Report No. CG-D-16-83

SUMMARY OF THE FALL 1981 SPRINGING RESPONSE TRIALS AND HULL GIRDER CALIBRATION OF THE M/V STEWART J. CORT



This document is available to the U.S. public through the National Technical Information Service, Springfield, Virginia 22161

SUMMARY REPORT

JULY 1982

Prepared for:

JUN 1 6 1983

83 06 16

and the second second and the second

038

U.S. Department of Transportation United States Coast Guard

Office of Research and Development Washington, D.C. 20593

NOTICE

This document is disseminated under the sponsorship of the Department of Transportation in the interest of information exchange. The United States Government assumes no liability for its contents or use thereof.

The contents of this report do not necessarily reflect the official view or policy of the Coast Guard; and they do not constitute a standard, specification, or regulation.

This report, or portions thereof may not be used for advertising or sales promotion purposes. Citation of trade names and manufacturers does not constitute endorsement or approval of such products.

Technical Report Documentation Page

L. Report No.	2. Gevernment Area	sion No.	3. Recipient's Catalos I	1e.
CG-D-16-83			1	· · · · · · · · · · · · · · · · · · ·
4. Title and Subtitle	A~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		5. Report Date	
SUMMARY OF THE FALL 1981 S	SPRINGING RESP	ONSE TRIALS	JULY 1982	
AND HULL GIRDER CALIBRATIC	ON OF THE M/V S	STEWART J. CORT	6. Performing Organizati	en Code
			8. Performing Organizati	en Report No.
7. Author's)				
DAVID P. KIHL				
9. Performing Organization Name and Addres	85		10. Work Unit No. (TRA	5)
STRUCTURES DEPARTME	INT		1/30-603	
SHIP STRUCTURES DIVISION,	DTNSRDC		MTPR-7-70099-	-8-85117-5B
BEIHESDA, MARILAND	20084		13. Type of Report and I	Period Covered
12. Sponsoring Agency Name and Address			SUMMARY REE	ORT
U. S. COAST GUARD (G-DMT-1	L)		FALL, 1981	
2100 SECOND STREET S.W.			14 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.40
WASHINGTON, D.C. 20593			14. Sponsoring Agency (,6d4
work was LTJG K.A. NUGENT. Continued full 1000 ft. Great Lakes ore of trials data base. The new agreement of results betwe analytical predictions. As part of the which came within 10% of the axis showed very good agree stresses. Limited funding for the hull girder calibr summary of the 1981 spring since the 1979 trials, the calibration. No trials da	scale wave and carrier, the M ad for a larger een the full so l981 trials en the expected re- mement with the prevented all cation which in ging response to data runs tal ita, except for	i stress measur /V STEWART J. C r data base was cale data compi ffort a hull gi esults. A chec e neutral axis l of the data f s presented. T trials with des ken, and a disc r the hull gird	ements were cond ORT: to increase decided based of led from the 197 rder calibration k of the calcula location of the rom being analyz his report is the criptions of the hu er calibration,.	lucted on a the 1979 on the limited '9 trials and a was performed ated neutral calibrated and except arefore a changes made and girder is present.
The U.S.C.G. Office of Mer Mr. P. COJEEN.	rchant Marine	Safety technics	l representative	2 W88
17. Key Words		18. Distribution State	ment	
WAVE INDUCED STRESS		the National 7	alladie to the j Cechnical Informa	ation Service
LONGITUDINAL STRENGTH		Springfield. N	/A 22161	
SPRINGING STRESSES				
STRESS COMBINATIONS				
19. Security Classif. (af this report)	20. Security Cles	sif. (of this page)	21. Ne. of Peges	22. Price
INCLASSIFIED	UNCLASSIF	TED	54	
E DOT E 1700 7 /#-72\				
Form DUI F 1700.7 (4=727	Keproduction of Co	mpieraa paga dumeriz		• . • .

and the second second and the second s

أواحد للناكر المدرو تعاوروا

4

TABLE OF CONTENTS

.

. .

ABSTRACT	1
ADMINISTRATIVE INFORMATION	1
INTRODUCTION	1
TEST OBJECTIVES	2
FALL 1981 FULL SCALE MEASUREMENTS	3
MEASUREMENTS AND INSTRUMENTATION	3
DATA COLLECTION	9
STATIC CALIBRATION	11
SUMMARY AND RECOMMENDATIONS	14
ACKNOWLEDGMENTS	16
R%PERENCES	17
APPENDIX A - STATIC CALIBRATION CALCULATIONS	19
APPENDIX B - TRANSDUCER CALIBRATIONS AND SENSITIVITIES	27
APPENDIX C - HEADER LOGS FOR M/V S. J. CORT DATA RUNS	39

The second second second second second second second second second

-



111

PRECEDING PLON MANK-NOT FILMED

1

Page

LIST OF FIGURES

Page

i	-	Transducer Locations on the Ship	5
2	-	Forward Section with Wave Measuring Devices and Instrumentation	6
3	-	Midship Strain Gage Locations	[′] 7
A1	-	Actual Bending Moment Diagrams With and Without Buoyancy Corrections For Deflection, Sinkage, and Trim	25
B1	-	Strain Bridge Circuits for Main Deck Bending	29
B 2	-	Strain Bridge Circuits for Lateral Bending	30
B 3	-	Strain Bridge Circuits for Bottom Bending	31
B4	-	Strain Bridge Circuits for Torsion	32
B 5	-	Phase Lag Characteristics of Main Deck Bending Filters	33
B 6	-	Rolloff Characteristics of Main Deck Bending Filters	34
87	~	Collins Rader Altimeter Celibration Procedure	36

LIST OF TABLES

1	- Measurements for 1981 M/V S. J. CORT Full Scale Trials	4
A1	- Sounding Depths of Tank Ballast Before and During Calibration	26
▲2	- Section Properties of the CORT Midship Section	26
B 1	- NRL Installed Transducer Sensitivities	37
Cl	- CORT Drafts For Losd/Ballast Conditions	40

ABSTEACT

Continued full scale wave and stress measurements were conducted on a 1000 ft Great Lakes ore carrier to increase the 1979 trials data base. The need for a larger data base was decided based on the limited agreement between the full scale results from the 1979 trials and analytical predictions.

Also as part of the 1981 trials effort a hull girder calibration was performed which came within 10% of the expected results. A check of the calculated neutral axis showed very good agreement with the neutral axis location of the calibrated stresses. Limited funding prevented all of the data from being analyzed, except for the hull girder calibration which is presented. This report is therefore a summary of the 1981 springing response trials with descriptions of the changes made since the 1979 trials, the data runs taken, and a discussion of the hull girder calibration. No trials data, except for the hull girder calibration, is presented.

ADMINISTRATIVE INFORMATION

The work described herein was performed by the Ship Structures Division at the David Taylor Naval Ship R&D Center (DTNSRDC) under funds provided by the U.S. Cosst Guard MIPR-2-70099-8-85117 under work unit 1730-603.

INTRODUCTION

This report is an account of the 1981 effort into the continued investigation of springing responses on the Great Lakes ore carrier M/V STEWART J. CORT. In the fall 1979, full scale trials were conducted on the CORT from which response amplitude operators (RAO's) were developed between midship stress and wave height measurements.¹⁴ These RAO's were compared with theoretical RAO's computed by the American Bureau of Shipping (ABS) and Webb Institute of Naval Architecture. These initial comparisons did not completely agree in some cases, indicating the need to more fully understand the structural response of Great Lakes ore carriers. The 1981 trials were intended to continue the measurement of midship stresses and wave height, and generate a larger data base of RAO's for comparison with the analytical predictions.

References are listed on page 17 .

The overall objective of the research effort is to accurately predict springing and wave induced responses of ore carriers so that the longitudinal strength standards can be validated, to insure adequate longitudinal strength for longer (than 750 ft) ore carriers.

TEST OBJECTIVES

The original test objectives of the fall 1981 trisks season of simultaneous wave and stress measurements were to:

1. Continue simultaneous full scale measurements of wave and stress during the 1981 fall shipping season.

2. Continue the data analysis and develop RAO's using the midship deck stress and the collins radar altimeter.

3. To complete the springing research on the CORT and to arrive at some specific conclusions concerning wave induced and springing stress combination.

As part of the approach to arrive at the above objectives, a static vertical calibration of the ships hull girder was to be performed at some time during the trials season. The results of this calibration were to be used to obtain a relationship between applied bending moment and stresses in the deck and keel, and to offer a check of the actual neutral axis against the calculated neutral axis and section moduli.

The rest objectives were revised when funds remaining to complete the project became unavailable. As per sponsor request, simultaneous full scale measurements of wave and stress during the 1981 fall season were to continue and the static calibration of the hull girder would be performed, in lieu of generating RAO's between the midship stresses and measured wave height. The idea being that the data, once collected, could be analyzed at a later date when funds became svailable. The static hull girder calibration data was analyzed and the results are presented

in Appendix A of this report. Also included in the report is a summary of the trials preparation, full scale trials and the hull girder calibration. Information on the calibration of all tranducers used in these trials is given in Appendix B and a list of the header logs for each of the runs taken is presented in Appendix C. These header logs contain the ship conditions (speed, heading, location and draft) and the wind and wave conditions existing at the start of each run.

FALL 1981 FULL SCALE MEASUREMENTS

MEASUREMENTS AND INSTRUMENTATION

The 1981 fall trials were a continuation of the 1979 trials effort; the primary measurements being midship vertical bending stresses and wave height, both of which are used to calculate the RAO'S. The same two wave height measuring systems used in the 1979 trials were used again during the 1981 trials. Both were configured and installed by the Naval Research Laboratory. The first, a Collins Radar Altimeter was mounted on a born which extended about 4.5 meters off the shipe bow. The second, a microwave radar unit was mounted on the port side on top of the pilot house.

As will be described later, the NRL microwave radar unit developed problems early in the trials and stopped functioning altogether, exhibiting continuous loss of signal. All wave height data is therefore based on the collins radar altimeter measurements.

A total list of transducer measurements is given in Table 1, and shown in Figures 1 through 3. The list includes midship stresses (main deck bottom and lateral bending and torsion), wave height, and corresponding vertical and horizontal accelerations of the wave height measuring units.

The major changes between the 1979 trials and 1981 trials, besides the static hull girder calibration are that, in 1981;

TABLE 1 - MEASUREMENTS FOR M/V S.J. CORT FULL SCALE TRIALS

1. HICRO-WAVE RADAR*

2. COLLINS RADAR*

1 - P - P - P

3. BOW VERTICAL ACCELERATION (AT COLLINS)*

4. BOW HORIZONTAL ACCELERATION (AT COLLINS)*

5. BOW VERTICAL ACCELERATION (AT HICRO-WAVE)*

6. BOW HORIZONTAL ACCELERATION (AT MICRO-WAVE)*

7. HIDSHIP DECK VERTICAL BENDING STRESS (COMBINED) .

8. MIDSHIP DECK VERTICAL BENDING STRESS (WAVE INDUCED)

9. MIDSHIP DECK VERTICAL BENDING STRESS (SPRINGING)

10. HIDSHIP BOTTCH VERTICAL BENDING STRESS (COMBINED)

11. MIDSHIP LATERAL BENDING STRESS

12. MIDSHIP TORSIONAL STRESS

NRL INSTALLED MEASUREMENTS



بل خقيدهم المعار أرغه



LOCATIONS FOR COMPUTER, SIGNAL CONDITIONING, AND WAVE MEASURING SYSTEMS

1

Figure 2 - Forward Section with Wave Measuring Devices and Instrumentation

- --- -

و مدر المرو معلو معلو المرود المواد المواد الم





STATE OF A LEAST STATE AND A LEAST STATE

2

Service and the service of the

فميانيون السارية المرا

1. Full scale pressure measurements in the bow ware not recorded. The pressure transducers were removed and replaced with plugs early in 1981 while the CORT was laid up for the winter.

