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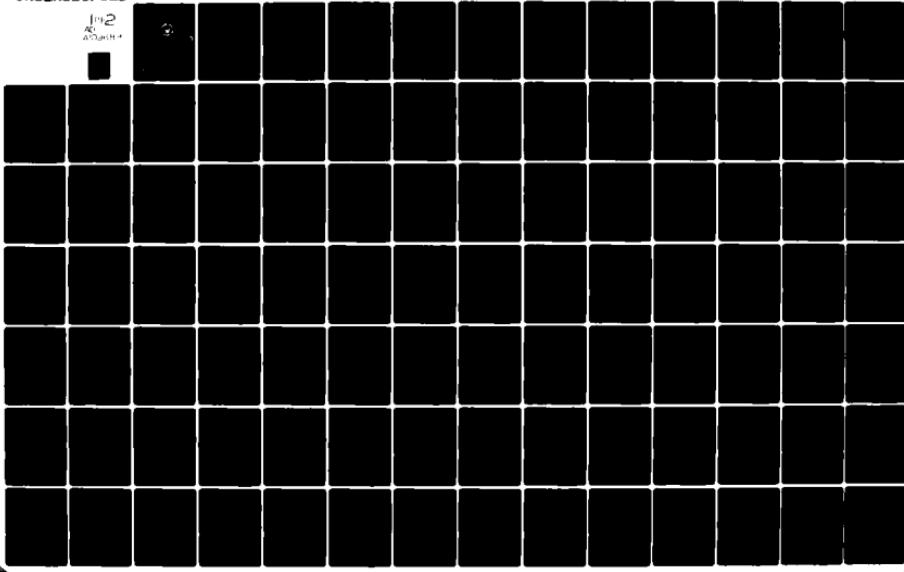
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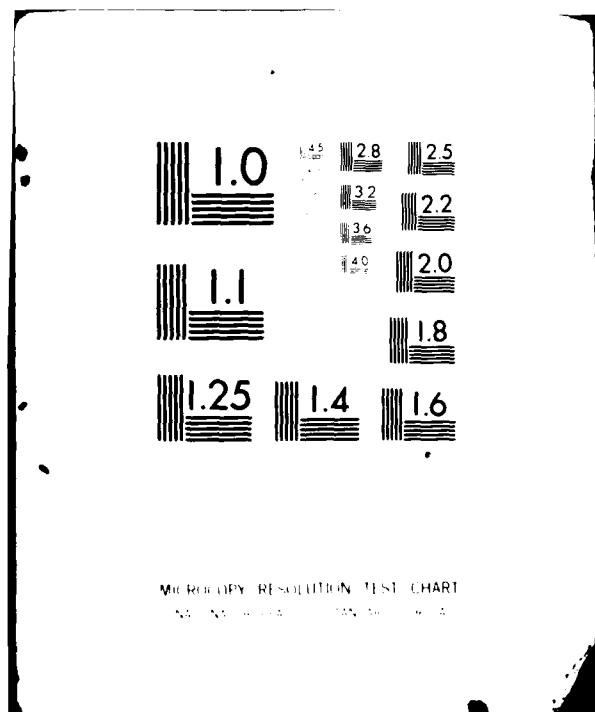
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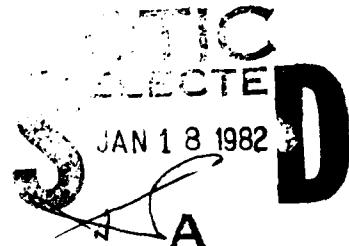
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NAVAL POSTGRADUATE SCHOOL
Monterey, California



THESIS

AN OPERATIONAL LANCHESTER-TYPE MODEL OF
SMALL-UNIT AMPHIBIOUS OPERATIONS

by

Soon Dae Park

September 1981

Thesis Advisor:

J. G. Taylor

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An Operational Lanchester-Type Model of
Small-Unit Amphibious Operations

by

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Lieutenant Colonel, Republic of Korea Marine Corps
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Submitted in partial fulfillment of the
requirements for the degree of

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ABSTRACT

This thesis presents an operational Lanchester-type model of small-unit amphibious operations. This relatively simple model has been developed to demonstrate the basics of model building to the beginning student interested in amphibious warfare. The model is a time sequenced, deterministic, force-on-force combat model that is implemented on a digital computer. A brief discussion of considerations for modeling amphibious operations is given. The details of the model are presented for a specific amphibious-warfare scenario. Additionally, a computer terrain-contour-line plotting program is provided to assist the combat modeler to fit a parameterized-terrain to real terrain.

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I. INTRODUCTION

During the past several decades, combat models have been widely used to support military decisions. As the art of combat modeling becomes more advanced, combat modelers are continuously building more and more complicated models. To the beginning modeler, the ability to understand how those models operate is difficult, if not impossible. It is the purpose of this thesis to develop a simple amphibious-operations model that will demonstrate the basics of model building to the beginning student interested in amphibious warfare. In the broadest sense, an amphibious operation is a combined-arms operation which includes all forms of combat--land, air, sea. This thesis will limit itself to the small-unit amphibious operation.

This project started with two basic models: one was developed as the auxiliary model for the evaluation of design and employment alternatives for the LVA (Landing Vehicle Assault) in the thesis of David Larkin Chadwick (September 1978). The other is the Smoler-Mills model which was developed in the thesis of Josef Smoler (September 1979) and enriched in the thesis of Glen Mills (September 1980).

In Chapter II, general considerations for modeling amphibious operations are briefly discussed. Then, a small-scale computer-based Lanchester-type amphibious-operations model is presented, including analytical details of the algorithms used

to represent each of the combat processes considered. Although the model was developed for a specific scenario, it is sufficiently general in design so that it can be adapted to other small-scale amphibious-operations scenarios with only relatively few modifications.

II. GENERAL CONSIDERATIONS FOR MODELING AMPHIBIOUS OPERATIONS

A. CHARACTERISTICS OF AMPHIBIOUS OPERATIONS

In order to model an amphibious operation, it is first of all necessary to understand what is going on in a real amphibious operation. Only after one knows the details of what is happening in such a complex combat operation, can one begin to sift out the cluttering details and make valid simplifying assumptions to come up with a tractable model.

One of the key characteristics that serves to distinguish amphibious operations from other types of military operations is that a complete military force must be transferred ashore in an orderly manner under the constant pressure of actual or potential attack from hostile forces. Because the over-all amphibious assault requires precise and timely execution, the various component operations must be carried out in a planned sequence (especially early in the assault) according to a strict schedule. This sequence and these schedules, however, must be sufficiently flexible to permit rapid changes in line with unexpected development afloat and ashore.

The notable success of amphibious operations during and after World War II is testimony to the fact that, with proper planning and organization, this dual problem can be solved. In today's environment, it is well known that the modern battlefield will be dominated by highly lethal weapons. This has raised serious questions about the survivability of amphibious

forces. On the other hand, the long-range, high-speed assault potentially gives one the capability to launch assaults from far out to sea, land at times and places of one's choosing, and carry more firepower to accomplish the amphibious assault with greater safety for ships and men. Use of some type of combat model is the only way to explore such issues today. In order to build such a combat model of an amphibious operation, it is necessary to develop and consider detailed and specific information on individual tactical and support elements of the landing force, on the size, numbers, and characteristics of the equipments of these elements, and on the sequence of movement of these elements.

The amphibious operation is a combined operation, the entire spectrum of activities involved in an amphibious operation includes:

- pre-assault bombardment by ships and aircraft
- sea mine clearance
- attack on ships by enemy aircraft and cruise missile
- ship-to-shore movement
- surface assault landing
- helicopter operation
- ground combat between maneuver units
- artillery and naval gunfire support
- tactical aircraft support
- mine warfare (sea and land).

While an amphibious operation is one of the most complex of all military operations, defending against it is even more

complex: it is absolutely impossible for an enemy to defend all coastal areas at all times. The flexibility to conduct helicopter-borne vertical assault and surface-borne assault simultaneously will greatly enhance the complexity of defending against an amphibious assault.

Airborne troops and supplies were valuable during the Second War, and further developments in that direction are under way. But whether or not modern airborne tactics and techniques have supplanted (in a practical sense) seaborne assaults (such as those used from 1942 through 1945 in the Pacific and elsewhere), it should be noted that the military problem of landing forces on shores held by an enemy remains. The emphasis in the future will most likely continue to be on having the ability to project forces from the sea onto a hostile shore and to hold such a beachhead.

B. MODELING APPROACH

All models of military operations must abstract from the real world. Since it is obvious that an engagement between modern military forces is a very complicated process, one has to abstract, aggregate, and interpolate in order to scale a combat process down to manageable size for modeling purposes. A variety of modeling approaches are available. These range from simple Lanchester-type models to highly complicated, computer assisted, high-resolution simulations in which the actions of each individual combatant are traced through a combat scenario second by second. Between these two extremes are

other approaches covering the whole spectrum of land combat, from one-on-one duels to theater-level models covering huge geographical dimensions.

There are basically four different types of combat models: war games, analytical (or mathematical), simulations and some combination of these first three types. According to Bonder [Ref. 2], war games are not a feasible mechanism for analyzing a broad spectrum of system alternatives in a responsive manner to meet a planning cycle requirement. However, they are diagnostic in the sense that they reveal problems that need to be resolved with future systems, and are a viable mechanism for training decision makers. Analytical models seek to describe the combat process mathematically. They simplify the conduct of sensitivity analysis and provide an increased ease in interpreting results, since the dynamics of the combat process are contained in readily examined equations. Analytical models of any degree of complexity usually do not yield convenient analytical solutions but require numerical approximation methods. Simulation is the most widely used technique in military system analysis. Simulation can generally produce very useful data, which are needed for further analysis, and sometimes for planning itself. However, the large amount of detail contained in most Monte Carlo simulations makes it difficult to use as the sole vehicle to single out those systems capabilities, tactics, and environmental conditions which significantly contribute to or delimit the system's effectiveness. Since, as we have seen above, no one type of combat model

is unconditionally preferred to another, it is proposed that a combat model should be selected or designed based on a specific scenario and upon analytical requirements.

In most cases, detailed models are more credible to decision makers. However, for many people such detailed models of large-scale combat operations are far too complicated to be understood, require too much input data, and (in general) are not responsive enough. When one looks at computer storage and run time requirements for even the smallest high resolution model, it is easy to see why a high resolution model of a corps or theater is presently impractical, and is likely to remain so. In order to avoid the complexity of the large-scale model and to better understand land combat there is a growing trend among analysts to combine small unit and large unit models in such a way that the output data of a high-resolution small unit combat model is used as the input data for a low-resolution large unit model. The obvious drawback of this hierarchical-modeling approach is that any errors in the small unit models will be carried through, and possibly multiplied, as the process proceeds from model to model. In the large units the emphasis has been away from simulation and towards detailed Lanchester-based models.

So far the emphasis has been adding more and more detail to the high resolution models so as to pick up as many interactions as possible. No matter how much detail is added to the small-unit simulation, it seems impossible that reality will ever be matched exactly. With this in mind, it is proposed

that a well-constructed Lanchester-based model of small unit engagements could give results that are just as valid as the results of a high-resolution simulation.

III. THE MODEL

A. GENERAL

1. The Scenario

The scenario considers an amphibious-landing team, consisting of reconnaissance, a light infantry unit, and landing-assault vehicles. This team is part of an Amphibious Task Force (ATF), and it disembarks from ships that are on station over the horizon from the selected landing site. The assault vehicles, after transmitting from the amphibious shipping to the designated area for the landing formation, form into conventional landing waves at a distance offshore which is greater than the effective range of the direct-fire weapon systems of the shore-defense force. During the ship-to-shore movement the defender's anti-tank guided missile and improved gunnery system respond to the landing. Naval gun-fire ships provide fire support for the assault team during the ship-to-shore movement and the initial stages of landing.

As the assault vehicles reach the beach, they (together with the assault vehicles and any weapons landed by landing vehicles) launch an attack on the enemy shore defense positions. The defenders occupying those positions fight until their losses exceed a maximum permissible amount. The attacking force, however, continues the assault regardless of losses incurred. Once the shore assault has been completed, the landing force with tactical mobility moves inland to

carry out the tasks, while the enemy prepares to mount a counter attack.

The attacker may engage the advance force of the defender's initial counter attack force on the way to move inland. The advantage will likely go to that force which has gained the initiative (i.e., the landing force) provided it can maintain its momentum.

2. General Description of the Model

The model developed in this thesis is a time sequenced, deterministic, force-on-force computerized model, coded in FORTRAN. The model conducts the battle in uniform time steps of 10 seconds each. Figure 1 shows the general scheme for the sequence of events in the model. The model simulates two main phases in the amphibious operations: (I) the amphibious-assault phase, and (II) the subsequent ground attack. The framework and the logical interrelationships of these two phases will be discussed in the following subsections.

B. THE AMPHIBIOUS ASSAULT PHASE

1. General

In this phase the model considers attrition between the shore-defense force and the landing-assault force during its water-borne movement and subsequent assault to shore. The model aggregates the various actual combat organizations involved in the waterborne phase of the amphibious operation into several homogeneous combat units. Each of these units is characterized by certain relative offensive and defensive

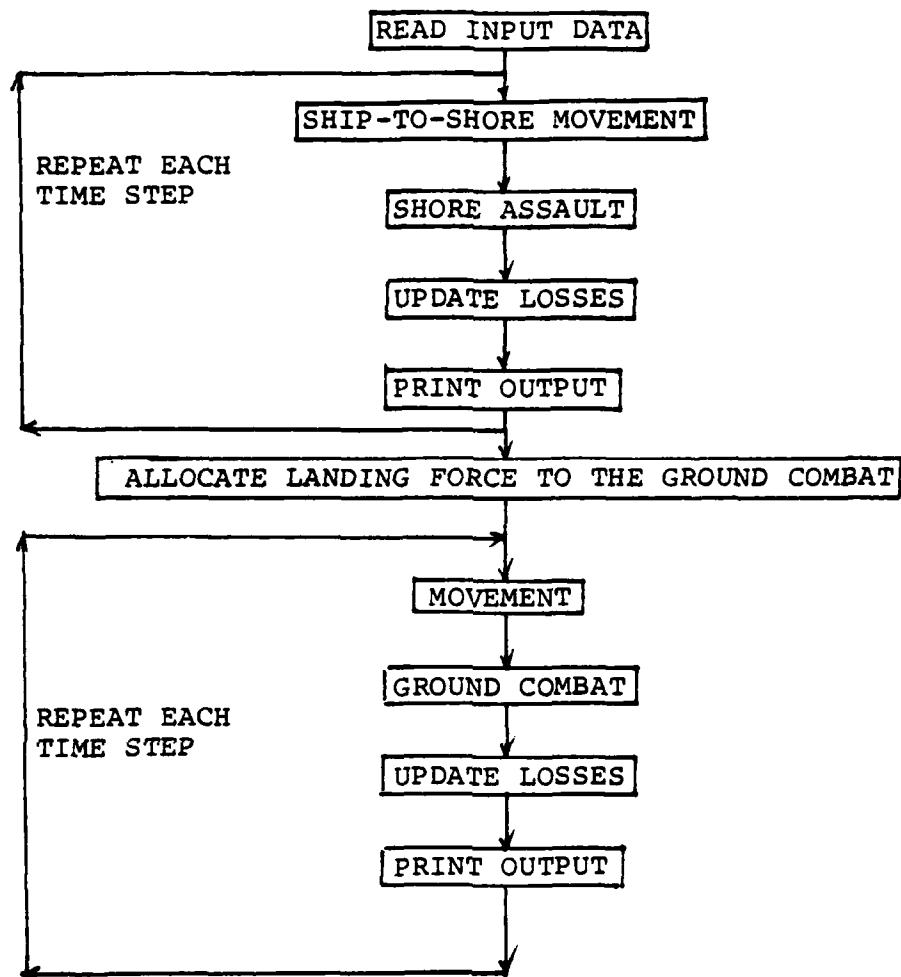


Figure 1. General Scheme for the Amphibious Operation Model

capabilities. The following table illustrates the combat organizations that were explicitly modeled. The combat strength of each unit was represented by the state variables indicated.

<u>combat organization</u>	<u>state variable</u>
Shore Defense--TANK assets	DT
Shore Defense--ATGM assets	DS
Incoming assault waves of LVA representing waves 1 through 5	WV(I), I = 1,2,3,4,5
A cumulative combat force comprised of those Marine ground units which have arrived at the beach and have debarked the LVA	TLF
Fire Support Assets of The Amphibious Task Force	ATFFS

The initial strength in each of the above units is input data to the model.

The schematic of the method of employment for the LVA in the ship-to-shore phase of an amphibious assault is shown in Figure 2. It is assumed that the conventional landing formation composed of waves of landing vehicles will be used as prescribed by current doctrine. The movement of assault vehicles to the beach is simulated using a time step approach. At each time increment the positions of vehicles are updated.

The tactical interrelationships which exist between various combat units are illustrated in Figure 3. Assuming that in such a future amphibious operation the attrition of

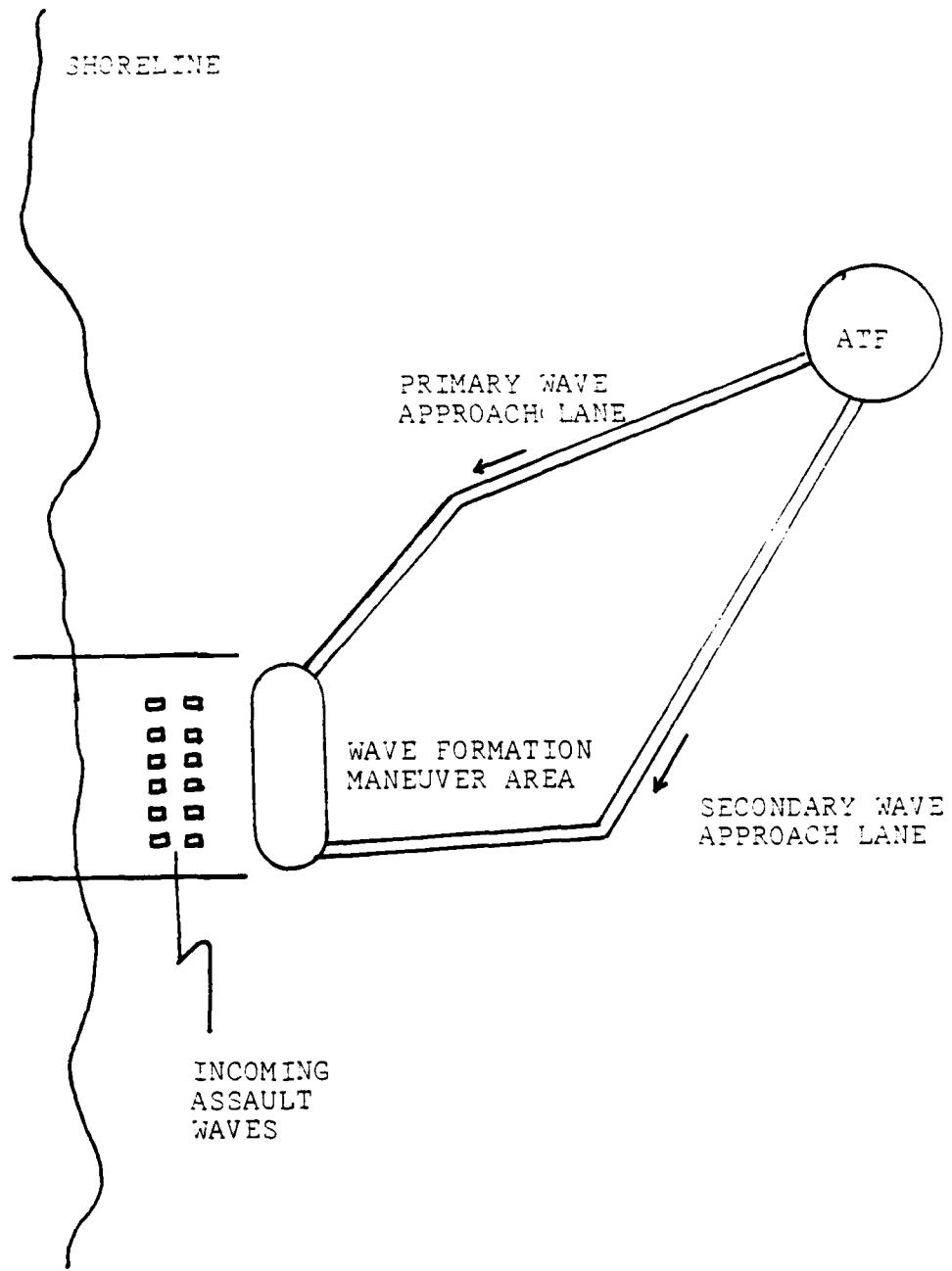


Figure 2. Concept of Ship to Shore Movement

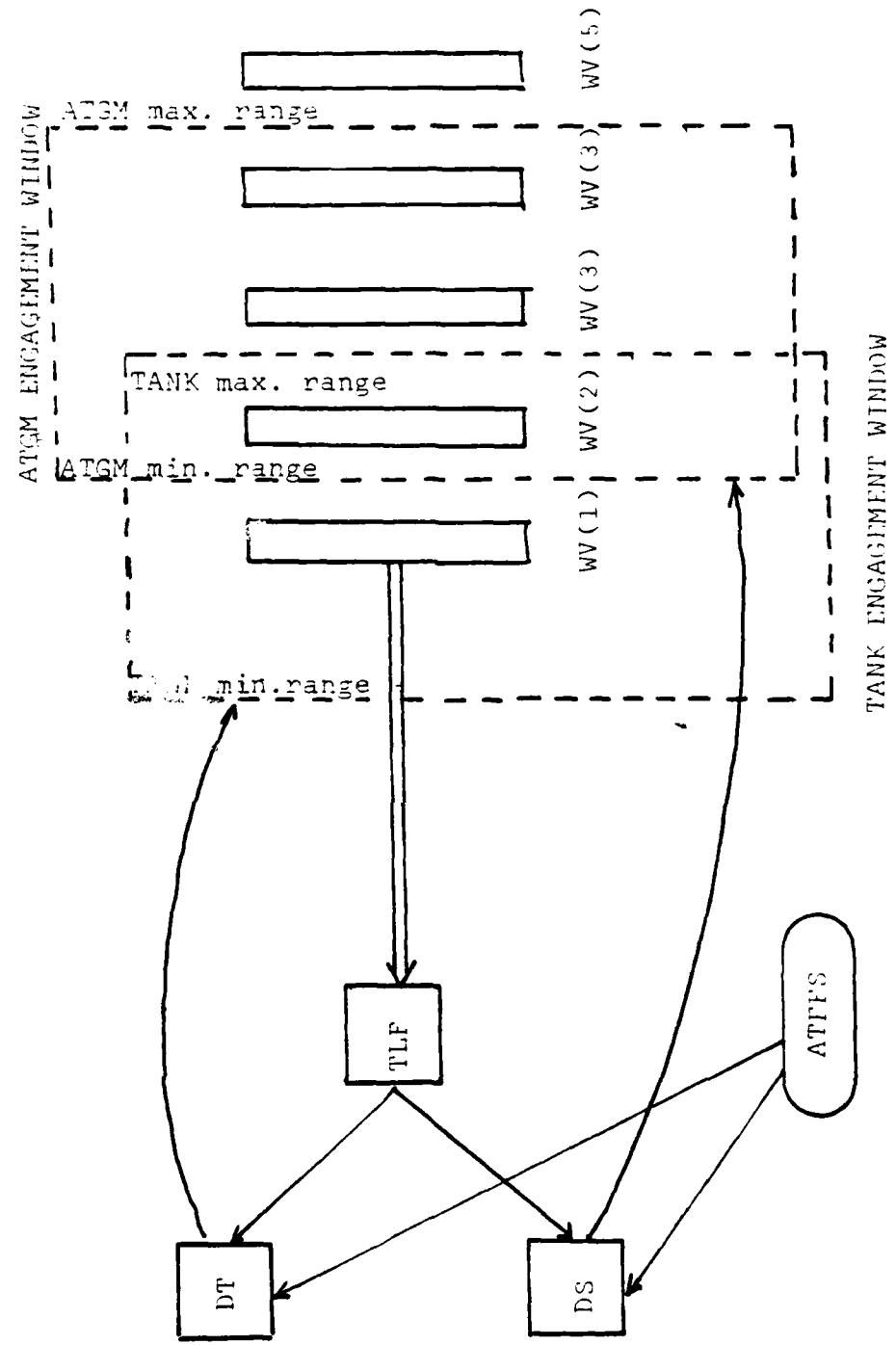


Figure 3. Schematic of Tactical Interrelationship between Combat Units during Amphibious Assault Phase

incoming landing vehicles would be dominated by the effects of shore defense direct-fire weapon systems (specifically, tank and anti-tank guided missile (ATGM) assets), the model essentially omits the effect of the defensive indirect fire capabilities.

