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SATELLITE-BORNE 'NON-DOD SENSORS' FOR TERRESTRIAL OBSERVATIONS. (U)

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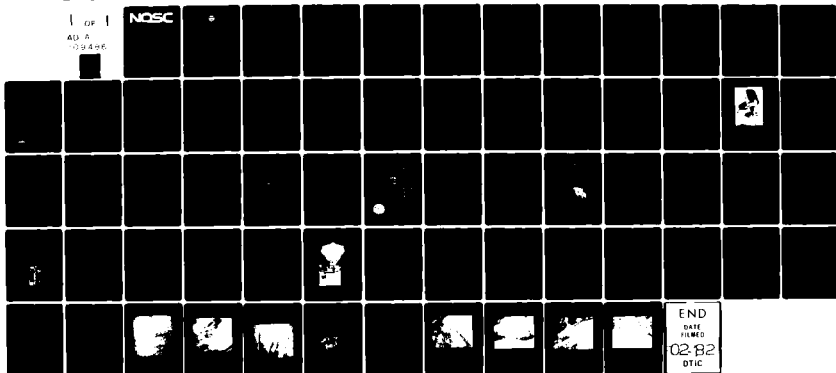
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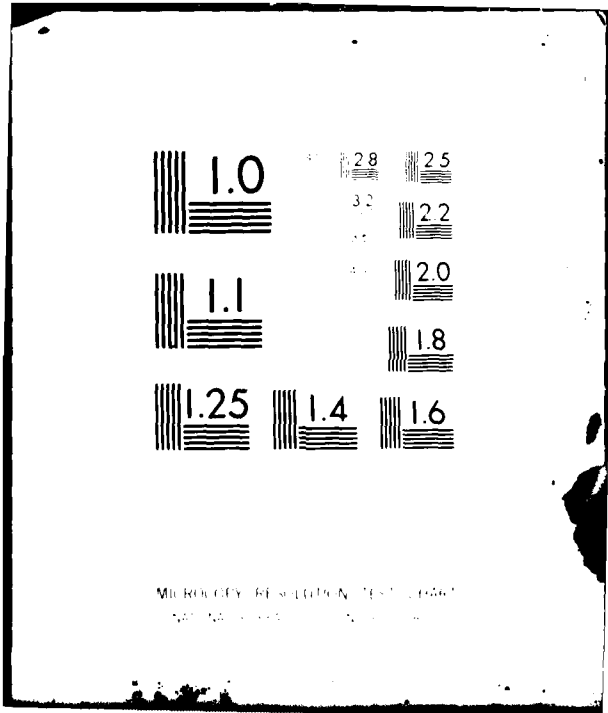
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SATELLITE-BORNE "NON-DoD SENSORS" FOR TERRESTRIAL OBSERVATIONS

H.M. Wight

August 1981

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AN ACTIVITY OF THE NAVAL MATERIAL COMMAND

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HL BLOOD
Technical Director

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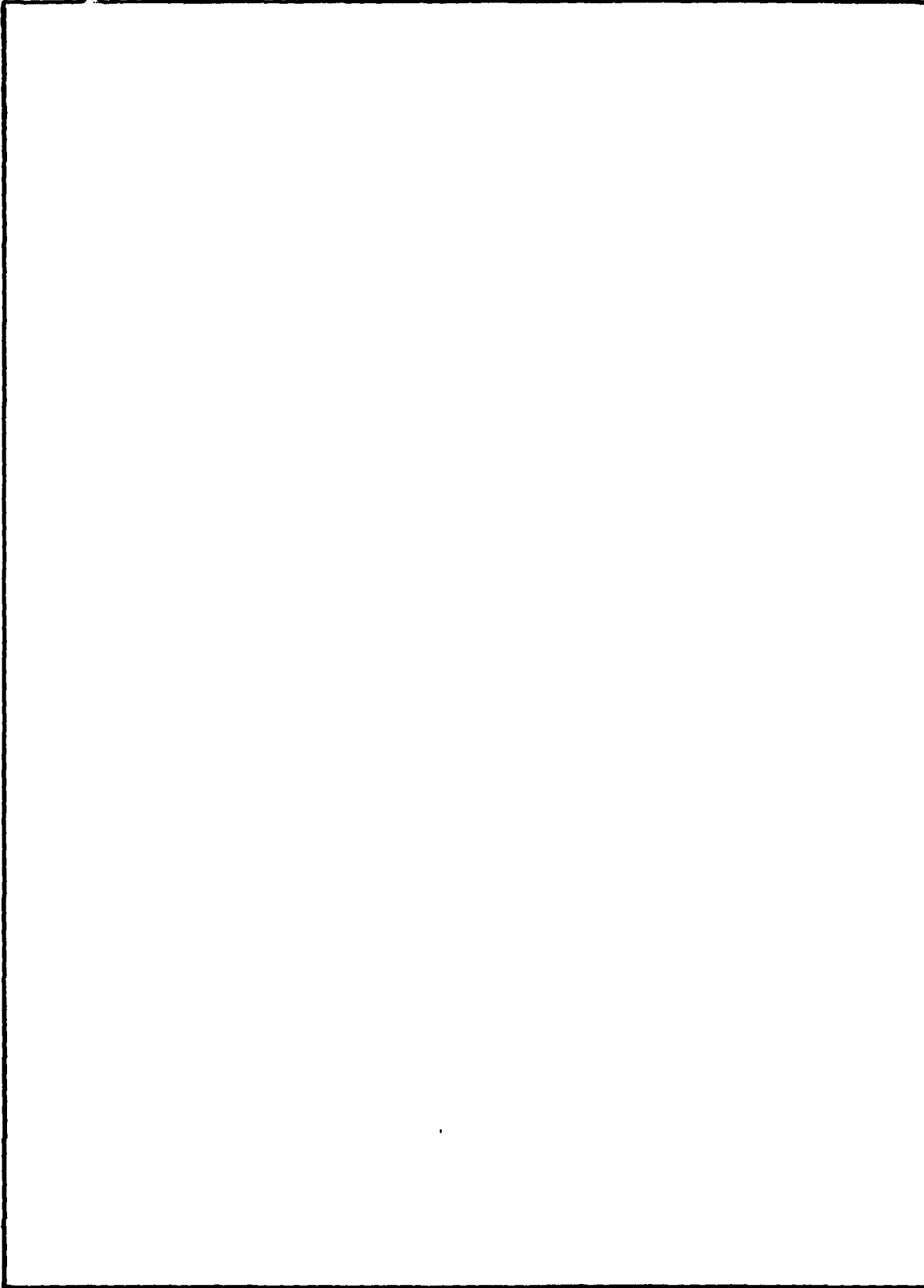
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EXECUTIVE SUMMARY

This is a summary review that was made of satellite-borne "non-DoD sensors" used for terrestrial observations. The term "non-DoD sensors" refers to "civil" (as contrasted with "military") remote sensing systems. The civil satellite-borne sensing systems were developed for the most part by NASA and are employed "operationally" by NOAA/NESS.

An ultimate goal (of the preliminary, initial effort) will be the identification of promising civil sensors, experience and associated technology which could be utilized profitably by the U.S. Navy in the area of ocean surveillance. Summary information is presented concerning the NIMBUS, LANDSAT, TIROS and GOES programs. Satellite-borne sensors for earth viewing - image forming, operating in the visible/IR and microwave portions of the EM spectrum, are also summarized.

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PREFACE

The author makes no claim for originality in this document. Most of the material contained herein was adapted from the many sources listed in the bibliography.

GLOSSARY OF ACRONYMS AND ABBREVIATIONS

A/D	Analog-to-Digital
AF	Audio Frequency, Air Force
AFB	Air Force Base
AM	Amplitude Modulation, Ante Meridian
APL	Applied Physics Laboratory
APT	Automatic Picture Transmission
AVCS	Advanced Vidicon Camera System
AVHRR	Advanced Very High Resolution Radiometer
BCD	Binary Coded Decimal
bps	Bits per second
°C	Degrees Centigrade
CCD	Charged Coupled Device
CDHS	Communications and Data Handling Subsystem
CDIU	Command and Data Interface Unit
CID	Charge Injection Device
cm	Centimeter
CO ₂	Carbon Dioxide
CRT	Cathode Ray Tube
CZCS	Coastal Zone Color Scanner
D/A	Digital-to-Analog
dB	Decibel
DCS	Data Collection System
DEMUX	Demultiplex
DIP	Digital Information Processor
DMSP	Defense Meteorological Satellite Program
DoD	Department of Defense
DPS	Data Processing System
EM	Electromagnetic
ERBE	Earth Radiation Budget Experiment
EROS	Earth Resources Observation System
ERTS	Earth Resources Technology Satellite
ESA	European Space Agency
ESS	Environmental Satellite Survey
ESSA	Environmental Sciences Services Administration
ETR	Eastern Test Range (Cape Canaveral, Florida)

FDM	Frequency Division Multiplex
FIR	Far IR
FM	Frequency Modulation
FNOC	Fleet Numerical Oceanographic Center
FNWC	Fleet Numerical Weather Central (Currently, FNOC)
FOV	Field of View
FSK	Frequency Shift Keying
GARP	Global Atmospheric Research Program
GE	General Electric Company
GHz	Gigahertz (10^9 cycles/second)
GOES	Geostationary Operational Environmental Satellite
GSFC	Goddard Space Flight Center (Greenbelt, Maryland)
HAC	Hughes Aircraft Company
HF	High Frequency
(Hg Cd) Te	Mercury Cadmium Telluride
HIRS	High Resolution Infrared Radiation Sounder
HRPT	High Resolution Picture Transmission
Hz	Hertz (cycles per second)
IEEE	Institute of Electrical and Electronic Engineers
I/F	Interface
IFOV	Instantaneous Field of View
InSb	Indium Antimonide
I/O	Input/Output
ips	Inches per second
IR	Infrared
ITOS	Improved TIROS Operational System
JPL	Jet Propulsion Laboratory
°K	Degrees Kelvin
kbps	Kilobits per second
kHz	Kilohertz (10^3 cycles/second)
kms	Kilometers
LANDSAT	Land Satellite
LaRC	Langley Research Center (Hampton, Virginia)

LIDAR	Light Detection and Ranging
LIMS	LIMB IR Monitoring of the Stratosphere
LOS	Line-of-Sight
L/V	Launch Vehicle
MLA	Multispectral Linear Array
mm	Millimeter
MOS	Metal Oxide Silicon
mrad	Milliradian
MS	Microwave Scatterometer
ms	Millisecond
MSS	Multispectral Scanner
MUX	Multiplexer
NASA	National Aeronautics and Space Administration
NESS	National Environmental Satellite Service
NETD or	
NEΔ T	Noise-Equivalent Temperature Difference
NIMBUS	Program Named for Rain Cloud (from the Latin)
NIR	Near IR
nm	Nautical Mile or Nanometer (10^{-9} cm)
NOAA	National Oceanic and Atmospheric Administration
NOSS	National Oceanic Satellite Service
PAM	Phase Amplitude Modulation
PCM	Pulse Code Modulation
PFM	Pulse Frequency Modulation
Pixel	Picture Element
PM	Phase Modulation, Post Meridian
PMEL	Pacific Marine Environmental Laboratory (Seattle, Washington)
PPS	Pulses Per Second
PSK	Phase Shift Keying
Rad	Radian
Radar	Radio Detection and Ranging
RBV	Return Beam Vidicon
RCA	Radio Corporation of America
RF	Radio Frequency

SAMS	Stratospheric and Mesospheric Sounder (Experiment) (Currently USAF Space Div.)
SAMSO	Space and Missile System Organization
SBUV/TON	Solar Backscatter Ultraviolet/Total Ozone Mapping Spectrometer (Experiment)
SAR	Synthetic Aperture Radar
SBRC	Santa Barbara Research Center (Part of HAC)
SEM	Space Environment Monitor
SEMS	Space Environmental Monitor System
SIO	Scripps Institution of Oceanography
SIRS	Satellite IR Spectrometer
SMIRR	Shuttle Multispectral IR Reflectance Radiometer
SMMR	Scanning Multichannel Microwave Radiometer
SNR	Signal-to-Noise Ratio
SOSS	Satellite Ocean Surveillance System
SSU	Stratospheric Sounder Unit
SWIR	Short Wavelength IR
THIR	Temperature and Humidity IR Radiometer
TIP	TIROS Information Processor
TIROS	Television IR Observatory Satellite
TM	Thematic Mapper
TOVS	Tiros Operational Vertical Sounder
TV	Television
TWERLE	Tropical Wind, Energy Conversion and Reference Level Experiment
UCSD	University of California at San Diego
UHF	Ultra-High Frequency
UV	Ultraviolet
VAS	Visible and IR Spin Scan Radiometer and Atmospheric Sounder
VHF	Very High Frequency
VIP	Versatile Information Processor
W	Watts
$W_{cm^{-2}}$	Watts per square centimeter
$W_{m^{-2}}$	Watts per square meter
WTR	Western Test Range, Vandenberg AFB, California
WWW	World Weather Watch
μ	Micron (10^{-6} meters)
μm	Micrometer (10^{-6} meters)
λ	Wavelength

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1.0 INTRODUCTORY COMMENTS

This document presents an initial survey and review of civil, i.e., *non-DoD sensor systems*, aboard satellites for remote sensing of the earth's surface. The sensors involved (multi-spectral visible/IR radiometric scanners, multichannel microwave radiometric scanners and synthetic aperture radar) were developed initially by NASA (or under its direct sponsorship) and utilized operationally by NOAA/NESS.

The ultimate goal of the present effort is to assess and identify the possible benefits for the U.S. Navy in the area of technology transfer based on civil remote sensing system experience. Specifically such technology transfer would be directed toward aiding in the accomplishment of the U.S. Navy's satellite ocean surveillance missions.

Non-DoD satellite-borne earth sensing systems primarily have emphasized image mapping of the earth's surface and the generation of large scale synoptic meteorological data (e.g., cloud cover associated with storm fronts). LANDSAT and SEASAT-A sensors are of particular interest in the context of the present review.

The basic difference between DoD and non-DoD remote sensing missions has influenced the somewhat divergent development trends for sensor systems in the two domains (military vs civil). DoD remote sensing systems usually have required rapid detection, localization, classification and identification of potentially hostile threat targets (missiles, aircraft, surface naval ships, etc.), often under poor weather conditions on a 24-hour per day basis. Civil applications usually do not require such a rapid "real-time" response for the processing and imaging of phenomena on the earth's surface. Many of the civil data acquired are processed on a relatively leisurely basis and then archived for future use. The daily acquisition data rate generated by the LANDSAT MSS (multispectral scanner) is very large, of the order of 10^{10} bits. The resolution size for MSS images is roughly 80m. Many satellite generated meteorological pictures have a resolution size of several km (such a large resolution gain size would very likely preclude classification of a military platform of interest).

For the readers' benefit, the ultimate goal of this report and potential follow-on work is illustrated in Figure 1. Civil applications involving remote sensing of the earth from satellites include oceanography, meteorology, agriculture and forestry, geology, geodesy, hydrology, large scale pollution monitoring, ecology and land use, etc.

Remote sensing from satellites has reached such a state of maturity that it is currently treated in university courses (e.g., UCSD Extension Course No. 823.4 winter quarter, titled "Land and Sea Applications of Remote Sensing from Satellites").

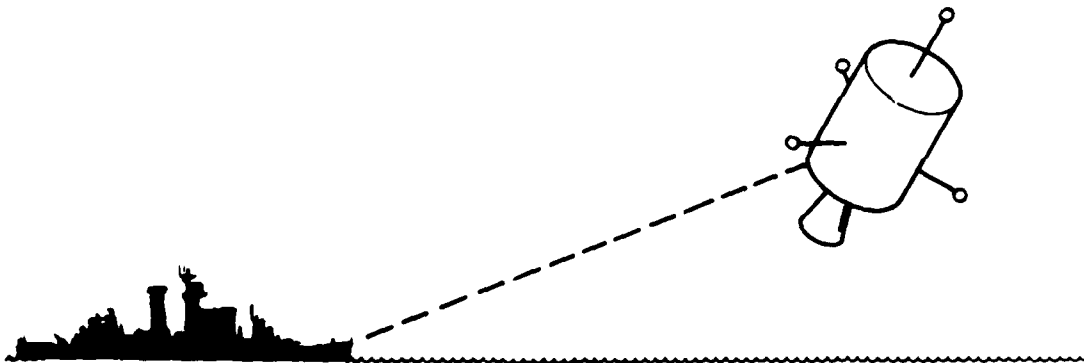


Figure 1. Ocean surveillance by remote sensing.

2.0 BACKGROUND INFORMATION

The remote sensors of interest in the present survey have been carried aboard spacecraft satellites launched for the NIMBUS, LANDSAT, TIROS and GOES projects. The National Aeronautics and Space Administration (NASA) R&D projects are managed by NASA's Office of Space and Terrestrial Applications. Project management is centered in NASA GSFC (Goddard Space Flight Center) in Greenbelt, Maryland. Certain follow-on operational satellite systems, evolving from the original NASA R&D efforts (such as TIROS and GOES), are managed by NOAA/NESS (National Oceanic and Atmospheric Agency/National Environmental Satellite System) which is headquartered in Suitland, Maryland. NASA and NOAA/NESS have had a close working relationship over the past 20 years. The operational responsibility for certain systems, such as LANDSAT, has remained with NASA.

2.1 NIMBUS

The NIMBUS (Latin for "rain cloud") program originated at NASA in the early 1960s as a series of R&D earth-sensing spacecraft and associated sensor systems. NIMBUS has served in the role of a test bed for many of the sensors later flown on TIROS, GOES, DMSP and SEASAT satellites. The space division of the General Electric Company (Valley Forge, Pennsylvania) has been the prime contractor for the NIMBUS program.

