

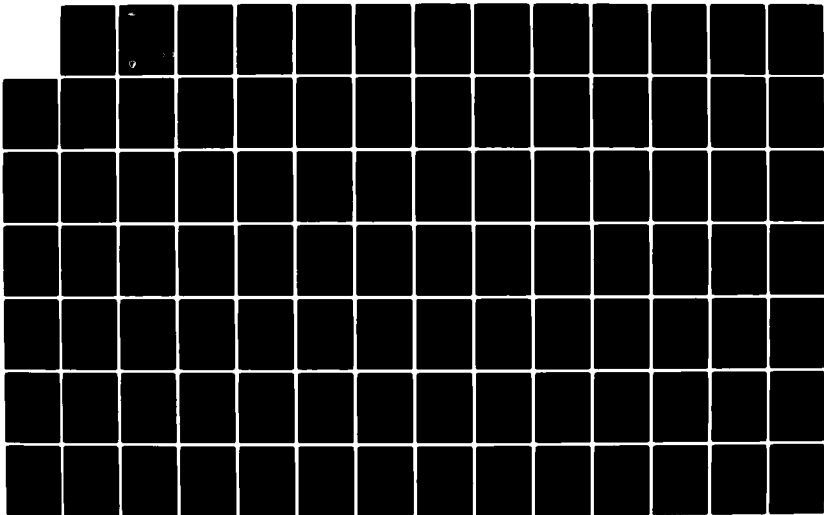
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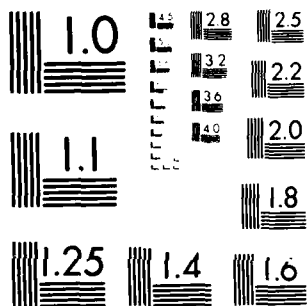
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**MODELS FOR BALLISTIC WIND MEASUREMENT
ERROR ANALYSIS VOLUME II:
USERS' MANUAL**

By

Arthur W. Dudenhoeffer

January 1983

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Under Contract DAAD07-79-C-0008

Contract Monitor: Bernard F. Engebos

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US Army Electronics Research and Development Command
Atmospheric Sciences Laboratory

White Sands Missile Range, NM 88002

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Three models for ballistic wind measurement error analysis are discussed. These models, which were originally formulated by Donald M. Swingle, are named RAWIN, RADAR, and NAVAIID. Each is applicable to a different type of meteorological acquisition system. RAWIN models the case of a balloon-borne radiosonde and ground based set for radiodirection finding and telemetry data reception. RADAR models the case in which a ground based radar | | |

set tracks an ascending balloon. NAVOID models the case in which radionavigation techniques are used to determine radiosonde position.

Expressions for the variance in the East and North components of ballistic wind are obtained in terms of bias and random measurement errors and other parameters. Also, an average error quantity called the component velocity variance is defined.

In volume I each model is described and the necessary computational expressions are derived. In volume II the utilization of the associated computer programs on the UNIVAC 1108 at White Sands Missile Range is described.

ACKNOWLEDGEMENTS

The measurement error analysis models discussed in this report were originally formulated by Donald M. Swingle for use in cost operational effectiveness analyses of competitive meteorological data acquisition systems. Numerous discussions with him were helpful in the development of this presentation.

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The author also wishes to acknowledge Douglas Anderson, who did the majority of the computer programming. William Shuster also helped in this regard.



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1.0 INTRODUCTION

The ballistic wind error analysis models, RAWIN, RADAR, and NAVAID, are formulated in Volume I of this report. The reader is referred to Volume I for a general discussion of each model and for definitions of various terms, such as ballistic line, component velocity variance (CVV), etc.

Each error analysis model has been programmed in the ASCII FORTRAN language. Each separate program is named for its corresponding model. The implementation of these programs on the UNIVAC 1108 computer at White Sands Missile Range is described in this Users' Manual.

The utilization of the auxiliary program LRDC is described in Section 10.

2.0 PRELIMINARY CONSIDERATIONS

Each of the error analysis programs RAWIN, RADAR, and NAVAIID, consists of a single main program unit. No subroutines are called. Each program may be executed in either batch or demand mode. The reader is referred to the accompanying listings for actual program source code.

Execution is similar for all three programs. One complete execution of any of the programs is referred to here as a complete run. A complete run consists of one or more separate problems. The general sequence of input and execution is described below.

| <u>STEP</u> | <u>EXPLANATION</u> |
|-------------|--|
| 1 | Three card images are read on logical unit I05. These are used to document the complete run. |
| 2 | Each disk file described in Section 4 is read once on its appropriate logical unit. The program uses these inputs to perform preliminary computations required for the complete run. |
| 3 | Two card images are read on unit I05 in order to initiate the first problem. The first card image documents the problem, while the second contains data. Execution then proceeds. Output is written to logical units I06 and I020. |
| 4 | Step 3 may be repeated for any number of problems. Program execution is terminated only by substituting an end-of-file image, i.e., @EOF, for any of the cards in Step 1 or 3. |

None of the cards noted above may be omitted. In demand usage each of the input card images is solicited by the executing program.

None of the programs requires more than 6000 words of storage (IBANK plus DBANK) on the UNIVAC 1108. The demand time required for the execution of a complete run consisting of a single problem is on the order of ten seconds.

3.0 CARD INPUT

The card image inputs described below for each program are entered on logical unit I05. Currently I05 is taken to be unit 5, which on the UNIVAC 1108 corresponds to a card reader in batch usage or to terminal keyins in demand usage. Logical unit I05 can be respecified to a different value by changing the appropriate data statement in each program.

3.1 RAWIN (Logical Unit I05)

| <u>CARD</u> | <u>DATA</u> | <u>FORMAT</u> |
|-------------|--|---------------|
| 1 | COMM | (20A4) |
| | COMM contains up to 80 characters which are used to document the complete run. A blank card may be used if no documentation is desired. | |
| 2 | COMM | (20A4) |
| | COMM contains up to 80 characters. It may contain a user supplied list of input files used for the complete run and/or it may contain further comment. This card may also be blank if desired. | |
| 3 | INTR | (A4) |
| | INTR may have the value YES or NO and must begin in column 1. If INTR is YES, results of preliminary and intermediate computations are outputted to unit 1020. If INTR is NO, only final results are outputted to unit 1020. | |
| 4 | COMM | (20A4) |
| | COMM contains up to 80 characters which are used to document the first problem. This card may be blank if desired. | |
| 5 | BEL, RE, BA, RA, RLED, RLEA, FE | Free Field |
| | This set of nonnegative real variables is input for the first problem. | |

BEL is the bias error (degrees) in elevation tracking of the apparent target.

RE is the random error (degrees) in elevation tracking of the apparent target.

BA is the bias error (degrees) in azimuth tracking of the apparent target.

RA is the random error (degrees) in azimuth tracking of the apparent target.

RLED is the random error (meters) associated with the measurement of the displacement of the launch site of the balloon-radiosonde combination from the receiving set.

RLEA is the random error (degrees) associated with the launch azimuth.

FE is the foreground elevation (degrees).

With changed information or values, cards 4 and 5 may be repeated in sequence any number of times in order to execute further problems. Values of all variables listed for card 5 must be entered for each problem, even if, for example, only one value is changed.

To terminate execution, enter a final input card containing the end-of-file image @EOF. If this is not done, the program will expect comment and data pertaining to further problems.

3.2 RADAR (Logical Unit IO5)

| <u>CARD</u> | <u>DATA</u> | <u>FORMAT</u> |
|-------------|---|---------------|
| 1,2,3 | Same description and formats as for RAWIN | |
| 4 | Initiates first problem. Same description and formats as for RAWIN. | |
| 5 | BEL, RE, BA, RA, BS, RS, RLED, RLEA, FE | Free Field |

This set of nonnegative real variables is input for the first problem.

BEL, RE, BA, RA, RLED, RLEA, and FE are the same as described for RAWIN.

BS is the bias error (meters) in slant range.

RS is the random error (meters) in slant range.

Further problems are initiated in the same manner as described for RAWIN. Input of the card image @EOF is required to terminate execution.

3.3 NAVAID (Logical Unit I05)

| <u>CARD</u> | <u>DATA</u> | <u>FORMAT</u> |
|-------------|--|---------------|
| 1,2,3 | Same description and formats as for RAWIN. | |
| 4 | Initiates first problem. Same description and mats as for RAWIN. | - |
| 5 | REX, REY, RLE | Free Field |

This set of nonnegative real variables is input for the first problem.

REX is the random error (meters) associated with fixing the East coordinate of the ascending radiosonde.

REY is the random error (meters) associated with fixing the North coordinate of the ascending radiosonde.

RLE is the random error (meters) associated with the direct measurement of the launch position.

Further problems are initiated in the same manner as described for RAWIN. Input of the card image @EOF is required to terminate execution.

3.4 Example Card Input

RAWIN:

```
EXAMPLE RAWIN RUN USING 15 ZONES AND 3 ASCENT RATES
USE INPUT FILES AR, ZHHE, WF, UV, HRE, AD712
YES
EXAMPLE RAWIN PROBLEM
.03, .05, .03, .05, 5., 0., 5.
@EOF
```

RADAR:

EXAMPLE RADAR RUN USING 15 ZONES AND 3 ASCENT RATES
USE INPUT FILES AR, ZHHE, WF, UV, HRE, AD712

YES

EXAMPLE RADAR PROBLEM

.03, .05, .03, .05, 0., 16., 5., 0., 5.

@EOF

NAVAID:

EXAMPLE NAVAIID RUN FOR 15 ZONES AND 3 ASCENT RATES
USE INPUT FILES AR, ZHHE, UV, WF

YES

EXAMPLE NAVAIID PROBLEM

100., 100., 5.

@EOF

4.0 FILE INPUT

Each of the programs, RAWIN, RADAR, and NAVAID, requires data to be inputted from similar sets of disk files. For purposes of identification each required input file is given a name. Since the names are transparent to the programs, the user may rename the files to suit his own needs.

The input files are named, respectively, AR, ZHHE, UV, WF, HRE, and AD. RAWIN and RADAR each requires all of these files. NAVAID requires only AR, ZHHE, UV, and WF. In this section the files are described in the same order that they are read by the executing program.

The logical unit which each program uses to read a given file is designated by ION, where N is an appropriate integer. For example, file AR is read from unit I02, where I02 is currently assigned the value 2. If the user desires, any or all of the logical units may be reassigned to different values by changing the appropriate data statement in the program.

The following mnemonic labels are used here to describe the records in each file.

| <u>LABEL</u> | <u>EXPLANATION</u> |
|--------------|--|
| IA | Balloon ascent rate index. IA = 1, NA |
| NA | Total number of balloon ascent rates. NA = 1, 2, 3, or 4 |
| IZ | Ballistic zone index. IZ = 1, NZ |
| NZ | Total number of ballistic zones in the complete zone structure. For the NATO zone structure NZ = 15. However, the input files may be constructed for any value of NZ between 1 and 30. |
| IL | Ballistic line index. IL = 1, NL |
| NL | Total number of ballistic lines. NL = NZ |

In each of the programs various arrays involving NZ and/or NL are currently dimensioned to allow for the NATO zone structure of 15 zones. These arrays must be redimensioned for larger zone structures.

4.1 File AR

File AR contains the balloon ascent rates.

Required by RAWIN, RADAR, and NAVAID

Logical unit I02 (currently I02 = 2)

Total number of records: NA

Number of data items per record: 1

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|-------------|---------------|
| IA | AR(IA) | Free Field |

AR(IA) is the ascent rate (meters/minute) for balloon IA.

4.2 File ZHHE

File ZHHE contains zone top altitudes and the bias and random errors associated with the determination of these altitudes.

Required by RAWIN, RADAR, and NAVAID

Logical unit I03 (currently I03 = 3)

Total number of records: NZ

Required number of data items per record: 3

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|-----------------------|---------------|
| IZ | Z(IZ), BZ(IZ), RZ(IZ) | Free Field |

Z(IZ) is the altitude (meters) at the top of zone IZ.

BZ(IZ) is the bias error (meters) in the determination of Z(IZ).

RZ(IZ) is the random error (meters) in the determination of Z(IZ).

4.3 File UV

File UV contains the zone wind profile

Required by RAWIN, RADAR, and NAVAID

Logical unit IO10 (currently IO10 = 10)

Total number of records: NZ

Required number of data items per record: 2

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------|
| IZ | U(IZ), V(IZ) | Free Field |
| | U(IZ) is the East component (meters/second) of the average wind velocity in zone IZ. | |
| | V(IZ) is the North component (meters/second) of the average wind velocity in zone IZ. | |

4.4 File WF

File WF contains the zone wind weighting factors.

Required by RAWIN, RADAR, and NAVAID

Logical unit IO1 (currently IO1 = 1)

Total number of records: NL

Required number of data items per record: NZ

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------|
| IL | WF(1), WF(2), ..., WF(IZ), ..., WF(NZ) | Free Field |
| | WF(IZ) is the wind weighting factor for zone IZ appropriate to ballistic line IL. | |

Each record must contain NZ values. This means that for IL less than NL, each record must be padded at the end with sufficient zero values to make the total number of data items in the record equal to NZ.

4.5 File HRE

For each ascent rate, file HRE contains values of positional variables relating to the launch site and to the radiosonde as it passes each zone top.

Required by RAWIN and RADAR

Logical unit IO8 (currently IO8 = 8)

Total number of records: $NA * (NZ + 1)$

Required number of data items per record: 2

For descriptive purposes we divide file HRE into NA successive groups, each group corresponding to a different value of ascent rate index IA and containing $NZ + 1$ records. The following is a description of records within any one group.

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------------|
| 1 | DISPL(IA), AZL(IA) | (F10.0, 20X, F10.2) |
| | DISPL(IA) is the distance (meters) from the RAWIN or radar receiving set to the launch site for balloon ascent rate index IA. | |
| | AZL(IA) is the launch azimuth (degrees) for ascent rate index IA. | |
| 1+IZ | E(IZ,IA), A(IZ,IA) | (20X, 2F10.2) |
| | E(IZ,IA) is the elevation (degrees) associated with radiosonde IA at the top of zone IZ. | |
| | A(IZ,IA) is the azimuth (degrees) associated with radiosonde IA at the top of zone IZ. | |

For each ascent rate there is a group of records identical to the group listed above. The groups must be appended one after the other in file HRE in the same order that the ascent rates are entered in file AR. There are no blank records or other markers of any kind between the groups.

The X fields in this file can be used to store further data for informational purposes. For example, each record of the example HRE file in the accompanying listing contains information in the following order: horizontal distance, slant range, elevation, azimuth. This example file is constructed for 3 ascent rates and 15 zones; hence, each ascent rate group contains 16 records to yield a total of 48 records for the complete file.

4.6 File AD

File AD contains bias and random errors in elevation associated with ground reflection. These errors depend on a number of factors, including the antenna voltage pattern of the particular receiving set under consideration and the dielectric constant of the reflecting surface. The example AD file in the accompanying listing is mnemonically called AD712, corresponding to a seven foot diameter antenna and a surface dielectric constant of 12. Program LRDC may be used to generate file AD in the appropriate format.

Required by RAWIN and RADAR

Logical unit I09 (currently I09 = 9)

Total number of records: 279

Required number of data items per record for records 9 through 279: 2

In the following table the index J takes on the values J = 1, 271.

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------|
| 1--8 | Miscellaneous | (////////) |
| | Records 1-8 contain miscellaneous information describing the parameters which were used to create the AD file. (See example listing.) Program LRDC writes these records when it creates this file. Although the RAWIN and RADAR programs skip these records, they must be present. They may be blank if the user desires. | |
| 8+J | BB(J), RR(J) | (8X, 2F15.8) |

BB(J) is the bias error (degrees) in elevation due to ground reflection for a possible elevation angle of $\text{FLOAT}(J-1)/3$ degrees.

RR(J) is the random error (degree) in elevation due to ground reflection for a possible elevation angle of $\text{FLOAT}(J-1)/3$ degrees.

In other words, record 9 ($J = 1$) contains error data appropriate to 0.0 degrees elevation; record 10 ($J = 2$) contains error data for 0.33 degrees elevation; record 11 ($J = 3$) contains error data for 0.67 degrees elevation, and so on at 0.33 degree intervals. Finally record 279 ($J = 271$) contains error data for 90.0 degrees elevation.

If desired by the user, the X field in each record may contain a further datum for informational purposes. In the example file AD712 in the accompanying listing, each record 9 through 279 contains information in the following order: possible elevation angle, bias error due to reflection, random error due to reflection, the index J. (All this is generated by program LRDC.)

5.0 OUTPUT

A complete run of RAWIN, RADAR, or NAVAID produces two output print files. The program writes brief output to logical unit I06 (currently I06 = 6) and more extensive output to logical unit I020 (currently I020 = 20). If the user desires, the logical units may be redesignated to different values by changing the appropriate data statement in each program.

5.1 Output to Unit I06

In demand usage this output is directed to the demand terminal. The output is formatted for printing on a CRT screen which can display 80 characters per line. In batch mode the output to unit I06 is redundant; it will nevertheless be directed to a line printer unless the user takes steps to prevent this.

The first part of the output consists of solicitations for the card images described in Section 3 of this Users' Manual.

After the computations for any given problem are complete, the program writes brief results to unit I06. These results, which are entirely numerical, may be interpreted from the following table. (In this table the term 'record' is used rather loosely, since records '2' and '3' may each consist of several lines of output.)

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------|
| 1 | AR(1) | Free Field |
| | AR(1) is the ascent rate (meters/minute) for balloon 1. | |
| '2' | (CVV(IL,1), IL=1, NL) | (1X, 5F13.6) |
| | CVV(IL,1) is the component velocity variance (knots**2) in the ballistic wind computed for ballistic line IL and ascent rate index 1. | |

'3' (SIGMA(IL),1), IL=1, NL)

(IX, 5F13.6)

SIGMA(IL,1) is the standard deviation (knots)
obtained from CVV(IL,1).

For a given problem the output described above is repeated for each balloon ascent rate specified in the run.

As an example, consider the case of 15 ballistic lines and one ascent rate. For this case record 1 consists of one printed line of data displaying the balloon ascent rate. Record '2' consists of three printed lines, five data items per line, containing the values of the CVV the values are printed from left to right in order of increasing ballistic line number IL. Record '3' also consists of three printed lines, five data items per line, and contains the values of SIGMA; the values are printed from left to right in order of increasing IL. Thus, for this example, the total number of printed lines of data is seven. For three ascent rates 21 lines are printed, and so on.

5.2 Output to Unit I020

In either demand or batch mode, this output is meant to be directed to a line printer. In order for paging and line spacing commands to be honored, logical unit I020 should represent an alternate print file.

If the user entered the value NO on input card 3, only a short, self-explanatory output listing is produced. It consists of the following:

Comments and user designated file names appropriate to the complete run;

Comments and input data for each individual problem;

For each problem, values of component velocity variance (knots)² and standard deviation (knots) computed for each ballistic line for each ascent rate.

If the user entered YES on card 3, numerous preliminary and intermediate results are also outputted. The reader is referred the accompanying listings for examples of this output for each program.

6.0 JOB CONTROL

The job control run streams required by RAWIN, RADAR, and NAVAID are similar for all three programs. The main difference among them is due to the fact that NAVAID requires fewer input files than the other two.

Two example run streams for RAWIN are shown below for use on the UNIVAC 1108. Many variations on these are possible; see Reference 1. Individual variations for RADAR and NAVAID are noted at the end of each run stream.

6.1 Initial Batch Run

This run stream achieves the following:

Creates and lists individual temporary input data files from cards, where each file is designated by an appropriate logical unit number;

Creates a permanent program file called INPUTFILES and copies the individual temporary data files into separate elements in INPUTFILES;

Compiles program source language from cards and creates an absolute executable element;

Places symbolic, relocatable, and absolute elements into a newly created permanent program file called PROGRAM;

Executes the program for a complete run consisting of one problem;

Directs all output to a specific printed labelled PR3.

| <u>STEP</u> | <u>STATEMENT</u> |
|-------------|---|
| 1 | @RUN with user supplied options and information |
| 2 | @PASSWD with valid user password |
| 3 | @SYM PRINT\$,1,PR3 |
| 4 | @ASG,CP INPUTFILES. |
| 5 | @USE I.,INPUTFILES. |
| 6 | @ASG,CP PROGRAM. |
| 7 | @USE P.,PROGRAM. |
| 8 | @ASG,CP 20. |
| 9 | @ASG,T 2.,///32 |
| 10 | @ASG,T 3.,///32 |
| 11 | @ASG,T 10.,///32 |
| 12 | @ASG,T 1.,///32 |
| 13 | @ASG,T 8.,///32 |
| 14 | @ASG,T 9.,///32 |

```

15      @DATA,IL 2.
16      -- AR deck goes here --
17      @END
18      @DATA,IL 3.
19      -- ZHHE deck goes here --
20      @END
21      @DATA,IL 10.
22      -- UV deck goes here --
23      @END
24      @DATA,IL 1.
25      -- WF deck goes here --
26      @END
27      @DATA,IL 8.
28      -- HRE deck goes here --
29      @END
30      @DATA,IL 9.
31      -- AD deck goes here --
32      @END
33      @COPY,I 2.,I.AR
34      @COPY,I 3.,I.ZHHE
35      @COPY,I 10.,I.UV
36      @COPY,I 1.,I.WF
37      @COPY,I 8.,I.HRE
38      @COPY,I 9.,I.AD
39      @FREE I.
40      @FTN,IS P.RAWIN
41      -- RAWIN source deck goes here --
42      @MAP,I ,P.RAWIN
43      IN P.RAWIN
44      END
45      @XQT P.RAWIN
46      Card stating user comment for complete RAWIN run
47      Card designating files used and/or further comment
48      Card requesting or rejecting detailed output
49      Card stating user comment for first RAWIN problem
50      Card containing data for first RAWIN problem
51      @EOF
52      @FREE 20.
53      @SYM 20.,1,PR3
54      @FIN

```

Miscellaneous Variations

Steps 49 and 50 can be repeated for any number of problems. Insert additional pairs of cards after step 50.

The L option of each @DATA card causes a listing of the file data to be produced. If this listing is not desired, omit the L option.

If a permanent file containing data elements is not desired, omit Steps 4, 5, 33--39.

If a permanent file PROGRAM is not desired, omit Steps 6--7 and replace Steps 40--45 with the following sequence:

```
@FTN,IS
-- RAWIN source deck goes here --
@XQT
```

If only file creation without execution is desired, omit Steps 45--53.

Variations for RADAR

The job control sequence for RADAR is the same as for RAWIN. In the above run stream, simply replace the designation RAWIN, wherever it occurs, with RADAR.

Variations for NAVAID

The job control sequence for NAVAID is very similar to that for RAWIN. In the above run stream, simply replace the designation RAWIN, wherever it occurs, with NAVAID. Since NAVAID does not require files HRE and AD, the following steps may be omitted: 13, 14, 27--32, 37, 38.

6.2 Typical Demand Run

It is assumed that all required input data exist in appropriately named elements in the permanent program file INPUTFILES. Also, it is assumed that an absolute element called RAWIN exists in file PROGRAM. Typically, the file PROGRAM will also contain symbolic and relocatable elements.

The creation of appropriately numbered temporary data files from elements in INPUTFILES can be a tedious task in demand mode. To facilitate the demand run, it is assumed that the user has previously created an element called, for example, RAWIN in a program file called ADDFILE. The contents of this element are shown below.

Contents of ADDFILE.RAWIN

| <u>RECORD</u> | <u>STATEMENT</u> |
|---------------|-------------------------|
| 1 | @ASG,T 2.,///32 |
| 2 | @ASG,T 3.,///32 |
| 3 | @ASG,T 10.,///32 |
| 4 | @ASG,T 1.,///32 |
| 5 | @ASG,T 8.,///32 |
| 6 | @ASG,T 9.,///32 |
| 7 | @DATA,I 2. |
| 8 | @ADD,DP I.AR . UNIT 2 |
| 9 | @END |
| 10 | @DATA,I 3. |
| 11 | @ADD,DP I.ZHHE . UNIT 3 |
| 12 | @END |
| 13 | @DATA,I 10. |
| 14 | @ADD,DP I.UV . UNIT 10 |
| 15 | @END |
| 16 | @DATA,I 1. |
| 17 | @ADD,DP I.WF . UNIT 1 |
| 18 | @END |
| 19 | @DATA,I 8. |
| 20 | @ADD,DP I.HRE . UNIT 8 |
| 21 | @END |
| 22 | @DATA,I 9. |
| 23 | @ADD,DP I.AD . UNIT 9 |
| 24 | @END |

An element ADDFILE.RADAR would be identical to the one listed above. In an element ADDFILE.NAVID the following records could be omitted: 5, 6, 19--24.

Once the appropriate ADDFILE element has been created, it can be used with any number of future runs in demand mode. The actual demand run consists of the following steps (where it is assumed that the user is already properly signed on to the terminal).

| <u>STEP</u> | <u>STATEMENT</u> |
|-------------|--|
| 1 | @ASG,AZ PROGRAM. |
| 2 | @ASG,AZ ADDFILE. |
| 3 | @ASG,AZ INPUTFILES. |
| 4 | @USE I.,INPUTFILES. |
| 5 | @ASG,CP 20. |
| 6 | @ADD ADDFILE.RAWIN |
| 7 | @XQT PROGRAM.RAWIN |
| 8 | Entry stating user comment for complete RAWIN run |
| 9 | Entry designating input files and/or further comment |

| | |
|----|--|
| 10 | Entry requesting or rejecting detailed output |
| 11 | Entry stating user comment for first RAWIN problem |
| 12 | Entry containing data for first RAWIN problem |
| 13 | @EOF |
| 14 | @FREE 20. |
| 15 | @SYM 20.,1,PR3 |
| 16 | @FIN . IF DESIRED |

Miscellaneous Variations

Steps 11 and 12 may be repeated in sequence for any number of problems.

If the user wants to test changes he may have made in the symbolic element PROGRAM.RAWIN, he can easily compile this element and execute it without retaining new relocatable and absolute elements. This is accomplished by replacing Step 7 with the following sequence:

```
@FTN,N PROGRAM.RAWIN,TPF$.RAWIN
@EOF
@XQT
```

The complete run stream listed above can also be used in batch mode if the following three cards are prefixed to it:

```
@RUN with user supplied options and information
@PASSWD with valid user password
@SYM PRINT$,1,PR3
```

The @SYM card listed here is necessary only if the user desires to direct the PRINT\$ output (logical unit 6) to the specific printer PR3. The @FIN card of Step 16 is, of course, required in batch mode. In batch usage, the user may want to omit Step 2 and replace Step 6 with the 24 actual cards listed for the element ADDFILE.RAWIN; however, this is not necessary.

Variations for RADAR

The job control language for RADAR is the same as for RAWIN. In the above run stream, simply replace the designation RAWIN, wherever it exists, with RADAR. In Step 6, the element ADDFILE.RAWIN will also work

for RADAR, or the user may add the element ADDFILE.RADAR if it has been created.

Variations for NAVAID

In the above run stream, replace the designation RAWIN, wherever it exists, with NAVAID. It is assumed that an element ADDFILE.NAVAID exists for Step 6.

7.0 MODIFICATIONS

Certain easily implemented modifications to the error analysis programs are described below:

7.1 Logical Units

The logical units numbers used in input/output operations in RAWIN, RADAR, and NAVAID are assigned to integer variables (beginning with characters IO) in a DATA statement in each program. For example, in RAWIN we have

```
DATA IO1,IO2,IO3,IO5,IO6,IO8,IO9,IO10,IO20/1,2,3,5,6,8,9,10,20/
```

The user may change the assigned values in the DATA statement to suit his convenience and/or the requirements of the computer system. However, it is recommended that IO5 always correspond to a card reader or terminal keyin, IO6 to a line printer or terminal write, and IO20 to an alternate print file.

