



| | | READ INSTRUCTIONS |
|--|--|---|
| REPORT NUMBER I2. GOVT ACCESSION N | | BEFORE COMPLETING FOR |
| TL R-052 | AN A125 | |
| TITLE (and Subtitio) | | 5. TYPE OF REPORT & PERIOD COVERED |
| Applicability of Stella: Position Determination | r Rate for Astronomic | 6. PERFORMING ORG. REPORT NUMBER |
| AUTHOR(=) | | 8. CONTRACT OR GRANT NUMBER() |
| Dr. Angel A. Baldini | | |
| PERFORMING ORGANIZATION NAME A | ND ADDRESS | 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS |
| - CONTROLLING OFFICE NAME AND AD | DDRESS | 12. REPORT DATE |
| US Army Engineer Topogr Fort Belvoir, VA 22060 | aphic Laboratories | SEPT 1983 13. NUMBER OF PAGES |
| 4. MONITORING AGENCY NAME & ADDR | ESS(II dillerent from Controlling Off | ice) 15. SECURITY CLASS. (of this report) |
| | | 15. DECLASSIFICATION/DOWNGRADING SCHEDULE |
| . DISTRIBUTION STATEMENT (of this R | eport) | DTIC |
| 7. DISTRIBUTION STATEMENT (of the ab | etract entered in Block 20, if differe | D |
| Presented at at ACSM-AS | | Lake City, Ut., 19-23 Sep 83 |
| 8. SUPPLEMENTARY NOTES astronomic position | instrument constants | |
| latitude | refraction | |
| longitude | | |
| | If necessary and identify by block m | mber) |
| | | |
| | | |
| | | |
| | | |
| This paper deals with a me star rate of change in azis star is observed a number third order. can be obtain | thod of determining an muth and zenith distan of times. Coefficient and with a high degree | n stronomic position by using the nce, with respect to time. The ts of Taylor expansion, up to the of accuracy as a function of |
| sections of a small great time, zenith distance, and arbitrarily chosen star po a test of the accuracy of | circle of arc. Method azimuth are considered sition. A comparison of the observation. It is | ds of application of observed dat d. They can be reduced to an of the results so obtained gives s shown that astronomic refraction |
| problems can be reduced us | ing_the_method_descril | LASSIFIED |

Ť

| Accession For |] • • | |
|------------------------------|---|--------------|
| NTIS GRALI | | ELECTE |
| Justification | $ = \begin{pmatrix} 0 T I C \\ C O P \gamma \\ INSPECTO \end{pmatrix} $ | DEC 1 5 1983 |
| By | | |
| Availability Codes | - | D |
| Avail and/or Dist Special | APPLICABILITY OF STELLAR RATE FOR ASTRONOMIC POSITION DETERMINA | TION |
| | | |

U.S. Army Engineer Topographic Laboratories Fort Belvoir, VA 22060

BIOGRAPHICAL SKETCH

Dr. Angel A. Baldini joined ETL's predecessor organization in 1960. From 1957-1960 he was associated with the Georgetown University Observatory, Washington, D.C. Prior to 1957, he was Professor and Head, Department of Geodesy, La Plata University, Argentina. At ETL, Dr. Baldini worked primarily in the field of astro-geodesy. Since 1974 he has been senior scientist in the Center for Geodesy, Research Institute, ETL. He authored 40 reports and papers since 1963 and presented results thereof at 25 Army, national, and international meetings. He received an Army Research Development achievement award in 1969. He has been a member of the American Geophysical Union since 1960.

ABSTRACT

This paper deals with a method of determining an astronomic position by using the star rate of change in azimuth and zenith distance, with respect to time. The star is observed a number of times. Coefficients of Taylor expansion, up to the third order, can be obtained with a high degree of accuracy as a function of sections of a small great circle of arc.

Methods of application of observed data, time, zenith distance and azimuth are considered. They can be reduced to one arbitrarily chosen star position. A comparison of the results so obtained gives a test of the accuracy of the observation.

It is shown that astronomic refraction problems can be reduced using the method described in this report.

INTRODUCTION

This report deals with the determination of astronomic latitude, longitude and azimuth as well as the instrument constants, in a quite different way than of the classical methods, by using a star rate of change of zenith angle and azimuth with respect to time, and in a way that is independent of refraction problems. The observed times, zenith angles, or azimuth can be reduced to an arbitrary chosen star position, independent of the station coordinates.