2. Midship motions (pitch, roll, and heave) were not measured and,

3. Buoy wave height measurements were omitted, since the collins radar altimeter and the microwave radar units were validated (using the 1979 trials buoy data and buoy data obtained again in 1980 by the Coast Guard see Reference 2) using helicopter deployed buoys.

A shakedown trial was conducted on the CORT during the summer of 1981 to reestablish the entire data collection and analysis system in preparation for the fall trials.

Problems with the keel strain gages (which had begun to drift toward the end of the 1979 trials season), and one of the main deck dyadic gages (which failed during the 1980 Coast Guard wave height correlation tests) dictated a partial reinstrumentation of the CORT prior to any data collection.

All main deck and keel strain gages located at midships were replaced, and duplicate gages were placed in the same vicinity and orientation as backups.

The main deck gages and spares were placed in a dyadic configuration approximately on foot forward of the gages used in the fall 1979 trials. The bottom bending gages and spares were placed on the top of the stiffener on the bottom plating, because of water lying on the plating surface. The bottom bending gages are in the same location as those used in the 1979 trials to eliminate local bending (i.e. 0.211 x transverse frame spacing).

The midship torsion and lateral bending strain gages, although not replaced, showed desired high resistance to ground and proper resistance through the gages themselves. The lateral bending gages are also laid out in a dyadic configuration.

All strain bridges, accelerometers, and wave height radar units were calibrated and functioning properly at the beginning of the 1981 trials (Appendix B gives details of transducer calibrations). The NRL microwave radar unit, when turned on, displayed the usual peaked oscilloscope display; although not specifically calibrated a board, it is assumed working properly when the peaked oscilloscope display is seen. Occasional signal drop-out occurred as the NRL microwave radar unit was tracking approximately 2 foot waves.

The PDP 11/03 computer, which was used to control the collection and storage of the digitized data on magnetic tape, was loaded on board at the end of the shakedown trials. At this time the computer was not fully operational in that it was unable to collect, new data but was able to reduce and analyze previously collected data. An attempt was made to identify and correct the computer problem before the fall trials began but the results did not confirm the computer would be operational by the start of the trials. As a precautionary measure, an analog tape recorder was brought on board and added to the instrumentation package at the start of the fall trials as backup to the digital tape system. The problems affecting the computer were identified and corrected during the first few days of the dedicated trials.

DATA COLLECTION

田田 一般ないかちのかち ちょうちょう ちゅうちょう ひろう ひんちょうちょう ちょうちょう ちょうちょう

Over fifty data runs of 25 minute duration each were collected on board the CORT. The data collected consisted of roughly an even mixture of head and oblique sea headings. Most of the rougher weather was encountered in oblique sea conditions. On the last day of trials, however, when rough following seas prevented the ship from entering Burns Harbor, the Captain turned the ship around and headed back up Lake Michigan, allowing a series of head and bow sea runs to be recorded. Although the ship was traveling at a reduced speed, the waves were probably the highest and longest of any data runs collected during the 1979 and 1981 trials.

Host runs (Runs 1-40) were recorded on oscillograph traces to check for data consistency as well as being recorded on analog and digital tape. The remaining runs (41-57) were only recorded on digital tape and oscillograph traces.

The NRL microwave radar unit coased functioning at the beginning of the trials and exhibited the same signal loss and dropout characteristics as it did during the 1979 trials. Daily attempts to bring the unit up and working failed, and subsequently no wave height data from the NRL microwave unit were collected. The horizontal accelerometer mounted on the NRL microwave unit began functioning unreliably after run #9.

The runs recorded on digital tape were digitized at 5 samples per second, (10 samples per second was used in 1979 to be compatable with the NRL microwave digital output signal, and then the data would be analyzed using every other data point to establish an effective digitizing rate of 5 samples per second).

Since the NRL microwave radar unit was not functioning properly, the digitizing rate was set at 5 samples per second, and every date point would be used in the data analysis, thus reducing the number of date points being handled and the amount of computer time required for data analysis. A sample rate of 5 samples per second still adequately defines the frequencies of interest for this vessel.

The Collins radar unit exhibited some drop out (loss of return radar signal), but these occurred very infrequently. The signal drop out is none-the-less compensated for in the software (if less than 2 seconds in duration) by linearly connecting the last data point before the dropout with the next data point after the dropout, and interpolating the missing data points before proceeding with the analysis. If the drop out is more than 2 seconds in duration the software prints a statement to that effect and stops the analysis.

A description of the data format used to store the data on the digital magnetic tape can be found in Appendix B of Reference 1.

a contract second second

STATIC CALIBRATION

As part of the fall 1981 full scale trials effort, a longitudinal hull girder bending moment calibration of the CORT was performed. During the 1981 season only one calibration was performed due to ship schedule. More than one would have been attempted had the opportunity to do so become available. The purpose of this calibration was to establish a relationship between a statically applied bending moment and the response of the main deck and bottom bending strain gages. In this way, induced bending moments can be derived from strains measured during the fall 1981 shipping season. The results of this calibration were also used as a check against the calculated neutral axis and section moduli.

The calibration was performed by selectively changing ballast in the seven middle ballast tanks as outlined in Reference 3. With minimal interference to the ships schedule, the calibration was performed dockside at Burns Harbor with the ship initially in the code 1 ballast condition ready for departure.

The whole calibration took approximately 3 hours, starting at 1730 hours with the initial code 1 ballast condition, to the specified calibration ballast condition and then back again to the code 1 ballast condition.

Through the two step calibration, the main deck, bottom bending and torsional strain bridges were monitored, in addition to the draft meters (forward, amidships, and aft), temperature (deck, air, and water) and athwartship trim lights located on the engine room deckhouse. The torsion bridge output and the trim lights indicated the second step was not fully complete as the ship was preparing for departure, and was therefore not used in the calculations.

The weather conditions during the calibration were overcast during the day with drizzling rain beginning in the late afternoon and continuing through the night. The main deck and keel (water) temperatures $(38^{\circ} \text{ and } 44^{\circ} \text{ Fahrenheit respectively})$ remained constant during the calibration, with the air temperature fluctuating only one degree Fahrenheit $(37^{\circ} \text{ to } 36^{\circ})$. Since the main deck and water temperatures remained constant during the calibration, any effect of diurnal stresses on the calibration was assumed to be negligible.

The ballast level in each ballast tank was checked by looking down the scuttle hatch at the top of the tank and counting down the number of ladder rungs to the ballast surface. The rungs are spaced one foot spart, the first rung being one foot off the bottom of the tank, and the top rung being twenty seven feet off the bottom.

When the ballast in each of the tanks was at the specified level, the lines holding the ship to the dock were elecked so that the friction between the ship and dock would not interfere with the calibration. Voltage outputs from the main deck bending, bottom bending and torsion bridges were then monitored at the signal conditioning in the forward machinery room, the terminal strip on the back of the computer, and were recorded on digital tape. All three voltage readings were consistent, at each step of the calibration. Shunt calibrations of the strain gage circuits were also performed at each of the calibration steps to insure the signal conditioning, amplifiers, etc. were working properly.

The ship was not intended to trim or change draft, but the change in draft readings indicated by the ships draft gages, showed that it did set slightly deeper in the water and trimmed slightly by the bow, comparing the change from the initial code 1 ballast condition to the calibration ballast condition. Drafts were initially 12'6" FWD, 16'3" AMID, 20'6" AFT and changed to 12'7 1/2" FWD, 16'8 1/2" AMID and 20'3" aft at the calibration ballast condition. Some change in draft readings is

attributable_to bending of the hull due to the induced loading, as will be discussed later, as well as the combined effects of the free water surface of the ballast and the accuracy to which the ballast can be loaded to the nominal specified depth. The remaining changes are felt to be errors in the draft gage readings themselves, as will be discussed later in Appendix A. The effects of these changes were taken into account in the calculations and plots given in Appendix A.

The bending moment, based on the nominal change in ballast, draft and trim was found to be bounded between 235,100 and 198,000 Ft-Ltons (SAG) at the gage locations.

Based on the voltage outputs from the main deck and keel bending strain bridges, the gages read stresses of 5.125 ksi compression in the deck plating and 4.437 ksi tension on top of the bottom plating stiffener, corresponding to an average bending moment of 217,836 Ft-Ltons (SAG).

Comparing the average bending moment obtained from the strain gage outputs with the actual applied bending moment limits based on the nominal ballast changes and corrected for any draft and trim charges, the actual comes within 10% of that seen by the main deck and bottom bending strain gages.

The neutral axis location was calculated to be 23.01 ft above the baseline, and based on the recorded stresses during the calibration, was found to be located 23.10 feet above the baseline; a very good comparison.

It should be kept in mind that the above calculations relating stress at a point on the cross section of the ship with the banding moment acting on that cross section assumed a uniform stress distribution along the width of the ship, with little or no lateral restraint.

The effects of a non-uniform stress distribution (shear lag effect) would produce slightly higher than nominal stresses near the edges of the ship (where the strain gages are located) and near the edges of the cargo hatches due to the

longitudinal bulkheads, with slightly lower than nominal stresses occurring at the mid points. The material between the hatches is assumed to be ineffective in carrying load. The actual shape and magnitude of the stress distribution across the width of the ship with respect to the nominal stress is not known, but could be determined from a simple finite element model.

The effects of mill tolerances, which on the average produces plating and scantlings slightly above the nominal dimensions, can alightly reduce measured responses below the nominal calculated values.

Some error was undoubtably introduced in ballasting the tanks to the nominal specified levels, due not only to the difficulty of sighting the water level down inside the tanks, but also the effect of the size of the tanks (large surface area) has on the ballast weight based on the depth readings.

Another factor to be considered in the comparison would be electronic drift of the instrumentation when readings are taken with respect to the same initial reference over a long period of time.

SUMMARY AND RECOMMENDATIONS

Dedicated fall trials have been completed for the 1981 shipping season. Over fifty data runs of 25 minute duration each were collected on board the CORT. The data collected contains roughly an even mixture of head, bow and oblique sea headings. Most of the rougher weather was encountered in oblique seas, except for a series of used and bow sea runs obtained on the last leg of trials in very rough seas. Most of the data remains to be analyzed due a change in project objectives and available funding.

As part of the fall 1981 trials effort, a longitudinal hull girder banding moment calibration of the CORT was performed by recording hull strains while making

known changes in the ship's ballast condition. The actual bending moment, after being corrected for changes in the buoyancy distribution caused by the deflected shape and slight draft and trim changes, agreed to within 10% of the average seen by the main deck and bottom bending strain gages.

The correction due to the buoyancy distribution was found to be between 15.5% and 28.8% of the uncorrected bending moment distribution. The measured stresses show this correction to be 21.7%.

Possible explanations for the 10% disagreement include the effect of shear lag in the plating, which sheds load from the unsupported sections of the plate to the edges which are supported by longitudinal bulkheads, effectively increasing the etresses in those areas; mill tolerances of plating and scantlings which can be slightly above nominal; error introduced from the draft gage readings; error introduced in ballasting the tanks to specified levels due to the large size of the tanks and the difficulties in sighting the depth from the scuttle hatch at the top of the tank; and errors inherent in any electronic signal conditioning when teadings are taken with respect to the same initial reference over a long period of time.

