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ELECTRICAL RESISTIVITY OF ALKALINE EARTH ELEMENTS

By

T. C. CHI

**CINDAS REPORT 42** 

December 1976

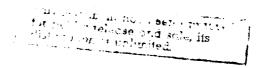
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#### PREFACE

This technical report was prepared by the Thermophysical and Electronic Properties Information Analysis Center (TEPIAC), a Department of Defense Information Analysis Center. This Center is operated by the Center for Information and Numerical Data Analysis and Synthesis (CINDAS), Purdue University, West Lafayette, Indiana, under Contract No. DSA900-76-C-0860 with the Defense Supply Agency (DSA), Alexandria, Virginia, with Mr. J. L. Blue being the Program Manager, and under the technical direction of the Army Materials and Mechanics Research Center (AMMRC), Watertown, Massachusetts, with Mr. Samuel Valencia being the Contracting Officer's Technical Representative.

This report reviews the recorded world knowledge on the electrical resistivity of alkaline earth elements in a most comprehensive and detailed form making it possible for all users of the subject to have access to the original data without having to duplicate the laborious and costly process of literature search and data extraction. It is quite appropriate at this point to mention that only original sources of data have been used for the critique of the data and that all cited documents are available at CINDAS. Also, for the active researchers in the field, a detailed discussion is presented for each material, reviewing the available information together with the considerations used by the author in arriving at the final recommended reference values.

It is hoped that this work will prove useful not only to the scientists in the field but also to other engineering research and development programs and for industrial applications, as it provides a wealth of knowledge heretofore unknown or inaccessible to many. In particular, it is felt that the critical evaluation, analysis and synthesis, and reference data generation constitute a unique aspect of this work.

While this work is prepared by the staff of TEPIAC/CINDAS's Reference Data Division, it would not have been possible without the direct input of TEPIAC/CINDAS' Scientific Documentation Division. Furthermore, valuable suggestions and guidance to this work have come from Dr. H. M. James and Dr. C. Y. Ho of CINDAS' senior staff.

West Lafayette, Indiana December 1976 Y. S. TOULOUKIAN
Director of CINDAS
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#### ABSTRACT

This technical report presents and discusses the available data and information on the electrical resistivity of alkaline earth elements (beryllium, magnesium, calcium, strontium, barium, and radium) and contains recommended or provisional reference values. The compiled data include all the experimental data available from the literature. The temperature range covered by the compiled data is from cryogenic temperatures to above the melting temperature of the elements. The recommended values are generated from critical evaluation, analysis, and synthesis of the available data and information and are given for both the total electrical resistivity and the intrinsic electrical resistivity. For most of the elements, the recommended values cover the temperature range from 1 K to 1000 K.

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## LIST OF SYMBOLS

- A Code for d.c. potentiometer method
- B Magnetic flux density: Code for d. c. bridge method
- C Code for a.c. potentiometer method; constant
- D Code for a.c. bridge method
- E Code for eddy current method
- G Code for galvanometer amplifier method
- I Code for induction method
- L<sub>F</sub> Latent heat
- M Atomic weight
- P Pressure; constant
- Q Code for Q-meter method
- R Resistance
- S<sub>1</sub> Constant
- S<sub>2</sub> Constant
- S<sub>3</sub> Constant
- T Temperature
- T<sub>m</sub> Melting point
- T<sub>c</sub> Critical temperature
- V Voltmeter and ammeter direct reading
- Electrical resistivity
- Pe Residual electrical resistivity
- ρi Intrinsic electrical resistivity
- Electrical resistivity parallel to the principal crystal-axis
- D Electrical resistivity perpendicular to the principal crystal-axis
- **On** Debye temperature
- AR Empirical temperature
- ' 'de for mi' ellaneous methods

#### 1. INTPODUCTION

The purpose of this work is to present and discuss the available data and information on the electrical resistivity of alkaline earth elements, to critically evaluate, analyze, and synthesize the data, and to make recommendations for the most probable values of the electrical resistivity over a wide temperature range. Of this group of elements experimental electrical resistivity data are available in the world literature for Be, Mg, Ca, Sr, and Ba and there is no resistivity data for Ra.

Table 1 contains information on the densities, crystal structures, phase transition temperatures, and certain other pertinent physical constants of the alkaline earth elements. This information is very useful in data analysis and synthesis. For example, the electrical resistivity of a material generally changes abruptly when the material undergoes any transformation. One must, therefore, be extremely cautious in attempting to extrapolate the electrical resistivity value across any transition temperature. No attempt has been made to critically evaluate the temperatures and constants given in Table 1, and they should not be considered as recommended values.

This work is organized in six sections. In the theoretical background section, some results of the theory of electrical resistivity are presented and briefly discussed. In the section on data evaluation and generation of recommended values, the general procedures and methods for data evaluation and for the generation of recommended values are outlined.

In the data presentation section, the electrical resistivity of each of the alkaline earth elements is presented separately in the order of increasing atomic number. Values of electrical resistivities are given for both the solid and liquid states. For an element at moderate and high temperatures the true electrical resistivity values for different highpurity (99.9+) samples at each temperature should be but little different; therefore, a set of recommended electrical resistivity values can be given for a high-purity element. At low temperatures, however, the electrical resistivity values for different samples with small differences in impurity and/or imperfection differ greatly, and a set of recommended values applies only to a sample with that particular amount of impurity and imperfection. Thus, the low-temperature electrical resistivity of an element could be presented as a family of curves, each of which would be recommended for a sample with a particular amount of impurity and degree of imperfection, and hence a particular residual resistivity,  $\rho_0$ . In this work, two well-defined curves are recommended for the full temperature range: one representing the intrinsic electrical resistivity,  $ho_i$ , which is a unique function of temperature and is zero at absolute zero, and the other representing the total resistivity,  $\rho$ , for the purest form of each element on which measurements have

Table 1. Physical constants of alkaline earth elements  $^{\mathbf{a}}$ 

Name	Atomic No.	Atomic b Weight k	Density <sup>c</sup> kg m <sup>-3</sup> x10 <sup>3</sup>	Crystal <sup>d</sup> T. Structure	Phase Debye Transition Temperature Temp., K at 0 K 293 K	Debye Temperatur at 0 K 293	e tture 293 K	Melting Point, K	Normal Boiling Point, K	Critical Temp., K
Beryllium (Be)	4	9.01218	1.85	c.p.h. (x)	1530 (α-β) 1160	1160	1031	1562	2749	6170
Magnesium (Mg)	12	24.305	1.74	c.p.h.		396±54	330	922	1364	3537
Calcium (Ca)	20	40.08	1.55	f.c.c. (α)	20±2 (α-β)	234±5	230	$1113\pm 2$	1759	3273
Strontium (Sr)	38	87.62	2.60	f. c. c. (2)	830 (x-y) 147±1	147±1	148	1042	1652	3064
Barium (Ba) Radium (Ra)	56 88	137.4 226.0254	က က	b.c.c. (2)		$110.5\pm 1.8$	116	$1002\pm 2$	2174 1900	3670

Information taken from Ref. [1].

Atomic weights based on <sup>12</sup>C = 12 as adopted by the International Union of Pure and Applied Chemistry in 1971. The number in parentheses is the mass number of the isotope of longest known half life.

Density values given for 293 K.

Structure below the melting temperature.

Deduced from specific heat measurements.

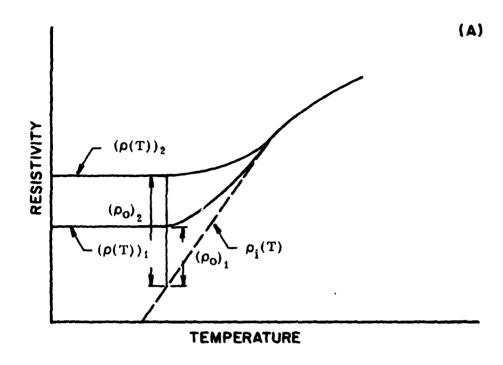
been made. The latter curve at low temperatures is only applicable to the particularly characterized specimen with residual electrical resistivity clearly specified. These two curves approach each other closely, on a logarithmic scale, for temperatures above about 100 K. Figure 1 shows the relationship between  $\rho_i$ ,  $\rho_0$ , and  $\rho$ .

The recommended or provisional electrical resistivities are tabulated with uniform but step-wise increasing increments in temperature as the temperature increases. The estimated accuracy of the recommended or provisional values for each element in each different temperature range is given in the discussion. The asterisked values in the tables are interpolated, extrapolated, or estimated in the temperature ranges where no experimental data are available.

From the recommended values of  $\rho$  and  $\rho_i$  which are tabulated in this work, the electrical resistivity of a particular sample at low temperatures can be estimated in either of the following two ways. One way is to find the difference between the measured resistivity value and the recommended  $\rho$  value at the same low temperature (i.e. below 100 K) and then add this difference to the recommended  $\rho$  values at other temperatures. The second way is to compare the measured low temperature value with  $\rho_i$ , get the difference which is the residual resistivity of this particular sample, and then add this  $\rho_0$  to the recommended  $\rho_i$  at the other temperatures.

In the figure showing experimental data, a data set that consists of a single point is denoted by a number enclosed by a square, and a curve that connects a set of data points is denoted by a ringed number. These numbers correspond to those in the data table and in the accompanying table on specimen characterization and measurement information. When several sets of data are too close together to be distinguishable, some of the data sets or data points, though listed in the table, are omitted from the figure for the sake of clarity. For all elements except francium, both logarithmic plotting and linear plotting of electrical resistivity are used in order that details may be clearly shown for both the low and high temperature regions. The recommended curves are presented in the same figure. The solid curve represents recommended values, and the dashed curves give provisional values. In the figure, the melting point (M.P.), normal boiling point (N. B. P.), and critical temperature (C. T.) of the elements are indicated. Some of these transition points are also mentioned in the text. At the melting point the resistivity exhibits large discontinuity.

The tables on specimen characterization and measurement information give for each set of data the following information: the publication reference number, author's name, year of publication, experimental method used for the measurement, temperature



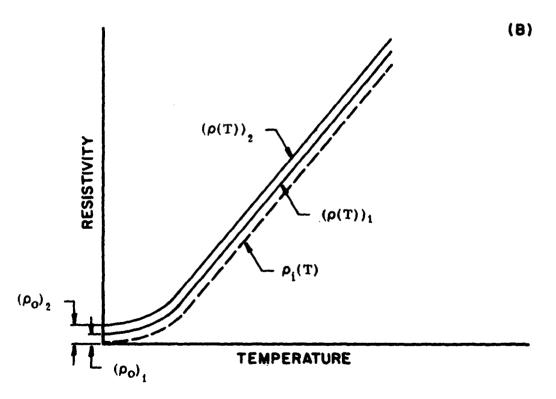


Figure 1. Relationship between intrinsic resistivity  $\rho_i(T)$ , residual resistivity,  $\rho_0$ , and total resistivity,  $\rho(T)$ . (A) logarithm scale, (B) linear scale.

range covered by the data, substance name and specimen designation, as well as the detailed description and characterization of the specimen and information on measurement conditions that are reported in the original paper. In these tables the code designations used for the experimental methods for electrical resistivity determination are as follows:

- A D.C. Potentiometer Method
- B D.C. Bridge Method
- C A.C. Potentiometer Method
- D A.C. Bridge Method
- E Eddy Current Method
- G Galvonometer Amplifier Method
- I Induction Method
- Q Q-Meter Method
- V Voltmeter and Ameter Direct Reading
- Other than above and described in the remarks

For a comprehensive yet concise review of all these methods, the reader is referred to the references given in Appendix 7.1.

In the Thirteenth General Conference on Weights and Measures held in October 1967 in Paris, the unit "ohm-meter" (symbol:  $\Omega$  m) was adopted as the SI unit for electrical resistivity. In this work, the SI units are used. Table 2 gives conversion factors which may be used to convert the electrical resistivity values in  $\Omega$  m presented in this work to values in any of the several other units listed.

In the summary and conclusions section, figures are presented in which all the recommended curves on the intrinsic electrical resistivity are grouped together in order to facilitate a visual comparison.

TABLE 2. CONVERSION FACTORS FOR UNITS OF ELECTRICAL RESISTIVITY\*

MULTIPLY by appropriate factor to OBTAIN-	аьд сш	mo On	O cm	stats cm	G El	O cir. mil ft-1	O in.	ii U
abohm-centimeter (emu)	1	0.001	10-	1.113×10 <sup>-21</sup>	10-11	6.015x10-3	6.015x10-3 3.937x10-10 3.281x10-11	3.281 x 10 <sup>-11</sup>
microohm- centimeter	1000	-	10-6	1.113×10 <sup>-18</sup>	10-8	6.015	3.937×10° 3.281×10°	3.281×10-6
ohm-centimeter	109	106	1	1.113×10 <sup>-12</sup>	0.01	6.015x10 <sup>6</sup>	0,3937	0.0328
statohm-centimeter (esu)	8.987 x 10 <sup>20</sup>	8.987 x 10 <sup>17</sup>	8.987 x 10 <sup>11</sup>	1	8.987 x 10 <sup>9</sup>	5.406 x 10 <sup>18</sup>	5.406x1018 3.538x1011 2.949x1010	2,949 x 10 <sup>10</sup>
ohm-meter	1011	108	100	1.113×10 <sup>-10</sup>	۲	$6.015 \times 10^{8}$	39.37	3.281
obm-circular mil	166.2	0,1662	1.662×10-7	1.662x10-7 1.850x10-19 1.662x10-9	1.662×10		6.54×104	5.45×10
ohm-inch	2.54×109	2.54×106	2.54	2.827 x 10 <sup>-12</sup>	0.0254	1.528×107	1	0.083
ohm-foot	3.048×10 <sup>10</sup>	3.048×107	30.48	3.3924 x 10 <sup>-11</sup>	0.3048	1.833×108	12	<b>,</b>

<sup>\*</sup>This table is based on the universal constants from "The International System of Units (SI)," National Bureau of Standards, NBS Special Publication 330, 43 pp, 1974.

## 2. THEORETICAL BACKGROUND

The electrical resistivity,  $\rho$ , of a metal is often described approximately by the Matthiessen rule [2]

$$\rho(\mathbf{T}) = \rho_0 + \rho_1(\mathbf{T}), \tag{1}$$

where  $\rho_0$  is the residual resistivity at absolute zero temperature and  $\rho_1$  is the intrinsic resistivity, which is the temperature-dependent resistivity of an ideally pure sample of the metal. The quantity  $\rho_0$  arises from the presence of impurities, defects, and strains in the metal lattice, while  $\rho_1$  is caused by the interaction of the conduction electrons with the thermally induced vibrations of the lattice ions; that is, the phonons in the crystal. For a pure annealed sample at room temperature,  $\rho_0$  is only a small fraction of the total resistivity. There are a number of mechanisms that could produce a deviation from the Matthiessen rule, resulting in a term  $\Delta \rho$  appearing on the right-hand side of equation (1). The first comprehensive survey of such deviations was made by J. Bass [3]. A more recent study by Cimberle et al. [4] brings references up to date.

The intrinsic resistivity due to electron-phonon interactions may be approximated by the Bloch-Grüneisen-relation [5]

$$\rho_{i}(T) = \frac{C}{M \theta_{R}} \left(\frac{T}{\theta_{R}}\right)^{5} \int_{0}^{\theta_{R}} \frac{z^{5} dz}{(e^{z} - 1) (1 - e^{-z})}, \qquad (2)$$

where C is a constant, M is the atomic weight, T is the absolute temperature, and  $\theta_R$  is an empirical temperature characterizing the metal's ideal electrical resistivity in the same way that the Debye temperature,  $\theta_D$ , characterizes a solid's lattice specific heat. It is often true that  $\theta_R \approx \theta_D$ . Below about 0.1  $\theta_R$  this relation reduces to

$$\rho_{\rm i}({\rm T}) \approx 124.4 \frac{\rm C}{\rm M} \frac{{\rm T}^5}{\theta_{\rm R}^6} \tag{3}$$

At high temperatures, as  $T \ge \theta_R$ ,

$$\rho_{\rm i}({\rm T}) \approx \frac{{\rm C}}{4{\rm M}} \frac{{\rm T}}{\theta_{\rm R}^2} .$$
(4)

The Grüneisen-Bloch equation is derivable only for idealized monovalent metals with Debye phonon spectra and spherical Fermi surfaces, totally neglecting the effect of Umklapp processes. However, because of its comparative simplicitity, this equation is still a most valuable tool for analyzing and discussing experimental data.

The Grüneisen-Bloch equation never holds over the entire temperature range for

the alkaline earth metals. By inverting the computation, one may intercompare the behavior of different metals by interpreting the experimental results in terms of deviations from the Gruneisen-Bloch equation. This is often done by employing  $\theta_R$  as a variable parameter and computing the value that it must possess at any temperature in order that the Gruneisen-Bloch equation may agree with the experiment at that temperature.

In all alkaline earth metals the electrical resistivity increases abruptly at the melting point and shows weakly negative temperature dependence in the liquid phase. The sudden change is due to the greater disorder of the liquid state and the disappearance of any definite crystal structure.

Mott [6] has presented a simple and fairly successful theory of liquid metals. He ignored the disordered positions and diffusive movements of the vibrating ions and assumed that near the melting point the ions of the liquid metal still maintain a more or less regular pattern. With an Einstein model of single frequency oscillators he obtained

$$\left(\frac{\rho_{L}}{\rho_{S}}\right) = \exp\left(\frac{80 L_{F}}{T_{m}}\right), \tag{5}$$

where  $ho_L$  and  $ho_S$  are the electrical resistivities of the liquid and solid phases,  $T_m$  is the melting point, and  $L_F$  is the latent heat of fusion in kilojoules per mole. The calculated values of  $(
ho_L/
ho_S)_{T_m}$  according to this formula compare moderately well with experimental data for alkaline earth metals.

A single crystal of a metal with a cubic crystal structure has an isotropic resistivity, and the resistivity of the polycrystalline material is the same, apart from a small extra contribution in a polycrystal that may sometimes be caused by grain boundaries. But in a single crystal of noncubic metal, the resistivity is often very anisotropic, its value depening on the direction of the flow current. Likewise, polycrystalline specimens of such metals, if preferentially oriented, as by rolling or drawing, will have direction-dependent resistive properties.

In isotropic metals with the close-packed bexagonal and rhombohedral (trigonal) structures, the electrical resistivity parallel to the principal crystalline axis is designated as  $\rho_{\parallel}$  and electrical resistivity perpendicular to the principal axis is designated as  $\rho_{\perp}$ . When values for  $\rho_{\parallel}$  and  $\rho_{\perp}$  have been determined for a single crystal, one may calculate a value of  $\rho$  for a polycrystalline sample without preferential orientation by using the equation of Voigt [7]:

$$\rho = \frac{3\rho_{//}\rho_{\perp}}{2\rho_{//} + \rho_{\perp}} \tag{6}$$

Equation (6) has been used fairly commonly for the determination of  $\rho$  of a polycrystalline specimen from single crystal axial resistivities, and it usually gives satisfactory agreement with direct observation on polycrystals. However, Nichols [8] has found the relation

$$\rho = \frac{1}{3} \left( \rho_{/\!/} + 2\rho_{\perp} \right) \tag{7}$$

to be more suitable for metals with large anisotropy ratio, and to be perfect in the case of c.p.h. Mg.

#### 3. DATA EVALUATION AND GENERATION OF RECOMMENDED VALUES

The data analysis and synthesis employed in this work whenever possible included critical evaluation of available data and related information, reconciliation of disagreements in conflicting data, correlation of data in terms of various parameters, and curve fitting with theoretical or empirical equations. Besides critical evaluation and analysis of the existing data, semiempirical techniques have been employed to fill gaps in data and to extrapolate existing data so that the resulting recommended values are internally consistent and cover as wide a range of temperature as possible.

In the critical evaluation of the validity of electrical resistivity data, any unusual dependence or anomaly was carefully investigated, the experimental technique was reviewed to see whether the actual boundary conditions in the experiment agreed with those assumed in the theory, and the author's estimations of uncertainty were checked to ensure that all the possible sources of errors were considered. The sources of errors may have included uncertainty in the measurement of specimen dimensions and of the distance between the potential probes, uncertainty due to the effects of thermal expansion, uncertainty in temperature measurements, uncertainty in the sensitivity of measuring circuits, and so on.

Many authors have included detailed error estimates in their published papers, and from these it is possible to evaluate the uncertainty for a particular method. However, experience has shown that the uncertainty estimates of most authors are unreliable. In many cases the difference between the results of two sets of data is much larger than the sum of their stated uncertainties.

Besides evaluating and analyzing individual data sets, correlating data in terms of various relevant parameters was a valuable technique and frequently used in data analysis. These parameters may include purity, density, residual electrical resistivity and so on.

For a meaningful data correlation, information on specimen characterization is very important. A full description of the specimen should include, wherever applicable, the following: purity or chemical composition, type of crystal, crystal axis orientation for a single crystal, microstructure, grain size, preferred grain orientation, inhomogeneity or additional phases for a polycrystalline specimen, specimen shape and dimensions, method and procedure of fabrication, sample history or treatment, test environment, and pertinent physical properties such as density, hardness, and transition temperature. Data on poorly characterized materials can hardly be analyzed or used for data correlation.

Besides specimen characterization, a full description of experimental details should be given by the author in order that his data can be meaningfully evaluated and fully utilized. Sometimes, as an initial method of evaluating the quality of a paper, consideration might be given to the amount of experimental detail reported in the paper; lack of experimental detail might lead to the results being given less weight.

Our preliminary recommended values for the electrical resistivity of the alkaline earth elements were derived from experimental data that were considered reliable, using computer least-mean-square error fit to a modified Bloch-Grüneisen formula of the form

$$\rho_{i}(T) = [S_{1} + S_{2} \times (T/\theta_{R}) + S_{3} \times (\theta_{R}/T)^{P}] \Phi(\theta_{R}/T)$$
(8)

where  $S_1$ ,  $S_2$  and  $S_3$  are the coefficients,

$$\theta_{\mathbf{R}} = (\theta_{\mathbf{R}})_0 - \mathbf{CT} , \qquad (9)$$

$$\Phi(\theta_{R}/T) = 4(T/\theta_{R})^{5} \int_{0}^{\theta_{R}/T} \frac{z^{5} dz}{(e^{z}-1)(1-e^{-z})}, \qquad (10)$$

 $(\theta_R)_0$ , C, P,  $S_1$ ,  $S_2$  and  $S_3$  are used as the variable parameters.

The first term represents the basic Bloch-Grüneisen form; the second term was added in order to get better fit to high temperature data and the third term can represent a dominating low power law at very low temperatures. The computer provides a best fit to a fixed number of specified data points  $(T_n, \rho_n)$  minimizing the sum Q of the squares of the <u>fractional</u> errors with which  $\rho_n$  are represented by the fitting function  $\rho = f(T)$ . If desired, variable weights are assigned to the data points, minimizing

$$Q = \sum_{n} W_{n} [(f(T_{n}) - \rho_{n})/\rho_{n}]^{2}$$
(11)

The suitability of the form of eq. (8) has been tested by fitting it to previously smoothed data for a number of metals. The r.m.s. fractional errors in these fits were as follows:

Li	(80-450 K),	.0024
Na	(50-350 K),	.012
K	(40-300 K),	.0044
Rb	(30-273 K),	.012
Cs	(30-273 K),	.009
Cu	(60-1200 K),	. 005
Ag	(40-1200 K),	.004
Au	(40-1200 K),	.0044
Mg	(60-900 K),	.007

Ca	(40-306 K),	. 0056
Zn	(60-600 K),	. 006
Al	(60-900 K),	. 0033
Ni	(60-600 K),	. 015
Fe	(80-1000 K),	. 0095
Pd	(80-1300 K).	. 003

In some cases errors in the smoothing contributed to these fractional errors.

The final recommended values are obtained by extrapolating the resulting values from curve fitting values to somewhat lower and higher temperatures and correcting them for thermal linear expansion.

In estimating the uncertainty of our recommended values, the accuracy that can be achieved by the various experimental techniques, the scatter of data, and the purity of the materials, among other factors, were taken into consideration. The ranges of uncertainties of recommended and provisional values are less than or equal to  $\pm 5\%$  and greater than  $\pm 5\%$ , respectively.

#### 4. ELECTRICAL RESISTIVITY OF ALKALINE EARTH ELEMENTS

## 4.1. Beryllium

Beryllium, with atomic number 4, is a steel-gray, very hard metal, similar to magnesium in appearance and in chemical properties. It has a close-packed hexagonal crystalline structure with a density of 1.85 g cm<sup>-3</sup> at 293 K. It has been reported that the crystal transforms to a body-centered cubic form at 1530 K, only 32 degrees below the melting point of 1562 K. The normal boiling point is about 2749 K. Its critical temperature has been estimated to be about 6170 K. Beryllium has only one stable isotope, <sup>9</sup>Be, but four other radioactive isotopes are known. Beryllium ranks 46th in the order of abundance of elements in the continental crust of the earth (0.00028% by weight).

## Temperature Dependence

There are 80 sets of experimental data available for the electrical resistivity of beryllium. The information on specimen characterization and measurement conditions for each of the data sets is given in Table 4. The data are tabulated in Table 5 and shown in Figures 2 and 3. Determinations of the electrical resistivity for the solid phase cover continuously the temperature range from 1.35 to 1454 K.

Since beryllium is an anisotropic metal, resistivity values will vary according to the relation of the direction of the resistivity measurements to the hexagonal axis of the crystal. Grüneisen and Adenstedt [9] (curves 16 and 17), Grüneisen and Erfling [10,11] (curves 12-14, 48-50), Martin, Bunel and Tilbury [12] (curves 59 and 60) and Mitchell [13] (curves 51 and 52) are the investigators who have made measurements on single crystals. However, their results are inconsistent and a need clearly exists for further det rmination to be made.

Falge [14] has found that bulk beryllium becomes superconducting when cooled below 0.026 K. Yoshihivo and Glover [15] have measured the resistivity of thin film crystalline beryllium on a quartz substrate (curve 53) and found a superconducting transition temperature at about 9.3 K. Williams, Hinkle and Eatherly [16] investigated the neutron irradiation effects on the electrical resistivity of polycrystalline beryllium samples from 72 to 400 K (curves 34-43).

Most earlier determinations of the electrical resistivity of polycrystalline beryllium resulted in higher resistivities than the later ones. These results can be explained by the lower purity of the specimens and by the omission of a heat treatment, which appears to

be essential. Powell [17] (curves 18-33) demonstrated the important effect that annealing at 973 K has on the resistivity; for his best polycrystalline specimen,  $\rho_{00}$  was lowered from 6.7 to 3.2 x 10<sup>-6</sup>  $\Omega$  m by such treatment. The resistivity values obtained by Losana [18] (curves 9-11) form an anomalous group from which it would seem that the samples have much lower purity than was claimed.

From the examination of the data available for the electrical resistivity, it is evident that there are deviations from the Matthiessen's Rule. The lowest values of  $\rho$  for polycrystalline beryllium were reported by Berteaux [19] (curve 44). From his graph, we obtained  $Q_{200} = 3.0 \times 10^{-8} \Omega$  m. However, this value is lower than those for all single crystal samples with perpendicular orientation, and the reported residual resistance ratio  $R_{300}/R_{4.2} = 49$  is inconsistent with that shown in his graph, which gives  $\rho_{300}/\rho_{4.2} = 200$ . Therefore, his data were not considered in the generation of recommended values. Reich, Quang, Kinch, and Boumain [20] (curve 3) and Powell [17] (curve 23) have the next lowest electrical resistivity values for polycrystalline samples, and they are in fair agreement. Comparison of their data with the single crystal data indicates that these samples had highly preferred perpendicular orientation, as is known for the sample of Reich et al. (Although Powell has annealed his sample at 973 K, this temperature was too low for sample recrystallization). The above data and the low-temperature single-crystal data of Grüneisen were used to generate provisional values for the single crystal measured perpendicular to the c-axis. A least mean-square-error fit to the selected values of  $\rho - \rho_0$  was made with a modified Bloch-Grüneisen equation (8), from 20 to 873 K. The following values were found for the coefficients in equation (8):

 $S_1$   $S_2$   $S_3$   $(\theta_R)_0$  C P  $25.945 \cdot 10^{-8} \Omega m$   $-1.996 \cdot 10^{-8} \Omega m$   $0.3377 \cdot 10^{-8} \Omega m$  1327.9 K 0.373 1.90

The resulting values calculated from eq. (8) were extrapolated to lower and higher temperatures, corrected for thermal linear expansion, and the final provisional values were obtained.

Assuming that the anisotropy ratio of the resistivity can be used for the pure element and using the results of Grüneisen and Erfling [10] and of Mitchell [13] and the provisional values of electrical resistivity for single crystals measured perpendicular to the c-axis, the resistivity values for single crystals measured parallel to the c-axis were obtained. These values and the data of Grüneisen et al. were then fitted by the modified Bloch-Grüneisen equation (8) and the following results were obtained:

S<sub>1</sub> S<sub>2</sub> S<sub>3</sub>  $(\theta_R)_0$  C P 32.258·10<sup>-8</sup>Ωm 11.776·10<sup>-8</sup>Ωm 0.1815·10<sup>-8</sup>Ωm 1196.1 K .02085 1.90

By using equation (7) and the above single-crystal results, resistivity values for the polycrystalline specimen were calculated from 10 to 1200 K. Above 1200 K, our provisional values follow the trend of the experimental data of Tye [217] (curves 63-68) and of Ho and Wright [22] (curves 73-80). These values were then fitted by the modified Bloch-Grüneisen equation (8) with the following constants:

 $S_1$   $S_2$   $S_3$   $(\theta_R)_0$  C P 28.117·10<sup>-8</sup>Ωm 2.0718·10<sup>-8</sup>Ωm 0.2676·10<sup>-8</sup>Ωm 1267.28 K 0.2253 1.90

No data are available for the electrical resistivity of beryllium above the phase transition temperature (1530 K) or in the liquid state.

The provisional values for the total and intrinsic electrical resistivities are listed in Table 3, and those for the total resistivity are also shown in Figures 2 and 3. The provisional values are corrected for the thermal linear expansion. The correction amounts to -0.15% at 1 K, -0.1% at 200 K, 0.3% at 500 K, 1.3% at 1000 K and 2.4% at 1500 K. The provisional values for the total electrical resistivity are for 99.9+% beryllium and those below 100 K are applicable to specimens with residual resistivities of  $0.00718 \times 10^{-8} \Omega$  m ( $\perp$  to c-axis),  $0.00426 \times 10^{-8} \Omega$  m ( $\parallel$  to c-axis), and  $0.0332 \times 10^{-8} \Omega$  m (Polycrystalline). The uncertainty of the provisional values for the total electrical resistivity is believed to be within  $\pm 8\%$  below 1000 K and within  $\pm 10\%$  from 1000 K to 1500 K. Above 40 K, the uncertainty of the provisional values for the intrinsic resistivity is a little higher than that of the total electrical resistivity because of possible deviations from the Matthiessen's Rule; below 40 K the uncertainty can be very large and values are not listed in the table.

