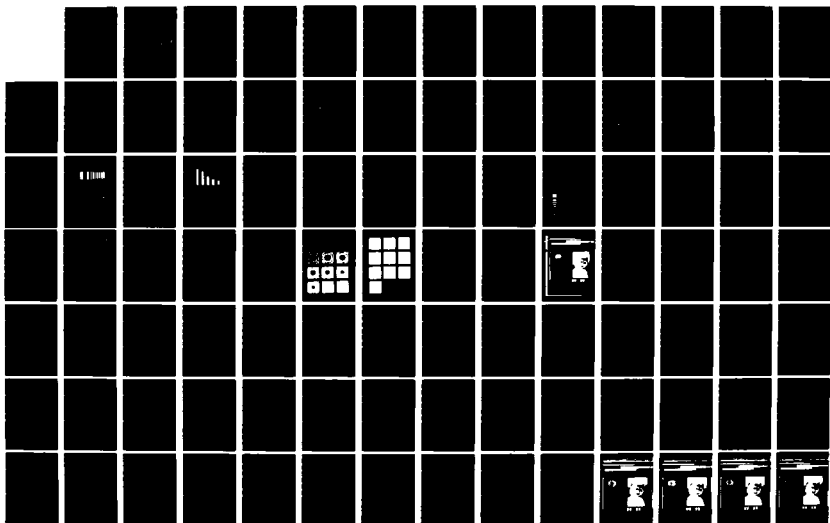


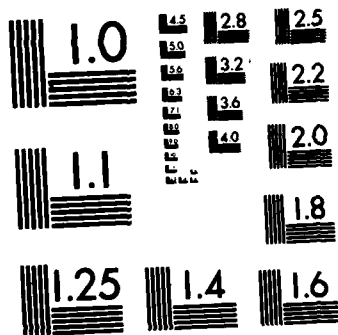
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AUTOMATIC THRESHOLD DESIGN FOR A
BOUND DOCUMENT SCANNER

by

BILL JAMES STANTON, JR

Captain, United States Air Force

Submitted to the Department of Electrical Engineering
and Computer Science August 1982 in partial
fulfillment of the requirements for the
Degree of Master of Science in
Electrical Engineering

ABSTRACT

Research was carried out on an electro-optical bound document scanner using a charge-coupled device (CCD) as a sensing element. The goal was to develop a means whereby the voltage threshold level of the video analog-to-digital converter could be set automatically to provide optimum hard-copy output over a range of lighting conditions and document background colors and qualities. To determine an acceptable component of the analog video signal as a thresholding reference, an extensive study of the signal behavior was conducted over a variety of conditions.

An Automatic Threshold Control (ATC) was designed that exploited the modulation transfer function of the CCD's analog signal. A CALIBRATION PATTERN is superimposed at the left-hand margin of the page being scanned. This pattern contains various discrete spatial frequencies. The threshold voltage is varied automatically until the number of black/white (zero/one) transitions is maximized for the CALIBRATION PATTERN. The threshold voltage producing this maximum number of transitions is equivalent to the threshold required to produce optimum resolution in the scanner hard-copy output. This threshold value is then locked in for the duration of the page being scanned.

System performance using this ATC scheme is excellent. The scanner selects a threshold voltage on a per-page basis that yields acceptable copies. The ATC is able to automatically compensate for various types of paper and changes in lighting conditions due to fluorescent tube deterioration. Slightly less than optimum thresholding may occur about 10 to 15 percent of the time, but this is due to data uncertainty and other shortcomings in the scanner rather than in the ATC scheme. (Page count: 224)

Thesis Supervisor: Dr. J. F. Reintjes
Title: Professor Emeritus, Electrical Engineering



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AUTOMATIC THRESHOLD DESIGN FOR A BOUND DOCUMENT SCANNER

by

BILL JAMES STANTON, Jr

Captain, United States Air Force

S. B., United States Air Force Academy
Electrical Engineering (1973)

Submitted to the Department of Electrical
Engineering and Computer Science
in Partial Fulfillment for
the Degree of

MASTER OF SCIENCE IN

ELECTRICAL ENGINEERING

at the

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J. F. Reintjes, Thesis Supervisor

Accepted by


Chairman, Departmental Graduate Committee

To Donna, Spencer, and Stuart

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BIOGRAPHICAL NOTE

B. J. Stanton, a Captain in the U. S. Air Force, is a distinguished graduate of the U. S. Air Force Academy, Class of 1973. As an undergraduate, his work included research in the security of defense communications systems. He completed Undergraduate Pilot Training with top honors in 1974 and Advanced Fighter Training in 1975. He served as an F4D Aircraft Commander and Wing Weapons and Tactics Officer at Royal Air Force Base Woodbridge, England from 1975 to 1978. During that time he participated in joint NATO Force exercises and taught laser weapon tactics. From 1978 to 1981 he served as an AT-38B fighter instructor pilot and academic instructor. His duties included aerial instruction in basic and advanced fighter maneuvers, surface attack tactics, low-level ingress techniques, and various tactical formations. Additionally, he was responsible for significant phases of the surface attack academic curriculum. He is an experienced fighter pilot with 1125 hours of flying time.

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SYMBOLS AND ABBREVIATIONS

AC	Alternating Current
ATC	Automatic Threshold Control
CALIBRATION PATTERN	Series of black and white line-pairs of varying thicknesses used to generate a specific analog video waveform for threshold-setting purposes
CCD	Charge Coupled Device
DC	Direct Current
ECP	Experimental Calibration Pattern
EOPS	Electro-Optical Page Scanner; also the mnemonic used to describe the complete F8 software package for the scanner
F8	Designation of the microprocessor used with the scanner for various control functions; complete nomenclature is: Fairchild F8 Formulator
ISE	Image Sensing Element
MTC	Maximum value of VTC obtained from scanning a particular Calibration Pattern
N	Decimal equivalent of the value supplied by the F8 to the Threshold Level Generator to produce a specific threshold voltage
Np	Value of N generating the maximum value of VTC in a given series of samples
Pass	The act of taking seven samples of VTC at N-values that are separated by a fixed step size
Pel Swing	Positive difference between the black and white voltage levels in the analog video signal

Symbols and Abbreviations

QSET	Mnemonic used for the algorithm that picks the optimum threshold value by taking four sets of seven samples per set with each set using a progressively smaller sampling increment of N
R	Reduced range of N-values that have been defined from the results of the previous pass of the algorithm QSET; the reduced range R is that range sampled on the next pass of QSET
RV	Span of values of N producing significant VTC values (where significant is defined as $VTC > 1$)
S1	Step size used to increment the value of N while taking VTC samples in the first pass of the algorithm QSET; subsequent passes use step sizes labeled in sequence: S2, S3, S4
TLG	Threshold Level Generator
Vref	Output of op amp U3 of the Threshold Level Generator; used as the reference voltage for the 10-bit D-to-A converter
V2	Output of op amp U2 of the Threshold Level Generator; represents the inverted fraction of V2 as determined by the quotient $(N/1024)$
V0	Voltage output of the Threshold Level Generator
VTC	Video Transition Count: the sum of digitized video black/white transitions encountered in one scan line for a given threshold value

CHAPTER 1

INTRODUCTION

A. PROBLEM STATEMENT

The goal of this research was to refine an existing electro-optical bound document scanner under development in the Laboratory for Information and Decision Systems by reducing the need for manual adjustments. Specifically this involved designing and incorporating a means of automatically setting the voltage threshold level of the video one-bit analog-to-digital converter at a value that would provide optimum quality in the reproduced copy. The subsystem accomplishing this task will be referred to as an Automatic Threshold Control, or ATC in this report. A further objective of the ATC was to provide the scanner with the capacity for automatically compensating for paper color and/or quality and for variations in illumination.

B. PROJECT BACKGROUND

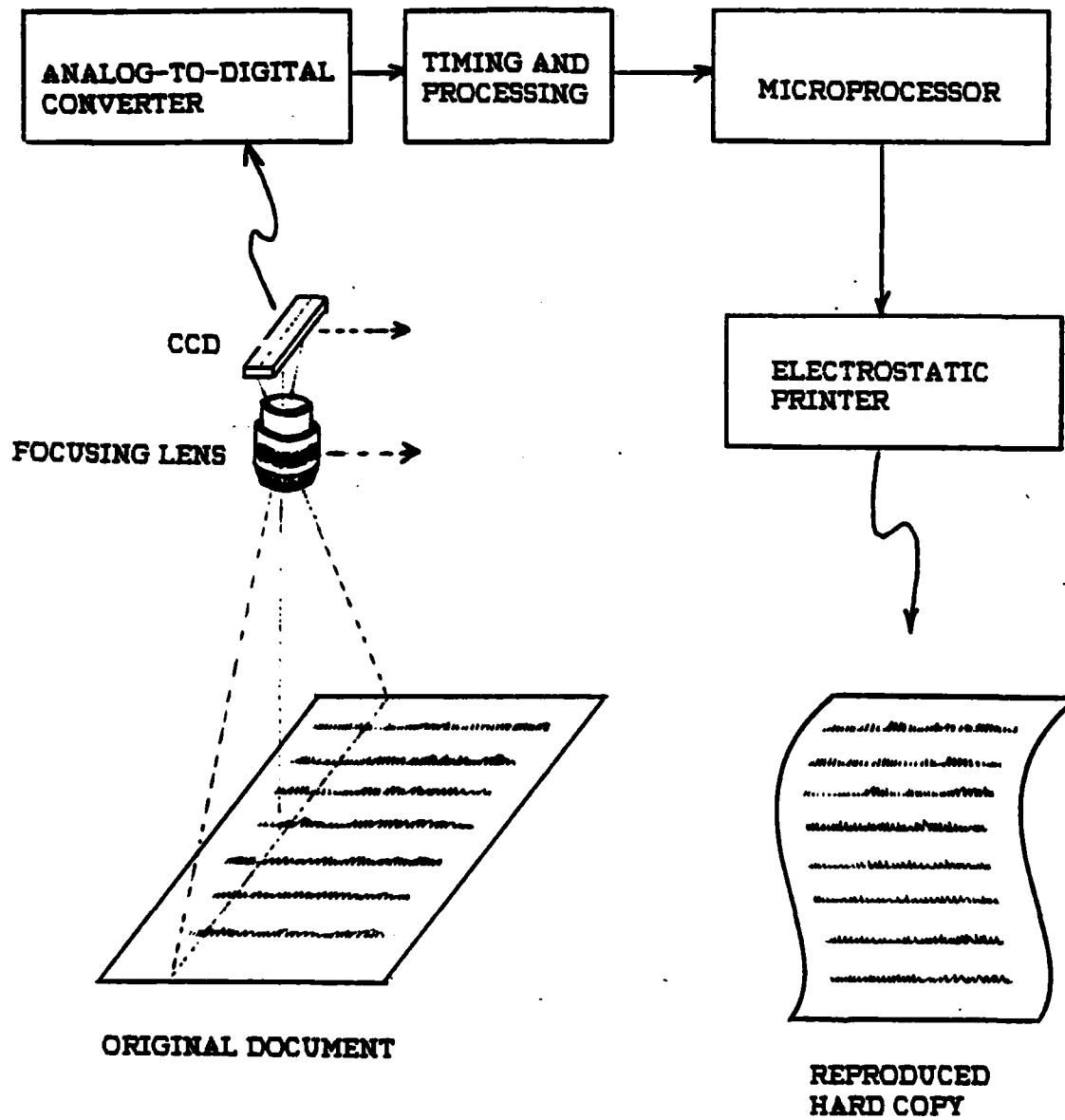
The immediate thrust behind the development of a bound document scanner at the Laboratory for Information and Decision Systems is to improve the interlibrary resource sharing process which now works on a "lending-borrowing" principle. The requirement to physically move either originals or copies from one geographic location to another can take up to two to four weeks from the initial request. On the other hand, the ability to electronically move hard copy material economically would essentially reduce turn-around time to only that required to process the request, locate the document, and transmit the

specified pages. Conceivably, turn-around time could be reduced to less than a day, and in many cases less than one hour. In addition, the follow-on applications of such a system in commercial, industrial, and military areas could result in significant increases in efficiency of information management.

The principle of the bound document scanner to which the ATC will be applied is to convert the information content of an 8.5 x 11 inch printed page into 3.6 megabits of digital information through line-by-line scanning. The digital signal can then be compressed for transmission on a 56 kilobit/second data line, such a line representing a tradeoff between transmission cost and per-page transmission time. Copy is produced at the destination by an electrostatic printer.

In the laboratory, scanning is accomplished by a system that uses a Fairchild Charge Coupled Device (CCD) to convert light to analog electrical signals. The CCD consists of a linear array of 2048 image sensing elements (ISEs). The output of each element is proportional to the intensity of light and integration time allowed. One "line" of information is obtained in parallel form and then shifted out of the CCD serially for subsequent processing. The CCD, light source, and focusing lens are mounted on a common structure and physically moved in the second dimension by a phase-locked loop DC motor to provide a raster scan of the entire page.

Several theses have been written concerning the bound document scanner either directly or indirectly. They are listed



SIMPLIFIED BLOCK DIAGRAM OF THE BOUND DOCUMENT SCANNER

FIGURE 1.1

in Chapter 7, but they also deserve mentioning now for those interested in more extensive background review. Aghamohammadi conducted the original design and fabrication of the bound document scanner. If a working knowledge of the scanner is required, his thesis should be read and thoroughly understood before proceeding. Keverian, while primarily concerned with a parallel project on microfiche scanning, developed hardware interfaces with the F8 microprocessor available in the laboratory. These interfaces are used in the bound document scanner system. Agudelo worked on a document cradle, light non-uniformity, and other problems associated with the existing scanner. Medley accomplished extensive software and hardware modifications to the F8 microprocessor independent of any other projects supported by the F8. His thesis should be reviewed when information concerning current operation of the F8 is required. Vinciguerra studied the feasibility of various data compression schemes for application to document transmission, and Dishop followed this work with further evaluation and design.

C. RESEARCH PLAN

The first phase of this research consisted of analyzing the analog video signal behavior with respect to various light conditions, paper reflectivities, and spatial frequency excitation. The objective was to pinpoint critical variables that would be suitable for obtaining a proper threshold relation. In the second phase, a subsystem was designed and built that would sense the video signal variable and control the voltage

threshold level according to the performance of this variable. Finally, the system was evaluated with different lighting conditions, paper colors, and spatial frequency patterns to determine its feasibility.

D. SUMMARY OF RESULTS

An ATC was designed that exploited the modulation transfer function of the CCD as a means for selecting an optimum voltage threshold level. A CALIBRATION PATTERN consisting of several sets of parallel lines is superimposed at the left-hand margin of the page being scanned. This pattern contains various discrete spatial frequencies. The threshold voltage is varied automatically until the number of black/white transitions is maximized for the CALIBRATION PATTERN. The threshold voltage producing this maximum number of transitions is then locked in for the duration of the page being scanned.

System performance using this ATC scheme has been excellent. The scanner now selects a threshold voltage on a per-page basis that yields acceptable copies. The ATC is able to automatically compensate for various types of paper and changes in lighting conditions due to fluorescent tube deterioration. Thresholding errors occur about 10 to 15 percent of the time, but they are due to other shortcomings in the scanner rather than in the ATC scheme. When threshold errors do not occur, the threshold chosen is the best that can be obtained.

E. PREVIEW OF DISCUSSION

Chapter 2 presents an analysis of the analog video waveforms that are derived from the CCD under operational conditions. The results of this analysis are used to develop a conceptual approach to automatic threshold control. Chapter 3 discusses the evaluation of various experimental CALIBRATION PATTERNS to determine the characteristics necessary to produce the desired analog video waveform for thresholding purposes. A practical implementation of the ATC is developed in Chapter 4, together with considerations that led to the implementation. Chapter 5 contains the development of sampling algorithms that allow the thresholding process to be accomplished in minimum time along with the incorporation of these algorithms into the existing scanner software. Finally the results, conclusions, and recommendations for further research are detailed in Chapter 6.

CHAPTER 2

ANALOG VIDEO SIGNAL ANALYSIS

A. OBJECTIVE

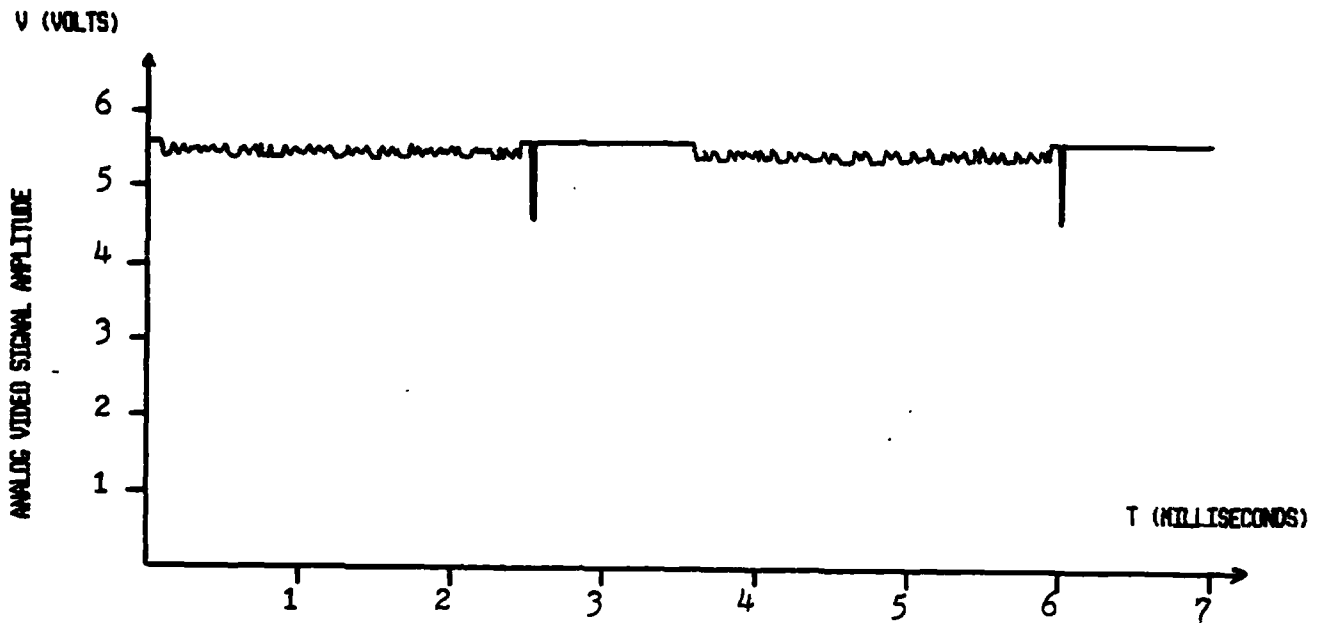
A thorough analysis of the analog video signal derived from the CCD during the line-scanning process was conducted to classify its components and learn its behavior under different conditions. The purpose was to develop a sound basis for selecting a parameter of this signal for use in controlling the voltage threshold level of the A-to-D converter. Ultimately, the analog video signal is dependent on the amount of light reaching the individual image sensing elements (ISEs) of the CCD. Many factors affect the amount of light that the CCD sees, but the relevant factors are those that normally occur in a "user environment", rather than abnormal conditions that could be induced in a "laboratory environment". The factors researched were:

1. Intensity of the light source (1)
2. Color content of the document
3. Spatial-frequency content of the document

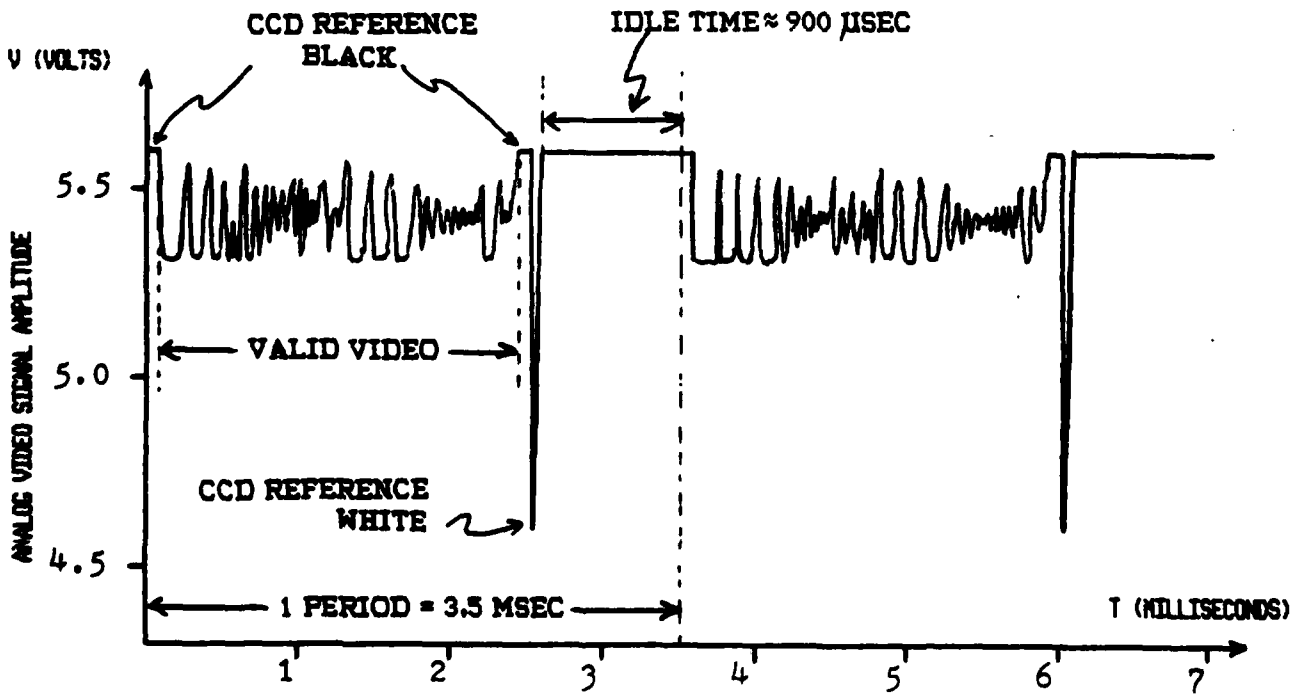
B. FINDINGS

The general configuration of the analog video signal will first be described with reference to Figure 2.1 and the CCD142 data in Appendix A. One period of the signal is equivalent to

(1) Note that the distance between the document and the CCD also affects the amount of light reaching the ISEs. This fact, due to the optics and the geometry of the scanner, gives rise to a light non-uniformity issue which was addressed by Agudelo. Additional information on this subject is included in Chapter 6.



(A) TWO PERIODS OF THE CCD ANALOG VIDEO SIGNAL



(B) EXPANDED SCALE OF AC COMPONENT

FIGURE 2.1

Ch 2

one line of video information. In turn, the period is controlled by the signal, EXTERNAL EXPOSURE (1) which initiates the dump of data from the CCD. The CCD analog data stream for one line is in the following order: black reference level, valid video, black reference level, and white reference level. Once the CCD data dump is complete, there are almost 900 microseconds of idle time to allow for microprocessor command functions. In terms of magnitude, the video information is contained in an AC component obtained by subtracting the instantaneous total analog voltage from a fixed DC component of 5.6 volts. The maximum voltage of 5.6 volts represents absolute black, and negative departures from this maximum result from various light levels absorbed by the CCD ISEs. The CCD typically saturates at 1400 millivolts below absolute black, and the fluorescent lights used as the illumination source provide ample output to drive the CCD to saturation. But in the current design, the focusing lens f-stop is set at 5.6 for depth-of-field considerations. This resulted in the largest white levels observed being 200 to 300 millivolts below black, depending on the condition of the lights. In other words, the existing combination of illumination source and f-stop setting drives the CCD at 14 to 21 percent of its capacity. Valid video information therefore was found in the extreme to reside in the range 5.3 to 5.6 volts and more commonly in the range 5.4 to 5.6 volts. The major issue of setting the proper

(1) Reference Aghamohammadi, Chapter 6 and TIMING AND PROCESSING circuit, Appendix E.

Ch 2

threshold level is finding the value of voltage that is LESS THAN all black voltage values and GREATER THAN all white voltage values. For this purpose, it is important to understand how the black and white video levels react to the factors listed above. First, however, it will be convenient to introduce the term "pel swing," defined as the magnitude of the DIFFERENCE between black and white voltage levels in the video signal. Pel swing is normally measured in millivolts and provides a convenient quantity for expressing the analog signal behavior.

That light intensity has a predictable effect on pel swing was easily demonstrated by varying the f-stop of the focusing lens. A blank piece of white paper was scanned with soft white fluorescent lights providing illumination. Pel swing was measured from absolute black (5.6 volts) to the maximum deviation from absolute black. The results are illustrated in Figure 2.2. Note that f-stops of 2.8 and below saturate the CCD.

The background color of the document being scanned is also an important parameter because in a user environment the scanner will certainly encounter different qualities and textures of white paper and, less commonly, a variety of paper colors. CCD response to paper color and texture at a fixed f-stop of 5.6 was measured experimentally by scanning a blank piece of construction paper of a uniform color and recording the pel swing from absolute black to the maximum deviation. Again, soft white fluorescents were used. These results are shown in Figure 2.3. In a predictable fashion, white and black paper yield the two

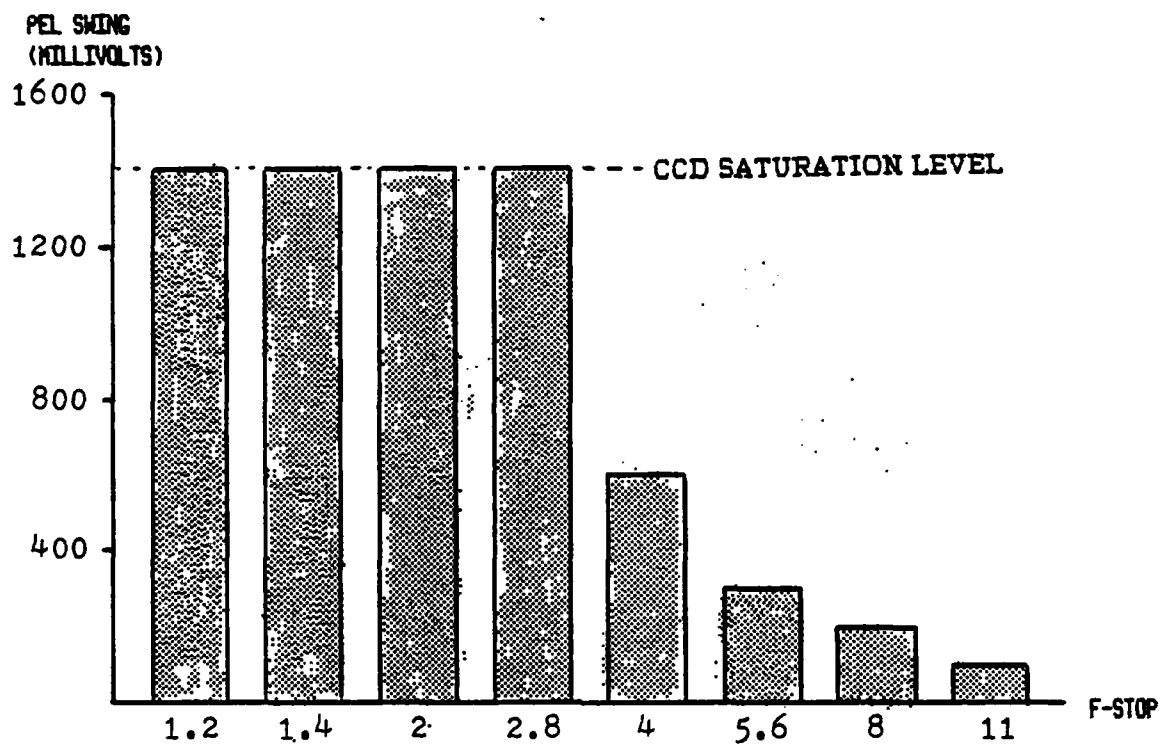


FIGURE 2.2 PEL SWING VERSUS LIGHT INTENSITY AS CONTROLLED BY THE FOCUSING LENS F-STOP

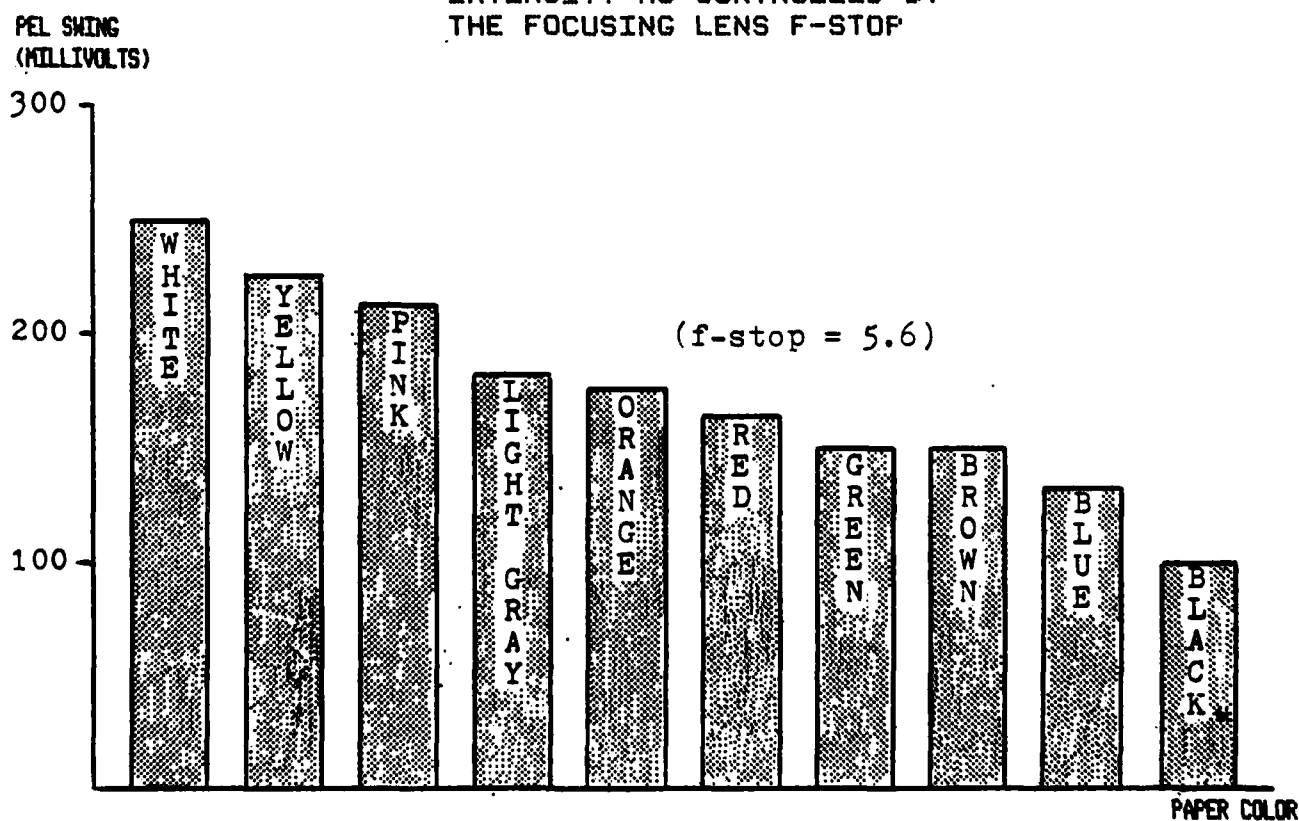


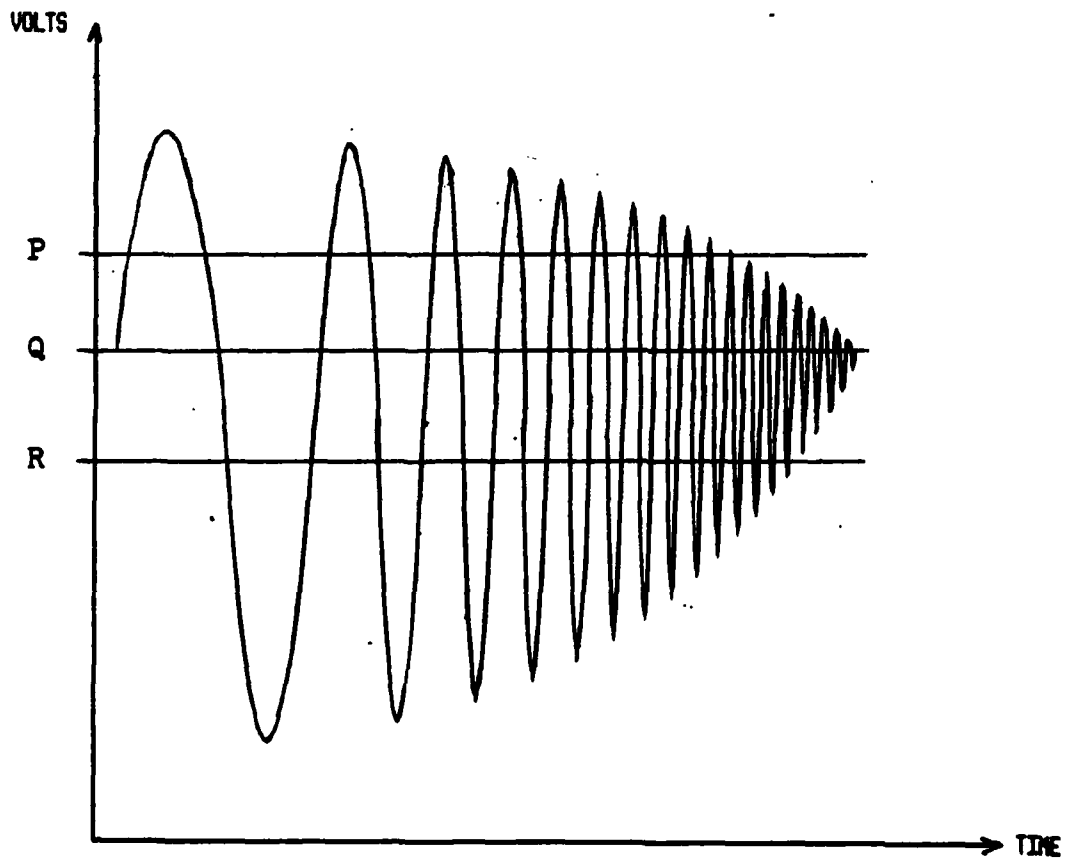
FIGURE 2.3 PEL SWING VERSUS PAPER COLOR

extremes in the range of pel swings. But from a more critical standpoint, one would expect the resulting analog signal from scanning black paper to be very close to absolute black, that is, to yield a very small pel swing. However, this experiment revealed considerable pel swing with black paper. The cause was traced to stray light "leaking" to the CCD ISEs due to a design deficiency in the scanner's optical path. This problem is covered in Chapter 6.

The behavior of the video signal with respect to spatial-frequency content of the information contained on a page is a more complicated issue. As stated above, pel swing has been measured between absolute black and the maximum white level generated by the CCD under blank, monochromatic paper conditions (zero spatial frequency). But with increases in spatial frequency information on the page resulting from alternating black and white lines, signals corresponding to the black level migrate downward away from absolute black, while signals corresponding to the white level migrate upward although not at the same rate. Figure 2.4 illustrates this behavior by showing the CCD response to a series of black lines and white spaces that represent increasing spatial frequency. This phenomenon is due to "crosstalk" between ISEs in the form of hole-electron spillovers. In other words, when one ISE is excited while an adjacent ISE is not excited, there tends to be a certain amount of charge transfer between the two ISEs. The result is less signal output from the principal ISE and a small signal output from adjacent



(A) SERIES OF LINES AND SPACES REPRESENTING INCREASING SPATIAL FREQUENCY



(B) ANALOG VIDEO SIGNAL RESULTING FROM SCANNING LINES IN (A)

FIGURE 2.4

ISEs, and this is exhibited in the modulation transfer function discussed in Appendix A. For the CCD142 in this particular application, a spatial frequency of 100, equivalent to a resolution of 200 lines on the scanned document, will produce the Nyquist rate at the face of the CCD. The Nyquist rate is defined as the spatial frequency that will excite every other ISE in the CCD's linear array. Hence, it is the maximum spatial frequency the CCD is physically capable of resolving. Experimental measurements of pel swing versus spatial frequency are displayed in Figure 2.5. The measurements of black and white level migrations as a function of spatial frequency are presented in Figure 2.6. It is important to understand the relationship among Figures 2.4 to 2.6. First observe the fact that the curves in Figure 2.6 exactly form the envelope of the waveform of Figure 2.4. (1) Also note in Figure 2.6 that the vertical distance between the two curves at a particular spatial frequency is precisely the pel swing generated by that spatial frequency as pictured in Figure 2.5.

The results presented thus far are correct in showing the general trend of analog signal behavior, but the data have limited accuracy for a number of reasons. One reason already cited is the stray light leakage which has the effect of inducing unwanted bias signals. Another reason is the fact that the analog signal contains 30 to 50 millivolts of clocking noise

(1) The apparent curving envelope in Figure 2.4 is due to a scaling factor in the computer generation of the waveform.

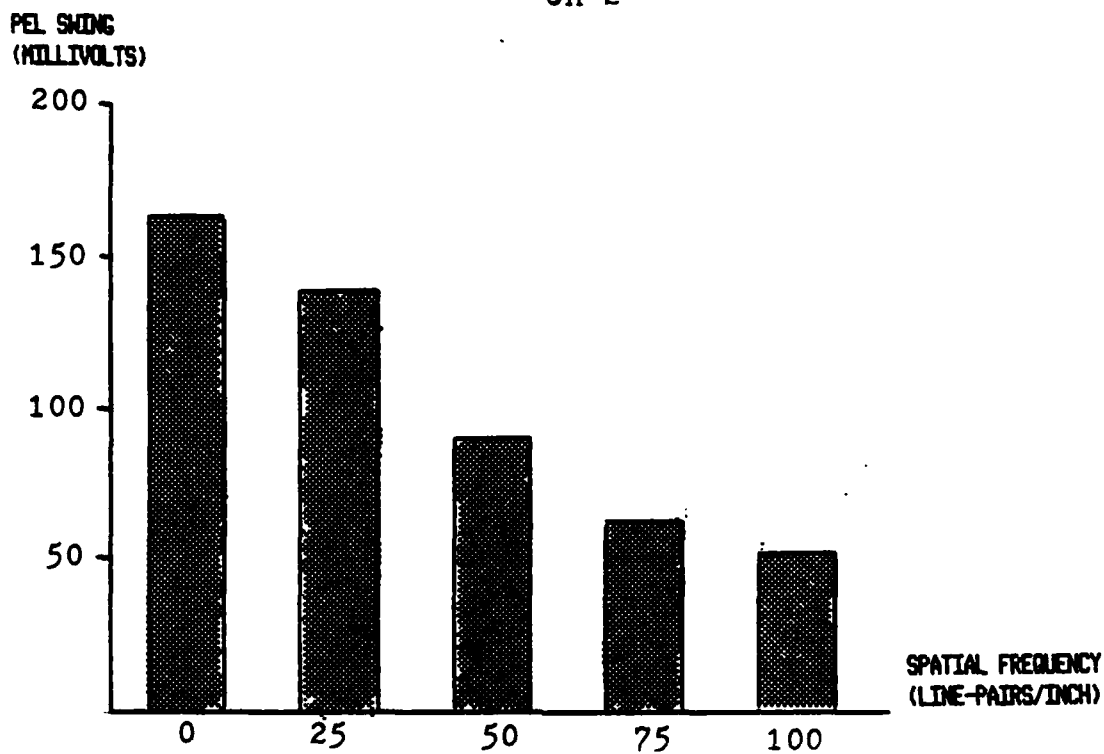


FIGURE 2.5 PEL SWING VERSUS SPATIAL FREQUENCY

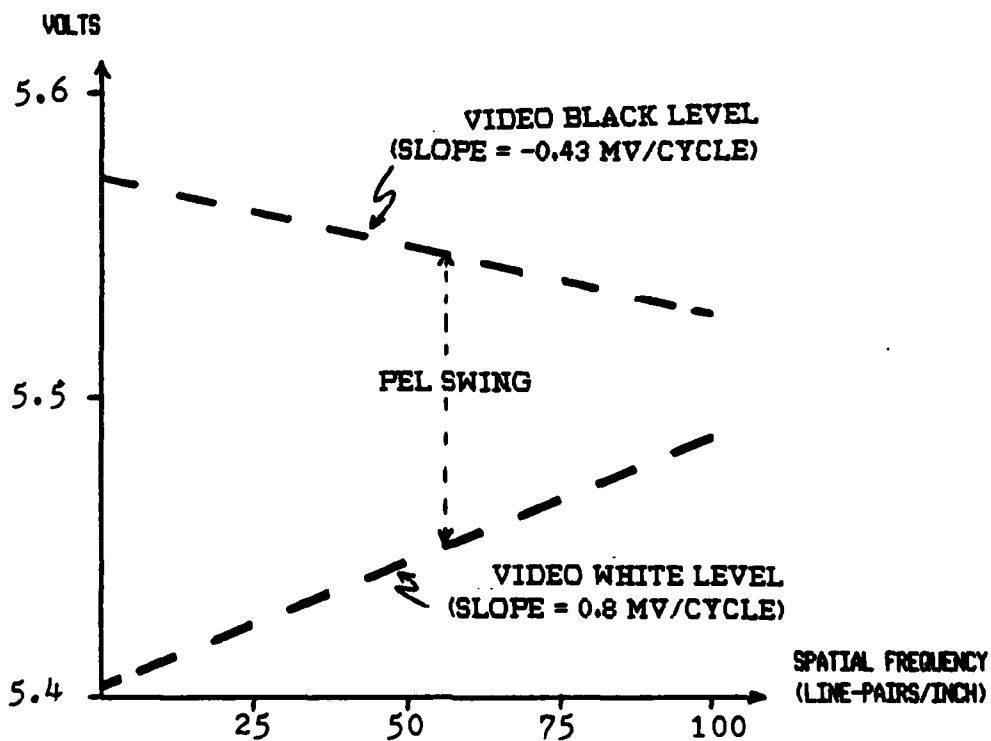


FIGURE 2.6 BLACK AND WHITE ANALOG VIDEO LEVELS VERSUS SPATIAL FREQUENCY

which makes precise measurements extremely difficult to obtain. A third reason stems from the deterioration of fluorescent lights with time, causing slightly different light levels from day to day. Despite these uncertainties, however, adequate information had been obtained at this point to proceed with the ATC design.

C. CHOICE OF PARAMETER FOR THRESHOLD CONTROL

Recall from Chapter 1 that the threshold value being sought is that which will enable the scanner to give the highest quality output possible. Output quality can be measured by "resolution" or the ability to resolve a set of alternating black and white lines of equal width. The more lines/unit length of the ensemble the scanner can resolve, the better will be the quality of the output. Resolution, in turn, is directly related to spatial frequency. Therefore, it can be said that the desired threshold level is one that will digitize all spatial frequencies represented in the analog video signal thereby producing the highest resolution in the output. With the goal now defined as preserving all spatial frequencies as the video signal is digitized, it is logical to exploit the analog video-signal behavior with respect to spatial frequency as the parameter for controlling the threshold. The concept is more easily understood by the following example.

Referring back to Figure 2.4, if one were required to select a threshold voltage that would permit proper digitization of all alternations between black and white, one should choose voltage-level Q as the correct value. Other threshold levels

such as P or R would cause loss of the higher spatial-frequency information in the A-to-D conversion process. This leads to a simple algorithm for selecting the optimum threshold, using the particular analog signal of Figure 2.4:

1. Vary the A-to-D threshold voltage through an appropriate range of discrete values.
2. Count the number of zero/one (black/white) transitions at each discrete threshold value.
3. Select the threshold value that resulted in the maximum number of black/white transitions.

It is important to highlight the fact that, for threshold-setting purposes, use of an analog video signal containing linearly increasing spatial frequencies is fundamental to the success of the algorithm. A signal such as this must be obtained by scanning a CALIBRATION PATTERN such as that shown in Figure 2.4(A). Issues concerning choice of a CALIBRATION PATTERN will be discussed in Chapter 3.

D. PARAMETERS REJECTED FOR THRESHOLD CONTROL

Other options that were considered but not chosen for threshold control include:

1. Video white and black levels
2. CCD reference white and black levels
3. Combinations of the above

Use of one of the above parameters would have been in the context of a real-time threshold control scheme; that is, one that would have continuously modified the threshold level based on incoming video information. In general, controlling the threshold level by direct reference to a particular voltage value of the time-varying video signal was explored but rejected due to the

complexity involved in extracting the required information from the video signal. The clocking noise in the video signal, relatively long durations of white signal, and the migration of the white and black signal levels toward each other as the spatial frequency of the textual patterns increases, all complicate the task of pinpointing a particular level of video signal. Further complexities arise in selecting a video level or combination of video levels that would provide a stable reference for selecting an optimum threshold value. A relatively simple method of detecting both peak white and black levels of the time-varying video signals and then averaging the two for a correct threshold level was also deemed unfeasible due to the different migration rates (1) of the black and white levels, and due to the video signal normally containing substantially more white information than black information. Finally, using the CCD reference white and black levels was eliminated from consideration because these levels contained no information about light intensity, paper reflectivity, or spatial frequency content of the document.

(1) Note the absolute values of the slopes of the two curves in Figure 2.6 are different.

CHAPTER 3

CALIBRATION PATTERN EVALUATION

As implied in Chapter 2, the term CALIBRATION PATTERN will be used in this thesis to denote a series of parallel black and white lines for forcing the CCD to produce a specific analog video signal for threshold-setting purposes. The design of the ATC calls for the CALIBRATION PATTERN to be located in the left-hand margin of the document being scanned. During a normal scanning sequence, the first lines that the scanner sees would be those of the CALIBRATION PATTERN. Transmission of video information to the printer would be inhibited until the threshold-setting sequence is complete.

Optimally, the CALIBRATION PATTERN should consist of black lines on a transparent surface, thereby allowing the margin of the document being scanned to provide the background. This would permit the analog video signal to be indicative of the characteristics of the paper being scanned, and in this way the threshold setting could be based on the reflectivity and/or color of the paper. On the other hand, using the left margin of the document as the background for the CALIBRATION PATTERN implies that a certain portion of the margin will be unavailable for information content. This was not considered to be a problem since it is highly unlikely there will be a need to transmit a document having no margins. A more critical question, however, is just how much of the margin will be required to support the CALIBRATION PATTERN, or equivalently, how many lines will the ATC

require to properly select an optimum threshold level. This issue is addressed Chapter 5.

A. PERFORMANCE REQUIREMENTS

In the selection of a CALIBRATION PATTERN, certain criteria should be followed. First and foremost, the pattern should allow the ATC to select the optimum threshold level, that is, the level that produces the highest resolution in the output. Secondly, the pattern should allow the ATC to produce consistent results; that is, with all inputs constant, the ATC should generate the same threshold level again and again. Thirdly, the pattern characteristics should be invariant to light and/or paper characteristics. And finally, the pattern should be of the proper dimensions in order to fit in the margin of the document.

B. PATTERN COMPOSITION

The discussion thus far has been directed toward the fact that the CALIBRATION PATTERN would consist of a series of parallel lines, and it is easy to see why this would be a logical choice. At the very low spatial frequencies, a series of black lines separated by white spaces of equal width (called line-pairs) produces a square wave in the analog video signal. As the line-pairs become thinner, thus causing the spatial frequency to increase, the black and white analog levels migrate together, and the resulting analog video signal becomes very nearly sinusoidal and extremely predictable. The relationship, illustrated before in Figure 2.4, is re-oriented in Figure 3.1(A)

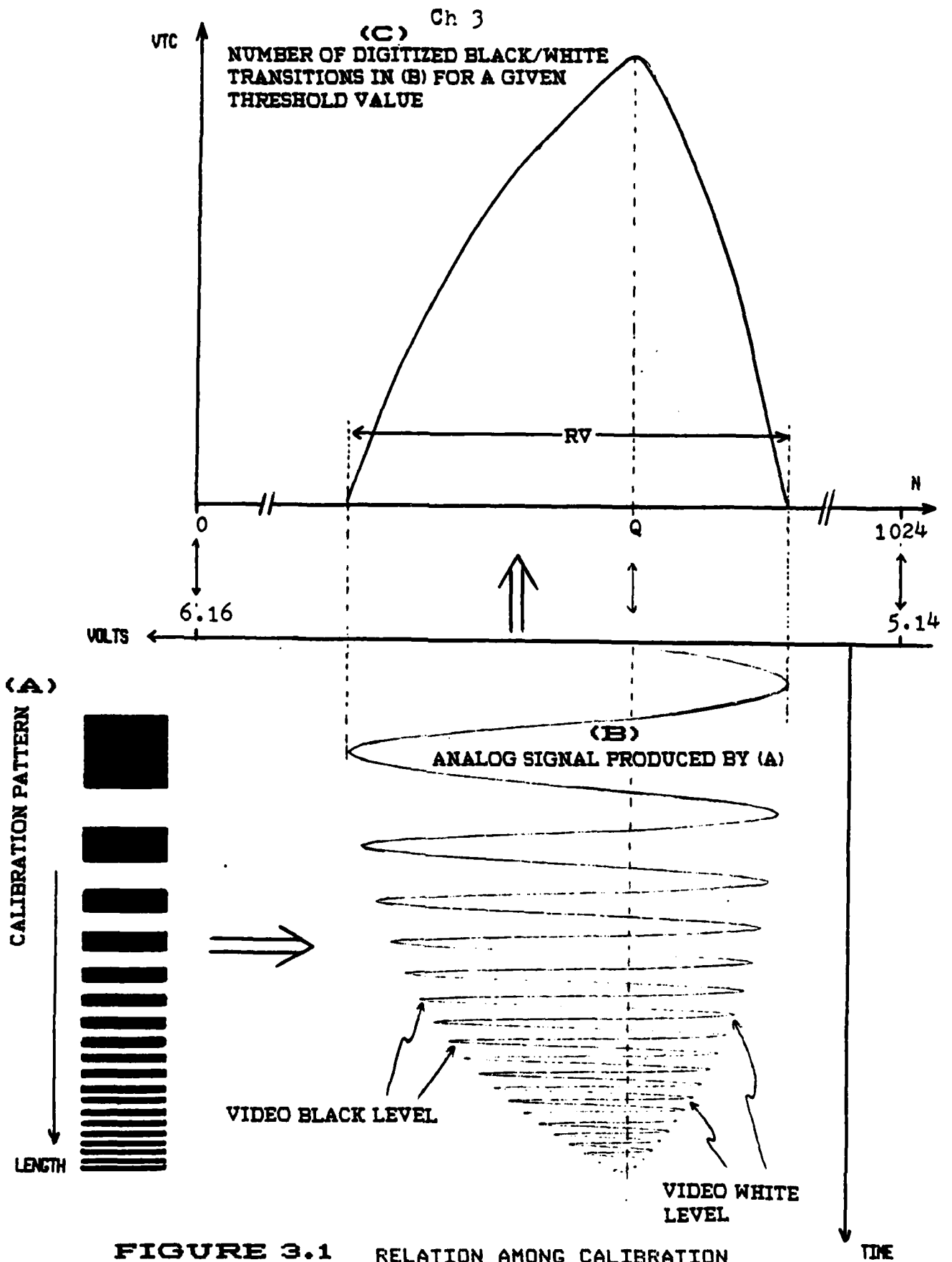


FIGURE 3.1 RELATION AMONG CALIBRATION PATTERN, ANALOG VIDEO SIGNAL, AND VTC-VERSUS-N CURVE

and (B). (1) So given that the CALIBRATION PATTERN will consist of line-pairs, the real question therefore is what spatial frequency or frequencies will be represented by the line-pairs. As mentioned in Chapter 2, the theoretical best choice would be a pattern that equally represented all spatial frequencies up to the CCD Nyquist rate of 100 line-pairs/inch. However it might also be possible that a pattern containing only the Nyquist frequency would be the best choice. It turns out that the very small pel swing generated by the Nyquist rate would be a significant disadvantage to the development of an efficient sampling algorithm. This point is covered in Chapter 5. The object of this phase of research was to ascertain the proper CALIBRATION PATTERN composition by direct evaluation of various candidate patterns. Unfortunately, within the scope of the project, there were relatively few sample patterns available for evaluation. Still much insight was gained with the patterns at hand, and a workable facsimile for a CALIBRATION PATTERN was obtained.

Another important question in CALIBRATION PATTERN composition is, in physical terms: How far along the left margin should the pattern extend? Or in other words, how much of one line of analog video does it take to successfully select the optimum threshold level? The answer, while not simple, can be illustrated fairly easily. Figure 3.2(A) shows the analog video

(1) Disregard Figure 3.1(C) for the present time.

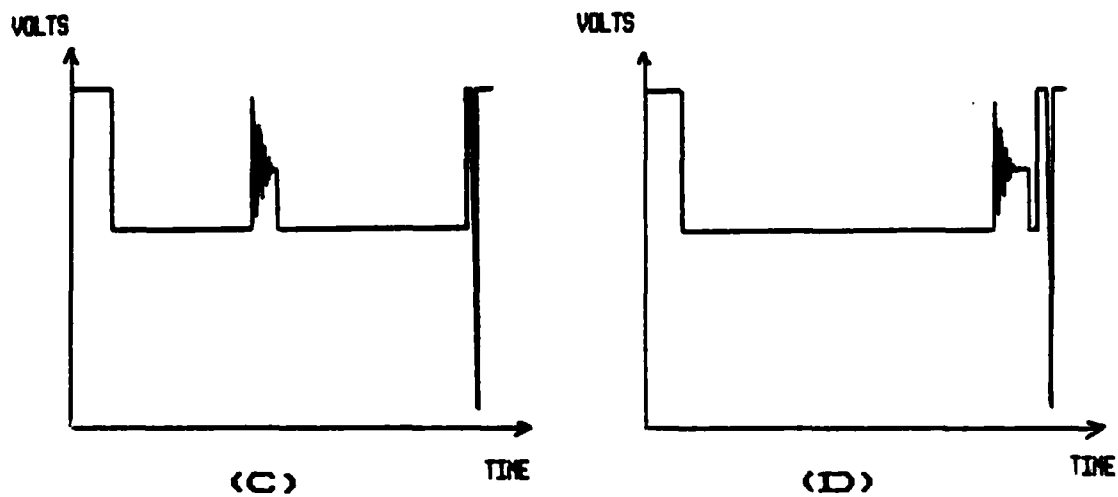
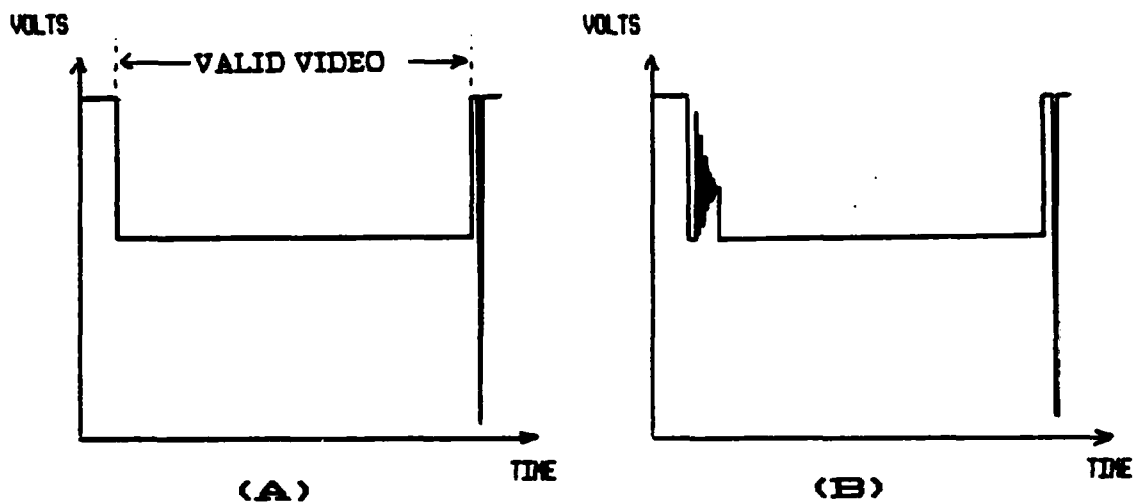


FIGURE 3.2 CALIBRATION PATTERN PLACEMENT EFFECTS ON THE ANALOG VIDEO SIGNAL

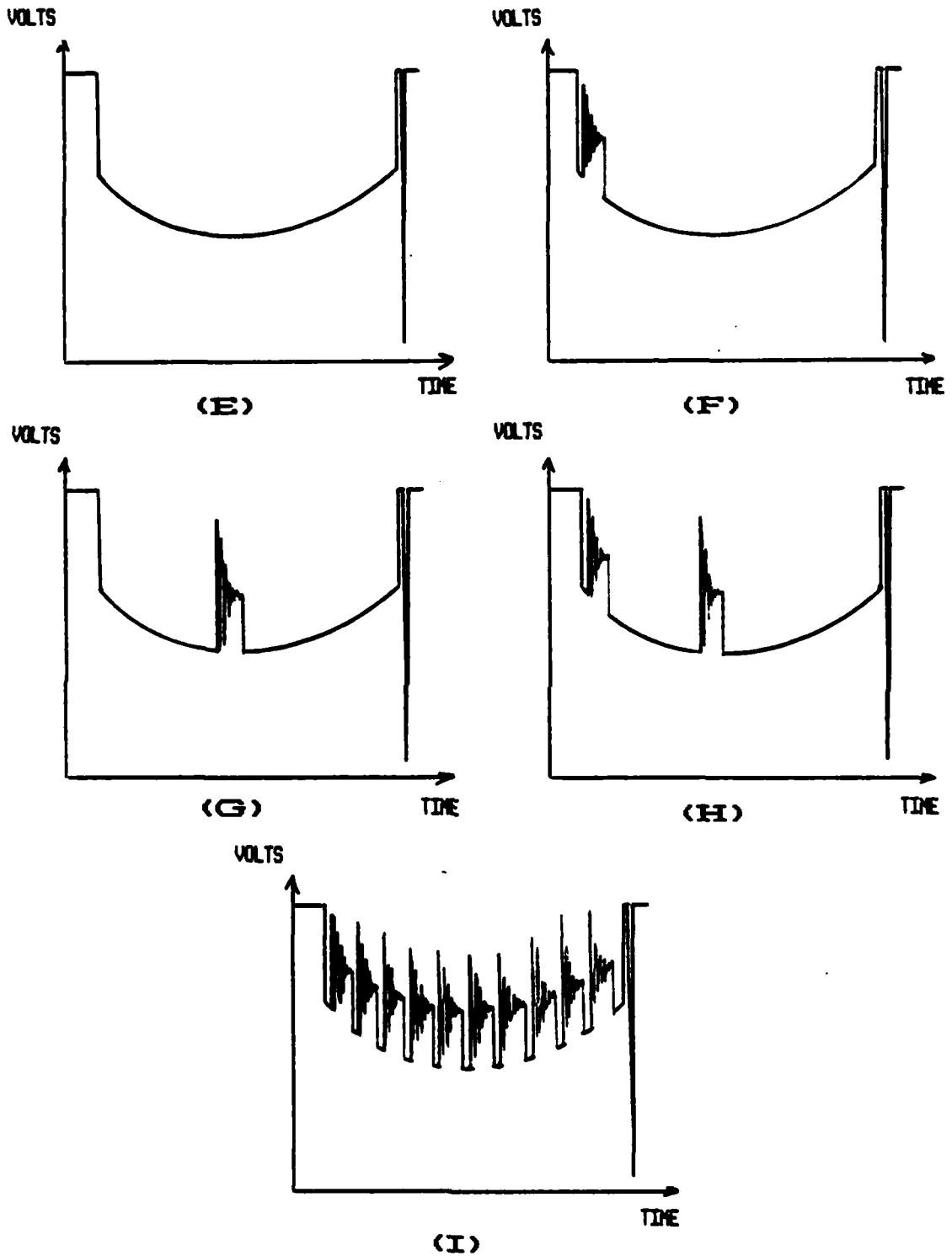


FIGURE 3.2 (CONT.)

signal resulting from scanning a blank white page with perfectly compensated illumination. Under these conditions, the CALIBRATION PATTERN that is superimposed on the white page would only need to be long enough to contain the necessary spatial frequencies, and could be located anywhere along the length of the margin. Figures 3.2(B), (C), and (D) show the analog signal that would result for pattern length of about an inch and placement in the bottom, middle, and top of the margin respectively. Now, for some reason, let us assume the illumination is not uniform over the length of the page, as illustrated in 3.2(E). The threshold level is now sensitive to pattern placement along the length of the margin as shown in 3.2(F) and (G). However, two patterns placed as in 3.2(H) would result in a threshold being chosen somewhere between the levels of 3.2(F) and (G). Realizing that this is indeed a compromise necessitated by less than optimum illumination, it is still a better choice than either extreme. Extrapolating to the limit, it would be necessary to use an entire line of video to get the best average over a line for non-uniform lighting conditions. This line corresponds to the entire left margin and should be filled with repeated CALIBRATION PATTERNS as in 3.2(I).

C. EVALUATION RESULTS

CALIBRATION PATTERN evaluation consisted of two stages: plotting the digital video transition count (VTC) versus threshold level value (N) for all possible threshold values; and running actual copies with the threshold value that yielded the

maximum video transition count (MTC). The experimental CALIBRATION PATTERNS (ECPs) evaluated were obtained from the IEEE Std 167A-1975 Facsimile Test Chart whose data are contained in Appendix A. To simplify documentation, the ECPs that were examined are labeled A through F in Figure 3.3. Referring to this figure, ECP A (IEEE Facsimile Test Pattern 9) consists of repetitions of 12 discrete spatial frequencies ranging from 30.5 to 203 line-pairs/inch. ECPs B, C, and D (IEEE Facsimile Test Patterns 5, 4, and 3) are single-frequency patterns containing 48, 25, and 5 line-pairs/inch respectively. ECP E (IEEE Facsimile Test Pattern 19) contains 0.01-inch lines spaced 0.10 inch apart. ECP F is a vertical strip of pseudo-random text taken from the IEEE Facsimile Test Chart and chosen so as to fall in the 50-to-100 line-pairs/inch region of Test Pattern 12. While none of the ECPs precisely satisfy the theoretical criterion of containing all spatial frequencies up to the Nyquist value, it can be predicted that ECP A will exhibit the best performance due to its controlled distribution of discrete spatial frequencies. ECP F was included in the testing to get an idea of the behavior of the VTC curve when scanning a relatively uncontrolled variety of spatial frequencies.

A general plot of a VTC-versus-N curve is illustrated in Figure 3.4. To fully appreciate the information presented on this and similar plots to follow, a few details deserve highlighting. Recall first that the x and y scales represent integers; each unit increase in N corresponds to a decrease of

Ch 3



A



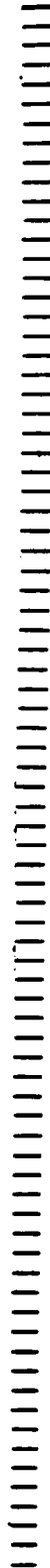
B



C



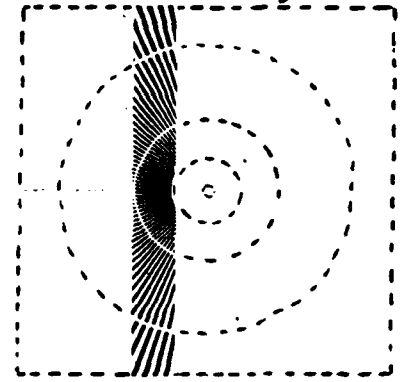
D



E



IEEE TEST
PATTERN 12



11C
Gt
9UV
FGt
'Z
'J4
'GH
cd
yz
HIJ
hij
89C
NOPO
KLMt
mnop
Spa
4UK
klmr
'O S

F GH
ijkl
89C



FIGURE 3.3

EXPERIMENTAL CALIBRATION
PATTERNS (ECP) OBTAINED
FROM IEEE FACSIMILE
TEST CHART

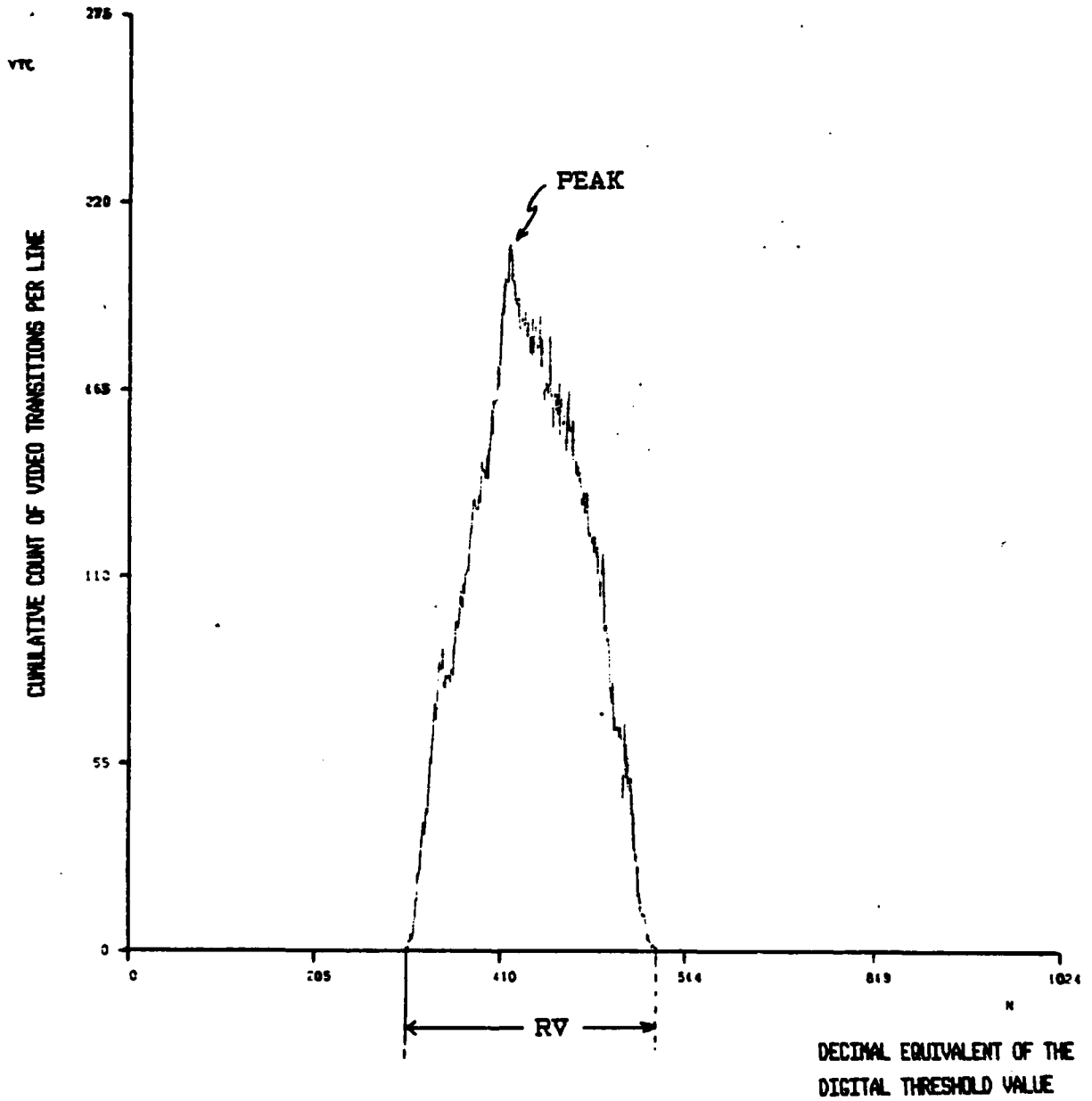


FIGURE 3.4 VTC CURVE PLOTTED OVER THE FULL RANGE OF N

one millivolt in the threshold level, and the dependent variable, VTC, is an accumulation of black/white transitions along one line of video for a given value of N. Although the full range of N is depicted, only a relatively small span contains pertinent information. Therefore, subsequent plots will constrain the N-axis to the span of significant VTC information. It should also become apparent that the span of N containing significant VTC information (subsequently called RV) is directly correlated to pel swing; larger pel swings will result in larger spans of RV, as illustrated by the relationship between parts (B) and (C) of Figure 3.1. This feature will be especially useful when comparing various plots. As for the vertical axis, VTC, it is emphasized that the absolute value, while interesting, is not nearly so significant as where along the horizontal axis the PEAK of VTC occurs. As an example, it is easy to see that ECP B in Figure 3.3 will have a much larger overall VTC than ECP D simply because it provides more black/white transitions per video line. This however does not mean that the peak of ECP B will be easier to detect. Since the idea is to work with digital information, the ATC will be equally capable of detecting a peak with a value of 800 or a peak with a value of 200. The absolute value of the peak is arbitrary. The important information is the value of N that causes the peak, because it is that value of N that the ATC should choose for its optimum threshold. One final property of these plots can best be described by referring to Figure 3.1. When N equals zero, the threshold level is at 6.16

volts, or well above the video signal. As N increases, the voltage threshold level decreases, eventually passing through the span of the analog video signal. On the basis that any portion of the analog video signal below the threshold level is decoded as white, and any portion of the analog signal above the threshold level is decoded as black, it can be seen that, when the threshold voltage lies between 6.16 volts and point Q, a portion of the video transitions to black are being lost. In other words, the digitized video signal contains less black information than it should. Conversely, when the threshold voltage is between point Q and 5.14 volts, the digitized video signal contains less white information than it should. So, when this information is applied to the VTC-versus- N plot in Figure 3.4, the values of N to the left of the VTC peak equate to thresholds that give lighter-than-optimum copy, and values of N to the right of the VTC peak equate to thresholds giving darker-than-optimum copy. This, of course, assumes that the VTC peak is indeed AT the optimum threshold N value. Figure 3.5 illustrates this point by showing scanner reproductions of IEEE Facsimile Test Pattern 12 for incremental increases of N . Note the lack of black information with the smaller values of N followed by lack of white information as N increases beyond optimum.

