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The Three-Dimensional Non-Linear Theory of the Free Electron Laser in the Amplifying Configuration

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This paper presents a self-consistent non-linear treatment of the finite transverse dimensional effects associated with (i) the wiggler field, (ii) the electron beam and (iii) the radiation beam of the free electron laser (FEL) in a steady state amplifying configuration. Our formulation incorporates various efficiency enhancement schemes. A linearly polarized magnetic wiggler is used for our formulation. The inherent gradient of the magnetic wigglers in the transverse direction introduces betatron oscillations, which cause an increase in the effective axial beam temperature. (Continued) | | |

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20. ABSTRACT (Continued)

The radiation beam in the presence of the electron beam and the magnetic wiggler experience diffraction as well as refraction effects. We find that the 3-D effects can lead to substantial differences in the results compared to the 1-D theory. Finally a 3-D numerical illustration of a 10.6 μm FEL is given.

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THE THREE-DIMENSIONAL NON-LINEAR THEORY OF THE FREE ELECTRON LASER IN THE AMPLIFYING CONFIGURATION

I. INTRODUCTION

The development of lasers in which the active medium is a relativistic beam of electrons has recently evoked much interest. These radiation sources can be characterized by frequency tunability with output wavelength ranging from millimeter to beyond the optical regime, very high power levels, and high efficiencies.

The purpose of this paper is to present a non-linear 3-D formulation of the FEL in the steady state amplifying configuration including the various efficiency improvement schemes. The 3-D effects are associated with the wiggler field, the electron beam and the radiation beam. We find that the 3-D effects can lead to significantly different results than results obtained from the 1-D theory. Numerous publications have treated the 1-D free electron laser mechanism⁽¹⁻¹⁴⁾, while 3-D effects in the FEL have just recently been considered.⁽¹⁵⁻²⁰⁾

The transverse effects associated with a static magnetic wiggler field introduces modifications in the electron dynamics. A physically realizable magnetic wiggler field has transverse spatial variations as well as an axial component of the magnetic field in order to satisfy $\nabla \times \mathbf{B}_w = \nabla \cdot \mathbf{B}_w = 0$. The physically realizable wiggler fields causes slow betatron oscillations, which result in an increase in the effective axial beam temperature. If the effective beam temperature is large, it will significantly reduce the fraction of electrons trapped in the ponderomotive potential buckets.

The effects of finite transverse dimensions of the radiation and electron beam are interrelated. The radiation beam can be considered to be a superposition of the input field and excited field. The input Gaussian radiation beam diffracts as it propagates through the interaction region; its amplitude and phase change as a function of axial position. The excited radiation beam suffers from both diffraction and refraction. The profile of the excited radiation beam is in general not Gaussian. The waist of the input field is typically somewhat greater than the electron beam radius, whereas the effective waist of the excited field is comparable to the radius of the electron beam and hence it diffracts more rapidly than the input field. In general, the potential exists for destructive interference between the two fields. This would result in a decrease in the depth of the ponderomotive potential wells and cause detrapping of the electrons. However, destructive interference, in the parameter regime which we consider, is not observed.

A number of efficiency enhancement schemes^(7,10,11) for the FEL have been identified. Improved efficiency can be achieved by any or all of the following methods: (i) contouring, spatially in the longitudinal direction, the amplitude and/or wavelength of the magnetic wiggler field, and (ii) applying an external D.C. electric field. By applying one or more of these efficiency enhancement schemes, the phase of the electrons trapped in the ponderomotive wave can be adjusted so that electron kinetic energy is converted into radiation. Our formulation will include and show the equivalence of the above enhancement schemes.

In Section II, we describe the 3-D particle dynamics in a linearly polarized magnetic wiggler. We obtain a general 3-D solution for the radiation field using Fourier transform techniques in Section III. Section IV is devoted to a FEL operating in the low gain limit with an electron beam possessing an axially symmetric Gaussian beam profile. Section V derives the expression for total power gain and efficiency. In the last section, we give a numerical example of an FEL operating at 10.6 μm .

II. PARTICLE DYNAMICS—DERIVATION OF PHASE EQUATION

Our model of the FEL configuration is shown in Figure 1. We consider a linearly polarized magnetic wiggler field that is independent of x . The generalized linearly polarized wiggler and radiation field are represented by the following vector potentials.

$$A_w(y,z) = A_w(z) \cosh(k_w(z)y) \cos\left(\int_0^z k_w(z') dz'\right) \hat{e}_x, \quad (1)$$

$$A_R(x,y,z,t) = A_R(x,y,z) \sin\left(\frac{\omega}{c}z - \omega t + \varphi(x,y,z)\right) \hat{e}_x, \quad (2)$$

where $A_w(z)$ and $k_w(z) = 2\pi/l_w(z)$ are the slowly varying amplitude and wave number of the wiggler field, l_w is the wiggler wavelength, A_R and φ are the slowly varying amplitude and phase of the total radiation field, ω is the frequency of the radiation and c is the speed of light.

We also include an external D.C. electric field $E_{DC}(z) = -\partial\phi_{DC}(z)/\partial z \hat{e}_z$. In all cases of interest $|A_w| \gg |A_R|$ by many orders of magnitude. Furthermore, it is necessary to have $k_w r_b \ll 1$ where r_b is the electron beam radius.⁽⁴⁾

Space charge effects will be neglected. This is appropriate if the beam density satisfies⁽¹⁶⁾

$$n_0 \ll (k_w^2 \gamma_{z0}^4 A_w A_R) (2\pi \gamma_0 m_0 c^2)^{-1} \quad (3)$$

where $\gamma_{z0} = (1 - v_{z0}^2/c^2)^{-1/2}$, v_{z0} is the axial velocity of the electron in the wiggler field, $\gamma_0 = (1 - v_0^2/c^2)^{-1/2}$, and v_0 is the magnitude of the total particle velocity. Equation (3) can be derived by comparing the ponderomotive term to the space charge term in the pendulum equation or the equation for phase, see Ref. (8).

Electrons execute complicated trajectories in three-dimensions. If the radiation field, $A_R(x,y,z)$, varies little in the x -direction over the electron beam, there is a constant of motion in the x -direction

$$P_x = \frac{|e|\hbar}{c} (A_w + A_R) \cdot \hat{e}_x. \quad (4)$$

The particles execute betatron types of orbits in the y -direction due to the gradient in the magnetic wiggler field. If a particle entered the interaction region $z = 0$ with transverse coordinates (x_0, y_0) , and initial transverse velocity v_{y0} , the particle's transverse location at z is

$$\bar{x} = x_0 + \frac{\beta_{\alpha}}{k_w} \cosh(k_w(z)\bar{y}) \sin \int_0^z k_w(z') dz' \quad (5a)$$

and

$$\bar{y} = y_0 \cos K_0 z + \frac{v_{y0}}{K_0 v_{z0}} \sin K_0 z \quad (5b)$$

where $\beta_{\alpha} = v_{\alpha}/c$, $v_{\alpha} = |e|A_w/(\gamma_0 m_0 c)$ is the wiggler velocity, $\gamma_0 = (1 - v_0^2/c^2)^{-1/2}$, v_0 is the magnitude of total particle velocity and $K_0 = \beta_{\alpha} k_w/\sqrt{2}$. The derivation of the betatron oscillation is given in Appendix I.

The envelope of the electron beam in the y direction is not a constant in general. For example, if there is no initial transverse velocity spread in the y direction, i.e., $v_{y0} = 0$, the electron beam undergoes periodic pinching in the y -direction. All realizable electron beams have finite emittance. The emittance, ϵ_y , is defined as $\epsilon_y = \pi y_{0,\max} (v_{y0,\max}/c)$, where $y_{0,\max}$ and $v_{y0,\max}$ are the electron beam waist and the maximum velocity spread respectively in the y -direction at the entrance of the magnetic wiggler. The condition for the envelope of the electron beam to remain approximately constant inside the realizable wiggler with transverse gradient is to require that the first and second term on the right-hand-side of (5b) be equal, i.e.,

$$y_{0,\max} = v_{y0,\max}/(K_0 v_{z0}) = \sqrt{\epsilon_y/(\pi K_0)}. \quad (6a)$$

The condition⁽¹⁵⁽ⁱ⁾⁾ on $y_{0,\max}$ in (6a) also leads to the smallest electron beam radius inside the wiggler field,

$$r_b = \sqrt{\frac{2\epsilon_y}{\pi K_0}}. \quad (6b)$$

The gradient in the wiggler field will lead to an increase in the energy spread associated with the axial motion. Let us consider a cold electron beam with total energy $\gamma_0 m_0 c^2$. Since part of the energy is associated with the transverse motion, the axial velocity of a particle decreases as the amplitude of

the betatron oscillation increases. The maximum axial velocity shear, due to the wiggler gradient, is given by

$$\Delta v_{\text{shear}} = c(\beta_{0z} k_w r_b/2)^2, \quad (7)$$

while the corresponding longitudinal energy spread is

$$\Delta E_{\text{shear}} = \gamma_{0z}^2 \gamma_0 (\Delta v_{\text{shear}}/c) m_0 c^2. \quad (8)$$

One efficiency enhancement approach is to initially trap a large fraction of the electrons in the ponderomotive potential wells and adiabatically extract kinetic energy from the particles. In order to trap a substantial fraction of the electrons, we require the trapping potential to be larger or at least comparable to the axial particle energy spread, i.e., $|e|\phi_{\text{trap}} > \Delta E_{\text{shear}}$. The initial depth of the trapping potential is

$$|e|\phi_{\text{trap}}/(\gamma_0 m_0 c^2) = 2\sqrt{2} \gamma_{0z} \beta_{0z} (A_R/A_w)^{1/2}. \quad (9)$$

Combining Eqs. (7), (8) and (9), the radius of the electron beam is found to be limited by

$$r_b < (\gamma_{0z} k_w)^{-1} \left(\frac{8\sqrt{2} \gamma_{0z}}{\beta_{0z}} \right)^{1/2} \left(\frac{A_R}{A_w} \right)^{1/4}. \quad (10)$$

The axial electron dynamics is most crucial in the FEL mechanism. With this in mind, we start with the equation of motion for the axial electron velocity, which can be written in the form

$$\begin{aligned} \frac{dv_z}{dt} = & \frac{|e|}{\gamma_z^2 \gamma m_0} \frac{\partial \phi_{DC}}{\partial z} - \frac{|e|^2}{2\gamma^2 m_0^2 c^2} \left[\frac{\partial}{\partial z} \left(A_w \cosh(k_w y) \cos \left(\int_0^z k_w dz' \right) \right)^2 \right. \\ & \left. + 2k_w A_w \cosh(k_w y) A_R \cos \left(\int_0^z \left(\frac{\omega}{c} + k_w \right) dz' - \omega t + \varphi \right) \right] \end{aligned} \quad (11)$$

where $v_z = v_z(x, y, z, t)$ is the axial electron velocity, $\gamma_z = (1 - v_z^2/c^2)^{-1/2}$, $\gamma = \gamma_z \gamma_{0z}$, $\gamma_{0z}(z) = (1 + (|e|A_w(z)/(m_0 c^2))^2)^{1/2}$. In obtaining Eq. (11) we have taken $\omega \approx \gamma_z^2(1 + v_z/c) ck_w$ and the x component of electron momentum to be $(|e|/c) (A_w(y, z) + A_R(x, y, z, t)) \cdot \hat{e}_x$.