A comparison of the results so obtained gives not only a test of the accuracy of the observations, but also the kind of error committed. Independent sets of observations are considered. A closedformula gives accurate values of the difference between zenith angles, which are related to power series according to Taylor's theorem, for determining the station's coordinates.

83 12 14 049

ZENITH DISTANCES RATE AS A FUNCTION OF TIME

Developing in power series according to Taylor's theorem, the following equation is considered:

$$\frac{Z_1 - Z_0}{\theta_1 - \theta_0} = \frac{dZ}{d\theta} + \frac{1}{2} \frac{d^2 Z}{d\theta^2} \left(\theta_1 - \theta_0\right) + \frac{1}{6} \frac{d^3 Z}{d\theta^3} \left(\theta_1 - \theta_0\right)^2 + .$$
(1)

 $\begin{pmatrix} \theta_1 - \theta_0 \end{pmatrix}$ must be taken in radius. Z_1 represents the true zenith distances that correspond to the sidereal times θ_1 , and Z_0 the true zenith distance that corresponds to the sidereal time θ_0 . The difference between these true zenith distances are known through computations from the closed formula:

$$\cos \left(z_{i}^{-} - z_{o}^{-} \right) = \frac{2 \cos s_{i}^{-} - \cos \left(\overline{z}_{i}^{-} + \overline{z}_{o}^{-} \right) \left(1 - \cos \Delta_{i}^{-} \right)}{1 + \cos \Delta_{i}^{-}}, \quad (2)$$

in which Δ represents the difference in azimuth between the two observations

$$\Delta_{i} = A_{i} - A_{o} = L_{i} - L_{o}$$

 $L_{i}, L_{o} = horizontal readings$

S represents the great circle of arc computed from

$$\sin \frac{1}{2} S_i = \cos \delta \sin \frac{1}{2} (\theta_i - \theta_o).$$

t i

(3)

 \overline{Z}_1 and \overline{Z}_0 are observed zenith distances with respect to the times θ_1 and θ_0 , or derived by computation as can be shown later.

To obtain a higher degree of accuracy in evaluating (Z_1-Z_0) we may choose a star whose declination is greater than that of the observer's latitude. Observations taken before and after the star maximum elongation angles A can be small, on the order of few minutes of arc, while the changes in zenith distances have maximum variations; or we may observe two stars with small differences in azimuth, so the term $(1-\cos A)$ will be small. The sum of the zenith distances may not be far from 90°, so that the second term in the numerator of equation (2) becomes small, and therefore corrections due to refraction and index error can be disregarded. Table 1 shows the influence of an error of six minutes of arc in the sum of the two zenith distances.

| <u>le 1.</u> | | |
|---------------------------|------------------|---------------------------------|
| $\Delta \qquad Z_1 + Z_0$ | | $\cos (z_1+z_0)(1-\cos \Delta)$ |
| 6' | 120 [°] | -0.00000 076 |
| 6* | 1200 06' | 76 |
| 12' | 120 ⁰ | -0.00000 305 |
| 12' | 1200 06' | 306 |
| 181 | 120 | -0.00000 685 |
| 18' | 120 06' | 6R7 |
| | | |

Solution by Pairs of Observations

Q.1.61 - 6

Any two observations provide enough information to obtain the rate $\frac{dZ}{dt}$. In this case we have

$$\frac{Z_2 - Z_1}{\theta_2 - \theta_1} = \frac{dZ}{dt} + \frac{1}{24} \left(\frac{\pi}{180}\right)^2 \left[\left(\theta_2 - \theta_1\right)^0\right]^2 \frac{d^3 Z}{dt^3} .$$
 (4)

The second term of this equation is small and the value of $(\theta_2 - \theta_1)^0$ is expressed in degrees and fraction of it.