A comparison of the calculated neutral axis location, 23.01 feet above the base line and the neutral axis location determined experimentally during the hull girder calibration, 23.10 feet above the base line shows very good agreement.

To establish some definite conclusions about springing and wave induced stresses, (their combination to produce a maximum, consistency of the theoretical and measured RAO's, assymetry of the measured main deck and bottom banding time history data^{4,5}), a concerted effort is recommended to reduce and analyze the remaining data collected during the 1981 trials, and along with the data collected during the 1979 trials, be compared and collectively analyzed.

Included in this effort, in addition to developing RAO's, histograms of the vertical bending channels (main deck combined, wave induced, springing, and bottom bending) should be analyzed to determine their actual distribution, which is important when maximum expected values are determined from the area under the response spectra.

A brief analysis of some of the data collected early in the 1981 trials suggests the distribution of the data is not quite a Rayleigh distribution as was initially assumed, but rather a more general Weibull distribution, (of which a Rayleigh distribution is a specific form).

At the end of the 1981 trials season, all instrumentation and equipment associated with these trials was removed, and the CORT was restored to pre-trials condition. The digital data tapes will be available at DTNSRDC for future analysis.

ACKNOWLEDGHENTS

The author wishes to express his appreciation to the following individuals for their support in this trials effort.

Hr. David Walden who was the technical representative for the Coast Guard. The Bethlehem Steel Corporation for the use of the M/V S.J. CORT for these trials, and Mr. Charles Walburn of the Marine Division of Bethlehem Steel for arranging the schedule of operations aboard the CORT. Captain Robert Brabander, master of the CORT, and the crew for their cooperation and willingness to help throughout the trials season. Mr. John C. Davies III of the DTNSRDC Central Instrumentation Department for his help with the data acquisition and analysis software. Messrs. Mr. William Hay and Frederick Palmer for assisting in the instrumentation setup, data collection, and support. Mr. Alfred L. Dinsenbacher who provided guidance and suggestions throughout the project.

REFERENCES

 Swanek, R. A. and D. P. Kihl, "Investigation of Springing Responses on the Great Lakes Ore Carrier M/V STEWART J. CORT," Enclosure (1) of DINSRDC Structures Department letter 80-173-210, dated 19 January 1981.

2. Walden, D. A. and M. D. Noll, "Springing Research of a Great Lakes Ore Carrier," CG-D-13-82, Accession No. AD-A115 466, April 1981.

3. Kihl, D. P., "Test Plan for Vertical Bending Moment Static Calibration of the M/V STEWART J. CORT," Enclosure (1) of DTNSRDC Structures Department letter 81-173-168, dated 25 November 1981.

4. Dalzell, J. F., "An Analysis of Data Observed on M/V STEWART J. CORT During the 1979 Trial Program," Davidson Laboratory Report SIT-DL-81-9-2221.

5. Dalzell, J. F., "An Analygis of Bottom Bending Stress Data Observed on M/V STEWART J. CORT During the 1979 and 1980 Trial Programs," Davidson Laboratory Report SIT-DL-82-9-2257, Feb 1982

6. Critchfield, N. O., "Hull Vibration Evaluation of Great Lakes Ore Carrier M/V STEWART J. CORT," Structures Department, DTNSRDC Report 4225, January 1973.

7. Constock, John F. (Editor), "Principles of Naval Architecture," The Society of Naval Architects and Marine Engineers, 1974.

APPENDIX A STATIC CALIBRATION CALCULATIONS

The bending moment produced from the change in ballast loading has to be corrected to account for the change in buoyancy distribution reacting any change in trim, draft or deflected shape. This net bending moment, the bending moment due to the change in ballast minus the bending moment due to the change in buoyancy distribution, is the actual bending moment being applied to the ship.

Although the ship was not intended to trim or change draft, the draft readings indicated that it did set slightly deeper in the water and trim slightly by the bow. Slight changes car attributed to the bending of the hull due to the induced loading as well as the combined effect of the free water surface in the ballast tank and the accuracy to which the ballast can be loaded to the nominal specified depth, and are accounted for in the calculations. The draft readings themselves are also felt to be slightly in error, as will be discussed later. Overall trim, i.e. nominally 8 ft by the stern, appears to be correct.

The calculations are based on the initial assumption that the draft meters were reading the draft accurately. The draft meters are located 447.92° fwd $32.33.67^{\circ}$ fwd 32.25° aft 31.2° ; and initially read 12'6" fwd, 16'3" amid, 20'6" aft and changed to 12' 7 1/2" fwd, 16'8 1/2" amid, and 20'3" aft at the calibration ballast condition.

The overall trim of the CORT, in the initial ballast condition, indicated by the fore and aft draft gages was 8 ft by the stern, which gives a ballast depth differential of 0.88 ft inside each ballast tank, the ballast level at the aft end of the tank being 0.88 ft deeper than the forward end.

The overall trim of the CORT, in the calibration ballast condition, was 7' 7 $1/2^{-1}$ by the stern, which gave a ballast depth differential of .84 ft inside each ballast tank. Taking the specified depth at the ladder (located 10 1/2 feet from

19

PRECEDING PACE MANK-NOT FILMED

the aft and of the tank) to be the nominal depth of ballast in the tank, see Table Al, the ballast depth at the fore and aft ends of each tank could be determined, and an average weight of ballast calculated for each tank at the initial and calibration ballast conditions. The difference between the two conditions is the nominal calibration loading, which is nearly 300 Ltons of excess weight, the calibration condition being heavier than the initial condition. By integrating the change in load diagram once, the shear force diagram is developed. Integrating once again, the bending moment diagram due to the change in ballast loading is developed. For the sake of comparison, the bending moment diagram due only to the change in ballast loading is shown in Figure Al. This is not the only bending moment that is acting on the ship. There is a reaction due to the change in buoyancy distribution corresponding to the deflected shape, and change in trim and draft of the ship.

Using the bending moment due only to the change in loading as a starting point, an approximate deflected shape was obtained by integrating the bending moment distribution twice; the stiffness EI, was assumed to be constant along the length of the ship. The deflection curve thus obtained was forced to fit through the three changes in draft readings and indicates the change in draft along the length of the ship, which was used to obtain a change in buoyancy diagram.

The ship was divided up into twenty stations of fifty foot lengths, and the average buoyancy force was calculated at the midpoint of each station. By adding the load diagram due to the change in ballast loading (sag amidships) to the load diagram due to the buoyancy reaction of the loading (hog amidships) the first iteration to the actual load acting on the ship was obtained. Integrating the change in load diagram once gave the shear force diagram, and integrating twice gave the bending moment diagram due to the combined buoyancy reaction and change in the ballast loading acting on the ship.

This new bending moment diagram was then integrated twice to obtain a new deflected shape, which in turn was used to obtain a new change in buoyancy distribution. When added to the load disgram due to the change in ballast loading, new shear and moment diagrams due to the combined load distribution were obtained. Each cycle of the iteration gave a slightly better estimate of the deflected shape. The deflection disgram due to the combined load distribution were found to be quite insensitive to each successive iteration; converging to mearly the same values after each iteration. Each time there was found to be about 600 Ltons of excess buoyancy at an LCG of about 170 ft FWD \mathbf{X} . The amount of excess weight from the free surface effect of the ballast loading, about 300 Ltons, at a LCG of about 11 ft FWD \mathbf{X} had already been accounted for. The remaining 300 Ltons, difference (leas than 4 \mathbf{X} of the total ballast change), was considered to be partially the effect of the scular ballast depth with respect to the specified nominal ballast depths, the accuracy to which the ballast can be added to the tanks and partially the effect of the nominal draft readings.

It seems most likely, from the discrepancy in the LCG locations of the change in ballast and resulting buoyancy distributions, that most of the error is due to the draft readings (particularly the forward reading) since the LCG of the buoyancy distribution disagrees the most from the nominal expected values.

Further, for example, even if the actual ballast depths were off by as much as 1 1/2 inches from the specified levels in the tanks, in both the initial and final condition, in such a way as to shift the LCG of the ballast forward toward the LCG of the buoyancy reaction, the ballast weight only increases to 393.4 Ltons and the LCG of the ballast moves to 55.36 ft FWD ZI.

A solution was therefore obtained by bounding the problem within upper and lower limits. A lower limit was obtained by using the measured draft readings,

even though were fult to they contain some error, and using the above specified changes in ballast (corrected for the free surface affect) conservatively assuming them to be off by as much as 1 1/2 inches, so that the LOG of the ballast would be closer to that of the buoyancy distribution. The moment diagram was forced to close, effectively forcing equilibrium. Even this conservative lower limit (198,000 Ft-Lton at the gage location) is within 10% of the measured value. See Figure Al for bending moment distribution. It should be noted that as the LCG's of the ballast and buoyancy distributions approach each other, the bending moment diagram approaches the measured value.

- -

An upper limit was obtained by calculating a reactive buoyancy distribution to match the change in ballast distribution (corrected for the free surface effect) and using these distributions to obtain a moment diagram. The first estimate of the buoyancy distribution was obtained by substituting the measured stresses into equations 1 and 2 of reference 6 which relate midship stress in terms of midpoint to bow or stern deflection, averaging the results and scaling the previous deflected shape. Subsequent deflections were obtained by integrating the shear and bending moment diagram (see reference 7 for details) of the combined ballast and buoyancy loadings to obtain a consistent midpoint to bow or stern deflection. The resulting deflected shape was then positioned using the TPI and MTI obtained from the ships hydrostatic plans for a mean draft of 16'6" (TPI=224.5 Ltons/in and MTI=16,150 Ft-Ltons/in) to achieve equilibrium between the change in ballast loads and the change in buoyancy reaction. This upper limit (235,100 Ft-Ltons at the gage location) is within 8% of the measured value. See Figure Al for the upper limit bending moment distribution.

BENDING MOMENT CALCULATIONS FROM STRAIN GAGE READINGS

Changes in stress were monitored from the main deck and bottom bending strain gages as the ballast in the middle seven ballast tanks was changed from the initial

code 1 ballast condition to the calibration ballast condition (the torsion gages were also monitored but had a negligible change in output voltage, as expected).

A change in stress of 5.125 ksi compression and 4.437 ksi tension were recorded from the main deck and bottom bending strain gages respectively. The deck gages were located on top of the deck plating and the bottom gages were located on top of the stiffener on the bottom plating (.67 feet above the outside bottom plating). The section properties given in Reference 2 were recalculated with greater securacy and are given in Table A2. Based on the recalculated section properties of the midship cross section, these changes in stress can be converted to a bending moment. Assuming the stress distribution along the width of the ship to be uniform when a vertical bending moment is applied, the vertical bending moment based on the recorded changes in stress were found to be 217,055 Ft-Ltons and 218,619 Ft-Ltons for the deck and bottom bending mages respectively. The average vertical bending moment based on the output from the strain gages is therefore 217,835 ft-Ltons (sag).

Comparing the actual vertical bending moment calculated from the nominal ballast loading and draft readings with that obtained from the strain gage outputs, the actual bending moments come within 10% of the bending moment obtained from the strain gage outputs.

As a comparison of the upper and lower limit curves, and the measured bending moment shown between them on Figure Al, it is seen that the upper limit curve employs a 15.5% correction, due to buoyancy, of the uncorrected bending moment curves shown in Figure Al; the lower limit curve, a 28.8% correction; and the measured bending moment, between the two limits, a 21.7% correction due to the change in buoyancy distribution which is a combination of deflection, sinkage and trim.

