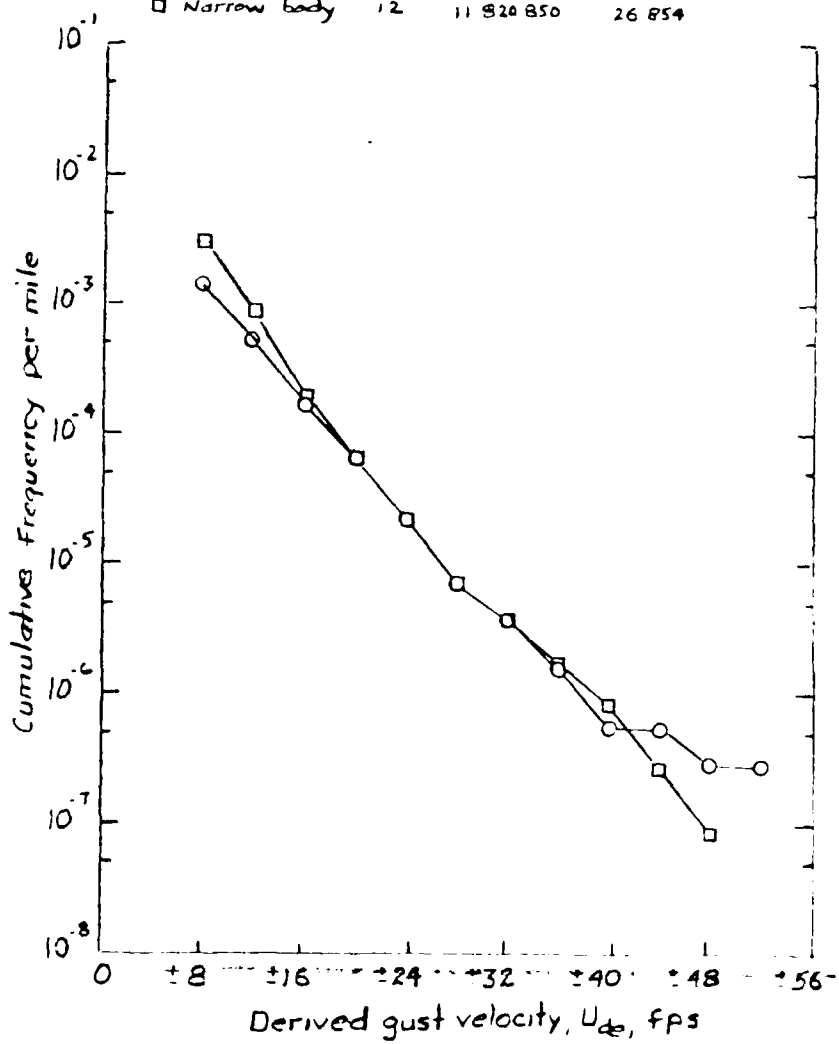
# COMPARISON OF GUST ACCELERATIONS FOR WIDE AND NARROW-BODY JET TRANSPORTS

| Aircraft type | No. A/c | Miles      | Flt. hours |
|---------------|---------|------------|------------|
| ○ Wide body   | 6       | 3 440 081  | 7 450      |
| □ Narrow body | 12      | 11 820 850 | 26 854     |



### COMPARISON OF DERIVED GUST VELOCITIES FOR WIDE AND NARROW-BODY JET TRANSPORTS

| Type A/c      | No A/c | miles      | flth hours |
|---------------|--------|------------|------------|
| ○ Wide body   | 6      | 3 460 081  | 7 450      |
| □ Narrow body | 12     | 11 820 850 | 26 854     |

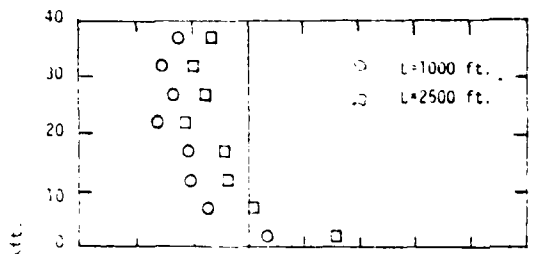


CONCLUSIONS

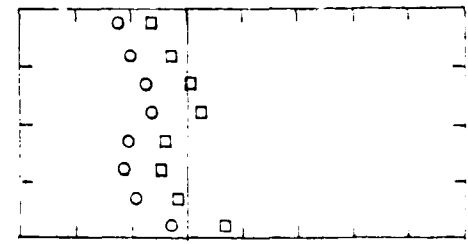
1. COMPETITIVE AEROBATIC AND INSTRUCTIONAL AIRPLANES REACH OR EXCEED THE DESIGN DIVING SPEED MORE FREQUENTLY THAN AIRPLANES IN OTHER TYPES OF OPERATIONS.
2. AVERAGE FLIGHT ALTITUDES FOR PISTON-POWERED AIRPLANES ARE BELOW 7,000 FT AND MAXIMUM ALTITUDES DO NOT EXCEED 15,000 FT.
3. THE MOST SEVERE OVERALL IN-FLIGHT LOADS ARE RECORDED BY AIRPLANES FLOWN IN COMPETITIVE AEROBATICS, AND IN PIPELINE PATROL OPERATIONS OVER MOUNTAINOUS REGIONS.
4. THE FREQUENCY OF OCCURRENCE OF GIVEN GUST ACCELERATIONS VARIES BY AS MUCH AS THREE ORDERS OF MAGNITUDE BETWEEN AIRPLANES FLOWN IN DIFFERENT OPERATIONS.
5. THE MOST SEVERE DERIVED GUST VELOCITIES FROM THE STANDPOINT OF MAGNITUDE AND FREQUENCY OF OCCURRENCE WERE EXPERIENCED BELOW 10,000 FT.
6. THE MOST SEVERE MANEUVER LOADS WERE EXPERIENCED BY AIRPLANES FLOWN IN AERIAL APPLICATIONS, COMPETITIVE AEROBATICS, AND INSTRUCTIONAL OPERATIONS.
7. GENERAL AVIATION AIRPLANES ARE FLOWN CLOSER TO THE DESIGN FLIGHT ENVELOPE THAN COMMERCIAL TRANSPORT AIRPLANES.

$$\frac{N}{N_0} = p e^{-U/\sigma_1}$$

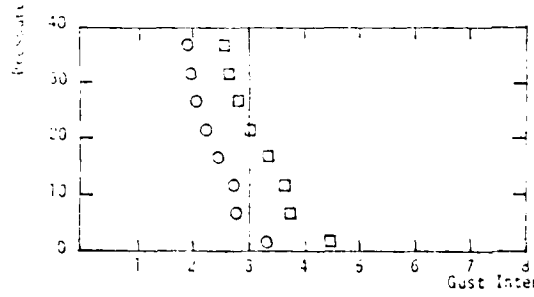
$$\sigma_{W_1} = \sigma_1 (\pi)^{1/2} \left( \frac{2L}{c} \right)^{1/3}$$



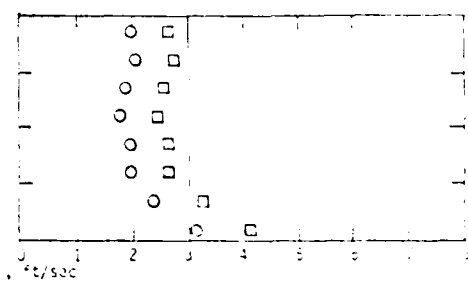
a) L-1011, 2/73-5/73, 201 hours



b) B-727, 6/78-3/79, 575 hours



c) L-1011, 3/78-8/78, 565 hours

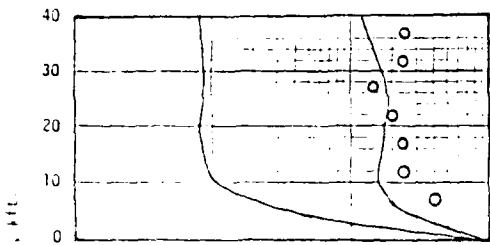


d) B-747, 2/78-4/79, 546 hours

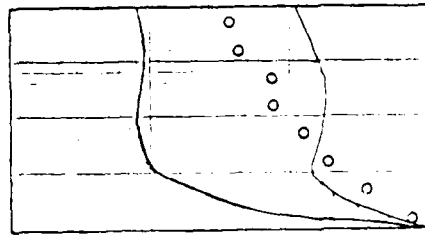
DVGH GUST INTENSITY CALCULATIONS

11/11/79

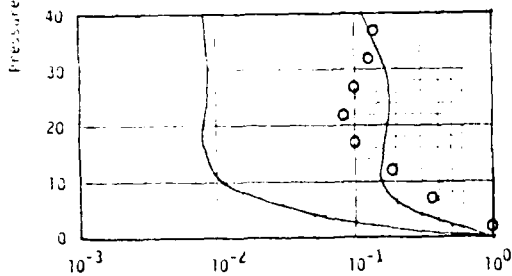
$$\frac{N}{N_0} = P e^{-U_3/31}$$



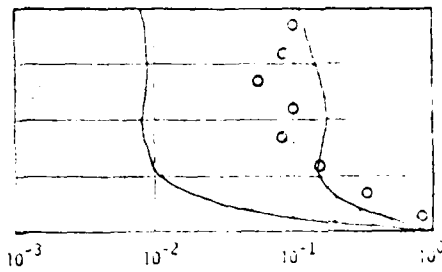
a) L-1011 , 2/73-5/73 , 201 Hours



b) B-727 , 6/78-3/79 , 575 Hours

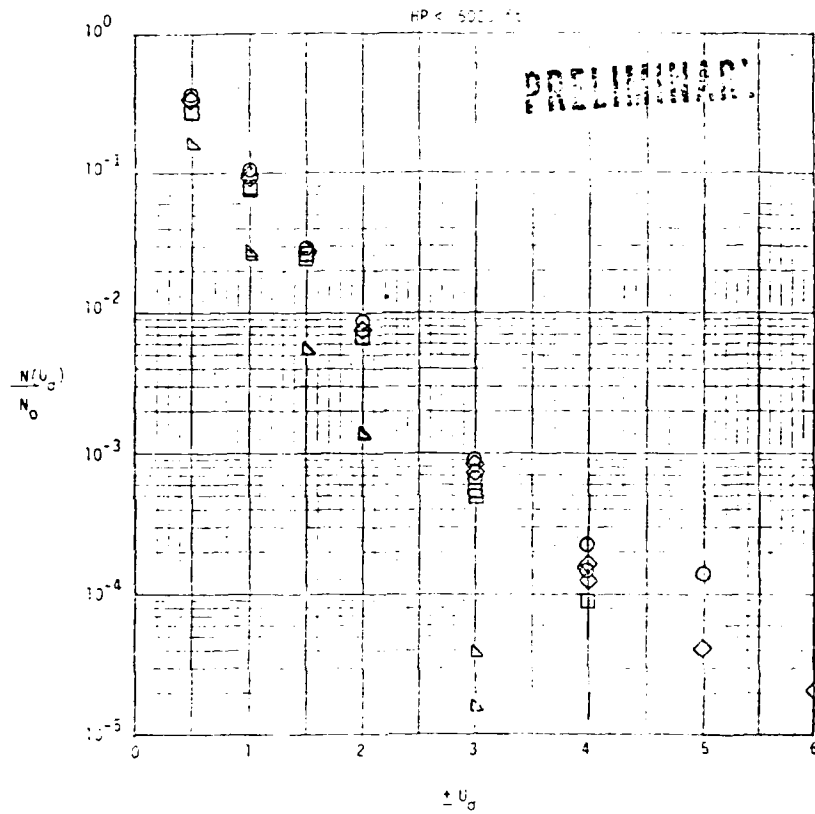


c) L-1011 , 3/78-8/78 , 565 Hours



d) B-747 , 5/78-4/79 , 546 Hours

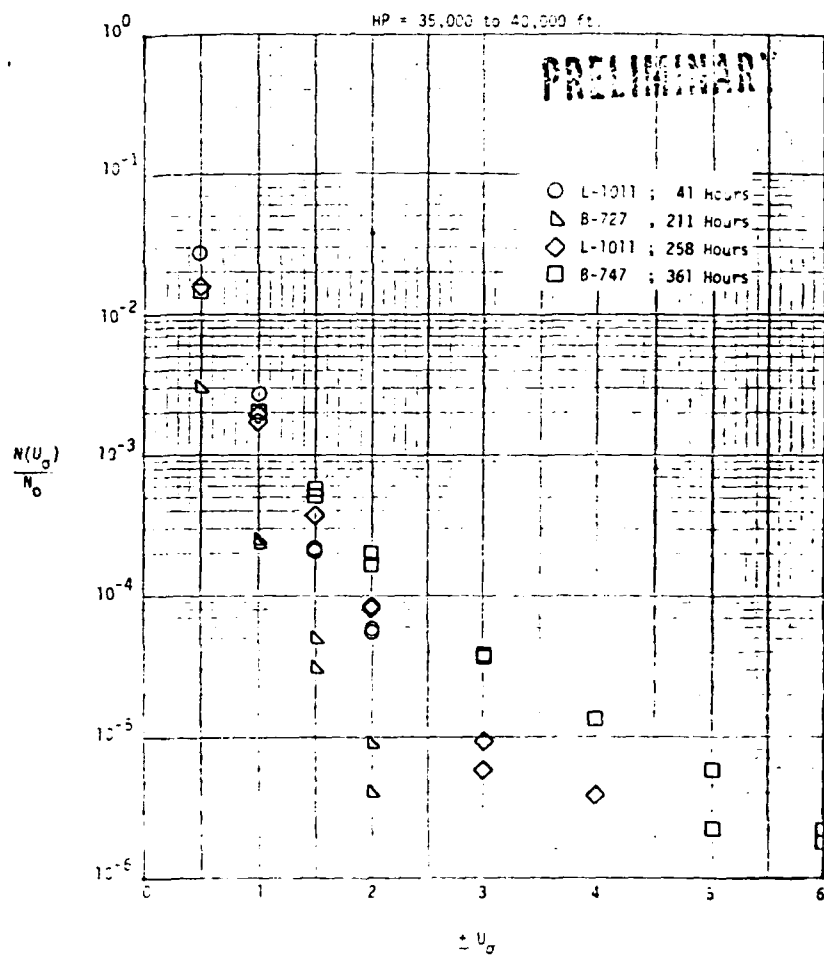
DMH PERCENT TIME IN TURBULENCE CALCULATIONS



| Symbol   | ○                          | □   | ◇                          | △                                    |
|----------|----------------------------|---|----------------------------|--------------------------------------|
| Aircraft | L-1011                     | B-747   | L-1011                     | B-727                                |
| Period   | 2/73-6/73                  | 5/78-4/79                                       | 3/75-8/75                  | 6/78-3/79                            |
| Hours    | 13                         | 21  | 41                         | 35                                   |
| Route    | Eastern U.S. and Caribbean | Southern Canada, Continental U.S. Transatlantic | Eastern U.S. and Caribbean | Southern Canada and Continental U.S. |

DATA COMPARISON OF NORMALIZED LEVEL-CHORDING COUNTS PER SECOND





GRAPH COMPARISON OF NORMALIZED LEVEL-CROSSING COUNTS PER SECOND

NASA LANGLEY RESEARCH CENTER

STORM HAZARDS PROGRAM

MARCH 1981

NLCRABILL - 1

## NASA STORM HAZARDS PROGRAM

- 0 PROGRAM ORIGINATED IN 1977 IN RESPONSE TO:
  - o NTSB REVIEW CALLING FOR "MORE SOPHISTICATED MEASUREMENT OF THUNDERSTORM AND TURBULENCE"
  - o ALPA CALL FOR "REALISTIC POLICIES FOR FLIGHT OPS IN SEVERE STORM AREAS"
  - o NASA ASSESSMENT OF LIGHTNING HAZARD
    - . NON-METALLIC STRUCTURES
    - . DIGITAL AVIONICS AND CONTROLS
    - . DATA NEEDED AT FLIGHT ALTITUDES
- 0 EVOLVED BROAD SCOPE PROGRAM IN RESPONSE
  - o HAZARD PREDICTION, DETECTION, AND AVOIDANCE; DESIGN CRITERIA FOR UNAVOIDABLE HAZARDS
  - o HAZARDS OF RAIN, HAIL, WIND SHEAR, TURBULENCE, AND LIGHTNING

LARC STORM HAZARDS PROGRAM MATRIX

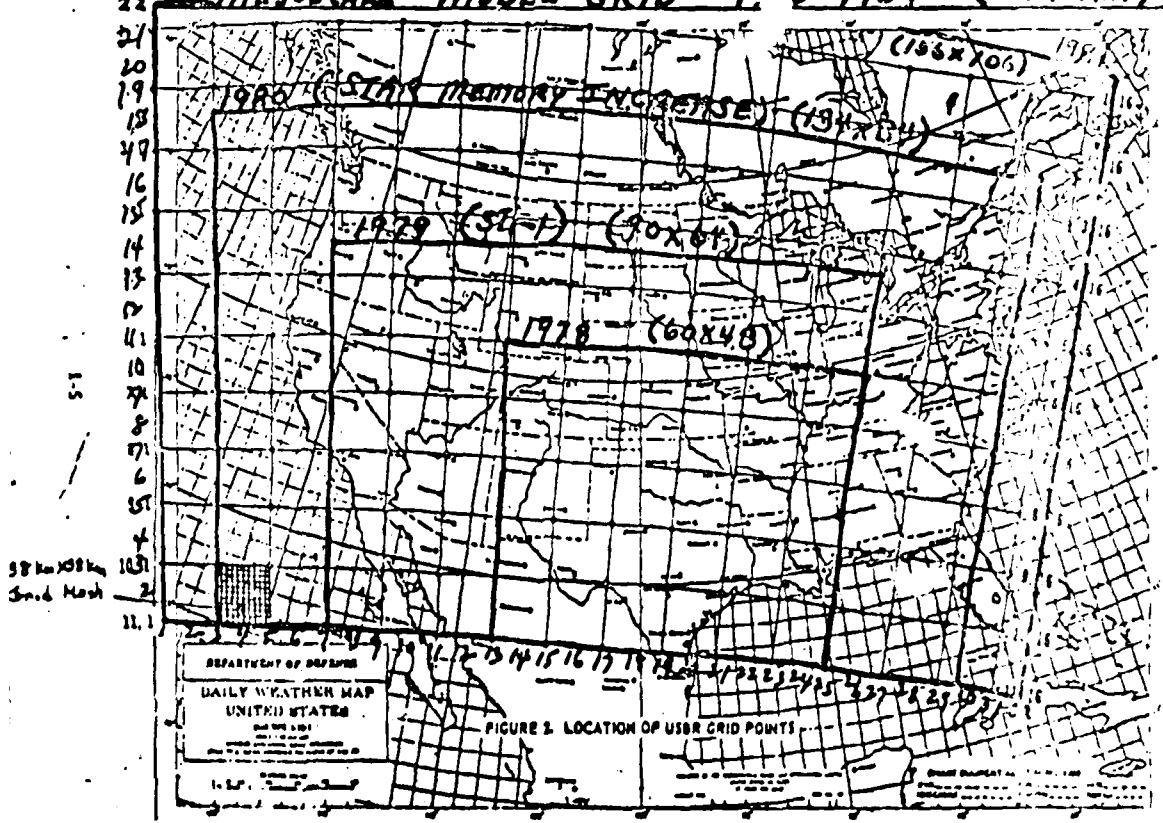
|            | PRECIP  | WIND SHEAR   | TURBULENCE   | LIGHTNING  |
|------------|---|--|--|--|
| PREDICTION | ← COMPUTER FORECASTING →  |  |  |  |
| DETECTION  | <ul style="list-style-type: none"> <li>EFFECTS OF RAIN LAYER ON AIRBORNE RADOME PERFORMANCE</li> </ul>              | <ul style="list-style-type: none"> <li>GROUND-BASED DOPPLER RADAR MEASUREMENTS CORRELATION WITH AIRBORNE TRUTH MEASUREMENTS OF WIND AND TURBULENCE</li> <li>AIRBORNE DOPPLER RADAR MEASUREMENTS AND CORRELATION WITH AIRBORNE AND GROUND MEASUREMENTS</li> </ul> |  | <ul style="list-style-type: none"> <li>STORM TRACKING</li> <li>LDAR</li> <li>ATMOSPHERIC ELECTRICITY</li> <li>X-RAY</li> <li>OPTICAL DETECTION</li> </ul>  |
| DESIGN     | <ul style="list-style-type: none"> <li>EFFECTS OF RAIN LAYER ON AIRCRAFT AERODYNAMICS ?</li> </ul>                  | <ul style="list-style-type: none"> <li>AIRBORNE INS-TAS DIFFERENCING ON TAKE-OFF AND LANDING                             <ul style="list-style-type: none"> <li>TWA</li> <li>F-106</li> </ul> </li> </ul>  | <ul style="list-style-type: none"> <li>AIRLINER GUST AND MANEUVER LOADS (DIGITAL VGH PROGRAM)</li> </ul> | <ul style="list-style-type: none"> <li>DIRECT LIGHTNING TRANSDUCERS</li> <li>COMPARISON OF MATERIALS                             <ul style="list-style-type: none"> <li>FRUIT BREAD</li> <li>LEAD TESTS</li> </ul> </li> </ul> |
| AVOIDANCE  | <ul style="list-style-type: none"> <li>MAP ALL HAZARDS ON MANY SEVERE STORMS AND REVIEW CURRENT CRITERIA</li> </ul> |  |  |  |

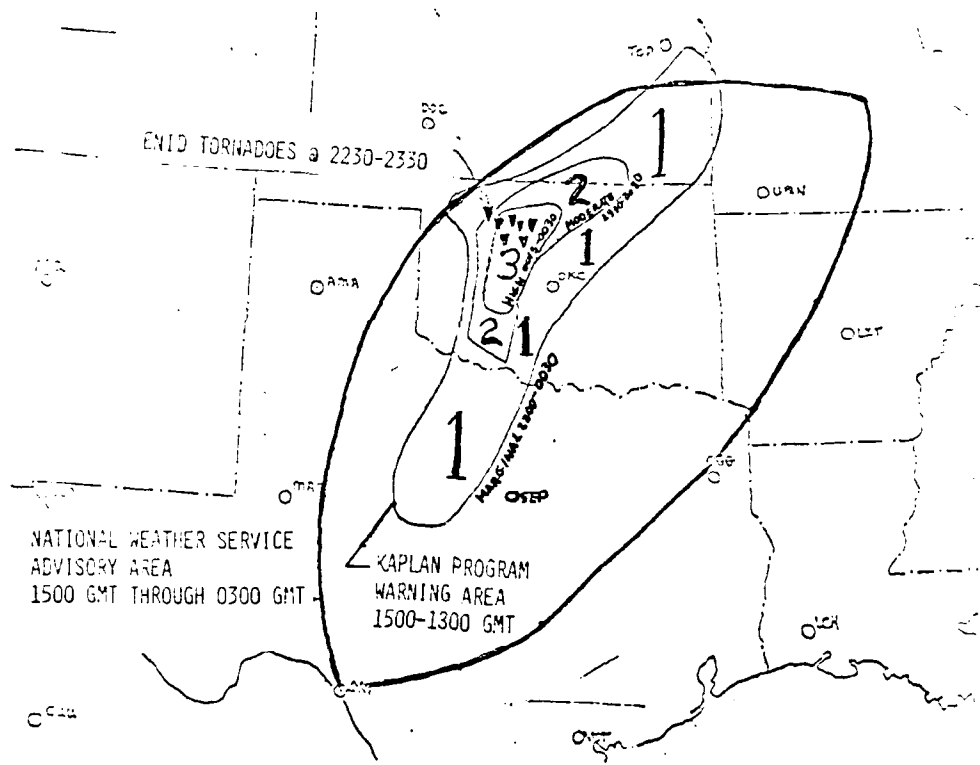
F-106 FLIGHT PROGRAM 3

## COMPUTER FORECASTING SEVERE STORMS

- SEVERE CONVECTIVE STORM MODEL
  - DIFFERENTIAL EQUATIONS OF ATMOSPHERE; HYDROSTATIC
    - . 15 LEVELS TO 15 KM
    - . 38, 19, AND 9 KM GRID MESH
    - . 156 X 106 GRID POINTS (~5900 X 4000 KM)
  - COMPUTES DYNAMIC STATE OF ATMOSPHERE FOR NEXT 24 HOURS IN 1 MINUTE STEPS (USUALLY PLOT AT 1 HOUR INTERVALS)
  - OPERATIONAL TEST IN 78, 79, 80
    - 30 - 50 CONSECUTIVE DAYS
    - NATIONAL SEVERE STORMS LAB 80 EVALUATION PROMISING
  - FURTHER TESTS PLANNED
    - 1982 MAR - AUG (180 DAYS)
    - GODDARD SPACE FLIGHT CENTER EVALUATION
      - . SUBJECTIVE
      - . OBJECTIVE

1981 MESOSCALE MODEL GRID 8-1989 (30.1 KM)

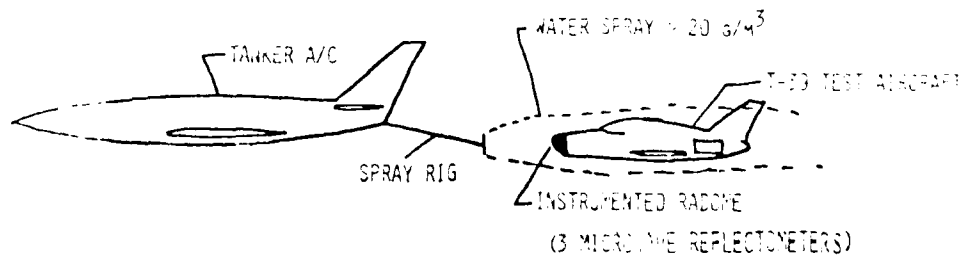




ENID OKLAHOMA - MAY 2, 1979

EFFECTS OF RAIN LAYER ON  
AIRBORNE RADOME PERFORMANCE

- 1st ORDER THEORY PREDICTS ~ 15 dBZ LOSS AT  $20 \text{ g/m}^3$  & 500 KTS AT X BAND
- FLIGHT TEST PLANNED SUMMER 1981 TO MEASURE WATER LAYER THICKNESS WITH MICROWAVE REFLECTOMETERS - FAA/NASA/USAF





EFFECTS OF RAIN LAYER ON AIRCRAFT AERODYNAMICS

- 0 THEORETICAL STUDY BY U. DAYTON SHOWS @ 500 MM/HR  
(67.5 dBZ OR 16.5 G/M<sup>3</sup>) ON 747 ON APPROACH
  - o FILM THICKNESS = .8 MM AVERAGE ON TOP OF WING
  - o  $\Delta C_{D_{WING}} = + 13\%$  DUE TO DROP CRATERING ) EFFECTS ON ROUGHNESS  
+ 21% DUE TO WAVINESS
- 0 LARC IS INVESTIGATING METHODS OF EXPERIMENTALLY VERIFYING THESE
  - o MEASURE FILM THICKNESS, OR
  - o MEASURE INTEGRATED EFFECTS

## WIND SHEAR

- 0 WIND PROFILES TO 2000 FEET ON TAKE-OFF AND LANDING FROM:  
INS & TAS VELOCITY DIFFERENCING
  - o 1082 FLIGHTS FROM TWA 747
  - o ALL FUTURE F-106 FLIGHTS
  
- 0 PROBLEM
  - o DEFINE SUITABLE STATISTICAL FORMATS
  - o REDUCE PROFILES TO THOSE FORMATS AND PUBLISH

AD-A136 364

REPORT ON A VISIT TO THE USA DURING JANUARY 1982  
RELATING TO THE EFFECT OF (U) AERONAUTICAL RESEARCH  
LABS MELBOURNE (AUSTRALIA) D J SHERMAN AUG 82

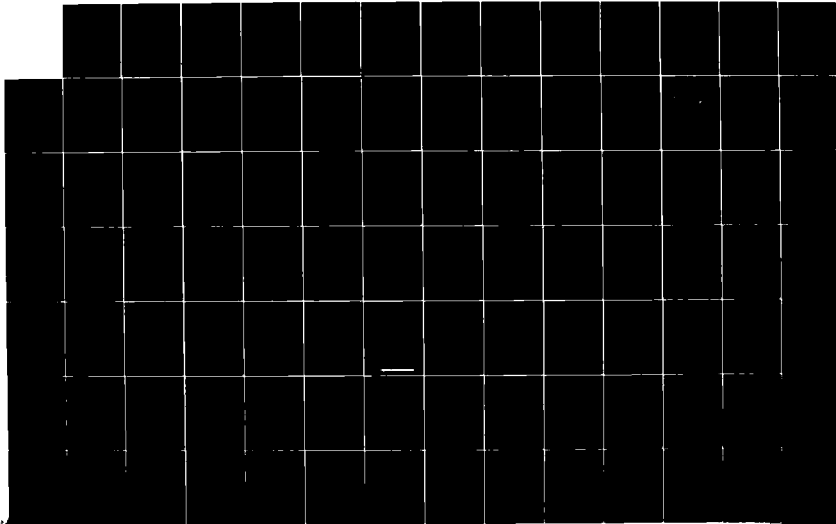
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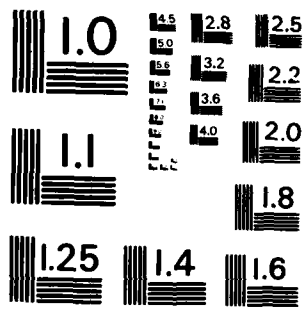
UNCLASSIFIED

ARL/STRUC-TM-344-SUPPL

F/G 4/2

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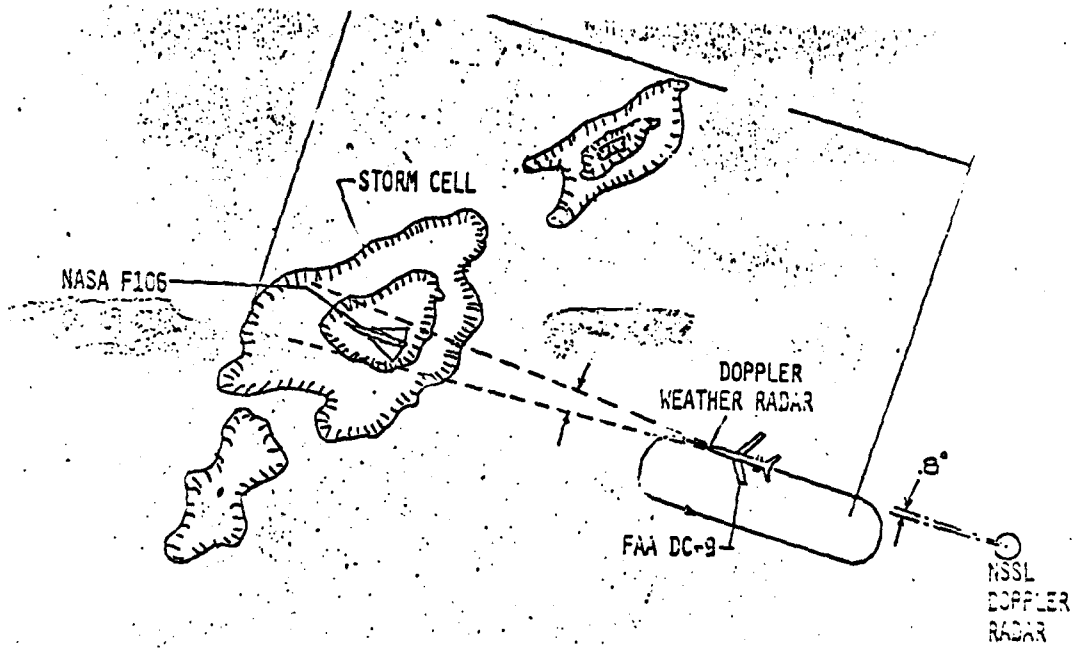




MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS - 1963 - A

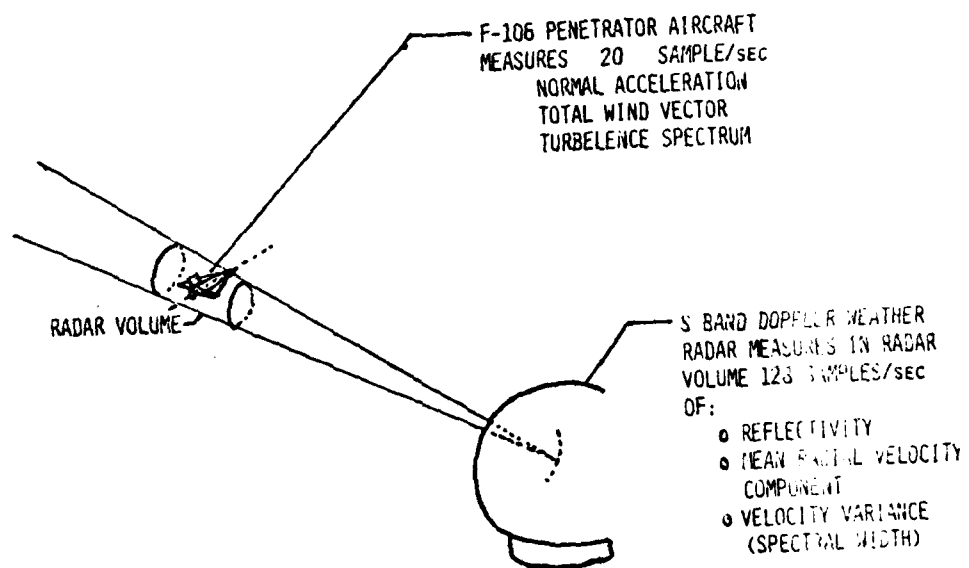
## AIRLINER GUST AND MANEUVER LOADS

- PROVIDE DATA FOR DESIGN CRITERIA UPDATING
- GUST EXCEEDANCES DERIVED FROM AIRLINER FLIGHT RECORDER DATA
- RESULTS
  - 1973 DATA ~ 200 HOURS ON L1011 - METHODOLOGY
  - 1978-79 DATA ~ 2000 HOURS ON L1011, B727, B747
  - 1981-82 DATA ~ 2000 HOURS ON DC-10

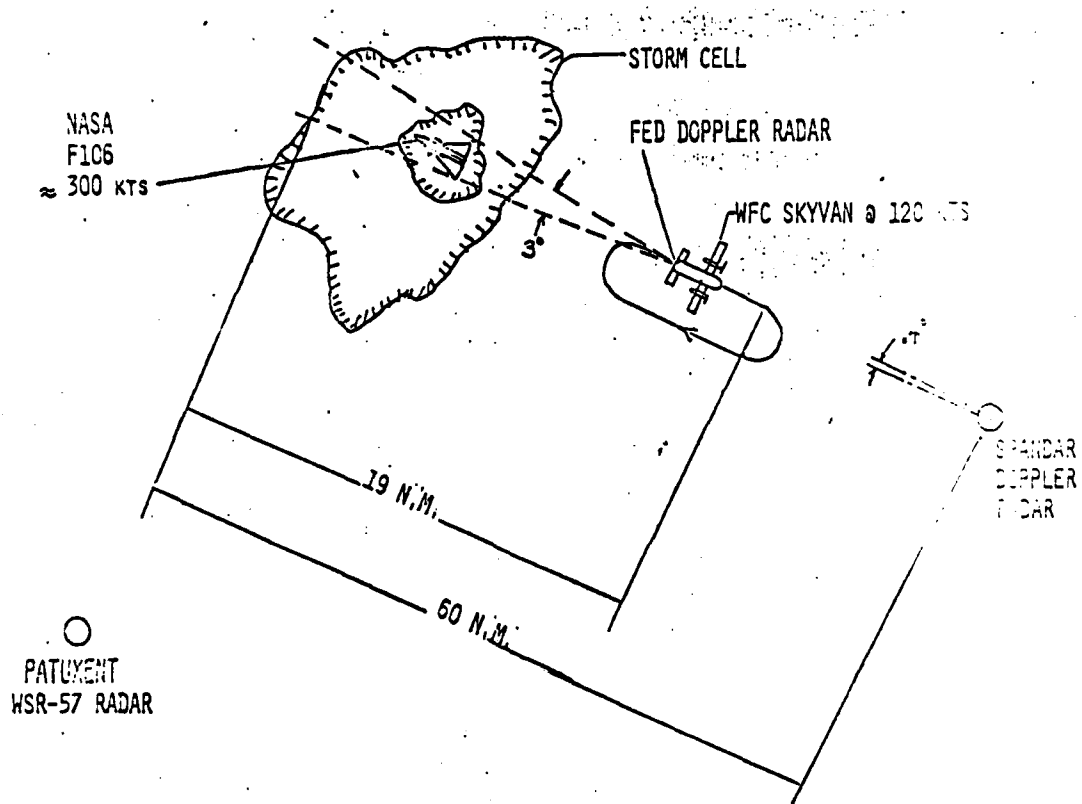


COMMERCIAL "HARD WIRED" DOPPLER WEATHER RADAR  
AIRBORNE DOPPLER WEATHER RADAR TEST FOR 1981

GROUND-BASED DOPPLER RADAR MEASUREMENTS  
OF WIND AND TURBULENCE WITH F-106



EXPERIMENT WILL DETERMINE CORRELATION OF SPECTRUM WIDTH OVER THE RADAR  
VOLUME WITH AIRCRAFT MEASUREMENTS OF ATMOSPHERIC TURBULENCE AND NORMAL  
ACCELERATION RESPONSE



RESEARCH DOPPLER WEATHER RADAR  
AIRBORNE DOPPLER WEATHER RADAR TEST FOR 1931



## LIGHTNING DETECTION AND HAZARD CORRELATION

- ① FLIGHT TEST
    - TWIN OTTER 1978 @ NSSL - REPORTED
    - F-106 1979, 1980, 1981 @ NSSL & WFC
  - ① WALLOPS HAS INSTALLED
    - STORMSCOPE (X, Y LIGHTNING LOCATION TO 200 N.MI.)
    - LDAR (X, Y, Z LIGHTNING LOCATION OUT TO 40-50 MILES)
    - ELECTRIC & MAGNETIC FIELD TRANSIENTS TO 30-40 MILES
    - SFERICS DETECTION TO 75-500 MILES
    - SPANDAR
      - . REFLECTIVITY
      - . MEAN WIND
      - . TURBULENCE
- } TO 64 N.MI. @ 1280 PRF
- ① MEASUREMENTS AND CORRELATION OF LIGHTNING LOCATION, STRENGTH, AND POLARITY WITH RADAR REFLECTIVITY, WIND, AND TURBULENCE CAN BE PERFORMED ROUTINELY EVEN WITHOUT THE F-106 FLIGHT OPERATION

LIGHTNING EFFECTS ON COMPOSITE STRUCTURES  
WITH  
MATERIALS DIVISION

o OBJECTIVE:

- . PROVIDE TECHNICAL DATA-BASE FOR GENERAL AVIATION DESIGN
- . PROVIDE GUIDELINES FOR DESIGN INCLUDING ELECTRICAL AND FUEL SYSTEMS OF GA AIRCRAFT
- . PROVIDE VERIFICATION PROCEDURES FOR DESIGN EVALUATION
- . DEVELOP NON-DESTRUCTIVE TEST TECHNIQUES

o GROUND TEST - LIGHTNING TECHNOLOGIES INCORPORATED:

- . BONDED METAL STRUCTURES - DUCHESS WING  
CESSNA XOX WING
- . ALL COMPOSITE STRUCTURES - LEAR FAN WING

o FLIGHT TEST - F-106B-COMPOSITE FIN CAP

## DIRECT-STRIKE LIGHTNING ELECTROMAGNETIC TRANSIENT EXPERIMENT ON F-106

- o PAST LIGHTNING PROTECTION DESIGN BASED ON CLOUD-TO-GROUND DATA DIRECT EFFECTS
- o AIRCRAFT STRUCTURES WERE METAL "FARADAY SHIELDS" WITH ANALOG ELECTRONICS, MECHANICAL, AND HYDRAULIC CONTROL SYSTEMS -- DESIGN APPROACHES EVOLVED WITH EXPERIENCE
- o FUTURE AIRCRAFT WILL USE MORE COMPOSITE STRUCTURES AND DIGITAL AVIONICS AND FIBER-OPTIC WIRE SYSTEMS
- o NEED EXISTS TO MORE ACCURATELY CHARACTERIZE LIGHTNING HAZARD FOR DESIGN PURPOSES AT AIRCRAFT OPERATING ALTITUDES:
  - . DIRECT AND NEARBY LIGHTNING STRIKE
  - . ASSESSMENT OF INDUCED EFFECTS
  - . FREQUENCY-OF-OCCURRENCE DATA
- o F-106 AIRCRAFT:
  - . INSTRUMENTED TO MEASURE AND RECORD ELECTROMAGNETIC TRANSIENTS
  - . PENETRATION OF MODERATE ~ 40 DBZ THUNDERSTORMS
  - . CORRELATE WITH GROUND-BASED MEASUREMENTS
- o DEVELOP SIMPLIFIED "FREQUENCY-OF-OCCURRENCE" MEASUREMENT SYSTEM FOR FLEET USE

## STORM HAZARDS '80 FLIGHT EXPERIMENTS - F-106

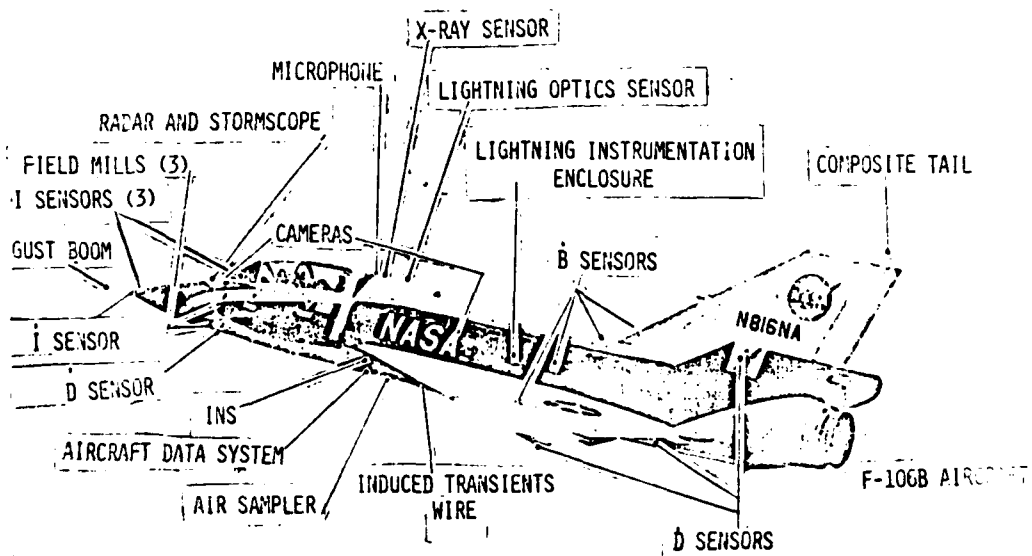
## LIGHTNING RELATED:

- ① DIRECT-STRIKE LIGHTNING (NASA - PITTS)
- ① LIGHTNING DATA LOGGER (BOEING)
- ① ATMOSPHERIC CHEMISTRY (NASA - LEVINE)
- ① LIGHTNING X-RAYS (UNIV. OF WASHINGTON - PARKS)
- ① LIGHTNING OPTICAL SIGNATURE (NSSL - RUST)
- ① LIGHTNING STRIKE PATTERNS (NASA - FISHER)
- ① COMPOSITE FIN CAP (NASA - HOWELL)
- ① FIELD MILLS (NASA - PITTS)
- ① CAMERAS (NASA - PITTS)
- ① INDUCED TRANSIENTS EXPERIMENT (NASA - PITTS)

## NON-LIGHTNING RELATED:

- ① TURBULENCE (NASA - DUNHAM)
- ① WIND SHEAR (NASA - DUNHAM)
- ① STORM HAZARDS CORRELATION (NASA - FISHER)

I = STRIKE CURRENT  
D = ELECTRIC FLUX DENSITY  
B = MAGNETIC FLUX DENSITY



NASA-LANGLEY RESEARCH CENTER STORM HAZARDS RESEARCH VEHICLE

F-106 MISSION SUMMARY  
THROUGH SEPTEMBER 10, 1980

|               | LARC | TIK | ACY | LARC | FERRY | TOTALS |
|---------------|------|-----|-----|------|-------|--------|
| FLIGHTS       | 5    | 13  | 3   | 14   | 4     | 39     |
| STORM FLIGHTS | 0    | 9   | 0   | 11   | -     | 11     |
| PENETRATIONS  | 0    | 32  | 0   | 37   | -     | 69     |
| LIGHTING:     |      |     |     |      |       |        |
| DIRECT HITS   | 0    | 3   | 0   | 7    | 0     | 10     |
| TRANSIENTS    | 0    | 2   | 0   | 25   | 0     | 27     |
| ACE SAMPLES   | 0    | 63  | 0   | 72   | 0     | 135    |

TOTAL FLIGHT TIME

39 HOURS AND 55 MINUTES

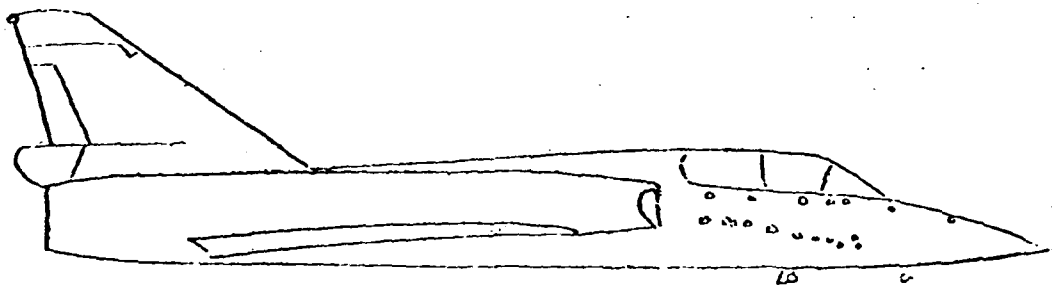
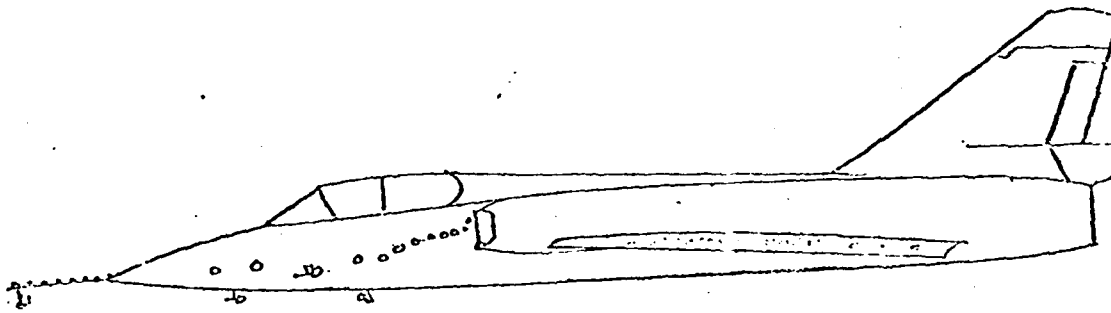
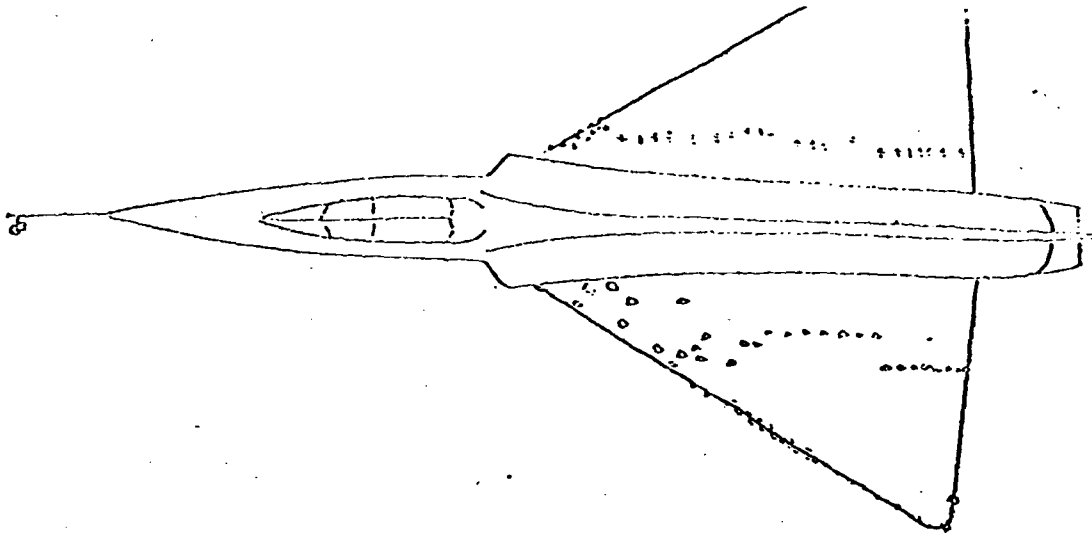
SOME PRINCIPAL RESULTS OF 1980  
F-106 STORM HAZARDS FLIGHTS

- 0 DIRECT STRIKE LIGHTNING
  - o 27 TRANSIENTS OBTAINED
  - o MAGNETIC FIELD RATES SMALLER THAN EXPECTED
- 0 ATMOSPHERIC CHEMISTRY EXPERIMENT
  - o 116 USEABLE THUNDERSTORM SAMPLES - 34% SHOW ENHANCED  $N_2O$  VALUES ABOVE CLEAR AIR
- 0 X-RAY
  - o SIGNIFICANTLY ENHANCED COUNTS HAVE BEEN MEASURED FOR THE FIRST TIME AT FLIGHT ALTITUDES - BELIEVED TO BE DUE TO ELECTRON BREMSSTRAHLUNG PROCESS
- 0 COMPOSITE STRUCTURE
  - o MINOR DAMAGE TO 5 MIL ALUMINUM COATING IN ONE STRIKE
- 0 LIGHTNING OPTICAL SIGNATURES
  - o TRANSIENTS IDENTIFIED - ANALYSIS CONTINUING
- 0 HIT PATTERNS
  - o THREE SWEEP STROKES ACROSS WING IN MID SPAN

F-106 LIGHTNING STRIKE PATTERNS

- ① UNEXPECTED DATA TYPE
- ② FULL-SCALE, IN-FLIGHT DATA
- ③ SIGNIFICANT TO AIRCRAFT DESIGN = PLATE THICKNESS
- ④ DATA ALREADY BEING APPLIED BY INDUSTRY





• APPROXIMATE LOCATION OF F-106 LIGHTNING HITS  
FLIGHTS 018 AND 019, JUNE 17, 1961, OKLAHOMA

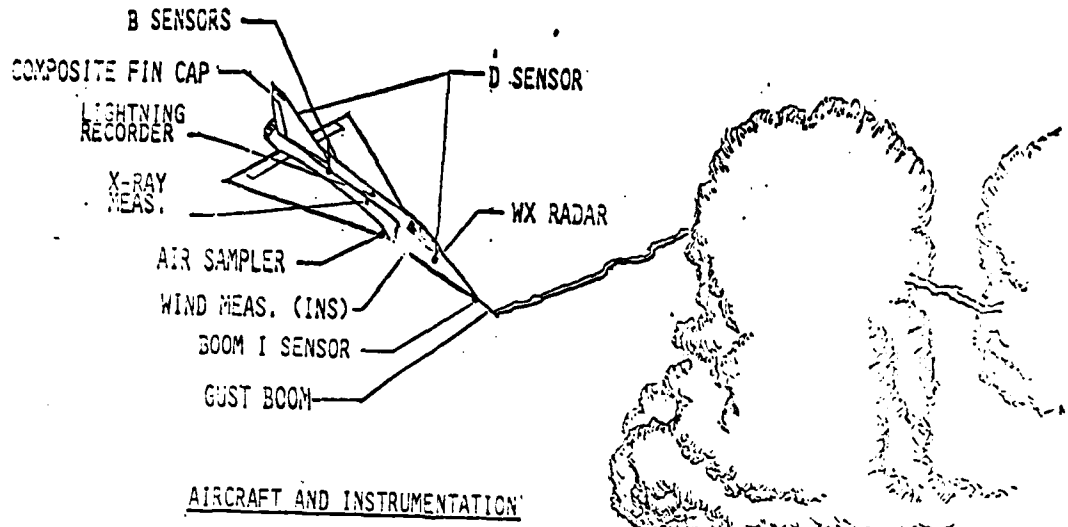
THUNDERSTORM TURBULENCE

R. E. DUNHAM  
(N. L. CRABILL)

JANUARY 1982

## ▲ NASA STORM HAZARDS PROGRAM

- T-STORMS MAJOR PROBLEM
  - CURRENT OPERATIONS
    - NTSB - TODD '77
    - ALPA - MUDGE '78
  - NEW TECHNOLOGY AIRCRAFT - LIGHTNING EFFECTS - PLUMER
    - DIGITAL AVIONICS
    - COMPOSITE STRUCTURES
- STORM HAZARDS PROGRAM OBJECTIVES
  - IMPROVE STATE OF THE ART IN DETECTING AND CHARACTERIZING ALL T.STORMS HAZARDS: LIGHTNING, WIND, TURBULENCE, PRECIPITATION
  - IMPROVE UNDERSTANDING OF CURRENT AND FUTURE AIRCRAFT RESPONSE TO T.STORM HAZARDS FOR DESIGN AND OPERATING CRITERIA IMPROVEMENTS
  - RESEARCH MESOSCALE FORECASTING TECHNIQUES USING NUMERICAL MODELING



AIRCRAFT AND INSTRUMENTATION

| BOX SCORE        |      |      |      |
|------------------|------|------|------|
|                  | 1980 | 1981 | GOAL |
| FLIGHTS          | 40   | 48   |      |
| PENETRATIONS     | 69   | 111  |      |
| HITS             | 10   | 10   | 300  |
| TRANSIENTS: NASA | 22   | 32   |      |
| BOEING           | 0    | 1    |      |

LIGHTNING  
DIRECTION AND  
RANGING

ELECTRIC  
FIELD (GSFC)

MSR 57 E  
PILGRIM

SPINDLE  
(JOBBER)  
WFSL

## WINDS AND TURBULENCE MEASUREMENTS IN SEVERE STORMS

### OBJECTIVES

- o CHARACTERIZE WINDS AND TURBULENCE IN SEVERE STORMS
- o CORRELLATION OF WINDS AND TURBULENCE LEVELS WITH OTHER STORM HAZARDS (LIGHTNING AND PRECIPITATION)
- o PROVIDE DATA FOR EVALUATING REMOTE SENSING METHODS OF TURBULENCE DETECTION
- o PROVIDE WIND FIELD DATA FOR VALIDATING MODELS OF SEVERE STORMS

## DATA REDUCTION

AIRSPEED - INERTIAL SPEED = WINDSPEED

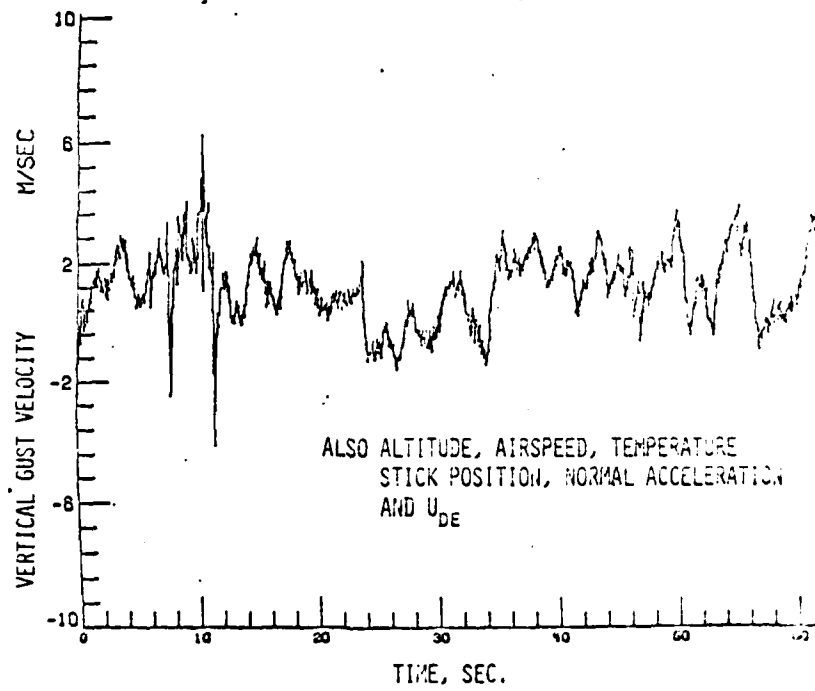
$$\left\{ \begin{array}{l} \text{EULER ANGLE} \\ \text{TRANSFORMATION} \end{array} \right\} \left\{ \begin{array}{l} V \cos \alpha \cos \beta \\ V \sin \alpha \cos \alpha \\ V \sin \alpha \end{array} \right\} - \left\{ \begin{array}{l} V_N \\ V_E \\ \int a_z dt \end{array} \right\} - \left\{ \begin{array}{l} \text{EULER ANGLE} \\ \text{TRANSFORMATION} \end{array} \right\} \left\{ \begin{array}{l} 0 \\ 1r \\ 1q \end{array} \right\} = \left\{ \begin{array}{l} \text{NORTH WIND} \\ \text{SOUTH WIND} \\ \text{VERTICAL WIND} \end{array} \right\}$$

DATA RECORDED ON MAGNETIC TAPE

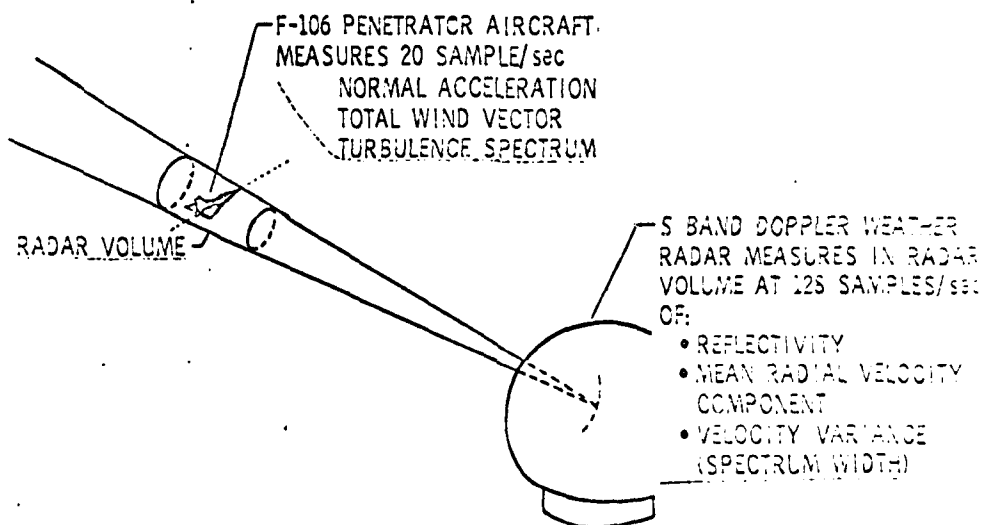
FREQUENCY RESPONSE GOOD TO 10 HERTZ

VELOCITIES ACCURATE TO  $\pm 1\%$  (AIRSPEED 200 M/S)

505-44-13 AVIATION METEOROLOGY RESEARCH-STORM HAZARDS  
F.Y. 81 RESULTS F-106 WIND AND GUST TIME HISTORIES-1980 DATA



**GROUND-BASED DOPPLER RADAR MEASUREMENTS OF WIND AND  
TURBULENCE AND CORRELATION WITH F-106 RESULTS**



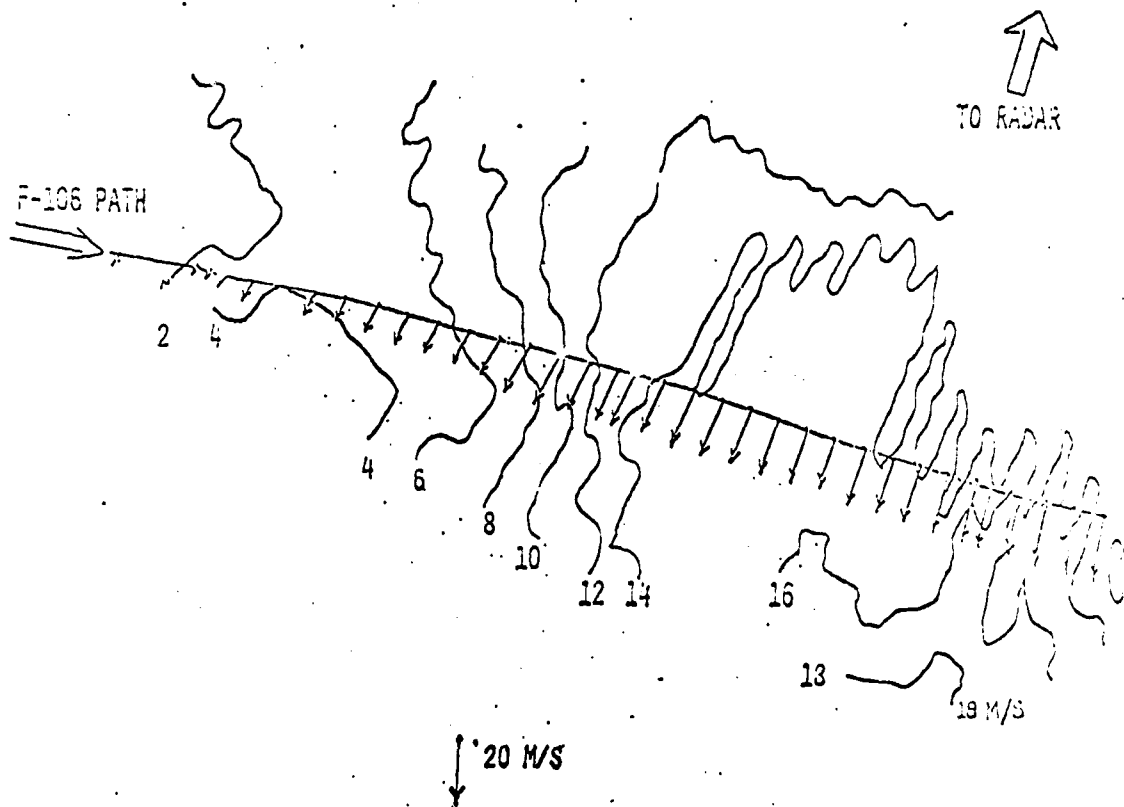
EXPERIMENT WILL DETERMINE CORRELATION OF SPECTRUM WIDTH OVER  
THE RADAR VOLUME WITH AIRCRAFT MEASUREMENTS OF ATMOSPHERIC  
TURBULENCE AND NORMAL ACCELERATION RESPONSE