We have found for the differential coefficients:

$$\frac{d^{3}Z}{dt^{3}} = -\frac{dZ}{dt} \left[1+3 \cot Z \frac{d^{2}Z}{dt^{2}} - \left(\frac{dZ}{dt}\right)^{2}\right]$$
(5)

and

$$\frac{d^2 Z}{dt^2} = \frac{\cos Z(\sin^2 \phi + \sin^2 \delta) - \sin \phi \sin^2 (1 + \cos^2 Z)}{\sin^3 Z} .$$
(6)

Inserting equation (5) into equation (4) we get

$$\frac{z_2^{-2}}{\theta_2^{-\theta_1}} = \frac{dz}{dt} \left\{ 1 - \frac{1}{24} \left(\frac{\tau(\theta_2^{-\theta_1})^0}{180} \right)^2 \left(1 + 3 \cot z \frac{d^2 z}{dt^2} - \left(\frac{dz}{dt} \right)^2 \right) \right\} . (7)$$

In this equation for the zenith distance we use for Z the value which results from

$$Z = \frac{Z_1 + Z_2}{2} - \frac{1}{g} \frac{\pi}{180} \left(\theta_2 - \theta_1\right)^2 \frac{d^2 Z}{dt^2}.$$
 (8)

Expressing $(\theta_2 - \theta_1)$ in degrees and fractions of it, we have

$$z = \frac{z_1 + z_2}{2} - 7, 85 \ (\theta_2 - \theta_1)^2 \frac{d^2 z}{dt^2} . \tag{9}$$

The differential coefficient $\frac{d^2z}{dt^2}$ is very small, zero at the maximum elongation, so we can compute it from equation (5) using

$$z = \frac{z_{1}+z_{2}}{2}$$
.

For abbreviation let .

$$P = \frac{1}{24} \left[\frac{\pi}{180} \left(\theta_2 - \theta_1 \right)^0 \right]^2$$

$$Q = 1 + 3 + z \frac{d^2 z}{dt^2},$$
(10)

so equation (6) is rewritten as follows:

$$\frac{Z_{z}-Z_{z}}{\theta_{z}-\theta_{1}} = \frac{dZ}{dt} \left[1 - P\left(Q_{z}-\left(\frac{dZ}{dt}\right)^{2}\right)\right], \qquad (11)$$

and because of the size of P, we use the approximate value

$$\frac{dZ}{dt} = \frac{Z_2 - Z_1}{\theta_2 - \theta_1} \left(\frac{1}{1 - P[Q - (Z_2 - Z_1)^2 / (\theta_2 - \theta_1)^2]} \right), \quad (12)$$

in the brakets of equation (11), and derive the true value of the differential coefficient $\frac{dZ}{dt}$.

Solution for Any Number of Observations

Let

-1

Consider a set of observations made with a theodolite in a direct position, and a second set with a theodolite in reverse position.

i = number of observations in direct position j = number of observations in reverse position θ_1, Z_1 = time and zenith distance in direct position θ_j, Z_j = time and zenith distance in reverse position θ_0, Z_0 = a reference time and zenith distance $\tau_1 = \theta_1 - \theta_0$ $\tau_j = \theta_j - \theta_0$

Two sets of equations can be formed where the differential coefficients refers to the time θ_0 as follows:

$$\mathcal{L}_{i} = Z_{i} - Z_{0} = \frac{dZ}{dt} \tau_{i} + \frac{1}{2} \frac{d^{2}Z}{dt^{2}} \tau_{i}^{2} + \frac{1}{6} \frac{d^{3}Z}{dt^{3}} \tau_{i}^{3} + \cdots$$

$$\mathcal{L}_{z}_{j} = Z_{j} - Z_{0} = \frac{dZ}{dt} \tau_{j} + \frac{1}{2} \frac{d^{2}Z}{dt^{2}} \tau_{j}^{2} + \frac{1}{6} \frac{d^{3}Z}{dt^{3}} \tau_{j}^{3} + \cdots$$
(13)

We eliminate the second differential coefficient by postulating that

$$\sum \tau_{1}^{2} - \sum \tau_{1}^{2} = 0.$$
 (14)

Consider an equal number of observations in each set, that is

i = j = n.