TABLE 3. PROVISIONAL ELECTRICAL RESISTIVITY OF BERYLLIUM (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8}\Omega m$ ; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8}\Omega m$ ]

			Solid	····	··	
r	⊥ t	o c-axis	// to	c-axis	Polyc	rystalline
•	P	$ ho_{ ext{i}}$ †	ρ	Pit	ρ	Pi t
1	0.0072		0.0043		0.0336	
4	0.0072		0.0043		0.0332	
7	0.0072		0.0043		0.0332	
10	0.0072		0.0043		0.0332	
15	0.0073		0.0044		0.0334	
20	0.0076		0.0046		0.0336	
25	0.0080		0.0049		0.0339	
30	0.0086		0.0054		0.0345	
35	0.0096		0.0062		0.0354	
40	0.0109	0.0037	0.0074	0.0031	0.0367	0.0035
45	0.0127	0.0055	0.0090	0.0047	0.0384	0.0052
50	0.0150	0.0078	0.0112	0.0069	0.0407	0.0078
60	0.0218	0.0146	0.0180	0.0137	0.0675	0.0143
70	0.0325	0.0253	0.0293	0.0250	0.0584	0.0252
80	0.0483	0.0411	0.0471	0.0428	0.0748	0.0416
90	0.0711	0.0639	0.0736	0.0693	0.0989	0.0657
100	0.103	0.0954	0.111	0.107	0.133	0.0993
110	0.1 <del>44</del>	0.137	0.163	0.159	0.178	0.145
120	0.199	0.192	0.232	0.228	0.237	0.204
130	0.266	0.259	0.318	0.314	0.311	0.278
140	0.349	0.342	0.424	0.420	0.401	0.368
150	0. <b>44</b> 7	0.440	0.550	0.546	0.510	0.477
175	0.758	0.751	0. 95 <b>6</b>	0.952	0.851	0.818
200	1.16	1.15	1.48	1.48	1.29	1.26
225	1.64	1.63	2.11	2.11	1.82	1.79
250	2.18	2.17	2.82	2.82	2.42	2.39
	15 2.72	2.71	3.54	3. <b>54</b>	3.02	2.99
293	3.21	3.20	4.19	4.19	3.56	3.53
300	3.38	3.38	4.43	4.43	3.76	3.73
350	4.70	4.69	6.20	6.20	5.22	5.19
100	6.08	6.07	8.07	8.07	6.76	6.73
<b>450</b>	7.48	7.47	9.99	9. 99	8.33	8,30
500	8.91	8.90	12.0	12.0	9.94	9.91
550	10.3	10.3	14.0	14.0	11.5	11.5
300	11.8	11.8	16.0	16.0	13.2	13.2

 $<sup>\</sup>dagger$  At temperatures below 40 K, the uncertainty of  $\rho_i$  is so large that values are not listed.

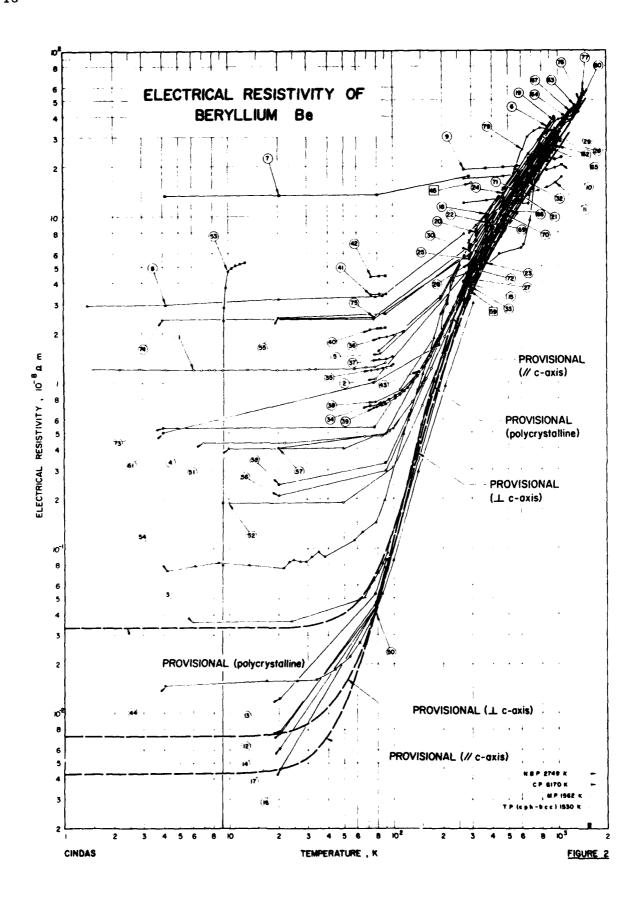
The provisional values for the total electrical resistivity are for 99.9+% beryllium and those below 100 K are applicable to specimens with residual resistivities of 0.00718 x  $10^{-8}\Omega$  m ( $\perp$  to c-axis), 0.00426 x  $10^{-8}\Omega$  m (//to c-axis), and 0.0332 x  $10^{-8}\Omega$  m (Polycrystalline).

TABLE 3. PROVISIONAL ELECTRICAL RESISTIVITY OF BERYLLIUM (Continued) (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8} \Omega m$ ; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8} \Omega m$ ]

			Solid			
Т	⊥ to	c-axis	// to	c-axis	Polycr	ystalline
1	ρ	ρi	ρ	$ ho_{ m i}$	ρ	ρi
650	13.3	13.3	18.1	18.1	14.8	14.8
700	14.8	14.8	20.2	20.2	16.5	16.5
750	16.3	16.3	22.3	22.3	18.3	18.3
800	17.9	17.9	24.5	24.5	20.0	20.0
850	19.5	19.5	26.7	26.7	21.8	21.8
900	21.1	21.1	28.9	28.9	23.7	23.7
950	22.7	22.7	31.2	31.2	25.6	25.6
1000	24.4	24.4	33.5	33.5	27.5	27.5
1100	27.8	27.8	38.3	38.3	31.5	31.5
1200	31.5	31.5	43.3	43.3	35.7	35.7
1300					40.1	40.1
1400					44.8	44.8
1500					49.9	49.9

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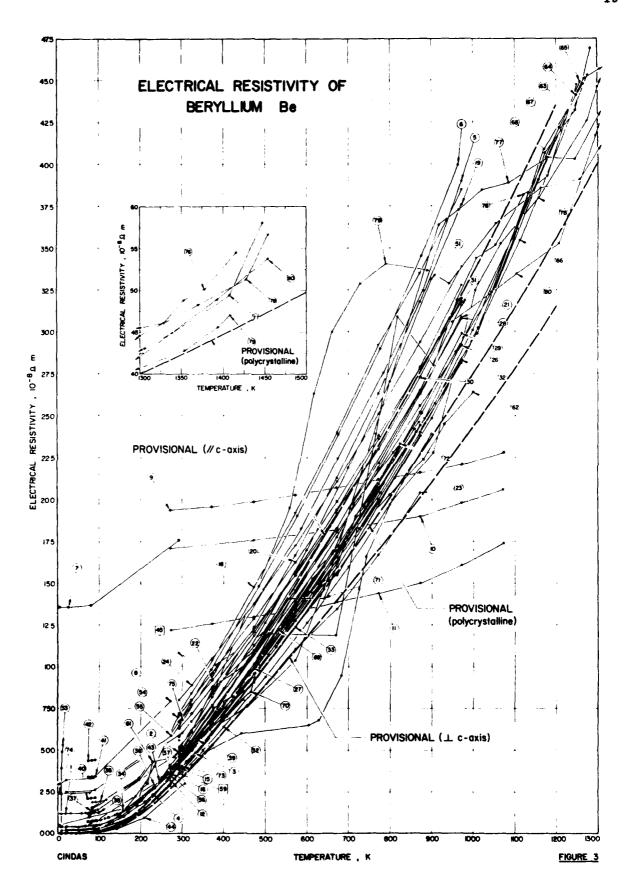


TABLE 4. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperante Dependence)

So.	, Se F.	Author (s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
<u> </u>	23	White, G.K. and Woods, S.B.	1955	<	2-295	<b>Be</b> 2	High purity; <0.1 Mg, trace of Fe; specimen was obtained from A.D. Mackay; sintered rod specimen, 4 mm in diameter; the connections to rods were made with inclum solder.
cı	7.	Spangler, G. E., Herman, M., Arrit, E. J., Hoover, D. B., Damiano, V. V., Tint, G. S., and Lee, C. H.	1962	E, A	77,293	å.	Commercial purity; cylindrical rod specimen 0,635 cm (1/4 ln.) in diameter and 10 to 15 cm (4 to 6 in.) long.
m	20	Reich, R., Kinh, V.Q., and Bonmarin, J.	1963		4.2-400	H1209	Pure; 0.2 BeO, 0.0085 Fe, <0.003 Al, <0.001 each Ni, Cr, 0.0015 Si, and <0.0005 Mn; cast by induction; grain size 30-200 \(\mu\); specimen was annexied at 800 C for 150 hr.
•	20	Reich, R., & al.	1963		4.2-400	H978	Pure; 0.1 BeO, 0.126 Fe, 0.6045 Al, 0.609 Ni, 0.602 Si, < 0.601 Cr, and 0.0007 Aln; specimen was cast by induction; grain size 30-200 µ; specimen was anotaled at 800 C for 150 hr.
NO.	22	Lewis, E.J.	1929		84-973	Be 1	Commercially pure; 99, 5 Be, trace of Al, Cr, Fe, Mn, Si, and <0.5 Mg; specimen was obtained from the Beryllium Co. of America; specimen cross section was 0.792 cm² and 22.5 cm long.
œ	52	Lewis, E.J.	1929		84-973	Be 2	Similar to the above specimen; sample cross section was 6. Sc5 cm² and length was 18 cm.
7	56	McLeman, J.C. and Niven, C.D.	1927	m	4.2-293	æ	Pure; specimen was obtained from Beryillum Corp. of America.
•	2	Messiner, W. and Voigt, B.	1930		1.35-273.16	e <b>2</b>	0.5 Fe; specimen was prepared by melting; red specimen dimension 1.5 x 1.5 x 8 mm; electrical resistivity data were calculated from the resistance ratio, resistance at 273.16 K, specimen cross section, and potential probes distance; no thermal expansion correction.
o	8	Losana, L.	1939		273-1073	Be 5	99.58 pure, 0.21 Al, 0.152 Fe, 0.0121 Cu, trace of Ca, C, Ni specimen was refined in beryllia crucibles under Ar atm.
91	18	Losana, L.	1939		273-1073	Be 6	99.781 pure, 0.17 Al, 0.042 Fe, and 0.011 Cu; specimen was refined in beryllia crucibles under Ar aim.
=	18	Losana, L.	1939		273-1073	Be 9	99.962 pure, trace of Zn. Fe; specimen was refined in beryllia crucibles under Ar atm; density 1.816 g cm <sup>-3</sup> at 291 K.
12	10	Grüneisen, E. and Erfling, H.D.	1940	≺	20.36-273	Be 13	Pure; single crystal specimen with length perpendicular to hexagonal axis: $\angle (J,X) \approx 12^{\circ}$ , where $\angle (J,X)$ is the angle between the current and secondary axis.
53	07	Gribeisen, E. and Erfling, H.D.	1940	∢	20.37-273	Be 14	Pure; single crystal specimen with length perpendicular to hexagonal axis; $\angle (J_i X) = 2^\circ$ .
<b>.</b>	2	Grimeisen, E. and Eriling, H.D.	1940	< <	20. 34-273	Be L B	Pure; single crystal specimen with length perpendicular to bexagonal axis; $\angle (J, X) = 30^\circ$ ,
<b>21</b>		Campbell, J.E., Goodwin, H.B., Wagner, H.J., Douglas, R.W., and Allen, B.C.	1961		293.15	<b>a</b>	Pure; melting point = 1550.8 K, density = 1.856 g cm <sup>-3</sup> .
91	•	Grünelsen, E. and Adenatodt, H.	1938	∢	20.33-273	Be 2	Pure; single crystal specimen with length parallel to bezagonal axis; specimen 1 mm in diameter and 1.55 cm in length; density 1.54 g cm - Reported error 1.55.
11	o	Grimeisen, E. and Adenstedt, H.	1938	<	20.32-273	Be 1	Similar to the above specimen; length 1 cm. Reported error 1.5%.

TABLE 4. MEASTREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperame Dependence (continued)

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No. N	itef. No.	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
18 17	Powell, R. W.	1953		293-973	Be No. B.7 (D) (i)	96. 5 Be, 1.81 Mg, 1.52 F, 0.55 Fe, 0.06 Al, 0.035 Ca, 0.005 Cu, 0.005 Mn, and 0.032 C: bar 0.5 cm square section, 13.1 cm long machined from a chilled cast bar prepared from the Brush Beryllium's crude reactor products density 1.826.
19 17	Powell, R.W.	1953		293-973	Be No. B.7 (D) (i)	The above specimen; heat treated at 973 K.
20 17	r Powell, R. W.	1953		293-973	Be No. B. 26 (1) (11)	Bar 2.25 cm diameter and 7.7 cm long was machined from a chilled cast bar prepared from the Brush Beryllium Company's crude reactor products; density 1.642.
21 17	Powell, R.W.	1953		293-973	Be No. B.26 (1) (ii)	The above specimen; heat treated at 973 K.
22 17	Powell, R.W.	1953		293-873	Be No. B. 26 (2) A (iii)	Bar 0.865 cm diameter and 1.884 cm long; this had come from the same casting as No. B. 26(1) but after an attempt had been made to extrude the metal at 1000 C; subsequently the metal had been heated in vacuum for I hr and furnace cooled.
23 17	Powell, R.W.	1953		293-873	Be No. B. 26 (2) A (iii)	The above specimen; heat truated at 973 K.
24 17	Powell, R. W.	1953		293-973	Be No. B.28 (2) (iv)	98. 5 Be, 0.13 Al, 0.18 Fe, 0.03 Cu, 0.05 Cl. Be insoluble in HCl 0.18; bar 2.23 cm diameter and 11.1 cm long was machined from a chilled cast bar prepared from German flake beryllium; density 1.523 g cm <sup>-2</sup> .
25 17	Powell, R. W.	1953		293-973	Be No. B. 28 (2) (iv)	The above specimen; heat treated at 973 K.
26 17	Powell, R. W.	1953		293-973	Be No. B47B (v)	Bar 2. 287 cm diameter and 15.72 cm long was machined from a chilled cast bar prepared from the Brush Beryllium Company's crude reactor product.
71 17	Powell, B. W.	1953		293-973	Be No. B47B (v)	The above specimen; heat treated at 973 K.
28 17	Powell, R.W.	1953		293-973	Be No. 2(b) (vi)	Bar 1.0 cm square section, 6.6 cm long; this was a block of beryllium by the "sintering" process by the American G. E. C.; density 1.83 g cm - 1.
23 17	Powell, R.W.	1953		293-973	Be No. 2(b) (vi)	The above specimen; heat treated at 973 K.
30 17	Powell, R.W.	1953		293-973	Be (vii)	Slice approximately 0.33 cm thick, 0.62 cm wide, and 5 cm long; density 1.85 g cm "
31 17	Powell, R.W.	1953		293-973	Be (vii)	The above specimen; heat treated at 973 K.
32 17	Powell, R. W.	1953		293-973	Be (xi)	Bar 1 in. in diameter and 6 in. long; density 1. 865 g cm-1, Mg and C main impurities, 0.34 Mg.
33 17	Powell, R.W.	1953		293-973	Be (xd)	The above specimen; heat treated at 973 K.
<b>2</b> 2. 16	Williams, J.M., Hinkle, N.E., and Eatherly, W.P.	1972	<	72.5-402.5	K38-1	Pure; specimen axis was parallel to the pressing condition. Reported error ?.
35 16	Williams, J.M., et al.	1972	< <	73.75-100.41 K38-1	K38-1	The above specimen; sample was irradiated by 7.41 x $10^{17}$ neutrons/cm <sup>2</sup> with $E > 1.0$ MeV. Reported error 2%.

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TABLE 4. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperature Dependence) (continued)

36         18 williams, J.M., Hiadle, N.E., 1972         A 82.78-91.77 Months appearing a speciment sample was irradiated by 1. In sufficiently, W.P., 1. In sufficiently, M.P., 1. In s	Cur. No.	. S	Author(s)	Year	Method	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
16 Williams, J.M., et al.  1972 A 82.32-117.74 K38-1  16 Williams, J.M., et al.  1972 A 76.35-370.16 K37-1  16 Williams, J.M., et al.  1972 A 73.5-370.16 K37-1  16 Williams, J.M., et al.  1972 A 73.5-370.16 K37-1  16 Williams, J.M., et al.  1972 A 73.5-30.16 K37-1  16 Williams, J.M., et al.  1972 A 73.5-30.16 K37-1  19 Berteaux, F.  1972 A 73.7-32-90 K37-1  19 Berteaux, F.  1972 A 73.7-32-90 K37-1  19 Berteaux, F.  1972 A 73.7-32-90 K37-1  10 Babkina, M.A., Zhermunskaya, 1972 A 71.28-329.76 K37-1  10 Babkina, M.A., zhermunskaya, 1972 A 71.28-329.76 K37-1  11 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be// 6  11 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be// 6  13 Mitchell, M.A.  1975 A 10-900  15 Yoshkhiro, K. and Grüneisen, E. 1975 A 10-900  15 Yoshkhiro, K. and Grüneisen, E. 1975 A 10-900  17 Zakasaki, Y., and Ohla, T.  1974 A 9.0-13	98	16	Williams, J.M., Hinkle, N.E., and Entherly, W.P.	1972	¥	82.78-59.57	K38-1	The above specimen; sample was irradiated by 1.02 x 10° neutrons/cm² with $E > 1.0~{\rm MeV}$ . Roported error 2%.
16 Williams, J.M., et al. 1972 A 88.25-294.75 K38-1 16 Williams, J.M., et al. 1972 A 76.55-370.16 K37-1 16 Williams, J.M., et al. 1972 A 73.35-90 K37-1 16 Williams, J.M., et al. 1972 A 73.35-90 K37-1 16 Williams, J.M., et al. 1972 A 73.492.66 K37-1 19 Berteaux, F. 1970 A 73.293.76 K37-1 19 Berteaux, F. 1970 A 73.293.76 29 Bridgman, P.W. 1927 A 73.293.76 20 Babkina, M.A., Zbermunakaya, 1972 A 73.293.76 20 Babkina, M.A., et al. 1972 A 73.293.76 21 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be_/2 22 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 23 Babkina, M.A., et al. 1972 A 79-273.15 Be_/2 24 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 25 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 26 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 27 A 79-273.15 Be_/2 28 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 29 Bridgman, M.A., et al. 1972 A 79-273.15 Be_/2 20 Babkina, M.A., et al. 1972 A 79-273.15 Be_/2 20 Babkina, M.A., et al. 1972 A 79-273.15 Be_/2 21 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be_/6 21 Xoshibiro, K. and Grüneisen, E. 1975 A 10-900 21 Xamaguchi, M.A. Takahashi, Y., 1974 B0-300 21 Takasaki, Y., and Othia, T.	33	18	Williams, J. M., et al.	1972	₹	82.52-117.74	K38-1	The above specimen; sample was irradiated by 2.15 x 10% neutrons/cm² with $E > 1.0 \text{ MeV}$ . Reported error $2\%$ .
16 Williams, J.M., et al. 1972 A 76.55-370.16 K37-1 16 Williams, J.M., et al. 1972 A 73.35-90 K37-1 16 Williams, J.M., et al. 1972 A 73.35-90 K37-1 16 Williams, J.M., et al. 1972 A 73.74-92.66 K37-1 16 Williams, J.M., et al. 1972 A 73.74-92.66 K37-1 19 Berteaux, F. 1970 A 71.28-329.76 K37-1 19 Berteaux, F. 1970 A 71.28-329.76 K37-1 19 Berteaux, F. 1970 A 71.28-329.76 K37-1 19 Bertina, M.A., Zhermunakaya, 1972 A 71.28-329.76 K37-1 10 Babkina, M.A., Zhermunakaya, 1972 A 71.28-329.78 Be./2 11 Erfling, H.D. and Grüneisen, E. 1942 A 71-273.15 Be./2 11 Erfling, H.D. and Grüneisen, E. 1942 A 71-273.15 Be./2 11 Erfling, H.D. and Grüneisen, E. 1942 A 71-273.15 Be./6 13 Mitchell, M.A. 1975 A 10-900 13 Mitchell, M.A. 7akahashi, Y., 1974 A 9.0-13 14 Varnaguchi, M., Takahashi, Y., 1974 B 90-300	æ	16	Williams, J.M., et al.	1972	∢	88.25-294.75	K38-1	The above specimen; after irradiation the sample was annealed at 324.3 K.
16       Williams, J.M., et al.       1972       A       72.91-90       K37-1         16       Williams, J.M., et al.       1972       A       73.35-90       K37-1         16       Williams, J.M., et al.       1972       A       73.35-90       K37-1         16       Williams, J.M., et al.       1972       A       71.28-329.76       K37-1         19       Berteaux, F.       1970       A:1-307.6       K37-1         29       Bridgman, P.W.       1927       A       71.28-329.76       K37-1         19       Berteaux, F.       1970       A:1-307.6       A       73-303       B         10       Babkina, M.A., Zhermuskaya, T.V.       1972       A       79-273.15       Be_/2         11       Erfling, H.D. and Grünelsen, E.       1942       A       77-273.15       Be_/2         11       Erfling, H.D. and Grünelsen, E.       1942       A       78-273.15       Be_/3         11       Erfling, H.D. and Grünelsen, E.       1942       A       78-273.15       Be_/3         13       Mitchell, M.A.       A       1975       A       10-900         13       Yamaguchi, M.A. Takahashi, Y.,       1974       A       9.0-13 <td>8</td> <td>16</td> <td>Williams, J.M., et al.</td> <td>1972</td> <td>&lt;</td> <td>76.55-370.16</td> <td>K37-1</td> <td>Pure; specimen axis was perpendicular to the pressing condition. Reported error 2%.</td>	8	16	Williams, J.M., et al.	1972	<	76.55-370.16	K37-1	Pure; specimen axis was perpendicular to the pressing condition. Reported error 2%.
16 Williams, J.M., et al.  173.35–90 K37–1  18 Williams, J.M., et al.  1972 A 73.74–92.66 K37–1  19 Berteaux, F.  29 Bridgman, P.W.  30 Babkina, M.A., Zhermunskaya, 1972 A 71.28–329.76 K37–1  11 Erfling, H.D. and Grüneisen, E. 1942 A 79–273.15 Be_//2  11 Erfling, H.D. and Grüneisen, E. 1942 A 79–273.15 Be_//2  11 Erfling, H.D. and Grüneisen, E. 1942 A 79–273.15 Be_//6  11 Erfling, H.D. and Grüneisen, E. 1942 A 79–273.15 Be_//6  11 Erfling, H.D. and Grüneisen, E. 1942 A 79–273.15 Be_//6  12 Mitchell, M.A.  13 Mitchell, M.A.  14 Yoshihro, K. and Grüneisen, E. 1975 A 10–900  15 Yoshihro, K. and Grüneisen, E. 1975 A 10–900  16 Yoshihro, K. and Grüneisen, E. 1975 A 10–900  17 Yamaguchi, M. Takahashi, Y., 1974 A 9.0–13	9	36	Williams, J.M., et al.	1972	<	72.91-90	K37-1	The above specimen; sample was irradiated by 2, 53 x 10% neutrons/cm, with E > 1 MeV. Reported error 2%.
16 Williams, J.M., et al.  1972 A 71.74-92.66 K37-1  19 Bertenux, F.  29 Bridgman, P.W.  30 Babkina, M.A., Zhermunskaya, 1972 A 79-233  1.B., Timofoeva, Z.A., and Tsukanova, N.V.  30 Babkina, M.A., et al.  11 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be_//2  11 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be_//2  11 Erfling, H.D. and Grüneisen, E. 1942 A 78-273.15 Be_//6  13 Mitchell, M.A.  14 Yoshibiro, K. and  Glover, R.E. III.  31 Yamaguchi, M., Takahashi, Y., 1974 B0-300	7	97	Williams, J.M., et al.	1972	<	73.35-90	K37-1	The above specimen; sample was irradiated by 6.19 x $10^{4}$ neutrons/cm² with $E > 1$ MeV. Reported error $2\%$
16 Williams, J.M., et al. 1972 A 71.28-329.76 K37-1 19 Berteaux, F. 1970 4.1-307.6 29 Britisman, P.W. 1927 A 303 30 Babkina, M.A., Zhermunakaya, 1972 ~293 1. B., Timforera, Z.A., and Tarkanova, N.V. 309 31 Erfling, H.D. and Grüneisen, E. 1942 A 79-273.15 Be_/2 31 Mitchell, M.A. 1975 A 10-900 32 Mitchell, M.A. 1975 A 10-900 33 Mitchell, M.A. 1975 A 10-900 34 Voshihiro, K. and Grüneisen, E. 1975 A 10-900 35 Yoshihiro, K. and Grüneisen, E. 1975 A 10-900 36 Yoshihiro, K. and Grüneisen, E. 1975 A 10-900 37 Yamaguchi, M.A. 1974 A 9.0-13 38 Yamaguchi, M., Takahashi, Y., 1974 B 90-300	3	16	Williams, J. M., et al.	1972	<	13.74-92.66	K37-1	The above specimen; sample was irradiated by 10.53 x $10^{43}$ neutrons/cm² with $E > 1$ MeV. Reported error $2\%$ .
19 Berteaux, F.  29 Bridgman, P.W.  30 Babkina, M.A., Zhermunakaya,  1972 ~293  L.B., Timoforera, Z.A., and  Tarkanova, N.V.  30 Babkina, M.A., et al.  11 Erfling, H.D. and Grüneisen, E.  11 Erfling, H.D. and Grüneisen, E.  12 Erfling, H.D. and Grüneisen, E.  13 Mitchell, M.A.  14 Yoshhiro, K. and  15 Yoshhiro, K. and  16 Glover, R.E. III.  31 Yamaguchi, M., Takahashi, Y., 1974 A 9.0-13  Takasaki, Y., and Ohia, T.	5	16	Williams, J.M., et al.	1972	∢	71.28-329.76	K37-1	The above specimen; after irradiation the sample was annealed at 338, 6 K.
29 Bridçman, P.W. 1927 A 303  30 Babkina, M.A., Zbermunskaya, 1972 ~293  L.B., Timofcera, Z.A., and Tsukanova, N.V. 30 Babkina, M.A., et al. 1972 A 79-273.15 Be//2 11 Erflug, H.D. and Grüneisen, E. 1942 A 78-273.15 Be//6 11 Erflug, H.D. and Grüneisen, E. 1942 A 78-273.15 Be//6 113 Mitchell, M.A. 1975 A 10-900  13 Mitchell, M.A. 1975 A 9.0-13 Glover, R.E. III. Glover, R.E. III. 1974 A 9.0-13 Takasaki, Y., and Ohia, T. 1974 B0-300	;	13	Berteaux, F.	1970		4.1-307.6		High purity; Debye temperature 8 = 1160 K, data were extracted from the smooth graph.
10. Babkina, M.A., Zhermunskaya, 1972 ~293 .99.  11. B., Timofoeva, Z.A., and Tsukanova, N.V.  12. B., Timofoeva, Z.A., and Grüneisen, E. 1942 A 79-273.15 Be//2 Put 11 Erflug, H.D. and Grüneisen, E. 1942 A 79-273.15 Be//6 Put 11 Erflug, H.D. and Grüneisen, E. 1942 A 78-273.15 Be//6 Put 11 Erflug, H.D. and Grüneisen, E. 1942 A 78-273.15 Be//6 Put 13 Mitchell, M.A. 1975 A 10-900 Sin Sin 13 Mitchell, M.A. 1975 A 10-900 Sin Sin Glover, R.E. III.  13 Yoshihiro, K. and Glover, R.E. III.  14 Yoshihiro, K. and Ohla, T. 1974 A 9.0-13 99.	3	53	Bridgman, P.W.	1927	<	303		Pure; the specimen was a casted rod 4.6 mm in diameter and 9 cm long; the specimen was obtained from Dr. H.S. Cooper of the Nemet Laboratories; density at 293 K was found to be 1.820.
20 Babkina, M.A., et al. 11 Erfling, H.D. and Grüneizen, E. 1942 A 79-273.15 Be// 2 Pur 11 Erfling, H.D. and Grüneizen, E. 1942 A 273.15 Be// 6 Pur 11 Erfling, H.D. and Grüneizen, E. 1942 A 78-273.15 Be// 6 Pur 13 Mitchell, M.A. 1975 A 10-900 Sin 13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshibiro, K. and Grüneizen, E. 1974 A 9.0-13 99, Glower, R.E. III. 21 Yamaguchi, M., Takahashi, Y., 1974 B0-300 0.0	ş	ဗ္ဗ	Babkina, M.A., Zhermunskaya, L.B., Timofceva, Z.A., and Tsukanova, N.V.	1972		~293		99.6 pure; 0.09 mm diameter wire specimen was obtained by casting, bot extraction, and hot drawing.
11 Erfling, H.D. and Grüneizen, E. 1942 A 79-273.15 Be// 2 Pur 11 Erfling, H.D. and Grüneizen, E. 1942 A 273.15 Be// 8 Pur 11 Erfling, H.D. and Grüneizen, E. 1942 A 78-273.15 Be// 8 Pur 13 Mitchell, M.A. 1975 A 10-900 Sin 13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshibiro, K. and Glover, R.E. III. 23 Yamnguchi, M., Takahashi, Y., 1974 A 9.0-13 99. Takasaki, Y., and Ohia, T.	41.	30	Babkins, M.A., et al.	1972		~293		Similar to the above specimen; except it was tempered at 773 K.
11 Erfling, H.D. and Grüneisen, E. 1942 A 273.15 Be_18 Pur 11 Erfling, H.D. and Grüneisen, E. 1942 A 78-273.15 Be_/6 Pur 13 Mitchell, M.A. 1975 A 10-900 Pur 13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshibiro, K. and Glover, R.E. II. 21 Yamnguchi, M., Takahashi, Y., 1974 A 9.0-13 99. Takasaki, Y., and Ohia, T.	49	11	Erfling, H.D. and Grüneisen, E.	1942	<	79-273.15	Be // 2	Pure; single crystal specimen with its acts parallel to becagenal axis.
11 Erfling, H.D. and Grüboison, E. 1942 A 78-273.15 Be// 6 Pur 13 Mitchell, M.A. 1975 A 10-900 Pur 13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshihiro, K. and Glover, R.E. III. 31 Yamnguchi, M., Takahashi, Y., 1974 B0-300 0.0	•63	11	Erfling, H.D. and Grüneisen, E.	1942	<	273.15	Be⊥8	Pure; single crystal specimen with its axis perpendicular to hexagonal axis.
13 Mitchell, M.A. 1975 A 10-900 Pu. 13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshibiro, K. and Glover, R.E. III. 21 Yamaguchi, M., Takahashi, Y., 1974 80-300 0.0	3	11	Erfling, H.D. and Grünoisen, E.	1942	<	78-273.15	Be// 6	Pure; single crystal specimen with its axis parallel to hexagonal axis.
13 Mitchell, M.A. 1975 A 10-900 Sin 15 Yoshibiro, K. and 1974 A 9.0-13 99. Glover, R. E. III. 31 Yamnguchi, M., Takahashi, Y., 1974 80-300 0.0	ផ	13	Michell, M.A.	1975	<	10-900	:	Pure; sincle crystal specimen with its axis parallel to the hexagoral axis; sample dimension 2 x 2 x 19 mm; the specimen was grown by triple pars zone refining of pure like in vacuum at the Franklin Institute Research Labs., data are extracted from the smoothed table; reported error 1.8%.
15 Yoshibiro, K. and 1974 A 9.0-13 99. Glover, R.E. III.  31 Yammguchi, M., Takahashi, Y., 1974 80-300 0.0	33	13	Mitchell, N.A.	1975	∢	10-900		Similar to the above specimen except its axis is perpendicular to the bexagonal axis and sample dimension 4 x 4 x 41 mm.; repetted error 1.8%.
31 Yamuguchi, M., Takahashi, Y., 1974 80-300 Takasaki, Y., and Ohia, T.	ន	92	Yoshibiro, K. and Glover, R.E. 田.	1974	<	9. 0-13		99, 95 pure; beryillum film were prepared by vacuum evaporation of distillation purified Be on crystalline quartz substrate; film thickness 150 $\lambda_i$ ; Ge resistance thermometer was used to measure the temperature; resistance per square data were reported; data were extracted from graph.
	<b>3</b>	ដ	Yamaguchi, M., Takabashi, Y., Takasaki, Y., and Ohia, T.			80-300		0.01 Ni, 0.008 Fe, 0.003 Mn, 0.002 Al, 0.002 Mg, 0.002 Si, 0.6001 Ca, 0.0001 Na, and < 0.0001 Cu; polycrystalline specimen was obtained from Johnsen Matthey Co.; page = 7 x 10° (3m; data were extracted from the graph.