As a check on the calculated neutral axis (calculated to be 23.01 ft above the outside bottom plating, or baseline) the stresses recorded during the calibration were used to determine the measured neutral axis location. With a compressive stress of 5.125 ksi located 49 feet above the baseline and a tensile stress of 4.437 ksi located 0.67 feet above the baseline, the location of zero stress or the neutral axis is found to be 23.10 feet above the baseline, which agrees fairly well with the calculated neutral axis location.



Corrections For Deflection, Sinkage, and Trim

TABLE	Al - SO	UNDING	DEPTHS	3 OF	TANK	BALLAST
	BEFORE	AND D	URING (CALI	BRATIC	n

TANK	SOUNDING (FT) (SHIP IN BALLAST CODE 1)	SOUNDING (FT) (DURING CALIBRAITON)
1	16	16
2	14	1
3	15	22
4	25	FULL
5	26	FULL
6	25	FULL
7	21	FULL.
8	21	9.5
9	21	21

TABLE A2 - INERTIAL PROPERTIES AT CORT MIDSHIP SECTION*

MOMENT OF INERTIA ABOUT N.A.	2465640 IN ² FT ²
DISTANCE FROM N.A. TO DECK	25.99 FT
DISTANCE FROM N.A. TO KEEL	23.01 FT
SECTION MODULUS DECK	94832 IN ² FT
SECTION MODULUS KEEL	107202 IN ² FT

* Calculations are based on scantling dimensions shown on Erie Marine Inc. Drawing \$101-S11-11-6 "Midship Section Final."

APPENDIX B TRANSDUCER CALIBRATIONS AND SENSITIVITIES

The measurements listed in Table 1 of the text consist of stress, wave height and acceleration, each of which were calibrated periodically to check their sensitivities, the ratio of engineering units to output voltage, and insure they were operating properly.

The four strain bridge channels (main deck, bottom and lateral bending and torsion) were electrically calibrated with shunt resistors. Each of the strain. gages were wired up in a Wheatstone Bridge circuit with active strain gages and dummy resistors as shown in Figures B1, B2, B3 and B4. The main deck and lateral bending gages were mounted in 2 dyadic configuration on the hull plating; the torsion, at 45° to the vertical and the bottom bending gages, longitudinally on the top of the bottom plating stiffener at the local bending inflection points.

The calibrations were performed by placing shunt resistors in parallel with the strain gages to simulate a compressive strain in that arm of the bridge. These shunt calibrations were performed at the gage site initially to obtain the true sensitivity and daily thereafter at the instrumentation site in the forward machinery room. The output voltages compared well with the calculated values, indicating the signal conditioning and amplifiers were all working properly. The transducer output voltages for the strain gages based on shunt calibrations at the gage site are also included in Figures B1 through B4.

The main deck bending signal was filtered into its wave induced and springing components to assess the relative magnitudes of the stresses as an aid in determining when to take data runs. The wave induced component was produced by low pass filtering the main deck bending signal with a cutoff frequency of 0.2 Hz, and the springing component by high pass filtering the main deck bending signal with a cutoff frequency of 0.25 Hz. Each of the two filtered channels employed two

48 db/octave Khronhite variable filters, which were cascaded to provide a 96 db/ octave rolloff. The filter characteristics, phase lag and attenuation as a function of normalized frequency with respect to cutoff frequency, were calibrated at DTNSRDC with a function generator and frequency counter and are given in Figures B5 and B6. Each of the four strain channels were initially filtered at the signal conditioning using low pass 2 pole Butterworth filters with a 12 db/octave rolloff and a cutoff frequency of 10 Hz.

ACCELEROMETERS

The vertical and horizontal accelerometers mounted on each of the wave measuring units were installed by NRL with the sensitivities given in Table Bl. The transducers were periodically calibrated (in port with calm conditions) by tilting them at various angles to simulate fractions of gravitational acceleration and measuring the output voltage to assure that they were still functioning as calibrated in the NRL lab. The accelerometer signals were filtered at 4 Hz at the NRL instrumentation using a 4-pole Bessel filter.

COLLINS ALTIMETER

The Collins Radar Altimeter was calibrated, to insure it was functioning properly, when the ship was in port, and in calm water. The antenna horns, which were angled outward at 25° from the vertical during data runs, were angled down vertically for the calibrations. The calibration consisted of monitoring the change in output voltage as the horns, attached to the boom, were swung out over the water and clear of the ship, and then back again over the deck. The sensitivity was checked by dividing this change in distance by the change in output voltage as shown in Figure 37.





SHUNT CALIGRATION = Rs= 750 KL LEAD WIRE RESISTANCE = RL= 6L BRIDGE RESISTANCE = RA = 700 JARM EXCITATION VOLTAGE = Ext= 10 youts CAGE FACTOR = F=2.125 NUMBER OF ACTIVES = N=2 POISSON'S RATIO = L=.28 YOUNG'S MODULUS = E=20=104951

SIMULATED STRESS FROM SHUNT AT RAGE

OUTPUT FROM GAGE SITE SHUNT : 2.23 WITS

SENSITIVITY= 9150 AST/2.23 YOUR = 4100 AST/YOUT POSITIVE VOLTS CORRESPONDS TO COMPRESSION OR SHIP SAG

Figure B1 - Strain Bridge Circuits for Main Deck Bending



SHUNT CALIBRATION - RE · 500 KL LETAD WIRE RESISTANCE · R. · 7L GRIDGE RESISTANCE · RA · 740 Mar EXCITATION VOLTAGE · Ex: 10 WINS

GAGE FACTOR = F. 2.125 NUMBER OF Actives: n: 2 PUISSON'S RAHD = A: .28 YOUNG'S MUDULUSS 5+30- 460;

SIMULATED STRESS FROM SHUNT AT GAGE

S. ERAINERS

· (30×10*)(700)/(2)(2.125)(500,000)

= 9880 ps;

OUT PUT FROM GAGE SITE SHUNT = 3.38 VOLTE

SENSITIVITY = 9880 psi/3.38 was = 2900 psi/volr Positive VOLTS CORRESPONDS to comPRESSION OR SHIP HOG

Figure B2 - Strain Bridge Circuits for Bottom Bending



SHUNT CALIBRATION: R= 300KA LEAD WIRE RESISTRACE + R= 7A BRICKE RESISTANCE + RA + 240 -/ARA EXCITATION YOLTAGE + EX + 7 VAIS

GAGE FACTOR = F = 1.875 NUMBER OF ACTIVES = N = 2 POISSON'S RATIO = A = .28 YOUNG'S MODULUS= E = 30 = 10² pr

SINIULATED STRESS FROM SHUNT AT GAGE

5: ERA/NF(1-L)R:

=(30×10⁺)(240)/(2)(1.875)(.72X300,000)

= 8890 psi

OLTPUT FROM GAGE SITE SHUNT = 1.34 WARTS

SENSITIVITY = 8890 PSi/1.34 volts = 6640 PSi/volt

POSITIVE VOLTS CORRESPONDS TO TENSION ON THE PORT SIDE

Figure B3 - Strain Bridge Circuits for Lateral Bending



SHUNT CALIBRATION . R. + 150 KA LEAD WIRE RESISTANCE , R. T.A. BRIDGE RESISTANCE = RATIZONIAR EXCITATION VOLTAGE . E. . : TVOLTS

CAGE FACTOR = F: 2.04 NWIBER OF ACTIVES + A . 4 POISSON'S BATION L . 28 YOUNC'S MODULUS+ E= 30+104Pil

SIMULATED STRESS FROM SHUNT AT GAGE

Js: ERA/NF(1+L)Rs =(30=104)(120)/(4)(2.04)(1.28)(150,000) = 2298 pri

OUT PUT FROM GAGE SITE SHUNT = 1.26 YOUTS SENSITIVITY = 2298 PS :/1.26 VOLTE = 1820 Mi/volt POSITIVE VOLTS CORRESPONDS TO STED BOW UP

Figure B4 - Strain Bridge Circuit: for Torsion



.,

-**F**









1. Position RADAR HORNS VERTICALLY OVER WATER, TAKE VOLTAGE READING - VH-W 2. Swing collins horns in over DECK and Take Second Reading - VH-D 3. Record ship draft

RANGE SENSITIVITY = $\frac{D_{a-b} - D_{RAFT}}{V_{H-w} - V_{H-b}} = \frac{FT}{VOLT}$ (decreasing Range)

TYPICALLY,

WITH HORNS AT A 25" ANGLE THE SENSITIVITY = (US 25" (-1596) - - 14.5 FRONT

Figure B7 - Collins Radar Altimeter Calibration procedure

Table B1 - NRL INSTALLED TRANSDUCER SENSITIVITIES

1

and the second the first state of the second

7 17 10

MEASUREMENT	SENSITIVITY	SENSE
Collins Rødar Rønge	14.50 ft/volt	Increasing Range
	-	@ 25° to Vertical
Collins Vertical Acceleration	1.855 ft/sec ² /volt	Acceleration Up
Collins Horizontal Acceleration	3.240 ft/sec ² /volt	Λ cceleration to STBD
NPL Range	24.61 ft/volt	Increasing Range
NRL Vertical Acceleration	1.408 ft/sec ² /volt	Acceleration Up
NRL Horizontal Acceleration	2.512 ft/sec ² /volt	Acceleration to Port

LASCEDING PACE BLANK-NOT FILMED

÷

APPENDIX C BEADER LOGS FOR H/V S.J. CORT PATA RUNS

A list of the header logs for each of the runs taken during the 1981 trials is provided in this appendix. The header logs list the ship conditions, speed, heading location and draft as well as wind and wave conditions at the start of each run. Also included are remark statements which give additional information about the run.

The location in terms of north latitude and wast longitude were obtained from the Loran C tracking receiver used onboard. Vessel speed was obtained by the mates on watch by logging distance covered over a period of time. Direct speed was obtainable from the Loran C but was considered unreliable. Vessel heading was read directly from the ship's gyrocompass. The wind speed and direction are the true wind speed and direction existing at the start of sach run. Wave height and direction are based upon visual estimates of the predominant sea at the start of each Sometimes the wave direction would be taken to be the same as the wind direc-TUDtion if the wind direction had been steady for a long period of time as the waves were building. The draft indicated in the header log was read off of the forward draft meter as the ship was underway. The other drafts were usually listed in the remark statements. An error in draft readings is evident when the ship is underway due to the effect of speed. True draft readings were taken when the ship was either in port or passing through the locks at Sault Ste. Marie. Runs 1-5 were taken with the ship ballasted between code 1 and code 2 with true drafts ap, moximately 13'10" fwd, 15'3" amid, and 19'7" aft. Runs 6-12, 25-40, and 42-57, were taken with the ship in the loaded condition, with true drafts 27'0" fwd, 27'0" amid and 27'0" aft. The remaining runs 13-24 and run 41 were taken with the ship in the code 1 ballast condition, with true drafts 12'5" fwd, 15'8" amid, and 19'6" aft. These and other draft conditions are listed in Table Cl.