The second term on the right-hand side of Eq. (11) indicates that the axial velocity in a linearly polarized wiggler has an oscillatory component at twice the wiggler wave number. In Ref. (14), we showed that the axial oscillation is not large enough to cause particle detrapping in the ponderomotive potential well and, thus, it does not have a qualitative effect on the FEL mechanism.

At this point we perform a transformation⁽⁷⁾ from the Eulerian independent variables x, y, z, t to Lagrangian independent variables $z, \psi_0, x_0, y_0, v_{y0}$ where ψ_0, x_0, y_0, v_{y0} are the particle's phase in the ponderomotive potential wave, transverse coordinates and transverse velocity at the entrance to the interaction region, i.e., $z = 0$.

The equation governing the relative phase between the electrons and the ponderomotive wave (see Ref. (8) for 1-D derivation) is given by the generalized pendulum like equation

$$\begin{aligned} \frac{\partial^2 \tilde{\psi}}{\partial z^2} &= \frac{d^2 \varphi}{dz^2} + \frac{dk_w}{dz} + \frac{|e|\omega/c}{\tilde{\gamma}_z^2 \tilde{\gamma} m_0 c^2} \frac{\partial \phi_{DC}}{\partial z} \\ &- \frac{|e|^2 \omega/c}{2\tilde{\gamma}^2 m_0^2 c^4} \left[\frac{\partial}{\partial z} \left(A_w \cosh(k_w \tilde{y}) \cos \int_0^z k_w dz' \right)^2 \right. \\ &\left. + 2k_w A_w \cosh(k_w \tilde{y}) A_R(\tilde{x}, \tilde{y}, z) \cos \tilde{\psi} \right] \end{aligned} \quad (12)$$

where $\tilde{\psi}(z, \psi_0, x_0, y_0, v_{y0}) = \int_0^z (\omega/c + k_w(z') - \omega/v_z(\tilde{x}, \tilde{y}, \psi_0, z')) dz' + \varphi(\tilde{x}, \tilde{y}, z) + \psi_0$ is the phase, $\tilde{\gamma} = \tilde{\gamma}_z \gamma_\perp$, $\tilde{\gamma}_z = (1 - \tilde{v}_z^2/c^2)^{-1/2}$, $\tilde{v}_z = \omega/(\omega/c + k_w(z) - \partial \tilde{\psi}/\partial z + d\varphi/dz)$ is the electron axial velocity and ψ_0 is the initial phase at $z = 0$.

Equations (5) and (12) completely describe the non-linear particle dynamics in terms of the fields A_w and A_R . From the structure of Eq. (12), it becomes clear that contouring the wiggler wavelength and/or amplitude, i.e., dk_w/dz or dA_w^2/dz , is directly equivalent to applying D.C. electric field, i.e., $\partial \phi_{DC}/\partial z$.

III. EVOLUTION OF GENERAL 3-D TOTAL RADIATION FIELD

This section will derive the total radiation field in the presence of the electron beam. The radiation field satisfies the wave equation

$$\left(\nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) A_R = - \frac{4\pi}{c} J_x \hat{e}_x \quad (13)$$

where the current density⁽⁷⁾ is given by

$$\begin{aligned} J_x(x, y, z, t) &= - \frac{|e| n_0 v_0}{\omega} \int_{-\infty}^{\infty} d\psi_0 \int_{-\infty}^{\infty} dx_0 \int_{-\infty}^{\infty} dy_0 \int_{-\infty}^{\infty} dv_{y0} \\ &\sigma(v_{y0}) \theta(x_0, y_0) \delta(x - \tilde{x}) \delta(y - \tilde{y}) \delta(t - \tilde{t}) \frac{\tilde{P}_x}{\tilde{P}_z} \end{aligned} \quad (14)$$

where $\theta(x_0, y_0)$ is a function which describes the initial electron beam profile, $\sigma(v_{y0})$ is a function which describes the initial transverse velocity profile in y direction, n_0 is the electron beam density on axis outside of the interaction region, $\tilde{P}_x \approx (|e|/c) A_w(\tilde{y}, z) \cdot \hat{e}_x$ is the equilibrium particle momentum in the x -direction, and $\tilde{P}_z = \tilde{\gamma} m_0 \tilde{v}_z$ is the axial particle momentum. We can solve for A_R using Fourier transform techniques.

The radiation field in (2) can be represented in the form

$$A_R(x, y, z, t) = (2i)^{-1} a(x, y, z) \exp i(\omega z/c - \omega t) \hat{e}_x + c.c. \quad (15)$$

where $a = A_R \exp(i\varphi)$ is the complex field amplitude. A_R and φ are slowly varying functions of z . Substituting (15) into the wave Eq. (13), we obtain an equation for $a(x, y, z)$,

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + 2i \frac{\omega}{c} \frac{\partial}{\partial z} \right) a(x, y, z) = j(x, y, z), \quad (16)$$

where

$$j(x, y, z) = - \frac{4\omega i}{c} \int_0^{2\pi/\omega} dt J_x(x, y, z, t) e^{-i(\frac{\omega}{c}z - \omega t)}.$$

By applying arguments presented in Ref. (7), the integral over time can be eliminated. The variable $j(x, y, z)$ can now be rewritten as

$$j(x, y, z) = \frac{\omega_b^2}{c^2} i \int_0^{2\pi} \frac{d\psi_0}{2\pi} \int_{-\infty}^{\infty} dx_0 \int_{-\infty}^{\infty} dy_0 \theta(x_0, y_0) \int_{-\infty}^{\infty} dv_{y0} \quad (17)$$

$$\sigma(v_{y0}) \delta(x - \bar{x}) \delta(y - \bar{y}) \frac{A_w}{\bar{y}} \cosh(k_w \bar{y}) \exp(-i(\bar{\psi} - \varphi)).$$

where $\omega_0 = (4\pi |e|^2 n_0 / m_0)^{1/2}$ is the plasma frequency, \bar{x}, \bar{y} and $\bar{\psi}$ are functions of $(z, \psi_0, x_0, y_0, v_{y0})$. The term that is not resonant with the ponderomotive wave is dropped from $j(x, y, z)$.

The solution for $a(x, y, z)$ can be easily obtained by going to the transformed space. Let \bar{j} be the Fourier transform of j ,

$$\bar{j}(k_x, k_y, z) = \int_{-\infty}^{\infty} dx \int_{-\infty}^{\infty} dy j(x, y, z) e^{-i(k_x x + k_y y)}. \quad (18)$$

Equation (16) becomes

$$\left[-(k_x^2 + k_y^2) + 2i \frac{\omega}{c} \frac{\partial}{\partial z} \right] \bar{a}(k_x, k_y, z) = \bar{j}(k_x, k_y, z). \quad (19)$$

Equation (19) can be easily integrated in z to yield \bar{a} in terms of \bar{j} . The complex field amplitude $a(x, y, z)$ can be obtained by taking the inverse transform.

$$\begin{aligned} a(x, y, z) &= \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \bar{a}(k_x, k_y, 0) e^{i(k_x x + k_y y - \frac{k^2 z}{2\omega/c})} dk_x dk_y \\ &- \frac{i}{2\omega/c} \frac{1}{(2\pi)^2} \int_0^z \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \bar{j}(k_x, k_y, z') e^{i(k_x x + k_y y - \frac{k^2(z-z')}{2\omega/c})} dk_x dk_y dz', \end{aligned} \quad (20)$$

where $k^2 = k_x^2 + k_y^2$. We can write $a = a_{in} + a_{ex}$, where a_{in} is the input radiation field (homogeneous solution) represented by the first term on the right-hand-side of (20), and a_{ex} is the excited radiation field (particular solution) represented by the second term.

Since the homogeneous solution is the input radiation field, the only field at $z = 0$ is a_{in} and

$$\bar{a}(k_x, k_y, 0) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} a(x, y, 0) \exp(-i(k_x x + k_y y)) dx dy.$$

Taking the input field to be the lowest order Gaussian radiation beam we find

$$a_{in}(x, y, z) = A_{in} \frac{1}{\sqrt{1 + (z/z_0)^2}} \exp\left[\frac{-z_0^2 r^2 / r_0^2}{(z^2 + z_0^2)}\right] \exp\left\{i\left[\frac{z_0 z}{z^2 + z_0^2} \left(\frac{r^2}{r_0^2}\right) - \tan^{-1}\left(\frac{z}{z_0}\right)\right]\right\} \quad (21)$$

where A_{in} is the amplitude of the input field, r_0 is the minimum waist, $z_0 = r_0^2 \omega / 2c$ is the Rayleigh length of the input field.

The excited field in Eq. (20) can be rewritten in the form of convolution integrals,

$$a_{ex}(x, y, z) = \frac{-i}{2\omega/c} \int_0^z dz' \int_{-\infty}^{\infty} dx' \int_{-\infty}^{\infty} dy' \quad (22)$$

$$G(x - x', y - y', z - z') j(x', y', z')$$

where

$$G(x, y, z) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} dk_x \int_{-\infty}^{\infty} dk_y \exp[-i\frac{(k_x^2 + k_y^2)z}{2\omega/c}] \exp[i(k_x x + k_y y)]$$

$$= -i\frac{\omega/c}{2\pi} \frac{1}{z} \exp\left[i\left(\frac{x^2 + y^2}{2z}\right)\frac{\omega}{c}\right] \quad (23)$$

is the Green's function. Substituting the expression for the current (17) into (22), the excited radiation field is found to be

$$a_{ex}(x, y, z) = -\frac{i}{4\pi} \frac{\omega_b^2}{c^2} \int_0^z dz' \int_0^{2\pi} \frac{d\psi_0}{2\pi} \int_{-\infty}^{\infty} dx_0 \int_{-\infty}^{\infty} dy_0 \int_{-\infty}^{\infty} dv_{y_0} \quad (24)$$

$$\sigma(v_{y_0}) \theta(x_0, y_0) \frac{A_w'}{\tilde{y}'} \cosh(k_w' \tilde{y}') \frac{1}{z - z'}$$

$$\exp\left[i\left((x - \tilde{x}')^2 + (y - \tilde{y}')^2\right)\frac{\omega/c}{2(z - z')}\right] \exp[-i(\tilde{\psi}' - \varphi')]$$

where the primes on quantities denote functions of z' . Equations (5), (12) and (24) describe self-consistently a general nonlinear 3-D steady state FEL amplifier.