<sup>\*</sup> Not shown in the figure.

TABLE 4. MEASUREMENT INFORMATION OF THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperature Dependence: (continued)

3%	Ref.	Author (s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
3	33	Denton, H.W.	1947	<	20. 2-273. 2		Pure; cylindrical specimen 3.5 cm long and 0.3 cm in diameter was prepared by "sintering" process by the American G. E. C.; result of the x-ray examination show that the grains of order $10^{-3}$ cm in size, almost completely stain free, and with a small proportion of considerably smaller grains.
8	e;	Dentoz, H.W.	1947	∢	20.2-273.2		Similar to the above specimen except it was anneated at 955 k for 12 hr and for shorter periods over the temperature ranges: 943 k and 833-513 k during cooling; result of x-ray examination showed the removal of any residual strain and removal of very small grains.
17	32	Denton, H. W.	1947	<	20. 2-273. 2		Similar to the above specimen except it was further "quenched" in water from above 1023 K.
9	32	Denton, H. W.	1947	∢	20. 2-273. 2		Similar to the above specimen except it was again receiving the 938 K heat.
30	13	Martin, A.J., Bunce, J.E., and Tithurg, P.D.	1962	∢	293	8	Pure; 0, 024 Mg, 0, 003 Al, 0, 037 Si, and 0.1 Fe; single crystal specimen approximately 0.5 in, in diameter and 6 in, long; crystal was extracted ingot stock by zone refining three times; the specimen was annealed in argon at 1133 K for 16 hr.
90	12	Martin, A.J., et al.	1962	<	293	15B	Similar to the above specimen except it was zone refining twice.
13	33	Kuczynski, G.C.	1960		4-300	QMV	Pure; the specimen was obtained from Brush Beryllium Corp., Cleveland, Ohio; melting point 1538 K; density 1.63 g/cm²; the specimen was annealed at 973 K for 1/2 hr; data were extracted from the figure.
62	ដ	Kuczynski, G.C.	1960		270-1000	QMV	Similar to the above specimen; the measurements were done by Battelle Instinute staff; data were extracted from the figure.
3	22	Tye, R.P.	1968		295-1283	Be 2 (4921)	98.4 Bc, 1.08 BcO, 0.13 C, 0.13 Fe, 0.09 Al, 0.01 Mg, 0.03 Si, 0.01 Mg, other metallic impurity 0.04; density 1.86 g cm²; bot pressed specimen is obtained from Brush Beryllium Company; cylindrical sample 13 mm in diameter and 100 mm in length; reported arror 1%.
3	21	Tye, R.P.	1968		295-1249	Be 4 (5085)	98.2 Be, 1.7 BeO, 0.12 C, 0.13 Fe, 0.12 Al, 0.03 Mg, 0.04 Si, 0.01 Ma, other metallic impurity 0.04; density 1.553 g/cm²; other specifications are similar to the above specimen; reported error 1%.
8	21	Tye, R.P.	1968		299-1258	Be 6 (4814)	98.46 Be, 1.6 BcO, C.12 C, 0.12 Fe, 0.09 Al, 0.01 Mg, 0.03 Si, 0.01 Mg, other metallic impurity 0.04; density 1.86 g/ml; other specifications are similar to the ubove specimen; reported error 1%.
9,	21	Tye, R.P.	1968		295-1276	Be 8 (4914)	Similar to the above specimen; reported error 1%.
2	2	Tye, R.P.	1968		297-1268	Be 9 (4811)	98, 41 Be, 1. 64 BeO, 0.12 C, 0.12 Fe, 0.09 Al, 0.01 Mg, 0.03 Si, 0.01 Ma, other metallic impurity 0.04; density 1.86 g/m³; other specifications are similar to the above specimen; reported error 1°.
3	21	Tye, R.P.	1968		298-1266	Be 11 (4811)	Similar to the above specimen, reported error 1%
<b>3</b> 3	ጃ	Tyc, R.P. and Quinn, J.F.	1968		293-859	Be 1	Pure; 2 BcO, 0.15 C, 0.18 Fe, 0.08 Si, 0.08 Mg, 0.16 Al, and 0.04 other metallic impurities; specimen are obtained from Brush Beryllium Company; cylindrical specimen 13 mm in diameter and 100 mm in length.

TABLE 4. MEANTREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF BERYLLRIN Be (Temperature Dependence) (continued,

j.	Cur. Raf.	Authorial	Year	Method	Temp.	Name and Specimen	Composition (weight percent), Specifications, and Remarks
; }	i					Ne ikuraa	
92	ক	Tye, R. P. and Quina, J. F.	1968		293-860	Be 2	Similar to the above specimen.
: =	7		1968		293-801	Be 3	Similar to the above specimen.
: 8	3		1968		293-825	Be 5	Similar to the above specimen.
i ti	; #		1960	Ø	4-300	T1 Y2-2	Pure; 0.087 nonmetallic impurity, 0.094 metallic impurity; the specimens were 2 in. long and 0.1 in. by 0.5 in. rectangular bars or 0.25 in. diameter cylinders. Leeds and Northup Precision Kelvin Bridge was used for measurements; measurements were made in vacuum.
7.	22	Bo, J. and Wright, E.S.	1960	m	4-300	T3 Y2-3	Purc; 0.144 nonmetallic impurity, 0.222 metallic impurity; other specifications similar to the above specimen.
73	2	Ho. J. and Wright, E.S.	1960	æ	4-300	T3 Y2-4	Similar to the above specimen.
2	2 2		1960	Ø	295-1416	Y6825	0.947 O, 0.0013 H, 0.0071 N, 0.003 Mg, 0.015 Al, 0.01 Si, 0.004 Ca. 0.002 Ti, 0.005 Mn, 0.15 Fe, 0.01 Ni, and 0.004 Cui measurements below 973 K were made in yacuum, purificed argon are admitted at higher temperatures to relard the evaporation of specimen; data were extracted from the figure; other specifications are similar to the above specimens.
#	2	Ho, J. and Wright, E. S.	1960	Ø	292-1447	Y9384	0.54 O. 0.0106 N. 0.006 Mg. 0.05 Al, 0.008 Si, 0.002 Ca, 0.004 Tl, 0.01 Cr, 0.008 Mg, 0.15 Fe, 0.015 Ni, and 0.01 Cu; other specifications are similar to the above specimen.
Ę	22	Ho, J. and Wright, E. S.	1960	ø	295-1454	Y6826	0.827 O, 0.0012 H, 0.0026 N, 0.01 Mg, 0.03 Al, 0.02 St, 0.002 Ca, 0.002 Ti, 0.01 Cr, 0.006 Mn, 0.15 Fe, 0.015 Nt, and 0.01 Cu; other specifications are similar to the above specimen.
23	22	Ho, J. and Wright, E.S.	1960	ф	303-1409	YB 1000	0. 786 O, 0.0056 N, 0.015 Mg, 0.03 Al, 0.008 Si, 0.002 Cs, 0.002 Ti, 0.01 Cr, 0.01 Mn, 0.15 Fe, 0.02 Ni, and 0.015 Cu; other specifications are similar to the above specimen.
2	23	Ho, J. and Wright, E.S.	1960	ø	360-1454	LYB 1102	0, 635 O, 0, 0101 H, 0, 005 N, 0, 02 Mg, 0, 04 Al, 0, 04 Sl, 0, 002 Ca, 0, 004 Ti, 0, 02 Cr, 0, 008 Mn, 0, 2 Fe, 0, 02 Ni, and 0, 01 Cu; other specifications are similar to the above specimen.

TABLE 5. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperature Dependence)

• Not shown in figure.

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TABLE S. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM Be (Temperature Dependence) (comminued)

CURVE 20 (CORIL)  CURVE 20 (CORIL)  CURVE 21 (CORIL)  CURVE 21 (CORIL)  CURVE 21 (CORIL)  CURVE 21 (CORIL)  CURVE 22 (CORIL)  CURVE 22 (CORIL)  CURVE 23 (CORIL)  CURVE 24 (CORIL)  CURVE 25 (CORIL)  CURVE 25 (CORIL)  CURVE 25 (CORIL)  CURVE 26 (CORIL)  CURVE 27 (	CUITY 20			EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM		Be (Temperature Dependence) (continued)	(continued)
CUINTE SO   CUIN	CURIVE 59   CORNE 50   CURIVE 50   CURIVE 50   CORNE 50   CORNE 50   CORNE 50     Fig. 21.2   Fig. 21.2   Fig. 21.2   Fig. 20.2   Fig. 50   Fig. 50     Fig. 21.2   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 21.2   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 21.2   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 21.2   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 21.2   Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 21.3   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50     Fig. 50   Fig. 50   Fig. 50	<b>a</b>	<b>a</b>	a H	t a	d d	Q.
14.6	14.6	RVE 26 (cont.)	8	CURVE 34 (cont.)	CURVE 39 (cont.)		
18.1   17.2   22.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0   20.0	18.1   17.2   22.0   21.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0			60			
The color of the	Table   Tabl						
Curve 20   Curve 30	Column   C						
Curre 2	Curre 2						
Color   Colo	Colored   Colo		50 AMELIO				
Column   C	Color   Colo		CONVE 31				
4.2         2.23         6.1         366.2         6.23         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08         170.08	4.2         2.2.7         6.1         2.6.2         6.2.9         1.7.0         6.1         2.6.2         6.2.9         1.7.0         6.1         2.6.2         6.2.9         6.2.2         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3         6.2.3 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
Colore   C	Color   Colo	•					
5.0         473         7.7         402.5         7.79         25.4.31         7.51         100.0         0.0831         CURVE           19.3         473         11.0         CURVE         27.37         3.339         14.0         0.0831         CURVE           19.3         47.3         11.0         CURVE         27.37         3.39         40.0         0.0831         CURVE           20.7         47.3         11.13         312.70         3.39         20.2         0.0831         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0	5.0         473         1.7         402.5         7.799         254.31         7.51         100.0         0.0631         CUNVE           15.3         6.0         473         11.0         CUNVE         23         273.91         3.339         14.0         0.0631         CUNVE         10           15.3         4.3         11.0         CUNVE         23         25.2         2.396         0.0383         10.6         10           24.4         87.3         12.1         32.2         2.396         2.31         10.6         1.31         30.7         10.6         10.9         0.0831         10           25.2         2.2         1.2         1.23         2.2         1.23         2.0         10.6         1.23         2.0         10.6         1.23         2.0         1.0         2.0         10         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0 <td< td=""><td>÷</td><td></td><td>ဖ</td><td></td><td></td><td></td></td<>	÷		ဖ			
5.6         473         11.0         CTRVE 55         222, 02, 3, 30, 30, 12.3         18.3         CTRVE 55         3.39         18.3         CTRVE 55         3.39         18.3         CTRVE 55         3.09         18.3         CTRVE 54         0.035         CTRVE 51         3.00         18.3         CTRVE 54         0.035         CTRVE 50         0.035         CTRVE 50         0.035         CTRVE 50         0.035         1.00         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035         0.035 <th< td=""><td>6, 6         473         11.0         CURVE 23         22.77.97         3.33         14.29         0.235         CURVE 24           15.3         573         14.29         CURVE 23         22.77.97         3.83         104.29         0.235         CURVE 41           15.3         573         14.29         73.75         1.13         3.04.16         6.349         90.25         10           24.4         873         24.5         86.18         1.214         37.10         6.349         90.25         10           25.2         24.4         873         22.7         1.244         30.3         10.6         3.02         10           25.2         4.3         10.0         1.247         2.00         CURVE 23         90.10         2.13         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         <td< td=""><td></td><td></td><td>۲.</td><td></td><td></td><td></td></td<></td></th<>	6, 6         473         11.0         CURVE 23         22.77.97         3.33         14.29         0.235         CURVE 24           15.3         573         14.29         CURVE 23         22.77.97         3.83         104.29         0.235         CURVE 41           15.3         573         14.29         73.75         1.13         3.04.16         6.349         90.25         10           24.4         873         24.5         86.18         1.214         37.10         6.349         90.25         10           25.2         24.4         873         22.7         1.244         30.3         10.6         3.02         10           25.2         4.3         10.0         1.247         2.00         CURVE 23         90.10         2.13         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00         2.00 <td< td=""><td></td><td></td><td>۲.</td><td></td><td></td><td></td></td<>			۲.			
13.5   57.3   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5   14.5	1.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5   5.5						CURVE 52
13.3   16.3   18.3   18.3   18.3   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5   18.5	13.3   14.3   14.3   14.3   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4   14.4			CURVE 35			
The color of the	1.6.9   17.3   22.2   2.7   2.7   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1   2.1						
Curre 2	The color   1.24   27.5   26.5   26.5   1.24   27.0   27.0   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.04   2.						
The color of the	The color of the					CURVE 45	
Table   Curve   22	Curve 30   20.18   1.247   1.2249   2.118   1.247   2.109   2.00   1.0 6   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.00   2.				Ġ		
CURVE 28	Curve 24   Curve 32   St. 1. 1. 2. 2. 34   Curve 40   Curve 40   St. 1. 2. 2. 35   St. 1. 35   Curve 40   Curve 40   St. 1. 2. 2. 35   St. 1. 35   S				i		
CHRVE 28   23	CINVE 20		CURVE 32		CURVE 40		
Color   Colo	The color of the	CURVE 28				CURVE 46*	
The color of the	CLINVE 25         32         CLINVE 36         80.46         2.13         20.9         5.0         4.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	G. 2- 10.9         417 11.5         6. p- 573         CURVE 34         91.00 10.9         2. 149 2. 186         91.00 2. 186         2. 149 2. 186         91.00 2. 186         2. 149 2. 186         91.00 2. 186         2. 149 2. 186         CURVE 41 2. 186         90.00 2. 186         2. 149 2. 186         CURVE 41 2. 186         90.00 2. 186         2. 149 2. 186         CURVE 41 2. 186         90.00 2. 186         2. 140 2. 186         CURVE 42 2. 186         90.00 2. 186         2. 140 2. 186         2. 110 2. 186         2. 110 2. 186         2. 140 2. 186         2. 110 2. 186		500				
10.5   57.2   12.8   82.52   1.865   90.00   2.168   CURVE 41**   600   1.05     10.5   57.3   12.8   82.52   1.865   90.00   2.168   CURVE 41**   600   1.05     10.5   57.3   12.8   91.7   1.899   CURVE 41**   293   4.5   900   2.05     27.4   28.3   117.74   2.066   62.81   3.435   78.95   0.045     27.5   29.3   2.4,0   115.90   2.053   62.81   3.435   78.95   0.045     27.5   29.3   2.4   2.066   2.063   62.81   3.435   78.95   0.045     27.5   29.3   2.4   2.066   2.063   91.00   3.458   89.97   0.0763   91.00     28.0   37.3   6.1   99.57   1.453   82.45   4.401   2.131   3.12   9.40     28.0   37.3   12.4   2.066   4.386*   CURVE 42**   2.131   3.12   9.40     28.0   37.3   12.4   2.066   4.386*   CURVE 42**   2.131   3.12   9.40     28.0   37.3   12.4   2.066   4.386*   CURVE 42**   2.131   3.12   9.40     28.1   2.4   2.1   2.4   2.066   4.386*   CURVE 42**   2.131   3.12   9.40     28.2   2.3   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.3   2.4   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.3   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.3   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.3   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.4   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.4   2.4   2.4   2.3   2.4   2.3   2.4   2.3   2.4     28.5   2.4   2.4   2.3   2.4   2.3   2.4   2.4     28.5   2.4   2.4   2.4   2.4   2.4   2.4   2.4     28.5   2.4   2.4   2.4   2.4   2.4   2.4   2.4     28.5   2.4   2.4   2.4   2.4   2.4   2.4   2.4     28.5   2.4   2.4   2.4   2.4   2.4   2.4   2.4   2.4     28.6   2.4   2.4   2.4   2.4   2.4   2.4   2.4   2.4     28.7   28.2   28.2   28.2   28.2   28.2   28.2   28.2   28.2     28.7   28.2   28.2   28.2   28.2   28.2   28.2   28.2   28.2     28.7   28.2   28.2   28.2   28.2   28.2   28.2   28.2   28.2     28.8   28.4   28.2   28.2   28.2   28.2   28.2   28.2   28.2     28.8   28.8   28.8   28.8   28.2   28.2   28.2   28.2   28.2   28.2     28.8   28.8   28.8   28.2   28.2   28.2   28.2   28.2   28.2   28.2   28.2     28.8   28.8   28.8   28.2   28.2	17.7         47.3         9.6         CLRVE 41         CURVE 41         600         1.0           10.5         57.3         12.8         8.2.5         1.865         90.0         2.168         CURVE 41         593         4.5         600         1.0           18.2         67.3         16.2         91.77         1.898         CURVE 41         293         4.5         900         2           26.4         97.3         24.0         115.94         2.053         73.35         3.410         CURVE 42.         900         2           26.4         97.3         24.0         115.94         2.053         7.335         3.410         CURVE 42.         9.00         2           26.4         97.3         1.6         90.02         1.407         7.34         3.48         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.045         9.00         2.015         2.00         2.015 <t< td=""><td></td><td>373</td><td>CLRVE 36</td><td></td><td></td><td></td></t<>		373	CLRVE 36			
10.9   573   12.8   82.52   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865   1865	10.9   57.3   12.8   52.2   1.865   1.899   CURVE 41   293   4.5   900   1.999   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.945   1.9		473				_
14.5   773   16.2   91.77   1899   CURVE 41   293   4.5   900   1   1   1   1   1   1   1   1   1	14.5   677   16.2   91.77   1899   CURVE 41   293   4.5   900   22.2   25.4   24.0   10.134   1.948   73.35   3.410   CURVE 42   25.6   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.65   20.6		573				
18.2°   173   20.0   101.34   1.946   115.90   2.053   13.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   14.00   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.435   3.43	18.2   773   20.0   101.34   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946   1.946		673		CIRVE 41		
Table   Tabl	Table   Tabl						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	27.4         973         28.3         117.74         2.066         62.81         3.438         73.39         CURVE         29.00         3.458         78.93         0.045         9.00           LRNE         29.8         3.8         82.78         1.382         CURVE         27         0.763         9.00           4.1*         2293         3.8         82.78         1.382         CURVE         27         0.763         9.15           5.0*         373         6.1         99.57         1.453         82.45         4.401         273.15         3.58         9.15           6.0*         4.73         9.3         6.1         99.57         1.453         82.45         4.401         273.15         3.12         9.40         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.47         9.45         9.47         9.47					CITRVE 45*	
10.08         CURVE 33         CURVE 33         CURVE 34         T8,95         0.045         CURVE 37           URVE 25         293         3.8         82.78         1.382         CURVE 37         CURVE 37         S. 0.763         9.00           4.1*         323         4.6         99.57         1.453         CURVE 37         CURVE 37         CURVE 37         9.10         CURVE 37         9.00         9.75         9.75         9.00         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75         9.75 <th< td=""><td>30.8         CURVE 23         CURVE 24         CURVE 25         1.00         3.458         78.95         0.045         CURVE 25           4.1*         253         3.8         82.78         1.382         CURVE 42         2.71.15         3.58         9.27           4.1*         373         4.6         90.12         1.407         73.74         4.701         CURVE 42         2.71.15         3.58         9.27           5.0         4.1*         373         6.1         90.12         1.407         73.74         4.701         2.718         9.27           5.0         4.1*         373         6.1         90.12         1.407         73.74         4.401         2.718         9.27           5.0         4.73         6.1         90.12         1.407         73.74         4.401         2.401         9.27           9.9**         573         12.4         90.12         1.407         73.44         4.401         2.713         3.12         9.27           17.1         573         12.4         2.004         4.425         2.713         3.12         9.61         10.54           2.0.2         9.6         4.425         2.7213         2.7213         2.7213</td><td></td><td></td><td></td><td></td><td></td><td>C1201.E 63</td></th<>	30.8         CURVE 23         CURVE 24         CURVE 25         1.00         3.458         78.95         0.045         CURVE 25           4.1*         253         3.8         82.78         1.382         CURVE 42         2.71.15         3.58         9.27           4.1*         373         4.6         90.12         1.407         73.74         4.701         CURVE 42         2.71.15         3.58         9.27           5.0         4.1*         373         6.1         90.12         1.407         73.74         4.701         2.718         9.27           5.0         4.1*         373         6.1         90.12         1.407         73.74         4.401         2.718         9.27           5.0         4.73         6.1         90.12         1.407         73.74         4.401         2.401         9.27           9.9**         573         12.4         90.12         1.407         73.44         4.401         2.713         3.12         9.27           17.1         573         12.4         2.004         4.425         2.713         3.12         9.61         10.54           2.0.2         9.6         4.425         2.7213         2.7213         2.7213						C1201.E 63
CURVE 25         CURVE 23         CURVE 23         CURVE 23         CURVE 24         S5, 97         0.0763         9.00           4.1*         253         3.8         82.78         1.382         CURVE 42         273.15         3.58         9.15           5.0*         4.5*         323         4.6         90.12         1.407         73.74         4.376         CURVE 42         9.15         9.15           5.0*         4.5*         323         4.6         90.12         1.407         82.45         4.401         273.15         3.12         9.47           6.0*         4.73         6.1         99.57         1.453         92.06         4.421         273.15         3.12         9.47           13.5         15.0         6.3         9.764         4.385         CURVE 43         273.15         3.12         9.47           20.9         873         23.8         114.85         0.9032         CURVE 43         273.15         3.12         9.75           20.9         9.7         2.218         1.126         7.128         0.74135         13.19         113.10           20.9         7.2         2.2         2.219         1.456         2.218         0.723	CURVE 23         CURVE 33         CURVE 37         S. 18         82.78         1.382         CURVE 42         273.15         3.58         9.13           4.1*         323         4.6         90.12         1.407         73.74         4.376         CURVE 42         273.15         3.58         9.47           5.0*         4.3         5.3         12.4         90.12         1.407         73.74         4.376         CURVE 42         9.47         9.47           5.0*         4.3         5.4         4.401         CURVE 42         9.00         0.4455         273.15         3.12         9.40           9.9*         573         12.4         CURVE 38         92.06         4.385*         CURVE 43         7.85*         9.75         9.75         9.75           17.1         17.3         19.8         88.25         0.7697         CURVE 43         7.85*         0.7713*         11.10         11.10         11.10         11.11         11.10         11.11         11.11         11.11         11.11         11.11         11.11         11.11         11.11         11.11         11.11						3,022
LRNE 29         293         3.8         82.78         1.382         CURVE 42         273.15         3.58         9.15           4.1*         329         3.8         82.78         1.382         CURVE 42         273.15         3.58         9.15           5.0*         4.1*         323         4.6         90.12         1.407         73.74         4.35         273.15         3.58         9.15           5.0*         473         9.1         99.77         1.453         90.00         4.425         273.15         3.12         9.47           9.5         6.5         9.7         1.453         0.7697         CURVE 43         273.15         3.12         9.41           17.1         773         19.8         88.25         0.7697         CURVE 43         773.63         0.0404         10.54           20.9         9.3         11.6         88.25         0.7637         CURVE 43         773.63         0.0404         10.54           20.9         9.3         11.2         11.2         11.2         11.3         11.3         11.3           20.9         9.3         11.2         11.2         11.2         11.2         11.2         11.3         11.3	CURVE 29         293         3.8         8.7 m s = 1.382         CURVE 42         273.15         3.58         9.13           4.1*         329         4.1*         90.12         1.482         CURVE 42         273.15         3.15         9.27           5.0*         373         6.1         99.57         1.453         82.45         4.401         CURVE 49         9.47           9.9*         573         12.4         90.12         1.453         90.00         4.425         273.15         3.12         9.47           9.9*         573         12.4         90.12         1.453         90.00         4.425         273.15         3.12         9.40           13.5         673         16.0         88.25         0.7697         CURVE 43         273.15         3.12         9.60         4.425         273.15         3.12         9.61           25.9         673         28.3         1.126         82.35         0.7213*         9.73         10.09           25.9         973         2.219         1.126         82.35         0.7445         7.825         0.109           27.2         96.0         7.2         2.448         2.863         1.450         1.173 <t< td=""><td></td><td></td><td>CIRVE 37</td><td></td><td></td><td></td></t<>			CIRVE 37			
4.1*         293         3.8         82.78         1.382         CURVE 36         99.57         1.467         73.74         4.376         CURVE 49*         9.40         9.27         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.40         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41         9.41 <td>4.1*         293         3.8         82.78         1.382         7.3.74         4.376         CURVE 49*         9.27           5.0*         4.1*         323         4.6         90.12         1.407         7.3.74         4.376         CURVE 49*         9.40           5.0*         4.73         5.1         90.12         1.467         7.3.74         4.376         CURVE 49*         9.40           5.0*         4.73         5.1         90.12         1.467         90.12         1.401         9.40           9.9*         573         12.4         90.12         90.06         4.356         2.73.15         3.12         9.41           17.3         6.3         873         23.8         114.85         0.7697         CURVE 43         CURVE 30         0.0044         11.10           20.9         90.0         90.00         4.1487         20.303         71.28         0.7139*         89.57         0.0128         11.10           20.9         90.0         90.00         90.00         90.00         90.00         90.00         90.00           20.9         90.0         90.00         90.00         90.00         90.00         90.00         90.00           <t< td=""><td>TRVE 29</td><td></td><td>10 74 100</td><td>CIRVE 49</td><td></td><td></td></t<></td>	4.1*         293         3.8         82.78         1.382         7.3.74         4.376         CURVE 49*         9.27           5.0*         4.1*         323         4.6         90.12         1.407         7.3.74         4.376         CURVE 49*         9.40           5.0*         4.73         5.1         90.12         1.467         7.3.74         4.376         CURVE 49*         9.40           5.0*         4.73         5.1         90.12         1.467         90.12         1.401         9.40           9.9*         573         12.4         90.12         90.06         4.356         2.73.15         3.12         9.41           17.3         6.3         873         23.8         114.85         0.7697         CURVE 43         CURVE 30         0.0044         11.10           20.9         90.0         90.00         4.1487         20.303         71.28         0.7139*         89.57         0.0128         11.10           20.9         90.0         90.00         90.00         90.00         90.00         90.00         90.00           20.9         90.0         90.00         90.00         90.00         90.00         90.00         90.00 <t< td=""><td>TRVE 29</td><td></td><td>10 74 100</td><td>CIRVE 49</td><td></td><td></td></t<>	TRVE 29		10 74 100	CIRVE 49		
4.1*         323         4.6         90.12         1.407         73.74         4.376         CURVE 49*         9.47           5.0*         4.1*         323         4.6         90.12         1.453         82.45         4.401         CURVE 49*         9.47           5.0*         4.25         4.25         2.2.1         3.73         12.4         CURVE 38         90.00         4.425         273.15         3.12         9.47           9.9*         573         12.4         CURVE 38         92.05         4.385         92.05         4.425         273.15         3.10         9.47           17.1         773         12.8         88.25         0.7697         CURVE 43         78.29         0.00404         110.9           25.2         973         28.3         114.85         0.932         71.28         0.7213*         78.29         0.00404         110.9           25.9         973         28.3         114.85         0.932         71.28         0.7213*         78.95         0.7415         78.50         12.79           25.9         95.0         95.0         95.0         95.0         95.4         1.35.4         1.35.4         1.27         1.27 <t< td=""><td>4.1*         323         4.6         90.12         1.407         73.74         4.376         CURNE 49*         9.47           5.0*         4.37         6.1         99.57         1.453         90.12         1.453         90.00         4.455         273.15         3.12         9.47           5.0*         4.35         573         12.4         CURVE 38         92.66         4.385*         CURNE 50         10.09           17.1         773         12.4         6.73         16.0         88.25         0.7697         CURNE 43         78.29         0.00404         10.54           20.9         873         28.3*         114.85         0.9032         CURNE 43         78.29         0.00404         110.54           20.9         873         28.3*         114.85         0.9032         CURNE 43         78.95         0.7128         78.95         0.0445         110.54           20.9         873         12.5         13.3         11.26         82.95         0.7445         27.315         13.75         CURNE 51         11.97           20.9         9.4         0.753         29.4.75         4.487         2.44.87         2.45.84         3.05         0.041         4.2</td><td></td><td></td><td>-</td><td>25 7 100</td><td></td><td></td></t<>	4.1*         323         4.6         90.12         1.407         73.74         4.376         CURNE 49*         9.47           5.0*         4.37         6.1         99.57         1.453         90.12         1.453         90.00         4.455         273.15         3.12         9.47           5.0*         4.35         573         12.4         CURVE 38         92.66         4.385*         CURNE 50         10.09           17.1         773         12.4         6.73         16.0         88.25         0.7697         CURNE 43         78.29         0.00404         10.54           20.9         873         28.3*         114.85         0.9032         CURNE 43         78.29         0.00404         110.54           20.9         873         28.3*         114.85         0.9032         CURNE 43         78.95         0.7128         78.95         0.0445         110.54           20.9         873         12.5         13.3         11.26         82.95         0.7445         27.315         13.75         CURNE 51         11.97           20.9         9.4         0.753         29.4.75         4.487         2.44.87         2.45.84         3.05         0.041         4.2			-	25 7 100		
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6.64 473 9.1 CURVE 38 90.00 4.425 273.15 3.12 9.15 9.15 9.15 9.15 9.15 9.15 9.15 9.15	6.6			•		2000	
13.5	9.94 573 12.4 CURVE 38 90.00 4.423 273.13 3.12 9.14 9.14 9.14 9.2 6 4.3854 CURVE 50 10.09 17.1 17.3 12.8 184.2 0.7697 CURVE 43 78.2 0.00404 11.10 10.54 11.37 25.9 13.38 1.126 82.95 0.7445 79.67 0.0428 11.10 11.97 25.9 0.727 25.9 0.727 25.2 1.564 82.95 0.7445 79.97 0.0728 11.10 11.97 11.37 23.4 8 2.863 11.56 82.95 0.7445 79.97 0.0728 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 11.37 1						
13.5   673   12.4   CURVE 30   92.06   4.385*   CURVE 50   10.09   17.1     17.1   19.8   88.25   0.7697   CURVE 43   79.63   0.0404   10.54     20.9   873   23.8   114.85   0.9032   71.28   0.7234   79.63   0.0425   11.10     22.2   973   28.3*   114.85   0.9032   71.28   0.7234   79.63   0.0425   11.10     22.9   CURVE 34   28.3*   1.126   71.28   0.7245   273.15   3.56   12.79     CURVE 34   2.863   1.956   1.955   273.15   3.56   12.79     CURVE 34   2.863   1.9401   1.925   CURVE 31   CURVE 31     24.5   6.3   68.4   0.7552   294.75   4.487   245.83   3.060   5.0   0.41   4.2     24.5   6.4   0.7552   CURVE 39   256.44   4.121   100   0.53   6.5     25.5   0.7904   76.55   0.7058   329.76   5.343   200   2.00   2.15     21.5   20.5   20.750   2.955   2.957   2.957   2.957   2.957     25.5   25.5   25.5   2.7058   329.76   5.343   2.00   2.00   2.15     25.5   25.5   25.5   2.7058   329.76   5.343   2.00   2.00   2.15     25.5   25.5   25.5   2.7058   329.76   5.343   2.00   2.00     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00     25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00   2.15     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00   2.15     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00   2.15     25.5   25.5   25.5   25.5   2.7058   2.25   2.343   2.00   2.00   2.15     25.5   25.5   25.5   25.5   2.7058   2.25   2.25   2.7058   2.15     25.5   25.5   25.5   25.5   2.7058   2.25   2.25   2.25   2.25   2.25     25.5   25.5   25.5   2.7058   2.25   2.25   2.25   2.25   2.25   2.25     25.5   25.5   25.5   2.7058   2.25   2.25   2.25   2.25   2.25   2.25   2.25     25.5   25.5   25.5   25.5   2.7058   2.25   2.25   2.25   2.25   2.25   2.25   2.25   2.25   2.25   2.25     25.5   25.5   25.5   25.5   2.7058   2.25   2.25   2.25   2.25   2.25	13.5   673   16.0     13.5   673   16.0     17.1   19.8   88.25   0.7697     20.5   87.2   23.8   11.85   0.9032     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.8   11.20     20.5   87.2   23.4     20.5   87.2   23.8     20.5   87.2   23.8     20.5   87.2   23.8     20.6   82.95   0.7445     20.7   26.2   294.75     20.7   26.2   294.75     20.7   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.7     20.8   20.8     20.8   20.7     20.8   20.8     20.8   20.7     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20.8     20.8   20			20 1114110			
17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1	12.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1   17.1	•		COUVE 30			
LINE         36         13.5         14.87         0.7697         CLIVE 43         78.29         0.00404         10.54           25.2         973         23.8         1.14.85         0.9022         71.28         0.7213*         78.53         0.04125         11.97           25.9         973         23.8         1.126         82.95         0.7445         79.63         0.0128         11.97           25.9         CURVE 34         205.87         2.19         102.42         0.726*         273.15         3.56         12.79           17.2         6.3         72.2         2.863         145.03         1.173         CURVE 31         12.79           17.2         88.4         0.7527         2.65.20         3.656*         104.01         1.925         10         0.41         4.2           17.2         88.4         0.7566         2.947.7         4.487         2.44.87         2.45.83         3.060         0.41         4.2           12.1         95.0         0.7904*         0.7904*         76.55         0.7058         329.76         4.563*         1.00         0.53         6.6           15.5         0.03.8         0.7058         329.76         5.343	CLINVE 30   71.28   71.28   71.28   71.28   71.28   71.28   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29   71.29					CURVESO	
25.2         973         25.5         11.10         79.63         0.04125         11.10           25.2         973         28.3*         1.126         71.28         0.7213*         79.63         0.04125         11.10           25.9         CURVE 34         28.3*         1.126         1.126         1.126         1.22         1.139           25.9         CURVE 34         205.87         2.19         1.02.42         0.7256*         1.273         12.79           12.5         0.7207         265.20         1.45.03         1.173         CURVE 51         1.25         1.00         0.41         4.2         1.79           7.2         6.3         6.4         0.7532         294.75         4.487         2.45.83         3.060         50         0.41         4.2           8.5         94.0         0.7939         CURVE 39         2.26.44         4.121         1.00         0.53         5.6           12.4         10.3         0.7954         7.658         3.29.76         5.343         2.00         2.00         2.15	Table   Tabl				CCICVE 43		
25.2         973         28.3*         1.126         71.28         0.7213*         89.97         0.0728         11.87           29.9         CURVE 34         1.264         82.95         0.7445         273.15         3.56         12.79           CVRVE 34         CURVE 34         2.214         102.42         0.7445         273.15         3.56         12.79           CLRVE 34         2.214         2.214         102.42         1.73         CURVE 31         CURVE 31         CURVE 31         CURVE 31         CURVE 31         CURVE 31         CURVE 32         CURVE 32         2.945.81         3.060         0.41         4.2         6.2         8.5         9.40         0.753         CURVE 39         2.86.44         4.121         100         0.41         4.2         6.2         8.6         2.26.44         4.121         100         0.53         8.6         2.6         8.6         2.26.44         4.121         100         0.53         8.6         2.6         2.6         2.6         2.2         3.05         8.6         3.05         8.6         3.0         9.6         9.6         9.6         9.6         9.6         9.6         9.6         9.6         9.6         9.6         9.6         9.6 <td>25.2         973         28.3*         1.126         71.28         0.7213*         89.97         0.0728         11.97           29.9         CURVE 34         171.55         1.564         82.95         0.7445         273.15         3.56         12.79           CVRVE 30         CURVE 34         2.219         102.42         0.7445         273.15         3.56         12.79           CS         3.48         2.219         102.42         0.7536*         1.07.45         273.15         3.56         12.79           CS         4.487         2.14.21         2.945*         10         0.41         4.2           E. 9         94.0         0.7532         294.75         4.487         245.83         3.060         0.41         4.2           12.1         95.0         0.7939         CURVE 39         286.44         4.121         100         0.53         6.6           12.1         103.8         0.8351         76.55         0.7058         329.76         5.343         200         2.00         2.1.5</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	25.2         973         28.3*         1.126         71.28         0.7213*         89.97         0.0728         11.97           29.9         CURVE 34         171.55         1.564         82.95         0.7445         273.15         3.56         12.79           CVRVE 30         CURVE 34         2.219         102.42         0.7445         273.15         3.56         12.79           CS         3.48         2.219         102.42         0.7536*         1.07.45         273.15         3.56         12.79           CS         4.487         2.14.21         2.945*         10         0.41         4.2           E. 9         94.0         0.7532         294.75         4.487         245.83         3.060         0.41         4.2           12.1         95.0         0.7939         CURVE 39         286.44         4.121         100         0.53         6.6           12.1         103.8         0.8351         76.55         0.7058         329.76         5.343         200         2.00         2.1.5						
29.9         CURVE 34         171.55         1.564         82.95         0.7445         273.15         3.56         12.79           URVE 34         CURVE 34         2.05.87         2.219         102.42         0.7856*         2.73.15         3.56         12.79           CASA         1.5.5         1.564         102.45         1.07.24         0.7856*         1.75         0.7856*         1.07         0.41         4.2           R. 9         0.766         2.65.2         2.65*         1.04.01         1.925         1.00         0.41         4.2           R. 9         0.766         CURVE 39         2.86.44         4.121         1.00         0.41         6.2           12.1         95.0         0.7904*         CURVE 39         2.86.44         4.121         100         0.53         6.6           15.5*         103.8         0.8951         76.55         0.7058         329.76         5.343         200         2.00         21.5	29.9         CURVE 34         171.55         1.564         82.95         0.7445         273.15         3.56         12.79           URVE 34         CURVE 34         205.87         2.219         102.42         0.7856*         273.15         3.56         12.79           1.2         84.7         0.7532         2.86.7         4.87         2.84.21         1.925         104.01         1.925         104.01         1.925         100         0.41         4.2           7.2         84.7         0.7532         2.94.75         4.487         2.24.21         2.945*         10         0.41         4.2           6.5         94.0         0.7939         CURVE 39         2.86.4         4.121         100         0.53         6.2           12.1         95.0         0.77904*         76.55         0.7058         329.76         5.343         200         2.00         2.05           15.5         103.8         0.8351         76.55         0.7058         329.76         5.343         200         2.00         21.5						
CURVE 34         205.87         2.219         102.42         0.856*         CURVE 34         CURV	CRNE 34         205.87         2.219         102.42         0.856*         CURVE 31         CURVE 32         CURVE						
CFALE 30         12.5         0.7207         234.48         2.863         145.03         1.173         CURVE 51         CURVE 52         CURVE 52 <td>CRNE 30         72.5         0.7207         253.48         2.863         145.03         1.173         CURVE 51         CURVE 52         245.83         3.060         50         0.41         4.2         CURVE 51         2.945.83         3.060         50         0.41         4.2         CURVE 51         2.256.44         4.121         100         0.41         4.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         7.2         7.2         7.2         7.2         4.121         100         0.41         4.2         6.2         6.2         6.2         6.2         6.2         6.6         7.2         6.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2</td> <td></td> <td>CURVE 34</td> <td></td> <td></td> <td></td> <td></td>	CRNE 30         72.5         0.7207         253.48         2.863         145.03         1.173         CURVE 51         CURVE 52         245.83         3.060         50         0.41         4.2         CURVE 51         2.945.83         3.060         50         0.41         4.2         CURVE 51         2.256.44         4.121         100         0.41         4.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         6.2         7.2         7.2         7.2         7.2         4.121         100         0.41         4.2         6.2         6.2         6.2         6.2         6.2         6.6         7.2         6.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2         7.2		CURVE 34				
6.3 64.7 0.7207 265.20 3.655* 1194.01 1.925 10 0.41 4.2 7.2 88.4 0.7666 294.75 4.487 245.81 2.945* 10 0.41 4.2 4.2 5.5 94.9 0.7939 CURVE 39 256.44 4.121 100 0.53 6.6 13.3 13.5 103.8 0.8551 76.55 0.7058 329.76 5.343 200 2.00 2.00 21.5	6.3 64.7 0.7207 265.20 3.656* 1194.01 1.925 10 0.41 4.2 7.2 68.4 0.766 2047 4.487 245.83 3.060 50 0.41 6.2 8.5 94.0 0.766 CURVE 39 286.44 4.121 100 0.53 8.6 12.1 95.0 0.7904 76.55 0.7058 329.76 5.343 200 2.00 2.00 21.5  ***Spown in figure.**			234.48			
6.3 86.7 0.7552 294.75 4.487 214.21 2.945* 10 0.41 4.2 7.2 88.4 0.7666 20.7666 50 0.41 6.2 8.5 9.4 0.7666 20.709 226.83 3.060 50 0.41 6.2 12.1 95.0 0.7904* 76.55 0.7058 329.76 5.343 200 2.00 21.5	6.3 84.7 0.7552 294.75 4.487 214.21 2.945* 10 0.41 4.2 7.2 68.4 0.7566 2.45.83 3.050 5.0 0.41 6.2 8.5 94.0 0.7939 <u>CURVE 39</u> 286.4 4.121 100 0.53 8.6 13.5 103.8 0.8351 76.55 0.7058 329.76 5.343 200 2.00 21.5			265.20			
7.2 58.4 0.7666 245.83 3.050 50 0.41 6.2 8.5 94.9 0.7939 <u>CURVE 39</u> 256,44 4.121 100 0.53 8.6 12.1 95.0 0.7904 76.55 0.7058 329.76 5.343 200 2.00 21.5	7.2 88.4 0.7666 CURVE 39 245.83 3.060 50 0.41 6.2 6.5 94.0 0.7939 CURVE 39 256,44 4.121 100 0.53 8.6 12.1 95.0 0.7904• 76.55 0.7058 329.76 5.343 200 2.00 21.5  s blown in figure.			294.75			
8.5 94.9 0.7939 CURVE 39 286.44 4.121 100 0.53 8.6 12.1 95.0 0.7904• CURVE 39 302.62 4.863* 150 1.00 13.3 15.5• 103.8 0.8551 76.55 0.7058 329.76 5.343 200 2.00 21.5	8.5 94.0 0.7939 CURVE 39 256.44 4.121 100 0.53 6.6 12.1 95.0 0.7904 76.55 0.7058 329.76 5.343 200 2.00 21.5  sebown in figure.						
12.1 95.0 0.7904* 302.62 4.563* 150 1.00 13.3 15.5* 103.8 0.8351 76.55 0.7058 329.76 5.343 200 2.00 21.5	12.1 95.0 0.7904* 76.55 0.7058 329.76 5.343 200 2.00 21.5 21.5 51.5 51.5 51.5						
15.5* 103.8 0.8351 76.55 0.7058 329.76 5.343 200 2.00 21.5	15.5* 103.8 0.8351 76.55 0.7058 329.76 5.343 200 2.00 21.5 21.5 st shown in figure.	_					
				76.55			
	tor shown in figure.						

