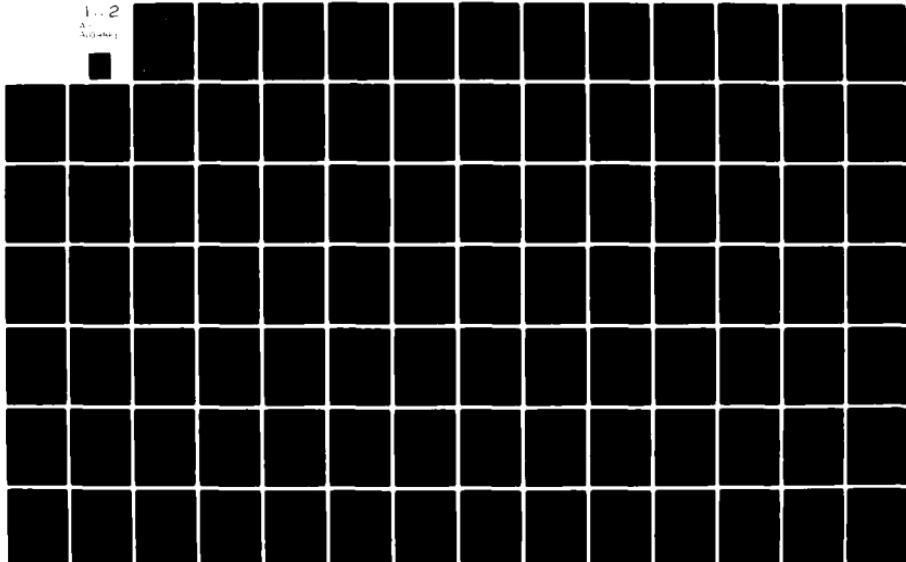


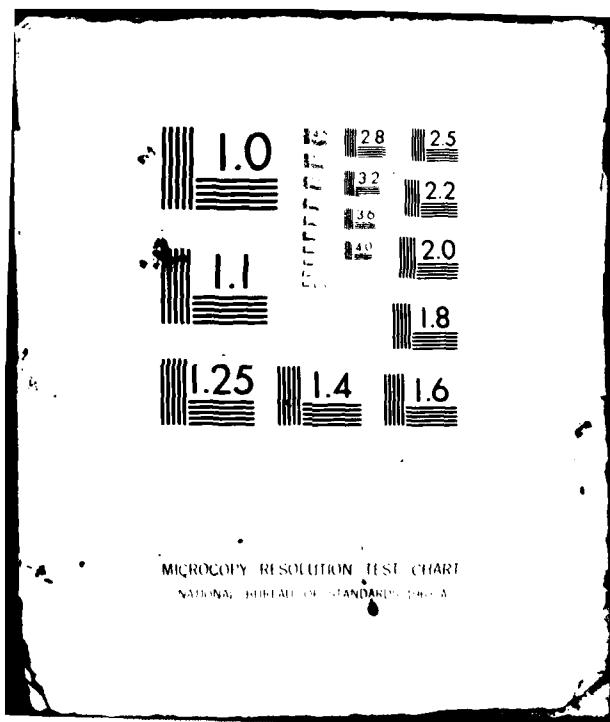
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LEVEL II

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A SHORT TAKEOFF PERFORMANCE COMPUTER PROGRAM

David Bruce Kobus  
Aircraft and Crew Systems Technology Directorate  
NAVAL AIR DEVELOPMENT CENTER  
Warminster, Pennsylvania

25 NOVEMBER 1981

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AIRTASK NO. ZR020302  
Work Unit No. GC172

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SUMMARY

A computer program has been developed which is capable of analyzing the short takeoff of typical V/STOL aircraft configurations. This program can be used as a means for performance estimation as well as for assisting in aircraft conceptual design.

This program was written in FORTRAN for use on a CDC 6600 and uses five supporting subroutines. This report describes the analytical development and logic development for the program. In addition it includes a user description and complete listing of the program

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## LIST OF SYMBOLS

$a_x, a_z$	Longitudinal and vertical acceleration ( $m/sec^2$ , or $ft/sec^2$ )
$a/g$	Normalized longitudinal acceleration
$C_D$	Drag coefficient
$C_L$	Lift coefficient
$C_M$	Pitching moment coefficient
$D$	Drag (N or lb f)
$F_G$	Gross thrust (N or lb f)
$F_{GF}, F_{GA}$	Fore and aft engine gross thrust (N or lb f)
$F_{GH}, F_{GV}$	Horizontal and vertical gross thrust (N or lb f)
$g$	Acceleration due to gravity ( $9.8 m/sec^2$ or $32.2 ft/sec^2$ )
$I_{yycg}$	Lateral moment of inertia ( $kg\cdot m^2$ or $slug\cdot ft^2$ )
$L$	Lift (N or lb f)
$M_y$	Lateral pitching moment (N-m or ft-lb f)
$m$	Aircraft mass (kg or lb)
$R_F, R_A$	Fore and aft gear wheel reaction force (N or lb f)
$RD_F, RDA$	Fore and aft engine ram drag (N or lb f)
$S_x, S_z$	Longitudinal and vertical distance (m or ft)
$T$	Time (sec)
$V_x, V_z$	Longitudinal and vertical velocity ( $m/sec$ or $ft/sec$ )
$WOD$	Wind over deck
$W_F$	Fuel flow ( $kg/hr$ or $lb/hr$ )
$W$	Aircraft weight ( $m\cdot g$ )
$\alpha$	Angle of attack (deg)
$\alpha_{MG}$	Angular acceleration about main gear wheel ( $deg/sec^2$ )
$\gamma$	Flight path angle (deg)

LIST OF SYMBOLS

$\Delta$	Increment
$\delta_e$	Control surface deflection angle (deg)
$\theta_j$	Jet nozzle inclination angle (deg)
$\theta_p$	Pitch Angle (deg)
$\mu$	Coefficient of friction
$\Sigma$	Sum

## INTRODUCTION

A methodology for predicting the short takeoff (STO) performance of Vertical or Short Takeoff and Landing (V/STOL) aircraft is essential for the preliminary design of these vehicles as the propulsion system may be sized by STO requirements. Since a wide range of VSTOL configurations may be of interest to the Navy, and each would have its own unique set of thrust and drag variations during the takeoff run, a generalized computer program offers the most feasible method of analyzing STO performance.

Several STO programs currently available in the technical community were examined for applicability. It was found that each program was developed for a specific configuration and did not provide the flexibility necessary to examine arbitrary V/STOL aircraft concepts. Since the existing programs could not be easily modified, it was necessary to develop a new program.

The resulting program can be utilized for performance estimation and for aircraft conceptual design. In the performance estimation mode, inputs are aircraft aerodynamics, propulsion data, takeoff gross weight (TOGW), and STO technique while outputs are time, distance, velocity, longitudinal acceleration, lift, drag, and horizontal and vertical gross thrust. These data can be calculated at the condition of liftoff, at some specified rate of climb (R/C), or at some specified sink distance. In the conceptual design mode, inputs are given design parameters such as takeoff distance, rate of climb at liftoff, and longitudinal acceleration (with or without one engine inoperative (OEI)), and outputs such as engine size and optimum STO technique can be determined.

## DISCUSSION

Theoretical Considerations

This program utilizes an open form, time history, numerical integration. The forces included in this treatment are lift, drag, gross thrust, and friction. A force diagram is presented in Figure 1. The horizontal forces are summed and divided by the aircraft mass to yield a horizontal acceleration. This acceleration in turn is equated to the following kinematic formula:

$$a_x = \frac{\Delta v_x}{\Delta t} = \frac{1}{\Delta s_x} \frac{\Delta(v_x^2)}{\Delta t}$$

Using time increments, a change in velocity and distance can be determined. More specifically, the basic equations are:

$$\text{DRAG} = C_D * 1/2 \rho V^2 S + D_{\text{ENGINE RELATED}} + D_{\text{STORE}} + D_{\text{OEI}} + D_{\text{INDUCED}}$$

where:  $D_{\text{ENGINE RELATED}}$  = ram drag, spillage drag, boattail drag, etc.

$$\text{LIFT} = C_L * 1/2 \rho V^2 S + L_{\text{INDUCED}}$$

Summing vertical gross thrust components:

$$F_{Gv} = F_{GFv} + F_{GAv}$$

$$F_{GV} = F_{G1} * \sin \beta_1 + F_{G2} * \sin \beta_2$$

where:  $F_{G1} = F_{GF}$  - fore engine gross thrust loss

$F_{G2} = F_{GA}$  - aft engine gross thrust loss

$\beta_1 = \theta_{jF} + \theta_p$  + engine datum angle

$\beta_2 = \theta_{jA} + \theta_p$  + engine datum angle

Summing horizontal gross thrust components:

$$F_{GH} = F_{GFH} + F_{GAH}$$

$$F_{GH} = F_{G1} * \cos \beta_1 + F_{G2} * \cos \beta_2$$

Balancing the vertical forces:

$$\text{BALANCE} = W - \text{Lift} - F_{GV}$$

The change in velocity over a time increment  $\Delta T$  is:

$$\Delta V_x = \Delta T * g * (F_{GH} - \text{DRAG} - \mu * \text{BALANCE}) / W$$

where:  $\Delta V_x = V_{x2} - V_{x1}$

Finally, the distance gained over  $\Delta T$  is:

$$\Delta S_x = 1/2 * \Delta T * ((V_{x2} - \text{WOD})^2 - (V_{x1} - \text{WOD})^2) / \Delta V_x$$

By using this technique the forces which vary as a function of time and angle can be accurately represented and, in addition, pilot technique can also be closely approximated. Also by using small time increments any procedural changes can be fitted through the input.

Increased program accuracy can be obtained by accounting for and by correcting a pitching moment imbalance. This is done through the following formula:

$$\sum M_y = I_{yyCG} \alpha_{MG}$$

By making use of the supplied aircraft moment of inertia and a power-on pitching moment, an angular acceleration about the main gear can be taken into account. The moment about the vehicle center of gravity is:

$$\text{MOMENT} = C_M * 1/2 \rho V^2 * \text{MAC}$$

The fore gear wheel reaction force is therefore:

$$R_F = (\text{BALANCE} * \beta_3 - \text{MOMENT}) / (\text{LRF} + \beta_3 + \cos \theta_p)$$

where:  $\beta_3 = LRA \cos \theta_p + LRA \mu \sin \theta_p + LR \mu \cos \theta_p - LR \sin \theta_p$

See Table I for the definitions of LR, LRA, LRF and MAC.

If the supplied aerodynamic data is a function of control surface deflection, the deflection required to nullify any moments can be calculated. This is accomplished by the following algorithm:

initialize  $\alpha$ ,  $\theta_j$  and  $\delta e$   
 $C_L = f(\alpha, \delta e, \theta_j)$   
 $C_D = f(C_L, \delta e, \theta_j)$   
 $C_M = f(C_L, \delta e, \theta_j)$

DRAG =  $f(C_D) + D_{\text{ENGINE RELATED}} + D_{\text{STORE}} + D_{\text{OEI}} + D_{\text{INDUCED}}$

LIFT =  $f(C_L) + L_{\text{INDUCED}}$

MOMENT =  $f(C_M)$

$F_{G_V} = f(F_G, \theta_j, \theta_p)$

BALANCE =  $W - \text{Lift} - F_{G_V}$

$R_F = f(\text{BALANCE}, \text{MOMENT})$

iterate  $\delta e$  until  $R_F = 0$

Rates of climb or sink can be calculated if the horizontal component of velocity is considered much larger than the vertical component ( $V_z < .02 V_x$ ). Here the vertical acceleration is:  $a_z = \frac{\Delta V_z}{\Delta T}$

and the vertical velocity is:  $V_z = \frac{\Delta S_z}{\Delta T}$

Hence, climb or sink accelerations, velocities, and distances can be determined. For rate of climb velocity over the  $\Delta T$  increment:

$$a_z = (-\text{BALANCE}) * g / w$$

$$\bar{a}_z = 1/2 * (a_{z2} + a_{z1})$$

To determine the incremental ROC:

$$\Delta \text{ROC} = \bar{a}_z * \Delta T$$

For sink off the bow distance over the  $\Delta T$  increment:

$$a_z = \text{BALANCE} * g / w$$

$$\bar{a}_z = 1/2 * (a_{z2} + a_{z1})$$

$$\Delta V_z = \bar{a}_z * \Delta T$$

$$V_{z2} = V_{z1} + \Delta V_z$$

$$\bar{V}_z = 1/2 * (V_{z2} + V_{z1})$$

The incremental sink distance is:

$$\Delta SINK = \bar{V}_z * \Delta t$$

If an instantaneous ROC at liftoff is needed, the following formula is used:

$$a_x = (F_{GH} - DRAG - \mu * BALANCE) / W$$

Assuming a small flight path angle at liftoff:

$$ROC_{instantaneous} = V \sin \gamma \approx V_Y$$

$$\text{Where } V_Y = V * ((LIFT + F_{GY} - W) / F_{GH})$$

The main program logic, which illustrates how all the above equations are implemented, is presented in Appendix D.

#### Program Description

In addition to the main program, which performs the computations on the dynamic equations, there are five supporting subroutines, as described below.

**TAKE 5** - In the formulation of the STO computer program a four degree-of-freedom interpolation routine was developed from an earlier three degree-of-freedom routine (reference (a)). This was done to accomodate aerodynamic inputs which are a function of four variables.

This subroutine has two modes of operation. In the first mode, table data representing aerodynamic and propulsion characteristics are input and stored. Each table is assigned a predetermined reference number. In the second mode, table data is interpolated and extrapolated by the function SPLNQ1 for use in the dynamic calculations. TAKE5 subroutine logic is presented in Appendix D.

**SPLNQ1** - This function is used to interpolate or extrapolate tabular data. The interpolation is calculated using a local curve fit scheme described in reference (b). Linear extrapolations are made using each end point slope of the local curve fit.

**UPDATE** - This subroutine is used to reshape data arrays into a form usable by the function SPLNQ1.

**SNEST** - This is an iteration subroutine used to solve one degree-of-freedom problems. A slope intercept convergence technique is employed.

ATMOS - This is a 1962 standard atmosphere table which returns properties of density, pressure, temperature, and sound velocity for an input geometric altitude.

The data required for the program consists of a series of single-value, fixed inputs and multiple-valued tabular inputs. The form of the computer data deck necessary to make a run is presented in Figure 2.

The tabular data includes:

- Gross thrust as a function of Mach number and engine speedup time.
- Fuel flow as a function of Mach number and engine speedup time.
- Drag coefficient as a function of lift coefficient, control surface deflection, jet nozzle inclination, and velocity.
- Lift coefficient as a function of angle of attack, control surface deflection, jet nozzle inclination, and velocity.
- Induced lift increment as a function of jet inclination angle
- Induced drag increment as a function of jet inclination angle
- Pitching moment coefficient as a function of lift coefficient, control surface deflection, jet nozzle inclination, and velocity.
- Aircraft moment of inertia as a function of aircraft mass.
- Distance from aircraft center of gravity to main gear wheel as a function of aircraft mass.
- Gross thrust loss relative to zero nozzle deflection gross thrust as a function of jet nozzle angle.
- Throttle dependent, ram, and external store drag as a function of Mach number.

These tabular inputs are graphically illustrated in Appendix A.

The fixed inputs consist of aircraft size and mass data, ambient conditions, initial thrust vector angles and control surface deflections, rotation rates for the nozzles and specification for events that may occur during the takeoff run (e.g. loss of an engine). Table I contains a fixed input variable list.

#### Program Options

Available to the user are two main options which concern the type of STO vehicle that can be approximated. First, is a Harrier type vehicle which maintains moment balance by a reaction control system, rotates its jet nozzles, and pitches up at a given rate and at a predetermined airspeed. Second, is a vehicle which maintains moment balance by a control surface deflection and has a fixed jet nozzle angle.

For vehicles using control surfaces to maintain moment balance on the ground, the program will search for the start of auto rotation (stick free pitch up) and either give information on the rotation of the aircraft about the aft wheel or attempt to correct this rotation by the deflection of a control surface. Pertinent tabular inputs for this vehicle type include:

$$C_M = f(C_L, \delta_e, \theta_j, V_x)$$

$$I_{yyCG} = f(m)$$

$$\text{Distance from CG to aft wheel} = f(m)$$

Fixed inputs concerned with this type of vehicle are LR, LRA, LRF, DELTAE, VSTARR, MAC, SEGMENT, IYYCG, XCG, YCG, DELMAX and ALPHMIN. Examination of the above data, by considering the descriptions made in Table I and Appendix A, will clearly illustrate the options available for this type of vehicle.

If a Harrier type vehicle is to be considered, the previously mentioned input can be ignored.

By viewing the form of the remaining tabular and fixed input, in Table I and Appendix A, it is seen that a wide variety of pilot techniques can be approximated. This is because any continuous or discontinuous tabular aerodynamic or propulsion function can be fitted. In addition, a large variety of fixed input switches are available for duplication of aircraft rotation and thrust deflection at any prescribed airspeed.

The following comments offer some additional options that can be implemented for a Harrier type vehicle.

1. If a series of data cases are to be run, put the additional aircraft weights or velocities in ascending order. Set RUN not equal to zero for interpolated weight or set RUN and PSINT not equal to zero for interpolated pitch speed.
2. Apply variables RS, ALPHARR, ALPHAAR, ALPHA, PHI2, PHI2AR, and PS for desired rotation method. For the fore engine nozzle variation apply RSF, PHI1, PHILAR, PHI1RR accordingly.
3. Set NOEDRAG not equal to zero and NOSTORE not equal to zero if engine related drags and store drags exist in reference table 33 (nos. 1 and 2) (see Appendix A). Set NODOEI not equal to zero if engine out drag exists in reference table 33 (no. 3).
4. For OEI at brake release, read in NEF = NEA = 0.5 or any appropriate scale down, or put in single engine tabular data inputs and add failed engine drag in store drag (reference table 33 (no. 2)). For OEI at liftoff, set EFAILA not equal to zero and OEILOS to an appropriate front engine scale down value and add failed engine drag as additional drag (reference table 33 (no. 3)). Set OEITAB not equal to zero for OEI at liftoff when thrust, fuel flow, and drags (engine related and external store) for one engine out are supplied in tabular form (reference table 10, 11, and 33 (nos. 3 and 4)). Put in RAM for a constant ram drag scale down during OEI.

5. For dynamic R/C constraint, put in ROC limit. Set PHONY not equal to zero when instantaneous R/C is desired (fore and aft nozzle angles and aircraft pitch angle are set to maximum values for instantaneous R/C calculation). Set SINKD to bow height for sink calculations. (If PS, RS, and RSF have not been reached at SINKD, these variables will be set to the airspeed at SINKD). NOTE: rate of climb and sink estimates assume that the horizontal velocity is much greater than the vertical velocity.

ACKNOWLEDGEMENTS

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REFERENCES

- (a) Caddy, M. J., "TREAD/TLOOK - Multipurpose Computer Routine for Interpolation and Extrapolation of Tabular Data," NAVAIRDEVCE Report No. NADC-76366-30, 11 January 1977
- (b) Akima, Hiroshi, "Interpolation and Smooth Curve Fitting Based on Local Procedures," Institute for Telecommunication Sciences, 1 March 1972

FOR THIS CONDITION:

$$\gamma = 0^\circ$$

$$\alpha = \alpha_i$$

ENGINE DATUM  $\approx 0^\circ$

$$\Theta_p = \alpha - \alpha_i = 0^\circ$$

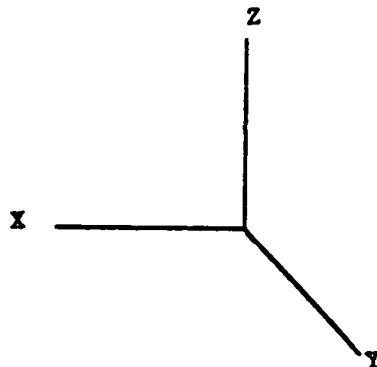
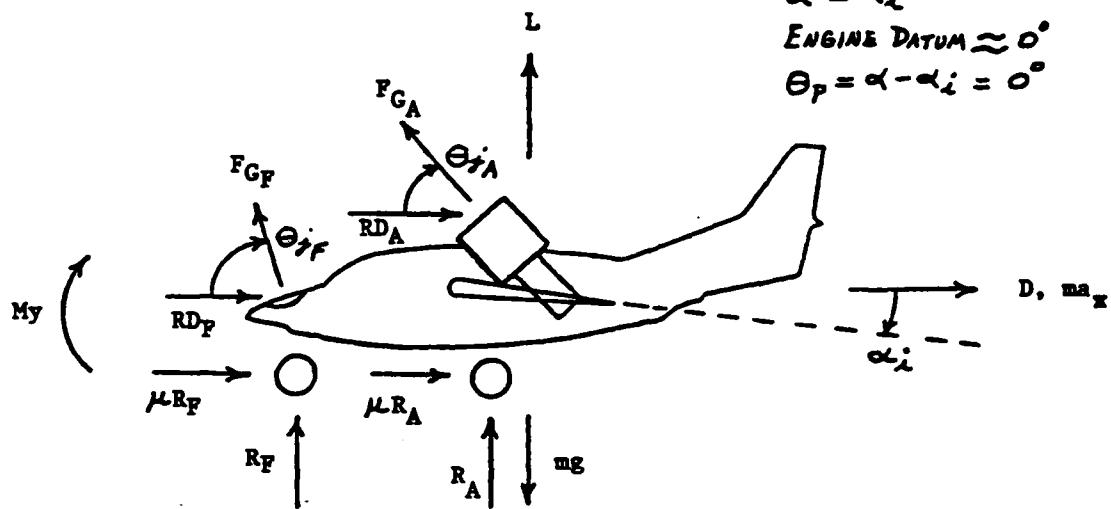


FIGURE 1. Force Diagram (Ground Run)

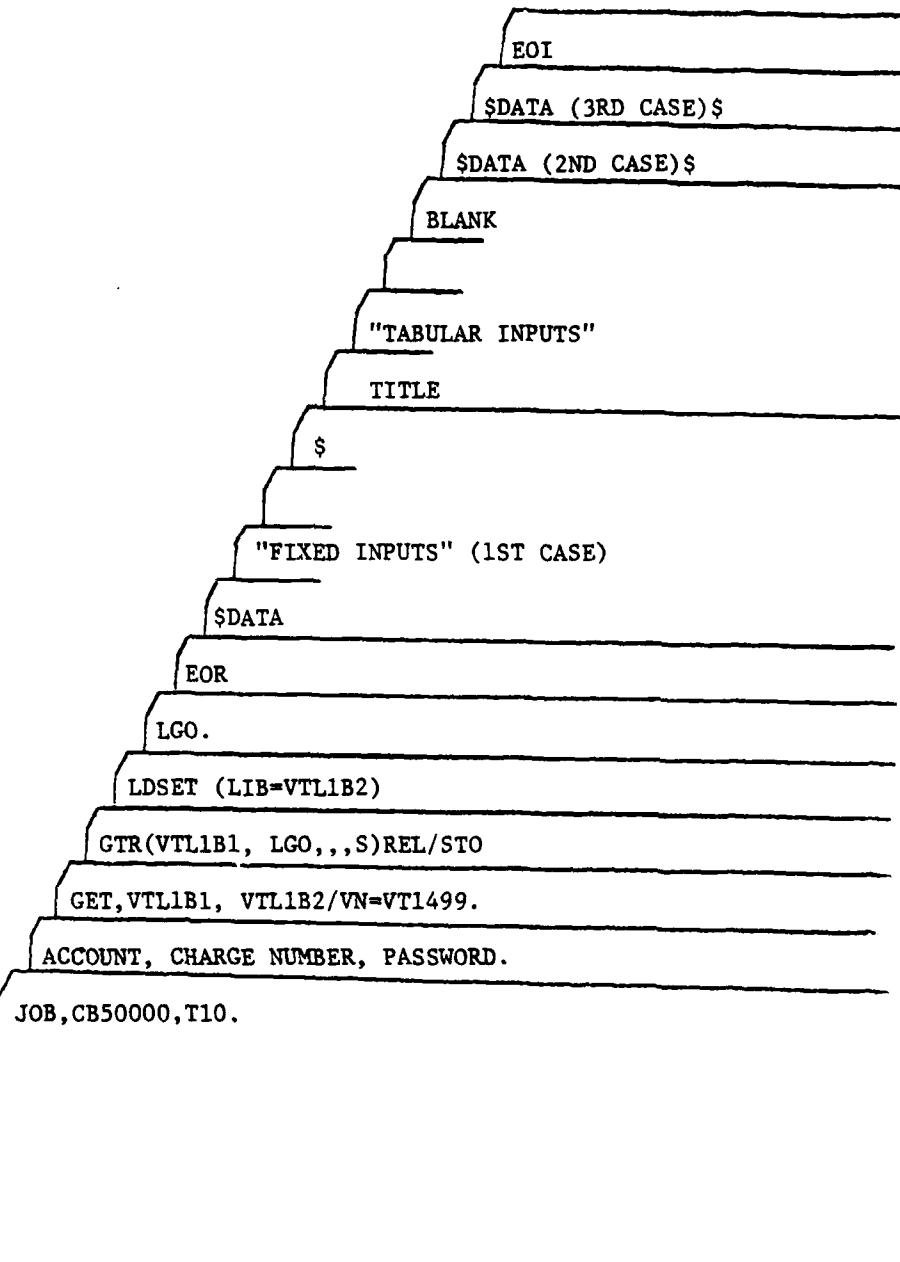


FIGURE 2. Data Input Deck Structure

TABLE I  
FIXED INPUT VARIABLE LIST

<u>Variable Name</u>	<u>Description</u>	<u>Units</u>	<u>Default Value</u>
ALPHA	Initial angle of attack (for $C_L-\alpha$ curve)	deg.	-----
ALPHAAR	Pitch angle after rotation	deg.	0.0
ALPHARR	Pitch up rotation rate	deg/sec	0.0
ALPHMIN	Maximum angle of attack before auto rotation control attempted	deg	0.0
ALT	Field altitude	m. or ft.	0.0
ANGFRL	Initial fuselage reference line angle (for engine reference)	deg	0.0
DELMAX	Maximum control surface deflection angle (maximum $\delta_e$ )	deg	-----
DELTAE	Initial control surface deflection angle	deg	0.0
DISTMAX	Abort run if this takeoff distance is exceeded	m. or ft.	$10^6$
DT	Time integration increment	sec.	.05
EDATUM	Engine datum (with respect to fuselage reference line)	deg	0.0
EFAILA	If ≠ zero, failure of one engine assumed at liftoff	-----	0.0
EI	If ≠ zero, two thrust vectors are present	-----	0.0
FLDTEMP	Field ambient temperature	°C or °F	59.
IPRINT	If ≠ zero, a time history of parameters will be printed	-----	0
IYYCG	Constant aircraft moment of inertia	kg-m <sup>2</sup> or slug-ft <sup>2</sup>	-----
LR	Vertical distance from center of gravity (CG) to ground	m. or ft.	-----
LRA	Horizontal distance from CG to aft wheel	m. or ft.	-----
LRF	Horizontal distance from CG to fore wheel	m. or ft.	-----
MAC	Mean aerodynamic chord	m. or ft.	-----
METRIC	If ≠ zero, metric units present	-----	0
MU	Wheel friction coefficient	-----	.02
NEA	Number of lift cruise engines	-----	1.
NEF	Number of lift engines	-----	1.
NODEOI	If ≠ zero, tabular engine out drag present	-----	0
NOEDRAG	If ≠ zero, tabular throttle dependent drag present (includes ram drag)	-----	0
NOSTORE	If ≠ zero, tabular external store drag data present	-----	0
NPRINT	If ≠ zero, tabular input will be printed	-----	0
OEILOSF	Lift engine scale down when OEI occurs	-----	.0
OEITAB	If ≠ zero, OEI at liftoff assumed with tabular OEI data present	-----	0.
PHI1	Initial lift engine jet nozzle angle (with respect to engine datum)	deg	0.0
PHI1AR	Lift engine nozzle angle after rotation	deg	0.0

TABLE I  
(Continued)

## FIXED INPUT VARIABLE LIST

<u>Variable Name</u>	<u>Description</u>	<u>Units</u>	<u>Default Value</u>
PHI1RR	Lift engine nozzle rotation rate	deg/sec	0.0
PHI2	Initial lift cruise engine jet nozzle angle (with respect to engine datum)	deg	0.0
PHI2AR	Lift cruise engine nozzle angle after rotation	deg	0.0
PHI2RR	Lift cruise nozzle rotation rate	deg/sec	0.0
PHONY	If ≠ zero, instantaneous R/C is calculated	-----	0.0
PS	Pitch up aircraft speed	m/sec or ft/sec	0.0
PSINT	If ≠ zero, and RUN ≠ zero, will give interpolated pitch up speed	-----	0.0
RAM	Ram drag scale factor for OEI; if default value selected, tabular OEI ram drag is used	-----	1.
RDSCALE	Tabular ram drag scale factor	-----	1.
REVTIME	Engine speed up time	sec	0.0
ROC	If ≠ zero, dynamic liftoff characteristics at this R/C will be given	m/sec or ft/sec	0.0
RS	Airspeed which initiation of lift cruise engine nozzle rotation occurs	m/sec or ft/sec	0.0
RSF	Airspeed which initiation of lift engine nozzle rotation occurs	m/sec or ft/sec	0.0
RUN	IF ≠ zero, STO distance to determine interpolated TOGW	m or ft	0.0
S	Wing area	m <sup>2</sup> or ft <sup>2</sup>	-----
SEGMENT	If default value used, no pitching moment estimation is entered in calculations; if = 1, auto rotation included in estimates; and if = 2, elevator correction to auto rotation applied	-----	0
SINKD	If ≠ zero, this is bow distance for sink calculations	m or ft	0.0
VSTARR	Maximum velocity before which a constant linear extrapolation of aerodynamic tabular data occurs	m/sec or ft/sec	0.0
W	Aircraft mass	kg or lb	-----
WOD	Wind over deck (+ for headwind, - for tailwind)	m/sec or ft/sec	0.0
XCG	Constant horizontal distance from CG to main gear wheel (presumes no tabular CG locations inputting)	m or ft	-----
YCG	Constant vertical distance from CG to main gear wheel (supposes no tabular CG locations inputted)	m or ft	-----

APPENDIX A

TABULAR INPUTS

A list of the tabular data inputs is presented in graphical form. An example of this data in numerical form can be found in Appendix B and reference (a).

Table Reference No. 13  
 $C_D = f(C_L, \delta_e, \theta_j, V_x)$

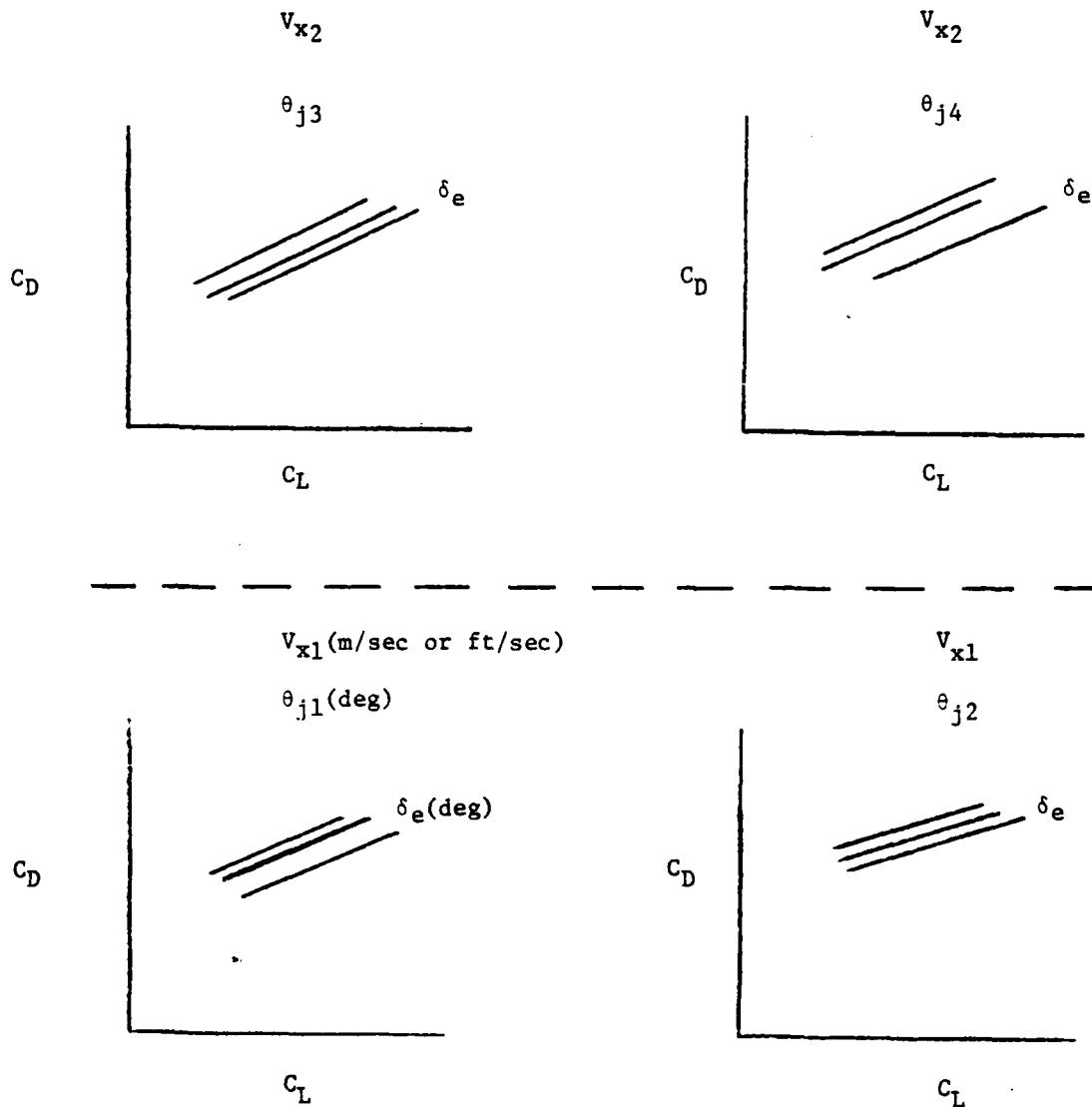


FIGURE A1. Drag Coefficient Tabular Input

Table Reference No. 14  
 $C_L = f(\alpha, \delta_e, \theta_j, V_x)$

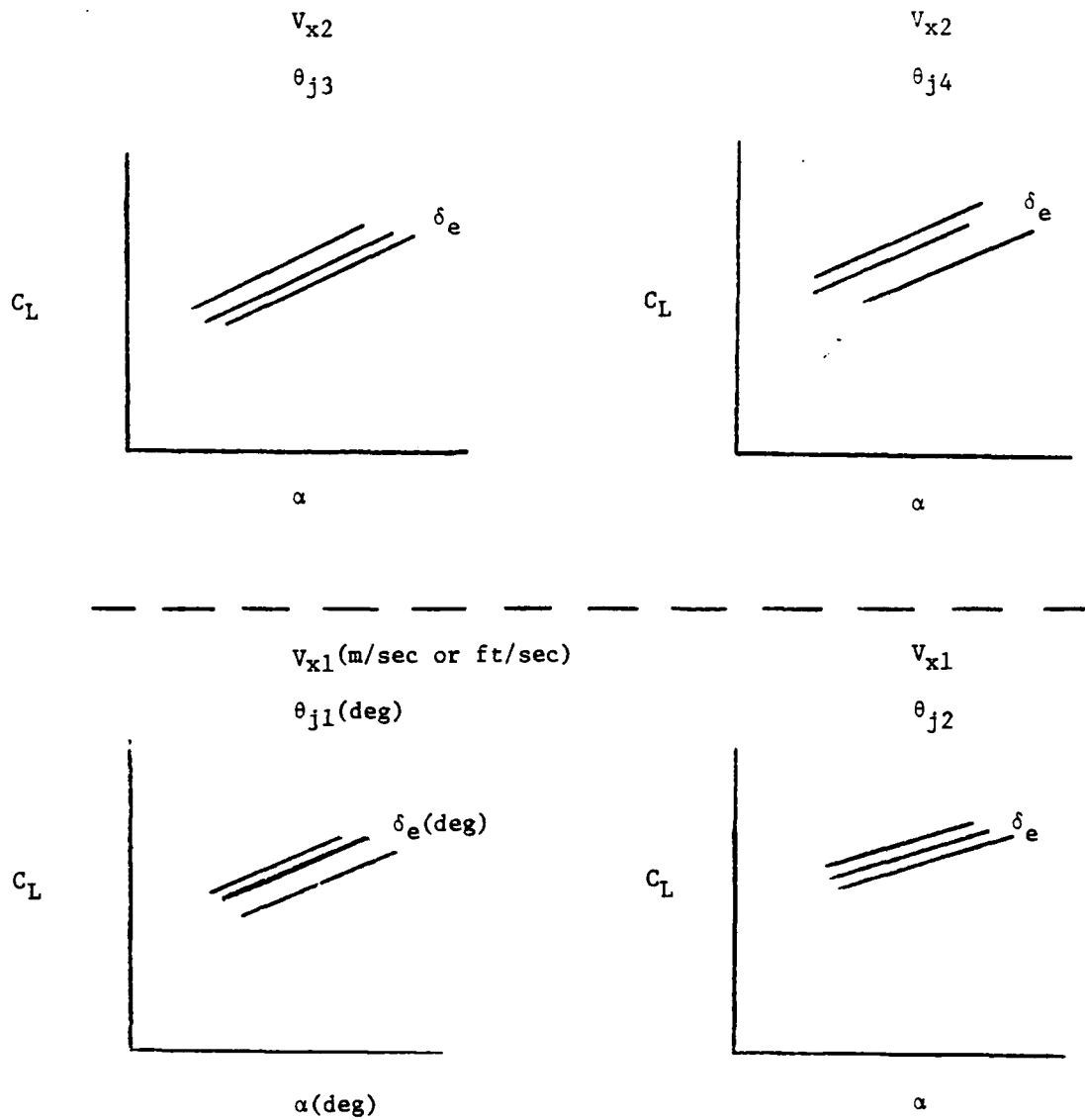
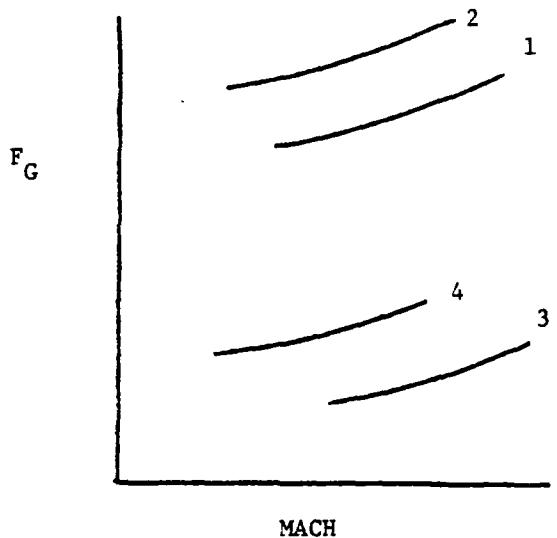


FIGURE A2. Lift Coefficient Tabular Input

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Table Reference No. 10  
 $F_G = f(MACH, \text{Engine Type}, \text{REVTIME})$

$\text{REVTIME}_2$



$\text{REVTIME}_1 (\text{sec})$

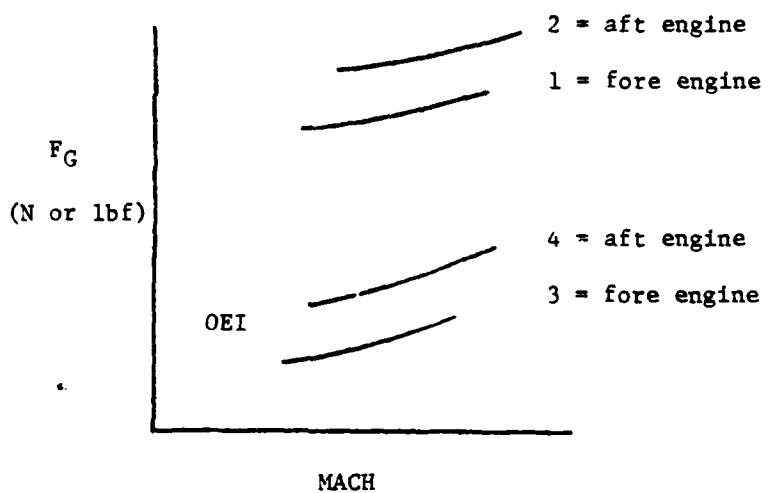


FIGURE A3. Gross Thrust Tabular Input

Table Reference No. 11  
 $W_F = f(MACH, \text{Engine Type}, REVTIME)$

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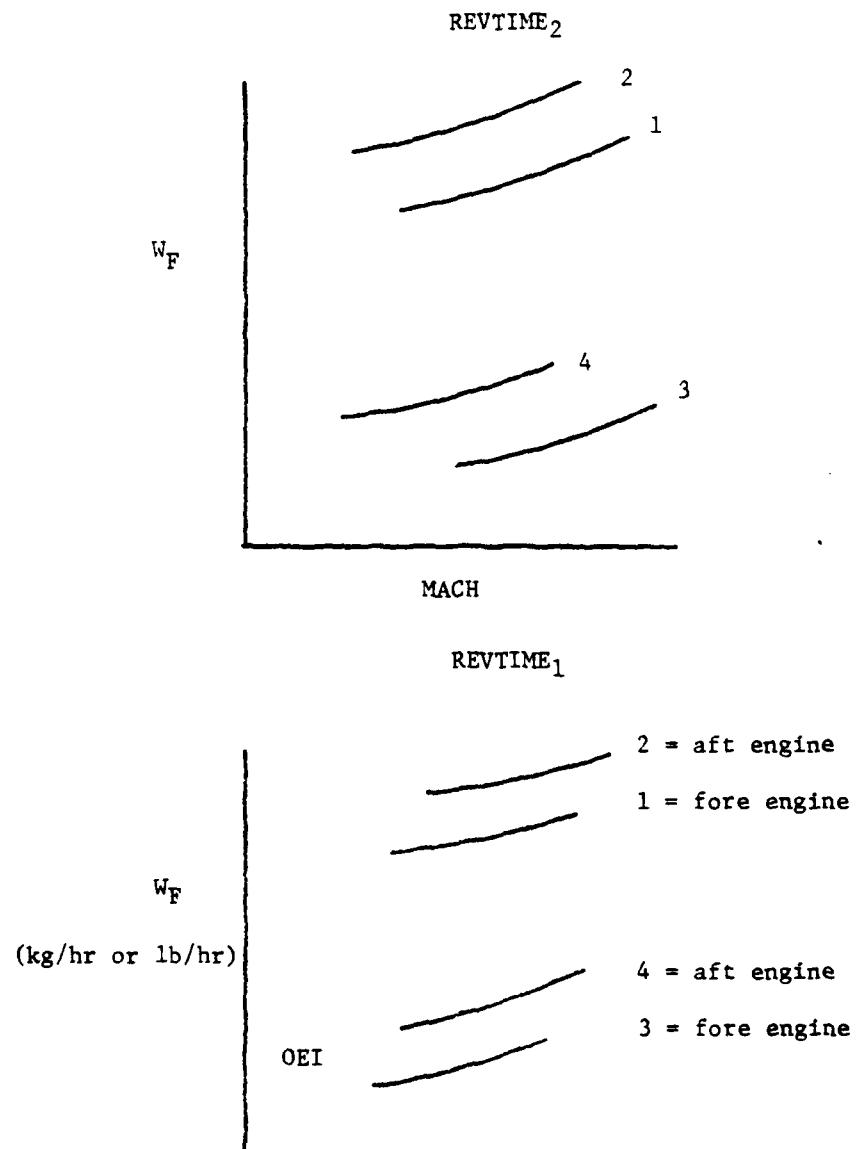