2. Attrition Process

The model represents the attrition of all combatant units as a deterministic process. The primary consideration in the ship-to-shore movement of incoming waves of assault vehicle is the attrition effects upon those waves due to the direct fire weapon assets ashore. The attrition of each wave utilizes Lanchester "aimed-fire" equations with variable attrition-rate coefficients.

The classical Lanchester hypothesis for aimed-fire attrition (combat under "modern condition") is that the casualty rate of a unit is proportional to the "size" of the opposing forces. If the unit "A" is being engaged by "D", this may be expressed by the differential equation:

$$\frac{dA}{dt} = - \text{BETA}_{DA} \times D$$

The proportionality constant BETA_{DA} is called the Lanchester attrition-rate coefficient. It is assumed that this functional relationship holds for each (firing unit, target unit) pairing over a small time interval dt . The problem then is to determine numerical values for the Lanchester attrition-rate coefficients. In this model, these coefficients were expressed

as the product of the rate of fire (ROF) and the kill probability per round (P_k). Thus,

$$\text{BETA}_{\text{DA}} = \text{ROF}_{\text{DA}} \times P(k)_{\text{DA}}$$

The rate of fire (ROF) can be expressed as the reciprocal of TBF (Time Between Firings) which can be evaluated by

$$\text{TBF} = \text{AIM-RELOAD TIME} + \frac{\text{TARGET RANGE}}{\text{TARGET SPEED} + \text{PROJECTIVE VELOCITY}}$$

In determining the probability of a vehicle "KILL" per round, it is assumed that a hit by a large caliber projectile would constitute a "KILL" and the two defensive weapon systems addressed would exhibit normal, uncorrelated horizontal and vertical errors. Then the single shot kill probability is given by

$$P(k) = \left[\left(\frac{1}{\sqrt{2\pi}} \right) \frac{(-a-u)/\sigma_x}{\sigma_x} \int_{-\infty}^{a-u/\sigma_x} \exp\left(-\frac{x^2}{2}\right) dx \right] \\ \cdot \left[\left(\frac{1}{\sqrt{2\pi}} \right) \frac{(-b-v)/\sigma_y}{\sigma_y} \int_{-\infty}^{(b-v)/\sigma_y} \exp\left(-\frac{y^2}{2}\right) dy \right]$$

where:

- a = semilength of a target
- b = semiwidth of a target
- u = horizontal aiming error
- v = vertical aiming error

σ_x = round-to-round standard deviation in vertical

σ_y = round-tround standard deviation in horizontal

Model functions RNG, HT and SPD are called upon within the model logic to generate the range, height and speed respectively for each assault wave as time is incremented throughout the course of the amphibious assault phase. This information and typical dispersion data (both mean and standard deviation for the tank and ATGM weapons) are then incorporated into the rate of fire and hit probability calculations.

The Amphibious Task Force's fire support assets contribute significantly to the combat effectiveness of the shore defense units. Since it is assumed that the exact positions of the defensive units DT and DS emplaced on shore are unknown to the Amphibious Task Force and consequently the ATF fires into the general areas thought to contain the defensive units. The following Lanchester-type area-fire equations are applied to compute the attrition of DT and DS.

$$\frac{dDT}{dt} = -(\text{ALPHA}_{DT} \times \text{ATFFS}) \times DT$$

$$\frac{dDS}{dt} = -(\text{ALPHA}_{DS} \times \text{ATFFS}) \times DS$$

The combat effectiveness of the ATF fire support assets is to be considered relatively constant during this segment of combat time. Thus the terms in parentheses on the right hand side of these equations are to be considered an input parameter.

Once a particular defensive unit has initiated its engagement of incoming waves it is considered that their fire "gives away" their exact locations. At this point it is assumed that the ATF fires will engage that defensive unit through the use of aimed-fire and the loss rate will be in accordance with the Lanchester hypothesis for aimed fire. That is,

$$\frac{dDT}{dt} = -\text{BETA}_{DT} \times \text{ATFFS}$$

$$\frac{dDS}{dt} = -\text{BETA}_{DS} \times \text{ATFFS}$$

Again, the parameters on the right-hand sides of both these equations are provided as input.

The casualty rates applied against the DT and DS by the Total Landed Force (TLF) are determined by means of the Lanchester aimed-fire attrition rate coefficients by the equations

$$\frac{dDT}{dt} = -\text{WBETA}_{TLF-DT} \times \text{TLF}_{DT}$$

$$\frac{dDS}{dt} = -\text{WBETA}_{TLF-DS} \times \text{TLF}_{DS}$$

The computation of these WBETA coefficients is not performed within the model utilizing the detailed rate of fire and P(k) arguments described previously but is required as input. Although the defensive losses are considered significant,

a high level of complexity for computing these coefficients has not been incorporated into the model at this time.

Figure 4 describes the schematic of the attrition process of the amphibious assault phase in the model. The attrition during each time step was computed using the Euler integration method to approximate Lanchester's force-on-force attrition differential equations.

3. Fire Allocation

Each weapon category was assigned an engagement window as illustrated in Figure 3. Only those LVA located within these range windows could be fired upon by the shore defenders. A defensive weapon only engages the two closest incoming waves if more than two waves of LVA are at any time located within the weapon's engagement window. If only one wave of LVA is present in a weapon's engagement window, defensive fires of that particular weapon type will be distributed uniformly against the surviving LVA in that wave.

If two waves of LVA are both contained within the engagement window, defensive fires of that particular weapon type will be distributed according to a tactical allocation submodel. A weighting factor (DEFWT) is utilized in establishing the proportion of the total weapon strength to be allocated against the surviving LVAs in each of the two waves. As an example, if DEFWT(1) = 2 and DEFWT(2) = 1, then each surviving LVA in the closer of the two incoming waves would be allocated twice as much fire as surviving LVA in the seaward

DIRECT FIRE DT/DS AGAINST FOR EACH INCOMING WAVE I

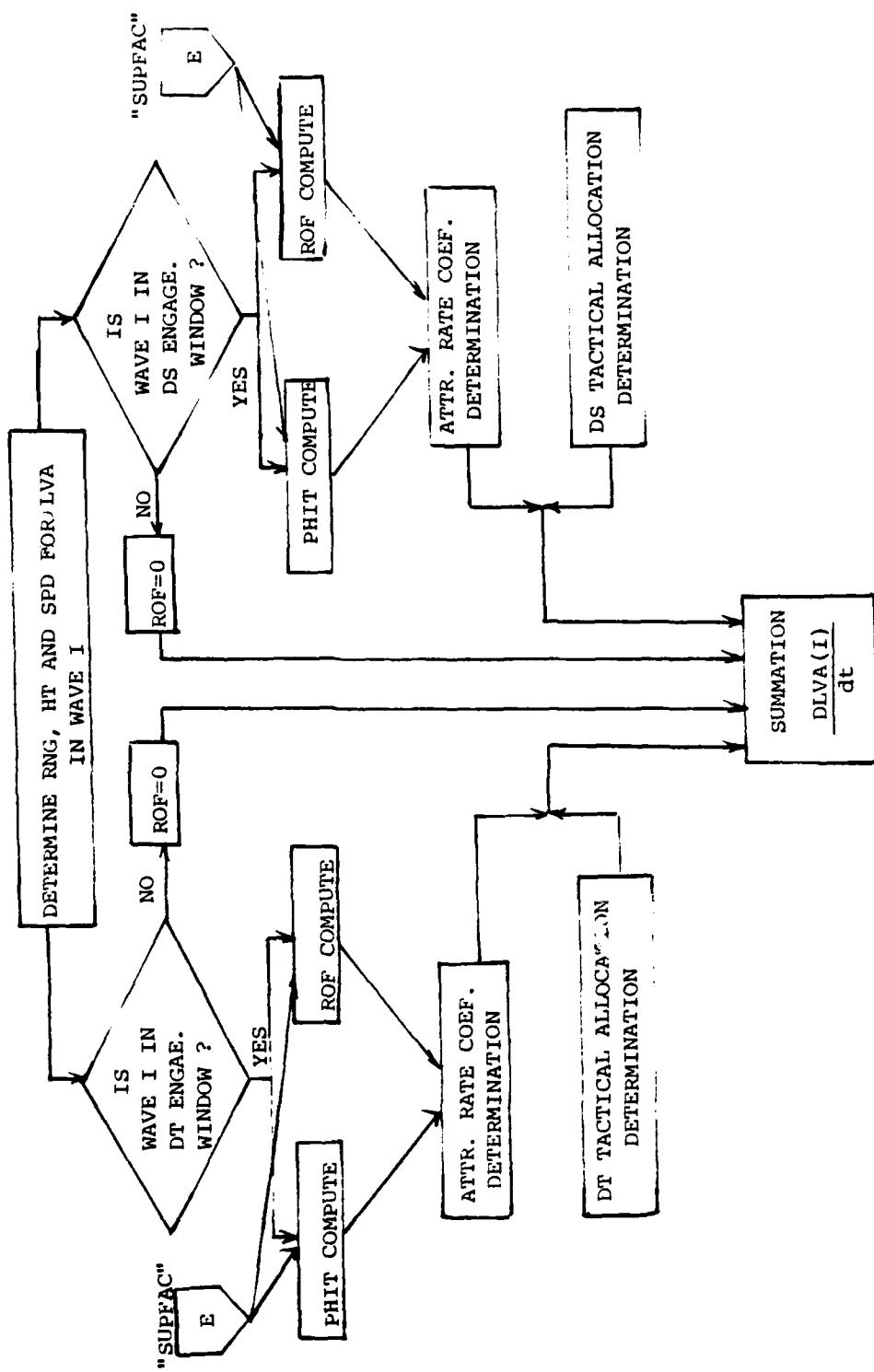


Figure 4. Schematic of The Attrition Process for The Assault Phase

ATTRITION FOR THE SHORE DEFENSE FORCE

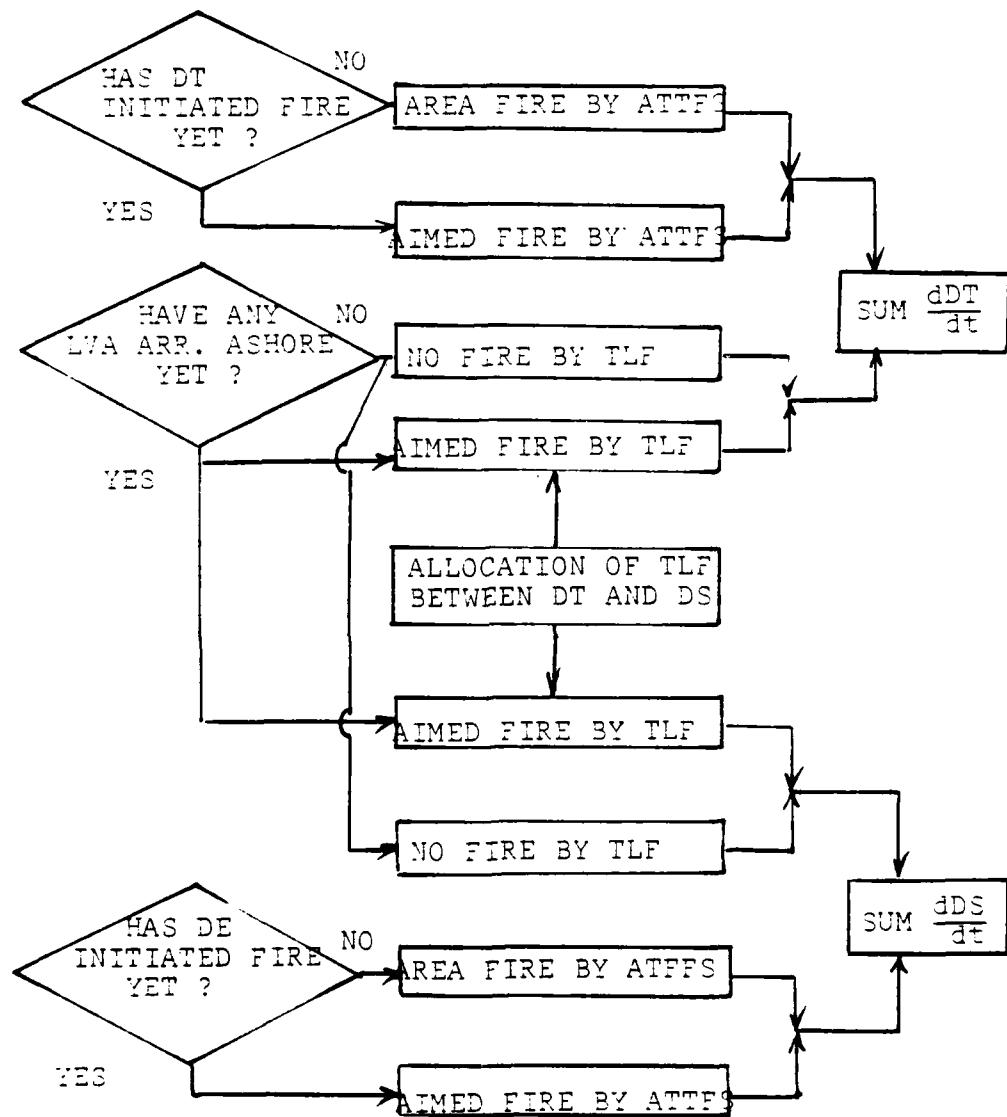


Figure 4.(cont)

wave. For the purpose of these examples, if waves 3 and 4 were both located within the tank engagement window, then the proportion of DT's fire allocated to surviving LVA in wave 3 would be

$$\frac{\text{DEFWT}(1) \times \text{WV}(3)}{\text{DEFWT}(1) \times \text{WV}(3) + \text{DEFWT}(2) \times \text{WV}(4)} \times \text{DT}$$

where WV(3) is the state variable for the current number of survivors in wave 3.

As each assault wave arrives at the beach, the total surviving strength of that wave is transferred to the variable TLF (Total Landed Force). TLF represents a ground combat force equal to that transported by the number of LVA survivors having arrived ashore. Once established, TLF engages the two shore defensive units allocating its fires between the two defensive weapon categories in the same proportion as the number of surviving tanks and ATGM's, that is

$$\text{TLF}_{\text{DS}} = \frac{\text{DS}}{\text{DT} + \text{DS}} \times \text{TLF}$$

$$\text{TLF}_{\text{DT}} = \frac{\text{DT}}{\text{DT} + \text{DS}} \times \text{TLF}$$

4. Suppression

The suppression effects of incoming fire upon each of the defensive units was considered a significant factor with respect to its effect on the survivability of the incoming assault waves of LVA. Generally, the effect of suppression

fire will hinder an individual from observing and firing at the enemy.

It was assumed that suppression would degrade unit effectiveness by increasing the aim-reload time (ARTM) and round-to-round error standard deviation for each weapon system. Hypothesizing that attrition rate is the dominating variable, and therefore, a good indicator of the suppression level, ARTM and such round-to-round errors were assumed to be functions of the force's attrition rate. This is an area, however, requiring further study. Analytically,

$$\text{ARTM}_{\text{sup}} = \text{ARTM}_{\text{nonsup}} (1 + \text{GAMMA} \times \text{DA})$$

$$\text{ERROR}_{\text{sup}} = \text{ERROR}_{\text{nonsup}} (1 + \text{DELTA} \times \text{DA})$$

where:

DA = attrition rate for defensive unit due to the effect of AFTTS and TLF

GAMMA = parameter representing relationship between DA and ARTM

DELTA = parameter representing relationship between DA and error standard deviation

This increase of ARTM and round-to-round error (expressed as a standard deviation) decreases the kill probability (P_k) for both defensive weapon categories. Parameter estimation would appear to be the largest problem. But, since determining these parameters in the model is beyond the scope of this thesis, these parameters GAMMA, DELTA are provided as input.

5. The Termination of the Assault Phase

It is assumed that if during the course of the amphibious operation the shore defense forces suffer a cumulative loss in excess of 70% of their initial force strength, the remaining shore defense will try to withdraw, resulting in termination of the engagement.

C. THE INITIATION OF GROUND ATTACK

In the amphibious operation, the landing-force must seize critically-important inland objectives as rapidly as possible before the defenders start to react to the landing. The decision for the initiation of ground attack should be based upon the enemy threat and desired landing-force build-up ashore, among other factors. To model this decision rule, it is assumed that once the landing has begun, the landing-force commander will base his decision about initiation of ground attack primarily on the strength of the landing-force ashore and the shore defender's strength. The criteria for the decision should meet these two conditions:

- (1) The survived landing-force strength has to be greater than the minimum force required to carry out the ground attack.
- (2) The defender's strength must fall below the minimum required to continue coordinated shore defense before breakoff and retreating.

These conditions are then checked after each time step. If all waves landed without reaching the above second conditions, it

is assumed that the next wave group will engage any leftover defenders. Thus, the decision to implement the ground attack is based on the size of the total landed force.

D. THE GROUND ATTACK PHASE

The attacking force which is composed of three subunits of three LVAs armed with TOW antitank missile system attacks along predetermined routes. The defending force is comprised of three subunits of three tanks in a static defense.

The battle takes place on parameterized terrain which will be discussed later. The ground-attack process contains five main subprocesses: (1) movement, (2) detection, (3) fire-allocation, (4) attrition and (5) battle termination. The general flow of the ground attack phase is shown in Figure 5.