We are now in a position to intelligently analyze the VTC-versus- N plots for the various ECPs to see if an optimum threshold value is indeed pinpointed by the peak of the VTC

Ch 3

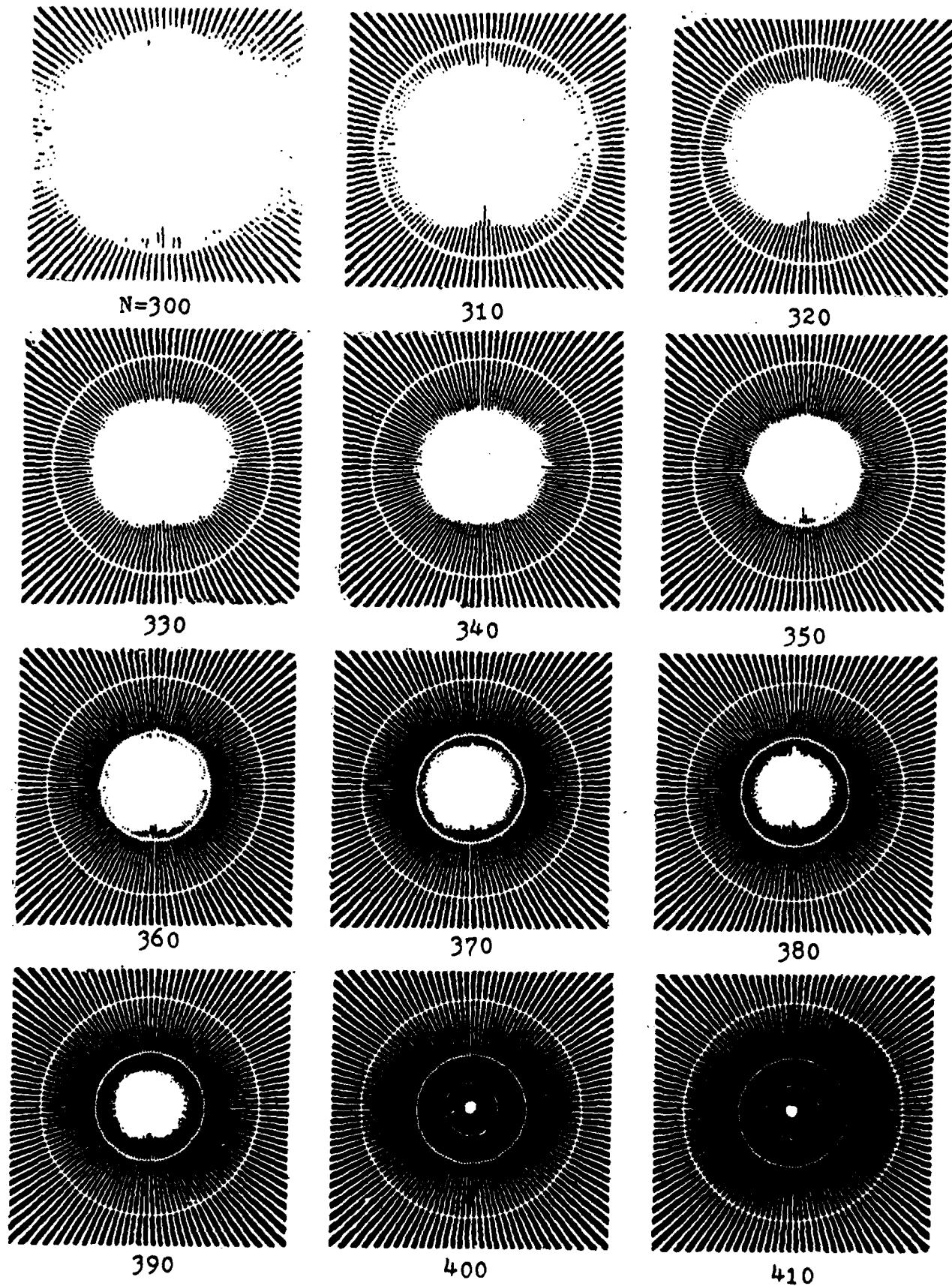
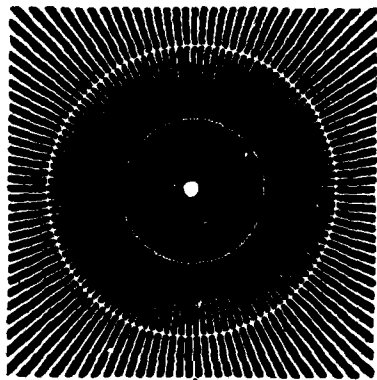


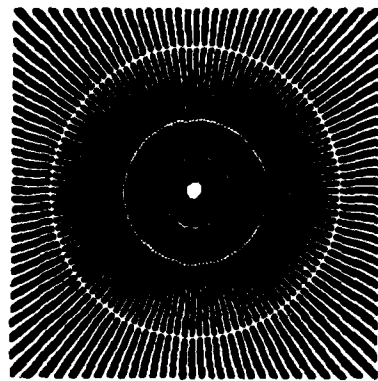
FIGURE 3.5

IEEE TEST PATTERN 12 SCANNED
WITH INCREASING VALUES OF N
WHICH CORRESPONDS TO
DECREASING VALUES OF
THRESHOLD VOLTAGE

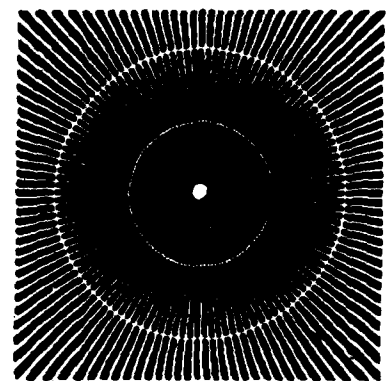
Ch 3



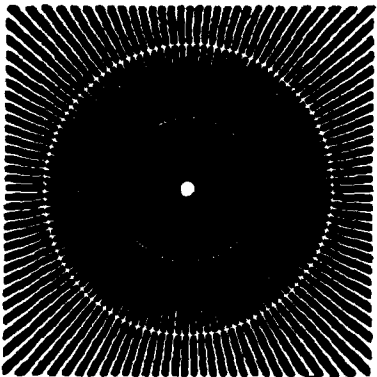
N=420



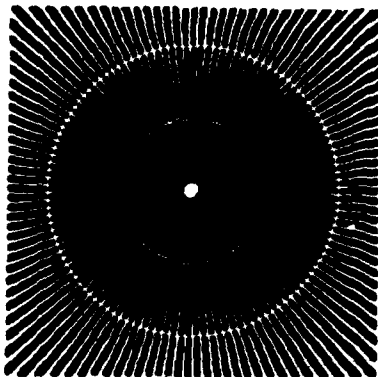
430



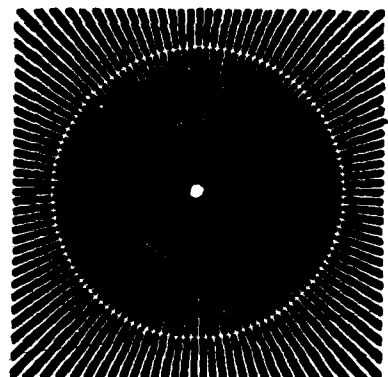
440



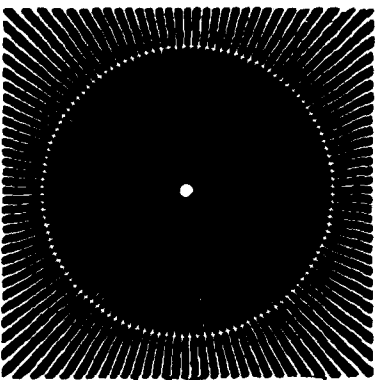
450



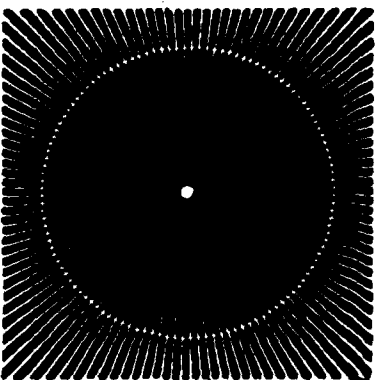
460



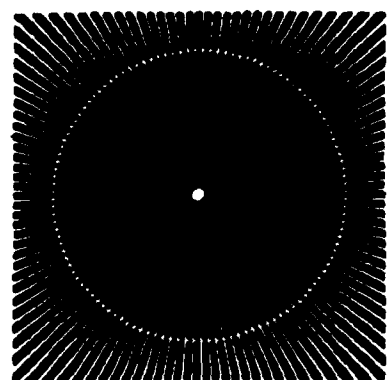
470



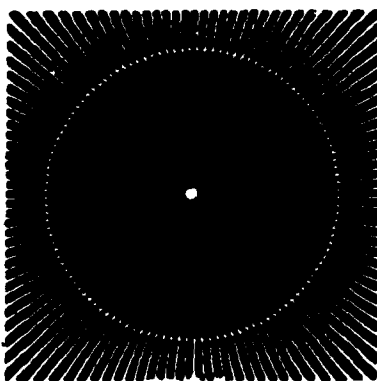
480



490



500



510

FIGURE 3.5 (CONT.)

curve. Figures 3.6 to 3.12 contain individual plots of the various ECPs. In Figure 3.6(A) ECP A was found to exhibit the desired characteristics required for the ATC. The peak of VTC was well defined and indeed occurred at a value of N that produced optimum hard copy as in Figure 3.6(B). Note that even in the copy in this report, (1) the capital letters in the 4-point type are legible.

When scanning a single discrete spatial frequency, the analog signal will be very nearly sinusoidal with constant amplitude. For this reason the number of black/white transitions will be constant in the span of significant video information. Accordingly, constant-frequency ECPs B, C, and D in Figure 3.3 produced predictable plateau-type curves. These curves are shown in Figures 3.7 to 3.9. The peaks for some undetermined reason occurred at either end of the plateau region, but intuitively it can be concluded that these peaks were not precipitated by valid video transitions. When hard copy was produced by thresholds based on these peaks, the results were as anticipated: either too light in the cases of ECPs B and C, or too dark in the case of ECP D. A comparison of the VTC plots of these three ECPs in Figure 3.10 provides an interesting manifestation of the

(1) Subsequent scanner outputs in this thesis will be xerox reproductions which fail to do complete justice to the actual scanner hard-copy output. Therefore in some cases, scanner output will only be described rather than included for viewing. Also the reader should be aware that the scanner system digitizes to only one binary level. Hence, gray tones in the IEEE Test Chart are not reproduced as such. The photograph, for example, (IEEE Test Pattern 15) is substantially degraded from the original.

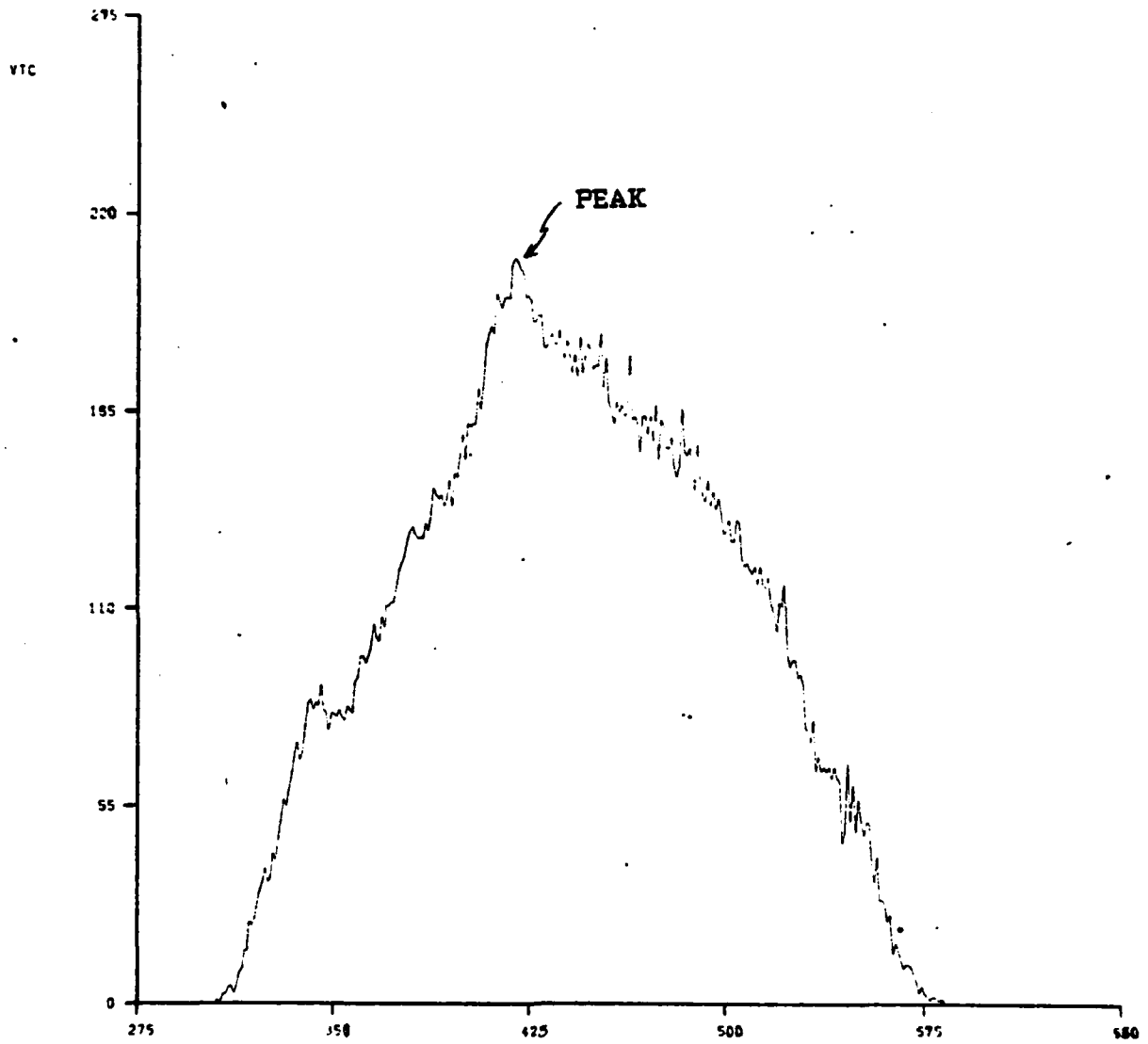
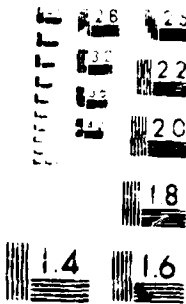
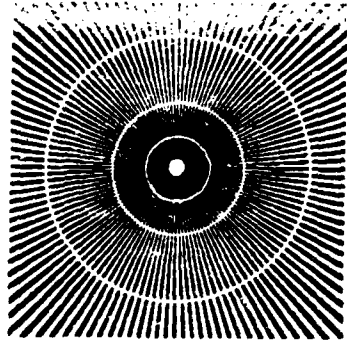
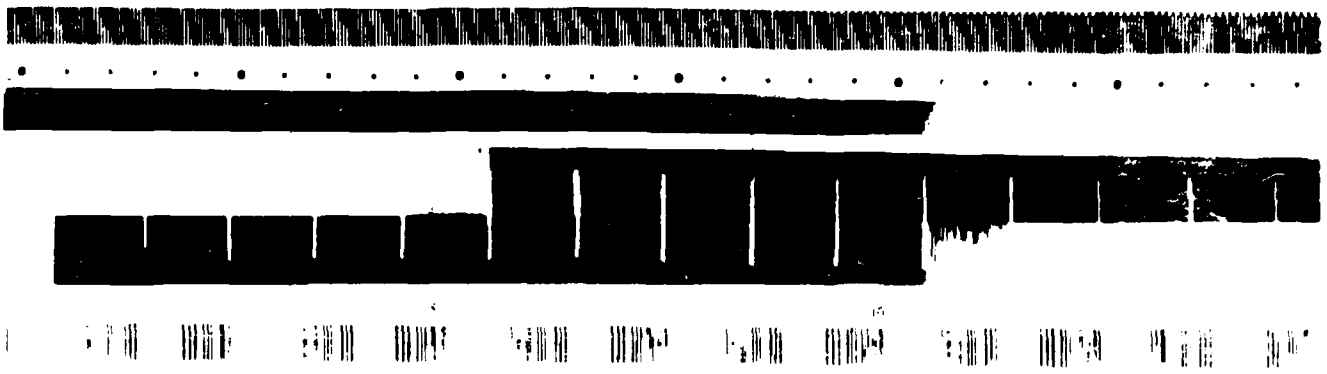


FIGURE 3.6(A) VTC-VERSUS-N CURVE FOR ECF A

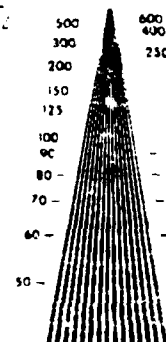


NMA MICROFONT QJKLPYZ
6BSI2GH5D4X7U3W8V9E
QJLKPYZ 6BSI2GH5D4X7U3W8V9E

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
-03%04h ASA OCR-A

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890 PIIte



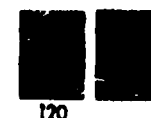
ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890

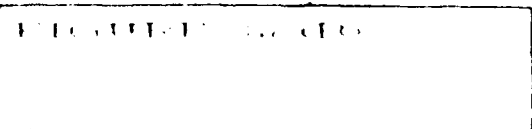
ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNOPS
TUVWXYZ 0123456789
stuvwxyz1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975 FACSIMILE TEST CHART



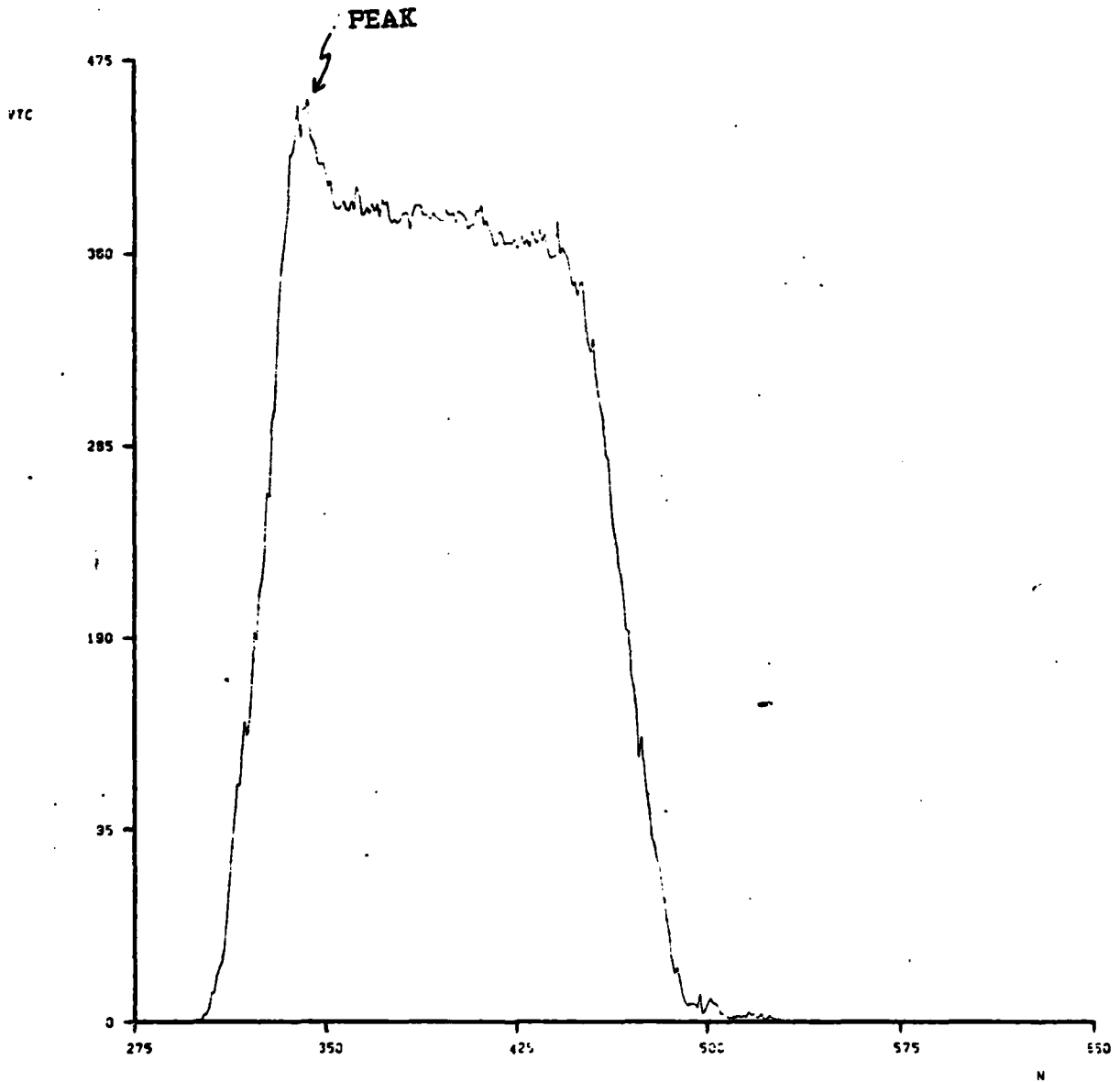


FIGURE 3.7 VTC-VERSUS-N CURVE FOR ECP B

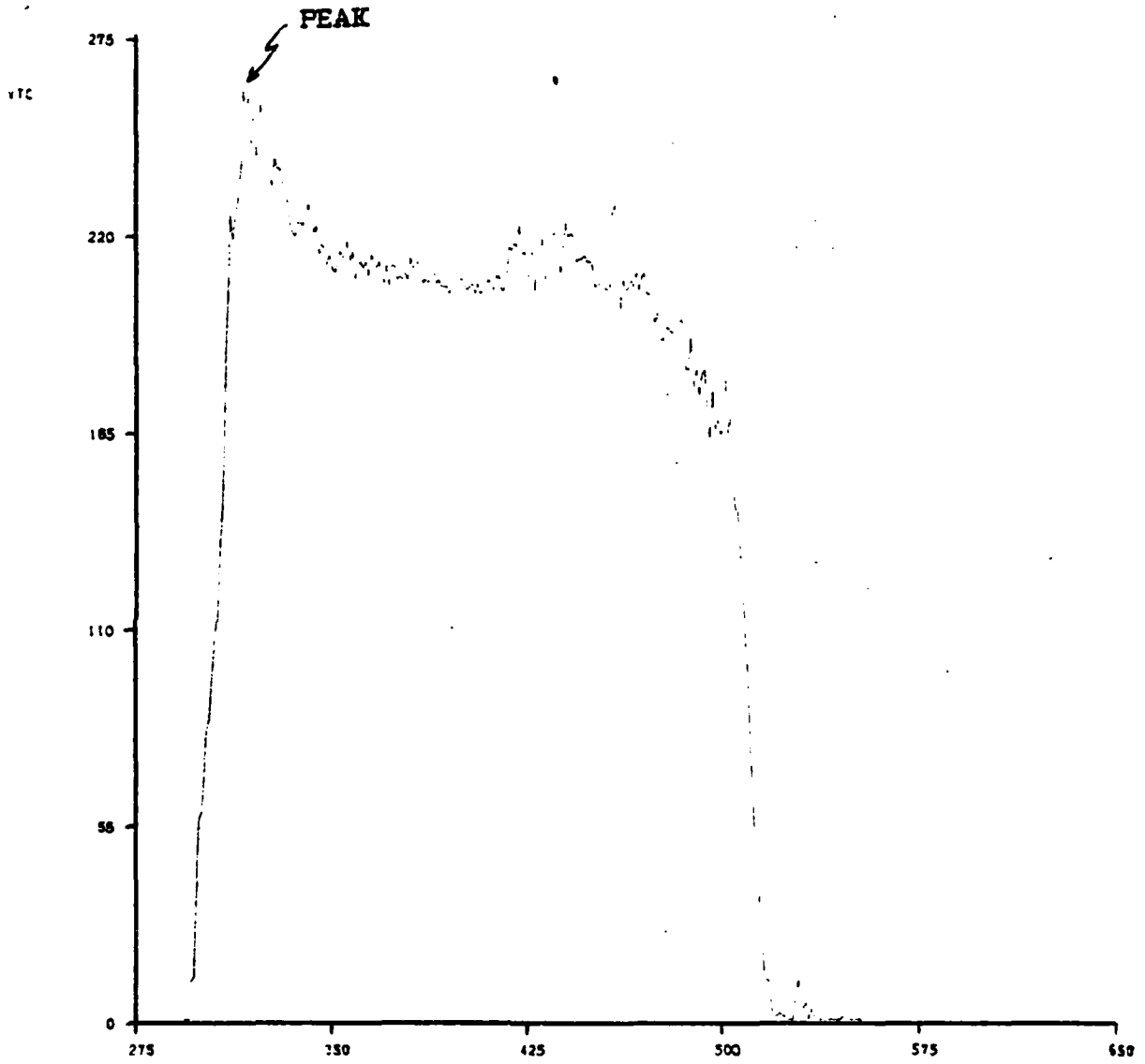


FIGURE 3.8 VTC-VERSUS-N CURVE FOR ECP C

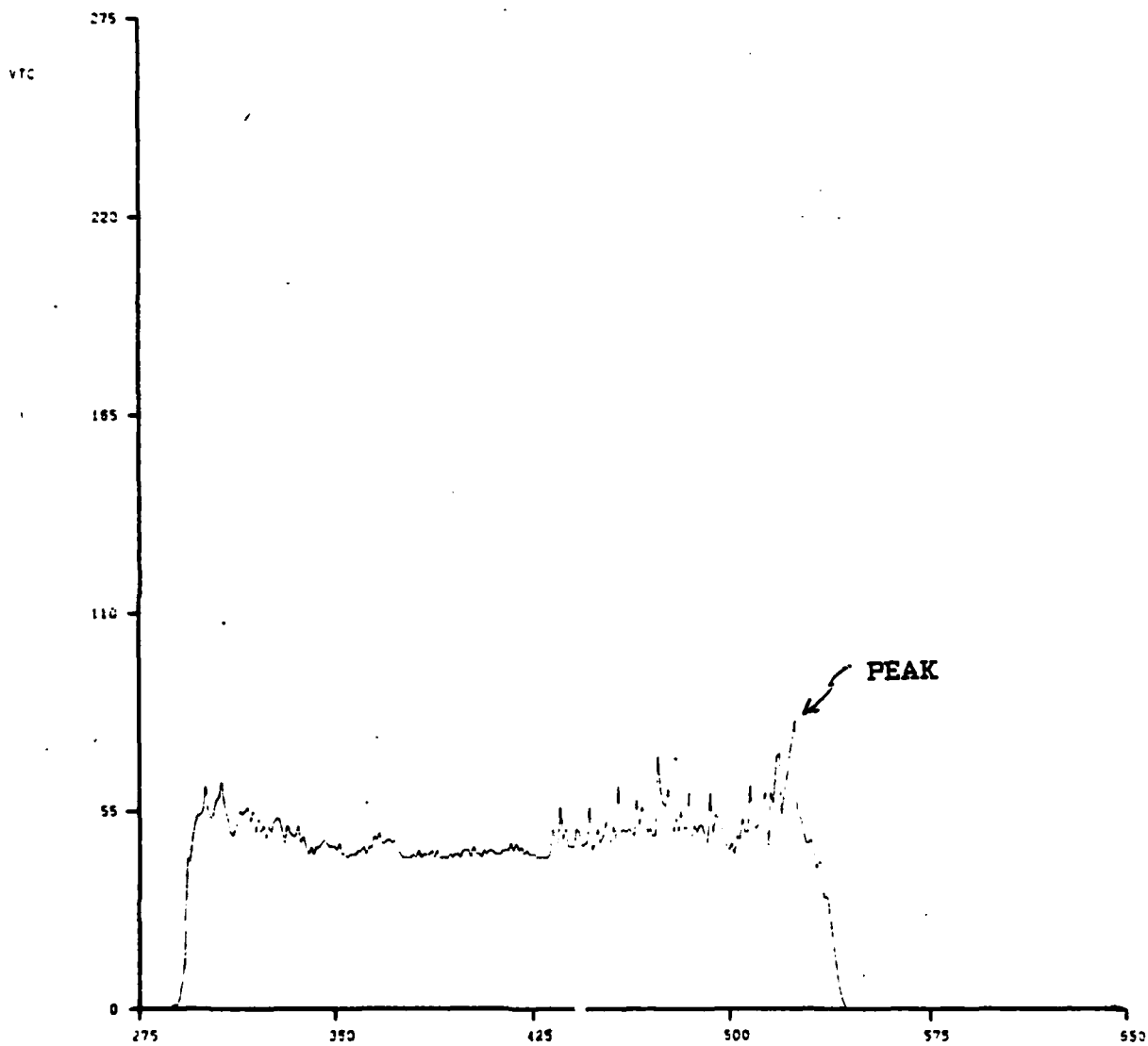


FIGURE 3.9 VTC-VERSUS-N CURVE FOR ECP D

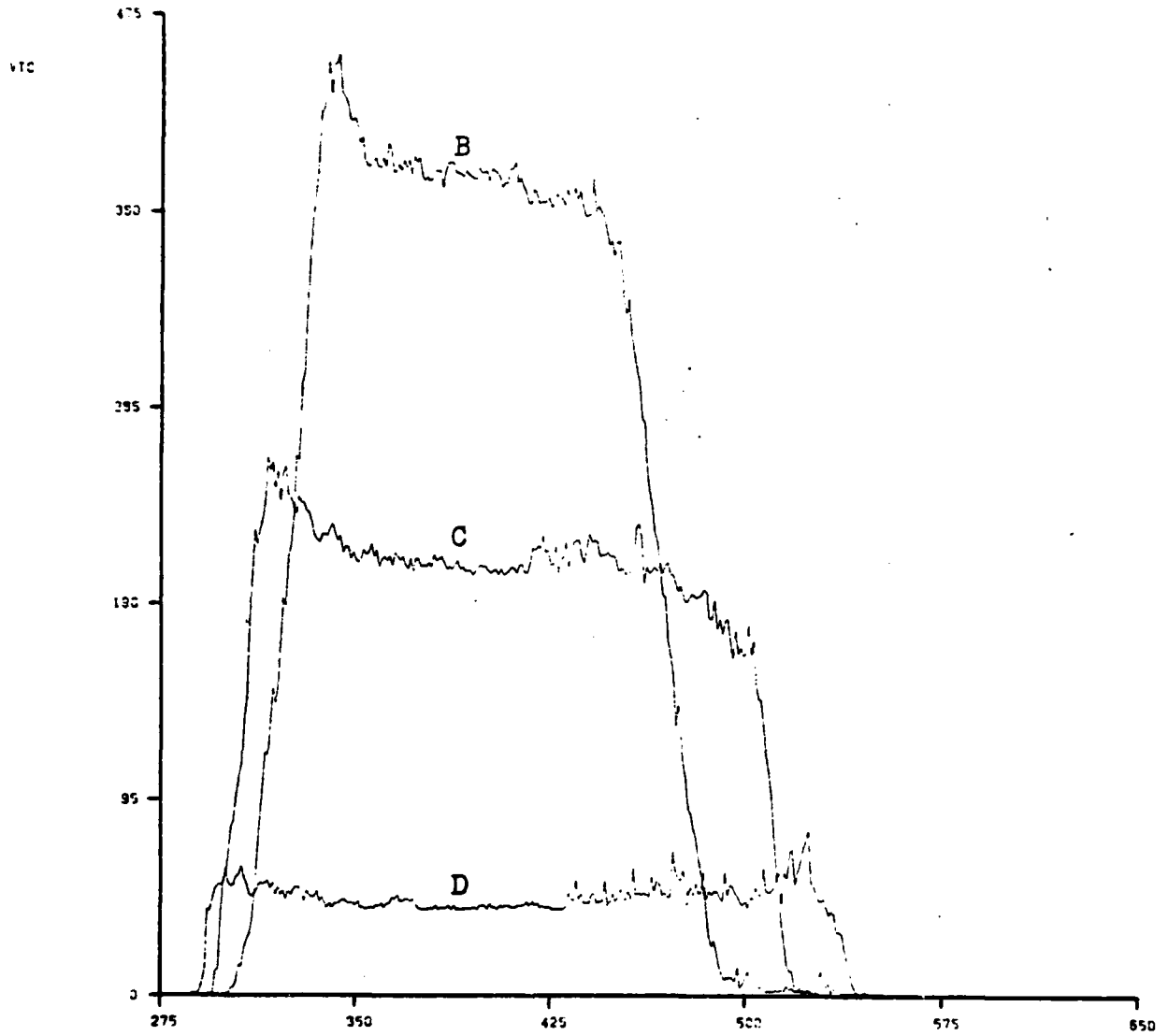


FIGURE 3.10 COMPARISON OF CONSTANT-FREQUENCY ECP PLOTS

reduction in RV spans with increasing spatial frequency due to smaller pel swings. And with increases in spatial frequency, the VTC curves naturally are higher due to more black/white transitions. The trend exhibited by these curves provides the probable conclusion that if an ECP were available containing the Nyquist frequency of 100 line-pairs/inch, it would most likely produce an impulse-like VTC curve centered around the value of N providing the optimum threshold level.

ECP E in Figure 3.3, due to its constant frequency nature, also yielded a plateau-shaped curve. See Figure 3.11. Its utility was no better than the other discrete-frequency ECPs. On the other hand, ECP F had a definable peak because of the variety of spatial frequencies present (Figure 3.12), but its usefulness was marginal since the actual peak information was occluded by the uncertainty in the data. Therefore, ECP A is obviously the best choice as a CALIBRATION PATTERN for the ATC. Figure 3.13 presents a comparison of all ECP plots as a convenience to the reader.

When the behavior of ECP A plots is analyzed with respect to other variables, further insight is gained to the robustness of its ability to select the optimum threshold value based on the VTC peak. For example, Figure 3.14 shows the behavior of the VTC curve with the loss of one fluorescent light. As expected, less light causes a smaller pel swing which is evidenced by comparing the spans of N in the two curves. Looking more closely, one can see that while the curves begin to rise at almost the same value

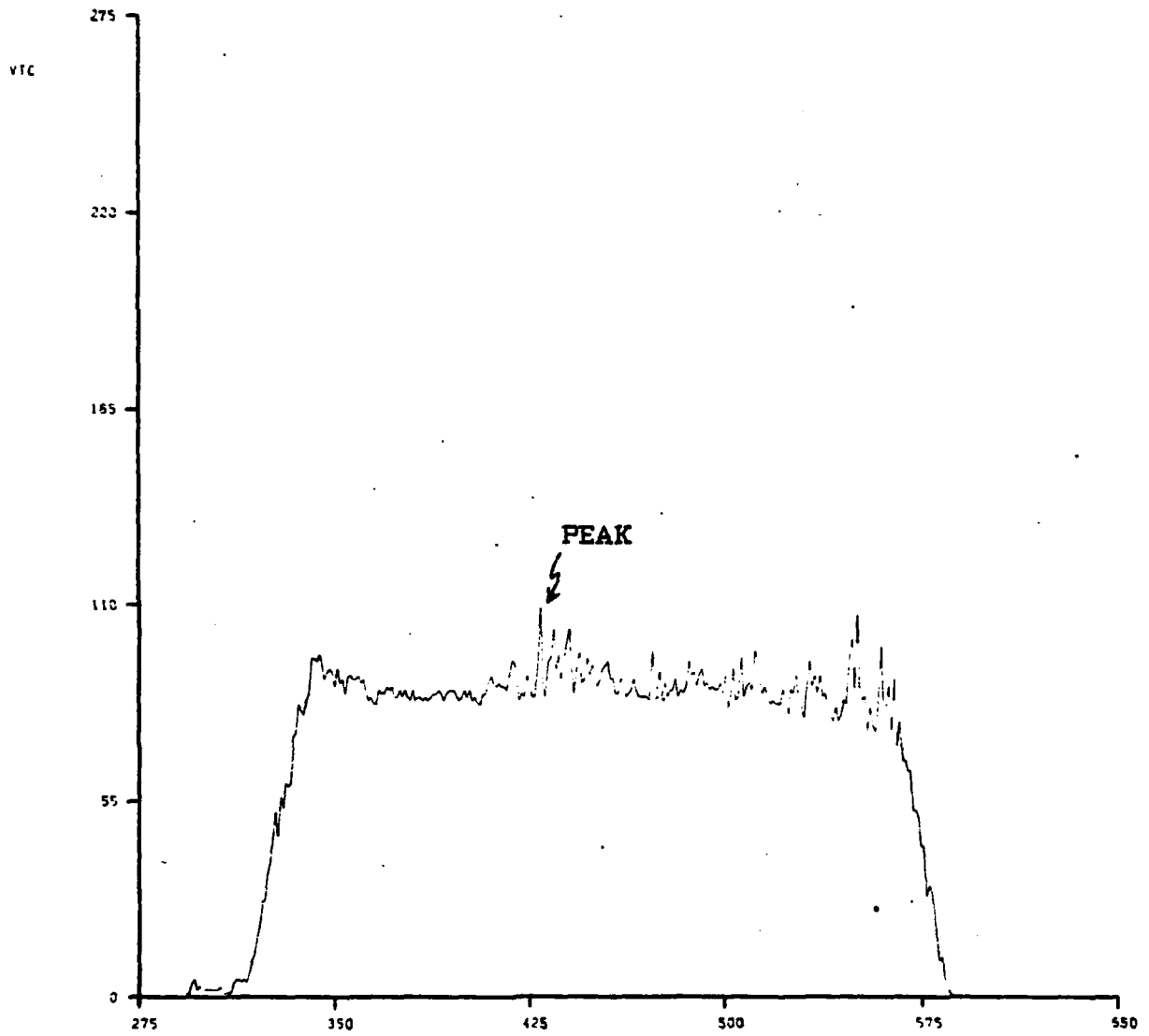


FIGURE 3.11 VTC-VERSUS-N CURVE FOR ECP E

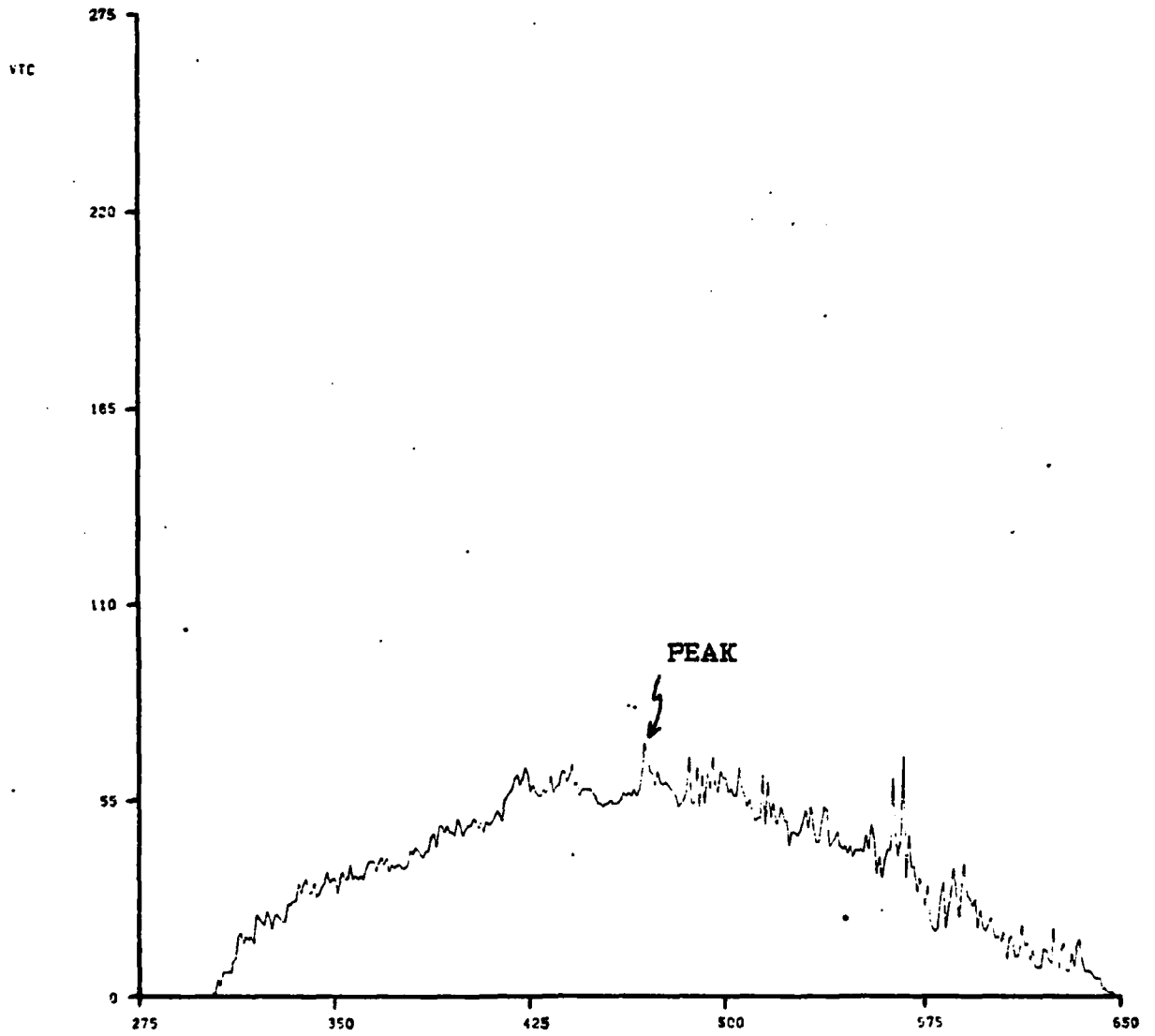


FIGURE 3.12 VTC-VERSUS-N CURVE FOR ECP F

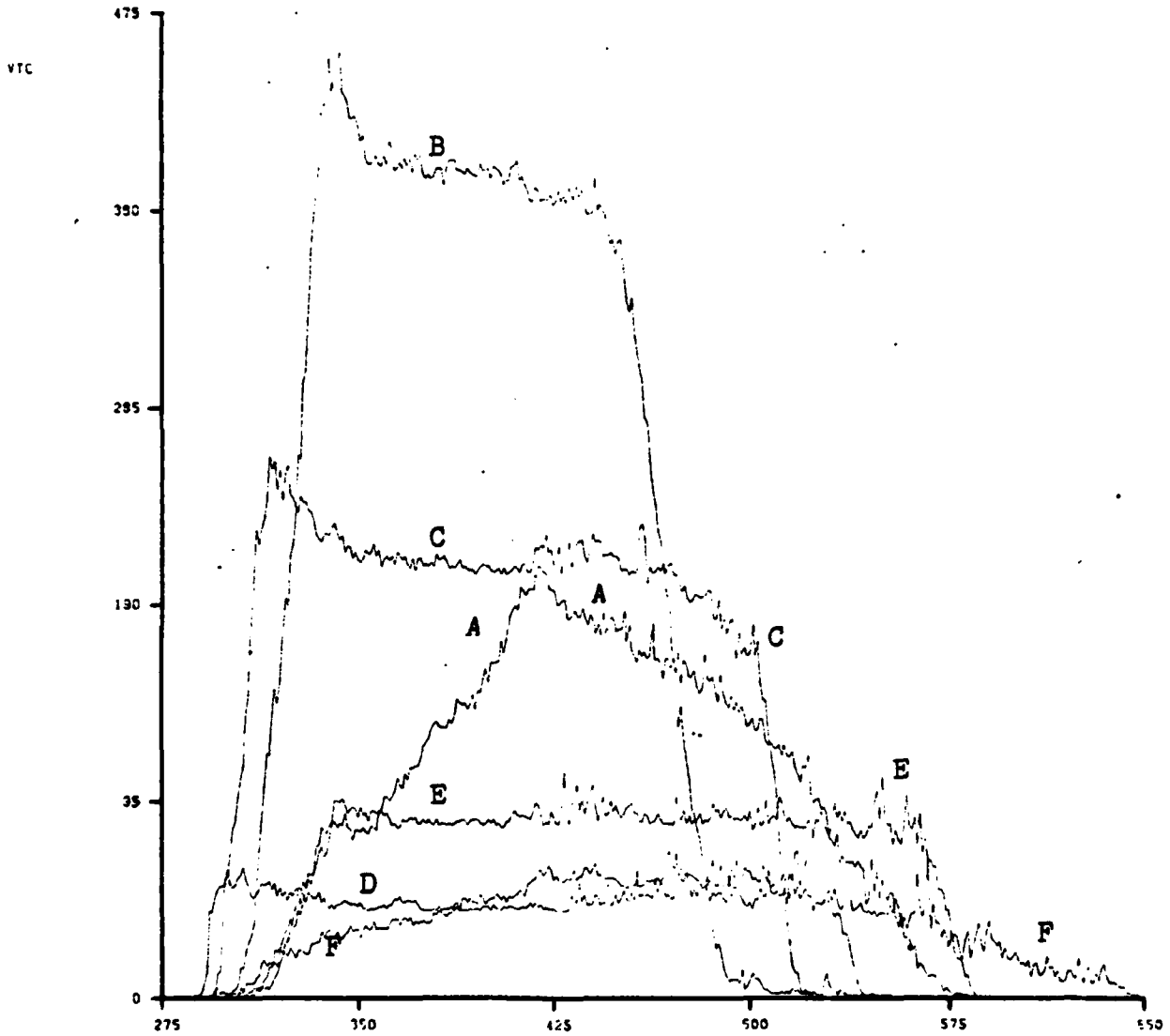


FIGURE 3.13 COMPARISON OF ECPs A THROUGH F

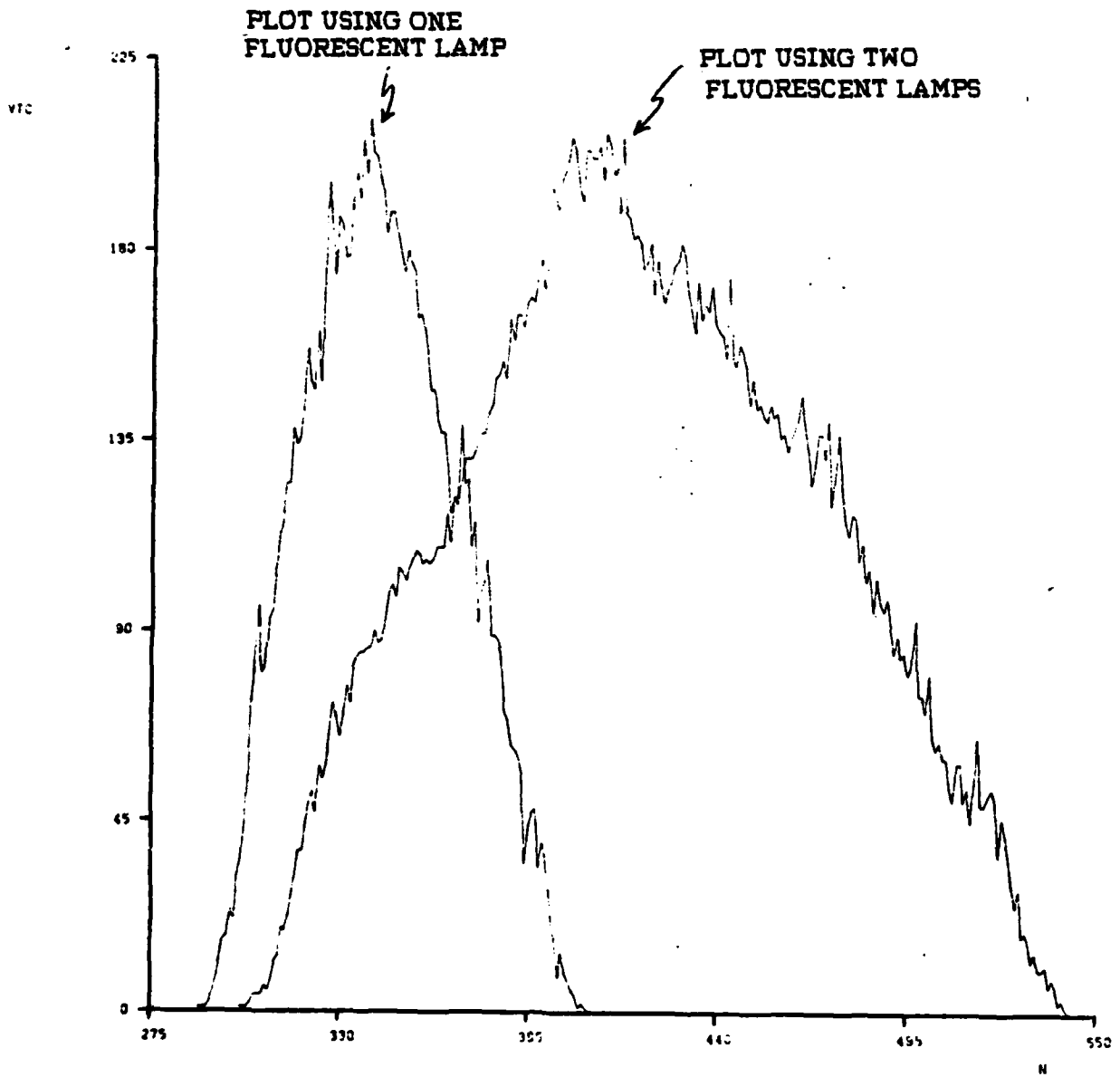


FIGURE 3.14 EFFECT OF ONE FLUORESCENT LAMP VERSUS TWO ON ECP A

of N on the left, they return to zero at much different N-values on the right. The interpretation is thus: In the analog video signal, different amounts of light cause small shifts in the black signal level but large shifts in the white signal level. It can also be seen that of the two curves, the curve resulting from one lamp has the steeper slopes on both sides. This means that an increase in light causes a more dramatic increase in pel swing at the lower spatial frequencies versus the higher spatial frequencies. But by far the most important result is that both curves display an obvious peak; one that will be chosen by the ATC algorithm. The threshold level defined by the two peaks were clearly optimum for the available light, as judged by the quality of hard copy output. (1)

Figure 3.15 illustrates similar effects with different colors of paper. Here the diminishing pel swing and increasing slopes are even more dramatic with the darker colors. As in Figure 3.14, there is a definite shift of the optimum threshold value, but the ATC design will inherently compensate for these shifts and continue to select the threshold providing the best resolution. (2) Figure 3.16 consists of plots using fluorescent lights with various spectral contents. The conclusion is that among the colors examined -- green, cool white, and warm white -- there was not a significant difference in performance, although

(1) Hard-copy samples resulting from single-lamp illumination are contained in Chapter 6.

(2) Scanner output of the IEEE Test Chart on red background is contained in Chapter 6.

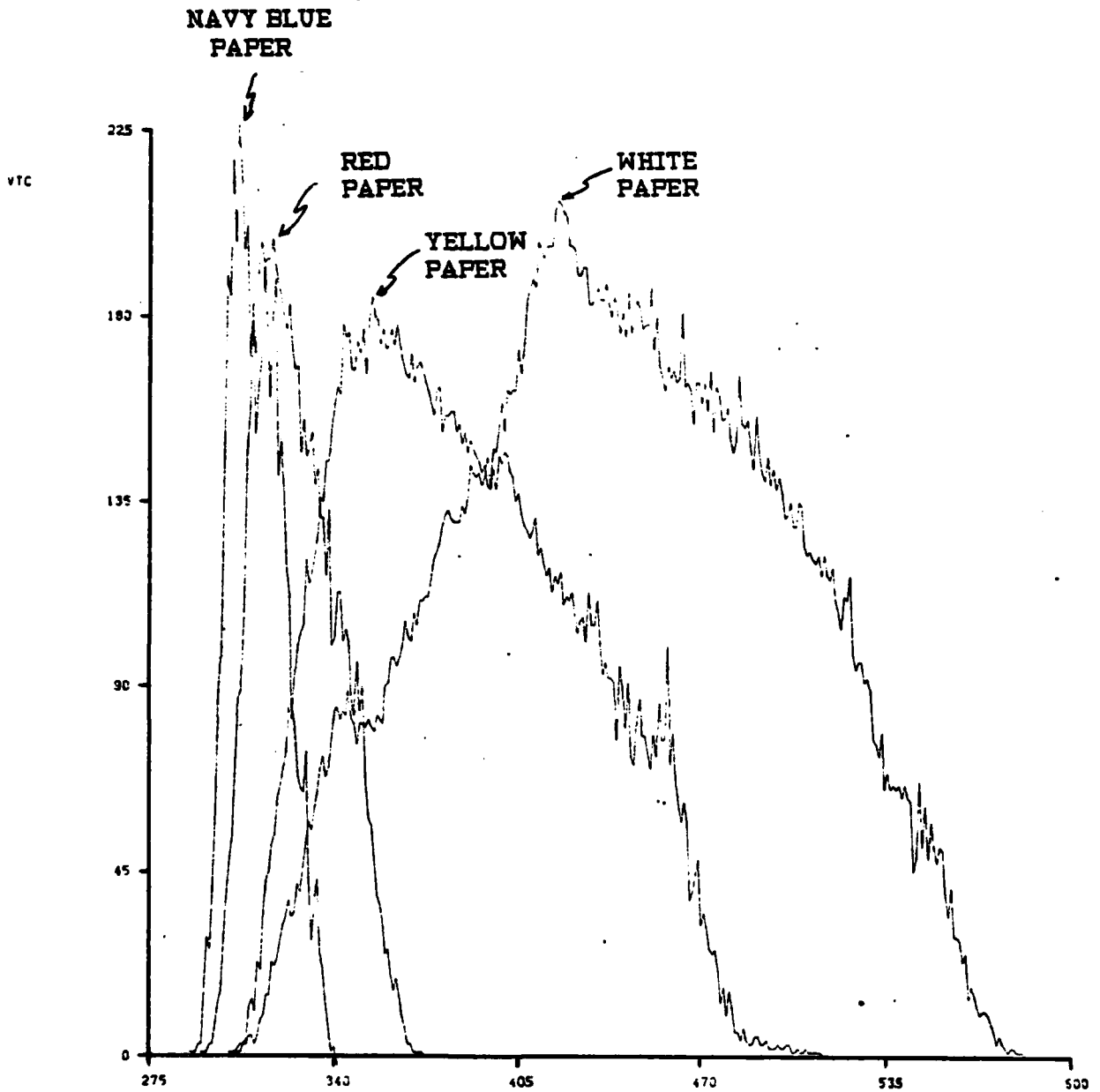


FIGURE 3.15 EFFECT OF DIFFERENT PAPER COLORS ON ECP A

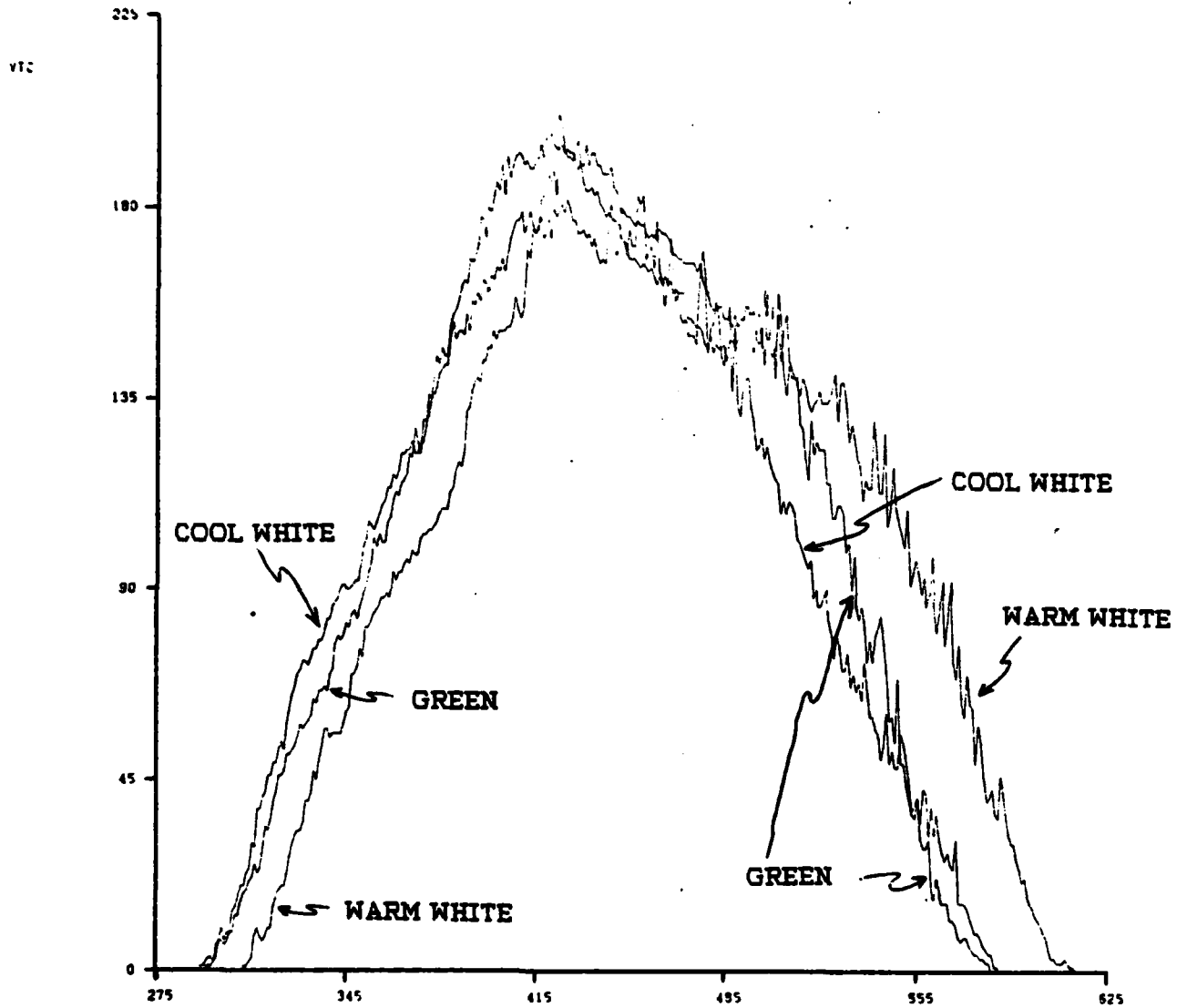


FIGURE 3.16 EFFECT OF FLUORESCENT LAMPS OF DIFFERENT SPECTRAL CONTENT ON ECP A

the warm white bulbs did appear to generate a slightly larger pel swing. On the other hand, Figure 3.17 demonstrates that fluorescent lights experience a certain amount of degradation over their lifetime. Once again the ATC will compensate for this effect. It should be noted that fluorescent lights deteriorate in a non-uniform manner over the length of the tube. Deposits on the inner walls near the filaments at either end cause excessive degradations in light emission at the ends, resulting in precisely the analog waveform illustrated in Figure 3.2(E).

As one final point, note that the curves contain a small degree of uncertainty rather than being smooth. It is hypothesized that the jitter is caused at least in part by the clocking noise in the scanner circuitry. Another cause could be power supply fluctuations producing minor deviations in the output of the circuitry generating the threshold voltage. The important conclusion is that while the general shape of the VTC curve is stable, individual plots will differ by some small amount as illustrated in Figure 3.18, which shows several runs taken under identical conditions. In this instance, extreme care was taken to insure all inputs remained constant, and yet there was still a small degree of inconsistency in the plots taken. The uncertainty that is present is by no means a barrier to the proper operation of the ATC, but the reader must be aware that the DEGREE of uncertainty in the VTC curve will have an effect on ATC performance especially with respect to the VTC sampling activities detailed in Chapter 5.

