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OPTICAL PROPERTIES OF NATURAL MINERALS AND OTHER MATERIALS IN THE 350-50,000 CM<sup>-1</sup> SPECTRAL

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FINAL REPORT MARVIN R. QUERRY, Ph.D. AUGUST 1983

U.S. ARMY RESEARCH OFFICE CONTRACT NUMBER DAAG-29-79-C0131

DEPARTMENT OF PHYSICS UNIVERSITY OF MISSOURI-KANSAS CITY

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of gypsum. A method was developed for obtaining complex refractive indices from reflectance spectra of the pellets and transmittance spectra of the powder/KBr pellet. The best specularly reflecting pellets were formed from powders of smaller particle size and with forces of from 14 to 16 tons on the 13 mm dia circular face of the pellet.

The complex refractive indices of water were also updated by applying Kramers-Kronig methods to a new composite k spectrum in order to determine the n spectrum.



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#### ABSTRACT

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Reflectance spectra were measured in the UV, VIS, and/or IR for several natural minerals and for several aqueous solutions of  $ZnCL_2$  and  $H_3FO_4$ . Complex refractive indices were determined for most of these materials by applying Kramers-Kronig methods to the reflectance spectra. Powders of some of the natural minerals were pressed in to pellets in order to obtain the reflectance spectra. Gypsum was studied in the crystalline form, the powder-pellet form, and by transmittance spectra through KBr pellets containing minute quantities of gypsum. A method was developed for obtaining complex refractive indices from reflectance spectra of the pellets and transmittance spectra of the powder/KBr pellet. The best specularly reflecting pellets were formed from powders of smaller particle size and with forces of from 14 to 16 tons on the 13 mm dia. circular face of the pellet.

The complex refractive indices of water were also updated by applying Kramers-Kronig methods to a new composite k spectrum in order to determine the n spectrum.

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#### I. Statement of Research Problem

Research conducted during the term of this contract was measurement of reflectance spectra R(v) in the uv, visible, and/or infrared for selected liquids and solids; computational analysis of the measured spectra to obtain spectral values of the complex refractive indices N(v) = n(v)+ik(v) of those materials, and further analysis of the spectra in terms of fundamental intra- and inter-molecular vibrational modes.

#### II. Summary of Most Important Results

The most significant accomplishments of this project were determination of spectral values of N(v) of natural and man made aerosol/obscurant materials and providing these values of N(v) to scientists at the Aberdeen Proving Ground, Md. We determined and sent to the Aberdeen Proving Ground values of N(v) for the materials listed in Tab es I-III. Tabulations of these values of N(v) can be obtained from Aerosol/Obscuration Sciences, DRDAR-CLB-PS, Aberdeen Proving Ground, Md. 21010.

Current knowledge of the manner in which electromagnetic radiation propagates through aerosol clouds is based primarily on Mie-scattering computations. Such computations are possible only when there is prior knowledge of N(v) for the aerosol. The values of N(v) obtained during the term of this contract are now used for Mie-scattering computations by scientists at several U.S. Army Laboratories and by many DOD contractors.

TABLE I. Materials for which reflectance spectra R(v) and complex refractive indices N(v) were obtained during the term of contract DAAG-29-79-C-0131.

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Material	Form	Spectral Region	Spectral Region
Gypsum X	Crystal (010)	0.2 - 55 µm	2.5 - 52 µm
Gypsum Y	Crystal	0.2 - 55	2.5 - 52
Gypsum Z	Crystal (010)	0.2 - 55	2.5 - 52
Biotite A	Crystal (010)	2 <b>.</b> 5 <b>-</b> 55	2.5 - 33
<b>Biotite</b> B	Crystal (100)	2.5 - 55	2.5 - 33
Biotite C	Crystal (010)	2.5 - 55	2.5 - 28
Rutile O	Crystal	2.5 - 55	2.5 - 55
Philogopite A	Crystal (001)	2.5 - 55	-
Philogopite B	Crystal (001)	2.5 - 55	-
Philogopite C	Crystal (100)	0.25 - 55	2.5 - 25
Muscovite A	Crystal (001)	2.5 - 55	-
Muscovite B	Crystal (001)	2.5 - 55	-
Muscovite C	Crystal (010)	2.5 - 55	2.5 - 25
Calcite O	Crystal	2.5 - 55	2.5 - 54
Calcite E	Crystal	2.5 - 55	-
Gypsum	Pellet 8T	0.2 - 55	2 <b>.</b> 5 <b>-</b> 52
Montmorillonite	Pellet 8T	2.5 - 55	2.5 - 55
Ga. Limonite	Pellet 8T	0.2 - 55	-
Al. Limonite	Pellet 8T	0.2 - 55	0.2 - 54
Kaolin	Pellet 8T	0.2 - 55	0.25 - 54
Illite	Pellet 8T	0.2 - 55	0.20 - 54
Colemanite	Pellet 8T	0.2 - 55	0.21 - 43.8
Pyrolusite	Pellet 8T	0.2 - 55	0.2 - 54
Kernite	Pellet 8T	0.2 - 55	0.32 - 54
Cn. Vermiculite	Pellet 3T	2.5 - 55	-
Id. Vermiculite	Pellet 3T	2.5 - 55	• •
Wavellite	Pellet 8T	0.2 - 55	0.3 - 54
Chalcedony	Solid	0.2 - 55	
Diesel Fuel	Liquid	2.5 - 55	2.5 - 55
20% ZnC 2/H20	Liquid	0.2 - 2.0	0.2 - 2
30% ZnC 2/H20	Liquid	0.2 - 2.0	0.2 - 2
50% ZnC 2/H20	Liquid	0.2 - 2.0	0.2 - 2
05) ZnC 2/H20	Liquid	0.2 - 2.0	0.2 - 2
75% Znc 2/H20	Liquid	0.2 - 2.0	0.2 - 2
5% H <sub>3</sub> PU <sub>4</sub> /H <sub>2</sub> U	Liquid	0.2 - 2.0	0.2 - 2
10% H <sub>3</sub> P04/H <sub>2</sub> 0	Liquid	0.2 - 2.0	0.2 - 2
207 n3r04/H20	Liquid	0.2 - 2.0	0.2 - 2
40% H <sub>3</sub> PO <sub>4</sub> /H <sub>2</sub> O	Liquid	0.2 - 2.0	0.2 - 2
50% H <sub>3</sub> PO <sub>4</sub> /H <sub>2</sub> O	Liquid	0.2 - 2.0	0.2 - 2
65% H <sub>3</sub> PO <sub>4</sub> /H <sub>2</sub> O	Liquid	0.2 - 2.0	0.2 - 2
75% H3PO4/H20	Liquid	0.2 - 2.0	0.2 - 2
85\$ H <sub>3</sub> PO4/H <sub>2</sub> O	Liquid	0.2 - 2.0	0.2 - 2
Water	Liquid		

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TABLE II.	Mineral S	pecimens	used	during	this	Investigation
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Mineral	Source	Cat. No.
Gypsum	R. Coveney	
Biotite	R. Coveney	
Pholgopite	R. Coveney	
Muscovite	R. Coveney	
Calcite	R. Coveney	
Montmorillonite	#Ward's (Wyomming)	46W 0439 LS
Limonite	Ward's (Alabama)	46W 4684 LS
Kaolin	Ward's (Georgia)	46w 4334 LS
Illite	Ward's (N.Y.)	46W 0319 LS
Colemanite	Ward's (California)	46W 2144 LS
Pyrolusite	Ward's (Brazil)	64W 6424 LS
Kernite	Ward's (California)	46W 4364 LS
Vermiculite	Ward's (CN & Idaho)	46W 0829 LS
Wavellite	Ward's (Arkansas)	46W 8724 LS
Chalcedony	Ward's (California)	46W 0050 LS

\*Wards Natural Science Establishment, Inc.

P.O. Box 1712, Rochester, NY 14603

# TABLE III. Chemical composition of natural minerals investigated during the period of this project

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Mineral	Composition	Structure
Gypsum	Ca SO <sub>4</sub> . 2H <sub>2</sub> O	Monoclinic
Biotite	$K(Mg, Fe^{2+})_{3-1.5}(A, Fe^{3+})_{0-1}$	Monoclinic
	(OH,F)2/Al1-1.5 <sup>S1</sup> 3-2.5 <sup>0</sup> 10	
Pholgopite	K Mg <sub>3</sub> (OH,F) <sub>2</sub> /AlSi <sub>3</sub> 0 <sub>10</sub>	Monoclinic
Muscovite	K Al2[(OH)2/ALS13010]	Monoclinic
Calcite	Ca CO <sub>3</sub>	Trigonal
Montmorillonite	$Al_{1.67}Mg_{0.33}[(OH)_2/Si_4O_{10}Na_{0.33}(H_2O)_4]$	Monoclinic
Limonite	Fe0.0H.nH20	Amorphous
Kaolin	A <sup>2</sup> 4S14010(OH)8	Triclinic
Illite	hydromuscovite	
Colemanite	Ca[B <sub>3</sub> 0 <sub>4</sub> (OH) <sub>3</sub> ].H <sub>2</sub> O	Monoclinic
Pyrolusite	Mn <sup>0</sup> 2	Tetragonal
Kernite	$Na_{2}[B_{4}O_{6}(OH)_{2}].3H_{2}O$	Monoclinic
Vermiculite	$(Mg, Fe^{3+}, Al)_{3}[(OH)_{2}/Al_{>1}Si_{3}O_{10}].$	Monoclinic
	Mg0.33 <sup>(H20)</sup> 4	
Wavelength	Al <sub>3</sub> [(OH) <sub>3</sub> /(PO <sub>4</sub> ) <sub>2</sub> ].5H <sub>2</sub> O	Orthorombic
Chalcedony	Fibrous Low quartz	

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#### III. Publications

- M. R. Querry, "Complex refractive indices of selected materials in the infrared," Proceedings of the 1979 CSL Scientific Conference on Obscuration and Aerosol Research," Dec 1980, pp. 363-374.
  M. R. Querry, "Complex refractive indices of selected materials in the infrared," Proceedings of the 1980 CSL Scientific Conference on Obscuration and Aerosol Research," In Press, Proceedings have not been released.
- M. R. Querry, "Complex refractive indices of Liquids & Powders," Proceedings of the 1981 CSL Scientific Conference on Obscuration and Aerosol Research, In Press, Proceedings have not been released.

M. R. Querry & "Optical Properties of Gypsum," Proceedings of

- R. L. Strecker, The 1982 CSL Scientific Conference on Obscuration and Aerosol Research, In Press, Proceedings have not been released.
- D. J. Segelstein, "The Complex refractive index of Water," M.S. Thesis, University of Missouri-K.C., 1981, 167 pages.
- R. L. Strecker, Infrared optical properties of gypsum, "M.S. Thesis, University of Missouri-K.C., 1982, 83 pages.

# IV. Personnel Employed on the Project

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Name	Position	Degrees Received	
Marvin R. Querry, Ph.D.	Principal Investigator	None	
Raymond Coveney, Jr., Ph.D.	Mineralogist	None	
Terrence Heese, B.S.	Research Assistant	None	
Thomas Hogan, B.S.	Grad. Research Assistant	M.S.	
David Segelstein, B.S.	Grad. Research Assistant	M.S.	
Richard Strecker, B.S.	Grad. Research Assistant	M.S.	
Jan Ben,	Undergraduate Assistant	None	

#### V. <u>Report of Research</u>

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#### A. Experimental Methods

One purpose of the research conducted during the term of DAAG-29-79-C-0131 was to measure the reflectance spectra of selected liquids, crystals, and powdered materials which were pressed into pellets. In this section we present the methods for measuring reflectance spectra.

#### 1. Methods for Acquiring Reflectance Spectra of Aqueous Solutions

Reflectance spectra of aqueous solutions of  $ZnCl_2$  and  $H_3PO_4$ were measured in the 0.2 - 2  $\mu$ m wavelength region. This constituted an extension of our previous investigations of the reflectance spectra of those solutions in the infrared region.

A block diagram of the reflectometer and data acquisition system used to measure the reflectance spectra of the aqueous solutions is shown in Fig. A1. Radiant flux from a light source G was chopped at C and was then focussed by an f/5 optical system, consisting of plane mirror M, and spherical mirror M<sub>2</sub> on the surface of the sample S. The angle of incidence  $\theta$  was 6.2 degrees for the central ray from M<sub>2</sub> incident on the surface S. Radiant flux reflected from S was imaged by an identical optical system (M<sub>3</sub> and M<sub>4</sub>) on the entrance slit of a Perkin-Elmer Ebert double-pass grating monochromator. The entrance slits were manually adjusted to assure spectral resolution  $\nu/\Delta\nu$  of 100 or better. After passage through the monochromator, the radiant flux was optically filtered to remove higher diffraction orders,



and was then focussed on either a InSb or photomultiplier detector. The signal from the detector was synchronously processed by a Princeton Applied Research (PAR) model 124 lockin amplifier. The analog output signal from the Model 124 was applied to the input of a PAR model 260 analog-to-digital converter (ADC) which both digitized the signal and inserted an index corresponding to the spectral position of the monochromator.

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In order to facilitate data acquisition and analysis the system described above was interfaced to a Hewlett-Packard (HP) Model 9820A programmable calculator equipped with an HP 9862A plotter and an HP11223A magnetic cassette tape unit. This entire system was then interfaced through a decwriter LA-36 terminal to either an Amdahl 470 or VAX 11/780 computer which was used for the subsequent Kramers-Kronig analysis of the reflectance data.

During this investigation of the liquids we measured relative specular reflectance  $R(v) = R_s(v)/R_w(v)$ , where s denotes the sample and w denotes the water standard. Prior to use the water standard was purified, deionized, and filtered through a 0.2 µm Millipore filter. Aqueous solutions were prepared using purified water and reagent grade chemicals. The aqueous solutions and purified water were placed in separate petri dishes which served as sample holders. Each dish was filled to precisely the same level as determined by use of a cathetometer. The levels of all samples were monitored

routinely during data collection and purified water was added to the samples as needed to compensate for evaporation. Each sample was also stirred thoroughly at the beginning of a spectral scan to assure isotropic homogeneity. Data were acquired at 200 equally spaced wavelength positions in each of the wavelength regions 0.2-0.3, 0.3-0.4, 0.4-0.6, 0.6-0.8, 0.8-1.0, 1.0-1.5, and  $1.5-2 \mu m$ .

All spectra were obtained with the samples at about  $27^{\circ}$ C. The reflectance spectra R(v) were converted from wavelength to wave number and then plotted either by the HP9862A, a Tektronix graphics terminal, or by a calcomp plotter. The standard deviations, based on three independent measurements, were generally  $\pm$  0.03 R(v).

#### 2. Methods for Acquiring Reflectance Spectra of Crystals.

Reflectance spectra for optically uniaxial crystalline Calcite and Rutile, and for optically biaxial crystalline Gypsum, Biotite, Phlogopite, and Muscovite were obtained during the term of this contract.

A Perkin-Elmer Model 580 B dual beam infrared spectrophotometer with a common beam wire grid polarizer and a Perkin-Elmer combination 3x beam condenser and specular reflectance accessory were used to obtain the reflectance spectra in the  $180-4,000 \text{ cm}^{-1}$  (55-2.5 µm) spectral region. The common beam wire grid polarizer was on a KBr substrate and thus was used only in the 400-4,000 cm<sup>-1</sup> region. This type of polarizer

characteristically passes about 5% of the undesired polarization component so a second wire grid (KBr) polarizer was mounted in the sample beam for measurements in the 400-4,000 cm<sup>-1</sup> region. A single wire grid polarizer on a polyethylene substrate was mounted in the sample beam for measurements in the 180-400 cm<sup>-1</sup> region. The reflectance accessory provided a convergent beam incident on the sample with the central ray incident at  $6.5^{\circ}$  and the total included angle of the convergent beam was approximately  $10^{\circ}$ . All spectra were acquired with the spectrophotometer operating in the transmission mode.

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The procedure was to acquire a minimum of three scans each for an aluminum reference mirror, the crystalline sample, and the zero with the sample beam blocked by a shutter. The spectra were digitized at 1 cm<sup>-1</sup> intervals and stored on floppy discs. The three scans each for the reference mirror, sample, and zero were averaged. The averaged zero as subtracted from the averaged reference mirror and sample spectra and the ratio of the resultant sample spectrum to the resultant reference mirror spectrum provided the reflectance of the sample relative to the reflectance of the mirror. The relative reflectance spectrum was then multiplied by the reflectance of the reference mirror to obtain the absolute reflectance spectrum of the sample. The fractional uncertainty in the absolute reflectance was about 0.025 R(v).

The crystalline samples were oriented so that all measurements were made for the electric vector of the incident

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radiant flux perpendicular to the plane of incidence and parallel to the desired optical direction of the crystal. This required rotating the crystals rather than the polarizers.

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The Perkin-Elmer E-system spectrophotometer and data acquisition system described in Section VA1 (see Fig. A1) was used in the  $4.000-40.000 \text{ cm}^{-1}$  (2.5-0.25 µm) region to acquire the reflectance spectra of the crystalline samples. However, the Perkin-Elmer combined 3x beam condenser and specular reflectance accessory, also used with the PE-580B, was installed just prior to the entrance slit of the E-system monochromator, and the sample S denoted in Fig. A1 was replaced by a first surface aluminum mirror. Additionally, a calcite polarizer was placed between the exit slit of the monochrometer and the detector. The procedures for acquiring the initial spectra for the reference mirror, the sample, and the zero, and for obtaining the absolute reflectance of the sample were similar to those used with the PE-580B. Initial spectra were acquired at 200 equally spaced wavelength positions in each of the wavelength regions 0.2-0.3, 0.3-0.4, 0.4-0.6, 0.6-0.8, 0.8-1.0, 1.0-1.5, 1.5-2.0, 2.0-3.0  $\mu$ m. The calcite polarizer cuts off at about 0.25 µm.

#### 3. Methods for Acquiring Reflectance Spectra for Pellets

Many natural mineral materials occur in nature only as powder materials or in forms that prevent one from preparing bulk crystalline samples suitable for specular reflectance measurements. The clay minerals are examples of such

materials. In order to obtain reflectance spectra of such materials they were reduced to powder by grinding and the powder was then formed into a 13 mm diameter pellet by loading the powder in a die between polished stainless steel rams and pressing the powder with a hydraulic press. Mateials for which pellets were prepared were Gypsum, Montmorillomite, Ga. Limonite, Al. Limonite, Kaolin, Illite, Colemanite, Pyrolusite, Kernite, Cn. Vermiculite, Id. Vermiculite and Wavellite. The procedure for obtaining the initial spectra and absolute reflectance spectra of the pellets was similar to those for the crystalline samples except the polarizers were not used when obtaining reflectance spectra of the pellets.

#### 4. Methods for Acquiring Reflectance Spectra of Diesel Fuel

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The PE-580B spectrophotometer and a Barnes reflectance accessory modifided for use with liquids was used to acquire spectra in the 180-4,000 cm<sup>-1</sup> region for Diesel Fuel. The reflectance of the Diesel Fuel was measured relative to a first surface Aluminum mirror. A cathetometer was used to insure that the surface of the reference mirror and the Diesel Fuel were the same when each was separately placed in the reflectance unit. The modified reflectance unit is housed in a small plexiglas box. The box was equipped with entrance and exit windows of KBr in the 400-4,000 cm<sup>-1</sup> region and of polyethylene in the 180-400 cm<sup>-1</sup> region. The plexiglas box was separately and continually purged with dry CO<sub>2</sub>-free air to eliminate absorption spectra of diesel-fuel vapor.

The procedures for acquiring the initial reference mirror, Diesel Fuel, and zero spectra and the absolute reflectance spectrum of the Diesel Fuel were similar to those described in Section VA2.

#### B. Theoretical Methods

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The reflectance spectra R(v) were analyzed by use of causal Fourier transform dispersion relations and algorithms based on the Fresnel reflectivity equations to obtain N(v) the complex refractive index. The Fourier transform dispersion relations are equivalent to Kramers-Kronig methods but require much less computer time when digital fast Fourier transforms are used rather than the numerical integration techniques required for conventional Kramers-Kronig methods.

If one measures R(v) for a material over a broad spectral region then the modulus  $\rho(v)$  of the complex reflectivity  $\rho(v)exp[i\phi(v)]$  is the square root of R(v). The dispersion relation provides a means for computing the phase shift spectrum  $\phi(v)$  by use of the  $\rho(v)$  spectrum. The dispersion relation is

$$\phi(\omega_{o}) = \frac{1}{2\pi} \left\{ \int_{-\infty}^{0} K(t) e^{i\omega_{o}t} dt - \int_{0}^{\infty} K(t) e^{i\omega_{o}t} dt \right\}, \qquad (1)$$

where

$$K(t) = \int_{-\infty}^{+\infty} Ln[\rho(\omega)] e^{-i\omega t} d\omega.$$
 (2)
The angular frequency  $\omega$  is  $2\pi vc$  where v is wave number in units of  $cm^{-1}$  and c is the speed of light in vacuum.

In theory  $\rho(\omega)=\rho(-\omega)$  must be known throughout the region  $-\infty \le \omega \le \infty$ . In practical situations measurements of  $\rho(\omega)$  can only be made over some finite spectral region  $\omega_1 \le \omega \le \omega_2$ . One must therefore extend  $\rho(\omega)$ into the regions  $o \le \omega_1$  and  $\omega_2 \le \omega \le \infty$  to make ultimate use of the dispersion relation. In these investigations we assigned  $\rho(\omega) =$  $\rho(\omega_1)$  in the region  $o \le \omega \le \omega_1$ , and  $\rho(\omega) = \rho(\omega_2)$  in the region  $\omega_2 \le \omega \le \infty$ . Our experience shows that in most cases such assignments of  $\rho(\omega)$ introduces error in  $\phi(\omega_0)$  predominantly in spectral regions nearer the end points  $\omega_1$  and  $\omega_2$  of the measured spectrum.

The Fresnel reflectivity equation for the component of the incident radiant flux linearly polarized with the electric vector perpendicular to the plane of incidence (s-polarization) is

$$\rho_{s}(v)e^{i\phi_{s}(v)} = [Z(v) - \cos\theta_{s}]/[Z(v) + \cos\theta_{s}] \qquad (3)$$

where

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$$z^{2}(v) = N^{2}(v) - \sin^{2}\theta, \qquad (4)$$

N(v) = n(v) + ik(v) is the complex refractive index, and  $\theta$  is the angle of incidence. Denoting the left-hand side of Eq. (3) as  $r_s(v)$  and solving Eq. (3) for Z(v) one obtains

$$Z(v) = \cos\theta \left[ 1 + r_{v}(v) \right] / \left[ 1 - r_{v}(v) \right].$$
 (5)

Thus, N(v) is determined by applying Eqs. (1) and (2) to  $\rho(v)$  the square root of R(v), compute Z(v) by use of Eq. (5), and then compute N(v) by use of Eq. (4). This was the procedure used to determine N(v) for the materials investigated during the term of this contract.

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The complex dielectric function  $\varepsilon(v)$  of the non magnetic materials investigated is given by

$$\varepsilon(v) = N^{2}(v)$$
$$= Z^{2}(v) + \sin^{2}\theta.$$
 (6)

# C. Uncertainties in N(v)

It is important to know what uncertainties in N(v) can be expected from uncertainties in the measured reflectance R(v), the measured angle of incidence  $\theta$ , and the phase shift  $\phi(v)$  determined by use of Eqn. (1). Solving Eqns. (4) and (5) for N(v) provides

$$N^{2} = \sin^{2}\theta + \cos^{2}\theta (1 + r)^{2} / (1 - r)^{2}$$
(7)

where subscript s and explicit functional dependence on v have been surpressed. Differentials of Eqn. (7) provide the means for computing uncertainties in N. We find

$$\frac{\Delta N}{\Delta \theta} = -\frac{4r \sin \theta \cos \theta}{N(1-r)^2}, \qquad (8)$$

$$\frac{\Delta N}{(\Delta R/R)} = \frac{r(1+r)\cos^2\theta}{N(1-r)^3}, \text{ and} \qquad (9)$$

$$\frac{\Delta N}{\Delta \phi} = \frac{i2r(1+r)\cos^2\theta}{N(1-r)^3}$$
 (10)

Or we could write

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$$\Delta N = \frac{r(1+r)\cos^2\theta}{N(1-r)^3} \left\{ \frac{-4(1-r)\tan\theta\Delta\theta}{(1+r)} + \frac{\Delta R}{R} + i2\Delta\phi \right\}$$
(11)

We computed  $\Delta N/\Delta\theta$ ,  $\Delta N/(\Delta R/R)$ , and  $\Delta N/\Delta\phi$  with  $\theta = 6.5$  deg. and for n ranging from 1.3 to 1.6 and k ranging from 0.01 to 3.0. Results of these computations are presented in Table IV. Columns 1 and 2 of Table IV are values of N=n+ik. Columns 3 and 4 are  $\Delta N/\Delta \theta$ , columns 5 and 6 are  $\Delta N/(\Delta R/R)$ , and columns 7 and 8 are  $\Delta N/\Delta \phi$ . Note that  $\Delta N = \Delta n + i \Delta k$ . Uncertainties  $\Delta N$  for a specific set of data would be obtained by appropriately multiplying the entries in Table IV by  $\Delta \theta$ ,  $\Delta \mathbf{R}/\mathbf{R}$ , and/or  $\Delta \phi$  for that set of data. For example, a typical value for  $\Delta R/R$  is 0.025, and all entries in columns 5 and 6 would be multiplied by 0.025 to determine  $\Delta N$  for this fractional uncertainty in R. As will be seen later in this report, diffuse reflectance from rough pellet surfaces can yield systematic errors in specular reflectance of the order  $\Delta R/R = -0.3$  at 4,000 cm<sup>-1</sup>. Values of  $\Delta \theta$ and  $\Delta \phi$  used as multiplication factors for columns 3,4 and 7,8, respectively, should be in radians. Typical values are  $\Delta \theta = 0.01745$ and  $\Delta \phi = 0.05236$  corresponding to 1 and 3 degrees, respectively.

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	N	ΔN	/Δθ	ΔN/(	$\Delta R/R$ )	<u>ΔΝ/</u>	Δφ
1.300	0.010	-0.060	-0.002	0.173	0.007	-0.013	0.346
1.300	0.030	-0.061	-0.005	0.173	0.020	-0.039	0.345
1.300	0.050	-0.061	-0.009	0.172	0.033	-0.065	0.345
1.300	0.070	-0.061	-0.013	0.172	0.046	-0.091	0.343
1.300	0.090	-0.061	-0.016	0.171	0.059	-0.117	0.342
1.300	0.100	-0.061	-0.018	0.170	0.065	-0.131	0.341
1.300	0.300	-0.065	-0.053	0.150	0.196	-0.392	0.300
1.300	0.500	-0.072	-0.086	0.110	0.327	-0.653	0.219
1.300	0.700	-0.080	-0.116	0.049	0.457	-0.915	0.098
1.300	0.900	-0.089	-0.144	-0.032	0.588	-1.176	0.063
1.300	1.000	-0.093	-0.156	-0.079	0.654	-1.307	0.159
1.300	3.000	-0.134	-0.374	-2.093	1.963	-3.925	4.185
1.400	0.010	-0.078	-0.002	0.241	0.007	-0.014	0.481
1.400	0.030	-0.078	-0.005	0.241	0.021	-0.042	0.481
1.400	0.030	-0.078	-0.009	0.240	0.035	-0.070	0.480
1.400	0.070	-0.078	-0.012	0.240	0.049	-0.098	0.479
1.400	0.090	-0.078	-0.015	0.239	0.063	-0.127	0.477
1.400	0.100	-0.079	-0.017	0.238	0.070	-0.141	0.476
1.400	0.300	-0.082	-0.051	0.218	0.211	-0.422	0.436
1.400	0.500	-0.087	-0.083	0.178	0.352	-0.704	0.355
1.400	0.700	-0.094	-0.112	0.117	0.493	-0.985	0.234
1.400	0.900	-0.102	-0.140	0.036	0.634	-1.267	0.073
1.400	1.000	-0.106	-0.152	-0.012	0.704	-1.408	-0.023
1.400	3.000	-0.145	-0.373	-2.025	2.113	-4.227	-4.049
1.500	0.010	-0.095	-0.002	0.314	0.008	-0.015	0.627
1.500	0.030	-0.095	-0.905	0.313	0.023	-0.045	0.627
1.500	0.050	-0.095	-0.008	0.313	0.038	-0.075	0.626
1.500	0.070	-0.095	-0.012	0.312	0.053	-0.106	0.625
1.500	0.090	-0.095	-0.015	0.312	0.068	-0.136	0.623
1 500	0.100	-0.095	-0.016	0.311	0.075	-0.151	0.622
1.500	0.300	-0.098	-0.049	0.291	0.226	-0.452	0.582
1.500	0.500	-0.103	-0.080	0.251	0.377	-0.754	0.501
1.500	0.700	-0.109	-0.109	0.190	0.528	-1.056	0.380
1.500	0.900	-0.115	-0.136	0.109	0.679	-1.358	0.219
1.500	1.000	-0.118	-0.149	0.061	0.754	-1.509	0.123
1.500	3.000	-0.156	-0.372	-1.952	2.264	-4.529	-3.903
1.000	0.010	-0.111	-0.002	0.392	0.008	-0.016	0.783
1.000	0.030	-0.111	-0.005	0.391	0.024	-0.048	0.783
1.000	0.050	-0.111	-0.008	0.301	0.040	-0.080	0.782
1.600	0.070	-0.111	-0.011		0.056	-0.113	0.781
1.000	0.090	-0.111	-0.014	0.389	0.072	-0.145	0.779
1.600	0.100	-0.111	-0.016	0.389	0.080	-0.101	0.778
1.000	0.300	-0.114	-0.047	0.309	0.241	-0.403	0.750
1 600	0.500	-0.117	-0.077	0.320	0.402		0.526
1 600	0.700	-0.123	-0.100	0.200	0.303		0.750
1 600	1 000	-0.120	-0.133	0.107	0.005	- 1 • 449 1 £ 10	0.370
1 600	2 000	-0.151	-0.140	0.139	0.005	→1.01U	U.4(9 -2 7117
1.000	2.000	-0.10/	-0.3/1	-0.0/4	6.412		-2+(+(

in reflectance  $\Delta N/(\Delta R/R)$ , and phase angle  $\Delta N/\Delta \phi$ .

# D. Gypsum Crystals & Powder

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 Gypsum is an optically biaxial material that we investigated in crystalline form and pellet form to learn how measurements of reflectance for the pellets compared with measurements of the reflectance for each of the three optical directions X, Y, Z of the crystal. The following two publications provide the preliminary results of those investigations. The first paper is a reprint of an article that appeared in the Proceedings of the 1982 CSL Scientific Conference on Obscuration and Aerosol Research. The second is the M.S. thesis of Mr. Richard Strecker. The thesis presents a more detailed description of the investigations of Gypsum. Only the 8T Gypsum pellet is consider in this Section. Eight tons of force were applied to the 13 mm surface to press the 8T pellet. Additional investigations of Gypsum are presented in Section VF1 of this report.

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#### OPTICAL PROPERTIES OF GYPSUM

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#### M. R. Querry and R. Strecker Department of Physics University of Missouri-Kansas City Kansas City, Missouri 64110

ABSTRACT

Near-normal incidence specular reflectance spectra in the 180-4,000 cm<sup>-1</sup> spectral region were measured for crystalline Gypsum and for powdered Gypsum that was compressed into a pellet. Complex dielectric functions for the crystal and the pellet were obtained from the reflectance spectra. A composite dielectric function was constructed from the three dielectric functions of the crystal and compared to the dielectric function for the pellet. These investigations were recently extended to the UV-vis-nir (4,000-50,000 cm<sup>-1</sup>) spectral region.

#### EXPERIMENTAL METHODS

Gypsum is an optically biaxial (+) crystal with monoclinic prismatic-2/m layered structure and eminent (010) cleavage. The optical directions X,Y,Z are mutually perpendicular with directions X and Z lying in the (010) plane. Two crystalline samples were prepared; one was a (010) cleavage surface, the other was cut perpendicular to (010) and polished. The orientation of the optical directions was determined with light of sodium D wavelengths. A portion of the same crystal was reduced to a powder and was then compressed to form a disc-shaped pellet. The density of the crystal was 2.3 g/cm<sup>3</sup> and was 2.1 g/cm<sup>3</sup> for the pellet.

Near-normal incidence reflectance spectra were measured in the 180-4,000 cm<sup>-1</sup> spectral region for incident radiant flux linearly polarized parallel to the X,Y, and Z optical directions of the crystal. A similar reflectance spectrum was measured for unpolarized radiant flux incident on the pellet. The spectra were obtained with a Perkin-Elmer 580B Spectrophotometer and specular reflectance accessory.

Spectral values of the complex dielectric functions  $\varepsilon_x$ ,  $\varepsilon_y$ ,  $\varepsilon_z$ , and  $\varepsilon_p$  were determined from the reflectance spectra by use of Kramers-Kronig (kk) methods.

#### NORMALIZATION PROCEDURES

The real and imaginary parts of the dielectric-function spectra  $\epsilon_x$ ,  $\epsilon_y$ , and  $\epsilon_z$  were normalized according: to the following procedure. In the 1,800-2,200 cm<sup>-1</sup> region where Gypsum has no strong absorption bands, the normalization factors were obtained as simple averages of the ratios

$$R_{i} = \frac{\text{Re}\left[\varepsilon_{p}(v_{i})\right]}{\frac{1}{3}} \sum_{k=x}^{n} \frac{1/\text{Re}\left[\varepsilon_{k}(v_{i})\right]}{k=x},$$

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$$I_{i} = \underbrace{[Im \ e_{p}(v_{i})]}_{3} \underbrace{\sum_{k=x}^{z} 1/Im[e_{k}(v_{i})]}_{k=x}$$

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which were computed at 1 cm<sup>-1</sup> intervals (401 points). Index k ranges over X,Y,Z; subscript p denotes pellet; and v denotes wave-number in units of cm<sup>-1</sup>. The normalization factors were R = 0.934 and I = 0.598 for the real and imaginary parts, respectively. The normalized dielectric functions  $\overline{\epsilon}_{x}$  = R $\epsilon_{xx}$  + i $\epsilon_{xi}$ , etc. were then computed throughout the 180-4,000 cm<sup>-1</sup> region.

The normalization factors determined in this region of relatively low absorption show fairly good agreement between  $\epsilon_r = n^2 - k^2 = n^2$  for the crystal and the pellet; i.e. R = 0.938 is a favorable comparison with 0.913 the ratio of the density of the pellet to that of the crystal. There is poorer agreement, however, between  $\epsilon_i = 2nk$  for the pellet and the crystal; i.e. I = 0.598 shows the k value for the pellet are about 60% of the k values for the crystal in the 1,800-2,200 cm<sup>-1</sup> region. This is possibly due to multiple reflections by the particles in the pellet.

### COMPOSITE DIELECTRIC FUNCTION

A composite dielectric function  $\overline{\epsilon}_c$  was constructed from  $\overline{\epsilon}_x$ ,  $\overline{\epsilon}_y$ , and  $\overline{\epsilon}_z$  according to

$$\overline{\epsilon}_{c} = \alpha \overline{\epsilon}_{x} + \beta \overline{\epsilon}_{y} + \gamma \overline{\epsilon}_{z}$$
,

where  $a, \beta, \gamma$  were adjustable parameters subject to the condition  $a+\beta+\gamma=1$ . Parameters  $a, \beta, \gamma$  were adjusted in 0.05 increments and  $\overline{e_c}$  was tested for a least-squares fit to  $e_p$ . There were 231 different combinations of  $a, \beta, \gamma$  subject to  $a+\beta+\gamma=1$  and incremental adjustments of 0.05. The combination a=0.50,  $\beta=0.10$ , and  $\gamma=0.40$  produced the best fit. The poorest fit was given by  $a=\gamma=0.00$  and  $\beta=1.00$ . The 231 sets of parameters  $a, \beta, \gamma$  were then weighted; a weighting factor of 231 for the best fit and successive weighting downward to a factor of one for the poorest fit. The weighted average for the parameters  $a = 0.40, \beta = 0.21, \gamma = 0.39$ .

The general indication of 
$$\alpha, \beta, \gamma$$
 is that the particles of Gypsum in the pellet are preferentially,  
but not totally, oriented so the (010) cleavage plane made the greatest contribution to  $\varepsilon_p$ . It is  
obysically reasonable that grinding the Gypsum to produce a powder produced irregularly shaped platelets  
with (015) cleavage faces. When the Gypsum powder was poured in the die, and when the powder was  
compressed to form the pellet, the platelets naturally tended toward horizontal alignment; an alignment  
similar to leaves on the floor of the forest.

We also noted that all spectral features in  $\overline{\epsilon}_c$  were also in  $\epsilon_p$ . Also, there were no spectral features in  $\epsilon_p$  that were not in  $\overline{\epsilon}_c$ . Any shifts in spectral features in  $\epsilon_p$  compared to those in  $\overline{\epsilon}_c$  were

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quite small. The greatest disagreement between  $\varepsilon_c$  and  $\varepsilon_p$  occurred in the 180-500 cm<sup>-1</sup> region. This could be due in part to the kk analysis of reflectance spectra that extended only to 180 cm<sup>-1</sup>, or it could be due to relatively weak, broad, overlapping surface modes in the particles comprising the Gypsum pellet.

### UV-VIS-NIR SPECTRA

Similar reflectance spectra were also obtained for the crystal in the 4,000-50,000 cm<sup>-1</sup> region by use of a Perkin-Elmer E-System Spectrophotometer. Only one spectrum, that for the Y optical direction of the crystal, resembled a true reflectance spectrum. Beyond about 5,000 cm<sup>-1</sup> the other spectra appear to be multiple reflectance superimposed with a transmittance spectrum. Physically, we attribute this to lower absorption coefficients in the near infrared and visible regions compared to those in the infrared. Lower absorption increases the penetration depth thus allowing for multiple reflections from particles in the pellet, and from successive planes or the back surface of the cleaved sample. The failure of the KK analysis (negative values of k) provided additional proof that the "reflectance" is higher that is physically allowable for first-surface specular reflection.

### CONCLUSIONS

From the investigation we concluded that:

- (1) One can obtain a specular reflectance spectrum and subsequent dielectric function for a powder that has been compressed to a density comparable to that of the individual particles of the powder,
- (2) The material must be opaque in the spectral region in which the reflectance spectrum is to be measured,
- (3) The dielectric function of the compressed pellet will contain all the spectral features of the bulk material, and
- (4) The particle constituents of the compressed powder may be preferentially oriented thus predisposing the dielectric function of the pellet to be weighted more to specific orientations of uniaxial or biaxial materials.

Encouraged by this investigation of Gypsum we proceeded to obtain similar reflectance spectra for compressed pellets of Montmorillonite, Limonite, Kaolin, Illite, Colemanite, Pyrolusite, Kernite, Vermiculite, and Wavellite. These spectra are now being reduced to obtain complex refractive indices.