PRECEDING PLOT BLANK NOT TILLED

	TABLE C1 - CORT	DRAFTS FOR LOAD/B	ALLAST CONDITIONS	
CONDITION	LOG ENTRY	DRAFT FWD	DRAFT AMID	DRAFT AFT
Ballast Code 1	12'-12'	12' -5"	15' -3"	19'-6"
Ballust Code 2	15'-16'	15'-4"	16'-11"	· 19'-8"
Ballast Code 3	17'-18'	17'-0"	18'-11"	21'-3"
Ballast Code 4	19'-20'	20"-7"	20'-7"	22'-0"
Ship Loaded	27 *	27'-0"	27'-0-	27'-0"

25.000 11150128 45 28 85 27 225 ŝ 225 1.5.4 91 TIME DATE 10-HDV-81 TIME TIME DATE 10-HDV-81 TIME TURATION OF RUN IN MIMUTES IS HORTH LATITUDE (DD MN) E UEST LONGTIUGE (DD MN) TE UESSEL'S HEADING (DEGRECS) TE UTRD DIRECTION (DEGRECS) 2 UIRD SFEEL (NNOTS) 2 UIRD SFEEL (NNOTS) POLNT REMARKS FOLLOWING SEAS APPROX 3.5 WAVE HEIGHT HAVE FIRECTION (DEGREES) HAVE REIGHT (FEET) WIND & COAT FALL '8' TRIALS RUN

End-of-run messafe Follouisko seas, sl 7 not earking, diultizing at 5 SAM/BEC

25.000 EEIIEIIO E 46 39 84 50 14.6 332 22 82 **310** 151 THE DATE 11-MOU-81 THE DURATION OF RUN IN MINUTES IS NORTH LATITUDE (DD MM) VESSEL'S HEADING (DE MM) VESSEL'S HEADING (DEGREES) VESSEL'S GRAFT (FEET) VESSEL'S GRAFT (FEET) MIND DIRECTION (DEGREES) WIND DIRECTION (DEGREES) WIND DIRECTION (DEGREES) FOINT WAVE HEIGHT (FEET) M/V S J CORT FALL BI TRIALS REMARNE CODE 14 HEAD SEAS RUN

End-of-run desserte 4 FT UAVES, NEAR WHITEFISH PDIMI/SI 7 NOT WORKING/5 6FG

25.000 02112117 49 49 23 14.8 10 320 **1**62 IATE 11-NOV-81 TIME DURATION OF RUN IN MINUTES IS MARTH LATIUDE (DD MM) HEST LONGITUDE (DD MM) VESSEL'S SFEED (MPH - XX.X) VESSEL'S HEADING (DEGRES) VESSEL'S HEADING (DEGRES) VESSEL'S HEADING (DEGRES) MIND DIRECTION (DEGRES) MAVE HEIGHT (FEET) POINT M/U D J CORT FALL B1 TRIALS REMARNS COLE 14 MEAU SEAS RUN

Erd-of-run Bessage SL 7 (111-5 5PS: MAN'S BUILDING BLOWLY

02129145 113 113 DATE 11-MOV-BI TIME DURATION OF RUM IN MIMUTES IS NORTH LATITUDE (DD MM) UE551LOMORTUDE (DD MM) UE552L'8 BAFED (MM) - XX.X 1 VE552L'8 DRAFT (FEET) VE552L'8 DRAFT (FEET) VE552L'8 DRAFT (FEET) WIND SPEED (KNOTS) WAVE DIRECTION (DEGREES) HAVE HEIGHT (FEET) REMARKS CODE 14 HEAD SEAS

25.000

POINT

M/U & J CORT FALL BI TRIALS

M 10

End-of-run messate BL 7 OUT+5 SP3+ HEAD-DOM-SEAB

1191150 293 22 10.01 EIE 3.50 n.n DURATION DF RUN IN NIMUTES IS NORTH LATITUDE (DD NN) NEST LONGITUDE (CD NN) VESSEL'S BFEED (NPH - XX,X) VESSEL'S LEAFT (FFET) VESSEL'S LEAFT (FFET) ULIND DIRECTION (DEGREES) NIQ. WIND SPEED (KMOTS) WAVE DIRECTION (DEGREES) HAVE HEIGHT (FEET) H/U S J CORT FALL BI TRIALS 11-NOV-81 DATE REMARKS CODE+1 DOM SEAS ¥52

End-of-run bestafte BL 7 DUT.WIND DIR 330.WIND SPD 18 KNT8, DDM SEAS

23.000 24114131 47 21 5 112 162) 1 2 1 REMARKS LOADED DNBND, DRAFTS 24,27,27,54. 7 AUT,554"; DATE 12-MOV-DI TIME LURATION OF RUM IN MIMUTEB 18 MORTH LATITUDE (DD MM) LEST LOWGITUDE (DD MM) VESSEL'S SPEED (MPH - XX.X) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) POINT WIND BPEED (KMOTS) Wave direction (regres) Wave Height (feet) M/V & J CORT FALL BI TRIALS

End-of-run message Lowe MAVES

25.000 13 24124105 47 18 50 182 14.3 182 HEADED TOUARD HAITEFISH RAY LOADED TUBND, DRAFTS 24,27,27, SL 7 OUT,5 SPS 86 MATE 12-NDV-01 TIME NUKATION OF RUM IM MIMUTEB IS NUKH LATIUDE (DD MM) WESSEL'S SFEED (MFH - XX.X) 14 VESSEL'S SFEED (MFH - XX.X) 14 VESSEL'S KADING (DEGREER) 1 VESSEL'S KANING (DEGREER) 1 UNIO FIRECTION (DEGREES) 1 WIND FIRECTION (DEGREES) 1 WAVE FIRECTION (DEGREES) 1 POINT WAVE HEIGHT (FEET) N/V B J CORT FALL BI TRIALS End-of-run eosaado 4-5 ft ream seas RUN **RZHARNS**

22.000 15 24134112 47 15 86 31 112 192 192 MATE 12-MOU-81 TIME DUKATION OF RUM IM MINUFS 13 MORTH ATTIDUE (DD MM) LEST LONGITUDE (DD MM) VESSEL'S SFEED (MPH - XX,X) VESSEL'S REALT (FEET) VESSEL'S GRAFT (FEET) VESSEL'S GRAFT (FEET) INIO4 WAVE DIRECTION (DEGREES) WAVE HEIGHT (FEET) WIND SPEED (KNOTS) M/U S J CORT FALL BI TRIALS RH2

REMARKS Meaded Toward Whitefish Bay Loaded Darnd, drafts 24,27,27, 81, 7 Out.5 8PS

End-of-run messate 4-5FT REAM SEAS

23.000 24140155 86 23 47 13 8 14.3 REMANAS Headed Touard Unitefich Bay Loaded Dhudi Drafts 24:27:27: 81 7 Dut;5 5PS 192 112 25. DATE 12-NOU-BI TIME DURATION OF RUM IM MIMUTES IS NORTH LATITUDE (DD MM) LEST LONGITUDE (DD MM) UESSEL'S BFEED (MPH - XX,X) 14 VESSEL'S HEADING (DEGREES) VESSEL'S DRAFT (FEET) TKIO9 WIND DIRECTION (DEGREES) WIND SPEED (KNOTS) WAVE DIRECTION (DEGREES) WAVE HEIGHT (FEET) M/V S J CORT FALL B1 TRIALS RUN

End-of-run messate 3-4 FT DEAN SEAS.DA 13-MOV-01+ TI 02123100

23.000 41 41 15 37 11.2 200 300 POINT DATE 14-MOV-81 TIME DURATION OF RUM IN MIMUTES 18 HORTH LATITURE (DD MM) HEST LONGITURE (DD MM) VESSEL'S SPEED (NPH - XX,X) VESSEL'S RAAINO (DEGREES) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) VIND DIFECTION (DEGREES) NORTHERN MICHIGAN+DWBND+DRAFTS 24,27,27 5L 7 1 BL 7 H ACC OUT+ 5 8PB WAVE DIRECTION (DEGREFS) WAVE HEIGHT (FEET) N/V 5 J CORT FALL BI TRIALS DATE RUN REMARK8

End-of-run messade HEAD SEAS 3 FT

19.00 19.00 05112110 15 30 ~ 187 203 187 UNATION OF THAN IN NIMUTES IS NORTH LAITTUDE (DD NH) UEST LONGITUDE (DD NH) VESSEL'S SPEED (NPH - XX,X) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) POINT POINT WAVE DIRECTION (DEOREES) WIND SPEED (KNOTS) M/V & J CORT FALL BI TRIALS 14-NOV-81 DATE RUN

REVARKS Horthern Michigan, DNBND, DRAFIS 24,27,27 3L 7 8 8L 7 H ACC OUT, 5 8P8

End-of-run ansaste HEAD BEAS J FT

12.000 23 02128146 2 182 182 ņ POINT REMARKS MORTHERM MICHIGAN+DUBND+DRAFTS 24+27+27 MURATICH OF RUN IN MINUTES 18 NORTH LATITUDE (DD NN) WEST LONGITUDE (DD NN) Vessel's Speed (NPM - XX,X) Vessel's Haading (degares) Vessel's Darft (feet) Wind Direction (degrees) WIND SPEED (KHOTS) WAVE DIRECTION (DEGREES) HAVE HEIGHT (FEET) PLA S J CORT FALL BI TRIALS 14-NOV-11 DATE RUN

BL 7 1 BL 7 N NCC CUT. 5 \$PB

HEAD BEAS 3 FT End-of-run

25.000 25 06141108 86 46 15.3 290 47 15 10 8 290 290 CLAR 17-NOV-81 POINT 17-NOV-81 FURATION OF SUN IN MINUTES 18 FURATION OF SUN IN MINUTES 18 FURATION OF SUN IN MINUTES 18 CESSEL'S GFEED (MPH - XX,X) VESSEL'S HEADINO (DEGREES) VESSEL'S HEADINO (DEGREES) VESSEL'S LANOTS) ULID DIRECTION (DEGREES) POINT MENARXS UPBRO SUPERIOR DRAFTS 10.16.5.21.5. SL 7 1 St 7 H ACC OUT. 5 5F8 W/W G J CORT FALL BI THIALS

End-of-run wessed HEAD SEAS, 2-3 FT, ACTUAL FUD DRAFT 11'11"

23.000 42112190 47 19 86 59 15.3 291 0 290 290 TIME 17-MOV-81 DUKATION OF RUN IN HINUTES 18 MORTH LATITUDE (DD MM) HEST LONGITUDE (DD MM) VESSEL'S HEADING (DECHEES) VESSEL'S UKAFI (FLET) VESSEL'S UKAFI (FLET) Z'VESSEL'S UKAFI (FLET) Z' POINT REMARKS UPBNJ GUPERIOR DRAFT8 10,14,3,21,5, SL 7 1 SL 7 H ACC OUT, 5 5P8 UIND SPEED (KNOTS) UAVE DIRECTION (DEOREES) WAVE HEIGHT (FEET) M/V B J CORT FALL BI TRIALS UNUE RUN

End-of-run assante Head sens 3-4 ft .code 1 .achal fud draft 12 ft

25.000 2 07119142 47 23 87 14 18 2 297 297 15.1 291
 RUN
 15
 POINT

 DATE
 17-NOV-81
 TIME

 DURATION OF RUN IN MINUTES 13
 0

 DURATION OF RUN IN MINUTES 13
 0

 NORTH LATTUDE
 00 MN

 UESSEL'S GFEED (NPH - XX,X)
 13,0

 UESSEL'S HEADING
 05,000 MN

 UESSEL'S AFADING
 05,000 MN

 UESSEL'S DRAFT
 15,0

 UESSEL'S DRAFT
 15,0
 UP BHD EUPERIOR DRAFTS 10.16.5.21.5. BL. 7 B SL. 7 H ACC DUT. 5 8P8 WIND SPEED (KNOTS) WAVE DIRECTION (DECREES) WAVE HEIGHT (FEET) M/V B J CORT FALL OI TRIALS RENARXS

