





A FRIEDLAND-LIKE FILTERING TECHNIQUE FOR ESTIMATING PIECEWISE CONSTANT CONTROLS IN DISCRETE LINEAR STOCHASTIC SYSTEMS*

BY

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*Research supported by the U.S. Naval Research Office under NONR N00014-80-C-0775 (NR 041-568).

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ABSTRACT

We consider discrete linear stochastic processes in which the control variables take unknown jumps at unknown times and remain constant between jumps. We develop a Friedland-like filtering technique for obtaining the optimum estimates \hat{x} of the state and \hat{u} of the control:

 $\hat{\mathbf{x}} = \tilde{\mathbf{x}} + \mathbf{S}_{\mathbf{u}}\tilde{\mathbf{u}} + \mathbf{S}_{\mathbf{x}}\tilde{\Delta \mathbf{u}}$ $\hat{\mathbf{u}} = \tilde{\mathbf{u}} + \mathbf{S}_{\Delta \mathbf{u}}\tilde{\Delta \mathbf{u}}$

where x is the control-free, jump-free estimate of the state x, \tilde{u} is the jump-free estimate of the control u and Δu is the optimum estimate of the jump Δu in control. The matrix S_u is a function of the x-filter gain. The matrices S_x and $S_{\Delta u}$ depend on the gains of both the x-and the u-filters.

A GLR algorithm is presented for detecting . ump time. It consists of the \tilde{x} - and the \tilde{u} -filters and a bank of Δu -filters. A procedure is developed for reinitializing the \tilde{x} - and the

*President, Practical Sciences, Inc., 40 Long Ridge Road, Carlisle, MA 01741 u-filters after a jump has been detected. After reinitialization the optimum estimates \hat{x} and \hat{u} are functions only of \hat{x} and \hat{u} , satisfying Friedland's expression. The reinitialization procedure provides the tri-filter technique with the capability to handle multiple jumps.

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The advent of the tri-filter technique together with the reinitialization procedure makes it unnecessary to augment the state x with the control u and to use augmented state filters in the estimation of state and piecewise constant controls. The new GLR algorithm avoids, therefore, computational problems that may be associated with processing large matrices in augmented state filters. It uses only unaugmented state filters and, consequently, it has particular application to problems involving a large number of state and/or jump variables.

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1. INTRODUCTION

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Techniques for the detection and estimation of abrupt changes in discrete linear stochastic systems have a variety of applications. They are applicable to target motion analysis and the tracking of maneuvering targets, [1] - [5]. In aircraft control they are used for the detection of actuator and sensor failures, e.g., [6] and [7]. In electrocardiogram analysis, they are used to detect sudden changes in the rhythm of the heart, [8]. They have been applied to the problem of detecting sudden structure variations in the Italian power system, [9]. A survey of such techniques are given in [10].

The generalized likelihood ratio (GLR) method, [11] and [12], is one of the most attractive and promising approaches with which to develop such techniques. The GLR method provides an optimum decision rule for detecting and estimating abrupt changes (jumps) in stochastic systems. Several techniques have been developed using the GLR approach, [1], [1], [13] - [18]. Willsky and Jones' GLR technique [16] has spurred interest in reducing the computational requirements of the GLR approach and in reducing the computational difficulties associated with large matrices. Chang and Dunn, [17] and [18] have shown that the requirement for matrix inversions (or for solving matrix equations) in GLR techniques such as [16] can be reduced or avoided by using the sequentially updated

Kalman filtering technique described in [19] and [20]. Stalford [1] shows that further reductions in computation and storage are realized by using a decomposition of the maneuver signature matrix (failure signature matrix of [10] and [16]).

Herein, we are interested in discrete linear control (stochastic) processes in which the control vector takes unknown jumps at unknown times and remains constant between jumps (i.e., piecewise constant controls). The extension of the work contained herein, to the case of a time varying control between jumps is dealt with in a future report. Chang and Dunn [18] have treated the time varying bias jump case but their work is based on the underlying assumptions: (1) the jump variable is zero before the jump and (2) there is only one jump. That is, in [18] the vector taking the jump has no influence on the dynamics of the state before the jump; the jump vector jumps from a zero state as far as the dynamics of the system is concerned. They, in essence, treat the case of an unknown time varying bias which appears as a system input at some unknown time. Since we address the case of multiple jumps in control we must necessarily, as a consequence, treat jumps in control that jump from nonzero values.

It is a common practice in engineering to augment the state vector by adding bias terms (such as the control variable considered herein) as additional state variables. We call the resulting system the augmented system and we term the original system the unaugmented system. Augmenting the state vector with the control vector may be undesirable when the augmented state vector is substantially larger in dimension than that of the unaugmented state vector. That is, the additional computations required by augmented state filtering algorithms may become excessive. Also, numerical inaccuracies may be introduced by computations with the larger vectors and matrices of augmented state filters. Friedland [21] and [22] investigated the problem of estimating the state x of a linear process without augmenting to the state a constant but unknown bias vector b. He showed that the optimum estimate \hat{x} of the state could be expressed as

 $\hat{\mathbf{x}} = \hat{\mathbf{x}} + \hat{\mathbf{s}}\hat{\mathbf{b}}$

where x and b are computed using two unaugmented filters. The estimate \tilde{x} is the bias-free estimate, computed as if the bias were zero. The estimate \hat{b} is the optimum estimate of the bias and it is the output of a filter whose state vector is b. The matrix S is a funtion of the bias-free gain matrix. Consequently, Friedland's filtering technique avoids excessive computations and numerical inaccuracies resulting from augmented state filters. Tacker and Lee [23] extended Friedland filtering to the case of estimating a state x in the presence of a time varying bias b.

Chang and Dunn [18] essentially investigated the same problem as that considered by Friedland [21] and Tacker and Lee [23] but with the one difference that the jump time is unknown. That is, the problem considered in [21] and [23] is equivalent to the problem of estimating a jump in the bias vector (from a zero value) when the jump time is known. Chang and Dunn assume the jump time is unknown. They apply the GLR method to estimate the jump time and Friedland's filtering technique to estimate the state x and the time varying bias b. In addition, their GLR algorithm makes use of the sequentially updated Kalman filtering technique for the purpose of minimizing the computations.

Herein, we develop a GLR algorithm for the problem of estimating the state x in the presence of a piecewise constant control variable u with multiple jumps Δu . We show that the optimum estimate \hat{x} is the sum of the outputs of three unaugmented filters:

 $\hat{\mathbf{x}} = \tilde{\mathbf{x}} + \mathbf{S}_{\mathbf{u}}\tilde{\mathbf{u}} + \mathbf{S}_{\mathbf{x}}\tilde{\Delta \mathbf{u}}$

where x is the control-free, jump-free estimate (computed as if no control and no jump were presence), \tilde{u} is the jump-free estimate of the control (computed as if the no jump were presence) and $\tilde{\Delta u}$ is the optimum estimate of the jump. We show that the optimum estimate \hat{u} satisfies the expression

 $\hat{u} = \tilde{u} + S_{\Delta u} \quad \tilde{\Delta u}$

The matrix S_u is a function of the Kalman gain used to compute \tilde{x} . The matrices S_x and $S_{\Delta u}$ are functions of the Kalman gains used to compute \tilde{x} and \tilde{u} . The GLR method is used to detect and estimate the jump time.

Multiple jumps are handled by a reinitialization of the x and \tilde{u} filters after a jump has been detected and estimated. After the reinitialization the optimum estimates satisfy Friedland's expressions [21]:

 $\hat{\mathbf{x}} = \hat{\mathbf{x}} + \mathbf{S}_{\mathbf{u}} \hat{\mathbf{u}}$ $\hat{\mathbf{u}} = \hat{\mathbf{u}}$

where the prime indicates the quantities after reinitialization.

2. SYSTEM DEFINITION: UNAUGMENTED AND AUGMENTED

Consider the following discrete linear stochastic system with control jump:

System Dynamics

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$$x (k+1) = A (k+1,k) x (k) + B (k+1,k) (u (k) + \Delta u_q \delta_{qk}) + \Gamma (k) w (k)$$
(1)

$$u(k+1) = u(k) + \Delta u_{q} \delta_{qk}$$
⁽²⁾

where x is the state vector, u is the control, Δu_q is the jump in control at time q, δ_{qk} is the Kronecker delta, and Γ is the system noise coefficient matrix. The matrix A is the state transition matrix and B is the input control matrix. The jump time q and the jump magnitude Δu_q are unknowns.

Measurement Equation

$$z(k) = H(k) x(k) + U(k)$$
 (3)

where z is the measurement vector and H is the measurement matrix.

The noise sequences w and υ are zero-mean, independent, white Gaussian sequences with covariances defined by

$$E \{w(k) \ w^{T}(j)\} = Q(k) \ \delta_{kj}$$
(4)

$$E\{\upsilon(k) \ \upsilon^{T}(k)\} = R(k) \ \delta_{kj}$$
(5)

where $E\{\cdot\}$ denotes the expectation and the matrix R(k) is bounded positive definite. The initial state x(0) is normally distributed with mean $\hat{x}(0)$ and covariance $P_x(0)$. The initial control u(0) is normally distributed with mean $\hat{u}(0)$ and covariance $P_u(0)$. The cross covariance of x(0) and u(0) is denoted by $P_{xu}(0)$. A description of the variables and their dimensions are given in Table 1. We assume that the linear system (1) - (3) is observable.