Support provided by the U.S. Army Research Office Contract DAAG-29-79-C-0131.



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Figure 1. Real part of  $\epsilon_p$  the complex dielectric function for the gypsum pellet.

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Imaginary part of  $\epsilon_p$  the complex dielectric function for the gypsum pellet.

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# INFRARED OPTICAL PROPERTIES OF GYPSUM

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## A THESIS IN Physics

Presented to the Faculty of the University of Missouri-Kansas City in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE

by RICHARD L. STRECKER

B.A., Benedictine College, 1980

Kansas City, Missouri 1982

### INFRARED OPTICAL PROPERTIES OF GYPSUM

**#** 

Richard L. Strecker, Master of Science University of Missouri-Kansas City, 1982

### ABSTRACT

The optical properties of crystalline and powdered gypsum were studied in the infrared region. Gypsum is an optically biaxial (+) crystal with monoclinic, prismatic-2/m layered structure. It posesses a perfect (010) cleavage and two less distinct cleavages.

Relative reflectance spectra were measured in the 180-4000 cm<sup>-1</sup> region for radiant flux polarized parallel to each of the three principal optic directions of a crystal gypsum sample. A powder was obtained from the same sample material and compressed to produce a pellet. A relative reflectance spectrum was obtained for this powder sample. The complex index of refraction and the complex dielectric function for each direction and for the powder were obtained using Kramers-Kronig techniques. The four complex dielectric function spectra were normalized and a composite crystal dielectric function was developed using the description

 $\overline{\epsilon}_{c}(\omega) = \Lambda \overline{\epsilon}_{x}(\omega) + B \overline{\epsilon}_{y}(\omega) + C \overline{\epsilon}_{z}(\omega)$ 

where c denotes composite, x, y, and z denote the optical directions and A, B, and C are adjustable coefficients. The coefficients were systematically varied and a fitting routine performed to find the  $\overline{\epsilon}_{c}$ which best agreed with the powder complex dielectric function,  $\overline{\epsilon}_{p}$ . The optimum coefficients were determined to be A = 0.44, B = 0.12, and C = 0.44. This result indicates that the powder dielectric function closely resembles the dielectric functions from the XZ plane and implies that the powder surface is predominantly comprised of (010) cleavage platelets.

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Normalization factors and the above coefficients were applied to the non-normalized real and imaginary parts of the crystal dielectric functions to obtain a final composite crystal dielectric function. Visual and numerical comparisons of the composite and powder dielectric functions were found to be very satisfactory.

This abstract of about 275 words is approved as to form and content.

Marvin R. Querry, Ph.D.

The undersigned, appointed by the Dean of the School of Graduate Studies, have examined a thesis entitled "Infrared Optical Properties of Gypsum," presented by Richard L. Strecker, candidate for the degree of Master of Science, and hereby certify that in their opinion it is worthy of acceptance.

Marvin R. Querry, Ph.D. Department of Physics

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Date

James M. Phillips, Ph.D. Department of Physics

John R. Urani, Ph.D. Department of Physics

Date

Date

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### ACKNOWLEDGEMENTS

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I would like to thank the faculty of the Physics Departments at Benedictine College and the University of Missouri-Kansas City for their efforts and inspiration.

I especially thank Dr. Marvin Querry for his assistance and advice during this project. His careful and helpful manner have been enjoyed inside and outside the classroom.

I also thank my colleagues at UMKC Physics for their friendship and encouragement throughout this research.

Finally, I thank my parents, Bill and Theresa, for making this all possible and worthwhile.

### CHAPTER I

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## INTRODUCTION

The major motivation for this project is to determine if the optical properties of a bulk crystalline mineral can be predicted from an analysis of a powdered sample of the same material. This subject is of importance because of a desire to identify a material without requiring optimum crystal samples for examination. It is also of interest to determine the relationship between different natural states of a material and their interaction with electromagnetic phenomena. Of concern is whether this interaction is similar for bulk crystalline and powdered dust forms.

Gypsum was chosen for this study because it is a common crystalline mineral which has been generally well researched. Because of characteristics in the crystalline structure, gypsum lends itself well to an examination of the individual optical directions. The samples obtained polished well and provided excellent reflection surfaces. In addition, gypsum is a rather general mineral in the crystallographic sense and it is hoped that an examination of it may provide results which are applicable to other minerals as well.

The material was examined for this project in the infrared region primarily to take advantage of the availability of sophisticated spectroscopic equipment capable of analysis in the infrared. The

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the powder dielectric function was quite satisfactory. Each prominent feature for the powder was nearly echoed, both qualitatively and quantitatively, by the composite crystal dielectric function.

The final objective of the project was an analysis of the optical results based on crystallographic considerations of the mineral. Specifically, it was desired to distinguish which physical characteristics of the crystal and of the powder were responsible for the parameters found using the fitting techniques. This analysis would hopefully provide analytical criteria for predicting the optical properties of other mineral systems in powdered form.

It was initially believed that the nature of this project was original. A comparison of the optical properties of a mineral material in crystalline and powdered forms had yet to be completed. An initial effort to find similar studies was made by M. R. Querry and the author with no success. An interactive computer based search was completed by Dialog Information Services of Palo Alto, California through the University of Missouri-Kansas City library. Five mineralogical and physics abstracts services were accessed. None of the descriptions provided by this search indicated that similar projects had been undertaken.

Two reference manuals describing crystallographic and optical properties of mineral sytems, by Deer, Howie and Zussman  $\frac{1}{}$  and Hurlbut and Klein  $\frac{2}{}$ , were used to develop the descriptions of gypsum found in the next chapter.

The theoretical and computational methods used in this project to determine the optical constants of a material are well documented in the literature. The time-domain method described by Peterson and Knight  $\frac{3}{2}$ 

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is shown to be equivalent to the Kramers-Kronig method. The method for determining the optical constants from the relative reflectance and phase angle values was developed by Querry et al.  $\frac{4/}{2}$ .

## CHAPTER II

### EXPERIMENTAL METHODS

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# Description of Gypsum (CaSO, 2H, 0)

Gypsum is the most abundant of sulphate minerals. It occurs generally in large masses in association with limes and shales in evaporite deposits. Gypsum is typically colorless but is occasionally tinted brown or gray or pale shades of red, yellow, or blue due to impurities. It is considered transparent to translucent and is given a Mohs' scale of hardness rating of 2, indicating it to be one of the softer minerals. Although it is found in most parts of the world it is primarily produced in the United States, France, Canada, England, and the Soviet Union. Its primary commercial use is in the manufacture of Plaster of Paris.

Gypsum is a monoclinic crystal which implies three unequal crystallographic axes; two of which, a and c, are inclined to each other at an oblique angle,  $\beta = 114^{\circ}12$ ' (See Figure 1). These axes both lie perpendicular to the third axis, b. Gypsum is further classified as a 2/m prismatic crystal which indicates the two-fold rotation symmetry of the b axis and that the a and c axes lie in a mirror plane. The axial lengths of the unit cell constructed using the three shortest vectors are; a = 6.28 Å, b = 15.15 Å, and c = 5.67 Å. These result in the axial ratios a:b:c = 0.414:1:0.374.

Gypsum has a perfect cleavage at (010) and less distinct cleavages



at (100) and (011). The perfect cleavage is provided by sheets of adjacent layers comprised of  $Ca^{++}$  ions and tetrahedral  $SO_4^{--}$  ions. Between successive sheets the water molecules are hydrogen bonded to the oxygens in the sulphate groups. Each  $Ca^{++}$  ion is thus coordinated by six oxygens of  $SO_4$  groups and by two water molecules. Each water molecule links a  $Ca^{++}$  ion to an oxygen in the same sheet and to an oxygen in an adjacent sheet. The perfect cleavage results between the water molecules.

Gypsum is an optically biaxial (+) crystal which indicates that the crystal has two directions in which light travels with zero birefringence. In any direction other than these two electromagnetic waves propagating through gypsum travel as two rays with perpendicular vibrations. These two rays differ in velocity according to which direction they travel through the crystal. The vibration direction of the faster and of the slower rays are at right angles to each other and are designated X and Z, respectively. The vibration direction perpendicular to the plane of X and Z, corresponding to the vibration of an intermediate velocity ray, is designated as Y.

Due to the velocity differences in each of these directions, there are accordingly three indices of refraction corresponding to the different optical directions. The indices  $\alpha$ ,  $\beta$ , and  $\gamma$  are associated with the optical directions X, Y, and Z, respectively;  $\alpha = 1.520$ ,  $\beta = 1.523$ , and  $\gamma = 1.530$  at the wavelength of the Sodium D lines.

In gypsum, as in all other monoclinic crystals, the Y optical direction corresponds to the b crystallographic axis. The XZ plane is therefore identical to the plane defined by the a and c crystal axes.

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The angle between the optical X direction and the crystallographic c axis is  $-37^{\circ}$ . The negative sign indicates that the X direction lies between the +c axis and the -a axis (See Figure 2).

An important consideration is to note the parallel nature of the XZ plane and the ac plane. The importance is that the (010) cleavage plane in gypsum corresponds to the XZ optical plane as well as to the ac crystallographic plane. A desirable experimental result is that the optical properties, specifically the reflectance, may be determined from an excellent cleaved surface in the X and Z directions.

In addition, when the gypsum sample is powdered, it is hypothesized that the crystal will easily separate along the cleavage planes and then break further into small platelets having XZ surfaces perpendicular to the Y direction. When the powder is compressed into pellet form for optical examination it is unlikely that the platelets will line up vertically, or parallel to the compression forces. If this were to occur, the platelets would probably continue to break until a more stable arrangement was found. Rather, the platelets would probably shuffle together horizontally with their surfaces perpendicular to the compression forces.

The result of this alignment is that the pellet surface to be examined will largely be a collection of XZ platelets. This leads to an initial assumption that the optical properties of the powdered pellet will primarily be due to characteristics of the X and Z optical directions and be less influenced by characteristics of the Y direction.

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## Sample Preparation

The gypsum material to be used in the project was initially examined by R. Coveney, Department of Geosciences, University of Missouri-Kansas City. Crystallographic determination of the a,b, and c axes was completed and samples providing XZ and XY surfaces were obtained. The XZ surface was cleaved at the (010) cleavage plane and was clearly evidenced by a natural shine. The XY surface sample was cut from the same large sample piece. The surface was polished by J. Potter, Department of Physics, University of Missouri-Kansas City using a series of polishing compounds until a large percentage of the surface damage due to the cut was removed.

The density of the crystal samples was 2.30  $g/cm^3$ . Each of the crystal samples were approximately 6 mm thick and provided ample cross sectional area for examination with the experimental equipment.

The same large sample piece was used to provide the powder for examination. The powder was ground by R. Coveney using conventional methods and a pellet was produced from the powder using a hydraulic press. Several pellets were manufactured and one providing an optimum reflectance surface was chosen for optical examination.

The powder pellet sample measured 0.75 mm in thickness, was 13.00 mm in diameter and had a mass of 0.210 grams. Density = 2.11 g/cm<sup>3</sup>.

### Measurement of Reflectance Spectra

The crystal samples were securely fixed to circular platforms of outside diameter 28 mm, inside diameter 11 mm, and of thickness 4.8 mm. These dimensions were required to mount the samples in the reflectance accessory to be discussed below.

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The lower face of the platform was beveled from the outer diameter to the inner diameter. The inner circular opening at the top of the bevel provided for optical examination of the sample surface. A flat black adherent was applied to the beveled surface to avoid reflectance from the mount itself.

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The gypsum pellet was mounted in a similar device which additionally was indented to accomodate the pellet. This mount was fitted with a removable top plate used to hold the pellet in place.

The primary experimental instrument used was the Perkin-Elmer PE-580 B Infrared Spectrophotometer. This instrument is double beam ratio recording device which provides a record of the transmission or reflectance of a sample as a function of frequency. The system is capable of being purged with nitrogen gas or dry air to eliminate spurious data, contributed especially by atmospheric  $H_2O$  and  $CO_2$  gases.

Source radiation for the spectrophotometer is provided by a ceramic tube heated by an internal element to approximately 1200°C. This provides a continuous source of radiation largely in the infrared. This radiation is then divided into reference and sample beams by a chopper mirror. The reference beam follows an unaffected path while the sample beam is reflected and absorbed by the material being examined.

The reference and reflected beams are recombined by a second chopper mirror and the combined beam is directed toward a grating monochromator which disperses the beam into its spectral components. A polarization accessory for the spectrophotmeter allows the operator

to eliminate all radiation not polarized corresponding to the optical axis being examined. The radiation corresponding to the wavenumber selected by the grating is then passed through a filter which rejects unwanted radiation which is also diffracted by the grating.

This radiation is then focused onto a blackened gold-leaf thermocouple detector. The thermoelectric voltage produced by the radiation absorption of the thermocouple is representative of the intensity of radiation reaching the detector. The chopped signal from the detector is processed electronically to give separate sample and reference beam signals. A ratiometer produces the ratio of the two signals which is the reflectance value for the sample.

The reflectance recorder and the grating monochromator scan mechanism are driven in synchronism by a single scan motor. Internal corrections assure that the wavenumber and corresponding reflectance information are accurately recorded at a variety of scan speeds.

The spectrophotometer is additionally equipped with scaled plotting capability which indicates the reflectance ratio data as a function of frequency in wavenumber units. The data are recorded using the disk memory capability of the spectrophotometer companion Perkin-Elmer Data Station.

For examination of sample reflectance the mounted samples are fitted in a Perkin-Elmer Combination Beam Condenser and Specular Reflectance Accessory. This device is necessary to use the spectrophotometer in the reflectance capacity. First surface aluminum mirrors are used to focus and condense the sample beam before incidence with the sample. The reflected radiation is then directed to the

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second chopper mirror. The beam was directed to the sample surface at an angle of incidence of  $\theta = 6.5^{\circ}$ .

Preliminary trial runs for each of the sample types were made to examine the general features of the reflectance spectra and the behavior of the experimental equipment. Guidelines and procedural techniques were developed to insure the quality and validity of the data obtained.

The first of these guidelines was to insure adequate warm up time for the equipment electronics, for the source and for the detector. The second guideline was to insure adequate time for the system to purge itself of troublesome atmospheric gases. These two checks were accomplished by taking spectra at various time intervals after the equipment was turned on. When the spectrum from an initial test agreed with that from a much later test the wait time for the initial test was determined to be sufficient.

The procedures were carefully examined to insure that the polarizing accessory was passing radiation corresponding to the desired optical direction. The initial identification of the optical directions was done with crystallographic techniques and these directions were marked. Fine tuning on the directions was accomplished by identifying reflectance peaks for each direction and then slightly turning the sample in the beam until the maximum reflectance at the peaks was found. This method "zeroed in" on lattice characteristics responsible for the reflectance peaks.

The next tests were made to determine appropriate time scale settings for the reflectance scans through the spectrum. This insured that the time response for the equipment electronics was not a limiting factor for the validity of the data. This check was accomplished by

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examining the spectra taken using different time scales. When the spectrum from a faster scale closely agreed with a more extended time spectrum the faster scale was determined to be sufficient.

Computational methods to determine the index of refraction and the complex dielectric function from the relative reflectance data were used on the trial data to construct N and  $\varepsilon$  spectra. These computational methods will be discussed in more detail in Chapter 3. The n, k, and  $\varepsilon$  spectra were plotted and carefully examined for any evident discontinuous or non-physical characteristics.

It was found that the relative reflectance spectra for the X and Z directions contained a nump which centered for both at approximately 2600 cm<sup>-1</sup>. The anomalous feature in the X spectrum was quite distinct and extended from roughly 2300 cm<sup>-1</sup> to 2900 cm<sup>-1</sup>. Over this frequency span the peak relative reflectance rose to 70% higher than a straight line joining the endpoints of the affected span. The relative reflectance for the Z direction contained a similar feature, although the peak reflectance was only 20% higher than a straight line correction.

As would be expected, these anomalies contributed to questionable features in the n, k, and complex  $\varepsilon$  values in the same region.

It was speculated that the additional reflectance was the result of radiation reflection from the back surface of the sample. This thought implies a relatively high transmission through the gypsum in the affected region. As noted previously, the XZ plane corresponds to the (010) cleavage plane for gypsum. The cleaved sample was very transparent through this plane, at least for visible radiation. The transmission "window" from 2300 cm<sup>-1</sup> to 2900 cm<sup>-1</sup> is not altogether surprising in view of these considerations.

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The transmission was experimentally verified by removing the reflectance accessory from the spectrophotmeter and examining the transmission spectra for the X and Z directions. The transmission windows expected were found in the regions specified by the reflectance humps.

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A variety of corrections was discussed, including roughing up the second surface so that the transmitted radiation would scatter upon incidence at the second interface. Also considered was application of a coating to the second surface that would possibly absorb the transmitted radiation at the interface.

Attempts with other samples using the above methods yielded inconclusive results. Although the transmission decreased, this effect had little influence on the reflectance hump. The reflectance from the second surface was apparently still present.

It was decided to leave the experimental sample unaltered and to obtain the reflectance data without corrective action. After the data were obtained 'the results were corrected for the second surface reflectance by joining the unaffected regions on both sides of the anomalous region with a straight line. Preliminary results for the reflectance, the complex index of refraction, and the complex dielectric function using this correction proved satisfactory.

The data for the final set of relative reflectance spectra were acquired continuously to avoid deviations in the equipment response that might occur otherwise. The equipment was allowed to warm up and purge for one hour prior to any data acquisition. The reflectance data were obtained and converted to digital values at one  $cm^{-1}$  intervals from 180 cm<sup>-1</sup> to 4000 cm<sup>-1</sup> for the aluminum mirror. The data were stored on a floppy disk memory using the terminal capability of the PE 580 B. Three runs for the aluminum mirror were completed.

The above procedures were completed for the crystal X, Y, and Z directions, for the powder sample, and for the zero. The data from the three runs for each of the samples were averaged at each wavenumber position. The average zero value at each wavenumber position was then subtracted from the average values for the gypsum samples and for the aluminum mirror. The corrected reflectance values for the samples were · divided by the Al mirror reference values to obtain relative reflectance values throughout the spectrum (See Figures 3-6).

The relative reflectance data were transmitted to storage files on the University of Missouri Computer Network for further calculations.

As was noted when examining the preliminary runs, it was necessary to correct for transmission effects in the X and Z spectra in the region from about  $2300 \text{ cm}^{-1}$  to  $2900 \text{ cm}^{-1}$ . A straight line was drawn smoothly joining the endpoints of the spectra considered to be affected by the transmission. Points along this line were used in further analysis of the reflectance.

It is well known that aluminum does not reflect 100% of the incident radiation, nor does it reflect equally throughout the spectrum. Corrections were made on the relative reflectance for each sample using the absolute reflectance values for aluminum at different wavenumber positions as were determined by Smith et. al.  $\frac{5}{.}$ 

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Figure 3. Relative Reflectance of Gypsum - X Direction

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Figure 4. Relative Reflectance of Gypsum - Y Direction

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## CHAPTER III

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## THEORETICAL METHODS

## Monochromatic Waves in Conducting Media

For monochromatic waves travelling in a nonconducting medium the simple index of refraction is defined in terms of the dielectric function of the medium according to the equation

$$n^2 = \epsilon$$
 (1)

For similar waves in a conducting medium, the presence of an induced current density implies a necessary change in the generalized Ampere's Law from the Maxwell Equations. A result of this change is that the dielectric function of the conducting material takes on a complex nature due to the interaction of the medium and the electromagnetic wave. The relationship between the dielectric function and the index of refraction remains quite similar

$$N^2 = \epsilon_c$$
, (2)

where the subscript c denotes complex. The complex index of refraction is

$$N = n + ik$$
 (3)

and the complex dielectric function is

$$\varepsilon_c = \varepsilon_r + i\varepsilon_i$$
 (4)

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The following relationships are evident:

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$$\varepsilon_r = n^2 - k^2 , \qquad (5)$$

$$\varepsilon_i = 2nk$$
 , (6)

$$n = \left(\frac{1}{2}(\epsilon_{r} + (\epsilon_{r}^{2} + \epsilon_{i}^{2})^{\frac{1}{2}})\right)^{\frac{1}{2}}, \qquad (7)$$

$$k = \left(\frac{1}{2}\left(-\varepsilon_{r} + \left(\varepsilon_{r}^{2} + \varepsilon_{i}^{2}\right)^{\frac{1}{2}}\right)\right)^{\frac{1}{2}} . \tag{8}$$

The important utility of these relationships is that simple calculations will lead from the complex dielectric function to the complex index of refraction, or vice-versa, if one of the quantities is known.

In this project Kramers-Kronig relations were used to determine the optical constants, n and k, for each crystal sample and for the powder sample at each wavenumber position in the infrared region. The relations above were used to determine the complex index of refraction.

## Peterson-Knight Transformations

Kramers-Kronig methods for determining optical constants from relative reflectance spectra have been used for three decades. The fundamental relations were first advanced by Kramers and Kronig in 1927  $\frac{6}{}$ .

Applications of these methods have been researched and are widely in use today. In 1973 Peterson and Knight  $\frac{3}{}$  derived a time-domain method procedure equivalent to the Kramers-Kronig procedure which is computationally more efficient. This analysis is known as the Peterson-Knight Fourier Transform Dispersion Relation.

The time-domain method is based on observations that a physical

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systems response is zero for negative times (a causality relation) and may be expressed as the sum of two functions which are equal for positive times and opposite for negative times. Additionally, the Fourier transforms of the two functions are the real and imaginary parts of the same physical systems frequency response.

Peterson and Knight begin their development of the time-domain method noting that the impulse response of a system in the time domain, I(t), after the input of an impulse may be represented as the Fourier transform of the frequency response,  $F(\omega)$ , to a sinusoidal input

$$I(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} d\omega F(\omega) e^{i\omega t}$$
(9)

where

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$$F(\omega) = \int_{-\infty}^{\infty} dt I(t) e^{-i\omega t} . \qquad (10)$$

By imposing the causality relation, I(t) = 0 for t < 0 and by separating the frequency response into real and imaginary parts

$$F(\omega) = S(\omega) + iA(\omega)$$
 (11)

Peterson and Knight show that  $A(\omega)$  can be determined if  $S(\omega)$  is known. With the proper operations in the time and frequency domains the resulting relationships between  $S(\omega)$  and  $A(\omega)$  are shown to be equivalent to the Kramers-Kronig relations for the real and imaginary parts of a complex function. The efficiency of the time-domain method relating two functions of physical interest provides a computational advantage over the Kramers-Kronig methods.

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A computational algorithm relating the modulus,  $\rho(\omega)$ , of the complex reflectivity,  $\rho(\omega)e^{i\phi(\omega)}$ , to the phase,  $\phi(\omega)$ , was prepared by Querry et al.  $\frac{4}{2}$  using the time-domain method. The principal relationship invoved in the operation is

$$\phi(\omega_{0}) = P\left[\frac{\omega_{0}}{\pi} \int_{0}^{\infty} \frac{\ln \rho(\omega) \, d\omega}{\omega^{2} \, \omega_{0}^{2}}\right]$$
(12)

where P indicates the Cauchy principal value of the integral. The modulus,  $\rho(\omega) = (R(\omega))^{\frac{1}{2}}$ , is determined from the experimentally obtained values of the relative reflectance of the material. The condition that the integral must be evaluated for  $0 < \omega < \infty$  is resolved satisfactorily by setting the reflectance values outside our experimental region equal to constants. The constants above and below the region were determined by averaging a set of reflectance values near the appropriate endpoints.

## Determination of Complex Refractive Index

The complex reflectivity for a sample can be related to the complex index of refraction of the sample using the following Fresnel equation for normal incidence

$$\rho e^{1\varphi} = (Z - \cos\theta)/(Z + \cos\theta)$$
(13)

where

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$$Z = (N^2 - \sin^2 \theta)^{\frac{1}{2}} .$$
 (14)

As noted earlier  $\rho_{gyp} = (R_{gyp})^{\frac{1}{2}}$  where  $R_{gyp}$  is determined from our relative reflectance values according to the relation

$$R_{gyp} = \frac{R_{gyp}}{R_{A1}} \times R_{A1} .$$
 (15)

Solving equation (13) for Z we obtain

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$$Z = \cos\theta (1 + \rho e^{i\phi})/(1 - \rho e^{i\phi})$$
 (16)

and the complex index of refraction is described by

$$N = (Z^{2} + \sin^{2}\theta)^{\frac{1}{2}} .$$
 (17)

A computational algorithm implementing these results to determine  $N(\omega)$  if  $\rho(\omega)$  and  $\phi(\omega)$  are known was developed by Querry et. al.<sup>4/</sup>. This algorithm has proved successful in a number of studies and will be used here to determine the complex index of refraction.

The real and imaginary parts of the complex index of refraction are plotted as a function of frequency for each of the samples (See Figures 7 - 14).



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Figure 9. Index of Refraction of Gypsum - Z Direction

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Figure 10. Index of Refraction of Gypsum - Powder

INDEX OF REFRACTION OF GYPSUM POWDER

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## CHAPTER IV

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#### ANALYSIS OF COMPLEX DIELECTRIC FUNCTION

## Composite Crystal Complex Dielectric Function

The complex dielectric function was determined from the complex index of refraction according to the relationship discussed earlier

$$\epsilon = N^2$$
 (2)

(The subscript c indicating the complex nature of the dielectric function is no longer necessary for clarity.) This calculation was done for each of the crystal directions and for the powder.

The complex dielectric function for each of the samples was plotted as a function of frequency (See Figures 15-22). These graphical results provided incentive to continue the project and some verification of the initial speculations. The dielectric function for the powder resembled both the real and imaginary parts of the dielectric functions of the crystal. In addition, the dielectric function for the powder more closely resembled the functions for the X and Z directions than it did for the Y functions. This agrees well with the predictions made earlier based on the compression of the powder into pellet form.

The major goal of the project is to determine some combination of the complex dielectric functions of the crystal which would closely resemble the complex dielectric function of the powder. It is therefore

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Figure 15. Real Dielectric Function of Gypsum - X Direction

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Real Dielectric Function of Gypsum - Y Direction Figure 16.

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REAL DIELECTRIC FUNCTION OF GYPSUM

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MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A desired to find multiplicative coefficients A, B, and C for the crystal dielectric functions such that

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$$\varepsilon_{\rm p} = A\varepsilon_{\rm x} + B\varepsilon_{\rm y} + C\varepsilon_{\rm z}$$
 (18)

throughout the spectrum. The subscripts indicate the powder and the three optical directions. An additional condition is that A + B + C = 1. By adjusting these coefficients in a systematic fashion and utilizing the graphics equipment available through the University of Missouri Computer Network an attempt to computationally and visually determine the best combination of coefficients was made.

## Computational Methods

It was determined that the powder, due to surface and density considerations, did not reflect at the same levels as did the polished crystals. The phenomenological model of  $\varepsilon(\omega)$  suggests that the dielectric function is dependent upon the density of oscillators in the material considered  $\frac{7}{}$ . This implies a dependence also on the mass density of the sample. Since the powder pellet is of lower density than the crystal samples we might therefore expect a lower  $\varepsilon(\omega)$  for the powder. The ratio of the densities is

$$\rho_p / \rho_c = 2.30 \ g/cm^3 / 2.11 \ g/cm^3 = 0.92$$
 (19)

The relative effect of the surface differences is uncertain, but is assumed to be present. The powder surface probably causes some scattering of the reflected beam.

In order to normalize the crystal data to the powder data

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a normalization constant for the crystal dielectric functions was determined using a comparison with the powder over a relatively featureless region of the spectrum (1800 cm<sup>-1</sup> to 2200 cm<sup>-1</sup>). At each wavenumber position in this region the following ratios were determined;

$$R_{x} = \frac{\operatorname{Re}(\varepsilon_{p})}{\operatorname{Re}(\varepsilon_{x})}, \qquad (20)$$

and

$$I_{x} = \frac{Im(\varepsilon_{p})}{Im(\varepsilon_{r})} .$$
(21)

The normalization constants for the X direction were then computed as the average of these ratios throughout the normalization region. This calculation was also completed for the Y and Z directions.

Although the real normalization constants for the X, Y, and Z directions (and correspondingly the imaginary constants) were slightly different, they were averaged to yield a single normalization for  $\varepsilon_r$ and a single normalization for  $\varepsilon_i$ ;

$$R = 0.934$$
 I = 0.598 . (22)

The normalization for  $\varepsilon_r$  shows fairly good agreement with 0.92, the density ratio discussed earlier. The normalization for  $\varepsilon_i$  is in poorer agreement with the density ratio and indicates  $\varepsilon_i$  values which are only 60% of the values for the crystal. This effect can possibly be attributed to the low absorption of the crystal in this region. Multiple reflections by the powder particles could affect the absorption coefficient and ultimately the  $\varepsilon_i$  values.

A preliminary composite complex dielectric function for the crystal was determined by use of the normalized X, Y, and Z dielectric functions and by setting the coefficients A, B, and C equal to one third. The results were quite satisfactory as the composite dielectric function was very similar to the powder dielectric function.

The next step was an effort to find which coefficients would provide a best fit between the composite  $\varepsilon$  and the powder  $\varepsilon$ . The A, B, and C coefficients were incremented in 0.1 step intervals covering each possible combination. The composite  $\varepsilon$  was constructed for each set of coefficients according to the equation

$$\varepsilon_{c} = R(A\varepsilon_{xr} + B\varepsilon_{yr} + C\varepsilon_{zr}) + iI(A\varepsilon_{xi} + B\varepsilon_{yi} + C\varepsilon_{zi})$$
(23)

where the r and i subscripts indicate the real and imaginary parts of the dielectric functions, respectively. The subscript c on the left side of the equation distinguishes the composite crystal dielectric function. If we allow  $\overline{\epsilon}$  to indicate the normalized dielectric functions then the description becomes

$$\overline{\varepsilon}_{c} = A\overline{\varepsilon}_{x} + B\overline{\varepsilon}_{y} + C\overline{\varepsilon}_{z} . \qquad (24)$$

A least squares routine was performed by comparing the real parts and the imaginary parts of the composite and powder dielectric functions at each wavenumber position in order to find the best fit. The real parts and the imaginary parts were necessarily separated during the least squares routine because of the nature of the complex squaring operation. Treating them separately implies that the real part of the

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dielectric functions and the imaginary part of the dielectric functions are fit independently of each other. In a second operation, however, the quantitative results of the real fit and the imaginary fit were added together and a search was done to find the best agreement between  $\overline{\epsilon}_c$  and  $\epsilon_p$ . A pleasant indication was that the coefficients which provided the best fits for the real  $\overline{\epsilon}_c$  and  $\epsilon_p$  also generally gave the best fits for the imaginary  $\overline{\epsilon}_c$  and  $\epsilon_p$ . The best combination of coefficients was;

$$A = 0.50$$
,  $B = 0.20$ ,  $C = 0.30$ . (25)

After examination of the plotted results using these coefficients it was thought that the large band feature at approximately 1130 cm<sup>-1</sup> might be unreasonably prejudicing the least squares results. There was also some concern that two other large features below 1130 cm<sup>-1</sup> might be causing similar difficulties. In order to examine the effect of the large band on the least squares fit it was decided to do an independent least squares examination on the region above 1450 cm<sup>-1</sup>. The second fit serves a desire to qualitatively match  $\overline{e}_c$  and  $\epsilon_p$ . Without the influence of the dominant peak it was thought that the second fit would be predominantly affected by the exact placement of the more subtle features in the 1450 cm<sup>-1</sup> to 4000 cm<sup>-1</sup> region. It was also thought that the coefficients provided would yield a good qualitative match throughout the entire spectrum. The coefficients provided by the second fit were;

A = 0.50, B = 0.10, C = 0.40. (26)

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A visual comparison of  $\overline{\epsilon}_c$  using these coefficients and  $\varepsilon_p$  was very encouraging. Features throughout the spectrum in  $\overline{\epsilon}_c$  were closely echoed by  $\varepsilon_n$ .

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A further least squares examination was done by adjusting the coefficients in 0.05 increments in a similar fashion. The best fit coefficients in this arrangement were again A = 0.50, B = 0.10, and C = 0.40. These were followed by A = 0.45, B = 0.10, and C = 0.45. The 50 best combinations of coefficients are listed in Table 1.

An examination of the best fit values generated by the least squares routine yields some important observations. The top group of fit values for the second region are very close together. The first five are separated by only 2.7%. So, although the designation of A = 0.50, B = 0.10, and C = 0.40 as the optimum coefficients is of some importance, the more important result is the trend of the first group of coefficients listed in the table. The trend definitely shows that the values of the coefficients A and C are very close. They are both significantly higher than the values for the coefficient B. However, the B coefficient is clearly non-negligible.

In order to examine these trends in more quantitative detail a further calculation was done. The coefficients were weighted according to their rank; i.e. the coefficients A = 0.50, B = 0.10, and C = 0.40were given rank 231 (there were 231 possible combinations of coefficients). The coefficients with the worst fit, A = 0.00, B = 1.00, and C = 0.00were given weight 1. The coefficients were multiplied by their assigned weight and these weighted coefficients were summed. The weighted sums for A, B, and C were then reduced such that A + B + C = 1. The results of this calculation were;

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# TABLE 1

## BEST FIT COEFFICIENTS FOR COMPOSITE DIELECTRIC FUNCTION

145	50-4000	cm <sup>-1</sup>	Region		180-40	00 cm <sup>-1</sup>	Region
A	B	С	FIT	A	В	С	FIT
0.50	0.10	0.40	8.856	0.5	0 0.1	5 0.35	476.34
0.45	0.10	0.45	8.938	0.5	5 0.1	0 0.35	477.26
0.45	0.15	0.40	9.095	0.5	5 0.1	5 0.30	482.11
0.55	0.10	0.35	9.103	0.5	0.2	0 0.30	488.03
0.40	0.15	0.45	9.108	0.4	5 0.2	0 0.35	488.87
0.40	0.10	0.50	9.348	0.6	0.1	0 0.30	489.64
0.50	0.15	0.35	9.411	0.6	0.0	5 0.35	491.62
0.35	0.15	0.50	9.449	0.5	0 0.1	0 0.40	497.45
0.60	0.10	0.30	9.678	0.4	5 0.1	5 0.40	503.14
0.55	0.15	0.30	10.055	0.5	5 0.0	5 0.40	505.20
0.35	0.10	0.55	10.087	0.4	5 0.2	5 0.30	507.38
0.30	0.15	0.55	10.119	0.6	5 0.0	5 0.30	510.60
0.55	0.05	0.40	10.120	0.4	0 0.2	5 0.35	514.83
0.50	0.05	0.45	10.271	0.6	5 0.0	0 0.35	519.41
0.60	0.05	0.35	10.298	0.5	5 0.2	0 0.25	519.75
0.65	0.10	0.25	10.582	0.6	0 0.1	5 0.25	520.44
0.45	0.05	0.50	10.750	0.4	0 0.2	0 0.40	522.27
0.35	0.20	0.45	10.780	0.6	0 0.0	0 0.40	526.39
0.65	0.05	0.30	10.804	0.5	0 0.2	5 0.25	532.50
0.40	0.20	0.40	10.837	0.6	5 0.1	0 0.25	534.57
0.60	0.15	0.25	11.028	0.4	0 0.3	0 0.30	540.18
0.30	0.20	0.50	11.053	0.7	0 0.0	0 0.30	545.00
0.25	0.15	0.60	11.117	0.4	5 0.1	0 0.45	550.20
0.30	0.10	0.60	11.154	0.5	0.0	5 0.45	551.35
0.45	0.20	0.35	11.222	0.3	5 0.3	0 0.35	554.23
0.40	0.05	0.55	11.558	0.3	5 0.2	5 0.40	554.83
0.70	0.05	0.25	11.638	0.4	5 0.3	0 0.25	558.69
0.25	0.20	0.55	11.653	0.7	0.0	5 0.25	562.14
0.70	0.10	0.20	11.814	0.4	0 0.1	5 0.45	562.50
0.50	0.20	0.30	11.935	0.5	5 0.0	0 0:45	565.93
0.65	0.15	0.20	12.329	0.6	0 0.2	0 0.20	584.04
0.20	0.15	0.65	12.444	0.3	5 0.3	5 0.30	586.41
0.25	0.10	0.65	12.550	0.3	5 0.2	0 0.45	588.23
0.20	0.20	0.60	12.582	0.5	5 0.2	5 0.20	590.19
0.35	0.05	0.60	12.695	0.6	5 0.1	5 0.20	591.34
0.75	0.05	0.20	12.801	0.4	0 0.3	5 0.25	598.32
0.60	0.00	0.40	12.887	0.3	0.3	0 0.40	600.84
0.55	0.20	0.25	12.977	0.7	5 0.0	0 0.25	603.14
0.65	0.00	0.35	12.995	0.3	0.3	5 0.35	607.07
0.55	0.00	0.45	13.107	0.5	0.3	0 0.20	609.77

$$A = 0.40$$
,  $B = 0.21$ ,  $C = 0.39$ . (27)

The nature of this calculation increases the relative value for B slightly. However, the exact result is not as important as the general indication. The A and C coefficients should be nearly equal and the B coefficient should be significantly lower.

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Examining both the weighted coefficients and the actual best fit coefficients the following ranges seem reasonable;

$$A = 0.40 - 0.45$$
,  $B = 0.10 - 0.15$ ,  $C = 0.40 - 0.45$ , (28)

A representative set of coefficients within these ranges might be:

$$A = 0.44$$
,  $B = 0.12$ ,  $C = 0.44$ , (29)

The above coefficients and the normalizations previously determined were used to generate a final combination crystal dielectric function. This function over the infrared spectrum was then plotted along with the powder complex dielectric function using identical scales. (See figures 23-26). The visual results of this comparison were very favorable. The qualitative features of the two were almost exactly reproduced. The normalization had very nearly duplicated the quantitative nature of the spectra. The large sulphate band at 1130 cm<sup>-1</sup> is the only large quantitative disparity. The only other significant disagreement between  $\overline{e}_c$  and  $e_p$  occurs in the 180 - 500 cm<sup>-1</sup> region. This could possibly be an effect of the average value of the reflectance used in the Kramers-Kronig analysis for frequencies below the experimental region. An extremely pleasing result was the almost perfect duplication



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Figure 23. Real Composite Dielectric Function of Gypsum

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KEAL DIELECTRIC FUNCTION OF CYPSUM POWDER (\*10)

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Figure 25. Imaginary Composite Dielectric Function of Gypsum

INVELIVERY COMPOSITE DIFLECTRIC FUNCTION OF GYPSUM (x10)

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80 of the two faceted feature at approximately 3300 cm<sup>-1</sup> since one part

of the feature can be identified with the X and Z optical directions and the smaller part is identified with the Y optical direction.

