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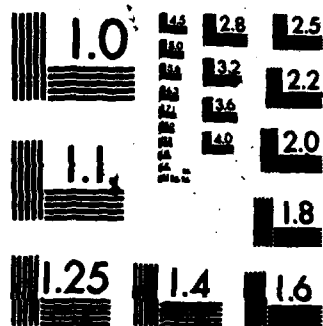
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## THERMAL CONDUCTIVITY OF TEN SELECTED BINARY ALLOY SYSTEMS

By

C. Y. Ho, M. W. Ackerman, K. Y. Wu, S. G. Oh, and T. N. Havill

CINDAS-TPRC Report 30

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## PREFACE

This technical report was prepared by the Thermophysical Properties Research Center (TPRC) of the Center for Information and Numerical Data Analysis and Synthesis (CINDAS), Purdue University, West Lafayette, Indiana, under the auspices of the Office of Standard Reference Data of the National Bureau of Standards (NBS), Department of Commerce, Washington, D.C. It represents the most exhaustive review and critical evaluation of the recorded world knowledge on the thermal conductivity of ten selected binary alloy systems, and is a continuation of a similar work on the thermal conductivity of the elements already published. The recommended self-consistent thermal conductivity values presented in this report cover the full ranges of composition and temperature for most of the alloy systems and go far beyond the limited experimental data, which are often conflicting and uncertain in many cases. Thus, new knowledge has been generated in this process of data analysis and synthesis.

This report serves many purposes. It provides engineering and design data for virtually all compositions of the ten alloy systems for industrial applications. It provides reliable data for those alloys that can be used as reference materials to check apparatus for thermal conductivity measurements or as standards in comparative thermal conductivity measurements. It provides reliable data against which theoreticians can test their theories. Furthermore, the knowledge of the thermal conductivity of binary alloy systems is essential for the study and estimation of the thermal conductivity of ternary and more complex engineering alloys. A reliable method for the calculation of the thermal conductivity of binary alloys has also been developed in this work, which will have wide applications.

Although this report is primarily the result of financial support and interest of the NBS Office of Standard Reference Data, the extensive documentary activity essential to this work was supported by the Defense Supply Agency of the Department of Defense. Throughout the course of this work, Dr. P. G. Klemens, who is a Visiting Research Professor at CINDAS and Professor of Physics at the University of Connecticut, has given the staff of this project invaluable technical guidance and advice; his contributions are hereby gratefully acknowledged. Thanks are also due Dr. H. J. White, Jr., of the NBS Office of Standard Reference Data for his sympathetic understanding and help in many ways and to Dr. D. L. McElroy of the Oak Ridge National Laboratory for useful comments and discussions.

**Y. S. TOULOUKIAN**

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## ABSTRACT

This work presents and discusses the available data and information on the thermal conductivity of ten selected binary alloy systems and contains the recommended reference values (or provisional or typical values) resulting from critical evaluation, analysis, and synthesis of the available data and information. The ten binary alloy systems are the systems of aluminum-copper, aluminum-magnesium, copper-gold, copper-nickel, copper-palladium, copper-zinc, gold-palladium, gold-silver, iron-nickel, and silver-palladium. The recommended (or provisional or typical) values given include the total thermal conductivity, electronic thermal conductivity, and lattice thermal conductivity. The values for each of the alloy systems except two are given for 25 alloy compositions: 0.5, 1, 3, 5, 10(5)95, 97, 99, and 99.5%. For most of the alloy compositions, the values cover the temperature range from cryogenic temperature to the solidus point or 1200 K. In addition, reliable methods for the estimation of the electronic and lattice thermal conductivities of alloys have been developed in this work.

**Key words:** Alloys; conductivity; critical evaluation, data analysis; data compilation; data synthesis; electrical resistivity; metals; reference data; thermal conductivity; thermoelectric power.

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## NOMENCLATURE

$a$	Lattice constant
$e$	Electronic charge; Base of natural logarithm (2.71828)
$E$	Electron energy
$E_{\vec{k}}$	Energy of electron in $\vec{k}$ th state
$f(\vec{k})$	Distribution function representing the number of carriers in $\vec{k}$ th state
$f^0$	Fermi-Dirac distribution function at equilibrium
$\hbar$	Reduced Planck constant
$I_a, I_b, I_c$	Transport integrals
$I_n$	Modified transport integrals
$J_n$	Standard transport integrals
$k$	Total thermal conductivity
$k_e$	Electronic thermal conductivity
$k_{ei}$	Intrinsic electronic thermal conductivity
$k_g$	Lattice thermal conductivity
$k_u$	Lattice thermal conductivity of a virtual crystal
$\vec{k}$	Electron wave vector
$K$	Kelvin temperature unit
$K_n$	Electronic transport integrals
$L$	Lorenz function
$L_0$	Lorenz number ( $2.443 \times 10^{-8} \text{ V}^2 \text{ K}^{-2}$ )
$M$	Average atomic mass
$M_H$	Atomic mass of the heavier element
$M_L$	Atomic mass of the lighter element
$n$	Number of conduction electrons per atom
$S$	Absolute thermoelectric power
$T$	Temperature
$v$	Speed of sound
$v(E)$	Electron velocity in spherical symmetry

$v(\vec{k})$	Velocity of electron in $\vec{k}$ th state
$V$	Average atomic volume
$V_H$	Atomic volume of the heavier element
$V_L$	Atomic volume of the lighter element
$W_e$	Electronic thermal resistivity
$W_{ei}$	Intrinsic electronic thermal resistivity
$W_{eo}$	Residual electronic thermal resistivity
$W_{Hi}$	Contribution to $W_{ei}$ of electrons moving parallel to the Fermi surface
$W_{Vi}$	Contribution to $W_{ei}$ of electrons moving perpendicular to the Fermi surface
$\Delta W$	Deviation from thermal analog of Matthiessen's rule
$x$	Reduced phonon frequency
$x_0$	Reduced phonon frequency at which the relaxation times for point-defect scattering and U-processes are equal
$y$	Atomic fraction of the solute
$y_H$	Atomic fraction of the heavier element
$y_L$	Atomic fraction of the lighter element
$\alpha$	Ratio of reciprocal relaxation times for N- and U-processes
$\beta$	Impurity-imperfection parameter of elements
$\gamma$	Grüneisen parameter
$\epsilon$	Quantity characterizing the perturbation due to mass defects and lattice distortion
$\zeta$	Fermi energy
$\eta$	Reduced electron energy
$\theta$	Debye temperature
$\kappa$	Boltzmann constant
$\mu$	Ferromagnetic ordering parameter
$\rho$	Total electrical resistivity
$\rho^*$	Resistivity of ferromagnetic metal in the absence of ferromagnetic ordering
$\rho_0$	Residual electrical resistivity
$\rho_1$	Intrinsic electrical resistivity

$\Delta\rho$	Deviation of electrical resistivity from Matthiessen's rule
$\tau(\vec{k})$	Relaxation time for electron in $\vec{k}$ th state
$\tau(E)$	Relaxation time for electron with energy $E$ in spherical symmetry
$\tau_c$	Combined relaxation time
$\tau_N$	Relaxation time for N-processes
$\tau_p$	Relaxation time for point-defect scattering
$\tau_U$	Relaxation time for U-processes
$\omega$	Frequency of lattice wave
$\omega_0$	Phonon frequency at which the relaxation times for point-defect scattering and U-processes are equal

## 1. INTRODUCTION

The primary objective of this study was to critically evaluate, analyze, and synthesize all the available data and information on the thermal conductivity of ten selected binary alloy systems and to generate recommended reference data over the widest practicable ranges of temperature and alloy composition for each of the alloy systems. It will become evident that for most of these alloy systems there are serious gaps in the thermal conductivity data, as concerns dependence on composition or temperature, or both, and that most of the available data show large uncertainties or wide divergences. It has, therefore, been necessary to set other objectives: (1) to develop reliable methods for the estimation of the thermal conductivity of alloys, (2) to determine the extent to which the methods of data estimation developed in this study are applicable in general, and (3) to identify those areas where further theoretical and experimental research is needed.

The ten alloy systems selected for this study are the systems with the largest amount of experimental data among some 200 alloy systems for which thermal conductivity data are available. This selection of alloy systems with the largest amount of experimental data is necessary since data evaluation is possible only when data are available and the availability of fairly sufficient data for an alloy system is prerequisite for detailed data analysis, correlation, and synthesis.

The systems selected represent all three different kinds of binary alloy systems: non-transition-metal and nontransition-metal systems (aluminum-copper, aluminum-magnesium, copper-gold, copper-zinc, and gold-silver), nontransition-metal and transition-metal systems (copper-nickel, copper-palladium, gold-palladium, and silver-palladium), and a transition-metal and transition-metal system (iron-nickel). The inclusion of this wide range of alloy systems in this study has tested the broad applicability of the methods developed for data estimation and synthesis.

The methods developed for the estimation of the thermal conductivity of alloys are detailed in Section 2. These methods have been extensively tested with key sets of reliable experimental data. In Section 3 the procedures for data evaluation and for the generation of recommended values are outlined, including the procedures for data estimation using the methods detailed in Section 2.

The recommended (or provisional) values for the total thermal conductivity, electronic thermal conductivity, and lattice thermal conductivity and the original experimental data for the thermal conductivity of the ten selected binary alloy systems are reported in Section 4, together with a discussion of each system, reviewing individual pieces of available data and information, giving details of data analysis and synthesis, and discussing the considerations involved in arriving at the final assessment and recommendations. For each

of the alloy systems except two (aluminum-magnesium and copper-zinc), the recommended (or provisional) thermal conductivity values are given for 25 alloy compositions: 0.5, 1, 3, 5, 10(5)95, 97, 99, and 99.5%, which greatly facilitates the interpolation of values for alloys with intermediate compositions. These values are for well-annealed disordered alloys.

The complete bibliographic citations for the 184 references are given in Section 6.

## 2. THEORETICAL BACKGROUND

In metals and alloys the principal carriers of thermal energy are electrons and lattice waves, and it is commonly assumed that the total thermal conductivity is

$$k = k_e + k_g \quad (1)$$

where  $k_e$  is the electronic thermal conductivity and  $k_g$  is the lattice thermal conductivity; these are the thermal conductivity components due to the transport of heat by the electrons and by the lattice waves or phonons, respectively.

In pure normal metals, conduction by lattice waves is negligible in comparison with conduction by electrons at all temperatures, but in alloys the lattice component is often comparable to and sometimes even greater than the electronic component at low temperatures and is not negligible even at temperatures well above the Debye temperature in some cases. Hence, in order to estimate the thermal conductivity of an alloy it is necessary to estimate both the electronic and lattice components. Since the principal thermal resistance mechanisms differ in different temperature regions, it is necessary to devise different methods for making predictive estimates in different temperature regions. In the course of developing these methods a number of specific areas in which further experimental and theoretical studies are needed were identified.

### 2.1. Electronic Thermal Conductivity

In alloys at temperatures below about 25 K the only significant contribution to the electronic thermal resistivity,  $W_e$ , is the scattering of electrons by solute atoms, so that the electronic thermal conductivity may be calculated from the Wiedemann-Franz-Lorenz relationship,

$$k_e = \frac{1}{W_e} \approx \frac{1}{W_{e0}} = \frac{L_0 T}{\rho_0} \quad (2)$$

where  $W_{e0}$  is the residual electronic thermal resistivity due to impurity scattering of electrons,  $\rho_0$  is the residual electrical resistivity,  $T$  is the temperature, and  $L_0$  is the classical theoretical Lorenz number and has a value of  $2.443 \times 10^{-8} \text{ V}^2 \text{ K}^{-2}$ .

At higher temperatures the scattering of electrons by lattice waves becomes significant. At temperatures between about 25 K and 100 K the electronic thermal resistivity has commonly been estimated from the thermal analog of Matthiessen's rule,

$$W_e = W_{e0} + W_{ei} = \rho_0 / L_0 T + W_{ei} \quad (3)$$

where  $W_{ei}$  is the intrinsic electronic thermal resistivity, which is the reciprocal of the intrinsic electronic thermal conductivity,  $k_{ei}$ , of the "parent" element, and Matthiessen's



rule states that the electrical resistivity is composed of a residual and an intrinsic component:

$$\rho = \rho_0 + \rho_1 \quad (4)$$

Equation (3) is based on the assumption that the deviations from Matthiessen's rule,  $\Delta\rho = \rho - \rho_0 - \rho_1$ , and its thermal analog,  $\Delta W = W_e - W_{e0} - W_{e1}$ , can be neglected. This is not the case at higher temperatures;  $\Delta\rho$  and  $\Delta W$  may be significant even at temperatures below 100 K. These deviations may be taken into account by assuming that they are related by the Wiedemann-Franz-Lorenz law:  $\Delta\rho/\Delta W = LT$ , where  $L$  is the Lorenz ratio which may or may not be equal to  $L_0$ . This assumption is based on an argument by Klemers [1] \* which may be summarized as follows.

The intrinsic electrical and thermal resistivities arise from interactions between electrons and phonons which take electrons from regions of momentum space where there are too many into regions where there are too few electrons relative to the equilibrium concentration. Since the phonon energies are relatively small, the electron energies are little changed by these interactions, and their initial and final states must both lie near the Fermi surface.

In the case of electrical conduction the deviation of the distribution function from the equilibrium distribution due to the electric field is proportional [2] to a function,  $f(\vec{k})$ , of the direction of the electron wave vector, the sign of the deviation depending on the direction of the electron wave vector. The intrinsic electrical resistivity,  $\rho_1$ , is the result of the motion of electrons in  $\vec{k}$  space through interactions with phonons to distant regions of the Fermi surface, involving substantial changes in the direction of  $\vec{k}$ , which is a "horizontal" movement on the Fermi surface.

In the case of thermal conduction, the deviation from the electronic equilibrium distribution due to the temperature gradient is proportional to the same function  $f(\vec{k})$  of the direction of the electron wave vector but it is also proportional to the reduced electron energy,  $\eta = (E - \zeta)/KT$ ,  $E$  being the electron energy,  $\zeta$  the Fermi energy, and  $K$  the Boltzmann constant. Thus the sign of the deviation of the distribution function can be changed not only by "horizontal" movement on the Fermi surface but also by changing the sign of  $\eta$ , which is a "vertical" movement through the Fermi surface. These motions in  $\vec{k}$  space contribute approximately additively to the intrinsic electronic thermal resistivity:  $W_{e1} \approx W_{H1} + W_{V1}$ . Since  $f(\vec{k})$  is the same for electrical and thermal conduction, horizontal movement is equally effective in both cases, so that  $\rho_1$  and  $W_{H1}$  are related by the Wiedemann-Franz-Lorenz law. Now  $W_{V1}$  depends on a local property of the Fermi surface and is, therefore, relatively insensitive to changes in the band structure due to alloying. On the other hand  $W_{H1}$ ,

\* Numbers in brackets designate references listed in Section 6.

being due to motion of the electrons over large distances on the Fermi surface, is sensitive to changes in its overall shape, particularly when these changes involve contact with the zone boundary which effectively short circuits the horizontal movement. Hence the change in  $W_{H1}$  on alloying is much larger than the change in  $W_{V1}$  and makes the dominant contribution to the deviations from Matthiessen's rule. Thus, to a good approximation, the deviations from Matthiessen's rule and its thermal analog are related by the Wiedemann-Franz-Lorenz law,

$$W_e = (\rho - \rho_1)/LT + W_{ei} \quad (5)$$

or

$$k_e = \frac{1}{(\rho - \rho_1)/LT + W_{ei}} \quad (6)$$

In applying eq. (6),  $W_{ei}$  and  $\rho_1$  are taken to be the intrinsic thermal and electrical resistivities of the virtual crystal obtained by interpolating between the values for the elements, linearly for alloys of ordinary metals and according to Mott's theory [3,4] for alloys containing transition elements. For most alloys  $W_{ei}$  is much smaller than the other term in eq. (6) so that the error introduced in common practice by taking  $W_{ei}$  of the elements to be the reciprocals of their total thermal conductivities is also small. However, in dilute alloys of elements which do not have electronic thermal conductivities comparable to those of the noble elements this error is significant, and  $W_{ei}$  is therefore calculated in this work from the expression

$$W_{ei} = \frac{1}{k_{ei}} = \frac{1}{k_e} - \frac{\beta}{T} = \frac{1}{k - k_g} - \frac{\beta}{T} \quad (7)$$

where  $\beta$  is the impurity-imperfection parameter of the element. The values of  $k$  and  $\beta$  of the elements are available from ref. [5] \* and the values of  $k_g$  of an element at moderate and high temperatures are calculated from eq. (36). The values of electrical resistivities of the ten selected binary alloy systems and their nine constituent elements used in eq. (6) are available from ref. [7].

From the argument leading to eq. (6) it is clear that the value of  $L$  used therein should be that for horizontal motion on the Fermi surface, or for elastic scattering; the values of  $L$  appropriate for use in eq. (6) and in the Wiedemann-Franz-Lorenz law, which one might expect to be valid at high temperatures where phonons scatter electrons through large angles, are discussed below.

It should be noted that eq. (6) may not be valid in some cases. If the deviations from Matthiessen's rule are due to the fact that two bands of electrons, such as those on

\* The recommended values for the thermal conductivities of the elements given in ref. [5] in some cases are slightly different from those given in ref. [6], and the values given in ref. [5] are preferred and should be used whenever there is a difference.

the neck and belly regions of the Fermi surface, contribute significantly to the electrical conduction, then, in general, the deviations from Matthiessen's rule and its thermal analog are not related by the Wiedemann-Franz-Lorenz law.

Significant deviations of the Lorenz ratio from its classical value can result from band structure effects and from electron-electron scattering.

The possibility of deviations due to band structure effects and the difficulties they present may be seen from the following. Assuming the existence of a relaxation time, the electronic transport properties can be expressed through integrals over reciprocal space of the form

$$K_n = -\frac{1}{3} \iiint v^2(\vec{k}) \tau(\vec{k}) (E_{\vec{k}} - \zeta)^n \frac{\partial f^0}{\partial E_{\vec{k}}} d^3\vec{k} \quad (8)$$

which for spherical symmetry [182] reduces to

$$K_n = \frac{1}{12\pi^3 \hbar} \int_{-\infty}^{\infty} v(E) \tau(E) (E - \zeta)^n \frac{\partial f^0}{\partial E} dA dE \quad (9)$$

Here  $\hbar$  is the reduced Planck constant,  $v$  is the electron velocity,  $\tau$  is the relaxation time,  $E$  is the electron energy,  $f^0$  is the Fermi-Dirac distribution function,  $\zeta$  is the Fermi energy, and  $dA$  is an element of a constant energy surface in reciprocal space. In particular, the absolute thermoelectric power is given by

$$S = \frac{1}{eT} \frac{K_1}{K_0} \quad (10)$$

and the Lorenz ratio by

$$L = \frac{1}{e^2 T^2} \left[ \frac{K_2}{K_0} - \frac{K_1^2}{K_0^2} \right] = \frac{1}{e^2 T^2} \frac{K_2}{K_0} - S^2 \quad (11)$$

Because of the factor  $\partial f^0 / \partial E$ , the only significant contributions to these integrals are from energies differing from  $\zeta$  by no more than  $\kappa T$ , where  $\kappa$  is the Boltzmann constant, so that the usual procedure is to expand each integrand in a Taylor series about  $\zeta$ . Retaining only the leading term of the series leads to the result  $L = L_0 - S^2$ , where  $L_0$  is the classical theoretical Lorenz number. The values of  $L$  obtained from this result are used in eq. (6) to give the equation employed in our calculations:

$$k_e = \frac{1}{\frac{p - p_1}{(L_0 - S^2) T} + W_{el}} \quad (12)$$

The values of absolute thermoelectric powers of the ten selected binary alloy systems used in eq. (12) are available from ref. [40].

There is some question about the choice of  $L_0$  in the case of transition-element alloys. The difficulties occur also in the treatment of the pure transition metals, and will be reviewed briefly in that context.

If, as in the case of some transition metals, a narrow band with a high density of states overlaps the conduction band at the Fermi energy, then at high temperatures it is necessary to include higher order terms in the series and this will cause a deviation of the Lorenz ratio from the classical value. It is possible, at least in principle, to evaluate the second order terms from the thermoelectric power and the series expansion for the electrical conductivity (see Williams and Fulkerson, 1969 [8, pp. 443-7]). However, if the relaxation time is a strong function of energy, as is the case in transition metals on the assumption [9] that it may be written as the reciprocal of the product of the density of states and a scattering probability per unit time, then a Taylor series expansion about  $\zeta$  may not be adequate to represent the integrand over the energy range  $kT$  at high temperatures. In such cases the integrals must be evaluated numerically. This has been done for Pd [10] and reasonable agreement between theory and experiment was obtained; the discrepancies were presumably due to electron-electron scattering [11, p. 412] which occurs in both ordinary and transition metals. In ordinary metals, normal electron-electron scattering, in which electron quasi-momentum is conserved, contributes to the thermal resistivity but not to the electrical resistivity and thus causes a negative deviation of the Lorenz ratio. Such a deviation has been observed in Cu [12, 13]. In transition metals normal electron-electron interactions between s and d band electrons contribute to the electrical resistivity as well as to the thermal resistivity; these processes are very strong [14, 15] and are generally thought to be responsible for the  $T^2$  temperature dependence of the electrical resistivity observed in these metals at low temperatures. The deviation of the Lorenz ratio due to electron-electron scattering may either enhance or partially cancel the effects of band structure. The latter appears to be the case in the group VIII elements [16]. The deviations of the Lorenz ratio of transition metals due to band structure effects are significant and cannot yet be calculated directly; further, in order to calculate correlations between the electrical resistivity and the Lorenz ratio, the density of states function of the material must be known and there are difficulties in including the effects of electron-electron scattering in such an analysis.

The Wiedemann-Franz-Lorenz law is valid in alloys at very low temperatures where one need consider only impurity scattering, and in both metals and alloys at high temperatures where phonons scatter electrons through large angles. Equation (12) was developed in order to calculate the electronic component at intermediate temperatures. However,

as is clear from the preceding discussion, in the case of transition-metal alloys there is considerable uncertainty about the values of the Lorenz ratio to be used in the Wiedemann-Franz-Lorenz law at high temperatures. The method tried was to interpolate for the deviation from the classical value on the basis of the questionable assumption that the net deviation resulting from band structure effects and s-d electron-electron scattering is proportional to the number of holes in the d band. It was found that in the Cu-Ni system the resulting values of  $k_e$  nowhere differed from those obtained from eq. (12) by more than 5 percent and it was decided to use eq. (12) over the entire temperature range above 25 K.

In view of the uncertainties associated with eq. (12), it is reassuring that the values obtained from it have been found to be in good agreement with the values of the electronic component obtained from experimental values of thermal conductivity considered to be reliable on the basis of the usual criteria.

While a considerable amount of effort has been concentrated on the study of deviations from Matthiessen's rule, far less attention has been given to their relation to the deviations from its thermal analog [1,17,18]. Work in this area is hindered by the failure of many authors to include the corresponding electrical resistivity data when reporting thermal conductivity values. Further work in this area would help to determine the limitations of eq. (12) and very probably lead to improvements on it.

## 2.2. Lattice Thermal Conductivity

The processes limiting lattice conduction are different in the temperature regions below, about, and above the temperature at which it has its maximum value. At very low temperatures, typically below one twentieth of the Debye temperature,  $\theta$ , these are the ordinary and impurity-induced electron-phonon interactions and, in strained specimens, phonon scattering by dislocations. These processes are also important in the temperature range in which the lattice component has its maximum value, typically between  $\theta/20$  and  $\theta/5$  for alloys of ordinary metals but considerably higher for some transition elements, but in this region point-defect scattering and three-phonon anharmonic interactions also contribute to the thermal resistivity. At temperatures above this region the important resistive processes in alloys of ordinary metals are three-phonon anharmonic interactions and point-defect scattering; in alloys containing transition metals the effect of electron-phonon interactions may also be significant in the lower portion of this temperature range. This third region is the only one in which it is possible to estimate the lattice component on the basis of present theory.

### a. Low Temperature Region

The problem of calculating the coupling constant for the electron-phonon interaction is a very difficult one even in the simplest cases; in fact, measurements of low temperature

alloy thermal conductivity were initially undertaken to obtain information about this interaction. From results reported by Lindenfeld and Pennsbaker [19] for Cu alloys it appeared that it might be possible to estimate the lattice component from electrical resistivity data on the basis of present theory. This did not prove to be the case. It was found that values obtained from an expression which follows from the equations in ref. [19] differed from those obtained from measurements by as much as a factor of three. It is almost certain that these discrepancies are largely the result of the use of Pippard's early results [20] which are based on the free electron model; this simple model is inadequate for most metals and alloys.

At temperatures below  $\theta/20$ , the lattice thermal conductivity of a pure ordinary metal may be calculated from an expression derived by Klemens [21]

$$k_g = \frac{313 k_{ei} T^4}{n^{4/3} \theta^4} \quad (13)$$

where  $n$  is the number of conduction electrons per atom,  $\theta$  is the Debye temperature, and  $k_{ei}$  is the intrinsic electronic thermal conductivity. Since in this region  $k_{ei}$  is inversely proportional to  $T^2$ ,  $k_g$  has a  $T^2$  temperature dependence. Equation (13) is based on the assumption of a reciprocal effect of the electron-phonon interaction on electronic and lattice conduction and therefore does not apply to transition elements in which electron-phonon interactions involving only  $d$  band electrons have little effect on electrical conductivity but may have a significant effect on lattice conduction. It also does not apply to alloys in which the electron mean free path is so short that the usual treatment of the electron-phonon interaction is invalid; typically, these are alloys in which the residual resistivity is  $10 \mu\Omega \text{ cm}$  or greater.

However, if one attempts to estimate the  $k_g$  of an alloy from this expression the value obtained is greater than the experimental value by a factor which increases rapidly with solute concentration up to approximately 10 atomic percent. A possible explanation of this behavior is that it is due to phonon scattering by dislocations which are so strongly anchored by solute atoms that they remain even after prolonged annealing at high temperatures. The experimental support for this idea is some recent measurements on Cu-Al alloys at the University of Connecticut [22] which show that such behavior is not observed at temperatures below about 0.5 K, where the dominant phonon wavelengths are larger than the range of the dislocation strain fields so that scattering by dislocations is greatly reduced [23].

Consequently, at present one cannot make reliable estimates of the  $k_g$  of alloys at low temperatures and it must be obtained by subtracting  $k_g$  from the measured total thermal conductivity. Further, one can obtain reliable values of the  $k_g$  from thermal conductivity measurements only in those cases in which the corresponding values of electrical resistivity

are given, as there is often a significant variation in the resistivities of specimens having the same nominal composition. It is unfortunate that while there is a sizable body of experimental data showing strong composition dependence of the low-temperature thermal conductivity of alloys, in most cases the corresponding values of the electrical resistivity are not reported, so that it is not possible to relate the changes in the two quantities. Finally, in view of the probability that residual dislocations are responsible for a large portion of the thermal resistivity, one cannot reliably extrapolate curves of the lattice component down to temperatures below about 1.5 K.

In order to make it possible to estimate the lattice component at low temperatures by other than empirical means, it is necessary to develop both a quantitative theory of impurity enhancement of the phonon scattering in alloys of ordinary metals and a theory of low temperature lattice conduction in transition element and high residual resistivity alloys. It seems that progress in these directions will involve the use of Pippard's more general equations [24] which apply to a non-spherical Fermi surface, taking into account changes in its shape with the addition of solutes. However, application of this theory to transition metals presents a difficult problem. Since electrical conduction is mainly by s band electrons, the residual resistivity is a measure of the mean free path of the s electrons and provides no information about the mean free path of the d band holes, which is probably very short.

#### b. Intermediate Temperatures

At temperatures near the maximum of the lattice component the resistive processes which limit lattice conduction at lower and higher temperatures are comparable in magnitude and the problem of estimating the lattice component in this region is a formidable one. It is, first, because of the difficulties associated with the electron-phonon interaction discussed above and, secondly, because the treatment of the resistive three-phonon anharmonic interaction in this region is complicated by the fact that here the strength of these interactions is a rapidly varying function of temperature.

At present there is no method available for the calculation of  $k_g$  in this temperature region. In this work the values of  $k_g$  in this region are derived from experimental data and the calculated values of  $k_e$ .

#### c. High Temperature Region

At temperatures above the region of the maximum of the lattice component, typically  $\theta/5$  for alloys of ordinary metals but considerably higher for some transition-element alloys, it is possible to estimate the lattice thermal conductivity on the basis of a theory developed by Klemens [25] and Callaway [26] assuming that the effect of the electron-phonon interaction can be neglected; this is not the case for some transition elements in the lower portion of this temperature range.

The reciprocal relaxation time for the thermally resistive three-phonon anharmonic interactions, U-processes, at frequencies not too close to the Debye limit is of the form  $BT \omega^2$  where  $B$  is a constant determined from experiment,  $T$  is the temperature, and  $\omega$  is the frequency of the lattice wave. The reciprocal relaxation time for point-defect scattering is of the form  $(a^3/4\pi v^3) \epsilon \omega^4$  where  $a^3$  is the average volume per atom,  $v$  is the speed of sound, and  $\epsilon$  is a quantity which characterizes the perturbation due to mass defects and distortions of the lattice. In addition, there are three-phonon anharmonic interactions, N-processes, which do not contribute directly to the thermal resistivity but do contribute indirectly by redistributing energy from the low frequency modes to the high frequency modes which are strongly scattered by the point defects. The reciprocal relaxation time for N-processes has the same form as that for the U-processes and, as argued by Klemens, et al. [27], appears to have approximately the same magnitude in this temperature region.

Since N-processes do not contribute directly to the thermal resistivity, the effective total reciprocal relaxation time is not simply the sum of the individual reciprocal relaxation times. Callaway devised a formalism in which the N-processes are taken into account correctly for steady state lattice conduction.

Callaway found that the lattice thermal conductivity is given by

$$k_g = \frac{\kappa}{2\pi^2 v} \left( \frac{\kappa T}{\hbar} \right)^3 \left( I_a + \frac{I_b^2}{I_c} \right) \quad (14)$$

where

$$I_a = \int_0^{\theta/T} \tau_c \frac{x^4 e^x}{(e^x - 1)^2} dx \quad (15)$$

$$I_b = \int_0^{\theta/T} \frac{\tau_c}{\tau_N} \frac{x^4 e^x}{(e^x - 1)^2} dx \quad (16)$$

$$I_c = \int_0^{\theta/T} \frac{1}{\tau_N} \left( 1 - \frac{\tau_c}{\tau_N} \right) \frac{x^4 e^x}{(e^x - 1)^2} dx \quad (17)$$

and  $\kappa$  and  $\hbar$  are the Boltzmann constant and the reduced Planck constant,  $v$  is the speed of sound, and  $x = \hbar\omega/\kappa T$  is the reduced phonon frequency. Here  $\tau_c$  is a combined relaxation time, obtained as the reciprocal of the sum of the reciprocal relaxation times for the various interactions,  $\tau_N$  is the relaxation time for N-processes, and the term  $I_b^2/I_c$  occurs because of the difference between  $\tau_c$  and the effective total relaxation time resulting from the fact that N-processes do not contribute directly to the thermal resistivity.

Writing the reciprocal relaxation times for point-defect scattering, U-processes and N-processes as  $\tau_p^{-1} = A\omega^4$ ,  $\tau_u^{-1} = BT \omega^2$ , and  $\tau_N^{-1} = \alpha BT \omega^2$  respectively, where  $\alpha$



is the temperature-independent ratio of reciprocal relaxation times for N- and U-processes, the reciprocal combined relaxation time when the lattice thermal conductivity is limited by these interactions is

$$\tau_c^{-1} = \omega^2 [A\omega^2 + BT (1+\alpha)] \quad (18)$$

so that

$$\frac{\tau_c}{\tau_N} = \frac{\alpha BT}{A\omega^2 + BT (1+\alpha)} \quad (19)$$

and

$$\frac{1}{\tau_N} \left(1 - \frac{\tau_c}{\tau_N}\right) = \alpha BT \omega^2 \left(1 - \frac{\alpha BT}{A\omega^2 + BT (1+\alpha)}\right) = \frac{\alpha BT \omega^2 (A\omega^2 + BT)}{A\omega^2 + BT (1+\alpha)} \quad (20)$$

Upon denoting the frequency at which the reciprocal relaxation times for point-defect scattering and U-processes are equal by  $\omega_0$ , noting that  $\omega_0^2 = BT/A$ , and introducing the reduced frequency  $x = \hbar \omega / \kappa T$ , so that  $x_0 = \hbar \omega_0 / \kappa T$ , these relations become:

$$\tau_c^{-1} = BT \omega^2 (1 + \alpha + \omega^2/\omega_0^2) = BT \left(\frac{\kappa T}{\hbar}\right)^2 x^2 (1 + \alpha + x^2/x_0^2) \quad (21)$$

$$\frac{\tau_c}{\tau_N} = \frac{\alpha}{1 + \alpha + \omega^2/\omega_0^2} = \frac{\alpha}{1 + \alpha + x^2/x_0^2} \quad (22)$$

and

$$\frac{1}{\tau_N} \left(1 - \frac{\tau_c}{\tau_N}\right) = \frac{\alpha BT \omega^2 (1 + \omega^2/\omega_0^2)}{1 + \alpha + \omega^2/\omega_0^2} = \alpha BT \left(\frac{\kappa T}{\hbar}\right)^2 x^2 \frac{(1 + x^2/x_0^2)}{1 + \alpha + x^2/x_0^2} \quad (23)$$

Thus, for the present case, eqs. (15) to (17) become:

$$\begin{aligned} I_a &= \left(\frac{\hbar}{\kappa T}\right)^2 \frac{1}{BT} \int_0^{\theta/T} \frac{x^2 e^x dx}{(e^x - 1)^2 (1 + \alpha + x^2/x_0^2)} \\ &= \left(\frac{\hbar}{\kappa T}\right)^2 \frac{1}{(1 + \alpha) BT} \int_0^{\theta/T} \frac{x^2 e^x dx}{(e^x - 1)^2 \left[1 + \frac{x^2}{x_0^2 (1 + \alpha)}\right]} \\ &= \left(\frac{\hbar}{\kappa T}\right)^2 \frac{1}{(1 + \alpha) BT} I_2 (\theta/T) \end{aligned} \quad (24)$$

$$I_b = \alpha \int_0^{\theta/T} \frac{x^4 e^x dx}{(e^x - 1)^2 (1 + \alpha + x^2/x_0^2)} = \frac{\alpha}{(1 + \alpha)} I_4 (\theta/T) \quad (25)$$

$$\begin{aligned} I_c &= \left(\frac{\kappa T}{\hbar}\right)^2 \alpha BT \int_0^{\theta/T} \frac{x^6 e^x (1 + x^2/x_0^2) dx}{(e^x - 1)^2 (1 + \alpha + x^2/x_0^2)} \\ &= \left(\frac{\kappa T}{\hbar}\right)^2 \frac{\alpha BT}{(1 + \alpha)} \left[ I_6 (\theta/T) + \frac{I_8 (\theta/T)}{x_0^2} \right] \end{aligned} \quad (26)$$

Substituting eqs. (24) to (26) into eq. (14) yields

$$k_g = \frac{\kappa^2}{[2\pi^2 \hbar v (1 + \alpha) B]} \left[ I_2 (\theta/T) + \frac{\alpha I_4^2 (\theta/T)}{I_6 (\theta/T) + I_8 (\theta/T)/x_0^2} \right] \quad (27)$$

where  $I_n (\theta/T)$  is the modified transport integral given by

$$I_n (\theta/T) = \int_0^{\theta/T} \frac{x^n e^x dx}{(e^x - 1)^2 \left[ 1 + \frac{x^2}{x_0^2 (1 + \alpha)} \right]} \quad (28)$$

and  $x_0$  is the reduced frequency at which the reciprocal relaxation times for U-processes and point-defect scattering are equal; that is (see eq. (32))

$$x_0 = \hbar \omega_0 / \kappa T = \frac{\hbar}{\kappa} \sqrt{\frac{4\pi v^3 B}{a^3 \epsilon T}} \quad (29)$$

Equation (27) is for the lattice thermal conductivity as limited by both point-defect scattering and three-phonon anharmonic interactions. In the limit of vanishing point-defect scattering, when the thermal conductivity is limited by three-phonon anharmonic interactions only (denoted by  $k_u$ ),  $x_0$  becomes infinite so that the modified transport integral  $I_n (\theta/T)$  reduces to the standard transport integral  $J_n (\theta/T)$  and eq. (27) reduces to

$$k_u = \frac{\kappa^2}{[2\pi^2 \hbar v (1 + \alpha) B]} [J_2 (\theta/T) + \alpha J_4^2 (\theta/T) / J_6 (\theta/T)] \quad (30)$$

where

$$J_n (\theta/T) = \int_0^{\theta/T} \frac{x^n e^x dx}{(e^x - 1)^2} \quad (31)$$

$k_L$  is the high-temperature lattice thermal conductivity of an isotopically pure element; in the case of an alloy it is the lattice thermal conductivity of an idealized "virtual" crystal in which each atom has the same average mass and volume of the alloy. Point defect scattering is that scattering which results from the fact that the actual atoms do not have these masses and volumes.

The quantity  $\epsilon$  in the expression for the reciprocal relaxation time for point-defect scattering,

$$\tau_p^{-1} = \frac{a^3}{4\pi v^3} \epsilon \omega^4 \quad (32)$$

is calculated from the expression

$$\epsilon = y_L \left[ \frac{M_L - M}{M} + \gamma \left( \frac{V_L - V}{V} \right) \right]^2 + y_H \left[ \frac{M_H - M}{M_H} + \gamma \left( \frac{V_H - V}{V} \right) \right]^2 \quad (33)$$

where  $M$  and  $V$  are the average atomic mass and volume,  $y_L$ ,  $M_L$ , and  $V_L$  are the atomic fraction, mass, and volume of the lighter element,  $y_H$ ,  $M_H$ , and  $V_H$  are the corresponding values for the heavier element, and  $\gamma$  is the Grüneisen parameter.  $M$  is calculated in the usual way,  $\gamma$  is obtained by linear interpolation, and  $V$  is estimated from Vegard's law,

$$V^{1/3} = y V_1^{1/3} + (1-y) V_2^{1/3} \quad (34)$$

where  $y$  is the atomic fraction of the solute and  $V_1$  and  $V_2$  are the atomic volumes of the solute and solvent elements respectively. The mass defect terms are based on the results of Klemens [28] and Tavernier [29] who respectively treated the case of a light atom in a heavy matrix and that of a heavy atom in a light matrix. The difference lies in the response of the atom to the driving frequency of a wave; in the former case the atom can respond rapidly enough that the speed of oscillation may be considered unaffected so that the perturbation is proportional to the deviation from the average mass while in the latter case it is better to consider the momentum as being unaffected so that the perturbation is proportional to the difference of the reciprocals of the average and impurity masses. The distortion terms and the form of  $\epsilon$  are based on the results of Ackerman and Klemens [30] who rediscovered the fact [31] that, contrary to what is often stated, the displacement field of a spherical impurity in an elastic continuum has a non-vanishing non-uniform dilation and used a treatment that retained the phase relationship between the effects of the dilation and mass defect. Equation (33) does not take into account the difference,  $\Delta f$ , in the force constant due to the mismatch of atomic bonds; however, neutron scattering and Mössbauer experiments [32, 33] indicate that  $\Delta f$  is very small.

The coefficient in eq. (27) is the same as the coefficient in eq. (30) and is estimated from the latter. This is done by estimating  $\theta$  in the manner described below, estimating

$k_u$  of the virtual crystal at some temperature  $T'$  below the Debye temperature by linear interpolation between the values for the elements, and taking  $\alpha$  equal to unity; it has been found that the values of  $k_g$  are not sensitive to small changes in  $\alpha$ . Then  $k_g$  is estimated from the expression

$$k_g = k_u(T') \frac{I_2(\theta/T) + I_4^2(\theta/T)/[I_6(\theta/T) + I_8(\theta/T)/x_0^2]}{J_2(\theta/T') + J_4^2(\theta/T')/J_6(\theta/T')} \quad (35)$$

which, for a pure element, reduces to

$$k_g = k_u(T') \frac{J_2(\theta/T) + J_4^2(\theta/T)/J_6(\theta/T)}{J_2(\theta/T') + J_4^2(\theta/T')/J_6(\theta/T')} \quad (36)$$

Equations (35) and (36) are the equations used in our calculations for the lattice thermal conductivity of alloys and of pure elements, respectively. It should be noted that eq. (35) applies only to disordered solid-solution alloys.

The accuracy of the estimates obtained from eq. (35) clearly depends on the accuracy of the values of  $k_u$  for the virtual crystal. Experimental values of  $k_u$  for the elements, which essentially are the values of the lattice component of very dilute alloys, are available for only three of the metals included in this study: Cu, Au, and Ag. However, it was found that the experimental values for these metals each differed from the values obtained from the modified [34] Leibfried-Schlömann [35] equation by approximately the same factor. Accordingly initial estimates of the values of  $k_u$  for the other elements were obtained from this equation multiplied by the reciprocal of that factor, i. e.,

$$k_u T' = 5.7 \times 10^{-6} \frac{M \theta^3 V^{1/3}}{(\gamma + 0.5)^2} \quad (37)$$

where  $M$ ,  $\theta$ ,  $\gamma$ , and  $V$  have the same meanings as before. It is unfortunate that in this equation the Debye temperature is raised to the third power, as the high temperature values of the Debye temperature obtained from various physical properties differ considerably. The values of the Debye temperatures and other parameters used in eq. (37) for the nine elements constituting the ten selected binary alloy systems covered in this work are given in Table 1.

While in some cases it was possible to improve on the initial estimates of  $k_u$  for some elements on the basis of experimental data for a range of compositions, in others it was not, and the estimates of the lattice thermal conductivities of alloys containing the latter elements are accordingly less reliable than those containing the former. While measurements of the thermal conductivity of very dilute alloys of additional elements would make possible more reliable estimates of alloy lattice thermal conductivity, in view of the

Table 1. Parameters for the Calculation of Lattice Thermal Conductivity of Elements Using Equation (37)<sup>a</sup>

Element	M	V	$\gamma$	$\theta$
Aluminum	26.98154	10.00 <sup>b</sup>	2.18	385
Copper	63.54	7.114	1.97	313
Gold	196.9665	10.22	3.09	160
Iron	55.847	7.094	1.81	373
Magnesium	24.305	14.00 <sup>c</sup>	1.63	363
Nickel	58.71	6.593	2.00	312
Palladium	106.4	8.879	2.18	264
Silver	107.868	10.27	2.46	213
Zinc	65.38	9.165 <sup>d</sup>	2.05	326

<sup>a</sup> The values of  $\gamma$  and  $\theta$  are selected from ref. [36] with some of the values adjusted in order to be consistent with the experimental thermal conductivity data.

<sup>b</sup> In calculating  $\epsilon$ , the molar volumes used for aluminum were 8.576 and 9.032. The first value corresponds to the size of aluminum atoms in copper as determined from the change in the lattice parameter of copper upon the addition of aluminum [37, Vol. 1]. The second value was obtained from the change in the volume of the primitive cell upon the addition of aluminum to magnesium as calculated from the changes in the lattice parameters of magnesium upon the addition of aluminum [37, Vol. 2].

<sup>c</sup> In calculating  $\epsilon$ , the molar volume used for magnesium was 13.77 corresponding to the size of magnesium atoms in aluminum as determined from the change in the lattice parameter of aluminum upon the addition of magnesium [37, Vol. 2].

<sup>d</sup> In calculating  $\epsilon$ , the molar volume used for zinc was 8.534 corresponding to the size of zinc atoms in copper as determined from the change in the lattice parameter of copper upon the addition of zinc [37, Vol. 2].

uncertainty of the separation of the electronic and lattice components of very dilute alloys at temperatures above that of the maximum of the lattice component, it would also be useful to have measurements of the thermal conductivity of some denser alloys of pairs of these elements in this temperature range.

The value of the Debye temperature,  $\theta$ , for the upper limit of the integrals in eq. (35) is estimated from the value of  $k_u$  for the virtual crystal by means of the modified Leibfried-Schlömann equation, adjusted to yield values for the lattice component in agreement with those obtained from experimental data on very dilute alloys as described above:

$$\theta = 260 \left[ \frac{(\gamma + 0.5)^2 k_u T}{MV^{1/3}} \right]^{1/3} \quad (38)$$

where  $\gamma$  is the Grüneisen parameter, and  $M$  and  $V$  are the average molar mass and volume.

Agreement between the values obtained from eq. (35) and those obtained from measurements of thermal conductivity for the various alloy systems is discussed in the text; in general, it was better for alloy systems exhibiting complete solid solubility. Another general result is that the values from eq. (35) for dilute alloys tended to be too low at the low end of this temperature range. A possible explanation of this discrepancy is that the present treatment does not take into account the "freezing out" of U-processes which occurs when the temperature is reduced to the point at which there are few phonons having wave vectors of sufficient length to participate in such processes. Such a reduction in U-processes could significantly reduce the thermal resistivity of dilute alloys but cause only a small decrease in the thermal resistivity of dense alloys.

The most important deficiency of the present treatment is that the analysis leading to eq. (35) does not include the electron-phonon interaction, for which an adequate theory has not yet been developed. As noted earlier, this interaction contributes significantly to the thermal resistivity in some transition element alloys; this is true of the Pd-rich alloys considered in this study and eq. (35) could not be used to calculate the values of the lattice component in these alloys below their Debye temperatures.

At high temperatures the values obtained from eq. (35) are nearly the same as those from an approximate expression derived independently by Abeles [38] and Parrott [39], but there are significant differences below the Debye temperature, where the high temperature approximation used by these authors,

$$x^2 e^x / (e^x - 1)^2 \approx 1$$

ceases to be valid. However, because of a partial cancellation of errors these differences are much smaller than might be expected from the use of the high temperature approximation.

The use of eq. (35) rather than an approximate expression for the calculation of the lattice thermal conductivity is to some extent a reflection of the present availability of high-speed digital computers. The expression for the quantity  $\epsilon$ , eq. (33), which takes into account the point-defect scattering due to both the mass difference and the distortion of the lattice and is first derived and given in the present work, is definitely an improvement of the theory.

### 3. DATA EVALUATION AND GENERATION OF RECOMMENDED VALUES

Due to the difficulties in accurate measurement of the thermal conductivity of solids and in exact characterization of test specimens, the available experimental data on thermal conductivity extracted from various research documents are usually widely divergent and subject to large uncertainty. It is therefore very important to critically evaluate the validity and reliability of the available data and related information, to resolve and reconcile the disagreements in conflicting data, and to generate recommended reference values.

In the critical evaluation of the validity and reliability of a particular set of thermal conductivity data, the temperature dependence of the data was examined and any unusual dependence or anomaly carefully investigated, the experimental technique reviewed to see whether the actual boundary conditions in the measurement agreed with those assumed in the theory and whether all the stray heat flows and losses were prevented or minimized and accounted for, the reduction of data examined to see whether all the necessary corrections had been appropriately applied, and the estimation of uncertainties checked to ensure that all the possible sources of errors had been considered.

Experimental data could be judged to be reliable only if all sources of systematic error had been eliminated or minimized and accounted for. Major sources of systematic error include unsuitable experimental method, poor experimental technique, poor instrumentation and poor sensitivity of measuring devices, sensors, or circuits, specimen and/or thermocouple contamination, unaccounted for stray heat flows, incorrect form factor, and perhaps most important, the mismatch between actual experimental boundary conditions and those assumed in the analytical model used to derive the value of thermal conductivity. These and other possible sources of errors have been carefully considered in critical evaluation of experimental data.

The uncertainty of a set of data depends, however, not only on the estimated error of the data but also on the adequacy of characterization of the material for which the data are reported. For instance, suppose a set of thermal conductivity data obtained for a cold-worked specimen of brass with a composition of 70.06% Cu, 28.77% Zn, and 1.17% Pb is accurate to within  $\pm 2\%$ . If the author knew and reported his specimen only as 70:30 brass, the uncertainty of his data for a 70:30 brass would not be just  $\pm 2\%$  but might exceed  $\pm 20\%$ . It has been found in this and other studies that the chemical composition of a specimen reported by the author is often unreliable. This may be because in many cases the stated composition is the result of ladle analysis which the author obtained from the company who supplied the specimen and it can at best represent only the nominal composition; the actual composition varies from sample to sample. In other cases there is a strong tendency for only certain elements to be covered by a particular chemical analysis which could miss other important constituents. Furthermore, the chemical composition of a specimen may change



when it is measured at high temperatures. For binary alloys it has been found that the actual composition of a specimen may be inferred from its electrical resistivity if reported.

In the process of critical evaluation of experimental data described above, erroneous data were eliminated. The remaining data were then subjected to further critical analysis. For those test specimens for which experimental data on both thermal conductivity and electrical resistivity were reported, the electrical resistivity data were used for the calculation of electronic thermal conductivity values using eq. (12). Lattice thermal conductivity values were derived as the differences of the experimental  $k$  data and the calculated  $k_e$  values. These "experimental"  $k_g$  values derived from different sets of experimental  $k$  data were then intercompared and also compared with the calculated values from eq. (35) regarding their temperature dependence and magnitude. During these comparisons, the validity and reliability of the available experimental data could further be judged. The electrical resistivity data reported for the test specimens on which thermal conductivity measurements were made were also evaluated critically in connection with evaluation of all the electrical resistivity data available from the literature for each of the alloy systems, from which the recommended electrical resistivity values were generated.

As detailed in Section 2, the electronic component of the thermal conductivity was calculated from eq. (12), which is applicable to alloys in both the solid solution region and the mechanical mixture region. In this calculation, the recommended electrical resistivity values for the selected compositions of the present ten alloy systems and their constituent elements are available from ref. [7], the recommended thermoelectric power values are available from ref. [40], the recommended thermal conductivity values and the values of  $\beta$  for the pure elements are available from ref. [5], and the lattice thermal conductivity values of the pure elements used as corrections in the calculation of  $W_{el}$  from eq. (7) are calculated from eq. (36). As examples to show the recommended electrical resistivity and thermoelectric power values used for the calculations, Figures 1 and 2 show the recommended electrical resistivity of the copper-nickel alloy system available from ref. [7] and Figures 3 and 4 show the recommended absolute thermoelectric power of the same alloy system.

The lattice thermal conductivity of alloys was calculated from eq. (35), in which the  $k_u$  values were calculated from eq. (37) using the values of the Debye temperatures and the other parameters given in Table 1. The value of the Debye temperature for the upper limit of the integrals in eq. (35) was estimated from eq. (38). It is important to note that eq. (35) is applicable only to disordered solid-solution alloys and only for moderate and high temperatures. Beyond the solid solution region and at low temperatures, the lattice thermal conductivity was first obtained as the difference of the experimental total thermal conductivity and the calculated electronic thermal conductivity. The "experimental"  $k_g$  values

were then graphically smoothed and synthesized to obtain the values for alloys of the selected compositions. In the solid-solution region and at moderate and high temperatures, the "experimental"  $k_g$  values were used to check the  $k_g$  values calculated from eq. (35). If there were disagreements and the "experimental"  $k_g$  values were considered more reliable, the values of the lattice thermal conductivity of the virtual crystals,  $k_u$ , used in eq. (35) would be adjusted so that the calculated  $k_g$  values were in agreement with the "experimental"  $k_g$  values.

In graphical smoothing and synthesis of data, cross-plotting from conductivity versus temperature to conductivity versus composition and vice versa was often used. Smooth curves were drawn which approximate the best fit to the conductivity data versus temperature, and points from the smoothed curves were used to construct conductivity versus composition curves for a convenient set of selected temperatures. In the conductivity versus composition graph, the families of isotherms were similar and any required smoothing of the data could be done more easily and with greater confidence than when working directly with the conductivity-temperature curves. The points from the smoothed curves were then used to construct conductivity-temperature curves for the selected compositions, and these curves were further smoothed. In the graphical smoothing process it is extremely important that the alloy phase diagrams [104,183,184] be constantly consulted and the phase boundaries between solid solutions and/or mechanical mixtures and the boundaries of magnetic transitions be kept in mind, so as to be aware of any possible discontinuity or sudden change of slope in the thermal conductivity curves.

The total thermal conductivity values were thus obtained as the sum of the  $k_e$  values calculated from eq. (12) and the  $k_g$  values derived from the "experimental"  $k_g$  values or calculated from eq. (35), which might have been adjusted to fit the "experimental"  $k_g$  values, if such values were available and reliable.

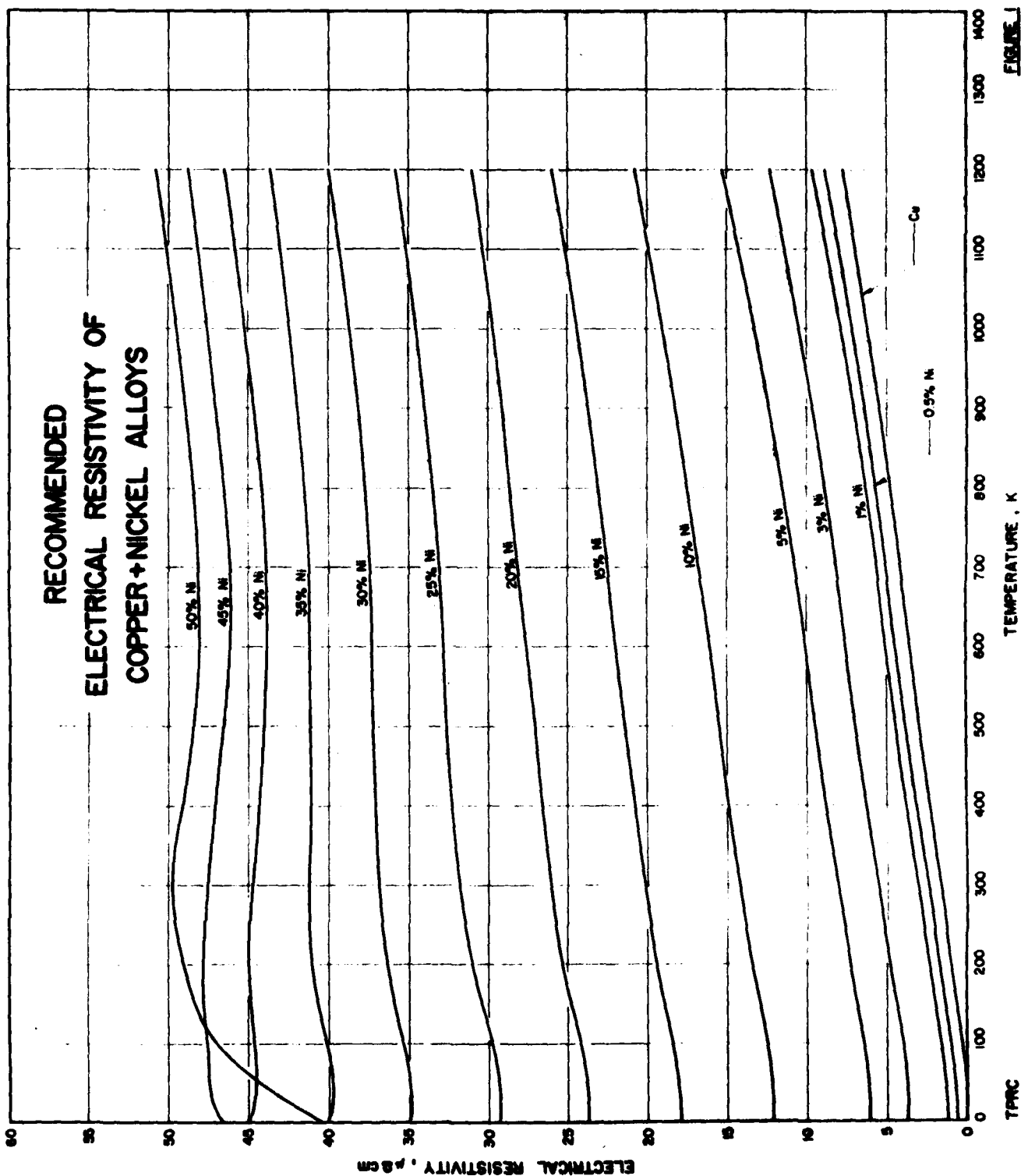


FIGURE 1

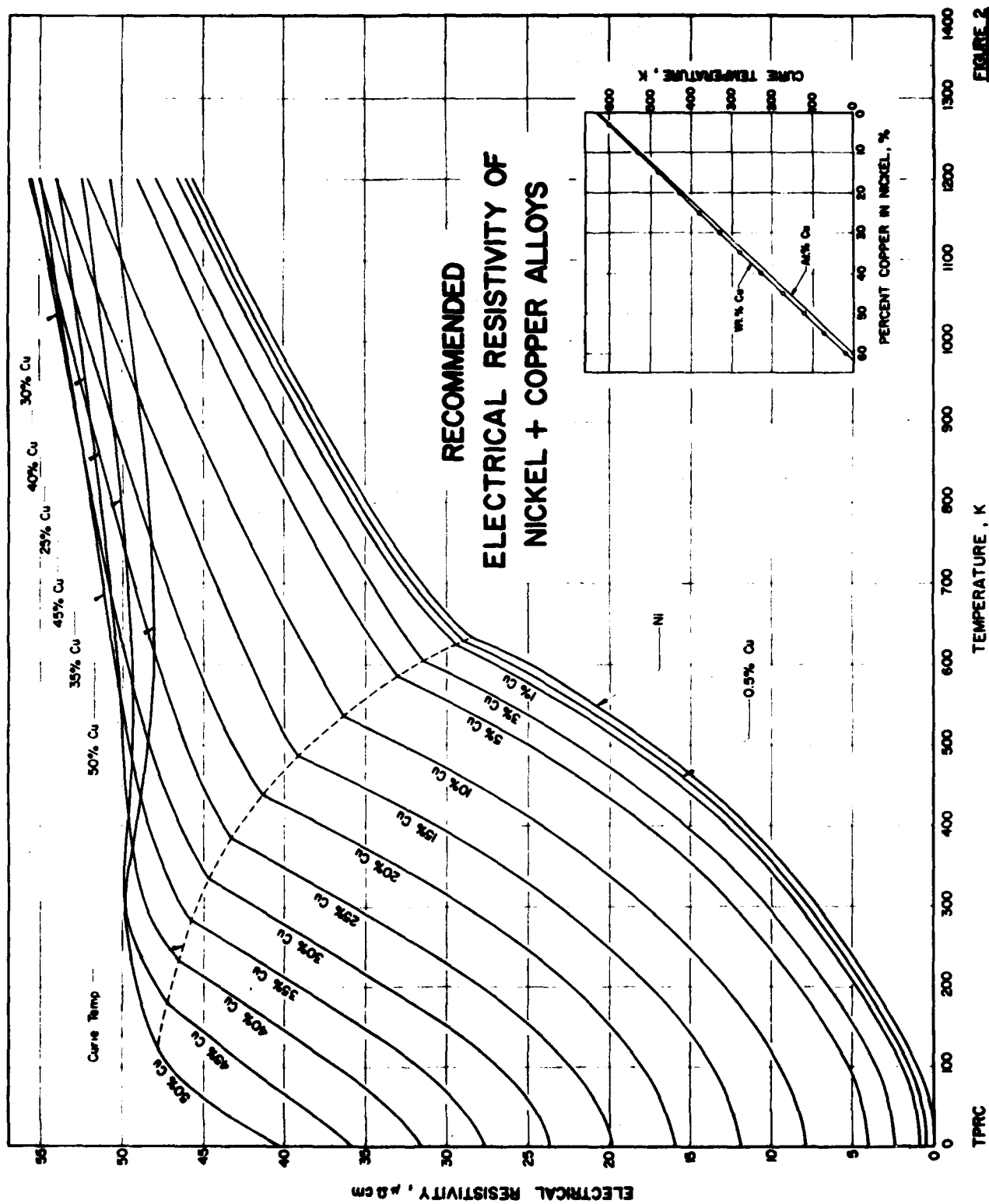


FIGURE 2

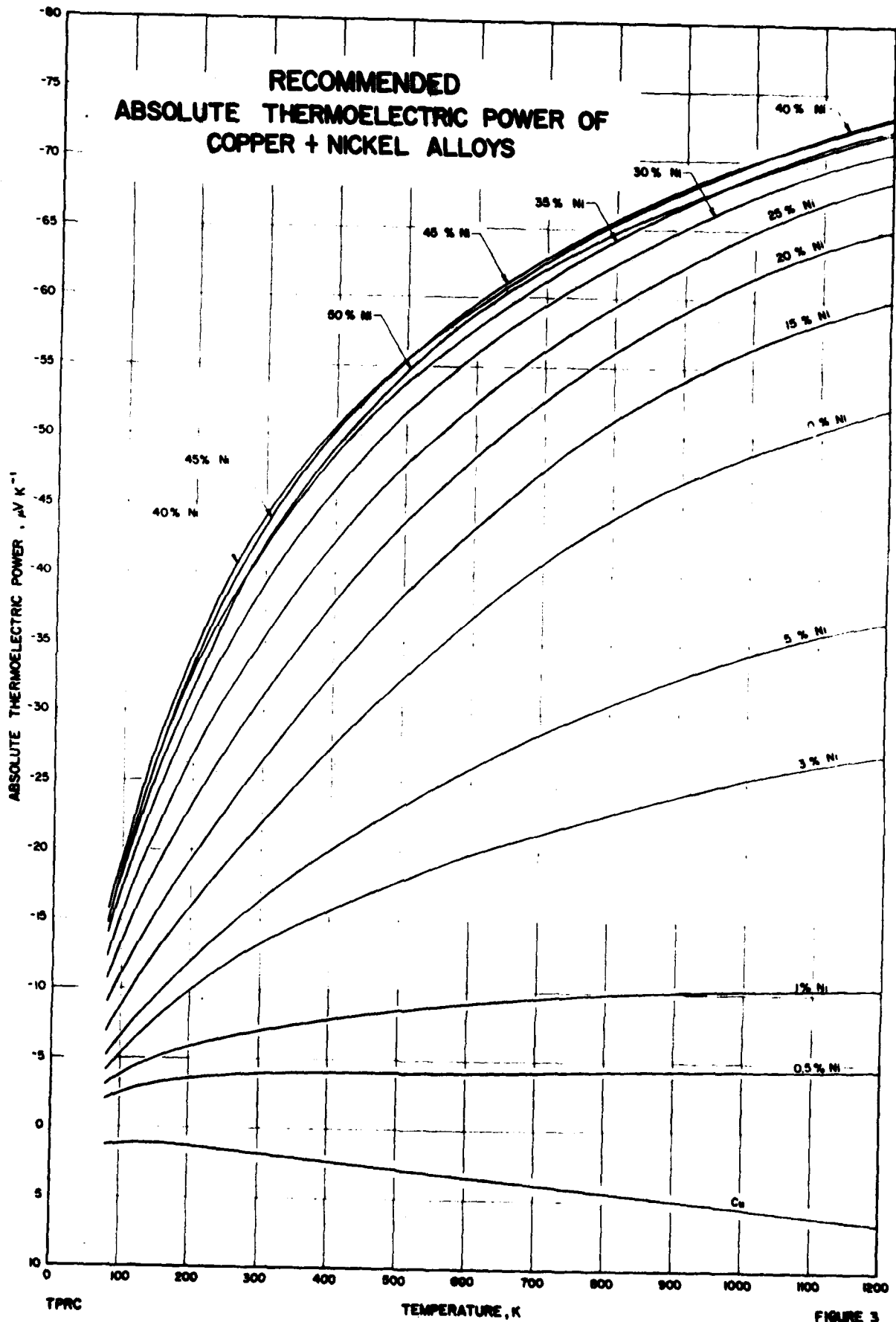
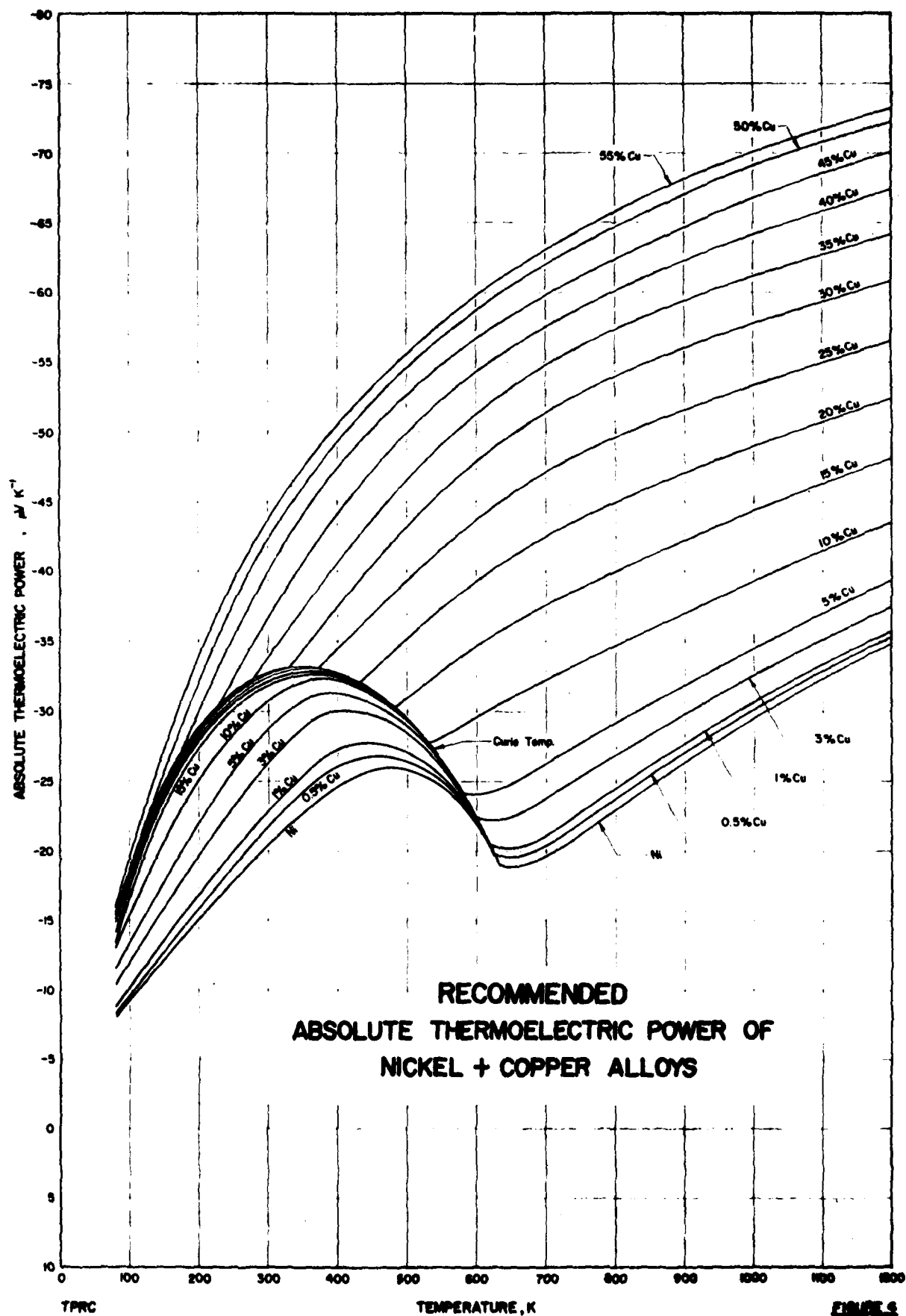


FIGURE 3



#### 4. THERMAL CONDUCTIVITY OF BINARY ALLOY SYSTEMS

In the following subsections the recommended (or provisional or typical) values for the total thermal conductivity, electronic thermal conductivity, and lattice thermal conductivity and the original experimental data for the thermal conductivity of the ten selected binary alloy systems are given, together with a discussion of each system, reviewing individual pieces of available data and information and discussing the considerations involved in arriving at the final assessment and recommendations. The conductivity values are for well-annealed disordered alloys.

In this work, the term "binary alloy system" refers to the full range of composition of two alloying elements and is signified by a hyphen between the two elements, such as aluminum-copper alloy system. The term "binary alloys" refers to a group of binary alloys in which the first alloying element is predominant and is signified by a plus between the two elements, such as aluminum + copper alloys.

In the figures and tables, weight percent is denoted by % and atomic percent by At. %. In the figures of recommended (or provisional or typical) values continuous (solid) curves represent recommended values, long-dashed curves represent provisional values, and dash-dot-dash curves represent typical values. The short-dashed portion of any of the above three kinds of curves represents values in the temperature ranges where no experimental data are available. In the tables of recommended (or provisional or typical) values, the values of residual electrical resistivity of the alloys are given, which is for the purpose of helping to characterize and identify the alloys for which the values are presented. The difference among recommended, provisional, and typical values is due to their ranges of uncertainties assigned. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15\%$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively. In the tables on specimen characterization and measurement information, the code designations used for experimental methods for thermal conductivity determinations are as follows:

- C Comparative method
- E Direct electrical heating method
- F Forbes' bar method
- L Longitudinal heat flow method
- P Periodic or transient heat flow method
- R Radial heat flow method
- T Thermoelectrical method

In each of the subsections that follow, the thermal conductivity data and information are presented in the following order: discussion text, tables of recommended values, figures of recommended curves, figures of experimental data, and tables of specimen characterization and measurement information.

#### 4.1. Aluminum-Copper Alloy System

The aluminum-copper alloy system does not form a continuous series of solid solutions. The maximum solid solubility of copper in aluminum is 5.70% (2.50 At.%) at 821 K and the solubility decreases to 0.1-0.2% (0.04-0.08 At.%) at 523 K. The maximum solid solubility of aluminum in copper is 9.4% (19.6 At.%) in the range from about 650 to 838 K and the solubility decreases at higher and lower temperatures. Thus the region of solid solution is limited. However, the equation derived for the calculation of the electronic component of thermal conductivity, eq. (12), is applicable to all phases, though the equation for the calculation of the lattice component, eq. (35), can be used only for solid solutions, as noted before in Sections 2 and 3. Beyond the solid solution region, the lattice thermal conductivity has been derived from the experimental total thermal conductivity and the calculated electronic component.

There are 188 sets of experimental data available for the thermal conductivity of this alloy system. However, of the 49 data sets for Al + Cu alloys listed in Table 3 and shown in Figure 7, 10 sets are merely single data points around room temperature and 27 sets cover only a narrow temperature range from around room temperature to about 500 K. Of the 139 data sets for Cu + Al alloys listed in Table 4 and shown in Figure 8, 20 sets are single data points, 15 sets cover the narrow temperature range from around room temperature to about 500 K, and 84 sets are for temperatures below 4.5 K.

For the Al + Cu alloys, all measurements were made between room temperature and 800 K except four (Al + Cu curves 6-8, and 16) which were measured down to about 80 K for specimens containing 4.0, 8.0, and 15.0% Cu [41,42] and except the two of Satterthwaite [43] who investigated the thermal conductivity of a specimen containing 0.3% Cu in both the superconducting and normal states (Al + Cu curves 25 and 26). A thermal conductivity versus composition curve for 300 K was constructed following mainly the data of Griffiths and Schofield [44] (Al + Cu curves 1-5) and of Smith [45] (Al + Cu curves 12-15). Electronic thermal conductivity values at 300 K were calculated from eq. (12) using electrical resistivity reported in [7], thermoelectric power reported in [40], thermal conductivity of aluminum and the value of  $\beta$  reported in [5], and lattice thermal conductivity of aluminum calculated from eq. (36). These  $k_e$  values were also plotted on the conductivity-composition graph. The differences  $k_g$  between the experimental total thermal conductivity  $k$  and the calculated electronic component  $k_e$  for the various compositions were taken. These  $k_g$  values were extrapolated to higher temperatures up to the solidus points according to the temperature dependence of eq. (35) and to lower temperatures according to the pattern of  $k_g$  curves of aluminum-copper system derived from the available experimental  $k$  and the calculated  $k_e$  around the region of maximum  $k_g$  and according to  $T^2$  dependence at lower temperatures assuming  $k_g$  to be negligible at 1 K. The values were then adjusted so that the extrapolated



$k_g$  values plus their corresponding  $k_e$  values yield total  $k$  values which fit the experimental data in those regions. The total thermal conductivity values were then obtained by adding the calculated values of  $k_e$  to the adjusted extrapolated values of  $k_g$ . The results are in agreement with the data of Griffiths and Schofield [44] (Al + Cu curves 1-5), Smith [45] (Al + Cu curves 12-14), and Griffiths and Shakespear [46] (Al + Cu curve 17) above room temperature to within 5%. No appropriate comparison is available below room temperature.

On the copper-rich side, several measurements were made between 4 K and 80 K [48] (Cu + Al curves 111-121) for alloys containing 4.07, 0.43, and 6.97% Al. The conductivity-composition curve at 300 K was constructed, based mainly on the data of Smith and Palmer [49] (Cu + Al curves 2-9) and Smith [45] (Cu + Al curves 14-18), which are considered reliable. The  $k_e$  values were calculated from eq. (12) and those at 300 K were plotted on the conductivity-composition graph. The differences  $k_g$  between  $k$  and  $k_e$  were obtained for all compositions. These  $k_g$  values were adjusted so that their extrapolations to lower temperatures, according to the method described above for Al + Cu alloys, fit the  $k_g$  values derived from experimental data of Chu and Lipschultz [48] (Cu + Al curves 111-121) and of Friedman [50] (Cu + Al curves 122-126). Above 300 K the  $k_g$  values were extrapolated to the solidus points. The total thermal conductivity values were then obtained by adding the calculated values of  $k_e$  to the adjusted extrapolated values of  $k_g$ . Because of the lack of experimental electrical resistivity data, no total  $k$  values are given below 200 K for the alloy with 10% Al, below 300 K for the alloy with 15% Al, and at temperatures other than 300 K for the alloy with 20% Al. The resulting recommended values at low temperatures are in agreement with the data of Salter and Charsley [51] (Cu + Al curves 19-26), Kusunoki and Suzuki [53] (Cu + Al curves 45-52), Chu and Lipschultz [48] (Cu + Al curves 111-121), and Friedman [50] (Cu + Al curves 122-126) to within 6%, and those at higher temperatures are in agreement with the data of Smith and Palmer [49] (Cu + Al curves 2-9), Hanson and Rodgers [47] (Cu + Al curves 10-13), Inouye [55] (Cu + Al curves 37 and 38), Smith and Palmer [49] (Cu + Al curve 78), and Aliev [116] (Cu + Al curves 57-65 and 67) to within 10%.

The resulting recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 2 for 25 alloy compositions. These values are for well-annealed alloys. The values for  $k$  are also shown in Figures 5 and 6. For most of the alloy compositions, the temperature range covered is from 4 K to the temperature where melting starts. The values of residual electrical resistivity for the alloys are also given in Table 2. The uncertainties of the  $k$  values are stated in a footnote to Table 2, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 99.50% (99.79 At.%) Cu: 0.50% (0.21 At.%)				Al: 99.00% (99.57 At.%) Cu: 1.00% (0.43 At.%)				Al: 97.00% (98.70 At.%) Cu: 3.00% (1.30 At.%)				Al: 95.00% (97.81 At.%) Cu: 5.00% (2.19 At.%)			
$\rho_0 = 0.0600 \mu\Omega \text{ cm}$				$\rho_0 = 0.1203 \mu\Omega \text{ cm}$				$\rho_0 = 0.340 \mu\Omega \text{ cm}$				$\rho_0 = 0.532 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	1.56*			4	0.814*			4	0.292*			4	0.189*	0.183	0.00378*
6	2.36*			6	1.23*			6	0.442*			6	0.288*	0.275	0.0130*
8	3.11*			8	1.65*			8	0.593*			8	0.388*	0.366	0.0222*
10	3.81*			10	2.05*			10	0.741*			10	0.488*	0.456	0.0330*
15	5.46*			15	3.04*			15	1.10*			15	0.738*	0.677	0.0610*
20	6.73*			20	3.92*			20	1.45*			20	0.977*	0.892	0.0849*
25	7.56*	7.30	0.265*	25	4.64*	4.42	0.221*	25	1.75*	1.61	0.139*	25	1.19*	1.09	0.102*
30	8.06*	7.78	0.285*	30	5.14*	4.90	0.239*	30	2.02*	1.87	0.152*	30	1.39*	1.28	0.113*
40	8.22*	7.94	0.285*	40	5.64*	5.40	0.239*	40	2.44*	2.28	0.155*	40	1.71*	1.59	0.117*
50	7.36*	7.09	0.265*	50	5.45*	5.23	0.221*	50	2.68*	2.53	0.147*	50	1.92*	1.81	0.112*
60	5.99*	5.75	0.241*	60	4.80*	4.60	0.202*	60	2.70*	2.56	0.138*	60	2.00*	1.89	0.106*
70	4.74*	4.52	0.218*	70	4.04*	3.85	0.185*	70	2.54*	2.41	0.127*	70	1.88*	1.88	0.0985*
80	3.77*	3.57	0.199*	80	3.35*	3.18	0.170*	80	2.33*	2.21	0.118*	80	1.99*	1.80	0.0916*
90	3.11*	2.93	0.183*	90	2.85*	2.69	0.157*	90	2.11*	2.00	0.110*	90	1.79*	1.70	0.0887*
100	2.78*	2.61	0.168*	100	2.58*	2.43	0.145*	100	1.99*	1.89	0.102*	100	1.72*	1.64	0.0804*
150	2.30*	2.18	0.123*	150	2.20*	2.09	0.107*	150	1.89*	1.81	0.0758*	150	1.67*	1.61	0.0612*
200	2.24*	2.14	0.0968*	200	2.15*	2.07	0.0847*	200	1.90*	1.84	0.0607*	200	1.72*	1.67	0.0495*
250	2.25*	2.17	0.0601*	250	2.17*	2.10	0.0704*	250	1.94*	1.89	0.0509*	250	1.79*	1.75	0.0416*
273	2.26*	2.19	0.0745*	273	2.18*	2.12	0.0652*	273	1.97*	1.92	0.0474*	273	1.82*	1.78	0.0388*
300	2.28*	2.21	0.0685*	300	2.21	2.15	0.0602*	300	1.99*	1.95	0.0438*	300	1.85	1.81	0.0360*
350	2.31	2.25	0.0596*	350	2.25	2.20	0.0526*	350	2.04	2.00	0.0386*	350	1.90	1.87	0.0319*
400	2.32	2.27	0.0530*	400	2.26	2.21	0.0467*	400	2.07	2.04	0.0345*	400	1.93	1.90	0.0285*
500	2.29	2.25	0.0430*	500	2.24	2.20	0.0382*	500	2.07	2.04	0.0285*	500	1.95	1.93	0.0237*
600	2.25	2.21	0.0362*	600	2.19	2.16	0.0322*	600	2.05	2.03	0.0243*	600	1.94	1.92	0.0203*
700	2.19	2.16	0.0312*	700	2.15	2.12	0.0279*	700	2.02	2.00	0.0212*	700	1.92	1.90	0.0177*
800	2.13*	2.10	0.0273*	800	2.09*	2.06	0.0245*	800	1.97*	1.95	0.0188*	800	1.89*	1.87	0.0157*
900	2.09*	2.04	0.0243*	900	2.02*	2.00	0.0219*	864	1.94*	1.92	0.0177*	831	1.88*	1.86	0.0152*
919	2.09*	2.03	0.0239*	910	2.01*	1.99	0.0217*								

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:99.50 Al - 0.50 Cu:  $\pm 6\%$  below 200 K, and  $\pm 3\%$  above 200 K.99.00 Al - 1.00 Cu:  $\pm 6\%$  below 200 K, and  $\pm 3\%$  above 200 K.97.00 Al - 3.00 Cu:  $\pm 6\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 6\%$  above 500 K.95.00 Al - 5.00 Cu:  $\pm 6\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 6\%$  above 500 K.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 80.00% (35.49 At.%) Cu: 10.00% (4.51 At.%)				Al: 85.00% (93.03 At.%) Cu: 15.00% (6.97 At.%)				Al: 80.00% (90.40 At.%) Cu: 20.00% (9.60 At.%)				Al: 75.00% (87.00 At.%) Cu: 25.00% (12.00 At.%)			
$\rho_0 = 0.868 \mu\Omega \text{ cm}$				$\rho_0 = 1.118 \mu\Omega \text{ cm}$				$\rho_0 = 1.312 \mu\Omega \text{ cm}$				$\rho_0 = 1.483 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.115*	0.110	0.004663	4	0.0913*	0.0870	0.004263	4	0.0786*	0.0745	0.004063	4	0.0699*	0.0659	0.003863
6	0.176*	0.165	0.01053	6	0.140*	0.130	0.009563	6	0.121*	0.112	0.009123	6	0.108*	0.0993	0.008683
8	0.238*	0.220	0.01763	8	0.189*	0.173	0.01633	8	0.165*	0.149	0.01563	8	0.147*	0.132	0.01383
10	0.300*	0.273	0.02463	10	0.240*	0.216	0.02433	10	0.209*	0.186	0.02323	10	0.189*	0.165	0.02173
15	0.455*	0.406	0.04913	15	0.365*	0.320	0.04493	15	0.317*	0.274	0.04283	15	0.285*	0.245	0.04083
20	0.604*	0.536	0.06843	20	0.484*	0.421	0.06253	20	0.420*	0.360	0.05973	20	0.376*	0.319	0.05693
25	0.741*	0.659	0.08233	25	0.594*	0.519	0.07523	25	0.515*	0.443	0.07183	25	0.463*	0.398	0.07003
30	0.869*	0.774	0.09093	30	0.694*	0.611	0.08273	30	0.602*	0.522	0.07893	30	0.549*	0.463	0.07743
40	1.06*	0.932	0.09423	40	0.862*	0.776	0.08613	40	0.749*	0.667	0.08223	40	0.676*	0.583	0.08063
50	1.24*	1.15	0.09953	50	0.993*	0.910	0.09273	50	0.866*	0.787	0.07893	50	0.777*	0.700	0.07743
60	1.39*	1.26	0.09833	60	1.09*	1.01	0.07793	60	0.951*	0.877	0.07443	60	0.857*	0.764	0.07293
70	1.38*	1.26	0.07943	70	1.14*	1.07	0.07253	70	1.01*	0.938	0.06923	70	0.911*	0.843	0.06773
80	1.30*	1.21	0.07383	80	1.16*	1.09	0.06743	80	1.03*	0.964	0.06443	80	0.945*	0.868	0.06313
90	1.35	1.26	0.06913	90	1.16	1.10	0.06313	90	1.04*	0.964	0.06023	90	0.960*	0.881	0.05913
100	1.35	1.27	0.06473	100	1.16	1.10	0.05923	100	1.06*	1.00	0.05653	100	0.976*	0.923	0.05503
150	1.29	1.24	0.04833	150	1.26	1.21	0.04513	150	1.15*	1.11	0.04303	150	1.09*	1.05	0.04233
200	1.47	1.43	0.03893	200	1.34	1.30	0.03853	200	1.25*	1.22	0.03483	200	1.18*	1.15	0.03513
250	1.53	1.52	0.03353	250	1.42	1.39	0.03063	250	1.33*	1.30	0.02923	250	1.27*	1.24	0.02973
273	1.53	1.55	0.03133	273	1.45	1.42	0.02863	273	1.37*	1.34	0.02733	273	1.30*	1.27	0.02803
300	1.61	1.59	0.02903	300	1.49	1.46	0.02653	300	1.40	1.37	0.02533	300	1.33*	1.31	0.02503
350	1.67	1.64	0.02573	350	1.54	1.52	0.02353	350	1.46	1.44	0.02243	350	1.38*	1.37	0.02193
400	1.71	1.69	0.02293	400	1.58	1.56	0.02093	400	1.50*	1.48	0.02003	400	1.43*	1.41	0.01983
500	1.74	1.72	0.01913	500	1.62	1.60	0.01743	500	1.54*	1.52	0.01663	500	1.47*	1.45	0.01633
600	1.75	1.73	0.01633	600	1.64*	1.63	0.01493	600	1.56*	1.55	0.01423	600	1.50*	1.49	0.01463
700	1.74	1.73	0.01423	700	1.64*	1.63	0.01303	700	1.56*	1.55	0.01243	700	1.50*	1.49	0.01293
800	1.72	1.71	0.01273	800	1.62*	1.61	0.01163	800	1.55*	1.54	0.01113	800	1.50*	1.49	0.01063
821	1.72	1.71	0.01243	821	1.62*	1.61	0.01133	821	1.55*	1.54	0.01093	821	1.50*	1.49	0.01063

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 30.00 Al - 10.00 Cu:  $\pm 8\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 6\%$  above 500 K.  
 35.00 Al - 15.00 Cu:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 6\%$  above 500 K.  
 40.00 Al - 20.00 Cu:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 7\%$  above 500 K.  
 75.00 Al - 25.00 Cu:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 7\%$  above 500 K.

\* Typical values.

† In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)\*

† Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>

$\rho_0 = 1.633 \mu\Omega \text{ cm}$						$\rho_0 = 1.754 \mu\Omega \text{ cm}$						$\rho_0 = 1.983 \mu\Omega \text{ cm}$						$\rho_0 = 2.02 \mu\Omega \text{ cm}$					
Al: 70.00% (84.60 At. %) Cu: 30.00% (15.40 At. %)						Al: 65.00% (81.39 At. %) Cu: 35.00% (18.61 At. %)						Al: 60.00% (77.94 At. %) Cu: 40.00% (22.06 At. %)						Al: 55.00% (74.22 At. %) Cu: 45.00% (25.78 At. %)					
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0641*	0.0602	0.00392†	4	0.0596*	0.0557	0.00392†	4	0.0559*	0.0519	0.00394†	4	0.0524*	0.0484	0.00395†	4	0.0524*	0.0484	0.00395†	4	0.0524*	0.0484	0.00395†
6	0.0603*	0.0605	0.00880†	6	0.0924*	0.0836	0.00880†	6	0.0866*	0.0778	0.00884†	6	0.0812*	0.0723	0.00887†	6	0.0812*	0.0723	0.00887†	6	0.0812*	0.0723	0.00887†
8	0.139*	0.130	0.0150†	8	0.127*	0.112	0.0150†	8	0.118*	0.103	0.0151†	8	0.111*	0.0955	0.0152†	8	0.111*	0.0955	0.0152†	8	0.111*	0.0955	0.0152†
10	0.173*	0.150	0.0223†	10	0.160*	0.138	0.0223†	10	0.150*	0.128	0.0224†	10	0.142*	0.119	0.0225†	10	0.142*	0.119	0.0225†	10	0.142*	0.119	0.0225†
15	0.263*	0.221	0.0413†	15	0.244*	0.203	0.0413†	15	0.228*	0.187	0.0415†	15	0.217*	0.175	0.0417†	15	0.217*	0.175	0.0417†	15	0.217*	0.175	0.0417†
20	0.349*	0.290	0.0575†	20	0.324*	0.267	0.0575†	20	0.306*	0.248	0.0576†	20	0.290*	0.232	0.0580†	20	0.290*	0.232	0.0580†	20	0.290*	0.232	0.0580†
25	0.435*	0.356	0.0693†	25	0.399*	0.330	0.0693†	25	0.377*	0.307	0.0696†	25	0.357*	0.287	0.0700†	25	0.357*	0.287	0.0700†	25	0.357*	0.287	0.0700†
30	0.497*	0.421	0.0761†	30	0.466*	0.390	0.0761†	30	0.439*	0.363	0.0764†	30	0.416*	0.339	0.0768†	30	0.416*	0.339	0.0768†	30	0.416*	0.339	0.0768†
40	0.616*	0.539	0.0793†	40	0.579*	0.500	0.0793†	40	0.546*	0.466	0.0796†	40	0.517*	0.437	0.0799†	40	0.517*	0.437	0.0799†	40	0.517*	0.437	0.0799†
50	0.724*	0.638	0.0861†	50	0.669*	0.593	0.0761†	50	0.631*	0.555	0.0764†	50	0.597*	0.520	0.0768†	50	0.597*	0.520	0.0768†	50	0.597*	0.520	0.0768†
60	0.787*	0.715	0.0718†	60	0.740*	0.668	0.0718†	60	0.700*	0.628	0.0721†	60	0.663*	0.590	0.0724†	60	0.663*	0.590	0.0724†	60	0.663*	0.590	0.0724†
70	0.841*	0.774	0.0668†	70	0.793*	0.726	0.0668†	70	0.751*	0.684	0.0670†	70	0.711*	0.644	0.0673†	70	0.711*	0.644	0.0673†	70	0.711*	0.644	0.0673†
80	0.877*	0.815	0.0621†	80	0.830*	0.768	0.0621†	80	0.787*	0.725	0.0623†	80	0.746*	0.685	0.0626†	80	0.746*	0.685	0.0626†	80	0.746*	0.685	0.0626†
90	0.900*	0.842	0.0581†	90	0.856*	0.798	0.0581†	90	0.813*	0.755	0.0583†	90	0.778*	0.719	0.0586†	90	0.778*	0.719	0.0586†	90	0.778*	0.719	0.0586†
100	0.924*	0.869	0.0545†	100	0.880*	0.825	0.0545†	100	0.850*	0.785	0.0547†	100	0.805*	0.750	0.0549†	100	0.805*	0.750	0.0549†	100	0.805*	0.750	0.0549†
150	1.04*	0.996	0.0415†	150	0.996*	0.957	0.0415†	150	0.963*	0.921	0.0417†	150	0.929*	0.887	0.0418†	150	0.929*	0.887	0.0418†	150	0.929*	0.887	0.0418†
200	1.14*	1.11	0.0336†	200	1.10*	1.07	0.0336†	200	1.06*	1.03	0.0337†	200	1.03*	0.993	0.0338†	200	1.03*	0.993	0.0338†	200	1.03*	0.993	0.0338†
250	1.23*	1.19	0.0283†	250	1.17*	1.14	0.0283†	250	1.14*	1.11	0.0283†	250	1.10*	1.07	0.0284†	250	1.10*	1.07	0.0284†	250	1.10*	1.07	0.0284†
273	1.28*	1.22	0.0263†	273	1.21*	1.18	0.0263†	273	1.17*	1.14	0.0264†	273	1.13*	1.10	0.0266†	273	1.13*	1.10	0.0266†	273	1.13*	1.10	0.0266†
300	1.28	1.26	0.0244†	300	1.24*	1.22	0.0244†	300	1.20	1.18	0.0245†	300	1.17	1.15	0.0246†	300	1.17	1.15	0.0246†	300	1.17	1.15	0.0246†
350	1.24	1.22	0.0216†	350	1.29*	1.27	0.0216†	350	1.25	1.23	0.0217†	350	1.22	1.20	0.0218†	350	1.22	1.20	0.0218†	350	1.22	1.20	0.0218†
400	1.30*	1.26	0.0193†	400	1.33*	1.31	0.0193†	400	1.29*	1.27	0.0194†	400	1.26*	1.24	0.0194†	400	1.26*	1.24	0.0194†	400	1.26*	1.24	0.0194†
500	1.40*	1.40	0.0160†	500	1.39*	1.36	0.0160†	500	1.34*	1.32	0.0161†	500	1.32*	1.30	0.0162†	500	1.32*	1.30	0.0162†	500	1.32*	1.30	0.0162†
600	1.45*	1.44	0.0137†	600	1.40*	1.39	0.0137†	600	1.37*	1.36	0.0138†	600	1.34*	1.33	0.0138†	600	1.34*	1.33	0.0138†	600	1.34*	1.33	0.0138†
700	1.46*	1.45	0.0120†	700	1.43*	1.41	0.0120†	700	1.38*	1.37	0.0120†	700	1.35*	1.34	0.0121†	700	1.35*	1.34	0.0121†	700	1.35*	1.34	0.0121†
800	1.46*	1.44	0.0107†	800	1.41*	1.40	0.0107†	800	1.39*	1.37	0.0107†	800	1.35*	1.34	0.0108†	800	1.35*	1.34	0.0108†	800	1.35*	1.34	0.0108†
821	1.48*	1.44	0.0105†	821	1.41*	1.40	0.0105†	821	1.38*	1.37	0.0105†	821	1.35*	1.34	0.0106†	821	1.35*	1.34	0.0106†	821	1.35*	1.34	0.0106†

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:70.00 Al - 30.00 Cu:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 7\%$  above 500 K.65.00 Al - 35.00 Cu:  $\pm 15\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 7\%$  above 500 K.60.00 Al - 40.00 Cu:  $\pm 15\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 7\%$  above 500 K.55.00 Al - 45.00 Cu:  $\pm 15\%$  below 80 K,  $\pm 5\%$  between 80 and 900 K, and  $\pm 7\%$  above 500 K.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 50.00% (70.19 At. %) Cu: 50.00% (29.81 At. %)				Al: 45.00% (65.83 At. %) Cu: 55.00% (34.17 At. %)				Al: 40.00% (61.09 At. %) Cu: 60.00% (38.91 At. %)				Al: 35.00% (55.91 At. %) Cu: 65.00% (44.09 At. %)			
$\rho_0 = 2.26 \mu\Omega \text{ cm}$				$\rho_0 = 2.59 \mu\Omega \text{ cm}$				$\rho_0 = 3.25 \mu\Omega \text{ cm}$				$\rho_0 = 4.42 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.047*	0.0434	0.00366*	4	0.0420*	0.0390	0.00400*	4	0.0342*	0.0302	0.00402*	4	0.0269*	0.0239	0.00405*
6	0.0736*	0.0647	0.00894*	6	0.0659*	0.0569	0.00900*	6	0.0541*	0.0450	0.00900*	6	0.0430*	0.0338	0.00923*
8	0.101*	0.0857	0.0153*	8	0.0909*	0.0755	0.0154*	8	0.0753*	0.0597	0.0156*	8	0.0605*	0.0447	0.0159*
10	0.130*	0.107	0.0227*	10	0.117*	0.0942	0.0229*	10	0.0974*	0.0744	0.0230*	10	0.0786*	0.0552	0.0234*
15	0.200*	0.159	0.0436*	15	0.181*	0.139	0.0422*	15	0.154*	0.111	0.0426*	15	0.128*	0.0816	0.0434*
20	0.260*	0.206	0.0595*	20	0.242*	0.183	0.0590*	20	0.206*	0.146	0.0595*	20	0.169*	0.106	0.0603*
25	0.320*	0.266	0.0704*	25	0.296*	0.225	0.0706*	25	0.252*	0.181	0.0714*	25	0.206*	0.133	0.0726*
30	0.383*	0.326	0.0774*	30	0.344*	0.267	0.0779*	30	0.293*	0.215	0.0783*	30	0.237*	0.158	0.0795*
40	0.479*	0.394	0.0806*	40	0.426*	0.345	0.0810*	40	0.361*	0.279	0.0817*	40	0.290*	0.207	0.0830*
50	0.540*	0.471	0.0774*	50	0.494*	0.416	0.0779*	50	0.419*	0.337	0.0794*	50	0.339*	0.232	0.0797*
60	0.600*	0.536	0.0729*	60	0.550*	0.477	0.0730*	60	0.463*	0.369	0.0737*	60	0.399*	0.268	0.0746*
70	0.650*	0.590	0.0679*	70	0.596*	0.528	0.0680*	70	0.499*	0.430	0.0686*	70	0.400*	0.308	0.0697*
80	0.690*	0.632	0.0631*	80	0.631*	0.568	0.0634*	80	0.535*	0.471	0.0640*	80	0.431*	0.346	0.0699*
90	0.720*	0.667	0.0591*	90	0.661*	0.502	0.0594*	90	0.565*	0.505	0.0596*	90	0.457*	0.386	0.0610*
100	0.750*	0.696	0.0554*	100	0.689*	0.533	0.0559*	100	0.594*	0.538	0.0562*	100	0.483*	0.426	0.0571*
150	0.890*	0.836	0.0426*	150	0.814*	0.772	0.0429*	150	0.723*	0.679	0.0439*	150	0.599*	0.565	0.0439*
200	0.970*	0.945	0.0341*	200	0.915*	0.861	0.0343*	200	0.830*	0.785	0.0349*	200	0.691*	0.666	0.0350*
250	1.09*	1.03	0.0297*	250	0.996*	0.967	0.0299*	250	0.903*	0.873	0.0291*	250	0.772*	0.748	0.0306*
273	1.09*	1.06	0.0296*	273	1.03*	1.00	0.0270*	273	0.933*	0.906	0.0271*	273	0.804*	0.776	0.0276*
300	1.12	1.10	0.0268*	300	1.06	1.04	0.0250*	300	0.966	0.943	0.0252*	300	0.840	0.814	0.0256*
350	1.19	1.16	0.0219*	350	1.12*	1.10	0.0220*	350	1.02*	1.00	0.0223*	350	0.897*	0.874	0.0236*
400	1.29*	1.26	0.0190*	400	1.18*	1.14	0.0197*	400	1.07*	1.05	0.0199*	400	0.943*	0.923	0.0206*
500	1.39*	1.26	0.0163*	500	1.23*	1.20	0.0164*	500	1.14*	1.12	0.0166*	500	1.01*	0.997	0.0169*
600	1.39*	1.29	0.0140*	600	1.25*	1.24	0.0140*	600	1.17*	1.16	0.0141*	600	1.06*	1.05	0.0144*
700	1.39*	1.31	0.0123*	700	1.27*	1.26	0.0123*	700	1.20*	1.19	0.0123*	700	1.10*	1.09	0.0126*
800	1.39*	1.31	0.0106*	800	1.28*	1.27	0.0106*	800	1.22*	1.21	0.0106*	800	1.13*	1.11	0.0111*
864	1.39*	1.31	0.0106*	864	1.29*	1.28	0.0101*	864	1.23*	1.22	0.0102*	864	1.14*	1.13	0.0104*

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:50.00 Al - 50.00 Cu:  $\pm 12\%$  below 80 K,  $\pm 5\%$  between 80 and 500 K, and  $\pm 7\%$  above 500 K.45.00 Al - 55.00 Cu:  $\pm 11\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 7\%$  above 200 K.40.00 Al - 60.00 Cu:  $\pm 15\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 8\%$  above 200 K.35.00 Al - 65.00 Cu:  $\pm 20\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 8\%$  above 200 K.

\* Provisional values.

† Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)\*

(Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>)

Al: 38.00% (59.23 At.%) Cu: 78.00% (48.77 At.%)				Al: 25.00% (43.98 At.%) Cu: 75.00% (56.02 At.%)				Al: 20.00% (37.06 At.%) Cu: 80.00% (62.94 At.%)				Al: 15.00% (29.36 At.%) Cu: 85.00% (70.64 At.%)			
$\rho_0 = 6.61 \mu\Omega\text{cm}$				$\rho_0 = 12.4 \mu\Omega\text{cm}$											
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0191 <sup>†</sup>	0.0149	0.00416 <sup>‡</sup>	4	0.0121 <sup>†</sup>	0.00788	0.00424 <sup>‡</sup>	4	0.00440 <sup>‡</sup>	0.00440 <sup>‡</sup>	0.00440 <sup>‡</sup>	4	0.00440 <sup>‡</sup>	0.00440 <sup>‡</sup>	0.00440 <sup>‡</sup>
6	0.0318 <sup>†</sup>	0.0224	0.00938 <sup>‡</sup>	6	0.0214 <sup>†</sup>	0.0118	0.00955 <sup>‡</sup>	6	0.00991 <sup>‡</sup>	0.00991 <sup>‡</sup>	0.00991 <sup>‡</sup>	6	0.00991 <sup>‡</sup>	0.00991 <sup>‡</sup>	0.0107 <sup>‡</sup>
8	0.0497 <sup>†</sup>	0.0397	0.0100 <sup>‡</sup>	8	0.0321 <sup>†</sup>	0.0158	0.0163 <sup>‡</sup>	8	0.0169 <sup>‡</sup>	0.0169 <sup>‡</sup>	0.0169 <sup>‡</sup>	8	0.0169 <sup>‡</sup>	0.0169 <sup>‡</sup>	0.0182 <sup>‡</sup>
10	0.0696 <sup>†</sup>	0.0570	0.0226 <sup>‡</sup>	10	0.0439 <sup>†</sup>	0.0197	0.0242 <sup>‡</sup>	10	0.0251 <sup>‡</sup>	0.0251 <sup>‡</sup>	0.0251 <sup>‡</sup>	10	0.0251 <sup>‡</sup>	0.0251 <sup>‡</sup>	0.0269 <sup>‡</sup>
15	0.0857 <sup>†</sup>	0.0657	0.0440 <sup>‡</sup>	15	0.0743 <sup>†</sup>	0.0294	0.0449 <sup>‡</sup>	15	0.0464 <sup>‡</sup>	0.0464 <sup>‡</sup>	0.0464 <sup>‡</sup>	15	0.0464 <sup>‡</sup>	0.0464 <sup>‡</sup>	0.0498 <sup>‡</sup>
20	0.134 <sup>†</sup>	0.0723	0.0614 <sup>‡</sup>	20	0.102 <sup>†</sup>	0.0391	0.0627 <sup>‡</sup>	20	0.0650 <sup>‡</sup>	0.0650 <sup>‡</sup>	0.0650 <sup>‡</sup>	20	0.0650 <sup>‡</sup>	0.0650 <sup>‡</sup>	0.0696 <sup>‡</sup>
25	0.163 <sup>†</sup>	0.0896	0.0737 <sup>‡</sup>	25	0.124 <sup>†</sup>	0.0485	0.0750 <sup>‡</sup>	25	0.0709 <sup>‡</sup>	0.0709 <sup>‡</sup>	0.0709 <sup>‡</sup>	25	0.0709 <sup>‡</sup>	0.0709 <sup>‡</sup>	0.0734 <sup>‡</sup>
30	0.189 <sup>†</sup>	0.107	0.0806 <sup>‡</sup>	30	0.140 <sup>†</sup>	0.0580	0.0823 <sup>‡</sup>	30	0.0851 <sup>‡</sup>	0.0851 <sup>‡</sup>	0.0851 <sup>‡</sup>	30	0.0851 <sup>‡</sup>	0.0851 <sup>‡</sup>	0.0913 <sup>‡</sup>
40	0.234 <sup>†</sup>	0.149	0.0942 <sup>‡</sup>	40	0.163 <sup>†</sup>	0.0766	0.0960 <sup>‡</sup>	40	0.0891 <sup>‡</sup>	0.0891 <sup>‡</sup>	0.0891 <sup>‡</sup>	40	0.0891 <sup>‡</sup>	0.0891 <sup>‡</sup>	0.0954 <sup>‡</sup>
50	0.253 <sup>†</sup>	0.172	0.0910 <sup>‡</sup>	50	0.177 <sup>†</sup>	0.0947	0.0925 <sup>‡</sup>	50	0.0952 <sup>‡</sup>	0.0952 <sup>‡</sup>	0.0952 <sup>‡</sup>	50	0.0952 <sup>‡</sup>	0.0952 <sup>‡</sup>	0.0917 <sup>‡</sup>
60	0.277 <sup>†</sup>	0.201	0.0780 <sup>‡</sup>	60	0.190 <sup>†</sup>	0.112	0.0775 <sup>‡</sup>	60	0.0801 <sup>‡</sup>	0.0801 <sup>‡</sup>	0.0801 <sup>‡</sup>	60	0.0801 <sup>‡</sup>	0.0801 <sup>‡</sup>	0.0860 <sup>‡</sup>
70	0.298 <sup>†</sup>	0.228	0.0710 <sup>‡</sup>	70	0.201 <sup>†</sup>	0.129	0.0722 <sup>‡</sup>	70	0.0748 <sup>‡</sup>	0.0748 <sup>‡</sup>	0.0748 <sup>‡</sup>	70	0.0748 <sup>‡</sup>	0.0748 <sup>‡</sup>	0.0901 <sup>‡</sup>
80	0.323 <sup>†</sup>	0.256	0.0663 <sup>‡</sup>	80	0.213 <sup>†</sup>	0.145	0.0676 <sup>‡</sup>	80	0.0699 <sup>‡</sup>	0.0699 <sup>‡</sup>	0.0699 <sup>‡</sup>	80	0.0699 <sup>‡</sup>	0.0699 <sup>‡</sup>	0.0749 <sup>‡</sup>
90	0.343 <sup>†</sup>	0.281	0.0620 <sup>‡</sup>	90	0.224 <sup>†</sup>	0.161	0.0631 <sup>‡</sup>	90	0.0653 <sup>‡</sup>	0.0653 <sup>‡</sup>	0.0653 <sup>‡</sup>	90	0.0653 <sup>‡</sup>	0.0653 <sup>‡</sup>	0.0700 <sup>‡</sup>
100	0.363 <sup>†</sup>	0.305	0.0580 <sup>‡</sup>	100	0.235 <sup>†</sup>	0.176	0.0592 <sup>‡</sup>	100	0.0613 <sup>‡</sup>	0.0613 <sup>‡</sup>	0.0613 <sup>‡</sup>	100	0.0613 <sup>‡</sup>	0.0613 <sup>‡</sup>	0.0655 <sup>‡</sup>
150	0.450 <sup>†</sup>	0.411	0.0442 <sup>‡</sup>	150	0.293 <sup>†</sup>	0.248	0.0451 <sup>‡</sup>	150	0.0467 <sup>‡</sup>	0.0467 <sup>‡</sup>	0.0467 <sup>‡</sup>	150	0.0467 <sup>‡</sup>	0.0467 <sup>‡</sup>	0.0501 <sup>‡</sup>
200	0.534 <sup>†</sup>	0.499	0.0357 <sup>‡</sup>	200	0.347 <sup>†</sup>	0.311	0.0364 <sup>‡</sup>	200	0.0377 <sup>‡</sup>	0.0377 <sup>‡</sup>	0.0377 <sup>‡</sup>	200	0.0377 <sup>‡</sup>	0.0377 <sup>‡</sup>	0.0404 <sup>‡</sup>
250	0.600 <sup>†</sup>	0.576	0.0300 <sup>‡</sup>	250	0.399 <sup>†</sup>	0.368	0.0306 <sup>‡</sup>	250	0.0317 <sup>‡</sup>	0.0317 <sup>‡</sup>	0.0317 <sup>‡</sup>	250	0.0317 <sup>‡</sup>	0.0317 <sup>‡</sup>	0.0340 <sup>‡</sup>
273	0.630 <sup>†</sup>	0.607	0.0280 <sup>‡</sup>	273	0.422 <sup>†</sup>	0.393	0.0286 <sup>‡</sup>	273	0.0296 <sup>‡</sup>	0.0296 <sup>‡</sup>	0.0296 <sup>‡</sup>	273	0.0296 <sup>‡</sup>	0.0296 <sup>‡</sup>	0.0318 <sup>‡</sup>
300	0.666	0.643	0.0280 <sup>‡</sup>	300	0.446	0.420	0.0265 <sup>‡</sup>	300	0.278 <sup>†</sup>	0.278 <sup>†</sup>	0.278 <sup>†</sup>	300	0.442 <sup>‡</sup>	0.412	0.0295 <sup>‡</sup>
350	0.722 <sup>†</sup>	0.699	0.0230 <sup>‡</sup>	350	0.489 <sup>†</sup>	0.466	0.0234 <sup>‡</sup>	350	0.0243 <sup>‡</sup>	0.0243 <sup>‡</sup>	0.0243 <sup>‡</sup>	350	0.477 <sup>‡</sup>	0.451	0.0280 <sup>‡</sup>
400	0.768 <sup>†</sup>	0.748	0.0205 <sup>‡</sup>	400	0.529 <sup>†</sup>	0.508	0.0209 <sup>‡</sup>	400	0.0217 <sup>‡</sup>	0.0217 <sup>‡</sup>	0.0217 <sup>‡</sup>	400	0.507 <sup>‡</sup>	0.484	0.0233 <sup>‡</sup>
500	0.845 <sup>†</sup>	0.825	0.0170 <sup>‡</sup>	500	0.596 <sup>†</sup>	0.579	0.0174 <sup>‡</sup>	500	0.0180 <sup>‡</sup>	0.0180 <sup>‡</sup>	0.0180 <sup>‡</sup>	500	0.556 <sup>‡</sup>	0.537	0.0183 <sup>‡</sup>
600	0.890 <sup>†</sup>	0.883	0.0146 <sup>‡</sup>	600	0.652 <sup>†</sup>	0.637	0.0148 <sup>‡</sup>	600	0.0154 <sup>‡</sup>	0.0154 <sup>‡</sup>	0.0154 <sup>‡</sup>	600	0.593 <sup>†</sup>	0.576	0.0166 <sup>‡</sup>
700	0.941 <sup>†</sup>	0.938	0.0137 <sup>‡</sup>	700	0.698 <sup>†</sup>	0.685	0.0130 <sup>‡</sup>	700	0.0135 <sup>‡</sup>	0.0135 <sup>‡</sup>	0.0135 <sup>‡</sup>	700	0.620 <sup>†</sup>	0.606	0.0144 <sup>‡</sup>
800	0.971 <sup>†</sup>	0.960	0.0113 <sup>‡</sup>	800	0.735 <sup>†</sup>	0.723	0.0116 <sup>‡</sup>	800	0.0120 <sup>‡</sup>	0.0120 <sup>‡</sup>	0.0120 <sup>‡</sup>	800	0.642 <sup>†</sup>	0.629	0.0128 <sup>‡</sup>
900	0.983 <sup>†</sup>	0.972	0.0103 <sup>‡</sup>	900	0.763 <sup>†</sup>	0.753	0.0104 <sup>‡</sup>	900	0.0108 <sup>‡</sup>	0.0108 <sup>‡</sup>	0.0108 <sup>‡</sup>	900	0.659 <sup>†</sup>	0.647	0.0116 <sup>‡</sup>
				933	0.773 <sup>†</sup>	0.763	0.0101 <sup>‡</sup>	1000	0.00990 <sup>‡</sup>	0.00990 <sup>‡</sup>	0.00990 <sup>‡</sup>	1000	0.671 <sup>†</sup>	0.660	0.0106 <sup>‡</sup>
								1100	0.00902 <sup>‡</sup>	0.00902 <sup>‡</sup>	0.00902 <sup>‡</sup>	1200	0.686 <sup>†</sup>	0.677	0.00896 <sup>‡</sup>
								1224	0.00821 <sup>‡</sup>	0.00821 <sup>‡</sup>	0.00821 <sup>‡</sup>	1308	0.691 <sup>†</sup>	0.683	0.00832 <sup>‡</sup>

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:38.00 Al - 78.00 Cu:  $\pm 2\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 8\%$  above 200 K.25.00 Al - 75.00 Cu:  $\pm 3\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 8\%$  above 200 K.20.00 Al - 80.00 Cu:  $\pm 2\%$  at 300 K.15.00 Al - 85.00 Cu:  $\pm 2\%$  above 300 K.

‡ Provisional values.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 10.00% (20.77 At.%) Cu: 90.00% (79.23 At.%)				Al: 5.00% (11.03 At.%) Cu: 95.00% (88.97 At.%)				Al: 3.00% (6.79 At.%) Cu: 97.00% (93.21 At.%)				Al: 1.00% (2.32 At.%) Cu: 99.00% (97.68 At.%)			
ρ <sub>0</sub> = 7.23 μΩcm				ρ <sub>0</sub> = 5.53 μΩcm				ρ <sub>0</sub> = 2.36 μΩcm							
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4			0.00322 <sup>‡</sup>	4	0.0197	0.0134	0.00628 <sup>‡</sup>	4	0.0259	0.0177	0.00816 <sup>‡</sup>	4	0.0331	0.0412	0.0119 <sup>‡</sup>
6			0.0118 <sup>‡</sup>	6	0.0345	0.0204	0.0141 <sup>‡</sup>	6	0.0450	0.0265	0.0185 <sup>‡</sup>	6	0.0686	0.0363	0.0267 <sup>‡</sup>
8			0.0201 <sup>‡</sup>	8	0.0509	0.0288	0.0241 <sup>‡</sup>	8	0.0689	0.0352	0.0317 <sup>‡</sup>	8	0.129	0.0834	0.0468 <sup>‡</sup>
10			0.0290 <sup>‡</sup>	10	0.0694	0.0386	0.0358 <sup>‡</sup>	10	0.0896	0.0441	0.0455 <sup>‡</sup>	10	0.173	0.103	0.0700 <sup>‡</sup>
15			0.0551 <sup>‡</sup>	15	0.116	0.0495	0.0662 <sup>‡</sup>	15	0.151	0.0654	0.0856 <sup>‡</sup>	15	0.284	0.183	0.131 <sup>‡</sup>
20			0.0772 <sup>‡</sup>	20	0.159	0.0665	0.0922 <sup>‡</sup>	20	0.207	0.0867	0.120 <sup>‡</sup>	20	0.382	0.201	0.181 <sup>‡</sup>
25			0.0924 <sup>‡</sup>	25	0.193	0.0824	0.111 <sup>‡</sup>	25	0.249	0.106	0.143 <sup>‡</sup>	25	0.463	0.250	0.213 <sup>‡</sup>
30			0.101 <sup>‡</sup>	30	0.220	0.0984	0.122 <sup>‡</sup>	30	0.282	0.128	0.157 <sup>‡</sup>	30	0.538	0.288	0.239 <sup>‡</sup>
40			0.166 <sup>‡</sup>	40	0.257	0.130	0.127 <sup>‡</sup>	40	0.329	0.169	0.160 <sup>‡</sup>	40	0.619	0.389	0.290 <sup>‡</sup>
50			0.192 <sup>‡</sup>	50	0.283	0.161	0.122 <sup>‡</sup>	50	0.361	0.209	0.182 <sup>‡</sup>	50	0.687	0.474	0.213 <sup>‡</sup>
60			0.0963 <sup>‡</sup>	60	0.304	0.189	0.115 <sup>‡</sup>	60	0.388	0.246	0.142 <sup>‡</sup>	60	0.746	0.551	0.195 <sup>‡</sup>
70			0.0906 <sup>‡</sup>	70	0.324	0.217	0.107 <sup>‡</sup>	70	0.414	0.283	0.131 <sup>‡</sup>	70	0.796	0.618	0.178 <sup>‡</sup>
80			0.0831 <sup>‡</sup>	80	0.344 <sup>‡</sup>	0.244	0.0993 <sup>‡</sup>	80	0.440 <sup>‡</sup>	0.318	0.122 <sup>‡</sup>	80	0.832 <sup>‡</sup>	0.688	0.164 <sup>‡</sup>
90			0.0779 <sup>‡</sup>	90	0.364 <sup>‡</sup>	0.271	0.0931 <sup>‡</sup>	90	0.465 <sup>‡</sup>	0.352	0.113 <sup>‡</sup>	90	0.902 <sup>‡</sup>	0.751	0.151 <sup>‡</sup>
100			0.0730 <sup>‡</sup>	100	0.385 <sup>‡</sup>	0.298	0.0873 <sup>‡</sup>	100	0.491 <sup>‡</sup>	0.386	0.105 <sup>‡</sup>	100	0.953 <sup>‡</sup>	0.813	0.140 <sup>‡</sup>
150			0.0555 <sup>‡</sup>	150	0.496 <sup>‡</sup>	0.420	0.0665 <sup>‡</sup>	150	0.618 <sup>‡</sup>	0.540	0.0782 <sup>‡</sup>	150	1.18 <sup>‡</sup>	1.08	0.103 <sup>‡</sup>
200	0.462 <sup>‡</sup>	0.387	0.0448 <sup>‡</sup>	200	0.581 <sup>‡</sup>	0.527	0.0538 <sup>‡</sup>	200	0.740 <sup>‡</sup>	0.677	0.0626 <sup>‡</sup>	200	1.38 <sup>‡</sup>	1.30	0.0816 <sup>‡</sup>
250	0.523 <sup>‡</sup>	0.494	0.0377 <sup>‡</sup>	250	0.673 <sup>‡</sup>	0.628	0.0453 <sup>‡</sup>	250	0.854 <sup>‡</sup>	0.802	0.0525 <sup>‡</sup>	250	1.55 <sup>‡</sup>	1.48	0.0678 <sup>‡</sup>
273	0.560 <sup>‡</sup>	0.530	0.0359 <sup>‡</sup>	273	0.713 <sup>‡</sup>	0.671	0.0433 <sup>‡</sup>	273	0.903 <sup>‡</sup>	0.854	0.0489 <sup>‡</sup>	273	1.63 <sup>‡</sup>	1.57	0.0638 <sup>‡</sup>
300	0.596	0.563	0.0327 <sup>‡</sup>	300	0.757	0.718	0.0391 <sup>‡</sup>	300	0.960	0.915	0.0432 <sup>‡</sup>	300	1.71	1.65	0.0590 <sup>‡</sup>
350	0.665	0.636	0.0289 <sup>‡</sup>	350	0.835	0.800	0.0348 <sup>‡</sup>	350	1.06	1.02	0.0398 <sup>‡</sup>	350	1.83	1.78	0.0506 <sup>‡</sup>
400	0.739	0.704	0.0259 <sup>‡</sup>	400	0.905	0.874	0.0309 <sup>‡</sup>	400	1.15	1.11	0.0366 <sup>‡</sup>	400	1.94	1.89	0.0450 <sup>‡</sup>
500	0.959	0.922	0.0214 <sup>‡</sup>	500	1.03	1.00	0.0257 <sup>‡</sup>	500	1.30	1.27	0.0294 <sup>‡</sup>	500	2.10	2.06	0.0368 <sup>‡</sup>
600	0.941	0.923	0.0183 <sup>‡</sup>	600	1.13	1.11	0.0230 <sup>‡</sup>	600	1.43 <sup>‡</sup>	1.40	0.0251 <sup>‡</sup>	600	2.22 <sup>‡</sup>	2.19	0.0310 <sup>‡</sup>
700	1.03	1.01	0.0160 <sup>‡</sup>	700	1.22	1.20	0.0192 <sup>‡</sup>	700	1.51 <sup>‡</sup>	1.49	0.0219 <sup>‡</sup>	700	2.31 <sup>‡</sup>	2.28	0.0268 <sup>‡</sup>
800	1.09	1.06	0.0143 <sup>‡</sup>	800	1.30	1.28	0.0171 <sup>‡</sup>	800	1.59 <sup>‡</sup>	1.57	0.0195 <sup>‡</sup>	800	2.37 <sup>‡</sup>	2.35	0.0236 <sup>‡</sup>
900	1.14	1.13	0.0123 <sup>‡</sup>	900	1.36	1.34	0.0154 <sup>‡</sup>	900	1.66 <sup>‡</sup>	1.64	0.0175 <sup>‡</sup>	900	2.41 <sup>‡</sup>	2.39	0.0211 <sup>‡</sup>
1000	1.18	1.17	0.0117 <sup>‡</sup>	1000	1.39	1.38	0.0140 <sup>‡</sup>	1000	1.70 <sup>‡</sup>	1.68	0.0168 <sup>‡</sup>	1000	2.44 <sup>‡</sup>	2.42	0.0190 <sup>‡</sup>
1200	1.25	1.24	0.00991 <sup>‡</sup>	1200	1.47 <sup>‡</sup>	1.46	0.0119 <sup>‡</sup>	1200	1.77 <sup>‡</sup>	1.76	0.0135 <sup>‡</sup>	1200	2.48 <sup>‡</sup>	2.46	0.0159 <sup>‡</sup>
1351	1.27	1.26	0.00918 <sup>‡</sup>	1351	1.50 <sup>‡</sup>	1.49	0.0108 <sup>‡</sup>	1351	1.80 <sup>‡</sup>	1.79	0.0123 <sup>‡</sup>	1351	2.49 <sup>‡</sup>	2.48	0.0142 <sup>‡</sup>

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

10.00 Al - 90.00 Cu: ±10% above 200 K.

5.00 Al - 95.00 Cu: ±5% below 80 K, ±6% between 80 and 500 K, and ±5% above 500 K.

3.00 Al - 97.00 Cu: ±5% below 80 K, ±5% between 80 and 500 K, and ±7% above 500 K.

1.00 Al - 99.00 Cu: ±5% below 80 K, ±5% between 80 and 500 K, and ±6% above 500 K.

<sup>‡</sup> Provisional values.<sup>§</sup> Typical values.<sup>•</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 2. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-COPPER ALLOY SYSTEM (continued)†  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 0.50% (1.17 At. %) Cu: 99.50% (98.83 At. %)					
ρ <sub>0</sub> = 1.370 μΩcm					
T	k	k <sub>e</sub>	k <sub>g</sub>		
4	0.0011	0.0771	0.0140		
6	0.146	0.115	0.0314		
8	0.200	0.154	0.0552		
10	0.277	0.192	0.0854		
15	0.445	0.282	0.163		
20	0.591	0.369	0.222		
25	0.715	0.455	0.260		
30	0.819	0.530	0.280		
40	0.975	0.695	0.290		
50	1.09	0.832	0.290		
60	1.18	0.945	0.296		
70	1.26	1.05	0.214		
80	1.34*	1.15	0.195		
90	1.40*	1.22	0.190		
100	1.47*	1.30	0.166		
150	1.74*	1.62	0.1218		
200	1.96*	1.87	0.0960*		
250	2.14*	2.06	0.0786*		
273	2.21*	2.14	0.07318		
300	2.28	2.21	0.06734		
350	2.39	2.33	0.0585*		
400	2.49	2.44	0.0520*		
500	2.63*	2.59	0.0422*		
600	2.73*	2.69	0.03558		
700	2.76*	2.73	0.03068		
800	2.79*	2.76	0.0268*		
900	2.86*	2.78	0.0239*		
1000	2.89*	2.78	0.0215*		
1200	2.79*	2.77	0.0180*		
1354	2.76*	2.74	0.0160*		

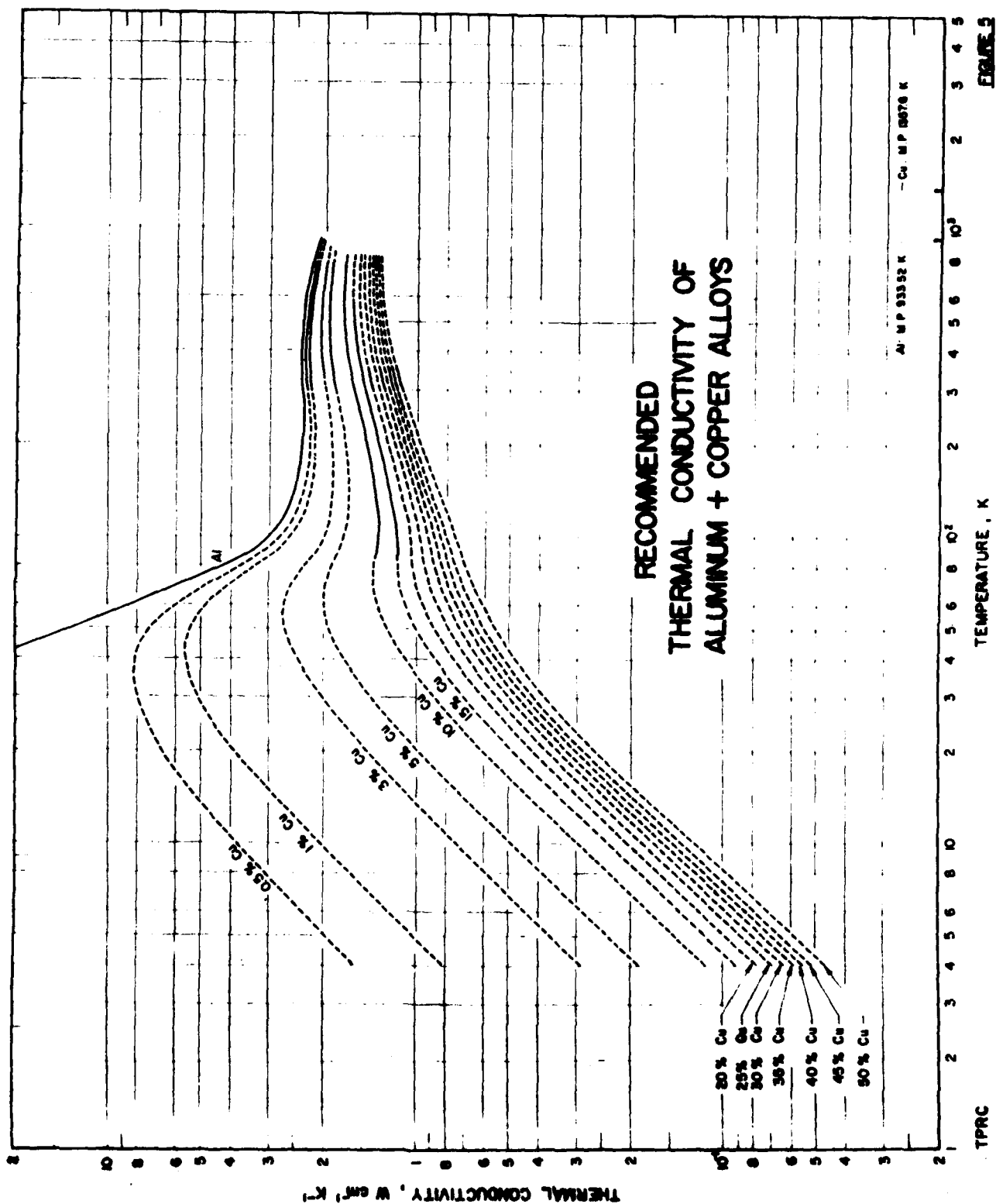
† Uncertainties of the total thermal conductivity, k, are as follows:

0.50 Al - 99.50 Cu: ±6% below 80 K, ±5% between 80 and 500 K, and ±6% above 500 K.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.





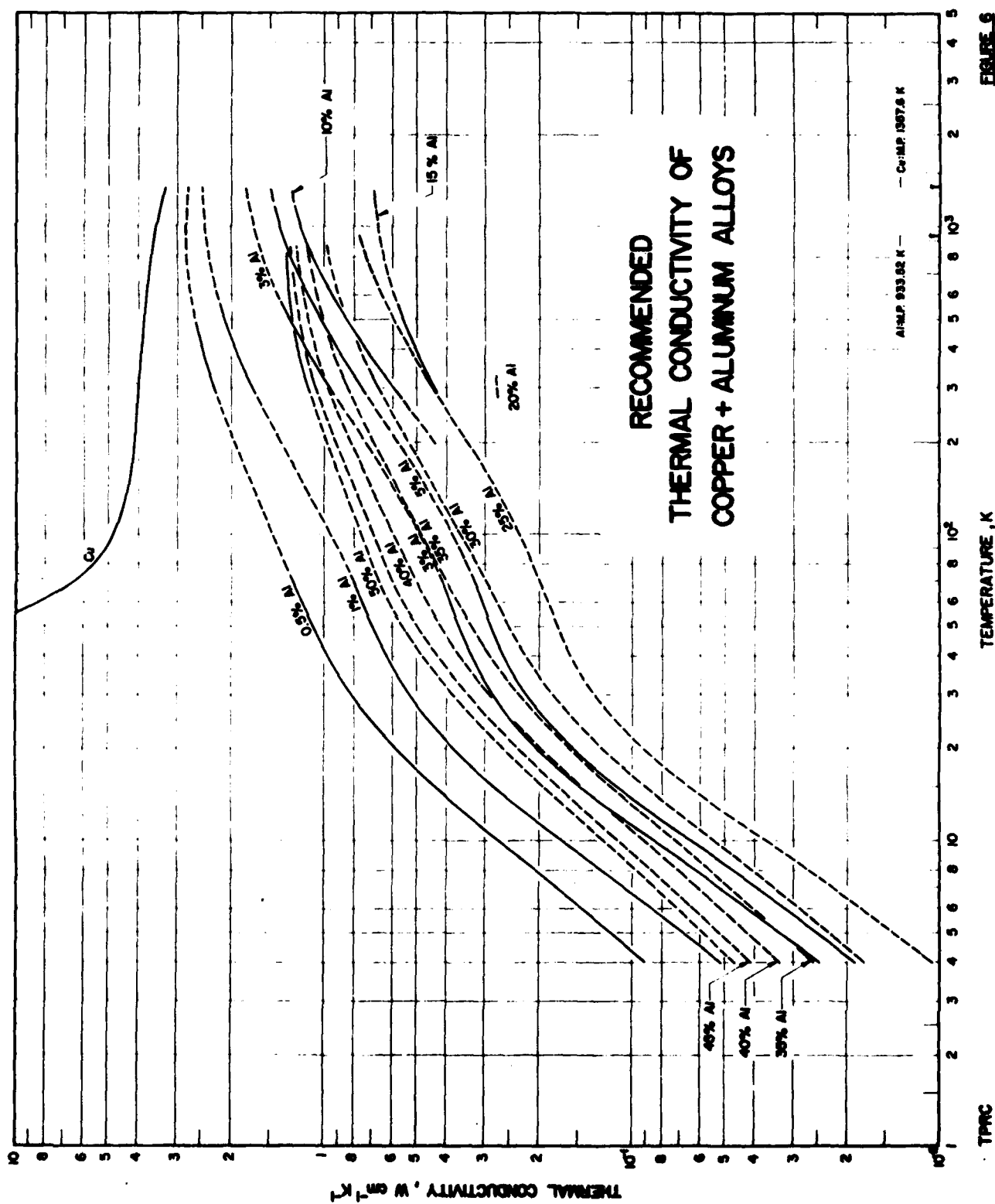


FIGURE 6

TPRC

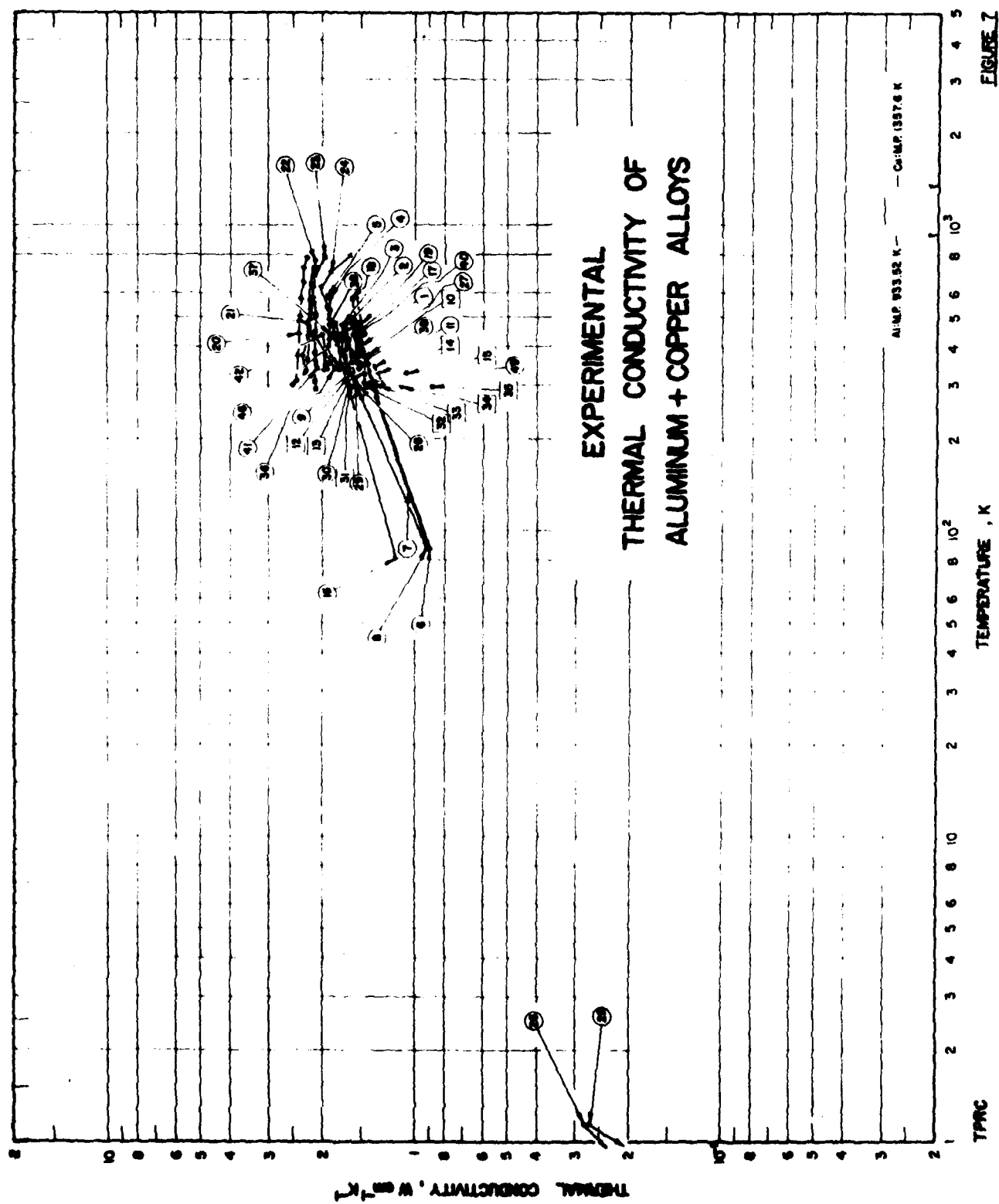


FIGURE 7

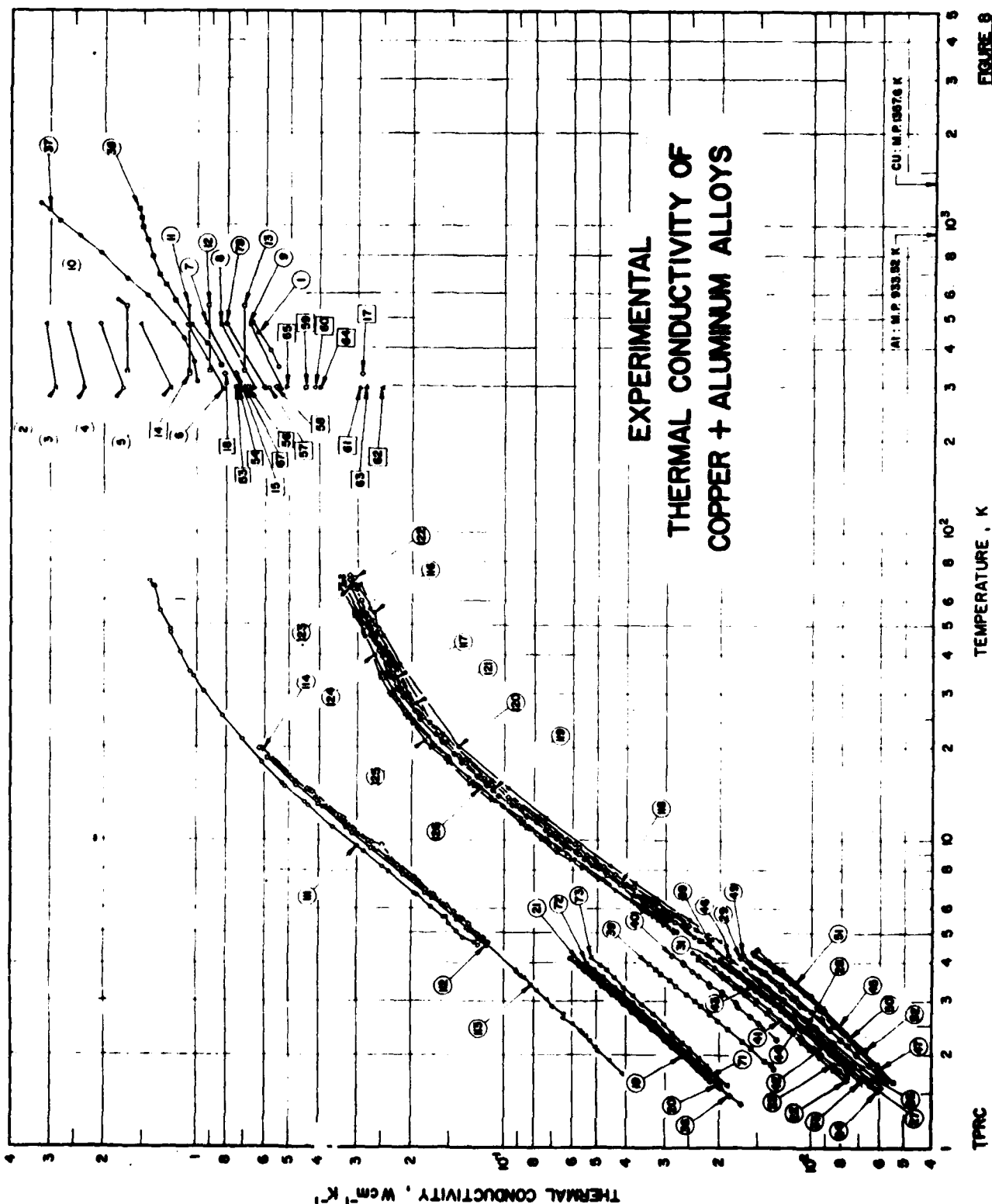


TABLE 3. THERMAL CONDUCTIVITY OF ALUMINUM + COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Al	Cu	
1 44	Griffiths, E. and Schofield, F.H.	1928	L	353-473	No. 655	96.0	14.0	1.125 in. diameter and 15.5 in. long; 2 specimens chill-cast and 2 specimens sand-cast; one of each annealed at 450 C for 1 hr; electrical resistivity reported as 5.24, 6.26, 6.97, 7.69, 8.40, and 9.14 $\mu\Omega$ cm at 353, 423, 473, 523, 573, and 623 K, respectively; smoothed values reported.
2 44	Griffiths, E. and Schofield, F.H.	1928	L	353-473	No. 671	88.0	12.0	Similar to above except electrical resistivity reported as 5.20, 5.96, 6.51, 7.03, 7.57, and 8.11 $\mu\Omega$ cm at 353, 423, 473, 523, 573, and 623 K, respectively.
3 44	Griffiths, E. and Schofield, F.H.	1928	L	353-473	No. 921	~88.0	~12.0	Trace Fe; 1.125 in. diameter and 15.5 in. long; 2 specimens chill-cast; one of which annealed at 450 C for 1 hr; electrical resistivity reported as 4.64, 5.61, 6.34, 7.12, 7.98, and 8.82 $\mu\Omega$ cm at 353, 423, 473, 523, 573, and 623 K, respectively; smoothed values reported.
4 44	Griffiths, E. and Schofield, F.H.	1928	L	353-573	No. 2313	92.0	8.0	Similar to above except electrical resistivity reported as 4.06, 4.77, 5.40, 6.16, 7.03, and 8.08 $\mu\Omega$ cm at 353, 423, 473, 523, 573, and 623 K, respectively.
5 44	Griffiths, E. and Schofield, F.H.	1928	L	353-573	No. 2312	95.5	4.5	Similar to above except electrical resistivity reported as 4.04, 4.96, 5.61, 6.26, 6.92, and 7.58 $\mu\Omega$ cm at 353, 423, 473, 523, 573, and 623 K, respectively.
6 41	Mannchen, W.	1931	L	87-476		92.0	8.0	Cast; electrical conductivity reported as 65.1, 29.3, 26.2, and 14.6 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively; Lorenz function 1.549, 1.650, 1.891, and 2.18 $\times 10^{-6} \text{ V}^2 \text{ K}^{-1}$ at the above temperatures, respectively.
7* 41	Mannchen, W.	1931	L	87-476				The above specimen; Lorenz function 1.58, 1.64, 1.94, and 2.30 $\times 10^{-6} \text{ V}^2 \text{ K}^{-1}$ at the above temperatures, respectively.
8 41	Mannchen, W.	1931	L	87-476		85.0	15.0	Cast; electrical conductivity reported as 59.6, 22.3, 16.0, and 14.2 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively; Lorenz function 1.74, 2.43, 2.79, and 2.67 $\times 10^{-6} \text{ V}^2 \text{ K}^{-1}$ at the above temperatures, respectively.
9 113	Grand, C. and Villey, J.	1927	E	353-423		96.0	4.0	Approximate composition; cast.
10 113	Grand, C. and Villey, J.	1927	E	373.2		88.0	12.0	Cast; density 2.95 g $\text{cm}^{-3}$ ; electrical conductivity 0.16 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 100 C.
11 114	Cacchirelli, J.	1921		301-346		92.0	~8.0	Trace Si; density 2.86 to 2.9 g $\text{cm}^{-3}$ .
12 45	Smith, A.W.	1925	L	326.2		90.0	10.0	1.9 cm in diameter and 10 cm long; prepared by fusing 99.97% pure aluminum and copper supplied by Baker; electrical conductivity 28.6 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
13 45	Smith, A.W.	1925	L	326.2		80.0	20.0	Similar to above except electrical conductivity 20.9 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
14 45	Smith, A.W.	1925	L	326.2		70.0	30.0	Similar to above except electrical conductivity 18.5 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
15 45	Smith, A.W.	1925	L	326.2		50.0	50.0	Similar to above except electrical conductivity 15.3 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
16 42	Eucken, A. and Warrentup, H.	1935	R	51.273		96.0	4.0	Cast sheet; annealed at 510 C for 45 min and quenched in ice water; electrical resistivity 1.409 and 3.600 $\mu\Omega$ cm at -192 and 0 C, respectively.

\* Not shown in figure.

TABLE 3. THERMAL CONDUCTIVITY OF ALUMINUM - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Al	Composition Cu	Composition (continued), Specifications, and Remarks
17 46	Griffiths, E. and Shakespear, G.A.	1922	L	353-453	V 671 A	85.0	12.0	15 in. long and 1 in. in diameter; supplied by Metallurgical Dept. of National Physical Laboratory (England); chill-cast.
18 46	Griffiths, E. and Shakespear, G.A.	1922	L	373-573	V 671 D	88.0	12.0	Prepared from commercially pure aluminum; 15 in. long and 1 in. in diameter; supplied by Metallurgical Dept. of National Physical Lab.; annealed at 450 C.
19 46	Griffiths, E. and Shakespear, G.A.	1922	L	373-573	V 671 C	88.0	12.0	Similar to above specimen except sand-cast.
20 58	Mikryukov, V.E. and Karagetyan, A.G.	1961	E	288-777		99.5	0.5	3 mm diameter and 300 mm long; prepared from 99.9 pure Al.
21 58	Mikryukov, V.E. and Karagetyan, A.G.	1961	E	328-723		99.0	1.0	Similar to above.
22 58	Mikryukov, V.E. and Karagetyan, A.G.	1961	E	333-762		96.0	4.0	Similar to above.
23 58	Mikryukov, V.E. and Karagetyan, A.G.	1961	E	288-781		93.0	7.0	Similar to above.
24 58	Mikryukov, V.E. and Karagetyan, A.G.	1961	E	334-792		90.0	10.0	Similar to above.
25 43	Setherthwaite, C.B.	1962	L	0.4-1.2	Al-26		0.3	Bar specimen with end sections machined to 0.5 in. diameter and 0.375 in. long, and with center portion 3.2 cm long milled to 0.5 mm thick and 2 mm wide; electrical resistivity ratio $\rho(273K)/\rho(1.2K) = 28$ ; transition temperature (a.c.) $T_c = 1.148 K$ ; in superconducting state.
26 43	Setherthwaite, C.B.	1962	L	0.4-1.2	Al-26			The above specimen measured in normal state; reported values calculated from the given formula $k = 0.242 T (W cm^{-1} K^{-1})$ in the same temperature range as above.
27 115	Ellis, M.	1937	L	298-398	I, 1		5	Cylindrical specimen 1.5 cm in diameter and 3.0 cm in length; cast from 98 to 99 pure Al bar (contamination: < 1.0 Fe, < 0.9 Si, and < 0.1 Cu + Zn) and key alloy (50 Al and 50 Cu) at 750 C, and then cooled in air; electrical resistivity reported as $5.00 \mu\Omega$ cm at 20 C.
28 115	Ellis, M.	1937	L	298-398	I, 5		5	Similar to the above specimen except 99.5 pure Al notch bar (contamination: 0.28 Fe and 0.22 Si) used for the melting; electrical resistivity reported as $4.56 \mu\Omega$ cm at 20 C.
29 115	Ellis, M.	1937	L	298-398	I, 5A		5	Similar to the above specimen except electrical resistivity reported as $4.66 \mu\Omega$ cm at 20 C.
30 115	Ellis, M.	1937	L	298-398	I, 5B		5	Similar to the above specimen except electrical resistivity reported as $4.42 \mu\Omega$ cm at 20 C.
31 116, 168	Aher, M.A.	1953	L	295.2	1		10.24	1.25 cm <sup>2</sup> in cross-section and 0.64 cm thick; electrical conductivity $21.18 \times 10^4 \Omega^{-1} cm^{-1}$ ; total Lorens function $2.564 \times 10^4 V^2 K^2$ .
32 116, 168	Aher, M.A.	1953	L	295.2	2		20.78	1.25 cm <sup>2</sup> in cross-section and 0.79 cm thick; electrical conductivity $18.79 \times 10^4 \Omega^{-1} cm^{-1}$ ; total Lorens function $2.994 \times 10^4 V^2 K^2$ .
33 116, 168	Aher, M.A.	1953	L	295.2	3		30.32	1.25 cm <sup>2</sup> in cross-section and 0.90 cm thick; electrical conductivity $16.72 \times 10^4 \Omega^{-1} cm^{-1}$ ; total Lorens function $2.682 \times 10^4 V^2 K^2$ .

TABLE 3. THERMAL CONDUCTIVITY OF ALUMINUM - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Al Cu	Composition (continued), Specifications, and Remarks
34 116, 169	Alien, N.A.	1953	L	295.2	4	40.82	1.25 cm <sup>2</sup> in cross-section and 0.68 cm thick; electrical conductivity $15.26 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.455 \times 10^{-6} \text{ V}^2 \text{ K}^{-2}$ .
35 116, 169	Alien, N.A.	1953	L	295.2	5	48.00	1.25 cm <sup>2</sup> in cross-section and 0.70 cm thick; electrical conductivity $12.41 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.378 \times 10^{-6} \text{ V}^2 \text{ K}^{-2}$ .
36 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	3	98.47 1.01	0.209 Fe; original composition reported as 98.99 Al (containing 0.21 Fe and 0.29 Si) and 0.287 Si; as cast.
37 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	5	94.47 5.06	0.199 Fe; original composition reported as 94.94 Al (containing 0.21 Fe and 0.29 Si) and 0.275 Si; as cast.
38 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	6	92.34 7.20	0.195 Fe; original composition reported as 92.80 Al (containing 0.21 Fe and 0.29 Si) and 0.269 Si; as cast.
39 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	8	88.05 11.51	0.186 Fe; original composition reported as 88.49 Al (containing 0.21 Fe and 0.29 Si) and 0.257 Si; as cast.
40 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	9	79.52 15.46	0.78 Fe; original composition reported as 84.54 Al (containing 0.21 Fe and 0.29 Si) and 0.245 Si; as cast.
41 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	3A	98.49 1.01	0.209 Fe; original composition reported as 98.49 Al (containing 0.21 Fe and 0.29 Si) and 0.287 Si; as cast.
42 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	5A	94.47 5.06	0.199 Fe; original composition reported as 94.94 Al (containing 0.21 Fe and 0.29 Si) and 0.275 Si; annealed at 500 C for 24 hr, furnace cooled.
43 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	6A	92.34 7.20	0.195 Fe; original composition reported as 92.80 Al (containing 0.21 Fe and 0.29 Si) and 0.269 Si; annealed at 500 C for 24 hr, furnace cooled.
44 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	8A	88.05 11.51	0.186 Fe; original composition reported as 88.49 Al (containing 0.21 Fe and 0.29 Si) and 0.257 Si; annealed at 500 C for 24 hr, furnace cooled.
45 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	9A	84.12 15.46	0.178 Fe; original composition reported as 84.54 Al (containing 0.21 Fe and 0.29 Si) and 0.245 Si; annealed at 500 C for 24 hr, furnace cooled.
46 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	10A	79.52 20.08	0.166 Fe; original composition reported as 79.92 Al (containing 0.21 Fe and 0.29 Si) and 0.232 Si; annealed at 500 C for 24 hr, furnace cooled.
47 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	11A	74.03 25.60	0.156 Fe; original composition reported as 74.40 Al (containing 0.21 Fe and 0.29 Si) and 0.216 Si; annealed at 500 C for 24 hr, furnace cooled.
48 47	Hanson, D. and Rodgers, C.E.	1932	L	338, 438	12A	69.17 30.46	0.146 Fe; original composition reported as 69.54 Al (containing 0.21 Fe and 0.29 Si) and 0.202 Si; annealed at 500 C for 24 hr, furnace cooled.
49 47	Hanson, D. and Rodgers, C.E.	1932	L	303, 373	10	79.52 20.08	0.165 Fe; original composition reported as 79.92 Al (containing 0.21 Fe and 0.29 Si) and 0.232 Si; as cast.

\* Not shown in figure.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER - ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
1 44	Griffiths, E. and Schofield, F.H.	1928	L	343-450	Aluminum bronze; 6	90.0 10.9	2.53 cm in diameter and 38 cm long; chill-cast and annealed; electrical resistivity reported as 14.7, 15.6, 16.0, 16.7, 17.5, and 18.3 $\mu\Omega$ cm at 293, 348, 373, 423, 473, and 523 K, respectively.
2 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	100	99.77 0.22	0.01 Fe; 0.75 in. in diameter and 8 in. long; rolled, annealed, and cold-drawn; heat-treated at 750 C for 2 hr; electrical conductivity reported as 41.91 and 27.59 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
3 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	101	99.47 0.47	0.02 Fe; similar to the above specimen except electrical conductivity reported as 32.10 and 22.91 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
4 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	76	99.20 0.71	0.09 Fe; similar to the above specimen except heat-treated at 700 C; electrical conductivity reported as 23.40 and 17.95 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
5 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	77	98.08 1.89	0.03 Fe; similar to the above specimen except electrical conductivity reported as 15.91 and 13.00 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
6 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	45	95.25 4.61	0.14 Fe; similar to the above specimen except electrical conductivity reported as 10.26 and 8.824 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
7 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	46	92.15 7.72	0.13 Fe; 0.75 in. in diameter and 8 in. long; rolled, annealed, and cold-drawn; heat-treated at 750 C for 3.5 hr; slowly cooled in furnace; electrical conductivity reported as 8.834 and 7.68 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
8 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	102	90.56 9.37	0.07 Fe; similar to the above specimen except heat-treated at 750 C for 2 hr, then very slowly cooled in furnace to 550 C, held for 4 hr, again furnace-cooled to 450 C, held for 16 hr, cooled to room temperature; electrical conductivity reported as 8.24 and 7.064 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
9 49	Smith, C.S. and Palmer, E.W.	1935	L	293, 473	130	87.76 12.15	0.09 Fe; similar to the above specimen except electrical conductivity reported as 6.925 and 5.738 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
10 47	Hanson, D. and Rodgers, C.E.	1932	L	333, 543	30a	98.25 1.75	Prepared from Al (containing 0.21 Fe, 0.29 Si) and high grade Cu; 0.5 in. diameter and 6.5 in. long; cast in iron mould 7 in. long and 9/16 in. in diameter, machined to size; annealed at 500 C.
11 47	Hanson, D. and Rodgers, C.E.	1932	L	333, 543	29	94.90 5.10	Similar to the above specimen.
12 47	Hanson, D. and Rodgers, C.E.	1932	L	333, 543	27a	91.55 8.45	Similar to the above specimen.
13 47	Hanson, D. and Rodgers, C.E.	1932	L	333, 543	25	87.22 12.78	Similar to the above specimen.
14 45	Smith, A.W.	1925	L	326.2		50.0 50.0	1.9 cm in diameter and 10 cm long; prepared by double-fusing the Baker's analyzed copper and aluminum; electrical conductivity 15.3 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 23 C.
15 45	Smith, A.W.	1925	L	326.2		60.0 40.0	Similar to the above specimen except electrical conductivity 10.6 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 23 C.
16 45	Smith, A.W.	1925	L	326.2		70.0 30.0	Similar to the above specimen except electrical conductivity 2.76 $\times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 23 C.



TABLE 4. THERMAL CONDUCTIVITY OF COPPER + ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
17	Smith, A.W.	1925	L	326.2		80.0 20.0	Similar to the above specimen except electrical conductivity $3.60 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
18	Smith, A.W.	1925	L	326.2		90.0 10.0	Similar to the above specimen except electrical conductivity $9.98 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 23 C.
19	Salter, J.A.M. and Charley, P.	1967	L	1.7-4.2	2S	99.17 0.83	Calculated composition; single crystal; grown in a sealed graphite mould using the Bridgman technique; annealed in vacuo at 750 C for 14 hr; residual electrical resistivity $2.07 \mu\Omega \text{ cm}$ .
20	Salter, J.A.M. and Charley, P.	1967	L	1.6-4.2	2	99.10 0.90	Calculated composition; polycrystalline; rod specimen 3 mm in diameter; annealed in vacuo at 750 C for 14 hr; residual electrical resistivity $2.12 \mu\Omega \text{ cm}$ ; grain size 0.008 cm.
21	Salter, J.A.M. and Charley, P.	1967	L	1.8-4.1	2AR	99.17 0.83	Calculated composition; polycrystalline; rod specimen 3 mm in diameter; residual electrical resistivity $2.10 \mu\Omega \text{ cm}$ ; grain size 0.0015 cm.
22	Salter, J.A.M. and Charley, P.	1967	L	1.7-4.2	8S	96.69 3.31	Calculated composition; single crystal; grown in a sealed graphite mould using the Bridgman technique; annealed in vacuo at 750 C for 14 hr; residual electrical resistivity $6.50 \mu\Omega \text{ cm}$ .
23	Salter, J.A.M. and Charley, P.	1967	L	1.7-4.2	8	95.91 4.09	Calculated composition; polycrystalline; rod specimen 3 mm in diameter; annealed in vacuo at 750 C for 14 hr; grain size 0.0063 cm; residual electrical resistivity $6.63 \mu\Omega \text{ cm}$ .
24	Salter, J.A.M. and Charley, P.	1967	L	1.5-4.2	12	94.89 5.11	Calculated composition; similar to the above specimen except residual electrical resistivity $7.21 \mu\Omega \text{ cm}$ and grain size 0.011 cm.
25*	Salter, J.A.M. and Charley, P.	1967	L	1.9-4.1	12(550)	94.72 5.28	Calculated composition; polycrystalline; rod specimen 3 mm in diameter; annealed in vacuo at 550 C for 14 hr; grain size 0.0025 cm; residual electrical resistivity $7.41 \mu\Omega \text{ cm}$ .
26	Salter, J.A.M. and Charley, P.	1967	L	1.7-4.0	12(450)	94.72 5.26	Calculated composition; polycrystalline; rod specimen 3 mm in diameter; annealed in vacuo at 450 C for 14 hr; residual electrical resistivity $7.57 \mu\Omega \text{ cm}$ ; grain size 0.0009 cm.
27	Charley, P., Loefer, A.D.W. and Salter, J.A.M.	1968	L	1.7-4.1		94.87 5.13	Single crystal; $0.2 \times 10 \times 2.5 \text{ cm}$ ; prepared by International Research and Development Co.; grown in graphite mould using Bridgman technique; measured in jig in the relaxed condition.
28	Charley, P., et al.	1968	L	1.8-4.1		94.87 5.13	The above specimen; measured in jig under a stress of $7 \text{ kg mm}^{-2}$ .
29	Charley, P., et al.	1968	L	1.7-4.2		94.87 5.13	Polycrystalline; prepared by International Research and Development Co.; measured in jig in the relaxed condition.
30*	Charley, P., et al.	1968	L	1.7-4.1		94.87 5.13	The above specimen; annealed at 750 C for 15 hr and measured in jig under a stress of $7 \text{ kg mm}^{-2}$ .
31	Charley, P., et al.	1968	L	1.9-4.1	$A_1A_2$ ; cross 1	94.87 5.13	Single crystal; grown in graphite mould using Bridgman technique; prepared by International Research and Development Co.; cross shape specimen obtained by cutting perpendicular to the large face of the crystal ( $0.2 \times 10 \times 2.5 \text{ cm}$ ); the orientation of the cross was chosen such that the primary edge dislocations made equal angles with both arms $A_1A_2$ and $B_1B_2$ ; the angle between the screw dislocations and these two directions however differed; heat flow in the arm $A_1A_2$ direction (angle to edges $55^\circ$ , and angle to screws $35^\circ$ ).

\* Not shown in figure.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER + ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
32* 117	Charley, P., Leaver, A.D.W. and Salter, J.A.M.	1968	L	2.0-4.2	A <sub>1</sub> A <sub>2</sub> ; cross 1	94.87 5.13	The above specimen measured in different cryostats.
33 117	Charley, P., et al.	1968	L	1.7-4.1	B <sub>1</sub> B <sub>2</sub> ; cross 1		The above specimen; heat flow in the arm B <sub>1</sub> B <sub>2</sub> direction (angle to edges 63°, and angle to screws 75°).
34* 117	Charley, P., et al.	1968	L	1.7-4.2	A <sub>1</sub> A <sub>2</sub> ; cross 2	94.87 5.13	Similar to the above specimen except the orientation of the cross was chosen such that the primary edge dislocations made different angles with both arms A <sub>1</sub> A <sub>2</sub> and B <sub>1</sub> B <sub>2</sub> , the angle between the screw dislocations and these two directions however equal; heat flow in the arm A <sub>1</sub> A <sub>2</sub> direction (angle to edges 80°, and angle to screws 53°).
35* 117	Charley, P., et al.	1968	L	1.8-3.4	B <sub>1</sub> B <sub>2</sub> ; cross 2		The above specimen; heat flow in the arm B <sub>1</sub> B <sub>2</sub> direction (angle to edges 46°, and angle to screws 52°).
36 19	Lindenthal, P. and Poundstone, W.B.	1962	L	1.4-4.2		0.617	Calculated composition: 3 x 0.125 x 0.001 in.; prepared from 99.999 pure Cu and 99.99% pure Al; materials melted, outgassed in vacuum, stirred for 0.5 hr, then cast; annealed at 700 C for 22 hr; residual electrical resistivity 2.10 μΩ cm.
37 56	Isawa, E.	1967	C	309-1171		94 6	Iron and aluminum used as comparative materials; data taken from smoothed curve.
38 56	Isawa, E.	1967	C	348-1125		92 8	Similar to the above specimen.
39 118	Charley, P. and Salter, J.A.M.	1965	L	1.8-4.0	4	1.84	Calculated composition; polycrystalline; 3 mm diameter and 12 cm long; prepared by International Research and Development Co., Ltd.; materials melted in pure argon, cast, machined, swaged, and drawn; annealed in vacuum at 750 C for 14 hr; residual electrical resistivity 3.88 μΩ cm.
40 118	Charley, P. and Salter, J.A.M.	1965	L	2.3-4.2	6	2.88	Similar to the above specimen except residual electrical resistivity 5.20 μΩ cm.
41 118	Charley, P. and Salter, J.A.M.	1965	L	2.0-4.4	10	4.22	Similar to the above specimen except residual electrical resistivity 6.62 μΩ cm.
42 118	Charley, P. and Salter, J.A.M.	1965	L	1.8-3.1	125	5.11	Calculated composition; single crystal; 3 mm diameter and 12 cm long; grown by the Bridgman technique; grain size 0.1 ~ 0.3 mm; residual electrical resistivity 7.49 μΩ cm.
43 118	Charley, P. and Salter, J.A.M.	1965	L	2.2-4.2	125		The above specimen; 2nd run.
44 118	Charley, P. and Salter, J.A.M.	1965	L	2.5-4.0	125		Similar to the above specimen.
45 53	Kanemaki, M. and Suzuki, E.	1969	L	1.7-4.3	Specimen No. 5	93.03 6.97	Calculated composition; single crystal; cross-sectional area 2.946 mm <sup>2</sup> ; prepared from 99.999 pure Cu (Mitsubishi-Kasei Co. Ltd.) and 99.99 pure Al (Sumitomo-Kasei Co. Ltd.) by melting in a high purity graphite crucible by induction heating; grown in a spinning graphite mould by the Bridgman method using a seed crystal; annealed at 1000 C for 48 hr in a vacuum better than 10 <sup>-5</sup> mm Hg; electrolytically polished in phosphoric acid-ethyl alcohol; dislocation density 8.8 x 10 <sup>6</sup> cm <sup>-2</sup> ; residual electrical resistivity 7.617 μΩ cm.

\* Not shown in figure.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER - ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Al	
46 53	Kusunoki, M. and Suzuki, H.	1969	L	1.7-4.3	Specimen No. 9	93.03	6.97	Similar to the above specimen except specimen cross-sectional area 2.924 mm <sup>2</sup> , dislocation density $1.0 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.108 $\mu\Omega \text{ cm}$ .
47 53	Kusunoki, M. and Suzuki, H.	1969	L	1.9-4.3	Specimen No. 11			Similar to the above specimen except specimen cross-sectional area 1.535 mm <sup>2</sup> , dislocation density $6.6 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.568 $\mu\Omega \text{ cm}$ .
48* 53	Kusunoki, M. and Suzuki, H.	1969	L	1.7-4.3	Specimen No. 12(1)			Similar to the above specimen except specimen cross-sectional area 1.915 mm <sup>2</sup> , dislocation density $2.0 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.562 $\mu\Omega \text{ cm}$ .
49 53	Kusunoki, M. and Suzuki, H.	1969	L	1.7-4.3	Specimen No. 13(1)			Similar to the above specimen except specimen cross-sectional area 2.318 mm <sup>2</sup> , dislocation density $3.6 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.571 $\mu\Omega \text{ cm}$ .
50 53	Kusunoki, M. and Suzuki, H.	1969	L	1.6-4.3	Specimen No. 13(2)			Similar to the above specimen except specimen cross-sectional area 2.055 mm <sup>2</sup> , dislocation density $4.4 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.605 $\mu\Omega \text{ cm}$ .
51 53	Kusunoki, M. and Suzuki, H.	1969	L	1.9-4.3	Specimen No. 14			Similar to the above specimen except specimen cross-sectional area 1.569 mm <sup>2</sup> , dislocation density $8.4 \times 10^6 \text{ cm}^{-2}$ , and residual electrical resistivity 7.641 $\mu\Omega \text{ cm}$ .
52 53	Kusunoki, M. and Suzuki, H.	1969	L	1.7-4.4	Specimen No. 12(2)			Same fabrication method and heat-treatment as the above specimen except no other details reported.
53 116, 166	Aliev, M.A.	1963	L	295.2	6	50.45		1.25 cm <sup>2</sup> in cross-section and 0.50 cm thick; electrical conductivity $10.68 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.345 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
54 116, 166	Aliev, M.A.	1963	L	295.2	7	53.00		1.28 cm <sup>2</sup> in cross-section and 0.96 cm thick; electrical conductivity $10.74 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.334 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
55* 116, 166	Aliev, M.A.	1963	L	295.2	8	55.00		1.25 cm <sup>2</sup> in cross-section and 0.52 cm thick; electrical conductivity $10.82 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.348 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
56 116, 166	Aliev, M.A.	1963	L	295.2	9	59.62		1.25 cm <sup>2</sup> in cross-section and 0.52 cm thick; electrical conductivity $9.98 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.994 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
57 116, 166	Aliev, M.A.	1963	L	295.2	10	69.99		1.25 cm <sup>2</sup> in cross-section and 1.18 cm thick; electrical conductivity $8.86 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.253 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
58 116, 166	Aliev, M.A.	1963	L	295.2	11	71.00		1.25 cm <sup>2</sup> in cross-section and 0.96 cm thick; electrical conductivity $7.75 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.436 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
59 116, 166	Aliev, M.A.	1963	L	295.2	12	73.00		1.25 cm <sup>2</sup> in cross-section and 1.49 cm thick; electrical conductivity $6.71 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.247 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
60 116, 166	Aliev, M.A.	1963	L	295.2	13	76.00		1.25 cm <sup>2</sup> in cross-section and 0.80 cm thick; electrical conductivity $6.02 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.438 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
61 116, 166	Aliev, M.A.	1963	L	295.2	14	77.00		1.25 cm <sup>2</sup> in cross-section and 0.74 cm thick; electrical conductivity $4.25 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.438 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .
62 116, 166	Aliev, M.A.	1963	L	295.2	15	75.00		1.25 cm <sup>2</sup> in cross-section and 0.80 cm thick; electrical conductivity $3.54 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ ; total Lorenz function $2.392 \times 10^{-1} \text{ V}\cdot\text{K}^{-2}$ .

\* See above in figure.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER - ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Al	
63 116, 163	Aliev, N.A.	1953	L	295.2	16	79.53		1.25 cm <sup>2</sup> in cross-section and 0.95 cm thick; electrical conductivity $4.16 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ ; total Lorenz function $2.360 \times 10^{-8} \text{V}\mu\text{K}^{-2}$ .
64 116, 163	Aliev, N.A.	1953	L	295.2	17	83.00		1.25 cm <sup>2</sup> in cross-section and 1.16 cm thick; electrical conductivity $5.95 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ ; total Lorenz function $2.277 \times 10^{-8} \text{V}\mu\text{K}^{-2}$ .
65 116, 163	Aliev, N.A.	1953	L	295.2	18	93.00		1.25 cm <sup>2</sup> in cross-section and 1.35 cm thick; electrical conductivity $7.40 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ ; total Lorenz function $2.346 \times 10^{-8} \text{V}\mu\text{K}^{-2}$ .
66* 116, 163	Aliev, N.A.	1953	L	295.2	19	99.22		1.25 cm <sup>2</sup> in cross-section and 0.60 cm thick; electrical conductivity $10.04 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ ; total Lorenz function $2.304 \times 10^{-8} \text{V}\mu\text{K}^{-2}$ .
67 116, 163	Aliev, N.A.	1953	L	295.2	20	95.00		1.25 cm <sup>2</sup> in cross-section and 0.51 cm thick; electrical conductivity $10.50 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ ; total Lorenz function $2.258 \times 10^{-8} \text{V}\mu\text{K}^{-2}$ . Polycrystalline specimen; annealed.
69* 169	Charney, P. and Salter, J.A.M.	1965	L	1.6-4.1			5.47	Polycrystalline specimen; plastically deformed (6%).
69 169	Charney, P. and Salter, J.A.M.	1965	L	1.6-4.5			5.47	Polycrystalline specimen; plastically deformed (6%).
70* 169	Charney, P. and Salter, J.A.M.	1965	L	2.4-4.2			5.47	Polycrystalline specimen; plastically deformed (12%).
71 52	Charney, P., Salter, J.A.M. and Leaver, A.D.W.	1968	L	1.6-4.2	2		0.90	Polycrystalline; 3 mm in diameter and 10 cm long; prepared by International Research and Development Co., Ltd.; annealed at 750 C for 15 hr in graphite tubes in vacuo and furnace cooled.
72 52	Charney, P., et al.	1968	L	1.6-4.0	2 (2.9%)		0.90	Similar to the above specimen except 2.9% deformed.
73 52	Charney, P., et al.	1968	L	1.6-4.2	2 (10%)		0.83	Similar to the above specimen except 10% deformed.
74* 52	Charney, P., et al.	1968	L	1.7-4.2	6 (6%)		4.09	Similar to the above specimen except 6% deformed.
75* 52	Charney, P., et al.	1968	L	1.6-4.4	12 (6.2%)		5.11	Similar to the above specimen except 6.2% deformed.
76* 52	Charney, P., et al.	1968	L	2.4-4.2	12 (12.5%)		5.28	Similar to the above specimen except 12.5% deformed.
77* 49	Smith, C.S. and Palmer, E.W.	1935	L	293.473	Bar 50	59.38	9.90	0.22 Fe; 0.75 in. diameter and 8 in. long; rolled to 1.25 in. in diameter. annealed at 700-750 C, cold-drawn to size; heat-treated at 750 C for 3.5 hr, slowly air-cooled; electrical conductivity $7.923$ and $6.724 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
78 49	Smith, C.S. and Palmer, E.W.	1935	L	293.473	Bar 49	89.38	9.41	0.52 Fe, 0.38 Sn, 0.31 Ni, and trace Zn; 0.75 in. diameter and 5 in. long; same fabrication method as the above specimen; heat-treated at 750 C for 3.5 hr, very slowly cooled; electrical conductivity $7.314$ and $6.304 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
79 119, 169	Friedman, A.J., Chu, T.K., Elomets, P.G., and Reynolds, C.A.	1972	L	1.7-4.0	A		4.07	Polycrystalline; form factor 37.50 cm <sup>-1</sup> ; prepared from 99.999 pure copper supplied by Johnsons and Matthey and from 99.99 pure aluminum supplied by Jarrell Ash Co. by melting in an evacuated quartz boat, casting into a quartz capillary and quenching in an ice bath; annealed in vacuo at 1273 K for 16 hr; average grain size 1 mm; residual electrical resistivity $7.51 \mu\Omega \text{cm}$ .

\* Not shown in figure.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER + ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
80 119, 100	Friedman, A.J., Chu, T.K., Klemens, P.G., and Reynolds, C.A.	1972	L	1.5-3.9	A		The above specimen irradiated for 6 hr at 25 to 60 C at the Brookhaven National Laboratory BMRR facility for a total fast neutron (>1 MeV) dosage of $4 \times 10^{17}$ n cm <sup>-2</sup> and a total thermal dosage of $1 \times 10^{14}$ a cm <sup>-2</sup> ; form factor 37.57 cm <sup>-1</sup> ; residual electrical resistivity 7.46 $\mu\Omega$ cm.
81 119, 100, 170	Friedman, A.J., et al.	1972	L	1.7-3.6	B	4.07	Some fabrication method as the above specimen A; form factor 35.97 cm <sup>-1</sup> ; residual electrical resistivity 7.60 $\mu\Omega$ cm.
82 119, 100, 170	Friedman, A.J., et al.	1972	L	1.3-3.7	B		The above specimen deformed in tension, 6.1%, at room temperature; form factor 47.4 cm <sup>-1</sup> ; residual electrical resistivity 7.89 $\mu\Omega$ cm.
83 119, 100	Friedman, A.J., et al.	1972	L	1.3-3.6	B		The above specimen annealed in vacuum at 873 K for 24 hr; form factor 47.0 cm <sup>-1</sup> ; residual electrical resistivity 7.90 $\mu\Omega$ cm.
84 119, 100	Friedman, A.J., et al.	1972	L	1.4-3.9	B		The above specimen irradiation treated same as the above specimen A for curve No. 78; form factor 46.9 cm <sup>-1</sup> ; residual electrical resistivity 7.83 $\mu\Omega$ cm.
86 119, 100	Friedman, A.J., et al.	1972	L	1.6-3.8	B		The above specimen annealed in vacuum at 873 K for 24 hr; form factor 46.6 cm <sup>-1</sup> ; residual electrical resistivity 7.95 $\mu\Omega$ cm.
88 84	Mitchell, M.A., Klemens, P.G., and Reynolds, C.A.	1971	L	1.3-4.1	A	4.5	Obtained from Materials Research Corp., Orangeburg, N.Y.; prepared from 99.999 pure Al and Cu by vacuum induction melting, then machining and swaging to 0.125 in. in diameter; cold-worked in liquid nitrogen, then kept at 293 K for 3 hr; residual electrical resistivity 7.995 $\mu\Omega$ cm.
87 84	Mitchell, M.A., et al.	1971	L	1.4-4.1	B		Similar to the above specimen A but annealed at 1193 K for 48 hr after cold-work; residual electrical resistivity 7.461 $\mu\Omega$ cm.
88 84	Mitchell, M.A., et al.	1971	L	1.3-4.2	C1		Similar to the above specimen A but annealed at 1123 K for 28 hr after cold-work, then given 9.5% torsional strain at 293 K, re-annealed at 300 K for 12 hr; residual electrical resistivity 7.468 $\mu\Omega$ cm.
89 84	Mitchell, M.A., et al.	1971	L	1.4-4.1	C2		The above specimen re-annealed at 373 K for 48 hr; residual electrical resistivity 7.450 $\mu\Omega$ cm.
90 84	Mitchell, M.A., et al.	1971	L	1.4-4.0	C3		The above specimen re-annealed at 693 K for 20 hr; residual electrical resistivity 7.463 $\mu\Omega$ cm.
91 84	Mitchell, M.A., et al.	1971	L	1.3-4.1	C4		The above specimen re-annealed at 713 K for 48 hr; residual electrical resistivity 7.404 $\mu\Omega$ cm.
92 84	Mitchell, M.A., et al.	1971	L	1.2-4.1	D		Same composition, supplier, and fabrication method as the above specimen A but swaged to 3/16 in. in diameter; annealed at 1205 K for 48 hr; residual electrical resistivity 7.350 $\mu\Omega$ cm.
93 84	Mitchell, M.A., et al.	1971	L	1.5-4.1	E1		Similar to the above specimen D but given, after annealing, 9.35% tensile strain at 77 K with maximum stress 28.5 kg mm <sup>-2</sup> and strain rate 0.0093 s <sup>-1</sup> ; then re-annealed at 300 K for 12 hr; residual electrical resistivity 7.506 $\mu\Omega$ cm.
94 84	Mitchell, M.A., et al.	1971	L	1.3-4.1	E2		The above specimen re-annealed at 422 K for 48 hr; residual electrical resistivity 7.475 $\mu\Omega$ cm.
95 84	Mitchell, M.A., et al.	1971	L	1.4-4.1	E3		The above specimen re-annealed at 532 K for 48 hr; residual electrical resistivity 7.498 $\mu\Omega$ cm.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER-ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
96 54	Mitchell, M.A., Klumpp, P.G., and Reynolds, C.A.	1971	L	1.2-4.1	E4	4.5	The above specimen re-annealed at 973 K for 48 hr; residual electrical resistivity 7.542 $\mu\Omega$ cm.
97 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	E5		The above specimen re-annealed at 797 K for 48 hr; residual electrical resistivity 7.456 $\mu\Omega$ cm.
98 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	E6		The above specimen re-annealed at 920 K for 48 hr; residual electrical resistivity 7.483 $\mu\Omega$ cm.
99 54	Mitchell, M.A., et al.	1971	L	1.4-4.1	E7		The above specimen re-annealed at 1202 K for 48 hr; residual electrical resistivity 7.441 $\mu\Omega$ cm.
100 54	Mitchell, M.A., et al.	1971	L	1.3-4.2	F1		Similar to the above specimen F1 but annealed at 1202 K for 48 hr, then given 8.13% tensile strain at 77 K with maximum stress 29 kg mm <sup>-2</sup> and strain rate 0.0081 s <sup>-1</sup> , re-annealed at 360 K for 48 hr; residual electrical resistivity 7.507 $\mu\Omega$ cm.
101 54	Mitchell, M.A., et al.	1971	L	1.4-4.2	F2		The above specimen re-annealed at 564 K for 0.5 hr; residual electrical resistivity 7.536 $\mu\Omega$ cm.
102 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	F3		The above specimen re-annealed at 565 K for 1.5 hr; residual electrical resistivity 7.536 $\mu\Omega$ cm.
103 54	Mitchell, M.A., et al.	1971	L	1.5-4.2	F4		The above specimen re-annealed at 567 K for 48 hr; residual electrical resistivity 7.498 $\mu\Omega$ cm.
104 54	Mitchell, M.A., et al.	1971	L	1.5-4.2	F5		The above specimen re-annealed at 570 K for 97 hr; residual electrical resistivity 7.498 $\mu\Omega$ cm.
105 54	Mitchell, M.A., et al.	1971	L	1.3-4.2	G1		Similar to the above specimen F1 but given, after annealing, 9.26% tensile strain at 77 K with maximum stress 25.1 kg mm <sup>-2</sup> and strain rate 0.004 s <sup>-1</sup> , re-annealed at 344 K for 48 hr; residual electrical resistivity 7.644 $\mu\Omega$ cm.
106 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	G2		The above specimen re-annealed at 570 K for 0.5 hr; residual electrical resistivity 7.625 $\mu\Omega$ cm.
107 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	G3		The above specimen re-annealed at 561 K for 1.5 hr; residual electrical resistivity 7.612 $\mu\Omega$ cm.
108 54	Mitchell, M.A., et al.	1971	L	1.2-4.1	G4		The above specimen re-annealed at 560 K for 48 hr; residual electrical resistivity 7.601 $\mu\Omega$ cm.
109 54	Mitchell, M.A., et al.	1971	L	1.2-4.2	G5		The above specimen re-annealed at 732 K for 48 hr; residual electrical resistivity 7.563 $\mu\Omega$ cm.
110 54	Mitchell, M.A., et al.	1971	L	1.2-4.1	G6		The above specimen re-annealed at 1308 K for 48 hr; residual electrical resistivity 7.876 $\mu\Omega$ cm.
111 48, 171	Chu, T.K. and Lipschultz, F.P.	1972	L	4.6-69	C1	0.43	Supplied by American Amacorda Brass Co.; 0.5 in. diameter $\pm$ 8 in. long with central 5 in. machined to 0.25 in. in diameter; annealed at 1273 K for 48 hr; electrical resistivity 1.066, 1.066, 1.308, and 2.879 $\mu\Omega$ cm at 1.1, 4.2, 77, and 273 K, respectively.
112 48, 171	Chu, T.K. and Lipschultz, F.P.	1972	L	4.5-55	C2		The above specimen fatigued for 500 cycles with maximum load 6.4 kg mm <sup>-2</sup> ; electrical resistivity 1.071, 1.067, 1.301, and 2.664 $\mu\Omega$ cm at 1.1, 4.2, 77, and 273 K, respectively.

TABLE 4. THERMAL CONDUCTIVITY OF COPPER-ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
113 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	1.7-72	C3	0.43	The above specimen fatigued for $10^4$ cycles with maximum load $6.4 \text{ kg mm}^{-2}$ ; electrical resistivity 1.069, 1.069, 1.304, and $2.663 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
114 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.6-69	C5		Similar to the above specimen C1 but given a 5% plastic deform under uniaxial stress; electrical resistivity 1.066, 1.066, 1.294, and $2.660 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
115 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.6-66	C6		The above specimen fatigued for $10^4$ cycles with maximum load $6.4 \text{ kg mm}^{-2}$ ; electrical resistivity 1.064, 1.306, and $2.665 \mu\Omega \text{ cm}$ at 4.2, 77, and 273 K, respectively.
116 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.6-66	B1	6.97	Same supplier and dimensions as the above specimen C1; annealed at 1237 K for 48 hr; electrical resistivity 7.866, 7.867, 8.253, and $10.19 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
117 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.9-68	B2		The above specimen fatigued for 500 cycles with maximum load $8.3 \text{ kg mm}^{-2}$ ; electrical resistivity 7.850, 7.853, 8.260, and $10.16 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
118 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.7-68	B3		The above specimen fatigued for $10^4$ cycles; electrical resistivity 7.806, 7.806, 8.204, and $10.19 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
119 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	5.4-68	B4		The above specimen fatigued for $10^4$ cycles; electrical resistivity 7.813, 7.813, 8.217, and $10.14 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
120 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.7-68	B5	6.97	Similar to the above specimen B1 but given a 5% plastic deform under uniaxial stress; electrical resistivity 7.859, 7.859, 8.288, and $10.16 \mu\Omega \text{ cm}$ at 1.1, 4.2, 77, and 273 K, respectively.
121 46, 171	Chu, T.K. and Lapachwitz, F.P.	1972	L	4.8-65	B6		The above specimen fatigued for $2 \times 10^4$ cycles with maximum load $8.3 \text{ kg mm}^{-2}$ ; electrical resistivity 7.891, 8.272, and $10.21 \mu\Omega \text{ cm}$ at 4.2, 77, and 273 K, respectively.
122 50	Friedman, A.J.	1974	L	5.3-73	6	4.07	The same irradiated specimen B for curve No. 52; electrical resistivity 7.832, 7.832, 8.204, and $10.033 \mu\Omega \text{ cm}$ at 1.2, 4.2, 77, and 273 K, respectively.
123 50	Friedman, A.J.	1974	L	5.3-70	5		The above specimen re-annealed at 573 K for 24 hr; electrical resistivity 7.949, 7.949, 8.314, and $10.150 \mu\Omega \text{ cm}$ at 1.2, 4.2, 77, and 273 K, respectively.
124 50	Friedman, A.J.	1974	L	5.3-68	6	4.07	Form factor $37.497 \text{ cm}^{-1}$ ; annealed in vacuum at 1273 K for 18 hr; electrical resistivity 7.513, 7.513, 7.867, and $9.630 \mu\Omega \text{ cm}$ at 1.2, 4.2, 77, and 273 K, respectively.
125 50	Friedman, A.J.	1974	L	5.0-72	6		The above specimen.
126 50	Friedman, A.J.	1974	L	5.0-67	6		The above specimen given the same irradiation treatment as the specimen B for curve No. 52; form factor $37.569 \text{ cm}^{-1}$ ; electrical resistivity 7.461, 7.461, 7.812, and $9.564 \mu\Omega \text{ cm}$ at 1.2, 4.2, 77, and 273 K, respectively.
127 120	Leaver, A.D.W. and Charsley, F.	1971	L	1.9-4.0	2 Al	0.83	Similar to the specimen for curve No. 73; annealed; residual electrical resistivity $2.080 \mu\Omega \text{ cm}$ .
128 120	Leaver, A.D.W. and Charsley, F.	1971	L	1.9-4.1	2 Al		The above specimen tensile strained 8.2% under a stress of $16.90 \text{ kg mm}^{-2}$ ; residual electrical resistivity $2.109 \mu\Omega \text{ cm}$ .
129 120	Leaver, A.D.W. and Charsley, F.	1971	L	2.0-4.0	12 Al	5.56	Polycrystalline; obtained from International Research and Development Co., Ltd.; residual electrical resistivity $7.61 \mu\Omega \text{ cm}$ .

TABLE 4. THERMAL CONDUCTIVITY OF COPPER + ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Al	Composition (continued), Specifications, and Remarks
130	Leaver, A.D.W. and Charalcy, P.	1971	L	1.8-4.0	12 Al		The above specimen tensile strained 1.8% under a stress of 16.35 kg mm <sup>-2</sup> ; residual electrical resistivity 7.62 $\mu\Omega$ cm.
131	Leaver, A.D.W. and Charalcy, P.	1971	L	2.0-4.2	12 Al	5.56	Single crystal; grown in a graphite mold by the Bridgman technique; annealed.
132	Leaver, A.D.W. and Charalcy, P.	1971	L	2.2-4.1	12 Al		The above specimen tensile strained 7.3% under a stress of 3.03 kg mm <sup>-2</sup> .
133	Leaver, A.D.W. and Charalcy, P.	1971	L	1.9-4.0	12 Al		The above specimen tensile strained 17.0% under a stress of 4.48 kg mm <sup>-2</sup> .
134	Leaver, A.D.W. and Charalcy, P.	1971	L	2.0-4.1	12 Al		The above specimen tensile strained 22.5% under a stress of 6.73 kg mm <sup>-2</sup> .
135	Kogure, Y. and Hiki, Y.	1973	L	1.6-6.6		97.8 2.2	Calculated composition (5 a/o Al); 2.5 mm dia x 70 mm long; prepared from 99.99% Cu and Al by vacuum melting and casting; annealed in vacuum at 850 C for 15 hrs.
136*	Kapoor, A.; Rowlands, J.A., and Woods, S.B.	1974	L	0.48-3.9		95.5 4.5	Calculated composition (10 a/o Al); cylindrical specimen 3.6 mm in diameter; prepared by melting the pure materials in a quartz container in vacuum, resulted ingot swaged to size; cold-worked; residual electrical resistivity 7.54 $\mu\Omega$ cm.
137*	Kapoor, A., et al.	1974	L	0.52-4.0			The above specimen annealed in vacuum at 600 K for 12 hr; residual electrical resistivity 6.79 $\mu\Omega$ cm.
138*	Kapoor, A., et al.	1974	L	0.48-3.7			The above specimen reannealed in vacuum at 675 K for 12 hr; residual electrical resistivity 6.88 $\mu\Omega$ cm.
139*	Kapoor, A., et al.	1974	L	0.65-4.0			The above specimen reannealed in vacuum at 1000 K for 12 hr; residual electrical resistivity 6.69 $\mu\Omega$ cm.

\* Not shown in figure.



#### 4.2. Aluminum-Magnesium Alloy System

The aluminum-magnesium alloy system does not form a continuous series of solid solutions. The maximum solid solubility of magnesium in aluminum is 17.4% (18.9 At.%) at 723 K and the solubility decreases at higher and lower temperatures, being only 1.9% (2.1 At.%) at 373 K. The maximum solid solubility of aluminum in magnesium is 12.7% (11.6 At.%) at 710 K and likewise it decreases at higher and lower temperatures, being only about 1.5% (1.3 At.%) at 373 K. Thus the region of solid solution for this system is even more limited than that of the aluminum-copper alloy system.

There are 40 sets of experimental thermal conductivity data available for this system. Of the 22 data sets for Al + Mg alloys listed in Table 6 and shown in Figure 11, seven sets are merely single data points. Of the 18 data sets for Mg + Al alloys listed in Table 7 and shown in Figure 12, 10 sets are single data points.

For the Al + Mg alloys, measurements were limited to specimens containing no more than 15% Mg. The recommended curves are, therefore, given for 0.5 to 10% Mg alloys only. They follow the general trend of the data of Johnson [56] (Al + Mg curves 5 and 6) and Powell, et al. [57] (Al + Mg curves 18-22) at low temperatures and the data of Mikryukov and Karagezyan [58] (Al + Mg curves 8-11) at high temperatures. At 300 K the  $k_e$  values were calculated from eq. (12), and the  $k_g$  values at 300 K were derived as the differences between  $k$  and  $k_e$  values. These  $k_g$  values were extrapolated to higher temperatures up to the solidus points according to the temperature dependence of eq. (35) and to lower temperatures according to the pattern of  $k_g$  curves derived from the available experimental  $k$  and the calculated  $k_e$  around the region of maximum  $k_g$  and according to  $T^2$  dependence at lower temperatures assuming  $k_g$  to be negligible at 1 K. The total thermal conductivity values were then obtained by adding the extrapolated  $k_g$  and the calculated  $k_e$ . The resulting recommended values agree with the data of Powell et al. [57] (Al + Mg curves 18-20) at low temperatures to within 10% and with the data of Meyer-Rassler [122] (Al + Mg curve 7) and of Mikryukov and Karagezyan [58] (Al + Mg curves 8-11) at higher temperatures to within 8%. The  $k_g$  values are very uncertain and are merely to serve as correction terms for the derivation of the total thermal conductivities.

For the Mg + Al alloys, no measurements were made below 85 K and none for alloys containing more than 14% Al. The data of Smith [45] (Mg + Al curves 1 and 2) and Kikuchi [59] (Mg + Al curves 8-13) were favored in constructing the conductivity-composition curve for 300 K. The  $k_e$  values were calculated from eq. (12) and those at 300 K were plotted on the conductivity-composition graph. The  $k_g$  values at 300 K were taken as the differences between  $k$  and  $k_e$  values. These  $k_g$  values were similarly extrapolated to low and high temperatures according to the appropriate temperature dependences, which are very uncertain. The total thermal conductivity values were obtained by adding these  $k_g$  to the calculated  $k_e$ . Since

there is no information as to where the maxima of the  $k_g$  curves occur, no  $k_g$  values are given below 100 K and hence no total  $k$  values are reported at low temperatures for the dilute alloys, even though the  $k_e$  values are known. The  $k$  values of the 5 and 10% Al alloys are restricted to the range between 250 and 350 K, since electrical resistivity values are available only in this range. The recommended values are in agreement with the data of Kikuchi [59] (Mg + Al curves 8-13), Smith [45] (Mg + Al curves 1 and 2), and Giuliani [125] (Mg + Al curve 14) to within 6%.

The resulting recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 5 for 10 alloy compositions. These values are for well-annealed alloys. The  $k$  values are also shown in Figures 9 and 10. The values of residual electrical resistivity for eight of the 10 alloys are also given in Table 5. The uncertainties of the  $k$  values are stated in a footnote to Table 5, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 5. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-MAGNESIUM ALLOY SYSTEM†

[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Al: 99.50% (99.45 At. %) Mg: 0.50% (0.55 At. %)				Al: 99.00% (98.99 At. %) Mg: 1.00% (1.11 At. %)				Al: 97.00% (96.68 At. %) Mg: 3.00% (3.32 At. %)				Al: 95.00% (94.48 At. %) Mg: 5.00% (5.52 At. %)			
$\rho_0 = 0.210 \mu\Omega \text{ cm}$				$\rho_0 = 0.420 \mu\Omega \text{ cm}$				$\rho_0 = 1.260 \mu\Omega \text{ cm}$				$\rho_0 = 2.10 \mu\Omega \text{ cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4	0.476			4	0.240			4	0.0809			4	0.0486		
6	0.720			6	0.365			6	0.124			6	0.0738		
8	0.968			8	0.494			8	0.168			8	0.0988		
10	1.23			10	0.625			10	0.213			10	0.125		
15	1.81			15	0.942			15	0.328			15	0.191		
20	2.34			20	1.25			20	0.343			20	0.257		
25	2.76			25	1.52			25	0.552			25	0.322		
30	3.10			30	1.75			30	0.659			30	0.386		
40	3.50			40	2.09			40	0.835			40	0.504		
50	3.56			50	2.23			50	0.964			50	0.600		
60	3.31			60	2.21			60	1.05			60	0.675		
70	2.95			70	2.10			70	1.10			70	0.728		
80	2.64			80	1.98			80	1.12			80	0.768		
90	2.38			90	1.89			90	1.13			90	0.800		
100	2.23	2.09	0.141‡	100	1.85	1.74	0.113‡	100	1.15	1.07	0.0649‡	100	0.832	0.761	0.0710‡
150	2.08*	1.96	0.117‡	150	1.84*	1.74	0.0974‡	150	1.28*	1.21	0.0731‡	150	0.978	0.916	0.0615‡
200	2.06*	1.98	0.0978‡	200	1.89*	1.81	0.0832‡	200	1.40*	1.34	0.0631‡	200	1.10	1.05	0.0535‡
250	2.11*	2.03	0.0941‡	250	1.96*	1.89	0.0723‡	250	1.50*	1.44	0.0555‡	250	1.21	1.16	0.0474‡
273	2.14*	2.06	0.0791‡	273	2.00*	1.93	0.0684‡	273	1.54*	1.49	0.0528‡	273	1.25	1.21	0.0449‡
300	2.17	2.10	0.0739‡	300	2.03	1.97	0.0640‡	300	1.57	1.52	0.0498‡	300	1.29	1.25	0.0425‡
350	2.22	2.16	0.0658‡	350	2.10	2.04	0.0574‡	350	1.63	1.59	0.0451‡	350	1.36	1.32	0.0387‡
400	2.34	2.18	0.0590‡	400	2.13	2.08	0.0520‡	400	1.68	1.64	0.0413‡	400	1.41	1.38	0.0356‡
500	2.24	2.19	0.0491‡	500	2.14	2.10	0.0438‡	500	1.73	1.69	0.0356‡	500	1.47	1.44	0.0308‡
600	2.21	2.17	0.0419‡	600	2.13	2.10	0.0379‡	600	1.75	1.72	0.0315‡	600	1.50	1.48	0.0274‡
700	2.16	2.13	0.0366‡	700	2.09	2.06	0.0334‡	700	1.76	1.74	0.0283‡	700	1.53	1.51	0.0247‡
800	2.10*	2.07	0.0325‡	800	2.04*	2.02	0.0298‡	800	1.76*	1.74	0.0257‡	800	1.55*	1.54	0.0223‡
900	2.03*	2.00	0.0291‡	900	1.99*	1.97	0.0270‡	881	1.76*	1.74	0.0240‡	849	1.53	1.53	0.0216‡
922	2.02*	1.99	0.0266‡	913	1.98*	1.96	0.0267‡								

† Uncertainties of the total thermal conductivity, k, are as follows:

99.50 Al - 0.50 Mg:  $\pm 10\%$  below 200 K and  $\pm 6\%$  above 200 K.99.00 Al - 1.00 Mg:  $\pm 10\%$  below 200 K and  $\pm 8\%$  above 200 K.97.00 Al - 3.00 Mg:  $\pm 12\%$  below 100 K,  $\pm 7\%$  between 100 and 500 K, and  $\pm 8\%$  above 500 K.95.00 Al - 5.00 Mg:  $\pm 12\%$  below 100 K,  $\pm 7\%$  between 100 and 500 K, and  $\pm 8\%$  above 500 K.

‡ Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 3. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-MAGNESIUM ALLOY SYSTEM (continued)†  
 (Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>)

Al: 99.00% (99.02 At. %) Mg: 10.00% (10.98 At. %)				Al: 10.00% ( 8.10 At. %) Mg: 90.00% (90.90 At. %)				Al: 5.00% ( 4.53 At. %) Mg: 95.00% (95.47 At. %)				Al: 3.00% ( 2.71 At. %) Mg: 97.00% (97.29 At. %)			
$\rho_0 = 4.978 \mu\Omega \text{ cm}$												$\rho_0 = 4.78 \mu\Omega \text{ cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4	0.0000			4				4				4		0.0204	
6	0.0070			6				6				6		0.0307	
8	0.0095			8				8				8		0.0409	
10	0.0047			10				10				10		0.0508	
15	0.0097			15				15				15		0.0752	
20	0.126			20				20				20		0.0998	
25	0.109			25				25				25		0.124	
30	0.304			30				30				30		0.148	
40	0.308			40				40				40		0.192	
50	0.321			50				50				50		0.232	
60	0.379			60				60				60		0.266	
70	0.412			70				70				70		0.295	
80	0.449			80				80				80		0.318	
90	0.485			90				90				90		0.339	
100	0.519	0.402	0.05728	100		0.05648		100			0.07238	100	0.453*	0.302	0.6911‡
150	0.653	0.603	0.04904	150		0.04778		150			0.0613‡	150	0.553*	0.476	0.0771‡
200	0.763	0.719	0.04378	200		0.04098		200			0.05278	200	0.634*	0.568	0.04598
250	0.882	0.813	0.03868	250	0.444‡	0.408		250	0.576	0.530	0.04008	250	0.699*	0.642	0.0872‡
273	0.908	0.851	0.03708	273	0.461‡	0.427	0.0338‡	273	0.598	0.554	0.0435‡	273	0.728*	0.674	0.0640‡
300	0.936	0.881	0.03508	300	0.477‡	0.445	0.03178	300	0.619	0.578	0.04078	300	0.756	0.705	0.0805‡
350	0.969	0.907	0.03208	350	0.504‡	0.475	0.02858	350	0.653	0.616	0.03878	350	0.799*	0.754	0.0453‡
400	1.04	1.01	0.02908	400			0.02598	400			0.03548	400	0.835*	0.794	0.04098
500	1.15	1.16	0.02578	500			0.02308	500			0.02838	500	0.888*	0.854	0.0343‡
600	1.17	1.18	0.02398	600			0.01918	600			0.02478	600	0.924*	0.894	0.0295‡
700	1.20	1.18	0.02008	700			0.01708	700			0.02188	700	0.946*	0.920	0.0260‡
708	1.22	1.21	0.01938	756			0.01598	800			0.01968	800	0.964*	0.941	0.0232‡
								839			0.01898	872	0.975*	0.953	0.0210‡

† Uncertainties of the total thermal conductivity, k, are as follows:

99.00 Al - 10.00 Mg:  $\pm 15\%$  below 100 K,  $\pm 7\%$  between 100 and 500 K, and  $\pm 9\%$  above 500 K.

10.00 Al - 90.00 Mg:  $\pm 10\%$  between 250 and 300 K.

5.00 Al - 95.00 Mg:  $\pm 15\%$  between 250 and 300 K.

3.00 Al - 97.00 Mg:  $\pm 10\%$  below 200 K,  $\pm 6\%$  between 200 and 500 K, and  $\pm 9\%$  above 500 K.

‡ Provisional values.

§ Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 5. RECOMMENDED THERMAL CONDUCTIVITY OF ALUMINUM-MAGNESIUM ALLOY SYSTEM (continued) +  
 (Temperature, T, K; Thermal Conductivity,  $k$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ )

Al: 1.00% (0.90 AL. %) Mg: 99.00% (99.10 AL. %)				Al: 0.50% (0.45 AL. %) Mg: 99.50% (99.55 AL. %)			
$\rho_0 = 1.990 \mu\Omega \text{ cm}$				$\rho_0 = 0.980 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0500			4		0.0596	
6	0.0750			6		0.150	
8	0.100			8		0.200	
10	0.125			10		0.249	
15	0.186			15		0.369	
20	0.245			20		0.481	
25	0.301			25		0.586	
30	0.355			30		0.683	
40	0.451			40		0.836	
50	0.525			50		0.920	
60	0.573			60		0.950	
70	0.602			70		0.962	
80	0.619			80		0.971	
90	0.634			90		0.978	
100	0.793		0.133 <sup>‡</sup>	100	1.07*	0.982	0.152 <sup>‡</sup>
150	0.904	0.792	0.112 <sup>‡</sup>	150	1.18*	1.05	0.127 <sup>‡</sup>
200	0.969	0.896	0.0932 <sup>‡</sup>	200	1.23*	1.13	0.104 <sup>‡</sup>
250	1.03	0.972	0.0797 <sup>‡</sup>	250	1.27*	1.18	0.0874 <sup>‡</sup>
273	1.06	1.01	0.0746 <sup>‡</sup>	273	1.29*	1.21	0.0916 <sup>‡</sup>
300	1.10	1.03	0.0692 <sup>‡</sup>	300	1.30*	1.23	0.0756 <sup>‡</sup>
350	1.14	1.06	0.0613 <sup>‡</sup>	350	1.32*	1.25	0.0661 <sup>‡</sup>
400	1.17	1.12	0.0546 <sup>‡</sup>	400	1.33	1.27	0.0589 <sup>‡</sup>
500	1.19	1.15	0.0449 <sup>‡</sup>	500	1.34	1.29	0.0481 <sup>‡</sup>
600	1.21	1.17	0.0363 <sup>‡</sup>	600	1.34	1.30	0.0406 <sup>‡</sup>
700	1.22	1.19	0.0311 <sup>‡</sup>	700	1.33	1.30	0.0350 <sup>‡</sup>
800	1.22	1.19	0.0282 <sup>‡</sup>	800	1.33*	1.30	0.0308 <sup>‡</sup>
900	1.22	1.19	0.0263 <sup>‡</sup>	900	1.32*	1.30	0.0274 <sup>‡</sup>
906	1.22	1.19	0.0260 <sup>‡</sup>	914	1.32*	1.30	0.0270 <sup>‡</sup>

+ Uncertainties of the total thermal conductivity,  $k$ , are as follows:

1.00 Al - 99.00 Mg:  $\pm 12\%$  below 200 K,  $\pm 6\%$  between 200 and 500 K, and  $\pm 8\%$  above 500 K.  
 0.50 Al - 99.50 Mg:  $\pm 12\%$  below 200 K,  $\pm 6\%$  between 200 and 500 K, and  $\pm 8\%$  above 500 K.