We define the augmented state vector X as

The augmented system is given by

$$X(k+1) = \Phi(k+1,k) \quad (X(k) + \Delta X_{\alpha} \delta_{\alpha k}) + \Gamma_{a}(k)w(k)$$
(7)

$$z(k) = H_{a}(k) X(k) + \upsilon(k)$$
 (8)

TABLE 1

SYCTEM VARIABLES FOR DISCRETE LINEAR STOCHASTIC SYSTEM WITH CONTROL JUMP: UNAUGMENTED SYSTEM

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| VARIABLE | DEFINITION | DIMENSION |
|---------------------|---------------------------------------|--------------|
| v (k) | State vector | n¥1 |
| X (K) | | 1171 |
| A(k+1,k) | State transition matrix | nxn |
| B(k+1,k) | Input control matrix | nxp |
| u (k) | Control vector | pxl |
| ∆uq | Jump in control at time q | px1 |
| Γ(k) | System noise coefficient matrix | nxr |
| w(k) | Gaussian white system noise | rxl |
| Q(k) | System noise covariance matrix | rxr |
| z (k) | Measurement at time k | mx1 |
| H(k) | Measurement matrix | mxn |
| υ (k) | Gaussian white measurement noise | mx 1 |
| R(k) | Measurement noise covariance matrix | mxm |
| x (0) | Mean value of x(0) | nxl |
| û (0) | Mean value of u(0) | pxl |
| P _x (0) | Covariance of x(0) | n x n |
| P _{xu} (0) | Cross covariance of $x(0)$ and $u(0)$ | nxp |
| P _u (0) | Covariance of u(0) | pxp |
| $\hat{\Delta u}(q)$ | Mean value of <u></u> ug | px1 |
| P _{Au} (q) | Covariance of Δu_q | pxp |

where

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$$\Phi (k+1,k) = \begin{bmatrix} A(k+1,k) & B(k+1,k) \\ 0 & I \end{bmatrix}$$
(9)

$$\Delta X_{q} = D \Delta u_{q}$$
(10)

$$D = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$
(11)

$$H_{a}(k) = [H(k) O]$$
 (12)

and where $\Gamma_{a}(k)$ is defined as the augmented matrix

$$\Gamma_{a}(k) = \begin{bmatrix} \Gamma(k) \\ 0 \end{bmatrix}$$
 (13)

The initial mean value and covariance are given by

$$\hat{X}(0) = \begin{bmatrix} \hat{X}(0) \\ \hat{X}(0) \end{bmatrix}$$
(14)
$$\hat{U}(0)$$

$$P(0) = \begin{bmatrix} P_{x}(0) & P_{xu}(0) \\ P_{xu}^{T}(0) & P_{u}(0) \end{bmatrix}$$
(15)

A description of the variables and their dimensions for the augmented system are given in Table 2.

TABLE 2

SYSTEM VARIABLES FOR THE AUGMENTED SYSTEM

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| VARIABLE | DEFINITION | DIMENSION |
|---------------------|-------------------------------------|---------------|
| | | |
| X(k) | State vector (augmented) | (n+p) x1 |
| ¢ (k+1,k) | State transition matrix | (n+p) x (n+p) |
| ſ _a (k) | System noise coefficient matrix | (n+p) xr |
| Q(k) | System noise covariance matrix | rxr |
| Δxq | Jump in state at time q | (n+p) x1 |
| z (k) | Measurement at time k | mx1 |
| H _a (k) | Measurement matrix | mx (n+p) |
| R(k) | Measurement noise covariance matrix | mxm |
| w (k) | Gaussian white system noise | rxl |
| υ (k) | Gaussian white measurement noise | mxl |
| Âx (0) | Mean value of X(0) | (n+p) x1 |
| P(0) | Covariance of X(0) | (n+p) x (n+p) |
| D | Jump coefficient matrix | (n+p) xp |
| Δuq | Jump in control at time q | pxl |
| Δ u (q) | Mean value of Δu_q | pxl |
| P _{Au} (q) | Covariance of Δu_q | pxp |

We let Z(j) denote the sequence of measurements from time 1 to time j:

$$Z(j) = \{ z(1), z(2), ..., z(j) \}$$

Our problem is that of obtaining the optimum estimates of x, u, Δu_q and q without using augmented state filters.

3. EQUIVALENT FILTERING: UNAUGMENTED AND AUGMENTED

In this section we address the nonjump system:

System Dynamics

$$x(k+1) = A(k+1,k) x(k) + B(k+1,k) u(k) + \Gamma(k)w(k)$$
(16)

$$u(k+1) = u(k)$$
 (17)

Measurement Equation

$$z(k) = H(k) x(k) + v(k)$$
 (18)

We are given the initial means $\hat{x}(0)$ and $\hat{u}(0)$ and the initial covariances $P_x(0)$, $P_{xu}(0)$ and $P_u(0)$. It is customary to augment the state x with the control vector u (the control u serves as a bias state vector) and then apply the Kalman-Bucy filter to the augmented system. One obtains the optimal estimates $\hat{X}(k)$ and P(k). The Kalman-Bucy filter equations [24] - [28] are given in Table 3 for the augmented system. The filter variables are described in Table 4.

TABLE 3

DISCRETE KALMAN-BUCY FILTER EQUATIONS FOR AUGMENTED SYSTEM

1

$$X(k+1,k) = \Phi(k+1,k) X(k)$$
 (i)*

$$P(k+1|k) = \Phi(k+1,k) P(k) \Phi^{T}(k+1,k) + \Gamma_{a}(k)Q(k) \Gamma_{a}^{T}(k)$$
(ii)

 $\gamma_{a}(k) = z(k) - H_{a}(k) \hat{X}(k|k-1)$ (iii)

$$V_{a}(k) = H_{a}(k) P(k|k-1) H_{a}^{T}(k) + R(k)$$
 (iv)

$$K_{a}(k) = P(k|k-1) H_{a}^{T}(k) V_{a}^{-1}(k)$$
 (v)

$$X(k) = X(k|k-1) + K_{a}(k) Y_{a}(k)$$
 (vi)

$$P(k) = [I-K_{a}(k) H_{a}(k)] P(k|k-1)$$
 (vii)

*The usual notations \hat{X} (k|k) and P (k|k) have been shortened to $\hat{X}(k)$ and P(k).

TABLE 4

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FILTER VARIABLES FOR AUGMENTED SYSTEM

| VARIABLE | DEFINITION | DIMENSION |
|--------------------|--|-----------------|
| ^ | | |
| X(k) | State estimate at k given Z(k) | (n+p) x1 |
| P(k) | Covariance matrix of the error in $\hat{X}(k)$ | (n+p) x (n+p) |
| ^ X(k+1 k) | State estimate at k+1 given Z(k) | (n+p) x1 |
| P (k+1 k) | Covariance matrix of the error . in $\hat{X}(k+1 k)$ | (n+p) x (n+p) |
| Ya ^(k) | Predicted measurement residual | mxl |
| V _a (k) | Covariance of $\gamma_a(k)$ | mxm |
| K _a (k) | Filter (Kalman) gain matrix at k | (n+p) xm |

Friedland [21] has shown that it is unnecessary to augment the state vector x by adding additional components (e.g., bias vector such as the control u) in order to obtain the optimal estimates \hat{x} and \hat{u} . He showed that the optimum estimates could be obtained by employing two Kalman-Bucy filters: a "bias-free" unaugmented filter and a bias filter. In particular, he showed that the optimum estimate \hat{x} of the state could be expressed as $\hat{x} = \tilde{x} + S\hat{u}$ where \tilde{x} is the output of the "bias-free" unaugmented filter and \hat{u} is the output of the $\frac{1}{2} \frac{1}{2} \frac{1$

The purpose of this section is to show that Friedland's unaugmented filtering technique [21] holds for the case when there is correlation between the state x and the control vector u, i.e.,

 $P_{yy}(0) \neq 0 \tag{19}$

We make the following definitions

And Andrews Contraction

$$S_0 = P_{xu}(0) P_u^{-1}(0)$$
 (20)

$$\tilde{x}_{0} = \hat{x}(0) - s_{0}\hat{u}(0)$$
 (21)

^{*}Ignagni [29] has rederived Friedland's two-stage estimator in which he assumed at the outset that x and u are initially correlated by means of a given form. We show here that it is unnecessary to assume the given form.

$$\tilde{P}_{x}(0) = P_{x}(0) - S_{0} P_{u}(0) S_{0}^{T}$$
(22)

$$\tilde{u}_0 = \hat{u}(0) \tag{23}$$

$$\tilde{P}_{u}(0) = P_{u}(0)$$
 (24)

In view of (20) - (24) the initial values x(0), u(0) and P(0) have the form

$$\hat{x}(0) = \hat{x}_0 + s_0 \tilde{u}_0$$
 (25)

$$\hat{u}(0) = \hat{u}_0$$
 (26)

$$P(0) = \begin{bmatrix} \tilde{P}_{x}(0) + S_{0}\tilde{P}_{u}(0)S_{0}^{T} & S_{0}\tilde{P}_{u}(0) \\ \tilde{P}_{u}(0)S_{0}^{T} & \tilde{P}_{u}(0) \end{bmatrix}$$
(27)

We call the above form the Friedland form. Friedland [21] showed under the condition

$$P_{xu}(0) = 0$$
 (28)

that the optimal estimates $\hat{x}(k)$, $\hat{u}(k)$ and P(k) of the augmented system satisfy

$$\hat{x}(k) = \hat{x}(k) + S(k) \hat{u}(k)$$
 (29)
 $\hat{u}(k) = \hat{u}(k)$ (30)

$$P(k) = \begin{bmatrix} \widetilde{P}_{x}(k) + S(k) \ \widetilde{P}_{u}(k) \ S^{T}(k) \\ \widetilde{P}_{u}(k) \ S^{T}(k) \end{bmatrix}$$
(31)

where $\tilde{x}(k)$, $\tilde{P}_{x}(k)$ and S(k) are output of a "bias-free" unaugmented filter and where $\tilde{u}(k)$ and $\tilde{P}_{u}(k)$ are output of a bias filter. We are to show that the Friedland form (29) - (31) holds under condition (19).

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We treat the non-jump system (16) - (18) as a jump process at time zero in the following manner. At time zero before the jump we assume that the augmented system has the following initial state, mean and covariance

$$X_{0} = \begin{bmatrix} x(0) - S_{0} & u(0) \\ 0 \end{bmatrix}$$
(32)

$$\hat{\mathbf{x}}_0 = \begin{bmatrix} \mathbf{x}_0 \\ \mathbf{0} \end{bmatrix}$$
(33)

 $P_{1}(0) = \begin{bmatrix} \tilde{P}_{x}(0) & 0 \\ 0 & 0 \end{bmatrix}$ (34)

Eqs. (32) - (34) imply that the control u is known to be zero before the jump.