The general objectives of the NIMBUS program were to:

1. Develop advanced passive radiometric and spectrometric sensors for daily global surveillance of the earth's atmosphere to provide a data base for long-range weather forecasting
2. Develop and evaluate new active and passive sensors for sounding the earth's atmosphere and mapping both land and water surface characteristics
3. Develop advanced space technology and ground techniques for meteorological and earth-observational spacecraft
4. Develop new techniques and knowledge useful for the exploration of other planetary atmospheres
5. Participate in global observation programs (World Weather Watch) by expanding daily global weather observation capability
6. Provide a supplemental source of operational meteorological data

Seven NIMBUS spacecraft were launched during the course of the program. They were:

- NIMBUS-1 August 1964
- NIMBUS-2 May 1966
- NIMBUS-3 April 1969
- NIMBUS-4 April 1970
- NIMBUS-5 December 1972
- NIMBUS-6 June 1975
- NIMBUS-7 September 1978

All of the above launches were in polar orbit from NASA's Western Test Range (Vandenberg AFB, California).

During the evolution of the program the sensor/data telemetering system payload gradually increased from 100 pounds (NIMBUS-1) to roughly 600 pounds (NIMBUS-7). Table 1 summarizes the various experiments and associated sensors flown during the NIMBUS program.

Details of the final NIMBUS spacecraft, NIMBUS-7, and its sensor package are summarized below. NIMBUS-7 data products and their users are summarized in Table 2; Figure 2 depicts the NIMBUS-7 spacecraft. NIMBUS-7 represented a \$79M effort.

NIMBUS-7 mission objectives were to:

1. Provide additional and new meteorological data in support of the Global Atmospheric Research Program (GARP)
 - a. Earth radiation budget; solar inputs and earth reflected
 - b. Global monitor of gases and temperature in stratosphere, within troposphere and mesospheric regions
 - c. Measurement of aerosol atmospheric contamination
2. Provide new and additional oceanographic data, relating to:
 - a. Chlorophyll concentration
 - b. Sediment distribution
 - c. Salinity concentration via Gelbstoffe determination
 - d. Coastal and open water temperature

Sensor	Film and Tape Output Products	Scientific Parameters	Applications	Users
ERB	Daily, monthly and seasonal world grids Monthly and seasonal contour maps Zonal statistics	Earth fluxes Solar fluxes Zonal insolation	Climatology Ocean/atmosphere dynamics Weather modeling Terrestrial reflectance studies	GSFC, NOAA, LaRC CSU Drexel U of C (Dava) Epply Lab Cal Tech
SMR	Orbital Observations Bi-daily and monthly color contour maps	SEA/ICE parameters Ocean surface conditions Atmospheric conditions Land parameters Glacial features	Ocean dynamics Ice dynamics Ocean/atmosphere interactions Cryospheric dynamics Climatology and weather modeling	GSFC, MIT, U of Wash. NOAA, JPL U.K., Switzerland Denmark Canada
SAM-II	Daily aerosol profiles Seasonal and annual contour maps and atmospheric cross sections	Aerosol backscatter profiles Optical Properties of stratospheric aerosols	Atmospheric sinks Earth radiation budget studies Aerosol injection dynamics	LaRC, U of Wyo. NCAR, SRI, U of Ariz. NOAA
LIMS	Daily atmospheric profile Daily, monthly and seasonal contour maps and atmospheric cross sections	Gas concentrations and temperature profiles in the stratosphere	Atmospheric pollution monitoring Photo-chemical studies Atmospheric gas dynamics Climatology	LaRC, NCAR, NOAA Drexel, U of Wash, JPL UK France
SAMS	Daily atmospheric profile Daily, monthly, and seasonal contour maps and atmospheric cross sections	Gas concentrations and temperature profiles in the stratosphere and mesosphere	Atmospheric pollution monitoring Photo-chemical studies Atmospheric gas dynamics Climatology Wind dynamics	Oxford GSFC LaRC Drexel NCAR
SBUV/TOMS	Daily profiles of O ₃ Daily, monthly and seasonal contour maps Solar spectra Zonal O ₃ statistics	O ₃ profiles Total atmospheric O ₃ Solar irradiances Terrestrial radiances	O ₃ dynamics/modeling Climatology and meteorology O ₃ solar relationships	GSFC, NOAA, MIT, CDC, U of Fla. NSF, LaRC Lashford, Oxford Cal Tech Canada
CZCS	2-minute images	Temperature Spectral radiances Chlorophyll Sediment	Geodynamics of coastal regions Chemical and thermal pollution studies Fishery resources Deep ocean monitoring OH spill monitoring	GSFC, NOAA, U of Cal (Davis) U of Fla, AMES Tex A&M EURASEP
THIR	Daily montages of temperature	Surface temperature Cloud top temperature	Effects of cloudiness on other Nimbus-6 instruments data	All sensors

Table 2. NIMBUS-7 data products and users.

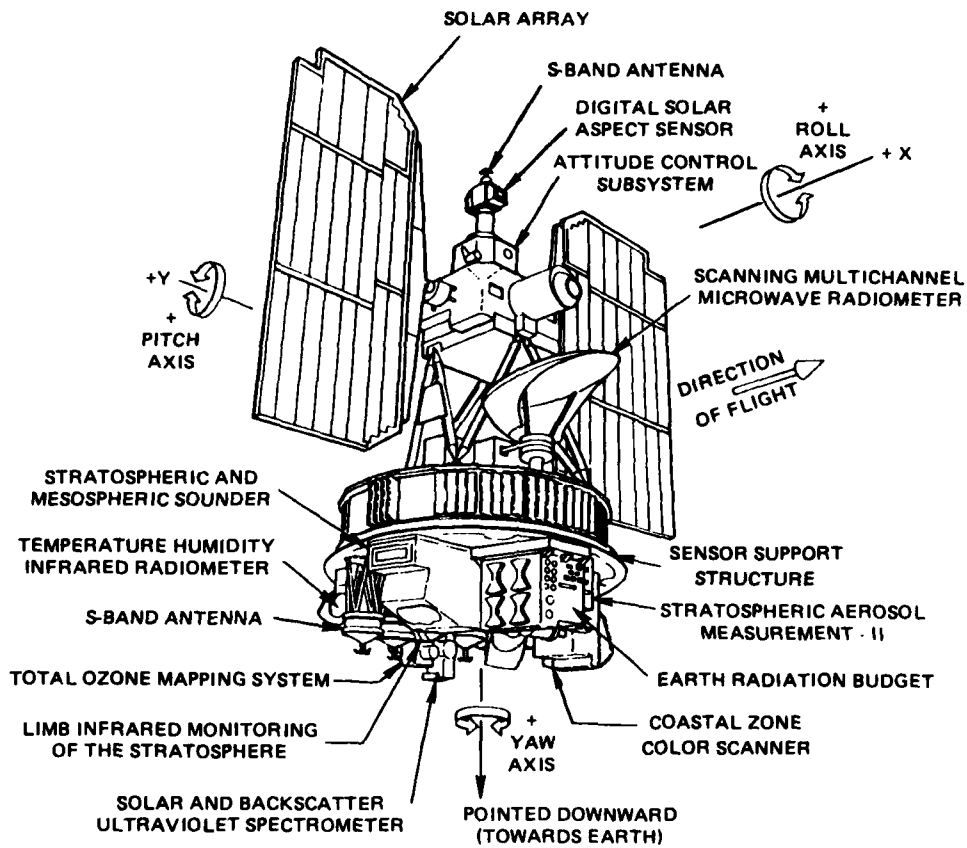


Figure 2. NIMBUS-7 spacecraft.

3. Provide additional and continued earth surface sensing capability related to:
 - a. Cloud cover
 - b. Cloud-land-ocean temperature mapping
 - c. Earth IR radiation measurements

The spacecraft operated in a near polar orbit at an altitude of 955 kms, with an orbital period of roughly 104 minutes. The longitudinal separation (at the equator) for successive orbits was 26° or approximately 160 nms. The system operating goal was one year in orbit.

The NIMBUS-7 spacecraft weighs 2123 pounds and has a configuration similar to an ocean buoy. It is 10 feet tall, 5 feet in diameter at the base, and 13 feet wide with the solar paddles fully extended. The sensor mount that forms the satellite base houses the electronics equipment and battery modules. The lower surface of the torus provides mounting space for sensors and antennas. A boxbeam structure mounted within the center of the torus provides support for the larger sensor experiments. The control housing unit is located on top of the spacecraft and above this unit are the sun sensors, horizon scanners and a command antenna.

The spacecraft power subsystem consists of solar arrays, nickel-cadmium batteries, charge and discharge regulators and voltage regulators to operate all spacecraft support subsystems and to provide maximum power for the instrument payload.

The orbit average regulated power provided by the observatory power subsystem is approximately 300 watts, of which 123 watts are allocated to the spacecraft subsystems. If all the instruments were on full-time, the power requirements would exceed the available supply. Because of this power limitation, the subsystems will operate for approximately the percentage of time given in Table 3. Only the temperature and humidity IR radiometer (THIR) is scheduled to operate on a full-time basis. This schedule is in accordance with the specific objectives of the NIMBUS project.

Instrument	Power Requirements, watts	Operational Mode, %
CZCS	11.4	30
ERB	36.3	80
LIMS	24.5	80
SAM II	0.8	8
SAMS	23.0	80
SBUV/TOMS	20.0	80
SMMR	61.6	50
THIR	8.5	100
Subsystem Total	186.1	
Basic Spacecraft	123.6	
Observatory Total	309.7	

Table 3. Instrument power requirements for the percentage of operational time allotted each sensor.

The NIMBUS-7 communications and data handling subsystem (CDHS) is composed of the S-band communications system and tape recorder subsystem and handles all spacecraft information flow. The S-band communication system includes the S-band command and telemetry system, the data processing system (DPS) and the command clock. The S-band command and telemetry system consists of two S-band transponders, a command and data interface unit (CDIU), four earth-view antennas, a sky-view antenna and two S-band transmitters (2211 MHz). Commands are transmitted to the observatory by pulse code modulation (PCM), phase-shift keying (PSK)/frequency modulation (FM) and phase modulation (PM) of the assigned 2093.5 MHz S-band uplink carrier. Stored command capability provides for command execution at predetermined times.

Table 4 lists the NIMBUS-7 contractors.

Company	Contribution
<p>Prime Contractor:</p> <p>General Electric Co. Space Systems Space Division Valley Forge, Pennsylvania</p>	<ul style="list-style-type: none"> ● Spacecraft structure and antennas ● Separation and unfold subsystem ● Thermal control subsystem ● Electrical distribution harness ● Electro-mechanical components ● Ground support equipment ● Attitude control system components ● Spacecraft integration and test ● Spacecraft subcontracts management
<p>Contributing Contractors:</p> <p>Gulton Industries Albuquerque, New Mexico</p> <p>Ball Bros. Boulder, Colorado</p> <p>Beckman Instruments Fullerton, California</p> <p>Bendix Corporation Teterboro, New Jersey</p> <p>California Computer Products Anaheim, California</p> <p>Control Data Corporation Philadelphia, Pennsylvania</p> <p>Fairchild Hiller Germantown, Maryland</p> <p>Honeywell Boston, Massachusetts</p> <p>Ithaco Ithaca, New York</p> <p>Jet Propulsion Laboratories Pasadena, California</p> <p>Kearfott Clifton, New Jersey</p> <p>Lear Siegler, Inc. Anaheim, California</p> <p>Ludwig Honold Philadelphia, Pennsylvania</p> <p>Motorola, Inc. Scottsdale, Arizona</p>	<ul style="list-style-type: none"> ● Earth radiation budget ● Coastal zone color scanner ● Solar backscatter ultra-violet energy and total ozone mapping spectrometer ● Pitch and yaw momentum wheels ● Command/clock subsystems ● Interface switching modules ● Ground station computer ● Attitude control system structure ● Attitude control system thermal control louvers ● LIMB infrared monitoring of the stratosphere experiment ● Magnetic moment compensating assembly ● Roll reaction wheel scanner/signal processor ● Control logic box ● Scanning multichannel microwave radiometer experiment ● Rate measuring package gyro (ball bearing) ● Ground station computer ● Flight adapter structure ● S-band transponder

Table 4. NIMBUS-7 contractors.

Company	Contribution
Northrop Corporation Electronics Division Norwood, Massachusetts	<ul style="list-style-type: none"> • Yaw rate gyro • Rate measuring package gyro (gas bearing)
Oxford University, U.K. and Hawke-Siddley Stevenage, Herts SG1 2AS	<ul style="list-style-type: none"> • Stratospheric and mesospheric sounder
Parsons Stockton, California	<ul style="list-style-type: none"> • Solar array assembly
Radio Corporation of America Communications System Div. Camden, New Jersey	<ul style="list-style-type: none"> • Tape recorder
Radio Corporation of America Astro Electronics Division Princeton, New Jersey	<ul style="list-style-type: none"> • Power subsystem (regulator, storage modules)
Rutherford Laboratory Chilton, Didcot Berkshire, England and Elliott Automation Frimley, Camberly Surrey, England	<ul style="list-style-type: none"> • Pressure modulation radiometer experiment
Santa Barbara Research Center Santa Barbara, California	<ul style="list-style-type: none"> • Temperature humidity infrared radiometer
Spectrolab, Inc. Sylmar, California	<ul style="list-style-type: none"> • Solar array substrates
Sperry Gyroscope Great Neck, L.I., New York	<ul style="list-style-type: none"> • Rate measuring package (ball and gas bearing gyros)
Teledyne Los Angeles, California	<ul style="list-style-type: none"> • S-band transmitters
TRW Redondo Beach, California	<ul style="list-style-type: none"> • Attitude control pneumatics Solar array drives
University of Wyoming Laramie, Wyoming	<ul style="list-style-type: none"> • Stratospheric aerosol measurement II

Table 4. (Continued)

2.2 LANDSAT

The LANDSAT program evolved from the earlier ERTS (Earth Resources Technology Satellite) program. The LANDSAT spacecraft and its orbital patterns are quite similar to the previously described NIMBUS-7. The LANDSAT program is managed by NASA's Office of Space and Terrestrial Applications. Actual day-to-day project management is centered at NASA's Goddard Space Flight Center (GSFC). The prime contractor is the GE Space Division. The primary sensor used in LANDSAT-1, -2 and -3 is the MSS (multispectral scanner), which was developed by Santa Barbara Research Corporation of Hughes Aircraft Company (Goleta, California).

A follow-on effort will see the launch of "quasi-operational" LANDSAT D (probably mid-1982) and LANDSAT D' (probably mid-1983). LANDSAT D' will probably carry the Thematic Mapper (TM) which also was developed by Hughes.

The primary goal of LANDSAT is to provide good spectral imaging of surface terrain and accompanying growing vegetation throughout the world. These data are obtained using the MSS. A limited amount of additional "image" data has been obtained in the visible, using the TV camera RBV (Return Beam Vidicon).

A concise history (and projection) of the LANDSAT program status is given in Table 5, while Table 6 provides a summary of LANDSAT operations up to September 1980.

Primary governmental users of the data generated by the MSS are the Department of Agriculture (for crop and forestry assessments) and the U.S. Geological Survey (for determining fault lines and rock characteristics which are useful in petroleum and mineral exploration).

When a fully operational status is obtained by LANDSAT's D and D', the day-to-day operations of the system will be taken over by NOAA/NESS.

Satellite	Launch	Status
LANDSAT-1	July 23, 1972	Ceased data collection January 10, 1978
LANDSAT-2	January 22, 1975	Ceased data collection November 5, 1979
LANDSAT-3	March 5, 1978	In operation
LANDSAT D	Planned for Summer 1982	Under development
LANDSAT D'	Available for launch 6 months after D	Approved

Table 5. LANDSAT program status.

Scenes Acquired (September 1980)	U.S.		Foreign	
	MSS	RBV	MSS	RBV
LANDSAT-1*	149,640	1,546	122,146	144
LANDSAT-2*	151,955	2,289	231,987	542
LANDSAT-3*	49,858	16,754	96,240	56,542

All digital data MSS production initiated 2/1/79

Backlog 3/2/80	5,659 scenes
Current acquisition rate	345 scenes/week (average past 4 weeks)
Current processing rate	621 scenes/week (average past 4 weeks)
Backlog eliminated	8/15/80 date (at present acquisition rate)
Current turnaround time (GSFC)	80% complete within 5 days (February sample)

All digital RBV production 3/31/80

*LANDSAT-1 (Launched 23 July 1972, Shut down 16 January 1978)

LANDSAT-2 (Launched 22 January 1975)

LANDSAT-3 (Launched 15 March 1978)

Table 6. LANDSAT operations - summary.

2.3 TIROS-N/NOAA-A

TIROS-N and its twin NOAA-A are operational weather satellites, managed by NOAA/NESS. These satellites operate in sun-synchronous, near polar, orbits to provide cloud cover, surface, temperature, atmospheric temperature and humidity profiles, etc. These satellites were designed and built by RCA Astro-Electronics in Princeton, New Jersey. NASA funded the development and launch of TIROS-N; NOAA provided the funds to NASA for the procurement and launch of NOAA-A (sometimes designated NOAA-6). Each satellite cost approximately \$20M.

The satellites were launched from NASA's Western Test Range, using ATLAS-F boosters. Each satellite has an estimated design operating life of roughly two years.

Figure 3 depicts TIROS-N. The TIROS-N spacecraft is 12 feet long and six feet wide. Its solar panels have a collecting area of approximately 125 square feet.