FIGURE A4. Fuel Flow Tabular Input

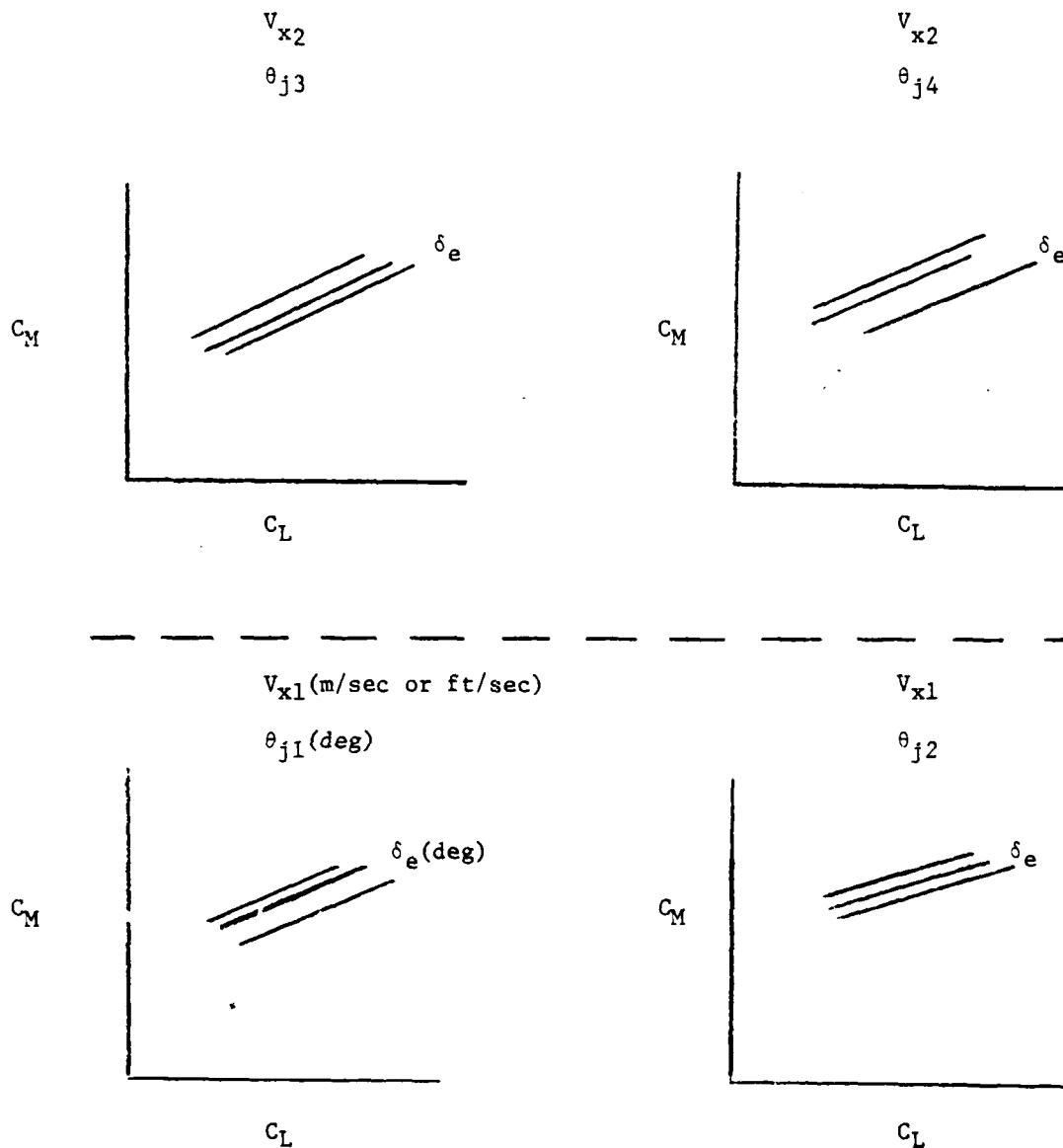
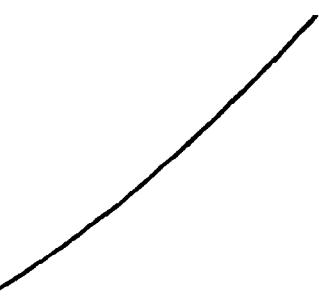


FIGURE A5. Moment Coefficient Tabular Input

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Table Reference No. 30  
 $I_{yyCG} = f(m)$

$I_{yyCG}$   
(kg-m<sup>2</sup> or slug-ft<sup>2</sup>)



m (kg or lb)

FIGURE A6. Moment of Inertia Tabular Input

Table Reference No. 15

$$\frac{\Delta L}{F_G}, \frac{\Delta D}{F_G} = f(\theta_j)$$

$$1 = \frac{\Delta L}{F_G}$$

$$2 = \frac{\Delta D}{F_G}$$

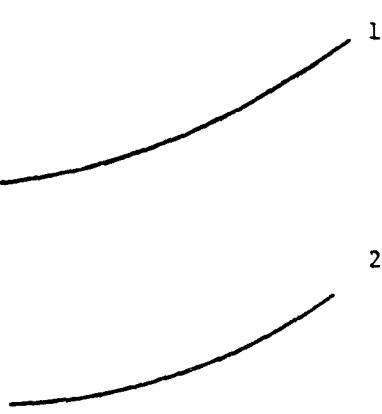
 $\theta_j$  (deg)

FIGURE A7. Induced Lift and Drag Tabular Input

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Table Reference No. 33  
D = f(MACH, Drag Type)

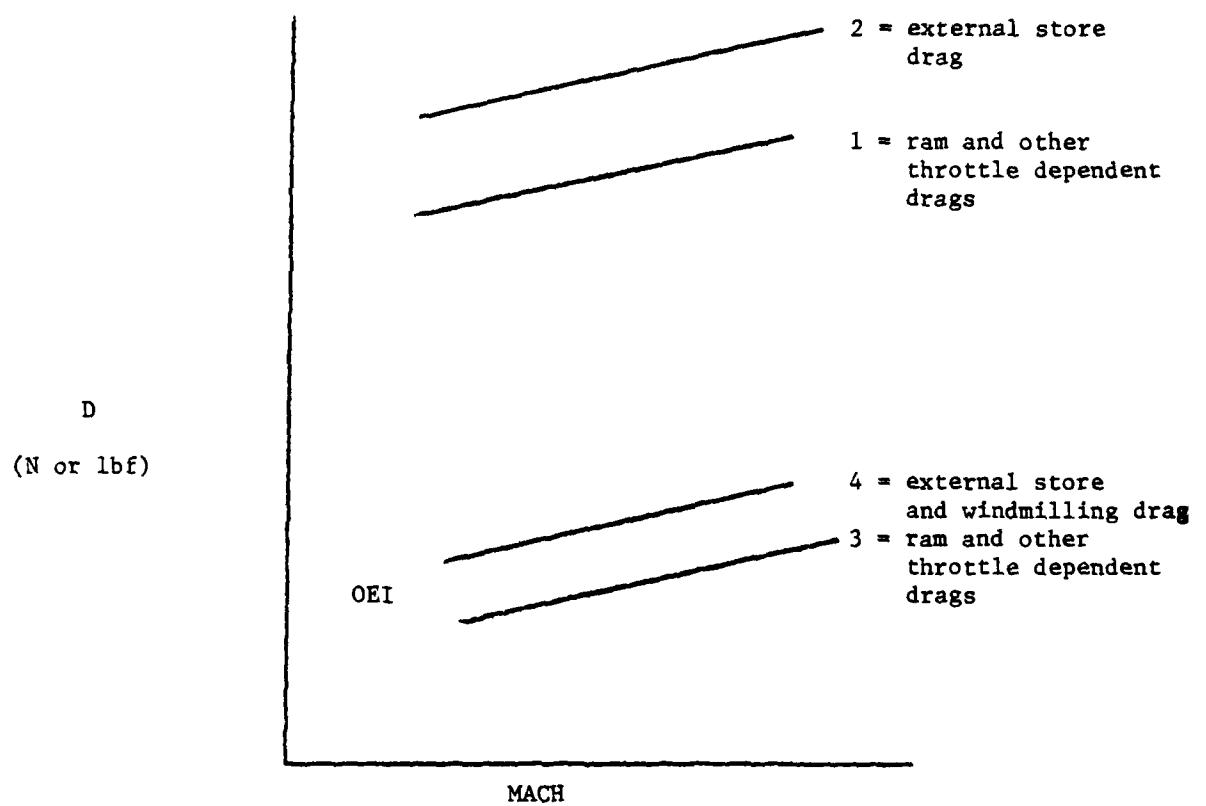


FIGURE A8. External Store and Ram Drag Tabular Input

NADC-81259-60

Reference Table No. 31  
 $X_{CG}, Y_{CG} = f(m)$

1 =  $X_{CG}$   
2 =  $Y_{CG}$   
(m or ft)

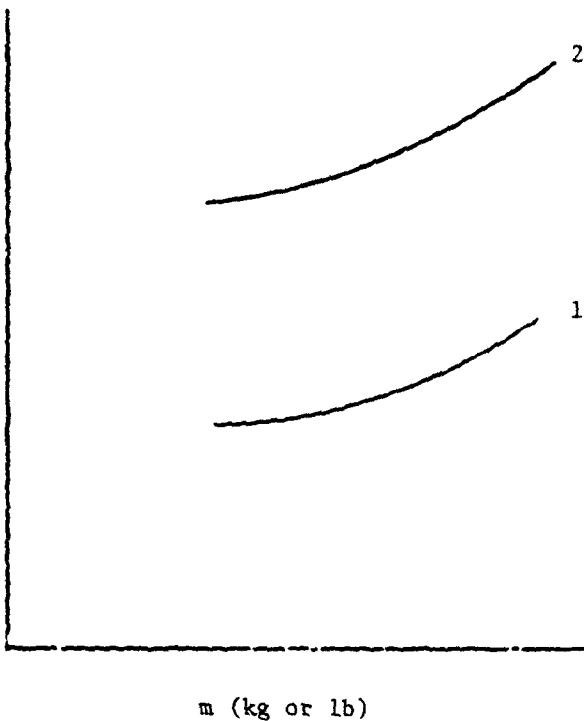


FIGURE A9. Center of Gravity Location Tabular Input

NADC-81259-60

Reference Table No. 12

$$\frac{F_{G\text{Loss}}}{F_G} \text{ (No nozzle deflection)} = f(\theta_j, \text{ ENGINE TYPE})$$

$\frac{F_{G\text{Loss}}}{F_G}$   
F<sub>G</sub>(no nozzle  
deflection)

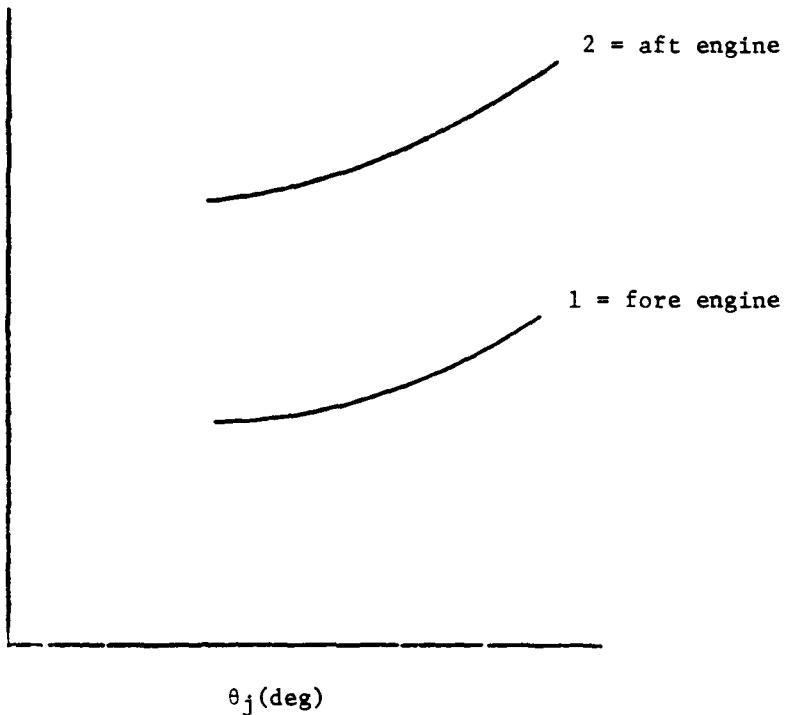


FIGURE A10. Gross Thrust Loss Tabular Input

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APPENDIX B

EXAMPLE CASE

An example card deck and printout is presented. The required programs, supporting subroutines, and control cards to execute this program with any charge number under the NAVAIRDEVCEN KRONOS 2.1 operating system is illustrated. An explanation of the sample case is also presented.

**Example Case****Card Deck**

An example card deck listing, similar in form to the arrangement illustrated in Figure 2, is presented. As shown, three cases are to be run and they require less than 50,000 octal central memory core and ten octal seconds central processor unit time.

For the first case an aircraft, with a wing area of 430 square feet, is initially resting on the ground with a wing angle of attack and fuselage reference line at negative five degrees from the horizontal. The lift engine nozzle angle is set at 45 degrees while the cruise engine nozzle angle is set at five degrees. Both nozzle angles are with respect to the fuselage reference line (or to the engine datum line for the cruise engines). On examining the initial case's fixed inputs, at an airspeed of 66 ft/sec the vehicle will rotate its lift engine nozzles to 75 degrees at a rate of 15 degrees/sec and it will rotate its cruise engine nozzles to 54 degrees also at 15 deg/sec. At an airspeed of 80 ft/sec the aircraft will pitch up to 13 degrees at 5.9 deg/sec. This vehicle weighs 40,000 lbs. Additional fixed inputs state that the vehicle has a tabular ram drag input (NOEDRAG), two thrust vectors are present (E1), and the analysis is for a 90°F day (FLDTEMP). The default value of METRIC causes English units to be used. If the deck run exceeds 750 feet the case runs will be terminated. The variables RUN and PSINT are used, in combination, to interpolate or extrapolate the case values of PS. This is to determine the appropriate value of this variable for a deck run of 400 feet. The variable SINKD specifies the carrier bow length and signals for sink calculations to be done for this case. The IPRINT parameter indicates that a time history of pertinent parameters for this specific case will be printed.

Example tabular data includes  $C_L$  versus  $\alpha$ , drag polars, engine thrusts, ram drag, and induced aerodynamics. The table numbers used for each table are predetermined as outlined in Appendix A. Notice that omitted input, such as fuel flow data, is assumed to be zero by the program.

The second and third fixed input cases switch off the sink calculations and the time history printout and change the lift and cruise nozzle rotation initiation airspeeds. These additional cases also change the airspeed in which the vehicle begins pitching up. Note that a maximum of one card is permitted for each additional case. For the additional cases a value for ROC causes dynamic rate of climb calculations to be made.

```

TEST.C950000.T10.
ACCOUNT,CHARGE NUMBER,PASSWORD.
GET,VTL1R1,VTL1R2/UN=VTL1R2,
GTP(VTL1R1+LG0...S1FEL/STO
LDSET(VTL1R2)
LGO.
END OF RECPD
$DATA ALPHA=5,S=430,PH12=5,PH12AR=54,PH12RA=15,ALPHAARR=5.9,ALPHAAR=13,
AN/FPL=-5,NDENDRAG=1,E)=1,FLDTEW=90,PH1=45,DISTMAX=750,PH11AR=75,
PH11RA=15,RS=6,PS=40,RSF=66,W=40000,IPRINT=1,PSINT=1,MIN=600,
SINKP=200+NPR(INT),
5
      EXAMPLE CASE
14    EXAMPLE CL VS. ALPHATABLE
      VEL 1   0.
      PH12 3   0.      50.     40.
      DLTE 1   0.
      ALPH 9   -8.     -4.     0.      4.      8.      12.     16.
          20.     24.     0.      4.      8.      12.     16.
      CL   4   -0.48   -0.175   -0.175   -0.05   -0.78   1.04   1.375
          1.49
      DLTE 1   0.
      CL   8   -0.13   -0.15   -0.12   -0.09   -0.06   1.02   1.45
          1.57
      DLTE 1   0.
      CL   9   -0.34   -0.59   -0.86   -1.11   -1.34   1.47   1.56
          1.55
      EOT
13    EXAMPLE CRAG POLARS (POWER OFF) TABLE
      DUMM 1   0.
      PH12 1   0.
      DLTE 1   0.
      CL   6   -0.4   0.      0.6     0.8     1.2     1.4
      CD   6   .34159   .02938   .03742   .06533   .17463   .22905
      EOT
10    EXAMPLE ENGINE THRUST TABLE
      DUMM 1   0.
      TIME 1   0.
      SET  4   1.      2.      3.      4.
      MACH 5   0.      .05     .1      .15     .2
      FG   5   13755.   14044.   14332.   14675.   15417.
      FG   5   29437.   29888.   30538.   31606.   32673.
      FG   5   10994.   11330.   11645.   12342.   13018.
      FG   5   23734.   24346.   24958.   25161.   27363.
      EOT
33    EXAMPLE WAM DRAG TABLE
      DUMM 1   0.
      TIME 1   0.
      SET  2   1.      3.
      MACH 5   0.      .05     .1      .15     .2
      DAWD 5   0.      3926.   9123.   12740.   16021.
      DAWD 5   0.      3862.   7931.   12023.   16486.
      EOT
15    EXAMPLE INCUPED AERODYNAMICS TABLE
      DUMM 1   2.
      Y   1   4.
      SFT  2   1.      2.
      PFD2 3   0.      50.     100.
      CFL  3   .02     .12     .214
      CFD 3   2.3     44.5    44.7
      CFL  1   -.058   -.031   -.042
      EOT

```

---

```
BLANK CARD
SDATA SINKD=0,ROC=1,A7,PS=90,RC=76,RSE=76,IPRINT=0
SDATA SINKD=0,ROC=1,A7,PS=100,RS=94,RSE=94,IPRINT=0
NOTE: MAXIMUM OF ONE CARD FOR EACH ADDITIONAL CASE.
END OF INFORMATION
```

## Printout

The computer printout of the previously mentioned card deck is now presented. On the second page of the printout a loader map illustrating all the supporting subroutines and their individual core requirements is presented. On the bottom of this page the fixed inputs for the first case are shown. The variable NPRINT enables the tabular input to be printed in full on the following five successive pages. This data, in turn, is followed by a summary of core requirements for each table. Next, the output data begins with a time history of the first of three sample cases. Each element is a successive point in a time variance of parameters. These parameters include:

W - Aircraft mass (kg or lb) (English units for this example)  
 V - Vehicle airspeed (m/sec or ft/sec)  
 L - Lift force (N or lbf)  
 DR - Drag force (N or lbf)  
 RF - Nose gear reaction force (N or lbf) (not used in this example)  
 EDRG - Engine related drags (N or lbf)  
 FN2 - Cruise engines gross thrust (N or lbf)  
 PH2I - Cruise engine nozzle angle (deg)  
 ALPHA - Angle of attack (deg)  
 T - Time (sec)  
 D2 - Distance (m or ft)  
 BALANCE - Lifting forces minus weight (N or lbf)  
 PH1I - Lift engine nozzle angle (deg)  
 FN1 - Lift engines gross thrust (N or lbf)  
 C<sub>L</sub> - Lift coefficient  
 C<sub>D</sub> - Drag coefficient  
 C<sub>M</sub> - Pitching moment coefficient (not used this example)  
 A/G - Normalized longitudinal acceleration  
 RHO - Atmospheric density (kg/m<sup>3</sup> or slug/ft<sup>3</sup>)  
 DELTAE - Control surface deflection angle (deg) (not used this example)

The following parameters were not printed in this listing because they were not used for this example case.

DALPHAD - Angle of attack increment caused by auto rotation (deg)  
 IYYCG - Lateral aircraft moment of inertia (kg-m<sup>2</sup> or slug-ft<sup>2</sup>)  
 XCG - Horizontal distance from CG to main gear wheel (m or ft)  
 YCG - Vertical distance from CG to main gear wheel (m or ft)  
 N - Iteration number for elevator correction to counter auto rotation  
 RF - Nose gear reaction force during iteration (N or lbf)  
 DELTAE - Control surface deflection during iteration (deg)

The following parameters are printed if dynamic rate of climb calculations are made. These parameters are printed only after liftoff.

ROC - Dynamic rate of climb (m/sec or ft/sec)  
 ACCY - Vertical dynamic acceleration (m/sec<sup>2</sup> or ft/sec<sup>2</sup>)

Finally, the following parameters (which are used for this example case) are printed after liftoff when sink calculations are made.

ASINK - Sink acceleration (m/sec<sup>2</sup> or ft/sec<sup>2</sup>) (sink calculations cease when this value becomes zero)

VSINK - Sink velocity (m/sec or ft/sec)  
DSINK - Sink distance (m or ft)

The time history printout concludes on the following page of output. After liftoff the appropriate sink parameters are shown. After the time history the final liftoff parameters are presented. These parameters include maximum sink height and time, distance, and airspeed at that sink height condition. Other characteristics at this condition include lift, drag, horizontal acceleration, gross thrust, and vertical gross thrust.

Since the IPRINT was switched off for the two additional cases no time history is printed. These cases were done with dynamic rate of climb calculations so instead of sink parameters the prescribed rate of climb along with the vertical height when this rate of climb is achieved is printed.

After all the cases are determined an extrapolation is made to estimate the pitchup airspeed and horizontal acceleration for a deck run of 400 feet.



LOAD MAP - STO

CYBER LOADER 1.4-4AS

81/09/28 14.54.01

PAGE 1

FWA OF THE LOAD 111  
 LWA1 OF THE LOAD 32715

TRANSFER ADDRESS -- STO 6206

PROGRAM ENTRY POINTS -- STO 6206

## PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR	VER	LEVEL	HARDWARE	COMMENTS
/PRINT/	111	1							
STO	112	11662	LGO	78/01/0	FTN	3.0	P380	6666	
/TSIZE/	11774	5671							
TAKES	17465	1353	JL-VTL1R2	77/03/0	FTN	3.0	P380	6666	
SPLN01	21240	504	JL-VTL1R2	77/10/1	FTN	3.0	P380	6666	
UPDATE	21744	135	JL-VTL1R2	75/07/1	FTN	3.0	P380	6666	
ATMOS	22101	213	JL-VTL1R2	76/10/2	FTN	3.0	P380	6666	
SNEST	22314	110	JL-VTL1R2	75/08/1	FTN	3.0	P380	6666	
SYSTEMS	22424	1035	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
ACGERS	23461	13	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
RACKSPS	23474	334	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
IFENDFS	24030	57	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
INPUTCS	24107	131	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
INPUTNS	24240	1171	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
OUTPTCS	25431	76	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
REWINDS	25525	52	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
EXPE	25577	44	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
SINCSE	25643	55	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
SORTS	25720	22	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
XTOYE	25742	7	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
KODERS	25751	1422	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
KRAKERS	27373	1525	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
ALNLOGE	31120	37	SL-FTN3L1B	80/09/02	COMPASS	3.6	485		
GETBA	31157	17	SL-FTN3L1B	80/09/02					
S105	31176	1517	SL-FTN3L1B	80/09/02					

.106 CP SECONDS

467008 CH STORAGE USED

11 TABLE MOVES

```

SDATA ALPHAB=5,S=410,PH12=5,PH12AH=56,PH12PP=15,ALPHABH=5,0,ALPHAAH=13,
ALPHQL=5,NOENHAG=1,F1=1,FLDTEHPu90,PH7)=5,0,ISTHAY=750,PH11AH=75,
PH11PR=15,NSEAK,PS=40,RSF=66,W=40000,DIRINT=1,HSHINT=1,RUNE=400,
SINNN=200,PRINT=1.

```

## 14 EXAMPLE CL VS. ALPHAS TABLE

VEL = .0	CLTE = .0									
PHI2= .0	ALPH	-.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02	
	CL	-.48000E+00	-.17500E+00	.17500E+00	.45000E+00	.78000E+00	.10400E+01	.13750E+01	.14900E+01	
VEL = .0	CLTE = .0									
PHI2= .50000E+02	ALPH	-.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02	
	CL	-.13000E+00	.15000E+00	.42000E+00	.69000E+00	.96000E+00	.12000E+01	.14500E+01	.15700E+01	
VEL = .0	CLTE = .0									
PHI2= .90000E+02	ALPH	-.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02	
	CL	-.24000E+00	.59000E+00	.86000E+00	.11100E+01	.13400E+01	.14700E+01	.15600E+01	.15500E+01	

13 EXAMPLE DRAG POLARS (POWER OFF) TABLE

DUMMA= .0	DLTE= .0
PHI2= .0	CL -.40000E+00 .0 .40000E+00 .80000E+00 .12000E+01 .14000E+01
	CD .41590E-01 .29380E-01 .37420E-01 .65330E-01 .17463E+00 .22905E+00

## 10 EXAMPLE ENGINE THRUST TABLE

DUMM#	TIME#	SET #	MACH	FG	.10000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00	.15417E+05
DUMM#	TIME#	SET #	MACH	FG	.13755E+05	.14044E+05	.14312E+05	.14475E+05	.14475E+05	.15417E+05
DUMM#	TIME#	SET #	MACH	FG	.20000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00	.32673E+05
DUMM#	TIME#	SET #	MACH	FG	.29417E+05	.29948E+05	.30534E+05	.31606E+05	.31606E+05	.32673E+05
DUMM#	TIME#	SET #	MACH	FG	.30000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00	.13018E+05
DUMM#	TIME#	SET #	MACH	FG	.10994E+05	.11330E+05	.11645E+05	.12342E+05	.12342E+05	.13018E+05
DUMM#	TIME#	SET #	MACH	FG	.40000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00	.27363E+05

## 33 EXAMPLE RAM DATA TABLE

DUMM= .0	TIME= .0	SET = .10000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00
		MACH .0	.39460E+04	.81230E+04	.12240E+05	.16621E+05
DUMM= .0	TIME= .0	SET = .30000E+01	.50000E-01	.10000E+00	.15000E+00	.20000E+00
		MACH .0	.38620E+04	.79310E+04	.12023E+05	.16486E+05

15 EXAMPLE INDUCED AERODYNAMICS TABLE

DUMMS = .0	SET = .10000E+01		
Y = .0	PHI2 = .0	.50000E+02	.10000E+03
	CEL = .20000E-01	.12000E+00	.21400E+00
DUMMS = .0	SET = .20000E+01		
Y = .0	PHI2 = .20300E+02	.44500E+02	.84700E+02
	CEL = -.58000E-01	-.31000E-01	.42000E-01

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TABLE DATA INPUT SUMMARY 5 TABLES

TABLE NUMBER	REFERENCE NUMBER	ARRAY LOCATION
1	10.	217.
2	13.	178.
3	14.	61.
4	15.	373.
5	33.	316.