We assume that a jump ΔX_0 occurs at time 0⁺ in the augmented state

$$\Delta X_0 = \begin{bmatrix} S_0 \\ I \end{bmatrix} u(0)$$
(35)

where u(0) has mean u_0 and covariance $P_u(0)$ and is independent of \tilde{x}_0 . The covariance $\Delta P(0)$ of ΔX_0 is given by

$$\Delta P(0) = \begin{bmatrix} S_0 & P_u(0) & S_0^T & S_0 & P_u(0) \\ P_u(0) & S_0^T & P_u(0) \end{bmatrix}$$
(36)

The mean value of ΔX_0 is

$$\hat{\Delta x}_0 = \begin{bmatrix} s_0 \\ I \end{bmatrix} \quad \tilde{u}_0 \tag{37}$$

From Eqs. (27), (34) and (36) we note that

$$P(0) = P_1(0) + \Delta P(0)$$
(38)

From Eqs. (32) and (35) we observe that

$$\begin{array}{c} x(0) \\ x(0) = \begin{bmatrix} \\ \\ \\ u(0) \end{bmatrix} = x_0 + \Delta x_0 \tag{39}$$

From Eqs. (21), (33) and (37) we see that

$$\hat{\mathbf{x}}(0) = \begin{bmatrix} \hat{\mathbf{x}}(0) \\ \hat{\mathbf{x}}(0) \end{bmatrix} = \hat{\mathbf{x}}_{0} + \hat{\Delta}\hat{\mathbf{x}}_{0}$$
(40)

Eqs. (38) - (40) show that we have a well-defined jump process at time zero. Consequently, we can employ the results of [1] which applies to jumps in the augmented state vector.

For this purpose consider the following filtering conditions for the Kalman-Bucy filter:

- H₁: There is a jump in state and control but the filter is unaware that the jump (35) has taken place and it operates as if the jump is zero. The control u(k) is assumed to be perfectly known as a zero control. The initial conditions (32) - (34) are used.
- H₂: There is a jump in state and control, the jump (35) is known to the filter and the jump information is made use of in the filter. Before the jump, the control u is assumed to be perfectly known as zero control. The initial conditons are (34), (41) and (42).

$$\hat{x}_{2}(0) = x_{0} + S_{0}u(0)$$
 (41)

 $u_2(0) = u(0)$ (42)

The discrete Kalman-Bucy filter equations are given in Tables 5 and 6 for Conditions \tilde{H}_1 and H_2 , respectively. The Kalman gains, the state covariances and the predicted measurement covariance satisfy

$$\widetilde{K}_{\mathbf{x}}(\mathbf{k}) = K_{2}(\mathbf{k}) \tag{43}$$

$$P_{x}(k) = P_{2}(k)$$
 (44)

$$\tilde{P}_{x}(k+1|k) = P_{2}(k+1|k)$$
(45)

$$V_{\mathbf{x}}(\mathbf{k}) = V_{2}(\mathbf{k}) \tag{46}$$

We make the definitions

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$$\Delta A(k+1,k) = [I-K_{x}(k+1)H(k+1)]A(k+1,k)$$
(47)

$$\Delta B(k+1,k) = [I-K_{x}(k+1)H(k+1)]B(k+1,k)$$
(48)

In view of (43) it follows from Tables 5 and 6 that

$$\tilde{x}_{1}(k+1) = \Delta A(k+1,k) \tilde{x}_{1}(k) + \tilde{K}_{x}(k+1) z(k+1)$$
 (49)

$$\hat{x}_{2}(k+1) = \Delta A(k+1,k) \hat{x}_{2}(k) + \Delta B(k+1,k) u(0) + \tilde{K}_{x}(k+1) z(k+1)$$
(50)

TABLE 5

DISCRETE KALMAN-BUCY FILTER EQUATIONS FOR CONDITION \tilde{H}_1

$$\widetilde{P}_{x}(k+1|k) = A(k+1,k)x_{1}(k)$$
(i)*

$$\widetilde{P}_{x}(k+1|k) = A(k+1,k)\widetilde{P}_{x}(k) A^{T}(k+1,k) + \Gamma(k) Q(k)\Gamma^{T}(k)$$
(ii)

$$Y_{1}(k) = z(k) - H(k) x_{1}(k|k-1)$$
 (iii

$$V_{x}(k) = H(k) P_{x}(k|k-1)H^{T}(k) + R(k)$$
 (iv)

$$K_{x}(k) = P_{x}(k|k-1) H^{T}(k) V_{x}^{-1}(k)$$
(v)

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$$x_{1}^{(k)} = x_{1}^{(k|k-1)} + K_{x}^{(k)} \gamma_{1}^{(k)}$$
(vi)

$$P_{x}(k) = [I - K_{x}(k) H(k)] P_{x}(k|k-1)$$
(vii)

$$\Delta z_{1}(k) = z(k) - H(k) x_{1}(k)$$
(viii)
 $\tilde{x}_{1}(0) = \tilde{x}_{0}$ (ix)

$$\tilde{P}_{x}(0) = P_{x}(0) - S_{0} P_{u}(0) S_{0}^{T}$$
 (x)

*The usual notations
$$\tilde{x}_1(k|k)$$
 and $\tilde{P}_x(k|k)$ have been shortened
to $\tilde{x}_1(k)$ and $\tilde{P}_x(k)$.

TABLE 6

DISCRETE KALMAN-BUCY FILTER EQUATIONS* FOR CONDITION H_2

$$x_{2}(k+1|k) = A(k+1,k) x_{2}(k) + B(k+1,k) u(k)$$
 (i)*

$$P_{2}(k+1|k) = A(k+1,k) P_{2}(k) A(k+1,k) + I(k) Q(k)I(k)$$
(11)

$$\gamma_2(k) = z(k) - H(k) x_2(k|k-1)$$
 (11)

$$V_2(k) = H(k) P_2(k|k-1) H^T(k) + R(k)$$
 (iv)

$$K_{2}(k) = P_{2}(k|k-1) H^{T}(k) V_{2}^{-1}(k)$$
(v)

$$x_{2}(k) = x_{2}(k|k-1) + K_{2}(k) \gamma_{2}(k)$$
 (vi)

$$P_{2}(k) = [I - K_{2}(k) H(k)] P_{2}(k|k-1)$$
 (vii)

$$\Delta z_{2}(k) = z(k) - H(k) x_{2}(k)$$
 (viii)

$$x_2(0) = x_0 + S_0 u(0)$$
 (ix)

$$P_2(0) = P_x(0) - S_0 P_u(0) S_0^T$$
(x)

$$u(k) = u(0) \tag{xi}$$

*The usual notations $\hat{x}_2(k|k)$ and $P_2(k|k)$ have been shortened to $\hat{x}_2(k)$ and $P_2(k)$.

We define the Δ -state variable $\Delta x_1(k)$ as

$$\Delta x_{1}(k) = \hat{x}_{2}(k) - \tilde{x}_{1}(k)$$
 (51)

Subtracting (49) from (50) gives

and the second second second

$$\Delta x_{1}(k+1) = \Delta A(k+1,k) \Delta x_{1}(k) + \Delta B(k+1,k)u(0)$$
 (52)

In view of Eqs. (41) and (51) this becomes

$$\Delta x_{1}(0) = S_{0}u(0)$$
 (53)

$$\Delta x_{1}(k+1) = \Delta A(k+1,k) \Delta x_{1}(k) + \Delta B(k+1,k)u(0), k \ge 0$$
(54)

We define the S_u matrix as $S_u(k+1;0) = \Delta A(k+1,k) S_u(k;0) + \Delta B(k+1,k), k \ge 0$ (55)

$$S_u(0;0) = S_0$$
 (56)

Consequently, $\Delta x_1(k)$ satisfies

$$\Delta x_{1}(k) = S_{u}(k;0)u(k)$$
(57)

since u(k) = u(0).

The measurement equation for Δx_1 is easily derived. We define the two a posteriori measurement residuals for Conditions \tilde{H}_1 and H_2 :

$$\tilde{\Delta z_1}(k) = z(k) - H(k) \tilde{x_1}(k)$$
 (58)

$$\Delta z_2(k) = z(k) - H(k) \hat{x}_2(k)$$
 (59)

Subtracting (59) from (58) gives the measurement equation for $\Delta x^{}_{1}$

$$\widetilde{\Delta z_1}(k) = H(k) \Delta x_1(k) + \widetilde{\Delta v_1}(k)$$
(60)

where

$$\Delta v_1(k) = \Delta z_2(k)$$
(61)

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The measurement noise $\Delta v_1(k)$ is a zero-mean white Gaussian sequence with covariance defined by

$$E\{\widetilde{\Delta v_1}(k) \Delta \widetilde{v_1}^T(k)\} = R_u(k) \delta_{kj}$$
(62)

where

$$R_{u}(k) = R(k) \tilde{v}_{x}^{-1}(k) R(k)$$
 (63)

We have made use of Eq. (46) in obtaining (62).

The system equations for u(k) are

System Dynamics

$$u(k+1) = u(k) , k > 0$$
 (64)

Measurement Equation

$$\tilde{\Delta z_1}(k) = H_u(k)u(k) + \tilde{\Delta v_1}(k)$$
 (65)

where

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$$H_{1}(k) = H(k) S_{1}(k;0)$$
 (66)

Eqs. (57) and (60) give (65).

The Kalman-Bucy filtering equations for estimating u(k) are given in Table 7.