	a	CURVE 76 (cont.)	31.9	35.	38.2	39.3		1.6.1	50.1	75		CURVE ::			10.4	10.01	19.5	36.4	37.3	3.5	38.9			· ·	7.07	5.5	•	CURVE 78		4.1*		n (	r, u		9 9 5	0 0	L.	32. 5	35.3	35.0	42.6	44.6	£8.3	51.3	×.
(penuj	1	CURVE	1962	1033	12	0.1	1250	1329	1378	1416			606	1 5	573	653	10.	918	295	107	1085	0611	1206	000	140.6	177		5	}	5.	7 8	200	2 3	4 C		20%	₹.	1003	1067	1158	1274	13%	1370	1428	3.1
(Temperature Dependence) (continued)	T A	CURVE 71	293 4.66#	ın.				718 19.02 807 23.40		CUBVE 72		293 4. 584		678 15.00		755 20.20			CURVE 73		4 0.54		300 4.03		CURIE 14		17 C 7.7	300 6.03		CLRVE 75		20.40	500 000		25 3.18.10				452 10.1						
RYLLIUM Be	Q.	(cont.)	28.81	38.30	42.20	45.60	;	. es	4.70*	1.43*	10.82	15.03	20.41	24.83	40.90	44.80		69 3		4.56*	4.00°	4.65	6 03	9 6	3.00	20.00	24.20	:	E 70		<b>4.</b> 66*	40.70	*	# 75 0 0	5.01	15.30	16.00	16.80	18.70	22.80	24. 60				
INITY OF BE	H	CURVE 67 (cont.	959.3	1133	1208	1268		CURVE 68	5 266	396	495	626.5	778.2	1107 5	1172	1266		CLRVE 69		293	293	293	404	7.5	#07 231	4 0	000	3	CURVE 70		293	200	200	307	4.2	1 2	641	663	713	808	870				
CTRICAL RESIST	a	3 (cont.)	40.66	46.90		2		4. 50 5. 50 8. 52 8. 53	12.32	13.20	24.03	29.92	39, 10	0T -6.6	E 65	1	4.61*	6.88	10.18	15.15	20.42	29.72	30.12	37.10	44.50	99 6	3[	4.25*	7.10	10.74	14. 42	18,93	24.52	22.50	4 50	3	E 67		4.72	7.40	10.95	16.95	19.60	25.15	
ON THE ELE	<b>(-</b>	CURVE 63 (cont.	1173.5	1283		CURVE		295.2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	641.3	864.3	1010.1	1158	2421	CURVE		298.6	374.3	483.4	630	169	20 CO	199	1217	1739	טו שוום.וט		295	396	506.3	614.2	746.2	883.2	1112.5	1976	2	CLRVE 67		299.3	393	500.5	665. 5	739.3	876.3	
EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BERYLLIUM	a	CURVE 58.	0.243	3. 5004		CURVE 59	,	3.60	CTRVE 60*		4.38		CURVE 61		1.0	1.7	2.7	3.0	4.3	4.6	* 6	5.2	63 31.0.1.0	F 92	4.1	e u	, r	8.5	18.3	20.3	22.4	24.5	<b>76.4</b>	רופ לים	21	4.05	6.90	11.22	14.98	15.53	21.30	24.83	30.22	35.60	
	۲	CUR	20.2	273.2			;	293	21.5		293		CCR	4	- 92	191	202	215	238	251	282	305	1010		970	200	9 (5)	123	727	900	890	156	30	71.01.5		295.1	305.5	526.3	635.5	677	812	006	1012.5	1099	
TABLE S.		_						_ *	,																																				
	a	CURVE 34 (cont.)	0.094	3	0, 031	0, 000	0.656	0.020		201	0.145	0.155	0.451	0.00	0.903	1.14	1.35	1.35*	1.36	2.21	2 : 2 :	200	3. 534		÷ "	\$ J.C. W	5 6	:	VE 55	;	2.43	70.7		92 3.14.13		0.21	0,297	3, 50		CLPVE 57		0.407	6. 455	3, 700	
	<b>(-</b>	CURVE	93.3	27.2	25. <b>4</b>	31.6	35.0	۵ ا ا	4	5	1. 2	E) E	115.4	124.	141.9	151.4	162.9	167. 5	177.0	157.5	155.4	211.3	274.5		7 6 6 6	0.00	25.61		CURVE	;	20.2 20.3	20.2	2:5:2	4.10		20.2	8	273.2		CLT	1	20.2	50.2	273.2	

" Not shown in figure.

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4.8	6.9	15.5	26.3	39. C	32.9	34.1	33.7	32.9	36.5	34.6	39.1	42.8	4.°.	47.0
ဗ္ဗ	38	585	617	ניט	7:30	151	<del>,</del> 91	5.5	1033	1163	1257	7.27	1354	1409

CLRVE 50

10.1 12.0 36.6 37.8 41.7 8.9 8.9 030 454 554 1165 11267 11393 11393 11393

\* Not shown in figure.

## 4.2. Magnesium

Magnesium, with atomic number 12, is a silvery-white, light, and fairly tough metal. It has a close-packed hexagonal crystalline structure with a density of 1.74 g cm<sup>-3</sup> at 293 K, which is 35% lighter than aluminum. It melts at 922 K and boils at about 1364 K. Its critical temperature has been estimated to be 3537 K. Naturally occuring magnesium is composed of three stable isotopes, the most abundant being <sup>24</sup>Mg, which constitutes 78.7%. Five other radioactive isotopes are known to exist. Magnesium is the seventh most abundant element in the continental crust of the earth (2.33% by weight).

## Temperature Dependence

There are 59 sets of experimental data available for the electrical resistivity of magnesium. The information on specimen characterization and measurement condition for each of the data sets is given in Table 7. The data are tabulated in Table 8 and shown in Figures 4 and 5. Determinations of the electrical resistivity for both the solid and liquid phases cover continuously the temperature range from 1 to 1171 K.

Since monocrystalline magnesium is an anisotropic metal, resistivity values will vary with the direction of the resistivity measurements relative to the hexagonal axis of the crystal. Goens and Schmidt [35-37] (curves 46-59), Alderson and Hund [38] (curves 41 and 42), and Nichols [8] (curves 12-17) have made measurements on single crystals up to 473 K.

Only one data set is available for amorphous magnesium. Ferrier and Herrell [39] (curve 44) have measured the electrical resistivity of an amorphous specimen, which was produced by vapor quenching at liquid nitrogen temperature (curve 44). At 273 K the electrical resistivity of amorphous magnesium is about 4.5 times that of the polycrystalline material.

The resistivity minimum apparent in the results of Rorschack and Herlin [40] (curve 11), Spohr and Webber [41] (curves 19 and 20), and Sharkoff [42] (curves 38-40), can be attributed to an impurity effect caused by trace amounts of certain transition metals in solid solution [43].

Most earlier determinations of the electrical resistivity of polycrystalline magnesium resulted in higher resistivities than the recent ones. These results can be explained by the lower purity of the specimens. The present recommended values are based on the data of Roll and Motz [44] (curve 8), Delaplace et al. [45] (curves 23 and 24), Das and Gerritsen [46] (curve 29), Hedgeock and Muir [47] (curve 32), Seth and Wood [48] (curve

34), and Powell, Hickman and Tye [49] (curves 36 and 37). A least-mean-square-error fit to weighted values of  $\rho^-\rho_0$ , uncorrected for thermal expansion of the material, was made with the modified Bloch-Grüneisen equation (8) from 20 to 900 K. Weights are assigned to individual data sets in such a way that they have approximately equal weight at the low and high temperature range. The following results were obtained for the coefficients in equation (8):

$$S_1$$
  $S_2$   $S_3$   $(\theta_R)_0$  C P  $6.83 \cdot 10^{-8} \Omega$  m  $-0.302 \cdot 10^{-8} \Omega$  m  $0.141 \cdot 10^{-8} \Omega$  m 426 K 0.044 1.90

The Debye temperature deduced from the specific heat measurements is  $396\pm54~\rm K$ , in rough agreement with our  $\theta_R$ . Correction to the fitted values for thermal linear expansion yielded the final recommended values.

The recommended electrical resistivity values for single crystals of magnesium as measured along the c-axis are based on the data of Alderson and Hund [38] (curve 41), Toens and Schmidt [35] (curves 46-59), and Nichols [8] (curve 17). A least-mean-square-error fit to their data for  $\rho$ - $\rho$ 0 was made with the modified Bloch-Grüneisen equation (8) from 15 to 472 K. The following values were found for the coefficients in equation (8):

$$S_1$$
  $S_2$   $S_3$   $(6_R)_0$  C P 5.06·10<sup>-8</sup>Ω m 0.670·10<sup>-8</sup>ζ m 0.074·10<sup>-8</sup>ζ m 363 K -0.109 1.90

The resulting values were corrected for thermal linear expansion to get the final recommended values. The recommended values above 472 K are estimated.

The recommended electrical resistivity values for single crystals measured perpendicular to the c-axis are based on the data of Alderson and Hund [38] (curve 42), Goens and Schmidt [35] (curves 46-59), and Nichols [8] (curve 12). A least-mean-square-error fit to their data for  $\rho$ - $\rho_0$  was made with the modified Bloch-Grüneisen equation (8) from 15 to 469 K. The following values were found for the coefficients in equation (8):

$$S_1$$
  $S_2$   $S_3$   $(\theta_R)_0$   $C$   $P$  8.04·10<sup>-8</sup>Ω m -1.06·10<sup>-8</sup>Ω m 0.349·10<sup>-8</sup>Ω m 522 K 0.202 1.90

The resulting values were corrected for thermal linear expansion to get the final recommended values. The recommended values above 469 K are estimated.

By using equation (7) and the above single crystal results, the resistivity values for the polycrystalline material can be calculated. The resulting calculated values are within ±3% of the recommended values obtained from the experimental data for polycrystal-

line specimens. This indicates that the grains in the polycrystalline specimens were essentially random in orientation.

There are three data sets available on the electrical resistivity of magnesium in the liquid state. Van Zytveld et al. [50] (curve 28) found a very small temperature dependence of the electrical resistivity. Scala and Robertson [51] (curve 43) found a weak negative temperature dependence, while Roll and Motz [44] (curve 8) found a positive temperature dependence. Comparision with the electrical resistivity data of other alkaline earth elements in the liquid state suggests that the electrical resistivity of liquid magnesium should have a weak negative temperature dependence. The data of Scala et al. have been normalized by matching their values with the data of Van Zytveld et al. at the melting point, 922 K. The normalized values from 922 to 1171 K were fitted with a linear equation to obtain:

$$\rho(T) = 26.1 - 0.0016 \times (T - 922) \qquad 922 \text{ K} \leq T \leq 1200 \text{ K} \qquad (12)$$

where  $\rho$  is in units of  $10^{-8}\Omega$  m and T in K. At the melting point (922 K), the electrical resistivity of magnesium in the liquid state is about 76% higher than that of the solid state.

The recommended values for the total and intrinsic electrical resistivities are listed in Table , and those for the total resistivity are also shown in Figures 4 and 5. The recommended values are corrected for the thermal expansion. The correction amounts to -0.48% at 1 K, -0.20% at 200 K, 0.57% at 500 K and 1.90% at 900 K. The recommended values for the total electrical resistivity are for 99.9<sup>+</sup>% magnesium and those below 100 K are applicable only to specimens with residual resistivities of  $0.008 \cdot 10^{-8} \Omega$  m(//to c-axis),  $0.01 \cdot 10^{-8} \Omega$  m ( $\pm$  to c-axis), and  $0.0062 \cdot 10^{-8} \Omega$  m (polycrystalline). The uncertainty in the recommended values for the total electrical resistivity is believed to be within  $\pm 8\%$  below 30 K,  $\pm 5\%$  from 30 to 100 K,  $\pm 3\%$  from 100 to 600 K,  $\pm 5\%$  from 600 to 922 K, and within  $\pm 10\%$  above 922 K. Above 30 K the uncertainty in the recommended values for the intrinsic resistivity is slightly higher than that in the total electrical resistivity, because of possible deviations from the Matthiessen's Rule; below 30 K the values are very uncertain and are not listed in the table.

TABLE 6. RECOMMENDED ELECTRICAL RESISTIVITY OF MAGNESIUM (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8} \Omega m$ ; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8} \Omega m$ ]

			Solid			
T	// to c	-axis	⊥ to c	-axis	Polycr	ystalline
•	ø	$ ho_{ ext{i}}$	ρ	$\boldsymbol{\rho_i}$	ρ	$ ho_{\mathbf{i}}$
1	0.0080*		0.0100*		0.0062*	
4	0.0080*		0.0100*		0.0062*	
7	0.0082*		0.0100*		0.0064*	
10	0.0086*		0.0108*		0.0069*	
15	0.0101*		0.0130*		0.0086*	
20	0.0136*		0.0175*		0.0123*	
25	0.0204*		0.0255*		0.0193*	
30	0.0320	0.0240	0.0383	0.0283	0.0309	0.0247
35	0.0502	0.0422	0.0572	0.0472	0.0488	0.0426
40	0.0760	0.0680	0.0837	0.0737	0.0744	0.0682
45	0.110	0.102	0.119	0.109	0.109	0.102
50	0.151	0.143	0.164	0.154	0.151	0.145
60	0.255	0.247	0.282	0.272	0.261	0.255
70	0.381	0.373	0.430	0.420	0.398	0.392
80	0.520	0.512	0.603	0.593	0.557	0.551
90	0.671	0.663	0.789	0.778	0.728	0.722
100	0.827	0.819	0.983	0.973	0.908	0.902
110	0.986	0.978	1.18	1.17	1.10	1.09
120	1.15	1.14	1.38	1.37	1,28	1.27
130	1.31	1.30	1.58	1.57	1.47	1.46
140	1.47	1.46	1.77	1.76	1.66	1.65
150	1.63	1.62	1.96	1.95	1,84	1.83
175	2.02	2.01	2.44	2.43	2,30	2.29
200	2.42	2.41	2.90	2.89	2.75	2.74
225	2.81	2.80	3.35	3.34	3, 19	3.18
250	3.19	3.18	3.80	3.79	3.61	3.60
273.15	3.54	3.53	4.20	4.19	4.05	4.04
293	3.84	3.83	4.55	4,54	4.39	4.38
300	3.94	3.93	4.67	4.66	4.51	4.50
350	4.68	4.67	5.52	5.51	5.36	5.35
400	5.42	5.41	6.39	6.38	6.19	6.18
450	6.16	6.15	7.25	7.24	7.03	7.02
500	6.90	6.89	8.09	8.08	7.86	7.85
550	7.53	7.52	8.93	8.92	8.69	8.68
600	8.35	8.34	9.76	9.75	9.52	9.51

<sup>\*</sup> Provisional Values

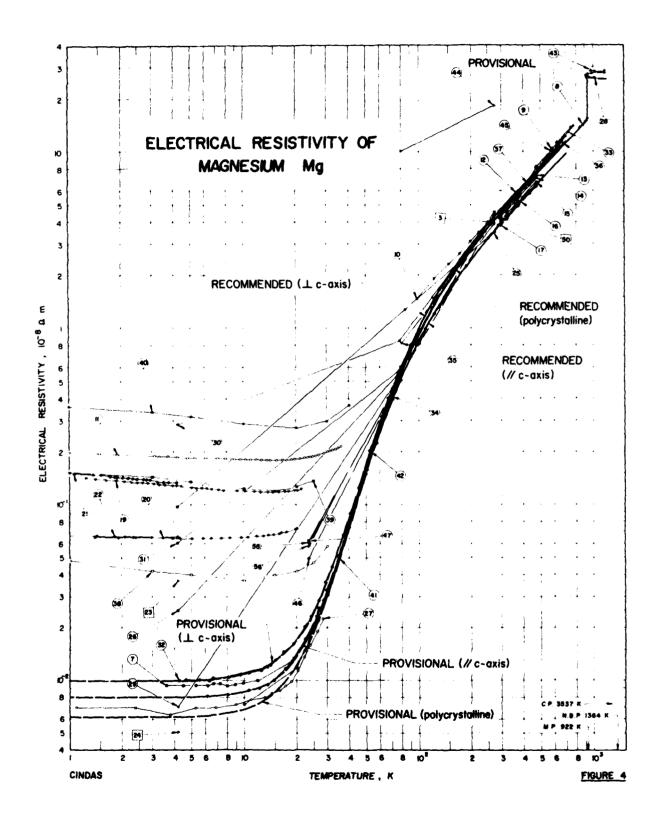
The recommended values for the total electrical resistivity are for 99.9 magnesium and those below 100 K are applicable only to specimens with residual resistivities of  $0.008 \cdot 10^{-8} \Omega$  (//to c-axis),  $0.01 \cdot 10^{-8} \Omega$  m ( $\perp$  to c-axis), and  $0.0062 \cdot 10^{-8} \Omega$  m (polycrystalline).