Table 7 lists the basic characteristics of TIROS-N/NOAA-A.

Four primary spacecraft instrument systems are aboard these satellites: the Advanced Very High Resolution Radiometer (AVHRR), the TIROS Operational Vertical Sounder (TOVS), the Data Collection System (DCS) and the Space Environment Monitor (SEM).

The AVHRR will provide image data for real-time transmission to both Automatic Picture Transmission (APT) and High Resolution Picture Transmission (HRPT) users and for storage on the spacecraft tape recorders for later playback.

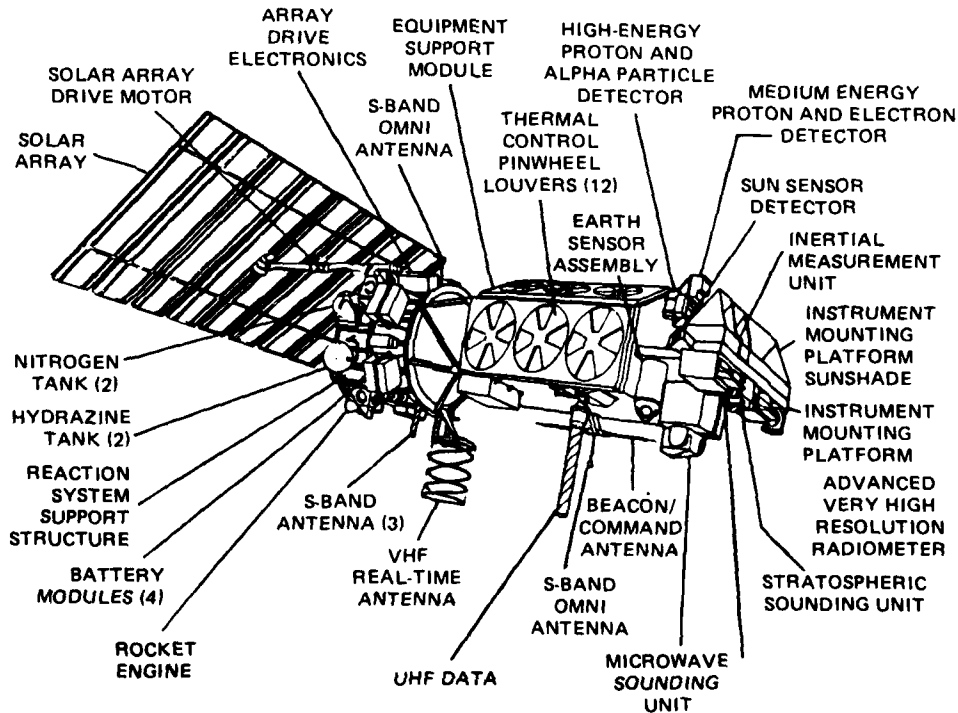


Figure 3. TIROS-N spacecraft.

Spacecraft	:	Total weight (includes expendables)	1421 kg (3127 lb)
Payload	:	Weight including tape recorders	194 kg (427 lb)
	:	Reserved for growth	36.4 kg (80 lb)
Instrument Complement	:	Advanced Very High Resolution Radiometer (AVHRR) High Resolution Infrared Radiation Sounder (HIRS/2) Stratospheric Sounder Unit (SSU) Microwave Sounder Unit (MSU) Data Collection System-ARGOS (DCS) Space Environment Monitor (SEM)	
Spacecraft Size	:	3.71 meters in length (146 in.)	
	:	1.88 meters in diameter (74 in.)	
Solar Array	:	2.37 m × 4.91 m : 11.6 sq m	
	:	(7.8 ft × 16.1 ft : 125 sq ft)	
		420 watts, end of life, at worst solar angle	
Power Requirement	:	Full operation -- 330 watts	
	:	Reserved for growth -- 90 watts	
Attitude Control System	:	0.2° all axes 0.14° determination	
Communications			
Command Link	:	148.56 MHz	
Beacon	:	136.77; 137.77 MHz	
S-Band	:	1698; 1702.5; 1707 MHz	
APT	:	137.50; 137.62 MHz	
DCS (uplink)	:	401.65 MHz	
Data Processing	:	All digital (APT; analog)	
Polar Orbit	:	TIROS 833; NOAA-A 870 km nominal altitudes	
Launch Vehicle	:	Atlas E/F	
Lifetime	:	2 years planned	

Table 7. TIROS-N/NOAA-A summary sheet.

2.4 Geostationary Operational Environmental Satellite (GOES)

The GOES (Geostationary Operational Environmental Satellite) is an operational weather satellite, managed by NOAA/NESS. The technological developments and launches were provided to NOAA by NASA GSFC. The GOES satellites are the source of the nightly satellite weather pictures on TV. The GOES satellites are in geostationary orbits, approximately 19,600 nm above the equator. The "Eastern Bird" (GOES-3) is located above the equator at 75°W longitude and the "Western Bird" (GOES-4) is at 135°W longitude.

To date there have been four successful launches of GOES spacecraft, as shown in Table 8. Each of these spacecraft was launched from NASA's Eastern Test Range (Cape Canaveral, Florida).

Spacecraft	Launch Year	Manufacturer
GOES-1	1975	Ford Aerospace and Communications Corporation, Palo Alto, California
GOES-2	1977	Ford Aerospace and Communications Corporation, Palo Alto, California
GOES-3	1978	Ford Aerospace and Communications Corporation, Palo Alto, California
GOES-4	1980	Hughes Aircraft Company, Space and Communications Group, Fullerton, California

Table 8. GOES spacecraft.

Figure 4 depicts GOES-4. The spacecraft was launched using a DELTA 3914 launch vehicle. GOES-4 has an estimated operating design life of roughly seven years; Table 9 lists its characteristics.

The primary sensor of major interest aboard GOES-4 is VAS (Visible and IR Spin Scan Radiometer and Atmospheric Sounder). This sensor provides cloud and temperature imaging in terms of visible and IR spectra. The combination GOES-3 and GOES-4 provides cloud cover data in the Western Hemisphere between latitudes 60°N and 60°S. Cloud cover data closer to the poles is provided by the TIROS-N/NOAA-A system.

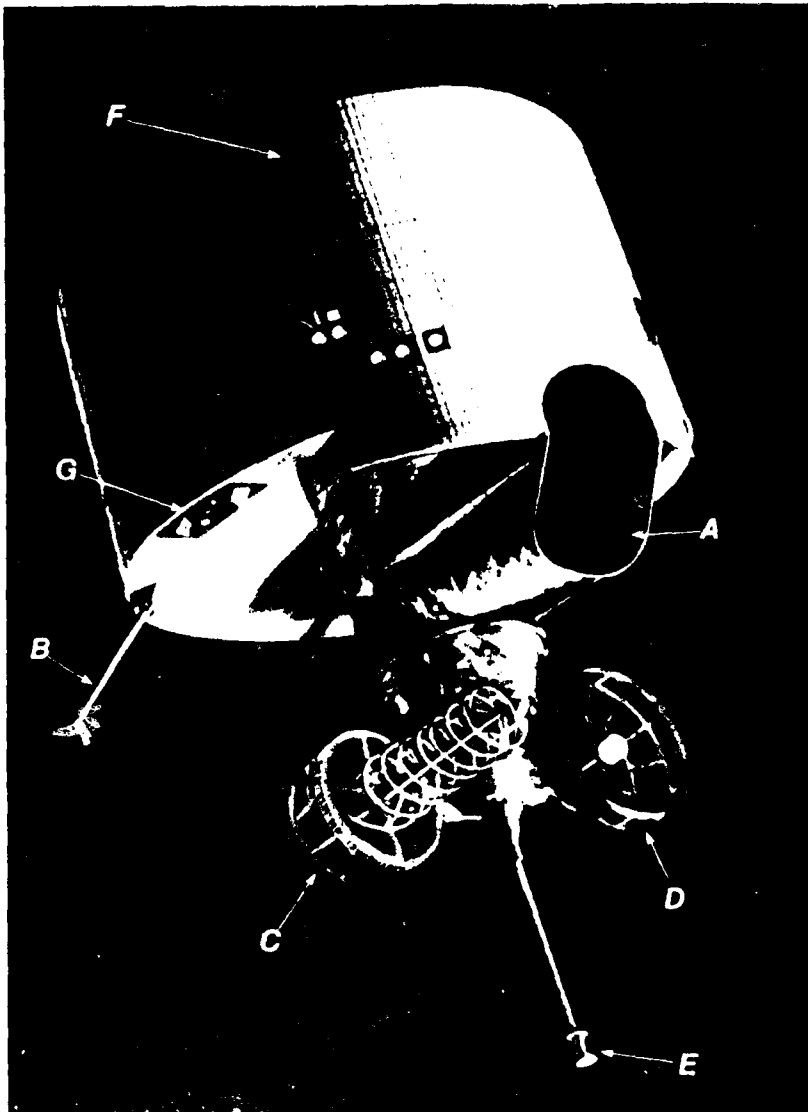


Fig. 1. Turbine engine of the "Molniya" satellite. A - turbine; B - compressor; C - combustion chamber; D - turbine; E - turbine; F - turbine; G - turbine.

Launch Vehicle
 Spacecraft Mass, lb
 Launch (separated spacecraft)
 On station beginning of life
 On station end of life (dry weight)

Delta 3914

1841.0
 874.0
 762.0

Spacecraft Dimensions, in.
 Length along Z-axis

174.3 (with adapter)
 138.7 (without adapter)
 84.5

Diameter

Apogee Motor

Thiokol TE-M 616 derivative

Communications

Coverage at S-band
 Coverage at UHF

Visible earth-western hemisphere

Frequencies

Multifunction Repeater

Receive, MHz

Multifunction/VAS	WEFAX	Trilateration
2029.1 (S VAS)	2033.0	2026.0 2030.2 2032.2
1681.6 (VAS) 1687.1 (S VAS)	1691.0	1684.0 1688.2 1690.2

Transmit, MHz

Frequencies

Receive, MHz

Transmit, MHz

EIRP, dBm

Margins, dB*

G/T, dB/K

Margins, dB

Bandwidth, MHz

MFR	DCPI	DCPR	CDA TM	STDN TM	STDN RNG	STDN/CDA CMD
See above	2034.925 468.850	401.9 1694.5	- 1694.0	- 2214.0	2034.2 2209.086	2034.2 -
56.4	46.2 3.3	35.6 10.0	33.4 6.9	26.6 7.8	13.9 11.4	- -
-17.6	-17.6 7.4	-18.5 6.5	- -	- -	-36.9 3.1	-36.9 3.1
8.2/20	0.2	0.4	0.1	0.1	1.0	0.08

Antennas

S-band (high gain)

UHF

S-band (T&C)

Antenna Pointing, deg

East-west

Parabolic, linear (vertical) polarization - 18.2/18.1 dB peak gain transmit/receive
 Helix, RHCP - 11.7/9.4 dB peak gain transmit/receive
 Bicone-linear (vertical) polarization - 1.0/3.0 dB peak gain transmit/receive

≤ ±0.5 (sun reference)
 ≤ ±0.75 (earth reference)

Attitude Control and Stationkeeping

On-orbit spin to transverse inertia ratio (EOL)

On-orbit spin stabilized

Attitude

N-S stationkeeping

E-W stationkeeping

Spin rate

Transfer Orbit Spin Stabilized

Transfer orbit

Attitude control

Active nutation control moment

Predicted stability margin

Fuel usage

Attitude Determination

Sensors

Accuracy

± 1.13 I_{ZZ}/I_{TEFF}

On-orbit spin rate: 100 rpm

Axial jet control to ± 0.2°

Axial jet control to ± 1.0°

Adjacent pair of radial jets for control to ± 0.5°

Moment pair of radial jets for control to ± 5 rpm

Spin rate 55 rpm

Axial jet control with automatic nutation control. Time constant < 10 sec

3.7 ft-lb

> 1500:1 at threshold (0.2°) (T dedamp/T damp)

1.0 lb (9 orbits)

Earth and sun

< ± 0.1° (on orbit); ± 0.5° (transfer orbit)

Table 9. GOES-4 characteristics.

3.0 SENSORS

The non-DoD satellite-borne sensor systems of potential interest to the Navy's ocean surveillance community can be divided into two general categories: (1) those operating in the visible and IR portions of the electromagnetic spectrum and (2) those in the microwave region.

Sensors operating in the visible and IR domain to be discussed include:

- MSS (multispectral scanner)
- CZCS (coastal zone color scanner)
- AVHRR (advanced very high resolution radiometer)
- VAS (visible and IR spin scan radiometer and atmospheric sounder)
- TM (thematic mapper)
- SMIRR (shuttle multiband visible/IR radiometer)
- MLA (multispectral linear array).

Sensors operating in the microwave domain to be discussed include:

- SAR (synthetic aperture radar)
- MS (microwave scatterometer)
- SMMR (scanning multichannel microwave radiometer).

All of the preceding sensor systems are passive with the exception of SAR. The MSS, CZCS, AVHRR, VAS, SAR and SMMR have all been operated successfully aboard various spacecraft. The TM and SMIRR have undergone limited engineering tests on the ground. The MLA is just entering the conceptual design phase and a "flyable" unit will not be ready until 1989.

3.1 VISIBLE/IR SENSORS

The sensors to be discussed are passive devices, operating in the visible and IR portion of the electromagnetic spectrum. Most utilize reflected solar energy and thus are limited to daylight operations.

3.1.1 COASTAL ZONE COLOR SCANNER (CZCS)

The CZCS has been successfully aboard NIMBUS-7. It was used primarily to determine the nature of suspended particulate matter and chlorophyll in coastal and open ocean waters.

The CZCS is a conventional multi-channel scanning radiometer utilizing a rotating plane mirror at a 45° angle to the optic axis of a Cassegrain telescope. The rotating mirror scans 360°; however, only ±40° of data centered on the spacecraft nadir are collected for ocean color measurements. During the rest of the scan, the instrument acquires a view of deep space and of internal instrument sources for calibration of the various channels. The radiation collected by the telescope is divided into two portions by a dichroic beam splitter. One portion is transmitted to a field stop that is also the entrance aperture of a small polychromator. The radiant energy entering the polychromator is dispersed and reimaged in five wavelengths on five silicon detectors in the focal plane of the polychromator. The portion of the beam reflected off of the dichroic mirror is directed to a cooled mercury cadmium telluride detector sensing in the 10.5 μm to 12.5 μm region. The CZCS utilizes a radiative cooler that cools the mercury cadmium telluride detector to approximately 120° Kelvin during spacecraft flight.

The CZCS scanning system is depicted in Figure 5 while the CZCS device is depicted in Figure 6 and the CZCS optical arrangement is shown in Figure 7. Performance parameters are listed in Table 10 and the CZCS spectral bands/channels in Table 11.

Channels 1-5 depend on reflected sunlight and, therefore, are operable during daylight hours (local time). Channel 6 depends upon thermally radiated energy at the ocean surface and is operable day and night. Radiation detectors for channels 1-5 consist of silicon photodiodes while channel 6 employs a radiatively cooled (HgCd) Te photoconductor. The six channels of digital radiometric data are tape recorded and later transmitted to ground stations using 800 kbps biphasic telemetry at S-band.

3.1.2 MULTISPECTRAL SCANNER (MSS)

The characteristics of the Hughes MSS are summarized in Figure 8. The incoming light is dispersed from a reflecting grating. The MSS utilizes spectral bands in the visible, centered at $0.55 \mu\text{m}$, and $0.65 \mu\text{m}$ and two bands in the near IR, centered at $0.75 \mu\text{m}$ and $0.95 \mu\text{m}$. The detectors are silicon photodiodes.

The MSS depends on the presence of reflected sunlight and, therefore, is operable only during daylight hours (local time). The scan is obtained mechanically by vibrating a mirror transverse to the spacecraft's motion.

The MSS has been flown successfully aboard LANDSAT-1, -2 and -3 and is scheduled for use aboard LANDSAT-D and -D'.

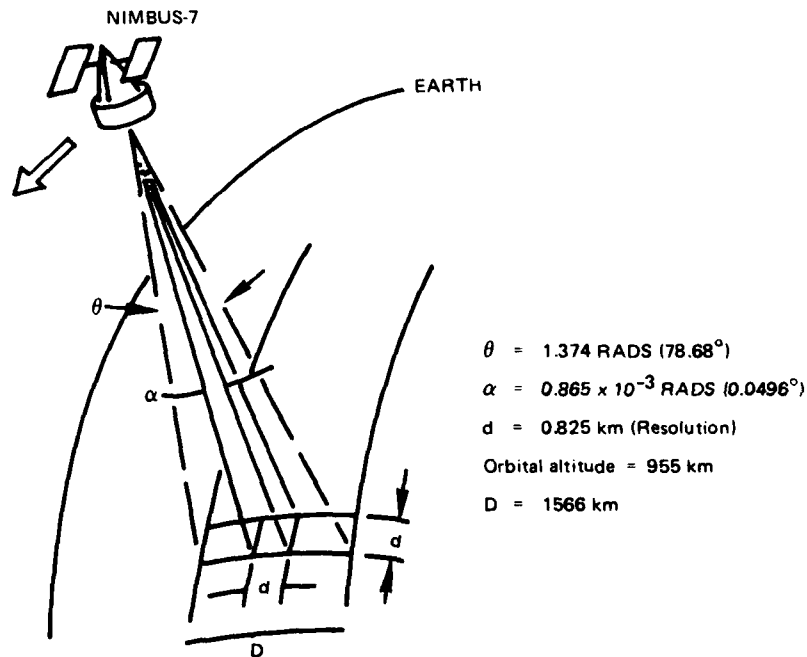


Figure 5. CZCS scanning arrangement and parameters.