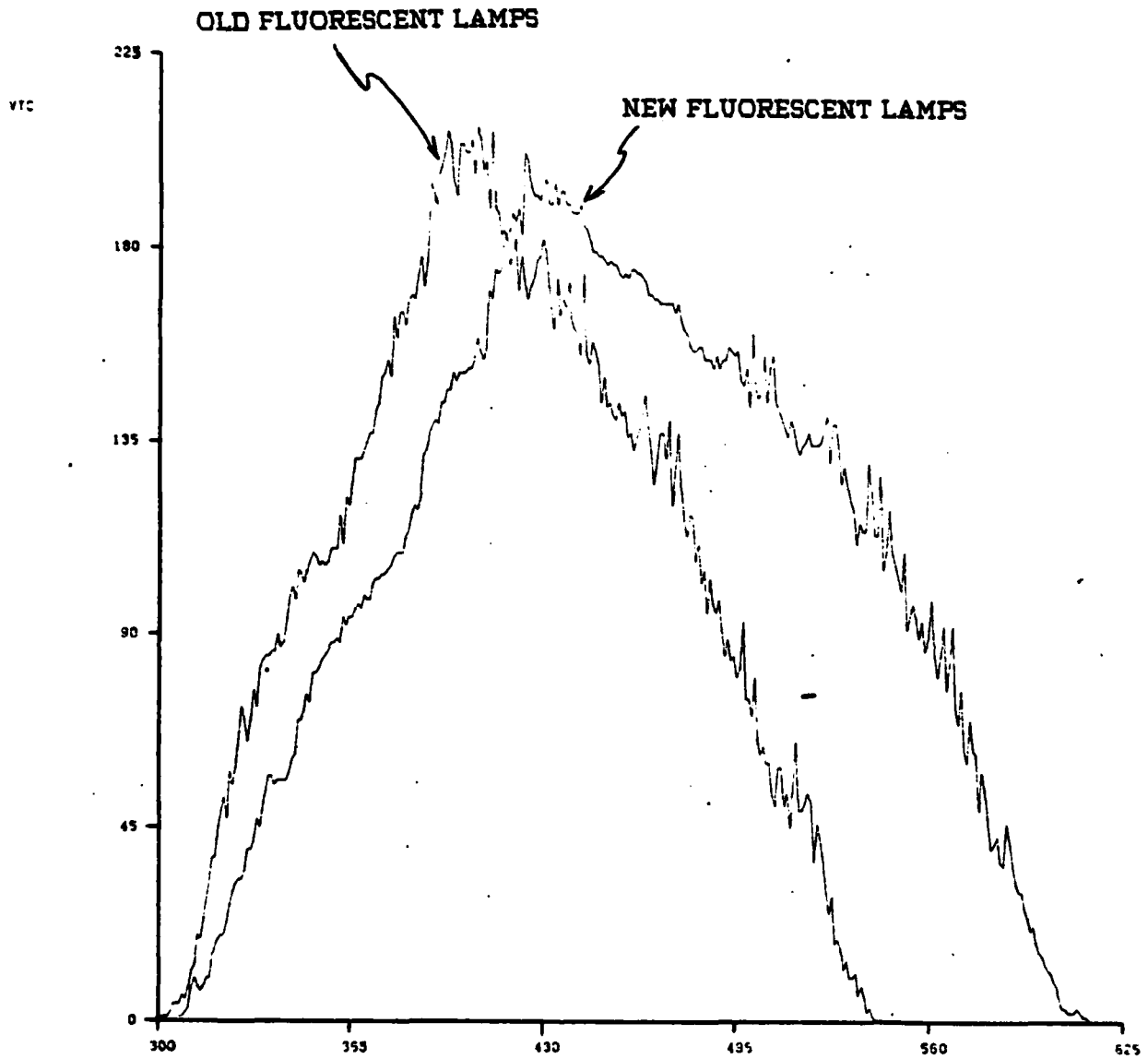


FIGURE 3.17. EFFECT OF OLD VERSUS NEW FLUORESCENT LAMPS ON ECP A

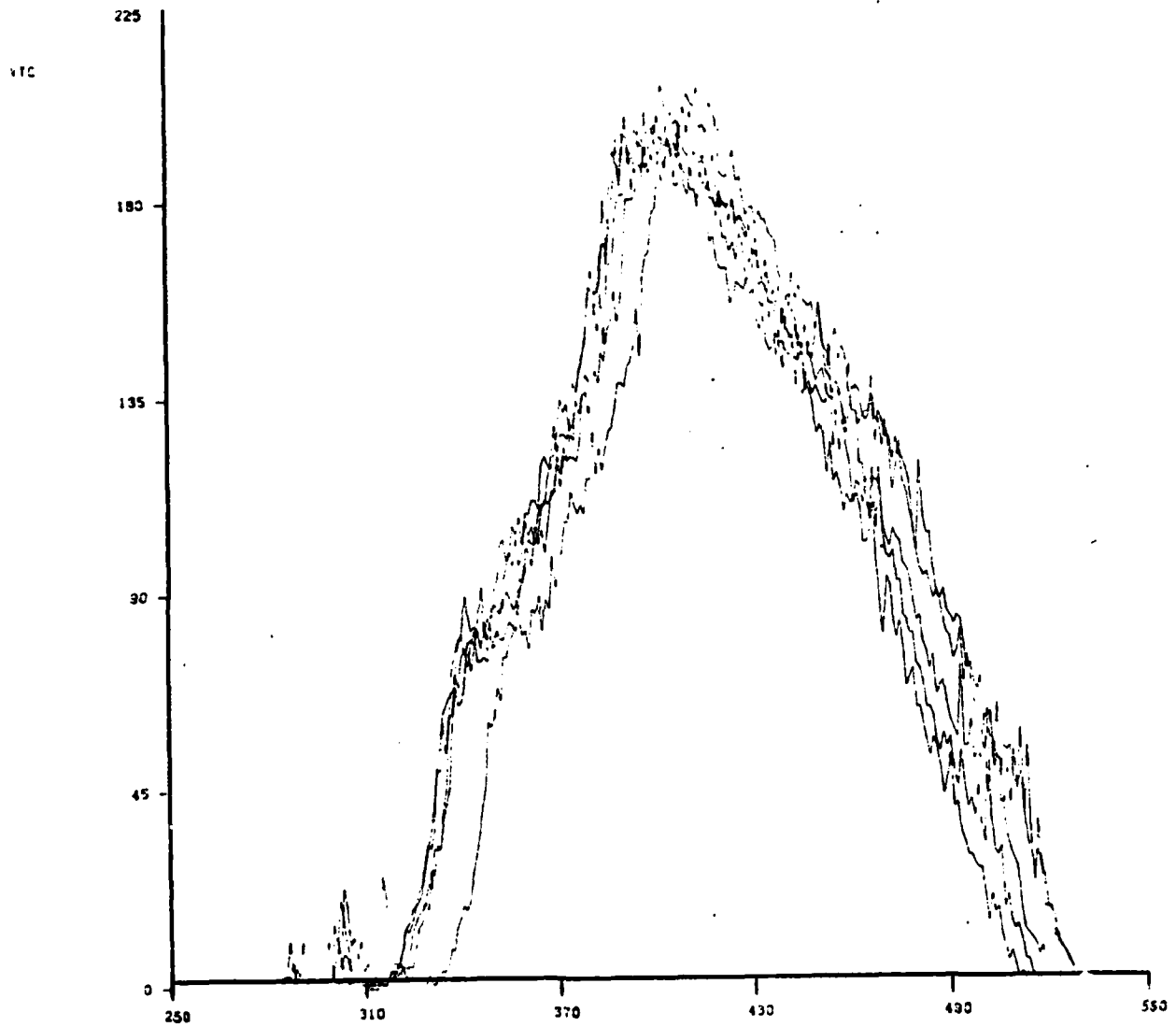


FIGURE 3.18 VTC FOR ECP A PLOTTED FIVE TIMES UNDER IDENTICAL CONDITIONS

CHAPTER 4

AUTOMATIC THRESHOLD CONTROL (ATC) DESIGN

A. ATC BLOCK DESCRIPTION

In terms of Chapter 3, the goal is now to design the necessary hardware to expeditiously pinpoint the threshold value, N , that generates the maximum number of black/white transitions. With the CALIBRATION PATTERN producing the desired analog signal, the THRESHOLD CONTROL UNIT (Figure 4.1) commands the THRESHOLD LEVEL GENERATOR to set a series of tentative threshold values for the A-to-D CONVERTER. The number of black/white transitions produced by each threshold value is summed by the VIDEO COUNTERS, and the sum, VTC, is correlated by the THRESHOLD CONTROL UNIT. Once all threshold values in the series have been tested, the THRESHOLD CONTROL UNIT locks in the threshold value that produced the maximum number of black/white transitions.

B. CHOICES FOR IMPLEMENTATION

Because of its availability and inclusion in the existing scanner, it was a logical decision to use the F8 microprocessor as the THRESHOLD CONTROL UNIT and to design a digital-to-analog circuit as the THRESHOLD LEVEL GENERATOR. The VIDEO COUNTERS provided a natural interface to the F8, but modifications in the video A-to-D section were required to upgrade the digital video signal to the quality required for accurate counting. The actual design details are covered in the next section.

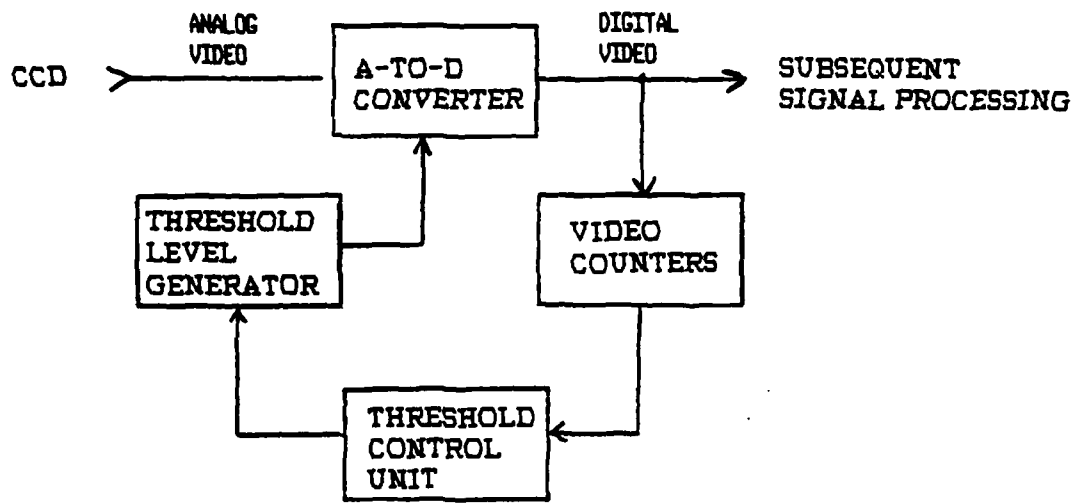


FIGURE 4.1 AUTOMATIC THRESHOLD CONTROL BLOCK DIAGRAM

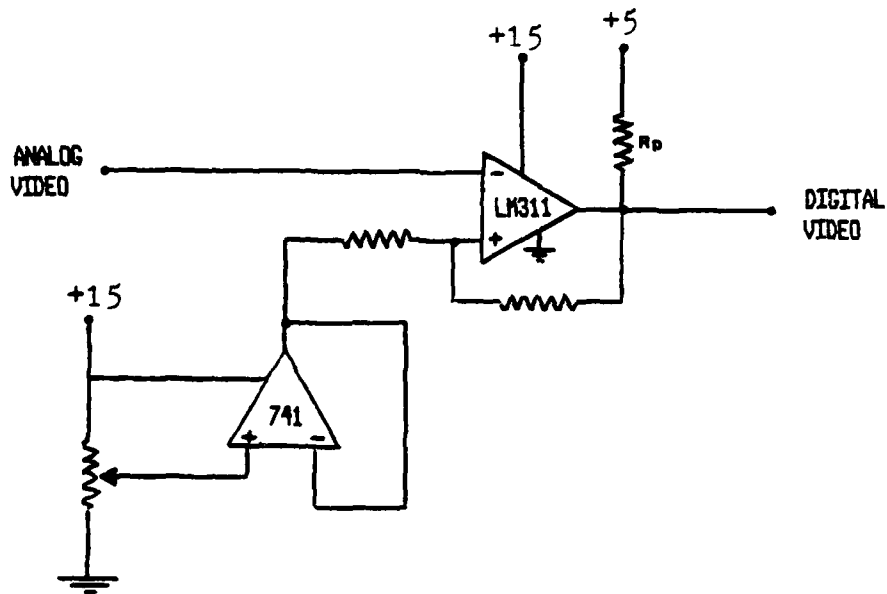


FIGURE 4.2 ORIGINAL VIDEO A-TO-D CONVERTER AND THRESHOLD LEVEL GENERATOR

C. CIRCUIT MODIFICATIONS

1. DIGITAL THRESHOLD LEVEL GENERATOR (TLG)

The existing scanner used a potentiometer buffered by a unity-gain 741 operational amplifier for manually setting the threshold level. See Figure 4.2. This circuit, which included an LM311 comparator as the A-to-D converter, was located on the TIMING & PROCESSING circuit board. It was removed entirely and is documented in Appendix E. A primary theme in the design of the new TLG was flexibility. That is, the circuit was constructed in such a way to allow for future alterations in voltage ranges and sensitivity for experimental purposes. The first consideration was the voltage range of the threshold level. In Chapter 2, it was found that the video information was within a span of 5.3 to 5.6 volts. Changes in the video signal were of the order of 10 to 300 millivolts. Therefore, the TLG had to be able to resolve millivolts in the 5.3 to 5.6-volt range. A 10-bit (1024-step) D-to-A converter was selected which would give a sensitivity of less than a millivolt/digital step over a range of one volt. Additional circuitry had to be added to the D-to-A converter to provide the necessary DC offset. Refer to Figure 4.3. The TLG consists of U1 through U6 with U4 providing the threshold output voltage, V_0 . U1 is an AD7533 D-to-A converter using an R-2R ladder network described in Appendix A, and U2 is a 741 operational amplifier used as a unity-gain buffer. The output of U2 is given as:

$$V_2 = -V_{ref}(N/1024) \quad (1)$$

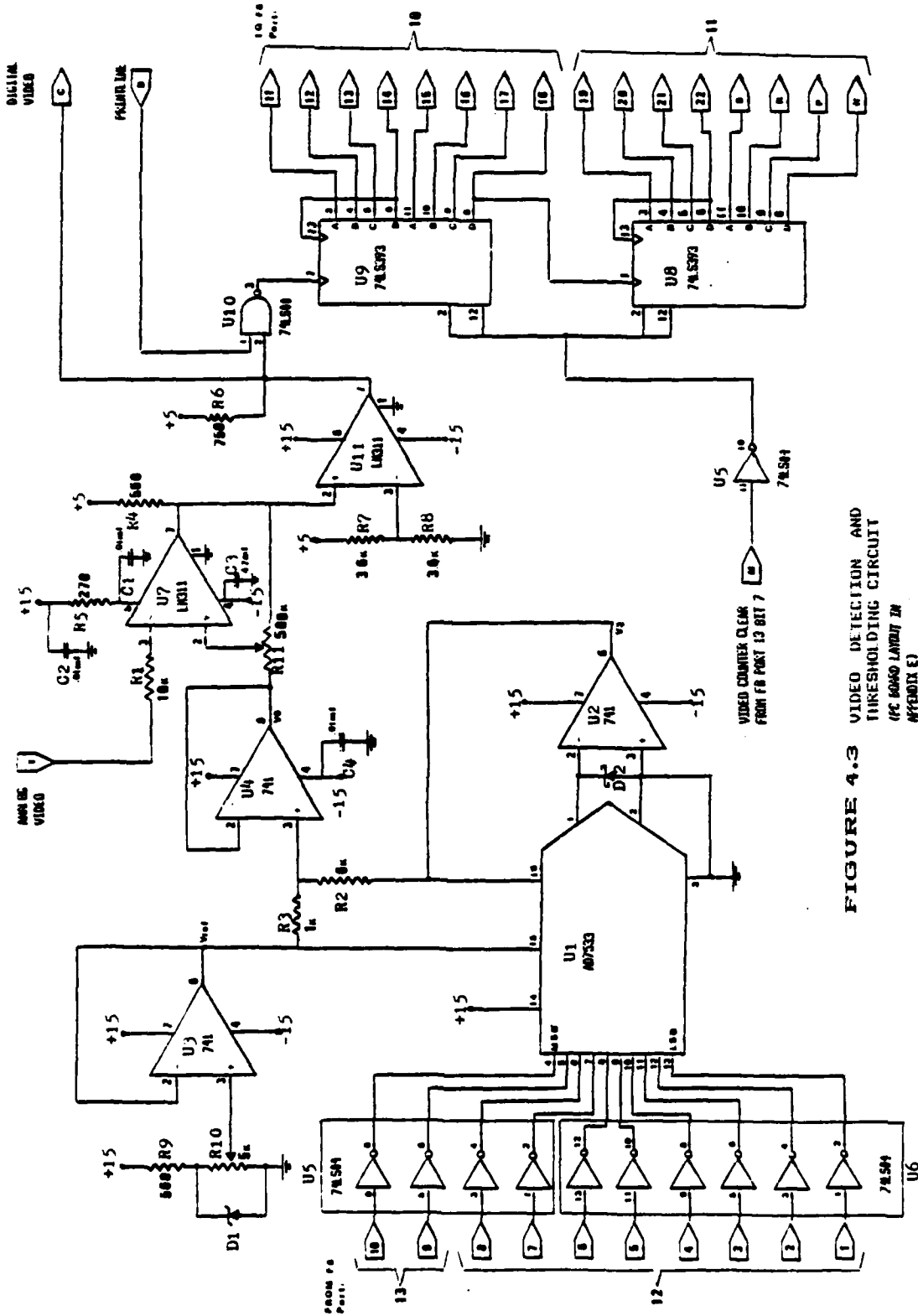


FIGURE 4.3 VIDEO DETECTION AND THRESHOLDING CIRCUIT (PC BOARD LAYOUT IN APPENDIX E)

where N is the decimal equivalent of the 10-bit binary input from the F8 to U1 through pins 4 through 13, and Vref is controlled by R10 and buffered with unity-gain op amp U3. Since op amp U4 is also a unity-gain buffer, V0 can be expressed as a function of the voltage division between Vref and V2:

$$V_0 = \frac{(R_3 \times V_2) + (R_2 \times V_{ref})}{(R_2 + R_3)} \quad (2)$$

Eliminating V2, we have:

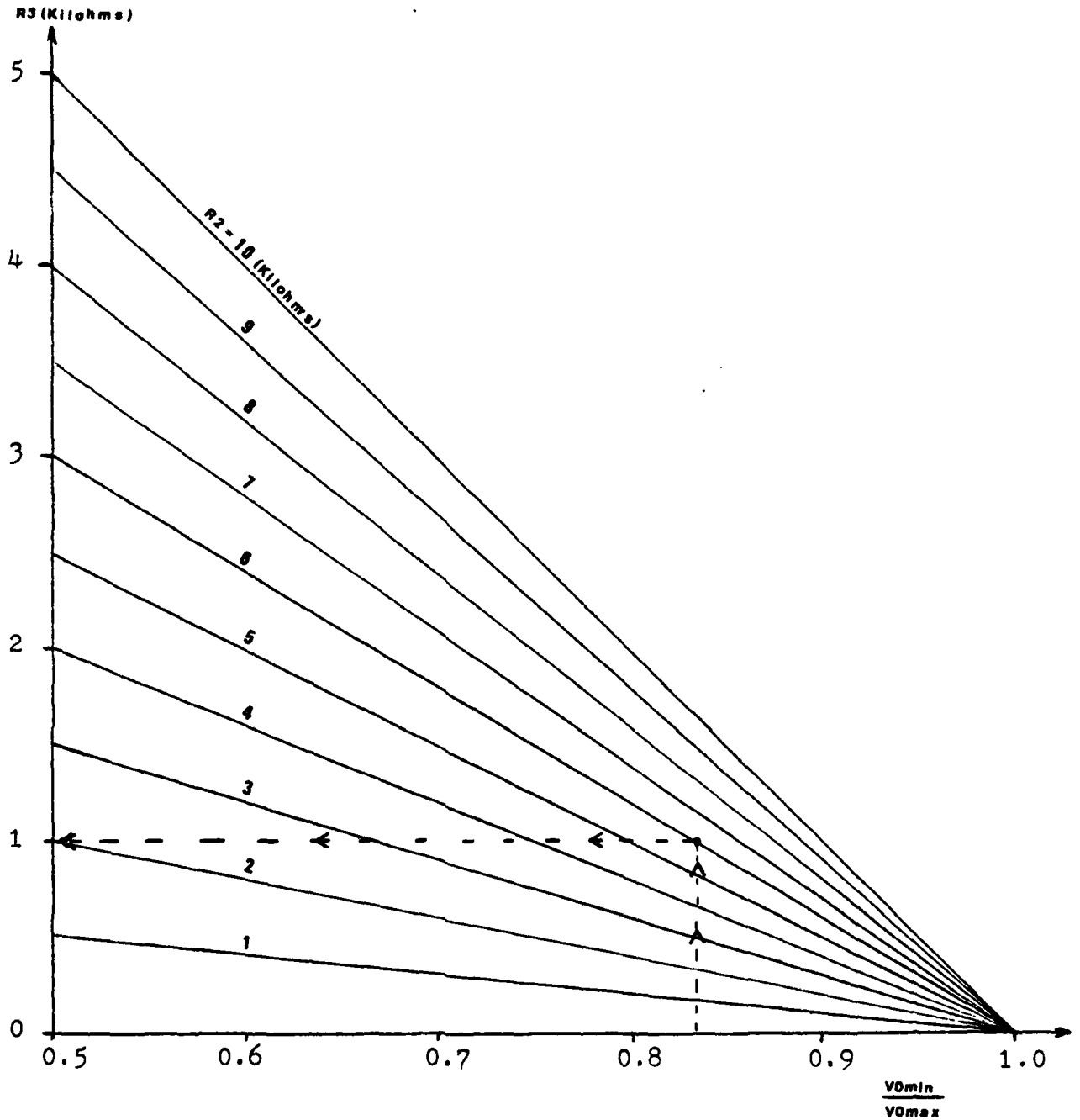
$$V_0 = V_{ref} \left[\frac{R_2}{(R_2 + R_3)} - \left(\frac{R_3}{(R_2 + R_3)} \right) \left(\frac{D}{1024} \right) \right] \quad (3)$$

Therefore, resistors R2, R3, and R10 control the width and placement of the range of the TLG. From Equation (3), a particular range (V0min to V0max) for the TLG can be established with the following procedure:

1. Determine values of V0min and V0max.
2. Arbitrarily select a nominal value for R2 in the range 1K to 10K ohms.
3. Calculate R3 for the R2-R3 voltage divider by:

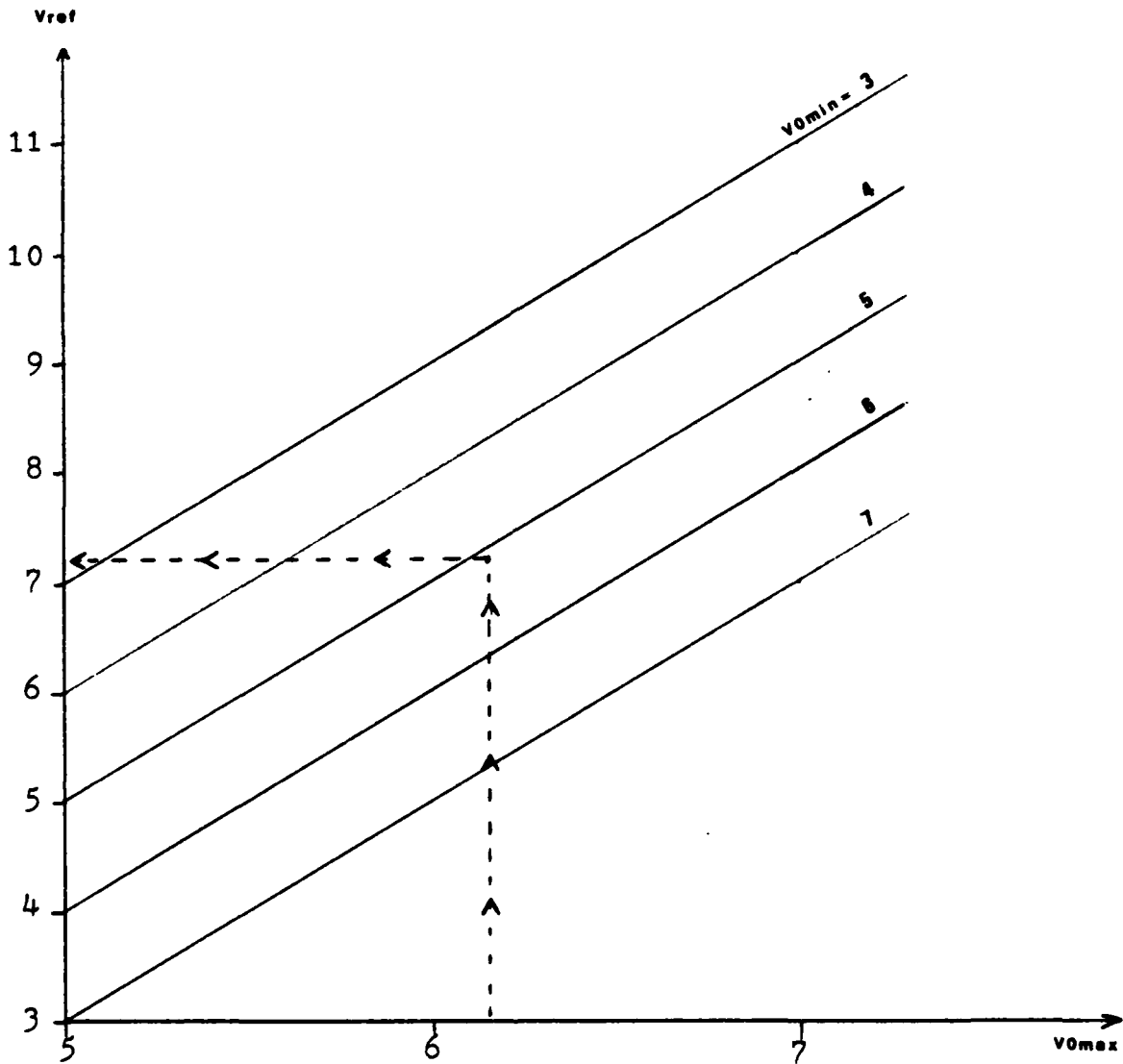
$$R_3 = R_2(1 - (V_{0min}/V_{0max}))$$
4. Calculate Vref by: $V_{ref} = (2 \times V_{0max}) - V_{0min}$
5. Set Vref by adjusting R10.

As an alternative, the graphs implementing Equation (3) in Figures 4.4 and 4.5 can be used as an aid to the calculations. The voltage range of the TLG used for this report was 5.14 to 6.16 volts giving a sensitivity of 1 millivolt/digital step. This choice is realistic and makes the results of the other



1. ENTER WITH VOLTAGE RATIO $\frac{V_{0min}}{V_{0max}}$
2. TRAVEL VERTICALLY TO DESIRED R_2
3. TRAVEL LEFT TO READ VALUE OF R_3

FIGURE 4.4 GRAPH FOR CALCULATING R_3 OF TLG



1. ENTER WITH UPPER LIMIT OF VOLTAGE RANGE V_{0max}
2. TRAVEL VERTICALLY TO LOWER LIMIT OF VOLTAGE RANGE V_{0min}
3. TRAVEL LEFT TO READ VALUE OF V_{ref}

FIGURE 4.5 GRAPH FOR CALCULATING V_{ref} OF TLG

chapters particularly simple to interpret.

2. VIDEO A-TO-D DESIGN

Referring again to the scanner's original video A-to-D circuit in Figure 4.2, the response of this circuit to the highest spatial frequencies was found to be rather slow (3.03 microseconds) due to the size of the pull-up resistor, R_p . While this was adequate for the existing design and in fact helped prevent clock noise feed-through, it was found that the performance was inadequate as a clocking input to the VIDEO COUNTERS. Therefore in the re-design of the video A-to-D circuit, R_p was changed to 560 Ohms giving a rise time of 332 nanoseconds. This allowed the circuit to more faithfully digitize the spatial frequencies up to the Nyquist rate. This feature was essential so the VIDEO COUNTERS could record the black/white transitions of all the spatial frequencies. Unfortunately with the smaller R_p , unwanted clock noise was now passing through the one-stage comparator circuit, which would have been disastrous for the VIDEO COUNTERS. Therefore a second LM311 with a constant threshold of 2.5 volts was cascaded with the first LM311 to effectively bar the clock noise from triggering spurious counts in the VIDEO COUNTERS. The revised video A-to-D circuit consists of comparators U7 and U11 in Figure 4.3.

3. DIGITAL VIDEO COUNTER STAGES

The VIDEO COUNTERS, consisting of U8 and U9 in Figure 4.3, were rather simple to implement once the digital video signal had

been upgraded. Dual, 4-bit, binary, asynchronous counters served the purpose adequately, making 16 bits available with minimal hardware. As a precaution, the digital video is gated to the counters by the signal PRINTLINE to insure only valid video transitions are recorded.

4. F8 HARDWARE INTERFACE REQUIREMENTS

To use the F8 as the THRESHOLD CONTROL UNIT, I/O ports had to be made available for data transfer. The existing ports (4, 5, 8, and 9) were already being used for scanner coordination with the hard and soft copy printing devices. (1) The threshold control requirements could have been implemented through these ports, but it would have taken considerable multiplexing and hardware design. Fortunately the research completed by Medley (2) included the addition of four new I/O ports (10, 11, 12, and 13) to the F8 system. So the only requirement to make these I/O ports available for use was to complete the wiring to a compatible connector. Details are contained in Appendix E.

5. COMBINED THEORY OF OPERATION

During the period that the optimum threshold is being sought, the circuitry of Figure 4.3 operates in the following manner. A value of N generated by the THRESHOLD CONTROL UNIT (F8) is applied to pins 4 through 13 of U1. The voltage threshold value V_0 is obtained from the division between V_{ref} and V_2 by resistors R2 and R3. The voltage threshold level, with the

(1) See Aghamohammadi, Chapter 7.

(2) Reference Chapter 7.

degree of hysteresis controlled by R11, is applied to the non-inverting input of U7 while the analog video signal from the CCD is applied to the inverting input. The digitized video is then fed through a non-inverting comparator stage provided by U11 with threshold fixed at 2.5 volts to help remove digitized clock noise. The clean digital video is then gated by PRINTLINE through U10 into cascaded counters U9 and U8. For a given line of video, the number of black/white transitions in the digital video signal can be read from the counters to ports 10 and 11 of the F8. Once the optimum threshold has been found, the value is loaded to ports 12 and 13 and valid digitized video passes off the board via pin C for synchronization and hard-copy printing. The outputs of U8 and U9 are now ignored.

6. SCANNER CIRCUIT BOARD RELOCATIONS

During the course of this project, inter-circuit interference due to clocking noise and physical separation of several critical circuit boards degraded system performance to the extent that several circuit boards had to be moved in order to shorten the connections containing critical signals. These relocations are documented in Appendix E.

CHAPTER 5
SAMPLING ALGORITHMS

In this chapter, the procedures for finding the VTC peak are discussed in detail. The purpose of this phase of research was to design a method whereby the THRESHOLD CONTROL UNIT could, in the most efficient manner possible, search the entire range of possible threshold values, $[N = 0 \text{ to } N = 1024]$, and find that value of N corresponding to the peak of the video transition count, VTC. The major constraint on this design was to keep the algorithm simple enough to be easily implemented on the F8 microprocessor. At one extreme, the algorithm could entail stepping through every value of N and doing a simple comparison of the present value of VTC and the maximum preceding value of VTC (called MTC) to find the VTC peak. In fact this method was used in gathering the data for Chapter 3. The obvious drawback, however, in implementing this procedure in an operational scanner system is the fact that, since each sample requires one scan line of video, a total of 1024 video lines would have to be dedicated to thresholding. With the scanner on the move, that means the CALIBRATION PATTERN would need to be over five inches wide! One can immediately see a way to decrease the number of video lines by recognizing that only a certain span of N (labeled RV in Chapter 3) contains significant VTC information worth sampling.

(1) Recall from Figure 3.1 that when $N = 0$, the voltage threshold level is greater than the analog video signal which prevents any digital encoding of the video information. VTC therefore is zero until the threshold encounters the span of significant analog

(1) Since the analog video information generally covers a span of 200 to 300 millivolts, and each incremental change in N equates to a one-millivolt shift in the threshold level, the total number of video lines required could be reduced to around 200 to 300. The width of the CALIBRATION PATTERN now must be 1 to 1.5 inches which is still unacceptably large. At the same time the range of N sampled is dangerously small, which would limit the ATC's ability to adapt to drastic changes. So the research centered on finding a feasible algorithm that could cover the largest range of N in the least number of samples. The algorithm explored for implementation with the ATC is detailed below.

A. SUCCESSIVE APPROXIMATION

Under the assumption that the VTC-versus- N curve to be sampled is relatively smooth and has the general shape of Figure 3.1(C), a fairly straightforward approach can be used to pinpoint the VTC peak. When the automatic thresholding sequence is initiated, the idea is to start with a large step size (increments) for N and take a small number of VTC samples over the entire range of N , [0 to 1024]. This will be called the first pass. Since keeping the step size a binary multiple greatly simplifies programming, the initial step size, S_1 , was chosen as 128. Referring to Figure 5.1, we see that this divides the range [0 to 1024] into eight segments. For reasons that will soon

signal. VTC will again be zero once the threshold level is less than the smallest value of the analog signal.

-----PASS 1

N	VTC
128	1
256	1
384	130
512	117
640	0
768	0
896	0

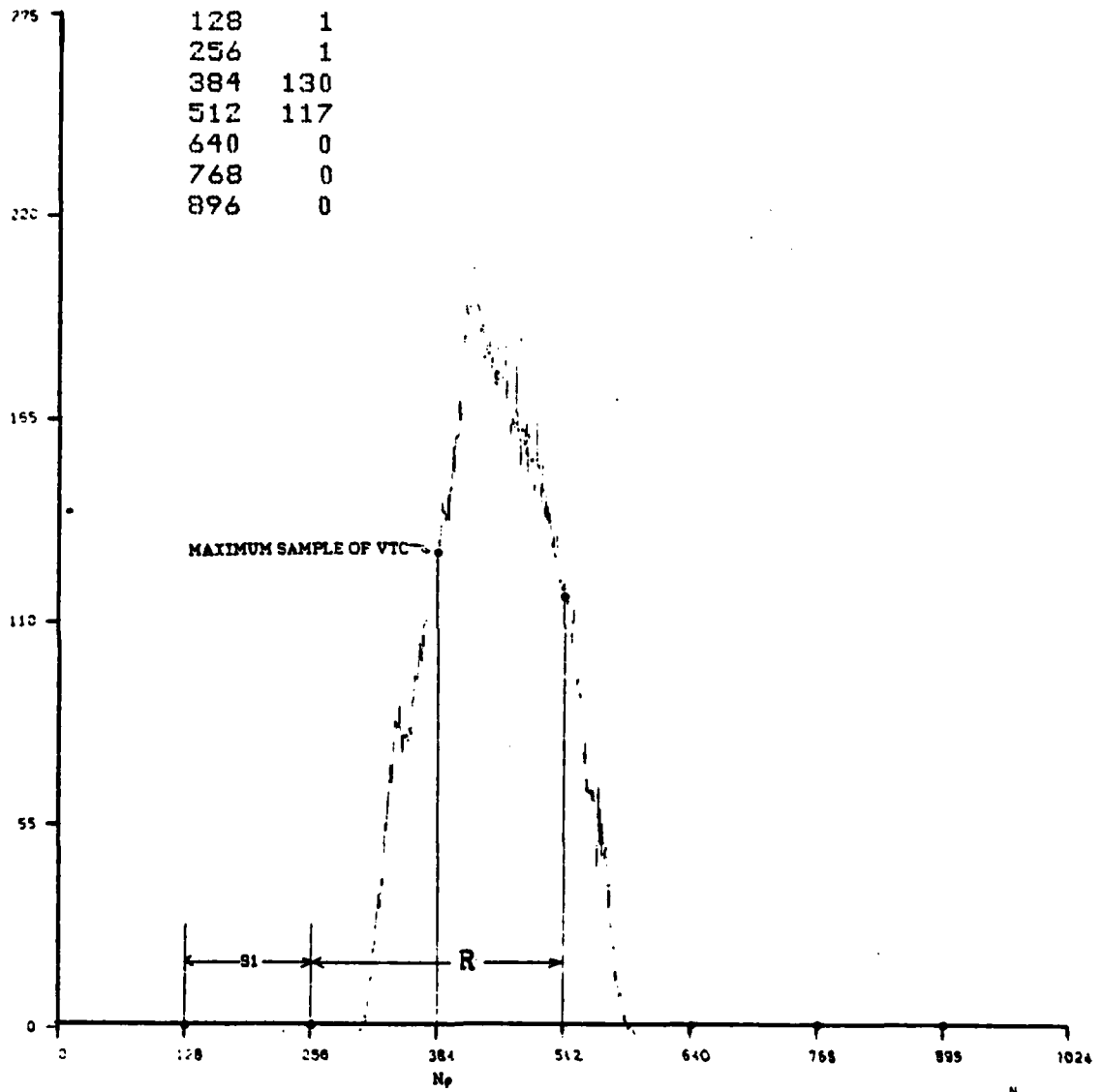


FIGURE 5.1 FIRST PASS OF ATC SAMPLING ALGORITHM QSET1

become apparent, the end points, $N = 0$ and $N = 1024$, are ignored, and seven samples of VTC are taken beginning at $N = 128$. For those samples, the value of N giving the maximum VTC, called N_p , becomes the middle of a new range, R , to be sampled with the end points defined as $(N_p - S_1)$ and $(N_p + S_1)$, as shown in Figure 5.2. Note that $R = 2 \times S_1$. The new range R is now divided into eight segments by using a new step size, S_2 , which turns out to be equal to $S_1/4$. Again end points are ignored and seven samples are taken at the points shown in Figure 5.2. (1) Repeating the procedure to the limit, it can be seen from Figures 5.3 and 5.4 that a total of four passes or 28 video lines are required to pinpoint the VTC peak within one millivolt. With each video line being 0.05 inch wide, the procedure requires 0.14 inch of CALIBRATION PATTERN to find the optimum threshold value. This width is considered to be acceptable in the context of the amount of margin of the original document required for threshold-setting purposes.

The complete algorithm summarizing the above procedure is flowcharted in Figure 5.5. Block 1 initializes the necessary registers for the overall algorithm, and Block 2 initializes the video line counter for each new pass of 7 video lines. Blocks 3

(1) Notice that in this case, the end points were sampled in the first pass and therefore do not need to be re-sampled in the second pass. Although the discarded endpoints of the second pass ($N = 256$ and $N = 512$) do not provide an exact analogy to the discarded endpoints of the first pass ($N = 0$ and $N = 1024$), it is still easy to see that excluding $N = 0$ and $N = 1024$ does not preclude the segments [0 to 128] or [896 to 1024] from being sampled in a subsequent pass if necessary. In this manner, each pass consists of identical procedures.

-----P. SS 2

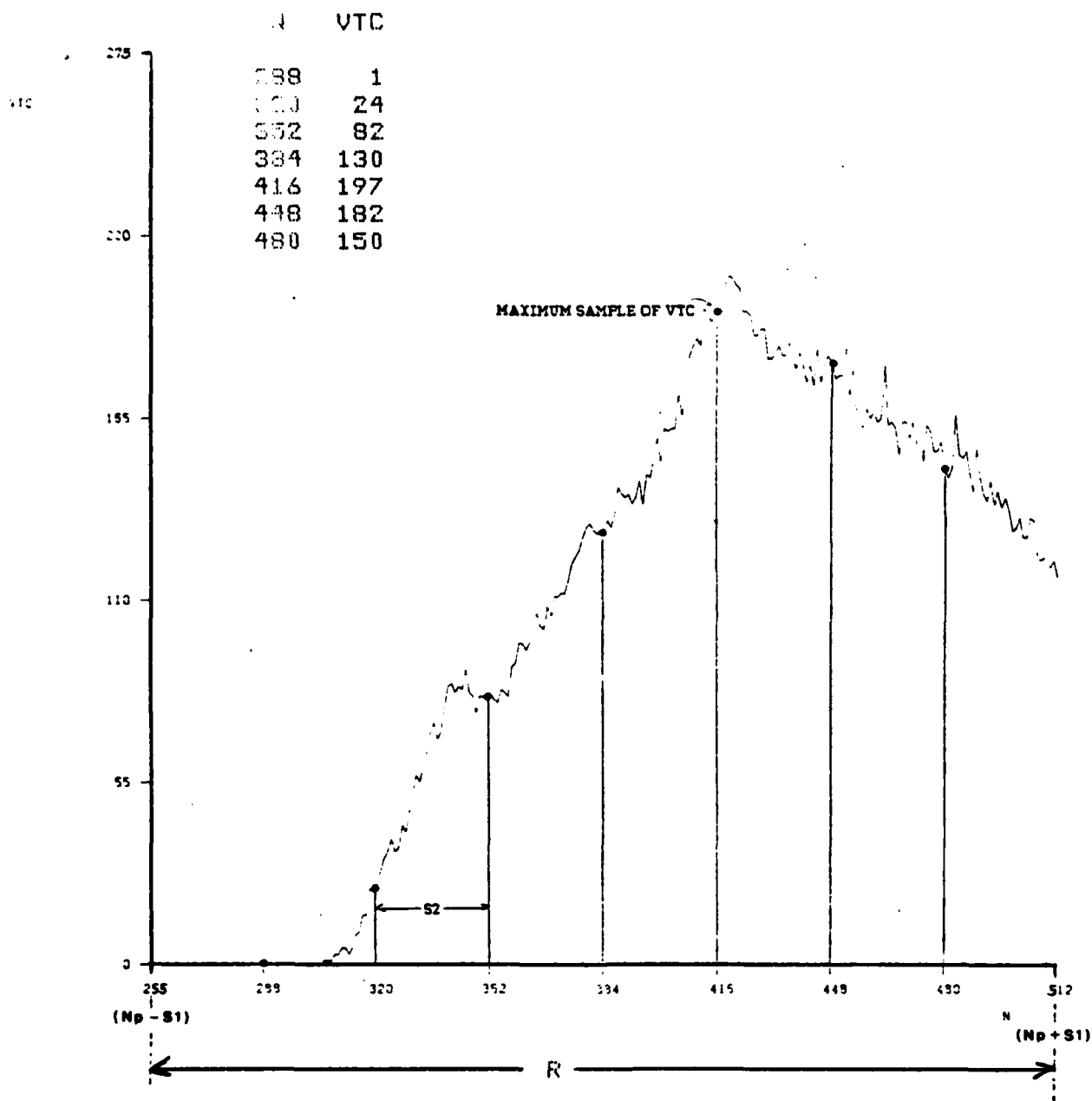


FIGURE 5.2 SECOND PASS OF ATC SAMPLING ALGORITHM QSET1

-----PASS 3

N	VTC
392	139
400	152
408	184
416	197
424	197
432	185
440	181

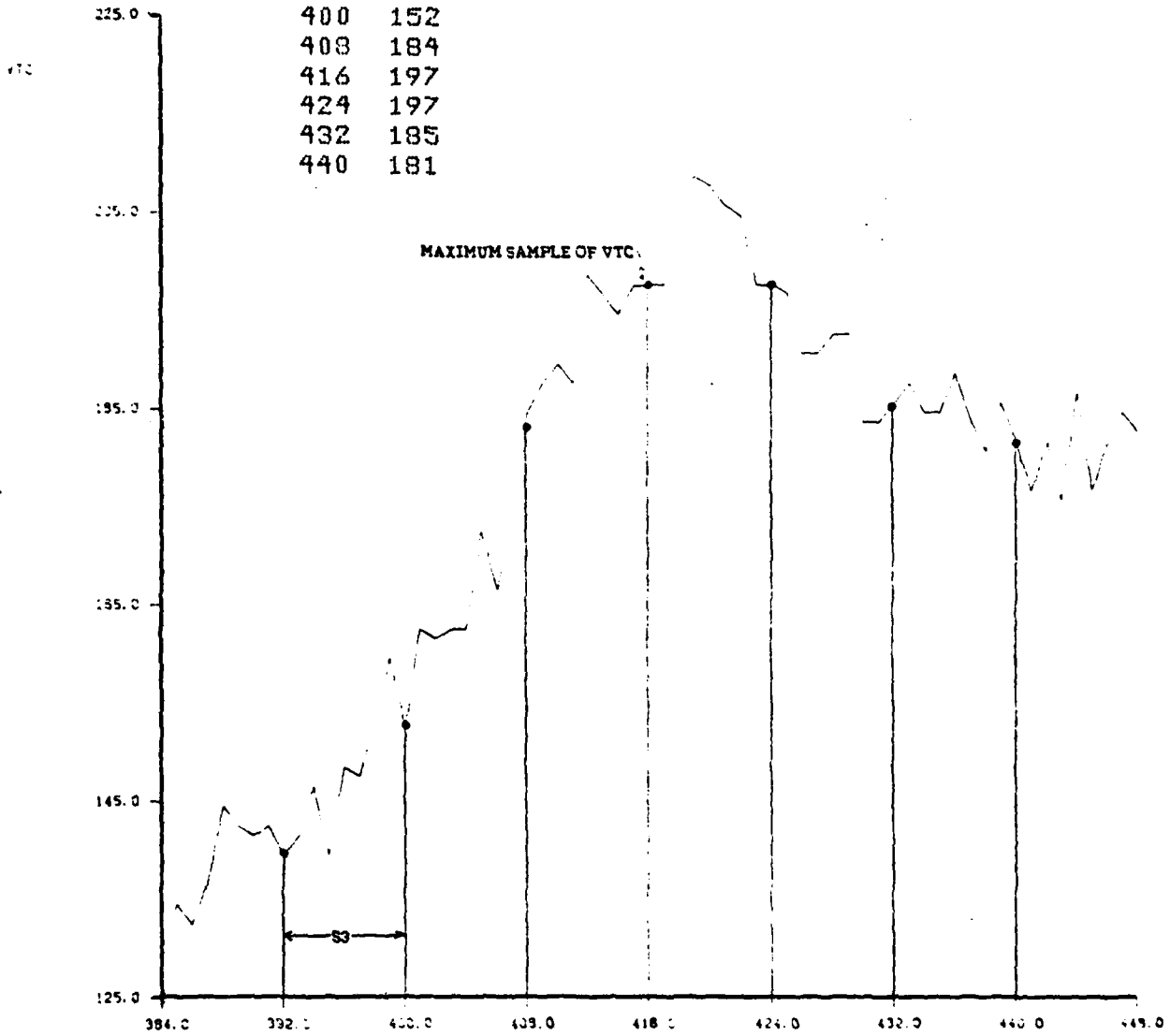


FIGURE 5.3 THIRD PASS OF ATC SAMPLING ALGORITHM QSET1

-----PASS 4

N	VTC
410	189
412	198
414	194
416	197
418	206
420	207
422	204

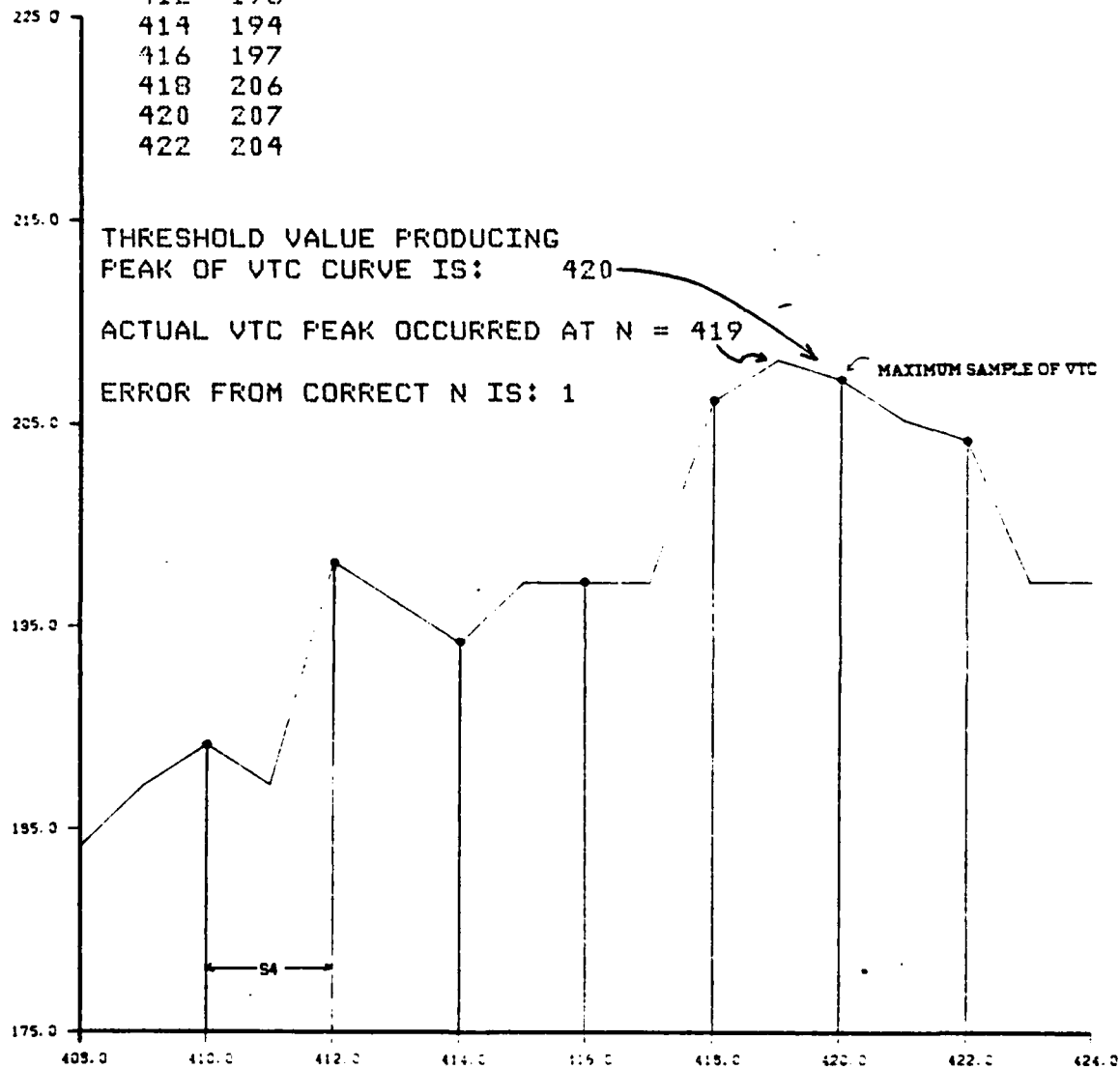


FIGURE 5.4 FOURTH PASS OF ATC SAMPLING
ALGORITHM QSET1

through 7 are executed for every line of video. In Block 3 the VIDEO COUNTERS of Figure 4.1 are set to zero, and in Block 4, N is incremented by the existing step size. When PRINTLINE goes active signifying valid video is being transmitted, the digital black/white transitions are counted in Block 5. (1) At the end of the video line, the number of black/white transitions obtained is subtracted from the previous maximum number of transitions. If the result is negative, this means that the VTC just obtained is greater than any VTC previously obtained. Therefore this value of VTC is retained in MTC as the new maximum transition count encountered thus far, and the value of N producing this maximum VTC is also saved. Block 7 counts the number of video lines taken in a particular pass, and the flow is transferred back to Block 3 until the 7 lines of one pass have been completed. For each new pass, Block 8 adjusts the starting value of N for the new range to be sampled, alters the step size, and keeps track of the number of passes executed. At the end of the fourth pass, Block 9 loads the N value that produced the overall maximum VTC into the Threshold Level Generator. This threshold value is used for the entirety of the page being scanned. The algorithm as presented is called QSET1, and computer simulations of QSET1 on actual VTC curves are detailed in Appendix C.

(1) It is important in understanding the sequencing and timing of the algorithm that Block 5 is the only block that is executed during the transmission of valid video information as depicted in Figure 2.1(B). All remaining blocks are executed in the relatively short time gap between successive video lines.

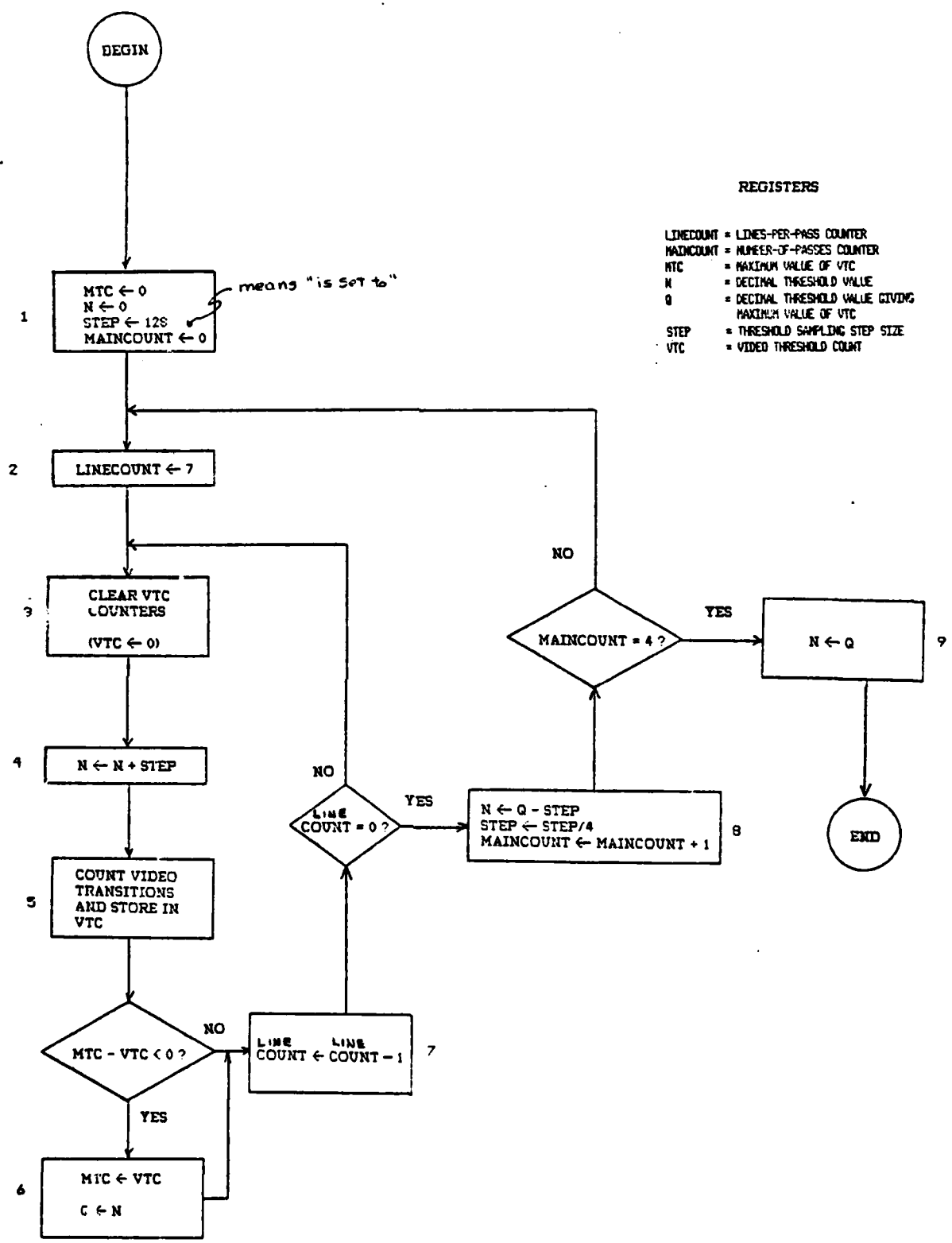


FIGURE 5.5 FLOWCHART OF QSET1 ALGORITHM

B. SAMPLING CONSIDERATIONS

Of prime importance in utilizing a sampling technique such as QSET1 is proper consideration of the initial step size, S_1 . Specifically, if the range of valid VTC information, RV , is less than S_1 , then it is possible for all valid VTC information to reside between samples of the first pass as in Figure 5.6. The only instances where the range RV was found to be less than 128 using ECP A were with one-lamp illumination and with the darker paper colors: orange, red, green, brown, and blue. (Remember that f -stop = 5.6 was used throughout the research.) Still, in these cases, the algorithm has the potential of breaking down in its search for the VTC maximum. (1)

The three alternatives to solving the problem of dealing with a small span of VTC information are to either change the voltage range of the TLG, implement a different sampling algorithm, or modify the parameters of the QSET1 algorithm. To maintain a basis for reference throughout this research, the TLG voltage range was not altered although in practice this might be the most reasonable solution. Different sampling algorithms were also considered but rejected due to the additional programming complexity involved. Therefore due to the simplicity of implementation with a microprocessor, the latter alternative was

(1) It should now be clear why a single-frequency CALIBRATION PATTERN at the Nyquist rate is not a good choice as implied in Chapter 3. The resultant impulse-like VTC curve having a very small RV would require a prohibitively small initial step size, S_1 , to detect.

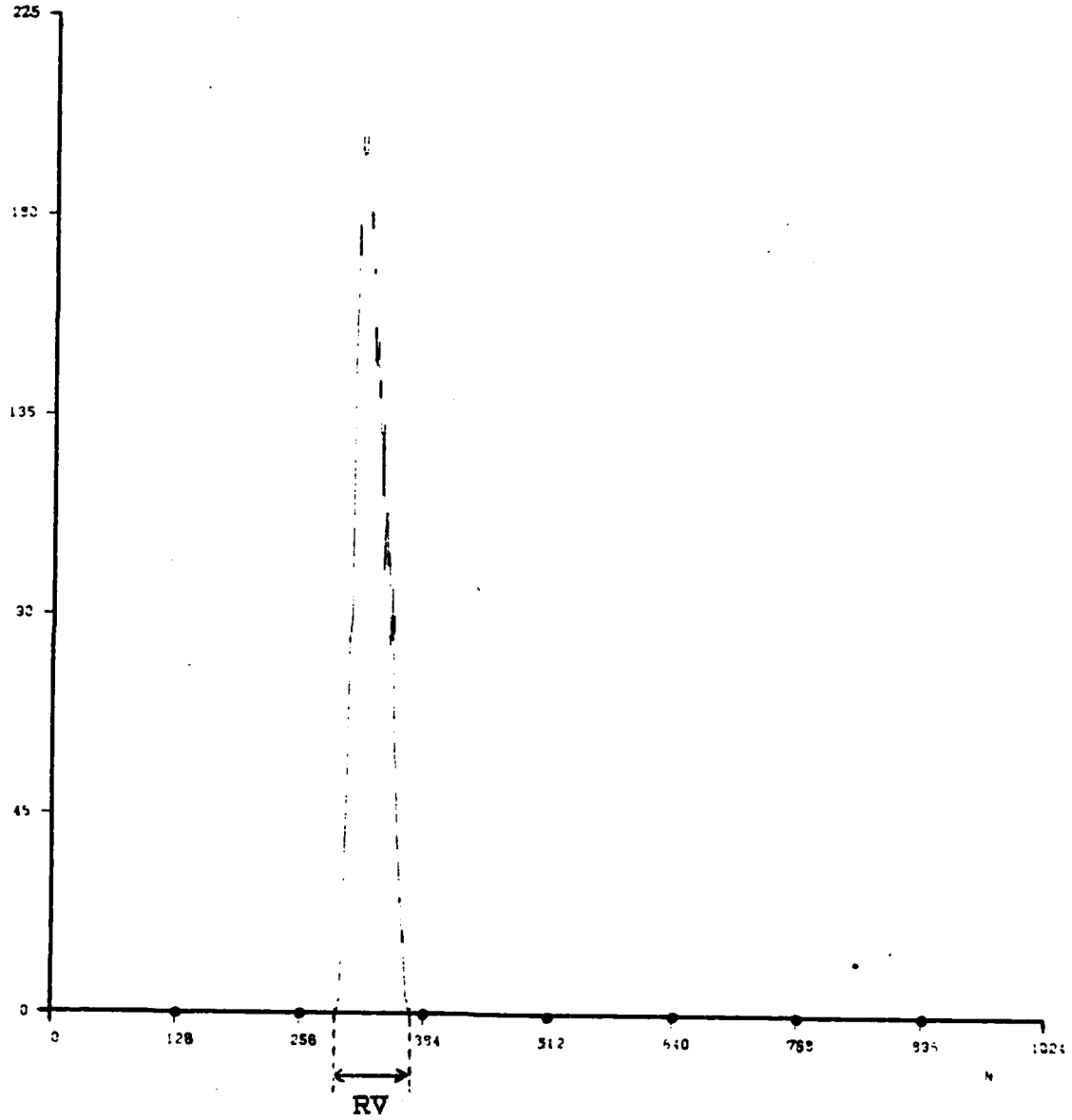


FIGURE 5.6 VTC CURVE PRODUCED FROM SCANNING ECP A ON A RED BACKGROUND. (VTC CURVE IS NEVER FOUND BY QSET1 BECAUSE RV FALLS BETWEEN SAMPLES)

preferred for rectifying the problem. Working within the framework of QSET1, the challenge becomes one of decreasing the initial step size, S_1 , with minimal penalties. Of all experimental observations using ECP A, the smallest span of N over which all VTC values were generated was $RV = 67$, resulting from navy blue paper. So one possibility is to choose $S_1 = 64$, dividing the range [0 to 1024] into 16 segments, and collecting 15 samples on the first pass. Maintaining 15 samples on subsequent passes results in three passes required in all, or 45 lines of video to set the optimum threshold. Subsequent step sizes would be obtained by dividing by 8:

$$\begin{aligned} S_2 &= S_1/8 = 8 \\ S_3 &= S_2/8 = 1 \end{aligned}$$

Another possibility is to choose $S_1 = 64$ but only collect 7 samples per pass as QSET1 prescribes. This requires the initial sampling range to be cut from 1024 to 512 samples. Maintaining 7 samples per pass results in four passes, or a total of 28 video lines required. Subsequent step sizes are obtained as in QSET1:

$$\begin{aligned} S_2 &= S_1/4 = 16 \\ S_3 &= S_2/4 = 4 \\ S_4 &= S_3/4 = 1 \end{aligned}$$

In an effort to preserve the small number of video lines used by QSET1, the latter option was chosen. The major compromise was the halving of the overall range of N to be sampled. The impact of this compromise was minimized by using the knowledge of the behavior of the analog video signal to select the starting and ending values of the sampling range as $N = 128$ and $N = 640$.

Implemented in the algorithm, QSET2, these choices produced robust performance throughout the range of abnormal paper colors and lighting conditions. The flowchart for QSET2 is identical to that of QSET1 in Figure 5.5 except for Block 1 which becomes:

MTC ← 0
N ← 128
STEP ← 64
MAINCOUNT ← 0

Another sampling consideration deals with the performance of the QSET algorithm with VTC curves having peaks that are less well-defined. The primary factor that can cause an obscuration of the actual VTC peak is the uncertainty discussed in Chapter 3 and depicted in Figure 3.18. As long as the degree of uncertainty is relatively small, as is the case with ECP A in Figure 3.6(A), the algorithm is quite successful in locating the peak. But if the uncertainty is a significant component of the VTC curve as in Figure 3.12, the results of the algorithm search are not as consistent; the final N value produced by the algorithm becomes more a function of how the samples fall along the VTC curve. These effects are covered more extensively in Appendix C.

C. INCORPORATION WITH SCANNER PRINT SEQUENCE

Once the QSET algorithm was perfected, the next step consisted of adding the necessary software to the F8 program, EOPS (electro-optical page scanner). Since all pertinent F8 source codes are contained in Appendix B, the discussion here will be restricted to the block level. Figure 5.7 is a

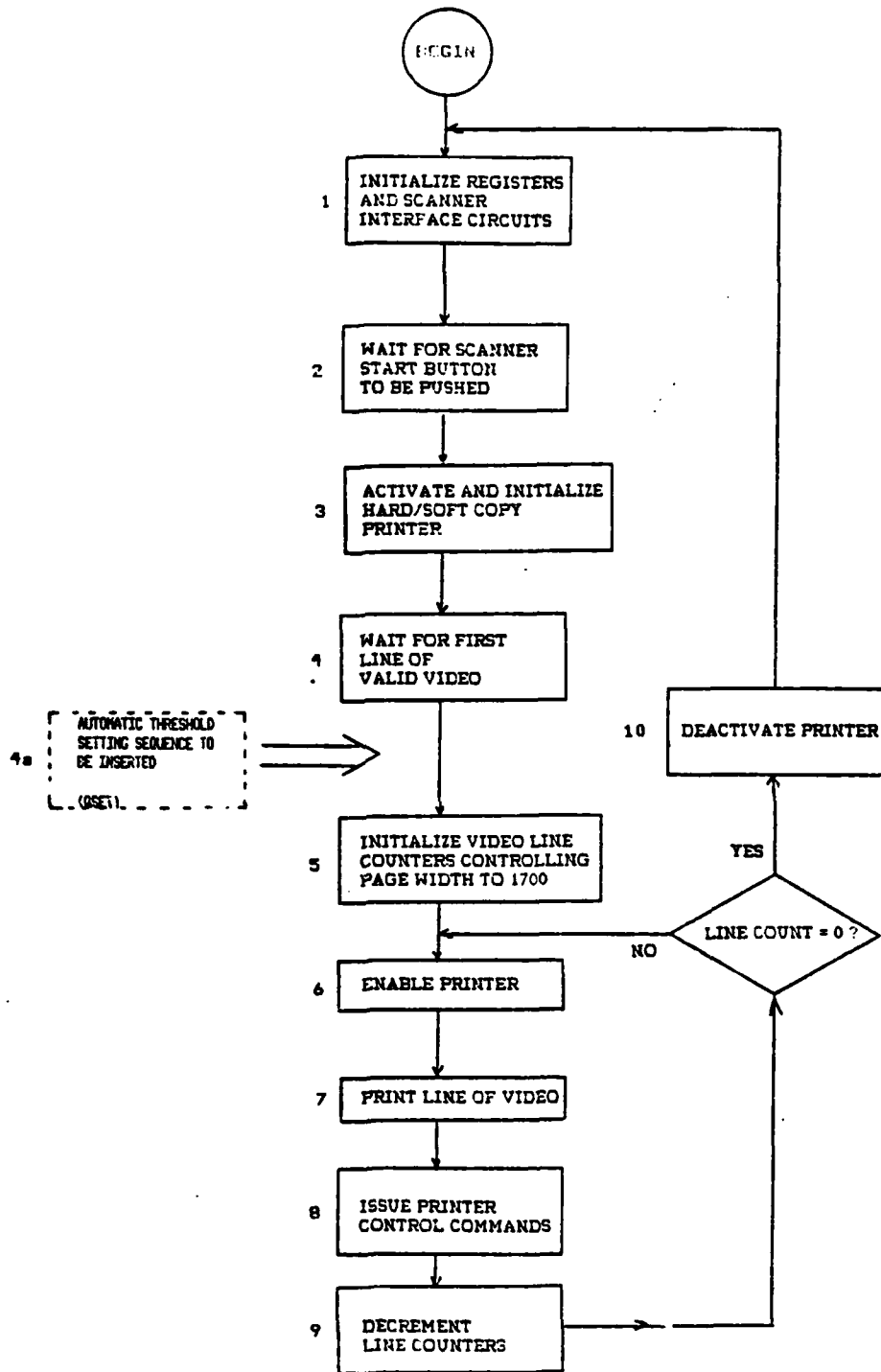


FIGURE 5.7 SIMPLIFIED FLOWCHART OF EXISTING F8 SOFTWARE (EOPs) FOR THE SCANNER

simplified flowchart of the existing scanner algorithm. As stated in Chapter 3, placement of the CALIBRATION PATTERN in the left-most margin allows the first lines of video to provide the necessary information for threshold-setting purposes. Therefore it was necessary for the ATC sequence to be located between Blocks 4 and 5 of Figure 5.7 in order to catch the first lines of valid video. This configuration also turned out to be the most advantageous in terms of software modifications required. With Block 4a included in the flow, the sequence of scanning a document now becomes:

1. After positioning the document, the operator pushes the scanner start button.
2. A start-up delay of just over 1.5 seconds is initiated which allows the fluorescent lights to preheat and the phase-locked loop motor control to stabilize. This delay is accomplished by counting a preset number of pulses generated by the phase-locked loop rate-feedback wheel. Video information is ignored during this time because of the status of the signal PRINTLINE.
3. At the termination of the start-up delay, PRINTLINE goes active, signalling that valid video is now available.
4. The automatic threshold-setting sequence begins and uses 28 video lines to establish the optimum threshold level.
5. Once the optimum threshold is locked in, the VIDEO LINE COUNTERS are set to 1700, giving a page width of 8.5 inches (200 lines/inch).
6. As the video lines are shot, they are printed in real time with the F8 providing the necessary pacing for the printer.
7. When 1700 lines have been read, the printer is shut down automatically, and the F8 software resets. The scanner mechanical assembly is retracted to its starting point upon activation of a limit switch beyond the right-most margin.

For future research purposes, two new versions of EOPS were produced. EOPS1, containing QSET1, provides ATC that samples the entire range of N , [0 to 1024]. EOPS2, containing QSET2, provides ATC that samples the range of N , [128 to 640].

Ch 5

Additional user-oriented features added to EOPS1 and EOPS2 are detailed in Appendix B.