In view of (57) the augmented $\Delta X(k)$ is given by

$$\Delta X(k) = \begin{bmatrix} \Delta x_1(k) & S_u(k;0) \\ u(k) & I \end{bmatrix} u(k)$$
(67)

The estimate of $\Delta X(k)$ is

$$\hat{\Delta X}(k) = \begin{bmatrix} S_{u}(k;0) & \sim \\ 0 & 1 \end{bmatrix} u(k)$$
(68)

| TABLE | 7 | |
|-------|---|--|
| | | |

FILTERING EQUATIONS FOR ESTIMATING u(k)

| ~ ~ | |
|--|-------|
| u(k+1 k) = u(k) | (i) |
| $\widetilde{P}_{u}(k+1 k) = \widetilde{P}_{u}(k)$ | (ii) |
| $\gamma_{u}(k) = \Delta z_{1}(k) - H_{u}(k) \tilde{u}(k k-1)$ | (iii) |
| $\widetilde{V}_{u}(k) = H_{u}(k) \widetilde{P}_{u}(k k-1) H_{u}^{T}(k) + R_{u}(k)$ | (iv) |
| $\widetilde{K}_{u}(k) = \widetilde{P}_{u}(k k-1) H_{u}^{T}(k) \widetilde{V}_{u}^{-1}(k)$ | (v) |
| $\widetilde{u}(k) = \widetilde{u}(k k-1) + \widetilde{K}_{u}(k) \gamma_{u}(k)$ | (vi) |

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$$\tilde{P}_{u}(k) = [I - \tilde{K}_{u}(k) H_{u}(k)] \tilde{P}_{u}(k|k-1)$$
 (vii)

where

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| u(0) = | • u(0) | (viii | L) |
|--------|--------|-------|----|
| | | | |

$$P_{u}(0) = P_{u}(0)$$
 (ix)

$$H_{u}(k) = H(k) S_{u}(k;0)$$
 (x)

$$S_{u}(k+1;0) = \Delta A(k+1,k) S_{u}(k;0) + \Delta B(k+1,k)$$
 (xi)

$$S_{u}(0,0) = S_{0}$$
(X11)

$$\Delta A(k+1,k) = [I - K_{x}(k+1) + I(k+1)] + A(k+1,k)$$
(X11)
(X11)

$$\Delta B(k+1,k) = [I - K_{x}(k+1) H(k+1)] B(k+1,k)$$
(xiv)

$$\tilde{R}_{u}(k) = R(k) \tilde{V}_{x}^{-1}(k) R(k)$$
(xv)

$$\widetilde{\Delta z}_{1}(k) = z(k) - H(k) \widetilde{x}_{1}(k)$$
 (xvi)

The covariance of $\widetilde{\Delta X}(\mathbf{k})$ is

$$\Delta P(k) = \begin{bmatrix} S_{u}(k;0) & \widetilde{P}_{u}(k) & S_{u}^{T}(k;0) & S_{u}(k;0) & \widetilde{P}_{u}(k) \\ & \widetilde{P}_{u}(k) & S_{u}^{T}(k;0) & & \widetilde{P}_{u}(k) \end{bmatrix}$$
(69)

where $\tilde{u}(k)$ and $\tilde{P}_{u}(k)$ are given by the filter of Table 7.

In view of Eqs. (33) and (34) and the filter of Table 5 the augmented $\tilde{X}_1(k)$ satisfies

$$\tilde{x}_{1}(k) = \begin{bmatrix} \tilde{x}_{1}(k) \\ 0 \end{bmatrix}$$
 (70)

and has covariance

$$P_{1}(k) = \begin{bmatrix} P_{x}(k) & 0 \\ 0 & 0 \end{bmatrix}$$
(71)

The optimal estimates $\hat{X}(k)$ and P(k) follow from the Kalman-Bucy filter of Table 3 for the augmented system:

$$\hat{\mathbf{x}} (\mathbf{k}) = \begin{bmatrix} \hat{\mathbf{x}} (\mathbf{k}) \\ [\hat{\mathbf{x}}] \\ u (\mathbf{k}) \end{bmatrix}$$
(72)

$$P(k) = \begin{bmatrix} P_{x}(k) & P_{xu}(k) \\ P_{xu}^{T}(k) & P_{u}(k) \end{bmatrix}$$
(73)

It is shown in [1] that the following identities hold: $\hat{X}(k) = \hat{X}_{1}(k) + \hat{\Delta X}(k)$ (74)

$$P(k) = P_{1}(k) + \Delta P(k)$$
(75)

Consequently, Eqs. (74) and (75) verify that the Friedland form (29) - (31) holds under the condition that there is correlation initially between the state x and the control vector u, i.e., Eq. (19) holds.

It is also shown in [1] that the gains are related by the expression

$$K_{a}(k) = \tilde{K}_{1}(k) + \Delta K(k) [I - H_{a}(k) \tilde{K}_{1}(k)]$$
 (76)

where

$$\widetilde{K}_{1}(k) = \begin{bmatrix} \widetilde{K}_{x}(k) \\ 0 \end{bmatrix}$$
(77)

$$\Delta K(\mathbf{k}) = \begin{bmatrix} S_{\mathbf{u}}(\mathbf{k};0) & \widetilde{K}_{\mathbf{u}}(\mathbf{k}) \\ & \widetilde{K}_{\mathbf{u}}(\mathbf{k}) \end{bmatrix}$$
(78)

Eq. (78) follows from Eq. (vi) of Table 7, Eqs. (57) and (67). Eq. (77) follows from Eq. (70) and Eq. (vi) of Table 5. We define

$$K_{a}(k) = \begin{bmatrix} K_{x}(k) \\ K_{u}(k) \end{bmatrix}$$
 (79)

Using (76) - (78) we obtain

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$$K_{x}(k) = \tilde{K}_{x}(k) + S_{u}(k;0) \tilde{K}_{u}(k) [I - H(k) \tilde{K}_{x}(k)]$$
 (80)

$$K_{u}(k) = 0 + \tilde{K}_{u}(k) [I - H(k) \tilde{K}_{x}(k)]$$
 (81)

It follows from Eqs. (68) - (75) that

$$\hat{x}(k) = \tilde{x}_{1}(k) + S_{u}(k;0)\tilde{u}(k)$$
 (82)

$$\hat{\mathbf{u}}(\mathbf{k}) = \tilde{\mathbf{u}}(\mathbf{k}) \tag{83}$$

$$P_{x}(k) = \tilde{P}_{x}(k) + S_{u}(k;0) \tilde{P}_{u}(k) S_{u}^{T}(k;0)$$
 (84)

$$P_{xu}(k) = S_{u}(k;0) \tilde{P}_{u}(k)$$
 (85)

$$P_{u}(k) = \tilde{P}_{u}(k)$$
(86)

We show now that the predicted measurement residual covariances are related by

$$V_{a}(k) = \tilde{V}_{x}(k) R^{-1}(k) \tilde{V}_{u}(k) R^{-1}(k) \tilde{V}_{x}(k)$$
 (87)

It is shown in [1] that the augmented matrices $V_a(k)$, $\tilde{V}_1(k)$ and $\Delta V(k)$ are related by

$$V_{a}(k) = \tilde{V}_{1}(k) R^{-1}(k) \Delta V(k) R^{-1}(k) \tilde{V}_{1}(k)$$
 (88)

where

$$\Delta V(k) = H_{a}(k) \Delta P(k|k-1) H_{a}^{T}(k) + R(k) \widetilde{V}_{1}^{-1}(k) R(k)$$
(89)

$$\tilde{V}_{1}(k) = H_{a}(k) P_{1}(k|k-1) H_{a}^{T}(k) + R(k)$$
 (90)

Since

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$$H_{a}(k) \Delta P(k|k-1)H_{a}^{T}(k) = H_{u}(k) \widetilde{P}_{u}(k|k-1)H_{u}^{T}(k)$$
(91)

$$H_{a}(k) P_{1}(k|k-1)H_{a}^{T}(k) = H(k) \widetilde{P}_{x}(k|k-1)H^{T}(k)$$

It follows that

$$\widetilde{\mathbf{V}}_{\mathbf{x}}(\mathbf{k}) = \widetilde{\mathbf{V}}_{\mathbf{1}}(\mathbf{k})$$
(92)

$$\widetilde{V}_{u}(k) = \Delta V(k)$$
(93)

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4. OPTIMAL FILTERING OF UNAUGMENTED JUMP PROCESSES: REINITIALIZATION AT JUMP

We address the jump process described by Eqs. (1) - (3). A jump in the control variable occurs at time q. The jump Δu_q is normally distributed with mean $\Delta u(q)$ and covariance $P_{\Delta u}(q)$. We assume the jump is independent of all other processes. In this section we assumed that the jump time q is known. We use the time q to denote the time before the jump and we use q^+ to denote the time just after the jump.

Before the jump the augmented estimates X(q) and P(q) satisfy

$$\hat{x}(q) = \tilde{x}_1(q) + S_u(q;0) \tilde{u}(q)$$
 (94)

$$\mathbf{u}\left(\mathbf{q}\right) = \mathbf{u}\left(\mathbf{q}\right) \tag{95}$$

$$P_{x}(q) = \tilde{P}_{x}(q) + S_{u}(q;0) \tilde{P}_{u}(q) S_{u}^{T}(q;0)$$
 (96)

$$P_{xu}(q) = S_u(q;0) \tilde{P}_u(q)$$
 (97)

$$P_{u}(q) = \widetilde{P}_{u}(q)$$
(98)

After the jump they satisfy

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$$\hat{X}(q^+) = \hat{X}(q) + \hat{\Delta X}(q)$$
 (99)

$$P(q^{\dagger}) = P(q) + \Delta P(q)$$
(100)

where

$$\hat{\Delta X}(q) = \begin{bmatrix} 0 \\ \Delta u(q) \end{bmatrix}$$
(101)

$$\Delta P(q) = \begin{bmatrix} 0 & 0 \\ 0 & P_{\Delta u}(q) \end{bmatrix}$$
(102)

Therefore, after the jump we have for the augmented system

$$\hat{x}(q^{+}) = \hat{x}(q)$$
 (103)

$$\hat{u}(q^+) = \hat{u}(q) + \hat{\Delta u}(q)$$
 (104)

$$P_{x}(q^{+}) = P_{x}(q)$$
 (105)

$$P_{xu}(q^+) = P_{xu}(q)$$
 (106)

$$P_{u}(q^{+}) = P_{u}(q) + P_{\Delta u}(q)$$
(107)