<sup>‡</sup> Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

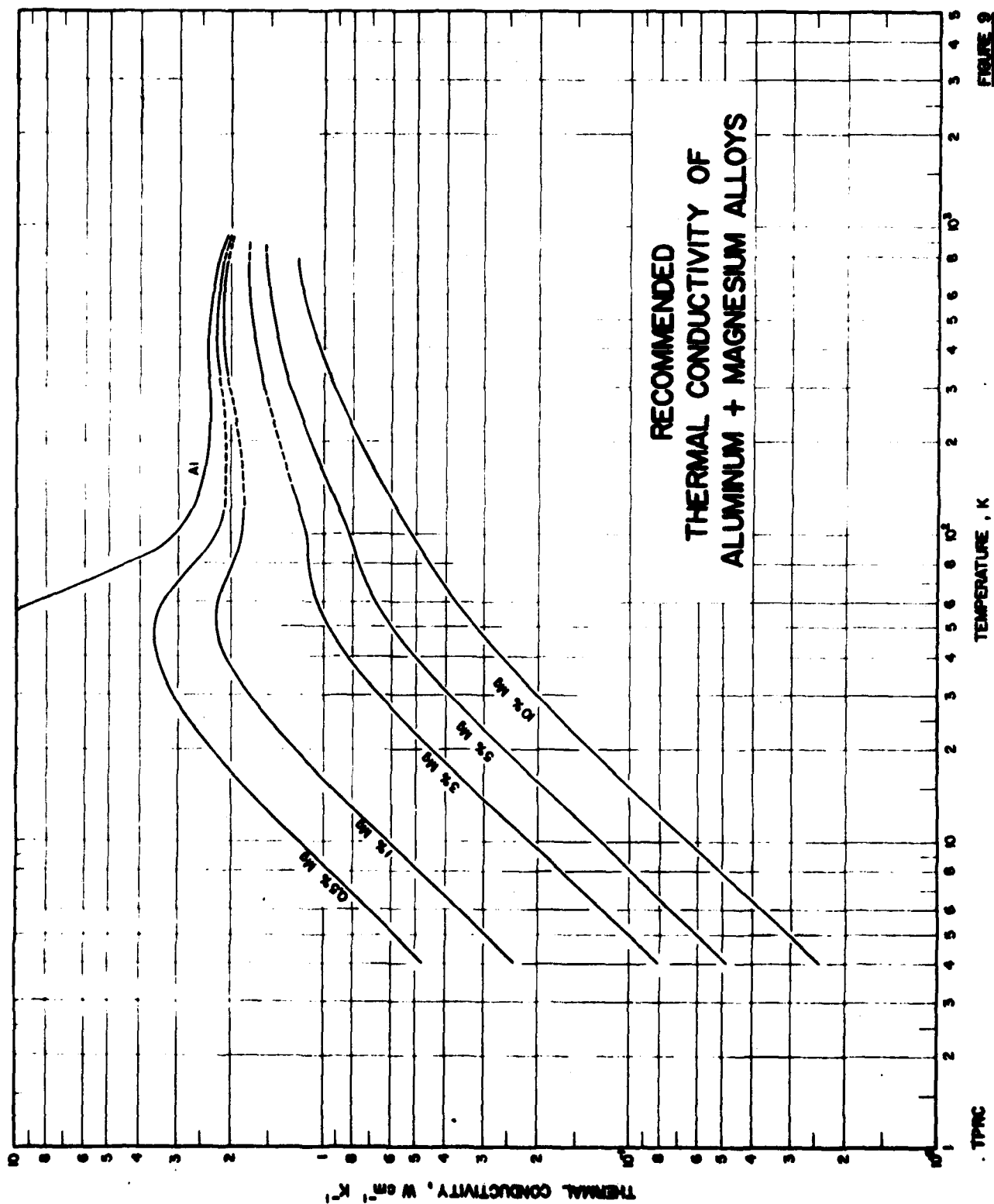


FIGURE 2

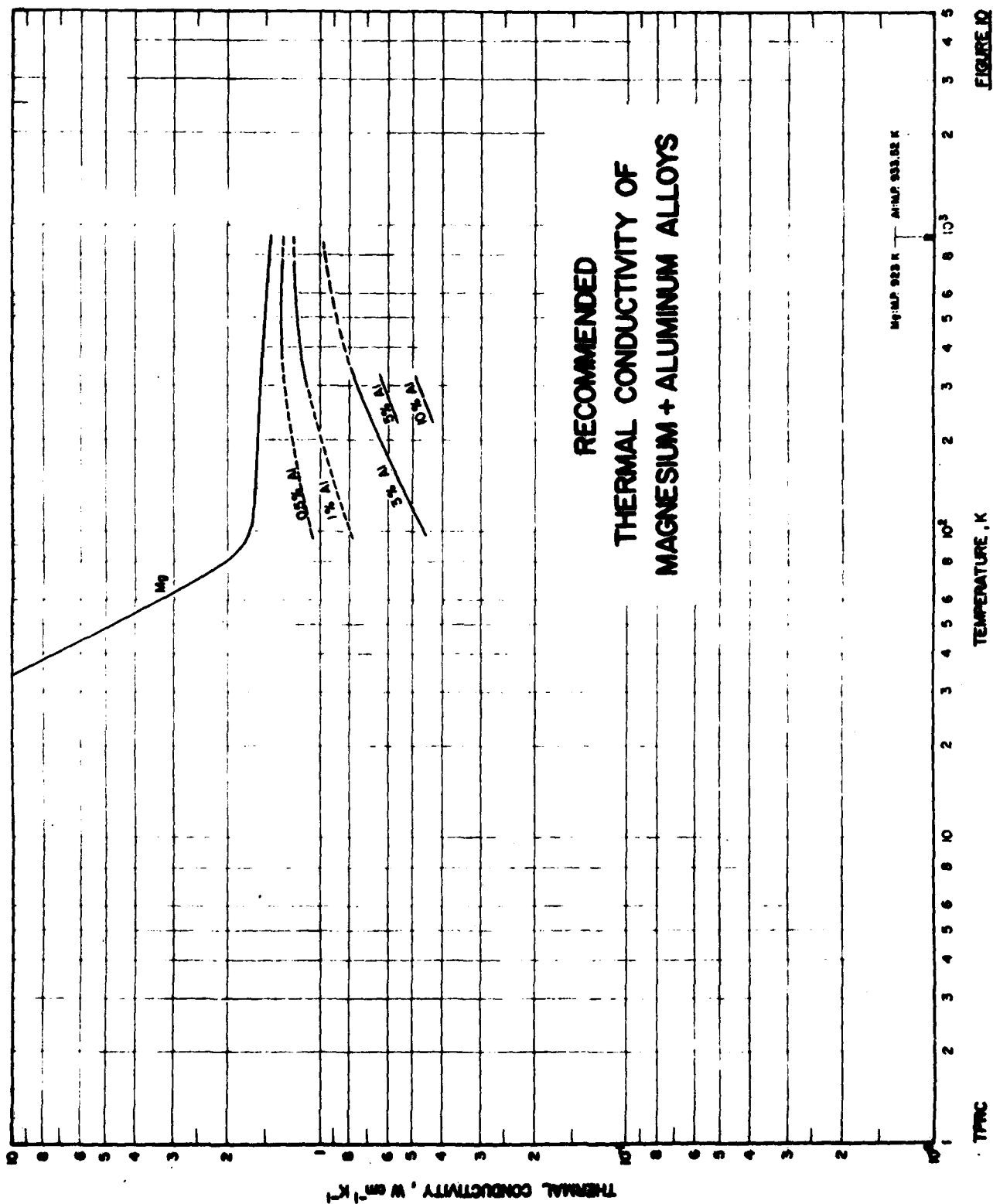


FIGURE 10

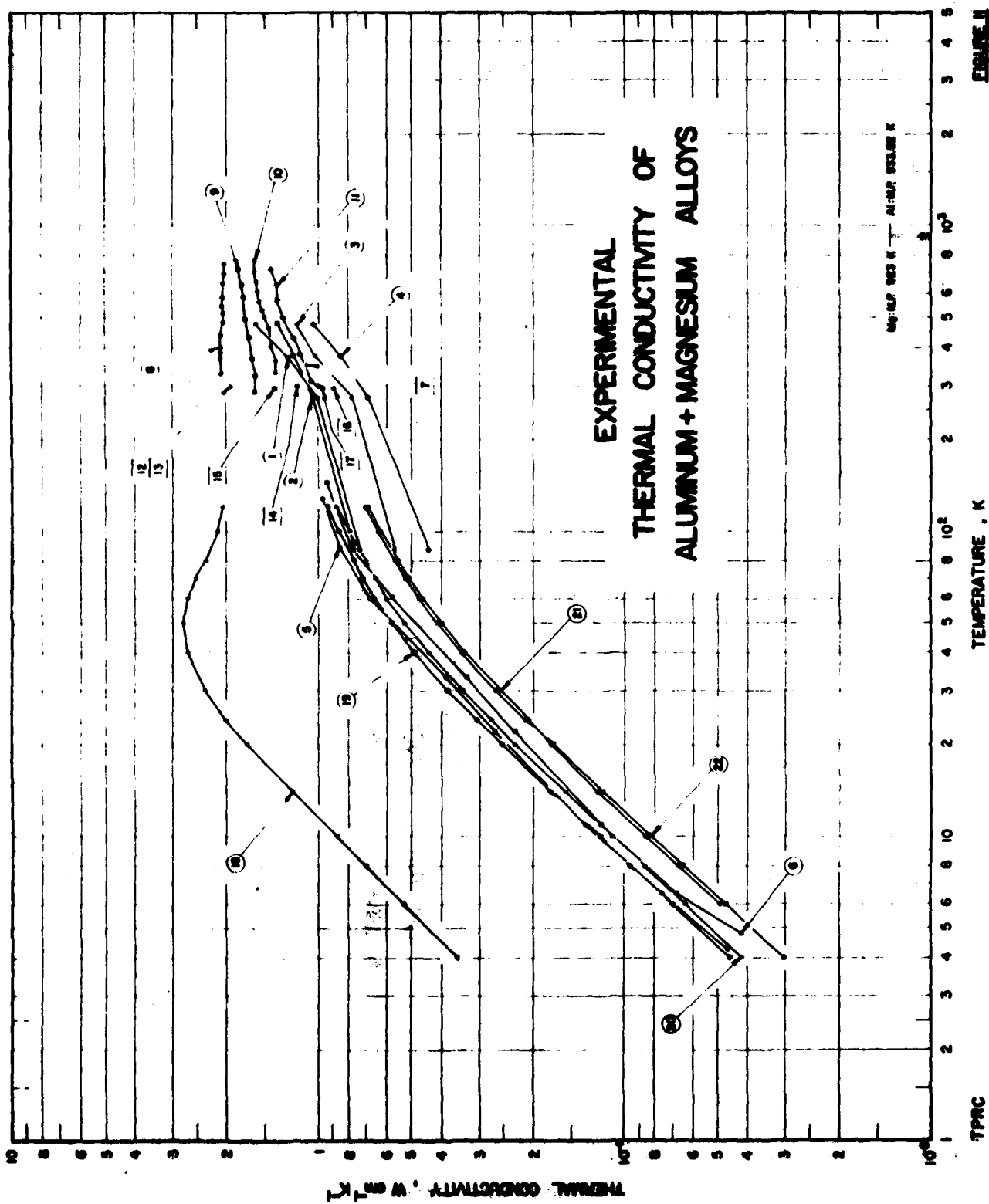


FIGURE 1



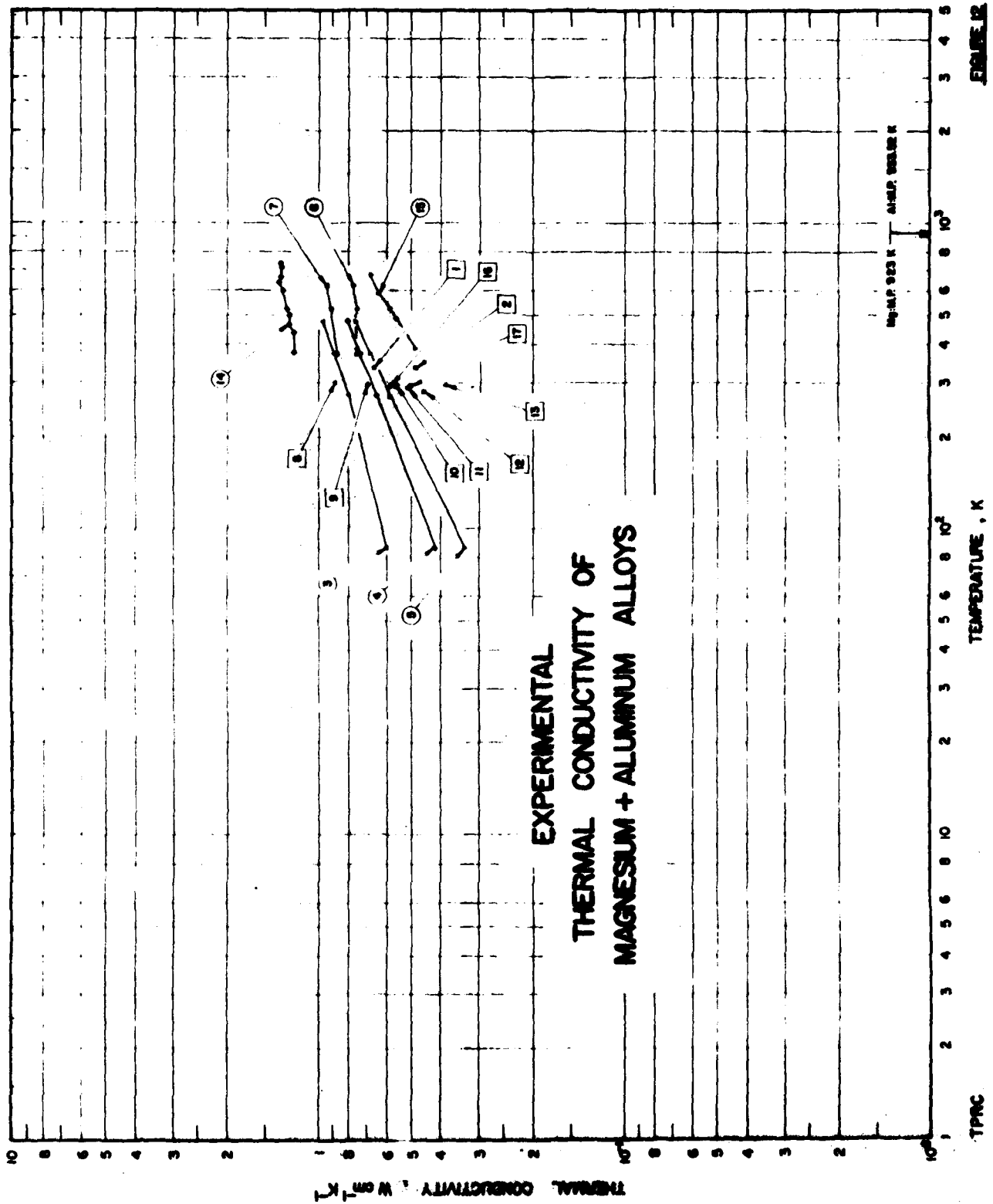


FIGURE 12

TABLE 6. THERMAL CONDUCTIVITY OF ALUMINUM - MAGNESIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Al	Mg	
1 41	Mannchen, W.	1931	L	57-476		92.0	8.0	Cast; electrical conductivity reported as 20.02, 13.21, 10.5, and $5.5 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
2 41	Mannchen, W.	1931	L	97-476		92.0	9.0	Annealed; electrical conductivity reported as 24.5, 15.05, 12.25, and $10.25 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
3 41	Mannchen, W.	1931	L	87-476		88.0	12.0	Cast; electrical conductivity reported as 19.6, 11.95, 9.4, and $7.55 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
4 41	Mannchen, W.	1931	L	87-476		86.0	14.0	Annealed; electrical conductivity reported as 12.7, 8.96, 8.05, and $7.6 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
5 56	Johnson, E.W.	1960		4.3-128	5052	97.7-97.1	2.2-2.8	0.10 Mn; annealed.
6 56	Johnson, E.W.	1960		4.8-144	5154	96.8-96.0	3.1-3.9	0.10 Mn; annealed.
7 122	Meyer-Rascher, E.	1940		348.2	Magnesium	93.0	7.0	15 mm in diameter and 72 mm long; density $2.63 \text{ g cm}^{-3}$ .
8 56	Mikryukov, V.E. and Karagzyan, A.G.	1961	E	327-746		99.3	0.7	3 mm diameter and 300 mm long; prepared from 99.9 pure Al.
9 56	Mikryukov, V.E. and Karagzyan, A.G.	1961	E	285-716		97.0	3.0	Similar to the above specimen.
10 56	Mikryukov, V.E. and Karagzyan, A.G.	1961	E	330-766		95.0	5.0	Similar to the above specimen.
11 56	Mikryukov, V.E. and Karagzyan, A.G.	1961	E	289-717		92.0	8.0	Similar to the above specimen.
12 123	Materials in Design Engineering	1959		296.2	5005	Bal.	0.8	Nominal composition; annealed at 617 K; density $2.68 \text{ g cm}^{-3}$ ; electrical resistivity $3.4 \mu\Omega \text{ cm}$ at 20 C.
13 123	Materials in Design Engineering	1959		296.2	5050	Bal.	1.0-1.8	Nominal composition; annealed at 617 K; density $2.69 \text{ g cm}^{-3}$ .
14 123	Materials in Design Engineering	1959		296.2	5056	Bal.	4.7-5.6	0.05-0.20 Cr and 0.05-0.20 Mn (nominal composition); annealed at 617 K; density $2.63 \text{ g cm}^{-3}$ ; electrical resistivity $5.94 \mu\Omega \text{ cm}$ at 20 C.
15 123	Materials in Design Engineering	1959		293.2	G4A	96.0	4.0	Nominal composition; as cast; density $2.63 \text{ g cm}^{-3}$ .
16 123	Materials in Design Engineering	1959		293.2	G10A	96.0	4.0	Nominal composition; as cast; density $2.67 \text{ g cm}^{-3}$ .
17 123	Materials in Design Engineering	1959		293.2	G8A	92.0	8.0	Nominal composition; as cast; density $2.67 \text{ g cm}^{-3}$ .
18 97	Powell, R. L., Hall, W.J. and Roder, H.M.	1960	L	4-120	6063-T5	Bal.	0.65	0.38 Si, 0.1 each Fe, Cu, Mn, 0.01 each Cr, Ca, Ti, V, Zn, 0.001 Ca, and 0.001 Pb; 3.66 mm diameter rod specimen; grain size 0.063 mm x 0.049 mm (longitudinal) and 0.062 mm (transverse); precipitation heat-treated; electrical resistivity 0.28, 0.28, 0.33, 0.43, 0.8, 2.3, and $3.5 \mu\Omega \text{ cm}$ at 4, 10, 40, 60, 100, 200, and 300 K, respectively; smoothed values reported.

TABLE 6. THERMAL CONDUCTIVITY OF ALUMINUM + MAGNESIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Al	Mg	
19 57	Powell, R. L., Hall, W. J. and Roder, H. M.	1960	L	4-120	5052-O	Bal.	2.46	0.22 Cr, 0.1 each Cu, Fe, Si, Ga, Mn, Zn, 0.01 Ti, 0.01 V, 0.001 Ca, and 0.001 Zr; grain size 0.056 mm x 0.032 mm (longitudinal) and 0.040 mm (transverse); annealed in vacuum for 1 hr at 350 C; electrical resistivity 2.0, 2.1, 2.2, 2.7, 4.4, and 5.0 $\mu\Omega$ cm at 4, 20, 60, 100, 200, and 300 K, respectively; smoothed values reported.
20 57	Powell, R. L., et al.	1960	L	4-120	5154-O	Bal.	3.32	0.21 Cr, 0.1 each Cu, Fe, Si, Mn, 0.01 each Ti, V, Zn, 0.001 Ca, and 0.001 Pb; grain size 0.036 mm x 0.028 mm (longitudinal) and 0.032 mm (transverse); annealed in vacuum for 1 hr at 350 C; electrical resistivity 2.2, 2.3, 2.4, and 2.5 $\mu\Omega$ cm at 4, 10, 30, and 60 K, respectively; smoothed values reported.
21 57	Powell, R. L., et al.	1960	L	6-120	5083-O	Bal.	4.44	0.7 Mn, 0.1 each Cr, Fe, Si, 0.04 Cu; supplied by R. D. Olleman, Kaiser Aluminum and Chemical Co.; average crystal grain size 0.74 mm x 0.21 mm (longitudinal) and 0.54 mm x 0.14 mm (transverse); annealed in vacuum for 1 hr at 350 C.
22 57	Powell, R. L., et al.	1960	L	4-120	5086-F	Bal.	4.10	0.51 Mn, 0.28 Fe, 0.1 each Cr, Si, Zn, 0.07 Cu, and 0.02 Ti; average crystal grain size 0.061 mm x 0.023 mm (longitudinal) and 0.086 mm x 0.080 mm (transverse); as-fabricated; electrical resistivity 3.0, 3.0, 3.1, 3.6, 5.0, and 5.7 $\mu\Omega$ cm at 4, 40, 60, 100, 200, and 300 K, respectively; smoothed values reported.

TABLE 7. THERMAL CONDUCTIVITY OF MAGNESIUM - ALUMINUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Mg	Al	
1 45	Smith, A.W.	1925	L	336.2		95.82	4.12	0.028 Fe and 0.019 Si; ~5 cm long and 0.3 cm <sup>2</sup> in cross-section; supplied by Aluminum Co. of America; electrical conductivity $9.06 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 63 C.
2 45	Smith, A.W.	1925	L	336.2		89.82	10.12	0.023 Si and 0.028 Fe; similar to the above specimen except electrical conductivity $6.00 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 63 C.
3 124, 41	Steebler, J.; Mammchen, W.	1929 1931	L	87-476		94.0	6.0	1.23 cm <sup>2</sup> in cross-section and 3 cm long; cast; electrical conductivity 14.7, 8.04, 6.47, and $5.99 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
4 124, 41	Steebler, J.; Mammchen, W.	1929 1931	L	87-476		92.0	8.0	1.23 cm <sup>2</sup> in cross-section and 3 cm long; electrical conductivity 13.32, 7.31, 5.95, and $5.55 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
5 124, 41	Steebler, J.; Mammchen, W.	1929 1931	L	87-476		88	12	1.23 cm <sup>2</sup> in cross-section and 3 cm long; electrical conductivity 9.65, 5.99, 5.27, and $4.90 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 87, 273, 373, and 476 K, respectively.
6 60	Mayhew, H.J.	1928	L	373-423		94	6	12 in. long and 1 in. in diameter; annealed at 300 C for 3 hr.
7 60	Mayhew, H.J.	1928	L	373-423		89	11	Similar to the above specimen.
8 50	Kilachi, R.	1932	E	300.2		97.9	2.1	3 mm diameter and 200 mm long; electrical conductivity $11.9 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 27 C.
9 50	Kilachi, R.	1932	E	295.5		95.8	4.2	3 mm diameter and 200 mm long; electrical conductivity $8.9 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 22.3 C.
10 50	Kilachi, R.	1932	E	286.1		93.8	6.2	3 mm diameter and 200 mm long; electrical conductivity $6.9 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 21.9 C.
11 50	Kilachi, R.	1932	E	291.5		91.8	8.2	3 mm diameter and 200 mm long; electrical conductivity $5.9 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 18.3 C.
12 50	Kilachi, R.	1932	E	281.5		89.7	10.3	3 mm diameter and 200 mm long; electrical conductivity $5.5 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 19.3 C.
13 50	Kilachi, R.	1932	E	296.5		87.8	12.2	3 mm diameter and 200 mm long; electrical conductivity $5.1 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 23.1 C.
14 125	Challand, S.	1967	C	375-736	Magnox; Al 80		0.80	0.0050 Be, 0.0020 Mn, and 0.0004 Cu; 1.2 to 1.3 cm in diameter and 1.8 to 2.5 cm long; Armco iron used as comparative material.
15 125	Challand, S.	1967	C	387-674	Magnox; Atesia T		8-9	0.5-1 Zn and 0.2 Mn; 1.2 to 1.3 cm in diameter and 1.8 to 2.5 cm long; Armco iron used as comparative material.
16 125	Materials in Design Engineering	1959		283.2	AZ60A-F		5.8-7.2	0.4-1.5 Zn and >0.15 Mn (nominal composition); density 1.80 g cm <sup>-3</sup> ; electrical resistivity 12.5 $\mu\Omega$ cm at 20 C.
17 125	Materials in Design Engineering	1959		293.2	AZ80A-T		7.8-9.2	0.2-0.8 Zn and >0.12 Mn (nominal composition); density 1.83 g cm <sup>-3</sup> ; electrical resistivity 14.5 $\mu\Omega$ cm at 20 C.
18 173	Powell, R.W.; Robinson, M.J.; and Tye, R.F.	1964	C	323-773	Magnox B		1.0	0.002-0.003 Be; 2.5 cm diameter x 20' cm long; electrical resistivity 6.05, 6.5, 7.3, 8.9, 10.6, 12.3, and 14.15 $\mu\Omega$ cm at 20, 50, 100, 200, 300, 400, and 500 C, respectively.

\* Not shown in figure.

### 4.3. Copper-Gold Alloy System

The copper-gold alloy system forms a continuous series of solid solutions over the entire range of compositions. Ordered structures are formed at temperatures below about 663 K for compositions ranging from about 40 to 63% Au (17.7 to 35.5 At.% Au) and at temperatures below about 683 K for compositions ranging from about 63 to 94% Au (35.5 to 83.5 At.% Au). These ordered structures are due to the formation of the intermetallic compounds  $\text{Cu}_3\text{Au}$  (50.85% Au),  $\text{CuAu}$  (75.63% Au), and  $\text{CuAu}_2$  (90.30% Au). In this work only the thermal conductivity data of disordered alloys are treated.

There are 75 sets of experimental data available for the thermal conductivity of this alloy system. Of the 17 data sets for Cu + Au alloys listed in Table 9 and shown in Figure 15, nine sets are merely single data points around room temperature. Of the 58 data sets for Au + Cu alloys listed in Table 10 and shown in Figure 16, 35 sets are single data points.

For the Cu + Au alloys, the data can be separated into three groups: the low temperature data of Grüneisen and Reddemann [61] (Cu + Au curves 1 and 2) and Kemp, et al. [62] (Cu + Au curves 8 and 9), the data of Sedström [63,64] (Cu + Au curves 10-15) at the ice point, and the five points around 440 K measured by Zolotukhin [65] (Cu + Au curves 3-7) for a partially ordered 5% Au. No data are available above 470 K. Hence, the experimental data are very limited. To derive recommended values, the electronic component  $k_e$  was calculated from eq. (12) and the lattice component  $k_g$  was calculated from eq. (35). The total  $k$  was obtained by adding  $k_g$  to  $k_e$ . The results agree with the data of Sedström [63] (Cu + Au curves 10, 12, 13, and 15) at the ice point and with the data of Kemp, et al. [62] (Cu + Au curves 8 and 9) and of Leaver and Charsley [120] (Cu + Cu curve 16) at lower temperatures to within 8%. The recommended values are for disordered alloys only; hence Zolotukhin's data (Cu + Au curves 3-7) were not used for comparison. The recommended curves were extended to the solidus points at high temperatures. The curves for alloys containing 10% Au or less were not extended to temperatures below 40 K because of the large uncertainties of the calculated  $k_g$  values. For denser alloys, however, the curves were extended to 4 K using  $k_g$  values derived from the data of Kemp, et al. [62]. The  $k_g$  values for dilute alloys are extremely uncertain at low temperatures and are not reported below 60 K.

For the Au + Cu alloys, the experimental data were mostly obtained below the order-disorder transition temperature on specimens in the ordering range, except for two measurements made by Grüneisen and Reddemann [61] (Au + Cu curves 40 and 41) on specimens containing 1.57 and 3.10% Cu at low temperatures and one made by Goff, et al. [66] (Au + Cu curve 56) on a disordered  $\text{Cu}_3\text{Au}$  specimen. The recommended values for disordered alloys were derived from  $k_e$  calculated from eq. (12) and  $k_g$  calculated from eq. (35). Due to poor experimental data, detailed quantitative comparison of the calculated values

is not practical. However, the recommended values agree with the data of Grüneisen and Reddemann [61] (Au + Cu curves 38-41, 45, 46, and 48) at low temperatures and the data of Goff, et al. [66] (Au + Cu curves 56-58) from 60 to 300 K to within 10%. The recommended curves were extended to the solidus points at the high temperature end, but not below 40 K at the low temperature end owing to the large uncertainties of the calculated  $k_g$  values at very low temperatures, except for the curves for alloys with 45 and 50% Cu, which were extended to 4 K using the  $k_g$  values derived from the data of Kemp, et al. [62]. The  $k_g$  values for alloys containing 40% Cu or less are very uncertain at low temperatures and are not reported below 60 K.

The resulting recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 8 for 25 alloy compositions. These values are for well-annealed disordered alloys. The values for  $k$  are also shown in Figures 13 and 14. The values of residual electrical resistivity for the alloys are also given in Table 8. The uncertainties of the  $k$  values are stated in a footnote to Table 8, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 99.50% (99.94 At.%) Au: 0.50% (0.16 At.%)			Cu: 99.00% (99.68 At.%) Au: 1.00% (0.32 At.%)			Cu: 97.00% (98.01 At.%) Au: 3.00% (0.99 At.%)			Cu: 95.00% (98.33 At.%) Au: 5.00% (1.67 At.%)		
$\rho_0 = 0.10 \mu\Omega$ cm			$\rho_0 = 0.20 \mu\Omega$ cm			$\rho_0 = 0.530 \mu\Omega$ cm			$\rho_0 = 0.870 \mu\Omega$ cm		
T	k	$k_e$	T	k	$k_e$	T	k	$k_e$	T	k	$k_e$
4		0.977	4		0.469	4		0.164	4		0.112
6		1.47	6		0.733	6		0.276	6		0.168
8		1.95	8		0.977	8		0.369	8		0.225
10		2.44	10		1.22	10		0.461	10		0.281
15		3.66	15		1.83	15		0.691	15		0.421
20		4.99	20		2.44	20		0.922	20		0.562
25		5.76	25		2.96	25		1.14	25		0.697
30		6.11	30		3.49	30		1.36	30		0.832
40		6.76	40		4.17	40		1.73	40		1.08
50		6.30	50		4.46	50		1.99	50		1.28
60	5.57*	5.26	60	4.34*	4.09	60	2.29*	2.12	60	1.55*	1.41
70	4.80*	4.50	70	3.98*	3.74	70	2.34*	2.18	70	1.63*	1.50
80	4.37*	4.09	80	3.75*	3.52	80	2.36*	2.21	80	1.70*	1.58
90	4.12*	3.85	90	3.60*	3.38	90	2.39*	2.24	90	1.76*	1.64
100	4.01*	3.75	100	3.55*	3.34	100	2.44*	2.30	100	1.83*	1.72
150	3.92*	3.71	150	3.60*	3.44	150	2.74*	2.63	150	2.17*	2.08
200	3.86*	3.71	200	3.65*	3.51	200	2.92*	2.82	200	2.42*	2.34
250	3.86*	3.71	250	3.69*	3.56	250	3.05*	2.97	250	2.60*	2.53
273	3.85*	3.71	273	3.70*	3.58	273	3.10*	3.02	273	2.67	2.60
300	3.85*	3.72	300	3.71*	3.60	300	3.15*	3.07	300	2.74*	2.68
350	3.86*	3.74	350	3.73*	3.63	350	3.21*	3.14	350	2.85*	2.79
400	3.83*	3.73	400	3.72*	3.63	400	3.26*	3.20	400	2.92*	2.87
500	3.77*	3.68	500	3.69*	3.61	500	3.32*	3.26	500	3.03*	2.98
600	3.71*	3.64	600	3.65*	3.58	600	3.34*	3.29	600	3.08*	3.04
700	3.68*	3.59	700	3.60*	3.54	700	3.35*	3.31	700	3.12*	3.08
800	3.66*	3.54	800	3.55*	3.50	800	3.34*	3.30	800	3.14*	3.11
900	3.63*	3.50	900	3.50*	3.45	900	3.31*	3.27	900	3.14*	3.11
1000	3.46*	3.44	1000	3.45*	3.41	1000	3.28*	3.25	1000	3.13*	3.10
1200	3.36*	3.32	1200	3.33*	3.29	1200	3.20*	3.17	1200	3.03*	3.06
1300	3.26*		1303	3.24*		1346	3.13*		1339	3.04*	

\* Uncertainties of the total thermal conductivity,  $k$ , are as follows:

99.50 Cu - 0.50 Au:  $\pm 15\%$  below 100 K,  $\pm 10\%$  between 100 and 300 K, and  $\pm 8\%$  above 300 K.

99.00 Cu - 1.00 Au:  $\pm 15\%$  below 100 K,  $\pm 10\%$  between 100 and 300 K, and  $\pm 8\%$  above 300 K.

97.00 Cu - 3.00 Au:  $\pm 15\%$  below 200 K and  $\pm 10\%$  above 200 K.

95.00 Cu - 5.00 Au:  $\pm 15\%$  below 200 K and  $\pm 10\%$  above 200 K.

† Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 90.00% (96.54 At.%) Au: 10.00% ( 3.46 At.%)					Cu: 85.00% (94.61 At.%) Au: 15.00% ( 5.39 At.%)					Cu: 90.00% (92.54 At.%) Au: 20.00% ( 7.46 At.%)					Cu: 75.00% (90.29 At.%) Au: 25.00% ( 9.71 At.%)				
$\rho_0 = 1.72 \mu\Omega \text{ cm}$					$\rho_0 = 2.58 \mu\Omega \text{ cm}$					$\rho_0 = 3.32 \mu\Omega \text{ cm}$					$\rho_0 = 4.45 \mu\Omega \text{ cm}$				
T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>	
4	0.0568				4	0.0462	0.0379	0.00829		4	0.0358	0.0278	0.00805		4	0.0299	0.0220	0.00788	
6	0.0662				6	0.746	0.0568	0.0178		6	0.0580	0.0416	0.0164		6	0.0482	0.0329	0.0153	
8	0.117				8	0.104	0.0758	0.0287		8	0.0811	0.0555	0.0256		8	0.0675	0.0439	0.0236	
10	0.142				10	0.134	0.0947	0.0397		10	0.104	0.0694	0.0350		10	0.0867	0.0549	0.0318	
15	0.213				15	0.205	0.142	0.0631		15	0.158	0.104	0.0542		15	0.131	0.0823	0.0486	
20	0.284				20	0.269	0.189	0.0799		20	0.206	0.139	0.0674		20	0.170	0.110	0.0598	
25	0.353				25	0.324	0.234	0.0901		25	0.248	0.173	0.0755		25	0.204	0.137	0.0665	
30	0.421				30	0.375	0.280	0.0950		30	0.286	0.206	0.0795		30	0.233	0.163	0.0697	
40	0.553				40	0.462	0.368	0.0942		40	0.351	0.272	0.0789		40	0.284	0.216	0.0694	
50	0.666				50	0.534	0.446	0.0879		50	0.407	0.333	0.0743		50	0.332	0.267	0.0647	
60	0.856	0.756	0.100 <sup>‡</sup>		60	0.600	0.518	0.0816 <sup>‡</sup>		60	0.458	0.389	0.0694 <sup>‡</sup>		60	0.373	0.312	0.0606 <sup>‡</sup>	
70	0.932	0.839	0.0939 <sup>‡</sup>		70	0.658	0.582	0.0763 <sup>‡</sup>		70	0.506	0.441	0.0649 <sup>‡</sup>		70	0.414	0.358	0.0585 <sup>‡</sup>	
80	1.00	0.916	0.0886 <sup>‡</sup>		80	0.714	0.642	0.0719 <sup>‡</sup>		80	0.552	0.491	0.0610 <sup>‡</sup>		80	0.453	0.400	0.0532 <sup>‡</sup>	
90	1.07	0.982	0.0841 <sup>‡</sup>		90	0.769	0.701	0.0682 <sup>‡</sup>		90	0.597	0.539	0.0578 <sup>‡</sup>		90	0.491	0.441	0.0503 <sup>‡</sup>	
100	1.13 <sup>*</sup>	1.05	0.0801 <sup>‡</sup>		100	0.824 <sup>*</sup>	0.759	0.0649 <sup>‡</sup>		100	0.643	0.568	0.0550 <sup>‡</sup>		100	0.530	0.482	0.0478 <sup>‡</sup>	
150	1.44 <sup>*</sup>	1.37	0.0657 <sup>‡</sup>		150	1.08 <sup>*</sup>	1.03	0.0532 <sup>‡</sup>		150	0.861 <sup>*</sup>	0.816	0.0450 <sup>‡</sup>		150	0.717 <sup>*</sup>	0.678	0.0391 <sup>‡</sup>	
200	1.76 <sup>*</sup>	1.64	0.0565 <sup>‡</sup>		200	1.31 <sup>*</sup>	1.26	0.0437 <sup>‡</sup>		200	1.06 <sup>*</sup>	1.02	0.0388 <sup>‡</sup>		200	0.882 <sup>*</sup>	0.848	0.0337 <sup>‡</sup>	
250	1.90 <sup>*</sup>	1.85	0.0500 <sup>‡</sup>		250	1.50 <sup>*</sup>	1.46	0.0406 <sup>‡</sup>		250	1.22 <sup>*</sup>	1.18	0.0344 <sup>‡</sup>		250	1.03 <sup>*</sup>	1.00	0.0289 <sup>‡</sup>	
273	1.98	1.93	0.0476 <sup>‡</sup>		273	1.58	1.54	0.0386 <sup>‡</sup>		273	1.29 <sup>*</sup>	1.26	0.0328 <sup>‡</sup>		273	1.09	1.06	0.0285 <sup>‡</sup>	
300	2.08 <sup>*</sup>	2.03	0.0452 <sup>‡</sup>		300	1.66 <sup>*</sup>	1.62	0.0367 <sup>‡</sup>		300	1.37 <sup>*</sup>	1.34	0.0311 <sup>‡</sup>		300	1.17	1.14	0.0271 <sup>‡</sup>	
350	2.22 <sup>*</sup>	2.18	0.0414 <sup>‡</sup>		350	1.80 <sup>*</sup>	1.77	0.0336 <sup>‡</sup>		350	1.50 <sup>*</sup>	1.47	0.0286 <sup>‡</sup>		350	1.29	1.26	0.0249 <sup>‡</sup>	
400	2.33 <sup>*</sup>	2.29	0.0383 <sup>‡</sup>		400	1.91 <sup>*</sup>	1.88	0.0312 <sup>‡</sup>		400	1.62 <sup>*</sup>	1.59	0.0265 <sup>‡</sup>		400	1.40 <sup>*</sup>	1.38	0.0231 <sup>‡</sup>	
500	2.50 <sup>*</sup>	2.47	0.0335 <sup>‡</sup>		500	2.11 <sup>*</sup>	2.08	0.0274 <sup>‡</sup>		500	1.81 <sup>*</sup>	1.79	0.0234 <sup>‡</sup>		500	1.59 <sup>*</sup>	1.57	0.0204 <sup>‡</sup>	
600	2.61 <sup>*</sup>	2.58	0.0300 <sup>‡</sup>		600	2.25 <sup>*</sup>	2.23	0.0246 <sup>‡</sup>		600	1.97 <sup>*</sup>	1.95	0.0210 <sup>‡</sup>		600	1.74 <sup>*</sup>	1.72	0.0184 <sup>‡</sup>	
700	2.76 <sup>*</sup>	2.67	0.0274 <sup>‡</sup>		700	2.37 <sup>*</sup>	2.35	0.0224 <sup>‡</sup>		700	2.09 <sup>*</sup>	2.07	0.0192 <sup>‡</sup>		700	1.87 <sup>*</sup>	1.85	0.0168 <sup>‡</sup>	
800	2.76 <sup>*</sup>	2.73	0.0252 <sup>‡</sup>		800	2.46 <sup>*</sup>	2.44	0.0207 <sup>‡</sup>		800	2.19 <sup>*</sup>	2.17	0.0178 <sup>‡</sup>		800	1.97 <sup>*</sup>	1.95	0.0156 <sup>‡</sup>	
900	2.80 <sup>*</sup>	2.78	0.0234 <sup>‡</sup>		900	2.51 <sup>*</sup>	2.49	0.0193 <sup>‡</sup>		900	2.26 <sup>*</sup>	2.24	0.0166 <sup>‡</sup>		900	2.05 <sup>*</sup>	2.04	0.0145 <sup>‡</sup>	
1000	2.83 <sup>*</sup>	2.80	0.0219 <sup>‡</sup>		1000	2.56 <sup>*</sup>	2.54	0.0181 <sup>‡</sup>		1000	2.33 <sup>*</sup>	2.31	0.0155 <sup>‡</sup>		1000	2.12 <sup>*</sup>	2.11	0.0136 <sup>‡</sup>	
1200	2.84 <sup>*</sup>	2.82	0.0195 <sup>‡</sup>		1100	2.59 <sup>*</sup>	2.57	0.0171 <sup>‡</sup>		1100	2.39 <sup>*</sup>	2.37	0.0147 <sup>‡</sup>		1100	2.18 <sup>*</sup>	2.17	0.0128 <sup>‡</sup>	
1320	2.83 <sup>*</sup>				1303	2.63 <sup>*</sup>				1289	2.47 <sup>*</sup>				1277	2.27 <sup>*</sup>			

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

- 90.00 Cu - 10.00 Au:  $\pm 12\%$  below 100 K,  $\pm 8\%$  between 100 and 400 K, and  $\pm 10\%$  above 400 K.  
 85.00 Cu - 15.00 Au:  $\pm 12\%$  below 100 K,  $\pm 8\%$  between 100 and 400 K, and  $\pm 10\%$  above 400 K.  
 90.00 Cu - 20.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.  
 75.00 Cu - 25.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.

<sup>‡</sup> Provisional values.

<sup>\*</sup> In temperature range where no experimental thermal conductivity data are available.



TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)<sup>†</sup>(Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>)

Cu: 70.00% (87.85 At. %) Au: 30.00% (12.15 At. %)				Cu: 65.00% (55.20 At. %) Au: 35.00% (14.80 At. %)				Cu: 60.00% (82.30 At. %) Au: 40.00% (17.70 At. %)				Cu: 55.00% (79.12 At. %) Au: 45.00% (20.88 At. %)			
$\rho_0 = 5.47 \mu\Omega$ cm				$\rho_0 = 6.52 \mu\Omega$ cm				$\rho_0 = 7.52 \mu\Omega$ cm				$\rho_0 = 8.48 \mu\Omega$ cm			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0236	0.0179	0.00772	4	0.0226	0.0150	0.00758	4	0.0205	0.0130	0.00746	4	0.0188	0.0115	0.00735
6	0.0413	0.0268	0.0145	6	0.0364	0.0225	0.0139	6	0.0327	0.0195	0.0132	6	0.0298	0.0173	0.0125
8	0.0575	0.0357	0.0218	8	0.0505	0.0300	0.0205	8	0.0452	0.0260	0.0192	8	0.0409	0.0230	0.0179
10	0.0739	0.0447	0.0292	10	0.0645	0.0375	0.0270	10	0.0575	0.0325	0.0250	10	0.0518	0.0288	0.0230
15	0.111	0.0670	0.0441	15	0.0962	0.0562	0.0400	15	0.0853	0.0487	0.0366	15	0.0765	0.0432	0.0333
20	0.143	0.0893	0.0539	20	0.124	0.0749	0.0488	20	0.109	0.0650	0.0444	20	0.0978	0.0576	0.0402
25	0.171	0.111	0.0596	25	0.147	0.0930	0.0540	25	0.130	0.0807	0.0491	25	0.116	0.0717	0.0445
30	0.195	0.133	0.0623	30	0.168	0.111	0.0566	30	0.148	0.0964	0.0515	30	0.132	0.0856	0.0468
40	0.236	0.175	0.0615	40	0.203	0.147	0.0559	40	0.178	0.127	0.0509	40	0.160	0.113	0.0467
50	0.275	0.217	0.0576	50	0.233	0.181	0.0522	50	0.204	0.157	0.0472	50	0.183	0.140	0.0430
60	0.309	0.255	0.0537	60	0.262	0.214	0.0482	60	0.230	0.186	0.0436	60	0.204	0.164	0.0396
70	0.343	0.293	0.0501	70	0.291	0.246	0.0449	70	0.254	0.214	0.0405	70	0.228	0.191	0.0369
80	0.376	0.329	0.0470	80	0.319	0.277	0.0421	80	0.279	0.241	0.0381	80	0.251	0.216	0.0346
90	0.409	0.364	0.0445	90	0.348	0.308	0.0398	90	0.305	0.269	0.0360	90	0.274	0.241	0.0327
100	0.442	0.400	0.0423	100	0.377	0.339	0.0379	100	0.331	0.297	0.0342	100	0.296	0.265	0.0311
150	0.603	0.568	0.0346	150	0.518	0.487	0.0309	150	0.456	0.428	0.0279	150	0.410	0.385	0.0254
200	0.730	0.720	0.0298	200	0.651	0.624	0.0267	200	0.576	0.552	0.0241	200	0.520	0.498	0.0219
250	0.866	0.859	0.0265	250	0.773	0.749	0.0237	250	0.687	0.666	0.0214	250	0.622	0.603	0.0194
273	0.942	0.917	0.0253	273	0.825	0.802	0.0226	273	0.735	0.716	0.0204	273	0.666	0.647	0.0186
300	1.01	0.986	0.0240	300	0.886	0.865	0.0215	300	0.791	0.772	0.0194	300	0.717	0.699	0.0176
350	1.12	1.10	0.0221	350	0.988	0.968	0.0198	350	0.887	0.869	0.0179	350	0.807	0.791	0.0162
400	1.32	1.20	0.0205	400	1.08	1.06	0.0184	400	0.976	0.959	0.0166	400	0.890	0.875	0.0151
500	1.40	1.38	0.0181	500	1.25	1.23	0.0162	500	1.14	1.13	0.0147	500	1.04	1.03	0.0134
600	1.53	1.53	0.0163	600	1.40	1.39	0.0147	600	1.27	1.26	0.0133	600	1.18	1.17	0.0121
700	1.68	1.67	0.0150	700	1.53	1.52	0.0134	700	1.40	1.39	0.0122	700	1.29	1.28	0.0111
800	1.79	1.78	0.0138	800	1.63	1.62	0.0124	800	1.50	1.49	0.0113	800	1.39	1.38	0.0103
900	1.88	1.87	0.0129	900	1.72	1.71	0.0116	900	1.59	1.58	0.0106	900	1.48	1.47	0.00962
1000	1.98	1.96	0.0122	1000	1.80	1.79	0.0109	1000	1.67	1.66	0.00993	1000	1.56	1.55	0.00906
1100	2.03	2.02	0.0115	1100	1.88	1.87	0.0104	1100	1.74	1.73	0.00938	1100	1.63	1.62	0.00856
1265	2.15			1265	1.97			1245	1.82			1236	1.71		

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:70.00 Cu - 30.00 Au:  $\pm 10\%$  below 200 K,  $\pm 5\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.65.00 Cu - 35.00 Au:  $\pm 10\%$  below 200 K,  $\pm 7\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.60.00 Cu - 40.00 Au:  $\pm 10\%$  below 200 K,  $\pm 7\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.55.00 Cu - 45.00 Au:  $\pm 10\%$  below 200 K,  $\pm 7\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.<sup>‡</sup> Provisional value.<sup>\*</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

$\rho_0 = 9.34 \mu\Omega \text{ cm}$				$\rho_0 = 10.1 \mu\Omega \text{ cm}$				$\rho_0 = 10.9 \mu\Omega \text{ cm}$				$\rho_0 = 11.4 \mu\Omega \text{ cm}$			
Cu: 50.00% (75.61 At.%) Au: 50.00% (24.39 At.%)				Cu: 45.00% (71.72 At.%) Au: 55.00% (28.28 At.%)				Cu: 40.00% (67.39 At.%) Au: 60.00% (32.61 At.%)				Cu: 35.00% (62.54 At.%) Au: 65.00% (37.46 At.%)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0178	0.0105	0.00725	4	0.0168	0.00964	0.00717	4	0.0158	0.00898		4	0.0148	0.00835	
6	0.0277	0.0157	0.0130	6	0.0259	0.0144	0.0115	6	0.0249	0.0135		6	0.0239	0.0128	
8	0.0376	0.0209	0.0167	8	0.0350	0.0193	0.0157	8	0.0340	0.0180		8	0.0330	0.0171	
10	0.0474	0.0262	0.0212	10	0.0437	0.0241	0.0196	10	0.0427	0.0224		10	0.0417	0.0214	
15	0.0694	0.0392	0.0302	15	0.0636	0.0361	0.0275	15	0.0626	0.0337		15	0.0616	0.0321	
20	0.0907	0.0523	0.0394	20	0.0811	0.0482	0.0329	20	0.0801	0.0449		20	0.0791	0.0427	
25	0.105	0.0649	0.0493	25	0.0961	0.0599	0.0362	25	0.0951	0.0557		25	0.0941	0.0532	
30	0.120	0.0777	0.0622	30	0.110	0.0716	0.0379	30	0.109	0.0689		30	0.108	0.0638	
40	0.145	0.108	0.0821	40	0.133	0.0947	0.0380	40	0.126	0.0885	0.0370	40	0.118	0.0842	0.0362
50	0.166	0.137	0.0994	50	0.153	0.117	0.0390	50	0.143	0.110	0.0334	50	0.136	0.104	0.0309
60	0.187	0.161	0.0362	60	0.172	0.139	0.0333	60	0.161	0.130	0.0307	60	0.153	0.124	0.0283
70	0.207	0.173	0.0337	70	0.192	0.161	0.0309	70	0.179	0.150	0.0285	70	0.169	0.143	0.0263
80	0.228	0.196	0.0316	80	0.211	0.182	0.0290	80	0.197	0.170	0.0267	80	0.187	0.162	0.0247
90	0.250	0.220	0.0296	90	0.231	0.204	0.0274	90	0.216	0.191	0.0252	90	0.204	0.181	0.0233
100	0.271	0.243	0.0284	100	0.250	0.224	0.0260	100	0.234	0.210	0.0240	100	0.222	0.200	0.0221
150	0.376	0.353	0.0232	150	0.348	0.327	0.0212	150	0.326	0.306	0.0196	150	0.310	0.292	0.0180
200	0.478	0.456	0.0200	200	0.441	0.423	0.0183	200	0.413	0.396	0.0168	200	0.394	0.378	0.0166
250	0.570	0.552	0.0178	250	0.530	0.514	0.0163	250	0.496	0.481	0.0150	250	0.473	0.459	0.0138
273	0.612	0.595	0.0170	273	0.589	0.553	0.0166	273	0.534	0.520	0.0143	273	0.509	0.496	0.0132
300	0.660	0.644	0.0161	300	0.614	0.599	0.0149	300	0.575	0.561	0.0136	300	0.549	0.536	0.0126
350	0.743	0.728	0.0149	350	0.692	0.678	0.0136	350	0.651	0.638	0.0125	350	0.621	0.609	0.0116
400	0.823	0.809	0.0138	400	0.768	0.755	0.0127	400	0.721	0.709	0.0117	400	0.688	0.677	0.0108
500	0.967	0.955	0.0122	500	0.904	0.893	0.0112	500	0.850	0.840	0.0103	500	0.812	0.802	0.00954
600	1.09	1.08	0.0110	600	1.02	1.01	0.0102	600	0.966	0.957	0.00935	600	0.922	0.913	0.00864
700	1.20	1.20	0.0101	700	1.13	1.12	0.00922	700	1.07	1.06	0.00859	700	1.02	1.01	0.00793
800	1.30	1.29	0.00942	800	1.23	1.21	0.00865	800	1.16	1.15	0.00797	800	1.11	1.10	0.00736
900	1.39	1.38	0.00881	900	1.30	1.29	0.00810	900	1.23	1.22	0.00746	900	1.18	1.17	0.00689
1000	1.46	1.45	0.00829	1000	1.38	1.37	0.00763	1000	1.30	1.29	0.00703	1000	1.25	1.24	0.00649
1100	1.53	1.52	0.00786	1100	1.44	1.43	0.00722	1100	1.37	1.36	0.00666	1100	1.31	1.30	0.00615
1200	1.63			1216	1.51			1206	1.43	1.42	0.00632	1196	1.37	1.36	0.00587

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

50.00 Cu - 50.00 Au:  $\pm 10\%$  below 200 K,  $\pm 7\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.  
 45.00 Cu - 55.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.  
 40.00 Cu - 60.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.  
 35.00 Cu - 65.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.

<sup>‡</sup> Provisional values.<sup>\*</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)†  
 Temperature, T, K; Thermal Conductivity,  $k$ ,  $W\ cm^{-1}\ K^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $W\ cm^{-1}\ K^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $W\ cm^{-1}\ K^{-1}$

$\rho_0 = 11.8\ \mu\Omega\ cm$				$\rho_0 = 12.0\ \mu\Omega\ cm$				$\rho_0 = 11.7\ \mu\Omega\ cm$				$\rho_0 = 10.8\ \mu\Omega\ cm$			
Cu: 30.00% (57.05 At. %) Au: 70.00% (42.95 At. %)				Cu: 25.00% (50.82 At. %) Au: 75.00% (49.18 At. %)				Cu: 20.00% (43.66 At. %) Au: 80.00% (56.34 At. %)				Cu: 15.00% (35.36 At. %) Au: 85.00% (64.63 At. %)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.00827		4		0.00818		4		0.00834		4		0.00869	
6		0.0124		6		0.0123		6		0.0125		6		0.0136	
8		0.0165		8		0.0164		8		0.0167		8		0.0182	
10		0.0207		10		0.0204		10		0.0208		10		0.0227	
15		0.0310		15		0.0307		15		0.0313		15		0.0341	
20		0.0413		20		0.0409		20		0.0417		20		0.0454	
25		0.0514		25		0.0508		25		0.0518		25		0.0565	
30		0.0615		30		0.0607		30		0.0620		30		0.0675	
40	0.113*	0.0814	0.0318*	40	0.110	0.0803	0.0296*	40	0.110	0.0820	0.0277*	40	0.115	0.0892	0.0282*
50	0.129*	0.100	0.0286*	50	0.127	0.0998	0.0267*	50	0.127	0.102	0.0260*	50	0.134	0.110	0.0236*
60	0.146*	0.120	0.0263*	60	0.143	0.118	0.0245*	60	0.144	0.121	0.0228*	60	0.153	0.131	0.0217*
70	0.163*	0.139	0.0244*	70	0.159	0.136	0.0227*	70	0.161	0.140	0.0213*	70	0.172	0.152	0.0201*
80	0.180*	0.157	0.0229*	80	0.176	0.155	0.0213*	80	0.178	0.158	0.0198*	80	0.191	0.172	0.0188*
90	0.197*	0.175	0.0216*	90	0.193*	0.173	0.0201*	90	0.196*	0.177	0.0188*	90	0.209	0.191	0.0178*
100	0.214*	0.194	0.0205*	100	0.209*	0.190	0.0191*	100	0.213*	0.195	0.0178*	100	0.226*	0.211	0.0169*
150	0.299*	0.282	0.0167*	150	0.294*	0.279	0.0155*	150	0.299*	0.294	0.0145*	150	0.321*	0.307	0.0137*
200	0.381*	0.367	0.0144*	200	0.375*	0.362	0.0134*	200	0.381*	0.369	0.0125*	200	0.409*	0.397	0.0118*
250	0.459*	0.445	0.0128*	250	0.452*	0.440	0.0119*	250	0.459*	0.448	0.0111*	250	0.492*	0.481	0.0109*
273	0.492	0.480	0.0122*	273	0.486	0.475	0.0114*	273	0.493	0.482	0.0106*	273	0.529	0.519	0.0100*
300	0.531*	0.519	0.0116*	300	0.525*	0.514	0.0108*	300	0.532*	0.522	0.0101*	300	0.570	0.560	0.00951*
350	0.600*	0.589	0.0107*	350	0.593*	0.583	0.00996*	350	0.601*	0.592	0.00929*	350	0.643	0.634	0.00875*
400	0.686*	0.676	0.00997*	400	0.678	0.669	0.00926*	400	0.687	0.678	0.00864*	400	0.712*	0.704	0.00814*
500	0.786*	0.777	0.00894*	500	0.775*	0.767	0.00820*	500	0.785*	0.777	0.00765*	500	0.836	0.829	0.00720*
600	0.893*	0.885	0.00799*	600	0.881*	0.874	0.00742*	600	0.892*	0.885	0.00692*	600	0.947*	0.940	0.00650*
700	0.990*	0.983	0.00734*	700	0.975*	0.968	0.00681*	700	0.988*	0.982	0.00635*	700	1.04*	1.03	0.00596*
800	1.08*	1.07	0.00682*	800	1.06*	1.05	0.00632*	800	1.07*	1.06	0.00589*	800	1.13*	1.12	0.00553*
900	1.18*	1.16	0.00638*	900	1.13*	1.12	0.00592*	900	1.14*	1.13	0.00551*	900	1.20*	1.20	0.00517*
1000	1.21*	1.20	0.00601*	1000	1.19*	1.18	0.00558*	1000	1.21*	1.20	0.00520*	1000	1.26*	1.26	0.00487*
1100	1.27*	1.26	0.00570*	1100	1.25*	1.24	0.00528*	1100	1.26*	1.25	0.00492*	1100	1.31*	1.31	0.00461*
1185	1.32*	1.31	0.00547*	1185	1.29*	1.28	0.00507*	1185	1.30*	1.30	0.00473*	1185	1.35*	1.35	0.00442*

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 30.00 Cu - 70.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 25.00 Cu - 75.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 20.00 Cu - 80.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 15.00 Cu - 85.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.

\* Provisional value.

.. In temperature range where no experimental thermal conductivity data are available.

TABLE S. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)<sup>†</sup>

† Temperature, T, K; Thermal Conductivity,  $k$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $\text{W cm}^{-1} \text{K}^{-1}$

Cu: 10.00% (25.82 At.%) Au: 90.00% (74.38 At.%)				Cu: 5.00% (14.03 At.%) Au: 95.00% (85.97 At.%)				Cu: 3.00% (8.75 At.%) Au: 97.00% (91.25 At.%)				Cu: 1.00% (3.04 At.%) Au: 99.00% (96.96 At.%)			
$\rho_0 = 8.72 \mu\Omega \text{ cm}$				$\rho_0 = 5.27 \mu\Omega \text{ cm}$				$\rho_0 = 3.44 \mu\Omega \text{ cm}$				$\rho_0 = 1.40 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.0112		4		0.0185		4		0.0294		4		0.0698	
6		0.0168		6		0.0278		6		0.0426		6		0.105	
8		0.0224		8		0.0371		8		0.0568		8		0.140	
10		0.0280		10		0.0464		10		0.0701		10		0.174	
15		0.0430		15		0.0695		15		0.106		15		0.262	
20		0.0560		20		0.0927		20		0.142		20		0.349	
25		0.0696		25		0.114		25		0.174		25		0.430	
30		0.0832		30		0.136		30		0.206		30		0.492	
40	0.135	0.110	0.0254 <sup>‡</sup>	40	0.204	0.178	0.0265 <sup>‡</sup>	40	0.297	0.267	0.0300 <sup>‡</sup>	40	0.663	0.622	0.0410 <sup>‡</sup>
50	0.159	0.136	0.0229 <sup>‡</sup>	50	0.242	0.218	0.0240 <sup>‡</sup>	50	0.351	0.324	0.0271 <sup>‡</sup>	50	0.758	0.721	0.0370 <sup>‡</sup>
60	0.181	0.160	0.0210 <sup>‡</sup>	60	0.278	0.256	0.0220 <sup>‡</sup>	60	0.403	0.378	0.0248 <sup>‡</sup>	60	0.848	0.814	0.0337 <sup>‡</sup>
70	0.205	0.185	0.0193 <sup>‡</sup>	70	0.314	0.294	0.0204 <sup>‡</sup>	70	0.453	0.430	0.0229 <sup>‡</sup>	70	0.932	0.901	0.0312 <sup>‡</sup>
80	0.228	0.210	0.0183 <sup>‡</sup>	80	0.350	0.331	0.0191 <sup>‡</sup>	80	0.502	0.480	0.0215 <sup>‡</sup>	80	1.01	0.981	0.0290 <sup>‡</sup>
90	0.251	0.234	0.0172 <sup>‡</sup>	90	0.385	0.367	0.0180 <sup>‡</sup>	90	0.549	0.529	0.0201 <sup>‡</sup>	90	1.09	1.06	0.0272 <sup>‡</sup>
100	0.274 <sup>*</sup>	0.258	0.0163 <sup>‡</sup>	100	0.420 <sup>*</sup>	0.403	0.0171 <sup>‡</sup>	100	0.597 <sup>*</sup>	0.578	0.0190 <sup>‡</sup>	100	1.17 <sup>*</sup>	1.14	0.0256 <sup>‡</sup>
150	0.385 <sup>*</sup>	0.372	0.0133 <sup>‡</sup>	150	0.594 <sup>*</sup>	0.570	0.0138 <sup>‡</sup>	150	0.812 <sup>*</sup>	0.797	0.0150 <sup>‡</sup>	150	1.47 <sup>*</sup>	1.45	0.0203 <sup>‡</sup>
200	0.485 <sup>*</sup>	0.478	0.0114 <sup>‡</sup>	200	0.731 <sup>*</sup>	0.719	0.0118 <sup>‡</sup>	200	0.993 <sup>*</sup>	0.980	0.0129 <sup>‡</sup>	200	1.69 <sup>*</sup>	1.68	0.0172 <sup>‡</sup>
250	0.585 <sup>*</sup>	0.575	0.0101 <sup>‡</sup>	250	0.862 <sup>*</sup>	0.852	0.0104 <sup>‡</sup>	250	1.15 <sup>*</sup>	1.14	0.0114 <sup>‡</sup>	250	1.86 <sup>*</sup>	1.84	0.0150 <sup>‡</sup>
273	0.627	0.617	0.00844 <sup>‡</sup>	273	0.918	0.908	0.00995 <sup>‡</sup>	273	1.21	1.20	0.0108 <sup>‡</sup>	273	1.92 <sup>*</sup>	1.91	0.0142 <sup>‡</sup>
300	0.675	0.666	0.00815 <sup>‡</sup>	300	0.979	0.970	0.00943 <sup>‡</sup>	300	1.28	1.27	0.0102 <sup>‡</sup>	300	1.98 <sup>*</sup>	1.97	0.0134 <sup>‡</sup>
350	0.757	0.749	0.00841 <sup>‡</sup>	350	1.08	1.07	0.00865 <sup>‡</sup>	350	1.39	1.38	0.00935 <sup>‡</sup>	350	2.09 <sup>*</sup>	2.07	0.0122 <sup>‡</sup>
400	0.834 <sup>*</sup>	0.826	0.00781 <sup>‡</sup>	400	1.17 <sup>*</sup>	1.16	0.00801 <sup>‡</sup>	400	1.49 <sup>*</sup>	1.48	0.00865 <sup>‡</sup>	400	2.16 <sup>*</sup>	2.15	0.0112 <sup>‡</sup>
500	0.967	0.960	0.00690 <sup>‡</sup>	500	1.33 <sup>*</sup>	1.32	0.00704 <sup>‡</sup>	500	1.64 <sup>*</sup>	1.63	0.00758 <sup>‡</sup>	500	2.27 <sup>*</sup>	2.26	0.00974 <sup>‡</sup>
600	1.08 <sup>*</sup>	1.07	0.00622 <sup>‡</sup>	600	1.45 <sup>*</sup>	1.44	0.00633 <sup>‡</sup>	600	1.76 <sup>*</sup>	1.75	0.00678 <sup>‡</sup>	600	2.34 <sup>*</sup>	2.33	0.00864 <sup>‡</sup>
700	1.18 <sup>*</sup>	1.17	0.00570 <sup>‡</sup>	700	1.55 <sup>*</sup>	1.54	0.00578 <sup>‡</sup>	700	1.86 <sup>*</sup>	1.85	0.00618 <sup>‡</sup>	700	2.37 <sup>*</sup>	2.36	0.00780 <sup>‡</sup>
800	1.27 <sup>*</sup>	1.26	0.00528 <sup>‡</sup>	800	1.62 <sup>*</sup>	1.61	0.00534 <sup>‡</sup>	800	1.92 <sup>*</sup>	1.91	0.00569 <sup>‡</sup>	800	2.38 <sup>*</sup>	2.37	0.00712 <sup>‡</sup>
900	1.34 <sup>*</sup>	1.34	0.00493 <sup>‡</sup>	900	1.68 <sup>*</sup>	1.68	0.00498 <sup>‡</sup>	900	1.96 <sup>*</sup>	1.95	0.00529 <sup>‡</sup>	900	2.37 <sup>*</sup>	2.36	0.00687 <sup>‡</sup>
1000	1.39 <sup>*</sup>	1.39	0.00464 <sup>‡</sup>	1000	1.73 <sup>*</sup>	1.73	0.00467 <sup>‡</sup>	1000	1.98 <sup>*</sup>	1.98	0.00495 <sup>‡</sup>	1000	2.34 <sup>*</sup>	2.33	0.00610 <sup>‡</sup>
1100	1.44 <sup>*</sup>	1.44	0.00439 <sup>‡</sup>	1100	1.77 <sup>*</sup>	1.77	0.00441 <sup>‡</sup>	1100	1.99 <sup>*</sup>	1.99	0.00466 <sup>‡</sup>	1100	2.31 <sup>*</sup>	2.30	0.00571 <sup>‡</sup>
1196	1.48 <sup>*</sup>	1.48	0.00417 <sup>‡</sup>	1241	1.81 <sup>*</sup>			1270	1.98 <sup>*</sup>			1296	2.22 <sup>*</sup>		

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 10.00 Cu - 90.00 Au:  $\pm 10\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 5.00 Cu - 95.00 Au:  $\pm 15\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 3.00 Cu - 97.00 Au:  $\pm 15\%$  below 200 K,  $\pm 8\%$  between 200 and 500 K, and  $\pm 10\%$  above 500 K.
- 1.00 Cu - 99.00 Au:  $\pm 15\%$  below 200 K and  $\pm 10\%$  above 200 K.

<sup>\*</sup> Provisional values.

<sup>‡</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 8. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-GOLD ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>

Cu: 0.50% (1.53 At.%) Au: 99.50% (98.47 At.%)					
$\rho_0 = 0.770 \mu\Omega \text{ cm}$					
T	k	k <sub>e</sub>	k <sub>g</sub>		
4		0.127			
6		0.190			
8		0.254			
10		0.317			
15		0.476			
20		0.634			
25		0.740			
30		0.843			
40	1.08 <sup>*</sup>	1.08			0.0641 <sup>‡</sup>
50	1.20 <sup>*</sup>	1.15			0.0400 <sup>‡</sup>
60	1.30 <sup>*</sup>	1.25			0.0443 <sup>‡</sup>
70	1.35 <sup>*</sup>	1.35			0.0409 <sup>‡</sup>
80	1.40 <sup>*</sup>	1.44			0.0378 <sup>‡</sup>
90	1.50 <sup>*</sup>	1.52			0.0351 <sup>‡</sup>
100	1.60 <sup>*</sup>	1.61			0.0329 <sup>‡</sup>
120	1.80 <sup>*</sup>	1.80			0.0257 <sup>‡</sup>
140	2.10 <sup>*</sup>	2.14			0.0213 <sup>‡</sup>
160	2.30 <sup>*</sup>	2.28			0.0185 <sup>‡</sup>
173	2.30 <sup>*</sup>	2.32			0.0175 <sup>‡</sup>
200	2.30 <sup>*</sup>	2.37			0.0104 <sup>‡</sup>
300	2.40 <sup>*</sup>	2.43			0.0149 <sup>‡</sup>
400	2.50 <sup>*</sup>	2.48			0.0126 <sup>‡</sup>
500	2.50 <sup>*</sup>	2.55			0.0116 <sup>‡</sup>
600	2.50 <sup>*</sup>	2.56			0.0102 <sup>‡</sup>
700	2.50 <sup>*</sup>	2.56			0.00914 <sup>‡</sup>
800	2.50 <sup>*</sup>	2.57			0.00828 <sup>‡</sup>
900	2.50 <sup>*</sup>	2.58			0.00757 <sup>‡</sup>
1000	2.50 <sup>*</sup>	2.59			0.00695 <sup>‡</sup>
1200	2.40 <sup>*</sup>	2.39			0.00605 <sup>‡</sup>
1323	2.35 <sup>*</sup>				

† Uncertainties of the total thermal conductivity, k, are as follows:  
0.50 Cu - 99.50 Au:  $\pm 15\%$  below 200 K and  $\pm 10\%$  above 200 K.

<sup>‡</sup> Provisional values.

\* In temperature ranges where no experimental thermal conductivity data are available.

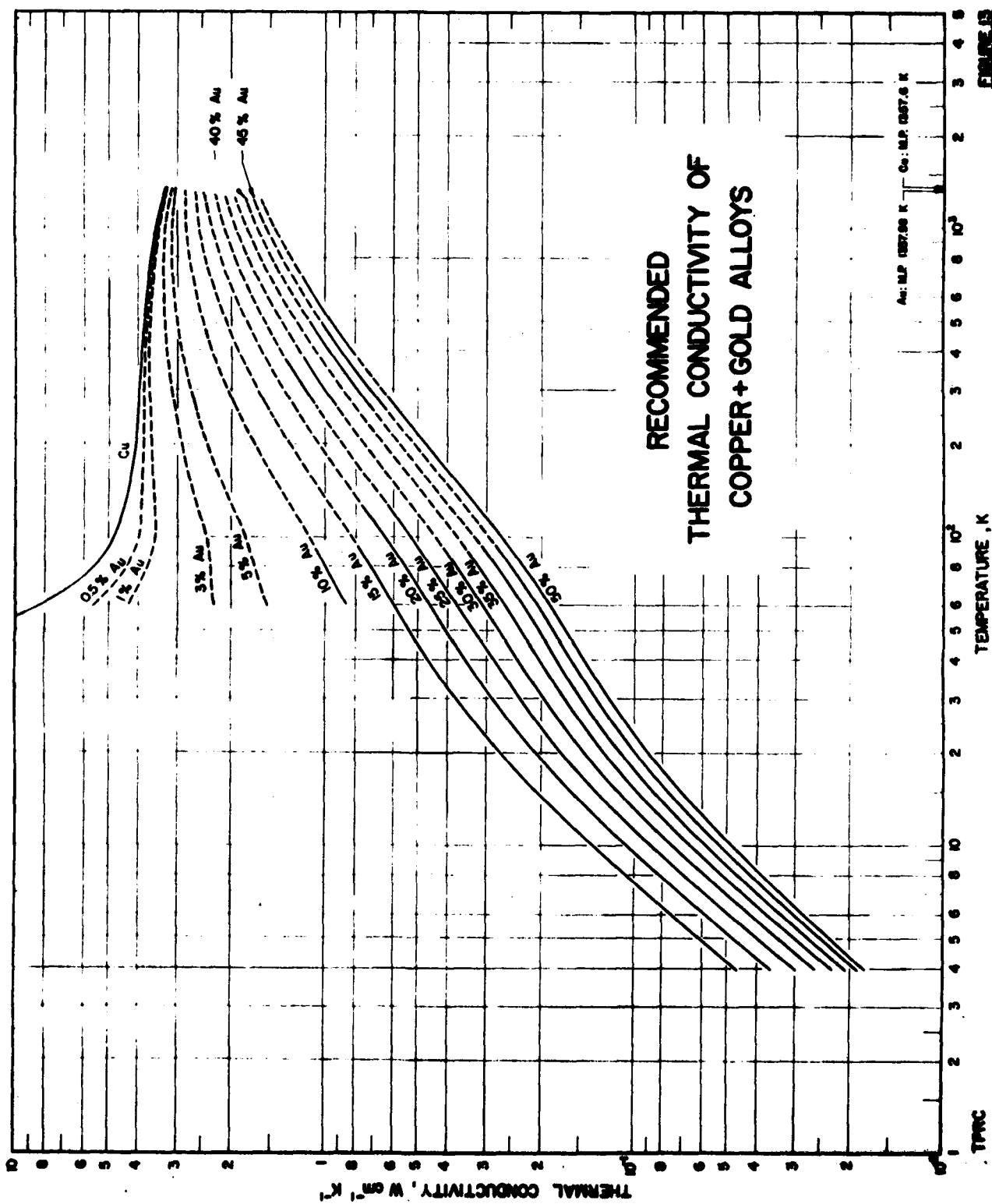
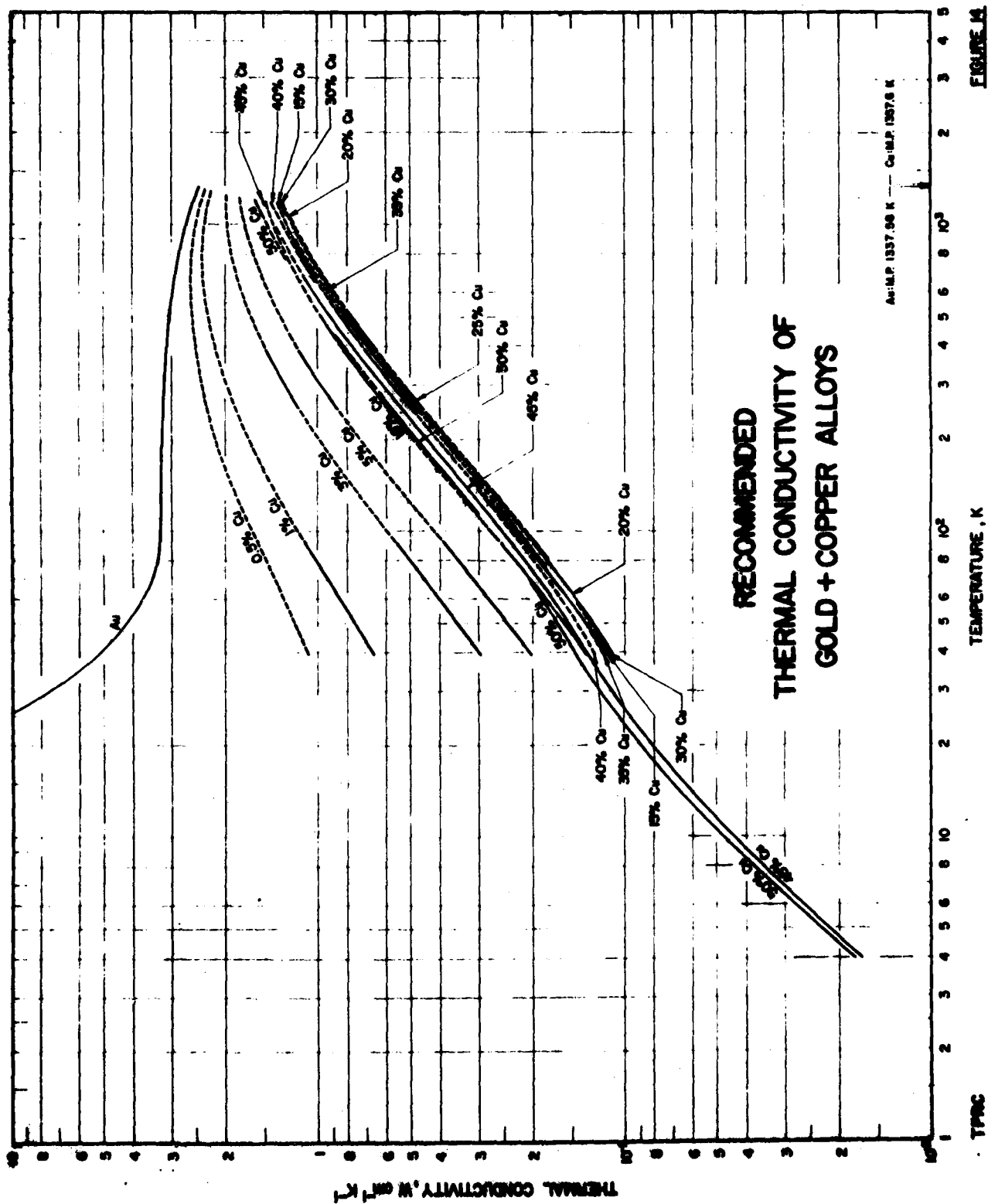


FIGURE 13



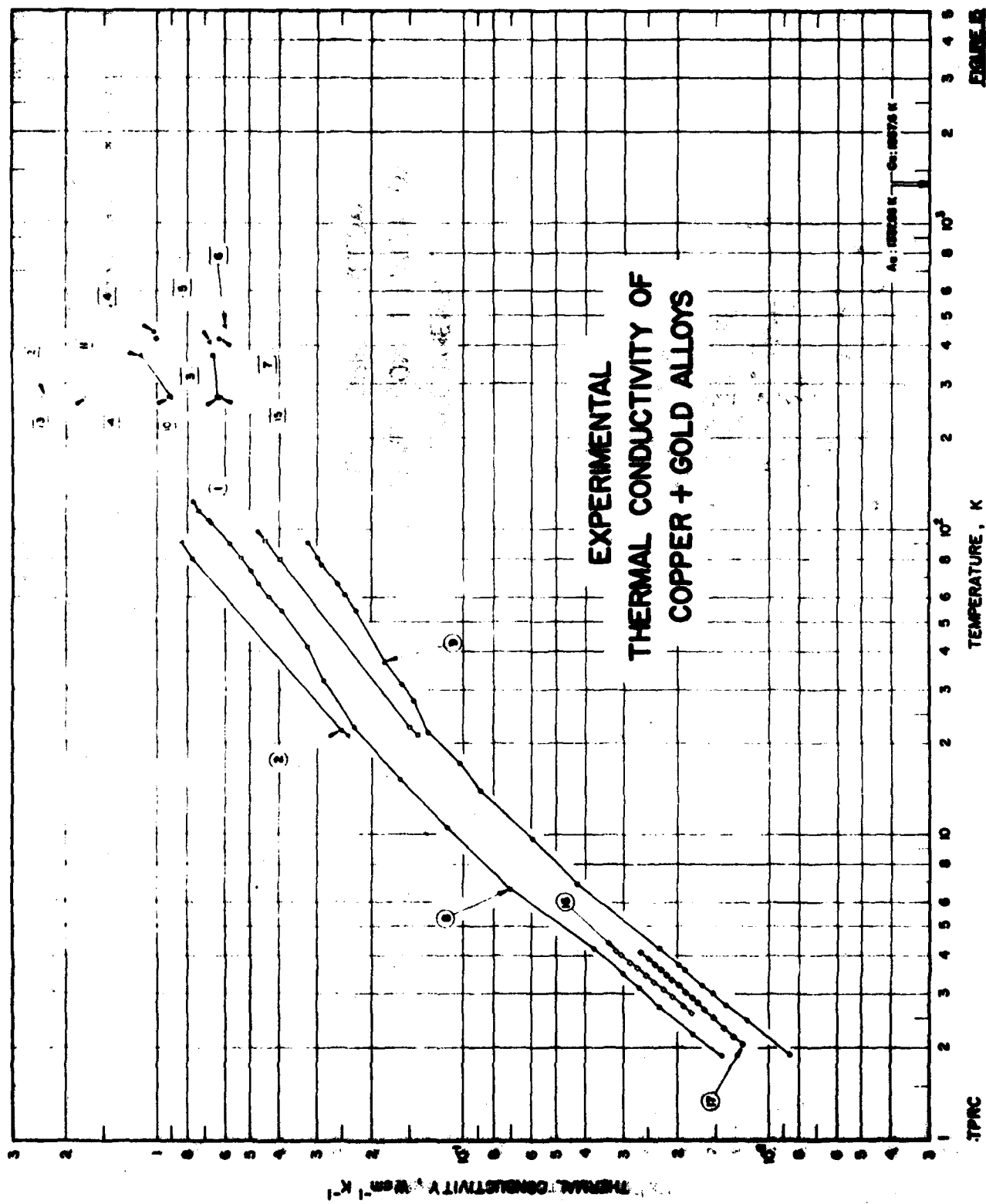


FIGURE 12



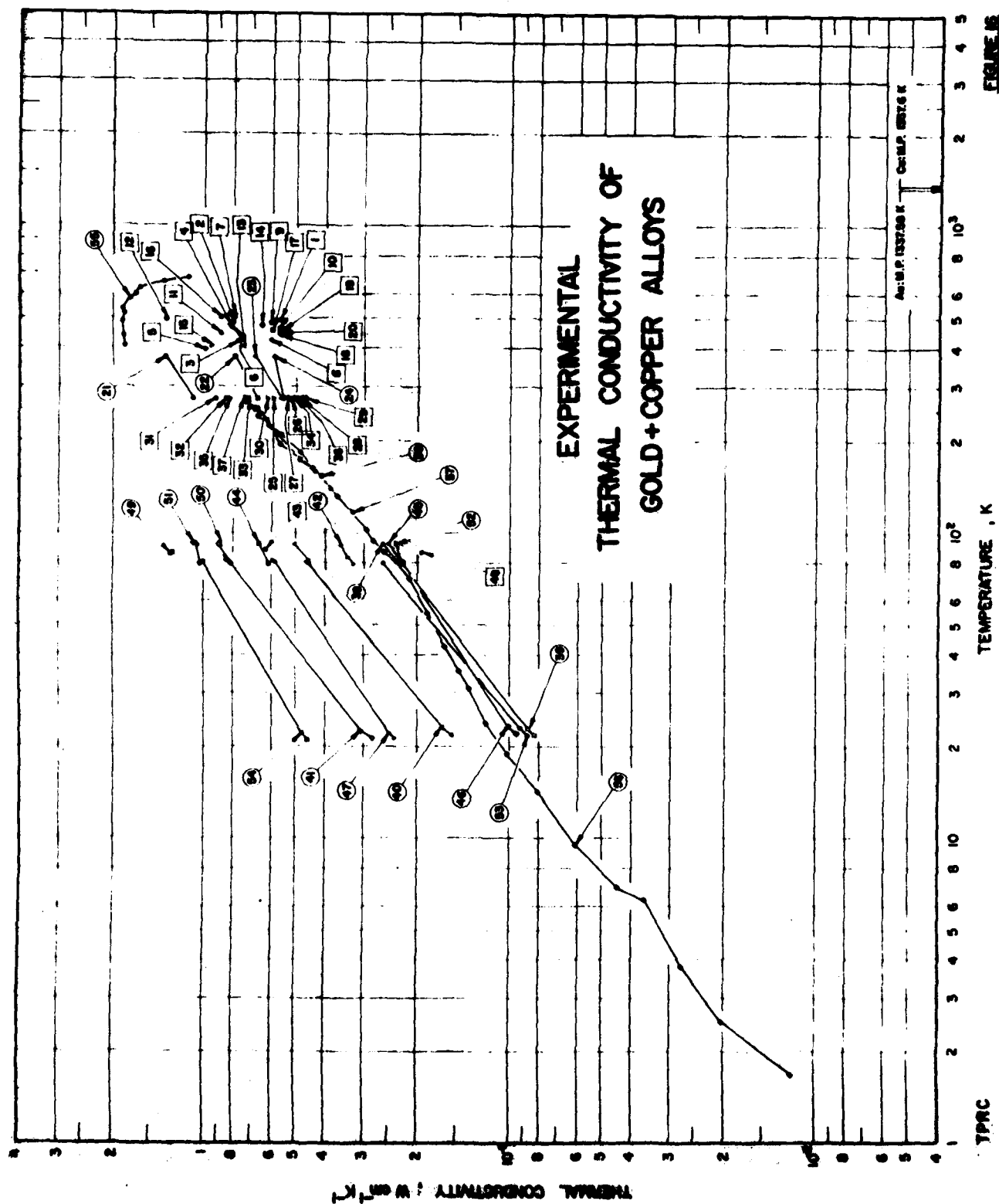


TABLE 9. THERMAL CONDUCTIVITY OF COPPER - GOLD ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Authors	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Au	
1 61	Grüisen, E. and Reddmann, H.	1934	L	21-93	10	75.2	24.8	Calculated composition; polycrystalline; form factor $1.53 \times 10^4$ ; residual electrical resistivity $6.54 \mu\Omega$ cm; electrical resistivity $8.09$ and $4.71 \mu\Omega$ cm at $-190$ and $-251$ C, respectively.
2 61	Grüisen, E. and Reddmann, H.	1934	L	21-91	9	87.4	12.6	Calculated composition; polycrystalline; form factor $2.61 \times 10^4$ ; residual electrical resistivity $3.63 \mu\Omega$ cm; electrical resistivity $2.487$ and $2.172 \mu\Omega$ cm at $-190$ and $-251$ C, respectively.
3 65	Zolotarev, G. E.	1957	L	422.7		56.33	43.67	Calculated composition; cylindrical specimen $1.43$ cm long and $0.63$ cm <sup>2</sup> in cross-section; cast; density $14.30$ g cm <sup>-3</sup> .
4 65	Zolotarev, G. E.	1957	L	448.2				The above specimen; annealed for 10 hr.
5 65	Zolotarev, G. E.	1957	L	411.2				The above specimen; annealed for 20 hr.
6 65	Zolotarev, G. E.	1957	L	467.2				The above specimen; annealed for 30 hr.
7 65	Zolotarev, G. E.	1957	L	422.2				The above specimen; annealed for 40 hr.
8 63	Kemp, W.R.G., Klemens, P.G., and Tinsch, R.J.	1957	L	1.9-124			20.09	8 cm long and 0.5 cm in diameter; annealed at 750 C for 1 hr; electrical resistivity reported as 3.53, 3.91, and 5.37 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
9 62	Kemp, W.R.G., et al.	1957	L	1.9-91			37.99	Similar to the above specimen except electrical resistivity reported as 7.04, 7.36, and 8.59 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
10 63	Sedström, E.	1919	T	273, 373		55.24	44.76	Calculated composition; specimen rolled and drawn to wire 1 mm diameter; heated to near melting point for 0.5 hr; electrical conductivity $5.7 \times 10^4$ and $5.5 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 0 and 100 C, respectively.
11 63	Sedström, E.	1919	T	273, 373		73.52	26.48	Similar to the above specimen except electrical conductivity $10.7 \times 10^4$ and $9.1 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 0 and 100 C, respectively.
12 63	Sedström, E.	1924	T	273.2		94.6	5.4	Calculated composition; specimen rolled and drawn to a wire of 3 cm in length and 1 mm <sup>2</sup> in cross-section, then heated to the melting point; electrical resistivity $6.2 \mu\Omega$ cm at 0 C.
13 63	Sedström, E.	1924	T	273.2		87.6	12.4	Similar to the above specimen except electrical resistivity $4.7 \mu\Omega$ cm at 0 C.
14 63	Sedström, E.	1924	T	273.2		72.7	27.3	Similar to the above specimen except electrical resistivity $7.3 \mu\Omega$ cm at 0 C.
15 63	Sedström, E.	1924	T	273.2		55.0	45.0	Similar to the above specimen except electrical resistivity $10.4 \mu\Omega$ cm at 0 C.
16 126	Leaver, A.D.W. and Charley, P.	1971	L	2.6-4.2	10 Au		25.4	Polycrystalline; obtained from the International Research and Development Co., Ltd.; annealed; residual electrical resistivity $4.306 \mu\Omega$ cm.
17 126	Leaver, A.D.W. and Charley, P.	1971	L	2.1-4.1	10 Au			The above specimen (annealed) strained 13.4% under a stress of $36.66$ kg mm <sup>-2</sup> ; residual electrical resistivity $4.444 \mu\Omega$ cm.

TABLE 10. THERMAL CONDUCTIVITY OF GOLD - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Au	Cu	
1	65 Zolotarev, G. E.	1957	L	468.7	IV	75.61	24.39	Calculated composition; cast; 1.30 cm long and 0.63 cm <sup>2</sup> in cross-section; density 18.34 g cm <sup>-3</sup> .
2	65 Zolotarev, G. E.	1957	L	483.2	IV			The above specimen annealed 10 hr at 200 C.
3	65 Zolotarev, G. E.	1957	L	420.7	IV			The above specimen annealed 20 hr at 200 C.
4	65 Zolotarev, G. E.	1957	L	473.7	IV			The above specimen annealed 30 hr at 200 C.
5	65 Zolotarev, G. E.	1957	L	396.2	IV			The above specimen annealed 40 hr at 200 C.
6	65 Zolotarev, G. E.	1957	L	466.2	V	85.20	14.80	Calculated composition; cast; 1.30 cm long and 0.63 cm <sup>2</sup> in cross-section; density 19.40 g cm <sup>-3</sup> .
7	65 Zolotarev, G. E.	1957	L	504.7	V			The above specimen annealed 10 hr at 200 C.
8	65 Zolotarev, G. E.	1957	L	426.2	V			The above specimen annealed 20 hr at 200 C.
9	65 Zolotarev, G. E.	1957	L	481.7	V			The above specimen annealed 30 hr at 200 C.
10	65 Zolotarev, G. E.	1957	L	460.7	V			The above specimen annealed 40 hr at 200 C.
11	65 Zolotarev, G. E.	1957	L	445.7	II	50.82	49.18	Calculated composition; cast; 1.49 cm long and 0.63 cm <sup>2</sup> in cross-section; density 15.05 g cm <sup>-3</sup> .
12	65 Zolotarev, G. E.	1957	L	493.2	II			The above specimen annealed 10 hr at 200 C.
13	65 Zolotarev, G. E.	1957	L	401.7	II			The above specimen annealed 20 hr at 200 C.
14	65 Zolotarev, G. E.	1957	L	470.2	II			The above specimen annealed 30 hr at 200 C.
15	65 Zolotarev, G. E.	1957	L	493.7	II			The above specimen annealed 40 hr at 200 C.
16	65 Zolotarev, G. E.	1957	L	497.7	III	62.54	37.46	Calculated composition; cast; 1.45 cm long and 0.63 cm <sup>2</sup> in cross-section; density 16.70 g cm <sup>-3</sup> .
17	65 Zolotarev, G. E.	1957	L	455.7	III			The above specimen annealed 10 hr at 200 C.
18	65 Zolotarev, G. E.	1957	L	437.7	III			The above specimen annealed 20 hr at 200 C.
19	65 Zolotarev, G. E.	1957	L	467.7	III			The above specimen annealed 30 hr at 200 C.
20	65 Zolotarev, G. E.	1957	L	444.7	III			The above specimen annealed 40 hr at 200 C.
21	65 Sedström, E.	1919	T	273, 373		96.73	3.27	Calculated composition; rolled and drawn to 1 mm diameter wire; annealed close to melting point for 0.5 hr; electrical conductivity 14.3 and 13.4 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 0 and 100 C, respectively.
22	63 Sedström, E.	1919	T	273, 373		92.55	7.45	Similar to the above specimen except electrical conductivity 8.5 and 8.2 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 0 and 100 C, respectively.
23	63 Sedström, E.	1919	T	273, 373		87.77	12.23	Similar to the above specimen except electrical conductivity 6.3 and 5.9 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 0 and 100 C, respectively.
24	63 Sedström, E.	1919	T	273, 373		59.25	40.75	Similar to the above specimen except electrical conductivity 5.0 and 4.6 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 0 and 100 C, respectively.
25	64 Sedström, E.	1924	T	273.2		50.8	49.2	Rolled and drawn to 1 mm <sup>2</sup> in cross-sectional area and 3 cm long; annealed close to melting point for 0.5 hr; electrical resistivity 10.8 μΩ cm at 273 K.
26	64 Sedström, E.	1924	T	273.2		54.0	46.0	Similar to the above specimen except electrical resistivity 11.4 μΩ cm at 273 K.

TABLE 10. THERMAL CONDUCTIVITY OF GOLD - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent): Au Cu	Composition (continued), Specifications, and Remarks
27	64 Sedström, E.	1924	T	273.2		57.0 43.0	Similar to the above specimen except electrical resistivity 11.8 $\mu\Omega$ cm at 273 K.
28	64 Sedström, E.	1924	T	273.2		62.6 37.4	Similar to the above specimen except electrical resistivity 13.0 $\mu\Omega$ cm at 273 K.
29	64 Sedström, E.	1924	T	273.2		67.2 32.8	Similar to the above specimen except electrical resistivity 13.6 $\mu\Omega$ cm at 273 K.
30	64 Sedström, E.	1924	T	273.2		71.9 28.1	Similar to the above specimen except electrical resistivity 10.5 $\mu\Omega$ cm at 273 K.
31	64 Sedström, E.	1924	T	273.2		78.1 21.9	Similar to the above specimen except electrical resistivity 7.6 $\mu\Omega$ cm at 273 K.
32	64 Sedström, E.	1924	T	273.2		78.2 21.8	Similar to the above specimen except electrical resistivity 7.6 $\mu\Omega$ cm at 273 K.
33	64 Sedström, E.	1924	T	273.2		78.9 21.1	Similar to the above specimen except electrical resistivity 8.4 $\mu\Omega$ cm at 273 K.
34	64 Sedström, E.	1924	T	273.2		82.1 17.9	Similar to the above specimen except electrical resistivity 11.6 $\mu\Omega$ cm at 273 K.
35	64 Sedström, E.	1924	T	273.2		82.4 17.6	Similar to the above specimen except electrical resistivity 11.6 $\mu\Omega$ cm at 273 K.
36	64 Sedström, E.	1924	T	273.2		87.5 12.5	Similar to the above specimen except electrical resistivity 11.6 $\mu\Omega$ cm at 273 K.
37	64 Sedström, E.	1924	T	273.2		94.1 5.9	Similar to the above specimen except electrical resistivity 8.0 $\mu\Omega$ cm at 273 K.
38	61 Grönqvist, E. and Reddemann, H.	1934	L	80-92	11	89.6 10.4	Calculated composition; polycrystalline; cast; electrical resistivity 9.27 $\mu\Omega$ cm at 83 K.
39	61 Grönqvist, E. and Reddemann, H.	1934	L	22-80	11a		The above specimen annealed in vacuo for 40 hr at 365 C; electrical resistivity 10.88 $\mu\Omega$ cm at 273 K.
40	61 Grönqvist, E. and Reddemann, H.	1934	L	22-91	12	96.9 3.10	Calculated composition; polycrystalline; cast; electrical resistivity 3.826, 4.345, and 5.94 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
41	61 Grönqvist, E. and Reddemann, H.	1934	L	21-91	13	98.43 1.57	Calculated composition; polycrystalline; cast; electrical resistivity 1.841, 2.353, and 3.93 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
42	61 Grönqvist, E. and Reddemann, H.	1934	L	79-91	14a	50.1 49.9	Calculated composition; polycrystalline; cast; quenched from 800 C; electrical resistivity 6.64 $\mu\Omega$ cm at 83 K.
43	61 Grönqvist, E. and Reddemann, H.	1934	L	87.4	14b		The above specimen annealed at ~400 C for 20 hr; electrical resistivity 3.23 and 5.80 $\mu\Omega$ cm at 83 and 273 K, respectively.
44	61 Grönqvist, E. and Reddemann, H.	1934	L	79, 92	14c		The above specimen annealed at ~360 C for 32 hr; electrical resistivity 3.126 and 5.42 $\mu\Omega$ cm at 83 and 273 K, respectively.
45	61 Grönqvist, E. and Reddemann, H.	1934	L	90, 92	14d		The above specimen annealed at ~820 C for 2 hr and then quenched; electrical resistivity 11.49 $\mu\Omega$ cm at 273 K.
46	61 Grönqvist, E. and Reddemann, H.	1934	L	22-80	14e		The above specimen measured after 5 months; electrical resistivity 9.88 and 11.46 $\mu\Omega$ cm at 83 and 273 K, respectively.

TABLE 10. THERMAL CONDUCTIVITY OF GOLD-COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Au Cu	Composition (continued), Specifications, and Remarks
47 61	Griffioen, E. and Reddemann, H.	1934	L	21-81	14f		The above specimen annealed at ~325 C for 30 hr; electrical resistivity 2.70 and 3.41 $\mu\Omega$ cm at 22 and 83 K, respectively.
48 61	Griffioen, E. and Reddemann, H.	1934	L	86.9	15a	75.6 24.4	Calculated composition; polycrystalline; cast; quenched from 800 C; electrical resistivity 11.57, 13.2, and 13.41 $\mu\Omega$ cm at 83, 273, and 292 K, respectively.
49 61	Griffioen, E. and Reddemann, H.	1934	L	85, 85	15b		The above specimen annealed at 360 C for 22 hr; electrical resistivity 1.753, 3.974, and 4.82 $\mu\Omega$ cm at 83, 273, and 298 K, respectively.
50 61	Griffioen, E. and Reddemann, H.	1934	L	81, 92	15c		The above specimen annealed at 345 C for 30 hr; electrical resistivity 2.226 and 4.48 $\mu\Omega$ cm at 83 and 273 K, respectively.
51 61	Griffioen, E. and Reddemann, H.	1934	L	79-91	15d		The above specimen annealed at 325 C for 30 hr; electrical resistivity 1.797 and 4.07 $\mu\Omega$ cm at 83 and 273 K, respectively.
52 61	Griffioen, E. and Reddemann, H.	1934	L	79, 91	15e		The above specimen annealed at 800 C for 2 hr and then quenched; electrical resistivity 9.17 $\mu\Omega$ cm at 83 K.
53 61	Griffioen, E. and Reddemann, H.	1934	L	22-79	15f		The above specimen measured after 4 months; electrical resistivity 7.90 $\mu\Omega$ cm at 83 K.
54 61	Griffioen, E. and Reddemann, H.	1934	L	21-80	15g		The above specimen annealed at ~325 C for 30 hr; electrical resistivity 1.826 and 4.09 $\mu\Omega$ cm at 83 and 273 K, respectively.
55 126, 174, 175	Lindemann, S. D. and Quimby, S. L.	1962	L	407-680	Cu <sub>3</sub> Au	49.18	Intermetallic compound; 0.1858 in. diameter and 2.41 in. long; successively annealed at 360 C for 90 hr, 240 C for 110 hr, and 220 C for 600 hr; critical temperature lies between 387.5 and 358.2 C; electrical resistivity reported as 4.2582, 4.3684, 4.8367, 5.2834, 5.8889, 6.2509, 6.6710, 7.2362, 8.2142, 9.3036, 10.6252, 10.8963, 11.3171, 12.1987, 13.6671, 14.0257, 14.0355, 14.0752, 14.1064, and 14.2969 $\mu\Omega$ cm at 33.30, 43.74, 83.38, 124.04, 160.92, 211.71, 248.80, 278.71, 311.98, 345.78, 373.61, 377.83, 382.60, 385.80, 387.54, 388.19, 390.97, 395.25, 404.20, and 419.77 C, respectively (selected from 76 points reported by the authors).
56 66	Goff, J. F., Verbalis, A. C., Rhys, J. J., and Klemens, P. G.	1968	L	1.7-275	Cu <sub>3</sub> Au	49.18	0.1 Fe; intermetallic compound; specimen 60 mm x 3.2 mm x 3.2 mm; prepared from ASARCO five-9 Cu and Au material; the melt was first homogenized by rocking for about 10 min then cast in a constricted end of the same tube; annealed for 2 hr at 850 C and quenched from 700 C by breaking the capsule in water (all melting and annealing the specimen and specimen materials were done in quartz tubes had been evacuated to less than 10 <sup>-4</sup> torr at close-off); residual electrical resistivity 0.092 $\mu\Omega$ cm; electrical resistivity ratio $\rho(300K)/\rho(4.2K) = 1.23$ ; electrical resistivity reported as 9.1, 9.1, 9.2, 9.3, 9.3, 9.3, 9.4, 9.4, 9.5, 9.7, 9.6, 9.9, 10.2, 10.5, 10.8, 11.0, 10.9, and 11.3 $\mu\Omega$ cm at 1.8, 5.6, 13.0, 16.4, 19.6, 30.0, 41.3, 63.2, 86.6, 101, 114, 131, 163, 191, 221, 254, 281, and 299 K respectively.

TABLE 10. THERMAL CONDUCTIVITY OF GOLD - COPPER ALLOYS - SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Au	Cu	
57	Goff, J. F., Verbaars, A. C., Rhyne, J. J., and Klemens, P. G.	1965	L	117-269	Cu <sub>3</sub> Au	49.18		Intermetallic compound; similar to the above except electrical resistivity reported as 9.7, 9.9, 10.1, 10.3, 10.4, 10.6, 10.8, 10.7, 10.9, and 11.3 $\mu\Omega$ cm at 88, 115, 148, 159, 180, 194, 224, 232, 247, and 283 K, respectively; measurement was made with an insulating packing inside the radiation shield.
58	Goff, J. F., et al.	1965	L	154-276	Cu <sub>3</sub> Au	49.18		Similar to the above except electrical resistivity reported as 9.1, 9.9, 9.8, 9.9, 10.1, 10.5, 11.0, 10.7, 10.9, 11.0, and 11.4 $\mu\Omega$ cm at 9.0, 112, 129, 143, 171, 211, 235, 240, 260, 265, and 287 K, respectively; measurement was made in the original condition but with a measured radiation loss correction.