End-of-run messate Head Send:4-5 fr:East of Keueennu PT.TI 08:33

25.000 31 07125141 47 25 07 24 297 241 2 MATE 17-HOU-BI TIME DATE 17-HOU-BI TIME DATE 17-HOU-BI TIME HORTH LATITUDE (DD NN) WEST LONGITUDE (DD NN) VESSEL'S SFEED (MPH - XX,X) UESSEL'S BRATIMO (DEGREES) UESSEL'S BRATIMO (DEGREES) ULIND SFEED (KNOTS) ULIND SFEED (KNOTS POINT 2 RUM

M/U S J CORT FALL BI TRIALS

REMARKS UPBUD BUPERION DRAFTS 10,14,5,21,5, BL 7 & BL 7 H ACC OUT, 5 8PS

End-of-run messade HEAD BEAS:4-5 FT. TI 09104 , CODE 1

POINT HO2

M/U & J CORT FALL BI TRIALS

1

10.000 10111101 274 274 5 DATE 17-NOV-81 TIME DURATION OF RUM IN NINUTG 16 WORTH LATITUDE (DD MN) WEST LONGTIUDE (DD MN) VESSEL'S BREED (MPH - XX.X) VESSEL'S BRAFT (FEET) VESSEL'S BRAFT (FEET) WIND BPEED (KNOT8) Wave Direction (deonees) Wave Height (feet)

UPAND SUPERION DRAFTS 10-16-5-21-5-SL 7 & SL 7 H ACC DUT- 5 6PS REMARKS

End-of-run assade HEAD-BON BEAS+TI 10143

23.000 35 10121103 Q 47 30 0 2 276 276 ULRATION OF RUM IN MIMUTES 13 MORTH LATITUDE (DD MM) WEST LONGITUDE (DD MM) UESSEL'S HEADING (DEGNEES) VESSEL'S HEADING (DEGNEES) VESSEL'S DRAFT (FEET) UIND DIRECTION (DEGNEES) POINT TIR REMARKS UPBND SUPERIOR DRAFTS 10-14-5-21-5-BL 7 & SL 7 H ACC OUT: 5 80-5 WIND SPEED (KNOTS) Wave Direction (Deorees) Wave Height (Feet) M/U B J CORT FALL BI TRIALS DATE 17-HOV-81 NDa

End-of-run messade HeEAD-BON BEAS:2-3 FT +CODE 1 +TE 1113

13142143 10127112 23.000 921441EI 14 -17 22 47 30 17 24 2 88 11 20 273 0 0 4.4 275 275 14.3 258 220 273 14.6 259 2 275 REMARKS (FEMARKS) 51.7 & 81.7 H ACC OUT: 5 6P8 TIME TO THE TAY AND TAKE TAY AND TAY A ULEATION OF ANN IN MINUTES IS NORTH LATITUDE (DD MM) UESSEL'S SFEED (MPH - XX,X) UESSEL'S AFEED (MPH - XX,X) UESSEL'S HEADING (AEGAEES) UESSEL'S DKAFT (FEET) WIND DIRECTION (DEGREES) POINT POINT TATE 17-MOU-81 TIME THEATTOM OF FIM TW MIMUTES TS HUNTH LATITUSE (DD MM) UNST LONGITURE (DD MM) UNST L'S SFT A (MM) - XX.X) End-of-run messess HEAD-BOW SEAS:2-3 FT, CODE 1. TI 11144 VESSEL'S HEADING (DEGNEES) VESSEL'S HEAT (FLF1) VESSEL'S HEAT (FLF1) WIND BIKLETICH (DEGNEER) REHACKS (# 5410 SIFFILION DRAFTS 10+14-5-21-5-81 7 8 81 7 H ACC GUT- 5 5PB WIND SPEED (KHOTS) HAVE DIRECTION (DEDREES) DIRITING (DEGREFS) WAVE DIRECTION (DEOREES) UNVE HEIGHT (FEET) WAVE HEIGHT (FEET) WIND SPEED (KNOTS) WAVE DIRITING (DEG WAVE DEGUNT (SEET) N/V S J CORT FALL 'BI TRINLS SPEED (AMOTS) RAU B J CORT FALL 'UI TRIMB AN B J CORT FALL BI TRIMB End-of-run arusado STBD DON 4-5 FT , TI 14110 LATE 17-NOV-BI GNIA RUN 21110

REMARKS. UPDHD SUPERIOR, DAAFTS 10,14,5,21,75, CODE 1 RL 7 8 8L 7 M ACC GUT, 5 9PS

End-of-run pessass BTBS BCS 8-5 FT T1 14141

23.000 13155124 47 21 54 57 54 14.4 273 MATE 17-MOU-R1 TIME DURATION OF RUM IN MIMUTES IS HORTH LATITUDE (DD MN) VEST LONGITUDE (DD MN) VESSEL'S SFEED (MPH - XX.X) VESSEL'S HAAFT (FEET) VESSEL'S NAAFT (FEET) VESSEL'S NAAFT (FEET) VESSEL'S NAAFT (FEET) VESSEL'S CONCES) VESSEL'S CONCES) VAIND DIRECTION (DECONEES) VAIND DIRECTION (DECONEES) VAINE DIRECTION (DECONES) VAINE DIRECTION (DECONES) VAINE DIRECTION (DEC POINT W/W & J CORT FALL 'BI TRINLE

REMARKS UPBAD BUPERIOR, DRAFTS 10,14,5,21,75, CODE 1 BL 7 & BL 7 A ACC OUT, 5 848

End-of-run messade STBP BDW BEA8, 4-5 FT, TI 15111

25.000 14114142 41 44 49 40 234 235 280 9 20 WATE 17-MOV-B1 TIME DURATION UF RUN IN NIMUTED 16 MORTH LATITUDE (DD MM) LUEST LONGIILITE (DD MM) LUESTL 26 FEED (MPH - XX,X) VESSEL'S FREED (MPH - XX,X) VESSEL'S PKATT (FEET) VESSEL'S PKATT (FEET) POINT WAVE DIRECTION (DEONGES) WAVE HEIGHT (FEET) H/V B J CORT FALL 'BI TRIALS WIND SPEED (XMOTB)

REMARAS UPDAD SUPERIOR: DRAFTS 10/14.5,21.75, CODE 1 BL 7 8 BL 7 H ACC OUT: 5 5P8

End-of-run sessate STBD SEAS DOW: 3-4 FT TI 16141

8.5 17103124 E1 74 380²⁰ 280 2 DATE 17-HOV-B1 TIME DURATION OF RUN IN MIMUTES IS MORTH LATITUDE (DD MM) LEST LONGITUDE (DD MM) VESSEL'S SFFED (MPM - XX.X) VESSEL'S HEADING (MECHTES) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) POINT WIND GPEED (KNOTB) . Wave Direction (Deorees) Wave Height (Feet) . W/V S J CORT FALL 'BI TRIALS . ND

NEWARKS UPBHD SUPERION, DAAFTS 10,17,22, CODE BL 7 8 SL 7 H ACC OUT, 5 SPS

End-of-run messale DOM BEAS STBD: 2-3 FT: T1 17135

14138117 25.000 5 -14133100 47 23 9 CCRI FALL "DI INIMUE POINT FUN 23 FOINT INTE 10-NOV-81 INMUTE8 18 MITATION OF RUH IN MIMUTE8 18 MICATION OF RUH IN MIMUTE8 18 MIRU SEEL'S HEADING (DEOREES) 14 VESSEL'S VESSEL'S VENTS POINT REMARX8 BNDH3 6UPERIOR, DRAFTS 24,27,26,75 61 7 8 81 7 H ACC 0HT, 5 5F6 HAVE DIRECTION (DEGREES) HAVE MEIGHT (FEET) End-of-run anssade 908 BEAN SIAS, 1-2 FT, TI 14158 MAN S J COMI FALL '81 TRIALS BAN 3 J COST FALL 'BI TRIALS 18-MOM-81 EATE RUR

1 33 0 0 WAVE DIRECTION (DEGREER) WAVE MEIGHT (FEET) SPEED (KNOTS) UNIN

REMARKS DH349 BUPERION DAM'TS 24.27.24.75 BL 7 3 8L 7 H ACC OUT: 3 878

End-of-rum gestade DOM-DEAN SFAS: 1-2 FT: TI 15129

25,000 5 17146144 47 31 88 27 20 3 355 14.1 335 FATE 18-MOU-81 TIME FURATION OF RUN IN NIMUTES 18 HORTH LATITURE (DD NN) USSEL'S SPEED (MPN - XX.X) 14 UESSEL'S MEADING (DEOREES) UTINE DIRECTION (DEOREES) 3 UTINE DIRECTION (DEOREES) 3 POINT REMARKS DWEND SUPERIOR: DAAFTS 24.75,224.5 DL 7 4 8L 7 H ACC OUT: 5 8PB WINT SPEED (KNOTS) WAVE DIRECTION (DEDREES) WAVE HEIGHT (FEET) NAV S J CORT FALL 'BI TRIALS N I I N

End-of-run arnaade bou-bean seas 4-5 ff. fl 118110

55 10112101 25.000 355 DATE 18-MOV-01 TIME DURATION OF KUN IN MIMUTES IS HORTH LATITUDE (DD MM) WESTEL'S SFEED (MPH - XX.X) 14 VESSEL'S SFEED (MPH - XX.X) 14 VESSEL'S DRAFT (FEET) UESSEL'S DRAFT (FEET) POINT SPEED (NNOTS) DIRECTION (DEOREES) WAVE DIRECTION (DEG WAVE HEIGHT (FEET) N/V S J CORT FALL 'BI TRIALS **DHIN** RIM

REMARKS DNBUD BUPERIOR: DRAFT8 24.25,27,24.5 BL 7 & GL 7 H ACC OUT: 5 5P8

End-of-run messase DEAN SEAS, 4-5 FT ,TT 18159

H/V S J CORT FALL 'B' TRIALS

57 18117125 25.000 47 35 POINT DURATION OF RUN IN NIMUTES IS NORTH LATITURE (DD NN) LEST LONGITURE (DD NN) VESSEL'8 SPILU (NPH - XX,X) VESSEL'8 HEADING (DEGNEES) VESSEL'5 DEAT (FEET) VESSEL'5 DEAT (FEET) 18-NOV-81 DATE **N**

ลี่ย ลี่ย UAVE DIRECTION (DEGREES) HAVE HEIGHT (FEET) SPEED (ANNTR)

REMARKB Burdind Buperion, drafts 24.25,27,24.5 BL 7 & BL 7 H Acc Out, 5 8PE

End-of-run messate BEAN SEAS: 4-5 FT, TT 19132

23.000 10124181 45 47 35 87 44 0 ñ 0 ñ 0 14.2 TIME 19-000-81 DURATION DF RUM IN MIMUTES IS WEST LONGTIURE (DD MM) WESSEL'S SPEED (MPH - XX,X) VESSEL'S SPEED (MPH - XX,X) VESSEL'S SPAIT (FEET) VESSEL'S DRAIT (FEET) WIND STREETION (DEGREES) WIND STREETION (DEGREES) WIND STREETION (DEGREES) **THIO** WAVE HEIGHT (FEET) W/V B J CORT FALL 'BI TRIALS ñ RUN