PRELIMINARY THEORY INDICATES TURBULENCE IN PRECIPITATION HAS  
DIFFERENT POWER SPECTRUM

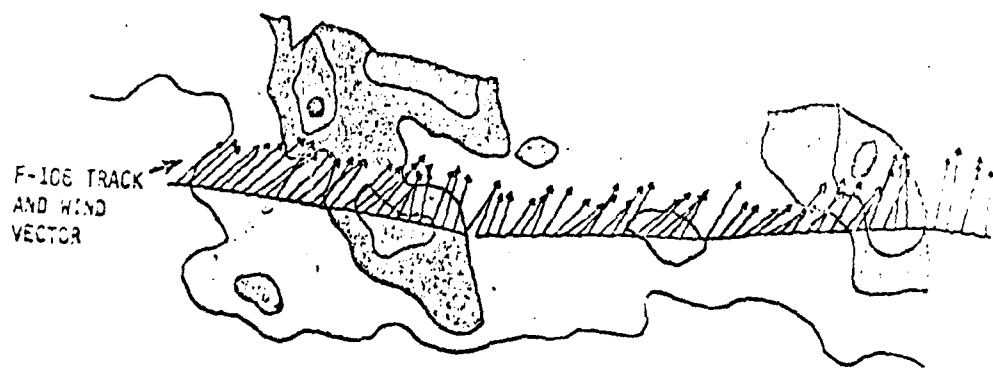






505-44-13 AVIATION METEOROLOGY RESEARCH-STORM HAZARDS

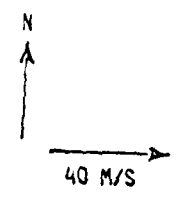
F.Y. 81 RESULTS WIND GROUND BASED DOPPLER WIND-'80 DATA



505-44-13 AVIATION METEOROLOGY RESEARCH-STORM HAZARDS  
F.Y. 81 RESULTS WIND AND GUST DATA VS RADAR REFLECTIVITY - 1980 DATA



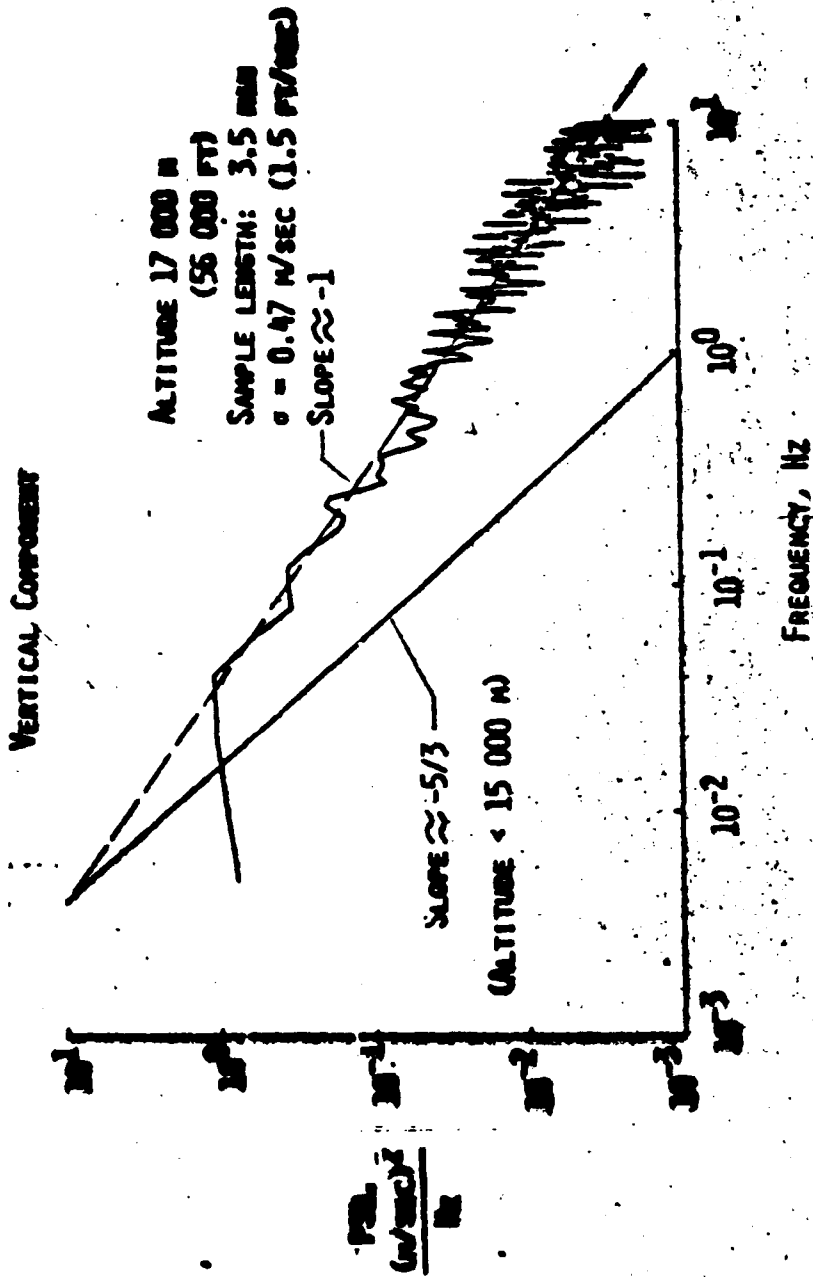
- RAIN FALL RATE
-  56 mm/hr
  -  23 mm/hr
  -  5 mm/hr
  -  .8 mm/hr



## SUMMARY

- 0 IN 1980, 104 MINUTES OF TURBULENCE DATA IN SEVERE STORMS WERE COLLECTED AND TRANSMITTED TO NSSL FOR COMPARISON WITH GROUND BASED STORM MEASUREMENTS (DOPPLER RADAR AND WS-57)
  
- 0 IN 1981, 25 THUNDERSTORM FLIGHTS WERE FLOWN WITH USEABLE TURBULENCE DATA. THESE DATA WILL BE REDUCED IN THE COMING YEAR.

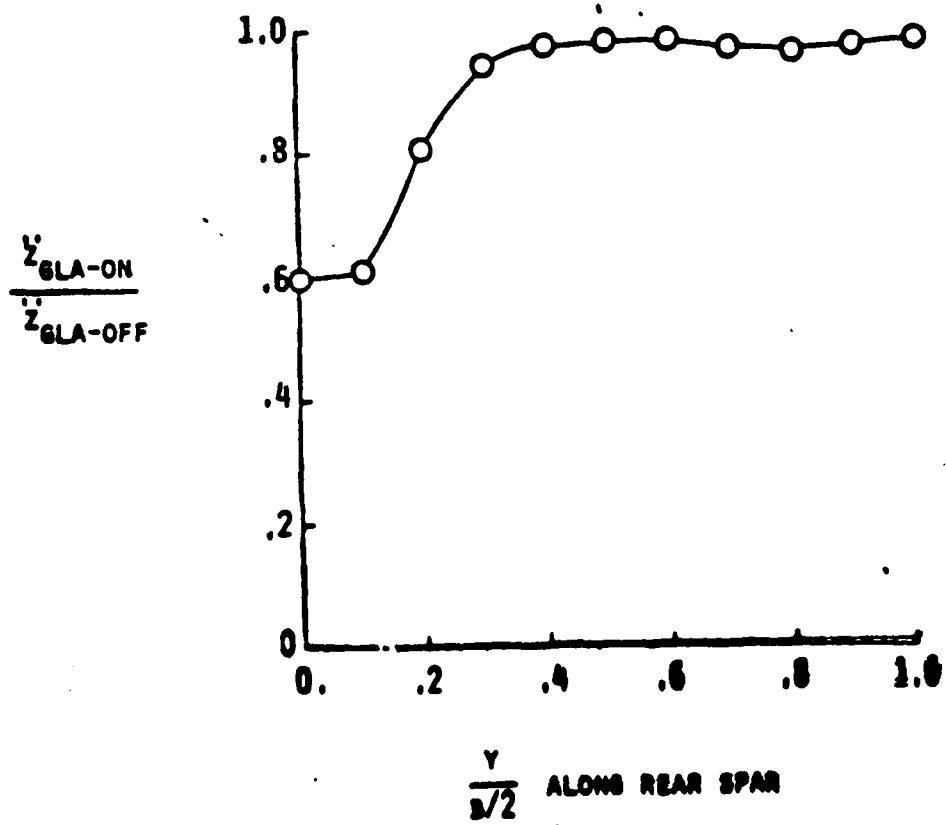
INITIAL SPECTRUM OF 800 ALTITUDE GEOMAGNETIC TURBULENCE EMITS SURPRISING FEATURE

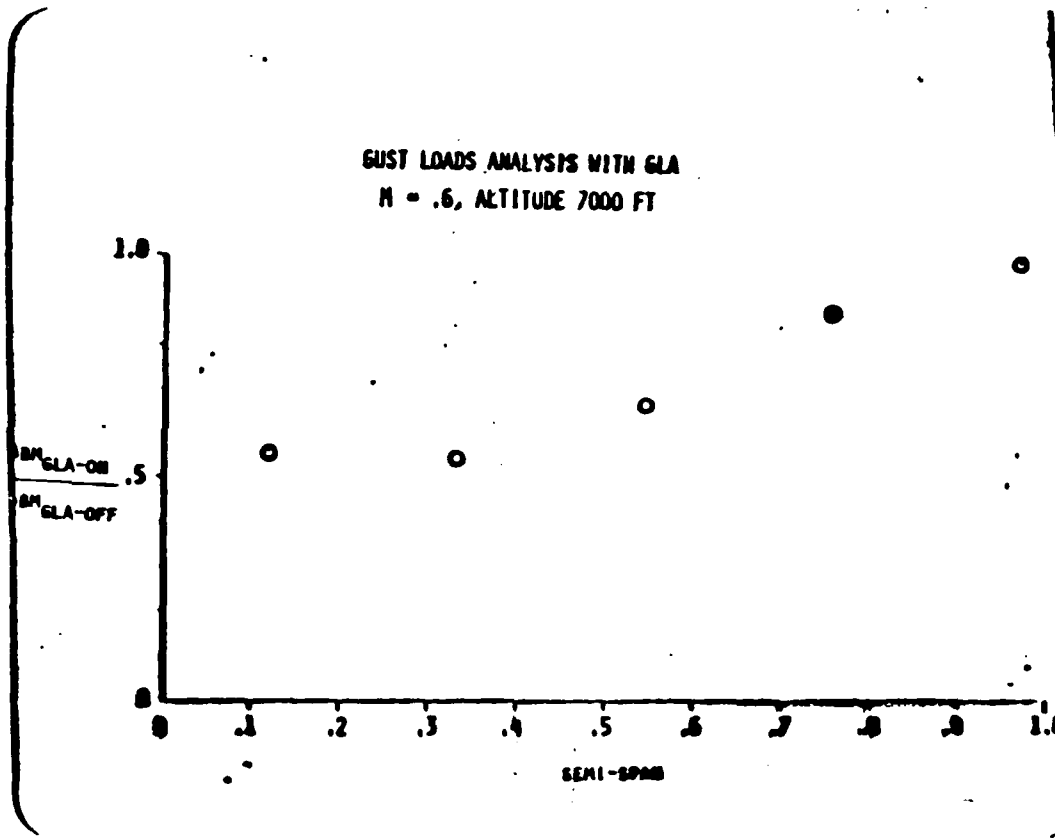


ANALYSIS OF GLA-SYSTEM USING DYLOFLEX

M = 0.6

ALTITUDE = 7000 FT





WIND-SHEAR

R. E. DUNHAM  
(N. L. CRABILL)

JANUARY 1982

IN-FLIGHT WIND SHEAR ENCOUNTERS

OBJECTIVES:

DETERMINE THE FEASIBILITY OF OBTAINING AIRBORNE MEASUREMENTS OF WINDS AND WIND SHEARS FROM COMMERCIAL OPERATIONS DURING LANDINGS AND TAKEOFFS

APPROACH:

OBTAIN DATA FROM A COMMERCIAL AIR CARRIER OPERATING AIRPLANES EQUIPPED WITH INERTIAL NAVIGATION SYSTEMS AND DIGITAL FLIGHT DATA RECORDERS



METHOD:

OBTAINED 2 WEEKS OF DATA IN THE SPRING OF 1977 ON A  
U.S. AIR CARRIER (TWA) EQUIPPED WITH DFDR-AIDS AND INS

DATA RECORDED:

TRUE AIRSPEED  
ANGLE OF ATTACK  
RADAR ALTIMETER  
TIME  
HEADING  
LATITUDE  
LONGITUDE  
DRIFT ANGLE  
GROUNDSPEED  
PITCH ATTITUDE  
ROLL ATTITUDE

DATA REDUCTION

HORIZONTAL WIND IS THE DIFFERENCE BETWEEN THE TRUE AIRSPEED AND THE GROUND SPEED. WIND VECTOR IS BROKEN INTO COMPONENTS ALONG THE NORTH-SOUTH AND EAST-WEST DIRECTIONS.

$$\text{NORTH-SOUTH} = V_{\text{GROUNDSPEED}} \cos(\text{HEADING} + \text{DRIFT ANGLE}) - V_{\text{AIRSPEED}} \cos(\text{PITCH ATTITUDE} - \text{AOA}) \cos(\text{HEADING})$$

$$\text{EAST-WEST} = V_{\text{GROUNDSPEED}} \sin(\text{HEADING} + \text{DRIFT ANGLE}) - V_{\text{AIRSPEED}} \cos(\text{PITCH ATTITUDE} - \text{AOA}) \sin(\text{HEADING})$$

DATA BASE

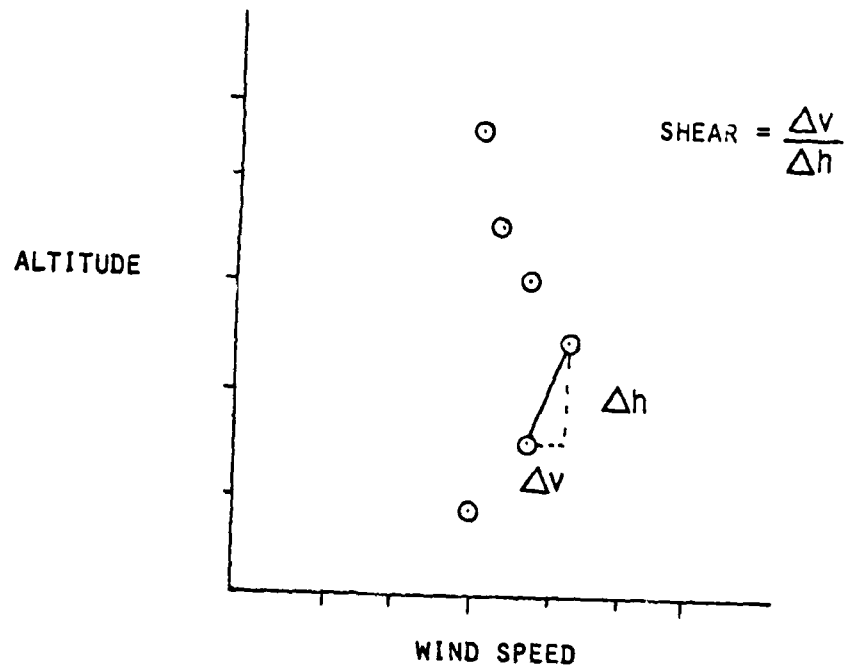
9 HOURS DATA

OVER 640 OPERATIONS (LANDINGS OR TAKEOFFS)

14 AIRPORTS

60% OF THE DATA OBTAINED AT LONDON, NEW YORK,  
ATLANTIC CITY, AND NEW JERSEY

WIND SHEAR



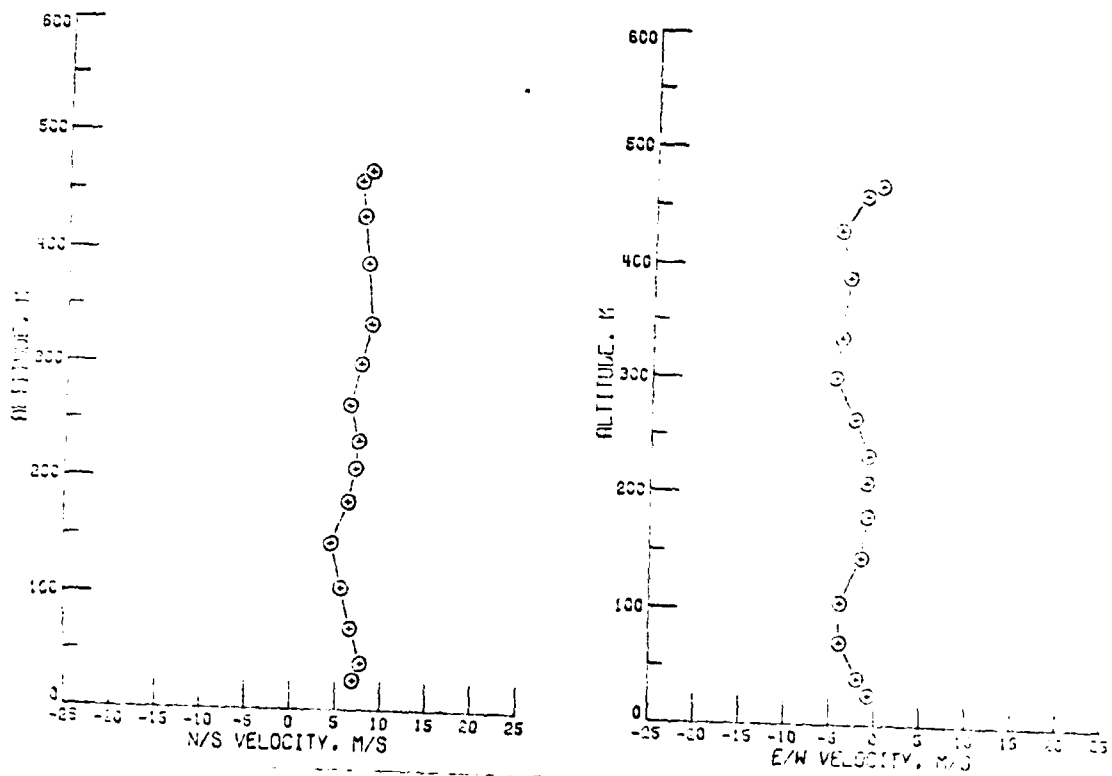


Figure 1.- Typical measurement of North/South and East/West wind components as a function of altitude for a take-off.

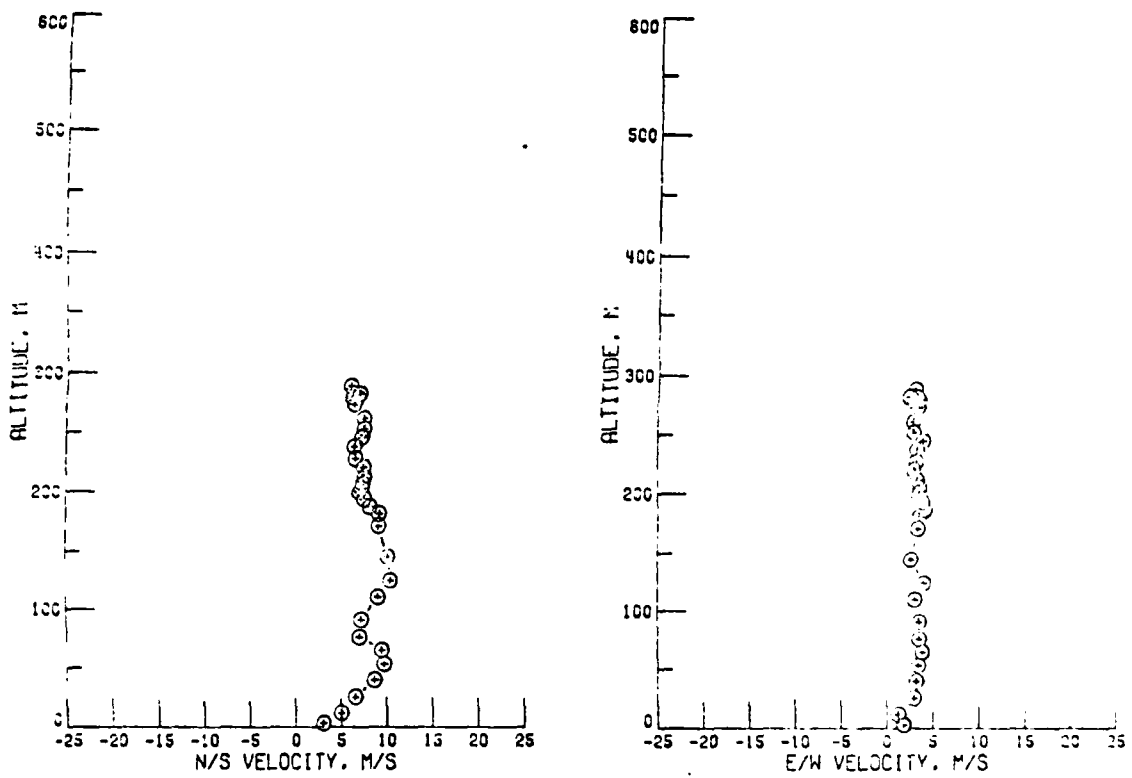


Figure 2.- Typical measurement of North/South and East/West wind components as a function of altitude for a landing.

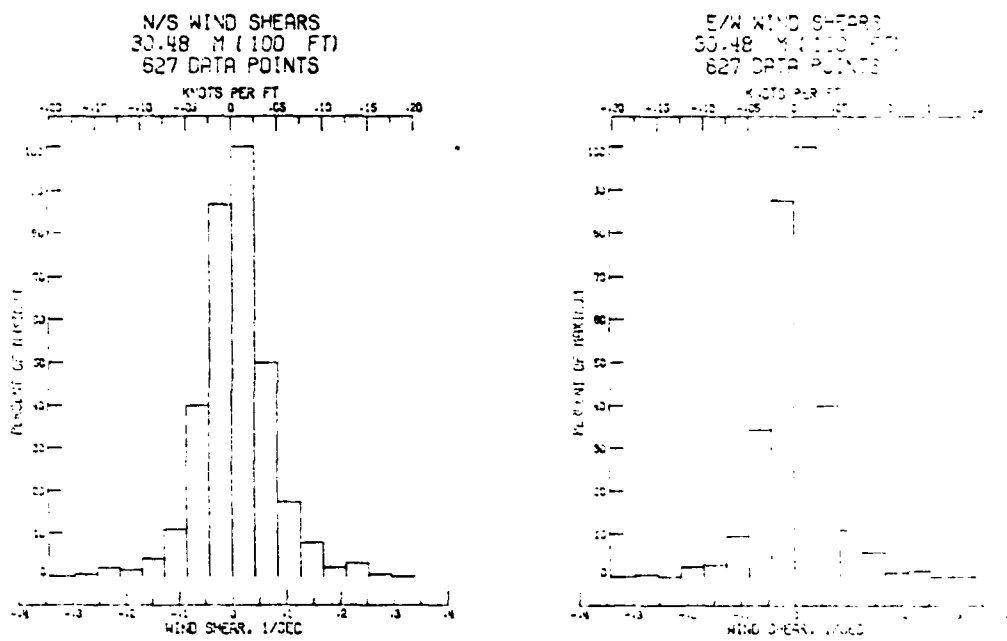


Figure 3.- Distribution of North/South and East/West wind shears in 100 ft (30.48m) altitude increments.

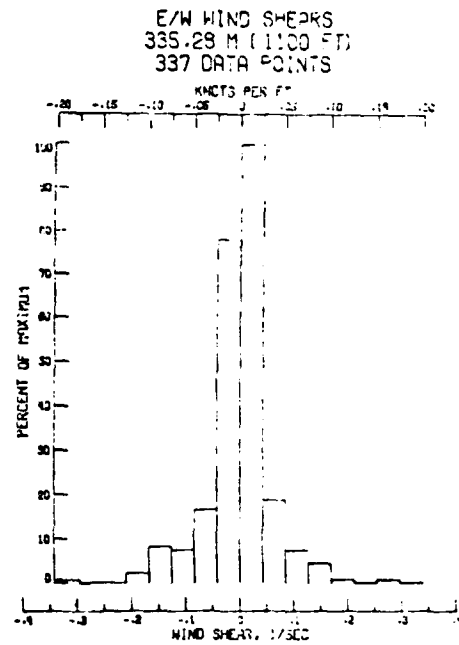
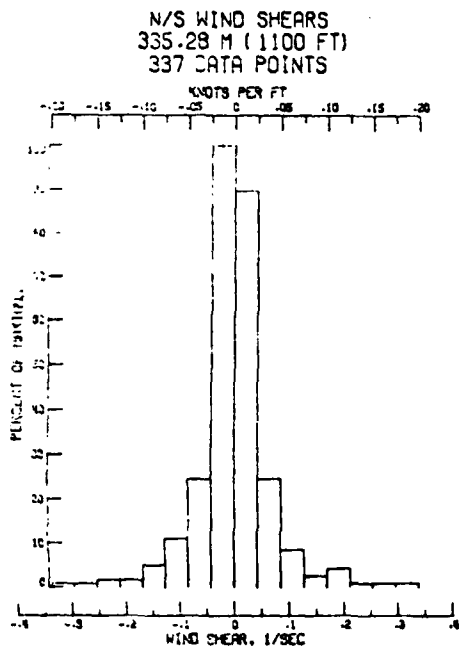
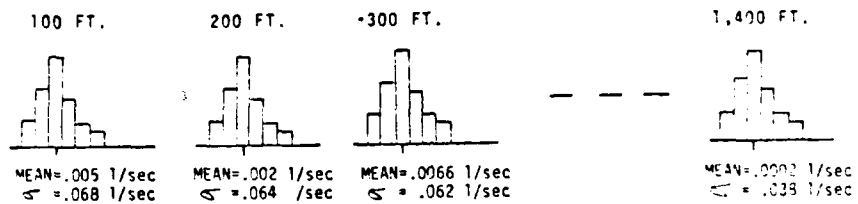


Figure 3.- Continued





- o FOR ALL ALTITUDES THE MEAN IS APPROXIMATELY 0, AND THE STANDARD DEVIATION IS .07 1/SEC (4.1 KNOTS/100 FT.)
- o FOR ALL ALTITUDES THE VARIATION IN THE STANDARD DEVIATION IS SMALL, APPROXIMATELY .008 1/SEC (.47 KNOTS/100 FT.)

### 6277 DATA POINTS

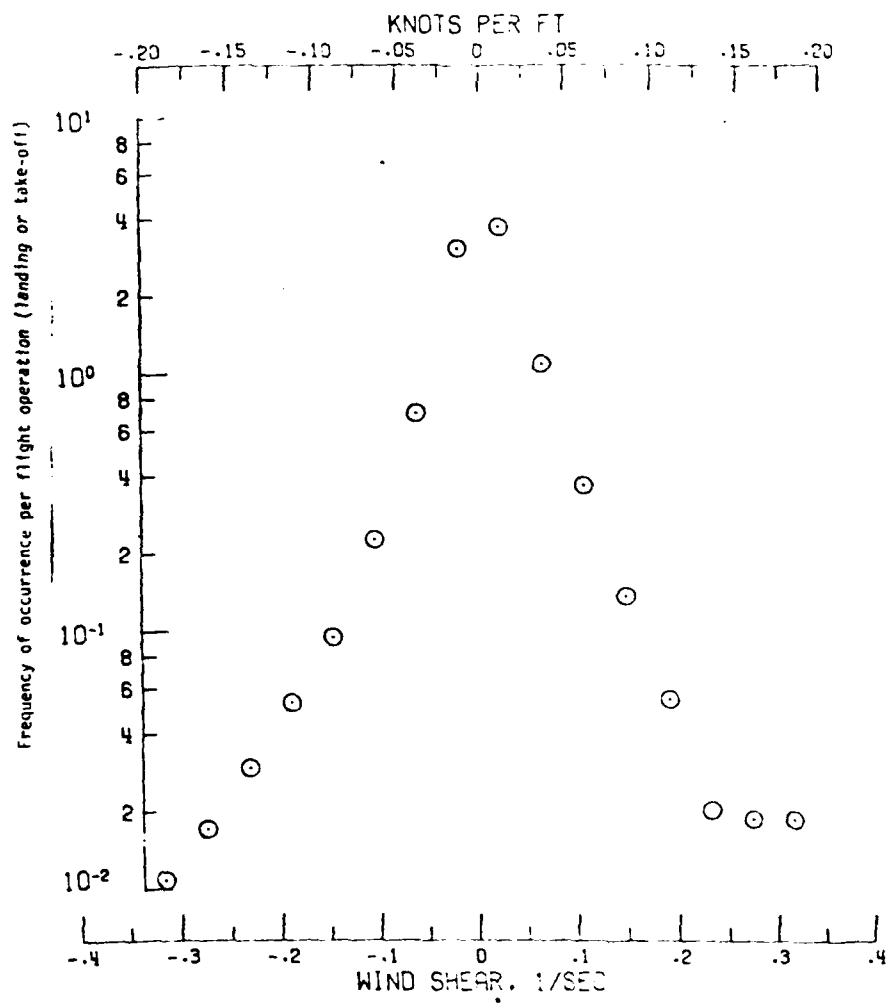


Figure 8.- Frequency of occurrence of wind shear per landing or take-off.