1. Movement Process

Every attack unit is advanced to the next interval along a predetermined route unless this unit is destroyed already or is in firing status. To use his own determined routes, the user is required to input the original location of each attacking subunit and from one to ten nodes he wishes each attacking subunit to move through. This information, along with vehicle speed, is used to calculate route intervals that move the attacking unit through each of the designated nodes. The straight line ground distance between the first two adjacent nodes, DIST, is calculated as

$$DIST = \sqrt{x^2 + y^2}$$

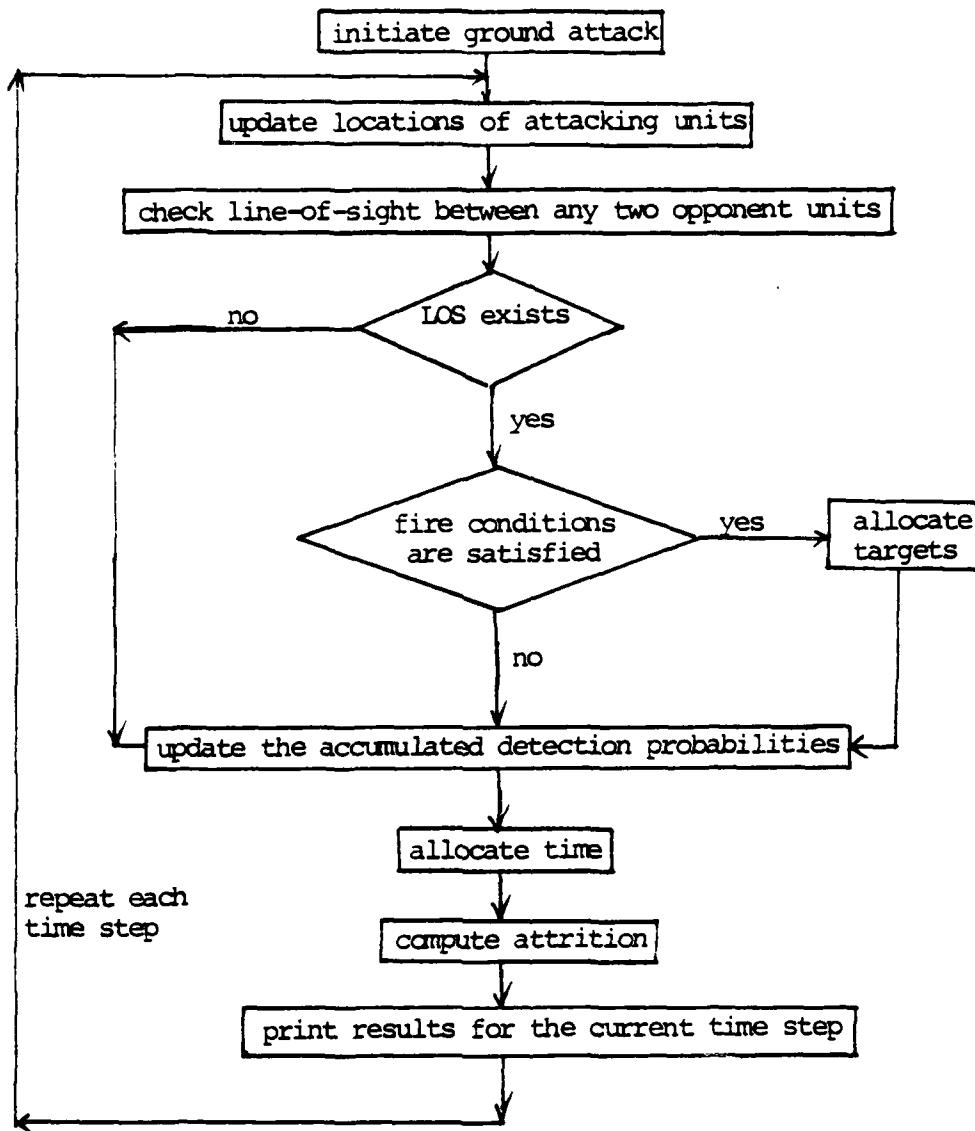


Figure 5. Flow Chart for the Ground Attack Phase

where:

X = distance between two nodes in straight west-east direction

Y = distance between two nodes in straight south to north direction

The angle between the desired direction of movement and straight west to east movement, α , is then calculated.

Utilizing these quantities, the distance desired to move during each time step (DST) and the distance to be moved in the X and Y direction (XLN, YLN) is computed. These distances (XLN, YLN) are then added to the coordinates of the previous interval endpoint to determine the coordinates of the next interval endpoint. This process is repeated between the next two nodes until the unit has traversed the entire route.

2. Detection and Fire Allocation

The detection phenomena are modeled in two ways:

(I) non-firing detection, and (II) firing-detection. A non-firing detection can occur as a result of an observer's random search within his designated sector of responsibility. The probability (P_k) that an observer A looking at the direction which enables him to detect a target is computed by integrating the Limicon Function over limits are $\pm 15^\circ$ from the primary direction the observer is looking. The Limicon Function, $f(\theta)$, is the following probability density function:

$$f(\theta) = A + B \times \cos(\theta) \quad -\pi \leq \theta \leq \pi$$

where:

$$D = \text{assigned sector width}/2$$

$$A = -B \times \cos(D)$$

$$B = \frac{1}{2}(\sin(D) - D \times \cos(D))$$

θ = primary direction observer is looking

Assuming 30° field of view for any observer A target B might be seen only if the observer A is looking at the direction such that $\text{ANGRT} \leq \theta \leq \text{ANGLFT}$ where:

ANGLE = the absolute value of the angle between the primary direction (IPRDIR) and the observer-target direction (OTANG)

$$\text{ANGLFT} = \text{angle} + 15^\circ \text{ if } \text{angle} + 15 \leq D$$

$$D \quad \text{if } \text{angle} + 15 > D$$

$$\text{ANGRT} = \text{angle} - 15^\circ$$

Thus

$$P_k = \text{pr}(\text{ANGRT} \leq \alpha \leq \text{ANGLFT})$$

$$= \int_{\text{ANGRT}}^{\text{ANGLFT}} f(\alpha) d\alpha$$

Given that observer A is looking at the direction, the conditional detection rate (λ_{AB}) is determined by the regression curve [Ref. 11]. The probability that unit j is detected by unit i at time $t + \Delta t$ [$P_{ij}(t + \Delta t)$] is computed according to:

$$P_{ij}(t + \Delta t) = 1 - e^{- \int_t^{t + \Delta t} \lambda(t) dt}$$

$P_{ij}(t)$ can be interpreted as the average fraction of unit i that detects unit j.

The second method of detection played in the model is a so-called firing detection. This phenomena occurs when the following happens: if a firing location is within $\pm 15^\circ$ of an observer's primary direction of observation when he is firing, he is assumed to be detected and is added to the observer's target list. In summary, the following conditions are necessary for unit j to be a target of unit i:

- (a) Line-of-sight must exist between unit i and unit j.
- (b) The range between the two units should be between maximum range and minimum range of the firer's weapon system.
- (c) $P_{ij}(t - \Delta t) > 0$.

The fire-allocation routine determines what fraction of each unit is allocated to fire each target in target list since it is assumed that each fire unit is not restricted to fire at one target. This fraction is determined as a function of the predetermined fire policy and $P_{ij}(t)$. The fire policy is as follows:

# of target	% of unit i allocated to each target		
	1 st priority	2 nd priority	3 rd priority
1	100%		
2	80%	20%	
3	80%	15%	5%

The priority of a target is taken to be a function of range only. The fire allocation rule which is used in the model is documented in detail in Smoller's thesis [Ref. 9].

3. Attrition

The attrition process in the ground attack phase utilizes Lanchester "aimed-fire" equation used with variable attrition coefficients. The calculation of the attrition coefficients is accomplished through the use of one of two optional methods. The first option uses the following Bonder-Farrell formula to compute the reciprocal of the expected time to kill. The coefficients, A_{ij} , the rate at which one firer of unit i kills unit j targets are computed according to:

$$A_{ij} = 1/E(T_{ij})$$

where $E(T_{ij})$ is the expected time for one firer of unit i to kill one target of unit j. The $E(T_{ij})$ is computed using:

$$\begin{aligned} E(T_{ij}) &= t_a + t_l - t_h + (t_h + t_f)/P(K/H) \\ &\quad + (t_m + t_f)/P(h/m) \times ((1-P(h/h))/P(K/H)) \\ &\quad + P(h/h) - p \end{aligned}$$

where:

t_a = time to acquire a target

t_l = time to fire first round following acquisition

t_h = time to fire following a hit

t_m = time to fire following a miss

t_f = time of flight of a round

P = probability of a first round hit

$P(h/h)$ = probability of a hit following a hit

$P(h/m)$ = probability of a hit following a miss

$P(k/h)$ = probability of a kill given a hit

This formula holds for the conditions that the hit probability of any round depends only on the result of the previous round and no accumulated damage is considered. It is assumed that $P(K/H) = 1.0$ and $P(h/m) = p(h/h) = P$, thus reducing the equation to:

$$E(T_{ij}) = t_a + t_1 + t_f + (t_m + t_f)(1-P)/P$$

The second method, called the stochastic method, interprets the attrition rate coefficient, A_{ij}^0 , as a measure of the fighting ability of a unit which has a random phenomena affected by many different factors. It is assumed that the random fighting ability should be distributed between .3 and .8 with the majority of the unit being rated between .5 and .6. A "fitted" distribution to these assumed fighting levels which is devised by Mills is:

$$A_{ij}^0 = -2U^2 + 2U + .3 ; \quad U \text{ is a random Uniform } (0,1) \text{ number}$$

The A_{ij}^0 's are a realization of the random variable denoting a unit's initial fighting capability prior to the battle. Then,

during each time step, a new attrition rate coefficient for each unit is computed using the equation:

$$A_{ij}^0 (1 - r/r_e) ; \text{ for } 0 \leq r \leq r_e$$
$$A_{ij} = \begin{cases} 0 & \text{for } r_e \leq r \end{cases}$$

where:

r_e = maximum effective range of a firer's weapon

r = current range between firer and target

Utilizing one of the above formulas to calculate A_{ij} 's, the attrition during each time step was computed using the Euler-Cauchy differencing equations to approximate Lanchester's force-on-force attrition differential equations.

4. Termination of Ground Attack

The ground attack is terminated when either:

- (1) One of the two opponent forces is annihilated;
- (2) A distance between each attacking subunit and each defensive subunit which is still engaging becomes "too close";
- (3) Any attacking subunit passes by the flanks of the forward most defensive subunit still in the battle.

The criteria for being "too close" is user input. This allows for flexibility of breakpoint distance for various weapon systems on the battlefield.

E. THE PARAMETRIC TERRAIN

The terrain affects a great deal on detection, mobility, tactics, and intervisibility between weapon systems in ground combat environments. In the model, the battle is simulated on 3 x 4 Km piece of terrain represented as a part of the coastal area east of the Korean Peninsula. It is important to have a terrain representation to emulate actual terrain areas. The model uses the parametric terrain representation method which was proposed by Chris Needle [Ref. 8]. The idea of the parameterized terrain is that the elevation of any hill mass can be represented by a bivariate normal density function. Mathematically, if $f_I(X, Y)$ is a function giving the elevation of the I's hill masses at any X, Y map coordinates on the battlefield, the overall terrain elevation at X, Y is obtained as the positive maximum over all the hill masses,

$$Z = f(X, Y) = \max_{I=1, \dots, NHILLS} f_I(X, Y)$$

where NHILLS is the total number of hill masses on the battlefield. Then, elevation data is used to compute the existence of line of sight between opposing forces which is a key element in detection process. The model uses the line-of-sight routine which was written by Prof. James K. Hartmann [Ref. 5].

In order to represent a piece of real terrain with parametric terrain, it is necessary to fit hill mass functions $f_I(X, Y)$ to a contour map of the terrain to be modeled. The fitting

process can be done by comparing a computer generated contour map by varying the bivariate normal parameters to the original terrain map. The computer generated terrain map of the battle area is inclosed as Figure 6. Appendix D presents the program listing for plotting a contour map from hill mass functions. This program can be used for the user to fit a specific real terrain which he has in mind into the parameterized terrain.

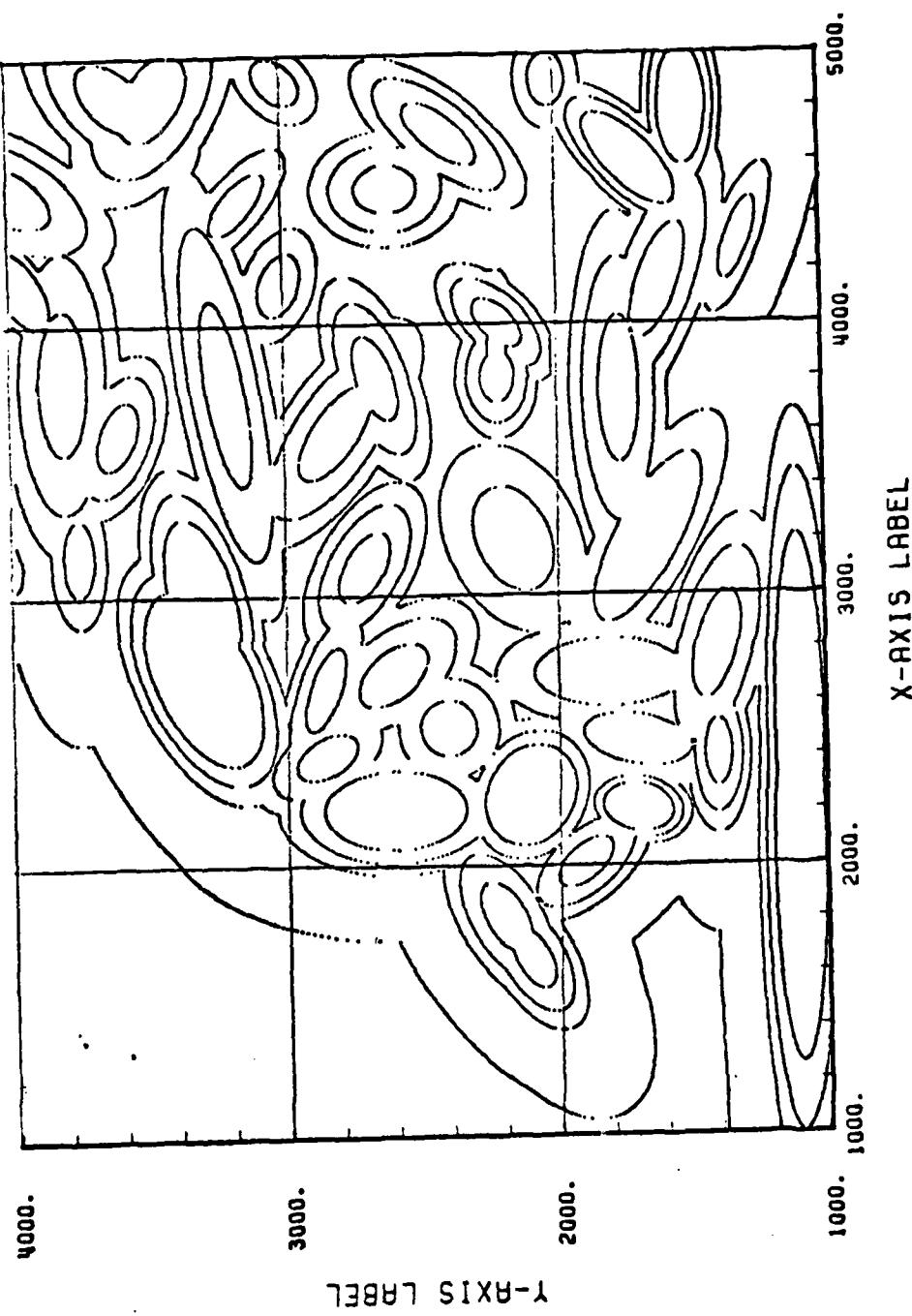


Figure 6. Model Terrain Map

IV. FINAL REMARKS

In order to illustrate basic modeling points for understanding and developing complex-operational amphibious-warfare models, a simplified model (specially tailored to a small-unit-amphibious-operation scenario) has been developed. Although several user options and varieties of modeling techniques have been incorporated into the model, the model should not be viewed as the final product.

There are several areas of model enhancement and enrichment that should be considered in the future. Only the aggregated amphibious task force fire support is played explicitly in the amphibious assault phase. The effect of artillery, naval gunfire and close air support during the various phases of amphibious operations should be added to the model. Ammunition consumption and resupply are considered vital to the success of any military operation, and such aspects should be also added to the model. Enemy forces should be played in greater detail. The movement of reacting enemy force and their dynamic-defensive-position selection are being considered for future model inclusion. A module which considers enemy reaction time, the terrain, and the tactical situation, and which dynamically determines which side is going to take the defensive role, as well as its defensive position, has been proposed to enhance the existing model. Inclusion of these features would create a more complicated model, adding realism but detracting from the current simple and transparent form.

The model currently simulates the ground combat on a 3 x 4 Km piece of coastal terrain representing an area of Ham-Hung, Korea. In order to simulate combat on a user's specific terrain, he needs to fit a parameterized terrain model to the actual terrain of interest. Doing so using the terrain fitting method described in the preceding chapter is an extremely tedious and time consuming process. The development of a more efficient terrain fitting technique will greatly enhance the model flexibility, and increase its utility in responding to interrogations from the real world.

The interested reader may obtain the model program deck and the sample input data deck from Prof. James G. Taylor, Naval Postgraduate School. Since the data used for the model run is hypothetical and greatly simplified, the reader is cautioned not to draw any analytical conclusions from the output.

APPENDIX A

SAMPLE EXPECTED OUTPUT

I. Amphibious Assault Summary

AMPHIBIOUS ASSAULT INFORMATION

INITIAL FORCE STRENGTH

WAVE	1	2	3	4	5
LVA	10.0	11.0	11.0	10.0	3.0

DT = 3.0 DS = 1.0

LVA ENGR SPECS

SPDMAX	SPDMIN	HTMAX	HTMIN	WID
10.30	3.50	1.70	0.60	3.53

DEFENSIVE TACTICAL PARAMETERS

	RANGE	AIM-RELOAD	PROJECTILE
	MAX	MIN	VELOCITY
TANK	1500.0	15.00	350.00
ATGM	2000.0	200.0	350.00

DEFENSIVE TACTICAL ALLOCATION WEIGHTS:

WAVE 1 = 2.00 WAVE 2 = 1.00

DEFENSIVE FORCE ATTRITION COEFFICIENTS

	ALPHA*A	BETA*A
DT	0.00006	0.00070
DS	0.00008	0.00090

WBETA(1) = 0.00050 WBETA(2) = 0.00070

BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEP FORCE)

DEFENSIVE FORCE LEVEL FOR GROUND ATK 0.32

DISPERSION DATA

RANGE	TSIGV	RANGE	TSIGH	RANGE	TMEANH
25.0	0.0	25.0	0.0	25.0	0.0
500.0	2.0	500.0	2.0	500.0	1.0
1000.0	5.0	1000.0	5.0	1000.0	5.0
2000.0	20.0	2000.0	20.0	2000.0	10.0
5000.0	25.0	5000.0	25.0	5000.0	15.0
10000.0	25.0	10000.0	25.0	10000.0	15.0

RANGE	SSIGV	RANGE	SSIGH
25.0	0.0	25.0	0.0
250.0	5.0	250.0	5.0
500.0	7.5	500.0	7.5
1000.0	14.0	1000.0	14.0
2500.0	15.5	2500.0	15.5
5000.0	17.0	5000.0	17.0
10000.0	20.0	10000.0	20.0

II. Assault Phase Time Step Summary

TIME = 815.0 SECONDS

WAVE	FORCE LEVEL	STATUS	LOST-PCT	TSURV
1	0.7322	1	0.927	
2	1.7451	1	0.841	
3	4.5060	1	0.590	
4	9.8051	3	0.019	
5	3.0000	2	0.0	
TANK	0.0		1.000	19.79
ATGM	0.0		1.000	0.0
FINAL LVA SURVIVORS ASHORE = 19.788				
GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT				

GROUND ATK TIME = 825.0

III. Initial Ground Combat Summary

INITIAL GROUND COMBAT INFORMATION			
UNIT	X	Y	FORCE LEVEL
1	2000.0	1900.0	3.0
2	1900.0	2400.0	3.0
3	1500.0	2100.0	3.0
4	3800.0	2700.0	3.0
5	3800.0	2300.0	3.0
6	3600.0	1700.0	3.0

ATTRITION IS DETERMINISTIC

ROUTES DETERMINED BY USER

ATTACK VEHICLE SPEED IS 12.0

BREAKPOINT DISTANCE IS 500.0

DEFENDER WILL MOVE TO ALTERNATE POSITIONS
ALTERNATE POSITIONS ARE:

UNIT	X	Y
4	4500.0	3800.0
5	4500.0	2700.0
6	4600.0	1800.0

ATK KILL PROBABILITIES				
RANGE	P	PHH	PHM	PKH
500	0.85	0.85	0.75	0.70
1000	0.80	0.80	0.75	0.70
1500	0.75	0.75	0.70	0.65
2000	0.60	0.65	0.60	0.55
2500	0.45	0.50	0.50	0.35
3000	0.20	0.20	0.20	0.20

DEF. KILL PROBABILITIES				
RANGE	P	PHH	PHM	PKH
500	0.60	0.70	0.65	0.85
1000	0.85	0.90	0.85	0.90
1500	0.80	0.85	0.85	0.80
2000	0.75	0.80	0.75	0.70
2500	0.60	0.70	0.65	0.65
3000	0.40	0.45	0.40	0.50

IV. Ground Combat Time Step Summary

TIME = 1395 SECONDS

UNIT	X	Y	FORCE LEVEL	STATUS	LOST-PCT	TARGETS
1	2420.8	1984.2	0.0	2	1.000	
2	3664.1	2253.0	0.0	2	1.000	
3	4397.4	1742.2	2.9	0	0.038	
4	4500.0	3800.0	0.0	2	1.000	
5	4500.0	2700.0	2.8	0	0.055	
6	4600.0	1800.0	0.0	2	1.000	

* DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE.

APPENDIX B

LISTING OF SAMPLE INPUTS

I. Amphibious Assault Input

1	1					
10.30	3.5	1.7	0.6	3.533		
10.						
1500.	2000.	200.				
15.	30.	350.	350.			
25.	500.	1000.	2000.	5000.	10000.	0.
2.	5.	20.	25.	25.		
25.	500.	1000.	2000.	5000.	10000.	0.
2.	5.	20.	25.	25.		
25.	500.	1000.	2000.	5000.	10000.	0.
1.	5.	10.	15.	15.		
25.	250.	500.	1000.	2500.	5000.	10000.
0.	5.	7.5	14.	15.5	17.	20.
25.	250.	500.	1000.	2500.	5000.	10000.
0.	5.	7.5	14.	15.5	17.	20.
2.	1.					
10.	11.	11.	10.	3.		
3.	1.					
0.00006	0.00008					
0.0007	0.0009					
0.0005	0.0007					
.32						
50.	100.					