DATA STORAGE ALLOCATION 3000  
DATA STORAGE NOT USED 2582

## VSTOL TAKEOFF PERFORMANCE ESTIMATION

## EXAMPLE CASE

TOGW = .40000E+05

## INITIAL GROUND RUN PARAMETERS

```

W,V,L,DY,RF,EDPA,FV2
PH2I,ALPHA,T,D2,BALANCE,PHII,FN1
CL,CD,CH,A/G,RHO,DELTAE
ALPHA,DELPHAO,IYYCG,XCG,YCG
N,RF,DELTAE
R0C,ACCY
ASINK,VSINK,DSINK
.40000E-05 .86470E-01 .13032E+04 -.24604E+04 I!!!! .57810E+03 .29518E+05
.50000E+01 -.50000E+01 .25000F+00 .15292E+01 .29828E+05 .45000E+02 .13984E+05
-.23039E+00 .33947E-01 I!!!! .10483E+01 .22429E-02 .0
.40000E-05 .16842E+02 .12832F+04 -.16718E+04 I!!!! .11518E+04 .29599E+05
.50000E+01 -.50000E+01 .50000F+00 .51215E+01 .29821E+05 .45000E+02 .13840E+05
-.23089E+00 .33947E-01 I!!!! .10369E+01 .22429E-02 .0
.40000E-05 .25186E+02 .12679E+04 -.13042E+04 I!!!! .17221E+04 .29679E+05
.50000E+01 -.50000E+01 .75000F+00 .10797E+02 .29829E+05 .45000E+02 .13882E+05
-.23089E+00 .33947E-01 I!!!! .10255E+01 .22429E-02 .0
.40000E-05 .33199E+02 .11980F+04 -.73685E+03 I!!!! .22900E+04 .29757E+05
.50000E+01 -.50000E+01 .10000F+01 .18532E+02 .29852E+05 .45000E+02 .13923E+05
-.23089E+00 .33947E-01 I!!!! .10141E+01 .22429E-02 .0
.40000E-05 .41518E+02 .11339F+04 -.16891E+03 I!!!! .28563E+04 .29835E+05
.50000E+01 -.50000E+01 .12500F+01 .28304E+02 .29890E+05 .45000E+02 .13964E+05
-.23089E+00 .33947E-01 I!!!! .10026E+01 .22429E-02 .0
.40000E-05 .49645E+02 .10560F+04 -.4027E+03 I!!!! .3216E+04 .29912E+05
.50000E+01 -.50000E+01 .15000F+01 .40039E+02 .29942E+05 .45000E+02 .14004E+05
-.23089E+00 .33947E-01 I!!!! .49132E+00 .22429E-02 .0
.40000E-05 .57679E+02 .96502E+03 .97133E+03 I!!!! .39869E+04 .29988E+05
.50000E+01 -.50000E+01 .17500F+01 .53865E+02 .30004E+05 .45000E+02 .14044E+05
-.23089E+00 .33947E-01 I!!!! .47938E+00 .22429E-02 .0
.40000E-05 .65719E+02 .86111F+03 .15422E+04 I!!!! .45496E+04 .30059E+05
.50000E+01 -.50000E+01 .20000F+01 .69604E+02 .30044E+05 .45000E+02 .14081E+05
-.23089E+00 .33947E-01 I!!!! .66755E+00 .22429E-02 .0
.40000E-05 .73004E+02 .11342F+04 .22311E+04 I!!!! .51025E+04 .30123E+05
.87500E+01 -.50000E+01 .22500F+01 .17247E+02 .27135E+05 .46750E+02 .14115E+05
-.21161E+00 .31105F+01 I!!!! .23703E+00 .22429E-02 .0
.40000E-05 .80434E+02 .14937E+04 .24017E+04 I!!!! .56376E+04 .30183E+05
.12500E+02 -.47050E+01 .25000F+01 .10646E+03 .23413E+05 .52500E+02 .14147E+05
-.16461E+00 .32045E+01 I!!!! .40064E+00 .22429E-02 .0
.40000F+05 .47525E+02 .12332F+04 .15441E+04 I!!!! .61487E+04 .30242E+05
.16750E+02 -.32100F+01 .27500F+01 .11415E+01 .19427E+05 .56240E+02 .14174E+05

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-.3466E-01	.24430E-01	11111	.45141E+00	.22429E-02	.0
-.40000E+05	.94195E-02	.31384E+04	.41654E+04	11111	.66297E+04
.20000E+02	-.17550E+01	.30000E+01	.15125E+03	.15293E+05	.60000E+02
.10182E+00	.29417E-01	11111	.79463E+00	.22429E-02	.0
-.40000E+05	.10039E+03	.41758E+04	.7722E+04	11111	.70759E+04
.23750E+02	-.28000E+00	.32500E+01	.17589E+03	.10990E+05	.63750E+02
.23248E+00	.32481E-01	11111	.77104E+00	.22429E-02	.0
-.40000E+05	.10404E+03	.53114E+04	.53659E+04	11111	.76430E+04
.27500E+02	.11450E+01	.35000E+01	.20199E+03	.67826E+04	.67500E+02
.35522E+00	.30594E-01	11111	.65930E+00	.22429E-02	.0
SINK DATA	.56556E+01		.13639E+00		.34097E-02
.40000E+05	.11111E-03	.65542E+04	.59320E+04	11111	.76481E+04
.31250E+02	.26700E+01	.37500E+01	.22939E+03	.26876E+04	.71250E+02
.47496E+00	.38411E-01	11111	.58321E+00	.22429E-02	.0
SINK DATA	.21618E+01		.10477E+01		.17277E+00

VEHICLE IS AIRBORNE  
MAXIMUM SINK DISTANCE IS .41562E+00 FT.  
DISTANCE = .25216E+03 FT.  
VELOCITY = .11553E+01 FT./SEC.  
TIME = .40000E+01 SEC.  
END WEIGHT FOR THIS PHASE IS .40000E+05 POUNDS MASS

## LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION =	.51570E+00 G/S
LIFT =	.76359E+04 POUNDS FORCE
DRAG =	.63560E+04 POUNDS FORCE
VERTICAL GROSS THRUST =	.32863E+05 POUNDS FORCE
HORIZONTAL GROSS THRUST =	.26984E+05 POUNDS FORCE

NEXT  
SOATA SINKD=0,POC=1,A7,PS=90,RS=76,RSF=7A,IPRINT=09  
TOGW = .40000E+05

## INITIAL GROUND RUN PARAMETERS

VEHICLE IS AIRBORNE  
VEHICLE HAS A W/C OF .16700E+01 FT./SFC.  
VECTICAL HEIGHT IS .36921E+00 FT.  
DISTANCE = .35474E+01 FT.  
VELOCITY = .13093E+01 FT./SEC.  
TIME = .40000E+01 SEC.  
END WEIGHT FOR THIS PHASE IS .40000E+05 POUNDS MASS

## LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION =	.36394E+00 G/S
LIFT =	.11300E+05 POUNDS FORCE
DRAG =	.81452E+04 POUNDS FORCE
VERTICAL GROSS THRUST =	.17272E+05 POUNDS FORCE
HORIZONTAL GROSS THRUST =	.22634E+05 POUNDS FORCE

NEXT  
SOATA SINKD=0,WOC=1,A7,PS=100,RS=84,RSF=8A,IPRINT=09  
TOGW = .40000E+05

## INITIAL GROUND RUN PARAMETERS

VEHICLE IS AIRPLANE  
 VEHICLE HAS A NYC OF .1A700E+01 FT./SEC.  
 VERTICAL HEIGHT IS .73650E+00 FT.  
 DISTANCE = .79324E+01 FT.  
 VELOCITY = .13848E+03 FT./SEC.  
 TIME = .50500E+01 SEC.  
 END WEIGHT FOR THIS PHASE IS .40000E+05 POUNDS MASS

## LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION = .36907E+00 G/S  
 LIFT = .11639E+05 POUNDS FORCE  
 DRAG = .86602E+04 POUNDS FORCE  
 VERTICAL GROSS THRUST = .36461E+05 POUNDS FORCE  
 HORIZONTAL GROSS THRUST = .23423E+05 POUNDS FORCE

NEXT NEXT

BY CUBIC SPLINE INTERPOLATION OF THE ABOVE DATA POINTS  
 FOR A HIN OF .40000E+03 FEET THE PS IS .10320E+03 FT./SEC.  
 AND THE HORIZONTAL ACCELERATION IS .37630E+00 G/S

TESTAVG. 11/04/24, RUNNDS 2.1.1-SYS-C25-NADC.

.51-TEST+CH50000-T10.  
.51-ACCOUNT#A0336A..  
.51-MASTER DEVICE: A  
.52-RF(VTL1H1),VTL1H2/UN=VTL499.  
.57-RTW(VTL1H1-L00...S1TEL/STO  
.00-EDITING COMPLETE.  
.00-LG0.  
.00-STOP  
.04-COMPUTER UNITS AT.100 P = 1.  
.04-CP 1.680 SEC. \$ 0.88  
.04-AC4 14.373 sec. \$ 0.09  
.04-IO 1.895 SEC. \$ 0.09  
.04-TM 19.478 sec. \$ 0.09  
.04-TAPES SCHEDULED 00  
.04-PACKS SCHEDULED 00  
.04-SERVICE CHARGE \$ 2.20  
.04- \$ -----  
.04-SUBTOTAL \$ 3.17

NADC-81259-60

APPENDIX C

Program Listings

A listing of the FORTRAN source code for the main STO program and a four degree-of-freedom interpolating subroutine TAKE5 is presented.

PROGRAM STC 7-7-74 JPT=1 PTN 4.04423 81/09/27 10,15,43 PAGE 1

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1      CSTD011
2      PROGRAM STD (INPUTJ, JUTPUT, TAPE8, TAPE9=INPJT)
3      ***** CREATED BY KJBL'S ON APRIL 1977. *****
4      ***** J1=1,517N TITLE(1),ICOPY(L01,RUNJDATA(33),<(4),AGJDATA(33)). *****
5      * PHJDATA(33)
6      C043DPRINT/NPRINT
7      READ AGJDATA(NR,LR,MU,L,LEVE,LRA,LRF,IVAC,IMOMENT,LEVENS,ITYY,ITYCG
8      INTEGER SEGMENT
9      NAMELIST/DATA/LPH4,S,DELTA,NCF,NIA,NUS,PLR,LRA,LRF,REVTIME,DT,
10     PIRPRINT/NPRINT,V3A44,P3C5,324E7,I1Y03,K53TCG,E1,DELMAX,P411,
11     BANDSL,FLUTE4,P412,P412A,P412B,P412C,P412D,ALP4444,ALP4444,ALT,
12     RUMSEGATJ,MLDRAG,DIST3,FAIL4,CEIL3SF,NDDEI,RETR12,PSI+DD, STJ 0013
13     D1,T444SF,PH1144F,F1144,P5INT,R3C0,IST44,SI44,GRSCALE,PAR,PH0NY STJ 0014
14     IC1J444 8 J1=RJNUTA(11)*AGJDATA(1)+PHJDATA(1)*0. STJ 0015
15     10 4*SEGMENT=NPRINT+IPRINT+NEDRAG+NSTD01+E*METRIC+NJ0JEI+3 STJ 0016
16     FLS3SAVPLDSE=3. STJ 0017
17     DT=0.9 S RA9=1. STJ 0018
18     REVTIME=ANGFLR+ALPH4IN+MLDRAG+DIST3RE +V*T=ALT=D=61+WF1+PH11+PH12+ STJ 0019
19     P51=642*DLFG+D3FS +VSTARREDATUM=FAILA=JEI=DEILDSE=0. STJ 0020
20     DEILDF=2SF*PH11AR=P41LRR+P5INT=AGY=DRDC=93C=d3D=R3C4=P434Y=0. STJ 0021
21     P2=2S+DELTA+P412A+P412B+P412C+ALP4444+ALP4444+J4+PS+JEITA3=02=0. STJ 0022
22     FLTE*P503, S 43*0.02 S 4E4+NEF=1. S 01=1. S 02=2. S DISTMAX=1.E5 STJ 0023
23     SIN<0=SINK=DSINK*CSIN4+C, S RDSCALE=1. STJ 0024
24     IF(ICOUNT.NE.0) GO TO 90 STJ 0025
25     IC=1 STJ 0026
26     20 READ 30,ICOPY STJ 0027
27     30 F1RMAT(2A1,A9,7A10) STJ 0028
28     40 F1RMAT(1A,2A1,A9,7A10) STJ 0029
29     IF(E3F(1)) 60,50 STJ 0030
30     50 I=1C+2 STJ 0031
31     WRITE(1,30) ICOPY STJ 0032
32     PRINT NC,ICOPY STJ 0033
33     IF(IC.NE.0,AN0,ICOPY(21,E1,14)) GO TO 60 STJ 0034
34     60 T1 20 STJ 0035
35     61 07 T1 1,I,C STJ 0036
36     73 BACKSPACE 9 STJ 0037
37     READ DATA STJ 0038
38     READ3D,TITLE STJ 0039
39     CALL T0,A5(1,0,0,0,0,ZD,F4X7Z) STJ 0040
40     P0 FORMAT(8A1) STJ 0041
41     GO T3 L10 STJ 0042
42     90 REWIND 3 STJ 0043
43     READ(3,DATA) STJ 0044
44     READ 3D,ICOPY STJ 0045
45     IF(E3F(9)) 750,130 STJ 0046
46     100 P11F 4D,ICCPY STJ 0047
47     BACKSPACE 9 $ READ DATA STJ 0048
48     110 PH2I=PH12 STJ 0049
49     ALPH4A=ALPHA STJ 0050
50     PH11=PH11 STJ 0051
51     PH11=(PH11+ANGFLR)*3.141592654/180. STJ 0052
52     IF(SEGMENT,E3,0) GO T3 120 STJ 0053
53     LEVE4=LRA+MU*L4 $ DELVER=LRA+LRF STJ 0054
54     120 VVV+DD STJ 0055
55     IF(ICOUNT.EQ.0) PRINT 13J,TITLE STJ 0056

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PROGRAM STO	74/75 DPT#1	FTN 4.0+42E	81/07/25. 10.19.43	PAGE 2
	130 FORMAT(1H1, //, 10X, *4STO) TAKEOFF PERFORMANCE ESTIMATION, //, 10X, 3a(STO 0058 (I=1, //, 34IC, //) 1CJNT=0 T35d=v PRINT 140, * 140 FORMAT(1A4, *10X, *8, 10X, 3a(STO 0059 *INITIAL GROUND RUN PARAETERS*, /) IF(IPRINT,NE,0) PRINT 150 150 FORMAT(10X, 120(14S), /, 10X, 3a(STO 0060 , /, T02, *BALANCE, F11L, FN4, /, 10X, *CL, CD, CR, A/G, R4D, DELTAE, /, 10X, *ALP, STO 0061 , /, 4, *ALPHAO, IVYCG, VCG, /, 10X, *REF, DELTAE, /, 10X, *RDC, ACCY, /, 1, STO 0062 *0, *ASINKA, VSINK, JS14K, /, 10X, 120(14S)) 1F14ETRIC,NE,0) ALT=ALT*.3343 CALL AT4JS(ALT, A1, A2, A3, A4, A5, A6, A7, A8) IF(4ETRIC,NE,0) J1 TO 150 ALT=ALT*3.2E039995 A5=A5*3.290638895 A3=A2*2.3769E-3 AFLOTEM=FLDTEM*459.7 A5=A5*SOR(T, AFLOTEM/510.7) A3=A3*918.7/AFLOTEM GO TJ 170 180 AFLOTEM=FLDTEM*273.16 A5=A5*SORT(AFLDTEM/288.16) A3=A3*288.16/AFLDTEM 170 EUATJ=EDATU4*3.141592654/180. G032,1761 IF(4ETRIC,NE,0) G=9.8 GOGC=1, S IF(4ETRIC,NE,0) GOGC=9.3 ***GOGC J=1 S MAC=0, S COLNT=(1.25/DT)*1.0E-1w S I=COUNT S M=I+1 180 MAC=V/A5 J=j+1 S IF(J>GE,1) J=1 T0U4=T S IF(T0U4>T, REVTIME) T0U4=REVTIME P4I2=P4I2 IF(SEGMENT,NE,0) GO TO 210 ***** FIRE ENGINE NOZZLE VARIATION IF(P4I1AR,EQ,0, .JR,V,LT,RSF) GO TO 190 P4I1=P4I1*P4I1R*GT IF(P4I1,GT,P4I1R) P4I1=P4I1R P4I2=(P4I1+ANGFRL)*3.141592654/180. C FDR ANY FUTURE TABLE LOOK UPS USE P4I1 ***** 190 I=(V,LT,RS) GO TJ 200 P4I2=P4I2*P4I2R*GT IF(P4I2,GT,P4I2R) P4I2=P4I2R 200 IF(V,LT,PS) GO TJ 210 ALPHA=ALPHA+ALPHAR*DT IF(ALPHA,GT,ALPHAR) ALPHA=ALPHAR 210 IF(E1,NE,0,) CALL TL035(11,MAC4,01,T0U4,0,.,#F1) CALL TL035(11,MAC4,02,T0U4,0,.,#F2) #F1=dF1*4EF*GOGC #F2=dF2*NE*#GOGC IF(E1,NE,0,) CALL TL035(10,MAC4,01,T0U4,0,.,FN1) CALL TL035(10,MAC4,02,T0U4,0,.,FN2) CALL TL035(12,P4I1,i,.,J,.,0,.,FL3SSF) CALL TL035(12,P4I2,2,.,J,.,0,.,FL3SSA)	STO 0063 STO 0064 STO 0065 STO 0066 STO 0067 STO 0068 STO 0069 STO 0070 STO 0071 STO 0072 STO 0073 STO 0074 STO 0075 STO 0076 STO 0077 STO 0078 STO 0079 STO 0080 STO 0081 STO 0082 STO 0083 STO 0084 STO 0085 STO 0086 STO 0087 STO 0088 STO 0089 STO 0090 STO 0091 STO 0092 STO 0093 STO 0094 STO 0095 STO 0096 STO 0097 STO 0098 STO 0099 STO 0100 STO 0101 STO 0102 STO 0103 STO 0104 STO 0105 STO 0106 STO 0107 STO 0108 STO 0109 STO 0110 STO 0111 STO 0112 STO 0113 STO 0114		

PROGRAM	STO	74/74	OP1+1	FT4 4.6+423	91/03/26. 10.18.43	PAGE	3
115						STJ 0115	
						STJ 0116	
						STO 0117	
C **** * INDUCED AERC						STJ 0118	
						STJ 0119	
						STJ 0120	
120						STJ 0121	
						STJ 0122	
C ***** * FN1=(FN1-FLOSSF*FN1)*NEF * FN2=(FN2-FLOSSA*FN2)*NEA						STJ 0123	
						STJ 0124	
						STJ 0125	
121						STJ 0126	
						STJ 0127	
						STJ 0128	
						STJ 0129	
						STJ 0130	
						STJ 0131	
						STJ 0132	
						STJ 0133	
						STJ 0134	
132						STJ 0135	
						STO 0136	
						STO 0137	
						STO 0138	
						STO 0139	
						STO 0140	
						STJ 0141	
						STJ 0142	
						STJ 0143	
						STJ 0144	
						STJ 0145	
						STJ 0146	
						STJ 0147	
						STJ 0148	
						STJ 0149	
150						STO 0150	
						STJ 0151	
						STJ 0152	
						STJ 0153	
220						STJ 0154	
						STJ 0155	
						STO 0156	
						STJ 0157	
						STJ 0158	
						STJ 0159	
						STJ 0160	
						STJ 0161	
						STJ 0162	
						STJ 0163	
						STJ 0164	
						STJ 0165	
165						STO 0166	
						STJ 0167	
						STJ 0168	
						STJ 0169	
170						STO 0170	
						STJ 0171	

PROGRAM STN	74/74 3PT+1	FTV 4.5+426	31/39/26 10.19.63	PAGE 4
	270 FORMATT(10X,*INSTANTANEOUS ROTATION AT DEI*)		ST3 0172	
	PHOTO=-.13 S GJ TO 180		ST3 0173	
178	280 IF(BALANCE.GT.0..JR.EFAILA.EQ.0..DEI.NE.0.) GJ TO 290		ST3 0174	
	DEI=.1, MEANNEA=.5 & MEANREF=1.L)SF S GJ TO 180		ST3 0175	
	291 D=02 S VVZ T=T0DT S =-((F1+F2)*DT/3600.)		ST3 0176	
	IF(P43NT.EG.=-.13) GJ T1 355		ST3 0177	
	[(3.LT.DISTMAX) GJ T1 310		ST3 0178	
	PRINT 303		ST3 0179	
180	300 FORMATT(10X,*CASE TERMINATED (DISTMAX EXCEEDED)*)		ST3 0180	
	GJ T1 730		ST3 0181	
	310 IF(ICOUNT.GT.100) GJ T1 610		ST3 0182	
	IF(BALANCE.GE.0..JR.RJC.EQ.0.) GJ TO 330		ST3 0183	
	MU=0,S ASYL=AGY & DRCL=DRDC		ST3 0184	
185	AGY=(-BALANCE)*G/4		ST3 0185	
	AGYA=(AGY+AGYL)*.5		ST3 0186	
	DRCL=DRCL+AGYA*D		ST3 0187	
	AROC=(DRDC+DRCL)*.5		ST3 0188	
	RJC+=RCH+AROC*D		ST3 0189	
190	IF([METRIC.NE.0.A40.J.E1.I] PRINT 320,DRDC,AGYA		ST3 0190	
	320 FORMATT(1X,*CLIMB DATA*,2(10X,E20.5))		ST3 0191	
	IF(DROC.GE.ROC) GJ TO 430		ST3 0192	
	GJ T1 350		ST3 0193	
	330 IF(SINK.GT.0..A40.SINKE.LE.0.) GJ TO 500		ST3 0194	
195	340 IF(BALANCE.LE.0.) GJ T1 433		ST3 0195	
	350 ICOUNT=ICOUNT+1		ST3 0196	
	GJ T1 180		ST3 0197	
	360 IF(METRIC.NE.0) GJ T1 380		ST3 0198	
	PRINT 370,D,V,T,d		ST3 0199	
200	370 FORMATT(10X,*DISTANCE = *,E20.5,* FT.,/,10X,*VELOCITY = *,E20.5,*		ST3 0200	
	(FT./SEC.*/,/,10X,*TIME = *,5X,E20.5,* SEC.*/,/,10X,*END WEIGHT FOR T*)		ST3 0201	
	(IS PHASE IS *,E20.5,* POUNDS MASS*)		ST3 0202	
	GJ T1 400		ST3 0203	
	380 PRINT 390,D,V,T,d		ST3 0204	
205	390 FORMATT(10X,*DISTANCE = *,E20.5,* 4.0/,10X,*VELOCITY = *,E20.5,*		ST3 0205	
	(4.0/SEC.*/,/,10X,*TIME = *,5X,E20.5,* SEC.*/,/,10X,*END WEIGHT FOR T*)		ST3 0206	
	(IS PHASE IS *,E20.5,* KILOGRAMS *)		ST3 0207	
	400 IF(SEGMENT.EQ.0) GJ TO 630		ST3 0208	
	GJ T1 (500,610), SEGMENT		ST3 0209	
210	410 PRINT 420		ST3 0210	
	420 FORMAT(10X,*T03 MUCH TIME*)		ST3 0211	
	GJ T1 365		ST3 0212	
	430 PRINT 440		ST3 0213	
215	440 FORMATT(10X,*VEHICLE IS AIRBORNE*)		ST3 0214	
	ISINK=104 FT,		ST3 0215	
	IF(METRIC.NE.0) [ISINK=LWH 4.		ST3 0216	
	IF(SINK.GT.0.) PRINT 450,JSINK,ISINK		ST3 0217	
	450 FORMATT(10X,*MAXIMUM SINK DISTANCE IS *,E20.5,A10)		ST3 0218	
	IF(DEI.NE.0.JR.RJC.NE.0.) PRINT 460		ST3 0219	
220	460 FORMATT(10X,*DEI AT PSEUDO LIFTOFF*)		ST3 0220	
	IF(RJC.E4.0.) GJ TO 493		ST3 0221	
	IROC=10M FT./SEC.		ST3 0222	
	IF(METRIC.NE.0) IROC=104 M./SEC.		ST3 0223	
	PRINT 470,RCC,IRJC		ST3 0224	
225	470 FORMATT(10X,*VEHICLE HAS A R/C OF *,E20.5,A10)		ST3 0225	
	IROC=104 FT.		ST3 0226	
	IF(METRIC.NE.0) IROC=104 M.		ST3 0227	
	PRINT 480,RCC,IRJC		ST3 0228	

PROGRAM STD 74/74 DPT=1 PTH 4.54428 81/09/28 10.19.43 PAGE 5

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        480 PRINT(10X,"VERTICAL HEIGHT IS ",E2C.5,ALJ)
490 GJ TJ 360 STJ 0229
500 PRINT 510 STJ 0230
510 FORMAT(10X,"AUTO ROTATION IS OCCURRING")
      GJ TJ 630 STJ 0231
C   ALP44 CORRECTION AUTO ROTATION$#####$#####$#####$#####
520 IF(SEGMENT,6T,1,AND,ALP44,GE,ALPHMIN) GO TJ 550 STJ 0232
530 CALL TL035(30.0,0.0,0.0,0.0,YCG) STJ 0233
      CALL TL035(31.0,0.1,0.0,0.0,LCG) STJ 0234
      CALL TL035(31.0,0.2,0.0,0.0,TCG) STJ 0235
      DCSS=RCG*+2*YCG*+2 S LRC=XCG S LRF=DLEVER+FCG STJ 0236
      ITY=ITYCG*+2*DCCG S IF((RC,E,0,J,3)) GO TO 531 S WR=LRC-FCG S FRC=1. STJ 0237
531 LRC=CG+DR S DALP44R=DT*+2*(+F1*DLEVER/ITY) STJ 0238
      DALP44D=DALP44*18L,3.161532694 STJ 0239
      ALPHA=ALPHA+DALP44D STJ 0240
      IF(SEGMENT,6T,1,AND,ALP44,GE,ALPHMIN,AND,ITRIP,3,0) GO TJ 550 STJ 0241
      ITRIP=0 STJ 0242
      IF(IPPRINT,NE,0,4ND,0,J,3,I) PRINT 540,ALPHA,DALPHAD,ITYCG,XCG,YCG STJ 0243
540 FORMAT(10X,(5X,E12.5),/1X,3(154 AUTO ROTATION )) STJ 0244
      GJ TJ 260 STJ 0245
      CCCCCCCCCCCCCCCCC TRY TO COUNTER ROTATION BY ELEVATOR STJ 0246
550 DELTAE=1. S ITRIP=0 STJ 0247
560 CALL SNEST(N,RF,DELTAE,DELTAE,310.4305,DL,ABDYL,XCHECK,XLCJ) STJ 0248
      IF(IPPRINT,NE,0,4ND,0,J,3,1) PRINT 570,N,RF,DELTAE STJ 0249
570 FORMAT(10X,25(1#),5X,110,2(10X,E12.5)) STJ 0250
      IF(DELTAE,LT,DELYAX) GJ TJ 580 STJ 0251
      DELTAE=DELMAX S =0 S ITRIP=1 STJ 0252
580 CALL TL005(14,ALPHA,DELTAE,P42I,VSTAR1,CL) STJ 0253
      CALL TL005(13,CL,DELTAE,P42I,VSTAR1,CD) STJ 0254
      CALL TL005(17,CL,DELTAE,P42I,VSTAR1,CM) STJ 0255
      DCSS=V*+2*A3*S STJ 0256
      DRDR+DRAGDSTRE+DCEILDF+DDFS STJ 0257
      L=+3*CL*V*+2*A3*S STJ 0258
      L=+3*LFG STJ 0259
      BALANCE=4-L-FGV STJ 0260
      DVDT*G *(FSH-DR-4U*BALANCE)/# STJ 0261
      V2V*DV STJ 0262
      A3C4T*3*CR*V*+2*A3*S*MAC STJ 0263
      RF=(LEVER*BALANCE-MQ4ENT)/(DLEVER) STJ 0264
      IF(PITCH,LE,0,J) GO TJ 590 STJ 0265
      ANG4ESS=LRA*COS(PITCH)+U*LRA+SIN(PITCH)+LR*SIN(PITCH)-LZ*SIN(PITCH) STJ 0266
      PITCH= STJ 0267
      AF=(BALANCE+ANG4ESS-404ENT)/(LRF+ANG4ESS+COS(PITCH)) STJ 0268
590 DCSS=590T*(V2-4DD)*#2-(V-4DD)*#2./DV STJ 0269
      IF(ITRIP,330,0) STJ 0270
600 IF(4) 560,260 STJ 0271
610 PRINT 620 STJ 0272
620 FORMAT(10X,"ELEVATOR CORRECTION ATTEMPTED") STJ 0273
C ***** LIFTOFF CHARACTERISTICS ***** STJ 0274
C ***** LIFTOFF CHARACTERISTICS ***** STJ 0275
250 630 PRINT 640 STJ 0276
640 FORMAT(//,10X,"LIFTOFF CHARACTERISTICS",/) STJ 0277
      AGV=(FG-DR-U*BALANCE)/# STJ 0278
      IF(P43NY,NE,0,-,3) GJ TJ 670 STJ 0279
      PRC=V*60.0*(L+F3V-d)/FG
      DCSS=104 FT/MIN STJ 0280
      STJ 0281
      STJ 0282
      STJ 0283
      STJ 0284
      STJ 0285

```

PROGRAM STEP	74/76 JPF=1	FTN 4.0+420	E1/03/25 10.18.43	PAGE 5
	IF(I=ETRIC.EQ.0) GO TO 650		STO 0286	
	I=72+10H 9/SEC		STO 0287	
	PHRC=PHRC/60.		STO 0288	
240	650 PRINT 650,PHRC,I=3C		STO 0289	
	OC. F04447(10X,INSTANTANEOUS R/C IS *E20.5,A10)		STO 0290	
	670 IF(I=ETRIC.EQ.0) GO TO 570		STO 0291	
	PRINT 600,AGK,L,3A,PJV,F3.4		STO 0292	
	680 F04447(10X,INSTANTANEOUS ACCELERATION *E20.5,GES*,/10X,		STO 0293	
	**LIFT **,10X,E20.5,* POUNDS FORCE**,/10X,DRAF **,10X,E20.5,		STO 0294	
295	** POUNDS FORCE**,/10X,VERTICAL GROSS THRUST **,2X,E20.5,		STO 0295	
	** POUNDS FORCE**,/10X,E20.5,VERTICAL GROSS THRUST **,E20.5,		STO 0296	
	** POUNDS FORCE**)		STO 0297	
	GO TO 710		STO 0298	
300	590 PRINT 700,AGK,L,JR,PJV,F3.4		STO 0299	
	700 F04447(10X,INSTANTANEOUS ACCELERATION *E20.5,GES*,/10X,		STO 0300	
	**LIFT **,10X,E20.5,* NEUTONS **,10X,DRAF **,10X,E20.5,		STO 0301	
	** NEUTONS **,10X,VERTICAL GROSS THRUST **,2X,E20.5,		STO 0302	
	** NEUTONS **,10X,VERTICAL GROSS THRUST **,E20.5,		STO 0303	
	** NEUTONS **)		STO 0304	
305	710 IF(RJN=L.E.C.) GO TO 730		STO 0305	
	CALL UPDATE(AGDATA,D,AGK)		STO 0306	
	IF(P40NY.EQ.-13) CALL UPDATE(PHDATA,D,PHRC)		STO 0307	
	IF(P5INT.LE.3.) GO TO 720		STO 0308	
	CALL UPDATE(RUNDATA,D,PS)	S GO TO 730	STO 0309	
310	720 CALL UPDATE(RUNDATA,D,T3G4)		STO 0310	
	730 PRINT 700		STO 0311	
	740 F04447(/1X,22(64 NEXT ),/)		STO 0312	
	63 T3 10		STO 0313	
315	750 IF(RJN=L.E.C.) STJ2		STO 0314	
	IF(P40DATA(1).EQ.0.) I GO TO 770		STO 0315	
	PHRC=SPLN01(1,P40DATA,RJN)		STO 0316	
	PRINT 700,PHRC,I=3C		STO 0317	
	760 F04447(10X,INSTANTANEOUS INTERPOLATED R/C IS *E20.5,A10)		STO 0318	
	770 AG=SPLN01(1,AGDATA,RUN)		STO 0319	
320	RJN=SPLN01(1,RJN,DATA,RUN)		STO 0320	
	K(1)=6M FEET S <(2)+64 T200 S <(3)=10H POUNDS MA S K(4)=2HSS		STO 0321	
	IF(I=ETRIC.EQ.0.AND.PSINT.EQ.0.) GO TO 730		STO 0322	
	K(1)=6M MA S <(3)=10H KILograms S K(4)=2H		STO 0323	
	IF(P5INT.EQ.0.) GO TO 730		STO 0324	
325	K(2)=6M PS S K(3)=10H M./SEC.		STO 0325	
	IF(I=ETRIC.NE.0) GO TO 780		STO 0326	
	<(1)=64 FEET S <(3)=104 FT./SEC.		STO 0327	
	780 PRINT 700,RUN,K(1),K(2),RJN,K(3),K(4),AG		STO 0328	
330	790 F04447(10X,931C SPLINE INTERPOLATION OF THE ABOVE DATA POINTS STO 0329			
	***/.25X, FOR A RUN OF *E20.5,A10,*THE*,A5,*VIS*,*E20.5,A10,*A3*/.60X STO 0330			
	*AND THE HORIZONTAL ACCELERATION IS *E20.5,GES*)		STO 0331	
	STOP		STO 0332	
	???????????????????? SINK JPF THE 334 CALCULATIONS		STO 0333	
335	800 IF(RJN.EQ.0) GO TO 810		STO 0334	
	IF(*3.GT.0.) PS=V S IF(RSF.GT.C.) RS=V S IF(RSF.GT.3.) RS=V S VU=JSTO 0335			
	810 ASINKL=ASINK S VSINKL=VSINK S DSINKL=DSINK		STO 0336	
	ASINK=BALANCE*G/4		STO 0337	
	ASINKA=(ASINK+ASINKL)*.5		STO 0338	
	VSINK=VSINKL+ASINKA*DT		STO 0339	
	VSINKA=(VSINK+VSINKL)*.5		STO 0340	
340	DSINK=DSINKL+VSINKA*DT		STO 0341	
	IF(IPRINT.NE.0.AND.J.EQ.1) PRINT 920,ASINK,VSINK,DSINK		STO 0342	

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0235219 STD 74/74 JPT=1

FTY 4.69423

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PAGE 7

020 FJN447(1X,0SINC DATA0,3(101,E23.9))  
60 T3 340

STD 0343

STD 0344

345

\*\*\*\*\*STD 0345  
END STD 0346

SUBROUTINE TAKES5      7-74      JPT=1      F77 6.5+92.      81/09/29 10:13:43      PAGE      1  
 1      CTAKES5  
       SUBROUTINE TAKES5(II,JD,X,Y,Z,FXYZ)  
       \*\*\* MODIFIED CTAKES5 TO INCLUDE FCJR INDEPENDENT VARIABLES- DEC 3/77  
       COMMON /TSIZE/NMAX,TDATA(3300)  
       COMMON/PRINT/NPRINT  
       DIMENSION A(100),IDD(5),SIRIUS(30)  
       DATA NMAX,NTBL/3300/0/  
       DATA NPRINT/0/  
       ENTRY TAKES5  
       MRIGEL=0  
       ITPRT = NPRINT  
       IF(NTBL.LE.0) GO TO 20  
       LDC=61  
       DO 13 I=1,NMAX  
 10      TDATA(I)=0.  
       ILAST=1  
 20      READ 30, IP,ITAB4  
 25      FORMAT (I1,I4,7.5)  
       1  
 20      IF(IITAB4.NE.0) GO TO 110  
       NTBL = NTBL+1  
       ENIF=TDATA(NTBL)-ITAB4  
       TDATA(NTBL+30)=LDC  
 40      IF(NTBL.LE.1) GO TO 210  
 45      D3=53 LYRA=2,NTBL  
       IF(ENIF.EQ.TDATA(LYRA-1)) GO TO 50  
 50      CONTINUE  
       GO TO 210  
 60      IARIES=MERAK=TDATA(LYRA+29)  
       MRIGEL=MRIGEL+1  
       STRIJS=(MRIGEL)\*ENIF  
       LIBRAM=100000  
       IZAR=LDC-1  
       DO 70 IRK=1,NTBL  
       LIBRA=TDATA(IRK+30)  
       IF((LIBRA.GT.MERAK).AND.(LIBRA.LT.LIBRAM)) LIBRAM=LIBRA  
 70      CONTINUE  
       LEO=LIBRAM-MERAK  
 80      D3=93 NEKKAR=LIBRAM,IZAR  
       TDATA(NEKKAR)=TDATA(MERAK)  
 85      MERAK=MERAK+1  
       D3=93 NEKKAR=LDC  
       LLDC=TDATA(NEKKAR+30)  
       IF(LLDC.GT.IARIES) TDATA(NEKKAR+30)=LLDC-LEO  
 90      CONTINUE  
       TDATA(LYRA+29)=LDC-LEO  
 95      D3=100 IBALT=MERAK,LDC  
 100     TDATA(IBALT)=0.  
       LDC=MERAK  
 110     NTBL=NTBL-1  
       GO TO 210  
 110     NMEM=NMAX-LOC  
       IF(NTBL.LE.1) GO TO 140  
 120     NMME=1  
       D3=130 L=2,NTBL  
       41=L-1

TAK50001  
           TAK50002  
           TAK50003  
           TAK50004  
           TAK50005  
           TAK50006  
           TAK50007  
           TAK50008  
           TAK50009  
           TAK50010  
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           TAK50054  
           TAK50055  
           TAK50056  
           TAK50057

SUBROUTINE TAKED 74/74 JPT=1 FTN 4.5+2c 31/03/2b, 10.10.43 PAGE 2

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      K2=L
      IF(TDATA(<1)<LT,TDATA(<2)) GJ TJ 130
      XSAVE=TDATA(K1)
      TDATA(K1)=TDATA(<2)
      TDATA(K2)=XSAVE
      XSAVE=TDATA(K1+3)
      TDATA(K1+3)=TDATA(K2+3)
      TDATA(K2+3)=XSAVE
      NDO=N6
      130 CONTINUE
      IF(NDNE,20,3) GJ TJ 120
      140 IF(II.LE.0) GJ TJ 470
      IF(NPRINT,0,0) GJ TJ 150
      PRINT 150
      150 FORMAT(1I4)
      160 PRINT 170,NTSL
      170 FORMAT(1X,45HTABLE DATA INPUT SUMMARY,1X,I2,1X,5HTABLES//,2d
      1X,45HTABLE NUMBER REFERENCE NUMBER ARRAY LOCATION )
      PRINT 190,((N,TDATA(1),TDATA(N+30)),4=1,NTSL)
      180 FORMAT(32X,I2,I2,X,F5.0,194,X,F5.0)
      PRINT 190,MAX,NEM
      190 FORMAT(1/,35X,24HDATA STORAGE ALLOCATION ,14,35X,24HDATA STORAGE)
      200 FJRNAT(10X,THE FOLLOWING TABLES HAVE BEEN REPLACED,,515X,FIG,J,*)
      Z=J,/(8*(5X,F10.J,*,*))
      PRINT 1111,((4,TDATA(M)),4=1, LOC)
      C1111 FORMAT(5(1X,I4,E12.5))
      RETURN
      210 IP=1
      IF(NPRINT,0,0) IP=0
      PRINT 30, IP,ITA3D
      IF(IPPRINT,0,0) PRINT 320
      220 FORMAT(1111)
      ICC = 0
      L=LJC
      IJ=4
      230 DO 230 ICL=1,5
      230 IJ=(ICL)*4H
      240 IDL=ID
      READ 250, ID,4,(A(I),I=1,4)
      250 FJRNAT(44,I3,34,(T1,7F10.0))
      IF(IJ.EQ.4)HEDT 1 GJ TJ 20
      ICC=ICC+1
      IF((CC.LE.5) .AND.(ICC).EQ.ID)
      IF((IJ.EQ.IDL) .AND.(TJ.EQ.35))
      IF((IJ.NE.IDD(5))) GJ TJ 250
      IF((IJ.EQ.IDD(3))) GJ TJ 350
      LDC=L
      L=LX
      GJ TJ 290
      260 TDATA(LOC)=N
      L=LDC
      IF((IJ.EQ.IDD(2))) GJ TJ 390
      270 IF((IJ.EQ.IDD(4))) LX=L
      IF((IJ.NE.IDD(3))) GJ TJ 390
      LY=L
      TAK50058
      TAK50059
      TAK50060
      TAK50061
      TAK50062
      TAK50063
      TAK50064
      TAK50065
      TAK50066
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      TAK50112
      TAK50113
      TAK50114

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SUBROUTINE TAKES 74/74 JPT=1 FTV 4.0+428 31/09/26 10.19.43 PAGE 3

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115      LZ=LZ+1
      G3 T3 330
      280 IF(IP.EQ.0) G3 T3 330
      LY=LY+1
      IF(NPRINT.NE.0) PRINT 290,IDO(1),TODATA(LY)
120      290 FJRMAT(LX,A4,L4,E13,5)
      IF(NPRINT.NE.0) PRINT 300,IDO(2),TODATA(LZ),IDO(3),TODATA(LY)
      300 FJRMAT(LX,A4,L4,E13,5),LX,A4,L4,E13,5)
      JE=0
      RN=
125      LF=LK
      310 NP=4
      IF(V.GT.8)NP=3
      V=V-2
      LE=LF+NP
      LF=LF+1
      IF(NPRINT.NE.0) PRINT 320,IDO(4),(TODATA(I),I=LF,LE)
130      320 FJRMAT(204,A4,LX,E13,5)
      LF=LE
      JE=JE+NP
      JP=JP+1
      IF(NPRINT.NE.0) PRINT 320,IDO(5),(A(I),I=JP,JE)
      JE=JE
      IF(V.GT.0) G3 T3 310
      330 D3 340 I=1,V
      340 TDATA(LJC)=A(I)
      L=LJC
      IF(IJ.E3.IDO(5)) TODATA(LJC+2)=1.
      LJC=L+3*NP+3
      IF(LJC.GT.NMAX)370,290
      350 TDATA(LJC)=TODATA(LX)
      L=LJC
      D3 350 I=1,V
      LJC=LJC+1
      360 TDATA(LJC)=TDATA(LX+I)
      G3 T3 280
      370 PRINT 380, ITABN3
      380 FJRMAT (11,32H*****TABLE OVER FILE ,TABLE ,15,11H NOT LOADED) TAK50153
      G3 T3 40
      390 LZ=LJC S Lw=Lw+1 S G3 T3 270
      ENTRY TL395
      **** SEARCH FOR CORRECT TABLE
      IF(IJ.LE.0) RETURN
      **** SEARCH FOR CORRECT TABLE
      160 M=M+TLB+1
      NL=1
      <@LAST
      XTAB=II
      KT=0
      165 4C0 KT=KT+1
      IF(KT.GT.6) G3 T3 470
      IF((XTAB-TDATA(K1)).EQ.0.) G3 T3 430
      IF(((XTAB-TDATA(K1)).LT.0.) G3 T3 410
      NL=" "
      G3 T3 420
      410 M=M<

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TAK50115  
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TAK50171

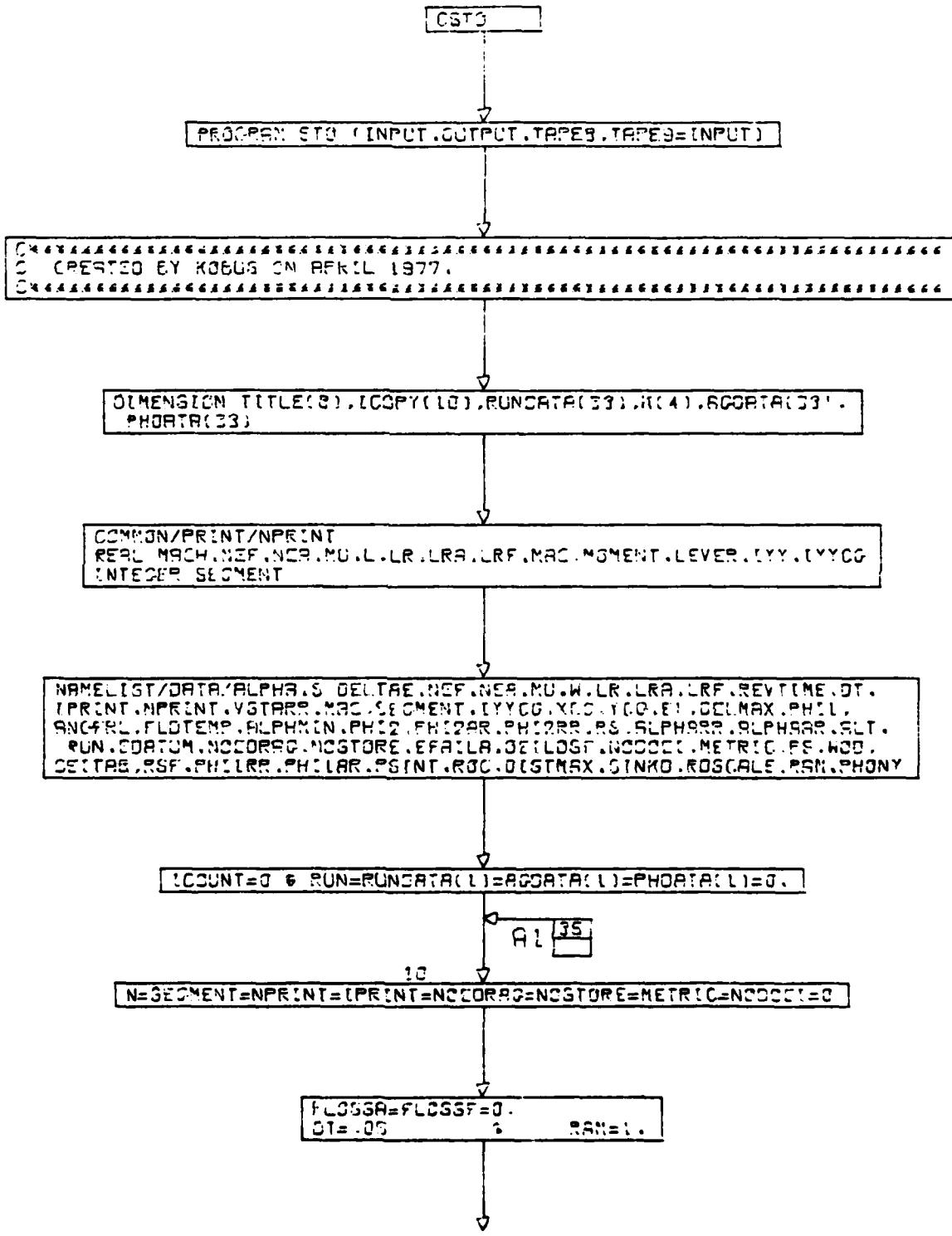
SUBROUTINE TAKES	74/74	OPT=1	FTN 4.5+420	01/09/28. 10.18.43	PAGE
					4
	626	K=(N4-NL)/2+N1			
	630	GJ T3 400			
	430	ILAST=N			
175	12=T3ATA(K+30)	[N2=T3ATA(12)		TAK50172	
	IY=3*INZ+12+3	IY=3*INZ+12+3		TAK50173	
	ID=IY	ID=IY		TAK50174	
	I2L=I2*INZ+1	I2L=I2*INZ+1		TAK50175	
180	I2Z=I2*2*INZ	I2Z=I2*2*INZ		TAK50176	
	DO 450 IZS=I2L,I2Z	DO 450 IZS=I2L,I2Z		TAK50177	
	INY=T3ATA(IY)	INY=T3ATA(IY)		TAK50178	
	IY=3*INY+IX+3	IY=3*INY+IX+3		TAK50179	
	ID=IY	ID=IY		TAK50180	
185	IY1=IY+INY+1	IY1=IY+INY+1		TAK50181	
	IY2=IY+2*INY	IY2=IY+2*INY		TAK50182	
	DO 450 IYS=IY1,IY2	DO 450 IYS=IY1,IY2		TAK50183	
	IX=IY+T3ATA(IX)	IX=IY+T3ATA(IX)		TAK50184	
	ID=3*INX+IX+3	ID=3*INX+IX+3		TAK50185	
190	IX1=IX+1*IX+1	IX1=IX+1*IX+1		TAK50186	
	IX2=IX+2*INX	IX2=IX+2*INX		TAK50187	
	DO 440 IXS=IX1,IX2	DO 440 IXS=IX1,IX2		TAK50188	
	T3ATA(IXS)=SPLN31(ID,T3ATA,W)	T3ATA(IXS)=SPLN31(ID,T3ATA,W)		TAK50189	
195	440 ID=ID+3*T3ATA(ID)+3	440 ID=ID+3*T3ATA(ID)+3		TAK50190	
	TUATA(IYS)=SPL491(IX,T3ATA,X)	TUATA(IYS)=SPL491(IX,T3ATA,X)		TAK50191	
	450 IX=ID	450 IX=ID		TAK50192	
	T3ATA(IZS)=SPL491(IV,T3ATA,Y)	T3ATA(IZS)=SPL491(IV,T3ATA,Y)		TAK50193	
	460 IV=IX	460 IV=IX		TAK50194	
	F=IX2=SPLN01(IZ,T3ATA,Z)	F=IX2=SPLN01(IZ,T3ATA,Z)		TAK50195	
200	470 RETURN	470 RETURN		TAK50196	
	E40	E40		TAK50197	
				TAK50198	
				TAK50199	
				TAK50200	
				TAK50201	

NADC-81259-60

APPENDIX D

Program Logic

Flow charts for the main STO program and the subroutine TAKE5 are presented.



```

REV TIME=ANGF RL=ALPHMIN=50PAC=0 STORE =V=T=AL T=0=t =WF1=PH11=PH12=
FN1=FN2=0LFG=00FG =VGSTAR=EDATUM=ETAILA=0E1=0E LOGI=0

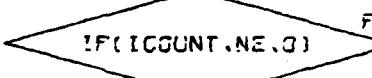
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001 *LOF=RSF=PH11AR=PH11RR=P5INT=ACY=0PDC=R0C=W0D=R0CH=PH0NY=0 .
WF2=RS=0ELTAE=PH12AR=PH12RR=ALPHARR=ALPHARR=RUN=PG=0E1TAB=0G=0 .
FL0TEMP=59 . $ MU=.02 $ NCP=NCF=1 . $ Q1=1 . $ Q2=2 . $ DISTMAX=1.E6
SINK0=ASINK=VSINK=0GINK=0 . $ R0SCALE=1 .