IV. ANALYTIC AXIALLY SYMMETRIC SOLUTION

For purposes of illustrating transverse effects in the radiation field, we will consider a FEL having axial symmetry and operating in the low gain limit, i.e., $|a_{in}| \gg |a_{ex}|$. We chose a Gaussian electron beam profile, $\theta = \exp(-(x_0^2 + y_0^2)/r_b^2)$, where r_b is the radius of the electron beam. If r_b satisfies Eqs. (6) and (10) and $k_w r_b \ll 1$, then we can neglect the gradient in the wiggler and replace \tilde{x} , \tilde{y} in Eq. (24) by x_0 , y_0 and $\sigma(v_{y0})$ by $\delta(v_{y0})$. For a low gain FEL and a plane wave input field, a_{in} , (or Gaussian like TEM_{00} radiation field with the waist of the radiation beam r_0 much larger than the radius of the electron beam) the phase $\tilde{\psi}$ is very nearly a function of z and ψ_0 only. With these simplifying assumptions, equation (24) can be integrated to give

$$a_{ex}(r, z) = -\frac{i}{4} \frac{\omega_b^2/c^2}{\gamma_0} r_b^2 \int_0^{2\pi} \frac{d\psi_0}{2\pi} \int_0^z dz' A_w(z') e^{i\varphi(z')} \quad (25)$$

$$\left[\frac{z - z' + iz_b}{(z - z')^2 + z_b^2} \right] \exp -i \left[\tilde{\psi}(z', \psi_0) - z_b \left(\frac{z - z' + iz_b}{(z - z')^2 + z_b^2} \right) \frac{r^2}{r_b^2} \right]$$

where $z_b = r_b^2 \omega/2c$ is the effective Rayleigh length associated with the excited radiation. The excited radiation can be written in a more familiar form,

$$A_{ex}(r, z, t) = \frac{\omega_b^2 r_b^2}{4c^2 \gamma_0} \int_0^{2\pi} \frac{d\psi_0}{2\pi} \int_0^z dz' A_w(z') \frac{e^{-\frac{z_b^2 r^2/r_b^2}{(z - z')^2 + z_b^2}}}{\sqrt{(z - z')^2 + z_b^2}} \quad (26)$$

$$\cos \left[\frac{\omega}{c} z - \omega t - \tan^{-1} \left(\frac{z - z'}{z_b} \right) + \frac{z_b(z - z')}{(z - z')^2 + z_b^2} \left(\frac{r^2}{r_b^2} \right) \right]$$

$$- \tilde{\psi}(z', \psi_0) + \varphi(z') \Big] \hat{e}_x.$$

The excited radiation has a very simple interpretation. Each cross section of the electron beam produces an Gaussian like TEM_{00} radiation beam (see Eq. (21)) propagating to the right with the minimum spot size equal to the electron beam radius. The total excited radiation at a location $z = L$ down stream is the sum of all the Gaussian radiation beams which originated from $z = 0$ to L , see Fig. 2.

A square or Lorentzian electron beam profile may also be readily integrated in (24). The 1-D limit of (26) is obtained by letting z_b or r_b approach infinity.

We will now make the constant phase, resonant particle approximation. In this approximation all particles are assumed to have the same constant phase, $\tilde{\psi}_R$. The electron beam in this approximation consists of a pulse train of macro particles separated in distance by $2\pi v_{0z}/\omega$. Furthermore, we will limit ourselves at this point to a constant parameter wiggler and consider only an external D.C. electric potential. The rate of change, on axis, of the resonant particle energy is

$$\frac{\partial(\gamma_R m_0 c^2)}{\partial z} = |e| \frac{\partial \phi_{DC}(z)}{\partial z} - \frac{|e|^2 \omega / c}{2\gamma_R m_0 c^2} A_w A_R(r=0, z) \cos \tilde{\psi}_R. \quad (27)$$

To obtain the total radiation field, we first evaluate $a_{ex}(r, z)$ under the assumption that $|\varphi| \ll 1$ (this will be shown later to be valid). The excited resonant particle radiation a_{ex} for all r and z is

$$a_{ex}(r, z) = -i \alpha_0^2 A_w \left[E_i \left(\frac{-r^2}{r_b^2} \right) - E_i \left(\frac{-r^2}{r_b^2} \frac{z_b^2 - i z_b z}{z_b^2 + z^2} \right) \right] \exp(-i \tilde{\psi}_R) \quad (28)$$

where $\alpha_0 = \omega_b r_b / 2c \sqrt{\gamma_0}$ and E_i is the exponential integral function. The derivation of (28) is given in Appendix II. The exponential integral function E_i can be written in series forms (see Appendix III). The amplitude and phase of the *total* field, near the axis $r \leq r_b$, are

$$A_R(r, z) = A_{in} + \alpha_0^2 A_w \left[\left[\tan^{-1} \left(\frac{z}{z_b} \right) + \zeta_i \right] \cos \tilde{\psi}_R - \left[\ln \left(\frac{z^2 + z_b^2}{z_b^2} \right)^{1/2} + \zeta_r \right] \sin \tilde{\psi}_R \right], \quad (29a)$$

$$\phi(r, z) = -\alpha_0^2 (A_w / A_R) \left[\left[\tan^{-1} \left(\frac{z}{z_b} \right) + \zeta_i \right] \sin \tilde{\psi}_R + \left[\ln \left(\frac{z^2 + z_b^2}{z_b^2} \right)^{1/2} + \zeta_r \right] \cos \tilde{\psi}_R \right], \quad (29b)$$

where $A_{in} = |a_{in}|$, $\zeta_r = \text{Re}(\zeta)$, $\zeta_i = \text{Im}(\zeta)$ and

$$\zeta = \sum_{n=1}^{\infty} \frac{(-1)^n (r/r_b)^{2n}}{n n!} \left[1 - \left(\frac{z_b}{z^2 + z_b^2} \right)^n (z_b - iz)^n \right].$$

The stationary phase $\tilde{\psi}_R$ is obtained from (12). We notice that in the absence of any efficiency enhancement schemes, the constant resonant phase $\tilde{\psi}_R = -\pi/2$ is stationary. The resonant particle energy also remain constant, see Eq. (27). According to (29a), however, the total radiation field amplitude increases on axis and is given by

$$A_R(r=0, z) = A_{in} + \alpha_0^2 A_w \ln((z^2 + z_b^2)/z_b^2)^{1/2}.$$

The growth of the total radiation field on axis is due to refraction. The index of refraction, in this case, is greater than unity, $n = 1 + (c/\omega)\partial\varphi/\partial z > 1$ over the electron beam, hence the input field tends to focus while the electron beam will defocus. The net radiation energy flux along the z axis (integrated from $r = 0$ to $r = \infty$) is constant (to be shown in the next section), since for large r the radiation amplitude is less than the input amplitude.

V. POWER GAIN AND EFFICIENCY

The increase in total radiation power comes either from the kinetic energy of the electron beam or from the applied D.C. electric field. The increase in the radiation energy flux is

$$\Delta S_R(x, y, z) = \frac{c(\omega^2/c^2)}{8\pi} (a^2(x, y, z) - a^2(x, y, 0)) \hat{e}_z \quad (30)$$

where $a = a_{in} + a_{ex}$. For the low gain limit, i.e. $|a_{in}| \gg |a_{ex}|$,

$$\Delta S_R = \frac{c(\omega^2/c^2)}{8\pi} A_{in} (a_{ex} + a_{ex}^*) \hat{e}_z \quad (31)$$

and total power gain is

$$\Delta P_R(z) = \frac{c}{8\pi} \left(\frac{\omega^2}{c^2} \right) A_{in} \int_0^\infty \int_0^{2\pi} a_{ex} r dr d\theta + \text{c.c.} \quad (32)$$

where a_{ex} is found in Eq. (24). The integrals in Eq. (32) can be evaluated analytically with the following simplifying assumptions: $|\varphi| \ll 1$, and that $\tilde{\gamma}'$ and $\tilde{\psi}'$ are independent of transverse coordinates over the cross sectional areas of the electron beam. Furthermore, if r_b satisfies Eqs. (6) and (10) and $k_w r_b \ll 1$, we can neglect the gradient in the wiggler, and replace \tilde{x} , \tilde{y} in Eq. (32) by x_0 , y_0 and $\sigma(v_{y0})$ by $\delta(v_{y0})$. To evaluate Eq. (32), we will write $x = r \cos \theta$, $y = r \sin \theta$, $x_0 = r_0 \cos \theta_0$, and $y_0 = r_0 \sin \theta_0$. Integrating over all angles, we find that

$$\Delta P_R(z) = -i \frac{c}{16\pi} \left(\frac{\omega_b^2}{c^2} \right) \left(\frac{\omega^2}{c^2} \right) A_{in} \int_0^z dz' \int_0^{2\pi} \frac{d\psi_0}{2\pi} \int_0^\infty r_0 dr_0 \quad (33)$$

$$\int_0^{2\pi} d\theta_0 \theta(r_0, \theta_0) \frac{A_w'}{\tilde{\gamma}'} \int_0^\infty r dr \frac{e^{i(r^2+r_0^2)\frac{\omega/c}{2(z-z')}}}{z-z'} J_0 \left(\frac{rr_0\omega/c}{z-z'} \right) e^{-i\tilde{\psi}}.$$

After integrating over all radii, the total power gain given by (33) becomes

$$\Delta P_R = \frac{\omega A_{in}}{8\pi} \frac{\omega_b^2}{c^2} \int_0^z dz' \int_0^{2\pi} \frac{d\psi_0}{d\pi}$$

$$\int_{-\infty}^{\infty} dx_0 \int_{-\infty}^{\infty} dy_0 \theta(x_0, y_0) \frac{A_w'}{\tilde{\gamma}'} \cos \tilde{\psi}'. \quad (34)$$

For a Gaussian beam profile for the electron beam, i.e., $\theta(x_0, y_0) = \exp - (x_0^2 + y_0^2)/r_b^2$, and assuming that all the particles have the same stationary resonant phase $\tilde{\psi}_R$, the total power gain is

$$\Delta P_R = \frac{c(\omega/c)}{8\pi} \frac{\omega_b^2}{c^2} \pi r_b^2 \frac{A_w A_{in}}{\gamma_R} z \cos \tilde{\psi}_R. \quad (35)$$

Let us apply ΔP_R to $\cos \tilde{\psi}_R = 0$ ($\tilde{\psi}_R = -\pi/2$), for which case the electrons do not lose any kinetic energy. Even though the radiation amplitude grows on axis, the total radiation energy flux is constant $\Delta P_R = 0$, consistent with the fact that electrons remains at the same kinetic energy. The increase in the radiation amplitude on axis is due to refraction effects at the expense of a corresponding decrease in the off axis radiation field.