7.2 Redimensioning of Arrays

Pertinent arrays in RAWIN, RADAR, and NAVAID are currently dimensioned to accommodate 15 zones, 15 ballistic lines, and four balloon ascent rates. The DIMENSION statement in RAWIN, for example, is of the form:

```
DIMENSION AR(4),BB(271),RR(271),U(15),DISPL(4),AZL(4),V(15),WO(15)
1          ,WF(15),Z(15),A(15,4),CVV(15,4),DXDA(15,4),DXDE(15,4),
2          DXDZ(15,4),DYDA(15,4),DYDE(15,4),DYDZ(15,4),E(15,4),
3          WV(15,15),SIGMA(15,4),VVX(15,4),VVY(15,4),W(15,15),
4          WU(15,15),BZ(15),RZ(15);COMM(20)
```

Structures of 15 zones or less do not require the redimensioning of arrays. Of course, care should be observed in preparing the various input data files, as described in Section 4. (For example, each of the programs determines the number of zones and ballistic lines from the number of records in file WF.)

Structures of up to 30 zones can be accommodated by the programs. For structures containing 16 to 30 zones, all of the array dimensions currently set at 15 must be changed to at least the maximum number of zones in the structure. For a structure of 26 zones, for example, U(15) becomes U(26), A(15,4) becomes A(26,4), W(15,15) becomes W(26,26), and so on. Array dimensions which are not currently set at 15 should not be changed.

7.3 Special Changes in NAVAID

If the user desires, any of the values assigned in the following DATA statement in NAVAID may be changed:

```
DATA TFIX, TLM, HINTL, HINTH, IZLO /1.,5.,200.,400.,5/
```

where the variables are defined below. Note the following restrictions: TFIX, TLM, HINTL, and HINTH must have real values greater than zero; IZLO may be zero or any positive integer.

| <u>VARIABLE</u> | <u>EXPLANATION</u> |
|-----------------|--|
| IZLO | Highest zone for which height interval HINTL is used. Currently IZLO = 5 |
| HINTL HINTH | Height interval (meters) centered at zone tops and utilized in fixing the East and North coordinates of the ascending balloon. HINTL is used for IZ = 1, IZLO, and HINTH is used for IZ greater than IZLO. Currently HINTL = 200. meters and HINTH = 400 meters. |
| TFIX | Time interval (seconds) between successive hyperbolic fixes of balloon position. Currently TFIX = 1. second. |
| TLM | Amount of time (minutes) used in fixing the initial launch position. Currently TLM = 5. minutes. |

8.0 PROGRAM SEQUENCE OF OPERATIONS

Each program performs computations and input/output operations in essentially the same sequence. The general program flow is given below:

| <u>STEP</u> | <u>EXPLANATION</u> |
|-------------|---|
| 1 | Solicit and read on unit I05 three card images containing general documentation and instructions for the complete run. Output the general documentation to unit I020. |
| 2 | Read data from files AR, AHHE, and UV on appropriate logical units. |
| 3 | Read zone wind weighting factors, line by line, from file WF on unit I01, and compute the weighting arrays W, WU, and WV. |
| 4 | Read files HRE and AD on the appropriate logical units. (Omit this step for NAVAID.) |
| 5 | Compute all required partial derivatives for each zone for each ascent rate. |
| 6 | Optionally output results of preliminary computations to unit I020. These results include arrays W, WU, and WV, as well as arrays containing partial derivatives. |
| 7 | Solicit and read on unit I05 the documentation card image and the data card image for specific problem, and output this information to unit I020. If @EOF is read, skip to Step 18. |
| 8 | Do through Step 14 for ascent rate index IA = 1, NA. |
| 9 | Compute launch component errors appropriate to IA. |
| 10 | Do through Step 14 for ballistic line IL = 1, NL. |
| 11 | Compute all required individual error sums for IL, IA. |
| 12 | Optionally output individual error sums for IL, IA to unit I020. |
| 13 | Compute East and North component variances in ballistic wind, VVX(IL, IA) and VVY(IL, IA), respectively. |
| 14 | Compute the component velocity variance CVV(IL, IA) in ballistic wind and its square root SIGMA(IL, IA). |
| 15 | Optionally output to unit I020 the arrays VVX and VVY. |
| 16 | Output to units I020 and I06 the arrays CVV and SIGMA. |

17 Return to Step 17 for next problem.

18 Terminate execution.

9.0 MNEMONICS

In all three error analysis programs the type of each variable is in general in accordance with the ASCII FORTRAN default rule. The only exceptions to the default rule involve certain explicitly defined character type variables containing page or column headings which are written to output. See program listings.

Numerous variables are defined elsewhere in this Users' Manual. These definitions are not repeated here. For convenience, however, reference is made below to the sections in which the definitions may be found. Also, the various error sums and required partial derivatives are discussed under separate headings. Finally, additional miscellaneous key variables are defined individually.

9.1 Variables Defined Elsewhere In This Users' Manual

It should be noted that the physical units of a variable may change during computation. For example, the program reads BA in degrees and later converts the units to radians.

Variables defined in Section 3:

BA, BEL, BS, COMM, FE, INTR, IO5, RA, RE, REX, REY, RLE, RLEA, RLED, RS.

Variables defined in Section 4:

A(IZ, IA), AR(IA), AZL(IA), BB(J), BZ(IZ), DISPL(IA), E(IZ,IA), IA, IL, IO1, IO2, IO3, IO8, IO9, IO10, IZ, NA, NL, NZ, RR(J), RZ(IZ), U(IZ), V(IZ), WF(IZ), Z(IZ).

Variables defined in Section 5.

AR(1), CVV(IL, 1), IO6, IO20, SIGMA(IL,1).

Variables defined in Section 7:

HINTH, HINTL, IZLO, TFIX, TLM.

9.2 Bias and Random Error Sums

Current values of the individual bias and random error sums are represented by nonsubscripted variable names which are comprised of four or five characters beginning with either BE or RE. See Volume I of this report of the definition of each of these sums.

9.3 Partial Derivatives (RAWIN and RADAR)

The mnemonic DpDq represents the partial derivative of p with respect to q. (However, see last paragraph under the current subheading.) In the Fortran code p and q are written as characters selected from the following list, where all distances are in meters and all angles are in radians.

| <u>p OR q</u> | <u>CHARACTER EXPLANATION</u> |
|---------------|--|
| A | Azimuth of the balloon-borne radiosonde |
| D | Distance along the surface of the earth from the RAWIN or RADAR set to a point directly below the ascending radiosonde |
| E | Elevation of the radiosonde |
| S | Slant range (RADAR only) |
| X | East coordinate of radiosonde position |
| Y | North coordinate of radiosonde position |
| Z | Altitude of the radiosonde |

For the most part, values of the partial derivative are contained in arrays indexed by IZ and IA. For example, DXDA(IZ,IA) represents the partial derivative (meters/radian) of the East coordinate of radiosonde position with respect to azimuth, appropriate to zone IZ and ascent rate index IA. Non-subscripted partials represent current computational values only. A complete listing of partial derivatives utilized in RAWIN and/or RADAR follows, where IA = 1, NA, and IZ = 1, NZ; partials used only in RADAR are marked with an asterisk*:

DDDE, DDDZ, DXDA(IZ,IA), DXDE(IZ,IA), DXDZ(IZ,IA), DYDA(IZ,IA), DYDE(IZ,IA),
DYDZ(IZ,IA), DZDE(IZ,IA)*, DXDS(IZ,IA)*.

In DO loops indexed by IA and IZ, a nonsubscripted variable of the form DpDqI
is used as a convenience to hold temporarily the array value DpDq(IZ,IA). For
example, DXDAI = DXDA(IZ,IA).

The variables DXDL, DXDLA, DYDL, and DYDLA are not strictly partial derivatives.
They are defined below.

9.4 Miscellaneous Key Variables

Definitions of many of the variables used in RAWIN, RADAR, and NAVAID are
given elsewhere in this Users' Manual, and the meanings of many others can be
readily determined from an examination of the FORTRAN code itself. Only
certain key remaining variables are defined in the following list. Indication
is made of the program(s) in which each variable is used.

| <u>VARIABLE</u> | <u>EXPLANATION</u> |
|-----------------|--|
| BER | Current value of the bias error (degrees, radians) in elevation due to ground reflection. (RAWIN, RADAR) |
| CVV(IL,IA) | Component velocity variance (knots) ² in ballistic wind associated with ballistic line IL and ascent rate IA. (RAWIN, RADAR, NAVAID) |
| DXDL | Current value of the product (meters) of the random error in launch displacement times the partial derivative of the East launch coordinate with respect to launch dis- placement. (RAWIN, RADAR) |
| DXDLA | Current value of the product (meters) of the random error in launch azimuth times the partial derivative of the East launch coordinate with respect to launch azimuth. (RAWIN, RADAR) |
| DYDL | Similar to DXDL except that the partial derivative of the North launch coordinate is used. (RAWIN, RADAR) |
| DYDLA | Similar to DXDLA except that the partial derivative of the North launch coordinate is used. (RAWIN, RADAR) |
| D2R | Conversion factor, degrees to radians. (RAWIN, RADAR) |
| FNFL | Real variable representing the number of hyperbolic fixes of balloon launch position. (NAVAID) |

FNFZ Real variable representing the number of hyperbolic fixes of balloon position in the neighborhood of any zone top. (NAVAID)

G Current value of the angle (radians) subtended at the center of the earth by the measuring set and the ascending balloon. (RAWIN, RADAR)

NFIXL Number of hyperbolic fixes of balloon launch position. (NAVAID)

NFIXZH Number of hyperbolic fixes of balloon position in the neighborhood of zone tops greater than IZLO. (NAVAID)

NFIXZL Number of hyperbolic fixes of balloon position in the neighborhood of zone tops for zones IZ = 1, IZLO. (NAVAID)

Q Current value of the ratio of the radius of the earth to the sum of the radius of the earth and the altitude of the ascending balloon. (RAWIN, RADAR)

R Mean radius (meters) of the earth. (RAWIN, RADAR)

RER Current value of the random error (degrees, radians) in elevation due to ground reflection. (RAWIN, RADAR)

SIGMA(IL, IA) Standard deviation (knots) obtained from the component velocity variance in ballistic wind appropriate ballistic line IL and ascent rate IA. (RAWIN, RADAR, NAVAIID)

TOKNOT Conversion factor by division, meters/second to knots. (RAWIN, RADAR, NAVAIID)

TOKN2 Conversion factor by division, (meters/second)² to (knots)². (RAWIN, RADAR, NAVAIID)

VV Current value of the component velocity variance (meters/second)² in ballistic wind. (RAWIN, RADAR, NAVAIID)

VVX(IL, IA) Variance (meters/second)² in the East component of ballistic wind for ballistic line IL, ascent rate IA. (RAWIN, RADAR, NAVAIID)

VVY(IL, IA) Variance (meters/second)² in the North component of ballistic wind for ballistic line IL, ascent rate IA. (RAWIN, RADAR, NAVAIID)

VV1 Current value of the variance (meters/second)² in the East component of ballistic wind. (RAWIN, RADAR).

VV2 Current value of the variance (meter/second)² in the North component of ballistic wind. (RAWIN, RADAR)

W(IZ,IL) A defined weighting factor (1/meter) appropriate to ballistic line IL and equal to the wind weighting factor per unit zone width for zone IZ minus the wind weighting factor per unit zone width for zone IZ + 1. (RAWIN, RADAR, NAVAID)

WU(IZ,IL) A defined weighting factor (1/second) appropriate to ballistic line IL and equal to the product of the East component of zone wind times the wind weighting factor per unit zone width (all for zone IZ + 1) minus the product of the East component of zone wind times the wind weighting factor per unit zone width (all for zone IZ). (RAWIN, RADAR, NAVAID)

WV(IZ,IL) A defined weighting factor (1/second) similar to WU(IZ, IL) except that the North component of zone wind is used. (RAWIN, RADAR, NAVAID)

WO(IL) A defined weighting factor (1/meter) appropriate to ballistic line IL and equal to the negative of the wind weighting factor per unit zone width for zone 1. (RAWIN, RADAR, NAVAID)

10.0 PROGRAM LRDC

10.1 Introduction

The RAWIN and RADAR models require as input an estimate of the error in elevation angle of a radiosonde's position due to the fact that a portion of the signal reaching the RAWIN or RADAR set is reflected from the surface of the earth. The LRDC model provides such an estimate.

The reader is referred to Reference 2, for example, for a general discussion of tracking by the sequential lobing (or lobe switching) and conical scan techniques. In its current form LRDC is a simplified modelling of the sequential lobing technique. Reference 3 contains a useful discussion on tracking errors due to ground reflections.

The intent here is not to give a complete description of LRDC, which is still under development, but rather to point out some of the restrictions associated with its use:

The antenna patterns for the upper beam and lower beam switched positions must have the same shape. Further development will be required to remove this restriction.

In order to find the attenuation in amplitude of a reflected (vertically polarized) beam, the model currently assumes that the reflectivity is characterized completely by the angle of incidence of the beam at the surface of the reflecting medium and by the real dielectric constant of the medium. This restriction may be removed in further development to include the effect of signal frequency and the conductivity of the reflecting medium.

For each of the possible elevation angles 0., 0.33, 0.67, 1.00, 1.33, ..., 90.0 degrees, LRDC computes a bias error in elevation and a random error in elevation due to reflection. The computed bias error associated with a given elevation is typically much smaller than the random error and may be of either sign.

Program LRDC is written in the ASCII FORTRAN language. It may be executed in either demand or batch mode.

10.2 Card Input

In either demand or batch usage, each execution of program LRDC requires one input card image from logical unit I05 (currently I05 = 5).

| <u>CARD</u> | <u>DATA</u> | <u>FORMAT</u> |
|-------------|---|---------------|
| 1 | AS, DC, SQA, B | Free Field |
| | AS is the antenna size (dish diameter) in any convenient units. This parameter is used solely for documentation. | |
| | DC is the dielectric constant of the reflecting medium. | |
| | SQA is the squint angle (degrees) appropriate to the antenna pattern of the tracking device. Typically the upper beam antenna voltage pattern entered from file AV on logical unit I02 will already have the squint angle built into it; if this is the case, enter 0. for SQA. | |
| | B is the lower beam reduction factor. Enter 1. if the lower beam voltage pattern is not reduced in magnitude from the upper beam pattern. | |

10.3 File Input

Data describing the upper beam antenna voltage pattern are inputted from file AV.

Logical unit 102 (currently 102 = 2).

Total number of records: 1080.

Required number of data items per record: 4.

In the following table I takes on the values I = 1, 1080.

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|---|---------------|
| I | T1(I), AV(I), DAV(I), DAVO(I) | Free Field |
| | T1(I) is the angle (degrees) of the antenna beam pattern measured from the forward antenna axis. It must have the value | |

given by $T1(I) = \text{FLOAT}(I-1)/3. -180.$
 In other words, $T1(1) = -180., T1(2) = -179.67, T1(3) = -179.33, \dots, T1(541) = 0.00, \dots, T1(1080) = 179.67,$ all in degrees.

AV(I) is the absolute value of the upper beam voltage corresponding to T1(I). Note that the values of the AV(I) are normalized such that the maximum value of the set of all the AV is equal to 1. (This maximum value will typically be located near, but not necessarily precisely at, index I = 541.)

DAV(I) is an antenna voltage difference given by $\text{DAV}(I) = \text{AV}(I+1) - \text{AV}(I).$

DAVO(I) is an antenna voltage difference given by $\text{DAVO}(I) = (\text{AV}(I+1) - \text{AV}(I-1))/2.$

The variables AV(I), DAV(I), and DAVO(I) should be entered to as many significant figures as is feasible.

10.4 Output

Program LRDC writes output to logical units 103 and 106. Currently 103 = 3, and 106 = 6. These units can be redesignated to different values by changing the appropriate data statement in LRDC.

10.4.1 Output to Unit I03

The output to unit I03 can be used to create an AD file suitable for use by programs RAWIN and RADAR.

Total number of records: 279.

Number of data items per record for records 9 through 279: 5.

In the following table J assumes the values J = 1, 271.

| <u>RECORD</u> | <u>DATA</u> | <u>FORMAT</u> |
|---------------|--|---------------|
| 1--8 | Miscellaneous | Various |
| | These records repeat the card input data, display the computed elevation offset (degrees), and write column headings. (See AD712 listing.) | |

8+J T1(J), ELAV(J), SIGMA(J), RMS(J), J (1X,F7.2,3F15.8,I5)

T1(J) is the possible target elevation angle (degrees) given by $T1(J) = \text{FLOAT}(J-1)/3$. (The program redefines the array T1 from its input values given in section 10.3 to the values noted here for output.)

ELAV(J) Is the computed mean elevation error (degrees) due to reflection for angle T1(J).

SIGMA(J) is the computed standard deviation (degrees) of elevation errors due to reflection for angle T1(J).

RMS(J) Is the computed root mean square error (degrees) in elevation due to reflection for angle T1(J).

J Is the counting index $J = 1,271$.

The values ELAV(J) and SIGMA(J) are taken, respectively, to be the bias and random error due to reflection for elevation angle T1(J). The quantities RMS(J) and J are outputted for informational purposes only.

The output to unit I03 is in the correct form of an AD file for input to programs RAWIN and RADAR. See the example file AD712 in the accompanying listing.

10.4.2 Output to Unit I06

In batch usage the output to unit I06 will result in a printed listing. In demand mode this output is directed to the demand terminal.

Output to unit I06 is similar to the output to unit I03. However, the following differences should be noted: The first eight records in the above table are omitted; the counting index J is replaced by an iteration index appropriate to each elevation angle.

10.5 Job Control

Shown below are two example LRDC run streams for use on the UNIVAC 1108.
Numerous variations on these are possible. See Reference 1.

10.5.1 Initial Batch Run

This run stream achieves the following:

Creates from cards a data element AV7 in a previously catalogued file called INPUTFILES;

Compiles LRDC source language from cards and creates an absolute executable element;

Places symbolic, relocatable, and absolute elements into a previously catalogued file called PROGRAM;

Executes LRDC for the case of dielectric constant of 10.;

Places the resulting output to unit 3 into the element INPUTFILES.AD710.

| <u>STEP</u> | <u>STATEMENT</u> |
|-------------|---|
| 1 | @RUN with user supplied options and information |
| 2 | @PASSWD with valid user password |
| 3 | @SYM PRINT\$,1,PR3 |
| 4 | @ASG.A INPUTFILES. |
| 5 | @USE I., INPUTFILES. |
| 6 | @ASG, A PROGRAM. |
| 7 | @USE P.,PROGRAM. |
| 8 | @ASG, T 2. |
| 9 | @ASG, T 3. |
| 10 | @DATA,I 2. |
| 11 | -- AV 7 deck goes here -- |
| 12 | @END |
| 13 | @COPY, I 2., I.AV7 |
| 14 | @FTN,IS P.LRDC |
| 15 | -- LRDC deck goes here -- |
| 16 | @MAP,I ,P.LRDC |
| 17 | IN P.LRDC |
| 18 | END |
| 19 | @XQT P.LRDC |
| 20 | 7., 10., 0., 1. |
| 21 | @ELT,ID I.AD710 |
| 22 | @ADD,D 3. |
| 23 | @END |
| 24 | @FIN |

10.5.2 Typical Demand Run

It is assumed that the input data from file AV7 exists in an element called INPUTFILES.AV7. It is also assumed that an absolute executable element called PROGRAM.LRDC exists.

The program is executed for an input dielectric constant of 12. the resulting output to logical unit 3 is catalogued in a data file called AD712 and is also placed in an element INPUTFILES.AD712.

After the user is properly signed on to the terminal, one possible sequence of commands is as follows:

| <u>STEP</u> | <u>STATEMENT</u> |
|-------------|---------------------|
| 1 | @ASG,AZ INPUTFILES. |
| 2 | @USE I.,INPUTFILES. |
| 3 | @ASG,AZ PROGRAM. |
| 4 | @USE P., PROGRAM. |
| 5 | @ASG,CP AD712. |
| 6 | @USE 3.,AD712. |
| 7 | @ASG,T 2. |
| 8 | @DATA,I 2. |
| 9 | @ADD,D I.AV7 |
| 10 | @END |
| 11 | @XQT P.LRDC |
| 12 | 7., 12., 0., 1. |
| 13 | @ELT,ID I.AD712 |
| 14 | @ADD,D 3. |
| 15 | @END |
| 16 | @FIN. IF DESIRED |

REFERENCES

1. Computer Branch, NROD, WSMR UNIVAC 1108 User Guide, Technical Report No. 69.
2. Skolnik, Merrill I., 1962, Introduction To Radar Systems, McGraw-Hill, NY.
3. Barr, William C., and Peterson, Arnold C., 1977, "Wind Measuring Accuracy Test of Meteorological Systems", ECOM-5831, Atmospheric Sciences Laboratory, US Army Electronics Command, White Sands Missile Range, NM.