CONCLUDING REMARKS

- o AN EXTENSIVE DATA BASE COULD BE CONSTRUCTED FROM DATA PRESENTLY BEING RECORDED BY COMMERCIAL AIRPLANE OPERATORS
  
- o A GIVEN MAGNITUDE WIND SHEAR IS EQUALLY LIKELY TO OCCUR AT ANY ALTITUDE (LESS THAN 1,800 FEET)

APPENDIX 14 14-1

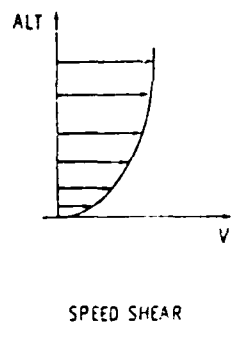
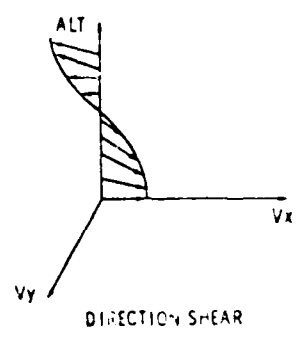
WIND HAZARD MODELS  
FOR  
PILOTED AIRCRAFT SIMULATIONS

ROLAND L. BOWLES  
ACD/ASB

### SIMULATION OF WIND SHEARS AND TURBULENCE

- WIND SHEAR DEFINITION (8TH. ICAO AIR NAV. CONF. 1974)  
"CHANGE IN WIND VECTOR IN A RELATIVELY SHORT AMOUNT OF SPACE"

#### DEFINITION OF WIND SHEAR



- FOR AVIATION PURPOSES WE ARE INTERESTED IN WIND VARIATION ALONG THE FLIGHT PATH OF AN AIRCRAFT.

### THE HAZARD

- WIND SHEARS AND DOWNDRAFTS ENCOUNTERED DURING TAKEOFF AND LANDING POSE SERIOUS AVIATION HAZARDS.



- FOR A SWEEPWING TRANSPORT A 5 KNOT DOWNDRAFT IS COMPARABLE IN SEVERITY TO A 5 KNOT PER HUNDRED FEET SHEAR.

- AIRCRAFT ACCIDENTS

- MAJOR FACTOR IN 39 PERCENT OF ALL FATAL AIRCRAFT ACCIDENTS BETWEEN 1964-1973 (FAA-RD-77-36)
- RECENT ACCIDENTS
  - IBERTIAN DC-10, DECEMBER 1973, LOGAN
  - CONTINENTAL 727, AUGUST 1975, DENVER
  - EASTERN 727, JUNE 1975, JFK
  - ALLEGHENY DC-9, JUNE 1976, PHILADELPHIA
  - SOUTHERN DC-9, APRIL 1977, NEW HOPE, GEORGIA

## THE EFFECT OF WIND SHEAR

- AIRCRAFT PHUGOID STABILITY ADVERSELY EFFECTED
- WIND SHEAR HAS LITTLE EFFECT ON SHORT PERIOD MOTION
- USE FULL PARAMETER FOR ANALYSIS

$$\sigma = \frac{VA}{g} \cdot \text{WIND GRADIENT}$$

TABLE II. - EFFECT OF POSITIVE AND NEGATIVE SHEAR  
ON PHUGOID MODE - BASIC AIRPLANE  
[ $\delta_F = 0.4363$  rad;  $\sigma_W = 0.0$ ]

| $\Gamma_0$<br>rad | $\sigma_u$ | Roots      |                 | $T_{1/2}$<br>sec | $T_{double}$<br>sec | $P$<br>sec | $\omega_p$<br>rad | $\zeta_p$ |
|-------------------|------------|------------|-----------------|------------------|---------------------|------------|-------------------|-----------|
| 0.0               | 0.0        | -0.002954  | $\pm 0.140281$  | 238.59           | -----               | 44.79      | 0.14031           | 0.021     |
| -0.05236          | .0         | -0.0052453 | $\pm 0.140501$  | 132.09           | -----               | 44.72      | .1406             | .037      |
|                   | -.5        | -0.0052994 | $\pm 0.171474$  | 130.77           | -----               | 36.64      | .1716             | .031      |
|                   | -1.0       | -0.0054139 | $\pm 0.197251$  | 128.00           | -----               | 31.85      | .1973             | .027      |
|                   | -1.5       | -0.0055879 | $\pm 0.219691$  | 124.02           | -----               | 28.60      | .2198             | .025      |
|                   | -2.0       | -0.0058200 | $\pm 0.239741$  | 119.07           | -----               | 26.21      | .2398             | .024      |
|                   | -2.5       | -0.0061076 | $\pm 0.25771$   | 113.47           | -----               | 24.36      | .2580             | .024      |
|                   | -3.0       | -0.0064496 | $\pm 0.274751$  | 107.45           | -----               | 22.87      | .2748             | .023      |
|                   | -3.5       | -0.0068442 | $\pm 0.290321$  | 101.25           | -----               | 21.64      | .2904             | .023      |
|                   | .5         | -0.0052567 | $\pm 0.0996191$ | 131.83           | -----               | 63.07      | .9962             | .00528    |
|                   | 1.0        | -0.012747  | .0020821        |                  | 332.84              | -----      | -----             | -----     |
|                   | 1.5        | -0.10647   | .095524         |                  | 7.25                | -----      | -----             | -----     |
|                   | 2.0        | -0.14893   | .13756          |                  | 5.04                | -----      | -----             | -----     |
|                   | 2.5        | -0.18207   | .17013          |                  | 4.07                | -----      | -----             | -----     |
|                   | 3.0        | -0.21051   | .19785          |                  | 3.50                | -----      | -----             | -----     |
|                   | 3.5        | -0.23600   | .22249          |                  | 3.11                | -----      | -----             | -----     |

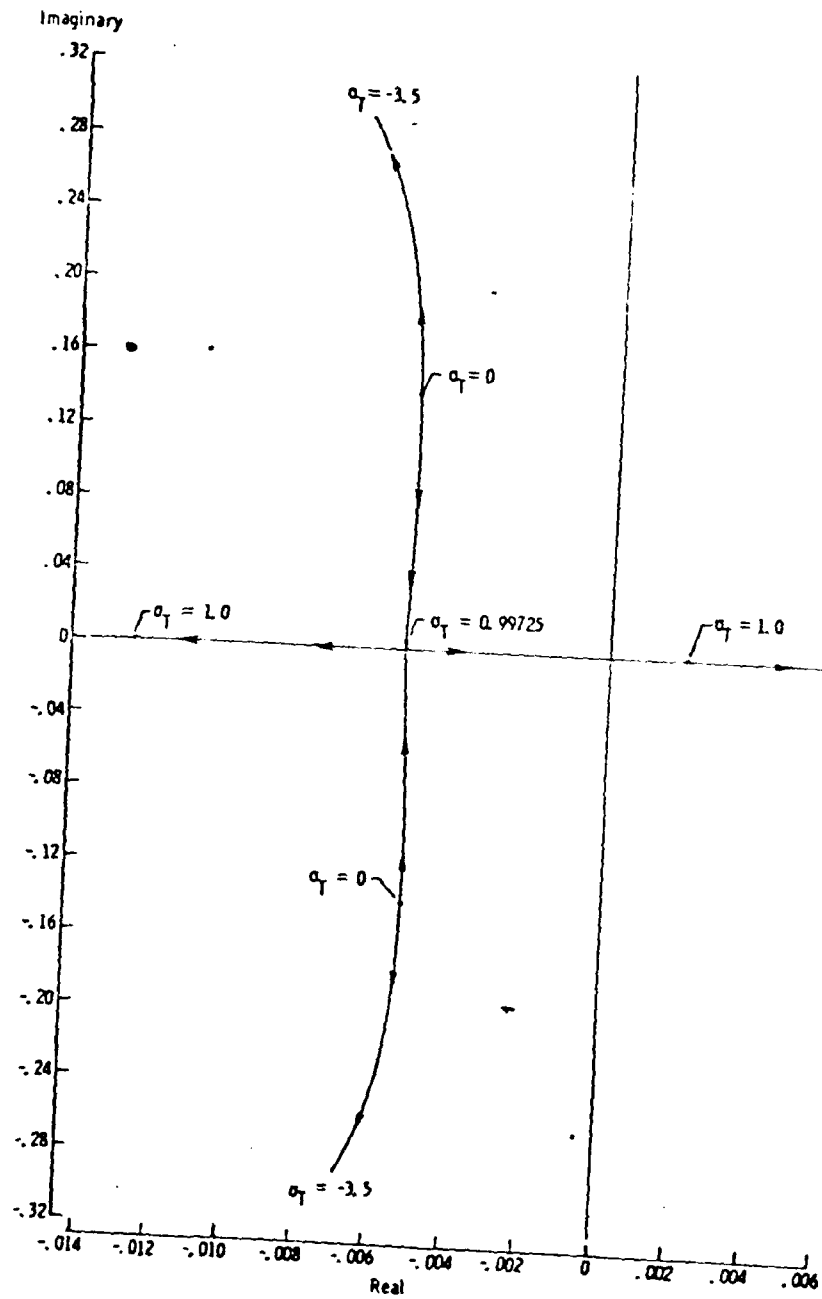
$\sigma > 0$  (DECREASING HEAD WIND) HW  $\longrightarrow$  TW

$\sigma < 0$  (DECREASING TAIL WIND) TW  $\longrightarrow$  HW

FOR TYPICAL JET TRANSPORT WITH APPROACH SPEED 120 KIAS

$$-4 \leq \sigma \leq 4$$





Root-locus plot for the phugoid mode  $\Gamma_0 = -0.05236$  radian;  
 $\sigma_W = 0$ ;  $\sigma_T = \sigma_U$ .

## ON-GOING PROGRAMS

- FAA WIND-HAZARD PROGRAM (FAA-ED-15-2)
  - WIND SHEAR CHARACTERIZATION
  - HAZARD DEFINITION
  - GROUND-BASED WIND SHEAR DETECTION SYSTEMS
  - AIRBORNE WIND SHEAR DETECTION EFFORTS
  - WIND SHEAR DATA MANAGEMENT
  - INTEGRATION OF WIND SHEAR SYSTEMS AND DATA INTO NATIONAL AIRSPACE SYSTEM (NAS)
- NASA TCV PROGRAM
  - AIRBORNE WIND SHEAR DEVELOPMENT EFFORTS
    - ENERGY SENSOR
    - ON-LINE SHEAR ESTIMATION AND CONTROL
    - DISPLAY OF WIND HAZARD IN COCKPIT

*PROPOSED FAA "STANDARD BENCH MARK"*

- FAA/SRI WIND HAZARD PACKAGE
    - 21 WIND HAZARD PROFILES REPRESENTING
      - NEUTRAL
      - NIGHTTIME STABLE
      - FRONTALS
      - THUNDERSTORMS
- } ATMOSPHERIC  
CONDITIONS
- EACH PROFILE COMPRISED OF THREE AXIS
    - MEAN WIND SPECIFICATIONS
    - TURBULENCE SPECIFICATIONS
- DRYDEN MODEL
- EACH PROFILE GIVEN AS A FUNCTION OF ALTITUDE AND RANGE FROM TOUCHDOWN

TABLE 1.- WIND PROFILES CROSS REFERENCE GUIDE

| Profile Label | Relative Wind Profile Severity | Source of Wind Data                  | Atmospheric Condition |
|---------------|--------------------------------|--------------------------------------|-----------------------|
|               | <u>Approach</u>                |                                      |                       |
| B1/D1         | Low                            | Meteorological math model            | Neutral               |
| B2            | Low                            | Meteorological math model            | Nighttime stable      |
| B3            | Low                            | Meteorological math model            | Nighttime stable      |
| B4            | Low                            | Tower measurements                   | Nighttime stable      |
| B5/D5         | Low                            | Logan accident reconstruction        | Warm front            |
| B6            | Low                            | Same as B5, rotated 40°              | Warm front            |
| B7/D7         | Moderate                       | Tower measurements                   | Thunderstorm          |
| B8/D8         | Moderate                       | Tower measurements                   | Thunderstorm          |
| D2            | Moderate                       | Tokyo accident reconstruction        | Warm front            |
| B9/D9         | Moderate                       | Tower measurements                   | Cold front            |
| B10           | Moderate                       | Philadelphia accident reconstruction | Thunderstorm          |
| B11           | Moderate                       | Kennedy accident reconstruction      | Thunderstorm          |
| B12/D6        | High                           | Kennedy accident reconstruction      | Thunderstorm          |
| D10           | High                           | Kennedy accident reconstruction      | Thunderstorm          |
| D4            | High                           | Philadelphia accident reconstruction | Thunderstorm          |
| D3            | High                           | Mathematical model                   | Thunderstorm          |
|               | <u>Takeoff<sup>e</sup></u>     |                                      |                       |
| D15           | Low                            | Tower measurements                   | Cold front            |
| D12           | Moderate                       | Philadelphia accident reconstruction | Thunderstorm          |
| D14           | Moderate                       | Philadelphia accident reconstruction | Thunderstorm          |
| D11           | High                           | Kennedy accident reconstruction      | Thunderstorm          |
| D13           | High                           | Philadelphia accident reconstruction | Thunderstorm          |

TABLE 2.- TURBULENCE SPECIFICATIONS FOR PROFILE D10  
(Kennedy/Eastern 66 Accident Reconstruction)

| Altitude (meters) | Longitudinal Scale Length (meters) | Lateral Scale Length (meters) | Vertical Scale Length (meters) | Longitudinal RMS (knots) | Lateral RMS (knots) | Vertical RMS (knots) |
|-------------------|------------------------------------|-------------------------------|--------------------------------|--------------------------|---------------------|----------------------|
| 6.10              | 32.23                              | 15.15                         | 3.17                           | 3.40                     | 2.70                | 2.34                 |
| 30.49             | 66.07                              | 40.91                         | 16.16                          | 4.05                     | 3.46                | 3.53                 |
| 60.98             | 93.45                              | 65.09                         | 32.32                          | 4.43                     | 3.95                | 4.35                 |
| 121.95            | 132.16                             | 103.54                        | 64.63                          | 4.85                     | 4.50                | 5.36                 |
| 182.93            | 161.86                             | 135.85                        | 96.95                          | 5.11                     | 4.86                | 6.05                 |
| 457.32            | 256.37                             | 251.37                        | 242.47                         | 5.74                     | 5.78                | 7.94                 |

TABLE I: WIND PROFILES CROSS REFERENCE GUIDE

| Profile Label | Relative Severity |          |      | Flight Experiment |         | Atmospheric Condition |
|---------------|-------------------|----------|------|-------------------|---------|-----------------------|
|               | Low               | Moderate | High | Landing           | Takeoff |                       |
| B1            | X                 |          |      | X                 |         | Neutral               |
| B2            | X                 |          |      | X                 |         | Nighttime Stable      |
| B3            | X                 |          |      | X                 |         | Nighttime Stable      |
| B4            | X                 |          |      | X                 |         | Nighttime Stable      |
| B5            |                   | X        |      | X                 |         | Frontal               |
| B6            |                   | X        |      | X                 |         | Frontal               |
| B7            |                   | X        |      | X                 |         | Thunderstorm          |
| B8            |                   | X        |      | X                 |         | Thunderstorm          |
| B9            |                   |          | X    | X                 |         | Frontal               |
| B10           |                   |          | X    | X                 |         | Thunderstorm          |
| B11           |                   |          | X    | X                 |         | Thunderstorm          |
| B12           |                   |          | X    | X                 |         | Thunderstorm          |
| D2            |                   | X        |      | X                 |         | Frontal               |
| D3            |                   |          | X    | X                 |         |                       |
| D4            |                   |          | X    | X                 |         | Thunderstorm          |
| D10           |                   |          | X    | X                 |         | Thunderstorm          |
| D11           |                   |          | X    |                   | X       |                       |
| D12           |                   | X        |      |                   | X       |                       |
| D13           |                   |          | X    |                   | X       |                       |
| D14           |                   | X        |      |                   | X       |                       |
| D15           | X                 |          |      |                   | X       |                       |

COMPARISON OF WIND HAZARD SPECIFICATIONS

|                            | <u>FAA AC 20-57A</u>                        | <u>FAA/SRI PACKAGE</u>                                     |
|----------------------------|---|--|
| LONGITUDINAL<br>TURBULENCE | $L_U = 600$ FEET<br>$\sigma_U = 0.15$ KNOTS | $L_U = 65$ TO 80,000 FEET<br>$\sigma_U =$ UP TO 7.93 KNOTS |
| LATERAL<br>TURBULENCE      | $L_V = 600$ FEET<br>$\sigma_V = 0.15$ KNOTS | $L_V = 49$ TO 80,000 FEET<br>$\sigma_V =$ UP TO 7.93 KNOTS |
| VERTICAL<br>TURBULENCE     | $L_W = 30$ FEET<br>$\sigma_W = 1.5$ KNOTS   | $L_W = 10$ TO 795 FEET<br>$\sigma_W =$ UP TO 7.94 KNOTS    |
| MEAN WINDS                 |   |  |
| LONGITUDINAL               | HW-25 KNOTS, TW-10 KNOTS                    | HW-53 KNOTS, TW-79 KNOTS                                   |
| LATERAL                    | CW-15 KNOTS                                 | CW-65 KNOTS  |
| VERTICAL                   | NOT GIVEN                                   | UD-10 KNOTS, DD-31 KNOTS                                   |
| WIND SHEARS                |   |  |
| LONGITUDINAL               | 8 KNOTS/100 FEET                            | 50 KNOTS/100 FEET  |
| LATERAL                    | FROM 200 FEET                               | 17 KNOTS/100 FEET  |
| VERTICAL                   | TO TOUCHDOWN                                | 20 KNOTS/100 FEET  |

RESULTS OF TCV SIMULATION FLOWN AGAINST  
WIND HAZARD PACKAGE

- MODE OF OPERATION
  - FULL NONLINEAR SIMULATION
  - STRAIGHT-IN APPROACH ( $\approx$  6 MILES OUT)
  - INITIAL TRIM WITH WINDS PRESENT
  - AUTOLAND ENGAGED
  - AUTOTHROTTLE ENGAGED
  - AUTOTHROTTLE INCLUDES A WIND SHEAR DETECTOR  
(PRESENT STATE OF THE ART)
  
- SIMULATION FLOWN AGAINST ALL 21 PROFILES
  
- TOUCHDOWN FOOTPRINT
  
- ACCEPTABILITY CRITERIA
  
- ACCEPTABILITY RESULTS

| TEST CASE | TECHNOLOGY CRITERIA |                 |                 |                 |                |                 |                 |                 |                 | COMMENTS                                    |
|-----------|---------------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|-----------------|---|
|           | X <sub>TD</sub>     | U <sub>TD</sub> | a <sub>TD</sub> | U <sub>TD</sub> | C <sub>L</sub> | Y <sub>TD</sub> | Y <sub>TD</sub> | β <sub>TD</sub> | σ <sub>TD</sub> |   |
| B1        |                     |                 |                 |                 | N/A            |                 |                 |                 |                 |   |
| B2        |                     |                 |                 |                 | ↑              |                 |                 |                 |                 |   |
| B3        |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B4        |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B5        |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B6        |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B7        |                     |                 |                 | X               |                |                 |                 |                 |                 |   |
| B8        | X                   |                 |                 | X               |                |                 |                 |                 |                 | LONG, >1.3 U <sub>STALL</sub>               |
| B9        |                     | X               | X               | X               |                |                 |                 |                 |                 | BOUNCE, AUTO THROTTLE PROBLEM               |
| B10       |                     |                 |                 | X               |                |                 |                 |                 |                 | <1.0 U <sub>STALL</sub>                     |
| B11       |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B12       |                     |                 |                 | X               |                |                 |                 |                 |                 |   |
| B2        |                     |                 |                 |                 |                |                 | X               |                 |                 |   |
| B3        | X                   | X               | X               |                 |                |                 |                 |                 |                 | CRASH SHORT OF RW                           |
| B4        | X                   | X               | X               | X               |                |                 |                 |                 | X               | CRASH SHORT OF RW, STALL                    |
| B10       | X                   | X               | X               | X               |                |                 | X               |                 | X               | CRASH SHORT OF RW                           |
| B11       |                     |                 |                 |                 |                |                 |                 |                 |                 |   |
| B12       | X                   |                 |                 | X               |                |                 |                 |                 |                 | LONG, >1.3 U <sub>STALL</sub>               |
| B13       |                     |                 |                 | X               |                |                 |                 |                 | X               | >1.3 U <sub>STALL</sub> , EXCESSIVE ROLLING |
| B14       | X                   |                 |                 | X               |                |                 |                 |                 |                 | LONG, >1.3 U <sub>STALL</sub>               |
| B15       |                     |                 |                 |                 | ↓              |                 |                 |                 |                 | N/A   |

x - DENOTES UNACCEPTABLE PERFORMANCE  
 N/A - DENOTES DATA NOT AVAILABLE

100 KT. CASE



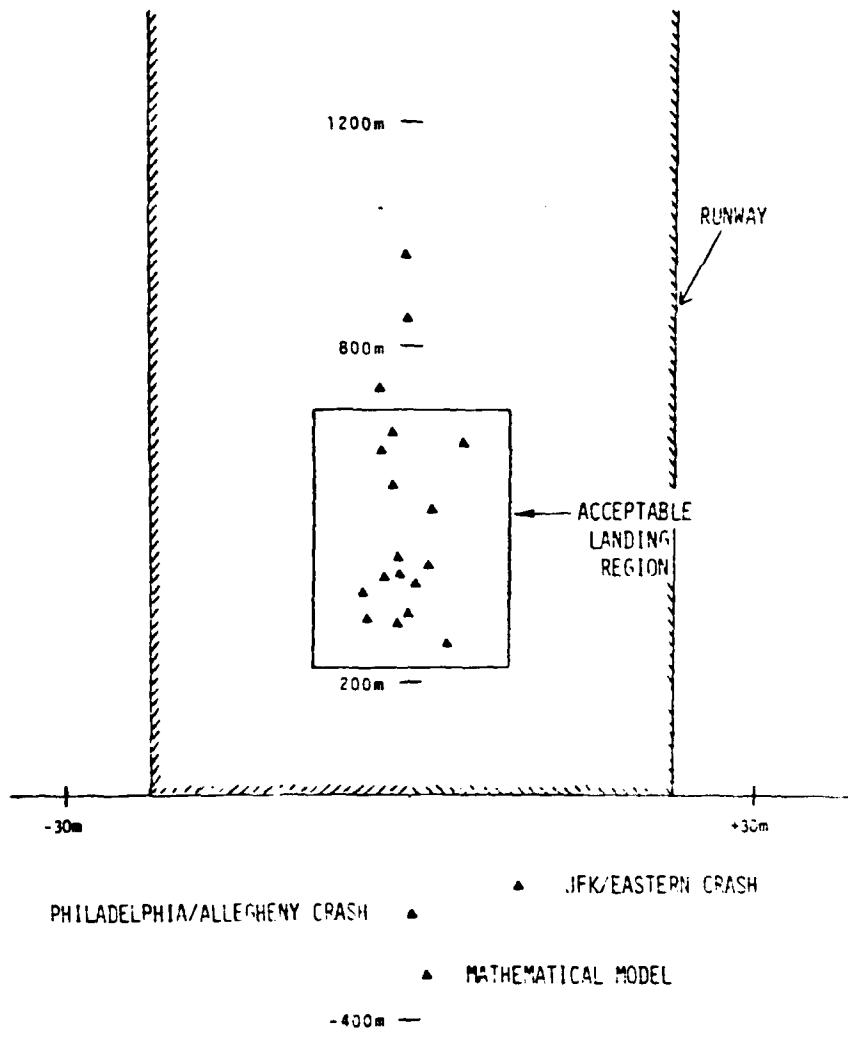


Figure 4.- Touchdown footprint for autolands vs. all profiles (IAS-120 kts).

TABLE 5. - TOUCHDOWN RESULTS FOR PILOTED RUNS

| Profile Label | Touchdown Criteria |                |               |          |       |               |               |              |             |
|---------------|--------------------|----------------|---------------|----------|-------|---------------|---------------|--------------|-------------|
|               | $x_{TD}$           | $h_{TD}$       | $\theta_{TD}$ | $u_{TD}$ | $C_L$ | $\gamma_{TD}$ | $\delta_{TD}$ | $\beta_{TD}$ | $\psi_{TD}$ |
| D1            | 2                  | 1              |               | 3        |       | 1,2,3         |               |              |             |
| D2            | 3                  | 1,3            |               |          |       | 2             |               |              |             |
| D3            |                    |                | 2             | 1,2      |       | 1             |               |              |             |
| D4            | 1,2,3              | 1,2,3          | 3             | 3        |       | 1             |               |              |             |
| D5            |                    |                | 2             | 1        | 2     |               |               |              |             |
| D6            | 3                  |                |               | 1        |       | 1             |               |              |             |
| D7            | 3                  |                |               | 3        |       | 1,2           |               |              |             |
| D8            |                    | 3              | 2             | 1,2,3    |       | 1             |               |              |             |
| D9            | 1                  | 1 <sup>a</sup> |               |          |       | 1,2           |               |              |             |
| D10           | 1,2 <sup>b</sup>   | 1              | 2             | 1,2,3    |       | 2             |               |              |             |

a - Touchdown hard enough to cause structural damage  
b - Crash short of runway  
1 - Pilot number 1, unacceptable performance  
2 - Pilot number 2, unacceptable performance  
3 - Pilot number 3, unacceptable performance

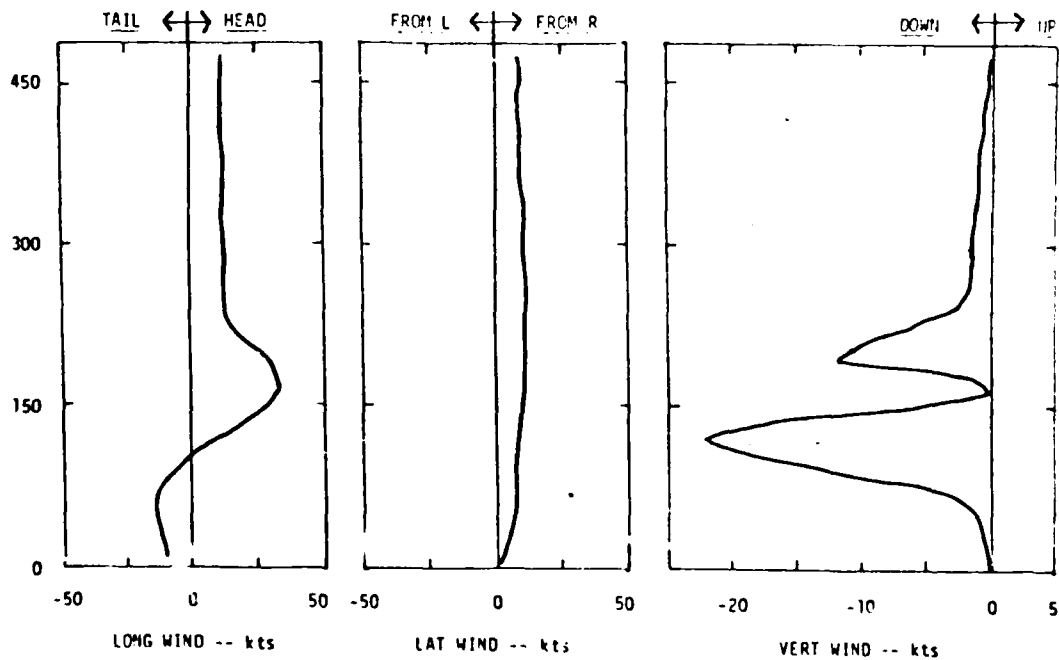


Figure 1. - Mean winds for profile D10, thunderstorm, similar to Kennedy/Eastern accident.