```

IF (ICOUNT.NE.0)



GO TO 90

4 P3

IC=1

A2 3

20 RE90 30 . !COPY

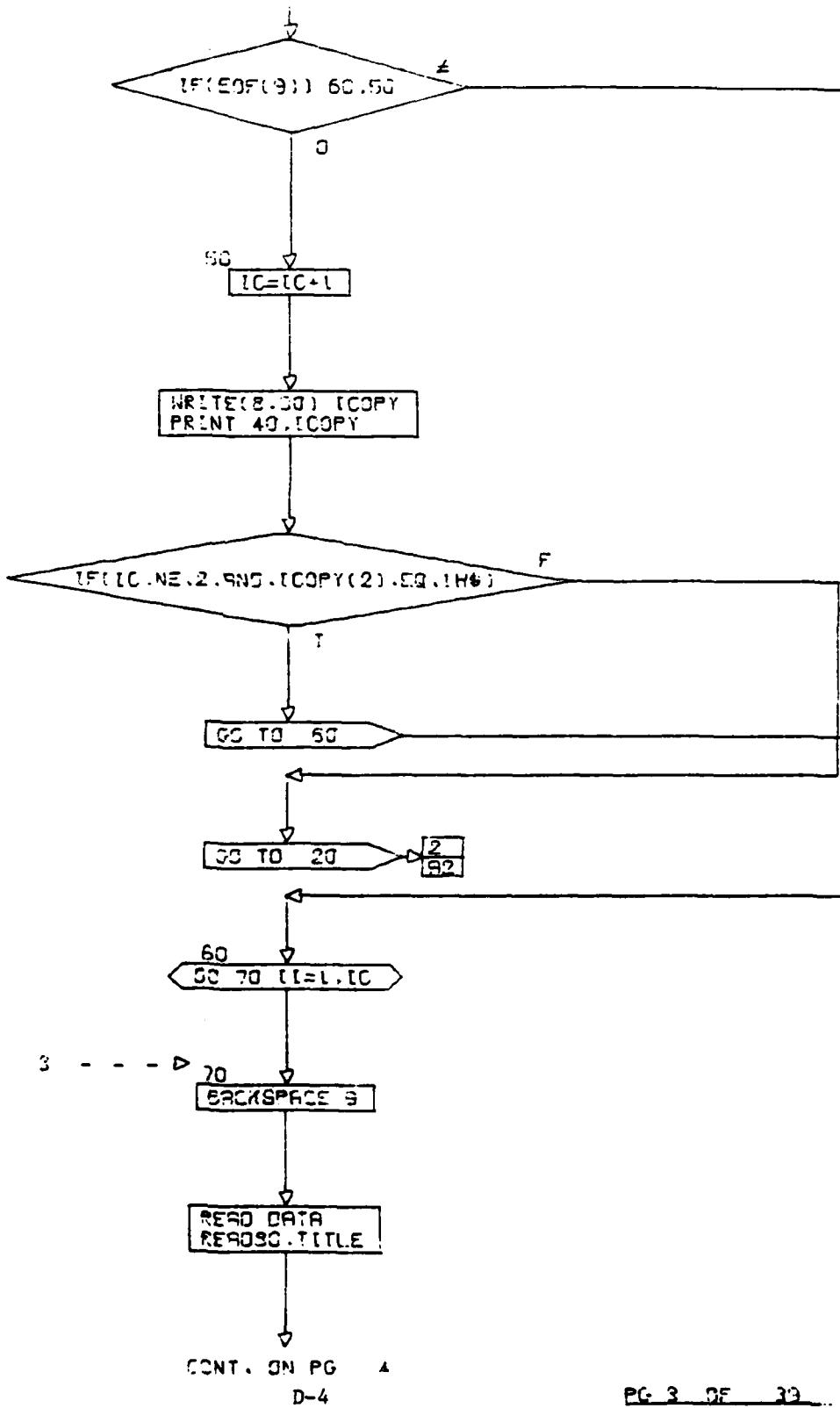
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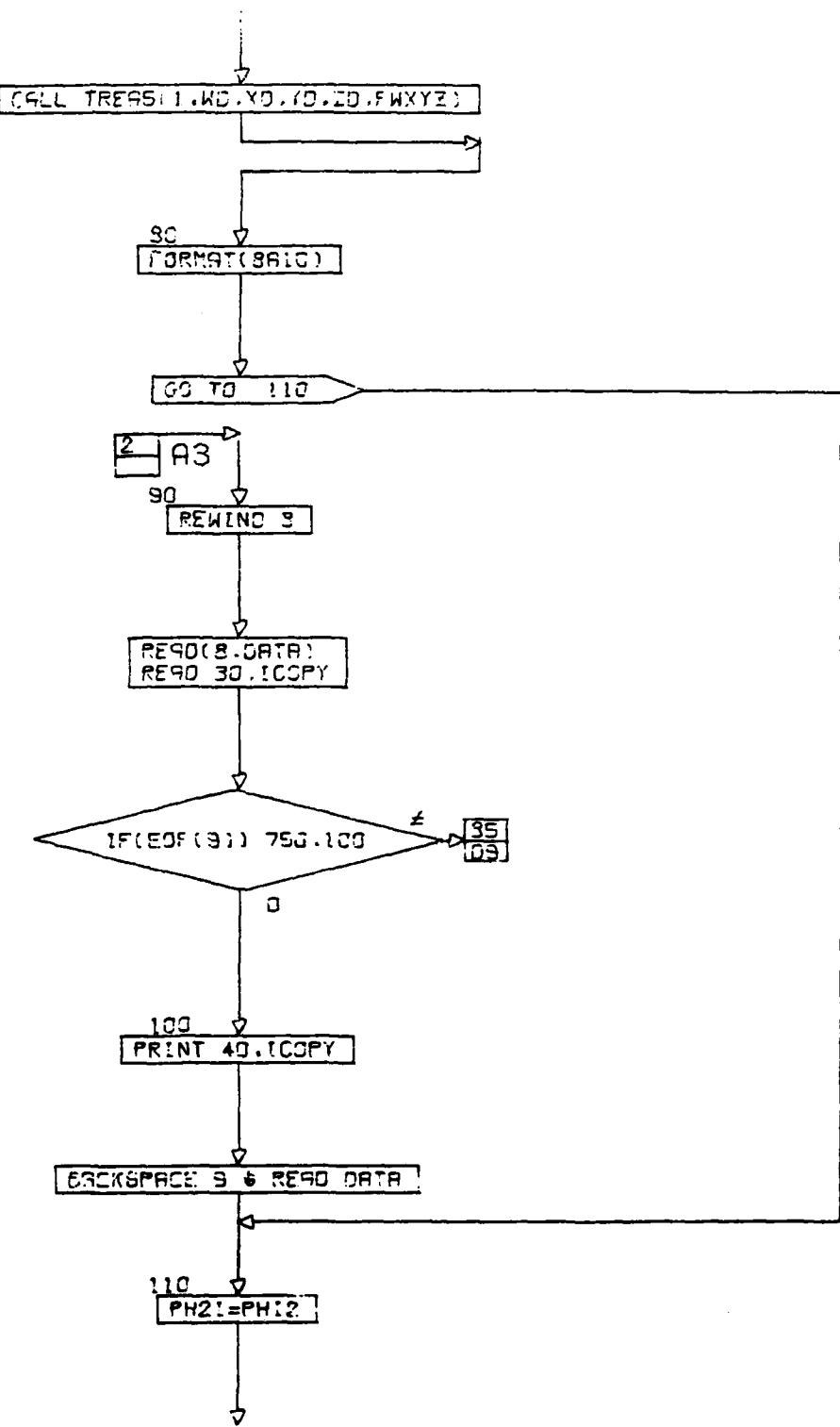
40 FORMAT(1X,2B1,AB,7A1C)

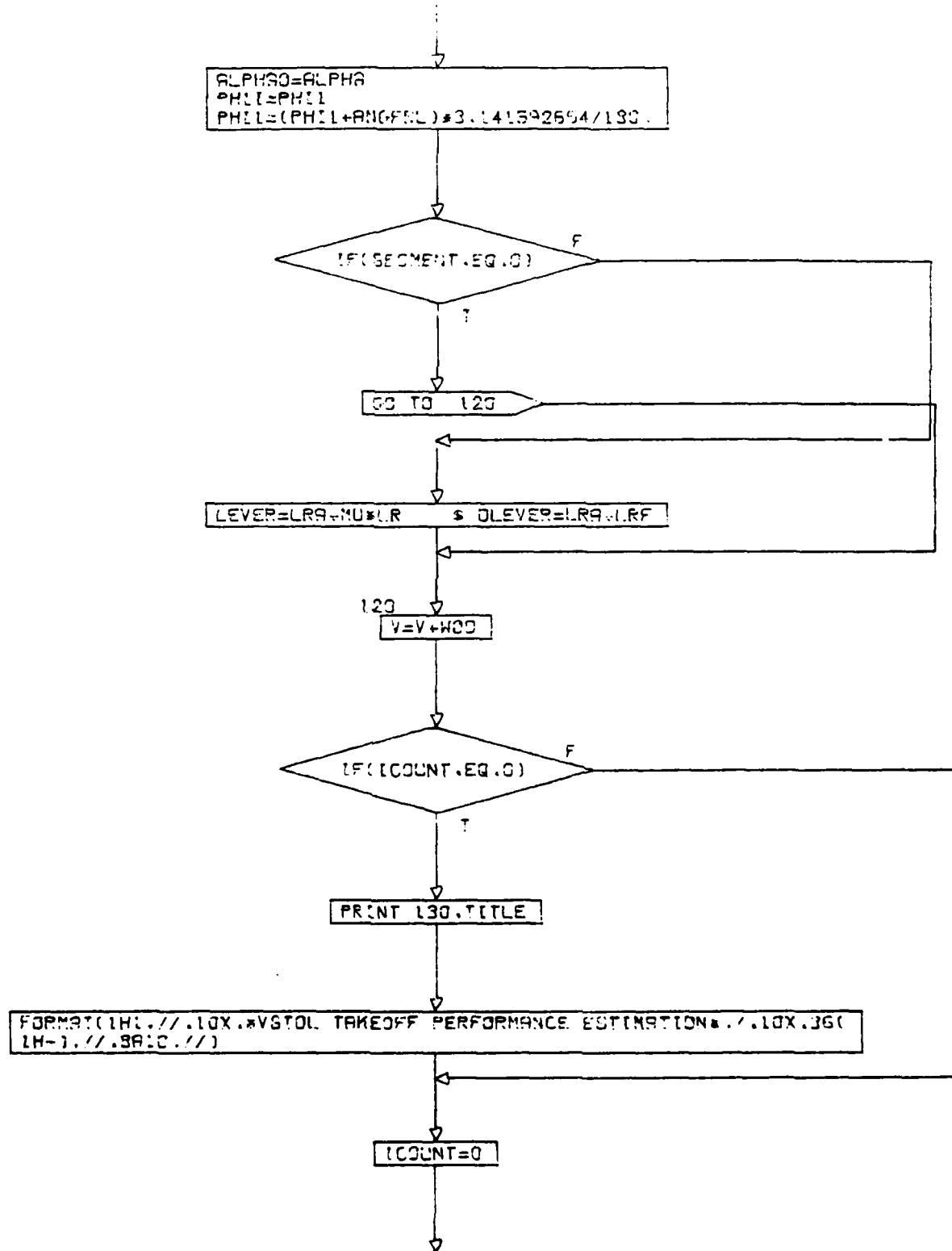
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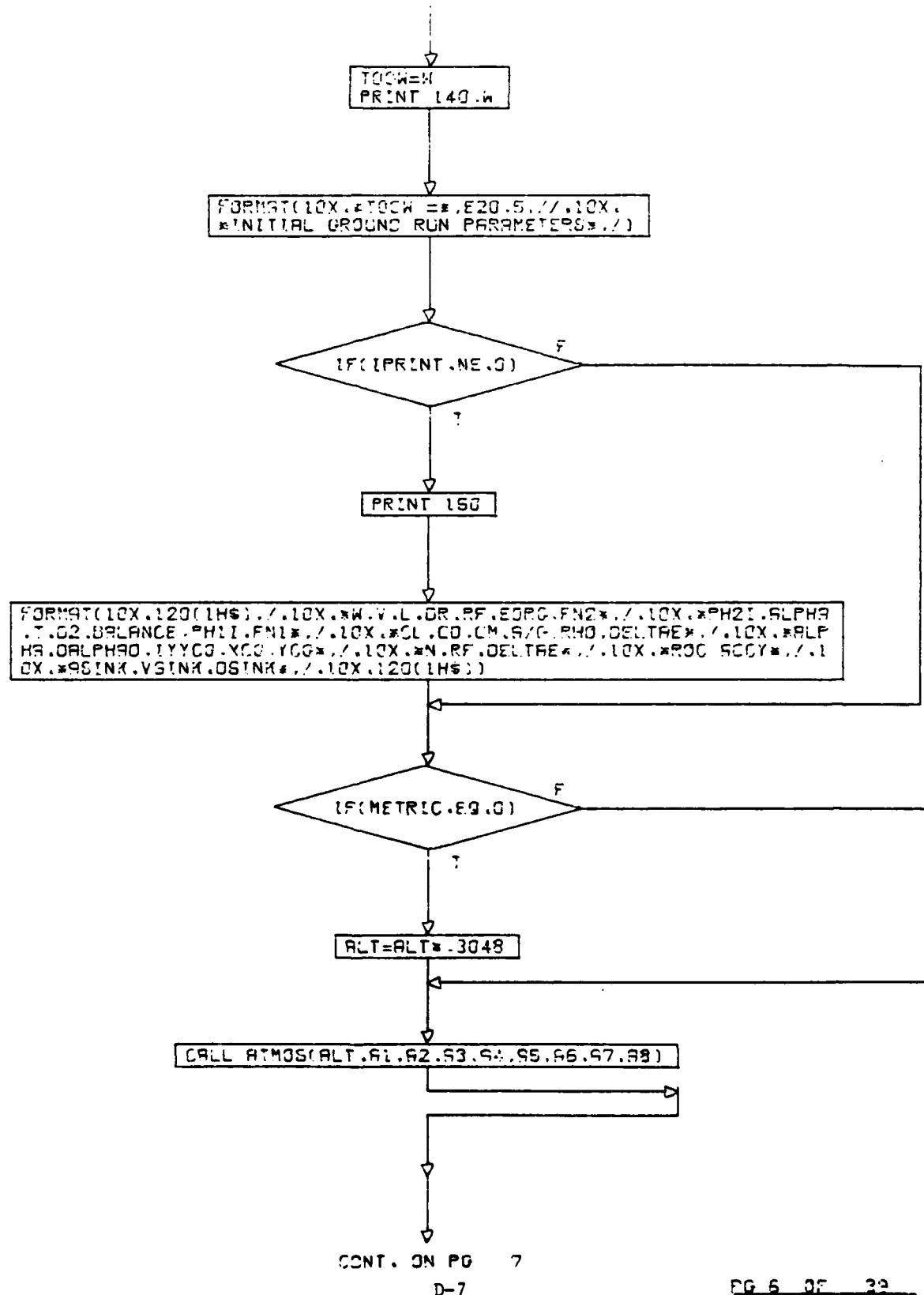
D-3

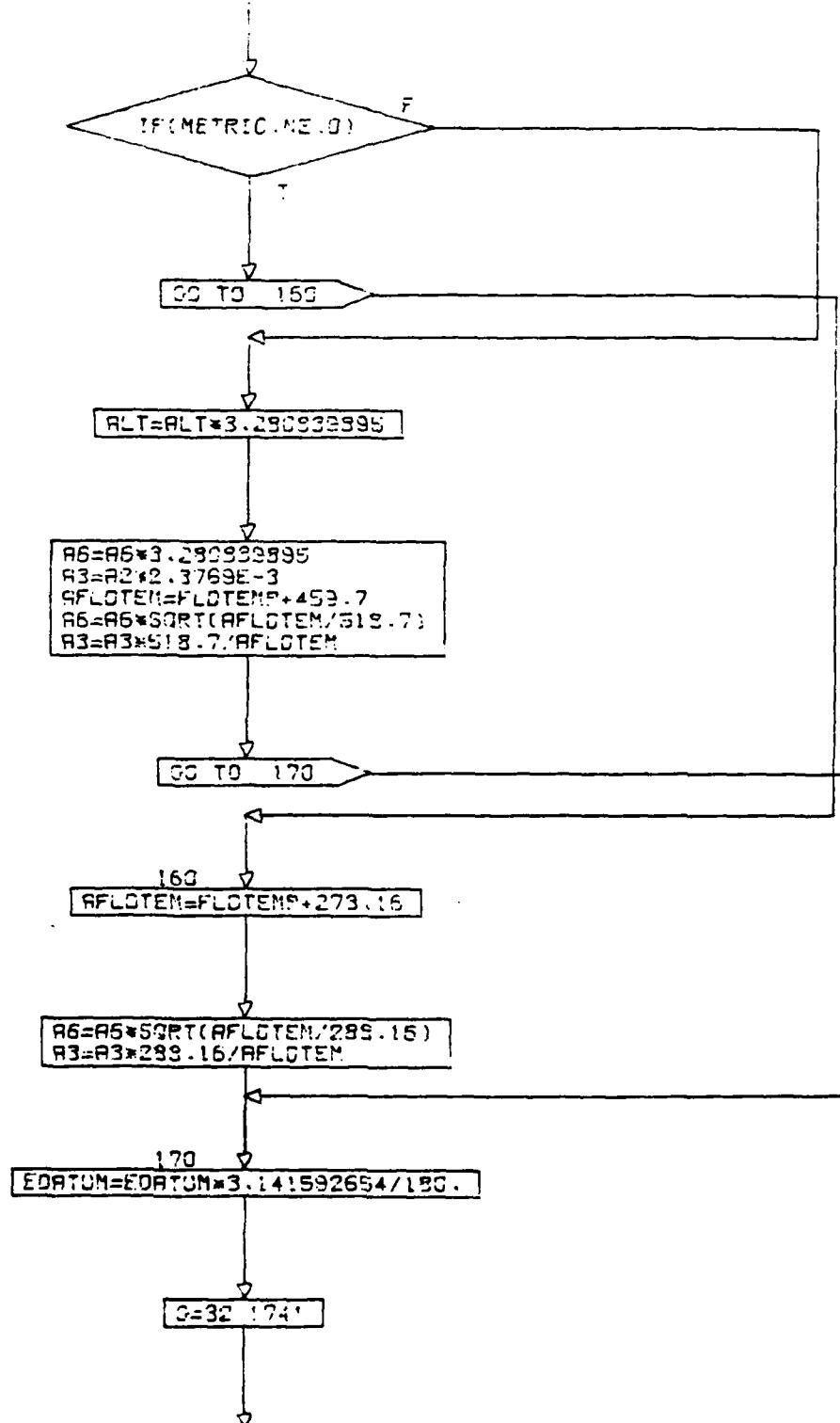
PG 2 OF 34







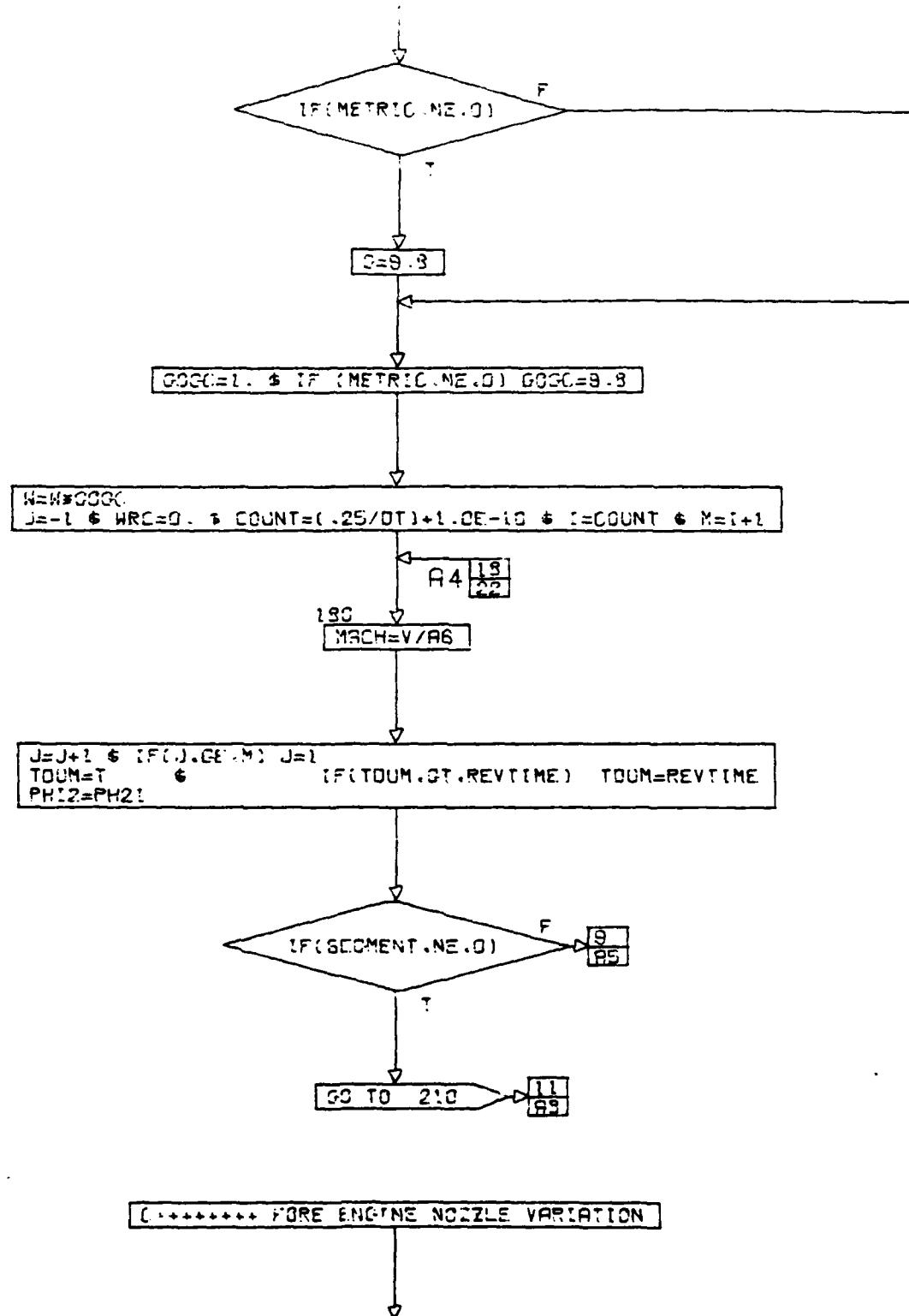


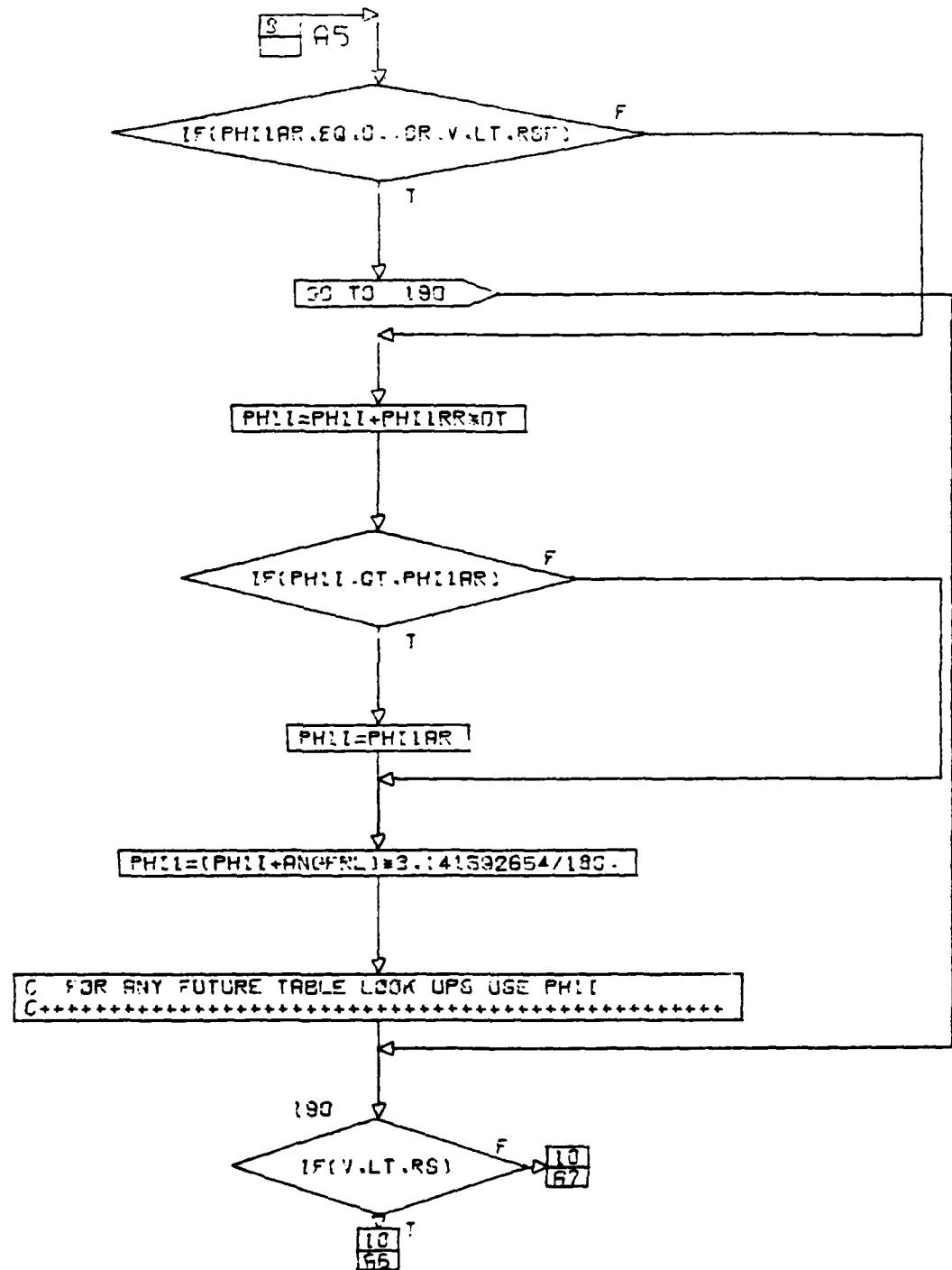


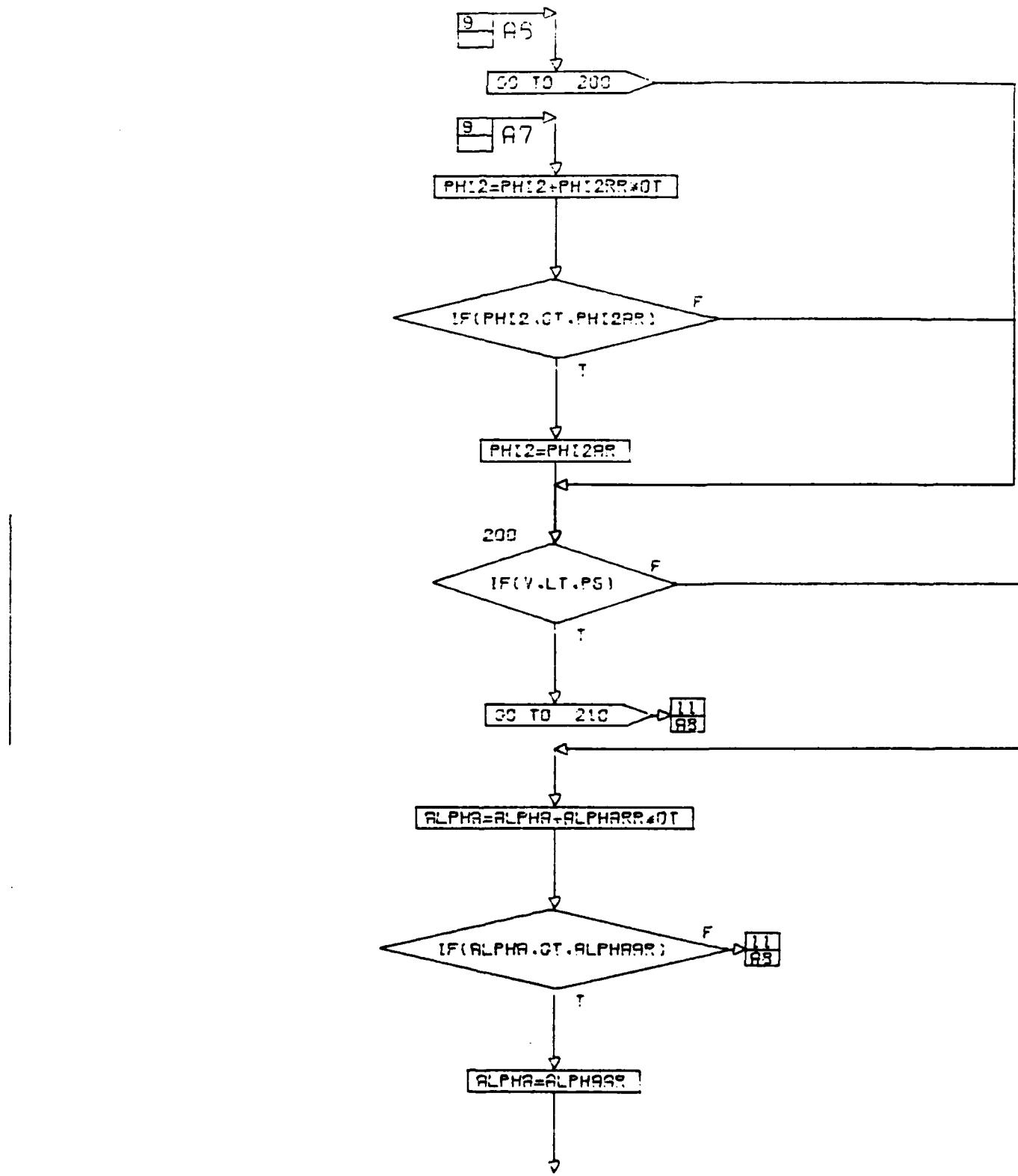
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D-8

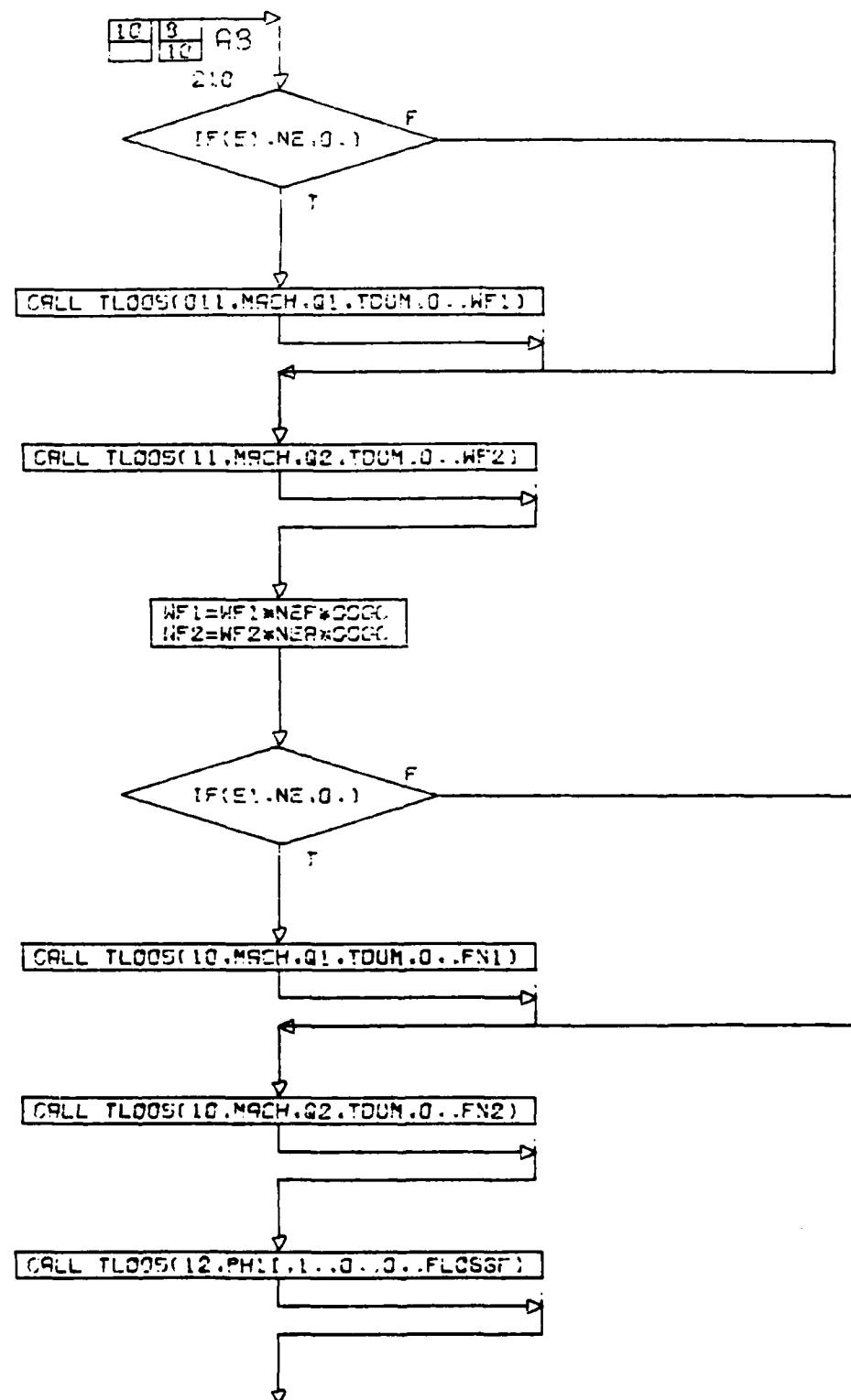
PG 7 OF 39







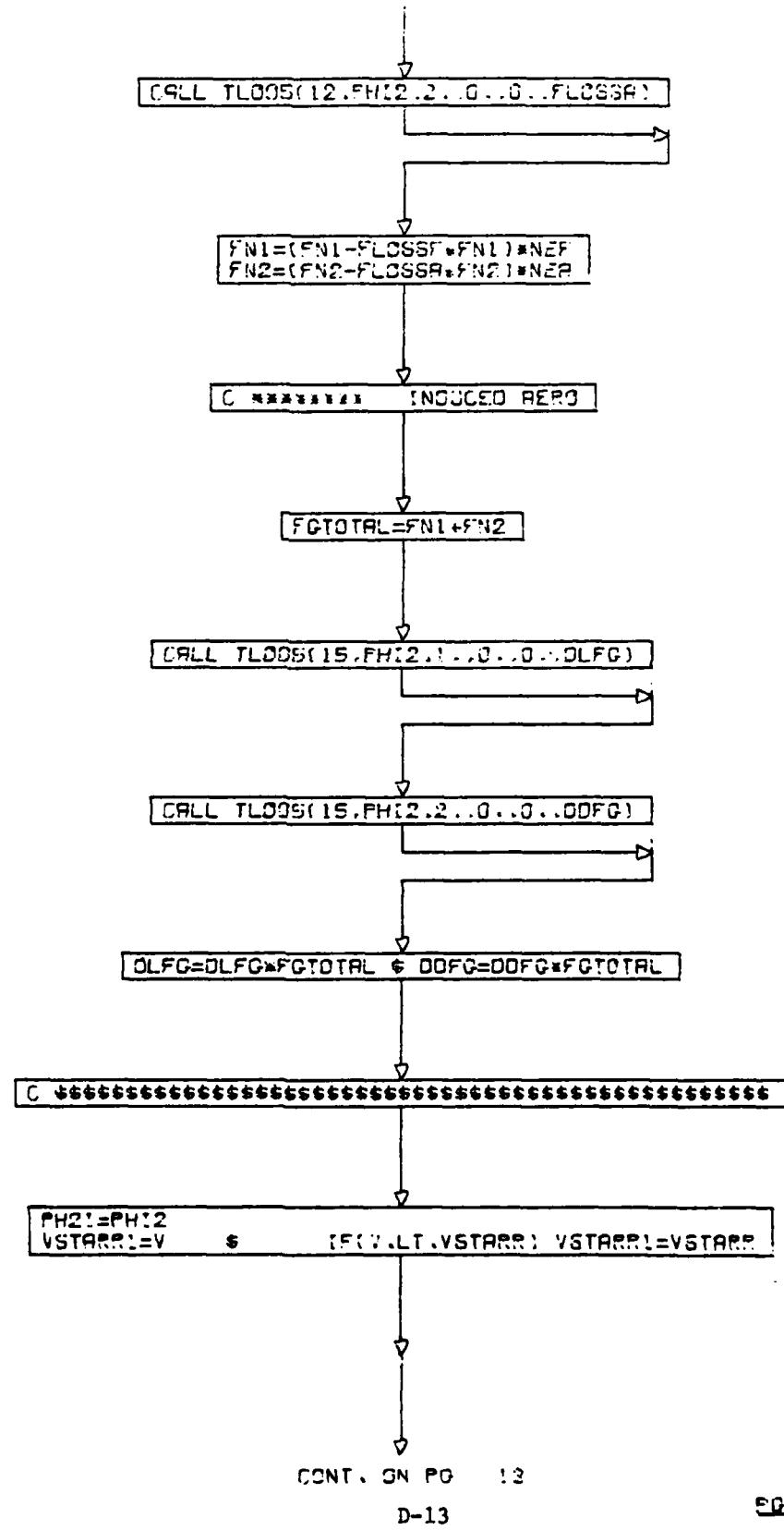
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D-11

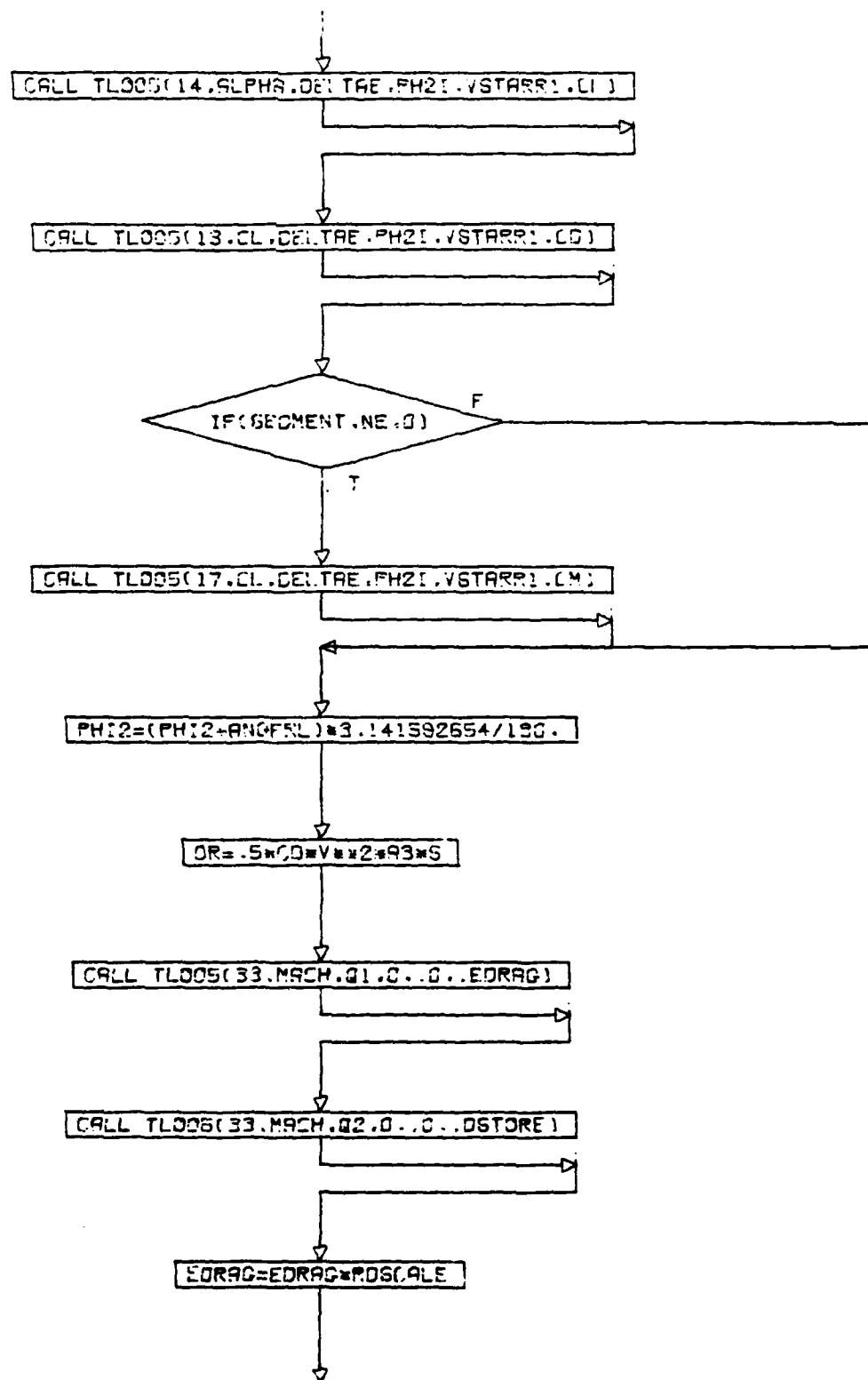


CONT. ON PG 12

D-12

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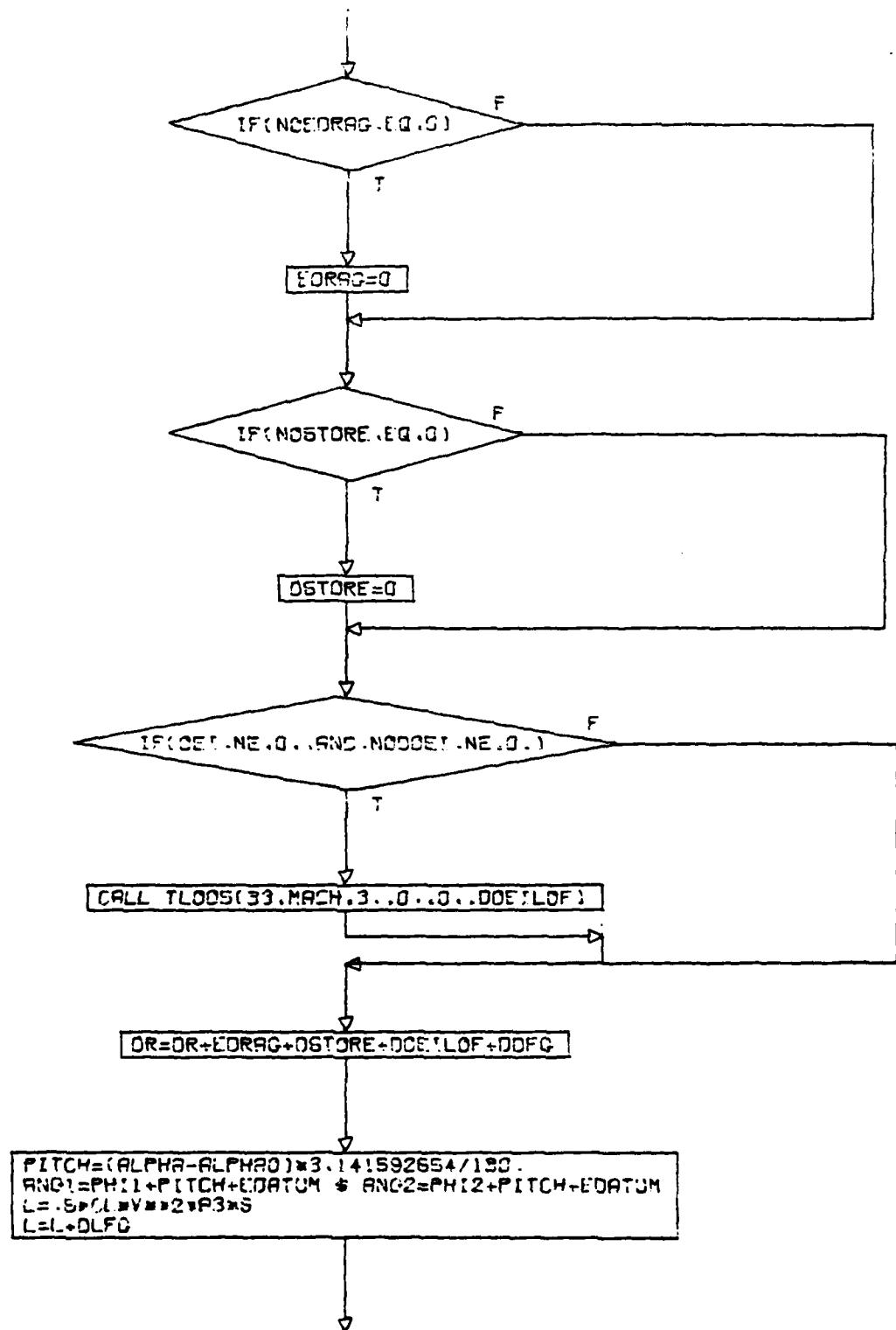