From the sum of each set, we obtain by substraction of eduation (13):

$$\left[\Delta z_{j} - \sum \Delta z_{i} = \frac{dz}{dt} \left(\sum \tau_{j} - \sum \tau_{i} \right) + \frac{1}{6} \frac{d^{3}z}{dt^{3}} \left(\sum \tau_{j}^{3} - \sum \tau_{i}^{3} \right) . \quad (15)$$

To satisfy equation (14) the value of θ_0 must be known. To obtain it we proceed as follows:

Let $\overline{\theta}_0$ be an approximate value of θ_0 . We may select the mean value between the last observation of the first set and the first of the second set, so $\theta_{\pm 0}$

$$\bar{\theta}_{0} = \frac{\theta_{n} + \theta_{1}}{2} , \qquad (16)$$

and let x be the amount of correction to obtain θ_{o} , therefore

$$\theta_0 = \overline{\theta}_0 + \mathbf{x}$$
 (17)

from which equation (13) becomes

$$[(\theta_{j}-\overline{\theta}_{o})^{2}-[(\theta_{i}-\overline{\theta}_{o})-2 \times [[(\theta_{j}-\overline{\theta}_{o})-[(\theta_{i}-\overline{\theta}_{o})]=0$$
(18)

and x is computed from

$$\mathbf{x} = \frac{\sum (\mathbf{\theta}_{1} - \mathbf{\overline{\theta}}_{0})^{2} - \sum (\mathbf{\theta}_{1} - \mathbf{\overline{\theta}}_{0})^{2}}{2\left[\sum (\mathbf{\theta}_{1} - \mathbf{\overline{\theta}}_{0}) - \sum (\mathbf{\theta}_{1} - \mathbf{\overline{\theta}}_{0})\right]}.$$
 (19)

Adding this value of x to $\overline{\theta}_0$, we obtain the desired value θ_0 . The M2's are computed according to equation (2).

Evaluation of the Second Differential Equation d^2Z/dt^2 .

Consider the total number of observations of each group to be

 $i = j = 1, 2 \dots, n$.

For the sum of each group of equations (13), two equations are fixed as follows:

$$\frac{\sum (z_1 - z_0)}{\tau_1} = n \frac{dz}{dt} + \frac{1}{2} \frac{d^2 z}{dt^2} \sum \tau_1 + \frac{1}{6} \frac{d^3 z}{dt^3} \sum \tau_1^2$$
(20)
$$\sum \frac{(z_1 - z_0)}{\tau_1} = n \frac{dz}{dt} + \frac{1}{2} \frac{d^2 z}{dt^2} \sum \tau_1 + \frac{1}{6} \frac{d^3 z}{dt^3} \sum \tau_1^2.$$

Under the condition established in equation (14) we obtain for the second differential equation

$$\frac{1}{2} \frac{d^{2}z}{dt^{2}} = \left[\frac{\sum_{i=1}^{2} (z_{i} - z_{o})}{\tau_{i}} - \frac{\sum_{i=1}^{2} (z_{i} - z_{o})}{\tau_{i}} \right] \frac{180}{(\sum_{i=1}^{2} (z_{i} - \sum_{i=1}^{2} z_{i}))^{2}} .$$
 (21)

Let the parameters M and N be defined as follows:

$$M = \frac{1}{n} \sum_{i=1}^{n} \frac{z_i^{(z_i - z_o)}}{\tau_i}$$

(22)

$$N = \frac{1}{n} \sum_{j=1}^{n} \frac{(z_j - z_o)}{\tau_j}.$$

Adding the two equations (15), dividing by n and on account of equation (17) we obtain

$$\frac{M+N}{2} = \frac{dZ}{dt} + \frac{1}{4n} \frac{d^2Z}{dt^2} \left[(\tau_j + \tau_i) + \frac{1}{12n} \frac{d^3Z}{dt^3} \left(\sum_{\tau_j} \tau_j^2 + \sum_{\tau_i} \tau_i^2 \right) \right].$$
(23)

The second term in the left hand of this equation is very small and the thrid term will also be small. To evaluate the first differential we must evaluate the third coefficient, which we found is

$$\frac{d^{3}Z}{dt^{3}} = -\frac{dZ}{dt} \left[1+3 \cot Z \frac{d^{2}Z}{dt^{2}} - \left(\frac{dZ}{dt}\right)^{2} \right] .$$
(24)

Let

$$C = \frac{1}{4n} \frac{d^2 z}{dt^2} \sum_{i} (\tau_j + \tau_i)^o \frac{\pi}{180}$$
(25)

in which the $\tau's$ are expressed in degrees and fractions of it, and let

$$P = 1 + 3 \cot 2 \frac{d^2 z}{dt^2}$$
 (26)
 $Q = \frac{M+N}{2} - C$,

where d^2Z/dt^2 is derived from equation (16). Inserting these values into equation (18) we obtain for evaluating the first differential equation:

$$\frac{dZ}{dt} = \frac{Q}{1 - \frac{1}{6} (P - Q^2) \sum (\tau_i^2 + \tau_i^2) (\frac{\pi}{180})^2} .$$
 (27)