In order to utilize the unaugmented filtering technique we need to put Eqs. (103) - (107) into the Friedland form (25) - (27). We make use of the reinitialization equations (20) - (24) of the unaugmented filters. Consequently, we make the definitions

$$S_q = P_{xu}(q^+) P_u^{-1}(q^+)$$
 (108)

$$\tilde{x}_{1}(q^{+}) = \hat{x}(q^{+}) - S_{q}\hat{u}(q^{+})$$
 (109)

$$\tilde{P}_{x}(q^{+}) = P_{x}(q^{+}) - S_{q}P_{u}(q^{+})S_{q}^{T}$$
 (110)

$$\tilde{u}(q^+) = \hat{u}(q^+)$$
 (111)

$$\tilde{P}_{u}(q^{+}) = P_{u}(q^{+})$$
 (112)

The initial conditions (108) - (112) ensure that we have the Friedland form

$$\hat{\mathbf{x}}(q^+) = \tilde{\mathbf{x}}_1(q^+) + S_q \tilde{\mathbf{u}}(q^+)$$
 (113)

$$\hat{u}(q^{+}) = \tilde{u}(q^{+})$$
 (114)

$$\widetilde{P}_{\mathbf{x}}(q^{\dagger}) + S_{\mathbf{q}} \widetilde{P}_{\mathbf{u}}(q^{\dagger}) S_{\mathbf{q}}^{\mathbf{T}} \qquad S_{\mathbf{q}} \widetilde{P}_{\mathbf{u}}(q^{\dagger})$$

$$P(q^{\dagger}) = \begin{bmatrix} \widetilde{P}_{\mathbf{u}}(q^{\dagger}) S_{\mathbf{q}}^{\mathbf{T}} & \widetilde{P}_{\mathbf{u}}(q^{\dagger}) \end{bmatrix}$$
(115)

In view of Eqs. (94) - (98) and (103) - (107) we can rewrite Eqs. (108) - (112) as follows

$$S_{q} = S_{u}(q;0) \widetilde{P}_{u}(q) [\widetilde{P}_{u}(q) + P_{\Delta u}(q)]^{-1}$$
 (116)

$$\tilde{x}_{1}(q^{+}) = \tilde{x}_{1}(q) + S_{u}(q;0) \tilde{u}(q) - S_{q}[\tilde{u}(q) + \Delta u(q)]$$
 (117)

$$\widetilde{u}(q^{\dagger}) = \widetilde{u}(q) + \widehat{\Delta u}(q)$$
(118)

$$\widetilde{P}_{\mathbf{x}}(q^{+}) = \widetilde{P}_{\mathbf{x}}(q) + S_{\mathbf{u}}(q;0)\widetilde{P}_{\mathbf{u}}(q)S_{\mathbf{u}}^{T}(q;0) - S_{q}[\widetilde{P}_{\mathbf{u}}(q) + P_{\Delta \mathbf{u}}(q)] S_{q}^{T}$$
(119)

$$\widetilde{P}_{u}(q^{+}) = \widetilde{P}_{u}(q) + P_{\Delta u}(q)$$
(120)

Note that

$$S_{q} [\tilde{P}_{u}(q) + P_{\Delta u}(q)] = S_{u}(q;0) \tilde{P}_{u}(q)$$
 (121)

$$\mathbf{S}_{\mathbf{q}} \tilde{\mathbf{P}}_{\mathbf{u}}(\mathbf{q}) \; \mathbf{S}_{\mathbf{u}}^{\mathbf{T}}(\mathbf{q}; 0) = \mathbf{S}_{\mathbf{u}}(\mathbf{q}; 0) \; \tilde{\mathbf{P}}_{\mathbf{u}}(\mathbf{q}) \; \mathbf{S}_{\mathbf{q}}^{\mathbf{T}}$$
(122)

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Eqs. (121) and (122) are used in showing that $\tilde{P}_{x}(q^{+})$ as defined by Eq. (119) is the covariance of $\tilde{x}_{1}(q^{+})$ as defined by Eq. (117).

Eqs. (116) - (120) are the equations for reinitializing the unaugmented filters defined by the equations in Tables 5 and 7. Equations (x) - (xii) of Table 7 are replaced with the following:

$$H_{ij}(k) = H(k) S_{ij}(k;q)$$
 (123)

$$S_{ij}(k+1);q) = \Delta A(k+1,k) S_{ij}(k;1) + \Delta B(k+1,k)$$
 (124)

$$S_{u}(q;q) = S_{q}$$
(125)

5. OPTIMAL FILTERING OF UNAUGMENTED JUMP PROCESSES: REINITIALIZATION BEYOND JUMP

We continue to address the jump process described by Eqs. (1) - (3). In this section we make the same assumptions as those given in the first paragraph of the previous section. Herein, we develop the equations for the optimal estimates in terms of the unaugmented estimates for the case that we do not reinitialize the unaugmented filters at the jump time. Rather, we initialize at some time k* beyond the jump time q.

Consider the following conditions for the Kalman-Bucy filter of the augmented system:

- H₁: There is a jump in control but the filter is unaware that the jump (10) has taken place and it operates as if the jump at time q is zero. The initial conditions immediately after the jump are (126) and (127). That is, it uses the same estimates immediately after the jump as it had just before the jump.
- H₂: There is a jump in control, the jump (10) is known to the filter and the jump information is made use of in the filter. The initial conditions immediately after the jump are (128) and (129).

$$\tilde{X}_{1}(q^{+}) = \hat{X}(q)$$
 (126)

$$P_1(q^+) = P(q)$$
 (127)

$$\hat{x}_{2}(q^{+}) = \hat{x}(q) + \Delta x_{q}$$
 (128)

$$P_2(q^+) = P(q)$$
 (129)

It is shown in [1] that after the jump the optimal estimates $\hat{X}(k)$ and P(k) are given by

$$\hat{\mathbf{X}}(\mathbf{k}) = \mathbf{X}_{1}(\mathbf{k}) + \mathbf{A}\mathbf{X}(\mathbf{k})$$
(130)

$$P(k) = P_1(k) + \Delta P(k)$$
 (131)

where $\Delta X(k)$ and $\Delta P(k)$ are the output of a Kalman-Bucy filter having the initial conditions

$$\Delta X(q) = \Delta X_{q}$$
(132)

$$\Delta P(q) = \begin{bmatrix} 0 & 0 \\ 0 & P_{AU}(q) \end{bmatrix}$$
(133)

Therein, the Δ -state $\Delta X(k)$ is defined as

$$\Delta X(k) = \hat{X}_{2}(k) - \tilde{X}_{1}(k)$$
(134)

It satisfies the Δ -state equation

$$\Delta X(k) = \Delta \varphi (k, k-1) \quad \Delta X(k-1) \tag{135}$$

where

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$$\Delta \phi (k, k-1) = [I - K_1(k) H_k(k)] \phi (k, k-1)$$
(136)

The matrix H_a is defined by Eq. (12). The Kalman gain K_1 is that which is given by the filter operating under Condition H_1 . From Eqs. (80) and (81) we see that K_1 can be expressed in terms of the unaugmented gains \tilde{K}_x and \tilde{K}_u :

$$K_{1}(k) = \begin{bmatrix} K_{1x}(k) \\ K_{1u}(k) \end{bmatrix}$$
(137)

where

$$K_{1x}(k) = K_{x}(k) + S_{u}(k;0) K_{1u}(k)$$
 (138)

$$K_{1u}(k) = \tilde{K}_{u}(k) [I - H(k) \tilde{K}_{x}(k)]$$
 (139)

The augmented state ΔX in terms of the unaugmented states is given by

$$\Delta X(k) = \begin{bmatrix} \Delta x(k) \\ 0 \end{bmatrix}$$
(140)

We have the initial conditions

$$\Delta \mathbf{x}(\mathbf{q}) = \mathbf{0} \tag{141}$$

$$\Delta u(q) = \Delta u_{q} \tag{142}$$

We define the nxp matrix S_x and the pxp matrix $S_{\Delta u}$ as follows $S_x(k+1;q) = \Delta A_1(k+1,k) S_x(k;q) + \Delta B_1(k+1,k) S_{\Delta u}(k;q)$ (143) $S_{\Delta u}(k+1;q) = \Delta A_2(k+1,k) S_x(k;q) + \Delta B_2(k+1,k) S_{\Delta u}(k;q)$ (144) $S_x(q;q) = 0$ (145)

$$S_{\Delta U}(q;q) = I \tag{146}$$

where

$$\Delta A_{1}(k,k-1) = [I - \tilde{K}_{x}(k)H(k) - S_{u}(k;0)K_{1u}(k)H(k)] A(k,k-1) (147)$$

$$\Delta B_{1}(k,k-1) = [I - \tilde{K}_{x}(k)H(k) - S_{u}(k;0) K_{1u}(k)H(k)] B(k,k-1) (148)$$

$$\Delta A_{2}(k,k-1) = -K_{1u}(k) H(k) A(k,k-1)$$
(149)

$$\Delta B_{2}(k,k-1) = [I - K_{1u}(k) H(k) B(k,k-1)]$$
(150)

Using Eqs. (135) - (150) one can verify that

$$\Delta x(k) = S_{x}(k;q)\Delta u_{q}$$
(151)

$$\Delta u(\mathbf{k}) = S_{\Delta u}(\mathbf{k}; \mathbf{q}) \Delta u_{\mathbf{q}}$$
(152)

The measurement equation for $\Delta X(k)$ is shown in [1] to be

$$\Delta z(k) = H_{a}(k) \Delta X(k) + \Delta u(k)$$
(153)

where

$$\Delta z(k) = z(k) - H_a(k) \tilde{X}_1(k)$$
 (154)

$$\Delta \upsilon (k) = z(k) - H_{a}(k) \hat{X}_{2}(k)$$
 (155)

Note that Δv is the a posteriori measurement residual under Condition H₂. It follows that Δv (k) is a zero mean white Gaussian sequence with covariance defined by

$$E \{ \Delta \upsilon (k) \Delta \upsilon^{T}(j) \} = \Delta R(k) \delta_{kj}$$
(156)

where

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$$\Delta R(k) = R(k) V_2^{-1}(k) R(k)$$
 (157)