REMARKS DNDND SUPERIOR: DRAFTS 24.23,27,24.5 BL 7 1 SL 7 H ACC DUT: 5 8PS

End-of-run messade PORT BEAN,4-SFT, TE 20127

 GAT FAL '81 TRIALS
 POINT
 41

 AUM
 31
 POINT
 41

 AUM
 31
 POINT
 41

 ANTE
 18-WOV-81
 TIME
 18153104

 MARATION OF RAU IN MINUTES 18
 23:000
 47
 35

 MIKATIONE OF RUM IN MINUTES 18
 47
 35

 WCTT LUNGIULE (DD MM)
 67
 34

 VESSEL'S SFEED (MPH - XX,X)
 47
 35

 VESSEL'S SFEED (MPH - XX,X)
 24
 0

 VESSEL'S SFEED (MPH - XX,X)
 24
 0

 VESSEL'S MARS
 24
 0
 24

 UIND SFEED (MPH - XX,X)
 24
 0
 24

 UIND SFEED (MPH - XX,X)
 24
 0
 24

 UIND SFEED (MPH - XX,X)
 24
 0
 24

End-of-run masses Stran Almatfring Bens Heading Chunge to 113 +3 Minuics Into Run

ALV B J CORT FALL "BI TRIALS FUN 32 POINT FUN 12 19-MOV-81 TIME 04153107 FUNATION OF RUN 18 MINUTES 18 MORTH LATTUDE (DD MM) 65 21 VESSEL 9 SFEED (MPH - XXXX) 14.2 VESSEL 9 SFEED (MPH - XXXX) 14.2 VESSEL 9 NAVET (FEET) 24 UIND DIRECTION (FEENES) 11 VESSEL 9 DARFES 101 (DEGREES) 10 UIND DIRECTION (FEERES) 10 UNVE HEIGHT (FEET) 10 MAVE HEIGHT (FEET) 10 MAVE HEIGHT (FEET) 10 MAVE DIRECTION (FEERES) 10 UNVE HEIGHT (FEET) 10 UNVE HEIGHT (FEET) 10 UNVE HEIGHT (FEET) 10 UNVE DIRECTION (FEERES) 10 UNVE HEIGHT (FEET) 10 UNVE DIRECTION (FEERES) 10 UNVE HEIGHT (FEET) 10 UNVE HEIGHT (FEET) 10 UNVE DIRECTION (FEERES) 10 UNVE DI

End-of-run bossess Port Beam, Radio Comes 12 min Into Rum. TI 5118

 MAV 8 J CORT FALL "81 TRIAL8
 FOINT 645

 RUN
 33
 FOINT
 65

 FUN
 33
 FOINT
 65

 FALL
 19-MOU-81
 TIME
 25:000

 FUNEATION OF RUM INMUTES IS
 25:000
 25:000

 FUNEATION OF RUM INMUTES IS
 25:000
 25:000

 FUNEATION OF RUM INMUTES IS
 46:52
 25:000

 WOTT LONDITION (FON MI)
 85:7
 11

 UNCELSE FRED (MMH - XX.X)
 14:2
 24

 UNUED SFEED (MHH - XX.X)
 14:2

End-of-run sessade DEAM BEAM PORT: 3-4 FT, TL 5130

END THPE

25.000 23.000 25.000 10132128 13100143 08128113 43 21 44 15 84 47 R 5 320 2 14.3 0**9**5 09 m 164 320 340 2.11 360 185 \$ UNITION THE A TITUE OF POINT ALM TIME A TIME A DURATION OF RUN IN MINITES IS HORTH LATIFUE (DD MH) UEST LONGITUDE (DD MH) UESSEL'S SPEED (NHM - XX,X) 14 UESSEL'S HEADING (DE OREES) 32 URD DIRECTION (DE OREES) 32 URD DIRECTION (DE OREES) 32 UND DIRECTION (DE OREES) 35 UND DIRECTION (DE OR TINE TO-NOV-91 TINE TO THE TOT INTE ZO-MOU-BI INTE ZO-MOU-BI FURATION OF RUM IN MINUTES IS HOGTH LATITUDE (DD MA) UEST LONGITUDE (UD MA) VESSEL'S SFLED (NVH - XX.X) 14 VESSEL'S BRAFI (FEET) VESSEL'S DRAFI (FEET) 3 POINT POINT REMANKS DHBHD HICHIGAN, DRAFTS 24.25.27.24.5 BL 7 9 EL 7 H ACC OUT: 5 6PS REMARKS Darand Michigan, Drafts 24.25,27,24.3 SL 7 3 Si 7 H Acc Out: 5 5P3 CHAND MICHIGAN, DRAFTS 24.25.27.24.5 6L 7 2 SL 7 H ACC OUT 5 6F8 STEFD (KNOTS) DIRECTION (DEOREES) End-of-run pessaae Fouldwing SEAS: 6-7 FT: TI 9123 End-of-run mensade Fouldwike SEAS: 6 FT : TIBI54 M/V 2 J CORT FALL '81 TRIALS UAVE DIRECTION (DEC UAVE HEIGHT (FEET) BININ S L CORT FALL 'S TRINLS ALV S J CONTENL OF TRIME ព្អ **DIVIN** RUA RCE いとうてんしい

23.000 13104134 41 14 320 320 1 THIO? DATE 20-MOU-B1 TIME LUKATION OF RUM IN NIMUTES 18 HORTH LATITURE (DD MM) MEST LOMOTIUDE (DD MM) VESSEL'S SFEED (MFM - XX,X) VESSEL'S HEADING (DEOUCES) VESSEL'S KAAT (FEET) VESSEL'S UKATT (FEET) UND SPEED (KAOTS) MAVE DIRECTIOM (DEONEES) MAVE HEIGHT (FEET) REMARKS Undad Michidam, drafts 24.25,27,24.5 BL 7 & BL 7 H Acc Out, 5 8PS N/N S J CORT FALL 'S' TRIALS NUM

End-of-run message Fouldwing Sibb Quartry, 4-7 FTr II 13155

23.000 13114126 URATION OF AUM IN NIMUTES IS HOKTH LATITUDE (DD MN) UESSEL 1.006111/DE (DD MN) UESSEL'S BAFED (MPH = XX.X) UESSEL'S BAFED (DEGNEES) UESSEL'S NEAT (FET) UIND DIRECTION (DEGNEES) HIND SPEED (KNOTB) HAVE DIRECTION (DEONEES) HAVE HEIGHT (FEET) M/V & J CORT FALL '81 TRIALS 20-NOV-BI DATE ž

REMARKS DNBND NICHIGAN: DRAFTS 24,25,27,24,5 BL 7 & BL 7 H ACC DUT: 5 8PB

End-of-run messate Foll Berb Stern, Radio Comme During Last 1.5 Ning.ti 14130

11	23.000 42 59 84 56	14.3 18.4 24 113	•	. •
M/U 8 J CORT FALL '81 TRIALS POINT	DURATION OF RUN IN NIMUTES IS	USSEL'S BYEED (NGH - XX.X)	UIND SPEED (KNOTS)	REMARKS
RUN 39 POINT	MORTH LATITUDE (DD MN)	UESSEL'S HEADING (DEGNEES)	UAVE DIRECTION (DEGNEES)	Dudnd Michigan, Drafts 24.25.27.24.5
ATT JALANLAL TIME	LEST I AMGITUDE (DD MN)	USSEL'S DAART (FEET)	UAVE HEIGHT (FEET)	BL 7 8 BL 7 H Acc Out. 5 878

End-of-run messade Foull BIDD DUMATER: 4-7 FT: TE 15105

End-of-run message Fouldwin Gras. 7-4 FT.TT 13124

13158110 25.000 2 50 42 50 86 58 14.3 186 MATE 20-NOU-81 TIME LUKATION OF RUM IN MINUTES IN UVESTICHOTIUNE (DD MH) UVESTICHOTIUNE (DD MH) UVESSEL'S SFEED (MLM - XX,X) 1A UVESSEL'S HEADING (DEGREES) UVESSEL'S HEADING (DEGREES) UVESSEL'S HEATING (DEGREES) UVESSEL'S HEAT POINT REMARKS DM940 MICHIDAN, DKAFTS 24,25,27,26,5 54,7 6 54,7 H ACC OUT: 5 5PB End-of-run sessage FOLL 5133 DUARTER, 6-7FT +11 14103 WV S J COULFALL 'BI TRIALS Ŷ 20 7

23.000 20102140 11 11 2 ņ 13.8 940 045 DATE 05-MOU-BI TIME NURATIGN OF RUN IN NINUTES 18 WORTH LAITUDE (DD MN) WESSEL'S BFTED (MPM - XX,X) UTSSEL'S IN NILMI (NEGREES) UTSEL'S UNNIT (NEGREES) UTSEL'S UNNIT (NEGREES) UTSEL'S UNNIT (NEGREES) UTSEL'S UNNIS) WAVE DIFECTION (DEGREES) UNNIS PEED (NNIS) WAVE FEIGHT (FEET) POINT MV \$ J CORI FALL 'BI TRIALS EUM.

NEWAKKS UPDND MHITEFISH DAY, SHUN TS 11,17,21,5, CODE 1 SL 7, SL7 H ACC, 1 LAIL DEND GUT, 5 8P8

End-of-run arssede HEAB SAES

33.000 REMARKS Dadad acatifical lake michigam (prafts 24, 24 10, 24 7 DL 7 and SL 7 H Acc Out, 5 SPB 5 09149100 10.000 27 345 TATE 08-DEC-81 TINE UURATION OF RUM IN NIMUTES IS NORTH LATITUDE (DD HN) UEST LONGITUDE (DD HN) UEST STAFT (FEET) UITUD DIRECTION (DEGREES) 3 POINT WIND SFEED (MOTB) HAVE DIRECTION (DEGREEB) MAVE HEIGHT (FEET) MAV & J CORT FALL 'BI TRIMS Đ

EN-of-run sessate STBB 504, 11 101115

20.00 01154102 2 2 2 2 2 2 11.5 1041 1 279 HIND BPEED (MOTS) HAVE DIRECTION (BEONLES) HAVE HEIGHT (FEET) H/V S J COKT FALL 'BI TRIALS

NEMMARS Daidand Montherki Lake Michtgam Daafts 24 7, 24 10, 24 BL 7 And BL 7 H Acc Out, 5 595

End-of-run messate STBD DEAN TI 10146

200.L 10103115 22 22 14.1 MATE 08-DEC-01 TIME DURATION OF RUN IN NIMUTES 19 MORTH LANITUME (DB MN) VESSEL SPFED (MM) - XX.X) VESSEL'S HEADING (DE MES) VESSEL'S HEADING (DE ONEES) VESSEL'S DAAFT (FEET) VESSEL'S DAAFT (FEET) VIND SFEED (MADTE) TNIC N/V B J CONT FALL 'BI TRIALS No.

newakks Dnumd morthern lake michigan drafts 24 7, 24 10, 24 BL 7 and BL 7 H acc out, 5 593

End-of-run aessase 8789 JEAN 7111119

23.00 23 **1** 241 DATE 08-DEC-81 TINE DURATION OF RUN IN NIMUTES IS MORTH LATITUDE (DD NN) (LUEST LONGITUTE (DD NN) (LUESTL'S SPTII) (MPN - XX,X) 14 VESSEL'S HEADING (DEGREES) 2 THIO? VESSEL'S DRAFT (FEET) WIND DIRFCTIOM (PEONEED) WIND SFED (KNOTS) -WAVE DIRECTIOM (DEONEED) WAVE HEIGHT (FEET) N/U B J CORT FALL ' BI TRIALS RUN