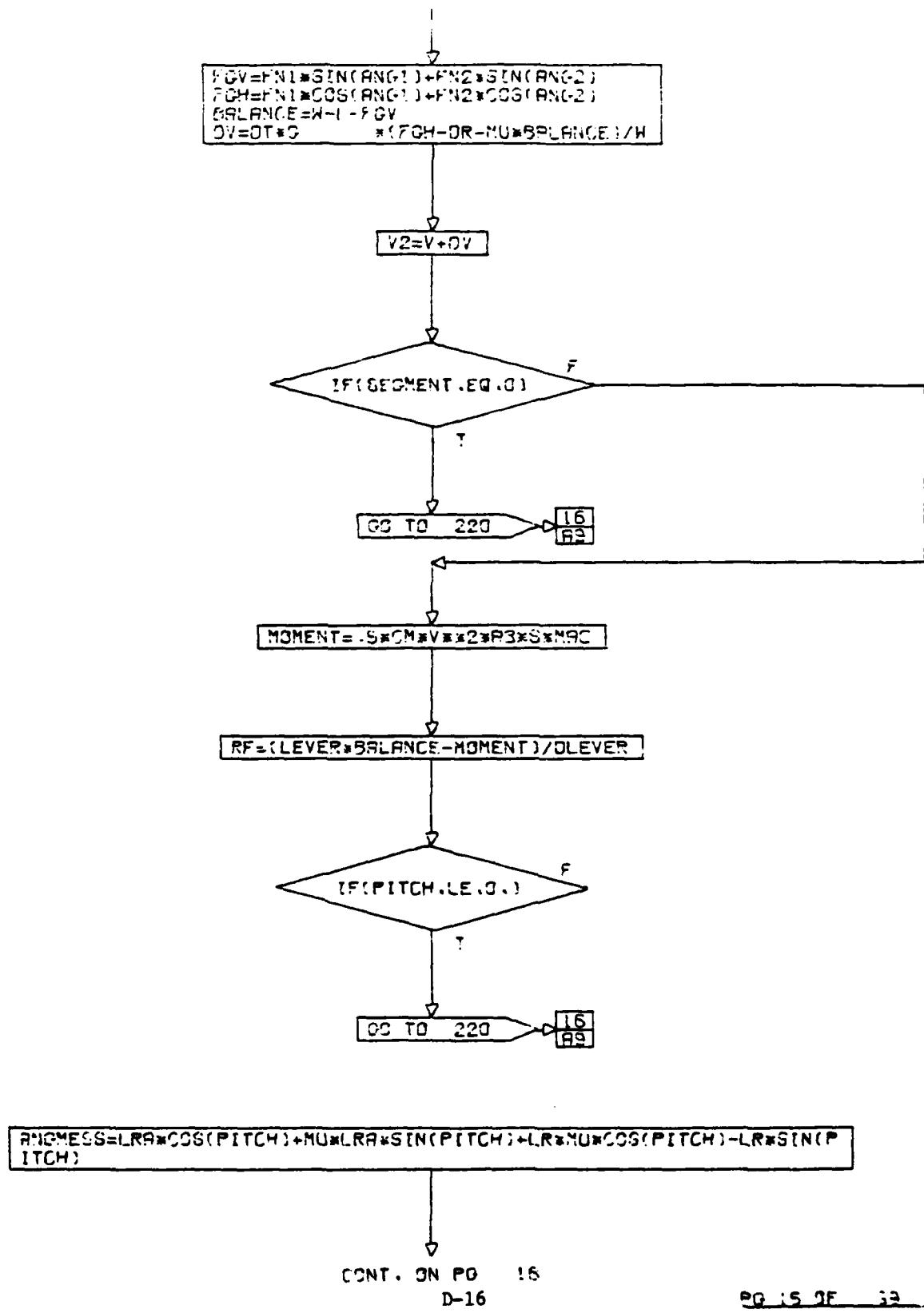


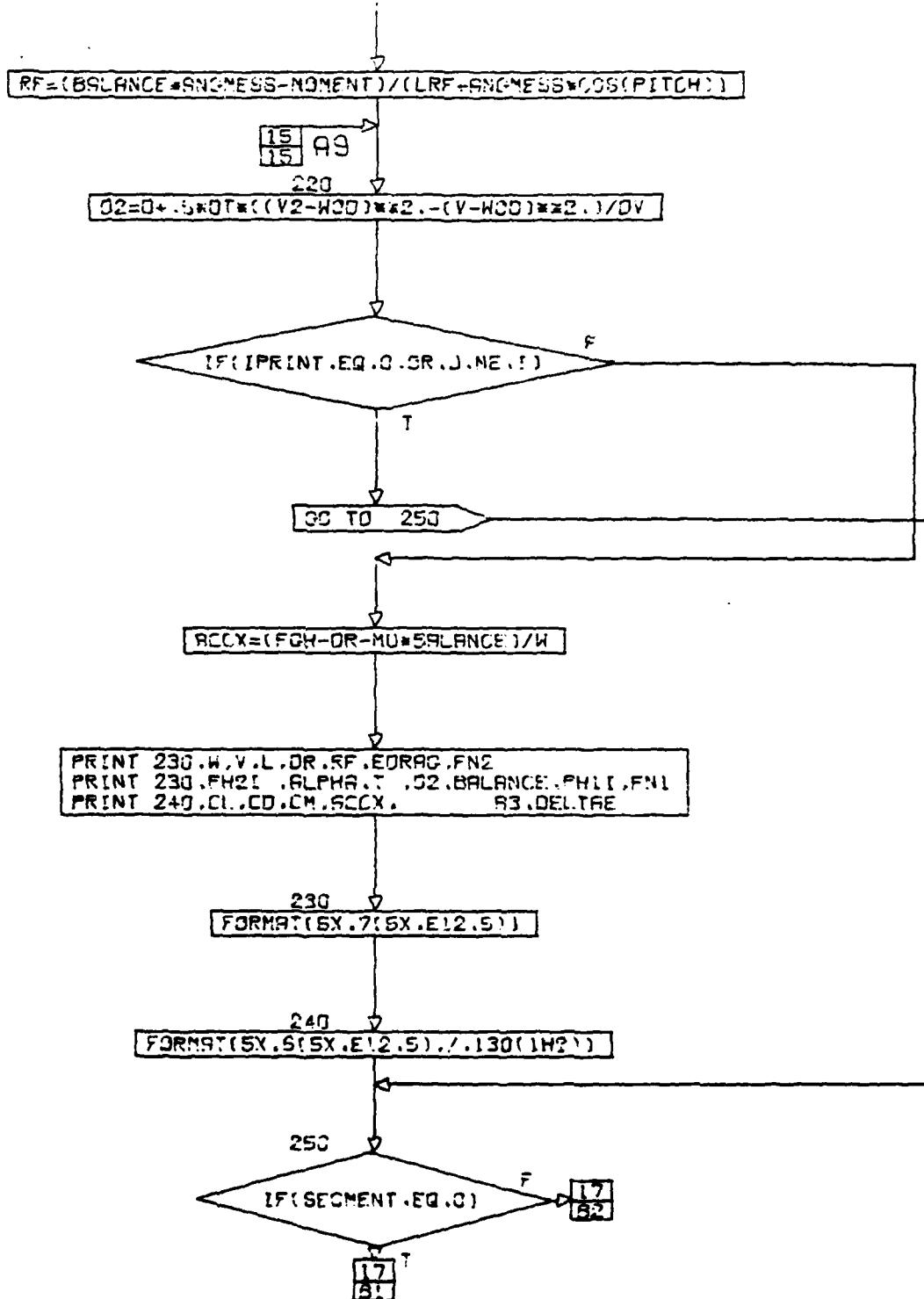
CONT. ON PG 14

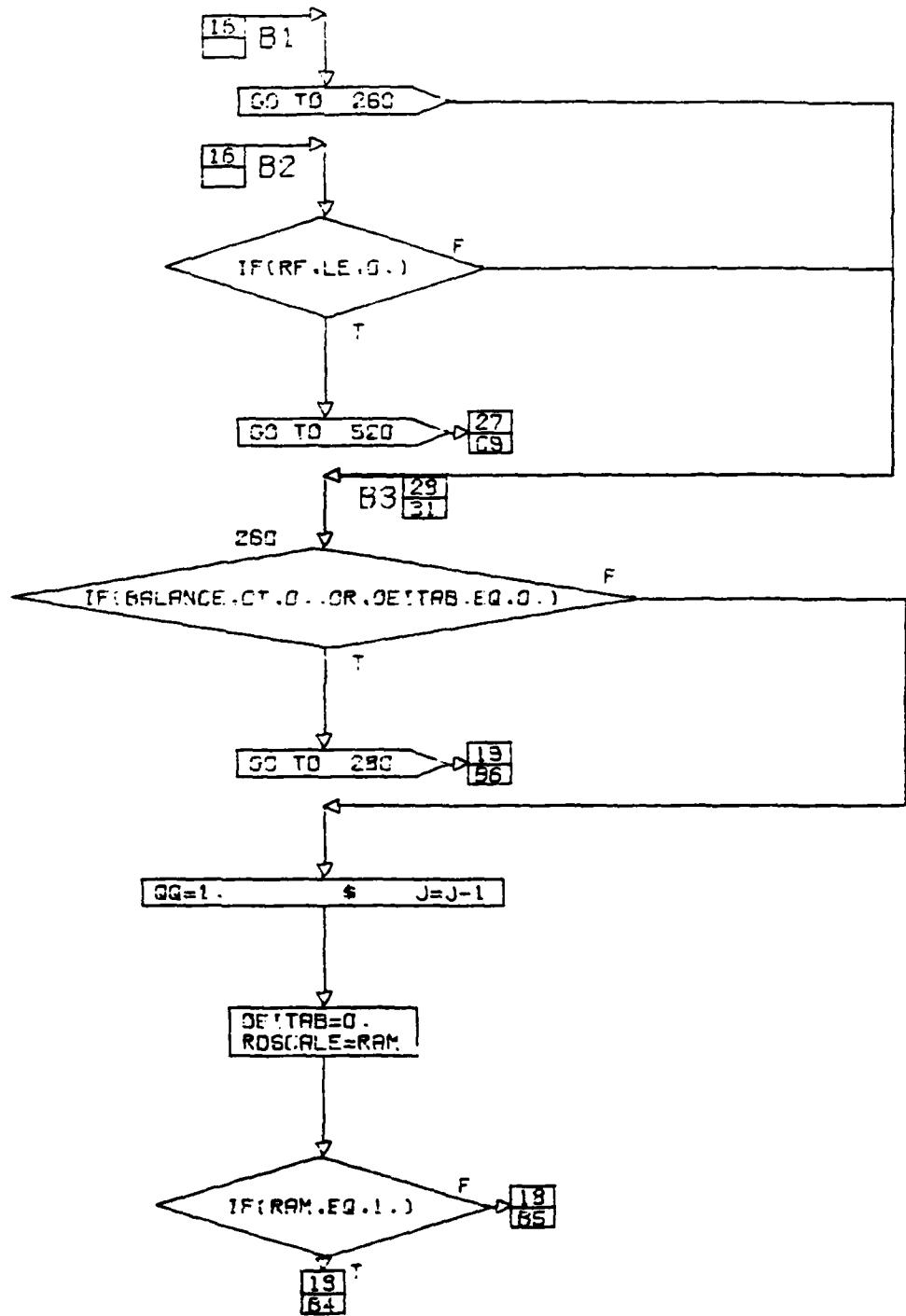
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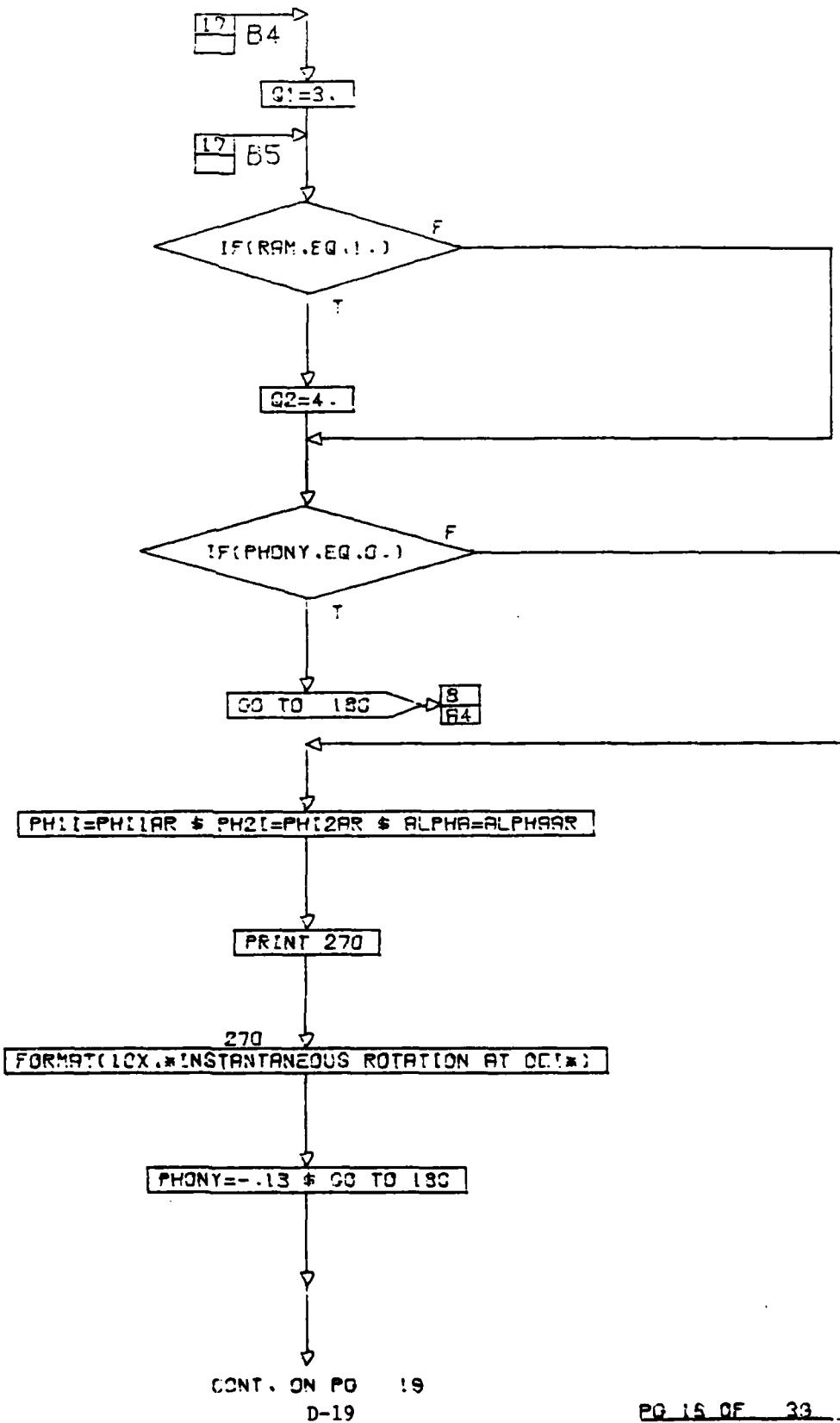
PG 13 OF 39