TABLE6. RECOMMENDED ELECTRICAL RESISTIVITY OF MAGNESIUM (Continued) (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8} \Omega m$ ; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8} \Omega m$ ]

			Se	ol i <b>d</b>			Liq	uid
T	// to	c-axis	⊥ to c-	axis	Polyci	rystalline	T	
1	ρ	$ ho_{\mathbf{i}}$	ρ	$o_i$	ρ	$ ho_i$	1	O
650	9.07	9.06	10.6	10.6	10.4	10.4	922	26.1*
700	9.78	9.77	11.4	11.4	11.2	11.2	950	26.1*
750					12.0	12.0	1000	26.0*
800					12.8	12.8	1050	25.9*
850					13.6	13.6	1100	25.8*
900					14.4	14.4	1150	25.7*
922					14.7	14.7	1200	25.6*

<sup>\*</sup> Provisional Values.



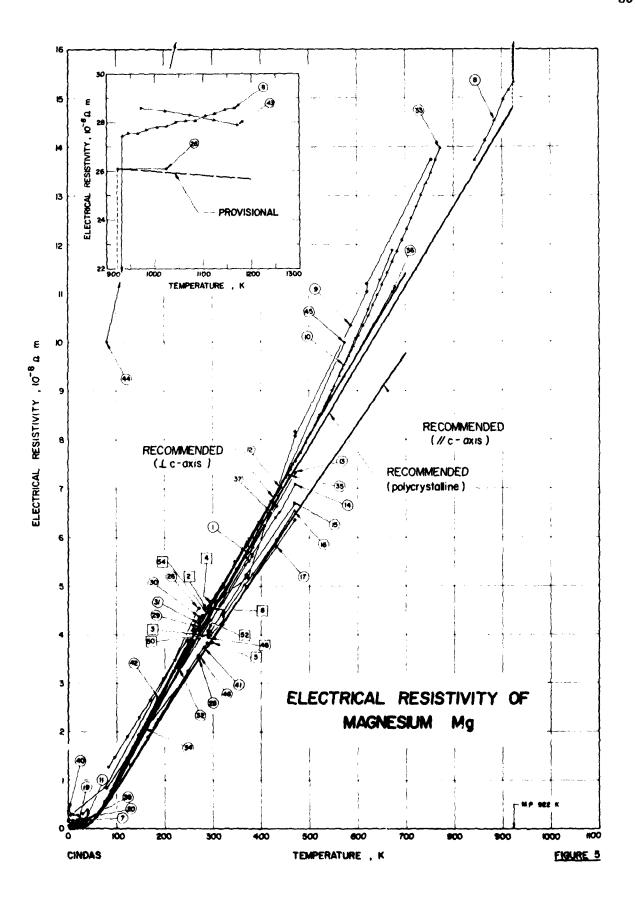


TABLE 1. NEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM Mg (Temperature Dependence)

1962 293 Mg Pu 1962 293 Mg Spe 1963 273 Mg Pu 1960 300 Mg Pu 1960 300 Mg Pu 1960 3-26,300 Mg Pu 1960 3-26,300 Mg Pu 197 R 844-1166 99. 1954 V 293-753 99. 1955 B 273-497 Sin 1955 B 273-497 Sin 1957 300 99.		Author (s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
1962 293 Mg Spe 1943 273 Mg Pu 1961 M 299 Mg Pu 1960 300 Mg Pu 1960 300 Mg Pu 1960 3-26,300 Mg Pu 1960 3-26,300 Mg Pu 1960 1952 M 293-753 99. 1952 W 293-753 Pu 1953 B 273-497 Sin 1955 B 273-497 Sin 1957 300 99.	2	Lorentz, L.	1881		273,373	Mg	Pure.
1961 Mg 273 Mg Pur 1960 1961 Mg 299 Mg Pur 1960 300 Mg Mg Pur 1960 300 Mg Mg Pur 1960 300 Mg Mg Mg Pur 1960 300 Mg	Ā	Das, K.B. and Gerritsen, A.N.	1962		293	Mg	Spectrographically pure magnesium (Johnson-Matthey, 11d., 1ab. No. 4220); samples were alternately annealed at 400 C for 90 min; the samples varied in width from 0.15 to 0.311 cm, in thickness from 0.0037 to 0.0167 cm, and in length from 3.59 to 10.55 cm.
1960 Mg Mg Pur Pur 1960 300 Mg	Š	and, v.	1943		273	Mg	Pure.
1960   300   Mg_1   Pur     1960   300   Mg_//   Pur     1960   3-26,300   Mg_//   Pur     1957   R   844-1166   99.     1958   W   293-753   99.     1958   B   273-497   Shr     1955   B   273-497   Shr     1957   300   99.	Ø	Baveja, K. D.	1961	*	299	Mg	Pure; the electrical resistivity was measured by magnetic damping method; unannealed specimen; diameter 0.2497 cm, thickness 0.0858 cm disc sample.
1960 300 Mg// Pur 1960 3-26,300 Mg// S00 1990 1992 404-1166 999.	×	uczynski, G.C.	1960		300	T SM	Pure.
1957 R 844–1166 99.  1924 V 293–753 99.  14. 1951 1.5–36 Pur  1955 B 273–497 0.0  1955 B 273–497 Sin  1955 B 273–497 Sin  1955 B 273–497 Sin  1955 B 273–497 Sin  1957 300 99.	×	uczynski, G.C.	1960		300	Wg//	Pure.
1957 R 944-1166 99.  1924 V 293-753 99.  14.4. 1951 1.5-36 Puu  1955 B 273-497 0.0  1955 B 273-497 S5in  1955 B 273-497 S5in  1955 B 273-497 S5in  1957 300 99.	21 4	Hedgeock, F.T., Muir, W. B. and Wallingfold, E.	1960		3-26, 300		<0.001 each Al, Fe, Mn, Pb, Sl, Zn, <0.01 each Ca, Sn, <0.0005 Ni; the sample was amealed at 450 C for 46 hr in atm of helium gas. Reported error 1%.
1908 84-673 Pur 14. 1951 1.5-36 Pur 1955 B 273-497 0.0 1955 B 273-497 Sim 1955 B 273-497 Sim 1957 300 899	щ.	Roll, A. and Motz, H.	1957	æ	844-1166		99.8 pure; in solid and liquid states; M.P. 923 K; data corrected for thermal linear expansion. Reported error 1%.
1908   84-673   Pur   Pur   1.5-36   Pur   Pur   1955   B   273-497   Co.0   Co.0	•,	Scholleld, F. H.	1924	>	293-753		99.6 purity magnesium specimen was extruded to 0.75 in. diameter from a billet 5 in. in diameter; amealed at 360 C for 6 hr, and allowed to cool slowly; density at 294 K = 1.75 gm/cm³. Reported error 1%.
1.5-36 Pure 1955 B 273-497 0.0 G 1955 B 273-497 Sim 1957 300 99.	•	itecolal, G.	1908		84-673		Pure.
1955 B 273-497 0.0 1955 B 273-497 Sin 1957 300 99.	-	torschach, H. E. and Herlin, M.	A. 1951		1.5-36		Pure, bulk cylindrical sample; the resistivity was obtained by measuring the mutual inductance of two coaxial coils surrounding the sample.
B 273-497 B 273-497 B 273-497 B 273-497 B 273-497 1-25 Mg (Fe)	•••	Nichols, J. L.	1955	<b>m</b>	273-497		0.0036 C, 0.0005 Fc, 0.0002 Min, 0.001 Ca, 0.0019 each K, Na, 0.0004 H, <0.01 Zn, <0.0005 Pb, <0.0001 each Al, Cu, Sr, B, <0.001 each Sl, Sa, <0.0003 Ni; single crystal samples, 0.50 in. in diameter and 7 in. long, were grown in a gradient furnace; a Kelvin Double Bridge was used in conjunction with a high-sensitivity D'Arsonval rype galvanometer for the resistance measurements; cos² ≥ 0.002, ∅ is the angle between sample's axis and c-axis.
1955 B 273-497 1955 B 273-497 1955 B 273-497 1957 300	#1	Cichols, J. L.	1955	Ø	273-497		Similar to the above specimen; cost : " 0.213.
1955 B 273-497 1955 B 273-497 1957 300 1957 1-25 Mg (Fe)	••	Vichols, J. L.	1955	Ø	273-497		Similar to the above specimen; $\cos^2 \phi = 0.430$ .
1955 B 273-497 1955 B 273-497 1957 300 1957 1-25 Mg (Fe)	•	debols, J. L.	1955	Ø	273-497		Similar to the above specimen; $\cos^2 \phi = 0.667$ .
1955 B 273-497 1957 300 1957 1-25 Mg (Fe)	•	Sichols, J. L.	1955	Ø	273-497		Similar to the above spectmen; $\cos^2 \theta = 0.841$ .
1957 300 1957 1-25 Mg (Fe)	<b>4</b>	sichols, J. L.	1955		273-497		Similar to the above specimen; $\cos^2 \phi = 0.990$ .
1957 1-25 Mg (Fe)	<b>V</b> 1	alkovitz, E.I.,	1957		300		99.98 pure, annealed extruded polyctystalline stripes; specimen width from 0.412 cm to 0.640 cm, thickness from 0.212 cm to 0.240 cm, and length from 9.54 cm to 29.3 cm; resistivity was obtained by using the Reeves modification of Kelvin double buings.
	<b>6</b> 7	pohr, D.A. and Webber, R.T.	1957		1-25	Mg (Fe)	99.98° Mg. 0.013 Fe. 0.0013 Pb. 0.0023 Mn; cold-worked polycrystal from Johnson-Matthey and Co., London, England; the rod specimen was about 3.2 mm in diameter and 9 cm long. Reported error 0.3%.

. Not shown in figure.

TABLE 7. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM Mg (Temperature Dependence) (continued)

Cur.	Ref.	Author(s)	Year	Method Used	Temp. Range, K	Nume and Specimen Designation	Composition (weight percent), Specifications, and Remarks
ຊ	ş	Spohr, D.A. and Webber, R.T.	1957		1-25	Mg (Mn)	99.95* Mg, 0.043 Mn, 0.001 cach Fe. Si, 0.0011 each Pb, Sn, 0.0002 Al, 0.0001 each Cu, Ni, 0.0046 Zn, 0.0012 Ca; annealed polycrystal rod, 3.2 nm in diameter and 9 cm long; prepared by Dow Chemical Co. Reported erros 0.3°.
ដ	09	Hein, R.A. and Falge, R. L.	1957		0.3-4.3	Mg (Fe)	99.98* Mg, 0.013 Fe, 0.0023 Ma, 0.0013 Pb; cold-worked polycrystal red 3.2 mm in diameter and 9 cm long; specimen was obtained from Johnson- Matthey and Co., England.
23	09	Hein, R.A. and Falge, R. L.	1957		0.3-4.3	Mg (Ma)	99.95 Mg, 0.043 Mn. 0.001 each Fe, Si, 0.0011 each Pb, Sn, 0.002 M, 0.0001 each Cu, Ni, 0.0043 Zn, 0.0012 Ca; annexied polycrystal rod 3.2 mm in diameter and 9 cm long; specimen was prepared by Dow Chemical Co.
23	45	Delaplace, J.,	1968		4.2,300	Mg 1	99.95 pure wire specimen; 0.2 mm in diameter; $R_{300 \text{ K/R4}, 2 \text{ K}}$ = 120.
2	<b>4</b>	Delaplace, J.,	1968		4.2,300	Mg 2	99, 999 pure zone refined wire specimen; 0.2 mm in diameter; $R_{300}~\rm K^-R_4$ 2 K = 870.
133	61	Hedgecek, F.T. and Muir, W.B.	1961		4.2,273	Mg	0.04 Ma, $R_{4.2}/R_{273} = 0.028$ .
58	62	Bijvoet, J., dellon, B., Dekker, J.A., and Rathenau, G.W.	1962		4.2-273	D Mg	Pure magnesium sample was supplied by Dow Chemical international.
£;	2	Panova, G.Kh., Zhernov, A.P., and Kutaitsev, V.I.	1968	<	1.2-20	Mg	Pure magnesium wire sample 1 mm in diameter and 50 mm in length was pre- pared by drawing through a die and annealing subsequently is _ belium atm at 350 C, Reported error 1.25.
60 61	00	Van Zytveld, J. B., Enderby, J. E., and Collings, E. W.	1972	∢	924,1023	Mg	99.98 pure, < 0.001 each Al, Si, Zn, < 0.005 each Cu. Pb, 0.033 Fe. 0.032 Mr, < 0.0041 Ni, < 0.005 each C, Cy, < 0.005 Hg. 0.0015 Mg sample was obtained from Noch Light Lab. Ltd. Reported error 4%.
ន	4	Das, S. B. and Gerritsen, A. N.	1964	<	4.2-273	Mg	<0.01 Ca, <0.02 Zn, <0.001 each M, Cu, 0.001 Fe, 0.0011 Ma, <0.002 Ni, 0.0005 Pb, <0.001 each Si, Ni specimen was supplied by Dow Metal Products Co, polycrystalline specimen: R <sub>4,2</sub> /R <sub>273</sub> = 1.7 x 10 <sup>-3</sup> .
8	<b>4</b>	Das, S.B. and Gerritsen, A.N.	1964	<	4.2-273	0,16 Li	0.16 LJ, <0.001 each AJ, Cu, Ma, Zn, <0.01 each Ca, Sn, <0.0005 Fe, 0.0009 Ni, <0.002 Pb, <0.005 Si; polycrystalline specimen was supplied by Dow Metal Products Co; R4, 2/R <sub>273</sub> = 0.0455.
ដ	\$	Das, S.B. and Gerritsen, A.N.	1964	<	4.2-273	0.047 B	0.047 Sp, < 0.001 cach Al, Cu, Fe, Min, < 0.01 Ca, < 0.0003 sach Ni, Pb, < 0.0001 Si, 0.003 Zn; polycrystalline specimen was supplied by Dow Metal Products Co; R4, 2/Rgr3 = 0.0144.
33	4	Hedgeock, F.T. and Muir, W.B.	1964	Ω	4.27-571.2	728	Pure; specimen was rolled into 0.01 in. strips, etched, cut into 0.125 x 4 in. and anneaded in a helium atm at 7 cm of Hg at 450 C for 12 hr; $R_{\star, c}/R_{27.3}$ = 2.467 x 10 <sup>-3</sup> .
ន	2	Grube, G. and Burkhardt, A.	1929	ф	373-773		99.93 Pure; 0.019 Si, 0.052 Fc, and trace of Al, Cu; the electrical resistivity was measured in 1 atm press re of very pure hydrogen.
8	<b>4</b>	Seth, R. S. and Woods, S. B.		1970	10-295		<0.0014 impurity; obtained from Johnson Matthey, and Mallory, Ltd., Canada; prepared by Dow Chemical Co. from sublimed magnessium that was at least 99.98 pure after fabrication; slightly non-uniform 0.035 in. diameter wire drawn through 0.032 in. diamond due to produce uniform, smooth wire; annealed at 350 C for 8 hr in 10 torr H <sub>2</sub> .
ક્ષ	65	Szebler, J.	1929		80-460		Pure; 3 cm x 1.23 cm.

TABLE 7. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM Mg (Temperature Dependence) (continued)

Cur. Ref. No. No.	Ref.	Author(s)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
8	ş	Powell, R.W., Hickman, M.J., and Tye, R.P.	1964		293-673	Mg 1	99.95 Mg, 0.033 Al, 0.012 Zn; 1.9 cm diminiter x 30 cm long; supplied by the Metallurgy Division of the National Physical Laboratory; forged and heat treated.
H	6	Powell, R.W., or al.	1964		293-423	Mg 2	99.98 Mg, 0.017 Al, 0.004 Zn; 0.635 cm diameter x 10 cm long; supplied by Messrs. Johnson, Matthey and Co., Ltd.
<b>8</b> .	. 2	Sharkoff, E.G.	1953		1.0-30 &	Sample No. 765	99.95 Mg, 0.01 Mn, 0.003 Zn, 0.0012 Pb, 0.001 Ca, < 0.001 each Si, Sp, 0.0008 Fe, 0.0002 Al, < 0.0001 each Cu, Ni; 0.310 cm diameter x 9.03 cm long.
8	42	Sharkoff, E.G.	1953		1.0-25 S	Sample No. 767	99.95 Mg, 0.043 Mn, 0.0043 Zn, 0.0012 Ca, 0.0011 cach Pb, Sq, 0.0010 Fe, <0.001 Si, 0.0002 Al, <0.0001 each Cu, M; 0.307 cm diameter x \$.93 cm long.
\$	<b>2</b>	Sharkoff, E.G.	1953		1.0-40 S	1.0-40 Sample No. 370	99, 87 <sup>+</sup> Mg, 0.12 Mn, 0.0036 Zn, 0.0014 Pb, 0.0011 Fe, <0.001 each Si, Sn, 0.0006 Ca, 0.0002 Al, <0.0002 Ni, 0.0001 Cu; 0.305 cm diameter x 5.35 cm long.
<b>7</b>	m ei	Alderson, J.E.A. and Hurd, C.M. 1975	1975	<	3-300	Mg 1, Mg 2	99.9 purity; single crystals; for Mg 1 specimen - 0.315 mm thick, probe separation 6.325 cm, angle between c-axis and sample's axis θ = 6.35°, ρ <sub>στ3</sub> K, Pres * 420; for Mg2 - 0.295 mm thick, probe separation 5.36 cm, θ = 70.5° ρ:3K/ρres = 440; longitudinal resistivity (ρ <sub>γ</sub> ) data were obtained.
42	38	Alderson, J.E.A. and Hurd, C.M. 1975	1975	<	3-300	Mg 1, Mg 2	Same as the above specimen; transverse resistivity (p1) data were obtained.
<b>\$</b>	25	Scala, E. and Robertson, W.D.	1953	∢	973-1171		99, 975 Mg, 0. 01 Cu, 0. 004 Al, 0. 003 Pb, and 0. 003 Si; in liquid state; supplied by Dominion Magnesium, Ltd.; contained in a graphite tube about 0.6 cm 1.D. and 13 cm long.
3	39	Ferrice, R.P. and Herrell, D.J.	1970		80,273		Pure; amorphous specimen was obtained by capor quenching at liquid nitrogen temperature; data was extracted from the figure.
45	67	IIcal, T.J.	1958		273-573		Pure; density 1, 7398 g cm <sup>-3</sup> ; melting point \$23 K; boiling point 1353 K.
<del>p</del>	35	Goeas, E. and Schmid, E.	1936	-	20.35-373.15	s Mg 50	Pure; single crystal specimens were grown from the melt of 99.95 pure starting material; cylindrical specimen is about 4, 53 cm in length and 0, 1369 cm in radius; angle ¢ between sample axis and the bezagonal axis is 14:30°, resistance ratio are reported, the resistivity are calculated from p(291.15 K) = 3.813 · 10 <sup>-8</sup> Ωnn.
41.	35	Gocas, E. and Schmid, E.	1936		20. 35-373. 15	s XI	Similar to the above specimen except the specimen is about 14.36 cm in length, 0.2463 cm in radius; $\phi \approx 18^{\circ}20^{\circ}$ and $\rho(291.15\mathrm{K}) \approx 3.548 \cdot 10^{\circ}$ Gm.
<b>\$</b>	g	Goens, E. and Schmid, E.	1936		291.15	ΧΛ	Similar to the above specimen except the specimen is about 11.38 cm in length, 0.2452 cm in radius; and $\mathfrak{g}=29^\circ$ .
<u>3</u>	35	Coens, E. and Schmid, E.	1936		291.15	XIX	Similar to the above specimen except the specimen is about 9.193 cm in length and 0.1647 cm in radius; and $\rho \approx 34^{\circ}30^{\circ}$ .
	35	Goens, E. and Schmid, E.	1936		291.15	06	Similar to the above specimen except 0 = 49°.
214	99	Goens, E. and Schmid, E.	1936		291.15	XVI	Similar to the above specimen except the specimen is 6.304 cm in length, 0.16 cm in radius and $\phi = 52^{\circ}45^{\circ}$ .

Not shown in figure.

\* Not shown in figure.

TABLE 7. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM Mg (Temperature Dependence) (cominued)

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, j. j.	C.e. Ref. No. No.	Author (s)	Year	Method Used F	Temp. Range, K	Numer and Specimen Designation	Composition (weight percent), Specifications, and Remarks
3	R	35 Goeas, E. and Schmid, E.	1936		291.15	169	Similar to the above specimen except the specimen is about 6. 628 cm in length, 0.2002 cm in radius and $z=55^\circ20^\circ$ .
ħ	33	35 Couns, E. and Schmid, E.	1,36		291.15	<del>4</del> 6	Similar to the above specimen except the specimen is about 10, 36 cm in length 0.1765 cm in radius and $z=63^\circ$ .
ß	55	35 Gocas, E. and Schmid, E.	1936		291.15	85	Similar to the above specimen except the specimen is about §, 486 cm in length, 0.1838 cm in radius and $\varphi = 73^{\circ}$ 50 %.
15	iS.	Goens, E. and Schmid, E.	1936	20.	20.35-373.15	116	Similar to the above specimen except the specimen is about 8, 202 cm in length, 0, 2053 cm in radius, $\phi = 80^\circ$ ; resistance ratio at different temperatures were reported, the electrical resistivity data are calculated for $\rho(291.15~{\rm K}) = 4.492 \cdot 10^\circ$ ( $\rho$ ).
26	35	Goens, E. and Schmid, E.	1936	20.	20, 35-373, 15	188	Similar to the above specimen except p = \$2°; the electrical resistivity data are calculated from resistance ratio data and p(291.15 K) = 4.516 · 10° fm.
<b>t</b> 5	13	Goens, E. 226 Schmid, E.	1936	20.	20. 35-373. 15	162	Similar to the above specimen except the specimen is about 5, 445 cm in length, 0, 1919 cm in radius; the electrical resistivity data are calculated for resistance ratio data and $\rho(291.15~\mathrm{K}) = 4.492 \cdot 10^{-9}~\mathrm{Gm}$ .
<b>*</b>	36,37	36,37 Goens, E. and Schmid, E.	1931		291.15	٩	Pure; single crystal specimen; specimen's axis perpendicular to the bexagonal axis; resistivity temperature coefficient 0.00416/K (273-373 K).
869	36,33	36,37 Coens, E. and Schmid, E.	1831		291.15	<i>\</i>	Pure; single crystal specimen; specimen's axis parallel to the becagonal axis; resistivity temperature coefficient 0.00427/K (273-373 K).

TABLE 8. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM Mg (Temperature Dependence)

	٩	CIRVE 19 (com.)	0.1139	0.1189	0.1150		0.1.00	0.1214	0.1219	0.1231	CIRVE		0.0639	0.0055	0.0653	0.0651	0.0651	0.0048	0.0646	0.0647	0.0048	0.0648	0.0650	0.0653	9.00	7000.0	0.000	0.0679	0.0658	0.0692	0.0703	0.0725	0.0732		CLRVE 71	0.1692	0.1652	0.1675	0.1663	0.1647	0.1651	0.1606	0.1624	0.1613	
	٠	CLRVE	12.57	13.70	98 41		2 2 2	19.61	30.30	21.26	117	;	1.41	1.92	달	30.	3.46	1	3.5	5.85	6.51		98. 36 1	0.0	3 2	20.11	13.05	14:87	16.18	16.54	17.65	19.67	20. 22	;	3	0.24	0.25	0.33	0.28	9: .0	0.40	0.43	<b>7</b> .0	0.52	
ochement of	a	16	4.009	4.302	4.032		5 967	6.555		17	3, 853	4.225	4.992	5.813	6.361		184	4.45	<u>:</u>	5 19	]	0.1430	0.1412	0.1397	0.1385	0.1.10	0.1359	0.1340	0.1331	0.1321	0.1313	0.1303	0.1295	6.1.59	0.1281	0.1259	0.1250	0.1240	0.1233	0.1224	0.1216	0.1216	0.1200	0.1193	
> • • • • • • • • • • • • • • • • • • •	۲	CLRVE 16	297.5	323.1	367.9	200	133.1	471.7		CLRVE 17	297.5	323.3	373.7	433.1	472.3		CCRVE 18	300		CLRVE 19		1.25	1.42	1.63	3. c	50.0	77.6	2.65	 	3.07	3.30 3.30	3, 55	3.93	<b>4</b> . 14	4.40	, v,	5.71	6.17	6.51	7.11	7.63	9.13	10.11	11.55	
[ma]	<b>a</b>	(cont.)	0.2028	0.2059	0.2088	2155		12	j	4.578	4. 999 . 999	5.022	5.907	5.998	6.841	7.047	7. 500	13	1	4.431	4.468	4.822	5,603	5.808	6.245	4 . 0.4 1 . 0.4	1.331	14	1	4.306	4.677	5. 435	5.521	9.018	5.653	6. 526	7.091		15		4.080	4.439	4.48	5. 227	0.150
esistivity, p. 1	۴	CIRVE 11 (cont.						CURVE 12		297.5							468. s	CURVE 13		297.5			368,9					CURVE 14			323.7					440.8			CURVE 15					370.5	
[Temperature, T, K; Resistivity, p, 10-6 [m]	a	cont.)	7.132	7.576	8.031 8.031		536	10,030	0.672	11, 285	1. 69.5	11	1	0. 1996	0.1966	0.1946	0.1906	0,1890	0.1879	0.1868	0.1861	0.1850	0.1842	0.1835	0.1829	. 105.	0.1821	0.1813	0.1811	0.1808	0.1506	0.1805	0.1807	0.1812	0.1820	0.1839	0.1855	0.1867	0.1878	0.1891	0.1907	0.1929	0.1974	0. 2011	
[Temper	H	CURVE 10 (cont.			# CC		5. C.			648		CURVE 11		1.0	1.6	6 ·	 	, e,	4.2	<b>4</b> .8	m	6.1	_	<b>.</b>	ກຸ່		10.3						16.7						24.1			26.8	28.9	30.2	
	a	cont.)	15.34	27.47	27.30	20.	27.53	100	25.01	25.05	28.29	28.36	28.34	26. 39	28, 70			<b>.</b>	4.59	6. 194	6. 21	6.19	8.17	80.6	10.33	77.11	13.74	:	•	4	1.275	1.471	1.907	20.300	2.043	3.491	3, 694	4.312	4.700	5.0c9	5. 507	5.915	6.318	6. 735	
	۲	CLRVE 8 (co			ر د د د د د د د د د د د د د د د د د د د					1000							e avera		293.1	374.5							951.1		CURVE 10		35	86	123	9	173	223	248	273	298	323	348	373	398	423	
			ð	<b></b>			4 63 40 15	21.5			2			33			¥	2			55				0094	F.600.0	0.0094	0.0096	0.0006	0.0093	0.0005	0.0097	=	6.013	0.0186				ត	10	<u>.</u>	Ş	9		
	4	CURVE 1	273.15 4.09		6 3.10.10	7712	3 7 .00		CURVE 3		8.4 2.72	CLRVE 4		239 4.663	1	CLRVE	700		CLRVE 6		300 4.35		CLAVE 7	•	9.0		3,0	6.7	7.3 0.0	•	6	•	٠.		25.8	5	CURVE 9					204 14.35			

Not shown in figure.

TAB	TABLE 8. EXPERIM	LENTAL DATA ON	THE ELEC	EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM	IN OF MAC		g (Temperature	Mg (Temperature Dependence) (continued)	(pen	
a F	4	a	۴	Q	ī	Q	₽	a	H	a.
CULIVE 21 (cont.)	CURV	WE 26	CURVE	E 32	CLRVE	CURVE 33 (com.)		CURVE 36	CURVE	7
50.100	2	0.025	4.27	0.010	603	10.141	293	4.5	6. 17	0, C0-2
•	11	0.55	6.34	0.010	613	10.345	S:5	5.01*	) (2)	3.5
1.0	273	4.55	14.15	0.012*	623	10.558	ر د ا		10 % 60 %	20000
3		;	20.10	0.016	633	10.162	£13	300.0	10.6	0.00
0.1370	CCRO	(VE 27	27.56	0.051	653	11.198	673	11.04	11.25	0.60.9
1.01 0.1310	1.1	0.0070	41.32	0.085	663	11.436	•		12.36	c. 0091
1.53	2,5	0.000	59.30	0.257	673	11,661		CURVE 37	12.88	0.00931
1.75 0.1469	.5	0.000	79.9	0.530*	683	11.850	•		13.62	0.000
1.44 0.1138	5,3	0.0010	89.3	0.720	693	12.118	283	77.	70	0.000
13 6.1447	6.9	0.00.0	107.4	1.0.3*	703		253	9 in	15.92	0.01113
2.04 0.1440	⊃. n :	200.0	1.16 6	1.371	793	12 803	40.5	2.5	17.10	0.0115
2.19 0.1529	13.1	0.0080	177.1	2.342	733	13.039		• • •	17.62	0.01233
2.45 0.1413	14.4	0.0085	195.3	2.732*	743	13, 262	티	CURVE 38	19.23	0.0133
2.63 0.1401	16.0	6.003	230.5	3.310	753	13.498	•		21.60	T 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
	17.3	6.00.0	200	4.053	763	13.751	~+ C	0.048	# 0 m	
	18.6	0.000	292.2	4.368	773	14.000		0.040	00.90	0.0232
	20.3	0.0114	309.6	1,000		į	9	250.0	; ;	0.00333
	22.1	0.0136	329.8	4. U.C. r.		CURVE 34	3 5	0.030	9 (5) (5) (6)	0.0286
2007 O 07 10 0	B 577	0.0139	371.2	5.69.4	10	0.00732	ຸຊ	0.042	29.52	0.0027
	26.2	0.0190			200	0.01347	25	0.047	30.98	0.0379
+.15 0.1344	28.2	0.0225	CUR	CURVE 33	30	0.0311	စ	0.058	3.5 5.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7	0.0000
					) • u	0.530				0.000
CLRVF. 22	CURVE	E 28	373	5,843	99	0.2661	티	CURVE 39	300	0.06784
			200	610.9	70	0.4072	•	0.153	40.31	0.0803
0.27 0.0689	200	7.041.96	403	6 257	90	0, 56×3	4 ex	0.144	42.57	0.0571*
18540 O 05 0	501	70.1 70.1	5.14	6, 538	06	0.7443	'n	0,136	44.37	0.107
	CURVE	67 37	423	6.719*	100	0.0284	10	0.123	48.21	0.134
1. 42 0.0562			433	6.889	071	8.00.1	15	0.120	50.13	0.138
2.09 0.0000	4.2	0.00709	443	7.063	7 -	2000 c	20	0.127	6 c	0.151
	78	0.538	453	7.244	180	2.442	25	0.137	51.13	3 9
4.20 0.0654	2/3	.T.	403	7 503	200	2, 808	נוט	C172 VE 40	67.0	0.315
11010	CLRVE	/E 30	483	7.758	220	3.169	i		71.0	998.0
			493	7.952	240	3.525		0.365	79.0	0.30%
~	4.2	0.287	503	8.120	500 500	3.817	က	 	89.0	0.00
4.40	78	0.848	513	8.317	2.5.2	4.108	ĸ	0.32	101	0.818
CURVE 24	273	4.38	523	8.493*	067		ន្ទ	0.29	110	2.6
10000			533	8.684	CURVE	VE 35	ខ្ល	0.275	101	200
	CURVE	(E)	0 00 00	0.00 0.00 0.00 0.00	9	0.82	3 9	3.5	ខ្ម	1.304
Se divario	4.2	0.063	263	9.307	273	3.91			146	1.6284
2000	78.	0,573	573	9,5224	373	5.56			153	1.70%
4.2 0.093	273	4.23	583	9.721	460	7.27			302	1.76%
273 3.5 ± 0.5			<b>59</b> 3	9.929					90 .	2.033
									?	5.7

. Not shown in figure.