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THERMAL CONDUCTIVITY OF TEN SELECTED BINARY ALLOY  
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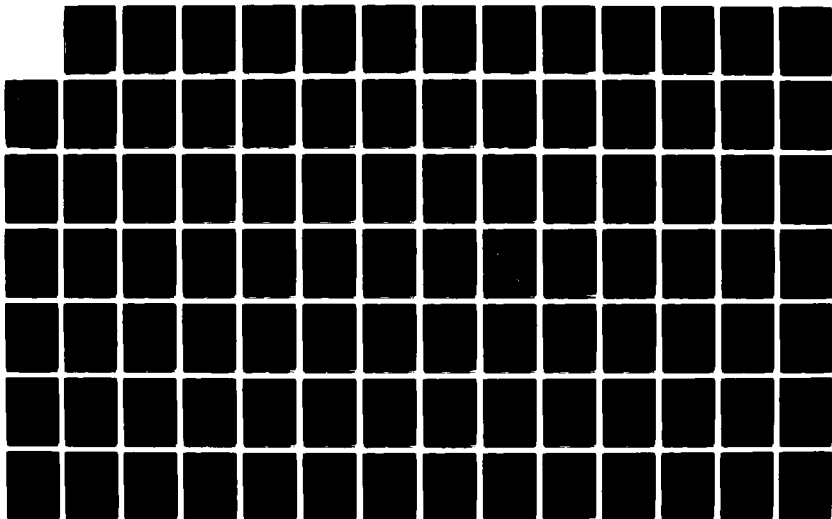
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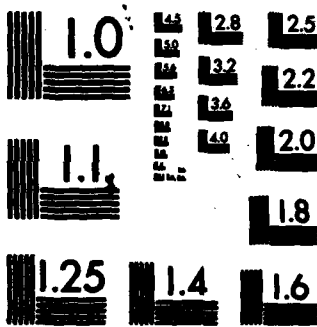
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#### 4.4. Copper-Nickel Alloy System

The copper-nickel alloy system forms a continuous series of solid solutions and is free of all transformations except that of ferromagnetism. As shown in Figure 2, the electrical resistivity versus temperature curves for Ni + Cu alloys change slope abruptly at the Curie temperature of the alloys. The Curie temperature decreases as the concentration of copper in the alloys increases. The ferromagnetism disappears and the Curie temperature drops to zero as the concentration of copper reaches 61.88% (60 At.%).

Mott [3] has given an explanation of the ferromagnetic behavior of these alloys based on the filling of holes in the d band of nickel by the s electrons of copper. The d-shell in a copper atom is completely occupied and there is a single s electron outside, whereas the 3d<sup>7</sup> band of a nickel atom is full but there are 0.54 holes in the 3d<sup>7</sup> band; these d-band holes are the elementary magnets in nickel. The Curie temperature is proportional to the number of elementary magnets per unit volume, which in nickel is thus 0.54 times the number of atoms per unit volume. The density of states in the d band of nickel atom at the Fermi surface is approximately ten times greater than the density of states in the s band, so that as copper is added to nickel about 90 percent of the extra s electrons go to fill up the d band, and thus decrease the number of elementary magnets per unit volume, until at 60 At.% Cu the d band of nickel is full, at which point the ferromagnetism disappears and the Curie temperature drops to 0 K. The insert in Figure 2 shows the Curie temperature as a function of percent copper in nickel, which is linear for the atomic percent of copper. This straight-line relationship was determined from the electrical resistivity data shown in Figure 2. The behavior of the electrical resistivity of these alloys has a direct bearing on the behavior of the thermal conductivity (see Figure 18), and therefore the knowledge of the former is prerequisite to the understanding of the latter.

There are 153 sets of experimental data available for the thermal conductivity of this alloy system. However, of the 104 data sets available for Cu + Ni alloys listed in Table 12 and shown in Figure 19, 27 sets are merely single data points and 25 sets cover only a narrow temperature range from around room temperature to about 500 K. Of the 49 data sets for Ni + Cu alloys listed in Table 13 and shown in Figure 20, 23 sets are single data points. Furthermore, many sets of data show large discrepancies.

For the Cu + Ni alloys, the most reliable measurements at room temperature were made by Smith and Palmer [49] (Cu + Ni curves 1-7), surprisingly in 1935, for a set of well-annealed alloys. Electrical resistivity data were also reported for the same specimens used for the thermal conductivity measurements. These provided the basis for the easy separation of the lattice component from the measured thermal conductivity.

Hulm [69] measured the thermal conductivity of an alloy with 20% Ni below 25 K (Cu + Ni curve 15). Berman [70] measured thermal conductivity of a sample of Constantan

(40% Ni) below 100 K (Cu + Ni curve 21). Wilkinson and Wilks [71] measured the thermal conductivity of an alloy with 30% Ni below 20 K (Cu + Ni curve 14). These three sets of low-temperature data appear to be reliable and consistent in view of the cold-work condition of the 30% Ni specimen of Wilkinson and Wilks (curve 14).

In the temperature range below 70 K, Erdmann and Jahoda have measured the thermal conductivity of the Cu-Ni alloy system several times [72-74] (Cu + Ni curves 52-55, 62-66, 68, and 84; Ni + Cu curves 13-19 and 21-23). One set of their measurements [74] (Cu + Ni curves 52-55 and Ni + Cu curves 13-19) is the only one that covers a wide range of composition at low temperature. However, it was very difficult to evaluate the reliability of their results. For copper-rich alloys, the lattice thermal conductivities derived from their measured total thermal conductivities are about 40% higher than those derived from other authors' results. Since their samples seemed to be the best annealed (at 930 C) among the alloy samples, it had been thought that the lattice thermal conductivities of their samples might be higher than those of the others because annealing could eliminate dislocations. However, after the effect of annealing on the electrical resistivity and lattice thermal conductivity of binary alloys had been reviewed carefully, it was concluded that the differences are too large to be accounted for by annealing. Furthermore, around liquid helium temperature, the difference between the lattice thermal conductivities of their own dilute and concentrated alloys are too large compared with those of other measurements. If their measured total thermal conductivities are connected to the total thermal conductivities above 300 K measured by other authors, the slopes of the conductivity-temperature curves become negative between 100 and 300 K for concentrated alloys. This seems unlikely as it does not occur in the conductivity-temperature curves of the analogous silver-palladium alloys. Recent private communication from Klemens [76] provided useful thermal conductivity data for a copper alloy with 4 At.% Ni at temperatures below 40 K (Cu + Ni curve 103). The sample was annealed at 1075 C for 72 hours and slowly cooled. The results also indicate that the lattice thermal conductivities of Erdmann and Jahoda are too high. Consequently, the results of Erdmann and Jahoda were not used in the present data synthesis.

For Ni + Cu alloys, Sager [77] (Ni + Cu curves 1 and 2), Smith [45] (Ni + Cu curves 3-6), and Sedström [63] (Ni + Cu curves 7 and 8) have measured the thermal conductivity around room temperature. There is some doubt about the reported compositions of their specimens as the electrical resistivity data reported for the same specimens differ from those obtained by other authors for alloys with the same nominal compositions.

Greig and Harrison [78] measured the thermal conductivities of nickel alloys with 0.32, 0.6, 1.5, and 4.2 At.% Cu below 100 K (Ni + Cu curves 9-12). More recently Farrell and Greig [79] studied the electrical resistivity and thermal conductivity of a nickel alloy with 0.31 At.% Cu below 100 K (Ni + Cu curve 34). They concluded that the lattice thermal conductivity of pure nickel is quite high and close to those of dilute copper alloys.

Chari [80] has suggested a method to separate the lattice thermal conductivity from total thermal conductivity of pure nickel and dilute nickel-rhenium alloys above 400 K. There is, however, doubt concerning his method of graphical separation of electrical resistivity into the intrinsic and magnetic components, because the anomaly of the temperature dependence of the electrical resistivity of the ferromagnetic metals can be explained by the ferromagnetic ordering of metals below the Curie point. Many authors have tried to express the resistivities of the ferromagnetic alloys in the form of  $\rho = \rho^* (1 + \mu)$ , where  $\mu$ , the ferromagnetic ordering parameter, is negative and vanishes above the Curie point [167], and  $\rho^*$  represents the resistivity of ferromagnetic metal in the absence of ferromagnetic ordering. In other words,  $\rho^*$  represents the resistivity of the "normal" non-ferromagnetic metal. Farrell and Greig [81] indicated that deviations from Matthiessen's rule due to spin mixing must be taken into account when analyzing the electronic transport properties of nickel alloys.

In the present data synthesis, the electronic thermal conductivities of the alloys for which both thermal conductivity and electrical resistivity were reported were calculated from eq. (12) in order to separate the lattice component from the measured total thermal conductivity. The resulting "experimental" lattice thermal conductivity data were then used for the adjustment of the lattice thermal conductivities of the virtual crystals so that the  $k_g$  values calculated from eq. (35) at moderate and high temperatures are in agreement with the experimental data. At low temperatures the lattice thermal conductivity values were obtained from the experimental data similarly as the difference of the measured  $k$  and the calculated  $k_e$ . The recommended total thermal conductivity values at low temperatures are in agreement with the data of Greig and Harrison [78] (Ni + Cu curves 9-12), Zimmerman [130] (Cu + Ni curves 17 and 20), Berman [70] (Cu + Ni curve 21), and Bouley, et al. [76] (Ni + Cu curve 104) to within 12%, and those at higher temperatures are in agreement with the data of Smith and Palmer [49] (Cu + Ni curves 1-7 and 85-90), Mikryukov [136] (Cu + Ni curve 44), Mikryukov [144] (Cu + Ni curves 71-73), Willett [146] (Cu + Ni curves 98-102), and Smith [45] (Ni + Cu curves 3-6) to within 10%.

The resulting recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 11 for 25 alloy compositions covering the temperatures from 4 to 1200 K. These values are for well-annealed alloys. The values for  $k$  are also shown in Figures 17 and 18. The values of residual electrical resistivity for the alloys are also given in Table 11. The uncertainties of the thermal conductivity values are stated in a footnote to Table 11, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 99.50% (99.46 At.%) Ni: 0.50% (0.54 At.%)				Cu: 97.00% (96.76 At.%) Ni: 3.00% (3.24 At.%)				Cu: 95.00% (94.61 At.%) Ni: 5.00% (5.39 At.%)			
$\rho_0 = 0.030 \mu\Omega \text{ cm}$				$\rho_0 = 1.25 \mu\Omega \text{ cm}$				$\rho_0 = 3.70 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.170*	0.138	0.0135 <sup>†</sup>	4	0.0347	0.0254	0.0030	4	0.0215	0.0160	0.00550
6	0.231*	0.236	0.0435 <sup>†</sup>	6	0.130	0.117	0.0335 <sup>†</sup>	6	0.0391	0.0240	0.0151
8	0.300*	0.315	0.0645 <sup>†</sup>	8	0.218	0.156	0.0635 <sup>†</sup>	8	0.0616	0.0380	0.0395
10	0.353*	0.354	0.131 <sup>†</sup>	10	0.295	0.195	0.100 <sup>†</sup>	10	0.132	0.0650	0.0490
15	0.505*	0.391	0.285 <sup>†</sup>	15	0.496	0.293	0.203 <sup>†</sup>	15	0.234	0.0990	0.104
20	1.14*	0.798	0.355 <sup>†</sup>	20	0.664	0.391	0.293 <sup>†</sup>	20	0.340	0.132	0.179
25	1.39*	0.945	0.439 <sup>†</sup>	25	0.940	0.482	0.358 <sup>†</sup>	25	0.428	0.164	0.264
30	1.89*	1.11	0.489 <sup>†</sup>	30	0.978	0.573	0.403 <sup>†</sup>	30	0.498	0.196	0.302
40	1.93*	1.39	0.539 <sup>†</sup>	40	1.20	0.743	0.460 <sup>†</sup>	40	0.599	0.258	0.341
50	2.14*	1.60	0.545 <sup>†</sup>	50	1.36	0.889	0.470 <sup>†</sup>	50	0.666	0.315	0.351
60	2.26*	1.73	0.539 <sup>†</sup>	60	1.46	1.00	0.465 <sup>†</sup>	60	0.715	0.366	0.349
70	2.37*	1.82	0.565 <sup>†</sup>	70	1.54	1.10	0.445 <sup>†</sup>	70	0.756	0.414	0.341
80	2.36*	1.89	0.485	80	1.61	1.19	0.420	80	0.790	0.459	0.331
90	2.39*	1.98	0.439	90	1.66*	1.27	0.395	90	0.823*	0.504	0.319
100	2.43*	2.03	0.400	100	1.72*	1.35	0.370	100	0.854*	0.548	0.306
150	2.64*	2.38	0.293	150	1.96*	1.70	0.281	150	1.01*	0.789	0.248
200	2.87*	2.68	0.234	200	2.20*	1.97	0.227	200	1.19*	0.947	0.204
250	2.93*	2.74	0.194	250	2.36*	2.17	0.189	250	1.29*	1.11	0.172
273	2.97	2.79	0.179	273	2.41*	2.24	0.175	273	1.34*	1.18	0.161
300	3.04	2.87	0.164	300	2.49	2.32	0.161	300	1.41	1.26	0.149
350	3.10	2.94	0.143	350	2.58	2.45	0.140	350	1.51	1.38	0.131
400	3.16	3.04	0.126	400	2.68	2.56	0.124	400	1.61	1.49	0.116
500	3.24*	3.13	0.102	500	2.80	2.70	0.100	500	1.77*	1.67	0.0953
600	3.26*	3.18	0.0853	600	2.90	2.81	0.0843	600	1.90*	1.82	0.0807
700	3.29*	3.21	0.0734	700	2.96	2.89	0.0727	700	2.01*	1.94	0.0699
800	3.27*	3.21	0.0644	800	2.98	2.92	0.0638	800	2.09*	2.02	0.0617
900	3.26*	3.21	0.0674	900	2.98	2.92	0.0569	900	2.14*	2.09	0.0552
1000	3.23*	3.17	0.0517	1000	2.96	2.91	0.0513	1000	2.18*	2.13	0.0499
1100	3.20*	3.15	0.0471	1100	2.96*	2.91	0.0468	1100	2.22*	2.17	0.0455
1200	3.16*	3.12	0.0432	1200	2.94*	2.89	0.0429	1200	2.23*	2.19	0.0419

\* Uncertainties of the total thermal conductivity,  $k$ , are as follows:99.50 Cu - 0.50 Ni:  $\pm 10\%$  below 200 K and  $\pm 5\%$  above 200 K.97.00 Cu - 3.00 Ni:  $\pm 10\%$  below 200 K and  $\pm 5\%$  above 200 K.95.00 Cu - 5.00 Ni:  $\pm 5\%$ .

† Provisional values.

‡ Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued)<sup>†</sup>

[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 90.00% (89.27 At.%) Ni: 10.00% (10.73 At.%)					Cu: 80.00% (78.71 At.%) Ni: 20.00% (21.29 At.%)					Cu: 75.00% (73.49 At.%) Ni: 25.00% (26.51 At.%)				
$\rho_0 = 12.16 \mu\Omega\text{-cm}$					$\rho_0 = 17.95 \mu\Omega\text{-cm}$					$\rho_0 = 23.70 \mu\Omega\text{-cm}$				
T	k	k <sub>e</sub>	k <sub>g</sub>	T	T	k	k <sub>e</sub>	k <sub>g</sub>	T	T	k	k <sub>e</sub>	k <sub>g</sub>	T
4	0.0112	0.00004	0.00315	4	0.00800 <sup>±2</sup>	0.00544	0.00335 <sup>±</sup>	4	0.00762 <sup>±</sup>	0.00412	0.00350 <sup>±</sup>	4	0.00724 <sup>±</sup>	0.00300 <sup>±</sup>
6	0.0216	0.0131	0.00090	6	0.0170 <sup>±2</sup>	0.00817	0.00890 <sup>±</sup>	6	0.0153 <sup>±</sup>	0.00619	0.00910 <sup>±</sup>	6	0.0143 <sup>±2</sup>	0.00090 <sup>±</sup>
8	0.0300	0.0161	0.0107	8	0.0240 <sup>±2</sup>	0.0109	0.0175 <sup>±</sup>	8	0.0253 <sup>±</sup>	0.00825	0.0170 <sup>±</sup>	8	0.0234 <sup>±2</sup>	0.00067
10	0.0360	0.0091	0.0535	10	0.0420 <sup>±2</sup>	0.0136	0.0290 <sup>±</sup>	10	0.0373 <sup>±</sup>	0.0103	0.0270 <sup>±</sup>	10	0.0345 <sup>±2</sup>	0.00034
15	0.105	0.0002	0.0700	15	0.0630 <sup>±2</sup>	0.0204	0.0635 <sup>±</sup>	15	0.0725 <sup>±</sup>	0.0155	0.0570 <sup>±</sup>	15	0.0660 <sup>±2</sup>	0.0135
20	0.104	0.0402	0.124	20	0.128 <sup>±2</sup>	0.0272	0.101 <sup>±</sup>	20	0.111 <sup>±</sup>	0.0206	0.0900 <sup>±</sup>	20	0.100 <sup>±2</sup>	0.0167
25	0.215	0.0002	0.165	25	0.169 <sup>±2</sup>	0.0339	0.138 <sup>±</sup>	25	0.144 <sup>±</sup>	0.0297	0.118 <sup>±</sup>	25	0.139 <sup>±2</sup>	0.0009
30	0.205	0.0001	0.196	30	0.202 <sup>±2</sup>	0.0407	0.161 <sup>±</sup>	30	0.172 <sup>±</sup>	0.0369	0.141 <sup>±</sup>	30	0.165 <sup>±2</sup>	0.157 <sup>±</sup>
40	0.316	0.0759	0.236	40	0.253 <sup>±2</sup>	0.0541	0.198 <sup>±</sup>	40	0.215 <sup>±</sup>	0.0411	0.174 <sup>±</sup>	40	0.198 <sup>±2</sup>	0.155 <sup>±</sup>
50	0.305	0.0006	0.265	50	0.284 <sup>±2</sup>	0.0673	0.217 <sup>±</sup>	50	0.245 <sup>±</sup>	0.0512	0.195 <sup>±</sup>	50	0.212 <sup>±2</sup>	0.170 <sup>±</sup>
60	0.270	0.118	0.260	60	0.295 <sup>±2</sup>	0.0802	0.225 <sup>±</sup>	60	0.261 <sup>±</sup>	0.0611	0.200 <sup>±</sup>	60	0.230 <sup>±2</sup>	0.180 <sup>±</sup>
70	0.306	0.137	0.256	70	0.317 <sup>±2</sup>	0.0931	0.234 <sup>±</sup>	70	0.273 <sup>±</sup>	0.0711	0.202 <sup>±</sup>	70	0.241 <sup>±2</sup>	0.183 <sup>±</sup>
80	0.407	0.195	0.262	80	0.327	0.106	0.221	80	0.281 <sup>±</sup>	0.0808	0.200 <sup>±</sup>	80	0.245 <sup>±2</sup>	0.180 <sup>±</sup>
90	0.419 <sup>*</sup>	0.174	0.263	90	0.335 <sup>±</sup>	0.118	0.215	90	0.285 <sup>±</sup>	0.0904	0.196	90	0.253 <sup>±</sup>	0.179
100	0.433 <sup>*</sup>	0.190	0.263	100	0.339 <sup>±</sup>	0.130	0.200	100	0.290 <sup>±</sup>	0.0904	0.191	100	0.267 <sup>±</sup>	0.176
150	0.465 <sup>*</sup>	0.275	0.193	150	0.363 <sup>±</sup>	0.189	0.174	150	0.306 <sup>±</sup>	0.144	0.162	150	0.290 <sup>±</sup>	0.153
200	0.510 <sup>*</sup>	0.323	0.163	200	0.372 <sup>±</sup>	0.244	0.148	200	0.324 <sup>±</sup>	0.167	0.138	200	0.293 <sup>±</sup>	0.151
250	0.500 <sup>*</sup>	0.423	0.141	250	0.437 <sup>±</sup>	0.299	0.126	250	0.349 <sup>±</sup>	0.226	0.120	250	0.300 <sup>±</sup>	0.134
273	0.502	0.466	0.138	273	0.444 <sup>±</sup>	0.333	0.121	273	0.361	0.247	0.113	273	0.300 <sup>±</sup>	0.108
300	0.621	0.493	0.124	300	0.464	0.380	0.113	300	0.375	0.269	0.106	300	0.300 <sup>±</sup>	0.101
350	0.670	0.505	0.119	350	0.502	0.490	0.102	350	0.403	0.268	0.097	350	0.341 <sup>±</sup>	0.0913
400	0.757	0.627	0.096	400	0.540	0.446	0.0922	400	0.432	0.345	0.0870	400	0.394 <sup>±</sup>	0.0832
500	0.821	0.747	0.0633	500	0.615 <sup>±</sup>	0.537	0.0778	500	0.491	0.417	0.0730	500	0.415 <sup>±</sup>	0.0706
600	0.839	0.809	0.0716	600	0.684 <sup>±</sup>	0.617	0.0673	600	0.548	0.483	0.0641	600	0.462 <sup>±</sup>	0.0617
700	1.01	0.940	0.0696	700	0.759 <sup>±</sup>	0.694	0.0594	700	0.601	0.544	0.0588	700	0.511 <sup>±</sup>	0.0648
800	1.07	1.00	0.0600	800	0.830 <sup>±</sup>	0.767	0.0531	800	0.654	0.603	0.0500	800	0.597 <sup>±</sup>	0.0608
900	1.10	1.11	0.0606	900	0.979 <sup>±</sup>	0.830	0.0481	900	0.706	0.662	0.0463	900	0.661 <sup>±</sup>	0.0606
1000	1.22	1.15	0.0400	1000	0.937 <sup>±</sup>	0.894	0.0438	1000	0.756	0.714	0.0433	1000	0.642 <sup>±</sup>	0.0613
1200	1.20 <sup>*</sup>	1.21	0.0432	1200	0.958 <sup>±</sup>	0.948	0.0404	1200	0.804 <sup>±</sup>	0.765	0.0390	1200	0.683 <sup>±</sup>	0.0670
1300	1.33 <sup>*</sup>	1.29	0.0390	1300	1.04 <sup>±</sup>	1.00	0.0373	1300	0.851 <sup>±</sup>	0.814	0.0362	1300	0.723 <sup>±</sup>	0.0382

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

- 90.00 Cu - 10.00 Ni: ± 5%.
- 85.00 Cu - 15.00 Ni: ± 10% below 80 K, and ± 5% above 200 K.
- 80.00 Cu - 20.00 Ni: ± 10% below 80 K, and ± 5% above 200 K.
- 75.00 Cu - 25.00 Ni: ± 10% below 80 K, and ± 5% above 200 K.

\* Provisional values.

• In temperature range where no experimental thermal conductivity data are available.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 70.00% (62.31 At.%) Ni: 30.00% (31.69 At.%)				Cu: 60.00% (58.09 At.%) Ni: 40.00% (41.91 At.%)				Cu: 55.00% (53.04 At.%) Ni: 45.00% (46.96 At.%)			
$\rho_0 = 34.50 \mu\Omega$ cm				$\rho_0 = 40.05 \mu\Omega$ cm				$\rho_0 = 45.00 \mu\Omega$ cm			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.00730 <sup>‡</sup>	0.00300	0.00430 <sup>‡</sup>	4	0.00797 <sup>‡</sup>	0.00217	0.00580 <sup>‡</sup>	4	0.00900 <sup>‡</sup>	0.00210	0.00690 <sup>‡</sup>
6	0.0143 <sup>‡</sup>	0.00430	0.0100 <sup>‡</sup>	6	0.0152 <sup>‡</sup>	0.00326	0.0119 <sup>‡</sup>	6	0.0160 <sup>‡</sup>	0.00315	0.0129 <sup>‡</sup>
8	0.0231 <sup>‡</sup>	0.00500	0.0181 <sup>‡</sup>	8	0.0233 <sup>‡</sup>	0.00434	0.0190 <sup>‡</sup>	8	0.0250 <sup>‡</sup>	0.00419	0.0208 <sup>‡</sup>
10	0.0330 <sup>‡</sup>	0.00700	0.0260 <sup>‡</sup>	10	0.0334 <sup>‡</sup>	0.00543	0.0280 <sup>‡</sup>	10	0.0347 <sup>‡</sup>	0.00524	0.0295 <sup>‡</sup>
15	0.0500 <sup>‡</sup>	0.0105	0.0395 <sup>‡</sup>	15	0.0505 <sup>‡</sup>	0.00814	0.0424 <sup>‡</sup>	15	0.0509 <sup>‡</sup>	0.00786	0.0431 <sup>‡</sup>
20	0.0630 <sup>‡</sup>	0.0140	0.0490 <sup>‡</sup>	20	0.0639 <sup>‡</sup>	0.0109	0.0530 <sup>‡</sup>	20	0.0630 <sup>‡</sup>	0.0105	0.0535 <sup>‡</sup>
25	0.115 <sup>‡</sup>	0.0175	0.100 <sup>‡</sup>	25	0.104 <sup>‡</sup>	0.0137	0.0900 <sup>‡</sup>	25	0.101 <sup>‡</sup>	0.0130 <sup>‡</sup>	0.0885 <sup>‡</sup>
30	0.130 <sup>‡</sup>	0.0210	0.110 <sup>‡</sup>	30	0.121 <sup>‡</sup>	0.0164	0.105 <sup>‡</sup>	30	0.118 <sup>‡</sup>	0.0155 <sup>‡</sup>	0.103 <sup>‡</sup>
40	0.170 <sup>‡</sup>	0.0280	0.142 <sup>‡</sup>	40	0.147 <sup>‡</sup>	0.0219	0.125 <sup>‡</sup>	40	0.142 <sup>‡</sup>	0.0200 <sup>‡</sup>	0.121 <sup>‡</sup>
50	0.185 <sup>‡</sup>	0.0300	0.155 <sup>‡</sup>	50	0.164 <sup>‡</sup>	0.0274	0.137 <sup>‡</sup>	50	0.159 <sup>‡</sup>	0.0237 <sup>‡</sup>	0.133 <sup>‡</sup>
60	0.207 <sup>‡</sup>	0.0416	0.166 <sup>‡</sup>	60	0.178 <sup>‡</sup>	0.0339	0.145 <sup>‡</sup>	60	0.170 <sup>‡</sup>	0.0300 <sup>‡</sup>	0.138 <sup>‡</sup>
70	0.217 <sup>‡</sup>	0.0485	0.169 <sup>‡</sup>	70	0.185 <sup>‡</sup>	0.0383	0.147 <sup>‡</sup>	70	0.178 <sup>‡</sup>	0.0330 <sup>‡</sup>	0.142 <sup>‡</sup>
80	0.235 <sup>‡</sup>	0.0504	0.185 <sup>‡</sup>	80	0.192 <sup>‡</sup>	0.0437	0.148 <sup>‡</sup>	80	0.184 <sup>‡</sup>	0.0400	0.143
90	0.250 <sup>‡</sup>	0.0521	0.195 <sup>‡</sup>	90	0.196 <sup>‡</sup>	0.0491	0.147 <sup>‡</sup>	90	0.189	0.0430	0.143
100	0.257 <sup>‡</sup>	0.0570	0.200 <sup>‡</sup>	100	0.200 <sup>‡</sup>	0.0536	0.146	100	0.192	0.0482	0.142
150	0.260 <sup>‡</sup>	0.0601	0.144	150	0.212 <sup>‡</sup>	0.0786	0.133	150	0.204	0.0736	0.130
200	0.250 <sup>‡</sup>	0.120	0.125	200	0.231 <sup>‡</sup>	0.103	0.118	200	0.213	0.0906	0.116
250	0.260 <sup>‡</sup>	0.110	0.110	250	0.240 <sup>‡</sup>	0.107	0.104	250	0.232	0.110	0.103
273	0.270 <sup>‡</sup>	0.171	0.104	273	0.250 <sup>‡</sup>	0.151	0.101	273	0.237	0.130	0.0976
300	0.285	0.186	0.0977	300	0.260 <sup>‡</sup>	0.165	0.0950	300	0.244	0.151	0.0931
350	0.280	0.214	0.0801	350	0.270 <sup>‡</sup>	0.190	0.0858	350	0.246	0.163	0.0831
400	0.285	0.241	0.0604	400	0.293 <sup>‡</sup>	0.215	0.0783	400	0.261 <sup>‡</sup>	0.185	0.0780
500	0.300	0.264	0.0400	500	0.330 <sup>‡</sup>	0.263	0.0669	500	0.290 <sup>‡</sup>	0.230	0.0640
600	0.407	0.267	0.0300	600	0.380 <sup>‡</sup>	0.310	0.0585	600	0.347	0.280	0.0575
700	0.440	0.297	0.0202	700	0.400 <sup>‡</sup>	0.356	0.0521	700	0.364	0.333	0.0512
800	0.491	0.443	0.0400	800	0.440 <sup>‡</sup>	0.390	0.0470	800	0.419	0.373	0.0462
900	0.500	0.480	0.0407	900	0.480 <sup>‡</sup>	0.438	0.0428	900	0.453	0.411	0.0421
1000	0.500	0.500	0.0401	1000	0.510 <sup>‡</sup>	0.475	0.0393	1000	0.485	0.447	0.0387
1200	0.500	0.500	0.0371	1200	0.540 <sup>‡</sup>	0.512	0.0364	1200	0.517	0.481	0.0358
1500	0.500	0.500	0.0345	1500	0.561 <sup>‡</sup>	0.549	0.0339	1500	0.547	0.514	0.0304

<sup>†</sup> Derivations of the total thermal conductivity,  $k$ , are as follows:  
 70.00 Cu - 30.00 Ni:  $\pm 10\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 5\%$  above 200 K.  
 60.00 Cu - 40.00 Ni:  $\pm 10\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 5\%$  above 200 K.  
 55.00 Cu - 45.00 Ni:  $\pm 10\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 5\%$  above 200 K.  
 50.00 Cu - 50.00 Ni:  $\pm 10\%$  below 80 K,  $\pm 10\%$  between 70 and 200 K, and  $\pm 5\%$  above 200 K.  
<sup>‡</sup> Fractional values.  
<sup>§</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 50.00% (48.02 At. %) Ni: 50.00% (51.98 At. %)			Cu: 45.00% (43.05 At. %) Ni: 55.00% (56.95 At. %)			Cu: 40.00% (39.12 At. %) Ni: 60.00% (61.88 At. %)			Cu: 35.00% (32.22 At. %) Ni: 65.00% (67.78 At. %)		
$\rho_0 = 40.30 \mu\Omega \text{ cm}$			$\rho_0 = 35.85 \mu\Omega \text{ cm}$			$\rho_0 = 31.60 \mu\Omega \text{ cm}$			$\rho_0 = 27.65 \mu\Omega \text{ cm}$		
T	k	$k_g$	T	k	$k_g$	T	k	$k_g$	T	k	$k_g$
4	0.0297 <sup>‡</sup>	0.00843	4	0.0120 <sup>‡</sup>	0.00273	4	0.0131 <sup>‡</sup>	0.00309	4	0.0126	0.00883
6	0.0104 <sup>‡</sup>	0.00364	6	0.0243 <sup>‡</sup>	0.00409	6	0.0216 <sup>‡</sup>	0.00464	6	0.0238	0.00350
8	0.0074 <sup>‡</sup>	0.00485	8	0.0232 <sup>‡</sup>	0.00545	8	0.0307 <sup>‡</sup>	0.00619	8	0.0321	0.00707
10	0.0071 <sup>‡</sup>	0.00666	10	0.0385 <sup>‡</sup>	0.00682	10	0.0402 <sup>‡</sup>	0.00773	10	0.0418	0.00864
15	0.0080 <sup>‡</sup>	0.00800	15	0.0617 <sup>‡</sup>	0.0102	15	0.0631 <sup>‡</sup>	0.0116	15	0.0658	0.0133
20	0.0081 <sup>‡</sup>	0.0121	20	0.0642 <sup>‡</sup>	0.0137	20	0.0860 <sup>‡</sup>	0.0155	20	0.0882	0.0177
25	0.101 <sup>‡</sup>	0.00444	25	0.102 <sup>‡</sup>	0.0163 <sup>‡</sup>	25	0.105 <sup>‡</sup>	0.0188 <sup>‡</sup>	25	0.106 <sup>‡</sup>	0.0216 <sup>‡</sup>
30	0.137 <sup>‡</sup>	0.0171 <sup>‡</sup>	30	0.118 <sup>‡</sup>	0.0194 <sup>‡</sup>	30	0.121 <sup>‡</sup>	0.0224 <sup>‡</sup>	30	0.126 <sup>‡</sup>	0.0267 <sup>‡</sup>
40	0.129 <sup>‡</sup>	0.0223 <sup>‡</sup>	40	0.145 <sup>‡</sup>	0.0255 <sup>‡</sup>	40	0.147 <sup>‡</sup>	0.0294 <sup>‡</sup>	40	0.144 <sup>‡</sup>	0.0329 <sup>‡</sup>
50	0.185 <sup>‡</sup>	0.0075 <sup>‡</sup>	50	0.180 <sup>‡</sup>	0.0312 <sup>‡</sup>	50	0.180 <sup>‡</sup>	0.0361 <sup>‡</sup>	50	0.174 <sup>‡</sup>	0.0417 <sup>‡</sup>
60	0.187 <sup>‡</sup>	0.0354 <sup>‡</sup>	60	0.172 <sup>‡</sup>	0.0368 <sup>‡</sup>	60	0.180 <sup>‡</sup>	0.0423 <sup>‡</sup>	60	0.180 <sup>‡</sup>	0.0491 <sup>‡</sup>
70	0.175 <sup>‡</sup>	0.0373 <sup>‡</sup>	70	0.181 <sup>‡</sup>	0.0421 <sup>‡</sup>	70	0.180 <sup>‡</sup>	0.0487 <sup>‡</sup>	70	0.201 <sup>‡</sup>	0.0589 <sup>‡</sup>
80	0.182	0.0481 <sup>‡</sup>	80	0.183 <sup>‡</sup>	0.0460 <sup>‡</sup>	80	0.198	0.0545 <sup>‡</sup>	80	0.219 <sup>‡</sup>	0.0689 <sup>‡</sup>
90	0.187 <sup>‡</sup>	0.0408 <sup>‡</sup>	90	0.194 <sup>‡</sup>	0.0522 <sup>‡</sup>	90	0.204 <sup>‡</sup>	0.0600 <sup>‡</sup>	90	0.217 <sup>‡</sup>	0.0804 <sup>‡</sup>
100	0.190 <sup>‡</sup>	0.0507 <sup>‡</sup>	100	0.197 <sup>‡</sup>	0.0582 <sup>‡</sup>	100	0.206 <sup>‡</sup>	0.0645 <sup>‡</sup>	100	0.232 <sup>‡</sup>	0.0745 <sup>‡</sup>
150	0.202 <sup>‡</sup>	0.0720	150	0.209 <sup>‡</sup>	0.0775 <sup>‡</sup>	150	0.219 <sup>‡</sup>	0.0862 <sup>‡</sup>	150	0.239 <sup>‡</sup>	0.0985 <sup>‡</sup>
200	0.200 <sup>‡</sup>	0.0944	200	0.214 <sup>‡</sup>	0.0969	200	0.225 <sup>‡</sup>	0.109 <sup>‡</sup>	200	0.259 <sup>‡</sup>	0.117 <sup>‡</sup>
250	0.217 <sup>‡</sup>	0.116	250	0.219 <sup>‡</sup>	0.116	250	0.224 <sup>‡</sup>	0.121	250	0.259 <sup>‡</sup>	0.132 <sup>‡</sup>
275	0.251 <sup>‡</sup>	0.134	275	0.222 <sup>‡</sup>	0.125	275	0.228	0.130	275	0.257 <sup>‡</sup>	0.138
300	0.257	0.136	300	0.227 <sup>‡</sup>	0.136	300	0.232	0.140	300	0.260 <sup>‡</sup>	0.147
350	0.239	0.126	350	0.230 <sup>‡</sup>	0.156	350	0.243	0.160	350	0.269 <sup>‡</sup>	0.158
400	0.200 <sup>‡</sup>	0.178	400	0.232 <sup>‡</sup>	0.177	400	0.255	0.179	400	0.281 <sup>‡</sup>	0.165
500	0.207 <sup>‡</sup>	0.232	500	0.204 <sup>‡</sup>	0.220	500	0.284	0.219	500	0.289 <sup>‡</sup>	0.202
600	0.203 <sup>‡</sup>	0.285	600	0.319 <sup>‡</sup>	0.263	600	0.318	0.262	600	0.323 <sup>‡</sup>	0.265
700	0.261 <sup>‡</sup>	0.351	700	0.307 <sup>‡</sup>	0.307	700	0.358	0.306	700	0.360 <sup>‡</sup>	0.309
800	0.200 <sup>‡</sup>	0.390	800	0.302 <sup>‡</sup>	0.347	800	0.391	0.345	800	0.392 <sup>‡</sup>	0.359
900	0.400 <sup>‡</sup>	0.500	900	0.439 <sup>‡</sup>	0.385	900	0.439	0.383	900	0.439 <sup>‡</sup>	0.383
1000	0.400 <sup>‡</sup>	0.500	1000	0.439 <sup>‡</sup>	0.431	1000	0.458	0.420	1000	0.458 <sup>‡</sup>	0.420
1100	0.400 <sup>‡</sup>	0.456	1100	0.491 <sup>‡</sup>	0.456	1100	0.491 <sup>‡</sup>	0.456	1100	0.491 <sup>‡</sup>	0.456
1200	0.400 <sup>‡</sup>	0.402	1200	0.522 <sup>‡</sup>	0.499	1200	0.525 <sup>‡</sup>	0.493	1200	0.525 <sup>‡</sup>	0.493

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:50.00 Cu - 50.00 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 100 K,  $\pm 10\%$  between 100 and 200 K, and  $\pm 5\%$  above 200 K.45.00 Cu - 55.00 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 150 K, and  $\pm 10\%$  above 150 K.40.00 Cu - 60.00 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 200 K, and  $\pm 10\%$  above 200 K.35.00 Cu - 65.00 Ni:  $\pm 10\%$  below 20 K,  $\pm 20\%$  between 20 and 250 K, and  $\pm 10\%$  above 250 K.<sup>‡</sup> Provisional values.<sup>\*</sup> In temperature ranges where no experimental thermal conductivity data are available.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued) †  
 † Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>

Cu: 30.00% (28.37 At.%) Ni: 70.00% (71.63 At.%)					Cu: 20.00% (18.76 At.%) Ni: 80.00% (81.24 At.%)					Cu: 15.00% (14.02 At.%) Ni: 85.00% (85.98 At.%)				
$\rho_0 = 23.70 \mu\Omega \text{ cm}$					$\rho_0 = 19.80 \mu\Omega \text{ cm}$					$\rho_0 = 16.00 \mu\Omega \text{ cm}$				
T	k	$k_e$	$k_g$		T	k	$k_e$	$k_g$		T	k	$k_e$	$k_g$	
4	0.0142 <sup>+</sup>	0.00412	0.0103 <sup>+</sup>		4	0.0148 <sup>+</sup>	0.00494	0.00983 <sup>+</sup>		4	0.0153 <sup>+</sup>	0.00511	0.00923 <sup>+</sup>	
6	0.0237 <sup>+</sup>	0.00419	0.0173 <sup>+</sup>		6	0.0239 <sup>+</sup>	0.00740	0.0164 <sup>+</sup>		6	0.0244 <sup>+</sup>	0.00916	0.0152 <sup>+</sup>	
8	0.0339 <sup>+</sup>	0.00423	0.0251 <sup>+</sup>		8	0.0338 <sup>+</sup>	0.00887	0.0235 <sup>+</sup>		8	0.0339 <sup>+</sup>	0.0122	0.0217 <sup>+</sup>	
10	0.0439 <sup>+</sup>	0.0103	0.0330 <sup>+</sup>		10	0.0435 <sup>+</sup>	0.0123	0.0310 <sup>+</sup>		10	0.0435 <sup>+</sup>	0.0153	0.0285 <sup>+</sup>	
15	0.0670 <sup>+</sup>	0.0155	0.0515 <sup>+</sup>		15	0.0675 <sup>+</sup>	0.0185	0.0490 <sup>+</sup>		15	0.0689 <sup>+</sup>	0.0229	0.0460 <sup>+</sup>	
20	0.0900 <sup>+</sup>	0.0205	0.0695 <sup>+</sup>		20	0.0917 <sup>+</sup>	0.0247	0.0670 <sup>+</sup>		20	0.0935 <sup>+</sup>	0.0305	0.0639 <sup>+</sup>	
25	0.110 <sup>+</sup>	0.0254 <sup>+</sup>	0.0845 <sup>+</sup>		25	0.114 <sup>+</sup>	0.0303 <sup>+</sup>	0.0835 <sup>+</sup>		25	0.120 <sup>+</sup>	0.0375 <sup>+</sup>	0.0899 <sup>+</sup>	
30	0.129 <sup>+</sup>	0.0303 <sup>+</sup>	0.0990 <sup>+</sup>		30	0.135 <sup>+</sup>	0.0382 <sup>+</sup>	0.0985 <sup>+</sup>		30	0.144 <sup>+</sup>	0.0449 <sup>+</sup>	0.0973 <sup>+</sup>	
40	0.180 <sup>+</sup>	0.0409 <sup>+</sup>	0.139 <sup>+</sup>		40	0.189 <sup>+</sup>	0.0577 <sup>+</sup>	0.131 <sup>+</sup>		40	0.195 <sup>+</sup>	0.0599 <sup>+</sup>	0.125 <sup>+</sup>	
50	0.190 <sup>+</sup>	0.0492 <sup>+</sup>	0.131 <sup>+</sup>		50	0.190 <sup>+</sup>	0.0596 <sup>+</sup>	0.136 <sup>+</sup>		50	0.213 <sup>+</sup>	0.0725 <sup>+</sup>	0.129 <sup>+</sup>	
60	0.190 <sup>+</sup>	0.0492 <sup>+</sup>	0.140 <sup>+</sup>		60	0.216 <sup>+</sup>	0.0801 <sup>+</sup>	0.145 <sup>+</sup>		60	0.239 <sup>+</sup>	0.0855 <sup>+</sup>	0.139 <sup>+</sup>	
70	0.215 <sup>+</sup>	0.0605 <sup>+</sup>	0.145 <sup>+</sup>		70	0.230 <sup>+</sup>	0.0792 <sup>+</sup>	0.151 <sup>+</sup>		70	0.255 <sup>+</sup>	0.0777 <sup>+</sup>	0.157 <sup>+</sup>	
80	0.235 <sup>+</sup>	0.0744 <sup>+</sup>	0.146 <sup>+</sup>		80	0.243 <sup>+</sup>	0.0884 <sup>+</sup>	0.154 <sup>+</sup>		80	0.270 <sup>+</sup>	0.109 <sup>+</sup>	0.161 <sup>+</sup>	
90	0.235 <sup>+</sup>	0.0815 <sup>+</sup>	0.150 <sup>+</sup>		90	0.252 <sup>+</sup>	0.0972 <sup>+</sup>	0.159 <sup>+</sup>		90	0.294 <sup>+</sup>	0.130 <sup>+</sup>	0.164 <sup>+</sup>	
100	0.237 <sup>+</sup>	0.0877 <sup>+</sup>	0.149 <sup>+</sup>		100	0.255 <sup>+</sup>	0.104 <sup>+</sup>	0.154 <sup>+</sup>		100	0.293 <sup>+</sup>	0.133 <sup>+</sup>	0.164 <sup>+</sup>	
150	0.289 <sup>+</sup>	0.116 <sup>+</sup>	0.187 <sup>+</sup>		150	0.291 <sup>+</sup>	0.136 <sup>+</sup>	0.143 <sup>+</sup>		150	0.329 <sup>+</sup>	0.169 <sup>+</sup>	0.151 <sup>+</sup>	
200	0.289 <sup>+</sup>	0.134 <sup>+</sup>	0.123 <sup>+</sup>		200	0.297 <sup>+</sup>	0.161 <sup>+</sup>	0.126 <sup>+</sup>		200	0.330 <sup>+</sup>	0.196 <sup>+</sup>	0.133 <sup>+</sup>	
250	0.289 <sup>+</sup>	0.150 <sup>+</sup>	0.107 <sup>+</sup>		250	0.286 <sup>+</sup>	0.176 <sup>+</sup>	0.110 <sup>+</sup>		250	0.325 <sup>+</sup>	0.217 <sup>+</sup>	0.115 <sup>+</sup>	
273	0.297 <sup>+</sup>	0.164 <sup>+</sup>	0.101 <sup>+</sup>		273	0.285 <sup>+</sup>	0.181 <sup>+</sup>	0.104 <sup>+</sup>		273	0.321 <sup>+</sup>	0.223 <sup>+</sup>	0.106 <sup>+</sup>	
300	0.287 <sup>+</sup>	0.162 <sup>+</sup>	0.0949 <sup>+</sup>		300	0.285 <sup>+</sup>	0.177 <sup>+</sup>	0.0977 <sup>+</sup>		300	0.330 <sup>+</sup>	0.228 <sup>+</sup>	0.103 <sup>+</sup>	
350	0.261	0.175	0.0883 <sup>+</sup>		350	0.283 <sup>+</sup>	0.195 <sup>+</sup>	0.0890 <sup>+</sup>		350	0.325 <sup>+</sup>	0.234 <sup>+</sup>	0.0913 <sup>+</sup>	
400	0.273	0.154	0.0780 <sup>+</sup>		400	0.280 <sup>+</sup>	0.206	0.0800 <sup>+</sup>		400	0.320 <sup>+</sup>	0.237 <sup>+</sup>	0.0809 <sup>+</sup>	
500	0.284	0.222	0.0644 <sup>+</sup>		500	0.313 <sup>+</sup>	0.245	0.0675 <sup>+</sup>		500	0.333	0.263	0.0791 <sup>+</sup>	
600	0.281	0.273	0.0479 <sup>+</sup>		600	0.347 <sup>+</sup>	0.268	0.0591 <sup>+</sup>		600	0.367	0.306	0.0696 <sup>+</sup>	
700	0.280	0.294	0.0344 <sup>+</sup>		700	0.385 <sup>+</sup>	0.335	0.0524 <sup>+</sup>		700	0.411	0.357	0.0537 <sup>+</sup>	
800	0.404 <sup>+</sup>	0.267	0.0453 <sup>+</sup>		800	0.422 <sup>+</sup>	0.375	0.0471 <sup>+</sup>		800	0.445	0.387	0.0431 <sup>+</sup>	
900	0.439 <sup>+</sup>	0.266	0.0451 <sup>+</sup>		900	0.450 <sup>+</sup>	0.413	0.0437 <sup>+</sup>		900	0.478	0.435	0.0439 <sup>+</sup>	
1000	0.473 <sup>+</sup>	0.423	0.0383 <sup>+</sup>		1000	0.489 <sup>+</sup>	0.450	0.0391 <sup>+</sup>		1000	0.511 <sup>+</sup>	0.471	0.0399 <sup>+</sup>	
1100	0.509 <sup>+</sup>	0.476	0.0357 <sup>+</sup>		1100	0.521 <sup>+</sup>	0.485	0.0361 <sup>+</sup>		1100	0.545 <sup>+</sup>	0.508	0.0337 <sup>+</sup>	
1200	0.509 <sup>+</sup>	0.505	0.0331 <sup>+</sup>		1200	0.535 <sup>+</sup>	0.518	0.0335 <sup>+</sup>		1200	0.572 <sup>+</sup>	0.536	0.0311 <sup>+</sup>	

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 28.37 Cu - 70.63 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 300 K, and  $\pm 10\%$  above 300 K.
- 28.60 Cu - 71.40 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 350 K, and  $\pm 15\%$  above 350 K.
- 28.80 Cu - 71.20 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 400 K, and  $\pm 15\%$  above 400 K.
- 14.02 Cu - 85.98 Ni:  $\pm 15\%$  below 20 K,  $\pm 20\%$  between 20 and 400 K, and  $\pm 15\%$  above 400 K.

‡ Predicted values.

§ Typical values.

†† Uncertainties of the total thermal conductivity,  $k$ , are as follows:



TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 16.00% ( 9.31 At.%) Ni: 84.00% (90.69 At.%)				Cu: 3.00% ( 2.78 At.%) Ni: 97.00% (97.22 At.%)				Cu: 1.00% ( 0.92 At.%) Ni: 99.00% (99.08 At.%)			
$\rho_0 = 8.00 \mu\Omega$ cm				$\rho_0 = 2.40 \mu\Omega$ cm				$\rho_0 = 0.90 \mu\Omega$ cm			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0185 <sup>‡</sup>	0.0132	0.0053 <sup>‡</sup>	4	0.0481 <sup>‡</sup>	0.0407	0.0074 <sup>‡</sup>	4	0.123 <sup>‡</sup>	0.109	0.014 <sup>‡</sup>
6	0.0209 <sup>‡</sup>	0.0153	0.0056 <sup>‡</sup>	6	0.0741 <sup>‡</sup>	0.0611	0.0130 <sup>‡</sup>	6	0.186 <sup>‡</sup>	0.163	0.023 <sup>‡</sup>
8	0.0215 <sup>‡</sup>	0.0244	0.0171 <sup>‡</sup>	8	0.101 <sup>‡</sup>	0.0814	0.0192 <sup>‡</sup>	8	0.250 <sup>‡</sup>	0.217	0.033 <sup>‡</sup>
10	0.0209 <sup>‡</sup>	0.0209 <sup>‡</sup>	0.0083 <sup>‡</sup>	10	0.128 <sup>‡</sup>	0.102	0.0260 <sup>‡</sup>	10	0.314 <sup>‡</sup>	0.271	0.043 <sup>‡</sup>
15	0.0211 <sup>‡</sup>	0.0255	0.0083 <sup>‡</sup>	15	0.186 <sup>‡</sup>	0.153	0.0445 <sup>‡</sup>	15	0.477 <sup>‡</sup>	0.407	0.065 <sup>‡</sup>
20	0.115 <sup>‡</sup>	0.0411 <sup>‡</sup>	0.0676 <sup>‡</sup>	20	0.269 <sup>‡</sup>	0.204	0.0630 <sup>‡</sup>	20	0.638 <sup>‡</sup>	0.543	0.094 <sup>‡</sup>
25	0.126 <sup>‡</sup>	0.0710 <sup>‡</sup>	0.0710 <sup>‡</sup>	25	0.333 <sup>‡</sup>	0.242 <sup>‡</sup>	0.0979 <sup>‡</sup>	25	0.771 <sup>‡</sup>	0.649 <sup>‡</sup>	0.128 <sup>‡</sup>
30	0.126 <sup>‡</sup>	0.0904 <sup>‡</sup>	0.0904 <sup>‡</sup>	30	0.397 <sup>‡</sup>	0.287 <sup>‡</sup>	0.1149 <sup>‡</sup>	30	0.900 <sup>‡</sup>	0.742 <sup>‡</sup>	0.148 <sup>‡</sup>
40	0.146 <sup>‡</sup>	0.1175 <sup>‡</sup>	0.1175 <sup>‡</sup>	40	0.516 <sup>‡</sup>	0.363 <sup>‡</sup>	0.153 <sup>‡</sup>	40	1.07 <sup>‡</sup>	0.875 <sup>‡</sup>	0.195 <sup>‡</sup>
50	0.200 <sup>‡</sup>	0.143 <sup>‡</sup>	0.143 <sup>‡</sup>	50	0.613 <sup>‡</sup>	0.424 <sup>‡</sup>	0.189 <sup>‡</sup>	50	1.19 <sup>‡</sup>	0.932 <sup>‡</sup>	0.235 <sup>‡</sup>
60	0.321 <sup>‡</sup>	0.165 <sup>‡</sup>	0.165 <sup>‡</sup>	60	0.686 <sup>‡</sup>	0.473 <sup>‡</sup>	0.213 <sup>‡</sup>	60	1.21 <sup>‡</sup>	0.848 <sup>‡</sup>	0.265 <sup>‡</sup>
70	0.369 <sup>‡</sup>	0.176 <sup>‡</sup>	0.176 <sup>‡</sup>	70	0.734 <sup>‡</sup>	0.504 <sup>‡</sup>	0.230 <sup>‡</sup>	70	1.21 <sup>‡</sup>	0.824 <sup>‡</sup>	0.283 <sup>‡</sup>
80	0.369 <sup>‡</sup>	0.194 <sup>‡</sup>	0.194 <sup>‡</sup>	80	0.768 <sup>‡</sup>	0.524 <sup>‡</sup>	0.241 <sup>‡</sup>	80	1.18 <sup>‡</sup>	0.809 <sup>‡</sup>	0.293 <sup>‡</sup>
90	0.411 <sup>‡</sup>	0.213 <sup>‡</sup>	0.213 <sup>‡</sup>	90	0.784 <sup>‡</sup>	0.537 <sup>‡</sup>	0.247 <sup>‡</sup>	90	1.16 <sup>‡</sup>	0.806 <sup>‡</sup>	0.295 <sup>‡</sup>
100	0.439 <sup>‡</sup>	0.234 <sup>‡</sup>	0.234 <sup>‡</sup>	100	0.786 <sup>‡</sup>	0.536 <sup>‡</sup>	0.250 <sup>‡</sup>	100	1.11 <sup>‡</sup>	0.823 <sup>‡</sup>	0.296 <sup>‡</sup>
150	0.449 <sup>‡</sup>	0.297 <sup>‡</sup>	0.297 <sup>‡</sup>	150	0.779 <sup>‡</sup>	0.544 <sup>‡</sup>	0.225 <sup>‡</sup>	150	0.993 <sup>‡</sup>	0.741 <sup>‡</sup>	0.252 <sup>‡</sup>
200	0.474 <sup>‡</sup>	0.323 <sup>‡</sup>	0.323 <sup>‡</sup>	200	0.743 <sup>‡</sup>	0.537 <sup>‡</sup>	0.186 <sup>‡</sup>	200	0.900 <sup>‡</sup>	0.693 <sup>‡</sup>	0.202 <sup>‡</sup>
250	0.473 <sup>‡</sup>	0.343 <sup>‡</sup>	0.343 <sup>‡</sup>	250	0.717 <sup>‡</sup>	0.521 <sup>‡</sup>	0.156 <sup>‡</sup>	250	0.838 <sup>‡</sup>	0.670 <sup>‡</sup>	0.168 <sup>‡</sup>
273	0.483 <sup>‡</sup>	0.346 <sup>‡</sup>	0.346 <sup>‡</sup>	273	0.704 <sup>‡</sup>	0.509 <sup>‡</sup>	0.145 <sup>‡</sup>	273	0.819 <sup>‡</sup>	0.643 <sup>‡</sup>	0.155 <sup>‡</sup>
300	0.471 <sup>‡</sup>	0.380 <sup>‡</sup>	0.380 <sup>‡</sup>	300	0.692 <sup>‡</sup>	0.508 <sup>‡</sup>	0.134 <sup>‡</sup>	300	0.801 <sup>‡</sup>	0.638 <sup>‡</sup>	0.143 <sup>‡</sup>
350	0.484 <sup>‡</sup>	0.389 <sup>‡</sup>	0.389 <sup>‡</sup>	350	0.665 <sup>‡</sup>	0.547 <sup>‡</sup>	0.118 <sup>‡</sup>	350	0.764 <sup>‡</sup>	0.440 <sup>‡</sup>	0.124 <sup>‡</sup>
400	0.489 <sup>‡</sup>	0.399 <sup>‡</sup>	0.399 <sup>‡</sup>	400	0.639 <sup>‡</sup>	0.530 <sup>‡</sup>	0.105 <sup>‡</sup>	400	0.724 <sup>‡</sup>	0.615 <sup>‡</sup>	0.110 <sup>‡</sup>
500	0.459 <sup>‡</sup>	0.377 <sup>‡</sup>	0.377 <sup>‡</sup>	500	0.581 <sup>‡</sup>	0.495 <sup>‡</sup>	0.085 <sup>‡</sup>	500	0.653 <sup>‡</sup>	0.505 <sup>‡</sup>	0.080 <sup>‡</sup>
600	0.451 <sup>‡</sup>	0.371 <sup>‡</sup>	0.371 <sup>‡</sup>	600	0.527 <sup>‡</sup>	0.455 <sup>‡</sup>	0.0723 <sup>‡</sup>	600	0.599 <sup>‡</sup>	0.523 <sup>‡</sup>	0.0747 <sup>‡</sup>
700	0.449 <sup>‡</sup>	0.400 <sup>‡</sup>	0.400 <sup>‡</sup>	700	0.581 <sup>‡</sup>	0.518 <sup>‡</sup>	0.0626 <sup>‡</sup>	700	0.619 <sup>‡</sup>	0.553 <sup>‡</sup>	0.0643 <sup>‡</sup>
800	0.509 <sup>‡</sup>	0.489 <sup>‡</sup>	0.489 <sup>‡</sup>	800	0.611 <sup>‡</sup>	0.556 <sup>‡</sup>	0.0551 <sup>‡</sup>	800	0.643 <sup>‡</sup>	0.567 <sup>‡</sup>	0.0585 <sup>‡</sup>
900	0.509 <sup>‡</sup>	0.509 <sup>‡</sup>	0.509 <sup>‡</sup>	900	0.638 <sup>‡</sup>	0.598 <sup>‡</sup>	0.0493 <sup>‡</sup>	900	0.669 <sup>‡</sup>	0.618 <sup>‡</sup>	0.0503 <sup>‡</sup>
1000	0.519 <sup>‡</sup>	0.529 <sup>‡</sup>	0.529 <sup>‡</sup>	1000	0.662 <sup>‡</sup>	0.618 <sup>‡</sup>	0.0415 <sup>‡</sup>	1000	0.692 <sup>‡</sup>	0.648 <sup>‡</sup>	0.0454 <sup>‡</sup>
1100	0.609 <sup>‡</sup>	0.569 <sup>‡</sup>	0.569 <sup>‡</sup>	1100	0.687 <sup>‡</sup>	0.646 <sup>‡</sup>	0.0406 <sup>‡</sup>	1100	0.715 <sup>‡</sup>	0.673 <sup>‡</sup>	0.0413 <sup>‡</sup>
1200	0.609 <sup>‡</sup>	0.599 <sup>‡</sup>	0.599 <sup>‡</sup>	1200	0.710 <sup>‡</sup>	0.672 <sup>‡</sup>	0.0373 <sup>‡</sup>	1200	0.738 <sup>‡</sup>	0.698 <sup>‡</sup>	0.0379 <sup>‡</sup>

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 16.00 Cu - 84.00 Ni:  $\pm 20\%$  below 20 K,  $\pm 25\%$  between 20 and 500 K, and  $\pm 15\%$  above 500 K.
- 3.00 Cu - 97.00 Ni:  $\pm 20\%$  below 20 K,  $\pm 25\%$  between 20 and 500 K, and  $\pm 15\%$  above 500 K.
- 1.00 Cu - 99.00 Ni:  $\pm 20\%$  below 20 K,  $\pm 25\%$  between 20 and 500 K, and  $\pm 15\%$  above 500 K.

<sup>‡</sup> Provisional values.<sup>§</sup> Typical values.

Thermal conductivity data are available.

TABLE 11. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOY SYSTEM (continued)<sup>a</sup>  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>l</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 0.25% (0.45 At.%) Ni: 99.75% (99.55 At.%)		T, K		k, W cm <sup>-1</sup> K <sup>-1</sup>		k <sub>e</sub> , W cm <sup>-1</sup> K <sup>-1</sup>		k <sub>l</sub> , W cm <sup>-1</sup> K <sup>-1</sup>	
P <sub>0</sub> = 0.100 MPa		T, K		k, W cm <sup>-1</sup> K <sup>-1</sup>		k <sub>e</sub> , W cm <sup>-1</sup> K <sup>-1</sup>		k <sub>l</sub> , W cm <sup>-1</sup> K <sup>-1</sup>	
4	0.313 <sup>b</sup>	4	0.100	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>
6	0.321 <sup>b</sup>	6	0.093	0.077 <sup>b</sup>	0.077 <sup>b</sup>	0.077 <sup>b</sup>	0.077 <sup>b</sup>	0.077 <sup>b</sup>	0.077 <sup>b</sup>
8	0.329 <sup>b</sup>	8	0.351	0.030 <sup>b</sup>	0.030 <sup>b</sup>	0.030 <sup>b</sup>	0.030 <sup>b</sup>	0.030 <sup>b</sup>	0.030 <sup>b</sup>
10	0.337 <sup>b</sup>	10	0.400	0.010 <sup>b</sup>	0.010 <sup>b</sup>	0.010 <sup>b</sup>	0.010 <sup>b</sup>	0.010 <sup>b</sup>	0.010 <sup>b</sup>
15	0.353 <sup>b</sup>	15	0.725	0.000 <sup>b</sup>	0.000 <sup>b</sup>	0.000 <sup>b</sup>	0.000 <sup>b</sup>	0.000 <sup>b</sup>	0.000 <sup>b</sup>
20	1.00 <sup>b</sup>	20	0.977	0.110 <sup>b</sup>	0.110 <sup>b</sup>	0.110 <sup>b</sup>	0.110 <sup>b</sup>	0.110 <sup>b</sup>	0.110 <sup>b</sup>
25	1.35 <sup>b</sup>	25	1.170	0.140 <sup>b</sup>	0.140 <sup>b</sup>	0.140 <sup>b</sup>	0.140 <sup>b</sup>	0.140 <sup>b</sup>	0.140 <sup>b</sup>
30	1.60 <sup>b</sup>	30	1.30 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>	0.170 <sup>b</sup>
40	1.80 <sup>b</sup>	40	1.40 <sup>b</sup>	0.220 <sup>b</sup>	0.220 <sup>b</sup>	0.220 <sup>b</sup>	0.220 <sup>b</sup>	0.220 <sup>b</sup>	0.220 <sup>b</sup>
50	2.00 <sup>b</sup>	50	1.50 <sup>b</sup>	0.260 <sup>b</sup>	0.260 <sup>b</sup>	0.260 <sup>b</sup>	0.260 <sup>b</sup>	0.260 <sup>b</sup>	0.260 <sup>b</sup>
60	2.20 <sup>b</sup>	60	1.60 <sup>b</sup>	0.300 <sup>b</sup>	0.300 <sup>b</sup>	0.300 <sup>b</sup>	0.300 <sup>b</sup>	0.300 <sup>b</sup>	0.300 <sup>b</sup>
70	2.40 <sup>b</sup>	70	1.70 <sup>b</sup>	0.340 <sup>b</sup>	0.340 <sup>b</sup>	0.340 <sup>b</sup>	0.340 <sup>b</sup>	0.340 <sup>b</sup>	0.340 <sup>b</sup>
80	2.60 <sup>b</sup>	80	1.80 <sup>b</sup>	0.380 <sup>b</sup>	0.380 <sup>b</sup>	0.380 <sup>b</sup>	0.380 <sup>b</sup>	0.380 <sup>b</sup>	0.380 <sup>b</sup>
90	2.80 <sup>b</sup>	90	1.90 <sup>b</sup>	0.420 <sup>b</sup>	0.420 <sup>b</sup>	0.420 <sup>b</sup>	0.420 <sup>b</sup>	0.420 <sup>b</sup>	0.420 <sup>b</sup>
100	3.00 <sup>b</sup>	100	2.00 <sup>b</sup>	0.460 <sup>b</sup>	0.460 <sup>b</sup>	0.460 <sup>b</sup>	0.460 <sup>b</sup>	0.460 <sup>b</sup>	0.460 <sup>b</sup>
150	3.50 <sup>b</sup>	150	2.50 <sup>b</sup>	0.550 <sup>b</sup>	0.550 <sup>b</sup>	0.550 <sup>b</sup>	0.550 <sup>b</sup>	0.550 <sup>b</sup>	0.550 <sup>b</sup>
200	4.00 <sup>b</sup>	200	3.00 <sup>b</sup>	0.640 <sup>b</sup>	0.640 <sup>b</sup>	0.640 <sup>b</sup>	0.640 <sup>b</sup>	0.640 <sup>b</sup>	0.640 <sup>b</sup>
250	4.50 <sup>b</sup>	250	3.50 <sup>b</sup>	0.730 <sup>b</sup>	0.730 <sup>b</sup>	0.730 <sup>b</sup>	0.730 <sup>b</sup>	0.730 <sup>b</sup>	0.730 <sup>b</sup>
275	4.75 <sup>b</sup>	275	3.75 <sup>b</sup>	0.775 <sup>b</sup>	0.775 <sup>b</sup>	0.775 <sup>b</sup>	0.775 <sup>b</sup>	0.775 <sup>b</sup>	0.775 <sup>b</sup>
300	5.00 <sup>b</sup>	300	4.00 <sup>b</sup>	0.820 <sup>b</sup>	0.820 <sup>b</sup>	0.820 <sup>b</sup>	0.820 <sup>b</sup>	0.820 <sup>b</sup>	0.820 <sup>b</sup>
350	5.50 <sup>b</sup>	350	4.50 <sup>b</sup>	0.910 <sup>b</sup>	0.910 <sup>b</sup>	0.910 <sup>b</sup>	0.910 <sup>b</sup>	0.910 <sup>b</sup>	0.910 <sup>b</sup>
400	6.00 <sup>b</sup>	400	5.00 <sup>b</sup>	1.000 <sup>b</sup>	1.000 <sup>b</sup>	1.000 <sup>b</sup>	1.000 <sup>b</sup>	1.000 <sup>b</sup>	1.000 <sup>b</sup>
450	6.50 <sup>b</sup>	450	5.50 <sup>b</sup>	1.090 <sup>b</sup>	1.090 <sup>b</sup>	1.090 <sup>b</sup>	1.090 <sup>b</sup>	1.090 <sup>b</sup>	1.090 <sup>b</sup>
500	7.00 <sup>b</sup>	500	6.00 <sup>b</sup>	1.180 <sup>b</sup>	1.180 <sup>b</sup>	1.180 <sup>b</sup>	1.180 <sup>b</sup>	1.180 <sup>b</sup>	1.180 <sup>b</sup>
550	7.50 <sup>b</sup>	550	6.50 <sup>b</sup>	1.270 <sup>b</sup>	1.270 <sup>b</sup>	1.270 <sup>b</sup>	1.270 <sup>b</sup>	1.270 <sup>b</sup>	1.270 <sup>b</sup>
600	8.00 <sup>b</sup>	600	7.00 <sup>b</sup>	1.360 <sup>b</sup>	1.360 <sup>b</sup>	1.360 <sup>b</sup>	1.360 <sup>b</sup>	1.360 <sup>b</sup>	1.360 <sup>b</sup>
700	9.00 <sup>b</sup>	700	8.00 <sup>b</sup>	1.450 <sup>b</sup>	1.450 <sup>b</sup>	1.450 <sup>b</sup>	1.450 <sup>b</sup>	1.450 <sup>b</sup>	1.450 <sup>b</sup>
800	10.00 <sup>b</sup>	800	9.00 <sup>b</sup>	1.540 <sup>b</sup>	1.540 <sup>b</sup>	1.540 <sup>b</sup>	1.540 <sup>b</sup>	1.540 <sup>b</sup>	1.540 <sup>b</sup>
900	11.00 <sup>b</sup>	900	10.00 <sup>b</sup>	1.630 <sup>b</sup>	1.630 <sup>b</sup>	1.630 <sup>b</sup>	1.630 <sup>b</sup>	1.630 <sup>b</sup>	1.630 <sup>b</sup>
1000	12.00 <sup>b</sup>	1000	11.00 <sup>b</sup>	1.720 <sup>b</sup>	1.720 <sup>b</sup>	1.720 <sup>b</sup>	1.720 <sup>b</sup>	1.720 <sup>b</sup>	1.720 <sup>b</sup>
1200	14.00 <sup>b</sup>	1200	13.00 <sup>b</sup>	1.860 <sup>b</sup>	1.860 <sup>b</sup>	1.860 <sup>b</sup>	1.860 <sup>b</sup>	1.860 <sup>b</sup>	1.860 <sup>b</sup>

<sup>a</sup> Uncertainties of the total thermal conductivity, k, are as follows:  
 0.30 Cu - 0.70 Ni: ±20% below 20 K, ±25% between 20 and 600 K, and ±15% above 600 K.

<sup>b</sup> Interpolated values.

<sup>c</sup> Typical values.

<sup>d</sup> In temperature ranges where no experimental thermal conductivity data are available.

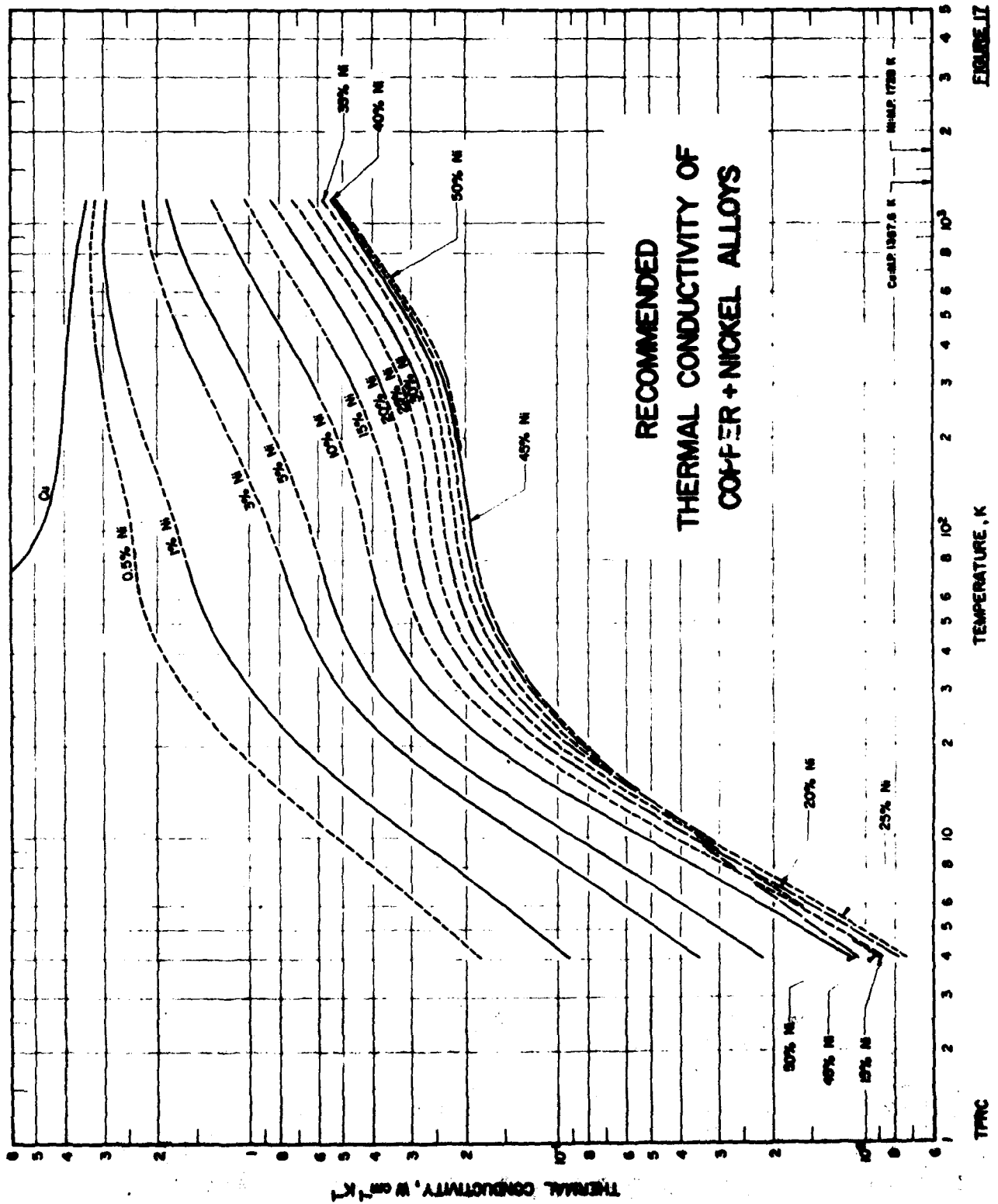
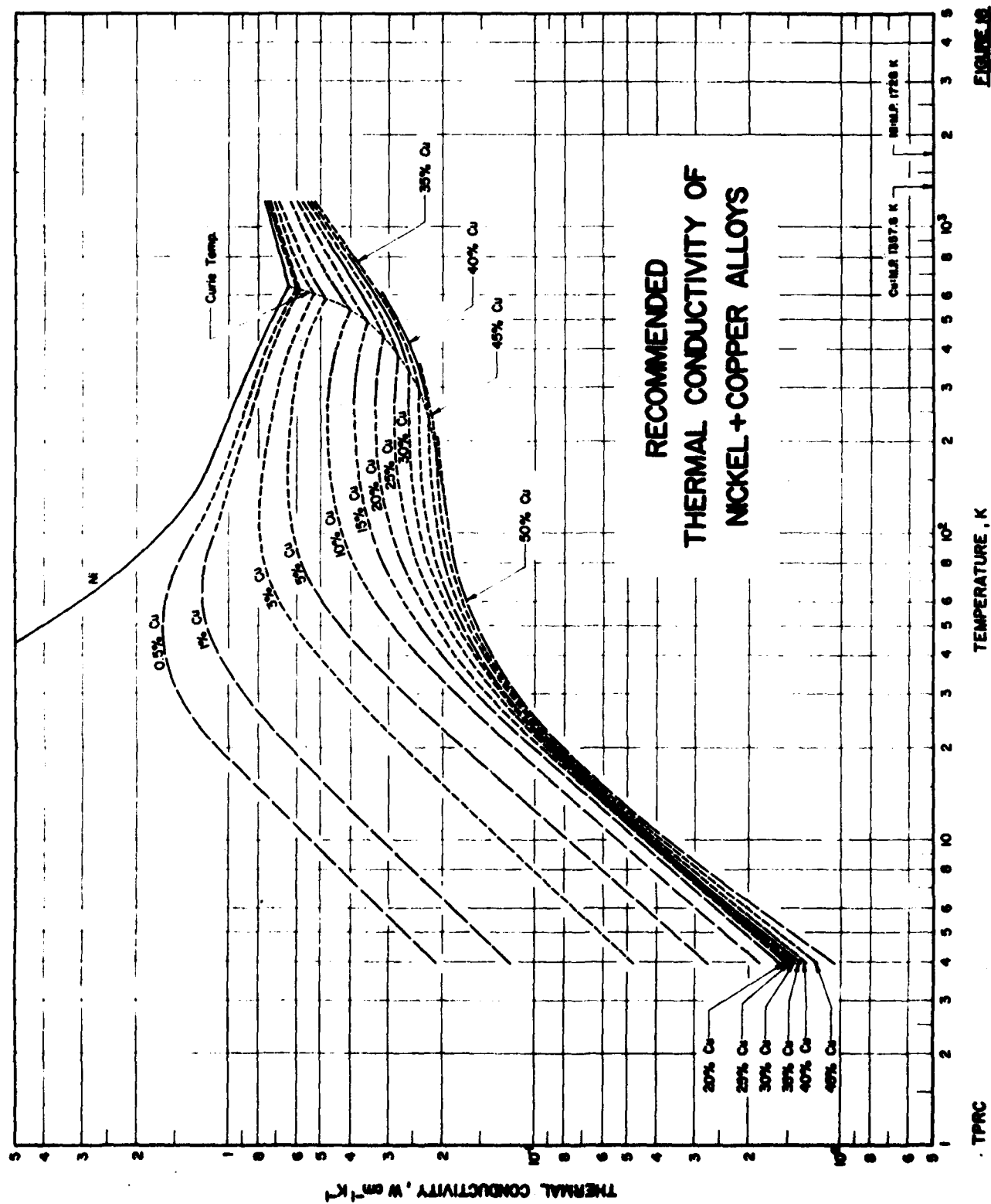


FIGURE 17



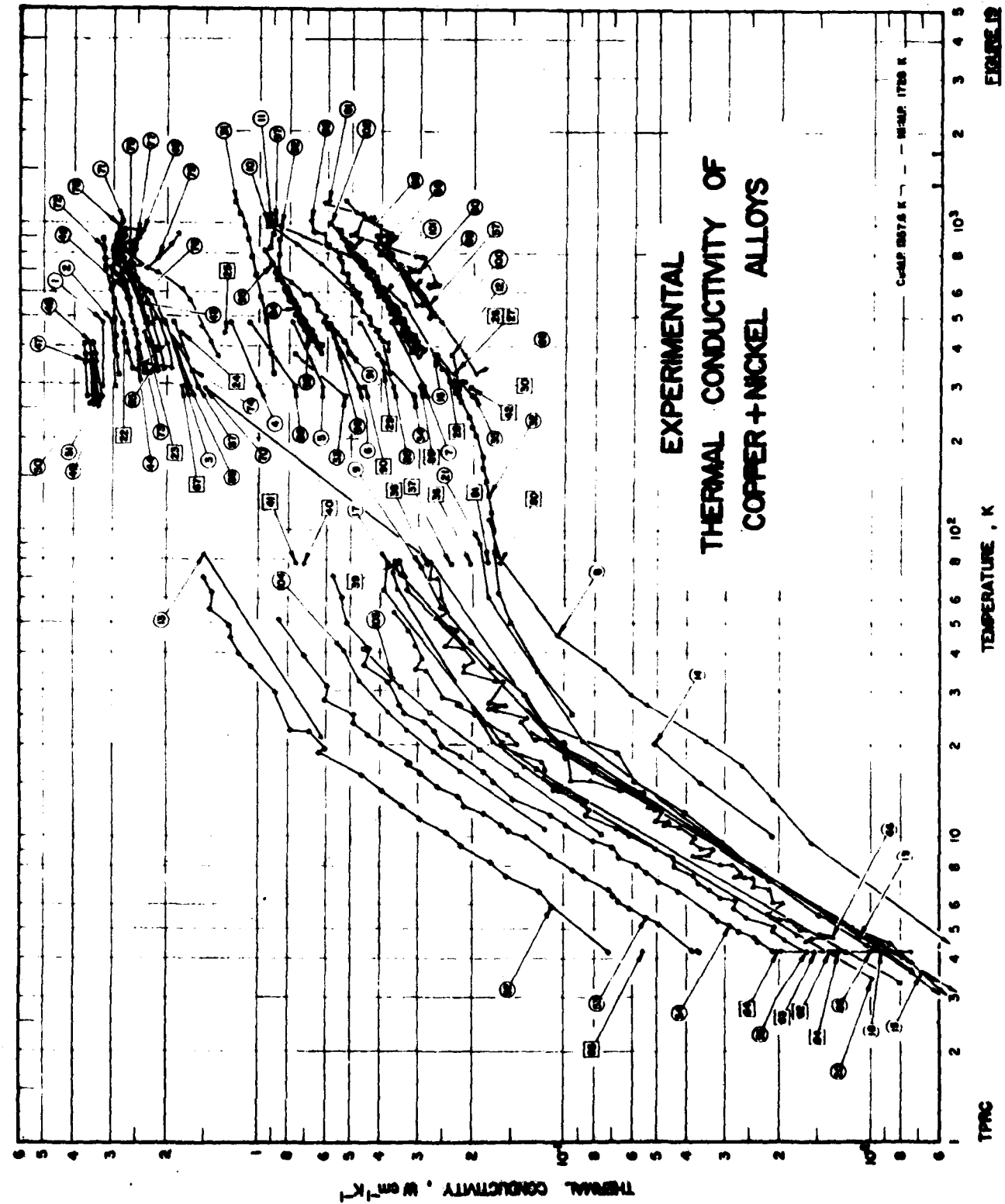


FIGURE 12

TPAC

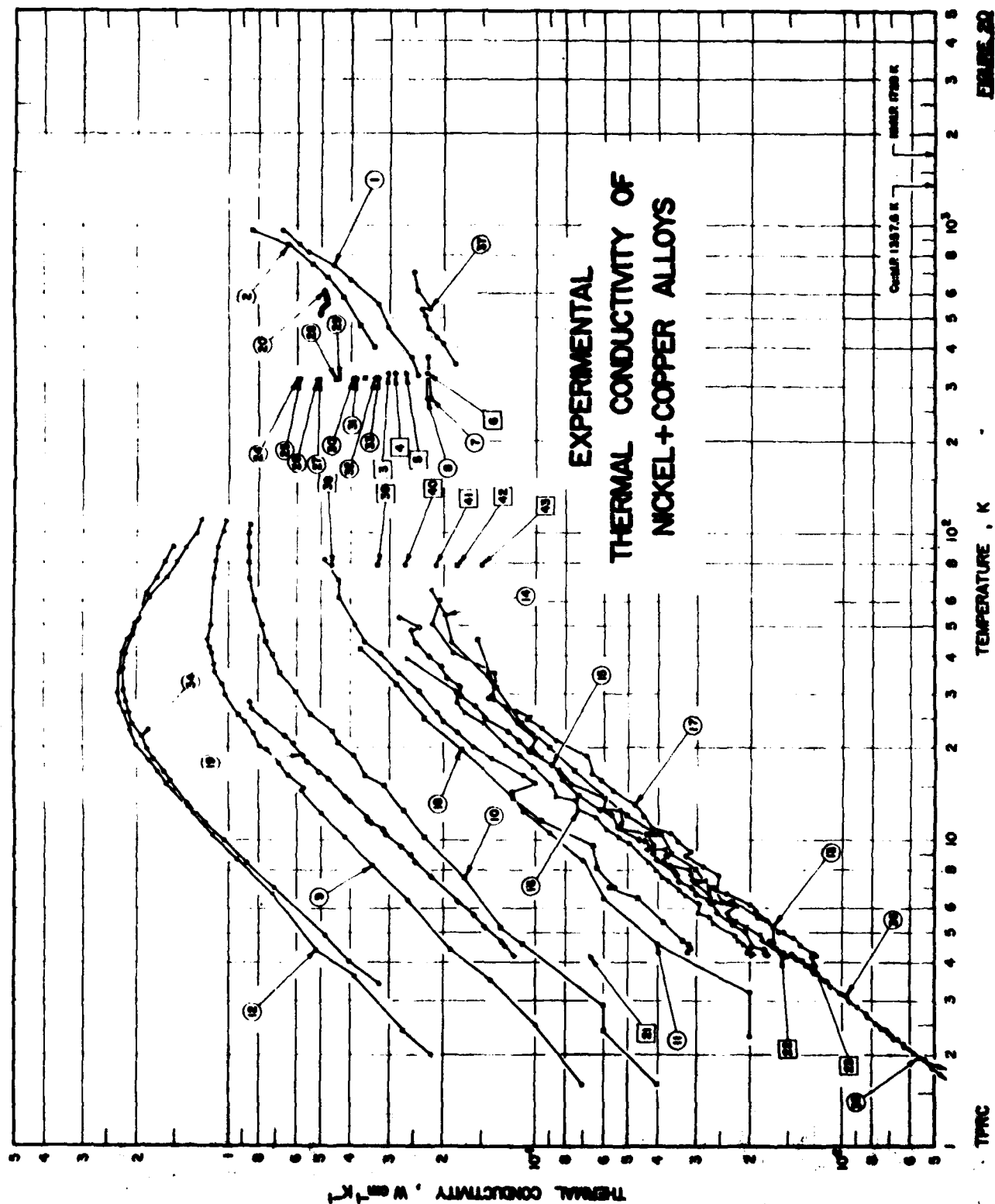


FIGURE 20

TABLE 12. THERMAL CONDUCTIVITY OF COPPER + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Ni	
1	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 107	99.73	0.26	0.03 Mg and 0.01 Fe; specimen 0.75 in. in diameter and 8 in. long; supplied by American Brass Co.; cold-rolled, annealed, and cold-drawn; annealed at 800 C for 2 hr; electrical conductivity $45.70 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
2	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 108	99.47	0.54	0.04 Mg and 0.02 Fe; similar to the above specimen except electrical conductivity $39.94$ and $26.86 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
3	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 109	97.94	1.97	0.04 Mg and 0.02 Fe; similar to the above specimen except annealed at 800 C for 4 hr; electrical conductivity $22.71$ and $17.56 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
4	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 110	94.92	5.09	0.03 Mg and 0.01 Fe; similar to the above specimen except electrical conductivity $12.39$ and $10.64 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
5	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 111	89.90	10.07	0.03 Mg, 0.004 C, and 0.02 Fe; similar to the above specimen except electrical conductivity $7.07$ and $6.46 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
6	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 125	84.85	15.07	0.06 Fe, 0.08 Mn, and 0.01 Mg; similar to the above specimen except electrical conductivity $5.094$ and $4.795 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
7	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	Bar 124	69.54	30.23	0.13 Mn, 0.05 Fe, and 0.05 Mg; similar to the above specimen except electrical conductivity $2.754$ and $2.730 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
8	68 Zavaritskii, N.V. and Zeldovich, A.G.	1955	L	2.3-106	Russian cupro nickel NM-81; 7	81.0	19.0	Specimen in strip form cut from a $6 \times 5$ mm tube; measured in helium.
9	68 Zavaritskii, N.V. and Zeldovich, A.G.	1955	L	2.5-76	Russian cupro nickel NM-81; 6	81.0	19.0	The above specimen; annealed at 800 C; measured in helium.
10	77 Sager, G.F.	1930	P	321-964		~79.8	20.0	0.2 Mn and trace Mg; ~0.25 cm in diameter and ~3.5 cm long; chill cast, hot rolled and cold drawn; annealed at 700 C for 12 hr; electrical conductivity $3.54$ , $3.46$ , $3.33$ , $3.21$ , $3.12$ , and $3.03 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 46, 150, 315, 462, 575, and 711 C, respectively.
11	77 Sager, G.F.	1930	P	335-991		~59.8	40.0	Similar to the above specimen except electrical conductivity $1.99$ , $1.99$ , $1.96$ , and $1.92 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 92, 206, 510, and 717 C, respectively.
12	137 Barnett, T.	1914	F	273-373	Eureka	60.0	40.0	0.0996 cm diameter and 40.0 cm long; electrical resistivity $45.90$ and $45.67 \mu\Omega \text{ cm}$ at 0 and 100 C, respectively.
13	136 Gifford, E. and Gunn, E.	1927	L	21, 63	Cu 11	99.0	1.0	7 cm long and 0.1 to 0.3 cm wide; drawn; electrical resistivity $2.97$ , $1.60$ , and $1.295 \mu\Omega \text{ cm}$ at 0, -190, and -252 C, respectively.
14	71 Williams, K.R. and Wilson, J.	1949	L	10-20	Cupro-nickel	70	30	4.1 mm in O.D., 2.5 mm in I.D., and 21 mm long; supplied by Yorkshire Copper Works Ltd.; cold-worked.
15	69 Balm, J.E.	1951	L	1.9-22		80	20	Average grain size 0.011 mm.
16	139 Jager, W. and Benedict, H.	1900	E	291, 375	Constantan	60	40	1.996 cm diameter and 27 cm long; density $8.92 \text{ g cm}^{-3}$ at 16 C; electrical conductivity $2.04$ and $2.037 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 16 and 100 C, respectively.

TABLE 12. THERMAL CONDUCTIVITY OF COPPER - NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Ni	Composition (continued), Specifications, and Remarks
17 130, 176	Zimmerman, J.E.	1951	L	3.3-75	CN 1	90 10	Cylindrical specimen 0.125 in. in diameter; machined from a forged bar; electrical resistivity 12.50, 12.72, and 14.66 $\mu\Omega$ cm at 19.7, 75.9, and 296 K, respectively.
18 130, 176	Zimmerman, J.E.	1951	L	3.0-77	CN 2	90 10	Cylindrical specimen 0.125 in. in diameter; cold-worked by rolling from 0.25 in. thick to 0.14 in. before being machined to size; electrical resistivity 12.65 and 14.49 $\mu\Omega$ cm at 76.2 and 296 K, respectively.
19 130, 176	Zimmerman, J.E.	1951	L	3.6-79	CN 3	90 10	Cylindrical specimen 0.125 in. in diameter; severely cold-worked; rolled from 0.5 in. cross section to 0.22 x 0.24 in. before machining; electrical resistivity 12.63 and 14.65 $\mu\Omega$ cm at 78.7 and 298 K, respectively.
20 130, 176	Zimmerman, J.E.	1951	L	3.4-79	CN 4	90 10	Single crystal; cylindrical specimen 0.125 in. in diameter; electrical resistivity 13.0, 13.10, and 15.04 $\mu\Omega$ cm at 20.5, 79.3, and 296 K, respectively.
21 70	Berman, R.	1951	L	3.0-91	Constantan	60 40	317 36 gauge wires bound and soldered together at ends; electrical resistivity 44.3, 45.3, and 52.7 $\mu\Omega$ cm at 20, 90, and 290 K, respectively.
22 47	Hanson, D. and Rodgers, C.E.	1932	L	438.2		Bal. 0.78	Prepared from high grade electrolytic Cu with traces of impurities; 6.5 in. long and 0.5 in. in diameter; annealed at 900 C.
23 47	Hanson, D. and Rodgers, C.E.	1932	L	438.2		Bal. 1.57	Similar to the above specimen.
24 47	Hanson, D. and Rodgers, C.E.	1932	L	438.2		Bal. 2.76	Similar to the above specimen.
25 47	Hanson, D. and Rodgers, C.E.	1932	L	438.2		Bal. 4.9	Similar to the above specimen.
26 45	Smith, A.W.	1925	L	330.2		50 50	~5 cm long with cross section 0.3 cm <sup>2</sup> ; made from Cu (< 0.03 of total impurity) supplied by Baker by fusing with Ni (99.75 to 99.95 pure including cobalt) supplied by International Nickel Co. of America; electrical conductivity 1.98 x 10 <sup>4</sup> $\Omega^{-1}$ cm <sup>-1</sup> at 25 C.
27 45	Smith, A.W.	1925	L	330.2		60 40	Similar to the above specimen except electrical conductivity 2.04 x 10 <sup>4</sup> $\Omega^{-1}$ cm <sup>-1</sup> at 25 C.
28 45	Smith, A.W.	1925	L	330.2		70 30	Similar to the above specimen except electrical conductivity 2.45 x 10 <sup>4</sup> $\Omega^{-1}$ cm <sup>-1</sup> at 25 C.
29 45	Smith, A.W.	1925	L	330.2		90 10	Similar to the above specimen except electrical conductivity 3.49 x 10 <sup>4</sup> $\Omega^{-1}$ cm <sup>-1</sup> at 25 C.
30 131	Ellis, W.C., Morgan, F.L. and Sager, F.G.	1928	P	305.2	Advance	55 45	0.25 cm diameter and 35 cm long; density 8.76 g cm <sup>-3</sup> ; electrical conductivity 2.023 x 10 <sup>4</sup> $\Omega^{-1}$ cm <sup>-1</sup> at 32 C; thermal conductivity value calculated from measured thermal diffusivity, specific heat capacity, and density.
31 132	Silverman, L.	1953	C	323-1174	Lohn	93.4 6.05	0.01 Mn and 0.01 Si; annealed at 900 C; advance used as comparative material.
32 133	Powers, R.W., Ziegler, J.B. and Johnston, H.L.	1951	L	26-295	Constantan	55 45	No details given.



TABLE 12. THERMAL CONDUCTIVITY OF COPPER + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Ni	Composition (continued), Specifications, and Remarks
33 63	Soderström, E.	1919	T	273, 373		89.94 10.06	Calculated composition; rolled and drawn to 1 mm thick; heated 0.5 hr close to melting point; electrical conductivity $6.2$ and $6.1 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
34 63	Soderström, E.	1919	T	273, 373		79.90 20.10	Similar to the above specimen except electrical conductivity $3.5$ and $3.3 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
35 63	Soderström, E.	1919	T	273, 373		60.02 39.98	Similar to the above specimen except electrical conductivity $2.0$ and $2.0 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
36 134	Aoyama, S. and No, T.	1940	L	78.2	8	29.89	0.03 Mn, 0.03 Fe, and traces of other impurities; prepared from electrolytic Ni (containing 0.53 Co, 0.06 Fe, and 0.02 Al) and electrolytic Cu (containing 0.015 Sb, 0.01 Fe, 0.007 S, and traces of P) by fusing; 4.00 mm in diameter and 60.0 mm long; electrical resistivity $49.3 \mu\Omega$ cm at $-196$ C.
37 134	Aoyama, S. and No, T.	1940	L	78.2	9	19.83	0.04 Mn, 0.02 Fe, and traces of other impurities; the same original materials and dimensions as the above specimen; electrical resistivity $27.1 \mu\Omega$ cm at $-196$ C.
38 134	Aoyama, S. and No, T.	1940	L	78.2	10	13.84	0.11 Fe and trace Mn; the same original materials and dimensions as the above specimen; electrical resistivity $17.6 \mu\Omega$ cm at $-196$ C.
39 134	Aoyama, S. and No, T.	1940	L	78.2	11	9.47	0.14 Fe, traces of Mn and other impurities; the same original materials and dimensions as the above specimen; electrical resistivity $11.9 \mu\Omega$ cm at $-196$ C.
40 134	Aoyama, S. and No, T.	1940	L	78.2	12	3.67	0.09 Fe and traces of other impurities; the same original materials and dimensions as the above specimen; electrical resistivity $3.43 \mu\Omega$ cm at $-196$ C.
41 134	Aoyama, S. and No, T.	1940	L	78.2	13	98.94 1.03	0.03 Fe and traces of other impurities; the same original materials and dimensions as the above specimen; electrical resistivity $1.039 \mu\Omega$ cm at $-196$ C.
42 136	Orlowski, E.	1900	L	291.2		54 46	Density $8.89 \text{ g cm}^{-3}$ ; electrical conductivity $1.99 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 18 C.
43 144	Miluyakov, V. E.	1937		336-825		99.05 0.70	0.1 Be and 0.15 Co; electrical conductivity $25.8$ , $23.1$ , $20.4$ , $18.25$ , $16.5$ , $15.67$ , and $14.33 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at $63.0$ , $114.6$ , $166$ , $273$ , $375.8$ , $438.5$ , and $581.3$ C, respectively.
44 136	Miluyakov, V. E.	1937		336-900		Bal. 0.90	0.10 Be and 0.10 Zr; electrical resistivity $3.34$ , $3.65$ , $4.33$ , $5.21$ , $5.78$ , $6.33$ , $7.06$ , and $8.14 \mu\Omega$ cm at $59.4$ , $118.6$ , $171.8$ , $291.8$ , $368.6$ , $457$ , $534.5$ , and $628.5$ C, respectively.
45 136	Miluyakov, V. E.	1937		336-947		Bal. 0.80	0.29 Ti; electrical resistivity $4.25$ , $4.89$ , $5.56$ , $6.01$ , $6.46$ , $6.87$ , $7.18$ , $7.59$ , $7.96$ , $8.33$ , and $9.78 \mu\Omega$ cm at $62.8$ , $139.9$ , $217.5$ , $290.9$ , $462.5$ , $440.3$ , $580.3$ , $674.3$ , $618.0$ , and $673.6$ C, respectively.
46 136	Miluyakov, V. E.	1937		345-923		Bal. 0.55	0.17 Zr; electrical resistivity $3.45$ , $4.13$ , $4.43$ , $5.10$ , $5.32$ , $6.78$ , $6.30$ , $6.83$ , $7.29$ , and $8.97 \mu\Omega$ cm at $71.8$ , $158.7$ , $201.0$ , $231.0$ , $331.0$ , $401.4$ , $473.6$ , $534.5$ , $578.0$ , and $649.5$ C, respectively.
47 137	Chubb, W. F.	1935	L	273-403		Bal. 0.204	$\approx 0.079$ O; specimen $50.6$ cm long.
48 137	Chubb, W. F.	1935	L	273-403		Bal. 0.303	$\approx 0.079$ O; specimen $50.6$ cm long.
49 137	Chubb, W. F.	1935	L	273-403		Bal. 0.506	$\approx 0.079$ O; specimen $50.6$ cm long.

TABLE 12. THERMAL CONDUCTIVITY OF COPPER + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Ni	
50 137	Chubb, W. F.	1938	L	273-403		Bal.	0.303	0.0042 Fe, 0.0014 Pb, trace Sn and Zn; specimen 50.6 cm long.
51 137	Chubb, W. F.	1938	L	273-403		Bal.	0.508	~0.022 O; specimen 50.6 cm long.
52 74	Erasmus, J. C. and Jahoda, J. A.	1968	L	4.2-70	Cu 98		2.29	Single crystal; 6.0-7.5 mm diameter and 12 cm long; prepared by electron beam float zoning; supplied by Materials Research Corp.; residual electrical resistivity 2.17 $\mu\Omega$ cm; measured in a vacuum of $10^{-6}$ mm Hg.
53 74	Erasmus, J. C. and Jahoda, J. A.	1968	L	4.2-51	Cu 98		4.05	Similar to the above specimen except residual electrical resistivity 4.95 $\mu\Omega$ cm.
54 74	Erasmus, J. C. and Jahoda, J. A.	1968	L	4.2-71	Cu 91		9.30	0.025 Al; polycrystalline; 5.0 mm in diameter and 19 cm long; vacuum cast ingot hammer forged, hot rolled to 18 mm diameter and rough turned, the rough swaged to 10 mm in diameter, then machined to size; annealed at 930 C for 24 hr in the argon furnace and allowed to cool slowly; residual electrical resistivity 11.22 $\mu\Omega$ cm; measured in a vacuum of $10^{-6}$ mm Hg.
55 74	Erasmus, J. C. and Jahoda, J. A.	1968	L	4.2-54	Cu 72		27.96	0.023 Al; similar to the above specimen except residual electrical resistivity 23.39 $\mu\Omega$ cm.
56 136	Kummer, D. L., Rosenthal, J. J. and Lam, D. W.	1965	C	490-949	Constantan, No. 103	~60	~40	Thermocouple grade; 1 in. diameter and 1 in. thick; Armco iron used as comparative material.
57 136	Kummer, D. L., et al.	1965	C	539-906	Constantan, No. 103	~60	~40	2.5 in. O.D., 0.75 in. I.D., and 3 in. long.
58 136	Carroll, J. M.	1964	C	492-850	Constantan; Specimen No. 1	~60	~40	Thermocouple grade; 1 in. in diameter and 1 in. long; Armco iron used as comparative material.
59 <sup>a</sup> 136	Carroll, J. M.	1964	C	499-850	Constantan; Specimen No. 2	~60	~40	Similar to the above specimen.
60 136	Carroll, J. M.	1964	R	692-1044	Constantan; Specimen No. 1	~60	~40	Thermocouple grade; 0.25 in. I.D., 1 in. O.D., and 1 in. long.
61 136	Carroll, J. M.	1964	R	623-1176	Constantan; Specimen No. 3	~60	~40	Similar to the above specimen.
62 73	Erasmus, J. C. and Jahoda, J. A.	1964	L	4.2	Ko	Bal.	~40	Polycrystalline; wire specimen 1.35 to 1.45 mm in diameter and 125 mm long; obtained from International Nickel Co.; vacuum cast ingot hammer forged; hot rolled to 18.5 mm diameter, rough turned, cold rolled to 6 mm diameter and drawn to 1.5 mm diameter, cut; annealed at 1000 C for 24 hr, slowly cooled in the furnace over a period of 6 hr, electro-polished; electrical resistivity 42.3 $\mu\Omega$ cm at 4.2 K.
63 73	Erasmus, J. C. and Jahoda, J. A.	1964	L	4.2	666	Bal.	9.3	0.025 Al; polycrystalline; same dimensions, supplier, and fabrication method as the above specimen; electrical resistivity 19.94 $\mu\Omega$ cm at 4.2 K.
64 73	Erasmus, J. C. and Jahoda, J. A.	1964	L	4.2	664	Bal.	4.74	<0.1 each of Fe, Mg, and Mn, and 0.043 Al; polycrystalline; same dimensions, supplier, and fabrication method as the above specimen; electrical resistivity 7.04 $\mu\Omega$ cm at 4.2 K.
65 73	Erasmus, J. C. and Jahoda, J. A.	1964	L	4.2	668	Bal.	1.96	Polycrystalline; same dimensions, supplier, and fabrication method as the above specimen; electrical resistivity 2.17 $\mu\Omega$ cm at 4.2 K.