#### CHAPTER V

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# CONCLUSION

The results of this investigation are quite encouraging and are assumed to be valid. Although the comparison of the complex dielectric function for powdered and crystalline forms of a mineral material appears to be a novel project, the theoretical and computational methods employed in the bulk of the project have been used effectively in numerous experimental studies. The computational algorithm developed by Querry implementing the time-domain method forwarded by Peterson and Knight has been shown successful in determining the optical properties of materials. The additional computations for the comparison of the powder and crystal dielectric functions are straightforward.

The comparison provided results which are in excellent agreement with the predictions initially made from crystallographic analysis of the gypsum crystal. The powder complex dielectric function closely resembles the X and Z complex dielectric functions and gives strong evidence to support the hypothesis that the powdered sample particles are predominantly oriented in the pellet with the (010) cleavage platelets parallel to the sample surface. This is encouraging since it predicts that most other biaxial and uniaxial minerals will behave in a similar manner if they posess strong cleavage planes.

Another important result is the indication that gypsum and possibly other materials may be effectively identified in either powdered or crystalline forms. The dielectric function of the powder will contain all of the spectral features of the crystalline material. From the transmission effects noted in the X and Z reflectance spectra it is found to be necessary that the material be opaque in the spectral region considered or the data must be corrected for the transmission before the optical constants may be determined from Kramers-Kronig analysis. A practical result of the investigation is that the methods used here should be helpful in remote airborne identifications of surface soil composition similar to those done by Lindberg et al.  $\frac{8}{}$  and Doda et al.  $\frac{9}{}$ .

The study of the optical constants in the infrared region seems to indicate that the optical characteristics of a crystalline powder may be predicted if the crystal optical properties are known and if a knowledge of the crystal structure is available. However, the molecular activity responsible for the spectral characteristics in the infrared region differs from the activity responsible for optical responses in other regions. So while it seems plausible that our results and conclusions may be applicable to other spectral regions, it is possible that the break up of the regular crystal structure in the reduction to powder form may provide different effects in other regions.

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#### VITA

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### E. Crystalline Samples

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# 1. Rutile O-Ray (E+C)

Rutile is an optically uniaxial (+) crystal of the  $P_{4_2}/mnm$  lattice and space group. The optical directions for the E- and O-rays are respectively parallel and perpendicular to the C-axis of the crystal. The reflectance spectrum was measured in the 180-4,000 cm<sup>-1</sup> region for a polished (001) plane (O-ray) and spectral values of N( $\nu$ ) were computed by use of the dispersion relations and the Fresnel equations. The reflectance spectrum is shown in Fig. E1-1 and the spectra for the real and imaginary parts of N( $\nu$ ) are presented in Figs. E1-2 and E1-3, respectively. The natural Rutile crystal used for this investigation was black in color and possessed a metallic appearance after polishing.



180-4,000 cm<sup>-1</sup> wave number region.

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Index of refraction n of rutile (0-ray) in the 180-4,000 Figure E1-2.

cm<sup>-1</sup> wave-number region.



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Extinction coefficient k of rutile (0-ray) in the 180-Figure E1-3.

4,000 cm<sup>-1</sup> wave-number region.

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2. <u>Calcite</u>

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Calcite is an optically uniaxial (-) hexagonal crystal of the R 32/m lattice and space group. The optical directions for the E- and O-rays are respectively parallel and perpendicular to the c-axis of the crystal. The crystalline sample used in this investigation was cut parallel to the c-axis and then mechanically polished. Reflectance spectra were obtained for the E-ray (0-ray) with the incident radiant flux linearly polarized so that the electric vector was parallel (perpendicular) to the caxis. The reflectance spectrum in the  $180-4,000 \text{ cm}^{-7}$ region for the O-ray (E-Ray) is presented in Fig. E2-1 (Fig. E2-4). The real and imaginary parts of N(v) for the O-ray are presented in Figs. E2-2 and E2-3, respectively; and for the E-Ray in Figs. E2-5 and E2-6, respectively, values of N(v) presented for the E-ray yielded non physical values for the phase shift  $\phi(v)$  in the 875-900 cm<sup>-1</sup> region. The absorption coefficient for the E-ray in the  $875-900 \text{ cm}^{-1}$  region is relatively small. We believe reflection from the back surface of the crystal was responsible for the non physical values of  $\phi(v)$ . Reflection from the back surface of the crystal was evident for both the E- and O-ray in the near infrared and visible regions. We therefore excluded from further analysis, and from this report, the reflectance spectra for Calcite in the near infrared and visible regions.



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Figure E2-2. Index of refraction n of calcite (0-ray) in the 180-4,000

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Extinction coefficient k of calcite (0-ray) in the 180-Figure E2-3.

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Extinction coefficient k of calcite (E-ray) in the 180-Figure E2-6.

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4,000 cm<sup>-1</sup> wave-number region.

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3. Biotite

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Biotite (Black Mica) is an optically biaxial (-) monoclinic crystal of the C 2/m lattice and space group possessing perfect (001) cleavage. Two crystalline samples were prepared for this investigation; one was cut on the (100) plane the other on the (010) plane. The two samples were mechanically polished. The Y optical direction coincides with the b-axis of the crystal. The Z optical direction forms an angle of 0-9 degrees with the a-axis of the crystal. Thus reflectance spectra were obtained for linearly polarized radiant flux with the electric vector E parallel to the a, b, and c axes of the crystal. Reflectance spectra were obtained in the 180-40,000 cm<sup>-1</sup> region. However, the reflectance spectra in the visible region contained an artifact due to a damaged calcite polarizer and those spectra were eliminated from further consideration. We now have a new uv-vis-nir spectrophotometer system on order and will remeasure the reflectance spectra of the Biotite with that instrument. The reflectance spectra for Biotite are shown in Figs. E3-1, E3-4, and E3-7 respectively for E parallel to the a, b, and c axes. The real and imaginary parts of N(v) in the infrared region are shown in Figs. E3-2 and E3-3 for E parallel to a, in Figs. E3-5 and E3-6 for E parallel to b, and Figs. E3-8 and E3-9 for E parallel to c.



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Figure E3-1. Reflectance spectrum of Biotite a-axis in the 2.5-33  $\mu m$ 

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Extinction coefficient k of Biotite a-axis in the 2.5-33 Figure E3-3.

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Figure E3-7. Reflectance spectrum of Biotite c-axis in the 2.5-28  $\mu$ m

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## 4. Phlogopite

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Phlogopite is an optically biaxial (-) monoclinic crystal of the C 2/m lattice and space group and possesses perfect (001) cleavage. Two crystal samples of phlogopite were prepared for this investigation; one was the (001) cleavage surface and the other was cut and polished parallel to the (100) plane. The Y optical direction coincides with the b-axis of the crystal, the X optical direction forms an angle of 0-5 degrees with the c axis of the crystal, and the Z optical direction forms an angle of 2-4 degrees with the a axis. Thus we obtained reflectance spectra for linearly polarized radiant flux with the electric vector E separately parallel to the a, b, and c axes. The reflectance spectra for E parallel to the a and b axes axes were obtained on the (001) cleaved surface, and for E parallel to the c axis on the cut and polished (100) surface. The reflectance spectra for E parallel to a, b, and c axes are presented in Figs. E4-1, E4-2, and E4-3, respectively.

The reflectance spectra presented in Figs. E4-1 and E4-2 show, in the 1,500-4,000  $\text{cm}^{-1}$  region, characteristics of transmittance spectra rather than ref<sup>-</sup> ctance spectra. It appears that cleaving the crystal for the reflectance studies also broke some of the bonds between (001) lamilar planes that remained with the sample. This produced multiple internal reflections that are the source of the

interference fringes and the  $H_2O$  absorption bands in the 3,600-3,700 cm<sup>-1</sup> region. All (001) cleaved surfaces yielded similar spectra.

The reflectance spectrum shown in Fig. E4-3 for E parallel to the c axis was obtained on the (010) surface which is perpendicular to the (001) cleavage. The interference fringes and absorption bands are not present in this spectrum.

Complex refractive indices were computed only for the spectrum in Fig. E4-3. The leakage of the single polarizer in the 180-400 cm<sup>-1</sup> gave inconsistent values of N(v) in this region. Thus N(v) for E parallel to the c axis is presented in Figs. E4-4 and E4-5 only for the 400-4,000 cm<sup>-1</sup> region.



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Extinction coefficient k of Phlogopite c-axis in the 180-Figure B4-5.

4,000 cm<sup>-1</sup> wave-number region.

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## 5. <u>Muscovite</u>

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Muscovite is an optically biaxial (-) monoclinic crystal of the C 2/m lattice and space group, and possesses perfect (001) cleavage. Two crystal samples of Muscovite were prepared, one was the (001) cleavage plane and the other was cut and polished parallel to the (010) plane. The Z optical direction corresponds to the b axis of the crystal, the X optical direction is at an angle from 0 to -5 degrees relative to the c axis, and the Y optical direction is at an angle of 1-3 degrees relative to the a axis. Thus we measured reflectance spectra of the (001) cleavage surface for radiant flux linearly polarized with the electric vector E parallel to the a and b crystal axes and reflectance spectra of the (010) plane with linear polarization parallel to the c axis. The reflectance spectrum for E parallel fo the a axis is presented in Fig. E5-1 for the  $400-4,000 \text{ cm}^{-1}$  region and in Fig. E5-2 for the  $180-400 \text{ cm}^{-1}$  region. Note that in the 1,800-4,000 cm<sup>-1</sup> region the spectrum in Fig. E5-1 has the appearance of a transmittance spectrum. Transmittance measurements on a thin cleaved (001) lamilar muscovite sample showed muscovite to possess less absorption in the 1,800-4,000 cm<sup>-1</sup> region. Additionally, there are multiple interference fringes in 1,500-4,000 cm<sup>-1</sup> region of the spectrum in Fig. E5-1. It thus appears that cleaving the crystal

for the reflectance studies also broke some of the bonds between (001) planes remaining with the sample and this produced multiple internal reflections and caused the interference fringes and also the water absorption bands in the 3,600-3,700 cm<sup>-1</sup> region.

The reflectance spectrum for E parallel to the b axis is shown in Figs. E5-3 and E5-4. This spectrum (Fig. E5-3) was also acquired from the (001) cleavage surface and shows interference fringes and absorptions similar to those previously described in Fig. E5-1.

The reflectance spectrum for E parallel to the c axis is shown in Figs. E5-5 and E5-6. This spectrum was acquired from the cut and polished (010) surface, i.e. perpendicular to the (001) cleavage planes. The interference fringes and absorptions are not present in Fig. E5-5. However, the reflectance at the peaks near 1,050 and 550 cm<sup>-1</sup> is about 35% which is lower than was expected. We attribute this to the extreme difficulty encounted in preparing a specular surface perpendicular to the cleavage planes, although we have no other spectra to compare.

Complex refractive indices N(v) were obtained only for the reflectance spectrum shown in Fig. E5-5. Leakage of the single polarizer used in the 180-400 cm<sup>-1</sup> region gave inconsistent values of N(v) in this lower frequency region. N(v) for E parallel to the c axis are presented in Fig. E5-7 and E5-8.



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Figure E5-6. Reflectance spectrum of Muscovite c-axis in the 180-400 cm<sup>-1</sup> wave-number region.



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 cm<sup>-1</sup> wave-number region.

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Extinction coefficient k of Muscovite c-axis in the 180-Figure E5-8.

4,000 cm<sup>-1</sup> wave-number region.

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## F. Powder/Pellet Samples

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Many natural minerals occur in nature only as small crystals, i.e. powders, that preclude preparation of bulk crystalline samples suitable for reflectance measurements. The clay minerals are examples. Also the clay minerals are relatively soft and if large crystalline specimens could be acquired they could not be polished by use of conventional methods. In order to obtain reflectance spectra of such minerals they were reduced to powder by grinding and the powder was then formed into a 13 mm diameter pellet by placing the powder between polished stainless steel rams in a die and applying pressure with a hydraulic press. The 13 mm die was rated for a maximum of 10 tons of force applied to the pellet. Most pellets, however, were pressed by applying 8 tons of force.

For such pellets two primary traits are desirable. First, the pellet should have a specular surface, and second, most natural minerals are either optically uniaxial or biaxial thus a random orientation of the particles within the pellet is preferable. The specular surface is necessary because rough surfaces reflect incident radiant flux in both specular and diffuse components. The application of the Fresnel equations to determine  $N(\nu)$  implicitly assumes that there is no diffuse reflectance. If diffuse reflectance is present, then values of  $N(\nu)$  for dielectric minerals computed from measurements of the specular component will have  $n(\nu)$ too small and  $k(\nu)$  too large. The random orientation of particles within the pellet is desirable so that  $N(\nu)$  is representative of all F 

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TABLE V. Data for natural minerals pressed into pellets

Mineral		Hardness	و <mark>س</mark> (g. cm <sup>3</sup> )	م(2/cm <sup>3</sup> )	۳ م/م	ę	n (589 nm) P	ո <sub>p</sub> (2.5 µm)
Colemanite	<b>8T</b>	4.5	2.40	2.06	0.858	1.586 - 1.614	1.301 (1.356)	1.311 (1.368)
Gypsum	8T	2.0	2.32	2.10	0.905	1.5205 - 1.5296		1.344 (1.381)
Illite	8T	2.0	2.70-2.78	2.46	0.894	1.555 - 1.610	1.195 (1.174)	1.331 (1.367)
Kaolin	81	2.0-2.5	2.57-2.68	2.13	0.810	1.553 - 1.570	1.263 (1.326)	1.341 (1.426)
Kernite	8T	2.5	1.73	1.91	1.10	1.454 - 1.488	1.285 (1.256)	1.283 (1.254)
Limonite (Al.)	81	5.0-5.5	4.09-4.48	2.97	0.694	2.150 - 2.415	1.225 (1.335)	1.40 (1.619)
Limonite (Ga.)	8T	5.0-5.5	4.09-4.48	2.40	0.561	2.150 - 2.415		
Montmorillonite	8Т	1.0-2.0	1.98-2.06	2.19	1.10	1.475 - 1.534		
Pyrolusite	8Т	1.0-2.0	4.75	3.48	0.732	1.303 - 1.623	1.176 (1.244)	1.418 (1.604)
Vermiculite (Cn.)	31	1.5-2.0	2.26-2.35	1.95	0.848	1.525 - 1.581		
Vermiculite (Id.)	3T	1.5-2.0	2.26-2.35	2.00	0.869	1.525 - 1.561		
Wavellite	8Т	3.5-4.0	2.31-2.46	2.00	0.851	1.520 - 1.561	1.259 (1.315)	1.235 (1.283)
Gypsum	14T	2.0	2.32	2.21	0.952	1.5205 - 1.5296		1.420 (1.444)
Pyrolusite	<b>16</b> T	1.0-2.0	4.75	3.44	0.724	1.303 - 1.623		1.882 (1.998)

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optical directions within the crystal. The effect of surface roughness on measurements of specular reflectance has been investigated by Bennet et. al. (1961).

This method of pressing pellets, measuring their specular reflectance, and computing N(v) from the reflectance spectrum was previously applied by Toon (1977) to montmorillonite and by Volz (1973) to  $(NH_{4})_2 SO_4$ . Toon (1976) has suggested that although diffuse reflectance is present with pellet surfaces one may be able to obtain values of N(v) from the specular reflectance that are adequate for Mie scattering computations.

The purpose of this investigation was to determine the validity of N( $\nu$ ) obtained from measurements of the specular component of reflectance from pellet surfaces. Natural minerals investigated by use to the pellet method are listed in column 1 of Table V. The hardness (Mohs Scale) and density  $\rho_m$  of these minerals are listed in columns 2 and 3, respectively. The density of the pellets  $\rho_p$  and the ratio  $\rho_p / \rho_m$  are listed in columns 4 and 5, respectively. The range of refractive indices  $n(\nu)$  at 589 nm wavelength (Sodium D lines) for the mineral is listed in column 6 and for the pellet in column 7. In column 7 values n in parenthesis have been corrected for density by applying the Lorentz-Lorenz formula

$$\frac{(n^2-1)}{(n^2-2)} = \frac{\rho_m (n_\rho^2-1)}{\rho_p (n_\rho^2+2)}$$
(12)

which provides

$$n^2 = (1 + 2a)/(1 - a),$$
 (13)

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$$\mathbf{a} = \frac{\rho_{\rm m}(n_{\rm \rho}^{2}-1)}{\rho_{\rm p}(n_{\rm \rho}^{2}+2)} \,. \tag{14}$$

Similarly, values of  $n_p$  at 2.5  $\mu m$  are listed in column 8 of Table V. Values of k(v) for these minerals are not available in the literature thus similar comparisons for k(v) could not be made.

1. Gypsum

A part of the investigations of gypsum were discussed in Section VD. Additional investigations of the optical properties of gypsum in the infrared are described in this section. Those additional investigations consisted of additional reflectance measurements on the same gypsum pellet discussed in Section VD. The pellet, however, was repressed with 14 tons of force applied to the 13 mm pellet rather than 8 tons. These will be referred to as the 14T and 8T pellets. Also, transmittance measurements were made for minute quantities of gypsum mixed with KBr and pressed into 13 mm dia. pellets.

The specular reflectance spectra of gypsum pellets pressed with 8 tons and 14 tons of force and the ratio of the specular reflectance of the 8T pellet to that of the 14T pellet is shown in Fig. F1-1. We conclude from the ratio reflectance spectrum shown in Fig. F1-1 that (1) the 14T pellet provided greater specular reflectance throughout the spectrum, (2) there are possible slight shifts in the infrared bands for the 8T and 14T pellets, and (3) the 14T pellet had a much smoother surface. The decrease in relative reflectance with increasing wave number (decreasing wavelength) indicates that the 14T pellet should yield superior values of N( $\nu$ ) for gypsum "powder". Values for n( $\nu$ ) and k( $\nu$ ) computed by Kramers-Kronig methods



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applied to the specular reflectance spectrum of the 14T pellet are presented in Figs. F1-2 and F1-3, respectively.

The specular reflectance R at normal inidence for a smooth surface is given by

$$R = \frac{(n-1)^2 + k^2}{(n+1)^2 + k^2}.$$
 (15)

Thus we see that measurements of R are sensitive to  $k^2$ where k is the imaginary part of N(v). If k =0.05, then  $k^2$ =0.0025 and reflectance measurements with some degree of confidence in the fourth significant digit would be required to determine k. Typical uncertainty in our reflectance measurements is ( $\Delta R/R$ )=0.025, which, at best, provides some degree of confidence in the third significant digit. An analysis of undertainties in  $\Delta N=\Delta n+i\Delta k$  was presented in Section VC.

In order to determine better values of k for Gypsum powder we mixed varying minute quantities of Gypsum powder with KBr and pressed the mixtures into 13 mm dia. pellets. Thirteen separate gypsum/KBr pellets were formed and transmittance spectra were obtained in the  $300-4,000 \text{ cm}^{-1}$ region. Transmittance spectra for three of the pellets are shown in Fig. F1-4. From the thirteen transmittance spectra four spectra were chosen which possessed the least scattering that is characteristic of some KBr pellets.



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These four transmittance spectra were converted to absorbance spectra and the six possible subtractions of one absorbance spectrum from another were made, this resulted in six difference spectra. Three absorbance spectra and the six difference spectra are shown in Figs. F1-5 & F1-6. The three difference spectra possessing the least scattering were then chosen for further analysis. Before we describe the analysis of the three chosen difference spectra, let us cast the procedures in this paragraph into mathematical form.

Let us assume that the fractional transmittance T through a gypsum/KBr pellet is given by

$$\Gamma = \frac{(1-R)^2 e^{-\alpha x}}{1-R^2 e^{-2\alpha x}},$$
 (16)

where R is the reflectance of the surfaces of the KBr pellet,  $\alpha$  is an attenuation coefficient due to absorption by the gypsum and scattering by the gypsum and KBr particles, and x we assign to the effective thickness of the gypsum in the pellet. Let us further assume that n for the KBr is 1.4-1.5 so that R=0.04 and R<sup>2</sup>=0.0016. Furthermore, the largest that  $e^{-2\alpha x}$  will be is 1 corresponding to  $\alpha$ =0; thus we may write for our gypsum/KBr pellet

 $T = (1-R)^2 e^{-\alpha x}$  (17)





$$A = -2 \log (1-R) + \alpha xc$$
 (18)

$$= -2 \log(1-R) + c\alpha_a x + \alpha_s tc, \qquad (19)$$

where we have recast  $\alpha x$  into the form  $\alpha x = \alpha_a x + \alpha_s t$  which represents absorption a and scattering s, and c=0.43429. Again, x represents the effective thickness of the gypsum and t is the thickness of the gypsum/KBr pellet. A difference between two absorbance spectra is

$$A_{2}-A_{1} = -2 \log[(1-R_{2})/(1-R_{1})] + c\alpha_{a}(x_{2}-x_{1}) + (c\alpha_{s}\tau)_{2} - (20)$$

$$(c\alpha_{s}\tau)_{1}$$

Assuming  $R_1 = R_2$  and  $(\alpha_s t)_1 = (\alpha_s t)_2$  we have

$$\mathbf{A}_{2} - \mathbf{A}_{1} = \mathbf{c}^{\alpha}_{a} (\mathbf{x}_{2} - \mathbf{x}_{1});$$
(21)

$$= c^{4\pi} k^{\nu} (x_2 - x_1).$$
 (22)

Thus, if the gypsum/KBr pellets are adequately prepared the difference spectra  $A_2$ - $A_1$  is directly proportional to k. However, one can not measure the effective thickness x of the gypsum in the pellet.

We now return to the further analysis of the three

difference spectra. The primary difference between two difference spectra is in the factors  $x_2-x_1$  which cannot be measured. Two of the three difference spectra were thus normalized to the third difference spectrum. The normalization factor was an average of such factors determined at the centers of the strong absorption bands of gypsum where k is relatively large. The average of the three normalized difference spectra was divided by 4mv throughout the  $300-4,000 \text{ cm}^{-1}$  region. This process produced the relative k spectrum shown in Fig. F1-7 and F1-8. Actually the relative k spectrum is a product  $ck\Delta x$ spectrum. The smoothed fractional standard deviation  $\Delta k/k$ is shown in Fig. F1-9;  $\Delta k/k$  was obtained as a byproduct of averaging the three normalized difference spectra. The ordinate scale for  $\Delta k/k$  in Fig. F1-9 is from 0 to 1.0; note that  $\Delta k/k$  is very large in regions where k is very small but is less than  $\Delta k/k$  for KK analysis for small k.

It is impossible to determine the effective thickness x of the Gypsum in the pellets. Thus we applied a calibration factor to the relative k spectrum shown in Figs. F1-7 and F1-8. The calibration factor was determined in the following manner. Values of k were available from Kramers-Kronig analysis of the reflectance spectrum of the Gypsum pellets. At the centers of four of the strong infrared bands the ratios of k values from KK analysis to

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Figure F1-7. Relative k spectrum for gypsum from the average of three

normalized difference spectra of the gypsum-powder/KBr

pellets; 300-4,000 cm<sup>-1</sup> wave-number region.





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relative k values were computed and averaged. The average of the four ratios was the calibration factor applied to the relative k spectrum throughout the  $300-4,000 \text{ cm}^{-1}$ region. The calibration factor corresponded to  $1/c\Delta x$ . Values of k determined in this manner are shown graphically as the dashed line in Fig. F1-10. The solid line in Fig. F1-10 is the k spectrum determined by KK analysis of the reflectance spectrum of the 8T Gypsum pellet.

We noted from Fig. F1-10 that the infrared band at 3,550  $cm^{-1}$ , which is a characteristic of the Y optical direction of Gypsum, is stronger from the transmittance measurements of the Gypsum/KBr pellet than from KK analysis of the reflectance spectrum of the 8T pellet. We attribute this to a more random orientation of the Gypsum particles in the Gypsum/KBr pellet than in the 8T Gypsum pellet. Preferred (010) orientation of the Gypsum particles in the 8T pellet was described in Section VD of this report. Also, we note from Fig. F1-10 that in spectral regions where k is ralatively small that k values from the transmittance measurements yield more accurate values of k. There is a general increase in base level k values for KK analysis from about 1,300 cm<sup>-1</sup> to 4,000 cm<sup>-1</sup> which would be expected as diffuse reflectance increases as frequency increases. The diffusely reflected radiant flux will be interpreted by the KK algorithms as absorption and k values

analysis (solid line) of the reflectance spectrum of the measurements of the gypsum-powder/KBr pellets, 300-4,000 Figure F1-10. Comparison of k spectra for gypsum obtained from KK 8T pellet and from transmittance (dahsed line) cm<sup>-1</sup> region.



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will thus increase as diffuse reflectance increases. This is exactly the situation that we observe with the 8T Gypsum pellet.

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$$R = \frac{(Z - \cos \theta) (Z^{*} + \cos \theta)}{/Z + \cos \theta/^{2}}$$
(23)

$$Z^2 = N^2 - \sin^2 \theta. \tag{24}$$

Values of n were systematically adjusted by use of a least squares method in Eqns. (23) and (24) until the measured value of R was obtained. The n spectrum thus obtained is the dashed curve in Fig. F1-11. The solid-line curve in Fig. F1-11 is the n spectrum of the 8T pellet. Differences in the two n spectra in Fig. F1-10 were attributed to differences in the orientation of Gypsum particles in the Gypsum/KBr pellet and the 8T Gypsum pellet.

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analysis (solid line) of the reflectance spectrum of the measurements and the reflectance spectrum of the pellet; 8T pellet and from application of the fresnel equation Figure F1-11. Comparison of n spectra for gypsum obtained from KK (dashed line) to the k spectrum from transmittance 300-4,000 cm<sup>-1</sup> region.

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## 2. Pyrolusite

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Pyrolusite MnO<sub>2</sub> is a tetragonal optically uniaxial opaque mineral of the 4/m 2/m 2/m lattice and space group and has a structure the same as that of Rutile. Pyrolusite is rarely found in well developed crystals. Our Pyrolusite sample was black in color and took on a metallic luster when pressed into pellets. Two pellets were prepared; one with 8 tons of force and the other with 16 tons of force applied to the 13 mm dia. surface. The powder used to prepare the 16T pellet was much smaller in particle size than that used for the 8T pellet. The 16T pellet possessed a more metallic luster than the 8T pellet due to the smaller particle size and the factor of 2 increase in the pressure used to form the pellet.

The reflectance spectrum for the 8T Pyrolusite pellet is shown in Fig. F2-1 for the 0.2-50  $\mu$ m wavelength range. The real and imaginary parts of N obtained by applying KK analysis to the reflectance spectrum of the 8T pellet are presented in Figs. F2-2 and F2-3, respectively.

The reflectance spectra of the 8T and 16T Pyrolusite pellets in the 180-4,000 cm<sup>-1</sup> spectral range are presented in Fig. F2-4. The ratio reflectance spectrum R(8T)/R(16T)of Pyrolusite in the 180-4,000 cm<sup>-1</sup> spectral range is shown in Fig. F2-5. Note that the 8T pellet specularly reflected much less than the 16T pellet at nearly all spectral

positions. The shape of the reflectance spectrum for the 16T pellet and the visual appearance of the 16T pellet suggest that there was probably increasing diffuse reflectance as the frequency increased. However, black metallic materials such as graphite exhibit decreasing reflectance with increasing frequency through the infrared and visible spectral regions. The reflectance of black metallic Pyrolusite will probably bear some similarities to that of graphite and decrease with increasing frequency from about 2,000 cm<sup>-1</sup> in the infrared to about 50,000 cm<sup>-1</sup> in the ultraviolet.

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Spectral values of n and k from KK analysis of the reflectance spectrum of the 16T pellet are presented graphically in Figs. F2-6 and F2-7, respectively.

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180-4,000 cm<sup>-1</sup> wave-number region.

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Figure F2-7. Extinction coefficient k for the 16T Pyrolusite pellet in the 180-4,000 cm<sup>-1</sup> wave-number region.

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## 3. Alabama Limonite

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Limonite is primarily composed of Goethite ( $\alpha$ -FeOOH). Limonite (FeOOH.nH<sub>2</sub>O) is a mineralogy field term referring to natural hydrous iron oxides of uncertain identity. The reflectance spectrum in the 0.2-50  $\mu$ m wavelength region for an 8T Alabama Limonite pellet is shown in Fig. F3-1. Spectral values of n and k determined by applying KK analysis to the reflectance spectrum of the 8T Alabama Limonite pellet are presented graphically in Figs. F3-2 and F3-3, respectively. The sample was yellow-orange in color. An 8T Georgia Limonite pellet had similar optical properties.



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4. Kaolin

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Kaolin, a member of the clay mineral group, is composed primarily of Kaolinite which is Triclinic and thus optically biaxial. The specular reflectance spectrum at 6.5 deg. angle of incidence in the 0.2-50 µm wavelength region for an 8T Kaolin pellet is shown in Fig. E4-1. Spectral values of n and k from KK analysis of the reflectance spectrum of the 8T Kaolin pellet are presented graphically in Figs. F4-2 and F4-3, respectively.

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Figure F4-2. Index of refraction n of the 8T Kaolin pellet in the 0.2-

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5. Illite

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Illite is an hydromuscovite mineral of clay particle size ( $2 \mu m$ ). Hydromuscovite is a monoclinic optically biaxial crystal with perfect (001) cleavage and a hardness of 2. The specular reflectance spectrum at 6.5 deg. angle of incidence in the 0.2-50  $\mu m$  wavelength region for an 8T Illite pellet is shown in Fig. F5-1. Spectral values of n and k obtained by KK analysis of the reflectance spectrum of the 8T Illite pellet are presented graphically in Figs. F5-2 and F5-3, respectively.

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0.2-50 µm wavelength region.

6. <u>Colemanite</u>

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Colemanite is a monoclinic optically biaxial crystal of the 2/m lattice and space group. It is transparent colorless to white in color. The specular reflectance at 6.5 deg. angle of incidence in the 0.2-50  $\mu$ m wavelength region for an 8T Colemanite pellet is shown in Fig. F6-1. Spectral values of n and k obtained from KK analysis of the reflectance spectrum of the 8T Colemanite pellet are presented grpahically in Figs. F6-2 and F6-3, respectively.



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Figure F6-2. Index of refraction n of the 8T Colemanite pellet in the the 0.2-50 µm wavelength region.

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the 0.2-50 µm wavelength region.

7. Kernite

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Kernite is a monoclinic optically biaxial mineral which is found in nonmarine evaporites and salt pans; it is a metamorph of Boxax. The specular reflectance spectrum at 6.5 deg. angle of incidence in the 0.2-50  $\mu$ m wavelength region is shown in Fig. F7-1. Spectral values of n and k obtained from KK analysis of the reflectance spectrum of the 8T Kernite pellet are presented graphically in Figs. F7-2 and F7-3, respectively.

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Figure F7-1. Reflectance spectrum of the 8T Kernite pellet in the 0.2-

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Figure F7-2. Index of refraction n of the 8T Kernite pellet in the 0.2-

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Figure F7-3. Extinction coefficient k of the 8T Kernite pellet in the

0.2-50 µm wavelength region.

## 8. Wavellite

Wavellite is an orthorhombic optically biaxial crystal of the 2/m 2/m 2/m lattice and space group. Single crystals of wavellite are rare. The specular reflectance spectrum at 6.5 deg. angle of incidence in the 0.2-50 µm wavelength region for an 8T wavellite pellet is shown in Fig. F8-1. Spectral values of n and k obtained by KK analysis of the reflectance spectrum of the 8T wavellite pellet are presented in Figs. F8-2 and F8-3, respectively.



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## 9. Montmorillonite

Montmorillonite is a monoclinic optically biaxial clay mineral. The specular reflectance spectrum of 6.5 deg. angle of incidence in the 2.5-50  $\mu$ m wavelength region is shown in Fig. F9-1 for the 8T pellet. Spectral values of n and k obtained from KK analysis of the reflectance spectrum of the 8T montmorillonite pellet are presented graphically in Figs. F9-2 and F9-3, respectively. The reflectance spectrum was also measured in the 0.2-2.5  $\mu$ m wavelength region but was judged to be in error and thus is not included in this report.







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Figure F9-3. Extinction coefficient k of the 8T Montmorillonite pellet

in the 2.5-50 µm wavelength region.

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10. Vermiculite

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Vermiculite is an altered form of Biotite with a structure similar to that of talc. Pellets of Vermiculite were very difficult to separate from the stainless steel rams between which the pellets were pressed. Only at very low relative pressure could the separation be made and then some of the Vermiculite would stick to the rams thus yielding a poor surface. Two pellets, a 3T pellet of Idaho Vermiculite and a 3T pellet of Connecticut Vermiculite were pressed and reflectance spectra were obtained. The spectra were of such poor quality due to the roughness of the surface that they were not included in this report.

Any future investigations of the optical properties of Vermiculite should be transmittance measurements of cleaved natural cyrstals. However, this would yield only the optical properties in the Y and Z optical directions and not in the X optical direction.
#### 11. Chalcedony

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Chalcedony is a term referring to several fibrous varieties of low quartz. Our sample was solid and appeared to be a polycrystalline material with red to pink colored impurities. The sample was cut, polished, and the reflectance spectrum at 6.5 deg. angle of incidence was measured throughout the 0.2-50  $\mu$ m wavelength region. The reflectance spectrum for the 0.2-2.5  $\mu$ m region is shown in Fig. F11-1, and for the 2.5-55  $\mu$ m (5,000-180 cm<sup>-1</sup>) region in Fig. F11-2. The KK analysis of reflectance spectrum yielded negative values of k in some spectral regions, particularly in the band near 0.3  $\mu$ m. We believe that band may thus be due to fluoresence (emission) rather than reflection. Because this problem was not fully understood values of n and k were not presented here.

#### G. Diesel Fuel

The reflectance spectra of diesel fuel at 6.5 degrees angle of incidence was remeasured during this contract in order to eliminate some spectral artifacts due to vapor from the water standard that was used for previous measurements of reflectance. A first surface aluminum mirror was used for these measurements. The absolute reflectance of diesel fuel is shown in Fig. G-1 for the  $180-4,000 \text{ cm}^{-1}$  spectral region. Spectral values of n and k obtained from KK analysis of the reflectance spectrum are presented graphically in Figs. G-2 and G-3, respectively.



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# H. $ZnC_{1/2}/H_2O$ Solutions and $H_3PO_4/H_2O$ Solutions

We had previously measured the reflectance spectra and computed spectral values of n and k in the 2-33  $\mu$ m wavelength region for 20/80, 30/70, 40/60, 50/50, 65/35, and 75/25 percent by weight ZnCl<sub>2</sub>/H<sub>2</sub>O solutions. During this contract we measured the reflectance spectra of similar solutions in the 0.2-2.0  $\mu$ m wavelength region and computed values of n. Values of k for these solutions were too small to determine accurately by use of reflectance measurements and therefore are not presented here. The reflectance spectra and spectral values of n for these ZnCl<sub>2</sub>/H<sub>2</sub>O solutions are presented graphically in Figs. H-1 -H-12.

Similarly reflectance spectra were measured and spectral values of n were determined for 5/95, 10/90, 20/80, 40/60, 50/50, 65/35, 75/25, and 85/15 percent by weight  $H_3PO_4/H_2O$  solutions. The reflectance spectra and spectral values of n for the  $H_3PO_4/H_2O$  solutions are presented graphically in Figs. H-13 - H-18.



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H10. Index of refraction n of the 65/35 ZnCl<sub>2</sub>/H<sub>2</sub>O solution in Figure

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H<sub>3</sub>PO<sub>4</sub>/H<sub>2</sub>O solution in the 2,500-50,000 cm<sup>-1</sup> wave-number region 211

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Figure H16. Index of refraction n of the 40/60, 50/50, and 65/35\$

H<sub>3</sub>PO<sub>4</sub>/H<sub>2</sub>O solutions in the 2,500-50,000 cm<sup>-1</sup> wave-number region. 213

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## J. Complex Refractive Indices of Water

Hale and Querry (1973) previously published values of the complex refractive index of water in the 200 mm to 200  $\mu$ m wavelength range. Their investigation was based on a KK analysis of a k spectrum for water compiled from about 80 papers in the scientific literature. The KK analysis provided spectral values of n. Other measurements of the optical properties of water have been published since 1973. Thus we have incorporated these new values of k into the k spectrum and determined the complex refractive index of water in the  $10^{-3}$  to  $10^{6}$  cm<sup>-1</sup> range. The following M.S. thesis by Mr. David Segelstein describes our updated investigations of the complex refractive index of water.

# THE COMPLEX REFRACTIVE INDEX OF WATER

A THESIS IN Physics

Presented to the Faculty of the University of Missouri-Kansas City in partial fulfillment of the requirements for the degree

MASTER OF SCIENCE

by DAVID J. SEGELSTEIN

B.A., Columbia University, 1971 J.D., University of Missouri-Kansas City, 1975

Kansas City, Missouri 1981

# THE COMPLEX REFRACTIVE INDEX OF WATER

David J. Segelstein, Master of Science University of Missouri-Kansas City, 1981

### ABSTRACT

A spectrum of the imaginary part of the complex index of refraction for water as a function of wave number was compiled from the literature and theoretical considerations. The spectrum ranged from  $10^{-6}$  through  $10^8$  cm<sup>-1</sup>. The curve was adjusted within the limits of error for the data used until an electronic sum rule gave proper results. The spectrum was then appropriately Fourier transformed to yield the real part of the complex refractive index. The results of several calculations over various ranges were combined into one spectrum over the range  $10^{-3}$  through  $10^6$  cm<sup>-1</sup>. Both real and imaginary parts are presented in graphical and tabular form.

This abstract of 106 words is approved as to form and content.

Marvin R. Querry

The undersigned, appointed by the Dean of the School of Graduate Studies, have examined a thesis entitled "The Complex Refractive Index of Water," presented by David J. Segelstein, candidate for the degree Master of Science, and hereby certify that in their opinion it is worthy of acceptance.

Marvin R. Querry, Ph.D. Department of Physics

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John R. Urani, Ph.D. Department of Physics

Wai Yim Ching, Ph.D. Department of Physics

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# ACKNOWLEDGMENTS

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I would like to thank the faculty of the Physics Department of the University of Missouri-Kansas City for struggling so tirelessly to bring me to this point. I would especially thank Dr. Marvin Querry, who is the most patient individual I have ever met, for his generous and warm guidance whenever it was requested. I would also express my gratitude to the entire staff of the University of Missouri-Kansas City Computer Center for their kind tolerance of my constant pestering, and for their always competent assistance.

#### CHAPTER I

#### INTRODUCTION

Water is one of earth's most common and important substances. Information concerning its optical properties is of great significance in many areas of science and engineering. Knowledge of its properties is a first step, for example, in the ability to interpret data on aqueous solutions, including the oceans and the atmosphere. Water is also interesting because it serves as a challenging object for the application of the full analytical power of classical electromagnetic theory. One tool in the analysis of its optical properties is the complex refractive index N(y) as a function of wave number:

$$N(v) \equiv n(v) + ik(v) \qquad (1.1)$$

where the wave number, v, is defined as the inverse of wavelength, and has units of cm<sup>-1</sup>. From N(v) one can calculate a variety of optical properties such as reflectance, transmittance, emittance, and Mie scattering parameters at any spectral location.