To complete our formulation of the FEL, we need an expression for the efficiency,

$$\eta = \frac{\Delta P_R}{v_{z0} n_0 (\gamma_0 - 1) m_0 c^2 \int_{-\infty}^{\infty} dx_0 \int_{-\infty}^{\infty} dy_0 \theta(x_0, y_0)}. \quad (36)$$

If a D.C. electric field is applied for efficiency enhancement, the trapped electrons do not change their kinetic energy. The radiation power gain, in this case, originates from the energy flux due to the D.C. electric field crossed with the self-magnetic field, i.e., $-\frac{\partial \phi_{DC}}{\partial z} \hat{e}_z \times \mathbf{B}_{self}$, which is in the radial direction flowing inward toward the electron beam.

The electric field required to maintain a stationary resonant phase $\tilde{\psi}_R$, based on Eq. (27), is

$$\frac{\partial \phi_{DC}}{\partial z} = \frac{1}{2} \left(\frac{|e|}{m_0 c^2} \right) \frac{\omega/c}{\gamma_R} A_w A_R(r=0, z) \cos \tilde{\psi}_R.$$

For a resonant macro particle, the efficiency can also be written as

$$\eta = |e| (\phi_{DC}(z) - \phi_{DC}(0)) / \gamma_0 m_0 c^2$$

or

$$\eta = - \left(\frac{|e|}{m_0 c^2} \right)^2 \frac{\omega/c}{2\gamma_0^2} \int_0^z A_w A_R(r=0, z') \cos \tilde{\psi}_R dz', \quad (37)$$

which is the same as Eq. (36) together with Eq. (35).

VI. NUMERICAL EXAMPLE

As an example of a 10.6 μm FEL utilizing a CO_2 laser as an input field, we choose an electron beam of energy 25 MeV ($\gamma_0 = 50$), current of $I = 5$ A and radius (Gaussian profile) of $r_b = 0.5$ mm. Such a beam has a peak density on axis of $n_0 = 1.3 \times 10^{11} \text{ cm}^{-3}$ ($\omega_b = 2.0 \times 10^{10} \text{ sec}^{-1}$). The constant parameter wiggler has a magnitude of $B_w = 5.0$ kG and wavelength of $\lambda_w = 2.8$ cm which gives $A_w = 2.2 \times 10^3$ statvolts. The wiggler velocity is $v_{01} = 2.6 \times 10^{-2}c$ and the input CO_2 power density is taken to the $P_{in} = 4 \times 10^8 \text{ W/cm}^2$ which gives $A_{in} = 0.30$ statvolts. Note that the inequalities in (3) and (10) are well satisfied.

Our first illustration makes the resonant macro particle approximation and is one in which the applied D.C. electric potential is zero, hence, $\tilde{\psi}_R = -\pi/2$ and the particle energy remains constant. The curves in Figs. 3a,b and 4a,b are the numerical results of Eq. (28). Figure 3a shows the gain,

$$G(r,z) = (A_R(r,z) - A_{in})/A_{in} \quad (38)$$

as a function of radius at $z = 20$ cm, 1 m and 2 m; and Fig. 3b shows the gain as a function of axial position z at various radial positions, i.e., $r = 0$, $r = r_b$, $r = 3r_b$ and $r = 5r_b$. The gain in the radiation amplitude at $z = 2$ m is maximum on axis and equal to 0.14.

Figure 4a shows the radial cross section of total radiation phase φ at $z = 20$ cm, 1 m and 2 m; and Fig. 4b shows the total radiation phase φ as a function of axial position at various radial positions. The maximum value of φ is along the z axis and is approximately 0.06 rad which certainly satisfies our approximation used in (25) to obtain (28). The index of refraction, in this case, is greater than unity, $n = 1 + (c/\omega)\partial\varphi/\partial z > 1$ over the electron beam, hence the input field tends to focus while the electron beam will defocus. The net radiation energy flux along the z axis (integrated from $r = 0$ to $r = \infty$) is constant, since for large r the radiation amplitude is less than the input amplitude.

Our next illustration still assumes resonant macro particles, but will include an applied D.C. electric potential $\phi_{DC}(z)$ such that $\cos \tilde{\psi}_R = 0.6$. Figures 5 a,b and 6 a,b are the numerical results of Eq. (28) for this example. The gain in radiation amplitude on axis at $z = 2$ m is 0.15, see Fig. 5. The efficiency at the end of $z = 2$ m is $\sim 3.6\%$. Figure 6a shows the phase φ as a function of radius, and Fig. 6b shows the phase φ as a function of z . For large z , n is less than unity on axis (defocusing) and becomes greater than unity for large r (focusing).

For our last example, we will not apply the stationary resonant phase approximation. Instead we take the electrons to enter the interaction region with a uniform distribution in initial phase ψ_0 . The wiggler amplitude is tapered to enhance the efficiency, $B_w(z) = B_w(0)(1 - \alpha z)$, where $\alpha = 0.0003 \text{ cm}^{-1}$. The form of the applied wiggler field is such that one particle is maintained at approximately constant phase,

$$\cos \psi_R = - (2k_w A_R)^{-1} \frac{dA_w}{dz} = 0.5.$$

Figure 7 is a plot of gain calculated from (26) as a function of axial position for $r = 0$, $r = r_b$ and $r = 3r_b$. The oscillations are due to the particles bouncing in the ponderomotive potential wells. The efficiency as a function of z , Eq. (36), is plotted in Fig. 8.

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Appendix I
BETATRON OSCILLATIONS DUE TO TRANSVERSE GRADIENT
OF THE WIGGLER FIELD

This appendix will obtain the particle's transverse motion (5a) and the axial velocity spread (7) inside a linearly polarized realizable wiggler field. For the illustrative purposes here, we will assume that the wiggler amplitude and wavelength are constant in the axial direction. The vector potential of the wiggler field is

$$\mathbf{A}_w(y,z) = A_w \cosh(k_w y) \cos(k_w z) \hat{e}_x. \quad (\text{I.1})$$

The associated wiggler magnetic field has a z component off the axis, in addition to the y component,

$$\mathbf{B}_w(y,z) = -A_w k_w [\cosh(k_w y) \sin(k_w z) \hat{e}_y + \sinh(k_w y) \cos(k_w z) \hat{e}_z]. \quad (\text{I.2})$$

For particle trajectories in the transverse directions, it is sufficient to assume that their motion is effected by the wiggler field alone, i.e., $\mathbf{P}_x(y,z) \approx \frac{|e|\hbar}{c} \mathbf{A}_w$.

The particle location in the x -direction can be obtained by integrating the momentum in the x direction.

$$\bar{x} = x_0 + \frac{\beta_{0x}}{k_w} \cosh(k_w \bar{y}) \sin k_w z \quad (\text{I.3})$$

where \bar{x} and \bar{y} are functions of $(z, \psi_0, x_0, y_0, v_{y_0})$, x_0 and y_0 are the initial transverse coordinates, v_{y_0} is the initial transverse velocity in the y -direction, and ψ_0 is the initial phase of the electron in the ponderomotive potential well at the entrance to the interaction region, i.e., $z = 0$.

The particle motion in the y -direction is due to the z component of the wiggler field,

$$\frac{dP_y}{dt} = \frac{|e|\hbar}{c} v_x B_z. \quad (\text{I.4})$$

We will assume that the fast oscillatory terms, with wavelength half the wiggler wavelength, are unimportant (see Ref. (14)), and replace v_x by c at appropriate places. We find that

$$\frac{d^2 y}{dz^2} + \frac{\beta_{0z}^2}{4} k_w \sinh 2k_w y = 0 \quad (I.5)$$

where $\beta_{0z} = |e|A_w/(\gamma_0 m_0 c^2)$. This equation can be integrated once to give

$$\frac{dy}{dz} = \left[\frac{\beta_{0z}^2}{4} (\cosh(2k_w y_0) - \cosh(2k_w y)) + \left(\frac{v_{y0}}{c}\right)^2 \right]^{1/2}. \quad (I.6)$$

To find an explicit solution of y as a function of z , we expand \cosh in Taylor series around zero, and keep only the first two terms of the expansion. Then, Eq. (I.6) can be rewritten as

$$z = \frac{\sqrt{2}}{\beta_{0z} k_w} \int_{y_0}^y \left[2 \left(\frac{v_{y0}/c}{\beta_{0z} k_w} \right)^2 + y_0^2 - y^2 \right]^{1/2}. \quad (I.7)$$

The results of the integral can be put into the following form

$$\begin{bmatrix} \bar{y} \\ \bar{v}_y \end{bmatrix} = \begin{bmatrix} \cos K_0 z & (K_0 c)^{-1} \sin K_0 z \\ -K_0 c \sin K_0 z & \cos K_0 z \end{bmatrix} \begin{bmatrix} y_0 \\ v_{y0} \end{bmatrix} \quad (I.8)$$

where $K_0 = \beta_{0z} k_w / \sqrt{2}$ is the wavenumber of the betatron oscillations. An equally convenient form for \bar{y} is

$$\bar{y} = y_B \cos(K_0 z - \phi_B) \quad (I.9)$$

where

$$y_B = \left[2 \left(\frac{v_{y0}/c}{\beta_{0z} k_w} \right)^2 + y_0^2 \right]^{1/2} \quad (I.10)$$

is the amplitude of the betatron oscillation and

$$\phi_B = \cos^{-1}(y_0/y_B) \quad (I.11)$$

is the initial phase of the betatron oscillation.

We will now show that the axial velocity of the particles decrease as the amplitude of the betatron oscillations increase. This results in an equivalent energy spread. For illustrative purposes, we will consider a cold electron beam with total energy $\gamma_0 m_0 c^2$. The axial velocity is found to be

$$\begin{aligned} \left(\frac{v_z}{c} \right)^2 &= \frac{\gamma_0^2 - 1}{\gamma_0^2} - \beta_{0z}^2 [\cosh^2(k_w y) \cos^2(k_w z) \\ &+ 1/4 (\cosh(2k_w y_0) - \cosh(2k_w y))] - \left(\frac{v_{y0}}{c} \right)^2. \end{aligned} \quad (I.12)$$

In the derivation of (1.12), we have used $v_y/c = dy/dz$ from (1.6) and $v_x/c = P_x/(\gamma_0 m_0 c)$. We will again drop terms that oscillate at twice the wiggler wavenumber. We obtain $v_z = v_{z0} - \Delta v_z$, where $v_{z0} = v_0 - \beta_{0L}^2 c/4$ (the mean axial velocity in the absence of the betatron oscillation in a non-realizable wiggler field without transverse gradient) is the axial velocity of the electron travelling on axis in a realizable wiggler field, and $\Delta v_z = c(\beta_{0L} k_w y_B/2)^2$ is the amount that the axial velocity is reduced by for particles executing betatron oscillations with oscillation amplitude y_B . Since the axial velocity spread is proportional to the radial excursion, the maximum axial velocity spread, due to betatron oscillation alone, is

$$\Delta v_z = c(\beta_{0L} k_w r_b/2)^2 \quad (1.13)$$

where r_b is the radius of the electron beam.