CHAPTER 6

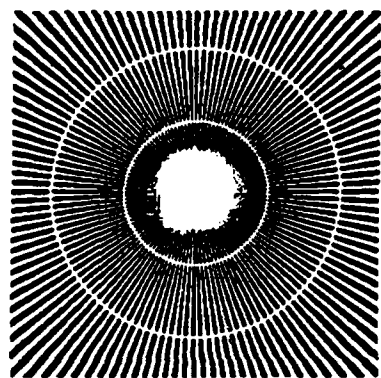
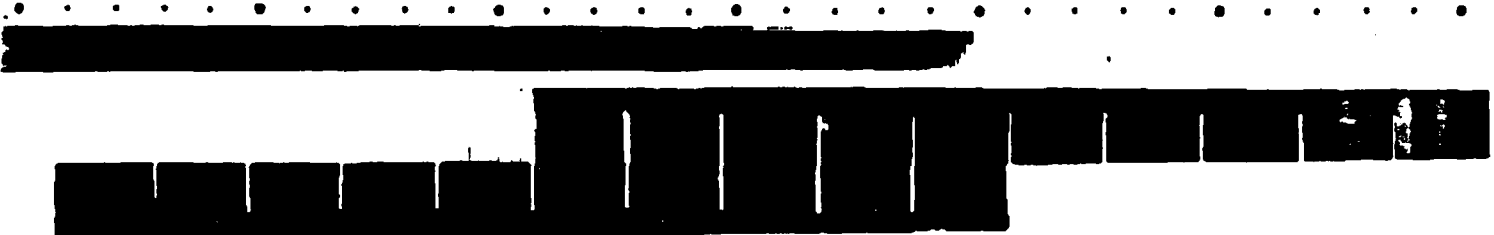
CONCLUSIONS AND RECOMMENDATIONS

A. GENERAL RESULTS

The performance of the scanner with automatic threshold control was considered to be excellent, especially in the context of proving the validity of the ATC concept that was developed. Xerox copies of scanner printouts are contained in this chapter, and if degradation due to xeroxing is ignored, the results are very good. Figures 6.1 to 6.5 represent consecutive scanner outputs of the same image with the automatically-chosen threshold value noted. Due to the uncertainty discussed in Chapter 3, each threshold value is somewhat different. Still, it can be seen that every copy possesses a high degree of quality, thereby demonstrating the consistency of the ATC. Observe, for example, the legibility of the 6-point type at the lower left of each reproduction of the IEEE Test Chart. Microscopic inspection of these scanner outputs revealed resolutions very close to 200 lines/inch.

Figures 6.6 to 6.8 were produced with EOPS2 and only one fluorescent light providing illumination. Even under the degraded lighting conditions, the ATC was able to select the optimum threshold and produce a very acceptable output. Again note the 6-point type in Figure 6.7 is quite readable.

Figure 6.9 is the result of scanning a transparency of the IEEE Facsimile Test Chart with red paper as a background. Again the threshold level chosen was considered the best possible under



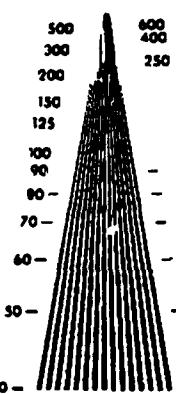
28	25
32	22
36	20
40	18
45	16

NMA MICROFONT QJKLPYZ
 6BSI2GH5D4X7U3W8V9E
 PGR45DERUVE70FG8STHJUNOWABYZ
 3KLM12C

ABCDEFGHIJKLMNOPS
 TUVWXYZ 0123456789
 '-[]%&'()* ASA OCR-A

ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890 Elite



ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890 Spartan Medium 10 pt

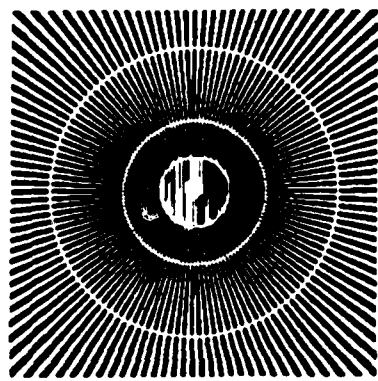
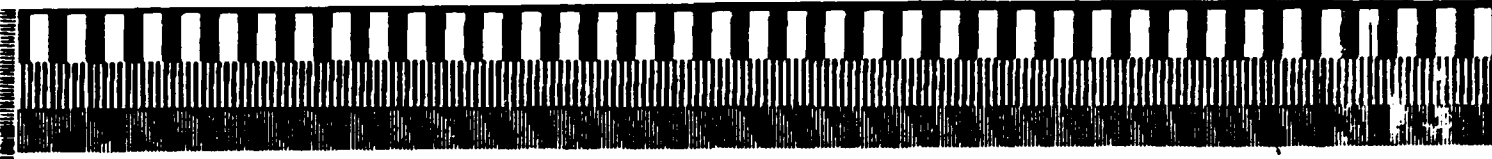
ABCDEFGHIJKLMNOPS
 TUVWXYZabcdefghijklmnopqr
 stuvwxyz1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975
 FACSIMILE TEST CHART
 FIGURE 6.1

SCANNER OUTPUT UNDER NORMAL CONDITIONS
 (WARM WHITE FLUORESCENTS)
 THRESHOLD AUTOMATICALLY SET AT N = 384





28	2.5
32	2.2
36	2.0
40	1.8
45	1.6

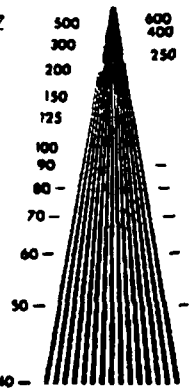


NMA MICROFONT GJKLPYZ
 6BSI2GH5D4X7U3W8V9E
 PGR45DE4UV67DFG8STHIJNOWXABYZ
 3KLM12C

ABCDEFGHIJKLMNOPS
 TUVWXYZ 0123456789
 '-[]%?JYH ASA OCR-A

ABCDEFGHIJKLMNOPQRSTU
 WXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Elite



ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 6 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 6 pt



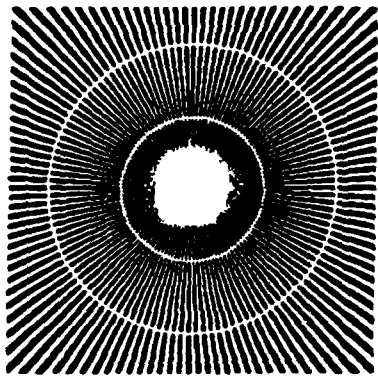
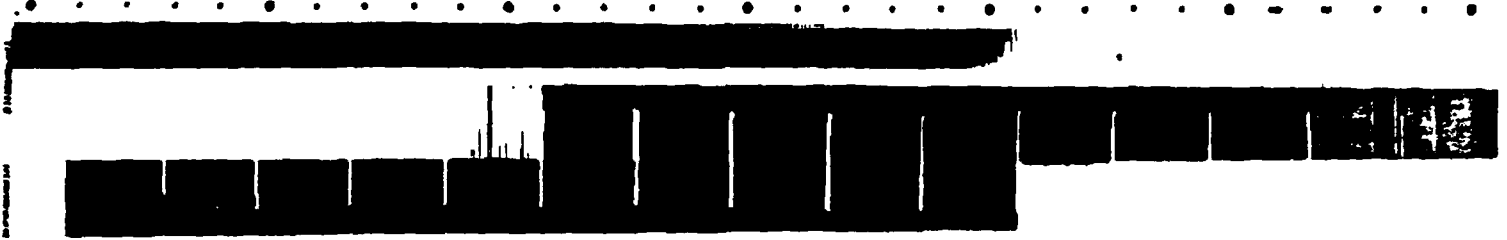
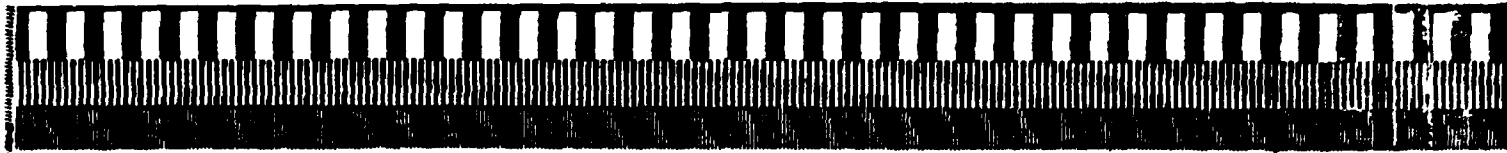
ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 12 pt

IEEE Std 167A-1975
 FACSIMILE TEST CHART
 FIGURE 6.2
 SCANNER OUTPUT UNDER NORMAL CONDITIONS
 (WARM WHITE FLUORESCENTS)
 THRESHOLD AUTOMATICALLY SET AT N = 403

1.4
 1.6
 1.8
 2.0
 2.2
 2.5
 2.8
 3.2
 3.6
 4.0
 4.5
 5.0
 5.6
 6.3
 7.1
 8.0
 9.0
 10.0
 11.2
 12.5
 14.1
 16.0
 18.0
 20.0
 22.5
 25.0
 28.0
 32.0
 36.0
 40.0
 45.0
 50.0
 56.0
 63.0
 71.0
 80.0
 90.0
 100.0
 112.0
 125.0
 141.0
 160.0
 180.0
 200.0
 225.0
 250.0
 280.0
 320.0
 360.0
 400.0
 450.0
 500.0



2.8	2.5
3.2	2.2
3.6	2.0
4.0	1.8
4.5	1.6

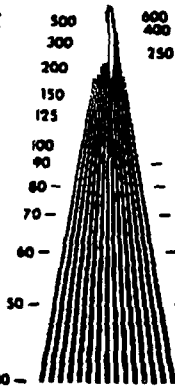


NMA MICROFONT QJKLPYZ
 6BSI2GH5D4X7U3W8V9E
 PGR45DFHJUV67JFG9STHIJNOW8ABYZ
 3KLM12

ABCDEFGHIJKLMNOPS
 TUVWXYZ 0123456789
 !-{}?@#H ASA OCR-A

ABCDEFGHIJKLMNQRSTU
 VXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Elite



ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 6 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ
 1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975

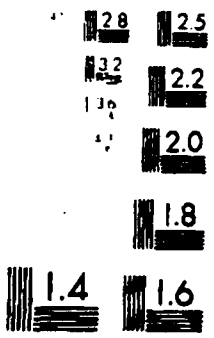
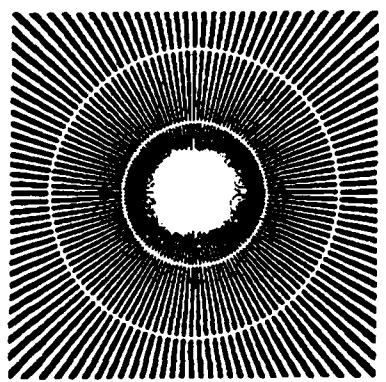
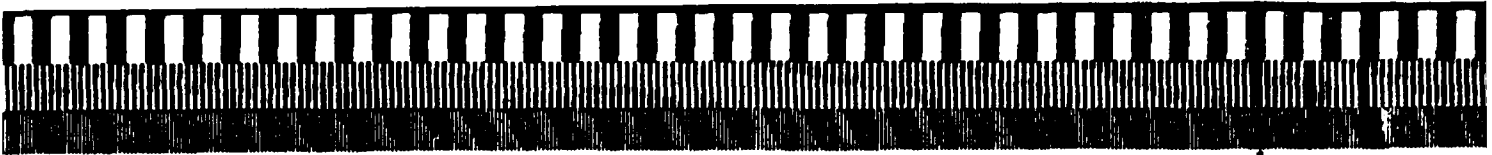
FACSIMILE TEST CHART

FIGURE 4.3

SCANNER OUTPUT UNDER NORMAL CONDITIONS
 (WARM WHITE FLUORESCENTS)
 THRESHOLD AUTOMATICALLY SET AT N = 393

1.4
1.6
1.8
2.0
2.2
2.5
2.8
3.2
3.6
4.0
4.5

print
with
right

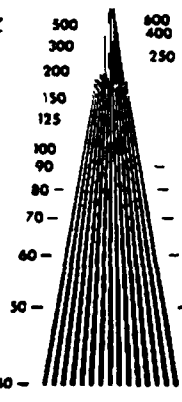


NMA MICROFONT QJKLPYZ
 6BSI2GH5D4X7U3W8V9E
 FGR45DFILV670FG8STHEJNDWABYZ
 3KLM12L

ABCDEFGHIJKLMNQPORS
 TUVWXYZ 0123456789
 '-[]%?JYH ASA OCR-A

ABCDEFGHIJKLMNQPQRSTU
 WXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Elite



ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

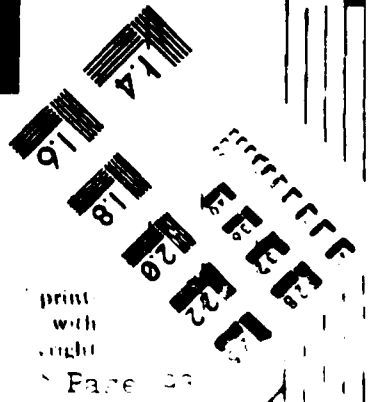
ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNQPQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975
 FACSIMILE TEST CHART

FIGURE 4.4
 SCANNER OUTPUT UNDER NORMAL CONDITIONS
 (WARM WHITE FLUORESCENTS)
 THRESHOLD AUTOMATICALLY SET AT N = 360



print with light
 Page 36

AD-A125 316

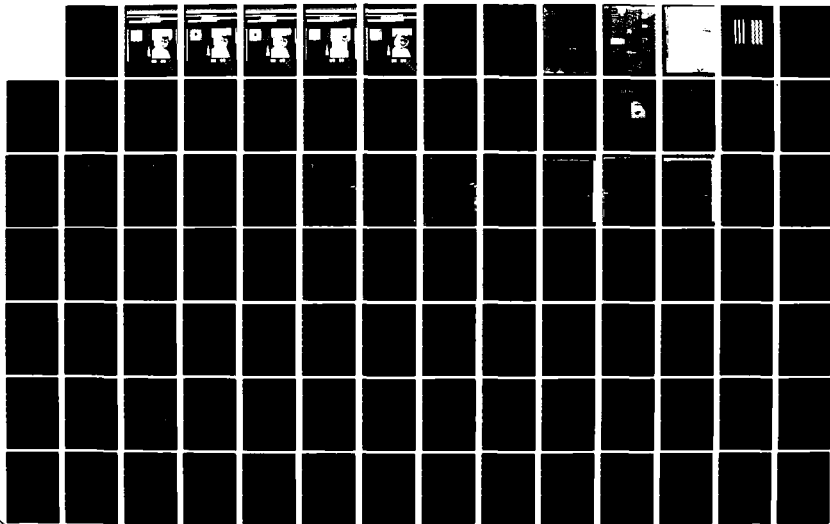
AUTOMATIC THRESHOLD DESIGN FOR A BOUND DOCUMENT SCANNER
(U) AIR FORCE INST OF TECH WRIGHT-PATTERSON AFB OH
B J STANTON DEC 82 AFIT-CI/NR-82-71T

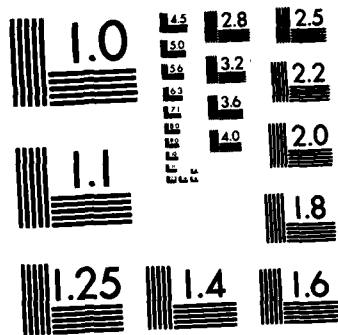
2/3

UNCLASSIFIED

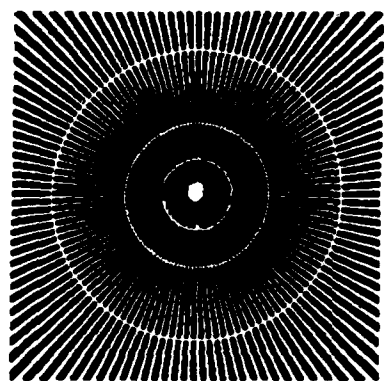
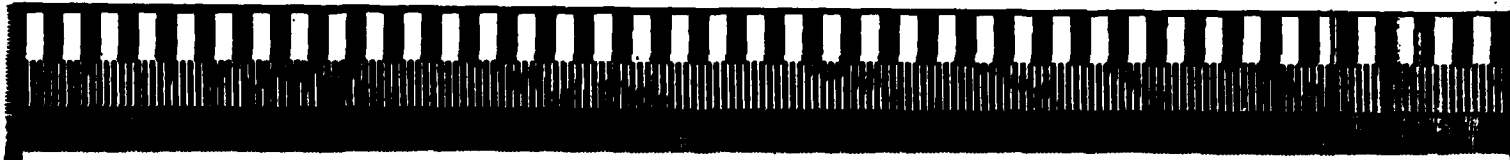
F/G 17/2

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A



2.8	2.5
3.2	2.2
3.6	2.0
4.0	1.8
1.4	1.6

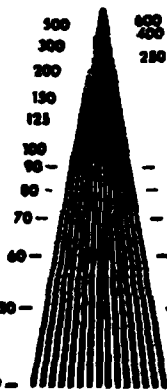


NMA MICROFONT QJKLPYZ
 6BS12GH5D4X7U3W8V9E
 PQR45DE9UV670FG8STHIJNOWKABYZ
 3KLM12C

ABCDEFGHIJKLMNOPS
 TUVWXYZ 0123456789
 '-{}%&@# ASA OCR-A

ABCDEFGHIJKLMNQRSTU
 VWXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Elite



ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 6 pt

ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNQRSTUWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975

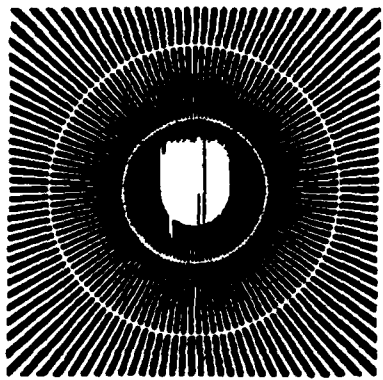
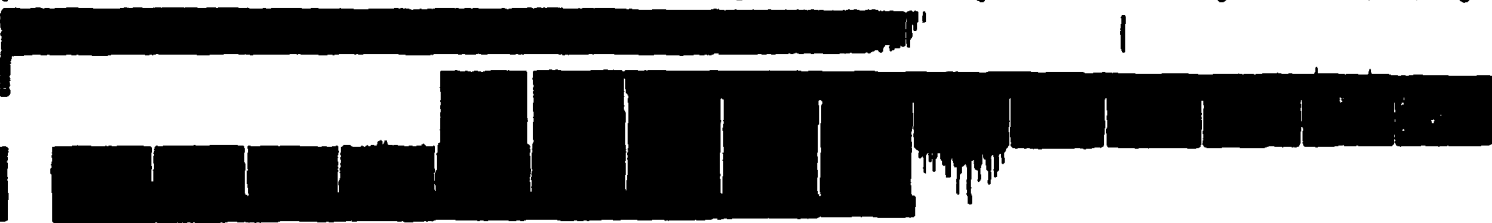
FACSIMILE TEST CHART

FIGURE 6.5

SCANNER OUTPUT UNDER NORMAL CONDITIONS
 (COOL WHITE FLUORESCENTS)
 THRESHOLD AUTOMATICALLY SET AT N = 395

1.4
1.6
1.8
2.0
2.2
2.5
2.8
3.2
3.6
4.0

print-
with
right
Page 94



2.8 2.5
 2.2
 2.0
 1.8
 1.4 1.6



NMA MICROFONT QJKLPYZ
 6BSI2GH5D4X7U3W8V9E
 P... .. THE HOWARD
 IN...

ABCDEFGHIJKLMNOPS
 TUVWXYZ 0123456789
 '-{ } % ? # \$ % ^ & * -

ABCDEFGHIJKLMNOPS
 TUVWXYZ abcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPS
 TUVWXYZ abcdefghijklmnopqr
 stuvwxyz1234567890 Elite



ABCDEFGHIJKLMNOPS
 TUVWXYZ 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ 1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMNOPS
 TUVWXYZ 1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975

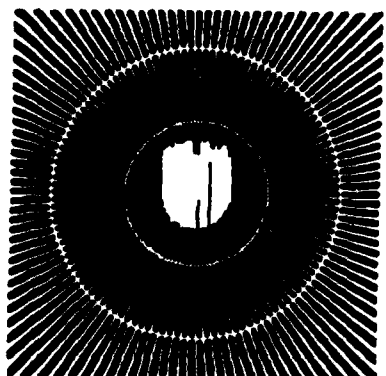
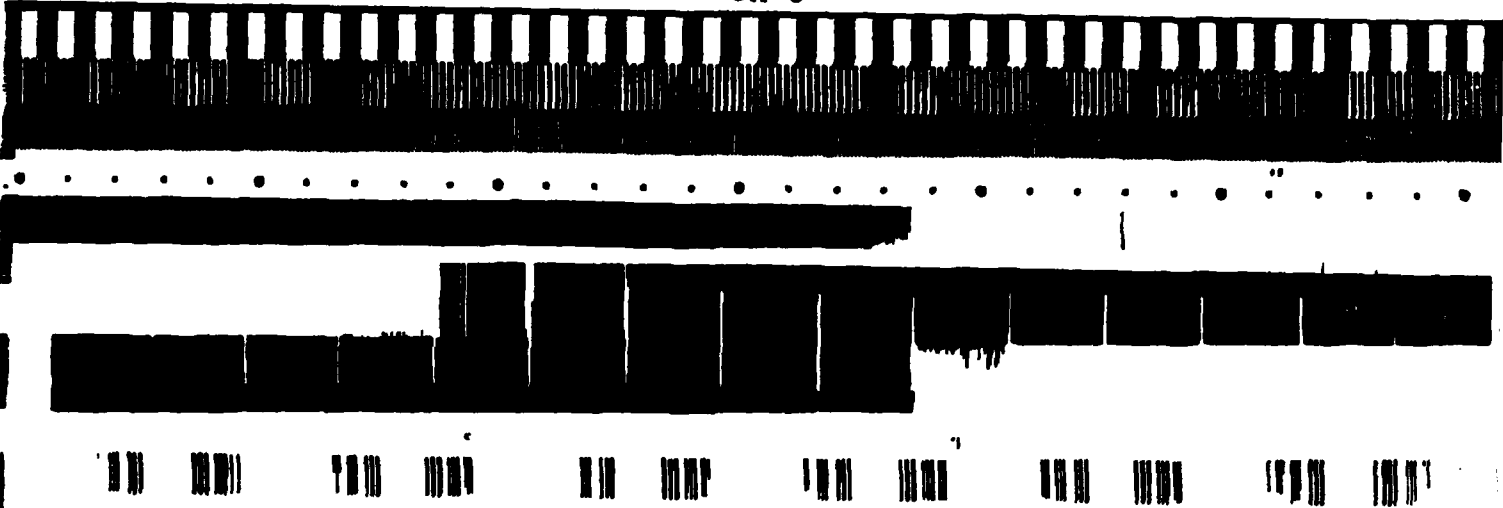
FACSIMILE TEST CHART

FIGURE 6.6

SCANNER OUTPUT WITH ONLY ONE COOL WHITE
 FLUORESCENT LIGHT PROVIDING ILLUMINATION
 THRESHOLD AUTOMATICALLY SET AT N = 303

14
 16
 18
 20
 22
 24
 26
 28
 30
 32
 34
 36
 38
 40
 42
 44
 46
 48
 50
 52
 54
 56
 58
 60
 62
 64
 66
 68
 70
 72
 74
 76
 78
 80
 82
 84
 86
 88
 90
 92
 94
 96
 98
 100

Printed with
 cyanide
 Page 95

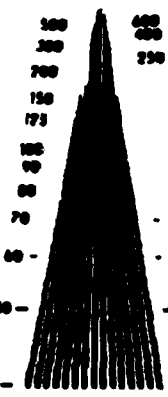


2.5
2.2
2.0
1.8
1.6
1.4



NMA MICROFONT QJKLPYZ
6BSI2GH5D4X7U3W8V9E

ABCDEF GHIJK LMNOPQRS
TUVWXY Z 0123456789
!-@%&'()* +,-./:;<=>? [\] ^ _ ` { | } ~ :
ABCDEF GHIJK LMNOPQRSTU
VWXYZ abcde fgh i jklmno pqr
stuvwxyz 1234567890 PICA
ABCDEF GHIJK LMNOPQRSTU
VWXYZ abcde fgh i jklmno pqr
stuvwxyz 1234567890 Elite



Small text block providing technical specifications or notes for the test chart.

ABCDEF GHIJK LMNOPQRSTU
VWXYZ abcde fgh i jklmno pqr
stuvwxyz 1234567890 Spartan Medium 8 pt

ABCDEF GHIJK LMNOPQRSTU
VWXYZ abcde fgh i jklmno pqr
stuvwxyz 1234567890 Spartan Medium 10 pt

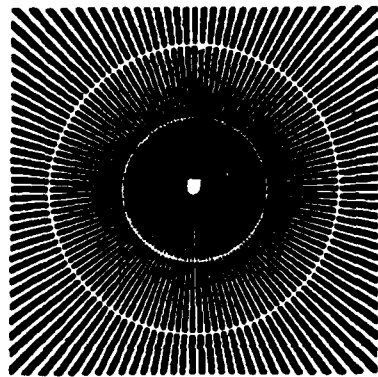
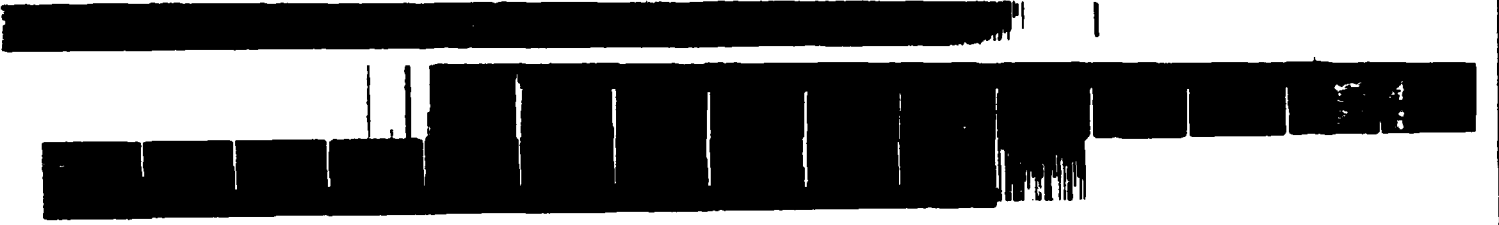
ABCDEF GHIJK LMNOPQRSTU
VWXYZ abcde fgh i jklmno pqr
stuvwxyz 1234567890 Spartan Medium 2 pt



IEEE Std 167A-1975
FACSIMILE TEST CHART

FIGURE 6.7
SCANNER OUTPUT WITH ONLY ONE COOL WHITE
FLUORESCENT LIGHT PROVIDING ILLUMINATION
THRESHOLD AUTOMATICALLY SET AT N = 303

Resolution test values (1.4, 1.6, 1.8, 2.0, 2.2, 2.5) and other technical parameters.



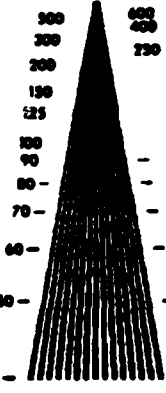
2.8 2.5
 2.2 2.0
 1.8
 1.6 1.4

NMA MICROFONT GJKLPYZ
 6BSI2GH3D4X7U3W8V9E
 PQR45DE9UV670FG8STHIJNOMXABYZ
 3KLM12C

ABCDEFGHIJKLMNOPQRS
 TUVWXYZ 0123456789
 '-{ } % ? # \$ % ^ & * - A

ABCDEFGHIJKLMNOPQRSTU
 VWXYZabcdefghijklmnopqr
 stuvwxyz1234567890PICA

ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Elite



ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 10 pt

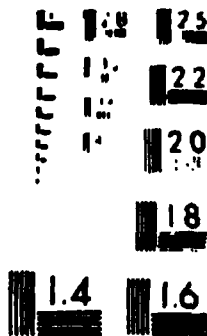
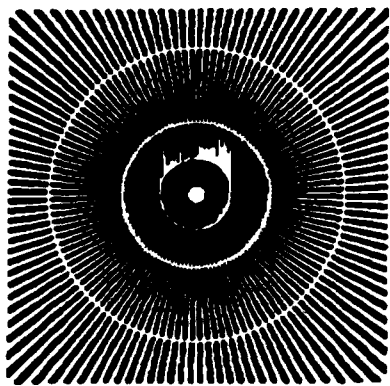
ABCDEFGHIJKLMNOPQRSTUVWXYZ
 abcdefghijklmnopqrstuvwxyz
 1234567890 Spartan Medium 12 pt



IEEE Std 167A-1975
 FACSIMILE TEST CHART

FIGURE 6.8
 SCANNER OUTPUT WITH ONLY ONE WARM WHITE
 FLUORESCENT LIGHT PROVIDING ILLUMINATION
 THRESHOLD AUTOMATICALLY SET AT N = 320

1.4
 1.6
 1.8
 2.0
 2.2
 2.5
 2.8
 3.2
 3.6
 4.0
 4.5
 5.0
 5.6
 6.3
 7.1
 8.0
 9.0
 10.0

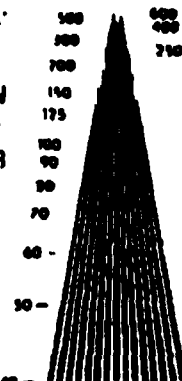


NMA MICROFONT QJKLPYZ
6BSI2GH5D4X7U3W8V9E

ABCDEFGHIJKLMN OPQRSTUW
XYZabcdefghijklmnopqr
stuvwxyz0123456789 OCR-B

ABCDEFGHIJKLMN OPQRSTUW
WXYZabcdefghijklmnopqr
stuvwxyz1234567890 PICA

ABCDEFGHIJKLMN OPQRSTUWXYZ
abcdefghijklmnopqrstu
vwxyz1234567890 Elite



ABCDEFGHIJKLMN OPQRSTUWXYZ
abcdefghijklmnopqrstu
vwxyz1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMN OPQRSTUWXYZ
abcdefghijklmnopqrstu
vwxyz1234567890 Spartan Medium 8 pt

ABCDEFGHIJKLMN OPQRSTUWXYZ
abcdefghijklmnopqrstu
vwxyz1234567890 Spartan Medium 10 pt

ABCDEFGHIJKLMN OPQRSTUWXYZ
abcdefghijklmnopqrstu
vwxyz1234567890 Spartan Medium 12 pt

IEEE Std 167A-1980

FACSIMILE TEST CHART

FIGURE 6.9
SCANNER OUTPUT USING RED PAPER AS BACKGROUND
(COOL WHITE FLUORESCENTS)
THRESHOLD AUTOMATICALLY SET AT N = 321



these conditions. This was by far the most demanding test of the ATC because total pel swing of the analog signal was less than 80 millivolts and the threshold level obtained still produced legible copy.

Figures 6.10 to 6.13 represent other document selections for evaluating the Automatic Threshold Control from a subjective standpoint. Figure 6.10 needs no comment, but Figures 6.11 and 6.12 represent fairly difficult text for scanner reproduction. Notice the excellent scanner performance with these documents. The original used to produce Figure 6.13 was a magazine advertisement with a very dark brown background and white print. Although the graphics cannot be interpreted, a majority of the print is legible.

A few points should be discussed concerning the actual limitations of the scanner/printer combination when evaluating the scanner's output. The first point concerns the observed resolution capability of the system. Although the scanner can detect resolutions up to 200 lines/inch, (1) the electrostatic printer used to produce hard copy will not faithfully reproduce this resolution due to the overlapping stylii. As illustrated in Figure 6.14, a resolution of 200 lines/inch will actually have more black than white resulting in a small amount of degradation in the output. Patterns approaching 200 lines/inch will appear

(1) Recall that resolution is measured in lines/inch while spatial frequency is measured in line-pairs/inch. This means there is a 2-to-1 correlation between resolution and spatial frequency. Therefore the CCD Nyquist rate theoretically can produce a resolution of 200 lines/inch.

Ch 6

The Federal Reserve Board could, if it chose, somewhat ease the pain of more business failures by flooding the financial system with money. We do not believe that they will choose this course. The nation has come a long way in winding down inflationary expectations and the Fed is unlikely to give up the fight now. We believe they understand that a critical weapon in the battle against inflation is the reintroduction of "risk" into the economic system. Excessive monetary growth and assured corporate bail-outs do not encourage prudent business planning. Rather, it fosters the immoderate use of borrowed funds and the belief that, in the long run, the ability to raise prices will subsequently justify buying extra inventory or paying excessive wage demands. If the Fed sticks to its guns, business will have to learn how to operate with a totally different philosophy. For some, the lesson will be learned too late.

What else can we look for? Certainly, capital spending plans will continue to be pared back. The latest McGraw-Hill survey of capital spending plans for 1982 pointed to a 3.9% dollar increase, representing a 4 1/2% decline in actual physical outlays. Six months ago, spending plans called for a 1982 advance of 9.6%. Commerce Department surveys have also suggested a scaling back of capital spending intentions. We think the process still has further to go. We expect capital spending to be the weakest sector of the economy until well into 1983 and perhaps for even longer if the economy "triple dips" in early 1983 as we think possible.

Operating expenses also get cut back when profits are under pressure. The unemployment rate may not have topped out yet although we suspect it doesn't have too much further to go. Wage "givebacks" have characterized labor negotiations in the depressed cyclical industries. Over the next few months we expect the business media to be rife with stories about white collar layoffs and executive salary cuts. Goodrich, for example, recently announced that its top management would take a 15% salary cut while other executives and salaried employees making more than \$20,000 a year would take reductions ranging from 5% to 10%.

We also look for a continuation in the surge of dividend cuts as corporations scramble to retain cash. According to Standard & Poor's, through the first 4 months of 1982, 158 companies decreased or omitted their dividend payments, more than twice the number of companies who took similar action last year. In recent months, dividend casualties included such companies as Inland and Republic Steel, Reynolds Metals, Sun Electric, Champion International, Harnischfeger and Manville. Another source of corporate cash is the sale of assets. Dome Petroleum and Inco, among others, have recently announced such plans. Chrysler and International Harvester, of course, have sold off large and profitable divisions. More such moves will follow.

We have painted a rather grim picture of the financial strains on the economy. The reliquefaction process is far from complete, a factor which will serve to slow the recovery process. Thus, for this and other reasons, our investment posture with regard to equities has been selective and opportunistic within a generally cautious framework. Companies with sound balance sheets and well-assured prospects of unit growth could do surprisingly well in a restrictive economic environment. Moreover, during uncertain times, some stocks get down to extraordinarily attractive prices in terms of their

FIGURE 6.10

SCANNER OUTPUT UNDER NORMAL CONDITIONS
(COOL WHITE FLUORESCENTS)
THRESHOLD AUTOMATICALLY SET AT N = 392

By Nicholas

ASCII/BAUDOT, STAND ALONE

Computer Terminal COMPLETE FOR ONLY \$149.95

The Nerocline ASCII/BAUDOT Computer Terminal Kit is a microprocessor-controlled, stand alone keyboard/terminal...

The highest follows the standard computer configuration and provides the entire 128 character ASCII upper/lower case...

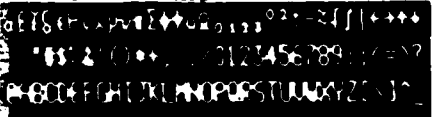
The Computer Terminal requires no I/O mapping and includes 1k of memory, character generator, 2 key rollover...

VIDEO DISPLAY SPECIFICATIONS

The heart of the Nerocline Computer Terminal is the microprocessor-controlled Nerocline Video Display Board (VID)...

When connected to a computer, the computer must echo the character received. This data is received by the VID which...

Video Outputs 1.5 P/P into 75 ohm (SIA RS-170) • Stand Rate: 110 and 50 ASCII • Outputs RS232-C or 20 ma. current loop...



ASCII Characters Kit ABCDEFGHIJKLMNOPQRSTUVWXYZ... [List of characters and symbols]

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To Order From Connecticut Or For Technical Assistance, Etc. Call (203) 264-6576

Nerocline R&D Ltd., Dept. PE-9 300 Lincoln Road, New Bedford, CT 06776

- Items and the items checked below: Nerocline Stand Alone ASCII Keyboard/Computer Terminal Kit, Deluxe Keyboard for Nerocline Keyboard Terminal, Video Display Board Kit, 12" Video Monitor, RF Modulator Kit, 1.5 amp Power Supply Kit, Total Estimated (Conv. res. add sales tax) \$, Payment options: Personal Check, Cashiers Check/Money Order, Visa, MasterCard, Bank #

Explorer/85

100% compatible with all DOS/2 and DOS software & development tools!

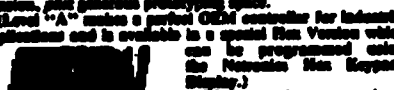
No matter what your future computing plans may be, Level "A" is at \$129.95 - a year saving point.

Starting at just \$129.95 for a Level "A" operating system, you can now build the exact computer you want.

Now, for just \$129.95, you can own the first level of a fully compatible computer with professional capabilities...

Level "A" Specifications: Explorer/85's Level "A" system features the advanced Intel 8085 CPU, an 8192 ROM with 2k deluxe monitor/operating system...

Level "A" makes a perfect OEM computer for industrial applications and is available in a special Rom Version which can be programmed using the Nerocline Rom KeyPad/Display.



Level "A" at \$129.95 is a complete operating system, perfect for engineers, hobbyists, or industrial controllers.

Level "A" at \$129.95 is a complete operating system, perfect for engineers, hobbyists, or industrial controllers. Includes tape reader control, speaker control, LED output indicator on SOD...

System Monitor (Terminal Version): 2k bytes of deluxe game monitor ROM located at P000 allowing 65535 free for user RAM/ROM. Features include tape load with labeling...

System Monitor (Rom Version): Tape load with labeling... tape dump with labeling... routine/change contents of memory... insert data... warm start... routine and change all registers...

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- Items and the items checked below: Explorer/85 Level "A" Kit (ASCII Version), Explorer/85 Level "A" Kit (Rom Version), IBM MicroVtC BASIC on cassette, IBM MicroVtC BASIC in ROM Kit, Level "B" (8-100) Kit, Level "C" (8-100 6-card expander) Kit, Level "D" (4k RAM) Kit, Level "E" (EPROM/ROM) Kit, Deluxe Steel Cabinet for Explorer/85, ASCII Keyboard/Computer Terminal Kit, Special Computer Grade Cassette Tapes, 12" Video Monitor, Power Supply Kit, Total Estimated (Conv. res. add sales tax) \$, Payment options: Personal Check, Cashiers Check/Money Order, Visa, MasterCard, Bank #

regions... single step with register display at each break point... go to cursor address. Level "A" in the Rom Version makes a perfect computer for industrial applications and is programmed using the Nerocline Rom KeyPad/Display.

Non KeyPad/Display Specifications: Calculator type keypad with 24 system defined and 16 user defined keys. 6 digit calculator type display which displays 6 character plus data as well as register and cursor information.

Level "B" Specifications: Level "B" provides the 8-100 signals plus buffer/drivers to support up to six 8-100 bus boards and includes address decoding for enhanced 4k RAM expansion...

Level "C" Specifications: Level "C" expands Explorer motherboard with a card cage allowing you to plug up to 3 8-100 cards directly into it. Explorer's deluxe steel cabinet...

Level "D" Specifications: Level "D" provides 4k of RAM, power supply regulation, floating decoupling capacitors and sockets to expand your Explorer/85 memory to 4k (plus the original 256 bytes located in the 8192A). The static RAM can be located anywhere from 0000 to EFFF in 4k blocks.

Level "E" Specifications: Level "E" adds sockets for 9k of EPROM to use the popular Intel 2716 or the TI 2916. It includes all sockets, power supply regulator, heat sink, filtering and decoupling components.

Order a Complete Explorer Applications Pack: Explorer's Pak SAVE \$129.95 - Buy Level "A" and Rom KeyPad/Display for \$199.95 and get FREE Intel 8085 user's manual plus FREE postage & handling!

Explorer's Pak SAVE \$149.95 - Buy Level "A" ASCII Keyboard/Computer Terminal, and Power Supply for \$199.95 and get FREE RF Modulator, plus FREE Intel 8085 user's manual plus FREE postage & handling!

Explorer's Pak SAVE \$249.95 - Buy Levels "A", "B", "C", "D", and "E" with Power Supply, ASCII Keyboard/Computer Terminal, and six 8-100 Bus Connectors for \$299.95 and get 10 FREE computer grade cassette tapes plus FREE 8085 user's manual plus FREE postage & handling!

Explorer's Pak SAVE \$399.95 - Buy Explorer/85 Levels "A", "B", and "C" (with cabinet), Power Supply, ASCII Keyboard/Computer Terminal (with cabinet), 1k RAM, 12 Video Monitor, Month Star 5-1/4" Disk Drive (includes Month Star BASIC) with power supply and cabinet, all for just \$399.95 and get 10 FREE 5-1/4" minidisks (40-50 words) plus FREE 8085 user's manual plus FREE postage & handling!

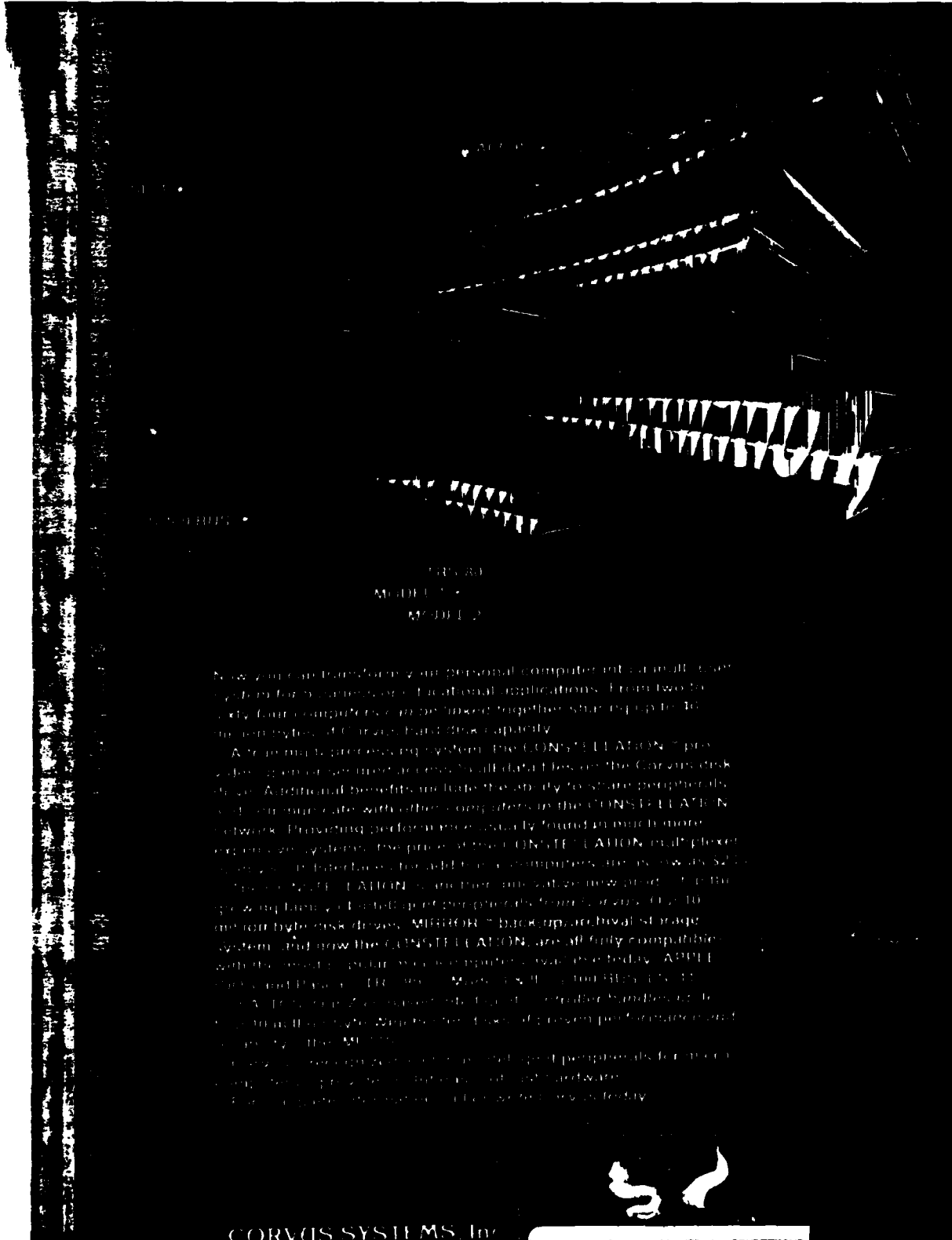
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- standard disk operating system - just plug it in and you're up and running! \$99.95 plus \$3.00 postage. Power Supply Kit for North Star Disk Drive, \$39.95 plus \$3.00 postage. Deluxe Case for North Star Disk Drive, \$39.95 plus \$3.00 postage. Explorer's Pak (see above), \$399.95 postage. Standard Pak (see above), \$399.95 postage. Engineering Pak (see above), \$644.75 postage. Nerocline Pak (see above), \$699.95 postage. Total Estimated (Conv. res. add sales tax) \$, Payment options: Personal Check, M.O./Cashier's Check, Visa, MasterCard, Bank #

FIGURE 6.12

SCANNER OUTPUT UNDER NORMAL CONDITIONS (COOL WHITE FLUORESCENTS) THRESHOLD AUTOMATICALLY SET AT N = 409



TRIVIAL
MODEL 1
MODEL 2

Now you can transform any personal computer into a multi-user system for business or educational applications. From two to thirty-four computers can be linked together sharing up to 36 million bytes of Corvus hard disk capacity.

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system can be configured to share and speed peripherals for other computers providing the most advanced and cost hardware.

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FIGURE 6.13

Page 103

SCANNER OUTPUT UNDER NORMAL CONDITIONS
(COOL WHITE FLUORESCENTS)
THRESHOLD AUTOMATICALLY SET AT N = 384

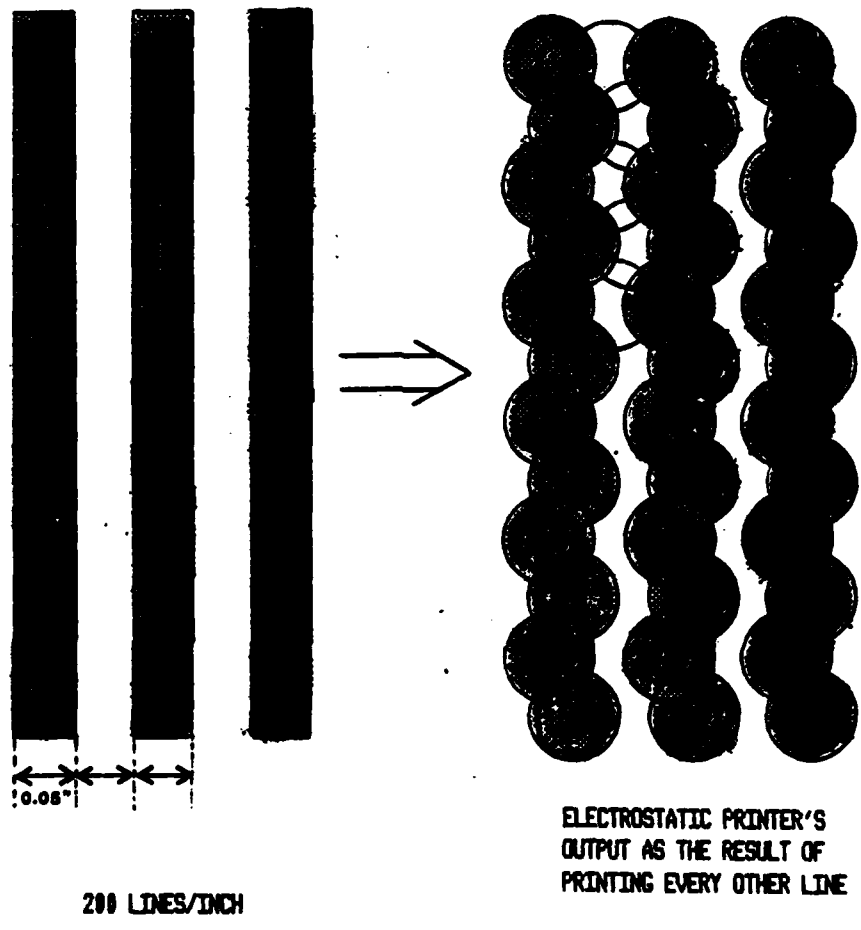


FIGURE 6.14 MAGNIFIED VIEW OF ELECTRO-
STATIC PRINTER'S REPRODUCTION
OF THE NYQUIST FREQUENCY

to have less white content than they should. This characteristic should be kept in mind when evaluating the resolution of the scanner output with the IEEE Facsimile Test Chart.

The next point deals with the hysteresis included in the video A-to-D converter as an additional measure to prevent clock noise feed-through. The hysteresis was experimentally set at a level that allows all spatial frequencies to be digitized under normal lighting conditions and pastel paper colors. However when abnormal conditions reduce the magnitude of the analog video signal, the pel swing from the highest spatial frequencies are too small to overcome the hysteresis barrier. This effect can be most easily seen with IEEE Test Pattern 12 in Figures 6.6 to 6.9. Distortion due to hysteresis is characterized by a "streaked" or "filled-in" appearance at the affected spatial frequencies.

The last point pertains to the effect of non-uniform illumination. As established in Chapter 3, the ATC will average any light irregularities and select the threshold level giving the highest resolution over the largest portion of the page. This feature of the ATC can be viewed in Figures 6.11 and 6.12. These two copies were produced with fluorescent tubes that had become blackened on the ends due to wear and tear. The ATC still reproduces a majority of the page faithfully with only the bottom of Figure 6.11 and top of Figure 6.12 being degraded because of insufficient light.

B. CONCLUSIONS

In summary, the method produced from this research for automatically selecting the voltage threshold level proved to be successful. The advantages of the ATC are many. First, substantial savings in time, energy, and resources are realized over manual threshold control. Second, the threshold level produced by the ATC is more accurate than one selected by subjective evaluation. Third, the scanner with ATC requires less skills of the user. Fourth, the scanner can automatically respond to a large variety of paper reflectivities and colors. Fifth, light non-uniformities due to deterioration of the fluorescent lamps are automatically compensated. And last, the scanner is able to continue operating automatically with the failure of one fluorescent lamp. On the other hand, a minor disadvantage observed was that the operator must take greater care in placing a document into scanning position to insure the left margin provides background for the CALIBRATION PATTERN.

There are a few critical issues to the proper operation of the ATC that merit discussion. First, it is crucial that the scanner is able to start transmitting video at the same precise physical point for every page. Before ATC incorporation, minor deviations in start position would have hardly been noticeable. But with the need to "see" a narrow CALIBRATION PATTERN in the first few lines, it is now mandatory that the scanner starts reading lines in exactly the same place every time. Inconsistency in the starting position can be offset to a certain

extent by widening the CALIBRATION PATTERN, and this measure was taken by using ECP A which is 0.219 inch wide whereas only 0.140 inch is actually needed. Still a small measure of inaccuracy was observed during research that sporadically caused the CALIBRATION PATTERN to be missed either partially or completely. This resulted in either thresholding errors or a portion of the CALIBRATION PATTERN being printed in the output (called pattern feed-through). This issue will be covered in more detail in the next section.

While established in Chapter 3, another critical issue that deserves repeating is the importance of the design of the CALIBRATION PATTERN itself. The pattern must produce a VTC curve spanning a reasonable amount of N values and producing a clearly definable peak that occurs at the value of N resulting in detection of the highest spatial frequencies. Additionally the CALIBRATION PATTERN should cover the length of the page and have each spatial frequency evenly distributed along its length so that light non-uniformity effects can be minimized.

The other issue that needs review is that of the sampling algorithm design. Not only is it important to maintain a simple scheme due to limitations of the F8 microprocessor, but it is also fundamental to remember that there are less than 900 microseconds available for threshold data processing between video lines. (1) In other words, any algorithm chosen must be able to execute on the F8 in less than 900 microseconds per video

(1) See Figure 2.1.

line. The other point is that as long as the threshold sequence is executed with the scanner in motion, the number of video lines used must be kept to a minimum to preclude the CALIBRATION PATTERN from taking excessive margin space.

C. AREAS FOR FURTHER RESEARCH

1. PHYSICAL POSITIONING ACCURACY

As mentioned earlier, the first line of video in a scan sequence is not necessarily taken from the same physical point each time. It is believed that this was a major cause of thresholding errors encountered during evaluation. To understand the problem, the mechanical sequence must first be studied in Figure 6.15. Once the start button is pushed, the first line of valid video will be transmitted after a preset number of pulses from the phase-locked loop rate-feedback wheel have been counted. Theoretically this should define a very precise distance since the wheel is physically mounted on the lead screw and generates 100 pulses per revolution. It is suspected that errors are being introduced by one or both of the following: either the counters in Block 7, Figure 6.15 are being misloaded by spurious noise, or the mechanical assembly is not coming to rest in exactly the same place each time in Block 8 due to tolerance of the left-most limit switch. This issue should be explored with the purpose of eliminating thresholding errors.

2. CALIBRATION PATTERN

Since this research was conducted with a limited number of available ECPs, a specially designed CALIBRATION PATTERN should

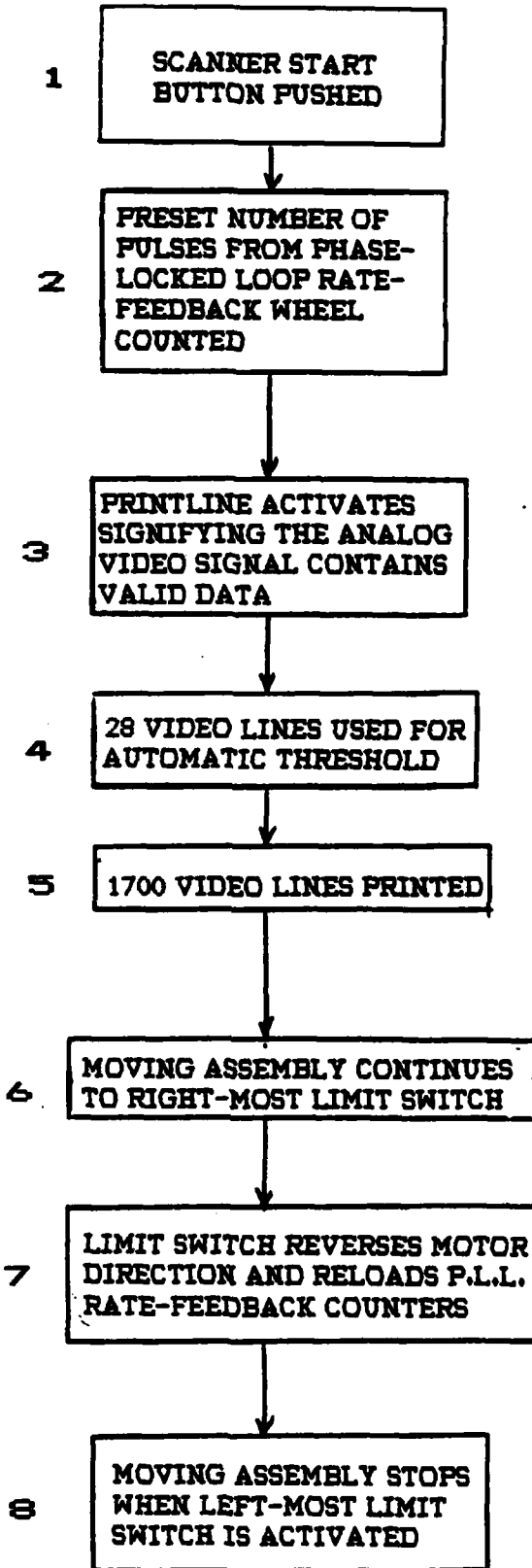


FIGURE 6.15 SCANNER MECHANICAL MOVEMENT SEQUENCE

now be fabricated for use with an operational scanner. Although ECP A works, each frequency burst has only seven discrete spatial frequencies that the CCD can detect; the other five spatial frequencies are above the Nyquist rate and therefore contribute nothing. Additionally, 50% of ECP A has no spatial frequency content whatsoever. In view of this, I suggest designing a CALIBRATION PATTERN specially tailored to the needs of the ATC. Two possible frequency-burst designs are: one with more discrete frequencies, and one containing a linearly increasing set of spatial frequencies. Each burst should be about one inch long and repeated along the length of the page. This effort will not improve the ATC's choice of threshold level since the optimum has already been achieved, but on the other hand, it could further enhance the ATC's robustness under abnormal conditions. Once the operational CALIBRATION PATTERN design has been completed, the pattern itself should be permanently etched into the glass face of the scanner. For expediency in this research, a transparency of ECP A was taped into position to serve the purpose of a CALIBRATION PATTERN.

3. ADJUSTABLE DARKNESS CONTROL

The ATC is designed to select the threshold that will give the most black/white transitions which in turn produces an output that gives equal priority to black and white information. During evaluation however, it was found that, from a subjective standpoint, copies were sometimes more pleasing if the threshold was shifted to slightly blacker than optimum. In this way,

portions of fine print (smaller than 6 point) having spatial frequencies above Nyquist tended to be more readable. The compromise involved the loss of some white information in the form of black fill-in, but this was not a major detraction. Therefore I suggest adding a control whereby the user could bias the threshold to lighter or darker than optimum, depending on the specific need. This could most easily be accomplished by using a multi-position multi-wafer switch configured to feed various 8-bit binary numbers to an F8 I/O part. At the end of the threshold-setting sequence, the F8 would alter the optimum threshold level by the value selected by the user.

4. INK COLOR

Due to time constraints, this research focused only on documents having black print. It is predictable that on a white background, colors of ink other than black will produce a smaller pel swing, but it is unclear what colors of print will not be detected with the threshold level set by the ATC. Future experimentation in this area will better define the capabilities and limitations of the scanner system.

5. SCANNER ILLUMINATION DESIGN

A number of issues concerning the scanner's light source were encountered during the course of this research. (1) First of all, a problem was noted with the light start-up at the beginning of the page-scanning sequence. Either one or both

(1) The reader should refer to Aghamohammadi and Agudelo as necessary for background concerning the existing design.

lights failed to illuminate approximately 30 to 40 percent of the time. Start-up failures were more prevalent with:

- a. new tubes
- b. very old tubes
- c. green tubes in general

Secondly, a fairly rapid deterioration at the end of the tubes (1) caused significant non-uniform illumination to occur over the lifetime of the tube. The results of this were seen in Figures 6.11 and 6.12. Thirdly, a significant amount of light leakage (2) into the CCD shifted the analog black level away from absolute black and thereby reduced the effective contrast of the document being scanned.

In view of these difficulties, I suggest that a thorough re-evaluation of the existing illumination design be conducted. This is not necessarily a suggestion to abandon fluorescent tubes for some other type of lamp. On the contrary, there are many advantages of fluorescent lighting to warrant further investigation on obtaining the desired performance with them. One possible source of aggravation for the fluorescent tubes could be the DC drive currently used. While the original idea was to avoid "flicker" problems, it may be a reason for the rapid deterioration and inconsistent start-ups. One alternative is to evaluate the feasibility of using a high-frequency AC drive and incorporating a quarter-wave phase shift between the two tubes.

(1) As discussed in Chapter 3.

(2) As discussed in Chapter 1.

The problem concerning the light leakage can be eliminated by adding a light-proof shroud between the face of the CCD and the focusing lens.

6. SCANNER START BUTTON

Throughout this project, it was noted that the scanner start button was not adequately resistant to various forms of interference. This problem was commonly manifested by the scanner going through one or more uncommanded page-scanning cycles immediately upon completion of a user-initiated page-scanning cycle. Additionally, the scanner would cycle through at least one page-scanning sequence when power was first applied to the system. Although this is not a disabling problem, it is a nuisance that should be corrected before the scanner is placed in a user environment for operational evaluation.

CHAPTER 7

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APPENDIX A

MANUFACTURER'S TECHNICAL DATA

This appendix contains technical data extracts of pertinent items and components used during the course of this research. This material is included for convenience as reference to support the discussion in the body of this report, and is not meant in any way to serve as a complete set of data. Readers desiring more information should refer to the manufacturers' publications.

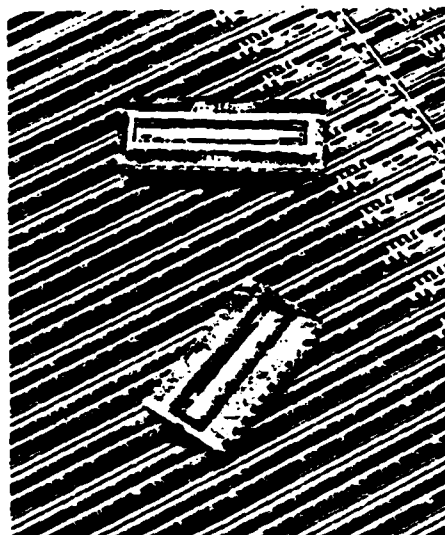
CCD122/142
1728/2048-ELEMENT LINEAR IMAGE SENSOR
FAIRCHILD CHARGE COUPLED DEVICE

GENERAL DESCRIPTION—The CCD122 and CCD142 are monolithic 1728 and 2048-element line image sensors, respectively. The devices are designed for page scanning applications including facsimile, optical character recognition and other imaging applications which require high resolution and high sensitivity.

The 1728 sensing elements of the CCD122 provide a 200-line per inch resolution across an 8-1/2 inch page adopted as an international facsimile standard. The 2048 sensing elements of the CCD142 provide an 8-line per millimeter resolution across a 256 millimeter page adopted as the Japanese facsimile standard.

The CCD122 and the CCD142 have overall improved performance compared with the CCD121H including higher sensitivity, an enhanced blue response and a lower dark signal. The devices also incorporate on-chip clock driver circuitry.

The photoelement size is 13 μ (0.51 mils) by 13 μ (0.51 mils) on 13 μ (0.51 mils) centers. The devices are manufactured using Fairchild advanced charge-coupled device n-channel isoplanar buried-channel technology.



- ENHANCED SPECTRAL RESPONSE (PARTICULARLY IN THE BLUE REGION)
- LOW DARK SIGNAL
- HIGH RESPONSIVITY
- ON-CHIP CLOCK DRIVERS
- DYNAMIC RANGE TYPICAL: 2500:1
- OVER 1V PEAK-TO-PEAK OUTPUT
- DARK AND WHITE REFERENCES CONTAINED IN A SAMPLED-AND-HELD OUTPUT
- SINGLE POWER SUPPLY

PIN NAMES

- | | |
|----------------------|---|
| V _{ps} | Photogate |
| or | Transfer Clock |
| or | Transport Clock |
| VIDEO _{out} | Output Amplifier Source |
| V _{od} | Output Amplifier Drain |
| or | Reset Clock |
| V _{cd} | Clock Driver Drain |
| V _e | Electrical Input Bias |
| V _r | Analog Transport Shift Register
DC Electrode |
| EOS _{out} | End-of-Scan Output |
| or | Sample-and-Hold Clock |
| V _{ss} | Substrate (GND) |
| NC | No Connection (Do not Ground) |

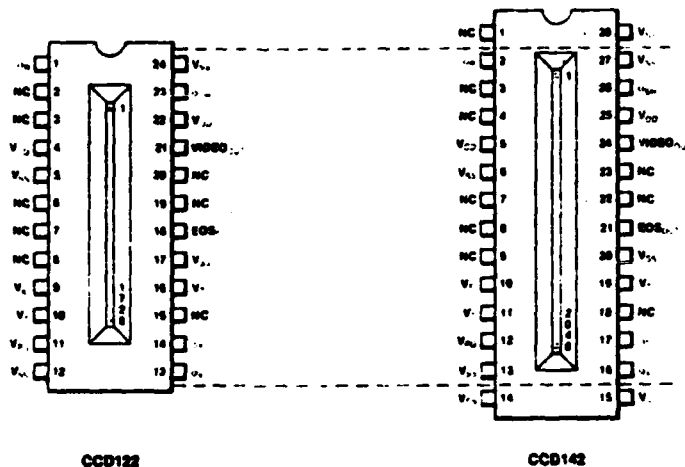
CCD122/142 VS. CCD121H COMPARISON

PARAMETER	CCD122/142	CCD121H
Spectral Response — Blue	4:1 Improvement	—
Overall	2:1 Improvement	—
Dark Signal	2:1 Improvement	—
Responsivity	2:1 Improvement	—
On-Chip Clock Drivers	Yes	No
Dark and White References	Yes	No
Single Power Supply	Yes	No



CCD122/142

**CONNECTION DIAGRAM
DIP (TOP VIEW)**



FUNCTIONAL DESCRIPTION—The CCD122/142 consists of the following functional elements illustrated in the Block Diagram:

Image Sensor Elements — A line of 1728/2048 image sensor elements separated by diffused channel stops and covered by a silicon dioxide surface passivation layer. Image photons pass through the transparent silicon dioxide layer and are absorbed in the single crystal silicon creating hole-electron pairs. The photon generated electrons are accumulated in the photosites. The amount of charge accumulated in each photosite is a linear function of the incident illumination intensity and the integration period. The output signal will vary in an analog manner from a thermally generated noise background at zero illumination to a maximum at saturation under bright illumination.

Transfer Gate — Gate structure adjacent to the line of image sensor elements. The charge-packets accumulated in the image sensor elements are transferred out via the transfer gate to the transport registers whenever the transfer gate voltage goes HIGH. Alternate charge-packets are transferred to the analog transport shift registers. The transfer gate also controls the exposure time for the sensing elements and permits entry of charge to the End-Of-Scan (EOS) shift registers creating the end-of-scan waveform.

Four 879/1038-Bit Analog Shift Registers — Two on each side of the line of image sensor elements and separated from it by the transfer gate. The two inside registers, called the transport shift registers, are used to move the image generated charge-packets delivered by the transfer gate serially to the charge-detector/amplifier. The complementary phase relationship of the last elements of the two transport shift registers provides for alternate delivery of

CCD122/142

charge-packets to establish the original serial sequence of the line of video in the output circuit. The outer two registers serve to deliver the end-of-scan waveform and reduce peripheral electron noise in the inner shift registers.

Gated Charge-Detector/Amplifier — Charge-packets are transported to a precharged diode whose potential changes linearly in response to the quantity of the signal charge delivered. This potential is applied to the gate of an n-channel MOS transistor producing a signal which passes through the sample-and-hold gate to the output at VIDEO_{out}. The sample-and-hold gate is a switching MOS transistor in the output amplifier that allows the output to be delivered as a sampled-and-held waveform. A reset transistor is driven by the Reset Clock (ϕ_R) and recharges the charge-detector diode capacitance before the arrival of each new signal charge-packet from the transport registers.

Clock Driver Circuitry — Allows the CCD122/142 to be operated using only three external clocks, (1) a Reset Clock signal which controls the integrated output signal amplifier, (2) a square wave Transport Clock which operates at half the reset clock frequency and controls the readout rate of video data from the sensor, and (3) a Transfer Clock pulse which controls exposure time of the sensor. The external clocks should be able to supply TTL level power.

Dark and White Reference Circuitry — Four additional sensing elements at both ends of the 1728/2048 array are covered by opaque metalization. They provide a dark (no illumination) signal reference which is delivered at both ends of the line of video output representing the illuminated 1728/2048 sensor elements (labelled "D" in the block diagram). Also included at one end of the 1728/2048 sense element array is a white signal reference level generator which likewise provides a reference in the output signal (labelled "W" in the block diagram). These reference levels are useful as inputs to external DC restoration and/or automatic gain control circuitry.