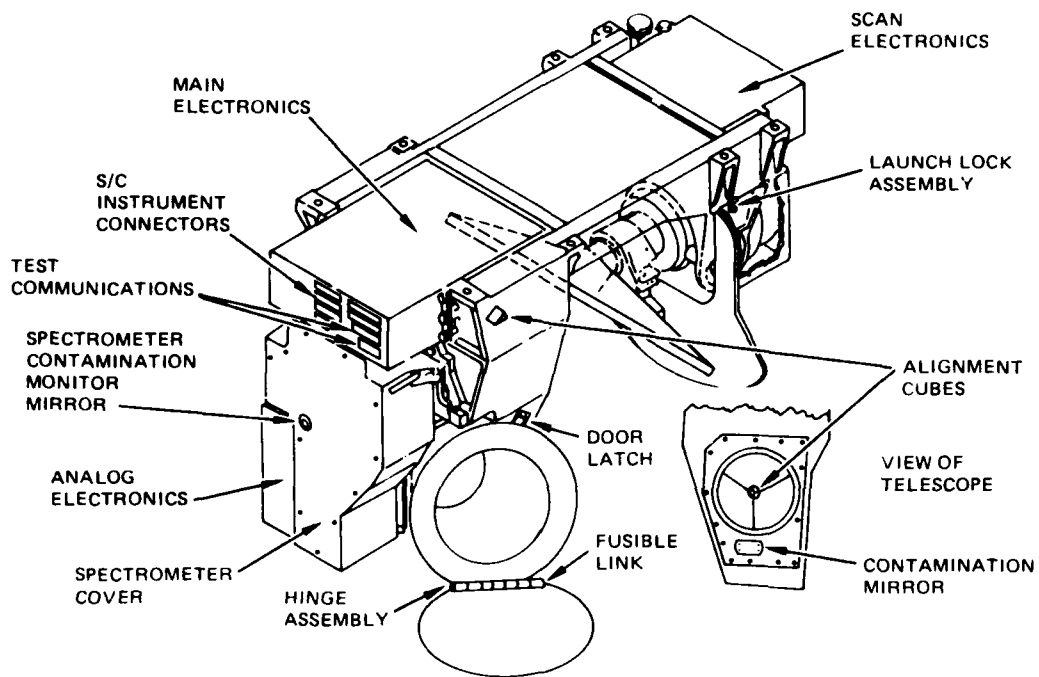


Figure 6. The CZCS.

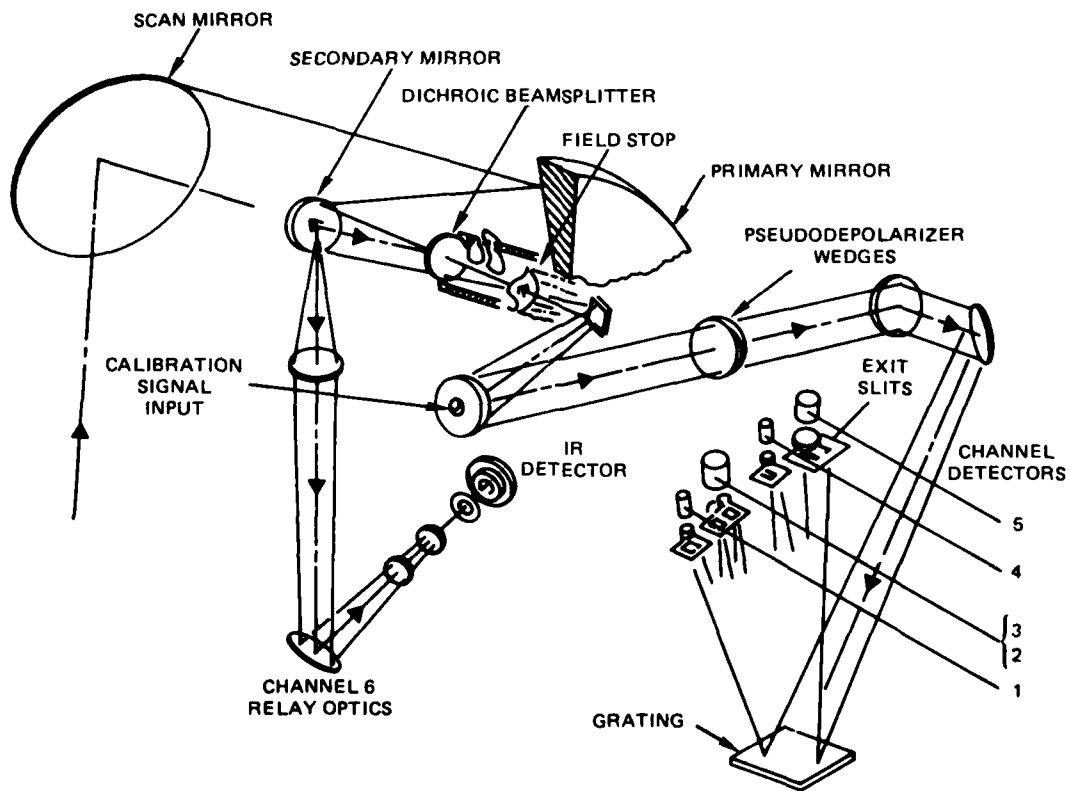


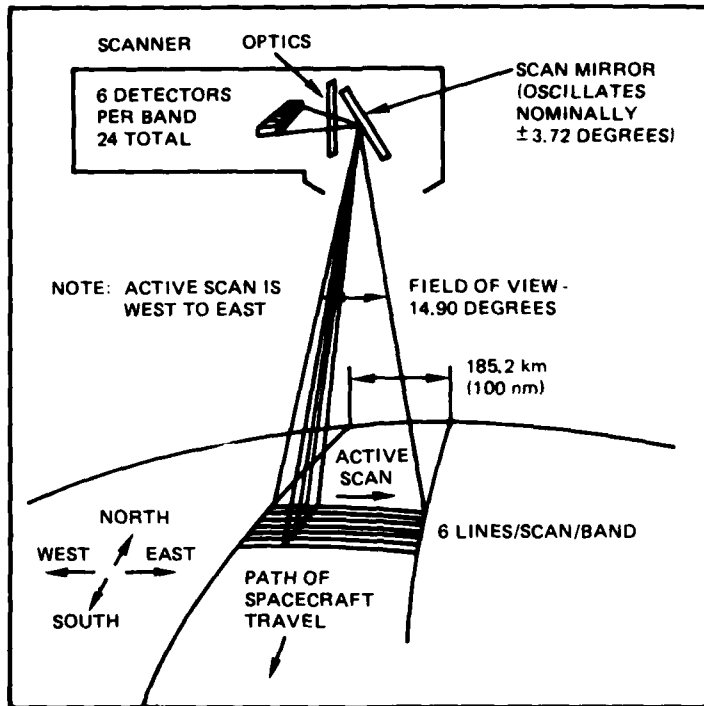
Figure 7. CZCS optics.

Performance Parameters	Channels					
	1	2	3	4	5	6
Scientific observation	Chlorophyll absorption	Chlorophyll correlation	Yellow stuff	Chlorophyll absorption	Surface vegetation	Surface temperature
Center wavelength λ micrometers	0.443 (blue)	0.520 (green)	0.550 (yellow)	0.670 (red)	0.750 (far red)	11.5 (infrared)
Spectral bandwidth $\Delta\lambda$ micrometers	0.433 -- 0.453	0.510 -- 0.530	0.540 -- 0.560	0.660 -- 0.680	0.700 -- 0.800	10.5 -- 12.5
Instantaneous field of view - Spatial resolution	0.865×0.865 Milliradians (0.825×0.825 km at sea level)					
Co-registration at NADIR	< 0.15 Milliradians					
Accuracy of viewing position information at NADIR	< 2.0 Milliradians					
Signal-to-noise ratio (min.) at Radiance input $N < (\text{mW/cm}^2 \cdot \text{STER} \cdot \mu\text{m})$	> 150 at 5.41	> 140 at 3.50	> 125 at 2.86	> 100 at 1.34	> 100 at 10.8	NETD of 0.220°K at 270°K
Consecutive scan overlap	25%					
Modulation transfer function (MFT)	1 at 150 km target size. 0.35 min. at 0.825 km target size					

Table 10. CZCS performance parameters.

Channel No.	Channel Response, μm	Signal-To-Noise Ratio at Specified Radiance	NETD at Specified Temperature
1	.433 - .453	218 @ 5.41 $\text{mW/cm}^2 \cdot \text{STER} \cdot \mu\text{m}$	0.15K @ 270K
2	.510 - .530	209 @ 3.50	
3	.540 - .560	196 @ 2.86	
4	.660 - .680	119 @ 1.34	
5	.700 - .800	244 @ 10.8	
6	10.5 - 12.5		

Table 11. CZCS spectral bands/channel.



- WEIGHT: 144 POUNDS
- SIZE: SCANNER – 24 IN X 35 IN X 16 IN
MULTIPLEXER – 6 IN X 4 IN X 7 IN
- POWER: 75 WATTS MAX. OPERATING
- DATA RATE: 15.06 MBPS AND INCLUDES
 - VIDEO DATA
 - TIME CODE (EVERY OTHER SCAN)
- SPECTRAL BANDS
 - BAND 1: 0.5 TO 0.6 MICROMETERS
 - BAND 2: 0.6 TO 0.7 MICROMETERS
 - BAND 3: 0.7 TO 0.8 MICROMETERS
 - BAND 4: 0.8 TO 1.1 MICROMETERS
- INSTANTANEOUS FIELD OF VIEW: 83 METERS

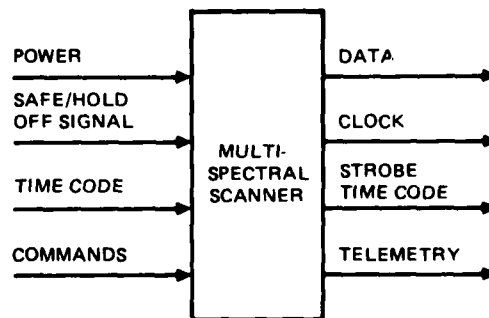


Figure 8. Hughes MSS (aboard LANDSAT-1, -2, -3).

3.1.3 ADVANCED VERY HIGH RESOLUTION RADIOMETER (AVHRR)

The AVHRR is an IR sensing instrument aboard TIROS-N that is used remotely to determine surface temperature. A scanning radiometer, its characteristics are listed in Table 12.

The detectors for each of the five spectral channels are squares, 0.254 cm on a side. The instantaneous field of view (IFOV) which they see 1.3×1.3 mrad corresponds to a ground resolution of 1.1 km at nadir. Channels 3 and 5 are used to provide both day and night sea-surface temperatures. Video image data are transmitted at 120 lines per minute using outputs from the AVHRR.

The AVHRR optical system consists of an 8-inch aperture telescope combined with a diffraction grating to generate the five spectral bands. A scanning mirror rotates at 360 rpm to produce a cross-track scan.

Characteristics	Channels				
	1	2	3	4	5
Spectral range (micrometers)	0.58 to 0.68	0.725 to 1.0	10.3 to 11.3	3.55 to 3.93	11.5 to 12.5
Detector	Silicon	Silicon	(HgCd) Te	InSb	(HgCd) Te
Resolution (km)	1.1	1.1	1.1	1.1	1.1
Instantaneous field of view (IFOV) (milliradians)	1.3 sq.	1.3 sq.	1.3 sq.	1.3 sq.	1.3 sq.
Signal-to-noise ratio @ 0.5 albedo	> 3:1	> 3:1	-	-	-
Noise-equivalent temperature difference @ 300°K	-	-	0.12 @ 300°K	0.12 @ 300°K	0.12 @ 300°K
Modulation transfer function (one IFOV/single bar)	0.30	0.30	0.30	0.30	0.30

Optics - 8-inch diameter afocal Cassegrainian telescope

Scanner - 360-rpm hysteresis synchronous motor with beryllium scan mirror

Cooler - Two-stage radiant cooler, infrared detectors controlled at 105° or 107°K

Data output - 10-bit binary, simultaneous sampling at 40-kHz rate

Table 12. AVHRR characteristics.

3.1.4 VISIBLE AND IR SPIN SCAN RADIOMETER AND ATMOSPHERIC SOUNDER (VAS)

VAS operates aboard GOES-4 as a visible and IR scan radiometer. The scanning process is produced by the rotation of the GOES-4 spacecraft. The operation of VAS is depicted in Figure 9.

Visible spectral data (0.55 - 0.75 μm) are detected using an array of eight photomultiplier tubes; each tube views an eighth of the scan width.

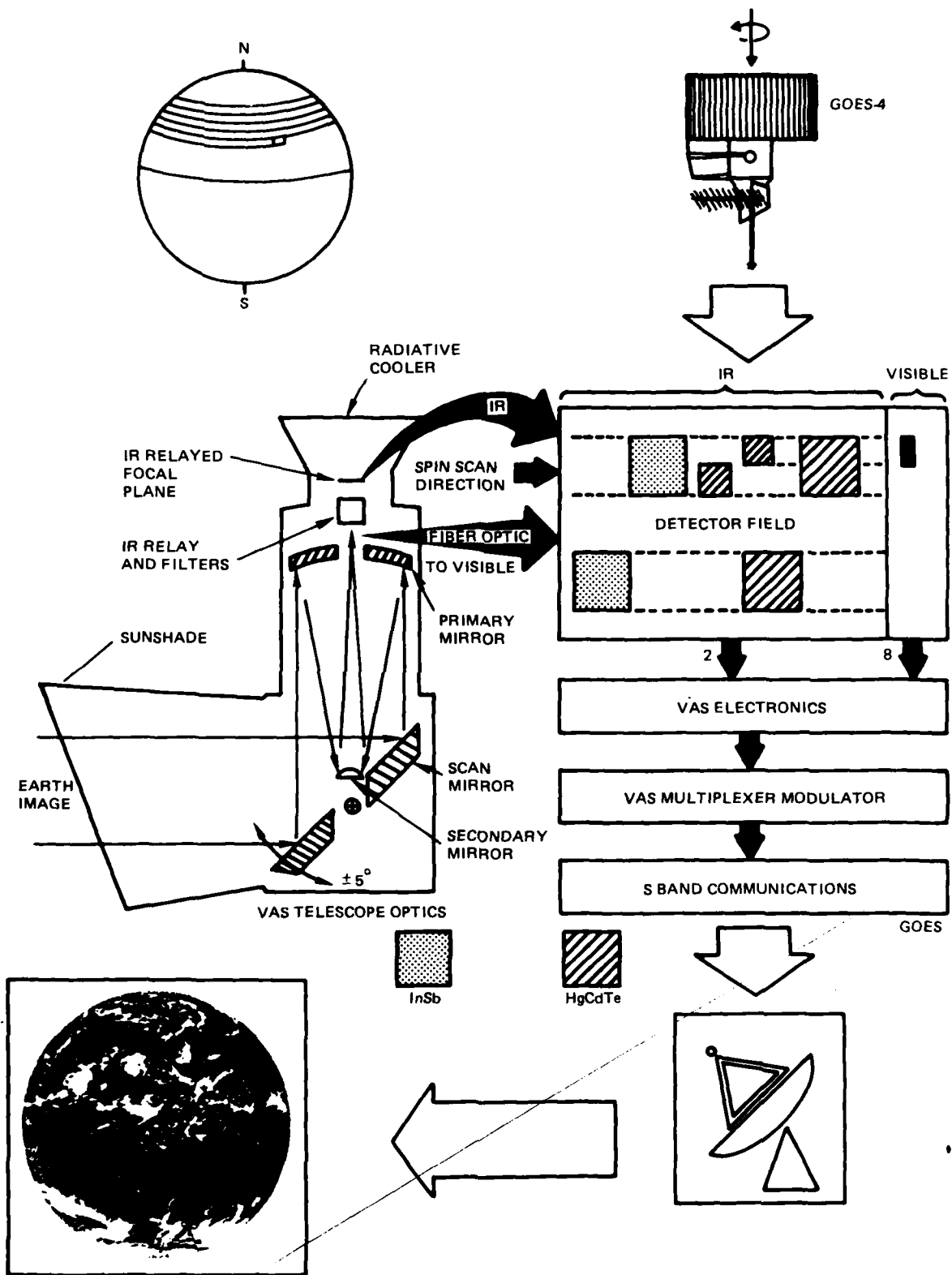


Figure 9. VAS system.

The IR spectrum (from narrow band filters) is collected in 12 bands, as listed in Table 13.

The VAS optical system utilizes a Ritchey-Chretien type telescope (similar to Cassegrain optics, except for surface contours which produce a larger field of view at the focal plane). Two focal planes are used in VAS. Visible spectrum signals are obtained at the principal focus. An optical fiber for each of the eight instantaneous fields of view defines the field to be imaged ($24 \times 25 \mu\text{rad}$) and conducts the corresponding light images to each of the eight photomultiplier tubes. The IR field of view is $192 \mu\text{rad}$.

The spatial resolution at the earth's surface in the visible channel is approximately 1 km. The resolution in the IR channels is 8 km. Detailed characteristics of VAS are summarized in Table 14.

3.1.5 THERMAL MAPPER (TM)

The TM is a multispectral scanning radiometer covering spectral bands in the visible and IR. It is scheduled to be flown aboard LANDSAT D or D' to perform an "earth resources" mapping function. An engineering model, tested in the laboratory, uses a rotating mirror for scanning. Figure 10 depicts the operation of the system.

Figure 11 summarizes the characteristics of TM; while Figure 12 is a cross-sectional view of TM. The significant TM parameters are summarized in Table 15.