The purpose of the research described in this thesis was a determination of N(v) for water throughout the wave number region of from  $10^{-3}$  to  $10^{6}$  cm<sup>-1</sup>. This corresponds to a frequency range of from  $10^{7}$  to  $10^{16}$  Hz, a wavelength range of from 100 Å to 10 m. This task has been undertaken previously by other investigators, but not over such a broad spectral region.

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Survey of the Literature

In 1973, Hale and Querry<sup>1</sup> reported optical constants for the region 50 to  $5 \times 10^4$  cm<sup>-1</sup> (200 nm to 200 µm wavelength). They compiled a composite spectrum of k(v), the extinction coefficient, from 58 sources representing data reported over a span of 81 years prior to their paper. This spectrum was transformed by Kramers-Kronig analysis to a spectrum of n(v) for the region reported.

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Some of the data used by Hale and Querry were incomplete or postulated. For example, a Gaussian-shaped absorption band was postulated for k(v) with a peak in the area of  $1.25 \times 10^6$  cm<sup>-1</sup> (80 Å wavelength). This would be the peak associated with the K-edge for electronic absorption. Also, the higher wave-number side of an absorption peak reported at approximately  $1.2 \times 10^5$  cm<sup>-1</sup> was postulated to be of Gaussian shape and appropriate width. These deficiencies were recognized by Hale and Querry, and were the basis for their implication that more and better data were needed for more accurate determination of N(v).

Since the 1973 paper by Hale and Querry, there have been additional compilations of n(v), k(v), or  $\alpha(v)$ , the latter being the Lambert absorption coefficient. It is defined in terms of <u>I</u>, the intensity, as the fractional decrease in intensity over distance:

$$\alpha(v) \equiv -\frac{1}{I}\frac{dI}{dx} = 4\pi k(v)v \qquad (1.2)$$

Of the more recent literature, the following are notable:

A report by Heller, Hamm, Birkhoff, and Painter<sup>2</sup> appeared in

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1974. The authors obtained n(v), k(v),  $\varepsilon_r(v)$ , and  $\varepsilon_i(v)$ , the latter two being the real and imaginary parts of the dielectric function,  $\varepsilon(v)$ , for the range  $6.1 \times 10^4$  to  $2.1 \times 10^5$  cm<sup>-1</sup> (48 to 163 nm wavelength). Reflectance was measured and the above constants were calculated by Kramers-Kronig analysis.

A 1975 paper by Downing and Williams<sup>3</sup> reported values for n(v), k(v), and a(v) for the region 10 to 5000 cm<sup>-1</sup> (2 µm to 1 mm wavelength). The values of k(v) were obtained by measurement and by calculation from reflectance data. The results for n(v) were determined by either Kramers- Kronig analysis or by calculation from reflectance and phase shift data, depending on whether accurate values of k(v) were available for the particular region.

A communication by Kopelevich<sup>4</sup> reported in 1976 discussed the range  $1.7 \times 10^4$  to  $4 \times 10^4$  cm<sup>-1</sup> (250 to 600 nm wavelength). The author criticized the values of k(v) used by Hale and Querry in their 1973 paper. The claim was that water samples in the measurements relied upon were not pure enough. Kopelevich asserted that lower values of k(v) were inherently better because they indicated a more pure sample.

A 1977 report by Afsar and Hasted<sup>5</sup> gave  $\alpha(v)$ , k(v), and n(v)for the range 6 to 450 cm<sup>-1</sup> (22 µm to 1.7 mm wavelength). These were calculated from reflectance data obtained by use of a Fourier-transform spectrophotometer, with an improved liquid cell and a more accurately measured reference interferogram, as compared with earlier measurements of the same type.

In a paper published in 1978, Querry, Cary, and Waring<sup>b</sup> reported

values for  $\alpha(v)$  for the region  $1.5 \times 10^4$  to  $2.4 \times 10^4$  cm<sup>-1</sup> (418 to 640 nm wavelength). These were experimental data obtained by a split-pulse laser method of measuring attenuation.

Tam and Patel<sup>7</sup> gave values for  $\alpha(v)$  for the interval 1.44x10<sup>4</sup> to 2.24x10<sup>4</sup> cm<sup>-1</sup> (446 to 694 nm wavelength) in a paper published in 1979. The technique used was pulsed dye-laser optoaccustic spectroscopy. The method eliminated the detection of spurious attenuation due to scattering.

In addition to the above data, there are relations which can be used to obtain reasonable data for optical constants. For example, in the region below approximately ten  $cm^{-1}$ , the semi-empirical Cole-Cole equation<sup>8</sup> gives sound values for the real and imaginary parts of the dielectric function. In the neighborhood of the oxygen K-edge, at 4.35x10<sup>6</sup> cm<sup>-1</sup>, the shape of the absorption curve above and below the discontinuity can be obtained from an empirical equation which gives the mass absorption coefficient as a power of wavelength.<sup>9</sup> One can find the height of the discontinuity from an empirically obtained relationship between the jump in the mass absorption coefficient across the K-edge and the atomic number.<sup>10</sup> Given these determinations, one needs only some data in the vicinity of the discontinuity to fix the position of the curve. These data are available.

# Description of the Research

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With the addition of the above data, it was hoped that a more reliable spectrum of N(v) could be obtained. The program was, first, to obtain reasonable values for  $\alpha(v)$ , or equivalently k(v), from the

literature and the relations mentioned above. These values would span the range from  $10^{-6}$  cm<sup>-1</sup>, the end of the spectrum obtained from the Cole-Cole equation, to  $10^{15}$  cm<sup>-1</sup>, the region for which the power law relation gives reasonable predictions. The compilation of this  $\alpha(v)$ spectrum is described in Chapter II.

This spectrum of  $\alpha(v)$  was tested for accuracy by use of a sum rule describing the contributions of electronic absorption. The spectrum was adjusted in the region from the low wave-number side of the absorption peak at  $1.14 \times 10^5$  cm<sup>-1</sup> to the bottom of the K-edge discontinuity. The adjustment was made, well within the experimental error stated for the data used, until the electronic sum rule indicated ten electrons.

The  $\alpha(v)$  spectrum was then appropriately Fourier transformed to give n(v) for the range  $10^{-3}$  to  $10^{6}$  cm<sup>-1</sup>. The Fourier transform technique is equivalent to conventional Kramers-Kronig analysis, as is shown in Chapter III. The advantage is in the ability to use the digital FAST FOURIER TRANSFORM yielding equivalent results with much less computing time.

The theoretical development of the Kramers-Kronig relations, their extension to a Fourier transform relationship, and the electronic sum rule derivation are presented in Chapter III. The application to direct computation is described in Chapter IV. Spectral values of N(v) are presented in tabular and graphical form in Chapter V. The results are discussed in Chapter VI.

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#### CHAPTER II

## ACQUISITION OF DATA

## The Middle Range

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So as not to discard the baby with the bath water, the absorption spectrum used by Hale and Querry was retained except where better data were available. Replacement of data began in the visible region.

A significant area of contention has been the purity of water samples for experimental determination of extinction coefficients in the visible region. The question involves how much intensity is lost due to scattering, a phenomenon which is aggravated by the presence of particles, bubbles, or other impurities. That was the substance of the objection by Kopelevich to the data used by Hale and Querry. The difficulty is neatly avoided by the technique of optoacoustic spectroscopy, as used by Tam and Patel. The method relies on the generation of transient acoustic waves by any material which absorbs a light pulse. Data were obtained by detection and comparison of sound waves over the particular range of frequencies of input light. The light source was a pulsed dye laser. Since there is no reliance on the intensity of light surviving passage through the sample, scattering is not involved. Tam and Patel measured only absorption.

The data of Tam and Patel were incorporated into the spectrum. The next task was to find values for  $\alpha(v)$  which joined continuously

with that data. At the lower end,  $1.44 \times 10^4$  cm<sup>-1</sup>, the data of Tam and Patel joined almost precisely with that of Hale and Querry. Nothing additional was required. At the high end, however,  $2.24 \times 10^4$  cm<sup>-1</sup>, there was no real agreement among investigators up to the area of  $5 \times 10^4$  cm<sup>-1</sup>. After considering data of many researchers, it was found that the most reasonable and the smoothest curve connecting the two areas was obtained by averaging the data of Lenoble and Saint-Guilly<sup>11</sup> with that quoted by Kopelevich.

The range from  $5 \times 10^4$  to  $6.49 \times 10^4$  cm<sup>-1</sup> was left intact with the data of Hale and Querry. There seems to be much agreement as to the values for that region, as is graphically illustrated by Painter, Birthoff, and Arakawa in Figure 4 of their 1969 paper.<sup>20</sup>

In the range  $6.49 \times 10^4$  to  $2.06 \times 10^5$  cm<sup>-1</sup>, the data of Heller, Hemm, Birkhoff, and Painter were used because, at the lower end, the curve fit quite accurately in position and shape with the data below that. Also, as this was the region which would have the greatest effect in adjustments to conform to the sum rule, an inability to reach ten electrons while staying within the experimental error quoted by Heller <u>et al.</u> would have indicated that the data there were inappropriate. Because conformity with the sum rule constraint was obtained while remaining well within the error bars, it was evident that the data were appropriate.

The range above  $2.06 \times 10^5$  cm<sup>-1</sup> is discussed under "High Frequency Data" below. For the other extreme, the part of the spectrum from  $10^{-6}$ to 5 cm<sup>-1</sup> is discussed below in the section entitled "Low Frequency Data." From 5 to 500 cm<sup>-1</sup>, data from Afsar and Hasted were used. Their

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work represents probably the first comprehensive investigation of that range of the spectrum. Further, their technique was advanced as compared with earlier measurements.

To join with the data of Afsar and Hasted, the values of  $\alpha(v)$  obtained by Robertson and Williams<sup>13</sup> fit quite well. In addition, their work was a direct experimental determination of absorption via transmittance measurements. The values of Robertson and Williams were used where they differed from those used by Hale and Querry, namely in the ranges  $5 \times 10^2$  to  $10^3$  cm<sup>-1</sup> and  $3.3 \times 10^3$  to  $4 \times 10^3$  cm<sup>-1</sup>.

# Low Frequency Data

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The behavior of a polar liquid in an alternating field is treated by Debye in his book <u>Polar Molecules</u>.<sup>14</sup> By calculating the distribution function for orientation of the molecules, Debye obtained the following expressions<sup>15</sup>:

$$\varepsilon' = \varepsilon_0 + \frac{\varepsilon_1 - \varepsilon_0}{1 + x^2}$$
(2.1)

$$\varepsilon^{*} = \frac{(\varepsilon_1 - \varepsilon_0)x}{1 + x^2}$$
(2.2)

$$\mathbf{x} = \left(\frac{\varepsilon_1 + 2}{\varepsilon_0 + 2}\right) \omega \tau \tag{2.3}$$

where  $\underline{\varepsilon}' = \varepsilon_{\mathbf{r}'}, \underline{\varepsilon}'' = -\varepsilon_{\mathbf{i}'}, \underline{\tau}$  = the "relaxation time" for the orientation of the molecules,  $\underline{\omega}$  = the angular frequency of the applied field,  $\underline{\varepsilon}_{\underline{0}}$  = the high frequency value for  $\varepsilon$ , and  $\varepsilon_{\underline{1}}$  = the static dielectric constant. The characteristic relaxation time for water at room temperature was calculated by Debye to be approximately  $2.5 \times 10^{-11}$  seconds.<sup>16</sup> This corresponds to a wavelength of the order of one cm. In this region, and for longer wavelengths, the Debye equations should yield good predictions, approaching the low frequency limit smoothly.

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A significant improvement over the Debye relation was made by Cole and Cole in their paper published in 1941. They first wrote the Debye equations in the form<sup>8</sup>

$$\varepsilon^* = \varepsilon_{\omega} + \frac{\varepsilon_0 - \varepsilon_{\omega}}{1 + i\omega\tau_0}$$
(2.4)

where  $\underline{\epsilon}^*$  is the complex dielectric function,  $\underline{\epsilon}_{\underline{o}}$  is the high frequency limit, and  $\underline{\epsilon}_{\underline{o}}$  is the static limit. Then the authors showed that better results are obtainable by writing<sup>17</sup>

$$\varepsilon^* = \varepsilon_{\alpha}^{\alpha} + \frac{\varepsilon_0^{\alpha} - \varepsilon_{\alpha}^{\alpha}}{1 + (i\omega\tau_{\alpha})^{1-\alpha}}$$
(2.5)

where  $\underline{\alpha}$  and  $\tau_0$  are parameters to be determined.

This equation can be used directly to calculate values for the dielectric function, and hence the complex refractive index, in the vicinity of the frequency corresponding to the relaxation time. Values for the parameters  $\varepsilon_0$ ,  $\varepsilon_{\infty}$ ,  $\tau_0$ , and  $\alpha$  are available, for example, from <u>Water, a Comprehensive Treatise</u>, <sup>18</sup> there obtained from experimental results. The values of the parameters in that reference were used in the Cole-Cole equation to calculate the extinction coefficient for

the range 
$$10^{-6}$$
 to 5 cm<sup>-1</sup>.

## High Frequency Data

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In the soft x-ray region, data are scarce. However, the evidence indicates a relationship of the form9

$$\frac{\mu}{\rho} = K\lambda^{n}Z^{m} + \frac{\sigma}{\rho}$$
(2.6)

for the mass absorption coefficient,  $\mu/\rho$ .  $\sigma/\rho$  is the attenuation due to scattering. This yields, since  $\mu = \alpha$ ,

$$\alpha = \rho K \lambda^{n} z^{m} + \sigma$$
 (2.7)

or if scattering is subtracted out,  $(\alpha-\sigma) + \alpha$ , and

$$a = Av^{-n}$$
(2.8)

Thus, the Lambert absorption coefficient is given by some negative power of wave number.

Engström suggests a value for <u>n</u> for the soft x-ray region of somewhat less than three. In the data used for this thesis, <u>n</u> was found to be 2.2297 in the area between  $2.1 \times 10^5$  and  $4.3 \times 10^6$  cm<sup>-1</sup> (the latter location being the bottom of the K-edge), a range corresponding to ultra-soft x-rays. Above the K-edge, <u>n</u> was found to be 2.6257.

This power law relationship was applied in the following manner: Data from the National Bureau of Standards<sup>19</sup> were available for the mass absorption coefficient for the range  $8 \times 10^7$  to  $8 \times 10^{14}$  cm<sup>-1</sup>. These data were extended by extrapolation to the K-edge location at  $4.35 \times 10^6$  cm<sup>-1</sup>. This only assumes that the power <u>n</u> remains constant from the K-edge discontinuity to the slightly higher wave numbers stated.

The magnitude of the discontinuity was determined from Figures 3 and 4 of Engström's book.<sup>20</sup> Those figures indicate, respectively, the ratio of mass absorption coefficients and the difference between the coefficients on either side of the discontinuity. This fixed the bottom of the K-edge and left only the region between  $2.1 \times 10^5$  and  $4.3 \times 10^6$  cm<sup>-1</sup> to be filled in. (Data were available up to approximately  $2.1 \times 10^5$  cm<sup>-1</sup> from the Heller, Hamm, Birkhoff, and Painter work.)

The data were joined between the points  $2.1 \times 10^5$  cm<sup>-1</sup> and the bottom of the K-edge by assuming a linear relationship on a plot of the log of the Lambert coefficient versus the log of the wave number. The slope of this line would then correspond to <u>n</u> in the power law relationship.

The data from the paper of Heller <u>et al</u>. could be adjusted within the experimental limits, and a new line would be calculated each time. This gave an efficient means of adjustment while maintaining self-consistency among all the data.

Data for frequencies above  $10^{15}$  cm<sup>-1</sup> were effectively ignored, that being the range in which absorption predominately involves nonatomic/molecular phenomena. Inclusion of these data would have made use of the electronic sum rule impossible as a measure of the accuracy of the absorption spectrum. Further, since optical properties were 236

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calculated only up to  $10^6$  cm<sup>-1</sup>, inclusion or exclusion of these data would have had negligible if any effect on the results. The means for evaluation of the sum rule in this region above  $10^{15}$  cm<sup>-1</sup> is described below.

# Application of the Sum Rule

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Once the new absorption spectrum was completed, the electronic sum rule was applied to test its accuracy. The sum rule, as derived in Chapter III, in SI units, is

$$Z = \left(\frac{4mc^2 \varepsilon_0}{n_0 e^2}\right) \int_0^\infty \alpha(v) dv$$
 (2.9)

where <u>m</u> is the mass of an electron, <u>c</u> is the speed of light in vacuum,  $\varepsilon_{\underline{0}}$  the permittivity constant, <u>n</u> the number of water molecules per cubic meter, and <u>e</u> the electronic charge.

If numerical values of  $\alpha(v)$  are available up to some appropriate  $v_{max}$ , the integration from  $v_{max}$  to infinity can be done analytically using the inverse power law relationship described above. The sum rule is written

$$z = \left(\frac{4mc^2 \varepsilon_0}{n_0 e^2}\right) \left[\int_0^{v_{\text{max}}} \sigma(v) dv + \int_{v_{\text{max}}}^{\infty} \sigma(v) dv\right]$$
(2.10)

Writing  $\alpha(v) = Av^{-n}$  for  $v \ge v_{max}$ , so that  $\alpha(\infty) = 0$ , and integrating the second term, we obtain

$$z = \left(\frac{4mc^2 \varepsilon_0}{n_0 e^2}\right) \left[ \int_0^{\nu_{\text{max}}} \alpha(\nu) d\nu + \frac{A\nu_{\text{max}}}{(n-1)} \right]$$
(2.11)

Since  $Av_{max}^{-n} = \alpha(v_{max})$ , the result is

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$$z = \left(\frac{4mc^{2}\epsilon_{o}}{n_{o}e^{2}}\right) \int_{0}^{\sqrt{max}} \alpha(v)dv + \left[\frac{4mc^{2}\epsilon_{o}v_{max}}{n_{o}e^{2}(n-1)}\right] \alpha(v_{max})$$
(2.12)

In the calculation of the sum rule integral,  $v_{max}$  was  $2 \times 10^7$  cm<sup>-1</sup>. The value of <u>n</u> was determined from the National Bureau of Standards data to be 2.6257. The numerical integration was done using Simpson's rule. As were all calculations for this research, the computation was done in a Fortran program with an AMDAHL 470 computer.

The first attempt yielded Z = 8.99086. Raising the experimental data of Heller <u>et al</u>. to their maximum within the stated error, except at the end points of the interval used, gave Z = 10.26559. A feature included in the data at  $2.016 \times 10^5$  cm<sup>-1</sup> had been easily smoothed over within the experimental error, and was therefore ignored for the above two calculations. The curve had been made to follow the power law relation from  $1.667 \times 10^5$  cm<sup>-1</sup> to the K-edge. For subsequent calculations, however, the power law relationship was applied only from  $2.083 \times 10^5$  cm<sup>-1</sup> to the K-edge, and the previously ignored feature was included. This had the effect of shifting the curve above its previous position for the entire region of the data calculated from the power law relation. It allowed the data below  $2.083 \times 10^5$  cm<sup>-1</sup> to be kept much closer to the

median experimental values. This is reasonable because the error stated by Heller <u>et al</u>. for the vicinity of  $2.083 \times 10^5$  cm<sup>-1</sup> is 20 percent, while it is 10 percent for the lower wave number regions.

After 16 adjustments, the spectrum yielded 2 = 10.00000. Figures 1 and 2 illustrate the first and last curve in the region of adjustment. Figure 3 is a graph of the final absorption spectrum in full. For the above illustrations,  $\log_{10}^{\alpha}(v)$  is plotted against  $\log_{10}v$ . Further, a graph of the value of the sum rule integral, Z plotted against  $\log_{10}v$ , is included as Figure 4 to show where the significant contributions to the sum rule occur. It is clear that the region of the data of Heller <u>et al</u>. corresponds to the greatest slope of the curve, thereby indicating the most significant contribution to the sum.

With the completion of this compilation, the absorption spectrum was ready to be Fourier transformed to give n(v).

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is plotted against the log of the wave number. The dashed line is the final log of the Lambert absorption coefficient, from 7.079x10<sup>4</sup> to 4.467x10<sup>6</sup> cm<sup>-1</sup>, The Fig. 1. The absorption spectrum in the region of adjustment. The curve obtained, which caused the sum rule integral to yield 10.00000. sharp feature on the right is the K-edge. 240

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5.35000 5.25000 5.05000 5.15000 Log of Mave Number 5.05000 4.95000 5.000 5.110 5.778 5.330 6.100 5.990 5.660 5.440 5.550 5.220 5.880

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Fig. 2. Detail of Figure 1 in the region of the broad absorption peak. The dashed line lies well within the experimental error quoted for the data represented by the solid line. 241

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## CHAPTER III

#### THEORETICAL METHODS

## The Complex Refractive Index

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The laws governing the propagation of electric and magnetic fields are Maxwell's equations. We can find an expression for the fields in a medium which will yield the relationship between absorption and phase velocity, the time response and dielectric functions, dispersion relationships, and sum rules.

Maxwell's equations, in cgs units, are<sup>21</sup>

$$\nabla \cdot \vec{D} = 4\pi\rho \tag{3.1}$$

$$\nabla \cdot \vec{B} = 0 \tag{3.2}$$

$$\nabla \mathbf{x} \, \vec{\mathbf{E}} + \frac{1}{c} \frac{\partial \vec{\mathbf{B}}}{\partial t} = \vec{\mathbf{0}} \tag{3.3}$$

$$\nabla \mathbf{x} \stackrel{+}{\mathbf{H}} = \frac{1}{c} \frac{\partial \vec{D}}{\partial t} = \frac{4\pi}{c} \vec{J}$$
(3.4)

The quantities in the equations are defined as follows:

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 $\vec{E} \equiv$  the electric field  $\vec{D} \equiv$  the electric displacement  $\vec{B} \equiv$  the magnetic induction  $\vec{R} \equiv$  the magnetic field  $\vec{J} \equiv$  the current density  $\rho \equiv$  the charge density

The constitutive relations for  $\vec{D}$ ,  $\vec{H}$ , and  $\vec{J}$  are

 $\vec{D} = \vec{e}\vec{E}$  (3.5)

where  $\underline{\epsilon}$  is the dielectric function,  $\underline{\mu}$  is the magnetic permeability, and  $\underline{\sigma}$  is the conductivity.

For an infinite medium which is charge free ( $\rho=0$ ), homogeneous, isotropic, and linear ( $\epsilon$ ,  $\mu$ , and  $\sigma$  do not depend on position or time), and conducting ( $\sigma\neq0$ ), the equations reduce to

∇ · Ĕ = 0 (3.8)

$$7 \times \dot{f} - \frac{\varepsilon}{c} \frac{\partial \dot{E}}{\partial t} = \frac{4\pi\sigma}{c} \dot{E}$$
(3.11)

Taking the curl of Equation (3.10),

$$\nabla \mathbf{x} (\nabla \mathbf{x} \, \vec{\mathbf{z}} + \frac{\mu}{c} \, \frac{\partial \vec{\mathbf{H}}}{\partial t}) = \nabla \mathbf{x} \, \vec{\mathbf{\sigma}} = \vec{\mathbf{\sigma}}$$

$$\nabla \mathbf{x} \nabla \mathbf{x} \, \vec{\mathbf{z}} + \frac{\mu}{c} \nabla \mathbf{x} \, \frac{\partial \vec{\mathbf{H}}}{\partial t} = \vec{\mathbf{\sigma}}$$
(3.12)

Interchanging the order of differentiation,

$$\nabla \mathbf{x} \nabla \mathbf{x} \, \vec{\mathbf{z}} + \frac{\mathbf{u}}{\mathbf{c}} \, \frac{\partial}{\partial \mathbf{t}} (\nabla \mathbf{x} \, \vec{\mathbf{t}}) = \vec{\mathbf{c}} \tag{3.13}$$

Using the identity  $\nabla x \nabla x \vec{E} = \nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E}$ , and noting from Equation (3.8) that the divergence of  $\vec{E}$  vanishes, we may replace the first term of Equation (3.13) by  $-\nabla^2 \vec{E}$ :

$$-\nabla^2 \vec{E} + \stackrel{\mu}{\leftarrow} \frac{\partial}{\partial t} (\nabla \times \vec{H}) = \vec{0}$$
(3.14)

We obtain the curl of  $\hat{H}$  from Equation (3.11):

$$-\nabla^{2} \vec{E} + \frac{\mu}{c} \frac{\partial}{\partial t} \left( \frac{\varepsilon}{c} \frac{\partial \vec{E}}{\partial t} + \frac{4\pi\sigma}{c} \vec{E} \right) = \vec{0}$$

$$\nabla^{2} \vec{E} - \frac{\mu\varepsilon}{c^{2}} \frac{\partial^{2} \vec{E}}{\partial t^{2}} - \frac{4\pi\sigma\mu}{c^{2}} \frac{\partial \vec{E}}{\partial t} = \vec{0}$$
(3.15)

Similarly, taking the curl of Equation (3.11),

$$\nabla \mathbf{x} (\nabla \mathbf{x} \cdot \vec{\mathbf{H}} - \frac{\varepsilon}{c} \cdot \frac{\partial \vec{\mathbf{E}}}{\partial t}) = \nabla \mathbf{x} (\frac{4\pi\sigma}{c} \cdot \vec{\mathbf{E}})$$

$$\nabla \mathbf{x} \nabla \mathbf{x} \cdot \vec{\mathbf{H}} - \frac{\varepsilon}{c} \cdot \frac{\partial}{\partial t} (\nabla \mathbf{x} \cdot \vec{\mathbf{E}}) = \frac{4\pi\sigma}{c} (\nabla \mathbf{x} \cdot \vec{\mathbf{E}})$$
(3.16)

Obtaining the curl of  $\vec{E}$  from Equation (3.10), and using the same identity for  $\nabla \times \nabla \times \vec{H}$ , with  $\nabla \cdot \vec{H} = 0$  from Equation (3.9),

$$-\nabla^{2} \vec{B} - \frac{\varepsilon}{c} \frac{\partial}{\partial t} \left( \frac{\mu}{c} \frac{\partial \vec{E}}{\partial t} \right) - \frac{4\pi\sigma}{c} \left( \frac{\mu}{c} \frac{\partial \vec{E}}{\partial t} \right) = \vec{0}$$

$$\nabla^{2} \vec{B} - \frac{\mu\varepsilon}{c^{2}} \frac{\partial^{2} \vec{E}}{\partial t^{2}} - \frac{4\pi\sigma\mu}{c^{2}} \frac{\partial \vec{E}}{\partial t} = \vec{0}$$
(3.17)

Thus,  $\vec{E}$  and  $\vec{H}$  both satisfy the same wave equation:

$$\left\{ \nabla^2 - \frac{\mu\varepsilon}{c^2} \frac{\partial^2}{\partial t^2} - \frac{4\pi\sigma\mu}{c^2} \frac{\partial}{\partial t} \right\} \begin{pmatrix} \vec{E} \\ \vec{R} \end{pmatrix} = \vec{0}$$
(3.18)

We assume a solution of the form

$$\vec{E} = \vec{E}_{e} e^{i(\vec{k} \cdot \vec{X} - \omega t)}$$
(3.19)

where  $\vec{E}_{0}$  is a constant vector. With  $\kappa \equiv |\vec{\kappa}|$ , we note the following:

$$\nabla^2 \vec{E} = \vec{E}_o(i\vec{k}) \cdot (i\vec{k}) e^{i(\vec{k}\cdot\vec{x}-\omega t)} = -\kappa^2 \vec{E}$$
(3.20)

$$\frac{\partial \vec{E}}{\partial t} = -i\omega \vec{E}$$
(3.21)

$$\frac{\partial^2 \vec{E}}{\partial t^2} = (-i\omega)(-i\omega) \vec{E} = -\omega^2 \vec{E}$$
(3.22)

Then, substituting Equations (3.20), (3.21), and (3.22) into Equation (3.18),

$$\left\{ \nabla^2 - \frac{\mu\varepsilon}{c^2} \frac{\partial^2}{\partial t^2} - \frac{4\pi\sigma\mu}{c^2} \frac{\partial}{\partial t} \right\} \vec{E} = \left[ -\kappa^2 + \frac{\mu\varepsilon}{c^2} \omega^2 + i\left(\frac{4\pi\sigma\mu}{c^2}\right) \omega \right] \vec{E} \qquad (3.23)$$

The coefficient of  $\vec{E}$  must vanish. This requires that

$$\kappa^{2} = \frac{\mu \varepsilon \omega^{2}}{c^{2}} + i\left(\frac{4\pi\sigma\mu\omega}{c^{2}}\right) \qquad (3.24)$$

Assuming  $\kappa$  is complex, we write  $\kappa \equiv \alpha + i\beta$ . Then,

$$\kappa^{2} = (\alpha + i\beta)^{2} = \alpha^{2} - \beta^{2} + 2i\alpha\beta \qquad (3.25)$$

$$\operatorname{Re}(\kappa^2) = \alpha^2 - \beta^2$$
 (3.26)

$$Im(\kappa^2) = 2\alpha\beta \tag{3.27}$$

To find the real and imaginary parts of  $\kappa^2,$  we assume that  $\epsilon,$   $\mu,$  and  $\sigma$  are complex:

$$\varepsilon \equiv \varepsilon_{r} + i\varepsilon_{i} \tag{3.28}$$

$$\mu \equiv \mu_r + i\mu_i \tag{3.29}$$

$$\sigma \equiv \sigma_{\mu} + i\sigma_{i} \tag{3.30}$$

Then, substituting into Equation (3.24),

$$\kappa^{2} = (\epsilon_{r} + i\epsilon_{i})(\mu_{r} + i\mu_{i})\frac{\omega^{2}}{c^{2}} +$$

$$i4\pi(\sigma_{r} + i\sigma_{i})(\mu_{r} + i\mu_{i})\frac{\omega}{c^{2}}$$
(3.31)

$$\kappa^{2} = \left[ (\epsilon_{\mathbf{r}} \mu_{\mathbf{r}} - \epsilon_{\mathbf{j}} \mu_{\mathbf{j}}) \frac{\omega^{2}}{c^{2}} - 4\pi (\sigma_{\mathbf{j}} \mu_{\mathbf{r}} + \sigma_{\mathbf{r}} \mu_{\mathbf{j}}) \frac{\omega}{c^{2}} \right] + i \left[ (\epsilon_{\mathbf{j}} \mu_{\mathbf{r}} + \epsilon_{\mathbf{r}} \mu_{\mathbf{j}}) \frac{\omega^{2}}{c^{2}} + 4\pi (\sigma_{\mathbf{r}} \mu_{\mathbf{r}} - \sigma_{\mathbf{j}} \mu_{\mathbf{j}}) \frac{\omega}{c^{2}} \right]$$
(3.32)

We then define

$$\gamma \equiv (\epsilon_{r}\mu_{r} - \epsilon_{i}\mu_{i})\frac{\omega^{2}}{c^{2}} - 4\pi(\sigma_{i}\mu_{r} + \sigma_{r}\mu_{i})\frac{\omega}{c^{2}}$$
(3.33)

$$\delta \equiv (\varepsilon_{i}\mu_{r} + \varepsilon_{r}\mu_{i})\frac{\omega^{2}}{c^{2}} + 4\pi(\sigma_{r}\mu_{r} - \sigma_{i}\mu_{i})\frac{\omega}{c^{2}}$$
(3.34)

Thus,

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$$\kappa^2 = \gamma + i\delta \tag{3.35}$$

From Equations (3.26) and (3.27), we obtain

$$\gamma = \alpha^2 - \beta^2 \tag{3.36}$$

$$\delta = 2\alpha\beta \tag{3.37}$$

Using  $\beta = \delta/2\alpha$  from Equation (3.37), the following quadratic results:

$$4\alpha^4 - \delta^2 = 4\gamma\alpha^2 \tag{3.38}$$

$$4(\alpha^2)^2 - 4\gamma(\alpha^2) - \delta^2 = 0$$
 (3.39)

The solutions are

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$$x^{2} = \frac{1}{2} [\gamma \pm (\gamma^{2} + \delta^{2})^{\frac{1}{2}}]$$
(3.40)

Since  $\alpha$  is real,  $\alpha^2$  must be greater than zero. We must choose the plus sign. Therefore,

$$\alpha = \left[\frac{\gamma + (\gamma^2 + \delta^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}}$$
(3.41)

Similarly,  $\alpha = \delta/2\beta$  yields the quadratic

$$4(\beta^2)^2 + 4\gamma(\beta^2) - \delta^2 = 0$$
 (3.42)

with solutions

$$\beta^{2} = \frac{1}{2} \left[ -\gamma \pm (\gamma^{2} + \delta^{2})^{\frac{1}{2}} \right]$$
(3.43)

Again we must choose the plus sign:

$$\beta = \left[\frac{-\gamma + (\gamma^2 + \delta^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}}$$
(3.44)

With the result  $\vec{k} = \kappa \hat{\kappa} = (\alpha + i\beta)\hat{\kappa}$ , the complex phase velocity  $\hat{v}_p$  can be defined:

$$\vec{k} \cdot \vec{x} - \omega t = \text{constant}$$
 (3.45)

$$d(\vec{k}\cdot\vec{x}-\omega t)=0 \qquad (3.46)$$

$$\vec{k} \cdot d\vec{x} - \omega dt = 0 \tag{3.47}$$

$$(\alpha + i\beta) \mathbf{k} \cdot d\mathbf{x} = \omega dt \tag{3.48}$$

$$\hat{\kappa} \cdot d\vec{x} = (\frac{\omega}{\alpha + i\beta}) dt$$
 (3.49)

Measuring  $\hat{v}_p$  in the direction of  $\hat{\kappa}$ ,  $\hat{\kappa} \cdot d\hat{x} = |\hat{\kappa}| |d\hat{x}| = dx$ , and

$$dx = \left(\frac{\omega}{\alpha + 1\beta}\right) dt \tag{3.50}$$

$$\frac{dx}{dt} = \hat{v}_p = \frac{\omega}{\alpha + i\beta}$$
(3.51)

If we define the complex refractive index  $\underline{N}$  as

$$N \equiv \frac{C}{\hat{v}_{p}} \equiv n + ik$$
 (3.52)

we finally obtain

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$$N = \frac{C}{m}(\alpha + i\beta)$$
(3.53)

Thus, with <u>n</u> the real part of the refractive index, and <u>k</u> the imaginary part, the result is

$$n = \frac{c}{\omega} \alpha \tag{3.54}$$

$$\mathbf{k} = \frac{\mathbf{C}}{n} \mathbf{\beta} \tag{3.55}$$

As an example of the relationship between  $\boldsymbol{\varepsilon}$  and N, consider a

non-conducting ( $\sigma=0$ ), non-magnetic ( $\mu=1$ ) material such as water. With these conditions,

$$\gamma = \varepsilon_r \frac{\omega}{c^2}$$
 and  $\delta = \varepsilon_i \frac{\omega}{c^2}$  (3.56)

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Then,

$$\alpha = \left[\frac{\gamma + (\gamma^2 + \delta^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}} = \frac{\omega}{c} \left[\frac{\varepsilon_r + (\varepsilon_r^2 + \varepsilon_1^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}}$$
(3.57)

$$\beta = \left[\frac{-\gamma + (\gamma^2 + \delta^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}} = \frac{\omega}{c} \left[\frac{-\epsilon_r + (\epsilon_r^2 + \epsilon_1^2)^{\frac{1}{2}}}{2}\right]^{\frac{1}{2}}$$
(3.58)

Using Equation (3.53),

$$N = \frac{c}{\omega} \left\{ \frac{\omega}{c} \left[ \frac{\varepsilon_r + (\varepsilon_r^2 + \varepsilon_i^2)^{\frac{1}{2}}}{2} \right]^{\frac{1}{2}} + \frac{\omega}{c} \left[ \frac{-\varepsilon_r + (\varepsilon_r^2 + \varepsilon_i^2)^{\frac{1}{2}}}{2} \right]^{\frac{1}{2}} \right\}$$
(3.59)

$$N = \left[\frac{1}{2}\left(\left|\varepsilon\right| + \varepsilon_{r}\right)\right]^{\frac{1}{2}} + i\left[\frac{1}{2}\left(\left|\varepsilon\right| - \varepsilon_{r}\right)\right]^{\frac{1}{2}}$$
(3.60)

Squaring both sides,

$$N^{2} = \frac{1}{2}(|\varepsilon| + \varepsilon_{r}) - \frac{1}{2}(|\varepsilon| - \varepsilon_{r}) + \frac{1}{2}[\frac{1}{2}(|\varepsilon| + \varepsilon_{r})]^{\frac{1}{2}}[\frac{1}{2}(|\varepsilon| - \varepsilon_{r})]^{\frac{1}{2}}$$
(3.61)

$$N^{2} = \varepsilon_{r} + i\varepsilon_{i} = \varepsilon \qquad (3.62)$$

The result is that, for water, the complex refractive index is the square of the dielectric function.

In general,

$$\kappa = \alpha + i\beta = \frac{\omega}{c} (n + ik)$$
 (3.63)

Substituting into Equation (3.19),

$$i \stackrel{\omega}{c} (n+ik) \hat{k} \cdot \vec{x} -i\omega t$$

$$\vec{E} = \vec{E}_{e} \qquad e \qquad (3.64)$$

$$\vec{E} = \vec{E}_{R} e e e \qquad (3.65)$$

Clearly, <u>k</u> governs attenuation of the wave amplitude, and <u>n</u> governs the real phase velocity. Thus, the terms <u>attenuation</u> (or <u>extinction</u>) <u>coefficient</u> and <u>real refractive index</u> for <u>k</u> and <u>n</u> respectively.

# The Lambert Absorption Coefficient

The Lambert absorption coefficient,  $\underline{\alpha}$ , is defined as the fractional decrease in intensity over distance:

$$\alpha \equiv -\frac{1}{I}\frac{dI}{dx}$$
(3.66)

We obtain an expression for the intensity by integrating:

 $-\alpha dx = \frac{dI}{I}$ (3.67)

$$\int_{-\infty}^{\infty} d\mathbf{x}' = \int_{-\infty}^{\infty} \frac{d\mathbf{T}'}{\mathbf{T}'}$$
(3.68)

$$-\alpha x = \ln\left(\frac{I}{I_0}\right)^{-\alpha}$$
(3.69)

$$I = I_{e} e^{-\alpha X}$$
(3.70)

The intensity is proportional to the square of the magnitude of the electric field vector:

$$I = |\vec{E}|^{2} = |\vec{E}_{0}|^{2} e^{-2\frac{\omega}{C}k(\hat{\kappa}\cdot\vec{x})}$$
(3.71)

$$\frac{d\mathbf{I}}{d\mathbf{x}} = \left| \vec{\mathbf{E}}_{0} \right|^{2} \left( -\frac{2\omega k}{c} \right) \quad \left| \vec{\kappa} \right| =$$
(3.72)

$$-\frac{1}{I}\frac{dI}{dx} = \frac{2\omega k}{c} = \alpha$$
(3.73)

Writing  $\omega = 2\pi f$  and  $f = c/\lambda$ ,  $\omega = 2\pi c/\lambda$ . Then,

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$$\alpha = \frac{2k}{c} \frac{2\pi c}{\lambda} = \frac{4\pi k}{\lambda}$$
(3.74)

With the definition of wave number,  $\nu$ , as  $1/\lambda$ ,

$$\alpha = 4\pi k \nu \qquad (3.75)$$

Absorption can also be written in terms of the formula

$$I = I_{e} e^{\rho}$$
(3.76)

where  $\underline{\mu}$  is defined as the linear absorption coefficient  $(cm^{-1})$ ,  $\underline{\rho}$  is the density of the absorber  $(gm/cm^3)$ , and  $\underline{m}$  is the mass per area of the absorber  $(gm/cm^2)$ . Then,  $\underline{\mu/\rho}$  is the mass absorption coefficient  $(cm^2/gm)$ .