The matrix $V_2(k)$ is the predicted measurement residual covariance under Condition H₂. From Eq. (87) we see that V_2 can be expressed as a function of \tilde{V}_x and \tilde{V}_u :

$$V_{2}(k) = \tilde{V}_{x}(k)R^{-1}(k)\tilde{V}_{u}(k)R^{-1}(k)\tilde{V}_{x}(k)$$
 (158)

Consequently, $\Delta R(k)$ is given by

$$\Delta R(k) = R(k) \tilde{V}_{x}^{-1}(k) R(k) \tilde{V}_{u}^{-1}(k) R(k) \tilde{V}_{x}^{-1}(k) R(k)$$
(159)

Using Eqs. (82) - (83) we see that $\tilde{X}_1(k)$ is given by

$$\widetilde{X}_{1}(k) = \begin{bmatrix} \widetilde{X}_{1}(k) + S_{u}(k;0) & \widetilde{u}(k) \\ \widetilde{u}(k) \end{bmatrix}$$
(160)

Consequently, Eq. (154) can be rewritten as

$$\Delta z(k) = z(k) - H(k) [\tilde{x}_{1}(k) + S_{u}(k;0)\tilde{u}(k)]$$
(161)

In view of Eqs. (12) and (140) we can rewrite (153) as

$$\Delta z(k) = H(k) \Delta x(k) + \Delta v(k)$$
(162)

Substituting (151) into (162) gives the measurement equation for $\Delta u^{}_{\alpha}$

$$\Delta z(k) = H(k) S_{x}(k;q) \Delta u_{\alpha}(k) + \Delta \upsilon(k)$$
(163)

where $\Delta u_{q}(k)$ satisfies the constant state equation

$$\Delta u_{q}(k) = \Delta u_{q}(k-1) = \Delta u_{q}$$
(164)

The filtering equations for estimating Δu_q are given in Table 8.

The optimal estimates $\hat{X}(k)$ and P(k) are given by Eqs. (130) and (131)

$$\hat{X}(k) = \tilde{X}_{1}(k) + \hat{\Delta X}(k)$$
 (165)

$$P(k) = P_1(k) + \Delta P(k)$$
 (166)

where

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$$\hat{\Delta X}(\mathbf{k}) = \begin{bmatrix} \hat{\Delta X}(\mathbf{k}) \\ \hat{\Delta U}(\mathbf{x}) \end{bmatrix}$$
(167)

$$\hat{\Delta \mathbf{x}}(\mathbf{k}) = \mathbf{S}_{\mathbf{x}}(\mathbf{k};\mathbf{q}) \quad \tilde{\Delta \mathbf{u}}_{\mathbf{q}}(\mathbf{k})$$
(168)

$$\hat{\Delta u}(k) = S_{\Delta u}(k;q) \quad \tilde{\Delta u}_{q}(k)$$
(169)

$$\Delta P(\mathbf{k}) = \begin{bmatrix} S_{\mathbf{x}}(\mathbf{k};\mathbf{q}) & \widetilde{P}_{\mathbf{u}}(\mathbf{k}) & S_{\mathbf{x}}^{\mathbf{T}}(\mathbf{k};\mathbf{q}) & S_{\mathbf{x}}(\mathbf{k};\mathbf{q}) & \widetilde{P}_{\Delta \mathbf{u}}(\mathbf{k}) & S_{\Delta \mathbf{u}}^{\mathbf{T}}(\mathbf{k};\mathbf{q}) \\ S_{\Delta \mathbf{u}}(\mathbf{k};\mathbf{q}) & \widetilde{P}_{\Delta \mathbf{u}}(\mathbf{k}) & S_{\mathbf{x}}^{\mathbf{T}}(\mathbf{k};\mathbf{q}) & S_{\Delta \mathbf{u}}(\mathbf{k};\mathbf{q}) & \widetilde{P}_{\Delta \mathbf{u}}(\mathbf{k}) & S_{\Delta \mathbf{u}}^{\mathbf{T}}(\mathbf{k};\mathbf{q}) \end{bmatrix}$$

$$(170)$$

$$P_{1}(k) = \begin{bmatrix} P_{1x}(k) & P_{1xu}(k) \\ P_{1xu}^{T}(k) & P_{1u}(k) \end{bmatrix}$$
(171)

$$P_{1x}(k) = \tilde{P}_{x}(k) + S_{u}(k;0) \tilde{P}_{u}(k) S_{u}^{T}(k;0)$$
(172)

$$P_{1xu}(k) = S_u(k;0) \widetilde{P}_u(k)$$
 (173)

$$P_{1u}(k) = \tilde{P}_{u}(k)$$
(174)

Using Eqs. (160), (165) - (174) we have the optimal estimates

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$$\tilde{x}(k) = \tilde{x}_{1}(k) + S_{u}(k;0)\tilde{u}(k) + S_{x}(k;q)\tilde{\Delta u}_{q}(k)$$
 (175)

$$\widehat{u}(k) = \widetilde{u}(k) + S_{\Delta u}(k;q) \widetilde{\Delta u}_{q}(k)$$
(176)

$$P_{x}(k) = \tilde{P}_{x}(k) + S_{u}(k;0)\tilde{P}_{u}(k) S_{u}^{T}(k;0) + S_{x}(k;q)$$
$$\tilde{P}_{\Delta u}(k) S_{x}^{T}(k;q)$$
(177)

$$P_{xu}(k) = S_{u}(k;0)\tilde{P}_{u}(k) + S_{x}(k;q)\tilde{P}_{\Delta u}(k) S_{\Delta u}^{T}(k;q)$$
(178)

$$P_{u}(k) = \widetilde{P}_{u}(k) + S_{\Delta u}(k;q) \widetilde{P}_{\Delta u}(k) S_{\Delta u}^{T}(k;q)$$
(179)

Eqs. (175) - (179) give the optimal estimates in terms of the unaugmented filter estimates described by the filters of Tables 5, 7 and 8. At some time k* beyond the jump we desire to reinitialize the filters of Tables 5 and 7. This is more efficient than operating the three filters of Tables 5, 7 and 8.

We make the following definitions with k=k*:

$$S_{k*} = P_{xu}(k) P_{u}^{-1}(k)$$
 (180)

$$\tilde{x}_{1}(k^{+}) = \hat{x}(k) - S_{k^{+}}\hat{u}(k)$$
 (181)

$$\tilde{P}_{x}(k^{+}) = P_{x}(k) - S_{k^{*}}P_{u}(k) S_{k^{*}}^{T}$$
 (182)

$$u(k^{+}) = \hat{u}(k)$$
 (183)

$$\widetilde{P}_{u}(k^{+}) = P_{u}(k)$$
(184)

The argument k^+ refers to values just after the reinitialization at k=k*. Eqs. (180) - (184) are the equations for reinitializing the unaugmented filters of Tables 5 and 7. Equations (x) - (xii) of Table 7 are replaced with the following (the time k* represents the time of reinitialization):

$$H_{11}(k) = H(k) S_{11}(k;k^*), k \ge k^*$$
 (185)

$$S_{ij}(k+1;k^{*}) = \Delta A(k+1,k) S_{ij}(k;k^{*}) + \Delta B(k+1,k), k \ge k^{*}$$
 (186)

$$S_{u}(k^{*};k^{*}) = S_{k}^{*}$$
 (187)

Using the expression derived in [1]

$$K(k) = K_{1}(k) + \Delta K(k) [I - H_{n}(k) K_{1}(k)]$$
(188)

The optimal Kalman gain K(k) is given by

$$K_{x}(k) = K_{1x}(k) + \Delta K_{x}(k) [I - H(k) K_{1x}(k)]$$
 (189)

$$K_{u}(k) = K_{1u}(k) + \Delta K_{u}(k) [I - H(k) K_{1x}(k)]$$
 (190)

where

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$$K_{1x}(k) = \tilde{K}_{x}(k) + S_{u}(k;0) K_{1u}(k)$$
 (191)

$$K_{1u}(k) = \tilde{K}_{u}(k) [I - H(k) \tilde{K}_{x}(k)]$$
 (192)

$$\Delta K_{\mathbf{x}}(\mathbf{k}) = S_{\mathbf{x}}(\mathbf{k};\mathbf{q}) \widetilde{K}_{\Delta \mathbf{u}}(\mathbf{k})$$
(193)

$$\Delta K_{u}(k) = S_{\Delta u}(k;q) \widetilde{K}_{\Delta u}(k)$$
(194)

Eqs. (193) and (194) follow from Eq. (vi) of Table 8 and Eqs. (151) - (152).

one may note that

$$[I - K_{\mathbf{x}}H] = [I - \Delta K_{\mathbf{x}}H] [I - S_{\mathbf{u}}\widetilde{K}_{\mathbf{u}}H] [I - \widetilde{K}_{\mathbf{x}}H]$$
(195)

The predicted measurement residual covariance V satisfies

$$V(k) = V_1(k) R^{-1}(k) \tilde{V}_{\Delta u}(k) R^{-1}(k) V_1(k)$$
 (196)

where

$$V_1(k) = \tilde{V}_x(k) R^{-1}(k) \tilde{V}_u(k) R^{-1}(k) \tilde{V}_x(k)$$
 (197)