## CONCLUSIONS

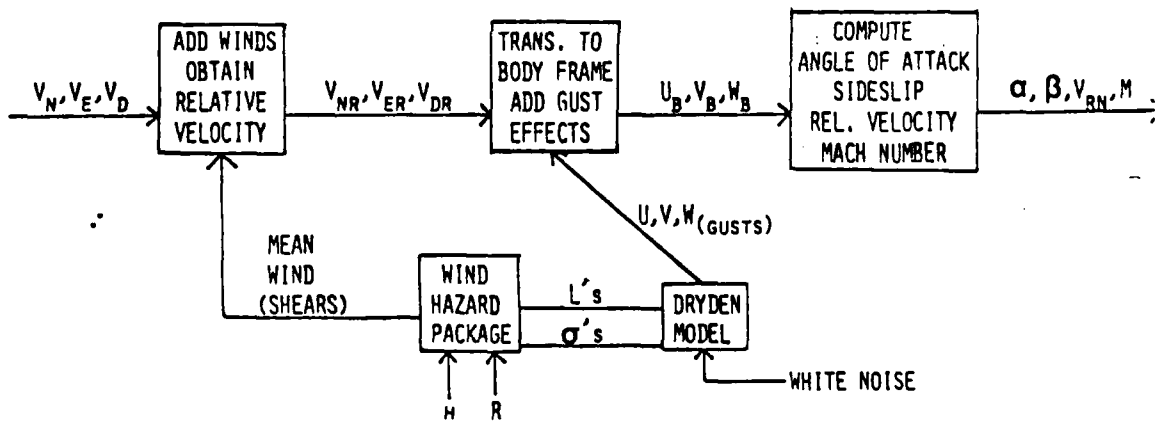
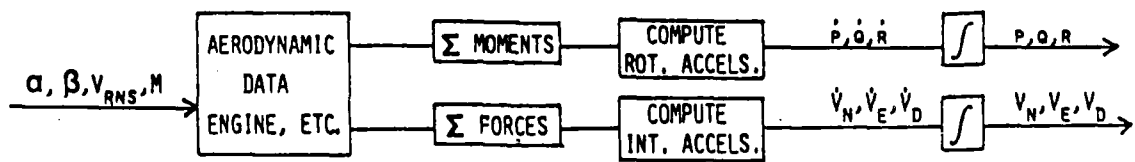
- CRASHES WILL OCCUR WITH PRESENT SYSTEM
- PILOTS COMMENTED THEY HAD NOT ENCOUNTERED SHEARS OF THESE MAGNITUDES IN ACTUAL FLIGHT
- MAGNITUDES OF TURBULENCE WERE SO GREAT THAT THEY WOULD HAVE INITIATED "GO AROUND" PRIOR TO ANY SHEAR PENETRATION
- RESPONSE OF THE AIRCRAFT TO TURBULENCE SEEMED UNREALISTIC. THIS COULD BE TO:
  - INCREASED VISUAL RESOLUTION OF ELECTRONIC DISPLAYS
  - LARGE MAGNITUDES OF TURBULENCE COMPONENTS
  - IMPROPER TURBULENCE MODEL OR IMPLEMENTATION

CONCERNS

- VALIDITY OF IMPLEMENTATION AND MODELING OF ATMOSPHERICS
- PROBLEMS WITH STANDARDIZATION BASED ON DISCUSSIONS WITH SRI, FAA, UAL, BOEING, DOUGLAS, SINGER-LINK AND SAFEFLIGHT
  - INCONSISTENCIES WITH PLACEMENT OF WINDSHEAR/TURBULENCE INTO EQUATIONS OF MOTION
  - CHARACTER AND IMPLEMENTATION OF TURBULENCE MODELS
  - INCLUSION OF SPAN AND AREA AVERAGING FILTERS (FAA ADVISORY CIRCULAR 20-57A)
  - UNSTEADY LIFT EFFECTS AS CONTRASTED TO LUMPED-PARAMETER (QUASI-STEADY) AERO MODELS

RECOMMENDATIONS

- SIMULATION COMMUNITY DRIVE TOWARD STANDARDS  
AS REGARDS
  - WIND HAZARDS DATA BASE
  - MODELS
  - IMPLEMENTATION TECHNIQUES
- LARC SEVERE ~~STORMS~~<sup>STORMS</sup> PROGRAM
  - NEW DATA BASE
  - IMPROVED MODELING OPPORTUNITIES
- FAA ROLE



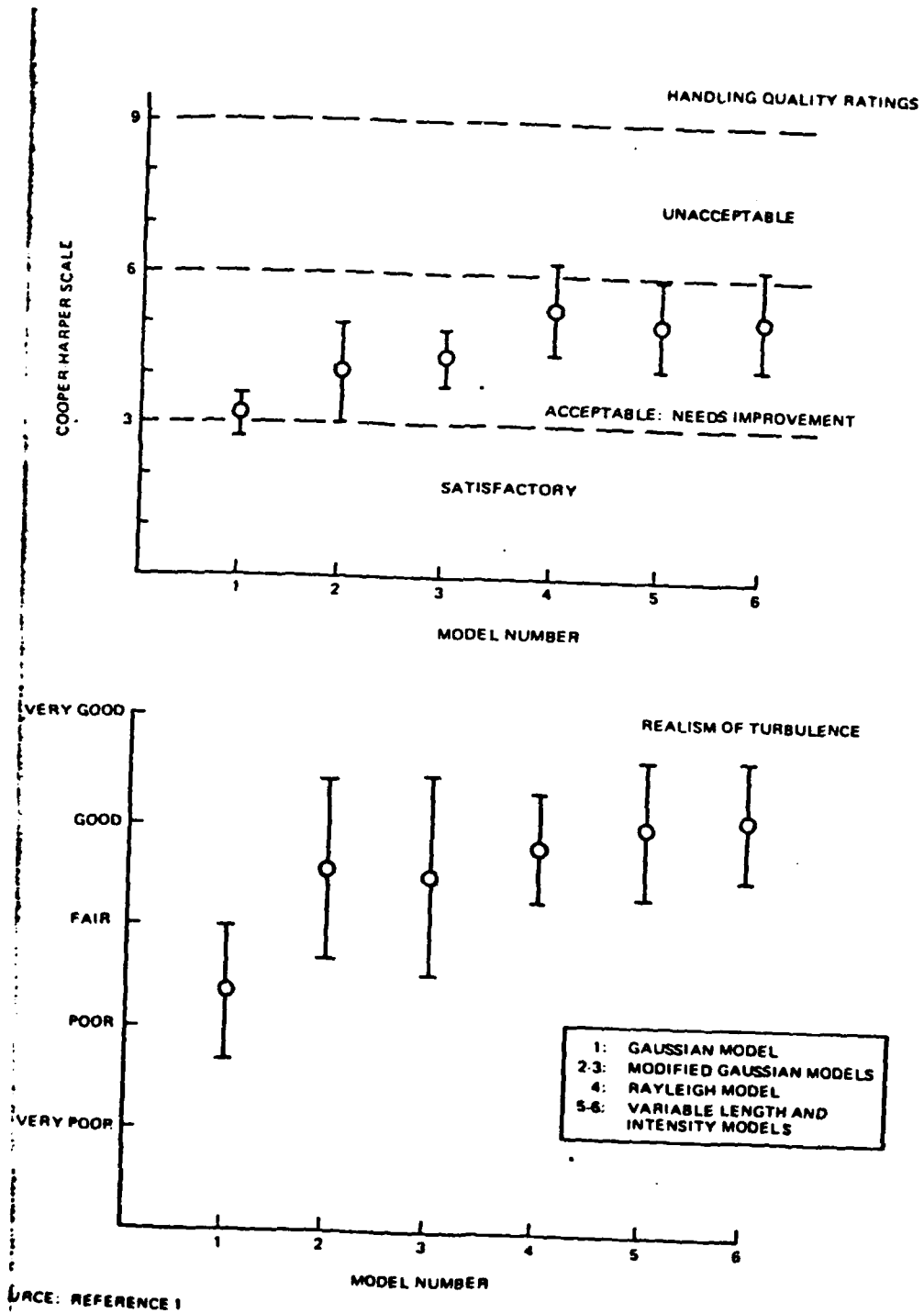


FIGURE 5. PILOT OPINION RATINGS

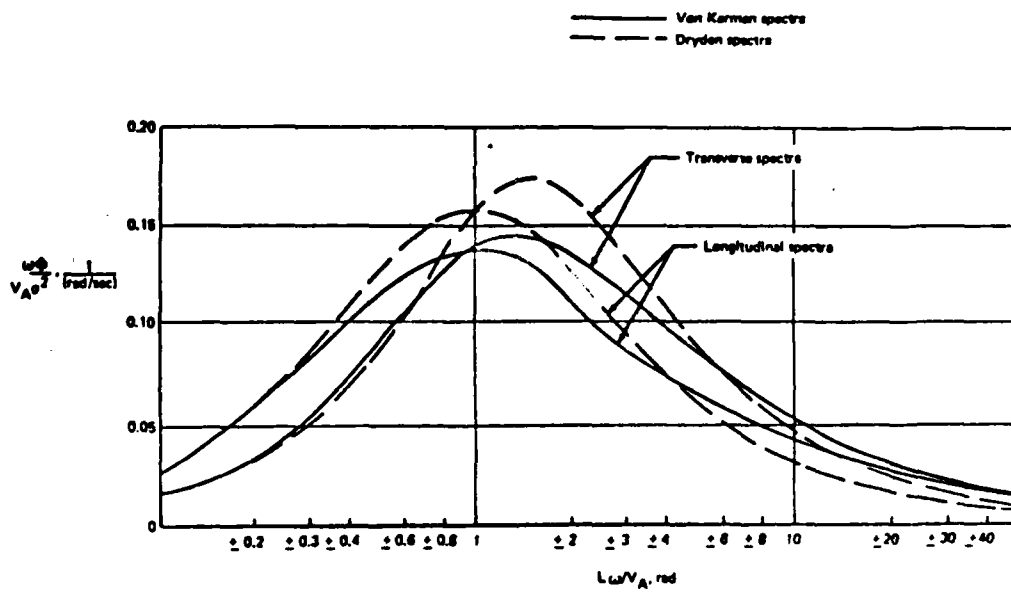


FIGURE 19 — COMPARISON: DRYDEN AND VON KARMAN VARIANCE DENSITY



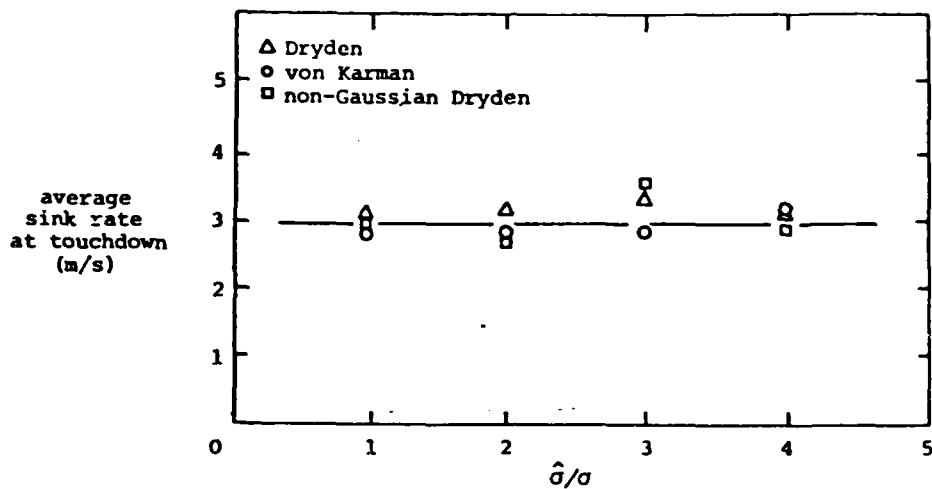


Figure 5-7. The average sink rate for different turbulence models ( $u_* = 0.5$ ,  $z_0 = 0.1$ ).

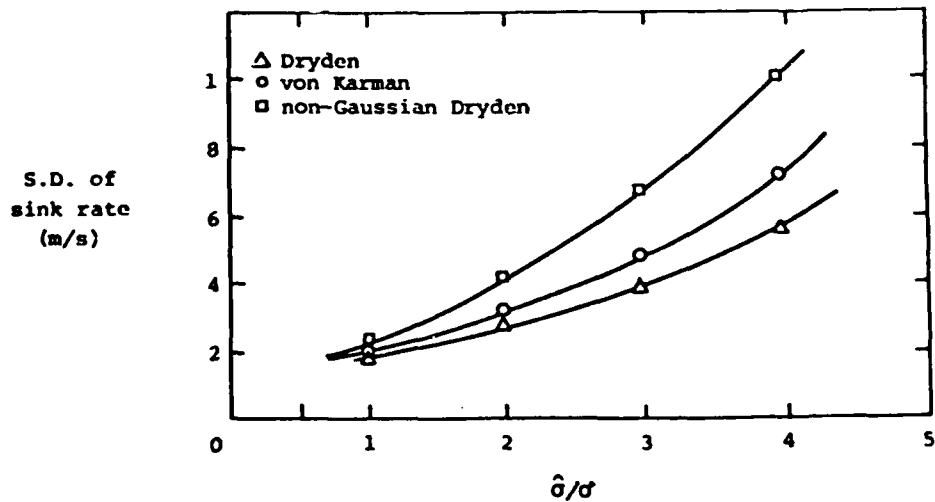


Figure 5-8. The standard deviation of sink rate for different turbulence models ( $u_* = 0.5$ ,  $z_0 = 0.1$ ).

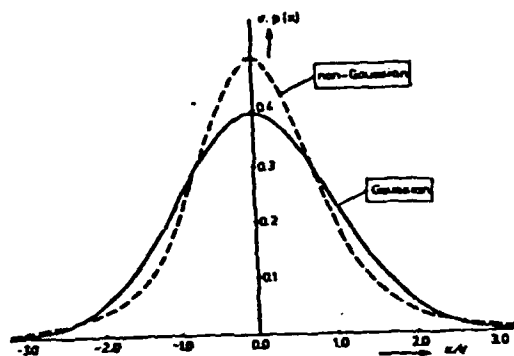


Fig. 1. The Gaussian - and a possible non-Gaussian distribution function.

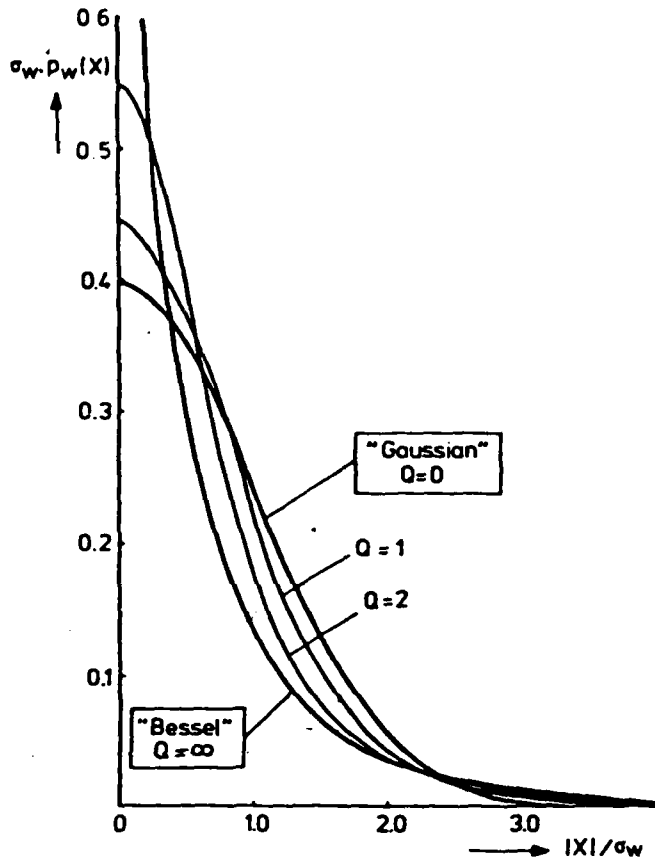


Fig. 4. Normalized probability density functions of  $w(t)$  for various values of  $Q$ .

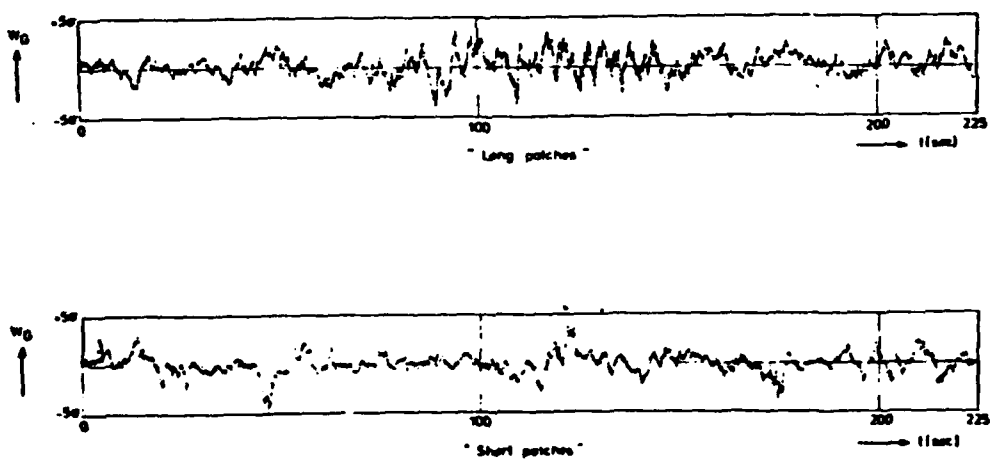


Fig. 5. Two non-gaussian turbulence records with the same fourth order moment setting but different "average patchlength".

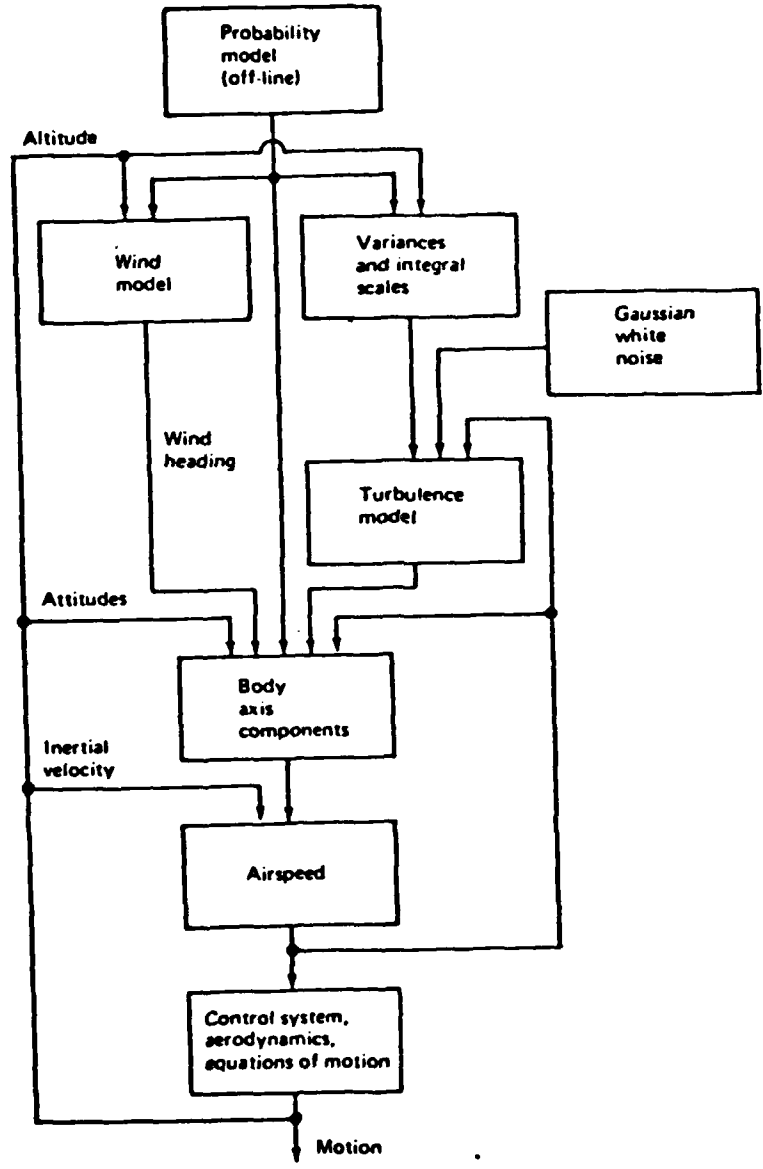


FIGURE 30 -COMPUTATION FLOW DIAGRAM

14-26

"THE ANSWER MY FRIEND IS BLOWING IN THE WIND . . ."

BOB DYLAN

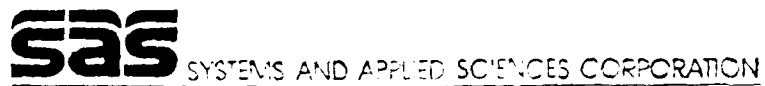
160.

CLEAR AIR TURBULENCE  
M. L. Kaplan (SASC)

OVERVIEW

- 1) MESOSCALE ATMOSPHERIC SIMULATION SYSTEM  
(M.A.S.S.)
- 2) DC-10 ACCIDENT/APRIL 3, 1981 WEATHER SITUATION
- 3) MODEL SIMULATION RESULTS
- 4) M.A.S.S. POTENTIAL UTILITY FOR C.A.T.,  
WIND SHEAR, AND TURBULENCE HAZARDS FORECASTING

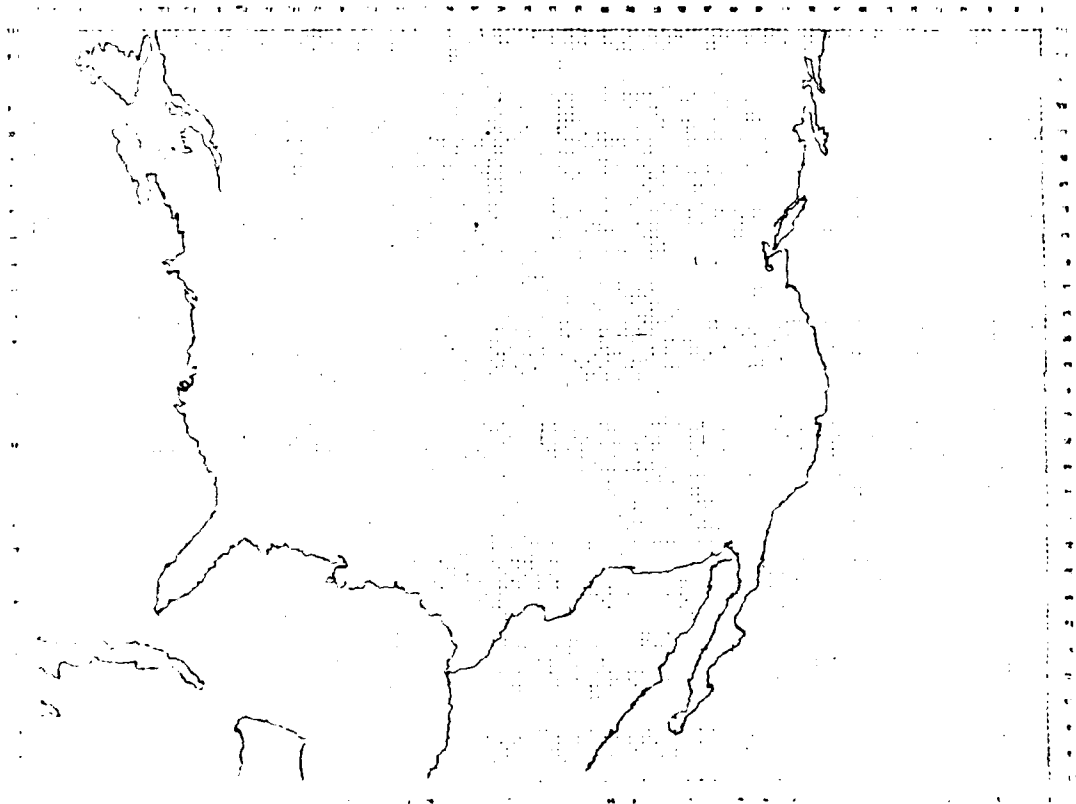
1) MESOSCALE ATMOSPHERIC SIMULATION SYSTEM  
(M.A.S.S.)



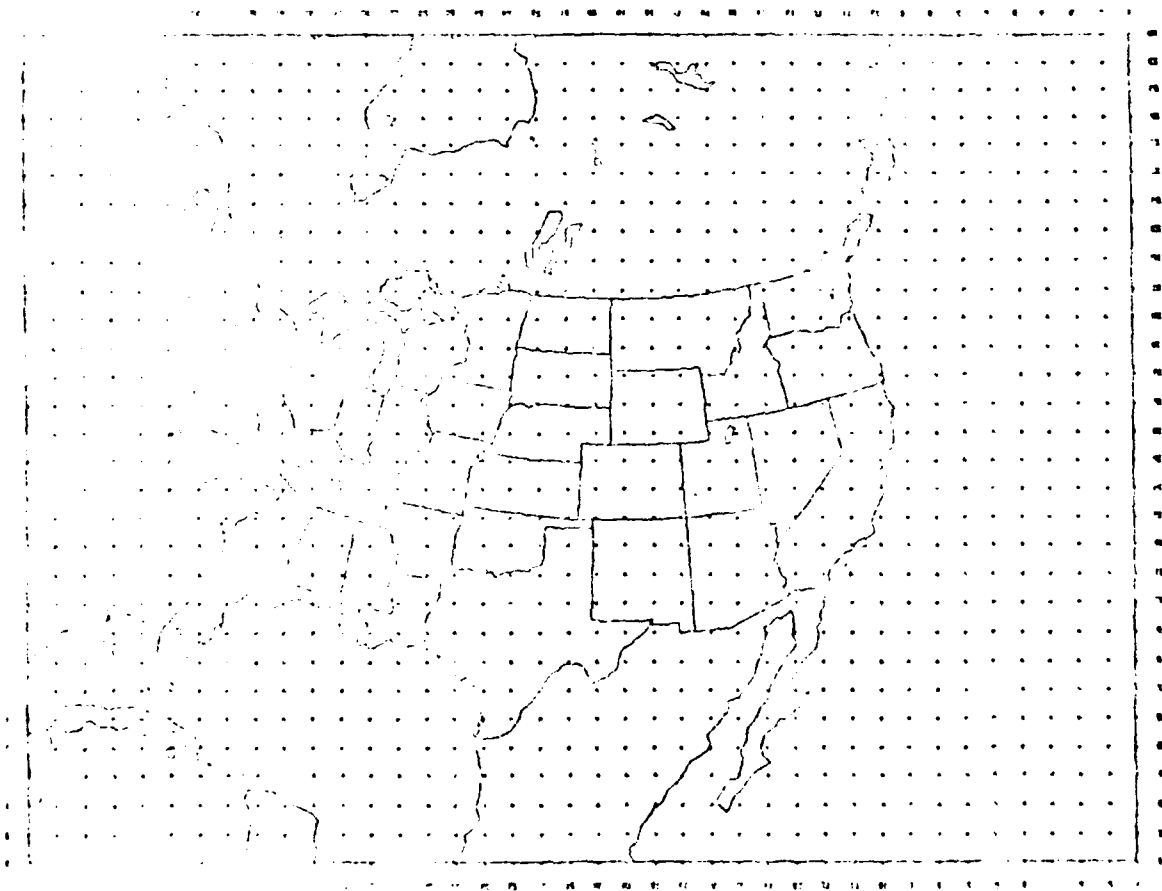
MESOSCALE ATMOSPHERIC SIMULATION SYSTEM

- \* 48 KM MESOSCALE MODEL
- \* SIXTH ORDER SPACE DIFFERENCING
- \* PREDICTOR-CORRECTOR TIME MARCHING
- \* 14 VERTICAL LAYERS IN A SIGMA COORDINATE
- \* 157 X 117 HORIZONTAL MATRIX
- \* PBL PARAMETERIZATION BASED ON SIMILARITY THEORY
- \* SURFACE ENERGY BUDGET
- \* DRY CONVECTIVE ADJUSTMENT
- \* STABLE LATENT HEATING
- \* CUMULUS PARAMETERIZATION UNDER DEVELOPMENT
- \* 24 HOUR SIMULATION IN 90 MINUTES ON CYBER 203
- \* CAPABILITY OF RESOLUTION TO 24, 12 AND 6 KM
- \* NON-LINEAR TYPICAL MODE DEVELOPMENT UNDER DEVELOPMENT





"Horizontal grid for MASS model"



"Horizontal grid used in routine operational simulation model"

M. A. S. S. APPLICATIONSI STRATOSPHERIC-TROPOSPHERE INTERACTIONS

- 1) JET STREAM TRAJECTORIES FOR AVIATION AND OZONE
- 2) MASS BUDGET CALCULATION NEAR TROPOPAUSE
- 3) OZONE BALANCE NEAR TROPOPAUSE

II POLLUTANT TRANSPORT

- 1) BOUNDARY LAYER TRANSPORT OF CONSTITUENTS
- 2) MIXING DEPTH ESTIMATION FROM BOUNDARY LAYER HEIGHT SIMULATION
- 3) EFFECT OF POLLUTANTS ON RADIATION BALANCE

III SATELLITE DATA

- 1) THOMS OZONE GRADIENTS FOR MODEL INITIALIZATION AND VERIFICATION
- 2) VAS AND NIMBUS FOR BETTER TEMPERATURE AND MOISTURE INITIALIZATION AND VERIFICATION
- 3) CLOUD STEREO WINDS FOR BETTER WIND INITIALIZATION AND VERIFICATION

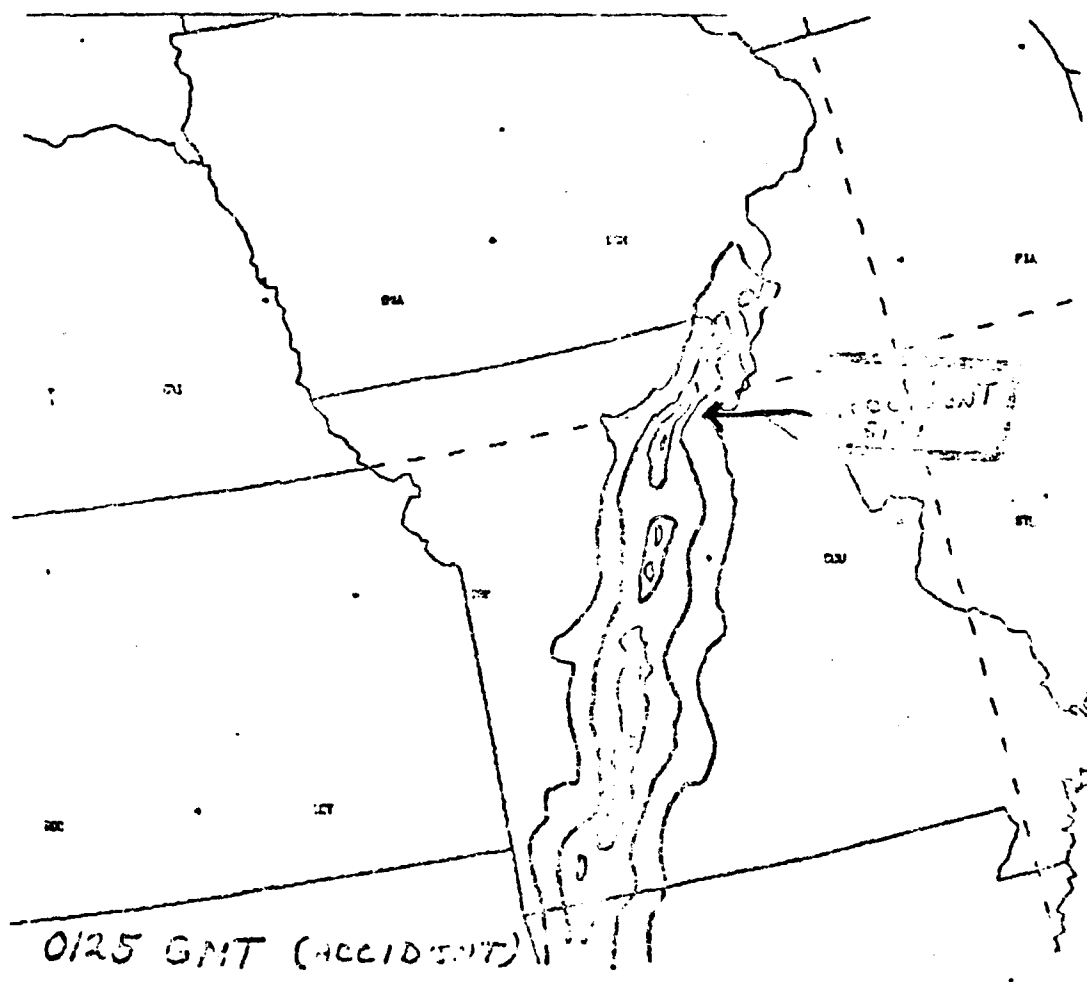
IV HEAVY PRECIPITATION

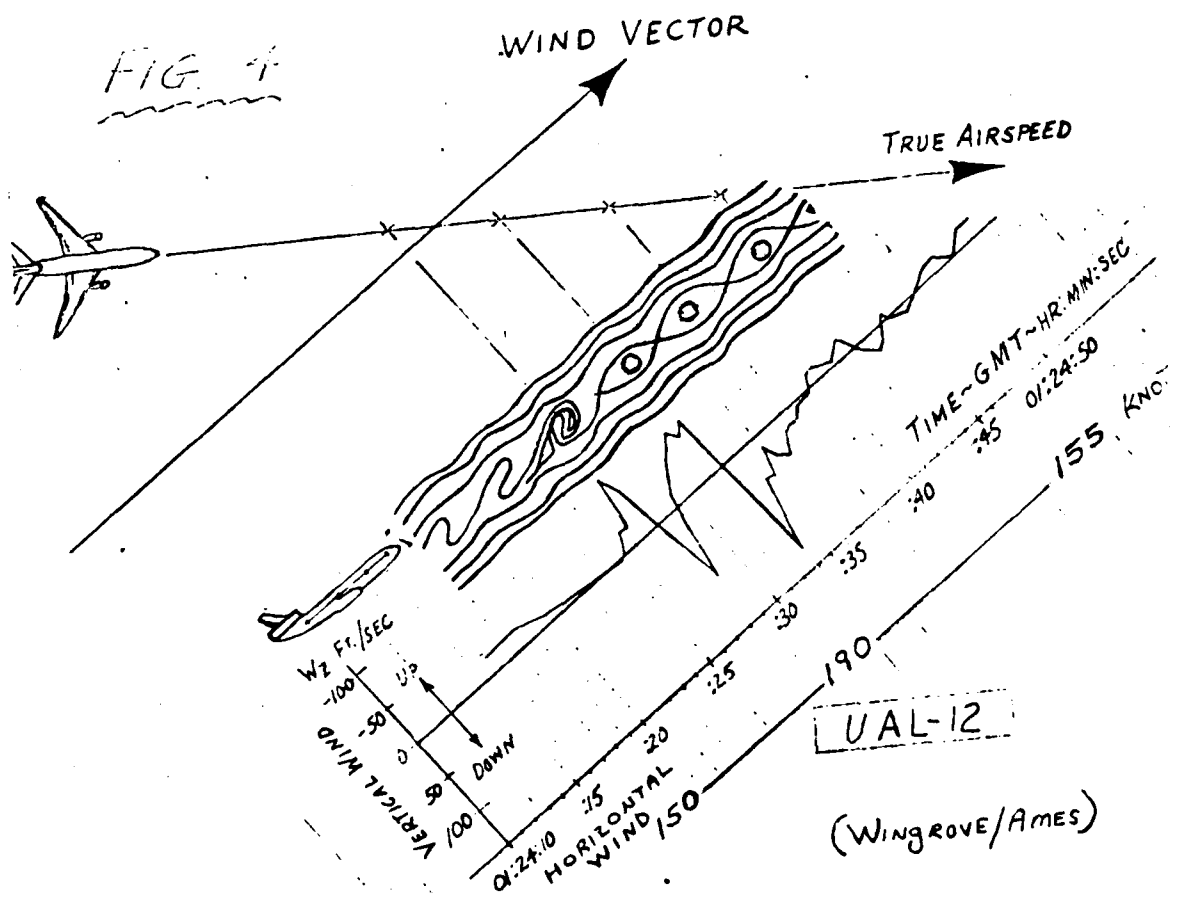
- 1) FLASH FLOOD/BETTER QUANTITATIVE PRECIPITATION FORECASTING
- 2) SHUTTLE/ACID RAIN PROBLEM
- 3) AIRCRAFT ICING PROBLEMS