DEFINITION OF TERMS:

Charge-Coupled Device — A charge-coupled device is a semiconductor device in which finite isolated charge-packets are transported from one position in the semiconductor to an adjacent position by sequential clocking of an array of gates. The charge-packets are minority carriers with respect to the semiconductor substrate.

Transfer Clock ϕ_T — The voltage waveform applied to the transfer gate to move the accumulated charge from the image sensor elements to the CCD transport shift registers.

Transport Clock ϕ_T — The clock applied to the gates of the CCD transport shift registers to move the charge-packets received from the image sensor elements to the gated charge-detector/amplifier.

Gated Charge-Detector/Amplifier — The output circuit of the CCD122/142 which receives the charge-packets from the CCD transport shift registers and provides a signal voltage proportional to the size of each charge-packet received. Before each new charge-packet is sensed, a reset clock returns the charge-detector voltage to a fixed base level.

Reset Clock ϕ_R — The voltage waveform required to reset the voltage on the charge-detector.

Sample-and-Hold Clock ϕ_{SH} — An internally supplied voltage waveform applied to the sample-and-hold gate in the amplifier to create a continuous sampled video signal at the output. The sample-and-hold feature can be defeated by connecting ϕ_{SH} to V_{DD} .

Dark Reference — Video output level generated from sensing elements covered with opaque metalization providing a reference voltage equivalent to device operation in the dark. Permits use of external dc restoration circuitry.

White Reference — Video output level generated by on-chip circuitry providing a reference voltage permitting external automatic gain control circuitry to be used. The reference voltage is produced by charge-injection under the control of the electrical input bias voltage (V_{BI}). The amplitude of the reference is typically 70% of the saturation output voltage.

Isolation Cell — A site on-chip producing an element in the video output that serves as a buffer between valid video data and dark and white reference signals. The output from an isolation cell contains no valid video information and should be ignored.

Dynamic Range — The saturation exposure divided by the peak-to-peak noise equivalent exposure. (This does not take into account any dark signal components.) Dynamic range is

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sometimes defined in terms of rms noise. To compare the two definitions a factor of four to six is generally appropriate in that peak-to-peak noise is approximately equal to four to six times rms noise.

Peak-to-Peak Noise Equivalent Exposure — The exposure level which gives an output signal equal to the peak-to-peak noise level at the output in the dark.

Saturation Exposure — The minimum exposure level that will produce a saturated output signal. Exposure is equal to the light intensity times the photosite integration time.

Charge Transfer Efficiency — Percentage of valid charge information that is transferred between each successive stage of the transport registers.

Spectral Response Range — The spectral band in which the response per unit of radiant power is more than 10% of the peak response.

Responsivity — The output signal voltage per unit exposure for a specified spectral type of radiation. Responsivity equals output voltage divided by exposure level.

Dark Signal — The output signal in the dark caused by thermally generated electrons which is a linear function of integration time and highly sensitive to temperature. (See accompanying photos for details of definition.)

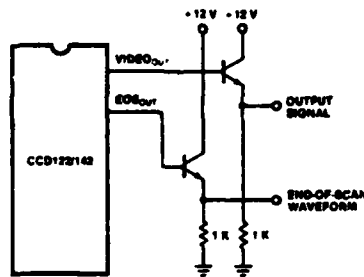
Total Photoresponse Non-Uniformity — The difference of the response levels between the most and least sensitive elements under uniform illumination. (See accompanying photos for details of definition.)

Saturation Output Voltage — The maximum usable signal output voltage, measured from the zero reference level. (See timing diagram.) Any photoelement whose video output < saturation output voltage has an in-spec charge transfer efficiency (CTE). CTE will be below the specification if the video output \geq saturation output voltage.

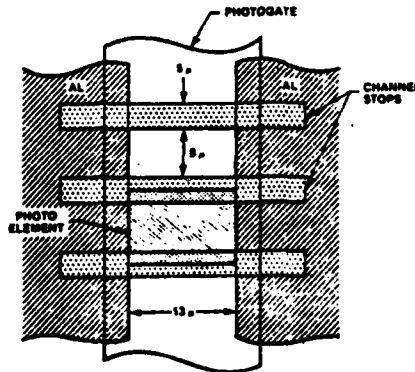
Integration Time — The time interval between the falling edges of any two successive transfer pulses α as shown in the timing diagram. The integration time is the time allowed for the photosites to collect charge.

Pixel — Picture element (photosite).

TEST LOAD CONFIGURATION



PHOTOELEMENT DIMENSIONS



All dimensions are typical values

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ABSOLUTE MAXIMUM RATINGS (Above which useful life may be impaired)

Storage Temperature	-25 °C to +125 °C
Operating Temperature (See curves)	-25 °C to +70 °C
CCD122: Pins 1, 4, 9, 10, 11, 13, 14, 16, 22, 23	-0.3 V to 15 V
Pins 5, 12, 17, 24	0 V
Pins 2, 3, 6, 7, 8, 15, 18, 19, 20, 21	NC
CCD142: Pins 2, 5, 10, 11, 12, 16, 17, 19, 25, 26	-0.3 V to 15 V
Pins 6, 13, 14, 15, 20, 27, 28	0 V
Pins 1, 3, 4, 7, 8, 9, 18, 21, 22, 23, 24	NC

CAUTION NOTE: These devices have limited built-in gate protection. It is recommended that static discharge be controlled and minimized. Care must be taken to avoid shorting pins VIDEOOUT and EOSOUT to VSS or VDD during operation of the devices. Shorting these pins temporarily to VSS or VDD may destroy the output amplifiers.

DC CHARACTERISTICS: T_p = 25°C (Note 1)

SYMBOL	CHARACTERISTIC	RANGE			UNITS	CONDITIONS
		MIN	TYP	MAX		
V _{cd}	Clock Driver Drain Supply Voltage	12.0	13.0	14.0	V	
I _{cd}	Clock Driver Drain Supply Current		6.9	12.5	mA	
V _{od}	Output Amplifier Drain Supply Voltage	12.0	13.0	14.0	V	
I _{od}	Output Amplifier Drain Supply Current		6.9	12.5	mA	
V _{pg}	Photogate Bias Voltage	6.5	7.0	7.5	V	
V _r	DC Electrode Bias Voltage	4.5	5.0	5.5	V	Note 2
V _{ei}	Electrical Input Bias Voltage		11.4		V	Note 3
V _{ss}	Substrate (Ground)		0.0		V	

AC CHARACTERISTICS: (Note 1)

T_p = 25°C, f_{clk} = 0.5 MHz, t_{int} = 10 ms, light source = 2854°K + 3.0 mm thick Corning 1-75 IR-absorbing filter. All operating voltages nominal specified values.

SYMBOL	CHARACTERISTIC	RANGE			UNITS	CONDITIONS
		MIN	TYP	MAX		
DR	Dynamic Range (relative to peak-to-peak noise) (relative to rms noise)	250:1 1250:1	500:1 2500:1			Note 9
NEE	RMS Noise Equivalent Exposure		0.0002		μJ/cm ²	Note 10
SE	Saturation Exposure		0.4		μJ/cm ²	Note 11
CTE	Charge Transfer Efficiency		0.999995			Note 12
V _o	Output DC Level	3.0	5.5	10.0	V	
Z	Output Impedance		1.4	3.0	kΩ	
P	On-Chip Power Dissipation					
	Clock Drivers		90	150	mW	
	Amplifiers		90	150	mW	
N	Peak-to-Peak Noise		2.0		mV	



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CLOCK CHARACTERISTICS: $T_P = 25^\circ\text{C}$ (Note 1)

SYMBOL	CHARACTERISTIC	RANGE			UNITS	CONDITIONS
		MIN	TYP	MAX		
V_{eL}	Transport Clock LOW	0.0	0.3	0.5	V	Notes 4, 5
V_{eH}	Transport Clock HIGH	9.75	10.0	10.5	V	Note 5
V_{sL}	Transfer Clock LOW	0.0	0.3	0.5	V	Notes 4, 6
V_{sH}	Transfer Clock HIGH	9.75	10.0	10.5	V	Note 6
V_{rL}	Reset Clock LOW	0.0	0.3	0.5	V	Note 7
V_{rH}	Reset Clock HIGH	9.75	10.0	10.5	V	Note 7
f_{en}	Maximum Reset Clock Frequency (Output Data Rate)	1.0	2.0		MHz	Note 8

PERFORMANCE CHARACTERISTICS: (Note 1)

$T_P = 25^\circ\text{C}$, $f_{en} = 0.5$ MHz, $t_{int} = 10$ ms, light source = $2854^\circ\text{K} \pm 3.0$ mm thick Corning 1-75 IR-absorbing filter. All operating voltages nominal specified values.

SYMBOL	CHARACTERISTIC	RANGE			UNITS	CONDITIONS
		MIN	TYP	MAX		
PRNU*	Photoresponse Non-uniformity					
	Peak-to-Peak		160	210	mV	Note 16
	Peak-to-Peak without Single-Pixel Positive and Negative Pulses		100		mV	Note 16
	Single-pixel Positive Pulses		85		mV	Note 16
	Single-pixel Negative Pulses		130		mV	Note 16
	Register Imbalance ("Odd"/"Even")		20		mV	Note 16
DS	Dark Signal					
	DC Component		5	15	mV	Notes 13, 14
	Low Frequency Component		5	10	mV	Notes 13, 14
SPDSNU	Single-pixel DS Non-uniformity		20	40	mV	Notes 13, 15
R	Responsivity	2.0	3.5	5.0	Volts per $\mu\text{J}/\text{cm}^2$	Note 17
V_{SAT}	Saturation Output Voltage	800	1400	1600	mV	Note 18

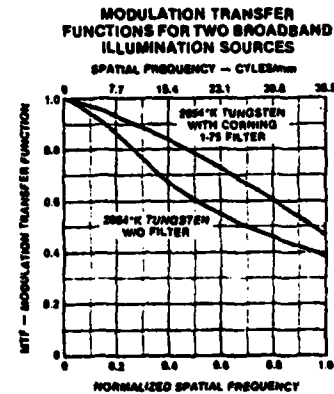
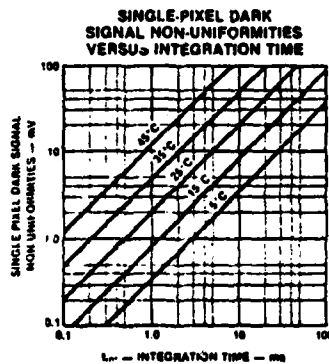
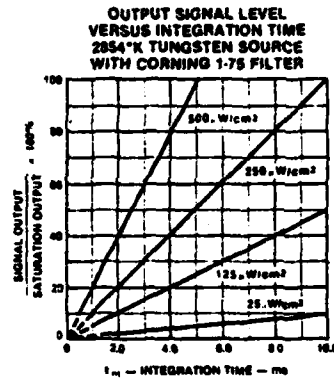
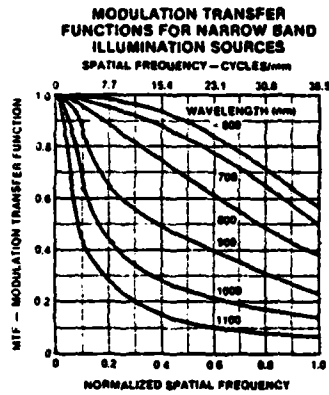
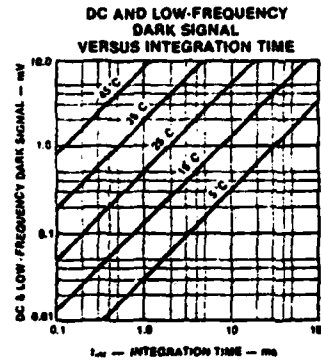
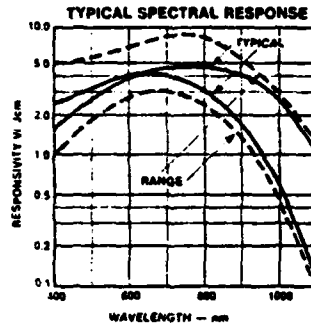
*All PRNU Measurements taken at a 700 mV output level using an f/2.8 lens and excluded the outputs from the first and last elements of the array. The "f" number is defined as the distance from the lens to the array divided by the diameter of the lens aperture. As the f number increases, the resulting more highly collimated light causes the package window aberrations to dominate and increase PRNU. A lower f number results in less collimated light causing device photo-site blemishes to dominate the PRNU.

NOTES:

1. T_P is defined as the package temperature.
2. V_T should be equal to $(1/2) V_{eH}$.
3. V_{BI} is used to generate the end-of-scan output and the white reference output. These two signals can be eliminated by connecting V_{BI} to a voltage level equal to $V_{eH} + 5$ V.
4. Negative transients on any clock pin going below 0.0 V may cause charge-injection which results in an increase of apparent DS.
5. $C_{eT} = 700$ pF
6. $C_{eR} = 300$ pF
7. $C_{eS} = 5$ pF
8. Minimum clock frequency is limited by increase in dark signal.
9. Dynamic range is defined as $V_{SAT}/\text{peak-to-peak (temporal)}$ or $V_{SAT}/\text{rms noise}$.
10. $1 \mu\text{J}/\text{cm}^2 = 0.02$ fcs at 2854°K , 1 fcs = $50 \mu\text{J}/\text{cm}^2$ at 2854°K .
11. SE for 2854°K for light without 3.0 mm thick Corning 1-75 IR-absorbing filter is typically $0.8 \mu\text{J}/\text{cm}^2$.
12. CTE is the measurement for a one-stage transfer.
13. See photographs for DS definitions.
14. Dark signal component approximately doubles for every 5°C increase in T_P .
15. Each SPDSNU is measured from the DS level adjacent to the base of the SPDSNU. The SPDSNU approximately doubles for every 8°C increase in T_P .
16. See photographs for PRNU definitions.
17. Responsivity for 2854°K light source without 3.0 mm thick Corning 1-75 IR-absorbing filter is typically 2 V per $\mu\text{J}/\text{cm}^2$.
18. See test load configurations.

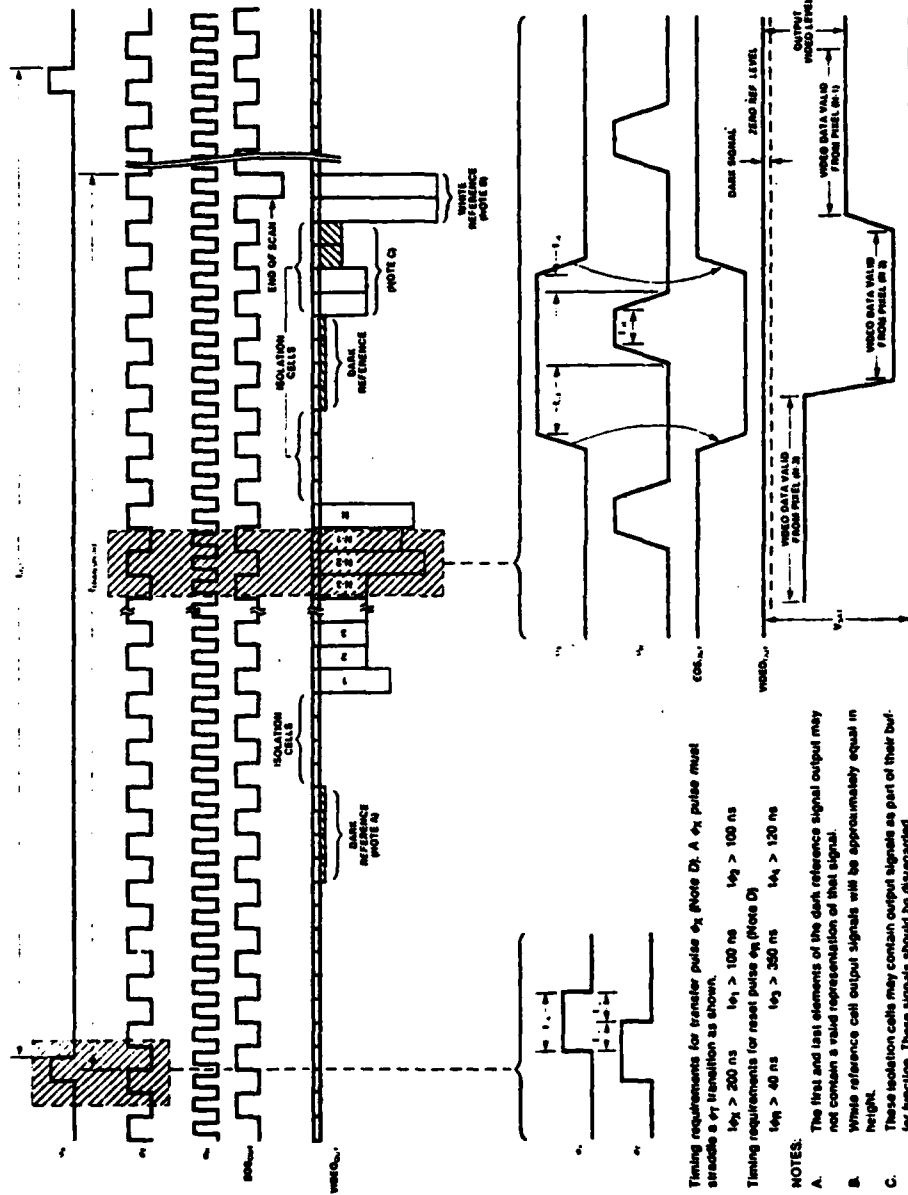
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TYPICAL PERFORMANCE CURVES



The Corning 1-75 filter has the following typical transmittance spectral characteristic: >85% at <600 nm, 80% at 700 nm, 30% at 800 nm, 5% at 900 nm and <2% at >1000 nm.

TIMING DIAGRAM DRIVE SIGNALS



IEEE Std 167A-1980 Facsimile Test Chart

Pattern Descriptions

The pattern number given in the following description may be identified from Figure 1. This chart is designed for scanning in either direction, horizontally across the page.

IEEE Std 167-1966, Test Procedure for Facsimile was based on previous issues of the IEEE Test Chart.

Patterns 1 and 2. 96 lines per inch (3.78 lines per millimeter) consisting of 48 dark and 48 light lines, substantially equal in width. In pattern 1, the black corresponds approximately to step 2 and gray to step 7 of pattern 8. In pattern 2, white represents paper white and gray to approximately step 11. These patterns are intended for generating low-modulation high-frequency signals at both ends of the density scale—useful for testing modulation characteristics at edges of band in a frequency shift system.

Patterns 3, 4, and 5. Vertical bar patterns at 10, 50, and 96 lines per inch (0.394, 1.97, and 3.78 lines per millimeter) of substantially equal width—useful for square-wave testing at several keying frequencies.

Pattern 6. A continuous density wedge designed so that at equal intervals of distance across the page, the variation in reflectance will be roughly equally perceptible to the eye. Reading left-to-right across the page, the relative reflection density values at the heavy dots are approximately as shown in Table 1. Pattern 6 is useful for cases where intermediate reflection densities are needed between the steps in Patterns 7 and 8.

Dot	1	2	3	4	5	6	7
Density	1.95	1.75	1.53	0.78	0.55	0.14	0.05

Patterns 7 and 8. Reversed step tablets of 15 steps with reflection densities corresponding to the approximately equal perceptibility modified to provide smaller low density increments. Consistent with conventional practice, paper white is understood to be equal to 0.00 in density (approximately 0.07 on an absolute scale). For patterns 7 and 8 the relative reflection densities are shown in Tables 2 and 3 respectively.

These patterns will assist in appraising gradient and absolute scale. They are useful for checking half-tone characteristics. Reversed sequences are used since the dynamic half-tone characteristics may differ for a rising density or a falling density scale.

Pattern 9. National Bureau of Standards (NBS) type repeating tri-bar resolution test pattern. Twelve complete sets of three-line patterns are repeated across the sheet. Alternate groups are of different line spacing. Density values are shown in Table 4. This pattern is useful for checking definition.

Pattern 10. Rectangle with 45° diagonal marks at each corner—useful for checking index of cooperation, skew, and paper-feed error.

Patterns 11 and 17. White wedge on black background and black wedge on white background, 0.07 in (1.78 mm) to zero—useful for checking single-line definition.

Pattern 12. W. and L. E. Gurley type Pestre-cov Star pattern. Outer circle 50, second circle 100, and third circle 200 lines per inch (1.97, 3.94, and 7.87 lines per millimeter).

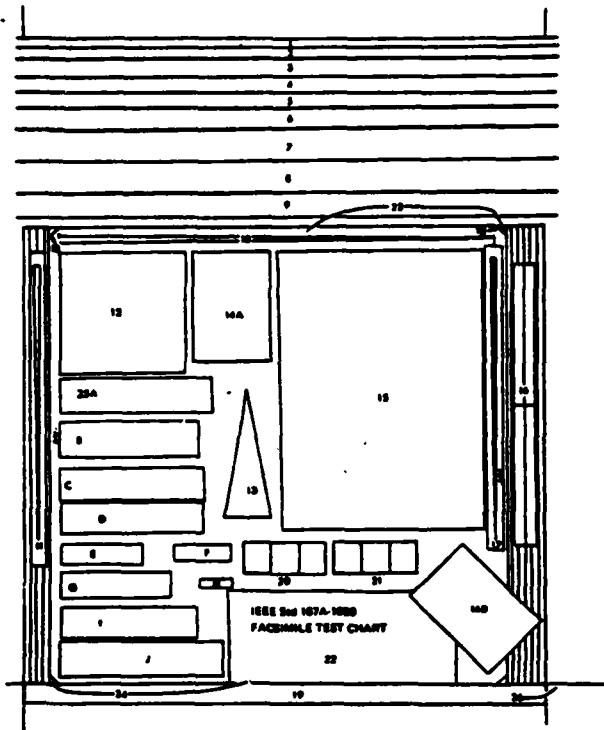


Fig 1
Pattern Arrangement

Pattern 13. Truncated fan-type multiple-line test pattern. Calibrated in lines per inch—useful for checking multiple-line definition along scanning line, envelope delay distortion, and ringing.

Patterns 14A and 14B. NBS type Microcopy Resolution test pattern. Numerals indicate the number of cycles (one black plus one white line) per millimeter (that is, line pairs)—useful in checking high definition systems.

Pattern 15. Photograph with detail in high-light and shadow. The limiting densities of the photograph approximate those of test patterns 7 and 8.

Pattern 16. Vertical gray steps with relative reflection densities of approximately 0.95 and 0.27—useful in testing rising and falling transient characteristics and level variations.

Pattern 18. Horizontal "V" pattern with 0.13 in (3.3 mm) opening. Number of scanning line crossings of both lines, multiplied by 7.7 will equal number of lines per inch (multiply by 0.3 for number of lines per millimeter).

Pattern 19. "Fence" pattern with 0.01 in (0.254 mm) lines 0.10 in (2.54 mm) apart—useful for checking jitter and measuring available line length.

Patterns 20 and 21. Halftone dot screens. Reproduced in approximately 10, 50 and 90 percent black, left to right and at 65 dots per inch (2.56 dots per millimeter) at a 45° angle for pattern 20, and 120 dots per inch (4.72 dots per millimeter) for pattern 21.

Pattern 22. Title and credit box. Three sizes of Times Roman type font.

Patterns 23 and 24. Fiducial dots forming a 3, 4, 5 right triangle—useful for indicating the presence of skew by comparing the hypotenuse of the two patterns.

Pattern 25. Type faces as indicated—useful for checking readability.

Pattern 26. Extension lines to permit measurement of available line and useful length of copy.

Step	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
Density	0.01	0.03	0.13	0.25	0.41	0.56	0.70	0.84	0.94	1.05	1.17	1.32	1.49	1.66	1.80

Step	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
Density	1.70	1.55	1.39	1.25	1.16	1.06	0.94	0.84	0.70	0.56	0.43	0.27	0.15	0.05	0.01

	Group A						Group B					
	1	2	3	4	5	6	1	2	3	4	5	6
Lines per Inch	61.0	66.4	122	173	244	345	406	284	303	142	102	71.1
Lines per Millimeter	2.40	2.60	4.80	6.81	9.60	13.6	16.0	11.2	7.99	5.59	4.02	2.80

NOTE: Group A has coarse lines starting at the left. Group B has coarse lines starting at the right.



CMOS Low Cost 10-Bit Multiplying DAC

AD7533

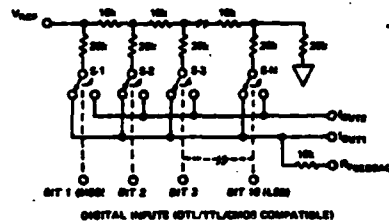
FEATURES

- Lowest Cost 10-Bit DAC
- Low Cost AD7520 Replacement
- Linearity: 1/2, 1 or 2LSB
- Low Power Dissipation
- Full Four-Quadrant Multiplying DAC
- CMOS/TTL Direct Interface
- Latch Free (Protection Schottky not Required)
- End-Point Linearity

APPLICATIONS

- Digitally Controlled Attenuators
- Programmable Gain Amplifiers
- Function Generation
- Linear Automatic Gain Control

AD7533 FUNCTIONAL BLOCK DIAGRAM



GENERAL DESCRIPTION

The AD7533 is a low cost 10-bit 4-quadrant multiplying DAC manufactured using an advanced thin-film-on-monolithic-CMOS wafer fabrication process.

Pin and function equivalent to the industry standard AD7520, the AD7533 is recommended as a lower cost alternative for old AD7520 sockets or new 10-bit DAC designs.

AD7533 application flexibility is demonstrated by its ability to interface to TTL or CMOS, operate on $\pm 5V$ to $+15V$ power, and provide proper binary scaling for reference inputs of either positive or negative polarity.

PACKAGE IDENTIFICATION¹

Suffix D: Ceramic DIP - (D16B)

Suffix N: Plastic DIP - (N16B)

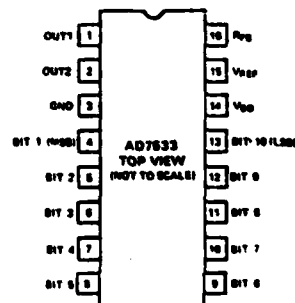
¹ See Section 20 for package outline information.

ORDERING INFORMATION

Nonlinearity	Temperature Range		
	Commercial 0 to +70°C	Industrial -25°C to +85°C	Military -55°C to +125°C
±0.2%	AD7533JN	AD7533AD AD7533AD/883B ¹	AD7533SD AD7533SD/883B ¹
±0.1%	AD7533KN	AD7533BD AD7533BD/883B ¹	AD7533TD AD7533TD/883B ¹
±0.05%	AD7533LN	AD7533CD AD7533CD/883B ¹	AD7533UD AD7533UD/883B ¹

¹ 100% screened to MIL-STD-883, method 5004, para. 3.1.1 through 3.1.12 for Class B device.

PIN CONFIGURATION



SPECIFICATIONS (V_{DD} = +15V; V_{OUT1} = V_{OUT2} = 0V; V_{REF} = +10V unless otherwise noted)

PARAMETER	T _A = 25°C	T _A = Operating Range ¹	Test Conditions
STATIC ACCURACY			
Resolution	10 Bits	10 Bits	
Relative Accuracy ^{2,3}			
AD7533JN, AD, SD	±0.2% FSR max	±0.2% FSR max	
AD7533KN, BD, TD	±0.1% FSR max	±0.1% FSR max	
AD7533LN, CD, UD	±0.05% FSR max	±0.05% FSR max	
Gain Error ^{3,4,5}	±1.4% FS max	±1.5% FS max	Digital Inputs = V _{INH}
Supply Rejection ⁶			
ΔGain/ΔV _{DD}	0.005%/%	0.008%/%	Digital Inputs = V _{INH} ; V _{DD} = +14V to -
Output Leakage Current			
I _{OUT1} (pin 1)	±50nA max	±200nA max	Digital Inputs = V _{INL} ; V _{REF} = ±10V
I _{OUT2} (pin 2)	±50nA max	±200nA max	Digital Inputs = V _{INH} ; V _{REF} = ±10V
DYNAMIC ACCURACY			
Output Current Settling Time	600ns max ⁷	800ns ⁶	To 0.05% FSR; R _{LOAD} = 100Ω; Digital Inputs = V _{INH} to V _{INL} or V _{INL} to V _{INH}
Feedthrough Error	±0.05% FSR max ⁶	±0.1% FSR max ⁶	Digital Inputs = V _{INL} ; V _{REF} = ±10V, 100kHz sinewave.
REFERENCE INPUT			
Input Resistance (pin 15)	5kΩ min, 20kΩ max	5kΩ min, 20kΩ max ⁸	
ANALOG OUTPUTS			
Output Capacitance			
C _{OUT1} (pin 1)	100pF max ⁶	100pF max ⁶	} Digital Inputs = V _{INH}
C _{OUT2} (pin 2)	35pF max ⁶	35pF max ⁶	
C _{OUT1} (pin 1)	35pF max ⁶	35pF max ⁶	} Digital Inputs = V _{INL}
C _{OUT2} (pin 2)	100pF max ⁶	100pF max ⁶	
DIGITAL INPUTS			
Input High Voltage			
V _{INH} ³	2.4V min	2.4V min	
Input Low Voltage			
V _{INL} ³	0.8V max	0.8V max	
Input Leakage Current			
I _{IN} ³	±1μA max	±1μA max	V _{IN} = 0V and V _{DD}
Input Capacitance			
C _{IN}	5pF max ⁶	5pF max ⁶	
POWER REQUIREMENTS			
V _{DD}	+15V ±10%	+15V ±10%	Rated Accuracy Functionality with degraded performance Digital Inputs = V _{INL} or V _{INH}
V _{DD} Range ⁴	+5V to +16V	+5V to +16V	
I _{DD} ³	2mA max	2mA max	

NOTES:

¹ Plastic (JN, KN, LN versions): 0 to +70°C
Commercial Ceramic (AD, BD, CD versions): -25°C to +85°C
Military Ceramic (SD, TD, UD versions): -55°C to +125°C

² "FSR" is Full Scale Range.

³ Final electrical tests are: Relative Accuracy, Gain Error, Output Leakage Current, V_{INH}, V_{INL}, I_{IN} and I_{DD} at +25°C and +125°C (SD, TD, UD versions) or +25°C and +85°C (AD, BD, CD versions).

⁴ Full Scale (FS) = $-(V_{REF}) \left(\frac{1023}{1024} \right)$

⁵ Max gain change from T_A = +25°C to T_{min} or T_{max} is ±0.1% FSR.

⁶ Guaranteed, not tested.

⁷ AC parameter, sample tested to ensure specification compliance.

⁸ Absolute temperature coefficient is approximately -300ppm/°C.

Specifications subject to change without notice.

ABSOLUTE MAXIMUM RATINGS
($T_A = +25^\circ\text{C}$ unless otherwise noted)

V_{DD} to GND	-0.3V, +17V
V_{FB} to GND	$\pm 25\text{V}$
V_{REF} to GND	$\pm 25\text{V}$
Digital Input Voltage Range	-0.3V to V_{DD}
Output Voltage (pin 1, pin 2)	-0.3V to V_{DD}
Power Dissipation (Package)	
Plastic (Suffix N)	
To $+70^\circ\text{C}$	670mW
Derates above $+70^\circ\text{C}$ by	8.3mW/ $^\circ\text{C}$

Ceramic (Suffix D)	
To $+70^\circ\text{C}$	450mW
Derates above $+75^\circ\text{C}$ by	6mW/ $^\circ\text{C}$
Operating Temperature Range	
Commercial (JN, KN, LN versions)	0 to $+70^\circ\text{C}$
Industrial (AD, BD, CD versions)	-25°C to $+85^\circ\text{C}$
Military (SD, TD, UD versions)	-55°C to $+125^\circ\text{C}$
Storage Temperature	-65°C to $+150^\circ\text{C}$
Lead Temperature (Soldering, 10 seconds)	$+300^\circ\text{C}$

CAUTION:

1. ESD sensitive device. The digital control inputs are Zener protected; however, permanent damage may occur on unconnected devices subjected to high energy electrostatic fields. Unused devices must be stored in conductive foam or shunts.
2. Do not apply voltages lower than ground or higher than V_{DD} to any pin except V_{REF} (pin 15) and R_{FB} (pin 16).

TERMINOLOGY

RELATIVE ACCURACY: Relative accuracy or end-point nonlinearity is a measure of the maximum deviation from a straight line passing through the endpoints of the DAC transfer function. It is measured after adjusting for ideal zero and full scale and is expressed in % or ppm of full-scale range or (sub) multiples of 1LSB.

RESOLUTION: Value of the LSB. For example, a unipolar converter with n bits has a resolution of $(2^{-n}) (V_{REF})$. A bipolar converter of n bits has a resolution of $[2^{-(n-1)}] (V_{REF})$. Resolution in no way implies linearity.

SETTLING TIME: Time required for the output function of the DAC to settle to within 1/2 LSB for a given digital input stimulus, i.e., 0 to Full Scale.

GAIN ERROR: Gain error or full-scale error is a measure of the output error between an ideal DAC and the actual device output.

FEEDTHROUGH ERROR: Error caused by capacitive coupling from V_{REF} to output with all switches OFF.

OUTPUT CAPACITANCE: Capacity from I_{OUT1} and I_{OUT2} terminals to ground.

OUTPUT LEAKAGE CURRENT: Current which appears on I_{OUT1} terminal with all digital inputs LOW or on I_{OUT2} terminal when all inputs are HIGH.

CIRCUIT DESCRIPTION

GENERAL CIRCUIT INFORMATION

The AD7533, a 10-bit multiplying D/A converter, consists of a highly stable thin film R-2R ladder and ten CMOS current switches on a monolithic chip. Most applications require the addition of only an output operational amplifier and a voltage or current reference.

The simplified D/A circuit is shown in Figure 1. An inverted R-2R ladder structure is used — that is, the binary weighted currents are switched between the I_{OUT1} and I_{OUT2} bus lines, thus maintaining a constant current in each ladder leg independent of the switch state.

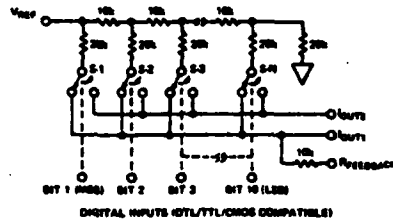


Figure 1. AD7533 Functional Diagram

One of the CMOS current switches is shown in Figure 2. The geometries of devices 1, 2 and 3 are optimized to make the digital control inputs DTL/TTL/CMOS compatible over the full military temperature range. The input stage drives two inverters (devices 4, 5, 6 and 7) which in turn drive the two output N-channels. The "ON" resistances of the switches are binary weighted so the voltage drop across each switch is the same. For example, switch 1 of Figure 2 was designed for an "ON" resistance of 20 ohms, switch 2 for 40 ohms and so on. For a 10V reference input, the current through switch 1 is 0.5mA, the current through switch 2 is 0.25mA, and so on, thus maintaining a constant 10mV drop across each switch. It is essential that each switch voltage drop be equal if the binary weighted current division property of the ladder is to be maintained.

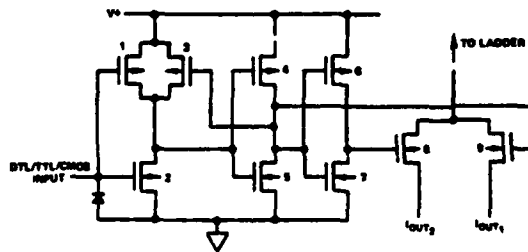


Figure 2. CMOS Switch

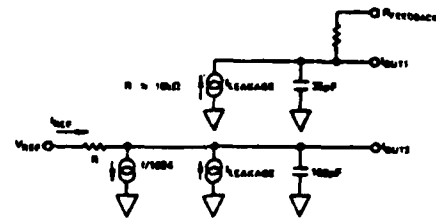


Figure 3. AD7533 Equivalent Circuit — All Digital Inputs Low

EQUIVALENT CIRCUIT ANALYSIS

The equivalent circuits for all digital inputs high and all digital inputs low are shown in Figures 3 and 4. In Figure 3 with all digital inputs low, the reference current is switched to I_{OUT2}. The current source I_{LEAKAGE} is composed of surface and junction leakages to the substrate while the $\frac{I}{1024}$ current source represents a constant 1-bit current drain through the termination resistor on the R-2R ladder. The "ON" capacitance of the output N channel switch is 100pF, as shown on the I_{OUT2} terminal. The "OFF" switch capacitance is 35pF, as shown on the I_{OUT1} terminal. Analysis of the circuit for all digital inputs high, as shown in Figure 4, is similar to Figure 3, however, the "ON" switches are now on terminal I_{OUT1}, hence the 100pF at that terminal.

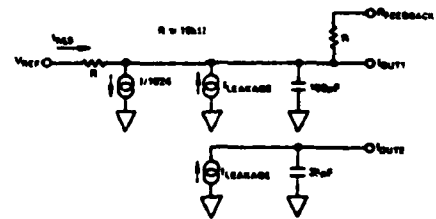


Figure 4. AD7533 Equivalent Circuit — All Digital Inputs High

TTL

TYPES SN54390, SN54LS390, SN54393, SN54LS393, SN74390, SN74LS390, SN74393, SN74LS393 DUAL 4-BIT DECADE AND BINARY COUNTERS

BULLETIN NO. DL-S 7612099, OCTOBER 1976

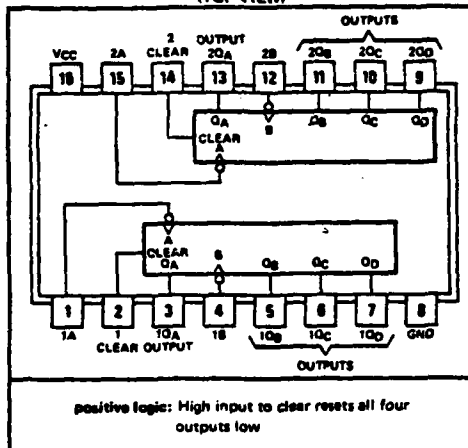
- Dual Versions of the Popular '90A, 'LS90 and '93A, 'LS93
- '390, 'LS390. . . Individual Clocks for A and B Flip-Flops Provide Dual +2 and +5 Counters
- '393, 'LS393. . . Dual 4-Bit Binary Counter with Individual Clocks
- All Have Direct Clear for Each 4-Bit Counter
- Dual 4-Bit Versions Can Significantly Improve System Densities by Reducing Counter Package Count by 50%
- Typical Maximum Count Frequency . . . 35 MHz
- Buffered Outputs Reduce Possibility of Collector Commutation

description

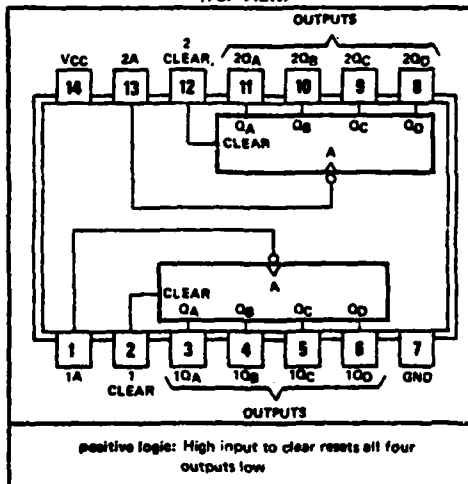
Each of these monolithic circuits contains eight master-slave flip-flops and additional gating to implement two individual four-bit counters in a single package. The '390 and 'LS390 incorporate dual divide-by-two and divide-by-five counters, which can be used to implement cycle lengths equal to any whole and/or cumulative multiples of 2 and/or 5 up to divide-by-100. When connected as a bi-quinary counter, the separate divide-by-two circuit can be used to provide symmetry (a square wave) at the final output stage. The '393 and 'LS393 each comprise two independent four-bit binary counters each having a clear and a clock input. N-bit binary counters can be implemented with each package providing the capability of divide-by-256. The '390, 'LS390, '393, and 'LS393 have parallel outputs from each counter stage so that any submultiple of the input count frequency is available for system-timing signals.

Series 54 and Series 54LS circuits are characterized for operation over the full military temperature range of -55°C to 125°C; Series 74 and Series 74LS circuits are characterized for operation from 0°C to 70°C.

SN54390, SN54LS390 . . . J OR W PACKAGE
SN74390, SN74LS390 . . . J OR N PACKAGE
(TOP VIEW)



SN54393, SN54LS393 . . . J OR W PACKAGE
SN74393, SN74LS393 . . . J OR N PACKAGE
(TOP VIEW)



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7-489

TYPES SN54390, SN54LS390, SN54393, SN54LS393, SN74390, SN74LS390, SN74393, SN74LS393 DUAL 4-BIT DECADE AND BINARY COUNTERS

'390, 'LS390
BCD COUNT SEQUENCE
(EACH COUNTER)
(See Note A)

COUNT	OUTPUT			
	Q _D	Q _C	Q _B	Q _A
0	L	L	L	L
1	L	L	L	H
2	L	L	H	L
3	L	L	H	H
4	L	H	L	L
5	L	H	L	H
6	L	H	H	L
7	L	H	H	H
8	H	L	L	L
9	H	L	L	H

FUNCTION TABLES
'390, 'LS390
BI-QUINARY (5-2)
(EACH COUNTER)
(See Note B)

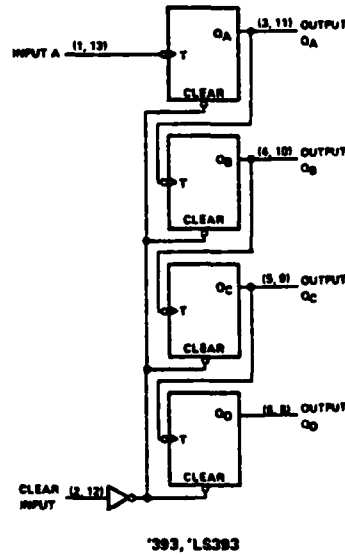
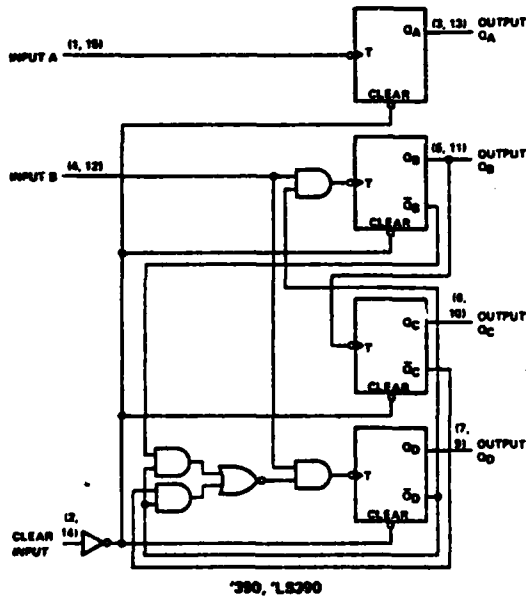
COUNT	OUTPUT			
	Q _A	Q _D	Q _C	Q _B
0	L	L	L	L
1	L	L	L	H
2	L	L	H	L
3	L	L	H	H
4	L	H	L	L
5	H	L	L	L
6	H	L	L	H
7	H	L	H	L
8	H	L	H	H
9	H	H	L	L

'393, 'LS393
COUNT SEQUENCE
(EACH COUNTER)

COUNT	OUTPUT			
	Q _D	Q _C	Q _B	Q _A
0	L	L	L	L
1	L	L	L	H
2	L	L	H	L
3	L	L	H	H
4	L	H	L	L
5	L	H	L	H
6	L	H	H	L
7	L	H	H	H
8	H	L	L	L
9	H	L	L	H
10	H	L	H	L
11	H	L	H	H
12	H	H	L	L
13	H	H	L	H
14	H	H	H	L
15	H	H	H	H

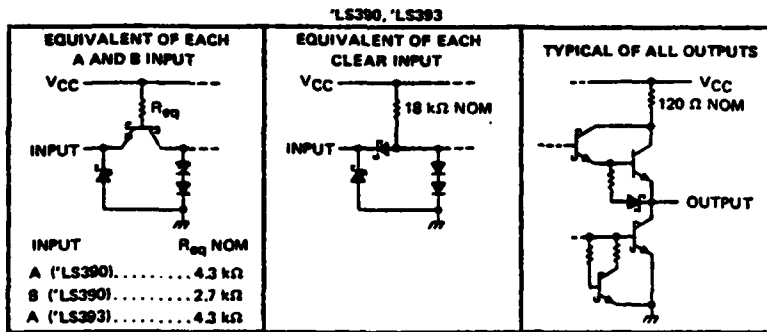
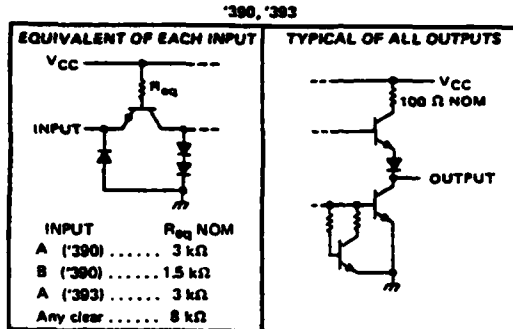
NOTES: A. Output Q_A is connected to input B for BCD count.
B. Output Q_D is connected to input A for bi-quinary count.
C. H = high level, L = low level.

functional block diagrams



**TYPES SN54390, SN54LS390, SN54393, SN54LS393,
SN74390, SN74LS390, SN74393, SN74LS393
DUAL 4-BIT DECADE AND BINARY COUNTERS**

Schematics of inputs and outputs



APPENDIX B

F8 MICROPROCESSOR SOFTWARE

This appendix contains the source codes for the F8 developed in conjunction with the design of the Automatic Threshold Control for the scanner. Assembly listings and linking information for each software module are included. The floppy disc HELP file describing the software package is also included to serve as an overview.

THIS IS THE MAIN DESCRIPTOR FILE FOR THIS DISK.
IT DESCRIBES THE PROGRAMS ON IT AND HOW TO USE THEM.

PROGRAMS MODIFIED AND DEBUGGED
BY
CAPT B. J. STANTON, JUNE 82.

----- USER INFORMATION -----

THE F8 PROVIDES THRESHOLD AND PRINTER CONTROL FOR THE ELECTRO-OPTICAL PAGE SCANNER (EOPS). THE SOFTWARE IS IN A VARIETY OF FORMS DESIGNATED BY THE FILE ATTRIBUTE:

- '00' IS A TEXT FILE SUCH AS THIS ONE OR ONE CONTAINING UNASSEMBLED SOURCE CODE.
- '10' IS AN OBJECT CODE FILE THAT CAN BE LOADED AND/OR LINKED, DEPENDING ON THE NATURE OF THE SOFTWARE.
- '30' IS A CORE IMAGE FILE THAT (WHEN LOCATED ON DISK DRIVE 0) IS LOADED AND EXECUTED AS A SYSTEM-LEVEL COMMAND WHEN THE FILENAME IS ENTERED.
- '40' IS AN EXECUTIVE FILE FOR FACILITATING VARIOUS FILE OPERATIONS.

THE FILES EOPS1,30:1 AND EOPS2,30:1 ARE COMPLETE SOFTWARE PACKAGES. EOPS1 AND EOPS2 ARE DISTINGUISHED BY THEIR THRESHOLD SAMPLING ALGORITHMS. EOPS1 HAS AN INITIAL STEP SIZE (S1) OF 128 AND SAMPLES THE ENTIRE RANGE 8 N (0 TO 1024). EOPS2 HAS AN INITIAL STEP SIZE OF 64 AND SAMPLES THE RANGE OF N (128 TO 640). TO USE EITHER OF THESE PACKAGES, FIRST INSURE THE DESIRED PACKAGE IS LOADED ONTO DISK DRIVE 0. YOU MAY WANT TO MAKE A COPY OF ONE OF THESE FILES ON DRIVE 0 BY EXECUTING A COMMAND SUCH AS:

COPY FILE EOPS1,30:1

TO PUT THE F8 INTO THE EOPS MODE, CALL THE APPROPRIATE SOFTWARE PACKAGE BY TYPING ITS NAME:

EOPS1

ONCE THE SOFTWARE IS LOADED AND RUNNING, USER CONTROL IS PROVIDED THROUGH THE 'SENSE' SWITCHES ON THE FRONT PANEL OF THE F8. THE FUNCTIONS ARE:

SENSE #	DOWN	UP
= 4	NORMAL OPERATION	RETURN TO DOS4
= 5	NORMAL PAGE	INFINITE LINES
= 6	AUTOMATIC THRESHOLD	THRESHOLD FREEZE
= 7	SOFT COPY	HARD COPY

SENSE 4 IS USED TO EXIT EOPS MODE AND RETURN CONTROL OF THE F8 TO THE ZENITH KEYBOARD. (CAUTION: THIS SWITCH MUST BE DOWN WHEN ENTERING EOPS) OTHERWISE AN IMMEDIATE JUMP BACK TO THE OPERATING SYSTEM WILL OCCUR.

SENSE 5 IS USED FOR CALIBRATION AND CAUSES THE LINE COUNTER TO BE DISABLED SO THAT, WITH THE SCANNER IN "FLEET MODE" THE SOFTWARE WILL CONTINUE TO ACQUIRE AN INFINITE STREAM OF LINES WITHOUT ENDING THE PAUL. WHEN SENSE 5 IS RETURNED TO TO THE DOWN POSITION THE SOFTWARE IMMEDIATELY EXECUTES THE END OF PAGE SEQUENCE AND RESETS.

SENSE 6 IS USED FOR CONTROL OF THE AUTOMATIC THRESHOLD FEATURE. IN AUTOMATIC THRESHOLD MODE, 28 LINES OF THE LEADING MARGIN CONTAINING THE TEST PATTERN ARE SAMPLED TO OBTAIN THE OPTIMUM THRESHOLD FOR EXISTING CONDITIONS. THE VALUE OF THE SELECTED THRESHOLD IS DISPLAYED ON THE SCREEN IN HEX. IN THRESHOLD FREEZE MODES, THE LAST THRESHOLD SET BY THE SOFTWARE IS RETAINED AND DISPLAYED ON THE SCREEN. NOTE: IF THE THRESHOLD IS ALTERED FROM THE FRONT PANEL OR BY OTHER DEBUGGING MEANS, THE MESSAGE TO THE SCREEN WILL NOT REFLECT THE ALTERATION.

SENSE 7 SELF EXPLANATORY.

EOPS IS IN TURN COMPOSED OF SMALLER LINKABLE SOFTWARE PACKAGES. THESE MODULES ARE DESCRIBED BELOW:

MAIN4 ----- MAIN CALLING PROGRAM, VERSION 4

THIS MODULE CONTAINS THE MAINLINE ROUTINES OF EOPS AND THEREFORE MUST BE AT THE BEGINNING LINK. IT CONTAINS ALL INITIALIZATIONS, SENSE SWITCH CONTROLS, LINE COUNTERS, COMMAND TRANSMISSIONS, CRT SCREEN PROMPTS, AND ATC CALLS. IT ALSO INITIALIZES THE SAMPLING ALGORITHM, QSET, THEREBY CONTROLLING SAMPLING RANGE AND INITIAL STEP SIZE (SI).

FSTLN ----- FIRST LINE

THIS SUBROUTINE POLLS THE SIGNAL CALLED 'PRINTLINE' WHICH IS PRESENT ON INPUT PORT 4 IN THE LEAST SIGNIFICANT BIT POSITION. THE PROGRAM IS DESIGNED TO DETECT A RISING TRANSITION OF THE INPUT SIGNAL. THIS IS ACCOMPLISHED BY LOOPING UNTIL THE SIGNAL IS FALSE AND THEN LOOPING UNTIL IT IS TRUE. WHEN THIS PROGRAM RETURNS, THE TRANSITION WILL HAVE JUST OCCURRED. THE SOFTWARE IS DESIGNED TO TAKE INTO ACCOUNT THE INVERSION THAT TAKES PLACE THROUGH THE FB I/O PORT. THEREFORE THIS MODULE ACTUALLY SENSES A DOWNWARD TRANSITION OF THE SIGNAL 'PRINTLINE' IN THE SCANNER. THE GOAL IS TO CATCH THIS DOWNWARD TRANSITION WHICH SIGNALS THE END OF A LINE OF VIDEO INFORMATION.

ENDLN ----- END OF LINE

THIS SUBROUTINE IS A SLIGHTLY MORE COMPLEX VERSION OF FSTLN. IT ALSO DETECTS A FALLING TRANSITION OF 'PRINTLINE' HOWEVER, IT IS DESIGNED TO WAIT FOR THIS TRANSITION FOR 10 MS. THIS FEATURE WAS INCLUDED TO PREVENT THE SOFTWARE FROM GETTING HUNG UP AND OUT OF SYNC IF THE SCANNER SHOULD EITHER STOP IN MIDPAGE OR PRODUCE A FALSE START. IN THE EVENT THAT THIS SUBROUTINE MUST WAIT MORE THAN 10 MS, IT SETS THE LINE COUNTER TO THE LAST LINE SO THAT WHEN THE RETURN TO THE MAIN PROGRAM OCCURS, THE LAST LINE CONDITION WILL BE INVOKED AND THE SOFTWARE WILL RESET. SHOULD IT BE NECESSARY TO HAVE THE SCANNER FROZEN IN MIDPAGE AND STILL HAVE THE SOFTWARE OPERATING SYNCHRONOUSLY WITH THE SCANNER (FOR ALIGNMENT ETC.), SENSE SWITCH 6 SHOULD BE USED.

YMITS ----- TRANSMIT COMMAND

THIS IS THE SIMPLEST OF ALL THE SUBROUTINES. IT IS THE ONE WHICH ACTUALLY SENDS THE COMMANDS TO THE PRINTER OR THE TEKTRONICS DISPLAY. IT EXPECTS THE COMMAND CHANNEL IN THE INTERFACE BOARD TO HAVE ALREADY BEEN OPENED AND THE COMMAND FOR TRANSMISSION TO BE STORED IN REGISTER 9.

QSET ----- QUICK THRESHOLD SAMPLING ALGORITHM

THIS MODULE SAMPLES THE RANGE OF THRESHOLD VALUES BY USING PROGRESSIVELY SMALLER AND SMALLER STEP SIZES. EACH TIME QSET IS CALLED, THE EXISTING STEP SIZE WILL BE USED FOR SEVEN SAMPLES AND WILL THEN BE DIVIDED BY FOUR BEFORE CONTROL IS RETURNED TO THE MAIN CALLING PROGRAM. WITH EACH VALUE OF N, VTC IS COMPARED TO THE PREVIOUS MAXIMUM VTC (MTC). THE VALUE OF N PRODUCING THE OVERALL MAXIMUM VALUE OF VTC IS STORED FOR EITHER THE NEXT INVOCATION OF QSET OR FOR THE MAIN CALLING PROGRAM TO LOAD INTO PORTS 12 AND 13 AS THE OPTIMUM THRESHOLD VALUE FOR THE PAGE TO BE SCANNED.

***** EXAMPLES *****

SHOULD IT BE NECESSARY TO REASSEMBLE AND RELINK THE LOPS SOFTWARE PACKAGE, THE FOLLOWING SEQUENCE OF COMMANDS WILL PRODUCE THIS RESULT:

```
ASM MAIN4,00:1 TO MAIN4,10:1 NOLIST ERRS
ASM FSTLN,00:1 TO FSTLN,10:1 NOLIST ERRS
ASM ENDLN,00:1 TO ENDLN,10:1 NOLIST ERRS
ASM YMITS,00:1 TO YMITS,10:1 NOLIST ERRS
ASM QSET ,00:1 TO QSET ,10:1 NOLIST ERRS
```

```
LINK 1 CLEAR DPG 0 MAIN4,10:1
LINK 1 FSTLN,10:1
LINK 1 ENDLN,10:1
LINK 1 YMITS,10:1
LINK 1 QSET ,10:1
```

THE SOFTWARE IS NOW LOADED IN RAM AND READY FOR EXECUTION EITHER FROM THE FRONT PANEL OR BY USING THE F8 DEBUG SOFTWARE. SHOULD IT BE NECESSARY TO CREATE A FILE FROM THE ABOVE MODULES THAT CAN BE LOADED WITH A SINGLE COMMAND, THE FOLLOWING COMMANDS CAN BE USED:

```
ASS DO DISK FILENAME,10:1
DUMP 0000-0255
```

THIS PACKAGE WILL BE STORED ON DISK, AND CAN BE LOADED INTO RAM AT ANY TIME BY THE COMMAND:

```
LOAD FILENAME,10:1
TO EXECUTE THE PROGRAM LOADED IN THIS MANNER, USE THE F8 FRONT PANEL:
```

```
HALT
```

CLEAR DISPLAY
LD ADDRESS
RUN

IF THE USER WISHES TO HAVE A FILE WHICH LOADS AND ALSO
AUTOMATICALLY EXECUTES FROM THE SYSTEM DISK, IN PLACE OF THE
ABOVE EXAMPLE, THESE FOLLOWING COMMANDS CAN BE EXECUTED:

CC1 FILENAME.JC:1 0000-0255
COPY FILE FILENAME.JC:1

THIS LAST COMMAND PLACES A COPY OF THE CORE IMAGE ON THE
SYSTEM DISK WHERE IS WILL BE FOUND BY THE OPERATING SYSTEM
IN RESPONSE TO THE USER TYPING 'FILENAME', SINCE THE SYSTEM
LOOKS FOR LOAD-AND-EXECUTE FILES ON DRIVE 0 WHERE THE SYSTEM
DISK USUALLY RESIDES.

IT MUST BE NOTED THAT THESE COMMANDS TO CREATE NEW COPIES OF THE
OPERATING PROGRAMS MUST BE EXECUTED IMMEDIATELY FOLLOWING THE
LINKING OPERATION SINCE SOME OF THE OTHER FDS PROGRAMS (LIKE
THE ASSEMBLER AND THE EDITOR) OBSCURE THE LOWER ADDRESSES OF
THE MEMORY WHERE THE SCANNER PROGRAMS ARE LOADED.

ON THIS DISK THE FILES EOPS1.JC:1 AND EOPS2.JC:1 ARE AUTOMATIC
LOAD-AND-EXECUTE FILES WHICH CAN BE COPIED TO A DISK IN DRIVE 0
FOR IMMEDIATE USE.

FOR FURTHER INFORMATION CONCERNING THE OPERATION OF THE FS AND
ITS OPERATING SYSTEM FDS, CONSULT THE USERS MANUALS SUPPLIED
WITH THE SYSTEM.