TABLE 8

FILTERING EQUATIONS FOR ESTIMATING Δu_q

$$\begin{split} & \Delta u_{q}(k+1|k) = \Delta u_{q}(k) \quad (i) \\ & \widetilde{P}_{\Delta u}(k+1|k) = \widetilde{P}_{\Delta u}(k) \quad (ii) \end{split}$$

$$\gamma_{\Delta u}(k) = \Delta z(k) - H_{\Delta u}(k) \tilde{\Delta u}_{q}(k|k-1)$$
 (iii)

$$\widetilde{V}_{\Delta u}(k) = H_{\Delta u}(k) \widetilde{P}_{\Delta u}(k|k-1) H_{\Delta u}^{T}(k) + R_{\Delta u}(k)$$
(iv)
$$\widetilde{V}_{\Delta u}(k) = \widetilde{V}_{\Delta u}(k|k-1) H_{\Delta u}^{T}(k) \widetilde{V}_{\Delta u}(k)$$
(iv)

$$\sum_{\Delta u} (k) = \sum_{\Delta u} (k|k-1) + \sum_{\Delta u} (k) = \sum_{\Delta u} (k|k-1) + \sum_{\Delta u} (k)$$
 (v)

$$\Delta u_{q}(k) = \Delta u_{q}(k|k-1) + K_{\Delta u}(k) \gamma_{\Delta u}(k)$$
(vi)

$$P_{\Delta u}(k) = [I - K_{\Delta u}(k) H_{\Delta u}(k)] P_{\Delta u}(k|k-1)$$
(vii)

where

ì

$$\tilde{\Delta u}_{q}(q) = \tilde{\Delta u}_{q}$$
(viii)

$$H_{\Lambda u}(k) = H(k) S_{x}(k;q)$$
(1x)
(1x)
(1x)

$$S_{x}(q;q) = 0$$
 (xi)

$$S_{\Lambda u}(q;q) = I$$
 (xii)

$$S_{x}(k+1;q) = \Delta A_{1}(k+1,k) S_{x}(k;q) + \Delta B_{1}(k+1,k) S_{\Delta u}(k;q)$$
(xiii)

$$S_{x}(k+1;q) = \Delta A_{2}(k+1,k) S_{x}(k;q) + \Delta B_{1}(k+1,k) S_{\Delta u}(k;q)$$
(xiii)

$$\Delta A_{1}(k,k-1) = [I - \tilde{K}_{x}(k)H(k) - S_{y}(k;0)K_{1y}(k)H(k)]A(k,k-1)$$
(xv)

$$\Delta B_{1}(k,k-1) = [I - \tilde{K}_{x}(k)H(k) - S_{u}(k;0)K_{1u}(k)H(k)]B(k,k-1)$$
 (xvi)

$$\Delta A_{2}(k,k-1) = -K_{1u}(k)H(k)A(k,k-1)$$
 (xvii)

$$\Delta B_{2}^{(k,k-1)} = [I - K_{1u}^{(k)H(k)B(k,k-1)}]$$
 (xviii)

$$K_{1u}(k) = \widetilde{K}_{u}(k) [I - H(k) \widetilde{K}_{x}(k)]$$
 (xix)

$$R_{\Delta u}(k) = R(k) \tilde{\nabla}_{x}^{-1}(k) R(k) \tilde{\nabla}_{u}^{-1}(k) R(k) \tilde{\nabla}_{x}^{-1}(k) R(k)$$
(xx)

 $\Delta z(k) = z(k) - H(k) [\tilde{x}_{1}(k) + S_{u}(k; 0)\tilde{u}(k)]$ (xxi)

6. DETECTION AND ESTIMATION OF JUMP USING THE GLR APPROACH: BANK OF Δ -FILTERS

We consider the employment of a bank of Kalman-Bucy constant Δ -state filters for detecting and estimating the jump Δu_q . The jump Δu_q and the jump time q are unknowns. We consider a moving window of length M. That is, at each j, k-M<j<k we employ the constant Δ -state filter defined by the equations of Table 8. Let j be a candidate jump time and let k be the current observation time. The filtering equations in Table 8 are used to obtain the estimate $\Delta u_j(k)$ and $\tilde{P}_{\Delta u,j}(k)$. The filter is started when the current observation time is j. It uses the initial conditions

$$\tilde{\Delta u}_{j}(j) = \tilde{\Delta u}_{q}$$
(198)

$$\widetilde{P}_{\Delta u,j}(j) = P_{\Delta u}(q)$$
(199)

$$S_{x}(j;j) = 0$$
 (200)

$$S_{Au}(j;j) = I$$
 (201)

At each new observation k the matrix $S_{\chi}(k;j)$ is computed using Eqs. (xiii) - (xix) of Table 8. Eqs. (i) - (vii) are then used to compute $\Delta u_{j}(k)$ and $\tilde{P}_{\Delta u,j}(k)$. The following are also computed

$$d_{j}(k) = d_{j}(k-1) + H_{\Delta u, j}^{T}(k) R_{\Delta u}^{-1}(k) \Delta z(k)$$
 (202)

$$\ell_{j}(k) = d_{j}^{T}(k) \widetilde{\Delta u}_{j}(k)$$
(203)

The vector d_i has the initial condition

$$d_{j}(j) = 0$$
 (204)

The above computations are carried out for each candidate jump time j, $k-M \le j < k$. A jump is detected at time k for the jump time q, $k-M \le q < k$, if

$$l_{q}(k) > 2 l_{n}(n)$$

 $l_{q}(k) = Max \{l_{j}(k) : k-M \le j \le k\}$ (205)

where the value η is chosen to provide a reasonable tradeoff between false and missed alarms. The above is a generalized likelihood ratio (GLR) algorithm for detecting and estimating the jump, [1] and [16]. In applying the filter described by the equations of Table 8 one should sequentially update the correlated subblocks of components of the measurement vector as discussed in [17] - [20].

After a jump has been detected and estimated we use Eqs. (175) - (187) to reinitialize the filters of Tables 5 and 7. The above GLR algorithm is used to detect and estimate the next jump.

7. SUMMARY OF DERIVED EXPRESSIONS

The optimum estimates \hat{x} of the state and \hat{u} of the control satisfy the expressions

$$\hat{\mathbf{x}} = \tilde{\mathbf{x}} + \mathbf{S}_{\mathbf{u}}\tilde{\mathbf{u}} + \mathbf{S}_{\mathbf{x}}\tilde{\Delta \mathbf{u}}$$
(206)

$$\hat{\mathbf{u}} = \tilde{\mathbf{u}} + \mathbf{S}_{\Delta \mathbf{u}} \quad \tilde{\Delta \mathbf{u}} \tag{207}$$

with covariances

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$$P_{x} = \tilde{P}_{x} + S_{u} \tilde{P}_{u} S_{u}^{T} + S_{x} \tilde{P}_{\Delta u} S_{x}^{T}$$
(208)

$$P_{xu} = S_{u} \tilde{P}_{u} + S_{x} \tilde{P}_{\Delta u} S_{\Delta u}^{T}$$
(209)

$$P_{u} = \tilde{P}_{u} + S_{\Delta u} \tilde{P}_{\Delta u} S_{\Delta u}^{T}$$
(210)

where \tilde{x} , \tilde{u} and $\tilde{\Delta u}$ are the output of a tri-system of unaugmented Kalman-Bucy filters with covariances \tilde{P}_x , \tilde{P}_u and $\tilde{P}_{\Delta u}$, respectively.

The matrices S_u , S_x and S_u satisfy

$$S_{u}(k+1) = \Delta_{x} A S_{u}(k) + \Delta_{x} B$$
(211)

$$S_{x}(k+1) = \Delta_{u}AS_{x}(k) + \Delta_{u}BS_{\Delta u}(k)$$
(212)

$$S_{\Delta u}(k+1) = \Delta_{\Delta u} A S_{x}(k) + \Delta_{\Delta u} B S_{\Delta u}(k) + S_{\Delta u}(k)$$
(213)

where

$$\Delta_{\mathbf{x}} = \mathbf{I} - \mathbf{\tilde{K}}_{\mathbf{x}} \mathbf{H}$$
(214)

$$\Delta_{u} = [I - S_{u} \tilde{K}_{u} H] \Delta_{x}$$
(215)

$$\Delta_{\Delta u} = -\kappa_{u} H \Delta_{x}$$
(216)

The initial conditions of ${\bf S}_{\bf u}^{},\,{\bf S}_{\bf x}^{}$ and ${\bf S}_{\Delta {\bf u}}^{}$ are

$$S_u(0) = P_{xu}(0) P_u^{-1}(0)$$
 (217)

$$S_{x}(q) = 0$$
 (218)

$$S_{\Delta u}(q) = I \tag{219}$$

where q is the jump time, $P_u(0)$ is the initial covariance of u and $P_{xu}(0)$ is the initial cross-covariance of x and u.

The optimal Kalman gains satisfy

$$K_{x} = \tilde{K}_{x} + [S_{u}\tilde{K}_{u} + S_{x}\tilde{K}_{\Delta u}(I - H S_{u}\tilde{K}_{u})] [I - H\tilde{K}_{x}]$$
(220)

$$K_{u} = [\tilde{K}_{u} + S_{\Delta u} \tilde{K}_{\Delta u} (I - H S_{u} \tilde{K}_{u})] [I - H \tilde{K}_{x}]$$
(221)

The predicted measurement residual covariance satisfies

$$v = v_1 R^{-1} \tilde{v}_{\Delta u} R^{-1} v_1$$
 (222)

where

$$\mathbf{v}_{1} = \widetilde{\mathbf{v}}_{\mathbf{x}} \mathbf{R}^{-1} \widetilde{\mathbf{v}}_{\mathbf{u}} \mathbf{R}^{-1} \widetilde{\mathbf{v}}_{\mathbf{x}}$$
(223)

and where $\tilde{v}_x = \tilde{v}_{\Delta u}$ and $\tilde{v}_{\Delta u}$ are the predicted measurement residual covariances of the \tilde{x} -, the \tilde{u} - and the Δu filters, respectively.