Appendix II
DERIVATION OF THE EXCITED RADIATION FIELD IN THE
RESONANT PARTICLE LIMIT

The details of the derivation of the excited resonant particle radiation field, Eq. (28), will be given here. The excited radiation field, for the electron beam with all initial phase ψ_0 , is given by (25). In the constant phase, resonant particle limit,

$$\int_0^{2\pi} \frac{d\psi_0}{2\pi} e^{-i\tilde{\psi}(z'; \psi_0)} = e^{-i\tilde{\psi}_R}$$

where all the particles have the same phase $\tilde{\psi}_R$. We can now rewrite (25) as

$$a_{ex}(r, z) = -i\alpha_0^2 A_w I(r, z) e^{-i\tilde{\psi}_R}, \quad (\text{II.1})$$

where

$$I(r, z) = \int_0^z dz' \left[\frac{(z-z') + iz_b}{(z-z')^2 + z_b^2} \right] \exp \left[iz_b \frac{r^2}{r_b^2} \left(\frac{z-z'+iz_b}{(z-z')^2 + z_b^2} \right) \right], \quad (\text{II.2})$$

and $\alpha_0 = \omega_b r_b / (2c\sqrt{\gamma_0})$. The integral (I.2) can be rearranged into the following form

$$I = -i \frac{r_b^2}{z_b} \frac{\partial}{\partial r^2} \int_0^z dx \exp \left[i \frac{r^2}{r_b^2} \left(\frac{z_b}{x-iz_b} \right) \right] \quad (\text{II.3})$$

where $x = z - z'$. We make another change of variables, $q = -iz_b/(x-iz_b)$, and we find

$$I = - \int_1^{-i \frac{z_b}{z-iz_b}} f \left(\frac{r^2}{r_b^2}, q \right) dq \quad (\text{II.4})$$

where

$$f(b, q) = \frac{1}{q} \exp(-bq). \quad (\text{II.5})$$

Since the function $f(b, q)$ satisfies the Cauchy-Riemann condition, we can evaluate the integral in (II.4) by changing the contour of integration to that below

$$I = - \int_1^\infty f \left(\frac{r^2}{r_b^2}, q \right) dq - \int_\infty^{-i \frac{z_b}{z-iz_b}} f \left(\frac{r^2}{r_b^2}, q \right) dq. \quad (\text{II.6})$$

Let $p = \frac{z - iz_b}{-iz_b} q$ in the second integral, we can rewrite (II.6) as

$$I = - \int_1^\infty f\left(\frac{r^2}{r_b^2}, q\right) dq + \int_1^\infty f\left(\frac{r^2}{r_b^2} \frac{z_b(z_b - iz)}{z_b^2 + z^2}, p\right) dp \quad (\text{II.7})$$

Since

$$E_i(-b) = - \int_1^\infty f(b, q) dq, \quad (\text{II.8})$$

we obtain (28),

$$a_{ex}(r, z) = -i\alpha_0^2 A_w \left[E_i\left(\frac{-r^2}{r_b^2}\right) - E_i\left(\frac{-r^2}{r_b^2} \left(\frac{z_b^2 - iz_b z}{z_b^2 + z^2}\right)\right) \right] \exp(-i\bar{\psi}_R), \quad (\text{II.9})$$

where E_i is the exponential integral function.

Appendix III
THE AMPLITUDE AND PHASE OF THE TOTAL FIELD IN THE
RESONANT PARTICLE LIMIT

This appendix will derive the amplitude and phase of the total field (Eqs. (29a, b)) from the excited radiation field, (Eq. (28)). The complex amplitude of excited radiation field can be written as

$$a_{ex}(r, z) = -i\alpha_0^2 A_w I(r, z) \exp(-i\bar{\psi}_R) \quad (\text{III.1})$$

where

$$I = E_i \left[-\frac{r^2}{r_b^2} \right] - E_i \left[-\frac{r^2}{r_b^2} \frac{z_b^2 - iz_b z}{z_b^2 + z^2} \right], \quad (\text{III.2})$$

$\alpha_0 = \omega_b r_b / (2c\sqrt{\gamma_0})$, and E_i is the exponential integral function. The function can be evaluated using the series representation

$$E_i(x) = C + \ln(-x) + \sum_{n=1}^{\infty} \frac{x^n}{nn!} \quad (x < 0) \quad (\text{III.3})$$

where C is the Euler's constant. Applying (III.3) to (III.2), we obtain

$$I = \ln \left[\frac{z^2 + z_b^2}{z_b^2} \right]^{1/2} + i \tan^{-1} \left[\frac{z}{z_b} \right] + \sum_{n=1}^{\infty} \frac{(-1)^n (r/r_b)^{2n}}{nn!} \left[1 - \left(\frac{z_b}{z^2 + z_b^2} \right)^n (z_b - iz)^n \right]. \quad (\text{III.4})$$

when $r^2/r_b^2 \gg 1$, an asymptotic expansion for E_i is more appropriate,

$$E_i(-\xi) = -\frac{e^{-\xi}}{\xi} \left[1 - \frac{1}{\xi} + \frac{2!}{\xi^2} - \frac{3!}{\xi^3} + \dots \right] \quad [\xi \gg 1]. \quad (\text{III.5})$$

The asymptotic expansion for (III.2) becomes

$$I = -\frac{\exp(-r^2/r_b^2)}{r^2/r_b^2} \left[1 + \sum_{n=1}^{\infty} \frac{(-1)^n n!}{(r/r_b)^{2n}} \right] + \frac{\exp(-\rho)}{\rho} \left[1 + \sum_{n=1}^{\infty} \frac{(-1)^n n!}{\rho^n} \right] \quad (\text{III.6})$$

where

$$p = \left(\frac{z_b}{z_b + lz} \right) \left(\frac{r^2}{r_b^2} \right).$$

We have defined

$$a_R = A_R e^{i\varphi} = a_{in} + a_{ex}$$

where a_R is the complex amplitude of the total radiation field, A_R and φ are the amplitude and phase of the total radiation field, $a_{in} = A_{in}$ is the amplitude of the input radiation field. In the limit that $|\varphi| \ll 1$, we can write

$$A_R = A_{in} + \alpha_0^2 A_w [I_i \cos \tilde{\psi}_R - I_r \sin \tilde{\psi}_R] \quad (\text{III.7a})$$

$$\varphi = -\alpha_0^2 \frac{A_w}{A_R} [I_i \sin \psi_R + I_r \cos \tilde{\psi}_R] \quad (\text{III.7b})$$

where $I_r = \text{Re}(I)$, $I_i = \text{Im}(I)$. For $r^2/r_b^2 \leq 1$, A_R and φ can be rewritten as (29a, b).

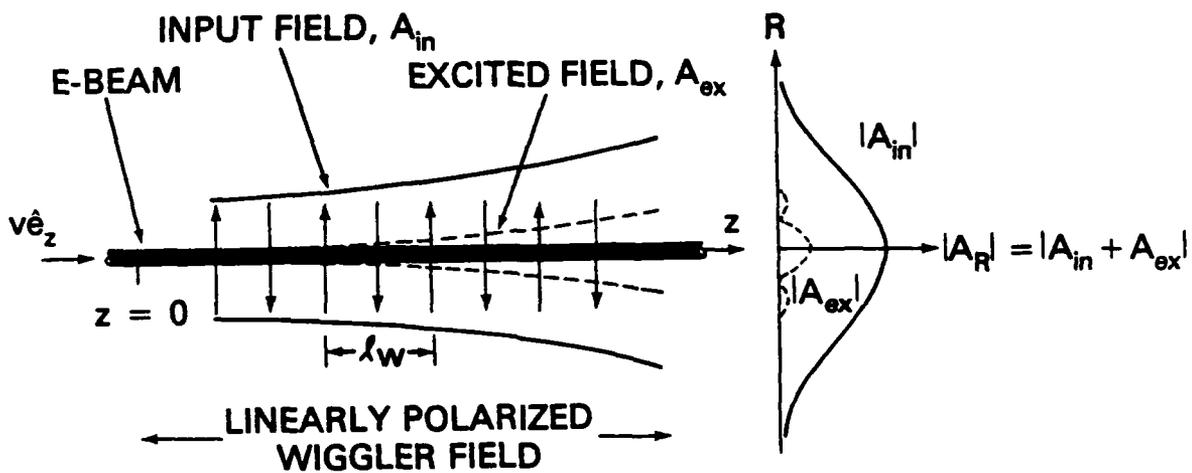


Fig. 1 -- Schematic of electron and radiation beams in 3-D FEL amplifier configuration.

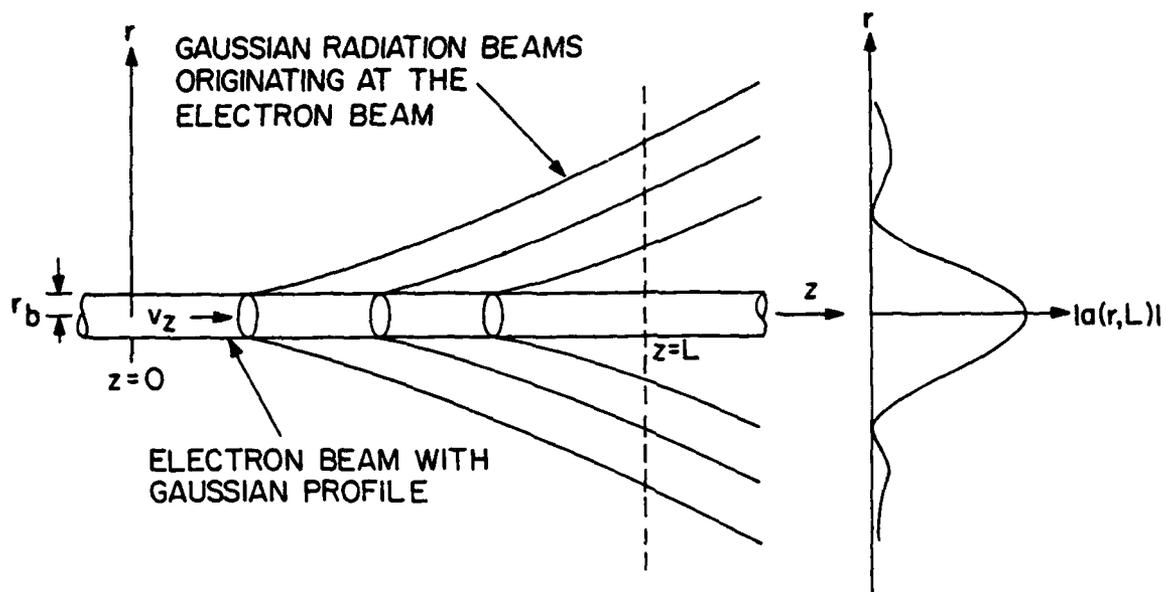


Fig. 2 — Schematic interpretation of the excited radiation. Gaussian like TEM_{00} radiation beams with the minimum spot size equal to the electron beam radius are continuously produced at each cross section of the electron beam. The total excited radiation at a location $z = L$ down stream is the sum of all the Gaussian radiation beams which originated from $z = 0$ to $z = L$.