MAIN CALLING PROGRAM-VERSN 4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0000 0001 MAIN4   RORG   0
0002 *
0003 *           TITLE 'MAIN CALLING PROGRAM-VERSN 4'
0004 *
0005 * WRITTEN BY CAPT B. J. STANTON, 21 JUN 82
0006 * EDITED 21 JULY 82.
0007 * THIS IS THE MAIN CALLING PROGRAM FOR THE
0008 * ELECTRO-OPTICAL PAGE SCANNER. IT MUST BE
0009 * LINKED FIRST WHEN BUILDING THE SOFTWARE
0010 * PACKAGE 'EGPS-'
0011 *
0012 * THE USE OF THE FS FRONT PANEL SENSE SWITCHES:
0013 *
0014 * #           DOWN           UP
0015 *-----
0016 * 4   NORMAL OPERATION      RETURN TO DOS4
0017 * 5   NORMAL PAGE           INFINITE LINES
0018 * 6   AUTOMATIC THRESHOLD   THRESHOLD FREEZE
0019 * 7   SOFT COPY             HARD COPY
0020 *-----
0021 *
0022 *
2330 0023 DOS4    EQU    H'2330'
0006 0024 LINEU   EQU    6           LINE CNTR HIGH BYTE
00A4 0025 LINEL   EQU    164        LINE CNTR LOW BYTE
0026 *
0027 * CODES FOR PORT 8
0028 *
0000 0029 ENCHD   EQU    H'00'        CODE FOR CMD CHANNEL
0020 0030 ENCCD   EQU    H'20'        CCD CHANNEL CMS
0040 0031 ENSENS  EQU    H'40'        CONN INP SW TO PRT4
0032 *
0033 * DEVICE ADDRESSES (FOR PORT 8)
0034 *
0001 0035 ADHARD  EQU    H'01'        ADDRESS OF PRINTER
0008 0036 ADSOFT  EQU    H'08'        ADDR OF TEX. DISPL
0037 *
0038 * CODES FOR PORT 9
0039 *
0002 0040 LEADDR  EQU    H'02'        ADDR LOAD CODE
0041 *
0042 * DEVICE COMMANDS SENT THRU PORT 9, AND
0043 * CONTROLLED BY PORT 9
0044 *
0003 0045 HARLMJ  EQU    H'08'        LEFT MARG JUSTIFY
0000 0046 HARFIL  EQU    H'00'        FILL,PRT LINE BUFF
0003 0047 HARDAV  EQU    H'03'        ADVANCE ONE LINE
000F 0048 HARDCUT EQU    H'0F'        CUT PAPER
0037 0049 HARDOFF EQU    H'37'        SHUT OFF PTR (PUMPS)
0006 0050 SOFTEN  EQU    H'06'        ENBLE SOFTCOPY DISPL
0003 0051 SOFTDSB  EQU    H'03'        DSBL SOFTCOPY DISPL
0001 0052 SOFTERS  EQU    H'01'        ERASE SOFTCOPY DISPL
0002 0053 SOFTRSY  EQU    H'02'        RESET Y COUNTER
0004 0054 SOFTINY  EQU    H'04'        INCREMENT Y COUNTER
0055 *
0056 *
0057 * LINKING INFO
0058 *           EXTRN ENDR,FSTLN,YNITE,RESET
0059 *
0060 *
0061 *

```

MAIN 9995	CALLING LOC	PROGRAM-VERSION OBJECT ADDR	LINE LINE	SOURCE STATEMENT			
0000	1A	0052	0052	DI	DISABLE INTERRUPTS		
0001	71	0053	0053	LI	1	RESET INTERFACE	
0002	39	0054	0054	OUTS	9		
0003	70	0055	0055	CLR			
0004	39	0056	0056	OUTS	9		
0005	2000	0057	0057	LI	ENCMD	SET FOR CMD XMIT	
		0058	0058	=			
		0059	0059	-----DATA CHANNEL CLOSED			
		0070	0070	=			
0007	35	0071	0071	OUTS	5		
		0072	0072	=			
0008	2040	0073	0073	BEGIN	LI	ENSENS	ENABLE SCANNER INPUT
000A	35	0074	0074	OUTS	5		
000B	70	0075	0075	CLR		LOOP TILL	
000C	34	0076	0076	OUTS	4	INIT = 0	
000D	A4	0077	0077	INS	4		
000E	2102	0078	0078	NI	H'02'	INIT = BIT 2	
0010	94F7	0008 0079	0079	BNZ	BEGIN		
		0080	0080	=			
0012	70	0081	0081	BEGIN2	CLR	TEST FOR QUIT SIG	
0013	30	0082	0082	OUTS	0	ON FB SENSE 4	
0014	A0	0083	0083	INS	0		
0015	2110	0084	0084	NI	H'10'		
0017	34C4	001C 0085	0085	BZ	SKIPM		
0019	292330	2330 0086	0086	JMP	0054	RETURN TO 005	
		0087	0087	=			
001C	70	0088	0088	SKIPM	CLR	LOOP TILL	
001D	34	0089	0089	OUTS	4	INIT = 1	
001E	A4	0090	0090	INS	4		
001F	2102	0091	0091	NI	H'02'	INIT = BIT 2	
0021	84F0	0012 0092	0092	BZ	BEGIN2		
		0093	0093	=			
		0094	0094	-----DELAY LOOP-----			
		0095	0095	=			
0023	70	0096	0096	CLR		WAIT 2.3 MS	
0024	1F	0097	0097	DLI	INC		
0025	94FE	0024 0098	0098	BNZ	DLI		
		0099	0099	=			
		0100	0100	-----END DELAY-----			
		0101	0101	=			
0027	70	0102	0102	CLR		CHECK START AGAIN	
0028	34	0103	0103	OUTS	4		
0029	A4	0104	0104	INS	4		
002A	2102	0105	0105	NI	H'02'		
002C	84E5	0012 0106	0106	BZ	BEGIN2		
		0107	0107	=			
002E	70	0108	0108	CLR		GET FB SENSE 7	
002F	30	0109	0109	OUTS	0	FOR HARD/SOFT OUTPUT	
0030	A0	0110	0110	INS	0		
0031	2150	0111	0111	NI	H'80'		
0033	55	0112	0112	LR	3.4		
		0113	0113	=			
0034	48	0114	0114	LR	A.3	USE REGS FOR HDR/STP	
0035	2500	0115	0115	CI	H'00'		
0037	3411	0049 0116	0116	BZ	SOFT		
		0117	0117	=			
0039	2001	0118	0118	HARD	LI	ADHARD	SETUP FOR PRINTER
003B	3E	0119	0119	OUTS	3		
003C	2008	0120	0120	LI	LDADDR	STORE PRINTER ADDR	
003E	39	0121	0121	OUTS	9		
003F	70	0122	0122	CLR			

MAIN CALLING PROGRAM-VERSN 4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0040 59          0123      OUTS  9
0041 2003        0124      LI     HARLMJ  START PUMPS IN PRTR
0043 59          0125      LR     9.A
0044 280000 0000 0126      PI     YMITS
0047 9015       005D 0127      BR     SKIPI
          0128      *
0049 2003        0129      SOFT   LI     ADSOFT  SETUP FOR TEK-DISPL
004B 38          0130      OUTS  5
004C 2008        0131      LI     LDADDR  STORE TEK ADDR
004E 39          0132      OUTS  9
004F 70          0133      CLR
0050 39          0134      OUTS  9
0051 2002        0135      LI     SOFTSY  INITIALIZE TEK-DISPL
0053 59          0136      LR     9.A
0054 280000 0000 0137      PI     YMITS
0057 2001        0138      LI     SOFTERS  ERASE SCREEN
0059 59          0139      LR     9.A
005A 280000 0000 0140      PI     YMITS
          0141      *
          0142      *****DELAY LOOPS*****
          0143      *
005D 20FA        0144      SKIPI  LI     0'250'  DELAY FOR PUMPS OR
005F 52          0145      LR     2.A      SUPPEN ERASE
0060 20C3        0146      LOOPO  LI     0'200'
0062 53          0147      LR     3.A
0063 33          0148      LOOPI  DS     3
0064 94FE        0063 0149      BNZ   LOOPI
0066 32          0150      DS     2
0067 94FE        0060 0151      BNZ   LOOPO
          0152      *
          0153      *****END DELAY*****
          0154      *
0069 280000 0000 0155      PI     FSTLN  WAIT FOR FIRST LINE
          0156      *
          0157      * CHECK FOR AUTO THRESHOLD DISABLE-----
          0158      *
006C 70          0159      CLR
006D 30          0160      OUTS  0
006E A0          0161      INS  0
006F 2140        0162      NI     X'40'
0071 9455        00C7 0163      BNZ   PRZ
          0164      *
          0165      *****
          0166      * BEGIN AUTOMATIC THRESHOLD SETTING SEQUENCE
          0167      *****
0073 70          0168      CLR
          0169      LR     6.A      MAX DIGITAL VIDEO
0074 56          0169      LR     7.A      (MTC) INITIALIZED
0075 57          0170      LR     7.A      TO ZERO
          0171      *
          0172      * INITIALIZE FOR THRESHOLD SAMPLING-----
          0173      *
          0174      ***** NOTE!!! *****
          0175      *
          0176      * AS IT STANDS NOW, QSET IS INITIALIZED TO
          0177      * SAMPLE THE RANGE 128 TO 540 WITH AN
          0178      * INITIAL STEP SIZE OF 64 AS DOCUMENTED FOR
          0179      * THE SOFTWARE PACKAGE, 'EDPS2'.
          0180      *
          0181      * TO SAMPLE THE ENTIRE RANGE OF N (0 TO 1024)
          0182      * SCRATCH REGISTER 5 MUST BE LOADED WITH ZERO
          0183      * AND SCRATCH REGISTER 3 MUST BE LOADED WITH

```

MAIN CALLING PROGRAM-VERSN 4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0184 = 128.
0185 =
0186 =====
0187 =
0188 =
0076 54          0189          LR      4,A      THRESHOLD SET TO
0077 2080        0190          LI      128      START AT 128
0079 55          0191          LR      5,A
007A 2040        0192          LI      64      STEP SIZE INITIALIZE
007C 53          0193          LR      3,A      TO 64
0194 =
0195 = TAKE FOUR PASSES (AT 7 LINES PER PASS)-----
0196 =
007D 280000 0000 0197          PI      QSET
0080 280000 0000 0198          PI      QSET
0083 280000 0000 0199          PI      QSET
0086 280000 0000 0200          PI      QSET
0201 =
0202 = LOAD OPTIMUM THRESHOLD-----
0203 =
0089 02          0204          LR      A,QU
008A 2713        0205          OUT     H'13'
008C 03          0206          LR      A,QL
008D 2712        0207          OUT     H'12'
0208 =
0209 = DISPLAY OPTIMUM THRESHOLD-----
0210 =
008F 2A017E 017E 0211  SHOW     DCI     MSG1+21
0092 2C          0212          XDC
0093 2A0197 0197 0213          DCI     MSG2+22
0096 02          0214          LR      A,QU
0097 2430        0215          AI      H'30'
0099 2539        0216          CI      H'39'
009B 3103        009F 0217          BP      SH1
009D 2407        0218          AI      H'07'
009F 17          0219  SH1     ST
00A0 2C          0220          XDC
00A1 17          0221          ST
00A2 03          0222          LR      A,QL
00A3 14          0223          SR      4
00A4 2430        0224          AI      H'30'
00A6 2539        0225          CI      H'39'
00A8 3103        00AC 0226          BP      SH2
00AA 2407        0227          AI      H'07'
00AC 17          0228  SH2     ST
00AD 2C          0229          XDC
00AE 17          0230          ST
00AF 03          0231          LR      A,QL
00B0 210F        0232          NI      H'0F'
00B2 2430        0233          AI      H'30'
00B4 2539        0234          CI      H'39'
00B6 3103        00BA 0235          BP      SH3
00B8 2407        0236          AI      H'07'
00BA 17          0237  SH3     ST
00BB 2C          0238          XDC
00BC 17          0239          ST
0240 =
00BD 2A0169 0169 0241          DCI     MSG1
00C0 71          0242          LIS     1
00C1 3C          0243          LR      3,A
00C2 293653 3653 0244          PI      H'3653'

```

MAIN CALLING PROGRAM-VERSN 4
 WRS LOC SUBJECT ADDR LINE

SOURCE STATEMENT

```

00C5 2009 00CF 0245 BF BJA
0246 *
0247 *****
0248 * END AUTOMATIC THRESHOLD SETTING SEQUENCE
0249 *****
0250 *
00C7 2A0181 0181 0251 FRZ DCI MSG2
00CA 71 0252 LIS 1
00CB 30 0253 LR 0,A
00CC 283653 3653 0254 PI H'3653'
0255 *
00CF 2005 0256 BJA LI LINEU INITIALIZE LINE CTR
00D1 50 0257 LR 0,A SC IS HIGH BYTE
00D2 20A4 0258 LI LINEL
00C4 51 0259 LR 1,A SI IS LOW BYTE
0260 *
00D5 2000 0261 LI ENCMD OPEN UP CMD CHANNEL
00D7 35 0262 OUTS 5
00D8 48 0263 NEWLN LR A,8
00D9 2500 0264 CI H'00'
0265 *
00DB 342E 01CA 0266 BZ NLSOFT
0267 *
00DD 200B 0268 NLHARD LI HARDEMU SEND MUJ
00DF 59 0269 LR 0,A
00E0 280000 0000 0270 PI XNITS
0271 *
0272 *****DELAY*****
0273 *
00E3 20FE 0274 LI 254 WAIT 18 US
00E5 1F 0275 DL1 INC
00E6 94FE 00E5 0276 BNZ DL1
0277 *
0278 *****END DELAY***
0279 *
00E8 2020 0280 LI ENCCD OPEN DATA CHAN
0281 -----DATA CHANNEL OPEN
00EA 35 0282 OUTS 5
0283 *
00EB 280000 0000 0284 PI ENDLN WAIT FOR END OF LINE
0285 *
00EE 2000 0286 LI ENCMD OPEN CMD CHANNEL
0287 -----DATA CHANNEL CLOSED -----
00F0 35 0288 OUTS 5
0289 *
00F1 2000 0290 LI HARDFIL SEND FILL CMD
00F3 59 0291 LR 0,A
00F4 280000 0000 0292 PI XNITS
0293 *
0294 *****DELAY*****
0295 *
00F7 20F0 0296 LI 240 WAIT 144 US
00F9 1F 0297 DL2 INC
00FA 94FE 00F9 0298 BNZ DL2
0299 *
0300 *****END DELAY*****
0301 *
00FC 2003 0302 LI HARDAV ADVANCE PAPER
00FE 59 0303 LR 0,A
00FF 280000 0000 0304 PI XNITS
0305 *

```


MAIN CALLING PROGRAM-VERSN 4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0306 *****DELAY*****
0307 *
0102 20FE 0308 LI 254 WAIT 18 US
0104 1F 0309 DL3 INC
0105 94FE 0104 0310 SNZ DL3
0311 *
0312 *****END DELAY*****
0313 *
0107 290132 0132 0314 JMP ENDCHK CHECK FOR LAST LINE
0315 *
0316 *
0317 *
010A 2006 0318 NLSOFT LI SOFTEN ENABLE TEK DISPLAY
010C 59 0319 LR 9,A
010D 280000 0000 0320 PI XMTS
0321 *
0322 *****DELAY*****
0323 *
0110 20FE 0324 LI 254 WAIT 18 US
0112 1F 0325 DL4 INC
0113 94FE 0112 0326 SNZ DL4
0327 *
0328 *****END DELAY*****
0329 *
0115 2020 0330 LI ENOCD OPEN DATA CHAN
0331 -----DATA CHANNEL OPEN
0117 35 0332 OUTS 5
0333 *
0118 280000 0000 0334 PI ENDLN WAIT FOR EOL SIG
0335 *
0119 2000 0336 LI ENCMD OPEN CMD CHANNEL
0337 -----DATA CHANNEL CLOSED
011D 35 0338 OUTS 5
0339 *
011E 20C3 0340 LI SOFTLSB DISABLE TEK-DISPLAY
0120 59 0341 LR 9,A
0121 280000 0000 0342 PI XMTS
0343 *
0124 20C4 0344 LI SOFTINY SEND INCREMENT Y CMD
0126 59 0345 LR 9,A
0127 280000 0000 0346 PI XMTS
0347 *
0348 *****DELAY*****
0349 *
012A 20FE 0350 LI 254
012C 1F 0351 DL5 INC WAIT 18 US
012D 94FE 012C 0352 SNZ DL5
0353 *
0354 *****END DELAY*****
0355 *
012F 290132 0132 0356 JMP ENDCHK
0357 -----
0132 70 0358 ENDCHK CLR IF FB SENSE 5
0133 20 0359 OUTS 0 =1 THEN LOOP
0134 A0 0360 INS 0 UNTIL FB SENSE
0135 2120 0361 NI H'2C' =0
0137 2500 0362 CI H'0C'
0139 3407 0141 0363 ST NORMONT
013B 2001 0364 LI H'01'
013C 51 0365 LR 1,A
013E 2000 0366 LI H'00'

```

MAIN CALLING PROGRAM-VERSN 4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

0140	50		0367	LR	C,A	
0141	41		0368	NORMCNT	LR	A,1
0142	240C		0369	AI	0	CHECK FOR LAST LINE
0144	9407	014C	0370	BNZ	OK	
0146	4C		0371	LR	A,0	
0147	2400		0372	AI	0	
0149	3406	0150	0373	BZ	DONE	
0148	30		0374	DS	0	
014C	31		0375	JK	DS	1
014D	2900D8	00D8	0375	JMP	NEWLN	
0150	45		0377	DONE	LR	A,5
0151	2500		0375	CI	X'00'	
0153	3412	0166	0379	BZ	SKIPSOF	
			0380	=		
			0381	=	PRINTER FINAL SECTION-----	
			0382	=		
0155	200F		0383	LI	HARDCUT	SEND OUT CMD
0157	59		0384	LR	9,A	
0159	280000	0000	0385	PI	XMITS	
			0386	=		
			0387	=	*****DELAY	
			0388	=		
0155	2076		0389	LI	246	
015D	1F		0390	CDL	INC	WAIT FOR OUT/
015E	94FE	015D	0391	BNZ	CDL	
			0392	=		
			0393	=	*****END DELAY	
			0394	=		
0160	2037		0395	LI	HARDOFF	SEND PRINTER OFF CMD
0162	59		0396	LR	9,A	
0163	290000	0000	0397	PI	XMITS	
			0398	=		
			0399	=		
			0400	=		
0166	290005	0005	0401	SKIPSOF	JMP	OVER RUN PROGRAM AGAIN
			0402	=		
			0403	=		
0169	0016		0404	MSG1	DC	HL2'0016'
016B	544852		0405	DC	C'THRESHOLD RESET '	
017B	544F20		0406	DC	C'TO ***'	
0181	0017		0407	MSG2	DC	HL2'0017'
0183	544852		0408	DC	C'THRESHOLD FROZEN '	
0194	415420		0409	DC	C'AT ***'	
			0410	=		
			0411	=		
			0412	END		

00 ERRS

```

FSTLN
ERRS LOC OBJECT ADDR LINE SOURCE STATEMENT

0000 0001 FSTLN RORG 0
0002 TITLE 'FSTLN'
0003 *
0004 * WRITTEN BY RALPH L. VINCIGUERRA 12/90
0005 *
0006 * THIS IS A SUBR WHICH WAITS FOR THE
0007 * SIGNAL CALLED PRINTLINE TO MAKE A
0008 * RISING TRANSITION SIGNALLING THE
0009 * END OF A SCAN LINE, AND TIME TO
0010 * SEND COMMANDS.
0011 * DUE TO AN INVERSION IN THE
0012 * INTERFACE THE ACTUAL LINE IN THE
0013 * SCANNER MAKES A FALLING TRANSITION.
0014 *
0015 *
0040 0016 ENSENS EQU H'40'
0017 *
0018 *
0000 2040 0019 LI ENSENS ENABLE SENSE INPUTS
0002 35 0020 DUTS 5
0021 *
0003 70 0022 LPI CLR LOOP UNTIL FALSE
0004 34 0023 DUTS 4
0005 A4 0024 INS 4
0006 2101 0025 NI H'01'
0007 34FA 0003 0026 BNZ LPI
0008 70 0027 LP2 CLR LOOP UNTIL TRUE
0009 34 0028 DUTS 4
000C A4 0029 INS 4
000D 2101 0030 NI H'01'
000F 34FA 000A 0031 BZ LP2
0011 1C 0032 POP
0033 END

00 ERRS

```

```

ENDLN
ERRS LOC OBJECT ADDR LINE          SOURCE STATEMENT

0000 0001  ENDLN  RORG 0
0002          TITLE 'ENDLN'
0003          *
0004          * WRITTEN BY RALPH L. VINCIGUERRA 12/30
0005          *
0006          * THIS IS A SUBR WHICH WAITS FOR THE
0007          * SIGNAL CALLED PRINTLINE TO MAKE A
0008          * RISING TRANSITION SIGNALLING THE
0009          * END OF A SCAN LINE, AND TIME TO
0010          * SEND COMMANDS.
0011          * DUE TO AN INVERSION IN THE
0012          * INTERFACE THE ACTUAL LINE IN THE
0013          * SCANNER MAKES A FALLING TRANSITION.
0014          *
0015          *
0016          * THIS SUBR ALSO WILL ONLY WAIT
0017          * ABOUT 10MS FOR THE
0018          * TRANSITION TO OCCUR. IF THE TRANSITION
0019          * TAKES MORE THE LINE COUNTER IS SET
0020          * THE THE END OF THE PAGE AND THE
0021          * MAIN PROGRAM CONCLUDES.
0040 0022  ENSENS  EGU  H'40'
0023          *
0024          *
0000 2040 0025          LI  ENSENS  ENABLE SENSE INPUTS
0002 35   0026          OUTS  5
0027          *
0003 20FF 0028          LI  D'255'
0005 59   0029          LR  9.A  INITIALIZE CNT REG
0030          *
0006 70   0031  LP1   CLR  LOOP UNTIL FALSE
0007 34   0032          OUTS  4
0008 A4   0033          INS  4
0009 2101 0034          NI  H'01'
000B 2406 0012 0035          BZ  RDY
000D 39   0036          DS  9
000E 2410 001F 0037          BZ  DUMPOUT
0010 20FS 0006 0038          BR  LP1
0039          *
0012 20FF 0040  RDY   LI  D'255'
0014 59   0041          LR  9.A
0015 70   0042  LP2   CLR  LOOP UNTIL TRUE
0016 34   0043          OUTS  4
0017 A4   0044          INS  4
0018 2101 0045          NI  H'01'
001A 2408 0023 0046          BZ  30
001C 39   0047          DS  9
001D 2477 0015 0048          BZ  LP2
001F 2000 0049  DUMPOUT LI  D'00'
0021 50   0050          LR  0.A
0022 51   0051          LR  1.A
0023 1C   0052          GO  POP
0053          END

CO ERRS

```

```

XMTS
ERRS LOC OBJECT ADDR LINE          SOURCE STATEMENT
                                0000 0001 XMTS      RORS 0
                                0002 *
                                0003 *          TITLE 'XMTS'
                                0004 *
                                0005 * WRITTEN BY RALPH L. VINCIGUERRA 12/80
                                0006 *
                                0007 *
                                0008 * THIS SUBR IS USED TO SEND THE COMMANDS
                                0009 * TO THE PRINTER OR THE TEK DISPLAY.
                                0010 * IT EXPECTS THAT THE COMMAND CHANNEL
                                0011 * HAS ALREADY BEEN OPENED THRU PORT 5,
                                0012 * AND THAT THE COMMAND TO BE SENT IS
                                0013 * WAITING IN REGISTER 9 TO BE SENT TO
                                0014 * PORT 9.
                                0015 *
                                0000 49 0016 *          LR      A:9      PUT CMD ON PORT 9
                                0001 39 0017 *          JUTS   9
                                0002 2010 0018 *          LI     R'10'     LOAD CMD INTO LOGIC
                                0004 39 0019 *          JUTS   9
                                0005 70 0020 *          CLR
                                0006 39 0021 *          OUTS   9
                                0007 2002 0022 *          LI     R'02'     SEND SYNC PULSE
                                0009 39 0023 *          JUTS   9
                                000A 70 0024 *          CLR
                                000B 39 0025 *          OUTS   9
                                000C 10 0026 *
                                0027 *          POP      POP RET ADDR
                                0028 *          END
CC ERRS

```

QUICK THRESHOLD SAMPLER,V6
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0000 0001 QSET      RORG 0
0002          TITLE 'QUICK THRESHOLD SAMPLER,V6'
0003          *
0004          * THIS IS THE NEXT GENERATION OF QSET
0005          * MODIFIED TO BE A RELOCATABLE MODULE.
0006          *
0007          * INTENDED TO BE LINKED WITH THE MAIN
0008          * CALLING PROGRAM OF THE ELECTRO-OPTICAL
0009          * PAGE SCANNER.
0010          *
0011          * INITIALIZING IS ACCOMPLISHED IN THE
0012          * MAIN CALLING PROGRAM. STARTING VALUE
0013          * OF N AND STEP SIZE (S1) ARE DETERMINED
0014          * AT THAT TIME.
0015          *
0016          *
0017          * WRITTEN BY CAPT B.J. STANTON, 9 JUN 82
0018          * DEBUGGED FROM QSET3, 21 JUN 82
0019          * EDITED FROM QSETS, 21 JULY 82
0020          *
0021          *
0030 0022 VCRSET    EQU  H'80'    DIG VIDEO CNT RESET
0031 0023 CNT       EQU  2        SAMPLE PGM COUNTER
0032 0024 STEP     EQU  3        THRESHOLD STEP SIZE
0033 0025 NU       EQU  4        THRESHOLD HIGH BYTE
0034 0026 NL      EQU  5        THRESHOLD LOW BYTE
0035 0027 MTCU    EQU  6        MAX DIG VIDEO HI BYT
0036 0028 MTCL    EQU  7        MAX DIG VIDEO LO BYT
0037 0029 MINU    EQU  10       MINUEND HIGH BYTE
0038 0030 MINL    EQU  11       MINUEND LOW  BYTE
0039 0031 ENSENS  EQU  H'40'
0040 0032          *
0041 0033          *
0042 0034          * -----SUBROUTINE SAMPLE-----
0043 0035          *
0044 0036          * THIS SUBROUTINE HAS PROVISIONS FOR A VAR-
0045 0037          * IABLE THRESHOLD STEP SIZE LOADED IN R3
0046 0038          * (STEP). IT EXPECTS THE STARTING THRESHOLD
0047 0039          * VALUE TO BE LOADED IN R4,R5 (N,NL)
0048 0040          *
0049          0041          LIS  7        INITIALIZE
0050          0042          LR   CNT,A    COUNTER
0051          0043          *
0052          0044          RVC  LI   VCRSET  RESET
0053          0045          OUT  H'13'  VIDEO
0054          0046          CUF  CUF     COUNTERS
0055          0047          OUT  H'13'
0056          0048          *
0057          0049          LF   A,NL    INCREMENT
0058          0050          AS  STEP   THRESHOLD N
0059          0051          LR   NL,A    VALUE ONE
0060          0052          OUT  H'12'
0061          0053          LR   A,NL    STEP
0062          0054          LAK
0063          0055          LR   A,NL
0064          0056          OUT  H'13'
0065          0057          *
0066          0058          * TEST FOR END OF PRINTLINE-----
0067          0059          *
0068          0060          LI   ENSENS
0069          0061          OUTS  E

```

QUICK THRESHOLD SAMPLER, 76
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

0016 70	0062	PL1	CLR		LOOP UNTIL FALSE
0017 B4	0063		OUTS	4	
0018 A4	0064		INS	4	
0019 2101	0065		NI	H'01'	
001B 94FA	0016 0066		BNZ	PL1	
001D 70	0067	PL2	CLR		LOOP UNTIL TRUE
001E B4	0068		OUTS	4	
001F A4	0069		INS	4	
0020 2101	0070		NI	H'01'	
0022 94FA	001D 0071		BZ	PL2	
	0072		=		
	0073		=	STORE NEW VTC IN SUBTRAHEND (X)-----	
	0074		=		
0024 70	0075		CLR		
0025 2711	0076		OUT	H'11'	
0027 2611	0077		IN	H'11'	
0029 18	0078		COM		
002A 04	0079		LR	KU,A	
002B 70	0080		CLR		
002C 2710	0081		OUT	H'10'	
002E 2610	0082		IN	H'10'	
0030 18	0083		COM		
0031 05	0084		LR	KL,A	
	0085		=		
	0086		=	LOAD MINUEND WITH MAX VTC (MTC)-----	
	0087		=		
0032 46	0088		LR	A,MTCU	
0033 5A	0089		LR	MINU,A	
0034 47	0090		LR	A,MTCL	
0035 5B	0091		LR	MINL,A	
	0092		=		
	0093		=	SUBTRACT FOR SIGN OF RESULT-----	
	0094		=		
0036 01	0095		LR	A,KL	LOAD SUBLOW AND
0037 18	0096		COM		COMPLEMENT
0038 0B	0097		AS	MINL	SUBLOW + MINLOW
0039 5B	0098		LR	MINL,A	STORE IN MINLOW
003A 4A	0099		LR	A,MINU	CARRY TO
003B 19	0100		LNK		MINHI
003C 5A	0101		LR	MINU,A	
003D 4B	0102		LR	A,MINL	ADD 1 TO MAKE
003E 1F	0103		INC		2'S COMPLEMENT
003F 4A	0104		LR	A,MINU	CARRY TO
0040 19	0105		LNK		MINHI
0041 5A	0106		LR	MINU,A	
0042 00	0107		LR	A,KU	LOAD SUBHI AND
0043 13	0108		COM		COMPLEMENT
0044 CA	0109		AS	MINU	SUBHI + MINHI
	0110		=		
	0111		=	END OF SUBTRACT FOR SIGN-----	
	0112		=		
0045 3209	004F 0113		BC	SKIP	
0047 00	0114		LR	A,KU	REPLACE MTC
0048 56	0115		LR	MTCU,A	WITH NEW MAXIMUM
0049 01	0116		LR	A,KL	VTC
004A 57	0117		LR	MTCL,A	
	0118		=		
004B 44	0119		LR	A,NU	STORE NEW
004C 06	0120		LR	NU,A	THRESHOLD VALUE
004E 45	0121		LR	A,NL	IN GIVING MTC
004E C7	0122		LR	NU,A	

QUICK THRESHOLD SAMPLER V6
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0123 *
004F 32          0124 SKIP    DS    CNT
0050 9481      0002 0125          BN?   RVC
0126 *
0127 * END OF SUBROUTINE SAMPLE-----
0128 *
0129 * DETERMINE STARTING VALUE OF NEW RANGE OF
0130 * N TO BE SAMPLED
0131 *
0132 * SUBROUTINE SUBTRACT-----
0133 * LOADS:
0134 * MINUEND    IN R10, R11 (K)
0135 * SUBTRAHEND IN R12, R13 (K)
0136 * RESULT     IN R10, R11 (K)
0137 *
0138 * FIRST LOAD VALUES-----
0139 *
0052 02          0140          LR    A,RU    LOAD
0053 5A          0141          LP    MINU,A  NR
0054 03          0142          LR    A,RL    IN
0055 5B          0143          LR    MINL,A  MINUEND
0144 *
0056 43          0145          LR    A,STEP  LOAD STEP
0057 05          0146          LR    KL,A    IN
0058 70          0147          CLR           SUBTRAHEND
0059 04          0148          LR    KU,A
0149 *
0150 * THEN SUBTRACT-----
0151 *
005A 01          0152          LR    A,KL    LOAD SUBLOW AND
005B 12          0153          COM           COMPLEMENT
005C 02          0154          AS    11    SUBLOW + MINLOW
005D 5B          0155          LR    11,A  STORE IN MINLOW
005E 9204      0063 0156          SMC    SB1    IF CARRY THEN
0060 4A          0157          LR    A,10    INCREMENT
0061 1F          0158          INC           MINHI
0062 5A          0159          LR    10,A
0160 *
0063 4B          0161          SBI    LR    A,11    ADD 1 TO MAKE
0064 1F          0162          INC           2'S COMPLEMENT
0065 5B          0163          LR    11,A
0066 9204      0063 0164          SMC    SB2    IF CARRY THEN
0068 4A          0165          LR    A,10    INCREMENT
0069 1F          0166          INC           MINHI
006A 5A          0167          LR    10,A
0168 *
006B 00          0169          SBI    LR    A,KU    LOAD SUBHI AND
006C 13          0170          COM           COMPLEMENT
006D 0A          0171          AS    10    SUBHI + MINHI
006E 5A          0172          LR    10,A  STORE IN MINHI
0173 *
0174 * FINALLY STORE NEW STARTING THRESHOLD-----
0175 *
0176 *
006F 4A          0177          LR    A,MINU
0070 54          0178          LR    NU,A
0071 4B          0179          LR    A,MINL
0072 55          0180          LR    NU,A
0181 *
0182 * ALTER STEP SIZE-----
0183 *

```


QUICK THRESHOLD SAMPLER.V6
ERRS LJC OBJECT ADDR LINE

SOURCE STATEMENT

0073	43	0184	LR	A,STEP	DIVIDE STEP
0074	12	0185	SR	1	SIZE BY 4
0075	12	0186	SR	1	
0076	53	0187	LR	STEP,A	
0077	1C	0188	POP		
		0189	=		
		0190	=	END OF SUBROUTINE SAMPLE-----	
		0191	*		
		0192		END	

CO ERRS

LISTING OF EXEC FILE 'LINKED' WHICH LINKS TOGETHER
THE INDIVIDUAL SOFTWARE MODULES THAT FORM 'EOPS-'

LINK 1 CLEAR.ORG 0 MAIN4.10:1
LINK 1 FSTLN.10:1
LINK 1 ENDLN.10:1
LINK 1 XMITS.10:1
LINK 1 QSET .10:1
ASS CI 2TI

LINKING INFORMATION FOR 'EOPS-'
FORMULATOR LOADER

SYMBOL ADDR
MAIN4 0000
NEXT ADDR: 019A 0000
UNDEF SYM:
ENDLN FSTLN XMITS QSET

FORMULATOR LOADER

SYMBOL ADDR
FSTLN 019A
NEXT ADDR: 01AC 0000
UNDEF SYM:
ENDLN XMITS QSET

FORMULATOR LOADER

SYMBOL ADDR
ENDLN 01AC
NEXT ADDR: 01D0 0000
UNDEF SYM:
XMITS QSET

FORMULATOR LOADER

SYMBOL ADDR
XMITS 01D0
NEXT ADDR: 01DD 0000
UNDEF SYM:
QSET

FORMULATOR LOADER

SYMBOL ADDR
QSET 01DD
NEXT ADDR: 0255 0000
UNDEF SYM:

APPENDIX C
COMPUTER SIMULATIONS

These simulations use the APL programs QSET1 and QSET2 on the following page to emulate the flowchart of Figure 5.5. The VTC data used in the simulations were taken with the scanner and F8 under operational conditions as noted in Table C.1. Therefore the simulated performance accurately represents the actual behavior of QSET when implemented with the F8 and incorporated with the normal page-scanning sequence.

A few details deserve special attention as one examines these simulations. First, the smallest step size of QSET1 is $S4 = 2$ whereas the smallest step size of QSET2 is $S4 = 1$. In other words, QSET1 is fundamentally limited to only being able to pinpoint N_p (the value of N producing the peak of the VTC curve, MTC) within an error of one millivolt. For this reason, errors of one millivolt with QSET1 are ignored when comparing QSET1 to QSET2 in Table C.3. Next, errors in the value of N are signed. If QSET produced an N -value less than the actual value of N_p , then the error is negative (\wedge), and if the QSET result is greater than the actual value of N_p , then the error is positive. However, it is more significant to ignore the sign and evaluate the MAGNITUDE of the QSET error since this will reveal information on how far QSET "misses" the actual VTC peak, or equivalently, how far from optimum the threshold will be set due to sampling error. Finally it is important to understand that the QSET algorithm was designed to find the peak of a relatively

smooth discrete curve with only one obvious maximum. But some of the data sets used in the simulations have much different characteristics, and it is instructive to note the behavior of the QSET algorithm in these situations.

The VTC data sets can be grouped into three general categories: (I) data sets using ECP A under normal conditions; (II) data sets using ECP A under abnormal conditions; and (III) data sets using other ECPs under normal conditions. Table C.2 lists the data sets belonging to each group, and Table C.3 summarizes the results of the simulation data. Although the data base is relatively small due to time constraints in this research, a few significant trends can still be identified. Notice first that the performance of both QSET1 and QSET2 are identical for Category I data sets. Looking at the individual simulations reveals that the same errors occurred mainly due to similar multiples in the samples taken. Also, the largest error occurred with data set A6232 which had an abnormal shape. And in general, it is important to realize that sampling errors are a product of the uncertainty in the VTC curve itself.

The performance with Category II data is a perfect example of the problem discussed in Chapter 5 concerning the occasion when the range of significant VTC information (RV) is smaller than the initial step size (S1). By examining the QSET1 simulations with data sets A606A and A606D, it can be seen that the algorithm will "freeze" on the initial sample because no significant VTC data is ever encountered. Recall however that

QSET2 was designed to overcome this specific problem, and as noted in the simulation results, its performance is excellent.

QSET evaluations with Category III data sets are more for example of the dependence of the algorithm on a properly shaped VTC curve. As discussed in Chapter 3, the CALIBRATION PATTERN must produce a VTC curve whose peak is at the value of N giving the optimum resolution in the scanner's output. While both algorithms faithfully locate the peaks in data sets B6062, C6062, and D6062, remember that these data sets are generated from constant-frequency ECPs that give erroneous VTC maximums. The large sampling errors occurring with data sets E6062 and F6062 are due to the significant ambiguities present in these VTC curves. Therefore it can be seen that ATC performance in general will be extremely unpredictable when scanning anything other than the proper CALIBRATION PATTERN.

TABLE C.1
VIDEO TRANSITION COUNT
DATA SETS

DATA CODE KEY:

First character:	Indicates ECP used
Second character:	Indicates month data taken
Third and fourth character:	Indicates day data taken
Fifth character:	Indicates run on given day

DATA CODE	REMARKS
A5261	Old green fluorescents used
A6061	Old soft white fluorescents used
A6062	Old cool white fluorescents used
B6062	Old cool white fluorescents used
C6062	Old cool white fluorescents used
D6062	Old cool white fluorescents used
E6062	Old cool white fluorescents used
F6062	Old cool white fluorescents used
A6063	Old warm white fluorescents used
A6064	Only one warm white fluorescent used
A6066	Old cool white fluorescents used; Yellow paper used as background
A606A	Old cool white fluorescents used; Red paper used as background
A606D	Old cool white fluorescents used; Navy blue paper used as background
A6071	Old cool white fluorescents used
A6072	Same conditions as A6071; 5 minutes later
A6073	Same conditions as A6072; 5 minutes later
A6074	Same conditions as A6073; 5 minutes later
A6075	Same conditions as A6074; 5 minutes later
A6231	New green fluorescents used
A6232	New cool white fluorescents used
A6233	New warm white fluorescents used

TABLE C.2
DATA SET GROUPINGS

Category I	Category II	Category III
A5261	A6064	B6062
A6061	A6066	C6062
A6062	A606A	D6062
A6063	A606D	E6062
A6071		F6062
A6072		
A6073		
A6074		
A6075		
A6231		
A6232		
A6233		

TABLE C.3
STATISTICAL SUMMARY OF QSET PERFORMANCE

	CAT I	CAT II	CAT III
Occurrences of Errors with QSET1 (> 1 millivolt)	25%	50%	40%
Occurrences of Errors with QSET2 (> 0 millivolt)	25%	0%	40%
Expected Value of Error with QSET1 (mV)	3.25	92.0	24.4
Standard Deviation of Error with QSET1 (mV)	7.62	106.3	35.3
Expected Value of Error with QSET2 (mV)	3.25	0.0	22.2
Standard Deviation of Error with QSET2 (mV)	7.62	0.0	35.7