<sup>a</sup> Not shown in figure.

TABLE 12. THERMAL CONDUCTIVITY OF COPPER + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Ni	
66 140	Erdmann, J. C. and Jaboda, J. A.	1968	L	4.6-78	Cu 72 Ni 28	72	28	Polycrystalline; 1.35 to 1.45 mm in diameter and 130 mm long; obtained from International Nickel Co., Inc.; vacuum cast ingot hammer forged, hot-rolled to 18.5 mm diameter, rough turned, cold-rolled to 6 mm diameter and drawn to 1.5 mm diameter, cut, annealed in argon atmosphere at 1000 C for 24 hr, slowly cooled in the furnace over a period of 6 hr, electropolished; grain size 50 to 200 $\mu$ .
67 83	Kierapo, W.	1967	L	293.2			1.86	Cylindrical specimen; electrical resistivity 2.3466, 2.3468, 2.3521, 2.3522, 2.3523, 2.3492, 2.4812, 2.5802, 2.7501, 2.8318, 3.0336, 3.1611, 3.3366, 3.4710, 3.6146, 3.7563, 3.8972, and 3.9674 $\mu\Omega$ cm at 4.2, 10, 20, 30, 40, 50, 70, 83, 103, 123, 143, 163, 183, 203, 223, 243, 263, and 273 K, respectively.
68 72, 141	Erdmann, J. C. and Jaboda, J. A.	1962	E	4.2	Constantan	60	40	Commercial alloy; about 1 to 3 mm in diameter and about 100 mm long; annealed; measured in different strain conditions.
69 132	Silverman, L.	1963	C	323-1173	Advance	54.79	44.04	1.20 Mn, 0.035 C, and 0.003 Si; cylindrical bar specimen; annealed at 900 C; lead used as comparative material; smoothed values reported.
70 142	Zientkova, S. and Savel'ov, I. V.	1966	L	18-290	Cupronickel	77.44	20.48	1.99 Zn; 4.97 mm O.D., 4.16 mm I.D., and 87 mm long.
71 144, 145	Mikryukov, V. E.	1967	E	321-1002		99.03	0.60	0.27 Zr and 0.1 P; electrical conductivity 26.70, 32.35, 37.01, 24.70, 21.70, 19.34, 17.54, 15.60, 13.36, 12.64, and 11.38 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 47.3, 94.0, 165.5, 211.0, 283.5, 354.3, 432.1, 493.6, 560.5, 616.3, 685.1, and 739.0 C, respectively.
72 144, 145	Mikryukov, V. E.	1967	E	334-804		98.99	0.60	0.26 Zr and 0.15 Bi; electrical conductivity 32.90, 28.95, 24.82, 22.12, 20.71, 18.47, 17.43, 16.23, and 15.00 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 61.9, 106.5, 163.0, 201.5, 331.3, 442.0, 483.0, 544.0, and 611.0 C, respectively.
73 136	Mikryukov, V. E.	1967	E	336-946		99.0	0.60	0.20 Ti; electrical conductivity 23.50, 20.50, 17.97, 16.65, 15.48, 13.20, 14.91, 12.72, 11.26, and 10.23 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 62.0, 130.9, 217.5, 290.6, 363.5, 440.3, 530.3, 618.0, and 673.6 C, respectively.
74 136	Mikryukov, V. E.	1967	E	329-774		98.35	0.40	0.25 P; electrical conductivity 19.86, 18.00, 17.35, 15.44, 14.22, and 13.40 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 64.0, 118.8, 201.0, 316.0, 422.0, and 500.5 C, respectively.
75 136	Mikryukov, V. E.	1967	E	370-920		98.50	1.20	0.30 Bi; electrical conductivity 15.82, 14.30, 13.87, 12.25, 11.80, 12.66, 13.13, 11.35, 9.11, and 8.96 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 56.6, 136.6, 194.9, 270.9, 333.1, 412.0, 439.0, 493.3, 570.0, and 646.6 C, respectively.
76 136	Mikryukov, V. E.	1967	E	331-815		98.73	0.60	0.33 Zr and 0.14 Bi; electrical conductivity 25.70, 22.10, 22.00, 19.25, 17.30, 15.66, 14.60, and 13.45 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 58.0, 132.0, 198.6, 265.0, 330.3, 406.6, 488.0, and 542.0 C, respectively.
77 136	Mikryukov, V. E.	1967	E	333-910		98.53	1.0	0.33 Zr and 0.14 Bi; electrical conductivity 24.65, 22.00, 19.25, 17.12, 16.20, 15.32, 12.75, and 11.35 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 60.0, 117.0, 195.0, 262.0, 354.3, 442.0, 544.0, and 637.0 C, respectively.
78 136	Mikryukov, V. E.	1967	E	326-974		99.13	0.62	0.28 Zr; electrical conductivity 20.3, 24.7, 21.1, 16.4, 17.5, 16.8, 12.9, and 11.7 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 32.6, 131.5, 225.4, 305.3, 400.0, 435.9, 532.9, 635.7, and 701.1 C, respectively.

TABLE 12. THERMAL CONDUCTIVITY OF COPPER-NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Ni	Composition (continued), Specifications, and Remarks
79 136	Milkyakov, V.E.	1957	E	333-855		49.3 0.28	0.24 Zr and 0.19 Be; electrical conductivity 26.10, 22.90, 19.50, 17.46, 15.30, 14.34, 13.40, and $12.12 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 59.8, 119.5, 216.5, 302.6, 393.0, 455.1, 522.0, and 581.6 C, respectively.
80 134	Aoyama, S. and Ho, T.	1940	L	78.2	6	Bal.	0.26 Co, 0.06 Fe, 0.05 Mn, 0.01 Al, 0.008 Sb, 0.004 S, and trace Pb (calculated composition); electrical resistivity $54.9 \mu\Omega \text{cm}$ .
81 134	Aoyama, S. and Ho, T.	1940	L	78.2	7	Bal.	0.21 Co, 0.07 Fe, 0.02 Mn, 0.008 Sb, 0.006 Al, 0.004 S, and trace Pb (calculated composition); electrical resistivity $51.4 \mu\Omega \text{cm}$ .
82* 143	Fairbank, H.A. and Lee, D.M.	1960	L	0.28-4.0	Cupronickel	69.60 30.0	0.40 Fe; nominal composition; supplied by Anascode; drawn into 0.0622 in. O.D. and 0.0647 in. I.D.
83 143	Milkyakov, V.Ye.	1959	E	340-827		Bal.	0.15 Co, 0.15 Fe, 0.1 Be, and 0.1 C; electrical resistivity 3.99, 4.29, 5.01, 5.60, 5.98, 6.37, 6.93, 7.55, and $9.32 \mu\Omega \text{cm}$ at 65, 115, 196, 275, 390, 440, 511, 589, and 700 C, respectively.
84 73	Erdmann, J.C. and Jaboda, J.A.	1964	L	4.2	667	Bal.	<1.0 each Mn, Mg, Fe, and 0.023 Al; polycrystalline; wire specimen 1.35 to 1.45 mm in diameter and 125 mm long; obtained from International Nickel Co.; vacuum cast ingot hammer forged, hot rolled to 18.5 mm diameter, rough turned, cold rolled to 6 mm diameter and drawn to 1.5 mm diameter, cut; annealed at 1000 C for 24 hr, cooled slowly in the furnace over a period of 6 hr, electropolished; electrical resistivity $32.3 \mu\Omega \text{cm}$ at 4.2 K.
85 49	Smith, C.S. and Palmer, E.W.	1936	L	293.473	Bar 39	79.68 19.79	0.30 Mn and 0.23 Fe; 0.75 in. diameter and 8 in. long; cold-rolled to 1.25 in. in diameter, annealed, cold-drawn to size; heat-treated at 800 C; electrical conductivity $3.786$ and $3.600 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
86 49	Smith, C.S. and Palmer, E.W.	1936	L	293.473	Bar 66	94.06 3.01	0.89 Si and 0.04 Fe; 0.75 in. diameter and 8 in. long; cold-rolled to 1.25 in. in diameter, annealed, cold-drawn to size; heat-treated at 870 C for 3 hr, quenched; electrical conductivity 9.778 and $9.140 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
87 49	Smith, C.S. and Palmer, E.W.	1936	L	293.473	Bar 64A		Similar to the above specimen except reheated after quenching at 500 C for 2 hr; electrical conductivity 20.69 and $16.38 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
88 49	Smith, C.S. and Palmer, E.W.	1936	L	293.473	Bar 64B		Similar to the above specimen bar 66 (Curve No. 86) except cooled slowly after heat-treatment at 870 C; electrical conductivity 22.60 and $17.34 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 and 200 C, respectively.
89 123	Materials in Design Engineering	1960		293.2	Cupro-nickel	68.9 30	0.6 Mn and 0.5 Fe; nominal composition; density 8.94 g $\text{cm}^{-3}$ ; electrical resistivity $37 \mu\Omega \text{cm}$ at 20 C.
90 123	Materials in Design Engineering	1960		293.2	Cupro-nickel	68.35 10	1.26 Fe and 0.4 Mn; nominal composition; density 8.94 g $\text{cm}^{-3}$ ; electrical resistivity $15 \mu\Omega \text{cm}$ at 20 C.
91 146	Willott, R.E.	1966	C	378-463	Copper-Nickel (76%) alloy	88.08 10.07	1.18 Fe, 0.67 Mn, <0.10 Zn, and <0.02 Pb; annealed at 780 C and cooled by waterfall spray at the exit of the furnace; Armco iron used as comparative material; equilibrium 1.
92 146	Willott, R.E.	1966	C	701-909	Copper-Nickel (76%) alloy		The above specimen; equilibrium 2.
93 146	Willott, R.E.	1966	C	368-466	Copper-Nickel (76%) alloy		The above specimen; equilibrium 3.

\* Not shown in figure.

TABLE 12. THERMAL CONDUCTIVITY OF COPPER + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Csr. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)			Composition (continued), Specifications, and Remarks
						Cu	Ni		
94 146	WILSON, R. E.	1968	C	447-566	Copper-Nickel (706) alloy	89.08	10.07		1.18 Fe, 0.67 Mn, <0.10 Zn, and <0.02 Pb; the above specimen; equilibrium 4.
95 146	WILSON, R. E.	1968	C	557-739	Copper-Nickel (706) alloy				The above specimen; equilibrium 5.
96 146	WILSON, R. E.	1968	C	391-486	Copper-Nickel (706) alloy				Similar to the above specimen except annealed at 750 C for 1 hr and water quenched.
97 146	WILSON, R. E.	1968	C	377-1017	Copper-Nickel (706) alloy				Similar to the above specimen except annealed at 750 C for 1 hr and furnace cooled.
98 146	WILSON, R. E.	1968	C	362-1020	Copper-Nickel (716) alloy	77.75	20.67		0.81 Fe, 0.55 Mn, 0.20 Zn, 0.01 Pb, and 0.017 C; annealed at 750 C and cooled by waterfall spray at the exit end of the furnace; Armco iron used as comparative material.
99 146	WILSON, R. E.	1968	C	406-927	Copper-Nickel (715) alloy; 1	68.33	30.72		0.53 Fe, 0.41 Mn, <0.10 Zn, 0.028 C, and <0.006 Pb; annealed at 650 C and cooled by waterfall spray at the exit end of the furnace; Armco iron used as comparative material.
100 146	WILSON, R. E.	1968	C	345-949	Copper-Nickel (715) alloy; 2	69.29	30.87		0.59 Mn, 0.51 Fe, 0.36 C, <0.10 Zn, and 0.006 Pb; similar to the above specimen except annealed at 750 C.
101 146	WILSON, R. E.	1968	C	366-948	Copper-Nickel (715) alloy	68.40	29.94		0.62 Fe, 0.50 Zn, 0.46 Mn, 0.063 C, and 0.010 Pb; similar to the above specimen.
102 146	WILSON, R. E.	1968	C	399-991	Copper-Nickel (715) alloy	68.60	29.94		0.61 Fe, 0.48 Mn, 0.30 Zn, 0.069 C, and 0.007 Pb; similar to the above specimen except annealed at 1000 C and water quenched.
103 76	Besley, A., Linn, R., 1974 Klaflay, R.; Duncanson, D.L., and Wilson, R.E.			11-40			3.71		Calculated composition from atomic percent; annealed at 1075 $\pm$ 5 C for 72 hrs and slowly cooled afterwards in 18 hrs; residual electrical resistivity reported as 4.93 $\mu\Omega$ cm.
104 76	Besley, A., et al.	1974		10-41			3.71		Calculated composition from atomic percent; heavily swaged; residual electrical resistivity reported as 4.54 $\mu\Omega$ cm.

TABLE 13. THERMAL CONDUCTIVITY OF NICKEL - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Ni	Composition (weight percent) Cu	Composition (continued), Specifications, and Remarks
1	77 Sager, G. F.	1930	P	325-970		60	40	0.2 Mn and 0.17 Mg; 2 mm diameter and 35 cm long; prepared from Mond nickel by fusing, chill-casting, hot-rolling, and cold-drawing; annealed at 700 C for 12 hr; density 8.81 g cm <sup>-3</sup> ; electrical conductivity 1.69, 1.86, 1.85, 1.82, 1.81, 1.78, 1.76, 1.75, and 1.73 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 26, 133, 204, 306, 467, 580, 642, 690, and 758 C, respectively; thermal conductivity values calculated from measured thermal diffusivity, specific heat capacity, and density.
2	77 Sager, G. F.	1930	P	317-966		80	20	Similar to above except density 8.83 g cm <sup>-3</sup> and electrical conductivity 3.60, 3.04, 2.90, 2.72, 2.67, 2.48, 2.46, 2.38, 2.27, 2.32, 2.17, 2.13, 2.04, 1.97, and 1.98 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 26, 76, 91, 126, 131, 164, 194, 231, 291, 331, 396, 451, 546, 688, and 744 C, respectively.
3	45 Smith, A. W.	1925	L	330		80	20	Prepared by fusing Ni (99.75 to 99.85 pure); supplied by International Nickel Co., and 99.97 pure Cu, supplied by Baker; ~5.5 cm long and 0.3 cm <sup>2</sup> in cross-sectional area; electrical conductivity 3.60 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 25 C.
4	45 Smith, A. W.	1925	L	330		70	30	Similar to the above specimen except electrical conductivity 2.17 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 25 C.
5	45 Smith, A. W.	1925	L	330		60	40	Similar to the above specimen except electrical conductivity 2.02 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 25 C.
6	45 Smith, A. W.	1925	L	330		50	50	Similar to the above specimen except electrical conductivity 1.98 x 10 <sup>4</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 25 C.
7	63 Sedatun, E.	1919	T	273, 373		60.93	39.07	Rolled and drawn; annealed at close to melting point for 0.5 hr.
8	63 Sedatun, E.	1919	T	273, 373		81.63	18.37	Similar to the above specimen.
9	78 Grubb, D. and Harrison, J. P.	1965	E	1.6-111	C		0.65	Cylindrical specimen, 4 mm in diameter; calculated composition from atomic composition; supplied by Johnson Matthey and Co.; chill cast from J.M. 899 Ni and J.M. 30 Cu; annealed at 850 C for 12 hr; small grains; very fine grain boundaries; electrical resistivities are estimated from reported Lorenz number L and thermal conductivity k as 0.504, 0.635, 0.622, 0.634, 0.638, 0.654, 0.664, 0.678, 0.684, 0.689, 0.698, 0.707, 0.694, 0.706, 0.726, 0.734, 0.738, 0.699, and 0.530 μΩ cm at 1.6, 2.5, 4.4, 6.4, 8.3, 10.3, 12.3, 14.9, 16.2, 17.9, 19.7, 20.3, 23.2, 24.4, 26.6, 29.6, 32.2, 35.1, 37.4, 40.6, 43.5, and 45.3 K, respectively.
10	78 Grubb, D. and Harrison, J. P.	1965	E	1.6-107	D		1.62	Similar to the above specimen; long grains running in one direction, very thick (~0.65 mm) grain boundaries; electrical resistivities are estimated from reported Lorenz number L and thermal conductivity k as 0.502, 1.004, 1.115, 1.209, 1.266, 1.306, 1.442, 1.387, 1.446, 1.425, 1.488, 1.497, 1.471, 1.497, 1.512, 1.528, 1.605, 1.522, 2.077, 2.297, and 2.023 μΩ cm at 1.6, 2.4, 3.2, 7.9, 10.2, 12.1, 16.2, 16.9, 20.7, 22.6, 25.7, 26.5, 28.2, 40.2, 45.4, 50.2, 50.4, 58.2, and 102.7 K, respectively.

TABLE 12. THERMAL CONDUCTIVITY OF NICKEL + COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Ni Cu	Composition (continued), Specifications, and Remarks	
11 78	Greig, D. and Harrison, J.P.	1965	E	2.3-82.1	E	4.53	Similar to the above specimen; various sizes of grains; various thicknesses of grain boundaries; electrical resistivities are estimated from reported Lorenz number $L$ and thermal conductivity $k$ as 2.997, 4.318, 2.944, 3.357, 2.804, 2.757, 2.769, 2.912, 2.086, 4.983, 4.422, 4.376, 4.361, 4.164, 4.246, 4.266, 4.211, 4.190, 4.086, 4.129, 4.268, 4.998, 4.989 $\mu\Omega$ cm at 2.3, 3.2, 4.6, 6.5, 8.6, 10.6, 12.5, 14.4, 15.4, 16.2, 18.5, 20.1, 22.4, 24.4, 26.1, 28.6, 30.6, 40.4, 45.2, 50.2, 61.7, 70.1, and 82.1 K, respectively.	
12 78	Greig, D. and Harrison, J.P.	1965	E	2.0-111	F	0.35	Similar to the above specimen; mostly small grains, but few long grains running from center; electrical resistivities are estimated from reported Lorenz number $L$ and thermal conductivity $k$ as 0.219, 0.199, 0.225, 0.224, 0.229, 0.225, 0.230, 0.227, 0.226, 0.244, 0.244, 0.250, 0.255, 0.264, 0.260, 0.266, 0.261, 0.414, 0.541, 0.712, 0.875, 1.064, and 1.323 $\mu\Omega$ cm at 2.6, 4.4, 6.7, 8.7, 10.4, 12.3, 14.6, 16.7, 18.2, 20.2, 22.3, 25.8, 28.0, 28.8, 28.9, 30.1, 35.2, 40.9, 45.5, 51.9, 62.1, 71.5, 81.3, 90.2, and 100.8 K, respectively.	
13 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-45	Cu 49	50.50	49.47	0.030 Al; polycrystalline; 5.0 mm diameter and 16 cm long; supplied by International Nickel Co., Inc; vacuum cast ingot hammer forged, hot-rolled to 18 mm diameter and rough turned; swaged to 10 mm diameter, and machined to size; annealed at 930 C for 24 hr in argon furnace and cooled slowly; residual electrical resistivity 48.10 $\mu\Omega$ cm; measured in a vacuum of $10^{-4}$ mm Hg.
14 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-65	Ni 65	64.87	Bal.	0.051 Al; similar to above except residual electrical resistivity 27.63 $\mu\Omega$ cm.
15 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-63	Ni 65	64.70	Bal.	0.064 Al; similar to above except residual electrical resistivity 11.14 $\mu\Omega$ cm.
16 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-39	Ni 70	90.24	Bal.	0.060 Al; similar to above except residual electrical resistivity 8.24 $\mu\Omega$ cm.
17 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-61	Ni 91	91.05	Bal.	0.046 Al; similar to above except residual electrical resistivity 18.88 $\mu\Omega$ cm.
18 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-42	Ni 96	95.60	Bal.	Similar to above except residual electrical resistivity 3.91 $\mu\Omega$ cm.
19 74	Erkman, J.C. and Jaboda, J.A.	1968	-	4.2-28	Ni 96	99.35	Bal.	Single crystal; 6.0-7.5 mm in diameter and 12 cm long; supplied by Materials Research Corp; prepared by electron beam flat casting; residual electrical resistivity 0.907 $\mu\Omega$ cm; measured in a vacuum of $10^{-4}$ mm Hg.
20 147	Jackson, P.J. and Saunders, N.H.	1968		514-614		Bal.	6.7	Polycrystalline; prepared from 4 N purity Ni and Cu; annealed; Curie point 278 C.
21 73	Erkman, J.C. and Jaboda, J.A.	1964	L	4.2	131	Bal.	2.03	Polycrystalline; wire specimen 1.35 to 1.45 mm in diameter and 125 mm long; obtained from International Nickel Co.; vacuum cast ingot hammer forged, hot-rolled to 18.5 mm in diameter, rough turned, cold rolled to 6 mm diameter and drawn to 1.5 mm diameter, cut; annealed at 1000 C for 24 hr, slowly cooled in the furnace for a period of 6 hr, electro-polished; grain size 50 to 250 $\mu$ ; electrical resistivity 1.65 $\mu\Omega$ cm at 4.2 K.

TABLE 13. THERMAL CONDUCTIVITY OF NICKEL - COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent): Ni Cu	Composition (continued), Specifications, and Remarks
22	73 Erdmann, J.C. and Jahoda, J.A.	1964	L	4.2	670	84.7	Bal. <0.1 each of Fe and Mn, 0.054 Al, and 0.02 C; polycrystalline; same supplier and fabrication method as the above specimen; electrical resistivity 10.64 $\mu\Omega$ cm at 4.2 K.
23	73 Erdmann, J.C. and Jahoda, J.A.	1964	L	4.2	669	64.87	Bal. 0.051 Al, 0.013 C, and <0.01 Fe; polycrystalline; same supplier and fabrication method as the above specimen; electrical resistivity 27.8 $\mu\Omega$ cm at 4.2 K.
24	148 Burger, R., Dittrich, H., and Koch, K.M.	1968	E	316.2		95	5 Prepared from 99.98 pure nickel; measured in transverse magnetic fields ranging from 0.48 to 10.63 kOe; reported data taken from smooth curve.
25	148 Burger, R., et al.	1968	E	316.2			The above specimen measured in longitudinal magnetic fields ranging from 0.16 to 10.59 kOe; smoothed values reported.
26	148 Burger, R., et al.	1968	E	316.2		90	10 Prepared from 99.98 pure nickel; measured in transverse magnetic fields ranging from 0.49 to 10.48 kOe; smoothed values reported.
27	148 Burger, R., et al.	1968	E	316.2			The above specimen measured in longitudinal magnetic fields ranging from 0.17 to 10.48 kOe; smoothed values reported.
28	148 Burger, R., et al.	1968	E	316.2		85	15 Prepared from 99.98 pure nickel; measured in transverse magnetic fields ranging from 0.47 to 10.50 kOe; smoothed values reported.
29	148 Burger, R., et al.	1968	E	316.2			The above specimen measured in longitudinal magnetic fields ranging from 0.19 to 10.47 kOe; smoothed values reported.
30	148 Burger, R., et al.	1968	E	316.2		80	20 Prepared from 99.98 pure nickel; measured in transverse magnetic fields ranging from 0.45 to 10.39 kOe; smoothed values reported.
31	148 Burger, R., et al.	1968	E	316.2			The above specimen measured in longitudinal magnetic fields ranging from 0.29 to 10.48 kOe; smoothed values reported.
32	148 Burger, R., et al.	1968	E	316.2		75	25 Prepared from 99.98 pure nickel; measured in transverse magnetic fields ranging from 0.48 to 10.34 kOe; smoothed values reported.
33	148 Burger, R., et al.	1968	E	316.2			The above specimen measured in longitudinal magnetic fields ranging from 0.33 to 10.46 kOe; smoothed values reported.
34	61 Farrell, T. and Greig, D.	1969	L	3.4-90			0.34 ~3 mm diameter and 9 cm long; supplied by Metals Research Ltd.; annealed at 850 C for 15 hr; residual electrical resistivity 0.247 $\mu\Omega$ cm; electrical resistivity 6.67 $\mu\Omega$ cm at 0 C.
35	149 Berger, L.	1969	L	1.7-4.3		Bal.	35 Polycrystalline from Johnson Matthey Ni and Cu, vacuum melted, swaged, homogenized for 48 hr at 1200 C in purified helium, and furnace cooled.
36	149 Berger, L.	1969	L	1.5-4.3			The above specimen measured in a constant longitudinal field of 58.9 kG.
37	166, 177 Yeh, W.B. and Berger, L.	1970	L	1.6-4.3			33.4 Prepared by melting high-purity Johnson Matthey metal in a vacuum of $6 \times 10^{-4}$ torr, after cooling, machining to round rod, homogenizing at 1300 C for 2400 hr, in helium, annealing in a vacuum of $10^{-4}$ torr at 1000 C for 0.5 hr, averaging to 0.797 cm in diameter, again annealing in a vacuum of $6 \times 10^{-4}$ torr at 750 C for 1 hr; grain size 0.1-0.5 mm; electrical resistivity 33.4 $\mu\Omega$ cm at 4.2 K; run 7.
38	166, 177 Yeh, W.B. and Berger, L.	1970	L	1.7-4.3			The above specimen; run 8.



TABLE 13. THERMAL CONDUCTIVITY OF NICKEL + COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Ni	Cu	
39	Yehia, W.B. and Berger, L.	1970	L	2.3-21				The above specimen measured in a parallel magnetic field of 58.96 kG; run 10.
40	Yehia, W.B. and Berger, L.	1970	L	1.4-2.1				The above specimen measured without the magnetic field; run 11.
41	Yehia, W.B. and Berger, L.	1970	L	1.4-4.3				The above specimen; run 9.
42	Yehia, W.B. and Berger, L.	1970	L	2.1-21				The above specimen; run 12.
43	Donalson, J.W.	1939	L	353-701	"G" Monel	66.73	29.76	2.50 Al, 0.35 Fe, 0.25 Si, 0.20 C, and 0.21 Mn; rolled and annealed.
44	Aoyama, S. and Ito, T.	1940	L	78	No. 0	94.77	4.36	0.51 Co, 0.26 Mn, 0.08 Fe, 0.02 Al, 0.001 Sb, 0.0004 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, then machined to size; electrical resistivity 5.00 $\mu\Omega$ cm at 78 K.
45	Aoyama, S. and Ito, T.	1940	L	78	No. 1	90.43	8.85	0.49 Co, 0.13 Mn, 0.09 Fe, 0.02 Al, 0.001 Sb, 0.0007 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, machined to size; electrical resistivity 8.50 $\mu\Omega$ cm at 78 K.
46	Aoyama, S. and Ito, T.	1940	L	78	No. 2	85.62	13.71	0.46 Co, 0.10 Mn, 0.094 Fe, 0.017 Al, 0.002 Sb, 0.001 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, machined to size; electrical resistivity 12.2 $\mu\Omega$ cm at 78 K.
47	Aoyama, S. and Ito, T.	1940	L	78	No. 3	77.73	21.69	0.414 Co, 0.091 Fe, 0.05 Mn, 0.015 Al, 0.003 Sb, 0.0015 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, machined to size; electrical resistivity 16.1 $\mu\Omega$ cm at 78 K.
48	Aoyama, S. and Ito, T.	1940	L	78	No. 4	69.14	30.35	0.37 Co, 0.05 Si, 0.068 Fe, 0.014 Al, 0.005 Sb, 0.0021 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, machined to size; electrical resistivity 28.0 $\mu\Omega$ cm at 78 K.
49	Aoyama, S. and Ito, T.	1940	L	78	No. 5	58.96	40.53	0.314 Co, 0.104 Fe, 0.012 Al, 0.04 Mn, 0.006 Sb, 0.0028 S, and trace Pb (calculated composition); 4.00 mm diameter and 60.0 mm long; cast, hot-rolled, machined to size; electrical resistivity 47.7 $\mu\Omega$ cm at 78 K.

#### 4.5. Copper-Palladium Alloy System

The copper-palladium system forms a continuous series of solid solutions over the entire range of compositions. Ordered structures are formed at temperatures below about 775 K for compositions ranging from slightly below 10 to somewhat above 25 At.% (16 to 36%) palladium and at temperatures below about 975 K for compositions ranging from slightly below 30 to somewhat above 50 At.% (42 to 63%) palladium. The maxima of the temperatures of transformation suggest that these ordered structures are based on  $\text{PdCu}_5$  and  $\text{Pd}_3\text{Cu}_5$  respectively. In this connection, it should be noted that curves 2 and 3 of the Cu + Pd alloys and curves 3, 5, 6, 12, 13, 14, 15, 22, 23, 24, and 25 of the Pd + Cu alloys are values obtained from specimens which were in a partially ordered state.

There are 49 sets of experimental data available for the thermal conductivity of this alloy system. However, of the 19 data sets available for Cu + Pd alloys listed in Table 15 and shown in Figure 23, 14 sets are merely single data points around room temperature, and of the 30 data sets for Pd + Cu alloys listed in Table 16 and shown in Figure 24, 19 sets are single data points around room temperature.

The thermal conductivity of these alloys was first investigated by Sedström [178, 179] who measured the thermal conductivity at 273 K of 14 specimens ranging from 3.5 to 93% Pd and the thermal conductivity at 323 K of 17 specimens ranging from 8.41 to 93.19% Pd. Later Grüneisen and Reddemann [61] measured the low temperature thermal conductivity of specimens containing 10.3, 57.8, 62.7, and 90.8% Pd (Cu + Pd curve 1 and Pd + Cu curves 1-5) and it was found that prolonged annealing just below the order-disorder transition temperature produced a 6-fold increase in the thermal conductivity at 80 K of the specimen containing 57.8% Pd. More recently, Pott [82] measured the thermal conductivity of specimens containing 24.18, 35.82, 52.75, 57.81, and 70.67% Pd at temperatures ranging from 293 to 1073 K. The first four specimens were measured both in the disordered state and after prolonged annealing just below the transition temperature (Cu + Pd curves 2-5 and Pd + Cu curves 6, 7, 9, and 10); the specimen containing 70.67% Pd was measured following two different heat treatments (Pd + Cu curves 8 and 10). The most recent measurement on alloys of this system was made in 1967 by Kierspe [83] (Cu + Pd curve 6) for a specimen containing 4.92% Pd at room temperature.

The low temperature experimental thermal conductivity values for disordered specimens are in satisfactory agreement with the values calculated from eqs. (12) and (35) for those compositions for which the  $k_g$  maximum occurs below 80 K. The investigation by Fletcher and Grieg [84] of the lattice thermal conductivity of palladium-silver alloys showed that the strong electron-phonon interaction in the palladium-rich alloys reduces the low temperature lattice thermal conductivity, causing its maximum to occur at much higher temperatures than in the silver-rich alloys. A similar elevation of the temperature of the

maximum of the lattice component is believed to occur in this alloy system. The discrepancy between the experimental and calculated values of the thermal conductivity at 80 K ranged from 2 to 12%, the calculated values being higher; the 12% discrepancy was with the specimen containing 57.8% Pd and the electrical resistivities reported for this specimen are 8% greater than those reported by other authors for this composition.

At ordinary temperatures Sedström's values for his disordered specimens tend to be lower than the calculated values, particularly for the more dilute alloys; this is not surprising in view of the fact that the electrical resistivities of these specimens are higher than those reported by other authors for the same nominal compositions. In this same temperature range the calculated values are within 3% of Kierspe's value for a specimen containing 4.9% Pd and Pott's value for a specimen containing 57.8% Pd. On the other hand, the calculated values were 16% below Pott's value for a specimen containing 24.18% Pd and 28% below his value for a specimen containing 70.67% Pd. After correcting for the lattice component, corresponding Lorenz ratios for these specimens are respectively 22 and 36% greater than the classical value; it is unlikely that band structure effects could cause such large deviations from the classical value for these alloys at 300 K.

At higher temperatures there are four large discrepancies between the calculated and experimental values, ranging from 30 to 40%. Three of these are with the 70.67% Pd specimen mentioned above and are associated with Lorenz ratios 33 to 38% greater than the classical value; the other discrepancy is with Pott's specimen containing 57.8% Pd and the corresponding Lorenz ratio is 36% greater than the classical value. While heavy alloying with a noble element would presumably reduce band structure effects, these Lorenz ratios are larger than those obtained by Laubitz and Matsumura [10] for pure palladium. Also, they are very much larger than those obtained by Laubitz and van der Meer [85] for a gold alloy with 34.95% Pd in which comparable band structure effects might be expected. Further experimental work on the palladium-rich alloys of this system is clearly in order. Until there is additional experimental evidence or some theoretical support for these very large Lorenz ratios it seems safer to use evidence from similar systems rather than the thermal conductivities associated with these Lorenz ratios as a guide in recommending values.

The recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 14 for 25 alloy compositions. These values are for well-annealed disordered alloys. The values for  $k$  are also shown in Figures 21 and 22. The  $k_e$  values cover the full temperature range from 4 to 1200 K, but  $k$  and  $k_g$  values are not given at very low temperatures. The values of residual electrical resistivity for the alloys are also given in Table 14. The uncertainties of the  $k$  values are stated in a footnote to Table 14, and those of the  $k_e$  and  $k_g$  values are of the order of  $\pm 10$  to  $\pm 15\%$ .

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM<sup>†</sup>[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 99.99% (99.79 At.%) Pd: 0.01% (0.20 At.%)				Cu: 99.00% (99.40 At.%) Pd: 1.00% (0.60 At.%)				Cu: 97.00% (98.19 At.%) Pd: 3.00% (1.81 At.%)				Cu: 95.00% (96.95 At.%) Pd: 5.00% (3.05 At.%)			
$\rho_0 = 0.2000 \mu\Omega\text{cm}$				$\rho_0 = 0.500 \mu\Omega\text{cm}$				$\rho_0 = 1.920 \mu\Omega\text{cm}$				$\rho_0 = 2.700 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.349		4		0.168		4		0.0603		4		0.0362	
6		0.504		6		0.253		6		0.0905		6		0.0543	
8		0.606		8		0.337		8		0.121		8		0.0734	
10		0.673		10		0.421		10		0.151		10		0.0905	
15		1.31		15		0.632		15		0.236		15		0.136	
20		1.75		20		0.943		20		0.302		20		0.181	
25		2.05		25		1.04		25		0.376		25		0.226	
30		2.44		30		1.24		30		0.450		30		0.270	
40		3.11		40		1.89		40		0.691		40		0.389	
50	3.69*	3.26	0.324	50	2.19*	1.87	0.277	50	0.917*	0.713	0.204	50	0.815*	0.442	0.173
60	3.89*	3.27	0.316	60	2.25*	1.96	0.267	60	1.01*	0.820	0.194	60	0.890*	0.516	0.163
70	3.48*	3.14	0.397	70	2.29*	2.04	0.258	70	1.09*	0.905	0.184	70	0.738*	0.582	0.155
80	3.53*	3.07	0.397	80	2.29*	2.05	0.248	80	1.19*	0.975	0.176	80	0.791*	0.644	0.147
90	3.29*	2.97	0.294	90	2.35*	2.11	0.239	90	1.23*	1.05	0.168	90	0.845*	0.705	0.140
100	3.29*	2.95	0.275	100	2.41*	2.18	0.239	100	1.29*	1.12	0.161	100	0.895*	0.761	0.134
150	3.31*	2.69	0.235	150	2.73*	2.53	0.190	150	1.60*	1.46	0.133	150	1.16*	1.04	0.110
200	3.40*	2.37	0.188	200	2.90*	2.74	0.161	200	1.83*	1.71	0.114	200	1.38*	1.26	0.0947
250	3.40*	2.32	0.160	250	3.06*	2.91	0.139	250	2.03*	1.93	0.100	250	1.53*	1.45	0.0834
273	3.50*	3.40	0.150	273	3.00*	2.95	0.131	273	2.11*	2.02	0.0949	273	1.61	1.53	0.0792
300	3.54*	3.40	0.140	300	3.10*	3.04	0.122	300	2.24*	2.15	0.0895	300	1.69	1.61	0.0748
350	3.59*	3.44	0.123	350	3.23*	3.12	0.109	350	2.31*	2.23	0.0811	350	1.82	1.75	0.0681
400	3.59*	3.45	0.110	400	3.30*	3.20	0.0987	400	2.43*	2.35	0.0743	400	1.93*	1.86	0.0626
500	3.64*	3.05	0.0913	500	3.26*	3.27	0.0828	500	2.60*	2.54	0.0636	500	2.15*	2.09	0.0542
600	3.59*	2.90	0.0778	600	3.37*	3.29	0.0713	600	2.73*	2.66	0.0561	600	2.26*	2.23	0.0481
700	3.59*	2.81	0.0677	700	3.37*	3.31	0.0637	700	2.81*	2.76	0.0502	700	2.40*	2.35	0.0433
800	3.59*	2.44	0.0599	800	3.20*	3.20	0.0559	800	2.94*	2.89	0.0455	800	2.49*	2.44	0.0395
900	3.47*	2.41	0.0503	900	3.31*	3.26	0.0495	900	2.89*	2.84	0.0416	900	2.53*	2.49	0.0353
1000	3.49*	2.37	0.0400	1000	3.29*	3.24	0.0400	1000	2.86*	2.84	0.0383	1000	2.56*	2.52	0.0327
1100	3.30*	2.25	0.0445	1100	3.20*	3.22	0.0423	1100	2.80*	2.85	0.0386	1100	2.59*	2.55	0.0314
1200	3.31*	2.37	0.0411	1200	3.31*	3.17	0.0391	1200	2.97*	2.94	0.0332	1200	2.59*	2.56	0.0294

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:99.99 Cu - 0.09 Pd:  $\pm 10\%$ .99.00 Cu - 1.00 Pd:  $\pm 10\%$ .97.00 Cu - 3.00 Pd:  $\pm 10\%$ .95.00 Cu - 5.00 Pd:  $\pm 10\%$ .

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued) †  
 † Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>

Cu: 50.00% (82.76 At.%) Pd: 10.00% (6.22 At.%)				Cu: 85.00% (90.47 At.%) Pd: 15.00% (9.53 At.%)				Cu: 60.00% (67.01 At.%) Pd: 20.00% (12.99 At.%)				Cu: 75.00% (82.40 At.%) Pd: 25.00% (16.60 At.%)			
$\rho_0 = 5.32 \mu\Omega\text{cm}$				$\rho_0 = 7.91 \mu\Omega\text{cm}$				$\rho_0 = 10.43 \mu\Omega\text{cm}$				$\rho_0 = 12.90 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.0124		4		0.0124		4		0.00937		4		0.00768	
6		0.0276		6		0.0185		6		0.0141		6		0.0114	
8		0.0387		8		0.0247		8		0.0187		8		0.0152	
10		0.0459		10		0.0309		10		0.0234		10		0.0189	
15		0.0609		15		0.0463		15		0.0351		15		0.0284	
20		0.0716		20		0.0618		20		0.0468		20		0.0379	
25		0.114		25		0.0771		25		0.0585		25		0.0473	
30		0.137		30		0.0824		30		0.0702		30		0.0567	
40		0.181		40		0.123		40		0.0934		40		0.0755	
50	0.300	0.235	0.136	50	0.267*	0.152	0.115	50	0.218*	0.116	0.102	50	0.186*	0.0839	0.0925
60	0.293	0.267	0.136	60	0.269*	0.181	0.107	60	0.233*	0.136	0.0945	60	0.196*	0.112	0.0857
70	0.424	0.305	0.119	70	0.306*	0.208	0.100	70	0.249*	0.160	0.0886	70	0.210*	0.130	0.0902
80	0.455	0.343	0.113	80	0.339*	0.234	0.0947	80	0.265*	0.161	0.0835	80	0.233*	0.147	0.0756
90	0.485	0.379	0.107	90	0.351*	0.261	0.0899	90	0.281*	0.202	0.0792	90	0.236*	0.164	0.0717
100	0.516*	0.414	0.102	100	0.373*	0.287	0.0857	100	0.299*	0.223	0.0755	100	0.249*	0.181	0.0682
150	0.600*	0.595	0.0837	150	0.494*	0.414	0.0703	150	0.396*	0.324	0.0618	150	0.321*	0.245	0.0568
200	0.515*	0.743	0.0719	200	0.593*	0.533	0.0604	200	0.472*	0.419	0.0532	200	0.393*	0.345	0.0480
250	0.369*	0.867	0.0636	250	0.690*	0.644	0.0534	250	0.557*	0.510	0.0471	250	0.465*	0.422	0.0425
273	1.91	0.945	0.0604	273	0.742	0.692	0.0509	273	0.594	0.549	0.0448	273	0.496	0.456	0.0405
300	1.07	1.01	0.0872	300	0.796	0.746	0.0482	300	0.636	0.596	0.0425	300	0.533	0.494	0.0384
350	1.18	1.13	0.0822	350	0.896	0.848	0.0441	350	0.715	0.676	0.0389	350	0.599	0.564	0.0352
400	1.28*	1.24	0.0482	400	0.971*	0.930	0.0408	400	0.787*	0.751	0.0360	400	0.662	0.629	0.0326
500	1.47*	1.43	0.0451	500	1.13*	1.10	0.0357	500	0.924*	0.893	0.0316	500	0.782	0.753	0.0287
600	1.63*	1.59	0.0375	600	1.27*	1.24	0.0319	600	1.05*	1.02	0.0283	600	0.895	0.869	0.0257
700	1.77*	1.73	0.0340	700	1.40*	1.37	0.0290	700	1.17*	1.14	0.0258	700	1.00	0.979	0.0235
800	1.90*	1.85	0.0313	800	1.51*	1.48	0.0267	800	1.27*	1.25	0.0238	800	1.10	1.08	0.0216
900	1.97*	1.94	0.0289	900	1.61*	1.58	0.0248	900	1.36*	1.34	0.0221	900	1.19	1.17	0.0201
1000	2.04*	2.01	0.0270	1000	1.69*	1.66	0.0232	1000	1.45*	1.43	0.0207	1000	1.27	1.25	0.0189
1100	2.06*	2.07	0.0253	1100	1.75*	1.73	0.0218	1100	1.52*	1.50	0.0195	1100	1.36*	1.33	0.0178
1200	2.14*	2.11	0.0238	1200	1.80*	1.78	0.0206	1200	1.59*	1.56	0.0184	1200	1.42*	1.40	0.0168

† Uncertainties of the total thermal conductivity, k, are as follows:

50.00 Cu - 10.00 Pd  $\pm 10\%$

60.00 Cu - 15.00 Pd  $\pm 10\%$

75.00 Cu - 25.00 Pd  $\pm 10\%$

85.00 Cu - 15.00 Pd  $\pm 10\%$

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued) †  
 (Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>)

Cu: 70.00% (78.62 At.%) Pd: 30.00% (20.38 At.%) $\rho_0 = 15.30 \mu\Omega\text{cm}$				Cu: 65.00% (75.67 At.%) Pd: 35.00% (24.33 At.%) $\rho_0 = 17.68 \mu\Omega\text{cm}$				Cu: 60.00% (71.52 At.%) Pd: 40.00% (23.48 At.%) $\rho_0 = 20.01 \mu\Omega\text{cm}$				Cu: 55.00% (67.18 At.%) Pd: 45.00% (32.82 At.%) $\rho_0 = 22.60 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.00639		4		0.00553		4		0.00488		4		0.00432	
6		0.00958		6		0.00829		6		0.00733		6		0.00649	
8		0.0128		8		0.0111		8		0.00977		8		0.00865	
10		0.0160		10		0.0138		10		0.0122		10		0.0108	
15		0.0240		15		0.0207		15		0.0183		15		0.0162	
20		0.0319		20		0.0276		20		0.0244		20		0.0216	
25		0.0399		25		0.0345		25		0.0305		25		0.0270	
30		0.0478		30		0.0414		30		0.0366		30		0.0324	
40		0.0636		40		0.0551		40		0.0487		40		0.0431	
50	0.185*	0.0791	0.0655	50	0.149*	0.0688	0.0799	50	0.136*	0.0606	0.0756	50	0.126*	0.0537	0.0721
60	0.174*	0.0945	0.0791	60	0.156*	0.0822	0.0739	60	0.143*	0.0724	0.0688	60	0.131*	0.0642	0.0685
70	0.183*	0.109	0.0739	70	0.164*	0.0953	0.0691	70	0.149*	0.0840	0.0652	70	0.137*	0.0745	0.0621
80	0.194*	0.125	0.0696	80	0.173*	0.108	0.0650	80	0.157*	0.0955	0.0613	80	0.143*	0.0847	0.0584
90	0.205*	0.139	0.0650	90	0.183*	0.121	0.0615	90	0.165*	0.107	0.0580	90	0.150*	0.0948	0.0553
100	0.217*	0.154	0.0608	100	0.193*	0.134	0.0585	100	0.173*	0.118	0.0552	100	0.158*	0.105	0.0526
150	0.276*	0.226	0.0514	150	0.246*	0.198	0.0479	150	0.219*	0.174	0.0451	150	0.198*	0.155	0.0439
200	0.339*	0.295	0.0442	200	0.300*	0.259	0.0412	200	0.267*	0.239	0.0388	200	0.240*	0.203	0.0369
250	0.401*	0.362	0.0392	250	0.364*	0.317	0.0365	250	0.318*	0.281	0.0344	250	0.283*	0.250	0.0338
273	0.430*	0.391	0.0373	273	0.378	0.344	0.0348	273	0.338	0.305	0.0328	273	0.302	0.271	0.0312
300	0.462*	0.426	0.0354	300	0.407	0.374	0.0330	300	0.363	0.332	0.0311	300	0.325	0.296	0.0297
350	0.530*	0.497	0.0325	350	0.459	0.428	0.0303	350	0.410	0.381	0.0286	350	0.367	0.340	0.0272
400	0.575*	0.545	0.0301	400	0.509	0.481	0.0281	400	0.454*	0.428	0.0265	400	0.407*	0.382	0.0252
500	0.683*	0.657	0.0264	500	0.608	0.583	0.0247	500	0.542*	0.519	0.0233	500	0.485*	0.463	0.0222
600	0.836*	0.802	0.0238	600	0.701	0.678	0.0222	600	0.627*	0.606	0.0210	600	0.561*	0.541	0.0200
700	0.985*	0.960	0.0217	700	0.790*	0.770	0.0203	700	0.707*	0.688	0.0192	700	0.633*	0.615	0.0183
800	0.972*	0.953	0.0200	800	0.873	0.854	0.0187	800	0.782*	0.764	0.0177	800	0.701*	0.685	0.0169
900	1.05*	1.04	0.0186	900	0.948	0.931	0.0175	900	0.853*	0.837	0.0165	900	0.765*	0.749	0.0157
1000	1.13*	1.11	0.0175	1000	1.02	1.00	0.0164	1000	0.920*	0.904	0.0155	1000	0.825*	0.810	0.0148
1100	1.20*	1.18	0.0165	1100	1.09	1.07	0.0154	1100	0.982*	0.967	0.0146	1100	0.881*	0.867	0.0140
1200	1.26*	1.25	0.0156	1200	1.15*	1.14	0.0146	1200	1.04*	1.03	0.0139	1200	0.933*	0.920	0.0132

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

70.00 Cu - 30.00 Pd:  $\pm 10\%$   
 65.00 Cu - 35.00 Pd:  $\pm 10\%$   
 60.00 Cu - 40.00 Pd:  $\pm 10\%$   
 55.00 Cu - 45.00 Pd:  $\pm 10\%$

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 50.00% (52.51 At.%) Pd: 50.00% (57.59 At.%)				Cu: 45.00% (57.81 At.%) Pd: 55.00% (42.19 At.%)				Cu: 40.00% (52.75 At.%) Pd: 60.00% (47.25 At.%)				Cu: 35.00% (47.41 At.%) Pd: 65.00% (52.59 At.%)			
$\rho_0 = 25.53 \mu\Omega\text{cm}$				$\rho_0 = 29.00 \mu\Omega\text{cm}$				$\rho_0 = 32.63 \mu\Omega\text{cm}$				$\rho_0 = 40.00 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.00263		4		0.00337		4		0.00300		4		0.00344	
6		0.00374		6		0.00505		6		0.00449		6		0.00386	
8		0.00766		8		0.00674		8		0.00599		8		0.00459	
10		0.00957		10		0.00842		10		0.00749		10		0.00611	
15		0.0144		15		0.0126		15		0.0112		15		0.00916	
20		0.0191		20		0.0168		20		0.0150		20		0.0122	
25		0.0239		25		0.0210		25		0.0186		25		0.0152	
30		0.0287		30		0.0252		30		0.0223		30		0.0182	
40		0.0351		40		0.0326		40		0.0296		40		0.0242	
50	0.117*	0.0476	0.0093	50		0.0419		50		0.0369		50		0.0301	
60	0.121*	0.0626	0.0240	60	0.113*	0.0500	0.0630	60		0.0440		60		0.0360	
70	0.126*	0.0839	0.0397	70	0.116*	0.0590	0.0578	70	0.108	0.0511	0.0565	70		0.0419	
80	0.131*	0.0750	0.0561	80	0.130	0.0660	0.0544	80	0.111	0.0582	0.0531	80	0.100	0.0477	0.0525
90	0.137*	0.0940	0.0631	90	0.125	0.0740	0.0514	90	0.115	0.0652	0.0503	90	0.103	0.0535	0.0496
100	0.143*	0.0929	0.0806	100	0.131*	0.0819	0.0489	100	0.120*	0.0722	0.0478	100	0.106*	0.0591	0.0471
150	0.176*	0.137	0.0412	150	0.161*	0.121	0.0399	150	0.145*	0.106	0.0350	150	0.126*	0.0672	0.0385
200	0.213*	0.180	0.0555	200	0.182*	0.158	0.0343	200	0.172*	0.139	0.0335	200	0.148*	0.114	0.0321
250	0.253*	0.222	0.0315	250	0.225*	0.195	0.0305	250	0.200*	0.170	0.0297	250	0.170*	0.141	0.0263
273	0.289	0.239	0.0300	273	0.240	0.211	0.0290	273	0.212	0.184	0.0283	273	0.181	0.158	0.0279
300	0.289	0.260	0.0265	300	0.257	0.230	0.0276	300	0.227	0.200	0.0269	300	0.193	0.167	0.0265
350	0.325	0.299	0.0261	350	0.289	0.263	0.0253	350	0.254	0.230	0.0247	350	0.216	0.192	0.0243
400	0.361	0.337	0.0242	400	0.320	0.296	0.0235	400	0.281	0.258	0.0229	400	0.239*	0.216	0.0226
500	0.430	0.409	0.0213	500	0.379	0.359	0.0207	500	0.333	0.312	0.0202	500	0.283*	0.263	0.0199
600	0.497	0.477	0.0192	600	0.437	0.418	0.0186	600	0.382	0.363	0.0182	600	0.325*	0.307	0.0179
700	0.561	0.543	0.0176	700	0.492	0.475	0.0170	700	0.429	0.413	0.0166	700	0.366*	0.350	0.0164
800	0.622	0.605	0.0162	800	0.545	0.529	0.0157	800	0.475	0.460	0.0154	800	0.407*	0.392	0.0151
900	0.680	0.663	0.0151	900	0.596	0.581	0.0147	900	0.530	0.506	0.0143	900	0.448*	0.433	0.0141
1000	0.734	0.729	0.0142	1000	0.645	0.631	0.0138	1000	0.563	0.549	0.0134	1000	0.488*	0.474	0.0132
1100	0.786	0.773	0.0134	1100	0.691	0.678	0.0130	1100	0.604	0.591	0.0127	1100	0.529*	0.516	0.0125
1200	0.836*	0.822	0.0127	1200	0.734*	0.722	0.0123	1200	0.643*	0.631	0.0120	1200	0.570*	0.558	0.0119

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:50.00 Cu - 50.00 Pd:  $\pm 10\%$ 45.00 Cu - 55.00 Pd:  $\pm 10\%$ 40.00 Cu - 60.00 Pd:  $\pm 10\%$ 35.00 Cu - 65.00 Pd:  $\pm 10\%$ 

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 30.00% (41.78 At.%) Pd: 70.00% (58.22 At.%)			Cu: 25.00% (35.82 At.%) Pd: 75.00% (64.18 At.%)			Cu: 20.00% (29.51 At.%) Pd: 80.00% (70.49 At.%)			Cu: 15.00% (22.81 At.%) Pd: 85.00% (77.19 At.%)		
$\rho_0 = 44.19 \mu\Omega\text{cm}$			$\rho_0 = 42.40 \mu\Omega\text{cm}$			$\rho_0 = 36.26 \mu\Omega\text{cm}$			$\rho_0 = 28.68 \mu\Omega\text{cm}$		
T	k	$k_e$ $k_g$	T	k	$k_e$ $k_g$	T	k	$k_e$ $k_g$	T	k	$k_e$ $k_g$
4		0.00231	4		0.00231	4		0.00270	4		0.00341
6		0.00332	6		0.00346	6		0.00404	6		0.00511
8		0.00442	8		0.00461	8		0.00539	8		0.00682
10		0.00553	10		0.00576	10		0.00674	10		0.00852
15		0.00839	15		0.00864	15		0.0101	15		0.0128
20		0.0111	20		0.0115	20		0.0135	20		0.0170
25		0.0137	25		0.0142	25		0.0165	25		0.0207
30		0.0165	30		0.0170	30		0.0196	30		0.0247
40		0.0219	40		0.0226	40		0.0261	40		0.0325
50		0.0273	50		0.0281	50		0.0323	50		0.0400
60		0.0326	60		0.0335	60		0.0394	60		0.0473
70		0.0379	70		0.0388	70		0.0444	70		0.0545
80		0.0432	80		0.0441	80		0.0503	80		0.0615
90		0.0485	90		0.0494	90		0.0561	90		0.0684
100		0.0535	100		0.0547	100		0.0619	100		0.0752
150	0.117*	0.0790 0.0364	150	0.119*	0.0801 0.0388	150		0.0893	150		0.107
200	0.137*	0.104 0.0330	200	0.130*	0.106 0.0334	200	0.150*	0.115	200	0.172*	0.136
250	0.157*	0.126 0.0292	250	0.150*	0.129 0.0296	250	0.171*	0.140	250	0.195*	0.163
300	0.167	0.139 0.0279	300	0.168	0.139 0.0282	300	0.180	0.151	300	0.206	0.175
350	0.176	0.152 0.0264	350	0.179	0.152 0.0267	350	0.192	0.164	350	0.218	0.189
400	0.199	0.175 0.0243	400	0.200	0.176 0.0245	400	0.214	0.189	400	0.242	0.215
450	0.220	0.196 0.0225	450	0.222	0.199 0.0227	450	0.236*	0.213	450	0.265*	0.240
500	0.242	0.219 0.0196	500	0.244	0.220 0.0200	500	0.260*	0.239	500	0.311*	0.289
550	0.263	0.235 0.0178	550	0.266	0.238 0.0180	550	0.323*	0.304	550	0.356*	0.336
600	0.283	0.257 0.0163	600	0.306	0.268 0.0164	600	0.366*	0.349	600	0.400*	0.383
700	0.343*	0.317 0.0151	700	0.347*	0.331 0.0152	700	0.408*	0.393	700	0.443*	0.427
800	0.383	0.359 0.0140	800	0.388	0.373 0.0142	800	0.450*	0.436	800	0.486*	0.470
900	0.423	0.406 0.0132	900	0.430	0.415 0.0133	900	0.492*	0.478	900	0.526*	0.511
1000	0.461	0.446 0.0124	1000	0.470	0.457 0.0125	1000	0.534*	0.521	1000	0.566*	0.553
1100	0.502	0.489 0.0118	1100	0.513	0.500 0.0119	1100	0.578*	0.566	1100	0.607*	0.594
1200	0.543*	0.531 0.0118	1200	0.550*	0.544 0.0119	1200			1200		

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

20.00 Cu - 70.00 Pd:  $\pm 15\%$

25.00 Cu - 75.00 Pd:  $\pm 15\%$

30.00 Cu - 80.00 Pd:  $\pm 15\%$

15.00 Cu - 85.00 Pd:  $\pm 15\%$

\* In temperature range where no experimental thermal conductivity data are available.



TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 10.00% (15.69 At. %) Pd: 90.00% (84.31 At. %)				Cu: 5.00% (8.10 At. %) Pd: 95.00% (91.90 At. %)				Cu: 3.00% (4.92 At. %) Pd: 97.00% (95.08 At. %)				Cu: 1.00% (1.66 At. %) Pd: 99.00% (98.34 At. %)			
$\rho_0 = 20.10 \mu\Omega\text{cm}$				$\rho_0 = 10.31 \mu\Omega\text{cm}$				$\rho_0 = 6.20 \mu\Omega\text{cm}$				$\rho_0 = 2.100 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.00406		4		0.00948		4		0.0158		4		0.0465	
6		0.00729		6		0.0142		6		0.0236		6		0.0888	
8		0.00972		8		0.0190		8		0.0315		8		0.0931	
10		0.0122		10		0.0237		10		0.0394		10		0.116	
15		0.0182		15		0.0355		15		0.0591		15		0.175	
20		0.0243		20		0.0474		20		0.0786		20		0.233	
25		0.0304		25		0.0572		25		0.0939		25		0.276	
30		0.0360		30		0.0676		30		0.113		30		0.315	
40		0.0489		40		0.0871		40		0.143		40		0.364	
50		0.0602		50		0.105		50		0.167		50		0.382	
60		0.0690		60		0.120		60		0.214		60		0.389	
70		0.0755		70		0.135		70		0.230		70		0.397	
80		0.0849		80		0.149		80		0.246		80		0.407	
90		0.0940		90		0.162		90		0.261		90		0.417	
100		0.103		100		0.175		100		0.273		100		0.432	
150		0.141		150		0.223		150		0.294		150		0.441	
200	0.216*	0.175	0.0407	200	0.312*	0.261	0.0509	200		0.329		200		0.454	
250	0.341*	0.266	0.0360	250	0.337*	0.293	0.0448	250	0.411*	0.358	0.0533	250	0.547*	0.471	0.0762
273	0.332	0.218	0.0342	273	0.348	0.305	0.0426	273	0.421*	0.371	0.0505	273	0.553*	0.481	0.0719
300	0.366	0.234	0.0324	300	0.362	0.322	0.0403	300	0.435*	0.387	0.0477	300	0.562*	0.494	0.0676
350	0.233	0.262	0.0297	350	0.389	0.352	0.0367	350	0.462*	0.419	0.0434	350	0.585*	0.534	0.0608
400	0.317*	0.299	0.0274	400	0.415*	0.381	0.0339	400	0.486*	0.446	0.0399	400	0.605*	0.549	0.0554
500	0.369*	0.343	0.0240	500	0.465*	0.436	0.0295	500	0.533*	0.499	0.0346	500	0.646*	0.599	0.0471
600	0.413*	0.391	0.0215	600	0.515*	0.489	0.0263	600	0.579*	0.548	0.0307	600	0.690*	0.649	0.0411
700	0.469*	0.436	0.0196	700	0.559*	0.535	0.0239	700	0.623*	0.595	0.0277	700	0.731*	0.694	0.0365
800	0.499*	0.491	0.0190	800	0.661*	0.639	0.0219	800	0.665*	0.640	0.0253	800	0.770*	0.737	0.0339
900	0.541*	0.535	0.0168	900	0.641*	0.621	0.0202	900	0.706*	0.682	0.0233	900	0.808*	0.778	0.0299
1000	0.581*	0.586	0.0157	1000	0.676*	0.657	0.0189	1000	0.743*	0.722	0.0216	1000	0.847*	0.819	0.0275
1100	0.621*	0.608	0.0145	1100	0.711*	0.693	0.0177	1100	0.775*	0.755	0.0202	1100	0.886*	0.861	0.0254
1200	0.669*	0.646	0.0140	1200	0.745*	0.728	0.0167	1200	0.810*	0.791	0.0190	1200	0.928*	0.903	0.0236

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

- 10.00 Cu - 90.00 Pd:  $\pm 15\%$   
 5.00 Cu - 95.00 Pd:  $\pm 15\%$   
 3.00 Cu - 97.00 Pd:  $\pm 15\%$   
 1.00 Cu - 99.00 Pd:  $\pm 15\%$

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 14. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 0.50% ( 0.53 At. %) Pd: 99.50% ( 99.47 At. %)					
$\rho_0 = 1.100 \mu\Omega\text{cm}$					
T	k	$k_e$	$k_g$		
4		0.0000			
6		0.133			
8		0.178			
10		0.222			
15		0.333			
20		0.444			
25		0.516			
30		0.567			
40		0.596			
50		0.602			
60		0.597			
70		0.539			
80		0.529			
90		0.530			
100		0.520			
150		0.504			
200		0.504			
250	0.000*	0.514	0.0023		
273	0.000*	0.521	0.0006		
300	0.015*	0.504	0.0009		
350	0.034*	0.502	0.0721		
400	0.050*	0.507	0.0499		
500	0.080*	0.604	0.0445		
600	0.120*	0.603	0.0409		
700	0.173*	0.731	0.0412		
800	0.210*	0.773	0.0397		
900	0.240*	0.816	0.0332		
1000	0.267*	0.867	0.0302		
1100	0.287*	0.899	0.0278		
1200	0.300*	0.940	0.0257		

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:  
 0.50 Cu - 99.50 Pd:  $\pm 1\%$ .

\* In temperature range where no experimental thermal conductivity data are available.

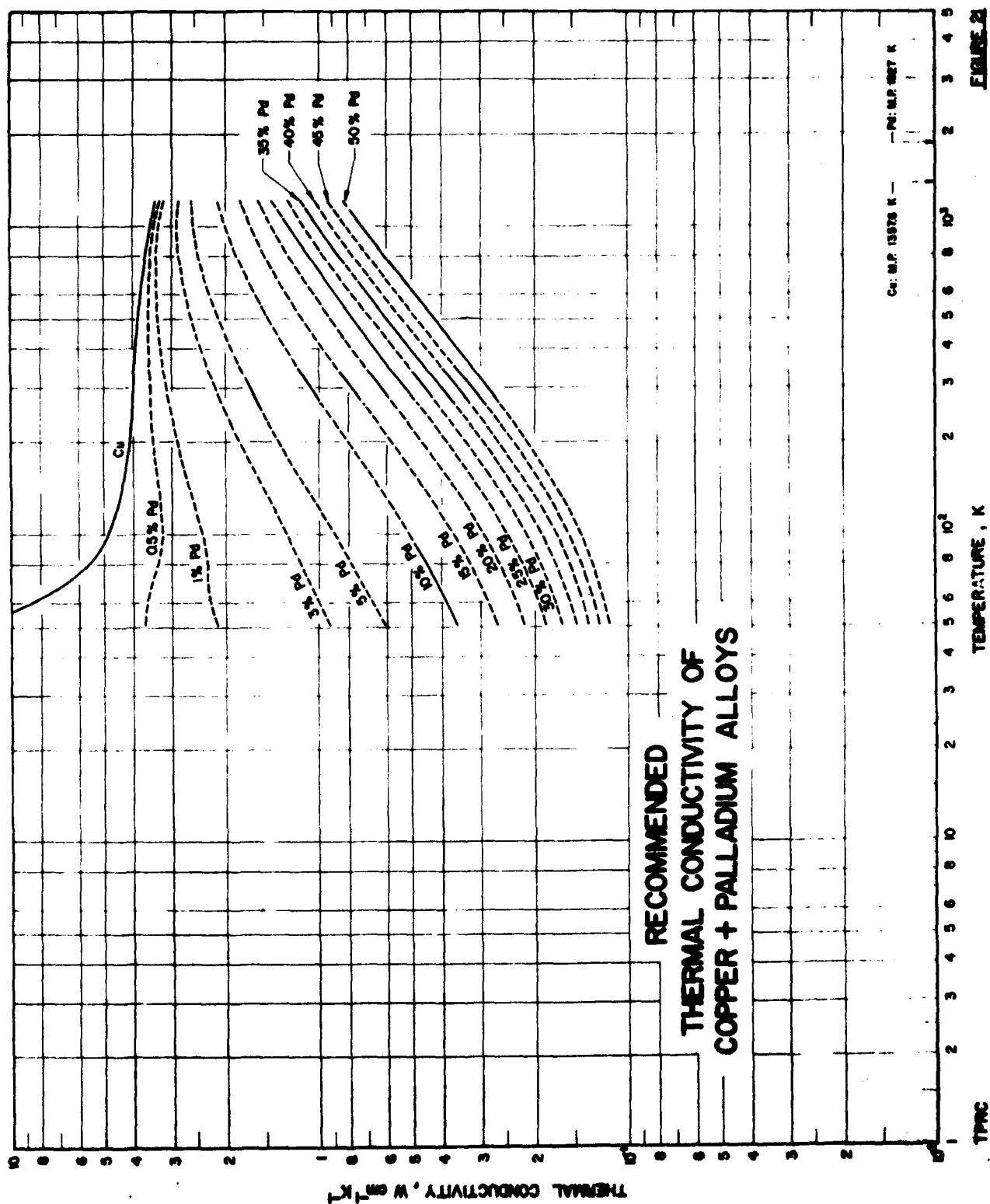


FIGURE 21

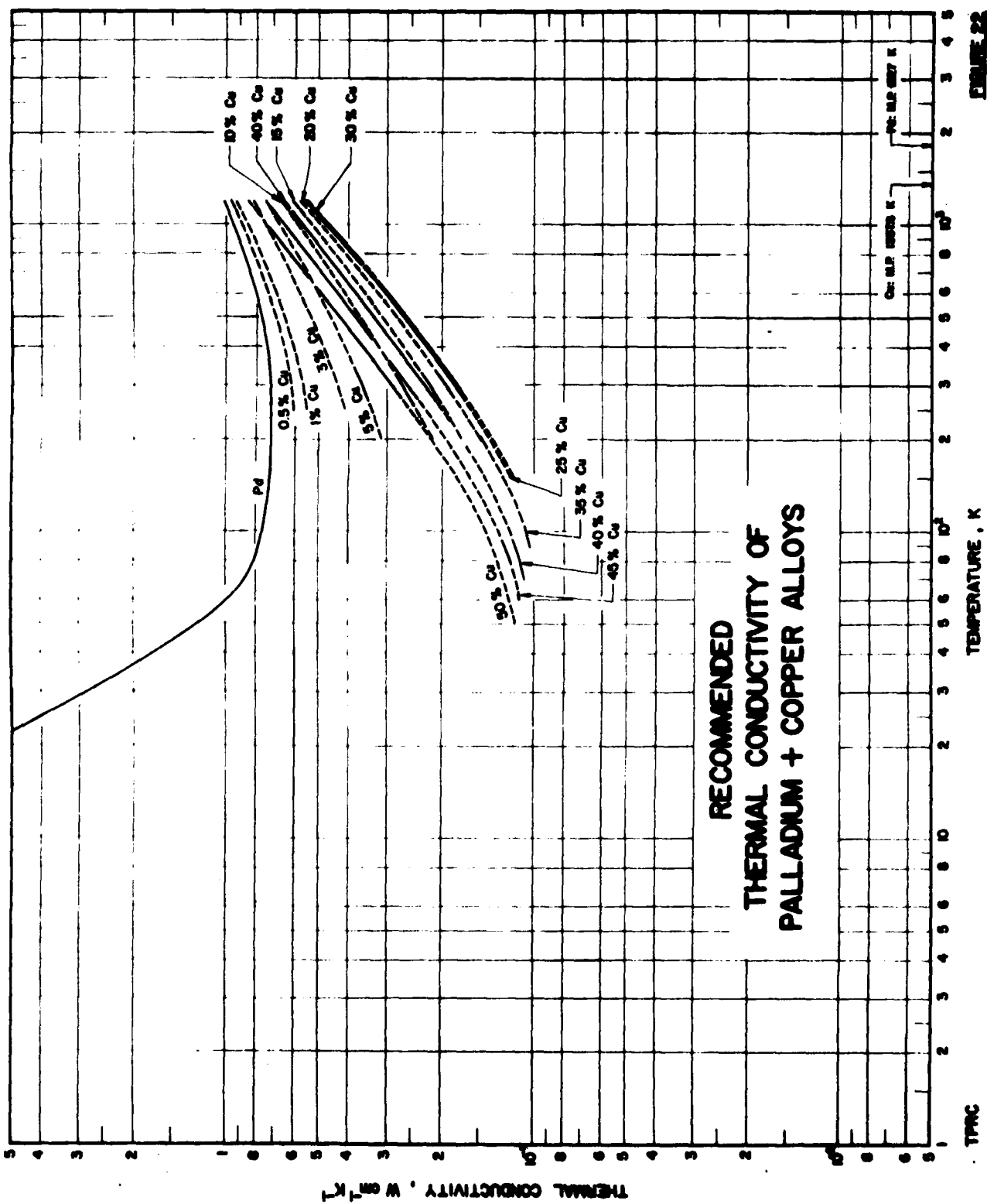


FIGURE 22

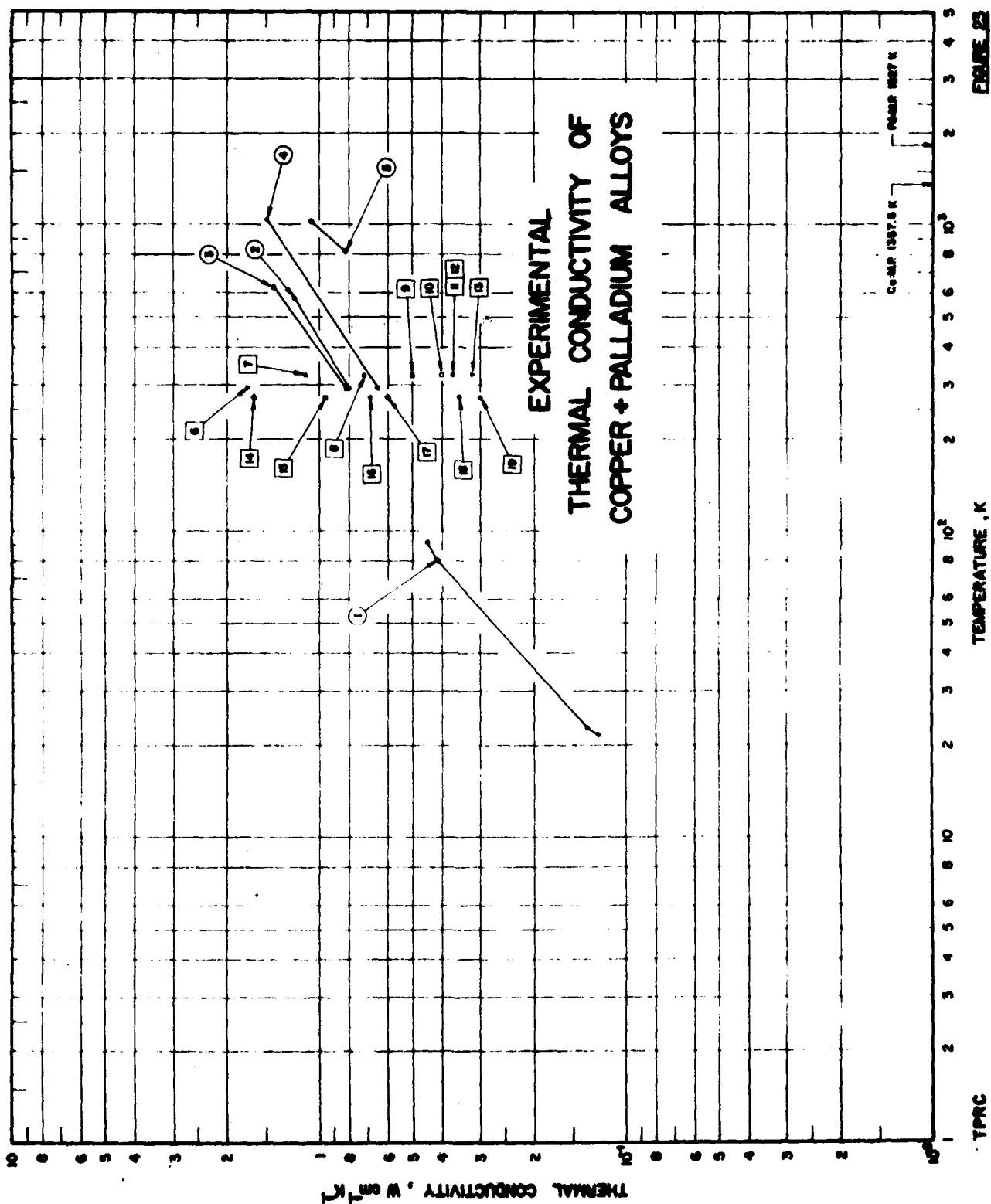


FIGURE 23

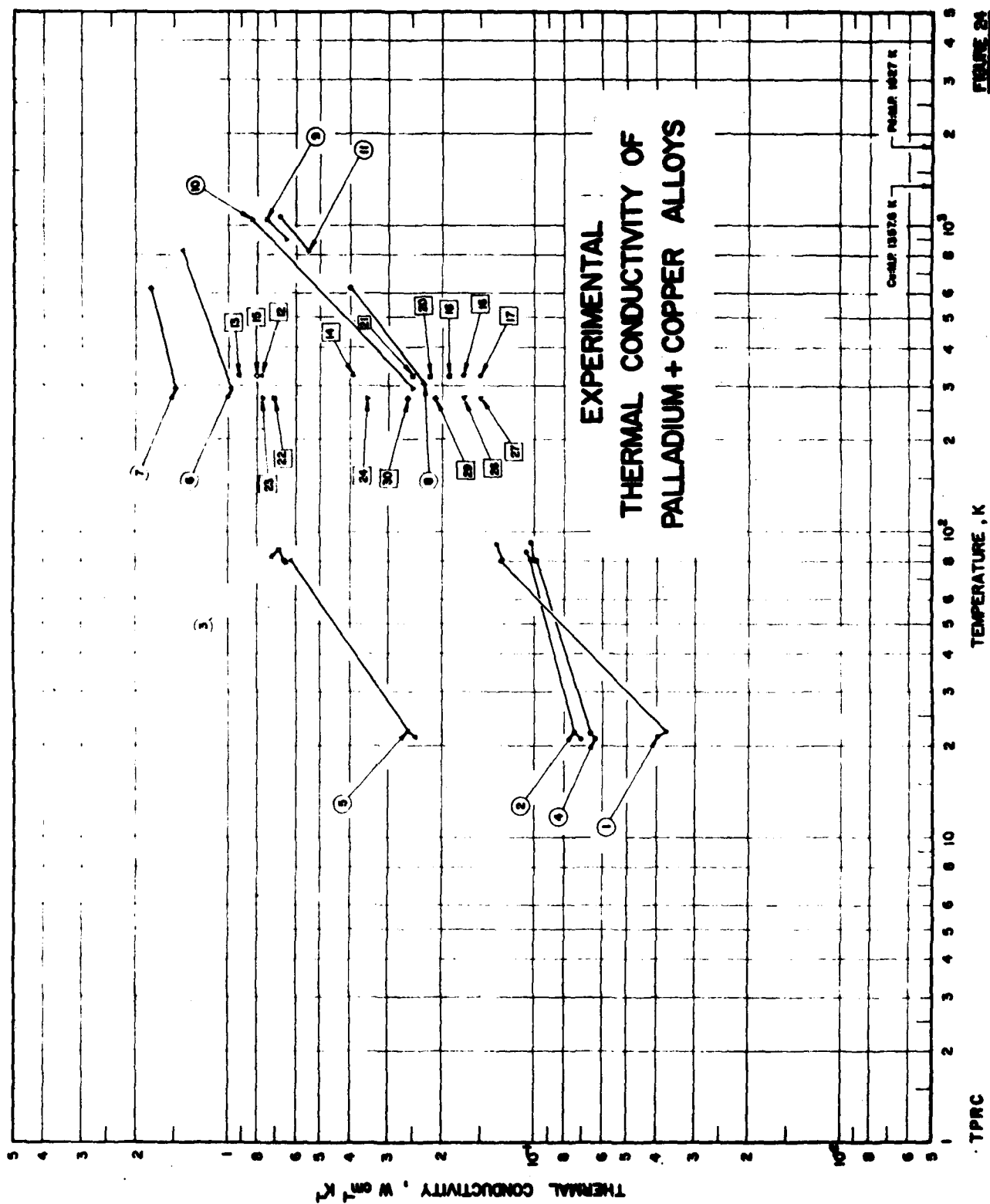


FIGURE 24

TABLE 15. THERMAL CONDUCTIVITY OF COPPER + PALLADIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Pd	Composition (continued), Specifications, and Remarks
1	Gränsen, E. and Reddemann, H.	1934	L	22-91	20	89.7	10.3 Calculated composition; polycrystalline; electrical resistivity 6.82, 5.508, and 5.184 $\mu\Omega$ cm at 0, -190, and -251 C, respectively.
2	Pott, F.P.	1966	L	293, 573			34.16 Calculated composition; annealed at 800 to 700 C for 2 hr; ordered; electrical resistivity 9.7, 12.4, and 13.9 $\mu\Omega$ cm at 36, 300, and 480 C, respectively.
3	Pott, F.P.	1966	L	293, 623			35.82 Similar to the above specimen except electrical resistivity 16.5, 12.9, and 15.2 $\mu\Omega$ cm at 34, 251, and 449 C, respectively.
4	Pott, F.P.	1966	L	293, 1048			24.16 Similar to the above specimen except disordered with electrical resistivity 14.2, 17.1, and 19.3 $\mu\Omega$ cm at 19, 441, and 779 C, respectively.
5	Pott, F.P.	1966	L	816, 1028			35.82 Similar to the above specimen except electrical resistivity 19.7, 22.4, and 25.6 $\mu\Omega$ cm at 25, 400, and 800 C, respectively.
6	Klarups, W.	1967	L	293.2			4.9 Cylindrical specimen; electrical resistivity 2.8982, 2.5865, 2.5901, 2.6052, 2.6379, 2.6849, 2.8092, 2.9047, 3.0440, 3.1847, 3.3258, 3.4636, 3.6005, 3.7351, 3.8703, 4.0055, 4.1351, and 4.2018 $\mu\Omega$ cm at 4.2, 10, 20, 30, 40, 50, 70, 83, 103, 123, 143, 163, 183, 203, 223, 243, 263, and 273 K, respectively.
7	Holgersson, S. and Sedström, E.	1924		323.2			8.41 Calculated composition (5.2 a/o Pd); electrical resistivity 6.8 $\mu\Omega$ cm at 50 C.
8	Holgersson, S. and Sedström, E.	1924		323.2			16.57 Calculated composition (10.6 a/o Pd); electrical resistivity 11.9 $\mu\Omega$ cm at 50 C.
9	Holgersson, S. and Sedström, E.	1924		323.2			22.40 Calculated composition (14.7 a/o Pd); electrical resistivity 15.4 $\mu\Omega$ cm at 50 C.
10	Holgersson, S. and Sedström, E.	1924		323.2			28.73 Calculated composition (19.4 a/o Pd); density 9.78 g cm <sup>-3</sup> ; electrical resistivity 18.8 $\mu\Omega$ cm at 50 C.
11	Holgersson, S. and Sedström, E.	1924		323.2			35.45 Calculated composition (24.7 a/o Pd); electrical resistivity 22.0 $\mu\Omega$ cm at 50 C.
12	Holgersson, S. and Sedström, E.	1924		323.2			42.36 Calculated composition (30.5 a/o Pd); electrical resistivity 27.0 $\mu\Omega$ cm at 50 C.
13	Holgersson, S. and Sedström, E.	1924		323.2			48.94 Calculated composition (36.4 a/o Pd); density 10.12 g cm <sup>-3</sup> ; electrical resistivity 29.8 $\mu\Omega$ cm at 50 C.
14	Sedström, E.	1924		273.2			3.5 Thermal conductivity value extracted from Schulze, A. (Z. Anorg. Chem., 159, 325-42, 1927).
15	Sedström, E.	1924		273.2			8.7 Same as above; electrical resistivity 6.90 $\mu\Omega$ cm at 0 C.
16	Sedström, E.	1924		273.2			11.1 Same data source as above.
17	Sedström, E.	1924		273.2			17.3 Same as above; electrical resistivity 11.79 $\mu\Omega$ cm at 0 C.
18	Sedström, E.	1924		273.2			42.8 Same as above; electrical resistivity 25.38 $\mu\Omega$ cm at 0 C.
19	Sedström, E.	1924		273.2			49.0 Same as above; electrical resistivity 29.67 $\mu\Omega$ cm at 0 C.

TABLE 16. THERMAL CONDUCTIVITY OF PALLADIUM + COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Pd	Cu	
1	Grüneisen, E. and Reddemann, H.	1934	L	21-91	18	90.8	9.2	Calculated composition; polycrystalline; electrical resistivity 20.59, 22.18, and 28.05 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
2	Grüneisen, E. and Reddemann, H.	1934	L	21-85	19	62.7	37.3	Calculated composition; electrical resistivity 32.49, 33.68, 36.8, and 37.15 $\mu\Omega$ cm at 22, 83, 273, and 291.60 K, respectively.
3	Grüneisen, E. and Reddemann, H.	1934	L	79-87	21a	57.8	42.2	Calculated composition; electrical resistivity 3.168, 5.1, and 5.32 $\mu\Omega$ cm at 83, 273, and 292.6 K, respectively.
4	Grüneisen, E. and Reddemann, H.	1934	L	21-82	21b			The above specimen annealed in vacuo for 2 hr at ~850 C; electrical resistivity 33.47, 34.01, 36.4, and 36.6 $\mu\Omega$ cm at 22, 83, 273, and 291.60 K, respectively.
5	Grüneisen, E. and Reddemann, H.	1934	L	21-80	21c			The above specimen annealed at ~325 C for 30 hr; electrical resistivity 2.812, 3.286, and 5.25 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
6	Pott, F.P.	1958	L	293, 823		52.75	47.25	Calculated composition; specimen cut from a 0.2 mm thick sheet; cold-rolled, annealed for 2 hr at ~650 C; ordered atomic arrangement; electrical resistivity 7.8, 10.8, and 14.0 $\mu\Omega$ cm at 35, 300, and 590 C, respectively.
7	Pott, F.P.	1958	L	293, 623		57.81	42.19	Similar to the above specimen except electrical resistivity 4.3, 7.7, and 11.0 $\mu\Omega$ cm at 0, 291, and 560 C, respectively.
8	Pott, F.P.	1958	L	303, 623		70.67	29.33	Similar to the above specimen except electrical resistivity 49.3, 50.6, and 51.4 $\mu\Omega$ cm at 0, 314, and 580 C, respectively.
9	Pott, F.P.	1958	L	893, 1048		52.75	47.25	Similar to the above specimen except disordered atomic arrangement and electrical resistivity 28.4, 31.4, and 35.9 $\mu\Omega$ cm at 25, 400, and 792 C, respectively.
10	Pott, F.P.	1958	L	293, 1048		57.81	42.19	Similar to the above specimen except electrical resistivity 34.2, 37.4, and 41.4 $\mu\Omega$ cm at 36, 400, and 800 C, respectively.
11	Pott, F.P.	1958	L	821, 1073		70.67	29.33	Similar to the above specimen except electrical resistivity 47.6, 49.7, and 51.7 $\mu\Omega$ cm at 32, 400, and 800 C, respectively.
12	Holgersson, S. and Sedström, E.	1924		323.2			48.40	Calculated composition (61.1 a/o Cu); electrical resistivity 11.9 $\mu\Omega$ cm at 50 C.
13	Holgersson, S. and Sedström, E.	1924		323.2			47.56	Calculated composition (60.3 a/o Cu); electrical resistivity 10.3 $\mu\Omega$ cm at 50 C.
14	Holgersson, S. and Sedström, E.	1924		323.2			41.70	Calculated composition (54.5 a/o Cu); density 10.35 g cm <sup>-3</sup> ; electrical resistivity 19.1 $\mu\Omega$ cm at 50 C.
15	Holgersson, S. and Sedström, E.	1924		323.2			37.58	Calculated composition (49.8 a/o Cu); electrical resistivity 10.0 $\mu\Omega$ cm at 50 C.
16	Holgersson, S. and Sedström, E.	1924		323.2			35.63	Calculated composition (46.1 a/o Cu); density 10.80 g cm <sup>-3</sup> ; electrical resistivity 48.1 $\mu\Omega$ cm at 50 C.
17	Holgersson, S. and Sedström, E.	1924		323.2			33.36	Calculated composition (45.6 a/o Cu); density 10.96 g cm <sup>-3</sup> ; electrical resistivity 50.1 $\mu\Omega$ cm at 50 C.
18	Holgersson, S. and Sedström, E.	1924		323.2			28.99	Calculated composition (40.6 a/o Cu); electrical resistivity 55.4 $\mu\Omega$ cm at 50 C.



TABLE 16. THERMAL CONDUCTIVITY OF PALLADIUM + COPPER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Pd Cu	Composition (continued), Specifications, and Remarks
19	Holgersson, S. and Sedström, E.	1924		323.2		20.22	Calculated composition (27.8 a/o Cu); density 11.26 g cm <sup>-3</sup> ; electrical resistivity 51.4 $\mu\Omega$ cm at 50 C.
20	Holgersson, S. and Sedström, E.	1924		323.2		14.13	Calculated composition (21.6 a/o Cu); electrical resistivity 41.1 $\mu\Omega$ cm at 50 C.
21	Holgersson, S. and Sedström, E.	1924		323.2		6.81	Calculated composition (10.9 a/o Cu); electrical resistivity 29.7 $\mu\Omega$ cm at 50 C.
22	Sedström, E.	1924		273.2		51.6	Thermal conductivity value extracted from Schulze, A. (Z. Anorg. Chem., 159, 325-42, 1927); electrical resistivity 11.10 $\mu\Omega$ cm at 0 C.
23	Sedström, E.	1924		273.2		52.5	Same as above but electrical resistivity 8.77 $\mu\Omega$ cm at 0 C.
24	Sedström, E.	1924		273.2		58.4	Same as above but electrical resistivity 18.28 $\mu\Omega$ cm at 0 C.
25	Sedström, E.	1924		273.2		62.4	Same as above but electrical resistivity 8.26 $\mu\Omega$ cm at 0 C.
26	Sedström, E.	1924		273.2		64.4	Same as above but electrical resistivity 47.39 $\mu\Omega$ cm at 0 C.
27	Sedström, E.	1924		273.2		66.7	Same data source as above.
28	Sedström, E.	1924		273.2		79.8	Same as above; electrical resistivity 50.76 $\mu\Omega$ cm at 0 C.
29	Sedström, E.	1924		273.2		85.9	Same as above but electrical resistivity 40.16 $\mu\Omega$ cm at 0 C.
30	Sedström, E.	1924		273.2		93.0	Same as above but electrical resistivity 27.32 $\mu\Omega$ cm at 0 C.

#### 4.6. Copper-Zinc Alloy System

The copper-zinc alloy system does not constitute a continuous series of solid solutions. The maximum solid solubility of zinc in copper is 38.3% (39.0 At.%) at 727 K and the solubility decreases at higher and lower temperatures. At lower temperatures, the attainment of equilibrium becomes very slow and the solubility data are uncertain. Massalski and Kittl [86] have analyzed existing data and have concluded that the boundary lies at about 35% Zn at 473 K and suggest that it may lie at less than 30% Zn at room temperature. Shinoda and Amano [87] have reported a much greater reduction in solubility at room temperature.

There are 91 sets of experimental data available for the thermal conductivity of Cu + Zn alloys as listed in Table 18 and shown in Figure 26. Of these, seven sets are merely single data points, 24 sets cover a narrow temperature range from around room temperature to about 500 K, and 17 sets are for temperatures below 4.5 K. Most of the measurements were on alloys in the solid solution region. Surprisingly there are no data available for the Zn + Cu alloys on either the thermal conductivity or the electrical resistivity. Consequently, only Cu + Zn alloys are treated in the present work.

In order to ascertain the reliability of experimental data and to fill gaps in data, the lattice and electronic components of the thermal conductivity of the Cu + Zn alloys were calculated. The electronic component was calculated from eq. (12). However, these calculations were limited to temperatures below 400 K, since no reliable electrical resistivity data were available at higher temperatures. Where values of the electronic component are reported at higher temperatures in Table 17, these were obtained by graphical smoothing of the differences between the experimental thermal conductivity data and the calculated values of the lattice thermal conductivity. Estimates of the lattice thermal conductivity in the low temperature region were based on experimental data and values in the high temperature region were calculated from eq. (35). In the intermediate range, near the maximum, graphical techniques were used to smoothly join the high and low temperature values (following a crude separation of  $k_g$  as a guide). The high temperature calculations of the lattice component were limited to alloys with Zn not exceeding 30%.

The low temperature lattice thermal conductivity of solid-solution Cu + Zn alloys in both strained and annealed states has been extensively investigated by Kemp, et al. [62, 88, 89] (curves 17-24 and 27-33). Their results show that the lattice and total thermal conductivities of the alloys increase markedly as the annealing temperature is increased, due to the removal of both point defects and dislocations. This increase is illustrated by curves 30-33 in Figure 26 for an alloy with 32% Zn. Apparently the dislocations are locked in by the impurity atoms, and cannot be removed by normal annealing just above the recrystallization temperature. Even annealing the alloys at temperatures near the melting point was found to remove only a fraction of the dislocations. In recommending low-temperature

lattice thermal conductivities, only the data for alloys annealed at high temperatures were used. The values given in Table 17 were based primarily on the data of Kemp, et al. [62] for alloys with 2.06, 5.14, and 10.26% Zn (curves 27-29), which were annealed at 1123 K. Because the low temperature lattice thermal conductivities of solid-solution Cu + Zn alloys do not vary greatly with composition in the 10-30% Zn range, it was possible to estimate the lattice components of alloys in this range by graphically extending the conductivity-composition curves formed by the 2.06, 5.14, and 10.26% Zn alloys to higher Zn concentrations, using data of Kemp, et al. [88] for alloys annealed at a lower temperature (773 K) (curves 18, 20, and 24) as a guide. Although this procedure should not introduce unacceptable uncertainties, the lattice components reported for the 10-30% Zn alloys should be accepted with more caution than those for which direct, supporting experimental data are available.

Problems were encountered in attempts to develop reliable estimates of the lattice thermal conductivities of the alloys at high temperatures. Initially, the lattice components for the alloys were calculated by using White and Woods' [90,91] value of 35.0 watts  $\text{cm}^{-1}$  for the value of  $k_g T$  of pure copper to determine  $k_u (T')$  in eq. (35). However, calculations of the lattice components from high temperature measurements by Kemp, et al. [62, 88, 89] (curves 17-24 and 27-33) and Smith [92] (curves 1-13) of the total thermal conductivity and the electrical resistivity for the same alloy samples were as much as 50% higher than the values calculated using eq. (35) with White and Woods' values for the lattice component of copper. It was found that this discrepancy could be reduced by increasing the values for the lattice component of pure copper by 50% at high temperatures. This resulted in a much better agreement between experimental and calculated values of the lattice component over the entire range of compositions. However, because of this conflict between White and Woods' value for the lattice component of copper and the available experimental data for copper-zinc alloys, the lattice components of the dilute copper-zinc alloys are not reported at high temperatures.

The recommended total thermal conductivity values are in agreement with the data at low temperatures of Lomer [161] (curves 80-86), Kemp, et al. [88] (curves 18, 20-22, and 24), Kemp, et al. [89] (curve 33), and Olsen [157] (curves 56-59) to within 10%, and with the data at higher temperatures of Smith [92] (curves 1-8, 11, 71, and 72), Smith and Palmer [49] (curve 14), Bailey [151] (curve 15), and Lees [152] (curve 16) to within 8%.

The recommended values for  $k$ ,  $k_g$ , and  $k_u$  are tabulated in Table 17 for nine alloy compositions ranging from 0.50 to 30% Zn. These values are for well-annealed alloys. The values for  $k$  are also shown in Figure 25, covering the temperature range from 4 to 700 K. The values of residual electrical resistivity for the alloys are also given in Table 17. The uncertainties of the  $k$  values are stated in a footnote to Table 17, while the uncertainties of the  $k_g$  and  $k_u$  values are indicated by their being designated as recommended or provisional

values. The ranges of uncertainties of recommended and provisional values are less than  $\pm 15\%$  and between  $\pm 15\%$  and  $\pm 30\%$ , respectively.

TABLE 17. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-ZINC ALLOY SYSTEM†

[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Cu: 99.50% (99.51 At.%) Zn: 0.50% (0.49 At.%)				Cu: 99.00% (99.03 At.%) Zn: 1.00% (0.97 At.%)				Cu: 97.00% (97.08 At.%) Zn: 3.00% (2.92 At.%)				Cu: 95.00% (95.13 At.%) Zn: 5.00% (4.87 At.%)			
$\rho_0 = 0.1800 \mu\Omega \text{ cm}$				$\rho_0 = 0.2650 \mu\Omega \text{ cm}$				$\rho_0 = 0.705 \mu\Omega \text{ cm}$				$\rho_0 = 1.090 \mu\Omega \text{ cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4	0.675*	0.651	0.0235†	4	0.389	0.369	0.0196†	4	0.152	0.139	0.0129	4	0.101	0.0897	0.0114
6	1.63*	0.977	0.0563†	6	0.603	0.553	0.0488†	6	0.242	0.208	0.0341	6	0.162	0.134	0.0280
8	1.40*	1.30	0.104†	8	0.834	0.738	0.0960†	8	0.345	0.277	0.0877	8	0.232	0.179	0.0530
10	1.73*	1.63	0.160†	10	1.07	0.922	0.148†	10	0.453	0.347	0.106	10	0.309	0.224	0.0850
15	2.73*	2.44	0.290†	15	1.64	1.38	0.264†	15	0.705	0.520	0.185	15	0.496	0.336	0.160
20	3.63*	3.26	0.385†	20	2.19	1.84	0.346†	20	0.945	0.693	0.252	20	0.667	0.448	0.219
25	4.24*	3.79	0.447†	25	2.61	2.21	0.399†	25	1.15	0.853	0.298†	25	0.808	0.547	0.261†
30	4.80*	4.31	0.489†	30	3.00	2.57	0.434†	30	1.33	1.00	0.331†	30	0.935	0.645	0.290†
40	5.30*	4.77	0.533†	40	3.48	3.01	0.468†	40	1.64	1.27	0.366†	40	1.14	0.823	0.320†
50	5.10*			50	3.61			50	1.82			50	1.30	0.968	0.327†
60	4.61*			60	3.52			60	1.89			60	1.39	1.07	0.320†
70	4.30*			70	3.34			70	1.95			70	1.46	1.15	0.308†
80	4.00*			80	3.24			80	1.99			80	1.51	1.22	0.295†
90	3.93*			90	3.22			90	2.05			90	1.58	1.29	0.284†
100	3.80*			100	3.21			100	2.11			100	1.64	1.37	0.274†
150	3.81*			150	3.34			150	2.42			150	1.95	1.72	0.230†
200	3.79*			200	3.47*			200	2.65			200	2.18	1.96	0.198†
250	3.77*			250	3.50*			250	2.80			250	2.36		
273	3.76*			273	3.52			273	2.85			273	2.41		
300	3.76			300	3.54			300	2.90			300	2.49		
350	3.75			350	3.56			350	2.97			350	2.58		
400	3.74			400	3.57			400	3.03			400	2.65		
500	3.70			500	3.57			500	3.11			500	2.77		
600	3.67*			600	3.57*			600	3.18*			600	2.89*		
700	3.63*			700	3.57*			700	3.26*			700	2.99*		
800				800				800				800			
900				900				900				900			
1000				1000				1000				1000			
1100				1100				1100				1100			
1200				1200				1200				1200			

† Uncertainties of the total thermal conductivity, k, are as follows:

99.50 Cu - 0.50 Zn ± 10%.

99.00 Cu - 1.00 Zn ± 10%.

97.00 Cu - 3.00 Zn ± 10%.

95.00 Cu - 5.00 Zn ± 10% below 300 K and ± 5% above 300 K.

\* Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 17. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-ZINC ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Cu 90.00% (90.25 At. %) Zn 10.00% ( 9.75 At. %)				Cu 85.00% (85.38 At. %) Zn 15.00% (14.62 At. %)				Cu 80.00% (80.45 At. %) Zn 20.00% (19.55 At. %)				Cu 75.00% (75.53 At. %) Zn 25.00% (24.47 At. %)			
$\rho_0 = 1.840 \mu\Omega\text{cm}$				$\rho_0 = 2.300 \mu\Omega\text{cm}$				$\rho_0 = 2.840 \mu\Omega\text{cm}$				$\rho_0 = 3.200 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0640	0.0631	0.0109	4	0.0519	0.0411	0.0108†	4	0.0448	0.0344	0.0104†	4	0.0408	0.0305	0.0103†
6	0.105	0.0797	0.0254	6	0.0855†	0.0616	0.0239†	6	0.0759	0.0516	0.0243†	6	0.0646	0.0458	0.0238†
8	0.132	0.106	0.0461	8	0.127*	0.0831	0.0448†	8	0.113	0.0688	0.0441†	8	0.104	0.0611	0.0433†
10	0.204	0.153	0.0708	10	0.173*	0.103	0.0694†	10	0.154	0.0860	0.0690†	10	0.144	0.0763	0.0672†
15	0.332	0.198	0.133	15	0.261*	0.154	0.127†	15	0.254	0.129	0.125†	15	0.237	0.115	0.123†
20	0.480	0.266	0.194	20	0.376*	0.205	0.173†	20	0.338	0.172	0.166†	20	0.313	0.153	0.160†
25	0.545	0.326	0.239	25	0.459*	0.252	0.203†	25	0.402	0.212	0.190†	25	0.373	0.189	0.184†
30	0.631	0.388	0.243	30	0.530*	0.299	0.231†	30	0.459	0.253	0.206†	30	0.422	0.226	0.197†
40	0.762	0.503	0.259†	40	0.623*	0.369	0.234†	40	0.546	0.339	0.217†	40	0.497	0.292	0.205†
50	0.851	0.601	0.269†	50	0.689*	0.466	0.233†	50	0.611	0.396	0.215†	50	0.556	0.353	0.203†
60	0.928	0.682	0.267†	60	0.761*	0.534	0.227†	60	0.660	0.452	0.206†	60	0.601	0.406	0.196†
70	0.986	0.748	0.269†	70	0.811*	0.592	0.219†	70	0.703	0.503	0.200†	70	0.636	0.450	0.189†
80	1.05	0.818	0.239†	80	0.854	0.644	0.210†	80	0.742	0.550	0.192†	80	0.673	0.493	0.180†
90	1.16	0.908	0.239†	90	0.896	0.697	0.201†	90	0.780	0.596	0.184†	90	0.707	0.535	0.172†
100	1.18	0.984	0.219†	100	0.943	0.751	0.192†	100	0.818	0.643	0.176†	100	0.742	0.578	0.164†
150	1.41	1.29	0.189†	150	1.16	1.00	0.160†	150	1.01	0.867	0.146†	150	0.918	0.782	0.136†
200	1.62	1.47	0.189†	200	1.36	1.21	0.136†	200	1.18	1.05	0.126†	200	1.07	0.951	0.118†
250	1.79	1.65	0.149†	250	1.50	1.36	0.122†	250	1.32	1.20	0.111†	250	1.20	1.09	0.104†
273	1.86	1.72	0.139†	273	1.56	1.44	0.116†	273	1.37	1.26	0.106†	273	1.24	1.15	0.099†
300	1.98	1.80	0.129†	300	1.62	1.51	0.110†	300	1.43	1.33	0.100†	300	1.30	1.20	0.0940†
350	2.03	1.88	0.114†	350	1.73	1.63	0.100†	350	1.52	1.43	0.0918†	350	1.39	1.30	0.0859†
400	2.12	2.02	0.109†	400	1.81	1.72	0.0925†	400	1.60	1.51	0.0847†	400	1.46	1.36	0.0783†
500	2.26	2.26	0.0819†	500	1.96	1.88	0.0805†	500	1.73	1.66	0.0758†	500	1.59	1.52	0.0692†
600	2.41*	2.33	0.0696†	600	2.09*	2.02	0.0716†	600	1.86*	1.79	0.0657†	600	1.70	1.64	0.0617†
700	2.51*	2.44	0.0729†	700	2.20*	2.14	0.0646†	700	1.96*	1.90	0.0595†	700	1.78	1.72	0.0559†
800				800				800				800			
900				900				900				900			
1000				1000				1000				1000			
1100				1100				1100				1100			
1200				1200				1200				1200			

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:  
 50.00 Cu - 10.00 Zn:  $\pm 10\%$  below 300 K and  $\pm 5\%$  above 300 K.  
 55.00 Cu - 15.00 Zn:  $\pm 10\%$  below 300 K and  $\pm 5\%$  above 300 K.  
 60.00 Cu - 20.00 Zn:  $\pm 10\%$  below 70 K and  $\pm 10\%$  above 70 K.  
 75.00 Cu - 25.00 Zn:  $\pm 10\%$  below 70 K and  $\pm 10\%$  above 70 K.