II. Terrain Data

46						
0.						
2000.	1100.	170.	0.1	999.9	8.0	
1800.	2200.	150.	30.	350.	2.0	
2000.	1900.	150.	130.	300.	2.	
2400.	1400.	150.	0.1	300.	2.5	
2450.	1700.	130.	80.	500.	2.2	
2700.	1800.	138.	90.	500.	2.2	
3200.	1650.	140.	150.	600.	3.	
4300.	1300.	130.	160.	400.	3.5	
3750.	1750.	150.	0.1	660.	3.6	
4150.	1600.	150.	160.	550.	3.	
3200.	2150.	130.	25.	500.	1.5	
4600.	1700.	170.	45.	300.	2.5	
4800.	1500.	170.	0.1	300.	2.5	
2200.	2600.	170.	90.	350.	1.8	
2400.	2850.	150.	120.	300.	1.8	
3100.	2700.	150.	150.	350.	2.	

2500.	2400.	150.	0.1	250.	1.0
2650.	2850.	150.	160.	400.	3.0
2700.	2600.	150.	130.	370.	1.8
3800.	2200.	150.	0.1	230.	1.5
4500.	2600.	150.	90.	280.	1.3
3600.	2800.	150.	145.	500.	2.5
2700.	3300.	190.	25.	350.	2.0
3000.	3300.	170.	15.	400.	2.5
3150.	3750.	130.	0.1	350.	2.5
3750.	3200.	150.	10.	850.	5.0
3800.	3800.	150.	0.1	650.	3.
3600.	3600.	150.	160.	320.	3.0
4150.	3950.	170.	30.	220.	2.2
1650.	2100.	150.	30.	300.	2.0
2250.	2100.	180.	150.	220.	1.2
4000.	2200.	150.	45.	280.	2.
3900.	2200.	150.	0.1	300.	3.5
0	0	0	0	1	7
0	33	39	53	62	0
0	0	0	0	0	6
0	6	14	9	12	0
101				3	6
1	2	3	30	4	43
6	32	33	7	11	31
8	9	10	11	33	43
8	42	2	14	30	10
16	17	18	19	20	23
2	31	11	16	20	22
46	20	21	22	12	34
42	45	46	14	23	35
26	14	25	26	27	36
35	44	26	27	29	24
40				35	37
				36	38
				37	39

III. Ground Combat Input

```

1 28943
03 03
0000.0 2500.0 0500. 4000.0
3.0 3.0 3.0
1 2
2000.0 1900.0
1900.0 2400.0
1500.0 2100.0
01
5000.0 2500.0
01
4900.0 2150.0
02
2200.0 1700.0
4800.0 1750.0
3800.0 2700.0 3.0 190 120

```

3800.0 2300.0 3.0 190 120
3600.0 1700.0 3.0 180 120
0 0500.0 4
4500.0 3800.0
4500.0 2700.0
4600.0 1800.0
0.85 0.85 0.75 0.70
0.80 0.75 0.70 0.65
0.75 0.75 0.70 0.65
0.60 0.65 0.60 0.55
0.45 0.50 0.50 0.35
0.20 0.20 0.20 0.20
0.60 0.70 0.65 0.85
0.85 0.90 0.84 0.90
0.80 0.85 0.85 0.80
0.75 0.80 0.75 0.70
0.60 0.70 0.65 0.65
0.40 0.45 0.40 0.50

APPENDIX C

DEFINITION OF VARIABLES IN COMPUTER PROGRAM

1. The Amphibious Assault Phase

CDSURV(I) = Current strength of defensive force I

I = 1 TANK

I = 2 ATGM

CSURV(I) = Current strength of assault wave I

DA(I) = Attrition rate for def. unit I due to the effects of ATFFS/TLF

DS1 = That portion of the DS unit assigned to engaging the closer of two multiple waves in the ATGM engagement window

DS2 = That portion of the Ds unit assigned to engaging the farther of two multiple waves in the ATGM engagement window

DT1 = That portion of the Dt unit assigned to engaging the closer of two multiple waves in the TANK engagement window

DT2 = That portion of the DT unit assigned to engaging the farther of two multiple waves in the TANK engagement window

DT1PH = Hit probability of rounds fired by DT1 against wave TENG(1)

DT1ROF = Rate of fire utilized by DT1 against wave TENG(1)

DINIT = Initial strength of def. force I

IL(I) = When equal to 1 indicates the wave landed shore

IWPN = Weapon code: TANK = 1, ATGM = 2

IWSTAT(I) = Current status of wave I

0 - not engaging

1 - landed

2 - under fire by ATGM

3 - under fire by TANK

4 - under fire both ATGM and TANK

GALF = Denote whether the LF build-up is sufficient
 for the ground attack
 0 - not sufficient
 1 - sufficient

GATK = Denote whether the LF initiated the ground attack
 0 - not started yet
 1 - started already

GATM = Time when the ground attack started

RD = Distance offshore at which waves initiate
 transition

RKSURV(I) = Concatenation of CSURV and CDSURV

SA(I) = Attrition rate for wave I due to ATGM

SENG(I) = The wave number of the closer of two waves in
 the ATGM engagement window

SRNG(I) = Firing range to wave SENG(I)

SSIGH = The std dev error in the horizontal for ATGM

SSIGV = The std dev error in the vertical for ATGM

SWTS(I) = The proportion of the total DS strength to be
 allowed to engaging SENG(I)

TA(I) = Attrition rate for wave I due to TANK

TBW = The interarrival time between waves arriving at
 the beach

TMEANH = The bias error in the horizontal for TANK

TMEANV = The bias error in the vertical for TANK

TENG(I) = The wave number of the closer of two waves in
 the tank engagement window

TRNG(I) = the firing range to wave TENG(I)

TSIGH = The std dev error in the horizontal for TANK

TSIGV = The std dev error in the vertical for TANK

TSURV = Total number of surviving LVA at the current time

TWTS(I) = The proportion of the total DT strength to be
 allowed to engaging TENG(I)

WVINT(I) = Initial strength of wave I

2. The Ground Attack Phase

ALPHA(I) = Initial attrition-rate coefficient for stochastic attrition module

APOA(I,J) = The average proportion of the j^{th} attacker of unit i allocated to fire on unit i

AVSP = Average speed of moving attacking units

BREAK = Breakpoint distance between attacking units and defenders

DISMAX = Maximum distance allowed between attacking units before the leading unit is delayed

DIST = The straight-line distance between two movement nodes inputted by the user

DST = The distance in meters to be moved each time step by attacking units

FL(I) = Force level of unit i

FO(I) = Force level of unit i

FO(I) = Initial force level of unit i

IALT = Denotes whether the user desires alternate defensive positions or not
0 - yes
1 - no

IC = Counts number of time units a defender has been moving

IDIR(I,J) = Direction of j^{th} interval in i^{th} route

II(I) = Interval index for unit i

IMOVE = Number of time units a defender is allowed for moving to an alternate position

IPRDIR(I) = Primary direction of movement for unit i

IRTE = Denotes whether user wants to input routes or not
0 - program determined routes
1 - user determined routes

IS = Random number seed used for stochastic attrition

ISECWD(I) = Width of search sector for unit i

ISPD = Input variable to denote user's desired speed
 for attackers movement
 1 - 9 mph
 2 - 12 mph
 3 - 15 mph
 4 - 18 mph

ITEM = Input variable denoting number of time steps
 allowed for defender's move

ITIME = Current time, in seconds, of battle

ITRIT = Input variable denoting whether attrition
 will be stochastic or deterministic
 0 - stochastic
 1 - deterministic

IUSTAT(I) = Current status of unit i
 0 - unit alive, not firing
 1 - unit alive and firing
 2 - unit killed
 3 - unit moving

LOA(I,J) = The number of the j^{th} attacker of unit i

LOST(I,J) = Denotes whether line-of-sight exists between
 unit i and j or not

LOT(I,J) = The number of the j^{th} target of unit i

MVTDIR(I) = Movement direction of unit i

N(I) = Number of nodes inputted by user for route i

NA(I) = Number of attackers of unit i

NBU = Number of defense units

NF(I) = Number of time units i is allowed to fire at
 the same location

NLOSC(I,J) = Number of continuous time steps that line-of-sight
 does not exist between unit i and unit j

NOI(I) = Number of intervals in the i^{th} route

NRU = Number of attack units

NT(I) = Number of targets of unit i

OFL(I) = Force level of unit i during previous time step

$P(I,J)$ = Probability of 1st round hit by unit i in range band j
 $PHH(I,J)$ = Probability of a hit following a hit by unit i in range band j
 $PHM(I,J)$ = Probability of a hit following a miss by unit i in range band j
 $PKH(I,J)$ = Probability of a kill given a hit by unit i in range band j
 PM = The proportion of time a moving unit is searching for targets
 $POA(I,J)$ = The proportion of the j^{th} attacker of unit i allocated to fire on unit i
 $POL(I)$ = Percent of unit i lost during the current time step
 $PTT(I)$ = Proportion of surviving firepower allocated to the i^{th} target if there are j targets available
 $RANGE$ = Current minimum distance between attackers and defenders
 $Q(I,J)$ = Probability that unit j is not detected by unit i at current time
 RF = Detection rate reduction factor for a firing unit (in comparison with non-firing unit)
 $RMINTK$ = Minimum effective range for defending weapon system
 $RMINTW$ = Minimum effective range for attacking weapon system
 $RMXTK$ = Maximum effective range for defending weapon system
 $RMXTW$ = Maximum effective range for attacking weapon system
 $ROT(I,J)$ = The range of the j^{th} target of unit i
 $SIZETK$ = Size of attacking vehicle
 $SIZETW$ = Size of defending vehicle
 $TA(K)$ = Time to acquire a target for k^{th} weapon system type ($k = 1,2$)
 $TF1(K)$ = Time of flight to 1000m for k^{th} weapon system type ($k = 1,2$)

TF2(K) = Time of flight to 2000m for kth weapon system type (k = 1,2)
 TF3(K) = Time of flight to 3000m for kth weapon system type (k = 1,2)
 TH(K) = Time to fire a round following a hit for weapon system type k (k = 1,2)
 TI(K) = Time to fire first round after target has been acquired for weapon system type k (k = 1,2)
 TM(K) = Time to fire a round following a miss for weapon system type k (k = 1,2)
 TNKFR = Firing rate for attacking weapon system
 TOWFR = Firing rate for defending weapon system
 TPOL(I) = Total percentage of lost since battle began for unit i
 VISFR(I,J) = The fraction of unit i seen by unit j
 VISFRA = Fraction of unit A as seen by unit B
 VISFRB = Fraction of unit B as seen by unit A
 X(I),Y(I) = Coordinates of unit i
 XA(I),YA(I) = Coordinates of alternate position for defender i
 XIC(I,J) = Coordinates of the jth interval endpoint of the route for unit i
 YIC(I,J) =
 XL,YL = Distance added to previous interval endpoint for vehicle to move DST during a time step
 XLOC(I,J) = Coordinates of the jth node inputed by the user for the route of unit i
 YLOC(I,J)

APPENDIX D
PROGRAM LISTING

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C AMPHIBIOUS ASSAULT PHASE
COMMON /AMPH/ IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TEWDINIT(2),STAT(5),
COMMON /ENGR/,SPDMAX,SPDMIN,HTMAX,HTMIN,TTS(6,2),TAA,TB,TFF
COMMON /DISPER/ TSGV(6,2),TSIGH(6,2),TMENH(6,2),
ISSIGV(7,2),
COMMON /DEF/ STENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
1SVEL'DE FWTS(2),
COMMON /SUPEFT/ GAMMA,DELTA
COMMON /IOUT/ ISURV,ITA,TTR
C GROUND ATTACK PHASE
COMMON /GRP1/ IPRDIR(6),SECWD(6),MYTDIR(6),X(6),Y(6),SPD(6)
COMMON /GRP2/ ITA(2),T(1)(2),TH(2),TF(2),F3(2),
PMM(2,6),PHH(2,6),PH(2,6),PKH(2,6),TF(2),
COMMON /GRP3/ NBU,NRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
LDIR(3,200),AVSP,ISP,
1LUSTAT(6),IT(6),LOST(6,6),VISFRB,SIZETK,
1LIZETWTNT(6),INF(6),LSRF,DISMAX,
INLOSC(6,6),VISFR(6,6),RMINT,WMINT,OP,TOWFR,TNKFR,
IPT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),NA(6,6),OF(6),POL(6),
COMMON /GRP4/ TPOL(6,6),OLDQ(6,6),Q(6,6),
COMMON /GRP5/ LOT(6,6),ROT(6,6),
COMMON /HILLS/ XCC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PYV(100),BASE
COMMON /HILLS/ NHILLS,
COMMON /COVER/ CXX(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/ KH,KHW,KV,KN,KGRS,KELL,KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150),
COMMON /ALPHA/ ALPHA(6),
COMMON /GRP7/ XA(6),YA(6),IMOVE(6)
C
GATM=0.
GATK=0.
CALL DATA IN
CALL SETUP
CALL SEA(GATM,GATK)
IF(GATK.NE.0.) GO TO 106
WRITE(6,105)
105 FORMAT(1X,TOTAL LANDED LF STRENGTH IS NOT SUFFICIENT FOR GATK*)

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STOP IF(GATK-2.0) 10,20,30
105 WRITE(6,107)
106 FORMAT(1X,'GROUND ATTACK STARTS WHILE SHORE COMBAT IS GOING ON')
107 GOTO 110
108 FORMAT(1X,'GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT')
109 GOTO 110
110 WRITE(6,109)
111 FORMAT(1X,'GROUND ATTACK STARTS AFTER ALL WAVES LANDED')
112 FORMAT(6,111)
113 FORMAT(1X,'GROUND ATK TIME=::,F6.1)
114 CALL GROUND(GATM)
STOP
END

C SUBROUTINE SEA(GATM,GATK)
115 COMMON /AMPH/ IL(15),WBC(2),A(2),ITE,ISE,RD,WVINT(5),WID,
116 ITBW,DINIT(2),GAINL,IWSTAT(5),
117 COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TAA,TB,TFF
118 CALL OUTPUT
119 RD=500
120 ITBW=120
121 RD=1
122 ITBW=1.0*ITBW
123 TINT=0.0
124

C COMPUTATION OF FIRST WAVE TIME PARAMETERS
125 TA-TIME FIRST WAVE INITIATES TRANSITION
126 TB-TIME FIRST WAVE COMPLETES TRANSITION
127 TFF-TIME FIRST WAVE REACHES THE BEACH
128 TAA=(5000.-RD)/SPDMAX
129 ITB=TA+TTSS
130 TFF=TB+(RD-(0.5*(SPDMAX-SPDMIN)*TTSI)-150.)/SPDMIN
131 DEL=10.*55.
132 WRITE(6,132)
133 FORMAT(1X,'ITERATION INITIATED...RD=:,F10.3,1X,`TBW='
134 1. F10.3)
135 CALL RKINT(DEL,TINT,N,GATM,GATK)
136 RETURN
137 END

C SUBROUTINE RKINT PROVIDES THE INTERFACE BETWEEN
138 THE EULER NUMERICAL INTEGRATION ROUTINE(RKLDQ)
139 AND THE SUBROUTINE ATR WHICH DETERMINES EACH
140 UNIT'S STATUS AS TIME PROGRESSES THROUGH THE
141

```

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C AMPHIBIOUS OPERATION
C COMMON /AMPH/ IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
C 1,TBW,DIN(2),GAINL,IWSAT(5)
C COMMON /OUT/ISURV,IASURV(5),CDSURV(2),TA(5),SA(5),DA(2),
C DIMENSION CSURV(5),RKATTR(1),RKATTR(200,12),TIME(200)
C IMAX - MAXIMUM ALLOWABLE NUMBER OF TIME INTERVALS
C ITE - A SWITCH VARIABLE SET TO 1 WHEN THE DEF.TANK
C UNIT INITIATES ITS FIRE
C ISE - A SWITCH VARIABLE SET TO 1 WHEN THE DEF.ATGM
C UNIT INITIATES ITS FIRE
C IT - CURRENT TIME
C IT - CURRENT TIME PERIOD
C GALF=0
C IMAX=199
C ITE=0
C ITSURV=0
C TITE(1)=0.
C DO 10 I=1,5
C CSURV(1)=WVINT(1)
C CSURV=TSURV+CSURV(1)
C IIT(1)=0
C IWSAT(1)=0
C CONTINUE
C 10 DO 15 I=1,2
C CDSURV(1)=DINIT(1)
C 15 CONTINUE
C DO 20 J=1,12
C 20 TATTR(1,J)=0.
C IT=1
C DO 25 I=1,5
C RKSURV(1)=CSURV(1)
C RKSURV(6)=CSURV(1)
C RKSURV(7)=CSURV(2)
C DO 30 I=1,7
C 30 RKATTR(1)=0.
C NT=0
C CALL ATTR(1,CSURV,CDSURV,TA,SA,DA,GALF,GATK,GATM)
C 1000 IF(IL(1) EQ .99) GO TO 1200
C DC 40 I=1,5
C RKSURV(1)=CSURV(1)
C RKATTR(1)=(TA(1)+SA(1))*(-1.0)
C 40 DO 45 I=1,2
C
GRA00900
GRA00910
GRA00920
GRA00930
GRA00940
GRA00950
GRA00960
GRA00970
GRA00980
GRA00990
GRA01000
GRA01010
GRA01020
GRA01030
GRA01040
GRA01050
GRA01060
GRA01070
GRA01080
GRA01090
GRA01100
GRA01110
GRA01120
GRA01130
GRA01140
GRA01150
GRA01160
GRA01170
GRA01180
GRA01190
GRA01200
GRA01210
GRA01220
GRA01230
GRA01240
GRA01250
GRA01260
GRA01270
GRA01280
GRA01290
GRA01300
GRA01310
GRA01320
GRA01330
GRA01340
GRA01350
GRA01360
GRA01370

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RKSURV(I+5)=CDSURV(1)
45 RKAATTR(I+5)=-1.0*DA(1)
S=RKLDEQ(7,RKSURV,RKAATTR,T,H,NT)
DC 50 I=1,5
CDSURV(1)=RKSURV(1)
50 CONTINUE
DO 55 I=1,2
CDSURV(1)=RKSURV(I+5)
55 CONTINUE
IF(S-1)1100,1000,1200
1100 WRITE(6,60)
60 FFORMAT(1X,ERRO..S.NE.1.OR.2)
STOP
1200 CONTINUE
IT=IT+1
TSURV=0.
DO 65 L=1,5
TSURV=TSURV+CSURV(L)
65 IF(TSURV.LE.0.)TSURV=0.
TIME(LIT)=T
C PRINT RESULT OF SHIP TO SHORE MOVEMENT AFTER EACH TIME STEP
WRITE(6,12)T
112 FORMAT(//1X,'TIME='',F6.1,1X,'SECONDS'//)
WRITE(6,13)T
113 FORMAT(1X,'WAVE'',2X,'FORCE LEVEL'',2X,'STATUS'',2X,'LOST-PCT'',
12X,'TSURV')
DO 66 I=1,4
PLOST=1.-CSURV(I)/WVINT(I)
WRITE(6,14)I,CSURV(I),IWSTAT(I),PLOST
66 CONTINUE
PLOST=1.-CSURV(5)/WVINT(5)
114 FORMAT(3X,I1,3X,F10.4,5X,I1,5X,F8.3)
115 PLOST=1.-CSURV(5)/F10.4,5X,I1,5X,F8.3)
116 PLOST=1.-CSURV(1)/DINIT(1)
WRITE(6,16)CSURV(1)/DINIT(1)PLOST
FORMAT(1X,'TANK',2X,F10.4,1X,F8.3)
117 PLOST=1.-CSURV(2)/DINIT(2)
TASURV=CDSURV(1)+CDSURV(2)
WRITE(6,17)CDSURV(2)/PLOST,TASURV
FORMAT(1X,'ATGM',2X,F10.4,1X,F8.3,2X,F5.2)
C DO 80 J=1,5
TATTR(I,J)=TA(J)
80 TATTR(I,J+5)=SA(J)
DO 85 J=1,2
85 TATTR(I,J+10)=DA(J)
R=RNG(T-4.*TBW)