TM has two focal planes on which ground images are focused. The prime focal plane assembly has 16 detectors in four spectral bands and the secondary focal plane (which is cooled) has three bands with 20 detectors. The optical configuration is depicted in Figure 13. Spectral responses of the seven spectral bands are listed in Table 16.

Spectral Band	Atmospheric Pressure, mb	$\lambda, \mu\text{m}$	$\Delta\nu, \text{cm}^{-1}$	Remarks		S/N Improvement Requirements		
				Band	Detector Type	NEN/IGFOV*	Sounding NEN*	Spin Budget
1	65	14.73	10	CO ₂	HgCdTe	10.390	0.25	6
2	100	14.48	16	CO ₂	HgCdTe	3.490	0.25	14
3	325	14.25	16	CO ₂	HgCdTe	3.000	0.25	11
4	450	14.01	20	CO ₂	HgCdTe	2.200	0.25	7
5	Surface	13.33	20	CO ₂	HgCdTe	2.080	0.25	7
6	700	4.525	45	CO ₂	InSb	0.063	0.004	35
7	Surface	12.66	20	H ₂ O	HgCdTe	1.930	0.25	7
8	Surface	11.17	140	Window	HgCdTe	0.296	0.25	1
9	375	7.261	40	H ₂ O	HgCdTe	1.770	0.15	16
10	330	6.725	150	H ₂ O	HgCdTe	0.482	0.10	3
11	280	4.444	40	CO ₂	InSb	0.073	0.004	46
12	Surface	3.945	140	Window	InSb	0.022	0.004	4

*Ergs/cm²-sec-sr-cm¹

Table 13. VAS IR spectral bands.

Size	
Length	~ 1.5 m
Radial dimension	~ 0.65 m
Weight	
Scanner	64.3 kg
Electronics module	10.5 kg
Structural material	Beryllium (structure and mirrors)
Optics	Ritchey-Chretien system 40.64 cm dia primary mirror Focal length 292.1 cm Optically flat scan mirror
Detectors	
Visible spectrum	8 photomultiplier tubes coupled to focal plane by optical fibers <i>which define IGFOV: $21 \times 25 \mu\text{rad}$</i>
Infrared spectrum	Solid state detectors cooled to 95°K 2 HgCdTe; IGFOV: $192 \mu\text{rad}$ 2 HgCdTe; IGFOV: $384 \mu\text{rad}$ 2 InSb; IGFOV: $384 \mu\text{rad}$
Spectral bands	By filters inserted in IR optical path; 12 filters selectable from rotating wheel
Radiative cooler	Servoed operating temperature $\sim 95^\circ\text{K}$ Heat rejection capacity $\sim 16 \text{ mw}$ Minimum temperature $\sim 82^\circ\text{K}$
In-orbit calibration	Radiometric IR: Temperature monitored blackbody, cyclically reflected into optical axis Visible: Optical aperture providing sun signal of 50% earth albedo Electronic IR and Visible: Stairstep voltage into amplifier chain
Onboard programmer	Reprogrammable by command link Selects and controls scan sector size and center position Controls filter wheel and selects transmitting detector pair

Table 14. VAS characteristics.

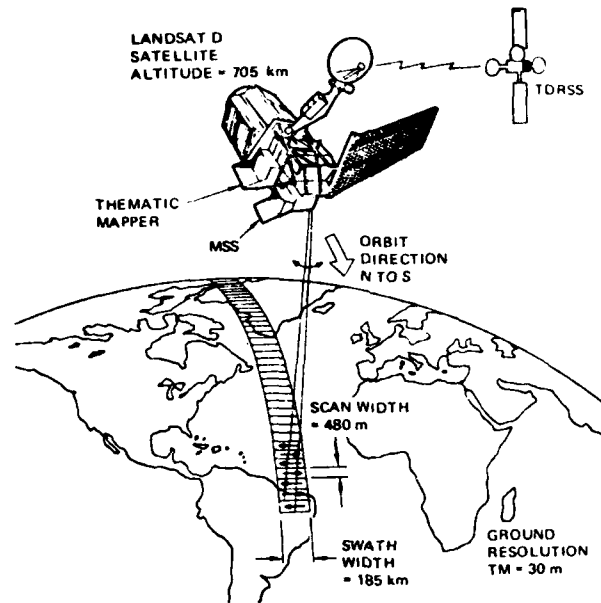


Figure 10. TM operations on LANDSAT D.

- WEIGHT: 570 POUNDS
- SIZE 76 IN X 43 IN X 28 IN
- POWER: 300 WATTS OPERATING
75 WATTS STANDBY
- DATA RATE: 34.0 MBPS AND INCLUDES
 - VIDEO DATA
 - TIME CODE
 - FLIGHT SEGMENT TELEMETRY
- SPECTRAL BANDS:
 - BAND 1: 0.45 - 0.52 MICROMETERS
 - BAND 2: 0.52 - 0.60 MICROMETERS
 - BAND 3: 0.63 - 0.69 MICROMETERS
 - BAND 4: 0.76 - 0.90 MICROMETERS
 - BAND 5: 1.55 - 1.75 MICROMETERS
 - BAND 6: 10.4 - 12.5 MICROMETERS
 - BAND 7: 2.08 - 2.35 MICROMETERS
- INSTANTANEOUS FIELD OF VIEW:
 - BAND 6 120 METERS
 - BANDS 1-5, 7 30 METERS

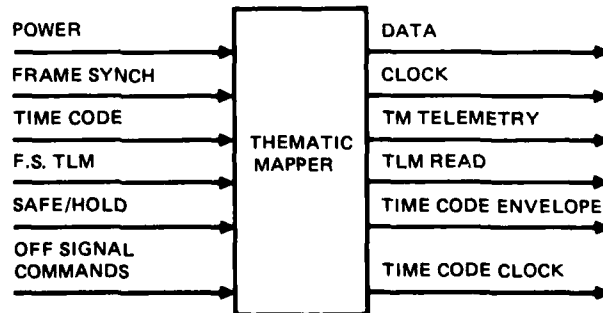
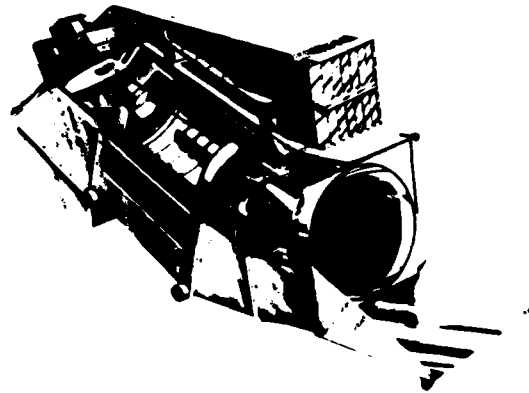


Figure 11. TM characteristics.

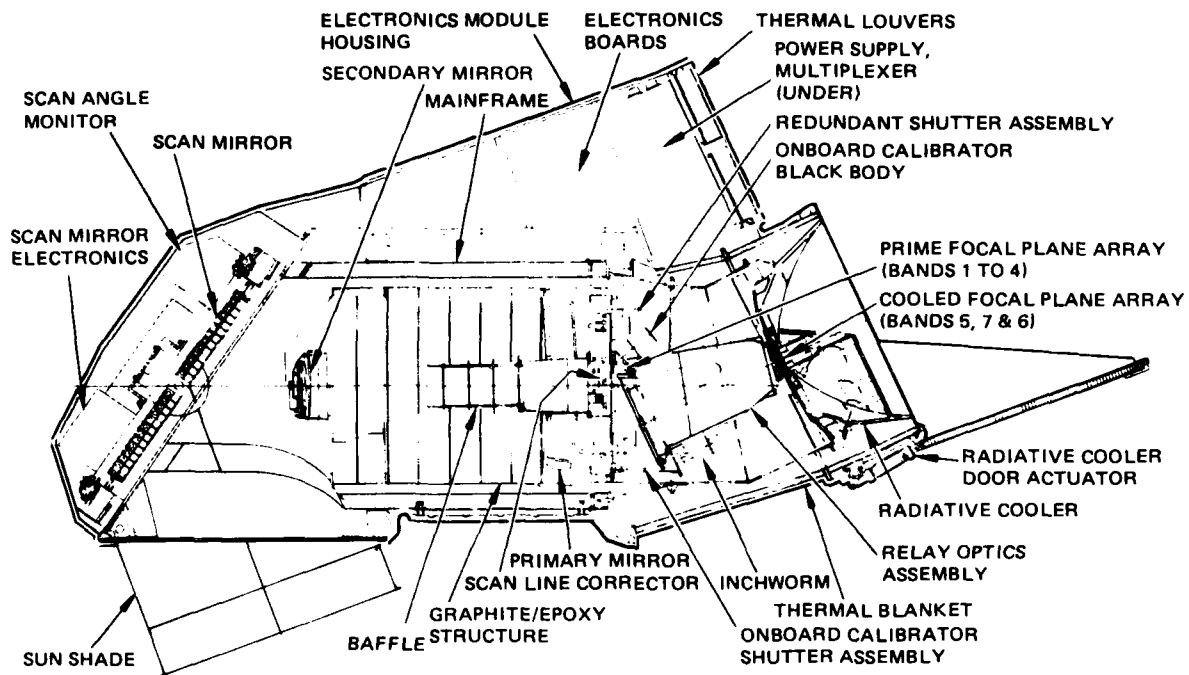


Figure 12. Cross-sectional view of TM.

LANDSAT Orbit	Near Polar, sun synchronous 705 km altitude 99 minute period 98.2° inclination angle 16-day repeat cycle
Scan	185 km swath 7 Hz rate
Optics	40.6 cm telescope aperture $f/6$ at prime focus 42.5 μrad IFOV, bands 1-4 $f/3$ at secondary focus (cooled) 43.8 μrad IFOV, bands 5, 7 170 μrad IFOV, band 6
Signal	8 bits/sample 52 kHz sampling rate, bands 1-5, 7 13 kHz sampling rate, band 6 1 sample/IFOV 85 Mbps multiplexed output

Table 15. Significant TM parameters.

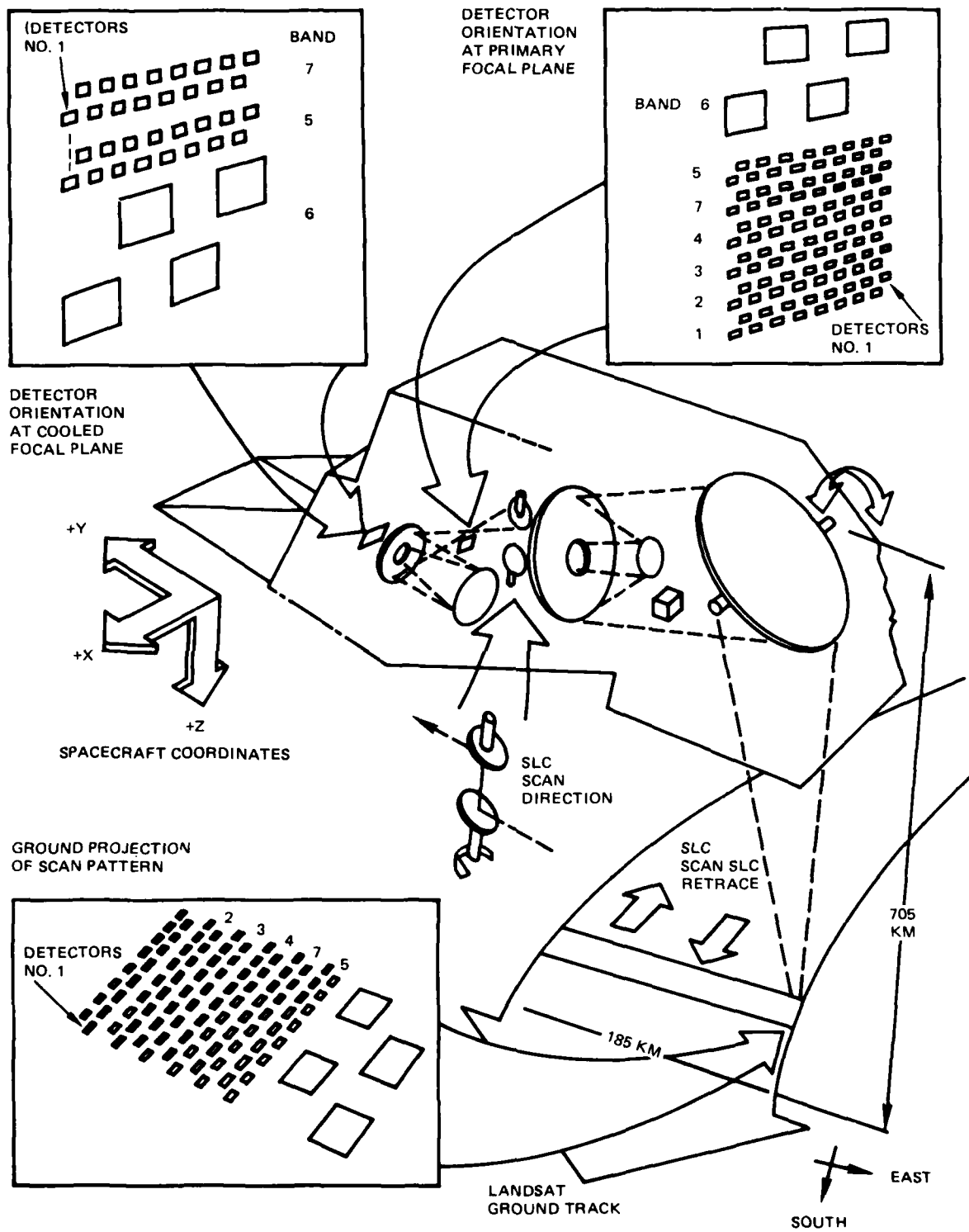


Figure 13. TM detector arrays.

Band	50% Response	
	Lower Band Edge	Upper Band Edge
1	0.452 μm	0.518 μm
2	0.526	0.609
3	0.624	0.693
4	0.776	0.906
5	1.568	1.784
6	10.420	11.610
7	2.017	2.347

Table 16. Measured spectral response.

Table 17 summarizes the characteristics of the cooled focal plane assembly.

The cooled focal plane contains InSb detectors for bands 5 and 7. An (Hg Cd) Te type detector is used for band 6. Table 18 summarizes information on the detectors contained in the prime focal plane assembly.

The intended use of the various TM spectral pass bands is summarized in Table 19.

Number of bands	3
Number of detectors	
Bands 5,7 (monolithic InSb)	16/Band
Band 6 (photoconductive HgCdTe)	4
Detector size	
Bands 5, 7	0.0021 in. sq. (0.00533 cm sq)
Band 6	0.00816 in. sq. (0.0207 cm sq)
IFOV size	
Bands 5, 7	43.75 μrad
Band 6	170.0 μrad
Center-to-center spacing in each row	
Bands 5, 7	0.00408 in. (0.01036 cm) (2 IFOV)
Band 6	0.01632 in. (0.04145 cm) (2 IFOV)
Center-to-center spacing between rows	
Bands 5, 7	0.00510 in. (0.01295 cm) (2.5 IFOV)
Band 6	0.02040 in. (0.0518 cm) (2.5 IFOV)
Operating temperatures	90°K, 95°K, 105°K

Table 17. Cooled focal plane assembly.

Number of bands	4, Band Nos. 1-4
Number of detectors (monolithic silicon)	16/Band
Detector size	0.00408 in. sq. (0.01036 cm sq)
IFOV size	42.5 μ rad
Band-to-band spacing	0.102 in. (0.259 cm) (25 IFOV)
Center-to-center spacing in each row	0.00816 in. (0.0207 cm) (2 IFOV)
Center-to-center spacing between rows	0.01020 in. (0.0259 cm) (2.5 IFOV)
Operating temperature	10° or 25°C

Table 18. Prime focal plane assembly.

Band	Range (μ m)	Radiometric Resolution	Principal Applications
1	0.45-0.52	0.8 NE ρ	Coastal water mapping Soil/vegetation differentiation Deciduous/coniferous differentiation
2	0.52-0.60	0.5% NE ρ	Green reflectance by healthy vegetation
3	0.63-0.69	0.5% NE ρ	Chlorophyll absorption for plant species differentiation
4	0.76-0.90	0.5% NE ρ	Biomass surveys water body delineation
5	1.55-1.75	1.0% NE ρ	Vegetation moisture measurement Snow/cloud differentiation
6	10.4-12.5	0.5K NETD	Plant heat stress management Other thermal mapping
7	2.08-2.35	2.4% NE ρ	Hydrothermal mapping

Table 19. Spectral passbands and utilization.

3.1.6 SHUTTLE MULTISPECTRAL IR REFLECTANCE RADIOMETER (SMIRR)

SMIRR is a multispectral IR reflectance radiometer, designed for use aboard the "space shuttle." This is not a scanning (mapping) instrument, although it represents a precursor for instruments of that type. Engineering laboratory and aircraft flight tests have been carried out with SMIRR at the Jet Propulsion Laboratory (JPL) by J. F. Wellman and A. F. H. Goetz. Figure 14 depicts SMIRR, a multichannel visual/IR radiometer, equipped with bore-sighted film cameras.

It provides visual and IR measurements of the ground track radiance in 10 selected bands. The specific bands were selected for the detection and identification of surface mineralogic types. Table 20 lists the spectral bands.

Figure 15 shows the imaging spectrometer.

SMIRR consists of a 1.37 m focal length Cassegrain telescope, followed by a rotating filter, chopper wheel and a thermoelectrically cooled detector. An (Hg Cd) Te photoconductor, with a $3.5 \mu\text{m}$ cut-off is used for all spectral channels.