COMPUTER LISTINGS

The following pages contain computer listings of programs RAWIN, RADAR, NAVAIID, and LRDC. Example input files are also listed as well as output from sample runs. (Due to its length an example File AV is not listed.)

```

1  PROGRAM RAMIN
2
3  C PROGRAM RAMIN MODELS INSTRUMENTAL (MEASUREM:IT) ERROR IN BALLISTIC
4  C WIND VELOCITY FOR RAMIN SOUNDING SYSTEMS. ITS INTENDED USE IS IN
5  C THE TRASANA COEA FOR 'AMAS' AND OTHER SYSTEMS. THE PROGRAM
6  C COMPUTES THE COMPONENT VELOCITY VARIANCE (CVV) AND ASSOCIATED
7  C STANDARD DEVIATION IN BALLISTIC WIND FOR ALL BALLISTIC LINES
8  C APPROPRIATE TO A GIVEN ZONE STRUCTURE.
9
10 C THE PROGRAM REQUIRES INPUT FROM FILES NOTED BELOW. (FOR EXAMPLE,
11 C FILE AD CONTAINS ELEVATION TRACKING ERRORS DUE TO GROUND REFLEC-
12 C TION. PROGRAM LRDC CAN BE USED TO COMPUTE THIS FILE.)
13
14 C FOR INFORMATION ON THE USE OF PROGRAM RAMIN, SEE PSL PUBLICATION
15 C 'BALLISTIC WIND MEASUREMENT ERROR ANALYSIS'
16 C VOL. 1, MODEL FORMULATION
17 C VOL. 2, USERS MANUAL
18
19 C UNIT 101 = FILE WF INPUT
20 C UNIT 102 = FILE AR INPUT
21 C UNIT 103 = FILE ZHME INPUT
22 C UNIT 105 = REMOTE TERMINAL INPUT OR CARD READER
23 C UNIT 106 = REMOTE TERMINAL OUTPUT OR LINE PRINTER
24 C UNIT 108 = FILE HRE INPUT
25 C UNIT 109 = FILE AD INPUT
26 C UNIT 1010 = FILE UV INPUT
27 C UNIT 1020 = ALTERNATE PRINT FILE TO BE DIRECTED TO LINE PRINTER
28
29 C DIMENSION AR(4),R(2/1),RM(27/1),U(15),DISPL(4),AZL(4),V(15),R0(15)
30 C ,MF(15),Z(15),A(15,4),CVV(15,4),DXCAL(15,4),UADL(15,4),
31 C DXDZ(15,4),DYDA(15,4),DYDEL(15,4),DYDZ(15,4),E(15,4),
32 C MV(15,15),SIGMA(15,4),VVX(15,4),VVY(15,4),W(15,15),
33 C MU(15,15),BZ(15),RZ(15),COMM(20)
34 C CHARACTER*6KNT,ACOMP,YCOMP
35 C CHARACTER*8STAN,VAR
36 C CHARACTER*9DEV,KNTZ
37 C CHARACTER*10MSZ
38 C DATA R,TOKNOT/637122Y,10.514789/
39 C DATA NO/4HNO /
40 C DATA XCOMP,YCOMP,MSZ/6H EAST ,6HNORTH ,10HM/SEC/0Z/
41 C DATA STAN,DEV,VAR/8HSTANDARD,9HDEVIATION,8HVARIANCE/
42 C DATA KNT,KNTZ/6HKNOT/,9H(RAOT*21/
43 C DATA 101,102,103,105,106,108,109,1010,1020/1.2,3.5,6.0,9,10,20/
44 C OZR=1./57.29578
45 C TUKN2=TOKNOT*10KNOT
46 C 1PKUB=0
47
48 C ..... GENERAL OUTPUT DOCUMENTATION .....
49 C
50 C INPUTS ARE REQUESTED TO BE USED FOR DOCUMENTING GENERAL OUTPUT

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8106 PROGRAM MARIN

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51 C TO ALTERNATE PRINT UNIT ZU.
52 C
53 WRITE (1020,1010)
54 WRITE (106,1020)
55 READ (105,1030,END=260) COMM
56 WRITE (1020,1040) COMM
57 WRITE (106,1050)
58 READ (105,1030,END=260) COMM
59 WRITE (1020,1040) COMM
60 WRITE (106,1060)
61 READ (105,1070,END=260) INTR
62 WRITE (106,1080)
63
64 C***** ENTK DATA FROM FILES AND PERFORM PRELIMINARY COMPUTATIONS *****
65 C
66 C READ TABLE OF ASCENT RATES.
67 C
68 IOERR=102
69 DO 10 IA=1,4
70 READ (102,1110,ERR=250,END=20) AR(IA)
71 NAME=IA
72 IO CONTINUE
73 C
74 C READ TABLE OF ALTITUDES, BIAS AND
75 C RANDOM ERRORS ASSOCIATED WITH ZONE TO-5.
76 C
77 20 IOERR=103
78 DO 30 IZ=1,30
79 READ (103,1110,ERR=250,END=90) Z(IZ),BZ(IZ),RZ(IZ)
80 NZ=IZ
81 30 CONTINUE
82 40 NL=NZ
83 C
84 C HEAD WIND PROFILE
85 C
86 IOERR=1010
87 READ (1010,1110,ERR=250,END=250) U(IZ),V(IZ),IZ=1,NZ)
88 C
89 C HEAD TABLE OF WIND WEIGHTING FACTORS WF, LINE BY LINE.
90 C FOR EACH ZONE FOR EACH LINE COMPUTE WEIGHTING
91 C ARRAY W AND COMPONENT VELOCITY WEIGHTING ARRAYS WU AND WV.
92 C
93 IOERR=101
94 DO 70 IL=1,NL
95 READ (101,1110,ERR=250,END=250) (WF(IZ),IZ=1,NZ)
96 B=WF(1)/Z(1)
97 WU(IL)=B
98 IF (IL.EQ.1) GO TO 60
99 DO 50 IZ=2,IL
100 IZM=IZ-1

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8106*PROGRAM MAIN

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101 BNEXT=RF(IZ)/IZ(IZ)-Z(IIZM)
102 W(IIZM,IL)=B*BNEXT
103 W(IIZM,IL)=B*BNEXT*(IZ)-B*U(IIZM)
104 W(IIZM,IL)=B*BNEXT*(IZ)-B*V(IIZM)
105 B=BNEXT
106 CONTINUE
107 W(IL,IL)=B
108 W(IL,IL)=B*U(IL)
109 W(IL,IL)=B*V(IL)
110 CONTINUE
111 DO 80 IA=1,NA
112 C
113 C READ LAUNCH DISPLACEMENT AND LAUNCH AZIMUTH
114 C FOR EACH BALLOON ASCENT RATE.
115 C
116 C IOERR=108
117 C HEAD (108,1120,ERR=250,END=250) DISPL(IA),AZL(IA)
118 C
119 C HEAD TABLES OF ELEVATION AND AZIMUTH ANGLES AT ZONE TOPS FOR
120 C EACH BALLOON ASCENT RATE.
121 C
122 C HEAD (108,1130,ERR=250,END=250)(E(IZ,IA),A(IZ,IA),IZ=1,NZ)
123 C CONTINUE
124 C
125 C HEAD BIAS AND RANDOM ELEVATION ERRORS DUE TO GROUND REFLECTION.
126 C
127 C IOERR=109
128 C HEAD (109,1220,ERR=250,END=250)
129 C HEAD (109,1230,ERR=250,END=250)(BB(IJ),RR(J),J=1,271)
130 C
131 C COMPUTE PARTIAL DERIVATIVES FOR EACH ZONE FOR EACH ASCENT RATE.
132 C
133 C DO 90 IA=1,NA
134 C DU YU IZ=J,NZ
135 C AZ=02H*(IZ,IA)
136 C CA=COS(AZ)
137 C SA=SIN(AZ)
138 C EL=D2R*(IZ,IA)
139 C SE=SIN(EL)
140 C CL=SQR(1.-SE**2)
141 C WR/(R+Z(IZ))
142 C SM=SQR(1.-((Q*CE)**2)
143 C UDDZ=G*Q*CE/5R
144 C DUDE=-((1.-Q*SE/SR)*R
145 C G=(ANCOS(CE*Q)-EL)
146 C DADZ(IZ,IA)=UDDZ*SA
147 C DTDZ(IZ,IA)=UDDZ*CA
148 C DADE(IZ,IA)=UDDZ*SA
149 C DTDE(IZ,IA)=UDDZ*CA
150 C DADA(IZ,IA)=R*G*CA

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8106*PROGRAM NAMJN

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151      YD(IZ,IA)=N*G*SA
152      YD CONTINUE
153
154      C***** OPTIONAL OUTPUT OF PRELIMINARY COMPUTATIONS *****
155      C
156      IF (INTR.EQ.N0) GO TO 140
157      WRITE (I020,I160) (IZ,IZ=1,NZ)
158      WRITE (I020,I340)
159      DO 100 IL=1,NL
160      WRITE (I020,I170) (L*(MU(IL),IL),(MU(IZ,IL),IZ=1,NZ)
161      WRITE (I020,I110)
162      C*****
163      WRITE (I020,I180)
164      WRITE (I020,I200) (IZ,IZ=1,NZ)
165      WRITE (I020,I340)
166      DO 110 IL=1,NL
167      WRITE (I020,I210) (L*(MU(IL),IL),(MU(IZ,IL),IZ=1,NZ)
168      WRITE (I020,I110)
169      C*****
170      WRITE (I020,I190)
171      WRITE (I020,I200) (IZ,IZ=1,NZ)
172      WRITE (I020,I340)
173      DO 120 IL=1,NL
174      WRITE (I020,I210) (L*(MU(IZ,IL),IZ=1,NZ)
175      WRITE (I020,I110)
176      C*****
177      WRITE (I020,I240) ARI(IA)
178      DO 130 IZ=1,NZ
179      WRITE (I020,I250) IZ,CX(IZ,IA),DY(IZ,IA),DAXE(IZ,IA),
180      DYDE(IZ,IA),UXDA(IZ,IA),OYDA(IZ,IA)
181      C*****
182      C*****
183      C*****
184      C*****
185      C*****
186      C*****
187      C*****
188      C*****
189      C*****
190      C*****
191      C*****
192      C*****
193      C*****
194      C*****
195      C*****
196      C*****
197      C*****
198      C*****
199      C*****
200      C*****

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BIUG*PROGRAM MAIN

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201 MLEA=MLEA*DZR
202 DO 180 I=1,NA
203 IF (INTR.NE.NO) WRITE (10ZU,126U) I,PROB,AR(IA)
204 AR=AR(I)/60.
205
206 C LAUNCH POINT ERROR.
207 C
208 C AZU=DZR*AZL(IA)
209 DXDL=MLEDSIN(AZU)
210 DYDL=MLEDCOS(AZU)
211 DXDLA=MLEA*DISPL(IA)*CUS(AZU)
212 DYDLA=-MLEA*DISPL(IA)*SIN(AZU)
213 DO 170 IL=1,NL
214 C
215 C COMPUTE RANDOM ERROR IN LAUNCH COMPONENTS.
216 C
217 REXL=(DXDL*WU(IL)*AR)**2+(DYDLA*WU(IL)*AR)**2
218 KEYL=(DYDL*WU(IL)*AR)**2+(DYDLA*WU(IL)*AR)**2
219 C
220 C INITIALIZE BIAS AND RANDOM ERROR SUMS FOR CURRENT
221 C BALLISTIC LINE.
222 C
223 BERX=0.
224 BERY=0.
225 BEXA=0.
226 BEXB=0.
227 KEXA=0.
228 KEXB=0.
229 BEXZ=0.
230 BEXZ=0.
231 KEYZ=0.
232 KEYZ=0.
233 BELX=0.
234 BELY=0.
235 KELX=0.
236 KELY=0.
237 KERX=0.
238 KERY=0.
239 DO 150 IZ=1,IL
240 C
241 C ASSIGN CURRENT VALUES TO USEFUL COMBINATIONS OF VARIABLES.
242 C
243 WAX=ARIW(IZ,IL)
244 RZ1=8Z(IZ)
245 RZ1=RI(IZ)
246 RZ1W=BZ1*WAR
247 RZ1W=RZ1*WAR
248 DXDZ1=DXDZ(IZ,IA)
249 DYDZ1=DYDZ(IZ,IA)
250 DXDA1=DXDA(IZ,IA)

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8106P0008AH MAIN

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251  D0AI=DY0A(IZ,IA)
252  D0EI=DX0E(IZ,IA)
253  D0EI=DY0E(IZ,IA)
254  D0EI=DY0E(IZ,IA)
255  C INCREMENT ALTITUDE ERROR SUMS
256  C
257  BEAZ=BEAZ+BZIM*DAUZI+MV(IZ,IL)*BZI
258  BEYZ=BEYZ+BZIM*DUZII+MV(IZ,IL)*BZII
259  REAZ=REAZ+(RZIM*DAUZI+MV(IZ,IL)*RZII)*2
260  REYZ=REYZ+(RZIM*DUZII+MV(IZ,IL)*RZII)*2
261  C
262  C FIND ERRORS IN ELEVATION DUE TO GROUND REFLECTION.
263  C
264  EL3=J*(EL3+IA)-FE)*I.
265  IEL=EL3
266  IP=IEL+I
267  BEH=BB(IEL)*IEL3-IEL)*IBB(IP)-BB(IEL)
268  BER=BB(IEL)*IEL3-IEL)*IBR(IP)-RR(IEL)
269  BER=BER*02M
270  RER=RER*02M
271  C
272  C INCREMENT ELEVATION ERROR SUMS
273  C
274  BELKE=BELKE+BEL*DADEI*BAR
275  BERKE=BERKE+BER*DADEI*BAR
276  BELYE=BELYE+BEL*DYDEI*BAR
277  BERYE=BERYE+BER*DYDEI*BAR
278  RELKE=RELKE+(RE*DADEI*BAR)*2
279  RERKE=RERKE+(RE*DADEI*BAR)*2
280  RELYE=RELYE+(RE*DYDEI*BAR)*2
281  RERYE=RERYE+(RE*DYDEI*BAR)*2
282  C
283  C INCREMENT AZIMUTH ERROR SUMS.
284  C
285  BEXA=BEXA+BA*DXDAI*BAR
286  BEYA=BEYA+BA*DYDAI*BAR
287  REXA=REXA+(RA*DXDAI*BAR)*2
288  REYA=REYA+(RA*DYDAI*BAR)*2
289  C
290  150
291  C OPTIONAL OUTPUT OF THE INDIVIDUAL ERROR SUMS FOR BALLISTIC LINE IL
292  C
293  IF (INTR*EQ*NO) GO TO 160
294  WRITE (1020,1270) IL,BEAZ*2,BELYE*2,BERKE*2,BERYE*2,BEAX*2,BEYX*2,
295  1 2,BELYL*2,BELYE*2,BEYA*2
296  WRITE (1020,1280) RELK,REYL,REKL,RELKE,REKKE,REXA,REYZ,RELYE,
297  1  HERYE,REYA
298  C
299  C COMBINE ERROR SUMS FOR EACH WIND COMPONENT, COMPUTE CVV,
300  C AND CONVERT UNITS TO KNOTS*2.

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8106*PROGRAM MARJN

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351 NA2=0
352 GO TO 210
353
354 C OUTPUT TO TERMINAL FOR IMMEDIATE USE.
355 C
356 C 230 DO 240 IA=1,NA
357 WRITE (106,111U) AR(IA)
358 WRITE (106,136U)(CV(I),IA),IL=1,NL)
359 WRITE (106,136U),SIGMA(1L,IA),IL=1,NL)
360 CONTINUE
361
362 C LOOP BACK TO DO FURTHER PROBLEMS RELATED TO THE SAME INPUT FILES.
363 C
364 C GO TO 140
365 C
366 C ..... PROGRAM END .....
367 C
368 250 WRITE (106,141U) IOERR
369 STOP
370
371 C ..... FORMATS .....
372 C
373 C
374 C
375 I110 FORMAT (I11,752,26H ***** PROGRAM RAMIN *****//)
376 I120 FORMAT (IX,39HGENERAL DOCUMENTATION FOR PROGRAM RAMIN/IX,6HENTER
377 J 19HONE LINE OF COMMENT)
378 I130 FORMAT (20A4)
379 I140 FORMAT (10D,20A4)
380 I150 FORMAT (IX,41MON ONE LINE ENTER FILE NAMES USED AND/OM /IX,
381 J 15HFURTHER COMMENT)
382 I160 FORMAT (IX,38HDO YOU WANT OUTPUT OF PRELIMINARY AND /IX,
383 J 37HINTERMEDIATE COMPUTATION? YES OR NO)
384 I170 FORMAT (A4)
385 I180 FORMAT (IX,48HGENERAL DOCUMENTATION IS COMPLETE. PROGRAM WILL /
386 J IX,51MON READ FILES AND PERFORM PRELIMINARY COMPUTATIONS)
387 I190 FORMAT (IX,37HENTER ONE LINE OF COMMENT FOR PROBLEM,14/IX,
388 J 47H10 STOP EXECUTION ENTER AN END-OF-FILE MARKER))
389 I1100 FORMAT (IX,48MON ONE FREE FIELD LINE, ENTER NON-NEG. VALUES OF//
390 J IX,37H BEL. RE. BA, MA, MLED, MLEA, FE /IX,6H(DEG,
391 J 31HDEG, DEG, DEG. M. DEG, DEG))
392 I1110 FORMAT (I)
393 I1120 FORMAT (F10.0,2D1,F10.2)
394 I1130 FORMAT (2D1,2F10.2)
395 I1140 FORMAT (I11,7HPROBLEM,14,47X,17HMIN ERROR INPUT /55X,8HASSUMED
396 J 16HONE SIGMA ERRORS//)
397 I1150 FORMAT (/25X,10HELEVATION ,22HBIAS ERORR (DEGREES) =,F6.2,10A,
398 J 10HELEVATION ,22HRANDOM ERR (DEGREES) =,F6.2//25X,
399 J 8HAZIMUTH ,24HBIAS ERORR (DEGREES) =,F6.2,10A,8HAZIMUTH
400 J 24HRANDOM ERORR (DEGREES) =,F6.2//25X,7HDISPL. ,7HLAUNCH

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8106*PROGRAM MAIN

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401 4 IBERMUR (METERS) =F6.2,10X,14HAZIMUTH LAUNCH,7M ERROR
402 5 IIM(METERS) =F6.2//25X,11MFUMEGROUND ,11MELEVATION I
403 6 I0H(DEGREES) =F6.2)
404 K4404 (LH,62X,7HARKAY M,/,62X,9H(L/METER),/,64X,4HCONE,/,
405 16H LINE MU,10(YX,12),21/,16X,1019X,12))
406 I170 FORMAT (1H,3X,13,3X,11(E11.3),21//21X,10E11.3))
407 I180 FORMAT (1H,62X,8HARKAY M)
408 I190 FORMAT (1H,62X,8HARKAY M)
409 I200 FORMAT (63X,7H(1/SEC),/,64X,4HZONE,/,7H LINE,1019X,13),21/
410 ,7X,1019X,13))
411 I210 FORMAT (3X,13,6X,101E12.3),21//12X,10E12.3))
412 I220 FORMAT (//////)
413 I230 FORMAT (8X,2F15.8)
414 I240 FORMAT (1H,52X,19HPARTIAL DERIVATIVE>,/,50X,7HASCENT ,6HRATE ,
415 1 F6.1,6H M/MIN,/,7H ZONE,10A,4HDOZ,16X,4HDOZ,16X,
416 2 4HDOZ,16X,4HDOZ,16X,4HDOZ,16X,4HDOZ,16X,4HDOZ,16X,
417 3 7H(M/RAD),/,13011H,1//)
418 I250 FORMAT (3X,13,618X,1E12.61//)
419 I260 FORMAT (1H,8HPROBLEM ,14,40X,15HINDIVIDUAL SUMS,/,49X,7HASCENT ,
420 1 6HRATE =F6.1,6H M/MIN,/,14X,10HUNITS ARE 10H(M/SEC),/2,//
421 2 /,8H LINE,34X,7HBEAZ,/,2,4X,8HBELE,/,2,3X,8HBERL,/,2,3X,
422 3 7HBEYA,/,2,4X,7HBEYE,/,2,4X,8HBELE,/,2,3X,8HBERYE,/,2,3X,
423 4 7HBEYA,/,2,/,40X,4HREAL,7X,4HREAL,7X,4HREAL,7X,4HREAL,7X,
424 5 5HREAL,6X,4HREAL,7X,4HREAL,7X,4HREAL,7X,4HREAL,6X,
425 6 4HREAL,/,13211H,1//)
426 I270 FORMAT (4X,13,9H BIAS ,22X,8(1X,FIU.6))
427 I280 FORMAT (7X,9H RANGUM,10(1X,FIU.61//)
428 I290 FORMAT (1H,8HPROBLEM ,14,36X,27HCOMPONENT VELOCITY VARIANCE//)
429 I300 FORMAT (22H ASCENT RATE (M/MIN) =,8X,F6.1,22X,F6.1,22X,
430 1 F6.1)
431 I310 FORMAT (7H0 LINE,6X,4(8X,A8,4X,A8))
432 I320 FORMAT (13X,4(19X,A9))
433 I330 FORMAT (13X,4(18X,A9,5X,A6))
434 I340 FORMAT (130(1H,1//)
435 I350 FORMAT (3X,13,10X,41X,FIU.5,2X,FIU.5,3X))
436 I360 FORMAT (1X,5F13.6)
437 I370 FORMAT (1H,8HPROBLEM ,14,40X,22H VARIANCE IN COMPONENTS,/)
438 I380 FORMAT (7H0 LINE,5X,4(10X,A6,6X,A6))
439 I390 FORMAT (13X,4(18X,A8,4X,A8))
440 I400 FORMAT (14X,4(6X,A10,2X,A10))
441 I410 FORMAT (130H END-OF-FILL ON ERROR ON UNIT ,12)
442 I420 FORMAT (44H EXECUTION OF THE PROGRAM IS NOW TERMINATED )
443 END

```

81U6 PROGRAM RADAR

```

1 PROGRAM RADAR
2
3 C PROGRAM RADAR MODELS INSTRUMENTAL (MEASUREMENT) ERROR IN BALLISTIC
4 C WIND VELOCITY FOR RADAR SYSTEMS.
5 C IT COMPUTES THE COMPONENT VELOCITY VARIANCE (CVV) AND ASSOCIATED
6 C STANDARD DEVIATION IN BALLISTIC WIND FOR ALL BALLISTIC LINES
7 C APPROPRIATE TO A GIVEN ZONE STRUCTURE.
8 C
9 C THE PROGRAM REQUIRES INPUT FROM FILES NOTED BELOW. IFOR EXAMPLE,
10 C FILE AD CONTAINS ELEVATION TRACKING ERRORS DUE TO GROUND REFLEC-
11 C TION. PROGRAM LROC CAN BE USED TO COMPUTE THIS FILE.)
12 C
13 C FOR INFORMATION ON THE USE OF PROGRAM RADAR, SEE PSL PUBLICATION
14 C 'BALLISTIC WIND MEASUREMENT ERROR ANALYSIS'.
15 C VOL. 1, MODEL FORMULATION
16 C VOL. 2, USERS MANUAL
17 C
18 C UNIT 101 = FILE WF INPUT
19 C UNIT 102 = FILE AR INPUT
20 C UNIT 103 = FILE ZMHE INPUT
21 C UNIT 105 = REMOTE TERMINAL INPUT OR CARD READER
22 C UNIT 106 = REMOTE TERMINAL OUTPUT OR LINE PRINTER
23 C UNIT 108 = FILE MHE INPUT
24 C UNIT 109 = FILE AD INPUT
25 C UNIT 1010 = FILE UV INPUT
26 C UNIT 1020 = ALTERNATE PRINT FILE TO BE DIRECTED TO LINE PRINTER
27 C
28 C DIMENSION AR(4),RR(27),R(127),U(15),DISPL(4),AZL(4),V(15),W(15)
29 C ,WF(15),Z(15),A(15,4),CVV(15,4),DXDA(15,4),DXDL(15,4),
30 C DZD(15,4),DZDE(15,4),DXDZ(15,4),DYDA(15,4),DYDE(15,4),
31 C DYDZ(15,4),E(15,4),W(15,15),S(15,15),SIGMA(15,4),VVA(15,4),
32 C VVT(15,4),W(15,15),MU(15,15),BZ(15),RZ(15),CUMM(20)
33 C
34 C CHARACTER*6KNT,XCOMP,YCOMP
35 C LCHARACTER*8STAN,VAR
36 C CHARACTER*9DEV,KNTZ
37 C CHARACTER*10MSZ
38 C DATA H,TOKNOT/637122Y,,0.514789/
39 C DATA NO/4HNO /
40 C DATA STAN,DEV,VAR/8HSTANDAKD,9HDEVIA TION,8HVARIANCE/
41 C DATA KNT,KNTZ/6H1KNO1,9H1KNO1*2/
42 C DATA ACOMP,YCOMP,MSZ/6H EAST ,6HNROUTH ,10H1M/SEC)02/
43 C DZM=1.757.29578
44 C TOKNTZ=TOKNOT,TUKNOT
45 C IPHUB=0
46 C
47 C ***** GENERAL OUTPUT DOCUMENTATION *****
48 C
49 C INPUTS ARE REQUESTED TO BE USED FOR DOCUMENTING GENERAL OUTPUT
50 C TO ALTERNATE PRINT UNIT 1040.

```

```

51 C
52 WRITE (1020,1010)
53 WRITE (106,1020)
54 READ (105,1030,END=240) CUMH
55 WRITE (1020,1040) CUMH
56 WRITE (106,1050)
57 READ (105,1030,END=240) CUMH
58 WRITE (1020,1040) CUMH
59 WRITE (106,1060)
60 READ (105,1070,END=240) INTR
61 WRITE (106,1080)
62
63 C***** ENTER DATA FROM FILES AND PERFORM PRELIMINARY COMPUTATIONS *****
64 C
65 C READ TABLE OF ASCENT RATES.
66 C
67 IOEMR=102
68 DO 10 IA=1,4
69 READ (102,1130,ERR=250,END=20) AR(IA)
70 NAME=IA
71 DO CONTINUE
72 C
73 READ TABLE OF ALTITUDES, BIAS AND
74 RANDOM ERRORS ASSOCIATED WITH ZONE TOPS.
75 C
76 DO IOEMR=103
77 DO 30 IZ=1,30
78 READ (103,1130,ERR=250,END=40) Z(IZ),RZ(IZ),RZ(IZ)
79 NZ=IZ
80 DO CONTINUE
81 40 NL=NZ
82 C
83 READ WIND PROFILE.
84 C
85 IOEMR=1010
86 READ (1010,1130,ERR=230,END=230)(U(IZ),V(IZ),IZ=1,NZ)
87 C
88 READ TABLE OF WIND WEIGHTING FACTORS WF, LINE BY LINE.
89 FOR EACH ZONE FOR EACH LINE COMPUTE WEIGHTING
90 ARRAY W AND COMPONENT VELOCITY WEIGHTING ARRAYS MU AND MV.
91 C
92 IOEMR=101
93 DO 70 IL=1,NL
94 READ (101,1130,ERR=250,END=230)(WF(IZ),IZ=1,NZ)
95 W=WF(1)/Z(1)
96 W(1:IL)=8
97 IF (1L-64.1) GO TO 60
98 DO 50 IZ=2,IL
99 IZM=IZ-1
100 WNEAT=WF(IZ)/(Z(IZ)-Z(IZM))

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RDU51
RDU52
RDU53
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RDU97
RDU98
RDU99
RDU100

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8106*PROGRAM MAUAR

```

101 R(I,ZM,IL)=B-BNEXT
102 R(I,ZM,IL)=BNEXT+U(I,Z)=B+U(I,ZM)
103 R(I,ZM,IL)=BNEXT+V(I,Z)=B+V(I,ZM)
104 B=BNEXT
105 50 CONTINUE
106 60 R(I,IL)=B
107 R(I,IL)=B+U(I,IL)
108 R(I,IL)=B+V(I,IL)
109 70 CONTINUE
110 DO 80 IA=1,NA
111 C
112 C HEAD LAUNCH DISPLACEMENT AND LAUNCH AZIMUTH
113 C FUM EACH BALLOON ASCENT RATE.
114 C
115 IOEMR=109
116 HEAD(I,IO,II,IO,EMR=230,END=230) DISPL(IA),AZL(IA)
117 C
118 C HEAD TABLES OF ELEVATION AND AZIMUTH ANGLES AT ZONE TOPS FUM
119 C EACH BALLOON ASCENT RATE.
120 C
121 HEAD(I,IO,II,IO,ERR=240,END=230)(E(I,Z,JA),A(I,Z,IA),IZ=1,NZ)
122 80 CONTINUE
123 C
124 C READ BIAS AND RANDOM ELEVATION ERRORS DUE TO GROUND REFLECTION.
125 C
126 IOEMR=109
127 HEAD(I,IO,II,IO,EMR=230,END=230)
128 READ(I,IO,II,IO,EMR=230,END=230)(BB(J),RR(J),J=1,271)
129 C
130 C COMPUTE PARTIAL DERIVATIVES FOR EACH ZONE FOR EACH ASCENT RATE.
131 C
132 DO 90 IA=1,NA
133 DO 90 IZ=1,NZ
134 AC=DSH*A(I,Z,IA)
135 CA=CCOS(AZ)
136 SA=SSIN(AZ)
137 EL=DSH*E(I,Z,IA)
138 SE=SSIN(EL)
139 CE=SCURT(1,-SE**2)
140 V=RR/IK+Z(I,Z)
141 SM=SCURT(1,-(V*CE)**2)
142 DDDZ=V*V*CE/SR
143 DUDE=1-1+V*SE/SR)*K
144 G=ARCOS(CE*V)-LL
145 OADZ(I,Z,IA)=DDUZ*SA
146 OYDZ(I,Z,IA)=DDUZ*CA
147 OXDE(I,Z,IA)=DDUE*SA
148 OYDE(I,Z,IA)=DDUE*CA
149 OXDA(I,Z,IA)=R*G*CA
150 OYDA(I,Z,IA)=R*G*CA

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BI06*PROGRAM MADAR

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151      DYDA(IZ,IA)=R*G*SA
152      UZ05(IZ,IA)=SR
153      DZDE(IZ,IA)=SIN(U)
154      YD CONTINUE
155
156      C***** OPTIONAL OUTPUT OF PRELIMINARY COMPUTATIONS *****
157      C
158      IF (INTR*EQ.NO) GO TO 140
159      WRITE (1020,1160)(IZ,IZ=1,NZ)
160      WRITE (1020,1240)
161      DO 100 IL=1,NL
162      WRITE (1020,1170) IL,MU(1L),M(IZ,1L),IZ=1,NZ)
163      WRITE (1020,1130)
164      C
165      WRITE (1020,1180)
166      WRITE (1020,1200)(IZ,IZ=1,NZ)
167      WRITE (1020,1340)
168      DO 110 IL=1,NL
169      WRITE (1020,1210) IL,IRU(IZ,1L),IZ=1,NZ)
170      WRITE (1020,1130)
171      C
172      WRITE (1020,1190)
173      WRITE (1020,1200)(IZ,IZ=1,NZ)
174      WRITE (1020,1340)
175      DO 120 IL=1,NL
176      WRITE (1020,1210) IL,(RV(IZ,1L),IZ=1,NZ)
177      WRITE (1020,1130)
178      C
179      DO 130 IA=1,NA
180      WRITE (1020,1240) AR(IA)
181      DO 130 IZ=1,NZ
182      WRITE (1020,1250) IZ,OXZ(IZ,IA),DYDZ(IZ,IA),DXDE(IZ,IA),
183      I      UYDE(IZ,IA),UXDA(IZ,IA),DYDA(IZ,IA),OZUS(IZ,IA),
184      2      OZDE(IZ,IA)
185      C
186      DO 130 CONTINUE
187      C***** ENTER USER COMMENT AND DATA FOR SPECIFIC PROBLEM *****
188      C
189      140 IPR08=IPR08+1
190      WRITE (106,1090) IPR08
191      READ (105,1030,END=240) COMM
192      WRITE (106,1100)
193      READ (105,1130,END=240) BEL,RE,BA,RA,BS,RS,RLED,RLEA,FE
194      WRITE (1020,1220) IPR08
195      WRITE (1020,1040) COMM
196      WRITE (1020,1230) BEL,RE,BA,RA,BS,RS,RLED,RLEA,FE
197      C
198      C***** DO ERROR COMPUTATIONS *****
199      C
200      BEL=BEL*02R

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RD151
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RD199
RD200

8106-PROGRAM MADAR

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201      ML=ME*DZR
202      RA=BA*DZR
203      KA=KA*DZR
204      KLEA=MLEA*DZR
205      UO 18U 1A=I,NA
206      IF (INTK.NE.NO) WRITE (JOU,IZAU) (PHUB,AK(IA)
207      ANI=ARI(IA)/60.
208
209      C LAUNCH POINT ERROR.
210
211      AZU=DZR*AZLI(IA)
212      DXUL=MLEO*SIN(AZU)
213      UTUL=MLEO*COS(AZU)
214      DXDLA=MLEA*DISPL(IA)*COS(AZU)
215      UTULA=-MLEA*DISPL(IA)*SIN(AZU)
216      DU 170 IL=I,NL
217
218      C COMPUTE RANDOM ERROR IN LAUNCH COMPONENTS.
219
220      KXL=DXDL*(MULL)*AKI**2+(DXULA*(MULL)*AF)**2
221      KYL=UTDL*(MULL)*AKI**2+(UTULA*(MULL)*AKI)**2
222
223      C INITIALIZE BIAS AND RANDOM ERROR SUMS FOR CURRENT BALLISTIC LINE.
224
225      BERX=0.
226      BERY=0.
227      BEXA=0.
228      BETA=0.
229      KETA=0.
230      KETA=0.
231      BEXS=0.
232      BEYS=0.
233      KEXS=0.
234      KETS=0.
235      BELX=0.
236      BELY=0.
237      KELX=0.
238      KELY=0.
239      KERX=0.
240      KERY=0.
241      DO 150 IZ=I,IL
242
243      C ASSIGN CURRENT VALUES TO USEFUL COMBINATIONS OF VARIABLES.
244
245      NAR=ARI*(IZ,IL)
246      DXZI=DXZI(IZ,IA)
247      OYZI=OYZI(IZ,IA)
248      DADA=DADA(IZ,IA)
249      DYDAI=DYDAI(IZ,IA)
250      OXDEI=OXDEI(IZ,IA)

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RDZU1
RDZU2
RDZU3
RDZU4
RDZU5
RDZU6
RDZU7
RDZU8
RDZU9
RDZU0
RDZU1
RDZU11
RDZU12
RDZU13
RDZU14
RDZU15
RDZU16
RDZU17
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RDZU40
RDZU41
RDZU42
RDZU43
RDZU44
RDZU45
RDZU46
RDZU47
RDZU48
RDZU49
RDZU50