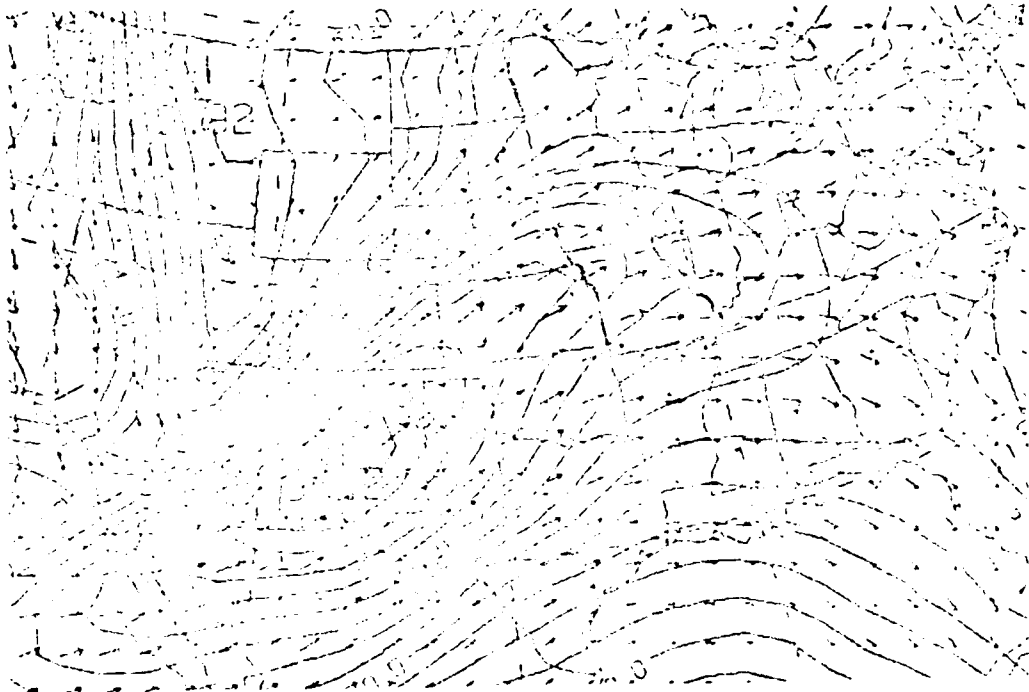
M. A. S. S. APPLICATIONS (CONTINUED)V SEVERE STORMS

- 1) CYCLOGENESIS
- 2) SEVERE STORMS AND TORNADOES
- 3) SHUTTLE LIFT-OFF AND RETURN ENVIRNMENTS
- 4) CONVECTIVE MIXING OF OZONE OR OTHER CONSTITUENTS
- 5) TROPICAL EXTRATROPICAL INTERACTION PROBLEMS
- 6) CLEAR AIR TURBULENCE/WIND SHEAR HAZARDS

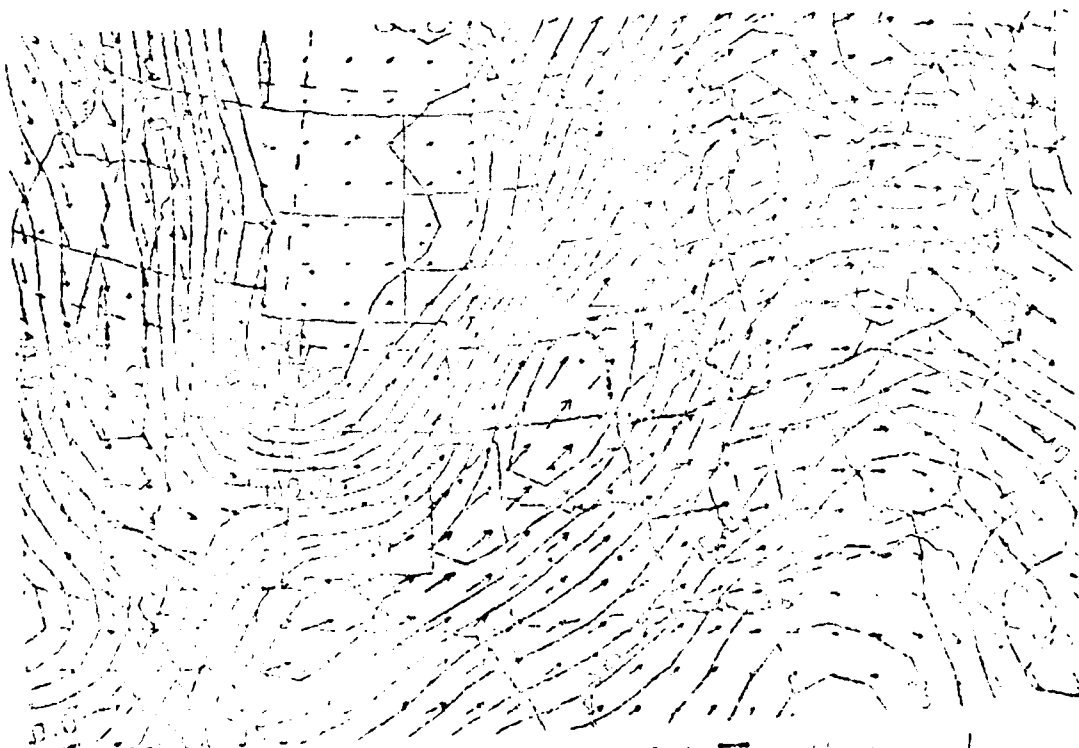
2) DC-10 ACCIDENT/APRIL 3, 1981 WEATHER SITUATION





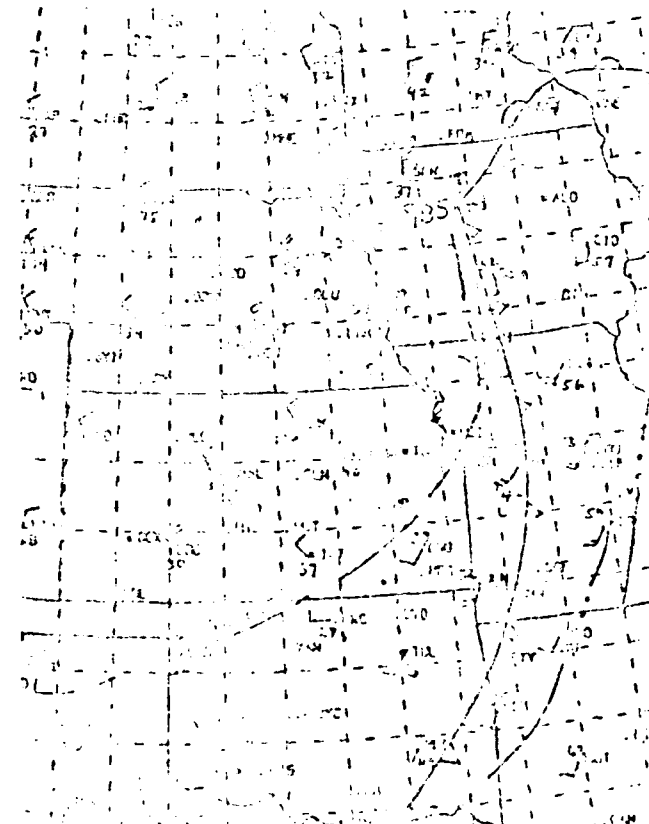
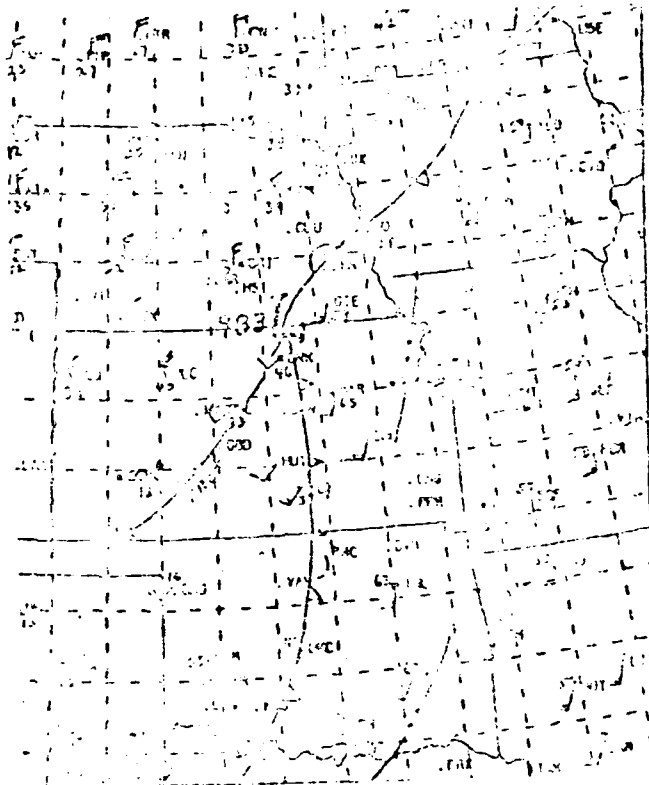


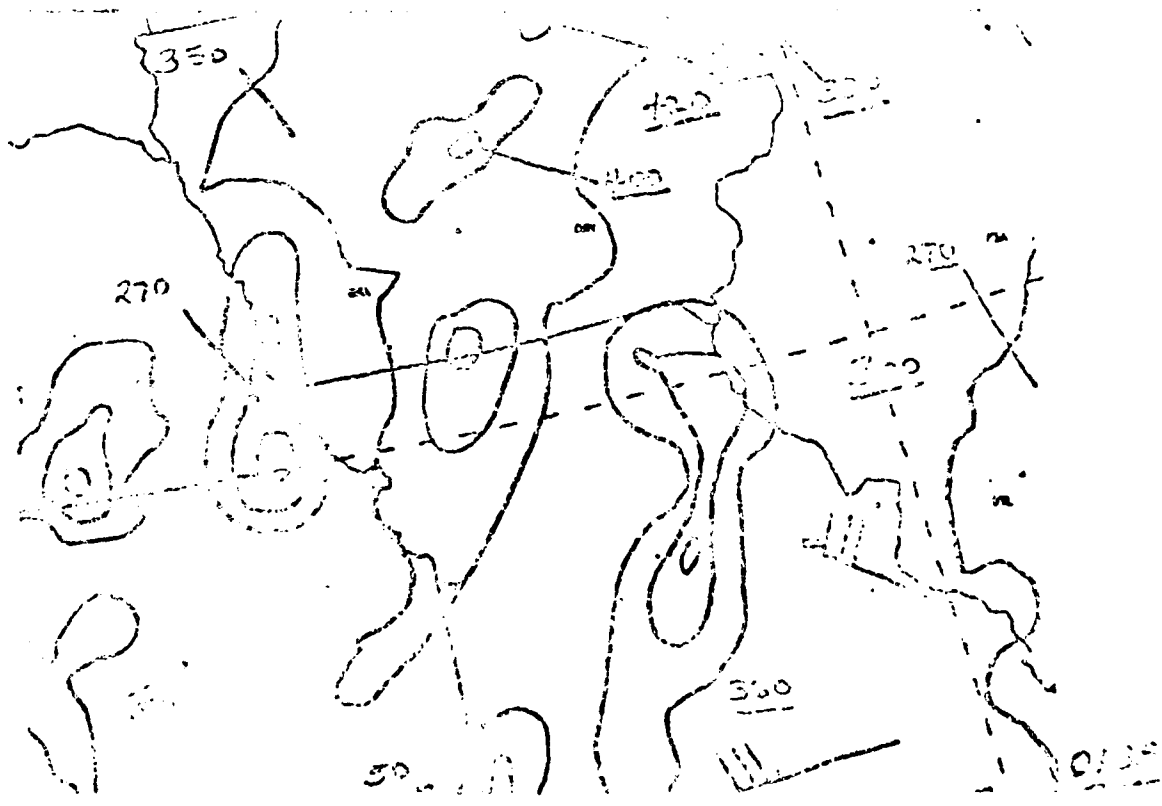
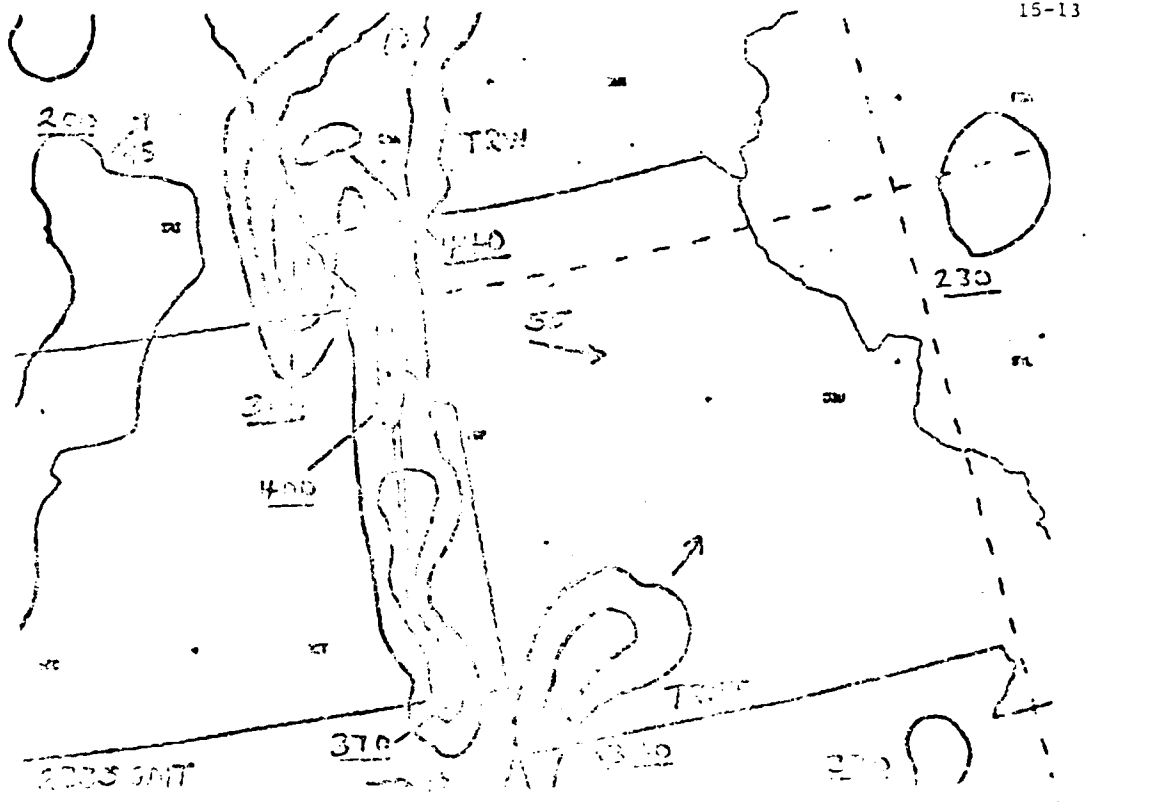
V 250 Mb 1200 GMT 3 APRIL



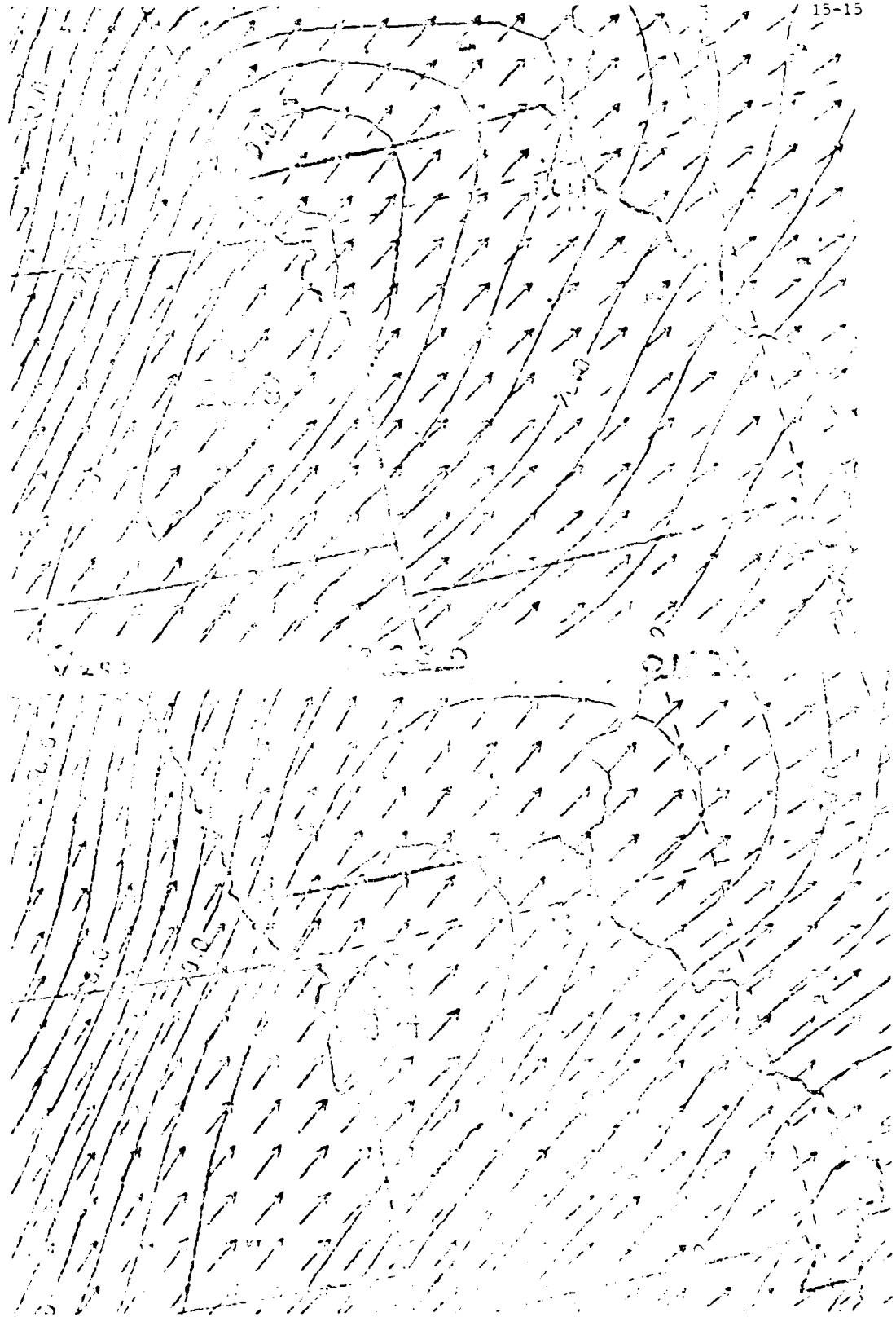
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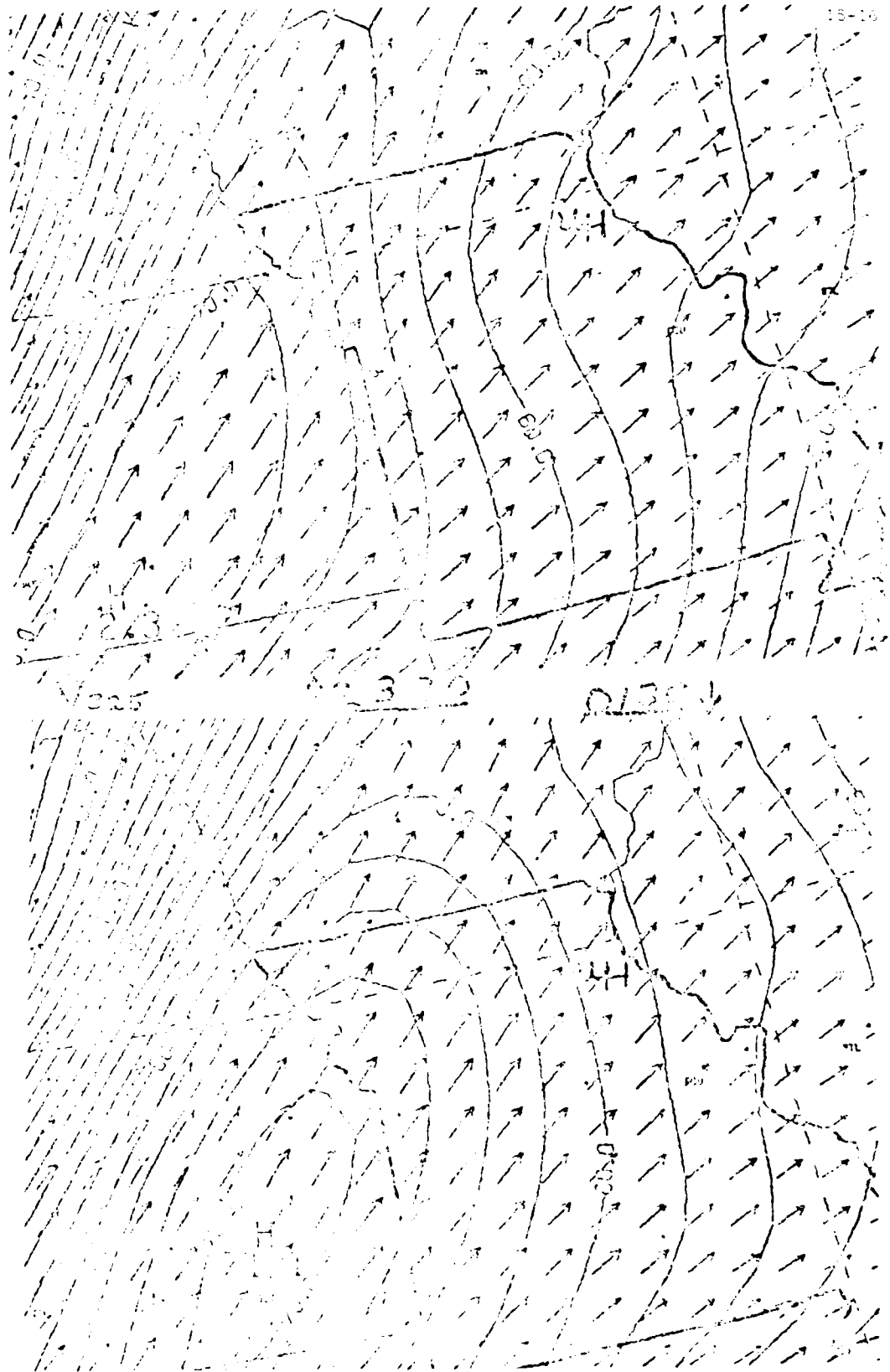