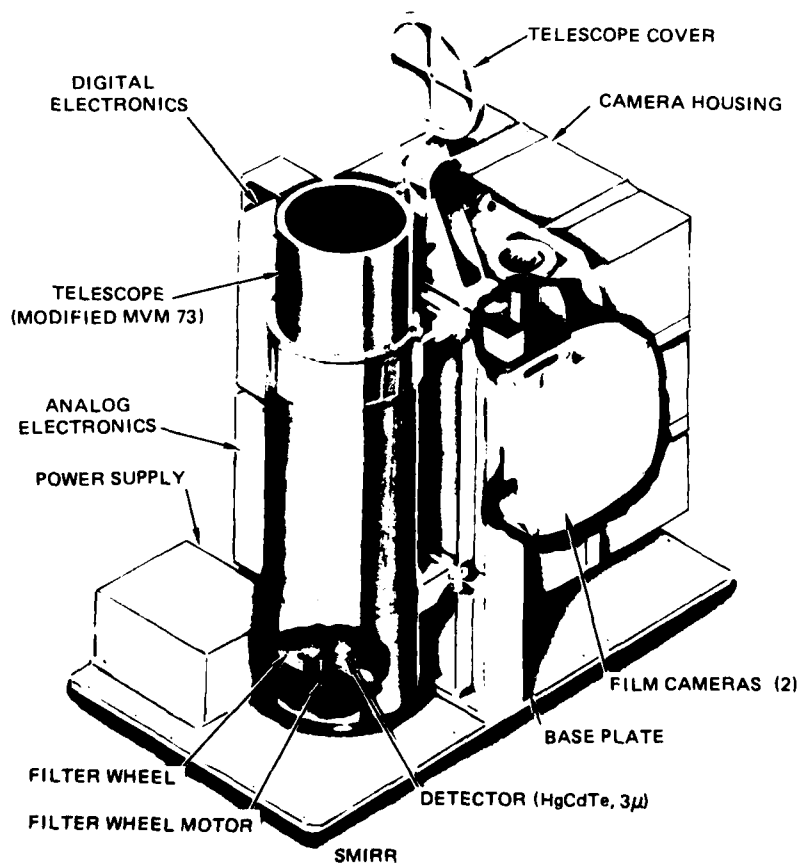


Figure 14. Shuttle multispectral infrared reflectance radiometer (SMIRR).

Channel	Center, μm	Half Power Bandwidth, μm
1	0.5 \pm .02	0.1
2	0.6 \pm .02	0.1
3	1.05 \pm .02	0.1
4	1.2 \pm .02	0.1
5	1.6 \pm .02	0.1
6	2.1 \pm .02	0.1
7	2.17 \pm .005	0.02
8	2.20 \pm .005	0.02
9	2.22 \pm .005	0.02
10	2.35 \pm .015	0.06

Table 20. Spectral bands for the SMIRR.

The imaging foreoptics are in an $f/3$ inverted Schwartzchild configuration with a folding flat to bring the image onto a source slit. Energy leaving the source slit passes through an aperture in the grating and is collimated by an $f/3$ paraboloid. The energy is then dispersed by the grating and reimaged by another $f/3$ paraboloid onto a 32×32 element area array detector contained in a demountable dewar. The grating is mounted on a set of swing arms (not shown) which permit it to be positioned at each of four angles with respect to the collimated beam, thereby selecting the subset of the full spectral range to be dispersed across the detector array. By stepping the mirror through a sequence of four steps per object line time, a total of 128 spectral lines is acquired with 32 spatial resolution elements per line. A spectral resolution of $0.01 \mu\text{m}$ is achieved.

The instrument electronics sample both signal and dark reference sections of the filter wheel. The dark reference values (associated with internal noise) are subtracted out, yielding corrected signal level values. Two 16 mm single-frame cameras, boresighted on the radiometer FOV, alternately acquire black and white images of the ground track for geographic reference.

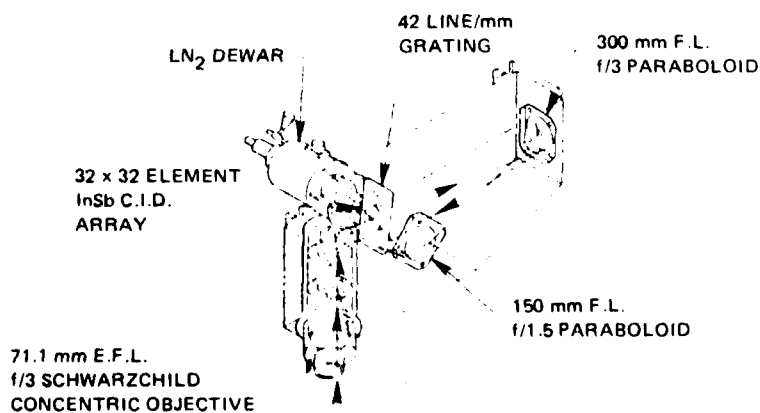


Figure 15. SMIRR spectrometer.

3.1.7 MULTISPECTRAL LINEAR ARRAY (MLA)

The MLA is envisioned as a follow-on multispectral scanning sensor to the TM in the LANDSAT series. It would operate in the so-called "pushbroom" scanning mode and thus provide much greater imaging times when viewing a given ground terrain pixel (picture element). This greater integration time (by a factor of 100 to 1000) results in a much improved S/N-ratio in the processed output. Figure 16 illustrates the geometry involved in the pushbroom scan technique. The detector array is composed of a set of independent detecting elements, aligned at right angles to the spacecraft projected upon the earth's surface.

The utilization of the pushbroom scan technique, in a multispectral array imager for an as yet undefined follow-on to LANDSAT D', is presently in the very early concept formulation stage. The development of a "flyable" prototype version of the device is a long way "down the road," (possibly by 1990).

Preliminary concepts of multispectral, pushbroom scanning devices have been presented by A. A. Stark ("Multispectral Pushbroom Imager," AIAA Sensor Systems for the 80's, pp. 109-112, conference held at Colorado Springs, Co., 2-4 Dec. 1980) and by J. B. Wellman and F.H. Goetz ("Experiments in IR Spectral Mapping of Earth Resources," AIAA Sensor Systems for the 80's, pp. 163-174).

The simplified pushbroom scan detecting array illustrated in Figure 16 does not provide for spectral monitoring. Spectral monitoring could be achieved using a two dimensional detector array complex, in conjunction with a spectrum grating. Figure 17 depicts the concept.

The "swath direction" in Figure 17 is oriented at right angles to the satellite's track on the earth's surface. The spectral analysis is done with independent detector elements at right angles to the "swath" coordinate. The spectral analysis coordinate direction in the figure is designated (Red ← Wavelength → Blue).

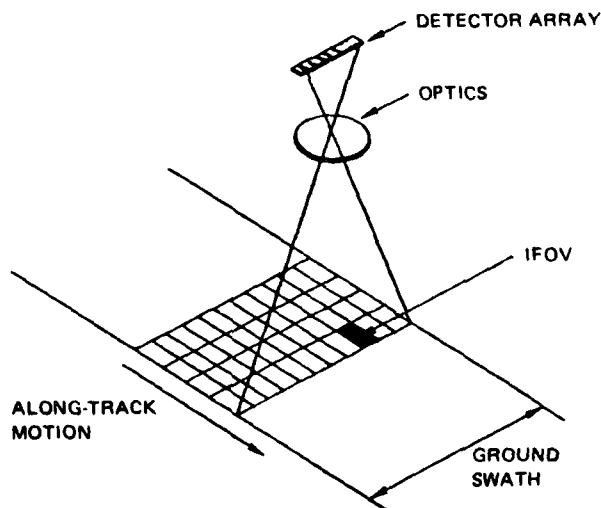


Figure 16. "Pushbroom" scan geometry.

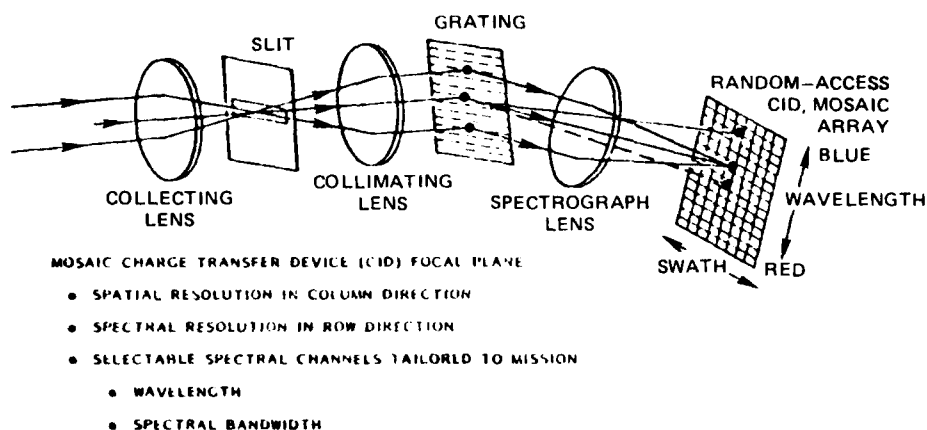


Figure 17. MLA sensor concept.

The outputs of the individual detector elements are read using a CID (Charge Injection Device) technique. The use of CID or CCD (Charged Coupled Device) image forming techniques is currently limited for the most part to MOS (Metal Oxide Silicon) structures. These photodiode arrays have a spectral energy gap cut-off in the neighborhood of $1.1 \mu\text{m}$.

3.2 MICROWAVE SENSORS

Three microwave sensor devices will be discussed: (1) synthetic aperture radar (SAR), (2) microwave scatterometer (MS) and (3) scanning multichannel microwave radiometer (SMMR). The first two are active radar devices and the third is a passive microwave radiometer.

3.2.1 SYNTHETIC APERTURE RADAR (SAR)

SAR, in the form of an L-band radar, was operated aboard SEASAT-A during the latter part of 1978. SEASAT-A was the first dedicated experimental oceanographic satellite whose primary goal was to provide information on middle and large scale oceanic and atmospheric processes, e.g., ocean circulation, wind and wave patterns, etc.

The processing of coherent SAR returns greatly increases the achievable spatial resolution (with a given antenna beamwidth) in the direction parallel to the satellite motion. Good resolution in the direction at right angles to the satellite track can be achieved using standard pulse compression waveforms. SAR aboard SEASAT-A achieved spatial resolutions in both directions of approximately 25 m.

SEASAT-A operated in a near polar orbit at an altitude of 800 km. The SAR radar traced out a swath width of approximately 100 km. The operating frequency was centered in the neighborhood of 1.28 GHz. The average power was 55 watts. The antenna dish had an area of 25 m^2 . A small portion of the recorded radar returns were digitally processed at JPL. SAR images can be processed using digital, optical correlators or CCD transverse filters. None of these techniques is easy to implement on a real-time basis. (See Radar Data Processing and Exploitation Facility by D.A. Ausherman et al in the proceedings of the IEEE 1977 International Radar Conference, Pub 75 CHO 938-1, AES, pp. 493-498.)

It is interesting to note that when LANDSAT-3 MSS images were combined with corresponding SEASAT-A/SAR digital data, the information content of the land cover maps was increased by 25 percent (Aviation Week and Space Technology, 29 September 1980, p. 65). The SAR data significantly increased the spatial resolution.

3.2.2 MICROWAVE SCATTEROMETER (MS)

An MS was operated aboard SEASAT-A to measure ocean surface wind speed and direction. The MS was a short pulse (4.8 ms) operating at 14.6 GHz. The radar return characteristics (Doppler shift) are a function of the surface wave motion (which in turn depends on the local wind speed and direction).

Figure 18 is a block diagram of the MS.

3.2.3 SCANNING MULTICHANNEL MICROWAVE RADIOMETER (SMMR)

SMMR devices were flown aboard NIMBUS-7 and SEASAT-A. SMMR senses the microwave thermal emission from the earth's surface and atmosphere and provides sea surface temperature and ocean surface wind speed data. It is pictured in Figure 19.

Figure 20 depicts the SMMR instrument configuration.

The SMMR instrument package consists of a radio frequency assembly, an electronics assembly, a power supply assembly and an antenna/scan mechanism assembly. The antenna/scan mechanism is mounted on the top of the spacecraft sensory ring. The remaining sub-assemblies are located in various bay sections within the sensory ring. The antenna, an offset parabolic reflector, points downward at an angle of 0.73 radian from nadir and scans ± 0.44 radian ($\pm 25^\circ$) about the vertical nadir.

The MS achieved a spatial resolution of 50 km.

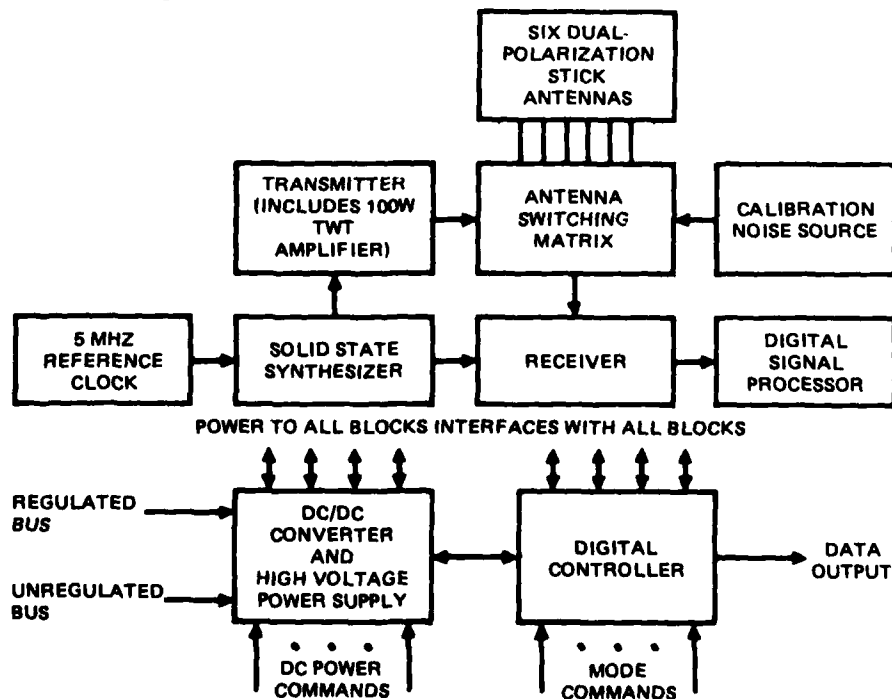


Figure 18. MS functional block diagram.

OFFSET REFLECTOR

MULTI-FREQUENCY FEED HORN (5 FREQUENCIES)

SKY HORN CLUSTER (3 CORRUGATED FEEDS)

ANTENNA SCAN MECHANISM

ELECTRONICS MODULE

POWER SUPPLY MODULE

RF MODULE

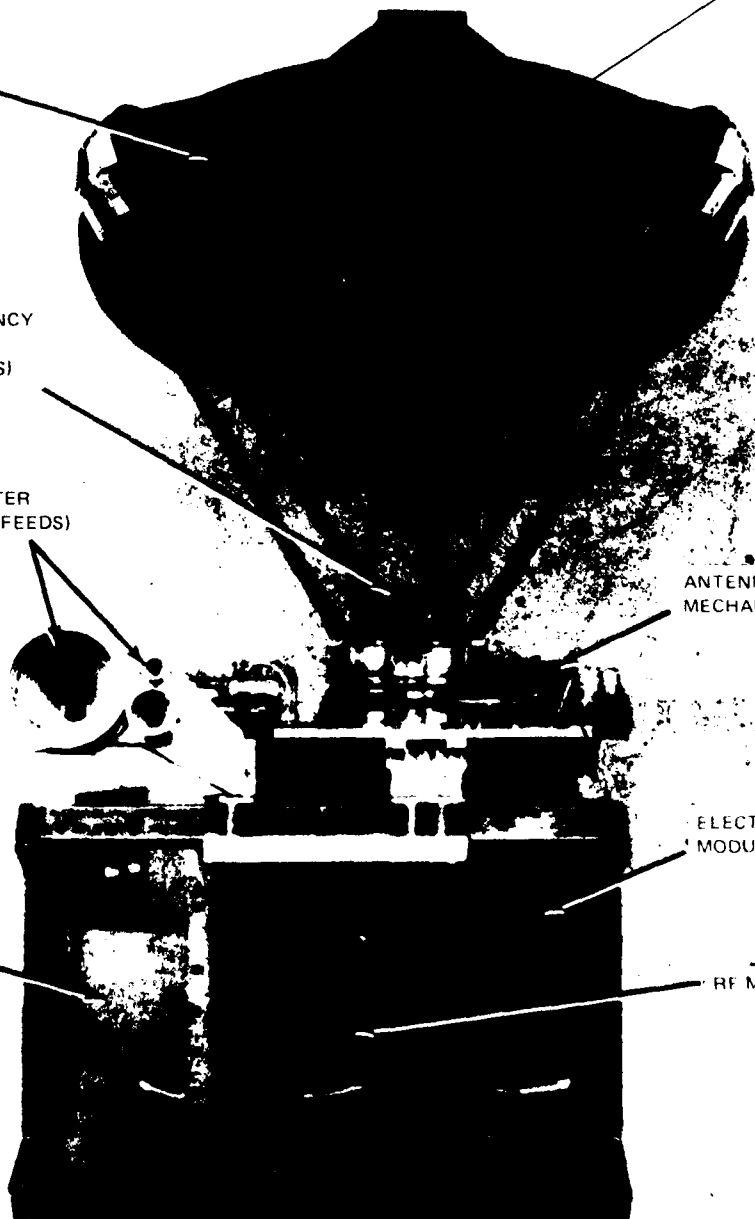


Figure 19. Scanning multichannel microwave radiometer (SMMR)

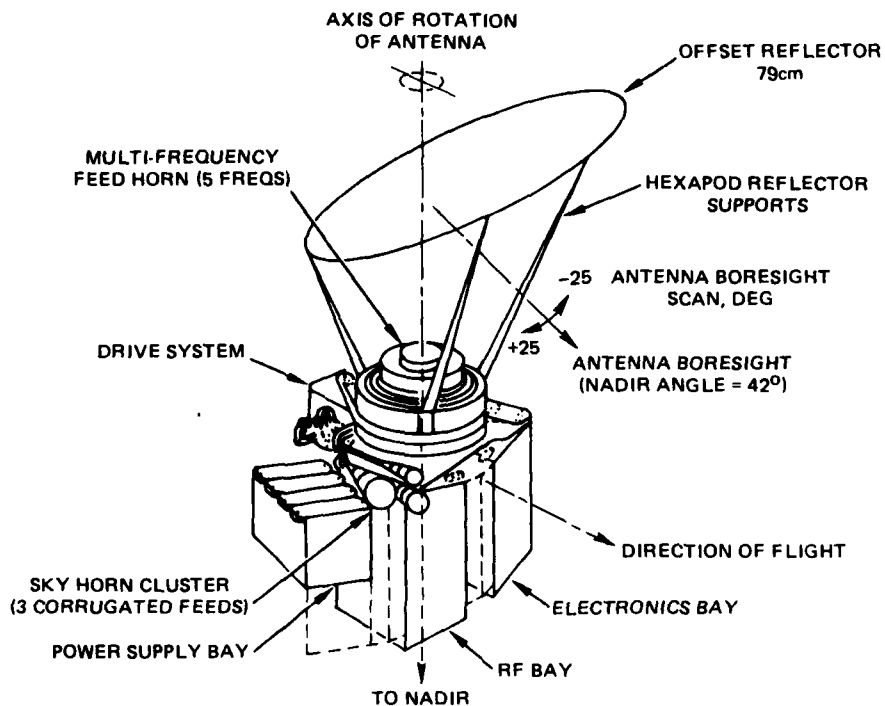


Figure 20. SMMR instrument configuration.