Evaluation of Latitude and Azimuth

a **F**h

Two procedures can be used, as follows:

Procedure 1. Latitude can be computed through the equation:

 $\sin \phi = \cos Z \sin \phi \pm \sin Z \sqrt{\cos^2 \phi - (dZ/dt)^2}$. (28)

The plus sign is used when the star's azimuth increases, otherwise it is negative. The value of $\rm Z_m$ is derived as follows:

Let Z_i be the zenith distances of the first set and Z_j those of the second set. Let R_i and R_j be their corrections due to refraction errors and let ε be the index error and P the observer personal equation. The first set gives:

$$Z_{i} = \overline{Z}_{i} + R_{i} + (\varepsilon + P)$$
(29)

The second set gives:

$$z_{j} = \overline{z}_{j} + R_{j} - (\varepsilon + P)$$
(30)

The \vec{z} means observed values. The value of Z_m is obtained by adding to each Z_i the computed value ΔZ_i or ΔZ_j , we get

$$n Z_{m} = \sum (\overline{Z}_{i} + \Delta Z_{i}) + \sum R_{i} + n(\varepsilon + P)$$

$$n Z_{m} = \sum (\overline{Z}_{j} + \Delta Z_{j}) + \sum R_{j} - n(\varepsilon + P)$$
(31)

from which we obtain

$$z_{m} = \frac{1}{2n} \left[\sum (\overline{z}_{i} + \Delta z_{i}) + \sum (z_{j} + \Delta z_{j}) + \sum (R_{i} + \sum R_{j}) \right]. \quad (32)$$

After the latitude has been obtained from equation (28), the azimuth, which is for the time θ_0 , is obtained from i

$$\sin A = \frac{dZ}{dt} \sec \phi . \tag{33}$$

<u>Procedure 2.</u> By observing a second star on the other side of the meridian the azimuth is determined independently of the latitude.

Let

$$W = \left(\frac{dZ}{dt}\right)_{W}$$
 the rate of the west star
$$E = \left(\frac{dZ}{dt}\right)_{e}$$
 the rate of the east star
$$L_{u}, L_{e} =$$
 theodolite horizontal readings

The azimuth is derived from

÷.

$$\tan \frac{1}{2} \left(A_{u} + A_{e} \right) = \frac{u + e}{u - e} \tan \frac{1}{2} \left(L_{u} - L_{e} \right) . \tag{34}$$

Let

$$\frac{V_2 (A_w + A_w)}{V_2 (L_w - L_w)} = x$$
(35)

then the star's azimuth are

$$\begin{array}{l} A_w = x + y \\ A_e = x - y \end{array}$$
(36)

Star's Hour Angle

The star's hour angle t, is computed using the equation:

$$\tan t = \frac{dZ/dt}{A-B \sin \delta}, \qquad (37)$$

when the denominator (absolute value) is greater than the numerator, otherwise from

$$\tan \gamma = \frac{A-B \sin \circ}{dZ/dt},$$
$$t = 90^{\circ} \gamma.$$

The meanings of A and B are:

$$A = \cos^{2} \delta \cot Z$$

$$B = \pm \sqrt{\cos^{2} \delta - (dZ/dt)^{2}}$$
(38)

where the positive sign corresponds when the star's azimuth (horizontal readings) increases and negative when it decreases.

COLLIMATION CONSTANT AND ITS EVALUATION FROM A STAR OBSERVATION

The line of sight of the instrument is in general not perpendicular to the horizontal axis of the instrument, but forms an angle with it of $90^{\circ}+c$ where c is a quantity called collimation to be evaluated. Consider a diagram of a theodolite as shown in Figure 1. Let C represent the center of the horizontal circle. Let NS be the meridian line through C. Let the telescope be pointed to the star A, and let CA' be its horizontal projection. This direction CA' has a reading L_g in the horizontal circle. Let B₀ be the origin of the horizontal scale reading of the theodolite and let B₁ be its symmetrical point. Then the angle formed by the line B₀CB₁ with respect to the meridian line NCS is the azimuth of B₀B₁, that is SCB₀. Let this angle be represented by β , so the car's szimuth A_g, is A_g = L_g + β which represents the value when no collimation exists but always a small collimation error exists so we must add to L_g a value δA . This correction is well known, therefore the star's szimith is:

$$A_{g} = L_{g} + \beta \pm c \operatorname{cosec} Z \qquad (39)$$

where the plus sign is assumed when the theodolite is in a direct position and negative sign when the instrument is in reverse position.