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BIUS*PROGRAM *ADAR

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251 DTUEI=DYDEI(Z,IA)
252 DZDSI=DZDSI(Z,IA)
253 DZDEI=DZDEI(Z,IA)
254
255 C INCREMENT SLANT RANGE ERROR SUMS.
256 C
257 BEXS=BEXS*BS*(DXZI*WAK+DZDSI*WU(I,Z,IL))
258 BEYS=BEYS*BS*(DYZI*WAK+DZDSI*WV(I,Z,IL))
259 HEXS=HEXS*IRS*(DADZ)*WAK+DZDSI*WU(I,Z,IL)**2
260 REYS=REYS*IRS*(DYDZ)*WAK+DZDSI*WV(I,Z,IL)**2
261
262 C FIND ERRORS IN ELEVATION DUE TO GROUND REFLECTION.
263 C
264 ELJ=J*(E(I,Z,IA)-FE)*I.
265 IEL=ELJ
266 IP=IEL+1
267 BER=BB(IEI)*(ELJ-IEL)*(BB(IPI)-BB(IEI))
268 RER=RR(IEI)*(ELJ-IEL)*(RR(IPI)-RR(IEI))
269 BER=BER*DZK
270 RER=RER*DZR
271
272 C INCREMENT ELEVATION ERROR SUMS.
273 C
274 BELXE=BELXE+BEL*IDAEI*WAK+DZDEI*WU(I,Z,IL))
275 BERXE=BERXE+BER*IDAEI*WAK+DZDEI*WV(I,Z,IL))
276 BELYE=BELYE+BEL*IDYDEI*WAK+DZDEI*WV(I,Z,IL))
277 BERXE=BERXE+BER*IDYDEI*WAK+DZDEI*WV(I,Z,IL))
278 RELXE=RELXE+(RE*IDAEI*WAK+DZDEI*WU(I,Z,IL))**2
279 RELYE=RELYE+(RE*IDYDEI*WAK+DZDEI*WV(I,Z,IL))**2
280 RERXE=RERXE+(RER*IDAEI*WAK+DZDEI*WU(I,Z,IL))**2
281 RERYE=RERYE+(RER*IDYDEI*WAK+DZDEI*WV(I,Z,IL))**2
282
283 C INCREMENT AZIMUTH ERROR SUMS.
284 C
285 BEKA=BEKA*WAK+DZDAI*WAK
286 BEYA=BEYA*WAK+DYDAI*WAK
287 REKA=REKA*(RA*DXUAI*WAK)**2
288 REYA=REYA*(RA*DYUAI*WAK)**2
289
290 C
291 C
292 C
293 C
294 C
295 C
296 C
297 C
298 C
299 C
300 C

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8106*PROGRAM MADAR

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351 C LOOP BACK TO DO FURTHER PROBLEMS RELATED TO THE SAME INPUT FILES. RD351
352 C GO TO 140 RD352
353 C RD353
354 C RD354
355 C ***** PROGRAM END ***** RD355
356 C RD356
357 230 WHITE (106,141U) 10EMH RD357
358 240 WHITE (106,142U) RD358
359 STOP RD359
360 C RD360
361 C ***** FORMATS ***** RD361
362 C RD362
363 C RD363
364 C RD364
365 1010 FORMAT (1H,152,26H ***** PROGRAM RADAR *****//) RD365
366 1020 FORMAT (1X,39HGENERAL DOCUMENTATION FOR PROGRAM RADAR/1X,6MENTER RD366
367 1 19HONE LINE OF COMMENT) RD367
368 1030 FORMAT (20A4) RD368
369 1040 FORMAT (1H0,20A4) RD369
370 1050 FORMAT (1X,41HON ONE LINE ENTER FILE NAMES USED AND/OR /1X, RD370
371 1 15HFURTHER COMMENT) RD371
372 1060 FORMAT (1X,38HDO YOU WANT OUTPUT OF PRELIMINARY AND /1X, RD372
373 1 37HINTERMEDIATE COMPUTATIONS? YES OR NO) RD373
374 1070 FORMAT (A4) RD374
375 1080 FORMAT (1X,49HGENERAL DOCUMENTATION IS COMPLETE. PROGRAM WILL / RD375
376 1 1X,51HNO* READ FILES AND PERFORM PRELIMINARY COMPUTATIONS) RD376
377 1090 FORMAT (1X,37HENTER ONE LINE OF COMMENT FOR PROBLEM,14/1X, RD377
378 1 47H( TO STOP EXECUTION ENTER AN END-OF-FILE MARKER)) RD378
379 1100 FORMAT (1X,48HON ONE FREE FIELD LINE, ENTER NON-NEG. VALUES OF// RD379
380 1 1X,49H BEL. RE. BA. MA. BS. MS. PLED. MLEA. FE / RD380
381 2 1X,49H1DEG. DEG. DEG. DEG. M. M. M. M. DEG. DEG)) RD381
382 1110 FORMAT (F10.0,20X,F10.2) RD382
383 1120 FORMAT (20X,2F10.2) RD383
384 1130 FORMAT (1) RD384
385 1140 FORMAT (1) RD385
386 1150 FORMAT (8X,2F15.8) RD386
387 1160 FORMAT (1H,62X,7HARMAT W,/,62X,9H(1/METER),/,64X,4HZONE,/, RD387
388 1 16H LINE RD388
389 1170 FORMAT (1H,3X,13,3X,11E11.3),21/12X,10E11.3)) RD389
390 1180 FORMAT (1H,62X,8HARMAT W) RD390
391 1190 FORMAT (1H,62X,8HARMAT W) RD391
392 1200 FORMAT (63X,7H(1/SEC),/,64X,4HZONE,/,7H LINE,1019X,13),21/ RD392
393 1 7X,1019X,13)) RD393
394 1210 FORMAT (3X,13,6X,10E11.3),21/12X,10E11.3)) RD394
395 1220 FORMAT (1H,7HPROBLEM,14,47X,17HMINO ERROR INPUT /55X,8HASSUMED RD395
396 1 16HONE SIGMA ERRORS)) RD396
397 1230 FORMAT (/25X,10HELEVATION,22HBIAS ERROR (DEGREES) =,F6.2,10X, RD397
398 1 10HELEVATION,21HRANDOM ERR (DEGREES) 1H,F6.2//25X, RD398
399 2 8HAZIMUTH,17HBIAS ERROR (10DEGREES) =,F6.2,10X, RD399
400 3 8HAZIMUTH,17HRANDOM 17HERROR (DEGREES) =,F6.2//25X, RD400
401 4 8HRANGE,125HBIAS ERROR (METERS) =,F6.2,10X,7HRRANGE RD401

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8100 PROGRAM MADAR

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401      5      24RANDOM ERRUR (METERS) =F6.2//25X,7MDISPL. 7M LAUNCH
402      6      18ERRUR (METERS) =F6.2,10A,14MAZIMUTH LAUNCH,7M ERROR
403      7      11(METERS) =F6.2//25X,11MF0REGROUND ,11MELEVATION I
404      8      8MDECKEES12H =F6.2)
405      1240 FORMAT (11I,52X,19HPARTIAL DERIVATIVES,/,50X,7MASCENT ,6MHATE =,
406      1      F6.1,6M M/MIN,/,7M ZONE,5X,4HDXDZ,11X,4HODYZ,11X,4HDXUE
407      2      ,11X,4HODYE,11X,4HUYDA,11X,4HDLDS,11X,4HDLDE, /
408      3      ,130(11H,))
409      1250 FORMAT (13X,13,8(13X,12.6))
410      1260 FORMAT (11I,8MPROBLEM ,14,40X,15HINDIVIDUAL SUMS,/,49X,7MASCENT
411      1      6MHATE =F6.1,6M M/MIN,/,1X,10UNITS ARE 10(M/SEC)*2,/,
412      2      /,6M LINE,34X,7MDEXS*2,4X,8MBELXE*2,3X,8MDEKX*2,3X,
413      3      7MBEXA*2,4X,7MBREYS*2,4X,8MBELYE*2,3X,8MBELTE*2,3X,
414      4      7MBEYA*2,/,20X,4HREXL,7A,4HREYL,7A,4HREXS,7A,5HRELXE,6X,
415      5      5HREXAL,6X,4HREXA,7A,4HREYS,7A,5HRELYE,6X,5HREYTE,6X,
416      6      4HREYA,/,132(1H,))
417      1270 FORMAT (4X,13,5H BIAS ,22X,8(1X,F10.6))
418      1280 FORMAT (7X,9M RANDOM,10(1X,F10.6))
419      1290 FORMAT (11I,8MPROBLEM ,14,36X,27MCOMPONENT VELOCITY VARIANCE,/,
420      1      F6.1)
421      1300 FORMAT (121H ASCENT RATE, M/MIN =,8X,F6.1,22X,F6.1,22X,F6.1,22X,
422      2      F6.1)
423      1310 FORMAT (7M0 LINE,14X,(A8,4X,A8,8X))
424      1320 FORMAT (32X,4(A9,19X))
425      1330 FORMAT (13X,4(8X,A9,5X,A6))
426      1340 FORMAT (125(1H,))
427      1350 FORMAT (13X,13,10X,4(13X,F10.5,2X,F10.5,3X))
428      1360 FORMAT (11X,5F13.6)
429      1370 FORMAT (11I,8MPROBLEM ,14,40X,22H VARIANCE IN COMPONENTS,/,
430      2      F6.1)
431      1380 FORMAT (7M0 LINE,5X,4(10X,A6,6X,A6))
432      1390 FORMAT (13X,4(8X,A8,4X,A8))
433      1400 FORMAT (14X,4(6X,A10,2X,A10))
434      1410 FORMAT (130H END-OF-FILL OR ERROR ON UNIT ,12)
435      1420 FORMAT (44H EXECUTION OF THE PROGRAM IS NOW TERMINATED )
436      END