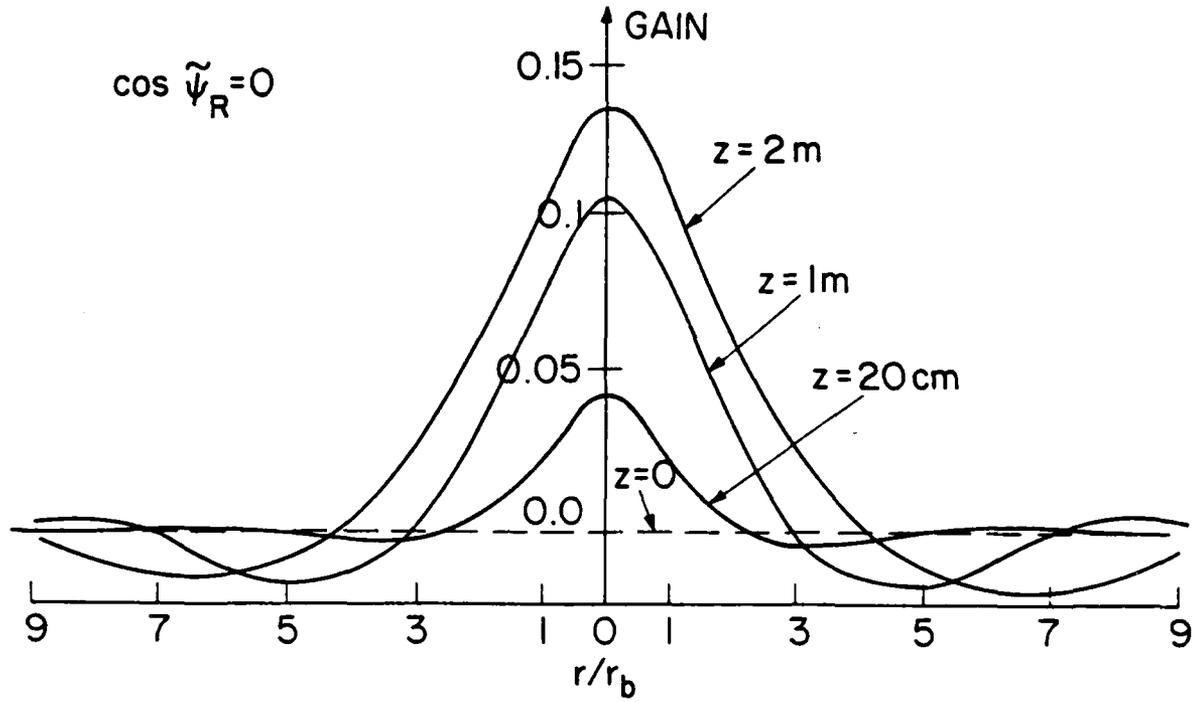


Fig. 3a — Gain as a function of radius at $z = 20\text{ cm}$, 1 m and 2 m for resonant particles with $\cos \tilde{\psi}_R = 0$.

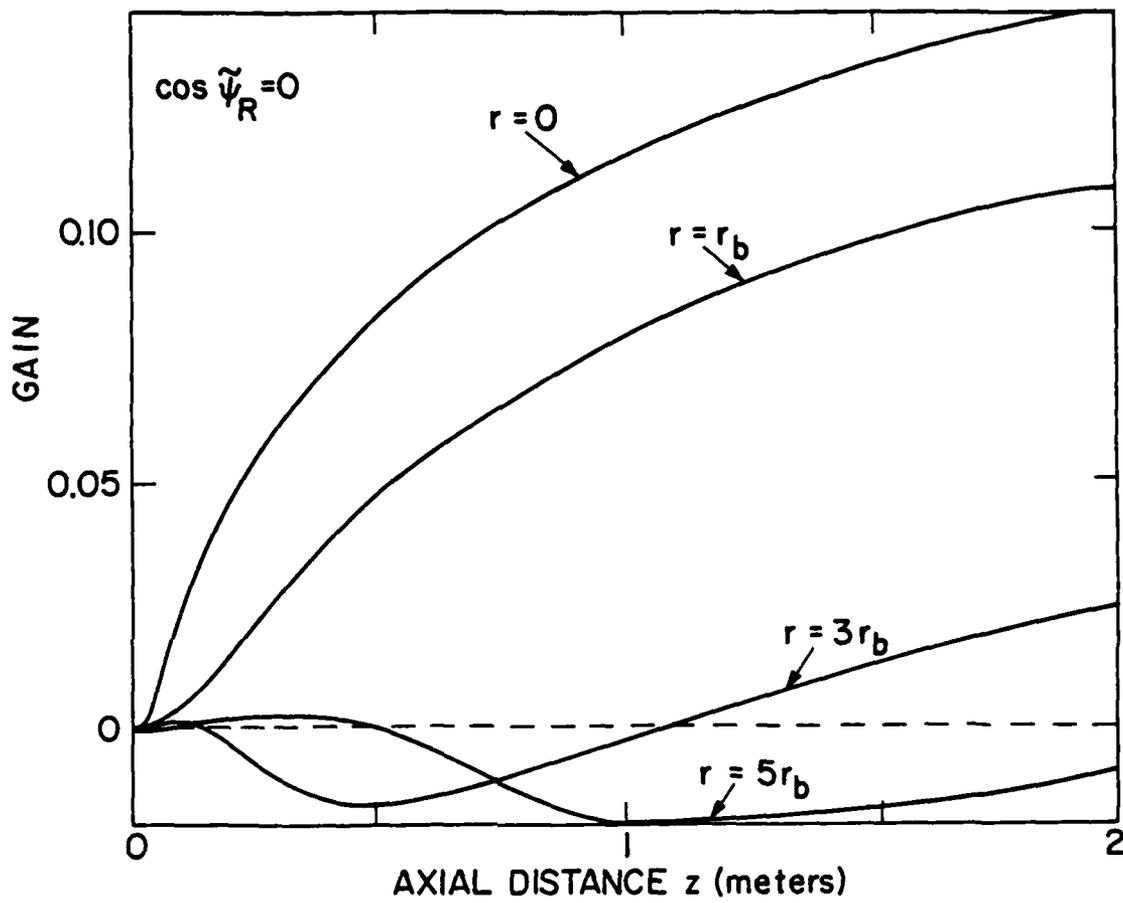


Fig. 3b — Gain as a function of z at various radial positions for resonant macro particles with $\cos \psi_R = 0$.

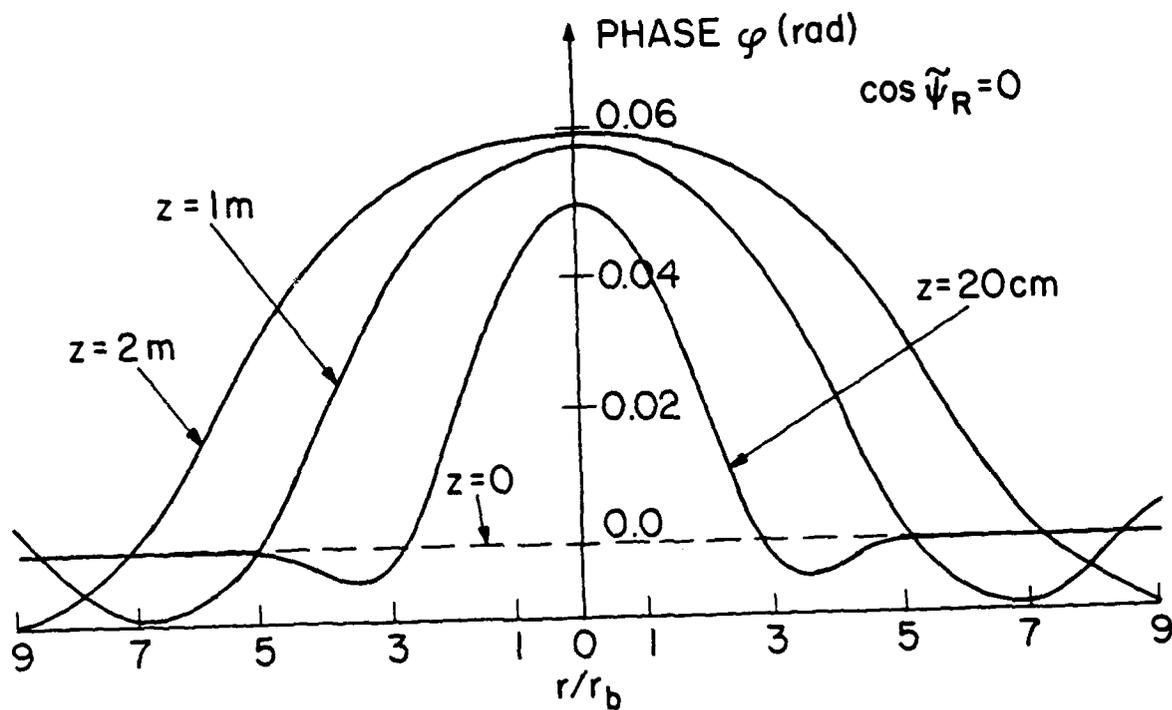


Fig. 4a - Total radiation phase, φ , as a function of radius at $z = 20\text{cm}$, 1m and 2m for resonant macro particles with $\cos \tilde{\psi}_R = 0$.