It is easily shown that  $\mu=\alpha$ . From the definition of the Lambert coefficient, Equation (3.70), we require that

$$\alpha \mathbf{x} = \frac{\mu}{\rho} \mathbf{m} \tag{3.77}$$

Now,  $x/m = volume/mass = 1/\rho$ . Thus,

$$\alpha \frac{\mathbf{x}}{\mathbf{m}} = \alpha \frac{1}{\rho} = \mu \frac{1}{\rho} \tag{3.78}$$

The result is  $\mu=\alpha$ . The mass absorption coefficient, then, can be written as  $\alpha/\rho$ .

# The Kramers-Kronig Relations as Obtained

## From the Response Function

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The real and imaginary parts of the dielectric function are related by a dispersion relation. This is a result of the frequency dependence of the quantities involved and our insistence on causality. The method was outlined by Peterson and Knight.<sup>22</sup> The relations will later be shown to apply also to the complex refractive index.

To be most general, the fields should be written as a Fourier superposition of the fields due to all frequencies. We begin by noting the definition of the electric displacement in cgs units:

$$\mathbf{\bar{D}} = \mathbf{\bar{E}} + 4\pi \mathbf{\bar{P}} \tag{3.79}$$

With the assumption of linearity, the polarization can be written

$$\dot{\mathbf{p}} = \mathbf{x}_{\mathbf{p}}(\boldsymbol{\omega}) \dot{\mathbf{E}} \tag{3.80}$$

 $\chi_{\mathbf{p}}\left(\omega\right)$  is the frequency-dependent electric susceptibility. Then,

$$\mathbf{\ddot{D}} = \mathbf{\ddot{E}} + 4\pi\chi_{a}(\omega) \mathbf{\ddot{E}} = [1 + 4\pi\chi_{a}(\omega)]\mathbf{\ddot{E}}$$
 (3.81)

In general, the frequency-dependent dielectric function is defined by

$$\vec{D} = \epsilon(\omega) \vec{E}$$
 (3.82)

The result is

$$\epsilon(\omega) = 1 + 4\pi\chi_{\alpha}(\omega) \tag{3.83}$$

The frequency-dependent fields are written as

$$\vec{D}(\vec{x},\omega) = \varepsilon(\omega) \vec{E}(\vec{x},\omega)$$
(3.84)

where  $\vec{D}(\vec{x},\omega)$  and  $\vec{E}(\vec{x},\omega)$  are members of the Fourier-transform pairs

$$\vec{D}(\vec{x},t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{D}(\vec{x},\omega) e^{-i\omega t} d\omega$$
(3.85)

$$\vec{D}(\vec{x},\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{D}(\vec{x},t) e^{\pm i\omega t} dt \qquad (3.86)$$

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$$\vec{E}(\vec{x},t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega \qquad (3.87)$$

$$\vec{E}(\vec{x},\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{E}(\vec{x},t) e^{\pm i\omega t} dt \qquad (3.88)$$

We proceed from Equation (3.85) as follows:

$$\vec{D}(\vec{x},t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \varepsilon(\omega) \vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega \qquad (3.89)$$

$$\vec{D}(\vec{x},t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [1+4\pi\chi_{e}(\omega)]\vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega \qquad (3.90)$$

$$\vec{D}(\vec{x},t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} 4\pi \chi_{e}(\omega) \vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega$$
(3.91)

$$\vec{D}(\vec{x},t) = \vec{E}(\vec{x},t) + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} 4\pi \chi_{e}(\omega) \vec{E}(\vec{x},\omega) e^{-i\omega t} d\omega \qquad (3.92)$$

We define the function  $G(\tau)$  as

$$G(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} 4\pi \chi_{e}(\omega) e^{-i\omega\tau} d\omega \qquad (3.93)$$

 $G(\tau)$  is thus the Fourier transform of  $4\pi\chi_{e}\left(\omega\right)$  . Thus,

$$4\pi\chi_{e}(\omega) = \frac{1}{\sqrt{2\pi}}\int_{-\infty}^{\infty}G(\tau) e^{\pm i\omega\tau}d\tau \qquad (3.94)$$

Substituting this into Equation (3.92) and interchanging the order of integration,

$$\vec{D}(\vec{x},t) = \vec{E}(\vec{x},t) + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} G(\tau) \left[ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \vec{E}(\vec{x},\omega) e^{-i\omega(t-\tau)} d\omega \right] d\tau \quad (3.95)$$

$$\vec{D}(\vec{x},t) = \vec{E}(\vec{x},t) + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} G(\tau) \vec{E}(\vec{x},t-\tau) d\tau \quad (3.96)$$

The fact that  $\varepsilon(\omega)$  is a function of  $\omega$  leads directly to this form for  $\vec{D}(\vec{x},t)$ , which has a non-local (temporally) contribution from

 $\vec{E}(\vec{x},t)$ .  $G(\tau)$  is, evidently, the response function. Causality requires that there be no contribution to  $\vec{D}(\vec{x},t)$  from  $\vec{E}(\vec{x},t-\tau)$  for  $\tau < 0$  (no contribution from the future). Then,  $G(\tau)$  must be zero for  $\tau < 0$ .

 $\vec{D}(\vec{x},t)$  and  $\vec{E}(\vec{x},t)$  must be real. Therefore, subtracting from Equation (3.96) its complex conjugate, we obtain the following:

 $\vec{D}(\vec{x},t) - \vec{D}^*(\vec{x},t) = \vec{E}(\vec{x},t) - \vec{E}^*(\vec{x},t) +$ 

$$\frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [G(\tau)\vec{E}(\vec{x},t-\tau) - G^{*}(\tau)\vec{E}^{*}(\vec{x},t-\tau)]d\tau \qquad (3.97)$$

$$0 = 0 + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [G(\tau) - G^{*}(\tau)] \vec{E}(\vec{x}, t-\tau) d\tau \qquad (3.98)$$

This implies that  $G(\tau) = G^*(\tau)$ , or that  $G(\tau)$  is real. We can, from this, deduce some properties of  $4\pi\chi_e(\omega)$ , and thus of  $\varepsilon(\omega)$ . Using the definition of  $G(\tau)$  and Equation (3.83),

$$G(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{-\infty} [\varepsilon(\omega) - 1] e^{-i\omega\tau} d\omega \qquad (3.99)$$

The complex conjugate is

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$$G^{\star}(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [\varepsilon^{\star}(\omega) - 1] e^{\pm i\omega\tau} d\omega \qquad (3.100)$$

In Equation (3.99) we substitute  $-\omega$  for  $\omega$  and obtain

$$G(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [\varepsilon(-\omega) - 1] e^{\pm i\omega\tau} d\omega \qquad (3.101)$$

Subtracting Equation (3.100) from Equation (3.101),

$$G(\tau) - G^{*}(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [\varepsilon(-\omega) - 1] e^{i\omega\tau} d\omega - \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [\varepsilon^{*}(\omega) - 1] e^{i\omega\tau} d\omega \qquad (3.102)$$

$$0 = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [\varepsilon(-\omega) - \varepsilon^{\star}(\omega)] e^{i\omega\tau} d\omega \qquad (3.103)$$

This implies that  $\varepsilon(-\omega) = \varepsilon^*(\omega)$ . Then

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$$\operatorname{Re}[\varepsilon(-\omega)] + \operatorname{iIm}[\varepsilon(-\omega)] = \operatorname{Re}[\varepsilon(\omega)] - \operatorname{iIm}[\varepsilon(\omega)] \qquad (3.104)$$

$$\operatorname{Re}[\varepsilon(-\omega)] = \operatorname{Re}[\varepsilon(\omega)] \tag{3.105}$$

Thus,  $\operatorname{Re}[\varepsilon(\omega)]$  is an even function in  $\omega$ ; further, the function  $\operatorname{Re}[\varepsilon(\omega)-1]=$  $\operatorname{Re}[4\pi\chi_{\rho}(\omega)]$  is even in  $\omega$ .

$$\operatorname{Im}[\varepsilon(-\omega)] = -\operatorname{Im}[\varepsilon(\omega)]$$
(3.106)

Thus,  $Im[\varepsilon(\omega)]$  is an odd function in  $\omega$ ; further, the function  $Im[\varepsilon(\omega)-1] = Im[4\pi\chi_{\omega}(\omega)]$  is odd in  $\omega$ .

Using the above results, we can separate  $G(\tau)$  into a part symmetric in  $\tau$ , and a part anti-symmetric in  $\tau$ . Beginning with the definition of  $G(\tau)$ , separating the susceptibility and the exponential into real and imaginary parts, we find

$$G(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \left\{ \operatorname{Re}\left[4\pi\chi_{e}(\omega)\right] \cos(\omega\tau) + \operatorname{Im}\left[4\pi\chi_{e}(\omega)\right] \sin(\omega\tau) \right\} d\omega + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \left\{ \operatorname{Im}\left[4\pi\chi_{e}(\omega)\right] \cos(\omega\tau) + \operatorname{Re}\left[4\pi\chi_{e}(\omega)\right] \sin(\omega\tau) \right\} d\omega \quad (3.107)$$

The integrand of the second integral is odd in  $\omega$  and, therefore, vanishes. Thus,

$$G(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \operatorname{Re}[4\pi\chi_{e}(\omega)] \cos(\omega\tau) d\omega + \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \operatorname{Im}[4\pi\chi_{e}(\omega)] \sin(\omega\tau) d\omega \qquad (3.108)$$

The first integral is even in  $\tau$ . We define it as  $G_{\underline{s}}(\tau)$  (where the subscript implies the symmetric property). Note that it can be written

$$G_{s}(\tau) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \operatorname{Re}[4\pi\chi_{e}(\omega)] e^{-i\omega\tau} d\omega \qquad (3.109)$$

since the term containing the sine function is odd, causing that part of the integral to vanish. It is evident that  $G_{s}(\tau)$  is the Fourier transform of  $\text{Re}[4\pi\chi_{e}(\omega)]$ . Then,

$$\operatorname{Re}\left[4\pi\chi_{e}(\omega)\right] = \frac{1}{\sqrt{2\pi}}\int_{-\infty}^{\infty}G_{s}(\tau)e^{+i\omega\tau}d\tau \qquad (3.110)$$

The second integral is odd in  $\tau$ . We define it as  $G_{\underline{a}}(\tau)$  (where the subscript implies the anti-symmetric property). Note that it can be written

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$$G_{a}(\tau) = \frac{i}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \operatorname{Im}[4\pi\chi_{e}(\omega)] e^{-i\omega\tau} d\omega \qquad (3.111)$$

since the term containing the cosine function is odd, causing that part of the integral to vanish. It is evident that  $G_a(\tau)$  is the Fourier transform of  $iIm[4\pi\chi_e(\omega)]$ . Then,

$$Im[4\pi\chi_{e}(\omega)] = -\frac{i}{\sqrt{2\pi}} \int_{-\infty}^{\infty} G_{a}(\tau) e^{+i\omega\tau} d\tau \qquad (3.112)$$

We can relate the components of  $G(\tau)$  by knowing that  $G(\tau) = 0$ for  $\tau < 0$ , that  $G_g(\tau)$  is even in  $\tau$ , and that  $G_a(\tau)$  is odd in  $\tau$ . For  $\tau < 0$ ,

$$G(\tau < 0) = G_{g}(\tau < 0) + G_{a}(\tau < 0) = 0$$
 (3.113)

$$G_{s}(\tau < 0) = -G_{a}(\tau < 0)$$
 (3.114)

For  $\tau > 0$  (and in general),

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$$G_{e}(-\tau) = G_{e}(\tau)$$
 (3.115)

$$G_{a}(-\tau) = -G_{a}(\tau)$$
 (3.116)

Since  $\tau > 0$  implies that  $-\tau < 0$ , Equations (3.114) and (3.116) give

$$G_{g}(-\tau) = -G_{g}(-\tau) = G_{g}(\tau)$$
 (3.117)

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Thus, for  $\tau > 0$ ,

$$G_{e}(-\tau) = G_{e}(\tau) = G_{a}(\tau)$$
 (3.118)

The first result is from the symmetry property, and the last result is from Equation (3.117). Therefore,

$$G_{a}(\tau>0) = G_{a}(\tau>0)$$
 (3.119)

Now we can relate the real and imaginary parts of  $4\pi\chi_e(\omega)$ . Separating the integral into one over negative  $\tau$  and another over positive  $\tau$ ,

$$\operatorname{Re}\left[4\pi\chi_{e}(\omega)\right] = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{0} G_{s}(\tau) e^{i\omega\tau} d\tau + \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} G_{s}(\tau) e^{i\omega\tau} d\tau \qquad (3.120)$$

Then, using Equations (3.114) and (3.119),

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{0} [-G_{a}(\tau)] e^{i\omega\tau} d\tau + \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} G_{a}(\tau) e^{i\omega\tau} d\tau \quad (3.121)$$

Substituting  $\underline{-\tau}$  for  $\underline{\tau}$  in the first integral, we can recombine the integrals into

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} G_{a}(\tau) \quad (e^{-i\omega\tau} + e^{i\omega\tau})d\tau \qquad (3.122)$$

We now substitute for  $G_a(\tau)$  from Equation (3.111):

 $\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} \left\{ \frac{i}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \operatorname{Im}[4\pi\chi_{e}(\omega^{\dagger})] e^{-i\omega^{\dagger}\tau} d\omega^{\dagger} \right\} \times (e^{-i\omega\tau} + e^{i\omega\tau}) d\tau \qquad (3.123)$ 

Interchanging the order of integration and performing the integral over  $\tau$ ,

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \operatorname{Im}[4\pi\chi_{e}(\omega')](\frac{1}{\omega'+\omega} + \frac{1}{\omega'-\omega}) d\omega' \qquad (3.124)$$

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Im}[4\pi\chi_{e}(\omega')]d\omega'}{(\omega'+\omega)} + \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Im}[4\pi\chi_{e}(\omega')]d\omega'}{(\omega'-\omega)} \qquad (3.125)$$

Substituting  $\underline{-\omega'}$  for  $\underline{\omega'}$  in the first integral, and using the fact that  $Im[4\pi\chi_e(\omega)]$  is odd in  $\omega$ , we obtain

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Im}[4\pi\chi_{e}(\omega^{*})]d\omega^{*}}{(\omega^{*}-\omega)}$$
(3.126)

Now, using

$$\operatorname{Re}[4\pi\chi_{o}(\omega)] = \operatorname{Re}[\varepsilon(\omega)-1] = \operatorname{Re}[\varepsilon(\omega)] - 1 \qquad (3.127)$$

$$\operatorname{Im}_{\iota=\pi\chi_{\omega}}(\omega) ] = \operatorname{Im}[\varepsilon(\omega) - 1] = \operatorname{Im}[\varepsilon(\omega)]$$
(3.128)

the result is
$$\operatorname{Re}\left[\varepsilon\left(\omega\right)\right] = 1 + \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Im}\left[\varepsilon\left(\omega'\right)\right] d\omega'}{\left(\omega'-\omega\right)}$$
(3.129)

Similarly, separating Equation (3.112) into two integrals and using Equations (3.114) and (3.119),

$$\operatorname{Im}[4\pi\chi_{e}(\omega)] = \frac{i}{\sqrt{2\pi}} \int_{0}^{\infty} G_{s}(\tau) \quad (e^{-i\omega\tau} - e^{i\omega\tau}) \, d\tau \qquad (3.130)$$

Substituting for  $G_{s}(\tau)$  from Equation (3.109),

$$Im[4\pi\chi_{e}(\omega)] = \frac{i}{\sqrt{2\pi}} \int_{0}^{\infty} \left\{ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} Re[4\pi\chi_{e}(\omega')] e^{-i\omega'\tau} d\omega' \right\} \times (e^{-i\omega\tau} - e^{i\omega\tau}) d\tau \qquad (3.131)$$

Interchanging the order of integration and performing the integral over  $\boldsymbol{\tau},$  we find

$$Im[4\pi\chi_{e}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} Re[4\pi\chi_{e}(\omega')](\frac{1}{\omega'+\omega} - \frac{1}{\omega'-\omega})d\omega' \qquad (3.132)$$

$$Im[4\pi\chi_{e}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{Re[4\pi\chi_{e}(\omega')]d\omega'}{(\omega'+\omega)} - \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{Re[4\pi\chi_{e}(\omega')]d\omega'}{(\omega'-\omega)} \qquad (3.133)$$

Substituting  $-\omega'$  for  $\omega'$  in the first integral and using the symmetry of Re[ $4\pi\chi_{e}(\omega)$ ], these integrals become

$$\operatorname{Im}[4\pi\chi_{e}(\omega)] = -\frac{1}{\pi}\int_{-\infty}^{\infty}\frac{\operatorname{Re}[4\pi\chi_{e}(\omega')]d\omega'}{(\omega'-\omega)}$$
(3.134)

Thus, we obtain

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$$\operatorname{Im}[\varepsilon(\omega)] = -\frac{1}{\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Re}[\varepsilon(\omega')] - 1 d\omega'}{(\omega' - \omega)}$$
(3.135)

These relations can be expressed slightly differently. Beginning with Equation (3.124), we combine the two terms in parentheses to form

$$\operatorname{Re}\left[4\pi\chi_{e}(\omega)\right] = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{\omega' \operatorname{Im}\left[4\pi\chi_{e}(\omega')\right] d\omega'}{(\omega'^{2}-\omega^{2})}$$
(3.136)

Relying on the evenness of the integrand,

$$\operatorname{Re}[4\pi\chi_{e}(\omega)] = \frac{2}{\pi} \int_{0}^{\infty} \frac{\omega' \operatorname{Im}[4\pi\chi_{e}(\omega')] d\omega'}{(\omega'^{2}-\omega^{2})}$$
(3.137)

$$\operatorname{Re}\left[\varepsilon\left(\omega\right)\right] = 1 + \frac{2}{\pi} \int_{0}^{\infty} \frac{\omega' \operatorname{Im}\left[\varepsilon\left(\omega'\right)\right] d\omega'}{\left(\omega'^{2} - \omega^{2}\right)}$$
(3.138)

Similarly, beginning with Equation (3.132),

$$\operatorname{Im}[4\pi\chi_{e}(\omega)] = -\frac{\omega}{\pi} \int_{-\infty}^{\infty} \frac{\operatorname{Re}[4\pi\chi_{e}(\omega^{\dagger})]d\omega^{\dagger}}{(\omega^{\dagger}^{2}-\omega^{2})}$$
(3.139)

$$\operatorname{Im}[4\pi\chi_{e}(\omega)] = -\frac{2\omega}{\pi} \int_{0}^{\infty} \frac{\operatorname{Re}[4\pi\chi_{e}(\omega^{\dagger})]d\omega^{\dagger}}{(\omega^{\dagger}^{2}-\omega^{2})}$$
(3.140)

$$\operatorname{Im}[\varepsilon(\omega)] = -\frac{2\omega}{\pi} \int_{0}^{\infty} \frac{\operatorname{Re}[\varepsilon(\omega')] - 1 \, d\omega'}{(\omega'^2 - \omega^2)}$$
(3.141)

Equations (3.129) and (3.135), or alternatively (3.138) and (3.141), are the Kramers-Kronig relations.

### The Lorentz Oscillator Model

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Derivation of the dispersion relations for the complex refractive index requires some knowledge of the analytic properties of the function  $N(\omega)$ . Since, for water,  $N^2(\omega) = \varepsilon(\omega)$ , it is clear that a knowledge of the properties of  $\varepsilon(\omega)$  will prove helpful in investigating the properties of  $N(\omega)$ . We begin with the Lorentz model of the dielectric function.

Consider the motion of an electron in an applied electric field. The electron is bound to the nucleus with a force constant  $\underline{k}$ , and it experiences a damping force, proportional to its velocity, -<u>myv</u>. The equation of motion is

$$\vec{F} = m \frac{d^2 \vec{x}}{dt^2} = -k \vec{x} - m \vec{v} \vec{v} + (-e) \vec{E}$$
 (3.142)

$$m \frac{d^2 \vec{x}}{dt^2} + m\gamma \frac{d \vec{x}}{dt} + k \vec{x} = -k \vec{z}$$
(3.143)

We assume an oscillating field vector with angular frequency w:

$$\vec{z} = \vec{z}_{e} e^{-i\omega t}$$
(3.144)

Then, substituting for  $\vec{E}$  in Equation (3.143),

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$$m \frac{d^2 \vec{x}}{dt^2} + m\gamma \frac{d \vec{x}}{dt} + k \vec{x} = -e \vec{E}_0 e^{-i\omega t}$$
(3.145)

We assume a solution of the form

$$\dot{\mathbf{x}} = \dot{\mathbf{x}}_{o} e^{-\mathbf{i}\omega t}$$
(3.146)

Then, taking derivatives,

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$$\frac{d\vec{x}}{dt} = -i\omega \vec{x}_{e} e^{-i\omega t}$$
(3.147)

$$\frac{d^2 \dot{x}}{dt^2} = -\omega^2 \dot{x}_0 e^{-i\omega t}$$
(3.148)

The equation of motion becomes

$$-m\omega \dot{x}_{o}^{2+} e^{-i\omega t} - i\gamma m\omega \dot{x}_{o}^{e^{-i\omega t}} + k\dot{x}_{o}^{e^{-i\omega t}} = -e\dot{E}_{o}^{e^{-i\omega t}}$$
(3.149)

Dividing by m and the exponential,

$$(-\omega^2 - i\gamma\omega + \frac{k}{m}) \vec{x}_0 = -\frac{e\vec{E}_0}{m} \qquad (3.150)$$

Writing  $\frac{\sqrt{k/m}}{2}$  as  $\omega_{0}$ , the natural oscillator frequency,

$$\dot{x}_{o} = -\frac{e\vec{E}_{o}}{m(\omega_{o}^{2}-\omega^{2}-i\gamma\omega)}$$
(3.151)

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Then, writing  $\dot{x}_{o}$  as in Equation (3.146), we obtain

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$$\dot{\mathbf{x}} = -\frac{e\vec{\mathbf{z}}_{o}e^{-\mathbf{i}\omega\mathbf{t}}}{m(\omega_{o}^{2}-\omega^{2}-\mathbf{i}\gamma\omega)} = -\frac{e\vec{\mathbf{z}}}{m(\omega_{o}^{2}-\omega^{2}-\mathbf{i}\gamma\omega)}$$
(3.152)

The dipcle moment for this single oscillator is

$$\vec{p} = -\vec{ex} = \frac{\vec{e} \cdot \vec{E}}{m(\omega_{\rho}^{2} - \omega^{2} - i\gamma\omega)}$$
(3.153)

If there are <u>N</u> such oscillators per unit volume, the polarization,  $\vec{\underline{P}}$ , is given by

$$\vec{P} = N\vec{p} = \frac{Ne^{2\vec{E}}}{m(\omega_{\rho}^{2} - \omega^{2} - i\gamma\omega)}$$
(3.154)

Therefore, the electric susceptibility,  $x_e$ , is given by

$$\vec{\mathbf{p}} = \chi_{\mathbf{e}} \vec{\mathbf{E}} = \left[ \frac{N e^2}{m (\omega_0^2 - \omega^2 - i\gamma \omega)} \right] \vec{\mathbf{E}}$$
(3.155)

The dielectric function is related to  $\boldsymbol{\chi}_{e}$  as follows:

$$\varepsilon = 1 + 4\pi \chi_e = 1 + \frac{4\pi Ne^2}{m(\omega_o^2 - \omega^2 - i\gamma\omega)}$$
 (3.156)

The term  $\frac{4\pi Ne^2/m}{p}$  is frequently written  $\frac{\omega}{p}^2$ , where  $\frac{\omega}{p}$  is called the plasma frequency.

$$\varepsilon = 1 + \frac{\omega_p^2}{(\omega_o^2 - \omega^2 - i\gamma\omega)}$$
(3.157)

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This single oscillator model can be extended to account for multiple oscillators. For <u>N</u> total electrons per unit volume, there are <u>N</u> with natural frequency  $\underline{\omega_{oj}}$  and damping constant  $\underline{\gamma_{j}}$ . The obvious constraint is

$$\sum_{j} N_{j} = N \tag{3.158}$$

Then, adding up contributions from all types of electrons (oscillators),

$$\varepsilon = 1 + \frac{4\pi e^2}{m} \sum_{j} \frac{N_j}{(\omega_{oj}^2 - \omega^2 - i\gamma_j \omega)}$$
(3.159)

This can be separated into real and imaginary parts:

$$\varepsilon = 1 + \frac{4\pi e^2}{m} \sum_{j} \frac{N_j \left[ (\omega_{Oj}^2 - \omega^2) + i\gamma_j \omega \right]}{(\omega_{Oj}^2 - \omega^2)^2 + \gamma_j^2 \omega^2}$$
(3.160)  
$$= \left[ 1 + \frac{4\pi e^2}{m} \sum_{j} \frac{N_j (\omega_{Oj}^2 - \omega^2)}{(\omega_{Oj}^2 - \omega^2)^2 + \gamma_j^2 \omega^2} \right] + i\left[ \frac{4\pi e^2}{m} \sum_{j} \frac{N_j \gamma_j \omega}{(\omega_{Oj}^2 - \omega^2)^2 + \gamma_j^2 \omega^2} \right]$$
(3.161)





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A PARADORNEL MAN

MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A Analytic Properties of  $N(\omega)$ 

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For water,  $\varepsilon(\omega) = N^2(\omega)$ . Then, Equation (3.157) gives

$$N^{2}(\omega) = 1 + \frac{\omega_{p}^{2}}{\omega_{0}^{2} - \omega^{2} - i\gamma\omega}$$
(3.162)

The zeroes of  $N^2(\omega)$  are  $\underline{\omega}_a$  and  $\underline{\omega}_b$ , obtained as follows:

$$0 = 1 + \frac{\omega_{p}^{2}}{\omega_{0}^{2} - \omega_{-}^{2} - i\gamma\omega}$$
(3.163)

$$\omega_{\rm p}^{2} = -\omega_{\rm o}^{2} + \omega^{2} + i\gamma\omega \qquad (3.164)$$

$$\omega^{2} + (i_{\gamma})\omega - (\omega_{p}^{2} + \omega_{o}^{2}) = 0 \qquad (3.165)$$

$$\omega = -i\left(\frac{\gamma}{2}\right) \pm \left(\omega_{0}^{2} + \omega_{p}^{2} - \frac{\gamma^{2}}{4}\right)^{\frac{1}{2}}$$
(3.166)

With the following definition.

$$\omega_1^2 \equiv \omega_0^2 + \omega_p^2 - \frac{\gamma^2}{4}$$
(3.167)

 $(\omega_1 \text{ is real})$ , the zeroes are

 $\omega_{a} = \omega_{1} - i\left(\frac{\gamma}{2}\right)$ (3.168)

$$\omega_{\rm b} = -\omega_1 - i\left(\frac{\gamma}{2}\right) \tag{3.169}$$

The poles of  $N^2(\omega)$  are  $\frac{\omega_c}{c}$  and  $\frac{\omega_d}{d}$ , obtained as follows:

$$\omega_{0}^{2} - \omega^{2} - i\gamma\omega = 0 \qquad (3.170)$$

$$\omega = -i\left(\frac{\gamma}{2}\right) \pm \left(\omega_0^2 - \frac{\gamma^2}{4}\right)^{\frac{1}{2}}$$
(3.171)

With the following definition

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$$\omega_2^2 \equiv \omega_0^2 - \frac{\gamma^2}{4}$$
 (3.172)

 $(\omega_2 \text{ is real})$ , the poles are

$$\omega_{c} = \omega_{2} - i\left(\frac{\gamma}{2}\right)$$
(3.173)

$$\omega_{\rm d} = -\omega_2 - i\left(\frac{\gamma}{2}\right) \tag{3.174}$$

We can write<sup>23</sup>

$$N^{2}(\omega) = \frac{(\omega - \omega_{a})(\omega - \omega_{b})}{(\omega - \omega_{c})(\omega - \omega_{d})}$$
(3.175)

This can be verified by direct substitution from Equations (3.168), (3.169), (3.173), and (3.174). The result is

$$N(\omega) = \left[\frac{(\omega - \omega_{a})(\omega - \omega_{b})}{(\omega - \omega_{c})(\omega - \omega_{d})}\right]^{\frac{1}{2}}$$
(3.176)

Since the function  $N(\omega)$  is multi-valued, its branch line structure must be found in order to determine where it is analytic. The procedure was outlined by Churchill.<sup>24</sup>

Consider the functions

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$$f_{a}(\omega) = \omega - \omega_{a} \qquad (3.177)$$

$$f_{\rm b}(\omega) = \omega - \omega_{\rm b} \tag{3.178}$$

both of which are entire in the complex plane. Using Equation (3.168),

$$f_{a}(\omega) = \omega - \omega_{1} + i\left(\frac{\gamma}{2}\right)$$
(3.179)

 $\omega_1$  and  $\gamma$  are real. We define

$$z \equiv \omega + i\left(\frac{\gamma}{2}\right)$$
 (3.180)

Then, redefining  $f_a(\omega)$  as  $f_1^2(z)$ ,

$$\omega - \omega_{a} = z - \omega_{1} \tag{3.181}$$

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$$f_1(z) = (z - \omega_1)^{\frac{1}{2}} = \sqrt{r_1} e^{\frac{i}{2} \left(\frac{\theta_1}{2}\right)}$$
 (3.182)

Similarly, using Equation (3.169),

$$f_{b}(\omega) = \omega + \omega_{1} + i\left(\frac{\gamma}{2}\right)$$
(3.183)

With the corresponding definition of  $f_b(\omega)$  as  $f_2^2(z)$ ,

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$$f_2(z) = (z+\omega_1)^{\frac{1}{2}} = \sqrt{r_2} e^{i\left(\frac{\theta_2}{2}\right)}$$
 (3.184)

The polar coordinates for  $f_1(z)$  and  $f_2(z)$  are defined as in the following:



We define the function

$$f(z) = [f_{1}(z)][f_{2}(z)]$$
(3.185)  
$$f(z) = (z-\omega_{1})^{\frac{1}{2}} (z+\omega_{1})^{\frac{1}{2}} = \sqrt{r_{1}r_{2}} e^{i\left[\frac{(\theta_{1}+\theta_{2})}{2}\right]}$$
(3.186)

We may define the domain of f(z) as  $\left\{0 \le \theta_1 < 2\pi, 0 \le \theta_2 < 2\pi, r_1 > 0, r_2 > 0, \text{ and } r_1 + r_2 > 2\omega_1\right\}$ . The last condition is imposed so that f(z) is analytic in its domain. This result is equivalent to the statement that f(z) is analytic everywhere except on the closed line segment connecting  $-\omega_1$  and  $+\omega_1$ . This is shown as follows:

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The branch cuts for  $f_1(z)$  and  $f_2(z)$  are the rays  $\theta_1=0$  and  $\theta_2=0$  respectively. Thus, f(z) is analytic whenever  $z\neq \omega_1$  and  $\theta_2\neq 0$ . The value of  $f_1(z)$  is continuous (analytic) across  $\theta_1=\pi$  ( $f_1=i\sqrt{r_1}$ ), but the value of  $f_2(z)$  jumps from  $+\sqrt{r_2}$  to  $-\sqrt{r_2}$  as z crosses from above to below this line segment connecting  $-\omega_1$  and  $+\omega_1$ . Thus, f(z) is not continuous (and not analytic) on that line segment.

Now, to investigate the behavior of f(z) on the ray  $\theta_1=0$ ,  $r_1>0$ , we define the function

$$\mathbf{F}(\mathbf{z}) \equiv \sqrt{r_1} \mathbf{e}^{i\left(\frac{\phi_1}{2}\right)} \sqrt{r_2} \mathbf{e}^{i\left(\frac{\phi_2}{2}\right)}$$
(3.187)

in the domain  $\{-\pi < \phi_1 < \pi, -\pi < \phi_2 < \pi, r_1 > 0, r_2 > 0\}$ . F(z) is continuous across the ray  $\phi_1 = 0$  and is thus analytic there. (This is the same region of the real line as  $\theta_1 = 0$ ,  $r_1 > 0$ .) If we can show that f(z)=F(z) on, above, and below the ray  $\theta_1 = \phi_1 = 0$ , then we will have shown f(z) to be analytic on that ray. On the ray  $\theta_1 = \phi_1 = 0$ , as well as above it,  $\theta_1 = \phi_1$  and  $\theta_2 = \phi_2$ . Thus, f(z)=F(z) for z on or above the ray  $\theta_1 = \phi_1 = 0$ . For z below this ray,  $\phi_1 = \theta_1 - 2\pi$  and  $\phi_2 = \theta_2 - 2\pi$ . Then,

$$\mathbf{F}(\mathbf{z}) = \sqrt{r_1} \mathbf{e}^{\mathbf{j}\left(\frac{\phi_1}{2}\right)} \sqrt{r_2} \mathbf{e}^{\mathbf{j}\left(\frac{\phi_2}{2}\right)}$$
(3.188)

$$\mathbf{F}(\mathbf{z}) = \sqrt{r_1} \mathbf{e}^{i\left[\frac{\theta_1 - 2\pi}{2}\right]} \sqrt{r_2} \mathbf{e}^{i\left[\frac{\theta_2 - 2\pi}{2}\right]}$$
(3.189)

$$F(z) = \sqrt{r_1 r_2} e^{i\left(\frac{\theta_1 + \theta_2}{2}\right)} e^{-i2\pi} = \sqrt{r_1 r_2} e^{i\left(\frac{\theta_1 + \theta_2}{2}\right)} = f(z) \quad (3.190)$$

Therefore, f(z) is analytic on the ray  $\theta_1=0$ ,  $r_1>0$ .

The branch line for f(z) is



In crossing from above to below the branch line, the function shifts from

$$f_{+} = \sqrt{r_{1}} e^{i\left(\frac{\pi}{2}\right)} e^{-i\delta} \sqrt{r_{2}} e^{i(0)} e^{+i\delta} = i\sqrt{r_{1}r_{2}}$$
(3.191)

(0<8<<1) to

$$f_{-} = \sqrt{r_{1}} e^{i\left(\frac{\pi}{2}\right)} e^{+i\delta} \sqrt{r_{2}} e^{i(\pi)} e^{-i\delta} = -i\sqrt{r_{1}r_{2}} \qquad (3.192)$$

Now consider the functions

$$f_{c}(\omega) \equiv (\omega - \omega_{c}) \tag{3.193}$$

$$f_{a}(\omega) \equiv (\omega - \omega_{a}) \tag{3.194}$$

both of which are entire in the complex plane. Using Equations (3.173), (3.174), and (3.180),

$$f_{c}(\omega) = \omega - \omega_{2} + i\left(\frac{\gamma}{2}\right) = z - \omega_{2} \qquad (3.195)$$

$$f_{a}(\omega) = \omega + \omega_{2} + i\left(\frac{\gamma}{2}\right) = z + \omega_{2}$$
 (3.196)

We now define the following functions:

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$$g_{1}(z) \equiv (z-\omega_{2})^{\frac{1}{2}} = \sqrt{r_{3}} e^{i\left(\frac{\theta_{3}}{2}\right)}$$
 (3.197)

$$g_2(z) \equiv (z+\omega_2)^{\frac{1}{2}} = \sqrt{r_4} e^{\frac{i(\frac{\sigma_4}{2})}{2}}$$
 (3.198)

The polar coordinates for  $g_1(z)$  and  $g_2(z)$  are defined as in the following:



We may define

$$g(z) \equiv g_1(z) g_2(z) = \sqrt{r_3 r_4} e^{i\left[\left(\frac{\theta_3 + \theta_4}{2}\right]\right]}$$
 (3.199)

in the domain  $\{0 \le \theta_3 < 2\pi, 0 \le \theta_4 < 2\pi, r_3 > 0, r_4 > 0, r_3 + r_4 > 2\omega_2\}$ . As in the treatment for f(z), the branch line for g(z) is the closed line segment

connecting  $-\omega_2$  and  $+\omega_2$ . Note that

$$|\omega_1| = |\operatorname{Re}(\omega_a)| = |\operatorname{Re}(\omega_b)| = |(\omega_0^2 + \omega_p^2 - \frac{\gamma^2}{4})^{\frac{1}{2}}|$$
 (3.200)

$$|\omega_2| = |\operatorname{Re}(\omega_c)| = |\operatorname{Re}(\omega_d)| = |(\omega_0^2 - \frac{\gamma^2}{4})^{\frac{1}{2}}|$$
 (3.201)

Therefore,

$$|\omega_1| > |\omega_2| \tag{3.202}$$

The branch line for g(z) is



In crossing from above to below the branch line, g(z) shifts from  $+i\sqrt{r_3r_4}$  to  $-i\sqrt{r_3r_4}$ . In crossing from above to below the ray  $\theta_4 = \pi$ , g(z) varies continuously through  $-\sqrt{r_3r_4}$ . In crossing from above to below the ray  $\theta_3 = 0$ , g(z) varies continuously through  $+\sqrt{r_3r_4}$ .

Now, given the composite function

$$h(z) \equiv \frac{f(z)}{g(z)}$$
(3.203)

h(z) is clearly continuous and analytic except perhaps on the closed line segment connecting  $-\omega_1$  and  $+\omega_1$ . (This segment contains the segment connecting  $-\omega_2$  and  $+\omega_2$ .)