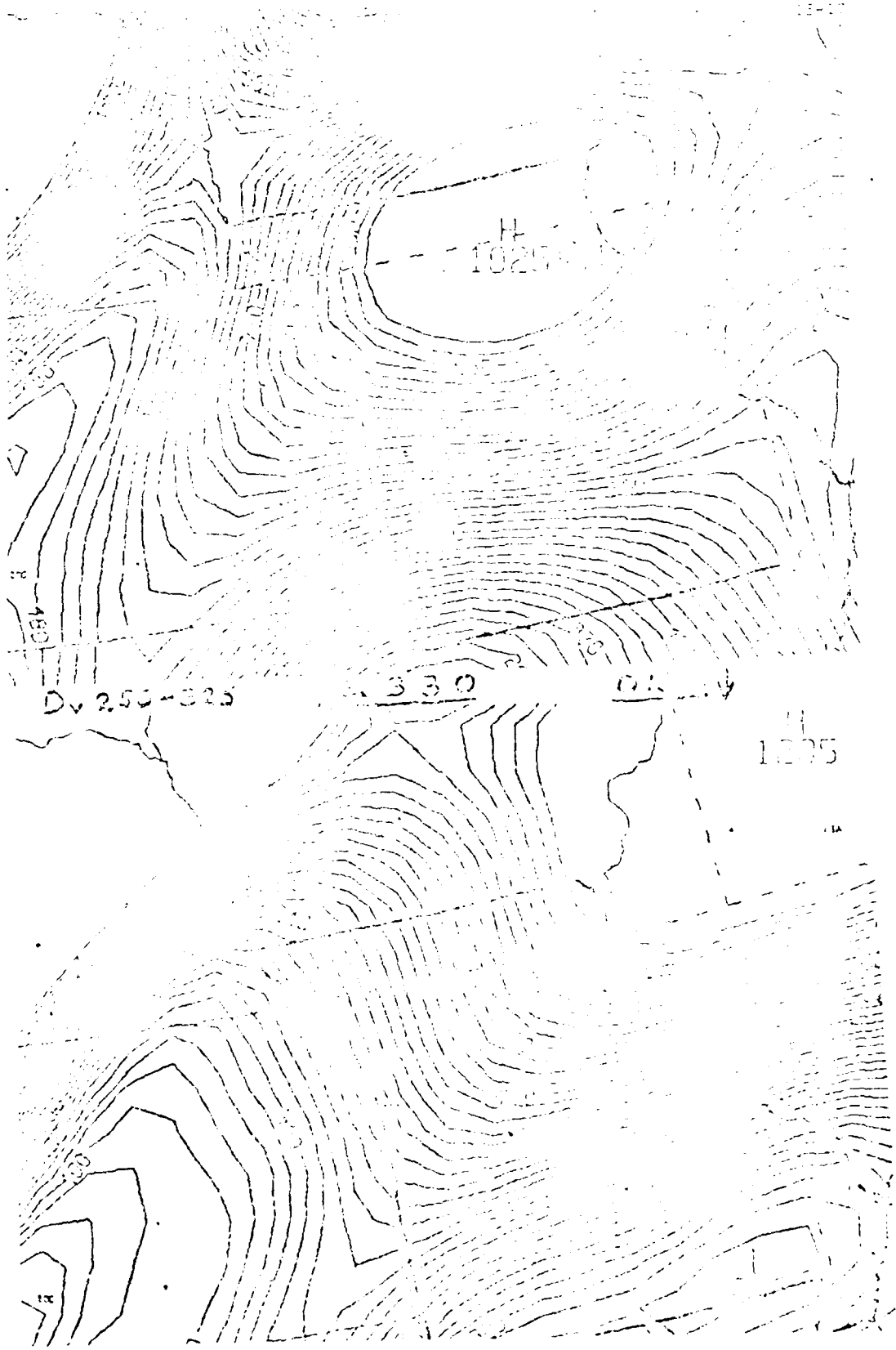


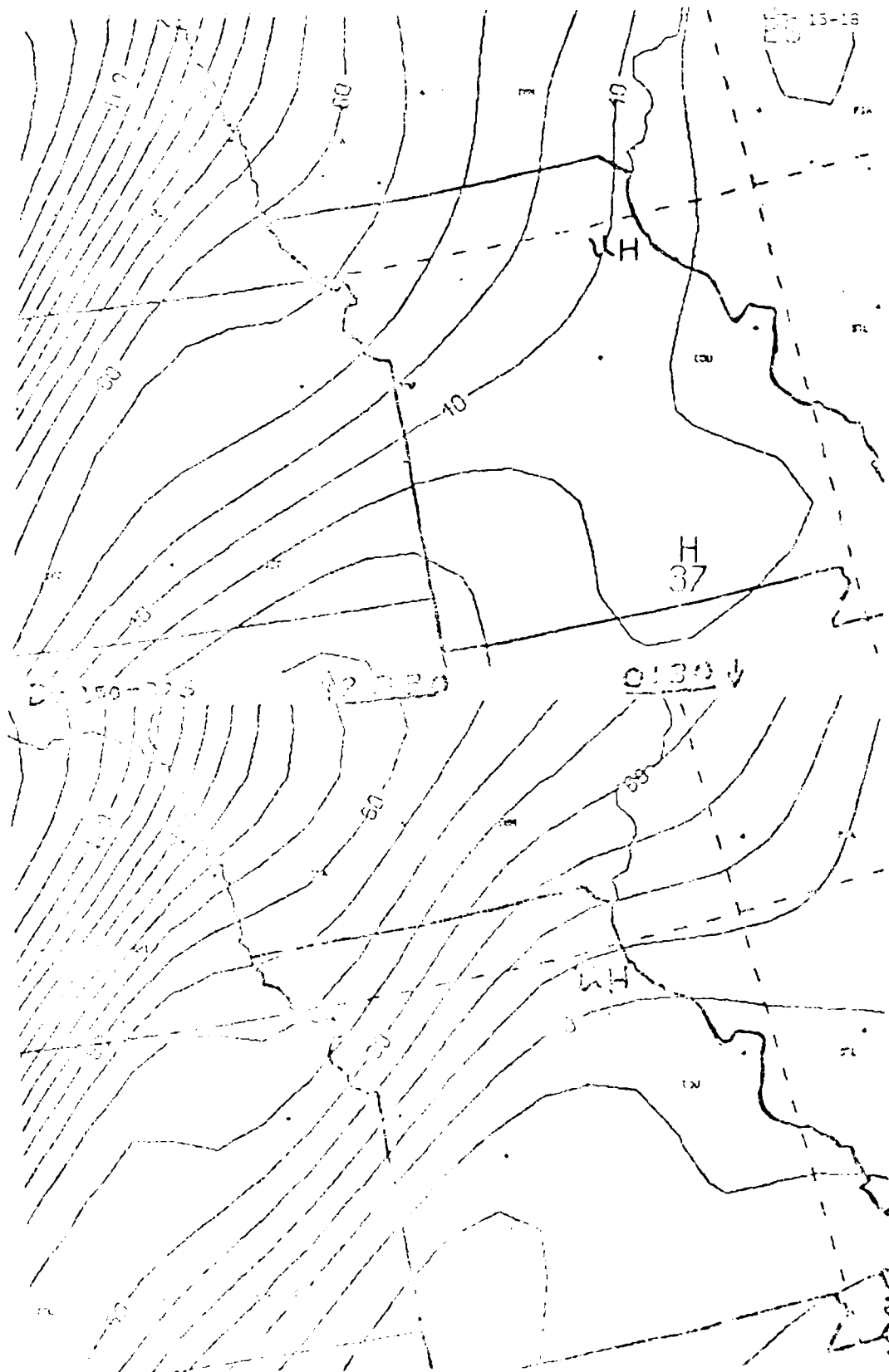


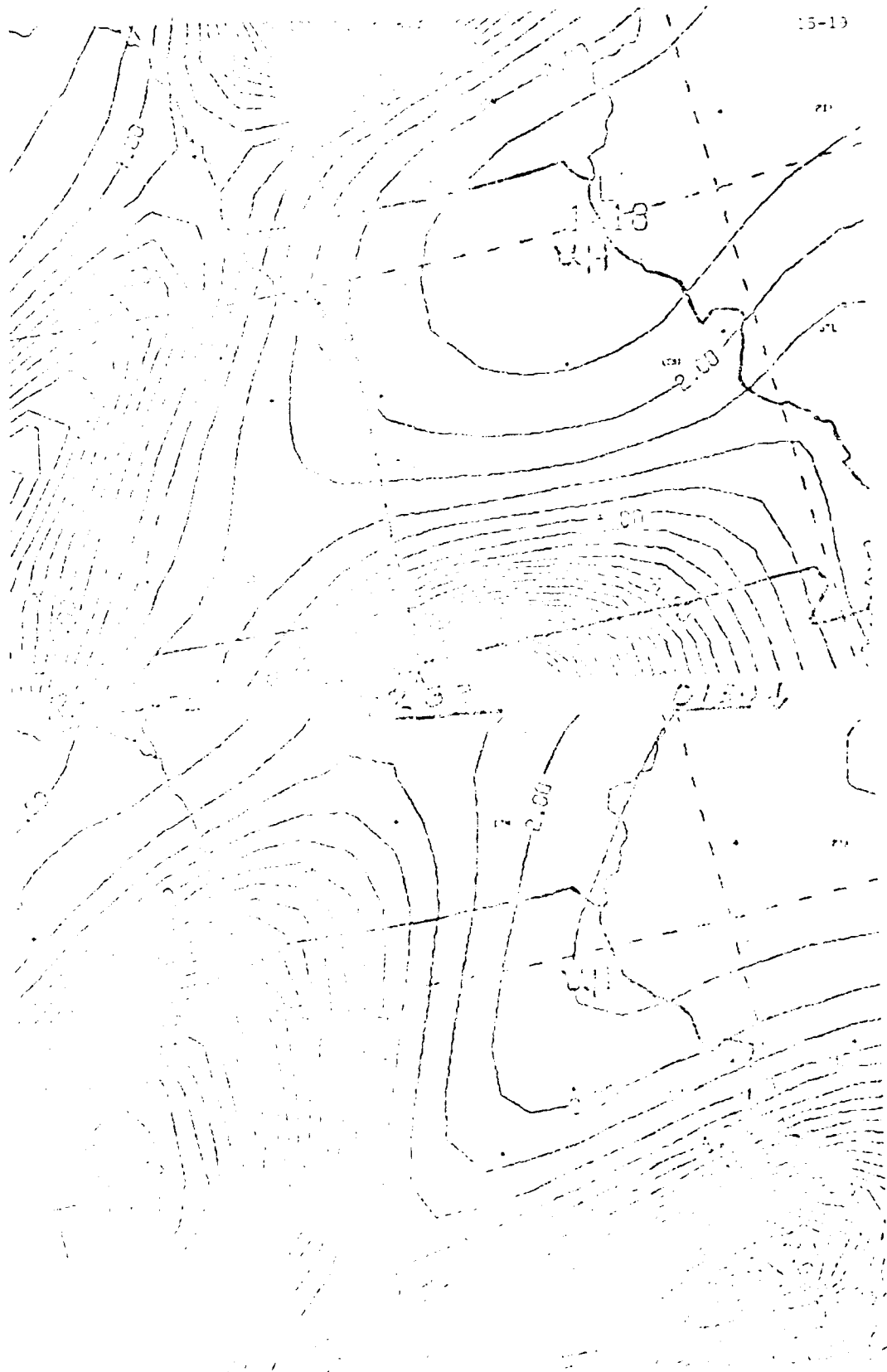
3) MODEL SIMULATION RESULTS



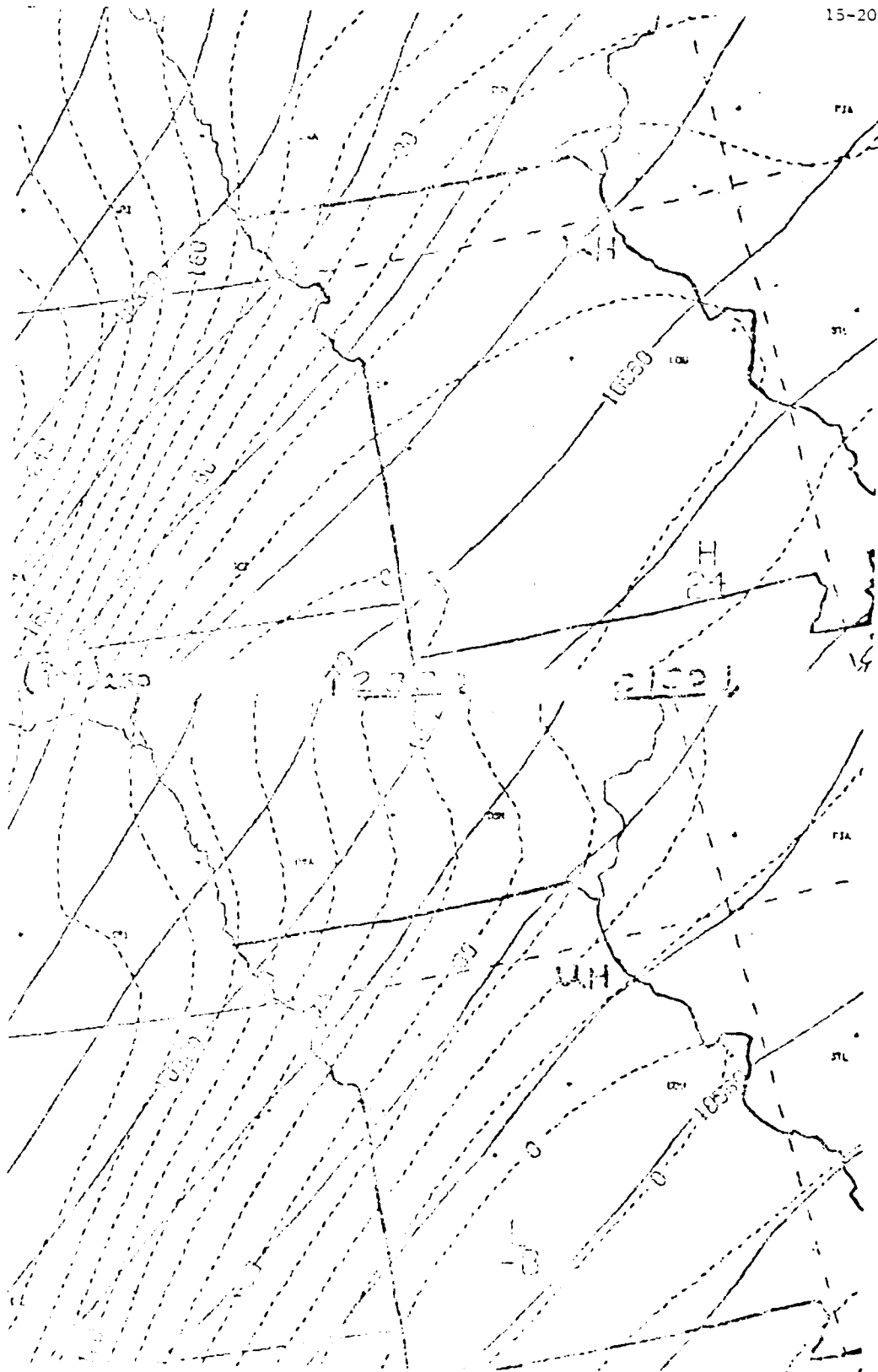


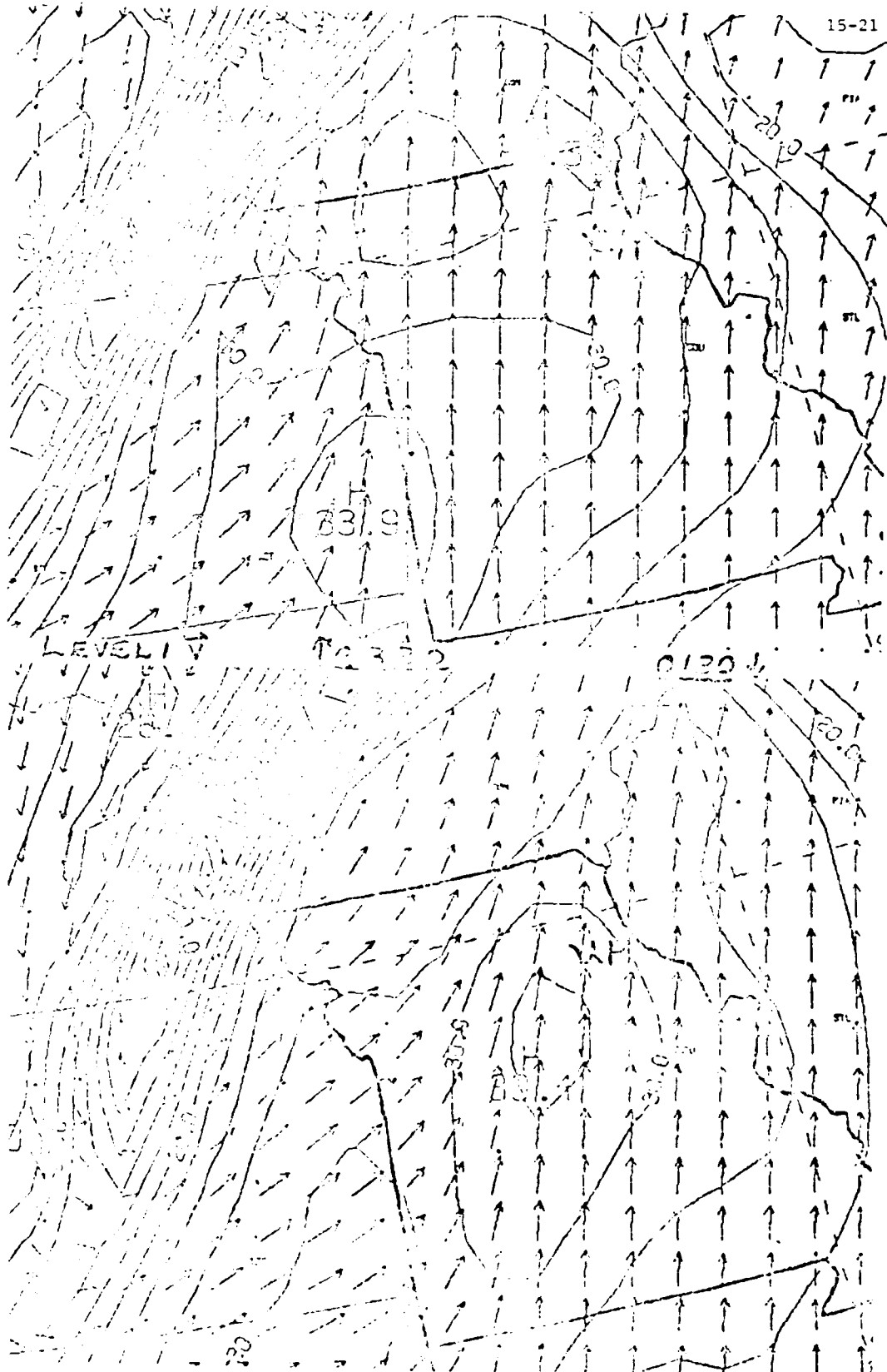












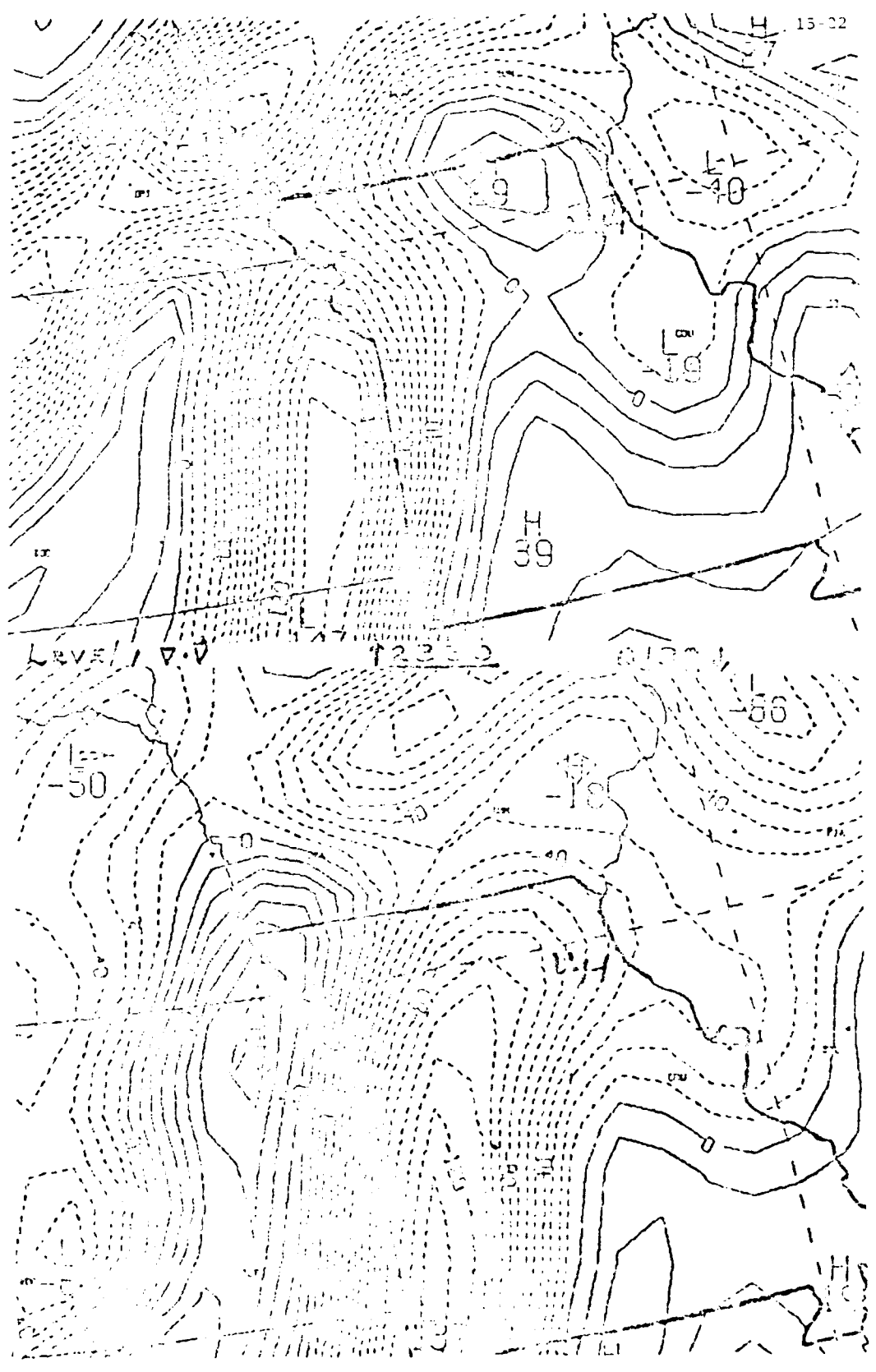
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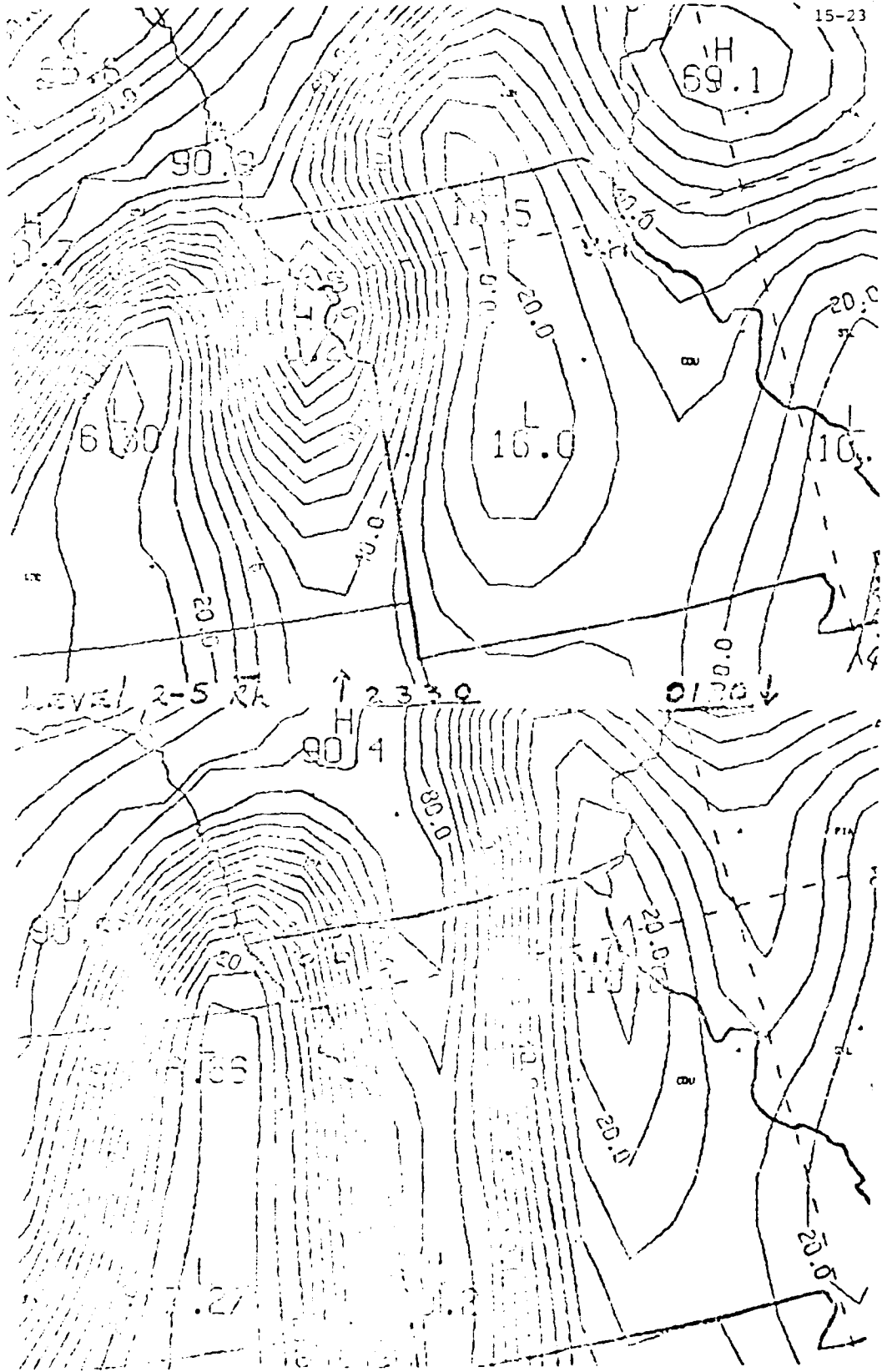
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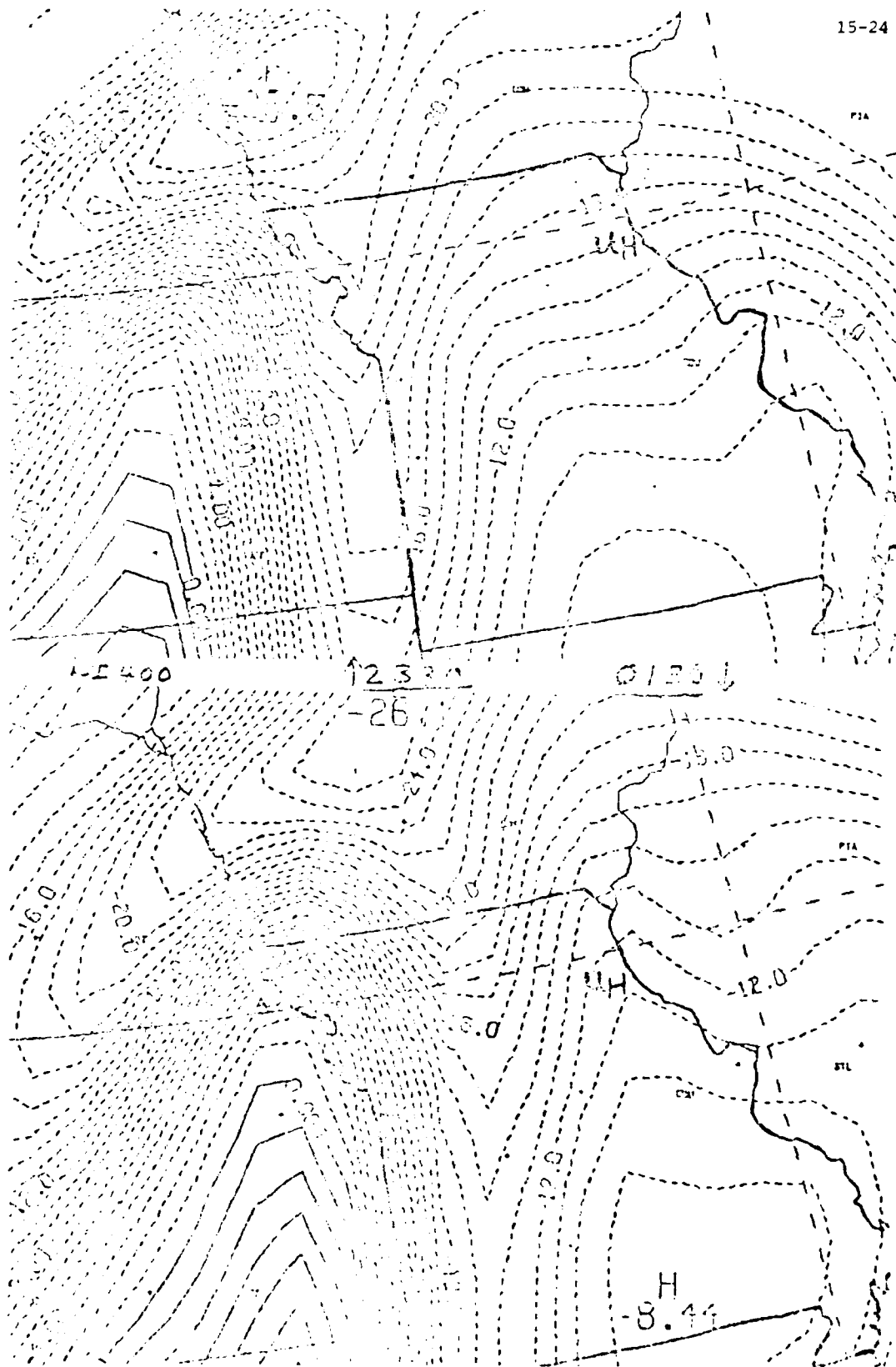
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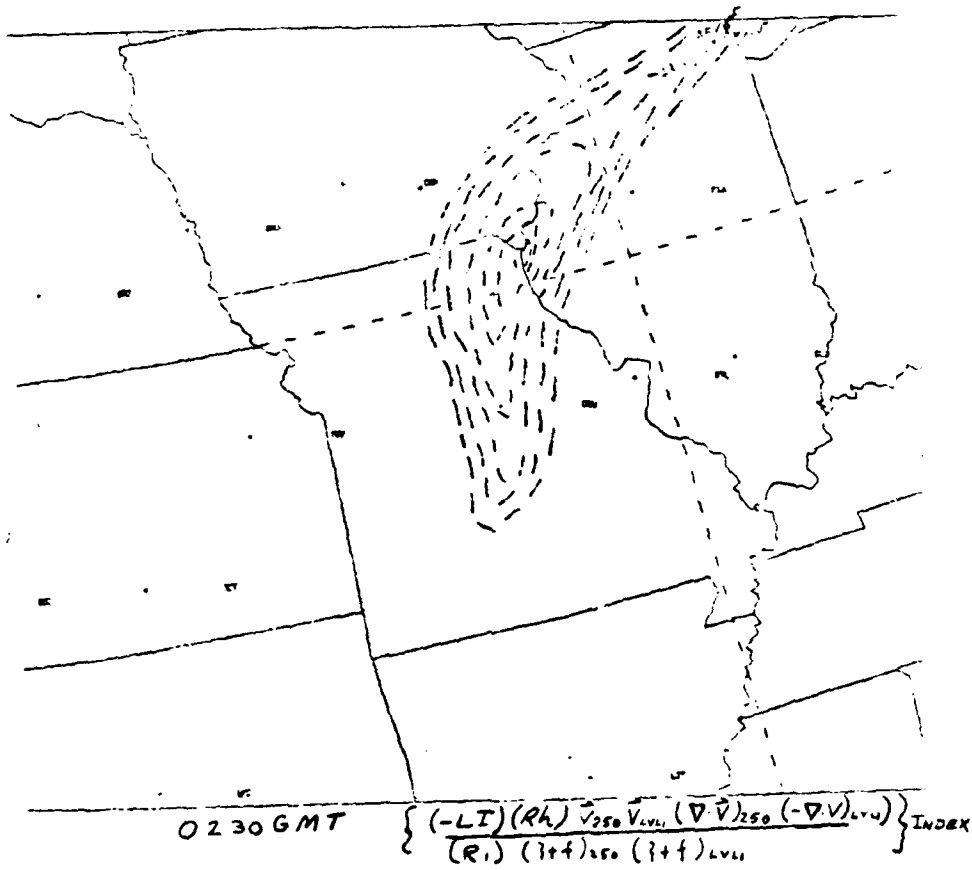
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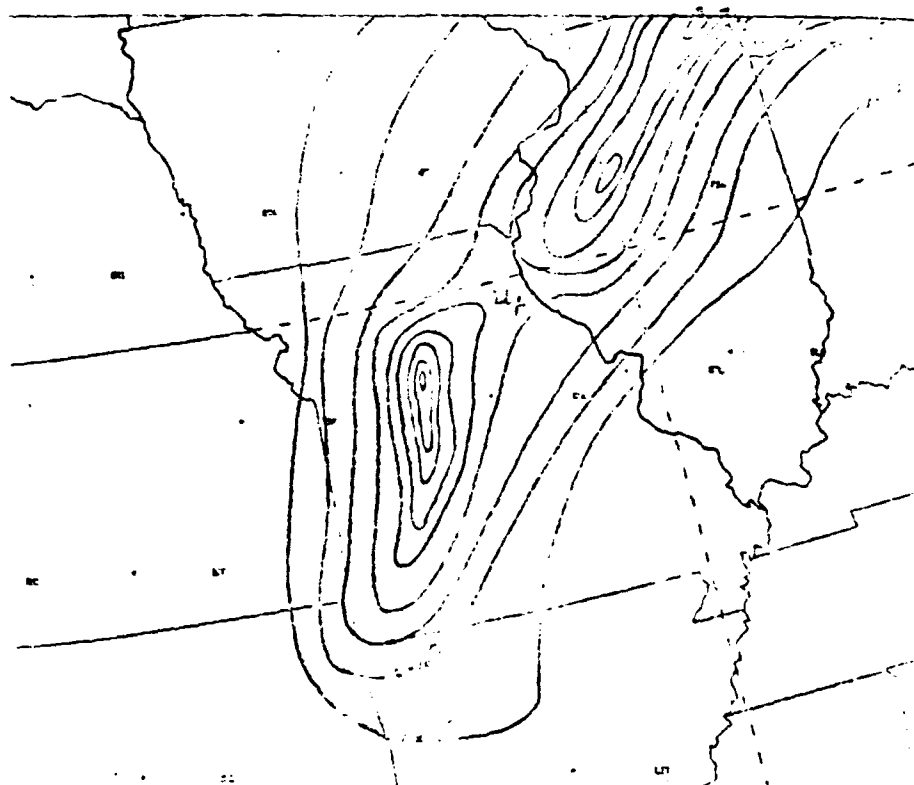






- 4) M.A.S.S. POTENTIAL UTILITY FOR C.A.T.,  
WIND SHEAR, AND TURBULENCE HAZARDS FORECASTING





0130 GMT

$\left\{ \begin{array}{l} (-LI)(RH) \overline{V_{250}} \overline{V_{500}} (\nabla \cdot V)_{250} (-\nabla \cdot V)_{500} \\ (R_i) (\nabla^2 T)_{250} (\nabla^2 T)_{500} \end{array} \right\} INDEX$



| P   | Density        |                | W.A.S.S. (MINIMUM) |       |
|-----|----------------|----------------|--------------------|-------|
|     | ρ <sub>1</sub> | ρ <sub>2</sub> |                    |       |
| 400 | 4500           |                | 77                 | (100) |
|     | 5000           |                | 78                 |       |
|     | 5500           | 220°           | 82                 |       |
|     | 6000           | 220°           | 87                 |       |
|     | 6500           |                | 91                 |       |
|     | 7000           | 200°           | 95                 |       |
| 325 | 7500           |                | 100                | (115) |
|     | 8000           |                | 104                |       |
|     | 8500           |                | 108                |       |
| 250 | 9000           |                | 112                | (132) |
|     | 9500           | 240°           | 117                |       |
|     | 10000          |                | 121                |       |
|     | 10500          | 250°           | 125                |       |
|     | 11000          |                | 130                |       |
|     | 11500          | 245°           | 134                |       |
|     | 12000          |                | 138                |       |
|     | 12500          | 255°           | 142                |       |

Robert, in his analysis of the stability of vortex layers, calculates a stability boundary in terms of a wave number  $k_0$ ,

where

$$k_0 = 2\pi \frac{\rho_1 - \rho_2}{\rho_1 + \rho_2} \frac{1}{(2U)^2}$$

$\rho_1$  = density at lower boundary of layer

$\rho_2$  = density at upper boundary of layer

$C$  = convective constant

$2U$  = shear in axial speed across vortex layer

$\lambda_0$  = Rayleigh critical wavelength

If the disturbance is perturbed at a wavelength  $\lambda$  and  $\lambda < \lambda_0$ , the disturbance will be unstable and the formation of cat's eyes will occur at  $\lambda_0$ .