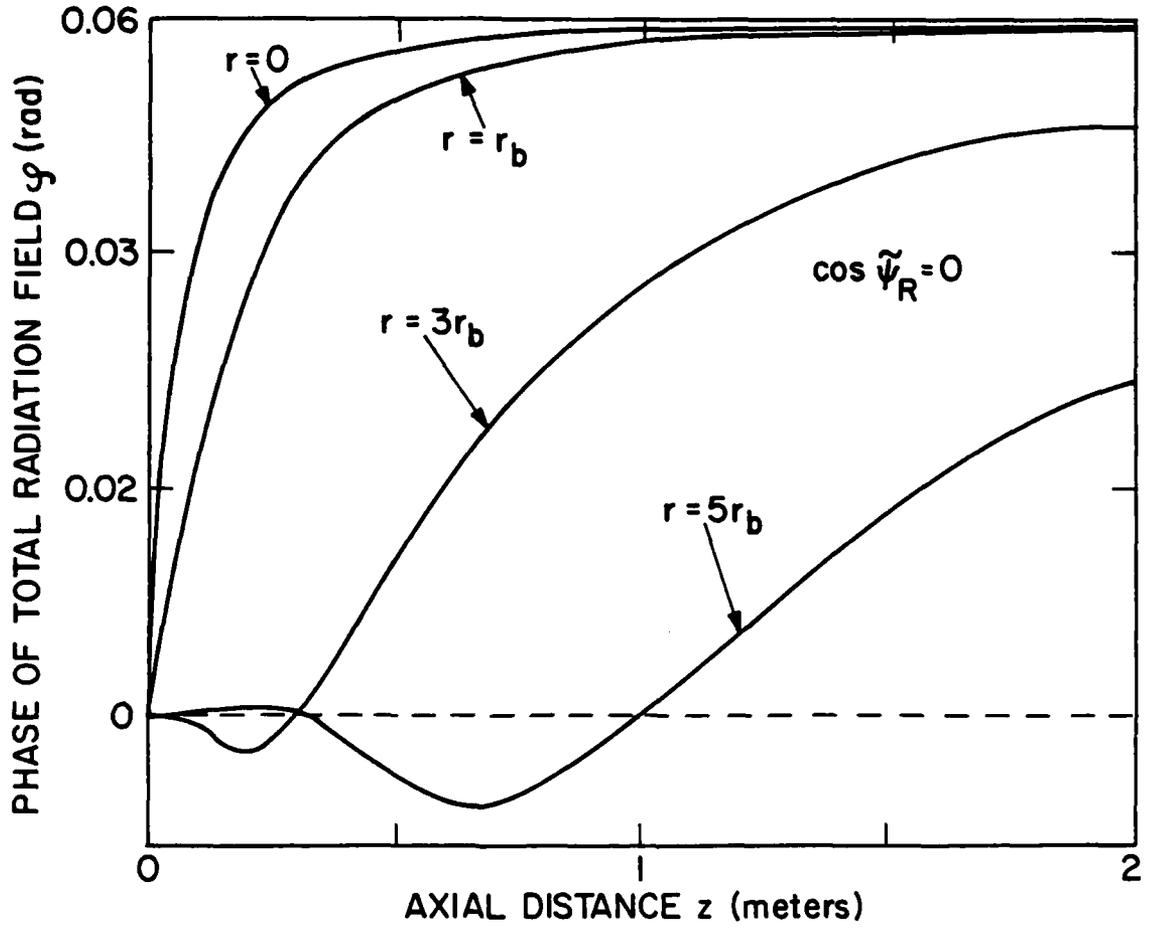


Fig. 4b - Total radiation phase, φ , as a function of z at various radial positions for resonant macro particles with $\cos \tilde{\psi}_R = 0$.

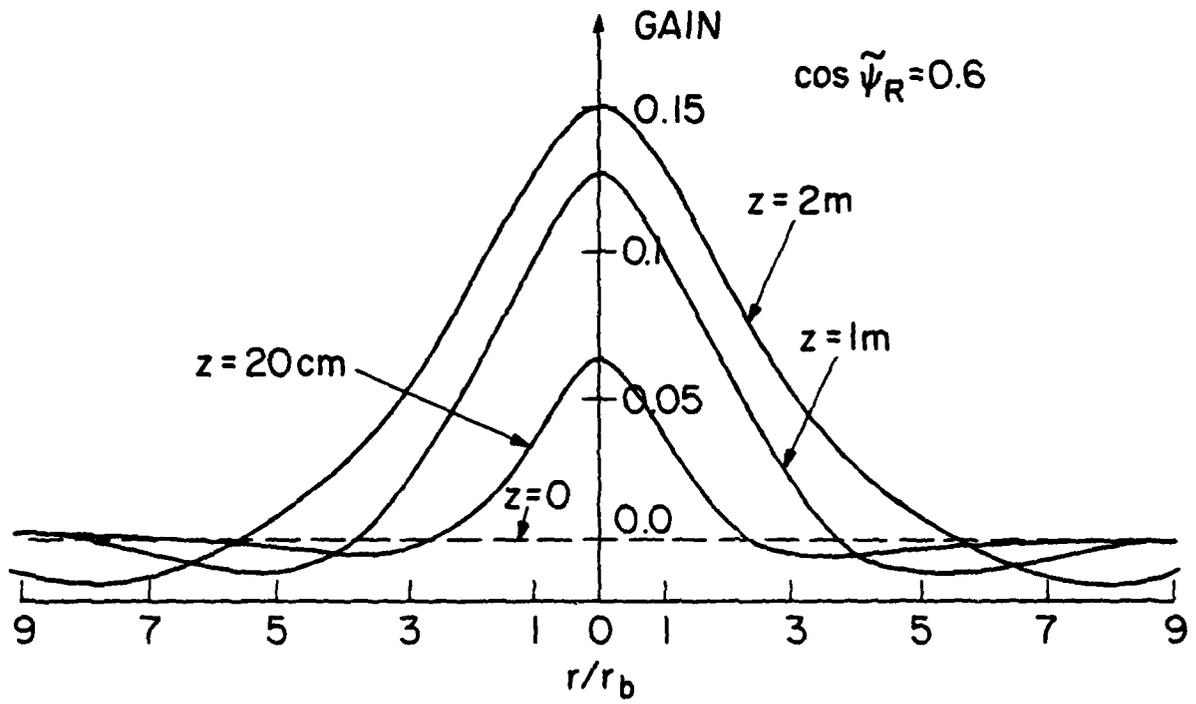


Fig. 5a - Gain as a function of radius at $z = 20cm, 1m$ and $2m$ for resonant macro particles with $\cos \tilde{\psi}_R = 0.6$.

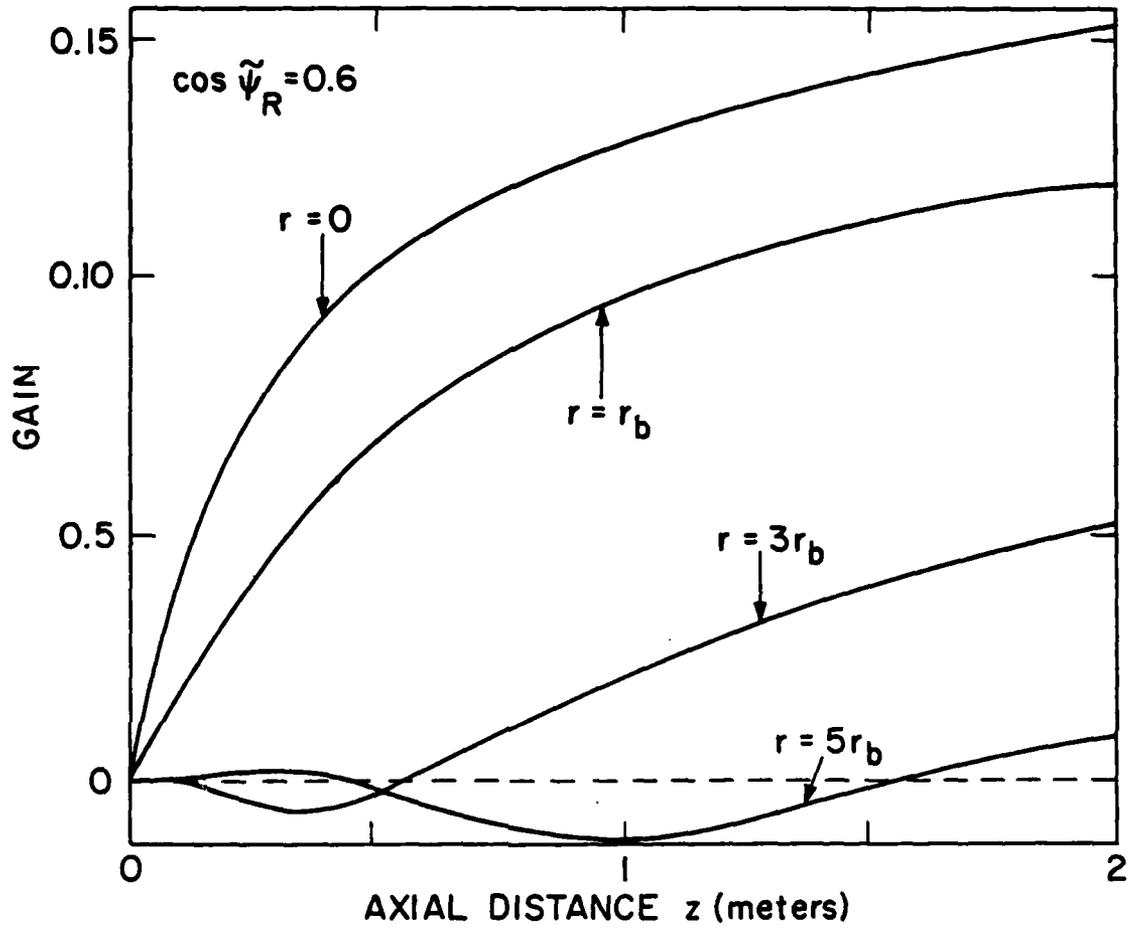


Fig. 5b - Gain as a function of z at various radial positions for resonant macro particles with $\cos \tilde{\psi}_R = 0.6$.

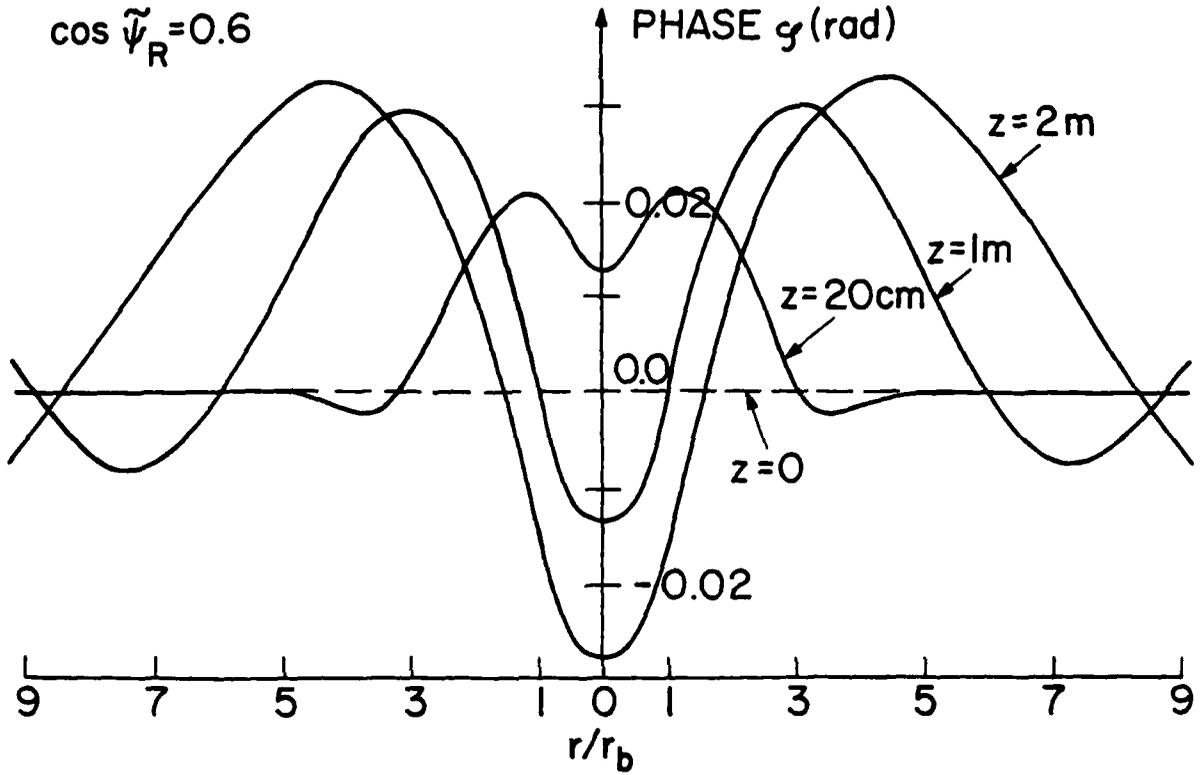


Fig. 6a — Total radiation phase, φ , as a function of radius at $z = 20\text{cm}$, 1m and 2m for resonant macro particles with $\cos \tilde{\psi}_R = 0.6$.