After reinitialization, the optimum estimates satisfy Friedland's expressions [21]

$$\hat{\mathbf{x}} = \tilde{\mathbf{x}}' + \mathbf{S}_{\mathbf{u}}' \tilde{\mathbf{u}}'$$

$$\hat{\mathbf{u}} = \tilde{\mathbf{u}}'$$
(224)
(225)

where the prime denotes the output of the \tilde{x} - and the \tilde{u} -filters after reinitialization. The reinitialized values of S_{u} , \tilde{x} , \tilde{P}_{x} , \tilde{u} and \tilde{P}_{u} satisfy the following expressions at reinitialization:

$$\mathbf{s}_{u}' = [\mathbf{s}_{u} \ \widetilde{\mathbf{P}}_{u} + \mathbf{s}_{x} \ \widetilde{\mathbf{P}}_{\Delta u} \ \mathbf{s}_{\Delta u}^{\mathrm{T}}] \ [\widetilde{\mathbf{P}}_{u} + \mathbf{s}_{\Delta u} \ \widetilde{\mathbf{P}}_{\Delta u} \ \mathbf{s}_{\Delta u}^{\mathrm{T}}]^{-1}$$
(226)

$$\widetilde{\mathbf{x}'} = \widetilde{\mathbf{x}} + \mathbf{S}_{\mathbf{u}} \widetilde{\mathbf{u}} + \mathbf{S}_{\mathbf{x}} \widetilde{\Delta \mathbf{u}} - \mathbf{S}_{\mathbf{u}}' [\widetilde{\mathbf{u}} + \mathbf{S}_{\Delta \mathbf{u}} \widetilde{\Delta \mathbf{u}}]$$
(227)

$$\widetilde{P}_{x}' = \widetilde{P}_{x} + s_{u} \widetilde{P}_{u} s_{u}^{T} + s_{x} \widetilde{P}_{\Delta u} s_{x}^{T} - s_{u}' [P_{u} + s_{\Delta u} \widetilde{P}_{\Delta u} s_{\Delta u}^{T}] s_{u}'T$$
(228)

$$\widetilde{u}' = \widetilde{u} + S_{\Delta u} \widetilde{\Delta u}$$
(229)

$$\widetilde{P}_{u}' = \widetilde{P}_{u} + S_{\Delta u} \widetilde{P}_{\Delta u} S_{\Delta u}^{T}$$
(230)

The equations of the x-, the u-, and the Δ u-filters are given in Tables 5, 7 and 8, respectively.

8. CONCLUSIONS

We have developed a Friedland-like filtering technique for estimating the state x of a discrete linear stochastic process which depends on a piecewise constant control vector u. It is composed of three unaugmented Kalman-Bucy filters. In the first filter the estimate \tilde{x} of the state is computed as if there were no control present and no jump in control present. This estimate is then corrected to account for the control and for the jump in control. In the second filter the estimate \tilde{u} of the control is computed as if there were no jump in control present. This estimate is corrected to account for the jump in control present. This estimate filter the estimate \tilde{u} of the control is computed as if there were no jump in control present. This estimate is corrected to account for the jump in control present. This estimate is corrected to account for the jump in control is computed.

The optimum estimate x is a vector sum of the three estimates \tilde{x} , \tilde{u} and $\tilde{\Delta u}$. The coefficient of \tilde{u} in the sum is a matrix having dependence on the gain of the \tilde{x} -filter. The coefficient of $\tilde{\Delta u}$ in the sum is a matrix that depends on the gains of the \tilde{x} - and the \tilde{u} -filters.

The optimum estimate u is a vector sum of the two estimates \tilde{u} and Δu . The coefficient of Δu is a function of the gains of the \tilde{x} - and the \tilde{u} -filters.

The x-filter processes the measurement z. The u-filter processes as its measurement the a posteriori measurement residual z-Hx of the x-filter. The Δu -filter processes the a posterior measurement residual z - Hx - H S_u of the u-filter in which S_u depends on the gain of the x-filter.

A procedure has been developed for reinitializing the xand the \tilde{u} -filters after a jump has been detected so that the optimum estimates \hat{x} and \hat{u} are functions only of the output of those filters and, as a result, satisfy Friedland's expressions [21]. The reinitialization procedure permits the treatment of multiple jumps.

We have presented a GLR algorithm for detecting the jump time q. It uses the \tilde{x} - and \tilde{u} -filters and a bank of Δu -filters. The algorithm reinitializes the \tilde{x} - and \tilde{u} -filters after a jump has been detected. This GLR algorithm avoids numerical inaccuracies introduced by computations with large vectors and matrices due to augmenting the state vector of the original system with the control vector. The algorithm has particular application to problems involving a large number of state and/or jump variables.

REFERENCES

- H. Stalford, "GLR algorithms for detecting and estimating abrupt maneuvers in ASMD scenarios using a decomposition of the maneuver signature matrix," PSI Technical Report 81-1, July 1981.
- [2] R. J.McAulay and E. Denlinger, "A decision-directed adaptive tracker," IEEE Trans. Aerosp. Electron. Syst., Vol. AES-9, pp. 229-236, March 1973.
- [3] R. R. Tenney, R. S. Hebbert, and Nils R. Sandell, Jr.,
 "A tracking filter for maneuvering sources," IEEE Trans.
 Automatic Control, Vol. AC-22, pp. 246-251, April 1977.
- [4] R. L. Moose, "An adaptive state estimation solution to the maneuvering target problem," IEEE Transactions on Automatic Control, pp. 359-362, June 1975.
- [5] C. B. Chang, R. H. Whiting and M. Athans, "On the state and parameter estimation for maneuvering reentry vehicles," IEEE Trans. on Automatic Control, pp. 99-105, February 1977.
- [6] R. Bueno, E. Y. Chow, K.-P. Dunn, S. B. Gershwin and A. S. Willsky, "Status report on the generalized likelihood ratio failure detection technique, with applications to the F-8 aircraft," Proc. 1976 IEEE Conf. on Decision and Control, Clearwater, FL, pp. 38-47, December 1976.

- [7] J. C. Deckert, M. N. DESAI, J. J. Deyst, A. S. Willsky,
 "F-8 DFBW sensor failure identification using analytic redundancy," IEEE Trans. on Automatic Control, Vol. AC-22, No. 5, pp. 795-803, October 1977.
- [8] Chr. Zyweitz and B. Schneider, <u>Computer Application on</u> <u>ECG and VCG Analysis</u>, North Holland, 1973.
- [9] M. Fiorina and C. Maffezzoni, "A direct approach to jump detection in linear time-invariant systems with application to power system perturbation detection, "IEEE Trans. Automatic Control, Vol. AC-24, pp. 428-434, June 1979.
- [10] A. S. Willsky, "A survey of design methods for failure detection in dynamic systems," Automatica, Vol. 12, pp. 601-611, 1976.
- [11] D. Middleton and R. Esposito, "Simultaneous optimum detection and estimation of signals in noise," IEEE Trans. Inf. Th., Vol. IT-14, No. 3, pp. 434-444, May 1968.
- [12] H. L. Van Trees, <u>Detection</u>, <u>Estimation and Modulation</u> <u>Theory</u>, <u>Part I:</u> <u>Detection</u>, <u>Estimation</u>, <u>and Linear</u> <u>Modulation Theory</u>, <u>Wiley</u>, <u>New York</u>, 1971.
- [13] J. J. Deyst and J. C. Deckert, "RCS jet failure identification for the space shuttle," Proc. IFAC 75, Cambridge, MA, August 1975.

- [14] P. Sanyal and C. N. Shen, "Bayes' decision rule for rapid detection and adaptive estimation scheme with space applications," IEEE Trans. Aut. Control AC-19, pp. 228-231, June 1974.
- [15] E. Chow, K.-P. Dunn and A. S. Willsky, "Research status report to NASA Langley research center: A dual-mode generalized likelihood ratio approach to self-reorganizing digital flight control system design," M.I.T. Electronic Systems Laboratory, Cambridge, MA, April 1975.
- [16] A. S. Willsky and H. L. Jones, "A generalized likelihood ratio approach to the detection and estimation of jumps in linear systems," IEEE Trans. Automat. Contr., Vol. AC-21, pp. 108-112, February 1976.
- [17] C. B. Chang and K. P. Dunn, "A recursive generalized likelihood ratio test algorithm for detecting sudden changes in linear discrete systems," in Proc. 17th IEEE Conf. on Decision and Control, San Diego, CA., January 1979.
- [18] C. B. Chang and K. P. Dunn, "On GLR detection and estimation of unexpected inputs in linear discrete systems," IEEE Trans. on Auto. Contr., Vol. AC-24, No. 3, pp. 499-501, June 1979.

 [19] H. W. Sorenson, "Kalman filtering techniques," in <u>Advances</u> <u>in Control Systems, Theory and Applications</u>, Vol. 3,
 C. T. Leondes, ed., Academic Press, N.Y., pp. 219-292, 1966.

and the second second

- [20] D. Willner, C. B. Chang, and K. P. Dunn, "Kalman filter algorithms for a multi-sensor system," in Proc. 1976 IEEE Conf. on Decision and Control, Clearwater, FL., pp. 570-574, December 1976.
- [21] B. Friedland, "Treatment of bias in recursive filtering," IEEE Trans. on Automatic Control, Vol. AC-14, No. 4, pp. 359-367, August 1969.
- [22] B. Friedland, "Notes on separate-bias estimation," IEEE Trans. on Automatic Control, Vol. AC-23, No. 4, pp. 735-738, August 1978.
- [23] E. C. Tacker and C. C. Lee, "Linear filtering in the presence of time-varying bias," IEEE Trans. on Automatic Control, AC-17, pp. 828-829, December 1972.
 - [24] R. E. Kalman, "A new approach to linear filtering and prediction problems," Trans. ASME, Series D, Journal of Basic Engineering, Vol. 82, pp. 35-45, March 1960.

- [25] R. S. Bucy, "Optimum finite-time filters for a special non-stationary class of inputs," JHU/APL Internal Memorandum BBD-600, 1959.
- [26] R. E. Kalman and R. S. Bucy, "New results in linear filtering and prediction theory," Trans. ASME, Series D, Journal of Basic Engineering, Vol. 83, pp. 95-108, March 1961.
- [27] R. E. Kalman, "New methods in Wiener filtering theory," in the 1960 Proc. of the 1st Symposium on Engineering Applications of Random Function Theory and Probability, Edited by John Bogdanoff and Frank Kozin, John Wiley & Sons, N.Y., pp. 270-388, 1963.
- [28] A. H. Jazwinski, <u>Stochastic Processes and Filtering</u> Theory, New York, Academic Press, 1970.
- [29] M. B. Ignagni, "An alternate derivation and extension of Friedland's two-stage Kalman estimator," IEEE Trans. Automatic Control, Vol. AC-26, No. 3, pp. 746-750, June 1981.