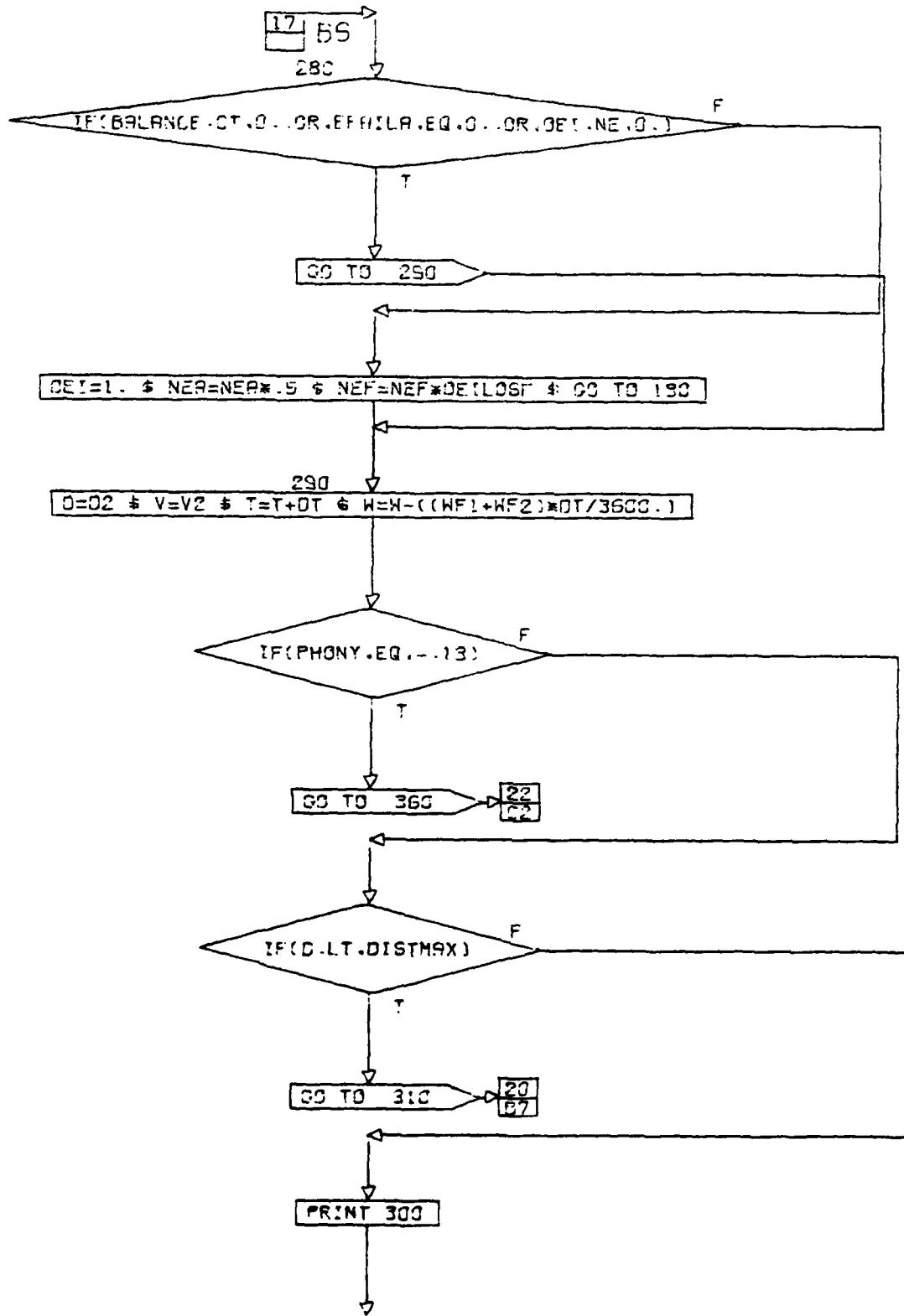


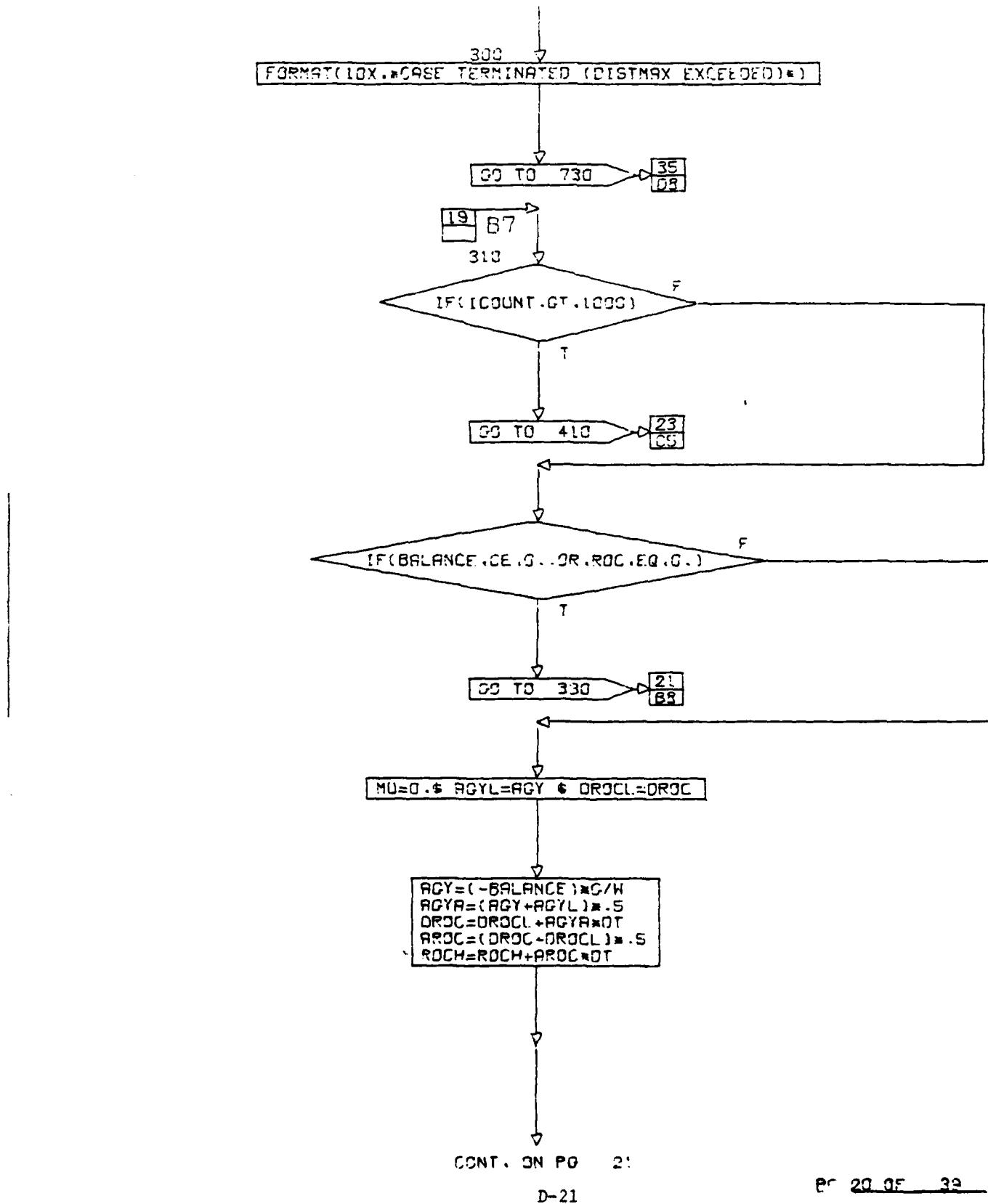


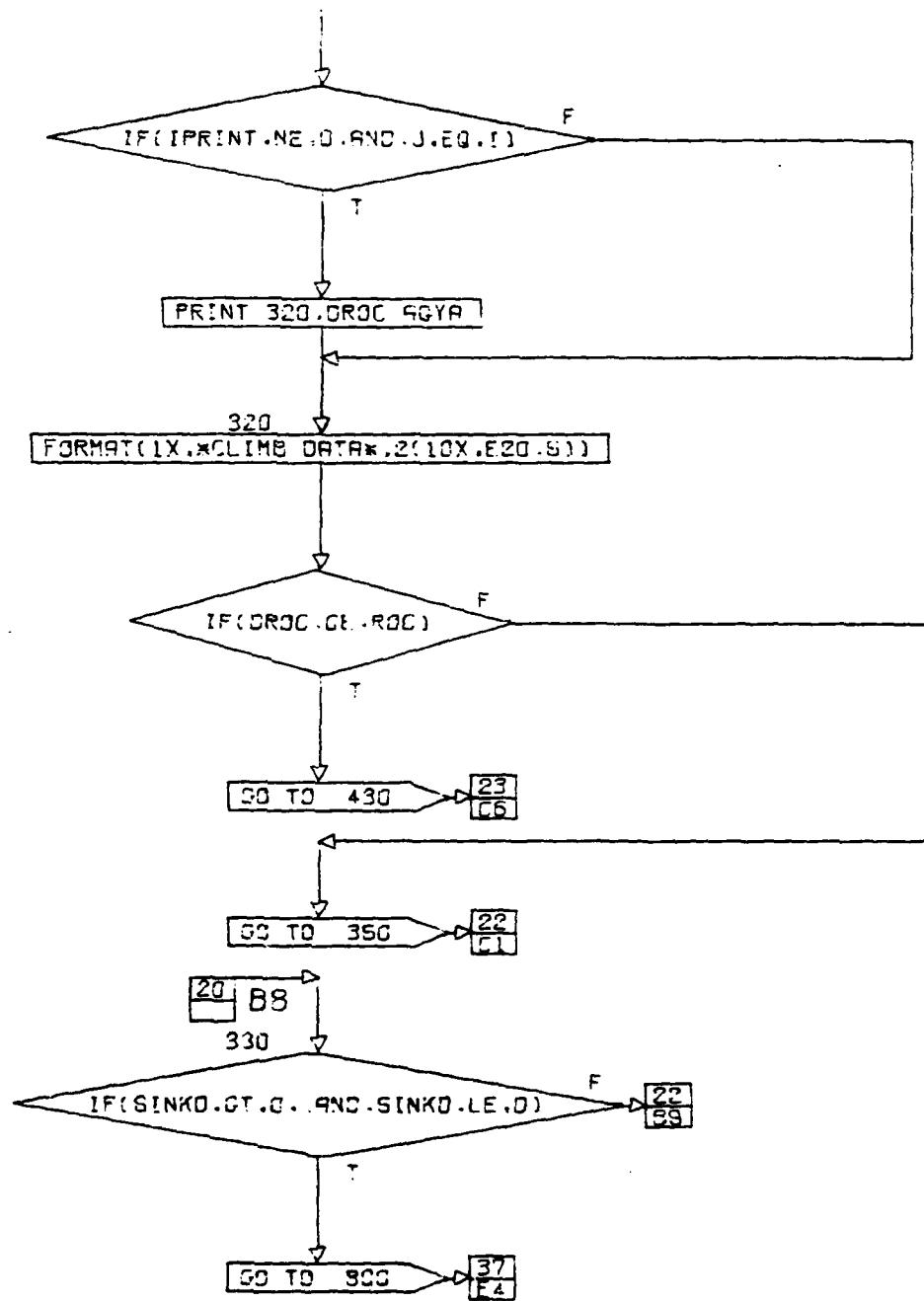


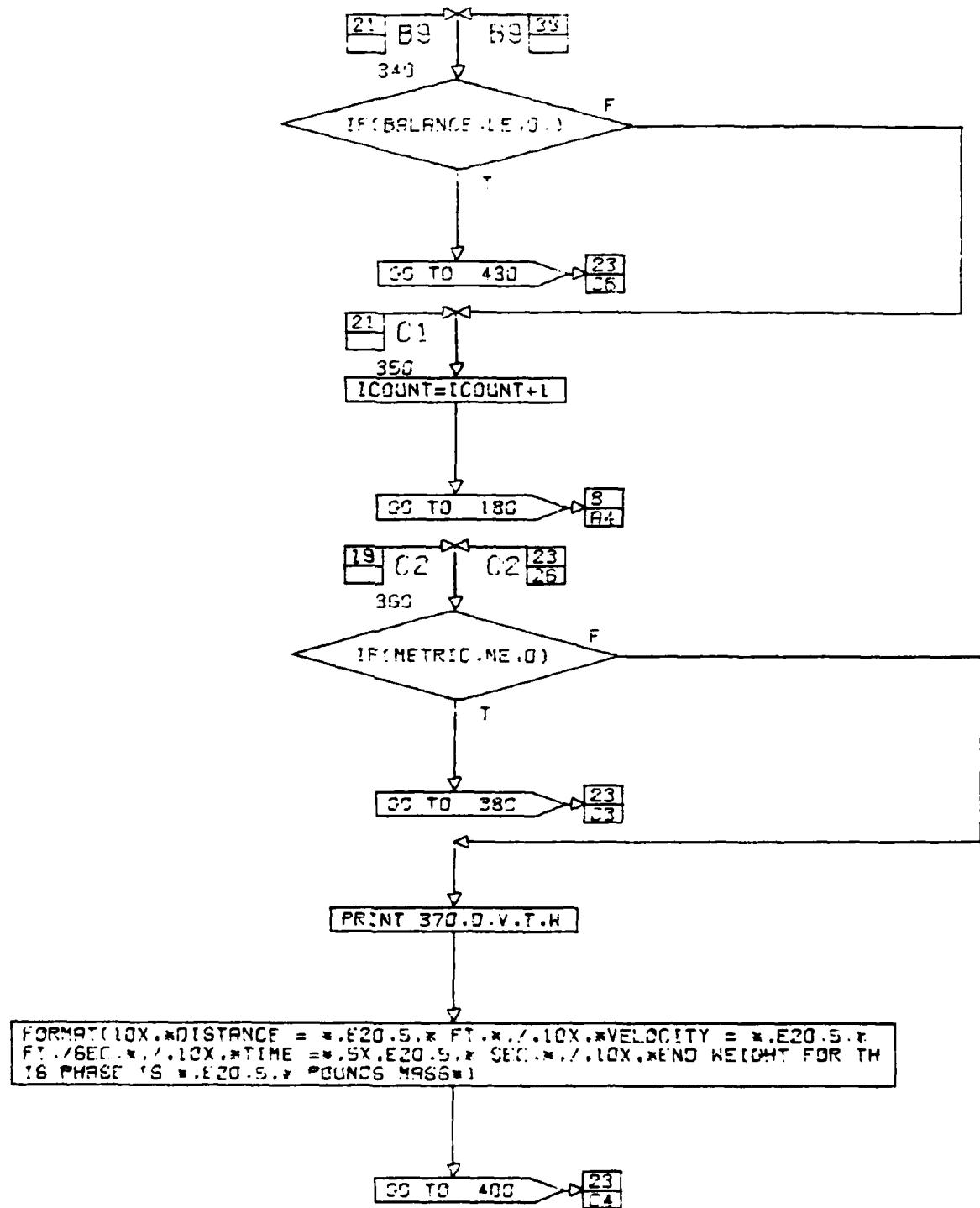


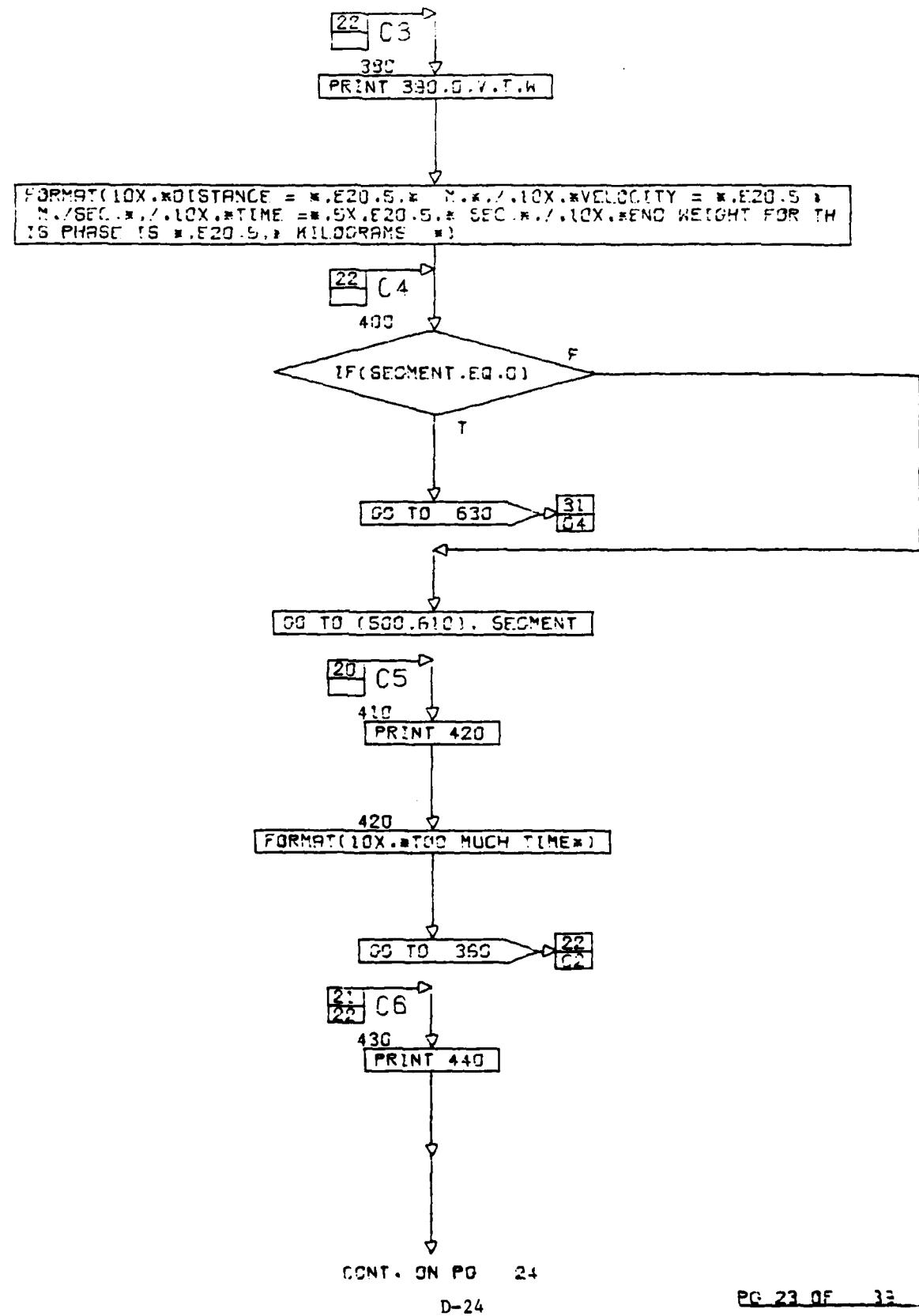


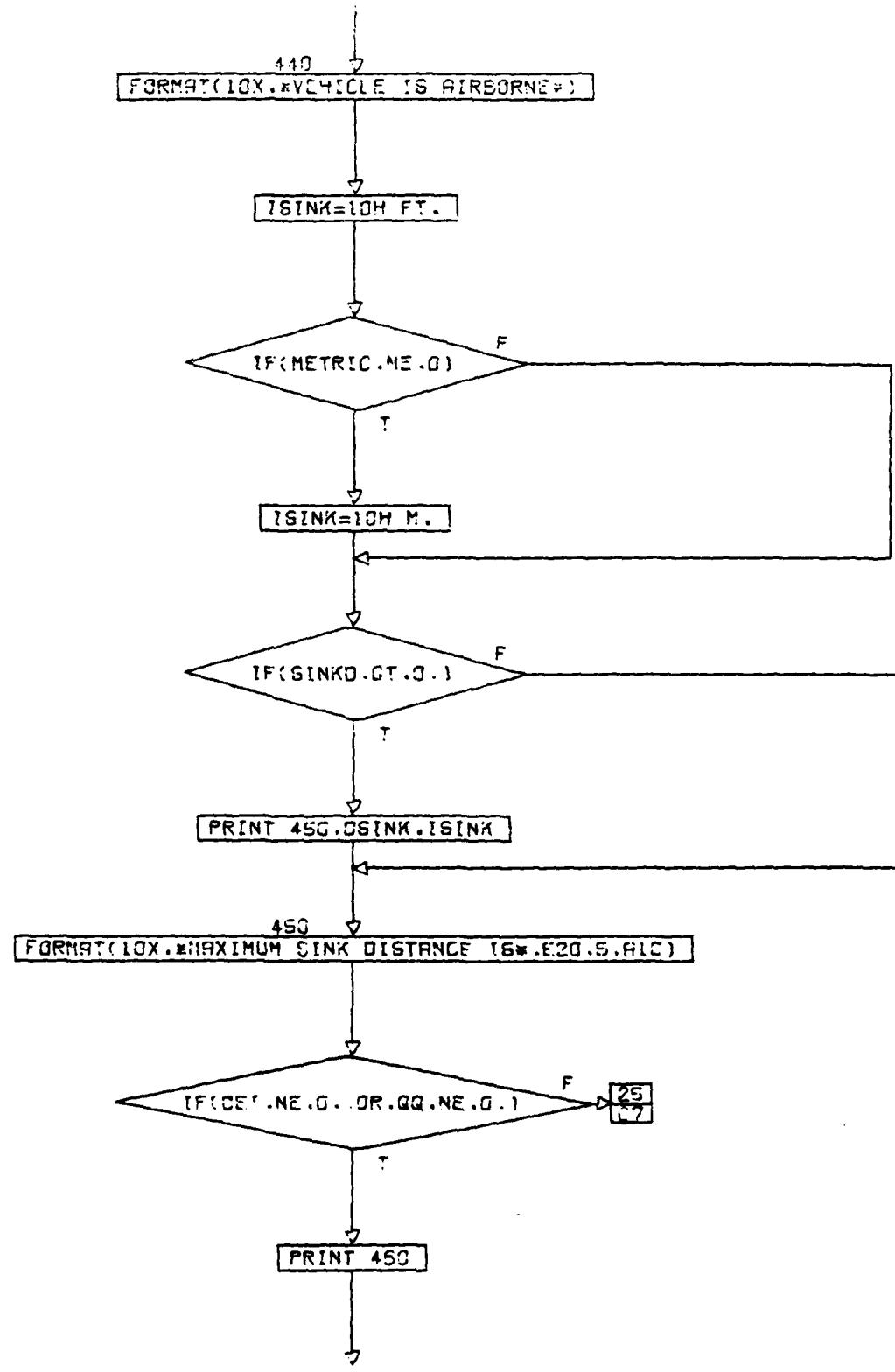


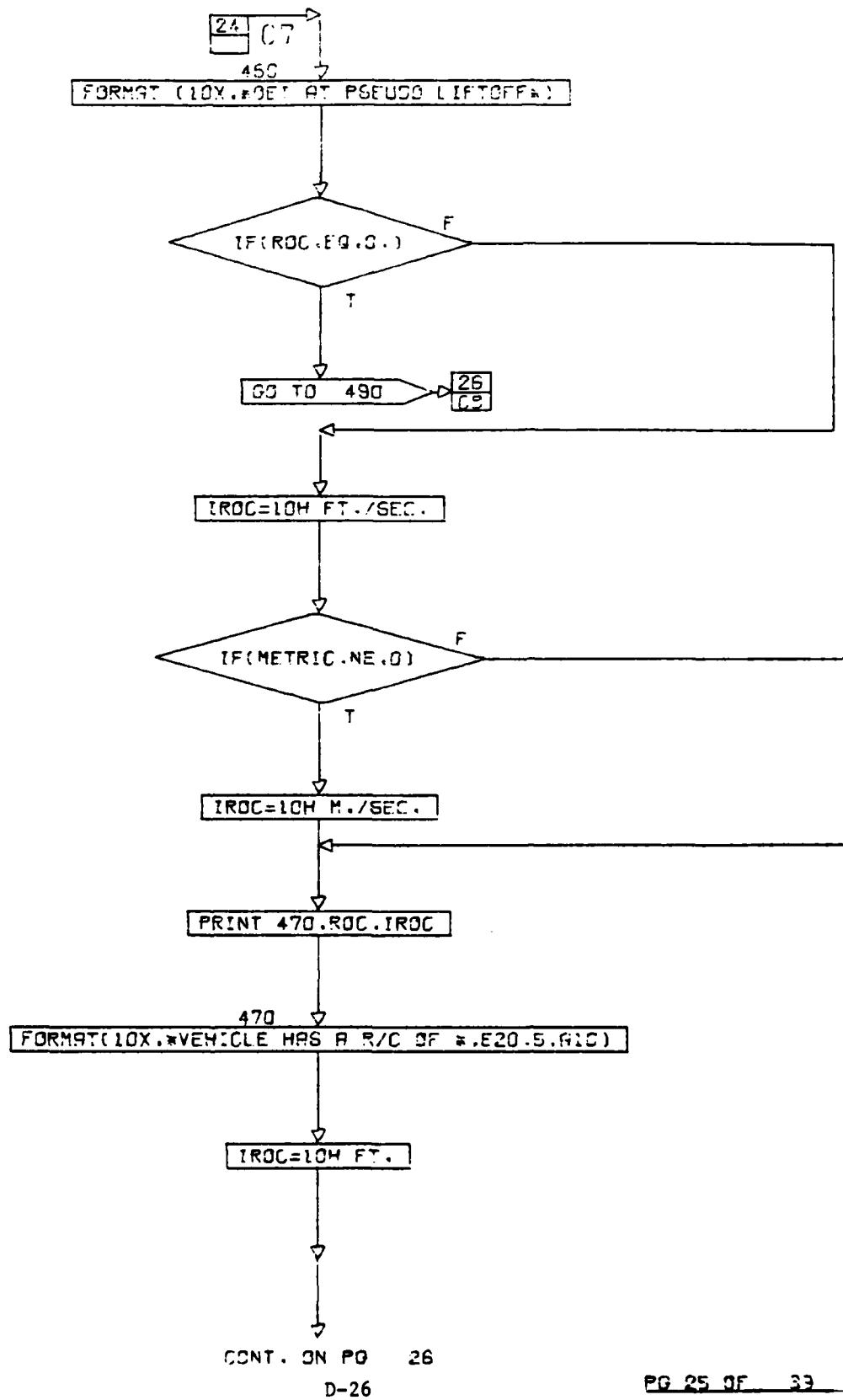


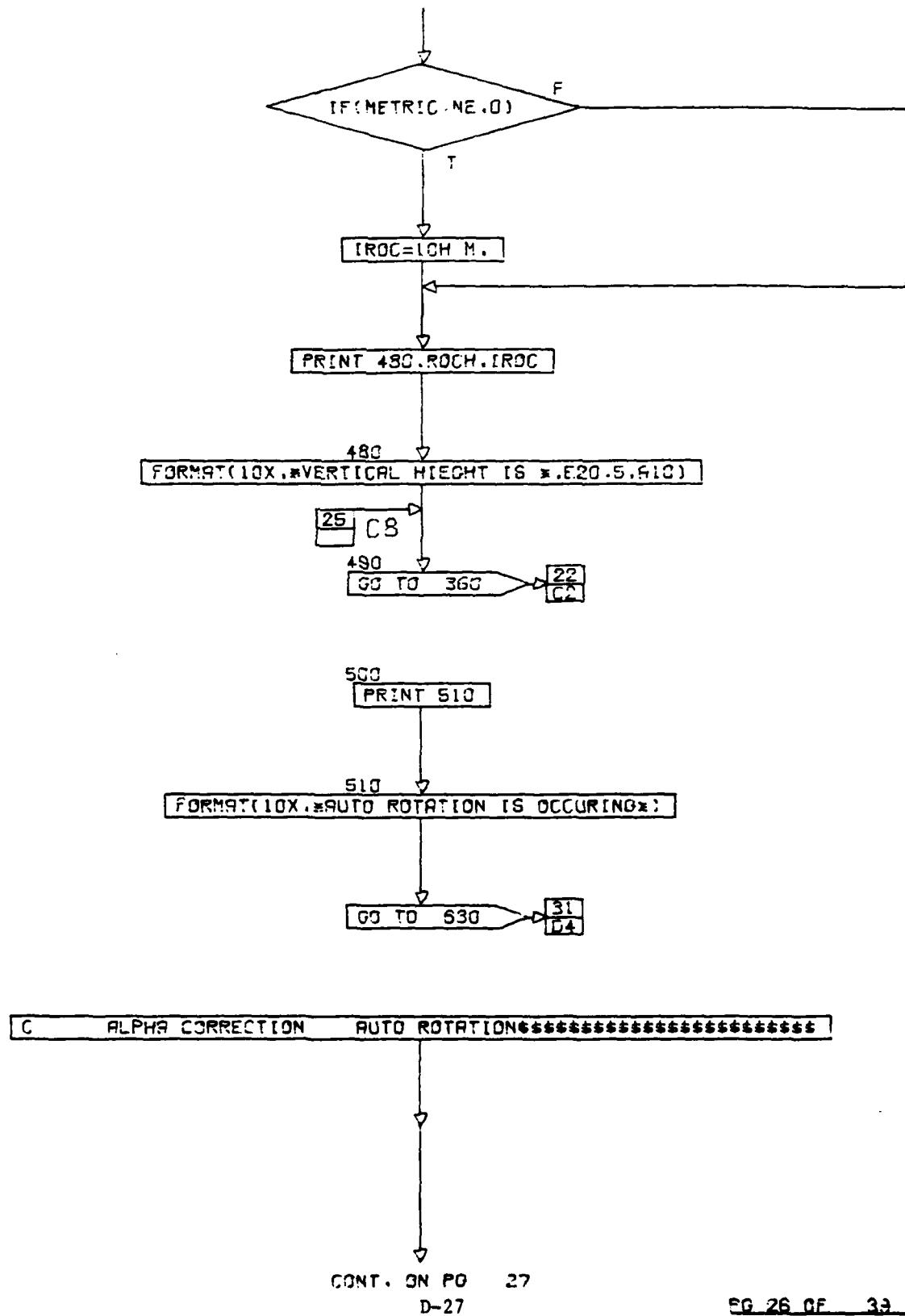


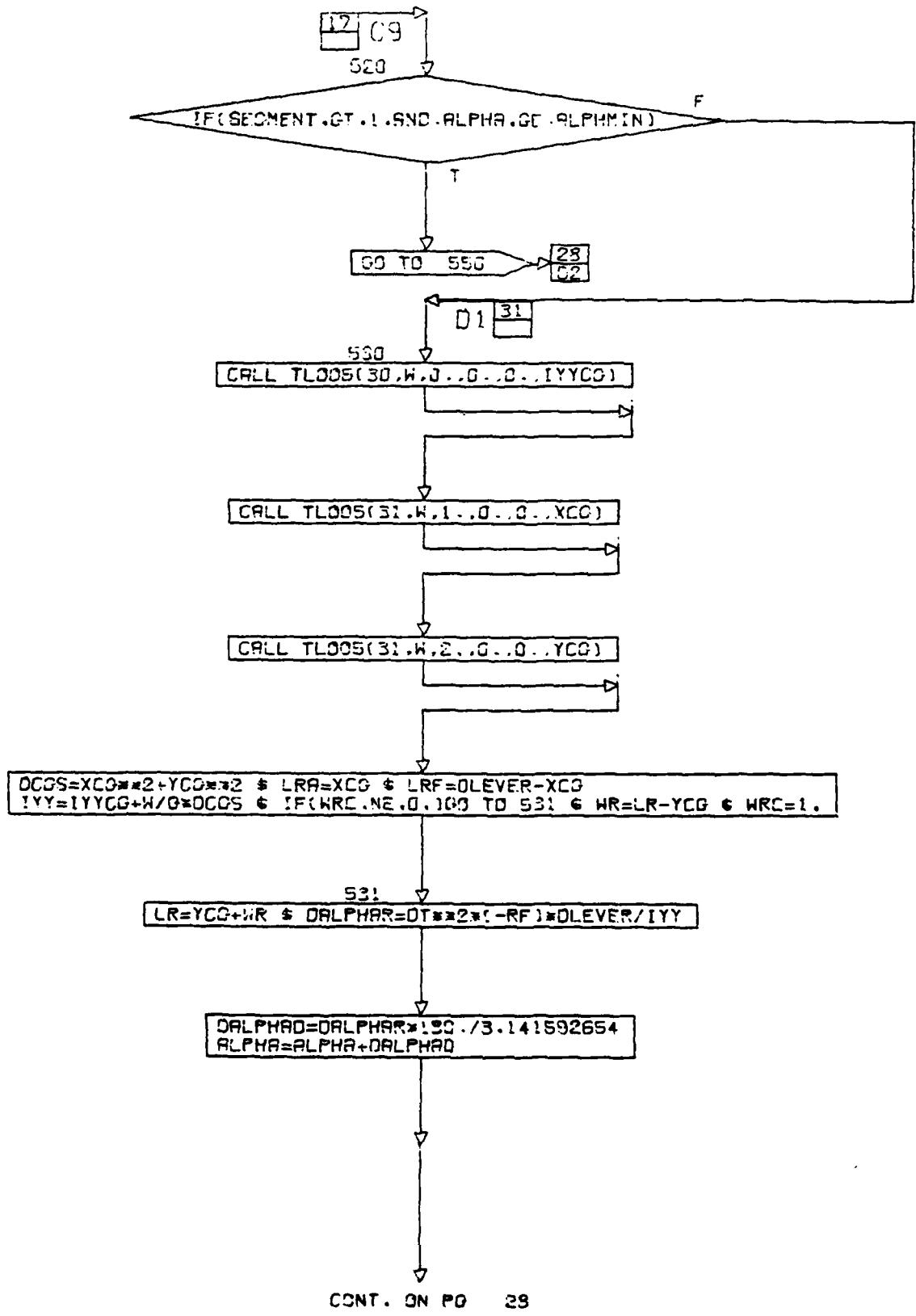


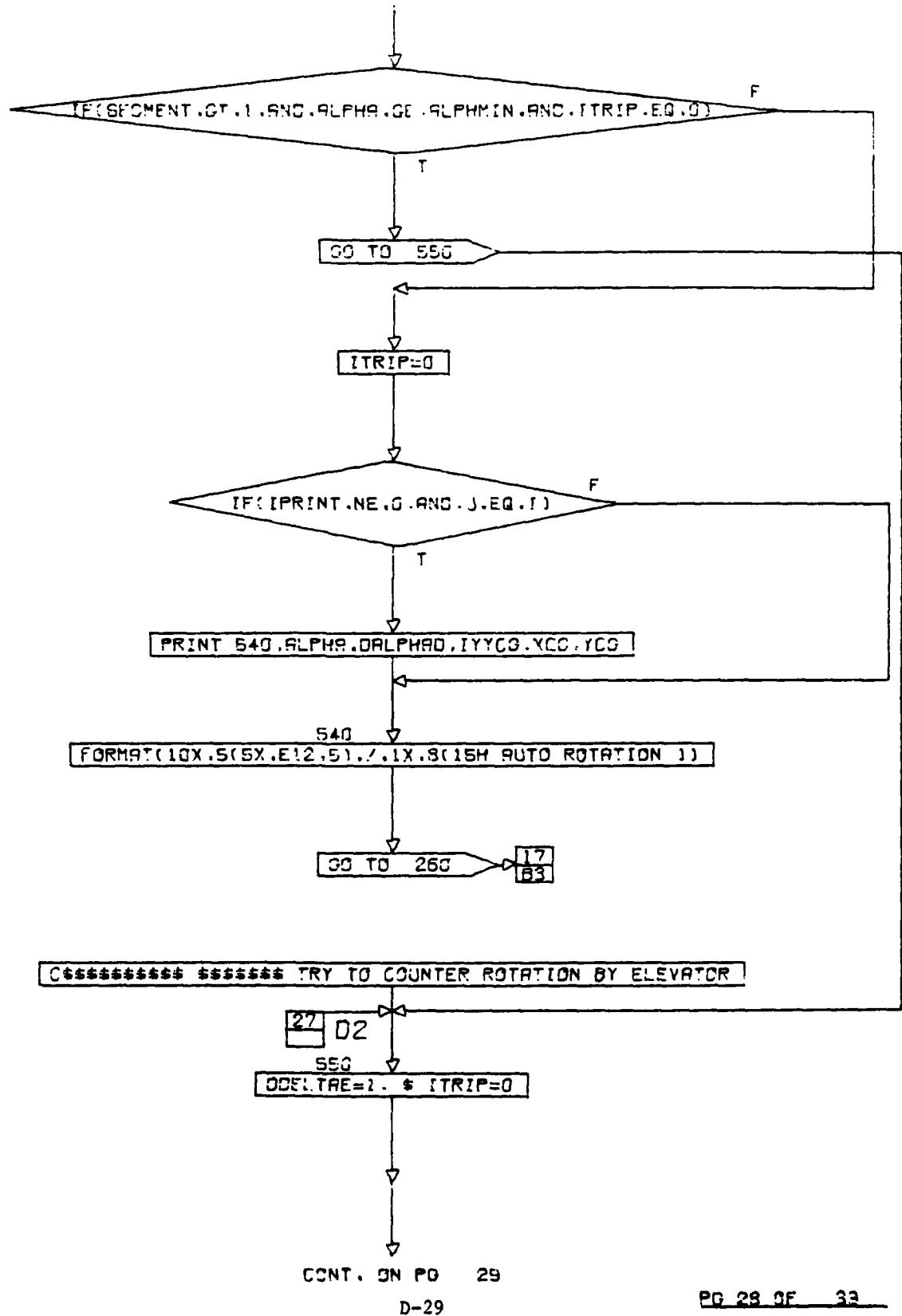


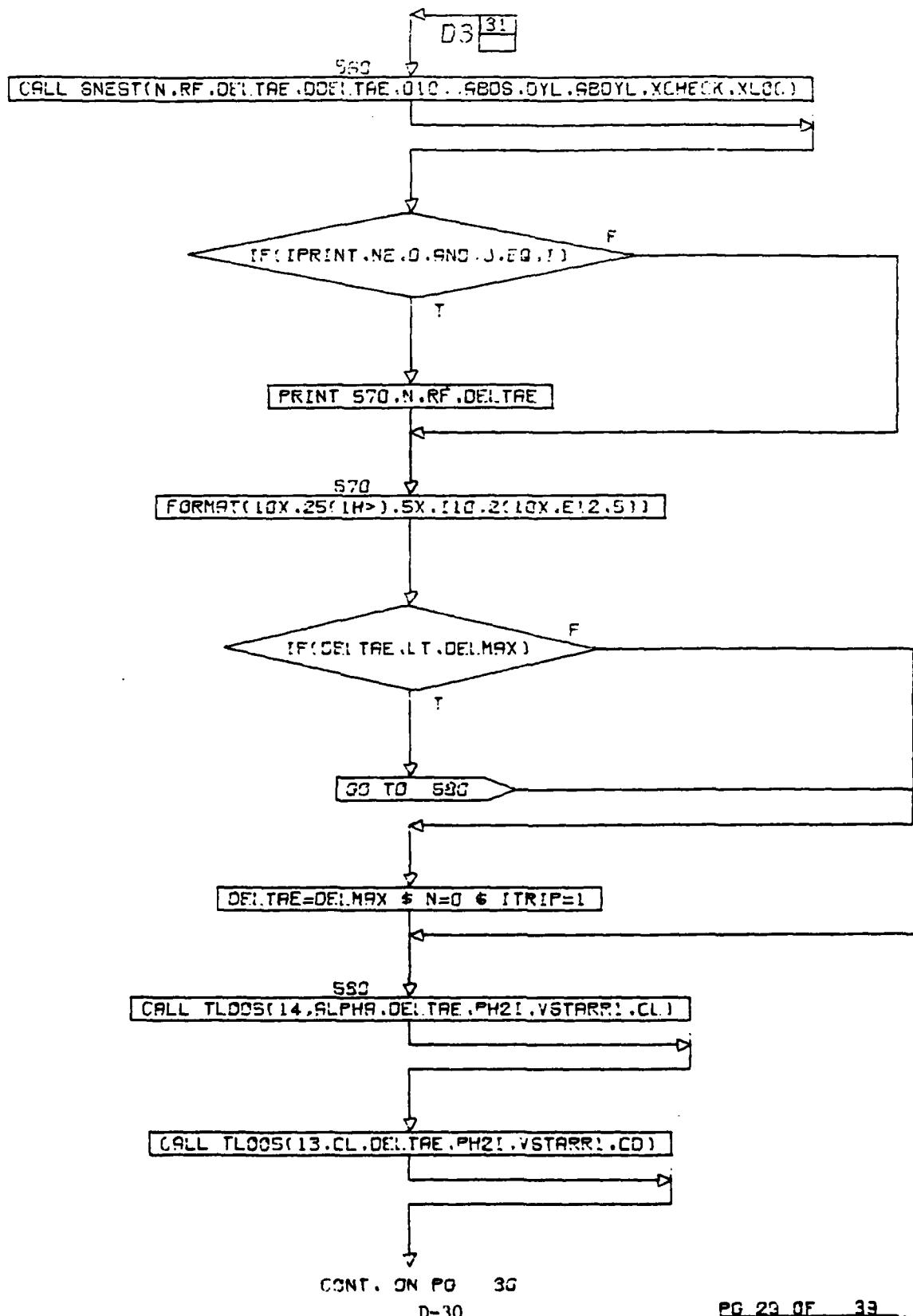


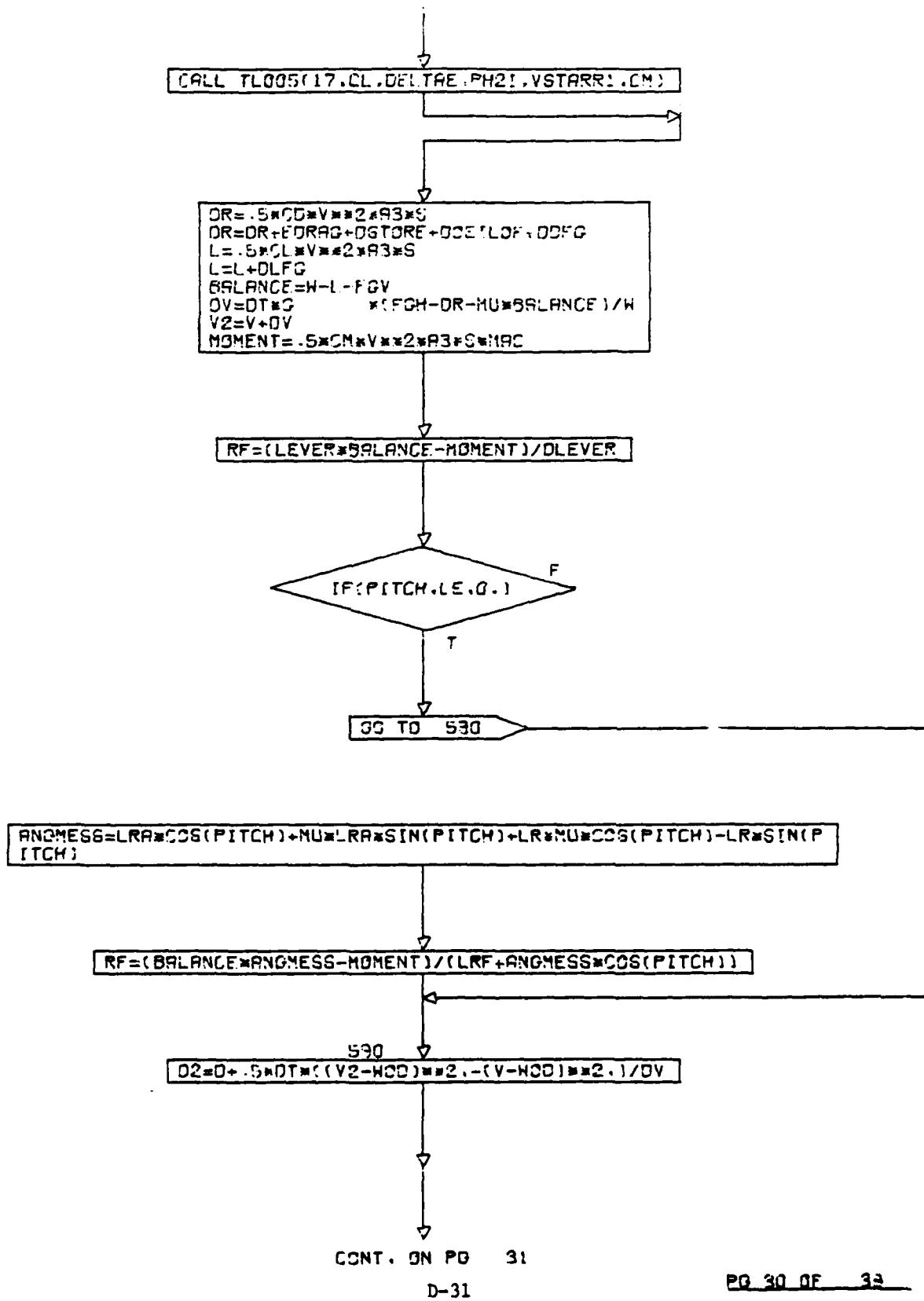


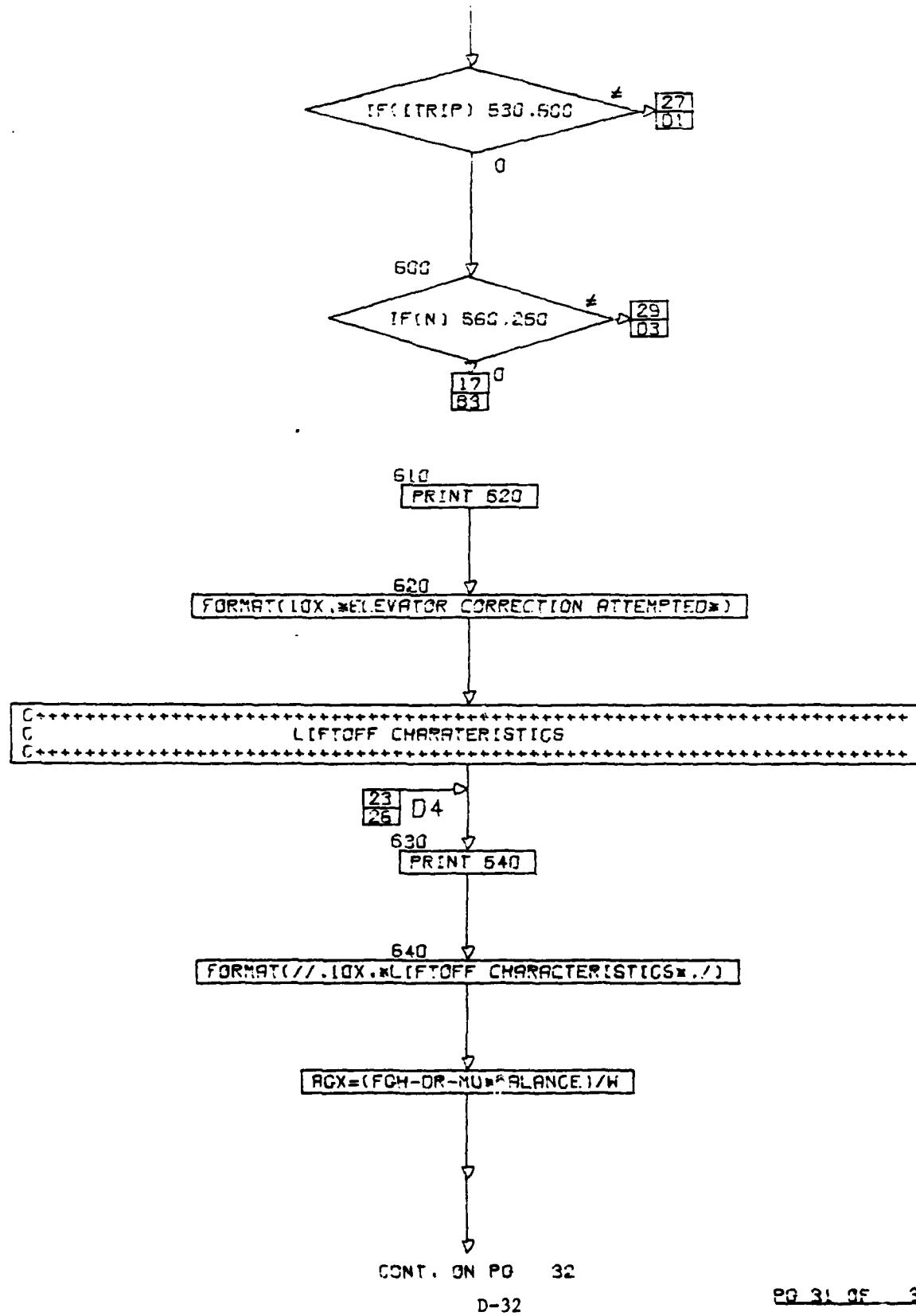


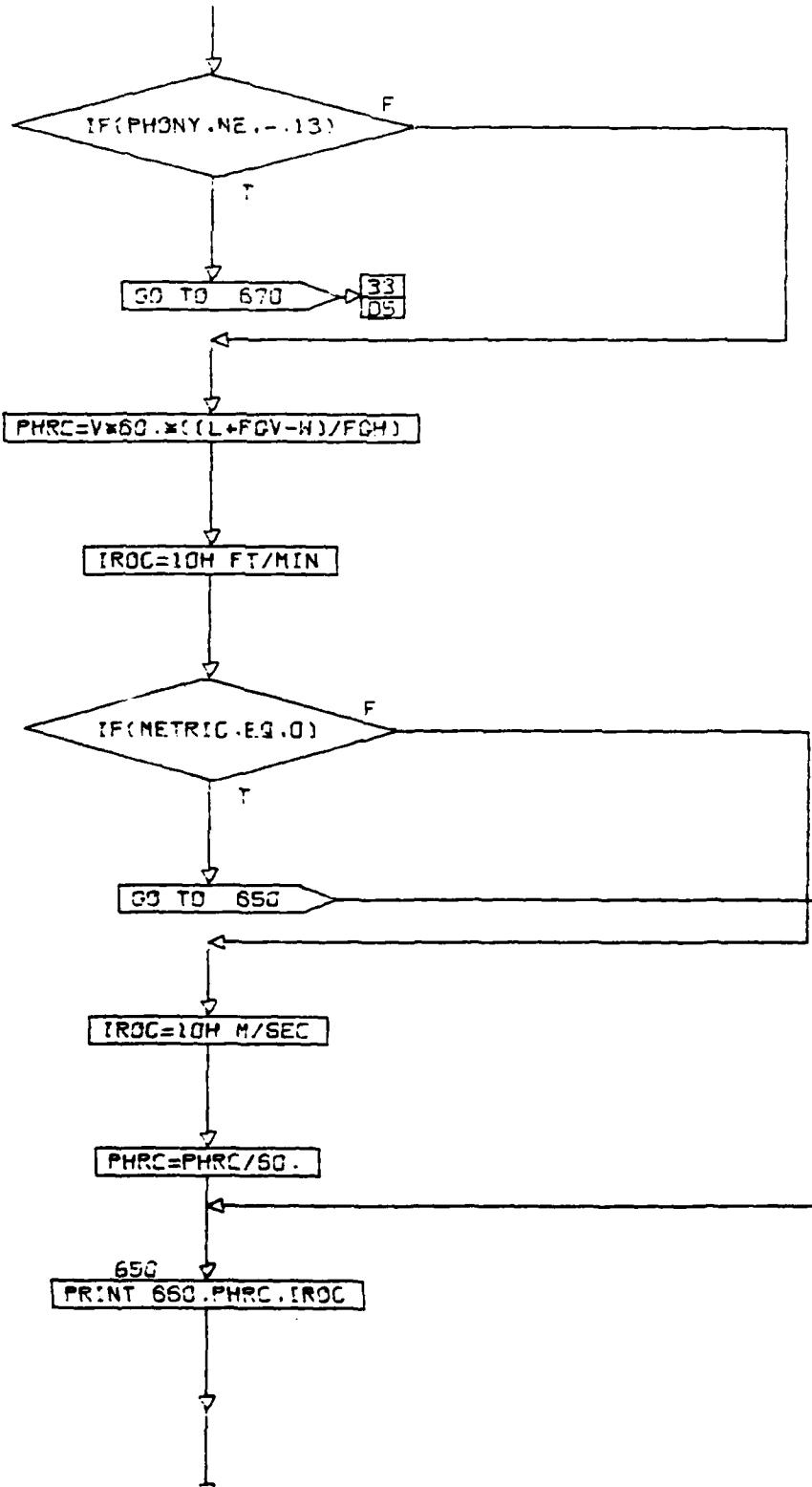








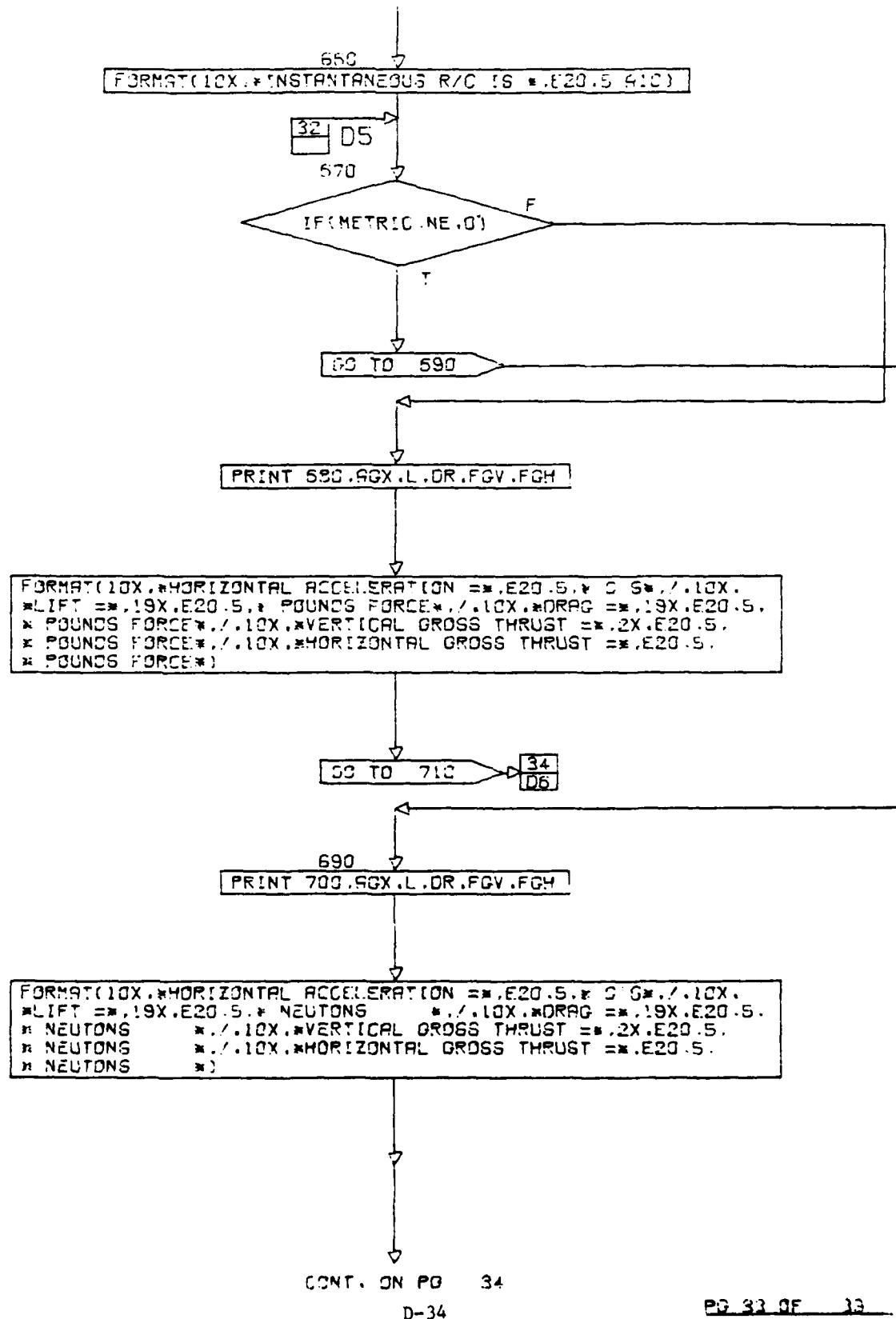


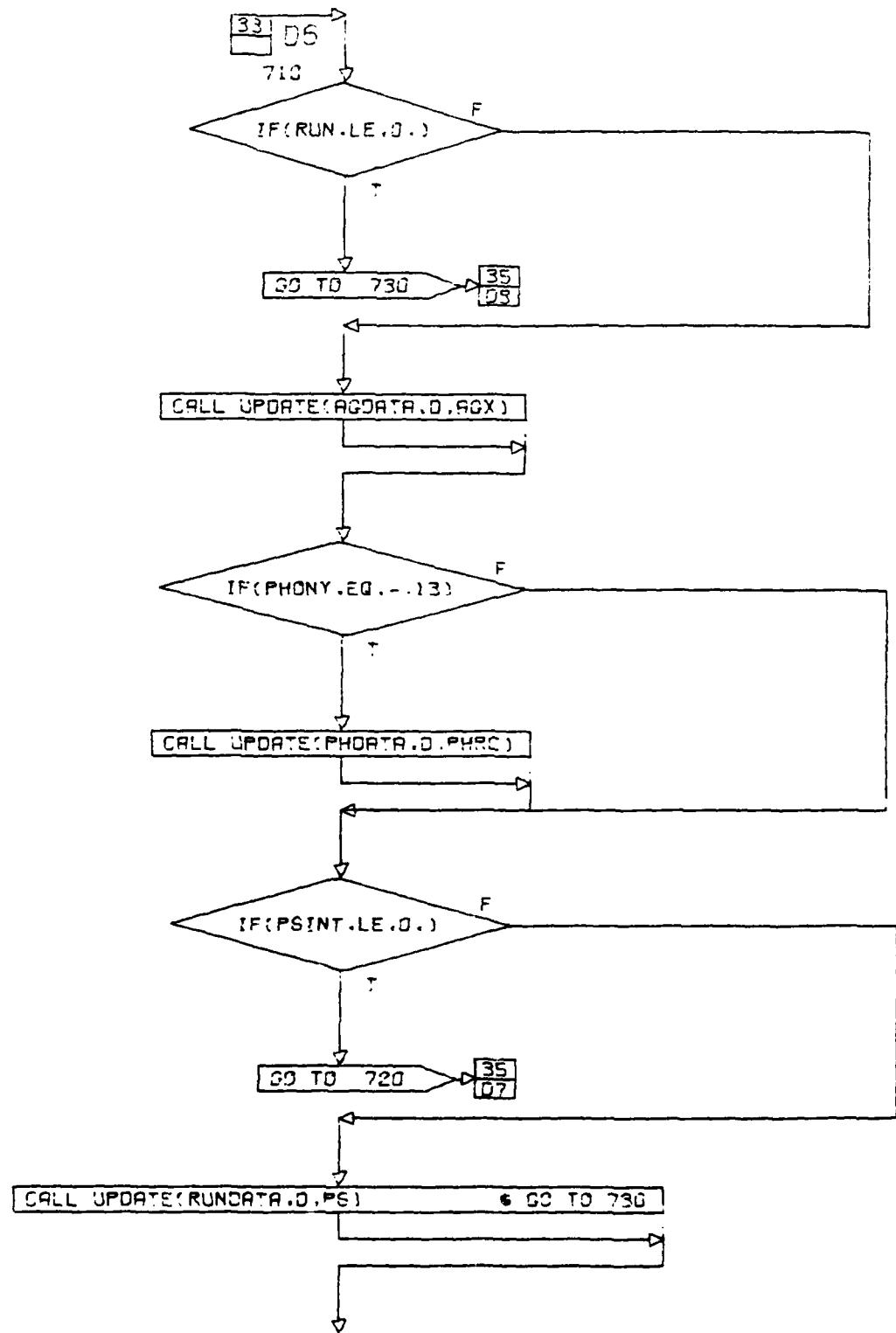


CONT. ON PG 33

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CONT. ON PG 35

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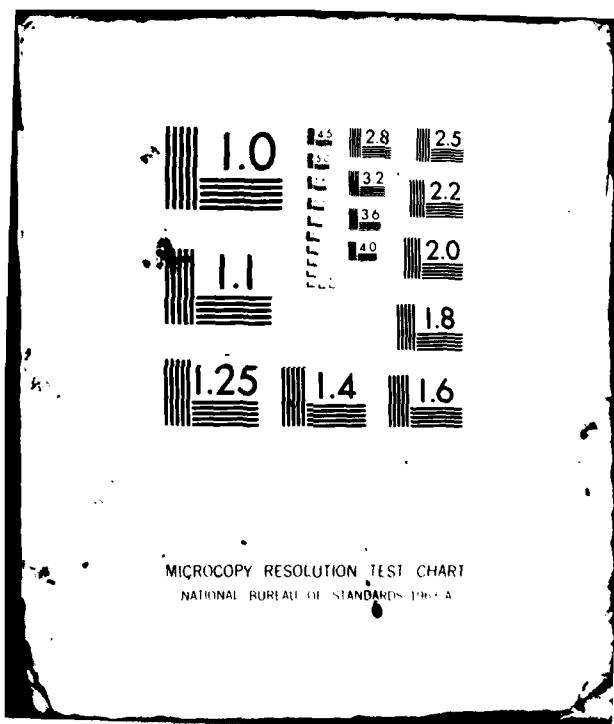
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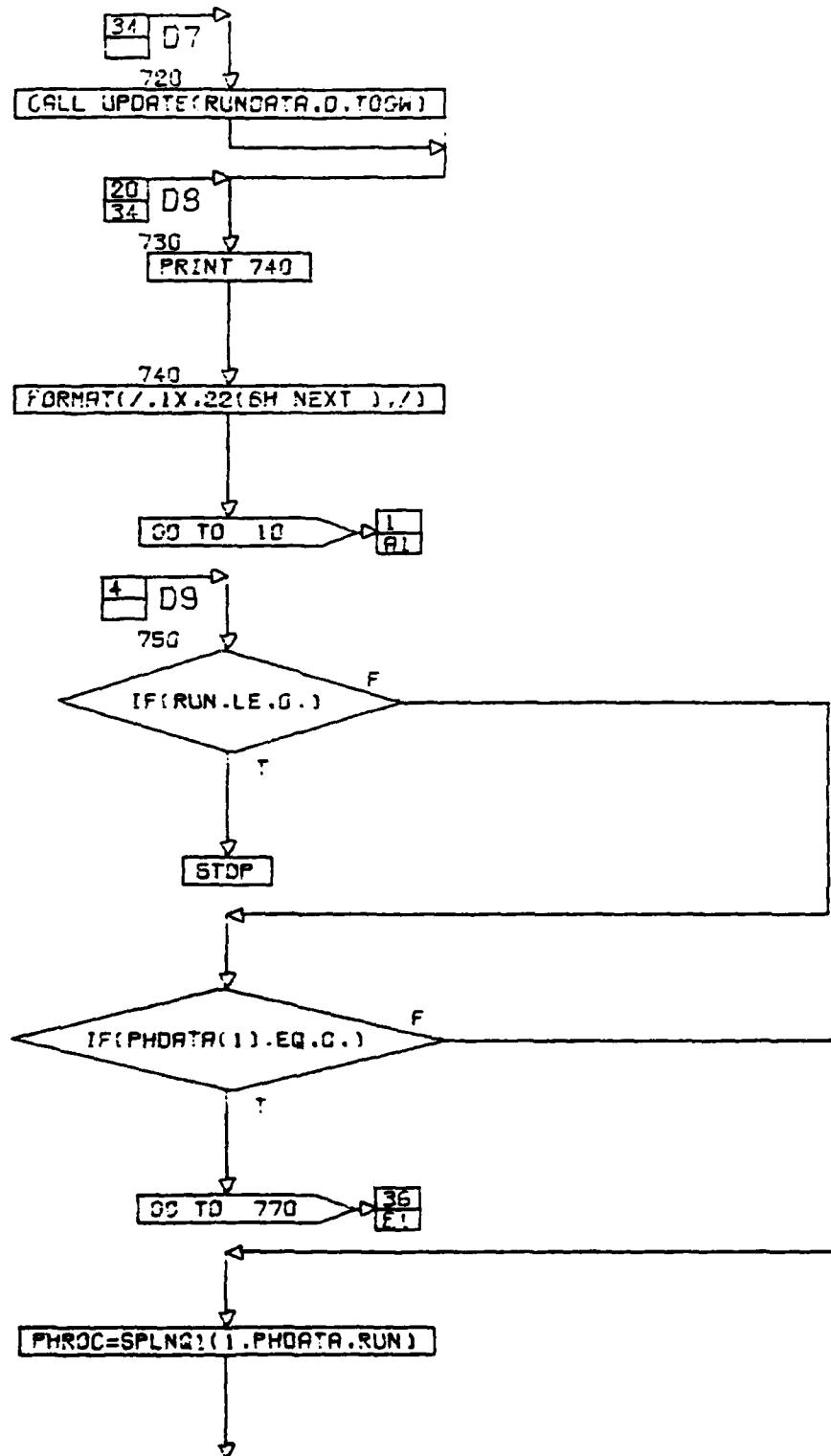
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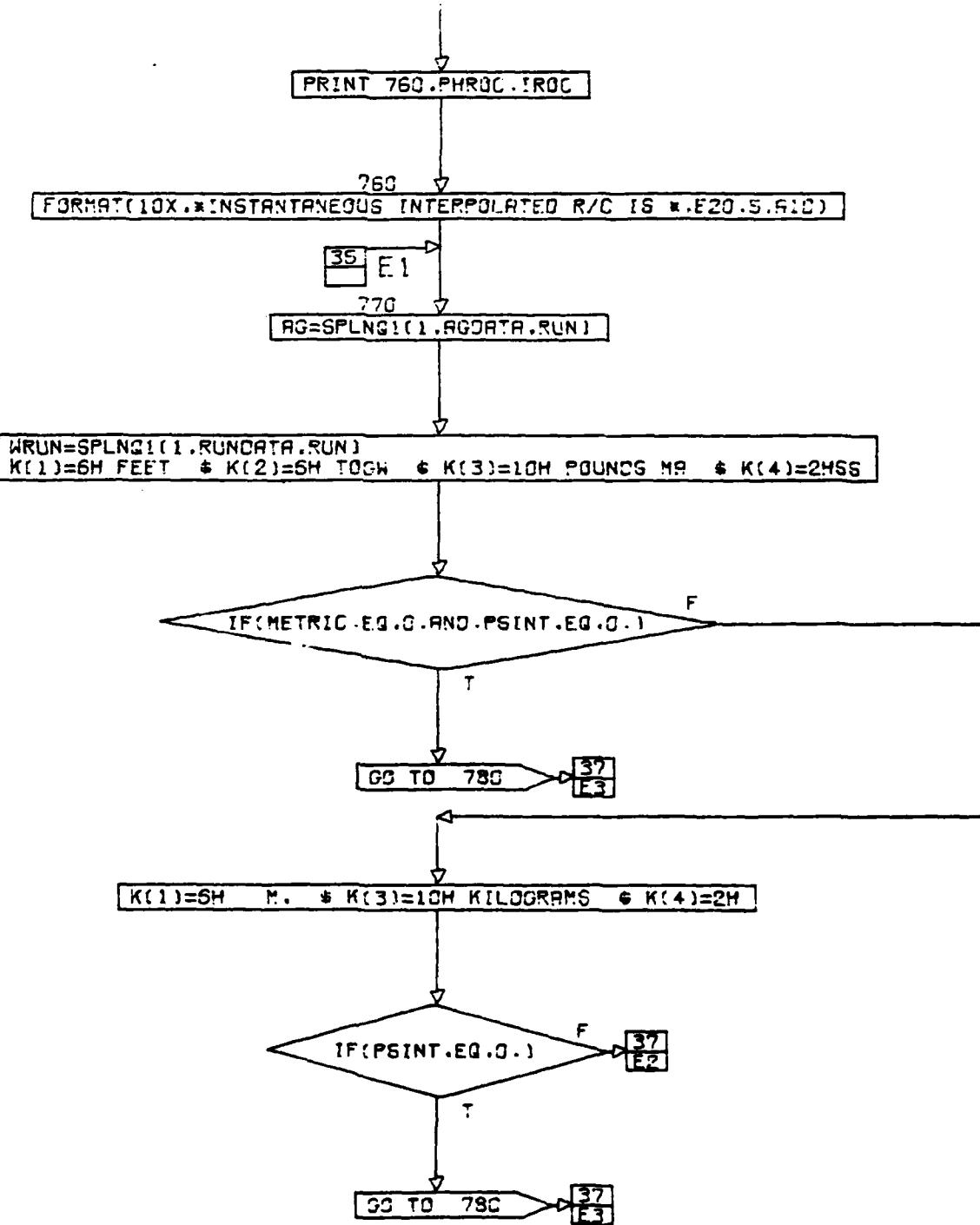
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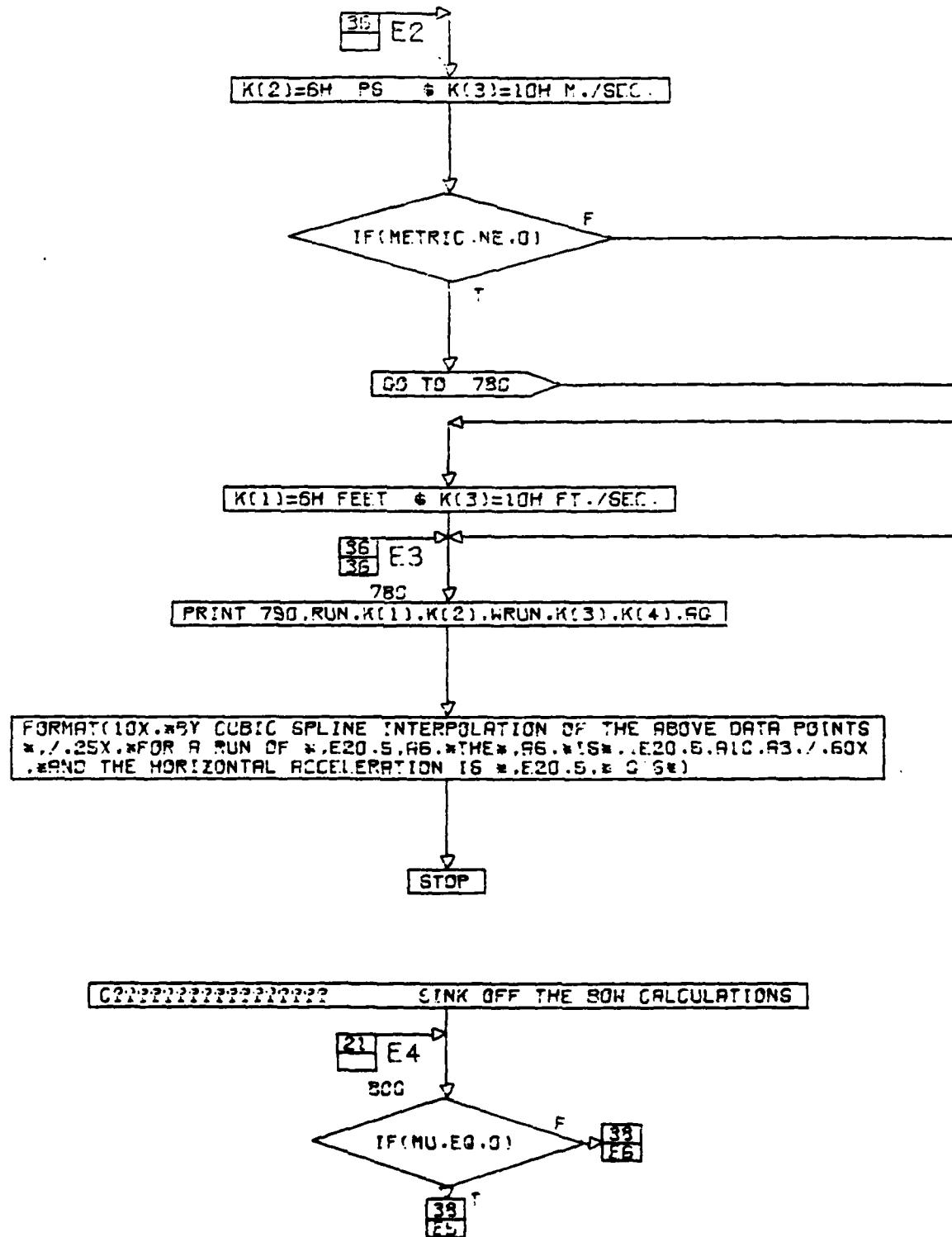