\* Provisional values.

† In temperature range where no experimental thermal conductivity data are available.

TABLE 17. RECOMMENDED THERMAL CONDUCTIVITY OF COPPER-ZINC ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ]

Cu 70.00% (70.59 At. %)					
Zn 30.00% (29.41 At. %)					
$\rho_0 = 2.300 \mu\Omega\text{cm}$					
T	k	$k_e$	$k_g$		
4	0.0200	0.0200	0.0101‡		
6	0.0207	0.0432	0.0235†		
8	0.0208	0.0577	0.0431‡		
10	0.126	0.0721	0.0730†		
15	0.237	0.100	0.119†		
20	0.300	0.144	0.150†		
25	0.306	0.170	0.170†		
30	0.400	0.211	0.180†		
40	0.472	0.275	0.197†		
50	0.506	0.321	0.190†		
60	0.506	0.370	0.180†		
70	0.601	0.431	0.180†		
80	0.630	0.463	0.170†		
90	0.604	0.500	0.164†		
100	0.607	0.501	0.180†		
120	0.603	0.723	0.120†		
200	1.00	0.802	0.115†		
250	1.13	1.03	0.0971‡		
273	1.17	1.00	0.0843†		
300	1.26	1.13	0.0804†		
350	1.30	1.22	0.0617†		
400	1.37	1.20	0.0735†		
500	1.46	1.42	0.0809†		
600	1.50	1.52	0.0800†		
700	1.56	1.61	0.0834†		
800					
900					
1000					
1100					
1200					

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:  
 70.00 Cu - 30.00 Zn  $\pm 10\%$  below 70 K and  $\pm 10\%$  above 70 K.

‡ Provisional values.

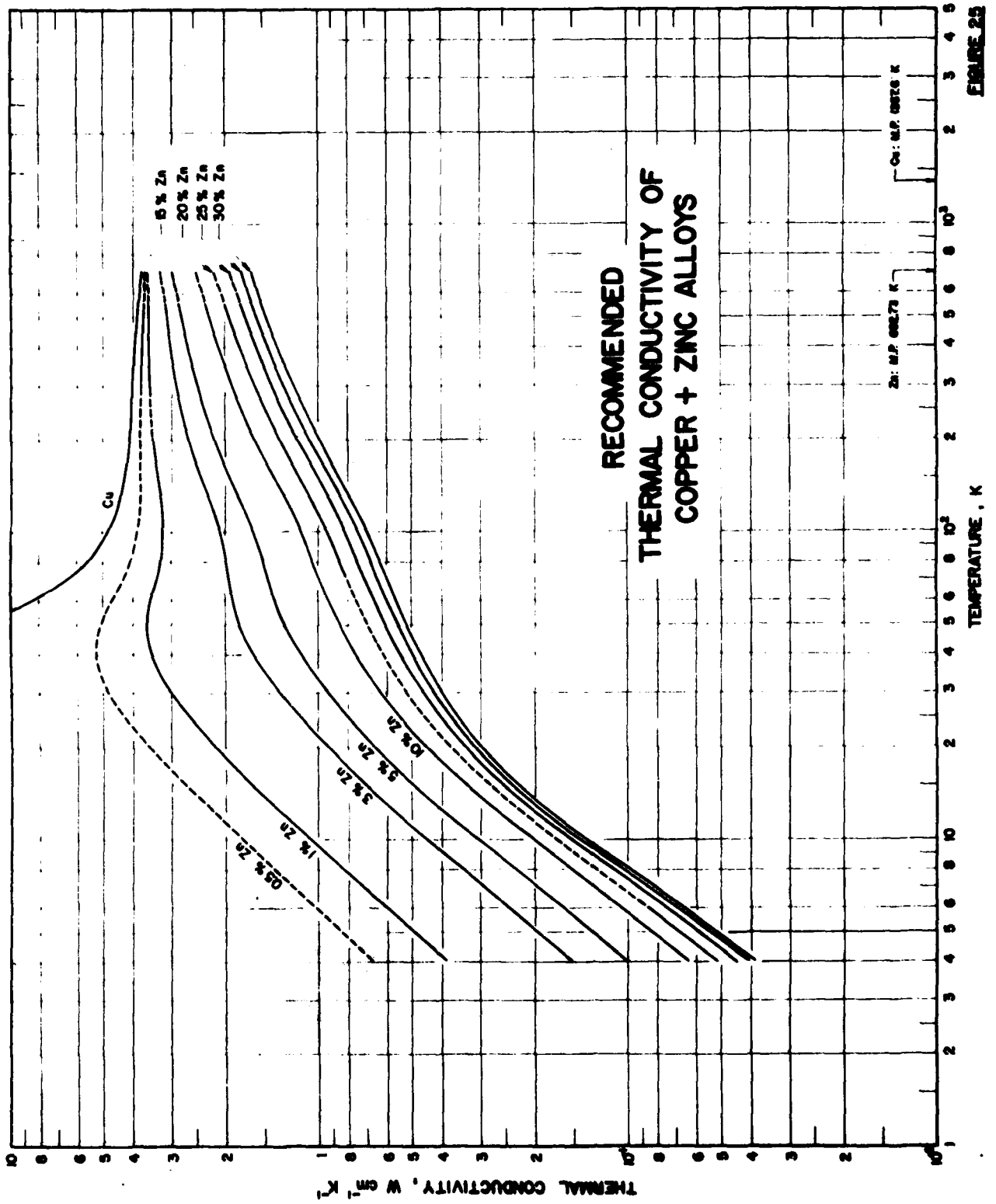


FIGURE 25



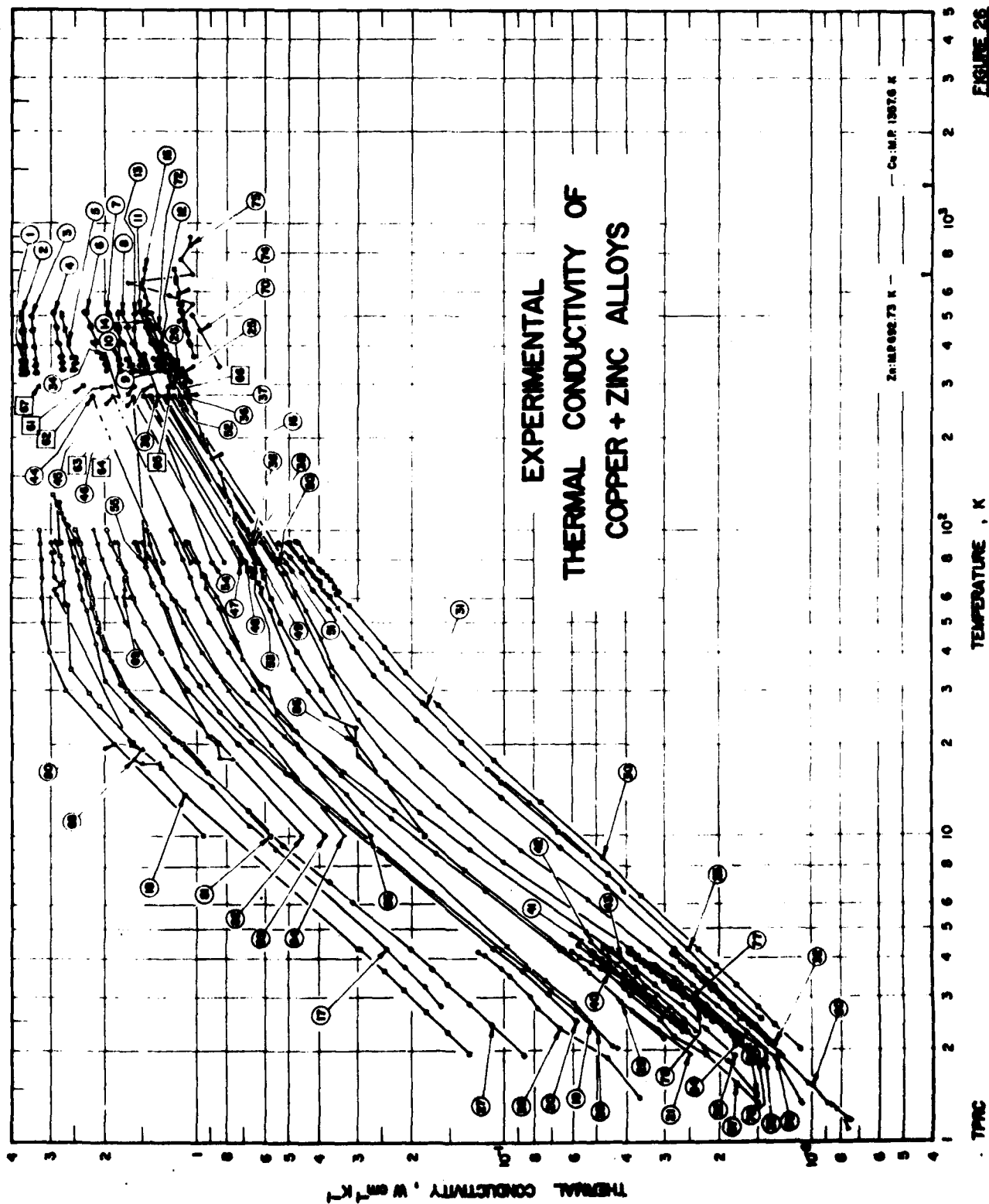


FIGURE 26

TABLE 18. THERMAL CONDUCTIVITY OF COPPER - ZINC ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Zn	
1	92 Smith, C.S.	1930	L	319-494	90	99.64	0.35	0.02 Fe and 0.01 Pb; polycrystalline; cylindrical specimen 12.25 in. long and 0.750 in. diameter; grain size 0.070 mm; annealed at 650 C for 1 hr, cooled in air; electrical conductivity $56.264 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
2	92 Smith, C.S.	1930	L	323-501	89	99.45	0.51	0.01 Fe and 0.01 Pb; similar to the above specimen except grain size 0.110 mm and electrical conductivity $53.325 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
3	92 Smith, C.S.	1930	L	324-494	73	98.93	0.95	0.02 Fe; similar to the above specimen except annealing temperature 700 C and grain size 0.120 mm; electrical conductivity $47.686 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
4	49, 92 Smith, C.S.	1930	L	332-506	12	96.94	3.04	0.02 Fe; similar to the above specimen except annealing time 0.75 hr, grain size 0.100 mm, and electrical conductivity $36.607$ and $26.21 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
5	49, 92 Smith, C.S.	1930	L	328-507	13	95.21	4.77	Similar to the above specimen except grain size 0.065 mm and electrical conductivity $33.063$ and $23.31 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
6	92 Smith, C.S.	1930	L	328-510	14	90.07	9.91	0.01 Fe and 0.01 Pb; similar to the above specimen but grain size 1 mm and electrical conductivity $25.293 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
7	92 Smith, C.S.	1930	L	326-504	15	83.20	16.76	0.03 Fe and 0.01 Pb; similar to the above specimen except grain size 0.125 mm and electrical conductivity $20.108 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
8	92 Smith, C.S.	1930	L	327-510	16	79.62	20.35	0.01 Fe and 0.02 Pb; similar to the above specimen except grain size 0.190 mm and electrical conductivity $18.459 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
9	92 Smith, C.S.	1930	L	325-512	22	59.20	40.75	0.02 Fe and 0.03 Pb; same structure and dimensions as the above specimen; grain size 0.070 mm; annealed at 650 C for 3 hr; cooled in furnace; electrical conductivity $16.700 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
10	92 Smith, C.S.	1930	L	328-508	85	50.30	49.49	0.01 Fe and 0.04 Pb; similar to the above specimen but annealing time 2 hr, grain size 16 mm, and electrical conductivity $23.812 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
11	92 Smith, C.S.	1930	L	329-512	18	69.14	30.81	0.03 Fe and 0.02 Pb; same structure and dimensions as the above specimen; annealed at 650 C for 0.75 hr, cooled in air; electrical conductivity $15.857 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
12	92 Smith, C.S.	1930	L	329-511	21	65.43	34.53	0.01 Fe and 0.03 Pb; similar to the above specimen except grain size 0.080 mm and electrical conductivity $15.325 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
13	92 Smith, C.S.	1930	L	326-505	88	54.96	45.02	0.01 Fe; similar to the above specimen except annealing time 2 hr, grain size 0.040 mm, and electrical conductivity $20.466 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 C.
14	49 Smith, C.S. and Palmer, E.W.	1935	L	293, 473	19	66.24	33.72	0.03 Pb and 0.01 Fe; annealed at 650 C for 0.75 hr; electrical conductivity 15.63 and $12.24 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 20 and 200 C, respectively.
15	151 Bailey, L.C.	1931	L	351-703	Brass 70/30	70	30	7 to 8 cm long and 0.585 cm in diameter; density $8.44 \text{ g cm}^{-3}$ at 22 C.
16	132 Lees, C.H.	1946	L	106-299	Brass 70/30	70	30	7 to 8 cm long and 0.585 cm in diameter; density $8.44 \text{ g cm}^{-3}$ at 22 C.
17	86 Kemp, W.R.G., Taitel, R.J., and White, G.K.	1957	L	2.8-123	25		1.63	~8 cm long and 0.5 cm in diameter; supplied by Johnson Matthey and Co., Ltd.; as drawn; residual electrical resistivity $0.035 \mu\Omega \text{ cm}$ .

TABLE 18. THERMAL CONDUCTIVITY OF COPPER + ZINC ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Zn	
18	Kemp, W.R.G., Klemens, P.G., Talsch, R.J., and White, G.K.	1967	L	2.0-130	2			The above specimen annealed at 500 C for 4 hr in helium atmosphere; residual electrical resistivity 0.38 $\mu\Omega$ cm.
19	Kemp, W.R.G., et al.	1967	L	2.1-91	58		5.37	Same dimensions and supplier as the above specimen; as drawn; residual electrical resistivity 1.22 $\mu\Omega$ cm.
20	Kemp, W.R.G., et al.	1967	L	2.5-91	5			The above specimen annealed at 500 C for 4 hr in a helium atmosphere; residual electrical resistivity 1.12 $\mu\Omega$ cm.
21	Kemp, W.R.G., et al.	1967	L	1.9-91	10		9.98	Similar to the above specimen except residual electrical resistivity 1.88 $\mu\Omega$ cm.
22	Kemp, W.R.G., et al.	1967	L	1.9-91	20		19.48	Similar to the above specimen except residual electrical resistivity 2.97 $\mu\Omega$ cm.
23	Kemp, W.R.G., et al.	1967	L	2.5-91	306		31.87	Same dimensions and supplier as the above specimen; as drawn; residual electrical resistivity 4.31 $\mu\Omega$ cm.
24	Kemp, W.R.G., et al.	1967	L	2.2-91	30			The above specimen annealed in a helium atmosphere at 500 C for 4 hr; residual electrical resistivity 3.60 $\mu\Omega$ cm.
25	Raeth, C.H.	1944	L	302-335	Brass			Cylindrical specimen 2.565 cm long and 5.017 cm <sup>2</sup> in cross-sectional area.
26	Raeth, C.H.	1944	L	314-344	Brass			Cylindrical specimen 2.570 cm long and 3.447 cm <sup>2</sup> in cross-sectional area.
27	Kemp, W.R.G., Klemens, P.G., and Talsch, R.J.	1967	L	1.9-121			2.06	8 cm long and 0.5 cm in diameter; drawn; annealed at 850 C for 4 hr; electrical resistivity reported as 0.563, 0.573, and 2.273 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
28	Kemp, W.R.G., et al.	1967	L	2.0-91			5.14	Similar to the above specimen except electrical resistivity reported as 1.20, 1.53, and 3.00 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
29	Kemp, W.R.G., et al.	1967	L	2.2-91			10.26	Similar to the above specimen except electrical resistivity reported as 1.94, 2.31, and 3.89 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
30	Kemp, W.R.G., et al.	1969	L	2.0-91	1		32	$\alpha$ -brass; machined from an annealed and torsionally deformed bar; electrical resistivity 4.59, 5.11, and 7.27 $\mu\Omega$ cm at 4.2, 90, and 293 K, respectively.
31	Kemp, W.R.G., et al.	1969	L	6.5-91	2			Similar to the above specimen except annealed (after machining) up to 250 C at a rate of 6 C min <sup>-1</sup> ; electrical resistivity 4.20, 4.84, and 6.88 $\mu\Omega$ cm at 4.2, 90, and 293 K, respectively.
32	Kemp, W.R.G., et al.	1969	L	2.1-91	3			Similar to the above specimen except annealed (after machining) up to 290 C at a rate of 6 C min <sup>-1</sup> ; electrical resistivity 3.90, 4.49, and 6.58 $\mu\Omega$ cm at 4.2, 90, and 293 K, respectively.
33	Kemp, W.R.G., et al.	1969	K	2.0-91	4			Similar to the above specimen except annealed after machining up to 400 C at a rate of 6 C min <sup>-1</sup> ; electrical resistivity 3.66, 4.27, and 6.31 $\mu\Omega$ cm at 4.2, 90, and 293 K, respectively.
34	Sedotšum, E.	1919	T	273, 373		92.65	7.35	Rolled and drawn; annealed close to the melting point for 0.5 hr.
35	Sedotšum, E.	1919	T	273, 373		85.65	14.35	Similar to the above specimen.
36	Sedotšum, E.	1919	T	273, 373		72.11	27.89	Similar to the above specimen.
37	Sedotšum, E.	1919	T	273, 373		66.97	33.03	Similar to the above specimen.

TABLE 16. THERMAL CONDUCTIVITY OF COPPER - ZINC ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cat. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Zn	
38	Eucken, A. and Neumann, O.	1924	L	90, 273	Red brass	82	18	Polycrystalline; grain size 0.006 cm; electrical conductivity 26.95 and $17.50 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 90 and 273 K, respectively.
39	Eucken, A. and Neumann, O.	1924	L	90, 273	Red brass	82	18	Polycrystalline; grain size 0.11 cm; electrical conductivity 27.36 and $17.75 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 90 and 273 K, respectively.
40	Lomer, J.N. and Rosenberg, H.M.	1959	L	2.3-4.4	Brass	85	15	$\alpha$ -brass; 2.5 mm diameter and 4 cm long; prepared from Johnson Matthey spectrographically standardized metals by melting in vacuo, cooling, and swaging; annealed just below melting point for 40 hr.
41	Lomer, J.N. and Rosenberg, H.M.	1959	L	2.3-4.5	Brass			The above specimen drawn to produce 4.6% strain.
42	Lomer, J.N. and Rosenberg, H.M.	1959	L	2.4-4.5	Brass			The above specimen drawn to produce 10.4% strain.
43	Lomer, J.N. and Rosenberg, H.M.	1959	L	2.3-4.4	Brass			The above specimen drawn to produce 19.9% strain.
44	Aoyama, S. and Ito, T.	1940	L, R	78, 273	1	95.46	4.54	Prepared from electrolytic copper containing impurities: 0.015 Sb, 0.010 Fe, 0.007 S, 0.0008 As, and 0.0008 Pb; $\alpha$ -brass; annealed in N <sub>2</sub> for 20 hr at 380-400 C; electrical conductivity 6.00 and $3.25 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
45	Aoyama, S. and Ito, T.	1940	L, R	78, 273	2	92.82	7.18	Similar to the above specimen except electrical conductivity 4.59 and $2.71 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
46	Aoyama, S. and Ito, T.	1940	L, R	78, 273	3	86.87	13.13	Similar to the above specimen except electrical conductivity 3.56 and $2.29 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
47	Aoyama, S. and Ito, T.	1940	L, R	78, 273	4	82.58	17.42	Similar to the above specimen except electrical conductivity 3.08 and $2.03 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
48	Aoyama, S. and Ito, T.	1940	L, R	78, 273	5	79.73	20.27	Similar to the above specimen except electrical conductivity 3.04 and $1.99 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
49	Aoyama, S. and Ito, T.	1940	L, R	78, 273	6	75.44	24.56	Similar to the above specimen except electrical conductivity 2.83 and $1.87 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
50	Aoyama, S. and Ito, T.	1940	L, R	73, 273	7	70	30	Similar to the above specimen except electrical conductivity 2.46 and $1.64 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
51	Aoyama, S. and Ito, T.	1940	L, R	73, 273	8	64.05	35.95	Similar to the above specimen except electrical conductivity 2.39 and $1.57 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
52	Aoyama, S. and Ito, T.	1940	L, R	73, 273	9	62.30	37.70	Prepared from the same original materials by the same fabrication method; $\alpha$ - $\beta$ -brass; electrical conductivity 2.63 and $1.61 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
53	Aoyama, S. and Ito, T.	1940	L, R	73, 273	10	59.93	40.07	Similar to the above specimen except electrical conductivity 3.28 and $1.76 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
54	Aoyama, S. and Ito, T.	1940	L, R	73, 273	11	55.62	44.38	Similar to the above specimen except electrical conductivity 4.73 and $2.05 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.
55	Aoyama, S. and Ito, T.	1940	L, R	73, 273	12	51.09	48.91	$\beta$ -brass; prepared from the same original materials by the same fabrication method; electrical conductivity 8.25 and $2.50 \times 10^5 \Omega^{-1} \text{cm}^{-1}$ at 78 and 273 K, respectively.

TABLE 16. THERMAL CONDUCTIVITY OF COPPER + ZINC ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Cu Zn	Composition (continued), Specifications, and Remarks
56	157 Olson, T.	1960	L	1.3-4.2	Z4	95.4 4.59	0.01 Pb; cylindrical specimen 10 cm long; machined; annealed for 21 hr at 540 C; electrical resistivity 1.13 and 1.08 $\mu\Omega$ cm at 1.06 and 4.2 K, respectively.
57	157 Olson, T.	1960	L	1.3-4.2	Z15	94.53 15.43	0.02 Fe and 0.02 Pb; cylindrical specimen 10 cm long; machined; annealed for 21 hr at 540 C; electrical resistivity 2.55 and 2.36 $\mu\Omega$ cm at 1.05 and 4.2 K, respectively.
58	157 Olson, T.	1960	L	1.4-4.2	Z20	96.56 13.43	0.01 Fe; cylindrical specimen 10 cm long; cold-worked and machined; annealed at 500 C for 17 hr; electrical resistivity 2.73 and 2.58 $\mu\Omega$ cm at 1.05 and 4.2 K, respectively.
59	157 Olson, T.	1960	L	1.3-4.1	Z30	99.95 30.02	0.02 Fe and 0.01 Pb; cylindrical specimen 10 cm long; machined; annealed for 21 hr at 540 C; electrical resistivity 4.22 and 4.10 $\mu\Omega$ cm at 1.05 and 4.2 K, respectively.
60	158 Gordon, J.E. and Ametani, L.I.	1965		1.1-4.1	CDA alloy; No. 260	69.3 $\pm$ 0.5 30.7 $\pm$ 0.5	0.07 Si, 0.025 Pb, <0.01 each of Fe, Co, and Ni; strip specimen 0.0150 cm in cross-section and 3.46 cm long; supplied by Chase Brass and Copper Co.; cold-rolled cartridge brass of nominal grain size 0.025-0.050 mm; electrical resistivity 3.78 and 6.65 $\mu\Omega$ cm at 4.2 K and room temperature, respectively.
61	123 Materials in Design Engineering	1969		293.2	Gliding	94.0-96.0 Bal.	Nominal composition; density 8.96 g cm <sup>-3</sup> .
62	123 Materials in Design Engineering	1969		293.2	Commercial bronze	89.0-91.0 Bal.	Nominal composition; density 8.80 g cm <sup>-3</sup> .
63	123 Materials in Design Engineering	1969		293.2	Red brass	84.0-86.0 Bal.	Nominal composition; density 8.75 g cm <sup>-3</sup> .
64	123 Materials in Design Engineering	1969		293.2	Low brass	76.5-81.5 Bal.	Nominal composition; density 8.66 g cm <sup>-3</sup> .
65	123 Materials in Design Engineering	1969		293.2	Cartridge brass	68.5-71.5 Bal.	Nominal composition; density 8.53 g cm <sup>-3</sup> .
66	123 Materials in Design Engineering	1969		293.2	Muntz metal	59.0-63.0 Bal.	Nominal composition; density 8.39 g cm <sup>-3</sup> .
67	63 Kierpke, W.	1967	L	293.2		1.54	Cylindrical specimen.
68	159 Srivastava, B.N., Chatterjee, S., and Sen, S.K.	1969	L	17-92		1.96	Prepared from spectrographically pure rods of copper and zinc, supplied by Johnson Matthey and Co., Ltd, by sealing the metals in appropriate portion in an evacuated quartz tube, heating to 1100 C, shaking thoroughly, cooling to 906 C and maintaining for 5 days, rolled, annealed at 500 C for 6 hr; residual electrical resistivity 0.549 $\mu\Omega$ cm.
69	159 Srivastava, B.N., et al.	1969	L	19-91		4.76	Same fabrication method as the above specimen; residual electrical resistivity 1.043 $\mu\Omega$ cm.
70	44 Griffiths, E. and Schofield, F.H.	1928	L	337-496	Bar 4	60.7 39.3	0.5 Sn and 0.30 Mn; 1 in. diameter and 15 in. long; electrical resistivity 9.3, 9.6, 10.0, 10.4, 10.9, and 11.3 $\mu\Omega$ cm at 20, 75, 100, 150, 200, and 250 C, respectively.
71*	93 Smith, C.S.	1909	L	405-515	Bar 55	81.16 18.84	0.20 Sn, 0.02 Fe, and trace Pb; 0.750 in. diameter and 13.25 in. long; annealed at 700 C for 2 hr; electrical conductivity $18.674 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 C.

\* Not shown in figure.

TABLE 18. THERMAL CONDUCTIVITY OF COPPER - ZINC ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Cu	Zn	
72	Smith, C. S.	1930	L	321-508	Bar 56	71.09	27.77	1.02 Sn, 0.02 Fe, and trace Pb; 0.750 in. diameter and 13.25 in. long; annealed at 700 C for 45 min; electrical conductivity $14.298 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 C.
73*	Smith, C. S.	1930	L	320-517	Bar 57	59.85	39.36	0.70 Sn, 0.07 Pb, and 0.02 Fe; 0.750 in. diameter and 13.25 in. long; annealed at 650 C for 3 hr; electrical conductivity $15.146 \times 10^4 \Omega^{-1} \text{cm}^{-1}$ at 20 C.
74	Donaldson, J. W.	1925	L	363-702	70-30 brass	70.29	28.71	0.35 Sn, 0.34 Pb, and 0.31 Fe; 0.75 in. diameter and 15.5 in. long; machined from a dry sand-cast bar.
75	Tadoboro, Y.	1936	P	479-888	Brass	71.00	28.43	0.25 Pb, 0.24 Fe, and trace Ni and Si; $110 \times 110 \times 70$ mm; annealed at 650 C for 1.5 hr; density $8.062 \text{ g cm}^{-3}$ ; thermal conductivity values calculated from measured thermal diffusivity, specific heat capacity, and density data.
76	Charley, P., Salter, J. A. M., and Leaver, A. D. W.	1968	L	1.8-4.2	$\alpha$ -brass		27.8	Poly-crystalline; supplied by the International Research and Development Co., Ltd.; prepared by induction melting; annealed in vacuum at 750 C for 15 hrs, furnace cooled.
77	Charley, P., et al.	1968	L	1.7-4.2	$\alpha$ -brass			The above specimen deformed by tensile strain of 4.4%.
78	Leaver, A. D. W. and Charley, P.	1971	L	2.1-4.1	30 Zn			Similar to the specimen for curve No. 76; deformed by tensile strain of 3.2%.
79	Lomer, J. N.	1958		10-100	0.1 Zn	99.9	0.1	Data taken from smooth curve presented by H. M. Rosenberg [180].
80	Lomer, J. N.	1958		10-100	1.0 Zn	99.0	1.0	Similar to above.
81	Lomer, J. N.	1958		10-100	2.0 Zn	98.0	2.0	Similar to above.
82	Lomer, J. N.	1958		10-100	3.0 Zn	97.0	3.0	Similar to above.
83	Lomer, J. N.	1958		10-100	4.5 Zn	95.5	4.5	Similar to above.
84	Lomer, J. N.	1958		10-100	7.2 Zn	92.8	7.2	Similar to above.
85	Lomer, J. N.	1958		10-100	10.0 Zn	90.0	10.0	Similar to above.
86	Lomer, J. N.	1958		10-100	25.5 Zn	74.5	25.5	Similar to above.
87*	Kapoor, A., Rowlands, J. A., and Woods, S. B.	1974	L	0.57-4.0	$\alpha$ -Brass	69.4	30.6	Calculated composition (30 z/o Zn); 4 mm diameter x 12 cm long; cast in air, swaged to 0.25 in. diameter, and machined to size; cold worked; residual electrical resistivity $4.59 \mu\Omega \text{ cm}$ .
88*	Kapoor, A., et al.	1974	L	0.52-3.9	$\alpha$ -Brass			The above specimen annealed in argon at 600 K for 12 hr; residual electrical resistivity $3.82 \mu\Omega \text{ cm}$ .
89*	Kapoor, A., et al.	1974	L	0.71-4.0	$\alpha$ -Brass			The above specimen reannealed in argon at 700 K for 12 hr; residual electrical resistivity $3.77 \mu\Omega \text{ cm}$ .
90*	Kapoor, A., et al.	1974	L	0.73-4.0	$\alpha$ -Brass			The above specimen reannealed in argon at 1000 K for 12 hr; residual electrical resistivity $3.86 \mu\Omega \text{ cm}$ .
91*	Kapoor, A., et al.	1974	L	0.68-4.0	Brass			Single crystal; 3 mm diameter x 15 cm long; obtained from Windsor Metal Crystals Inc., Md.; residual electrical resistivity $3.53 \mu\Omega \text{ cm}$ .

\* Not shown in figure.

#### 4.7. Gold-Palladium Alloy System

The gold-palladium alloy system forms a continuous series of solid solutions over the entire range of compositions and is free from the complicating effects of any kind of transitions.

There are 14 sets of experimental data available for the thermal conductivity of this alloy system. However, of the nine data sets available for Au + Pd alloys listed in Table 20 and shown in Figure 29, five sets are merely single data points at room temperature, and all the five data sets available for Pd + Au alloys are single data points at room temperature, as listed in Table 21 and shown in Figure 30.

The thermal conductivity of these alloys was first investigated by Schulze [93] (Au + Pd curves 1-5 and Pd + Au curves 1-5) who measured the room-temperature thermal conductivity of these alloys at intervals of 10%. These values, which include the only experimental values for this system for palladium concentrations greater than 40%, are thought to be more than 20% too high in some cases. This judgment is based primarily on the fact that interpolation between the values for 30 and 40% Pd yields a value 27% greater than that obtained by Laubitz and van der Meer [85] (Au + Pd curve 8) on a specimen containing 34.95% Pd and is supported by the fact that, after correcting for the lattice component, the Lorenz ratio for the specimen containing 40% Pd (55.24 At.% Pd) is 30% greater than the classical values. It is unlikely that band structure effects could cause such a large deviation from the classical value for this composition at 298 K.

In contrast to this, the early measurements by Grüneisen and Reddemann [61] of the thermal conductivity at liquid hydrogen and liquid nitrogen temperatures of specimens containing 5, 10, and 39.9% Pd (Au + Pd curves 6-8) are thought to be close to the true values. The values calculated from eqs. (12) and (35) are in good agreement with these measurements at those temperatures for which it was possible to calculate the lattice component. The investigation by Fletcher and Greig [84] of the thermal conductivity of palladium-silver alloys revealed that the strong electron-phonon interaction in palladium-rich alloys suppresses the low temperature lattice thermal conductivity, causing its maximum to occur at much higher temperatures than in silver-rich alloys. This elevation of the temperature of the maximum of the lattice component is believed to occur also in this alloy system; the evidence for this is that while the calculated and experimental values for the 5, 10, and 39.9% Pd (8.88, 17.06, and 55.24 At.% Pd) alloys differ by less than 5% at 80 K and the measured values at liquid hydrogen temperatures of the 5 and 10% Pd specimens are consistent with the calculated values at 30 K, the measured value for the 39.9% Pd specimen is far below the calculated value for 30 K when the expression for the lattice component at temperatures above that of its maximum is used.

At high temperatures the only measurements are those of Laubitz and van der Meer [85], but these range from 300 to 1200 K and provide a test of the temperature dependence of the calculated values of the thermal conductivity of these alloys in this region. While the slope of the calculated curve is slightly steeper than that of the experimental curve, the largest discrepancy between the calculated and experimental values is less than 7%; in view of the 3.5% experimental error estimated for these measurements this is considered satisfactory agreement.

The recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 19 for 25 alloy compositions. These values are for well-annealed alloys. The  $k_e$  values cover the full range of temperature from 4 to 1200 K, whereas the  $k$  and  $k_g$  values are not given for low temperatures. The values for  $k$  are also shown in Figures 27 and 28 and their uncertainties are stated in a footnote to Table 19, in which the values of residual electrical resistivity for the alloys are also given. The uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended or provisional values. The ranges of uncertainties of recommended and provisional values are less than  $\pm 15\%$  and between  $\pm 15$  and  $\pm 30\%$ , respectively.



TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM†

[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 99.50% (99.08 At.%) Pd: 0.50% (0.93 At.%)				Au: 99.00% (98.16 At.%) Pd: 1.00% (1.84 At.%)				Au: 97.00% (94.58 At.%) Pd: 3.00% (5.42 At.%)				Au: 95.00% (91.12 At.%) Pd: 5.00% (8.88 At.%)			
$\rho_0 = 0.3900 \mu\Omega \text{ cm}$				$\rho_0 = 0.680 \mu\Omega \text{ cm}$				$\rho_0 = 2.010 \mu\Omega \text{ cm}$				$\rho_0 = 3.270 \mu\Omega \text{ cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.279		4		0.144		4		0.0486		4		0.0299	
6		0.419		6		0.216		6		0.0729		6		0.0448	
8		0.568		8		0.287		8		0.0972		8		0.0598	
10		0.698		10		0.359		10		0.122		10		0.0747	
15		1.06		15		0.539		15		0.182		15		0.112	
20		1.40		20		0.719		20		0.243		20		0.149	
25		1.59		25		0.784		25		0.292		25		0.182	
30	1.57*		0.0917	30	0.955*		0.0774	30	0.401*		0.0593	30	0.269		0.0535
40	1.68*	1.60	0.0854	40	1.11*	1.04	0.0771	40	0.489*	0.436	0.0534	40	0.328	0.280	0.0479
50	1.78*	1.71	0.0793	50	1.23*	1.17	0.0656	50	0.567*	0.518	0.0488	50	0.382	0.339	0.0436
60	1.88*	1.81	0.0736	60	1.34*	1.28	0.0608	60	0.643*	0.598	0.0451	60	0.436	0.396	0.0402
70	1.98*	1.90	0.0684	70	1.43*	1.38	0.0566	70	0.715*	0.673	0.0419	70	0.488	0.451	0.0374
80	2.08*	1.95	0.0638	80	1.51*	1.46	0.0529	80	0.779*	0.740	0.0392	80	0.537	0.502	0.0350
90	2.18*	2.04	0.0597	90	1.60*	1.55	0.0497	90	0.846*	0.809	0.0369	90	0.587	0.554	0.0329
100	2.16*	2.10	0.0561	100	1.68*	1.64	0.0468	100	0.910*	0.875	0.0349	100	0.635*	0.604	0.0312
150	2.45*	2.37	0.0459	150	2.00*	1.97	0.0366	150	1.19*	1.16	0.0278	150	0.857*	0.832	0.0249
200	2.58*	2.52	0.0365	200	2.18*	2.15	0.0302	200	1.40*	1.38	0.0234	200	1.04*	1.02	0.0211
250	2.64*	2.61	0.0292	250	2.30*	2.28	0.0258	250	1.57*	1.55	0.0203	250	1.20*	1.18	0.0184
273	2.68*	2.63	0.0272	273	2.35*	2.33	0.0242	273	1.63*	1.61	0.0192	273	1.27*	1.25	0.0175
300	2.69*	2.64	0.0252	300	2.40*	2.37	0.0226	300	1.70*	1.69	0.0181	300	1.33*	1.32	0.0165
350	2.72*	2.69	0.0222	350	2.45*	2.43	0.0201	350	1.81*	1.79	0.0163	350	1.45*	1.43	0.0150
400	2.78*	2.73	0.0196	400	2.51*	2.49	0.0181	400	1.91*	1.89	0.0149	400	1.55*	1.54	0.0137
500	2.80*	2.78	0.0163	500	2.57*	2.55	0.0152	500	2.04*	2.03	0.0128	500	1.70*	1.69	0.0119
600	2.79*	2.77	0.0138	600	2.62*	2.61	0.0130	600	2.14*	2.13	0.0113	600	1.82*	1.81	0.0105
700	2.79*	2.74	0.0121	700	2.62*	2.61	0.0115	700	2.20*	2.19	0.0101	700	1.90*	1.89	0.00949
800	2.71*	2.70	0.0107	800	2.59*	2.58	0.0102	800	2.22*	2.21	0.00914	800	1.95*	1.94	0.00866
900	2.68*	2.64	0.0098	900	2.54*	2.54	0.00923	900	2.23*	2.22	0.00837	900	1.98*	1.98	0.00797
1000	2.60*	2.60	0.00970	1000	2.52*	2.51	0.00841	1000	2.23*	2.22	0.00772	1000	2.01*	2.00	0.00740
1100	2.53*	2.58	0.00796	1100	2.46*	2.45	0.00773	1100	2.21*	2.21	0.00717	1100	2.01*	2.01	0.00691
1200	2.47*	2.46	0.00733	1200	2.41*	2.40	0.00715	1200	2.19*	2.18	0.00670	1200	2.00*	2.00	0.00649

† Uncertainties of the total thermal conductivity, k, are as follows:

97.00 Au - 0.50 Pd  $\pm 10\%$  at moderate temperature and above  $\pm 10\%$  at extreme temperature.96.00 Au - 1.00 Pd  $\pm 10\%$  at moderate temperature and above  $\pm 10\%$  at extreme temperature.97.00 Au - 2.00 Pd  $\pm 10\%$  at moderate temperature and above  $\pm 10\%$  at extreme temperature.96.00 Au - 5.00 Pd  $\pm 10\%$  at moderate temperature and above  $\pm 10\%$  at extreme temperature.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 50.00% (52.94 At. %) Pd: 10.00% (17.06 At. %)				Au: 55.00% (75.38 At. %) Pd: 15.00% (24.62 At. %)				Au: 80.00% (68.36 At. %) Pd: 20.00% (31.64 At. %)				Au: 75.00% (61.84 At. %) Pd: 25.00% (38.16 At. %)			
$\rho_0 = 6.100 \mu\Omega\text{cm}$				$\rho_0 = 8.85 \mu\Omega\text{cm}$				$\rho_0 = 10.85 \mu\Omega\text{cm}$				$\rho_0 = 12.74 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.0159		4		0.0113		4		0.00901		4		0.00767	
6		0.0238		6		0.0169		6		0.0135		6		0.0115	
8		0.0317		8		0.0226		8		0.0190		8		0.0153	
10		0.0397		10		0.0282		10		0.0235		10		0.0192	
15		0.0595		15		0.0424		15		0.0338		15		0.0268	
20		0.0793		20		0.0565		20		0.0450		20		0.0384	
25		0.0945		25		0.0694		25		0.0554		25		0.0474	
30		0.115	0.0409	30		0.0829		30		0.0663		30		0.0566	
40	0.104	0.151	0.0435	40	0.152*	0.109	0.0429	40		0.0876		40		0.0749	
50	0.206	0.197	0.0395	50	0.174*	0.135	0.0389	50	0.148*	0.109	0.0396	50		0.0929	
60	0.268	0.222	0.0363	60	0.197*	0.161	0.0359	60	0.166*	0.129	0.0364	60	0.149*	0.111	0.0376
70	0.298	0.246	0.0338	70	0.239*	0.186	0.0333	70	0.184*	0.150	0.0339	70	0.163*	0.126	0.0350
80	0.309	0.269	0.0316	80	0.242*	0.211	0.0312	80	0.202*	0.170	0.0317	80	0.178*	0.146	0.0328
90	0.351	0.322	0.0298	90	0.265*	0.235	0.0294	90	0.220*	0.190	0.0299	90	0.194*	0.163	0.0310
100	0.383*	0.364	0.0282	100	0.287*	0.259	0.0279	100	0.238*	0.209	0.0284	100	0.209*	0.180	0.0294
150	0.589*	0.596	0.0237	150	0.397*	0.375	0.0225	150	0.327*	0.304	0.0230	150	0.285*	0.261	0.0238
200	0.698*	0.640	0.0193	200	0.500*	0.481	0.0192	200	0.412*	0.392	0.0196	200	0.357*	0.337	0.0204
250	0.778*	0.701	0.0170	250	0.594*	0.577	0.0169	250	0.491*	0.473	0.0173	250	0.423*	0.406	0.0180
273	0.823*	0.813	0.0161	273	0.635*	0.169	0.0161	273	0.525*	0.509	0.0165	273	0.452*	0.435	0.0171
300	0.868	0.871	0.0153	300	0.682*	0.666	0.0152	300	0.565	0.549	0.0156	300	0.486*	0.470	0.0162
350	0.963*	0.909	0.0139	350	0.762*	0.748	0.0139	350	0.631*	0.617	0.0143	350	0.544*	0.529	0.0149
400	1.07*	1.06	0.0128	400	0.838*	0.826	0.0129	400	0.695*	0.682	0.0132	400	0.599*	0.586	0.0138
500	1.23*	1.21	0.0112	500	0.966*	0.955	0.0113	500	0.806*	0.795	0.0116	500	0.696*	0.686	0.0121
600	1.34*	1.33	0.00998	600	1.08*	1.07	0.0101	600	0.909*	0.899	0.0104	600	0.785*	0.774	0.0108
700	1.44*	1.43	0.00907	700	1.17*	1.16	0.00917	700	0.996*	0.986	0.00947	700	0.861*	0.851	0.00989
800	1.51*	1.50	0.00832	800	1.25*	1.24	0.00844	800	1.07*	1.06	0.00873	800	0.927*	0.918	0.00912
900	1.57*	1.56	0.00771	900	1.31*	1.30	0.00784	900	1.13*	1.12	0.00812	900	0.981*	0.973	0.00849
1000	1.61*	1.61	0.00730	1000	1.37*	1.36	0.00733	1000	1.19*	1.18	0.00760	1000	1.03*	1.02	0.00796
1100	1.64*	1.64	0.00676	1100	1.41*	1.40	0.00690	1100	1.23*	1.22	0.00716	1100	1.06*	1.05	0.00750
1200	1.66*	1.66	0.00637	1200	1.43*	1.43	0.00652	1200	1.26*	1.25	0.00678	1200	1.09*	1.09	0.00711

† Uncertainties of the total thermal conductivity, k, are as follows:

50.00 Au - 10.00 Pd: ±10% at moderate temperature and above ±10% at extreme temperature.

55.00 Au - 15.00 Pd: ±10% at moderate temperature and above ±10% at extreme temperature.

60.00 Au - 20.00 Pd: ±10% at moderate temperature and above ±10% at extreme temperature.

75.00 Au - 25.00 Pd: ±10% at moderate temperature and above ±10% at extreme temperature.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued) †

Au: 70.00% (55.76 At. %) Pd: 30.00% (44.24 At. %)				Au: 65.00% (50.08 At. %) Pd: 35.00% (49.92 At. %)				Au: 60.00% (44.76 At. %) Pd: 40.00% (55.24 At. %)				Au: 55.00% (39.77 At. %) Pd: 45.00% (60.23 At. %)			
$\rho_0 = 15.00 \mu\Omega \text{ cm}$				$\rho_0 = 20.57 \mu\Omega \text{ cm}$				$\rho_0 = 23.55 \mu\Omega \text{ cm}$				$\rho_0 = 23.19 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.00432		4		0.00475		4		0.00415		4		0.00421	
6		0.00977		6		0.00713		6		0.00622		6		0.00632	
8		0.0130		8		0.00950		8		0.00830		8		0.00843	
10		0.0163		10		0.0119		10		0.0104		10		0.0105	
15		0.0244		15		0.0178		15		0.0156		15		0.0158	
20		0.0326		20		0.0238		20		0.0207		20		0.0211	
25		0.0402		25		0.0294		25		0.0257		25		0.0261	
30		0.0481		30		0.0352		30		0.0308		30		0.0312	
40		0.0637		40		0.0466		40		0.0408		40		0.0413	
50		0.0790		50		0.0579		50		0.0507		50		0.0512	
60	0.133*	0.0943	0.0393	60		0.0688		60		0.0605		60		0.0608	
70	0.146*	0.109	0.0545	70		0.0797		70		0.0701		70		0.0703	
80	0.159*	0.124	0.0693	80	0.127*	0.0905	0.0360	80	0.117	0.0793	0.0360	80		0.0796	
90	0.172*	0.139	0.0843	90	0.135*	0.101	0.0340	90	0.125	0.0687	0.0341	90		0.0689	
100	0.184*	0.153	0.0997	100	0.144*	0.112	0.0323	100	0.132*	0.0980	0.0341	100		0.0976	
150	0.240*	0.221	0.0249	150	0.188*	0.162	0.0262	150	0.169*	0.142	0.0277	150	0.169*	0.140	0.0295
200	0.285	0.265	0.0213	200	0.231*	0.209	0.0224	200	0.206*	0.162	0.0238	200	0.204*	0.178	0.0253
250	0.331	0.342	0.0188	250	0.272*	0.282	0.0199	250	0.240*	0.219	0.0210	250	0.236*	0.213	0.0224
273	0.365*	0.367	0.0179	273	0.290*	0.271	0.0189	273	0.256*	0.236	0.0200	273	0.250*	0.229	0.0213
300	0.413*	0.396	0.0170	300	0.311	0.293	0.0179	300	0.274	0.255	0.0190	300	0.267*	0.247	0.0202
350	0.461*	0.445	0.0156	350	0.349	0.333	0.0164	350	0.308*	0.291	0.0174	350	0.298*	0.280	0.0195
400	0.507*	0.492	0.0144	400	0.387	0.371	0.0152	400	0.341*	0.325	0.0161	400	0.329*	0.311	0.0173
500	0.589*	0.577	0.0127	500	0.460	0.447	0.0134	500	0.405*	0.391	0.0142	500	0.385*	0.370	0.0151
600	0.662*	0.651	0.0114	600	0.531	0.519	0.0120	600	0.467*	0.456	0.0128	600	0.441*	0.427	0.0136
700	0.723*	0.719	0.0104	700	0.599	0.586	0.0110	700	0.528*	0.517	0.0118	700	0.495*	0.483	0.0124
800	0.789*	0.779	0.00959	800	0.660	0.650	0.0101	800	0.587*	0.576	0.0107	800	0.546*	0.535	0.0114
900	0.843*	0.833	0.00893	900	0.716	0.706	0.00944	900	0.640*	0.630	0.0100	900	0.593*	0.582	0.0107
1000	0.889*	0.880	0.00838	1000	0.767	0.758	0.00895	1000	0.688*	0.679	0.00939	1000	0.634*	0.624	0.0100
1100	0.939*	0.932	0.00790	1100	0.815	0.807	0.00835	1100	0.734*	0.725	0.00886	1100	0.680*	0.671	0.00943
1200	0.973*	0.965	0.00749	1200	0.864	0.856	0.00792	1200	0.782*	0.773	0.00840	1200	0.724*	0.715	0.00894

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 70.00 Au - 30.00 Pd:  $\pm 10\%$  at moderate temperatures and above  $\pm 10\%$  at extreme temperatures.
- 65.00 Au - 35.00 Pd:  $\pm 10\%$  at moderate temperatures and above  $\pm 10\%$  at extreme temperatures.
- 60.00 Au - 40.00 Pd:  $\pm 10\%$  at moderate temperatures and above  $\pm 10\%$  at extreme temperatures.
- 55.00 Au - 45.00 Pd:  $\pm 15\%$ .

\* Provisional values.

† In temperature ranges where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 50.00% (35.07 At. %) Pd: 50.00% (64.93 At. %)				Au: 45.00% (30.65 At. %) Pd: 55.00% (89.35 At. %)				Au: 40.00% (26.48 At. %) Pd: 60.00% (73.52 At. %)				Au: 35.00% (22.53 At. %) Pd: 65.00% (77.47 At. %)			
$\rho_0 = 21.54 \mu\Omega\text{cm}$				$\rho_0 = 19.33 \mu\Omega\text{cm}$				$\rho_0 = 17.00 \mu\Omega\text{cm}$				$\rho_0 = 14.70 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.00454		4		0.00505		4		0.00575		4		0.00665	
6		0.00681		6		0.00759		6		0.00862		6		0.00997	
8		0.00997		8		0.0101		8		0.0115		8		0.0133	
10		0.0113		10		0.0126		10		0.0144		10		0.0164	
15		0.0179		15		0.0190		15		0.0216		15		0.0249	
20		0.0237		20		0.0253		20		0.0287		20		0.0332	
25		0.0281		25		0.0313		25		0.0353		25		0.0406	
30		0.0326		30		0.0373		30		0.0421		30		0.0486	
40		0.0444		40		0.0462		40		0.0533		40		0.0635	
50		0.0548		50		0.0605		50		0.0678		50		0.0776	
60		0.0649		60		0.0714		60		0.0796		60		0.0906	
70		0.0749		70		0.0820		70		0.0914		70		0.103	
80		0.0845		80		0.0923		80		0.103		80		0.116	
90		0.0941		90		0.102		90		0.114		90		0.137	
100		0.103		100		0.112		100		0.124		100		0.139	
150	0.179±	0.146±	0.0315±	150		0.186		150		0.170		150		0.187	
200	0.211±	0.164±	0.0370±	200	0.223±	0.194±	0.0290±	200	0.241±	0.209±	0.0314±	200	0.261±	0.237±	0.0343±
250	0.243±	0.218±	0.0439±	250	0.264±	0.228±	0.0257±	250	0.271±	0.243±	0.0278±	250	0.291±	0.261±	0.0303±
273	0.259±	0.239±	0.0459±	273	0.287±	0.243±	0.0245±	273	0.284±	0.258±	0.0265±	273	0.304±	0.278±	0.0288±
300	0.271±	0.249±	0.0481±	300	0.293±	0.260±	0.0233±	300	0.300±	0.274±	0.0251±	300	0.319±	0.288±	0.0273±
350	0.301±	0.281±	0.0198±	350	0.312±	0.291±	0.0213±	350	0.329±	0.306±	0.0230±	350	0.349±	0.324±	0.0250±
400	0.330±	0.311±	0.0184±	400	0.340±	0.320±	0.0197±	400	0.357±	0.335±	0.0213±	400	0.374±	0.351±	0.0231±
500	0.383±	0.367±	0.0161±	500	0.392±	0.375±	0.0173±	500	0.409±	0.391±	0.0187±	500	0.433±	0.413±	0.0203±
600	0.436±	0.420±	0.0145±	600	0.442±	0.428±	0.0158±	600	0.459±	0.443±	0.0169±	600	0.483±	0.464±	0.0183±
700	0.489±	0.479±	0.0132±	700	0.489±	0.474±	0.0142±	700	0.506±	0.490±	0.0153±	700	0.538±	0.513±	0.0166±
800	0.539±	0.517±	0.0123±	800	0.531±	0.518±	0.0131±	800	0.549±	0.535±	0.0141±	800	0.570±	0.554±	0.0153±
900	0.573±	0.551±	0.0114±	900	0.571±	0.559±	0.0122±	900	0.588±	0.575±	0.0132±	900	0.609±	0.594±	0.0143±
1000	0.619±	0.594±	0.0107±	1000	0.609±	0.598±	0.0115±	1000	0.626±	0.614±	0.0123±	1000	0.646±	0.633±	0.0134±
1100	0.667±	0.647±	0.0101±	1100	0.639±	0.628±	0.0104±	1100	0.653±	0.642±	0.0116±	1100	0.683±	0.671±	0.0126±
1200	0.701±	0.685±	0.0095±	1200	0.686±	0.676±	0.0102±	1200	0.700±	0.689±	0.0110±	1200	0.719±	0.707±	0.0120±

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 50.00 Au - 50.00 Pd: ±15% at moderate temperature and above ±15% at extreme temperature.
- 45.00 Au - 55.00 Pd: ±15% at moderate temperature and above ±15% at extreme temperature.
- 40.00 Au - 60.00 Pd: ±15% at moderate temperature and above ±15% at extreme temperature.
- 35.00 Au - 65.00 Pd: ±15% at moderate temperature and above ±15% at extreme temperature.

‡ Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>

Au: 30.00% (18.80 At.%) Pd: 70.00% (81.20 At.%)				Au: 25.00% (15.26 At.%) Pd: 75.00% (84.74 At.%)				Au: 20.00% (11.90 At.%) Pd: 80.00% (88.10 At.%)				Au: 15.00% (8.70 At.%) Pd: 85.00% (91.30 At.%)			
$\rho_0 = 13.00 \mu\Omega \text{ cm}$				$\rho_0 = 10.19 \mu\Omega \text{ cm}$				$\rho_0 = 8.00 \mu\Omega \text{ cm}$				$\rho_0 = 5.850 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.00752		4		0.00959		4		0.0122		4		0.0167	
6		0.0113		6		0.0144		6		0.0183		6		0.0251	
8		0.0150		8		0.0192		8		0.0244		8		0.0334	
10		0.0188		10		0.0240		10		0.0305		10		0.0417	
15		0.0282		15		0.0360		15		0.0458		15		0.0636	
20		0.0376		20		0.0479		20		0.0611		20		0.0835	
25		0.0459		25		0.0584		25		0.0761		25		0.0993	
30		0.0545		30		0.0692		30		0.0876		30		0.116	
40		0.0710		40		0.0897		40		0.112		40		0.147	
50		0.0864		50		0.108		50		0.134		50		0.178	
60		0.101		60		0.125		60		0.153		60		0.194	
70		0.114		70		0.140		70		0.170		70		0.214	
80		0.128		80		0.155		80		0.187		80		0.232	
90		0.140		90		0.170		90		0.202		90		0.250	
100		0.152		100		0.183		100		0.216		100		0.264	
150	0.280*	0.262	0.0376*	150	0.236	0.236	0.0418*	150	0.271	0.271	0.0472*	150	0.317	0.317	0.0536*
200	0.311*	0.277*	0.0332*	200	0.319*	0.278*	0.0369*	200	0.360*	0.313*	0.0417*	200	0.433*	0.364*	0.0462*
250	0.324*	0.292*	0.0316*	250	0.349*	0.312*	0.0359*	250	0.387*	0.345*	0.0386*	250	0.443*	0.387*	0.0458*
273	0.341*	0.311*	0.0300*	273	0.361*	0.326*	0.0351*	273	0.399*	0.359*	0.0375*	273	0.457*	0.416*	0.0434*
300	0.373*	0.344*	0.0274*	300	0.377*	0.344*	0.0333*	300	0.413*	0.376*	0.0343*	300	0.487*	0.447*	0.0396*
350	0.402*	0.377*	0.0254*	350	0.408*	0.378*	0.0304*	350	0.444*	0.410*	0.0317*	350	0.516*	0.479*	0.0368*
400	0.430*	0.407*	0.0223*	400	0.438*	0.409*	0.0282*	400	0.474*	0.442*	0.0277*	400	0.570*	0.539*	0.0319*
500	0.459*	0.437*	0.0200*	500	0.492*	0.467*	0.0247*	500	0.528*	0.500*	0.0248*	500	0.619*	0.591*	0.0285*
600	0.511*	0.491*	0.0182*	600	0.542*	0.520*	0.0221*	600	0.578*	0.553*	0.0226*	600	0.668*	0.640*	0.0259*
700	0.567*	0.539*	0.0168*	700	0.598*	0.568*	0.0201*	700	0.626*	0.604*	0.0208*	700	0.709*	0.685*	0.0237*
800	0.622*	0.595*	0.0150*	800	0.633*	0.615*	0.0185*	800	0.672*	0.652*	0.0183*	800	0.757*	0.735*	0.0205*
900	0.649*	0.630*	0.0146*	900	0.677*	0.660*	0.0172*	900	0.717*	0.696*	0.0169*	900	0.797*	0.776*	0.0193*
1000	0.681*	0.667*	0.0138*	1000	0.716*	0.700*	0.0161*	1000	0.756*	0.736*	0.0160*	1000	0.830*	0.817*	0.0163*
1100	0.718*	0.704*	0.0130*	1100	0.754*	0.739*	0.0152*	1100	0.795*	0.775*	0.0144*	1100	0.871*	0.853*	0.0132*
1200	0.753*	0.740*	0.0130*	1200	0.791*	0.776*	0.0144*	1200	0.832*	0.816*	0.0144*	1200	0.871*	0.853*	0.0132*

\* Uncertainties of the total thermal conductivity,  $k$ , are as follows:30.00 Au - 70.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.25.00 Au - 75.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.20.00 Au - 80.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.15.00 Au - 85.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.

† Provisional value.

\* In temperature ranges where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 10.00% ( 5.66 At. %) Pd: 90.00% (94.34 At. %)				Au: 5.00% ( 2.76 At. %) Pd: 95.00% (97.24 At. %)				Au: 3.00% ( 1.64 At. %) Pd: 97.00% (98.36 At. %)				Au: 1.00% ( 0.54 At. %) Pd: 99.00% (99.46 At. %)			
$\rho_0 = 3.850 \mu\Omega \text{ cm}$				$\rho_0 = 1.900 \mu\Omega \text{ cm}$				$\rho_0 = 1.100 \mu\Omega \text{ cm}$				$\rho_0 = 0.3000 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.0354		4		0.0514		4		0.0688		4		0.257	
6		0.0601		6		0.0771		6		0.133		6		0.396	
8		0.0806		8		0.103		8		0.178		8		0.514	
10		0.0936		10		0.129		10		0.222		10		0.643	
15		0.0983		15		0.193		15		0.333		15		0.964	
20		0.137		20		0.257		20		0.444		20		1.29	
25		0.151		25		0.296		25		0.483		25		1.16	
30		0.175		30		0.337		30		0.533		30		1.15	
40		0.237		40		0.393		40		0.576		40		1.03	
50		0.267		50		0.418		50		0.569		50		0.871	
60		0.299		60		0.423		60		0.560		60		0.782	
70		0.306		70		0.430		70		0.537		70		0.699	
80		0.305		80		0.435		80		0.527		80		0.663	
90		0.322		90		0.444		90		0.520		90		0.637	
100		0.333		100		0.447		100		0.515		100		0.615	
150		0.377		150		0.482		150		0.505		150		0.559	
200		0.407		200		0.475		200		0.506		200		0.545	
250	0.489±	0.451±	0.0383±	250	0.566±	0.459±	0.0775±	250	0.610±	0.517±	0.0930±	250		0.548	
273	0.497±	0.443±	0.0553±	273	0.571±	0.497±	0.0782±	273	0.612±	0.524±	0.0879±	273	0.671±	0.563±	0.118±
300	0.500±	0.467±	0.0533±	300	0.580±	0.510±	0.0692±	300	0.616±	0.534±	0.0836±	300	0.675±	0.565±	0.110±
350	0.540±	0.500±	0.0476±	350	0.606±	0.544±	0.0627±	350	0.650±	0.576±	0.0745±	350	0.691±	0.593±	0.0977±
400	0.560±	0.523±	0.0439±	400	0.629±	0.572±	0.0575±	400	0.663±	0.594±	0.0679±	400	0.706±	0.618±	0.0878±
500	0.617±	0.578±	0.0383±	500	0.677±	0.627±	0.0495±	500	0.704±	0.646±	0.0579±	500	0.739±	0.668±	0.0730±
600	0.660±	0.621±	0.0339±	600	0.720±	0.677±	0.0437±	600	0.746±	0.695±	0.0506±	600	0.778±	0.715±	0.0626±
700	0.711±	0.681±	0.0307±	700	0.761±	0.722±	0.0392±	700	0.786±	0.741±	0.0451±	700	0.819±	0.761±	0.0546±
800	0.764±	0.724±	0.0281±	800	0.806±	0.770±	0.0356±	800	0.829±	0.788±	0.0406±	800	0.859±	0.807±	0.0465±
900	0.809±	0.774±	0.0259±	900	0.850±	0.817±	0.0326±	900	0.872±	0.835±	0.0370±	900	0.899±	0.865±	0.0437±
1000	0.848±	0.817±	0.0241±	1000	0.887±	0.857±	0.0301±	1000	0.909±	0.875±	0.0340±	1000	0.933±	0.893±	0.0397±
1100	0.889±	0.857±	0.0226±	1100	0.925±	0.897±	0.0280±	1100	0.949±	0.917±	0.0314±	1100	0.972±	0.935±	0.0364±
1200	0.918±	0.887±	0.0213±	1200	0.958±	0.922±	0.0262±	1200	0.984±	0.955±	0.0293±	1200	1.01±	0.969±	0.0306±

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 10.00 Au - 90.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.
- 5.00 Au - 95.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.
- 3.00 Au - 97.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.
- 1.00 Au - 99.00 Pd:  $\pm 15\%$  at moderate temperature and above  $\pm 15\%$  at extreme temperature.

± Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 19. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-PALLADIUM ALLOY SYSTEM (continued)†  
 † Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>

Au 0.50% ( 0.27 At. %) Pd 99.50% ( 99.73 At. %)							
$\rho_0 = 0.3000 \mu\Omega \text{ cm}$							
T	k	$k_e$	$k_g$				
4		0.376					
6		0.564					
8		0.752					
10		0.940					
15		1.41					
20		1.88					
25		1.91					
30		1.48					
40		1.16					
50		0.944					
60		0.803					
70		0.728					
80		0.680					
90		0.667					
100		0.641					
150		0.593					
200		0.553					
250		0.553					
273	0.691±	0.588±	0.133±				
300	0.690±	0.588±	0.133±				
350	0.769±	0.597±	0.106±				
400	0.719±	0.683±	0.096±				
500	0.751±	0.672±	0.0731±				
600	0.788±	0.721±	0.0671±				
700	0.833±	0.765±	0.0651±				
800	0.863±	0.811±	0.0613±				
900	0.903±	0.867±	0.0480±				
1000	0.930±	0.906±	0.0416±				
1100	0.970±	0.949±	0.0380±				
1200	1.02±	0.99±	0.0360±				

† Uncertainties of the total thermal conductivity, k, are as follows:

0.50 Au - 99.50 Pd: ±15% at moderate temperature and above ±15% at extrinsic temperature.

± Provisional value.

\* In temperature range where no experimental thermal conductivity data are available.

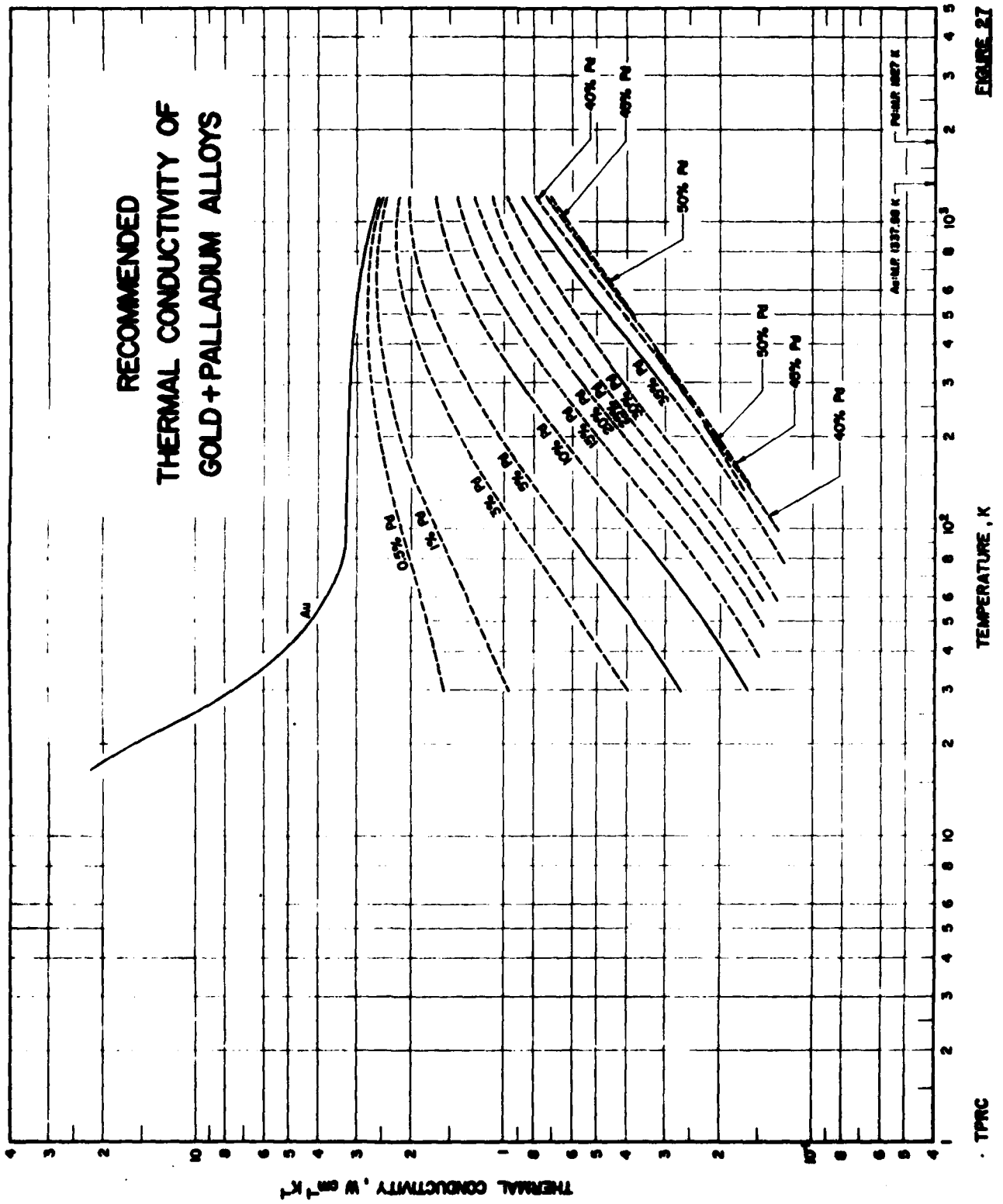


FIGURE 27



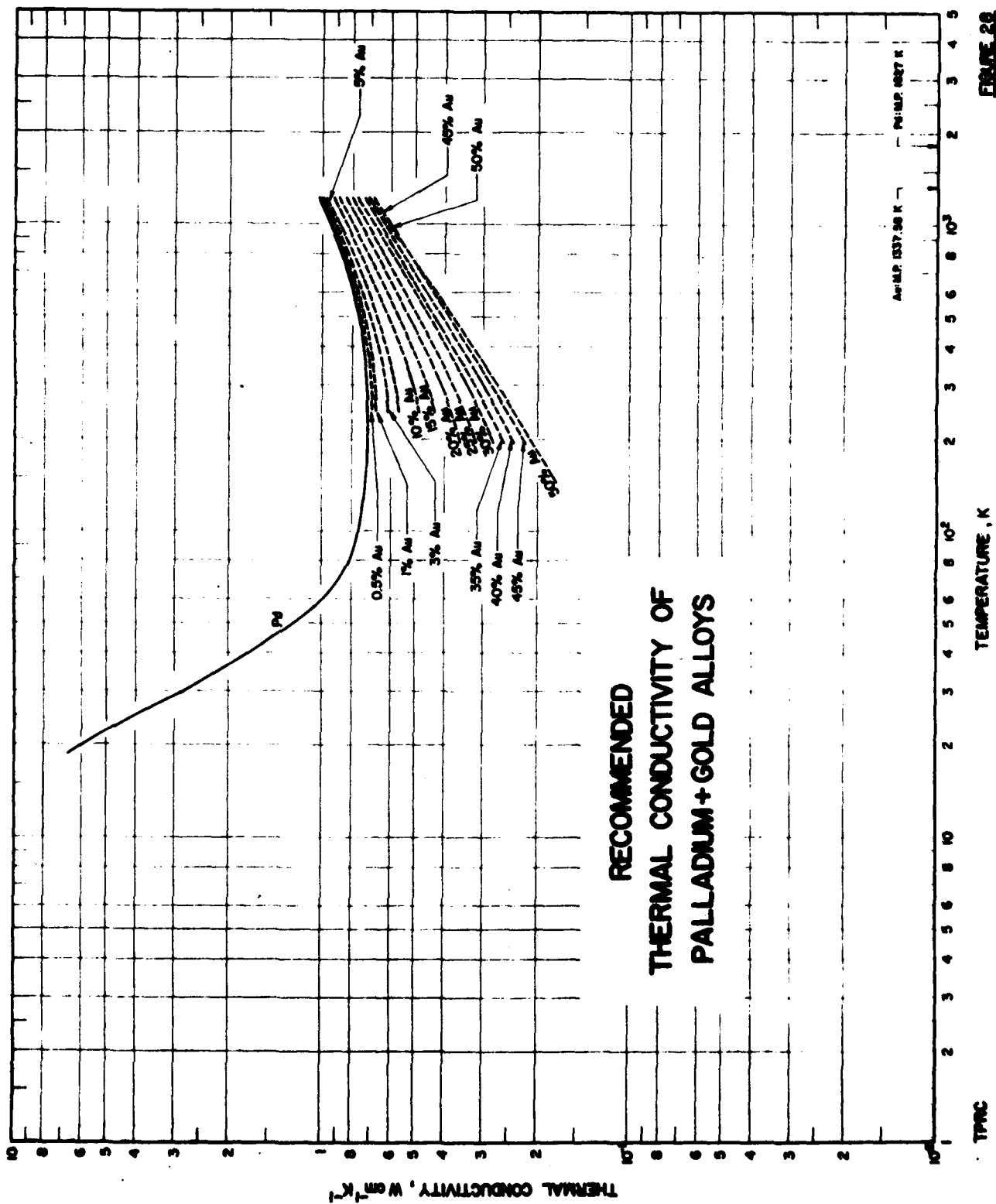


FIGURE 28

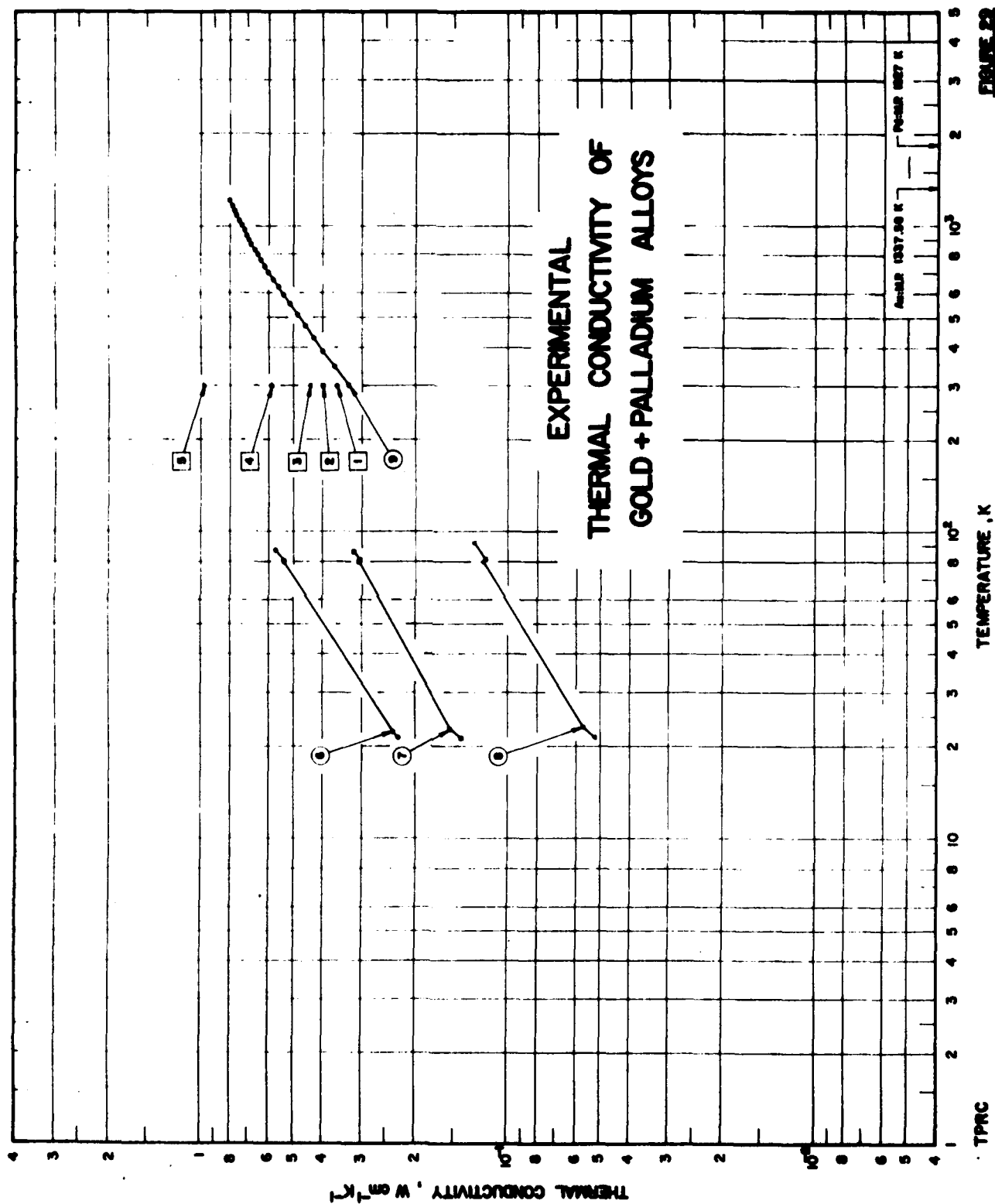


FIGURE 22

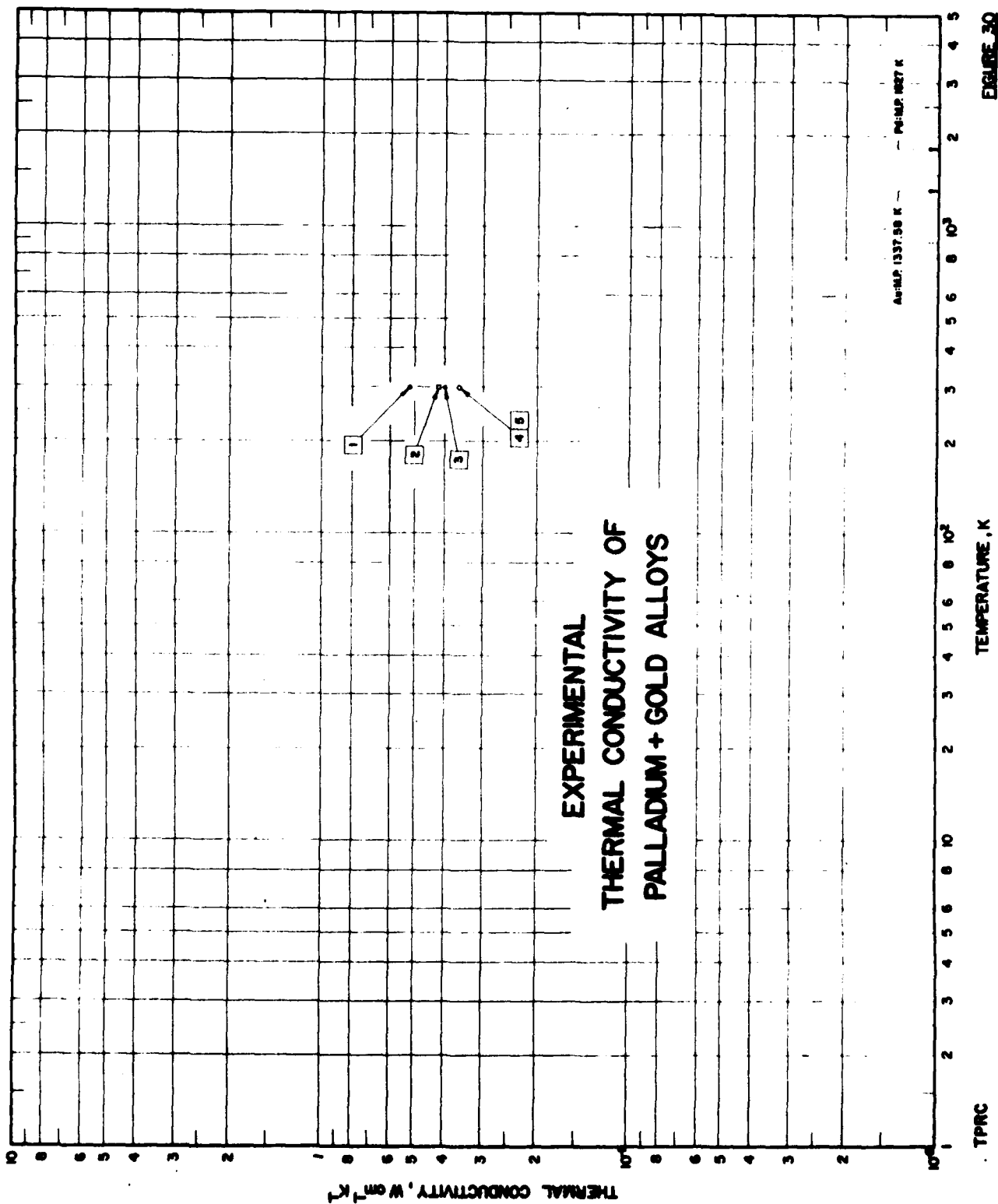


FIGURE 30

TABLE 20. THERMAL CONDUCTIVITY OF GOLD - PALLADIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Authors	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Au Pd	Composition (continued), Specifications, and Remarks
1 93	Schalze, F.A.	1911	E	296.2		50 50	Electrical conductivity $3.74 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
2 93	Schalze, F.A.	1911	E	298.2		60 40	Electrical conductivity $4.02 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
3 93	Schalze, F.A.	1911	E	298.2		70 30	Electrical conductivity $5.45 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
4 93	Schalze, F.A.	1911	E	298.2		80 20	Electrical conductivity $7.82 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
5 93	Schalze, F.A.	1911	E	298.2		90 10	Electrical conductivity $13.27 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
6 61	Grüneisen, E. and Reddemann, H.	1934	L	21-87	22	95 5	Calculated composition; heated at 800 C for 2 hr; electrical resistivity 3.479, 3.939, and $5.44 \mu\Omega \text{ cm}$ at 22, 83, and 273 K, respectively.
7 61	Grüneisen, E. and Reddemann, H.	1934	L	21-86	23	90 10	Calculated composition; heated at 800 C for 2 hr; electrical resistivity 7.175, 7.605, and $9.10 \mu\Omega \text{ cm}$ at 22, 83, and 273 K, respectively.
8 61	Grüneisen, E. and Reddemann, H.	1934	L	21-92	24	60.1 39.9	Calculated composition; heated at 800 C for 2 hr; electrical resistivity 23.66, 24.46, and $27.1 \mu\Omega \text{ cm}$ at 22, 83, and 273 K, respectively.
9 85	Laubitz, M.J. and Van der Meer, M.P.	1968	L	300-1203	Platinel 1503	65.05 34.95	~1.2 cm in diameter and 10 cm long; supplied by Engelhard Ind.; annealed at 800 to 900 K for 60 hr; electrical resistivity ratio $\rho(273\text{K})/\rho(4\text{K}) = 1.133$ ; electrical resistivity reported as 24.3, 25.1, 25.6, 25.9, 26.4, 26.9, 27.5, 28.2, 28.9, 29.5, 30.1, 30.8, 31.5, 31.9, 33.0 $\mu\Omega \text{ cm}$ at 310, 420, 485, 551, 614, 688, 755, 821, 890, 953, 1012, 1072, 1140, 1198, and 1304 K, respectively; data extracted from smooth curve.

TABLE 21. THERMAL CONDUCTIVITY OF PALLADIUM - GOLD ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Pd Au	Composition (continued), Specifications, and Remarks
1	Schulze, F.A.	1911	E	298.2		90 10	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $6.65 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
2	Schulze, F.A.	1911	E	298.2		80 20	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $5.33 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
3	Schulze, F.A.	1911	E	298.2		70 30	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $4.72 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
4	Schulze, F.A.	1911	E	298.2		60 40	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $3.89 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
5*	Schulze, F.A.	1911	E	298.2		50 50	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $3.74 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.

\* Not shown in figure.

#### 4.8. Gold-Silver Alloy System

The gold-silver alloy system forms a continuous series of solid solutions over the entire range of compositions. Possible existence of ordered structures due to the formation of AgAu intermetallic compound has been reported.

There are 39 sets of experimental data available for the thermal conductivity of this alloy system. Of the 22 data sets available for Au + Ag alloys listed in Table 23 and shown in Figure 33, 9 sets cover only a narrow temperature range from 273 to 373 K, which is the highest temperature at which data exist. Of the 17 data sets for Ag + Au alloys listed in Table 24 and shown in Figure 34, four sets likewise cover only the narrow temperature range from 273 to 373 K, which is also the highest temperature at which data exist.

Thermal conductivities of this alloy system have been reported in four papers [61, 63, 94, 95]. The measurements by Grüneisen and Reddemann [61] (Au + Ag curves 1-2 and Ag + Au curves 1-2) appear to be the most reliable, though there is some uncertainty in the compositions of their gold-rich specimens. Separation of the electronic component from their measured total thermal conductivities gives reasonable values for the lattice component, without much scatter when these  $k_g$  values are plotted against the composition. Values obtained from eq. (35) agree well with the  $k_g$  values derived from the experimental data of Grüneisen and Reddemann. The  $k_g$  values of alloys in this system are generally very small compared with the  $k_e$  values, especially at high temperatures.

The most recent measurements, by Crisp and Rungis [94] (Au + Ag curves 12-20 and Ag + Au curves 8-17), cover a wide range of composition below 300 K. Unfortunately, however, their measurements seem not to be accurate enough to give reasonable lattice thermal conductivities. Separation of the electronic component from their measured total thermal conductivities results in negative values for the lattice component for most of their specimens at 83 and 273 K. In their paper it was mentioned that the separation failed.

Early measurements by Sedström [63] (Au + Ag curves 3-11 and Ag + Au curves 3-7) in 1919 yield positive lattice thermal conductivities at 273 K, but his  $k_g$  values scatter and seem to be high.

Van Baarle et al. [95] have measured the thermal conductivity of dilute gold-rich alloys between 2 and 30 K, but they have reported only the lattice thermal conductivity values. At the present time, it is very difficult to judge the reliability of their results because total thermal conductivities are not reported and the low-temperature results of Crisp and Rungis [94] are somewhat uncertain.

Since the Au-Ag alloy system is a non-transition solid-solution alloy system, for which the calculations from eqs. (12) and (35) should be more reliable, and since the calculated results indeed match well with the reliable experimental data of Grüneisen and

Reddemann [61], the recommendations were entirely based on the calculated values. The recommended total thermal conductivity values are in agreement with the data of Grüneisen and Reddemann [61] (Au + Ag curves 1-2 and Ag-Au curves 1-2) around 80 to 90 K to within 4%, with the data of Crisp and Rungis [94] (Au + Ag curves 14, 15, and 17, and Ag + Au curves 9-13, and 15) between 40 and 200 K to within 10%, and with the data of Sedström [63] (Au + Ag curves 8-11 and Ag + Au curves 4, 6, and 7) around room temperature to within 5%.

The recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 22 for 25 alloy compositions mostly covering the temperature range from 40 K to the solidus points. These values are for well-annealed disordered alloys. For two alloys with 1% and 3% Ag, the tabulated values cover the range down to 4 K. The  $k_e$  values are given from 4 K to the solidus points for all 25 alloy compositions. The values for  $k$  are also shown in Figures 31 and 32 and their uncertainties are stated in a footnote to Table 22, in which the values of residual electrical resistivity for the alloys are also given. The uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 99.50% (99.09 At.%) Ag: 0.50% (0.91 At.%)				Au: 99.00% (99.19 At.%) Ag: 1.00% (1.81 At.%)				Au: 97.00% (94.66 At.%) Ag: 3.00% (5.34 At.%)				Au: 95.00% (91.23 At.%) Ag: 5.00% (8.77 At.%)			
$\rho_0 = 0.39 \mu\Omega\text{cm}$				$\rho_0 = 0.530 \mu\Omega\text{cm}$				$\rho_0 = 1.52 \mu\Omega\text{cm}$				$\rho_0 = 2.470 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.349		4	0.219 <sup>†</sup>	0.184	0.0345 <sup>†</sup>	4	0.0869 <sup>†</sup>	0.0643	0.0226 <sup>†</sup>	4		0.0396	
6		0.324		6	0.354 <sup>†</sup>	0.277	0.0769 <sup>†</sup>	6	0.146 <sup>†</sup>	0.0964	0.0500 <sup>†</sup>	6		0.0593	
8		0.696		8	0.486 <sup>†</sup>	0.369	0.117 <sup>†</sup>	8	0.202 <sup>†</sup>	0.129	0.0729 <sup>†</sup>	8		0.0791	
10		0.873		10	0.604 <sup>†</sup>	0.461	0.143 <sup>†</sup>	10	0.250 <sup>†</sup>	0.161	0.0896 <sup>†</sup>	10		0.0989	
15		1.31		15	0.855 <sup>†</sup>	0.691	0.164 <sup>†</sup>	15	0.350 <sup>†</sup>	0.241	0.109 <sup>†</sup>	15		0.146	
20		1.75		20	1.06 <sup>†</sup>	0.922	0.160 <sup>†</sup>	20	0.435 <sup>†</sup>	0.321	0.114 <sup>†</sup>	20		0.196	
25		1.86		25	1.21 <sup>†</sup>	1.06	0.150 <sup>†</sup>	25	0.497 <sup>†</sup>	0.390	0.107 <sup>†</sup>	25		0.241	
30		2.01		30	1.33 <sup>†</sup>	1.19	0.137 <sup>†</sup>	30	0.554 <sup>†</sup>	0.454	0.0999 <sup>†</sup>	30		0.284	
40	2.19	2.07	0.117	40	1.49	1.37	0.118	40	0.657	0.571	0.0861	40	0.437	0.363	0.0740
50	2.23	2.12	0.109	50	1.60	1.50	0.104	50	0.746	0.669	0.0770	50	0.503	0.437	0.0661
60	2.28	2.16	0.100	60	1.68	1.59	0.0829	60	0.836	0.767	0.0692	60	0.567	0.507	0.0600
70	2.33	2.24	0.0822	70	1.77	1.69	0.0840	70	0.917	0.853	0.0637	70	0.628	0.573	0.0551
80	2.36	2.27	0.0649	80	1.84	1.76	0.0763	80	0.989	0.930	0.0587	80	0.686	0.634	0.0515
90	2.42	2.34	0.0785	90	1.92	1.85	0.0701	90	1.06	1.01	0.0546	90	0.747	0.694	0.0531
100	2.49	2.41	0.0728	100	2.00	1.93	0.0657	100	1.14	1.08	0.0515	100	0.796	0.753	0.0450
150	2.70	2.65	0.0538	150	2.29	2.24	0.0489	150	1.43	1.39	0.0396	150	1.05 <sup>*</sup>	1.01	0.0352
200	2.80	2.76	0.0412	200	2.44	2.41	0.0388	200	1.64 <sup>*</sup>	1.61	0.0326	200	1.25 <sup>*</sup>	1.22	0.0292
250	2.83	2.80	0.0337	250	2.53	2.50	0.0320	250	1.80 <sup>*</sup>	1.77	0.0276	250	1.41 <sup>*</sup>	1.38	0.0250
273	2.85	2.82	0.0311	273	2.56	2.53	0.0297	273	1.86 <sup>*</sup>	1.83	0.0258	273	1.47	1.45	0.0235
300	2.86	2.83	0.0285	300	2.59	2.56	0.0273	300	1.92 <sup>*</sup>	1.90	0.0240	300	1.54	1.52	0.0219
350	2.89 <sup>*</sup>	2.84	0.0247	350	2.64 <sup>*</sup>	2.61	0.0236	350	2.02 <sup>*</sup>	2.00	0.0212	350	1.65	1.63	0.0196
400	2.89 <sup>*</sup>	2.86	0.0218	400	2.67 <sup>*</sup>	2.65	0.0211	400	2.10 <sup>*</sup>	2.09	0.0190	400	1.75 <sup>*</sup>	1.73	0.0177
500	2.89 <sup>*</sup>	2.83	0.0176	500	2.70 <sup>*</sup>	2.68	0.0171	500	2.22 <sup>*</sup>	2.21	0.0158	500	1.90 <sup>*</sup>	1.88	0.0149
600	2.83 <sup>*</sup>	2.82	0.0147	600	2.70 <sup>*</sup>	2.68	0.0145	600	2.30 <sup>*</sup>	2.28	0.0135	600	2.00 <sup>*</sup>	1.99	0.0128
700	2.80 <sup>*</sup>	2.78	0.0127	700	2.69 <sup>*</sup>	2.68	0.0125	700	2.34 <sup>*</sup>	2.33	0.0118	700	2.07 <sup>*</sup>	2.06	0.0133
800	2.75 <sup>*</sup>	2.74	0.0111	800	2.66 <sup>*</sup>	2.65	0.0110	800	2.36 <sup>*</sup>	2.35	0.0105	800	2.12 <sup>*</sup>	2.11	0.0101
900	2.67 <sup>*</sup>	2.68	0.0094	900	2.61 <sup>*</sup>	2.60	0.0082	900	2.35 <sup>*</sup>	2.34	0.0094	900	2.15 <sup>*</sup>	2.14	0.00913
1000	2.63 <sup>*</sup>	2.62	0.0086	1000	2.56 <sup>*</sup>	2.55	0.0088	1000	2.33 <sup>*</sup>	2.32	0.00858	1000	2.15 <sup>*</sup>	2.14	0.00834
1200	2.49 <sup>*</sup>	2.49	0.00748	1200	2.44 <sup>*</sup>	2.43	0.00744	1200	2.27 <sup>*</sup>	2.27	0.00725	1200	2.14 <sup>*</sup>	2.13	0.00710
1337	2.41 <sup>*</sup>	2.40	0.00670	1337	2.37 <sup>*</sup>	2.36	0.00668	1336	2.22 <sup>*</sup>	2.21	0.00655	1336	2.12 <sup>*</sup>	2.11	0.00645

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:99.50 Au - 0.50 Ag:  $\pm 10\%$ .99.00 Au - 1.00 Ag:  $\pm 15\%$  below 30 K,  $\pm 10\%$  between 30 and 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.97.00 Au - 3.00 Ag:  $\pm 15\%$  below 30 K,  $\pm 10\%$  between 30 and 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.95.00 Au - 5.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

\* Provisional value.

\* In temperature range where no experimental thermal conductivity data are available.



TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 90.00% (83.13 At.%) Ag: 10.00% (16.87 At.%)			Au: 85.00% (75.63 At.%) Ag: 15.00% (24.37 At.%)			Au: 80.00% (68.86 At.%) Ag: 20.00% (31.14 At.%)			Au: 75.00% (62.16 At.%) Ag: 25.00% (37.84 At.%)		
$\rho_0 = 4.53 \mu\Omega\text{cm}$			$\rho_0 = 6.12 \mu\Omega\text{cm}$			$\rho_0 = 7.36 \mu\Omega\text{cm}$			$\rho_0 = 8.24 \mu\Omega\text{cm}$		
T	k	$k_e$	T	k	$k_e$	T	k	$k_e$	T	k	$k_e$
4	0.0216		4	0.0160		4	0.0133		4	0.0119	
6	0.0204		6	0.0240		6	0.0199		6	0.0178	
8	0.0431		8	0.0319		8	0.0266		8	0.0237	
10	0.0639		10	0.0399		10	0.0332		10	0.0296	
15	0.0809		15	0.0599		15	0.0496		15	0.0445	
20	0.106		20	0.0798		20	0.0664		20	0.0603	
25	0.128		25	0.0969		25	0.0833		25	0.0735	
30	0.157		30	0.118		30	0.0980		30	0.0877	
40	0.208	0.0576	40	0.208	0.0531	40	0.129	0.0609	40	0.129	0.0609
50	0.260	0.0827	50	0.236	0.0494	50	0.159	0.0464	50	0.159	0.0464
60	0.306	0.0957	60	0.269	0.0447	60	0.231	0.0427	60	0.211	0.0419
70	0.339	0.0453	70	0.300	0.0416	70	0.257	0.0397	70	0.234	0.0389
80	0.421	0.0424	80	0.330	0.0389	80	0.282	0.0372	80	0.257	0.0365
90	0.459	0.0399	90	0.360	0.0366	90	0.308	0.0350	90	0.280	0.0345
100	0.497	0.0377	100	0.390	0.0346	100	0.334	0.0331	100	0.304	0.0325
150	0.676	0.0298	150	0.534	0.0275	150	0.457	0.0264	150	0.416	0.0259
200	0.839	0.0259	200	0.669	0.0232	200	0.579	0.0233	200	0.523	0.0219
250	0.971	0.0217	250	0.783	0.0202	250	0.676	0.0194	250	0.621	0.0192
273	1.03	0.0205	273	0.833	0.0191	273	0.723	0.0184	273	0.664	0.0181
300	1.09	0.0182	300	0.889	0.0180	300	0.775	0.0173	300	0.712	0.0171
350	1.20	0.0173	350	0.986	0.0162	350	0.864	0.0157	350	0.797	0.0155
400	1.29	0.0158	400	1.07	0.0149	400	0.947	0.0144	400	0.874	0.0143
500	1.44	0.0135	500	1.23	0.0128	500	1.09	0.0124	500	1.01	0.0123
600	1.57	0.0118	600	1.34	0.0112	600	1.21	0.0110	600	1.13	0.0109
700	1.66	0.0105	700	1.44	0.0101	700	1.32	0.0097	700	1.24	0.0098
800	1.74	0.00946	800	1.53	0.00913	800	1.40	0.00896	800	1.33	0.00895
900	1.79	0.00863	900	1.59	0.00838	900	1.47	0.00825	900	1.40	0.00823
1000	1.83	0.00794	1000	1.64	0.00772	1000	1.52	0.00753	1000	1.45	0.00743
1200	1.86	0.00664	1200	1.72	0.00671	1200	1.61	0.00666	1200	1.55	0.00668
1317	1.89	0.00430	1317	1.77	0.00620	1317	1.67	0.00615	1317	1.59	0.00620

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

50.00 Au - 50.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

55.00 Au - 45.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

60.00 Au - 40.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

75.00 Au - 25.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

<sup>\*</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 70.00% (50.10 At.%) Ag: 30.00% (43.90 At.%)				Au: 65.00% (50.42 At.%) Ag: 35.00% (49.58 At.%)				Au: 60.00% (45.10 At.%) Ag: 40.00% (54.90 At.%)				Au: 55.00% (40.10 At.%) Ag: 45.00% (59.90 At.%)			
$\rho_0 = 2.77 \mu\Omega$				$\rho_0 = 2.0 \mu\Omega$ cm				$\rho_0 = 8.93 \mu\Omega$ cm				$\rho_0 = 8.66 \mu\Omega$ cm			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.0111		4		0.0109		4		0.0109		4		0.0113	
6		0.0167		6		0.0163		6		0.0164		6		0.0169	
8		0.0223		8		0.0217		8		0.0219		8		0.0226	
10		0.0279		10		0.0271		10		0.0274		10		0.0282	
15		0.0418		15		0.0407		15		0.0410		15		0.0423	
20		0.0557		20		0.0543		20		0.0547		20		0.0564	
25		0.0691		25		0.0673		25		0.0679		25		0.0701	
30		0.0825		30		0.0803		30		0.0811		30		0.0836	
40	0.189*	0.109	0.0497	40	0.156	0.106	0.0502	40	0.158*	0.107	0.0511	40	0.163*	0.110	0.0526
50	0.199*	0.134	0.0453	50	0.177	0.131	0.0457	50	0.179*	0.132	0.0466	50	0.184*	0.136	0.0479
60	0.201*	0.160	0.0417	60	0.197	0.156	0.0421	60	0.200*	0.157	0.0429	60	0.205*	0.161	0.0441
70	0.223*	0.184	0.0386	70	0.218	0.179	0.0392	70	0.221*	0.181	0.0399	70	0.227*	0.186	0.0416
80	0.246*	0.206	0.0353	80	0.240	0.203	0.0367	80	0.242*	0.205	0.0374	80	0.249*	0.211	0.0364
90	0.267*	0.228	0.0323	90	0.261	0.227	0.0345	90	0.264*	0.229	0.0352	90	0.271*	0.235	0.0332
100	0.289*	0.256	0.0294	100	0.282	0.250	0.0327	100	0.285*	0.253	0.0333	100	0.294*	0.259	0.0313
150	0.299*	0.270	0.0259	150	0.297	0.261	0.0262	150	0.291*	0.264	0.0267	150	0.292*	0.275	0.0275
200	0.497*	0.475	0.0219	200	0.456	0.464	0.0221	200	0.490*	0.468	0.0226	200	0.505*	0.491	0.0222
250	0.501*	0.571	0.0198	250	0.579	0.580	0.0194	250	0.594*	0.564	0.0196	250	0.601*	0.581	0.0203
273	0.622	0.614	0.0181	273	0.620	0.601	0.0184	273	0.624	0.606	0.0187	273	0.643	0.623	0.0193
300	0.679	0.661	0.0171	300	0.666	0.649	0.0173	300	0.671	0.653	0.0177	300	0.689	0.671	0.0182
350	0.769	0.744	0.0155	350	0.746	0.731	0.0157	350	0.752	0.736	0.0161	350	0.773	0.756	0.0165
400	0.839*	0.823	0.0143	400	0.823*	0.808	0.0145	400	0.828	0.813	0.0148	400	0.853	0.837	0.0152
500	0.969*	0.967	0.0124	500	0.956*	0.943	0.0125	500	0.964*	0.951	0.0126	500	0.988*	0.978	0.0132
600	1.09*	1.08	0.0110	600	1.07*	1.06	0.0111	600	1.08*	1.07	0.0114	600	1.12*	1.10	0.0117
700	1.19*	1.18	0.00968	700	1.18*	1.17	0.0100	700	1.19*	1.18	0.0102	700	1.23*	1.21	0.0105
800	1.29*	1.27	0.00801	800	1.26*	1.26	0.00915	800	1.28*	1.27	0.00936	800	1.31*	1.30	0.00963
900	1.39*	1.36	0.00650	900	1.34*	1.33	0.00843	900	1.35*	1.34	0.00863	900	1.39*	1.38	0.00888
1000	1.41*	1.41	0.00770	1000	1.40*	1.39	0.00783	1000	1.42*	1.41	0.00801	1000	1.45*	1.44	0.00825
1200	1.51*	1.50	0.00676	1200	1.50*	1.49	0.00687	1200	1.52*	1.51	0.00704	1200	1.51*	1.50	0.00771
1311	1.59*	1.54	0.00630	1306	1.54*	1.53	0.00650	1300	1.55*	1.54	0.00660	1295	1.56*	1.55	0.00685

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

70.00 Au - 30.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.  
 65.00 Au - 35.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.  
 60.00 Au - 40.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.  
 55.00 Au - 45.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>† Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>

$\rho_0 = 8.30 \mu\Omega \text{ cm}$				$\rho_0 = 7.79 \mu\Omega \text{ cm}$				$\rho_0 = 7.16 \mu\Omega \text{ cm}$				$\rho_0 = 6.48 \mu\Omega \text{ cm}$			
Au: 50.00% (35.39 At.%) Ag: 50.00% (64.61 At.%)				Au: 45.00% (30.94 At.%) Ag: 55.00% (69.06 At.%)				Au: 40.00% (26.75 At.%) Ag: 60.00% (73.25 At.%)				Au: 35.00% (22.77 At.%) Ag: 65.00% (77.23 At.%)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4		0.0118		4		0.0125		4		0.0136		4		0.0188	
6		0.0177		6		0.0186		6		0.0205		6		0.0228	
8		0.0235		8		0.0251		8		0.0273		8		0.0304	
10		0.0294		10		0.0314		10		0.0341		10		0.0381	
15		0.0442		15		0.0470		15		0.0512		15		0.0571	
20		0.0589		20		0.0627		20		0.0682		20		0.0761	
25		0.0732		25		0.0778		25		0.0849		25		0.0945	
30		0.0874		30		0.0929		30		0.101		30		0.113	
40	0.179*	0.115	0.0544	40	0.179*	0.122	0.0548*	40	0.193	0.133	0.0565*	40	0.212	0.145	0.0634*
50	0.189*	0.142	0.0496	50	0.203*	0.151	0.0518*	50	0.219	0.164	0.0545*	50	0.240	0.168	0.0579*
60	0.214*	0.169	0.0458	60	0.227*	0.179	0.0478*	60	0.245	0.194	0.0503*	60	0.269	0.216	0.0535*
70	0.237*	0.194	0.0436	70	0.251*	0.206	0.0445*	70	0.271	0.224	0.0469*	70	0.298	0.248	0.0498*
80	0.260*	0.220	0.0390	80	0.275*	0.234	0.0417*	80	0.297	0.254	0.0439*	80	0.327	0.280	0.0467*
90	0.283*	0.246	0.0376	90	0.300*	0.261	0.0393*	90	0.324	0.283	0.0414*	90	0.356	0.313	0.0446*
100	0.306*	0.271	0.0356	100	0.324*	0.287	0.0372*	100	0.350*	0.311	0.0392*	100	0.385*	0.344	0.0418*
150	0.419*	0.391	0.0285	150	0.444*	0.414	0.0298*	150	0.479*	0.448	0.0313*	150	0.527*	0.493	0.0333*
200	0.526*	0.502	0.0241	200	0.557*	0.532	0.0252*	200	0.600*	0.573	0.0265*	200	0.659*	0.630	0.0288*
250	0.626*	0.605	0.0211	250	0.682*	0.640	0.0220*	250	0.712*	0.689	0.0232*	250	0.780*	0.756	0.0248*
273	0.679	0.659	0.0200	273	0.708	0.687	0.0209*	273	0.760*	0.738	0.0200*	273	0.833*	0.810	0.0220*
300	0.719	0.701	0.0189	300	0.760	0.740	0.0197*	300	0.816*	0.795	0.0207*	300	0.895*	0.870	0.0226*
350	0.806	0.789	0.0171	350	0.851	0.833	0.0179*	350	0.913*	0.894	0.0188*	350	0.996*	0.976	0.0200*
400	0.880*	0.873	0.0158	400	0.936*	0.920	0.0164*	400	1.00*	0.987	0.0173*	400	1.09*	1.07	0.0183*
500	1.03*	1.02	0.0136	500	1.09*	1.07	0.0142*	500	1.16*	1.15	0.0149*	500	1.26*	1.24	0.0168*
600	1.19*	1.15	0.0131	600	1.22*	1.21	0.0126*	600	1.30*	1.29	0.0132*	600	1.40*	1.39	0.0140*
700	1.37*	1.35	0.0109	700	1.34*	1.32	0.0114*	700	1.42*	1.41	0.0119*	700	1.53*	1.51	0.0126*
800	1.59*	1.56	0.0096	800	1.43*	1.42	0.0104*	800	1.52*	1.51	0.0109*	800	1.63*	1.61	0.0114*
900	1.84*	1.80	0.00818	900	1.51*	1.50	0.00955*	900	1.60*	1.59	0.00999*	900	1.71*	1.70	0.0105*
1000	2.08*	2.05	0.00653	1000	1.59*	1.57	0.00887*	1000	1.67*	1.66	0.00927*	1000	1.78*	1.77	0.00974*
1100	2.39*	2.35	0.00797	1100	1.63*	1.62	0.00828*	1100	1.73*	1.72	0.00865*	1100	1.84*	1.83	0.00909*
1200	2.69*	2.64	0.00710	1200	1.72*	1.71	0.00740*	1200	1.82*	1.81	0.00775*	1200	1.93*	1.92	0.00839*

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:50.00 Au - 50.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.45.00 Au - 55.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.40.00 Au - 60.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.35.00 Au - 65.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

\* Provisional value.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>  
 † Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>

Au: 30.00% (19.01 At.%) Ag: 70.00% (80.99 At.%)				Au: 25.00% (15.44 At.%) Ag: 75.00% (84.56 At.%)				Au: 20.00% (12.04 At.%) Ag: 80.00% (87.96 At.%)				Au: 15.00% (8.81 At.%) Ag: 85.00% (91.19 At.%)			
$\rho_0 = 5.60 \mu\Omega\text{cm}$				$\rho_0 = 4.75 \mu\Omega\text{cm}$				$\rho_0 = 3.86 \mu\Omega\text{cm}$				$\rho_0 = 2.94 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.0175		4		0.0206		4		0.0253		4		0.0332	
6		0.0363		6		0.0309		6		0.0390		6		0.0499	
8		0.0349		8		0.0411		8		0.0506		8		0.0665	
10		0.0436		10		0.0514		10		0.0633		10		0.0831	
15		0.0654		15		0.0771		15		0.0949		15		0.125	
20		0.0673		20		0.103		20		0.127		20		0.166	
25		0.108		25		0.127		25		0.157		25		0.206	
30		0.129		30		0.152		30		0.187		30		0.244	
40	0.237*	0.169	0.0679*	40	0.272*	0.198	0.0736*	40	0.326	0.245	0.0809*	40	0.406	0.317	0.0909*
50	0.270*	0.208	0.0831*	50	0.311*	0.244	0.0874*	50	0.373	0.299	0.0744*	50	0.469	0.385	0.0839*
60	0.309*	0.245	0.0574*	60	0.348*	0.286	0.0834*	60	0.418	0.349	0.0689*	60	0.524	0.446	0.0779*
70	0.335*	0.283	0.0535*	70	0.387*	0.328	0.0592*	70	0.464	0.400	0.0643*	70	0.580	0.508	0.0728*
80	0.368*	0.318	0.0502*	80	0.424*	0.370	0.0546*	80	0.509	0.448	0.0603*	80	0.635	0.567	0.0683*
90	0.401*	0.354	0.0473*	90	0.463*	0.411	0.0514*	90	0.553	0.496	0.0565*	90	0.691	0.626	0.0644*
100	0.434*	0.389	0.0447*	100	0.500*	0.451	0.0487*	100	0.597	0.543	0.0538*	100	0.744	0.683	0.0609*
150	0.588*	0.556	0.0356*	150	0.678*	0.640	0.0389*	150	0.805	0.762	0.0429*	150	0.990	0.942	0.0484*
200	0.737*	0.707	0.0303*	200	0.841*	0.808	0.0328*	200	0.987*	0.951	0.0361*	200	1.20*	1.16	0.0406*
250	0.871*	0.844	0.0263*	250	0.968*	0.960	0.0285*	250	1.15*	1.12	0.0313*	250	1.38*	1.35	0.0351*
273	0.928	0.903	0.0249*	273	1.05*	1.02	0.0270*	273	1.22	1.19	0.0296*	273	1.46*	1.43	0.0331*
300	0.993	0.969	0.0235*	300	1.12*	1.09	0.0254*	300	1.29	1.26	0.0278*	300	1.54*	1.51	0.0311*
350	1.10	1.06	0.0213*	350	1.24	1.21	0.0230*	350	1.42	1.39	0.0251*	350	1.88*	1.85	0.0279*
400	1.20*	1.18	0.0196*	400	1.35*	1.33	0.0210*	400	1.54*	1.51	0.0229*	400	1.90*	1.78	0.0254*
500	1.38*	1.36	0.0166*	500	1.53*	1.51	0.0181*	500	1.73*	1.71	0.0196*	500	2.01*	1.99	0.0216*
600	1.53*	1.51	0.0148*	600	1.68*	1.67	0.0159*	600	1.89*	1.87	0.0173*	600	2.17*	2.15	0.0188*
700	1.68*	1.64	0.0133*	700	1.81*	1.80	0.0142*	700	2.02*	2.00	0.0154*	700	2.29*	2.27	0.0167*
800	1.76*	1.74	0.0121*	800	1.91*	1.90	0.0129*	800	2.12*	2.10	0.0139*	800	2.38*	2.36	0.0151*
900	1.83*	1.83	0.0111*	900	1.99*	1.98	0.0118*	900	2.19*	2.18	0.0127*	900	2.45*	2.44	0.0137*
1000	1.91*	1.90	0.0103*	1000	2.06*	2.05	0.0109*	1000	2.26*	2.24	0.0117*	1000	2.50*	2.49	0.0126*
1100	1.97*	1.96	0.0096*	1100	2.13*	2.11	0.0101*	1100	2.31*	2.30	0.0106*	1100	2.54*	2.53	0.0116*
1207	2.04*	2.05	0.0080*	1201	2.20*	2.19	0.00920*	1256	2.38*	2.37	0.00960*	1251	2.59*	2.58	0.0105*

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

20.00 Au - 70.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

25.00 Au - 75.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

30.00 Au - 80.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

15.00 Au - 85.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

\* Provisional value.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Au: 10.00% ( 5.74 At.%) Ag: 90.00% (94.26 At.%)				Au: 5.00% ( 2.80 At.%) Ag: 95.00% (97.20 At.%)				Au: 3.00% ( 1.67 At.%) Ag: 97.00% (98.33 At.%)				Au: 1.00% ( 0.55 At.%) Ag: 99.00% (99.45 At.%)			
$\rho_0 = 1.97 \mu\Omega \text{ cm}$				$\rho_0 = 0.99 \mu\Omega \text{ cm}$				$\rho_0 = 0.59 \mu\Omega \text{ cm}$				$\rho_0 = 0.190 \mu\Omega \text{ cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4		0.0430		4		0.0987		4		0.166		4		0.514	
6		0.0744		6		0.148		6		0.248		6		0.771	
8		0.0902		8		0.197		8		0.331		8		1.03	
10		0.124		10		0.247		10		0.414		10		1.29	
15		0.196		15		0.370		15		0.621		15		1.93	
20		0.260		20		0.494		20		0.838		20		2.57	
25		0.305		25		0.598		25		1.00		25		2.90	
30		0.363		30		0.705		30		1.15		30		3.21	
40	0.871	0.485	0.108 <sup>‡</sup>	40	1.02	0.873	0.145 <sup>‡</sup>	40	1.53	1.36	0.170 <sup>‡</sup>	40	3.49	3.28	0.211 <sup>‡</sup>
50	0.935	0.937	0.681 <sup>‡</sup>	50	1.14	1.01	0.132 <sup>‡</sup>	50	1.65	1.50	0.154 <sup>‡</sup>	50	3.31	3.12	0.191 <sup>‡</sup>
60	0.726	0.635	0.684 <sup>‡</sup>	60	1.23	1.11	0.131 <sup>‡</sup>	60	1.73	1.59	0.140 <sup>‡</sup>	60	3.10	2.93	0.174 <sup>‡</sup>
70	0.801	0.715	0.865 <sup>‡</sup>	70	1.32	1.21	0.112 <sup>‡</sup>	70	1.84	1.71	0.129 <sup>‡</sup>	70	3.10	2.94	0.159 <sup>‡</sup>
80	0.872	0.783	0.893 <sup>‡</sup>	80	1.42	1.32	0.104 <sup>‡</sup>	80	1.95	1.83	0.119 <sup>‡</sup>	80	3.11	2.96	0.148 <sup>‡</sup>
90	0.946	0.859	0.973 <sup>‡</sup>	90	1.52	1.43	0.0962 <sup>‡</sup>	90	2.05	1.94	0.111 <sup>‡</sup>	90	3.18	3.04	0.137 <sup>‡</sup>
100	1.01	0.940	0.9716 <sup>‡</sup>	100	1.62	1.53	0.0908 <sup>‡</sup>	100	2.14	2.04	0.105 <sup>‡</sup>	100	3.26	3.13	0.128 <sup>‡</sup>
150	1.28	1.26	0.9506 <sup>‡</sup>	150	2.00	1.92	0.0766 <sup>‡</sup>	150	2.53	2.45	0.0799 <sup>‡</sup>	150	3.50	3.41	0.0941 <sup>‡</sup>
200	1.56	1.51	0.9471 <sup>‡</sup>	200	2.27	2.21	0.0577 <sup>‡</sup>	200	2.79	2.73	0.0643 <sup>‡</sup>	200	3.67	3.59	0.0737 <sup>‡</sup>
250	1.76	1.72	0.9464 <sup>‡</sup>	250	2.49	2.44	0.0468 <sup>‡</sup>	250	2.98	2.93	0.0538 <sup>‡</sup>	250	3.77	3.71	0.0605 <sup>‡</sup>
273	1.84	1.80	0.9390 <sup>‡</sup>	273	2.57	2.52	0.0456 <sup>‡</sup>	273	3.05	3.00	0.0500 <sup>‡</sup>	273	3.77	3.71	0.0558 <sup>‡</sup>
300	1.93	1.90	0.9365 <sup>‡</sup>	300	2.64	2.60	0.0423 <sup>‡</sup>	300	3.11	3.06	0.0462 <sup>‡</sup>	300	3.81	3.75	0.0513 <sup>‡</sup>
350	2.06	2.05	0.9318 <sup>‡</sup>	350	2.77	2.74	0.0374 <sup>‡</sup>	350	3.21	3.17	0.0405 <sup>‡</sup>	350	3.84 <sup>*</sup>	3.79	0.0444 <sup>‡</sup>
400	2.21 <sup>*</sup>	2.18	0.9287 <sup>‡</sup>	400	2.88 <sup>*</sup>	2.85	0.0335 <sup>‡</sup>	400	3.29 <sup>*</sup>	3.26	0.0360 <sup>‡</sup>	400	3.87 <sup>*</sup>	3.83	0.0391 <sup>‡</sup>
500	2.40 <sup>*</sup>	2.36	0.9243 <sup>‡</sup>	500	3.03 <sup>*</sup>	3.00	0.0277 <sup>‡</sup>	500	3.39 <sup>*</sup>	3.36	0.0295 <sup>‡</sup>	500	3.87 <sup>*</sup>	3.84	0.0316 <sup>‡</sup>
600	2.55 <sup>*</sup>	2.53	0.9209 <sup>‡</sup>	600	3.13 <sup>*</sup>	3.11	0.0237 <sup>‡</sup>	600	3.45 <sup>*</sup>	3.43	0.0250 <sup>‡</sup>	600	3.85 <sup>*</sup>	3.82	0.0265 <sup>‡</sup>
700	2.69 <sup>*</sup>	2.64	0.9185 <sup>‡</sup>	700	3.19 <sup>*</sup>	3.17	0.0206 <sup>‡</sup>	700	3.47 <sup>*</sup>	3.45	0.0217 <sup>‡</sup>	700	3.82 <sup>*</sup>	3.80	0.0229 <sup>‡</sup>
800	2.73 <sup>*</sup>	2.72	0.9163 <sup>‡</sup>	800	3.22 <sup>*</sup>	3.20	0.0183 <sup>‡</sup>	800	3.49 <sup>*</sup>	3.46	0.0192 <sup>‡</sup>	800	3.79 <sup>*</sup>	3.77	0.0201 <sup>‡</sup>
900	2.77 <sup>*</sup>	2.76	0.9150 <sup>‡</sup>	900	3.27 <sup>*</sup>	3.21	0.0165 <sup>‡</sup>	900	3.45 <sup>*</sup>	3.44	0.0171 <sup>‡</sup>	900	3.72 <sup>*</sup>	3.70	0.0179 <sup>‡</sup>
1000	2.80 <sup>*</sup>	2.79	0.9137 <sup>‡</sup>	1000	3.22 <sup>*</sup>	3.20	0.0149 <sup>‡</sup>	1000	3.41 <sup>*</sup>	3.40	0.0155 <sup>‡</sup>	1000	3.65 <sup>*</sup>	3.64	0.0161 <sup>‡</sup>
1100	2.83 <sup>*</sup>	2.82	0.9126 <sup>‡</sup>	1100	3.20 <sup>*</sup>	3.19	0.0137 <sup>‡</sup>	1100	3.38 <sup>*</sup>	3.36	0.0142 <sup>‡</sup>	1100	3.58 <sup>*</sup>	3.56	0.0147 <sup>‡</sup>
1200	2.87 <sup>*</sup>	2.86	0.9114 <sup>‡</sup>	1200	3.19 <sup>*</sup>	3.17	0.0123 <sup>‡</sup>	1200	3.32 <sup>*</sup>	3.31	0.0126 <sup>‡</sup>	1200	3.50 <sup>*</sup>	3.49	0.0133 <sup>‡</sup>

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

- 10.00 Au - 90.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.
- 5.00 Au - 95.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.
- 3.00 Au - 97.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.
- 1.00 Au - 99.00 Ag:  $\pm 10\%$  below 273 K,  $\pm 7\%$  between 273 and 500 K, and  $\pm 10\%$  above 500 K.

<sup>\*</sup> Provisional values.

<sup>‡</sup> Typical values.

<sup>\*</sup> In temperature range where no experimental thermal conductivity data are available.

TABLE 22. RECOMMENDED THERMAL CONDUCTIVITY OF GOLD-SILVER ALLOY SYSTEM (continued)<sup>†</sup>  
 (Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>)

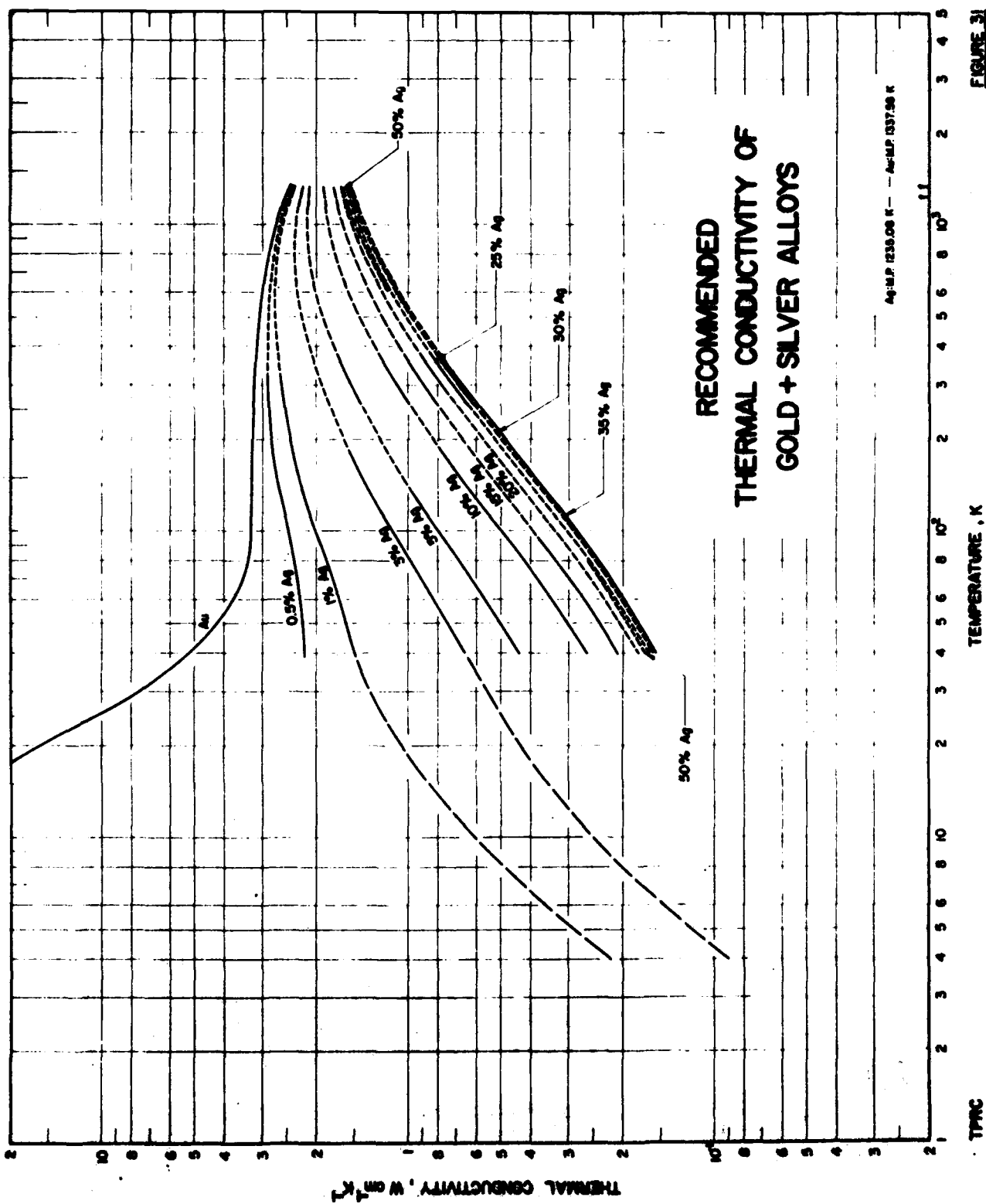
Au: 0.50% (0.50 At.%) Ag: 99.50% (99.50 At.%)					
ρ <sub>0</sub> = 0.0000 μΩcm					
T	k	k <sub>e</sub>	k <sub>g</sub>		
4	1.23				
6	1.83				
8	2.44				
10	3.06				
15	4.58				
20	6.11				
25	6.66				
30	6.20				
40	5.15				
50	4.40				
60	3.86				
70	3.73				
80	3.72				
90	3.74				
100	3.70				
120	3.50				
140	3.56				
160	4.02				
173	4.61				
200	4.03				
240	4.03				
260	4.60*				
300	4.03*				
350	3.97*				
400	3.90*				
450	3.87*				
500	3.79*				
550	3.73*				
600	3.64*				
650	3.50*				
700	3.54				
725	3.54				
750	3.54				
800	3.54				
850	3.54				
900	3.54				
950	3.54				
1000	3.54				
1100	3.54				
1200	3.54				

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

0.50 Au - 99.50 Ag ±10%.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.



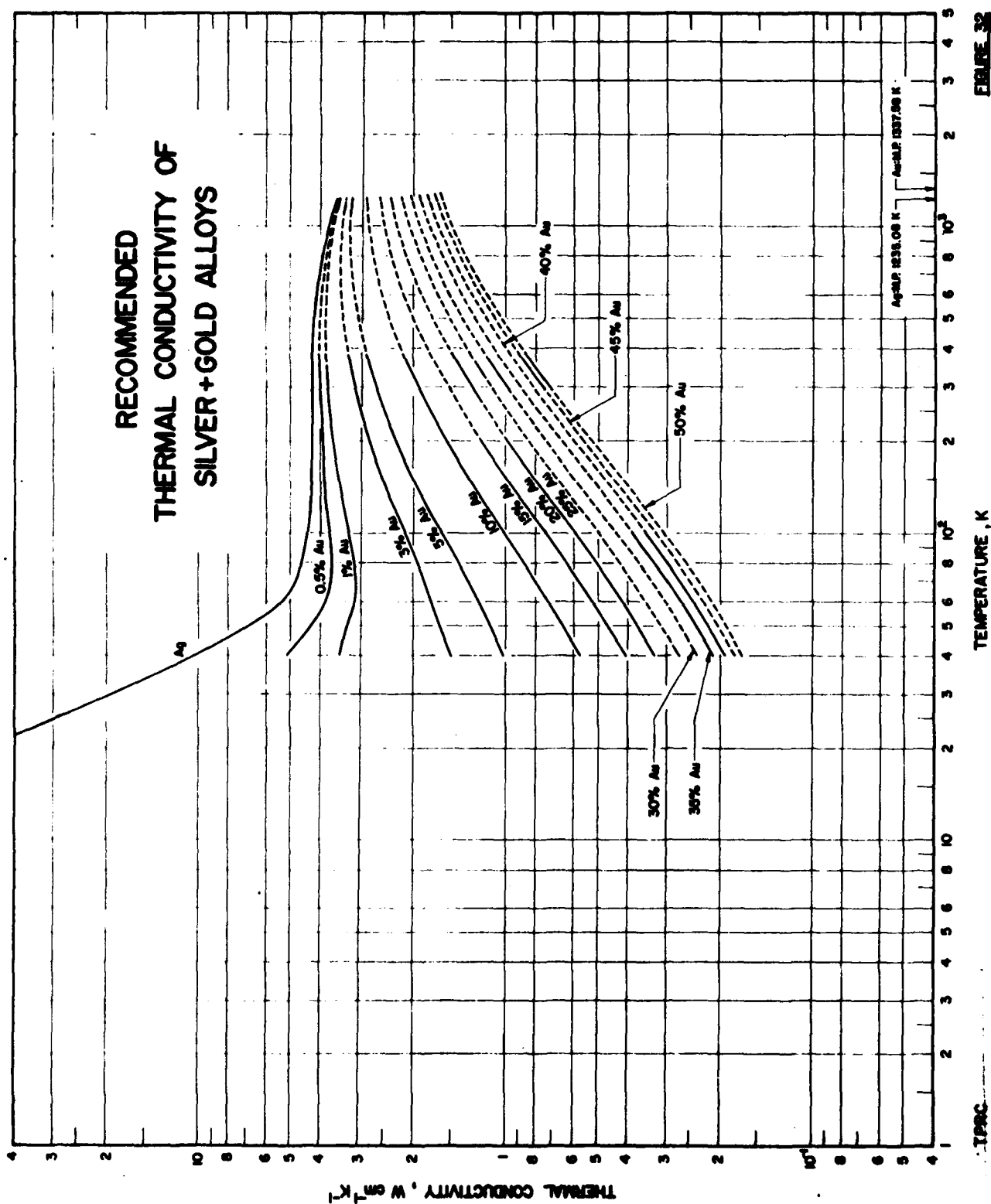
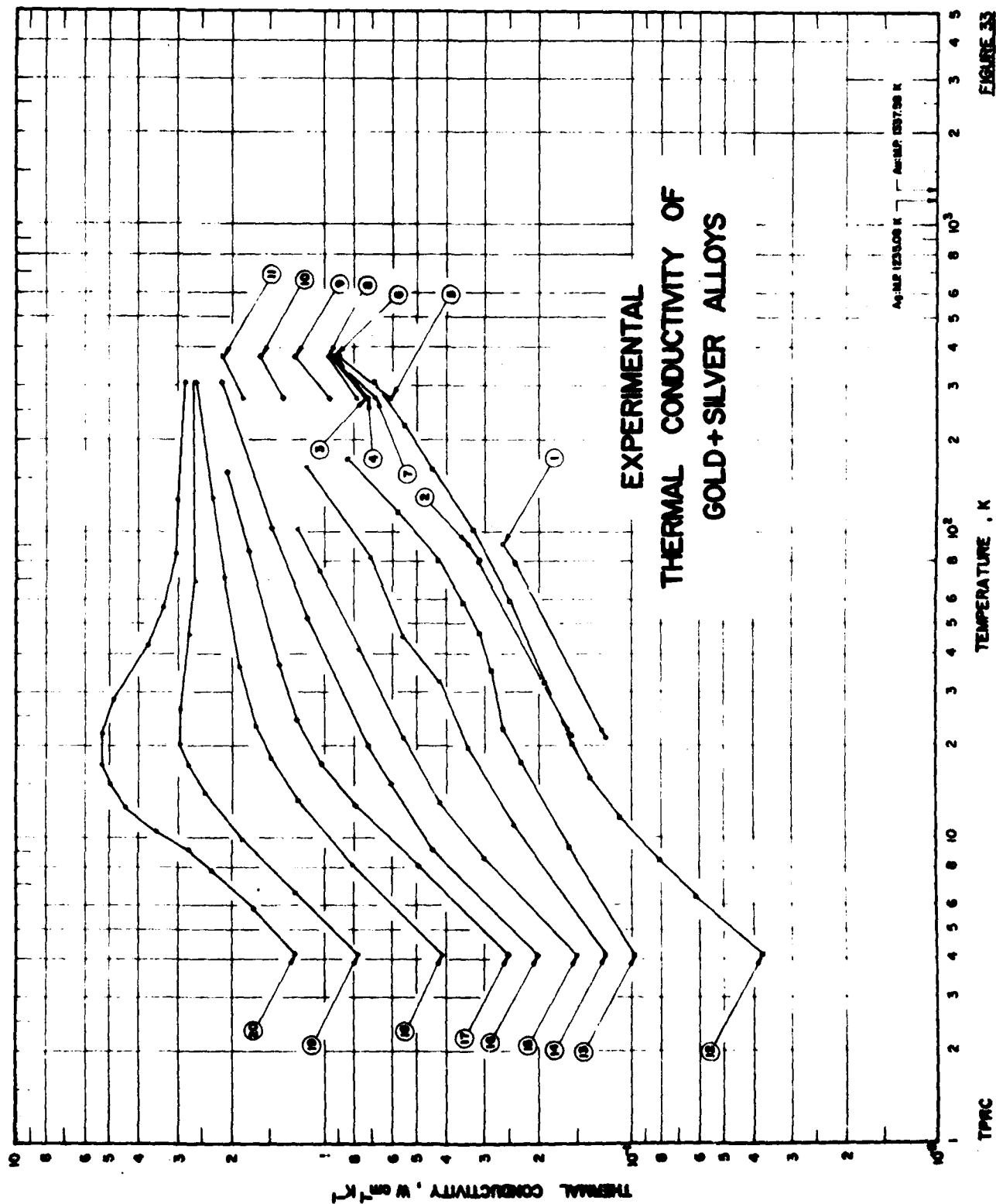


FIGURE 32

TPSC





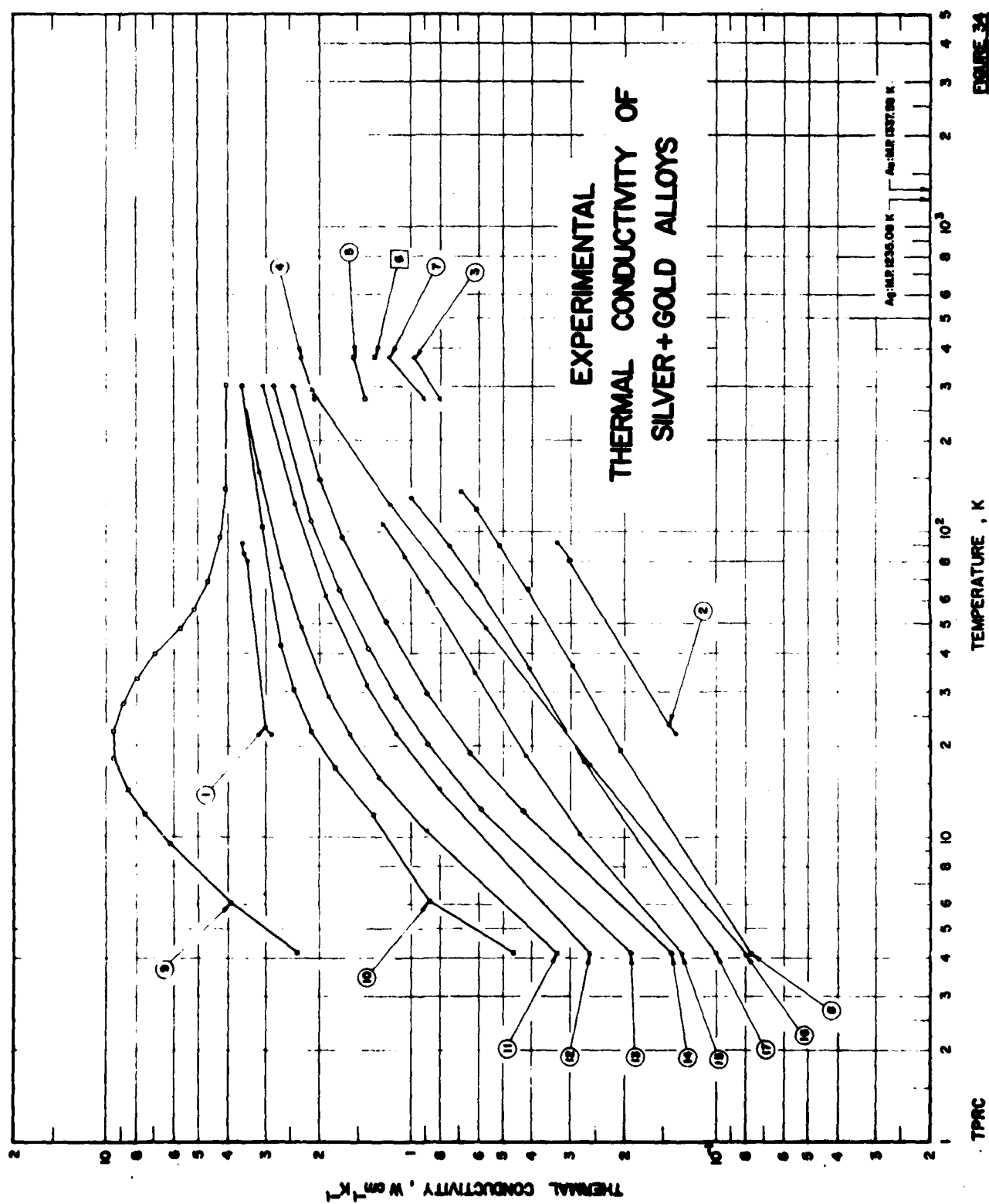


FIGURE 34

TABLE 23. THERMAL CONDUCTIVITY OF GOLD + SILVER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Au	Ag	
1 61	Grönroos, E. and Reddemann, H.	1934	L	21-91	6	64.6	35.4	Calculated composition; single crystal; electrical resistivity 8.85, 9.32, and $10.8 \mu\Omega$ cm at 22, 83, and 273 K, respectively.
2 61	Grönroos, E. and Reddemann, H.	1934	L	22-92	7	84.5	15.5	Calculated composition; single crystal; electrical resistivity 6.69, 7.16, and $8.69 \mu\Omega$ cm at 22, 83, and 273 K, respectively.
3 63	Soderström, E.	1919	T	273, 373		54.62	45.38	Calculated composition; specimen rolled and drawn to 1 mm thick; heated 0.5 hr at temperature near the melting point; electrical conductivity $9.1$ and $8.4 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
4 63	Soderström, E.	1919	T	273, 373		60.32	39.68	Similar to the above specimen except electrical conductivity 9.1 and $8.5 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
5 63	Soderström, E.	1919	T	273, 373		65.46	34.54	Similar to the above specimen except electrical conductivity 7.2 and $7.2 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
6 63	Soderström, E.	1919	T	273, 373		69.17	30.83	Similar to the above specimen except electrical conductivity 8.9 and $8.4 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
7 63	Soderström, E.	1919	T	273, 373		73.19	26.81	Similar to the above specimen except electrical conductivity 9.1 and $8.5 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
8 63	Soderström, E.	1919	T	273, 373		81.23	18.77	Similar to the above specimen except electrical conductivity 10.2 and $9.6 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
9 63	Soderström, E.	1919	T	273, 373		88.82	11.18	Similar to the above specimen except electrical conductivity 13.2 and $12.4 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
10 63	Soderström, E.	1919	T	273, 373		93.84	6.16	Similar to the above specimen except electrical conductivity 18.1 and $15.9 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
11 63	Soderström, E.	1919	T	273, 373		97.26	2.74	Similar to the above specimen except electrical conductivity 25.1 and $22.0 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
12 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-307		35.39		Calculated composition from atomic percent; specimen purchased in three batches from Cambridge Metals Research Ltd., England, prepared from 99.999 and 99.9999 Au and 99.9999 Ag; about 0.5 to 1 mm in diameter and about 1 to 5 cm long; drawn down, etched, washed in distilled water and alcohol, dried and sealed into quartz capsules with 1/3 atmosphere of oxygen and then annealed for 72 hr at 900 C.
13 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-173		12.7		Similar to the above specimen except the electrical resistivity reported as 6.038 and $8.107 \mu\Omega$ cm at 0 and 273 K, respectively.
14 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-165		4.43		Similar to the above specimen except the electrical resistivity reported as 2.603 and $4.895 \mu\Omega$ cm at 0 and 273 K, respectively.
15 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-100		2.29		Similar to the above specimen except the electrical resistivity reported as 1.404 and $3.517 \mu\Omega$ cm at 0 and 273 K, respectively.
16 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-307		1.33		Similar to the above specimen except the electrical resistivity reported as 0.855 and $2.921 \mu\Omega$ cm at 0 and 273 K, respectively.
17 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-156		1.05		Similar to the above specimen except the residual electrical resistivity reported as $0.670 \mu\Omega$ cm.
18 94	Crisp, R.S. and Rungie, J.	1970	L	4.1-307		0.47		Similar to the above specimen except the electrical resistivity reported as 0.370 and $2.421 \mu\Omega$ cm at 0 and 273 K, respectively.

TABLE 23. THERMAL CONDUCTIVITY OF GOLD + SILVER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Au	Ag	
19	Crisp, R. S. and Bungis, J.	1970	L	4.1-307			0.203	Similar to the above specimen except the electrical resistivity reported as 0.135 and 2.209 $\mu\Omega$ cm at 0 and 273 K, respectively.
20	Crisp, R. S. and Bungis, J.	1970	L	4.2-307			0.082	Similar to the above specimen except the electrical resistivity reported as 0.063 and 2.128 $\mu\Omega$ cm at 0 and 273 K, respectively.
21*	Kapoor, A., Rowlands, J. A., and Woods, S. B.	1974	L	0.65-4.0		94.26	5.74	Calculated composition (10 a/o Ag); 4 mm <sup>2</sup> in cross section and 10 cm long; prepared by induction melting 99.999 pure metals in argon, resealed ingot rolled to size; cold-worked; residual electrical resistivity 2.90 $\mu\Omega$ cm.
23*	Kapoor, A., et al.	1974	L	0.69-4.0				The above specimen annealed in vacuum at 1000 K for 12 hr; residual electrical resistivity 2.71 $\mu\Omega$ cm.

\* Not shown in figure.

TABLE 24. THERMAL CONDUCTIVITY OF SILVER + GOLD ALLOYS — SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Ag Au	Composition (continued), Specifications, and Remarks
1	Grüisen, E. and Redemann, H.	1934	L	22-92	4	99.3	0.7 Calculated composition; wire specimen; electrical resistivity 0.163, 0.473, and 1.63 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
2	Grüisen, E. and Redemann, H.	1934	L	22-92	5	62.2	37.6 Calculated composition; single crystal; wire specimen; electrical resistivity 6.87, 7.25, and 8.57 $\mu\Omega$ cm at 22, 83, and 273 K, respectively.
3	Sedström, E.	1919	T	273, 373		55.84	44.16 Calculated composition; wire specimen 1 mm in diameter; rolled and drawn; annealed at close to melting point for 0.5 hr; electrical conductivity 10.3 and 9.7 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
4	Sedström, E.	1919	T	273, 373		91.22	8.78 Similar to the above specimen; electrical conductivity 29.3 and 24.2 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
5	Sedström, E.	1919	T	273, 373		80.74	19.26 Similar to the above specimen except electrical conductivity 19.5 and 16.0 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
6	Sedström, E.	1919	T	273, 2		76.34	23.66 Similar to the above specimen except electrical conductivity 14.7 and 13.5 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
7	Sedström, E.	1919	T	273, 373		68.63	31.37 Similar to the above specimen except electrical conductivity 12.5 and 11.5 $\times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 0 and 100 C, respectively.
8	Crisp, R. S. and Rungta, J.	1970	L	4.1-136			40.31 Calculated composition from atomic percent; specimen purchased in three batches from Cambridge Metals Research Ltd., England; prepared from 99.9999 Ag and 99.999 Au; about 0.5 to 1 mm in diameter and about 1 to 5 cm long; drawn down, etched, washed in distilled water and alcohol, dried and sealed into quartz capsules with 1/3 atmosphere of oxygen and then annealed for 72 hr at 900 C; electrical resistivity reported as 7.084 and 8.874 $\mu\Omega$ cm at 0 and 273 K, respectively.
9	Crisp, R. S. and Rungta, J.	1970	L	4.1-136			0.164 Similar to the above specimen except the electrical resistivity reported as 0.033 and 1.532 $\mu\Omega$ cm at 0 and 273 K, respectively.
10	Crisp, R. S. and Rungta, J.	1970	L	4.1-300			1.25 Similar to the above specimen except the electrical resistivity reported as 0.249 and 1.758 $\mu\Omega$ cm at 0 and 273 K, respectively.
11	Crisp, R. S. and Rungta, J.	1970	L	4.1-300			1.43 Similar to the above specimen except the electrical resistivity reported as 0.285 and 1.788 $\mu\Omega$ cm at 0 and 273 K, respectively.
12	Crisp, R. S. and Rungta, J.	1970	L	4.1-300			2.47 Similar to the above specimen except the electrical resistivity reported as 0.493 and 2.052 $\mu\Omega$ cm at 0 and 273 K, respectively.
13	Crisp, R. S. and Rungta, J.	1970	L	4.1-300			2.97 Similar to the above specimen except the electrical resistivity reported as 0.583 and 2.126 $\mu\Omega$ cm at 0 and 273 K, respectively.
14	Crisp, R. S. and Rungta, J.	1970	L	4.1-300			3.95 Similar to the above specimen except the electrical resistivity reported as 0.768 and 2.507 $\mu\Omega$ cm at 0 and 273 K, respectively.
15	Crisp, R. S. and Rungta, J.	1970	L	4.2-106			9.27 Similar to the above specimen except the electrical resistivity reported as 1.813 and 3.406 $\mu\Omega$ cm at 0 and 273 K, respectively.
16	Crisp, R. S. and Rungta, J.	1970	L	4.2-294			9.94 Similar to the above specimen except the electrical resistivity reported as 1.923 and 3.561 $\mu\Omega$ cm at 0 and 273 K, respectively.
17	Crisp, R. S. and Rungta, J.	1970	L	4.1-129			16.87 Similar to the above specimen except the electrical resistivity reported as 3.303 and 4.958 $\mu\Omega$ cm at 0 and 273 K, respectively.

#### 4.9. Iron-Nickel Alloy System

The iron-nickel alloy system does not form a continuous series of solid solutions. The maximum solid solubility of nickel in iron is 6.81% (6.5 At.%) at 618 K and the solubility decreases at higher and lower temperatures. For nickel-rich alloys the solubility of iron in nickel is uncertain due to the possible formation of FeNi<sub>3</sub> ordered structures. The solid solubility of iron in nickel around room temperature may be below 3%.

There are 98 sets of experimental data available for the thermal conductivity of this alloy system. However, of the 63 data sets available for Fe + Ni alloys listed in Table 26 and shown in Figure 37, 34 sets are merely single data points, and of the 35 data sets for Ni + Fe alloys listed in Table 27 and shown in Figure 38, five sets are single data points and 21 sets are for temperatures below 4.5 K.

For Fe + Ni alloys, no specimen containing less than 3% Ni was measured below 100 K. The conductivity-composition curve for 300 K was constructed based on the data of Powell and Hickman [96] (Fe + Ni curves 3 and 4), Kohlhaas and Kierspe [97] (Fe + Ni curves 30, 31, and 63), and Ingersoll, et al. [98] (Fe + Ni curves 7-16). The electronic thermal conductivities were calculated from eq. (12) except for those alloys with nickel-content  $\geq 20\%$  at temperatures above 300 K where the  $k_e$  calculations appear to be unreliable. The  $k_e$  values at 300 K were also plotted in the conductivity-composition graph. The differences between  $k$  and  $k_e$  were taken as  $k_g$ , which were extrapolated to lower and higher temperatures on the basis of appropriate theoretical temperature dependences. The total thermal conductivity for each composition was then obtained by adding  $k_g$  to the calculated  $k_e$  except for those alloys containing more than 20% nickel at temperatures above 300 K, where  $k$ 's were derived from the experimental data and then  $k_e$ 's were obtained by subtracting  $k_g$  from  $k$ . The resulting values are in agreement with the data of Chari and de Nobel [99] (Fe + Ni curves 1, 33, and 34) and Kohlhaas and Kierspe [97] (Fe + Ni curves 30 and 31) at low temperatures to within 10%, and with the data of Bäcklund [101] (Fe + Ni curves 24 and 25) and Watson and Robinson [102] (Fe + Ni curves 19, 26, 28, 29, and 62) at higher temperatures to within 12%. In the process of calculating the electronic thermal conductivity, the correction due to the thermoelectric power was not made at this time, because there is an anomalous curve of thermopower vs composition at 260 C reported by Wang, et al. [103] which requires further study. Since the corrections are small, no more than 0.2% for all compositions except the 30% Ni alloy, for which it comes to nearly 1% at 260 C, the total thermal conductivity should not be in too large an error without this correction.

For Ni + Fe alloys, the conductivity-composition curve for  $k_g$  at 300 K was extrapolated from the Fe + Ni part to the Ni + Fe portion using the  $k$  value of Ingersoll [98] (Ni + Fe curve 1) for an alloy with 75.06% Ni as a reference point. That is, the sum of the extrapolated  $k_g$  value at 75% Ni and the  $k_e$  value calculated from the selected electrical resistivity for

this composition was required to approximate the Ingersoll value. The  $k_e$  values for all compositions from 1 to 1100 K were calculated from the selected electrical resistivities, and the  $k_g$  values at 300 K were extrapolated to higher temperatures according to the temperature dependence of eq. (35). At low temperatures, all data [81, 100, 105, 106] indicate that  $k_g$  is proportional to  $T$ , and the  $k_g$  values were extrapolated to higher temperature to join the  $k_g$  values extrapolated from 300 K to lower temperatures. The total thermal conductivity for each composition was then obtained by adding  $k_g$  to  $k_e$ , except below 60 K for alloys containing 5% iron or less. The respective  $\rho_0$  values were obtained based solely on the experimental data of ref. [81]. The resulting  $k$  values agree with the data of Farrell and Greig [81] (Ni + Fe curves 12-14) and de Nobel [100] (Ni + Fe curve 35) at low temperatures to within 5% and with the data of Ingersoll [98] (Ni + Fe curve 1), Silverman [132] (Ni + Fe curve 2), and Shelton and Swanger [108] (Ni + Fe curves 3-5) at higher temperatures to within 10%. The correction due to the thermoelectric power, which is no more than 2% of the total thermal conductivity for any composition at any temperature, was not made at this time for the same reason as for the Fe + Ni alloys. The recommended values are for totally disordered alloys only; there may be an order-disorder transformation in Ni + Fe alloys over a wide range of compositions.

The recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 25 for 25 alloy compositions, for most of which the temperature range covered is from 4 to 1100 K. These values are for well-annealed disordered alloys. The values for  $k$  are also shown in Figures 35 and 36. No values are given for temperatures above 1100 K at this time because there is a phase transformation in iron at 1183 K and it is as yet unknown what effect such a transition has on the lattice thermal conductivity of these alloys. It is noted that at high temperatures the differences between the  $k$  values of 5% and 10% nickel alloys are rather large. This is caused by the discontinuity of the Curie temperature at 5.5% nickel, where it drops from 1038 K to 677 K as nickel content increases [104]. The values of residual electrical resistivity for the alloys are also given in Table 25. The uncertainties of the  $k$  values are stated in a footnote to Table 25, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended, provisional, or typical values. The ranges of uncertainties of recommended, provisional, and typical values are less than  $\pm 15\%$ , between  $\pm 15$  and  $\pm 30\%$ , and greater than  $\pm 30\%$ , respectively.

TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Fe: 99.50% (99.52 At. %) Ni: 0.50% (0.48 At. %)				Fe: 99.00% (99.05 At. %) Ni: 1.00% (0.95 At. %)				Fe: 97.00% (97.14 At. %) Ni: 3.00% (2.96 At. %)				Fe: 95.00% (95.23 At. %) Ni: 5.00% (4.77 At. %)			
$\rho_0 = 2.06 \mu\Omega\text{cm}$				$\rho_0 = 3.45 \mu\Omega\text{cm}$				$\rho_0 = 7.37 \mu\Omega\text{cm}$				$\rho_0 = 10.37 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0523 <sup>†</sup>			4	0.0322 <sup>†</sup>			4	0.0146 <sup>†</sup>	0.0133	0.00123 <sup>†</sup>	4	0.0102	0.00944	0.000733 <sup>†</sup>
6	0.0616 <sup>†</sup>			6	0.0502 <sup>†</sup>			6	0.0224 <sup>†</sup>	0.0199	0.00250 <sup>†</sup>	6	0.0156	0.0141	0.00147 <sup>†</sup>
8	0.115 <sup>†</sup>			8	0.0890 <sup>†</sup>			8	0.0307 <sup>†</sup>	0.0266	0.00408 <sup>†</sup>	8	0.0213	0.0189	0.00239 <sup>†</sup>
10	0.144 <sup>†</sup>			10	0.0886 <sup>†</sup>			10	0.0391 <sup>†</sup>	0.0332	0.00582 <sup>†</sup>	10	0.0271	0.0236	0.00347 <sup>†</sup>
15	0.215 <sup>†</sup>			15	0.140 <sup>†</sup>			15	0.0610 <sup>†</sup>	0.0495	0.0115 <sup>†</sup>	15	0.0420	0.0382	0.00676 <sup>†</sup>
20	0.309 <sup>†</sup>			20	0.195 <sup>†</sup>			20	0.0839	0.0659	0.0180 <sup>†</sup>	20	0.0573	0.0466	0.0107 <sup>†</sup>
25	0.396 <sup>†</sup>			25	0.251 <sup>†</sup>			25	0.107	0.0821	0.0250 <sup>†</sup>	25	0.0726	0.0576	0.0150 <sup>†</sup>
30	0.485 <sup>†</sup>			30	0.306 <sup>†</sup>			30	0.130	0.0979	0.0325 <sup>†</sup>	30	0.0878	0.0682	0.0194 <sup>†</sup>
40	0.641 <sup>†</sup>			40	0.411 <sup>†</sup>			40	0.176	0.128	0.0481 <sup>†</sup>	40	0.118	0.0886	0.0294 <sup>†</sup>
50	0.764 <sup>†</sup>			50	0.503 <sup>†</sup>			50	0.222	0.159	0.0632 <sup>†</sup>	50	0.146	0.107	0.0391 <sup>†</sup>
60	0.845 <sup>†</sup>	0.577	0.268 <sup>†</sup>	60	0.573 <sup>†</sup>	0.371	0.202 <sup>†</sup>	60	0.257	0.180	0.0770 <sup>†</sup>	60	0.173	0.124	0.0485 <sup>†</sup>
70	0.878 <sup>†</sup>	0.590	0.288 <sup>†</sup>	70	0.618 <sup>†</sup>	0.395	0.223 <sup>†</sup>	70	0.289	0.200	0.0889 <sup>†</sup>	70	0.195	0.138	0.0568 <sup>†</sup>
80	0.885 <sup>†</sup>	0.583	0.300 <sup>†</sup>	80	0.643 <sup>†</sup>	0.408	0.235 <sup>†</sup>	80	0.314	0.216	0.0979 <sup>†</sup>	80	0.214	0.150	0.0636 <sup>†</sup>
90	0.873 <sup>†</sup>	0.569	0.303 <sup>†</sup>	90	0.654 <sup>†</sup>	0.414	0.240 <sup>†</sup>	90	0.333	0.229	0.104 <sup>†</sup>	90	0.230	0.161	0.0686 <sup>†</sup>
100	0.855 <sup>†</sup>	0.555	0.300 <sup>†</sup>	100	0.659 <sup>†</sup>	0.419	0.240 <sup>†</sup>	100	0.347	0.239	0.108 <sup>†</sup>	100	0.243	0.171	0.0724 <sup>†</sup>
150	0.810	0.549	0.261 <sup>†</sup>	150	0.663	0.450	0.213 <sup>†</sup>	150	0.393	0.288	0.105 <sup>†</sup>	150	0.288	0.214	0.0743 <sup>†</sup>
200	0.785	0.568	0.217 <sup>†</sup>	200	0.666	0.487	0.179 <sup>†</sup>	200	0.421	0.329	0.0923 <sup>†</sup>	200	0.321	0.255	0.0671 <sup>†</sup>
250	0.744	0.582	0.183 <sup>†</sup>	250	0.647	0.496	0.151 <sup>†</sup>	250	0.440	0.360	0.0800 <sup>†</sup>	250	0.344	0.285	0.0589 <sup>†</sup>
273	0.723	0.546	0.169 <sup>†</sup>	273	0.636	0.495	0.141 <sup>†</sup>	273	0.445	0.370	0.0750 <sup>†</sup>	273	0.351	0.296	0.0553 <sup>†</sup>
300	0.701	0.545	0.166 <sup>†</sup>	300	0.623	0.493	0.130 <sup>†</sup>	300	0.450	0.380	0.0695 <sup>†</sup>	300	0.360	0.306	0.0519 <sup>†</sup>
350	0.665	0.529	0.138 <sup>†</sup>	350	0.598	0.485	0.113 <sup>†</sup>	350	0.456	0.385	0.0613 <sup>†</sup>	350	0.372	0.326	0.0489 <sup>†</sup>
400	0.628	0.506	0.120 <sup>†</sup>	400	0.571	0.471	0.100 <sup>†</sup>	400	0.456	0.401	0.0545 <sup>†</sup>	400	0.382	0.341	0.0460 <sup>†</sup>
500	0.564 <sup>†</sup>	0.467	0.0973 <sup>†</sup>	500	0.521	0.440	0.0814 <sup>†</sup>	500	0.448	0.403	0.0446 <sup>†</sup>	500	0.393	0.360	0.0339 <sup>†</sup>
600	0.509 <sup>†</sup>	0.426	0.0617 <sup>†</sup>	600	0.475	0.406	0.0685 <sup>†</sup>	600	0.428	0.390	0.0376 <sup>†</sup>	600	0.385	0.357	0.0294 <sup>†</sup>
700	0.459 <sup>†</sup>	0.388	0.0703 <sup>†</sup>	700	0.436	0.377	0.0591 <sup>†</sup>	700	0.399	0.366	0.0325 <sup>†</sup>	700	0.371	0.346	0.0246 <sup>†</sup>
800	0.415 <sup>†</sup>	0.360	0.0616 <sup>†</sup>	800	0.396	0.344	0.0518 <sup>†</sup>	800	0.366	0.337	0.0286 <sup>†</sup>	800	0.350	0.328	0.0216 <sup>†</sup>
900	0.389 <sup>†</sup>	0.310	0.0448 <sup>†</sup>	900	0.353 <sup>†</sup>	0.307	0.0462 <sup>†</sup>	900	0.330	0.304	0.0255 <sup>†</sup>	900	0.317	0.298	0.0192 <sup>†</sup>
1000	0.316 <sup>†</sup>	0.269	0.0464 <sup>†</sup>	1000	0.309 <sup>†</sup>	0.267	0.0416 <sup>†</sup>	1000	0.293	0.270	0.0230 <sup>†</sup>	1000	0.280	0.263	0.0174 <sup>†</sup>
1100	0.239 <sup>†</sup>	0.244	0.0451 <sup>†</sup>	1100	0.385 <sup>†</sup>	0.247	0.0379 <sup>†</sup>	1100	0.274	0.244	0.0210 <sup>†</sup>	1100	0.268	0.268	0.0158 <sup>†</sup>

† Uncertainty of the total thermal conductivity,  $k$ , are as follows:50-150 Fe - 0.50 Ni:  $\pm 10\%$  below 150 K and  $\pm 10\%$  above 150 K.50-100 Fe - 1.00 Ni:  $\pm 10\%$  below 150 K and  $\pm 10\%$  above 150 K.57-100 Fe - 2.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 5\%$  above 500 K.55-100 Fe - 5.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 5\%$  above 500 K.

† Provisional values.

† Typical values.

\* In temperature range where no experimental thermal conductivity data are available.



TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)\*

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Fe: 50.00% (50.14 At.%) Ni: 50.00% (49.86 At.%)					Fe: 80.00% (80.79 At.%) Ni: 20.00% (19.21 At.%)					Fe: 75.00% (75.93 At.%) Ni: 25.00% (24.07 At.%)				
$\rho_0 = 10.50 \mu\Omega\text{cm}$					$\rho_0 = 19.22 \mu\Omega\text{cm}$					$\rho_0 = 22.11 \mu\Omega\text{cm}$				
T	k	$k_e$	$k_g$		T	k	$k_e$	$k_g$		T	k	$k_e$	$k_g$	
4	0.0000	0.0000	0.0000	0.0000	4	0.00535	0.00508	0.00027	0.00027	4	0.00371	0.00353	0.00017	0.00017
6	0.0000	0.0000	0.0000	0.0000	6	0.00915	0.00761	0.00154	0.00154	6	0.00564	0.00528	0.00035	0.00035
8	0.0130	0.0118	0.0012	0.0012	8	0.0110	0.0102	0.00088	0.00088	8	0.00763	0.00704	0.00056	0.00056
10	0.0166	0.0148	0.0018	0.0018	10	0.0140	0.0127	0.00129	0.00129	10	0.00968	0.00882	0.00060	0.00060
15	0.0206	0.0211	0.0045	0.0045	15	0.0214	0.0189	0.00253	0.00253	15	0.0149	0.0132	0.00170	0.00170
20	0.0260	0.0266	0.0053	0.0053	20	0.0291	0.0251	0.00405	0.00405	20	0.0201	0.0174	0.00273	0.00273
25	0.0442	0.0445	0.0075	0.0075	25	0.0370	0.0312	0.00575	0.00575	25	0.0252	0.0213	0.00359	0.00359
30	0.0436	0.0436	0.0102	0.0102	30	0.0449	0.0373	0.00760	0.00760	30	0.0305	0.0253	0.00515	0.00515
40	0.0737	0.0673	0.0063	0.0063	40	0.0606	0.0490	0.0116	0.0116	40	0.0412	0.0333	0.00785	0.00785
50	0.0713	0.0705	0.0097	0.0097	50	0.0759	0.0602	0.0157	0.0157	50	0.0516	0.0409	0.0107	0.0107
60	0.109	0.0937	0.0200	0.0200	60	0.0906	0.0709	0.0198	0.0198	60	0.0616	0.0481	0.0135	0.0135
70	0.135	0.0939	0.0309	0.0309	70	0.104	0.0806	0.0236	0.0236	70	0.0711	0.0548	0.0163	0.0163
80	0.139	0.104	0.0354	0.0354	80	0.117	0.0896	0.0271	0.0271	80	0.0801	0.0612	0.0189	0.0189
90	0.138	0.113	0.0391	0.0391	90	0.126	0.0978	0.0304	0.0304	90	0.0884	0.0671	0.0213	0.0213
100	0.104	0.123	0.0421	0.0421	100	0.138	0.105	0.0329	0.0329	100	0.0959	0.0726	0.0233	0.0233
150	0.246	0.159	0.0403	0.0403	150	0.177	0.139	0.0377	0.0377	150	0.126	0.0880	0.0260	0.0260
200	0.236	0.190	0.0437	0.0437	200	0.204	0.168	0.0360	0.0360	200	0.147	0.119	0.0276	0.0276
250	0.236	0.216	0.0390	0.0390	250	0.223	0.190	0.0326	0.0326	250	0.162	0.137	0.0253	0.0253
273	0.232	0.235	0.0370	0.0370	273	0.231	0.200	0.0310	0.0310	273	0.168	0.144	0.0242	0.0242
300	0.270	0.236	0.0349	0.0349	300	0.236	0.209	0.0294	0.0294	300	0.174	0.151	0.0229	0.0229
350	0.245	0.251	0.0311	0.0311	350	0.250	0.224	0.0263	0.0263	350	0.184	0.163	0.0207	0.0207
400	0.245	0.264	0.0279	0.0279	400	0.260	0.236	0.0236	0.0236	400	0.191	0.172	0.0187	0.0187
500	0.260	0.283	0.0231	0.0231	500	0.274	0.254	0.0206	0.0206	500	0.203	0.187	0.0157	0.0157
600	0.260	0.286	0.0194	0.0194	600	0.280	0.263	0.0166	0.0166	600	0.210	0.197	0.0133	0.0133
700	0.260	0.286	0.0169	0.0169	700	0.278	0.264	0.0144	0.0144	700	0.212	0.200	0.0116	0.0116
800	0.260	0.275	0.0149	0.0149	800	0.264	0.251	0.0128	0.0128	800	0.208	0.198	0.0102	0.0102
900	0.260	0.264	0.0123	0.0123	900	0.245	0.234	0.0114	0.0114	900	0.208	0.199	0.0091	0.0091
1000	0.240	0.233	0.0121	0.0121	1000	0.231	0.221	0.0103	0.0103	1000	0.213	0.205	0.0082	0.0082
1100	0.230	0.223	0.0110	0.0110	1100	0.230	0.221	0.0093	0.0093	1100	0.221	0.213	0.0073	0.0073

\* Densities of the solid thermal conductivity,  $k$ , are as follows:50.00 Fe - 50.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 10\%$  above 500 K.80.00 Fe - 20.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 10\%$  above 500 K.75.00 Fe - 25.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 10\%$  above 500 K.74.00 Fe - 26.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 5\%$  between 100 and 500 K, and  $\pm 10\%$  above 500 K.

\* Parenthetical values.

\* Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 26. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>

Fe: 70.00% (71.04 At.%) Ni: 30.00% (29.96 At.%)				Fe: 65.00% (66.13 At.%) Ni: 35.00% (33.87 At.%)				Fe: 60.00% (61.19 At.%) Ni: 40.00% (38.81 At.%)				Fe: 55.00% (56.23 At.%) Ni: 45.00% (43.77 At.%)			
$\rho_0 = 61.78 \mu\Omega\text{cm}$				$\rho_0 = 67.04 \mu\Omega\text{cm}$				$\rho_0 = 75.86 \mu\Omega\text{cm}$				$\rho_0 = 18.64 \mu\Omega\text{cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.00174	0.00156	0.00018	4	0.00160	0.00146	0.00014	4	0.00549	0.00578	0.00171	4	0.00690	0.00824	0.00166
6	0.00270	0.00239	0.00031	6	0.00246	0.00219	0.00029	6	0.00826	0.00867	0.00259	6	0.0104	0.00764	0.00251
8	0.00368	0.00317	0.00051	8	0.00338	0.00290	0.00048	8	0.0110	0.00758	0.00349	8	0.0138	0.0104	0.00335
10	0.00470	0.00395	0.00075	10	0.00434	0.00364	0.00070	10	0.0137	0.00936	0.00431	10	0.0171	0.0129	0.00418
15	0.00734	0.00584	0.00150	15	0.00681	0.00542	0.00139	15	0.0202	0.0138	0.00645	15	0.0252	0.0189	0.00625
20	0.0101	0.00770	0.00240	20	0.00939	0.00715	0.00224	20	0.0268	0.0182	0.00857	20	0.0330	0.0247	0.00830
25	0.0139	0.00956	0.00343	25	0.0120	0.00894	0.00317	25	0.0336	0.0223	0.0107	25	0.0405	0.0302	0.0103
30	0.0189	0.0114	0.00483	30	0.0147	0.0105	0.00422	30	0.0391	0.0264	0.0127	30	0.0479	0.0356	0.0123
40	0.0219	0.0150	0.00694	40	0.0203	0.0139	0.00644	40	0.0509	0.0343	0.0166	40	0.0620	0.0459	0.0161
50	0.0279	0.0185	0.00940	50	0.0258	0.0171	0.00871	50	0.0618	0.0418	0.0200	50	0.0748	0.0554	0.0194
60	0.0339	0.0219	0.0120	60	0.0318	0.0203	0.0112	60	0.0716	0.0487	0.0229	60	0.0856	0.0640	0.0218
70	0.0398	0.0251	0.0149	70	0.0368	0.0233	0.0135	70	0.0802	0.0550	0.0258	70	0.0943	0.0718	0.0246
80	0.0451	0.0282	0.0189	80	0.0419	0.0262	0.0157	80	0.0878	0.0608	0.0270	80	0.108	0.0787	0.0262
90	0.0503	0.0312	0.0230	90	0.0469	0.0291	0.0178	90	0.0944	0.0661	0.0283	90	0.112	0.0848	0.0275
100	0.0554	0.0341	0.0269	100	0.0514	0.0318	0.0196	100	0.100	0.0710	0.0291	100	0.119	0.0905	0.0283
150	0.0721	0.0476	0.0350	150	0.0687	0.0446	0.0241	150	0.119	0.0910	0.0322	150	0.141	0.113	0.0275
200	0.0894	0.0597	0.0433	200	0.0822	0.0522	0.0240	200	0.130	0.105	0.0350	200	0.154	0.129	0.0241
250	0.0944	0.0705	0.0538	250	0.0890	0.0566	0.0244	250	0.137	0.115	0.0350	250	0.162	0.140	0.0218
273	0.0976	0.0732	0.0564	273	0.0924	0.0710	0.0214	273	0.139	0.116	0.0308	273	0.164	0.144	0.0203
300	0.1004	0.0803	0.0612	300	0.0961	0.0759	0.0202	300	0.140	0.121	0.0196	300	0.167	0.148	0.0191
350	0.109	0.0891	0.0702	350	0.103	0.0846	0.0184	350	0.143	0.125	0.0175	350	0.171	0.154	0.0168
400	0.115	0.0975	0.0774	400	0.109	0.0928	0.0166	400	0.144	0.128	0.0158	400	0.173	0.157	0.0156
500	0.128	0.114	0.0948	500	0.122	0.108	0.0139	500	0.147	0.133	0.0133	500	0.176	0.163	0.0131
600	0.142	0.130	0.0944	600	0.137	0.125	0.0119	600	0.152	0.140	0.0115	600	0.178	0.167	0.0113
700	0.155	0.147	0.0908	700	0.153	0.143	0.0103	700	0.165	0.155	0.0100	700	0.184	0.174	0.0098
800	0.175	0.165	0.0860	800	0.169	0.160	0.00913	800	0.182	0.173	0.00893	800	0.198	0.189	0.0083
900	0.189	0.180	0.0809	900	0.183	0.175	0.00818	900	0.197	0.189	0.00807	900	0.213	0.206	0.0075
1000	0.204	0.193	0.0771	1000	0.195	0.188	0.00740	1000	0.209	0.202	0.00736	1000	0.225	0.218	0.00725
1100	0.216	0.203	0.0704	1100	0.204	0.197	0.00676	1100	0.219	0.213	0.00679	1100	0.236	0.230	0.00658

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:70.00 Fe - 30.00 Ni:  $\pm 1.5\%$  below 200 K, and  $\pm 10\%$  above 200 K.65.00 Fe - 35.00 Ni:  $\pm 1.5\%$  below 200 K, and  $\pm 10\%$  above 200 K.60.00 Fe - 40.00 Ni:  $\pm 0.5\%$  below 150 K,  $\pm 10\%$  between 150 and 500 K, and  $\pm 12\%$  above 500 K.55.00 Fe - 45.00 Ni:  $\pm 0.5\%$  below 150 K,  $\pm 5\%$  between 150 and 500 K, and  $\pm 10\%$  above 500 K.

a Provisional value.

b Typical value.

c In temperature ranges where no experimental thermal conductivity data are available.

TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)†

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

$\rho_0 = 14.67 \mu\Omega\text{cm}$				$\rho_0 = 12.17 \mu\Omega\text{cm}$				$\rho_0 = 10.23 \mu\Omega\text{cm}$				$\rho_0 = 8.81 \mu\Omega\text{cm}$			
Fe: 50.00% (51.25 At. %) Ni: 50.00% (48.75 At. %)				Fe: 45.00% (46.24 At. %) Ni: 55.00% (53.76 At. %)				Fe: 40.00% (41.21 At. %) Ni: 60.00% (58.79 At. %)				Fe: 35.00% (36.15 At. %) Ni: 65.00% (63.85 At. %)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.00230†	0.00661	0.00159†	4	0.00950	0.00793	0.00157†	4	0.0111*	0.00949	0.00163†	4	0.0128*	0.0111	0.00171†
6	0.0129†	0.00979	0.00239†	6	0.0142	0.0118	0.00238†	6	0.0168*	0.0143	0.00247†	6	0.0191*	0.0165	0.00258†
8	0.0163†	0.0131	0.00319†	8	0.0187	0.0157	0.00318†	8	0.0223*	0.0190	0.00330†	8	0.0254*	0.0220	0.00345†
10	0.0202†	0.0162	0.00398†	10	0.0234	0.0184	0.00397†	10	0.0276*	0.0235	0.00412†	10	0.0316*	0.0273	0.00431†
15	0.0297†	0.0237	0.00598†	15	0.0344	0.0285	0.00594†	15	0.0404*	0.0343	0.00615†	15	0.0468*	0.0403	0.00645†
20	0.0394†	0.0359	0.00796†	20	0.0451	0.0372	0.00791†	20	0.0530*	0.0448	0.00816†	20	0.0614*	0.0528	0.00857†
25	0.0477†	0.0378	0.00988†	25	0.0556	0.0458	0.00980†	25	0.0649*	0.0548	0.0101†	25	0.0753*	0.0646	0.0107†
30	0.0563†	0.0445	0.0118†	30	0.0656	0.0539	0.0117†	30	0.0766*	0.0644	0.0122†	30	0.0886*	0.0759	0.0127†
40	0.0723†	0.0588	0.0154†	40	0.0840	0.0688	0.0152†	40	0.0981*	0.0823	0.0158†	40	0.113*	0.0964	0.0166†
50	0.0867†	0.0681	0.0194†	50	0.100	0.0831	0.0184†	50	0.117*	0.0960	0.0191†	50	0.134*	0.114	0.0200†
60	0.0991†	0.0779	0.0232†	60	0.114	0.0930	0.0210†	60	0.134*	0.112	0.0218†	60	0.152*	0.139	0.0228†
70	0.116†	0.0861	0.0239†	70	0.128	0.104	0.0233†	70	0.147*	0.123	0.0240†	70	0.167*	0.142	0.0252†
80	0.119†	0.0943	0.0251†	80	0.138	0.113	0.0250†	80	0.159*	0.133	0.0258†	80	0.179*	0.152	0.0270†
90	0.127†	0.101	0.0264†	90	0.146	0.120	0.0262†	90	0.168*	0.141	0.0270†	90	0.188*	0.159	0.0283†
100	0.134†	0.106	0.0271†	100	0.154	0.127	0.0270†	100	0.176*	0.148	0.0278†	100	0.195*	0.166	0.0291†
150	0.195†	0.131	0.0285†	150	0.178	0.151	0.0283†	150	0.200*	0.173	0.0270†	150	0.219*	0.190	0.0283†
200	0.172	0.149	0.0236†	200	0.193	0.169	0.0235†	200	0.213*	0.189	0.0240†	200	0.232*	0.207	0.0250†
250	0.162	0.162	0.0206†	250	0.202	0.182	0.0207†	250	0.221*	0.200	0.0211†	250	0.238*	0.216	0.0220†
273	0.186	0.187	0.0197†	273	0.205	0.185	0.0197†	273	0.223*	0.203	0.0200†	273	0.240*	0.219	0.0208†
300	0.190	0.171	0.0194†	300	0.209	0.180	0.0185†	300	0.226*	0.207	0.0188†	300	0.242*	0.222	0.0194†
350	0.195	0.178	0.0157†	350	0.213	0.196	0.0167†	350	0.228*	0.211	0.0169†	350	0.244*	0.226	0.0175†
400	0.190	0.184	0.0153†	400	0.216	0.201	0.0151†	400	0.230*	0.215	0.0153†	400	0.245*	0.229	0.0158†
500	0.203	0.190	0.0129†	500	0.220	0.207	0.0127†	500	0.233*	0.220	0.0129†	500	0.247*	0.234	0.0133†
600	0.204	0.193	0.0110†	600	0.221	0.210	0.0109†	600	0.235*	0.224	0.0111†	600	0.249*	0.237	0.0113†
700	0.207	0.197	0.00943†	700	0.224	0.215	0.00958†	700	0.238*	0.228	0.00974†	700	0.253*	0.243	0.0100†
800	0.210	0.202	0.00839†	800	0.229	0.221	0.00854†	800	0.246*	0.237	0.00869†	800	0.262*	0.253	0.00893†
900	0.213	0.215	0.00774†	900	0.241	0.233	0.00771†	900	0.259*	0.251	0.00783†	900	0.276*	0.268	0.00807†
1000	0.226	0.228	0.00706†	1000	0.255	0.248	0.00701†	1000	0.273*	0.266	0.00714†	1000	0.291*	0.284	0.00730†
1100	0.245	0.239	0.00631†	1100	0.266	0.260	0.00648†	1100	0.286*	0.280	0.00659†	1100	0.304*	0.297	0.00679†

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:50.00 Fe - 50.00 Ni:  $\pm 1\%$  below 150 K,  $\pm 6\%$  between 150 and 500 K, and  $\pm 8\%$  above 500 K.45.00 Fe - 55.00 Ni:  $\pm 1\%$  below 100 K,  $\pm 8\%$  between 100 and 500 K, and  $\pm 10\%$  above 500 K.40.00 Fe - 60.00 Ni:  $\pm 1\%$  below 200 K and  $\pm 8\%$  above 200 K.35.00 Fe - 65.00 Ni:  $\pm 1\%$  below 200 K and  $\pm 8\%$  above 200 K.

\* Provisional values.

† Typical values.

\* In temperature ranges where no experimental thermal conductivity data are available.

TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)†

[Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Fe: 30.00% (31.06 At. %) Ni: 70.00% (68.94 At. %)				Fe: 25.00% (25.95 At. %) Ni: 75.00% (74.05 At. %)				Fe: 20.00% (20.81 At. %) Ni: 80.00% (79.19 At. %)				Fe: 15.00% (15.65 At. %) Ni: 85.00% (84.35 At. %)			
$\rho_0 = 7.53 \mu\Omega \text{ cm}$				$\rho_0 = 6.25 \mu\Omega \text{ cm}$				$\rho_0 = 5.04 \mu\Omega \text{ cm}$				$\rho_0 = 3.935 \mu\Omega \text{ cm}$			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0146	0.0128	0.00183 <sup>‡</sup>	4	0.0176	0.0156	0.00199 <sup>‡</sup>	4	0.0217	0.0194	0.00230 <sup>‡</sup>	4	0.0275 <sup>‡</sup>	0.0248	0.00266 <sup>‡</sup>
6	0.0219 <sup>*</sup>	0.0190	0.00276 <sup>‡</sup>	6	0.0262 <sup>*</sup>	0.0232	0.00300 <sup>‡</sup>	6	0.0324 <sup>*</sup>	0.0289	0.00346 <sup>‡</sup>	6	0.0410 <sup>*</sup>	0.0370	0.00401 <sup>‡</sup>
8	0.0289 <sup>*</sup>	0.0253	0.00370 <sup>‡</sup>	8	0.0345 <sup>*</sup>	0.0305	0.00401 <sup>‡</sup>	8	0.0429 <sup>*</sup>	0.0383	0.00462 <sup>‡</sup>	8	0.0543 <sup>*</sup>	0.0489	0.00539 <sup>‡</sup>
10	0.0360 <sup>*</sup>	0.0314	0.00462 <sup>‡</sup>	10	0.0429 <sup>*</sup>	0.0379	0.00503 <sup>‡</sup>	10	0.0533 <sup>*</sup>	0.0475	0.00578 <sup>‡</sup>	10	0.0674 <sup>*</sup>	0.0607	0.00675 <sup>‡</sup>
15	0.0537 <sup>*</sup>	0.0456	0.00657 <sup>‡</sup>	15	0.0628 <sup>*</sup>	0.0552	0.00759 <sup>‡</sup>	15	0.0778 <sup>*</sup>	0.0692	0.00864 <sup>‡</sup>	15	0.0985 <sup>*</sup>	0.0884	0.0101 <sup>‡</sup>
20	0.0697 <sup>*</sup>	0.0586	0.00812 <sup>‡</sup>	20	0.0815 <sup>*</sup>	0.0714	0.0101 <sup>‡</sup>	20	0.101 <sup>*</sup>	0.0896	0.0116 <sup>‡</sup>	20	0.128 <sup>*</sup>	0.114	0.0139 <sup>‡</sup>
25	0.0843 <sup>*</sup>	0.0730	0.0113 <sup>‡</sup>	25	0.0990 <sup>*</sup>	0.0863	0.0127 <sup>‡</sup>	25	0.122 <sup>*</sup>	0.108	0.0144 <sup>‡</sup>	25	0.156 <sup>*</sup>	0.138	0.0168 <sup>‡</sup>
30	0.0986 <sup>*</sup>	0.0860	0.0138 <sup>‡</sup>	30	0.116 <sup>*</sup>	0.100	0.0151 <sup>‡</sup>	30	0.142 <sup>*</sup>	0.125	0.0172 <sup>‡</sup>	30	0.181 <sup>*</sup>	0.161	0.0200 <sup>‡</sup>
40	0.139 <sup>*</sup>	0.106	0.0176 <sup>‡</sup>	40	0.145 <sup>*</sup>	0.125	0.0197 <sup>‡</sup>	40	0.177 <sup>*</sup>	0.155	0.0224 <sup>‡</sup>	40	0.224 <sup>*</sup>	0.198	0.0261 <sup>‡</sup>
50	0.165 <sup>*</sup>	0.127	0.0213 <sup>‡</sup>	50	0.170 <sup>*</sup>	0.146	0.0237 <sup>‡</sup>	50	0.206 <sup>*</sup>	0.179	0.0269 <sup>‡</sup>	50	0.258 <sup>*</sup>	0.227	0.0312 <sup>‡</sup>
60	0.189 <sup>*</sup>	0.143	0.0243 <sup>‡</sup>	60	0.190 <sup>*</sup>	0.163	0.0270 <sup>‡</sup>	60	0.228 <sup>*</sup>	0.197	0.0306 <sup>‡</sup>	60	0.284 <sup>*</sup>	0.249	0.0354 <sup>‡</sup>
70	0.194 <sup>*</sup>	0.157	0.0269 <sup>‡</sup>	70	0.206 <sup>*</sup>	0.176	0.0295 <sup>‡</sup>	70	0.245 <sup>*</sup>	0.212	0.0334 <sup>‡</sup>	70	0.303 <sup>*</sup>	0.264	0.0394 <sup>‡</sup>
80	0.196 <sup>*</sup>	0.160	0.0290 <sup>‡</sup>	80	0.219 <sup>*</sup>	0.187	0.0315 <sup>‡</sup>	80	0.259 <sup>*</sup>	0.223	0.0355 <sup>‡</sup>	80	0.316 <sup>*</sup>	0.276	0.0406 <sup>‡</sup>
90	0.200 <sup>*</sup>	0.176	0.0300 <sup>‡</sup>	90	0.228 <sup>*</sup>	0.196	0.0327 <sup>‡</sup>	90	0.268 <sup>*</sup>	0.231	0.0367 <sup>‡</sup>	90	0.324 <sup>*</sup>	0.283	0.0420 <sup>‡</sup>
100	0.213 <sup>*</sup>	0.183	0.0308 <sup>‡</sup>	100	0.236 <sup>*</sup>	0.203	0.0336 <sup>‡</sup>	100	0.275 <sup>*</sup>	0.238	0.0375 <sup>‡</sup>	100	0.329 <sup>*</sup>	0.286	0.0426 <sup>‡</sup>
150	0.230 <sup>*</sup>	0.206	0.0358 <sup>‡</sup>	150	0.257 <sup>*</sup>	0.225	0.0320 <sup>‡</sup>	150	0.295 <sup>*</sup>	0.260	0.0351 <sup>‡</sup>	150	0.342 <sup>*</sup>	0.303	0.0395 <sup>‡</sup>
200	0.240 <sup>*</sup>	0.222	0.0380 <sup>‡</sup>	200	0.268 <sup>*</sup>	0.240	0.0282 <sup>‡</sup>	200	0.305 <sup>*</sup>	0.274	0.0308 <sup>‡</sup>	200	0.348 <sup>*</sup>	0.313	0.0344 <sup>‡</sup>
250	0.250 <sup>*</sup>	0.232	0.0220 <sup>‡</sup>	250	0.274 <sup>*</sup>	0.249	0.0248 <sup>‡</sup>	250	0.309 <sup>*</sup>	0.282	0.0270 <sup>‡</sup>	250	0.350 <sup>*</sup>	0.320	0.0300 <sup>‡</sup>
273	0.257 <sup>*</sup>	0.235	0.0210 <sup>‡</sup>	273	0.276 <sup>*</sup>	0.252	0.0233 <sup>‡</sup>	273	0.309 <sup>*</sup>	0.284	0.0254 <sup>‡</sup>	273	0.350 <sup>*</sup>	0.322	0.0281 <sup>‡</sup>
300	0.259 <sup>*</sup>	0.236	0.0203 <sup>‡</sup>	300	0.277	0.256	0.0218 <sup>‡</sup>	300	0.310	0.286	0.0237 <sup>‡</sup>	300	0.351 <sup>*</sup>	0.324	0.0264 <sup>‡</sup>
350	0.260 <sup>*</sup>	0.242	0.0181 <sup>‡</sup>	350	0.279	0.259	0.0195 <sup>‡</sup>	350	0.311	0.290	0.0211 <sup>‡</sup>	350	0.350 <sup>*</sup>	0.327	0.0234 <sup>‡</sup>
400	0.261 <sup>*</sup>	0.246	0.0163 <sup>‡</sup>	400	0.280 <sup>*</sup>	0.262	0.0175 <sup>‡</sup>	400	0.311 <sup>*</sup>	0.292	0.0190 <sup>‡</sup>	400	0.352 <sup>*</sup>	0.331	0.0210 <sup>‡</sup>
500	0.263 <sup>*</sup>	0.249	0.0137 <sup>‡</sup>	500	0.280 <sup>*</sup>	0.265	0.0146 <sup>‡</sup>	500	0.310 <sup>*</sup>	0.294	0.0158 <sup>‡</sup>	500	0.349 <sup>*</sup>	0.330	0.0175 <sup>‡</sup>
600	0.264 <sup>*</sup>	0.252	0.0110 <sup>‡</sup>	600	0.279 <sup>*</sup>	0.267	0.0125 <sup>‡</sup>	600	0.308 <sup>*</sup>	0.294	0.0136 <sup>‡</sup>	600	0.342 <sup>*</sup>	0.327	0.0150 <sup>‡</sup>
700	0.267 <sup>*</sup>	0.257	0.0103 <sup>‡</sup>	700	0.281 <sup>*</sup>	0.270	0.0108 <sup>‡</sup>	700	0.309 <sup>*</sup>	0.297	0.0119 <sup>‡</sup>	700	0.338 <sup>*</sup>	0.325	0.0131 <sup>‡</sup>
800	0.270 <sup>*</sup>	0.260	0.0081 <sup>‡</sup>	800	0.290 <sup>*</sup>	0.280	0.00871 <sup>‡</sup>	800	0.311 <sup>*</sup>	0.300	0.0106 <sup>‡</sup>	800	0.333 <sup>*</sup>	0.322	0.0117 <sup>‡</sup>
900	0.269 <sup>*</sup>	0.264	0.0063 <sup>‡</sup>	900	0.305 <sup>*</sup>	0.296	0.00876 <sup>‡</sup>	900	0.324 <sup>*</sup>	0.315	0.00949 <sup>‡</sup>	900	0.346 <sup>*</sup>	0.336	0.0105 <sup>‡</sup>
1000	0.269 <sup>*</sup>	0.269	0.0075 <sup>‡</sup>	1000	0.321 <sup>*</sup>	0.313	0.00798 <sup>‡</sup>	1000	0.340 <sup>*</sup>	0.331	0.00863 <sup>‡</sup>	1000	0.368 <sup>*</sup>	0.353	0.00804 <sup>‡</sup>
1100	0.269 <sup>*</sup>	0.313	0.00698 <sup>‡</sup>	1100	0.338 <sup>*</sup>	0.330	0.00734 <sup>‡</sup>	1100	0.356 <sup>*</sup>	0.348	0.00764 <sup>‡</sup>	1100	0.376 <sup>*</sup>	0.369	0.00670 <sup>‡</sup>

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:20.00 Fe - 70.00 Ni:  $\pm 15\%$  below 200 K and  $\pm 8\%$  above 200 K.25.00 Fe - 75.00 Ni:  $\pm 10\%$  below 100 K,  $\pm 8\%$  between 100 and 500 K, and  $\pm 8\%$  above 500 K.30.00 Fe - 80.00 Ni:  $\pm 15\%$  below 100 K,  $\pm 8\%$  between 100 and 500 K, and  $\pm 8\%$  above 500 K.15.00 Fe - 85.00 Ni:  $\pm 15\%$  below 100 K,  $\pm 8\%$  between 100 and 500 K, and  $\pm 10\%$  above 100 K.

‡ Provisional values.

§ Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)†  
 [Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Fe: 10.00% (10.46 At.%) Ni: 89.00% (89.54 At.%)			Fe: 5.00% (5.24 At.%) Ni: 95.00% (94.76 At.%)			Fe: 3.00% (3.15 At.%) Ni: 97.00% (96.85 At.%)			Fe: 1.00% (1.05 At.%) Ni: 99.00% (98.95 At.%)		
ρ <sub>0</sub> = 2.943 μΩcm			ρ <sub>0</sub> = 2.045 μΩcm			ρ <sub>0</sub> = 1.227 μΩcm			ρ <sub>0</sub> = 0.409 μΩcm		
T	k	k <sub>e</sub>	T	k	k <sub>e</sub>	T	k	k <sub>e</sub>	T	k	k <sub>e</sub>
4	0.0200	0.0044	4	0.0741		4	0.115		4	0.225	
6	0.0200	0.0044	6	0.109		6	0.169		6	0.479	
8	0.0200	0.0044	8	0.143		8	0.221		8	0.680	
10	0.0200	0.0044	10	0.177		10	0.273		10	0.777	
15	0.130	0.133	15	0.356		15	0.396		15	1.06	
20	0.170	0.186	20	0.386		20	0.503		20	1.37	
25	0.213	0.191	25	0.386		25	0.590		25	1.53	
30	0.247	0.201	30	0.440		30	0.659		30	1.69	
40	0.304	0.270	40	0.530		40	0.751		40	1.56	
50	0.367	0.306	50	0.565		50	0.791		50	1.45	
60	0.370	0.300	60	0.583		60	0.794		60	1.39	
70	0.380	0.305	70	0.586		70	0.783		70	1.30	
80	0.400	0.306	80	0.585		80	0.768		80	1.13	
90	0.414	0.301	90	0.578		90	0.745		90	1.07	
100	0.417	0.304	100	0.570	0.0993	100	0.728	0.580	100	1.02	0.766
150	0.460	0.300	150	0.543	0.459	150	0.657	0.540	150	0.890	0.696
200	0.480	0.305	200	0.535	0.466	200	0.628	0.533	200	0.814	0.602
250	0.419	0.373	250	0.539	0.471	250	0.608	0.529	250	0.767	0.643
273	0.430	0.376	273	0.525	0.470	273	0.603	0.529	273	0.751	0.636
300	0.430	0.378	300	0.521	0.470	300	0.596	0.528	300	0.735	0.629
350	0.460	0.300	350	0.514	0.469	350	0.585	0.525	350	0.704	0.612
400	0.480	0.378	400	0.504	0.464	400	0.570	0.517	400	0.676	0.596
500	0.380	0.378	500	0.484	0.451	500	0.540	0.496	500	0.623	0.557
600	0.360	0.371	600	0.455	0.427	600	0.504	0.467	600	0.575	0.520
700	0.370	0.300	700	0.430	0.396	700	0.480	0.448	700	0.563	0.517
800	0.380	0.304	800	0.436	0.415	800	0.496	0.468	800	0.583	0.541
900	0.380	0.300	900	0.430	0.431	900	0.513	0.488	900	0.601	0.564
1000	0.380	0.300	1000	0.430	0.448	1000	0.529	0.507	1000	0.630	0.586
1100	0.400	0.300	1100	0.479	0.463	1100	0.546	0.526	1100	0.640	0.610

† Uncertainties of the total thermal conductivity, k, are as follows:

10.00 Fe - 99.00 Ni: ±15% below 100 K, ±8% between 100 and 500 K, and ±10% above 500 K.

5.00 Fe - 95.00 Ni: ±15% below 150 K, ±6% between 150 and 500 K, and ±8% above 500 K.

3.00 Fe - 97.00 Ni: ±15% below 150 K, ±6% between 150 and 500 K, and ±8% above 500 K.

1.00 Fe - 99.00 Ni: ±15% below 80 K, ±10% between 80 and 200 K, and ±6% above 200 K.

‡ Provisional values.

§ Typical values.

\* In temperature ranges where no experimental thermal conductivity data are available.

TABLE 25. RECOMMENDED THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity,  $k$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ 

Fe: 0.50% (0.48 At. %) Ni: 99.50% (99.52 At. %)							
$\rho_0 = 0.2045 \mu\Omega \text{cm}$							
T	k	$k_e$	$k_g$				
4	0.823 <sup>‡</sup>						
6	1.25 <sup>‡</sup>						
8	1.58 <sup>‡</sup>						
10	1.96 <sup>‡</sup>						
15	2.76 <sup>‡</sup>						
20	3.26 <sup>‡</sup>						
25	3.44 <sup>‡</sup>						
30	3.35 <sup>‡</sup>						
40	2.94 <sup>‡</sup>						
50	2.40 <sup>‡</sup>						
60	1.96 <sup>‡</sup>						
70	1.69 <sup>‡</sup>						
80	1.49 <sup>‡</sup>						
90	1.35 <sup>‡</sup>						
100	1.24 <sup>‡</sup>	0.936	0.3013				
150	0.991 <sup>*</sup>	0.765	0.226 <sup>‡</sup>				
200	0.869 <sup>*</sup>	0.715	0.177 <sup>‡</sup>				
250	0.833 <sup>*</sup>	0.686	0.145 <sup>‡</sup>				
273	0.811 <sup>*</sup>	0.678	0.133 <sup>‡</sup>				
300	0.789 <sup>*</sup>	0.666	0.123 <sup>‡</sup>				
350	0.749	0.643	0.109 <sup>‡</sup>				
400	0.714	0.631	0.0933 <sup>‡</sup>				
500	0.653	0.576	0.0753 <sup>‡</sup>				
600	0.600	0.537	0.0630 <sup>‡</sup>				
700	0.563	0.500	0.0542 <sup>‡</sup>				
800	0.512	0.505	0.0474 <sup>‡</sup>				
900	0.439 <sup>*</sup>	0.591	0.0423 <sup>‡</sup>				
1000	0.653 <sup>*</sup>	0.615	0.0390 <sup>‡</sup>				
1100	0.670 <sup>*</sup>	0.641	0.0346 <sup>‡</sup>				

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:0.50 Fe - 99.50 Ni:  $\pm 20\%$  below 80 K,  $\pm 10\%$  between 80 and 200 K, and  $\pm 6\%$  above 200 K.

‡ Provisional values.

§ Typical values.

\* In temperature range where no experimental thermal conductivity data are available.