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8106*PROGRAM NAVAID

```

1  C
2  C
3  C
4  C
5  C
6  C
7  C
8  C
9  C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
18 C
19 C
20 C
21 C
22 C
23 C
24 C
25 C
26 C
27 C
28 C
29 C
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31 C
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45 C
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47 C
48 C
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50 C

PROGRAM NAVAID

PROGRAM NAVAID MODELS INSTRUMENTAL (MEASUREMENT) ERROR IN BALLISTIC
WIND VELOCITY FOR NAVAID SYSTEMS. ITS INTENDED USE IS IN
THE TRASANA COEA FOR 'FAHAS'. THE PROGRAM
COMPUTES THE COMPONENT VELOCITY VARIANCE (CVV) AND ASSOCIATED
STANDARD DEVIATION IN BALLISTIC WIND FOR ALL BALLISTIC LINES
APPROPRIATE TO A GIVEN ZONE STRUCTURE.

THE PROGRAM REQUIRES INPUT FROM FILES NOTED BELOW.

FOR INFORMATION ON THE USE OF PROGRAM NAVAID, SEE PSL PUBLICATION
'BALLISTIC WIND MEASUREMENT ERROR ANALYSIS'
VOL. 1, MODEL FORMULATION
VOL. 2, USERS MANUAL

UNIT 101 = FILE WF INPUT
UNIT 102 = FILE AR INPUT
UNIT 103 = FILE ZHME INPUT
UNIT 105 = REMOTE TERMINAL INPUT OR CARD READER
UNIT 106 = REMOTE TERMINAL OUTPUT OR LINE PRINTER
UNIT 1010 = FILE UV INPUT
UNIT 1020 = ALTERNATE PRINT FILE TO BE DIRECTED TO LINE PRINTER

DIMENSION AR(4),WF(15),W(15,15),Z(15),U(15),V(15),CV(15,4),
1 SIGMA(15,4),VVA(15,4),VVV(15,4),W(15,15),WU(15,15),
2 W(15,15),WZ(15),RZ(15),COM(120)
CHARACTER*6KNT,XCOMP,YCOMP
CHARACTER*8STAN,VAR
CHARACTER*9DEV,KNTZ
CHARACTER*10MS2
DATA TFIX,TLM,MINTL,MINTM,IZLO/I,1.5,,200.,400.,5/
DATA TOKNOT/O*514789/
DATA NO/4HNO /
DATA XCOMP,YCOMP,MS2/6H EAST ,6HNORTH ,10H(M/SEC)**2/
DATA STAN,DEV,VAR/8HSTANDARD,9HDEVIATION,8HVARIANCE/
DATA KNT,KNTZ/6H(KNOT),9H(KNOT)**2//
DATA I01,I02,I03,I05,I06,I010,I020/I,2,3,5,6,10,20/
NFIAL=INT(60.*TLM/TFIX)
TOKN2=TOKNOT*10KNOT
IPRUB=0

C..... GENERAL OUTPUT DOCUMENTATION .....
C
C INPUTS ARE REQUESTED TO BE USED FOR DOCUMENTING GENERAL OUTPUT
C TO ALTERNATE PRINT UNIT 1020.
C
WRITE (1020,1010)
WRITE (106,1020)

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51      READ (105,1030,END=210) COMH
52      WRITE (1020,1040) COMH
53      WRITE (106,1050)
54      READ (105,1030,END=210) COMH
55      WRITE (1020,1040) COMH
56      WRITE (106,1060)
57      READ (105,1070,END=210) INTR
58      WRITE (106,1090)
59
60      C***** ENTER DATA FROM FILES AND PERFORM PRELIMINARY COMPUTATION *****
61      C
62      C READ TABLE OF ASCENT RATES.
63      C
64      C
65      IOERR=102
66      DO 10 IA=1,4
67      NA=IA
68      IO CONTINUE
69
70      C READ TABLE OF ALTITUDES, BIAS AND
71      C RANDOM ERRORS ASSOCIATED WITH ZONE TOPS.
72      C
73      20 IOERR=103
74      DO 30 IZ=1,30
75      READ (103,1080,ERR=200,END=30) Z(IZ),RZ(IZ),RZ(IZ)
76      NZ=IZ
77      30 CONTINUE
78      40 NL=NZ
79
80      C INPUT WIND PROFILE.
81      C
82      IOERR=1010
83      READ (1010,1080,ERR=200,END=200) (U(IZ),V(IZ),IZ=1,NZ)
84
85      C
86      C HEAD TABLE OF WIND WEIGHTING FACTORS WF, LINE BY LINE,
87      C FOR EACH ZONE FOR EACH LINE COMPUTE WEIGHTING
88      C ARRAY W AND COMPONENT VELOCITY WEIGHTING ARRAYS WU AND WV.
89
90      IOERR=101
91      DO 70 IL=1,NL
92      READ (101,1080,ERR=200,END=200) (WF(IZ),IZ=1,NZ)
93      W=WF(I)/Z(I)
94      IF (IL.EQ.1) GO TO 60
95      DO 50 IZ=2,IL
96      ICM=IZ-1
97      SNEXT=WF(IZ)/Z(IZ)-Z(I/CM)
98      W(IZ,IL)=S*BNEXT
99      WU(IZ,IL)=S*BNEXT*U(IZ)-W*U(IZM)
100     WV(IZ,IL)=S*BNEXT*V(IZ)-W*V(IZM)

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8100*PROGRAM NAVAIU

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101 NV101
102 NV102
103 NV103
104 NV104
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124 NV124
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126 NV126
127 NV127
128 NV128
129 NV129
130 NV130
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132 NV132
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134 NV134
135 NV135
136 NV136
137 NV137
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147 NV147
148 NV148
149 NV149
150 NV150

      B=BNEXT
50  CONTINUE
60  W(IL,IL)=B
    W(IL,IL)=-B*U(IL)
    W(IL,IL)=-B*V(IL)
70  CONTINUE
C ***** OPTIONAL OUTPUT OF PRELIMINARY COMPUTATIONS *****
C
      IF (INTR.EQ.NO) GO TO 110
      WRITE (1020,1150) (IZ,IZ=1,NZ)
      WRITE (1020,1280)
      DO 90 IL=1,NL
      WRITE (1020,1160) IL,WU(IL), (W(IZ,IL), IZ=1,NZ)
      WRITE (1020,1080)
90  CONTINUE
      WRITE (1020,1170)
      WRITE (1020,1190) (IZ,IZ=1,NZ)
      WRITE (1020,1280)
      DO 90 IL=1,NL
      WRITE (1020,1200) IL,(WU(IZ,IL), IZ=1,NZ)
      WRITE (1020,1080)
100 CONTINUE
C ***** ENTER USER COMMENT AND DATA FROM TERMINALS *****
C
110 IPHUB=IPROB+1
    HEAD (105,1030,END=210) COMM
    WRITE (106,1110)
    READ (105,1080) REY,REY,KLE
    WRITE (1020,1120) IPHUB
    WRITE (1020,1040) COMM
    WRITE (1020,1130) REY,REY,KLE
C ***** DO ERROR COMPUTATIONS *****
C
      BEGIN ERROR COMPUTATION.
      DO 150 I=1,NA
      IF (INTR.EQ.NO) WRITE (1020,1210) IPROB,AR(IA)
      AR=AR(IA)/60.
      AFIAZL=INT(MINL/(AR*TFIX))

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8106 PROGRAM NAVAID

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151 MFI2M=INT(MINTM/(ARI*TFI2))
152 DO 140 IL=1,NL
153   WARD=ARI*POIIL)
154
155 COMPUTE RANDOM ERROR IN LAUNCH COMPONENTS
156
157   REXL=(WARD**2)*(REX**2/FNFL*BLE**2/2.)
158   REYL=(WARD**2)*(REY**2/FNFL*BLE**2/2.)
159
160 INITIALIZE BIAS AND RANDOM ERROR SUMS FOR CURRENT BALLISTIC LINE.
161
162   BEZ=0.
163   BEYZ=0.
164   REXZ=0.
165   REYZ=0.
166   REXS=0.
167   REYS=0.
168   FNFZ=FLOAT(FI2ZL)
169   DO 120 IZ=1,IL
170
171 C ASSIGN CURRENT VALUES TO USEFUL COMBINATIONS OF VARIABLES.
172 C
173   IF (IZ.GT.1ZLO) FNFZ=FLOAT(FI2ZM)
174   WAR=ARI*(IZ,IL)
175   BZ1=0Z1IZ)
176   RZ1=RZ1IZ)
177
178 INCREMENT ALTITUDE SUMS.
179 C
180   BEZ=BEZ+BU(IZ,IL)*BZ1
181   BEYZ=BEYZ+BV(IZ,IL)*BZ1
182   REXZ=REXZ+(BU(IZ,IL)*KZ1)**2
183   REYZ=REYZ+(BV(IZ,IL)*KZ1)**2
184   REXS=REXS+(REX*WAR)**2/FNFZ
185   REYS=REYS+(REY*WAR)**2/FNFZ
186 CONTINUE
187
188 C OPTIONAL OUTPUT OF THE INDIVIDUAL ERROR SUMS FOR BALLISTIC LINE IL
189 C
190 IF (INTR.EQ.NO) GO TO 130
191 WRITE (1020,1220) IL,REAL,REYL,BEZ**2,REXZ,REXX,BEYZ**2
192   I 2,REYZ,REY
193
194 C COMBINE SUMS IN EACH WIND COMPONENT, COMPUTE COMPONENT VELOCITY VA
195 C AND CONVERT UNITS TO KNOTS**2.
196 C
197   VVX(IL,IA)=REAL+REXZ+BEZ**2
198   VVY(IL,IA)=REYL+REYZ+BEYZ**2
199   VV=VVX(IL,IA)+VVY(IL,IA)**2
200   CVV(IL,IA)=VV/TKM2

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B1U6 PROGRAM NAVAITD

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201 SIGMA(II,IA)=SQRT(CV(II,IA))
202 CONTINUE
203
204
205 140 CONTINUE
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250 C

SIGMA(II,IA)=SQRT(CV(II,IA))
140 CONTINUE
150 CONTINUE

OPTIONAL OUTPUT OF VARIANCE IN COMPONENTS
IF (INTR.EQ.NO) GO TO 170
WRITE (102,130) (PKOR
WRITE (102,1240)(AR(IA),IA=1,NA)
WRITE (102,1310)(ACOMP,TCOMP,IA=1,NA)
WRITE (102,1320)(VAK,VAR,IA=1,NA)
WRITE (102,1330)(MS2,MS2,IA=1,NA)
DO 160 IL=1,NL
WRITE (102,1290) IL,(VVX(II,IA),VVY(II,IA),IA=1,NA)
WRITE (102,1080)
160 CONTINUE

C***** OUTPUT COMPONENT VELOCITY VARIANCE AND STANDARD DEVIATION *****
C
C OUTPUT TO ALTERNATE PRINT FILE
170 WRITE (102,1230) (PKOR
WRITE (102,1240)(AR(IA),IA=1,NA)
WRITE (102,1250)(VAK,STAN,IA=1,NA)
WRITE (102,1260)(DEV,IA=1,NA)
WRITE (102,1270)(KNT2,KNT,IA=1,NA)
WRITE (102,1280)
DO 180 IL=1,NL
WRITE (102,1290) IL,(CVV(II,IA),SIGMA(II,IA),IA=1,NA)
WRITE (102,1080)
180 CONTINUE

C
C OUTPUT TO TERMINAL FOR IMMEDIATE USE.
DO 190 IAP=1,NA
WRITE (106,1080) AR(IAP)
WRITE (106,1140)(CVV(II,IA),IL=1,NL)
WRITE (106,1140)(SIGMA(II,IA),IL=1,NL)
190 CONTINUE

C
C LOOP BACK TO DO FURTHER PROBLEMS RELATED TO THE SAME INPUT FILES.
GO TO 110

C
C
C***** PROGRAM END *****
200 WRITE (106,1340) (0EMR
210 WRITE (106,1350)
STOP

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8106-PROGRAM NAVAID

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251 C ..... FORMATS .....
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300 C
1010 FORMAT (1M1,T52.27M,..... PROGRAM NAVAID .....//)
1020 FORMAT (1X,40MGENERAL DOCUMENTATION FOR PROGRAM NAVAID/1X,6MENTER
      1 19MONE LINE OF COMMENT)
1030 FORMAT (20X4)
1040 FORMAT (1M0,20A4)
1050 FORMAT (1X,41MONE ONE LINE ENTER FILE NAMES USED AND/OK /1X,
      1 15MFURTHER COMMENT)
1060 FORMAT (1X,38MDO YOU WANT OUTPUT OF PRELIMINARY AND /1X,
      1 37MINTERMEDIATE COMPUTATIONS? YES OR NO)
1070 FORMAT (A4)
1080 FORMAT (1)
1090 FORMAT (1X,49MGENERAL DOCUMENTATION IS COMPLETE. PROGRAM BILL /
      1 1X,51MNO READ FILLS AND PERFORM PRELIMINARY COMPUTATIONS)
1100 FORMAT (1X,37MENTER ONE LINE OF COMMENT FOR PROBLEM,14/1X,
      1 47MTO STOP EXECUTION ENTER AN END-OF-FILE MARKER))
1110 FORMAT (1X,48MONE ONE FREE FIELD LINE, ENTER NOM-MES, VALUES OF//
      1 1X,17M REY, REY, RLE /1X,17M IM M )
1120 FORMAT (1M1,7MPROBLEM,14,47X,17MBOUND ERROR INPUT /55X,8MASHASSUMED
      1 16MONE SIGMA ERRORS//)
1130 FORMAT (/50X,31MEAST TRACKING ERROR (METERS) =,FB,2,//5DX,
      1 31MORTH TRACKING ERROR (METERS) =,FB,2,//50X,7MRANDOM
      2 24MLAUNCH ERROR (METERS) =,FB,2)
1140 FORMAT (1X,5F13.6)
1150 FORMAT (1M1,62X,7MARMAY W,/,62X,9M11/METER),//,64X,4MZONE,/,
      1 16M LINE WU,1019X,121,21/,16X,1019X,121))
1160 FORMAT (1M ,3X,13,3X,11(E11.3),2/(21X,10E11.3))
1170 FORMAT (1M1,62X,8MARMAY W)
1180 FORMAT (1M1,62X,8MARMAY W)
1190 FORMAT (63X,7M11/SECI,//,64X,4MZONE,/,7M LINE,1019X,131,21/
      1 17X,1019X,131))
1200 FORMAT (3X,13,6X,10(E12.3),2/(12X,10E12.3))
1210 FORMAT (1M1,8MPROBLEM ,14,41X,15MINDIVIDUAL SUMS,/,49X,7MASCENT,
      1 6MATE =,F6.1,6H M/MIN,/,1X,20MUNITS ARE (M/SEC)02,///,
      2 8M LINE,8X,4MREKL,11X,4MREYL,10X,7MREZ02,9X,4MREYZ,
      3 11X,4MREXX,10X,7MREYZ02,9X,4MREYZ,11X,4MREY,/,13211M.))
1220 FORMAT (4X,13,815X,F10.61//)
1230 FORMAT (1M1,8MPROBLEM ,14,46X,27MCOMPONENT VELOCITY VARIANCE//1
      1 16.1)
1240 FORMAT (22M ASCENT RATE (M/MIN) =,8X,F6.1,22X,F6.1,22X,
      1 16.1)
1250 FORMAT (7M0 LINE,6X,410X,A8,4X,A8))
1260 FORMAT (13X,411X,A91)
1270 FORMAT (13X,418X,A9,5X,A61)
1280 FORMAT (13011M,1//)
1290 FORMAT (3X,13,10X,413X,F10.5,2X,F10.5,3X11)
1300 FORMAT (1M1,8MPROBLEM ,14,40X,22MVARIANCE IN COMPONENTS,///)
1310 FORMAT (7M0 LINE,5X,4110X,A6,6X,A61)

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PAGE

8106 PROGRAM NAVATO

NV301
NV302
NV303
NV304
NV305

1320 FORMAT (13X,4(6X,A8,7X,A6))
1330 FORMAT (14X,4(6X,A10,2X,A10))
1340 FORMAT (30H END-OF-FILE OR ERROR ON UNIT ,I2)
1350 FORMAT (44H EXECUTION OF THE PROGRAM IS NOW TERMINATED)
END

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302
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8106*PROGRAM LRDC

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PROGRAM LRDC

C- THIS PROGRAM COMPUTES MEAN, RMS AND SIGMA OF ANTENNA POINTING
C- ERROR DUE TO GROUND REFLECTIONS FOR RAIN/RADAR TRACKING SYSTEMS
C- USING VERTICAL POLARIZATION ON BOTH TRANSMITTER AND RECEIVER.
C- RESULTING DATA ARE USED TO COMPUTE METEOROLOGICAL MEASUREMENT ERRORS
C- WHICH ARE PROVIDED TO TRASANA, MIRADCOM AND OTHERS. THESE DATA ARE
C- USED IN COEAS FOR 'FAMAS' AND OTHER SYSTEMS.
C- THESE RESULTS ARE ALSO USED BY MIRADCOM IN THE GSRs PROGRAM.
C- THE PROGRAM INPUTS ANTENNA BEAM PATTERN (PILE 102), SURFACE DIELECTRIC
C- CONSTANT(IDC), SQUINT ANGLE(SQA) AND LOWER BEAM REDUCTION FACTOR(LB).
C- IT PREPARES DISK FILE 103 AND PRINTOUT OF ELEVATION ANGLE ERRORS
C- TO INPUT FINAL SYSTEM ERROR PROGRAMS(RAWIN OR RADAR).
C- FILE 105 = INPUT, FILE 106 = PRINTEK OUTPUT
C- FILE 102 = AV, UNIT = DISK
C- FILE 103 = AD, UNIT = DISK
      DOUBLE PRECISION SZEL
      DIMENSION ELAV(271), RMS(271), SIGMA(271), AV(1080), DAV(1080),
      1 DAVD(1080), V(4), DV(4), A(4), J(11080)
      DATA 102,103,105,106/2,3,5,6/

C- ***** BEGIN PROGRAM; ENTEK CONTROL DATA FROM REMOTES *****
C-
C-1 HEAD (105,210) AS,DC,SQA,B
      ZERO=541.-1.5*SQA
      P=3.141592654

C- ***** ENTER DATA FROM DISK FILES *****
C-
C-2 READ (102,210)(I(1),AV(I),DAV(I),DAVD(I),J=1,1080)
C-
C- ***** BEGIN ERROR COMPUTATIONS *****
C-
C-3 IDC=0
      EU=0.
      10 DO 110 I2=1,271
C-4
      T=1.0/(I2-1)
      EL=TOP/540.
      S=EL*SIN(EL)
      SZEL=SEL*SEL
      H=0.
      IF (IDC.EQ.1.0R.IDC.EQ.0) GO TO 20
      SZEL=H.-SZEL
      IF (I2.EQ.1) SZEL=1.00-46
      SZEL=P/(100.*SZEL)

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810A*PROGRAM LRDC

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51 DCSEL=DC*SEL
52 SQ=SQRT(DC-CZEL)
53 M=(DCSEL-SQ)/IDCSEL*SQ)
54 SE=U.
55 SE2=0.
56 E=-.001
57
58 DU 100 13=1.40
59
60 IF (ABS(E).GT+.5.) E=-.001
61 G=13-1)*P/2U.
62 CG2M=2.*R*CGS(G)
63 L=M
64
65 A(1)=ZERO-E
66 A(2)=ZERO-E*2*T
67 A(3)=ZERO+E
68 A(4)=ZERO+E*2*T
69
70 DO 60 I=1,4
71 A(I)=A(I)
72 IV=INITIAL
73 AA=1.*IV
74 IF (IV.GT.1) IV=IV+1000
75 IF (IV.GT.1000) IV=IV-1000
76 IF (AA.EQ.A1) GO TO 40
77
78 IV=1.*IV
79 IF (IV.(I.IU80) IV)=IV-1000
80 V(1)=A(1)*V-A(2)*A(1)*AV(IV)-AV(IV))
81 DV(1)=DAV(IV)
82 GO TO 50
83
84 V(1)=AV(IV)
85 DV(1)=DAV(IV)
86
87 IF (I.LE.2) GO TO 60
88 DV(1)=B*DV(1)
89 V(1)=B*V(1)
90 CONTINUE
91 SUMV(1)=2.*V(1)+V(2)+V(3)+V(4)+V(5)+V(6)+V(7)+V(8)+V(9)+V(10)+V(11)+V(12)+V(13)+V(14)+V(15)+V(16)+V(17)+V(18)+V(19)+V(20)+V(21)+V(22)+V(23)+V(24)+V(25)+V(26)+V(27)+V(28)+V(29)+V(30)+V(31)+V(32)+V(33)+V(34)+V(35)+V(36)+V(37)+V(38)+V(39)+V(40)+V(41)+V(42)+V(43)+V(44)+V(45)+V(46)+V(47)+V(48)+V(49)+V(50)+V(51)+V(52)+V(53)+V(54)+V(55)+V(56)+V(57)+V(58)+V(59)+V(60)+V(61)+V(62)+V(63)+V(64)+V(65)+V(66)+V(67)+V(68)+V(69)+V(70)+V(71)+V(72)+V(73)+V(74)+V(75)+V(76)+V(77)+V(78)+V(79)+V(80)+V(81)+V(82)+V(83)+V(84)+V(85)+V(86)+V(87)+V(88)+V(89)+V(90)+V(91)+V(92)+V(93)+V(94)+V(95)+V(96)+V(97)+V(98)+V(99)+V(100)
92 SUMV(1)=2.*V(1)+V(2)+V(3)+V(4)+V(5)+V(6)+V(7)+V(8)+V(9)+V(10)+V(11)+V(12)+V(13)+V(14)+V(15)+V(16)+V(17)+V(18)+V(19)+V(20)+V(21)+V(22)+V(23)+V(24)+V(25)+V(26)+V(27)+V(28)+V(29)+V(30)+V(31)+V(32)+V(33)+V(34)+V(35)+V(36)+V(37)+V(38)+V(39)+V(40)+V(41)+V(42)+V(43)+V(44)+V(45)+V(46)+V(47)+V(48)+V(49)+V(50)+V(51)+V(52)+V(53)+V(54)+V(55)+V(56)+V(57)+V(58)+V(59)+V(60)+V(61)+V(62)+V(63)+V(64)+V(65)+V(66)+V(67)+V(68)+V(69)+V(70)+V(71)+V(72)+V(73)+V(74)+V(75)+V(76)+V(77)+V(78)+V(79)+V(80)+V(81)+V(82)+V(83)+V(84)+V(85)+V(86)+V(87)+V(88)+V(89)+V(90)+V(91)+V(92)+V(93)+V(94)+V(95)+V(96)+V(97)+V(98)+V(99)+V(100)
93 SUMDV=2.*V(1)+V(2)+V(3)+V(4)+V(5)+V(6)+V(7)+V(8)+V(9)+V(10)+V(11)+V(12)+V(13)+V(14)+V(15)+V(16)+V(17)+V(18)+V(19)+V(20)+V(21)+V(22)+V(23)+V(24)+V(25)+V(26)+V(27)+V(28)+V(29)+V(30)+V(31)+V(32)+V(33)+V(34)+V(35)+V(36)+V(37)+V(38)+V(39)+V(40)+V(41)+V(42)+V(43)+V(44)+V(45)+V(46)+V(47)+V(48)+V(49)+V(50)+V(51)+V(52)+V(53)+V(54)+V(55)+V(56)+V(57)+V(58)+V(59)+V(60)+V(61)+V(62)+V(63)+V(64)+V(65)+V(66)+V(67)+V(68)+V(69)+V(70)+V(71)+V(72)+V(73)+V(74)+V(75)+V(76)+V(77)+V(78)+V(79)+V(80)+V(81)+V(82)+V(83)+V(84)+V(85)+V(86)+V(87)+V(88)+V(89)+V(90)+V(91)+V(92)+V(93)+V(94)+V(95)+V(96)+V(97)+V(98)+V(99)+V(100)
94 R=2.*V(1)+V(2)+V(3)+V(4)+V(5)+V(6)+V(7)+V(8)+V(9)+V(10)+V(11)+V(12)+V(13)+V(14)+V(15)+V(16)+V(17)+V(18)+V(19)+V(20)+V(21)+V(22)+V(23)+V(24)+V(25)+V(26)+V(27)+V(28)+V(29)+V(30)+V(31)+V(32)+V(33)+V(34)+V(35)+V(36)+V(37)+V(38)+V(39)+V(40)+V(41)+V(42)+V(43)+V(44)+V(45)+V(46)+V(47)+V(48)+V(49)+V(50)+V(51)+V(52)+V(53)+V(54)+V(55)+V(56)+V(57)+V(58)+V(59)+V(60)+V(61)+V(62)+V(63)+V(64)+V(65)+V(66)+V(67)+V(68)+V(69)+V(70)+V(71)+V(72)+V(73)+V(74)+V(75)+V(76)+V(77)+V(78)+V(79)+V(80)+V(81)+V(82)+V(83)+V(84)+V(85)+V(86)+V(87)+V(88)+V(89)+V(90)+V(91)+V(92)+V(93)+V(94)+V(95)+V(96)+V(97)+V(98)+V(99)+V(100)
95 DV(1)=R*DV(1)
96 IF (SUMDV.NE.0.) GO TO 60
97 SUMDV=.00000001
98
99 DE=SUMV/SUMDV
100 ADE=ABS(DE)

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8100 PROGRAM LRDC

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101 IF LADE.LT.UGU11 GO TO 80
102 IF LADE.GT.51 DE=5.0E/3E
103 EME=DE
104 I4=I+14
105 IF (I4.LE.40) GO TO J0
106 IF (JDC.EU.1) GO TO 90
107 LU=LE+DE
108 JDC=1
109 GO TO 10
110 E=E+DE-EO
111 SE=SE+E
112 SE2=SE2+E**2
113 CONTINUE
114 ELAV(12)=SE/40.1/3.
115 RMS(12)=SQRT(SE2/40.1/3.
116 SIG=SE2-(SE**2)/40.
117 IF (SIG.LE.0.1) SIG=0.
118 SIGMA(12)=SQRT(SIG/39.1/3.
119 T1(12)=T/3.
120 WRITE (106,240) T1(14),ELAV(12),SIGMA(12),RMS(12),14
121
122
123
124
125 C-110 CONTINUE
126
127
128
129
130
131
132
133
134
135
136
137
138
139
140
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150

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C-1 INPUT ANTENNA SIZE, SURFACE DIELECTRIC CONSTANT, SQUINT ANGLE.
C-2 AND LOWER BEAM REDUCTION FACTOR.
C-3 LOADS ANTENNA BEAM VOLTAGE AT 1/3 DEGREE STEPS UPWARD FROM
C-4 CROSSOVER ON UPPER BEAM DOWNWARD ON LOWER BEAM AND VOLTAGE
C-5 DERIVATIVES FROM PROGRAM CONVA.
C-6 1/3 INCREMENTS TRUE TARGET ANGLE T ABOVE BASE ANGLE 10 IN
C-7 1/3 DEGREE STEPS.
C-8 COMPUTE REFLECTION COEFFICIENT, R, FOR EACH
C-9 ELEVATION ANGLE PER TERM P699 (VERTICAL POLARIZATION).
C-10 SURFACE DIELECTRIC CONSTANT AND COMPUTE M AS FUNCTION OF ELEVATION.
C-11 1/3 ROTATES PHASE OF REFLECTED SIGNAL 6 IN 90 STEPS.
C-12 INITIALIZE ERROR AND INTERACTION COUNTER 14.
C-13 DEFINE UPPER AND LOWER, DIRECT AND REFLECTED ANGLES WITH ERROR.

BIU6 PROGRAM LRDC

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151 C- A1115 DIRECT UPPER BEAM MAY, A121 IS REFLECTED UPPER BEAM MAY, LR151
152 C- A131 IS DIRECT LOWER BEAM MAY, A141 IS REFLECTED LOWER BEAM MAY, LR152
153 C-B COMPUTE SUM OF SIGNALS AND DERIVATIVES, LR153
154 C-Y COMPUTE DIRECT AND REFLECTED VOLTAGES AND DERIVATIVES IF ANGLE LR154
155 C- IS NOT ON AN INPUT DATA POINT, LR155
156 C-10 COMPUTE VOLTAGES AND DERIVATIVES IF ANGLE IS ON INPUT VALUE, LR156
157 C-11 REVERSE SIGN OF DERIVATIVE FOR LOWER BEAM AND MULTIPLY BOTH LR157
158 C- VOLTAGES AND DERIVATIVES BY LOWER BEAM REDUCTION FACTOR, LR158
159 C-12 COMPUTE ANGLE INCREMENT WHICH WOULD REDUCE DIFFERENCE VOLTAGE LR159
160 C- TO ZERO, LR160
161 C-13 OUTPUT INPUT DATA, OFFSET ANGLE RESULTING FROM LOWER BEAM REDUCTION LR161
162 C- FACTOR, ELEVATION ANGLE, MEAN ERROR, SIGMA OF ERROR, RMS ERROR, LR162
163 C- AND MEAN, SIGMA, AND RMS ERRORS PER UNIT BALLOON HEIGHT, LR163
164 C- LR164
165 C- LR165
166 C- LR166
167 C- LR167
168 C- LR168
169 C- LR169
170 C- LR170
171 C-14 ANTENNA DIAMETER, F16.2, /, 190 DIELECTRIC CONSTANT, LR171
172 C- F14.2, /, 21 SIN SQUANT ANGLE, DEGREES, F12.2, /, 11 LOWER BEAM LR172
173 C- REDUCTION, /, M FACTOR, F6.2, /, 25 MELEVATION OFFSET, DEGREES, LR173
174 C- F12.6, /, / LR174
175 C-15 MELEVATION, 0X, 4HMEAN, 11X, 5MSIGMA, 10X, 3HRMS, /, 1016M, ..... LR175
176 C-16 MELEVATION, 0X, 4HMEAN, 11X, 5MSIGMA, 10X, 3HRMS, /, 1016M, ..... LR176
177 C-17 MELEVATION, 0X, 4HMEAN, 11X, 5MSIGMA, 10X, 3HRMS, /, 1016M, ..... LR177

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PAGE 1

8106 INPUT FILES AR

| | |
|---|------|
| 1 | 300. |
| 2 | 400. |
| 3 | 500. |

8106 INPUT FILES ZMHE

| | | |
|----|---------|----------|
| 1 | 200.. | 1.2, 1.2 |
| 2 | 500.. | 1.3, 1.3 |
| 3 | 1000.. | 1.3, 1.3 |
| 4 | 1500.. | 1.5, 1.5 |
| 5 | 2000.. | 1.6, 1.6 |
| 6 | 3000.. | 1.8, 1.8 |
| 7 | 4000.. | 2.2, 2.2 |
| 8 | 5000.. | 2.4, 2.4 |
| 9 | 6000.. | 2.7, 2.7 |
| 10 | 8000.. | 3.1, 3.1 |
| 11 | 10000.. | 4.1, 4.1 |
| 12 | 12000.. | 5.2, 5.2 |
| 13 | 14000.. | 5.9, 5.9 |
| 14 | 16000.. | 7.2, 7.2 |
| 15 | 18000.. | 8.3, 8.3 |

| | | |
|----|-------|-------|
| 1 | 6.28 | 7.40 |
| 2 | 13.02 | 7.43 |
| 3 | 18.21 | 6.46 |
| 4 | 23.66 | 5.07 |
| 5 | 28.62 | 3.90 |
| 6 | 32.82 | 3.29 |
| 7 | 35.77 | 4.48 |
| 8 | 37.14 | 4.95 |
| 9 | 38.11 | 5.24 |
| 10 | 38.83 | 4.75 |
| 11 | 40.43 | 3.21 |
| 12 | 42.90 | 3.19 |
| 13 | 44.32 | 3.35 |
| 14 | 39.40 | 1.33 |
| 15 | 32.86 | -0.76 |
| 16 | 32.86 | -0.76 |
| 17 | 32.86 | -0.76 |

8106-INPUTFILES MRE

| | | | | |
|----|---------|---------|-------|-------|
| 1 | 100. | 100. | 0.00 | 40.90 |
| 2 | 540. | 580. | 20.19 | 46.88 |
| 3 | 1430. | 1520. | 17.21 | 55.24 |
| 4 | 3340. | 3480. | 16.66 | 63.99 |
| 5 | 5720. | 5910. | 14.68 | 69.83 |
| 6 | 8560. | 8790. | 13.11 | 73.99 |
| 7 | 15100. | 15390. | 11.17 | 78.47 |
| 8 | 22490. | 22660. | 10.07 | 79.88 |
| 9 | 29780. | 30210. | 7.39 | 80.82 |
| 10 | 37470. | 37970. | 6.42 | 80.86 |
| 11 | 53110. | 53740. | 6.32 | 81.49 |
| 12 | 69400. | 70070. | 7.89 | 82.42 |
| 13 | 86990. | 87390. | 7.50 | 83.08 |
| 14 | 104250. | 105290. | 7.17 | 83.53 |
| 15 | 119980. | 121170. | 7.05 | 84.12 |
| 16 | 133030. | 134400. | 7.10 | 84.83 |
| 17 | 100. | 100. | 0.00 | 40.90 |
| 18 | 430. | 480. | 24.81 | 46.54 |
| 19 | 1100. | 1210. | 27.45 | 54.92 |
| 20 | 2530. | 2720. | 21.58 | 63.77 |
| 21 | 4310. | 560. | 19.17 | 69.67 |
| 22 | 6440. | 6750. | 17.22 | 73.87 |
| 23 | 11340. | 11730. | 14.76 | 78.39 |
| 24 | 16740. | 17220. | 13.36 | 79.83 |
| 25 | 22350. | 22920. | 14.50 | 80.48 |
| 26 | 28120. | 28770. | 11.91 | 80.83 |
| 27 | 39850. | 40670. | 11.16 | 81.47 |
| 28 | 52000. | 52990. | 10.64 | 82.40 |
| 29 | 64880. | 66040. | 10.18 | 83.06 |
| 30 | 78400. | 79530. | 7.79 | 83.51 |
| 31 | 90000. | 91520. | 7.66 | 84.11 |
| 32 | 99790. | 101530. | 5.76 | 84.82 |
| 33 | 100. | 100. | 0.00 | 40.90 |
| 34 | 370. | 420. | 28.69 | 46.24 |
| 35 | 900. | 1030. | 29.11 | 54.61 |
| 36 | 2040. | 2270. | 26.12 | 63.55 |
| 37 | 3470. | 3780. | 23.39 | 69.51 |
| 38 | 5170. | 5540. | 21.13 | 73.75 |
| 39 | 9090. | 9570. | 16.27 | 78.31 |
| 40 | 13410. | 13990. | 16.55 | 79.78 |
| 41 | 17900. | 18590. | 15.52 | 80.44 |
| 42 | 22510. | 23310. | 14.82 | 80.79 |
| 43 | 31900. | 32900. | 13.93 | 81.45 |
| 44 | 41610. | 42830. | 13.32 | 82.39 |
| 45 | 51920. | 53340. | 14.77 | 83.05 |
| 46 | 62580. | 64190. | 14.32 | 83.50 |
| 47 | 72010. | 73660. | 12.19 | 84.10 |
| 48 | 79850. | 81950. | 14.33 | 84.81 |

8106*INPUTFILES AD712

| | ANTENNA DIAMETER | 7.00 | | | | | | | |
|----|-----------------------------|------------|------------|------------|----|--|--|--|--|
| | OFFLECTRIC CONSTANT | 12.00 | | | | | | | |
| | SQUINT ANGLE, DEGREES | .00 | | | | | | | |
| | LOWER BEAM REDUCTION FACTOR | 1.00 | | | | | | | |
| | ELEVATION OFFSET, DEGREES | --000000 | | | | | | | |
| | ELEVATION | MEAN | SIGMA | RMS | | | | | |
| 1 | .00 | .00415949 | .02629945 | .02629945 | 1 | | | | |
| 2 | .33 | -.23897263 | .48235574 | .53287738 | 2 | | | | |
| 3 | .67 | -.34153870 | .84755244 | .90390003 | 3 | | | | |
| 4 | 1.00 | -.70133946 | .91800281 | 1.14609684 | 4 | | | | |
| 5 | 1.33 | -.78821335 | 1.10235050 | 1.34390384 | 5 | | | | |
| 6 | 1.67 | -.45962097 | 1.30052033 | 1.36393574 | 6 | | | | |
| 7 | 2.00 | -.51226228 | 1.34686168 | 1.42516598 | 7 | | | | |
| 8 | 2.33 | -.53748997 | 1.37203676 | 1.45750409 | 8 | | | | |
| 9 | 2.67 | -.52984440 | 1.34049395 | 1.42574051 | 9 | | | | |
| 10 | 3.00 | -.47979036 | 1.21692938 | 1.29386744 | 10 | | | | |
| 11 | 3.33 | -.43031228 | 1.03248802 | 1.10657540 | 11 | | | | |
| 12 | 3.67 | -.38734644 | .82120866 | .89864416 | 12 | | | | |
| 13 | 4.00 | -.30793107 | .59118012 | .66698048 | 13 | | | | |
| 14 | 4.33 | -.05111556 | .12354417 | .13284555 | 14 | | | | |
| 15 | 4.67 | .03623710 | .11551907 | .11968362 | 15 | | | | |
| 16 | 5.00 | .0362543 | .21398728 | .21444629 | 16 | | | | |
| 17 | 5.33 | .01439036 | .22547750 | .22312548 | 17 | | | | |
| 18 | 5.67 | .00811529 | .19653448 | .19423185 | 18 | | | | |
| 19 | 6.00 | .00516230 | .1568404 | .15497683 | 19 | | | | |
| 20 | 6.33 | .00602480 | .12168825 | .12030847 | 20 | | | | |
| 21 | 6.67 | .00604031 | .10091395 | .09982745 | 21 | | | | |
| 22 | 7.00 | .00573689 | .08962219 | .08848058 | 22 | | | | |
| 23 | 7.33 | .00467975 | .08209899 | .08120122 | 23 | | | | |
| 24 | 7.67 | .00364988 | .07357550 | .07274161 | 24 | | | | |
| 25 | 8.00 | .00242165 | .06342540 | .06267437 | 25 | | | | |
| 26 | 8.33 | .00133899 | .04893878 | .04833777 | 26 | | | | |
| 27 | 8.67 | .00077377 | .03324908 | .03283995 | 27 | | | | |
| 28 | 9.00 | .00043902 | .02054844 | .02029471 | 28 | | | | |
| 29 | 9.33 | .00018636 | .00955375 | .00943541 | 29 | | | | |
| 30 | 9.67 | .00001345 | .00071670 | .00070782 | 30 | | | | |
| 31 | 10.00 | -.00009644 | .00485599 | .00479588 | 31 | | | | |
| 32 | 10.33 | -.00012533 | .00648159 | .00640128 | 32 | | | | |
| 33 | 10.67 | -.00011825 | .00712511 | .00703648 | 33 | | | | |
| 34 | 11.00 | -.00010454 | .00708469 | .00699636 | 34 | | | | |
| 35 | 11.33 | -.00008463 | .00611620 | .00603986 | 35 | | | | |
| 36 | 11.67 | -.00005065 | .00396826 | .00391867 | 36 | | | | |
| 37 | 12.00 | -.00001219 | .00101045 | .00099781 | 37 | | | | |
| 38 | 12.33 | .00001831 | .00196297 | .00193836 | 38 | | | | |
| 39 | 12.67 | .00001534 | .00297976 | .00294232 | 39 | | | | |
| 40 | 13.00 | .00000625 | .00214015 | .00211323 | 40 | | | | |
| 41 | 13.33 | .00000140 | .00072763 | .00071848 | 41 | | | | |
| 42 | 13.67 | -.00000100 | .00060203 | .00059446 | 42 | | | | |

| | | | | | |
|-----|-------|--------------|-----------|-----------|----|
| 51 | 14.00 | --.00000269 | .00112529 | .00111114 | 43 |
| 52 | 14.33 | --.00000247 | .00097050 | .00097804 | 44 |
| 53 | 14.67 | --.00000080 | .00024205 | .00023901 | 45 |
| 54 | 15.00 | .00000228 | .00070769 | .00069879 | 46 |