First, consider the segment  $-\omega_1$  to  $-\omega_2$ . For z crossing from above to below, h(z) goes from

$$h_{+} = \frac{f_{+}}{g_{+}} = \frac{i\sqrt{r_{1}r_{2}}}{-\sqrt{r_{3}r_{4}}} = -i\sqrt{\frac{r_{1}r_{2}}{r_{3}r_{4}}}$$
(3.204)

to

$$h_{-} = \frac{f_{-}}{g_{-}} = \frac{-i\sqrt{r_{1}r_{2}}}{-\sqrt{r_{3}r_{4}}} = +i\sqrt{\frac{r_{1}r_{2}}{r_{3}r_{4}}}$$
(3.205)

The function is discontinuous, and thus not analytic, on that segment. Second, consider the segment  $-w_2$  to  $+w_2$ . For z crossing from above to below, h(z) goes from

$$h_{+} = \frac{f_{+}}{g_{+}} = \frac{i\sqrt{r_{1}r_{2}}}{i\sqrt{r_{3}r_{4}}} = \sqrt{\frac{r_{1}r_{2}}{r_{3}r_{4}}}$$
(3.206)

to

$$h_{-} = \frac{f_{-}}{g_{-}} = \frac{-i\sqrt{r_{1}r_{2}}}{-i\sqrt{r_{3}r_{4}}} = \sqrt{\frac{r_{1}r_{2}}{r_{3}r_{4}}}$$
(3.207)

The function is continuous and analytic on that segment.

Third, consider the segment  $+\omega_2$  to  $+\omega_1$ . For z crossing from above to below, h(z) goes from

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$$h_{-} = \frac{f_{-}}{g_{-}} = \frac{-i\sqrt{r_{1}r_{2}}}{\sqrt{r_{3}r_{4}}} = -i\sqrt{\frac{r_{1}r_{2}}{r_{3}r_{4}}}$$
(3.209)

The function is discontinuous, and thus not analytic, on that segment.

The branch line structure for h(z), therefore, is



Substituting  $z = \omega + i\left(\frac{\gamma}{2}\right)$ ,  $\omega = z - i\left(\frac{\gamma}{2}\right)$ , from Equation (3.180), we obtain N( $\omega$ ) with branch lines as follows:



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The result is that  $N\left(\omega\right)$  is analytic on the real line and in the upper half plane.

We can find the high frequency limit for  $N(\omega)$  as follows: For  $|\omega| >> |\omega_{\alpha}|$ ,

$$N^{2}(\omega) = 1 + \frac{\omega_{p}}{\omega_{o}^{2} - \omega - i\gamma\omega} + 1 - \frac{\omega_{p}}{\omega_{o}^{2}}$$
(3.210)

$$N(\omega) \approx \left(1 - \frac{\omega_p^2}{\omega^2}\right)^{\frac{1}{2}} = 1 - \frac{\omega_p^2}{2\omega^2} - \frac{\omega_p^4}{8\omega^4} - \dots \approx 1 - \frac{\omega_p^2}{2\omega^2}$$
(3.211)

As  $\omega \rightarrow \infty$ , N( $\omega$ )  $\rightarrow$  1.

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This derivation is not invalidated by requiring a more complicated, or more realistic, model of  $\varepsilon(\omega)$ . Any model can be written in the form

where  $\underline{Z}_{\underline{m}}$  are zeroes and  $\underline{P}_{\underline{n}}$  are poles of the function.<sup>25</sup> Causality implies that all the zeroes and poles lie below the real axis.<sup>26</sup> The result is the same analytical properties for  $N(\omega)$ .

# The Kramers-Kronig Relations as Obtained

### From the Cauchy Integral Formula

With the above examination of the analytical properties of  $\varepsilon(\omega)$  and  $N(\omega)$ , we can derive the dispersion relations for  $N(\omega)$ . We demonstrate the process first by obtaining the Kramers-Kronig relations for the dielectric function by contour integration.

We can show that the definition of  $\varepsilon(\omega)$  via the time response function is consistent with the derived analytic properties. The definition of  $G(\tau)$  yields

$$4\pi\chi_{e}(\omega) = \varepsilon(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} G(\tau) e^{i\omega\tau} d\tau \qquad (3.213)$$

Since  $G(\tau)=0$  for  $\tau<0$ , we can write

$$\varepsilon(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} G(\tau) e^{i\omega\tau} d\tau \qquad (3.214)$$

Separating  $\omega$  into its real and imaginary parts,

$$\varepsilon(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} G(\tau) e^{i\omega_{r}\tau} e^{-\omega_{i}\tau} d\tau \qquad (3.215)$$

It is clear that, for finite  $G(\tau)$ , the function  $\varepsilon(\omega)$ -l exists, as does its derivative, for all  $\omega$  such that  $\omega_j \ge 0$ . Therefore, the function  $\varepsilon(\omega)$ -l is analytic on the real axis and in the upper half plane.

As a result, for any closed contour in the domain of analyticity of  $\varepsilon(\omega)$ -1, the Cauchy integral formula allows us to write

$$\varepsilon(\omega) - 1 = \frac{1}{2\pi i} \oint \frac{[\varepsilon(\omega') - 1]d\omega'}{(\omega' - \omega)}$$
(3.216)

We will want to investigate the function for real, positive  $\omega$ .

Therefore, placing  $\omega$  on the positive real axis, we choose a contour <u>C</u> as follows:



The integral around this contour can be written as the sum of four parts:

$$\oint \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} = \int_{-R}^{\omega-r} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} + \int_{C_r}^{C} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} + \int_{C_r}^{R} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} + \int_{C_r}^{R} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)}$$
(3.217)

Now, writing

 $\omega' \equiv \omega + re^{i\theta}$  (3.218)

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$$d\omega' = ire^{i\theta}d\theta \qquad (3.219)$$

we can write the second integral as

$$\int_{-\pi}^{0} \frac{[\epsilon(\omega')-1]ire^{i\theta}d\theta}{(\omega+re^{i\theta}-\omega)} = \int_{-\pi}^{0} [\epsilon(\omega')-1]id\theta \qquad (3.220)$$

Writing

$$\omega' \equiv \mathbf{Re}^{\mathbf{i}\phi} \tag{3.221}$$

$$d\omega' = ire^{i\phi}d\phi \tag{3.222}$$

we can write the last integral as

$$\int_{0}^{\pi} \frac{[\epsilon(\omega')-1]iRe^{i\phi}d\phi}{(Re^{i\phi}-\omega)}$$
(3.223)

Then,

$$\int_{C} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} = \int_{-R}^{\omega-r} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} + \int_{\pi}^{\sigma} [\varepsilon(\omega')-1]id\theta + \int_{\pi}^{R} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} + \int_{\sigma}^{\pi} \frac{[\varepsilon(\omega')-1]iRe^{i\phi}d\phi}{(Re^{i\phi}-\omega)} \quad (3.224)$$

Now we apply a limiting process, allowing R to approach  $\infty$  and r to approach zero. Since this includes and excludes no new poles, the

integral on the left of Equation (3.224) remains the same. The first and third integrals on the right become the Cauchy principal value (denoted <u>P.V.</u>) of the integral along the real line. In the second integral on the right,  $\underline{\omega}^{*}$  becomes  $\underline{\omega}$  and the function  $\underline{\epsilon(\omega)-1}$  can be moved outside the integral sign, the remainder yielding  $\underline{\pi i}$ . The fourth integral on the right vanishes because  $\epsilon(\omega^{*})$  approaches one as the magnitude of  $\omega^{*}$  increases without bound. Thus,

$$\oint_{C} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)} = P.V.\left\{\int_{-\infty}^{\infty} \frac{[\varepsilon(\omega')-1]d\omega'}{(\omega'-\omega)}\right\} + \pi i[\varepsilon(\omega)-1] \quad (3.225)$$

Now, using this in Equation (3.216) and rearranging, we obtain

$$\varepsilon(\omega) - 1 = \frac{1}{\pi i} P.V. \left\{ \int_{-\infty}^{\infty} \frac{[\varepsilon(\omega') - 1] d\omega'}{(\omega' - \omega)} \right\}$$
(3.226)

Separating the functions into real and imaginary parts yields the Kramers-Kronig relations.

One difficulty with the above derivation is the excursion into the lower half plane by the contour  $C_{\underline{r}}$ . This path is of infinitesimal length; and with  $\omega_{\underline{i}} < \delta$  for all  $\delta$ , the function given by Equation (3.215) remains regular even with  $\tau \leftrightarrow \delta$ . Further, the physical constraints on  $G(\tau)$  require that  $G(\tau) \rightarrow 0$  as  $\tau \leftrightarrow \delta$ . However, this difficulty can be avoided by distorting the contour above, instead of below, the pole at  $\omega$  on the real axis. Then, since no poles are enclosed, the integral must yield zero:

$$\oint_{C} \frac{\left[\varepsilon\left(\omega'\right) - 1\right] d\omega'}{\left(\omega' - \omega\right)} = 0$$
(3.227)

As before, the integral is divided into four parts. The limit is taken allowing R+= and r+0. The only difference is the integration around the small semi-circular contour around  $\omega$  which is counterclockwise and yields  $-\pi i [\varepsilon(\omega)-1]$ , the negative of the prior result. This, however, conspires with the zero on the right of Equation (3.227) to give the same answer as before, namely Equation (3.226) and the Kramers-Kronig relations.

The only requirements for the derivation of the Kramers-Kronig relations above were the analyticity of the function  $\underline{\varepsilon}(\omega)-1$ in the upper half plane and on the real line, and the vanishing of the function for  $|\omega| \rightarrow \infty$ . We can, thus, derive similar relations for the complex index of refraction. We must use  $\underline{N}(\omega)-1$ , however, since  $N(\omega) \rightarrow 1$  as  $|\omega| \rightarrow \infty$ . We write

$$N(\omega) - 1 = \frac{1}{2\pi i} \oint \frac{[N(\omega') - 1]d\omega'}{(\omega' - \omega)}$$
(3.228)

using a contour enclosing the pole at  $\omega$  (real). If we wish to use a contour excluding that pole, the integral on the right of Equation (3.228) yields zero. In either case, the result is

$$N(\omega) - 1 = \frac{1}{\pi i} P.V. \left\{ \int_{-\infty}^{\infty} \frac{[N(\omega') - 1]d\omega'}{(\omega' - \omega)} \right\}$$
(3.229)

Separating the functions into their real and imaginary parts,

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$$n(\omega) = 1 + \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{k(\omega') d\omega'}{(\omega' - \omega)}$$
(3.230)

$$k(\omega) = -\frac{1}{\pi} \int_{-\infty}^{\infty} \frac{[n(\omega^{\dagger})-1]d\omega^{\dagger}}{(\omega^{\dagger}-\omega)}$$
(3.231)

These are the Kramers-Kronig relations for the complex refractive index.

## The Real Part of $N(\omega)$ as a Fourier Transform

We can obtain  $n(\omega)$  as a series of two Fourier transforms. This will be the basis for the calculation described in Chapter IV. Beginning with Equation (3.230), we divide the integral into two equal parts.

$$n(\omega) - 1 = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{k(\omega')d\omega'}{(\omega'-\omega)} + \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{k(\omega')d\omega'}{(\omega'-\omega)}$$
(3.232)

Substituting  $-\omega'$  for  $\omega'$  in the first integral, using the fact that  $k(\omega')$  is odd, and reversing the limits, we can recombine the integrals.

$$n(\omega) - 1 = \frac{1}{2\pi} \int_{-\infty}^{\infty} k(\omega') \left[ \frac{1}{(\omega' + \omega)} + \frac{1}{(\omega' - \omega)} \right] d\omega' \qquad (3.233)$$

Now we rely on the value of the integral

$$i\int_{0}^{\infty} \left[ e^{-i(\omega'+\omega)\tau} + e^{-i(\omega'-\omega)\tau} \right] d\tau = \frac{1}{(\omega'+\omega)} + \frac{1}{(\omega'-\omega)}$$
(3.234)

Substituting this integral over  $\tau$  into Equation (3.233), we obtain

$$\mathbf{n}(\omega) - \mathbf{l} = \frac{1}{2\pi} \int_{-\infty}^{\infty} \mathbf{k}(\omega') \left\{ i \int_{0}^{\infty} \left[ e^{-\mathbf{i}(\omega' + \omega)\tau} + e^{-\mathbf{i}(\omega' - \omega)\tau} \right] d\tau \right\} d\omega' \quad (3.235)$$

Since  $k(\omega)$  is continuous, we can reverse the order of integration.

$$n(\omega) - 1 = \frac{i}{2\pi} \int_{0}^{\infty} \left[ \int_{-\infty}^{\infty} k(\omega') e^{-i\omega'\tau} d\omega' \right] (e^{-i\omega\tau} + e^{i\omega\tau}) d\tau \qquad (3.236)$$

$$n(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} \left\{ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [ik(\omega')] e^{-i\omega'\tau} d\omega' \right\} e^{-i\omega\tau} d\tau +$$

$$\frac{1}{\sqrt{2\pi}}\int_{0}^{\pi}\left\{\frac{1}{\sqrt{2\pi}}\int_{-\infty}^{\pi}\left[ik\left(\omega^{\prime}\right)\right]e^{-i\omega^{\prime}\tau}d\omega^{\prime}\right\}e^{+i\omega\tau}d\tau$$
(3.237)

Substituting  $-\tau$  for  $\tau$ , the first integral in Equation (3.237) becomes

$$\frac{1}{\sqrt{2\pi}} \int_{-\infty}^{0} \left\{ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [ik(\omega')] e^{+i\omega'\tau} d\omega' \right\} e^{+i\omega\tau} d\tau \qquad (3.238)$$

Now, substituting  $\underline{-\omega^{i}}$  for  $\underline{\omega^{i}}$ , using the oddness of  $k(\omega^{i})$ , and reversing the limits, the integral (3.238) becomes

$$\frac{1}{\sqrt{2\pi}}\int_{-\infty}^{0} \left\{-\frac{1}{\sqrt{2\pi}}\int_{-\infty}^{\infty} [ik(\omega')]e^{-i\omega'\tau}d\omega'\right\}e^{+i\omega\tau}d\tau \qquad (3.239)$$

The result is

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$$n(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{0} \left\{ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [ik(\omega')] e^{-i\omega'\tau} d\omega' \right\} e^{+i\omega\tau} d\tau +$$

$$+ \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} \left\{ \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} [ik(\omega')] e^{-i\omega'\tau} d\omega' \right\} e^{i\omega\tau} d\tau \qquad (3.240)$$

If we define  $f(\tau)$  as the Fourier transform of  $\underline{ik}(\omega')$ ,

$$f(\tau) = \frac{1}{\sqrt{2\pi}} \int \left[ik(\omega')\right] e^{-i\omega'\tau} d\omega' \qquad (3.241)$$

the function  $\underline{n}(\omega) - \underline{l}$  can be written

$$n(\omega) - 1 = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{0} \left[ -f(\tau) \right] e^{i\omega\tau} d\tau + \frac{1}{\sqrt{2\pi}} \int_{0}^{\infty} \left[ f(\tau) \right] e^{i\omega\tau} d\tau \qquad (3.242)$$

Now we define  $q(\tau)$  as

$$g(\tau) \equiv \begin{cases} -f(\tau), \ \tau \leq 0 \\ +f(\tau), \ \tau > 0 \end{cases}$$
(3.243)

Then,

$$n(\omega)-1 = \frac{1}{\sqrt{2\pi}} \int g(\tau) e^{i\omega\tau} d\tau \qquad (3.244)$$

Thus,  $\underline{n}(\omega) - \underline{l}$  is the Fourier transform of the  $\underline{q}(\tau)$  function.

## The Electronic Sum Rule

We are now in a position to derive the electronic sum rule. Beginning with the Kramers-Kronig relation for the real part of the refractive index, Equation (3.230), we express the integral over positive frequencies.

$$n(\omega) - 1 = \frac{2}{\pi} \int_{0}^{\infty} \frac{\omega^{*} k(\omega^{*}) d\omega^{*}}{(\omega^{*} - \omega^{2})}$$
(3.245)

Now, we define  $\underline{\omega_c}$  as some cut-off frequency above which there is no absorption due to electronic oscillation. Then, that portion of the integral from  $\omega_c$  to  $\sim$  can be cmitted.

$$n(\omega) = 1 + \frac{2}{\pi} \int_{0}^{\omega} \frac{\omega' k(\omega') d\omega'}{(\omega'^2 - \omega^2)}$$
(3.246)

Choosing some  $\omega > \omega_c$ , the  $\underline{\omega}^2$  term dominates the  $\underline{\omega'}^2$  in the denominator of the integrand. Ignoring  $\underline{\omega'}^2$  by comparison,

$$n(\omega) \approx 1 + \frac{2}{\pi} \left( -\frac{1}{\omega^2} \right) \int_{0}^{\omega} \omega' k(\omega') d\omega' \qquad (3.247)$$

This expression becomes more accurate as  $\omega$  becomes larger. Also, for large  $\omega$ , Equation (3.211) gives

$$n(\omega) \approx 1 - \frac{\omega_p^2}{2\omega^2}$$
(3.248)

This also becomes more accurate as  $\omega$  becomes larger. We take the limiting case,  $\omega \rightarrow \infty$ . Then, equating the right sides of Equations (3.247) and (3.248),

$$1 - \frac{\omega_{p}^{2}}{2\omega^{2}} = 1 - \frac{2}{\pi\omega^{2}} \int_{0}^{\omega_{p}} \omega^{c} k(\omega') d\omega' \qquad (3.249)$$

$$\omega_{\rm p}^2 = \frac{4}{\pi} \int_0^{\infty} \omega' k(\omega') d\omega' \qquad (3.250)$$

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We can extend the upper limit to . since the integrand contributes nothing for  $\omega > \omega_c$ .

$$\omega_{\rm p}^2 = \frac{4}{\pi} \int_0^\infty \omega' k(\omega') d\omega' \qquad (3.251)$$

We substitute  $4\pi Ne^2/m$  for  $\omega_p^2$  and write N as  $Zn_o$ , where Z is the number of electrons in the molecule and  $n_{o}$  is the number of water molecules per unit volume.

$$\frac{4\pi n_{o} 2e^{2}}{m} = \frac{4}{\pi} \int \omega' k(\omega') d\omega' \qquad (3.252)$$

$$Z = \frac{m}{\pi^2 n_0 e^2} \int \omega' k(\omega') d\omega' \qquad (3.253)$$

Now, we write the angular frequency in terms of wave number.

$$\omega' = 2\pi c \nu \qquad (3.254)$$

$$d\omega' = 2\pi c d\nu \tag{3.255}$$

Substituting Equations (3.254) and (3.255) into Equation (3.253), we obtain

$$Z = \frac{4mc^2}{n_0 e^2} \int_0^{\infty} v k(v) dv$$
 (3.256)

We substitute  $\alpha(v)/4\pi v$  for k(v).

$$z = \frac{mc^2}{\pi n_0 e^2} \int_0^\infty \alpha(v) dv \qquad (3.257)$$

Transforming to mks units, we obtain the sum rule used in the calculations described in Chapter IV.

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$$z = \frac{4mc^2 \epsilon_0}{n_0 e^2} \int \alpha(v) dv \qquad (3.258)$$

### CHAPTER IV

#### NUMERICAL METHODS

### The Numerical Computation of $n(\omega)$ from $k(\omega)$

In Chapter III, we obtained Equation (3.230) expressing  $n(\omega)$  in terms of an integral involving  $k(\omega')$ . For numerical calculation of  $n(\omega)$ , we must rely on numerical values of  $k(\omega)$  known at discrete values of  $\omega$ over a finite spectrum.

Assuming there is some  $\omega_{\max}$  above which  $k(\omega)$  yields a negligible contribution to the integral, we can restrict our attention to those values of  $|\omega| \le \omega_{\max}$ . Since  $k(\omega)$  is an odd function,

$$k(0) = 0$$
 (4.1)

Further, if we know  $k(\omega)$  for  $0 < \omega \le \omega_{max}$ , we automatically know  $k(\omega)$  for  $-\omega_{max} \le \omega < 0$ . We divide the interval  $-\omega_{max} \le \omega \le \omega_{max}$  into N segments each of width  $\Delta \omega$ .

We begin by evaluating  $f(\tau)$ , the Fourier transform of  $ik(\omega^{\dagger})$ , as specified in Equation (3.241).

$$f(\tau) = \frac{1}{\sqrt{2\tau}} \int ik(\omega') e^{-i\omega'\tau} d\omega' \qquad (4.2)$$

This integral must be transformed into a discrete sum. For the N points

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(including j=0) from j=-N/2 to j=(N/2)-1, with

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$$\tau = \mathbf{m} \Delta \tau \tag{4.4}$$

(the index m to be summed over later), we find

$$f(\tau) = f(m) = \frac{i}{\sqrt{2\pi}} \sum_{j=\frac{N}{2}}^{N} k(j) e^{-i(j\Delta\omega)(m\Delta\tau)} \Delta\omega \qquad (4.5)$$

The summation is to (N/2)-l since the function is presumed periodic (to be Fourier transformable) with period  $N\Delta\omega$ .<sup>27</sup> The value at j=N/2 is the first value of the next period of the function. (N+= in the Fourier integral.) We write  $\omega$  and  $\Delta\omega$  in terms of wave number.

$$\omega = 2\pi c \nu \qquad (4.6)$$

 $\Delta \omega = 2\pi C \Delta \nu \tag{4.7}$ 

$$f(m) = ic\Delta v \sqrt{2\pi} \sum_{j=\frac{N}{2}} k(j) e^{-i2\pi j m c\Delta v \Delta \tau}$$
(4.8)

Now we impose the condition of periodicity by requiring that

$$f(\mathbf{m}+\mathbf{c}\mathbf{N}) = f(\mathbf{m}) \tag{4.9}$$

where g is any integer. Substituting  $\underline{m+qN}$  for  $\underline{m}$  in Equation (4.8) and

applying Equation (4.9) yields

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$$e^{-i2\pi j q N c \Delta v \Delta \tau} = 1$$
(4.10)

Therefore,  $jqNc\Delta v\Delta \tau$  must be an integer. With jq integral, we can require  $Nc\Delta v\Delta \tau$  to be unity. Then,

$$\Delta \tau = \frac{1}{NC\Delta v}$$
(4.11)

$$f(m) = ic\Delta v \sqrt{2\pi} \sum_{j=\frac{N}{2}}^{\frac{N}{2}-1} k(j) e^{-i2\pi \left(\frac{m}{N}\right)j}$$
(4.12)

• The only values of k(j) known from real data are those N/2 points for  $0 < j \le N/2$ . Since k(j) is odd about zero, the values of k(j) in that part of the sum over negative integers must be replaced by -k(-j).

$$f(m) = ic \Delta v \sqrt{2\pi} \left\{ \sum_{j=-\frac{N}{2}}^{-1} [-k(-j)] e^{-i2\pi \left(\frac{m}{N}\right)j} + \sum_{j=0}^{\frac{N}{2}-1} k(j) e^{-i2\pi \left(\frac{m}{N}\right)j} \right\}$$
(4.13)

This can be transformed into a sum over positive integers by defining a new index.

 $1 \equiv N + j \tag{4.14}$ 

We substitute 1 for j in the first sum in Equation (4.13), then change

the dummy index  $\underline{1}$  back to  $\underline{j}$ .

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$$f(m) = ic\Delta v \sqrt{2\pi} \left\{ \sum_{j=\frac{N}{2}}^{N-1} [-k(N-j)] e^{-i2\pi \left(\frac{m}{N}\right)j} + \sum_{j=0}^{\frac{N}{2}-1} k(j) e^{-i2\pi \left(\frac{m}{N}\right)j} \right\}$$
(4.15)

We define the function  $\underline{k'(j)}$  as follows:

$$k'(j) \equiv \begin{cases} -k(N-j), & \frac{N}{2} \le j < N \\ \\ k(j), & 0 \le j < \frac{N}{2} \end{cases}$$
(4.16)

Then we can combine the sums in Equation (4.15).

$$f(m) = ic\Delta v \sqrt{2\pi} \sum_{j=0}^{N-1} k^{*}(j) e^{-i2\pi \left(\frac{m}{N}\right)j}$$
 (4.17)

We can calculate  $n(\omega)$ -1 with this function f(m). The integral in Equation (3.242) can be transformed into a discrete sum. For a particular  $\omega_{o'}$ 

$$\omega_{O} = 1_{O} \Delta \omega \qquad (4.18)$$

$$n(\omega_{O}) - 1 = \frac{1}{\sqrt{2\pi}} \sum_{m=\frac{N}{2}}^{-1} [-f(m)] e^{i(1_{O} \Delta \omega) (m \Delta \tau)} +$$

+  $\frac{1}{\sqrt{2\pi}} \sum_{m=0}^{N-1} f(m) e^{i(1 \Delta \omega) (m \Delta \tau)} \Delta \tau$  (4.19)

Now, using Equations (4.7) and (4.11), we obtain

$$n(\omega_{O}) - 1 = \frac{1}{NC\Delta\nu^{2\pi}} \left\{ \sum_{m=-\frac{N}{2}}^{-1} [-f(m)] e^{i2\pi \left(\frac{1_{O}}{N}\right)m} + \frac{N^{2}}{2} \int_{m=0}^{N-1} f(m) e^{i2\pi \left(\frac{1_{O}}{N}\right)m} \right\}$$
(4.20)

As before, this can be written as a sum over positive integers.

$$n(\omega_{O})-1 = \frac{1}{NC\Delta v \sqrt{2\pi}} \left\{ \sum_{m=\frac{N}{2}}^{N-1} \left[ -f(m-N) \right] e^{i2\pi \left(\frac{1}{O}\right)m} + \frac{\sum_{m=0}^{N-1} f(m) e^{i2\pi \left(\frac{1}{O}\right)m}}{\sum_{m=0}^{N-1} f(m) e^{i2\pi \left(\frac{1}{O}\right)m}} \right\}$$

$$(4.21)$$

We obtain -f(m-N) and f(m) from Equation (4.17) and substitute into Equation (4.21).

$$n(\omega_{o})-1 = \left(\frac{i}{N}\right) \left\{ \sum_{\substack{m=N\\m=2}}^{N-1} \left[ -\sum_{\substack{j=0\\j=0}}^{N-1} k'(j) e^{-i2\pi \left(\frac{m}{N}\right)j} \right] e^{i2\pi \left(\frac{l_{o}}{N}\right)m} + \frac{\sum_{\substack{m=0\\m=0}}^{N-1} \left[ \sum_{\substack{j=0\\j=0}}^{N-1} k'(j) e^{-i2\pi \left(\frac{m}{N}\right)j} \right] e^{i2\pi \left(\frac{l_{o}}{N}\right)m} \right\}$$
(4.22)

Now we define the following function:

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$$A(m) = \begin{cases} -\sum_{j=0}^{N-1} k'(j) e^{-i2\pi \left(\frac{m}{N}\right)j}, & \frac{N}{2} \le m \le N-1 \\ & & \\ +\sum_{j=0}^{N-1} k'(j) e^{-i2\pi \left(\frac{m}{N}\right)j}, & 0 \le m \le \frac{N}{2}-1 \end{cases}$$
(4.23)

The result is

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$$n(\omega_{o}) = 1 + \left(\frac{i}{N}\right) \sum_{m=0}^{N-1} A(m) e^{i2\pi \left(\frac{1}{N}\right)m}$$
(4.24)

As one can see by tracing back from A(m) in Equation (4.23) through k'(j) in Equation (4.16), this enables the numerical calculation of  $n(\omega)$  directly from the  $k(\omega)$  spectrum.

### Calculations

Each of these sums was computed by arranging appropriate arrays and using the FAST FOURIER TRANSFORM algorithm on the AMDAHL 470 computer. The wave number spectrum was divided into  $2^{17} = 131,072$  equal intervals. Since, for most k(j)'s,  $j\Delta v$  fell between values of v for which k(v) data were available, the program interpolated to obtain the appropriate k(j). Then, the program calculated the n(v) spectrum, yielding a value of n(v)for each v for which a k(v) value had been input. Again, the program interpolated between the values of  $n(m\Delta v)$ , obtained for integral  $\underline{m}$ , to arrive at n(v) for the appropriate wave numbers.

The calculation was first done over the range 0 to  $5 \times 10^6$  cm<sup>-1</sup>. As is evident from the Kramers-Kronig integral, the greatest contribution
is obtained from those values of k(v) for v closest to the wave number for which n(v) is being calculated. Thus, as long as the wave number being investigated is not near an end point of the range of calculation, it should yield a reasonable result. The result should be less reliable as one approaches an endpoint. This was found to be true.

The density of the data points input was much greater at low wave numbers than at high wave numbers. As a result, even with  $2^{17}$ intervals, those intervals at the low end included, and glossed over, many data points. The resolution was, in effect, reduced at the low end. The phenomenon is illustrated by Figure 5, which shows the region 0 to 50 cm<sup>-1</sup>. The jagged line was calculated by dividing the region of 0 to  $5 \times 10^5$  cm<sup>-1</sup> into  $2^{17}$  intervals. The data, then, had influence every  $3.8 \text{ cm}^{-1}$ . The smooth line was calculated by dividing the region of 0 to  $5 \times 10^4$  cm<sup>-1</sup> into  $2^{17}$  intervals, resulting in effective data every  $0.38 \text{ cm}^{-1}$ , and increased resolution.

In order to overcome the problem of resolution, it was necessary to choose a smaller range for the calculation. Division of the larger range into more and smaller intervals would have required more computer memory than was available. So long as the region of interest was kept some distance from the endpoints of the range, the results were good. With the intention of combining the results into a composite spectrum, calculations were made over the following regions, illustrated by the indicated figures: 0 to  $5 \times 10^6$  cm<sup>-1</sup>, Figure 6; 0 to  $5 \times 10^5$  cm<sup>-1</sup>, Figure 7; 0 to  $5 \times 10^4$  cm<sup>-1</sup>, Figure 8; 0 to  $5 \times 10^3$  cm<sup>-1</sup>, Figure 9; 0 to  $5 \times 10^2$  cm<sup>-1</sup>, Figure 10; 0 to  $5 \times 10^1$  cm<sup>-1</sup>, Figure 11; 0 to  $5 \times 10^0$  cm<sup>-1</sup>, Figure 12; 0 to  $5 \times 10^{-1}$  cm<sup>-1</sup>, Figure 13.

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The phenomenon of deviation from good results as an endpoint is approached is illustrated by Figure 14. There, the values obtained from calculations over the two ranges 0 to  $5 \times 10^{6}$  and 0 to  $5 \times 10^{5}$  cm<sup>-1</sup> are superimposed. It is apparent that, as the vicinity of  $1 \times 10^{5}$  cm<sup>-1</sup> is passed, the calculation over the smaller range gives values which begin to differ from the other values, the latter being presumably more accurate since they are farther from an endpoint. This is characteristic of most of the calculations. The results seem accurate up to approximately  $1 \times 10^{n}$  cm<sup>-1</sup> for a calculation over the range of 0 to  $5 \times 10^{n}$  cm<sup>-1</sup>. It seems reasonable, then, to use that part of each spectrum not limited by poor resolution or by proximity to an endpoint.

Since the Fourier transform technique is most accurate in defining the shape of the curve, but less accurate in defining its absolute position, it was deemed desirable to fix the height of the curve at an appropriate point. This was done by calculating the difference between the number obtained at a particular point by the program and a reasonably certain number for the same point obtained from experimental or other data. This difference was then added to (or subtracted from) the values obtained for the entire spectrum. The point used to fix the first calculated spectrum, from 0 to  $5 \times 10^6$  cm<sup>-1</sup>, was v=  $1.5802781 \times 10^4$  cm<sup>-1</sup>, for which the value assigned was n=1.33146.

This same point was similarly fixed in the calculations over the ranges 0 to  $5 \times 10^5$  and 0 to  $5 \times 10^4$  cm<sup>-1</sup>. For calculations over the ranges 0 to  $5 \times 10^n$  for n<4, a point was chosen in the graph of the calculated spectrum for 0 to  $5 \times 10^{n+1}$  cm<sup>-1</sup> which seemed most likely to be

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stable; that is, a point was chosen as far to the left (low wave number) as was reasonable, provided it was a region not undergoing violent oscillations, and hopefully provided it had a slope approximately zero. Accordingly, the following points were fixed for the ranges specified: for 0 to  $5 \times 10^3$  cm<sup>-1</sup>, v=2.103778×10<sup>3</sup> cm<sup>-1</sup> was fixed at n=1.311148; for 0 to  $5 \times 10^2$  cm<sup>-1</sup>, v=1.064143×10<sup>2</sup> cm<sup>-1</sup> was fixed at n=1.886343; for 0 to  $5 \times 10^1$ , v=8.332974 cm<sup>-1</sup> was fixed at n=2.481153; for 0 to  $5 \times 10^0$ , v= 9.090965×10<sup>-1</sup> cm<sup>-1</sup> was fixed at n=6.094436; for 0 to  $5 \times 10^{-1}$  cm<sup>-1</sup>, v=1.204759×10<sup>-1</sup> cm<sup>-1</sup> was fixed at n=8.676634.

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The process of joining the parts into one complete spectrum was accomplished by matching slopes and applying a weighted average. The goal was to obtain a smooth transition from one curve to the next in the region where the greater accuracy was presumed to shift from the first to the second curve.

No adjustment was necessary in several cases. The curve calculated for the range 0 to  $5 \times 10^{1}$  cm<sup>-1</sup> was joined to the curve for the range 0 to  $5 \times 10^{2}$  cm<sup>-1</sup> at the point fixed as described above, at v=8.332974 cm<sup>-1</sup>. This is illustrated in Figure 18. The curve for the range 0 to  $5 \times 10^{2}$ cm<sup>-1</sup> was joined to that for 0 to  $5 \times 10^{3}$  cm<sup>-1</sup> at the point v=1.064143 \times 10^{2} cm<sup>-1</sup>, as illustrated in Figure 19. The curve for the range 0 to  $5 \times 10^{3}$ cm<sup>-1</sup> was joined to that for the range 0 to  $5 \times 10^{4}$  cm<sup>-1</sup> at v=2.103778 \times 10^{3} cm<sup>-1</sup>, as illustrated in Figure 20. The curve for the range 0 to  $5 \times 10^{5}$ cm<sup>-1</sup> was joined to that for 0 to  $5 \times 10^{6}$  cm<sup>-1</sup> at v=3.076097 \times 10^{4} cm<sup>-1</sup>, as shown in Figure 22.

Adjustments were necessary in four cases. For the low end, the

value for n(v) calculated from the Cole-Cole equation was used to fix the single point  $v=lx10^{-3}$  cm<sup>-1</sup>. The curve there was assumed to have nearly zero slope. Then, a smooth transition was created up to the slope at  $v=7.144963 \times 10^{-2}$  cm<sup>-1</sup> as calculated from the curve for 0 to 5x10<sup>-1</sup> cm<sup>-1</sup>. A weighted average was applied to assure that the values of n(v) were as required at the endpoints, n=8.8486 at  $1 \times 10^{-3}$  cm<sup>-1</sup> (from the Cole-Cole equation) and n=8.7978 at  $7.144963 \times 10^{-2}$  cm<sup>-1</sup> (from the calculation over the range 0 to  $5 \times 10^{-1}$  cm<sup>-1</sup>). The result is illustrated by Figure 15. The curves for the ranges 0 to  $5 \times 10^{-1}$  and 0 to  $5 \times 10^{\circ}$  cm<sup>-1</sup> were connected by a similar procedure, the difference being that the slope at the lower end was calculated from the data just as was the slope at the higher end. The transition is illustrated by Figure 16. The curves for the ranges 0 to  $5 \times 10^{0}$  and 0 to  $5 \times 10^{1}$  cm<sup>-1</sup> were connected by the same process, as shown in Figure 17. The curves for the ranges 0 to  $5 \times 10^4$  and 0 to  $5 \times 10^5$  cm<sup>-1</sup> were connected by applying only a weighted average since this resulted in a smooth transition and left the fixed point, v=1.580278x10<sup>4</sup> cm<sup>-1</sup>, intact. This is illustrated by Figure 21.

The final n(v) spectrum is presented in Chapter V in both graphical and tabular form.

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The dashed line is the curve obtained Fig. 5. An illustration of the increased resolution obtained by reducing by calculation over the range 0 to  $5 \times 10^5$  cm<sup>-1</sup>. The latter curve shows decreased the range of calculation. The solid line is the curve for n(v) obtained by calculation over the range 0 to  $5x10^4$  cm<sup>-1</sup>. resolution. 301

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The point) is a result of proximity to the endpoint of the range of calculation. inaccuracy at the right end of the curve (primarily due to the last datum This is characteristic of the results illustrated in Figures 7 through 13 The spectrum calculated for the range 0 to  $5 \times 10^{6}$  cm<sup>-1</sup>. The phenomenon is discussed in the text. Fig. 6. also. 302

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87 5.00000 ----- 5.8000 4.00000 MAVE NUMBER (1/CM) (X 10<sup>+04</sup>) 1.00000 1.140 1.660 | 8.6 1.350 1.280 1.210 1.870 1.420 1.700 1.630 1.560 1.498

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93 5.00000 4.00000 WAUE NUMBER (1/CM) (X 10) 3.00000 2.00000 1.00000 1.666 | 6.6 9.000 6.600 5.800 5.000 4.208 1.806 8.200 7.400 3.480 2.600

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Fig. 11. The spectrum calculated for the range 0 to  $5 \times 10^{1}$  cm<sup>-1</sup>.

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The solid line was obtained by calculation over the smaller range 0 to 5x10<sup>5</sup> cm<sup>-1</sup>. The dashed line is n(v) as obtained by calculation over the range 0 to  $5x10^{6}$  cm<sup>-1</sup> The latter deviates from the dashed line as it approaches the right endpoint of Fig. 14. An illustration of inaccuracy as an endpoint is approached. the range of calculation. 310

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are n(v) as calculated over the range 0 to 5 cm<sup>-1</sup>. The solid curve is the calculated The short dashes are The long dashes n(v) as obtained by calculation over the range 0 to  $5x10^{-1}$  cm<sup>-1</sup>. Fig. 16. The transition in the region of  $10^{-1}$  cm<sup>-1</sup>. transition between the two. a state of the sta

105 1.40000 Ĭ 1.26000 0.89000 1.00000 MAVE NUMBER (1/CM) 0.60000 5.000 L 7.800 7.520 7.240 6.969 6.120 5.840 5.560 5.280 6.680 6.400 aa Ou

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calculated over the range 0 to  $5 \times 10^{1}$  cm<sup>-1</sup>. The solid curve is the calculated transition Fig. 17. The transition in the region of  $1 \text{ cm}^{-1}$ . The short dashes are n(v)as obtained by calculation over the range 0 to 5 cm<sup>-1</sup>. The long dashes are n(v) as between the two. 313

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The solid line is n(v) The two curves were connected as obtained by calculation over the range 0 to  $5 \times 10^{1}$  cm<sup>-1</sup>. The dashed line is Fig. 18. The transition in the region of 10 cm<sup>-1</sup>. n(v) as calculated over the range 0 to  $5x10^2$  cm<sup>-1</sup>. at their point of intersection. 314



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The solid line is n(v) as obtained by calculation over the range 0 to  $5 \times 10^2$  cm<sup>-1</sup>. The dashed line is n(v)as calculated over the range 0 to 5x10<sup>3</sup> cm<sup>-1</sup>. The two curves were connected at Fig. 19. The transition in the region of  $10^2 \text{ cm}^{-1}$ . their point of intersection

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The solid line is n(v)as obtained by calculation over the range 0 to  $5 \times 10^3$  cm<sup>-1</sup>. The dashed line is n(v)their point of intersection. The curves are so close together in this region that as calculated over the range 0 to  $5 \times 10^4$  cm<sup>-1</sup>. The two curves were connected at Fig. 20. The transition in the region of  $10^3$  cm<sup>-1</sup>. they are difficult to distinguish.