The collimation can be determined by selecting any terrestrial object that presents some well defined point, and at a far distance so that the stellar focus of the telescope need not be changed to obtain a good definition of the point. From the horizontal readings of the theodolite in a direct and a reverse position the collimation can be obtained. But it appears that this collimation should not be the same when it is derived from a star's observations. We think that it is more appropriate to obtain the collimation constant by observing a moving object, a star, which is related to the observer's behavior in observing the stars for latitude and longitude determination. Instead of a distant terrestrial point, we substitute it by choosing a circumpolar star. The rate of change of azimuth as function of time is used to evaluate the collimation constant. The star is observed a number of times in a direct and reverse instrument position. The time when the star image crosses the central vertical wire is recorded as well as the horizontal readings of the theodolite. Let L_1 be the horizontal scale readings and T_1 be the corresponding times for a direct instrument position and L_j , T_j the values that corresponds to the reverse instrument position, where

i, j = 1, 2, 3,...n .

Let T_0 be an arbitrary time chosen between the two sets of observations, and let us reduce all observations, to the time T_0 through the Taylor's theorem, expressing all quantities in radiances and omitting the terms higher than the third. The amount AA_i to be added to each L_i to reduce it to the value that would correspond to the time T_o , is

$$\Delta A_{i} = \frac{\partial A}{\partial t} \sigma_{i} + \frac{1}{2} \frac{\partial^{2} A}{\partial t^{2}} \sigma_{i}^{2} + \frac{1}{6} \frac{\partial^{3} A}{\partial t^{3}} \sigma_{i}^{3} \qquad (40)$$

where

$$\sigma_i = T_i - T_o$$

The amount ΔA_j to be added to the readings L_j , to reduce them also to the time T_o , is

$$\Delta A_{j} = \frac{dA}{dt} \sigma_{j} + \frac{1}{2} \frac{d^{2}A}{dt^{2}} \sigma_{j}^{2} + \frac{1}{6} \frac{d^{3}A}{dt^{3}} \sigma_{j}^{3} \qquad (41)$$

$$\sigma_j = T_j - T_0$$

The star's azimuth to the time ${\rm T}_{\rm O}$ is

$$A_{g} = L_{i} + \beta + \Delta A_{i} + c \operatorname{cosec} Z_{i}$$

$$A_{z} = L_{z} + \beta + 180 + \Delta A_{z} - c \operatorname{cosec} Z_{i}$$

$$(42)$$

and

from which the collimation error results as

$$c = \frac{L_j + 180 - L_i + \Delta A_j - \Delta A_i}{\operatorname{cosec} Z_i + \operatorname{cosec} Z_i}.$$
 (43)

We do not give a detailed derivation of Taylor's coefficients, which are to be used in equations (33) and (34), and give only its final results. We find that such coefficients can be evaluated from:

$$\frac{dZ}{dt} = \pm \operatorname{cosec} Z \sqrt{2} \cos Z \sin \delta \sin \phi + \sin^2 Z - \sin^2 \phi - \sin^2 \delta - E$$
(44)

$$\frac{d^2 z}{dt^2} = \cot Z \left[1 - \left(\frac{d z}{dt} \right)^2 \right] = \sin \phi \sin \delta \csc \delta Z \quad (45)$$

$$\frac{dA}{dt} = \frac{\sin \phi - \cos z \sin^{\delta}}{\sin^2 z}$$
(46)

$$\frac{d^2 A}{dt^2} = \left(\sin \delta - 2 \frac{dA}{dt} \cos z\right) \frac{dZ}{dt} \operatorname{cosec} Z \qquad (47)$$

$$\frac{d^{3}A}{dt^{3}} = \frac{d^{2}z}{dt^{2}} \left(\frac{\sin \phi}{\sin z} - 2 \cot z \frac{dA}{dt} \right) + 2 \left(\frac{dz}{dt} \right)^{2} \frac{dA}{dt} - 3 \cot z \frac{dZ}{dt} \frac{d^{2}A}{dt^{2}}$$
(48)