```

```

C DETERMINE IF ALL WAVES LANDED AND GROUND ATK STARTED
C IF(R.LT.75.) GO TO 2000
C IF(LL(1).GT.1MAX) GO TO 2000
C IF(LL(1).EQ.99) GO TO 2000
C GO TO 1000
C
C 2000 N=1
C      WRITE(6,90) TSURV
C      90 FORMAT(1X,FINAL LYA SURVIVORS ASHORE= *,F10.3)
C      IF(GATK.GE.1) GO TO 2222
C      IF(TSURV.LT.9.) GO TO 2222
C      GATK=3.
C      GATH=T
C      RETURN
C
C 2222 END
C
C      SUBROUTINE RKLD(EQ(N),Y,F(X,H,NT))
C      DIMENSION Y(1),F(1),Q(25)
C      NT=NT+1
C      GO TO (1,2,3,4),NT
C
C 1 H1=H
C      AA=H/4.0
C      DO 11 J=1,N
C 11 Q(J)=0.
C      X=X+AA
C      GO TO 5
C
C 2 X=X+AA
C      GO TO 5
C
C 3 X=X+AA
C      GO TO 5
C
C 4 DO 93 L=1,N
C      93 Y(L)=Y(L)+AA*F(L)
C      NT=0
C      X=X+AA
C      RKLD(EQ=2.
C      GO TO 6.
C
C 5 DO 90 I=1,N
C      90 Y(I)=Y(I)+AA*F(I)
C      RKLD(EQ=1.0
C      6 RETURN
C      END
C
C  SUBROUTINE ATTRIT ,CSURV,DSURV,TA,SA,DA,GALF,GATK,GATH
C
C GIVEN THE CURRENT TIME AND STATE VARIABLE STRENGTHS, UPDATES
C SUBROUTINE ATTRIT DETERMINES THE ATTRITION RATES AND UPDATES
C THE STATUS OF EACH UNIT WITH RESPECT TO SHORE MOVEMENT
C AND IMPLEMENTS THIS INFORMATION INTO THE ATTRITION LOSS RATE
C COMPUTATION.

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C TAI(1) = CURRENT ATTRITION LOSS RATE FOR WAVE 1 DUE TO TANK FIRE
C TAI(2) = CURRENT ATTRITION LOSS RATE FOR WAVE 1 DUE TO ATGM FIRE
C TAI(3) = CURRENT ATTRITION LOSS RATE FOR DEF FORCE 1 DUE TO
C          FIRE SUPPORT/TLF EFFECTS
C
C COMMON /AMPHIL/ IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
C 1TBW,DIN(1),GAINL,IWSAT(5),
C COMMDEF/TEGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
C 1SYEL,DEFWS(2)
C INTEGRERTENG(2),SENG(2)
C DIMENSION TRNG(2),TWT(2),SRNG(2),DSURV(2),SWTS(2),
C 1CSURV(5),TA(5),SA(5),DA(2)
C
C DO 10 I=1,5
C   TA(1)=0.
C   SA(1)=0.
C   10 CONTINUE
C
C   DS1=0.
C   DS2=0.
C   DT1=0.
C   DT2=0.
C   FAC=1.0
C
C DETERMINE IF PART OF LANDING FORCE ADVANCE TO ATTACK INLAND
C KEY TERRAIN
C
C   IF(GATK.EQ.1.0) GO TO 2929
C   1IF(GALF.EQ.1.0) AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C     1+DINIT(2)) GATK=1
C   1IF(GALF.EQ.1.0) AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C     1+DINIT(2)) GATK=1.0
C
C DETERMINE IF DEF. BREAKPOINT HAS BEEN REACHED
C
C   2929 IF((DSURV(1)+DSURV(2)).LT.0.3*(DINIT(1)+DINIT(2)))
C     1 GO TO 20
C
C DETERMINE ATTRITION RATE ON DEFENSIVE FORCES BY ATFFS
C BASED UPON AREA OR AIMED FIRE STATUS
C
C   DA(1)=B(1)
C   DA(2)=B(2)
C   IF(ITE.EQ.0) DA(1)=A(1)*DSURV(1)
C   IF(ISE.EQ.0) DA(2)=A(2)*DSURV(2)
C   GO TO 30

```

```

20 DSURV(1)=0.
   DSURV(2)=0.
   DA(1)=0.
   DA(2)=0.
   IF(GATK.EQ.1.) GO TO 3939
   GAT=T

C DETERMINE IF DEF.BREAKPOINT HAS BEEN REACHED BEFORE SUFFICIENT
C LANDING FORCE IS BUILT UP ON THE SHORE FOR INLAND ATTACK
C
97 DO 91 I=1,5
   WVRNG=RNG(GAT-TBW*(I-1))
   IF(WVRNG.LT.75.) IL(I)=1
   IF(IL(I).EQ.1.) TLF=TLF+CSURV(I)
91 CONTINUE
   GAT=GAT+10.
   IF(TLF.LT.9.0.AND.IL(5).EQ.1) RETURN
   IF(TLF.LT.9.0.AND.IL(5).NE.1) GO TO 97
   GATK=2.
   GATM=GAT
   WRITE(6,220) GATM
220 FORMAT(7,1X,'GROUND ATK INITIATES AT TIME= ',F7.1)
3939 IL(1)=99
   WRITE(6,25) ! BEAKPOINT REACHED AT TIME = 0,F9.3!
25 FORMAT(1X,! )
   RETURN
30 CALL DTGTSIT,TENG,TRNG,TWTS,SENG,SRNG,SWTS,CSURV
C DETERMINE THE CUMULATIVE NUMBER OF SURVIVING LVA'S
C THAT HAVE BEEN REACHED THE BEACH - TLF
C
   TLF=0.
   DO 40 J=1,5
   IF(IL(J).EQ.1) TLF=TLF+CSURV(J)
40 CONTINUE

C DETERMINE IF TLF BUILT UP IS SUFFICIENT FOR GROUND ATK
C
   IF(TLF.GE.9.) GATF=1.
   IF(GATK.EQ.1.) TLF=TLF-9.

C ALLOCATE THE FORCE STRENGTH OF TLF BETWEEN THE TWO
C DEFENSIVE FORCE UNITS
C
   DSUM=DSURV(1)+DSURV(2)
   TLF1=(DSURV(1)/DSUM)*TLF
   TLF2=(DSURV(2)/DSUM)*TLF

```

```

CCCCC ADD TO DA1 AND DA2 THE ATTRITION LOSS RATE DUE
TO THE EFFECTS OF TLF1 AND TLF2
DA{1}=DA{1}+TLF1*WB{1}
DA{2}=DA{2}+TLF2*WB{2}
IF{DSURV{1}}.LE.0.0 DA{1}=0.0
IF{DSURV{2}}.LE.0.0 DA{2}=0.0

CCCCC DETERMINE IF THERE EXISTS AN INCOMING WAVE IN THE
TANK ENGAGEMENT WINDOW I.E. TENG{1}.NE.0
IF(TENG{1}.EQ.0.) GO TO 1.00
1 TE=1

CCCCC DETERMINE THE TIME SINCE WAVE TENG{1} CROSSED THE
5000. METER OFFSHORE MARK -T1
T1=T-TBW*TENG{1}
D1=TWT${1}*DSURV{1}
FAC=1.

CCCCC DETERMINE THE SUPPRESSION EFFECT TO BE IMPOSED
ON THE DT UNIT BASED ON THE ATTRITION LOSS RATE
CURRENTLY IN EFFECT
SUPFAC=DA{1}

CALL RATE(TRNG{1},SPD(T1),SUPFAC,DT1ROF)
CALL PHIT(TRNG{1},WID,HT{1},SUPFAC,DT1PH)

CCCCC DETERMINE THE ATTRITION LOSS RATE FOR WAVE TENG{1}
TA(TENG{1})=DT1PH*DT1ROF*DT1

CCCCC DETERMINE IF THERE IS A SECOND INCOMING WAVE THAT
IS IN THE TANK ENGAGEMENT WINDOW. IF THERE IS THE
ATTRITION RATE COMPUTATIONS ARE SIMILAR IN FORM
TC THOSE PREVIOUSLY PERFORMED FOR THE CLOSER WAVE
IF(TENG{2}.EQ.0) GO TO 100
T2=T-TBW*TENG{2}-1
DT2=TWT${2}*DSURV{2}
CALL RATE(TRNG{2},SPD(T2),SUPFAC,DT2ROF)
CALL PHIT(TRNG{2},WID,HT{2},SUPFAC,DT2PH)
TA(TENG{2})=DT2PH*DT2ROF*DT2

```

C DETERMINE IF THERE EXISTS AN INCOMING WAVE IN THE AIGM
 C ENGAGEMENT WINDOW. IF THERE IS DETERMINE THE ATTRITION
 C EFFECTS AGAINST THAT WAVE DUE TO AIGM THE ATTRITION
 C RATE COMPUTATION ARE SIMILAR IN FORM TO THOSE FOR THE
 C EFFECTS DUE THE TANK FIRE.

```

100  IF(SENG(1).EQ.0) GO TO 200
      ISE=1
      SI=T-TBW*(SENG(1)-1)
      DS1=SWTS(1)*DSURV(2)
      SUPFAC=DA(2)
      CALL RATE(SRNG(1),SPD(S1),1,WID,HT(1),2,SUPFAC,DS1PH)
      CALL PHIT(1)=DS1PH*DS1ROF*DS1
      SA(SENG(1))=DS1ROF*DS1
      IF(SENG(2).EQ.0) GO TO 200
      S2=SI-TBW*(SENG(2)-1)
      DS2=SWTS(2)*DSURV(2)
      CALL RATE(SRNG(2),SPD(S2),1,WID,HT(2),2,SUPFAC,DS2PH)
      CALL PHIT(2)=DS2PH*DS2ROF*DS2
      SA(SENG(2))=DS2PH*DS2ROF*DS2
      RETURN
200
  
```

C SUBROUTINE DTGTS(T,TENG,TRNG,TWTS,SENG,SRNG,SWTS,CSURV)
 C GIVEN THE CURRENT TIME AND LVA WAVE SURVIVOR POPULATIONS,
 C SUBROUTINE DTGTS DETERMINES THE WAVE NUMBERS THAT ARE
 C TO BE ENGAGED BY THE DT AND DS DEFENSIVE UNITS BASED
 C ON THE ENGAGEMENT WINDOW CRITERIA

```

COMMON /AMPH/ IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WINT(5),WID,
1 TBW,DNIT(2),GAINL,INSTAF(5)
COMMON /DEF/TENGX,SENGMX,SEGMN,TARTM,SARTM,TVEL,
1 $VEL,DEFWTS(2)
INTEGER TENG(2),SENG(2)
DIMENSION TRNG(2),SRNG(2),TWTS(2),CSURV(5),DEMO(5)
DO 10 I=1,2
  TENG(I)=0.
  TWTS(I)=0.
  TRNG(I)=0.
  SRNG(I)=0.
  SENG(I)=0.
  SWTS(I)=0.
  COUNTINUE
10 JT=0
  JS=0
  T$UM=0.
  S$UM=0.
  
```

```

DO 100 I=1,5
WVRNG=RNG(I-TBV)*(I-1)
IF(WVRNG.LT.75.) IWSTAT(I)=1
IF(WVRNG.LT.75.) IWSTAT(I)=1
C IF THE FIRING RANGE TO A WAVE IS LESS THAN 75 METERS,
THE WAVE IS CONSIDERED TO HAVE REACHED A COVERED AND
CONCEALED POSITION ON THE BEACH
IF((WVRNG.GT.TENGMX).OR.(CSURV(I).LT.0.05)).OR.
1((WVRNG.LT.75.).OR.(JT.GE.2)) GO TO 50
JT=JT+1
TENG(JT)=1
TWS(TJ)=DEFWTS(JT)*CSURV(I)
TRNG(JT)=WVRNG
50 IF((WVRNG.GT.SENGMM).OR.(CSURV(I).LT.0.05)).CR.
1((WVRNG.LT.SENGMN).OR.(JS.GE.2)) GO TO 100
JS=JS+1
SENG(JS)=1
SRNG(JS)=WVRNG
SWTS(JS)=DEFWTS(JS)*CSURV(I)
SSUM=SSUM+SWTS(JS)
100 CONTINUE
C DETERMINE WAVE STATUS
DO 20 I=1,2
DO 25 J=1,5
IF(IWSTAT(J).NE.1.AND.SENG(I).EQ.J) IWSTAT(J)=2
25 CONTINUE
20 CONTINUE
DO 30 I=1,2
DO 35 J=1,5
IF(IWSTAT(J).EQ.1) GO TO 35
IF(IWSTAT(J).EQ.2.AND.TENG(I).EQ.J) IWSTAT(J)=3
35 CONTINUE
30 CONTINUE
C IF(TENG(I).EQ.0) GO TO 500
DO 200 I=1,2
TWS(I)=TWS(I)/TSUM
200 CONTINUE
500 IF(SENG(I).EQ.0) RETURN
DO 600 I=1,2
SWTS(I)=SWTS(I)/SUM
600 CONTINUE

```

RETURN
END

C SUBROUTINE DATAIN /AMP/H/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
COMMON /DIN/IT(2),GAINL,IWSTAT(5),
1TBW,DIN/IT(2),GAINL,IWSTAT(5),
COMMON /DISPER/SPDMAX,SPDMIN,TSIGV(6,2),TMIN,TTS(TAA,TB,TFF
1SSIGV(7,2),TSIGH(6,2),TMÉANH(6,2),
COMMON /ENG/R/SPDMAX,SPDMIN,TMAX,SENGMX,SENGMN,SENGMX,SENGMN,TARTM,TVEL,
1SVEL&DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA

COMMON /IOUT/ISURVIATTR
READ(5,100) TTS
READ(5,100) TENGMX,SENGMX,SENGMN
READ(5,100) TARTM,SARTM,TVEL,SVEL
READ(5,100) TSIGH(I,J),I=1,6,J=1,2
READ(5,100) TSIGH(I,J),I=1,6,J=1,2
READ(5,100) TSIGH(I,J),I=1,6,J=1,2
READ(5,100) TSIGH(I,J),I=1,7,J=1,2
READ(5,100) TSIGH(I,J),I=1,7,J=1,2
READ(5,100) DEFWT(S(I,J),I=1,5)
READ(5,100) DINIT(I,J),I=1,2
READ(5,101) (A(I,J),I=1,2)
READ(5,101) (B(I,J),I=1,2)
READ(5,101) (WB(I,J),I=1,2)
READ(5,101) GAINL
READ(5,101) GAMMA,DELTA
110 FORMAT(F5.2)
150 FORMAT(2I5)
100 FORMAT(7F10.3)
101 FORMAT(2F10.5)
103 FORMAT(5F10.5)
RETURN
END

C SUBROUTINE OUTPUT
COMMON /AMP/H/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DIN/IT(2),GAINL,IWSTAT(5),
COMMON /DISPER/SPDMAX,SPDMIN,TSIGV(6,2),TSIGH(6,2),TMÉANH(6,2),
1SSIGV(7,2),TSIGH(7,2),
COMMON /ENG/R/SPDMAX,SPDMIN,TMAX,SENGMX,SENGMN,SENGMX,SENGMN,TARTM,TVEL,
1SVEL&DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA

```

C*** INPUT SUMMARY PRINTOUT
C
      WRITE(6,120) 1X,'AMPHIBIOUS ASSAULT INFORMATION'
  20 FORMAT(6,12) 1X,'INITIAL FORCE STRENGTH'
  22 FORMAT(6,12) 1X,'DEFENDER ATTRITION LEVEL ALLOWING GROUND ATTACK'
  23 FORMAT(6,12) 1X,'WAVE' 2X,1,5X,2,5X,3,5X,4,5X,5
  24 FORMAT(6,12) 1X,'LVA' 5,2X,F4.1)
  21 FORMAT(6,12) 1X,'DINI' 1,2)
  21 FORMAT(6,12) 1X,'DT' =,1X,F3.1)
  25 FORMAT(6,12) 1X,'LVA ENGR SPECS')
  26 FORMAT(6,12) 1X,'SPDMAX' 2X,'SPDMIN' 3X,'HTMAX' ,2X,'HTMIN' ,3X,'WID')
  26 FORMAT(6,12) 1X,'SPDMAX' 2X,'SPDMIN' 3X,'HTMIN' ,2X,'HTMAX' ,3X,'WID')
  27 FORMAT(6,12) 1X,'F5.2,3X,F5.2,3X,F5.2,3X,F4.2)
  27 FORMAT(6,12) 1X,'F5.2,3X,F5.2,3X,F5.2,3X,F4.2)
  630 FORMAT(6,12) 1X,'DEFENSIVE TACTICAL PARAMETERS')
  631 FORMAT(6,12) 1X,'RANGE' ,4X,'AIM-RELOAD' ,3X,'PROJECTILE')
  631 FORMAT(6,12) 1X,'MAX' ,3X,'MIN' ,4X,'TIME' ,7X,'VELOCITY')
  632 FORMAT(6,12) 1X,'TENGMX,TARTM,TVEL')
  633 FORMAT(6,12) 1X,'TANK' ,1X,F5.2,7X,F6.2)
  633 FORMAT(6,12) 1X,'SENMMN,SARIM,SVEL')
  634 FORMAT(6,12) 1X,'ATGM' ,1X,F6.1,1X,F6.1,2X,F5.2,7X,F6.2)
  634 FORMAT(6,12) 1X,'DEFWTS' ,1X,'DEFWTS' ,2)
  50 FORMAT(6,12) 1X,'DEFENSIVE TACTICAL ALLOCATION WEIGHTS:',,
  50 FORMAT(6,12) 1X,'WAVE' 1 = ,F5.2,1X,WAVE 2 = ,F5.2)
  100 FORMAT(6,12) 1X,'DEFENSIVE FORCE ATTRITION COEFFICIENTS')
  100 FORMAT(6,12) 1X,'ALPHA*A' 10X,'BETA*A')
  101 FORMAT(6,10) 2,A(1),B(1)
  102 FORMAT(6,10) 3,A(2),B(2)
  102 FORMAT(6,10) 3,A(2),B(2)
  103 FORMAT(6,10) 4,S,6X,F7.5)
  103 FORMAT(6,10) 4,WB(1),WB(2)
  104 FORMAT(6,10) 5,WBETA(1)=,F7.5,1X,'WBETA(2)=,F7.5)
  104 FORMAT(6,10) 5,WBETA(1)=,F7.5,1X,'WBETA(2)=,F7.5)
  105 FORMAT(6,12) 1X,'BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEF FORCE)')
  105 FORMAT(6,12) 1X,'GAIN')
  770 FORMAT(6,12) 1X,'DEFENDER ATTRITION LEVEL ALLOWING GROUND ATTACK')
  770 FORMAT(6,12) 1X,'TOTAL DEFENDER FORCE')
  1/ 1X,F5.2,1,4(TOTAL DEFENDER FORCE)
  1/ 1X,F5.2,1,4(GAMMA,DELTA)

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771 FORMAT( /1X, 'ARTM SUP FACTOR=*,F5.1,2X, 'ERROR SUP FACTOR=*,F5.1)
C*** DISPERSSION DATA PRINTOUT
C
1 DISP=1 SP=EQ.OI RETURN
      WRITE(6,601)
      FORMAT( /1X,'DISPERSSION DATA'//)
601   FORMAT(6,602)
      WRITE(6,602)
      FORMAT(3X,'RANGE',2X,'TSIGV',2X,'RANGE',2X,'TSIGH',
     12X,'RANGE',2X,'TMEANH')
     DO 55 I=1,6
      WRITE(6,603) TSIGV(I,1),TSIGH(I,1),TSIGH(I,2),
     1 TMEANH(I,1),TMEANH(I,2)
55   CONTINUE
603   FORMAT(1X,F7.1,2X,F5.1,1X,F5.1,1X,F7.1,1X,F5.1)
      WRITE(6,604)
604   FORMAT(73X,'RANGE',2X,'SSIGV',2X,'RANGE',2X,'SSIGH')
     DO 56 I=1,7
      WRITE(6,605) SSIGV(I,1),SSIGH(I,1),SSIGH(I,2)
56   CONTINUE
605   FORMAT(1X,F7.1,2X,F5.1,1X,F7.1,1X,F5.1)
      WRITE(6,606)
606   FORMAT(1,THE AMPHIBIOUS ASSAULT PHASE BEGINS'//)
      RETURN
END

C
SUBROUTINE PHIT(RANGE,WPN,SUPFAC,PRHIT)
CCMMON /AMPN/IL(5),WB(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DIN,IT(2),GAINT(5),IWSTAT(5)
1CCMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SUPFT/GAMMA,DELTA
C
PI=ARCSIN(-1.0)
IF(RANGE<LT:25.0) STOP
IF(WPN=EQ.1) GO TO 50
C ATGM FIRING DATA COMPUTATIONS
WMEANH=0.0
WMEANV=0.0
C TANK FIRING DATA COMPUTATIONS
50 WMEANV=0.0
CALL INTRP(SSIGV,RANGE,WSIGV,7)
CALL INTRP(SSIGV,RANGE,WSIGH,7)
C CONVERSION TO MILS
CALL INTRP(TSIGV,RANGE,WMEANH,6)
CALL INTRP(TSIGV,RANGE,WMEANH,6)
CALL INTRP(TSIGV,RANGE,WMEANH,6)
CONVERSION TO MILS

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100 Z=ARSIN(W/RANGE)
    WSIGNY=WSIGH*((1.+DELT)*SUPFAC)
    WSIGH=WSIGH*((1.+DELT)*SUPFAC)
    TGTW=(Z*6400.0)/(2.0*PI)
    TGTW=(ARSIN(W/RANGE))*(6400.0/(2.0*PI))
C INSTITUTE NORMALITY ASSUMPTIONS TO COMPUTE HORIZONTAL
C AND VERTICAL HIT PROBABILITIES
C
C = -1.0 * SQRT((1./2.) * WMEANH) / WSIGH
HOR1=((TGTW/2.*TGTW/2.0)-WMEANH) / WSIGH
HOR2=(((-1.0*TGTW/2.0)-TGTW/2.0)-WMEANH) / WSIGH
PHITX=1.0
IF(ABS(HOR1)>GT(.8)) GO TO 810
IF(ABS(HOR2)>GT(.8)) GO TO 810
C*HOR2)
810 PHIT1=5.0*ERFC(C*HOR1)-ERFC(C*HOR2)
    WERTH=(WMEANV)/WSIGH
    VER1=(((-1.0*TGTW/2.0)-TGTW/2.0)-WMEANV) / WSIGH
    PHITY=1.0
    IF(ABS(VER1)>GT(.8)) GO TO 820
    PHIT2=5.0*ERFC(C*VER1)-ERFC(C*VER2)
    PRHIT=PHITX*PHITY
    RETURN
END
C
C SUBROUTINE INTRP(X,ARG,VAL,N)
C DIMENSION X(N),VAL
C 777 WRITE(6,777) ARG
    FORMAT(IX,'ARG***=' F10.3)
    IF(ARG.LT.X(1,1)) GO TO 500
    DO 50 I=1,N
    IF(ARG.GT.X(I+1,1)) GO TO 50
    DIFF=X(I+1,1)-X(I,1)
    DELTA=ARG-X(I,1)
    VAL=X(I,2)+(DELTA/DIFF)*(X(I+1,2)-X(I,1))
    RETURN
50 CONTINUE
    IF(ARG.GT.X(N,1)) GO TO 600
    VAL=X(N,2)
    RETURN
600 WRITE(6,601)
    601 FORMAT(6,601)
    STOP
500 WRITE(6,501)
    501 FORMAT(6,501)
    STOP
END
C
C SUBROUTINE RATE(RANGE,SPEED,IMPN,SUPFAC,ROF)