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Fig. 21. The transition in the region of  $10^4$  cm<sup>-1</sup>. The short dashes are The long dashes are n(v) as calculated over the range 0 to  $5x10^5$  cm<sup>-1</sup>. The solid line is the n(v) as obtained by calculation over the range 0 to  $5x10^4$  cm<sup>-1</sup>. calculated transition between the two. 317



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n(v) as obtained by calculation over the range 0 to  $5x10^5$  cm<sup>-1</sup>. The dashed line is n(v) as calculated over the range 0 to  $5x10^{6}$  cm<sup>-1</sup>. The curves are so close The solid line is together in this region that they are difficult to distinguish. The transition in the region of  $10^5 \text{ cm}^{-1}$ . Fig. 22.

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## CHAPTER V

## RESULTS

The final spectrum we obtained by combination of the several calculated curves as described in Chapter IV. To present only data of reasonably certain accuracy, values are not reported for the extreme endpoint regions of less than  $1 \times 10^{-3}$  cm<sup>-1</sup> and greater than  $1 \times 10^{6}$  cm<sup>-1</sup>. The  $n(\nu)$  spectrum is shown in Figures 23 through 30. The values of both the real and imaginary parts of  $N(\nu)$  (n and k) are presented in Table 1, immediately below. These results are discussed in Chapter VI.

TABLE 1\*

Wave Number (cm <sup>-1</sup> )	n	k
1.000000D-03	8.848600	6.9309081D-03
1.0092529D-03	8.848600	7.0111643D-03
1.0209395D-03	8.848600	7.0597634D-03
1.0303861D-03	8.848600	7.1415116D-03
1.0423174D-03	8.848600	7.2075912D-03
1.0519619D-03	8.848600	7.2910511D-03
1.0641430D-03	8.848600	7.3585144D-03
1.0764552D-03	8.848599	7.4437220D-03
1.0864256D-03	8.848599	7.5299162D-03
1.0990058D-03	8.848599	7.59958970-03
1.1117317D-03	8.848599	7.6875888D-03
1.1246050D-03	8.848599	7.7587211D-03
1.1376273D-03	8.848599	7.8485629D-03
1.1481536D-03	8.848599	7.9577473D-03
1.1641260D-03	8.848599	8.0313794D-03

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
1.1776060D-03	8.848598	8.1243784D-03
1.1912420D-03	8.848598	8.2184543D-03
1.2050359D-03	8.848598	8.3327844D-03
1.2189896D-03	8.348598	8.4292735D-03
1.2359474D-03	8.848598	8.5268798D-03
1.2502590D-03	8.848598	8.6256165D-03
1.2647363D-03	8.848598	8.7455107D-03
1.2823306D-03	8.848597	8.8468801D-03
1.3001696D-03	8.848597	8.9493222D-03
1.3152248D-03	8.848597	9.0947370D-C3
1.3335214D-03	8.848597	9.2000491D-03
1.3520726D-03	8.848596	9.3280345D-03
1.3708818D-03	8.848596	9.4578004D-03
1.3899526D-03	8.848596	9.5673165D-03
1.4092888D-03	8.848596	9.7004112D-03
1.4288940D-03	8.848595	9.8580302D-03
1.4487719D-03	8.848595	9.9951690D-03
1.4689263D-03	8.848595	1.0157577D-02
1.4927944D-03	8.848594	1.0298883D-02
1.5135612D-03	8.848594	1.0442155D-02
1.5381546D-03	8.848594	1.0611827D-02
1.5631476D-03	8.848593	1.0759452D-02
1.5885467D-03	8.848593	1.0909131D-02
1.6143586D-03	8.848592	1.1111947D-02
1.64058980-03	8.848592	1.12925010-02
	8.848591	1.1475990D-02
1.69433/80-03	8.848591	1.1662459D-02
1./2383/90-03	8.848590	1.18519590-02
1.73388030-03	0.040207	1.20/23030-02
1.70090/09-03	0.040307	1.22084030-02
1.85353147-03	0.040700	1.24903300-02
1 88799130-03	0.04030/	1.2/200/90-02
1 92309170-03	0.040300	1.27033205-02
1 95884478-03	8 848585	1.32003/35-02
1.99986190-03	8 868586	1.37337820-02
2.04173790-03	2,242522	1 39891120-02
2.0844909D-03	8 848581	1 42820370-02
2.12813900-03	8.848580	1,45810950-02
2.17270120-03	8.848579	1,49207320-02
2.22330990-03	8.848577	1.5233165D-02
2.2750974D-03	8.848576	1.55879910-02
2.3280913D-03	8.848574	1.59143950-02
2.38231950-03	8.848572	1.6322630D-02

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TABLE 1-Continued

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Wave Number (cm *)	n	ĸ
Z.4378108D-03	8.848570	1.67028330-02
2.3UU3434D-U3 3.544440D-03	8.846388 8 868544	1.71312930-02
2.30448400-03	8.840J00 8.040547	
2.33028800-03	8.840J0J 9 948540	1.002140/0-02
2.70373040-03	0.040300	1.0403/320-02
2.27759050-03	8 848554	1.90013990-02
2 94442140-03	8 848550	2 00812220-02
3 02691360-03	8 848546	2.00012220-02
3,12607940-03	8 848541	2.13201440-02
3.2284941D-03	8 848536	2.20186220-02
3.3342641D-03	8.848531	2.2739983D-02
3.4514374D-03	8.848524	2.34849770-02
3.5727284D-03	8.848518	2.4366331D-02
3.7068072D-03	8.848510	2.5222617D-02
3.8459178D-03	8.848501	2.6229508D-02
3.9994475D-03	8.848491	2.7213860D-02
4.1686938D-03	8.848480	2.8365480D-02
4.3451022D-03	8.848467	2.9565835D-02
4.5498806D-03	8.848452	3.0888025D-02
4.7643099D-03	8.848435	3.2343733D-02
5.0003453D-03	8.848415	3.3946120D-02
5.2601727D-03	8.848392	3.5710024D-02
5.5590426D-03	8.848364	3.7652181D-02
5.8884366D-03	8.848330	3.9791485D-02
6.2517269D-03	8.848291	4.2343831D-02
6.6680677D-03	8.848243	4.5059892D-02
7.1449633D-03	8.848183	4.8282544D-02
7.6913044D-03	8.848109	5.1974479D-02
8.3368118D-03	8.848013	5.62069660-02
9.0991327D-03	8.847889	6.1205457D-02
1.000000D-02	8.847727	6.72651540-02
1.00925290-02	8.84//10	5.8U44U48D-02
1.0209395D-02 1.0303841D-02	8.84/588 9.967671	6.8515/07D-02
1.030301D-02	0.04/0/1 0 0/74/0	0.73U7U81D-U2 4 0050701D-02
1 6519419D-02	0.04/040 2 267430	0.7734371 <b>0-</b> 42 7 87683798-82
1.03170170 <sup>-</sup> 06 1.0661630D-09	0.07/0JU 2 267414	7 1415114D-02
1.07646520-02	0.07/000 8 847582	7 2262A66B-02
1.0864256D=02	8 847563	7 30785870-02
1,09900580-02	8.847537	7.37547750-02
1.11173170-02	8.847512	7.46088150-02
1.1246050D-02	8.847485	7.54727450-02
1.13762730-02	8.847459	7.61710850-02

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
1.1481536D-02	8.847437	7.7230731D-02
1.1641260D-02	8.847403	7.7945338D-02
1.177606CD-02	8.847374	7.8847902D-02
1.1912420D-02	8.847344	7.9760918D-02
1.2050359D-02	8.847314	8.0870503D-02
1.2189896D-02	8.847283	8.1806939D-02
1.2359474D-02	8.847244	8.2754219D-02
1.2502590D-02	8.847212	8.3905445D-02
1.2647363D-02	8.847178	8.4877024D-02
1.2823306D-02	8.847137	8.5859854D-02
1.3001696D-02	8.847094	8.7054283D-02
1.3152248D-02	8.847058	8.8265329D-02
1.3335214D-02	8.847013	8.9287393D-02
1.3520726D-02	8.846967	9.0529505D-02
1.3708818D-02	8.846920	9.1788895D-02
1.3899526D-02	8.846871	9.2851761D-02
1.4092888D-02	8.846821	9.4360480D-02
1.4288940D-02	8.846769	9.5673165D-02
1.4487719D-02	8.846716	9.7004112D-02
1.4689263D-02	8.846662	9.8580302D-02
1.4927944D-02	8.846596	9.9951690D-02
1.5135612D-02	8.846538	1.0134216D-01
1.5381546D-02	8.846468	1.0298883D-01
1.5631476D-02	8.846396	1.0442155D-01
1.5885467D-02	8.846321	1.0611827D-01
1.6143586D-02	8.846244	1.0759452D-01
1.6405898D-02	8.846164	1.09342790-01
1.66724720-02	8.846082	1.1137562D-01
1.69433/80-02	8.845997	1.13185330-01
1.72583790-02	8.845876	1.1502444D-01
1./5388050-02	8.843804	1.1/162910-01
1./8648/60-02	8.842070	1.19086550-01
1.819/0090-02	8.843363	1.212802/D-01
1.85555160-02	8.84343/ 8.84545/	1.23230910-01
1.00/97130-02	0.043343	1.23631/20-01
	0.047620	1.201/1110-01
1.730044/0-02	0.042007	1.34034730-01
1.77700170-V2 2 0617370D-02	0.044730	1.3320/720-01
2.071/J/70-VE 2 A8649A9N-A9	0.077//0 8 844400	1 32682590-61
2.0077707D-02 2 128139ND-02	8 844434	1 41510980-01
2.1727012D-02	8.844254	1.44807200-01
2.22330990-02	8.844044	1_47839380-01
2.27509760-02	8.843823	1,5093506D-01
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Wave Number (cm <sup>-1</sup> )	n	k
2.3280913D-02	8.843591	1.5445079D-01
2.3823195D-02	8.843349	1.5804841D-01
2.4378108D-02	8.843095	1.6210266D-01
2.5003454D-02	8.842801	1.6587852D-01
2.5644840D-02	8.842491	1.7013362D-01
2.6302680D-02	8.842166	1.7449788D-01
2.7039584D-02	8.841790	1.7897408D-01
2.7797133D-02	8.841394	1.8398827D-01
2.8575905D-02	8.840974	1.8914294D-01
2.9444216D-02	8.840491	1.9444203D-01
3.0269134D-02	8.840020	2.0081222D-01
3.1260794D-02	8.839434	2.0643824D-01
3.2284941D-02	8.838809	2.1320144D-01
3.3342641D-02	8.838141	2.2018622D-01
3.4514374D-02	8.837375	2.2739983D-01
3.5727284D-02	8.836475	2.3560806D-01
3.7068072D-02	8.835449	2.4411257D-01
3.8459178D-02	8.834348	2.5350711D-01
3.9994475D-02	8.833091	2.6344511D-01
4.1686938D-02	8.831656	2.7408808D-01
4.3451022D-02	8.830103	2.8595003D-01
4.5498806D-02	8.828230	2.9832534D-01
4.7643099D-02	8.826184	3.1231306D-01
5.0003453D-02	8.823834	3.2771034D-01
5.26017270-02	8.821129	3.4481817D-01
5.5590426D-02	8.817867	3.6298622D-01
5.8884366D-02	8.814082	3.8369854D-01
6.2517269D-02	8.809677	4.0727724D-01
6.66806//D-02	8.804337	4.3370072D-01
7.14496330-02	8./9/836	4.6364987D-U1
7.69130440-02	8./88091	4.98299150-01
8.33661180-02	8.//6133	5.38009/50-01
9.09913270-02	8./61392	5.8450/5/0-01
	8.743107	5.40899810-01
	0./41UZY 0.770010	6.4/053450-01
	8./38919 9.77/77/	6.53356390-01
1.03086070-01	0./30//0	0.3984229D-01 4 4474457D-01
1.04137//D-01 1.05248880-01	0./34347 8 723324	0.00340330-01 6 79861788-01
1 48380802-01	0./JEEJO 8 798924	0./670130D-U1 6 70751650-01
1 07899445-01	0./27004 8 797/0/	0./7/J14JU-U1 4 8479071D-01
1 18607418-01	0./6/474 8 796811	0.00/20/10-01 6.00/20/10-01
1 AGGAGESD-A1 1.40076010-41	0+/62VII 8 700630	0.73023323"V1 7 88878-81
1 11101000-01	0./22732 8 710202	7 NR3300/0-01 7 NR33083D-01
* • * * ± £ ± 7 7 U = ¥ ±	0.717000	1.40334037-41

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
1.1235697D-01	8.717139	7.1591612D-01
1.1363183D-01	8.714366	7.2363597D-01
1.1494762D-01	8.711486	7.3137505D-01
1.1627866D-01	8.708553	7.3940119D-01
1.1765219D-01	8.705507	7.4756704D-01
1.1904194D-01	8.702404	7.5603194D-01
1.2047585D-01	8.699181	7.6453988D-01
1.2195511D-01	8.695941	7.7326819D-01
1.2345253D-01	8.692637	7.8222221D-01
1.2499712D-01	8.689204	7.9142569D-01
1.2659017D-01	8.685638	8.0073746D-01
1.2820353D-01	8.681999	8.1038267D-01
1.2986736D-01	8.678217	8.2014406D-01
1.3158307D-01	8.674287	8.3021417D-01
1.3332144D-01	8.670273	8.4060147D-01
1.3514501D-01	8.666029	8.5092277D-01
1.3699351D-01	8.661691	8.6176756D-01
1.3889928D-01	8.657181	8.7275057D-01
1.4083156D-01	8.652568	8.8448433D-01
1.4285650D-01	8.647693	8.9596314D-01
1.4494392D-01	8.642623	9.0779993D-01
1.4706184D-01	8.637431	9.2021677D-01
1.4924507D-01	8.632030	9.3280345D-01
1.5153048D-01	8.626323	9.4556229D-01
1.5385089D-01	8.620473	9.5893715D-01
1.5624280D-01	8.614382	9.7272515D-01
1.5874498D-01	8.607948	9.8571139D-01
1.6128/240-01	8.601342	1.00112920+00
1.6394569D-01	8.594362	1.0159917D+00
1.6664/960-01	8.58/191	1.0310747D+00
1.694/2800-01	8.579613	1.0471048D+00
1.72424910-01	8.5/1605	1.06289450+00
1./3420440-01	8.263363	1.08016510+00
1./0000010-01	8.334032 8.546540	1.09695840+00
1.01002300-01	0.34330U 0 5750/7	1.11303920+00
	0.JJJ74/ 0 534005	1.13209630+00
1 92309170-01	0.J2077J 8 517600	1.13203370400
1.9686497D-81	0.JI/770 8 507816	- 1 1010160540 - 1 1010160540
1,9998619D-01	8 697291	1 211965200400
2.06079790-01	3.47/670 8.686478	1 23307620400
2.08353120-01	8.474673	1.25600150+00
2.1276491D-01	8.462521	1,27788020+00
2.17370200-01	8.449912	1,30223730+00

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
2.2222863D-01	8.435660	1.3270587D+00
2.2724796D-01	8.420858	1.3520419D+00
2.3254125D-01	8.405156	1.3781299D+00
2.3812226D-01	8.389151	1.4047212D+00
2.4389337D-01	8.371979	1.4341354D+00
2.4997697D-01	8.352700	1.4631544D+00
2.5538936D-01	8.332788	1.4931043D+00
2.6314796D-01	8.311297	1.5250713D+00
2.7027134D-01	8.288448	1.5570055D+00
2.7777938D-01	8.264599	1.5910731D+00
2.8569326D-01	8.238281	1.6270097D+00
2.9410337D-01	8.209818	1.6629919D+00
3.0304003D-01	8.179843	1.7009445D+00
3.1253596D-01	8.147128	1.7409654D+00
3.2255219D-01	8.112180	1.7811075D+00
3.3334965D-01	8.074469	1.8238543D+00
3.4482600D-01	8.033791	1.8680571D+00
3.5710835D-01	7.989355	1.9142125D+00
3.7033947D-01	7.941322	1.9610567D+00
3.8459178D-01	7.889643	2.0108985D+00
4.0003685D-01	7.831158	2.0639071D+00
4.1667745D-01	7.768902	2.1134411D+00
4.3481048D-01	7.701126	2.1701519D+00
4.5456919D-01	7.625553	2.2242835D+00
4.7621163D-01	7.544423	2.2802903D+00
5.0003453D-01	7.455943	2.3377074D+00
5.2625956D-01	7.358822	2.3965701D+00
5.5552038D-01	7.252419	2.4608783D+00
5.8830156D-01	7.135674	2.5187795D+00
6.2502876D-01	7.007965	2.5756695D+00
6.6665325D-01	6.867192	2.6296027D+00
7.1433183D-01	6.711149	2.6846653D+00
7.6930756D-01	6.538143	2.7333179D+00
8.3333572D-01	6.346035	2.7731295D+00
9.0909653D-01	6.131865	2.8065976D+00
1.000000D+00	5.879378	2.8300242D+00
1.0101015D+00	5.853423	2.8276467D+00
1.0204083D+00	5.827179	2.8314972D+00
1.0309320D+00	5.800631	2.8350462D+00
1.0416696D+00	5.773802	2.8317841D+00
1.0526403D+00	5.746661	2.8347198D+00
1.0638245D+00	5.719272	2.8308714D+00
1.0752761D+00	5.691521	2.8331537D+00
1.0869511D+00	5.663535	2.8351768D+00

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TABLE 1-Continued

		·
Wave Number (cm <sup>-1</sup> )	n	k
1.0989046D+00	5.635201	2.8302848D+00
1.1111175D+00	5.606586	2.8315885D+00
1.1235955D+00	5.577699	2.8325667D+00
1.1363706D+00	5.548489	2.8331537D+00
1.1494233D+00	5.519027	2.8268980D÷00
1.1627866D+00	5.489262	2.8267679D+00
1.1764677D+00	5.459203	2.8262472D+00
1.19047425+00	5.428878	2.8253363D+00
1.2048140D+00	5.398286	2.8240354D+0C
1.2195230D+00	5.367389	2.8157892D+00
1.2345537D+00	5.336323	2.8137152D+00
1.250000D+00	5.304929	2.8111249D+00
1.2659017D+00	5.273172	2.8079550D+00
1.282C353D+00	5.241539	2.8047241D+00
1.2986736D+00	5.209531	2.8008519D+00
1.3158307D+00	5.177179	2.7963411D+00
1.3332144D+00	5.146161	2.79183750+00
1.3514501D+00	5.116001	2.78605790+00
1.3699351D+00	5.083439	2.7866995D+00
1.38399280+00	5.047771	2.7802903D+00
1.4083156D+00	5.013994	2.7738958D+00
1.42856500+00	4.979800	2.76624180+00
1.44943920+00	4.946351	2./5/9/380+00
1.4/051840+00	4.915201	2.74973060+00
1.49245070+00	4.881015	2.74719910+00
1.51530480+00	4.844088	2./3/096/0+00
1.33030090700	4.811400	2.72703140+00
1.38242000400	4.//04/0	2.72263939400
1.30/77700700	4.740422	2.710/3425+00
1.61267240400	4.704320	2 69209350+00
1.63743695400	4.607070	
1 69672800+00	4.631130	
1 72626910+00	4.555811	2 66189020+00
1 75428440+00	4.518750	2 66661120+00
1.78536510+00	4 482558	2.6362716D+00
1.8180256D+00	4,442443	2.6253677D+00
1.8518252D+00	4,403706	2,6072948D+00
1.8866876D+00	4.367201	2.5947179D+00
1.9230917D+00	4.328263	2.5810127D+00
1.9606497D+00	4.288766	2.5667888D+00
1.9998619D+00	4.248425	2.5514681D+00
2.0407979D+00	4.207585	2.5350711D+00
2.0835312D+00	4.166540	2.5176198D+00

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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
2.1276491D+00	4.125763	2.49971300+00
2.1737020D+00	4.084851	2.4307908D+00
2.2222863D+00	4.045111	2.4603118D+00
2.2724796D+00	4.003601	2.4450635D+00
2.3254125D+00	3.960586	2.4226470D+00
2.3812226D+00	3.917021	2.4043082D+00
2.4389337D+00	3.873564	2.3800723D+00
2.4997697D+00	3.829496	2.3598812D+00
2.5638936D+00	. 3.785136	2.3328679D+00
2.6314796D+00	3.741930	2.3098839D+00
2.7027134D+00	3.695213	2.2855469D+00
2.7777938D+00	3.650102	2.2547072D+00
2.8569326D+00	3.607096	2.2278715D+00
2.9410337D+00	3.563346	2.1993287D+00
3.0304003D+00	3.516889	2.1741532D+00
3.1253596D+00	3.468221	2.1423486D+00
3.2255219D+00	3.422465	2.1095516D+00
3.3334965D+00	3.374610	2.0791707D+00
3.4482600D+00	3.326631	2.0426321D+00
3.5710835D+00	3.279470	2.0090472D+00
3.7033947D+00	3.228984	1.9732865D+00
3.8459178D+00	3.179887	1.9310350D+00
4.0003685D+00	3.133464	1.8909940D+00
4.1667745D+00	3.084049	1.8534896D+00
4.3481048D+00	3.032401	1.8092148D+00
4.5456919D+00	2.983258	1.7627476D+00
4.7621163D+00	2.933900	1.7178694D+00
5.0003453D+00	2.881863	1.6702833D+00
5.2625956D+00	2.831974	1.6165537D+00
5.5552038D+00	2.781861	1.5670763D+00
5.8830156D+00	2.729264	1.5107414D+0C
6.2502876D+00	2.679108	1.4517443D+30
6.6665325D+00	2.629097	1.3928044D+00
7.1433183D+00	2.577344	1.3301179D+00
7.6930756D+00	2.527536	1.2609276D+00
8.3329735D+00	2.481153	1.1912150D+00
9.0907560D+00	2.436760	1.1199281D+00
1.000000D+01	2.399111	1.0418139D+00
1.0519619D+01	2.385313	1.0110908D+00
1.1117317D+01	2.363856	9.8353573D-01
1.1776060D+01	2.337241	9.5014556D-01
1.2502590D+01	2.312599	9.1157025D-01
1.3335214D+01	2.290196	8.7254964D-01
1.4288940D+01	2.270109	8.3136195D-01

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TABLE	1-Continued	1

Wave Number (cm <sup>-1</sup> )	n	k
1.5381546D+01	2.254575	7.9211848D-01
1.6672472D+01	2.236685	7.6171085D-01
1.7258379D+01	2.228339	7.4780806D-01
1.7864876D+01	2.220374	- 7.3585144D-01
1.8535316D+01	2.210869	- 7.2408599D-01
1.9230917D+01	2.200349	7.1250865D-01
1.9998619D+01	2.188736	6.9950391D-01
2.0844909D+01	2.177335	6.8515707D-01
2.1727012D+01	2.166254	6.7265154D-01
2.2750974D+01	2.153213	6.5885545D-01
2.3823195D+01	2.139507	6.4534232D-01
2.5003454D+01	2.125742	6.2920207D-01
2.6302680D+01	2.112811	6.1346550D-01
2.7797133D+01	2.099543	5.9674686D-01
2.9444216D+01	2.086956	5.8048385D-01
3.1260794D+01	2.073976	5.6596574D-01
3.3342641D+01	2.059773	5.5054160D-01
3.4514374D+01	2.052476	5.4298789D-01
3.5727284D+01	2.045135	5.3553782D-01
3.7068072D+01	2.037243	<b>3.2818996D-01</b>
3.8459178D+01	2.029224	5.20942920-01
3.9994475D+01	2.020318	5.13795320-01
4.1686938D+01	2.010446	5.0558030D-01
4.34510220+01	2.001418	4.9635242D-01
4.34988060+01	1.992287	4.8729297D-01
4./6430390+01	1.983438	4.7839887D-01
5.00034330401	1.9/4559	4.6966713D-01
J.2001/2/D+01	1.900100	4.6109471D-01
5 88863640403	1.900/36	4.50598920-01
6 251726 QD+01	1.749417	4.40342030-01
6 66806770+01	1.741033	4.3330145D-01 6.3477766D-01
7 14494330+01	1 007410	4.20527700-01
7 69130640+01	1.72/912	4.2052338D-01
8.33681180+01	1 911471	4.16644000-01
9.09913270+01	1.7110/1	4.1742961D_01
1.00000000000	1.899131	4 3831885D-01 4 3831885D-01
1.0209395D+02	1.895435	4.43394360-01
1.0423174D+02	1.891384	4.48528600-01
1.0641430D+02	1.886330	4,54768260-01
1.0864256D+02	1.880545	4.60034230-01
1.1117317D+02	1.874242	4.6536117D-01
1.1376273D+02	1.867327	4.7183499D-01
1.1641260D+C2	1.859854	4.7729858D-01

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
1.19126200+02	1 851963	6 8393867D-01
1,2189896D+02	1.842330	4.90670720-01
1.2502590D+02	1.830882	4.9635242D-01
1.2823306D+02	1.819110	5.0209991D-01
1.3152248D+02	1.805539	5.0791395D-01
1.3520726D+02	1.790800	5.1025838D-01
1.3899526D+02	1.777162	5.1379532D-01
1.4288940D+02	1.762824	5.1735678D-01
1.4689263D+02	1.747333	5.2094292D-01
1.5135612D+02	1.729441	5.2334749D-01
1.5631476D+02	1.709762	5.2455393D-01
1.6143586D+02	1.690223	5.2455393D-01
1.6672472D+02	1.669053	5.2576315D-01
1.7258379D+02	1.643739	5.2334749D-01
1.7864876D+02	1.619157	5.1616689D-01
1.8535316D+02	1.594131	5.0791395D-01
1.9230917D+02	1.567492	4.9749663D-01
1.9998619D+02	1.542270	4.7729858D-01
2.0417379D+02	1.531473	4.6750918D-01
2.08449090+02	1.520272	4.5792056D-01
2.12813700+02	1.508821	4.4046/80D-01 6.3030680D-01
2.1/2/0120+02	1.497424	4.32304890-01
2.22334779442	1.491343	4.17526510-01
2.2/JU7/7D702 2.3220013D102	1.405200	7.0232240J-01 3.8794285D-01
2 32007130+02	1 477194	3 73929860+01
2 43781080+02	1 475642	3 58748540-01
2.50034540+02	1.476571	3.44183580-01
2.5644840D+02	1.478232	3.31734120-01
2.6302680D+02	1.481006	3.1899960D-01
2.7039584D+02	1.486740	3.0675394D-01
2.7797133D+02	1.492960	2.9908191D-01
2.8575905D+02	1.498932	2.9160176D-01
2.9444216D+02	1.505906	2.8627943D-01
3.0269134D+02	1.511879	2.8300242D-01
. 3.1260794D+02	1.519076	2.7976291D-01
3.2284941D+02	1.527225	2.7911948D-01
3.3342641D+02	1.535500	2.8170214D-01
3.4514374D+02	1.542658	2.8892834D-01
3.5727284D+02	1.546272	2.9903191D-01
3.7068072D+02	1.546670	3.1030598D-01
3.8459178D+02	1.544080	3.2269344D-01
3.9994475D+02	1.537967	3.3557542D-01
4.1686938D+02	1.529309	3.4816903D-01

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AL SURVEY SUBJECTION OF SUPERIORS IN SUCCESSION OF SUPERIORS

TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
4.3451022D+02	1.516402	3.6290265D-01
4.5498806D+02	1.499422	3.7221181D-01
4.7643099D+02	1.483693	3.8175976D-01
5.0003453D+02	1.467642	3.9335995D-01
5.0118723D+02	1.467249	3.9426674D-01
5.0234259D+02	1.467000	3.9517562D-01
5.0350061D+02	1.466543	3.9699967D-01
5.0466130D+02	1.465400	3.9883214D-01
5.0582466D+02	1.463349	4.0067306D-01
5.0815944D+02	-1.460391	4.0067306D-01
5.0933087D+02	1.459690	4.0159671D-01
5.1050500D+02	1.458719	4.0252248D-01
5.1168184D+02	1.457713	4.0345039D-01
5.1286138D+02	1.456898	4.0438044D-01
5.1404365D+02	1.455604	4.0624698D-01
5.1522864D+02	1.453825	4.0718347D-01
5.1641637D+02	1.452188	4.0812213D-01
5.1760683D+02	1.450255	4.0906295D-01
5.1999600D+02	1.447502	4.0906295D-01
5.2119471D+02	1.446666	4.1000594D-01
5.22396190+02	1.445486	4.1095110D-01
5.2360044D+02	1.444197	4.1189844D-01
5.2480746D+02	1.442846	4.1284796D-01
5.2601727D+02	1.441618	4.1379967D-01
5.2722936D+02	1.439563	4.1570969D-01
5.29663440+02	1.435881	4.1570969D-01
5.30884440+02	1.434643	4.1666800D-01 .
5.3210826D+02	1.432797	4.1762851D-01
5.3334900+02	1.431240	4.1762851D-01
5.3456436D+02	1.429982	4.1859125D-01
5.35796660+02	1.928308	4.19556200-01
5.5/051800+02	1.4251/8	4.20523380-01
5.39510620402	1.422820	4.20523380-01
5.40/54320402	1.42100/	4.21492/80-01
J. 42000070702 8 43384330403	1.417607	4.22464420-01
J. 4J2JUJJUTUZ	1.415274	4.23436310-01
J. 77JU20JU7U2 8. 47018040409	1.7132/0	4.23430310-01
3.77013705742 8 48974248119	1.716V76 1 618610	4.22730310-01 7.23730310-01
3.796/0705706 5.605419771400	1.71V717 1 68267	7.67717730-V1 6 96616638-01
5 502070705409 5 50207700409	1 464784	
5.50007766742	1 494694	
5.5642571D+02	1.401128	4 2539281D-01
5.5591426040	1.399826	4 25392810-01
	//WEV	

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TABLE	1-Conti	inued
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Wave Number (cm <sup>-1</sup> )	n	k
5.5718575D+02	1.398169	4.2637344D-01
5.5847019D+02	1.396377	4.2637344D-01
5.5975760D+02	1.394313	4.2735633D-01
5.6234133D+02	1.390838	4.2637344D-01
5.6363766D+02	1.389417	4.2735633D-01
5.6493697D+02	1.387734	4.2735633D-01
5.6623929D+02	1.385875	4.2834149D-01
5.6754461D+02	1.383660	4.2834149D-01
5.7016427D+02	1.380029	4.2834149D-01
5.7147864D+02	1.378598	4.2834149D-01
5.7279603D+02	1.376758	4.2932892D-01
5.7411646D+02	1.374519	4.2932892D-01
5.7676646D+02	1.370751	4.2932892D-01
5.7809605D+02	1.369211	4.2932892D-01
5.7942870D+02	1.367219	4.3031862D-01
5.8076442D+02	1.364655	4.3031862D-01
5.8344510D+02	1.361083	4.2932892D-01
5.8479008D+02	1.359301	4.3031862D-01
5.8613816D+02	1.356772	4.3031862D-01
5.8884366D+02	1.352834	4.2932892D-01
5.9020108D+02	1.351233	4.2932892D-01
5.9156163D+02	1.349696	4.2932892D-01
5.9292532D+02	1.347481	4.3031862D-01
5.9566214D+02	1.342949	4.2932892D-01
5.9703529D+02	1.341074	4.2932892D-01
5.9841160D+02	1.338869	4.2932892D-01
6.0117374D+02	1.334869	4.2834149D-01
6.0255959D+02	1.333056	4.2834149D-51
6.0394853D+02	1.330870	4.2834149D-01
6.0673633D+02	1.326773	4.2735633D-01
6.0813500D+02	1.324631	4.2735633D-01
6.0953690D+02	1.322675	4.2637344D-01
6.1094202D+02	1.320901	4.2637344D-01
6.1376201D+02	1.317122	4.2539281D-01
6.1517687D+02	1.315327	4.25392810-01
6.1659500D+02	1.313112	4.25392810-01
6.1944108D+02	1.308540	4.2441443D-01
6.2086903D+02	1.306556	4.2343831D-01
6.2373484D+02	1.303145	4.2246442D-01
6.2517269D+02	1.301310	4.2246442D-01
5.2661386D+02	1.298872	4.2246442D-01
6.2950618D+02	1.294706	4.2052338D-01
6.3095734D+02	1.292723	4.2052338D-01
6.3Z41185D+02	1.290576	4.1955620D-01

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
· · · · · · · · · · · · · · · · · · ·		
6.3533093D+02	1.286576	4.18591250-01
6.3679552D+02	1.284709	4.1762851D-01
6.3826349D+02	1.282639	4.1762851D-01
6.4120958D+02	1.278233	4.1570969D-01
6.4268772D+02	1.276473	4.1475358D-01
6.4565423D+02	1.272559	4.1379967D-01
6.4714262D+02	1.270391	4.1284796D-01
6.4863443D+02	1.268440	4.1189844D-01
6.5162839D+02	1.265082	4.1000594D-01
6.5313055D+02	1.263173	4.1000594D-01
6.5614527D+02	1.258880	4.0812213D-01
6.5765784D+02	1.256977	4.0718347D-01
6.6069345D+02	1.253631	4.0531264D-01
5.6221650D+02	1.251704	4.0531264D-01
6.6374307D+02	1.249380	4.0438044D-01
6.6680677D+02	1.245318	4.0252248D-01
6.6834392D+02	1.243348	4.0159671D-01
6.7142885D+02	1.239445	<b>3.9975154D-01</b>
6.7297666D+02	1.237500	3.9883214D-01
6.7608298D+02	1.233597	3.9699967D-01
6.7764151D+02	1.231631	3.9608659D-01
6.8076936D+02	1.227627	3.9426674D-01
6.8233869D+02	1.225566	3.9335995D-01
6.8548823D+02	1.220973	3.9155263D-01
6.8706844D+02	1.218762	3.8975361D-01
6.9023980D+02	1.215328	3.8707056D-01
6.9183097D+02	1.213645	3.8618032D-01
6.9502432D+02	1.209428	3.8440599D-01
6.9662651D+02	1.207465	3.8263980D-01
6.9984200D+02	1.203552	3.8088173D-01
7.0145530D+02	1.201594	3.7913174D-01
7.0469307D+02	1.197623	3.7738979D-01
7.0631755D+02	1.195603	3.7565584D-01
7.09577770+02	1.191399	3.7392986D-01
7.1121351D+02	1.189086	3.7221181D-01
7.1449633D+02	1.184740	3.6964952D-01
7.1614341D+02	1.182458	3.6795113D-01
7.1944898D+02	1.178513	3.6457774D-01
7.2276980D+02	1.174089	3.6206800D-01
7.2443596D+02	1.172049	3.5957554D-01
7.2777980D+02	1.167947	3.5710024D-01
7.2945751D+02	1.165763	3,5464198D-01
7.3282453D+02	1.161869	3.5139060D-01
7 76617070+00	1 1/0180	7 (4071(50-0)

1. A SARANA DARANA SARANA SARANA SARANA SARANA SA SARANA SAN INI MAMANINI KAMA SAMINI MANANA SANA SANA SANA SA

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
7.3790423D+02	1.156338	3.4656934D-01
7.4131024D+02	1.151643	3.4260220D-01
7.4301914D+02	1.149628	3.4024374D-01
7.4644876D+02	1.145850	3.3634900D-01
7.4989421D+02	1.141428	3.3249885D-01
7.5162289D+02	1.139515	3.2945048D-01
7.5509223D+02	1.135773	3.2567929D-01
7.5683290D+02	1.133825	3.2269344D-01
7.6032628D+02	1.130583	3.1826592D-01
7.6383578D+02	1.126485	3.1389915D-01
7.6559661D+02	1.124841	3.1030598D-01
7.6913044D+02	1.122067	3.0604842D-01
7.7268059D+02	1.118262	3.0115505D-01
7.7446180D+02	1.116753	2.9770775D-01
7.7803655D+02	1.114243	2.9294773D-01
7.8162780D+02	1,110319	2.8826382D-01
7.8342964D+02	1.108999	2.8365480D-01
7.8704579D+02	1.107403	2.7911948D-01
7.9067863D+02	1.104624	2.7402497D-01
7.9432823D+02	1.100816	2.6902345D-01
7.9615935D+02	1.099603	2.6411322D-01
7.9983426D+02	1.098011	2.5929261D-01
8.0352612D+02	1.095643	2.5280761D-01
8.0723503D+02	1.092375	2.4762252D-01
8.0909590D+02	1.091270	2.4198595D-01
8.1283052D+02	1.090913	2.35933790-01
8.1658237D+02	1.089721	2.2950394D-01
8.2035154D+02	1.087212	2.2376396D-01
8.2224265D+02	1.086723	2.1766577D-01
8.2603795D+02	1.087993	2.1124680D-01
8.2985077D+02	1.087926	2.0548974D-01
8.3368118D+02	1,087480	1.9897117D-01
8.3752928D+02	1.086163	1.9265937D-01
8.3945999D+02	1.086474	1.8654781D-01
8.4333476D+02	1.089062	1.80214670-01
8.4722741D+02	1.090622	1.7409654D-01
8.51138040+02	1.092339	1.6779930D-01
8.5506671D+02	1.094339	1.6210266D-01
8.5901332D+02	1.096068	1.5696042D-01
8.6297855D+02	1.096584	1.5198130D-01
8.6496792D+02	1.097503	1.4716012D-91
8.6896043D+02	1.100705	1.4216417D-01
8.72971370+02	1.103057	1.37021950-01
8.77000820+02	1.105361	1.3206573D-01