EXAMPLES OF COMPUTATION

To illustrate the process of reduction using the technique shown in this report we consider the following observations taken on February 22, 1955, in a place:

 $\lambda = 6^{h}47^{m}45.91$ West

 $\phi = 26^{\circ}37'22''$ South

with a theodolite Zeiss 1". The time was noted by a sidereal clock whose rate was so small as not to require notice. The Star's apparent place, α Pictoris, is:

$$\alpha = 6^{n}47^{m}45.91$$

$$5 = -61^{\circ}53'50".8$$

Tables 2 and 3 show: first column the sidereal time of observation; second column the zenith distance after correction for refraction; the third column are the horizontal readings. The Taylor's coefficients shown on each table were computed according to equations (37) through (41), from which the corrections I, II and III were made to reduce each observation to the chosen time T_0 , according to equations (33) and (34). The last column indicates the reduced azimuth with the plus or minus of collimation coefficient according to the instrument position. The collimation was computed according to equation (36). The resulting value is C = 7"83.

Table 4 shows the reduced zenith angles to a common time T_0 . The first column indicates the number of observations for the direct and reverse instrument position. The second gives the values of $(Z - Z_0)$ computed according to equation (2). The third dolumn gives the reduced zenith angles from direct observations and in column four from reverse instrument position. From the mean values of these two columns the index error was computed which was used to compute the final zenith angle reduced to the time T_0 .

| 1 | 2 | 3 | | | | 4 | 5 = 3-4+C co se u Z |
|---|--|--|--|---|--|---|---|
| Sidereal Time | Zenith Angle | Horizontal Angle | Cc | orrectio II | ns III | 1+11+111 | Reduced Azimuth to To = 11 ^h 55 m 0836 |
| 11 ^h 49 ^m 06 ⁵ 4 50 36.6 51.05.2 51 34.6 52 51.9 53 20.2 54 24.5 11 55 08.6 | 60°02'15" 12 54 16 15 19 41 28 35 28 89 32 10 39 43 60 44 55 | 31046 31" 46 16 45 10 46 03 45 52 45 43 45 75 45 15 31 45 02 | 2.02:03 1.31.64 1.22.03 1.12.10 0.58.15 0.46.06 0.36.52 1.14.86 0. | -33"20 -18.72 -14.99 -11.59 -7.54 -4.72 -2.97 -0.49 0 | -0723 -0.10 -0.07 -0.05 -0.02 -0.01 -0.01 0 | 1 2876 1 12.8 1 06.9 1 00.5 0 50.6 0 41.3 0 33.5 0 14.4 0 | 31 ⁰ 45'274+1,1540 3.2+1,152 3.2+1,152 2.5+1,151 1.4+1,150 1.7+1,150 0.5+1,147 2.5+1,147 2.5+1,147 |
| $12^{h}04^{m}26^{3}0$ $12^{o}0738.529$ dA/dt = -0.4 $d^{2}A/dt^{2} = -0.4$ | 022×6 •6399 | 31°45'02.0 31 45 02.0 | -3'07"80- -4 12.66- | 1 ' 18763 2 22 : 32 | 0784 2.04 12/dt 1 ² 2/dt ² | -u · 25.59 -6 ³ 3.0 = 0.4706 = 0.0170 | 31°45'02*0+1,1500 31°40'36741+1,1500 31'36'29.06+1,1500 31'36'29.06+1,1500 |

Table 2. Telescope Direct Position.