SMMR measures microwave thermal emissions from the earth's surface in five channels. Each channel monitors in two orthogonal linear polarizations.

Table 21 summarizes the SMMR performance parameters.

SMMR data from NIMBUS-7 and SEASAT-A indicate an agreement with "ground-truth" data for ocean surface temperatures of about 1° or 2°C. The actual measured "microwave brightness" is a function of the sea surface temperature, wind speed and salinity. The spatial resolution with SMMR is approximately 10 km. The swath width with the NIMBUS-7 spacecraft was approximately 780 km.

The SMMR sensor design characteristics are summarized in Table 22.

Figure 21 is a functional block diagram of MSSR.

Parameters	Channel				
	R1	R2	R3	R4	R5
Wavelength (cm)	4.0	2.8	1.7	1.4	0.8
Frequency (GHz)	6.633	10.69	18.0	21.0	37.0
RF bandwidth (MHz)	250	250	250	250	250
Integration time (msec) (approx)	126	62	62	62	30
IF frequency range (MHz)	10-110	10-110	10-110	10-110	10-110
Dynamic range (°K)	10-330	10-330	10-330	10-330	10-330
Absolute accuracy (°K rms)	<2.0	<2.0	<2.0	<2.0	<2.0
Temperature resolution, ΔT_{rms} (°K)	0.9	0.9	1.2	1.5	1.5
Antenna beamwidth ($\pm 0.1^\circ$)	4.4	2.75	1.65	1.32	0.77
Antenna beam efficiency (%)	87	87	87	87	87
Wavelength (cm)	4.54	2.80	1.66	1.43	0.81
Scan cycle ($\pm 25^\circ$) (seconds)	4.096	4.096	4.096	4.096	4.096
Double sideband noise figure (dB) (max.)	5.0	5.0	5.0	5.0	5.0

Table 21. SMMR performance parameters.

Item	Characteristics
Detectors:	RF diode -- Dicke -- superheterodyne
Size:	Two 15.3 - by 33.0 - by 20.4-cm modules (two NIMBUS bays) One 15.3- by 16.5- by 20.4-cm module (one-half NIMBUS bay) Parabolic section antenna, 80 cm in diameter Multifrequency antenna feed
Weight:	52.3 kg
Power:	60 watts
Commands:	12
Data:	DAPS -- 2 kbs ⁽¹⁾
Telemetry:	Digital B -- 9 ⁽²⁾ Analog -- 19
Clock:	Time code Strobe 1 Hz 10 kHz 1.6 MHz

(1) NIMBUS 7 data processing

(2) Lower data rate in DAPS for collecting digital words

Table 22. SMMR sensor design characteristics.

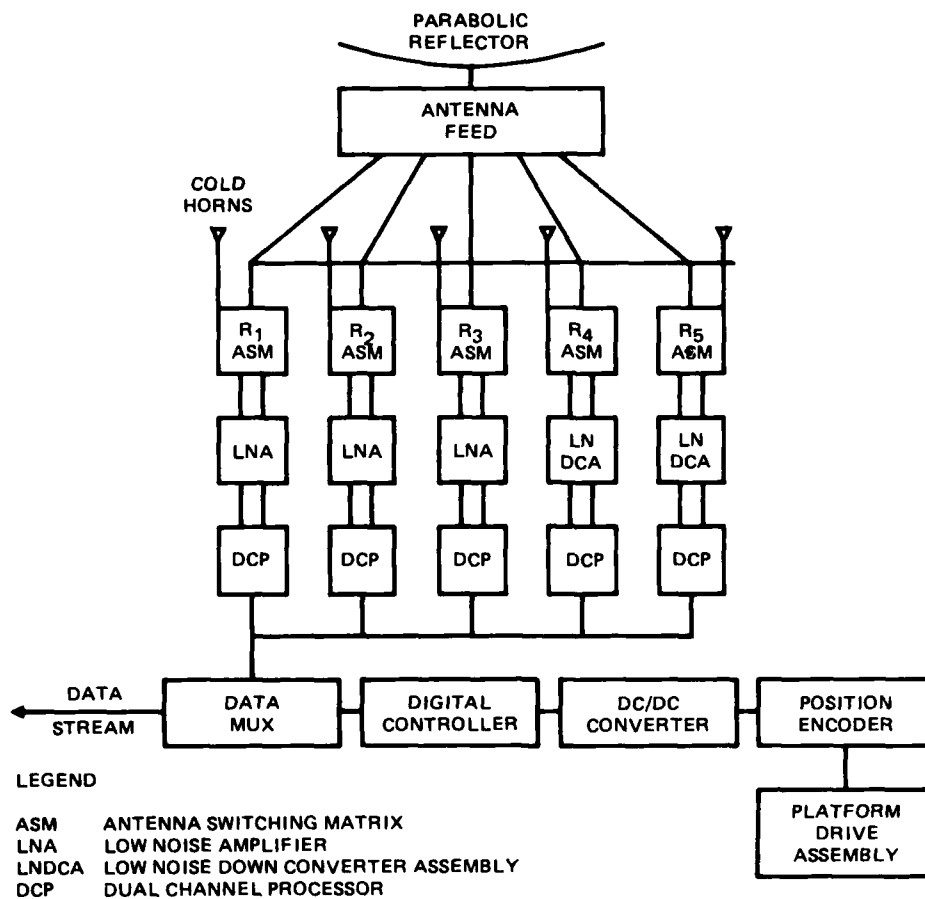


Figure 21. MSSR functional block diagram.

4.0 CONCLUSIONS AND RECOMMENDATIONS

An extensive body of knowledge and operating experience exists within NASA and NOAA concerning the development and utilization of satellite-borne non-DoD imaging sensors for terrestrial observations. It is most likely that some of this civilian technical knowledge and operational experience could be utilized profitably in the planning and development of future military satellite systems. Table 23 lists the initial launch dates of various civilian satellite series of primary interest.

Sensors of primary interest related to the Naval Ocean Surveillance mission are:

- SAR
- MSS
- TM
- MLA
- SMMR

Satellite Type	Initial Launch (Year)
TIROS	1960
ESS (Environmental Survey Satellite)	1960
ITOS/NOAA	1970
LANDSAT	1972
GOES	1974
DMSP	1976
SEASAT	1978

Table 23. Initial launch year for satellite types.

To usefully exploit the summary data and information contained in the present report, it is recommended that a "small-scale" (1 man-year) program be initiated. The recommended program consists of the following three elements:

- (1) In depth review and analysis of literature concerning satellite sensor systems, including military systems
- (2) Visitation and discussion with resident experts at GSFC, LaRC, JPL, APL, NOAA, SIO, EROS, SAMSO, etc., to obtain latest relevant information and examples of sensor products
- (3) Summary report

APPENDIX A
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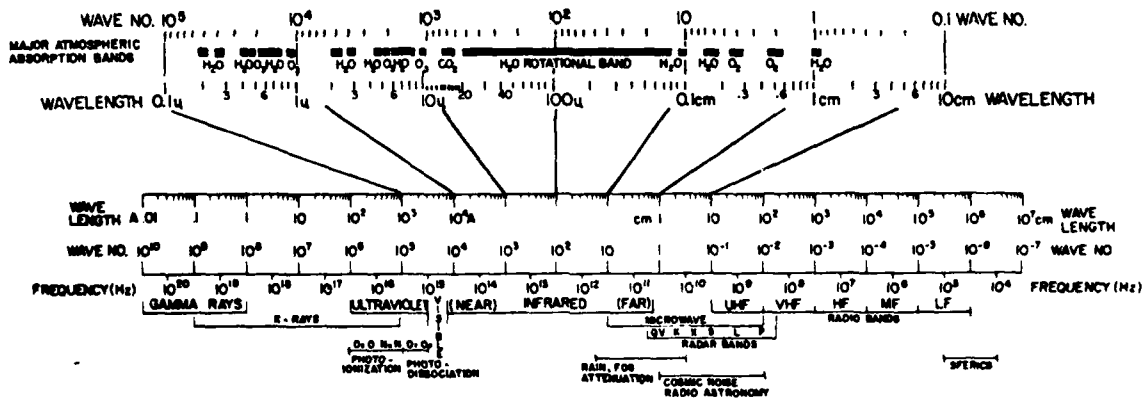
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APPENDIX B
PERSONS AND ORGANIZATIONS
(from whom information was obtained to be utilized in this study)