| 55 | 15.33 | .00000247 | .00116312 | .00114850 | 47 |
| 56 | 15.67 | .00000120 | .00107265 | .00105915 | 48 |
| 57 | 16.00 | .00000020 | .00033090 | .00032674 | 49 |
| 58 | 16.33 | .00000014 | .00085346 | .00084273 | 50 |
| 59 | 16.67 | .00000046 | .00193296 | .00190864 | 51 |
| 60 | 17.00 | .00000036 | .00259138 | .00255878 | 52 |
| 61 | 17.33 | .00000029 | .00284596 | .00281010 | 53 |
| 62 | 17.67 | .00000031 | .00262345 | .00259045 | 54 |
| 63 | 18.00 | .00000107 | .00227409 | .00224548 | 55 |
| 64 | 18.33 | .00000198 | .00207699 | .00205086 | 56 |
| 65 | 18.67 | .00000269 | .00205382 | .00202799 | 57 |
| 66 | 19.00 | .00000321 | .00222278 | .00219483 | 58 |
| 67 | 19.33 | .00000217 | .00230049 | .00227155 | 59 |
| 68 | 19.67 | .00000087 | .00195166 | .00192711 | 60 |
| 69 | 20.00 | .00000054 | .00122363 | .00120823 | 61 |
| 70 | 20.33 | .00000065 | .00057093 | .00056374 | 62 |
| 71 | 20.67 | --.00000019 | .00065008 | .00026174 | 63 |
| 72 | 21.00 | --.00000170 | .00073272 | .00072350 | 64 |
| 73 | 21.33 | --.000000387 | .00121912 | .00120379 | 65 |
| 74 | 21.67 | --.00000856 | .00178419 | .00176177 | 66 |
| 75 | 22.00 | --.00001259 | .00225876 | .00223038 | 67 |
| 76 | 22.33 | --.00001936 | .00276964 | .00273487 | 68 |
| 77 | 22.67 | --.00002646 | .00269806 | .00266172 | 69 |
| 78 | 23.00 | --.00002377 | .00214597 | .00211911 | 70 |
| 79 | 23.33 | --.00000840 | .00072792 | .00071882 | 71 |
| 80 | 23.67 | --.00000423 | .00035205 | .00034765 | 72 |
| 81 | 24.00 | .00000288 | .00218359 | .00215631 | 73 |
| 82 | 24.33 | .00006441 | .00482744 | .00476715 | 74 |
| 83 | 24.67 | .00008902 | .00740953 | .00731687 | 75 |
| 84 | 25.00 | .00012023 | .01017764 | .01005033 | 76 |
| 85 | 25.33 | .00012432 | .01302538 | .01286213 | 77 |
| 86 | 25.67 | .00006841 | .01435259 | .01417221 | 78 |
| 87 | 26.00 | --.00000993 | .01259289 | .01243449 | 79 |
| 88 | 26.33 | --.00000439 | .00766788 | .00757155 | 80 |
| 89 | 26.67 | --.00000060 | .00075664 | .00074470 | 81 |
| 90 | 27.00 | .00003421 | .00691691 | .00682998 | 82 |
| 91 | 27.33 | .00000278 | .01194420 | .01179399 | 83 |
| 92 | 27.67 | --.000004034 | .01634106 | .01613555 | 84 |
| 93 | 28.00 | --.00015648 | .01592487 | .01572532 | 85 |
| 94 | 28.33 | --.00017907 | .01366325 | .01349257 | 86 |
| 95 | 28.67 | --.00016153 | .01067717 | .01054410 | 87 |
| 96 | 29.00 | --.00012599 | .00727778 | .00718734 | 88 |
| 97 | 29.33 | --.00006344 | .00360395 | .00355918 | 89 |
| 98 | 29.67 | --.00002372 | .00145787 | .00143972 | 90 |
| 99 | 30.00 | .00001263 | .00074283 | .00073359 | 91 |
| 100 | 30.33 | .000003461 | .00207750 | .00207137 | 92 |

BIU*INPUTFILES AD712

| | | | | | |
|-----|-------|-----------|-----------|-----------|-----|
| 101 | 30.67 | .00004441 | .00292231 | .00286589 | 93 |
| 102 | 31.00 | .00005574 | .00387972 | .00383132 | 94 |
| 103 | 31.33 | .00006979 | .00480011 | .00474024 | 95 |
| 104 | 31.67 | .00008602 | .00603650 | .00596119 | 96 |
| 105 | 32.00 | .00010434 | .00730328 | .00721217 | 97 |
| 106 | 32.33 | .00011326 | .00872997 | .00862090 | 98 |
| 107 | 32.67 | .00009737 | .00920264 | .00917400 | 99 |
| 108 | 33.00 | .00009700 | .00936865 | .00925151 | 100 |
| 109 | 33.33 | .00009145 | .01027753 | .01014866 | 101 |
| 110 | 33.67 | .00004914 | .00986034 | .00973643 | 102 |
| 111 | 34.00 | .00002032 | .00685393 | .00676775 | 103 |
| 112 | 34.33 | .00003423 | .00533066 | .00526375 | 104 |
| 113 | 34.67 | .00005480 | .00578406 | .00571157 | 105 |
| 114 | 35.00 | .00006089 | .00616378 | .00608655 | 106 |
| 115 | 35.33 | .00006916 | .00655206 | .00647001 | 107 |
| 116 | 35.67 | .00006555 | .00650947 | .00642792 | 108 |
| 117 | 36.00 | .00006538 | .00620584 | .00612813 | 109 |
| 118 | 36.33 | .00006776 | .00621871 | .00614086 | 110 |
| 119 | 36.67 | .00006475 | .00592392 | .00584976 | 111 |
| 120 | 37.00 | .00005432 | .00508897 | .00502525 | 112 |
| 121 | 37.33 | .00004456 | .00399456 | .00394459 | 113 |
| 122 | 37.67 | .00005362 | .00360524 | .00357775 | 114 |
| 123 | 38.00 | .00006506 | .00421708 | .00416454 | 115 |
| 124 | 38.33 | .00007690 | .00488245 | .00482165 | 116 |
| 125 | 38.67 | .00008560 | .00504519 | .00498246 | 117 |
| 126 | 39.00 | .00012027 | .00661655 | .00653443 | 118 |
| 127 | 39.33 | .00015147 | .00820908 | .00810723 | 119 |
| 128 | 39.67 | .00019153 | .01006753 | .00994273 | 120 |
| 129 | 40.00 | .00020659 | .01145603 | .01131381 | 121 |
| 130 | 40.33 | .00022452 | .01257090 | .01241480 | 122 |
| 131 | 40.67 | .00024162 | .01347343 | .01330614 | 123 |
| 132 | 41.00 | .00025226 | .01398376 | .01381016 | 124 |
| 133 | 41.33 | .00028235 | .01535871 | .01516814 | 125 |
| 134 | 41.67 | .00028063 | .01634126 | .01613814 | 126 |
| 135 | 42.00 | .00030056 | .01720350 | .01698976 | 127 |
| 136 | 42.33 | .00030669 | .01818238 | .01795628 | 128 |
| 137 | 42.67 | .00031020 | .01882445 | .01859024 | 129 |
| 138 | 43.00 | .00032360 | .01971981 | .01947445 | 130 |
| 139 | 43.33 | .00027423 | .01956189 | .01931777 | 131 |
| 140 | 43.67 | .00027543 | .01858065 | .01834899 | 132 |
| 141 | 44.00 | .00032233 | .01929472 | .01905473 | 133 |
| 142 | 44.33 | .00036378 | .02131138 | .02104645 | 134 |
| 143 | 44.67 | .00029327 | .02254594 | .02226427 | 135 |
| 144 | 45.00 | .00025162 | .02164249 | .02137172 | 136 |
| 145 | 45.33 | .00022755 | .02030326 | .02004915 | 137 |
| 146 | 45.67 | .00021345 | .01890083 | .01866430 | 138 |
| 147 | 46.00 | .00023862 | .01762760 | .01740750 | 139 |
| 148 | 46.33 | .00025816 | .01812680 | .01790064 | 140 |
| 149 | 46.67 | .00022785 | .01796949 | .01774492 | 141 |
| 150 | 47.00 | .00019941 | .01732446 | .01701688 | 142 |

8106*INPUTFILES AD712

| | | | | | |
|-----|-------|------------|-----------|------------|-----|
| 151 | 47.33 | .00016903 | .01598993 | .01578970 | 143 |
| 152 | 47.67 | .00021062 | .01584760 | .01564967 | 144 |
| 153 | 48.00 | .00024927 | .01732367 | .01710757 | 145 |
| 154 | 48.33 | .00021770 | .01822908 | .01800109 | 146 |
| 155 | 48.67 | .00020811 | .01789059 | .01766676 | 147 |
| 156 | 49.00 | .00018896 | .01719028 | .01697509 | 148 |
| 157 | 49.33 | .00017465 | .01666629 | .01645757 | 149 |
| 158 | 49.67 | .00010657 | .01515725 | .01496698 | 150 |
| 159 | 50.00 | .00006226 | .01233148 | .01217652 | 151 |
| 160 | 50.33 | .00005005 | .01020303 | .01007481 | 152 |
| 161 | 50.67 | .00004662 | .00833559 | .00823087 | 153 |
| 162 | 51.00 | .00005051 | .00757831 | .00748315 | 154 |
| 163 | 51.33 | .00007447 | .00812660 | .00802472 | 155 |
| 164 | 51.67 | .00009336 | .00942745 | .00930933 | 156 |
| 165 | 52.00 | .00010440 | .01090401 | .01056992 | 157 |
| 166 | 52.33 | .00012114 | .01203109 | .01188037 | 158 |
| 167 | 52.67 | .00013763 | .01340877 | .01324081 | 159 |
| 168 | 53.00 | .00014479 | .01463668 | .01445329 | 160 |
| 169 | 53.33 | .00014742 | .01588691 | .01568776 | 161 |
| 170 | 53.67 | .00013525 | .01646292 | .01625639 | 162 |
| 171 | 54.00 | .00013472 | .01684139 | .01663008 | 163 |
| 172 | 54.33 | .00012768 | .01730312 | .01708594 | 164 |
| 173 | 54.67 | .00004984 | .01614187 | .01593890 | 165 |
| 174 | 55.00 | -.00000241 | .01241900 | .01226278 | 166 |
| 175 | 55.33 | -.00002278 | .00645317 | .00637204 | 167 |
| 176 | 55.67 | .00000173 | .00144237 | .00142422 | 168 |
| 177 | 56.00 | .00000614 | .00097964 | .00096734 | 169 |
| 178 | 56.33 | .00001658 | .00212867 | .00210196 | 170 |
| 179 | 56.67 | .00003224 | .00380826 | .00376049 | 171 |
| 180 | 57.00 | .00004759 | .00538979 | .00532220 | 172 |
| 181 | 57.33 | .00004530 | .00670296 | .006661860 | 173 |
| 182 | 57.67 | .00001943 | .00581298 | .00573989 | 174 |
| 183 | 58.00 | .00000978 | .00368107 | .00363478 | 175 |
| 184 | 58.33 | .00001134 | .00235982 | .00233016 | 176 |
| 185 | 58.67 | .00001351 | .00251708 | .00248546 | 177 |
| 186 | 59.00 | .00000904 | .00233671 | .00230733 | 178 |
| 187 | 59.33 | .00000505 | .00130645 | .00129003 | 179 |
| 188 | 59.67 | .00000488 | .00092122 | .00092122 | 180 |
| 189 | 60.00 | .00000966 | .00146624 | .00144783 | 181 |
| 190 | 60.33 | .00001656 | .00247409 | .00244303 | 182 |
| 191 | 60.67 | .00002682 | .00356734 | .00352257 | 183 |
| 192 | 61.00 | .00005043 | .00540110 | .00533340 | 184 |
| 193 | 61.33 | .00005785 | .00730119 | .00720958 | 185 |
| 194 | 61.67 | .00005161 | .00806897 | .00796764 | 186 |
| 195 | 62.00 | .00004401 | .00811862 | .00801662 | 187 |
| 196 | 62.33 | .00002044 | .00696553 | .00687794 | 188 |
| 197 | 62.67 | .00000827 | .00470915 | .00464992 | 189 |
| 198 | 63.00 | .00000508 | .00260430 | .00257155 | 190 |
| 199 | 63.33 | .00000244 | .00085496 | .00084421 | 191 |
| 200 | 63.67 | .00000004 | .00007194 | .00007103 | 192 |

8106*INPUTFILES AD712

| | | | | | |
|-----|-------|-------------|-----------|-----------|-----|
| 201 | 64.00 | --.0000157 | .00041663 | .00041139 | 193 |
| 202 | 64.33 | --.0000259 | .00062920 | .00062129 | 194 |
| 203 | 64.67 | --.0000325 | .00064278 | .00063471 | 195 |
| 204 | 65.00 | .0000115 | .00014566 | .00014384 | 196 |
| 205 | 65.33 | .00001061 | .00148977 | .00147107 | 197 |
| 206 | 65.67 | .0002107 | .00289731 | .00286094 | 198 |
| 207 | 66.00 | .0002620 | .00391755 | .00386836 | 199 |
| 208 | 66.33 | .0002603 | .00449259 | .00443615 | 200 |
| 209 | 66.67 | .0001570 | .00400808 | .00395769 | 201 |
| 210 | 67.00 | .0001113 | .00278905 | .00275399 | 202 |
| 211 | 67.33 | .0001160 | .00250858 | .00247706 | 203 |
| 212 | 67.67 | .0001427 | .00258295 | .00255050 | 204 |
| 213 | 68.00 | .0001500 | .00242173 | .00239132 | 205 |
| 214 | 68.33 | .0001989 | .00285132 | .00281553 | 206 |
| 215 | 68.67 | .0002132 | .00323901 | .00319834 | 207 |
| 216 | 69.00 | .0001909 | .00328580 | .00324452 | 208 |
| 217 | 69.33 | .0001461 | .00286588 | .00282987 | 209 |
| 218 | 69.67 | .0000906 | .00220397 | .00217627 | 210 |
| 219 | 70.00 | .0000425 | .00112767 | .00111349 | 211 |
| 220 | 70.33 | .0000173 | .00030979 | .00030590 | 212 |
| 221 | 70.67 | .0000032 | .00008271 | .00008167 | 213 |
| 222 | 71.00 | --.0000010 | .00000469 | .00000463 | 214 |
| 223 | 71.33 | .00000040 | .00007267 | .00007176 | 215 |
| 224 | 71.67 | .00000099 | .00014578 | .00014395 | 216 |
| 225 | 72.00 | .00000028 | .00000357 | .00000353 | 217 |
| 226 | 72.33 | .00000029 | .00000427 | .00000422 | 218 |
| 227 | 72.67 | .00000200 | .00030361 | .00029979 | 219 |
| 228 | 73.00 | .00000461 | .00078094 | .00077113 | 220 |
| 229 | 73.33 | .00001152 | .00164026 | .00161967 | 221 |
| 230 | 73.67 | .00002050 | .00273709 | .00270274 | 222 |
| 231 | 74.00 | .00004207 | .00444192 | .00438625 | 223 |
| 232 | 74.33 | .00005898 | .00722511 | .00664078 | 224 |
| 233 | 74.67 | .00005513 | .00775636 | .00765899 | 225 |
| 234 | 75.00 | .00003645 | .00754204 | .00744725 | 226 |
| 235 | 75.33 | .00002250 | .00614253 | .00606530 | 227 |
| 236 | 75.67 | .00001553 | .00456884 | .00451139 | 228 |
| 237 | 76.00 | .00001071 | .00319958 | .00315935 | 229 |
| 238 | 76.33 | .00000544 | .00182431 | .00180137 | 230 |
| 239 | 76.67 | .00000333 | .00080845 | .00079829 | 231 |
| 240 | 77.00 | .00000213 | .00043487 | .00042940 | 232 |
| 241 | 77.33 | .00000153 | .00028900 | .00028537 | 233 |
| 242 | 77.67 | .00000067 | .00014504 | .00014322 | 234 |
| 243 | 78.00 | .00000006 | .00007344 | .00007251 | 235 |
| 244 | 78.33 | --.0000097 | .00029072 | .00028706 | 236 |
| 245 | 78.67 | --.00000173 | .00036271 | .00035815 | 237 |
| 246 | 79.00 | --.00000117 | .00021739 | .00021465 | 238 |
| 247 | 79.33 | .00000126 | .00000074 | .00000146 | 239 |
| 248 | 79.67 | .00000088 | .00014570 | .00014387 | 240 |
| 249 | 80.00 | .00000246 | .00043741 | .00043191 | 241 |
| 250 | 80.33 | .00000408 | .00073563 | .00072639 | 242 |

8106*INPUTFILES AD712

| | | | | | |
|-----|-------|-------------|-----------|-----------|-----|
| 251 | 80.67 | .00000673 | .00119847 | .00118341 | 243 |
| 252 | 81.00 | .00000854 | .00152139 | .00150820 | 244 |
| 253 | 81.33 | .00000775 | .00159382 | .00157379 | 245 |
| 254 | 81.67 | .00000674 | .00112956 | .00111159 | 246 |
| 255 | 82.00 | .00000431 | .00110788 | .00109395 | 247 |
| 256 | 82.33 | .00000175 | .00036176 | .00035721 | 248 |
| 257 | 82.67 | .00000180 | .00028895 | .00028532 | 249 |
| 258 | 83.00 | .00000149 | .00028895 | .00028532 | 250 |
| 259 | 83.33 | .00000153 | .00028910 | .00028547 | 251 |
| 260 | 83.67 | .00000131 | .00021810 | .00021536 | 252 |
| 261 | 84.00 | .00000193 | .00036053 | .00035600 | 253 |
| 262 | 84.33 | .00000160 | .00028959 | .00028596 | 254 |
| 263 | 84.67 | .00000176 | .00028956 | .00028592 | 255 |
| 264 | 85.00 | .00000148 | .00028977 | .00028613 | 256 |
| 265 | 85.33 | .00000109 | .00021736 | .00021463 | 257 |
| 266 | 85.67 | .00000048 | .00007304 | .00007213 | 258 |
| 267 | 86.00 | -.00000080 | .00021813 | .00021539 | 259 |
| 268 | 86.33 | -.00000165 | .00029397 | .00029028 | 260 |
| 269 | 86.67 | .00000122 | .00014760 | .00014575 | 261 |
| 270 | 87.00 | .00000341 | .00058779 | .00058041 | 262 |
| 271 | 87.33 | .00000936 | .00149502 | .00147624 | 263 |
| 272 | 87.67 | .00000811 | .00188133 | .00185768 | 264 |
| 273 | 88.00 | .00000432 | .00119052 | .00117555 | 265 |
| 274 | 88.33 | -.00000055 | .00030265 | .00029884 | 266 |
| 275 | 88.67 | -.00000561 | .00135822 | .00134114 | 267 |
| 276 | 89.00 | -.00000655 | .00144495 | .00142678 | 268 |
| 277 | 89.33 | -.00000689 | .00202893 | .00200342 | 269 |
| 278 | 89.67 | -.000002063 | .00246170 | .00243082 | 270 |
| 279 | 90.00 | .00000128 | .00000074 | .00000147 | 271 |

***** PROGRAM RAWIN *****

EXAMPLE RAWIN RUN USING 15 ZONES AND 3 ASCENT RATES
USE INPUT FILES AR, IMHE, WF, UV, HDE, AD71?

ALBERTA
(11/1988)

| LINE | NO | ZONE | | | | | | | | | | | | | | | | | | | | | | | | |
|------|----------|----------|----------|----------|----------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | | | | | | | | | | |
| 1 | -500-002 | .500-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | | | | | | |
| 2 | -100-002 | .000 | .267-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 3 | -650-003 | .000 | .000 | .144-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | | | | |
| 4 | -300-003 | .000 | .000 | .000 | .112-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | | | |
| 5 | -200-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | | |
| 6 | -150-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | |
| 7 | -100-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 8 | -100-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 9 | -100-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 10 | -500-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 11 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 12 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 13 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 14 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 15 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

ARRAY = U
(1/5/5)

| LINE | ZONE | | | | | | | | | | | | | | |
|------|-----------------------|------------------------|-----------------------|-----------------------|-----------------------|-------------------|-------------------|-------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 1 | -.414-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 2 | .264-001 .000 | -.347-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 3 | .452-002 .000 | .180-001 .000 | -.262-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 4 | .272-002 .000 | .426-002 .000 | .170-001 .000 | -.265-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 5 | .182-002 .000 | .199-002 .000 | .400-002 .000 | .209-001 .000 | -.303-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 6 | .928-003 .000 | .744-003 .000 | .135-002 .000 | .241-002 .000 | .138-001 .000 | -.207-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 7 | .474-003 .000 | .125-002 .000 | .743-003 .000 | .127-002 .000 | .198-002 .000 | .124-001 .000 | -.190-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 8 | .400-004 .000 | .132-002 .000 | .654-003 .000 | .595-003 .000 | .116-002 .000 | .220-002 .000 | .992-002 .000 | -.167-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 9 | .400-004 .000 | .953-003 .000 | .545-003 .000 | .496-003 .000 | .108-002 .000 | .712-003 .000 | .278-002 .000 | -.137-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 10 | .454-003 .000 | -.140-003 .000 | .116-002 .000 | -.176-003 .000 | .580-003 .000 | .564-003 .000 | .481-003 .000 | .629-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 11 | -.768-002 .000 | .364-003 .000 | .153-002 .000 | -.176-003 .000 | .908-003 .000 | .236-003 .000 | .481-003 .000 | .873-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 12 | .434-003 .320-002 | -.698-004 -.643-002 | .582-003 .000 | .134-002 .000 | .750-005 .000 | .206-003 .000 | .959-004 .000 | .449-003 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 13 | .434-003 -.416-004 | -.698-004 .253-002 | .109-003 -.532-002 | .174-002 .000 | .580-003 .000 | .206-003 .000 | .959-004 .000 | .679-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 14 | .434-003 .161-003 | -.698-004 -.573-003 | .109-003 .183-002 | .672-003 -.355-002 | .115-002 .000 | .206-003 .000 | .959-004 .000 | .679-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 15 | .434-003 -.663-004 | -.698-004 -.144-003 | .109-003 -.640-003 | .672-003 .724-003 | .115-002 -.230-002 | .206-003 .000 | .959-004 .000 | .679-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |

APRAY #V
(17SER)

| LINE | ZONE | | | | | | | | | | | | | | |
|------|----------|----------|----------|----------|----------|----------|----------|----------|------|------|------|------|------|------|------|
| | 1 | 2 | 7 | 4 | 6 | 7 | 8 | 9 | 10 | 5 | 15 | 14 | 13 | 12 | 11 |
| 1 | .370-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 2 | .124-001 | .100-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 3 | .138-002 | .450-002 | .570-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 4 | .752-003 | .397-003 | .232-002 | .568-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 5 | .501-003 | .433-004 | .500-004 | .211-002 | .413-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 6 | .128-003 | .205-003 | .121-003 | .234-004 | .114-002 | .207-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 7 | .300-005 | .161-003 | .105-003 | .658-004 | .340-004 | .172-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 8 | .245-003 | .200-003 | .167-003 | .140-003 | .740-005 | .391-003 | .223-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 9 | .245-003 | .151-003 | .119-003 | .117-003 | .480-005 | .188-003 | .696-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 10 | .125-003 | .237-003 | .147-003 | .172-003 | .370-005 | .128-003 | .241-004 | .835-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 11 | .000 | .129-003 | .276-003 | .172-003 | .292-004 | .952-004 | .261-004 | .340-005 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 12 | .248-003 | .118-003 | .776-004 | .109-003 | .817-004 | .633-004 | .727-004 | .155-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 13 | .248-003 | .118-003 | .278-004 | .133-003 | .370-005 | .833-004 | .203-004 | .106-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 14 | .173-004 | .195-003 | .402-003 | .000 | .000 | .833-004 | .203-004 | .580-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 15 | .248-003 | .118-003 | .278-004 | .546-004 | .743-004 | .833-004 | .203-004 | .100- | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| | .171-004 | .795-005 | .114-003 | .106-003 | .532-004 | .833-004 | .203-004 | .818-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

PARTIAL DERIVATIVES
ASCENT RATE = 100.0 M/MIN

| ZONE | DXD7 | DYD7 | DXD5 (M/RAD) | DYD5 (M/RAD) | DXD4 (M/RAD) | DYD4 (M/RAD) | DXD3 (M/RAD) | DYD3 (M/RAD) |
|------|-------------|-------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| 1 | .199436+001 | .165823+001 | -.122547+004 | -.114757+004 | .371806+003 | -.397663+003 | | |
| 2 | .235595+001 | .163499+001 | -.179087+004 | -.243080+004 | .817920+003 | -.117859+004 | | |
| 3 | .299701+001 | .146235+001 | -.130904+005 | -.532065+004 | .146385+004 | -.307000+004 | | |
| 4 | .336920+001 | .131105+001 | -.218049+005 | -.801041+004 | .197043+004 | -.536414+004 | | |
| 5 | .410106+001 | .117673+001 | -.170355+005 | -.106278+005 | .236101+004 | -.822862+004 | | |
| 6 | .489865+001 | .999314+000 | -.176907+005 | -.156878+005 | .301724+004 | -.147905+005 | | |
| 7 | .562955+001 | .869105+000 | -.125001+006 | -.223112+005 | .391669+004 | -.219478+005 | | |
| 8 | .579642+001 | .936734+000 | -.177691+006 | -.287144+005 | .675272+004 | -.204092+005 | | |
| 9 | .638879+001 | .102789+001 | -.259433+006 | -.417402+005 | .630025+004 | -.391587+005 | | |
| 10 | .638215+001 | .954958+000 | -.147153+006 | -.519443+005 | .786115+004 | -.525374+005 | | |
| 11 | .661169+001 | .879838+000 | -.668620+006 | -.623808+005 | .914476+004 | -.687197+005 | | |
| 12 | .681028+001 | .826547+000 | -.601671+006 | -.730233+005 | .104241+005 | -.858884+005 | | |
| 13 | .695962+001 | .789258+000 | -.740365+006 | -.839613+005 | .117493+005 | -.107605+006 | | |
| 14 | .694708+001 | .715440+000 | -.850128+006 | -.875523+005 | .122865+005 | -.110101+006 | | |
| 15 | .661110+001 | .616263+000 | -.924894+006 | -.836837+005 | .119825+005 | -.117074+006 | | |

PARTIAL DERIVATIVES
ASCENT RATE = 400.0 M/MIN

| ZONE | DYD7 | DYD7 (M/RAD) | DYDF (M/RAD) | DYDF (M/RAD) | DYDA (M/RAD) | DYDA (M/RAD) |
|------|-------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| 1 | .156994+001 | .148765+001 | -.224598+003 | -.781421+003 | .297653+003 | -.314100+003 |
| 2 | .179890+001 | .124333+001 | -.238720+004 | -.167651+004 | .631355+003 | -.899706+003 |
| 3 | .226496+001 | .111597+001 | -.662011+004 | -.724181+004 | .111669+004 | -.200674+004 |
| 4 | .269077+001 | .096946+000 | -.130037+005 | -.481794+004 | .149723+004 | -.404103+004 |
| 5 | .308746+001 | .892902+000 | -.719090+005 | -.630721+004 | .179926+004 | -.418696+004 |
| 6 | .368949+001 | .758015+000 | -.447979+005 | -.920383+004 | .228279+004 | -.111110+005 |
| 7 | .409397+001 | .734408+000 | -.724873+005 | -.130034+005 | .295566+004 | -.164764+005 |
| 8 | .437243+001 | .733262+000 | -.102729+006 | -.172278+005 | .369800+004 | -.220511+005 |
| 9 | .457611+001 | .739709+000 | -.134688+006 | -.217424+005 | .448236+004 | -.277671+005 |
| 10 | .484667+001 | .726934+000 | -.201255+006 | -.301854+005 | .591363+004 | -.394278+005 |
| 11 | .504073+001 | .672577+000 | -.272304+006 | -.363331+005 | .687947+004 | -.515502+005 |
| 12 | .521212+001 | .634428+000 | -.350290+006 | -.426379+005 | .783751+004 | -.643887+005 |
| 13 | .535280+001 | .609928+000 | -.432629+006 | -.492381+005 | .883669+004 | -.775792+005 |
| 14 | .536947+001 | .553934+000 | -.499903+006 | -.515718+005 | .923876+004 | -.895564+005 |
| 15 | .527731+001 | .478415+000 | -.565353+006 | -.494391+005 | .901124+004 | -.994512+005 |

PARTIAL DERIVATIVES
 ASCENT RATE = 500.0 W/MIN

| ZONE | DXD7 | DYDZ | DXCF (M/RAD) | LYDF (M/RAD) | DXDA (M/RAD) | DYDA (M/RAD) |
|------|-------------|-------------|-----------------|-----------------|-----------------|-----------------|
| 1 | .131953+001 | .126362+001 | -.62478E+003 | -.600228+003 | .252771+003 | -.263556+003 |
| 2 | .146348+001 | .103565+001 | -.172161+004 | -.122304+004 | .519916+003 | -.731864+003 |
| 3 | .122421+001 | .907525+000 | -.661410+004 | -.229548+004 | .907950+003 | -.182505+004 |
| 4 | .216196+001 | .807695+000 | -.850669+004 | -.332457+004 | .121287+004 | -.324540+004 |
| 5 | .247740+001 | .722095+000 | -.167255+005 | -.629210+004 | .144621+004 | -.696171+004 |
| 6 | .295931+001 | .612304+000 | -.298427+005 | -.617470+004 | .184174+004 | -.850127+004 |
| 7 | .328436+001 | .592134+000 | -.479747+005 | -.864931+004 | .237842+004 | -.131923+005 |
| 8 | .350993+001 | .591140+000 | -.677812+005 | -.114157+005 | .297293+004 | -.176520+005 |
| 9 | .367473+001 | .555834+000 | -.884591+005 | -.143753+005 | .360213+004 | -.222156+005 |
| 10 | .389833+001 | .586088+000 | -.132305+006 | -.198911+005 | .474144+004 | -.315374+005 |
| 11 | .406149+001 | .542635+000 | -.178978+006 | -.239126+005 | .550877+004 | -.412314+005 |
| 12 | .421205+001 | .513444+000 | -.230763+006 | -.281297+005 | .628180+004 | -.515379+005 |
| 13 | .433471+001 | .493878+000 | -.285346+006 | -.325111+005 | .708163+004 | -.621547+005 |
| 14 | .435405+001 | .469947+000 | -.329758+006 | -.360772+005 | .740093+004 | -.716173+005 |
| 15 | .428521+001 | .389231+000 | -.360454+006 | -.327405+005 | .722136+004 | -.795031+005 |

PROBLEM 1

WIND ERROR INPUT
ASSUMED ONE SIGMA ERRORS

EXAMPLE RAWIN PROBLEM

| | | | |
|----------------------------------|------|----------------------------------|-----|
| ELEVATION BIAS ERROR (DEGREES) = | .03 | ELEVATION RANDOM ERR (DEGREES) = | .05 |
| AZIMUTH BIAS ERROR (DEGREES) = | .03 | AZIMUTH RANDOM ERROR (DEGREES) = | .05 |
| DISPL. LAUNCH ERROR (METERS) = | 5.00 | AZIMUTH LAUNCH ERROR (METERS) = | .00 |
| FOREGROUND ELEVATION (DEGREES) = | 5.00 | | |

PROBLEM 1 INDIVIDUAL SUMS
ASCENT RATE = 300.0 M/Min