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
8.8104887D+02	1.107674	1.2699603D-0
8.8511561D+02	1.110334	1.2184007D-0
8.8920112D+02	1.113289	1.1716291D-0
8.9330548D+02	1.116059	1.1292501D-0
8.9742879D+02	1.118841	1.0834033D-0
9.0157114D+02	1.122010	1.0394178D-0
9.0573260D+02	1.125456	9.9951690D-0
9.0991327D+02	1.128640	9.6781009D-0
9.1411324D+02	1.131445	9.3280345D-0
9.1833260D+02	1.134419	8.96995250-0
9.2257143D+02	1.137372	8.6455006D-0
9.2682982D+02	1.140345	8.2944987D-0
9.3110788D+02	1.143601	7.9577473D-0
9.3540567D+02	1,146959	7.65226750-0
9.39723310+02	1.150368	7.35851440-0
9.4406088D+02	1.153843	7.09234970-0
9.4841846D+02	1.157248	6.85157070-0
9.5279616D+02	1.160584	6.6189659D-0
9.57194070+02	1,163960	6.3942578D-0
9.61612280+02	1 167354	6.19141830-0
9.66050880+02	1.170827	5.99501320-0
9,70509970+02	1.174182	5.84507570-0
9.74989640+02	1,178360	5 63365360-0
9.79489990+02	1,180893	5.80483850-0
9.86279490+02	1.183900	5.38009750-0
9,9083194D+02	1.187365	5.26975160-0
9,95405420+02	1,190334	5.17356780-0
1.000000D+03	1,193164	5.07913950-0
1.0046158D+03	1.195932	4.99792970-0
1.00925290+03	1,198600	4.92935550-0
1,01626870+03	1 202228	6 8505406D-0
1.02093950+03	1.204471	4.78398870-0
1.02565190+03	1 206729	4 7183499D-0
1,03032610+03	1 208909	4 6663396D-0
1.0351422D+03	1.211068	4.60036230-0
1.04231740+03	1.214136	4.53722320-0
1.04712850+03	1 216115	6.4749702D-0
1 05796190+03	1 218113	4 4339434D-0
1.05925370+03	1.220909	4.3731074D=0
1.06616300+03	1 222699	4.33301450-0
1.06905490+03	1 226679	4.29302430-00 6.2932892D-00
1.07666520+03	1 226967	4 234323723-07
1.0816360D+03	1 228580	4 ]QEECOND-04
1 68469848468	1 230267	4.16753500000

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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
1.0939564D+03	1.232659	4.1095110D-02
1.0990058D+03	1.234142	4.0718347D-02
1.1040786D+03	1.235657	4.0345039D-02
1.1117317D+03	1.237862	3.9883214D-02
1.1168632D+03	1.239322	3.9517562D-02
1.1246050D+03	1.241424	3.9155263D-02
1.1297959D+03	1.242789	3.8796285D-02
1.1376273D+03	1.244791	3.8440599D-02
1.1428783D+03	1.246095	3.8088173D-02
1.1481536D+03	1.247433	3.7825976D-02
1.1561122D+03	1.249353	3.7479185D-02
1.1641260D+03	1.251193	3.7135574D-02
1.1694994D+03	1.252405	3.6879935D-02
1.1776060D+03	1.254220	3.6541817D-02
1.1830416D+03	1.255384	3.6373923D-02
1.1912420D+03	1.257072	3.6040445D-02
1.1967405D+03	1.258240	3.5792344D-02
1.2050359D+03	1.259903	3.5627893D-02
1.2133889D+03	1.261488	3.5301255D-02
1.2189896D+03	1.262564	3.5139060D-02
1.2274392D+03	1.264125	3.4897165D-02
1.2359474D+03	1.265652	3.4656934D-02
1.2416523D+03	1.266657	3.4497700D-02
1.2502590D+03	1.268163	3.4260220D-02
1.2589254D+03	1.269613	3.4102808D-02
1.2647363D+03	1.270543	3.3946120D-02
1.2735031D+03	1.271952	3.3712437D-02
1.2823306D+03	1.273363	3.3480362D-02
1.2912193D+03	1.274794	3.3249885D-02
1.3001696D+03	1.276220	3.3097115D-02
1.3061709D+03	1.277123	3.3020994D-02
1.3152248D+03	1.278508	3.2793679D-02
1.3243415D+03	1.279895	3.2718256D-02
1.3335214D+03	1.281248	3.2567929D-02
1.3427650D+03	1.282606	3.2493025D-02
1.3520726D+03	1.283912	3.2418293D-02
1.3614447D+03	1.285242	3.2269344D-02
1.3708818D+03	1.286624	3.2195127D-02
1.3803843D+03	1.287944	3.2195127D-02
1.3899526D+03	1.289296	3.2047204D-02
1.3995873D+03	1.290696	3.2047204D-02
1.4092388D+03	1.292093	3.1973497D-02
1.4190575D+03	1.293609	3.1899960D-02
1.4288940D+03	1.295193	3.1973497D-02

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
1.4387986D+03	1.296751	3.2121080D-02
1.4487719D+03	1.298382	3.2195127D-02
1.4588143D+03	1.300125	3.2418293D-02
1.4689263D+03	1.301901	3.2718256D-02
1.4825181D+03	1.304521	3.30971150-02
1.4927944D+03	1.306716	3.3712437D-02
1.5031420D+03	1.309021	3.4497700D-02
1.5135612D+03	1.311404	3.5627893D-02
1.5275661D+03	1.314837	3.7306984D-02
1.5381546D+03	1.317726	3.9245525D-02
1.5488166D+03	1.320468	4.1762851D-02
1.5631476D+03	1.325038	4.4852860D-02
1.5739829D+03	1.329242	4.9521084D-02
1.5885467D+03	1.335754	5.6988883D-02
1.5995580D+03	1.339863	6.9458855D-02
1.6143586D+03	1.341605	8.7859786D-02
1.6255488D+03	1.330121	1.1716291D-01
1.6405898D+03	1.295314	1.3085495D-01
1.6519618D+03	1.268459	1.2496550D-01
1.6672472D+03	1.242862	1.0685384D-01
1.6788040D+03	1.231892	8.6455006D-02
1.6943378D+03	1.229289	6.2199965D-02
1.7100153D+03	1.234896	4.3230489D-02
1.72583790+03	1.242239	3.2945048D-02
1.73780080+03	1.248370	2.48193350-02
1.75388070+03	1.256584	2.0313/520-02
1.1/010300+02	1.262994	
1./6048/00403	1.200002	1.4183/200-02
1.00301//0403	1.2/3003	1.23831720-02
1.017/0070703	1.2/0671	1.13021/00-02
1.03033030403	1.206177	1.07042330-02
1 \$704\$210+03	1.200/27	1.02700030-02
1 82700130+03	1.207013	9.00073335-03
1.00/77130+03	1 294933	9.90353280-03
3,92309170+03	1 297550	
1,94088590+03	1 299910	1 06118270-02
1,9588447D+03	1.301965	1,11119470-02
1.9815270D+03	1.304258	1.17975040-02
1.9998619D+03	1.305885	1.24105250-02
2.0183664D+03	1.307228	1.3115660D-02
2.0417379D+03	1.308720	1.37021950-02
2.0606299D+03	1.309721	1.44141870-02
2.0844909D+03	1.310657	1.4989603D-02

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
2.1037784D+03	1.311148	1.5516371D-02
2.1281390D+03	1.311451	1.5696042D-02
2.1527817D+03	1.311588	1.5480684D-02
2.1727012D+03	1.311785	1.4716012D-02
2.1978599D+03	1.312483	1.3607870D-02
2.2233099D+03	1.313587	1.23819810-02
2.2490546D+03	1.314920	1.1396989D-02
2.2750974D+03	1.316398	1.0298883D-02
2.3014418D+03	1.318113	9.3065806D-03
2.3280913D+03	1.319948	8.4487049D-03
2.3550493D+03	1.321906	7.5995897D-03
2.3823195D+03	1.323997	6.8831961D-03
2.4099054D+03	1.326183	6.2199965D-03
2.4378108D+03	1.328504	5.6206966D-03
2.4717241D+03	1.331403	5.0674578D-03
2.5003454D+03	1.333929	4.6003423D-03
2.5292980D+03	1.336658	4.1570969D-03
2.5644840D+03	1.340174	3.8000573D-03
2.6001596D+03 ·	1.343958	3.5301255D-03
2.6302680D+03	1.347393	3.4024374D-03
2.6668587D+03	1.351891	3.4024374D-03
2.7039584D+03	1.356937	3.5957554D-03
2.7415742D+03	1.362546	4.2343831D-03
2.7797133D+03	1.368863	5.1497974D-03
2.8183829D+03	1.376092	6.7887551D-03
2.8575905D+03	1.384213	9.3926933D-03
2.8973436D+03	1.393260	1.3206573D-02
2.9444216D+03	1.404875	1.9489026D-02
2.9853826D+03	1.417064	2.6108994D-02
3.0269134D+03	1.432585	3.6879935D-02
3.0760968D+03	1.449409	6.1064688D-02
3.1260794D+03	1.461522	9.2425146D-02
3.1768741D+03	1.466753	1.3483112D-01
3.2284941D+03	1.452013	1.9177418D-01
3.2809529D+03	1.411876	2.3976741D-01
3.3342641D+03	1.352917	2.7213860D-01
3.3496544D+03	1.334533	2.7213860D-01
3.3573761D+03	1.326310	2.7592442D-01
3.3728731D+03	1.307891	2.7847752D-01
3.3806484D+03	1.297762	2.8170214D-01
3.3884416D+03	1.285942	2.8235153D-01
3.4040819D+03	1.263935	2.8040783D-01
3.4119291D+03	1.252073	2.7976291D-01
3.4197944D+03	1.240033	2.7592442D-01

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
3.4276779D+03	1.229654	2.7151270D-01
3.4434993D+03	1.208002	2.6472207D-01
3.4514374D+03	1.195889	2.5810127D-01
3.4593938D+03	1.185419	2.4933896D-01
3.4673685D+03	1.178446	2.3921596D-01
3.4833732D+03	1.162372	2.2897609D-01
3.4914032D+03	1.152284	2.1816754D-01
3.4994517D+03	1.145545	2.0596344D-01
3.5075187D+03	1.142386	1.9399482D-01
3.5237087D+03	1.133346	1.7980019D-01
3.5318317D+03	1.127523	1.6702833D-01
3.5399734D+03	1.125351	1.5409557D-01
3.5481339D+03	1.125532	1.4216417D-01
3.5563132D+03	1.128413	1.3115660D-01
3.5727284D+03	1.129478	1.2100133D-01
3.5809644D+03	1.127558	1.1188971D-01
3.5892193D+03	1.127959	1.0204463D-01
3.5974934D+03	1.130913	9.2851761D-02
3.6140986D+03	1.132778	8.3519934D-02
3.6224300D+03	1.131711	7.4437220D-02
3.6307805D+03	1.132860	6.4832108D-02
3.6391504D+03	1.136183	5.4801209D-02
3.6475395D+C3	1.142068	4.6215765D-02
3.6643757D+03	1.149520	3.8000573D-02
3.6728230D+03	1.152876	2.8170214D-02
3.6812897D+03	1.160993	2.0501713D-02
3.6897760D+03	1.168874	1.8611876D-02
3.6982818D+03	1.174582	1.6397972D-02
3.7068072D+03	1.179962	1.4514101D-02
3.72391710+03	1.188087	1.2599603D-02
3.7325016D+03	1.191390	1.0490354D-02
3.74110590+03	1.195340	8.5465363D-03
3.7497300D+03 7.75877(0)+03	1.199289	7.3247051D-03
3./583/400+03	1.202951	6.27754950-03
3./5/03800+03	1.206519	5.36772360-03
J.//J/2190+03	1.209934	4.8282344D-03 4.747665D-07
J./7J1470D+0J Z 0010040D+0J	1.213077	4.36304950-03
3.0010740U703 3.0010740U703	1.610V/0 1.990E3E	2 2020004D-V1 4.07340/TD-03
J.GIUDJOCUTUJ 3 81044970103	1 221082	J.JUZU774D-UJ 9 47747760-42
J.017446/U7UJ 3.80806768163	1.663406	2.7//U//JU-V3 2.70268315-03
3.02027/70703 3.83707050103	1.26340J 1.997760	2./UZ0J610-UJ 9 87867488-63
3.85478340303	1 231234	2.J/JU/030-V3 2 4769989R-A3
3.86366980+03	1.631037	2.7/026360-V3 9 6956172N-A1
J. 9930070JTV3	1.6330/7	6.76J7J/00-UJ

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
3.8725764D+03	1.235426	2.3866577D-03
3.8815037D+03	1.237089	2.3377074D-03
3.8904514D+03	1.238670	2.3109478D-03
3.8994199D+03	1.240167	2.2687683D-03
3.9174188D+03	1.243014	2.1418554D-03
3.9355008D+03	1.245672	2.0691413D-03
3.9536662D+03	1.248127	2.0173913D-03
3.9719155D+03	1.250383	1.9897117D-03
3.9810717D+03	1.251445	1.9533953D-03
3.9994475D+03	1.253465	1.9001599D-03
4.0179081D+03	1.255347	1.8104650D-03
4.0364539D+03	1.257102	1.7091892D-03
4.0457589D+03	1.257969	1.5804841D-03
4.0644333D+03	1.259683	1.4716012D-03
4.0831939D+03	1.261297	1.3483112D-03
4.1020410D+03	1.262824	1.2496550D-03
4.1114972D+03	1.263577	1.1502444D-03
4.1304750D+03	1.265059	1.0710017D-03
4.1495404D+03	1.266450	9.9035328D-04
4.1686938D+03	1.267787	9.0947370D-04
4.1879357D+03	1.269059	8.4877024D-04
4.1975898D+03	1.269682	7.9211848D-04
4.2169650D+03	1.270902	7.4266019D-04
4.2364297D+03	1.272062	6.8515707D-04
4.25598410+03	1.273184	6.3648789D-04
4.2/562890+03	1.274257	5.9950132D-04
4.2953643D+03	1.275295	5.42987890-04
4.31319080+03	1.276305	5.1143464D-04
4.32313830+03	1.2/0/9/	4.91801830-04
· · · · · · · · · · · · · · · · · · ·	1.2///33	4.68366900-04
4.3031303U703 4.3031303U703	1.2/00/2	4.30398920-04
4.30330705403	1.2/7301	4.29328920-04
4.40552370103	1.200721	4.U012213D-04 3.8075341D-04
4.4631978483	1.201230	3.09/33010-04
4.44031270703	1 282852	3 57100260-04
4.4876539D+03	1 283619	3 45772260-04
4.5081670D+03	1.284365	3.41028080-04
4.5289758D+03	1.285087	3.38680460-04
4.5498806D+03	1.285790	3,37901520-04
4.57028190+03	1.286474	3.39461200-04
4.5919801D+03	1.287139	3.4339198D-04
4.6131757D+03	1.287787	3.50582430-04
4.6344692D+03	1.288418	3.5874854D-04

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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
4.6558609D+03	1.289033	3.7050165D-04
4.6773514D+03	1.289634	3.8263980D-04
4.6989411D+03	1.290221	3.9699967D-04
4.7206304D+03	1.290795	4.1762851D-04
4.7424199D+03	1.291353	4.4034203D-04
4.7643099D+0 <b>3</b>	1.291899	4.6429087D-04
4.7863009D+03	1.292438	4.8841629D-04
4.8083935D+03	1.292966	5.2940757D-04
4.8305880D+03	1.293476	5.7251932D-04
4.8528850D+03	1.293973	6.2056909D-04
4.8752849D+03	1.294457	6.7420217D-04
4.8977882D+03	1.294919	7.3924797D-04
4.9317380D+03	1.295606	8.0498937D-04
4.9545019D+03	1.296066	8.8877155D-04
4.9773708D+03	1.296499	9.9035328D-04
5.0003453D+03	1.296913	1.10100720-03
5.0234259D+03	1.297292	1.2496550D-03
5.0466130D+03	1.297607	1.4021360D-03
5.0815944D+03	1.298051	1.5480684D-03
5.1050500D+03	1.298308	1.7170785D-03
5.1286138D+03	1.298472	1.8483752D-03
5.1522864D+03	1.298590	1.9089306D-03
5.1760683D+03	1.298681	1.9221627D-03
5.2119471D+03	1.298793	1.8272171D-03
5.2360044D+03	1.298791	1.6779930D-03
5.2601727D+03	1.298998	1.1608875D-03
5.2966344D+03	1.299545	9.2212574D-04
5.3210826D+03	1.299860	7.2242064D-04
5.3456436D+03	1.300214	5.2094292D-04
5.3703180D+03	1.300633	3.2047204D-04
5.4075432D+03	1.301291	1.8611876D-04
5.4325033D+03	1.301709	1.5516371D-04
5.4701596D+03	1.302269	1.4183720D-04
5.4954087D+03	1.302616	1.3797174D-04
5.5207744D+03	1.302947	1.3711663D-04
5.5590426D+03	1.303418	1.3592212D-04
5.58470190+03	1.303718	1.3304242D-04
5.6234133D+03	1.304155	1.2186813D-04
5.6493697D+03	1.304442	1.1201860D-04
5.6754461D+03	1.304727	1.0512116D-04
5.7147864D+03	1.305142	9.9997730D-C5
5.7411646D+03	1.305413	9.5102108D-05
5.7809605D+03	1.305809	8.9000028D-05
5.8076442D+03	1.306070	8.4098867D-05

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
5.8479008D+03	1.306453	8.0498937D-05
5.8884366D+03	1.306829	7.7426592D-05
5.9156163D+03	1.307073	7.6013397D-05
5.9566214D+03	1.307435	7.4953194D-05
5.9841160D+03	1.307672	7.4044046D-05
6.0255959D+03	1.308021	7.3975881D-05
6.0673633D+03	1.308341	7.5908453D-05
6.0953690D+03	1.308548	7.9029665D-05
6.1376201D+03	1.308855	8.0963662D-05
6.1659500D+03	1.309055	8.3097918D-05 _
6.2086903D+03	1.309352	8.8042049D-05
6.2517269D+03	1.309642	9.3473853D-05
6.2950618D+03	1.309928	9.9400860D-05
6.3241185D+03	1.310114	1.0707551D-04
6.3679552D+03	1.310387	1.1402239D-04
6.4120958D+03	1.310659	1.2396245D-04
6.4565423D+03	1.310923	1.3483112D-04
6.4863443D+03	1.311097	1.4414187D-04
6.5313055D+03	1.311352	1.6024709D-04
6.5765784D+03	1.311604	1.7409654D-04
6.6221650D+03	1.311852	1.9578984D-04
6.6680677D+03	1.312093	2.2479681D-04
6.7142885D+03	1.312318	2.6594397D-04
6.7608298D+03	1.312525	3.0184928D-04
6.8076936D+03	1.312715	3.3868046D-04
6.8548823D+03	1.312888	3.6040445D-04
6.9023980D+03	1.313055	3.6373923D-04
6.9502432D+03	1.313220	3.6290265D-04
6.9984200D+03	1.313373	3.5382633D-04
7.0469307D+03	1.313518	3.1973497D-04
7.0957777D+03	1.313671	2.5397452D-04
7.1449633D+03	1.313871	1.5303478D-04
7.1944898D+03	1.314104	1.0599616D-04
7.2443596D+03	1.314329	7.8017161D-05
7.2945751D+03	1.314547	5.8035021D-05
7.3451387D+03	1.314760	4.5049517D-05
7.4131024D+03	- 1.315031	4.0465988D-05
7.4644876D+03	1.315228	2.84898490-05
7.5162289D+03	1.315425	2.25055770-05
7.5683290D+03	1.315618	1.9120099D-05
7.6383578D+03	1.315868	1.63904220-05
7.5913044D+03	1.316052	1.40020020-05
/./446180D+03	1.316233	1.22115320-05
7.8162780D+03	1.316470	1.1394365D-05

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TABLE 1-Continued

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Warve Number (cm <sup>-1</sup> )	n	k
7.8704579D+C3	1.316645	1.0904861D-05
7.9432823D+03	1.316873	1.0790713D-05
7.9983426D+03	1.317042	1.1002215D-05
8.0723503D+03	1.317263	1.1388857D-05
8.1283052D+03	1.317427	1.1602462D-05
8.2035154D+03	1.317641	1.1790172D-05
8.2603795D+03	1.317799	1.1905843D-05
8.3368118D+03	1.318008	1.1994997D-05
8.3945999D+03	1.318162	1.1812182D-05
8.4722741D+03	1.318366	1.1603263D-05
8.5506671D+03	1.318566	1.1195156D-05
8.6297855D+03	1.318763	1.0688829D-05
8.6896043D+03	1.318909	9.3064735D-06
8.7700082D+03	1.319103	5.9510026D-06
8.8511561D+03	1.319296	3.8689235D-06
8.9330548D+03	1.319488	2.6283920D-06
9.0157114D+03	1.319678	2.0384034D-06
9.0991327D+03	1.319865	1.7084023D-06
9.1833260D+03	1.320051	1.4986152D-06
9.2682982D+03	1.320233	1.3285874D-06
9.3540567D+03	1.320416	1.25889680-06
9.4406088D+03	1.320596	1.2989431D-06
9.5279616D+03	1.320775	1.4193521D-06
9.6161228D+03	1.320952	1.6900134D-06
9.7050997D+03	1.321128	2.0007376D-06
9.7948999D+03	1.321303	2.3522861D-06
9.9083194D+03	1.321521	2.6877579D-06
1.000000D+04	1.321695	2.9997851D-06
1.0046158D+04	1.321780	3.1310510D-06
1.0092529D+04	1.321866	3.2530455D-06
1.0162487D+04	1.321994	3.3364924D-06
1.0209395D+04	1.322080	3.4181423D-06
1.0256519D+04	1.322165	3.4800873D-06
1.0303861D+04	1.322249	3.5017904D-06
1.0351422D+04	1.322333	3.46409780-06
1.0423174D+04	1.322462	3.3580731D-06
1.04/12850+04	1.322546	3.1899960D-06
1.05005770+04 1.00130130404	1.322630	2.93217670-06
1.037233/0404	1.322757	2.33/34980-06
I. UQ4I4JUJTU4 1. 04045407+04	1.322842	2.10715280-06
1 . UQ 7UJ4 7U7U4 1 . A7444 898444	1.322920	1.//088410-06
1.040360704 1.04147405404	1.363434	1.30032/80-00
1 N266956774	1 122220	1.UJ7/1/0U-UD # 3040574D-07
1.00963300704	1.323222	0.JU4UJJDD-U/

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TABLE 1-Continued

Wave Number (cm <sup>-1</sup> )	n	k
		<u></u>
1.0939564D+04	1.323351	6.6956099D-07
1.0990058D+04	1.323434	5.698883D-07
1.1040786D+04	1.323520	<b>5.1497974D-07</b>
1.1117317D+04	1.323648	4.8617222D-07
1.1168632D+04	1.323732	4.6215765D-07
1.1246050D+04	1.323859	4.4034203D-07
1.1297959D+04	1.323946	4.2343831D-07
1.1376273D+04	1.324074	4.0531264D-07
1.1428783D+04	1.324159	3.9065208D-07
1.1481536D+04	1.324244	3.74791850-07
1.1561122D+04	1.324373	3.5464198D-07
1.1641260D+04	1.324502	3.3480362D-07
1.1694994D+04	1.324590	3.1534805D-07
1.1776060D+04	1.324718	2.92947730-07
1.1830416D+04	1.32480.5	2.6902345D-07
1.1912420D+04	1.324937	2.4591790D-07
1.1967405D+04	1.325025	2.2427979D-07
1.2050359D+04	1.325157	2.0407516D-07
1.2133889D+04	1.325290	1.8185218D-07
1.2139896D+04	1.325379	1.6210266D-07
1.22/43920+04	1.325512	1.4480/20D-07
1.23594/40+04	1.325648	1.329811/D-07
1.24165230+04	1.325/39	1.26996030-07
1.23023700704	1.3238/4	1.24965300-07
1.23072340704	1.320012	1.23831/20-07
3 27350310+04	1.320104	1.201/1110-0/ 1.33002950-07
	1 320677	1.33702739-07
1,29121930+04	1 326826	1.47839380-07
1.3001696D+04	1.326667	1 52682810-07
1,30617090+04	1.326764	1.56960420-07
1.3152248D+04	1.326989	1.5804841D-07
1.3243415D+04	1.327055	1.5804841D-07
1.3335214D+04	1.327201	1.55879910-07
1.3427650D+04	1.327350	1.5303478D-07
1.3520726D+04	1.327502	1.4581095D-07
1.3614447D+04	1.327652	1.3483112D-07
1.3708818D+04	1.327808	1.1502444D-07
1.3803843D+04	1.327963	9.1357164D-08
1.3899526D+04	1.328120	7.2910511D-08
1.3995873D+04	1.328279	5.9950132D-08
1.4092888D+04	1.328440	4.9979297D-08
1.4190575D+04	1.328603	4.1000594D-08
1.4288940D+04	1.328769	3.3480362D-08

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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
1.4387986D+04	1.328938	2.9633991D-08
1.4487719D+04	1.329106	2.6533231D-08
1.4588143D+04	1.329278	2.4705301D-08
1.4689263D+04	1.329452	2.3003300D-08
1.4825131D+04	1.329690	2.1766577D-08
1.4927944D+04	1.329869	2.0979259D-08
1.5031420D+04	1.330052	2.0313752D-08
1.5135612D+04	1.330238	1.9399482D-08
1.5275661D+04	1.330490	1.7774203D-08
1.5381546D+04	1.330683	1.6741337D-08
1.5488166D+04	1.330877	1.6061649D-08
1.5631476D+04	1.331144	1.5696042D-08
1.5739829D+04	1.331345	1.5516371D-08
1.5885467D+04	1.331619	1.5024158D-08
1.5995580D+04	1.331826	1.4716012D-08
1.6143586D+04	1.332106	1.3989112D-08
1.6255488D+04	1.332317	1.3298117D-08
1.6405898D+04	1.332598	1.2381981D-08
1.6519618D+04	1.332813	1.1318533D-08
1.6672472D+04	1.333100	9.6336340D-09
1.6788040D+04	1.333316	7.7230731D-09
1.6943378D+04	1.333609	6.3648789D-09
1.7100153D+04	1.333902	5.2214382D-09
1.72583790+04	1.334200	4.4339434D-09
1.7378038D+04	1.334425	3.8440599D-09
1.7538805D+04	1.334729	3.4339198D-09
1.7701090D+04	1.335035	3.1317720D-09
1./864876D+04	1.335344	2.8693937D-09
1.80301//D+04	1.335656	2.65943970-09
1.819/0090+04	1.3359/2	2.44225010-09
1.83653830+04	1.336292	2.26876830-09
1.83333160+04	1.336615	2.09792590-09
1.0/000210+04	1.336943	1.88/0/930-09
1.00544070+04	1.33/2/3	1./5/0/440-09
	1.33/50/	1.539/9/20-09
	1.33/744	1.30900420-09
1.05224475404	1.330200	1.4014/000-09
1 9818270D404	1.JJ00JJ 1 116/71	1.20/03730-07 1.078495555-00
1.9998419D±04	1.3370/3	1.0/072330-07 9 2426144R-10
2.01836647404	1.337730 1 330701	7.8485690D-10 7.8685690D-10
2.04173793404	1 360968	7 3415012D-10 7 3415012D-10
2.06062990+04	1 340620	7 1579766D-10
2.08449090+04	1.341093	7 89236975-10
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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
2.1037784D+04	1.341475	7.0111643D-10
2.1281390D+04	1.341961	7.2910511D-10
2.1527817D+04	1.342455	7.4953194D-10
2.1727012D+04	1.342858	7.5995897D-10
2.1978599D+04	1.343368	7.7945338D-10
2.2233099D+04	1.343889	8.0870503D-10
2.2490546D+04	1.344418	8.6854064D-10
2.2750974D+04	1.344956	9.3926933D-10
2.3014418D+04	1.345505	1.0180993D-09
2.3280913D+04	1.346066	1.0884040D-09
2.3550493D+04	1.346636	1.1689344D-09
2.3823195D+04	1.347219	1.2583172D-09
2.4099054D+04	1.347811	1.3390295D-09
2.4378108D+04	1.348417	1.4216417D-09
2.4717241D+04	1.349159	1.4886416D-09
2.5003454D+04	1.349793	1.5804841D-09
2.5292980D+04	1.350438	1.6626091D-09
2.5644840D+04	1.351231	1.7611248D-09
2.6001596D+04	1.352046	1.8398827D-09
2.6302680D+04	1.352740	1.9399482D-09
2.6668587D+04	1.353594	2.0313752D-09
2.7039584D+04	1.354470	2.1173378D-09
2.7415742D+04	1.355370	2.2171248D-09
2.7797133D+04	1.356295	2.3162751D-09
2.8183829D+04	1.357247	2.4198595D-09
2.8575905D+04	1.358224	2.5280761D-09
2.8973436D+04	1.359231	2.6533231D-09
2.9444216D+04	1.360441	2.7656049D-09
2.9853826D+04	1.361513	2.8826382D-09
3.0269134D+04	1.362616	2.9839404D-09
3.0760968D+04	1.363990	3.0816985D-09
3.1260794D+04	1.365376	3.1899960D-09
3.1768741D+04	1.366812	3.3249885D-09
<b>3.2284941D+04</b>	1.368287	3.5464198D-09
3.2809529D+04	1.369839	3.8263980D-09
3.3342641D+04	1.371437	4.1475358D-09
3.3884416D+04	1.373098	4.4034203D-09
3.4514374D+04	1.375086	4.7950169D-09
3.5075187D+04	1.376902	5.4049309D-09
3.5727284D+04	1.379072	5.7914878D-09
3.6391504D+04	1.381341	6.2920207D-09
3.7068072D+04	1.383726	6.8515707D-09
3.7757219D+04	1.386239	7.4437220D-09
3.8459178D+04	1.388881	7.9944786D-09

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TABLE 1-Continued

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Wave Number (cm <sup>-1</sup> )	n	k
3 9176188D±06	1 391474	\$ 60577810-09
3.9994475D+04	1 394993	9 30658060-09
4.0831939D+04	1.398535	9.90353280-09
4.1686938D+04	1.402321	1.0490354D-08
4.2559841D+04	1,406358	1.0710017D-08
4.34510220+04	1.410702	1,10100720-08
4.4463127D+64	1.415921	1.15821760-08
4.5498806D+04	1.421603	1.2699603D-08
4.6558609D+04	1.427828	1.99889570-08
4.7643099D+04	1.434685	3.84405990-08
4.8752849D+04	1.442296	6.7110449D-08
5.0003453D+04	1.451724	1.1010072D-07
5.1286138D+04	1.462543	1.8496525D-07
5.2601727D+04	1.475183	3.6223478D-07
5.4075432D+04	1.491881	1.2495112D-06
5.5590426D+04	1.513343	5.9950132D-05
5.7147864D+04	1.543062	8.3905445D-04
5.7411646D+04	1.549412	1.1824700D-03
5.8076442D+04	1.568183	2.0035037D-03
5.8884366D+04	1.605555	3.9975154D-03
5.9566214D+04	1.635062	3.9975154D-02
6.0255959D+04	1.647245	7.2408599D-02
6.0953690D+04	1.653100	1.0394178D-01
6.1659500D+04	1.652917	1.3514194D-01
6.2517269D+04	1.650184	1.6702833D-01
6.3241185D+04	1.641473	2.0220419D-01
6.4120958D+04	1.620422	2.3377074D-01
6.4863443D+04	1.596861	2.5810127D-01
6.5765784D+04	1.559942	2.7719803D-01
6.6680677D+04	1.521276	2.7719803D-01
6.7608298D+04	1.489551	2.6411322D-01
6.8548823D+04	1.469275	2.4087412D-01
6.9502432D+04	1.460977	2.1666569D-01
7.0469307D+04	1.461485	1.9265937D-01
7.1449633D+04	1.471129	1.6779930D-01
7.2443596D+04	1.496271	1.4216417D-01
7.3451387D+04	1.536403	1.3328772D-01
7.4644876D+04	1.586268	1.4886416D-01
7.5683290D+04	1.619420	1.8697784D-01
7.6913044D+04	1.633849	2.3921596D-01
7.8162780D+04	1.626822	2.8760C84D-01
7.9432823D+04	1.606068	3.2195127D-01
8.0723503D+04	1.584638	3.3868046D-01
8.2035154D+04	1.570304	3.4897165D-01

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TABLE 1-Continued

libus Number (m <sup>-1</sup> )	n	 F
		л 
8.3368118D+04	1.560870	3.5957554D-01
8.4722741D+04	1.553435	3.7050165D-01
8.6297855D+04	1.548070	3.8263980D-01
8.7700082D+04	1.543211	3.9883214D-01
8.9330548D+04	1.535363	4.1475358D-01
9.0991327D+04	1.528933	4.3031862D-01
9.2682982D+04	1.523589	4.4852860D-01
9.4406088D+04	1.516305	4.7074980D-01
9.6161228D+04	1.506677	4.9293555D-01
9.7948999D+04	1.493473	5.1854941D-01
1.000000D+05	1.476628	5.4298789D-01
1.0209395D+05	1.455868	5.7516194D-01
1.0423174D+05	1.425425	6.0504844D-01
1.0641430D+05	1.387639	6.2920207D-01
1.0864256D+05	1.346760	6.4385807D-01
1.1117317D+05	1.302663	6.5281503D-01
1.1376273D+05	1.259495	6.5734013D-01
1.1641260D+05	1.214969	6.5734013D-01
1.19124200+05	1.173382	6.4534232D-01
1.2189896D+05	1.140628	6.2920207D-01
1.2502590D+05	1.111682	6.1346550D-01
1.2823306D+05	1.087685	5.9812250D-01
1.3152248D+05	1.068724	5.8585500D-01
1.3520726D+05	1.049744	5.8048385D-01
1.3899526D+05	1.020921	5.8585500D-01
1.4288940D+05	0.981692	5.7914878D-01
1.4689263D+05	0.941801	5.6336536D-01
1.5135612D+05	0.903527	5.3553782 <u>D</u> -01
1.5631476D+05	0.866994	5.0325737D-01
1.6143586D+05	0.840575	4.5581661D-01
1.6672472D+05	0.830901	4.1189844D-01
1.7258379D+05	0.831628	3.7392986D-01
1.7864876D+05	0.835295	3.4977611D-01
1.8535316D+05	0.835240	3.3097115D-01
1.9230917D+05	0.830957	3.1534805D-01
1.9998619D+05	0.820742	2.9977136D-01
2.0844909D+05	0.805579	2.7656049D-01
2.1727012D+05	0.797007	2.4142939D-01
2.2750974D+05	0.797737	2.0882868D-01
2.3823195D+05	0.802291	1.7980019D-01
2.5003454D+05	0.809997	1.5338756D-01
2.6302680D+05	0.819753	1.3025372D-01
2.77971330+05	0.830720	1.0934279D-01
2.9444216D+05	0.842171	9.07381970-02

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TABLE	1-Conti	nued
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Wave Number (cm <sup>-1</sup> )	n	k
3.1260794D+05	0.854141	7.4608815D-02
3.3342641D+05	0.866493	6.0644322D-02
3.5727284D+05	0.873766	4.8505406D-02
3.8459178D+05	0.890837	3.8175976D-02
4.1686938D+05	0.902694	2.9497835D-02
4.5498806D+05	0.913973	2.2273586D-02
5.0003453D+05	0.924583	1.6360258D-02
5.5590426D+05	0.934744	1.1635636D-02
6.2517269D+05	0.944124	7.9577473D-03
7.1449633D+05	0.952792	5.1735678D-03
7.6913044D+05	0.956954	4.0718347D-03
8.3368118D+05	0.960953	3.1462276D-03
9.0991327D+05	0.964778	2.3702281D-03
1.000000D+06	0.968416	1.7449788D-03

\* The data in the first and third columns are in Fortran, double precision, exponential notation. For example, 5.0D-04 means  $5.0\times10^{-4}$ .



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153 1.00000 WAVE NUMBER (1/CM) (X 10<sup>+03</sup>) 0.20000 2.800 2.600 2.408 2.200 2.000 1.869 | 8.8 3.000 1.800 1.600 1.400 1.200

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Fig. 26. The final spectrum of n(v) from 0 to  $10^3$  cm<sup>-1</sup>.

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The final spectrum of n(v) from 0 to 1 cm<sup>-1</sup>. Fig. 29.

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## CHAPTER VI

## CONCLUSION

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The process of obtaining the complex refractive index of water began with the acquisition of an absorption spectrum that spanned approximately 14 decades, from  $10^{-6}$  to  $10^8$  cm<sup>-1</sup>. This spectrum comprised smoothly joined data from various sources, and was adjusted within experimental error until an electronic sum rule yielded proper results. This spectrum was appropriately Fourier transformed to give the real part of the complex refractive index. Calculations over several regions were joined to create a smooth spectrum over the range  $10^{-3}$  to  $10^6$  cm<sup>-1</sup>. The result was a complete and self-consistent spectrum of both real and imaginary parts of the complex refractive index over 9 decades.

To address the question of error in the calculation of  $n(\nu)$ , the literature was again consulted to find sufficient data for comparison. The following four spectral locations were chosen:  $10 \text{ cm}^{-1}$ ,  $5 \times 10^2 \text{ cm}^{-1}$ ,  $2 \times 10^3 \text{ cm}^{-1}$ , and  $1 \times 10^4 \text{ cm}^{-1}$ . The procedure was to average the data, then find the percent difference between the mean and the results obtained in this research.

At 10 cm<sup>-1</sup>, the data of Downing and Williams, Afsar and Hasted, and Zolotarev <u>et al.</u><sup>28</sup> yielded a mean value of 2.588.

The value obtained in this research was 2.399, a difference of 7.6 percent. In the paper by Downing and Williams, 10 cm<sup>-1</sup> was the lowest frequency point of their calculations. Their paper stated that the data become "coarse at the lowest frequencies."<sup>29</sup> Further, they obtained optical constants for their calculations from Rav.<sup>30</sup> whose data were presented graphically and not in tabular form, thereby allowing for considerable inaccuracy. The work by Afsar and Hasted used a Fourier transform spectrophotometer. As a result, their calculations for the low endpoint of the range, which is near 10 cm<sup>-1</sup>, are subject to the same problems as are outlined in Chapter IV above. The data of Zolotarev et al. are a result of Kramers-Kronig calculations, equivalent to the Fourier transform method. The data used are sparse in the region of 10 cm<sup>-1</sup>, thus raising the objection that resolution in that range was not good. Considering all the above factors, one might well conclude that the results of the present study are more accurate at 10 cm<sup>-1</sup> than the values used for comparison.

At  $5\times10^2$  cm<sup>-1</sup>, values by Hale and Querry, Downing and Williams, Pontier and Dechambenoy, <sup>31</sup> Rusk <u>et al.</u>, <sup>32</sup> and Zolotarev <u>et al.</u> gave a mean of 1.473. The present work gives 1.468, a difference of 0.4 percent. The same authors reported data at  $2\times10^3$  cm<sup>-1</sup> which gave a mean of 1.323. The present work gives 1.306, a difference of 1.3 percent. At  $1\times10^4$  cm<sup>-1</sup>, data of Hale and Querry, Pontier and Dechambency, and Zolotarev <u>et al.</u> gave a mean of 1.325. The present study gives 1.322, a 0.2 percent difference. These values are much closer

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to those of the comparison works than at lower wave number regions. To the extent that they differ, it is believed that the use of such a broad ranged and self-consistent absorption spectrum as is illustrated in Figure 3 gives more reliable results. Considering the uncertainty, however, it is probably reasonable to say that the values of  $n(\nu)$ are accurate only to three significant figures.

One might hope that the future will bring more efficient algorithms for the computation of a spectrum over a broad range. The ideal would be a single calculation over a very large range with very fine divisions among the data. This would give a spectrum accurate near the endpoints and high in resolution, one which is entirely self-consistent. Hopefully, the present work is a small step in that direction.

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## VI. <u>References</u>

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