```

```

COMMON /DEF/TENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,SVEL
COMMON /SUPERT/GAMMA,DELTA
R0F=0.0
IF (RANGE.EQ.25) GO TO 500
IF (IWPN.EQ.2) GO TO 500
IF (RANGE.GT.TENGMX) RETURN
TRTM=SRTM*(1.0+GAMMA*SUPFAC)
DT=TRTM+RANGE/(TVEL+SPEED)
R0F=1.0/DT
RETURN
IF (RANGE.GT.SENGMX) RETURN
IF (RANGE.LT.SENGNN) RETURN
SRTM=SRTM*(1.0+GAMMA*SUPFAC)
DT=TRTM+RANGE/(SVEL+SPEED)
R0F=1.0/DT
RETURN
END

500
FUNCTION SPD(T)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
IF (T.GT.TAA) GO TO 50
SPD=SPDMAX
RETURN
IF (T.GT.TB) GO TO 100
SPD=SPDMIN+((TB-T)/TTS)*(SPDMAX-SPDMIN)
RETURN
100 SPD=SPDMIN
RETURN
END

C
FUNCTION HT(T)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
IF (T.GT.TAA) GO TO 50
HT=HTMAX
RETURN
IF (T.GT.TB) GO TO 100
HT=HTMIN+((TB-T)/TTS)*(HTMAX-HTMIN)
RETURN
100 HT=HTMIN
RETURN
END

C
FUNCTION RNG(T)
COMMON /AMPH/ IL(5),WB(2),A(2),B(2),ITE,ISE,WVINT(5),WID,
1 TB,DINIT(2),GAINL,IWSTAT(5)
COMMON /ENGR/ SPDMAX
IF (T.GT.TAA) GO TO 50

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```

RNG=5000.0-(SPDMAX*T)
RETURN
50 IF(T>TB) GO TO 100
RNG=RD-0.5*(T-TAA)*(SPDMAX+SPD(T))
RETURN
100 RNG=RD-((TB-TAA)/2.0)*(SPDMIN+SPDMAX))-((T-TB)*SPDMIN)
IF(RNG.LT.75.) RNG=0.0
RETURN
END

C C
SUBROUTINE GROUND(GATM,ISECWD,MYTDIR(6),X(6),Y(6),SPD(6),
COMMON /GRP1/ TDIR(6),TM(2),TF1(2),TF2(2),TF3(2),
COMMON /GRP2/ TA(2),PHM(2,6),PKH(2,6),TF(2),
IP(2,6),PHH(2,6),NBU(NRU,FL(6),FO(6),NOI(3),XIC(3,200),
1 COMMON /GRP3/ IDIR(3,200),AVSP,ISPD,
1 IDIR(3,200),AVSP,ISPD,
1 IDUSTA(6,1),IDUST(6,6),VLOSSR,DISMAX,VISFRB,SIZETK,
1 IDIZETW(NT(6),NF(6),SRF,DIMINT,RMXTK,RMXTW,DP,TOWER,TNKFR,
1 NLOSSC(6,6),VISFR(6,6),VFSR(6,6),POA(6,6),POA(6,6),NA(6),NA(6),POL(6),
1 PT(3,3),RF,TPOL(6,6),OLDQ(6,6),Q(6,6),
COMMON /GRP4/ CCOMMON /GRP5/ CCOMMON /HILLS/ CCOMMON /HILLS/
COMMON /HILLS/ CCOMMON /HILLS/ CCOMMON /COVER/ CCOMMON /COVER/
COMMON /HILLS/ NHILLS,NHILLS,XCAE(100),XC(100),PEAK(100),SX(100),SY(100),RHO(100),
COMMON /COVER/ CXC(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150),
COMMON /COVER/ CPXY(150),NCVELS,KINT,KELL,KINT
COMMON /COUNTR/ KKH,KHV,KNN,KGRS,KELL,KINT
COMMON /GRID/ LSTC(10,10),NH(10,10),LISTH(450),KHREP(100),KTREP
COMMON /GRID/ LSTC(10,10),NC(10,10),LISTC(400),KCREP(150),
COMMON /GRID/ ALPHA(6),
COMMON /GRP7/ XA(6),YA(6),IMOVE(6),
INITIALIZATION.

C C
BL=0.0
RL=0.0
MP=0.0
PAI=3.14159
ZL=.00001

C C
READ TERRAIN DATA FOR LINE OF SIGHT
CHECK FOR STOCHASTIC OR DETERMINISTIC ATTRITION
I TRIT-ATTRITION MOD L=DETERMINISTIC
I S-SEED NUMBER
O=STOCHASTIC
C C

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```

130 READ(9,130) ITRIT,IS
DO 132 I=1,6
CALL LRND {1,SYRAN},{1,0}
ALPHA(I)=(-2.*YRAN,{1,2},{1,2},*YRAN+.3)
C WRITE(6,79) YRAN,ALPHA(I)
C 799 CONTINUE
C 132 FORMAT(2X,0 YRAN,ALPHA*,F10.5,2X,F10.5)
C READ IN NUMBER OF ATTACK AND DEFENSE UNITS
C READ(9,200) NBU,NRU
200 FORMAT(12,1X,12)NBU
C INITIALIZE WEAPON SIZES
C SIZETK=2.5
SIZETW=2.5
C READ IN EFFECTIVE WEAPON RANGES
C READ(9,102) RMINTK,RMXTK,RMINTW,RMXTW
102 FORMAT(F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X)
C INITIALIZE PM,RF,TOWFR,TNKFR AND NOD
PM=.352
RF=.5
TOWFR=.03
TNKFR=.1
NOD=2
DO 101 I=1,NRU
NOI(I)=125
CONTINUE
K=NRU+1
L=NRU+NBU
DO 111 I=1,L
I(I)=0
111 CONTINUE
C READ IN FORCE LEVELS OF EACH ATTACK UNIT
C READ(9,103) {FL},{1,IX},I=1,NRU
103 FORMAT(3(F3.1,1X),I=1,NRU)
C CHECK FOR TYPE OF ROUTE DETERMINITION
READ(9,106) IRTE,ISPD

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106 FORMAT(1I,1X,1I)
106 IF(IISPD.EQ.1) AVSP=9.0
106 IF(IISPD.EQ.1) DST=40.232
106 IF(IISPD.EQ.2) AVSP=12.0
106 IF(IISPD.EQ.2) DST=53.643
106 IF(IISPD.EQ.3) AVSP=15.0
106 IF(IISPD.EQ.3) DST=67.053
106 IF(IISPD.EQ.4) AVSP=18.0
106 IF(IISPD.EQ.4) DST=80.463
C READ IN INITIAL ATTACK UNIT'S LOCATIONS
DC 6 I=1 NRU
READ(91,107) XIC(1:1),YIC(1,1)
107 FORMAT(F6.1,1X,F6.1)
107 CONTINUE
107 IF(CIRTE.EQ.1) GO TO 108
DO 2 I=1,NRU
DO 2 J=2,125
YIC(1,J)=YIC(1,J-1)+DST*(J-1)
XIC(1,J)=XIC(1,J-1)+DST*(J-1)
107 DIR(1,J)=0
2 CONTINUE
2 GO TO 109
108 CALL ROUTE
109 SUMRO=0.0
DO 3 I=1,NRU
F0(I)=FL(I)
SUMRO=SUMRO+F0(I)
3 SUMRO=XIC(1,1)
Y(1)=YIC(1,1)
MYDIR(I)=DIR(I,1)
SPD(I)=AVSP
IUSTAT(I)=0
IPRDIR(I)=DIR(I,1)
ISECWD(I)=120
NFI(I)=1
II(I)=1
3 CONTINUE
C READ IN DEFENSE UNIT'S LOCATIONS
SUMBO=0.0
DO 4 I=K1,L
READ(91,104) X(I),Y(I),FL(I),IPRDIR(I),ISECWD(I)
104 FORMAT(F6.1,1X,F6.1,1X,F3.1,1X,13,1X,13)
F0(I)=FL(I)
SUMBO=SUMBO+F0(I)

```

```

MYDIR(I)=0
SPD(I)=0.0
ISUSTAT(I)=0
IMOVE(I)=0
4 CONTINUE
C CHECK FOR ALTERNATE DEFENSE POSITIONS AND READ IN IF WANTED
C
C READ(9,400) IALT, BREAK, ITEM
400 FORMAT(1I1,1X,F6.1,1X,I2)
      IF(IALT.EQ.1) GO TO 401
      DO 402 I=K_L READ(9,107) XA(I), YA(I)
      402 CONTINUE
      401 DELT=10.0
      TA(1)=20.
      TH(1)=8.0
      TF1(1)=10.
      TF2(1)=1.
      TF3(1)=1.
      TA(2)=20.
      TH(2)=8.0
      TF1(2)=15.
      TF2(2)=10.
      TF3(2)=12.
      TF3(2)=15.

C READ IN HIT AND KILL PROBABILITIES
C
C DO 5 I=1,2
      DO 514 J=1,6
      READ(9,515) P(I,J), PHM(I,J), PKH(I,J)
      515 FORMAT(4F4.2,1X)
      514 CONTINUE
      515
      PTT(1,1)=1.0
      PTT(1,2)=0.8
      PTT(2,2)=0.2
      PTT(1,3)=0.8
      PTT(2,3)=0.15
      PTT(3,3)=0.05
      DC 31,I=1,NRU
      DC 31,I,J=K_L
      NLOSC(J,I)=0
      GRA08580
      GRA08590
      GRA08600
      GRA08610
      GRA08620
      GRA08630
      GRA08640
      GRA08650
      GRA08660
      GRA08670
      GRA08680
      GRA08690
      GRA08700
      GRA08710
      GRA08720
      GRA08730
      GRA08740
      GRA08750
      GRA08760
      GRA08770
      GRA08780
      GRA08790
      GRA08800
      GRA08810
      GRA08820
      GRA08830
      GRA08840
      GRA08850
      GRA08860
      GRA08870
      GRA08880
      GRA08890
      GRA08900
      GRA08910
      GRA08920
      GRA08930
      GRA08940
      GRA08950
      GRA08960
      GRA08970
      GRA08980
      GRA08990
      GRA09000
      GRA09010
      GRA09020
      GRA09030
      GRA09040
      GRA09050

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Q(I,J)=1.0 GRA09060
Q(J,I)=1.0 GRA09070
VISFR(I,J)=0.0 GRA09080
VISFR(J,I)=0.0 GRA09090
31 CONTINUE GRA09100
IC=1 GRA09110
C PRINT INITIAL BATTLE INFORMATION GRA09120
      WRITE(6,599) GRA09130
599 FORMAT('1.1X, INITIAL GROUND COMBAT INFORMATION') GRA09140
      WRITE(6,600) UNIT,7X,X,8X,Y,FORCE LEVEL) GRA09150
600 FORMAT('1X,UNIT,7X,X,8X,Y,FORCE LEVEL') GRA09160
DO 601 I=1,L GRA09170
      WRITE(6,602) IX(Y(I),FL(I)) GRA09180
602 FORMAT(IX,13,3X,F7.1,2X,F7.1,7X,F3.1) GRA09190
CONTINUE GRA09200
601 IF(ATTRIT.EQ.1) GO TO 603 GRA09210
      WRITE(6,604) ATTRITION IS STOCHASTIC'// GRA09220
604 FORMAT('1X, ATTRITION IS DETERMINISTIC'//) GRA09230
      GO TO 605 GRA09240
603 WRITE(6,606) ROUTES DETERMINED BY USER'// GRA09250
606 FORMAT('1X,DETERMINISTIC'//) GRA09260
605 WRITE(6,608) AVSP GRA09270
608 FORMAT('1X,ATTACK VEHICLE SPEED IS ',F4.1/) GRA09280
607 WRITE(6,609) BREAKPOINT DISTANCE IS ,F6.1/) GRA09290
609 FORMAT('1X,BREAKPOINT DISTANCE IS ',F6.1/) GRA09300
610 FORMAT('1X,INITIAL EQUITY') GRA09310
611 IF(INITIAL.EQ.0) GO TO 615 GRA09320
      WRITE(6,620) DEFENDER WILL NOT MOVE TO ALTERNATE POSITIONS'// GRA09330
620 FORMAT('1X,DEFENDER WILL NOT MOVE TO ALTERNATE POSITIONS'//) GRA09340
      GO TO 625 GRA09350
615 WRITE(6,630) DEFENDER WILL MOVE TO ALTERNATE POSITIONS'// X, GRA09360
630 FORMAT('1X,ALTERNATE POSITIONS ARE: ',1X,UNIT,5X,X,8X,Y,) GRA09370
      DO 635 I=K,1 GRA09380
      WRITE(6,640) IX(XA(I),YA(I)) GRA09390
640 FORMAT(IX,13,3X,F7.1,2X,F7.1) GRA09400
635 CONTINUE GRA09410
625 TRAN=500 GRA09420
      WRITE(6,645) ATK,KILL,PROBABILITIES,'1X,RANGE',4X,P, GRA09430
645 FORMAT('14X,PHH,3X,PHH,3X,PKH') GRA09440
      DO 650 I=1,6 GRA09450
      WRITE(6,655) IRAN,P(1,1),PHH(1,1),PKH(1,1),GRA09460
      WRITE(6,655) IRAN,P(1,1),PHH(1,1),PKH(1,1),GRA09470
655 FORMAT(2X,14,4(2X,F4.2)) GRA09480

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GRA09540
GRA09550
GRA09560
GRA09570
GRA09580
GRA09590
GRA09600
GRA09610
GRA09620
GRA09630
GRA09640
GRA09650
GRA09660
GRA09670
GRA09680
GRA09690
GRA09700
GRA09710
GRA09720
GRA09730
GRA09740
GRA09750
GRA09760
GRA09770
GRA09780
GRA09790
GRA09800
GRA09810
GRA09820
GRA09830
GRA09840
GRA09850
GRA09860
GRA09870
GRA09880
GRA09890
GRA09900
GRA09910
GRA09920
GRA09930
GRA09940
GRA09950
GRA09960
GRA09970
GRA09980
GRA09990
GRA10000
GRA10010

IIRAN=IRAN+500
CONTINUE
IIRAN=500
FORMAT(6,660)
14X,'PHH',3X,'PHM',3X,'PKH')
DO 665 I=1,6
WRITE(6,655) IRAN,P(2,I),PHH(2,I),PKH(2,I)
IRAN=IRAN+500
CONTINUE
FORMAT(6,670)
FORMAT(10X,'BATTLE BEGINS',//)
UPDATE LOCATION OF RED UNITS.

665
C
DISMAX=50000.0
67 DO 9 I=1,NRU
IF(IUSTAT(I).EQ.2) GOTO 9
IF(IUSTAT(I)+1.EQ.0) GOTO 76
NF(I)=NF(I)+LT(NOD) GOTO 9
IF(NFI(I)=1) GOTO 9
NF(I)=1 J=1 NRU
DO 76 I=1,11
IF(IUSTAT(J).EQ.2) GOTO 11
IF(IUSTAT(J).EQ.2) GOTO 11
DIST=X(I)-X(J)
IF(DIST.GT.DISMAX) GOTO 9
CONTINUE
I(I)=I(I)+1
K7=I(I)
X(I)=X(I,K7)
Y(I)=Y(I,K7)
MVDIR(I)=IDIR(I,K7)
IPRDIR(I)=IDIR(I,K7)
WRITE(6,666) I,X(I,Y(I),MVDIR(I),IPRDIR(I))
CONTINUE
FORMAT(1,1X,I3,1X,F10.5,2X,I10,2X,I10,/)
LINE--OF-SIGHT CHECK BETWEEN UNITS AND TARGETS SELECTION
DO 17 J=K,L
NT(J)=0
CONTINUE
DO 12 I=1,NRU
NT(I)=0
IF(IUSTAT(I).EQ.2) GOTO 12
DO 16 K=L
IF(IUSTAT(J).EQ.2.OR.IUSTAT(J).EQ.3) GO TO 16
XX1=X(I)

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YY1=Y(I)
CALL ELEV(XX1,YY1,TMACJ)
XX2=X(J)
YY2=Y(J)
CALL ELEV(XX2,YY2,TMACJ)
LATTOB=1
LBTOA=1
WRITE(6,675) XX1,YY1,TMACJ,XX2,YY2,TMACJ
675 FORMAT(6,1X,PRELOS,1X,6(F10.5,1X))
CALL LOS(LBTDA,YY1,TMACJ,0,SIZETK,XX2,YY2,TMACJ,0,0,SIZETW,
1 LATTOB(LBTDA,VISFRA,VISFRB)
VVISFR(I,J)=VISFRA
VVISFR(J,I)=VISFRB
VISFRA=GTR.ZL) GOTO 18
LOST(I,J,I,J)=0
NLOSSC(I,J,I,J)=NLOSSC(I,J)+1
GOTO 16
18 LOST(I,J,I,J)=1
NLOSSC(I,J,I,J)=0
NLOSSC(I,J,I,J)=0
NLOSSC(I,J,I,J)=0
RANGE=SQR((X(I)-X(J))**2+(Y(I)-Y(J))**2)
IF(RANGE.LT.RMINLT.RMAX) OR RANGE.GT.RMAX) GOTO 20
IF(Q(I,J).EQ.1.0) GOTO 20
IUSTAT(I,I)=1
NT(I)=NT(I)+1
M=NT(I)
LOT(I,M)=J
RCT(I,M)=RANGE
IF(M.EQ.1) GOTO 20
CALL SORT(I,M)
IF(Q(I,J).EQ.1.0) GOTO 16
IUSTAT(I,J)=1
NT(J)=NT(J)+1
M=NT(J)
LOT(J,M)=I
RCT(J,M)=RANGE
IF(M.EQ.1) GOTO 16
CALL SORT(J,M)
CONTINUE
DO 25 I=1,NRU
IF(IUSTAT(I).EQ.2) GOTO 25
IF(NT(I).NE.0) GOTO 25
IUSTAT(I)=0
16

```

```

25      NF(1)=0
      CONTINUE
      DO 79 J=K,L
      IF(IUSTAT(J).EQ.0) IUSTAT(J)=0
      79  CONTINUE
C      UPDATE OF THE ACCUMULATED DETECTION PROBABILITIES.
C
      IAA=1
      IBB=NRU
      ICC=K
      IDD=L
      FR=TOWFR
      OP=PM
      DO 345 I=1,6
      CONTINUE
      DO 345 I=IAA,IBB
      IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 14
      DO 19 J=ICC,IDD
      PROP=0.0
      IF(IUSTAT(J).EQ.2.NR.IUSTAT(J).EQ.3) GO TO 19
      OLDQ=I
      QDQ=I
      IF(LOSS(I,J)) QDQ=0.0
      GOTO 15
      IF(NT(I,J)) GT(I,J)
      PCTVI=VSFR(I,J)
      CALL LAMDA(I,J,PCTVIS,DETRAT,PSUBK)
      QV=EXP(-FL(I,J)*DETRAT*OP*DELT*FL(J))
      IF(NT(J,0)) GOTO 23
      Q(I,J)=Q(I,J)*QV
      GOTO 19
      23  QP=(1.0-P(SUBK)*(FR*DELT*FL(I)*FL(J)))
      GOTOB19
      GOTO 19
      N5=NT(I)
      DO 24 I=1,N5
      K1=LOT(I)
      ANG1=ATAN2(Y(K1)-Y(I),X(K1)-X(I))
      ANG2=ATAN2(Y(J)-Y(I),X(J)-X(I))
      IF((ANG1*ANG2)<0.0) GOTO 77
      ANG=2*PAI+ANG1-ANG2
      GOTO 32
      32  ANG=2*PAI+ANG2-ANG1
      35  IF(ANG.GT.PAI) ANG=2*PAI-ANG
      GOTOB33
      77  ANG=ABS(ANG2-ANG1)
      AA=15.0*PAI/180.0
      GRA10500
      GRA10510
      GRA10520
      GRA10530
      GRA10540
      GRA10550
      GRA10560
      GRA10570
      GRA10580
      GRA10590
      GRA10600
      GRA10610
      GRA10620
      GRA10630
      GRA10640
      GRA10650
      GRA10660
      GRA10670
      GRA10680
      GRA10690
      GRA10700
      GRA10710
      GRA10720
      GRA10730
      GRA10740
      GRA10750
      GRA10760
      GRA10770
      GRA10780
      GRA10790
      GRA10800
      GRA10810
      GRA10820
      GRA10830
      GRA10840
      GRA10850
      GRA10860
      GRA10870
      GRA10880
      GRA10890
      GRA10900
      GRA10910
      GRA10920
      GRA10930
      GRA10940
      GRA10950
      GRA10960
      GRA10970

```

```

IF(ANG.GT.AA) GOTO 24
CONTINUE
24 IF(PROP.EQ.0.0) GOTO 34
IF(NT(J).EQ.0) GOTO 36
IF(LAMO(I,J).EQ.PCTVIS,DETRAT,PSUBK)
DETRAT=DETRAT*RF
QV=EXP(-FL(I)*PROP*DETRAT*DELT*FL(J))
Q(I,J)=Q(I,J)*QV
GOTO 19
36 Q(I,J)=0.0
GOTO 19
34 Q(I,J)=1.0
GOTO 19
GOTO 19
15 IF(NLOSC(I,J).LE.3) GOTO 19
Q(I,J)=1.0
19 CONTINUE
14 IF(CIAA.EQ.K) GOTO 38
FR=TNKFR
IAA=K
IBB=L
ICC=1
IDD=NNU
OP=1.0
GOTO 37