REMARKS DUPHD MICHIGAN, DRAFTS 23 10, 26 10, 26 BL 7 AND SL 7 M ACC OUT, 5 205

End-of-run aossado BTAD DEAN BTEAN GUARTER TE 14133

23.000 21140171 21140171 22.000 0.147 27 09147144 R 10127145 n 4 20 20 14.1 0 173 0 202 DATE 09-DEC-01 TIME DUPATION OF RUM IN MULTENE DUPATION OF RUM IN MULTENE MARTIN LATITUDE (DD MM) WESEL'S GPEED (MPM) - XX.X) 5 VESSEL'S HEANING (RECOREES) 3 VESSEL'S HEANING (RECOREES) INTE 09-DEC-WI TIME DURATION OF RUM IN MIMUTES IS DURATION OF RUM IN MIMUTES IS DURATION OF RUM IN MIMUTES IS UESSEL'S SPEED (MPH - XX.X) 14 VESSEL'S HEADING (DECHRES) 2 UESSEL'S DAAFT (FEET) UNIND SPEED (MOUTS) UNIND SPEED (MOUTS) UAVE WEIGHT (FEET) POINT TIME OB-DEC-BI TIME DUARTION OF NUM IN NIMUTER IS NORTION OF NUM IN NIMUTER IS NORT LONGTIUPE (DD MN) VESSEL'S BREED (MPH - XX,XX) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) N • POINT POINT NENNIKS Dudna Nichigan: Drifts 23 8, 24 10; 24 81, 7 and 51, 7 h Ac. Out: 5 878 REMARKS Dhand Nichigan, drafts 23 0, 24 10, 24 BL 7 And SL 7 H Acc Out, 5 875 WIND SPEED (KNOTS) WAVE DIRECTION (DEONEES) WAVE HEIGHT (FEET) End-of-run messate 10 BEC NUM TO AVOID VULTADE BPIKE. NAN B J COKT FALL 'BI TRIALS N/N B J CORT FALL 'B' TRINE End-of-run messafe STBD STERN DUARTER ,TT 18100 BLAT BY LAND LAND BY THE BY TH \$ RUN KINI NUN N

3.5 82112101 ĥ ī NUN 49 POINT DATE 09-DEC-01 TIME DURATION OF ALM IN NINUTES IS HORTH LATTULE (DB MN) VESSEL'S BPEES (MPH - XX.X) VESSEL'S HEADING (DEGMEES) 3-VESSEL'S DAAFT (FEET) 3-VESSEL'S DAAFT (FEET) 3-WIND SPEED (KMOTS) MAVE DIRECTION (DEDNETS) MAVE HEIGHT (FEET) REMARKS Outside Burns Hardor SL 7 And SL 7 H Acc Out, 5 995 N/V & J CORT FALL '81 TRIALS

End-of-run messate HEAD BEAB: DRWTIE 25 7: 26 4: 26 3: TI 11122

25.000 4EIOSIOT 41 52 87 50 POINT POINT COPPEC-01 PURATION OF RUN IN NIMUTES IS NORTH LATITURE (DD MN) MEST LONGITURE (DD MN) VESSEL'S PART (FEET) VESSEL'S VART (FEET) VESSEL' ŝ HAVE DIRECTION (DEDREES) HAVE HEIGHT (FEET) H/V S J CORT FALL 'BI TREALS

REMARKS Gutside Durks Hardon GL 7 And SL 7 H Acc Out, 5 **373**

End-of-run messade HEAD SEAS , DRNFTS 25 1 ,26 7, 26 3, TL 12114

22 UNATION OF BEC-B1 DUANTION OF RUM IN NIMUTES IL HORTH LATITUDE (DD MN) UESSEL'S HEADING (DE MES) VESSEL'S HEADING (DE MESS) VESSEL'S DRAFT (FEET) VESSEL'S DRAFT (FEET) 1110 UNVE DIRECTION (DEONETE) OUTSTRE NUMB HANDON BL. 7 AND BL. 7 H ACC OUT: 5 GPS UIND SPEED (KMOTS) N/V S J CORT FALL 'B1 TRIALS WAVE HEIGHT (FEET) RENARKS

SE

<u>ort</u>

WIND DIRECTION (DEONCES) WIND SPEED (NNOTS) JIRECTION (DEBREES)

HAVE DIRECTION (DEI WAVE HEIGHT (FEET)

17 End-of-run mescale HEAD BEAS TI 12150: MANTE 25 1: 24 7: 24

49

End-of-run messale MEAD BEAB 71 10154

REMARKS Outside Burns Handor BL 7 ANB SL 7 H Acc Out, 5 878

37 11140144 25.008 2 5 327 42 J 87 JS 5.1 340 327 NUM CALLEN CONTRACT OF A CONTR FEMARKS OUTSTRE DURNS EMADOR SL. 7 AMB SL. 7 H ACC OUTS 5 5P3 STURE TONE FALL B. THE FALL

End-of-run exeeter HEAB SAEE , R.ANJTE 25 8, 26 4, 24 1, 8PD 4,7 MPH+TE 13147

- 20 23,000 42 5 47 34 4.7 11147120 192 MAVE J CONT FALL 'EL TAIM.B RUN 33 DATE 07-04C-01 DATE 07-04C-01 NUMATION OF RUN 13 HIMUTER 18 NUMATION OF RUN 13 HIMUTER 18 NUMATION OF RUN 12 COD H13 VESSEL'S SHELE (00 H13 VESSEL'S REMARKS DUTGIDE EURNS (MARDOR DL 7 MIG LL 7 H ACC OUT: 5 CP3

End-of the passage HEAD DEAD TE 14117

Š

1112111 Ŧ 42 6 19.9 N 328 350 - 350 ANTE OP-RCL-0: ANTE OP-RCL-0: TINE 1 ANTE OP-RCL-0: TINE 1 CURATIONE COD NAI UNIT ATTIONE (OD NAI) VESSEL 7 SAEID (CEN - XX,X) VESSEL 8 EART (FEL) VESSEL 9 EART (FEL # J CCAT FMLL 'BI TRIALS 24 34

REMAINS CUTSTEE BUXKE MARBOLI SUL 7 AND SL 7 H ACC OUT: 5 4PB

٠, End-of-run bestelk MEAR BEAR TI 14147

20.5 17 12122121 NUM DEFINITION OF NUM IN NUMITED IS DATE OF DEC-UL TIME IS DATE OF DEC UL NUMITED IS NUMITUAL TITTOE OD NUL UESEL'S FRED (1994 - XX.X) 14: UESEL'S HEADING (DEOREES) 14: UNUN BFEED (10015) REMARKS DITELDE DURNE HANDOK BL 7 AND BL 7 H ACC DUTY 3 399 STATE TE TALE TORT TO THE STALE

End-bf-run pessade 9100 BYERN CUARTER TI 15155

052*0 00141112 57 42 47 17 300 3 163 HIN E J CORT FALL ' 11 TAINE

HERRINKS VOLYARE CALS SL 7 AND EL 7 H ACC OUT: 5 573 Enciratorum nessaer NG 6008

21120110 Ģ 10 S NUM 27 FOLMER 2 PATE OF-DEC-01 TIME 2 DATE OF-DEC-01 TIME 2 DATE OF-DEC-01 NHILES IS 02 MEST LONGITUDE (DD NH) 07 MEST LONGITUDE (DD NH) 07 MEST LONGITUDE (DD NH) 14 UESSEL'S HEADING (DEGNEES) 14 UESSEL'S WENT (FET) 14 UESSEL'S WENT (FE) NUMARE Veltage Cals BL 7 and SL 7 A Acc Outs 5 873 STWIRT 18, TTVI INCO F S //H

End-of-run sesate

END THPE

ょ

	ļ	1.1	<i>a</i> 3.1	ንንገ	14		*	
t Maasures	1	Sangara Sangara	ijį	tačni snupe tačni snupe talini snupe		the second print second perime control bet control bet	[febrembeit humperature	
irsions fram Matric	Meltiply by LENGTH		223	AREA 2.0.1 2.0.0.1 2.0.0	11455 (wająkt) 8.836 2.2	VOLUME 0.03 1.06 0.26 0.26 0.26 1.3	IPERATURE (asact 8.5 (asso ast 22)	986 1 1 4 11 10 100
Approximate Canve	When Yos Know	ni i Hensiec a Continuetor a	neter a Reizer Allanzter	Annual Contraction		al IIIIILIAN Al IIIIILIAN Hann Hann Hann Sold, anteo Code, anteo	TEN Celsue Lengunne	+7 + 4 + 6 + 6 + 1 + 1 + 1 + 1 + 1 + 1 + 0 + 1 + 1 + 0 + 1 + 1 + 0 + 1 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0
	Symbol	E 8	£ 1 Š	.	n 2 -	` 1îtî	9	1 1
52	21 23	CT 61	11 TB	• 79 70 	11 12 12 12 1 			
• • • • • • • •		•] • [•] • [•]	, I.	• • • • • • • • • • • • • • • • • • • •			יין יין יין יין יין יין יין יין יין יין	
	7							
	1 1		5 s s .5	ૻ૾ ૺૼૼૼૼ૾ૺૼૼૼ૾૾ૣૼ૾ૺ૱		īīl	_`'eîr •'	т 1 2 ЦК 1 - С
Heerster.	To Find Symbol		continues on on on one of the original of the	tquuera conficientes Poquera conficientes Poquera Pista Poqueta Povita	Repuert Milonates Mil	24111110000 241111110000 241111110000 241111110000 24111110000 24111110000 24111110000 24111110000 241111110000 241111111111	Litera Cubic molers Cubic molers Cubic molers Science moles Cubic molers	Langerelue Kangerelue Lanes, see MS to ic. Publ. 216,
irciana ta Motris Moasuros	Medician by To Find Symb	LENGTH	1.1.6 Canifmatiera Canifmatiera 231 Canifmatiera Canifmatiera 24 Canifmatiera Fa 0.9 matatra Fa 1.5 bitametera Ban	AREA 3.6 equates continuation cond 8.23 equates total 8.3 equate matica	2.8 Aques hilometes hu ² 2.4 beckes hu 155 (waight) 23 gama 0.44 hilogram 0.9 homas fi	VOLUME s s s s s s s s s s s s s s s s s s s	1.0 1100 1100 1100 1100 1100 1100 1100	at starter version sources at 12) 12) 12. Automatical and the set with the c. Publ. 206, 1. Causing May. C13,10.206.
Appierizante Coavartiana la Matric Massures	Websa Yes Keess Makigiy by To Find Symb	LENGTH	inches 2.8 continuetor can ber 21 continuetor can yada 0.9 anatara a actea 1.5 hitometers ba	AREA aquera teches 0.6 square concinence car equare teches 0.0 square tech.	Access axion 2.8 Aquara hilometers har berns 8.4 becauses ha MASS (waight) amera 28 grant hibopane ha berntans 0.64 hibopane ha	(2000 K) Asseptionary Asseptionary Total and and and Part and and and and and and Part and	TEMPERATURE (state)	Hempereture undersching vongeseilung Hempereture undersching kangeseilung 121) uchtigt. Für ober anschlammerum and mas data heter, ene MES Nuc. Publ. 216, and Nuceuret, Pucc 12,25, 50 Causicy Mo. C13,10,206.

METRIC CONVERSION FACTORS

•