## FUTURE PLANS

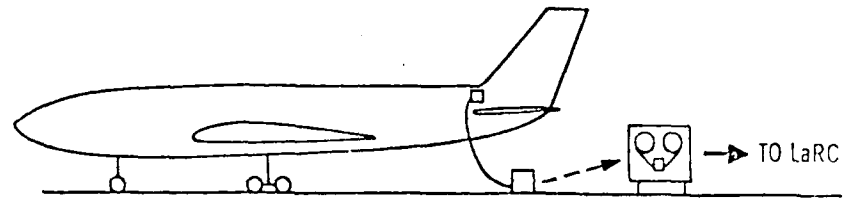
1. CONTINUED MODEL DEVELOPMENT
2. CONTINUED EXPANSION OF APPLICATIONS SOFTWARE FOR 5 PROBLEM AREAS
3. EXPANSION OF ROLE IN SHUTTLE APPLICATIONS
4. EXPAND MODEL TO HEMISPHERIC COVERAGE AT MESOSCALE ON C.D.C. CYBER 205 IN MINNEAPOLIS
5. 40-DAY SPRING TEST AND GODDARD LABORATORY EVALUATION

APPENDIX 16 16-1

DVGH PHASE II  
SYSTEM DESIGN APPROACH

WORK PERFORMED UNDER LARC CONTRACT NAS1-16098  
BY RESEARCH TRIANGLE INSTITUTE

AIRLINE READOUT AND TRANSCRIPTION: TWICE PER WEEK



AD-A136 364

REPORT ON A VISIT TO THE USA DURING JANUARY 1982  
RELATING TO THE EFFECT OF (U) AERONAUTICAL RESEARCH  
LABS MELBOURNE (AUSTRALIA) D J SHERMAN AUG 82

33

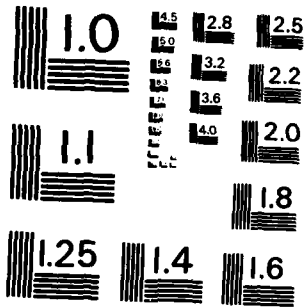
UNCLASSIFIED

ARL/STRUC-TM-344-SUPPL

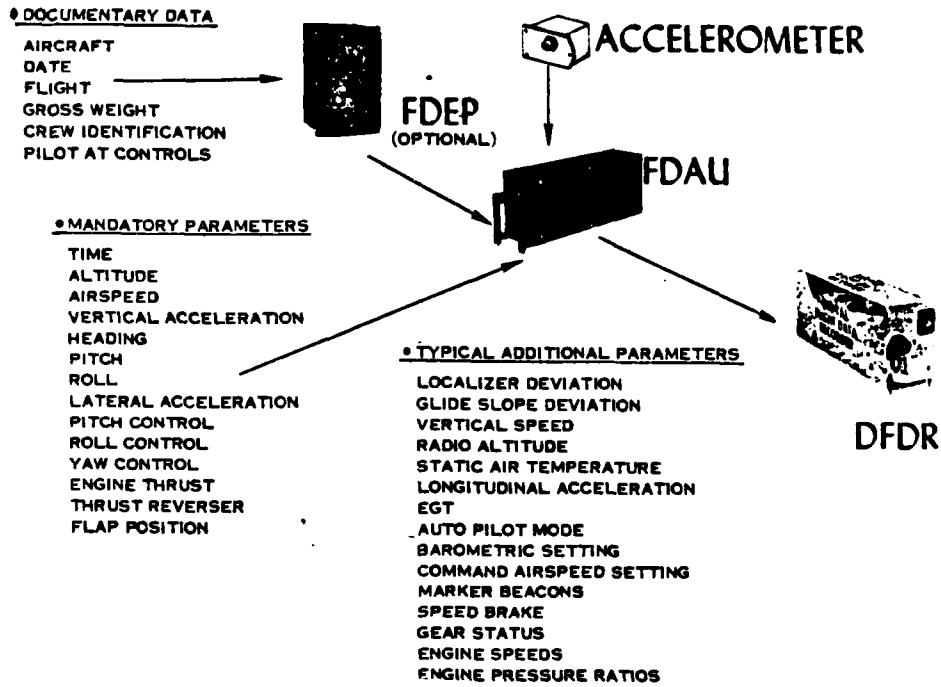
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS - 1963 - A



31-31-22 Customer Specified Parameters

- Radio Altitude
- Groundspeed
- Localizer Deviation
- Glideslope Deviation
- True Heading
- True Track Angle
- Mach Number
- Angle of Attack
- Total Air Temperature
- Static Air Temperature
- ADC Discretes - TBD
- Baro Correction (Captain's)
- Inertial Vertical Velocity
- Present Latitude
- Present Longitude
- Windspeed
- Wind Angle
- Drift Angle
- N1 - L
- N1 - R
- N2 - L
- N2 - R
- N3 - L
- N3 - R
- EGT - L
- EGT - R
- Fuel Flow - L
- Fuel Flow - R
- Engine Vibration - L
- Engine Vibration - R
- Caution and Warning Discretes (TBD)
- Engine Oil Temperature L & R
- Engine Oil Pressure L & R
- Engine Oil Quantity L & R
- APU EGT and RPM
- Flight Path Angle

ADDED REV SYM D

|               |                |   |
|---------------|----------------|---|
| <b>BOEING</b> | NO. D6-44010-2 | → |
|               | PAGE 31-2b     |   |



## STATEMENT OF WORK

- DESIGN AND IMPLEMENT A NASA TEST SYSTEM FOR USE IN IDENTIFYING THE NOISE ENVIRONMENT AND IN ISOLATING SOURCES OF DATA ANOMALIES IN THE AIRLINE DIGITAL DATA.
- ANALYZE AND COMPARE AIRLINE DIGITAL DATA TO THE DATA OBTAINED USING THE NASA SYSTEM. ASCERTAIN THE SOURCE OF THE DATA ANOMALIES.
- AUTOMATE THE TECHNIQUES USED IN THE MANUAL REMOVAL OF THE ANOMALIES ON GROUND-BASED COMPUTERS.
- DESIGN STATISTICAL DATA REDUCTION TECHNIQUES AND IMPLEMENT ON GROUND-BASED COMPUTERS.
- DESIGN OF AN ON BOARD STATISTICAL DATA PROCESSOR/RECORDER FOR USE IN THE DIGITAL VGH PROGRAM.

## DVGH PHASE II REQUIREMENTS

BRANCH LETTER SAME SUBJECT DATED DEC. 17, 1979

SPECIFIC

- . TABULATE LEVEL CROSSINGS  
FOR SPECIFIC ALT BANDS  
7 TABLES *x 9 alt. bands.*
- . MINI-MAX ACCELERATION & GUSTS  
5 TABLES
- . FLIGHT PROFILE STATISTICS  
7 TABLES
- . WEIGHT & ALTITUDE STATISTICS  
2 TABLES
- . AIRSPEED & ALTITUDE  
3 TABLES

TOTAL 24 TABLES

~ 5100 ENTRIES

IMPLIED

- . 250 FLIGHT HOURS
- . ARINC 573
- . CAS DATA 1/SEC
- . VERG DATA 4/SEC
- . LATG DATA 4/SEC
- . ALT DATA 1/SEC
- . GROSS WEIGHT AT TAKEOFF  
1 PER FLIGHT
- . MAINGEARSW 1/SEC
- . AUTOPILOTSW 1/SEC
- . FLIGHT TYPE
- . SEPARATE GUST & MANEUVER  
ACCELERATIONS
- . AIRCRAFT CHARACTERISTICS  
WING AREA  
LIFT CURVE SLOPE  
RATE OF FUEL BURN
- . ATMOSPHERIC TABLE DATA
- . DATA TRUTH
- . FUEL USE RATE

DVGH PHASE II FUNDAMENTAL REQUIREMENTS

DATA ACQUISITION AND PROCESSING

- RELIABLE AND ACCURATE DATA SOURCE
- ASSESSABLE DATA INTEGRITY
- REASONABLE PROCESSING AND MEMORY REQUIREMENTS

DIAGNOSTIC TESTS

- LARC LABORATORY TEST BED
  - AIRCRAFT SENSORS, DIGITAL ELECTRONICS, AND CRASH RECORDERS TESTED
  - NOMINAL AND WORSE CASE
  - ALL MANUFACTURERS
- FLIGHT TEST
  - NASA DIAGNOSTIC RECORDING SYSTEM FLOWN IN PARALLEL WITH ARINC 573
  - SYSTEM IN COMMERCIAL OPERATION >40 HRS
- RESULTS
  - ARINC 573 DIGITAL DATA STREAM IS AN EXCELLENT SOURCE OF DVGH PHASE II DATA
  - CRASH RECORDERS ARE NOT HIGH QUALITY VOLUME SOURCES OF DATA

SYSTEM DESIGN  
(IN PARALLEL WITH DIAGNOSTIC TESTS)

- PERMANENT MEMORY REQUIREMENT

<math>64 \times 10^3</math> BIT TO  $1 \times 10^9</math> BIT$

- PROCESSOR CAPABILITY

ALL FUNCTIONS; DECOMMUTATION, EDITING, FILTERING, COMPUTING  
AND STORAGE CAN BE ACCOMPLISHED IN REAL TIME

RESULTS

AIRBORNE DATA PROCESSING FEASIBLE

## AIRBORNE DIGITAL VGH SYSTEM DESIGN

### TASKS

#### HARDWARE

- BASIC SYSTEM LAYOUT
- MEMORY REQUIREMENTS
- COMPUTATIONAL SPEED REQUIREMENTS
- SHORT TERM STORAGE REQUIREMENTS
- LONG TERM STORAGE REQUIREMENTS
- AVAILABLE OPTIONS FOR EACH FUNCTION
- COST ANALYSIS
- FINAL SYSTEM CONFIGURATION

#### SOFTWARE

- SYSTEM SUPERVISOR
  - OPERATIONAL MODES
  - AUXILIARY FLIGHT DATA ENTRY
  - NON-FDAU DATA ENTRY
  - FRONT-END PROCESSING
  - DATA EDITING
  - COMPLEMENTARY FILTERING
  - GUST VELOCITY DETERMINATION
  - PER-FLIGHT TABULATIONS
  - ACROSS FLIGHT TABULATIONS
  - DATA STORAGE
- } SHUTDOWN/CONTINUE

PROCESSOR DEVELOPMENT

EDIT, FILTER, CALCULATION, FLIGHT MODE AND TABLE DERIVATION  
PROGRAMS WRITTEN AND ITERATED

DATA PROCESSOR STRATEGY TESTED AT RTI AGAINST A 10 FLIGHT  
SAMPLE OF ACTUAL DATA

VERG-1 LEVEL CROSSINGS PER HOUR WITHIN PRESSURE ALTITUDE BANDS

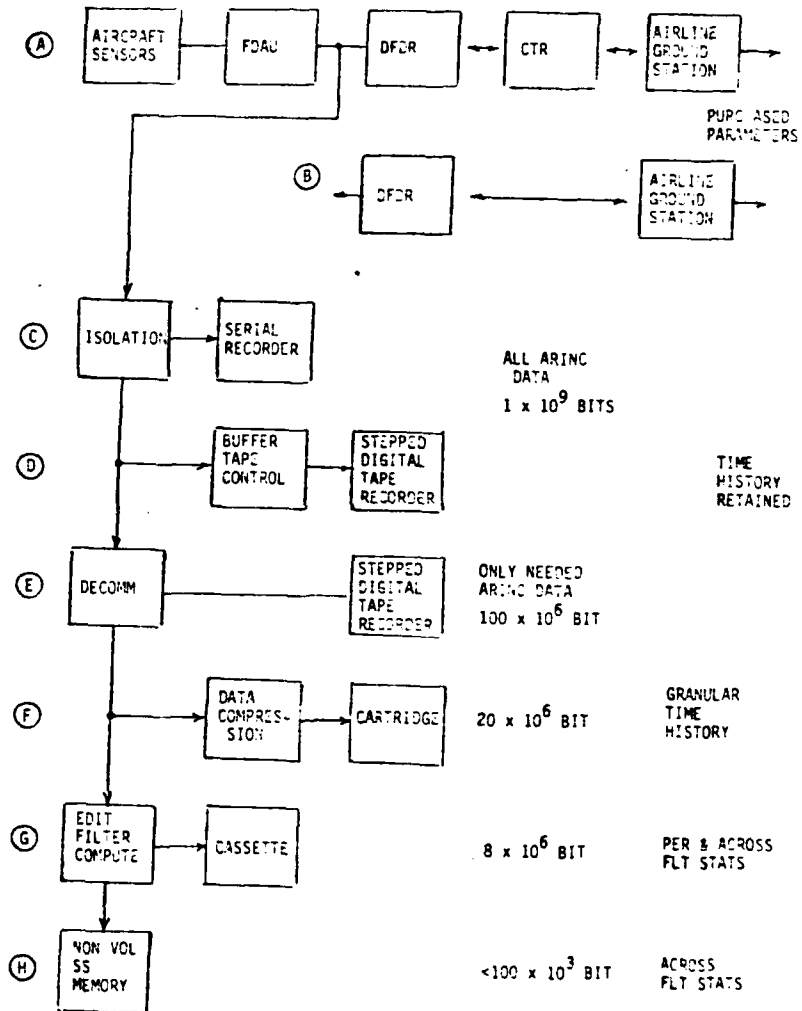
| G UNITS                   | -500               | 4500               | 9500                | 14500               | 19500               | 24500               | 29500               | 34500               | 39500               |
|---------------------------|--------------------|--------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
|                           | TO<br>4500<br>(FT) | TO<br>9500<br>(FT) | TO<br>14500<br>(FT) | TO<br>19500<br>(FT) | TO<br>24500<br>(FT) | TO<br>29500<br>(FT) | TO<br>34500<br>(FT) | TO<br>39500<br>(FT) | TO<br>44500<br>(FT) |
| 1.60                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 1.40                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 1.20                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 1.00                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.80                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.70                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.60                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.50                      | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.40                      | 0.00               | 0.05               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.30                      | 0.00               | 0.05               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.20                      | 11.04              | 5.92               | 3.35                | 1.09                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| 0.15                      | 40.72              | 20.29              | 6.71                | 3.20                | 0.00                | 0.00                | 0.42                | 2.41                | 0.00                |
| 0.10                      | 131.13             | 101.43             | 36.89               | 26.22               | 6.92                | 2.15                | 5.93                | 11.02               | 0.00                |
| 0.05                      | 295.40             | 195.26             | 151.75              | 146.59              | 66.20               | 53.29               | 57.59               | 59.04               | 0.00                |
| 0.00                      | 775.77             | 640.71             | 847.60              | 759.33              | 781.75              | 1317.70             | 1167.11             | 1027.12             | 0.00                |
| -0.05                     | 209.00             | 105.96             | 155.94              | 192.29              | 90.02               | 96.09               | 80.51               | 129.45              | 0.00                |
| -0.10                     | 55.21              | 35.50              | 39.40               | 24.04               | 6.92                | 3.23                | 0.47                | 14.72               | 0.00                |
| -0.15                     | 15.10              | 5.92               | 13.41               | 17.40               | 0.00                | 0.00                | 2.96                | 3.62                | 0.00                |
| -0.20                     | 1.30               | 0.05               | 6.71                | 7.65                | 0.00                | 0.00                | 2.54                | 0.04                | 0.00                |
| -0.30                     | 0.69               | 0.00               | 3.35                | 1.09                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -0.40                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -0.50                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -0.60                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -0.70                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -0.80                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -1.00                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -1.20                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -1.40                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| -1.60                     | 0.00               | 0.00               | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                | 0.00                |
| FLIGHT HRS @ ALT          | 1.45               | 1.10               | 1.19                | 0.92                | 1.01                | 1.06                | 2.36                | 0.29                | 0.00                |
| FLIGHT MILES              | 322.2              | 356.3              | 464.7               | 417.4               | 501.7               | 1027.7              | 1352.7              | 4707.2              | 0.0                 |
| TOTAL FLIGHTS 10          |                    |                    |                     |                     |                     |                     |                     |                     |                     |
| TOTAL FLIGHT HOURS 10.3   |                    |                    |                     |                     |                     |                     |                     |                     |                     |
| TOTAL FLIGHT MILES 9230.9 |                    |                    |                     |                     |                     |                     |                     |                     |                     |



RESULTS OF 10 FLIGHT COMPARISON

- AUTOMATIC FLIGHT MODE SEPARATION ALGORITHMS MATCH TIME HISTORIES
- TABLES GENERATED & MATCH <3% AVG.
- EDIT AND FILTERING PROGRAMS OPERATIONAL

DVGH PHASE II SYSTEM OPTIONS



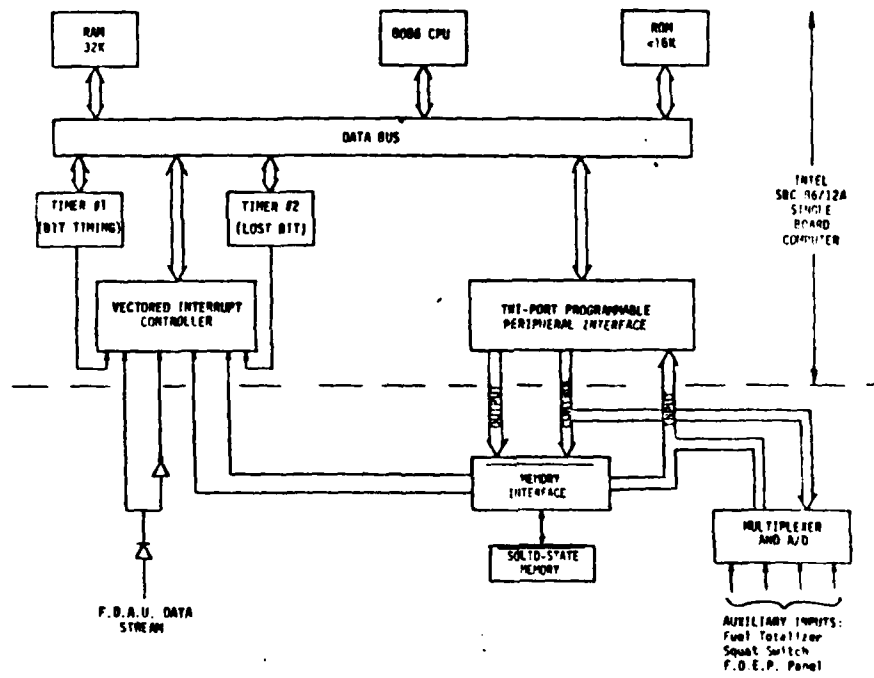
RECOMMENDATION FOR DVGH PHASE II SYSTEM DESIGN

ON-BOARD DATA COLLECTION PROCESSING STORAGE USING MICROCOMPUTER  
WITH ARINC 573 DATA STREAM SOURCE

DIRECTION

NASA DESIGN REVIEW RECOMMENDED EMPHASIS ON MAXIMUM DATA INTEGRITY

- SOLID-STATE TECHNOLOGY HIGHEST QUALITY STORAGE MEDIA
- BUILT IN TEST



SYSTEM HARDWARE CONFIGURATION

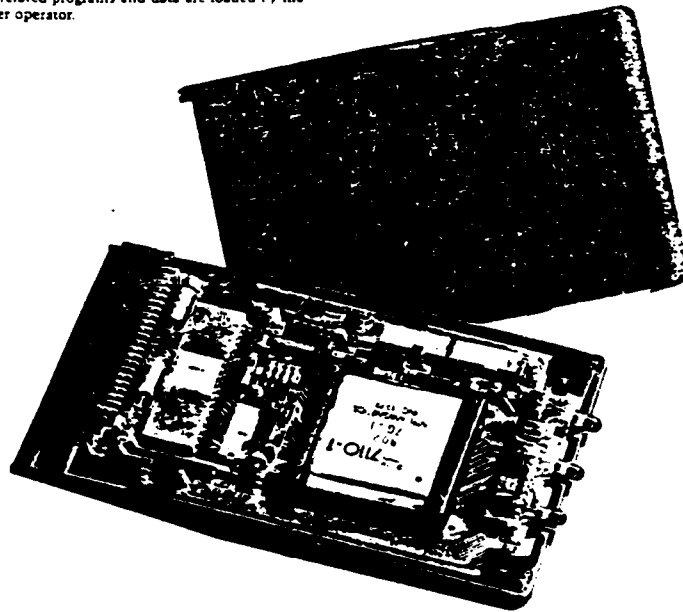
## NEW PRODUCTS

### NEW PLUG-A-BUBBLE SYSTEM PROVIDES COMPACT CASSETTE STORAGE FOR HARSH ENVIRONMENTS

The Plug-A-Bubble System™ features a new removable bubble cassette designed to provide portable, compact, permanent memory storage in harsh environments or critical storage applications. The basic iFAB system consists of a 128K-bit capacity bubble memory cassette and reader. It is ideal in environments that include temperature extremes, changes in air pressure and humidity, poor air quality, vibration, shock, or risk of power loss.

Users involved with test instrumentation, telecommunications and data acquisition terminals, and in industrial machine or process control will find the Plug-A-Bubble system particularly advantageous because of its easy portability. The system excels in situations that include handling or transportation, e.g. to and from a central processing center or where process-related programs and data are loaded by the computer operator.

The Plug-A-Bubble cassette is housed in a rugged cast aluminum cartridge. It contains Intel's 7110 1-Megabit bubble memory computer chip, the 7220 controller, the 7240 current pulse generator, the 7242 dual formater sense amplifier, a 7280 coil pre-driver, and two 7234 quad 100K-bit 2-transistors. All are mounted on a printed circuit board and packaged within the sealed cartridge. The cartridge also has a write protect switch which can be used to prevent accidental overwriting of the cassette. Data is transferred at transistor-transistor logic (TTL) levels between the cassette and reader.



12 The Plug-A-Bubble memory system provides permanent storage to provide rugged permanent storage in harsh environments.

DESCRIPTION

PHYSICAL

SIZE 1/2 ATR CASE  
13" x 7.625" x 4.875"

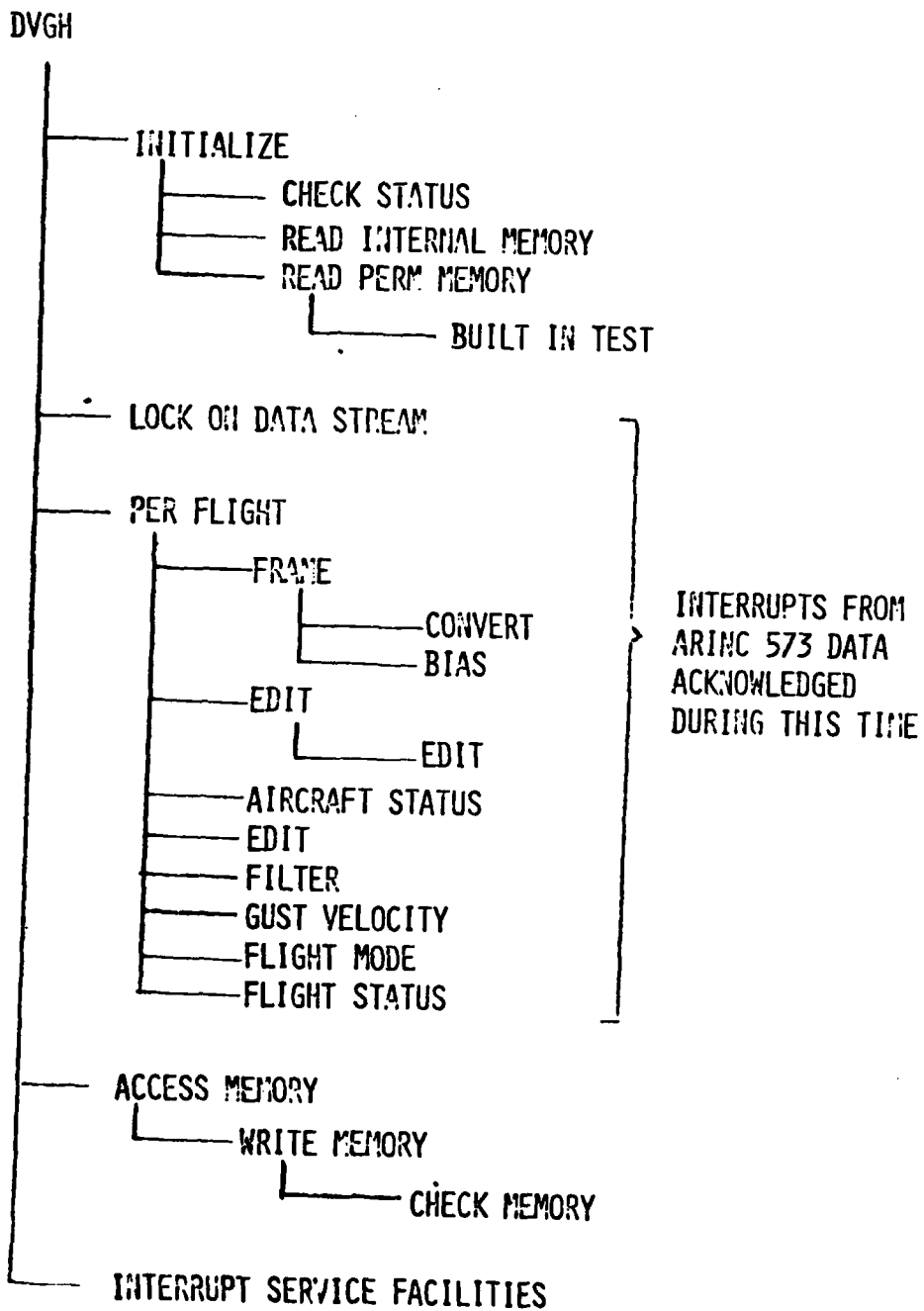
WEIGHT 4.5#

ELECTRICAL

POWER 24W

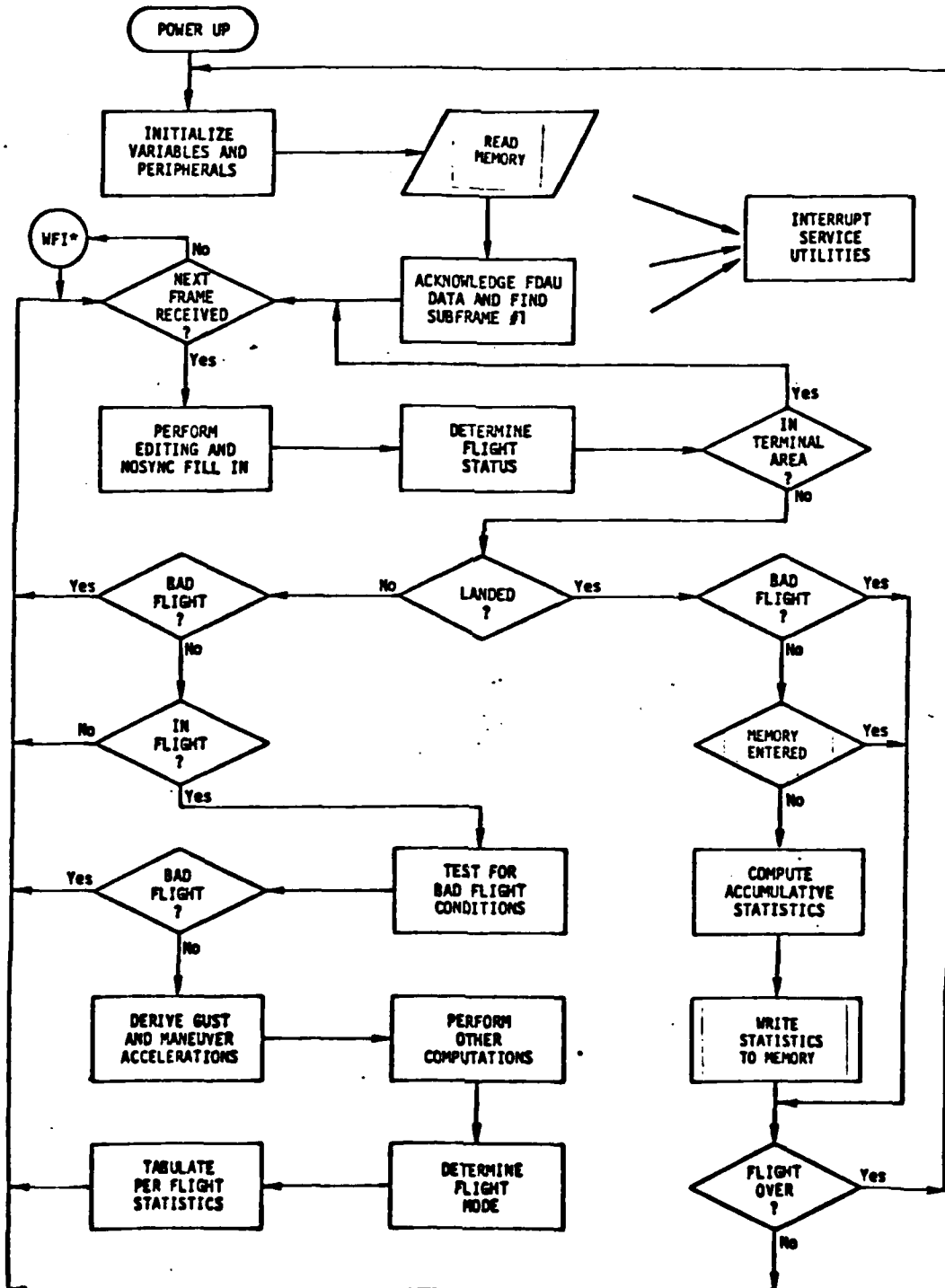
PROPOSED PROGRAM STRUCTURE

16-19



# GENERAL FLOW DIAGRAM

16-20



\*Wait for Interrupt

209



RECOMMENDATIONS FOR DVGH PHASE II PROGRAM DIRECTION

DEVELOPMENT

PROTOTYPE FABRICATION AND FLIGHT TEST

VERIFY ALL OPERATIONAL DESIGN FEATURES IN AIRLINE ENVIRONMENT

- ~1 YR
- FLTS OCT. 82

IMPLEMENTATION

DEPLOY DVGH PROCESSORS IN LARGE COMMERCIAL FLEET

- START 4TH QTR. 82
- DEPLOY 10 BY 83

EXPAND TO INCLUDE

G-A  
COMMUTER

MAINTENANCE

SUMMARY OF DVGH PHASE II CONTRACT

- THE ARINC 573 DATA STREAM VALID SOURCE OF VGH INFORMATION
- DATA ACQUISITION, EDITING, AND COMPUTATIONAL TASKS WITHIN THE CAPABILITIES OF MICROCOMPUTER
- DVGH PHASE II DESIGN HAS BEEN ESTABLISHED
- A PROTOTYPE VALIDATION PROGRAM IS PROPOSED
- COSTING AND SCHEDULING OF AN OPERATIONAL SYSTEM ESTIMATED

END

DATE  
FILMED

1-84

DTIC