```

FIRE ALLOCATION.

```

38 DO 28 I=1,L
NA(I)=0
DO 26 I=1,L
IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 26
IF(NT(I).EQ.0) GOTO 26
DC 27 J=1,3
APOA(I,J)=0.0
27 CONTINUE
IF(NT(I).EQ.1) GOTO 78
IF(NT(I).EQ.2) GOTO 29
NOT=3
MM1=LOT(I,1)
MM2=LOT(I,2)
MM3=LOT(I,3)
PROB=(1.0-Q(I,MM1))*Q(I,MM2)*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PROB
PROB=Q(I,MM1)*(1.0-Q(I,MM2))*Q(I,MM3)
APOA(I,2)=APOA(I,2)+PROB
28
29

```

C C C

```

PROB=Q(I,MM1)*Q(I,MM2)*(1.0-Q(I,MM3))
APOA(I,3)=APOA(I,1)*Q(I,MM1)*Q(I,MM2)*Q(I,MM3)
PROB=(I,0-Q(I,MM1)*Q(I,MM2)*Q(I,MM3))
APOA(I,1)=APOA(I,2)+PTT(I,2)*PROB
APOA(I,2)=APOA(I,1)+PTT(I,1)*PROB
PROB=(I,0-Q(I,MM1)*Q(I,MM2)*Q(I,MM3))
APOA(I,1)=APOA(I,3)+PTT(I,3)*PROB
APOA(I,3)=APOA(I,1)*Q(I,MM1)*Q(I,MM2)*Q(I,MM3)
PROB=(I,0-Q(I,MM1)*Q(I,MM2)*Q(I,MM3))
APOA(I,1)=APOA(I,2)+PTT(I,2)*PROB
APOA(I,2)=APOA(I,1)*Q(I,MM1)*Q(I,MM2)*Q(I,MM3)
PROB=(I,0-Q(I,MM1)*Q(I,MM2)*Q(I,MM3))
APOA(I,1)=APOA(I,3)+PTT(I,3)*PROB
APOA(I,3)=APOA(I,1)*NOT
DO 44 J=1,NOT
  KK=LOT(I,J)
  NA(KK)=NA((KK)+1
  IN=NA(KK)
  LOA(KK,IN)=I
  POA(KK,IN)=APOA(I,J)
CONTINUE
44 GOT0 26
29 NOT=2
  MM1=LOT(I,1)
  MM2=LOT(I,2)
  PROB=(I,0-Q(I,MM1)*Q(I,MM2))
  APOA(I,1)=APOA(I,1)+PTT(I,1)*PROB
  PROB=Q(I,MM1)*Q(I,0-Q(I,MM2))
  APOA(I,2)=APOA(I,1)+PTT(I,1)*PROB
  PROB=(I,0-Q(I,MM1)*Q(I,MM2))
  APOA(I,1)=APOA(I,2)+PTT(I,1)*PROB
  APOA(I,2)=APOA(I,1)+PTT(I,2)*PROB
GOT0 30
78 NOT=1
  MM1=LOT(I,1)
  PROB=(I,0-Q(I,MM1))
  APOA(I,1)=APOA(I,1)+PTT(I,1)*PROB
CONTINUE
26 ATTRITION.
      SUMR=0.0
      SUMB=0.0
      DO 40 I=1,1
        IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 40

```

```

M6=NA(I)
SUM=0.0
IF(M6.EQ.0) GOTO 47
DO 41 J=1,M6
M7=LOA(I,J)
IF(M7.LT.K) GOTO 42
I TYPE=2
1 GOTO 43
2 I TYPE=SQR T((X(I))-X(M7))*2+(Y(I)-Y(M7))*2
3 IF(ISTRIT.EQ.1) GO TO 131
CALL STOCH(I TYPE,RANGE,AJ1)
GO TO 5000
131 AJ1=L0/T
SUM=SUM+AJ1*FL(M7)*POA(L,J)*DELT
5000 CONTINUE
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C
58 C
59 C
60 C
61 C
62 C
63 C
64 C
65 C
66 C
67 C
68 C
69 C
70 C
71 C
72 C
73 C
74 C
75 C
76 C
77 C
78 C
79 C
80 C
81 C
82 C
83 C
84 C
85 C
86 C
87 C
88 C
89 C
90 C
91 C
92 C
93 C
94 C
95 C
96 C
97 C
98 C
99 C
C PRINT AND CHECK FOR BATTLE DETERMINATION.
C
C TIME=IC*10
DO 57 I=K,L
IF(IUSTAT(I).EQ.2) GO TO 57
DO 58 J=1,NRU(I)
IF(IUSTAT(J).EQ.2) GO TO 58
CHECK=X(I)-X(J)
AVD=SORT((X(I)-Y(J))*2+(Y(I)-Y(J))*2)
IF(AVD.LT.BREAK.OR.CHECK.LT.50.) GO TO 250
58 CONTINUE
57 CONTINUE
GO TO 99
C COMPLETE ATTACK UNIT'S MOVE
C 250 DO 251 I=K,L

```

```

IF(IALT.EQ.1.OR.IMOVE(I).EQ.0)IUSTAT(I)=3
IF(IUSTAT(I).EQ.0)IUSTAT(I)=1
IMOVE(I)=IMOVE(I)+1
IF(1MOVE(I).LT.ITEM) GO TO 251
X(I)=XA(I)
Y(I)=YA(I)
IF(IUSTAT(I).EQ.3) IUSTAT(I)=0
251 CONTINUE
99 IITIME=ITIME+IFIX(GATM)
      WRITE(6,112)IITIME
112 FORMAT(//1X,'TIME=',I4,1X,'SECONDS//')
113 WRITE(6,113)UNIT,'5X','X',8X,'Y',5X,'FORCE LEVEL',2X,'STATUS',
      12X,'LOST-PCT',2X,'TARGETS')
      DO 59 I=1,L
N6=N(I)
IF(N6.NE.0) GO TO 48
      WRITE(6,264)1,X(I),Y(I),FL(I),IUSTAT(I),TPCL(I)
264 FORMAT(3X,11,3X,F7.1,2X,F7.1,6X,F3.1,9X,11,6X,F5.0,3)
      GO TO 59
48 WRITE(6,114)I,X(I),Y(I),FL(I),IUSTAT(I),TPDL(I),
      115(I),J=1,N6
114 FORMAT(3X,11,3X,F7.1,2X,F7.1,6X,F3.1,9X,11,6X,F5.3,3X,3(I1,1X))
59 CONTINUE
C CHECK FOR BATTLE TERMINATION.
C
IOT=0
DO 53 I=1,NRU
IF(FL(I).EQ.0.0) GOTO 53
IOT=1
53 CONTINUE
IF(IOT.EQ.1) GOTO 54
      WRITE(6,I7)
      117 FORMAT(IX,*ATTACK FORCE IS ELIMINATED. END OF BATTLE.*)
      GOTO 66
54 DO 55 I=K,1
IF(FL(I).EQ.0.0) GOTO 55
IOT=1
55 CONTINUE
IF(IOT.EQ.1) GOTO 65
      WRITE(6,I8)
      118 FORMAT(1X,*DEFENSE FORCE IS ELIMINATED. END OF BATTLE.*)
      GOTO 66
6000 WRITE(6,I9)
      119 FORMAT(IX,*DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE
      1.)

```

```
60 TO 66  
65 IC=IC+1  
66 RETURN  
END
```

```
C SUBROUTINE SETUP IS USED TO READ IN THE TERRAIN DATA AND  
C CREATE PARAMETRIC TERRAIN DATA WILL BE USED  
C WHEN COMPUTING LINE-OF-SIGHT BETWEEN TARGETS AND OBSERVERS  
C AS WELL AS PROVIDING A GRID SYSTEM FOR UNIT LOCATIONS AND  
C MOVEMENT.
```

```
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)  
COMMON /HILLS/ EC(100),PXX(100),PYY(100),BASE  
COMMON /COVER/ NHILLS,NHILL  
COMMON /COVER/ CXC(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150)  
COMMON /COVER/ CPXY(150),NCVELS  
COMMON /COUNTR/KH,KV,KN,KGRS,KELL,KINT  
COMMON /GRID/ LST(54),NHL(54),LIST(150),KHREP(150),KTRP  
COMMON /GRID/ LSTC(54),NC(54),LISTC(400),KCREP(150)  
PAI=3.14159  
L=5  
READ(L,7) NHILLS  
READ(L,7) NHIL  
FORMAT(F10.4)  
FORMAT(F16.3)  
FORMAT(6F10.3)  
DO 50 I=1,NHILLS  
READ(L,17) XC(I),YC(I),PEAK(I),ANGH(I),SPRD(I),EC(I)  
CONTINUE  
READ(L,37) LST  
READ(L,37) NHL  
READ(L,7) NHTOT  
READ(L,37) LIST(I),I=1,NHTOT  
FORMAT(10.5)  
DO 100 I=1,NHILLS  
ANGLE=ANGH(I)*PAI/180.  
SANGE=SIN(ANGLE)  
SCANG=COS(ANGLE)  
A=PEAK(I)/(PEAK(I)-50.)  
A=ALOG(A)  
B=A*EC(I)**2  
SSPD=SPRD(I)**2  
PXX(I)=-(A*CANG*CANG+B*SANG*SANG)/SSPD  
PYY(I)=-(A*SANG*B*CANG+CANG)/SSPD  
PXY(I)=(2.*SANG*CANG*(B-A))/SSPD  
KHREP(I)=-2147483600
```

C ALL VALUES NOW IN METERS ON 0 -- 10,000 GRID

```
100 CONTINUE
      READ(I,7) NCVELS
      IF(NCVELS.EQ.0) GO TO 75
      DO 60 I=1,NCVELS
      READ(L,27) NCX(I),CYC(I),CPEAK(I),CPXX(I),CPYY(I)
      FORMAT(3F10.4,3E13.7)
      KCREP(I)=-2147483600
      60 CONTINUE
      READ(L,37) LSTC
      READ(L,37) NC
      READ(L,7) NCTOT
      READ(L,37) LISTC(I),I=1,NCTOT
      75 XTREP=-2147483600
      KH=0
      KV=0
      KN=0
      KGRS=0
      KELL=0
      KINT=0
      RETURN
      END
```

C SUBROUTINE ROUTE

SUBROUTINE ROUTE COMPUTES THE ROUTE OF EACH ATTACKING UNIT WHEN THE USER HAS SELECTED THE OPTION OF INPUTTING ATTACKER ROUTES. IT CALCULATES THE COORDINATES OF EACH INTERVAL ENDPOINT ALONG THE ROUTE, MAKING EACH INTERVAL LENGTH INSTANCE MOVED DURING A 10 SECOND TIME STEP. THE SAME THE INTERVAL LENGTH IS DETERMINED BY THE SPEED THE USER HAS SELECTED AND INPUTTED FOR THE CURRENT BATTLE.

```
COMMON /GRP3/NBU,NRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
1 1DIR(200),1AVSP,1SPD,1ISPD,1LSTAT(6,6),1LOST(6,6),1VISFRA,1VISFRB,SIZETK,
1 1SIZETW,NT(6),1INF(6),1SRF,1ISMAX,1RMXTK,1RMINTW,1RMXTW,1RMINTW,1TNKFR,
1 1NLOC(3,3),1RF,1POA(6,6),1POA(6,6),1POA(6,6),1POA(6,6),1POA(6,6),1POA(6,6),
1 1DIMENSION,XLOC(3,20),YLOC(3,20),N(3),
1 1IF1ISPD,EQ.4,DST=80,463
1 1IF1ISPD,EQ.3,DST=67,053
1 1IF1ISPD,EQ.2,DST=53,643
1 1IF1ISPD,EQ.1,DST=40,232
LN=9
DO 300 I=1,NRU
  READ(LN,15) N(I)
```

```

15 FORMAT(12)
NL=N(I)+1
DO 200 IN=2, NL
READ(ILN*201) XLOC$ YLOC$
FORMAT(F6.1,1X) LOC$ IN)=YLOC$  

XLOC(I,IN)=XLOC$  

CONTINUE
200 CYLOC(I,1)=XIC(I,I)
CYLOC(I,1)=YIC(I,I)
IDIR(I,1)=0
NL=N(I)
NUM=205 J=1, NL
XL=XLOC(I,J+1)-XLLOC(I,J)
YL=YLOC(I,J+1)-YLLOC(I,J)
DIST=SQRT(XL**2+YL**2)
Y=ABS(YL)
Z=Y/XL
ANGL=ATAN(Z)
DEG=ANGL*57.2958
IF(J.EQ.1) GO TO 320
XLN=(DIST-EXTRA)*COS(ANGL)
DIST=(DIST-EXTRA)-DST
YLN=(DIST-EXTRA)*SIN(ANGL)
XIC(I,NUM)=XIC(I,NUM-1)+XLN+XLE
IF(YL.GT.0.) GO TO 325
YLN=-YLN
YIC(I,NUM)=YIC(I,NUM-1)+YLN+YLE
325 IF(YL.GT.0.) GO TO 340
IDIR(I,NUM)=-IFIX(DEG)
GO TO 341
340 IDIR(I,NUM)=IFIX(DEG)
341 NUM=NUM+1
320 XLN=DST*COS(ANGL)
YLN=DST*SIN(ANGL)
IF(YL.GT.0.) GO TO 310
310 IF(DIST.LT.DST) GO TO 315
YLN=-YLN
XIC(I,NUM)=XIC(I,NUM-1)+XLN
YIC(I,NUM)=YIC(I,NUM-1)+YLN
IF(YL.GT.0.) GO TO 342
IDIR(I,NUM)=-IFIX(DEG)
GO TO 343
342 IDIR(I,NUM)=IFIX(DEG)
343 DIST=DST-DST
NUM=NUM+1
GO TO 310

```

```

315 EXTRA=DIST
      XLE=EXTRA*COS(ANGL)
      YLE=EXTRA*SIN(ANGL)
      IF(YL.GT.0.) GO TO 305
      YLE=-YLE
      CONTINUE
      305 CONTINUE
      RETURN
      END

C   SUBROUTINE LAMDA( I,J,PCTVIS,DETRAT,PK)
C
C   SUBROUTINE LAMDA IN CONJUNCTION WITH THE LOS ROUTINE COMPUTES
C   THE DETECTION RATE (DETRAT) OF TARGET J BY THE OBSERVER I GIVEN
C   THE PERCENT OF TARGET VISIBLE (PCTVIS) TO THE OBSERVER.
C
COMMON /GRP1/ IPRDIR(6),ISECWD(6),MVTDIR(6),X(6),Y(6),SPD(6)
      TCFAC=1.0
      TZERO=0.00001
      PAI=3.14159
      D=1.1SECWD(1)*PAI/180.0/2.0
      BBB=(1.0/(2.0*(SIN(0)-D*COS(0))))*
      IF(ABS(BBB).LT.ZERO) BBB=0.0
      AAA=(-BBB)*COS(D)
      IF(ABS(AAA).LT.ZERO) AAA=0.0
      OTANG=ATAN2((Y(J)-Y(I))(X(J)-X(I)))
      IF(OTANG.LT.-PAI/2.AND.OTANG.GT.-PAI) OTANG=2*PAI+OTANG
      PD=IPRDIR(1)*PAI/180.0
      IF((PD*OTANG).GE.0.0) GOTO 1
      IF((PD.LT.0.0).GE.0.0) GOTO 9
      ANGLE=2*PAI+OTANG-PD
      GOTO 10
      9 ANGLE=2*PAI+PD-OTANG
      10 IF(ANGLE.GT.PAI) ANGLE=2*PAI-ANGLE
      1 GOTO 2
      2 IF(ANGLE.GT.D) GOTO 3
      DUP=PD+D
      DLW=PD-D
      ANGLFT=OTANG+(15.0*PAI/180.)
      IF(ANGLFT.GT.DUP) ANGLFT=DUP
      ANGLRT=OTANG-(15.0*PAI/180.)
      IF(ANGLRT.LT.DLOW) ANGLRT=DLOW
      PK=BBB*ABS(ABS(SIN(ANGLFT))-ABS(SIN(ANGLRT)))+AAA*(ANGLFT-
      1 ANGLRT)
      1 IF(PK.LT.0.0) GOTO 3
      1 IF(PK.GT.1.0) GOTO 5
      GOTO 8

```

```

3 PK=0.0          GRA14820
DET RAT=0.0      GRA14830
GOTO 6           GRA14840
5 PK=1.0          GRA14850
RANGE=SQRT((X(J)-X(I))**2+(Y(J)-Y(I))**2)  GRA14860
RR=0.01*RANGE/PCTVIS  GRA14870
TOANG=ATAN2(Y(I)-Y(J),(X(I)-X(J)))  GRA14880
AD=MVTDIR(J)*PAI/180.0  GRA14890
HORVEL=ABS(SPD(J)*SIN(TOANG-AD))  GRA14900
HORVEL=HORVEL*160.9/3600.0  GRA14910
DENOM=1.453+TCFACT*(0.5978+2.188*(RR**2)-0.5038*HORVEL)  GRA14920
1F(DENOM.LE.0.003+1.088/DENOM)  GRA14930
DET RAT=0.003+1.088/DENOM  GRA14940
DET RAT=DET RAT*PK  GRA14950
RETURN  GRA14960
END  GRA14970
GRA14980
GRA14990
GRA15000
GRA15010
GRA15020
GRA15030
GRA15040
GRA15050
GRA15060
GRA15070
GRA15080
GRA15090
GRA15100
GRA15110
GRA15120
GRA15130
GRA15140
GRA15150
GRA15160
GRA15170
GRA15180
GRA15190
GRA15200
GRA15210
GRA15220
GRA15230
GRA15240
GRA15250
GRA15260
GRA15270
GRA15280
GRA15290
C SUBROUTINE ELEV(X,Y,TMAC)
C SUBROUTINE LEV DETERMINES THE TERRAIN ELEVATION FOR A GIVEN
C SET OF X, Y COORDINATES. THIS FUNCTION IS USED IN CONJUNCTION
C WITH THE LOS SUBROUTINE IN COMPUTING LINE-OF-SIGHT BETWEEN
C OBSERVER AND TARGET.
C
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100),
COMMON /HILLS/ ECC(100),PXX(100),PYX(100),BASE
COMMON /HILLS/ NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KTRFP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCRCP(150)
DATA GSZ/1000./
C FUNCTION TO COMPUTE TERRAIN ELEVATION FOR GIVEN X, Y COORDINATES.
ZMAX=BASE
IX=1+IFIX(X/GSIZE)
IY=1+IFIX(Y/GSIZE)
1F(NHL(IX,IY).EQ.0) GO TO 150
L=LIST(IX,IY)
LEND=L+NH(IX,IY)-1
DO 100 L=L,LEND
I=LISTH(L)
QX=X-XC(I)
QY=Y-YC(I)
QXSQ=QX*QX
QYSQ=QY*QY
FACTOR=PXX(I)*QXSQ+PYX(I)*QYSQ+PXY(I)*QXY
1F(FACTOR.LT.-3) GO TO 100
HT=PEAK(I)*EXP(FACTOR)
1F(HT.LE.ZMAX) GO TO 100

```

```

2 MAX=HT
100 CONTINUE
150 TMAX=ZMAX
END

```

```
C SUBROUTINE STOCH(I,I,RANGE,A)
```

```

C SUBROUTINE STOCH DETERMINES THE ATTRITION COEFFICIENTS WHEN
C A USER HAS SELECTED A STOCHASTIC ATTRITION OPTION. THE CALCULATION
C IS A FUNCTION OF THE ORIGINAL STOCHASTICALLY DETERMINED ATTRITION
C COEFFICIENT AS WELL AS A FUNCTION OF RANGE.