	-	TABLE 8.	EXPER	IMENTAL DATA O	N THE ELE	EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF MAGNESIUM	ITY OF MA	GNESIUM	Mg (Temper
۲	٩		۲	Q	۲	Q.	۲	a	
CURVE 4	CURVE 41 . cont.)		CURVE 42 (cont.)	(cont.)	CURVE	E 46	CURVE	CURVE 55 (cont.)*	
1. 2.	2.258		50.63	0.174	20.35	0.0492*	90.02	0. 795	
224	2.535		52.62	0.202	77.90	0. 505	273.15	4.179	
200 200 200 200 200 200 200 200 200 200	2.24.4		57.16	0.24%	90.05	0.686	291.15	4. 492	
	2000		63.0		291.15	3.813	373.43	076.0	
280	3,704		67.0	0.40	373.15	5.044	CURV	CURVE 56*	
183	3,748		72.0	0.47					
259	3,338		19.0	0.60	CURVE 47*	E 47*	20.35	0.0379	
ı			89.0	0.79			77.90	0. 382	
CUR	CLRVE 42		101	0.08	20.35	0.062	90.02	0.797	
	. 31.0		109 ::	1.20*	77.90	0.503	273.15	4.201	
. t. 5.	1010.0		123	1.10	973 15	9.083 3.578	271.13	4. 316 5. 940	
5.55	0.0101		132	1.56	291.15	3,848	3	,	
33	0.0161		147	1.93	373, 15	5.087	CURV	CURVE 57	
C. 00	6.0102		153	2.03				}	
17.9	6.9103		157	2.11*	CURVE 48	E 48	20.35	0,0573	
37:5	0.0163		991	2.26	 		77.90	0.579	
9,11	0.0165		175	2.45	291.15	3.957	90.05	0. 793	
10.72	6.00		225	7.03	*07 3A41J	7 40*	273.15	4.179	
11.22	0.01137		250	3.85			373.15	5.917	
12.20	0.0115		263	4.08	291.15	3.993			
12.53	0.0119		272	4.24*			CURVE 58*	E 58*	
13, 52	0.0121		280	4.40	CURVE 50	E 50			
14.03	0.6123		<b>1</b> 0	4,44.	:		291.15	<u>ئ</u> ي	
14.13	0.01257		682	2.36	291.15	4. 218	.,	9	
100	0.0138		CURVE 43	. 43	CHRVE SI	£ 51*	ברעיב פא	2	
16.95	0.0146					\$	291.15	3. 77	
17.79	0.0152*		973	28.6	291.15	4.272		: <b>:</b>	
19.15	0.0163		1023	28.5					
26.70	0.6141		1074	23.3	CURVE 52	25 25			
-# 60 61 - 61 6	0.6201		1124	29.1					
25, 49	0.0261		1 1 1 1	F. 7	631.13	4. 203			
26, 95	0.0255		CURVE 44	44	CURVE 53*	E 53*			
24.78	6.03192			<b>;</b>		Í			
29,65	0.0363		80	10.00	291.15	4.373			
31,49	0.0130		273	18.20		,			
31.70	0.0 4+10.0		4.76.10		CURVE 54	2			
, t	1000.0		C - 111 E 43	<del>?</del> ]	201 15	85.6			
25.92	0.0759		273.15	3.90					
40, 36	0.0483		373.15	5.54	CLRVE 55	E 55			
10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0347		573.15	10.00	3				
900	0.144 #				77.90	0.0502			
	\ P = ->				:				

\* Not shown in figure.

### 4.3. Calcium

Calcium, with atomic number 20, is a silvery-white moderately soft metal. It has a face-centered cubic crystalline structure, which transforms to body-centered cubic form around 720 K. Its density is 1.55 gm cm<sup>-3</sup> at 293 K. It melts at 113 K and boils at 1795 K. Impure calcium can also occur in a close-packed hexagonal form, which is stabilized by the impurities in calcium and is stable between about 523 and 720 K. Naturally occuring calcium is composed of six stable isotopes, the most abundant being <sup>40</sup>Ca which constitutes 96.97%. Eight other radioactive isotopes are known to exist. Calcium is the fifth most abundant element in the earth's continental crust, of which it forms 4.15% by weight.

## Temperature Dependence

There are 16 sets of experimental data available for the electrical resistivity of calcium. The information on specimen characterization and measurement condition for each of the data sets is given in Table 10. The data are tabulated in Table 11 and shown in Figures 6 and 7. Determinations of the electrical resistivity for both the solid and liquid states cover continuously the temperature range from 1.36 to 1138 K.

The data for the electrical resistivity of calcium show considerable scatter. Around room temperature, there is a sudden jump from the low-temperature data to those above room temperature as if there is a phase transition. This discrepancy is probably due to specimen contamination at higher temperatures. Katerberg et al. [68] (curve 10) found a small discontinuity near the phase transition temperature around 720 K. The data of Smith et al. [69] (curves 4 and 5) also show slope changes near the transition, which, however, give a quite different shape from that indicated by the data of Katerberg. The data of Swischer [70] (curves 14-16) do not show any discontinuities. The recommended values were generated based on the data of Cook and Laubitz [71] (curve 12) and Kayser and Soderquist [72] (curve 1). A least-mean-square-error fit was made with the modified Bloch-Grüneisen equation (8) to the selected data for  $\rho$ - $\rho$ - $\rho$ 0 from 30 to 300 K and to the estimated values up to 1113 K. At the phase transition temperature around 720 K the possible discontinuity was ignored. The following results were obtained for the coefficients in equation (8):

 $S_1$   $S_2$   $S_3$   $(\theta_R)_0$  C P  $3.341\cdot10^{-8}$  M  $0.296\cdot10^{-8}$  M  $0.087\cdot10^{-8}$  M 0.09 K 0.0281 2.0

The Debye temper ture deduced from specific heat measurements is 234 ± 5 K which is

about 20% lower that the present value for  $\theta_R$ . The resulting values from equation (8) were then corrected for thermal linear expansion to become the final recommended values.

Only one data set is available on the electrical resistivity of calcium in the liquid state. Van Zytveld et al. [50] (curve 6) found that the temperature dependence of electrical resistivity is small and weakly negative. At the melting point (1113 K), the electrical resistivity of calcium in the liquid state is about 126% higher than that of solid calcium.

The recommended values for the total and intrinsic electrical resistivities are listed in Table 9, and those for the total resistivity are also shown in Figures 6 and 7. The recommended values for the total electrical resistivity are for 99.96<sup>+%</sup> calcium and those below 30 K are applicable only to a specimen with residual resistivity of  $0.045 \cdot 10^{-8}\Omega$  m. The recommended values from 1 to 293 K are corrected for the thermal linear expansion. The correction amounts to -0.47% at 1 K, -0.38% at 100 K and -0.2% at 200 K. The uncertainty in the recommended values for the total electrical resistivity is believed to be within  $\pm 10\%$  below 40 K, within  $\pm 5\%$  from 40 to 300 K, and within  $\pm 20\%$  from 300 to 1150 K. Above 40 K the uncertainty in the recommended values for the intrinsic resistivity is slightly higher than that in the total electrical resistivity because of the possible deviations from the Matthiesen's Rule; below 40 K the  $\rho_i$  values are very uncertain and are not listed in the table.

TABLE 9. RECOMMENDED ELECTRICAL RESISTIVITY OF CALCIUM (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho_i$ ,  $10^{-8} \Omega$  m; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8} \Omega$  m]

S	Λl	i	r

T	ρ	$ ho_{ m i}$	Т	ρ	$ ho_{i}$
1	0.045*		250	2.82	2.77
4	0.045*		273.15	3.11	3.06
7	0.046*		293	3.36	3.31
10	0.047*		300	3.45	3.40
15	0.051*		350	4.09*	4.04*
20	0.060*		400	4.73*	4.68*
25	0.075*		450	5.37*	5.32*
30	0.100*		500	6.02*	5.97*
3 <b>5</b>	0.133*		550	6.68*	6.63*
40	0.175	0.130	600	7.35*	7.30*
45	0.224	0.179	650	8.02*	7.97*
50	0.277	0.232	700	8.70*	8.65*
60	0.396	0.351	750	9.38*	9.33*
70	0.522	0.477	800	10.0 *	10.0 %
80	0.652	0.607	850	10.7 *	10.7 *
90	0.782	0.737	900	11.4 *	11.4 *
100	0.913	0.868	950	12.1 *	12.1 *
110	1.04	0.997	1000	12.8 *	12.8 *
120	1.17	1.12	1100	14.3 *	14.3 *
130	1.30	1.25	1113	14.5 *	14.5 *
140	1.43	1.38			
150	1.56	1.51			
175	1.88	1.83			
200	2.19	2.14			
225	2.51	2.46	1		

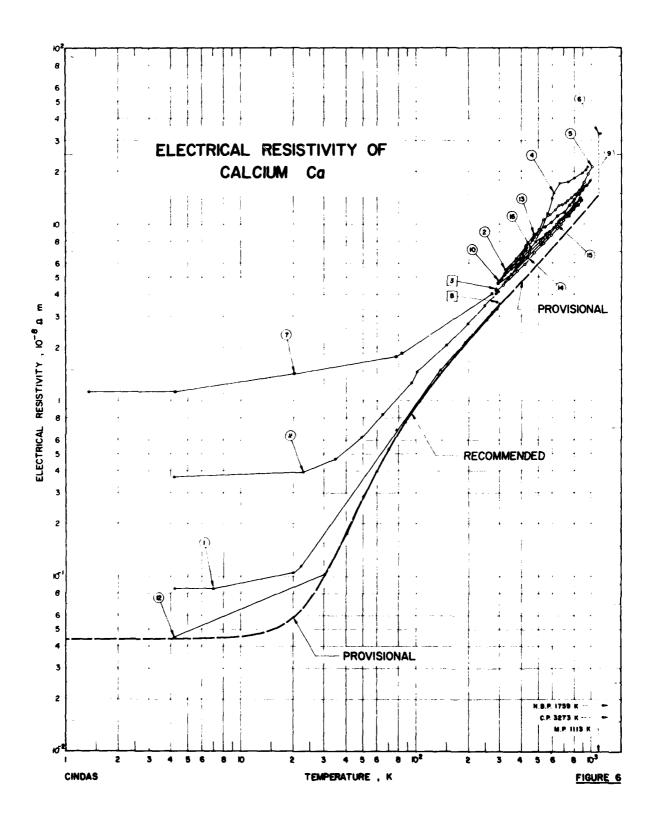
Liquid

T	ρ
1113	33.0*
1150	33.0*

The second of th

The recommended values for the total electrical resistivity are for 99.96+% pure calcium and those at temperatures below 30 K are applicable only to a specimen with residual resistivity of 0.045 x  $10^{-8}~\Omega$  m.

<sup>\*</sup> Provisional values.



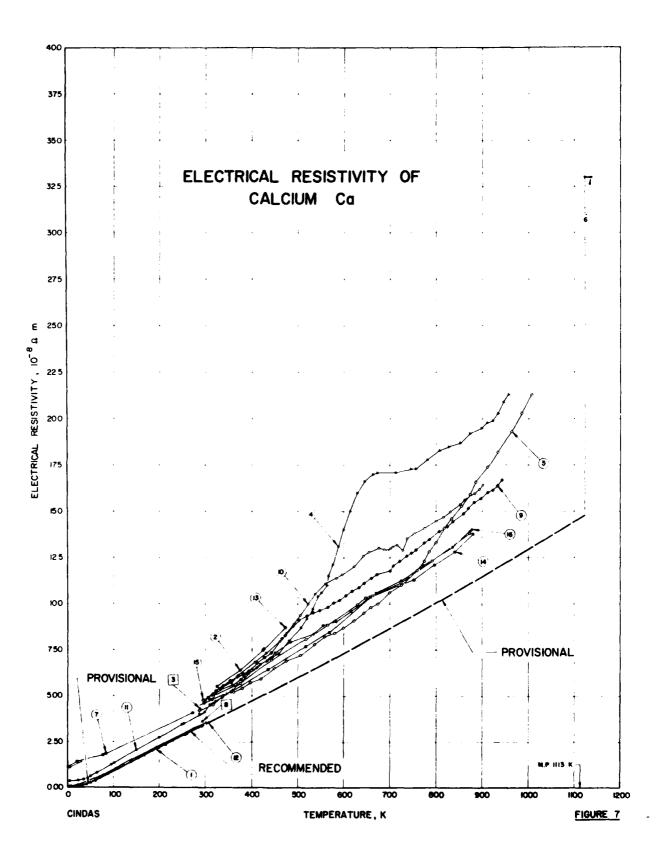


TABLE 10. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF CALCIUM Ca (Temperature Dependence)

Cur. Ref. No. No.	Kef.	Author(s)	Year	Method	Temp. Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
t 12	72	Kayser, F.Y. and Soderquist, S.D.	1967		4.2-300	5	99.96 Ca, 0.025 Sr, 0.005 O, 0.003 H, 0.0015 Mg, 0.0011 Ma; 0.0625 in. diameter wire specimens; amecaled for 2 hr at 525 K under 8 x 10 <sup>-4</sup> torr; ρ273.2 K ≈ 3.16 μΩ cm, reported error =2°.
7	5.	Cook, J.G. and Van der Meer, M.P.	1973		325-425	<b>5</b>	99* purity, smoothed values extracted from table, data uncorrected for thermal expansion; resistance ratio 3.
3 74	2	Rinck, E.	1831		289	ಕ	Pure calcium was prepared by diffusion technique, 1, 245 cm in dismeter and 10 cm long cylindrical sample.
<b>5</b>	<b>9</b>	Smith, J.F., Carlson, D.N., and Vest, R.W.	1956	<b>m</b>	273-973	Ca A	99.66 Ca, 0.3 Mg, 0.025 N, 0.006 Fe, 0.001 Al, 0.004 Mn; sample was bested at 600 C for 8 hr after four successive distillation at 900 C; 0.2 in. in diameter and 5 in. long.
69	9	Smith, J. F., et al.	1956	A	273-973	<b>5 6 7</b>	99.96 Cn, 0.01 Mg, 0.011 N, 0.010 Fe, 0.001 Al, 0.005 Mn; 0.2 in. in clameter and 5 in. long.
9	9	Van Zytveld, J. B., Enderby, J. E., and Colliegs, E. M.	1972		1123-1138		99.9 pure, 0.001 each Al, Fe, 0.02 N., 0.001-0.002 each Co, Be, B. 0.001-0.02 Li, 0.01-0.05 Mg; sample was obtained from Atomergic Cherretals Co.
2	2	Meisoner, W. and Volgt, B.	1930	•	1.36-273,16	Ca 1	Pure; specimen was enclosed in a glass rube filled with helium gras; specimen dimension 1.2 x 1.2 x 59 mm; electrical resistance was measured by companention method with a mirror galvanometer; no thermal expansion correction for electrical resistivity data.
8 75		Frank, V. and Joppesen, O.G.	1953		293.15	ಕ	99° Cn; 0.203 ±0.002 mm thickness, 17 mm width, 48 mm long; density = 1.543 ±0.004 g cm <sup>-3</sup> , lattice constant = 5.59 ±0.01 x $10^{-4}$ cm (face-centered cubic).
<b>9</b>		Katerborg, J., Nemeyer, S., Peming, D., and Van Zytveld, J.B.	1975	≺	306-944		99.5 pure, major metallic impurities were other alkaline earth metals; specimen was supplied by Atomergic Chemetals Co.; the sample was mounted on staintees steel and high purity aluminu with their surfaces exposed to the dynamic vacuum; measurements were takes with sample held under an atmosphere pressure of pure intert gas; data was extracted from figure.
10 68		Katerberg, J., et al.	1975	<	300-902		Similar to the above specimen except it was supplied by Hall Co.; data was extracted from the graph.
H H		Cock, J.G., Laubitz, M.J., and Van der Meer, M.P.	1975	<	4. 2-299. 3	C	High purity (995 pure) Ca was sublimed at 1100 K in an Ar atmosphere of 6 mm lig onto a 304 stainless sivel plate kept near 570 K; cylindrical sample was east from the puritied by Hilling 1.2 cm diameter tubes with dendrites, welding caps onto their ends, heating them above the melting points of Ca in a vactum furnace and then slowly cooling them; the resistance ratio near 10.
12 71		Cook, J. G., et al.	1975	Ω	4.2-306.27	Ca 3	Similar to the above specimen; except Ta tabing and caps were used; the resistance ratio was near 70.
13 71		Cook, J.G., et al.	1975	<	324.09-4731	Ca 1	99% pure commercial calcium.
14 70		Swinber, C. L.	1917	m	297569	0	99.57 pure; specimen was obtained from Kalilbaum; whe specimen 0.23 cm in diameter and 10.4 cm in length; measurements were taken in vacuum.
15 70		Swiaber, C. L.	1917	<b>m</b>	295-631	Ą	Similar to the above specimen; except 0.27 cm in diameter and 10.0 cm in length.

TABLE 10. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF CALCIUM Ca (Temperature Dependence) (Continued)

Composition (weight percent). Specifications, and Remarks		Similar to the above specimen; except 0.275 cm in diameter and 7.5 cm in	length.
Name and	Specifical Designation	d	,
Tema.	Used Range, K	362 300	200-007
Merchand	Csed	1	<b>2</b> 4
	Year		1917
	Author(s)		70 Swisher, C. L.
	Cur. Raf.	;   ;	16 70
1	ز ن	٠.	

TABLE 11. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF CALCIUM Ca (Temperature Dependence) | Temperature. T. K: Resistivity. a. 10-4 (Dm)

	<b>a</b>	CUBVE 12 (cont.)	50. 61 0.25-71												214.63 2.379						23		CLRVE 13			ئى		473.1 8.720		CURVE 14		÷.						15.08				CURVE 13			99.3		
	۲	~																			306						Ų	¥				166													373		
	<b>a</b>	CURVE 10 (cont.	10. St	11.09	:: 38 :: 38	11.36	12.07	12. 56	12. 77	13.01	12. 93	12.90	12. 98	13.07	13.16	12.01	3 .	1 1 2	14.47	14. 70	14.97	15.35	15.60	15.95	16.19	16.41		CURVE 11		0.369													CURVE 12	l	0.045		
	۳	CLRVE	538	261	585	200	623	27.9	#.59	919	689	969	101	707	977	250	25.5	77.5	800	816	831	853	863	884	†63 *	803		CUR		7	23.0	35.0	49.6	. 3	101	155.00	100.0	200.4	249, 7	23.5	299.3				4.2	4.00°	₩ ₩
y, p, 10-4 (7m)	a	CURVE 9 (cont.)	9.34*	9, 53 1		20.0	10.03	10.20	10.44	10.67	10.85	11.11	11.38	11.58	12 02	10.02	12.57	12.73	12, 93	13, 28	13.47	13.85	14.15	14.44	14.65	15, 16*	15.48	15.70	16.01	16.15	16.39	16.66	טו שווקונט	21	35.78	• 90	5.09	5.45	. 1. v	6.09	6.62	7.31	7,96	8· <del>1</del> 0	8.89	9.37	9. <b>98</b> .
Resistivit	۳	S	520	3	23.5	600	200	291	604	617	633	5.	099	219	702	3.5	137	747	757	775	766	807	824	837	860	871	<b>2</b> 8€	898	913	924	<b>7</b> ,	Ī	5	51	300	303	316	336	355	371	404	432	462	476	492	8	22
[Temperature, T. K; Resistivity, p. 104 (Im)]	a	CURVE 5 (cont.)	13.3	14.1		?	n 0	0.0	17.4	200	19.3	20.3	21.3	9 44 64 6	9	73002	33.0 + 1.4		CURVE 7	ł	1. 131	1.137	1.432	1.781	1.856	4.050		CURVE 8	;	3.60 ± 0.03	•	2	69 7	20.4	5.26	5. 53	5.80	6.03	6.19	6.34	6.76	7.08	7, 35	8.10	8. 29.	98.9	9.11.
Tea	۲	CURVE	800	218	# 55 G	760	# 000 000	8 6	516	3	596 6	300	7007	Ę		1193	1136	}	ED:	}	1.36	4.22	20.45	17.59	83.57	273.16				293.15	į	CCRVES	aŭ.	315	323	338	78	33	382	305	412	428	443	466	474	3	200
	a	E 4 (cont.)	13.1	0.4.	16.0	2.57	2.5		17.1	1.7.	17.3	2.7	0.0	, a.	0.00	6.61	19.5	19.8	19.9	20.3	20.9	21.3	:	CURVE 5			4.5	o i	ķ, .	<b>⊕</b> เ	- 6	n ka	9	61	7.8	8.2	₹.	8.7	9.1	9.5	<b>6</b> 0	10.0	10.6	11.0	8.1.2	7	0.27
	۲	CURVE	66.8	3 :	# OC 9	X:9	799		7.2	\$7.	367	625	700	900	64.8	874	668	116	923	76.6 6	9 <b>4</b> 8	958		리		287	317	866	2 2	985.	8	3 5	475	206	537	829	280	<b>96</b> 5	622	C+3	629	675	609	725	25	200	201
	Q	CLRVE 1	0.035	90.0	0.10	. C	5	3 :	i	67.7	 	3	CITAVE 9		5.50	6.37	7.46		CLRVE 3	1	<del>,</del> 3		CLRVE 4	•	•		÷	<b>+</b> .	ņ.	⊣ e ก๋ u	; u	9 ac	6.2	6.4	6.7	<b>6</b> .9	7.7	٠. ن	9.0		6,7	2.6	• · · ·	 	9 :	6.1.1	1.71
	H	33	4.2	* •	2.5	1	,		9.161	7	21:20	1.10	: :	Ä	325	27.2	425		5		286	į	덩	;	287	P.	317			9 g	e e		S.	404	419	<b>4</b> 53	4.0	<u>.</u>	492	3	220		3 :	77.00	3 5 5	3 5	

. Not shown in figure.

TABLE 11. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF CALCIUM Ca (Temperature Dependence) (Continued)

[Temperature, T, K; Resistivity, p. 10-5 Qm]

8.85 9.95 10.45 11.12 13.30 

CLRVE 15 (cont.)

CLRVE 16

 Not shown in figure.

## 4.4. Strontium

Strontium, with atomic number 38, is a silvery-white metal, resembling calcium in its properties but softer. It exists in three structural modifications: face-centered cubic  $\alpha$ -Sr stable below 488 K, close-packed hexagonal  $\beta$ -Sr stable between 488 and 815 K, and body-centered cubic  $\gamma$ -Sr stable above 815 K. The density of  $\alpha$ -Sr is 2.60 g cm<sup>-3</sup> at 293 K. The metal melts at 1042 K and boils at about 1645 K. At room temperature and a high pressure of 3.5 x 10<sup>9</sup> Pa,  $\alpha$ -Sr undergoes a phase transformation to a body-centered cubic structure similar to  $\gamma$ -Sr. Naturally occuring strontium is composed of four stable isotopes, the most abundant being <sup>88</sup>Sr which constitutes 82.56%. Twelve other radioactive isotopes are known to exist, one of which, the longest-lived <sup>90</sup>Sr with a half life of 28.1 years, is of great importance. This radioactive isotope is one of the best long-lived high energy beta emitters known and is very useful. But it also is a product of nuclear fallout and presents a health problem. Strontium is the fifteenth most abundant element in the continental crust of the earth (0.0375% by weight).

# Temperature Dependence

There are 11 sets of experimental data available for the temperature dependence of the electrical resistivity of strontium. The information on specimen characterization and measurement condition for each of the data sets is given in Table 13. The data are tabulated in Table 14 and shown in Figures 8 and 9. Determinations of the electrical resistivity for both the solid and liquid states cover the temperature range from 1.32 to 1093 K.

The data of Messiner and Voigt [27] (curves 8 and 9), Rinck [76] (curve 11), McWhan, Rice, and Schmidt [77] (curves 1-3), and Rashid and Kayser [78] (curve 4) were not for high-purity specimens. At temperatures below 815 K the recommended values are based on the data of Cook and Van der Meer [73] (curve 6), Rashid and Kayser [78] (curve 5), and Katerberg et al. [68] (curve 10). These three sets of data for 99.5% pure specimens appear to be reasonably consistent. A least-mean-square-error fit was made with the modified Bloch-Grüneisen equation (8) to the selected data for  $\rho p_0$  from 50 to 800 K. The following results were obtained for the coefficients in equation (8):

$\mathbf{s_i}$	S <sub>2</sub>	83	$(\theta_{\mathbf{R}})_{0}$	C	P
6.015·10 <sup>-8</sup> Ω m	-0.02743·10 <sup>-8</sup> Ω m	0	142.7 K	0.0108	0

The Debye temperature deduced from specific heat measurements is 147 K which is very

close to the present value for  $\theta_R$ . The resulting values from equation (8) were then corrected for thermal linear expansion to become the final recommended values.

There appears to be no discontinuity in the electrical resistivity at the temperature of 488 K where the transition from  $\alpha$ -Sr to  $\beta$ -Sr occurs. However, at the  $\beta$ -Sr to  $\gamma$ -Sr transition around 815 K, there is a sudden jump of about 40% in the resistivity values. Above 815 K the recommended resistivity values are based on the data of Katerberg et al. [68] (curve 10). Their data were fitted with a linear logarithmic equation up to the melting point resulting in the following equation:

$$\log_{10} \rho = -1.6233 + 1.137 \times \log_{10} T$$
 815 K \leq T \leq 1042 K (13)

Only one set of data is available on the electrical resistivity of strontium in the liquid state. Van Zytveld et al. [50] (curve 7) found that the temperature dependence of electrical resistivity is small and weakly negative. At the melting point (1042 K), the electrical resistivity of strontium in the liquid state is about 31% higher than that of solid strontium.

The recommended values for the total and intrinsic electrical resistivities of strontium are listed in Table 12, and those for the total electrical resistivity are also shown in Figures 8 and 9. The recommended values for the total electrical resistivity are for 99.95<sup>+%</sup> pure strontium and those at temperatures below 30 K are applicable only to a specimen with residual resistivity of  $0.80 \times 10^{-8} \Omega$  m. The recommended values from 1 to 293 K are corrected for the thermal linear expansion. The correction amounts to -0.54% at 1 K, -0.42% at 100 K, and -0.21% at 200 K. The uncertainty in the recommended values for the total electrical resistivity is believed to be within  $\pm 10\%$  below 50 K, within  $\pm 5\%$  from 50 to 815 K, within  $\pm 10\%$  from 815 K to 1042 K and within  $\pm 20\%$  above 1042 K. Above 40 K, the uncertainty in the recommended values for the intrinsic resistivity is slightly higher than that in the total electrical resistivity because of the possible deviations from the Matthiessan's Rule; below 40 K  $\rho_i$  values are very uncertain and are not listed in the table.

TABLE 12. RECOMMENDED ELECTRICAL RESISTIVITY OF STRONTIUM (Temperature Dependence)

[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8} \Omega$  m; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8} \Omega$  m]

~	•	٠	- 1
~^	,	9.	•

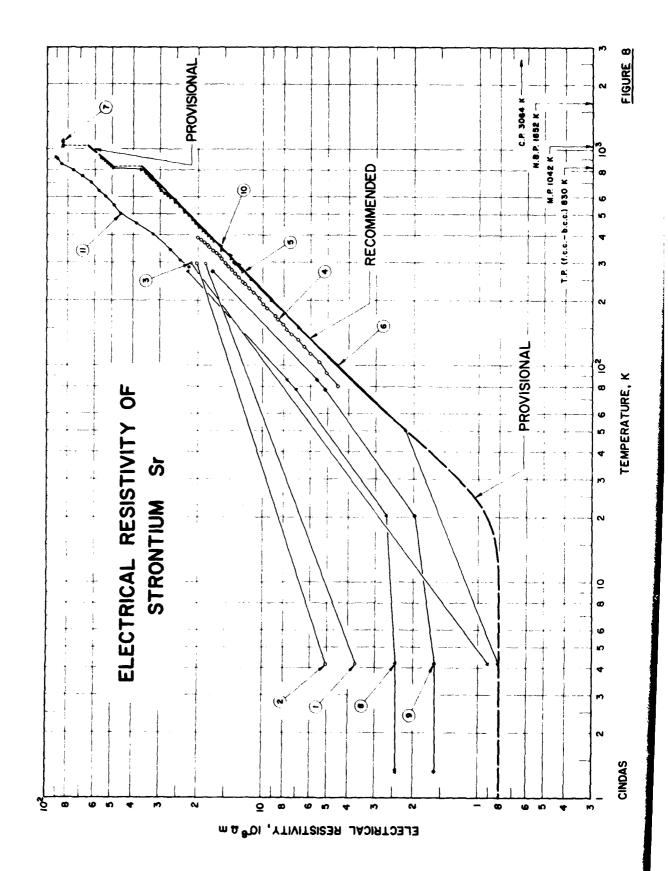
T	ρ	$ ho_{\mathbf{i}}$	т	ρ	$\rho_{i}$
	<del></del>	<u></u>			<u>' \</u>
1	0.800*		250	11.3	10.5
4	0.800*		<b>273.</b> 15	<b>12.</b> 3	11.5
7	0.800*		293	13.2	12.4
10	0.805*		300	13.5	12.7
15	0.835*		350	15. 7	14.9
20	0.918*		400	17.8	17.0
<b>2</b> 5	1.065*		450	20.0	19.2
30	1.257*		500	22.2	21.4
35	1.460*		550	24.5	23.7
40	1.700*		600	26.7	25.9
45	1.94*	1. 14*	650	28.9	28.1
50	2.18	1 <b>. 3</b> 8	700	31.2	30.4
60	2.68	1.88	750	33.4	<b>32.</b> 6
70	3. 16	2.36	800	35.6	<b>34.</b> 8
80	3.64	2.84	815	36. 1	35.3
90	4.12	3.32	815	48.8*	48.0*
100	4.58	3.78	950	54.5*	53.7*
110	5, 04	4.24	1000	<b>62. 2*</b>	61.4*
120	5.50	4.70	1042	65.6*	64.8*
130	5.94	5. 14	l		
140	6.39	5. 59	1		
150	6.84	6.04	1		
175	7.95	7. 15	Ī		
200	9.04	8.24	ł		
225	10.2	9.35			

Liquid

T	ρ
10 <b>42</b>	84.8*
10 <b>93</b>	84.7*

The recommended values for the total electrical resistivity are for 99.95 $^{+}$ % pure strontium and those at temperatures below 30 K are applicable only to a specimen with residual resistivity of 0.80 x  $10^{-8}\Omega$  m.