r -

Table 3. Telescope Reverse Position

| 1 | 2 | 3 | | | 4 | 5 x 3-4+ | C cosec Z |
|-----------------------|----------|--------------|------------|------------|---------|------------|---|
| Sidereal | Zenith | Horizontal | c | orrectio | ns | | Reduced Azimuth 12 |
| Time | Angle | Angle | I | 11 | 111 | I+II+III | to = 12 ^h 94 ^m 2€‡5 |
| 12h04=2650 | 61050140 | 211080-54* | 0 | 0 | | 0 | 211040-54 (-1.134) |
| 5 42.8 | 61 59 40 | 40 06 | -47 .20 | -1745 | ō | -48.6 | 54.5-1.173 |
| 6 37.6 | 62 06 05 | 39 28 | -1 20.87 | -4.24 | 0.01 | -1 25.1 | 53.1-1.132 |
| 7 23.7 | 62 11 30 | 38 56 | -1 49.21 | -7.74 | 0.02 | -1 56.9 | 52.9-1.131 |
| 7 58.9 | 62 15 37 | 18 33 | -2 10.84 | -11.11 | 0.04 | -2 21.9 | 54.9-1,130 |
| 6 28.8 | 62 19 08 | 38 11 | -2 29.21 | - 14 . 45 | 0.06 | -2 43.6 | 54.6-1.129 |
| 9 00.0 | 62 23 40 | 37 41 | -2 33.0/ | -19.57 | 0.10 | -3 13.1 | 54.1-1.126 |
| 12 10 35.6 | 62 24 00 | 211 36 34 | -3 47.14 | -33.48 | 0.10 | -1 20 4 | 211 40 54 4-1 127 |
| | | | | 37.00 | | | |
| | | | | | | | 211-40-54027-1.1300 |
| 11 55 08.6 | | 211040-54727 | 5 82.55 | 1 16.14 | -0.77 | -#125.564 | 211046-10491-1 1300 |
| 12 07 38.529 | | 211 40 54.27 | -1 58.32 | -9.08 | 0.03 | -2 07.37 | 211 38 46.90-1.1300 |
| | | | Collinson | | | | |
| | | Direct | COLLIMACI | .on Rev | erse | | |
| | | | | | | | |
| 11-55-08-6 | | 31~45'02704+ | 1.1150 = 2 | 11 45 19 | 191-1 | 30-1,1130C | C = 7784 |
| 12 04 20.0 | | 31 40 50.41+ | 1.1150 2.2 | 11 40 54 | 27-18 | 0-1.130C | C = 7.53 |
| 12 01 30.33 | · | 31 30 29.00+ | 1.1190 1.2 | 11 30 40 | . 40-10 | 0-1. 130C | |
| dA/dt = -0.0 | 04097 | | | đ | Z/dt | # 0.469 | 66 |
| 2 | | | | | 27 | | |
| • ***** I =0.* | ***) (| | | | 1-7\df. | · = -0.041 | • 7 |
| $d^3A/dt^3 = 0.3$ | 33525 | | | | | | |

Table 4. Reduced Zenith Angles to $T_0 = 11^h 55^m 08.6$.

| ΔΖ. | DIRECT $Z + \Delta Z + \epsilon$ | $\begin{array}{r} \text{REVERSE} \\ \text{Z} - \Delta \text{Z} - \epsilon \end{array}$ | zo |
|------------|---|--|-------------------------|
| 0°42′37"8 | 60°44′52"8 | | 60°44′59.5 |
| 32 00.7 | 54.7 | • | 61.4 |
| 28 38.7 | 53.7 | | 60.4 |
| 25 11.0 | 52.0 | | 58.7 |
| 20 18.7 | 53.7 | | 60.4 |
| 16 05.2 | 54.2 | | 60.9 |
| 12 45.3 | 55.3 | | 62.0 |
| 5 11.3 | 54.3 | | 61.0 |
| 0 0 0 | 60 44 55.0 | | 61.7 |
| -1006-3144 | | 60 ⁰ 45'8"7 | 62.0 |
| -1 14 32.3 | | 7.7 | 61.0 |
| -1 20 58.0 | | 7.0 | 60.3 |
| -1 26 22.5 | | 7.5 | 60.8 |
| -1 30 30.4 | | 6.6 | 59.9 |
| -1 34 00.7 | | 7.3 | 60.6 |
| -1 38 40.7 | | 7.3 | 60.6 |
| -1 44 17.7 | | 7.3 | 60.6 |
| -1 48 52.7 | | 60 45 7.3 | 60 44 60.6 |
| — | 60 ⁰ 44′ 53"97 | 60 ⁰ 45′7"38 | 60 ⁰ 45'00"7 |
| | 60 [°] 44′53"97 53.97 + £ = 6 | 60 ⁰ 4517"38 7"38 - E | 60°4510 |

53.97 + 5 = 6.70 5 = 6.70

Further sample calculations, not presented here because of space limitations, are available from the author upon request.