RESET[00]7

```

7 RESET A)F)F1)F2)F3)F4)F5)F6)F7)F8)F9)F10)F11)F12)F13)F14)F15)F16)F17)F18)F19)F20)F21)F22)F23)F24)F25)F26)F27)F28)F29)F30)F31)F32)F33)F34)F35)F36)F37)F38)F39)F40)F41)F42)F43)F44)F45)F46)F47)F48)F49)F50)F51)F52)F53)F54)F55)F56)F57)F58)F59)F60)F61)F62)F63)F64)F65)F66)F67)F68)F69)F70)F71)F72)F73)F74)F75)F76)F77)F78)F79)F80)F81)F82)F83)F84)F85)F86)F87)F88)F89)F90)F91)F92)F93)F94)F95)F96)F97)F98)F99)F100)F101)F102)F103)F104)F105)F106)F107)F108)F109)F110)F111)F112)F113)F114)F115)F116)F117)F118)F119)F120)F121)F122)F123)F124)F125)F126)F127)F128)F129)F130)F131)F132)F133)F134)F135)F136)F137)F138)F139)F140)F141)F142)F143)F144)F145)F146)F147)F148)F149)F150)F151)F152)F153)F154)F155)F156)F157)F158)F159)F160)F161)F162)F163)F164)F165)F166)F167)F168)F169)F170)F171)F172)F173)F174)F175)F176)F177)F178)F179)F180)F181)F182)F183)F184)F185)F186)F187)F188)F189)F190)F191)F192)F193)F194)F195)F196)F197)F198)F199)F200)F201)F202)F203)F204)F205)F206)F207)F208)F209)F210)F211)F212)F213)F214)F215)F216)F217)F218)F219)F220)F221)F222)F223)F224)F225)F226)F227)F228)F229)F230)F231)F232)F233)F234)F235)F236)F237)F238)F239)F240)F241)F242)F243)F244)F245)F246)F247)F248)F249)F250)F251)F252)F253)F254)F255)F256)F257)F258)F259)F260)F261)F262)F263)F264)F265)F266)F267)F268)F269)F270)F271)F272)F273)F274)F275)F276)F277)F278)F279)F280)F281)F282)F283)F284)F285)F286)F287)F288)F289)F290)F291)F292)F293)F294)F295)F296)F297)F298)F299)F300)F301)F302)F303)F304)F305)F306)F307)F308)F309)F310)F311)F312)F313)F314)F315)F316)F317)F318)F319)F320)F321)F322)F323)F324)F325)F326)F327)F328)F329)F330)F331)F332)F333)F334)F335)F336)F337)F338)F339)F340)F341)F342)F343)F344)F345)F346)F347)F348)F349)F350)F351)F352)F353)F354)F355)F356)F357)F358)F359)F360)F361)F362)F363)F364)F365)F366)F367)F368)F369)F370)F371)F372)F373)F374)F375)F376)F377)F378)F379)F380)F381)F382)F383)F384)F385)F386)F387)F388)F389)F390)F391)F392)F393)F394)F395)F396)F397)F398)F399)F400)F401)F402)F403)F404)F405)F406)F407)F408)F409)F410)F411)F412)F413)F414)F415)F416)F417)F418)F419)F420)F421)F422)F423)F424)F425)F426)F427)F428)F429)F430)F431)F432)F433)F434)F435)F436)F437)F438)F439)F440)F441)F442)F443)F444)F445)F446)F447)F448)F449)F450)F451)F452)F453)F454)F455)F456)F457)F458)F459)F460)F461)F462)F463)F464)F465)F466)F467)F468)F469)F470)F471)F472)F473)F474)F475)F476)F477)F478)F479)F480)F481)F482)F483)F484)F485)F486)F487)F488)F489)F490)F491)F492)F493)F494)F495)F496)F497)F498)F499)F500)F501)F502)F503)F504)F505)F506)F507)F508)F509)F510)F511)F512)F513)F514)F515)F516)F517)F518)F519)F520)F521)F522)F523)F524)F525)F526)F527)F528)F529)F530)F531)F532)F533)F534)F535)F536)F537)F538)F539)F540)F541)F542)F543)F544)F545)F546)F547)F548)F549)F550)F551)F552)F553)F554)F555)F556)F557)F558)F559)F560)F561)F562)F563)F564)F565)F566)F567)F568)F569)F570)F571)F572)F573)F574)F575)F576)F577)F578)F579)F580)F581)F582)F583)F584)F585)F586)F587)F588)F589)F590)F591)F592)F593)F594)F595)F596)F597)F598)F599)F600)F601)F602)F603)F604)F605)F606)F607)F608)F609)F610)F611)F612)F613)F614)F615)F616)F617)F618)F619)F620)F621)F622)F623)F624)F625)F626)F627)F628)F629)F630)F631)F632)F633)F634)F635)F636)F637)F638)F639)F640)F641)F642)F643)F644)F645)F646)F647)F648)F649)F650)F651)F652)F653)F654)F655)F656)F657)F658)F659)F660)F661)F662)F663)F664)F665)F666)F667)F668)F669)F670)F671)F672)F673)F674)F675)F676)F677)F678)F679)F680)F681)F682)F683)F684)F685)F686)F687)F688)F689)F690)F691)F692)F693)F694)F695)F696)F697)F698)F699)F700)F701)F702)F703)F704)F705)F706)F707)F708)F709)F710)F711)F712)F713)F714)F715)F716)F717)F718)F719)F720)F721)F722)F723)F724)F725)F726)F727)F728)F729)F730)F731)F732)F733)F734)F735)F736)F737)F738)F739)F740)F741)F742)F743)F744)F745)F746)F747)F748)F749)F750)F751)F752)F753)F754)F755)F756)F757)F758)F759)F760)F761)F762)F763)F764)F765)F766)F767)F768)F769)F770)F771)F772)F773)F774)F775)F776)F777)F778)F779)F780)F781)F782)F783)F784)F785)F786)F787)F788)F789)F790)F791)F792)F793)F794)F795)F796)F797)F798)F799)F800)F801)F802)F803)F804)F805)F806)F807)F808)F809)F810)F811)F812)F813)F814)F815)F816)F817)F818)F819)F820)F821)F822)F823)F824)F825)F826)F827)F828)F829)F830)F831)F832)F833)F834)F835)F836)F837)F838)F839)F840)F841)F842)F843)F844)F845)F846)F847)F848)F849)F850)F851)F852)F853)F854)F855)F856)F857)F858)F859)F860)F861)F862)F863)F864)F865)F866)F867)F868)F869)F870)F871)F872)F873)F874)F875)F876)F877)F878)F879)F880)F881)F882)F883)F884)F885)F886)F887)F888)F889)F890)F891)F892)F893)F894)F895)F896)F897)F898)F899)F900)F901)F902)F903)F904)F905)F906)F907)F908)F909)F910)F911)F912)F913)F914)F915)F916)F917)F918)F919)F920)F921)F922)F923)F924)F925)F926)F927)F928)F929)F930)F931)F932)F933)F934)F935)F936)F937)F938)F939)F940)F941)F942)F943)F944)F945)F946)F947)F948)F949)F950)F951)F952)F953)F954)F955)F956)F957)F958)F959)F960)F961)F962)F963)F964)F965)F966)F967)F968)F969)F970)F971)F972)F973)F974)F975)F976)F977)F978)F979)F980)F981)F982)F983)F984)F985)F986)F987)F988)F989)F990)F991)F992)F993)F994)F995)F996)F997)F998)F999)F1000)
010  * THIS PROGRAM SIMULATES THE PEAK SPECTRUM OF THE
020  * ENTIRE RANGE OF N: 0 TO 1024.
030  *
040  * THE FIRST PART TAKES THE INDICATED DATA SET AND STRETCHES
050  * IT TO COVER THE ENTIRE RANGE OF N.
060  *
070  N1 = A[1:1] - 1
080  K1 = 1/K1
090  F1 = (K1,1)*F1
100  F2 = (K1,1)*F2
110  F = F1,F2
120  A = F,[1]A
130  F = FA
140  F = F213
150  L = (1024 - ACF[1]) + 1
160  E1 = ACF[1] + 1/L
170  E1 = (L,1)*E1
180  E2 = (L,1)*E2
190  G = E1,E2
200  A = A,[1]E
210  *
220  * MAIN SAMPLING PORTION OF THE PROGRAM FOLLOWS.
230  *
240  MAINCOUNT = N = MTC = 0
250  STEP = 128
260  MAINLOOP: LINECOUNT = 7
270  *
280  * -----PASS 1,+(MAINCOUNT+1)
290  *
300  * N = MTC
310  *
320  LINELOOP: N = N + STEP
330  * ((MTC - A[N:2]) > 0)/NEXT
340  MTC = A[N:2]
350  G = ACF[1]
360  NEXT: (5 0)+ACF[1]
370  LINECOUNT = LINECOUNT + 1
380  * (LINECOUNT > 0)/LINELOOP
390  G = G - STEP
400  STEP = STEP + 4
410  MAINCOUNT = MAINCOUNT + 1
420  * (MAINCOUNT > 4)/MAINLOOP
430  N = N
440  *
450  *
460  * ACCORDING TO QDET], THE
470  * THRESHOLD VALUE PRODUCING
480  * THE PEAK OF THE MTC CURVE IS N = 1024
490  *
500  MTC = (1/A[1:2])
510  G = 1
520  NEXT: (MTC - ACF[2])/GISE
530  G = G + 1
540  * NEXT
550  *
560  * FULL MTC PEAK CURVE IS A[1:2] + GISE
570  *
580  * PEAKS = 1024 - 1024 + 1024 = 1024

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```

QSET1 A5261

-----PASS 1

N	VTC
128	1
256	1
384	190
512	0
640	0
768	0
896	0

-----PASS 2

N	VTC
288	4
320	126
352	253
384	190
416	71
448	3
480	0

-----PASS 3

N	VTC
328	169
336	210
344	222
352	253
360	244
368	226
376	215

-----PASS 4

N	VTC
340	226
348	241
350	254
352	253
354	255
356	246
358	244

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 354
 ACTUAL VTC PEAK OCCURRED AT N = 354
 ERROR FROM CORRECT N IS: 0

QSET2 A5261

-----PASS 1

N	VTC
192	1
256	1
320	126
384	190
448	3
512	0
576	0

-----PASS 2

N	VTC
336	210
352	253
368	226
384	190
400	121
416	71
432	20

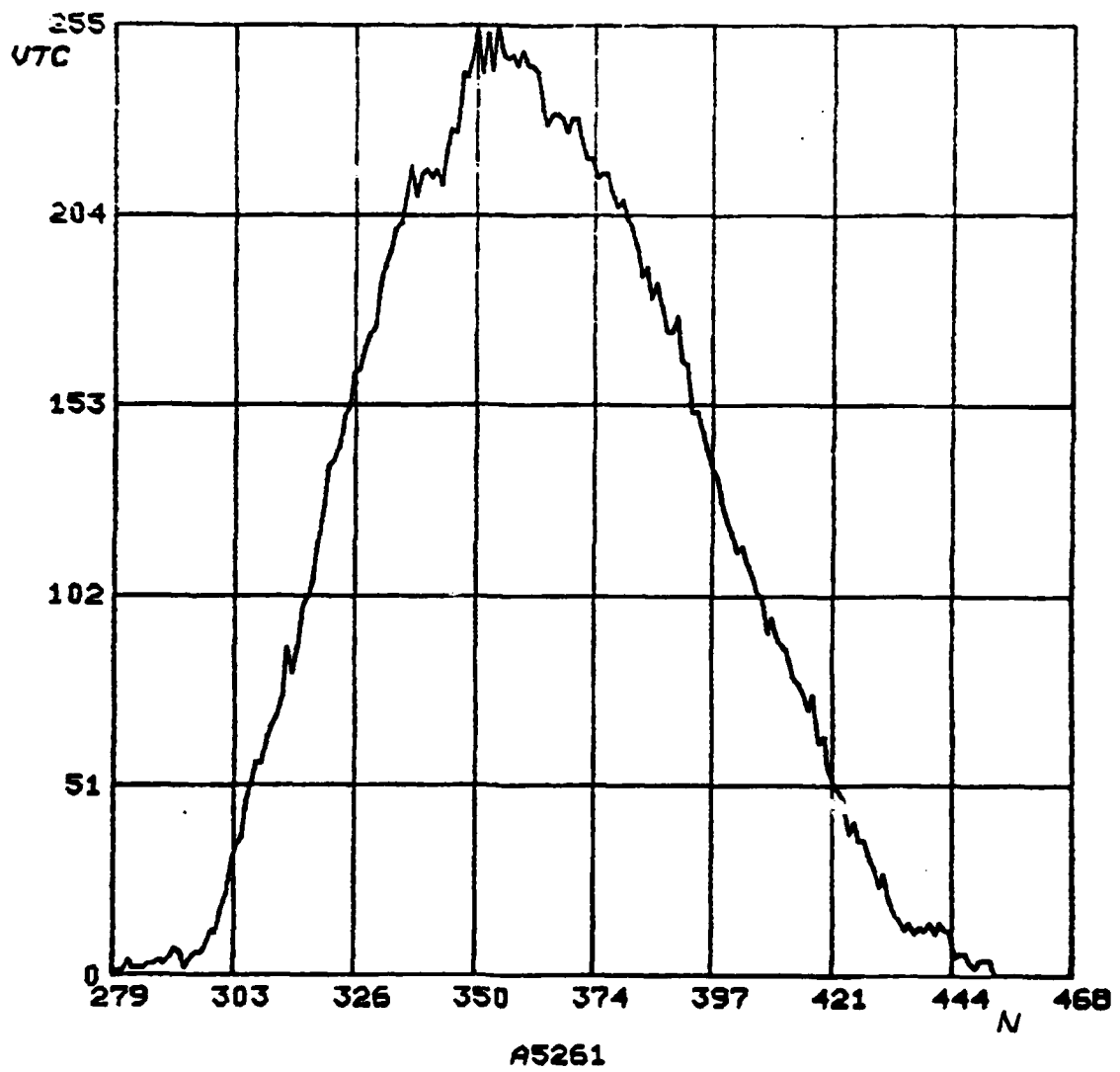
-----PASS 3

N	VTC
340	216
344	222
348	241
352	253
356	246
360	244
364	228

-----PASS 4

N	VTC
349	247
350	254
351	242
352	253
353	243
354	255
355	247

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 354
 ACTUAL VTC PEAK OCCURRED AT N = 354
 ERROR FROM CORRECT N IS: 0



QSET1 A6061

-----PASS 1

N	VTC
128	1
256	1
384	113
512	121
640	0
768	0
896	0

-----PASS 2

N	VTC
416	157
448	176
480	149
512	121
544	67
576	39
608	0

-----PASS 3

N	VTC
424	180
432	197
440	193
448	176
456	172
464	161
472	154

-----PASS 4

N	VTC
426	178
428	179
430	200
432	187
434	180
436	177
438	181

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 430
 ACTUAL VTC PEAK OCCURRED AT N = 430
 ERROR FROM CORRECT N IS: 0

QSET2 A6061

-----PASS 1

N	VTC
192	1
256	1
320	6
384	113
448	176
512	121
576	39

-----PASS 2

N	VTC
400	140
416	157
432	187
448	176
464	161
480	149
496	144

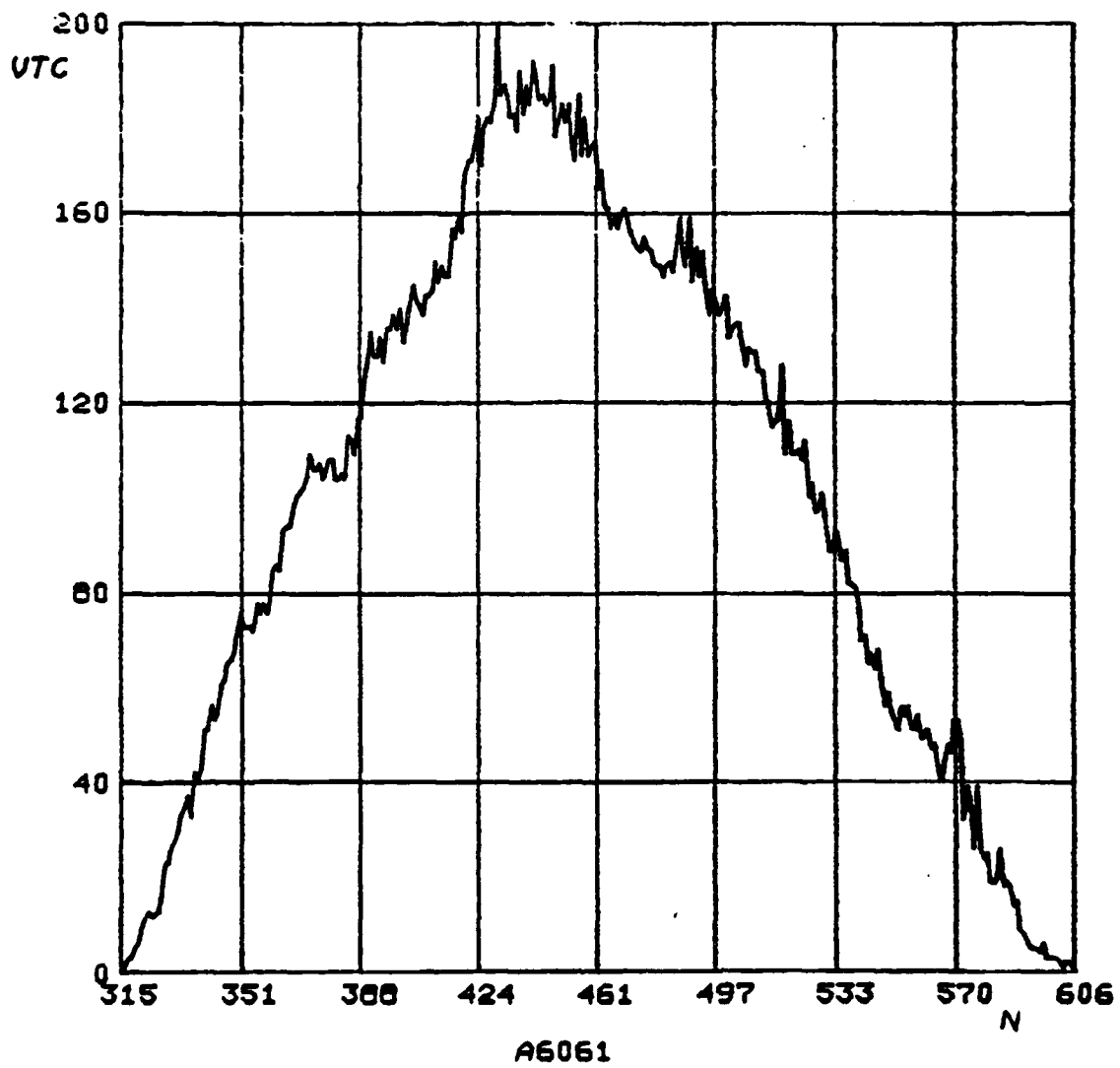
-----PASS 3

N	VTC
420	168
424	180
428	179
432	187
436	177
440	183
444	185

-----PASS 4

N	VTC
429	184
430	200
431	185
432	187
433	185
434	180
435	181

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 430
 ACTUAL VTC PEAK OCCURRED AT N = 430
 ERROR FROM CORRECT N IS: 0



QSET1 A6062

-----PASS 1

N	VTC
128	1
256	1
384	130
512	117
640	0
768	0
896	0

-----PASS 2

N	VTC
298	1
320	24
352	82
384	170
416	197
448	182
480	150

-----PASS 3

N	VTC
392	139
400	152
408	184
416	197
424	197
432	185
440	181

-----PASS 4

N	VTC
410	189
412	198
414	194
416	197
418	206
420	207
422	204

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 420
 ACTUAL VTC PEAK OCCURRED AT N = 419
 ERROR FROM CORRECT N IS: 1

QSET2 A6062

-----PASS 1

N	VTC
192	1
256	1
320	24
384	130
448	182
512	117
576	2

-----PASS 2

N	VTC
400	152
416	197
432	185
448	182
464	160
480	150
496	138

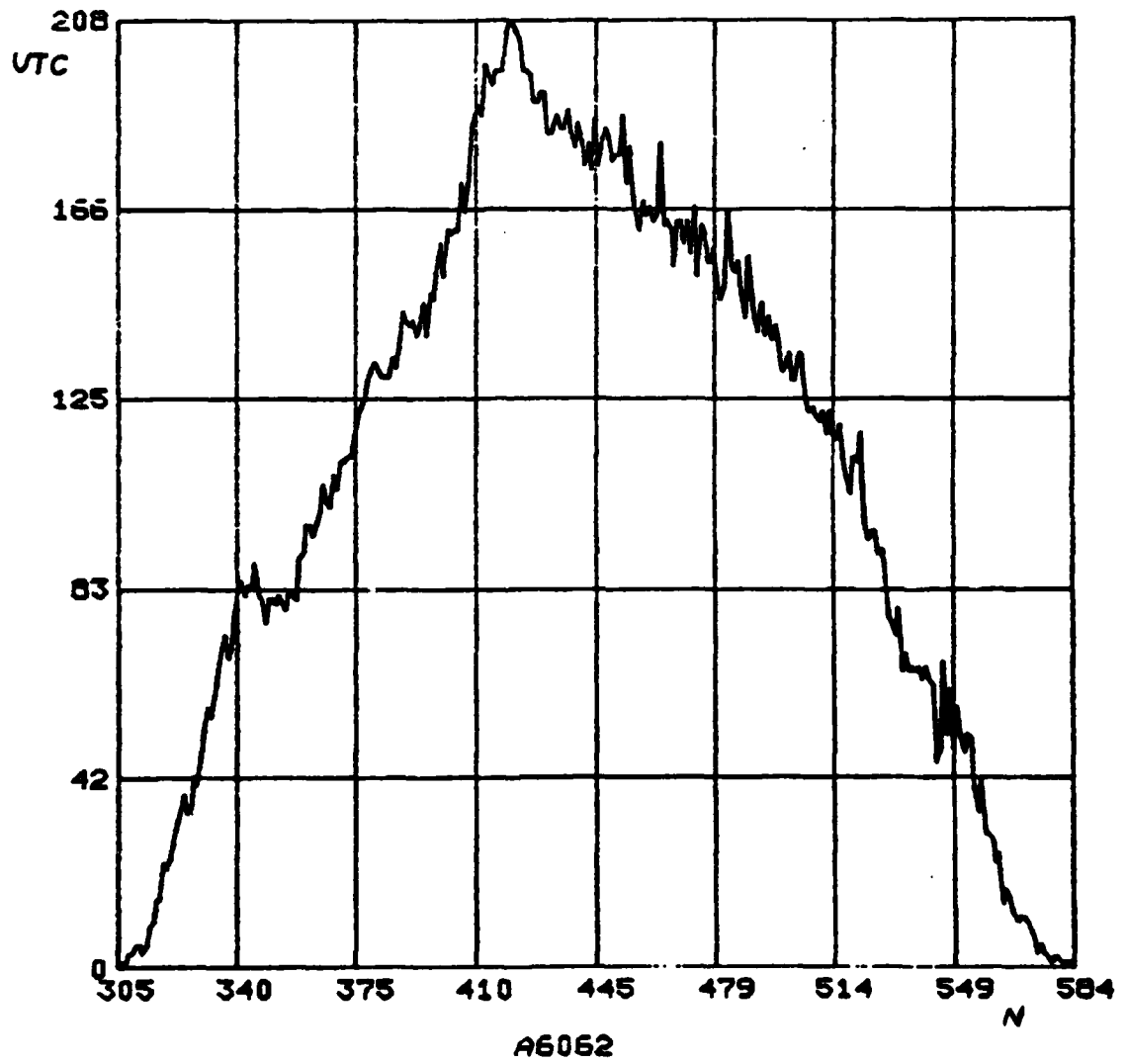
-----PASS 3

N	VTC
404	162
408	184
412	198
416	197
420	207
424	197
428	192

-----PASS 4

N	VTC
417	197
418	206
419	208
420	207
421	205
422	204
423	197

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 419
 ACTUAL VTC PEAK OCCURRED AT N = 419
 ERROR FROM CORRECT N IS: 0



QSET1 A6063

-----PASS 1

N	VTC
128	1
256	1
384	168
512	53
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	45
352	109
384	168
416	184
448	153
480	117

-----PASS 3

N	VTC
392	193
400	192
408	205
416	184
424	168
432	166
440	161

-----PASS 4

N	VTC
402	204
404	202
406	197
408	205
410	200
412	207
414	188

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 412

ACTUAL VTC PEAK OCCURRED AT N = 407

ERROR FROM CORRECT N IS: 5

QSET2 A6063

-----PASS 1

N	VTC
192	1
256	1
320	45
384	168
448	153
512	53
576	0

-----PASS 2

N	VTC
336	85
352	109
368	131
384	168
400	192
416	184
432	166

-----PASS 3

N	VTC
388	178
392	193
396	202
400	192
404	202
408	205
412	207

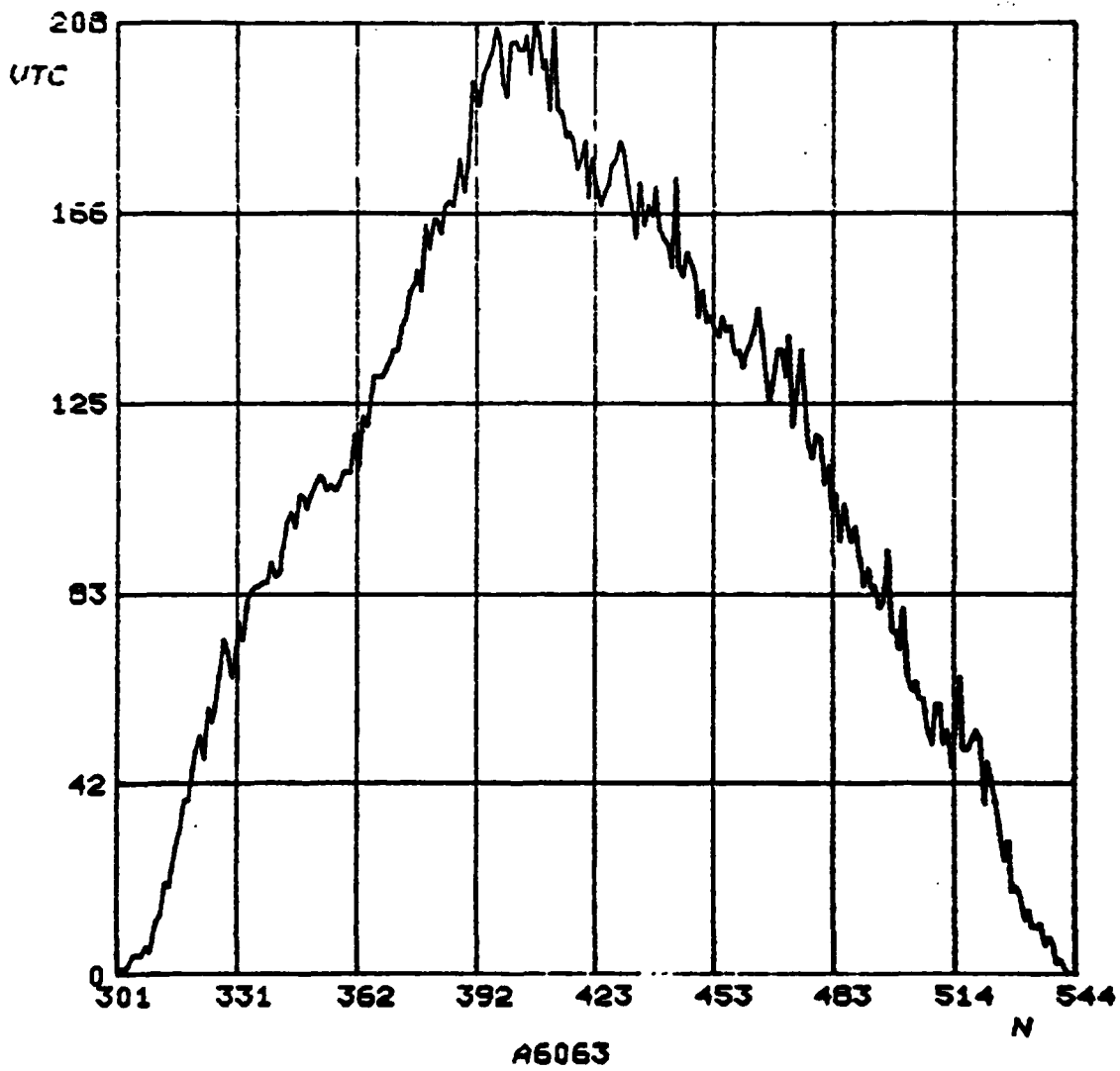
-----PASS 4

N	VTC
409	198
410	200
411	189
412	207
413	189
414	188
415	183

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 412

ACTUAL VTC PEAK OCCURRED AT N = 407

ERROR FROM CORRECT N IS: 5



QSET1 A6064

-----PASS 1

N	VTC
128	1
256	1
384	35
512	0
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	157
352	164
384	35
416	0
448	0
480	0

-----PASS 3

N	VTC
328	174
336	206
344	189
352	164
360	137
368	110
376	98

-----PASS 4

N	VTC
330	186
332	179
334	198
336	206
338	211
340	202
342	193

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 338
ACTUAL VTC PEAK OCCURRED AT N = 338
ERROR FROM CORRECT N IS: 0

QSET2 A6064

-----PASS 1

N	VTC
192	1
256	1
320	157
384	35
448	0
512	0
576	0

-----PASS 2

N	VTC
272	1
288	1
304	74
320	157
336	206
352	164
368	110

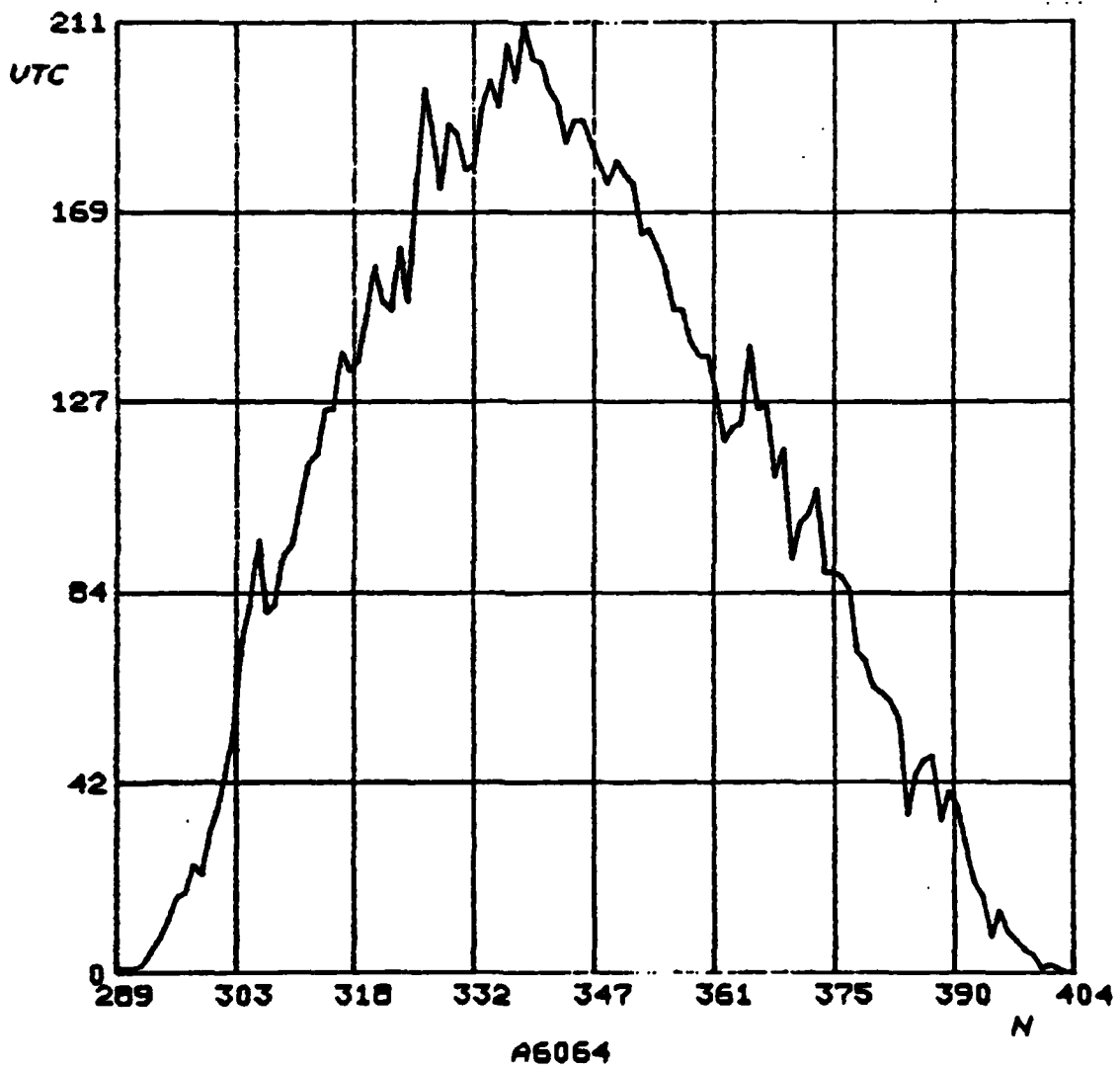
-----PASS 3

N	VTC
324	149
328	174
332	179
336	206
340	202
344	189
348	175

-----PASS 4

N	VTC
333	192
334	198
335	192
336	206
337	198
338	211
339	203

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 338
ACTUAL VTC PEAK OCCURRED AT N = 338
ERROR FROM CORRECT N IS: 0



QSET1 A6066

-----PASS 1

N	VTC
128	1
256	1
384	154
512	1
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	63
352	179
384	154
416	119
448	87
480	16

-----PASS 3

N	VTC
328	103
336	135
344	175
352	179
360	177
368	164
376	162

-----PASS 4

N	VTC
346	167
348	174
350	177
352	179
354	180
356	173
358	172

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 354

ACTUAL VTC PEAK OCCURRED AT N = 353

ERROR FROM CORRECT N IS: 1

QSET2 A6066

-----PASS 1

N	VTC
192	1
256	1
320	63
384	154
448	87
512	1
576	0

-----PASS 2

N	VTC
336	135
352	179
368	164
384	154
400	147
416	119
432	105

-----PASS 3

N	VTC
340	159
344	175
348	174
352	179
356	173
360	177
364	169

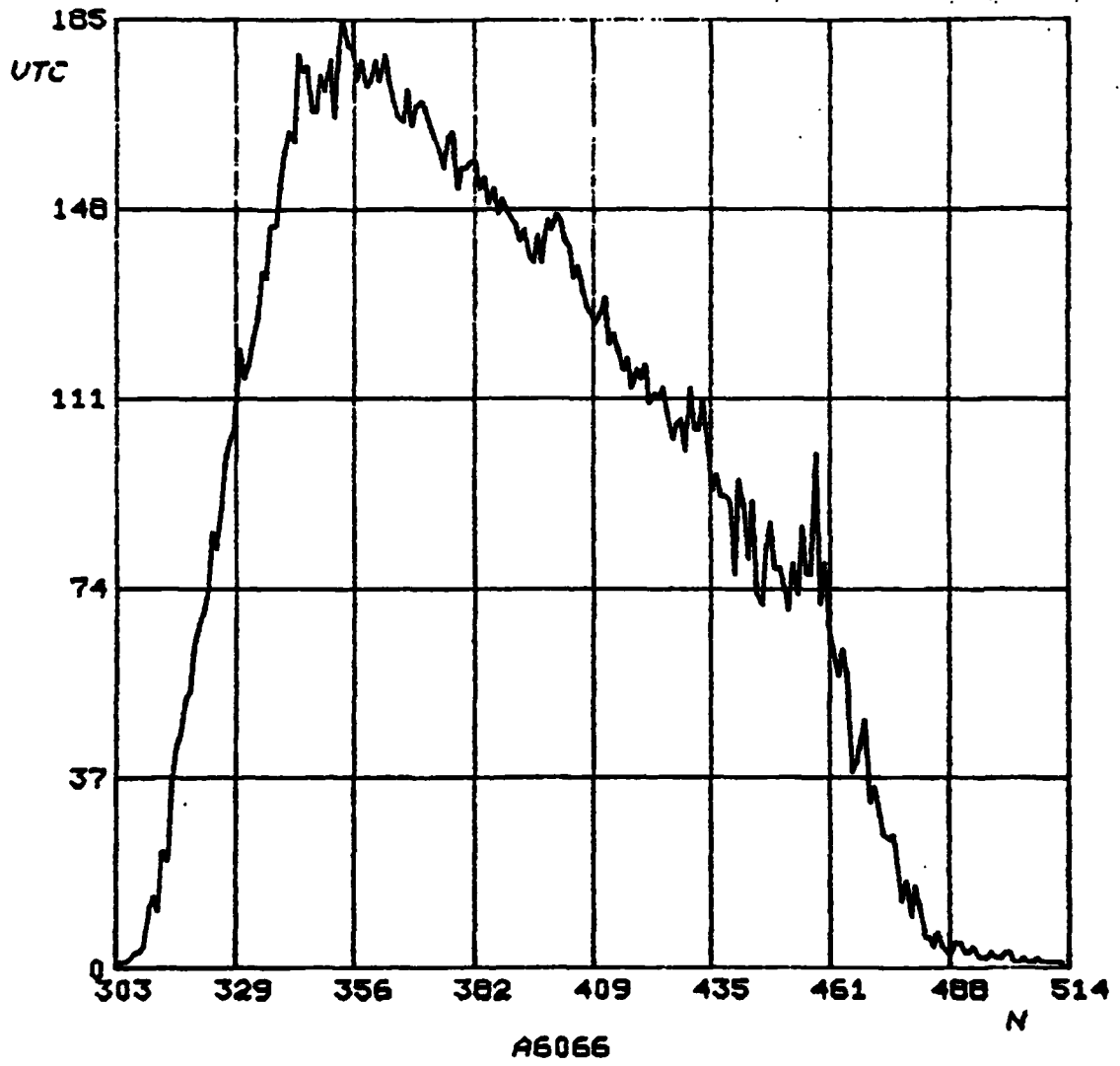
-----PASS 4

N	VTC
349	171
350	177
351	166
352	179
353	185
354	180
355	179

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 353

ACTUAL VTC PEAK OCCURRED AT N = 353

ERROR FROM CORRECT N IS: 0



QSET1 A606A

-----PASS 1

N	VTC
128	1
256	1
384	0
512	0
640	0
768	0
896	0

-----PASS 2

N	VTC
32	1
64	1
96	1
128	1
160	1
192	1
224	1

-----PASS 3

N	VTC
104	1
112	1
120	1
128	1
136	1
144	1
152	1

-----PASS 4

N	VTC
122	1
124	1
126	1
128	1
130	1
132	1
134	1

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 128
 ACTUAL VTC PEAK OCCURRED AT N = 318
 ERROR FROM CORRECT N IS: ^190

QSET2 A606A

-----PASS 1

N	VTC
192	1
256	1
320	188
384	0
448	0
512	0
576	0

-----PASS 2

N	VTC
272	1
288	1
304	54
320	188
336	131
352	58
368	1

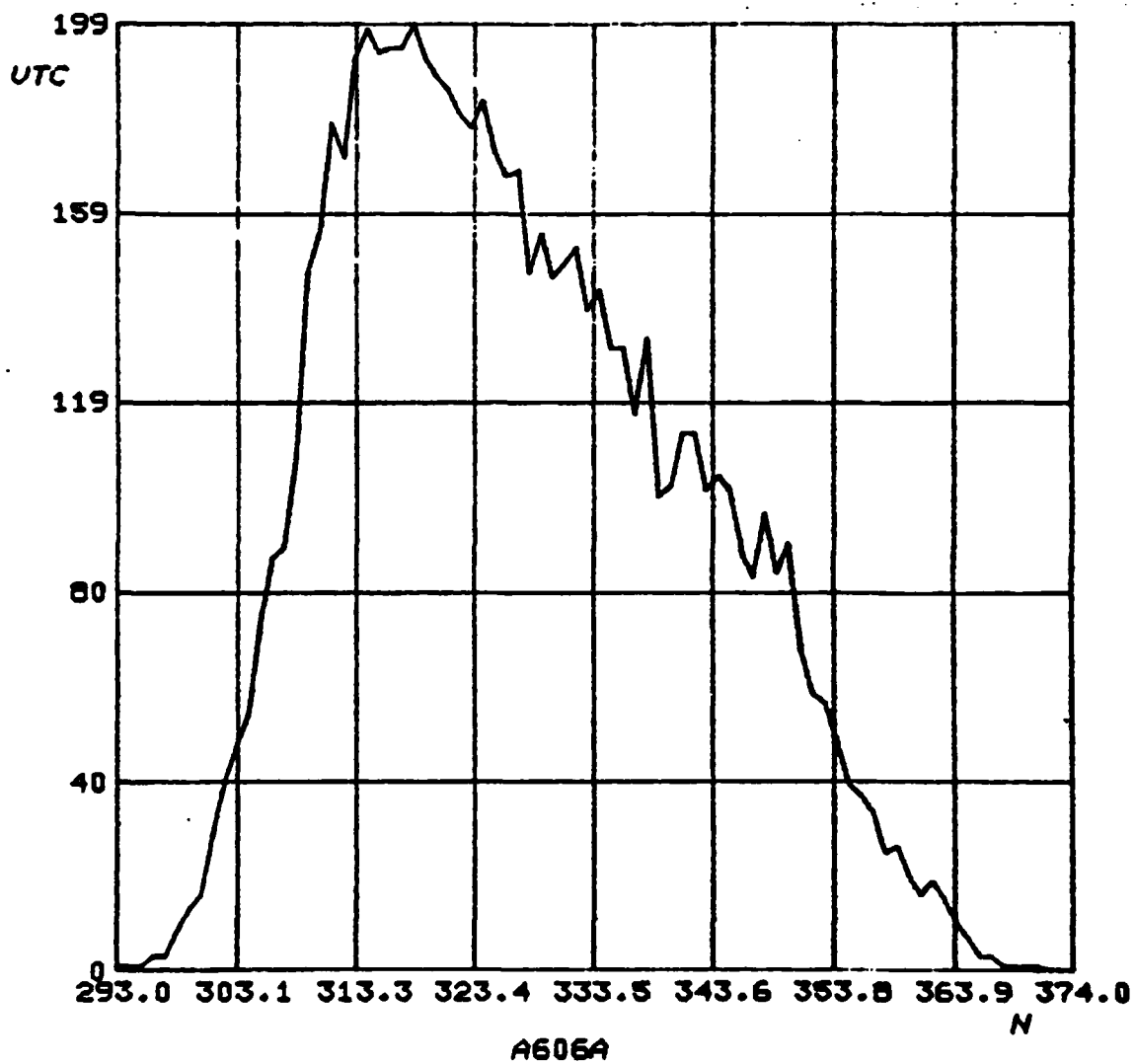
-----PASS 3

N	VTC
308	109
312	171
316	194
320	188
324	183
328	147
332	152

-----PASS 4

N	VTC
313	192
314	198
315	193
316	194
317	194
318	199
319	192

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 318
 ACTUAL VTC PEAK OCCURRED AT N = 316
 ERROR FROM CORRECT N IS: 0



QSET1 A606D

-----PASS 1

N	UTC
128	1
256	1
384	0
512	0
640	0
768	0
896	0

-----PASS 2

N	UTC
32	1
64	1
96	1
128	1
160	1
192	1
224	1

-----PASS 3

N	UTC
104	1
112	1
120	1
128	1
136	1
144	1
152	1

-----PASS 4

N	UTC
122	1
124	1
126	1
128	1
130	1
132	1
134	1

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE UTC CURVE IS N = 128

ACTUAL UTC PEAK OCCURRED AT N = 306

ERROR FROM CORRECT N IS: ^178

QSET2 A606D

-----PASS 1

N	UTC
192	1
256	1
320	145
384	0
448	0
512	0
576	0

-----PASS 2

N	UTC
272	1
288	1
304	218
320	145
336	25
352	1
368	0

-----PASS 3

N	UTC
292	3
296	26
300	97
304	218
308	200
312	155
316	182

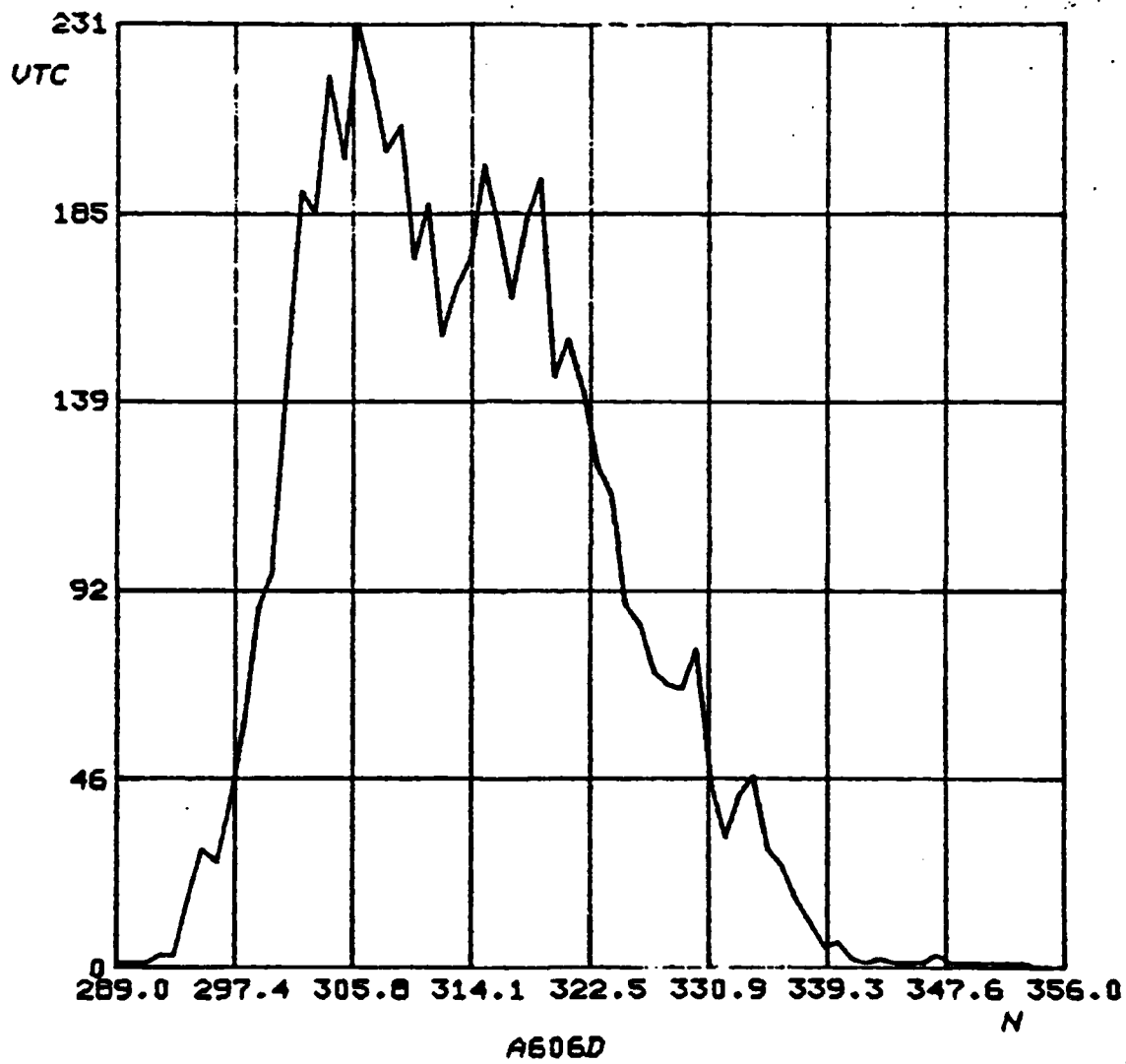
-----PASS 4

N	UTC
301	146
302	190
303	185
304	218
305	198
306	231
307	217

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE UTC CURVE IS N = 306

ACTUAL UTC PEAK OCCURRED AT N = 306

ERROR FROM CORRECT N IS: 0



QSET1 A6071

-----PASS 1

N	VTC
128	1
256	1
384	120
512	41
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	4
352	67
384	120
416	199
448	157
480	101

-----PASS 3

N	VTC
392	144
400	179
408	193
416	199
424	190
432	176
440	163

-----PASS 4

N	VTC
410	204
412	204
414	208
416	199
418	204
420	200
422	187

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 414
ACTUAL VTC PEAK OCCURRED AT N = 414
ERROR FROM CORRECT N IS: 0

QSET2 A6071

-----PASS 1

N	VTC
192	1
256	1
320	4
384	120
448	157
512	41
576	0

-----PASS 2

N	VTC
400	179
416	199
432	176
448	157
464	132
480	101
496	75

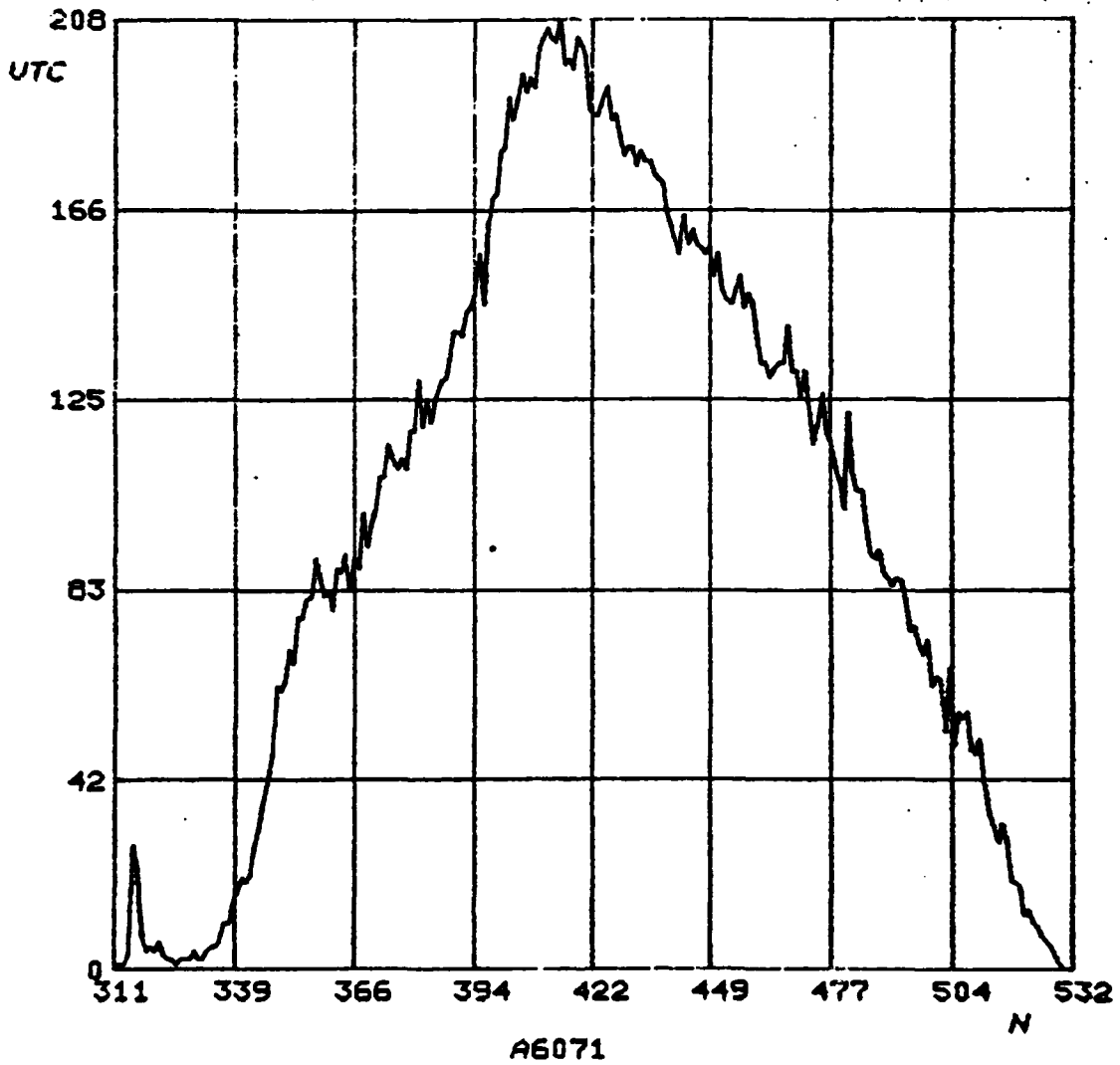
-----PASS 3

N	VTC
404	190
408	193
412	204
416	199
420	200
424	190
428	182

-----PASS 4

N	VTC
409	202
410	204
411	206
412	204
413	203
414	208
415	198

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 414
ACTUAL VTC PEAK OCCURRED AT N = 414
ERROR FROM CORRECT N IS: 0



QSET1 A6072

-----PASS 1

N	VTC
128	1
256	1
384	160
512	13
640	0
768	0
896	6

-----PASS 2

N	VTC
288	5
320	4
352	85
384	160
416	191
448	148
480	84

-----PASS 3

N	VTC
392	188
400	190
408	199
416	191
424	180
432	169
440	156

-----PASS 4

N	VTC
402	200
404	196
406	201
408	199
410	192
412	186
414	190

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 406
 ACTUAL VTC PEAK OCCURRED AT N = 398
 ERROR FROM CORRECT N IS: 8

QSET
 QSET2 A6072

-----PASS 1

N	VTC
192	1
256	1
320	4
384	160
448	148
512	13
576	0

-----PASS 2

N	VTC
336	46
352	85
368	113
384	160
400	190
416	191
432	160

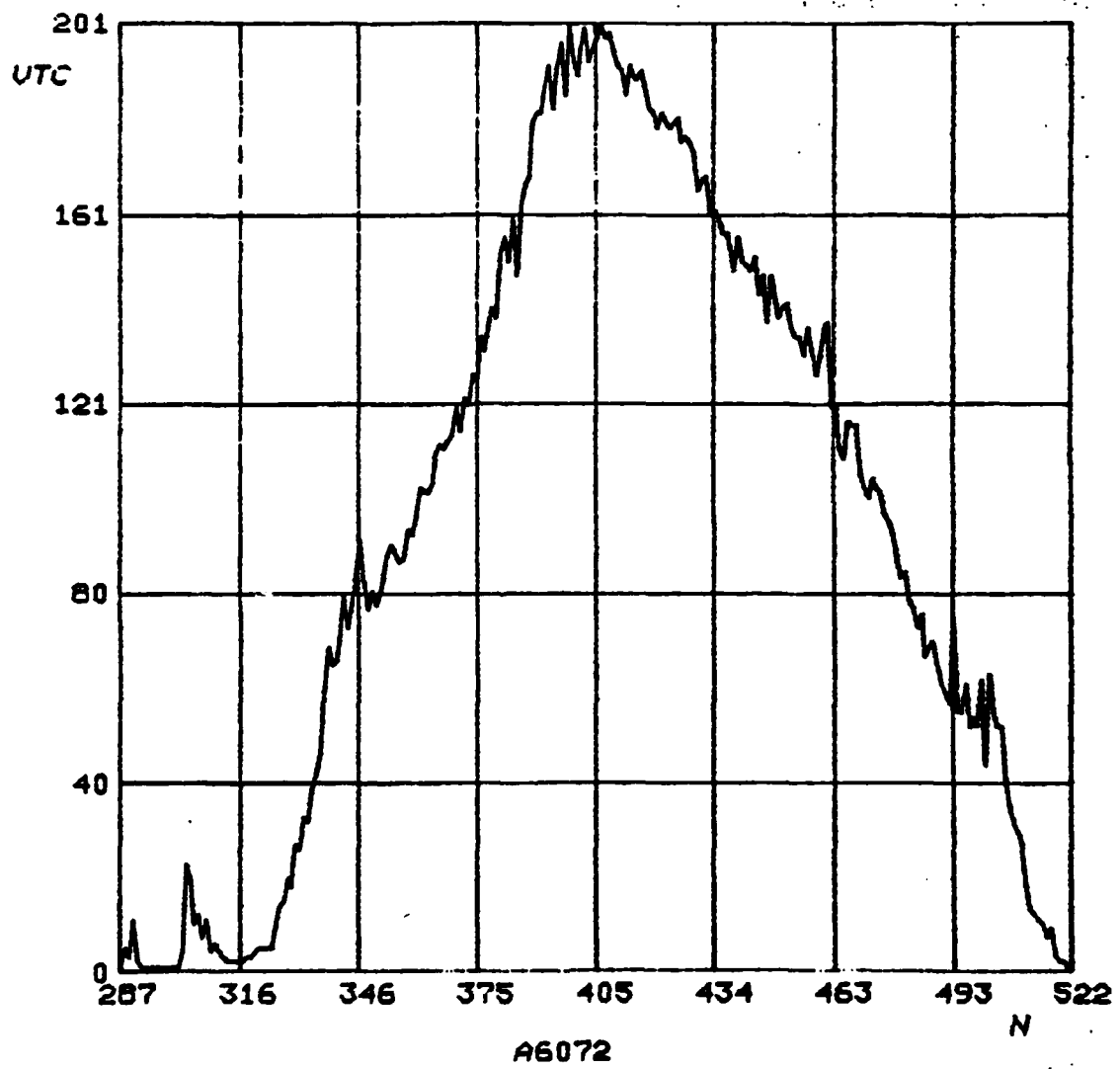
-----PASS 3

N	VTC
404	196
408	199
412	186
416	191
420	179
424	180
428	176

-----PASS 4

N	VTC
405	198
406	201
407	198
408	199
409	195
410	192
411	191

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 406
 ACTUAL VTC PEAK OCCURRED AT N = 398
 ERROR FROM CORRECT N IS: 8



QSET1 A6073

QSET2 A6073

-----PASS 1

-----PASS 1

N	VTC
128	1
256	1
384	169
512	7
640	0
768	0
896	0

N	VTC
192	1
256	1
320	6
384	169
448	140
512	7
576	0

-----PASS 2

-----PASS 2

N	VTC
288	2
320	6
352	87
384	169
416	185
448	140
480	75

N	VTC
336	68
352	87
368	123
384	169
400	197
416	185
432	154

-----PASS 3

-----PASS 3

N	VTC
392	196
400	197
408	197
416	185
424	170
432	154
440	149

N	VTC
388	193
392	196
396	195
400	197
404	194
408	197
412	184

-----PASS 4

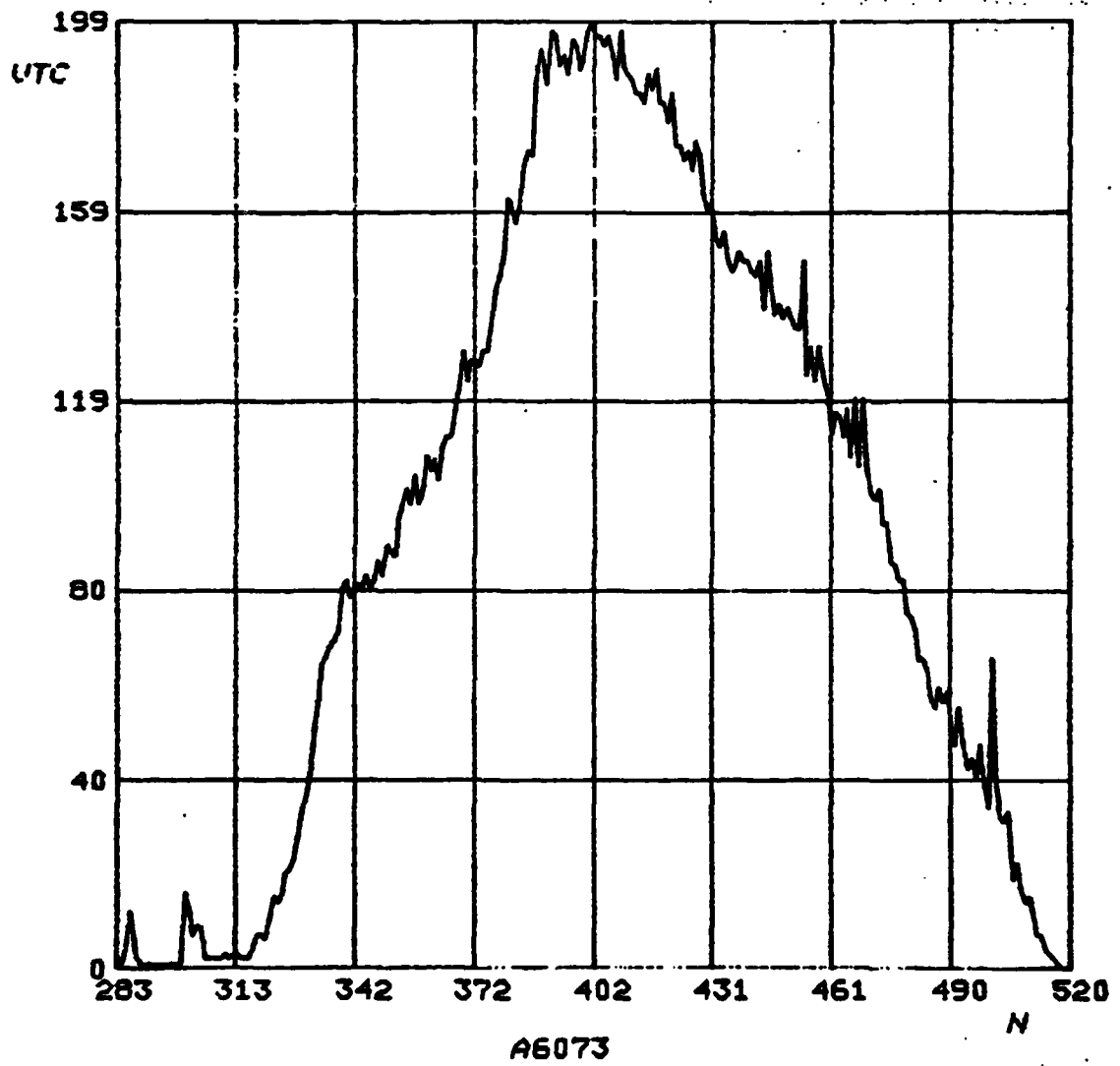
-----PASS 4

N	VTC
394	192
396	195
398	189
400	197
402	196
404	194
406	192

N	VTC
397	194
398	189
399	192
400	197
401	199
402	196
403	196

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 400
 ACTUAL VTC PEAK OCCURRED AT N = 401
 ERROR FROM CORRECT N IS: ^1

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 401
 ACTUAL VTC PEAK OCCURRED AT N = 401
 ERROR FROM CORRECT N IS: 0



QSET1 A6074

-----PASS 1

N	VTC
128	1
256	163
384	3
512	0
640	0
768	0

-----PASS 2

N	VTC
288	1
320	8
352	103
384	163
416	184
448	138
480	65

-----PASS 3

N	VTC
392	201
400	199
408	185
416	184
424	158
432	162
440	143

-----PASS 4

N	VTC
386	167
388	185
390	185
392	201
394	193
396	194
398	192

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 392
 ACTUAL VTC PEAK OCCURRED AT N = 392
 ERROR FROM CORRECT N IS: 0

QSET2 A6074

-----PASS 1

N	VTC
192	1
256	1
320	8
384	163
448	138
512	3
576	0

-----PASS 2

N	VTC
336	63
352	103
368	120
384	163
400	199
416	184
432	162

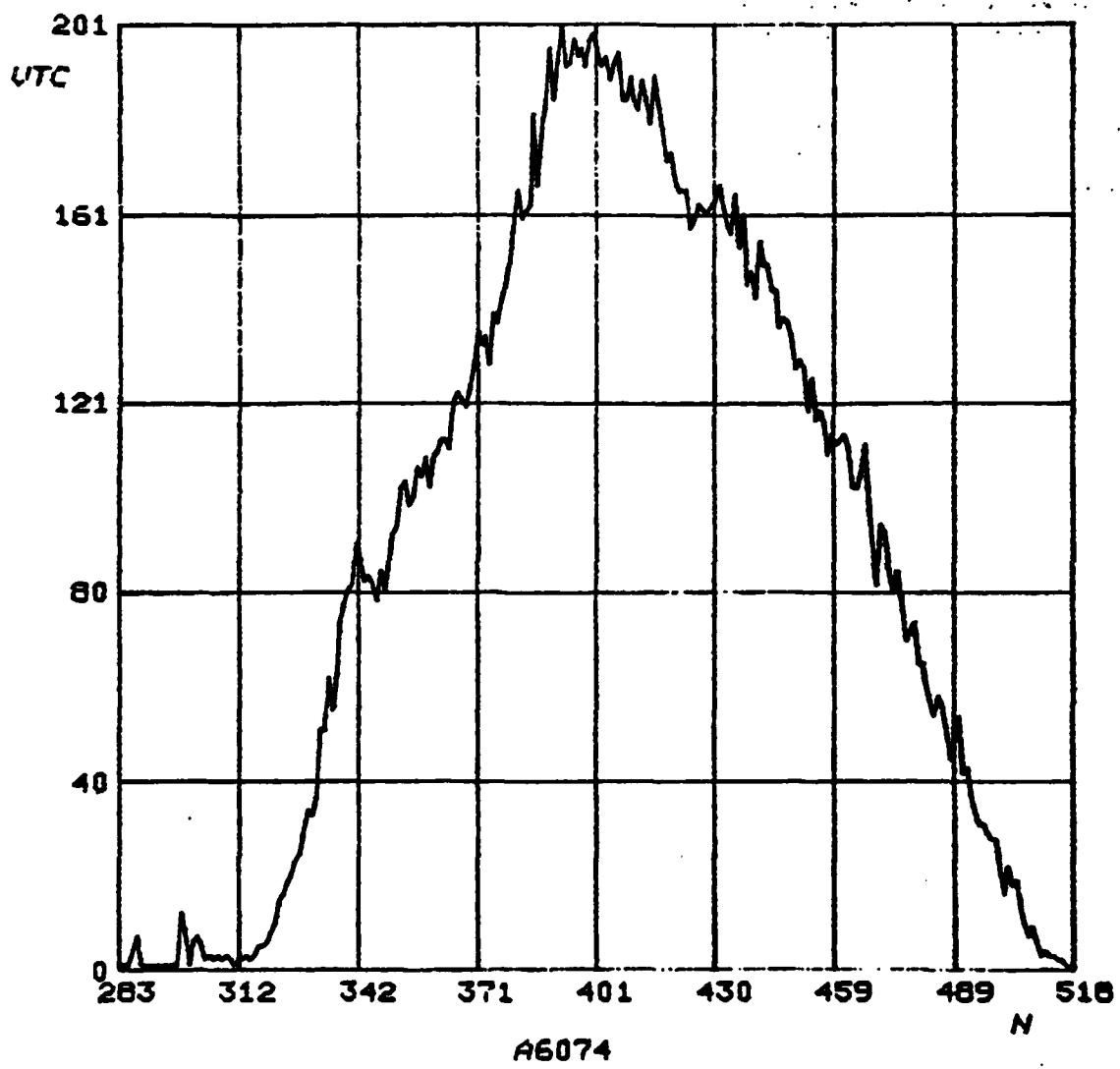
-----PASS 3

N	VTC
388	185
392	201
396	194
400	199
404	189
408	185
412	189

-----PASS 4

N	VTC
389	196
390	185
391	193
392	201
393	192
394	193
395	198

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 392
 ACTUAL VTC PEAK OCCURRED AT N = 392
 ERROR FROM CORRECT N IS: 0



QSET1 A6075

-----PASS 1

N	VTC
128	1
256	1
384	147
512	41
640	0
768	0
896	0

-----PASS 2

N	VTC
288	3
320	7
352	81
384	147
416	190
448	146
480	101

-----PASS 3

N	VTC
392	182
400	190
408	191
416	190
424	177
432	173
440	153

-----PASS 4

N	VTC
402	202
404	204
406	197
408	191
410	203
412	202
414	196

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 404
 ACTUAL VTC PEAK OCCURRED AT N = 403
 ERROR FROM CORRECT N IS: 1

QSET2 A6075

-----PASS 1

N	VTC
192	1
256	1
320	7
384	147
448	146
512	41
576	0

-----PASS 2

N	VTC
336	63
352	81
368	115
384	147
400	190
416	190
432	173

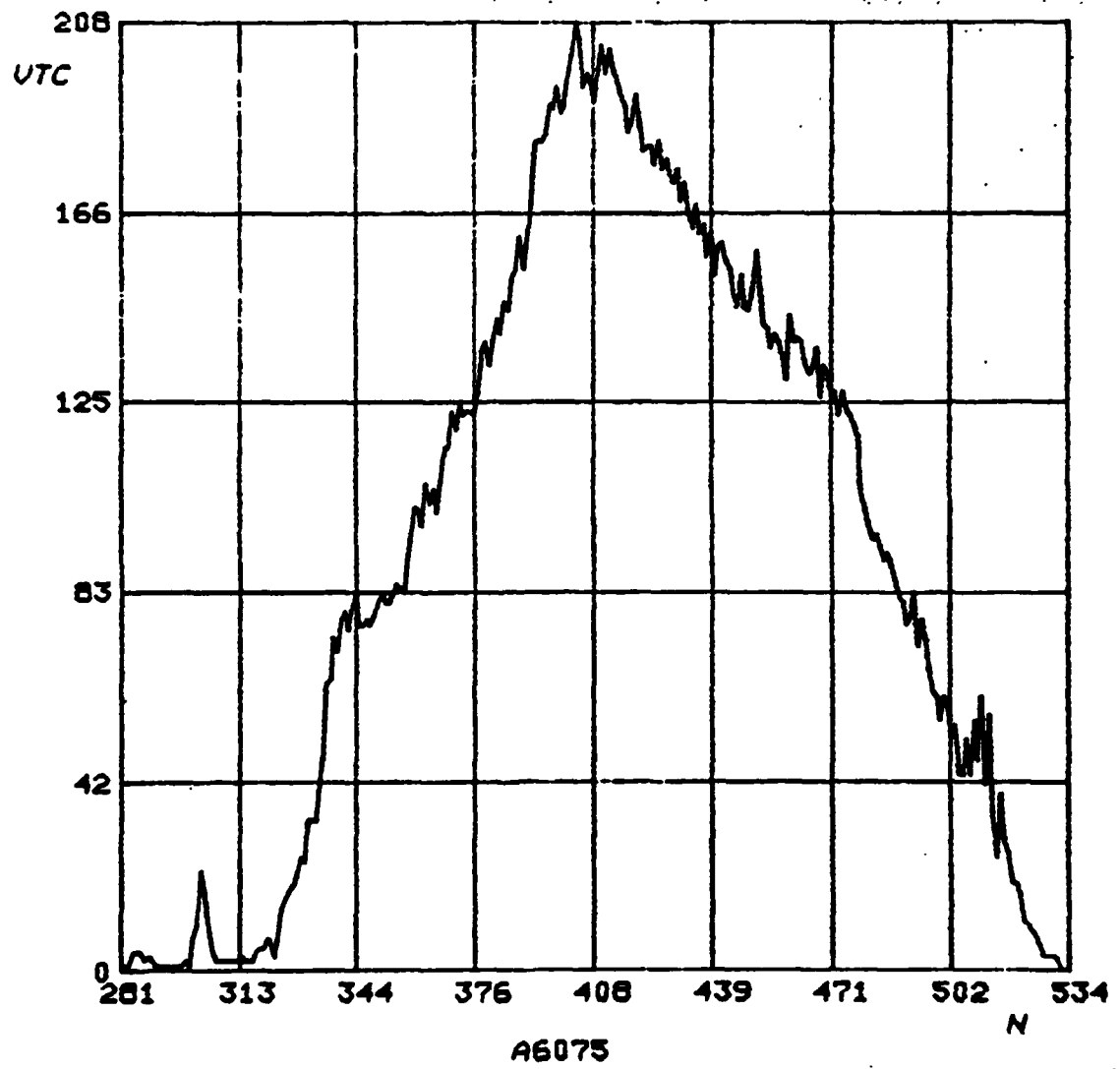
-----PASS 3

N	VTC
388	161
392	182
396	190
400	190
404	204
408	191
412	202

-----PASS 4

N	VTC
401	197
402	202
403	208
404	204
405	194
406	197
407	195

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 403
 ACTUAL VTC PEAK OCCURRED AT N = 403
 ERROR FROM CORRECT N IS: 0



QSET1 B6062

-----PASS 1

N	VTC
128	1
256	1
384	400
512	3
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	151
352	416
384	400
416	384
448	366
480	81

-----PASS 3

N	VTC
328	260
336	428
344	437
352	416
360	406
368	405
376	395

-----PASS 4

N	VTC
338	438
340	437
342	452
344	437
346	432
348	424
350	420

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 342

ACTUAL VTC PEAK OCCURRED AT N = 343

ERROR FROM CORRECT N IS: ^1

QSET2 B6062

-----PASS 1

N	VTC
192	1
256	1
320	151
384	400
448	366
512	3
576	0

-----PASS 2

N	VTC
336	428
352	416
368	405
384	400
400	400
416	384
432	387

-----PASS 3

N	VTC
324	213
328	260
332	360
336	428
340	437
344	437
348	424

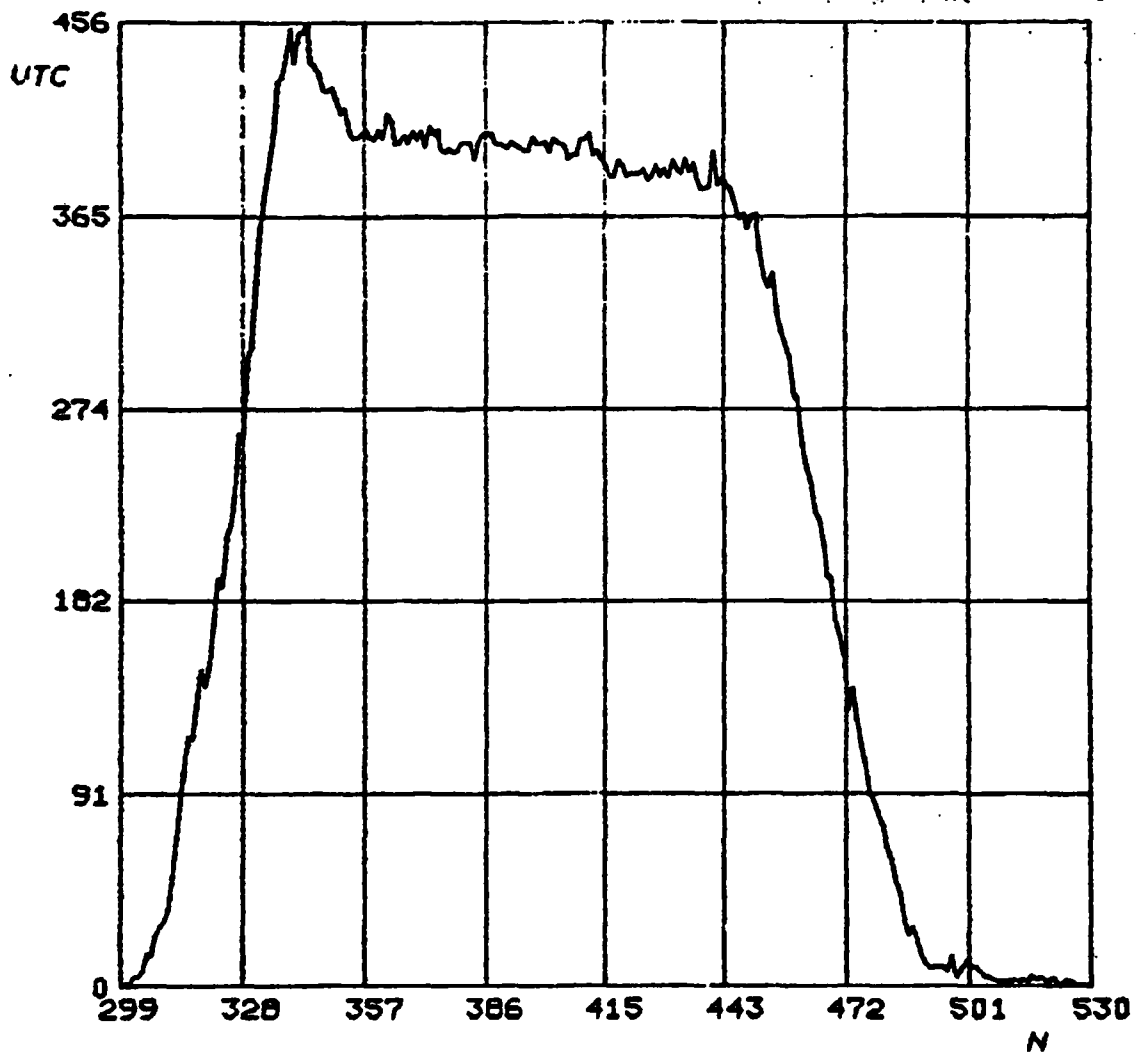
-----PASS 4

N	VTC
337	430
338	438
339	453
340	437
341	451
342	452
343	456

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 343

ACTUAL VTC PEAK OCCURRED AT N = 343

ERROR FROM CORRECT N IS: 0



B6062

QSET1 C6062

-----PASS 1

N	VTC
128	1
256	1
384	210
512	58
640	0
768	0
896	0

-----PASS 2

N	VTC
288	1
320	255
352	212
384	210
416	205
448	213
480	194

-----PASS 3

N	VTC
296	12
304	97
312	219
320	255
328	242
336	220
344	223

-----PASS 4

N	VTC
314	231
316	261
318	259
320	255
322	253
324	243
326	237

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 316
 ACTUAL VTC PEAK OCCURRED AT N = 316
 ERROR FROM CORRECT N IS: 0

QSET2 C6062

-----PASS 1

N	VTC
192	1
256	1
320	255
384	210
448	213
512	58
576	0

-----PASS 2

N	VTC
272	1
288	1
304	97
320	255
336	220
352	212
368	213

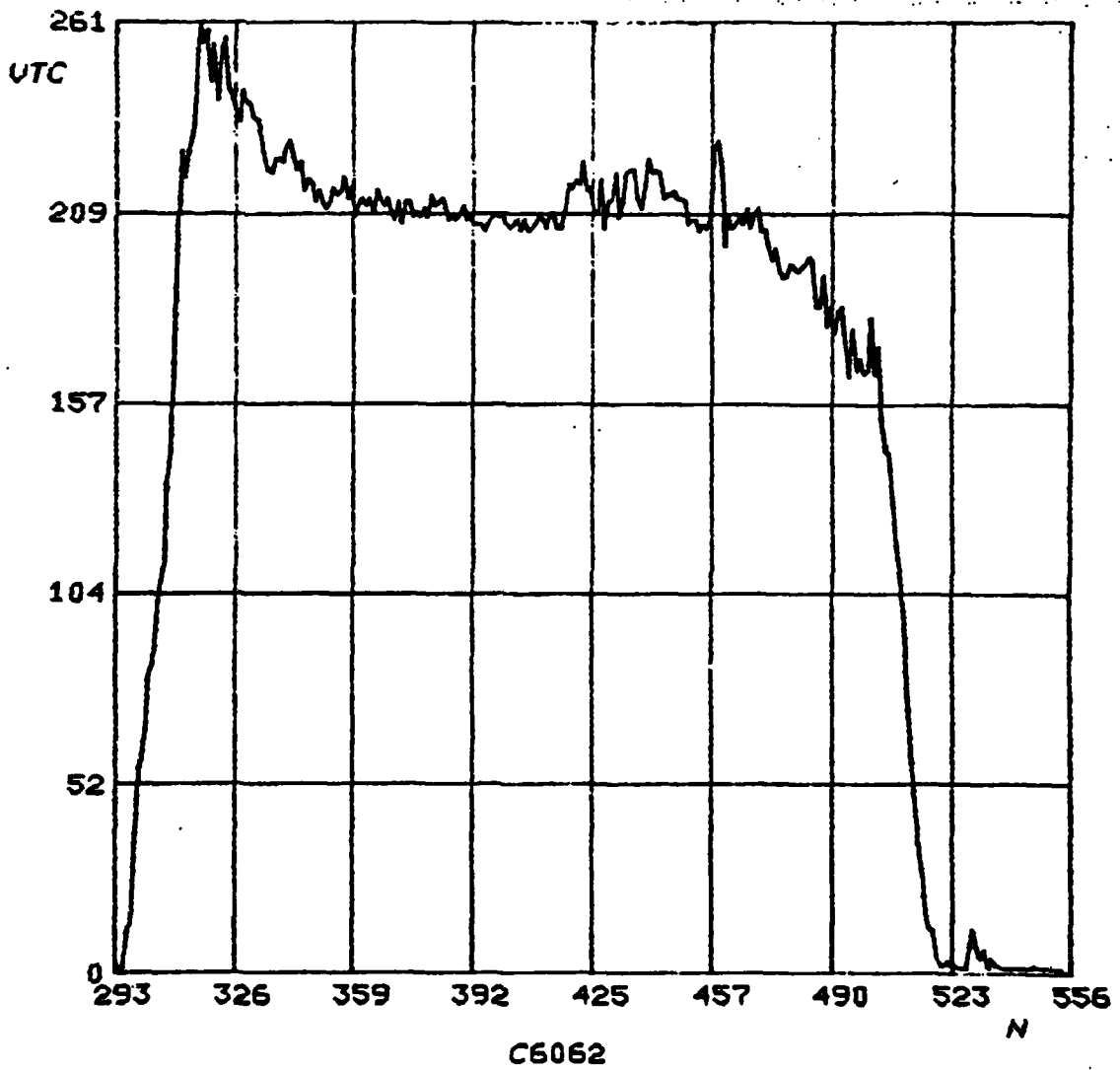
-----PASS 3

N	VTC
308	144
312	219
316	261
320	255
324	243
328	242
332	234

-----PASS 4

N	VTC
313	226
314	231
315	240
316	261
317	255
318	259
319	245

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE VTC CURVE IS N = 316
 ACTUAL VTC PEAK OCCURRED AT N = 316
 ERROR FROM CORRECT N IS: 0



QSET1 D6062

-----PASS 1

N	VTC
128	1
256	1
384	43
512	58
640	0
768	0
896	0

-----PASS 2

N	VTC
416	46
448	46
480	49
512	58
544	0
576	0
608	0

-----PASS 3

N	VTC
488	51
496	50
504	53
512	58
520	60
528	46
536	31

-----PASS 4

N	VTC
514	45
516	57
518	71
520	60
522	72
524	80
526	53

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 524

ACTUAL VTC PEAK OCCURRED AT N = 524

ERROR FROM CORRECT N IS: 0

QSET2 D6062

-----PASS 1

N	VTC
192	1
256	1
320	53
384	43
448	46
512	58
576	0

-----PASS 2

N	VTC
464	58
480	49
496	50
512	58
528	46
544	0
560	0

-----PASS 3

N	VTC
500	46
504	53
508	51
512	58
516	57
520	60
524	80

-----PASS 4

N	VTC
521	65
522	72
523	75
524	80
525	55
526	53
527	49

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 524

ACTUAL VTC PEAK OCCURRED AT N = 524

ERROR FROM CORRECT N IS: 0

AD-A125 316

AUTOMATIC THRESHOLD DESIGN FOR A BOUND DOCUMENT SCANNER
(U) AIR FORCE INST OF TECH WRIGHT-PATTERSON AFB OH
B J STANTON DEC 82 AFIT-CI/NR-82-71T

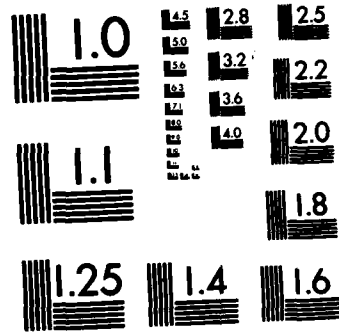
3/3

UNCLASSIFIED

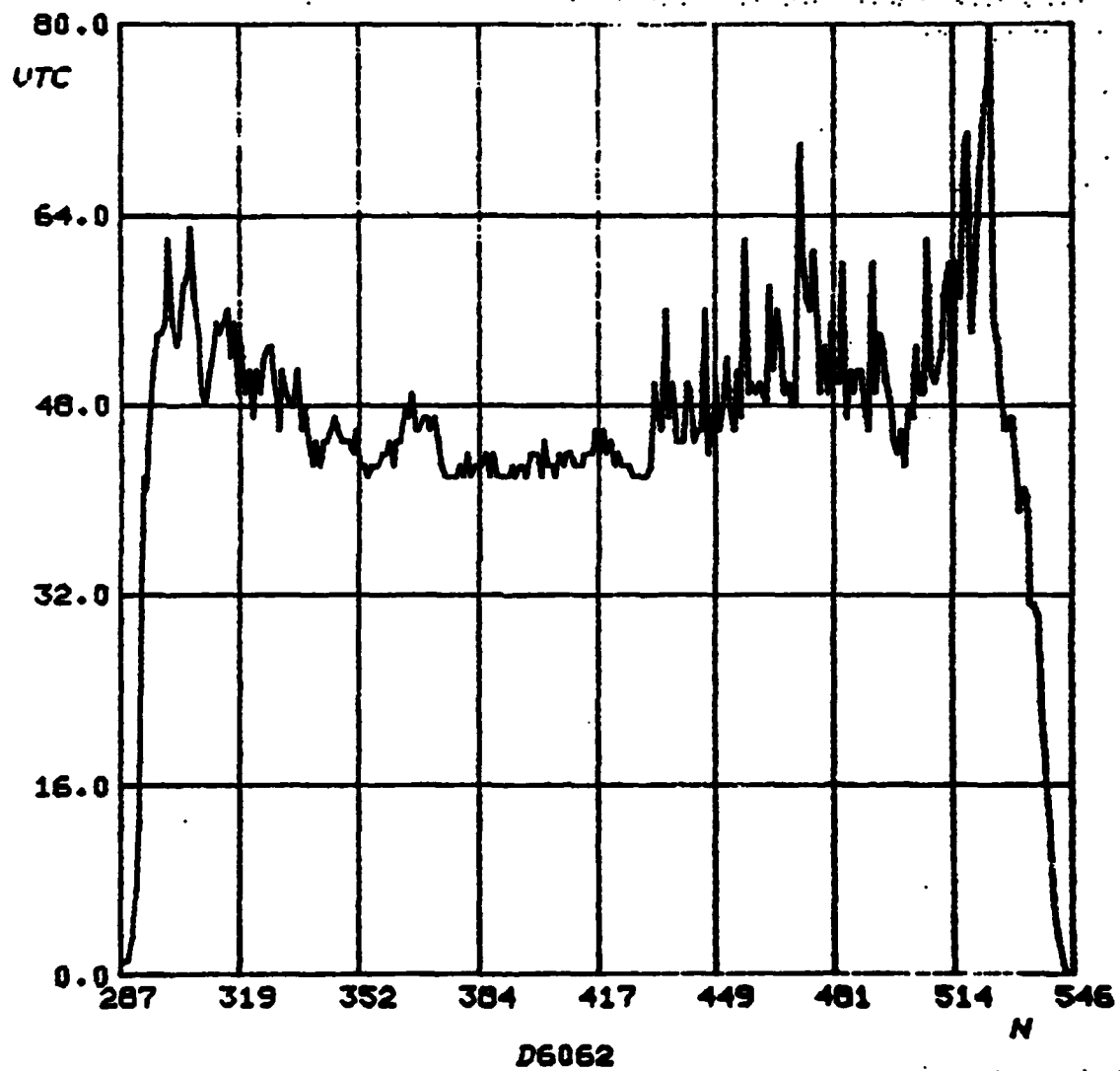
F/G 17/2

NL

									END				



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A



QSET1 E6062

QSET2 E6062

-----PASS 1

N	VTC
128	1
256	1
384	83
512	94
640	0
768	0
896	0

-----PASS 1

N	VTC
192	1
256	1
320	17
384	83
448	90
512	94
576	28

-----PASS 2

N	VTC
416	86
448	90
480	86
512	94
544	79
576	28
608	0

-----PASS 2

N	VTC
464	86
480	86
496	86
512	94
528	84
544	79
560	83

-----PASS 3

N	VTC
488	91
496	86
504	83
512	94
520	82
528	84
536	90

-----PASS 3

N	VTC
500	90
504	83
508	87
512	94
516	84
520	82
524	79

-----PASS 4

N	VTC
506	95
508	87
510	86
512	94
514	85
516	84
518	83

-----PASS 4

N	VTC
509	88
510	86
511	97
512	94
513	88
514	85
515	87

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 506

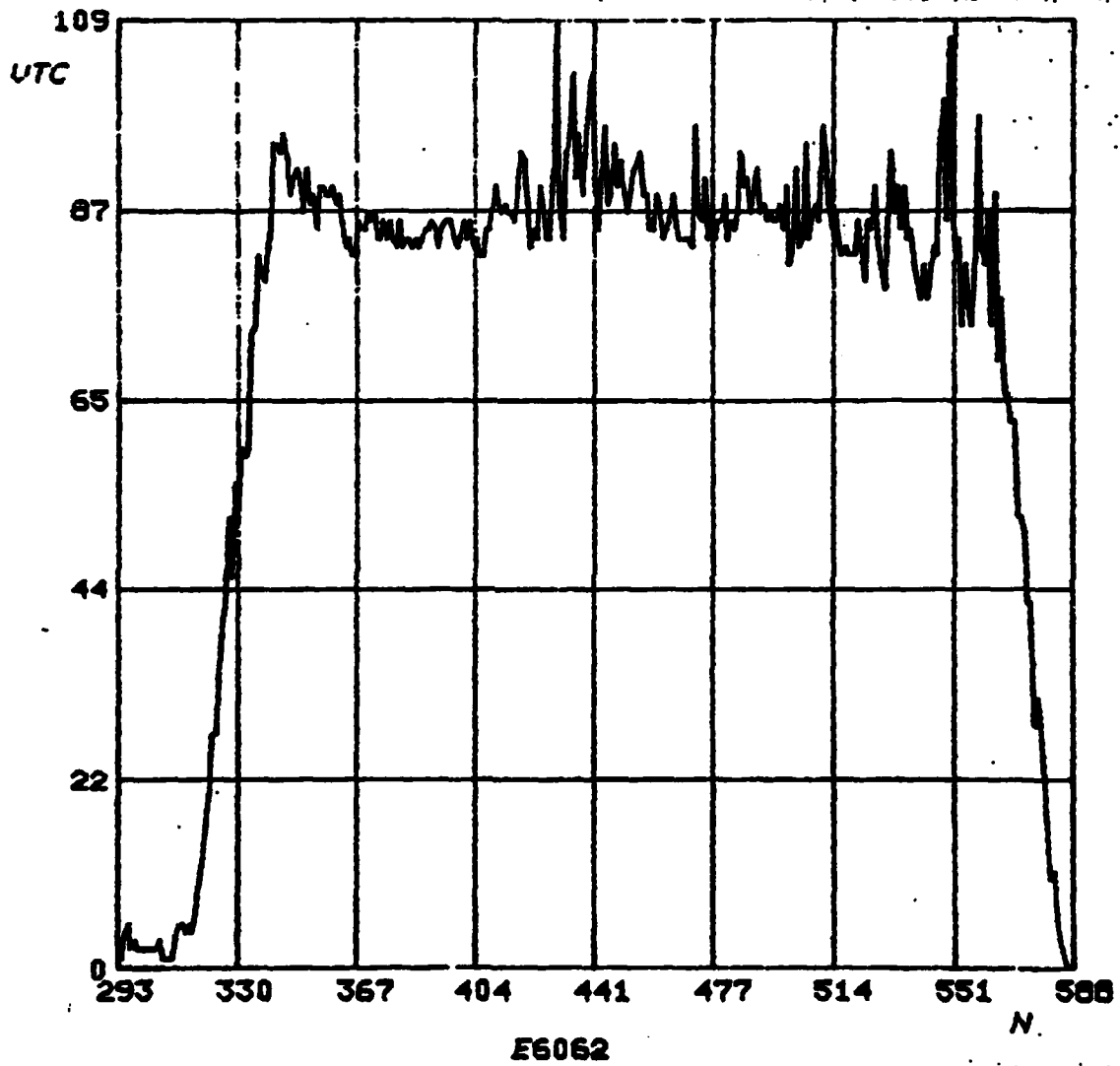
ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 511

ACTUAL VTC PEAK OCCURRED AT N = 429

ACTUAL VTC PEAK OCCURRED AT N = 429

ERROR FROM CORRECT N IS: 77

ERROR FROM CORRECT N IS: 82



QSET1 F6062

QSET2 F6062

-----PASS 1

N	VTC
128	1
256	1
384	39
512	50
640	5
768	0
896	0

-----PASS 1

N	VTC
192	1
256	1
320	23
384	39
448	58
512	50
576	31

-----PASS 2

N	VTC
416	56
448	58
480	57
512	50
544	41
576	31
608	17

-----PASS 2

N	VTC
400	47
416	56
432	58
448	58
464	56
480	57
496	59

-----PASS 3

N	VTC
424	62
432	58
440	62
448	58
456	55
464	56
472	62

-----PASS 3

N	VTC
484	55
488	54
492	54
496	59
500	61
504	56
508	53

-----PASS 4

N	VTC
418	58
420	62
422	61
424	62
426	59
428	56
430	58

-----PASS 4

N	VTC
497	57
498	63
499	61
500	61
501	57
502	58
503	56

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 424

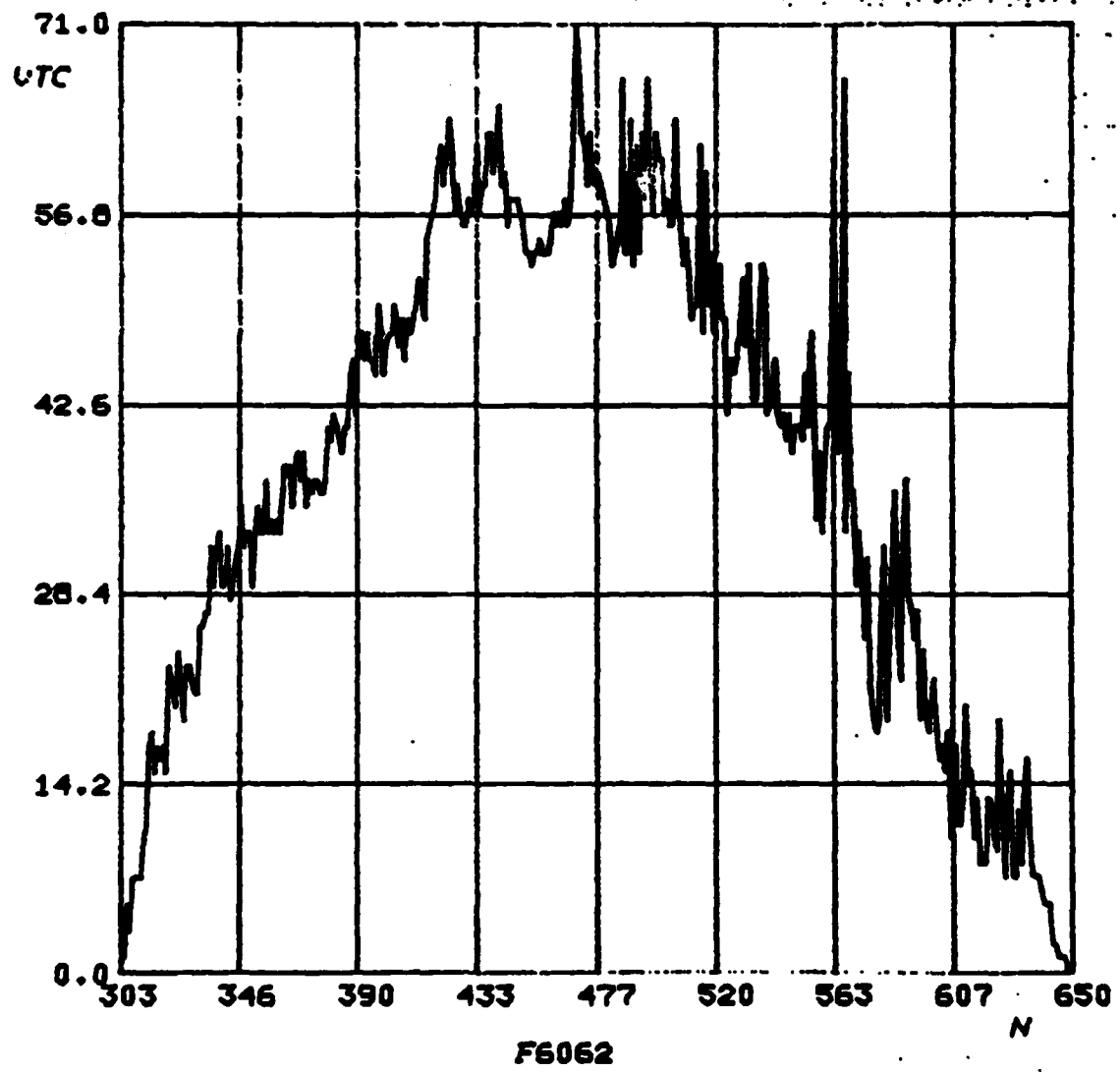
ACTUAL VTC PEAK OCCURRED AT N = 469

ERROR FROM CORRECT N IS: ^45

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 498

ACTUAL VTC PEAK OCCURRED AT N = 469

ERROR FROM CORRECT N IS: 29



QSET1 A6231

QSET2 A6231

-----PASS 1

-----PASS 1

N	VTC
128	1
256	1
384	155
512	129
640	0
768	0
896	0

N	VTC
192	1
256	1
320	52
384	155
448	170
512	129
576	4

-----PASS 2

-----PASS 2

N	VTC
288	1
320	52
352	102
384	155
416	195
448	170
480	146

N	VTC
400	186
416	195
432	186
448	170
464	163
480	146
496	151

-----PASS 3

-----PASS 3

N	VTC
392	169
400	186
408	193
416	195
424	195
432	186
440	178

N	VTC
404	192
408	193
412	189
416	195
420	198
424	195
428	193

-----PASS 4

-----PASS 4

N	VTC
410	190
412	189
414	191
416	195
418	197
420	198
422	194

N	VTC
417	192
418	197
419	195
420	198
421	195
422	194
423	194

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 420

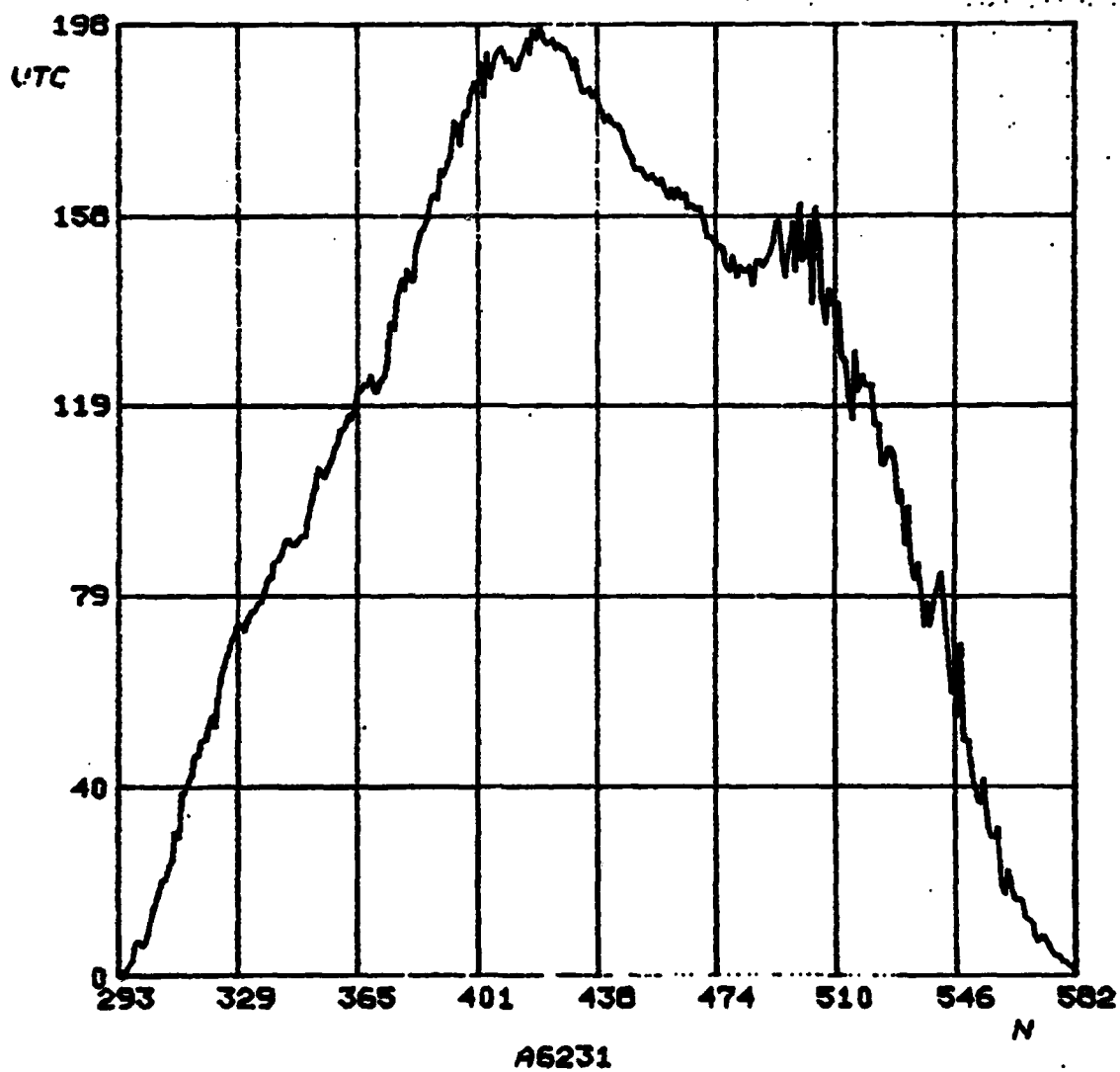
ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE VTC CURVE IS N = 420

ACTUAL VTC PEAK OCCURRED AT N = 420

ACTUAL VTC PEAK OCCURRED AT N = 420

ERROR FROM CORRECT N IS: 0

ERROR FROM CORRECT N IS: 0



QSET1 A6232

-----PASS 1

N	UTC
128	1
256	1
384	153
512	101
640	0
768	0
896	0

-----PASS 2

N	UTC
288	1
320	46
352	91
384	153
416	178
448	169
480	153

-----PASS 3

N	UTC
392	157
400	166
408	177
416	178
424	181
432	175
440	167

-----PASS 4

N	UTC
418	174
420	173
422	178
424	181
426	182
428	177
430	174

ACCORDING TO QSET1, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE UTC CURVE IS N = 426

ACTUAL UTC PEAK OCCURRED AT N = 452

ERROR FROM CORRECT N IS: ^26

QSET2 A6232

-----PASS 1

N	UTC
192	1
256	1
320	46
384	153
448	169
512	101
576	9

-----PASS 2

N	UTC
400	166
416	178
432	175
448	169
464	173
480	153
496	123

-----PASS 3

N	UTC
404	169
408	177
412	179
416	178
420	173
424	181
428	177

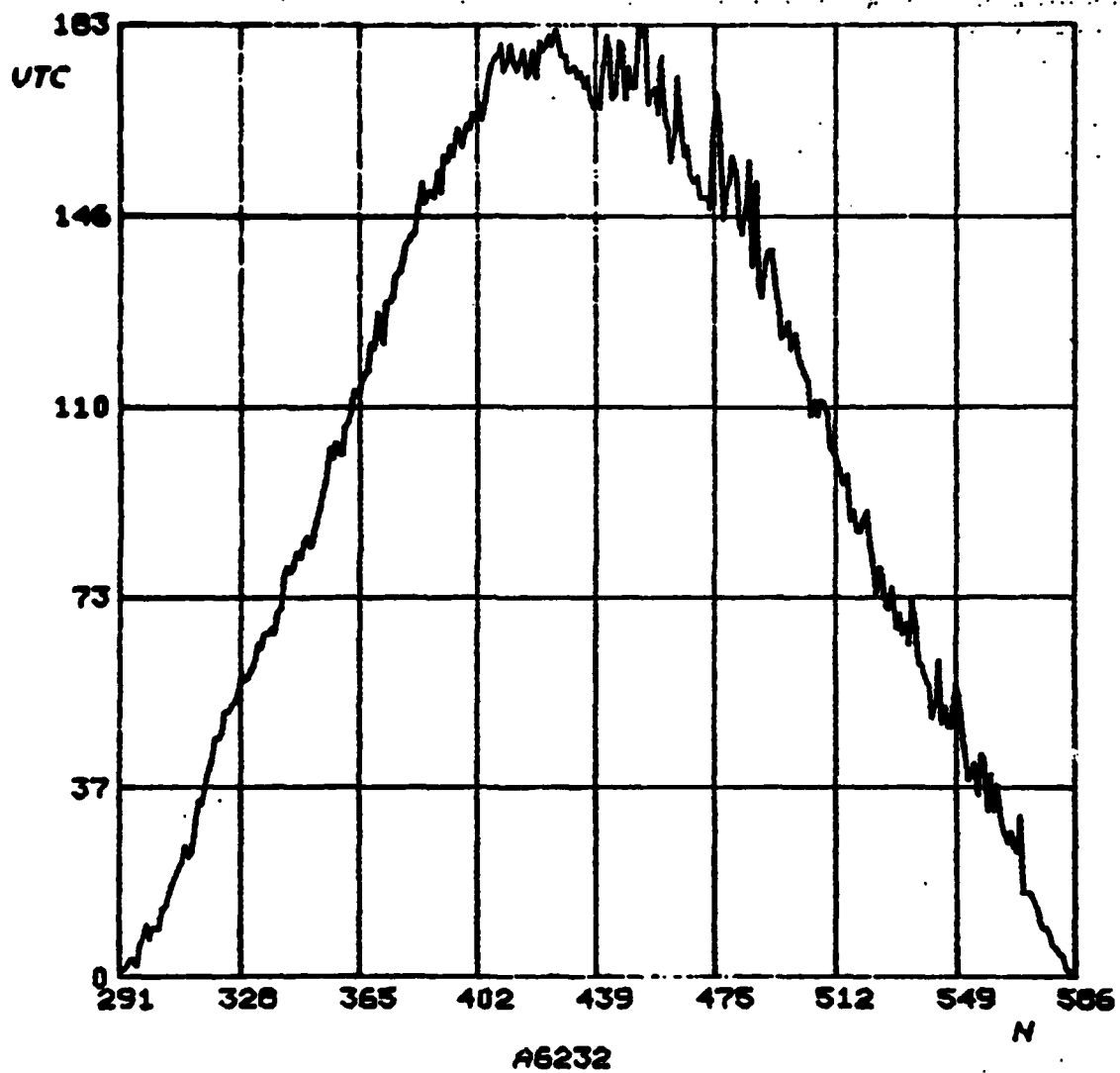
-----PASS 4

N	UTC
421	180
422	178
423	179
424	181
425	179
426	182
427	180

ACCORDING TO QSET2, THE
THRESHOLD VALUE PRODUCING
THE PEAK OF THE UTC CURVE IS N = 426

ACTUAL UTC PEAK OCCURRED AT N = 452

ERROR FROM CORRECT N IS: ^26



QSET1 A6233

-----PASS 1

N	UTC
128	1
256	1
384	114
512	136
640	0
768	0
896	0

-----PASS 2

N	UTC
416	182
448	178
480	156
512	136
544	105
576	49
608	2

-----PASS 3

N	UTC
392	139
400	149
408	156
416	182
424	200
432	190
440	188

-----PASS 4

N	UTC
418	184
420	186
422	183
424	200
426	192
428	191
430	196

ACCORDING TO QSET1, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE UTC CURVE IS N = 424
 ACTUAL UTC PEAK OCCURRED AT N = 423
 ERROR FROM CORRECT N IS: 1

QSET2 A6233

-----PASS 1

N	UTC
192	1
256	1
320	19
384	114
448	178
512	136
576	49

-----PASS 2

N	UTC
480	149
416	182
432	190
448	178
464	172
480	156
496	149

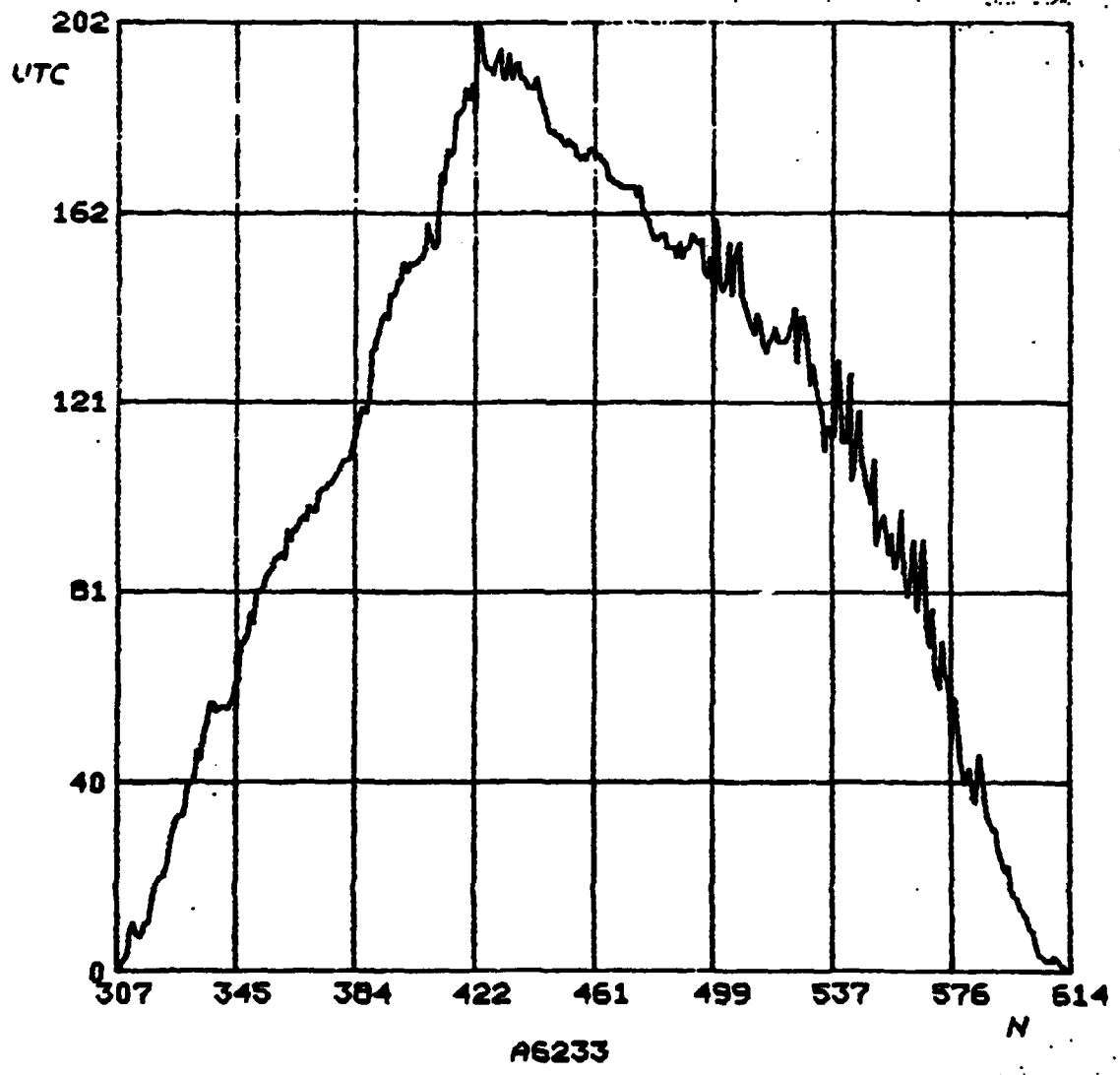
-----PASS 3

N	UTC
420	186
424	200
428	191
432	190
436	193
440	188
444	184

-----PASS 4

N	UTC
421	189
422	183
423	202
424	200
425	194
426	192
427	192

ACCORDING TO QSET2, THE
 THRESHOLD VALUE PRODUCING
 THE PEAK OF THE UTC CURVE IS N = 423
 ACTUAL UTC PEAK OCCURRED AT N = 423
 ERROR FROM CORRECT N IS: 0



APPENDIX D

DATA SET TRANSFER AND PLOTTING

The purpose of this appendix is to document the procedure for gathering VTC-versus-N data and transferring it to the Multics Computing System for analysis. Included are the source codes and explanations for the software used with the F8 microprocessor and with the Multics Graphics System.

To analyze the VTC curve for a particular set of conditions, the first step is to prepare the scanner for gathering a data set by loading and running the software package PLOT4 with Sense Switches 4, 5, and 6 in the DOWN position. (The Sense Switches are located on the front panel of the F8). With the Experimental Calibration Pattern (ECP) ready, the scanner start button should be pressed to initiate the page-scanning sequence. Once the moving assembly is approximately mid-page, the scanner should be frozen in position with the Crossfeed-Motor Pause Switch. Now, by referencing the shape of the analog video signal with an oscilloscope, the ECP to be scanned can be placed into position. VTC data are taken and stored in the F8 RAM memory when Sense 5 is placed to the UP position. Since PLOT4 gathers VTC data for every value of N from $N = 0$ to $N = 768$, it will take about three seconds from the time Sense 5 is activated until all data have been stored. The status of the lights on the front panel of the F8 will indicate when data transfer is complete. (Note that it is a simple software modification to alter the sampling range of

N if necessary.) At this point, if one is satisfied with the conditions under which the data was taken, Sense 4 can be placed UP which will terminate the PLOT4 routine. Otherwise PLOT4 can be recycled by first placing Sense 5 DOWN and then momentarily placing Sense 6 UP and then DOWN.

By resetting PLOT4, this enables the user to overwrite the original set of data with new data.

The next step is to enter the F8 DEBUG program to gain access to the data set that is now stored in RAM. The data buffer begins at memory location 0100(HEX), but significant data normally starts between 0500(HEX) and 0600(HEX). The data can be examined in BYTE form by using the DIM (display memory) command described in the F8 manuals. Values of N and VTC each require two bytes, and N-VTC data pairs are stored consecutively. As an example, data displayed by the command, DIM 0910-0A7F are shown in Figure D.1. To minimize the amount of storage and Multics computer time required, the bounds of significant VTC data should be ascertained before transferring any information out of RAM.

With the bounds of the data determined, the next step is to write the data into an F8 disk file for permanent storage and ease of manipulation. While still in the DEBUG program, the following sequence of commands will accomplish this:

```
MON
ASS CR WDISK <filename>,00:1
DEBUG
DIM <starting RAM address>--<ending RAM address>
MON
ASS CR ZTO
```

The data set is now in the form of an ASCII file on disk. To transfer the data to the Multics System, the following commands must be added to the file by the XEDIT editor. Before the data, include these lines:

```
&version 2
&trace off
&attach
apl -ttp ASCII
input2
```

After the data, include these lines:

```
stop
&detach
&quit
```

The disk file should now appear like the example in Figure D.2.

The F8 program, MULTX, is used to transfer the disk file to a Multics storage segment via dial-up link. Since the data set is now set up as an exec file, the Multics segment name must have the .ec suffix, e.g. filename.ec. With the data in a segment, any of a number of options can be employed to convert the data from its ASCII format to a usable decimal equivalent. However, this author used APL language for data manipulations. The procedure therefore continues as such: An APL workspace named CONTINUE must be already established and contain as a minimum the functions INPUT2 and CONVERT whose listings and explanations are included in this appendix. With these prerequisites met, execute the data set segment with the Multics command,

```
ec filename
```

A terminal prompt message will indicate when data transfer is complete. Multics is now in the APL ASCII mode and the proper

conventions must be followed. To complete the data conversion, select an appropriate variable name for the data set and invoke the function, CONVERT:

```
VARIABLENAME <- CONVERT
```

VARIABLENAME becomes a two-dimensional array with each row representing an X-Y (or N-VTC) data pair. The various APL functions described in the remainder of this appendix can now be used to operate on the data as necessary. One note of caution concerning the plotting functions should be observed. ALWAYS link and unlink the Multics Graphics I/O at the Multics Command level, NEVER while within the APL mode. The commands to do this are,

```
setup_graphics      (sg)  
remove_graphics    (rg)
```

The syntax associated with these commands should be reviewed in the Multics Users Manuals as necessary.

```

M0910 = 02 05 01 30 02 06 01 30
M0918 = 02 07 01 2C 02 08 01 2D
M0920 = 02 09 01 25 02 0A 01 24
M0928 = 02 0B 01 24 02 0C 01 25
M0930 = 02 0D 01 19 02 0E 01 19
M0938 = 02 0F 01 1D 02 10 01 19
M0940 = 02 11 01 1C 02 12 01 1C
M0948 = 02 13 01 19 02 14 01 15
M0950 = 02 15 01 14 02 16 01 14
M0958 = 02 17 01 11 02 18 01 0D
M0960 = 02 19 01 0D 02 1A 01 0D
M0968 = 02 1B 01 0C 02 1C 01 10
M0970 = 02 1D 01 05 02 1E 01 08
M0978 = 02 1F 01 08 02 20 00 FD
M0980 = 02 21 00 FD 02 22 00 FD
M0988 = 02 23 00 FD 02 24 00 F9
M0990 = 02 25 00 F9 02 26 00 F8
M0998 = 02 27 00 F4 02 28 00 EC
M09A0 = 02 29 00 F0 02 2A 00 EC
M09A8 = 02 2B 00 ED 02 2C 00 ED
M09B0 = 02 2D 00 EC 02 2E 00 E1
M09B8 = 02 2F 00 E0 02 30 00 E4
M09C0 = 02 31 00 E8 02 32 00 DD
M09C8 = 02 33 00 DD 02 34 00 DC
M09D0 = 02 35 00 E4 02 36 00 D9
M09D8 = 02 37 00 D8 02 38 00 D1
M09E0 = 02 39 00 D1 02 3A 00 D0
M09E8 = 02 3B 00 CC 02 3C 00 CD
M09F0 = 02 3D 00 C9 02 3E 00 C8
M09F8 = 02 3F 00 C5 02 40 00 C1
MOA00 = 02 41 00 C0 02 42 00 C0
MOA08 = 02 43 00 BC 02 44 00 BC
MOA10 = 02 45 00 BC 02 46 00 C1
MOA18 = 02 47 00 BC 02 48 00 B0
MOA20 = 02 49 00 AC 02 4A 00 AD
MOA28 = 02 4B 00 A8 02 4C 00 A5
MOA30 = 02 4D 00 A4 02 4E 00 98
MOA38 = 02 4F 00 98 02 50 00 94
MOA40 = 02 51 00 8D 02 52 00 8C
MOA48 = 02 53 00 8D 02 54 00 88
MOA50 = 02 55 00 8D 02 56 00 85
MOA58 = 02 57 00 80 02 58 00 89
MOA60 = 02 59 00 84 02 5A 00 84
MOA68 = 02 5B 00 7D 02 5C 00 7D
MOA70 = 02 5D 00 79 02 5E 00 78
MOA78 = 02 5F 00 74 02 60 00 75

```

FIGURE D.1 SAMPLE LISTING OF THE F8 DEBUG PROGRAM USING "DISPLAY MEMORY"

```

$version 2
$trace off
$attach
api -ttp ASCII
input2
MO5D8 = 01 37 00 01 01 38 00 01
MO5E0 = 01 39 00 01 01 3A 00 03
MO5E8 = 01 3B 00 1B 01 3C 00 16
MO5F0 = 01 3D 00 07 01 3E 00 04
MO5F8 = 01 3F 00 05 01 40 00 04
MO600 = 01 41 00 06 01 42 00 03
MO608 = 01 43 00 02 01 44 00 02
MO610 = 01 45 00 01 01 46 00 02
MO618 = 01 47 00 02 01 48 00 02
MO620 = 01 49 00 04 01 4A 00 02
MO628 = 01 4B 00 02 01 4C 00 04
MO630 = 01 4D 00 05 01 4E 00 05
MO638 = 01 4F 00 06 01 50 00 0A
MO640 = 01 51 00 0A 01 52 00 0F
MO648 = 01 53 00 11 01 54 00 14
MO650 = 01 55 00 13 01 56 00 15
MO658 = 01 57 00 18 01 58 00 1F
MO660 = 01 59 00 24 01 5A 00 2A
MO668 = 01 5B 00 2F 01 5C 00 3E
MO670 = 01 5D 00 3D 01 5E 00 3F
MO678 = 01 5F 00 46 01 60 00 43
MO680 = 01 61 00 4D 01 62 00 4D
MO688 = 01 63 00 51 01 64 00 52
MO690 = 01 65 00 5A 01 66 00 56
MO698 = 01 67 00 52 01 68 00 53
MO6A0 = 01 69 00 4F 01 6A 00 58
MO6A8 = 01 6B 00 57 01 6C 00 5B
MO6B0 = 01 6D 00 53 01 6E 00 5A
MO6B8 = 01 6F 00 58 01 70 00 64
MO6C0 = 01 71 00 5D 01 72 00 62
MO6C8 = 01 73 00 65 01 74 00 6C
MO6D0 = 01 75 00 6C 01 76 00 73
MO6D8 = 01 77 00 70 01 78 00 6E
MO6E0 = 01 79 00 70 01 7A 00 6E
MO6E8 = 01 7B 00 76 01 7C 00 76
MO6F0 = 01 7D 00 81 01 7E 00 77
MO6F8 = 01 7F 00 7D 01 80 00 78
MO700 = 01 81 00 7D 01 82 00 81
MO708 = 01 83 00 82 01 84 00 86
MO710 = 01 85 00 8C 01 86 00 8C
MO718 = 01 87 00 8B 01 88 00 90
MO720 = 01 89 00 91 01 8A 00 94
MO728 = 01 8B 00 9D 01 8C 00 92
MO730 = 01 8D 00 A4 01 8E 00 A9
MO738 = 01 8F 00 AA 01 90 00 B3
MO740 = 01 91 00 B4 01 92 00 BF
MO748 = 01 93 00 BA 01 94 00 BE
MO750 = 01 95 00 C4 01 96 00 C0
MO758 = 01 97 00 C3 01 98 00 C1
MO760 = 01 99 00 CA 01 9A 00 CC
MO768 = 01 9B 00 CE 01 9C 00 CC
MO770 = 01 9D 00 CB 01 9E 00 D0
MO778 = 01 9F 00 C6 01 A0 00 C7
MO780 = 01 A1 00 C5 01 A2 00 CC
MO788 = 01 A3 00 CA 01 A4 00 C8

```

```

MO790 = 01 A5 00 BC 01 A6 00 BB
MO798 = 01 A7 00 BB 01 A8 00 BE
MO7A0 = 01 A9 00 C1 01 AA 00 BA
MO7A8 = 01 AB 00 BB 01 AC 00 B6
MO7B0 = 01 AD 00 B2 01 AE 00 B4
MO7B8 = 01 AF 00 B4 01 B0 00 B0
MO7C0 = 01 B1 00 B3 01 B2 00 B1
MO7C8 = 01 B3 00 B1 01 B4 00 AE
MO7D0 = 01 B5 00 AD 01 B6 00 AC
MO7D8 = 01 B7 00 A5 01 B8 00 A3
MO7E0 = 01 B9 00 A0 01 BA 00 9D
MO7E8 = 01 BB 00 A5 01 BC 00 9F
MO7F0 = 01 BD 00 A2 01 BE 00 9F
MO7F8 = 01 BF 00 9E 01 C0 00 9D
MO800 = 01 C1 00 9E 01 C2 00 98
MO808 = 01 C3 00 9D 01 C4 00 95
MO810 = 01 C5 00 93 01 C6 00 92
MO818 = 01 C7 00 95 01 C8 00 98
MO820 = 01 C9 00 91 01 CA 00 94
MO828 = 01 CB 00 92 01 CC 00 8A
MO830 = 01 CD 00 85 01 CE 00 85
MO838 = 01 CF 00 82 01 D0 00 84
MO840 = 01 D1 00 85 01 D2 00 85
MO848 = 01 D3 00 8D 01 D4 00 83
MO850 = 01 D5 00 83 01 D6 00 7D
MO858 = 01 D7 00 83 01 D8 00 7C
MO860 = 01 D9 00 77 01 DA 00 78
MO868 = 01 DB 00 7E 01 DC 00 75
MO870 = 01 DD 00 73 01 DE 00 6E
MO878 = 01 DF 00 68 01 E0 00 65
MO880 = 01 E1 00 7A 01 E2 00 6D
MO888 = 01 E3 00 69 01 E4 00 69
MO890 = 01 E5 00 61 01 E6 00 5B
MO898 = 01 E7 00 5A 01 E8 00 5C
MO8A0 = 01 E9 00 73 01 EA 00 56
MO8A8 = 01 EB 00 54 01 EC 00 56
MO8B0 = 01 ED 00 55 01 EE 00 50
MO8B8 = 01 EF 00 4A 01 FO 00 4B
MO8C0 = 01 F1 00 47 01 F2 00 45
MO8C8 = 01 F3 00 48 01 F4 00 3E
MO8D0 = 01 F5 00 40 01 F6 00 3F
MO8D8 = 01 F7 00 34 01 F8 00 42
MO8E0 = 01 F9 00 31 01 FA 00 38
MO8E8 = 01 FB 00 37 01 FC 00 38
MO8F0 = 01 FD 00 30 01 FE 00 2F
MO8F8 = 01 FF 00 32 02 00 00 29
MO900 = 02 01 00 22 02 02 00 1F
MO908 = 02 03 00 1C 02 04 00 20
MO910 = 02 05 00 1C 02 06 00 13
MO918 = 02 07 00 13 02 08 00 12
MO920 = 02 09 00 0C 02 0A 00 0D
MO928 = 02 0B 00 0A 02 0C 00 09
MO930 = 02 0D 00 07 02 0E 00 06
MO938 = 02 0F 00 05 02 10 00 03
MO940 = 02 11 00 01 02 12 00 00
MO948 = 02 13 00 00 02 14 00 00
stop
$detach
$quit

```

FIGURE D.2

DATA FILE AS IT SHOULD APPEAR
BEFORE TRANSFERRING TO MULTIOS

DATA PLOT DATA GENERATOR, V4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0000 0001 PLOT4   ORG   0
0002 *
0003 *           TITLE 'DATA PLOT DATA GENERATOR, V4'
0004 *
0005 * THIS IS THE FOLLOW-ON SOFTWARE TO PLTT2
0006 * FOR GENERATING X-Y PAIRS TO EVALUATE
0007 * TEST PATTERNS TO BE USED BY THE AUTO-
0008 * Matic THRESHOLD SEQUENCE.
0009 *
0010 * APPROXIMATE RAM LOCATIONS ARE DISPLAYED
0011 * ON THE SCREEN WHERE SIGNIFICANT DATA
0012 * STARTS.
0013 *
0014 * WRITTEN BY CAPT B.J. STANTON, 22 JUN 62.
0015 *
0016 * SENSE SWITCH FUNCTIONS:
0017 *
0018 * #           DOWN           UP
0019 * -----
0020 * 4  NORMAL OPERATION   RETURN TO LOS4
0021 * 5  HOLD AT BEGINNING  TAKE DATA
0022 * 6  HOLD AT END       RETURN TO BEGINNING
0023 * -----
0024 *
0000 0025 THRSINL EQU  H'00'  THRESHOLD LOW INIT.
0000 0027 THRSINH EQU  H'00'  THRESHOLD HI  INIT.
0000 0028 VCRSET EQU  H'90'  DIG VIDEO CNT RESET
0003 0029 THRMX   EQU  H'03'  MAX THRESHOLD VALUE
0100 0030 DATBUF EQU  H'100'  1ST MEMORY LOCATION
0004 0031 F1      EQU  4
0002 0032 F2      EQU  2
0003 0033 F3      EQU  3
0005 0034 VLS     EQU  5
0005 0035 DLY     EQU  5
0035 *
0037 *
0200 2A0100 0100 0038 INIT   DCI  DATBUF  INITIALIZE DATA BUF
0003 2000      0039 LI     THRSINL INITIALIZE THRESHOLD
0005 50        0040 LR     0,A   COUNTERS
0006 2000      0041 LI     THRSINH R0 IS LOW BYTE
0005 51        0042 LR     1,A   R1 IS HI  BYTE
0009 70        0043 CLR                    .
000A 54        0044 LR     F1,A
000B 52        0045 LR     F2,A
000C 53        0046 LR     F3,A
000D 201E      0047 LI     0'30'
000F 56        0048 LR     DLY,A
0049 *
0010 70        0050 STARTER CLR                    HOLD
0011 30        0051 JUTS  0   UNTIL SENSE S
0012 A0        0052 INS   0   IS PLACED UP.
0013 2120      0053 NI     H'20'
0015 54FA      0010 0054 BZ     STARTER
0055 *
0056 * CALL SUBROUTINE FSTLN, 12/90 BY R.L.M.
0057 * TO TEST FOR FALLING EDGE OF PRINTLINE.
0058 *
0017 2800B2 0052 0059 PI     FSTLN
001A 208C      0060 LI     VCRSET  RESET VIDEO COUNT
001C 2713      0061 JUT   H'13'
  
```

DATA PLOT DATA GENERATOR.V4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

001E	70		0062		CLR		
001F	2713		0063		JUT	H'13'	
			0064	*			
0021	40		0065	INCTHR	LR	A,0	INCREMENT LOWER
0022	1F		0066		INC		THRESHOLD BYTE
0023	50		0067		LR	0,A	
0024	920C	0031	0068		BNC	OUTTHR	
0026	41		0069		LR	A,1	INCREMENT UPPER
0027	1F		0070		INC		THRESHOLD BYTE
0028	51		0071		LR	1,A	WITH CARRY
0029	2503		0072		CI	THRMAX	TEST FOR MAX
0029	9405	0031	0073		BNC	OUTTHR	THRESHOLD VALUE
002D	70		0074		CLR		(GIVES MIN THRES-
002E	51		0075		LR	1,A	HOLD VOLTAGE)
002F	906E	009E	0076		BR	RESET	
			0077	*			
0031	40		0078	JUTTHR	LR	A,0	UPDATE THRESHOLD
0032	2712		0079		JUT	H'12'	VALUE THROUGH
0034	41		0080		LR	A,1	PORTS 12 AND 13
0035	2713		0081		JUT	H'13'	
0037	2800B2	0062	0082		PI	FSTLN	TEST FOR END OF
			0083	*			PRINTLINE
003A	41		0084		LR	A,1	STORE THRESHOLD
003B	17		0085		ST		UPPER BYTE
003C	40		0086		LR	A,0	STORE THRESHOLD
003D	17		0087		ST		LOWER BYTE
003E	70		0088		CLR		
003F	2711		0089		JUT	H'11'	STORE DIGITAL VIDEO
0041	2611		0090		IN	H'11'	UPPER BYTE
0043	13		0091		COM		
0044	17		0092		ST		
0045	70		0093		CLR		
0046	2710		0094		JUT	H'10'	STORE DIGITAL VIDEO
0048	2610		0095		IN	H'10'	LOWER BYTE
004A	13		0096		COM		
004B	17		0097		ST		
004C	55		0098		LR	VLS,A	ALSO STORE IN 55
004D	44		0099		LR	A,F1	
004E	2400		0100		AI	0	TEST FLAG 1
0050	941E	006F	0101		BNC	=1	
0052	45		0102		LR	A,VLS	
0053	2102		0103		NI	H'02'	TEST FOR CHANGE IN
0055	34C4	001A	0104		BZ	RVC	VIDEO COUNT
0057	71		0105		LIS	1	
0058	54		0106		LR	FLW	CHANGE FLAG 1 TO 1
0059	2C		0107		YDC		
005A	2A0100	010C	0108		DCI	H1+21	
005D	2900C4	00C4	0109		PI	SHOV	
0060	2A00E3	0CE3	0110		DCI	H1	
0063	40		0111		LR	A,0	
0064	57		0112		LR	7,A	
0065	71		0113		LIS	1	
0066	50		0114		LR	0,A	
0067	283653	3653	0115		PI	H'3653'	DISPLAY ROUTINE
006A	2C		0116		YDC		
006B	47		0117		LR	A,7	RESTORE COUNT
006C	5C		0118		LR	0,A	
006D	9CAC	0C1A	0119		BP	RVC	
			0120	*			
006F	42		0121	AI	LR	A,F2	TEST FLAG 2
0070	240C		0122		AI	0	

DATA PLOT DATA GENERATOR, V4
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

```

0072 3423 0096 0123 BZ 32
0074 43 0124 LR A,F3 TEST FLAG 3
0075 2400 0125 AI 0
0077 34A2 001A 0126 BNZ RVC
0079 45 0127 LR A,7L3
007A 2400 0128 AI 0 CHECK VIDEO COUNT
007C 349D 001A 0129 BNZ RVC EQUAL TO ZERO
007E 71 0130 LIS 1
007F 53 0131 LR F3,A SET FLAG 3 TO 1
0080 2C 0132 XDC
0081 2A0113 0113 0133 DCI M2+16
0084 2900C4 00C4 0134 PI SHOW
0087 2A0103 0103 0135 DCI M2
008A 40 0136 LR A,0
008B 57 0137 LR 7,A SAVE THRESHOLD COUNT
008C 71 0138 LIS 1
008D 50 0139 LR 0,A
008E 283653 3653 0140 PI H'3653'
0091 2C 0141 XDC
0092 47 0142 LR A,7
0093 50 0143 LR 0,A
0094 3085 001A 0144 BR RVC
0145 *
0096 36 0146 BZ DS DLY
0097 3452 001A 0147 BNZ RVC
0099 71 0148 LIS 1
009A 52 0149 LR F2,A SET FLAG 2 TO 1
009B 29001A 001A 0150 JMP RVC
0151 *
0152 *
0153 *
009E 70 0154 RESET CLR HOLD UNTIL
009F 30 0155 JUTS 0 SENSE 5 IS PLACED UP
00A0 A0 0156 INS 0
00A1 2140 0157 NI H'40'
00A3 3404 00A3 0158 BZ RS2
00A5 290000 0000 0159 JMP INIT
00A8 70 0160 RS2 CLR
00A9 30 0161 JUTS 0 CHECK FOR SENSE 4
00AA A0 0162 INS 0 UP TO RETURN TO
00AB 2110 0163 NI H'10' D054
00AD 3470 009E 0164 BZ RESET
00AF 292330 2330 0165 JMP H'2330'
0166 *
0167 * SUBROUTINE FSTLN
0168 *
0169 * WRITTEN BY R.L. VINCIGUERRA, 12/80.
0170 *
0171 * THIS SUBROUTINE WAITS FOR THE SIGNAL PRINT-
0172 * LINE TO MAKE A FALLING TRANSITION SIGNALLING
0173 * THE END OF A LINE OF VIDEO INFORMATION.
0174 * DUE TO AN INVERSION IN THE FE I/O PORTS,
0175 * THIS PROGRAM IS DESIGNED TO CATCH A RISING
0176 * TRANSITION.
0177 *
0178 *
0040 0179 ENSENS EQU H'40'
0180 *
0032 2040 0181 FSTLN LI ENSENS ENABLE SENSE INPUTS
0034 35 0182 JUTS 5
0035 70 0183 LPI CLR LOOP UNTIL FALSE
  
```

DATA PLOT DATA GENERATOR, 74
 ERRS LOC OBJECT ADDR LINE

SOURCE STATEMENT

0086	B4		0184	OUTS	4	
0087	A4		0185	INS	4	
0088	2101		0186	NI	H'01'	
008A	94FA	0085	0187	BNZ	LPI	
008C	70		0188	CLR		LOOP UNTIL TRUE
008D	B4		0189	OUTS	4	
008E	A4		0190	INS	4	
008F	2101		0191	NI	H'01'	
00C1	84FA	008C	0192	BZ	LP2	
00C3	1C		0193	POP		
			0194	=		
			0195	=		END OF SUBROUTINE FSTLN-----
			0196	=		
			0197	=		SUBROUTINE TO CONVERT KEY TO ASCII-----
			0198	=		
00C4	2C		0199	SHOW	YDC	
00C5	11		0200	LR	H,DC	
00C5	2C		0201		YDC	
00C7	4A		0202	LR	A,10	
00C8	210F		0203	NI	H'0F'	
00CA	2430		0204	AI	H'30'	
00CC	2539		0205	CI	H'39'	
00CE	3103	00D2	0206	BP	SH1	
00D0	2407		0207	AI	H'07'	
00D2	17		0208	SH1	ST	
00D3	4B		0209	LR	A,11	
00D4	14		0210	SR	4	
00D5	2430		0211	AI	H'30'	
00D7	2539		0212	CI	H'39'	
00D9	3103	00DD	0213	BP	SH2	
00DB	2407		0214	AI	H'07'	
00DD	17		0215	SH2	ST	
00DE	4B		0216	LR	A,11	
00DF	210F		0217	NI	H'0F'	
00E1	2430		0218	AI	H'30'	
00E3	2539		0219	CI	H'39'	
00E5	3103	00E9	0220	BP	SH3	
00E7	2407		0221	AI	H'07'	
00E9	17		0222	SH3	ST	
00EA	1C		0223	POP		
			0224	=		
			0225	=		END SUBROUTINE SHOW-----
			0226	=		
00E3	0016		0227	::1	DC	HL2'0016'
00E5	444154		0228		DC	C'DATA STARTS AROUND '
0100	232323		0229		DC	C'***'
0103	0011		0230	::2	DC	HL2'0011'
0105	444154		0231		DC	C'DATA STOPS AT ***'
			0232	=		
			0233	=		
			0234		END	

CO ERRS

▽ADDPLOT1[]▽

```

▽ ADDPLOT1 A;SH;PC;P;V
[1]  ▽ THIS FUNCTION ACCEPTS A TWO DIMENSIONAL ARRAY
[2]  ▽ ARRANGED AS X-Y PAIRS, IT AUTOMATICALLY PLOTS THE DATA
[3]  ▽ TO THE SCALE ESTABLISHED BY ONE OF THE SCALING FUNCTIONS,
[4]  ▽ THE VIRTUAL GRAPHICS TABLE MUST BE INITIALIZED BY EITHER
[5]  ▽ SETSCALE OR GRIDSCALE,
[6]  ▽ THIS FUNCTION MAY BE USED TO PLOT MULTIPLE SETS OF
[7]  ▽ DATA ALTHOUGH EACH SET WILL BE DRAWN WITH A SOLID LINE,
[8]  ▽ ALSO NOTE THAT THE RANGES OF THE MULTIPLE SETS
[9]  ▽ OF DATA MUST BE COMPATIBLE,
[10] SH + PA
[11] P ← LL,(GFSCALE (SF,1))
[12] PC ← 1
[13] P ← P,(GFVECTOR (A[PC] - SX[1]),0)
[14] LP; PC ← PC + 1
[15] P ← P,(GFVECTOR (A[PC] - A[PC-1]),0)
[16] → (PC ≠ SH[1])/LP
[17] GFDISPLAYAPPEND (GFARRAY P)

```

▽ADDPLOT2[]▽

```

▽ ADDPLOT2 A;SH;PC;P;V
[1]  ▽ THIS FUNCTION ACCEPTS A TWO-DIMENSIONAL ARRAY
[2]  ▽ ARRANGED AS X-Y PAIRS AND PLOTS THE DATA ACCORDING
[3]  ▽ TO THE SCALE ESTABLISHED BY ONE OF THE SCALING FUNCTIONS,
[4]  ▽ THE VIRTUAL GRAPHICS TABLE MUST BE INITIALIZED BY EITHER
[5]  ▽ SETSCALE OR GRIDSCALE,
[6]  ▽ THIS FUNCTION MAY BE USED TO PLOT SUCCESSIVE SETS OF
[7]  ▽ DATA AS LONG AS THE RANGES ARE COMPATIBLE,
[8]  ▽ USES DIFFERENT LINETYPES FOR MULTIPLE PLOTS,
[9]  ▽
[10] SH + PA
[11] P ← LL,(GFSCALE (SF,1)),GFLINETYPE LT
[12] PC ← 1
[13] P ← P,(GFSHIFT (A[PC] - SX[1]),0)
[14] LP; PC ← PC + 1
[15] P ← P,(GFVECTOR (A[PC] - A[PC-1]),0)
[16] → (PC ≠ SH[1])/LP
[17] GFDISPLAYAPPEND (GFARRAY P)
[18] LT ← LT + 1

```


GRAPHSCALE

```

0100  GRAPHSCALE (YSCALE)XL)XSHIFT)YL)YS)YT)XMIN)YMIN)XMAX)YMAX)XMT)YMT
0110  * THIS FUNCTION INITIALIZES THE VERTICAL GRAPHICS TABLE
0120  * AND DRAWS X AND Y AXES ALONG WITH A GRID ACCORDING TO
0130  * THE RANGES MANUALLY INPUT FOR X AND Y. DATA IS MEANT
0140  * TO BE PLOTTED BY GDDPLOT1 OR GDDPLOT2.
0150  *
0160  * THE NUMBER OF TICKS ON EACH AXIS CAN BE CONTROLLED
0170  * BY STORING THE DESIRED NUMBER IN XMT AND YMT.
0180  *
0190  * BEFORE CALLING THIS FUNCTION,THE DESIRED LABELS
0200  * MUST BE ESTABLISHED IN THE FOLLOWING GLOBAL VARIABLES:
0210  * 'LABEL' SHOULD CONTAIN THE LABEL FOR THE GRAPH
0220  * 'XLABEL' SHOULD CONTAIN THE LABEL FOR THE X-AXIS
0230  * 'YLABEL' SHOULD CONTAIN THE LABEL FOR THE Y-AXIS
0240  *
0250  XMT = 8
0260  YMT = 5
0270  GFINIT
0280  SXY = (2 2F(X,Y))
0290  SXN = SXY[;1]
0300  R = (SXY[;2] - SXY[;1])
0310  W = 900 + R
0320  LL = GFSETPOSITION 7400 7400 0
0330  P = GFSETPOSITION 7400 500 0
0340  LT = CA + 0
0350  XL = 0 7900 0
0360  XS = (900+XMT),(0 0)
0370  XT = 0 710 0
0380  L1 = P + P,(GFLINETYPE LT),(GFVECTOR XL),GFSHIFT XT
0390  P = P,(2 GFTEXT ((PREC R[1])+(MIN[1] + R[1])xCA+XMT))
0400  P = P,(GFSHIFT (XS-XL+XT))
0410  CA = CA + 1
0420  LT = 2
0430  W = (CA * (XMT + 1))/L1
0440  P = P,(GFSETPOSITION 500 7400 0)
0450  YL = 7900 0 0
0460  YS = 0,(900+YMT),0
0470  YT = 710 0 0
0480  LT = CA + 0
0490  L2 = P + P,(GFLINETYPE LT),(GFVECTOR YL), GFSHIFT YT
0500  P = P,(6 GFTEXT ((PREC R[2])+(MIN[2] +R[2])xCA+YMT))
0510  P = P,GFSHIFT (YS-YL+YT)
0520  CA = CA +1
0530  LT = 2
0540  W = (CA * (YMT + 1))/L2
0550  P = P,(GFSETPOSITION 20 7475 0),(5 GFTEXT LABEL)
0560  P = P,(GFSETPOSITION 7500 450 0),(4 GFTEXT YLABEL)
0570  P = P,(GFSETPOSITION 450 7450 0),(5 GFTEXT XLABEL)
0580  GFDISPLAY (GFARRAY P)
0590  LT = 0

```

▽INPUT2[]▽

```
▽ INPUT2 (XYDAT);NEWLN
[11]  A THIS FUNCTION ACCEPTS ASCII DATA ON A LINE-BY-LINE
[21]  A BASIS.  EACH LINE MUST BE AT LEAST 10 CHARACTERS LONG.
[31]  A THE FUNCTION WILL TERMINATE ON ENCOUNTERING A LINE
[41]  A SHORTER THAN 10 CHARACTERS.  DATA IS LOADED INTO THE
[51]  A ONE-DIMENSIONAL GLOBAL ARRAY: CHAR,
[61]  COUNT←1
[71]  XYDAT←[]
[81]  LP: NEWLN←[]
[91]  →((PNEWLN)<10)/STOP
[101] XYDAT←XYDAT,NEWLN
[111] COUNT←COUNT+1
[121] →LP
[131] STOP: CHAR←XYDAT
[141] 'FILE TRANSFER COMPLETE'
```

▽

▽CONVERT[]▽

```
▽ XY ← CONVERT (R;CN;N;I;A;DEC;CVT);IO
[11]  A THIS FUNCTION IS TAILORED TO CONVERT ASCII DATA
[21]  A FROM THE F8 'DISPLAY MEMORY' FORMAT TO A
[31]  A TWO-DIMENSIONAL ARRAY OF X-Y DATA POINTS.  DATA
[41]  A MUST HAVE BEEN READ INTO THE WORKSPACE WITH THE
[51]  A FUNCTION, INPUT2.
[61]  R←(COUNT,31)PCHAR
[71]  N←R[9 10 12 13 15 16 18 19 21 22 24 25 27 28 30 31]
[81]  CN←((COUNT×4),4)PM
[91]  CVT←'0123456789ABCDEF'
[101] IO←0
[111] I←CVT{CN
[121] IO←1
[131] A←1
[141] DEC←16,I[A;]
[151] LP1: A←A+1
[161] DEC←DEC,(16,I[A;])
[171] →(A<((COUNT×4))/LP1
[181] XY←((COUNT×2),2)PDEC
[191] CHAR ← 0
```

▽

∇PLOTGRIDSSCALE[[]]∇

∇ PLOTGRIDSSCALE A

```
[1]  A THIS FUNCTION IS A SELF-CONTAINED PLOTTING FUNCTION  
[2]  A THAT AUTOMATICALLY SCALES THE X AND Y AXES ACCORDING  
[3]  A TO THE RANGES OF THE X-Y DATA, GRIDS ARE INCLUDED,  
[4]  A  
[5]  SKY ← (2 2*(L/AC[1]),(F/AC[1]),(L/AC[2]),(F/AC[2]))  
[6]  SKY[1:] GRIDSSCALE SKY[2:]  
[7]  ADOFPLOT1 A
```

∇

∇PLOTSCALE[[]]∇

∇ PLOTSCALE A

```
[1]  A THIS FUNCTION IS A SELF-CONTAINED PLOTTING FUNCTION  
[2]  A THAT AUTOMATICALLY SCALES THE X AND Y AXES ACCORDING  
[3]  A TO THE RANGES OF THE X-Y DATA, NO GRIDS ARE DRAWN,  
[4]  A  
[5]  SKY ← (2 2*(L/AC[1]),(F/AC[1]),(L/AC[2]),(F/AC[2]))  
[6]  SKY[1:] SETSCALE SKY[2:]  
[7]  ADOFPLOT1 A
```

∇

∇PREC[[]]∇

∇ N ← PREC R

```
[1]  A THIS FUNCTION IS CALLED BY THE SCALE FUNCTION TO  
[2]  A DETERMINE THE PRECISION OF THE X AND Y SCALES,  
[3]  →(R>154)/51  
[4]  →(R>100)/52  
[5]  →(R > 5)/53  
[6]  →(R ≥ 1)/54  
[7]  51: N ← 72  
[8]  → 0  
[9]  52: N ← 0  
[10] → 0  
[11] 53: N ← 1  
[12] → 0  
[13] 54: N ← 2
```

∇

VRANGE[00]7

```

V RANGE (R)MAX(R)C
E11  R THIS FUNCTION YIELDS THE R FOR OF AND Y VALUES
E12  R AND THE VALUE OF N GENERALLY 0 AND
E13  R USEFUL IN CHECKING FOR VALID DATA TRANSFER AFTER
E14  R EXECUTING THE SUBROUTINE TO GET AND CONVERT
E15  R
E16  R MIN AND MAX VALUES OF X ARE (1+(L/A[11])+(F/A[11]))
E17  R
E18  R MTC = (F/A[21])
E19  R MIN AND MAX VALUES OF Y ARE (1+(L/A[21]),MTC)
E20  R
E21  R
E22  R + PA
E23  R C + 1
E24  R LOOP: →(MTC = A[21])/DISP
E25  R C + C+1
E26  R → LOOP
E27  R DISP: 'THE THRESHOLD VALUE'
E28  R 'GENERATING'
E29  R 'MTC IS AT N = ',A[11]

```

VXYDUMP[00]7

```

V PRINT + XYDUMP A;L;E;C1;C2;S;P
E11  R THIS FUNCTION FORMATS A TWO-DIMENSIONAL DATA
E12  R SET FOR PRINTING ON AN 8.5 * 11 PAGE,
E13  R
E14  R SP ← 300 4P ' '
E15  R C2 ← 0
E16  R L ← (PA)[1]
E17  R S ← ' '
E18  R → (L<300)/L1
E19  R E ← ((300-L))+A[L;1]
E20  R L ← PE
E21  R C ← ((L,1)PE),(LE0)
E22  R A ← A,[1]E
E23  R L1: A ← 300 2PA
E24  R A ← 50 + A
E25  R A ← A,SP
E26  R C2: C2 ← C2 + 1
E27  R → (C2=41)/L4
E28  R C1 ← 0
E29  R L3: S ← S,A[(C2+C1*50);1]
E30  R → (C1=4)/L2
E31  R C1 ← C1 + 1
E32  R → L3
E33  R L4: S ← 1+S
E34  R S ← 50 70 PS
E35  R PRINT + S

```

GFSETSCALE[117]

```

V GFSETSCALE (MINIF) (RMAX) (XT) (YS) (T) (CA) (NXT) (NYT)
[11]  n THIS FUNCTION INITIALIZES THE VIRTUAL GRAPHICS TABLE
[12]  n AND DRAWS X AND Y AXES ACCORDING TO THE STYLES GIVEN
[13]  n FOR X AND Y. NO GRID IS PROVIDED, DATA TO
[14]  n BE PLOTTED BY ADDPLOT1 OR ADDPLOT2.
[15]  n
[16]  n THE NUMBER OF TICKS ON EACH AXIS CAN BE CONTROLLED
[17]  n BY STORING THE DESIRED NUMBER IN NXT AND NYT.
[18]  n BEFORE CALLING THIS FUNCTION, THE DESIRED LABELS
[19]  n MUST BE ESTABLISHED;
[20]  n GLOBAL VARIABLE 'LABEL' SHOULD CONTAIN THE TITLE OF THE
[21]  n GRAPH.
[22]  n GLOBAL VARIABLES 'XLABEL' AND 'YLABEL' ARE THE
[23]  n LABELS FOR THE TWO AXES.
[24]  n
[25]  NYT ← 5
[26]  NXT ← 8
[27]  GFINIT
[28]  SKY ← (2 2*(X,Y))
[29]  MIN ← SKY[11]
[30]  R ← (SKY[12] - SKY[11])
[31]  GF ← 900 + R
[32]  P ← P, GFSETPOSITION 7400 7400 0
[33]  P ← P, GFVECTOR 900 0 0
[34]  P ← P, LL, GFVECTOR 0 900 0
[35]  XS ← (900+NXT)*(0 0)
[36]  XT ← 0 710 0
[37]  CA ← 0
[38]  P ← P, LL
[39]  L1: P ← P, (GFVECTOR XT), GFSHIFT XT
[40]  P ← P, (2 GFTEXT ((PREC R[1])+(MIN[1] + R[1]*CA+NXT)))
[41]  P ← P, GFSHIFT (XS - (2 X XT))
[42]  CA ← CA + 1
[43]  → (CA*(NXT + 1))/L1
[44]  YS ← 0, (900-NYT), 0
[45]  YT ← 710 0 0
[46]  CA ← 0
[47]  P ← P, LL
[48]  L2: P ← P, (GFVECTOR YT), GFSHIFT YT
[49]  P ← P, (2 GFTEXT ((PREC R[2])+(MIN[2] + R[2]*CA+NYT)))
[50]  P ← P, GFSHIFT (YS - (2 X YT))
[51]  CA ← CA + 1
[52]  → (CA*(NYT + 1))/L2
[53]  P ← P, (GFSETPOSITION 20 7475 0), (5 GFTEXT LABEL)
[54]  P ← P, (GFSETPOSITION 7500 450 0), (4 GFTEXT YLABEL)
[55]  P ← P, (GFSETPOSITION 450 7450 0), (5 GFTEXT XLABEL)
[56]  GFDISPLAY (GFARRAY P)
V

```

708400T10019

7 084001

7

708400T20019

7 084002

011 LABEL + 'ECC A SCANNED UNDER THE SAME CONDITIONS'
012 250 550 SETSCALE 0 225
031 ADDPLOT A6071
041 ADDPLOT A6072
051 ADDPLOT A6073
061 ADDPLOT A6074
071 ADDPLOT A6075
081 LABEL + 'EFFECT OF ONE LAMP VERSUS TWO USING ECC A'
091 275 550 SETSCALE 0 225
101 ADDPLOT A6063
111 ADDPLOT A6064
121 LABEL + 'EFFECT OF OLD VERSUS NEW LAMPS USING ECC A'
131 300 625 SETSCALE 0 225
141 ADDPLOT A6063
151 ADDPLOT A6233
161 LABEL + 'EFFECT OF DIFFERENT PAPER COLORS USING ECC A'
171 275 600 SETSCALE 0 225
181 ADDPLOT A6062
191 ADDPLOT A6066
201 ADDPLOT A606A
211 ADDPLOT A606D
221 LABEL + 'EFFECT OF DIFFERENT COLORS OF FLUORESCENT LIGHTS USING ECC A'
231 275 625 SETSCALE 0 225
241 ADDPLOT A6231
251 ADDPLOT A6232
261 ADDPLOT A6233
271 LABEL + 'ECC B'
281 225 650 SETSCALE 0 475
291 ADDPLOT A6062

7

APPENDIX E

MODIFIED SCANNER CIRCUITS

This Appendix contains the documentation for all changes made to the scanner circuitry along with the pin connections for the new F8 I/O ports 10 through 13 (hex). The THRESHOLD LEVEL GENERATOR (TLG), Video A-to-D Converter, and VIDEO COUNTERS are located on the VIDEO DETECTION AND THRESHOLDING board. The old Video A-to-D Converter and manual threshold circuit were removed from the TIMING AND PROCESSING board.

Although no additional circuits were changed, it is also noted here that during the course of this project, severe clocking interference necessitated the relocation of several circuit boards that use the high-frequency clock signal generated on the CCD board. Specifically, the following boards were mounted on the top of the mechanical moving assembly of the scanner to minimize the lengths of the leads carrying clocking signals:

1. SYNCHRONIZED LINE-FREQUENCY GENERATOR
2. F8 INTERFACE BOARD NUMBER 4
3. TIMING AND PROCESSING
4. VIDEO DETECTION AND THRESHOLDING

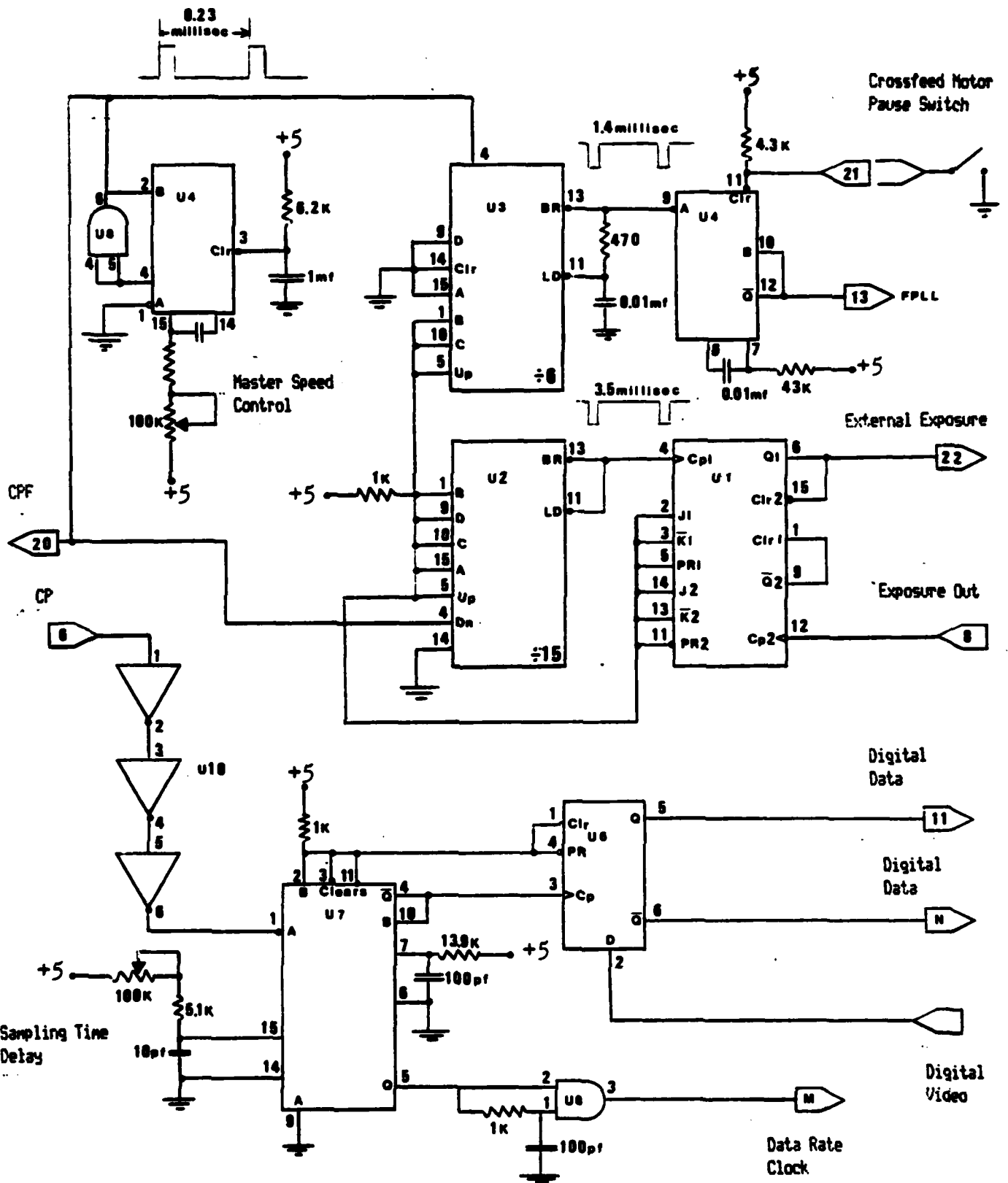
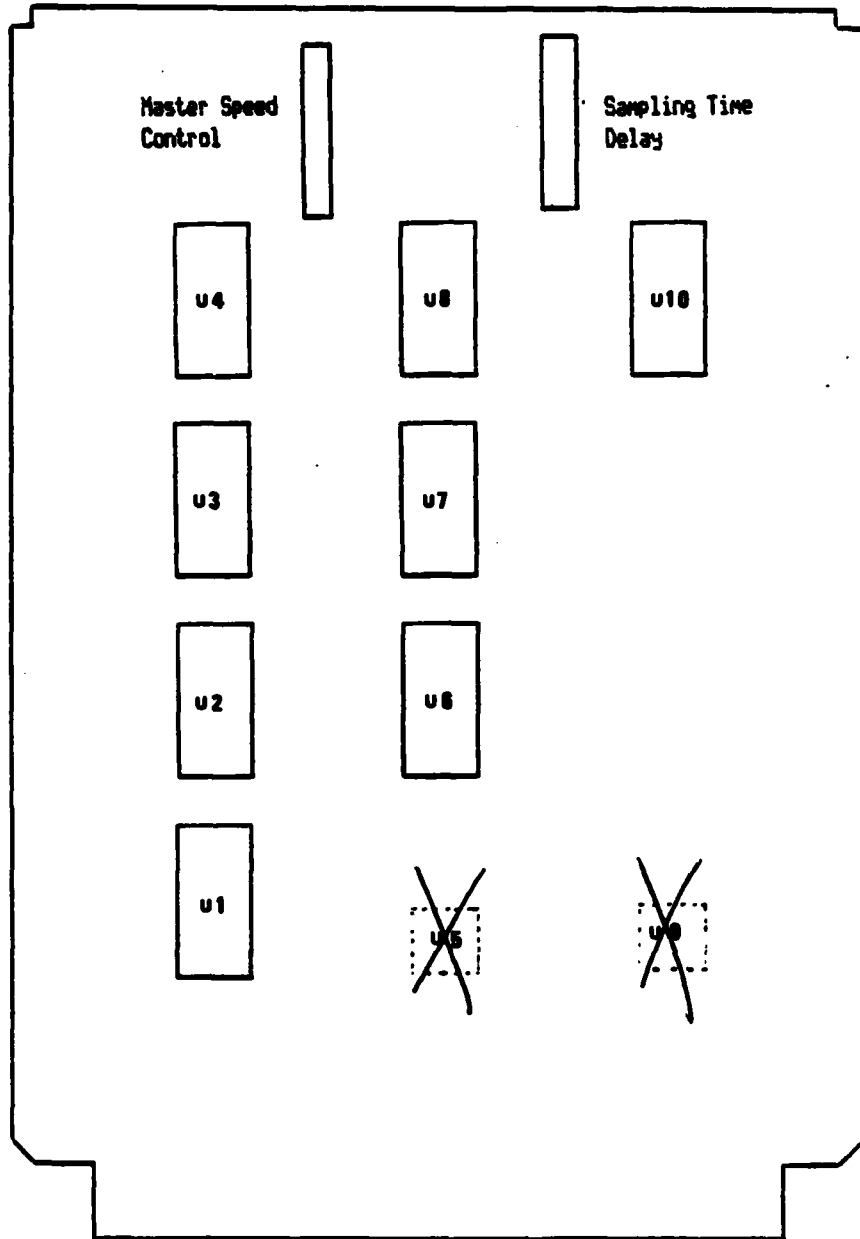


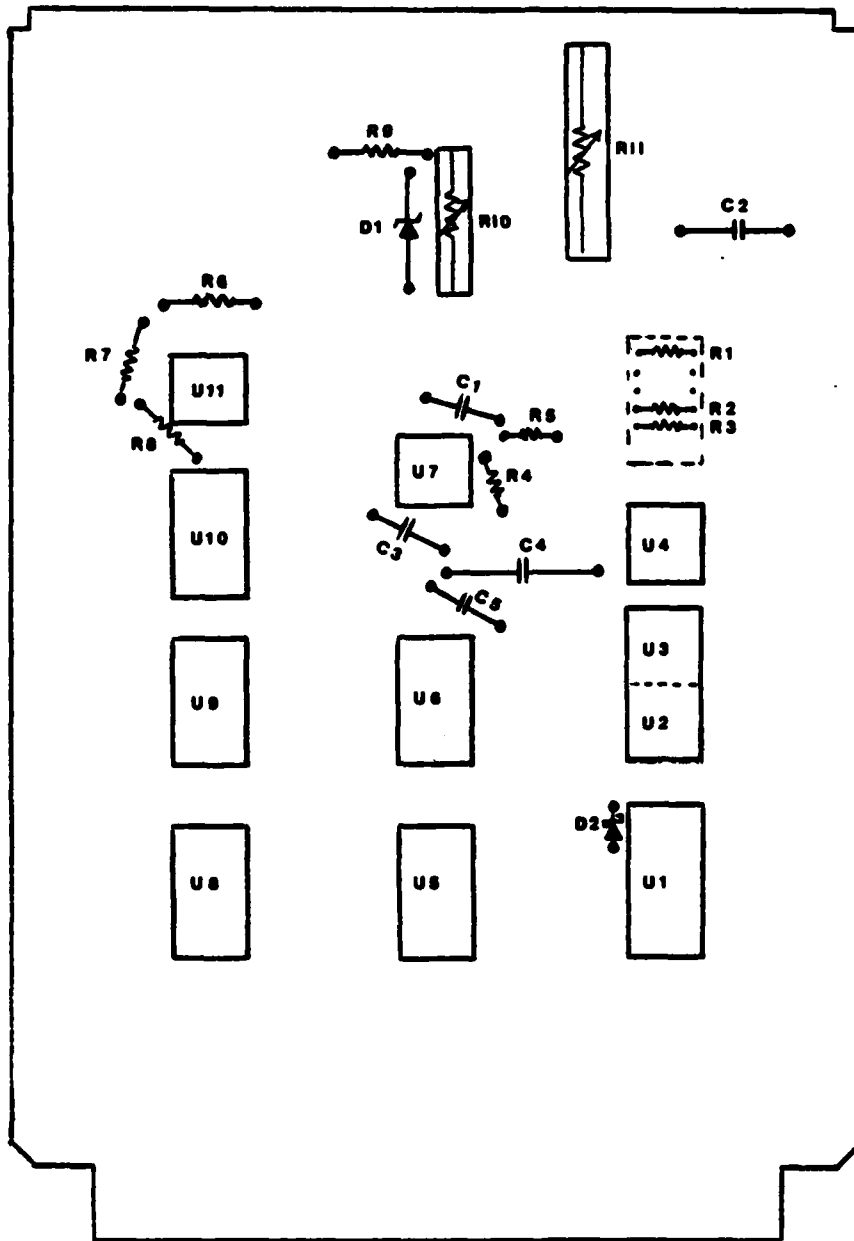
FIGURE E.1

TIMING AND PROCESSING CIRCUIT DIAGRAM
 Revision 2, June 1982
 (U5 and U9 Removed)



- U1 = 74LS109
- U2 = 74LS193
- U3 = 74LS193
- U4 = 74LS123
- U6 = 74LS74
- U7 = 74LS123
- U8 = 74LS08
- U10 = 74LS14

FIGURE E.2 TIMING AND PROCESSING CIRCUIT BOARD LAYOUT
 Revision 2, June 1982
 (U5 and U9 Removed)



- C1 = 0.01 Microfarads
- C2 = 0.01 Microfarads
- C3 = 47 Microfarads
- C4 = 2.01 Microfarads
- D1 = 13-Volt Zener
- D2 = HP5082-2811
- R1 = 5K Ohms
- R2 = 6K Ohms
- R3 = 1K Ohms
- R4 = 560 Ohms
- R5 = 270 Ohms
- R6 = 750 Ohms
- R7 = 3.6K Ohms
- R8 = 3.6K Ohms
- R9 = 560 Ohms
- R10 = 5K Ohms
- R11 = 500K Ohms
- U1 = AD7533
- U2 = 741
- U3 = 741
- U4 = 741
- U5 = 74LS04
- U6 = 74LS04
- U7 = LM311
- U8 = 74LS393
- U9 = 74LS393
- U10 = 74LS00
- U11 = LM311

FIGURE E.3 VIDEO DETECTION AND THRESHOLDING
CIRCUIT BOARD LAYOUT

VIDEO DETECTION AND THRESHOLDING BOARD

PIN CONNECTIONS

A	+15 Volts	1	N Value Bit 1
B	PRINTLINE In	2	N Value Bit 2
C	Digital Video Out	3	N Value Bit 3
D		4	N Value Bit 4
E		5	N Value Bit 5
F		6	N Value Bit 6
H		7	N Value Bit 7
J		8	N Value Bit 8
K		9	N Value Bit 9
L	+5 Volts	10	N Value Bit 10
M	MTC Clear	11	VTC Bit 1
N	VTC Bit 16	12	VTC Bit 2
P	VTC Bit 15	13	VTC Bit 3
R	VTC Bit 14	14	VTC Bit 4
S	VTC Bit 13	15	VTC Bit 5
T	Analog Video In	16	VTC Bit 6
U		17	VTC Bit 7
V	-15 Volts	18	VTC Bit 8
W		19	VTC Bit 9
X		20	VTC Bit 10
Y		21	VTC Bit 11
Z	Master Ground	22	VTC Bit 12

TIMING AND PROCESSING BOARD

PIN CONNECTIONS

A	+5 Volts	1	+5 Volts
B	Ground	2	Ground
C		3	
D		4	
E		5	Digital Video In
F		6	CP
H		7	
J		8	EXPOSURE OUT
K		9	
L		10	
M	DATA RATE CLOCK	11	DIGITAL DATA
N	DIGITAL DATA	12	
P		13	FPLL
R		14	
S		15	
T		16	
U		17	
V		18	
W		19	
X		20	Test Point
Y		21	
Z		22	EXTERNAL EXPOSURE

NEW FB I/O PORT PIN ASSIGNMENTS

<u>Port Address</u>	<u>Pin Connections (LSB to MSB)</u>
10	1 2 3 4 5 6 7 8
11	10 11 12 13 14 15 16 17
12	Z Y X W V U T S
13	P N M L K J H F

END

FILMED

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DTIC