<sup>\*</sup> Provisional values



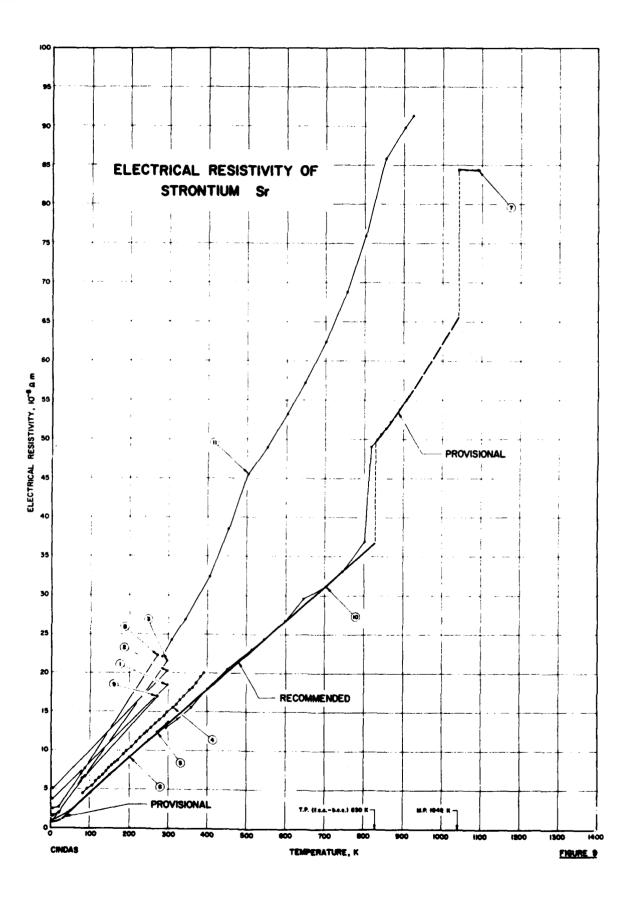


TABLE 13. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF STRONTIUM Sr (Temperature Dependence)

				-			
Cur.	Cur. Ref. No. No.	f. Authoris)	Year	Method Used	Temp. Range, K	Name and Specimen Designation	Composition (weight percentl, Specifications, and Remarks
-	77	McWhan, D.B., Rice, T.M., and Schmidt, P.H.	1969	Y	4.2,298	Sr 4	98.1 Sr. 1.9 (Mg. Ca. Ba), 0.04 other; Rogs,4.2 = 5; samples were made from metal purified by fractional distillation.
8	11	McWhan, D.B., et al.	1969	<	4.2,298	Sr5	98.8 Sr, 1.2 (Mg, Ça, Ba), 0.05 other; R298/4.2 = 4.
က	77	McWhan, D.B., et al.	1969	∢	4.2,298	Sr 6	98.6 Sr, 1.4 (Mg, Ca, Ba), 0.03 other; R298/4.2 = 24.
7	78	Rashid, M.S. and Kayser, F.X.	1971		80-400	Sr	96* Sr, 0.2 cach Ba, Ca, 0.025 Mg, 0.03 cach Fe, Ny, 0.015 Al, 0.05 (Li + Na + K); 3.8 mm diameter, 10 mm long wire specimen annealed at 470 K for 16 hr, 3 times.
10	78	Rushid, M.S. and Kaysor, F.X.	1971		273,298	273,298 Sr (distilled)	Same as above except the specimen was distilled at 1140 K.
•	73	Cook, J.G. and Van der Muer, M.P.	1973		4.2-300	S.	99 * purity; P(273.2) /P(4.2) = 15.5
	20	Van Zytveld, J. B., Endrtby, J. E., and Collings, E. M.	1972		1043-1093	డ	99.5 pure, < 0.08 Fc. 0.05 each Al. Ny. Ba, Mg. Ca, 0.01 Cly. 0.1 others; specimen was obtained from Atomergic Chemetals Co.
<b>8</b> 0	23	Muissner, W. and Voigt, B.	1930	t	1.32-273	Sr 1	<0.1 Fe; specimen was in a glass tube with heltum; specimen size was 0.5 x 2.5 x 34 mm; the electrical resistance was measured by compensation method with a mirror galvanometer; to thermal expansion correction for electrical resistivity data.
ø	Z	Meissner, W. and Voigt, B.	1930	•	1.32-273	Sr 2	Similar to the above specimen except it was heated in vacuo for 3 hr at 160 C.
9	89	Katerberg, J., Niemeyer, S., Peming, D., and Van Zytveld, J.B.	1975	∢	294-912		99.5-99.7 purity specimen was obtained from Atomergic Chemetals Co.; the measurements were taken with sample held under an aim of pure inert gas; data were extracted from figure.
11	76	Rinck, E.	1952	∢			Pure, double distilled specimen was obtained from Pechiney Co.; cylindrical specimen about 10 cm long; melting point 1041 K; data were extracted from graph.

TABLE 14. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF STHONELY Sr (Temperature Dependence) [Temperature, T, K; Resistivity, p, 10<sup>-4</sup> Cm]

	3	~ ž.	2.5		ኋ	<u> </u>	. Ž	_	<u>*</u>	* *	!	<u>.</u> _	_																													
Q.	CURVE 11 (cont.	68.9	5.5	76.	19.	82.6	85.0	85.9	8.	87.3	88	2	77.																													
۲	CURVE	756	1.67	Š	815	825	38	855	<b>964</b>	9:8 8:8	3	2 4 6	076																													
. or	(cont.)	53.81 34.59	35, 23	49.02	49.93	50.64	52.27	53.89	55.03	55.43	E 11		24.3	25.24	26.9	28.84	30.6*	32.4	¥.1	35.1*	36.6*	38.5	40.7*	42.73	44.4%	45.6	200	, a	69.0	50.23	50.6	$51.2^{\circ}$	52.0	53.3	55.23	57.2	58.8	60.4*	62.5	64,3	66.3	67.2
itemperature, 1, n; restaining, p, 10 ° 10m.	CURVE 10 (cont	763 779	793 804	819	835	<b>44</b>	698	892	806	913	CURVE 11	206	308	322	343	365	388	406	420	431	444	4.55	469	479	491	205	#10°	92.5	552	260	570	583	593	<b>7</b>	624	648	899	635	702	716	735	741
Bu iu i																																										
, d	(cont.)	2.662	7,717	; ;	CURVE 9	985	1.595	1.978	5.143	5,639			12.94	13,63	14.21	15.14	15.8g	16.72	17.28	17.70	18.01	18.26	18,62	19.38	20.12	50. 50. 50. 50. 50. 50. 50. 50. 50. 50.	22.00	23.42	24.33	25.26	25,92	26.90	27.00	23.20	29.00	29. 76	30, 33	30.963	31, 31	32, 11	32.66	33. 14
	CURVE 8 (cont.	20.40	86.32 273.16		CUR	1 39	4.20	20.40	77.75	86.32 273.16	CIMBILE		294	310	322	342	359	378	390	339	408	<b>4</b> 14	422	438	<b>7</b>	471	403	527	<b>3</b>	570	587	602	617	629	24.0	299	2 6	697	900	724	737	147
			1	•																															_ •	0						
a	(cont.)	15.13* 15.59	15.77*	16.09	16. 53	16.71	17.22*	17.35	17.82	18.17	18.517	18 964	19.24	19.53	19.80	20.05		F 5	;	12.46	13.46		9	•	908.0	81.7	3	9.12	11.38	12.5 *	13.65		E 7	6	0.5 2 6.0	<b>2.</b> 65 ± 2.		20	919	074.2	2.416	2.410
۲	CURVE 4 (cont.	302.6	327.1	326.7	330.8	335.6	344.9	349.6	353.9	362.8	367.3	7.12	379.7	383.6	398.1	391.0		CURVE 5		272.7	297.9		CURVE 6	•	7.7	3 5	3 5	200	250	273	8		CURVE 7	200	3	1093	į	CCKVE		25.7	5	4.21
a	LE 1	3.7	6 3	}	2.08	20.3	3	; 	8 . 3 .	3.12	<u> </u>	4.19	5.07	5.47	6. 62	6.42	6.86	£ .38	7.76	& . S :		9.70	3 8		10.13	10.47		1.35	:: ::	11.54	12.15	12, 43	12.65%	10.03 10.03 10.03		12.43	2	3.5	69:41	3 5		F9.47
<b>(-</b>	CLRVE 1	23 <del>1.</del> 2	CLRVE 2		4.2	86 84	CURVE 3		<b>7</b>	673	CLRVE 4	60.3	52.8	104.1	117.9	122.9	133.1	1.0.1	117.8	155.4	153.1	***	200	135.2	64.3	20%	21.5	222.8	229.9	274.3	233.1	6 : : : : : : : : : : : : : : : : : : :	201.2	3 6				+·/·	K56.0	*****	41.50	1.16

"Not shown in figure.

#### 4.5. Barium

Barium, with atomic number 56, is a soft, silver-white metal, resembling calcium chemically. It oxidizes very easily in air, melts at 1002 K, and boils at 2174 K. Its density is 3.5 g cm<sup>-3</sup> at 293 K. The critical temperature of barium has been estimated to be 3670 K. Barium crystal has a body-centered cubic structure. At a pressure of about 5.9 x 10<sup>9</sup> Pa, the body-centered cubic structure transforms to a close-packed hexagonal form. Naturally occurring barium is composed of seven stable isotopes, the most abundant being <sup>138</sup>Ba, which constitutes 71.66%. Thirteen other radioactive isotopes are known to exist. Barium is the fourteenth most abundant element in the continental crust of the earth (0.0524% by weight).

## Temperature dependence

There are 21 sets of experimental data available for the electrical resistivity of barium. The information on specimen characterization and measurement condition for each of the data sets is given in Table 16. The data are tabulated in Table 17 and shown in Figures 10 and 11. Determinations of the electrical resistivity for both the solid and liquid states cover continuously the temperature range from 1.26 to 1451 K.

The data for the electrical resistivity of barium show considerable scatter. At low temperatures, the data of Meissner and Voigt [27] (curve 5), Meissner, Franz, and Westerhoff [79] (curve 10), and of Rashid and Kayser [80] (curves 6 and 7) are not for high-purity specimen. Above room temperature, Rinck [81] found a distinct slope change about 650 K (curve 13) which he assumed to be due to phase change at this temperature. The data of Grüntherodt, Hause, and Kunzi [82] (curve 9) are similar to Rinck's. The data of Grube and Dietrich [83] (curve 14) also show a discontinuity near 650 K, which however, exhibits quite a different nature from that indicated by the data of Rinck. The data of Katerberg, Nieneyer, Penning, and Van Zytveld [68] (curves 11 and 12) show no slope change at 650 K, but show a slope change near 530 K. Cook and Laubitz [84] presented data for pure and hydrogen charged Ba from 300 to 750 K (curves 15-21). Their data for pure barium differ from all previous data and show no evidence of transition at any temperature.

A least-mean-square-error fit was made with the modified Bloch-Grüneisen equation (8) to the data of Cook and Laubitz [84] (with correnction for the effect of hydrogen) and of Rashid and Kayser [80] (curve 8) from 30 to 750 K. The following results were obtained for the coefficients in equation (8):

$\mathbf{S_{1}}$	$S_2$	S <sub>3</sub>	$(\mathbf{A_R})_{0}$	С	P
5.870·10 <sup>-8</sup> Ω m	0.3428·10 <sup>-8</sup> Ω m	0	72.8 K	0.0252	0

The Debye temperature deduced from specific heat measurements is 110 K which is almost 40% higher than the present value for  $\theta_R$ . The resulting values from equation (8) were then corrected for the thermal linear expansion and extrapolated to lower and higher temperatures to become the final recommended values.

There are three data sets available on the electrical resistivity of barium in the liquid state. Van Zytveld, Enderberg, and Collings [50] (curve 3) and Grüntherodt et al. [82] (curve 9) found that the temperature dependence of the electrical resistivity of liquid barium is small and weakly negative. However, Genter and Grosse [85] (curve 2) found a very large positive temperature dependence. On comparison with the electrical resistivity data for other alkaline earth elements in the liquid state, indicated that the electrical resistivity of liquid barium should have a weakly negative dependence on temperature. The data of Van Zytveld et al. and of Grüntherodt et al. were normalized by matching their values at the melting point of 1002 K. The normalized values were then least-mean-square-error fitted with a linear equation to yield the provisional values. At the melting point (1002 K), the electrical resistivity of barium in the liquid state is about 25% higher than that of solid barium.

The recommended values for the total and intrinsic electrical resistivities are listed in Table 15, and those for the total resistivity are also shown in Figures 10 and 11. The recommended values for the total electrical resistivity are for 99.5% pure barium and those at temperatures below 100 K are applicable only to a specimen with residual resistivity of  $0.081 \times 10^{-8} \Omega$  m. The recommended values from 1 to 293 K are corrected for the thermal linear expansion. The correction amounts to -0.5% at 1 K, -0.37% at 100 K, and -0.18% at 200 K. The uncertainty in the recommended values for the total electrical resistivity is believed to be within  $\pm 10\%$  below 30 K, within  $\pm 5\%$  from 30 to 750 K, and within  $\pm 10\%$  from 750 to 1300 K. Above 40 K the uncertainty in the recommended values for the intrinsic resistivity is slightly higher than that in the total electrical resistivity because of the possible deviations from the Matthiesen's Rule; below 40 K, the  $\rho_i$  values are very uncertain and are not listed in the table.

TABLE 15. RECOMMENDED ELECTRICAL RESISTIVITY OF BARIUM (Temperature Dependence)

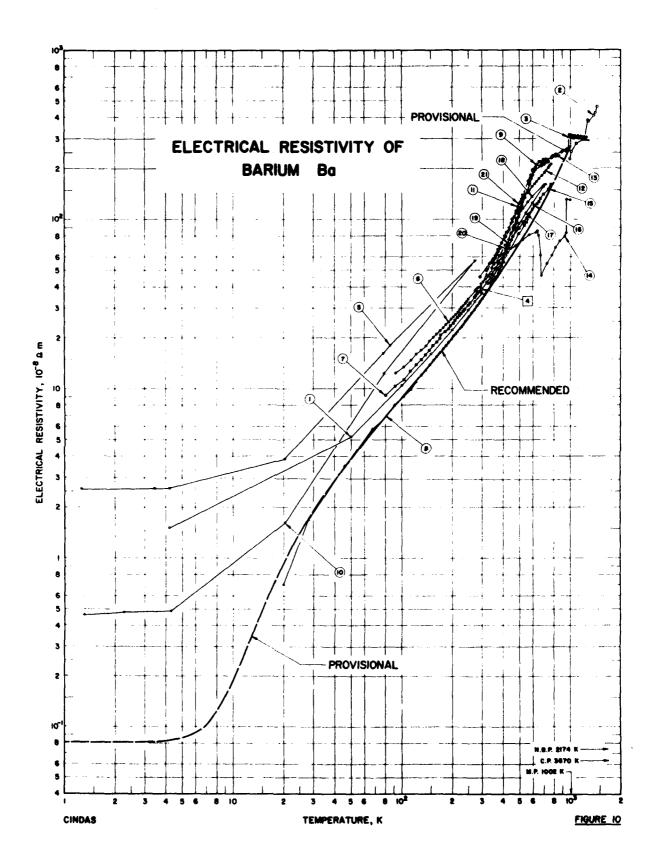
[Temperature, T, K; Total Resistivity,  $\rho$ ,  $10^{-8}$  % m; Intrinsic Resistivity,  $\rho_i$ ,  $10^{-8}$  % m;

			Solid		
T	ρ	$\rho_{\mathbf{i}}$	T	P	$ ho_{ m i}$
1	0.081*		250	26.9	26.8
4	0.082*		273.15	30.2	30.1
7	0.104*		293	33.2	33.1
10	0.189*		300	34.3	34.2
15	0.501*		350	42.4	42.3
20	0.940*		400	51.4	51.3
25	1.42 *		450	61.4	61.3
30	1.92 *		<b>§</b> 500	72.4	<b>72.</b> 3
35	2.41 *		550	84.7	84.6
40	2.91 *		600	98.2	98.1
45	3.39	3.31	650	113.	113.
50	3.88	3.80	700	130.	130.
60	4.86	4.78	750	148.	148.
70	5.84	5.76	∥ 800	168. *	168. *
80	6.83	6.75	900	216. *	216. *
90	7.83	7.75	950	244. *	244. *
100	8.85	8.77	1000	275. *	275. *
110	9.89	9.81	1002	276. *	276. *
120	11.0	10.9	<u> </u>		
130	12.0	11.9			
140	13.1	13.0			
150	14.3	14.2	]]		
175	17.2	17.1	<b>{</b> }		
200	20.2	20.1	<b>}</b>		
225	23.5	23.4			

L	iquid
T	ρ
1002	306. *
1050	303. *

<sup>\*</sup> Provisional values

The recommended values for the total electrical resistivity are for 99.5 $^+$ % pure barium and those at temperatures below 100 K are applicable only to a specimen with residual resistivity of 0.081 x  $10^{-6}\Omega$  m.



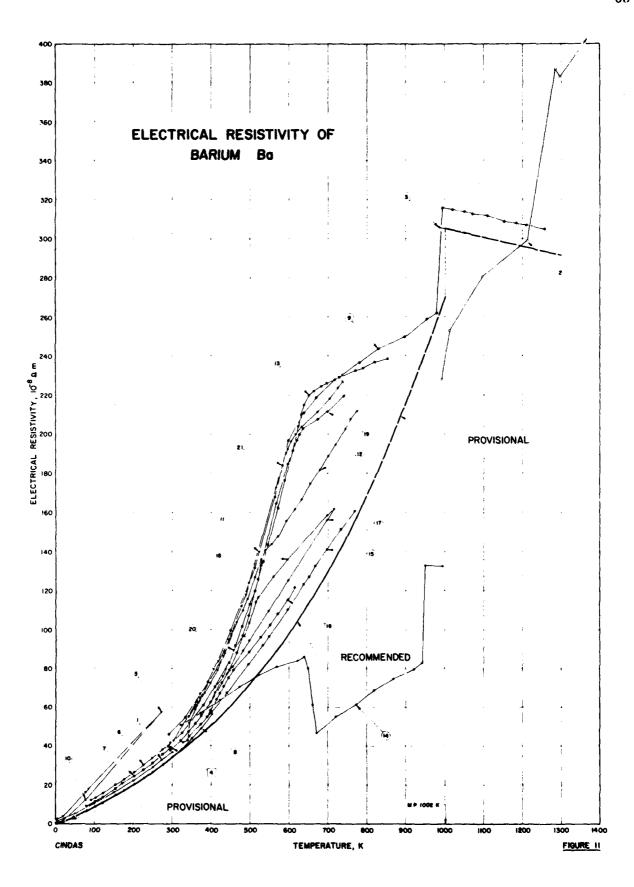


TABLE 16. MEASUREMENT INFORMATION ON THE ELECTRICAL RESSTIVITY OF BARIUM Bs (Temperature Dependence)

Cook.	Author (s)	Year	Method	Temp. Range, K	Specimen	Composition (weight percent), Specifications, and Remarks
	Cook, J.G. and Van der Meer, M.P.	1973		4.2-300		99 * purity; $\rho_{(273)}/\rho_{(4.2)}=21.8$ ; data were extracted from the smooth table.
Seate	Genter, R.B. and Grosse, A.V.	1971		993-1500		99.97 pure, 0.03 each Ca. Sr; liquid barium was contained to a Type 304 stain- less steel tube about 0.5 in O.D., 0.421 in I.D. and 10 in. long; the sample was obtained from Mackay Metals, New York.
Van Z	Van Zytveld, J. B., Enderby, J. E., and Collings, E.M.	1972		988, 1053		99.5 Ba, <0.1 each Sr. Na, C, <0.05 each Al, Fe, Nr, Zn; specimen was obtained from Atomergic Chemetals Co.
Xille	Müller, W.E.	1961		300		Pure;
Mels	Meissner, W. and Voigt, B.	1930		1.26-273	B <b>s</b> 1	Fure; specimen was placed in a glass tube filled with helium; sample size $0.2\mathrm{x}$ 4 x 40 mm; the electrical resistance was measured by compensation method, a mirror galvanometer was used.
Rash	Rashid, M.S. and Kayser, F.X.	1971	∢	80-300	<b>~</b>	99.0 pure Ba bar was obtained from Charles Pfirer Co., Inc.; it was entruded to 0.254 cm diameter wire and 3 cm long specimen; the specimen was in b.c.c. structure.
Resh	Rashid, M.S. and Kayser, F.X.	1761	<	80-300	89	Similar to the above specimen except it was in recrystallized treatment at 470 K for 16 hr.
Rash	Rashid, M.S. and Kayser, F.X.	1971	<	20-400	m	Similar to the above specimen except it was double distilled and annealed at 400 K for 4 days; p(300 K)/p(4.2 K) = 400 ~900.
S P P P P P P P P P P P P P P P P P P P	Günherodt, H.J., Hauser, E., and Künzl, H.V.	1975	O	292-1258		99.5 pure; the specimen was supplied by Fluka; a thin-wall vacuum tight stain- less steel crucible was used in mensurement; the specimens were eithed first in methyl alcohol and then in tolune, then the specimens were trans- ferred to the mensuring cell and the open end of the crucible was pressed together; data were extracted from the figure; reported error 4%.
Xeis Vest	Mesterhoff, H.	1932		1. 3-273. 16		Pure; the specimen was obtained from Dr. Friderich; relative resistance data were reported; resistance at temperature 273, 16 K, R <sub>0</sub> = 3, 12 x 10 <sup>-3</sup> Ω; the resistivity data were obtained by using A <sub>13,16K</sub> = 57, 6 x 10 <sup>-4</sup> Ω m.
X K E	Katerberg, J., Niemeyer, S., Penning, D., and Van Zyrveld, J.B.	1975	<	295-524		99.5-99.7 purity specimen was obtained from Atomergic Chemetals Co.; the experiment was measured with the sample held under an arm of pure argon; data were extracted from figure.
Kate	Katerberg, J., et al.	1975	∢	328-776		Similar to the above specimen.
Rinck, F.	p.	1831	∢.			Pure; double distilled specimen was prepared by Prof. Gumz; cylindrical specimen 10 cm long, 1.215 cm in diameter; because of crack only small section of the specimen was used to measure the resistance; melting point 994 K; data were extracted from figure.
g S	Grube, G. and Dietrich, A.	1938		322-995		98.72 Ba, 0.31 Mg, 0.18 Zn, 0.25 Si, 0.05 Fe + Al, 0.33 Cl, rest N; + O;: melting polm 950 ±2 K; the specimen was obtained from I. G. Farbenindustrie Aktiengeseilschaft, Bitterfeld,
Š	Cook, J. G. and Laubitz, M. J.	1976		344-770	<b>9</b> 8	Pure; specimen was prepared by sublimation at 1173 K in He at 8 mm Hg, a 405 stainless steel pot was used; a Ta tube degassed at 1173 K was filled with Ba dendrites and welded shut at both ends and it was kept at 1173 K in vacuum for three days in order to drive off as much H as possible, finally the Ta was removed from the Ba casting using a lathe in a glove box containing inert gas; the residual resistance ratio of the sample was 55; measurements were taken with increasing temperature; data were extracted from the smooth figure; no thermal expansion correction on data.

TABLE 16. MEASCREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF BARIUM B9 (Temperature Dependence) (continued)

Cur. Ref. No. No.	itef. No.	Author(s)	Year	Method	Year Method Temp. Used Range, K	Name and Specimen Designation	Composition (weight percent), Specifications, and Remarks
ã. ₹	2	16 84 Cook, J.G. and Laubitz, M.J.	1976		344-615	Ba3	The above specimen; the sample was first cooled to 620 K and after a 10 hr period measurements were taken with decreasing temperature.
7.	Š	17 54 Cook, J.G. and Laubitz, M.J.	1976		423-716	Ba3	The above specimen was allowed to react with H <sub>2</sub> at 535 K; measurements were taken with increasing temperature.
18 %		Cook, J. G. and Laubitz, M. J.	1976		485-716	ВаЗ	The above specimen; measurements were taken with decreasing temperature.
19 61		Cook, J.G. and Lsubitz, M.J.	1976		295-742	ВаЗ	The above specimen was allowed for II, charging at 620 K; measurements were taken with increasing temperature.
20 34		Cook, J.G. and Laubitz, M.J.	1976		295-742	ВаЗ	The above specimen; measurements were taken with decreasing temperature.
21 84		Cook, J.G. and Laubitz, M.J.	1976		324-739	Ba2	Commercially pure; residual resistance ratio was 10; data were extracted from the smooth figure and without thermal expansion correction.

TABLE 17. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BARIUM Bs (Temperature Dependence)

	<b>Q</b>	CURVE 12 (cont.)	573 148									CURVE 13							513 120.0														CURVE 14	322	
	Q.	CURVE 9 (cont.)	1154 309			CCRVE 10				20.47 1.61		273, 16 57.6*		CURVE 11					407 79.2					505 140 597 140		CURVE 12								240	
[Temperature, T. K; Rosistivity, p. 10 dm]	<b>a</b>	CURVE 8 (cont.)	361 34.3															395 54.5*		o man	CONVES	900	201	363		513 132									
(Temperature, T. K	Ft.	CURVE 7 (cont.)	250 31.4			256 37.7		CURVE 8		20 0.7	28 1.7	46 3.5	67 5.8						161 15.5																
	Q F	CURVE 6 (cont.)	139 17.9													249 34.0			CURVE 7							1.29									
	Q.	CURVE 1	4.2 1.51	100 10.51					CLRVF 2		533 228					1:36 412		CLRVE 3	989 306.0 ± 11			CLRVE 4		300	7 11812		1.26 2.57		75.00 16.39		CURVE 6			122 16.0	. Not shown in figure.

TABLE 17. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF BARIUM B& (Temperature Dependence) (continued

423 64.0 473 76.7 570 81.0 570 81.0 623 84.1 659 86.3						
		CURVE	CURVE 16 (cont.)	CURVE	VE 20	
	9.3	223	102.5	295	38.04	
	70.7	572	109.3	322	45.8	
	76.7	598	115.6	343	47.5*	
	81.0	615	121.9	360	51.5*	
	8.1			375	55.8*	
	85.9	CC	CURVE 17	399	62.7*	
	80.3	1	1	411	67.7	
•	61.4	423	67,3*	431	76.0	
	46.9	4	*6.07	458	2	
	25.2	3		479	201	
		¥	6	707	113	
		707		9 6 6	122.04	
		673	. 5	070	50.001	
		5 9		9 6		
	e . 6	ŝ	6.621	20 C	5.00	
	2.5	70	130.6	029	197, 1	
3	6.27	97,	6.191	1.29	200.14	
		-		20	Z03. I.	
		5	CURVE 18	674	207.8*	
CURVE 15	21			700	211.9*	
		495	6.96	742	219.9*	
	£.9	498	103.8			
	51.4	516	114.4		CURVE 21	
	55.1	521	116.6			
8	57.1	98	127.1	324	50.6	
	67.6	597	136.3	343	55.4	
	82.3	699	159.0	368	62.5	
	92.1	716	161.9*	386	67.6	
	9.96			399	72.6	
198	110.6	CC	CURVE 19	417	19.5	
	123.6	•		431	9	
	127.5	295	38.0	453	8 26	
	0 22	323	42.8	470		
200	141 4	3	47.0	807	2.71	
		2 6			2.921	
	9.101	9 1	0.10	200	172.8	
	61.0	375	55.00	284	184.3	
		388	62.7	<b>5</b> 98	192.7	
CLRVE 16	9	428	72.7	909	196.5	
	ı	447	79.4	618	200.2	
	£.9³	466	88.3	634	204.1	
	51.4	<b>4</b>	97.0	674	211.5	
	55.14	498	107.6	708	918.3	
399	58.2	528	133.0	726	0.00	
	7	5	164.6	730	2.6	
	2 2 3	8 65	2.75	}	÷.	٠
	0.00	000	107			
146	75.4	627	200.1			
		23	1 202			
	7.60		1.50			
			80,70			
		8	211.9			
		742	219.9			

#### 4.6. RADIUM

Radium, with atomic number 88, is a brilliant white, radioactive metal, and is the last member of Group II A elements. Its density has been estimated to be about 5 g cm<sup>-3</sup>, which is, however, questionable. The melting and boiling points of radium have been given as about 973 K and 1900 K, respectively. Radium has no stable isotope and has sixteen radioactive isotopes known to exist, with half-lives ranging from less than 1 millisecond ( $^{216}$ Ra) to 1620 years ( $^{226}$ Ra). One gram of the longest-lived  $^{226}$ Ra undergoes 3.7 x 10 $^{10}$  disintegrations per second; this amount of radioactivity has been defined as one curie. Radium occurs in nature and is present in all uranium minerals in trace quantities.

### Temperature Dependence

Although no information appears to have been published regarding the electrical resistivity of radium, a value of 0.186 W cm<sup>-1</sup> K<sup>-1</sup> attributed to Chirkin [87] for the room temperature thermal conductivity of radium does appear in the Handbook of the Physicochemical Properties of the Elements edited by Samsonov [88]. Neither the basis of this value nor its probable reliability is known.

We have roughly estimated the lattice thermal conductivity of radium at 293 K to be 0.013 W cm<sup>-1</sup> K<sup>-1</sup> by extrapolation to the atomic number 88 of a curve drawn through the lattice thermal conductivity values of calcium, strontium, and barium in a logarithmic graph of lattice thermal conductivity versus atomic number. The lattice thermal conductivity values of calcium, strontium, and barium are taken from Cook and Van der Meer [73]. Using the Wiedermann-Franz-Lorenz law, the electrical resistivity at 293 K is estimated to be 41 x  $10^{-8}$   $\Omega$  m.

On the basis of the expected similarities between radium and other cubic-structure alkaline earth elements, namely calcium, strontium, and barium, we have roughly estimated the provisional intrinsic electrical resistivity of radium from 200 to 500 K by a least-mean-square-error fitting to the intrinsic electrical resistivity values of calcium, strontium, barium with a logarithmic equation with temperature and atomic number as the independent variables. The resulting equation is as follows:

$$\log_{10} \rho_{i} = -0.95 \log_{10} T - 1.18 \log_{10} Z + 1.37 \log_{10} T \times \log_{10} Z$$
 (14)

where Z is the atomic number and T is the absolute temperature.