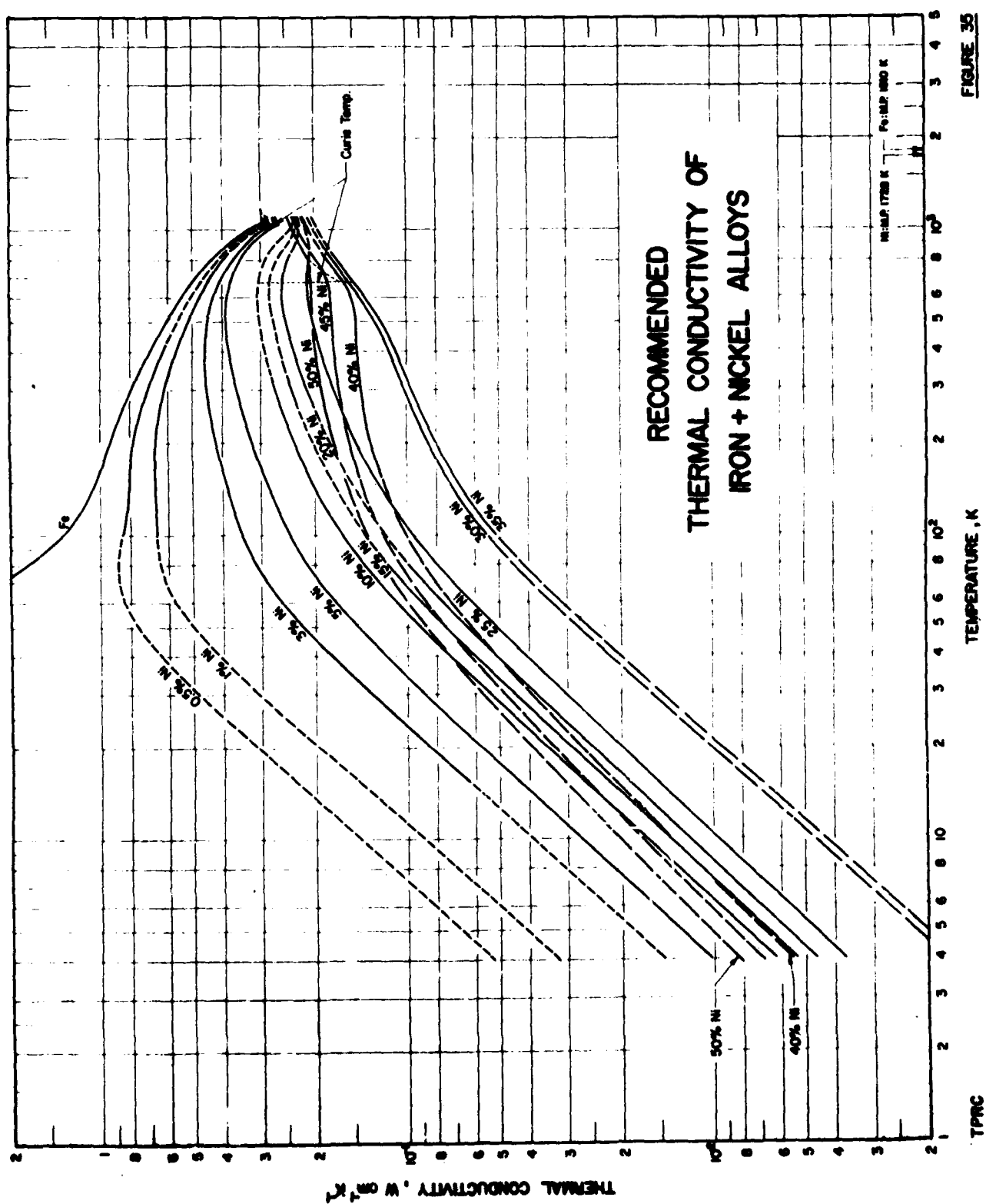


FIGURE 35

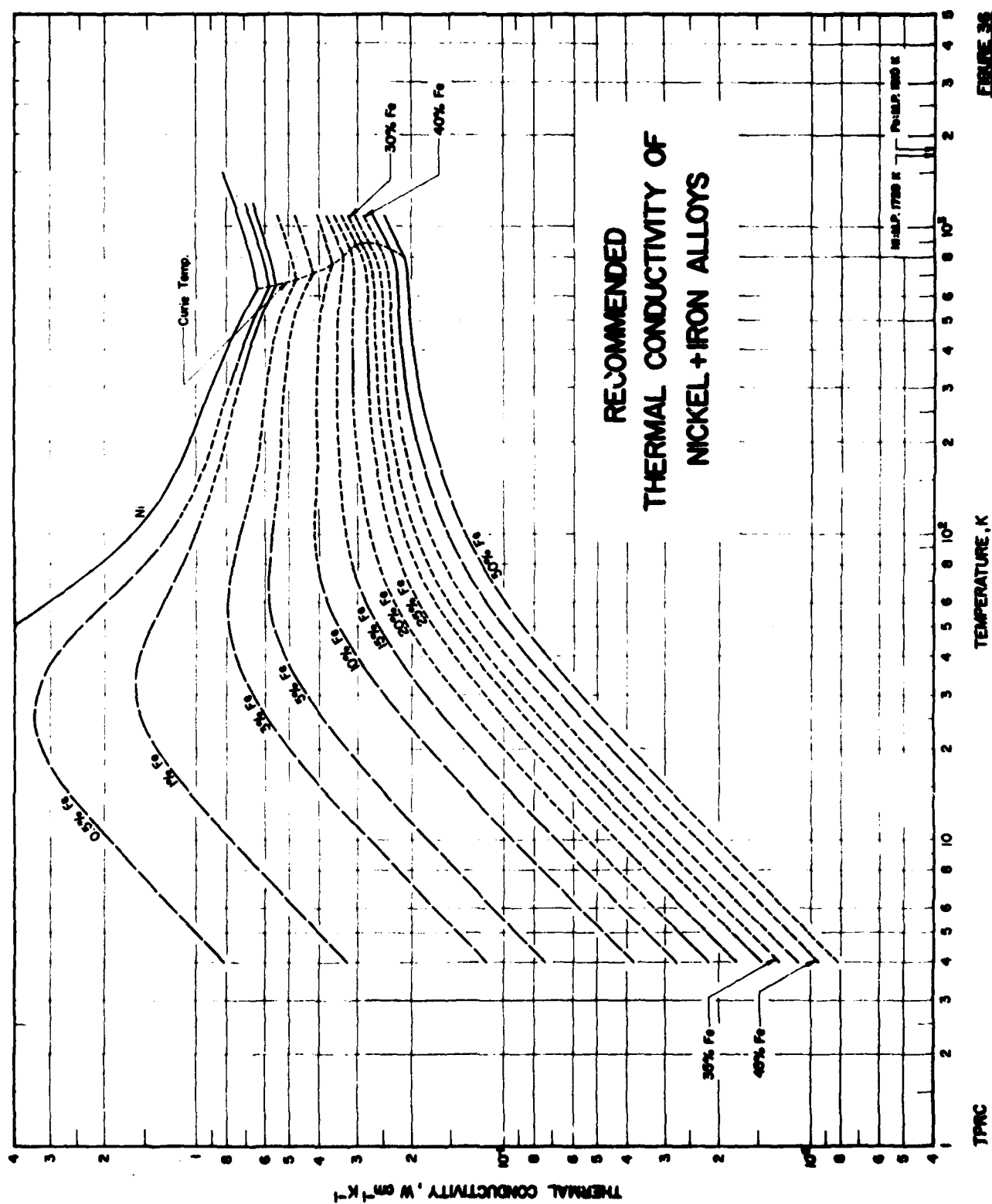


FIGURE 36

TPMC



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THERMAL CONDUCTIVITY OF TEN SELECTED BINARY ALLOY  
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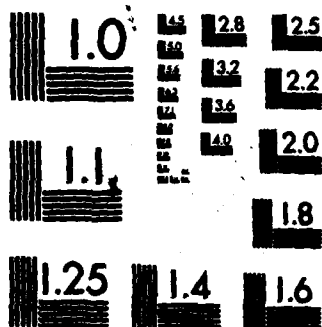
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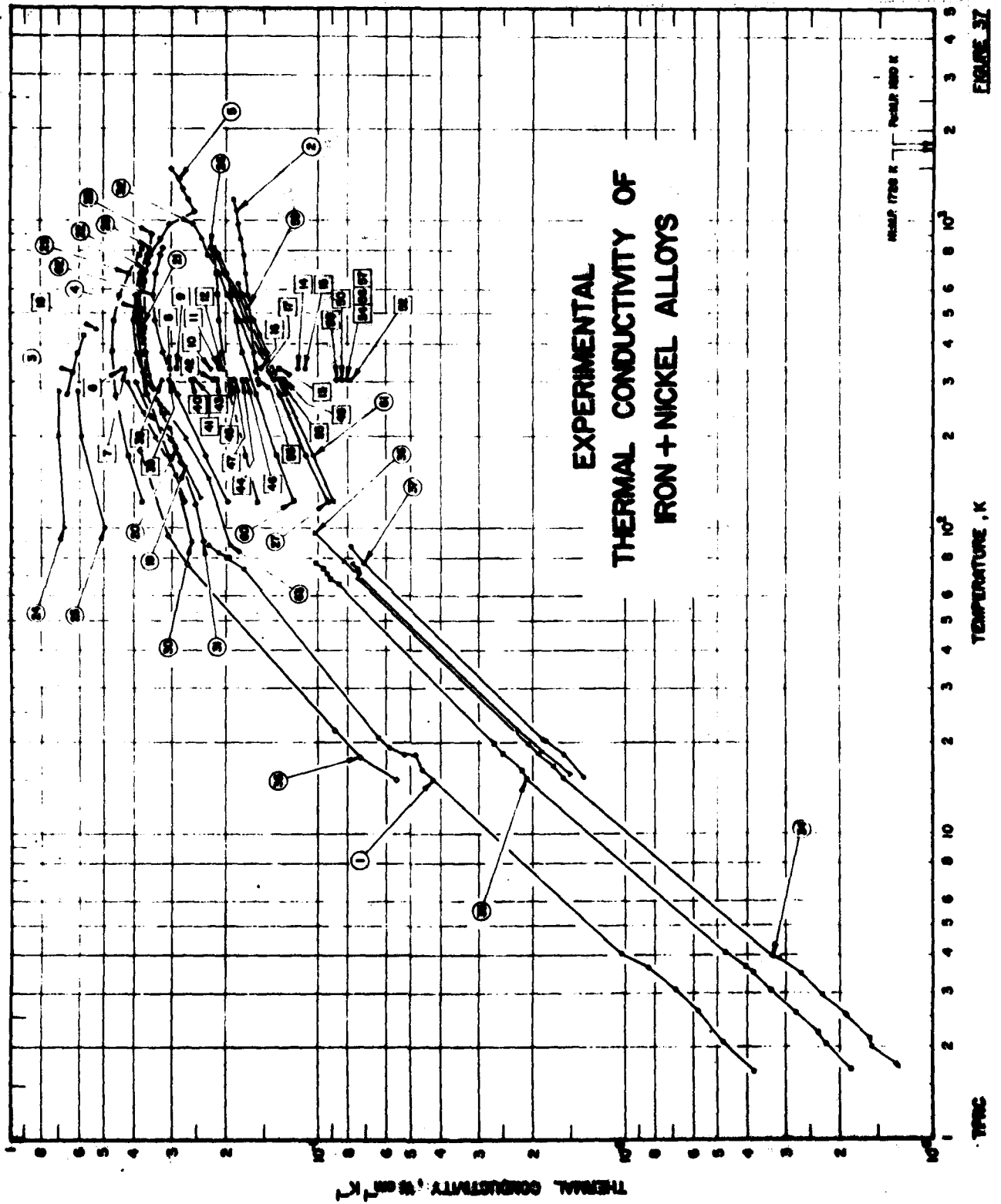
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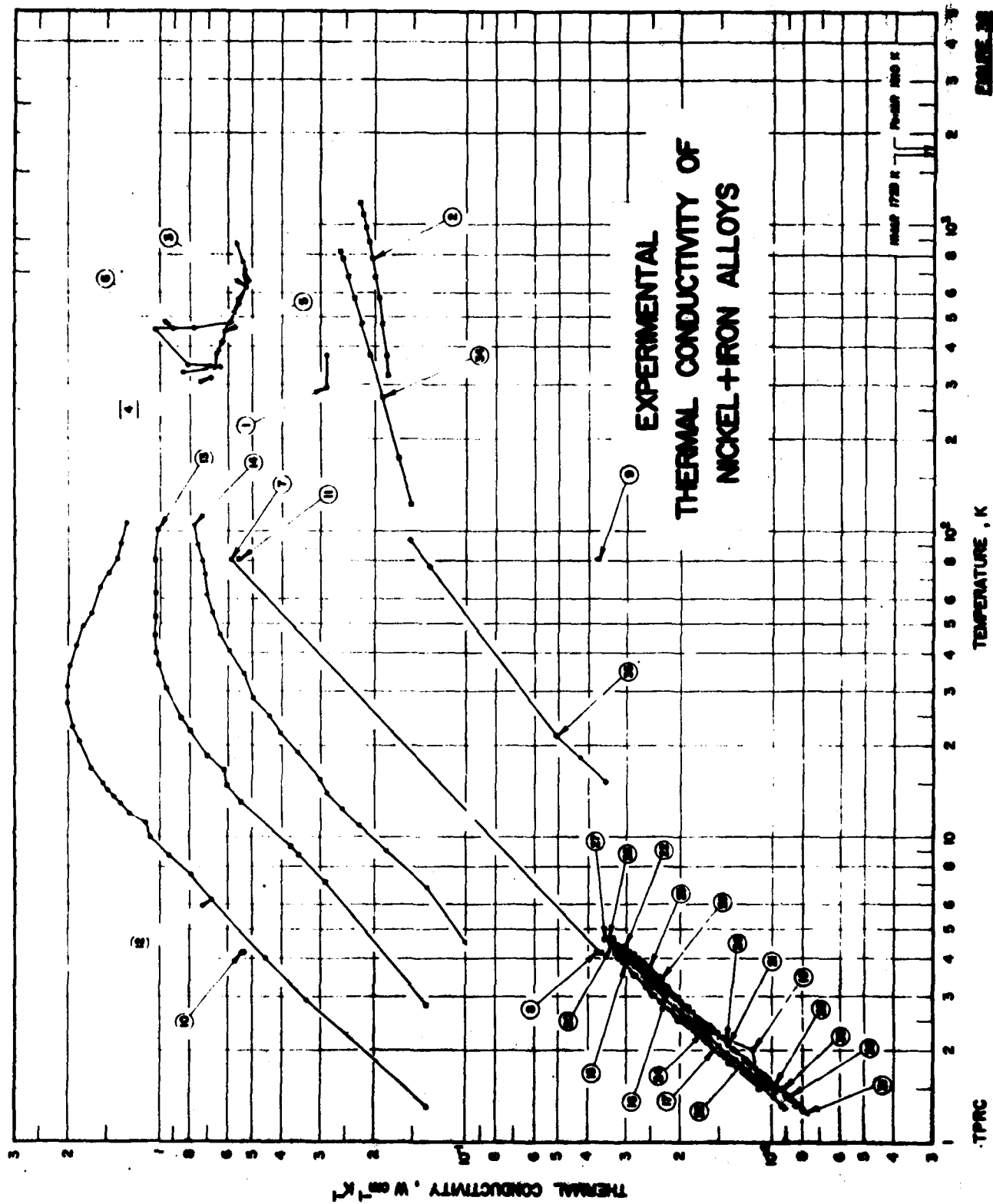


TABLE 24. THERMAL CONDUCTIVITY OF IRON + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Fe Ni	Composition (continued), Specifications, and Remarks
1	Chari, M.S.R. and de Mel, J.	1959	L	1.6-46	3703	Bal.	0.34 Mn, 0.16 Si, 0.11 C, 0.04 S, and 0.041 P; 7.8 mm diameter rod specimen; heated to 800 C and cooled in furnace.
2	Silversman, L.	1953	C	323-1173	45% Ni-iron	55.8	0.22 Mn, 0.050 C, and 0.003 S; annealed at 950 C; Advance used as comparative material.
3	Powell, R.W. and Richardson, M.J.	1959	C	373-423	Carbon steel; 1	Bal.	0.38 Mn, 0.06 Cu, 0.06 C, 0.039 As, 0.036 S, 0.03 Mo, 0.022 Cr, 0.017 P, 0.01 Si, and 0.001 Al; 1 in. diameter and 8 in. long; annealed at 930 C; density 7.871 g cm <sup>-3</sup> ; electrical resistivity 11.8, 14.6, 17.6, 21.1, and 24.9 μΩ cm at 9, 59, 109, 159, and 209 C, respectively.
4	Powell, R.W. and Richardson, M.J.	1959	C	373-573	Alloy steel; 9	Bal.	0.55 Mn, 0.325 C, 0.16 Si, 0.17 Cr, 0.066 Cu, 0.034 S, 0.022 P, 0.023 As, 0.04 Mo, 0.01 V, and 0.006 Al; annealed at 960 C; density 7.855 g cm <sup>-3</sup> ; electrical resistivity 28.5, 28.4, 31.5, 34.5, 38.5, 42.5, and 48.8 μΩ cm at 9, 90, 100, 150, 200, 250, and 300 C, respectively.
5	Powell, R.W.	1958	-	373-1473			The above specimen; thermal conductivity values calculated from measured electrical resistivity by the Wiedemann-Franz relation using extrapolated values of Lorenz function obtained from the previous thermal conductivity measurements.
6	Ingersoll, L.R., Kinsch, G.F., Garcia, D.L., Smith, R.F., Thompson, C.B., Mahro, M.A., Froelichsen, J.P., and Hubbard, D.R.	1959	L	330	144E	Bal.	<0.1 C; electrolytic.
7	Ingersoll, L.R., et al.	1959	L	330	144F	Bal.	<0.1 C; electrolytic.
8	Ingersoll, L.R., et al.	1959	L	330	144J	Bal.	<0.1 C; electrolytic.
9	Ingersoll, L.R., et al.	1959	L	330	137D	Bal.	<0.1 C; electrolytic.
10	Ingersoll, L.R., et al.	1959	L	330	144M	Bal.	<0.1 C; electrolytic.
11	Ingersoll, L.R., et al.	1959	L	330	144P	Bal.	<0.1 C; electrolytic.
12	Ingersoll, L.R., et al.	1959	L	330	146G	Bal.	<0.1 C; electrolytic; electrical resistivity reported as 36.7, 45.4, 53.4, 62.7, 72.5, 82.1, 106.3, and 111.6 μΩ cm at 373.2, 373.2, 473.2, 573.2, 673.2, 773.2, 873.2, and 973.2 K, respectively.
13	Ingersoll, L.R., et al.	1959	L	330	144S	Bal.	<0.1 C; electrolytic.
14	Ingersoll, L.R., et al.	1959	L	330	146C	Bal.	<0.1 C; electrolytic.
15	Ingersoll, L.R., et al.	1959	L	330	146L	Bal.	<0.1 C; electrolytic; electrical resistivity reported as 99.3, 100.0, 100.1, 118.2, 119.4, 123.2, 125.9, and 126.3 μΩ cm at 373.2, 373.2, 473.2, 573.2, 673.2, 773.2, 873.2, and 973.2 K, respectively.
16	Ingersoll, L.R., et al.	1959	L	330	146O	Bal.	<0.1 C; electrolytic; electrical resistivity reported as 44.2, 60.0, 75.6, 92.1, 103.3, 109.3, 112.3, and 114.6 μΩ cm at 373.2, 373.2, 473.2, 573.2, 673.2, 773.2, 873.2, and 973.2 K, respectively.
17	Ellis, W.C., Morgan, F.L., and Sager, G.F.	1959	P	305	Climax	Bal.	2.5 mm diameter and 25 mm long; density 8.01 g cm <sup>-3</sup> ; electrical conductivity 1.052 x 10 <sup>6</sup> Ω <sup>-1</sup> cm <sup>-1</sup> at 32 C; thermal conductivity values calculated from measured thermal diffusivity and specific heat capacity.

TABLE 24. THERMAL CONDUCTIVITY OF IRON + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Fe	Ni	
18 103	Maron, H.	1955	C	446	Nickel steel	Bal.	3.41	0.45 C; steel used as comparative material.
19 102	Watson, T.W. and Robinson, H.E.	1961	L	125-263	ANSI 2515	94.076	4.91	0.52 Mn, 0.33 Si, and 0.14 C; specimen about 2.54 cm in diameter and about 37 cm long; furnished by International Nickel Co.; normalized at 1144.3 K, tempered at 906.5 K.
20 103	Watson, T.W. and Robinson, H.E.	1961	L	183-483	ANSI 2515			The above specimen, run 2.
21 103	Watson, T.W. and Robinson, H.E.	1961	L	372-573	ANSI 2515			The above specimen, run 3.
22 103	Watson, T.W. and Robinson, H.E.	1961	L	400-696	ANSI 2515			The above specimen, run 4.
23 103	Watson, T.W. and Robinson, H.E.	1961	L	423-908	ANSI 2515			The above specimen, run 5.
24 101	McClum, H.G.	1961	L	100-280	3		0.946	Original material supplied by Horacius, Inc.; re-melted and rolled into bars with a cross-section of about 15 mm <sup>2</sup> and a length of 106 mm; after a short rolling, annealed at 1373 K for 2 hr in evacuated silica tubes, then rolled to final form and annealed at about 773 K for 18 hr; electrical resistivity 3.4, 7.9, and 12.9 $\mu\Omega$ cm at 90, 193, and 299 K, respectively. Similar to the above specimen; electrical resistivity 5.3, 9.5, and 15.1 $\mu\Omega$ cm at 90, 193, and 299 K, respectively.
25 101	McClum, H.G.	1961	L	100-280	5		1.90	0.44 Mn, 0.54 Si, 0.09 Cr, and 0.035 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; packed in powder and annealed in hydrogen 5 hr at 922.1 K, 5 hr at 1450 K; furnace cooled to 709 K; data presented as a smooth curve.
26 103	Watson, T.W. and Robinson, H.E.	1961	L	123-813	High-perm-49	49.503	49.15	0.13 Si, 0.06 C, and 0.04 Cr; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; annealed 30 min at 1102.6 K, water-quenched, air-cooled at 548.7 K for 1 hr and at 309.3 K for 48 hr; data presented as a smooth curve.
27 103	Watson, T.W. and Robinson, H.E.	1961	L	123-813	Invar	63.97	35.41	0.54 Mn, 0.32 Si, and 0.16 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; normalized at 1173.5 K and tempered at 906.5 K; data presented as a smooth curve.
28 103	Watson, T.W. and Robinson, H.E.	1961	L	123-813	ANSI 2515	95.483	3.46	0.56 Mn, 0.37 Si, and 0.126 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; normalized at 1200 K, tempered at 906.5 K; presented as a smooth curve.
29 103	Watson, T.W. and Robinson, H.E.	1961	L	123-813	1% Ni	97.964	1.04	0.45 Mn, 0.33 Si, and 0.06 C; heat-treated in air at 860 C for 0.5 hr and at 800 C for 2 hr; electrical resistivity 19.78, 21.99, 22.99, 24.31, 25.52, 27.06, 28.36, 29.50, and 30.76 $\mu\Omega$ cm at -199, -76, -50, -25, 0, 29, 49, 69, and 99 C, respectively.
30 97, 103	Kottmann, R. and Kluge, W.	1965	L	90-296	10 Ni 14		3.75	0.40 Mn, 0.35 Si, and 0.06 C; same heat-treatment as above; electrical resistivity 18.26, 23.43, 24.51, 25.96, 27.61, 28.78, 29.94, 31.13, and 32.43 $\mu\Omega$ cm at -199, -76, -50, -25, 0, 29, 49, 69, and 99 C, respectively.
31 97, 103	Kottmann, R. and Kluge, W.	1965	L	90-296	12 Ni 19		4.75	0.32 Mn, 0.012 P, 0.06 Al, 0.06 Si, 0.06 Mo, 0.06 Co, 0.02 C, and 0.008 S; cylindrical specimen; heat-treated in water at 1000 C for 24 hr; electrical resistivity 76.1, 86.8, 96.3, 101.7, 106.7, 109.0, 112.3, 115.0, 117.8, 119.7, 121.9, and 123.7 $\mu\Omega$ cm at 20, 100, 200, 300, 400, 500, 600, 700, 800, 900, 1000, and 1100 C, respectively; smoothed values reported.
32 104	Engel, E. and Speer, W.	1965	L	292-973	Ni 36	Bal.	36.91	

TABLE 24. THERMAL CONDUCTIVITY OF IRON + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Fe	Ni	
23	Chen, M.S.R. and de Nobel, J.	1969	L	1.7-76	1287 I		11.39	0.83 Mn, 0.22 Si, and 0.16 C; 5 mm diameter rod specimen; heated to 800 C and cooled in furnace.
24	Chen, M.S.R. and de Nobel, J.	1969	L	1.7-76	1798 H		19.64	1.09 Mn and 0.43 C; 7.5 mm diameter rod specimen; same heat-treatment as the above specimen.
25	de Nobel, J.	1961	L	15-180	1397 D		1.92	0.72 Mn, 0.21 Si, and 0.14 C; 0.5 cm diameter and 4 cm long; heated to 800 C and cooled in furnace.
26	de Nobel, J.	1961	L	15-96	1449 A		31.4	0.82 Mn and 0.70 C; 0.5 cm diameter and 4 cm long; heated to 800 C and cooled in furnace.
27	de Nobel, J.	1961	L	15-97	3450-3		36.17	0.92 Mn, 0.69 Si, and 0.16 C; 0.5 cm diameter and 4 cm long; heated to 1050 C and quenched in water.
28	Brash, K.	1918	E	303	2a		4.6	0.49 Cu, 0.31 Mn, 0.11 Si, 0.10 C, 0.028 P, 0.026 S, and 0.012 Co (calculated composition); 5 mm diameter and 20 cm long; prepared by melting together iron and nickel in a porcelain crucible, resulting alloy polished, forged, annealed, and filed to size; annealed at 900 C; electrical conductivity $2.63 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
29	Brash, K.	1918	E	303	2b			Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $3.64 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
40	Brash, K.	1918	E	303	3a		9.2	0.67 Cu, 0.32 Mn, 0.11 C, 0.11 Si, 0.027 P, 0.025 S, and 0.024 Co (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $2.81 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
41	Brash, K.	1918	E	303	3b			Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.79 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
42	Brash, K.	1918	E	303	4a		13.8	0.97 Cu, 0.32 Mn, 0.13 C, 0.13 Si, 0.028 Co, 0.025 P, and 0.025 S (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $2.65 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
43	Brash, K.	1918	E	303	4b			Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.66 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
44	Brash, K.	1918	E	303	5a		16.5	1.06 Cu, 0.32 Mn, 0.13 C, 0.13 Si, 0.046 Co, 0.024 P, and 0.024 S (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $2.33 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
45	Brash, K.	1918	E	303	5b			Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.45 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
46	Brash, K.	1918	E	303	6a		21.2	1.17 Cu, 0.32 Mn, 0.13 C, 0.13 Si, 0.046 Co, 0.023 P, and 0.024 S (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $2.61 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.

TABLE 26. THERMAL CONDUCTIVITY OF IRON + NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Fe Ni	Composition (continued), Specifications, and Remarks
47	165 Beach, K.	1918	E	303	6b		Same composition, dimensions, and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $2.20 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
48	165 Beach, K.	1918	E	303	7a	23.6	1.27 Cu, 0.32 Mn, 0.14 C, 0.12 Si, 0.061 Co, 0.024 S, and 0.022 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.82 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
49*	165 Beach, K.	1918	E	303	7b		Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.33 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
50	165 Beach, K.	1918	E	303	9a	27.7	1.44 Cu, 0.32 Mn, 0.15 C, 0.12 Si, 0.071 Co, 0.023 S, and 0.021 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.07 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
51*	165 Beach, K.	1918	E	303	9b		Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.40 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
52	165 Beach, K.	1918	E	303	10a	29.1	1.51 Cu, 0.32 Mn, 0.15 C, 0.12 Si, 0.078 Co, 0.023 S, and 0.021 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.88 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
53	165 Beach, K.	1918	E	303	10b		Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $2.35 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
54	165 Beach, K.	1918	E	303	11a	30.5	1.54 Cu, 0.32 Mn, 0.155 C, 0.12 Si, 0.078 Co, 0.023 S, and 0.020 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.86 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
55	165 Beach, K.	1918	E	303	11b		Same composition, dimensions, and fabrication method as the above specimen; cooled once to -190 C in liquid air; electrical conductivity $1.86 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
56	165 Beach, K.	1918	E	303	12a	32.8	1.65 Cu, 0.32 Mn, 0.16 C, 0.12 Si, 0.064 Co, 0.023 S, and 0.019 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.91 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
57	165 Beach, K.	1918	E	303	12b		Similar to the above specimen except cooled once to -190 C in liquid air instead of annealing.
58	165 Beach, K.	1918	E	303	13a	34.9	1.63 Cu, 0.32 Mn, 0.17 C, 0.12 Si, 0.095 Co, 0.023 S, and 0.019 P (calculated composition); same dimensions and fabrication method as the above specimen; annealed at 900 C; electrical conductivity $1.84 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 30 C.
59	56 Powell, E.W. and Williams, M.J.	1959	C	273-623	High-Ni steel; 14	28.37	0.89 Mn, 0.28 C, 0.15 Si, 0.030 Cu, 0.027 As, 0.012 Al, 0.009 P, 0.002 S, and trace Cr; 1 in. diameter and 8 in. long; heated to 500 C and cooled in water; electrical resistivity 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, and 104.8 $\mu\Omega \text{ cm}$ at 0, 50, 100, 150, 200, 250, and 300 C, respectively; iron used as comparative material.

\* Not shown in figure.



TABLE 26. THERMAL CONDUCTIVITY OF IRON-NICKEL ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Fe	Ni	
60 102	Watson, T. W. and Robinson, H. E.	1961	L	123-813	Low-exp-42	56.303	43.11	0.97 Mn, 0.16 Si, 0.09 Cr, and 0.006 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; annealed for 96 min at 1064.7 K, furnace cooled; data presented as a smooth curve.
61 102	Watson, T. W. and Robinson, H. E.	1961	L	123-813	Free cut larar	62.233	35.04	0.81 Mn, 0.34 Si, 0.12 Cr, and 0.00 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; annealed for 20 min at 1103.6 K, water quenched, and air cooled 1 hr at 888.7 K, then 48 hr at 389.3 K; data presented as a smooth curve.
62 102	Watson, T. W. and Robinson, H. E.	1961	L	123-813	95 Ni	90.29	8.56	0.77 Mn, 0.28 Si, and 0.10 C; specimen 2.54 cm in diameter and 37 cm long; supplied by International Nickel Co.; normalized at (1050 + 1050 F) (1172 + 1041 K), tempered at 888.7 K; data presented as a smooth curve.
63 97, 101	Koblmann, R. and Kierup, W.	1965	L	80-397	X3 Ni9		8.36	0.74 Mn, 0.28 Si, 0.021 C, 0.018 P, and 0.003 H; heat-treated in air at 730 C for 0.5 hr and at 570 C for 3.6 hrs; electrical resistivity 32.06, 28.20, 25.34, 20.04, 22.54, 22.04, 20.21, 20.05, and 27.70 $\mu\Omega$ cm at -100, -70, -50, -25, 0, 20, 40, 60, and 80 C, respectively.

TABLE 27. THERMAL CONDUCTIVITY OF NICKEL + IRON ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Ni	Fe	
1	90 Ingersoll, L. R.	1939	L	293-373	106 Q	75.06		<0.1 C; prepared from 99.97 pure iron and high-purity nickel by forging; 0.96 cm in diameter and 5.1 to 6.7 cm long; electrical resistivity 23.4, 31.3, 40.0, 51.0, 62.0, 70.2, 75.0, and 76.3 $\mu\Omega$ cm at 0, 100, 200, 300, 400, 500, 600, and 700 C, respectively.
2	132 Silverman, L.	1963	C	323-1173		50.85	48.5	0.12 Mn, 0.024 C, and 0.003 S; annealed at 950 C; Advance (55 Cu, 45 Ni) used as comparative material.
3	100 Shelton, S. M. and Swager, W. H.	1963	C	513-486	N.S. nickel, commercial	99 <sup>a</sup>	0.6	0.14 Cu, 0.09 Mn, and 0.014 S; 2 cm in diameter and 15 cm long; lead used as comparative material.
4	106 Shelton, S. M. and Swager, W. H.	1963	C	313.2	N.S. nickel, commercial			Similar to the above specimen.
5	106 Shelton, S. M. and Swager, W. H.	1963	C	339-964	N.S. nickel, commercial			Similar to the above specimen except nickel used as comparative material.
6	106 Bell, L. P. and MacDonald, J. J.	1963	L	338-472	Nickel, commercial	99.4	0.2	0.1 Mg, 0.05 Co, 0.03 Sn, 0.026 C, 0.02 Si, 0.01 Cr, 0.01 Mn, 0.005 S, 0.003 Ti, and 0.002 each of Al and Pb; cylindrical specimen.
7	107 Deuser, L. and Rivier, D.	1962	L	4.2, 80		95.2	14.8	0.2 cm diameter and 5.2 cm long; fused in an induction furnace under vacuum of $10^{-3}$ torr; the mixture of Ni and Fe supplied by Johnson-Matthey; cold-rolled, annealed at 1173 K for 2 hr, slowly cooled; electrical resistivity 3.78, 4.60, and 12.22 $\mu\Omega$ cm at 4.16, 86.6, and 292.7 K, respectively.
8	107 Deuser, L. and Rivier, D.	1962	L	4.2				The above specimen measured in transverse magnetic fields ranging from 0.150 to 1.92 W m <sup>-2</sup> .
9	107 Deuser, L. and Rivier, D.	1962	L	80				The above specimen measured in transverse magnetic fields ranging from 0.373 to 1.92 W m <sup>-2</sup> .
10	107 Deuser, L. and Rivier, D.	1962	L	4.2				The above specimen measured in longitudinal magnetic fields ranging from 0.079 to 1.76 W m <sup>-2</sup> .
11	107 Deuser, L. and Rivier, D.	1962	L	80				The above specimen measured in longitudinal magnetic fields ranging from 0.051 to 1.41 W m <sup>-2</sup> .
12	81 Farrell, T. and Greig, D.	1969	L	1.3-106			0.8	About 3 mm in diameter and 9 cm long; chill-cast under vacuum; annealed at 850 C for 16 hr; residual electrical resistivity 0.307 $\mu\Omega$ cm.
13	81 Farrell, T. and Greig, D.	1969	L	2.8-100			1.7	Similar to the above specimen except residual electrical resistivity 0.713 $\mu\Omega$ cm; electrical resistivity 7.99 $\mu\Omega$ cm at 8 C.
14	81 Farrell, T. and Greig, D.	1969	L	4.5-106			4.4	Similar to the above specimen except residual electrical resistivity 1.80 $\mu\Omega$ cm; electrical resistivity 9.94 $\mu\Omega$ cm at 8 C.
15	106 Yelen, W. B. and Deuser, L.	1970	L	1.3-4.1	Permalloy	82	18	Calculated composition.
16	106 Yelen, W. B. and Deuser, L.	1970	L	1.5-4.1	Permalloy	71	29	Calculated composition.
17	106 Yelen, W. B. and Deuser, L.	1970	L	1.5-4.0	Permalloy			The above specimen measured in a longitudinal magnetic field of 0.781 T.
18 <sup>a</sup>	106 Yelen, W. B. and Deuser, L.	1970	L	1.5-4.0	Permalloy			The above specimen measured in a longitudinal magnetic field of 3.3 T.

<sup>a</sup>Not shown in figure.

TABLE 27. THERMAL CONDUCTIVITY OF NICKEL + IRON ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Ni Fe	Composition (continued), Specifications, and Remarks
19 105	Yelon, W.B. and Burger, L.	1970	L	1.5-4.0	Permalloy		The above specimen measured in a longitudinal magnetic field of 5.34 T.
20 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.6-4.4		29.8	Prepared by fusing Johnson-Matthey metals in argon atmosphere, remelting and casting into 0.5 in. rods in helium, averaging to 0.3125 in. in diameter, homogenizing in hydrogen at 1200 C for 36 hr, cooling to 900 C in vacuum and annealing for 2 hr; grain size 0.1 ~ 0.5 mm; electrical resistivity 4.34 $\mu\Omega$ cm at 4.2 K; run 7.
21 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.5-4.4			The above specimen measured in a parallel magnetic field of 7.81 kG.
22 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.6-4.4			The above specimen measured in a parallel magnetic field of 33.00 kG.
23 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.6-4.4			The above specimen measured in a parallel magnetic field of 59.40 kG.
24 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.5-4.3			The above specimen, no magnetic field; run 8.
25 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.4			The above specimen measured in a parallel magnetic field of 7.81 kG.
26 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.5-4.4			The above specimen measured in a parallel magnetic field of 59.40 kG.
27 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.7		18.9	Same preparation method as the above specimen; grain size 0.1-0.5 mm; electrical resistivity 4.32 $\mu\Omega$ cm at 4.2 K; run 2.
28 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.6			The above specimen measured in a parallel magnetic field of 7.15 kG.
29 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.4-4.6			The above specimen measured in a parallel magnetic field of 59.40 kG.
30 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.6			The above specimen measured in a parallel magnetic field of 7.15 kG; run 3.
31 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.2-4.6			The above specimen measured in a parallel magnetic field of 33.00 kG.
32 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.6			The above specimen measured in the same magnetic field; run 4.
33 106, 177	Yelon, W.B. and Burger, L.	1970	L	1.3-4.6			The above specimen measured in a parallel magnetic field of 59.40 kG.
34 102	Walden, T.W. and Robinson, E.E.	1961	L	123-813	HyMu 90	79.24 15.283	0.71 Mn, 0.19 Si, 0.06 Cr, and 0.049 C; 2.54 cm diameter and 37 cm long; supplied by International Nickel Co.; powder packed in sealed in hydrogen at 922 K (1200 F) for 5 hr and at 1450 K (2150 F) for 5 hr, furnace cooled to 700 K (500 F), then cooled in hydrogen; smoothed values reported.
35 100	de Nobel, J.	1961	L	15-93	5277	57.5	1.31 Mn, 0.34 C, and 0.14 Si; as forged.

#### 4.10. Silver-Palladium Alloy System

The silver-palladium alloy system exhibits complete solid solubility and is analogous to the copper-nickel alloy system, but without the complications of ferromagnetic effects and with an electronic specific heat that is better behaved [109].

There are 32 sets of experimental data available for the thermal conductivity of this alloy system. However, of the 18 data sets available for Ag + Pd alloys listed in Table 29 and shown in Figure 41 six sets are merely single data points, and of the 14 sets for Pd + Ag alloys listed in Table 30 and shown in Figure 42 seven sets are single data points.

This alloy system is the most extensively studied among the noble metal-palladium alloy systems, but the only reliable experimental data on thermal conductivity are the low temperature measurements by Kemp, et al. [110] (Pd + Ag curves 6-8 and Ag + Pd curves 6-14), Tainsh and White [111] (Ag + Pd curves 16-18), and Fletcher and Greig [84] (Pd + Ag curves 11-14). The early measurements by Schulze [93] (Pd + Ag curves 1-5 and Ag + Pd curves 1-5) of the room temperature thermal conductivity of these alloys at intervals of 10% gave values that are considerably above the actual values in some cases. Even after correcting for the lattice component, the Lorenz ratios corresponding to Schulze's values for the 60, 70, and 80% Pd alloys are respectively 30, 44, and 35% greater than the classical value; it is unlikely that band structure effects could cause such large Lorenz ratios in these alloys at 298 K. Further evidence that Schulze's values are unreliable is that he used the same method to measure the thermal conductivity of gold-palladium alloys, and that interpolation between his values for his 30 and 40% Pd specimens yields a value which is more than 25% greater than that obtained by Laubitz and van der Meer [85] for a specimen containing 35% Pd. On the other hand, the more recent measurements by Zolotukhin [112] at somewhat higher temperatures on specimens containing 25 and 50% Ag (Pd + Ag curves 9 and 10 and Ag + Pd curve 15) appear to be too low, in the second instance by approximately 25%.

This alloy system is one of the few in which the thermal conductivity has been measured over a very wide range of compositions from liquid helium temperatures to 100 K. The measurements by Kemp, et al. were undertaken to obtain fundamental information about the electron-phonon interaction, in particular to see whether electrons interact with lattice waves of all polarizations, to determine the dependence of the interaction on electron concentration and to deduce, by interpolation between these and similar measurements on silver-cadmium alloys, the contribution of the electron-phonon interaction to the lattice thermal resistivity of silver. The study revealed the cusp-like behavior of the low temperature lattice conductivity as a function of composition, as discussed in Section 2 on Theoretical Background, and led to additional measurements by Tainsh and White following further

annealing at higher temperatures to determine whether or not this behavior was caused by the locking in of dislocations by solute atoms. While the cusp-like behavior persisted, it was found that an increase in the annealing temperature from 883 K to 1213 K resulted in increases of 30% or more in the lattice thermal conductivities of these specimens at liquid helium temperatures.

A comparison of the values calculated from eqs. (12) and (35) in the region above the lattice component maximum with the experimental values of Kemp, et al. revealed that the calculated values for the silver-rich alloys were too low, the total conductivity by as much as 8% and the lattice component by as much as 25%. It was found that both the total and lattice thermal conductivities could be brought into good agreement with the experimental values for all compositions from 2 to 30% Pd by increasing the value of the lattice thermal conductivity of silver by 50%. Although such an increase does not require unreasonable values for the Debye temperature or the Grüneisen parameter in the equation used to estimate the lattice thermal conductivity of the elements, it raises considerable doubt as to the reliability of such estimates. While the separation of the electronic and lattice components of very dilute alloys at temperatures above that of the maximum of the lattice component involves some uncertainty, a 50% error in the lattice component is unlikely, although excellent agreement was obtained for the lattice conductivities of both 2 and 5% Pd alloys, it was decided, in view of the conflicting evidence, not to report even provisional values for the lattice thermal conductivity of the dilute silver-rich alloys. In addition, while the measurements of Tainsh and White established that, in the region below its maximum, the lattice thermal conductivity of well-annealed samples is substantially greater than the values obtained from the first set of measurements, these later measurements were limited to temperatures below 10 K and to compositions of 2, 5, and 10% Pd and could, therefore, only serve as a rough guide for correcting the values of the lattice component obtained from measurements on specimens annealed at 883 K; accordingly, the values for the silver-rich alloys at temperatures below the maximum are provisional.

The lattice thermal conductivity of the palladium-rich alloys of this system was investigated by Fletcher and Greig, who measured the thermal conductivity of specimens containing 5, 10, 15, and 20% Ag from liquid helium temperatures to about 100 K. Their study showed that the strong electron-phonon interactions in these alloys greatly reduces the low temperature lattice thermal conductivity, causing its maximum to occur at much higher temperatures than in the silver-rich alloys. The increase in the temperature of the maximum of the lattice component is even greater than that shown in their graph because, at the higher temperatures, the method used to separate the electronic and lattice components yields values of the latter which are below the true values by an amount which increases with temperature, so that the lattice components of these alloys are still increasing at 100 K. This is consistent with the 100 K temperature of the maximum deduced from the measurements

by Kemp, et al. on a specimen containing 30% Ag. Since the measurements on the Pd-rich alloys did not extend to temperatures above those of the lattice thermal conductivity maxima, the values of the lattice component in this region were obtained by smoothly joining plots of the values deduced from measurements to those calculated from eq. (35).

The recommended values for  $k$ ,  $k_e$ , and  $k_g$  are tabulated in Table 28 for 25 alloy compositions covering the full range of temperature from 4 to 1200 K for most cases. These values are for well-annealed alloys. The values for  $k$  are also shown in Figures 39 and 40. The values of residual electrical resistivity for the alloys are also given in Table 28. The uncertainties of the  $k$  values are stated in a footnote to Table 28, while the uncertainties of the  $k_e$  and  $k_g$  values are indicated by their being designated as recommended or provisional values. The ranges of uncertainties of recommended and provisional values are less than  $\pm 15\%$  and between  $\pm 15$  and  $\pm 30\%$ , respectively.

TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM†

[Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>]

Ag: 99.50% (99.49 At. %) Pd: 0.50% (0.51 At. %)				Ag: 99.00% (98.99 At. %) Pd: 1.00% (1.01 At. %)				Ag: 97.00% (96.96 At. %) Pd: 3.00% (3.04 At. %)				Ag: 95.00% (94.93 At. %) Pd: 5.00% (5.07 At. %)			
$\rho_0 = 0.2400 \mu\Omega\text{cm}$				$\rho_0 = 0.4900 \mu\Omega\text{cm}$				$\rho_0 = 1.390 \mu\Omega\text{cm}$				$\rho_0 = 2.260 \mu\Omega\text{cm}$			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4	0.48*	0.407	0.0415*	4	0.230*	0.199	0.0310*	4	0.0963*	0.0703	0.0260*	4	0.0634*	0.0432	0.0202*
6	0.69*	0.611	0.0665*	6	0.365*	0.299	0.0655*	6	0.159*	0.105	0.0535*	6	0.109*	0.0649	0.0445*
8	0.94*	0.814	0.135*	8	0.505*	0.399	0.106*	8	0.228*	0.141	0.0870*	8	0.160*	0.0865	0.0735*
10	1.20*	1.02	0.190*	10	0.644*	0.499	0.145*	10	0.300*	0.176	0.124*	10	0.212*	0.108	0.104*
15	1.78*	1.53	0.246*	15	0.963*	0.748	0.215*	15	0.453*	0.264	0.189*	15	0.319*	0.162	0.157*
20	2.33*	2.04	0.295*	20	1.25*	0.997	0.254*	20	0.571*	0.352	0.219*	20	0.405*	0.216	0.189*
25	2.63*	2.35	0.298*	25	1.47*	1.20	0.272*	25	0.665*	0.433	0.232*	25	0.467*	0.262	0.205*
30	2.84*	2.54	0.300*	30	1.67*	1.39	0.276*	30	0.748*	0.513	0.235*	30	0.521*	0.311	0.210*
40	3.03*	2.73	0.295*	40	1.96*	1.69	0.272*	40	0.892*	0.661	0.231*	40	0.612*	0.404	0.208*
50	3.04*			50	2.11*			50	1.01			50	0.685		
60	2.96*			60	2.18*			60	1.09			60	0.750		
70	3.00*			70	2.26*			70	1.16			70	0.811		
80	3.07*			80	2.35*			80	1.25			80	0.877		
90	3.10*			90	2.44*			90	1.33			90	0.938		
100	3.19*			100	2.52*			100	1.41			100	0.998		
150	3.49*			150	2.87*			150	1.76			150	1.27		
200	3.89*			200	3.12*			200	2.02*			200	1.51*		
250	3.74*			250	3.27*			250	2.24*			250	1.71*		
273	3.76*			273	3.33*			273	2.33*			273	1.79*		
300	3.83*			300	3.41*			300	2.43*			300	1.88*		
350	3.89*			350	3.50*			350	2.57*			350	2.04*		
400	3.96*			400	3.57*			400	2.69*			400	2.18*		
500	3.91*			500	3.63*			500	2.89*			500	2.41*		
600	3.90*			600	3.69*			600	3.03*			600	2.58*		
700	3.84*			700	3.67*			700	3.12*			700	2.72*		
800	3.81*			800	3.67*			800	3.18*			800	2.83*		
900	3.74*			900	3.63*			900	3.21*			900	2.89*		
1000	3.67*			1000	3.57*			1000	3.22*			1000	2.93*		
1100	3.60*			1100	3.51*			1100	3.22*			1100	2.96*		
1200	3.59*			1200	3.46*			1200	3.22*			1200	2.98*		

† Uncertainties of the total thermal conductivity, k, are as follows:

99.50 Ag - 0.50 Pd:  $\pm 10\%$  below 40 K,  $\pm 7\%$  between 40 and 300 K, and  $\pm 10\%$  above 300 K.99.00 Ag - 1.00 Pd:  $\pm 15\%$  below 40 K and  $\pm 10\%$  above 40 K.97.00 Ag - 3.00 Pd:  $\pm 15\%$  below 40 K and  $\pm 10\%$  above 40 K.95.00 Ag - 5.00 Pd:  $\pm 15\%$  below 40 K and  $\pm 10\%$  above 40 K.

\* Provisional values.

† In temperature range where no experimental thermal conductivity data are available.

TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

$\rho_0 = 4.46 \mu\Omega \text{ cm}$				$\rho_0 = 6.46 \mu\Omega \text{ cm}$				$\rho_0 = 8.41 \mu\Omega \text{ cm}$				$\rho_0 = 10.60 \mu\Omega \text{ cm}$			
Ag: 90.00% (88.86 At.%) Pd: 10.00% (10.12 At.%)				Ag: 85.00% (84.82 At.%) Pd: 15.00% (15.18 At.%)				Ag: 80.00% (79.78 At.%) Pd: 20.00% (20.22 At.%)				Ag: 75.00% (74.74 At.%) Pd: 25.00% (25.26 At.%)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0344 <sup>‡</sup>	0.0219	0.0145 <sup>‡</sup>	4	0.0299 <sup>‡</sup>	0.0151	0.0148 <sup>‡</sup>	4	0.0270 <sup>‡</sup>	0.0116	0.0154 <sup>‡</sup>	4	0.0253 <sup>‡</sup>	0.00822	0.0161 <sup>‡</sup>
6	0.0463 <sup>‡</sup>	0.0333 <sup>‡</sup>	0.0333 <sup>‡</sup>	6	0.0553 <sup>‡</sup>	0.0227	0.0326 <sup>‡</sup>	6	0.0518 <sup>‡</sup>	0.0174	0.0344 <sup>‡</sup>	6	0.0483 <sup>‡</sup>	0.0138	0.0345 <sup>‡</sup>
8	0.1064 <sup>‡</sup>	0.0438	0.0562 <sup>‡</sup>	8	0.0853 <sup>‡</sup>	0.0303	0.0550 <sup>‡</sup>	8	0.0812 <sup>‡</sup>	0.0232	0.0580 <sup>‡</sup>	8	0.0764 <sup>‡</sup>	0.0184	0.0580 <sup>‡</sup>
10	0.1364 <sup>‡</sup>	0.0578	0.0773 <sup>‡</sup>	10	0.1194 <sup>‡</sup>	0.0378	0.0810 <sup>‡</sup>	10	0.112 <sup>‡</sup>	0.0290	0.0825 <sup>‡</sup>	10	0.107 <sup>‡</sup>	0.0280	0.0840 <sup>‡</sup>
15	0.201 <sup>‡</sup>	0.0822	0.119 <sup>‡</sup>	15	0.182 <sup>‡</sup>	0.0567	0.125 <sup>‡</sup>	15	0.165 <sup>‡</sup>	0.0436	0.121 <sup>‡</sup>	15	0.159 <sup>‡</sup>	0.0346	0.124 <sup>‡</sup>
20	0.233 <sup>‡</sup>	0.110	0.143 <sup>‡</sup>	20	0.224 <sup>‡</sup>	0.0756	0.148 <sup>‡</sup>	20	0.200 <sup>‡</sup>	0.0581	0.142 <sup>‡</sup>	20	0.192 <sup>‡</sup>	0.0461	0.146 <sup>‡</sup>
25	0.252 <sup>‡</sup>	0.135	0.157 <sup>‡</sup>	25	0.251 <sup>‡</sup>	0.0931	0.158 <sup>‡</sup>	25	0.224 <sup>‡</sup>	0.0717	0.152 <sup>‡</sup>	25	0.213 <sup>‡</sup>	0.0569	0.156 <sup>‡</sup>
30	0.324 <sup>‡</sup>	0.161	0.183 <sup>‡</sup>	30	0.272 <sup>‡</sup>	0.111	0.161 <sup>‡</sup>	30	0.241 <sup>‡</sup>	0.0856	0.155 <sup>‡</sup>	30	0.223 <sup>‡</sup>	0.0680	0.155 <sup>‡</sup>
40	0.374 <sup>‡</sup>	0.213	0.161 <sup>‡</sup>	40	0.301 <sup>‡</sup>	0.147	0.154 <sup>‡</sup>	40	0.263 <sup>‡</sup>	0.113	0.150 <sup>‡</sup>	40	0.238 <sup>‡</sup>	0.0901	0.148 <sup>‡</sup>
50	0.417	0.261	0.156	50	0.326 <sup>‡</sup>	0.181	0.145	50	0.281	0.140	0.141	50	0.248 <sup>‡</sup>	0.112	0.136
60	0.454	0.307	0.147	60	0.351 <sup>‡</sup>	0.215	0.136	60	0.298	0.167	0.131	60	0.259 <sup>‡</sup>	0.133	0.126
70	0.491	0.352	0.139	70	0.375 <sup>‡</sup>	0.248	0.127	70	0.316	0.193	0.123	70	0.271 <sup>‡</sup>	0.154	0.117
80	0.527	0.396	0.131	80	0.400 <sup>‡</sup>	0.281	0.119	80	0.333	0.219	0.114	80	0.285 <sup>‡</sup>	0.175	0.110
90	0.565	0.441	0.124	90	0.427 <sup>‡</sup>	0.314	0.113	90	0.352	0.245	0.107	90	0.299 <sup>‡</sup>	0.196	0.104
100	0.602	0.485	0.117	100	0.452 <sup>‡</sup>	0.346	0.106	100	0.371	0.270	0.101	100	0.314 <sup>‡</sup>	0.216	0.0975
150	0.780	0.687	0.0830	150	0.581 <sup>‡</sup>	0.497	0.0840	150	0.472	0.392	0.0800	150	0.393 <sup>‡</sup>	0.316	0.0770
200	0.943 <sup>‡</sup>	0.886	0.0775	200	0.706 <sup>‡</sup>	0.636	0.0700	200	0.573 <sup>‡</sup>	0.506	0.0670	200	0.475 <sup>‡</sup>	0.410	0.0645
250	1.10 <sup>‡</sup>	1.03	0.0665	250	0.827 <sup>‡</sup>	0.766	0.0610	250	0.671 <sup>‡</sup>	0.613	0.0580	250	0.556 <sup>‡</sup>	0.500	0.0600
273	1.16 <sup>‡</sup>	1.10	0.0627	273	0.881 <sup>‡</sup>	0.823	0.0575	273	0.716 <sup>‡</sup>	0.661	0.0545	273	0.593 <sup>‡</sup>	0.540	0.0630
300	1.24	1.16	0.0586	300	0.942 <sup>‡</sup>	0.888	0.0539	300	0.766	0.715	0.0511	300	0.635 <sup>‡</sup>	0.596	0.0484
350	1.30 <sup>‡</sup>	1.32	0.0526	350	1.05 <sup>‡</sup>	1.00	0.0487	350	0.858 <sup>‡</sup>	0.812	0.0463	350	0.711 <sup>‡</sup>	0.667	0.0448
400	1.50 <sup>‡</sup>	1.45	0.0479	400	1.16 <sup>‡</sup>	1.11	0.0444	400	0.946 <sup>‡</sup>	0.904	0.0424	400	0.783 <sup>‡</sup>	0.741	0.0411
500	1.73 <sup>‡</sup>	1.66	0.0406	500	1.35 <sup>‡</sup>	1.31	0.0380	500	1.11 <sup>‡</sup>	1.07	0.0364	500	0.922 <sup>‡</sup>	0.886	0.0384
600	1.91 <sup>‡</sup>	1.88	0.0354	600	1.52 <sup>‡</sup>	1.49	0.0333	600	1.26 <sup>‡</sup>	1.23	0.0320	600	1.05 <sup>‡</sup>	1.03	0.0313
700	2.07 <sup>‡</sup>	2.04	0.0313	700	1.68 <sup>‡</sup>	1.65	0.0297	700	1.39 <sup>‡</sup>	1.36	0.0287	700	1.17 <sup>‡</sup>	1.14	0.0281
800	2.21 <sup>‡</sup>	2.18	0.0282	800	1.83 <sup>‡</sup>	1.80	0.0268	800	1.53 <sup>‡</sup>	1.50	0.0260	800	1.29 <sup>‡</sup>	1.26	0.0255
900	2.33 <sup>‡</sup>	2.30	0.0256	900	1.93 <sup>‡</sup>	1.91	0.0245	900	1.63 <sup>‡</sup>	1.60	0.0238	900	1.38 <sup>‡</sup>	1.36	0.0234
1000	2.41 <sup>‡</sup>	2.38	0.0235	1000	2.02 <sup>‡</sup>	2.00	0.0226	1000	1.71 <sup>‡</sup>	1.69	0.0220	1000	1.45 <sup>‡</sup>	1.43	0.0216
1100	2.47 <sup>‡</sup>	2.45	0.0217	1100	2.10 <sup>‡</sup>	2.08	0.0209	1100	1.79 <sup>‡</sup>	1.76	0.0204	1100	1.53 <sup>‡</sup>	1.51	0.0201
1200	2.53 <sup>‡</sup>	2.51	0.0201	1200	2.16 <sup>‡</sup>	2.14	0.0195	1200	1.84 <sup>‡</sup>	1.82	0.0191	1200	1.60 <sup>‡</sup>	1.58	0.0188

<sup>†</sup> Uncertainties of the total thermal conductivity,  $k$ , are as follows:

- 90.00 Ag - 10.00 Pd:  $\pm 1\%$  below 40 K and  $\pm 10\%$  above 40 K.
- 85.00 Ag - 15.00 Pd:  $\pm 20\%$  below 40 K and  $\pm 10\%$  above 40 K.
- 80.00 Ag - 20.00 Pd:  $\pm 20\%$  below 40 K and  $\pm 10\%$  above 40 K.
- 75.00 Ag - 25.00 Pd:  $\pm 20\%$  below 40 K and  $\pm 10\%$  above 40 K.

<sup>‡</sup> Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.



TABLE 2A. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity, k<sub>g</sub>, W cm<sup>-1</sup> K<sup>-1</sup>

Ag: 70.00% (69.71 At. %) Pd: 30.00% (30.29 At. %)					Ag: 65.00% (64.69 At. %) Pd: 35.00% (35.31 At. %)					Ag: 60.00% (59.67 At. %) Pd: 40.00% (40.33 At. %)					Ag: 55.00% (54.66 At. %) Pd: 45.00% (45.34 At. %)				
$\rho_0 = 12.01 \mu\Omega\text{cm}$					$\rho_0 = 15.62 \mu\Omega\text{cm}$					$\rho_0 = 18.44 \mu\Omega\text{cm}$					$\rho_0 = 21.56 \mu\Omega\text{cm}$				
T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>		T	k	k <sub>e</sub>	k <sub>g</sub>	
4	0.0041*	0.00781	0.0100*		4	0.0231**	0.00626	0.0168*		4	0.0222*	0.00530	0.0169*		4	0.0213**	0.00453	0.0107*	
6	0.0072*	0.0113	0.0300*		6	0.0439**	0.00938	0.0345*		6	0.0410*	0.00795	0.0330*		6	0.0393**	0.00800	0.0316*	
8	0.0103*	0.0150	0.0400*		8	0.0690**	0.0125	0.0565*		8	0.0646*	0.0106	0.0540*		8	0.0626**	0.00907	0.0485*	
10	0.103*	0.0186	0.0535*		10	0.0945**	0.0156	0.0789*		10	0.0881*	0.0132	0.0749*		10	0.0778**	0.0113	0.0680*	
15	0.184*	0.0302	0.126*		15	0.144**	0.0235	0.121*		15	0.134*	0.0199	0.114*		15	0.119**	0.0170	0.101*	
20	0.180*	0.0376	0.140*		20	0.176**	0.0313	0.144*		20	0.163*	0.0265	0.136*		20	0.144**	0.0237	0.121*	
25	0.201*	0.0464	0.156*		25	0.191**	0.0367	0.163*		25	0.179*	0.0328	0.146*		25	0.163**	0.0280	0.134*	
30	0.212*	0.0545	0.169*		30	0.201**	0.0433	0.183*		30	0.188*	0.0393	0.150*		30	0.173**	0.0335	0.136*	
40	0.231*	0.0726	0.187*		40	0.210**	0.0614	0.199*		40	0.197*	0.0521	0.165*		40	0.183**	0.0445	0.150*	
50	0.237	0.0913	0.136		50	0.214**	0.0763	0.136		50	0.200	0.0648	0.135		50	0.183**	0.0553	0.136*	
60	0.235	0.100	0.126		60	0.216**	0.0909	0.125		60	0.201	0.0772	0.124		60	0.185**	0.0689	0.119	
70	0.243	0.116	0.117		70	0.230**	0.106	0.114		70	0.201	0.0896	0.115		70	0.187**	0.0764	0.111	
80	0.242	0.143	0.109		80	0.237**	0.130	0.107		80	0.205	0.102	0.107		80	0.191**	0.0870	0.104	
90	0.268	0.161	0.102		90	0.236**	0.134	0.101		90	0.214	0.114	0.100		90	0.195**	0.0974	0.0975	
100	0.276	0.178	0.0965		100	0.245**	0.149	0.0960		100	0.221	0.127	0.0940		100	0.200**	0.108	0.0909	
150	0.288	0.261	0.0765		150	0.294**	0.219	0.0750		150	0.280	0.186	0.0740		150	0.233**	0.158	0.0749	
200	0.464*	0.340	0.0440		200	0.346**	0.266	0.0635		200	0.304**	0.243	0.0630		200	0.269**	0.206	0.0689	
250	0.471*	0.415	0.0555		250	0.403**	0.349	0.0540		250	0.350**	0.296	0.0540		250	0.305**	0.251	0.0649	
273	0.591*	0.449	0.0359		273	0.438**	0.377	0.0510		273	0.371**	0.330	0.0510		273	0.323**	0.272	0.0619	
300	0.534	0.496	0.0484		300	0.457**	0.409	0.0479		300	0.396	0.349	0.0479		300	0.343**	0.286	0.0482	
350	0.590*	0.585	0.0439		350	0.511**	0.468	0.0436		350	0.441*	0.397	0.0435		350	0.390**	0.336	0.0438	
400	0.681*	0.631	0.0403		400	0.563**	0.523	0.0400		400	0.484*	0.444	0.0400		400	0.416**	0.376	0.0403	
500	0.780*	0.745	0.0369		500	0.664**	0.629	0.0346		500	0.587*	0.532	0.0347		500	0.482**	0.447	0.0349	
600	0.901*	0.869	0.0306		600	0.759**	0.727	0.0307		600	0.643*	0.613	0.0307		600	0.543**	0.512	0.0319	
700	0.980*	0.979	0.0277		700	0.846**	0.818	0.0276		700	0.715*	0.687	0.0276		700	0.599**	0.571	0.0279	
800	1.10*	1.07	0.0252		800	0.936**	0.901	0.0252		800	0.780*	0.754	0.0252		800	0.651**	0.626	0.0255	
900	1.19*	1.16	0.0232		900	0.997**	0.974	0.0231		900	0.837*	0.813	0.0232		900	0.701**	0.677	0.0236	
1000	1.29*	1.24	0.0215		1000	1.09*	1.04	0.0215		1000	0.889*	0.867	0.0216		1000	0.750**	0.728	0.0218	
1100	1.39*	1.36	0.0200		1100	1.12*	1.10	0.0200		1100	0.938*	0.917	0.0201		1100	0.796**	0.778	0.0204	
1200	1.39*	1.37	0.0187		1200	1.18*	1.16	0.0188		1200	0.984*	0.965	0.0189		1200	0.846**	0.837	0.0191	

† Uncertainties of the total thermal conductivity, k, are as follows:

70.00 Ag - 30.00 Pd  $\pm 30\%$  below 40 K and  $\pm 10\%$  above 40 K.65.00 Ag - 35.00 Pd  $\pm 30\%$  below 40 K and  $\pm 10\%$  above 40 K.60.00 Ag - 40.00 Pd  $\pm 30\%$  below 40 K and  $\pm 10\%$  above 40 K.55.00 Ag - 45.00 Pd  $\pm 30\%$  below 40 K and  $\pm 10\%$  above 40 K.

\* Provisional values.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued)†

† Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>

$\rho_0 = 27.44 \mu\Omega\text{cm}$				$\rho_0 = 36.50 \mu\Omega\text{cm}$				$\rho_0 = 40.15 \mu\Omega\text{cm}$				$\rho_0 = 39.40 \mu\Omega\text{cm}$			
Ag 58.00% (49.66 At.%) Pd 58.00% (50.34 At.%)				Ag 45.00% (44.66 At.%) Pd 55.00% (55.34 At.%)				Ag 40.00% (39.67 At.%) Pd 60.00% (60.33 At.%)				Ag 35.00% (34.69 At.%) Pd 65.00% (65.31 At.%)			
T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$	T	k	$k_e$	$k_g$
4	0.0197†	0.00308	0.0161†	4	0.0174†	0.00268	0.0147†	4	0.0150†	0.00243	0.0126†	4	0.0132†	0.00248	0.0107†
6	0.0247†	0.00534	0.0204†	6	0.0222†	0.00402	0.0252†	6	0.0243†	0.00365	0.0206†	6	0.0200†	0.00372	0.0163†
8	0.0309†	0.00713	0.0431†	8	0.0411†	0.00536	0.0356†	8	0.0335†	0.00487	0.0286†	8	0.0268†	0.00496	0.0216†
10	0.0384†	0.00900	0.0545†	10	0.0527†	0.00669	0.0460†	10	0.0423†	0.00609	0.0363†	10	0.0332†	0.00630	0.0270†
15	0.0474†	0.0134	0.0640†	15	0.0755†	0.0100	0.0655†	15	0.0611†	0.00913	0.0520†	15	0.0476†	0.00930	0.0383†
20	0.118†	0.0178	0.100†	20	0.914†	0.0134	0.0780†	20	0.0757†	0.0122	0.0635†	20	0.0599†	0.0124	0.0475†
25	0.131†	0.0220	0.109†	25	0.103†	0.0166	0.0860†	25	0.0866†	0.0151	0.0715†	25	0.0703†	0.0153	0.0566†
30	0.141†	0.0264	0.115†	30	0.111†	0.0199	0.0910†	30	0.0946†	0.0181	0.0765†	30	0.0795†	0.0183	0.0610†
40	0.148†	0.0349	0.117†	40	0.123†	0.0264	0.0965†	40	0.106†	0.0240	0.0820†	40	0.0939†	0.0243	0.0696†
50	0.157	0.0434	0.114	50	0.131†	0.0327	0.0985†	50	0.115†	0.0298	0.0850†	50	0.104†	0.0302	0.0740†
60	0.163	0.0518	0.110	60	0.137†	0.0390	0.0980†	60	0.122†	0.0356	0.0865†	60	0.113†	0.0359	0.0770†
70	0.165	0.0598	0.105	70	0.141†	0.0452	0.0960	70	0.128†	0.0414	0.0870†	70	0.121†	0.0417	0.0796†
80	0.168	0.0669	0.0996	80	0.144†	0.0514	0.0930	80	0.133†	0.0469	0.0860†	80	0.127†	0.0474	0.0796†
90	0.171	0.0760	0.0945	90	0.148†	0.0576	0.0900	90	0.138†	0.0526	0.0850	90	0.133†	0.0531	0.0800†
100	0.175	0.0841	0.0906	100	0.151†	0.0637	0.0870	100	0.142†	0.0582	0.0836	100	0.138†	0.0586	0.0800†
150	0.196†	0.123	0.0745	150	0.167†	0.0935	0.0735	150	0.159†	0.0859	0.0730	150	0.159†	0.0854	0.0730
200	0.222†	0.159	0.0630	200	0.186†	0.122	0.0635	200	0.175†	0.111	0.0640	200	0.177†	0.111	0.0655
250	0.259†	0.194	0.0556	250	0.206†	0.150	0.0560	250	0.193†	0.136	0.0570	250	0.199†	0.136	0.0599
273	0.269†	0.210	0.0525	273	0.216†	0.162	0.0535	273	0.202†	0.148	0.0543	273	0.204†	0.147	0.0595
300	0.276	0.229	0.0489	300	0.226†	0.176	0.0499	300	0.212	0.161	0.0513	300	0.214†	0.161	0.0532
350	0.304†	0.259	0.0445	350	0.249†	0.204	0.0454	350	0.233†	0.186	0.0467	350	0.233†	0.185	0.0494
400	0.339	0.299	0.0409	400	0.272†	0.231	0.0418	400	0.255†	0.212	0.0429	400	0.253†	0.208	0.0445
500	0.361	0.346	0.0354	500	0.318†	0.281	0.0362	500	0.297†	0.260	0.0372	500	0.293†	0.254	0.0395
600	0.439†	0.399	0.0314	600	0.362†	0.330	0.0321	600	0.339†	0.306	0.0330	600	0.334†	0.299	0.0342
700	0.477†	0.449	0.0254	700	0.407†	0.378	0.0280	700	0.381†	0.352	0.0296	700	0.379†	0.344	0.0306
800	0.504†	0.499	0.0209	800	0.453†	0.426	0.0264	800	0.424†	0.397	0.0272	800	0.417†	0.389	0.0281
900	0.573†	0.549	0.0209	900	0.499†	0.474	0.0244	900	0.468†	0.443	0.0250	900	0.461†	0.435	0.0259
1000	0.623†	0.600	0.0221	1000	0.545†	0.522	0.0226	1000	0.511†	0.498	0.0232	1000	0.503†	0.481	0.0249
1100	0.672†	0.651	0.0207	1100	0.591†	0.570	0.0211	1100	0.556†	0.535	0.0217	1100	0.551†	0.509	0.0224
1200	0.723†	0.704	0.0194	1200	0.637†	0.617	0.0196	1200	0.602†	0.582	0.0204	1200	0.596†	0.577	0.0211

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:58.00 Ag - 58.00 Pd  $\pm 10\%$  below 40 K, and  $\pm 10\%$  above 40 K.45.00 Ag - 55.00 Pd  $\pm 10\%$  below 60 K, and  $\pm 10\%$  above 60 K.40.00 Ag - 60.00 Pd  $\pm 10\%$  below 80 K, and  $\pm 10\%$  above 80 K.35.00 Ag - 65.00 Pd  $\pm 10\%$  below 100 K, and  $\pm 10\%$  above 100 K.

‡ Provisional value.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued)<sup>†</sup>  
 (Temperature, T, K; Thermal Conductivity, k, W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity, k<sub>e</sub>, W cm<sup>-1</sup> K<sup>-1</sup>)

$\rho_0 = 26.11 \mu\Omega\text{cm}$				$\rho_0 = 29.95 \mu\Omega\text{cm}$				$\rho_0 = 24.13 \mu\Omega\text{cm}$				$\rho_0 = 18.15 \mu\Omega\text{cm}$			
Ag: 26.00% (26.71 At.%) Pd: 73.00% (73.29 At.%)				Ag: 28.00% (24.74 At.%) Pd: 72.00% (75.26 At.%)				Ag: 20.00% (19.78 At.%) Pd: 80.00% (80.22 At.%)				Ag: 15.00% (14.83 At.%) Pd: 85.00% (85.17 At.%)			
T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>	T	k	k <sub>e</sub>	k <sub>g</sub>
4	0.0200	0.00378	0.00000	4	0.00908*	0.00326	0.00560	4	0.00805	0.00405	0.00400	4	0.00807	0.00538	0.00289
6	0.0163	0.00418	0.0121	6	0.0140*	0.00469	0.00910	6	0.0127	0.00608	0.00645	6	0.0127	0.00908	0.00465
8	0.0215	0.00537	0.0182	8	0.0190*	0.00653	0.0125	8	0.0175	0.00810	0.00940	8	0.0177	0.01108	0.00685
10	0.0273	0.00696	0.0203	10	0.0241*	0.00816	0.0159	10	0.0225	0.0101	0.0124	10	0.0228	0.0135	0.00925
15	0.0399	0.0104	0.0295	15	0.0362*	0.0122	0.0240	15	0.0350	0.0152	0.0198	15	0.0359	0.0202	0.0157
20	0.0516	0.0139	0.0377	20	0.0480*	0.0163	0.0317	20	0.0472	0.0202	0.0270	20	0.0496	0.0270	0.0226
25	0.0618	0.0179	0.0448	25	0.0583*	0.0198	0.0385	25	0.0583	0.0243	0.0340	25	0.0518	0.0323	0.0285
30	0.0713	0.0203	0.0509	30	0.0681*	0.0236	0.0445	30	0.0690	0.0289	0.0401	30	0.0748	0.0383	0.0355
40	0.0898	0.0288	0.0690	40	0.0855*	0.0310	0.0645	40	0.0869	0.0379	0.0510	40	0.0979	0.0499	0.0490
50	0.0995	0.0322	0.0803	50	0.0995*	0.0383	0.0812	50	0.105	0.0465	0.0685	50	0.117	0.0603	0.0685
60	0.110	0.0394	0.0908	60	0.111*	0.0452	0.0900	60	0.119	0.0548	0.0845	60	0.134	0.0711	0.0835
70	0.119	0.0455	0.0935	70	0.131*	0.0531	0.0985	70	0.131	0.0629	0.0960	70	0.147	0.0809	0.0905
80	0.137	0.0516	0.0970	80	0.131*	0.0589	0.0978	80	0.142	0.0708	0.0970	80	0.160	0.0906	0.0995
90	0.134	0.0577	0.0960	90	0.139*	0.0657	0.0920	90	0.152	0.0787	0.0930	90	0.172	0.100	0.0920
100	0.140	0.0587	0.0960	100	0.145*	0.0723	0.0925	100	0.159	0.0864	0.0940	100	0.183	0.109	0.0940
150	0.165	0.0618	0.0935	150	0.176*	0.109	0.0935	150	0.197*	0.121	0.0960	150	0.237*	0.149	0.0950
200	0.197*	0.119	0.0975	200	0.201*	0.133	0.0965	200	0.226*	0.153	0.0925	200	0.281*	0.194	0.0970
250	0.297*	0.145	0.0915	250	0.234*	0.160	0.0935	250	0.250*	0.182	0.0980	250	0.289*	0.215	0.0940
273	0.219*	0.136	0.0990	273	0.234*	0.172	0.0915	273	0.261*	0.195	0.0955	273	0.301*	0.239	0.0920
300	0.285	0.179	0.0955	300	0.246*	0.187	0.0939	300	0.274	0.211	0.0932	300	0.314*	0.245	0.0903
350	0.249*	0.156	0.0966	350	0.260*	0.213	0.0935	350	0.296*	0.239	0.0973	350	0.338*	0.275	0.0928
400	0.289*	0.219	0.0945	400	0.287*	0.239	0.0921	400	0.319*	0.266	0.0926	400	0.369*	0.305	0.0975
500	0.309*	0.265	0.0902	500	0.329	0.287	0.0945	500	0.364*	0.319	0.0954	500	0.409*	0.360	0.0960
600	0.249*	0.219	0.0997	600	0.375*	0.335	0.0976	600	0.410*	0.370	0.0901	600	0.454*	0.411	0.0935
700	0.297*	0.266	0.0931	700	0.417*	0.384	0.0938	700	0.459*	0.419	0.0960	700	0.499*	0.460	0.0950
800	0.439*	0.491	0.0903	800	0.461*	0.430	0.0908	800	0.499*	0.466	0.0937	800	0.541*	0.506	0.0933
900	0.474*	0.477	0.0970	900	0.504*	0.476	0.0983	900	0.543*	0.513	0.0900	900	0.585*	0.532	0.0954
1000	0.519*	0.519	0.0950	1000	0.547*	0.521	0.0962	1000	0.586*	0.558	0.0978	1000	0.627*	0.597	0.0929
1100	0.529*	0.541	0.0933	1100	0.583*	0.569	0.0945	1100	0.630*	0.604	0.0939	1100	0.669*	0.641	0.0977
1200	0.619*	0.591	0.0919	1200	0.640*	0.617	0.0929	1200	0.675*	0.651	0.0942	1200	0.712*	0.686	0.0959

<sup>†</sup> Uncertainties of the total thermal conductivity, k, are as follows:

- 26.00 Ag - 73.00 Pd:  $\pm 10\%$  below 100 K,  $\pm 7\%$  between 100 and 300 K, and  $\pm 10\%$  above 300 K.
- 28.00 Ag - 72.00 Pd:  $\pm 10\%$  below 150 K,  $\pm 7\%$  between 150 and 300 K, and  $\pm 10\%$  above 300 K.
- 20.00 Ag - 80.00 Pd:  $\pm 10\%$  below 150 K,  $\pm 7\%$  between 150 and 300 K, and  $\pm 10\%$  above 300 K.
- 15.00 Ag - 85.00 Pd:  $\pm 10\%$  below 150 K,  $\pm 7\%$  between 150 and 300 K, and  $\pm 10\%$  above 300 K.

\* In temperature range where no experimental thermal conductivity data are available.

TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ , W cm<sup>-1</sup> K<sup>-1</sup>; Electronic Thermal Conductivity,  $k_e$ , W cm<sup>-1</sup> K<sup>-1</sup>; Lattice Thermal Conductivity,  $k_g$ , W cm<sup>-1</sup> K<sup>-1</sup>]

Ag: 10.00% ( 9.88 At.%) Pd: 90.00% (90.12 At.%)			Ag: 5.00% ( 4.94 At.%) Pd: 95.00% (95.06 At.%)			Ag: 3.00% ( 2.96 At.%) Pd: 97.00% (97.04 At.%)			Ag: 1.00% ( 0.99 At.%) Pd: 99.00% (99.01 At.%)		
$\rho_0 = 12.16 \mu\Omega\text{cm}$			$\rho_0 = 6.08 \mu\Omega\text{cm}$			$\rho_0 = 3.670 \mu\Omega\text{cm}$			$\rho_0 = 1.270 \mu\Omega\text{cm}$		
T	k	$k_e$	T	k	$k_e$	T	k	$k_e$	T	k	$k_e$
4	0.00325	0.00804	4	0.0170	0.0161	4	0.0161	0.000900	4	0.0266	0.0769
6	0.0131	0.0121	6	0.0261	0.0241	6	0.0261	0.00199	6	0.0399	0.115
8	0.0239	0.0161	8	0.0355	0.0321	8	0.0355	0.00342	8	0.0533	0.154
10	0.0370	0.0201	10	0.0454	0.0402	10	0.0454	0.00515	10	0.0666	0.192
15	0.0423	0.0301	15	0.0708	0.0603	15	0.0708	0.0105	15	0.0999	0.289
20	0.0596	0.0402	20	0.0974	0.0804	20	0.0974	0.0170	20	0.133	0.385
25	0.0742	0.0481	25	0.120	0.0955	25	0.120	0.0240	25	0.163	0.416
30	0.0896	0.0532	30	0.143	0.112	30	0.143	0.0311	30	0.177	0.459
40	0.119	0.0728	40	0.184	0.139	40	0.184	0.0452	40	0.214	0.499
50	0.144	0.0875	50	0.217	0.159	50	0.217	0.0579	50	0.237	0.495
60	0.166	0.101	60	0.245	0.177	60	0.245	0.0682	60	0.254	0.482
70	0.184	0.114	70	0.269	0.192	70	0.269	0.0770	70	0.269	0.471
80	0.200	0.126	80	0.292	0.208	80	0.292	0.0842	80	0.285	0.472
90	0.216	0.136	90	0.312	0.222	90	0.312	0.0898	90	0.301	0.475
100	0.230	0.146	100	0.330	0.236	100	0.330	0.0940	100	0.313	0.479
150	0.283*	0.196	150	0.393*	0.287	150	0.393*	0.106	150	0.358	0.492
200	0.321*	0.233	200	0.433*	0.325	200	0.433*	0.108	200	0.389	0.490
250	0.346*	0.265	250	0.459*	0.356	250	0.459*	0.103	250	0.417	0.502
273	0.363*	0.280	273	0.470*	0.370	273	0.470*	0.0995	273	0.422	0.510
300	0.378	0.297	300	0.483*	0.387	300	0.483*	0.0958	300	0.445	0.523
350	0.400*	0.329	350	0.504*	0.419	350	0.504*	0.0858	350	0.472*	0.553
400	0.424*	0.360	400	0.525*	0.447	400	0.525*	0.0777	400	0.503	0.576
500	0.469*	0.414	500	0.563*	0.497	500	0.563*	0.0654	500	0.624*	0.624
600	0.514*	0.465	600	0.602*	0.546	600	0.602*	0.0566	600	0.661*	0.671
700	0.559*	0.511	700	0.641*	0.591	700	0.641*	0.0499	700	0.699*	0.718
800	0.596*	0.556	800	0.676*	0.632	800	0.676*	0.0446	800	0.733*	0.763
900	0.630*	0.600	900	0.713*	0.673	900	0.713*	0.0404	900	0.769*	0.806
1000	0.675*	0.643	1000	0.746*	0.709	1000	0.746*	0.0369	1000	0.799*	0.843
1100	0.715*	0.684	1100	0.779*	0.745	1100	0.779*	0.0339	1100	0.831*	0.881
1200	0.759*	0.727	1200	0.813*	0.781	1200	0.813*	0.0314	1200	0.862*	0.920
											0.955*

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

10.00 Ag - 90.00 Pd:  $\pm 10\%$ .

5.00 Ag - 95.00 Pd:  $\pm 10\%$ .

3.00 Ag - 97.00 Pd:  $\pm 10\%$ .

1.00 Ag - 99.00 Pd:  $\pm 10\%$ .

\* In temperature range where no experimental thermal conductivity data are available.

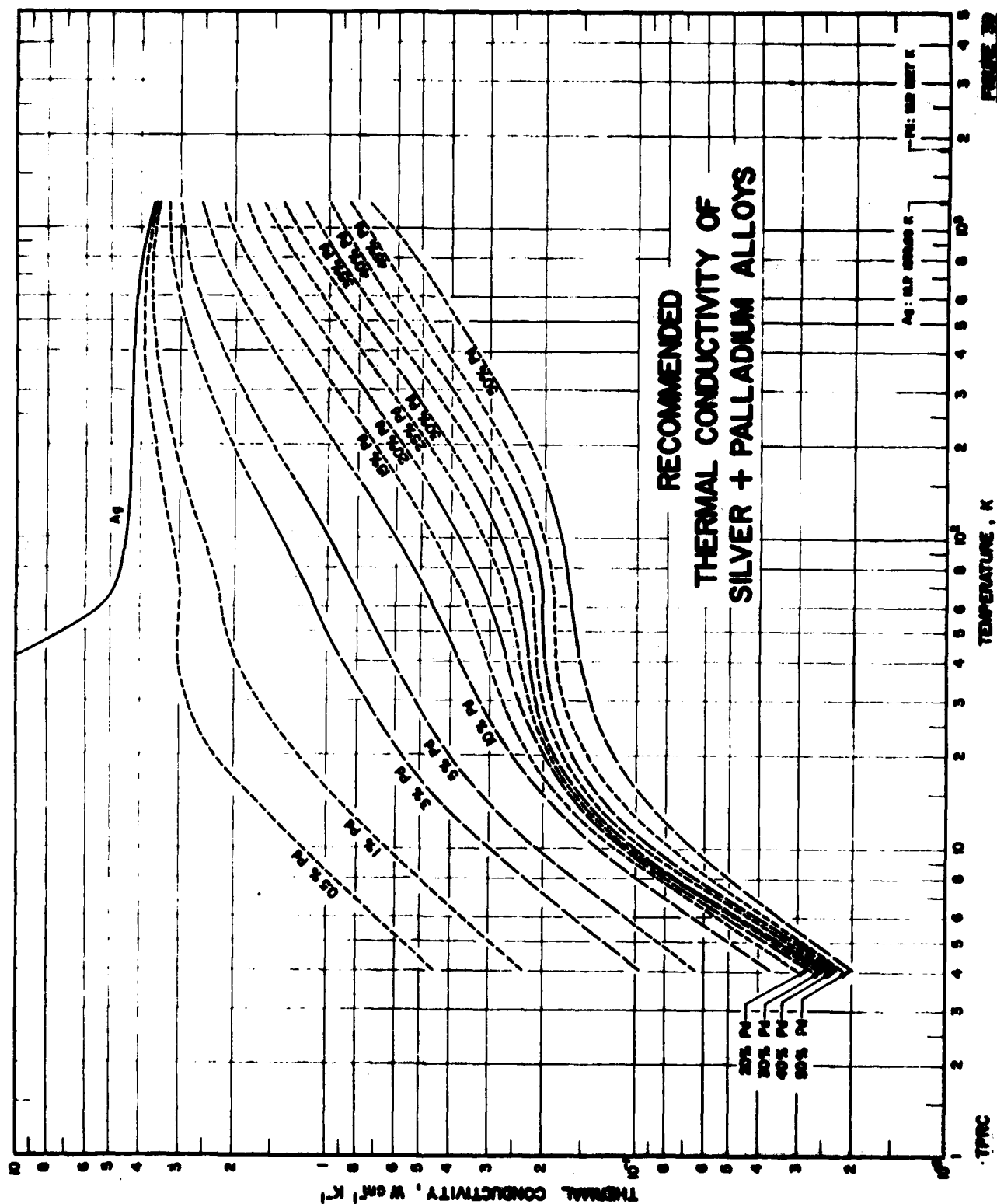
TABLE 28. RECOMMENDED THERMAL CONDUCTIVITY OF SILVER-PALLADIUM ALLOY SYSTEM (continued) †  
 [Temperature, T, K; Thermal Conductivity,  $k$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Electronic Thermal Conductivity,  $k_e$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ; Lattice Thermal Conductivity,  $k_g$ ,  $\text{W cm}^{-1} \text{K}^{-1}$ ]

Ag: 0.50% (.49 At. %) Pd: 99.50% (99.51 At. %)					
$\rho_0 = 0.009 \mu\Omega\text{cm}$					
T	k	$k_0$	$k_g$		
4		0.148			
6		0.222			
8		0.295			
10		0.370			
15		0.565			
20		0.740			
25		0.768			
30		0.743			
40		0.757			
50		0.765			
60		0.642			
70		0.601			
80		0.577			
90		0.572			
100		0.563			
150		0.534			
200		0.529			
250		0.534			
273		0.540			
300	0.686*	0.551	0.134		
350	0.894*	0.577	0.117		
400	0.769*	0.603	0.103		
500	0.738*	0.645	0.0837		
600	0.767*	0.697	0.0704		
700	0.883*	0.742	0.0607		
800	0.930*	0.786	0.0533		
900	0.979*	0.831	0.0475		
1000	0.913*	0.889	0.0439		
1100	0.949*	0.919	0.0391		
1200	0.980*	0.952	0.0339		

† Uncertainties of the total thermal conductivity,  $k$ , are as follows:

0.50 Ag - 99.50 Pd:  $\pm 10\%$ .

\* In temperature range where no experimental thermal conductivity data are available.



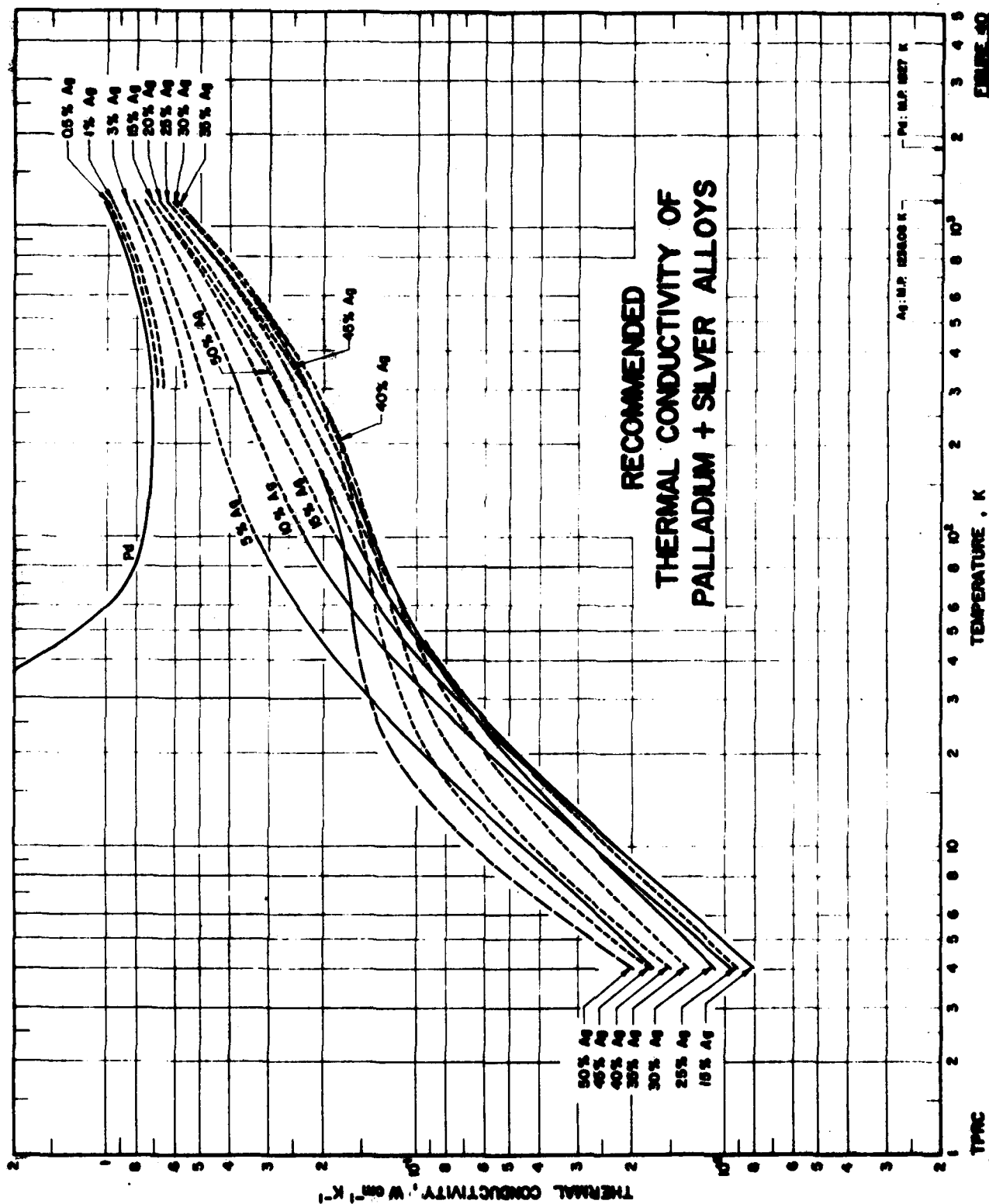
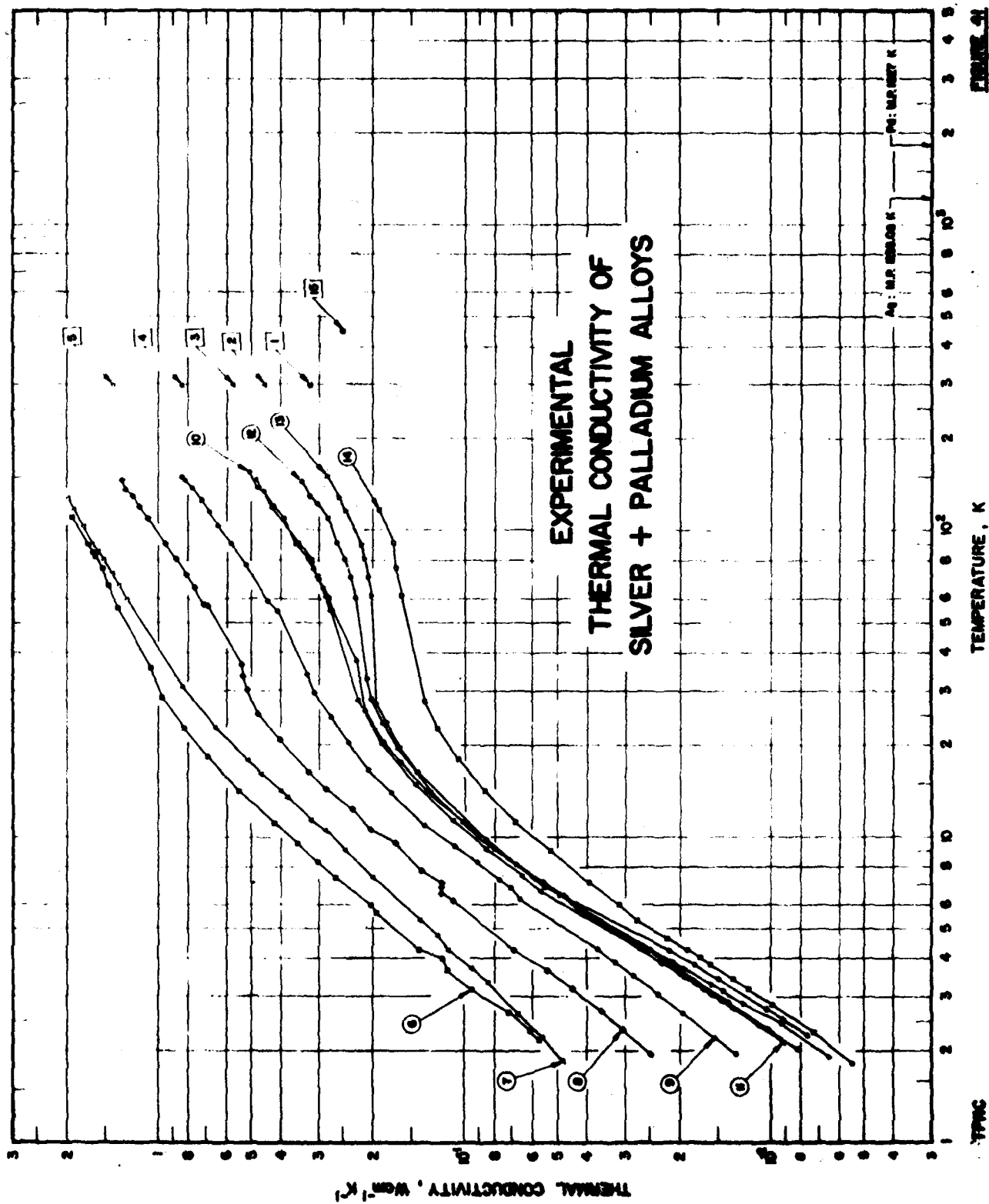


FIGURE 50





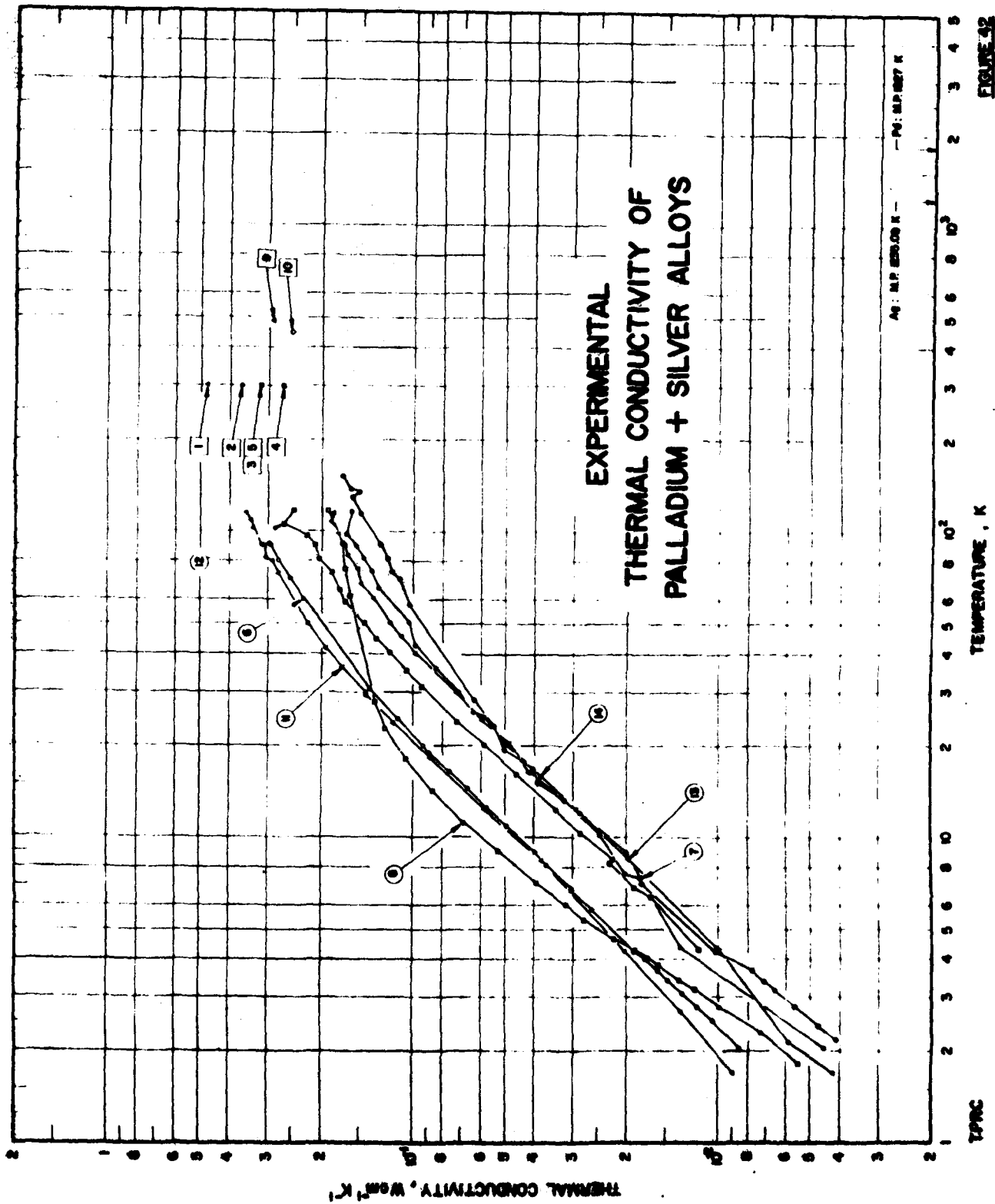


FIGURE 42

TABLE 29. THERMAL CONDUCTIVITY OF SILVER + PALLADIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent) Ag Pd	Composition (continued), Specifications, and Remarks
1	Schulze, F.A.	1911	E	296.2		50 50	1 mm wire specimen obtained from Firma Horacius; electrical conductivity $3.03 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
2	Schulze, F.A.	1911	E	296.2		60 40	1 mm wire specimen obtained from Firma Horacius; electrical conductivity $4.56 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
3	Schulze, F.A.	1911	E	296.2		70 30	1 mm wire specimen obtained from Firma Horacius; electrical conductivity $6.43 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
4	Schulze, F.A.	1911	E	296.2		80 20	1 mm wire specimen obtained from Firma Horacius; electrical conductivity $9.47 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
5	Schulze, F.A.	1911	E	296.2		90 10	1 mm wire specimen obtained from Firma Horacius; electrical conductivity $16.14 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
6	Kemp, W.R.G., Edwards, F.G., Sweeney, A.E. and White, G.E.	1966	L	2.2-112		97.95 2.05	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 610 C; residual electrical resistivity $0.88 \mu\Omega \text{ cm}$ ; electrical resistivity $2.82 \mu\Omega \text{ cm}$ at 293 K.
7	Kemp, W.R.G., et al.	1966	L	1.8-129			The above specimen; strained; residual electrical resistivity $0.94 \mu\Omega \text{ cm}$ ; electrical resistivity $2.84 \mu\Omega \text{ cm}$ at 293 K.
8	Kemp, W.R.G., et al.	1966	L	1.9-147		95.01 4.99	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 610 C; residual electrical resistivity $2.20 \mu\Omega \text{ cm}$ ; electrical resistivity $3.91 \mu\Omega \text{ cm}$ at 293 K.
9	Kemp, W.R.G., et al.	1966	L	2.0-150		90.22 9.78	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 650 C; residual electrical resistivity $4.15 \mu\Omega \text{ cm}$ ; electrical resistivity $6.0 \mu\Omega \text{ cm}$ at 293 K.
10	Kemp, W.R.G., et al.	1966	L	2.3-187		80.14 19.86	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 650 C.
11	Kemp, W.R.G., et al.	1966	L	2.1-147		80.14 19.86	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 800 C; residual electrical resistivity $8.45 \mu\Omega \text{ cm}$ ; electrical resistivity $10.0 \mu\Omega \text{ cm}$ at 293 K.
12	Kemp, W.R.G., et al.	1966	L	2.2-145		70.67 29.33	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 800 C; residual electrical resistivity $12.76 \mu\Omega \text{ cm}$ ; electrical resistivity $14.06 \mu\Omega \text{ cm}$ at 293 K.
13	Kemp, W.R.G., et al.	1966	L	1.9-151		60.33 39.67	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 880 C; residual electrical resistivity $16.10 \mu\Omega \text{ cm}$ ; electrical resistivity $21.1 \mu\Omega \text{ cm}$ at 293 K.
14	Kemp, W.R.G., et al.	1966	L	1.9-117		50.34 49.66	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 880 C; residual electrical resistivity $27.7 \mu\Omega \text{ cm}$ ; electrical resistivity $27.7 \mu\Omega \text{ cm}$ at 293 K.
15	Zakharov, G.F.	1966	L	445.2		50.34 49.66	$0.06 \text{ cm}^2$ in cross-section and 1.36 cm long.

TABLE 29. THERMAL CONDUCTIVITY OF SILVER - PALLADIUM ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION (continued)

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Ag	Pd	
16 111	Tainsh, R.J. and White, G.K.	1962	L	2.2-7.9		97.95	2.05	The specimen for curve no. 6 has been reannealed at 940 C in an effort to ensure that dislocation density is reduced to a minimum; rod specimen of about 6 cm long and 3 to 5 mm in diameter; electrical resistivity reported as 0.962, 1.372, and 2.612 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
17 111	Tainsh, R.J. and White, G.K.	1962	L	2.1-8.3		95.01	4.99	The specimen for curve no. 8 has been reannealed at 940 C in an effort to ensure that dislocation density is reduced to a minimum; rod specimen of about 6 cm long and 3 to 5 mm in diameter; electrical resistivity reported as 2.28, 2.66, and 3.87 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.
18 111	Tainsh, R.J. and White, G.K.	1962	L	2.3-7.9		90.22	9.78	The specimen for curve no. 9 has been reannealed at 940 C in an effort to ensure that dislocation density is reduced to a minimum; rod specimen of about 6 cm long and 3 to 5 mm in diameter; electrical resistivity reported as 4.37, 4.78, and 6.01 $\mu\Omega$ cm at 0, 90, and 293 K, respectively.

TABLE 30. THERMAL CONDUCTIVITY OF PALLADIUM - SILVER ALLOYS -- SPECIMEN CHARACTERIZATION AND MEASUREMENT INFORMATION

Cur. Ref. No.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent)		Composition (continued), Specifications, and Remarks
						Pd	Ag	
1 93	Schulze, F.A.	1911	E	298.2		90	10	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $4.71 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
2 93	Schulze, F.A.	1911	E	298.2		80	20	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $3.21 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
3 93	Schulze, F.A.	1911	E	298.2		70	30	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $2.56 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
4 93	Schulze, F.A.	1911	E	298.2		60	40	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $2.38 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
5 93	Schulze, F.A.	1911	E	298.2		50	50	1 mm thick wire specimen obtained from Heraeus Co.; electrical conductivity $3.09 \times 10^4 \Omega^{-1} \text{ cm}^{-1}$ at 25 C.
6 110	Kemp, W.R.G., Klemens, P.G., Sreedhar, A.K. and White, G.K.	1956	L	2.1-92		95	5	Rod specimen supplied by Johnson, Matthey and Co., Ltd.; annealed at 880 C; residual electrical resistivity $5.81 \mu\Omega \text{ cm}$ ; electrical resistivity $16.8 \mu\Omega \text{ cm}$ at 293 K.
7 110	Kemp, W.R.G., et al.	1956	L	2.2-152		70	30	Similar to the above specimen except residual electrical resistivity $35.6 \mu\Omega \text{ cm}$ and electrical resistivity $40.9 \mu\Omega \text{ cm}$ at 293 K.
8 110	Kemp, W.R.G., et al.	1956	L	1.6-117		50	50	Similar to the above specimen except residual electrical resistivity $27.7 \mu\Omega \text{ cm}$ and electrical resistivity $30.5 \mu\Omega \text{ cm}$ at 293 K.
9 112	Zolotarehin, G.E.	1956	L	486.7		75	25	Cylindrical specimen.
10 112	Zolotarehin, G.E.	1956	L	448.2		50	50	Cylindrical specimen.
11 84	Fletcher, R. and Greig, D.	1967	L	1.7-117			4.84	Calculated composition from atomic percent; specimen lost by International Nickel Ltd.; annealed at 700 C for 24 hrs previously; outgassed at 900 C for 4-5 hrs; residual electrical resistivity reported as $5.92 \mu\Omega$ original data obtained through private communication with author.
12 84	Fletcher, R. and Greig, D.	1967	L	4.3-118			9.85	Similar to the above specimen except the residual electrical resistivity reported as $12.18 \mu\Omega \text{ cm}$ .
13 84	Fletcher, R. and Greig, D.	1967	L	1.7-115			15.05	Similar to the above specimen except the residual electrical resistivity reported as $16.0 \mu\Omega \text{ cm}$ .
14 84	Fletcher, R. and Greig, D.	1967	L	2.1-116			20.53	Similar to the above specimen except the residual electrical resistivity reported as $24.5 \mu\Omega \text{ cm}$ .

## 5. CONCLUSIONS AND RECOMMENDATIONS

As evidenced by the available experimental thermal conductivity data presented in this work for the ten binary alloy systems selected as those most extensively investigated, it is clear that, still, for most of these alloy systems serious gaps exist for either the compositional or the temperature dependence or both and that most of the available data are widely divergent and subject to large uncertainty. The recommended self-consistent thermal conductivity values that cover the full ranges of composition and temperature are therefore very useful and valuable.

The recommended values are based upon both the critically evaluated, analyzed, and synthesized experimental data and the values calculated using the semitheoretical methods developed in this work.

It is thought that the reliability of the methods for the calculation of the thermal conductivity of binary alloys has been sufficiently tested with selected key sets of reliable data on alloys in the various binary alloy systems. The method for the calculation of the electronic thermal conductivity was found to be applicable to all types of binary alloys: nontransition, transition, solid solution, and mechanical mixture, whereas the method for the calculation of the lattice thermal conductivity was found to be applicable only to disordered solid-solution alloys; at present the lattice thermal conductivity of alloys in the mechanical-mixture region can be obtained only from experimental data.

For all but two of the binary alloy systems the recommended thermal conductivity values are given for 25 alloy compositions, which greatly facilitates interpolation for alloys with intermediate compositions. Furthermore, since the thermal conductivity of a binary alloy in many cases can be used as a first approximation to the thermal conductivity of a multiple alloy with the same major constituent elements and the same "effective" composition, the recommended thermal conductivity values for the binary alloy systems reported herein can lead the way for the study of the thermal conductivity of multiple alloys.

In the course of this study, a number of areas where further theoretical and experimental research is needed are identified. These areas of further research are recommended and listed below:

- (1) Experimental and theoretical work on band structure effects in binary alloys of transition elements and noble elements - in particular measurements on Cu + Pd and Pd + Cu alloys to determine the validity of large Lorenz ratios reported for this system.
- (2) Development of quantitative theory of impurity enhancement of phonon-electron interactions at low temperatures.

- (3) Measurements of alloy thermal conductivity down to liquid  $^3\text{He}$  temperatures to determine the extent to which residual dislocations cause the cusp-like behavior of the composition dependence of the low temperature lattice thermal conductivity.
- (4) Development of a theory of low-temperature lattice conduction in transition elements and high-residual-resistivity alloys.
- (5) Experimental and theoretical efforts on the lattice thermal conductivity outside the region of solid solubility.

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