UNITS APE (M/SEC)**2

| LINE | PIAS RANDOM | PEYL | REYL | PEYZ**2 PEYZ | REYZ**2 REYZ | PEXZ**2 PEXZ | REXZ**2 REXZ | PEYZ**2 PEYZ | REYZ**2 REYZ | PEXZ**2 PEXZ | REXZ**2 REXZ | PEYZ**2 PEYZ | REYZ**2 REYZ | PEXZ**2 PEXZ | REXZ**2 REXZ |
|------|----------------|---------|---------|-------------------|--------------------|------------------------|-------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 1 | PIAS RANDOM | .00669A | .008927 | .00097 .00097 | .00257 .00715 | .00000 .00000 | .00024 .00066 | .00129 .00129 | .00226 .00627 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 2 | PIAS RANDOM | .00026P | .000357 | .00058 .000160 | .00446 .002025 | .00000 .00000 | .00017 .000095 | .00001 .000020 | .00178 .001007 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 3 | PIAS RANDOM | .000054 | .000072 | .00068 .000168 | .001057 .004673 | .00000 .00000 | .00013 .000093 | .00002 .000009 | .00195 .001204 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 4 | PIAS RANDOM | .000024 | .000032 | .00042 .00023 | .00052 .012176 | .00000 .00000 | .00010 .000108 | .00001 .000014 | .00196 .001729 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 5 | PIAS RANDOM | .000011 | .000014 | .00044 .000392 | .003907 .033308 | .00050 .040364 | .00007 .000152 | .00002 .000023 | .00191 .002954 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 6 | PIAS RANDOM | .000004 | .000008 | .00030 .000185 | .007232 .048693 | .00045 .350453 | .00005 .000095 | .00001 .000008 | .00182 .002191 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 7 | PIAS RANDOM | .000003 | .000004 | .00012 .000169 | .010320 .095871 | .029611 1.640056 | .00004 .000101 | .00000 .000001 | .00243 .003177 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 8 | PIAS RANDOM | .000003 | .000004 | .00012 .000124 | .012502 .142117 | .119502 1.105868 | .00005 .000107 | .00000 .000000 | .00249 .003832 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 9 | PIAS RANDOM | .000003 | .000004 | .00020 .00059 | .020449 .182937 | 11.229731 63.596860 | .00009 .000110 | .00000 .000000 | .00490 .004749 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 10 | PIAS RANDOM | .000001 | .000001 | .00001 .000054 | .013980 .217424 | 3.421087 91.812114 | .00006 .000115 | .00000 .000000 | .00253 .005023 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 11 | PIAS RANDOM | .000000 | .000000 | .00001 .000044 | .019191 .169698 | 6.689401 103.587361 | .00005 .000067 | .00000 .000002 | .00256 .003096 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 12 | PIAS RANDOM | .000000 | .000000 | .00000 .000063 | .021035 .175727 | 7.810244 127.099808 | .00004 .000055 | .00000 .000001 | .00249 .002853 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 13 | PIAS RANDOM | .000000 | .000000 | .00000 .000059 | .022504 .173336 | 7.021540 126.574532 | .00004 .000044 | .00000 .000000 | .00246 .002246 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 14 | PIAS RANDOM | .000000 | .000000 | .00000 .000011 | .021250 .128759 | 6.535269 94.825549 | .00003 .000028 | .00000 .000004 | .00196 .001423 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |
| 15 | PIAS RANDOM | .000000 | .000000 | .00000 .000010 | .019289 .093662 | 6.023265 48.606710 | .00003 .000017 | .00000 .000008 | .00150 .000808 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 | .00000 .00000 |

PROBLEM 1

INDIVIDUAL SUMS
ASCENT RATE = 400.0 M/MIN

UNITS ARE (W/SEC)***

| LINE | PIAS RANDOM | REYL | REYL | PEVZ**2 PEVZ | REFLYE**2 REFLYE | PERXF**2 PERXF | PEAA**2 PEAA | REYZ**2 REYZ | BFLYE**2 BFLYE | BERYE**2 BERYE | UEYA**2 UEYA |
|------|----------------|---------|---------|--------------------|---------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| 1 | PIAS RANDOM | .01190* | .015870 | .000172 .000172 | .000207 .000575 | .000000 .000001 | .000027 .000075 | .000228 .000228 | .000196 .000517 | .000000 .000001 | .000000 .000003 |
| 2 | PIAS RANDOM | .000476 | .000635 | .000052 .000129 | .000304 .001476 | .000000 .000003 | .000017 .000104 | .000002 .000034 | .000122 .000734 | .000000 .000001 | .000043 .000204 |
| 3 | PIAS RANDOM | .000094 | .000129 | .000065 .000160 | .000577 .003202 | .000000 .000004 | .000013 .000096 | .000002 .000012 | .000125 .000809 | .000000 .000001 | .000075 .000378 |
| 4 | PIAS RANDOM | .000043 | .000057 | .000041 .000217 | .001273 .007716 | .000000 .000004 | .000010 .000111 | .000002 .000016 | .000122 .001117 | .000000 .000001 | .000112 .000756 |
| 5 | PIAS RANDOM | .000019 | .000025 | .000043 .000386 | .002300 .020596 | .000000 .000021 | .000007 .000155 | .000002 .000025 | .000115 .001859 | .000000 .000002 | .000159 .001698 |
| 6 | PIAS RANDOM | .000011 | .000014 | .000031 .000182 | .004310 .029429 | .000000 .000041 | .000005 .000087 | .000001 .000009 | .000198 .001346 | .000000 .000002 | .000225 .001558 |
| 7 | PIAS RANDOM | .000005 | .000006 | .000013 .000165 | .004116 .057391 | .000000 .000034 | .000006 .000102 | .000000 .000001 | .000144 .001922 | .000001 .001462 | .000249 .000908 |
| 8 | PIAS RANDOM | .000005 | .000006 | .000013 .000120 | .007377 .084530 | .000000 .000083 | .000004 .000114 | .000000 .000000 | .000169 .002429 | .000011 .005232 | .000295 .000345 |
| 9 | PIAS RANDOM | .000005 | .000006 | .000009 .000077 | .009263 .089604 | .000000 .000051 | .000007 .000102 | .000000 .000000 | .000187 .002340 | .000015 .007772 | .000312 .001849 |
| 10 | PIAS RANDOM | .000001 | .000002 | .000003 .000055 | .010305 .124719 | .000000 .000038 | .000006 .000113 | .000000 .000000 | .000194 .002882 | .000007 .000161 | .000352 .004874 |
| 11 | PIAS RANDOM | .000000 | .000000 | .000001 .000039 | .011658 .101797 | .000000 .001529 | .000005 .000048 | .000000 .000002 | .000154 .001867 | .000025 .002476 | .000393 .001679 |
| 12 | PIAS RANDOM | .000000 | .000000 | .000000 .000054 | .012758 .105938 | .000000 .001187 | .000004 .000055 | .000000 .000001 | .000151 .001607 | .000047 .000016 | .000422 .001603 |
| 13 | PIAS RANDOM | .000000 | .000000 | .000000 .000040 | .017784 .103994 | .000000 .000981 | .000004 .000045 | .000000 .000001 | .000152 .001371 | .000042 .001449 | .000420 .001371 |
| 14 | PIAS RANDOM | .000000 | .000000 | .000000 .000008 | .013024 .079624 | .000000 .015077 | .000003 .000028 | .000000 .000004 | .000119 .000876 | .000149 .005385 | .000409 .001559 |
| 15 | PIAS RANDOM | .000000 | .000000 | .000000 .000012 | .011752 .057816 | .000000 .016057 | .000003 .000017 | .000000 .000002 | .000091 .000500 | .000131 .003482 | .000358 .001913 |

PFCOLEM 1 VARIANCE IN COMPONENTS

| LINE | ASCENT RATE (M/MIN) = 300.0 | | 400.0 | | 500.0 | |
|------|-----------------------------|---------------------------|--------------------------|---------------------------|--------------------------|---------------------------|
| | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 |
| 1 | .00795 | .01014 | .01114 | .01714 | .01996 | .02628 |
| 2 | .00707 | .00180 | .00252 | .00178 | .00244 | .00202 |
| 3 | .00436 | .00194 | .00431 | .00153 | .00342 | .00140 |
| 4 | .01464 | .00283 | .00942 | .00219 | .00703 | .00191 |
| 5 | .07813 | .00836 | .02353 | .00189 | .01495 | .00337 |
| 6 | .40713 | .01929 | .03409 | .00355 | .02373 | .00315 |
| 7 | 1.79215 | .06146 | .10926 | .00684 | .04408 | .00476 |
| 8 | 1.38024 | .04273 | .27877 | .01214 | .06379 | .00609 |
| 9 | 75.03017 | 1.04743 | .39495 | .01450 | .06673 | .00592 |
| 10 | 95.46568 | 2.19090 | 1.02033 | .02847 | .10651 | .00766 |
| 11 | 110.46577 | 1.98363 | 1.63535 | .03359 | .13830 | .00654 |
| 12 | 135.10693 | 2.02191 | 2.14322 | .03634 | .21456 | .00722 |
| 13 | 137.79002 | 1.74783 | 1.23379 | .02021 | .26572 | .00727 |
| 14 | 101.51287 | 1.11050 | .58637 | .00950 | .21891 | .00536 |
| 15 | 74.79296 | .64643 | .53948 | .00691 | .15501 | .00364 |

PROBLEM 1 COMPONENT VELOCITY VARIANCE

| LINE | 300.0 | | | 400.0 | | | 500.0 | | |
|------|-----------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------------------|--|
| | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | |
| 1 | .03414 | .18476 | .05717 | .23902 | .08723 | .29535 | | | |
| 2 | .00920 | .09590 | .00811 | .09004 | .00842 | .09174 | | | |
| 3 | .01565 | .12509 | .01107 | .10502 | .00910 | .09538 | | | |
| 4 | .03298 | .18159 | .02188 | .14792 | .01685 | .12981 | | | |
| 5 | .16719 | .40897 | .05172 | .22742 | .03833 | .19577 | | | |
| 6 | .80455 | .89697 | .07105 | .26655 | .05070 | .22517 | | | |
| 7 | 3.50482 | 1.87712 | .21906 | .46804 | .09215 | .30357 | | | |
| 8 | 2.68477 | 1.63853 | .44890 | .74088 | .13183 | .36309 | | | |
| 9 | 145.23654 | 12.05141 | .77253 | .87894 | .13707 | .37023 | | | |
| 10 | 184.25233 | 13.57396 | 1.97882 | 1.40671 | .21541 | .46412 | | | |
| 11 | 212.16250 | 14.56580 | 3.14885 | 1.77450 | .27328 | .52276 | | | |
| 12 | 258.72813 | 16.06497 | 4.11225 | 2.02787 | .41845 | .64668 | | | |
| 13 | 255.72434 | 15.99138 | 2.36597 | 1.53817 | .51507 | .71768 | | | |
| 14 | 197.62336 | 13.91466 | 1.12425 | 1.06031 | .42314 | .65049 | | | |
| 15 | 142.33432 | 11.93039 | 1.03090 | 1.01537 | .29033 | .54711 | | | |

AD-A126 360

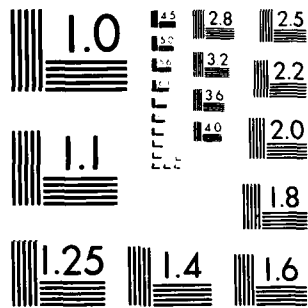
MODELS FOR BALLISTIC WIND MEASUREMENT ERROR ANALYSIS
VOLUME II USERS' MAN... (U) NEW MEXICO STATE UNIV LAS
CRUCES PHYSICAL SCIENCE LAB A W DUDENHOEFFER JAN 83
ERADCOM/ASL-CR-83-0008-1 DAAD07-79-C-0008 F/G 9/2

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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

***** PROGRAM RADAR *****

EXAMPLE RADAR RUN USING 15 ZONES AND 3 ASCENT RATES
USE INPUT FILES AR, ZMHE, WF, UV, MRE, AD712

APRAY M
(1/METFR)

| LINE | WD | ZONE | | | | | | | | | | | | | | | | | | |
|------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| | | 11 | 12 | 13 | 14 | 15 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | | | |
| 1 | .500-002 .000 | | | | | | | | | | | | | | | | | | | |
| 2 | -.167-002 .000 | -.167-002 .000 | .267-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 3 | -.450-003 .000 | -.407-003 .000 | -.407-003 .000 | .144-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 4 | -.100-003 .000 | -.120-003 .000 | -.120-003 .000 | -.600-003 .000 | .112-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 5 | -.200-003 .000 | -.667-004 .000 | -.333-004 .000 | -.100-003 .000 | -.660-003 .000 | .174-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 6 | -.150-003 .000 | -.167-004 .000 | .667-005 .000 | -.200-004 .000 | -.600-004 .000 | -.390-003 .000 | .630-003 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 7 | -.100-003 .000 | -.400-004 .000 | -.400-004 .000 | -.200-004 .000 | -.200-004 .000 | -.400-004 .000 | -.330-003 .000 | .530-003 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 8 | -.100-003 .000 | .333-004 .000 | -.533-004 .000 | .000 .000 | .000 .000 | .000 .000 | -.500-004 .000 | -.260-003 .000 | .450-003 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 9 | -.100-003 .000 | .333-004 .000 | -.333-004 .000 | .000 .000 | .000 .000 | .000 .000 | -.100-004 .000 | -.700-004 .000 | -.160-003 .000 | .360-003 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 10 | -.500-004 .000 | -.167-004 .000 | .267-004 .000 | -.400-004 .000 | .200-004 .000 | -.100-004 .000 | -.100-004 .000 | -.100-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 11 | .000 .190-003 | -.200-004 .000 | -.200-004 .000 | -.600-004 .000 | .200-004 .000 | -.200-004 .000 | .000 .000 | -.100-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 12 | .000 -.700-004 | .333-004 .000 | .133-004 .000 | -.200-004 .000 | -.400-004 .000 | .100-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 13 | .000 .500-005 | -.333-004 .000 | .133-004 .000 | .120-003 .000 | -.400-004 .000 | -.100-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 14 | .000 .000 | -.333-004 .000 | .133-004 .000 | -.400-004 .000 | -.300-004 .000 | .900-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 15 | .000 .500-005 | -.333-004 .000 | .133-004 .000 | -.200-004 .000 | -.300-004 .000 | .900-004 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |

ARRAY WU
(1/SEC)

| LINE | ZONE | | | | | | | | | | | | | | |
|------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | |
| 1 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 2 | .264-001 | .347-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 3 | .452-002 | .190-001 | .262-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 4 | .272-002 | .426-002 | .170-001 | .265-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 5 | .182-002 | .199-002 | .400-002 | .209-001 | .103-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 6 | .928-003 | .744-003 | .135-002 | .261-002 | .139-001 | .207-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 7 | .474-003 | .125-002 | .763-003 | .127-002 | .198-002 | .124-001 | .190-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 8 | .400-004 | .132-002 | .654-003 | .595-003 | .116-002 | .220-002 | .992-002 | .167-001 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 9 | .400-004 | .953-003 | .545-003 | .696-003 | .108-002 | .712-003 | .278-002 | .629-002 | .137-001 | .000 | .000 | .000 | .000 | .000 | .000 |
| 10 | .434-003 | .140-003 | .116-002 | .176-003 | .520-003 | .564-003 | .481-003 | .873-004 | .725-002 | .197-00 | .000 | .000 | .000 | .000 | .000 |
| 11 | .000 | .364-003 | .153-002 | .176-003 | .903-003 | .236-003 | .481-003 | .873-004 | .453-003 | .390-00 | .000 | .000 | .000 | .000 | .000 |
| 12 | .434-003 | .698-004 | .592-003 | .134-002 | .780-005 | .206-003 | .959-004 | .449-003 | .252-003 | .661-00 | .000 | .000 | .000 | .000 | .000 |
| 13 | .434-003 | .698-004 | .109-003 | .124-002 | .580-003 | .206-003 | .959-004 | .679-004 | .245-003 | .821-00 | .000 | .000 | .000 | .000 | .000 |
| 14 | .434-003 | .698-004 | .109-003 | .672-003 | .115-002 | .206-003 | .959-004 | .679-004 | .144-003 | .104-00 | .000 | .000 | .000 | .000 | .000 |
| 15 | .434-003 | .698-004 | .109-003 | .672-003 | .115-002 | .206-003 | .959-004 | .679-004 | .144-003 | .104-00 | .000 | .000 | .000 | .000 | .000 |

APRAY MW
(1/SEC)

| LINE | ZONE | | | | | | | | | | | | | | |
|------|-----------------------|------------------------|------------------------|-----------------------|----------------------|-------------------|-------------------|-------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 1 | -.370-001 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 2 | .124-001 .000 | -.198-001 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 3 | .138-002 .000 | .660-002 .000 | -.970-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 4 | .752-003 .000 | .397-003 .000 | .232-002 .000 | -.568-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 5 | .501-003 .000 | -.433-004 .000 | .900-004 .000 | .211-002 .000 | -.413-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 6 | .128-003 .000 | -.205-003 .000 | -.121-003 .000 | .274-004 .000 | .114-002 .000 | -.207-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 7 | .300-005 .000 | .161-003 .000 | -.195-003 .000 | -.858-004 .000 | .340-004 .000 | .172-002 .000 | -.237-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 8 | -.245-003 .000 | .290-003 .000 | -.167-003 .000 | -.140-003 .000 | -.740-005 .000 | .391-003 .000 | .138-002 .000 | -.223-002 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 9 | -.245-003 .000 | .151-003 .000 | -.139-003 .000 | -.117-003 .000 | .480-005 .000 | .199-003 .000 | .408-003 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 10 | .125-003 .000 | -.237-003 .000 | .147-003 .000 | -.172-003 .000 | -.370-005 .000 | .128-003 .000 | .871-004 .000 | .261-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 11 | .000 -.610-003 | .129-003 .000 | .276-003 .000 | -.172-003 .000 | .292-004 .000 | .952-004 .000 | .871-004 .000 | .261-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 12 | .248-003 .222-003 | -.118-003 -.478-003 | .776-004 .000 | .109-003 .000 | -.817-004 .000 | .633-004 .000 | .329-004 .000 | .727-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 13 | .248-003 -.173-004 | -.118-003 .195-003 | -.278-004 -.472-003 | .133-003 .000 | -.370-005 .000 | .833-004 .000 | .329-004 .000 | .203-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 14 | .248-003 -.130-005 | -.118-003 -.399-004 | -.278-004 -.478-004 | .546-004 -.120-003 | .743-004 .000 | .833-004 .000 | .329-004 .000 | .203-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 15 | .248-003 -.171-004 | -.118-003 -.795-005 | -.278-004 -.114-003 | .546-004 -.106-003 | .743-004 .532-004 | .833-004 .000 | .329-004 .000 | .203-004 .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

PARTIAL DERIVATIVES
ASCENT RATE = 300.0 M/MIN

| ZONE | D1DZ | D1DZ | DXDE | DYDF | DXDA | DYDA | D1FS | D1DF |
|------|-------------|-------------|--------------|--------------|-------------|--------------|-------------|-------------|
| 1 | .198436+001 | .185823+001 | -.122547+004 | -.116757+004 | .371806+003 | -.397043+003 | .345215+000 | .543951+003 |
| 2 | .23595+001 | .163499+001 | -.379087+004 | -.267080+004 | .817920+003 | -.117859+004 | .329244+000 | .143460+004 |
| 3 | .29701+001 | .166239+001 | -.109041+005 | -.532055+004 | .146385+004 | -.300000+004 | .287994+000 | .733709+004 |
| 4 | .356920+001 | .131109+001 | -.218069+005 | -.801041+004 | .197043+004 | -.536414+004 | .254288+000 | .571460+004 |
| 5 | .410106+001 | .117673+001 | -.370355+005 | -.105268+005 | .236107+004 | -.822862+004 | .228130+000 | .856966+004 |
| 6 | .48965+001 | .999314+000 | -.749017+005 | -.156878+005 | .301724+004 | -.147905+005 | .196045+000 | .150551+005 |
| 7 | .542955+001 | .969105+000 | -.125001+006 | -.223112+005 | .391469+004 | -.219438+005 | .178295+000 | .222906+005 |
| 8 | .576462+001 | .936739+000 | -.177681+006 | -.287144+005 | .475272+004 | -.794092+005 | .167765+000 | .297906+005 |
| 9 | .638879+001 | .102789+001 | -.259433+006 | -.417402+005 | .630025+004 | -.391587+005 | .152584+000 | .396620+005 |
| 10 | .638215+001 | .954958+000 | -.347153+006 | -.519443+005 | .786115+004 | -.525374+005 | .152947+000 | .531217+005 |
| 11 | .661169+001 | .879838+000 | -.468620+006 | -.623608+005 | .914476+004 | -.687197+005 | .148041+000 | .693241+005 |
| 12 | .681028+001 | .826547+000 | -.601471+006 | -.730233+005 | .104241+005 | -.858884+005 | .143977+000 | .865160+005 |
| 13 | .693962+001 | .789258+000 | -.740365+006 | -.839613+005 | .117493+005 | -.103605+006 | .141034+000 | .104244+006 |
| 14 | .694708+001 | .715460+000 | -.850128+006 | -.875523+005 | .122965+005 | -.119301+006 | .141994+000 | .110925+006 |
| 15 | .681110+001 | .616263+000 | -.924994+006 | -.836837+005 | .119825+005 | -.132434+006 | .144284+000 | .132945+006 |

PARTIAL DERIVATIVES
ASCENT RATE = 400.0 M/MIN

| ZONE | DYDZ | DYD7 | DYD6 | DYD5 | DYD4 | DYD3 | DYD2 | DYD1 | DYD0 |
|------|-------------|-------------|--------------|--------------|-------------|--------------|-------------|-------------|------|
| 1 | .156984+001 | .148765+001 | -.624598+003 | -.781471+003 | .297653+003 | -.314100+003 | .419672+000 | .432731+003 | |
| 2 | .179890+001 | .124335+001 | -.278720+004 | -.167651+004 | .631855+003 | -.899706+003 | .414054+000 | .109941+004 | |
| 3 | .226496+001 | .111597+001 | -.642011+004 | -.376181+004 | .111160+004 | -.226641+004 | .368169+000 | .252658+004 | |
| 4 | .269077+001 | .96948+000 | -.170037+005 | -.481794+004 | .149723+004 | -.404103+004 | .329011+000 | .430948+004 | |
| 5 | .308746+001 | .92692+000 | -.718090+005 | -.630721+004 | .178928+004 | -.619696+004 | .297007+000 | .644050+004 | |
| 6 | .368949+001 | .758015+000 | -.7979+005 | -.920783+004 | .228279+004 | -.111110+005 | .256492+000 | .113431+005 | |
| 7 | .409397+001 | .734408+000 | -.724873+005 | -.130634+005 | .295566+004 | -.164764+005 | .233624+000 | .167394+005 | |
| 8 | .437243+001 | .733262+000 | -.102729+006 | -.172276+005 | .369800+004 | -.220511+005 | .219864+000 | .223590+005 | |
| 9 | .457611+001 | .738709+000 | -.174468+006 | -.217424+005 | .448236+004 | -.277671+005 | .210693+000 | .281264+005 | |
| 10 | .484467+001 | .726934+000 | -.201255+006 | -.301854+005 | .591363+004 | -.394278+005 | .196685+000 | .398685+005 | |
| 11 | .504073+001 | .672577+000 | -.272304+006 | -.363331+005 | .687947+004 | -.515592+005 | .192655+000 | .520156+005 | |
| 12 | .521212+001 | .634428+000 | -.350290+006 | -.424379+005 | .783751+004 | -.643887+005 | .142757+000 | .648629+005 | |
| 13 | .535280+001 | .608928+000 | -.432829+006 | -.462381+005 | .683469+004 | -.776792+005 | .182117+000 | .781782+005 | |
| 14 | .536947+001 | .551934+000 | -.499903+006 | -.515718+005 | .523876+004 | -.895544+005 | .181714+000 | .900247+005 | |
| 15 | .527731+001 | .478415+000 | -.545353+006 | -.494391+005 | .901124+004 | -.994012+005 | .184939+000 | .968048+005 | |

PARTIAL DERIVATIVES
ASCENT RATE = 500.0 M/Min

| ZONE | DXRZ | DYD7 | DXDE | DYDF | DXDA | DYDA | DYDS | DYDF |
|------|-------------|-------------|--------------|--------------|-------------|--------------|-------------|-------------|
| 1 | .131953+001 | .126362+001 | -.626788+007 | -.600228+003 | .252771+003 | -.263956+003 | .480121+000 | .765447+003 |
| 2 | .146748+001 | .103965+001 | -.172161+004 | -.122304+004 | .519916+003 | -.731864+003 | .486611+000 | .897740+003 |
| 3 | .182421+001 | .907529+000 | -.461410+004 | -.229548+004 | .907950+003 | -.182505+004 | .440540+000 | .203843+004 |
| 4 | .216196+001 | .807895+000 | -.689469+004 | -.332457+004 | .121287+004 | -.724569+004 | .397487+000 | .346491+004 |
| 5 | .247740+001 | .722095+000 | -.147255+005 | -.429210+004 | .144621+004 | -.496171+004 | .361242+000 | .514818+004 |
| 6 | .205931+001 | .412304+000 | -.298427+005 | -.617470+004 | .184174+004 | -.890127+004 | .314021+000 | .908991+004 |
| 7 | .328436+001 | .592134+000 | -.479747+005 | -.864931+004 | .237842+004 | -.131923+005 | .286868+000 | .134050+005 |
| 8 | .350993+001 | .591140+000 | -.677812+005 | -.114157+005 | .257293+004 | -.176520+005 | .270281+000 | .179005+005 |
| 9 | .367473+001 | .595834+000 | -.886591+005 | -.147755+005 | .360213+004 | -.222156+005 | .259197+000 | .225057+005 |
| 10 | .389833+001 | .586088+000 | -.132305+006 | -.198911+005 | .474144+004 | -.315374+005 | .245992+000 | .319917+005 |
| 11 | .406149+001 | .542639+000 | -.178978+006 | -.239126+005 | .550877+004 | -.412314+005 | .236738+000 | .415975+005 |
| 12 | .421205+001 | .513444+000 | -.230763+006 | -.281297+005 | .628180+004 | -.515329+005 | .228977+000 | .519138+005 |
| 13 | .433471+001 | .493878+000 | -.285346+006 | -.325111+005 | .708163+004 | -.621547+005 | .222954+000 | .625558+005 |
| 14 | .435405+001 | .449947+000 | -.329758+006 | -.340772+005 | .740093+004 | -.716173+005 | .222184+000 | .719972+005 |
| 15 | .428521+001 | .389231+000 | -.360454+006 | -.327405+005 | .722136+004 | -.795031+005 | .225766+000 | .759283+005 |

PROBLEM 1

WIND ERROR INPUT
ASSUMED ONE SIGMA ERRORS

EXAMPLE RADAR PROBLEM

| | | | |
|----------------------------------|------|----------------------------------|-------|
| ELEVATION BIAS ERROR (DEGREES) = | .03 | ELEVATION RANDOM ERR (DEGREES) = | .05 |
| AZIMUTH BIAS ERROR (DEGREES) = | .03 | AZIMUTH RANDOM ERROR (DEGREES) = | .05 |
| RANGE BIAS ERROR (METERS) = | .00 | RANGE RANDOM ERROR (METERS) = | 16.00 |
| DISPL. LAUNCH ERROR (METERS) = | 5.00 | AZIMUTH LAUNCH ERROR (METERS) = | .00 |
| BACKGROUND ELEVATION (DEGREES) = | 5.00 | | |

PROBLEM 1

INDIVIDUAL SUMS
ASCENT RATE = 300.0 M/MIN

UNITS APE (M/SEC)**

| LINE | PIAS RANDOM | PEYL | PEYL | REYS REYS | BELXE**2 RELXE | PERXF**2 PERKF | BEXA**2 REXA | REYS**2 REYS | BELYE**2 RELVE | PERYF**2 PERYF | REYA**2 REVA |
|------|----------------|---------|---------|--------------------|---------------------|-------------------------|--------------------|--------------------|--------------------|----------------------|--------------------|
| 1 | PIAS RANDOM | .00669R | .008927 | .000000 .31930R | .00775 .00152 | .000000 .000001 | .000024 .000066 | .000000 .290440 | .000653 .001815 | .000000 .000001 | .000037 .000075 |
| 2 | PIAS RANDOM | .00026P | .000357 | .000000 .116260 | .001574 .008170 | .000000 .000003 | .000017 .000098 | .000000 .091855 | .000610 .003274 | .000000 .000001 | .000042 .000196 |
| 3 | PIAS RANDOM | .000054 | .000072 | .000000 .053822 | .004039 .022201 | .000000 .000134 | .000013 .000093 | .000000 .022801 | .000695 .003802 | .000000 .000024 | .000074 .000373 |
| 4 | PIAS RANDOM | .000024 | .000032 | .000000 .049742 | .002254 .063152 | .000000 .000057 | .000010 .00010R | .000000 .012752 | .000699 .004983 | .000000 .000004 | .000111 .000749 |
| 5 | PIAS RANDOM | .000011 | .000014 | .000000 .046954 | .015931 .186482 | .000769 .217838 | .000007 .000152 | .000000 .011052 | .000665 .007539 | .000011 .008912 | .000159 .001889 |
| 6 | PIAS RANDOM | .000006 | .000008 | .000000 .039229 | .030831 .262021 | .002241 1.844705 | .000005 .000085 | .000000 .003035 | .000626 .005671 | .000046 .019267 | .002325 .001651 |