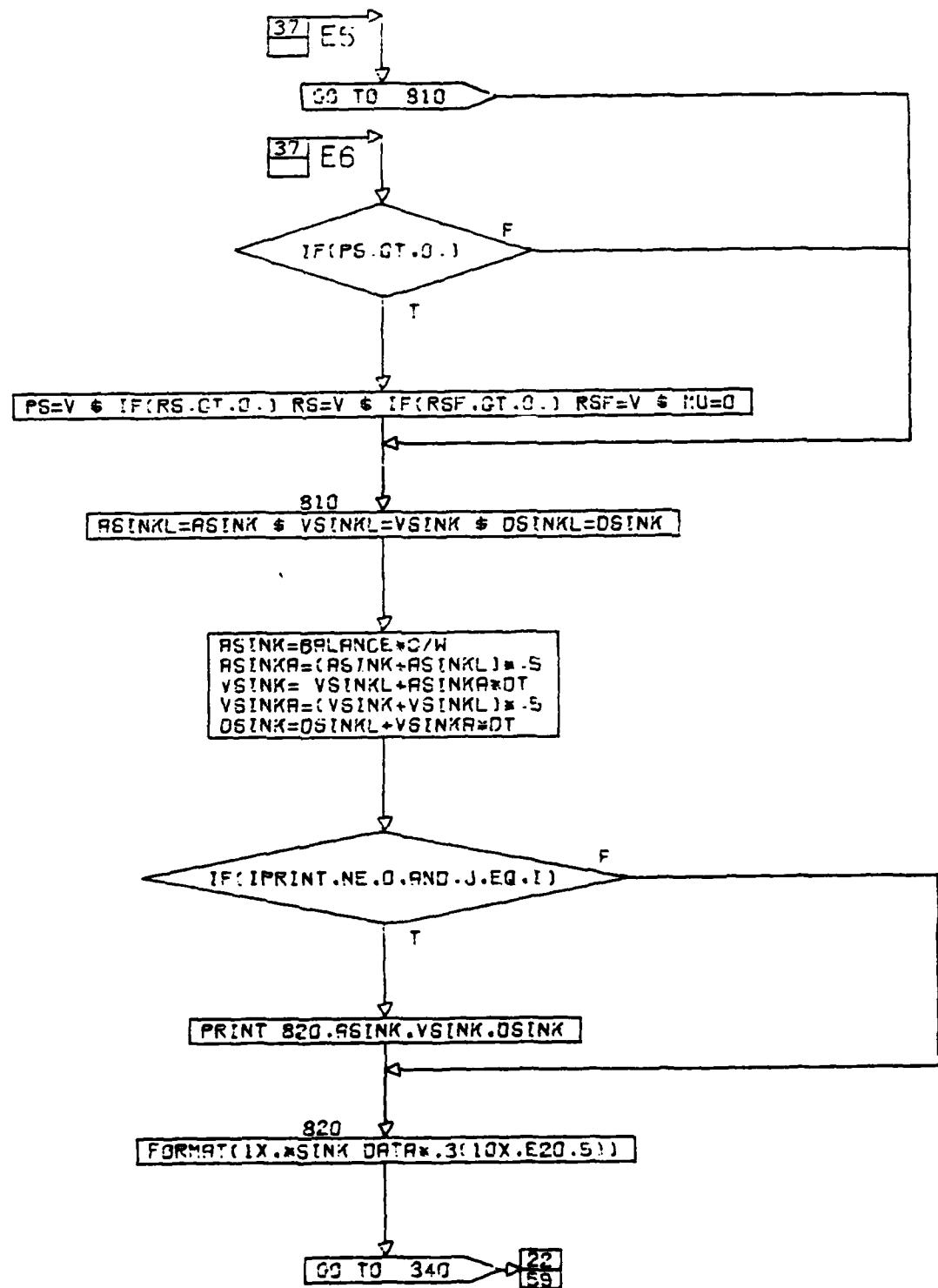


CONT. ON PG 37

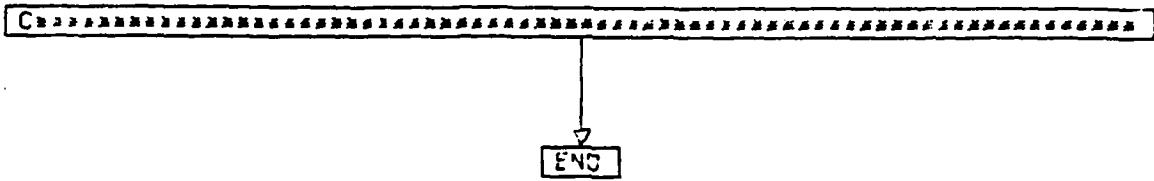
D-37

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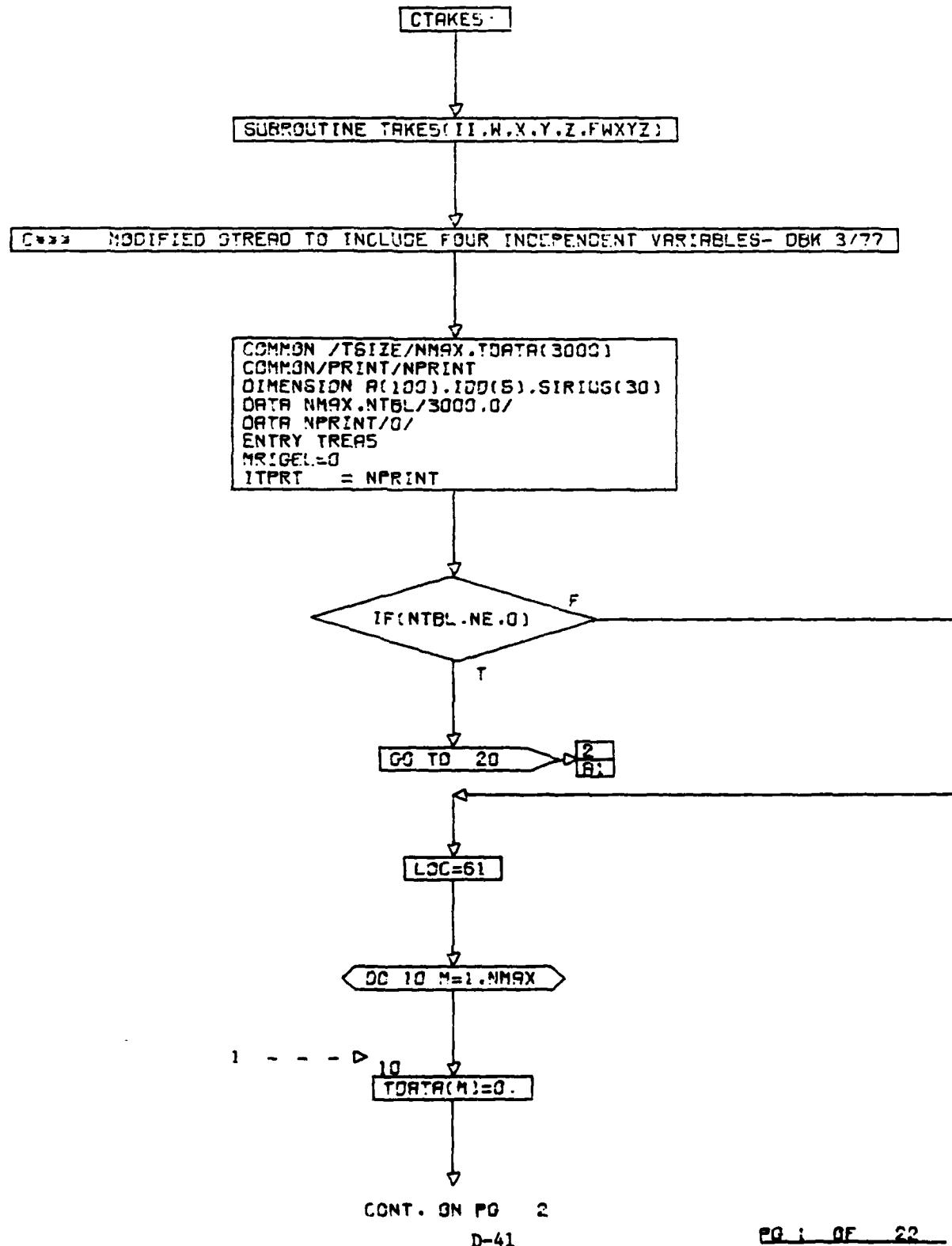


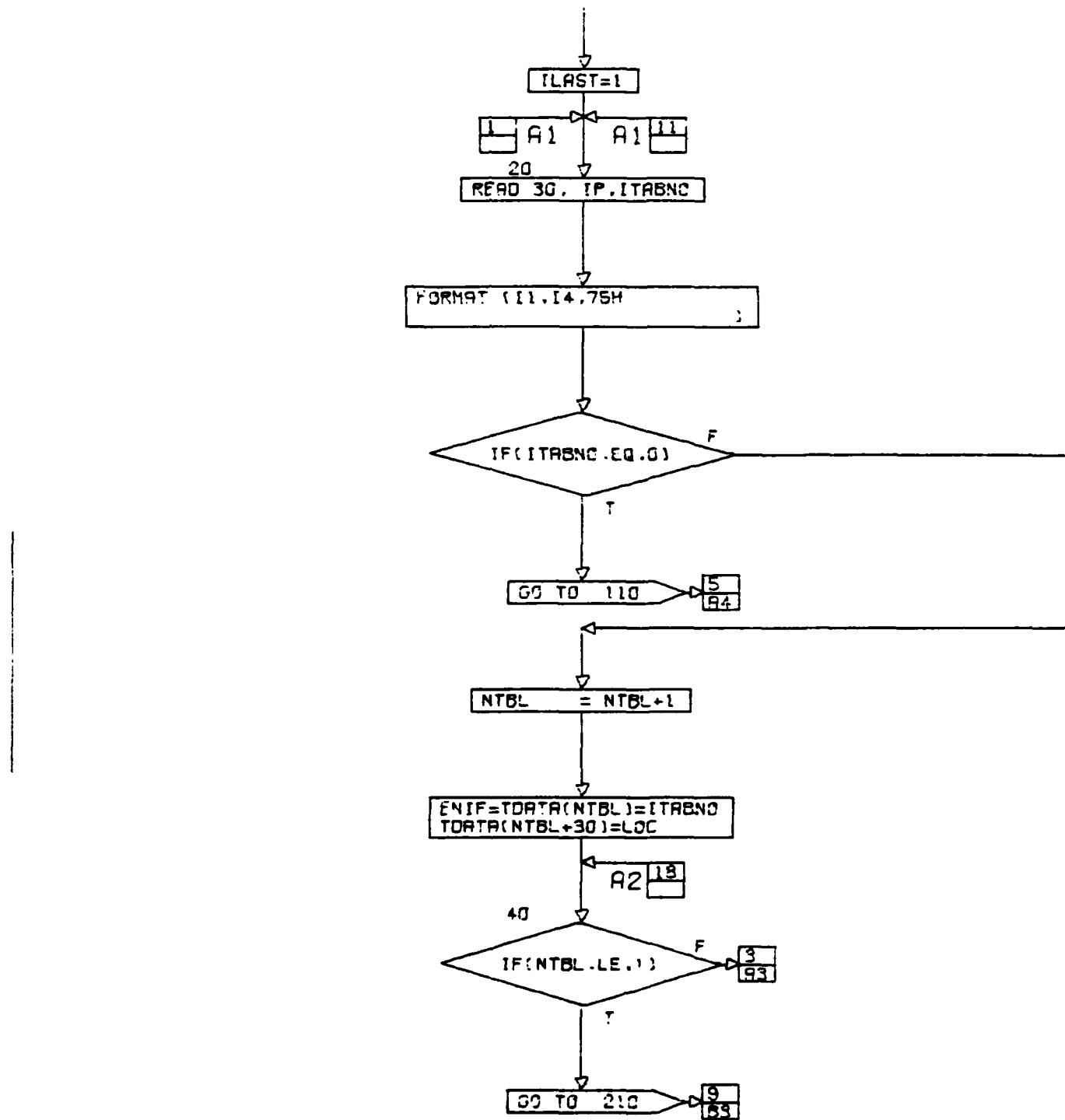
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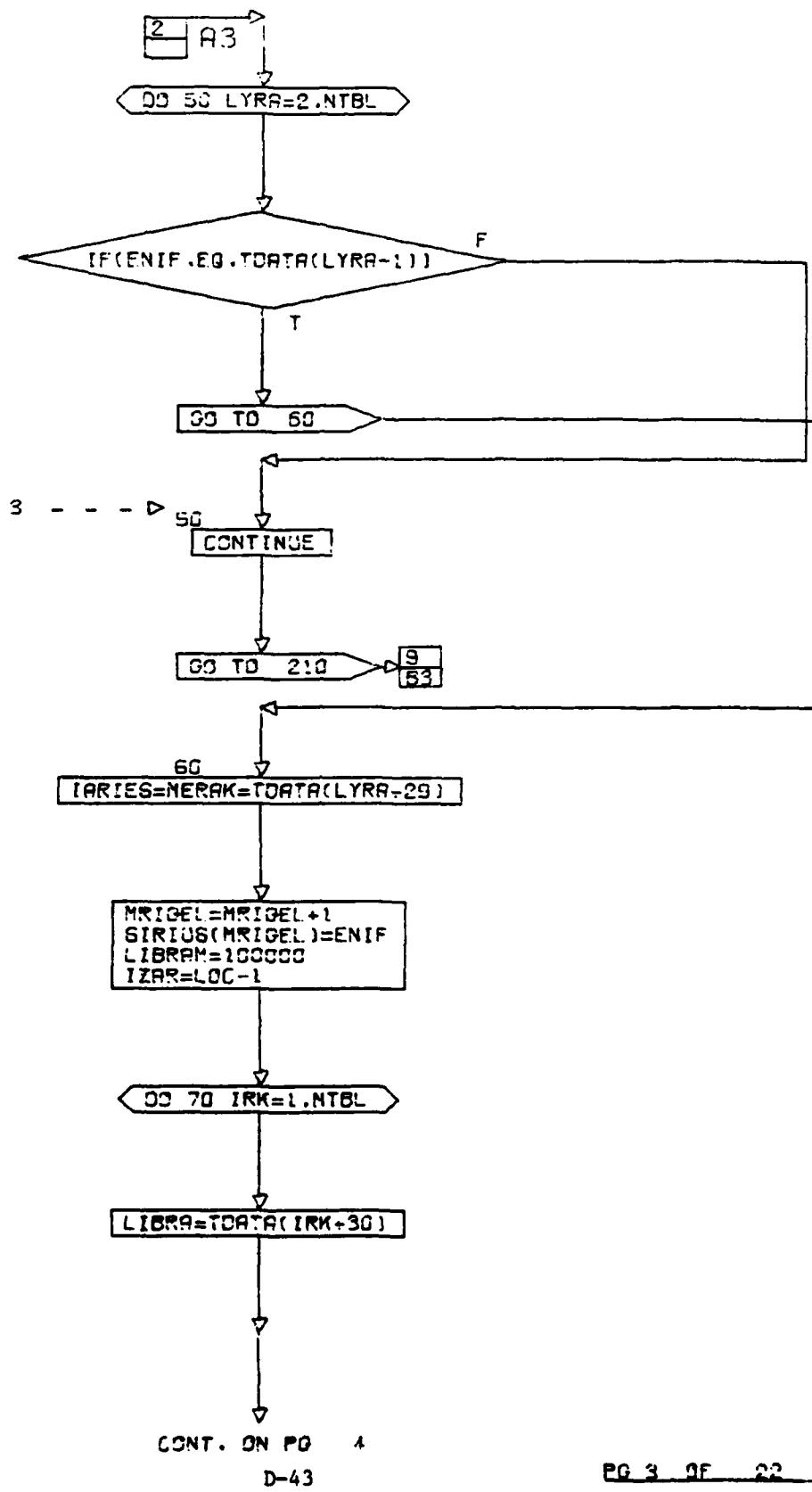


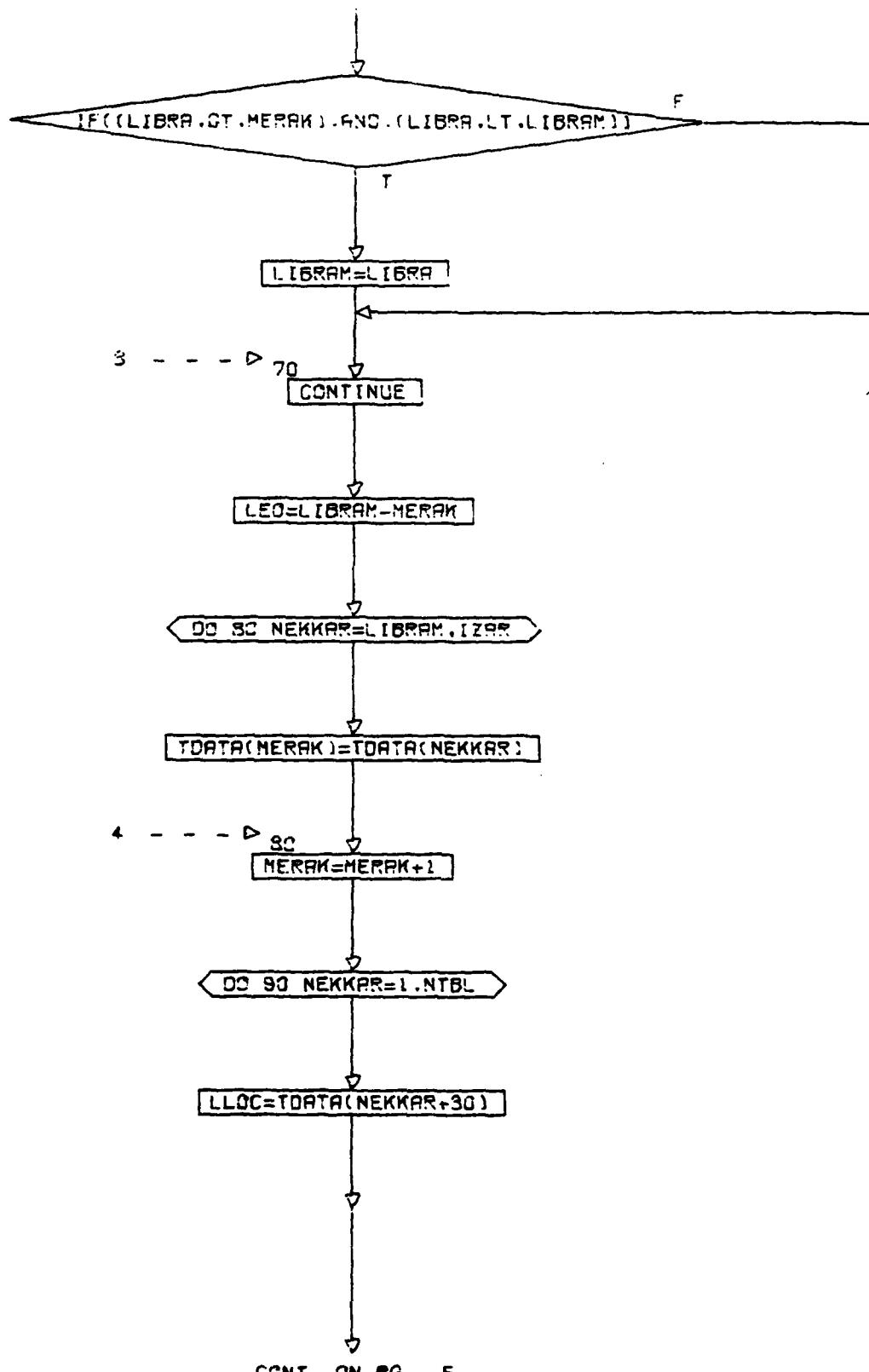
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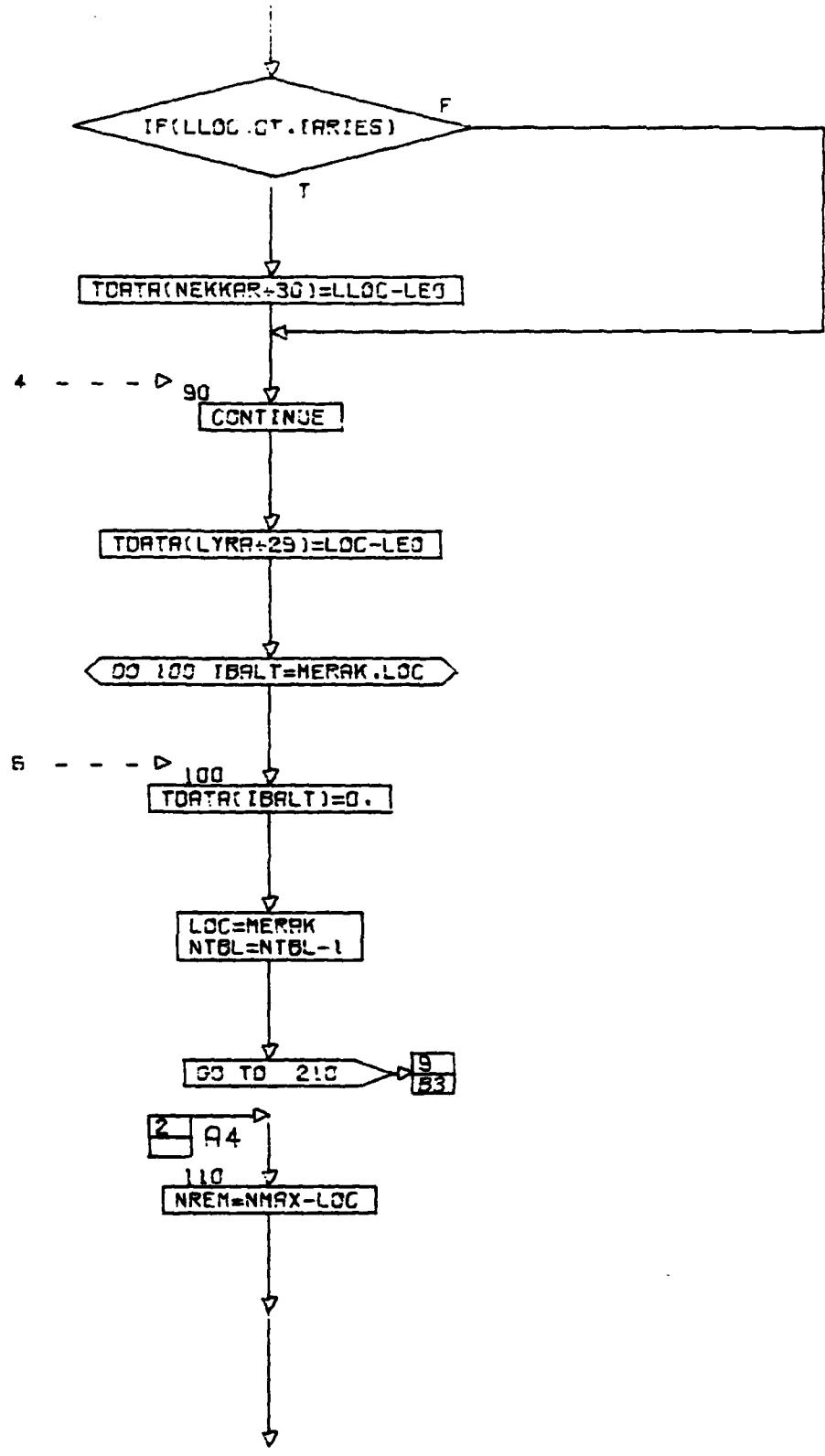
PG 39 FINAL