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APPENDIX C

EM SPECTRUM AND ATMOSPHERIC TRANSMISSION CHARACTERISTICS



APPENDIX D
SEASAT-SAR IMAGES

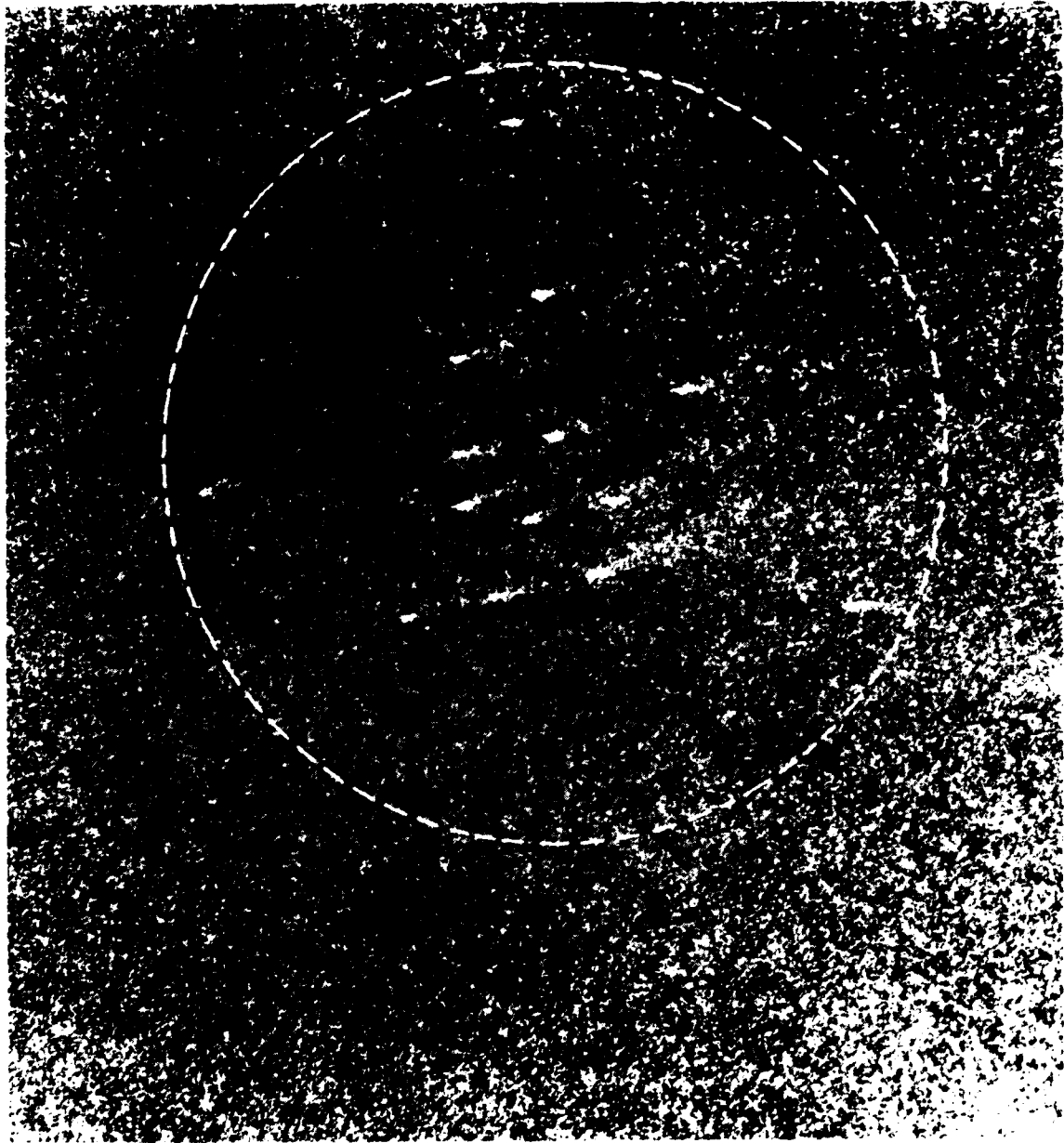


Figure 22. NATO task force in Irish Sea

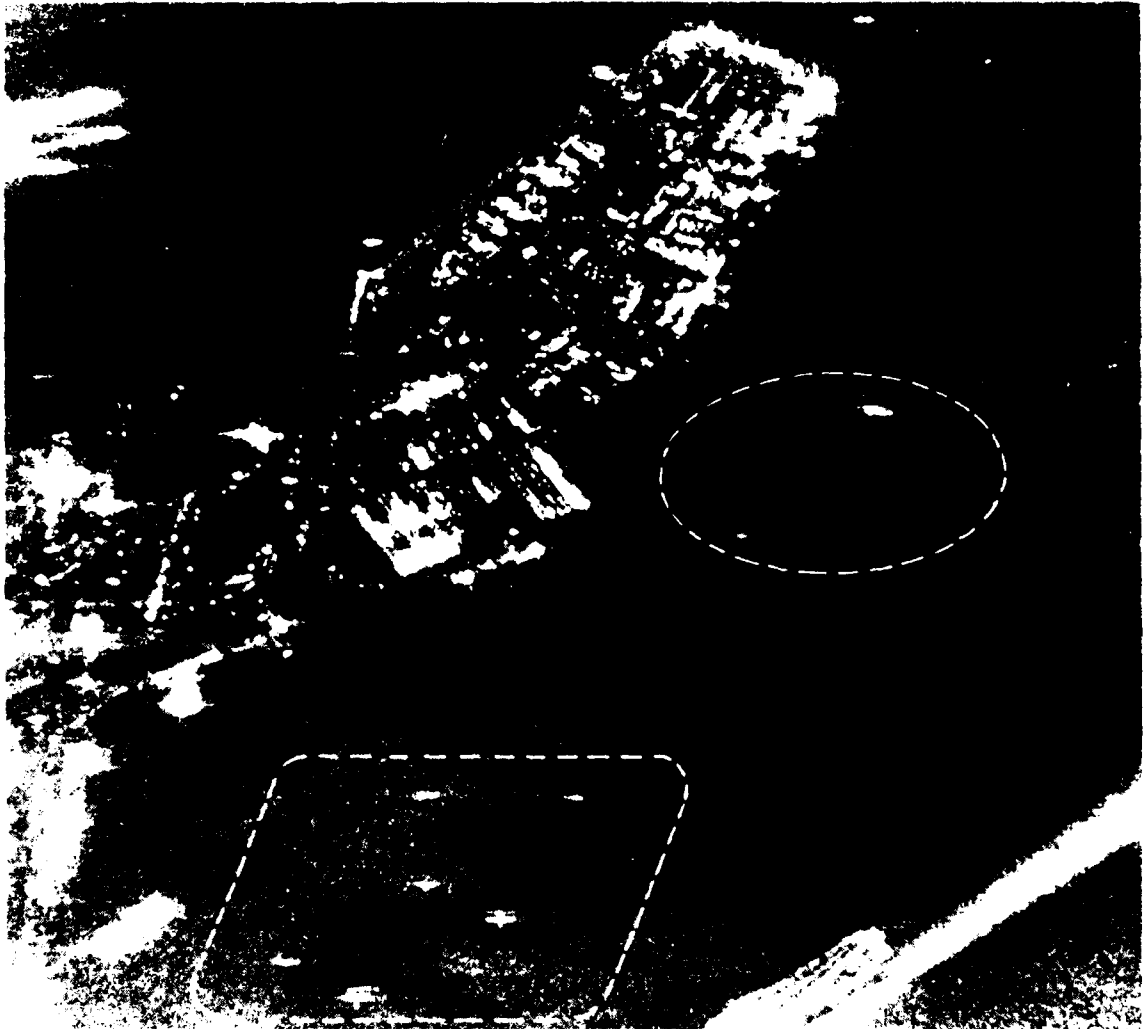


Figure 23 - Ships in San Francisco bay

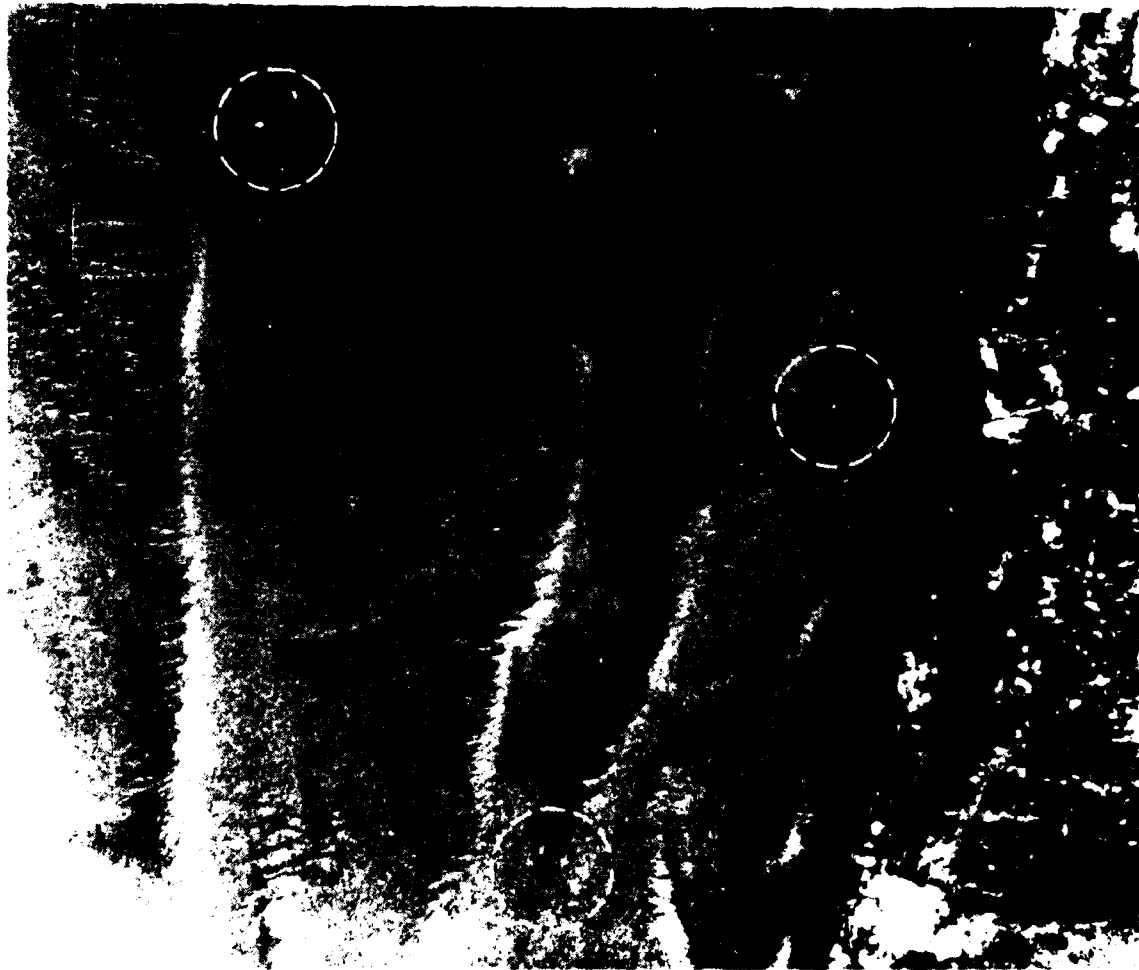


Figure 24. Small craft off French coast in English Channel.

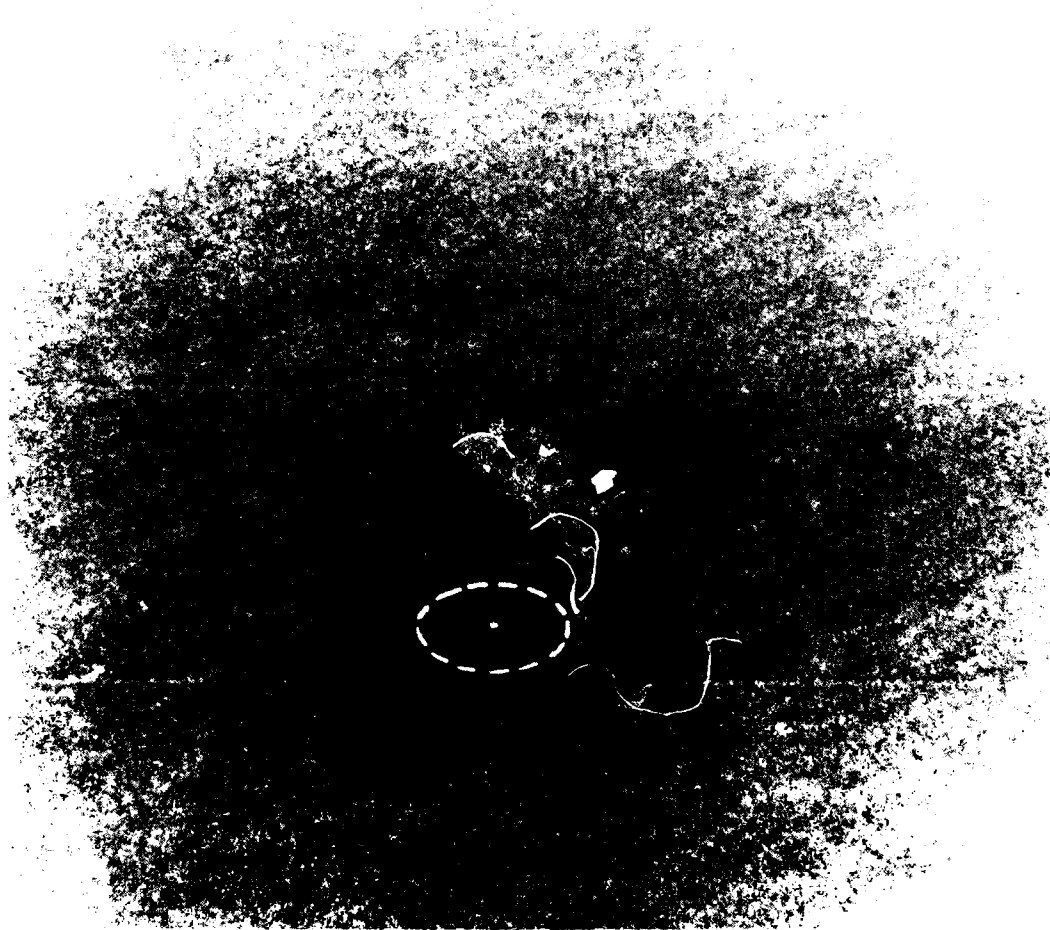


Figure 25. Oceanography vessels in Gulf of Alaska

APPENDIX E
LANDSAT IMAGES IN SHIPPING

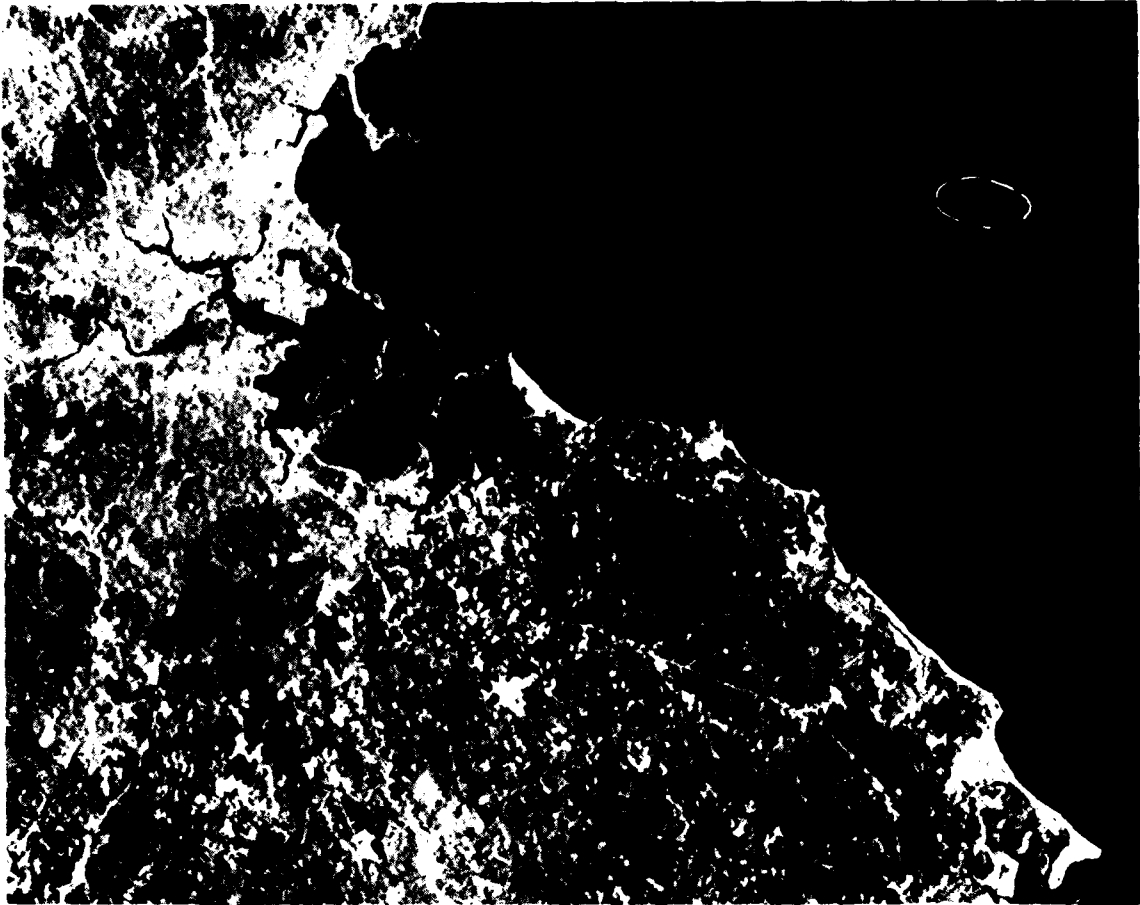


Figure 26. Shipping off of Boston

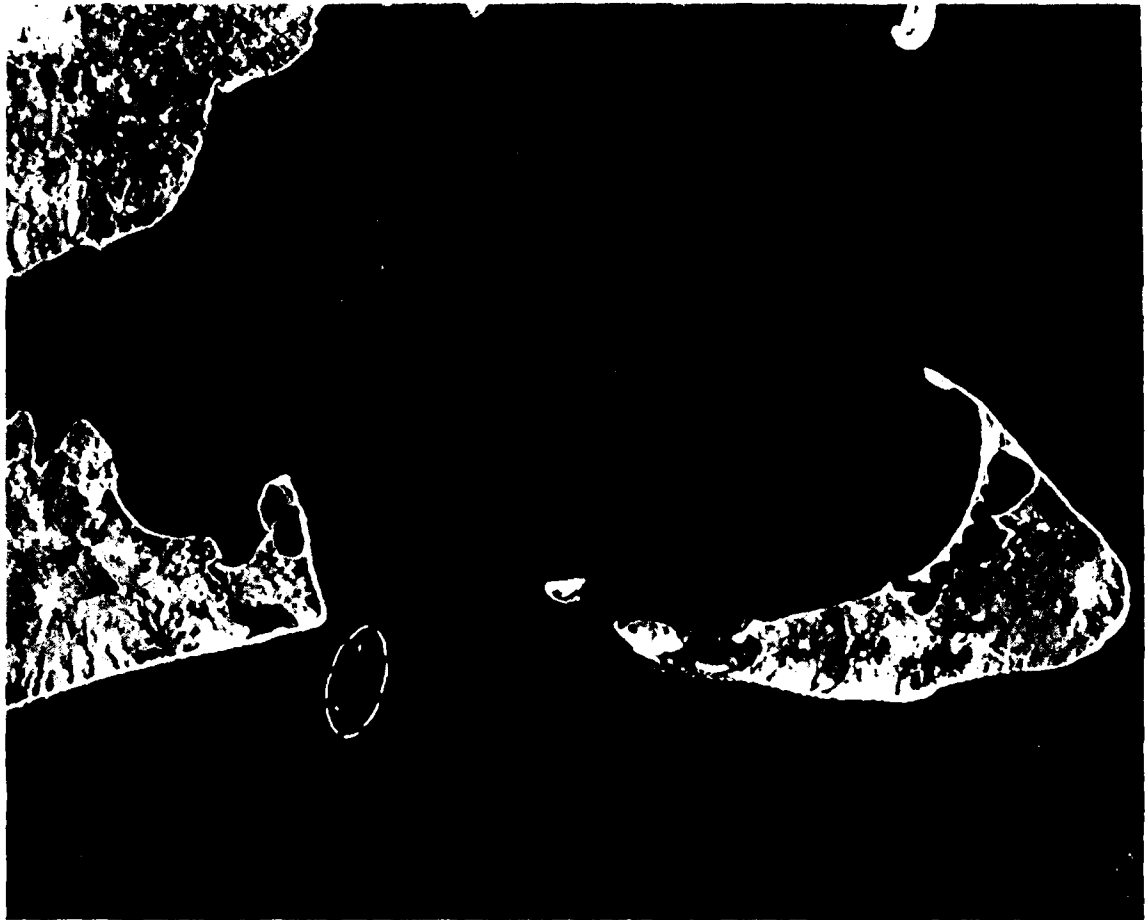




Figure 28. Shipping of 1 of New York City.

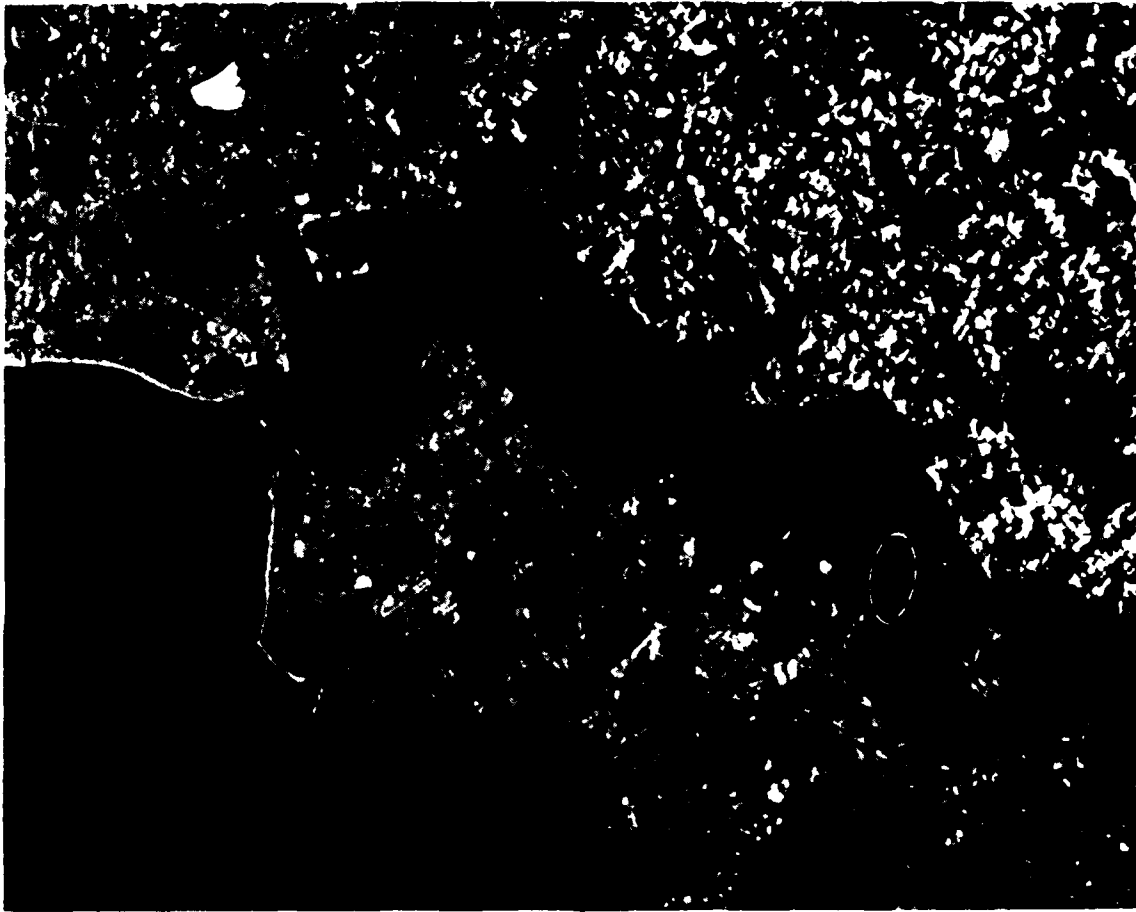


Figure 20. Shipping near Norfolk, Virginia.

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