| 7 | PIAS RANDOM | .000003 | .000004 | .000000 .03925R | .044017 .508372 | .151218 8.686936 | .000006 .000101 | .000000 .001658 | .000904 .011610 | .003288 .19488R | .000269 .003011 |
| 8 | PIAS RANDOM | .000003 | .000004 | .000000 .034220 | .053010 .727932 | .620512 5.78027R | .000005 .000107 | .000000 .001089 | .001022 .015851 | .013731 .129160 | .000296 .003985 |
| 9 | PIAS RANDOM | .000003 | .000004 | .000000 .026493 | .060508 .87010R | 52.548163 298.256569 | .000009 .000110 | .000000 .000765 | .001731 .019232 | 1.156321 6.560527 | .000387 .004251 |
| 10 | PIAS RANDOM | .000001 | .000001 | .000000 .019042 | .062076 1.043244 | 16.256746 440.389820 | .000006 .000115 | .000000 .000518 | .001081 .016035 | .290852 8.028242 | .000314 .004975 |
| 11 | PIAS RANDOM | .000000 | .000000 | .000000 .008236 | .082347 .826716 | 30.605093 503.115832 | .000005 .000067 | .000000 .000228 | .001020 .008581 | .402145 5.275267 | .000381 .003677 |
| 12 | PIAS RANDOM | .000000 | .000000 | .000000 .005428 | .091250 .827986 | 36.057017 641.198814 | .000004 .000055 | .000000 .000130 | .000997 .008177 | .406108 5.878863 | .000402 .003605 |
| 13 | PIAS RANDOM | .000000 | .000000 | .000000 .00365P | .098643 .827253 | 32.271132 646.754814 | .000004 .000044 | .000000 .000093 | .001092 .007590 | .341007 5.587165 | .000420 .003373 |
| 14 | PIAS RANDOM | .000000 | .000000 | .000000 .002241 | .092891 .566846 | 30.042880 414.040524 | .000003 .000028 | .000000 .000056 | .000793 .002404 | .275254 1.741392 | .000409 .002556 |
| 15 | PIAS RANDOM | .000000 | .000000 | .000000 .001406 | .084399 .746576 | 27.922839 253.838074 | .000003 .000017 | .000000 .000042 | .000622 .000631 | .220316 4.45535 | .000290 .001911 |

PROBLEM 1

INDIVIDUAL SUMS
ACCENT RATE = 40.0 M/MIN

UNITS ARE (M/SEC)**2

| LINE | REYL | RFYL | REXS**2 REXS | DELVE**2 RELVE | FERXF**2 FERXE | REXA**2 REXA | PEYS**2 PEYS | RFLYE**2 RELVE | PERVE**2 PERVE | BEYA**2 REYA |
|------|----------------|---------|--------------------|---------------------|---------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| 1 | PIAS RANDOM | .011908 | .000000 3.12771 | .000565 .001570 | .000000 .000002 | .000027 .000075 | .000000 2.96987 | .000495 .001367 | .000000 .000001 | .000030 .000053 |
| 2 | PIAS RANDOM | .000476 | .000000 .09950 | .000987 .002272 | .000000 .000010 | .000017 .000104 | .000000 .084930 | .000386 .002177 | .000000 .000004 | .000043 .000204 |
| 3 | PIAS RANDOM | .000096 | .000000 .078889 | .002435 .001364E | .000000 .000016 | .000013 .000096 | .000000 .020117 | .000421 .002441 | .000000 .000003 | .000075 .000378 |
| 4 | PIAS RANDOM | .000043 | .000000 .05132 | .004883 .037713 | .000000 .000019 | .000010 .000111 | .000000 .011597 | .000415 .003058 | .000000 .000002 | .000112 .000756 |
| 5 | PIAS RANDOM | .000019 | .000000 .048369 | .009276 .108686 | .000000 .000108 | .000007 .000155 | .000000 .010309 | .000398 .004563 | .000000 .000004 | .000159 .001608 |
| 6 | PIAS RANDOM | .000011 | .000000 .030814 | .017844 .152433 | .000000 .000200 | .000005 .000087 | .000000 .002860 | .000364 .003375 | .000000 .000005 | .000225 .001858 |
| 7 | PIAS RANDOM | .000005 | .000000 .032074 | .025402 .294307 | .000170 .227804 | .000006 .000102 | .000000 .001451 | .000523 .006797 | .000004 .005087 | .000269 .003038 |
| 8 | PIAS RANDOM | .000005 | .000000 .028849 | .030509 .429159 | .001848 .916099 | .000006 .000114 | .000000 .001033 | .000632 .005470 | .000040 .020448 | .000205 .003965 |
| 9 | PIAS RANDOM | .000005 | .000000 .019980 | .034110 .435740 | .002705 1.433578 | .000007 .000102 | .000000 .000618 | .000711 .009692 | .000058 .031913 | .000312 .003849 |
| 10 | PIAS RANDOM | .000001 | .000000 .016072 | .042422 .565429 | .001547 4.127723 | .000006 .000113 | .000000 .000458 | .000750 .010724 | .000028 .075493 | .000352 .004874 |
| 11 | PIAS RANDOM | .000000 | .000000 .007421 | .048258 .479108 | .006862 7.119745 | .000005 .000068 | .000000 .000220 | .000598 .005036 | .000064 .076111 | .000383 .003679 |
| 12 | PIAS RANDOM | .000000 | .000000 .004951 | .053264 .514804 | .080755 9.744292 | .000004 .000055 | .000000 .000127 | .000582 .004708 | .000777 .090244 | .000402 .003603 |
| 13 | PIAS RANDOM | .000000 | .000000 .073493 | .057891 .507768 | .129268 5.350929 | .000004 .000045 | .000000 .000082 | .000589 .004465 | .001137 .047358 | .000470 .003371 |
| 14 | PIAS RANDOM | .000000 | .000000 .002145 | .054471 .332875 | .069421 1.972405 | .000003 .000028 | .000000 .000057 | .000443 .001449 | .000515 .005518 | .000409 .002559 |
| 15 | PIAS RANDOM | .000000 | .000000 .001368 | .049219 .204820 | .072894 1.625837 | .000003 .000017 | .000000 .000043 | .000360 .000386 | .000417 .003247 | .000388 .001913 |

PROBLEM 1

INDIVIDUAL SUMS
ASCENT RATE = 500.0 M/MIN

UNITS ARE (M/SEC)**2

| LINE | PEXL | RFYL | PEXS**2 PEXS | EELYE**2 RELYE | PERXE**2 PERXF | REXA**2 REXA | REYS**2 PEYS | DELYE**2 RELYE | PERYE**2 PERYE | REYA**2 REYA |
|------|----------------|---------|-----------------|--------------------|--------------------|--------------------|--------------------|--------------------|---------------------|--------------------|
| 1 | PIAS RANDOM | .018606 | .024797 | .000466 .315456 | .000000 .000000 | .000330 .000004 | .000000 .311564 | .000407 .001131 | .000000 .000000 | .000033 .000022 |
| 2 | PIAS RANDOM | .000744 | .000992 | .000715 .070634 | .000000 .000014 | .000118 .000111 | .000000 .000784 | .000282 .001666 | .000000 .000004 | .000044 .000212 |
| 3 | PIAS RANDOM | .000151 | .000201 | .001699 .009608 | .000000 .000005 | .000013 .000100 | .000000 .018004 | .000294 .001765 | .000000 .000001 | .000075 .000394 |
| 4 | PIAS RANDOM | .000067 | .000089 | .001317 .025851 | .000000 .000041 | .000010 .000114 | .000000 .010618 | .000283 .002160 | .000000 .000003 | .000112 .000743 |
| 5 | PIAS RANDOM | .000030 | .000040 | .006196 .071979 | .000000 .000026 | .000007 .000159 | .000000 .009649 | .000260 .003172 | .000000 .000001 | .000159 .001707 |
| 6 | PIAS RANDOM | .000017 | .000022 | .011793 .101416 | .000000 .000054 | .000005 .000008 | .000000 .002697 | .000241 .002303 | .000000 .000001 | .000226 .001843 |
| 7 | PIAS RANDOM | .000007 | .000010 | .016703 .194471 | .000000 .001491 | .000006 .000104 | .000000 .001334 | .000344 .004546 | .000000 .0000034 | .000269 .001044 |
| 8 | PIAS RANDOM | .000007 | .000010 | .020044 .276777 | .000001 .004748 | .000006 .000115 | .000000 .000921 | .000417 .004289 | .000000 .000107 | .000295 .001970 |
| 9 | PIAS RANDOM | .000007 | .000010 | .022354 .286300 | .000000 .001308 | .000007 .000102 | .000000 .000552 | .000468 .006411 | .000000 .000030 | .000312 .001851 |
| 10 | PIAS RANDOM | .000002 | .000002 | .027814 .384201 | .000035 .068224 | .000006 .000114 | .000000 .000417 | .000492 .007080 | .000001 .001753 | .000352 .004873 |
| 11 | BIAS RANDOM | .000000 | .000000 | .031639 .314206 | .000159 .279456 | .000005 .000068 | .000000 .000210 | .000391 .001335 | .000002 .000047 | .000393 .001677 |
| 12 | PIAS RANDOM | .000000 | .000000 | .035122 .338397 | .000094 .627700 | .000004 .000055 | .000000 .000123 | .000383 .001811 | .000009 .000546 | .000403 .001605 |
| 13 | BIAS RANDOM | .000000 | .000000 | .038119 .331942 | .001422 .875051 | .000004 .000045 | .000000 .000079 | .000388 .002959 | .000012 .007661 | .000420 .001372 |
| 14 | BIAS RANDOM | .000000 | .000000 | .035843 .219379 | .001122 .631354 | | .000000 .000058 | .000305 .000973 | .000008 .002767 | .000408 .001558 |
| 15 | BIAS RANDOM | .000000 | .000000 | .032481 .135611 | .000709 .368247 | .000003 .000017 | .000000 .000044 | .000237 .000263 | .000004 .000664 | .000387 .001912 |

PROBLEM 1 VARIANCE IN COMPONENTS

| LINE | 300.0 | | 400.0 | | 500.0 | |
|------|--------------------------------|---------------------------------|--------------------------------|---------------------------------|--------------------------------|---------------------------------|
| | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 |
| 1 | .3202 | .30194 | .7262 | .31680 | .33594 | .33802 |
| 2 | .12635 | .09634 | .09652 | .08828 | .07616 | .08399 |
| 3 | .08045 | .02793 | .05459 | .02354 | .03924 | .02072 |
| 4 | .12085 | .01933 | .07791 | .01600 | .05399 | .01403 |
| 5 | .48764 | .02994 | .16762 | .01715 | .11436 | .01499 |
| 6 | 2.17912 | .05073 | .20120 | .00870 | .13680 | .00735 |
| 7 | 9.42991 | .21565 | .57987 | .01722 | .23850 | .00958 |
| 8 | 7.21609 | .16536 | 1.79849 | .03589 | .32565 | .01201 |
| 9 | 351.78196 | 7.74326 | 1.02823 | .04704 | .32701 | .01163 |
| 10 | 457.77105 | 8.34502 | 4.77331 | .09268 | .49431 | .01447 |
| 11 | 534.83798 | 5.59128 | 7.66147 | .08611 | .63205 | .01104 |
| 12 | 679.24055 | 6.29531 | 10.79822 | .10053 | 1.00656 | .01355 |
| 13 | 678.00104 | 5.94070 | 6.04930 | .05742 | 1.25163 | .01491 |
| 14 | 444.76541 | 2.02286 | 2.43831 | .01397 | .88973 | .00708 |
| 15 | 282.19330 | .66945 | 1.95416 | .00675 | .53835 | .00351 |

PROBLEM 1

COMPONENT VELOCITY VARIANCE

ASCENT RATE, W/MIN = 300.0

400.0

500.0

| LINE | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) |
|------|-----------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------------------|
| 1 | 1.19046 | 1.09108 | 1.21076 | 1.10035 | 1.27159 | 1.12765 |
| 2 | .62015 | .64819 | .74864 | .59047 | .70216 | .54969 |
| 3 | .20448 | .45220 | .14822 | .38499 | .11314 | .33636 |
| 4 | .26448 | .51427 | .17718 | .42093 | .12834 | .35825 |
| 5 | .97655 | .98820 | .74861 | .59047 | .24405 | .49402 |
| 6 | 4.20714 | 2.05113 | .39603 | .62931 | .27198 | .52152 |
| 7 | 18.19864 | 4.26599 | 1.12654 | 1.06139 | .66906 | .68415 |
| 8 | 13.92685 | 3.73187 | 2.70630 | 1.64508 | .53708 | .79817 |
| 9 | 478.32971 | 26.04476 | 3.72684 | 1.93050 | .63894 | .79933 |
| 10 | 970.43867 | 29.65533 | 9.18085 | 3.02999 | .95994 | .97977 |
| 11 | 1019.83685 | 31.93484 | 14.61765 | 3.92330 | 1.21334 | 1.10152 |
| 12 | 1291.53949 | 35.93799 | 19.80838 | 4.45064 | 1.92469 | 1.38733 |
| 13 | 1790.41855 | 35.92240 | 11.52177 | 3.39437 | 2.38963 | 1.54584 |
| 14 | 842.97221 | 29.03398 | 4.62681 | 2.15100 | 1.69204 | 1.30078 |
| 15 | 533.68775 | 23.10168 | 3.69972 | 1.92347 | 1.02236 | 1.01112 |

***** PROGRAM NAVAID *****

EXAMPLE NAVAID RUN FOR 15 ZONES AND 3 ASCENT RATES
USE INPUT FILFS AR, ZMHE, UV, WF

ARRAY W
(T/METER)

| LINE | WD | ZONE | | | | | | | | | | | | | | |
|------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 1 | -500-002 | .500-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 2 | -100-002 | -.167-002 | .267-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 3 | -450-003 | -.183-003 | -.807-003 | .146-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 4 | -300-003 | -.100-003 | -.120-003 | -.600-003 | .112-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 5 | -200-003 | -.667-004 | -.333-004 | -.100-003 | -.660-003 | .106-002 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 6 | -150-003 | -.147-004 | .667-005 | -.200-004 | -.600-004 | -.390-003 | .630-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 7 | -100-003 | .000 | -.400-004 | .000 | -.200-004 | -.400-004 | -.330-003 | .530-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 8 | -100-003 | .333-004 | -.533-004 | .000 | .000 | -.200-004 | -.500-004 | -.260-003 | .450-003 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 9 | -100-003 | .333-004 | -.333-004 | .000 | .000 | -.200-004 | -.100-004 | -.700-004 | -.140-003 | .360-003 | .000 | .000 | .000 | .000 | .000 | .000 |
| 10 | -500-004 | -.167-004 | .267-004 | -.400-004 | .200-004 | -.100-004 | -.100-004 | -.100-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 11 | .000 | .190-003 | -.200-004 | -.600-004 | .260-004 | -.200-004 | .000 | -.100-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 12 | .000 | -.333-004 | .133-004 | -.200-004 | -.400-004 | .100-004 | .000 | .000 | -.100-004 | -.500-005 | .500-005 | .000 | .000 | .000 | .000 | .000 |
| 13 | .000 | -.333-004 | .133-004 | .000 | -.400-004 | -.100-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 14 | .000 | -.333-004 | .133-004 | .000 | -.200-004 | -.300-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| 15 | .000 | -.333-004 | .500-005 | .100-004 | -.200-004 | -.300-004 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

APRAY LU
(1/SEC)

| LINE | ZONE | | | | | | | | | | | | | | |
|------|-----------------------|------------------------|-----------------------|-----------------------|-----------------------|-----------|-----------|-----------|-----------|-----------|--|--|--|--|--|
| | 1 11 | 2 12 | 3 13 | 4 14 | 5 15 | 6 | 7 | 8 | 9 | 10 | | | | | |
| 1 | -.414-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 2 | .266-001 .000 | -.347-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 3 | .452-002 .000 | .180-001 .000 | -.242-001 .000 | .000 .000 | .000 .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 4 | .272-002 .000 | .426-002 .000 | .170-001 .000 | -.265-001 .000 | .000 .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 5 | .182-002 .000 | .199-002 .000 | .400-002 .000 | .209-001 .000 | -.303-001 .000 | .000 | .000 | .000 | .000 | .000 | | | | | |
| 6 | .928-003 .000 | .744-003 .000 | .135-002 .000 | .261-002 .000 | .138-001 .000 | -.207-001 | .000 | .000 | .000 | .000 | | | | | |
| 7 | .474-003 .000 | .125-002 .000 | .763-003 .000 | .127-002 .000 | .198-002 .000 | .124-001 | -.190-001 | .000 | .000 | .000 | | | | | |
| 8 | .400-004 .000 | .132-002 .000 | .654-003 .000 | .595-003 .000 | .116-002 .000 | .220-002 | .992-002 | -.167-001 | .000 | .000 | | | | | |
| 9 | .400-004 .000 | .953-003 .000 | .545-003 .000 | .496-003 .000 | .108-002 .000 | .712-003 | .278-002 | .629-002 | -.137-001 | .000 | | | | | |
| 10 | .454-003 .000 | -.140-003 .000 | .116-002 .000 | -.176-003 .000 | .580-003 .000 | .564-003 | .481-003 | .873-004 | .725-002 | -.107-001 | | | | | |
| 11 | .000 -.768-002 | .364-003 .000 | .153-002 .000 | -.176-003 .000 | .908-003 .000 | .236-003 | .481-003 | .873-004 | .453-003 | .380-002 | | | | | |
| 12 | .434-003 .320-002 | -.698-004 -.643-002 | .582-003 .000 | .134-002 .000 | .780-005 .000 | .206-003 | .959-004 | .445-003 | .252-003 | -.641-004 | | | | | |
| 13 | .434-003 -.416-004 | -.698-004 .253-002 | .109-003 -.532-002 | .124-002 .000 | .580-003 .000 | .206-003 | .959-004 | .679-004 | .245-003 | -.821-004 | | | | | |
| 14 | .434-003 .161-003 | -.698-004 -.573-003 | .109-003 .133-002 | .622-003 -.355-002 | .115-002 .000 | .206-003 | .959-004 | .679-004 | -.144-003 | .104-003 | | | | | |
| 15 | .434-003 -.663-004 | -.698-004 -.144-003 | .109-003 -.640-003 | .622-003 .724-003 | .115-002 -.230-002 | .206-003 | .959-004 | .679-004 | -.338-003 | .940-004 | | | | | |

APRAY WV
(1/SEC)

| LINE | ZONE | | | | | | | | | |
|------|-----------------------|------------------------|------------------------|-----------------------|----------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 1 11 | 2 12 | 3 13 | 4 14 | 5 15 | 6 | 7 | 8 | 9 | 10 |
| 1 | -.370-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 2 | .124-001 .000 | -.198-001 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 3 | .138-002 .000 | .460-002 .000 | -.970-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 4 | .752-003 .000 | .387-003 .000 | .272-002 .000 | -.568-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 5 | .501-003 .000 | -.433-004 .000 | .900-004 .000 | .211-002 .000 | -.413-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 6 | .128-003 .000 | -.205-003 .000 | -.121-003 .000 | .224-004 .000 | .114-002 .000 | -.207-002 .000 | .000 .000 | .000 .000 | .000 .000 | .000 .000 |
| 7 | .300-005 .000 | .161-003 .000 | -.195-003 .000 | -.856-004 .000 | .340-004 .000 | .172-002 .000 | -.227-002 .000 | .000 .000 | .000 .000 | .000 .000 |
| 8 | -.245-003 .000 | .250-003 .000 | -.167-003 .000 | -.140-003 .000 | -.740-005 .000 | .391-003 .000 | .138-002 .000 | -.223-002 .000 | .000 .000 | .000 .000 |
| 9 | -.245-003 .000 | .151-003 .000 | -.139-003 .000 | -.117-003 .000 | .480-005 .000 | .188-003 .000 | .408-003 .000 | .896-003 .000 | -.199-002 .000 | .000 .000 |
| 10 | .125-003 .000 | -.237-003 .000 | .147-003 .000 | -.172-003 .000 | -.370-005 .000 | .128-003 .000 | .871-004 .000 | .261-004 .000 | .835-003 .000 | -.131-002 .000 |
| 11 | .000 -.610-003 | .129-003 .000 | .276-003 .000 | -.172-003 .000 | .292-004 .000 | .952-004 .000 | .871-004 .000 | .261-004 .000 | .140-005 .000 | .135-004 .000 |
| 12 | .248-003 .222-003 | -.118-003 -.478-003 | .776-004 .000 | .109-003 .000 | -.817-004 .000 | .833-004 .000 | .329-004 .000 | .727-004 .000 | -.155-004 .000 | -.147-004 .000 |
| 13 | .248-003 -.173-004 | -.118-003 .195-003 | -.275-004 -.402-003 | .133-003 .000 | -.370-005 .000 | .833-004 .000 | .329-004 .000 | .203-004 .000 | -.126-004 .000 | -.132-003 .000 |
| 14 | .248-003 -.130-005 | -.118-003 -.399-004 | -.276-004 -.478-004 | .546-004 -.120-003 | .743-004 .000 | .833-004 .000 | .329-004 .000 | .203-004 .000 | -.580-004 .000 | -.100-004 .000 |
| 15 | .248-003 -.171-004 | -.118-003 -.795-005 | -.276-004 -.114-003 | .546-004 -.106-003 | .743-004 .532-004 | .833-004 .000 | .329-004 .000 | .203-004 .000 | -.816-004 .000 | -.974-004 .000 |

PROBLEM 1

WIND ERROR INPUT
ASSUMED ONE SIGMA ERRORS

EXAMPLE NAVOID PROBLEM

EAST TRACKING ERROR (METERS) = 100.00
NORTH TRACKING ERROR (METERS) = 100.00
RANDOM LAUNCH ERROR (METERS) = 5.00

PROBLEM 1 INDIVIDUAL SUMS
ASCENT RATE = 300.0 M/MIN

UNITS ARE (M/SEC)**2

| LINE | REXL | REYL | BEYZ**2 | REXZ | REXY | REYZ**2 | REYZ | REYV |
|------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1 | .028646 | .028646 | .022468 | .022468 | .154250 | .001971 | .001971 | .156250 |
| 2 | .001146 | .001146 | .000180 | .003044 | .061806 | .000118 | .000885 | .041804 |
| 3 | .000232 | .000232 | .000028 | .001739 | .017237 | .000020 | .000185 | .017237 |
| 4 | .000103 | .000103 | .000077 | .002111 | .010242 | .000017 | .000083 | .010242 |
| 5 | .000046 | .000046 | .000053 | .003375 | .009842 | .000008 | .000054 | .009842 |
| 6 | .000026 | .000026 | .000054 | .001894 | .002218 | .000005 | .000017 | .002218 |
| 7 | .000011 | .000011 | .000124 | .002255 | .001241 | .000005 | .000037 | .001241 |
| 8 | .000011 | .000011 | .000080 | .002108 | .000879 | .000004 | .000039 | .000879 |
| 9 | .000011 | .000011 | .000102 | .001645 | .000517 | .000005 | .000032 | .000517 |
| 10 | .000003 | .000003 | .000118 | .001630 | .000363 | .000003 | .000024 | .000363 |
| 11 | .000000 | .000000 | .000154 | .001158 | .000169 | .000002 | .000007 | .000169 |
| 12 | .000000 | .000000 | .000225 | .001299 | .000107 | .000002 | .000007 | .000107 |
| 13 | .000000 | .000000 | .000193 | .001163 | .000073 | .000002 | .000007 | .000073 |
| 14 | .000000 | .000000 | .000252 | .000728 | .000047 | .000002 | .000001 | .000047 |
| 15 | .000000 | .000000 | .000228 | .000412 | .000035 | .000001 | .000002 | .000035 |

PROBLEM 1 INDIVIDUAL SUMS
ASCENT RATE = 400.0 M/MIN

UNITS ARE (M/SEC)**2

| LINE | REXL | REYL | RFXZ**2 | RFY7 | REXX | PEYZ**2 | REYZ | RFVY |
|------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1 | .050926 | .050926 | .02468 | .02468 | .370370 | .001971 | .001971 | .370170 |
| 2 | .002037 | .002037 | .000190 | .003044 | .146502 | .000118 | .000685 | .146502 |
| 3 | .000412 | .000412 | .000028 | .001738 | .040858 | .000020 | .000185 | .040858 |
| 4 | .000193 | .000193 | .000077 | .002111 | .024279 | .000017 | .000083 | .024279 |
| 5 | .000091 | .000091 | .000053 | .003375 | .023330 | .000008 | .000054 | .023330 |
| 6 | .000046 | .000046 | .000054 | .001894 | .005257 | .000005 | .000017 | .005257 |
| 7 | .000020 | .000020 | .000124 | .002255 | .002941 | .000005 | .000037 | .002941 |
| 8 | .000020 | .000020 | .000090 | .002108 | .002094 | .000004 | .000039 | .002084 |
| 9 | .000020 | .000020 | .000102 | .001645 | .001226 | .000005 | .000032 | .001224 |
| 10 | .000005 | .000005 | .000118 | .001630 | .000841 | .000003 | .000024 | .000841 |
| 11 | .000000 | .000000 | .000154 | .001158 | .000400 | .000002 | .000007 | .000400 |
| 12 | .000000 | .000000 | .000225 | .001299 | .000254 | .000002 | .000007 | .000254 |
| 13 | .000000 | .000000 | .000193 | .001163 | .000174 | .000002 | .000007 | .000174 |
| 14 | .000000 | .000000 | .000252 | .000728 | .000112 | .000002 | .000001 | .000112 |
| 15 | .000000 | .000000 | .000228 | .000412 | .000083 | .000001 | .000002 | .000083 |

PROGRAM 1 INDIVIDUAL SUMS
 ASCENT RATE = 500.0 M/IN

UNITS ARE (M/SEC)**2

| LINE | REXL | REYL | PEXZ**2 | REXZ | REX | PEY2**2 | REY2 | REY |
|------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1 | .079572 | .079572 | .002468 | .002468 | .723380 | .001971 | .001971 | .723380 |
| 2 | .003183 | .003183 | .000180 | .000180 | .266137 | .000118 | .000118 | .266137 |
| 3 | .000645 | .000645 | .000028 | .000028 | .079801 | .000020 | .000020 | .079801 |
| 4 | .000286 | .000286 | .000077 | .000077 | .047419 | .000017 | .000017 | .047419 |
| 5 | .000127 | .000127 | .000053 | .000053 | .045566 | .000008 | .000008 | .045566 |
| 6 | .000072 | .000072 | .000054 | .000054 | .010268 | .000005 | .000005 | .010268 |
| 7 | .000032 | .000032 | .000124 | .000124 | .005744 | .000005 | .000005 | .005744 |
| 8 | .000032 | .000032 | .000080 | .000080 | .004070 | .000004 | .000004 | .004070 |
| 9 | .000032 | .000032 | .000102 | .000102 | .002394 | .000005 | .000005 | .002394 |
| 10 | .000008 | .000008 | .000118 | .000118 | .001682 | .000003 | .000003 | .001682 |
| 11 | .000000 | .000000 | .000154 | .000158 | .000781 | .000002 | .000002 | .000781 |
| 12 | .000000 | .000000 | .000225 | .001299 | .000497 | .000002 | .000002 | .000497 |
| 13 | .000000 | .000000 | .000193 | .001163 | .000340 | .000002 | .000002 | .000340 |
| 14 | .000000 | .000000 | .000252 | .000728 | .000219 | .000002 | .000002 | .000219 |
| 15 | .000000 | .000000 | .000228 | .000412 | .000162 | .000001 | .000001 | .000162 |

PROBLEM 1

VARIANCE IN COMPONENTS

| LINE | 300.0 | | | 400.0 | | | 500.0 | | |
|------|--------------------------------|---------------------------------|---------------------------------|--------------------------------|---------------------------------|---------------------------------|--------------------------------|---------------------------------|---------------------------------|
| | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | EAST VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 | NORTH VARIANCE (M/SEC)**2 |
| 1 | .18983 | .18484 | .42423 | .42423 | .42424 | .42424 | .80789 | .80789 | .80889 |
| 2 | .06418 | .06395 | .15176 | .15176 | .14954 | .14954 | .29254 | .29254 | .29032 |
| 3 | .01923 | .01767 | .04304 | .04304 | .04148 | .04148 | .08221 | .08221 | .08065 |
| 4 | .01253 | .01045 | .02665 | .02665 | .02454 | .02454 | .04989 | .04989 | .04780 |
| 5 | .01332 | .00995 | .02654 | .02654 | .02347 | .02347 | .04912 | .04912 | .04576 |
| 6 | .00419 | .00227 | .00725 | .00725 | .00533 | .00533 | .01229 | .01229 | .01036 |
| 7 | .00363 | .00129 | .00534 | .00534 | .00300 | .00300 | .00815 | .00815 | .00582 |
| 8 | .00304 | .00093 | .00429 | .00429 | .00215 | .00215 | .00429 | .00429 | .00414 |
| 9 | .00227 | .00056 | .00299 | .00299 | .00128 | .00128 | .00417 | .00417 | .00246 |
| 10 | .00211 | .00039 | .00261 | .00261 | .00089 | .00089 | .00344 | .00344 | .00172 |
| 11 | .00168 | .00018 | .00171 | .00171 | .00041 | .00041 | .00209 | .00209 | .00079 |
| 12 | .00163 | .00012 | .00178 | .00178 | .00026 | .00026 | .00202 | .00202 | .00051 |
| 13 | .00143 | .00008 | .00153 | .00153 | .00018 | .00018 | .00170 | .00170 | .00035 |
| 14 | .00103 | .00005 | .00109 | .00109 | .00011 | .00011 | .00120 | .00120 | .00022 |
| 15 | .00068 | .00004 | .00072 | .00072 | .00000 | .00000 | .00080 | .00080 | .00017 |

PROBLEM 1

COMPONENT VELOCITY VARIANCE

| LINE | 300.0 | | | 400.0 | | | 500.0 | | |
|------|-----------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------------------|--|
| | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | VARIANCE (KNOT**2) | STANDARD DEVIATION (KNOT) | |
| 1 | .7145 | .84525 | 1.6050 | 1.2678 | 3.04667 | 1.74547 | | | |
| 2 | .24552 | .49550 | .56848 | .75398 | 1.09972 | 1.04867 | | | |
| 3 | .06964 | .26369 | .15945 | .39931 | .30728 | .55433 | | | |
| 4 | .04336 | .20822 | .09662 | .31084 | .18433 | .42934 | | | |
| 5 | .04390 | .20951 | .09493 | .30810 | .17901 | .42309 | | | |
| 6 | .01218 | .11038 | .02373 | .15404 | .04273 | .20672 | | | |
| 7 | .00929 | .09640 | .01574 | .12547 | .02636 | .16236 | | | |
| 8 | .00757 | .08701 | .01215 | .11023 | .01969 | .14031 | | | |
| 9 | .00536 | .07320 | .00807 | .08981 | .01252 | .11187 | | | |
| 10 | .00473 | .06878 | .00662 | .08135 | .00972 | .09861 | | | |
| 11 | .00313 | .05593 | .00400 | .06325 | .00544 | .07375 | | | |
| 12 | .00330 | .05743 | .00385 | .06207 | .00477 | .06904 | | | |
| 13 | .00285 | .05340 | .00323 | .05685 | .00386 | .06210 | | | |
| 14 | .00203 | .04509 | .00228 | .04772 | .00268 | .05177 | | | |
| 15 | .00135 | .03668 | .00153 | .03908 | .00183 | .04273 | | | |

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