```

```

COMMON /GRP6/ ALPHA(6),
COMMON /GRP3/ NBUINRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
1DIR(3,200),AVSP,ISPD,LOST(6,6),VIFRA,VISFRB,SIZETK,
1USTAT(6,6),INF(6,6),SRFDISMAX,
1SIZETW(6,6),VIFR(6,6),SRFDISMAX,
1NLOSSC(6,6),VIFR(6,6),SRFDISMAX,
1PTT(3,2),RFPOA(6,6),APOA(6,6),LOA(6,6),NA(6,6),OFL(6,6),
1F(1:EQ:2) GO TO 5003
A=ALPHA(1)*(1.0-RANGE/RMXTW)**2
GO TO 5004
A=ALPHA(1)*(1.0-RANGE/RMXTW)**2
5003 RETURN
5004 RETURN
END

```

```
C SUBROUTINE ETK(I,I,RANGE,T)
```

```

C SUBROUTINE ETK COMPUTES THE EXPECTED TIME FOR A GIVEN FIRER TO
C KILL A GIVEN TARGET. THE CALCULATION IS A FUNCTION OF RANGE,
C TIME OF FLIGHT FOR A ROUND AND HIT AND KILL PROBABILITIES FOR
C THE FIRING WEAPON SYSTEM. IT IS A NUMBER THAT IS USED IN THE
C COMPUTATION OF THE DETERMINISTIC ATTRITION COEFFICIENTS.

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COMMON /GRP2/ TA(2),T1(2),TH(2),TM(2),TF1(2),TF2(2),TF3(2),
1P(2,6),PHH(2,6),PHM(2,6),PKH(2,6),TF(2)
TF(I)=TF1(I)
GOTO 6
5 IF(RANGE.GT.1000.0)*(TF(I)-(TF1(I)*1000.0-RANGE)/1000.0)
GOTO 6
7 IF(RANGE.GT.2000.0)*(TF2(I)-(TF2(I)-TF1(I))*(2000.0-RANGE)/1000.0)
GOTO 6
8 TF(I)=TF3(I)-(TF3(I)-TF2(I))*(3000.0-RANGE)/1000.0
6 J=(RANGE+250.0)/500.0

```

```

IF (J.GT.6) J=6
T=T+(I+T)
1PHM(I,J)*((I-TH(I)+TF(I))/PKH(I,J))+P(I,J)+((TM(I)+TF(I))/PKH(I,J))
RETURN
END

C   SUBROUTINE SORT(I,M)
C   SUBROUTINE SORT IS USED TO SORT TARGETS IN ASCENDING RANGE
C   ORDER. THIS IS USED TO DETERMINE THE PRIORITY OF A TARGET
C   FOR FIRE ALLOCATION.
COMMON /GRPS/ LOT(6,6),ROT(6,6)
DO 19 J=1,M
  IF (ROT(I,J).GE.ROT(I,J)) GOTO 19
21 R=ROT(I,J)
  NN=LOT(I,J)
  RCT(I,J)=ROT(I,M)
  ROT(I,N)=R
  LOT(I,M)=NN
  CONTINUE
19 RETURN
END

C   SUBROUTINE KOVER(Z0,TMACT,SIZET,ZT,S,HTS,ZS,VISFRT)
C   SUBROUTINE KOVER DETERMINES WHAT PORTION OF A PARTICULAR TARGET
C   IS COVERED BY THE TERRAIN BETWEEN THE TARGET AND OBSERVER.
C   THIS NUMBER IS USED IN THE DETECTION AND ATTRITION COMPUTATION.
IF (S.EQ.0.) GO TO 2000
IF (HTS.GE.ZS) GO TO 2050
HEXT=Z0+(HTS-Z0)/S
EVIST=AMAX(HEXT,TMACT)
IF (EVIST.GE.ZT) GO TO 2050
IF (EVIST.LE.ZT-SIZET) RETURN
VIS=(ZT-EVIST)/SIZET
IF (VIS.LT.VISFRT) VISFRT=VIS
RETURN
IF (HTS.LT.Z0) RETURN
2000 VISFRT=0.0
RETURN
END

C   SUBROUTINE LOS(XA,YA,TMICA,SIZEA,XB,YB,TMACB,SIZEB,
-LATOB,LBTGA,VISFRB)

```

```

C SUBROUTINE LOS COMPUTES A PERCENT OF A TARGET VISIBLE TO A
C PARTICULAR OBSERVER, GIVEN THE COORDINATES OF BOTH.
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ EC(100),PXY(100),BASE
COMMON /COVER/ NHILLS(150),CYC(150),CPACK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/ KHT(150),KVN(150),KGRTSH(150),KINT
COMMON /GRID/ LST(54),NHL(54),LSTC(54),NC(54),LIST(400),KTRP
COMMON /GRID/ LSTC(400),KCREP(150),LISTC(100),IEL(100),CS1(100)
COMMON /DIMENSION/ IXG(100),IGY(100),IEL(100),CS2(100)
DATA GSIZE/1000/
DATA GSIZE/1000/
DATA GSIZE/1000/
DATA GSIZE/1000/
DATA GSIZE/1000/
DATA GSIZE/1000/
C SUBROUTINE TO COMPUTE FRACTION VISIBLE FOR OBSERVER TARGET PAIRS
VISFRB=1.
XBA=XB-XA
YEA=YB-YA
IF((XBA.EQ.0).AND.(YBA.EQ.0)) GO TO 510
IF((SIZEA+TMICA.LE.0.) GO TO 510
IF((SIZEB+TMICB.LE.0.) GO TO 510
IF(TMICA.LT.0.) VISFRB=1.0+TMICA/SIZEA
IF(TMICB.LT.0.) VISFRB=1.0+TMICB/SIZEB
ZA=TMACA+TMICA+SIZEA
ZB=TMACB+TMICB+SIZEB
KTREP=KTREP+1
ZBA=ZB-ZA
XBA=XB*XBA
YBASQ=XBA*YBA
XYBA=XBA*YBA
TWOXBA=2.*XBA
TWOYBA=2.*YBA
C COMPUTE GRID SQUARES CROSSED BY A TO B LINE
NGRSQ=0
IF((XBA) 110,95,100
95 XBA=0.1
100 ISGX=-1
XINC=GSIZE/XBA
GO TO 120
110 ISGX=1
XINC=-GSIZE/XBA
120 IF(YBA) 140,125,130
125 YBA=0.1
ISGY=-1
YINC=GSIZE/YBA
GC TO 150
130 ISGY=1
YINC=-GSIZE/YBA
140

```

```

150   IX=1+IF IX(XB/GSIZE)
      IY=1+IF IY(YB/GSIZE)
      XNEXT=GSIZE*(FLOAT(IX)+0.5*(ISGX-1.))
      YNEXT=GSIZE*(FLOAT(IY)+0.5*(ISGY-1.))
      XSTEP=(XB-XNEXT)/XBA
      YSTEP=(YB-YNEXT)/YBA
      NGRSQ=NGRSQ+1
      IGX(NGRSQ)=IX
      IGY(NGRSQ)=IY
      IF((XSTEP-YSTEP)>1) AND (YSTEP-GT.1.) GO TO 200
      IX=IX+ISGX
      IY=IY+ISGY
      XSTEP=XSTEP+XINC
      YSTEP=YSTEP+YINC
      GO TO 160
      GO TO 160
      IX=IX+ISGX
      XSTEP=XSTEP+XINC
      IY=IY+ISGY
      YSTEP=YSTEP+YINC
      KGRS=KGRS+NGRSQ
      C GRID SQUARE LIST NOW COMPLETE IN IGX. IGY WITH NGRSQ ENTRIES
      C NOW FIND WHICH COVER ELLIPSES TOUCH THE A TO B LINE,
      C CHECK ELEVATIONS AT S1 AND S2 FOR EACH SUCH ELLIPSE,
      NELS=0
      CHMAX=0
      IF(NCVELS.EQ.0) GOTO 270
      DO 260 K=i,NGRSQ
      IX=IGX(K)
      IY=IGY(K)
      N=NC(IX,IY)
      IF(N.EQ.0) GO TO 260
      LS=LSTC(IX,IY)
      LEND=LS+N-1
      KELL=KELL+1
      IC=LSTC(L)
      IF(KCREP(IC).EQ.KTREP) GO TO 250
      KCREP(IC)=KTREP
      RX=XA-CXC(IC)
      RY=YA-CYC(IC)
      PXX=CPXX(IC)
      PYY=CPYY(IC)
      PXY=CPXY(IC)
      AA=PPXX*XBA$Q+PPYY*YBA$Q+PPXY*XYBA
      BB=PPXX*TWOYBA*RX+PPY*TWOYBA*RY+PPXY*RX*RY-1.0
      CC=PPXX*RX*RY+PPYY*RY+PPXY*RX*RY-1.0
      ARG=BB*BB-4.0*AA*CC

```

```

IF( ARG .LE. 0.) GO TO 250
SQ = SQR(TARG)
S1 = -(SQ+BB)/(2.0*AA)
S2 = (SQ-BB)/(2.0*AA)
IF(S2 .GE. 0.) GO TO 250
IF(S2 .LE. 0.) GO TO 510
IF(S2 .GE. 1.) GO TO 510
IF(S2 .LT. 1.0) S1 AND S2
CHECK = KINT + 1
CPK = CPEAK(ICI)
XS = XA + S2*XBA
YS = YA + S2*YBA
CALL ELEV(XS,YS,HTS)
HTS = HTS + CPK
ZS = ZA + S2*ZBA
IF(LLATOB.EQ.0) GO TO 210
CALL KOVER(ZA, TMACB, SIZEB, ZB, S2, HTS, ZS, VISFRB)
IF(VISFRB.LE.0.) GO TO 510
210 S = 1 - S2
IF(LLATOA.EQ.0) GO TO 220
CALL KOVER(ZB, TMACA, SIZEA, ZA, S, HTS, ZS, VISFRA)
IF(VISFRA.LE.0.) GO TO 510
220 XS = XA + S1*XBA
YS = YA + S1*YBA
CALL ELEV(XS,YS,HTS)
HTS = HTS + CPK
ZS = ZA + S1*ZBA
IF(LLATOB.EQ.0) GO TO 230
CALL KOVER(ZA, TMACB, SIZEB, ZB, S1, HTS, ZS, VISFRB)
IF(LLATOA.EQ.0.) GO TO 240
S = 1 - S1
CALL KOVER(ZB, TMACA, SIZEA, ZA, S, HTS, ZS, VISFRA)
230 NELS = NELS + 1
IEL(NELS) = IC
CS1(NELS) = S1
CS2(NELS) = S2
IF(CPK.GT.CHTMAX) CHTMAX=CPK
250 CONTINUE
260 CALL ELLIPSES CHECKED
C NOW START ON THE HILLS
270 DO 600 K=1,NGRSQ
IX={GX{K}
IY={GY{K}

```

```

IF(NHL(IX,IY).EQ.0) GO TO 600
LS=LIST(LS+NHL(IX,IY)-1
DO 500 L=LS,LEND
I=LISTH(L)
IF(KHREP(I).EQ.KTREP) GO TO 500
C PROCESSING FOR HILL I STARTS HERE
K=K+1
C COMPUTE W = TOP OF THIS HILL ALONG O-T LINE
C
TRX=XA-XC(1)
TRY=YA-YC(1)
TPXX=PX(1)
TPYY=PY(1)
TPXY=PYX(1)
FQ=TPXX*XB*TPXY*TRY+TPXY*(TRX*YBA+TRY*XBA)
GQ=TPXX*XBASQ+TPYY*YBASQ+TPXY*XYBA
IF(GQ.EQ.0) GO TO 500
W=-FQ/(2.*GQ)
IF(LABS(W).GT.5.) GO TO 500
FSQ=FQ*FQ
EQ=TPXX*TRX+TPYY*TRY+TPXY*TRX*TRY
C
POWER=EQ-FSQ/(4.*GQ)
IF(POWER.LT.-3.) GO TO 500
KHW=KHW+1
IF(HHW.LE.BASE) GO TO 500
ZW=ZA+W*ZBA
IF((HW.LT.0.) OR. (W.GT.1.)) GO TO 300
CYHTW=0.*GE.
IF(NELS.EQ.0) GO TO 300
DO 280 M=1,NELS
IF((CS1(M).GE.W).OR. (CS2(M).LE.W)) GO TO 280
IC=IEL(M)
IF(CVHTW.LT.CPEAK(IC)) CVHTW=CPEAK(IC)
CONTINUE
300 IF((HHW+CVHTW).GE.ZW) GO TO 510
IF("WE GET TO HERE THEN NEED TO FIND LOWEST SIGHT LINE OVER HILL
C NEWTON ITERATION A TO B GIVING VISFRB
IF(LATOB.EQ.0) GO TO 400
KV=KV+1
V=W
HHV=HHW
NC=0
GRA17700
GRA17710
GRA17720
GRA17730
GRA17740
GRA17750
GRA17760
GRA17770
GRA17780
GRA17790
GRA17800
GRA17810
GRA17820
GRA17830
GRA17840
GRA17850
GRA17860
GRA17870
GRA17880
GRA17890
GRA17900
GRA17910
GRA17920
GRA17930
GRA17940
GRA17950
GRA17960
GRA17970
GRA17980
GRA17990
GRA18000
GRA18010
GRA18020
GRA18030
GRA18040
GRA18050
GRA18060
GRA18070
GRA18080
GRA18090
GRA18100
GRA18110
GRA18120
GRA18130
GRA18140
GRA18150
GRA18160
GRA18170

```

```

FV=FQ*V
TWOGV=2.*GQ*V
FCNV=ZA+HHV*((TWOGV*V+FV-1.)*
KN=KN+1
FACTOR=(TWOGV*TWOGV+2.)*(GQ+TWOGV*FQ)+FSQ)
DFCNV=HHV*V*FACTOR
IF(ABS(DFCNV).LT.1.E-10) GO TO 350
V=-FCNV/DFCNV
FV=FQ*V
TWOGV=2.*GQ*V
POWER=EQ+FV+GQ*V*V
IF(POWER.LT.-3.) GO TO 400
HHV=PEAK(I)*EXP(POWER)
DHHV=HHV*(FQ+TWOGV)
ELV=ZA+DHHV*V
IF(ABS(HHV-ELV).LT.1.) GO TO 350
NCT=NCT+1
IF(NCT.LT.10) GO TO 330
IF((V.GT.0.) OR .(V.GT.1.)) GO TO 400
CVHTV=0.*EQ GO TO 390
DO 380 M=1,NELS
IF((CS1(M).GE.V).OR.(CS2(M).LE.V)) GO TO 380
IC=IEL(M)
IF(CVHTV.LT.CPEAK(IC)) CVHTV=CPEAK(IC)
CONTINUE
HTV=HHV+CVHTV
ZV=ZA+V*ZBA
CALL KOVER(ZA,TMACB,SIZEB,ZB,V,HTV,ZV,VISFRB)
C NEWTON ITERATION B TO 510
IF(ABS(V).GT.5.) GO TO 400
IF(LBTOA.EQ.0) GO TO 500
KV=KV+1
V=W
VM1=V-1.
HHV=HHW
NCT=0
FV=FQ*V
TWOGV=2.*GQ*V
FCNV=ZB+HHV*((FQ+TWOGV)*VM1-1.)
KN=KN+1
FACTOR=(TWOGV*TWOGV+2.)*(GQ+TWOGV*FQ)+FSQ)
DFCNV=HHV*VM1*FACTOR
IF(ABS(DFCNV).LT.1.E-10) GO TO 450
V=-FCNV/DFCNV
IF(ABS(V).GT.5.) GO TO 500
VM1=V-1.

```

330

430

```

FV=FQ*V
TWOGV=2.*GQ*FV+GQ*V*V
POWER =EQ+LT+-3}*GO TO 500
HHV=PEAK(I)*EXP(POWER)
DHHV=HHV*(FQ+TWOGV)
ELV=ZB+DHHV*VM1
IF (ABS(HHV-ELV) .LT. 1.) GO TO 450
NCT=NCT+1
IF (NCT.LT.10) GO TO 430
450 IF ((V.LT.0.).OR.(V.GT.1.)) GO TO 500
CVHTV=0.
IF (NELS.EQ.0) GO TO 490
DO 480 M=1,NELS
IF ((CS1(M).GE.V).OR.(CS2(M).LE.V)) GO TO 480
IC=IEL(M)
IF (CYHTV.LT.CPEAK(IC)) CYHTV=CPEAK(IC)
CONTINUE
480 HTV=HHV+CYHTV
ZV=ZA+V*ZBA
S=VM1
CALL KOVER(ZB,TM,CA,SIZEA,ZA,S,HTV,ZV,VISFRA)
500 CONTINUE
600 RETURN
510 VISFRB=0.
      RETURN
END

```

AD-A109 689

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
AN OPERATIONAL LANCHESTER-TYPE MODEL OF SMALL-UNIT AMPHIBIOUS O-ETC(IU)
SEP 81 S D PARK

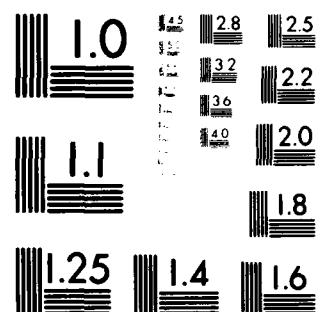
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS

APPENDIX E

PLOTTING PROGRAM FOR TERRAIN CONTOUR LINE

```

// EXEC FRTXCLGP
//FORT,SYSIN DD *
IMPLICIT REAL*4(A-H,O-Z)
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100)
COMMON /HILLS/ SPRD(100),ECC(100),PXX(100),PYY(100)
COMMON /HILLS/ PXY(100),BASE,NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(100)
COMMON /GRID/ KTREP
DIMENSION XXH(25000),YYH(25000)

C   PROGRAM READ IN HILL MASS DATA AND CALCULATE VALUE OF
C   VARIABLE FOR THE ELEVATION SUBROUTINE
C   THE DEFINITION OF DATA-IN VARIABLES SHOULD BE REFERED
C   TO(REF. 5)

PAI=3.14159
L=5
READ(L,7) NHILLS
READ(L,47) BASE
47 FORMAT(F10.4)
7 FORMAT(I6)
17 FORMAT(6F10.3)
DO 50 I=1,NHILLS
READ(L,17) XC(I),YC(I),PEAK(I),ANGH(I),SPRD(I),ECC(I)
50 CONTINUE
READ(L,37)LST
READ(L,37)NHL
READ(L,7)NHTOT
READ(L,37)(LISTH(I),I=1,NHTOT)
37 FORMAT(10I5)
65 DO 100 I=1,NHILLS
ANGLE=ANGH(I)*PAI/180.
SANG=SIN(ANGLE)
CANG=COS(ANGLE)
A=PEAK(I)/(PEAK(I)-50.)
A=ALOG(A)
B=A*ECC(I)**2
SPD=SPRD(I)**2
PXX(I)=-(A*CANG*CANG+B*SANG*SANG)/SPD
PYY(I)=-(A*SANG*SANG+B*CANG*CANG)/SPD
PXY(I)=(2.*SANG*CANG*(B-A))/SPD
KHREP(I)=-2147483600
C   ALL VALUES NOW IN METERS ON 0 -- 10,000 GRID
100 CONTINUE
KTREP=-2147483600
C   MAX AND MIN COORDINATES OF THE REAL TERRAIN REQUIRED
C   FOR THE PLOTTER ROUTINE. IN THIS CASE 3X4 KM TERRAIN
C   WILL BE PLOTTED

XMAX=5000.
YMAX=4000.
XMIN=1000.
YMIN=1000.
XXH(1)=1000.
YYH(1)=1000.
XXH(2)=1000.
YYH(2)=4000.
XXH(3)=5000.
YYH(3)=4000.

```

XXH(4)=5000.
YYH(4)=1000.

C C USING THE BISECTION SEARCH METHOD, FIND THE LOCATION
C WHICH HAS A ELEVATION,I.E. 20, 40...ETC.

ME=5
YELTA=20.
XELTA=5.
XEL=1000.
YEL=1000.
YCON=1000
XEND=5000
YEND=4000.
991 CALL ELEV(XEL,YEL,ZNEW)
TELTA=YELTA
NVAL1=IFIX(ZNEW/20.)
717 ZOLC=ZNEW
727 YEL=YEL+YELTA
IF(YEL.LT.YEND) GO TO 777
XEL=XEL+5.
IF(XEL.EQ.XEND) GO TO 333
YEL=YCON
GO TO 991
777 CALL ELEV(XEL,YEL,ZNEW)
NVAL2=IFIX(ZNEW/20.)
IZZ=IABS(NVAL2-NVAL1)
IF(IZZ.GE.1) GO TO 788
NVAL1=NVAL2
GO TO 717
788 KVAL=NVAL2
YRES=YEL
IF(NVAL2.GT.NVAL1) GO TO 630
ZVAL=NVAL1*20.
NK=1
TELTA=YELTA
631 YEL=YEL-TELTA/2.
632 CALL ELEV(XEL,YEL,ZNEW)
IF(ZNEW.LT.ZVAL+0.1.AND.ZNEW.GT.ZVAL-0.1) GO TO 800
IF(NK.GT.4) GO TO 800
ZOLC=ZNEW
TELTA=TELTA/2.
NK=NK+1
IF(ZNEW.LT.ZVAL) GO TO 631
YEL=YEL+TELTA/2.0
GO TO 632

C C CALCULATE INCREASING ELEVATION

630 ZVAL=NVAL2*20.
NK=1
TELTA=YELTA
642 YEL=YEL-TELTA/2.0
643 CALL ELEV(XEL,YEL,ZNEW)
IF(ZNEW.LT.ZVAL+0.1.AND.ZNEW.GT.ZVAL-0.1) GO TO 800
IF(NK.GT.4) GO TO 800
ZOLC=ZNEW
TELTA=TELTA/2.0
NK=NK+1
IF(ZNEW.GT.ZVAL) GO TO 642
YEL=YEL+TELTA/2.0
GO TO 643

C C COLLECT ELEVATION COOR INATE DATA WHICH IS WANTED TO BE
C PLOTTED.

C 800 IF(ZVAL.LT.20.) GO TO 189

```

IF(ZVAL.GT.140.) GO TO 189
IF(ZVAL.NE.20.AND.ZVAL.LT.100.) GO TO 189
XXH(ME)=XEL
YYH(ME)=YEL
ME=ME+1
189 NVAL1=KVAL
YEL=YRES
GO TO 727
333 NP=ME-1
CALL PLOTG(XXH,YYH,NP,1,0,75,'X-AXIS LABEL',12,
1 'Y-AXIS LABEL',12,XMIN,XMAX,YMIN,YMAX,8.,6.)
CALL PLOT(0.,0.,999)
STOP
END
SUBROUTINE ELEV(X,Y,TMAC)

C COMPUTE THE ELEVATION FOR A GIVEN X,Y COORDINATE
IMPLICIT REAL*4(A-H,O-Z)
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100)
COMMON /HILLS/ SPRD(100),ECC(100),PXX(100),PYY(100)
COMMON /HILLS/ PXY(100),BASE,NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(100),KHREP(100)
COMMON /GRID/ KTREP
DATA GSIZ/E/1000./
ZMAX=BASE
IX=1+IFIX(X/GSIZ)
IY=1+IFIX(Y/GSIZ)
IF(NHL(IX,IY).EQ.0) GO TO 150
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY)-1
DO 100 L=LS,LEND
I=LISTH(L)
QX=X-XC(I)
QY=Y-YC(I)
QXSQ=QX*QX
QYSQ=QY*QY
CXY=QX*QY
FACTOR=PXX(I)*QXSQ+PYY(I)*QYSQ+PXY(I)*QXY
IF(FACTOR.LT.-3.) GO TO 100
HT=PEAK(I)*EXP(FACTOR)
IF(HT.LE.ZMAX) GO TO 100
ZMAX=HT
100 CONTINUE
150 TMAC=ZMAX
RETURN
END

```

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