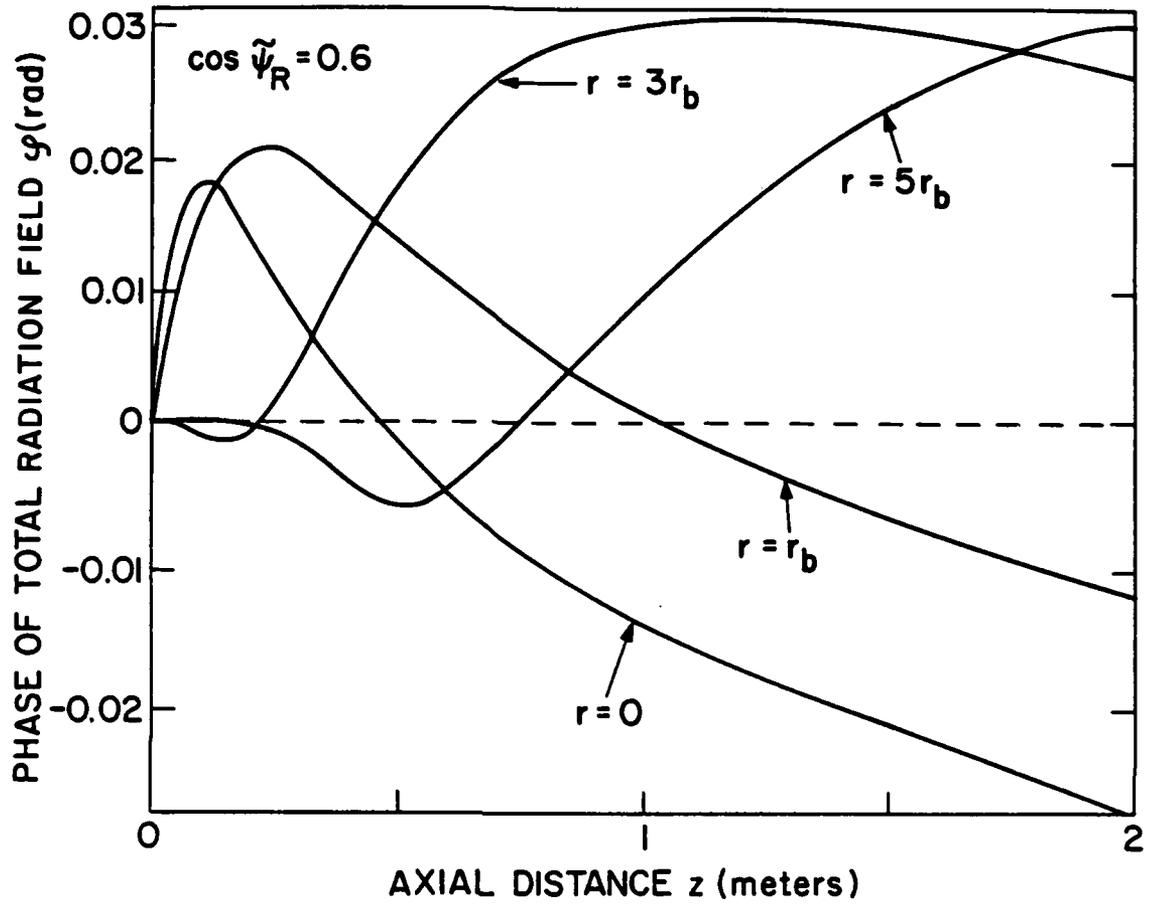


Fig. 6b — Total radiation phase, φ , as a function of z at various radial positions for resonant macro particles with $\cos \tilde{\psi}_R = 0.6$.

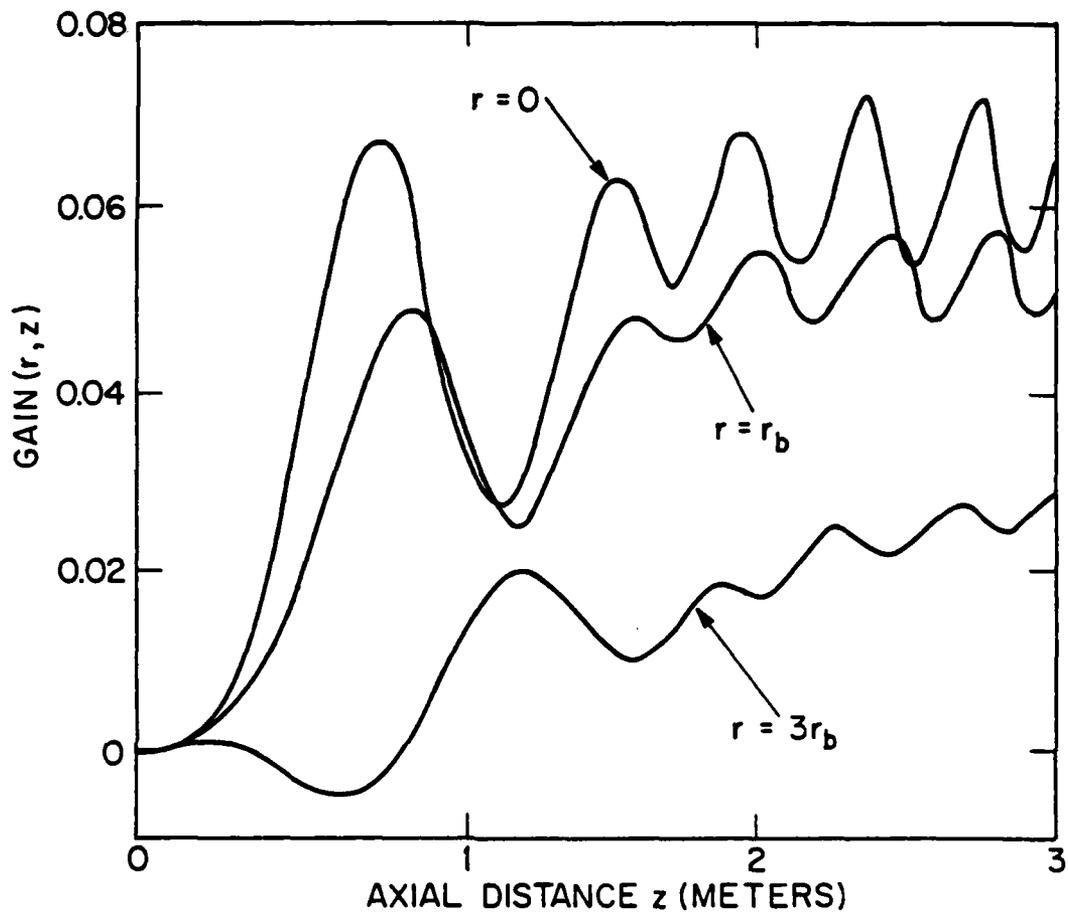


Fig. 7 — Gain as a function of z at $r = 0$, $r = r_b$ and $r = 3r_b$ for electron beam with uniform distribution of initial phase ψ_0 in a tapered wiggler field.

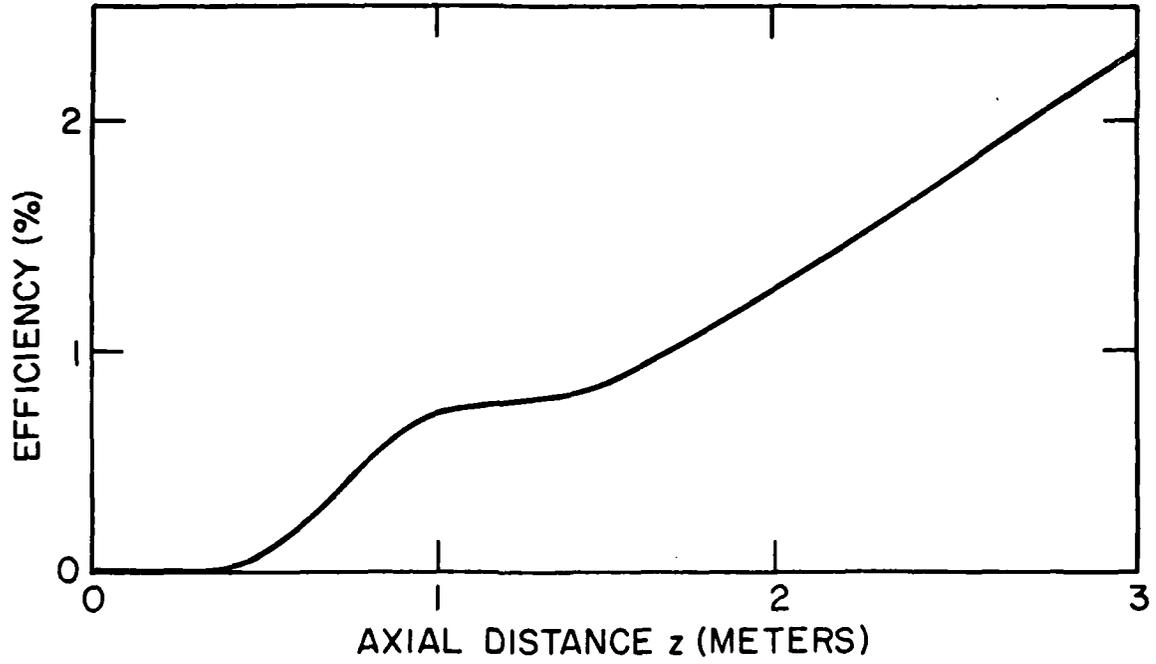


Fig. 8 — Efficiency as a function of z for electron beam with uniform distribution of initial phase ψ_0 in a tapered wiggler field.

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