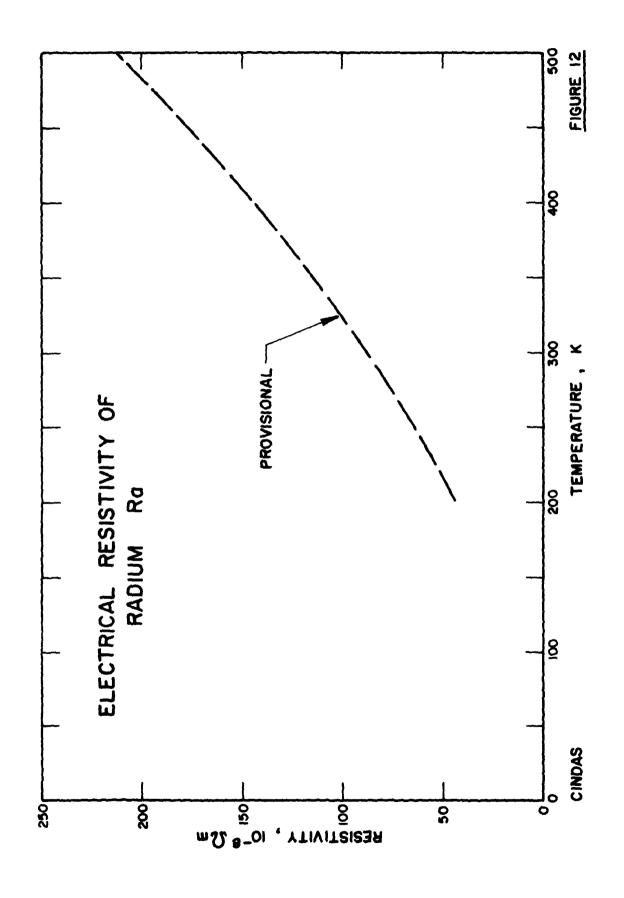
The provisional values are listed in Table 18 and shown in Figure 12. The uncer-

tainty in the provisional values is believed to be within  $\pm$  80%. The room temperature electrical resistivity value is about two times of the value calculated from Chirkin's thermal conductivity data.

TABLE 18. PROVISIONAL ELECTRICAL RESISTIVITY OF RADIUM (Temperature Dependence)

[Temperature, T, K; Intrinsic Resistivity,  $\rho_{\rm i}$ ,  $10^{-8}~\Omega$  m]

T	$ ho_{ m i}$
200	44
225	54
250	65
273.15	76
<b>29</b> 3	85
300	88
350	115
400	145
450	177
500	212



#### 5. SUMMARY AND CONCLUSIONS

The electrical resistivities of alkaline earth elements have been surveyed and studied over the years by a number of investigators, including Meaden [89] and Cook, Laubitz, and Van der Meer [71, 73, 84]. Electrical resistivity data are presented also in a number of handbooks such as those of Kaye and Laby [90], Landolt-Börnstein [91], AIP [92], CRC [93], etc. However, their main concern is to provide a general picture by giving only one or a few particular sets of data, and only a limited temperature range is covered.

The purpose of the present work is quite different from that of the above mentioned works. There are two major aims: (1) to exhaustively search the open literature so that all the available experimental data are comprehensively compiled, and (2) to generate recommended reference values by critical evaluation, analysis, and synthesis of the existing experimental data. These aims are now achieved. This work has presented the most comprehensively compiled experimental data and information on the electrical resistivity of alkaline earth elements and has provided the recommended reference values over a very wide range of temperature. The recommended values were obtained by least squares fitting of the selected experimental data or by correlating the related properties.

A comparison of electrical resistivity data from the literature with the present recommended values are shown in Table 19. Table 19 shows that the recommended electrical resistivity values from the various sources are quite different, up to 100% in some cases, that the more recent values are not necessarily closer to the truth, and that many of the values contained in popular handbooks are much in error. This attests to the need of reliable reference values such as those generated in the present work.

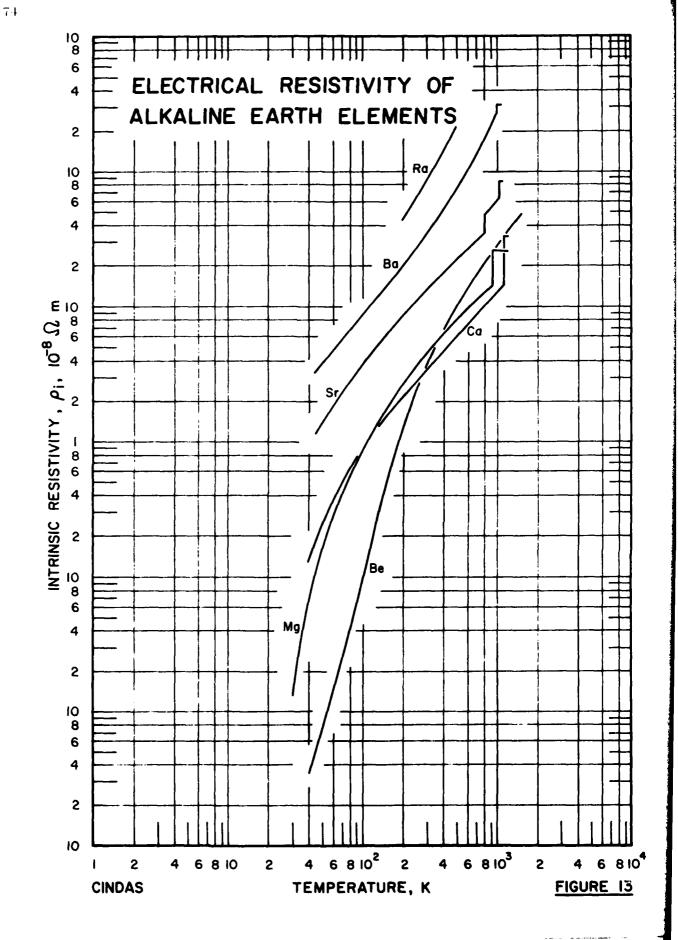
With a view to bring out any similarities or differences between the recommended values for the alkaline elements, the recommended values of the intrinsic resistivities for all the six elements are shown together in Figure 13. It can be seen from Figure 13 that the electrical resistivities of calcium, strontium, barium, and radium which have cubic crystalline structure, form a nice family of curves with systematic variations, those of heavier elements being the higher. The electrical resistivities of beryllium and magnesium, which have hexagonal crystalline structure, vary differently from the above mentioned and from each other. Their cross-over is due to the fact that beryllium has a much higher melting point.

TABLE 19. COMPARISON OF ELECTRICAL RESISTIVITY DATA FROM THE LITERATURE WITH THE PRESENT RECOMMENDED VALUES

				Total Res	Total Resistivity, $\rho$ , $10^{-8}\Omega$ m	m ℧ <sub>Զ-</sub> (		
Element	Temperature K	Present work	CRC	AIP	Kaye & Laby		Landolt & Börnstein	Cook, et al.
		(1976)	(1974)	(1972)	(1966)	(1965)	(1960)	(1973-6)
	20	0.0336	,	0.0054	•	0.0054	į	ı
ď	273.15	3.02	4.0 (293K)	2.72	2.8	2.72	3.2	•
DQ.	1000	27.5	,	1	26 (973 K)	1	ı	
	1500	49.9	1	1	1	1	ı	ı
	20	0.0123	,	0.0125	•	0.0125	,	•
26.00	273.15	4.05	4.45 (293 K)	3.94	3.9	3.94	4.31	ı
Mg	922	14.7	,	í	ı	1	,	ı
	1200	25.6	I	ſ	ŧ	ı	,	ı
	20	0.0600				1		0.104 (30 K)
ć	273.15	3.11	3.91	3.61 (293 K) 6.8	K) 6.8	3.6 (295 K)	.) 4.06	3.20 (277 K)
2	1000	12.8	ı	. 1	f			
	1150	33.0	ı	r	ſ	ı	į	ı
	20	0.918	] 	2.48		2.48		•
ć	273.15		23.0 (293 K)	21.8	23	21.8	30.3	12.5
70	1000			ı	1		1	1
	1093	84.7	1	,	ı	1	ı	I
	20	0.940	•	0.98	r	0.98	J	1
ģ	.15	30.2	ı	36.3	09	36.3	36.0	33
Pa		275	1	ı	,	ı	J	ı
	1050	303	ı	į	ı	1	i	1
	200	44*	<b>1</b>	,	ŀ	1	ı	ı
Ra	.15	*92	•	ı	ı	1	ı	•
	200	212*	ı	1	,	ı	,	•

Intrinsic resistivity

The values in the AIP Handbook are taken from the book by Meaden so that they are identical.



## 6. REFERENCES

- Touloukian, Y. S., Kirby, R. Y., Taylor, R. E., and Desai, P. D., "Thermal Expansion Metallic Elements and Alloys," Volume 12 of <u>Thermophysical</u>
   <u>Properties of Matter The TPRC Data Series</u>, Plenum Press, New York, 1440 pp., 1975. (T80643)
- 2. Matthiessen, A. and Vogt, C., "The Influence of the Temperature on the Electrical Conductivity of Alloys," Ann. Phys., 122, 19-68, 1864. (E62373)
- 3. Bass, J., "Deviations from Matthiessen's Rule," Advan. Phys. <u>21</u>(91), 431-604, 1972. (E82610)
- 4. Cimberle, M. R., Bobel, G., and Rizzuto, C., "Deviations from Matthiessen's Rule at Low Temperatures: An Experimental Comparison Between Various Alloy Systems," Adv. Phys. 23(4), 639-71, 1974. (E65579)
- 5. Grüneisen, E., "The Dependence of the Electrical Resistivity of Pure Metals from the Temperature," Ann. Phys., 16(5), 530-40, 1933. (E58987)
- 6. Mott, N. F., "The Resistance of Liquid Metals," Proc. Roy. Soc. (London), 146A, 465-72, 1934. (E60808)
- 7. Voigt, W., Textbook of Crystalphysics, Teubner, Leipzig, p. 959, 1928. (E
- 8. Nichols, J. L., "Orientation and Temperature Effects on the Electrical Resistivity of High-Purity Magnesium," J. of Applied Phys., 26(4), 470-72, 1955. (E19181)
- 9. Grüneisen, E. and Adenstedt, H., "The Effect of Transverse Magnetic Fields Upon the Electrical and Thermal Conductivity of Pure Metals at Low Temperatures," Ann. Phys. 5, 31(8), 714-44, 1938. (E58988)
- 10. Grüneisen, E. and Erfling, H. D., "Electric and Thermal Resistance of Beryllium Crystals in a Transverse Magnetic Field," Ann. Phys. 38, 399-420, 1940. (E59509)
- 11. Erfling, H. D. and Grüneisen, E., "Further Studies of Beryllium Crystals in Transverse and Longitudinal Magnetic Field," Anual der Physik 2, 5(41), 89-99, 1942. (E58989)
- 12. Martin, A. J., Bunce, J. E. J., and Tilbury, P. D., "A Study of the Electrical Conductivity of Beryllium and the Effect of Purity," J. of the Less-Common Metals, 4(2), 191-198, 1962. (E10676)
- 13. Mitchell, M. A., "Electrical Resistivity of Beryllium," J. Appl. Phys., 46(11), 4742-6, 1975. (E90107)

- 14. Falge, R. L., Jr., "Superconductivity of Hexagonal Beryllium," Physics Letter, A 24, 579, 1967. (E29835)
- 15. Yoshihiro, K. and Glover, R. E., III, "Carrier Concentration and the Superconducting Beryllium Films," Proc. Int. Conf. Low Temp. Phys. 13th 1972, 3, 547-51, 1974. (E88045)
- 16. Williams, J. M., Hinkle, N. E., and Eatherly, W. P., "Effect of Neutron Irradiation at Cryogenic Temperatures and Subsequent Annealing on the Thermal Conductivity and Electrical Resistivity of Beryllium," Oak Ridge Natl. Lab. Rept. 1972 ORNL-TM-3914, 145 pp. 1972. (E49673)
- 17. Powell, R. W., "The Thermal and Electrical Conductivities of Beryllium," Phil. Mag., 44 (353), 645-663, 1953. (E15807)
- 18. Losana, L., "Investigation on Beryllium," Aluminio 8, 67-75, 1939. (E64840)
- 19. Berteaux, F., "Electrical and Thermal Properties of Superconductors," Rev. Gen. Elec., 79(1), 7-14, 1970. (E61643)
- 20. Reich, R., Kinch, V. Q., and Bonmarin, J., "Study of Resistivity of Beryllium Samples of Different Purities as a Function of Temperature and Determination of Debye Temperatures of this Metal (F)," Academic des Sciences. Comptes Rendus, 256 (26), 5558-61, 1963. (E12551)
- 21. Tye, R. P., "Thermophysical Properties of Hot Pressed Beryllium," Dynatech Rept. 796 NASA-CR-9627, 1, 1-33, 1968. (E66505)
- 22. Ho, J. and Wright, E. S., "Electrical Resistivity of Beryllium," Lockheed Aircraft Corp. Missiles and Space Div. Rept. No. LMSD-288140. Contract No. Nord. 17017 AD-241 410, 1-1/14-1, 1960. (E11609)
- 23. White, G. K. and Woods, S. B., "Thermal and Electrical Conductivities of Solids at Low Temperatures," Canadian Journal of Physics, 33, 58-73, 1955. (E12395)
- 24. Spangler, G. E., Herman, M., Arndt, E. J., Hoover, D. B., Damiano, V. V., Tint, G. S., and Lee, C. H., "Preparation and Evaluation of High Purity Beryllium," Frank Inst. Lab. for Res. and Development. Final Rept., Oct. 1961-Oct. 1962. F-B 1933, Contract No. Now 62-0536
- 25. Lewis, E. J., "Some Thermal and Electrical Properties of Beryllium," Phys. Rev. 34(12), 1575-87, 1929. (E16875)
- 26. McLennan, J. C. and Niven C. D., "Electrical Conductivity at Low Temperatures," Phil. Mag. 4, 386-404, 1927. (21015)

- 27. Meissner, W. and Voigt, B., "Measurements with the Help of Aquid Helium XI, Resistance of Pure Metals at Low Temperature," Ann. Physik, 5, 7, 761-97, 892-936, 1930. (E58984)
- 28. Campbell, J. F., Goodwin, H. B., Wagner, H. J., Douglas, R. W., and Allen, B. C., "Introduction to Metals for Elevated-Temperature Use," Battle Memorial Inst. Defense Metals Information Center, Columbus, Ohio, DMIC Rept. 160, 1-92, 1961. (E100432)
- 29. Bridgman, P. W., "The Compressibility and Pressure Coefficient of Resistance of Ten Elements," Proc. Amer. Acad., 62, 207-26, 1927. (E65793)
- 30. Babkina, M. A., Zhermunskaya, L. B., Timofeeva, Z. A., and Tsukanova, N. V., "The Properties of Fine Beryllium Wire," Metal Science and Heat Treatment (8), 674-6, 1972. (E63245)
- 31. Yamaguchi, M., Takahashi, Y., Takasaki, Y., and Ohta, T., "A Note on the Transport Properties of Metallic Beryllium," Bull. Fac. Eng. Yokohama Natl. Univ. (Japan) 23(2), 175-78, 1974. (E67169)
- 32. Denton, H. W., "Low Temperature Electrical Resistivity of Uranium and Beryllium," A. E. R. E. Rept. No. G/R 101, 1947. (E94476)
- 33. Kuczynski, G. C., "Electronic Structure of Beryllium," Lockheed Aircraft Corp. Missles and Space Div., Rept. No. LMSD-288140 ASTIA AD-241 140, 1-23, 1960. (E13591)
- 34. Tye, R. P. and Quinn, J. E., "Thermal Conductivity of Hot Pressed Beryllium Blak," Proc. Symp. Thermophys. Prop., 4th Univ. Maryland, April 1-4, 1968, 144-9, 1968. (E72906)
- 35. Goene, F. and Schmid, E., "Elastical Constants, Electrical Resistivity and Thermal Expansion of the Magnesium Crystal," Physik. Z. 37(11), 385-91, 1936. (E63870)
- 36. Goens, E. and Schmid, E., "Determining a Few Physical Properties of Magnesium Crystals," Natuwissenschaften 18, 376-77, 1931. (E612 1)
- 37. Schmid, E., "Contributions to Physics and Metallography of Magnesium," Z. Electr. Chem., 37, 447-59, 1931. (E100431)
- 38. Alderson, J. E. A. and Hurd, C. M., "Anisotropic Temperature Dependent Resistivity of Cd, Zn, and Mg," Phys. Rev. B 12(2), 501-08, 1975. (E 87165)
- 39. Ferrier, R. P. and Herrell, D. J., "Conduction in Amorphous Mg-Bi and Mg-Sb Alloys," J. Non-Cryst. Solids 2(3), 278-83, 1970. (E75407)

- 40. Rorschach, H. E. and Herlin, M. A., "Low Temperature Resistance Minimum in Magnesium Measured by a Mutual Inductance Method," Phys. Rev. 81(3), 467, 1951. (E18602)
- 41. Spohn, D. A. and Webber, R. T., "Resistance Minimum of Magnesium Electrical and Thermal Resistivities," Phys. Rev. <u>105</u>(5), 1427-33, 1957. (E19401)
- 42. Sharkoff, E. G., "Impurity Effects on the Thermal Conductivity of Magnesium at Low Temperature, Ph.D. Thesis," Massachusetts Institute of Technology, 78 pp., 1953. (E100430)
- 43. Kondo, J., "Resistance Minimum in Dilute Magnetic Alloys," Progr. Theor. Phys. (Kyoto), 32(1), 37-49, 1964. (E62131)
- 44. Roll, A. and Motz, H., "The Electrical Resistivity of Molten Metals," Z. Metalik. 48(5), 272-80, 1957. (E60873).
- 45. Delaplace, J. et al., "Low Temperature Neutron Radiation Damage and Recovery in Magnesium," Phys. Statucs Solidi, 30(1), 119-26, 1968. (E37908)
- Das, S. B. and Gerritsen, A. N. "Deviation from the Matthiessen Rule Due to Possible Changes in the Phonon Spectrum of Dilute Magnesium Alloys," Phys. Rev. 135(4A), A1081-8, 1964. (E59020)
- 47. Hedgcock, F. T. and Muir, W. B., "Influence of Lattice Scattering on Mathiessen's Rule in Dilute Binary Magnesium Alloys," Phys. Rev., 136(2A), A561-8, 1964. (E17556)
- 48. Seth, R. S. and Woods, S. B., "Electrical Resistivity and Deviations from Matthiessen's Rule in Dilute Alloys of Aluminum, Cadmium, Silver and Magnesium," Phys. Rev., <u>B2</u>(8), 2961-72, 1970. (E45213)
- 49. Powell, R. W., Hickman, M. J., and Tye, R. P., "The Thermal and Electrical Conductivity of Magnesium and Some Magnesium Alloys," Metallurgia, 70(420), 159-63, 1964. (E17259)
- 50. Van Zytveld, J. B., Enderby, J. E., and Collings, E. M., "Electrical Resistivities of Liquid Alkaline Earth Metals," J. Phys. (Metal Phys.), F2, 73-78, 1972. (E59114)
- Scala, E. and Robertson, W. D., "Electrical Resistivity of Liquid Metals and of Dilute Liquid Metallic Solutions," Trans. Amer. Inst. Mining Eng. 197, 1141-47, 1953. (E61314)

- 52. Lorenz, L., "The Thermal and Electrical Conductivities of Metals," III Weber Das Leitungsvermögen Der Metalle Für Wärme und Elektricität, Ann. Physik, 13(3), 582-606, 1881. (E89796)
- 53. Das, R. B. and Gerritsen, A. N., "Electrical Resistivity of Dilute Alloys of Magnesium and Neodymium," J. of Appl. Phys., 33(11), 3301-04, 1962. (E7218)
- 54. Vand, V., "A Theory of the Irreversible Electrical Resistance Changes of Metallic Films Evaporated in Vacuum," Physical Society, Proceedings <u>55</u>(3), 222-47, 1943. (E10697)
- Baveja, K. D., "Electrical Resistivities of Metals by the Method of Magnetic Damping," J. of Sci. and Industrial Res., 20B, 343-44, 1961. (E11676)
- 56. Hedgcock, F. T., Muir, W. B., and Walbingfold, E., "The Electrical Resistance of Dilute Magnesium and Aluminum Alloys at Low Temperature," Can. J. of Phys. 38(3), 376-84, 1960. (E14737)
- 57. Schofield, F. H., "The Thermal and Electrical Conductivities of Some Pure Metals," Royal Soc. of London, Proc. 107, 206-27, 1925, (E27041)
- Niccolai, G., "Electrical Resistivity of Metals Between Very High and Very Low Temperatures," Ueber Den Elektrischen Widerstand Der Metalle Zwischen Sehr Hohen Und Sehr Tiefen Temperaturen, Physikalische Z. 9(11), 367-72, 1908. (E27515)
- 59. Salkovitz, E. I., et al., "Transport Properties of Dilute Binary Magnesium Alloys," Phys. Rev. 105(3), 887-96, 1957. (E19397)
- 60. Hein, R. A. and Falge, R. L., "Resistance Minimum of Magnesium Electrical Resistivity Below 1 Degree K," Phys. Rev. 109(4), 1433-4, 1957. (E19402)
- 61. Hedgcock, F. T. and Muir, W. B., "Thermoelectric Effects in Magnetism, Zinc, and Aluminum Containing Traces of Manganese," Physical Soc. of Japan, J., 16(2), 2599-2600, 1961. (E9937)
- 62. Bijvoet, J. et al., "The Electrical Resistivities of Dilute Magnesium Niobium and Magnesium Gadolinium Alloys," Solid State Comm., 1(7), 237-40, 1963. (E12977)
- 63. Panova, G. KH., et al., "Some Characteristic Features of the Temperature Dependent of the Electrical Resistivity of Magnesium Alloys Containing Heavy Non-Magnetic Impurities," Soviet Phys. JETP, <u>26</u>(2), 283-85, 1968, (E34246)
- 64. Grube, G. and Burkhardt, A., "The Electrical Conductivity, the Thermal Expansion and the Hardness of Mg-Zn Alloys," Z. Elektro Chem. 35(6), 315, 1929. (E60551)

- 65. Staebler, J., "Electrical and Thermal Conductivity and the Number of Wiedermann Franz of Light Metals and Magnesium Alloys," Ph.D. Thesis Tech. Hochschule (of Breslau), 35 pp., 1929. (E22782)
- 66. Mannchen, W., "Heat Conductivity, Electrical Conductivity and the Lorenz Number for a Few Light Metal Alloys," Z. Metallk, 23, 193-6, 1931. (E64153)
- 67. Heal, T. J., "Magnesium and Its Alloys," Nuclear Eng., 3(23), 52-61, 1958. (E61251)
- 68. Katerberg, J., Niemeyer, S., Penning, D., and Van Zytveld, J. B., "Electronic Properties and Phase Transitions in Ca, Sr and Ba at Elevated Temperatures," J. Phys., F5(5), LT4-9, 1975. (E90862)
- 69. Smith, J. F., Carlson, O. N., and Vest, R. W., "Allotropic Modifications of Calcium," J. Electro. Chem. Soc., 103, 409, 1956. (E59130)
- 70. Swiaber, C. L., "The Specific Resistance and Thermo-Electric Power of Metallic Calcium", Phys. Review 10(6), 601-8, 1917. (E92411)
- 71. Cook, J. G., Laubitz, M. J., and Van der Meer, M. R., "The Electrical Resistivity, Thermal Conductivity, and Thermoelectric Power of Calcium from 30 K to 300 K," Can. J. of Physics, 53, 486-97, 1975. (E66318)
- 72. Kayser, F. X. and Sederquist, S. D., "The Electrical Resistivity of f.c.c. Calcium from 4.2 to 300 °K," J. Phys. Chem. Solids, 28, 2343-46, 1967. (E32629)
- 73. Cook, J. G. and Van der Meer, M. P., "The Transport Properties of Ca, Sr and Ba," J. Phys., F3(8), L130-33, 1973. (E51817)
- 74. Rinck, E., "Concerning an Allotropic Transformation of Calcium in the Solid State," Compt. rend. Acad. Sci. Paris, 192, 421, 1931. (E59045)
- 75. Frank, V. and Jeppessen, O. G., "The Hall Coefficient of Calcium, Phys. Rev. 89, 1153, 1950. (E18657)
- 76. Rinck, E., "The Allotropic Transformation of Strontium," Compt. Rend. Acad. Sci. Paris, 234, 845-47, 1952. (E74448)
- 77. McWhan, D. B., Rice, T. M., and Schmid, P. H., "Metal-Semiconductor Transition in Ytterbium and Stronium at High Pressure," Physical Review, 177(3), 1063-71, 1969. (E38228)
- 78. Rashid, M. S. and Kayser, F. X., "The Electrical Resistivity of a Commercial Grade of Strontium from 80° to 400° K," J. of Less Common Metals, 24(1), 107-8, 1971. (E48982)

- 79. Meissner, W., Franz, H., and Westerhoff, H., "Measurements with the Aid of Liquid Helium. 15. Resistance of Barium, Indium, Thallium, Graphite and Titanium at Low Temperatures," Ann. der Physik, 5, 13, 555-63, 1932. (E58986)
- 80. Rashid, M. S. and Kayser, F. X., "The Electrical Resistivity of Distilled Burium from 20 to 400 K," J. Less-Common Met., (Switzerland), 24(3), 253-57, 1971. (E59603)
- 81. Rinck, E., "The Allotropic Transformation of Solid State Barium," C. R. Acad. Sci. Paris 193, 1328-30, 1931. (E74656)
- 82. Güntherodt, H. J., Hauser, E., and Künzi, H. V., "The Electrical Resistivity of Liquid Barium," J. Physics, F5(5), 889-92, 1975. (E91899)
- 83. Grube, G. and Dietrich, A., "Electrical Conductivity and Phase Diagram at Binary Alloys. The Alloys of Barium with Bismuth, Magnesium and Lead," Z. Elektro. Chem. 44(10), 755-67, 1938. (E5960)
- 84. Cook, J. G. and Laubitz, M. J., 'The Electrical Resistivity and Thermopower of Pure and of Hydrogen-charged Barium," Can. J. of Phys., <u>54</u>(9), 928-37, 1976. (E96888)
- 85. Genter, R. B. and Grosse, A. V., "Electrical Conductivity of Liquid Barium and an Estimate of Its Thermal Conductivity," High Temperature Science, 3(6), 504-10, 1971. (E60097)
- 86. Müller, W. E., 'Optical Properties and Electron Band of Europium and Barium," Phys. Kondens, Materic. <u>6</u>, 243-68, 1967. (E32852)
- 87. Chirkin, V. S., Thermal Conductivity of Industrial Materials, Mashgiz, 1962.
- 88. Samsonov, G. V., (Editor), <u>Handbook of the Physicochemical Properties of the Element IFI/Plenum Data Corp.</u>, New York, 141 pp., 1968.
- 39. Meaden, G. T., Electrical Resistance of Metals, Plenum Press, New York, 218 pp., 1965.
- 90. Kaye, G. W. and Laby, T. H., <u>Tables of Physical and Chemical Constants and Some</u>

  <u>Mathematical Functions</u>, Thirteenth Edition, John Wiley and Sons, Inc., New York,
  p. 92, 1966.
- 91. Landolt, H. H., "Numerical Values and Functions of Physics, Chemistry, Astronomy Geophysics, and Technics," Vol. 6 of <u>Electrical Properties I</u>, Berlin, Springer, 952 pp. 1960.

- 92. Gray, P. E. (Editor), American Institute of Physics Handbook, 3rd Edition, McGraw Hill Book Co., New York, 2342 pp., 1972.
- 93. Weast, R. C. (Editor), Handbook of Chemistry and Physics, 54th Edition, The Chemical Rubber Co., Ohio, 1974.
- 94. Laws, F. A., Electrical Measurements, 2nd Edition, McGraw Hill Book Co., Inc., New York, 739 pp., 1938.
- 95. van der Pauw, L. J., "A Method of Measuring the Resistivity and Hall Coefficient on Lamellae of Arbitrary Shape," Phillips Tech. Rev., 20(8), 220-4, 1958-9. (E59185)
- 96. MacDonald, D. K. C., Handbuch der Physik, Vol. XIV, 1956. (E80894)
- 97. Chambers, R. G. and Park, J. G., "Measurement of Electrical Resistivity by a Mutual Inductance Method," Brit. J. Appl. Phys., <u>12</u>, 507-10, 1961. (E59158)
- 98. Zimmerman, J. E., "Measurement of Electrical Resistivity of Bulk Metals," Rev. Sci. Instrum., 32(4), 402-5, 1961. (E58976)
- 99. Radenac, A., Lacoste, M., and Roux, C., "Apparatus Designed to Measure the Electrical Resistivity of Metals and Alloys by the Rotating Field Method up to About 2000 K," Rev. Int. Hautes Temp. Refract., 7, 389-96, 1970. (E58993)
- 100. Cezairliyan, A. and McClure, J. L., "Thermophysical Measurements on Iron Above 1500 K, Using a Transient (subsecond) Technique," J. Res. Nat. Bur. Stand., 78A(1), 1-4, 1974. (E53710)
- 101. Bean, C. P., DeBlois, R. W., and Nesbitt, L. B., "Eddy-Current Method for Measuring the Resistivity of Metals," J. Appl. Phys., 30, 1976-80, 1959. (E59131)

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#### 7. APPENDIX

# 7.1. Methods of Measuring Electrical Resistivity

## A. Steady State Methods

- 1. Voltmeter and ammeter direct reading (V) [94\*, p. 159, 119, pp. 244-5]
- 2. DC Potentiometric Method (A) [89\*, pp. 151-8]
  - a. 4-probe potentiometric method
- 3. DC Bridge Method (B) [89, pp. 141-51]
  - a. Kelvin Double Bridge
  - b. Mueller Bridge
  - c. Wheatstone Bridge
- 4. van der Pauw Method (P), [95]\*
- 5. Galvanometer Amplifier Method (G), [96\*, pp. 159-62]

### B. Non-steady State Methods

- 1. Periodic currents involved
  - a. Direct connection to sample
    - (1) AC Potentiometric Method (C) [89, pp. 161-2]
    - (2) AC Bridge Method (D) [89, p. 162]
    - (3) Q-Meter Method (Q)
  - b. No connection to sample
    - (1) Mutual Inductance Method (M) [97]\*
    - (2) Self-inductance Method (S) [98]\*
    - (3) Rotating Field Method (R) [99]\*
- 2. Non-periodic currents involved
  - Direct connection to sample
    - (1) Transient (subsecond) technique (T) [100]\*
  - b. No connection to sample
    - (1) Eddy current decay method (E) [101, 89, p. 103]

#### C. General Comments

1. Code "I" means Induction Method

This is a combination of Items B.1b. and B.2.b. above. Subsumed under I is M, R, S, or E. Used only if author indicates induction method used and does not report which specific one.

 The symbol "→" is used if method described by the author is not sufficient to assign a specific code presently used. For example, if the author stated that "AC Method"

<sup>\*</sup> References are given in Section 6.

was used in his measurement but no specifics were given, the following wording would be used in the column Composition, Specifications, and Remarks: "Experimental method described as an AC method." In the column for Method Used on the Specification Table the following symbol would appear: -.