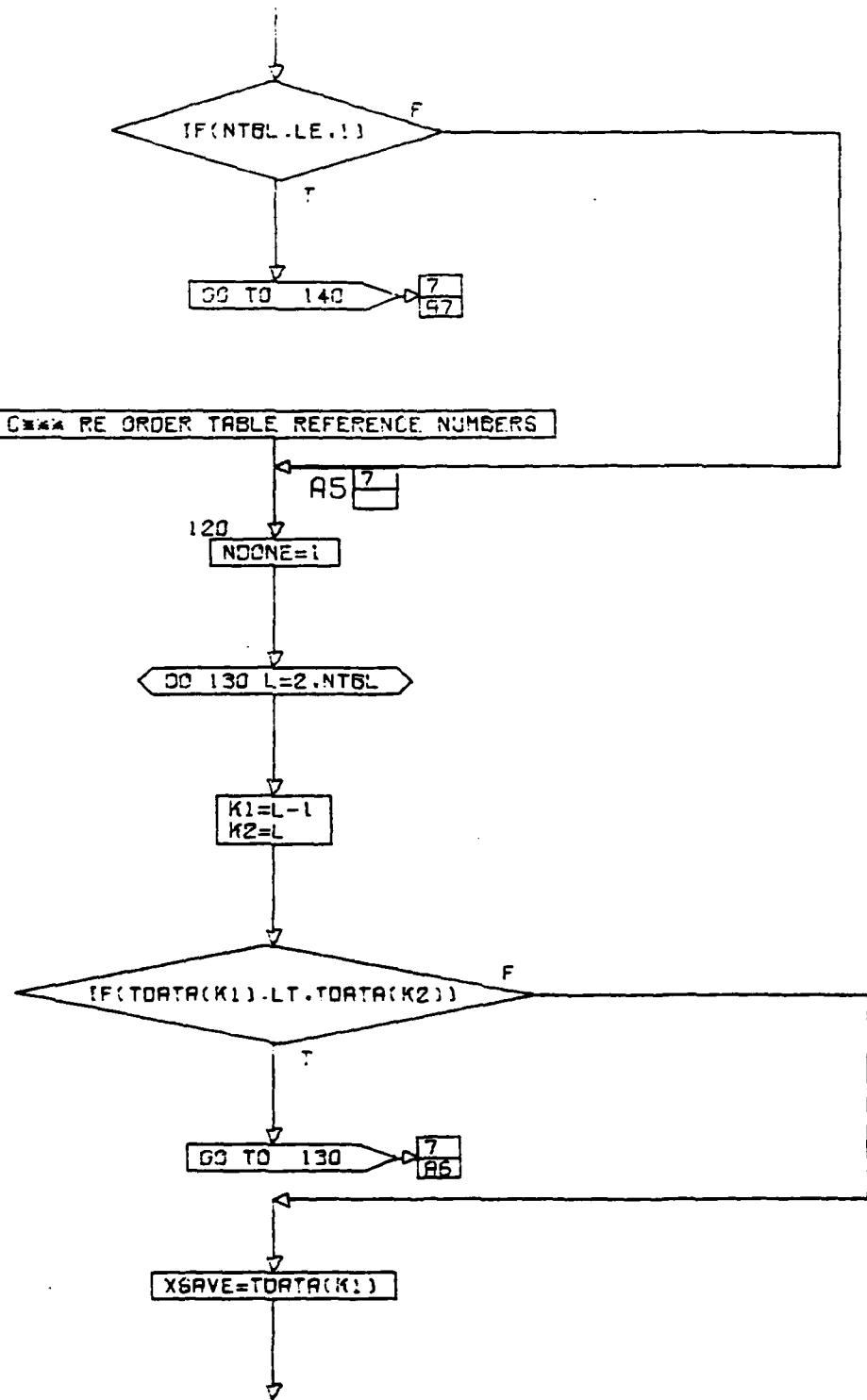


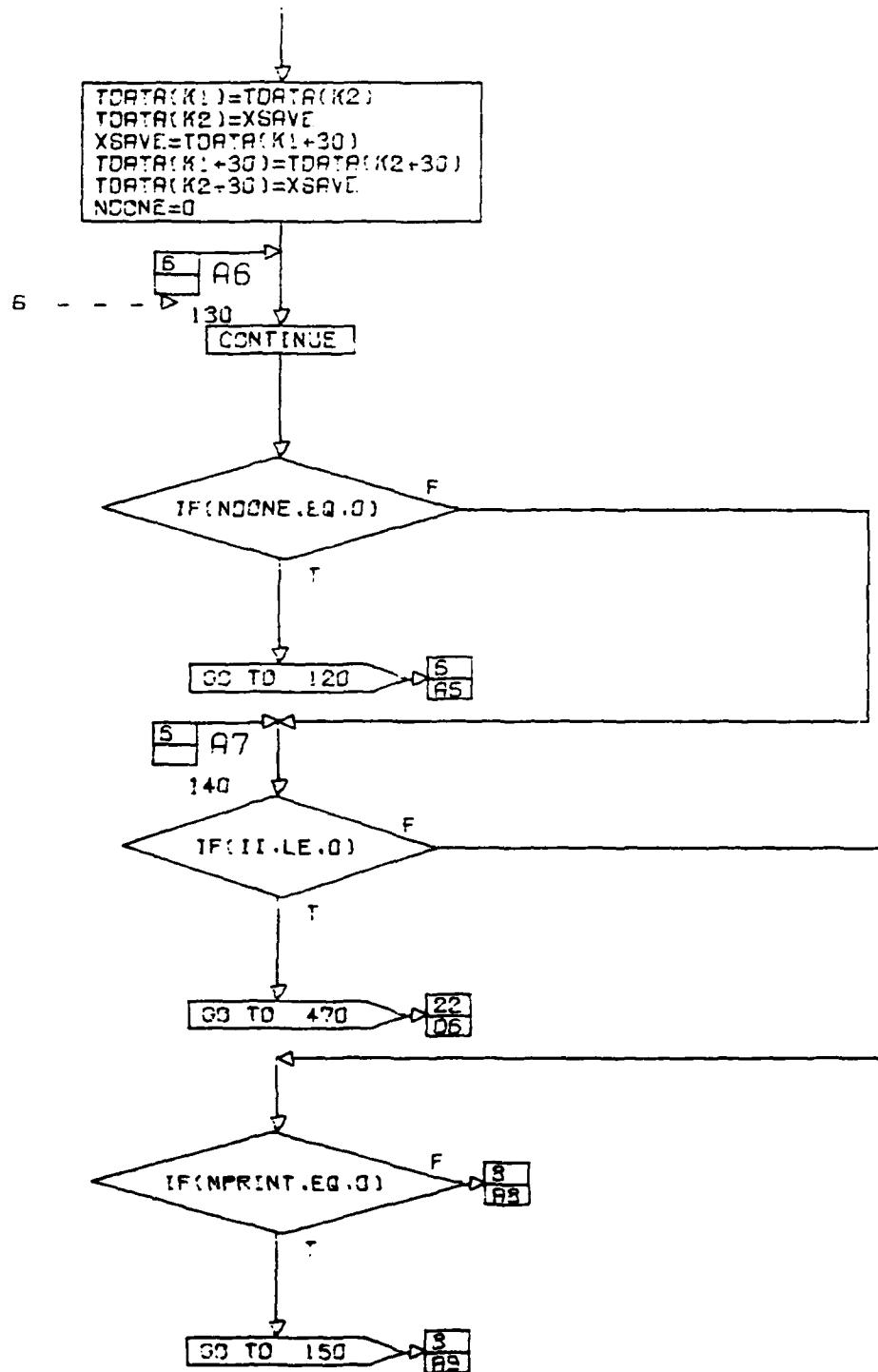


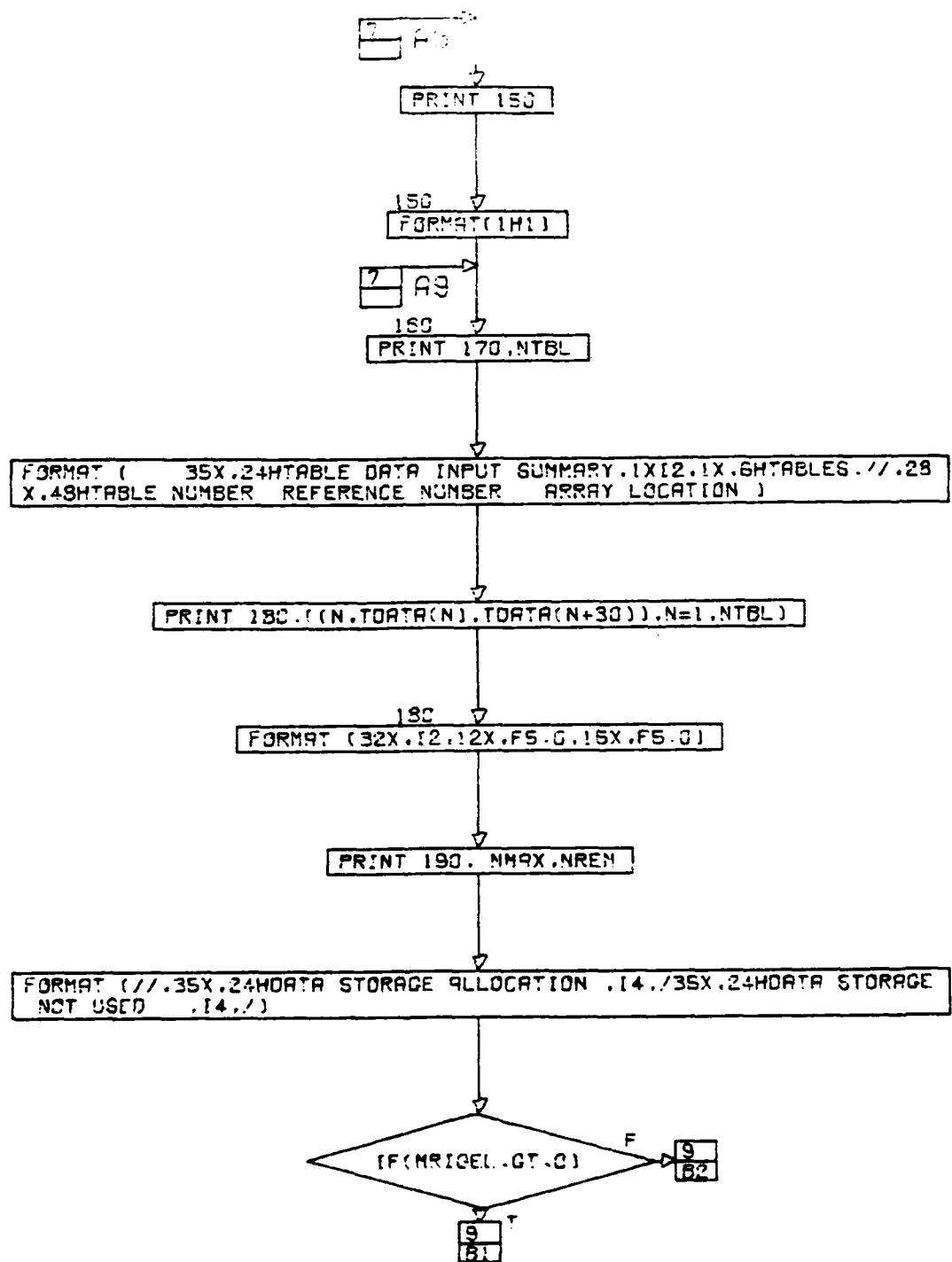


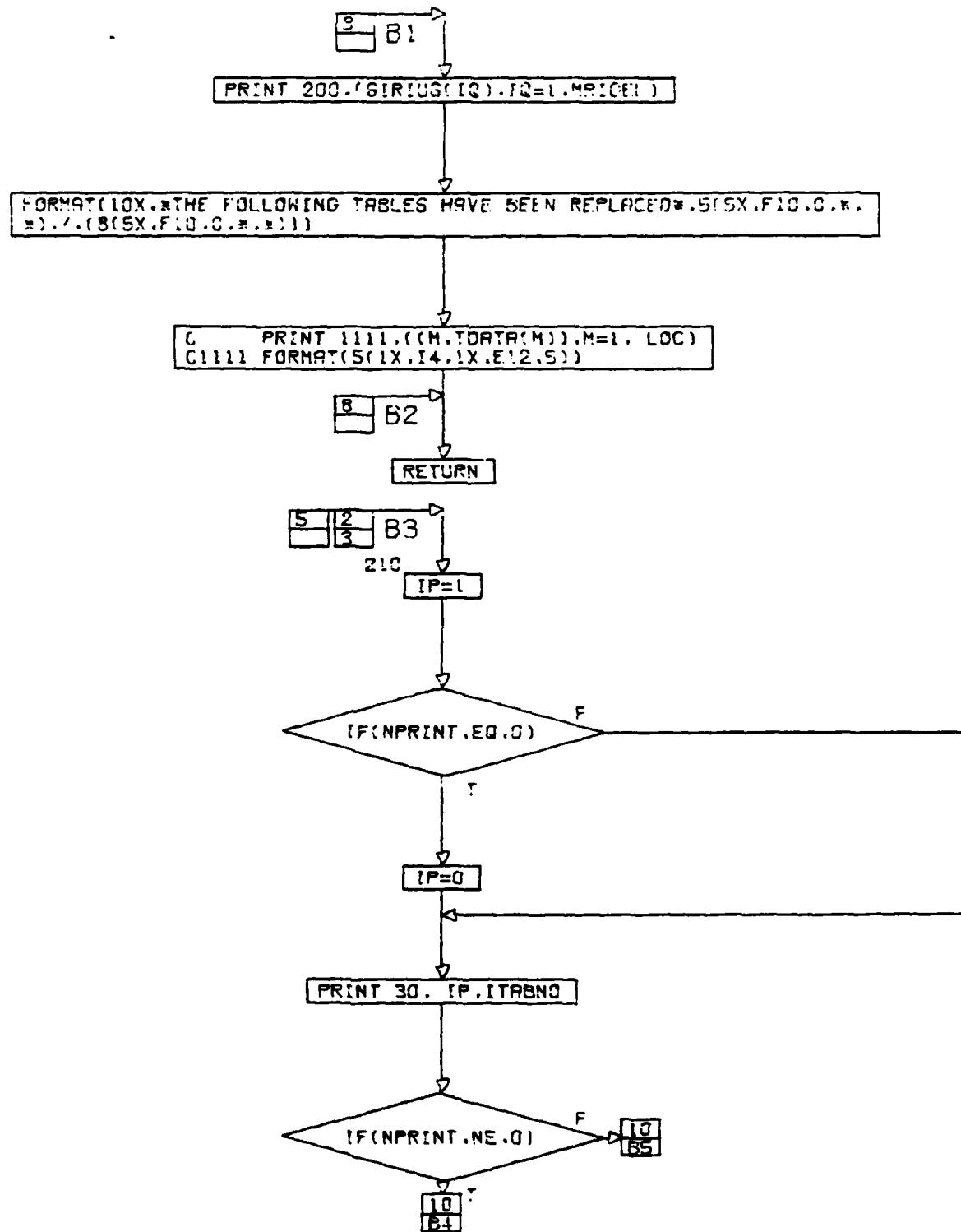


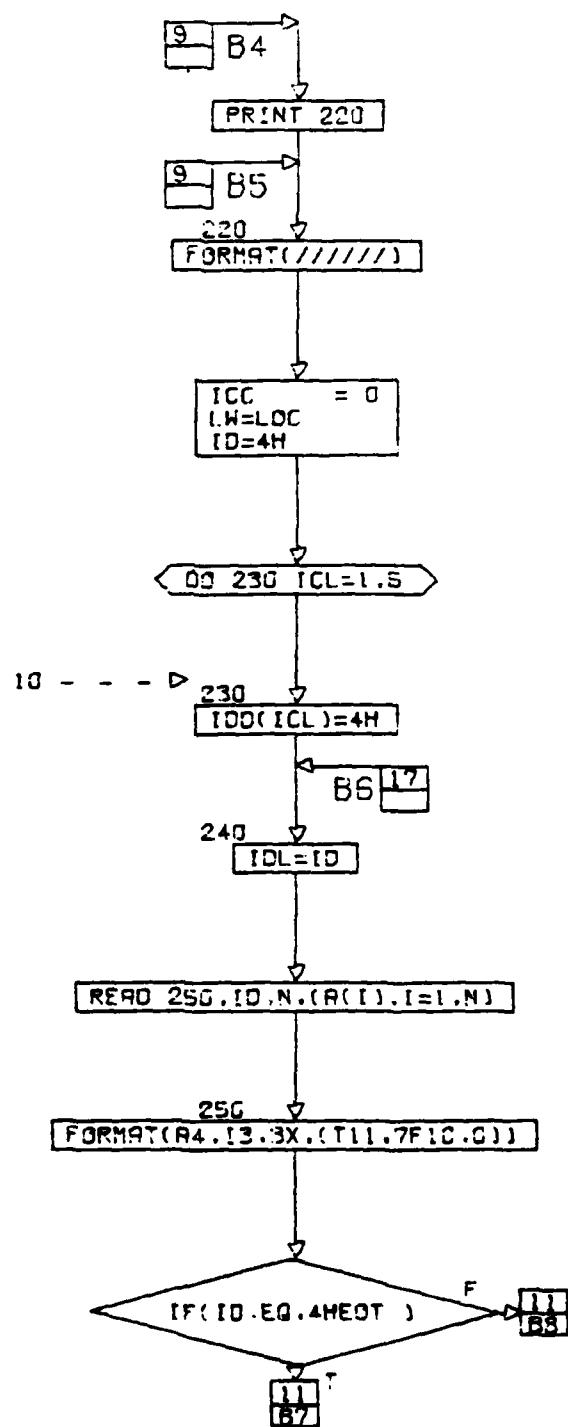








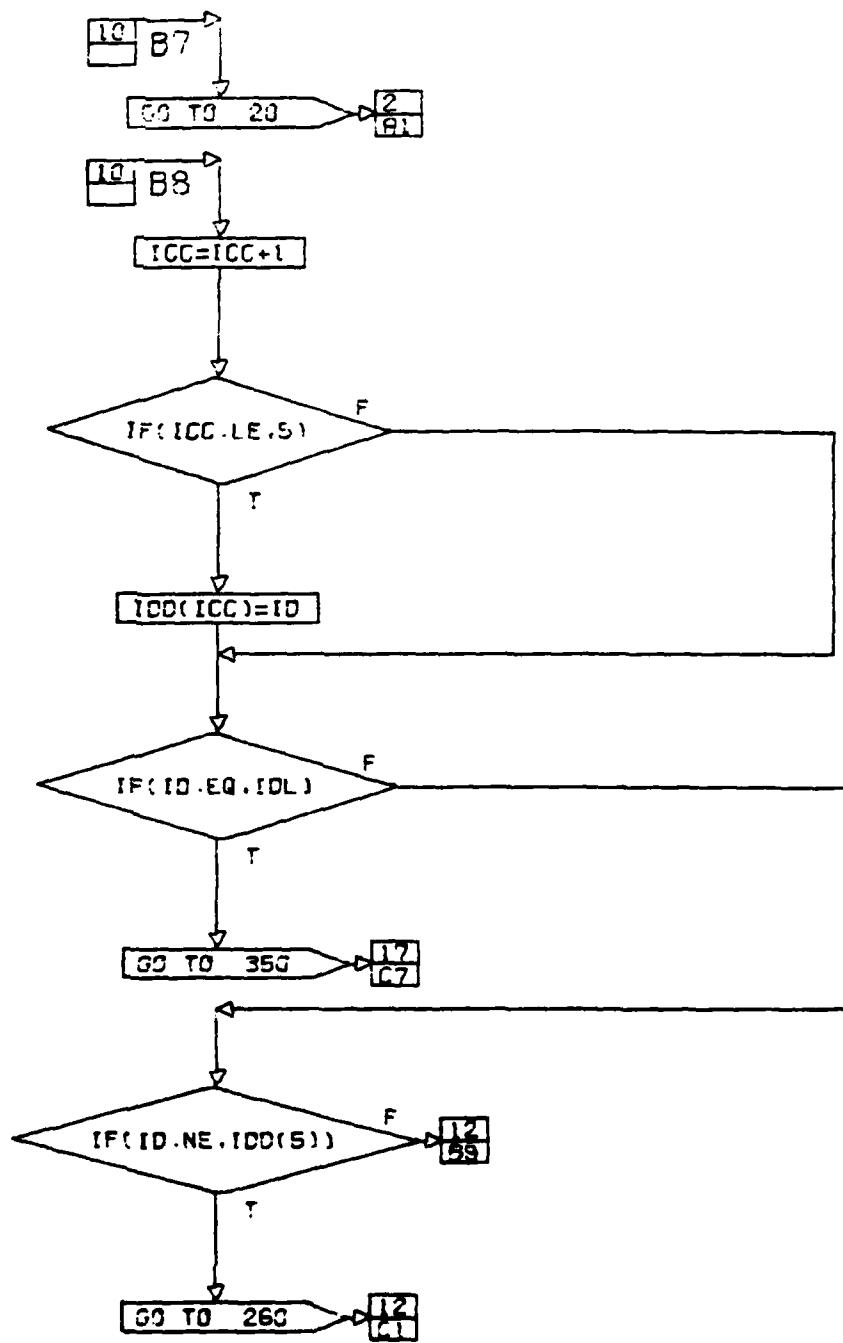




CONT. ON PG :1

D-50

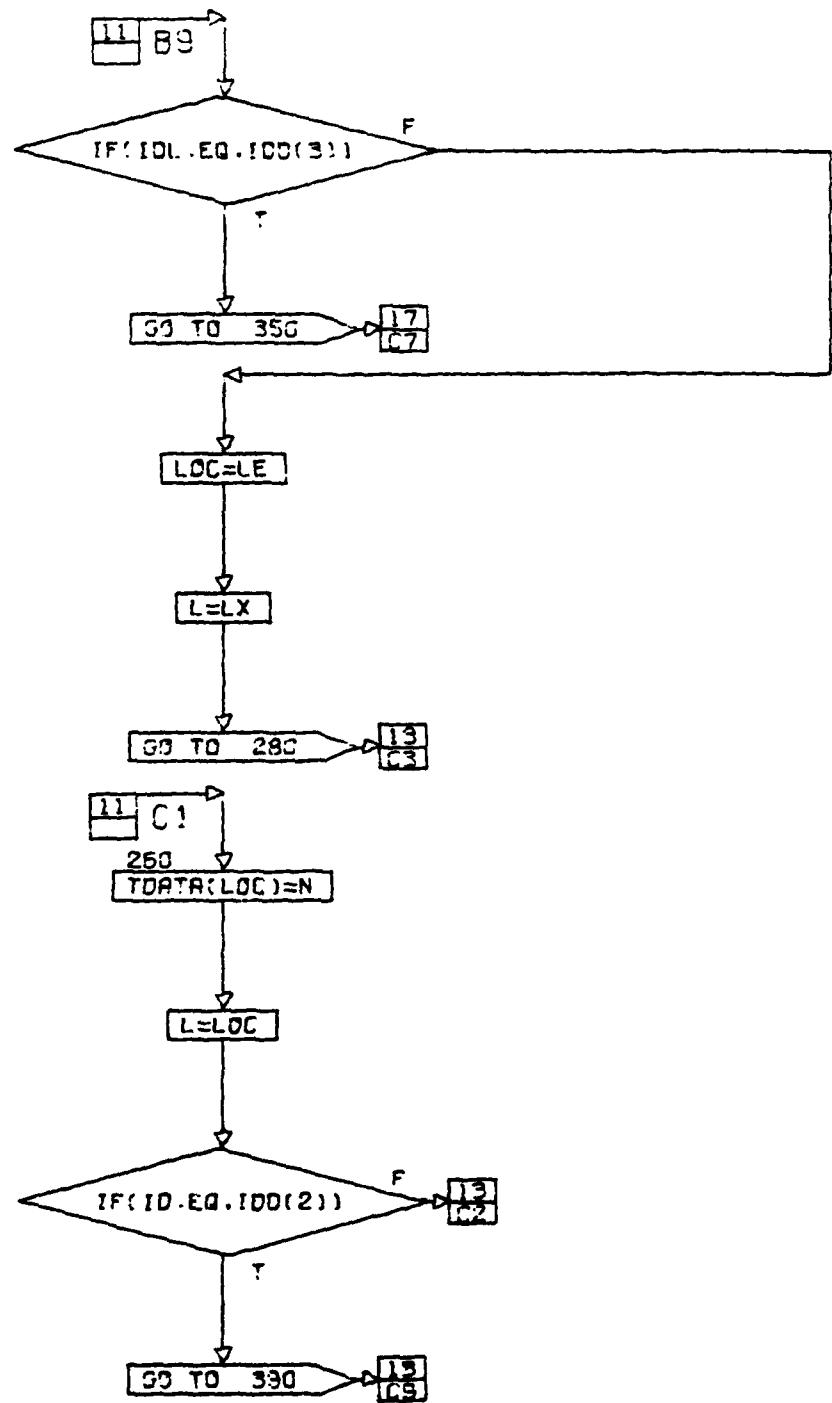
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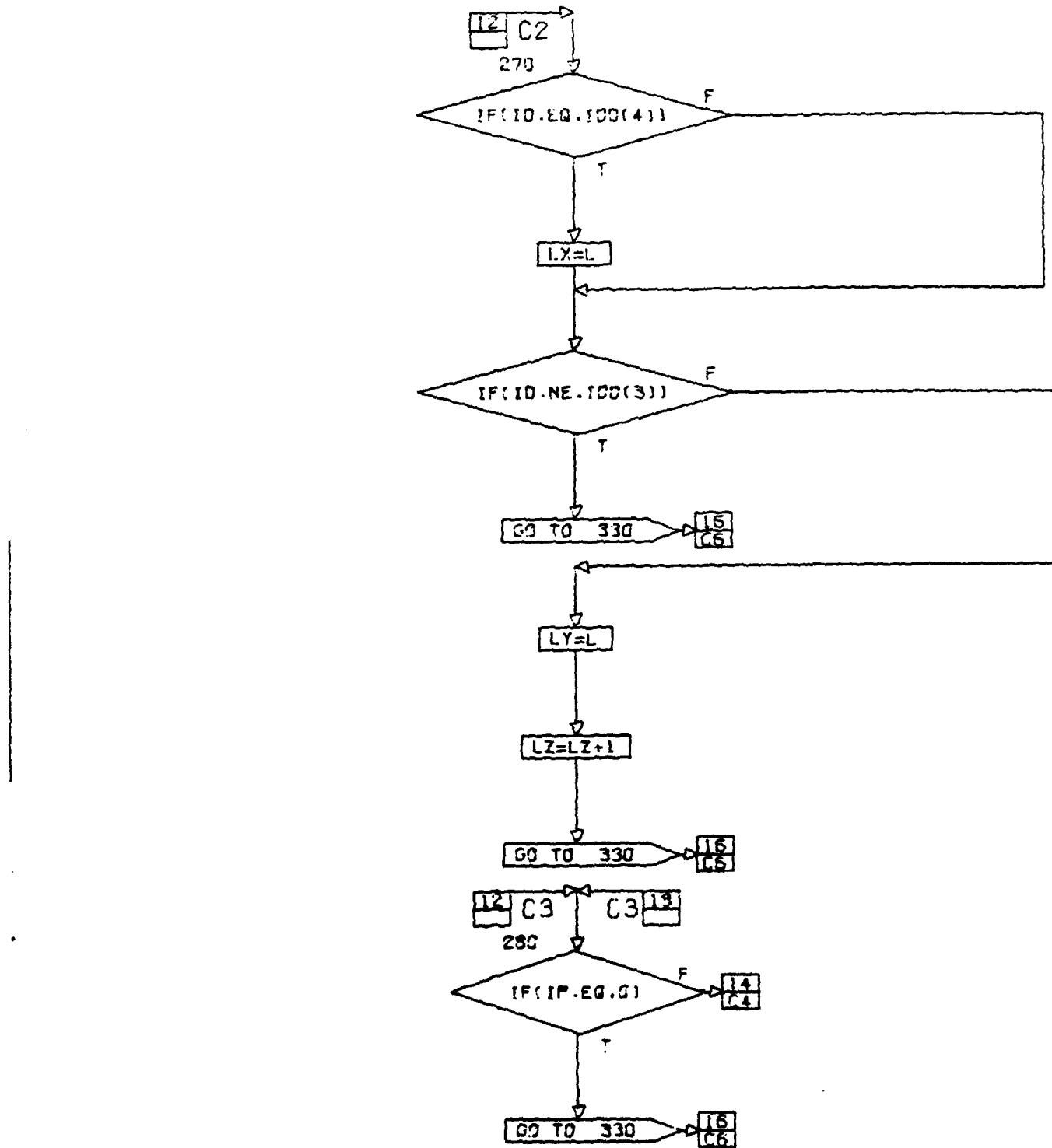


CONT. ON PG 12

D-51

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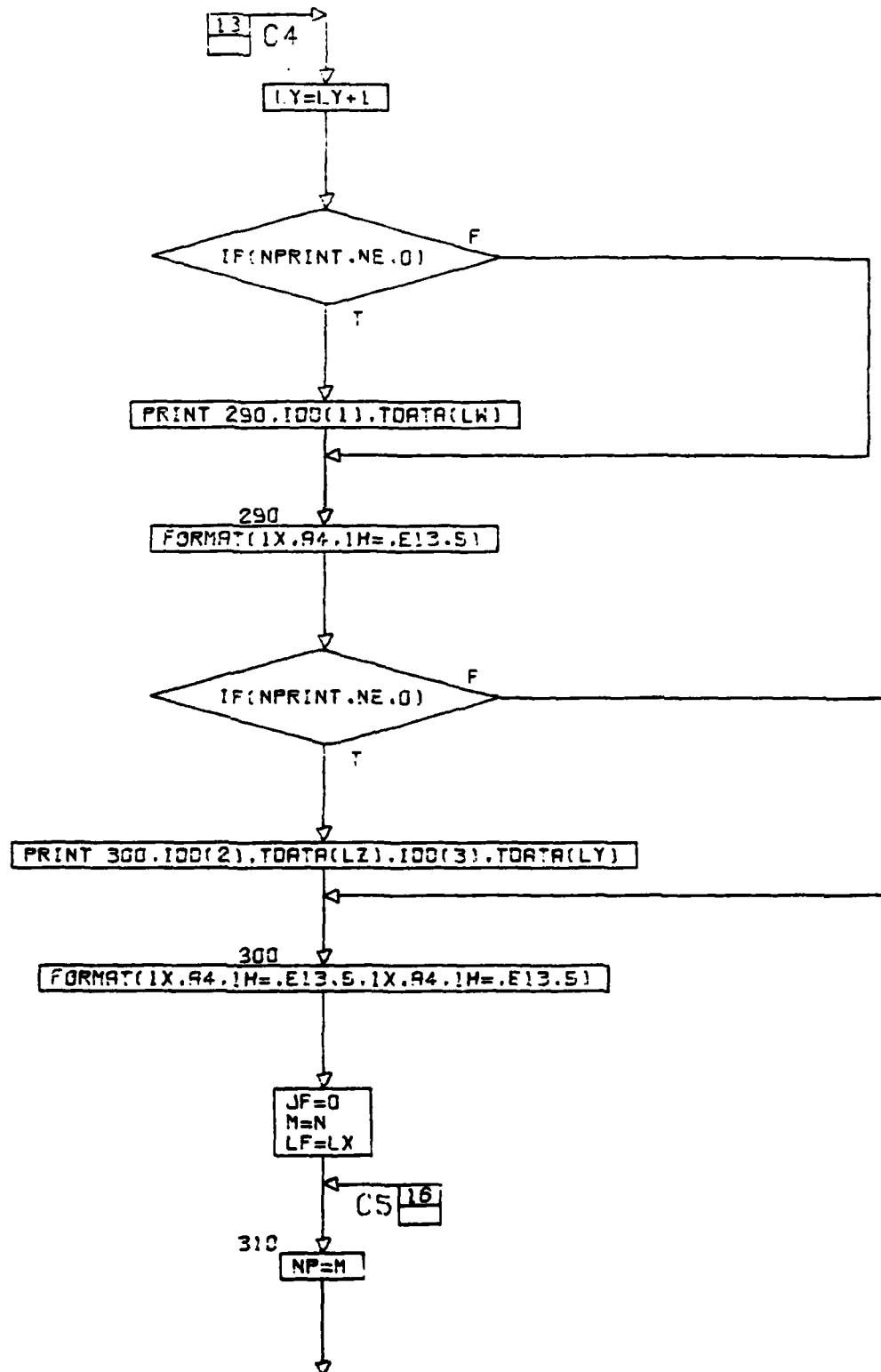




CONT. ON PG 14

D-53

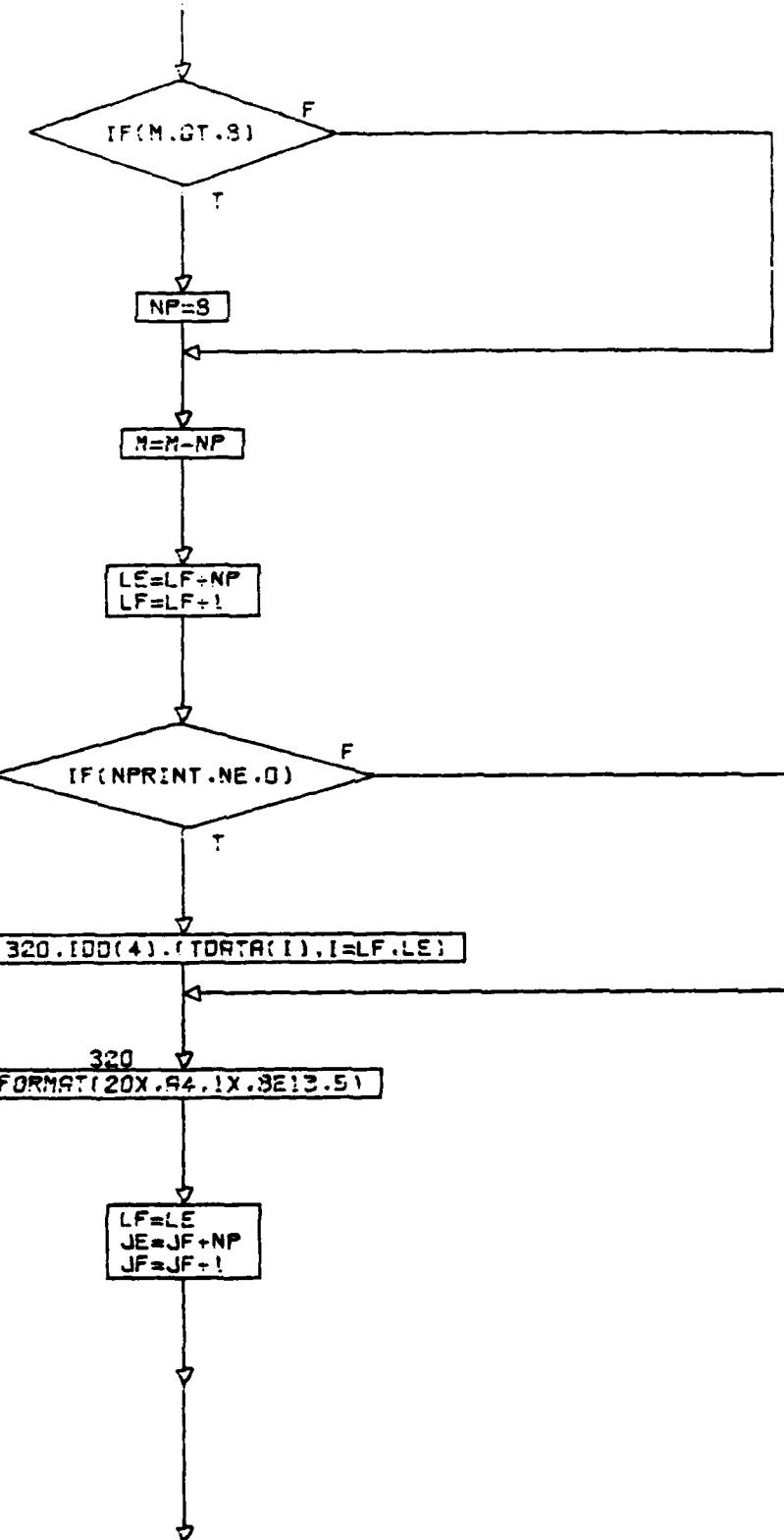
PG 13 OF 22

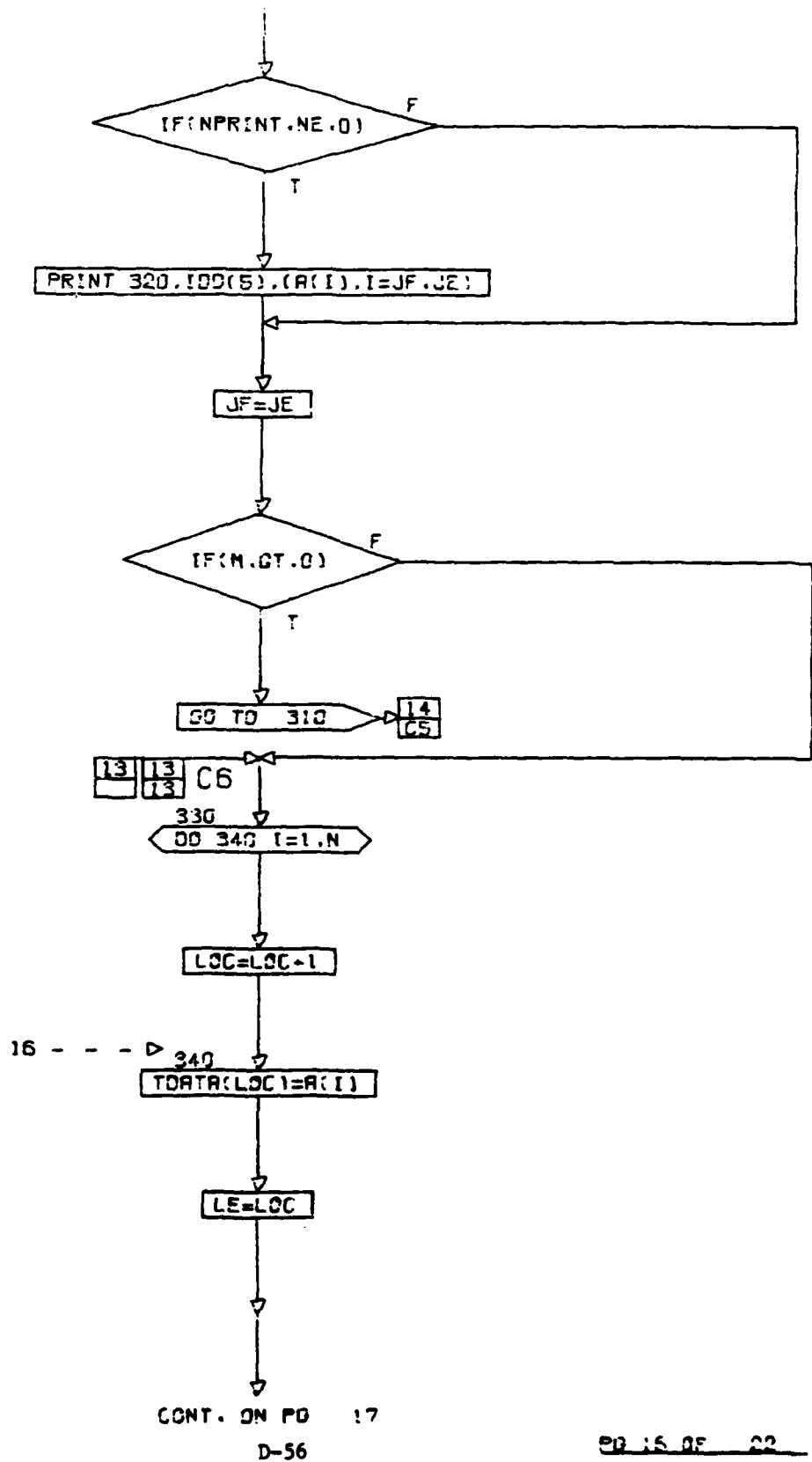


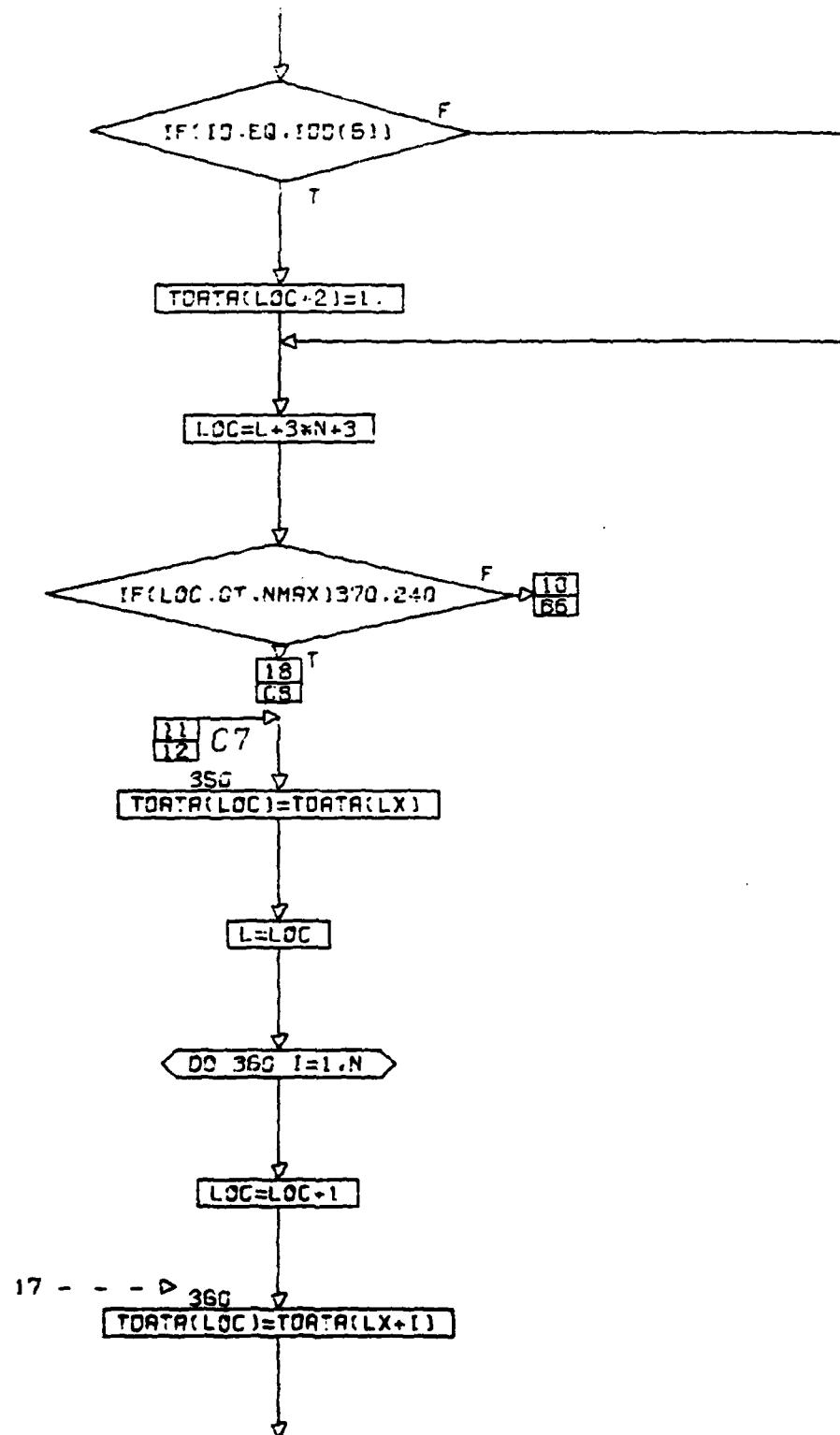
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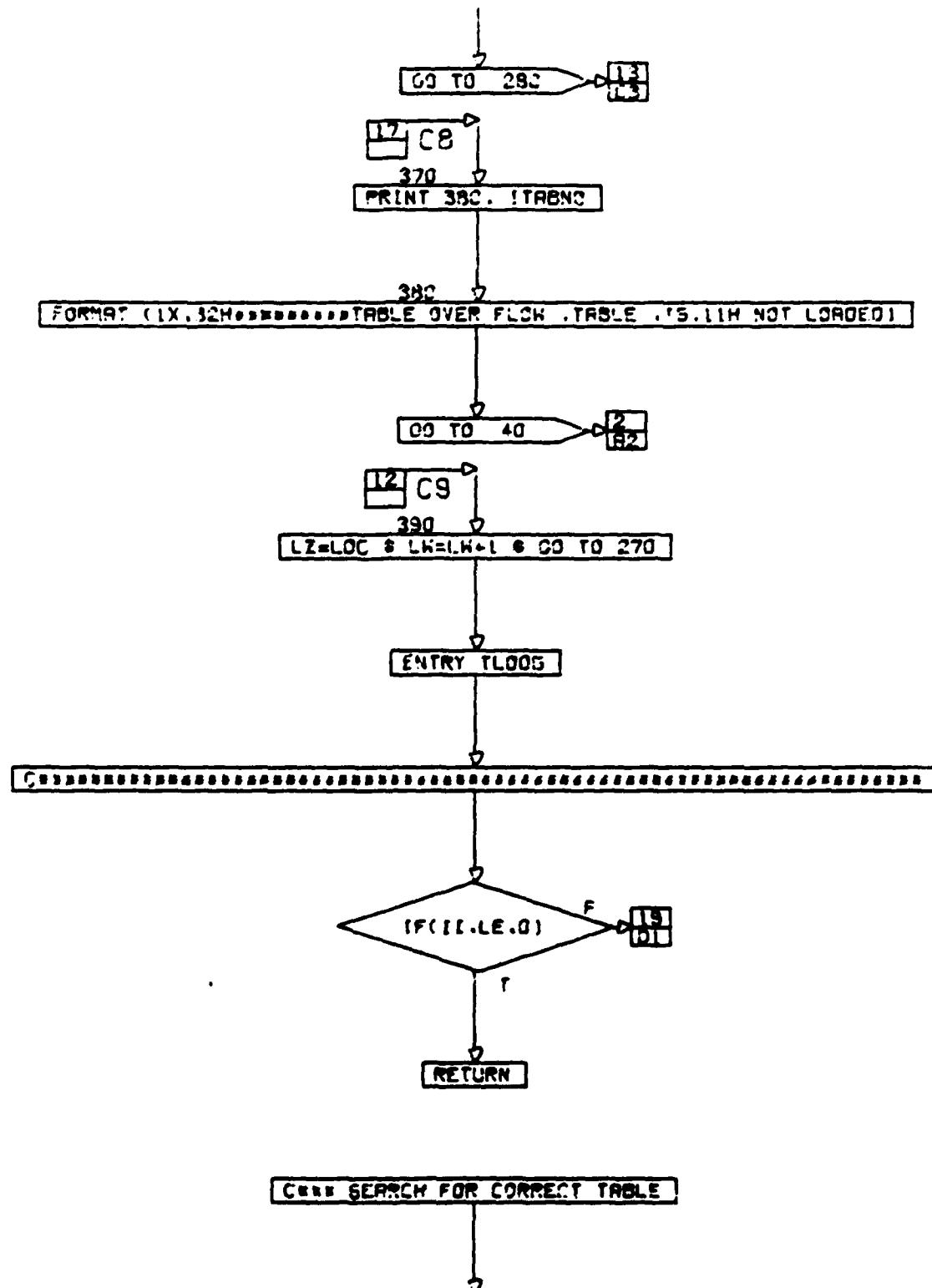
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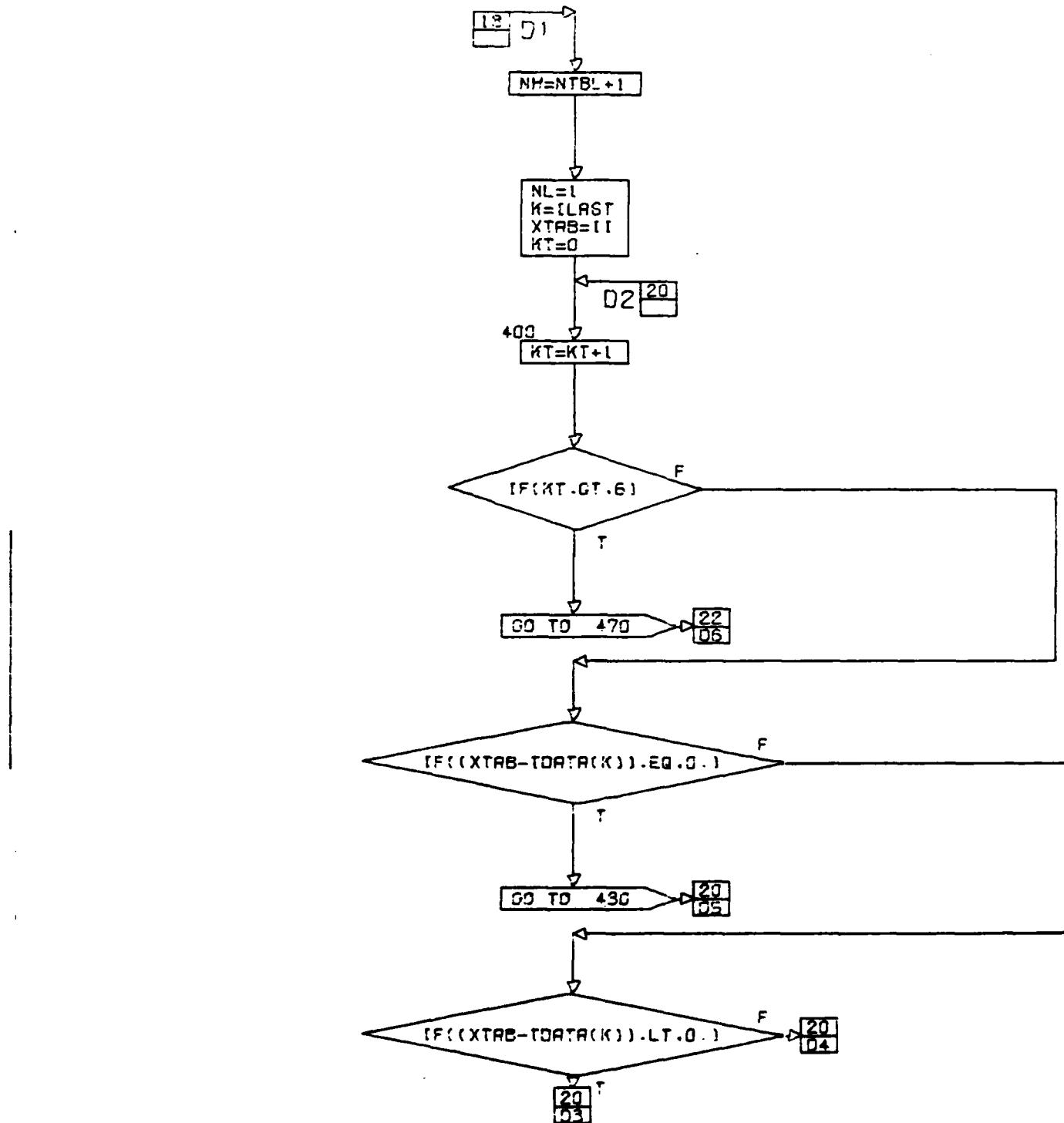
PG 14 OF 22

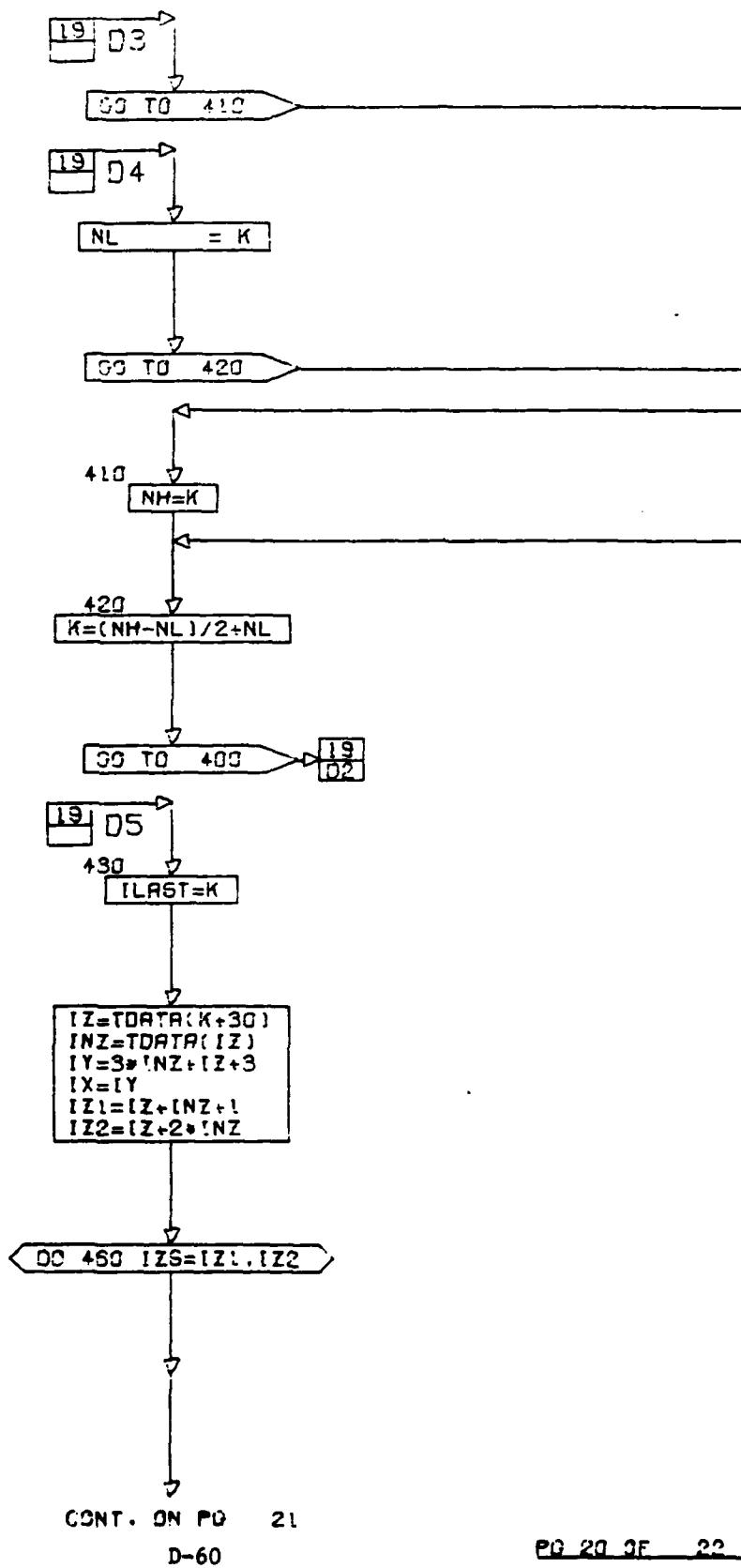








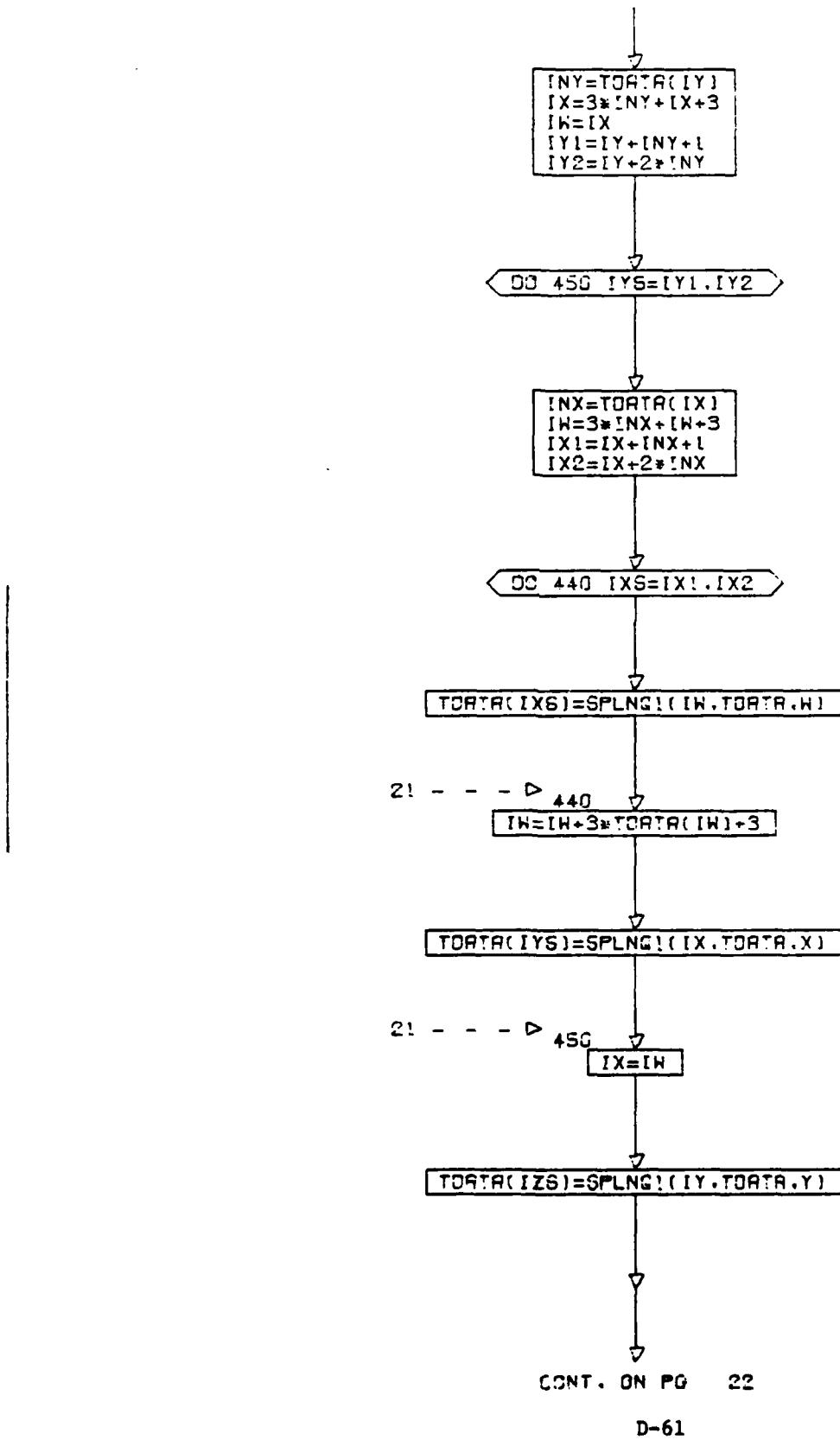




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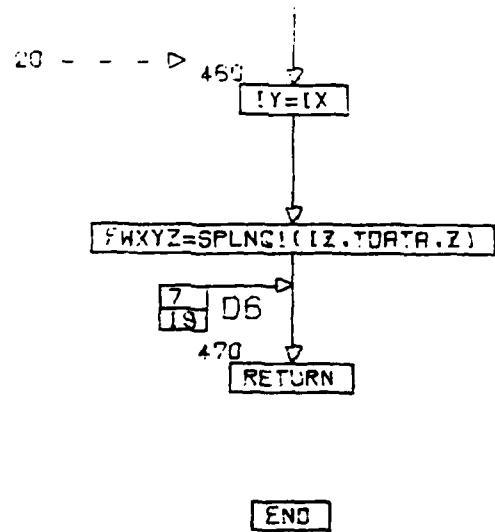
D-60

PG 20 3F 22



CONT. ON PG 22

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